

## **General Disclaimer**

### **One or more of the Following Statements may affect this Document**

- This document has been reproduced from the best copy furnished by the organizational source. It is being released in the interest of making available as much information as possible.
- This document may contain data, which exceeds the sheet parameters. It was furnished in this condition by the organizational source and is the best copy available.
- This document may contain tone-on-tone or color graphs, charts and/or pictures, which have been reproduced in black and white.
- This document is paginated as submitted by the original source.
- Portions of this document are not fully legible due to the historical nature of some of the material. However, it is the best reproduction available from the original submission.

(NASA-CR-132696) MANUAL FOR IMPROVED SOURCE  
FLCW CHARACTERISTICS PROGRAM (Advanced  
Technology Labs., Inc., Westbury, N.Y.)  
84 p HC \$4.75

N75-29360

CSSL 20D

G3/34

Unclas  
32396

|  |  |  |  |
|--|--|--|--|
|  |  |  |  |
|--|--|--|--|



**Advanced Technology Laboratories inc.**

MAY 1975

ATL TM 183  
MANUAL FOR IMPROVED SOURCE FLOW  
CHARACTERISTICS PROGRAM

By

Paul D. Del Guidice

PREPARED FOR  
NATIONAL AERONAUTICS AND SPACE ADMINISTRATION  
LANGLEY RESEARCH CENTER  
HAMPTON, VIRGINIA 23665

UNDER  
CONTRACT NO. NAS1-13303

BY  
ADVANCED TECHNOLOGY LABORATORIES, INC.  
Merrick and Stewart Avenues  
Westbury, New York 11590

TABLE OF CONTENTS

|             |                                       | <u>Page</u> |
|-------------|---------------------------------------|-------------|
| SECTION I   | INTRODUCTION                          | 1           |
| SECTION II  | DESCRIPTION OF INPUT                  | 2           |
|             | A. Input Format                       | 2           |
|             | B. Figures for Input                  | 9           |
| SECTION III | DESCRIPTION OF OUTPUT                 | 10          |
|             | A. Output Format                      | 10          |
|             | B. Identification of Output Variables | 10          |
| SECTION IV  | SUBROUTINES AND FUNCTIONS             | 12          |
|             | A. Subroutines                        | 12          |
|             | B. Functions                          | 13          |
| SECTION V   | MACHINE CONTROL CONSIDERATIONS        | 15          |
| SECTION VI  | SAMPLE INPUT FOR SOURCE FLOW          | 16          |
| APPENDIX    | PROGRAM LISTING                       | 17          |

TM 183  
SECTION I  
INTRODUCTION

The FORTRAN IV program described herein analyzes the nozzle for a hypersonic scramjet by a two dimensional second order characteristic procedure described in ATL TR 213, "A Source Flow Characteristic Technique for the Analysis of Scramjet Exhaust Flow Fields", Reference (1).

The program starts from the initial profile and marches along down-running characteristics until the final X station is reached. This process can be interrupted by "Change of Origin Profiles" in source flow cases. This is done by interpolating the characteristic data at the required axial station and setting up "F arrays" i.e., XF, YF, ... . Then the program continues on down-running characteristics using the "F arrays" as an initial profile. These "F arrays" are computed for all flows at an X station that coincides with the cowl tip if there is a cowl in the flow field. If the flow is overexpanded at the cowl the program will invert the problem as described in Reference (1). When the shock reflects off the lower wall "F arrays" are again calculated and the computation continues with the problem inverted until the final axial (X) station is attained.

## SECTION II

DESCRIPTION OF INPUTA. Input Format

| <u>Card Number</u> | <u>Columns</u> | <u>Format</u> | <u>Description</u>   |
|--------------------|----------------|---------------|--|
| 1                  | 1-5            | 15            | J1, type of flow (0-two dimensional, 1-axisymmetric)   |
|                    | 6-10           | 15            | J2, coordinate exponent for line source system (0-two dimensional or axisymmetric, 1-line source)                              |
|                    | 11-15          | 15            | NPTS, number of data points on initial profile   |
|                    | 16-20          | 15            | IEQ, chemistry indicator (0-frozen hydrogen-air chemistry, 1-equilibrium chemistry)  |
|                    | 21-25          | 15            | ICØWL, external data indicator (1-overexpansion or underexpansion interaction calculations is required, 0-internal flow only). |
|                    | 26-30          | 15            | IØVER, overexpansion indicator (0-flow definitely underexpanded, 1-flow overexpanded or marginal)                              |
|                    | 31-35          | 15            | MM, number of points in Prandtl-Meyer fan (MM=9, maximum)  |
|                    | 36-40          | 15            | IDEAL, indicator for ideal gas calculation, 1-for calculation, 0-non ideal gas   |
|                    | 1-5            | 15            | KSIDE-sidewall force and moment indicator, 0-no sidewall calculation, 1-for calculation  |
|                    | 6-10           | 15            | IVIS-viscous calculation indicator, 0-no calculation, 1-viscous forces and local heat transfer calculated                      |

| <u>Card Number</u> | <u>Columns</u> | <u>Format</u> | <u>Description</u>  |
|--------------------|----------------|---------------|---|
| 2                  | 11-15          | I5            | ITW-adiabatic wall indicator, 0-wall temperature must be specified if ITW=1, (see card 17) 1-adiabatic wall calculation |
| 3                  | 1-10           | E10.0         | *XBP, ratio of axial coordinate of cowl at initial station to throat height   |
|                    | 11-20          | E10.0         | XBØD, ratio of axial coordinate of lower wall at initial station to throat height                                       |
|                    | 21-30          | E10.0         | XCØWL, ratio of axial coordinate of cowl trailing edge to throat height   |
|                    | 31-40          | E10.0         | RTH, throat height (ft.), scaling parameter L*  |
|                    | 41-50          | E10.0         | TEST, maximum allowable axial step size, used for computing upper boundary - typical value = .1                         |
|                    | 51-60          | E10.0         | XFINAL, ratio of final axial coordinate of run to throat height   |
|                    | 6-170          | E10.0         | XTJ1, ratio of axial coordinate of beginning of Cartesian region to throat height                                       |
| 4                  | 1-10           | E10.0         | XSHFT, ratio of axial coordinate of moment axis to throat height  |
|                    | 11-20          | E10.0         | YSHFT, ratio of radial coordinate of moment axis to throat height   |
|                    | 21-30          | E10.0         | XTHX, initial thrust (lbs/RTH <sup>2</sup> )  |
|                    | 31-40          | E10.0         | YLFT, initial lift (lbs/RTH <sup>2</sup> )  |
|                    | 41-50          | E10.0         | XMØM, initial pitching moment (ft-lbs/RTH <sup>3</sup> )  |

---

\*(All length variables are non-dimensionalized by RTH.)

| <u>Card Number</u> | <u>Columns</u>   | <u>Format</u> | <u>Description</u>  |
|--------------------|--|---------------|---|
| 5                  | 1-10   | E10.0         | XTHS, initial sidewall thrust (lbs/RTH <sup>2</sup> )   |
|                    | 11-20  | E10.0         | XLFTS, initial sidewall lift (lbs/RTH <sup>2</sup> )  |
|                    | 21-30  | E10.0         | XMØMS, initial sidewall moment (ft-lbs/RTH <sup>3</sup> )   |
|                    | 31-40  | E10.0         | XVTHX, initial viscous thrust (lbs/RTH <sup>2</sup> )   |
|                    | 41-50  | E10.0         | XVLFT, initial viscous lift (lbs/RTH <sup>2</sup> )   |
|                    | 51-60  | E10.0         | SVMØM, initial viscous moment (ft-lbs/RTH <sup>3</sup> )  |
| 6                  | 1-5  | 15            | NXXJ1, number of locations in source flow where a new initial profile is desired, maximum is 4, minimum is 1 (i.e., changes of origin, cowl station, ...) |
| 7                  | One of the following cards is necessary for each NXXJ1. If two-dimensional flow, card 7a may be blank. |               |   |
| 7a                 | 1-10   | E10.0         | XXJ1, ratio of axial coordinate of new initial profile to throat height   |
|                    | 11-20  | E10.0         | AXX, coefficients of polynomial describing a segment of lateral extent of the nozzle  |
|                    | 21-30  | E10.0         | BXX, for the equation ( $Z_L = AXX(X-X_i) + BXX$ )  |
|                    | 31-40  | E10.0         | XØR, ratio of axial coordinate of line source origin  |
| 7b                 | 1-5  | 15            | IFENCE, fence indicator (0-no fence; 1-supersonic fence exists)   |
|                    | 11-20  | E10.0         | AFENCE, coefficients of fence for the equation  |
|                    | 21-30  | E10.0         | BFENCE, $Y=AFENCE (X-XBP) + BFENCE$   |



| <u>Card Number</u> | <u>Columns</u>   | <u>Format</u> | <u>Description</u>  |
|--------------------|--|---------------|---|
| 7b                 | 31-40  | E10.0         | XFENCE, ratio of axial coordinate of fence on lower surface to throat radius                                    |
| 8                  | 1-5  | I5            | NUWSEG, number of polynomial segments describing the cowl (maximum is 5)  |
|                    | 6-10   | I5            | NLWSEG, number of polynomial segments describing the lower wall (maximum is 5)                                  |
| 9                  | One of the following cards is necessary for each cowl segment.       |               |   |
| 9a                 | 1-10   | E10.0         | XXU(L), ratio of axial coordinate of beginning of "L <sup>th</sup> " segment of cowl to throat height           |
|                    | 11-20  | E10.0         | A, coefficients of the "L <sup>th</sup> " segment   |
|                    | 21-30  | E10.0         | B, of polynomial describing cowl for the equation   |
|                    | 31-40  | E10.0         | C, $Y=AX^2+BX+C$ ; $Y=Y/RTH$ & $X=X/RTH$  |
| 10                 | One of the following cards is necessary for each lower wall segment. |               |   |
| 10a                | 1-10   | E10.0         | XXL(L), ratio of axial coordinate of beginning of the "L <sup>th</sup> " segment of lower wall to throat height |
|                    | 11-20  | E10.0         | A, coefficients of the "L <sup>th</sup> " segment   |
|                    | 21-30  | E10.0         | B, of polynomial describing lower wall for the equation   |
|                    | 31-40  | E10.0         | C, $Y=AX^2+BX+C$ ; $Y=Y/RTH$ & $X=X/RTH$  |
| 11                 | 1-10   | E10.0         | EMINF, free stream of reference Mach number   |

| <u>Card Number</u> | <u>Columns</u>   | <u>Format</u> | <u>Description</u>  |
|--------------------|--|---------------|---|
| 11                 | 11-20  | E10.0         | TIN, free stream or reference temperature ( $^{\circ}$ K)           |
|                    | 21-30  | E10.0         | WINF, free stream or reference molecular weight (lbs/lb-mole)       |
|                    | 31-40  | E10.0         | PINF, free stream or reference pressure (lbs/ft <sup>2</sup> )      |
| 12                 | Read this card if IDEAL = 1.   |               |   |
| 12a                | 1-10   | E10.0         | GAMEY, ideal gas ratio of specific heats ( $\gamma$ )               |
|                    | 11-20  | E10.0         | XMWT, molecular weight  |
| 13                 | Initial Profile - One of the following cards are required for each data point as described below. The program reads data points beginning at the lower wall (point #1) and proceeds to the cowl (point #NPTS). |               |   |
| 13a                | 1-10   | E10.0         | X(1), ratio of axial coordinate of data point to throat height      |
|                    | 11-20  | E10.0         | Y(1), ratio of radial coordinate of data point to throat height     |
|                    | 21-30  | E10.0         | P(1), ratio of pressure at data point to free stream pressure       |
|                    | 31-40  | E10.0         | Q(1), ratio of velocity at data point to free stream velocity       |
|                    | 41-50  | E10.0         | T(1), ratio of temperature at data point to free stream temperature |
|                    | 51-60  | E10.0         | TH(1), flow inclination at data point (in radians)                  |
|                    | 61-70  | E10.0         | W(1), fuel to air equivalence ratio (only necessary if IEQ=1)       |

| <u>Card Number</u> | <u>Columns</u> | <u>Format</u> | <u>Description</u>  |
|--------------------|----------------|---------------|---|
| 14                 |                |               | Initial Mass Fractions - Same as card 13 above except for mass fractions at each data point. These cards are necessary only if IEQ=0. |
| 14a                | 1-10           | E10.0         | mass fraction of H  |
|                    | 11-20          | E10.0         | mass fraction of O  |
|                    | 21-30          | E10.0         | mass fraction of H <sub>2</sub> O   |
|                    | 31-40          | E10.0         | mass fraction of H <sub>2</sub>   |
|                    | 41-50          | E10.0         | mass fraction of O <sub>2</sub>   |
|                    | 51-60          | E10.0         | mass fraction of OH   |
|                    | 61-70          | E10.0         | mass fraction of N <sub>2</sub>   |
| 15                 |                |               | This card is necessary only if ICØWL =1.  |
| 15a                | 1-10           | E10.0         | *XM, axial location of cowl end   |
|                    | 11-20          | E10.0         | YM, vertical location of cowl end   |
|                    | 21-30          | E10.0         | PM, ratio of pressure external to the cowl to free stream or reference pressure   |
|                    | 31-40          | E10.0         | QM, ratio of velocity external to the cowl to free stream or reference velocity   |
|                    | 41-50          | E10.0         | TM, ratio of temperature equal the cowl to free stream or reference temperature   |
|                    | 51-60          | E10.0         | THM, flow inclination external to the cowl (in radians)   |
|                    | 61-70          | E10.0         | WM, external flow molecular weight assumed the same WINF  |

---

\*(All length variables are non-dimensionalized by RTH.)

| <u>Card Number</u> | <u>Columns</u>                                 | <u>Format</u> | <u>Description</u>  |
|--------------------|--|---------------|---|
| 16                 | This card necessary only if IVIS = 1.          |               |   |
| 16a                | 1-10   | E10.0         | XSTR, boundary layer virtual origin                                     |
|                    | 11-20  | E10.0         | Pr, Prandtl number  |
|                    | 21-30  | E10.0         | Rec, boundary layer recovery factor (turbulent flow)                    |
|                    | 31-40  | E10.0         | REIN, free stream Reynolds number per foot                              |
|                    | 41-50  | E10.0         | SH, constant for turbulent Reynolds analogy ( $ST = SH \cdot C_f / 2$ ) |
| 17                 | Wall temperature distributions-necessary only. |               |   |
|                    | If ITW = 0, L = 1 Cowl surface; L = 2          |               |   |
|                    | Vehicle surface; L = 3 sidewall                |               |   |
| 17a,b,c            | 1-10   | E10.0         | AH(L) coefficients in equations   |
|                    | 11-20  | E10.0         | BH(L) $T_{WALL} = AH(L) \cdot (X-XBP)^2 + BH(L)$                        |
|                    | 21-30  | E10.0         | CH(L) $(X-XBP) + CH(L)$   |

B. Figures for Input

EXTERNAL FLOW

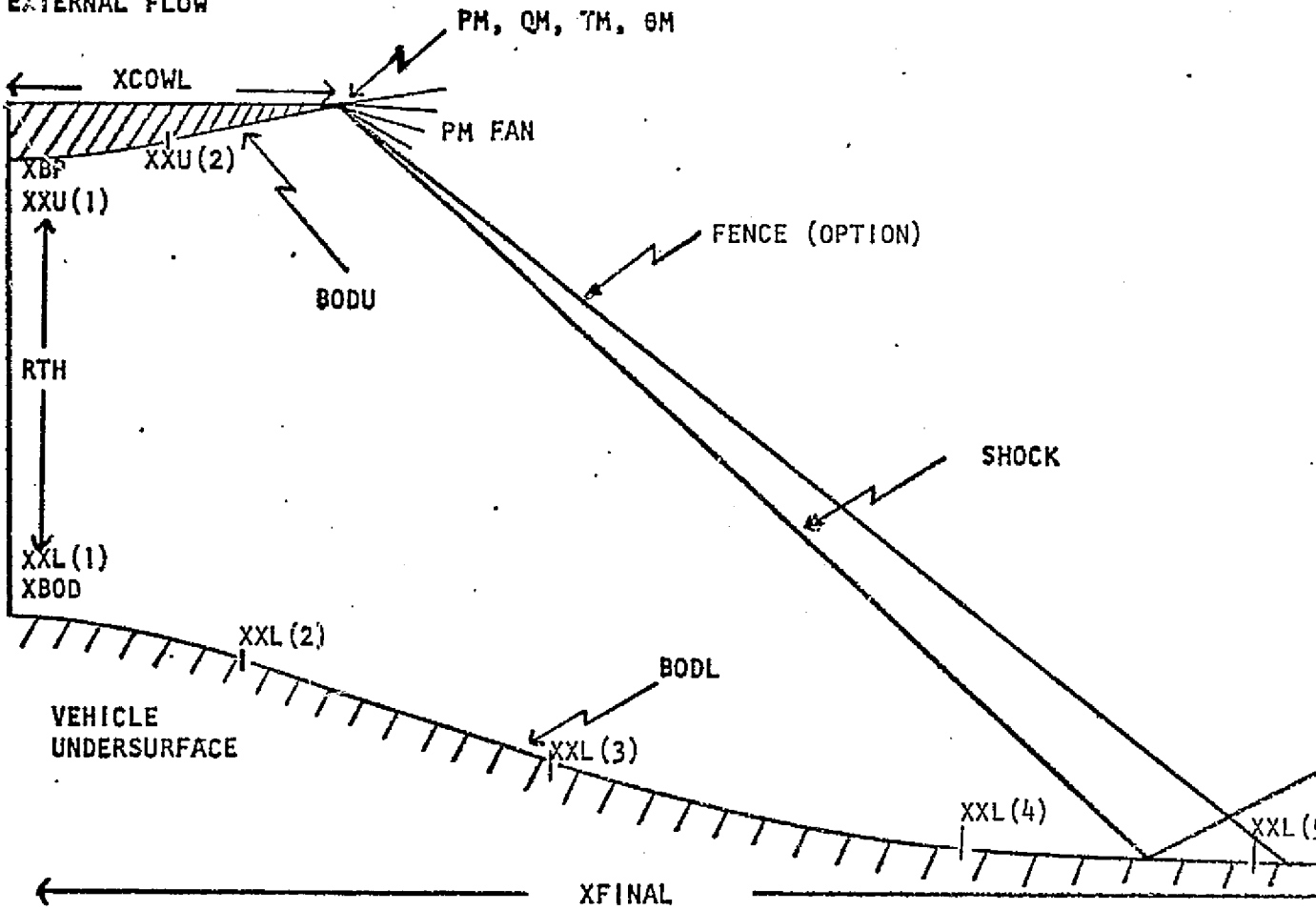


FIGURE #1. Definition of Physical Input Variables

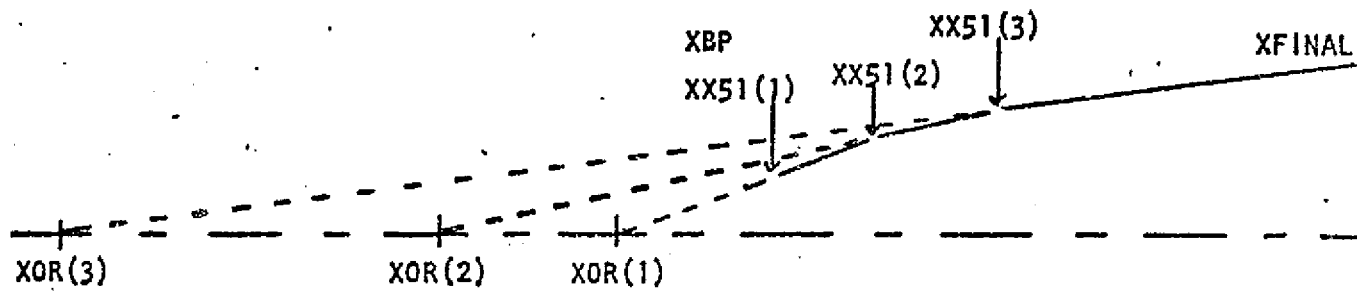


FIGURE #2. Definition of Change of Origin Variables

## SECTION 1.1

DESCRIPTION OF OUTPUT

A. Output Format - The heading page contains program constants, line source coordinates and origin changes, upper and lower wall coordinates, free stream data at the cowl and infinity conditions. The program then prints the "initial profile," the data at selected points along down-running characteristics in the flow field and the running lift, thrust, and pitching moment. The process continues until the input value for the final axial location is reached.

The above flow can be interrupted by "change of origin profiles" and a profile at the trailing edge of the cowl. If the flow is over-expanded at the cowl the output will switch to up-running characteristics from the lower wall to the contact surface and additional output covering the shock angle and external Mach number will be printed. When the shock reflects off the lower wall another profile will be printed and the run will proceed to the final axial location through down-running characteristics.

B. Identification of Output Variables

X - axial distance/throat height  
 Y - radial distance/throat height  
 Q - velocity/free stream velocity  
 T - temperature/free stream temperature  
 P - pressure/free stream pressure  
 TH - flow angle (radians)  
 EM - Mach number

ALP(1) = mass fraction of H  
 ALP(2) = mass fraction of O  
 ALP(3) = mass fraction of H<sub>2</sub>O  
 ALP(4) = mass fraction of H<sub>2</sub>  
 ALP(5) = mass fraction of O<sub>2</sub>  
 ALP(6) = mass fraction of OH  
 ALP(7) = mass fraction of N<sub>2</sub>

Frozen flow extra output is:

CPX - specific heat/free stream specific heat

W - molecular weight of mixture/free stream molecular weight

Equilibrium flow extra output is:

GAM - equilibrium isentropic exponent

PHI - fuel to air ratio

Vehicle Forces (thrust, lift, pitching moment):

Vehicle force data are given at every output

Station and are delineated as follows

- (a) Cowl and undersurface forces
- (b) Sidewall forces
- (c) Viscous forces

## SECTION IV

SUBROUTINES AND FUNCTIONSA. Subroutines

| <u>Name</u> | <u>Description</u>  |
|-------------|---|
| 1. INDATA   | reads and prints initial data and computes infinity conditions  |
| 2. COEFF    | sets thermodynamic coefficients as functions of temperature   |
| 3. ERROR    | prints program statement number nearest selected errors and terminates computer run   |
| 4. BODL     | locates axial and radial coordinates along lower vehicle surface  |
| 5. BODU     | locates axial and radial coordinates along upper cowl surface   |
| 6. COWL     | calculates shock jump relations and Prandtl-Meyer fan at cowl trailing edge for under-expanded flow                                       |
| 7. COWLO    | computes contact points, shock points and shock angle at cowl trailing edge for over-expanded flow  |
| 8. DPØINT   | computes location and properties of streamline intersection with characteristic ( $C_{\pm}$ )   |
| 9. SHOCK    | calculates shock jump conditions  |
| 10. SHOCPT  | computes shock angle by matching pressure from shock jump relations and pressure from characteristic relation on downstream side of shock |
| 11. PRM     | computes isentropic ideal gas expansion   |
| 12. DRTEST  | tests for dropping data points on free stream side of shock   |
| 13. ALL     | calculates density, ratio of specific heats, Mach number, Mach angle, frozen flow specific heat, molecular weight and gas constant        |
| 14. THERMO  | computes frozen flow specific heat, derivative of specific heat and enthalpy of each species from polynomial fits in temperature          |
| 15. XMASSS  | computes mass flow correction factor  |
| 16. FM      | computes mass function  |
| 17. PMI     | computes flow properties for given Prandtl-Meyer turning  |
| 18. GEM     | computes intersection of two straight lines   |



| <u>Name</u> | <u>Description</u>   |
|-------------|--|
| 19. SL      | computes streamline properties of newly calculated data point                            |
| 20. INT     | interpolation routine  |
| 21. ERR     | finds roots of a given function  |
| 22. FUZZY   | detects crossing of down-running characteristics   |
| 23. WUZZY   | detects crossing of up-running characteristics   |
| 24. LTHM    | computes incremental lift, thrust, pitching moment and side force                        |
| 25. VIS     | computes viscosity coefficient   |
| 26. SNARF   | computes surface area unit normal and area centroid for elemental surface quadrilaterals |
| 27. GNURE   | computes flat plate skin friction and heat transfer coefficients                         |
| 28. BØDL    | calculates body height and slope for vehicle surface given the axial location            |
| 29. BØDU    | calculates body height and slope for cowl surface given the axial location               |

## B. Functions

| <u>Name</u> | <u>Description</u>   |
|-------------|--|
| 1. FT       | calculates temperature at any data point in flow field                                 |
| 2. FH       | computes static enthalpy at any point in flow field                                    |
| 3. FGAM     | makes isentropic exponent and associated thermodynamic data at any point in flow field |
| 4. RHEQ     | computes equilibrium density   |
| 5. XM1      | calculates $\tan(\theta+\mu)$ along up-running characteristic                          |
| 6. XM2      | calculates $\tan(\theta+\mu)$ along down-running characteristic                        |
| 7. XM3      | calculates $\tan(\theta)$ along streamline   |

| <u>Name</u> | <u>Description</u>   |
|-------------|--|
| 8. F1       | *A <sub>1</sub> or B <sub>1</sub> coefficient along up-running and down-running characteristics respectively |
| 9. F2       | *A <sub>2</sub> or B <sub>2</sub> coefficient along up-running and down-running characteristics respectively |

---

\*Note: p - θ relationship along up-running characteristic:

$$A_1(p_C - p_A) + \theta_C - \theta_A + A_2(X_C - X_A) = 0$$

p - θ relationship along down-running characteristic:

$$B(p_C - p_B) - \theta_C + \theta_B + B_2(X_C - X_B) = 0$$

SECTION V

MACHINE CONTROL CONSIDERATIONS

1. Machine - program designed for CDC 6600.
2. Estimates for run.
  - a. Field length:
    - (1) compile - 65,000 octal locations
    - (2) load - 120,000 octal locations
    - (3) run - 100,000 octal locations
  - b. CP time: variable depending on number of points in initial profile and type of flow
  - c. IO: less than 100 octal seconds
  - d. Tapes or disks used:
    - (1) Tape 5 - card input
    - (2) Tape 6 - printed output
    - (3) no other tapes or disk files used
  - e. Printed output: as in CP time it is variable depending on case submitted.

SECTION VI

SAMPLE INPUT FOR SOURCE FLOW

|     | 0 | 1      | 21 | 1      | 1 | 0      | 9    | 0   |
|-----|---|--------|----|--------|---|--------|------|-----|
| 0.  | 1 | 0      | 0  |        |   |        |      |     |
| 0.  |   | 0.     |    | 3.     |   | 1.     | .1   | 21. |
| 0.  |   | .5     |    | 0.     |   | 0.     | 0.   | 22. |
| 0.  |   | 0.     |    | 0.     |   | 0.     | 0.   | 0.  |
| 2   |   |        |    |        |   |        |      |     |
| 0.  |   | .0875  |    | 1.     |   | -7.    |      |     |
| 3.  |   | .0875  |    | 1.     |   | -7.    |      |     |
| 1   |   | -.59   |    | 3.064  |   | 16.    |      |     |
| 2   |   | 3      |    |        |   |        |      |     |
| 0.  |   | .1314  |    | 0.     |   | 1.     |      |     |
| .4  |   | 0.     |    | .1051  |   | .979   |      |     |
| 0.  |   | -.5565 |    | 0.     |   | 0.     |      |     |
| .4  |   | 0.     |    | -.4452 |   | .08905 |      |     |
| 8.  |   | .01019 |    | -.6082 |   | .741   |      |     |
| 10. |   | 232.3  |    | 28.96  |   | 23.09  |      |     |
| 0.  |   | 0.     |    | 36.65  |   | .929   | 10.1 | 0.  |
| 0.  |   | .05    |    | 36.65  |   | .929   | 10.1 | 0.  |
| 0.  |   | .1     |    | 36.65  |   | .929   | 10.1 | 0.  |
| 0.  |   | .15    |    | 36.65  |   | .929   | 10.1 | 0.  |
| 0.  |   | .2     |    | 36.65  |   | .929   | 10.1 | 0.  |
| 0.  |   | .25    |    | 36.65  |   | .929   | 10.1 | 0.  |
| 0.  |   | .3     |    | 36.65  |   | .929   | 10.1 | 0.  |
| 0.  |   | .35    |    | 36.65  |   | .929   | 10.1 | 0.  |
| 0.  |   | .4     |    | 36.65  |   | .929   | 10.1 | 0.  |
| 0.  |   | .45    |    | 36.65  |   | .929   | 10.1 | 0.  |
| 0.  |   | .5     |    | 36.65  |   | .929   | 10.1 | 0.  |
| 0.  |   | .55    |    | 36.65  |   | .929   | 10.1 | 0.  |
| 0.  |   | .6     |    | 36.65  |   | .929   | 10.1 | 0.  |
| 0.  |   | .65    |    | 36.65  |   | .929   | 10.1 | 0.  |
| 0.  |   | .7     |    | 36.65  |   | .929   | 10.1 | 0.  |
| 0.  |   | .75    |    | 36.65  |   | .929   | 10.1 | 0.  |
| 0.  |   | .8     |    | 36.65  |   | .929   | 10.1 | 0.  |
| 0.  |   | .85    |    | 36.65  |   | .929   | 10.1 | 0.  |
| 0.  |   | .9     |    | 36.65  |   | .929   | 10.1 | 0.  |
| 0.  |   | .95    |    | 36.65  |   | .929   | 10.1 | 0.  |
| 0.  |   | 1.     |    | 36.65  |   | .929   | 10.1 | 0.  |
| 3.  |   | 1.3943 |    | 1.     |   | 1.     | 1.   | 0.  |

TM 183

APPENDIX

PROGRAM LISTING

The following is a listing of the Fortran IV program for Source Flow  
Characteristic

```

PROGRAM NOZ BOD (INPUT,OUTPUT,PUNCH,TAPE5=INPUT,TAPE6=OUTPUT,
1 TAPE7=PUNCH)
COMMON/COWL/ICOWL,MM,XM(9),YM(9),PM(9),WM(9),RHM(9),THM(9),GM(9),
1RM(9),TM(9),GM(9),XMUM(9),EMM(9),ALPM(7,9),CPXM(9)
COMMON/IPP/IPP
COMMON/SHAPE/AA1(5,2),AA2(5,2),AA3(5,2),XXU(5),XXL(5),XINTU,XINTL
COMMON/LTM/XSHFT,YSHFT,XTHX,YLFT,XMOM,XTHS,YLFTS,XMOMS,KSIDE
COMMON/HOT/AH(3),BH(3),CH(3),XSTR,PR,REC,REIN,RT,SH,ITW,IVIS
COMMON/VISF/XVTHX,YVLFT,XVMOM
COMMON/XXJ/NXXJ1,XXJ1(6),AXX(6),BXX(6),XOR(6)
COMMON/XFINAL/XFINAL
COMMON/IEQ/IEQ,PIN,RHOINF,UINF,PINF
COMMON/VAR/RHO(200),
1EM(200),XMU(200),CPX(200),W(200),R(200),GAM(200),XMASS(200),
2 XN(200),YN(200),QN(200),TN(200),PN(200),THN(200),RHON
3(200),EMN(200),XMUN(200),CPXN(200),WN(200),RN(200),GAMN(200),
4XMASSN(200),ALPN(10,200),SI(10),HI(10),TEMP(20)
5,ALPDUM(10)
COMMON /SP/ NSP
COMMON/FVAR/
1RHOF(200),CPXF(200),EMF(200),XMUF(200),WF(200),RF(200),GAMF(200),
2XMASSF(200), HF(200),SF(200),ALPD(10),
3THETA(20)
COMMON/X/ X(200),Y(200),P(200),Q(200),T(200),TH(200),ALP(10,200)
COMMON /I/ IOPUT
COMMON/A/ TIN,CPIN,RO
COMMON/B/ WTMOLE
COMMON/D/ GAMINF,EMINF,RINF,WINF
COMMON/F/A9,B9,IBOD,XWF,NBOD,YEND
COMMON/ETX/XJ,XJ1,NPTS,IO,IREFL,ICHEM,IPUNCH,IDESGN,IR,NXX,XBP,
1YBP,THBP,RAD,XBOD,YBOD,THBOD,RADB,XEND,THEEND,RTH,YEXIT,THST,TEST,
1IRFL,YO,RADB2,RRAD(20), NSTAR,YNOZ,EIN, PEN,H16,H17
COMMON/XF/XF(200),YF(200),PF(200),QF(200),TF(200),THF(200),ALPF(
110,200)
COMMON/XCOWL/XCOWL
COMMON/C1/ EMC1,TC1,QC1
COMMON /IOVER/ IOVER
COMMON/XTJ1/XTJ1
COMMON/FENCE/IFENCE,AFENCE,BFENCE,XFENCE
COMMON/ICMPLT/ICMPLT
COMMON/ICU/EMC2
COMMON/PFF/PFINF
DIMENSION STS(200)
DIMENSION WTMOLE(10)
COMMON/DD/XD,YD,THD,PD,QD,RHD,RD,WD,EMD,GAMD,XMUD,TD
DIMENSION TYPE2(2)
DIMENSION TYPE3(2)
DIMENSION TYPE9(2),PHIPR(2)
DATA PHIPR/3H ,3HPI/
DATA TYPE9/3HCPX,3HPI/
DATA TYPE3/3H W ,3HGAM/
DATA TYPE2 /10H NOZZLE ,10HCENTERBODY/
DATA XXP/1.E+06/
DATA ISHOC/-10000/
IDELG=0
WRITE(6,400)
400 FORMAT(1H1)

```

```

C      J=0 TWO DIMENSIONAL
C      J=1 AXISYMMETRIC
C      SPECIES 1 IS H
C      SPECIES 2 IS O
C      SPECIES 3 IS H2O
C      SPECIES 4 IS H2
C      SPECIES 5 IS O2
C      SPECIES 6 IS OH
C      SPECIES 7 IS N2
C      SPECIES 8 IS CO2
C      SPECIES 9 IS CO
C      SPECIES 10 IS C3H8
      IPTP=0
      NXXJ=2
      IFLIP=0
      IHALT=0
      ICMPLT=0
      NSTAR=0
      IOPUT=32
      IUNDR=0
      IAA=1
      CALL INDATA
      XCOWLH=XCOWL
      IEQ5=IEQ+1
      YNOZ=YBP
      PEN=      PIN
      XJ1SV=XJ1
      PFINF=PINF*2116./PIN
      IFENC1=0
7211  IPP=0
      LSTT=0
      WRITE(6,400)
      IF(IFENC1.EQ.1) WRITE(6,3100)
3100  FORMAT(30X*FENCE INITIAL PROFILE*)
      IF(IFENC1.EQ.1) GO TO 3101
      IF(IPTP.EQ.0) WRITE(6,9191) XOR(1)
9191  FORMAT(20X*INITIAL PROFILE*
1* - ORIGIN OF SYSTEM =*E13,5)
      IF(IFLIP.EQ.0.AND.IPTP.EQ.1.AND.XF(1).NE.XCOWLH) WRITE(6,9192)
1 XOR(NXXJ-1)
9192  FORMAT(16X*CHANGE OF ORIGIN PROFILE*
1* - ORIGIN OF SYSTEM =*E13,5)
      IF(IFLIP.EQ.0.AND.IPTP.EQ.1.AND.XF(1).EQ.XCOWLH) WRITE(6,3132)
1 XOR(NXXJ-1)
3132  FORMAT( 8X*PROFILE FOR UNDEREXPANDED SHOCK AT COWL*
1* - ORIGIN OF SYSTEM =*E13,5)
      IF(IFLIP.EQ.1) WRITE(6,600) XOR(NXXJ-1)
600  FORMAT( 8X*PROFILE FOR OVEREXPANDED SHOCK AT COWL*
1* - ORIGIN OF SYSTEM =*E13,5)
      IF(IFLIP.EQ.2) WRITE(6,621) XOR(NXXJ-1)
621  FORMAT( 6X*PROFILE WHEN SHOCK REFLECTS OFF LOWER WALL*
1* - ORIGIN OF SYSTEM =*E13,5)
3101  CONTINUE
      IEQ1=IEQ+1
      WRITE(6,6896) PHIPR(IEQ1)
6896  FORMAT(
1X,*X*,11X,*Y*,11X,*Q*,11X,*T*,11X,*P*,10X,*TH*10XA3)
//5X,*PT,*,8

```

```

IF(ICHEM.EQ.0.AND.IEQ.EQ.0) WRITE(6,7701)
7701 FORMAT(13X*ALP(1)=H*4X*ALP(2)=O*3X*ALP(3)=H2O*2X*ALP(4)=H2*
13X*ALP(5)=O2*3X*ALP(6)=OH*3X*ALP(7)=N2*)
3160 CONTINUE
DO 3163 I=1,NPTS
C=PF(I)/PIN
YFPR=YF(I)
THFPR=THF(I)
IF(IFLIP.EQ.1) YFPR=-YF(I)
IF(IFLIP.EQ.1) THFPR=-THF(I)
IF(IEQ.EQ.1) GO TO 9806
WRITE(6,16) I,XF(I),YFPR,QF(I),TF(I),C,THFPR
WRITE(6,1602) (ALPF(J,I),J=1,NSP)
GO TO 3163
9806 WRITE(6,16) I,XF(I),YFPR,QF(I),TF(I),C,THFPR,WF(I)
3163 CONTINUE
1800 FORMAT(* UNDERSURFACE AND COWL THRUST =*E13,5,7X*LIFT =*E13,5,7X*M
10MENT =*E13,5)
IPTP=1
XJ1SV=XJ1
WRITE(6,3130)
3130 FORMAT(/)
IF(KSIDE.EQ.0) GO TO 3104
WRITE(6,1800) XTHX,YLFT,XMOM
WRITE(6,3107)XTHS,YLFTS,XMOMS
3107 FORMAT(5X*SIDEWALL THRUST=*E12,4,5X*SIDEWALL LIFT=*E12,4,5X*SIDEW
1ALL MOMENT=*E12,4//)
IF(IVIS.EQ.1)WRITE(6,3153)XVTHX,YVLFT,XVMOM
3153 FORMAT(5X*VISCOUS THRUST =*E12,4,5X*VISCOUS LIFT =*E12,4,5X*VISCOU
1S MOMENT =*E12,4//)
3104 CONTINUE
N=2
LMAX=1
KMAX=2*(N-1)-1
IF(IOVER.NE.2) GO TO 7423
N=3
IPP=1
LMAX=2
KMAX=2
7423 NN1=N-1
DO 7424 I=1,NN1
II=NN1-I+1
DO 1500 J=1,NSP
ALP(J,I)=ALPF(J,II)
1500 ALPDUM(J)=ALP(J,I)
D=0.
CALL INT(0.,XF(II),YF(II),THF(II),PF(II),QF(II),RHOF(II),RF(II),
1WF(II),GAMF(II),EMF(II),XMUF(II),TF(II),
1D,D,D,D,D,D,D,D,D,D,D,D,D
1,X(I),Y(I),TH(I),P(I),Q(I),RHO(I),R(I),W(I),GAM(I),
1EM(I),XMU(I),T(I),ALPDUM,1,IEQ)
7424 CONTINUE
500 CONTINUE
IF(KMAX.GE.191) GO TO 9123
6060 IPP=IPP+1
6883 WRITE(6,7633) IPP
7633 FORMAT(5X,*LINE NO. = *,I4)

```



```

IF(IOVER.EQ.2.AND.KMAX.GE.10) GO TO 670
JJ=1+KMAX/10
JJ1=KMAX-1
IF(IO.EQ.1) JJ=1
WRITE(6,6885)TYPE3(IEQ5),TYPE9(IEQ5)
16  FORMAT(3X,I4,3X,10E12.4)
6885  FORMAT(5X,*PT,*,8X,*X*,11X,*Y*,11X,*P*,10X,*TH*,11X,*Q*,11X,*T*,
110X,*EM*,10X,A3,9X,A3)
DO 7637 I=1,JJ1,JJ
C=P(I)/PIN
YFPR=Y (I)
THFPR=TH (I)
DUPR=W(I)
IF(IEQ5.EQ.2) DUPR=GAM(I)
CPR=CPX(I)
IF(IEQ.EQ.1)CPR=W(I)
IF(IFLIP.EQ.1) YFPR=-Y (I)
IF(IFLIP.EQ.1) THFPR=-TH (I)
WRITE(6,7632) I,X(I),YFPR,C ,THFPR,Q(I),T(I),EM(I),DUPR,CPR
7632  FORMAT(3X,I4,3X,10E12.4)
7637  CONTINUE
1602  FORMAT(10X,10E12.4)
IF(IPP.EQ.1) GO TO 7759
I=KMAX
C=P(I)/PIN
YFPR=Y (I)
THFPR=TH (I)
DUPR=W(I)
IF(IEQ5.EQ.2) DUPR=GAM(I)
CPR=CPX(I)
IF(IEQ.EQ.1)CPR=W(I)
IF(IFLIP.EQ.1) YFPR=-Y (I)
IF(IFLIP.EQ.1) THFPR=-TH (I)
WRITE(6,7632) I,X(I),YFPR,C ,THFPR,Q(I),T(I),EM(I),DUPR,CPR
GO TO 7759
670  JJ=1+KMAX/10
JJ2=1
ISH=ISHDC
JJ1=ISH-1
WRITE(6,6885)TYPE3(IEQ5)
672  DO 671 I=JJ2,JJ1,JJ
C=P(I)/PIN
YFPR=Y (I)
THFPR=TH (I)
DUPR=W(I)
IF(IEQ5.EQ.2) DUPR=GAM(I)
CPR=CPX(I)
IF(IEQ.EQ.1)CPR=W(I)
IF(IFLIP.EQ.1) YFPR=-Y (I)
IF(IFLIP.EQ.1) THFPR=-TH (I)
WRITE(6,7632) I,X(I),YFPR,C ,THFPR,Q(I),T(I),EM(I),DUPR,CPR
671  CONTINUE
I=JJ1+1
C=P(I)/PIN
YFPR=Y (I)
THFPR=TH (I)
DUPR=W(I)

```

```

IF(IEQS, EQ, 2) DUPR=GAM(I)
CPR=CPX(I)
IF(IEQ, EQ, 1) CPR=W(I)
IF(IFLIP, EQ, 1) YFPR=-Y(I)
IF(IFLIP, EQ, 1) THFPR=-TH(I)
WRITE(6, 7632) I, X(I), YFPR, C, THFPR, Q(I), T(I), EM(I), DUPR, CPR
IF(JJ1, EQ, KMAX-1) GO TO 7759
JJ2=ISH+1
JJ1=KMAX-1
GO TO 672
7759 BETPR=BET
WRITE(6, 1800) XTHX, YLFT, XMOM
IF(KSIDE, EQ, 1)
1WRITE(6, 3107) XTHS, YLFTS, XMOMS
IF(IVIS, EQ, 1) WRITE(6, 3153) XVTHX, YVLFT, XVMOM
IF(IFLIP, EQ, 1) BETPR=-BET
IF(IOVER, EQ, 2) WRITE(6, 653) BETPR, EMC1
653 FORMAT(5X*SHOCK ANGLE =*E12.4, 5X*EXTERNAL MACH NO. =*E12.4)
IF(IUNDR, EQ, 1) WRITE(6, 596) EMC1
596 FORMAT(5X* EXTERNAL MACH NO. = *E12.4)
WRITE(6, 1603)
1603 FORMAT(///)
6884 ICMP=ICMPLT+1
IF(IOVER, NE, 2) GO TO 2658
ISHOC=ISHOC+1
IF(NSTAR, EQ, 1) ISHOC=ISHOC-2
2658 CONTINUE
IF(IHALT, EQ, 1) STOP
IF(IFLIP, EQ, 2, AND, N, GT, NPTS) STOP
GO TO (4300, 4301, 4302, 4303), ICMP
4301 IF(ICOWL, EQ, 0) STOP
ICMPLT=2
IUNDR=1
CALL COWL(-1.)
IPM=1
4302 IPM=IPM+1
IF(IPM, GT, MM-3) ICMPLT=0
IF(IPM, GT, MM-3) GO TO 8104
LMAX=KMAX+1
DO 4306 J=1, NSP
ALPN(J, 1)=ALPM(J, IPM)
4306 ALPDUM(J)=ALPM(J, IPM)
D=0.
CALL INT(0., XM(IPM), YM(IPM), THM(IPM), PM(IPM), QM(IPM), RHM(IPM),
1RM(IPM), WM(IPM), GM(IPM), EMM(IPM), XMUM(IPM), TM(IPM),
1D, D, D, D, D, D, D, D, D, D, D, D, D, D, D, D, D, D, D, D, D, D,
1, XN(1), YN(1), THN(1), PN(1), QN(1), RHDN(1), RN(1), WN(1), GAMN(1),
1EMN(1), XMUN(1), TN(1), ALPDUM, 0, IEQ)
GO TO 8060
4303 ICMPLT=3
STOP
4300 IF(X(1), EQ, XCOWLH, AND, IPP, EQ, NPTS, AND, IOVER, NE, 2) GO TO 4301
IF(N, GT, NPTS) GO TO 8104
LMAX=LMAX+2
L=1
K=1
D=0.

```

```

DO 510 J=1,NSP
ALPN(J,L)=ALPF(J,N)
510 ALPDUM(J)=ALPF(J,N)
CALL INT (0.,XF(N),YF(N),THF(N),PF(N),QF(N),RHOF(N),RF(N),
1WF(N),GAMF(N),EMF(N),XMUF(N),TF(N),
1D,D,D,D,D,D,D,D,D,D,D,D,D
1,XN(L),YN(L),THN(L),PN(L),QN(L),RHON(L),RN(L),WN(L),GAMN(L),
1EMN(L),XMUN(L),TN(L),ALPDUM,1,IEQ)
IFENC1=1
IF(IFENCE.EQ.1.AND.XN(L).EQ.XCOWLH.AND.N.EQ.NPTS) GO TO 2601
IFENC1=0
GO TO 8060
8104 ASL=TAN(TH(1))
ACH=TAN(TH(2)+XMU(2))
THSL=TH(1)
CALL GEM(X(2),Y(2),ACH,X(1),Y(1),ASL,XN(1),YDUM)
DELTH=XN(1)-X(1)
IF((DELTH/TEST).GT.1.) GO TO 9061
IT=1
IER=0
IF(IUNDR.GT.0)GO TO 9060
CALL BODU(X(1),Y(1),TH(1),X(2),Y(2),ACH,XN(1),YDUM ,THN(1))
THSL=THN(1)
IF(IOVER.NE.2) GO TO 694
YN(1)=-YN(1)
THN(1)=-THN(1)
694 CONTINUE
DELTH=ABS(THN(1)-TH(1))
IF(DELTH.GT.THST)GO TO 9061
DELTH=XN(1)-X(1)
IF((DELTH/TEST).LT.1.) GO TO 9060
9061 LMAX=KMAX+1
DO 9000 M1=2,KMAX
L=KMAX-M1+2
I=L+1
D=0.
DO 9001 J=1,NSP
ALP(J,I)=ALP(J,L)
9001 ALPDUM(J)=ALP(J,L)
CALL INT(0.,X(L),Y(L),TH(L),P(L),Q(L),RHO(L),R(L),W(L),GAM(L),
1EM(L),XMU(L),T(L),
1D,D,D,D,D,D,D,D,D,D,D,D,D
1,X(I),Y(I),TH(I),P(I),Q(I),RHO(I),R(I),W(I),GAM(I),EM(I),
1XMU(I),T(I),ALPDUM,0,IEQ)
9000 CONTINUE
ISHOC=ISHOC+1
KMAX=KMAX+1
RAT=.5
DO 9003 J=1,NSP
ALP(J,2)=ALP(J,1)+RAT*(ALP(J,3)-ALP(J,1))
9003 ALPDUM(J)=ALP(J,2)
CALL INT(RAT,X(1),Y(1),TH(1),P(1),Q(1),RHO(1),R(1),W(1),GAM(1),
1EM(1),XMU(1),T(1),X(3),Y(3),TH(3),P(3),Q(3),RHO(3),R(3),W(3),
1GAM(3),EM(3),XMU(3),T(3),X(2),Y(2),TH(2),P(2),Q(2),RHO(2),R(2),
1W(2),GAM(2),EM(2),XMU(2),T(2),ALPDUM,1,IEQ)
GO TO 8104
9060 LMAX=KMAX

```

```

A=1.
B=0.
IF(ISHOC.EQ.1) BETN=BET
8000 CONTINUE
IT=1
IER=0
IF(B.EQ.0) THN(1)=THSL
8030 EMSL=XM3(.5,.5,TH(1),THN(1))
EM1=XM1(A,B,TH(2),XMU(2),THN(1),XMUN(1))
IF(ISHOC.EQ.1) EM1=.5*(TAN(BET)+TAN(BETN))
CALL GEM(X(2),Y(2),EM1,X(1),Y(1),EMSL,XN(1),YN(1))
IF(IUNDR.GT.0)GOT O 8020
CALL BODU(X(1),Y(1),TH(1),X(2),Y(2),EM1,XN(1),YN(1),THN(1))
THSL=THN(1)
IF(IQVER.NE.2) GO TO 698
YN(1)=-YN(1)
THN(1)=-THN(1)
698 CONTINUE
8020 A1=F1(A,B,XMU(2),GAM(2),P(2),XMUN(1),GAMN(1),PN(1))
XDUM2=X(2)-XOR(NXXJ-1)
XDUMN=XN(1)-XOR(NXXJ-1)
A2=F2(A,B,1.,XJ,XJ1,XDUM2,Y(2),TH(2),XMU(2),XDUMN,YN(1),THN(1),XMU
1N(1))
DUM1=A2*(XN(1)-X(2))
IF(XJ1.GT.0.) DUM1=A2*ALOG(XDUMN/XDUM2)
DUM= (TH(2)-THN(1)-DUM1)/A1
PN(1)=P(2)*EXP(DUM)
IF(IUNDR.EQ.0)GO TO 1801
P2=PN(1)/P(1)
CALL PRM(P2,TH(1),EMC1,TH2T,EMC2,-1)
ER4=TH2T-THN(1)
IF(ABS(ER4).LT.1.E-04)GO TO 1801
CALL ERR(IER,IT,THN(1),ER4,1.01,THN1,ER1)
IF(IER.EQ.0)GO TO 73
WRITE(6,17)
17 FORMAT(1X,* TOO MANY ITERATIONS IN BODU CONTACT *)
STOP
73 IT=IT+1
GO TO 8030
1801 CONTINUE
DO 8050 J=1,NSP
ALPN(J,1)=ALP(J,1)
8050 ALPDUM(J)=ALPN(J,1)
CALL SL(P(1),Q(1),RHO(1),R(1),W(1),GAM(1),EM(1),XMU(1),T(1),
1PN(1),QN(1),RHON(1),RN(1),WN(1),GAMN(1),EMN(1),XMUN(1),TN(1),
1ALPDUM,IEQ,A,B)
IF(B.EQ.0..OR.IUNDR.EQ.1)GO TO 1798
IF(XN( 1).GT.XCOWL-1,E-04) GO TO 1798
IF(XN( 1).GT.XXJ1(NXXJ)-1,E-04) GO TO 1798
C *****COMPUTE COWL AND SIDEWALL FORCES *****C
Z1=AXX(NXXJ-1)*{X(1)-XBP)+BXX(NXXJ-1)
Z2=AXX(NXXJ-1)*{XN(1)-XBP)+BXX(NXXJ-1)
CALL LTHM( X(1),Y(1),Z1,X(1),Y(1),-Z1,XN(1),YN(1),-Z2,XN(1),
1YN(1),Z2,P(1),P(1),PN(1),PN(1),Q(1),Q(1),QN(1),QN(1),RHO(1),
2RHO(1),RHON(1),RHON(1),R(1),R(1),RN(1),RN(1),W(1),W(1),WN(1),
3WN(1),TH(1),TH(1),THN(1),THN(1),ALPDUM,.25,.25,.25,.25,
4XTHX,YLFT,XMOM,CF,ST,1)

```

```

STU=ST
IF(KSIDE, EQ, 0) GO TO 1798
Z4=AXX(NXXJ-1)*(X(2)-XBP)+BXX(NXXJ-1)
DO 2031 J=1, NSP
2031 ALPDUM(J)=(ALP(J,1)+ALP(J,2))/2.
CALL LTHM(X(1), Y(1), Z1, XN(1), YN(1), Z2, XN(1), YN(1), Z2, X(2), Y(2),
1 Z4, P(1), PN(1), PN(1), P(2), Q(1), QN(1), QN(1), Q(2), RHO(1), RHON(1),
2 RHON(1), RHO(2), R(1), RN(1), RN(1), R(2), W(1), WN(1), WN(1), W(2),
3 TH(1), THN(1), THN(1), TH(2), ALPDUM, .33333, .33333, 0., .33333,
4 XTHS, YLFTS, XMOMS, CF, ST, 3)
STS(1)=ST
1798 IF(B, GT, 0.) GO TO 8049
A=.5
B=.5
GO TO 8000
8049 IF(ISHOC, NE, 1) GO TO 2600
CALL SHOCPT(ISHOC, 3, BET, BETN, A, B)
BET=THN(2)-(BETN-THN(1))
IGG=1
2625 CALL SHOCK(BET, QN(2), THN(2), GAMN(2), EMN(2), RHON(2), PN(2), WN(2),
1 RN(2), QN(1), TH2, GAMN(1), EMN(1), RHON(1), PN(1), WN(1), RN(1), TN(1),
1 XMUN(1), -1.)
ER4=THN(1)-TH2
IF(ABS(ER4).LT, 1, E-04) GO TO 2601
IGG=IGG+1
IF(IGG, GT, 15) GO TO 2627
IF(IGG, GT, 2) GO TO 2628
ER1=ER4
BETP=BET
BET=BET+.02
GO TO 2625
2627 WRITE(6, 2629)
2629 FORMAT(* ERROR IN BETA LOOP IN MAIN*)
STOP
2628 DUMM=BETP-ER1*(BET-BETP)/(ER4-ER1)
ER1=ER4
BETP=BET
BET=DUMM
GO TO 2625
2600 CONTINUE
IF(IFLIP, EQ, 1, AND, XN(1), GT, XFINAL) IHALT=1
IF(XN(1), LE, XCDWL-1, Z-04, AND, XN(1), LE, XXJ1(NXXJ)-1, E-04) GOTO 8060
XNN=XCDWL
IF(XN(1), GT, XXJ1(NXXJ)-1, E-04) XNN=XXJ1(NXXJ)
RAT=(XNN -X(1))/(XN(1)-X(1))
DO 3519 J=1, NSP
ALPN(J, 1)=ALP(J, 1)
3519 ALPDUM(J)=ALP(J, 1)
CALL INT(RAT, X(1), Y(1), TH(1), P(1), Q(1), RHO(1), R(1), W(1), GAM(1),
1 EM(1), XMU(1), T(1),
1 XN(1), YN(1), THN(1), PN(1), QN(1), RHON(1), RN(1), WN(1), GAMN(1),
1 EMN(1), XMUN(1), TN(1),
1 XN(1), YN(1), THN(1), PN(1), QN(1), RHON(1), RN(1), WN(1), GAMN(1),
1 EMN(1), XMUN(1), TN(1), ALPDUM, 1, IEQ)
XN(1)=XNN
XZ=XN(1)-XINTU
L6=5

```

```

IF(XZ,LT,XXU(5))L6=4
IF(XZ,LT,XXU(4))L6=3
IF(XZ,LT,XXU(3))L6=2
IF(XZ,LT,XXU(2))L6=1
YN(1)=AA1(L6,1)*XZ*XZ+AA2(L6,1)*XZ+AA3(L6,1)
THN(1)=ATAN(2,*AA1(L6,1)*XZ+AA2(L6,1))
C *****COMPUTE COWL AND SIDEWALL FORCES *****C
Z1=AXX(NXXJ-1)*(X(1)-XBP)+BXX(NXXJ-1)
Z2=AXX(NXXJ-1)*(XN(1)-XBP)+BXX(NXXJ-1)
CALL LTHM(X(1),Y(1),Z1,X(1),Y(1),-Z1,XN(1),YN(1),-Z2,XN(1),
1YN(1),Z2,P(1),P(1),PN(1),PN(1),Q(1),Q(1),QN(1),QN(1),RHO(1),
2RHO(1),RHON(1),RHON(1),R(1),R(1),RN(1),RN(1),W(1),W(1),WN(1),
3WN(1),TH(1),TH(1),THN(1),THN(1),ALPDUM,,25,,25,,25,,25,
4XTHX,YLFT,XMOM,CF,ST,1)
STU=ST
IF(KSIDE,EQ,0)GO TO 2601
Z4=AXX(NXXJ-1)*(X(2)-XBP)+BXX(NXXJ-1)
DO 2033 J=1,NSP
2033 ALPDUM(J)=(ALP(J,1)+ALP(J,2))/2,
CALL LTHM(X(1),Y(1),Z1,XN(1),YN(1),Z2,XN(1),YN(1),Z2,X(2),Y(2),
1Z4,P(1),PN(1),PN(1),P(2),Q(1),QN(1),QN(1),Q(2),RHO(1),RHON(1),
2RHON(1),RHO(2),R(1),RN(1),RN(1),R(2),W(1),WN(1),WN(1),W(2),
3TH(1),THN(1),THN(1),TH(2),ALPDUM,,33333,,33333,0,,33333,
4XTHS,YLFTS,XMOMS,CF,ST,3)
STS(1)=ST
2601 CONTINUE
ICMPLT=1
IF(XN(1),EQ,XCOWL)XCOWL=1.E+06
IF(IDELG,EQ,1) GO TO 2622
IF(XJ1,EQ,0.,AND,I0VER,EQ,0) GO TO 8060
2622 CONTINUE
IX=1
IF(IFLIP,EQ,1) IX=2
2655 IAA=IAA+1
D=0,
DO 3470 J=1,NSP
ALPDUM(J)=ALPN(J,IX)
3470 ALPF(J,IAA)=ALPN(J,IX)
CALL INT(0.,XN(IX),YN(IX),THN(IX),PN(IX),QN(IX),RHON(IX),
1RN(IX),WN(IX),GAMN(IX),EMN(IX),XMUN(IX),TN(IX),
1D,D,D,D,D,D,D,D,D,D,D,D,D,D,
1XF(IAA),YF(IAA),THF(IAA),PF(IAA),QF(IAA),RHOF(IAA),RF(IAA),
1WF(IAA),GMF(IAA),EMF(IAA),XMUF(IAA),TF(IAA),ALPDUM,0,IEQ)
IF(IX,EQ,1) GO TO 2656
IX=1
GO TO 2655
2656 IF(IFLIP,EQ,1) IAA=IAA-1
ICMPLT=0
NSTAR=0
IF(XN(1)+.0001,GE,XTJ1) XJ1=0,
IF(IFLIP,NE,1 ) NXXJ=NXXJ+1
IF(IFENC1,EQ,1) IFENCE=0
IF(NXXJ,GT,NXXJ1) NXXJ=NXXJ1+1
IF(IFLIP,GT,0) GO TO 2602
IF(ICOWL,EQ,0) GO TO 7593
RP=PM (MM)/PF(IAA)*PIN
IF(RP,GT,1.) GO TO 5989

```

```

7593 NPTS=IAA
      IOVER=0
      IAA=1
      GO TO 7211
5989 CONTINUE
      EEXT=EMINF*QM(MM)/SQRT(TM(MM))
      CALL COWLO(IAA,THM(MM),EEXT,BET,PM (MM))
      XINTU=XINTL
      DO 691 I13=1,5
      XXU(I13)=XXL(I13)
      AA1(I13,1)=AA1(I13,2)
      AA2(I13,1)=AA2(I13,2)
691 AA3(I13,1)=AA3(I13,2)
2602 CONTINUE
      NPTS=IAA+1
      IFLIP=IFLIP+1
      IF(IFLIP.GT,1) XXP=XFINAL
      IAA=1
      LSTT=0
      IOVER=2
      CALL INDATA
      BET=-BET
      ISHOC=1
      GO TO 7211
8060 CONTINUE
      LM=LMAX-1
      IF(IDELG.EQ,1 .AND. IAA.GT,1) LM=1000
      IF(XJ1.GT,0.,AND,IAA.GT,1) LM=1000
      IF(IOVER.EQ,2,AND,LSTT,EQ,1) LM=1000
      LST=0
      LTH=1
      IF(NSTAR,EQ,0)LTH=0
      L=1
      M=0
      IDPT=0
      LWUZ=1000
      XXP=XFINAL
      IF(NSTAR,EQ,1) M=2
      IF(ICMPLT,EQ,2) M=1
C ***** COMPUTE SIDEWALL FORCES ***** C
5520 IF(KSIDE,EQ,0.OR,L,EQ,1)GO TO 5521
      NM=M-1
      LTH=LTH+1
      IF(M,EQ,1)NM=1
      Z1=AXX(NXXJ-1)*(X (NM)-XBP)+BXX(NXXJ-1)
      Z2=AXX(NXXJ-1)*(XN(K )-XBP)+BXX(NXXJ-1)
      Z3=AXX(NXXJ-1)*(XN(L )-XBP)+BXX(NXXJ-1)
      Z4=AXX(NXXJ-1)*(X (M )-XBP)+BXX(NXXJ-1)
      XK1=.25 $XK2=.25 $XK3=.25 $XK4=.25
      IF(M.GT,1)GO TO 683
      XK1=.33333 $XK2=.33333 $XK3=.33333 $XK4=0.
683 CONTINUE
      DO 687 J=1,NSP
687 ALPDUM(J)=XK1*ALP(J,NM)+ALPN(J,K)*XK2+XK3*ALPN(J,L)+XK4*ALP(J,M)
      CALL LTHM(X(NM),Y(NM),Z1,XN(K),YN(K),Z2,XN(L),YN(L),Z3,X(M),Y(M),
1Z4,P(NM),PN(K),PN(L),P(M),Q(NM),QN(K),QN(L),Q(M),RHO(NM),RHON(K),
2RHON(L),RHO(M),R(NM),RN(K),RN(L),R(M),W(NM),WN(K),WN(L),W(M),

```

```

3TH(NM), THN(K), THN(L), TH(M), ALPDUM, XK1, XK2, XK3, XK4,
4XTHS, YLFTS, XMODS, CF, ST, 3)
STS(LTH)=ST
IF(L.EQ.LMAX)GO TO 265
5521 L=L+1
IF(L.GT.LM) GO TO 6520
K=L-1
678 M=M+1
A=1.
B=0.
CALL FUZZY(K,L,M,N,LMAX,KMAX,NPTS,IPP,IFZ)
IF(IFZ.GT.0)GO TO 265
250 CONTINUE
IF(L.EQ.ISHOC+1) CALL SHOCPT(ISHOC,M,BET,BETN,A,B)
IF(L.NE.ISHOC+1.OR.B.EQ.0..OR.IFLIP.NE.1) GO TO 2603
IPL=3
2684 POLYC=-AA3(IPL,1)-YN(L)+TAN(BETN)*(XN(L)-XINTU)
POLYB=-AA2(IPL,1)-TAN(BETN)
POLYA=-AA1(IPL,1)
IF(POLYA.NE.0.)
1XXP =(-POLYB-SQRT(POLYB*POLYB-4.*POLYA*POLYC))/(2.*POLYA)
IF(POLYA.EQ.0.) XXP =-POLYC/POLYB
XXP =XXP +XINTU
IF(XXP .GE.XXU(IPL)) GO TO 2603
IPL=IPL-1
GO TO 2684
2603 CONTINUE
IF(L.EQ.ISHOC+1) GO TO 3003
EM1=XM1(A,B,TH(M),XMU(M),THN(L),XMUN(L))
EM9=EM1
IF(L.EQ.ISHOC) EM1=TAN(BET)
IF(L.EQ.ISHOC.AND.M.GT.1)EM1=TAN(BET+THN(L-1)+XMUN(L-1)-TH(M-1)
1-XMU(M-1))
EM2=XM2(A,B,THN(K),XMUN(K),THN(L),XMUN(L))
XN(L)=(YN(K)-Y(M)+EM1*X(M)-EM2*XN(K))/(EM1-EM2)
YN(L)=Y(M)+EM1*(XN(L)-X(M))
IF(B.GT.0.) GO TO 681
IDROP=0
BETT=BET
IF(M.GT.1.AND.IDOVER.EQ.2)BETT=BET+THN(L-1)+XMUN(L-1)-TH(M-1)-XMU(M
1-1)
IF(L.EQ.ISHOC-1) CALL DRTEST(XN(L),YN(L),EM1,BETT,IDROP,+1,M)
IF(L.EQ.ISHOC+2) CALL DRTEST(XN(L),YN(L),EM1,BETN,IDROP,-1,M)
IF(IDROP.EQ.0) GO TO 681
LMAX=LMAX-1
LM=LM-1
IF(L.LT.ISHOC) ISHOC=ISHOC-1
GO TO 678
681 CONTINUE
IF(L.NE.ISHOC) GO TO 601
YSHOC=Y(M)
XSHOC=X(M)
IF(L.GT.2) GO TO 602
YDUM=YN(L)-EM9*(XN(L)-X(M))
XDUM=X(M)
RAT=(YDUM-Y(M))/(YN(1)-Y(M))
D=0.

```



```

DO 644 J=1,NSP
ALP(J,M)=ALP(J,M)+RAT*(ALPN(J,1)-ALP(J,M))
644 ALPDUM(J)=ALP(J,M)
CALL INT(RAT,D,D,TH(M),P(M),Q(M),RHO(M),R(M),W(M),GAM(M),
1EM(M),XMU(M),T(M),D,D,THN(1),PN(1),QN(1),RHON(1),RN(1),WN(1),
1GAMN(1),EMN(1),XMUN(1),TN(1),D,D,TH(M),P(M),Q(M),RHO(M),R(M),
1W(M),GAM(M),EM(M),XMU(M),T(M),ALPDUM,1,IEQ)
GO TO 601
602 CONTINUE
EM8=XM2(.5,.5,TH(M-1),XMU(M-1),TH(M),XMU(M))
YDUM=(EM9*Y(M)-EM8*YN(L)+EM8*EM9*(XN(L)-X(M)))/(EM9-EM8)
XDUM=XN(L)-(YN(L)-YDUM)/EM9
RAT=(YDUM-Y(M))/(Y(M-1)-Y(M))
D=0.
DO 604 J=1,NSP
ALP(J,M)=ALP(J,M)+RAT*(ALP(J,M-1)-ALP(J,M))
604 ALPDUM(J)=ALP(J,M)
CALL INT(RAT,D,D,TH(M),P(M),Q(M),RHO(M),R(M),W(M),GAM(M),
1EM(M),XMU(M),T(M),D,D,TH(M-1),P(M-1),Q(M-1),RHO(M-1),R(M-1),
1W(M-1),GAM(M-1),EM(M-1),XMU(M-1),T(M-1),D,D,TH(M),P(M),Q(M),
1RHO(M),R(M),W(M),GAM(M),EM(M),XMU(M),T(M),ALPDUM,1,IEQ)
601 CONTINUE
A1=F1(A,B,XMU(M),GAM(M),P(M),XMUN(L),GAMN(L),PN(L))
B1=F1(A,B,XMUN(K),GAMN(K),PN(K),XMUN(L),GAMN(L),PN(L))
XDUMK=XN(K)-XOR(NXXJ-1)
XDUMM=X(M)-XOR(NXXJ-1)
XDUML=XN(L)-XOR(NXXJ-1)
A2=F2(A,B,1.,XJ,XJ1,XDUMM,Y(M),TH(M),XMU(M),XDUML,YN(L),THN(L),XMU
1N(L))
B2=F2(A,B,-1.,XJ,XJ1,XDUMK,YN(K),THN(K),XMUN(K),XDUML,YN(L),THN(L)
1,XMUN(L))
DUM1=-(A2+B2)*XN(L)+A2*X(M)+B2*XN(K)
IF(XJ1.GT.0.)DUM1=-(A2*ALOG(XDUML/XDUMM)+B2*ALOG(XDUML/XDUMK))
DUM=(A1*ALOG(P(M))+B1*ALOG(PN(K))+TH(M)-THN(K)+DUM1)/(A1+B1)
PN(L)=EXP(DUM)
DUM=ALOG(P(M)/PN(L))*A1
DUM2=XN(L)-X(M)
IF(XJ1.NE.0.)DUM2=ALOG(XDUML/XDUMM)
THN(L)=DUM+TH(M)-A2*DUM2
253 CONTINUE
CALL DPOINT(K,L,M,N,NPTS,A,B)
CALL SL(PD,QD,RHD,RD,WD,GAMD,EMD,XMUD,TD,PN(L),QN(L),RHON(L),
1RN(L),WN(L),GAMN(L),EMN(L),XMUN(L),TN(L),ALPDUM,IEQ,A,B)
DO 1502 J=1,NSP
1502 ALPN(J,L)=ALPDUM(J)
3003 CONTINUE
IF(IDPT.EQ.0) GO TO 8400
IF(B.GT.0.) GO TO 8401
A=.5
B=.5
GO TO 253
8400 CONTINUE
IF(B.GT.0.) GO TO 7520
IF(L.NE.1SHOC) GO TO 606
IF(L.GT.2) GO TO 650
RAT=(YN(1)-YSHOC)/(YN(1)-Y(M))
Y(M)=YSHOC

```

```

X(M)=XSHOC
D=0.
DO 655 J=1,NSP
ALP(J,M)=ALP(J,M)+RAT*(ALPN(J,1)-ALP(J,M))
655 ALPDUM(J)=ALP(J,M)
CALL INT(RAT,D,D,TH(M),P(M),Q(M),RHO(M),R(M),W(M),GAM(M),
1EM(M),XMU(M),T(M),D,D,THN(1),PN(1),QN(1),RHON(1),RN(1),WN(1),
1GAMN(1),EMN(1),XMUN(1),TN(1),D,D,TH(M),P(M),Q(M),RHO(M),R(M),
1W(M),GAM(M),EM(M),XMU(M),T(M),ALPDUM,1,IEQ)
GO TO 606
650 CONTINUE
RAT=(Y(M-1)-YSHOC)/(Y(M-1)-Y(M))
Y(M)=YSHOC
X(M)=XSHOC
D=0.
DO 605 J=1,NSP
ALP(J,M)=ALP(J,M)+RAT*(ALP(J,M-1)-ALP(J,M))
605 ALPDUM(J)=ALP(J,M)
CALL INT(RAT,D,D,TH(M),P(M),Q(M),RHO(M),R(M),W(M),GAM(M),
1EM(M),XMU(M),T(M),D,D,TH(M-1),P(M-1),Q(M-1),RHO(M-1),R(M-1),
1W(M-1),GAM(M-1),EM(M-1),XMU(M-1),T(M-1),D,D,TH(M),P(M),Q(M),
1RHO(M),R(M),W(M),GAM(M),EM(M),XMU(M),T(M),ALPDUM,1,IEQ)
606 CONTINUE
A=.5
B=.5
GO TO 250
7520 CONTINUE
IF(IFENCE.EQ.0.OR.XN(1).NE.XCOWLH) GO TO 3108
XXP=(YN(L)-BFENCE)/AFENCE+XBP
IF(XN(L).LT.XXP) GO TO 520
DUM=(YN(L)-YN(K))/(XN(L)-XN(K))
XXP=(AFENCE*XBP-BFENCE-DUM*XN(K)+YN(K))/(AFENCE-DUM)
3108 CONTINUE
IF(IDELG.EQ.1) GO TO 2623
IF(XJ1.EQ.0.AND.IOVER.EQ.0) GO TO 520
2623 CONTINUE
IF(XN(L).LT.XXJ1(NXXJ).AND.XN(L).LT.XXP) GO TO 520
IF(LST.GT.0) GO TO 520
LST=1
XNN=XXP
IF(XN(L).GE.XXJ1(NXXJ)) XNN=XXJ1(NXXJ)
RAT=(XNN-XN(K))/(XN(L)-XN(K))
IAA=IAA+1
IF(IPP.GT.NPTS.OR.IAA.LT.IPP)GO TO 3999
WRITE(6,3998)
3998 FORMAT(* INDEXING IN CHANGE OF ORIGIN OVERLAPS INITIAL DATA IAA EQ
1UALS IPP*)
STOP
3999 XN(L )=XNN
YN(L )=YN(K)+RAT*(YN(L)-YN(K))
THN(L )=THN(K)+RAT*(THN(L)-THN(K))
DUM1=ALOG(PN(K))
DUM2=ALOG(PN(L))
DUM=DUM1+RAT*(DUM2-DUM1)
PN(L )=EXP(DUM)
IDPT=1
A=1.

```

```

      B=0.
      GO TO 253
8401 IDPT=0
      IF(IFENCE, EQ, 0, OR, XN(1), NE, XCOWLH) GO TO 9804
      IF(IAA, LT, 3, OR, XF(1), EQ, XFENCE) GO TO 9804
      WRITE(6, 9805)
9805 FORMAT(* FENCE MAY NOT BE ENTIRELY SUPERSONIC - CHECK FLOW FIELD*)
      STOP
9804 CONTINUE
      DO 8402 J=1, NSP
      ALPDUM(J)=ALPN(J, L)
8402 ALPF(J, IAA)=ALPN(J, L)
      D=0.
      CALL INT(0, , XN(L), YN(L), THN(L), PN(L), , QN(L), RHON(L), RN(L),
1WN(L), GAMN(L), EMN(L), XMUN(L), TN(L),
1D, D, D, D, D, D, D, D, D, D, D, D, D, D, D,
1, XF(IAA), YF(IAA), THF(IAA), PF(IAA), QF(IAA), RHOF(IAA), RF(IAA),
1WF(IAA), GAMF(IAA), EMF(IAA), XMUF(IAA), TF(IAA), ALPDUM, 0, IEQ)
      IF(IAA, EQ, 2, AND, LSTT, EQ, 0) GO TO 520
C ***** COMPUTE SIDEWALL FORCES ***** C
      IF(KSIDE, EQ, 0) GO TO 521
      LT6=LTH+2
      MI=M
      I=M+1
      IF(I, GT, KMAX) GO TO 521
519 Z1=AXX(NXXJ-1)*(X(MI)-XBP)+BXX(NXXJ-1)
      Z2=AXX(NXXJ-1)*(XN(L)-XBP)+BXX(NXXJ-1)
      Z3=AXX(NXXJ-1)*(X(I)-XBP)+BXX(NXXJ-1)
      Z4=Z3
      DO 5363 J=1, NSP
5363 ALPDUM(J)=(ALP(J, MI)+ALPN(J, L)+ALP(J, I))/3.
      CALL LTHM(X(MI), Y(MI), Z1, XN(L), YN(L), Z2, X(I), Y(I), Z3, X(I), Y(I),
1Z4, P(MI), PN(L), P(I), P(I), Q(MI), QN(L), Q(I), Q(I), RHO(MI), RHON(L),
2RHO(I), RHO(I), R(MI), RN(L), R(I), R(I), W(MI), WN(L), W(I), W(I),
3TH(MI), THN(L), TH(I), TH(I), ALPDUM, , 33333, , 33333, , 33333, 0.,
4XTHS, YLFTS, XMOMS, CF, ST, 3)
      STS(LT6)=ST
      IF(I, EQ, KMAX) GO TO 521
      I=I+1
      LT6=LT6+1
      MI=MI+1
      GO TO 519
521 LMAX=L
      LWUZ=LMAX
      IF(KSIDE, EQ, 0) GO TO 265
      GO TO 5520
520 CONTINUE
      IF(XN(L), LT, XXJ1(NXXJ), AND, XN(L), LT, XXP) GO TO 5520
      IF(LSTT, EQ, 0) GO TO 5520
      LMAX=L
      LWUZ=LMAX
      GO TO 265
6520 CONTINUE
      A=1.
      B=0.
      L=LMAX
      KK=KMAX

```

```

      K=LMAX-1
5011 CONTINUE
      IF(B.EQ.0.) THN(L)=TH(KK)
      IB=1
      IER=0
630 CONTINUE
      EMSL=XM3(.5,.5,TH(KK),THN(L))
      EM2=XM2(A,B,THN(K),XMUN(K),THN(L),XMUN(L))
      IF(IDESGN.EQ.0.AND.IFLIP.NE.1)
1CALL BODL(X(KK),Y(KK),TH(KK),XN(K),YN(K),EM2,XN(L),YN(L),THN(L))
      IF(IFLIP.NE.1) GO TO 631
      CALL GEM(X(KK),Y(KK),EMSL,XN(K),YN(K),EM2,XN(L),YN(L))
631 CONTINUE
      B1=F1(A,B, XMUN(K), GAMN(K), PN(K), XMUN(L), GAMN(L), PN(L))
      XDUMK=XN(K)-XOR(NXXJ-1)
      XDUML=XN(L)-XOR(NXXJ-1)
      B2=F2(A,B,-1.,XJ,XJ1,XDUMK,YN(K),THN(K),XMUN(K),XDUML,YN(L),THN(L)
1,XMUN(L))
      DUM1=B2*(XN(L)-XN(K))
      IF(XJ1.GT.0.)DUM1=B2*ALOG(XDUML/XDUMK)
      DUM= (THN(L)-THN(K)-DUM1)/B1
      PN(L)=PN(K)*EXP(DUM)
1821 CONTINUE
      DO 1503 J=1,NSP
      ALPN(J,L)=ALP(J,KK)
1503 ALPDUM(J)=ALPN(J,L)
      CALL SL(P(KK),Q(KK),RHO(KK),R(KK),
1 W(KK),GAM(KK),EM(KK),XMU(KK),T(KK),
1PN(L),QN(L),RHON(L),RN(L),WN(L),GAMN(L),EMN(L),XMUN(L),TN(L),
1ALPDUM,IEQ,A,B)
      IF(B.EQ.0..OR.IFLIP.EQ.1)GO TO 1523
      L1=LMAX
      IF(XN(L1).GT,XXJ1(NXXJ)-1.E-04) GO TO 1523
C ***** COMPUTE FORCES ON LOWER SURFACE AND SIDEWALL *****C
      Z1=AXX(NXXJ-1)*(X (KK)-XBP)+BXX(NXXJ-1)
      Z2=AXX(NXXJ-1)*(XN(L )-XBP)+BXX(NXXJ-1)
      Z3=-Z2
      Z4=-Z1
      CALL LTHM(X(KK),Y(KK),Z1,XN(L),YN(L),Z2,XN(L),YN(L),Z3,X(KK),Y(KK)
1,Z4,P(KK),PN(L),PN(L),P(KK),Q(KK),QN(L),QN(L),Q(KK),RHO(KK),
2RHON(L),RHON(L),RHO(KK),R(KK),RN(L),RN(L),R(KK),W(KK),WN(L),WN(L),
3W(KK),TH(KK),THN(L),THN(L),TH(KK),ALPDUM,.25,.25,.25,.25,XTHX,YLFT
4,XMOM,CF,ST,2)
      STL=ST
      IF(KSIDE.EQ.0)GO TO 1523
      LTH=LTH+1
      DO 1596 J=1,NSP
1596 ALPDUM(J)=(ALP(J,KK)+ALPN(J,K))/2.
      Z1=AXX(NXXJ-1)*(X (KK)-XBP)+BXX(NXXJ-1)
      Z2=AXX(NXXJ-1)*(XN(K )-XBP)+BXX(NXXJ-1)
      Z3=AXX(NXXJ-1)*(XN(L )-XBP)+BXX(NXXJ-1)
      Z4=Z3
      CALL LTHM(X(KK),Y(KK),Z1,XN(K),YN(K),Z2,XN(L),YN(L),Z3,XN(L),YN(L),
1Z4,P(KK),PN(K),PN(L),PN(L),Q(KK),QN(K),QN(L),QN(L),RHO(KK),RHON(K)
2,RHON(L),RHON(L),R(KK),RN(K),RN(L),RN(L),W(KK),WN(K),WN(L),WN(L),
3TH(KK),THN(K),THN(L),THN(L),ALPDUM,.33333,.33333,.33333,0.,
4XTHS,YLFTS,XMOMS,CF,ST,3)

```

```

STS(LTH)=ST
1523 IF(IFLIP,NE,1) GO TO 632
P2=PN(L)/P(KK)
CALL PRM(P2,TH(KK),EMC1 ,TH2T,EMC2,+1)
ER4=TH2T-THN(L)
IF(ABS(ER4).LT,1.E-04) GO TO 632
CALL ERR(IER,IB,THN(L),ER4,1,01,THNL,ER1)
IF(IER,EQ,0)GO TO 166
633 WRITE(6,635)
635 FORMAT(* ERROR IN PM LOOP AT CONTACT IN MAIN*)
STOP
166 IB=IB+1
GO TO 630
632 CONTINUE
IF(B,GT,0.) GO TO1265
A=.5
B=.5
GO TO 5011
1265 IAAS=IAA
IF(IFLIP,EQ,2,AND,XN(L),GE,XFINAL) IHALT=1
IF(IHALT,EQ,1) GO TO 1802
IF(XN(L),GE,XFINAL) GO TO 1802
IF(IDELG,EQ,1) GO TO 3109
IF(XJ1,EQ,0.,AND,IOVER,EQ,0) GO TO 265
IF(IFENCE,EQ,0,OR,XN(1),NE,XCOWLH) GO TO 3109
IF(XN(L),LT,XFENCE) GO TO 265
XNN=XFENCE
GO TO 3110
3109 CONTINUE
IF(XN(L),LT,XXJ1(NXXJ)) GO TO 265
1802 CONTINUE
XNN=XXJ1(NXXJ)
3110 CONTINUE
RAT=(XNN-X(KK))/(XN(L)-X(KK))
IAA=1
LSTT=1
LWUZ=LMAX
XF(IAA)=XNN
IF(IFLIP,EQ,1) GO TO 2605
XCH=XNN -XINTL
LK=5
IF(XCH,LT,XXL(5))LK=4
IF(XCH,LT,XXL(4))LK=3
IF(XCH,LT,XXL(3)) LK=2
IF(XCH,LT,XXL(2)) LK=1
YF(IAA)=AA1(LK,2)*XCH*XCH+AA2(LK,2)*XCH+AA3(LK,2)
THF(IAA)=ATAN(2,*AA1(LK,2)*XCH+AA2(LK,2))
GO TO 2606
2605 YF(IAA)=Y(KK)+RAT*(YN(L)-Y(KK))
THF(IAA)=ATAN(TAN(TH(KK))+RAT*(TAN(THN(L))-TAN(TH(KK))))
2606 CONTINUE
YN(L)=YF(IAA)
THN(L)=THF(IAA)
XN(L)=XF(IAA)
PN(L)=P(KK)+RAT*(PN(L)-P(KK))
QN(L)=Q(KK)+RAT*(QN(L)-Q(KK))
TN(L)=T(KK)+RAT*(TN(L)-T(KK))

```

```

DO 3841 J=1,NSP
ALPF(J,IAA)=ALP(J,KK)
ALPN(J,L)=ALP(J,KK)
ALPDUM(J)=ALPN(J,L)
3841 CONTINUE
CALL SL(P(KK),Q(KK),RHO(KK),R(KK),
1 W(KK),GAM(KK),EM(KK),XMU(KK),T(KK),
1PN(L),QN(L),RHON(L),RN(L),WN(L),GAMN(L),EMN(L),XMUN(L),TN(L),
1ALPDUM,IEQ,.5,.5)
D=0.
CALL INT(0.,XN(L),YN(L),THN(L),PN(L), QN(L),RHON(L),RN(L),
1WN(L),GAMN(L),EMN(L),XMUN(L),TN(L),
1D,D,D,D,D,D,D,D,D,D,D,D,D
1,DUM3 ,DUM1 ,DUM2 ,PF(IAA),QF(IAA),RHOF(IAA),RF(IAA),
1WF(IAA),GAMF(IAA),EMF(IAA),XMU(IAA),TF(IAA),ALPDUM,0,IEQ)
C ***** COMPUTE FORCES ON LOWER SURFACE AND SIDEWALL *****C
Z1=AXX(NXXJ-1)*(X(KK)-XBP)+BXX(NXXJ-1)
Z2=AXX(NXXJ-1)*(XN(L)-XBP)+BXX(NXXJ-1)
Z3=-Z2
Z4=-Z1
CALL LTHM(X(KK),Y(KK),Z1,XN(L),YN(L),Z2,XN(L),YN(L),Z3,X(KK),Y(KK)
1,Z4,P(KK),PN(L),PN(L),P(KK),Q(KK),QN(L),QN(L),Q(KK),RHO(KK),
2RHON(L),RHON(L),RHO(KK),R(KK),RN(L),RN(L),R(KK),W(KK),WN(L),WN(L),
3W(KK),TH(KK),THN(L),THN(L),TH(KK),ALPDUM,.25,.25,.25,.25,XTHX,YLFT
4,XMOM,CF,ST,2)
STL=ST
IF(KSIDE.EQ.0)GO TO 264
LTH=LTH+1
DO 1597 J=1,NSP
1597 ALPDUM(J)=(ALP(J,KK)+ALPN(J,K))/2.
Z1=AXX(NXXJ-1)*(X(KK)-XBP)+BXX(NXXJ-1)
Z2=AXX(NXXJ-1)*(XN(K)-XBP)+BXX(NXXJ-1)
Z3=AXX(NXXJ-1)*(XN(L)-XBP)+BXX(NXXJ-1)
Z4=Z3
CALLLTHM(X(KK),Y(KK),Z1,XN(K),YN(K),Z2,XN(L),YN(L),Z3,XN(L),YN(L),
1Z4,P(KK),PN(K),PN(L),PN(L),Q(KK),QN(K),QN(L),QN(L),RHO(KK),RHON(K)
2,RHON(L),RHON(L),R(KK),RN(K),RN(L),RN(L),W(KK),WN(K),WN(L),WN(L),
3TH(KK),THN(K),THN(L),THN(L),ALPDUM,.33333,.33333,.33333,0.,
4XTHS,YLFTS,XMOMS,CF,ST,3)
STS(LTH)=ST
264 IAA=IAAS
265 CONTINUE
C IF(PN(LMAX).LE.PEN.AND.IDESGN.EQ.1) GO TO 7634
CALL WUZZY(N,NPTS,KMAX,LMAX,IPP,IFZ,LWUZ)
KMAX=LMAX
BET=BETN
EMC1=EMC2
D=0.
DO 270 K=1,KMAX
DO 271 J=1,NSP
271 ALP(J,K)=ALPN(J,K)
DO 1504 J=1,NSP
1504 ALPDUM(J)=ALP(J,K)
CALL INT(0.,XN(K),YN(K),THN(K),PN(K),QN(K),RHON(K),RN(K),WN(K),
1GAMN(K),EMN(K),XMUN(K),TN(K),
1D,D,D,D,D,D,D,D,D,D,D,D,D
1,X(K),Y(K),TH(K),P(K),Q(K),RHO(K),R(K),W(K),GAM(K),

```

```

1EM(K),XMU(K),T(K),ALPDUM,0,IEQ)
270 CONTINUE
LMAX=KMAX
7266 IF(N=NSPTS) 7201,7202,500
7201 N=N+1
GO TO 500
7202 CONTINUE
NSTAR=1
N=N+1
GO TO 500
9123 KTEST=KMAX/2
KTEST1=(KMAX-1)/2
KT3=KMAX-1
IF(KTEST,EQ,KTEST1) KT3=KMAX
I=0
DO 6412 L=1,KT3,2
I=I+1
D=0.
DO 6414 J=1,NSP
ALPDUM(J)=ALP(J,L)
6414 ALP(J,I)=ALP(J,L)
CALL INT(0.,X(L),Y(L),TH(L),P(L),Q(L),RHO(L),R(L),W(L),GAM(L),
1EM(L),XMU(L),T(L),
1D,D,D,D,D,D,D,D,D,D,D,D,D
1,X(I),Y(I),TH(I),P(I),Q(I),RHO(I),R(I),W(I),GAM(I),EM(I),
1XMU(I),T(I),ALPDUM,0,IEQ)
6412 CONTINUE
IF(KTEST,EQ,KTEST1) GO TO 6413
I=I+1
L=KMAX
D=0.
DO 6415 J=1,NSP
ALPDUM(J)=ALP(J,L)
6415 ALP(J,I)=ALP(J,L)
CALL INT(0.,X(L),Y(L),TH(L),P(L),Q(L),RHO(L),R(L),W(L),GAM(L),
1EM(L),XMU(L),T(L),
1D,D,D,D,D,D,D,D,D,D,D,D,D
1,X(I),Y(I),TH(I),P(I),Q(I),RHO(I),R(I),W(I),GAM(I),EM(I),
1XMU(I),T(I),ALPDUM,0,IEQ)
6413 KMAX=KMAX/2+1
LMAX=KMAX
GO TO 6060
END

```

```

SUBROUTINE INDATA
COMMON/HOT/AH(3),BH(3),CH(3),XSTR,PR,REC,REIN,RT,SH,ITW,IVIS
COMMON/VISF/XVTHX,YVLFT,XVMOM
COMMON/COWL/ICOWL,MM,XM(9),YM(9),PM(9),WM(9),RHM(9),THM(9),GM(9),
1RM(9),TM(9),GM(9),XMUM(9),EMM(9),ALPM(7,9),CPXM(9)
COMMON/SHAPE/A1(5,2),A2(5,2),A3(5,2),XXU(5),XXL(5),XINTU,XINTL
COMMON/LTM/XSHFT,YSHFT,XTHX,YLFT,XMOM,XTHS,YLFTS,XMOMS,KSIDE
COMMON/XXJ/NXXJ1,XXJ1(6),AXX(6),BXX(6),XOR(6)
COMMON/XFINAL/XFINAL
COMMON /SP/ NSP
COMMON/A/ TIN,CPIN,RO
COMMON/B/ WTMOLE
COMMON/D/ GAMINF,EMINF,RINF,WINF
COMMON/F/A9,B9,IBOD,XWF,NBOD,YEND
COMMON/ETX/XJ,XJ1,NPTS,IO,IREFL,ICHEM,IPUNCH,IDESGN,IR,NXX,XBP,
1YBP,THBP,RAD,XBOD,YBOD,THBOD,RADB,XEND,THEND,RTH,YEXIT,THST,TEST,
1IRFL,YO,RADB2,RRAD(20), NSTAR,YNQZ,EIN, PEN,H16,H17
COMMON/XF/XF(200),YF(200),PF(200),QF(200),TF(200),THF(200),ALPF(
110,200)
COMMON/X/ X(200),Y(200),P(200),Q(200),T(200),TH(200),ALP(10,200)
COMMON/XCOWL/XCOWL
COMMON/FVAR/
1RHOF(200),CPXF(200),EMF(200),XMUF(200),WF(200),RF(200),GAMF(200),
2XMASSF(200), HF(200),SF(200),ALPD(10),
3THETA(20)
COMMON/VAR/RHO(200),
1EM(200),XMU(200),CPX(200),W(200),R(200),GAM(200),XMASS(200),
2 XN(200),YN(200),QN(200),TN(200),PN(200),THN(200),RHON
3(200),EMN(200),XMUN(200),CPXN(200),WN(200),RN(200),GAMN(200),
4XMASSN(200),ALPN(10,200),SI(10),HI(10),TEMP(20)
5,ALPDUM(10)
COMMON/IEQ/IEQ,PIN,RHOINF,UINF,PINF
COMMON/IDEAL/IDEAL,GAMEY,XMWT ,CPI
COMMON /IOVER/ IOVER
COMMON/XTJ1/XTJ1
COMMON/FENCE/IFENCE,AFENCE,BFENCE,XFENCE
DIMENSION WTMOLE(10),TYPE(6),TYPE1(4),TYPE2(2),TYPE5(4),TYPE4(4)
DATA TYPE2 /10H NOZZLE ,10HCENTERBODY/
DATA TYPE1/10HHYDROGEN A,10HHYDROCARBO,2HIR,5HN AIR/
DATA TYPE/10HTWO DIMENS,10HAXISYMMETR,10HLINE SOURC,5HIDNAL,5HIC
1 ,5HE /
DATA TYPE5/10HF L O W ,10H D E S ,9HF I E L D,9H I G N /
DATA TYPE4/10HFROZEN ,10HEQUILIBRIU,1H ,1HM/
DATA XXU/5*1.E+06/,XXL/5*1.E+06/,END/1.E+06/
DATA IOVER/0/
THST=.02
IF(IOVER.EQ.2) GO TO 916
IO=0
IREFL=0
IPUNCH=0
IDESGN=0
ICHEM=0
READ(5,6895)J1,J2,NPTS,IEQ,ICOWL,IOVER,MM,IDEAL
READ(5,6895)KSIDE,IVIS,ITW
5100 NSP=7
READ(5,63) XBP,XBOD,XCOWL,RTH,TEST,XFINAL,XTJ1
6895 FORMAT(16I5)

```



```

READ(5,63) XSHFT,YSHFT,XTHX,YLFT,XMOM
READ(5,63) XTHS,YLFTS, XMOMS, XVTHX, YVLF1, XVMOM
READ(5,6895) NXXJ1
DO 9393 I=1,NXXJ1
9393 READ(5,9463) XXJ1(I),AXX(I),BXX(I),XOR(I)
9463 FORMAT(4E10.0)
READ(5,4) IFENCE,AFENCE,BFENCE,XFENCE
4 FORMAT(15,5X3E10.0)
XXJ1(NXXJ1+1)=XFENCE
AXX(NXXJ1+1)=AXX(NXXJ1)
BXX(NXXJ1+1)=BXX(NXXJ1)
XOR(NXXJ1+1)=XOR(NXXJ1)
IF(IFENCE.EQ.0) GO TO 321
XXJ1(NXXJ1+2)=XFENCE
AXX(NXXJ1+2)=AXX(NXXJ1)
BXX(NXXJ1+2)=BXX(NXXJ1)
XOR(NXXJ1+2)=XOR(NXXJ1)
321 CONTINUE
XINTU=XP
XINTL=XBOD
READ(5,6895) NUWSEG,NLWSEG
READ(5,6363) (XXU(L),A1(L,1),A2(L,1),A3(L,1),L=1,NUWSEG)
READ(5,6363) (XXL(L),A1(L,2),A2(L,2),A3(L,2),L=1,NLWSEG)
6363 FORMAT(4E10.0)
3531 WRITE(6,7329) TYPE5(IDESGN+1),TYPE5(IDESGN+3)
7329 FORMAT( 41X*NOZZLE = CENTERBODY //50XA10,A9)
JP1=J1+1+2*J2
JP2=JP1+3
WRITE(6,7330) TYPE(JP1),TYPE(JP2),TYPE1(ICHEM+1)
1,TYPE1(ICHEM+3),NPTS,RTH
7330 FORMAT( /37X,*FLOW NONUNIFORM GAS FLOW
2*/// 10X,*TYPE OF FLOW IS *,A10,A5,* FOR *,
3A10,A5/10X,*NUMBER OF POINTS ON INITIAL DATA LINE IS *,I3/10X,
4*THROAT RADIUS (RTH) = *,E13.5)
WRITE(6,5001) TYPE4(IEQ+1),TYPE4(IEQ+3)
5001 FORMAT(
110X*CHEMISTRY IS *A10,A1)
WRITE(6,7500) XCOWL,XFINAL
7500 FORMAT(10X*COWL TRAILING EDGE IS *E13.5/10X*AXIAL COORDINATE OF EN
1D OF RUN IS *E13.5)
IF(J2.EQ.0) GO TO 7510
WRITE(6,7501) XTJ1
7501 FORMAT(10X*AXIAL COORDINATE OF START OF CARTESIAN SYSTEM IS *E13.5
1)
WRITE(6,7502)
7502 FORMAT(//25X*LINE SOURCE COORDINATES*)
WRITE(6,7505)
DO 7503 I=1,NXXJ1
7503 WRITE(6,7504) XXJ1(I),XXJ1(I+1),AXX(I),BXX(I),XOR(I)
7504 FORMAT(10X,4E11.3,5X,E11.3)
7505 FORMAT(15X*X*4X*TU*4X*X*11X*COORDINATES*12X*ORIGIN X*)
7510 CONTINUE
WRITE(6,2020)
2020 FORMAT(//25X*UPPER WALL COORDINATES*)
WRITE(6,2071)
2071 FORMAT(15X*X*4X*TD*4X*X*15X*COORDINATES*)
2042 FORMAT(10X,5E11.3)

```

```

DO 2050 I=1,NUWSEG
IF(I.EQ.5)GO TO 2051
WRITE(6,2042) XXU(I),XXU(I+1),A1(I,1),A2(I,1),A3(I,1)
GO TO 2050
2051 WRITE(6,2042) XXU(I),END      ,A1(I,1),A2(I,1),A3(I,1)
2050 CONTINUE
WRITE(6,2010)
2010 FORMAT(/25X+LOWER WALL COORDINATES*)
WRITE(6,2071)
DO 2040 I=1,NLWSEG
IF(I.EQ.5)GO TO 2041
WRITE(6,2042) XXL(I),XXL(I+1),A1(I,2),A2(I,2),A3(I,2)
GO TO 2040
2041 WRITE(6,2042) XXL(I),END      ,A1(I,2),A2(I,2),A3(I,2)
2040 CONTINUE
DO 7373 L=1,NUWSEG
7373 XXU(L)=XXU(L)-XINTU
DO 7374 L=1,NLWSEG
7374 XXL(L)=XXL(L)-XINTL
READ(5,63) EMINF,TIN,WINF,PINF
IF(IDEAL.EQ.1)READ(5,63)GAMEY,XMWT
IF(IDEAL.EQ.1)IEQ=1
DO 5002 I=1,NPTS
DO 5002 J=1,NSP
5002 ALPF(J,I)=0.
READ(5,6364) (XF(I),YF(I),PF(I),QF(I),TF(I),THF(I),WF(I),I=1,NPTS)
IF(IEQ.EQ.0)
1 READ(5,6364) ((ALPF(J,I),J=1,NSP),I=1,NPTS)
6364 FORMAT(7E10.0)
IF(ICOWL.EQ.0)GO TO 7511
READ(5,6364)XM(MM),YM(MM),PM(MM),QM(MM),TM(MM),THM(MM),WM(MM)
DO 6186 J=1,NSP
6186 ALPM(J,MM)=0.
7511 CONTINUE
IF(ICOWL.EQ.1)WRITE(6,5005)MM,PM(MM),QM(MM),TM(MM),THM(MM),WM(MM)
5005 FORMAT(/20X*DATA AT COWL*/10X*NUMBER OF POINTS IN PRANDTL-MEYER F
1AN IS *I2/10X*PRESSURE           **E13.5/10X*VELOCITY           **E
113.5/10X*TEMPERATURE           **E13.5/10X*FLOW INCLINATION  **E13.5/
110X*FUEL TO AIR RATIO **E13.5)
IF(IVIS.EQ.0)GO TO 832
READ(5,63)XSTR,PR,REC,REIN,SH
IF(ITW.GT.0)GO TO 832
DO 831 L=1,3
831 READ(5,63)AH(L),BH(L),CH(L)
832 CONTINUE
IF(IREFL.EQ.0) GO TO 4000
916 CONTINUE
DO 4005 I=1,NPTS
II=NPTS-I+1
X(II)=XF(I)
Y(II)=-YF(I)
Q(II)=QF(I)
T(II)=TF(I)
P(II)=PF(I)
TH(II)=-THF(I)
R(II)=RF(I)
W(II)=WF(I)

```

```

DD 4910 J=1,NSP
4010 ALP(J,II)=ALPF(J,I)
4005 CONTINUE
DO 4006 I=1,NPTS
XF(I)=X(I)
YF(I)=Y(I)
QF(I)=Q(I)
TF(I)=T(I)
PF(I)=P(I)
THF(I)=TH(I)
RF(I)=R(I)
WF(I)=W(I)
DO 4007 J=1,NSP
4007 ALPF(J,I)=ALP(J,I)
4006 CONTINUE
DUM=-YBP
YBP=-YBOD
YBOD=DUM
DUM=-THBP
THBP=-THBOD
THBOD=DUM
YEND=-YEND
THEND=-THEND
IF(IOVER,EQ,2) RETURN
4000 CONTINUE
XJ=J1
XJ1=J2
WTMOLE(1)=1.008
WTMOLE(2)=16.
WTMOLE(3)=18.016
WTMOLE(4)=2.016
WTMOLE(5)=32.0
WTMOLE(6)=17.008
WTMOLE(7)=28.014
WTMOLE(8)=44.011
WTMOLE(9)=28.011
WTMOLE(10)=44.1
RO=1.987
CALL COEFF(5,TIN,AZ,BZ,CZ,DZ,EZ,FZ,GZ)
CPIN=(AZ+BZ*TIN+CZ*TIN**2+DZ*TIN**3+EZ*TIN**4)*RO/WTMOLE(5)
CALL COEFF(7,TIN,AZ,BZ,CZ,DZ,EZ,FZ,GZ)
CPII=(AZ+BZ*TIN+CZ*TIN**2+DZ*TIN**3+EZ*TIN**4)*RO/WTMOLE(7)
RINF=RO/WINF
CPIN=.232*CPIN+.768*CPII
GAMINF=1./(1.-RINF/CPIN)
GAMINF=1.4
EINF=(GAMINF-1.) * EMINF**2
PIN=1./GAMINF/EMINF**2
IF(IDEAL,EQ,1)CPI=49712.52*GAMEY/(GAMEY- 1.)/XMWT
WRITE(6,6899) EMINF,TIN,WINF,PINF
6899 FORMAT(/ / 50X,*INFINITY CONDITIONS*/50X,*-----/
1/40X,*VACH -----*,E13.5/40X,*TEMPERATURE (DEGREES
2 K) ---*,E13.5/40X,*MOLECULAR WEIGHT -----*,E13.5/40X
1*PRESSURE (PSF) -----*E13.5)
WRITE(6,6723)
6723 FORMAT(/ //40X,*OUTPUT VARIABLES ARE*/40X,*NONDIMENSIONALIZED*/
140X,*AS FOLLOWS --//40X,*X BY RTH*/40X,*Y BY RTH*/40X,*Q BY FREE S

```

```

2STREAM VELOCITY*/40X,*T BY FREE STREAM TEMPERATURE*/40X,*P BY FREE
3STREAM PRESSURE*)
IF(IEQ,EQ,0) WRITE(6,5003)
5003 FORMAT( /40X,*ALP(J) IS MASS FRACTION OF SPECIES J*)
DO 6897 I=1,NPTS
PF(I)=PF(I)*PIN
6897 CONTINUE
IF(ICOWL,EQ,1)PM(MM)=PM(MM)*PIN
UINF=1716.*TIN*1.8/PIN
RHOINF= PINF/TIN/1.8/1716.
H16=GAMINF/WINF/2.*EMINF*EMINF
H17=1./H16
63 FORMAT(8E10.0)
PINF=PINF/2116.
DO 4321 I=1,NPTS
DO 83 J=1,NSP
83 ALPDUM(J)=ALPF(J,I)
CALL ALL (PF(I),QF(I),RHO(I),RF(I),WF(I),GAMF(I),EMF(I),
1XMUF(I),TF(I),ALPDUM,IEQ,1)
4321 CONTINUE
IF(ICOWL,EQ,0)RETURN
IDEALS=0
IEQS=IEQ
CPIS=CPIN
GAMES=GAMINF
XMWS=WINF
IF(IDEAL,NE,1)GOTO 717
IDEALS=IDEAL
GAMES=GAMEY
CPIS=CPI
XMWS=XMWT
717 CPI=CPIN*25.02006*1.E+03
GAMEY=GAMINF
IDEAL=1
IEQ=1
XMWT=WINF
DO 84 J=1,NSP
84 ALPDUM(J)=ALPM(J,MM)
CALL ALL (PM(MM),QM(MM),RHM(MM),RM(MM),WM(MM),GM(MM),EMM(MM),
1XMUM(MM),TM(MM),ALPDUM,IEQ,1)
IEQ=IEQS
IDEAL=IDEALS
GAMEY=GAMES
CPI=CPIS
XMWT=XMWS
RETURN
END

```

```

SUBROUTINE COEFF(I,T,A ,B ,C ,D ,E ,F ,G )
IF(T=1000)10,10,20
10 GO TO (15,16,13,11,12,17,14,18,19),I
11 A = 2,8460849E 00
   B = 4,1932116E-03
   C =-9,6119332E-06
   D = 9,5122662E-09
   E =-3,3093421E-12
   F =-9,6725372E 02
   G =-1,4117850E 00
   GO TO 40
12 A = 3,7189946E 00
   B =-2,5167288E-03
   C = 8,5837353E-06
   D =-8,2998716E-09
   E = 2,7082180E-12
   F =-1,0576706E 03
   G = 3,9080704E 00
   GO TO 40
13 A = 4,1565016E 00
   B =-1,7244334E-03
   C = 5,6982316E-06
   D =-4,5930044E-09
   E = 1,4233654E-12
   F =-3,0288770E 04
   G =-6,8616246E-01
   GO TO 40
14 A = 3,6916148E 00
   B =-1,3332552E-03
   C = 2,6503100E-06
   D =-9,7688341E-10
   E =-9,9772234E-14
   F =-1,0628336E 03
   G = 2,2874980E 00
   GO TO 40
15 A = 2,5000000E 00
   B = 0,0
   C = 0,0
   D = 0,0
   E = 0,0
   F = 2,5470497E 04
   G =-4,6001096E-01
   GO TO 40
16 A = 3,0218894E 00
   B =-2,1737249E-03
   C = 3,7542203E-06
   D =-2,9947200E-09
   E = 9,0777547E-13
   F = 2,9137190E 04
   G = 2,6460076E 00
   GO TO 40
17 A = 3,8234708E 00
   B =-1,1187229E-03
   C = 1,2466819E-06
   D =-2,1035896E-10
   E =-5,2546551E-14
   F = 3,5852787E 03

```

G = 5.8253029E-01  
GO TO 40  
18 A=2.1701  
B=1.0378115E-02  
C=-1.0733938E-05  
D=6.3459175E-09  
E=-1.6280701E-12  
F=-4.8352602E+04  
G=1.0664388E+01  
GO TO 40  
19 A=3.7871332  
B=-2.1709526E-03  
C=5.0757337E-06  
D=-3.4737726E-09  
E=7.7216841E-13  
F=-1.4363508E+04  
G=2.6335459  
GO TO 40  
20 GO TO (25,26,23,21,22,27,24,28,29),I  
21 A = 3.0436897E 00  
B = 6.1187110E-04  
C =-7.3993551E-09  
D =-2.0331907E-11  
E = 2.4593791E-15  
F =-8.5491002E 02  
G =-1.6481339E 00  
GO TO 40  
22 A = 3.5976129E 00  
B = 7.8145603E-04  
C =- 2.2386670E-07  
D = 4.2490159E-11  
E: =-3.3460204E-15  
F =-1.1927918E 03  
G = 3.7492659E 00  
GO TO 40  
23 A = 2.6707532E 00  
B = 3.0317115E-03  
C =-8.5351570E-07  
D = 1.1790853E-10  
E =-6.1973568E-15  
F =-2.9888994E 04  
G = 6.8838391E 00  
GO TO 40  
24 A = 2.8545761E 00  
B = 1.5976316E-03  
C =-6.2566254E-07  
D = 1.1315849E-10  
E =-7.6897070E-15  
F =-8.9017445E+02  
G = 6.3902879E 00  
GO TO 40  
25 A = 2.5000000E 00  
B = 0.0  
C = 0.0  
D = 0.0  
E = 0.0  
F = 2.5470497E 04

G = -4.6001096E-01  
GO TO 40  
26 A = 2.5372567E 00  
C = -8.8017921E-09  
D = 5.9643621E-12  
E = -5.5743608E-16  
F = 2.9230007E 04  
G = 4.9467942E 00  
GO TO 40  
27 A = 2.8895544E 00  
B = 9.9835061E-04  
C = -2.1879904E-07  
D = 1.9802785E-11  
E = -3.8452940E-16  
F = 3.8811792E 03  
G = 5.5597016E 00  
GO TO 40  
28 A=4.4129266  
B=3.1922896E-03  
C=-1.297823E-06  
D=2.4147446E-10  
E=-1.6742986E-14  
F=-4.8944043E+04  
G=-7.2875769E-01  
GO TO 40  
29 A=2.9511519  
B=1.55255767E-03  
C=-6.1911411E-07  
D=1.1350336E-10  
E=-7.7882732E-15  
F=-1.4231827E-04  
G=6.531445  
40 RETURN  
END

```

SUBROUTINE ALL(P,Q,RH,R,W,GAM,EM,XMU,T,ALPDUM,IEQ,I66)
COMMON/IEQ/IEB, PIN, RHGINF, UINF, PINF
COMMON/A/ TIN, CPIN, RO
COMMON/D/ GAMINF, EMINF, RINF, WINF
COMMON/B/ WTMOLE
COMMON /SP/ NSP
COMMON /ENTH/ HX
DIMENSION H1(10), CP1(10), ALPDUM(10), WTMOLE(10)
CPX=0.
IF(IEQ, EQ, 1) GO TO 69
WX=0.
CPX=0.
HX=0.
DO 10 J=1, NSP
10 WX=WX+ALPDUM(J)/WTMOLE(J)
W=1./WX
IF(I66, EQ, 1) RH=P*W*EMINF**2*GAMINF/RO/T/WINF
IF(I66, EQ, 0)
1T=P*W*EMINF**2*GAMINF/RO/RH/WINF
CALL THERMD(T, H1, CP1, DUM)
DO 20 J=1, NSP
CPX=CPX+ALPDUM(J)*CP1(J)
HX=HX+ALPDUM(J)*H1(J)
20 CONTINUE
IF(I66, EQ, 1) R=HX+Q*Q/2.
IF(I66, EQ, 0)
1Q=SQRT(2.*(R-HX))
GAM=CPX/(CPX+RO/W/CPIN)
A=GAM*P/RH
A=SQRT(A)
EM=Q/A
XMU=ASIN(1./EM)
RETURN
69 CONTINUE
IER=0
IT=1
IF(I66, EQ, 0) GO TO 40
HX=FH(P, W, T)
R=HX+Q*Q/2.
RH=RHEQ(HX, P, W, T)
GO TO 45
40 HX=R-Q**2/2.
RHT=RHEQ(HX, P, W, T)
ER=(RH-RHT)/RH
IF(ABS(ER).LT.1.E-03) GO TO 45
CALL ERR(IER, IT, Q, ER, 1.01, Q1, ER1)
IF(IER, EQ, 1) GO TO 102
IT=IT+1
GO TO 40
45 GAM=FGAM(T, P, W)
A=SQRT(GAM*P/RH)
EM=Q/A
XMU=ASIN(1./EM)
RETURN
102 WRITE(6, 105)
105 FORMAT(* TOO MANY ITERATIONS IN ALL *)
STOP

```



```

SUBROUTINE BODL(XI,YI,THI,XL,YL,EM2,XN,YN,THN)
COMMON/SHAPE/A1(5,2),A2(5,2),A3(5,2),YXU(5),XYL(5),XINTU,XINTL
XI=XI-XINTL
XL=XL-XINTL
ICK=1
IER=0
L=5
ASL=TAN(THI)
XN=(YI-YL+XL*EM2-XI*ASL)/(EM2-ASL)
5 CONTINUE
IF(XN.LT.XXL(5)) L=4
IF(XN.LT.XXL(4)) L=3
IF(XN.LT.XXL(3)) L=2
IF(XN.LT.XXL(2)) L=1
YN=A1(L,2)*XN*XN+A2(L,2)*XN+A3(L,2)
YT=YL+(XN-XL)*EM2
ER=(YN-YT)
IF(ABS(ER).LT.1.E-04) GO TO 10
CALL ERR(IER,ICK,XN,ER,1.01,XN1,ER1)
IF(IER.EQ.0)GO TO 350
WRITE(6,3512)
3512 FORMAT(* TOO MANY ITERATIONS IN BODL*)
STOP
350 L=5
ICK=ICK+1
GO TO 5
10 THN=ATAN(2.*A1(L,2)*XN+A2(L,2))
XI=XI+XINTL
XL=XL+XINTL
XN=XN+XINTL
RETURN
END

```

```

SUBROUTINE BODU(XI, I, THI, XL, YL, EM1, X, Y, TH)
COMMON/SHAPE/A1(5,2), A2(5,2), A3(5,2), XXU(5), XXL(5), XINTU, XINTL
XI=XI-XINTU
XL=XL-XINTU
X=X-XINTU
ICK=1
IER=0
5 L=5
IF(X,LT,XXU(5)) L=4
IF(X,LT,XXU(4)) L=3
IF(X,LT,XXU(3)) L=2
IF(X,LT,XXU(2)) L=1
Y=A1(L,1)*X*X+A2(L,1)*X+A3(L,1)
YT=YL+(X-XL)*EM1
ER=(Y-YT)
IF(ABS(ER),LT,1.E-04)GO TO 10
CALL ERR(IER,ICK,X,ER,1.01,XN1,ER1)
IF(IER,EQ,0)GO TO 350
WRITE(6,3512)
3512 FORMAT(1X, * TOO MANY ITERATIONS IN BODU *)
STOP
350 CONTINUE
ICK=ICK+1
GO TO 5
10 TH=ATAN(2, *A1(L,1)*X+A2(L,1))
XI=XI+XINTU
XL=XL+XINTU
X=X+XINTU
RETURN
END

```

```

SUBROUTINE COWL(OPT)
COMMON/COWL/ICOWL,MM,XM(9),YM(9),PM(9),WM(9),RHM(9),THM(9),QM(9),
1RM(9),TM(9),GM(9),XMUM(9),EMM(9),ALPM(7,9),CPXM(9)
COMMON/IEQ/IEQ,PIN,RHOINF,UINF,PINF
COMMON/VAR/RHO(200),
1EM(200),XMU(200),CPX(200),W(200),R(200),GAM(200),XMASS(200),
2      XN(200),YN(200),QN(200),TN(200),PN(200),THN(200),RHON
3(200),EMN(200),XMUN(200),CPXN(200),WN(200),RN(200),GAMN(200),
4XMASSN(200),ALPN(10,200),SI(10),HI(10),TEMP(20)
5,ALPDUM(10)
COMMON /SP/ NSP
COMMON/X/ X(200),Y(200),P(200),Q(200),T(200),TH(200),ALP(10,200)
COMMON/A/ TIN,CPIN,RO
COMMON/D/ GAMINF,EMINF,RINF,WINF
COMMON/C1/ EMC1,TC1,QC1
COMMON/IDEAL/IDEAL,GAMEY,XMWT ,CPI
COMMON/ICU/EMC2
DO 4385 J=1,NSP
4385 ALPDUM(J)=ALPM(J,MM)
IER=0
ITT=1
BET=(THM(MM)-OPT*XMUM(MM)+TH(1))*1.1
IFAN=MM*3
3 CONTINUE
IDEALS=0
IEQS=IEQ
CPIS=CPIN
GAMES=GAMINF
XMWS=WINF
IF(IDEAL,NE,1)GOTO 717
IDEALS=IDEAL
GAMES=GAMEY
CPIS=CPI
XMWS=XMWT
717 CPI=CPIN*25.02006*1.E+03
GAMEY=GAMINF
IDEAL=1
IEQ=1
XMWT=WINF
II=MM-1
CALL SHOCK(BET,QM(MM),THM(MM),GM(MM),EMM(MM),RHM(MM),PM(MM),
1RM(MM),WM(MM),TM(MM),XMUM(MM),
2QM(II),THM(II),GM(II),EMM(II),RHM(II),PM(II),RM(II),WM(II),
3TM(II),XMUM(II),ALPDUM,1.,IEQ)
XM(II)=XM(MM)
YM(II)=YM(MM)
EMC2=EMM(II)
EMC1=EMM(II)
DO 4386 J=1,NSP
4386 ALPM(J,II)=ALPDUM(J)
KK=II-1
D=0.
CALL INT(0.,XM(II),YM(II),THM(II),PM(II),QM(II),RHM(II),RM(II),
1WM(II),GM(II),EMM(II),XMUM(II),TM(II),
1D,D,D,D,D,D,D,D,D,D,D,D,D
1,XM(KK),YM(KK),THM(KK),PM(KK),QM(KK),RHM(KK),RM(KK),WM(KK),
1GM(KK),EMM(KK),XMUM(KK),TM(KK),ALPDUM,0,IEQ)

```

```

IEQ=IEGS
IDEAL=IDEALS
GAMEY=GAMES
CPI=CPIS
XMWT=XWWS
DP=(P(1)-PM(II))/FLOAT(IFAN-1)
II=1
DO 4387 J=1,NSP
ALPM(J,II)=ALP(J,1)
4387 ALPDUM(J)=ALP(J,1)
D=0.
CALL INT(0.,X(1),Y(1),TH(1),P(1),Q(1),RHO(1),R(1),W(1),GAM(1),
1EM(1),XMU(1),T(1),
1D,D,D,D,D,D,D,D,D,D,D,D,D
1,XM(II),YM(II),THM(II),PM(II),QM(II),RHM(II),RM(II),WM(II),
1 GM(II),EMM(II),XMUM(II),TM(II),ALPDUM,0,IEQ)
DO 12 LL=2,IFAN
N=LL
KK=N-1
XM(N)=XM(KK)
YM(N)=YM(KK)
PM(N)=PM(KK)-DP
DO 4388 J=1,NSP
4388 ALPM(J,N)=ALPDUM(J)
A=1.
B=0.
CALL SL(PM(KK),QM(KK),RHM(KK),RM(KK),WM(KK),GM(KK),EMM(KK),
1XMUM(KK),TM(KK),PM(N),QM(N),RHM(N),RM(N),WM(N),GM(N),EMM(N),
1XMUM(N),TM(N),ALPDUM,IEQ,A,B)
A1=.5*(GM(N)/SIN(XMUM(N))/COS(XMUM(N))+GM(KK)/SIN(XMUM(KK))/COS
1(XMUM(KK)))
ALNR=ALOG(PM(N)/PM(KK))
THM(N)=THM(KK)+OPT*ALNR/A1
12 CONTINUE
ER4=THM(IFAN)-THM(IFAN+1)
IF(ABS(ER4).LT.1.E-04) GO TO 15
CALL ERR(IER,ITT,BET,ER4,1.05,BET1,ER41)
IF(IER.EQ.1)GO TO 102
ITT=ITT+1
GO TO 3
102 WRITE(6,203)
203 FORMAT(* ERROR IN BETA LOOP IN COWL*)
STOP
15 CONTINUE
WRITE(6,85)BET
85 FORMAT(1X,E13.5)
WRITE(6,86)(K,PM(K),QM(K),TM(K),THM(K),RHM(K),XMUM(K),K=1,MM)
86 FORMAT(1X,I5,6E13.5)
RETURN
END

```

```

SUBROUTINE COWLO(I,THM,EM,BET,PMM)
COMMON/FVAR/
1RHOF(200),CPXF(200),EMF(200),XMUF(200),WF(200),RF(200),GAMF(200),
2XMASSF(200),          HF(200),SF(200),ALPD(10),
3THETA(20)
COMMON/XF/XF(200),YF(200),PF(200),QF(200),TF(200),THF(200),ALPF(
110,200)
COMMON/D/ GAMINF,EMINF,RINF,WINF
COMMON/C1/ EMC1,TC1,QC1
COMMON /SP/ NSP
DIMENSION ALPDUM(10)
J=I+1
BET=THF(I)-XMUF(I)
BET=BET-.1*ABS(BET)
ITT=1
DO 4 JJ=1,NSP
4 ALPDUM(JJ) =ALPF(JJ,I)
IER=0
3 CONTINUE
CALL SHOCK(BET,QF(I),THF(I),GAMF(I),EMF(I),RHOF(I),PF(I),RF(I),
1WF(I),TF(I),XMUF(I),QF(J),THF(J),GAMF(J),EMF(J),RHOF(J),PF(J),
2RF(J),WF(J),TF(J),XMUF(J),ALPDUM,-1.,IEQ)
P2=PF(J)*GAMINF*EMINF*EMINF
P2=P2/PMM
TH2=THF(J)
CALL PRM(P2,THM,EM,TH2T,EM3,-1)
ER4=TH2T-TH2
IF(ABS(ER4),LT.1.E-04) GO TO 15
CALL ERR(IER,ITT,BET,ER4,1.05,BET1,ER41)
IF(IER,EQ.1)GO TO 102
ITT=ITT+1
GO TO 3
102 WRITE(6,203)
203 FORMAT(* ERROR IN BETA LOOP IN COWLO*)
STOP
15 CONTINUE
DO 300 JJ=1,NSP
300 ALPF(JJ,J)=ALPF(JJ,I)
XF(J)=XF(I)
YF(J)=YF(I)
EMC1=EM3
DUM1=1.+(GAMINF-1.)/2.*EMINF*EMINF
DUM2=1.+(GAMINF-1.)/2.*EM3*EM3
TC1=DUM1/DUM2
QC1=EM3/EMINF*SQRT(TC1)
RETURN
END

```

```

SUBROUTINE SHOCK(BET,Q1,TH1,G1,EM1,RH1,P1,H1,PHI1,T1,XMU1,
1 Q2,TH2,G2,EM2,RH2,P2,H2,PHI2,T2,XMU2,ALPDUM,FSH,IEQ)
COMMON/A/ TIN,CPIN,RO
COMMON/D/ GAMINF,EMINF,RINF,WINF
DIMENSION ALPDUM(10)
IT=1
IER=0
V1=Q1*Q1
HS1=H1-V1/2.
VT=Q1*COS(BET-TH1)
U1=ABS(Q1*SIN(BET-TH1))
GM1=G1-1.
GP1=G1+1.
XM1=EM1*SIN(BET-TH1)
XMS=RH1*U1
IF(IT,EQ,1)UM=U1*(GM1*XM1*XM1+2.)/GP1/XM1/XM1
7  H2=XMS/UM
P2=XMS*(U1-UM)+P1
V2=VT*VT+UM*UM
H2=H1
HS2=H2-V2/2.
PHI2=PHI1
IF(IEQ,EQ,0)GO TO 10
RH2T=RHEQ(HS2,P2,PHI2,T2)
ER=(RH2-RH2T)/RH1
GO TO 12
10 T2=P2*PHI2*GAMINF*EMINF **2/RO/RH2/WINF
CALL THERMO(T2,HS2T,DUM,DUM)
ER=(HS2T-HS2)/HS1
12 CONTINUE
IF(ABS(ER),LT,1.E-03)GO TO 9
CALL ERR(IER,IT,UM,ER,.99,UM1,ER1)
IF(IER,EQ,1)GO TO 100
IT=IT+1
GO TO 7
100 WRITE(6,200)
200 FORMAT(* ERROR IN HUGONIOT LOOP IN SHOCK*)
WRITE(6,46)IEQ,FSH,BET,TH1,P1,Q1,G1,EM1,RH1,H1,PHI1,T1,
1 P2,UM,U1,VT,RH2,T2,HS2,ER
46 FORMAT(1X,I2,9E13.5/3X,10E13.5)
STOP
9 IF(FSH.GT,0.) TH2=BET-ATAN(UM/VT)
IF(FSH.LT,0.) TH2=ATAN(UM/VT)+BET
Q2=SQRT(V2)
CALL ALL(P2,Q2,RH2,PHI2,H2,G2,EM2,XMU2,T2,ALPDUM,IEQ,1)
RETURN
END

```

```

SUBROUTINE SHOCPT(IS,M,BET,BETN,A,B)
COMMON/VAR/RHO(200),
1EM(200),XMU(200),CPX(200),W(200),R(200),GAM(200),XMASS(200),
2      XN(200),YN(200),QN(200),TN(200),PN(200),THN(200),RHON
3(200),EMN(200),XMUN(200),CPXN(200),WN(200),RN(200),GAMN(200),
4XMASSN(200),ALPN(10,200),SI(10),HI(10),TEMP(20)
5,ALPDUM(10)
COMMON/X/ X(200),Y(200),P(200),Q(200),T(200),TH(200),ALP(10,200)
COMMON/ETX/XJ,XJ1,NPTS,IO,IREFL,ICHEM,IPUNCH,IDESGN,IR,NXX,XBP,
1YBP,THBF,RAD,XBOD,YBOD,THBOD,RADB,XEND,THEND,RTH,YEXIT,THST,TEST,
1IKFL,YO,RADB2,RRAD(20),  NSTAR,YNOZ,EIN,  PEN,H16,H17
COMMON/IEQ/IEQ,PIN,RHOINF,UINF,PINF
IF(B,EQ,0.) BETN=BET+(THN(IS-1)+XMUN(IS-1)-TH(M-1)-XMU(M-1))
I=IS
J=IS+1
L=IS
ITT=1
IER=0
DO 75 JJ=1,7
75 ALPDUM(JJ)=ALPN(JJ,I)
3 CALL SHOCK(BETN,QN(I),THN(I),GAMN(I),EMN(I),RHON(I),PN(I),
1RN(I),WN(I), TN(I),XMUN(I),QN(J),THN(J),GAMN(J),EMN(J),RHON(J),
2PN(J),RN(J),WN(J),TN(J),XMUN(J),ALPDUM,1.,IEQ)
EM1=XM1(.5,.5,THN(J),XMUN(J),TH(M),XMU(M))
EM2=XM2(.5,.5,TH(M),XMU(M),TH(M+1),XMU(M+1))
YDUM=(EM1*Y(M)-EM2*YN(L)+EM1*EM2*(XN(L)-X(M)))/(EM1-EM2)
RAT=(YDUM-Y(M))/(Y(M+1)-Y(M))
IF(IS,EQ,2,AND,M,EQ,2) RAT=0.
CALL IVT(RAT,X(M),Y(M),TH(M),P(M),Q(M),RHO(M),R(M),W(M),GAM(M),
1EM(M),XMU(M),T(M), X(M+1),Y(M+1),TH(M+1),P(M+1),Q(M+1),
2RHO(M+1),R(M+1),W(M+1),GAM(M+1),EM(M+1),XMU(M+1),T(M+1),
3X2,Y2,TH2,P2,Q2,RH2,R2,W2,GAM2,EM2,XMU2,T2,ALPDUM,1,IEQ)
A1=F1(A,B,XMU2,GAM2,P2,XMUN(J),GAMN(J),PN(J))
A2=F2(A,B,1.,XJ,XJ1,X2,Y2,TH2,XMU2,XN(J),YN(J),THN(J),XMUN(J))
DUM1=A2*(XN(J)-X2)
DUM=(TH2-THN(J)-DUM1)/A1
PTEST=P2*EXP(DUM)
ER4=(PTEST-PN(J))/P(M)
IF(ABS(ER4).LT,1.E-04) GO TO 15
CALL ERR(IER,ITT,BETN,ER4,1.05,BETN1,ER41)
IF(IER,EQ,1)GO TO 102
ITT=ITT+1
GO TO 3
102 WRITE(6,203)
203 FORMAT(* ERROR IN BETA LOOP IN SHOCPT*)
STOP
15 CONTINUE
XN(J)=XN(I)
YN(J)=YN(I)
DO 300 JJ=1,7
300 ALPN(JJ,J)=ALPN(JJ,I)
RETURN
END

```

```

SUBROUTINE PRM(P,TH1, XM1, TH2, XM2, IS)
COMMON/D/ GAMINF,EMINF,RINF,WINF
G=GAMINF
GM1=G-1.
GP1=G+1.
DUM=1.+GM1/2.*XM1*XM1
P=P** (GM1/G)
XM2=(DUM/P-1.)*2./GM1
XM2=SQRT(XM2)
GX=SQRT(GP1/GM1)
DUM1=SQRT(XM1*XM1-1.)
DUM2=SQRT(XM2*XM2-1.)
DTH=      GX*(ATAN(DUM2/GX)-ATAN(DUM1/GX))+ATAN(DUM1)-ATAN(DUM2)
TH2=TH1+FLDAT(IS)*DTH
RETURN
END

```



```
SUBROUTINE PRM(P,TH1,XM1,TH2,XM2,IS)
COMMON/2/ GAMINF,EMINF,RINF,WINF
G=GAMINF
GM1=G-1.
GP1=G+1.
DUM=1.+GM1/2.*XM1*XM1
P=P**((GM1/G)
XM2=(DUM/P-1.)*.2./GM1
XM2=SQRT(XM2)
GX=SQRT(GP1/GM1)
DUM1=SQRT(XM1*XM1-1.)
DUM2=SQRT(XM2*XM2-1.)
DTH=    GX*(ATAN(DUM2/GX)-ATAN(DUM1/GX))+ATAN(DUM1)-ATAN(DUM2)
TH2=TH1+FLOAT(IS)*DTH
RETURN
END
```

```

FUNCTION FT(P1,F,H5)
COMMON/IPP/IPP
COMMON /THE/ A1,A2,A3,A4,A5,A6,XMM1
COMMON/IEQ/IEQ,PIN,RHOINF,UINF,PINF
COMMON/A/ TIN,CPIN,RO
COMMON/IDEAL/IDEAL,GAMEY,XMWT ,CPI
DATA I63/0/
IF(IDEAL.EQ.1)GO TO 6666
IFLAG=0
IHOLD=0
P=P1/PIN*PINF*1.01325E+05
H=H5*UINF/10.7639/1.E+06
F2=F*F
A10=ALOG(P)/2.3-5.
Z9=.125*A10*A10          =.275*A10
IT=1
IF(I63,EQ.1) GO TO 1000
I63=1
T=1500.
T0=1500.
IF(F,GE.0.) GO TO 120
T=600.
T0=T
1000 CONTINUE
IF(F,LT.0.) GO TO 400
GO TO 120
50 E0=(H-H1)/H
IF(ABS(E0),LT.1.E-04) GO TO 340
500 T =T0*1.1
502 IT=2
IF(F,LT.0.) GO TO 400
GO TO 120
100 E1=(H-H1)/H
IF(ABS(E1),LT.1.E-04) GO TO 340
IT=IT+1
IF(IT,LT.21) GO TO 10
IF(ABS(T-2000.),LT.10.) GO TO 830
IF(IHOLD,EQ.0) GO TO 800
WRITE(6,831) P1,H5,T
831 FORMAT(* ERROR IN FT*/* P1 = *E13,5,5X,*H1 = *E13,5,5X,*T = *E13,5
1)
STOP
800 T=THOLD
T0=T
H=HHOLD
IT=1
IHOLD=1
IF(T.LE.2000.) IHOLD=-1
GO TO 1000
830 IF(IFLAG,EQ.1) GO TO 504
IFLAG=1
T0=2000.
T=2000.
IF(F,LT.0.) GO TO 400
GO TO 120
504 WRITE(6,11) E1
11 FORMAT(* TEMPERATURE IN FT SET TO 2000          *          ERROR = *E13,5)

```

```

GO TO 340
10 T9=T0-E0*(T -T0)/(E1-E0)
505 E0=E1
    T0=T
    T=T9
    IF(F,LT,0.) GO TO 400
120 A=1,E-07*(-.1042*F2 +.8242*F+.987)
    B=.001*(.01167*F2 +.1503*F+.938)
    C=-.0284*F2 +.6731*F+.4293
    IF(F,LE,1.) GO TO 190
    A=1,E-07*(1.787*F2 -5.48*F+5.4)
    B=.001*(-.1867*F2 +1.11*F+ 1.76)
    C=-.0933*F2 +3.975*F-2.808
190 IF(T,LE,2000.,AND,IHOLD,NE,1) GO TO 290
    A=.000001*(1.792*F2 +.3983*F+.31)
    B=.001*(-9.05*F2 -.07917*F+.245)
    C=10.86*F2 -.1183*F+.97
    IF(F,LE,1.) GO TO 290
    A=.000001*(4.81*F2 -13.9*F+11.59)
    B=.001*(-23.08*F2 +66.82*F-52.61)
    C=27.05*F2 -73.73*F+58.39
290 H1=A*T*T+B*T+C
    IF(T,LE,2000.,AND,IHOLD,NE,1) GO TO 370
    H1=H1*(1,+(1,+F)*(T/2000,-1.))*Z9)
370 CONTINUE
    GO TO 350
400 T2=T*T
    T3=T2*T
    T4=T3*T
    T5=T4*T
    IF(F,LT,-1.5) GO TO 450
    XMM1=16.043
    A1=4.2497678
    A2=-6.9126562E-03
    A3=3.1602134E-05
    A4=-2.9715432E-08
    A5=9.5103580E-12
    A6=-1.0186632E+04
    GO TO 460
450 CONTINUE
    A1=1.1202436
    A2=1.3905716E-02
    A3=2.6568374E-06
    A4=-1.1560272E-08
    A5=5.2386929E-12
    A6=5.3328896E+03
    XMM1=28.054
460 H1=A1*T+A2*T2/2,+A3*T3/3,+A4*T4/4,+A5*T5+A6
    H1=H1*8314./XMM1/1.E+06
350 IF(IT,EQ,1) GO TO 50
    GO TO 100
340 T0=T
    FT=T/TIN
    THOLD=T
    HHOLD=H
    RETURN
6666 H=H5* UINF

```

39  
FT=H\*5./9./CPI/TIN  
RETURN  
END

```

FUNCTION FH(P1,F,T1)
COMMON /THE/ A1,A2,A3,A4,A5,A6,XMM1
COMMON /IEQ/ IEQ,PIN,RHOINF,UINF,PINF
COMMON /A/ TIN,CPIN,RO
COMMON /IDEAL/ IDEAL,GAMEY, XMWT ,CPI
T=T1*TIN
IF(IDEAL,EQ.1)GO TO 6666
P=P1/PIN*PINF*1.01325E+05
F2=F*F
IF(F,LT,0.) GO TO 400
IF(T,GT,2000.) GO TO 190
IF(F,GT,1.) GO TO 191
120 A=1.E-07*(.1042*F2 +.8242*F+.987)
B=.001*(.01167*F2 +.1503*F+.938)
C=-.0284*F2 +.6731*F+.4293
GO TO 290
191 A=1.E-07*(1.787*F2 -5.48*F+5.4)
B=.001*(-.1867*F2 +1.11*F+.176)
C=-.0933*F2 +3.975*F-2.808
GO TO 290
190 IF(F,GT,1.) GO TO 192
A=.000001*(1.792*F2 +.3983*F+.31)
B=.001*(-9.05*F2 -.07917*F+.245)
C=10.86*F2 -.1183*F+.97
GO TO 290
192 A=.000001*(4.81*F2 -13.9*F+11.59)
B=.001*(-23.08*F2 +66.82*F-52.61)
C=27.05*F2 -73.73*F+58.39
290 H1=A*T*T+B*T+C
IF(T,LE,2000.) GO TO 370
A10=ALOG(P)/2.3-5.
Z9=.125*A10*A10 -.275*A10
H1=H1*(1.+(1.+F)*(T/2000.-1.))*Z9)
370 H1=H1*1.E+06
GO TO 340
400 T2=T*T
T3=T2*T
T4=T3*T
T5=T4*T
H1=A1*T+A2*T2/2.+A3*T3/3.+A4*T4/4.+A5*T5+A6
H1=H1*8314./XMM1
340 CONTINUE
FH=H1*10.7639/UINF
RETURN
6666 FH=CPI*T*9./5./UINF
RETURN
END

```

```

FUNCTION FGAM(T1,P1,F)
COMMON /THE/ A1,A2,A3,A4,A5,A6,XMM!
COMMON/IEQ/IEQ,PIN,RHOINF,UINF,PINF
COMMON/A/ TIN,CPIN,RO
COMMON/IDEAL/IDEAL,GAMEY,XMWT ,CPI
IF(IDEAL.EQ.1)GO TO 6666
T=T1*TIN
T2=T*T
P=P1/PIN*PINF*1.01325E+05
XM=0.
IF(F.LT.0.) GO TO 550
IF(T.LE.1000.) GO TO 440
XM=-2.15E-08*T2 +.000091*T=.0695
440 XN=4.E-09*T2 -.00002*T=.019
IF(F.LE.1.) GO TO 470
XN=.0339*SQRT(T)-.000391*T=.681
470 G=-1.833E-07*T2 +.000075*T+1.367
IF(T.LT.500.) GO TO 520
G=2.E-08*T2 -.000138*T+1.423
IF(T.LT.2000.) GO TO 520
G=7.267E-08*T2 -.000457*T+1.85
520 G=G+XM*(ALOG(P)/2.3-5.)*XN*(F-1.)
GO TO 530
550 T3=T2*T
T4=T3*T
CP=A1+A2*T+A3*T2+A4*T3+A5*T4
G=CP*(CP-1.)
530 CONTINUE
FGAM=G
RETURN
6666 FGAM=GAMEY
RETURN
END

```

```

FUNCTION RHEQ(H,P1,F,T)
COMMON/IEQ/IEQ,PIN,RHOINF,UINF,PINF
COMMON/A/ TIN,CPIN,RO
COMMON/IDEAL/IDEAL,GAMEY,XMWT ,CPI
T1=FT(P1,F,H)
T=T1*TIN
IF(IDEAL.EQ.1)GO TO 6666
P=P1/PIN*PINF*1.01325E+05
IF(F.LT.0.) GO TO 2260
FNM=1.53*F*F-5.895*F+28.965
FNN=1.6*F*F-10.6*F+33.6
IF(T.GT.2000.) GO TO 2030
XM=FNM
IF(F.LT.1.) GO TO 2160
XM=FNN
GO TO 2160
2030 FF=F*F
A=-2.3*FF+4.01*F+1.736
R=8.61*FF-15.42*F-6.66
C=-16.88*FF+33.21*F+14.58
XN=-.4375*FF+.0625*F+2.08
D=A*(ALOG(P)/2.3)**1.5+B*(ALOG(P)/2.3)+C
XM=FNM-D*((T-2000.)/1000.)**XN
IF(F.LT.1.) GO TO 2160
A=-.822*FF+2.363*F+1.905
B=2.76*FF-7.56*F-8.68
C=-3.6*FF+7.36*F+27.15
XN=-.47*FF+1.825*F+.35
D=A*(ALOG(P)/2.3)**1.5+B*(ALOG(P)/2.3)+C
XM=FNN-D*((T-2000.)/1000.)**XN
GO TO 2160
2260 KF=F-.5
IF(KF.EQ.-1)XM=16.043
IF(KF.EQ.-2)XM=28.054
2160 RHEQ=P*XM/T/8314.3*6.2428E-02/32.174
T=T/TIN
RHEQ=RHEQ/RHOINF
RETURN
6666 RHEQ=P1*XMWT*5.*UINF/T/9./49712.52
T=T/TIN
RETURN
END

```

```
SUBROUTINE ERROR(IIII)
WRITE(5,100) IIII
100 FORMAT(7H1ERROR=IS)
CALL EXIT
RETURN
END
```



44

```
FUNCTION XM1( ALPHA, BETA, TA, XA, TC, XC)
  XM1=ALPHA*TAN(TA+XA)
  IF(BETA.GT.0.)XM1=XM1+BETA*TAN(TC+XC)
  RETURN
END
```

```
FUNCTION XM2(AL,B,TA,XA,TC,XC)
XM2=AL*TAN(TA-XA)
IF(B.GT.0.)XM2=XM2+B*TAN(TC-XC)
RETURN
END
```

```
FUNCTION XM3(A,B,TD,TC)
XM3=A*TAN(TD)
IF(B.GT.0.0)XM3=XM3+B*TAN(TC)
RETURN
END
```

```
FUNCTION F1(A, B, XMU1, GAM1, P1, XMU2,  
1GAM2, P2)  
F1=SIN(XMU1)*COS(XMU1)/GAM1  
IF(B.GT.0.0)F1=(F1+SIN(XMU2)*  
1COS(XMU2)/GAM2 )/2.  
RETURN  
END
```

```
FUNCTION F2(A,B,OPT,XJ,XJ1,X,Y,TH,XMU,XN,YN,THN,XMUN)
F21=0.
IF(XJ.EQ.0.) GO TO 15
F21=A*SIN(TH)*SIN(XMU)/COS(TH+OPT*XMU)/Y
IF(B.GT.0.) F21=F21+B*SIN(THN)*SIN(XMUN)/COS(THN+OPT*XMUN)/YN
15 F22=0.
IF(XJ1.EQ.0.) GO TO 10
F22=A*COS(TH)*SIN(XMU)/COS(TH+OPT*XMU)
IF(B.GT.0.) F22=F22+B*COS(THN)*SIN(XMUN)/COS(THN+OPT*XMUN)
10 F2=F21+F22
RETURN
END
```

```
SUBROUTINE DRTEST(XN,YN,EM1,BET,IDROP,L,M)
COMMON/X/ X(200),Y(200),P(200),Q(200),T(200),TH(200),ALP(10,200)
EM2=TAN(BET)
XNT=(Y(M)-Y(M+L)-EM1*X(M)+EM2*X(M+L))/(EM2-EM1)
YNT=Y(M)+EM1*(XNT-X(M))
DISNDR=SQRT((XN-X(M))**2+(YN-Y(M))**2)
DISEX =SQRT((XNT-X(M))**2+(YNT-Y(M))**2)
IF((DISEX-DISNDR)/DISEX.LT.,.1) IDROP=1
RETURN
END
```

```

SUBROUTINE XMASSS(RATM,NPTS)
COMMON/FVAR/
1RHOF(200),CPXF(200),EMF(200),XMUF(200),WF(200),RF(200),GAMF(200),
2XMASSF(200),HF(200),SF(200),ALPD(10),
3THETA(20)
COMMON/XF/XF(200),YF(200),PF(200),QF(200),TF(200),THF(200),ALPF(
110,200)
DO 170 I=1,NPTS
CALL FM(FM1,EMF(I),GAMF(I))
FM2=FM1/RATM
ITM=1
IER=0
EMT=RATM*EMF(I)
197 CONTINUE
CALL FM(FMT,EMT,GAMF(I))
ERM=(FM2-FMT)/FM2
IF(ABS(ERM).LT.1.E-03)GO TO 171
DUMD=1./RATM
CALL ERR(IER,ITM,EMT,ERM,DUMD,EMT1,ERM1)
IF(IER.EQ.1)GO TO 2
ITM=ITM+1
GO TO 197
2 WRITE(6,3)
3 FORMAT(* ERROR IN ITERATION LOOP IN XMASSS*)
STOP
171 CONTINUE
DUM=SQRT((GAMF(I)+1.)/(GAMF(I)-1.))
ETSQ=SQRT(EMT*EMT-1.)
ESQ=SQRT(EMF(I)*EMF(I)-1.)
XNU2=DUM*ATAN(ETSQ/DUM)-ATAN(ETSQ)
XNU1=DUM*ATAN(ESQ/DUM)-ATAN(ESQ)
DNU=XNU2-XNU1
CALL PM1(DNU,I)
170 CONTINUE
RETURN
END

```

51  
SUBROUTINE GEM(XA, YA, SLA, XB, YB, SLB, XC, YC)  
XC=(YB-YA+SLA\*XA-SLB\*XB)/(SLA-SLB)  
YC=YA+SLA\*(XC-XA)  
RETURN  
END



```

SUBROUTINE THERMO(TI,H,CP,DCP)
COMMON/IEQ/IEQ,PIN,RHO,INF,UINF,PINF
COMMON /SP/ NSP
COMMON/A/ TIN,CPIN,RO
COMMON/B/ WTMOLE
DIMENSION WTMOLE(10)
DIMENSION H(10),CP(10),DCP(10)
T=TI*TIN
C1=RO/CPIN
C2=C1/TIN
C3=C1*TIN
N=NSP
DO 10 J=1,N
H1=C2/NTMOLE(J)
H2=C1/NTMOLE(J)
H3=C3/NTMOLE(J)
CALL CDEFF(J,T,A,B,C,D,E,F,G)
H(J)=T*(A+T*(B/2.+T*(C/3.+T*(D/4.+E/5.*T))))+F
H(J)=H(J)*RO*4.506557*1.E+04/WTMOLE(J)/UINF
CP(J)=A+T*(B+T*(C+T*(D+E*T)))
CP(J)=CP(J)*H2
DCP(J)=B+T*(2.*C+T*(3.*D+4.*E*T))
DCP(J)=DCP(J)*H3
10 CONTINUE
RETURN
END

```

53

```
SUBROUTINE SL(P1,Q1,RH1,R1,W1,GAM1,EM1,XMU1,T1,  
1P2,Q2,RH2,R2,W2,GAM2,EM2,XMU2,T2,ALPDUM,IEQ,A,B)  
R2=R1  
RH2=RH1*(P2/P1)**(1./GAM1)  
IF(IEQ.EQ.1)W2=W1  
IF(IEQ.EQ.1.AND.B.EQ.0.)Q2=Q1+(P1-P2)/RH1/Q1  
CALL ALL(P2,Q2,RH2,R2,W2,GAM2,EM2,XMU2,T2,ALPDUM,IEQ,0)  
RETURN  
END
```

```

SUBROUTINE DPOINT(K,L,M,N,NPTS,A,B)
COMMON/X/ X(200),Y(200),P(200),Q(200),T(200),TH(200),ALP(10,200)
COMMON/IEQ/IEQ,PIN,RHOINF,UINF,PINF
COMMON/VAR/RHO(200),
1EM(200),XMU(200),CPX(200),W(200),R(200),GAM(200),XMASS(200),
2      XN(200),YN(200),QN(200),TN(200),PN(200),THN(200),RHON
3(200),EMN(200),XMUN(200),CPXN(200),WN(200),RN(200),GAMN(200),
4XMASSN(200),ALPN(10,200),SI(10),HI(10),TEMP(20)
5,ALPDUM(10)
COMMON /SP/ NSP
COMMON/DD/XD,YD,THD,PD,QD,RHD,RD,WD,EMD,GAMD,XMUD,TD
ITD=0
IF(M,EQ,1)GO TO 195
XD=.5*(X(M)+X(M-1))
SLD=.5*(TAN(THN(L))+.5*(TAN(TH(M))+TAN(TH(M-1))))
QD=Q(M-1)
SLM=(Y(M)-Y(M-1))/(X(M)-X(M-1))
S2=SQRT((X(M-1)-X(M))**2+(Y(M-1)-Y(M))**2)
10 CALL GEM(XN(L),YN(L),SLD,X(M),Y(M),SLM,XD,YD)
SD=SQRT((XD-X(M))**2+(YD-Y(M))**2)
IF(ITD,GT,0)GO TO 11
IF(SD,GT,S2)GO TO 100
11 RATD=1.-SD/S2
XT=XD
THD=TH(M-1)+RATD*(TH(M)-TH(M-1))
XD=X(M-1)+RATD*(X(M)-X(M-1))
ERD=ABS((XT-XD)/(X(M)-X(M-1)))
IF(ERD,LT,1.E-03)GO TO 15
SLD=(TAN(THN(L))+TAN(THD))/2.
ITD=ITD+1
IF(ITD,LT,10)GO TO 10
WRITE(6,75)
75 FORMAT(*TOO MANY ITERATIONS IN DPOINT*)
WRITE(6,76)K,XN(K),YN(K),THN(K),XD,YD,RATD,THD,ERD
WRITE(6,76)L,XN(L),YN(L),THN(L)
WRITE(6,76)M,X(M),Y(M),TH(M)
IF(M,GT,1)JJ=M-1
IF(M,GT,1)WRITE(6,76)JJ,X(JJ),Y(JJ),TH(JJ)
76 FORMAT(1X,I5,8E13,5)
STOP
15 DO 14 J=1,NSP
14 ALPDUM(J)=ALP(J,M-1)+RATD*(ALP(J,M)-ALP(J,M-1))
CALL INT(RATD,X(M-1),Y(M-1),TH(M-1),P(M-1),Q(M-1),RHO(M-1),
1R(M-1),W(M-1),GAM(M-1),EM(M-1),XMU(M-1),T(M-1),X(M),Y(M),TH(M),
2P(M),Q(M),RHO(M),R(M),W(M),GAM(M),EM(M),XMU(M),T(M),
3D1,D2,THD,PD,QD,RHD,RD,WD,GAMD,EMD,XMUD,TD,ALPDUM,1,IEQ)
RETURN
100 CONTINUE
SLP=(YN(K)-Y(M-1))/(XN(K)-X(M-1))
SLD=.5*(TAN(THN(L))+.5*(TAN(THN(K))+TAN(TH(M-1))))
XD=.5*(XN(K)+X(M-1))
101 CALL GEM(XN(L),YN(L),SLD,XN(K),YN(K),SLP,XD,YD)
RATD=(XD-X(M-1))/(XN(K)-X(M-1))
XT=XD
THD=TH(M-1)+RATD*(THN(K)-TH(M-1))
XD=X(M-1)+RATD*(XN(K)-X(M-1))
ERD=ABS((XT-XD)/(XN(K)-X(M-1)))

```

```

IF(ERD,LT,1.E-03)GO TO 150
SLD=(TAN(THN(L))+TAN(THD))/2.
ITD=ITD+1
IF(ITD,LT,10)GO TO 101
WRITE(6,75)
STOP
150 DO 140 J=1,NSP
140 ALPDUM(J)=ALP(J,M-1)+RATD*(ALPN(J,K)-ALP(J,M-1))
CALL INT(RATD,X(M-1),Y(M-1),TH(M-1),P(M-1),Q(M-1),RHO(M-1),
1R(M-1),W(M-1),GAM(M-1),EM(M-1),XMU(M-1),T(M-1),
2XN(K),YN(K),THN(K),PN(K),QN(K),RHON(K),RN(K),WN(K),GAMN(K),
3EMN(K),XMUN(K),TN(K),D1,D2,THD,PD,QD,RHD,RD,WD,GAMD,EMD,XMUD,
4TD,ALPDUM,1,IEQ)
RETURN
195 CONTINUE
QD=Q(M)
SLD=.5*(TAN(THN(L))+.5*(TAN(THN(K))+TAN(TH(M))))
XD=.5*(XN(K)+X(M))
I75=0
IF(ABS(XN(K)-X(M)),GT,1.E-06)I75=1
IF(I75,EQ,1)GO TO 290
XD=(XN(K)+X(M))/2.
191 IF(I75,EQ,1)GO TO 290
YD=YN(L)-SLD*(XN(L)-XD)
GO TO 291
290 SLP=(YN(K)-Y(M))/(XN(K)-X(M))
CALL GEM(XN(L),YN(L),SLD,XN(K),YN(K),SLP,XD,YD)
291 RATD=(YD-Y(M))/(YN(K)-Y(M))
YT=YD
THD=TH(M)+RATD*(THN(K)-TH(M))
YD=Y(M)+RATD*(YN(K)-Y(M))
ERD=(YT-YD)/(YN(K)-Y(M))
IF(ABS(ERD),LT,1.E-03)GO TO 197
SLD=(TAN(THD)+TAN(THN(L)))/2.
ITD=ITD+1
IF(ITD,LT,10)GO TO 191
WRITE(6,75)
STOP 1
197 DO 198 J=1,NSP
198 ALPDUM(J)=ALP(J,M)+RATD*(ALPN(J,K)-ALP(J,M))
CALL INT(RATD,X(M),Y(M),TH(M),P(M),Q(M),RHO(M),R(M),W(M),GAM(M),
1EM(M),XMU(M),T(M),XN(K),YN(K),THN(K),PN(K),QN(K),RHON(K),RN(K),
2WN(K),GAMN(K),EMN(K),XMUN(K),TN(K),D1,D2,THD,PD,QD,RHD,RD,WD,GAMD,
3EMD,XMUD,TD,ALPDUM,1,IEQ)
RETURN
END

```

```

SUBROUTINE INT(RAT,X1,Y1,TH1,P1,Q1,RH1,R1,W1,GAM1,EM1,XMU1,T1,
1X2,Y2,TH2,P2,Q2,RH2,P2,W2,GAM2,EM2,XMU2,T2,
2X3,Y3,TH3,P3,Q3,RH3,R3,W3,GAM3,EM3,XMU3,T3,ALPDUM,IAL,IEQ)
DIMENSION ALPDUM(10)
X 3=X 1+RAT*(X 2-X 1)
Y 3=Y 1+RAT*(Y 2-Y 1)
T 3=T 1+RAT*(T 2-T 1)
P 3=P 1+RAT*(P 2-P 1)
R 3=R 1+RAT*(R 2-R 1)
W 3=W 1+RAT*(W 2-W 1)
Q 3=Q 1+RAT*(Q 2-Q 1)
TH 3=TH 1+RAT*(TH 2-TH 1)
GAM3=GAM1+RAT*(GAM2-GAM1)
PRG1=P1/RH1**GAM1
PRG2=PRG1
IF(RAT.NE.0.)PRG2=P2/RH2**GAM2
PRG3=PRG1+RAT*(PRG2-PRG1)
RH3=(P3/PRG3)**(1./GAM3)
IF(IAL.EQ.1)GO TO 20
EM 3=EM 1+RAT*(EM 2-EM 1)
XMU3=XMU1+RAT*(XMU2-XMU1)
RETURN
20 CALL ALL(P3,Q3,RH3,R3,W3,GAM3,EM3,XMU3,T3,ALPDUM,IEQ,0)
RETURN
END

```

```
SUBROUTINE ERR(I,IT,X,ER,F,X1,ER1)
IF(IT.LT.15)GO TO 12
I=1
RETURN
12 IF(IT.GT.2)GO TO 14
ER1=ER
X1=X
X=X+F
IF(X.EQ.X1)X=X+.02
RETURN
14 XD=X1-ER1*(X-X1)/(ER-ER1)
ER1=ER
X1=X
X=XD
RETURN
END
```

```
SUBROUTINE VIS(T,XMUU)
COMMON/A/TIN,CPIN,RO
TC=198.*5./TIN/9.
XMUU=(1.+TC)*(T*1.5)/(T+TC)
RETURN
END
```

```

SUBROUTINE WUZZY(N,NPTS,KMAX,LMAX,IPP,IFZ,LWUZ)
COMMON/LDOWN/LDOWN
COMMON/ICMPLT/ICMPLT
COMMON/VAR/RHO(200),
1EM(200),XMU(200),CPX(200),N(200),R(200),GAM(200),XMASS(200),
2      XN(200),YN(200),QN(200),TN(200),PN(200),THN(200),RHON
3(200),EMN(200),XMUN(200),CPXN(200),WN(200),RN(200),GAMN(200),
4XMASSN(200),ALPN(10,200),SI(10),HI(10),TEMP(20)
5,ALPDUM(10)
COMMON/X/ X(200),Y(200),P(200),Q(200),T(200),TH(200),ALP(10,200)
LS=2
L=2
K=1
SLP1=TAN(THN(K)+XMUN(K))
M=3
IF(N,LE,NPTS)M=1
IF(ICMPLT.EQ,2)M=2
43 IF(K,GT,1)SLP1=(YN(K)-Y(M-1))/(XN(K)-X(M-1))
IF(IFZ,EQ,1,AND,L,EQ,LDOWN)RETURN
SLP2=(YN(L)-Y(M))/(XN(L)-X(M))
39 CONTINUE
IF(L,EQ,LWUZ)RETURN
IF(ABS(SLP2-SLP1),LT,1.E-06)GO TO 40
CALL GEM(XN(L),YN(L),SLP2,XN(K),YN(K),SLP1,XS,YS)
IF(XS,LT,XN(L))GO TO 40
IF((XS-XN(L))/(XN(L)-X(M)),GT,2,5)GO TO 40
IPT=IPP+1
BETA=.5*(SLP1+SLP2)
WRITE(6,10)IPT,L,K,M,LS,N,NPTS,
1      XN(L),X(M),XN(K),X(M-1),YN(L),Y(M),YN(K),
1Y(M-1),SLP1,SLP2,BETA,XS,YS
10 FORMAT(1X,7I5/1X,8E13,5/1X,8E13,5)
WRITE(6,33)
33 FORMAT( * UP RUNNING SHOCK DETECTED * )
WRITE(6,34)IPT,LS,XS,YS,BETA
34 FORMAT(* LINE NO. = *,I4,4X* POINT NO. = *,I4      ,4X*XS = *,E13,5,
14X* YS = *,E13,5,4X* SHOCK ANGLE = *,E13,5)
LL=L
LM=LMAX-1
IF(L,EQ,LMAX)LL=LM
DO 46 J=LL,LM
XN(J)=XN(J+1)
YN(J)=YN(J+1)
PN(J)=PN(J+1)
QN(J)=QN(J+1)
TN(J)=TN(J+1)
WN(J)=WN(J+1)
RN(J)=RN(J+1)
THN(J)=THN(J+1)
EMN(J)=EMN(J+1)
RHON(J)=RHON(J+1)
XMUN(J)=XMUN(J+1)
DO 1500 JL=1,7
1500 ALPN(JL,J)=ALPN(JL,J+1 )
46 CONTINUE
LMAX=LMAX-1
LS=LS-1

```



```
M=M+1
40 K=K+1
L=L+1
M=M+1
LS=LS+1
IF(L,LT,LMAX)GO TO 43
IF(L,GT,LMAX)RETURN
IF(IFZ,EQ,1,AND,L,EQ,LDOWN)RETURN
M=KMAX
K=L-1
SLP1=(YN(K)-Y(M))/(XN(K)-X(M))
SLP2=TAN(THN(L)+XMUN(L))
GO TO 39
END
```

```

SUBROUTINE FUZZY(K,L,M,N,LMAX,KMAX,NPTS,IPP,IFZ)
COMMON/LDOWN/LDOWN
COMMON/VAR/RHO(200),
1EM(200),XMU(200),CPX(200),W(200),R(200),GAM(200),XMASS(200),
2      XN(200),YN(200),QN(200),TN(200),PN(200),THN(200),RHON
3(200),EMN(200),XMUN(200),CPXN(200),WN(200),RN(200),GAMN(200),
4XMASSN(200),ALPN(10,200),SI(10),HI(10),TEMP(20)
5,ALPDUM(10)
COMMON/X/ X(200),Y(200),P(200),Q(200),T(200),TH(200),ALP(10,200)
COMMON/XCOWL/XCOWL
IFZ=0
DUMX=(XN(1)-X(1))**2
DUMY=(YN(1)-Y(1))**2
TEST=SQRT(DUMX+DUMY)
IF(TEST,EQ,0.)RETURN
SLP=TAN(TH(M)+XMU(M))
SLM=TAN(THN(K)-XMUN(K))
CALL GEM(XN(K),YN(K),SLM,X(M),Y(M),SLP,XC,YC)
DX=(XC-X(M))**2
DY=(YC-Y(M))**2
DC=SQRT(DX+DY)
IF((DC/TEST).GT,0.2)RETURN
LM=LMAX-1
LDOWN=L
I=L
J=M
85 XMUN(I)=XMU(J)
   YN(I)=Y(J)
   X  N(I)=X  (J)
   P  N(I)=P  (J)
   Q  N(I)=Q  (J)
   T  N(I)=T  (J)
   W  N(I)=W  (J)
   R  N(I)=R  (J)
   TH N(I)=TH (J)
   EM N(I)=EM (J)
   RHON(I)=RHO(J)
   GAMN(I)=GAM(J)
   DO 1500 JJ=1,7
1500 ALPN(JJ,I)=ALP(JJ,J)
      I=I+1
      J=J+1
      IF(I.GT,LM)GO TO 45
      GO TO 85
45 CONTINUE
   IPT=IPP+1
   BETA=.5*(TAN(TH(M)-XMU(M))+SLM)
   WRITE(6,33)
33  FORMAT(* DOWN RUNNING SHOCK DETECTED * )
   WRITE(6,34)IPT,L,XC,YC,BETA
34  FORMAT(* LINE NO. = *,I4,4X* POINT NO. = *,I4      ,4X*XS = *,E13.5,
14X* YS = *,E13.5,4X* SHOCK ANGLE = *,E13.5)
   LMAX=LMAX+1
   IF(N.GT,NPTS)LMAX=KMAX-1
   IFZ=1
   RETURN
END

```

```

SUBROUTINE GNURE(RH,Q,P,T,W,R,ALPDUM,X,X1,CF,ST,L)
COMMON/HOT/AH(3),BH(3),CH(3),XCTR,PR,REC,REIN,RT,SH,IT,IVIS
COMMON/SP/NSP
COMMON/IEQ/IEQ,PIN,RHOINF,UINF,PINF
DIMENSION ALPDUM(10),H1(10),CP1(10)
HDEL=R*Q*Q/2.
HAW=1.+REC*Q*Q/2./HDEL
IF(IT.EQ.0)TW=AH(L)*(X-X1)**2+BH(L)*(X-X1)+CH(L)
IF(IT.EQ.1)GO TO 46
IF(IEQ.EQ.0)GO TO 13
HW=PH(P,W,TW)/HDEL
GO TO 48
13 CALL THERMO(TW,H1,CP1,DUM)
HW=0.
DO 20 J=1,NSP
HW=HW+ALPDUM(J)*H1(J)
20 CONTINUE
HW=HW/HDEL
GO TO 48
46 HW=HAW
48 A=HAW-1.
B=HW-1.
C=SQRT((A+B)**2+4.*A)
FC=A/(ASIN((A-B)/C)+ASIN((A+B)/C))**2
FRX=HAW**(.772)/(FC*(HW)**(1.474))
CALL VIS(T,XMMU)
REX=RH*Q*(X+XSTR)/XMMU

REXI=FRX*REX*REIN*RT
CFI=.088*(ALOG10(REXI)-2.3686)/(ALOG10(REXI)-1.5)**3
CF=CFI/FC
ST=CF*SH/2.
RETURN
END

```

```

SUBROUTINE SNARF(X1,Y1,Z1,X2,Y2,Z2,X3,Y3,Z3,X4,Y4,Z4,AVX,AVY,AVZ,
1XNX,XNY,XNZ,AS,XO,YO,ZO)
DIMENSION XPA(4),YPA(4),ZPA(4),XI(4),ETA(4)
XPA(1)=X1
YPA(1)=Y1
ZPA(1)=Z1
ZPA(2)=Z2
YPA(2)=Y2
XPA(2)=X2
XPA(3)=X3
YPA(3)=Y3
ZPA(3)=Z3
ZPA(4)=Z4
YPA(4)=Y4
XPA(4)=X4
T1X=X3-X1
T1Y=Y3-Y1
T1Z=Z3-Z1
T2X=X4-X2
T2Y=Y4-Y2
T2Z=Z4-Z2
XNX=T2Y*T1Z-T1Y*T2Z
XNY=T1X*T2Z-T2X*T1Z
XNZ=T2X*T1Y-T1X*T2Y
VN=SQRT(XNX**2+XNY**2+XNZ**2)
XNX=XNX/VN
XNY=XNY/VN
XNZ=XNZ/VN
D=XNX*(AVX-X1)+XNY*(AVY-Y1)+XNZ*(AVZ-Z1)
PD=ABS(D)
T=SQRT(T1X*T1X+T1Y*T1Y+T1Z*T1Z)
T1X=T1X/T
T1Y=T1Y/T
T1Z=T1Z/T
T2X=XNY*T1Z-XNZ*T1Y
T2Y=XNZ*T1X-XNX*T1Z
T2Z=XNX*T1Y-XNY*T1X
DO 1000 J=1,4
XPA(J)=XPA(J)+XNX*D
YPA(J)=YPA(J)+XNY*D
ZPA(J)=ZPA(J)+XNZ*D
D=-D
XDIF=XPA(J)-AVX
YDIF=YPA(J)-AVY
ZDIF=ZPA(J)-AVZ
XI(J)=T1X*XDIF+T1Y*YDIF+T1Z*ZDIF
1000 ETA(J)=T2X*XDIF+T2Y*YDIF+T2Z*ZDIF
XIO=(XI(4)*(ETA(1)-ETA(2))+XI(2)*(ETA(4)-ETA(1)))/(ETA(2)-ETA(4))
1/3.
ETA0=-ETA(1)/3.
DO 1020 J=1,4
XI(J)=XI(J)-XIO
1020 ETA(J)=ETA(J)-ETA0
XO=AVX+T1X*XIO+T2X*ETA0
YO=AVY+T1Y*XIO+T2Y*ETA0
ZO=AVZ+T1Z*XIO+T2Z*ETA0
AS=(ETA(2)-ETA(4))*(XI(3)-XI(1))/2.

```

```
AS=ABS(AS)  
RETURN  
END
```

```

SUBROUTINE LTHM(X1,Y1,Z1,X2,Y2,Z2,X3,Y3,Z3,X4,Y4,Z4,P1,P2,P3,P4,
1Q1,Q2,Q3,Q4,RH1,RH2,RH3,RH4,R1,R2,R3,R4,W1,W2,W3,W4,
2TH1,TH2,TH3,TH4,ALPDUM,XK1,XK2,XK3,XK4,XXTHX,XYLFT,XXMOM,CF,ST,LH)
COMMON/LTM/XSHFT,YSHFT,DUMA,DUMB,DUMC,DUM1,DUM2,DUM3,DUM4
COMMON/ETX/XJ,XJ1,NPTS,IO,IREFL,ICHEM,IPUNCH,IDESGN,IR,NXX,XBP,
1YBP,THBP,RAD,XBOD,YBOD,THBOD,RADB,XEND,THEND,RTH,YEXIT,THST,TEST,
1IRFL,YO,RADB2,RRAD(20), NSTAR,YNOZ,EIN, PEN,H16,H17
COMMON/PFF/PFINF
COMMON/VISF/XVTHX,YVLFT,XVMOM
COMMON/IEQ/IEQ,PIN,RHOINF,UINF,PINF
COMMON/HOT/AH(3),BH(3),CH(3),XSTR,PR,REC,REIN,RT,SH,IT,IVIS
DIMENSION ALPDUM(10)
P=XK1*P1+XK2*P2+XK3*P3+XK4*P4
Q=XK1*Q1+XK2*Q2+XK3*Q3+XK4*Q4
R=XK1*R1+XK2*R2+XK3*R3+XK4*R4
W=XK1*W1+XK2*W2+XK3*W3+XK4*W4
RH=XK1*RH1+XK2*RH2+XK3*RH3+XK4*RH4
TH=XK1*TH1+XK2*TH2+XK3*TH3+XK4*TH4
AVX=XK1*X1+XK2*X2+XK3*X3+XK4*X4
AVY=XK1*Y1+XK2*Y2+XK3*Y3+XK4*Y4
AVZ=XK1*Z1+XK2*Z2+XK3*Z3+XK4*Z4
CALL SNARF(X1,Y1,Z1,X2,Y2,Z2,X3,Y3,Z3,X4,Y4,Z4,AVX,AVY,AVZ,XNX,
1XNY,XNZ,ASS,XO,YO,ZO)
CF=0.
IF(IVIS.EQ.1)CALL GNURE(RH,Q,P,W,R,ALPDUM,XO,XBP,CF,ST,LH)
IF(IVIS.EQ.1)CALL GNURE(RH,Q,P,T,R, XO,XBP,CF,ST,LH)
RHQ=RH*Q*Q/2.
PAV=(P/PIN-1.)*PINF*2116.
DXTHX=-PAV*XNX*ASS
DYLFT=-PAV*XNY*ASS
XNZZ=1.
IF(LH.EQ.3)XNZZ=XNZ
DXTHXV=-CF*PFINF*XNZZ*COS(TH)*ASS*RHQ
DYLFTV=CF*PFINF*SIN(TH)*ASS*RHQ
XMS=XO-XSHFT
YMS=YO-YSHFT
DMOMV=YMS*DXTHXV-XMS*DYLFTV
XVTHX=XVTHX+DXTHXV
YVLFT=YVLFT+DYLFTV
XVMOM=XVMOM+DMOMV
DXTHX=DXTHX+DXTHXV
DYLFT=DYLFT+DYLFTV
DMOM=YMS*DXTHX-XMS*DYLFT
XXTHX=XXTHX+DXTHX
XYLFT=XYLFT+DYLFT
XXMOM=XXMOM+DMOM
RETURN
END

```

REFERENCE

1. Del Guidice, P., Dash, S. and Kalben, P., "A Source Flow Characteristic Technique for the Analysis of Scramjet Exhaust Flow Fields," ATL TR 213 (NASA CR-132697) May 1975.