

NASA CR-2  
VOL. III

LOAN COPY: RETURN TO  
AFWL TECHNICAL LIBRARY  
KIRTLAND AFB, N. M.

# NASA CONTRACTOR REPORT

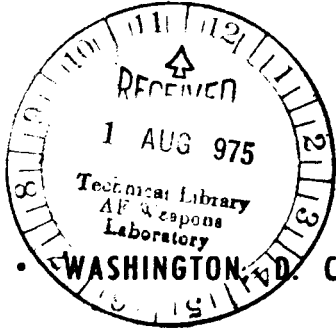
NASA CR-2559  
VOL. III

## NUMERICAL NONLINEAR INELASTIC ANALYSIS OF STIFFENED SHELLS OF REVOLUTION

Volume III - Engineer's Program Manual  
for STARS-2P Digital Computer Program

*V. Svalbonas, H. Levine, and P. Ogilvie*

Prepared by  
GRUMMAN AEROSPACE CORPORATION  
Bethpage, N.Y. 11714  
for George C. Marshall Space Flight Center



NATIONAL AERONAUTICS AND SPACE ADMINISTRATION • WASHINGTON, D. C. • JULY 1975



TECHNICAL

0061187

1. REPORT NO. NASA CR-2559		2. GOVERNMENT ACCESSION NO.		3. RECIPIENT'S CATALOG NO.	
4. TITLE AND SUBTITLE Numerical Nonlinear Inelastic Analysis of Stiffened Shells of Revolution, Volume III - Engineer's Program Manual for STARS-2P Digital Computer Program				5. REPORT DATE JULY 1975	
				6. PERFORMING ORGANIZATION CODE M142	
7. AUTHOR(S) V. Svalbonas, H. Levine, and P. Ogilvie				8. PERFORMING ORGANIZATION REPORT #	
9. PERFORMING ORGANIZATION NAME AND ADDRESS  Grumman Aerospace Corp. Bethpage, NY 11714				10. WORK UNIT NO.	
				11. CONTRACT OR GRANT NO. NAS8-28569	
12. SPONSORING AGENCY NAME AND ADDRESS  National Aeronautics and Space Administration Washington, D.C. 20546				13. TYPE OF REPORT & PERIOD COVERED  Contractor Report	
				14. SPONSORING AGENCY CODE	
15. SUPPLEMENTARY NOTES					
16. ABSTRACT  Volume III of this report contains engineering programming information for the STARS-2P (Shell Theory Automated for Rotational Structures-2P (Plasticity)) digital computer program. The report is written for the engineer who will need to make small alterations to the program, such as incorporating a new geometry or altering a table size to fit his specific needs. Each section of this volume covers one major subroutine.  This report is prepared in four volumes. The other volumes are:  Volume I - Theory Manual for STARS-2P Digital Computer Program Volume II - User's Manual for STARS-2P Digital Computer Program Volume IV - SATELLITE-1P Program for STARS-2P Digital Computer Program					
17. KEY WORDS			18. DISTRIBUTION STATEMENT  UNCLASSIFIED-UNLIMITED  STAR CATEGORY 39		
19. SECURITY CLASSIF. (of this report)  Unclassified		20. SECURITY CLASSIF. (of this page)  Unclassified		21. NO. OF PAGES  207	22. PRICE  \$7.25

ACKNOWLEDGEMENT

The authors wish to acknowledge the overall aid of Mr. J. Key, especially in the debugging phases of the UNIVAC program version.

## INTRODUCTION

This manual presents a general description of the STARS-2P digital computer program. FORTRAN IV is used exclusively in writing the various subroutines. The execution of this program requires the use of thirteen temporary storage units.

The program was initially written and debugged on the IBM 370-165 computer and then converted to the UNIVAC 1108 computer, where it utilizes approximately 60,000 words of core. Only basic FORTRAN Library routines are required by the program these being: sine, cosine, absolute value, and square root.

For ease and speed in usage, the Table of Contents on the following page has also been laid out to present the call sequence of the program.

CONTENTS

CALL SEQUENCE	CALLING ROUTINE	PAGE
MAIN		1
RIEMAN	MAIN	10
SETUP	RIEMAN	23
MAGIC	RIEMAN	23
ROBOT	RIEMAN	27
GEOMET	ROBOT	27
PLICO	GEOMET	27
PLINE	GEOMET	27
DIF1	RIEMAN	46
DIFF2	RIEMAN	46
SEGMAT	MAIN	63
SREVN2	SEGMAT	63
REGMAT	MAIN	72
RINGER	REGMAT	91
RITEPS	RINGER	91
RISULT	RINGER	91
RGRSRSE	RINGER	91
SYMSOC	REGMAT	72
BANDIT	SYMSOC	72
LLTRAN	SYMSOC	72
PREFCE	LLTRAN	72
HOTDOT	LLTRAN	72
TRISLV	SYMSOC	72
PREFCE	TRISLV	72
HOTDOT	TRISLV	72
FOREWD	TRISLV	72
TRISOL	SYMSOC	72
STRMAT	MAIN	112
RINGER	STRMAT	91
RITEPS	RINGER	91
RISULT	RINGER	91
RGRSRSE	RINGER	91
SYMSOC	STRMAT	72
BANDIT	SYMSOC	72

CALL SEQUENCE	CALLING ROUTINE	PAGE
LLTRAN	SYMSOC	72
PREFCE	LLTRAN	72
HOTDOT	LLTRAN	72
TRISLV	SYMSOC	72
PREFCE	TRISLV	72
HOTDOT	TRISLV	72
FOREWD	TRISLV	72
TRISOL	SYMSOC	72
INITAL	MAIN	122
LEBEGE	MAIN	129
FIXEM	LEBEGE	129
WAND	LEBEGE	129
TOBAR	LEBEGE	129
TEMOEG	TOBAR	129
PLYCO	TEMOEG	129
PLYNE	TEMOEG	129
ODE1	LEBEGE	129
ODE2	LEBEGE	157
SHPLAS	LEBEGE	157
SHSRSE	SHPLAS	171
SEPSIS	SHPLAS	171
LINEQU	SEPSIS	171
ORTHKN	SHPLAS	171
LINEQU	ORTHKN	171
EPSIS	SHPLAS	171
LINEQU	EPSIS	171
SMEAR	SHPLAS	171
SAVXES	SHPLAS	171
ARRAYS	SHPLAS	171
GRAPH	LEBEGE	129
ETRAP	MAIN	198

## SUBROUTINE MAIN

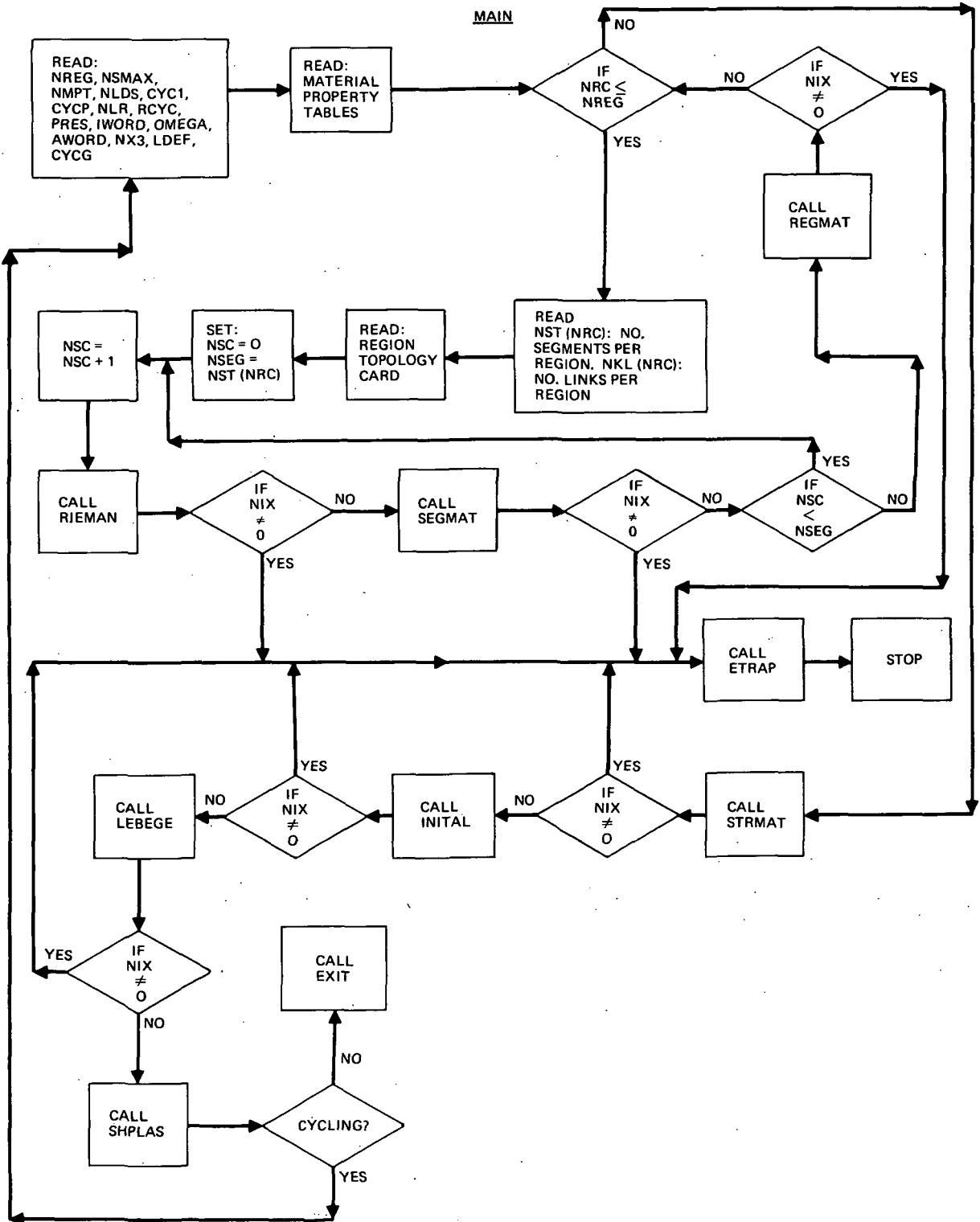
MAIN is the control link for the entire program. Sizing values are read into the program, as well as information for potential load cycling or changes and the material property tables. Calls are made to subroutines RIEMAN and SEGMAT once for each segment in a region; then subroutine REGMAT is called. This procedure is executed once for every region in the structure. Finally calls to subroutines STRMAT, INITAL and LEBEGE are made.

Subroutine SHEPLAS (which is actually called from LEBEGE) updates all the information per load step, and allows the program to loop back to MAIN for the next load increment. If the loading is cycling or progressively changing, the updates for the next load pattern are made before proceeding with the program loops.

There are also several counters in this control link. These are defined as follows:

- NSC - Counts the calls to subroutines RIEMAN and SEGMAT, from 1 to the number of segments within a region.
- NRC - Counts the calls to subroutine REGMAT, from 1 to the number of regions in the structure.
- P - Counts the load steps in the analysis.

The block data and overlay listings are included in this section.





```

RUN, //T STARSS, 1HNHSV440063, KEYJOHNBIN214, 05, 500
ASG, T PUR, T, SAVE05
FREE TPF$.
ASG, T TPF$, F/1/POS/10
FOR, IS BLDATA, BLDATA

```

```

BLOCK DATA
COMMON /NAM1/ FACE(4), STRGO(7), THERM(4), MATER(3), SEG TAB(12)
COMMON /GINT/ AA(8,4), WW(8,4)
DIMENSION A(32), W(32)
EQUIVALENCE (A(1), AA(1,1)), (W(1), WW(1,1))
DATA STRGO /11.0, 13.0, 21.0, 31.0, 12.0, 14.0, 15.0/
DATA THERM /4HST, 4HNOTH, 4HSTCN, 4HTHIN/
DATA MATER /4HISOT, 4HORTH, 4HSTIF/
DATA SEG TAB/4HST10, 4HST11, 4HST12, 4HST13/
1 DATA FACE /4HSING, 4HEQUA, 4HUNEQ, 4HBLAN/
DATA A/0.0, .57735027, .77459667, .86113631, .90617984, .93246951,
D .94910791, .96028986, 0.0, 0.0, 0.0, .33998104, .53846931, .66120939,
A .74153118, .79666648, 0.0, 0.0, 0.0, 0.0, 0.0, .23861919, .40584515,
T .52553241, 0.0, 0.0, 0.0, 0.0, 0.0, 0.0, .40584515, .18343464/
10010
10020
10030
10040
10050
10060
10070
10080
10090
10100
10110
10120
10130
10140
10150
10160
10170
10180
10190
10200
10210
END

```

C

```

FOR,IS MAIN,MAIN
C ..... ROUTINE **MAINPROG** ABACUS UPDATED 01/11/74 ..... 200000
INTEGER SAVJTC,SAVSTP,SEGTAB, Q ,THICK,TYPE 200010
INTEGER XN1,XN 200020
COMMON STORY(16),XMAT(270,10),STD(10),SADUS(30),RADUS(30) 200030
COMMON TADUS(30),UADUS(30),SAVTIC(900) 200040
COMMON XN,TEFREE,TIC,PHI,STOP,RESTOP,RTICK,G1,XNL(3),NH 200050
COMMON NST(30),NKL(30),NXMAT(20),SAVJTC(30),SAVSTP(30),JRTIC(30) 200060
COMMON JRSTOP(30),NREG,NMPT,NRC,NSC,NIX,IERROR,KGEOM,IGEOM,ISTTAB 200070
COMMON KELVIN,IBEGIN,NPROB,NSEG,NERROR,Q,THICK,NOJS,NLINKS,NLCASE 200080
COMMON NTSKL,NZ,NBCT,LINPUT,NTRKL,NPASS,XN1,KBC,NRINGS 200090
COMMON LODE,ICYCLE,LDISTL 200100
COMMON /NAM1/ FACE(4),STRGO(7),THERM(4),MATER(3),SEGTAB(12) 200110
COMMON /LYCORR/ YCORR(80) 200120
COMMON /ARING/ NRING(28),AMAT(30,8),RSIG(12),REPS(12),RALPH(12), 200130
C RBAPH(12) 200140
COMMON /PLS/ OMEGA,IWORD,XMERD,XPRES,XMONT 200150
COMMON /PLSTIC/ IO,JO,IDR,JOR,KORI,NEO 200160
COMMON /CDISP/ P,IMAX,DELP,DELP1,YEPS,ZEPS 200170
COMMON /GRAFIX/ X(100),Y(100,9),NGRAPH,LDEF(9),NGR,JCYC,NFLAG,JAM, 200180
C JNSC 200190
DIMENSION WORD(3) 200200
DATA WORD/'PLAS','NLIN','NLPL'/ 200210
REWIND 1 200240
REWIND 2 200250
REWIND 3 200260
REWIND 4 200270
REWIND 8 200280
REWIND 9 200290
REWIND 10 200300
REWIND 11 200310
REWIND 12 200320
REWIND 13 200330
REWIND 14 200340
REWIND 15 200350
YEPS = 0.999 200360
ZEPS = YEPS-1.0 200370
NCUPLE = 1 200380
NPROB = 1 200390
NGP = 1 200400
NLCASE = NPROB 200410
JDSRN = 28 200420
KDSRN = 23 200430
NFLAG = 0 200440
111 WRITE(6,1726) 200450
1726 FORMAT(1H1) 200460
READ(5,1000,END=555) STOKY 200470
1000 FORMAT(16A4) 200480
LODE = 1 200490
ICT = 0 200500
NH = 0 200510
XN = 0 200520
NIX = 0 200530
Q=5 200540
LDISTL = 5 200550
DO 100 J=1,3 200560
100 XNL(J) = 0.0 200570
READ(5,1001) NREG,NSMAX,NMPT,LINPUT,NLDS,CYC1,CYCP,NLR,RCYC,PRES, 200580
1 IWORD,OMEGA,AWORD,NX3,LDEF,CYCG 200590
1001 FORMAT(I2,I3,3I2,F6.0,F4.0,I2,4X,2F6.0,17X,I2,E14.7/A4,I6,10X,9I1, 200600

```

1 2X,F4.0)	200610
WRITE(6,602) NSMAX,NREG,NMPT,CYC1	
602 FORMAT(////19X,93HUNS YMMETRIC, ORTHOTROPIC, REINFORCED SHELL ANALY	200630
1SIS WITH COUPLING OF AT MOST 29 SHELL REGIONS,//62X,'STARS-2P',//	200640
262X,	200650
3'AS OF JULY 1, 1973'////8X,21HNUMBER OF SEGMENTS = ,I3,21H NUMBER	200660
4OF REGIONS = ,I2,43H NUMBER OF MATERIAL PROPERTY TABLES USED = ,I2	200670
5 ,17H NO. OF CYCLES = ,F6.0)	
DO 115 J=1,3	200690
115 IF (WORD(J).EQ.AWORD) GO TO 106	200700
STOP	200710
106 JPLS = J	200720
GO TO (615,616,617),JPLS	200730
615 WRITE(6,618)	200740
618 FORMAT(///55X,'ELASTIC-PLASTIC PROBLEM')	200750
GO TO 621	200760
616 WRITE(6,619)	200770
619 FORMAT(///50X,'LARGE DEFLECTION ELASTIC PROBLEM')	200780
GO TO 621	200790
617 WRITE(6,620)	200800
620 FORMAT(///50X,'LARGE DEFLECTION PLASTIC PROBLEM')	200810
621 CONTINUE	200820
WRITE(6,625)	200830
625 FORMAT(///)	200840
WRITE(6,605) (STORY(I),I=1,16)	200850
605 FORMAT(11(/),8X,16A4,18(/),80X,35HFOR INFORMATION CALL V. SVALBO	200860
1NAS/117X,14H(516) 575-7701/103X,10HP. OGILVIE//103X,9HH. LEVINE)	200870
NGRAPH = 0	200880
DO 700 J=1,9	200890
700 IF (LDEF(J).NE.0) NGRAPH = NGRAPH+1	200900
NGR = 0	200910
NEO = 0	200920
IF (PRES.NE.0.0) NEO = 1	200930
IF (NEO.EQ.0) GO TO 300	200940
IF (JPLS.GT.1) XNL(1) = 1.0	200950
IF (JPLS.NE.2) XNL(2) = 1.0	200960
IF (NX3.EQ.1) XNL(3) = -1.0	200970
300 IO = 13	200980
JO = JDSRN-IO	200990
IOR = 11	201000
P = PRES	201010
DELP = 1.0/CYC1	201020
DELP1 = DELP	201030
OMEGA = OMEGA*OMEGA	201040
NMAT = 1	201050
IF (CYCP.EQ.0.0) CYCP = 1.0	201060
IF (NLR.LE.1) GO TO 121	201070
LODE = 16	201080
REWIND LODE	201090
121 CONTINUE	201100
NROW = 0	201110
ICT = ICT+1	201120
ICYCLE = 0	201130
IF (ICT.EQ.1) ICYCLE = RCYC	201140
ICYC1 = ABS(CYC1)	201150
IMAX = ICYC1	201160
IF (NMAT.EQ.0) GO TO 1	201170
KK=-1	201180
NSAVE=0	201190
DO 13 I=1,NMPT	201200
KK=KK+2	201210

	NXMAT(KK)=NROW+1	201220
	II=NROW+1	201230
	READ(5,1004) STD(I),TYPE	201240
1004	FORMAT (A4,6X,A4,6X)	201250
	NROW = 27	201260
	DO 11 L=1,3	201270
11	IF(TYPE.EQ.MATER(L)) GOTO 12	201280
	GO TO 8000	201290
12	CONTINUE	201300
	IF (L.EQ.1) NROW = 7	201310
	IF (L.EQ.2) NROW = 17	201320
	LLL=NSAVE+NROW	201330
	READ (5,1005) ((XMAT(M,J),J=1,10),M=II,LLL )	201340
1005	FORMAT (5E14.7)	201350
	NROW=NSAVE+NROW	201360
	NXMAT(KK+1)=LLL	201370
13	NSAVE=NROW	201380
	READ(5,2000)	201390
2000	FORMAT(1X)	201400
1	CONTINUE	201410
	P = P+1.0	201420
	ICYCLE = ICYCLE+1	201430
	NGR = 0	201440
	IF (P.NE.CYCG*NGP) GO TO 10	201450
	NGR = 1	201460
	NGP = NGP+1	201470
10	CONTINUE	201480
	C = ICYCLE	201490
	IBEGIN = 0	201500
	N = C/CYCP	201510
	PP = N*CYCP	201520
	IF ((C.EQ.1.0.OR.C.EQ.PP.OR.ICYCLE.EQ.ICYCL.OR.NH.EQ.0).AND.	201530
1	LINPUT.EQ.1) IBEGIN = 1	201540
	JOR = KDSRN-IOR	201550
	DO 99 NRC=1,NREG	201560
	IF (NH.EQ.0.OR.IBEGIN.EQ.1) WRITE(6,1726)	201570
	IF (Q.EQ.5) READ(5,1003) NST(NRC),NKL(NRC),NRING(NRC),STORY	201580
1003	FORMAT(3I2,16A4)	201590
	IF (NH.NE.0) GO TO 613	201600
	WRITE(6,606)NRC,NST(NRC),NKL(NRC)	201610
606	FORMAT(//////////58X,13HREGION NUMBER,I3//35X,10HTH	201620
	HERE ARE ,I2,14H SEGMENTS AND ,I2,35H KINEMATIC LINKS WITHIN THIS R	201630
	2EGION)	201640
	GO TO 610	201650
613	IF (IBEGIN.EQ.0) GO TO 610	201660
	WRITE(6,612) NRC,NST(NRC),NKL(NRC)	201670
612	FORMAT(///58X,13HREGION NUMBER,I3//35X,10HTHERE ARE ,I2,14H SEGMENT	201680
	ITS AND ,I2,35H KINEMATIC LINKS WITHIN THIS REGION)	201690
610	CONTINUE	201700
	IF (Q.EQ.5) READ(5,1006) JRTIC(NRC),JRSTOP(NRC),STORY	201710
1006	FORMAT(5X,2I5,16A4)	201720
	NSEG = NST(NRC)	201730
201	NSC=0	201740
101	NSC=NSC+1	201750
	IF (NH.EQ.0.OR.IBEGIN.EQ.1) WRITE(6,1726)	201760
	CALL RIEMAN	201770
	IF (NIX.NE.0) GOTO 8888	201780
	CALL SEGMA	201790
	IF (NIX.NE.0) GOTO 8888	201800
	IF(NSC.LT.NSEG) GO TO 101	201810
	NSC= 0	201820

102	CALL REGMAT	201830
	IF(NIX.LT.0) GO TO 8888	201840
	NIX = 0	201850
	REWIND 2	201860
	REWIND 3	201870
99	CONTINUE	201880
	IF (C.EQ.1.0.OR.C.EQ.PP.OR.ICYCLE.EQ.ICYCL.OR.NH.EQ.0) IBEGIN = 1	201890
103	CALL STRMAT	201900
	IF (NIX.NE.0) GOTO 8888	201910
	REWIND 1	201920
105	CALL INITAL	201930
	REWIND IO	201940
	REWIND JO	201950
	REWIND LODE	201960
	CALL LEBEGE	201970
	REWIND IOR	201980
	REWIND JOR	201990
	IO = JOSRN-IO	202000
	JO = JOSRN-IO	202010
	REWIND IO	202020
	REWIND JO	202030
	IOR = KOSRN-IOR	202040
	Q = 1	202050
	REWIND 1	202060
	REWIND 2	202070
	REWIND 3	202080
	REWIND 4	202090
	REWIND 8	202100
	REWIND 9	202110
	REWIND 10	202120
	REWIND 11	202130
	REWIND 12	202140
	REWIND 13	202150
	REWIND 14	202160
	REWIND 15	202170
	REWIND LODE	202180
	JCYC = P	202190
	WRITE(6,2500) JCYC,ICYCLE	202200
2500	FORMAT(/5X,'CYCLE',I5,',',I5,' IS COMPLETE.')	202210
	IF (ICYCLE.NE.1.AND.NH.NE.0) GO TO 112	202220
	NH = 1	202230
	DELPI = DELP	202240
	LDISTL = 1	202250
112	CONTINUE	202260
	IF (JPLS.GT.1) XNL(1) = 1.0	202270
	IF (JPLS.NE.2) XNL(2) = 1.0	202280
	IF (NX3.EQ.1) XNL(3) = -1.0	202290
	IF (NIX.NE.0) GO TO 8888	202300
	IF (ICYCLE.EQ.ICYCL) GO TO 556	202310
	GO TO 1	202320
556	IF (NLDS.LE.ICT) GO TO 111	202330
	READ(5,1010) LINPUT,CYC1,CYCP,LDISTL,NMAT,OMEGA	202340
1010	FORMAT(7X,I2,2X,F6.0,F4.0,2X,2I2,3IX,E14.7)	202350
	DELP = 1.0/CYC1	202360
	IF (LDISTL.EQ.0) LDISTL = 1	202370
	OMEGA = OMEGA*OMEGA	202380
	GO TO 121	202390
555	IF (NGRAPH.NE.0) CALL ENDJOB	202400
	STOP	202410
8000	IERROR=8000	202420
	NERROR= 1	202430

**Page Intentionally Left Blank**

```
MAP,IS SYM,STARSS
LIB SYS$*MSFC$.
SEG ROOT
IN NBF24$
IN MAIN,BLDATA
SEG RIE*,(ROOT)
IN RIEMAN,SETUP,ROBOT,GEOMET,PLINE,PLICO
SEG DF1*,(RIE)
IN DIF1
SEG DF2*,(RIE)
IN DIFF2
SEG SGMAT*,(ROOT)
IN SGMAT,SREVN2
SEG RING*,(ROOT)
IN RINGER,RISULT,RITEPS,RGRSE,SYMSOC,BANDIT,LLTRAN,TRISLV,HOTDOT
SEG REG*,(RING)
IN REGMAT
SEG STR*,(RING)
IN STRMAT
SEG INI*,(ROOT)
IN INITAL
SEG LEB*,(ROOT)
IN LEBEGE,FIXEM,TOBAR,TEMOEG,PLYNE,PLYCO
SEG OD1*,(LEB)
IN ODE1
SEG OD2*,(LEB)
IN ODE2
SEG TRAP*,(ROOT)
IN ETRAP
COPOUT TPF$.,PUR.
XQT STARSS
```

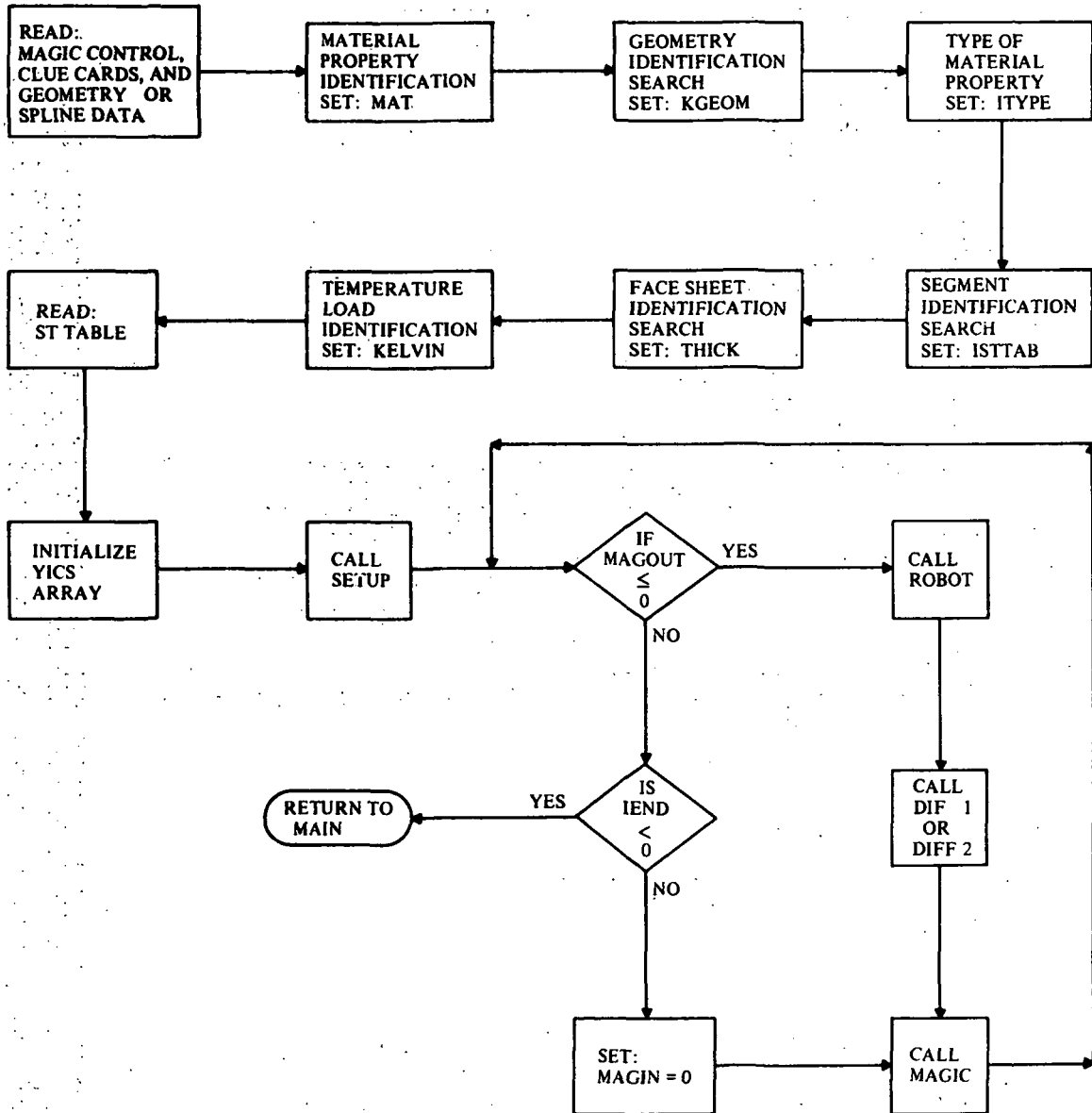
## SUBROUTINE RIEMAN

This subroutine link assembles the data tables for use in the integration procedure. The subprogram link, RIEMAN, utilizes the subroutines SETUP, ROBOT, DIF1 or DIFF2, to integrate the differential equations of each segment independently, under arbitrary load conditions. The results of the integrations of each segment are stored in the YCORR array in RIEMAN, and represent the stiffness and deflection coefficients of each segment.



FORTRAN CODE	ENGINEERING SYMBOLS (REF. 1)
XFTHLD	$r_{\theta}$
XFPHLD	$r_{\phi}$
XFZELD	$r_{\zeta}$
XMTHLD	$m_{\theta}$
XMPHLD	$m_{\phi}$
ETHET	$E_{\theta}$
EPHI	$E_{\phi}$
XGPT	$G_{\phi\theta}$
XNUTP	$v_{\theta\phi}$
XNUPT	$v_{\phi\theta}$
ALPHTH	$\alpha_{\theta}$
ALPHPH	$\alpha_{\phi}$
XNTTH	$N_{T\theta}$
XNTPH	$N_{T\phi}$
XMTTH	$M_{T\theta}$
XMTPH	$M_{T\phi}$
XK11	$K_{11}$
XK22	$K_{22}$
XD11	$D_{11}$
XD22	$D_{22}$
XK33	$K_{33}$
XD33	$D_{33}$

RIEMAN



```

FOR,IS RIEMAN,RIEMAN
C ..... ROUTINE ** RIEMAN ** ABACUS UPDATED 01/11/74 ..... 300000
SUBROUTINE RIEMAN 300010
INTEGER SAVJTC, SAVSTP, SEGTAB, Q , THICK, TYPE 300020
INTEGER XN 300030
DOUBLE PRECISION YNEW, YPRED 300040
COMMON STORY(16), XMAT(270, 10), STD(10), SADUS(30), RADUS(30) 300050
COMMON TADUS(30), UADUS(30), SAVTIC(900) 300060
COMMON XN, TEFREE, TIC, PHI, STOP, RESTOP, RTICK, G1, XNL(3), NH 300070
COMMON NST(30), NKL(30), NXMAT(20), SAVJTC(30), SAVSTP(30), JRTIC(30) 300080
COMMON JRSTOP(30), NREG, NMPT, NRC, NSC, NIX, IERROR, KGEOM, IGEOM, I STTAB 300090
COMMON KELVIN, IBEGIN, NPROB, NSEG, NERROR, Q, THICK, NOJS, NLINKS, NLCASE 300100
COMMON NTSKL, NZ, NBCT, LINPUT, NTRKL, NPASS, NI, KBC, NRINGS 300110
COMMON LODE, ICYCLE, LDISTL 300120
COMMON /NAM1/ FACE(4), STRGO(7), THERM(4), MATER(3), SEGTAB(12) 300130
COMMON /LYCORR/ YCORR(72) 300140
COMMON /MAGIK/ KKNT 300150
COMMON /EQUAZN/ YPRED(72), YDOT(72), YASAVE(72), 300160
1 YANTH, YAMTH, YAMPT, YAJPH, 300170
2 S, SN, CS, SNSQ, CSSQ, TAN, SEC, CN, X1CS, X1SN, TN, 300180
3 X1RO, X1ROSQ, X1SNRO, X1CSRO, CN1RO, SN1RO, CS1RO, 300190
4 X1R1, X1R2, CS1R1, CS1R2, SN1R1, X1R1SQ, R2SQ, RO, BESQ, 300200
5 ROSQ, XNSQ, BETA, R1, R2, S1, RIDOT, 300210
6 XNTTH, XNTPH, XMTTH, XMPH, XFTHLD, XFPHLD, XFZELD, 300220
7 XMTHLD, XMPHLD, ETHET, EPHI, XGPT, ALPHTH, ALPHPH, 300230
8 XNUTP, XNUPT, XC11, XC22, XC15, XD33, XD22, XD21, XD12, 300240
9 XK11, XK12, XK21, XK22, XK33, XD11, 300250
A XNPHI, M, I, BETTA, ZETTA, XC16 300260
COMMON /SPLINS/ ANG, PSI(100), RAD(100), CUR1(100), CUR2(100), 300270
1 DR1DP(100), ZI(14), RI(14), NRZIN 300280
COMMON /ARING/ NRING(28), AMAT(30, 8), RSIG(12), REPS(12), RALPH(12), 300290
C RBAPH(12) 300300
COMMON /PLS/ OMEGA, IWORD, XMERD, XPRES, XMONT 300310
COMMON /PLSTIC/ IO, JO, IOR, JOR, KORI, NEO 300320
COMMON /WOOD/ SAVY(53), NPLEV, NLPD, NPLA(21), STR(6), SIGMA(3, 21), 300330
C SEPS(3, 21), SALPH(3, 21), SBAPH(3, 21), STEPS(3, 21), 300340
O EFF(21), STSRN(3), NPLAST(3), STSIG(3), STREPS(3), 300350
M STALPH(3), STBAPH(3), EFFST(3), NPLEVS(3) 300360
COMMON /CMAIN/ ZETA1(21), ZETA2(21), NODE, ALF(4), CE(4), NLRS, HI, HD, T 300370
DIMENSION LST(13), YDEV(72), YICS(72), YNEW(72) 300380
DIMENSION TBDEL(72), FWDEL(72) 300390
DIMENSION ST(30, 31), XLAYER(26), HARD(3) 300400
DATA HARD/'ISOT', 'KINE', 'PERF'/' 300410
DATA APEX1/'APEX'/' 300420
1726 FORMAT(1H1) 300430
IF(Q.EQ.1) GO TO 191 300440
READ(5, 1001) RGO, ANG, NLRS, STORY 300450
1001 FORMAT(F2.0, A1, I2, 16A4) 300460
C GEOMETRY IDENTIFICATION SEARCH 300470
DO 504 I=1, 7 300480
IF(RGO-STRGO(I)) 504, 505, 504 300490
504 CONTINUE 300500
GOTO 8086 300510
505 KGEOM=I 300520
IGEOM = 0 300530
IF (KGEOM.EQ.1.OR.KGEOM.EQ.2.OR.KGEOM.EQ.5.OR.KGEOM.EQ.6) IGEOM =1 300540
IF (KGEOM.EQ.3) IGEOM=2 300550
IF (KGEOM.EQ.4) IGEOM=3 300560
IF ( KGEOM.EQ.7 ) IGEOM = 1 300570
WRITE(1) KGEOM, IGEOM, RGO, ANG, NLRS, STORY 300580
READ(5, 1002) OTAU, DIFF, STEP, APEX 300590
1002 FORMAT(3E14.1, 3X, A4) 300600

```

NAPEX = 0	300610
IF (APEX.EQ.APEX1) NAPEX = 1	300620
DELTA = 0.0	300630
WRITE(1) DTAU,DIFF,STEP,DELTA,NAPEX	300640
IF (RGD.EQ.14.0) GO TO 180	300650
READ(5,1006) G1,G2,G3	300660
1006 FORMAT(3E14.1)	300670
WRITE(1) G1,G2,G3	300680
GO TO 481	300690
180 READ(5,198) NRZIN,(ZI(J),RI(J),J=1,NRZIN)	300700
198 FORMAT(I2,7F10.0/7F10.0)	300710
WRITE(1) NRZIN,(ZI(J),RI(J),J=1,NRZIN)	300720
481 CONTINUE	300730
READ(5,1003) TYPE,HLAYR,SHEET,INTERP,RANKIN,HARDEN,NP	300740
1003 FORMAT(6(A4,6X),10X,I2)	300750
IF(NP.LT.2.OR.NP.GT.30) GO TO 8787	300760
C MATERIAL PROPERTY IDENTIFICATION	300770
DO 501 I=1,NMPT	300780
IF (HLAYR-STD(I)) 501,502,501	300790
502 MAT=I	300800
GOTO 503	300810
501 CONTINUE	300820
GOTO 8036	300830
503 DO 506 I=1,3	300840
IF(TYPE-MATER(I))506,507,506	300850
506 CONTINUE	300860
GOTO 8087	300870
507 ITYPE=1	300880
DO 510 I=1,12	300890
IF(INTERP-SEGTAB(I))510,511,510	300900
510 CONTINUE	300910
GO TO 8088	300920
511 ISTTAB=I	300930
DO 508 I=1,4	300940
IF (SHEET.EQ.FACE(I)) GOTO 509	300950
508 CONTINUE	300960
GOTO 8089	300970
509 THICK=1	300980
KLUE2=1	300990
GO TO (430,430,420,420,420,420,425,425,425, 430,430,430),ISTTAB	301000
420 KLUE2=2	301010
GO TO 430	301020
425 KLUE2=3	301030
430 KLUE1=THICK	301040
C TEMPERATURE LOAD IDENTIFICATION	301050
DO 401 I=1,4	301060
IF(RANKIN.EQ.THERN(I))GOTO 402	301070
401 CONTINUE	301080
GOTO 8090	301090
402 KELVIN=I	301100
C LINEAR ANALYSIS IDENTIFICATION	301110
IANYZ = 1	301120
IWD = 1-IWORD	301130
NROW = 3-IWD	301140
IF (THICK.GT.1) NROW = THICK+3-2*IWD	301150
IF (ISTTAB.EQ.1) NROW = 14-3*IWD	301160
IF (ISTTAB.EQ.3) NROW = 16-3*IWD	301170
IF (ISTTAB.EQ.4) NROW = 10-2*IWD	301180
IF (ISTTAB.EQ.5) NROW = 12-3*IWD	301190
IF (ISTTAB.EQ.6) NROW = 13-3*IWD	301200
IF (ISTTAB.EQ.7) NROW = 9-2*IWD	301210

IF (ISTTAB.EQ.8) NROW = 11-3*IWD	301220
IF (ISTTAB.EQ.9) NROW = 12-3*IWD	301230
IF (ISTTAB.EQ.10) NROW = 15-3*IWD	301240
IF (ISTTAB.EQ.11) NROW = 17-4*IWD	301250
IF (ISTTAB.EQ.12) NROW = 18-4*IWD	301260
IF (KELVIN.EQ.2.OR.KELVIN.EQ.4) GO TO 580	301270
IF (ISTTAB.GE.10) GO TO 581	301280
IF (ISTTAB.GE.4) NROW = NROW+1	301290
GO TO 580	301300
581 NROW = NROW+2	301310
580 CONTINUE	301320
TEFREE = 0.0	301330
DO 540 I=1,3	301340
IF (HARDEN-HARD(I)) 540,541,540	301350
541 KOR = I	301360
GO TO 542	301370
540 CONTINUE	301380
NERROR = 8013	301390
GO TO 8888	301400
542 IF (ITYPE.EQ.1) GO TO 550	301410
IF (KOR.GT.1) GO TO 551	301420
NERROR = 8008	301430
GO TO 8888	301440
551 KORI = 1	301450
GO TO 553	301460
550 KORI = -1	301470
IF (KOR.EQ.1) KORI = 0	301480
553 CONTINUE	301490
WRITE(1) ITYPE,MAT,THICK,ISTTAB,KELVIN,KORI,TEFREE,NP,KLUE1,KLUE2,	301500
1 IANLYZ,NROW	301510
GO TO 192	301520
191 READ(1) KGEOM,IGEOM,RGO,ANG,NLRS,STORY	301530
READ(1) DTAU,DIFF,STEP,DELTA,NAPEX	301540
IF (RGO.EQ.14.0) GO TO 182	301550
READ (1 ) G1,G2,G3	301560
GO TO 183	301570
182 READ(1) NRZIN,(ZI(J),RI(J),J=1,NRZIN)	301580
183 CONTINUE	301590
READ(1) ITYPE,MAT,THICK,ISTTAB,KELVIN,KORI,TEFREE,NP,KLUE1,KLUE2,	301600
1 IANLYZ,NROW	301610
192 EPSIL =1.0E-05	301620
DIFF =1.0E-04	301630
ERR = 1.0 E-07	301640
IF (NH.NE.0) GO TO 920	301650
I = RGO	301660
WRITE(6,651) NSC,I,STORY,DTAU,DIFF,STEP,DELTA	301670
651 FORMAT(/13X,15HSEGMENT NUMBER ,12,5X,13HSEGMENT CODE ,12,5X,	301680
1 16A4//22X,4HDTAU,15X,4HDIFF	301690
2,15X,4HSTEP,10X,5HDELTA//16X,5(E14.7,5X),2X,F2.0)	301700
IF (RGO.EQ.14.0) GO TO 185	301710
WRITE(6,652) G1,G2,G3	301720
652 FORMAT(/54X,24HGEOMETRY INPUT VARIABLES,//38X,3(E14.7,5X))	301730
GO TO 645	301740
185 WRITE(6,186) (ZI(I),RI(I),I=1,NRZIN)	301750
186 FORMAT(/57X,24HGEOMETRY INPUT VARIABLES//42X,16HAXIAL COORDINATE,	301760
1 9X,6HRADIUS/50X,1HZ,20X,1HR/(43X,1P1E15.8,5X,1P1E15.8))	301770
645 WRITE(6,653) TYPE,HLAYR,SHEET,INTERP,RANKIN,HARDEN,NP	301780
653 FORMAT(/12X,5(A4,6X),16HHARDENING LAW = ,A4,12X,	301790
1 26HNUMBER OF TABLE COLUMNS = ,I2)	301800
920 CONTINUE	301810
L= 2*(MAT-1)+1	301820
II=NXMAT(L)	301830

III=NXMAT(L+1)	301840
IF (NH.NE.0) GO TO 921	301850
WRITE(6,654) ((XMAT(I,J),J=1,10),I=II,III)	301860
654 FORMAT(/51X,28HMATERIAL PROPERTY TABLE USED,/(10(1H ,E12.5)))	301870
WRITE(6,655)	301880
655 FORMAT(/42X, 47HTABLE ORDER PHI OR S VS. CROSECTION PROPERTIES,)	301890
921 CONTINUE	301900
DO 901 I=1,NROW	301910
IF(Q.EQ.1) GO TO 193	301920
READ (5,1005) (ST(I,J),J=1,NP)	301930
1005 FORMAT (5E14.7)	301940
WRITE(1) (ST(I,J),J=1,NP)	301950
IF (NH.NE.0) GO TO 901	301960
194 WRITE(6,600) (ST(I,J),J=1,NP)	301970
600 FORMAT(1H ,8(E14.7,2X)/(3X,8(E14.7,2X)))	301980
GO TO 901	301990
193 READ (1) (ST(I,J),J=1,NP)	302000
901 CONTINUE	302010
DO 750 JJ=1,12	302020
750 LST(JJ) = 0	302030
NLCS = NLCASE	302040
NLPO = NLRS+1	302050
KBC = NLPO	302060
IF (THICK.NE.1) KBC = 2.0*NLPO	302070
TAP1 = NLRS/2	302080
DO 290 I=1,NLPO	302090
TAP2 = I-1	302100
ZETA1(I) = 1.0-TAP2/TAP1	302110
290 ZETA2(I) = 1.0-FLOAT(I-1)/FLOAT(NLRS)	302120
K=NROW+1	302130
JJ=1	302140
JJJ=6	302150
MM=1	302160
DO 17 NLC=1,NLCS	302170
JT = JJ	302180
JTT= JJJ	302190
L=0	302200
IF (LDISTL.EQ.1) GO TO 195	302210
READ(5,1004) (LST(J),J=JJ,JJJ)	302220
1004 FORMAT(6I1)	302230
WRITE(LODE) (LST(J),J=JJ,JJJ)	302240
GO TO 196	302250
195 READ(LODE) (LST(J),J=JJ,JJJ)	302260
196 CONTINUE	302270
IF(LST(JJ))8031,19,20	302280
20 L = LST(JJ)	302290
19 JJ=JJ+1	302300
23 IF(LST(JJ))8031,22,21	302310
21 L=L+1	302320
22 IF(JJ.EQ.JJJ) GOTO 24	302330
JJ=JJ+1	302340
GOTO 23	302350
24 IF(L.EQ.0) GO TO 71	302360
KK = K + L - 1	302370
DO 72 M=K,KK	302380
IF (LDISTL.EQ.1) GO TO 197	302390
READ (5,1005) (ST(M,J),J=1,NP)	302400
WRITE(LODE) (ST(M,J),J=1,NP)	302410
GO TO 72	302420
197 READ(LODE) (ST(M,J),J=1,NP)	302430
72 CONTINUE	302440

IF (LST(JT).EQ.0) GO TO 660	302450
LY = K	302460
KY = K	302470
KZ = K+LST(1)-1	302480
K = KZ+1	302490
IF (ICYCLE.NE.1.AND.NH.NE.0) GO TO 665	302500
WRITE(6,656)	302510
656 FORMAT(/45X,42HTABLE ORDER PHI OR S VS. TEMPERATURE LOADS,)	302520
DO 657 N=KY,KZ	302530
WRITE(6,600) (ST(N,J),J=1,NP)	302540
657 CONTINUE	302550
660 IF((L-LST(JT)).EQ.0) GO TO 665	302560
IF (NH.NE.0) GO TO 665	302570
WRITE(6,661) NLC	302580
661 FORMAT(/16X,8HPROBLEM ,12,5X,84HTABLE ORDER PHI OR S VS. DISTRIB	302590
LUTED LOADS (F THETA, F PHI, F ZETA, M THETA, M PHI),)	302600
WRITE(6,1968) (LST(J),J=JT,JTT)	302610
1968 FORMAT(27H LOAD IDENTIFICATION CLUES ,6I1/)	302620
DO 662 N = K, KK	302630
WRITE(6,600) (ST(N,J),J=1,NP)	302640
662 CONTINUE	302650
665 CONTINUE	302660
71 K = K + L - LST(JT)	302670
JJ=JJJ+1	302680
JJJ=JJ+5	302690
17 MM=MM+1	302700
590 CONTINUE	302710
IF (Q.EQ.1) GO TO 2004	302720
READ (5,591) IS,SAVJTC(IS),SAVSTP(IS),(STORY(I),I=1,16)	302730
591 FORMAT (3I5,16A4)	302740
READ(5,2000)	302750
2000 FORMAT(1X)	302760
WRITE(1) IS,SAVJTC(IS),SAVSTP(IS),STORY	302770
GO TO 2005	302780
2004 READ(1) IS,SAVJTC(IS),SAVSTP(IS),STORY	302790
2005 CONTINUE	302800
ITIC = SAVJTC(IS)	302810
ISTOP = SAVSTP(IS)	302820
JTIC = JRTIC(NRC)	302830
JSTOP = JRSTOP(NRC)	302840
TIC = ST(1,1)	302850
STOP = ST(1,NP)	302860
NEQNS=64+8*NPROB	302870
DO 73 I=1,NEQNS	302880
73 YICS(I)=0.0	302890
YICS(5) =1.0	302900
YICS(14)=1.0	302910
YICS(23)=1.0	302920
YICS(32)=1.0	302930
YICS(33)=1.0	302940
YICS(42)=1.0	302950
YICS(51)=1.0	302960
YICS(60)=1.0	302970
NCYC=0	302980
KKNT = 0	302990
NSAVE=NROW	303000
IEND=0	303010
PRINT=TIC	303020
DTA=DTAU	303030
DTAU = 0.DO	303040
IF (NH.NE.0.OR.NEO.NE.0)	303050
1READ(IO) SAVY	303060

2001	FORMAT(1X,1P1E16.7,15,1P6E16.7)	303070
59	CALL SETUP (MAGIN,MAGOUT,TIC,STEP,NEQNS,DTAU,EPSIL,DELTA,ERR,TIME, 1DTIME,YICS,YPRED,YCORR,YDOT,YNEW,YDEV,FWDEL,TBDEL)	303080
	GOTO 61	303090
60	CALL MAGIC (MAGIN,MAGOUT,TIC,STEP,NEQNS,DTAU,EPSIL,DELTA,ERR,TIME, 1DTIME,YICS,YPRED,YCORR,YDOT,YNEW,YDEV,FWDEL,TBDEL)	303100
61	IF(MAGOUT.LE.0) GOTO 25	303120
	IF(TIME.GT.STOP) GOTO 62	303130
	IF(TIME.LT.STOP) GOTO 63	303140
64	IEND=-1	303150
	GOTO 67	303160
62	IF(TIME.LE.(STOP+DIFF)) GOTO 64	303170
	GOTO 8001	303180
63	IF((STOP-DIFF).LE.TIME) GOTO 64	303190
	IF((TIME+DTIME).GT.STOP) GOTO 65	303200
	IF(PRINT.GT.TIME) GOTO 66	303210
	PRINT=TIME+DTA	303220
67	CONTINUE	303230
	IF(IEND.GT.0) GOTO 8002	303240
	IF(IEND.LT.0) GOTO 150	303250
66	CONTINUE	303260
	MAGIN = 0	303270
	GOTO 60	303280
65	DTIME=STOP-TIME	303290
	DELTA = 0.D0	303300
	GOTO 67	303310
75	NCYC=NCYC+1	303320
	MAGIN=-1	303330
	GOTO 60	303340
25	LT=0	303350
	IF ((NH.NE.0.OR.NEO.NE.0).AND.KKNT.EQ.3)	303360
	1 READ(IO) SAVY	303370
	JJ = NLCASE*6	303380
	DO 15 J=1,JJ	303390
15	LT=LT+LST(J)	303400
296	NTOTAL = LT+NSAVE	303410
	PHI=TIME	303420
	ARG=PHI	303430
	LL=NP+1	303440
	DO 51 I=1,NP	303450
	IF(ARG-ST(1,I)) 52,55,51	303460
52	IF(I-1) 55,55,54	303470
51	CONTINUE	303480
	I=NP	303490
	GO TO 55	303500
54	DO 57 IK=2,NTOTAL	303510
57	ST(IK,LL)=ST(IK,I-1)+(ST(IK,I)-ST(IK,I-1))*(ARG-ST(1,I-1))/(ST(1,I-1)-ST(1,I-1))	303520
	GOTO 80	303530
55	DO 58 IK=2,NTOTAL	303540
58	ST(IK,LL)=ST(IK,I)	303550
80	CONTINUE	303560
		303570
C	THE UPDATED INTERPOLATED VALUES OF THE MATERIAL PROPERTY COEFFIC	303580
C	IENTS ARE FOUND IN THE XMAT TABLE AND STORED IN THE XLAYER ARRAY	303590
	L = (MAT-1)*2+1	303600
	II=NXMAT(L)	303610
	III = NXMAT(L+1)	303620
	LL=NP+1	303630
	L=NROW + 1	303640
	M=1	303650
	GOTO (91,92,93,93),KELVIN	303660



91	ARG = (ST(L,LL)+ST(L+1,LL)+ST(L+2,LL)+ST(L+3,LL))/4.0	303670
	GOTO 94	303680
93	CONTINUE	303690
	ARG = ST(NROW+1,LL)	303700
94	DO 104 I = 2,10	303710
	IF (ARG-XMAT(II,I)) 121,123,104	303720
121	IF (I-2) 8007,8007,124	303730
104	CONTINUE	303740
	GOTO 8067	303750
123	L=II+1	303760
	DO 122 J=L,III	303770
	XLAYER(M)=XMAT(J,I)	303780
122	M=M+1	303790
	GOTO 111	303800
124	L=II+1	303810
	DO 125 J=L,III	303820
	XLAYER(M)=XMAT(J,I-1)+(XMAT(J,I)-XMAT(J,I-1))*(ARG-XMAT(II,I-1))/	303830
	1 (XMAT(II,I)-XMAT(II,I-1))	303840
125	M=M+1	303850
	GOTO 111	303860
92	L = II + 1	303870
	DO 922 J=L,III	303880
	XLAYER(M)= XMAT(J,1)	303890
922	M=M+1	303900
111	CONTINUE	303910
115	GO TO(101,102,103), ITYPE	303920
101	ETHET = XLAYER(1)	303930
	XNUTP = XLAYER(2)	303940
	ALPHTH = XLAYER(3)	303950
	EPHI = ETHET	303960
	XNUPT= XNUTP	303970
	ALPHPH = ALPHTH	303980
	XGPT = ETHET/(2.0*(1.0+XNUPT))	303990
	N = 4	304000
	GO TO 105	304010
102	ETHET = XLAYER(1)	304020
	EPHI = XLAYER(2)	304030
	XNUTP = XLAYER(3)	304040
	ALPHTH = XLAYER(4)	304050
	ALPHPH = XLAYER(5)	304060
	XGPT = XLAYER(6)	304070
	XNUPT = ETHET*XNUTP/EPHI	304080
	N = 7	304090
	GO TO 105	304100
103	ETHET = XLAYER(1)	304110
	EPHI = XLAYER(2)	304120
	XNUTP= XLAYER(3)	304130
	ALPHTH = XLAYER(4)	304140
	ALPHPH = XLAYER(5)	304150
	XGPT = XLAYER(6)	304160
	ER = XLAYER(17)	304170
	ES = XLAYER(18)	304180
	ALPHR = XLAYER(19)	304190
	ALPHS = XLAYER(20)	304200
	SIGOXR=XLAYER(23)	
	SIGOXS=XLAYER(26)	
	XNUPT = ETHET*XNUTP/EPHI	304210
	N = 7	304220
105	CONTINUE	304230
	SIGOX = XLAYER(N+2)	304240
	CALL ROBOT (ST,KLUE2,NROW,LL,ER,ES,G2,G3,TIME,ITIC,JTIC,NCYC,	304250
	1 SIGOX,ALPHR,ALPHS,SIGOXR,SIGOXS)	

IF (NIX.NE.0) GO TO 9999	304270
C COMPUTATION OF K AND D FOR K AND D INPUT	304280
LL=NP+1	304290
IF(XK11.EQ.0.0) GOTO 8101	304300
IF(ITYPE.EQ.3.AND.XK12.EQ.0.) GO TO 8102	304310
IF(ITYPE.EQ.3.AND.XK21.EQ.0.) GO TO 8103	304320
IF(XK22.EQ.0.0) GOTO 8104	304330
IF(XK33.EQ.0.0) GOTO 8105	304340
IF(XD11.EQ.0.0) GOTO 8106	304350
IF(ITYPE.EQ.3.AND.XD12.EQ.0.) GO TO 8107	304360
IF(ITYPE.EQ.3.AND.XD21.EQ.0.) GO TO 8108	304370
IF(XD22.EQ.0.0) GOTO 8109	304380
IF(XD33.EQ.0.0) GOTO 8110	304390
NL=0	304400
XSAVE1 = XNTTH	304410
XSAVE2 = XNTPH	304420
XSAVE3 = XMTTH	304430
XSAVE4 = XMTPH	304440
XSAVE5 = XNL(2)	304450
XSAVE6 = XNL(3)	304460
XNTTH = 0.0	304470
XNTPH = 0.0	304480
XMTTH = 0.0	304490
XMTPH = 0.0	304500
XFTHLD=0.0	304510
XFPHLD=0.0	304520
XFZELD=0.0	304530
XMTHLD=0.0	304540
XMPHLD=0.0	304550
XNL(2) = 0.0	304560
XNL(3) = 0.0	304570
JF=8+NPROB	304580
K = NROW	304590
DO 77 M=1, JF	304600
I = (M-1)*8 + 1	304610
IF (M.LT.9) GOTO 49	304620
XNTTH = XSAVE1	304630
XNTPH = XSAVE2	304640
XMTTH = XSAVE3	304650
XMTPH = XSAVE4	304660
XNL(2) = XSAVE5	304670
XNL(3) = XSAVE6	304680
NL=NL+1	304690
XFTHLD = 0.0	304700
XFPHLD = 0.0	304710
XFZELD = 0.0	304720
XMTHLD = 0.0	304730
XMPHLD = 0.0	304740
IR=NL*6-5	304750
IF (LST(IR).NE.0) K=K+LST(IR)	304760
IF (LST(IR+1).EQ.0) GOTO 44	304770
K=K+1	304780
XFTHLD=ST(K,LL)	304790
44 IF(LST(IR+2).EQ.0) GOTO 45	304800
K=K+1	304810
XFPHLD = ST(K,LL)+XMERD*IWORD	304820
45 IF(LST(IR+3).EQ.0) GOTO 46	304830
K=K+1	304840
XFZELD = ST(K,LL)+XPRES*IWORD	304850
46 IF(LST(IR+4).EQ.0) GOTO 47	304860
K=K+1	304870

XMTHLD = ST(K,LL)+XMONT*IWORD	304880
47 IF(LST(IR+5).EQ.0) GOTO 48	304890
K=K+1	304900
XMPHLD=ST(K,LL)	304910
48 CONTINUE	304920
49 CONTINUE	304930
50 IF (ISTTAB.GE.3.AND.ISTTAB.LE.9) GO TO 4002	304940
CALL DIF1	304950
GO TO 77	304960
4002 CALL DIFF2	304970
77 CONTINUE	304980
GOTO 75	304990
8001 IERROR=8001	305000
NERROR=11	305010
GOTO 8888	305020
8002 IERROR=8002	305030
NERROR=12	305040
GOTO 8888	305050
8007 IERROR=8007	305060
NERROR=15	305070
GOTO 8888	305080
8031 IERROR=8031	305090
NERROR= 9	305100
GOTO 8888	305110
8036 IERROR=8036	305120
NERROR= 2	305130
GOTO 8888	305140
8086 IERROR=8086	305150
NERROR= 3	305160
GOTO 8888	305170
8087 IERROR=8087	305180
NERROR= 4	305190
GOTO 8888	305200
8088 IERROR=8088	305210
NERROR=27	305220
GOTO 8888	305230
8089 IERROR=8089	305240
NERROR= 5	305250
GOTO 8888	305260
8090 IERROR=8090	305270
NERROR= 6	305280
GOTO 8888	305290
8067 IERROR= 8067	305300
NERROR=16	305310
GOTO 8888	305320
8101 IERROR = 8101	305330
NERROR=17	305340
GOTO 8888	305350
8102 IERROR = 8102	305360
NERROR=18	305370
GOTO 8888	305380
8103 IERROR = 8103	305390
NERROR=19	305400
GOTO 8888	305410
8104 IERROR = 8104	305420
NERROR=20	305430
GOTO 8888	305440
8105 IERROR = 8105	305450
NERROR=21	305460
GOTO 8888	305470
8106 IERROR = 8106	305480
NERROR=22	305490

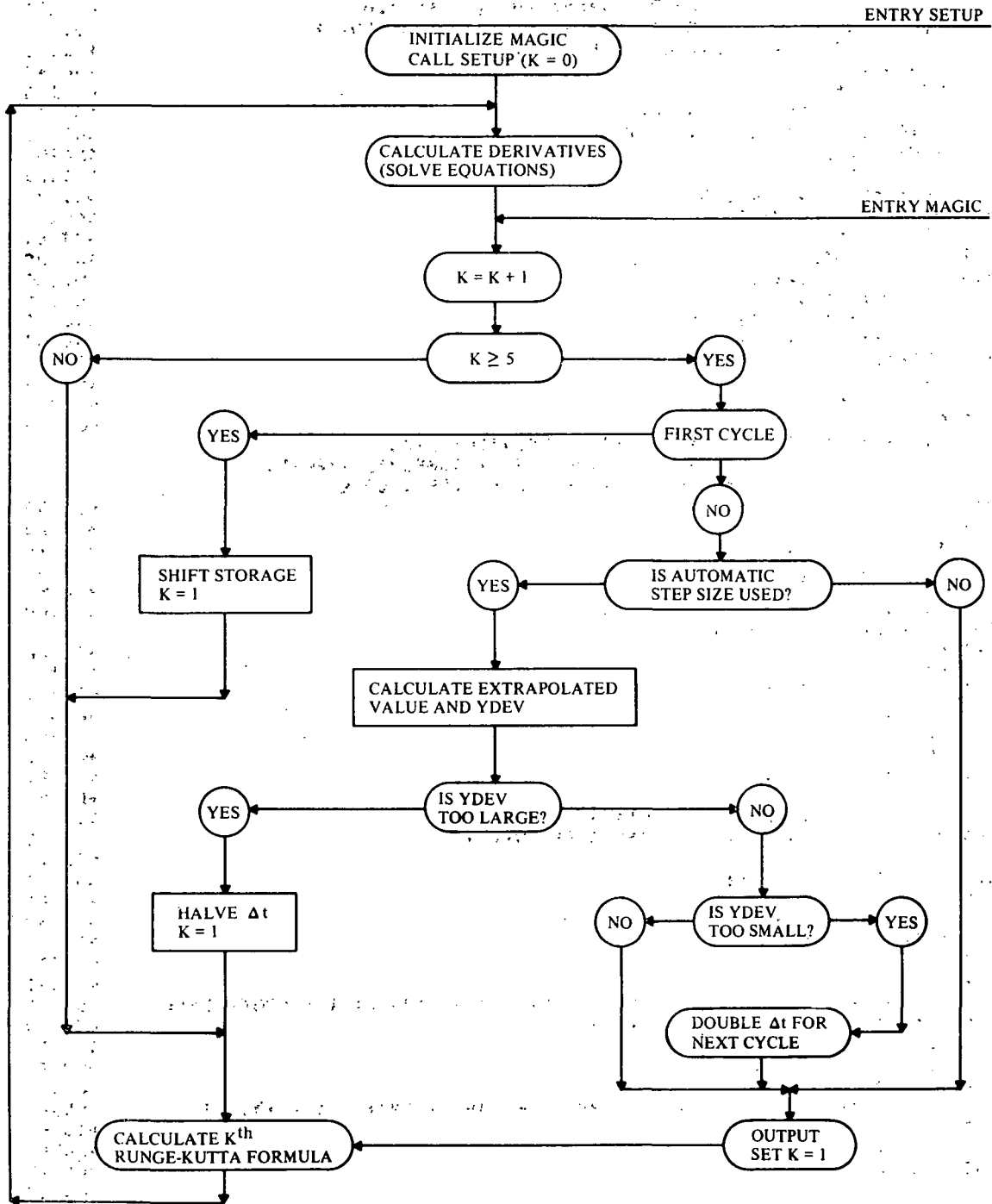
GOTO 8888	305500
8107 IERROR = 8107	305510
NERROR=23	305520
GOTO 8888	305530
8108 IERROR = 8108	305540
NERROR=24	305550
GOTO 8888	305560
8109 IERROR = 8109	305570
NERROR=25	305580
GOTO 8888	305590
8110 IERROR = 8110	305600
NERROR=26	305610
GOTO 8888	305620
8787 IERROR = 8787	305630
NERROR=34	305640
8888 NIX=1	305650
RETURN	305660
150 CONTINUE	305670
IF (NH.NE.0) GO TO 925.	305680
WRITE(6,670)	305690
670 FORMAT(/ /46X,41HMATRIX X AND Y (TRANPOSED) MAGIC OUTPUT)	305700
WRITE(6,672) (YCORR(I),I=1,NEQNS)	305710
672 FORMAT(8(2X,E14.7))	305720
925 CONTINUE	305730
RESTOP=RO	305740
RADUS(ISTOP) = RO	305750
TADUS(ISTOP)=RO	305760
GO TO (221,222,223),IGEOM	305770
221 SN = SIN(PHI)	305780
CS = COS(PHI)	305790
GO TO 224	305800
222 SN = COS(1.570796-G1)	305810
CS = SIN(1.570796-G1)	305820
IF (G1.NE.0.0) GO TO 224	305830
SN = 0.0	305840
CS = 1.0	305850
GO TO 224	305860
223 SN = 1.0	305870
CS = 0.0	305880
224 CONTINUE	305890
AMAT(ISTOP,1) = SAVY(22)	305900
AMAT(ISTOP,2) = SAVY(23)	305910
AMAT(ISTOP,3) = SAVY(5)	305920
AMAT(ISTOP,4) = SAVY(1)*CS-SAVY(3)*SN	305930
IF(NSC.LT.NSEG) GO TO 9999	305940
SADUS(JSTOP) = RO	305950
UADUS(JSTOP)=RO	305960
AMAT(JSTOP,5) = SAVY(22)	305970
AMAT(JSTOP,6) = SAVY(23)	305980
AMAT(JSTOP,7) = SAVY(5)	305990
AMAT(JSTOP,8) = SAVY(1)*CS-SAVY(3)*SN	306000
IF(ITIC.LE.ISTOP) GO TO 9999	306010
SADUS(JSTOP)=RADUS(ITIC)	306020
UADUS(JSTOP)=RADUS(ITIC)	306030
9999 RETURN	306040
END	306050

### SUBROUTINE SETUP

SETUP is a double entry subroutine called from RIEMAN. It is a mixed precision, numerical integration routine, with automatic selection of a variable integration step size, which utilizes fifth order Runge-Kutta equations to obtain the solution for first order differential equations.

### SUBROUTINE MAGIC

MAGIC is an alternate entry point to subroutine SETUP.



```

FOR,15 SETUP, SETUP
SUBROUTINE SETUP (MAGIN, MAGOUT, TIC, STEP, NEQNS, DTAU,
1          EPSIL, DELTA, ERR, TIME, DTIME, YICS, YPRED,
2          YCORR, YDOT, YNEW, YDEV, FWDEL, TBDEL)
400030
1          DIMENSION YICS(1), YPRED(1), YCORR(1), YDOT(1), YNEW(1),
400040
1          YDEV(1), FWDEL(1), TBDEL(1)
400050
1          DIMENSION C(3), D(3)
400060
COMMON /MAGIK/ KKNT
400070
DOUBLE PRECISION YNEW, YPRED
400080
DATA C, D / .5, .5, 1.0, .5, .0, .5/
400090
TIME = TIC
400100
TAU = TIC
400110
IF (DELTA) 200, 201, 200
400120
200 DTIME = 0.0078125
400130
GO TO 225
400140
201 DTIME = STEP
400150
225 DO 102 I = 1, NEQNS
400160
YDEV(I) = 0.0
400170
YPRED(I) = YICS(I)
400180
YCORR(I) = YICS(I)
400190
102 YNEW(I) = YICS(I)
400200
MAGOUT = -2
400210
GO TO 264
400220
5555 CONTINUE
400230
ENTRY MAGIC (MAGIN, MAGOUT, TIC, STEP, NEQNS, DTAU,
1          EPSIL, DELTA, ERR, TIME, DTIME, YICS, YPRED,
2          YCORR, YDOT, YNEW, YDEV, FWDEL, TBDEL)
400250
5556 CONTINUE
400260
MSET = 2
400270
IF (MAGOUT) 305, 101, 101
400280
101 IF (MAGIN) 21, 27, 14
400290
27 K = 0
400300
DO 202 I = 1, NEQNS
400310
202 YNEW(I) = YPRED(I)
400320
21 K = K + 1
400330
KKNT = K
400340
210 DO 2 I = 1, NEQNS
400350
GO TO (9, 6, 7, 4, 11), K
400360
9 FWDEL(I) = YDOT(I)
400370
GO TO 105
400380
6 TBDEL(I) = YDOT(I)
400390
GO TO 105
400400
7 TBDEL(I) = TBDEL(I) YDOT(I)
400410
105 YPRED(I) = YNEW(I) + C(K)*DTIME*YDOT(I)
400420
GO TO (2, 2, 400), K
400430
400 YCORR(I) = YPRED(I)
400440
2 CONTINUE
400450
TIME = TIME + D(K)*DTIME
400460
99 MAGOUT = 0.0
400470
264 RETURN
400480
4 DO 8 I = 1, NEQNS
400490
YPRED(I) = YNEW(I) + DTIME*(FWDEL(I) + 2.*TBDEL(I) + YDOT(I))/6.
400500
8 YDEV(I) = YCORR(I) - YPRED(I)
400510
GO TO 99
400520
11 IF (DELTA) 80, 5, 80
400530
80 DO 13 I = 1, NEQNS
400540
IF (EPSIL* ABS(YCORR(I)) + ERR - ABS(YDEV(I))) 14, 13, 13
400550
13 CONTINUE
400560
IF (SIGB) 15, 15, 205
400570
205 SIGB = 0.0
400580
GO TO 5
400590
15 SIGB = 0.0

```

DO 207 I = 1,NEQNS	400600
IF (ERR /100.+ DELTA* ABS(YCORR(I)) - ABS(YDEV(I))) 5,207,207	400610
207 CONTINUE	400620
DTIME = 2.*DTIME	400630
5 DO 208 I = 1,NEQNS	400640
208 YCORR(I) = YPRED(I)	400650
305 IF (DTAU) 19,30,19	400660
19 IF (TAU - TIME)20,20,27	400670
20 TAU = TAU + DTAU	400680
30 MAGOUT = 2	400690
GO TO 264	400700
14 DTIME = DTIME/2.0	400710
25 IF (K-3)48,26,26	400720
26 TIME = TIME - DTIME - DTIME	400730
GO TO 47	400740
48 TIME = TIME - DTIME	400750
47 SIGB = +2.	400760
DO 209 I = 1,NEQNS	400770
209 YDOT(I) = FWOEL(I)	400780
212 K = 0	400790
GO TO 21	400800
END	400810



### SUBROUTINE ROBOT

This subroutine is used by RIEMAN to calculate geometric and load coefficients for use in the differential equations. With reference to geometry, all the necessary radii are calculated, as well as the stiffness coefficients of the various shell wall constructions. Thermal load moments and direct forces are calculated from direct temperature input. Inertia loads due to shell spin are also calculated.

All the above values are passed back via the label common area EQUAZN.

In the case of a special point input geometry the ROBOT routine calls GEOMET.

### Subroutines GEOMET, PLICO, PLINE

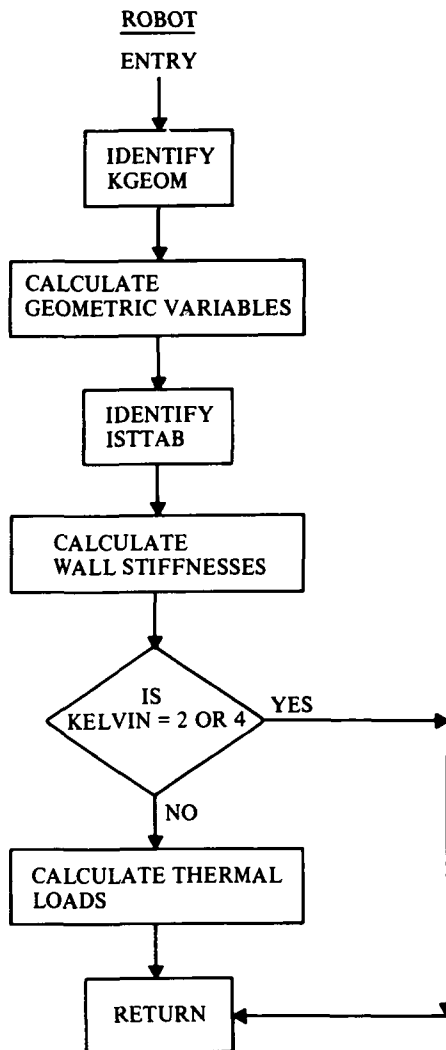
Starting from a set of z,r points these subroutines calculate the necessary radii of the shell curves using spline fits.

## FORTRAN CODE

## ENGINEERING SYMBOLS (REF. 1)

RO	$r_0$
R1	$r_1$
R1DOT	$r_{1,\phi}$
CS	$\cos \phi$
SN	$\sin \phi$
A	a
C	c
XN	n
F2	$f_2$
F3	$f_3$
TAN; TN	$\tan \phi$
SEC	$\sec \phi$
TII	$T_{ii}$
TIK	$T_{ic}$
TOK	$T_{oc}$
TOO	$T_{oo}$
TEFREE	$\bar{T}$
HI	$h_i$
HO	$h_o$
T	t
TI	$t_i$
TO	$t_o$
SNSQ	$\sin^2 \phi$
CSSQ	$\cos^2 \phi$
CN	$\cos \phi \sin \phi$
X1CS	$1/\cos \phi$
X1SN	$1/\sin \phi$
R2	$r_2$
BETA	$\beta$

FORTRAN CODE	ENGINEERING SYMBOLS (REF. 1)
X1ROSN	$1/r_0 \sin \phi$
X1ROCS	$1/r_0 \cos \phi$
CSX1R0	$\cos \phi/r_0$
CSX1R1	$\cos \phi/r_1$
CSX1R2	$\cos \phi/r_2$
SNX1R0	$\sin \phi/r_0$
SNX1R1	$\sin \phi/r_1$
X1R1	$1/r_1$
X1R2	$1/r_2$
X1R1SQ	$1/r_1^2$
X1ROSQ	$1/r_0^2$



```

FOR, IS ROBOT, ROBOT
SUBROUTINE ROBOT (ST, KLUE2, NROW, LL, ER, ES, G2, G3, TIME, ITIC, JTIC,
1 NCYC, SIGOX, ALPHR, ALPHS, SIGOXR, SIGOXS)
INTEGER SAVJTC, SAVSTP, Q, THICK
INTEGER XN1, XN2, XN
REAL*4 I2
DOUBLE PRECISION YPRED
COMMON STORY(16), XMAT(270, 10), STD(10), SADUS(30), RADUS(30)
COMMON TADUS(30), UADUS(30), SAVTIC(900)
COMMON XN, TEFREE, TIC, PHI, STOP, RESTOP, RTICK, G1, XNL(3), NH
COMMON NST(30), NKL(30), NXMAT(20), SAVJTC(30), SAVSTP(30), JRTIC(30)
COMMON JRSTOP(30), NREG, NMPT, NRC, NSC, NIX, IERROR, KGEOM, IGEOM, ISTTAB
COMMON KELVIN, IBEGIN, NPROB, NSEG, NERROR, Q, THICK, NOJS, NLINKS, NLCASE
COMMON NTSKL, NZ, NBCT, LINPUT, NTRKL, NPASS, XN1, KBC, NRINGS
COMMON LODE, ICYCLE, LDISTL
COMMON /EQUAZN/ YPRED(72), YDOT(72), YASAVE(72), YANTH, YAMTH,
1 YAMPT, YAJPH, S, SN, CS, SNSQ, CSSQ, TAN, SEC, CN, X1CS, X1SN, TN,
2 X1RO, X1ROSQ, X1SNRO, X1CSRO, CN1RO, SN1RO, CS1RO, X1R1, X1R2,
3 CS1R1, CS1R2, SN1R1, X1R1SQ, R2SQ, RO, BESQ, ROSQ, XNSQ, BETA, R1,
4 R2, S1, R1DOT, XNTTH, XNTPH, XMTTH, XMPH, XFTHLD, XFPHLD, XFZELD,
5 XMTHLD, XMPHLD, ETHET, EPHI, XGPT, ALPHTH, ALPHPH, XNUTP, XNUPT,
6 XC11, XC22, XC15, XD33, XD22, XD21, XD12, XK11, XK12, XK21, XK22,
7 XK33, XD11, XNPHI, M, I, BETTA, ZETTA, XC16
COMMON /SPLINS/ ANG, PSI(100), RAD(100), CUR1(100), CUR2(100),
1 DR1DP(100), ZI(14), RI(14), NRZIN
COMMON /ARING/ NRING(28), AMAT(30, 8), RSIG(12), REPS(12), RALPH(12),
C RBAPH(12)
COMMON /PLS/ OMEGA, IWORD, XMERD, XPRES, XMONT
COMMON /MAGIK/ KKNT
COMMON /PLSTIC/ IO, JO, IOR, JOR, KORI, NEO
COMMON /WOOD/ SAVY(53), NPLEV, NLPO, NPLA(21), STR(6), SIGMA(3, 21),
C SEPS(3, 21), SALPH(3, 21), SBAPH(3, 21), STEPS(3, 21),
O EFF(21), STSRN(3), NPLAST(3), STSIG(3), STREPS(3),
M STALPH(3), STBAPH(3), EFFST(3), NPLEVS(3)
COMMON /CMAIN/ ZETA1(21), ZETA2(21), NODE, ALF(4), CE(4), NLRS, HI, HO, T
DIMENSION ST(30, 31)
EQUIVALENCE ($INB, SNB), (COSB, CSB)
DATA A/'A' '/'
C
NCONT = NROW
GOTO (771, 772, 773, 774, 775, 776, 7077), KGEOM
C GEOMETRY FOR ELIPSE(G3=OFFSET DISTANCE)
771 A=G1
BE=G2
BETA = BE
BESQ=BE**2
ASQ=A**2
SN = SIN(PHI)
CS = COS(PHI)
SNSQ = SN**2
CSSQ = CS**2
R2 = A*SQRT(1.0/(SNSQ+BESQ*CSSQ))
R2SQ = R2**2
RO=R2*SN
R1=R2*R2SQ*BESQ/ASQ
BESQ=BE**2
R1DOT=0.0
IF(KGEOM.EQ.1.AND.BETA.NE.1.0.AND.SN.NE.0.0)R1DOT=3.0*(R2*BETA/
1A) **2*(CS/SNSQ)*(R1*SN-RO)
IF(SN.EQ.0.0)GO TO 779
R2 = R2-G3/SN
R2SQ = R2**2

```

	RO = RO-G3	700620
	GO TO 7775	700630
779	IF(G3 .EQ. 0.0)GO TO 7775	700640
	RIDOT = 3.0*G3	700650
	RO = -G3	700660
	GO TO 7775	700670
C	GEOMETRY FOR OGIVE	700680
772	R1=G1	700690
	C=G2	700700
	SN = SIN(PHI)	700710
	CS = COS(PHI)	700720
	IF (SN.EQ.0.0) GOTO 777	700730
	R2=R1-C/SN	700740
	GOTO 778	700750
777	R2 = 1.0	700760
778	RO = R1*SN-C	700770
	RIDOT=0.0	700780
	GOTO 7775	700790
C	GEOMETRY FOR CONE	700800
773	CS = COS(G1)	700810
	SN=SIN(G1)	700820
	S=PHI	700830
	S1=1.0/S	700840
	R2=CS*SN*PHI	700850
	RO=PHI*CS	700860
	RIDOT=0.0	700870
	GOTO 7775	700880
C	GEOMETRY FOR CYLINDER	700890
774	RO = G1	700900
	RIDOT=0.0	700910
	SN = 1.0	700920
	CS = 1.0	700930
	GOTO 7775	700940
C	MODIFIED ELLIPSE	700950
775	XNEXP = G1	700960
	A =G2	700970
	XN1 = 1.0 + XNEXP	700980
	XN2 = 1.0/XN1	700990
	XN3 = XN1 + 1.0	701000
	XN4 = XN3 + 1.0	701010
	XN5 = XN4/XN1	701020
	SN = SIN(PHI)	701030
	CS = COS(PHI)	701040
	R2 = A*(2.0/(1.0+SN**XN1))**XN2	701050
	R1 = (A/2.0)*(R2/A)**XN3	701060
	RO=R2*SN	701070
	RIDOT = -XN3*A*(SN**XNEXP*CS/4.0)*(2.0/(1.0+SN**XN1))**XN5	701080
	GOTO 7775	701090
C	GENERAL GEOMETRY	701100
776	SN = SIN(PHI)	701110
	CS = COS(PHI)	701120
	TAN= SN/CS	701130
	SEC= 1.0/CS	701140
	IF (TIME.EQ.TIC) CALL GEOMET	701150
	ARG = PHI	701160
	DO 204 J=1,100	701170
	PHO = PSI(J)	701180
	IF (ANG.EQ.A) IF (ARG-PHO) 221,223,204	701190
	IF (PHO-ARG) 221,223,204	701200
221	IF (J-1) 8502,8502,224	701210
204	CONTINUE	701220

	GO TO 8503	701230
223	RO = RAD(J)	701240
	R1 = CUR1(J)	701250
	R2 = CUR2(J)	701260
	R1DOT = DR1DP(J)	701270
	GO TO 7775	701280
8502	NERROR = 41	701290
	GO TO 8888	701300
8503	NERROR = 42	701310
8888	NIX = 1	701320
	GO TO 8889	701330
224	SUB1 = ARG-PSI(J-1)	701340
	SUB2 = PSI(J)-PSI(J-1)	701350
	RO = RAD(J-1)+(RAD(J)-RAD(J-1))*SUB1/SUB2	701360
	R1 = CUR1(J-1)+(CUR1(J)-CUR1(J-1))*SUB1/SUB2	701370
	R2 = CUR2(J-1)+(CUR2(J)-CUR2(J-1))*SUB1/SUB2	701380
	R1DOT = DR1DP(J-1)+(DR1DP(J)-DR1DP(J-1))*SUB1/SUB2	701390
	GOTO 7775	701400
C	ISOTENSOID GEOMETRY	701410
7077	CONTINUE	701420
	SN = SIN(PHI)	701430
	CS = COS(PHI)	701440
	A = G1	701450
	R2 = A/SQRT(SN)	701460
	R1 = 0.5 * R2	701470
	RO = R2 * SN	701480
	R1DOT = - ((A**2)*0.5)*(R1*CS)/RO**2	701490
7775	TAN=SN/CS	701500
	IF (TIME.EQ.TIC) RTICK=RO	701510
	IF (NCYC.GT.1) GO TO 491	701520
	IF (TIME.NE.TIC) GO TO 491	701530
	IF (NH.EQ.0.AND.NEO.EQ.0) GO TO 480	701540
	AMAT(ITIC,1) = SAVY(22)	701550
	AMAT(ITIC,2) = SAVY(23)	701560
	AMAT(ITIC,3) = SAVY(5)	701570
	AMAT(ITIC,4) = SAVY(1)*CS-SAVY(3)*SN	701580
480	RADUS(ITIC) = RO	701590
	IF (NSC.NE.1) GO TO 491	701600
	SADUS(JTIC) = RO	701610
	IF (NH.EQ.0.AND.NEO.EQ.0) GO TO 491	701620
	AMAT(JTIC,5) = SAVY(22)	701630
	AMAT(JTIC,6) = SAVY(23)	701640
	AMAT(JTIC,7) = SAVY(5)	701650
	AMAT(JTIC,8) = SAVY(1)*CS-SAVY(3)*SN	701660
491	CONTINUE	701670
	ROSQ = RO**2	701680
	XNSQ=XN**2	701690
	CN=CS*SN	701700
	X1CS=1.0/CS	701710
	TN=SN/CS	701720
	X1RO=1.0/RO	701730
	X1ROSQ=1.0/RO**2	701740
	X1CSRO=1.0/(CS*RO)	701750
	CN1RO=CN/RO	701760
	SN1RO=SN/RO	701770
	CS1RO=CS/RO	701780
	SNSQ=SN**2	701790
	CSSQ=CS**2	701800
	IF (KGEOM.EQ.4.OR.KGEOM.EQ.3) GOTO 79	701810
	R1SQ = R1**2	701820
	R2SQ = R2**2	701830
	X1SN=1.0/SN	701840

	X1SNRO=1.0/(SN*RO)	701850
	X1R1=1.0/R1	701860
	X1R2=1.0/R2	701870
	CS1R1=CS/R1	701880
	CS1R2=CS/R2	701890
	SN1R1=SN/R1	701900
	X1R1SQ=1.0/R1**2	701910
79	XNTTH=0.0	701920
	XNTPH=0.0	701930
	XMTTH=0.0	701940
	XMTPH = 0.	701950
C		701960
C	COMPUTATION OF K AND D FOR MATERIAL PROPEY INPUT	701970
C		701980
	HD = 0.0	701990
	T = 0.0	702000
	HI = 0.0	702010
	TS = 0.0	702020
	TR = 0.0	702030
	TR = 0.0	702030
	RHOR = 0.0	702040
	RHOS = 0.0	702050
	RHOI = 0.0	702060
	RHOC = 0.0	702070
	CTH = 0.0	702080
	CPH = 0.0	702090
	YBARI = 0.0	702100
	YBARC = 0.0	702110
	YBARO = 0.0	702120
	GO TO (711,600,711,32,33,34,35,36,37,28,29,30),ISTTAB	702130
C	THICK	702140
600	GO TO (703,702,701,701),THICK	702150
701	HO= ST(4,LL)	702160
702	T = ST(3,LL)	702170
	RHOC = ST(NCONT-1,LL)	702180
703	HI= ST(2,LL)	702190
	RHOI = ST(NCONT,LL)	702200
	GO TO 40	702210
C	ST11,ST12,ST13	702220
30	HO= ST(14,LL)	702230
29	T = ST(13,LL)	702240
	RHOC = ST(NCONT-3,LL)	702250
28	HI= ST(12,LL)	702260
	RHOI = ST(NCONT-2,LL)	702270
	RHOS = ST(NCONT-1,LL)	702280
	RHOR = ST(NCONT,LL)	702290
	GJPH= ST(2,LL)	702300
	GJTH= ST(3,LL)	702310
	APH = ST(4,LL)	702320
	ATH = ST(5,LL)	702330
	CPH = ST(6,LL)	702340
	CTH = ST(7,LL)	702350
	XIPH = ST(8,LL)	702360
	XITH= ST(9,LL)	702370
	SPH = ST(10,LL)	702380
	STH = ST(11,LL)	702390
	IF (KELVIN.EQ.2.OR.KELVIN.EQ.4) GO TO 40	702400
	ISTAB = ISTTAB-9	702410
	TS = ST(ISTAB+12,LL)	702420
	TR = ST(ISTAB+13,LL)	702430
	GO TO 40	702440



C	RWAF1,RWAF2,RWAF3	702450
	34. HO = ST(10,LL)	702460
	33 T = ST(9,LL)	702470
	RHOC = ST(NCONT-2,LL)	702480
	32 HI = ST(8,LL)	702490
	RHOI = ST(NCONT-1,LL)	702500
	RHOS = ST(NCONT,LL)	702510
	APH = ST(2,LL)	702520
	CPH = ST(3,LL)	702530
	XIPH= ST(4,LL)	702540
	SPH = ST(5,LL)	702550
	BETTA=ST(6,LL)	702560
	ZETTA = ST(7,LL)	702570
	ATH = APH	702580
	CTH = CPH	702590
	XITH= XIPH	702600
	STH = SPH	702610
	RHOR = RHOS*IWORD	702620
	IF (KELVIN.EQ.2.OR.KELVIN.EQ.4) GO TO 40	702630
	ISTAB = ISTAB-3	702640
	TS = ST(ISTAB+8,LL)	702650
	TR = TS	702660
	GO TO 40	702670
C	ISG1,ISG2,ISG3	702680
	37 HO = ST(9,LL)	702690
	36 T = ST(8,LL)	702700
	RHOC = ST(NCONT-2,LL)	702710
	35 HI = ST(7,LL)	702720
	RHOI = ST(NCONT-1,LL)	702730
	RHOS = ST(NCONT,LL)	702740
	APH = ST(2,LL)	702750
	CPH = ST(3,LL)	702760
	XIPH = ST(4,LL)	702770
	SPH = ST(5,LL)	702780
	BETTA = ST(6,LL)	702790
	ATH = APH	702800
	CTH = CPH	702810
	XITH = XIPH	702820
	STH = SPH	702830
	RHOR = RHOS*IWORD	702840
	IF (KELVIN.EQ.2.OR.KELVIN.EQ.4) GO TO 40	702850
	ISTAB = ISTAB-6	702860
	TS = ST(ISTAB+7,LL)	702870
	TR = TS	702880
	GO TO 40	702890
C	ST10,RWAF	702900
C	RANKIN=THSTND MEANS INTERPOLATE, COMPUTE NTEMP, MTEMP	702910
C	RANKIN=NOTHRM MEANS DO NOT INTERPOLATE, DO NOT COMPUTE NTEMP, MTEMP	702920
C	RANKIN=THCNST MEANS DO NOT AVERAGE, BUT INTERPOLATE, COMPUTE	702930
C	NTEMP, MTEMP	702940
C	RANKIN=THINHO MEANS INTERPOLATE, BUT DO NOT COMPUTE NTEMP, MTEMP	702950
C		702960
	711 CONTINUE	702970
	XK11=ST(2,LL)	702980
	XK12=ST(3,LL)	702990
	XK22 = ST(4,LL)	703000
	XK33 = ST(5,LL)	703010
	XD11 = ST(6,LL)	703020
	XD12 = ST(7,LL)	703030
	XD22 = ST(8,LL)	703040
	XD33 = ST(9,LL)	703050
	XC11 = ST(10,LL)	703060

	XC22 = ST(11,LL)	703070
	XC15 = ST(12,LL)	703080
	XC16 = ST(13,LL)	703090
	XMERD = ST(NCONT-2,LL)	703100
	XPRES = ST(NCONT-1,LL)	703110
	XMONT = ST(NCONT,LL)	703120
	XK21 = XK12	703130
	XD21 = XD12	703140
	GO TO 103	703150
C		703160
	40 CONTINUE	703170
	IF (IWORD.EQ.1) GO TO 140	703180
	RHOR = 0.0	703190
	RHOS = 0.0	703200
	RHOI = 0.0	703210
	RHOC = 0.0	703220
	XMERD = 0.0	703230
	XPRES = 0.0	703240
	XMONT = 0.0	703250
	140 CONTINUE	703260
	TEMP3= (1.0-XNUPT * XNUTP)	703270
	GO TO (42,47,49,41),THICK	703280
	41 GO TO (103,42,103,42,47,49,42,47,49,42,47,49),ISTTAB	703290
		703300
C		703310
C	SINGLE SHEET	703320
C		703330
	42 TEMP1 = ETHET*HI	703340
	TEMP2= TEMP1 * HI**2	703350
	XK11= TEMP1/TEMP3	703360
	XD11= TEMP2/(12.0* TEMP3)	703370
	TEMP1 = EPHI*HI	703380
	TEMP2= TEMP1*HI**2	703390
	XK22= TEMP1/TEMP3	703400
	XD22= TEMP2/(12.0* TEMP3)	703410
	XK33 = XGPT*HI	703420
	XD33= XK33*HI**2/12.0	703430
	YBARI = 0.0	703440
	YBARC = 0.0	703450
	YBARO = 0.0	703460
	GO TO 55	703470
C		703480
C	EQUAL SHEETS	703490
C		703500
	47 CONTINUE	703510
	XK11 = 2.0*ETHET*HI/TEMP3	703520
	XK22 = 2.0*EPHI*HI/TEMP3	703530
	XK33 = 2.0*XGPT	703540
	ZBR = HI+T/2.0	703550
	ZBH = (ZBR-HI/2.0)**2	703560
	XD33 = XGPT*HI*((HI**2)/6.0+2.0*ZBH)	703570
	XD11 = HI*(XK11*HI/12.0+2.0*ETHET*ZBH/TEMP3)	703580
	XD22 = HI*(XK22*HI/12.0+2.0*EPHI*ZBH/TEMP3)	703590
	YBARI = ZBR-HI/2.0	703600
	YBARC = ZBR-HI-T/2.0	703610
	YBARO = HI/2.0-ZBR	703620
	GO TO 55	703630
C		703640
C	UNEQUAL FACE SHEETS	703650
C		703660
	49 CONTINUE	703670
	ZBR = (HI*HI+HO*HO+2.0*(HO*(HI+T)))/(2.0*(HI+HO))	

ZBHIN = (ZBR-HI/2.0)**2	703680
ZBHOUT = (ZBR-HO/2.0)**2	703690
XK11 = ETHET*(HI+HO)/TEMP3	703700
XK22 = EPHI*(HI+HO)/TEMP3	703710
XK33 = XGPT*(HI+HO)	703720
HIO3 = HI**3+HO**3	703730
XD33 = HIO3*XGPT/12.0+XGPT*(HI*ZBHIN+HO*ZBHOUT)	703740
D11 = ETHET*HIO3/12.0	703750
XD11 = (D11+ETHET*(HI*ZBHIN+HO*ZBHOUT))/TEMP3	703760
O22 = EPHI*HIO3/12.0	703770
XD22 = (O22+EPHI*(HI*ZBHIN+HO*ZBHOUT))/TEMP3	703780
YBARI = ZBR-HI/2.0	703790
YBARC = ZBR-HI-T/2.0	703800
YBARO = HI/2.0-ZBR	703810

C  
C  
C

DETERMINE COMPLETE CONSTANTS DEPENDENT ON REINFORCEMENT CLUE

55 CONTINUE

ROI = RO-YBARI*SN	703860
ROU = RO-YBARO*SN	703870
ROC = RO-YBARC*SN	703880
IF (THICK.EQ.2) HO = HI	703890
IF (ISTTAB.EQ.5.OR.ISTTAB.EQ.8.OR.ISTTAB.EQ.11) HO = HI	703900
D3 = RHOI*ROI*HI	703910
D4 = RHOC*ROC*T	703920
D5 = RHOI*ROU*HO	703930
DD = D3+D4+D5	703940
XMERD = DD*OMEGA*CS	703950
XPRES = -DD*OMEGA*SN	703960
XMONT = -(D3*YBARI+D4*YBARC+D5*YBARO)*OMEGA*CS	703970
IF(ISTTAB .EQ.2)GO TO 103	703980
TBARR = ATH/STH	703990
TBARS = APH/SPH	704000
ROR = RO-CTH*SN	704010
ROS = RO-CPH*SN	704020
EASTH=ER*ATH/STH	704030
EASPH=ES*APH/SPH	704040
EISPH= ES* XIPH/SPH	704050
EISTH= ER* XITH/STH	704060
D1 = RHOR*ROR*TBARR	704070
D2 = RHOS*ROS*TBARS	704080
DD = D1+D2+D3+D4+D5	704090
GO TO (58,60,100),KLUE2	704100

C  
C  
C

ST CLUE (11,12,13)

58 CONTINUE

XK12= XK11*XNUTP	704140
XK11= XK11+ EASTH	704150
XK22= XK22+ EASPH	704160
XC11= EASTH*CTH	704170
XC22= EASPH*CPH	704180
XD22= - XD22 - EISPH	704190
XD33= XD33 + GJPH/(4.0*SPH)+ GJTH/(4.0*STH)	704200
XD12= -XD11*XNUTP	704220
XD11= -XD11- EISTH	704230
XK21 = XK12	704240
XD21 = XD12	704250
XMERD = DD*OMEGA*CS	704260
XPRES = -DD*OMEGA*SN	704270
XMONT = -(D1*CTH+D2*CPH+D3*YBARI+D4*YBARC+D5*YBARO)*OMEGA*CS	704280
GO TO 103	704290

C	RWA CLUE (1,2,3)	704300
C		704310
60	CONTINUE	704320
	SINB = SIN(BETTA)	704330
	COSB = COS(BETTA)	704340
	SN2TO4 = 2*(SINB**4.)	704350
	D= STH*(COSB+SINB)	704360
	ED = ER*ATH/D	704370
	SINB2= SINB**2.	704380
	HL = 2.0*(ABS(ZETTA)-ABS(CTH))	704390
	I2=(ATH**3.)/(3* HL**2)	704400
95	XC22 = 2.0*CTH*COSB**3*ED	704410
	XC15 = 2.0*CTH*COSB*SINB2*ED	704420
	XC16 = XC15	704430
	GRI= ER* I2/(2.0*(1.0 + XNUTP)*D)	704440
	XC11 = CTH*SN2TO4/COSB*ED	704450
	EDI = ER*XITH/D	704460
	SN4TO2 = 4.*SINB2	704470
	XD22 = -XD22-2.0*COSB**3*EDI-SN4TO2*COSB*GRI	704480
	TB= 2.0* BETTA	704490
	XD33 = XD33+((4.0*COS(TB)*	704500
	1*2*GRI)/ COSB) + (2.0*COSB*SINB2*EDI)	704510
	XD12 = -XD11*XNUTP-(2.0*COSB	704520
	1*SINB2*EDI)-(SN4TO2*COSB*GRI )	704530
	XK12= XK11*XNUTP + (2.0*COSB*SINB2*ED)	704540
	XK22=XK22+(2*COSB**3*ED)	704550
	XK33=XK33+(2*COSB*SINB2*ED)	704560
	XK11=XK11+(SN2TO4*ED/COSB)	704570
	XD11 = -XD11-SN2TO4*EDI/COSB-(	704580
	1 SN4TO2*COSB*GRI)	704590
	XK21 = XK12	704600
	XD21 = XD12	704610
	GO TO 108	704620
C		704630
C	ISG CLUE (1,2,3)	704640
C		704650
100	CONTINUE	704660
	SNB = SIN(BETTA)	704670
	CSB = COS(BETTA)	704680
	TBETTA= 2.0*BETTA	704690
	CS2B= COS(TBETTA)	704700
	ONEC2B=(1.0+ CS2B)/2.	704710
	SCB2 =(SNB-CS2B*SNB + 2.)/(2.0*CSB)	704720
	SN2B =SIN(TBETTA) /2.	704730
	XK12=XK11*XNUTP + (EASTH*SNB*ONEC2B/CSB)	704740
	XK11=XK11+ EASTH*SCB2	704750
	XK22=XK22+ EASTH*(CSB/SNB*ONEC2B)	704760
	XK33=XK33+ EASTH* SN2B	704770
	XC11= (EASTH*CTH* SCB2 )	704780
	XC15=EASTH*CTH*( SNB* ONEC2B/CSB )	704790
	XC16=EASTH*CTH*SN2B	704800
	XC22= EASTH*CTH* (CSB/SNB * ONEC2B)	704810
	XD12=-XD11*XNUTP- E1STH*(SNB*ONEC2B/CSB)	704820
	XD11=-XD11- E1STH*SCB2	704830
	XD22 = -XD22-E1STH*(CSB/SNB*ONEC2B)	704840
	XD33= XD33+ E1STH*SN2B	704850
	XK21 = XK12	704860
	XD21 = XD12	704870
C		704880
C		704890
108	XMERD = (DD-D2)*OMEGA*CS	704900

	XPRES = -(DD-D2)*OMEGA*SN	704910
	XMONT = -(D1*CTH+D3*YBARI+D4*YBARC+D5*YBARO)*OMEGA*C S	704920
C		704930
103	CONTINUE	704940
	IF (KGEOM.NE.4) GO TO 105	704950
	XMERD = 0.0	704960
	XMONT = 0.0	704970
105	CONTINUE	704980
C		704990
	GO TO (716,714,715,714),KELVIN	705000
716	TII = ST(NROW+1,LL)	705010
	TIK = ST(NROW+2,LL)	705020
	TOK = ST(NROW+3,LL)	705030
	TOO = ST(NROW+4,LL)	705040
	GOTO 717	705050
715	TII = ST(NROW+1,LL)	705060
	TIK = TII	705070
	TOK = TII	705080
	TOO = TII	705090
C		705100
717	TEMP1 = ALPHTH+XNUTP*ALPHPH	705110
	TEMP2 = ALPHPH+XNUPT*ALPHTH	705120
	TEMP3 = 1-XNUPT*XNUTP	705130
	TEMP4 = HI/4.0	705140
	ETHK1 = ETHET*TEMP1/TEMP3	705150
	TEMP5 = HI**2/24.0	705160
	TEMP61= TII+ TIK-2* TEFREE	705170
	TEMP62= TOO+ TOK-2* TEFREE	705180
	TEMP71= 2.0* TII +TIK-3*TEFREE	705190
	TEMP72= 2.0* TOO +TOK-3*TEFREE	705200
	EPHK1 = EPHI*TEMP2/TEMP3	705210
	GO TO (811,812,813,814),THICK	705220
C		705230
814	GO TO (815,811,815,811,812,813,811,812,813,811,812,813),ISTTAB	705240
C		705250
811	XNTTH= ETHK1 * TEMP4 * (TEMP61+ TEMP62)	705260
	XNTPH= EPHK1 * TEMP4 * (TEMP61 + TEMP62)	705270
	XMTTH= ETHK1 * TEMP5 * (TEMP71- TEMP72)	705280
	XMTPH= EPHK1 * TEMP5 * (TEMP71 - TEMP72)	705290
	GO TO 816	705300
812	TI = T/2.0	705310
	TEMP8= HI/2.0	705320
	XNTTH = ETHK1*TEMP8*(TEMP61+TEMP62)	705330
	XNTPH = EPHK1*TEMP8*(TEMP61+TEMP62)	705340
	XMTTH = ETHK1*TEMP8*(HI*(TEMP71-TEMP72)/3.0+TI*(TEMP61-TEMP62))	705350
	XMTPH = EPHK1*TEMP8*(HI*(TEMP71-TEMP72)/3.0+TI*(TEMP61-TEMP62))	705360
	GO TO 816	705370
813	TI = (HO**2-HI**2+2.0*HO*T)/(2.0*(HI+HO))	705380
	TO = (HI**2-HO**2+2.0*HI*T)/(2.0*(HI+HO))	705390
	XNTTH = ETHK1/2.0*(HI*TEMP61+HO*TEMP62)	705400
	XNTPH = EPHK1/2.0*(HI*TEMP61+HO*TEMP62)	705410
	XMTTH = ETHK1/2.0*(HI**2*TEMP71/3.0-HO**2*TEMP72/3.0+TI*HI*TEMP61-	705420
	1 TO*HO*TEMP62)	705430
	XMTPH = EPHK1/2.0*(HI**2*TEMP71/3.0-HO**2*TEMP72/3.0+TI*HI*TEMP61-	705440
	1 TO*HO*TEMP62)	705450
816	CONTINUE	705460
	IF (ISTTAB.EQ.2) GO TO 714	705470
	GO TO (817,818,819),KLUE2	705480
817	XNTPH = XNTPH+ES*APH/SPH*ALPHS*TS	705490
	XNTTH = XNTTH+ER*ATH/STH*ALPHR*TR	705500
	XMTPH = XMTPH+CPH*ES*APH/SPH*ALPHS*TS	705510
	XMTTH = XMTTH+CTH*ER*ATH/STH*ALPHR*TR	705520

	GO TO 714	705530
818	TEM = ES*APH/SPH*ALPHS*TS	705540
	XNTPH = XNTPH+TEM	705550
	XNTTH = XNTTH+TEM	705560
	XMTPH = XMTPH+CPH*TEM	705570
	XMTTH = XMTTH+CPH*TEM	705580
	GO TO 714	705590
819	TEM = ES*APH/SPH*ALPHS*TS	705600
	XNTPH = XNTPH+TEM*CSB/SNB	705610
	XNTTH = XNTTH+TEM*(1.0+SNB)/CSB	705620
	XMTPH = XMTPH+CPH*TEM*CSB/SNB	705630
	XMTTH = XMTTH+CPH*TEM*(1.0+SNB)/CSB	705640
	GO TO 714	705650
815	TEMP10 = ((-XK11*XD11)**.5)/(48.0**.5)	705660
	TEM11 = ((-XK22*XD22)**.5)/(48.0**.5)	705670
	XNTTH = XK11/4.0*TEMP1*(TEMP61+TEMP62)	705680
	XNTPH = XK22/4.0*TEMP2*(TEMP61+TEMP62)	705690
	XMTTH = TEMP10*TEMP1*(TEMP71-TEMP72)	705700
	XMTPH = TEM11*TEMP2*(TEMP71-TEMP72)	705710
714	CONTINUE	705720
	IF (NH.NE.0.OR.(NCYC.NE.0.AND.KKNT.NE.4)) GO TO 8889	705730
	IF (NEO.NE.0) GO TO 8889	705740
	DO 1234 K=1,KBC	705750
	DO 1235 J=1,3	705760
	SIGMA(J,K) = 0.0	705770
	SEPS(J,K) = 0.0	705780
	SALPH(J,K) = 0.0	705790
1235	SBAPH(J,K) = 0.0	705800
	EFF(K) = SIGOX	705810
1234	NPLA(K) = 0	705820
	DO 1238 J=1,3	705830
	STSRN(J) = 0.0	705840
	NPLAST(J) = 0	705850
	STSIG(J) = 0.0	705860
	STREPS(J) = 0.0	705870
	STALPH(J) = 0.0	705880
	STBAPH(J) = 0.0	705890
	NPLEVS(J) = 0	705900
1238	EFFST(J) = SIGOXS	705910
	IF (KLUE2.EQ.1) EFFST(2) = SIGOXR	705920
	DO 1237 J=1,6	705930
1237	STR(J) = 0.0	705940
	NPLEV = 0	705950
	IF (KELVIN.EQ.1.OR.KELVIN.EQ.3) GO TO 110	705960
	DO 111 K=1,KBC	705970
	DO 111 J=1,3	705980
111	STEPS(J,K) = 0.0	705990
	GO TO 112	706000
110	IF (THICK.NE.1) GO TO 113	706010
	NLH = NLRS/2+1	706020
	DO 115 LR=1,NLH	706030
	T = TOK+2.0*ZETA1(LR)*(TII-TOK)	706040
	STEPS(1,LR) = ALPHPH*T	706050
	STEPS(2,LR) = ALPHTH*T	706060
115	STEPS(3,LR) = 0.0	706070
	NLH = NLH+1	706080
	DO 116 LR=NLH,NLPO	706090
	T = TOK+2.0*ZETA1(LR)*(TOK-TOO)	706100
	STEPS(1,LR) = ALPHPH*T	706110
	STEPS(2,LR) = ALPHTH*T	706120
116	STEPS(3,LR) = 0.0	706130

GO TO 112	706140
113 DO 200 K=1,2	706150
DO 200 LR=1,NLPO	706160
LRT = LR+(K-1)*NLPO	706170
GO TO (300,400),K	706180
300 T = TIK+ZETA2(LR)*(TII-TIK)	706190
GO TO 500	706200
400 T = TOK+ZETA2(LR)*(TOO-TOK)	706210
500 STEPS(1,LRT) = ALPHPH*T	706220
STEPS(2,LRT) = ALPHTH*T	706230
200 STEPS(3,LRT) = 0.0	706240
112 CONTINUE	706250
DO 1236 K=1,53	706260
1236 SAVY(K) = 0.0	706270
WRITE(10) SAVY,NPLEV,NPLA,SIGMA,SALPH,SBAPH,STEPS,STR,EFF,STSRN,	706280
1 NPLAST,STSIG,STREPS,STALPH,STBAPH,NPLEVS,EFFST,SEPS	706290
8889 RETURN	706300
END	706310

```

FOR, IS GEOMET, GEOMET
SUBROUTINE GEOMET
THIS SUBROUTINE CALCULATES THE GEOMETRY FOR A SHELL SEGMENT.
THE INPUT VARIABLES ARE . . .
    RI(I) - - DISTANCE FROM AXIS OF REV. TO POINTS
                ON SHELL MERIDIAN.
    ZI(I) - - DISTANCE ALONG AXIS OF REV. TO THE
                INTERSECTION OF THE CORRESPONDING RI(I) AND
                THE AXIS OF REV.
    NRZIN - - NUMBER OF (RI,ZI) PAIRS READ AS INPUT.
COMMON /SPLINS/ ANG,PSI(100),RAD(100),CUR1(100),CUR2(100),
1 DR1DP(100),ZI(14),RI(14),NRZIN
DIMENSION CI(4,13),DRDZ(14),SOUT(14),S(101),RADD(100)
FUN(ARG) = SQRT(1.0 + ARG**2)
RADS = 3.1415926/180.0
DATA B/'B' '/'
AMULT = 1.0
IF (ANG.EQ.8) AMULT = -1.0
PASS SPLINE CURVE THROUGH INPUT POINTS ON SHELL MERIDIAN, AND
COMPUTE DR/DZ AT THESE POINTS.
CALL PLICO (ZI,RI,NRZIN,CI)
NDELZ = NRZIN - 1
DO 60 I=1,NRZIN
CALL PLINE (ZI,RI,NRZIN,CI,ZI(I),FAKE1,DRDZ(I),FAKE2)
60 CONTINUE
COMPUTE MERIDIONAL ARC LENGTH TO INTERPOLATED POINTS BY
NUMERICAL INTEGRATION (SIMPSONS RULE). SINCE SIMPSONS RULE
REQUIRES AN EVEN NUMBER OF PARTITIONS, INTERPOLATE A POINT
MIDWAY BETWEEN EACH PAIR OF POINTS USING SUBROUTINE SPLINE.
SOUT(1) = 0.
DO 70 I=1,NDELZ
DZ2=(ZI(I+1)-ZI(I))/2.0
DZ6=DZ2/3.0
CALL PLINE (ZI,RI,NRZIN,CI,ZI(I)+DZ2,FAKE1,DRDZM,FAKE2)
SOUT(I+1) = SOUT(I) + DZ6*(FUN(DRDZ(I)) + 4.0*FUN(DRDZM) +
1 FUN(DRDZ(I+1)))
70 CONTINUE
USE SPLICO TO REPRESENT RI(I) AS A FUNCTION OF SOUT(I). THEN USE
SPLINE TO INTERPOLATE RADD AND CORRESPONDING DERIVATIVES. FROM
THESE, COMPUTE THE TWO PRINCIPAL RADII OF CURVATURE,
    CUR1 = 1/R1
    CUR2 = 1/R2
OLDH1 = SOUT(NRZIN)/99.0
CALL PLICO (SOUT,RI,NRZIN,CI)
DO 110 I=1,100
S(I) = FLOAT(I-1)*OLDH1
CALL PLINE (SOUT,RI,NRZIN,CI,S(I),RAD(I),RADD(I),RADD2)
IF (ABS(RADD(I)).GT.1.0) RADD(I)=1.0
FACTOR = SQRT(1.0-RADD(I)**2)
CUR1(I) = -RADD2/FACTOR
CUR2(I) = FACTOR/RAD(I)

```



110	CONTINUE	2300600
	DO 180 J=1,100	2300610
	COSPSI = AMULT*RADD(J)	2300620
	PSI(J) = ARCOS(COSPSI)	2300630
	SINPSI = -AMULT*RAD(J)*CUR2(J)	2300640
	IF (ANG.EQ.B) GO TO 179	2300650
	PSI(J) = 2.0*3.1415926-PSI(J)	2300660
179	CONTINUE	2300670
	CUR1(J) = -AMULT/CUR1(J)	2300680
	CUR2(J) = -AMULT/CUR2(J)	2300690
	IF (J.EQ.1) GO TO 180	2300700
	I = 1	2300710
	IF (J.EQ.2) GO TO 181	2300720
	I = 2	2300730
181	IF (ANG.EQ.B) GO TO 190	2300740
	DR1DP(J-1) = (CUR1(J)-CUR1(J-I))/(PSI(J)-PSI(J-I))	2300750
	GO TO 180	2300760
190	DR1DP(J-1) = (CUR1(J-I)-CUR1(J))/(PSI(J-I)-PSI(J))	2300770
180	CONTINUE	2300780
	DR1DP(100) = DR1DP(99)	2300790
	DO 42 J=1,100	2300800
	DR1DP(J) = DR1DP(J)*0.1	2300810
42	CONTINUE	2300820
	RETURN	2300830
	END	2300840

FOR, IS PLICO, PLICO	
SUBROUTINE PLICO (X,Y,M,C)	2500010
C    SUBROUTINE TO DETERMINE C(1,K),C(2,K),C(3,K) AND C(4,K).	2500020
DIMENSION X(14),Y(14),A(14,3),B(14),Z(14)	2500030
DIMENSION D(13),P(13),E(13),C(4,13)	2500040
MM = M-1	2500050
DO 10 K=1,MM	2500060
D(K) = X(K+1) - X(K)	2500070
P(K) = D(K)/6.0	2500080
10    E(K) = (Y(K+1)-Y(K))/D(K)	2500090
DO 20 K=2,MM	2500100
20    B(K) = E(K) - E(K-1)	2500110
A(1,2) = -1.0-D(1)/D(2)	2500120
A(1,3) = D(1)/D(2)	2500130
A(2,3) = P(2)-P(1)*A(1,3)	2500140
A(2,2) = 2.0*(P(1)+P(2)) - P(1)*A(1,2)	2500150
A(2,3) = A(2,3)/A(2,2)	2500160
B(2) = B(2)/A(2,2)	2500170
DO 30 K=3,MM	2500180
A(K,2) = 2.0*(P(K-1)+P(K))-P(K-1)*A(K-1,3)	2500190
B(K) = B(K)-P(K-1)*B(K-1)	2500200
A(K,3) = P(K)/A(K,2)	2500210
30    B(K) = B(K)/A(K,2)	2500220
Q = D(M-2)/D(M-1)	2500230
A(M,1) = 1.0+Q+A(M-2,3)	2500240
A(M,2) = -Q-A(M,1)*A(M-1,3)	2500250
B(M) = B(M-2)-A(M,1)*B(M-1)	2500260
Z(M) = B(M)/A(M,2)	2500270
MN = M-2	2500280
DO 40 I=1,MN	2500290
K = M-I	2500300
40    Z(K) = B(K)-A(K,3)*Z(K+1)	2500310
Z(1) = -A(1,2)*Z(2)-A(1,3)*Z(3)	2500320
DO 50 K=1,MM	2500330
Q = 1.0/(6.0*D(K))	2500340
C(1,K) = Z(K)*Q	2500350
C(2,K) = Z(K+1)*Q	2500360
C(3,K) = Y(K)/D(K)-Z(K)*P(K)	2500370
50    C(4,K) = Y(K+1)/D(K)-Z(K+1)*P(K)	2500380
RETURN	2500390
END	2500400

FOR,IS PLINE,PLINE	2400010
C SUBROUTINE PLINE (X,Y,M,C,XINT,YINT,DYDX,D2YDX2)	2400020
C SUBROUTINE FOR SPLINE FIT INTERPOLATION IN THE TABLE OF VALUES	2400030
C (X1,Y1) TO (XM,YM), WHERE M MAY BE AS LARGE AS 100, WHERE THE	2400040
C CONSTANTS C(1,K),C(2,K),C(3,K) AND C(4,K) ARE ALREADY COMPUTED	2400050
C AND STORED.	2400060
C SUBROUTINE ALSO COMPUTES DY/DX AND D2Y/DX2 AT XINT.	2400070
DIMENSION X(14),Y(14),C(4,13)	2400080
IF (XINT-X(1)) 80,10,20	2400090
10 YINT = Y(1)	2400100
K=1	2400110
GO TO 70	2400120
20 K = 1	2400130
30 IF (XINT-X(K+1)) 60,40,50	2400140
40 YINT = Y(K+1)	2400150
GO TO 70	2400160
50 K = K + 1	2400170
IF (M-K) 80,80,30	2400180
60 YINT = (X(K+1) - XINT)*(C(1,K)*(X(K+1)-XINT)**2+C(3,K))	2400190
YINT = YINT + (XINT-X(K))*(C(2,K)*(XINT-X(K))**2+C(4,K))	2400200
70 DYDX=-3.0*(C(1,K)*(X(K+1)-XINT)**2-C(2,K)*(XINT-X(K))**2)	2400210
1 -C(3,K)+C(4,K)	2400220
D2YDX2=6.0*(C(1,K)*(X(K+1)-XINT)+C(2,K)*(XINT-X(K)))	2400230
RETURN	2400240
80 WRITE (6,90)	2400250
90 FORMAT (31H OUT OF RANGE FOR INTERPOLATION)	2400260
RETURN	2400270
END	

## SUBROUTINE DIF1 AND DIFF2

These subroutines are called in RIEMAN as necessary. DIF1 contains the differential equations for the THIC and ST clues, while DIFF2 contains the differential equations for the RWA and ISG clues. Geometry clues, trigonometric values, and predicted values of the differential equation variables are passed via label common area, EQUAZN, to subroutines DIF1 or DIFF2. The coefficients for nonlinear and load terms, X1, X2, X3 and K, are identified depending upon the input clues and pass number.

The specific derivative equations and auxiliary equations are contained in these subroutines. The values of each derivative equation, YDOT, and each auxiliary equation, YA---, are returned to RIEMAN via label common EQUAZN.

A special equation counter, I, is used in these subroutines, which counts in increments of eight. The first eight values of I, 1 through 57 (in increments of eight), correspond to the eight sets of initial conditions required to compute the segment stiffness matrices in subroutine SEGMAT. The subsequent value of I, 65 (again an increment of eight) corresponds to the computation of a set of eight equations for the loading condition.

FORTTRAN CODE

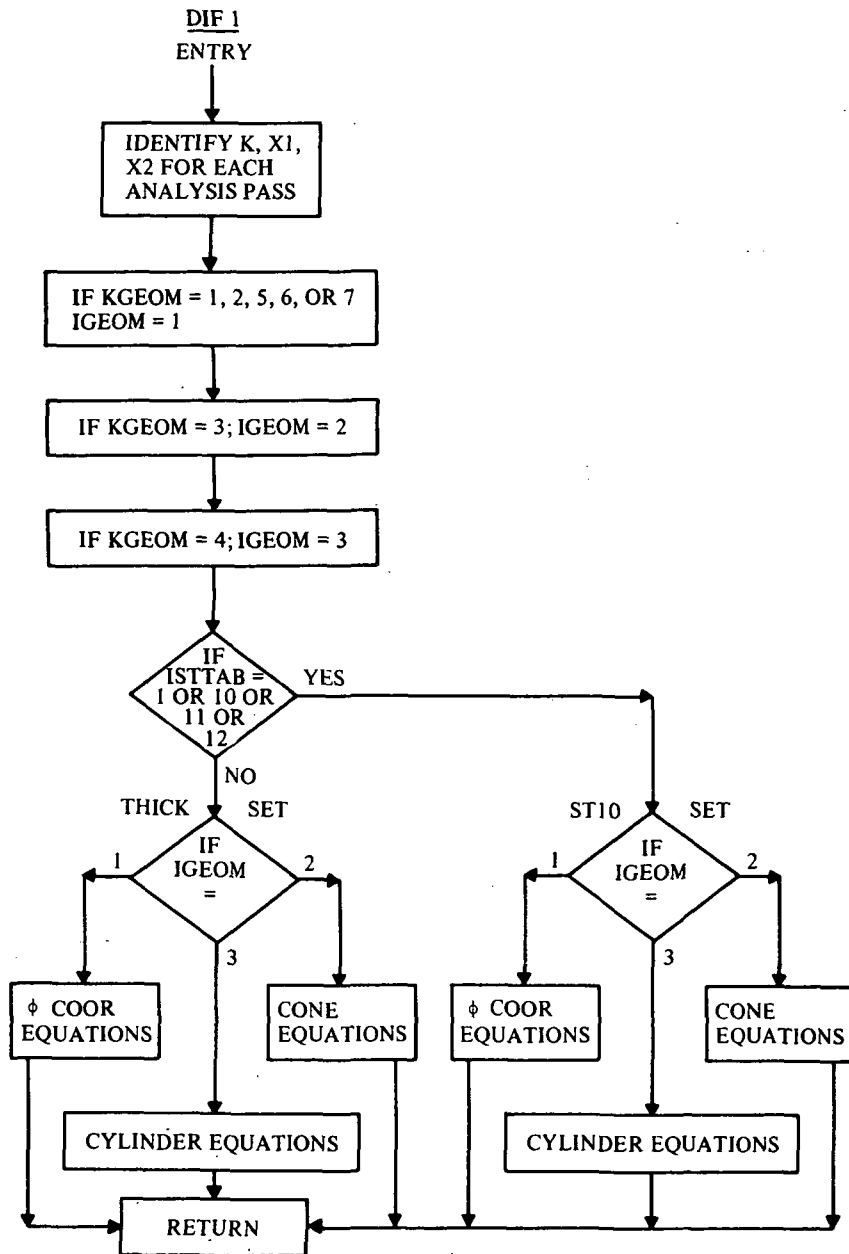
ENGINEERING SYMBOLS (REF. 1)

XN	n	
YDOT (I)	$T_{\phi\theta, \phi}$	$\frac{dT_{\phi\theta}}{ds}$
YDOT (I + 1)	$N_{\phi, \phi}$	$\frac{dN_{\phi}}{ds}$
YDOT (I + 2)	$J_{\phi, \phi}$	$\frac{dJ_{\phi}}{ds}$
YDOT (I + 3)	$M_{\phi, \phi}$	$\frac{dM_{\phi}}{ds}$
YDOT (I + 4)	$U_{\phi}$	$\frac{dU}{ds}$
YDOT (I + 5)	$V_{\phi}$	$\frac{dV}{ds}$
YDOT (I + 6)	$W_{\phi}$	$\frac{dW}{ds}$
YDOT (I + 7)	$\Omega_{\theta, \phi}$	$\frac{d\Omega_{\theta}}{ds}$
YPRED (I)	$T_{\phi\theta}$	
YPRED (I + 1)	$N_{\phi}$	
YPRED (I + 2)	$J_{\phi}$	
YPRED (I + 3)	$M_{\phi}$	
YPRED (I + 4)	U	
YPRED (I + 5)	V	
YPRED (I + 6)	W	
YPRED (I + 7)	$\Omega_{\theta}$	
YAMPT	$M_{\phi\theta}$	
YANTH	$N_{\theta}$	
YAMTH	$M_{\theta}$	

FORTRAN CODE	ENGINEERING SYMBOLS (REF. 1)
R2SQ	$r_2^2$
ROSQ	$r_0^2$
X1R0	$1/r_0$
S	s
XK12	$K_{12}$
XK21	$K_{21}$
XD12	$D_{12}$
XD21	$D_{21}$
XC11	$C_{11}$
XC22	$C_{22}$
XNSQ	$n^2$

Non-Linear Redefinitions (Ref. 2)

YDOT (I+2)	$*J_{\phi, \phi} \quad \frac{d*J_{\phi}}{ds}$
YPRED (I+2)	$*J_{\phi}$
YAJPH :	$J_{\phi}$
SAVY ( )	<p>appropriate nonlinear or plastic load terms updated from previous load increment.</p>



```

FOR,IS DIF1,DIF1
C ..... ROUTINE ** DIF1 ** ABACUS UPDATED 01/11/74 ..... 500000
SUBROUTINE DIF1 500010
INTEGER SAVJTC,SAVSTP,Q,THICK 500020
INTEGER XN1,XN 500030
REAL K 500040
DOUBLE PRECISION YPRED 500050
COMMON STORY(16),XMAT(270,10),STD(10),SADUS(30),RADUS(30) 500060
COMMON TADUS(30),UADUS(30),SAVTIC(900) 500070
COMMON XN,TEFREE,TIC,PHI,STOP,RESTOP,RTICK,G1,XNL(3),NH 500080
COMMON NST(30),NKL(30),NXMAT(20),SAVJTC(30),SAVSTP(30),JRTIC(30) 500090
COMMON JRSTOP(30),NREG,NMPT,NRC,NSC,NIX,IERROR,KGEOM,IGEOM,ISTTAB 500100
COMMON KELVIN,IBEGIN,NPROB,NSEG,NERROR,Q,THICK,NOJS,NLINKS,NLCASE 500110
COMMON NTSKL,NZ,NBCT,LINPUT,NTRKL,NPASS,XN1,KBC,NRINGS 500120
COMMON LODE,ICYCLE,LDISTL 500130
COMMON /EQUAZN/ YPRED(72),YDOT(72),YASAVE(72), 500140
1 YANTH,YAMTH,YAMPT,YAJPH, 500150
2 S,SN,CS,SNSQ,CSSQ,TAN,SEC,CN,X1CS,X1SN,TN, 500160
3 X1RO,X1ROSQ,X1SNRO,X1CSRO,CN1RO,SN1RO,CS1RO, 500170
4 X1R1,X1R2,CS1R1,CS1R2,SN1R1,X1R1SQ,R2SQ,RO,BESQ, 500180
5 ROSQ,XNSQ,BETA,R1,R2,S1,R1DOT, 500190
6 XNTTH,XNTPH,XMTTH,XMTPH,XFTHLD,XFPHLD,XFZELD, 500200
7 XMTHLD,XMPHLD,ETHET,EPHI,XGPT,ALPHTH,ALPHPH, 500210
8 XNUTP,XNUPT,XC11,XC22,XC15,XD33,XD22,XD21,XD12, 500220
9 XK11,XK12,XK21,XK22,XK33,XD11, 500230
A XNPHI,M,I,BETTA,ZETTA,XC16 500240
COMMON /WOOD/ SAVY(53),NPLEV,NLPO,NPLA(21),STR(6),SIGMA(3,21), 500250
C SEPS(3,21),SALPH(3,21),SBAPH(3,21),STEPS(3,21), 500260
D EFF(21),STSRN(3),NPLAST(3),STSIG(3),STREPS(3), 500270
M STALPH(3),STBAPH(3),EFFST(3),NPLEVS(3) 500280
COMMON /PLS/ OMEGA,IWORD,XMERD,XPRES,XMONT 500290
COMMON /CDISP/ P,PMAX,DELP,DELP1,YEPS,ZEPS 500300
EQUIVALENCE (XNL(1),X1),(XNL(2),X2),(XNL(3),X3),(K,DELP) 500310
IF (ISTTAB.NE.2) GO TO 7786 500320
C THE FOLLOWING EQUATIONS ARE THE 'THICK' SET 500330
GO TO (151,152,153),IGEOM 500340
C EQUATIONS FOR SHELLS OF REVOLUTION ( PHI COORDINATE ) 500350
151 CONTINUE 500360
YAOPH = XN*YPRED(I+6)*X1RO-YPRED(I+4)*SN1RO 500370
YANTH = XNUPT*YPRED(I+1)+(XK11-XNUPT**2*XK22)*((XN*YPRED(I+4)+ 500380
1 YPRED(I+5)*CS-YPRED(I+6)*SN)*X1RO+X1*YAOPH*SAVY(9))+K* 500390
2 (XNUPT*XNTPH-XNTTH)+X2*(XNUPT*SAVY(11)-SAVY(10)) 500400
3 +X3*SAVY(48) 500410
YAMTH = XNUPT*YPRED(I+3)-(XD11-XNUPT**2*XD22)*X1RO*(X1RO*(XN* 500420
1 YPRED(I+4)*SN-XNSQ*YPRED(I+6))+YPRED(I+7)*CS)+K* 500430
2 (XNUPT*XMTPH-XMTTH)+X2*(XNUPT*SAVY(14)-SAVY(13)) 500440
3 +X3*SAVY(49) 500450
YAMPT = (-1.0/((RO/XD33)+(SNSQ*X1RO/XK33)))*(-2.0*XN* 500460
1 YPRED(I+7)+YPRED(I+4)*(CS1R1-CN1RO)+XN*YPRED(I+5)* 500470
2 (SN1RO+X1R1)+2.0*XN*YPRED(I+6)*CS1RO+YPRED(I)*SN/ 500480
3 XK33+X2*(SAVY(12)*SN/XK33-SAVY(15)*RO/XD33)+SN*X1* 500490
4 (YAOPH*SAVY(5)+SAVY(9)*YPRED(I+7))) 500500
5 +X3*SAVY(50) 500510
YANPT = YPRED(I)+YAMPT*SN1RO 500520
YAJPH = YPRED(I+2)+X1*(SAVY(8)*YAOPH+YANPT*SAVY(9)-YPRED(I+1) 500530
1 *SAVY(5)-YPRED(I+7)*SAVY(6)) 500540
YDOT(I+4) = R1*(YPRED(I+4)*CS1RO+XN*YPRED(I+5)*X1RO+YPRED(I)/XK33+ 500550
1 X2*SAVY(12)/XK33+YAMPT*SN1RO/XK33)+R1*X1*(YAOPH* 500560
2 SAVY(5)+YPRED(I+7)*SAVY(9)) 500570
3 +X3*SAVY(51) 500580
YDOT(I+5) = R1*(YPRED(I+6)*X1R1+(1.0/(XK22-XNUTP**2*XK11))* 500590
1 (YPRED(I+1)-XNUTP*YANTH+K*(XNTPH-XNUTP*XNTTH))+X2* 500600

```



```

2          (SAVY(11)-XNUTP*SAVY(10))) -R1*YPRED(I+7)*X1*SAVY(5)      500610
3          +X3*SAVY(52)                                                    500620
A =      YPRED(I+5)*CS1RO-YPRED(I+6)*SN1RO+SAVY(9)*YAOPH+              500630
1        YDOT(I+5)/R1-YPRED(I+6)/R1+SAVY(5)*YPRED(I+7)                  500640
B =      SAVY(1)*CS1RO-SAVY(3)*SN1RO+.5*(SAVY(9)*SAVY(9)                500650
1        +SAVY(5)*SAVY(5))+(SAVY(2)-SAVY(3))/R1                          500660
YDOT(I)  = R1*(-2.0*YPRED(I)*CS1RO+XN*YANTH*X1RO-XN*YAMTH*SN*          500670
1        X1ROSQ-YAMPT*CS1RO*(X1R1-SN1RO))-R1*K*(XFTHLD+XMPHLD*          500680
2        SN1RO)-R1*X1*(SAVY(24)*A+K*XFTHLD*B+SAVY(25)*YDOT(I+4)        500690
3        /R1+SAVY(4)*K*XFPHLD/R1+SAVY(26)*YAOPH+SAVY(9)*K*              500700
4        XFZELD+SN/RO*(YANTH*SAVY(9)+YAOPH*SAVY(7)-YPRED(I+7))*          500710
5        SAVY(8)-YANPT*SAVY(5))-X3*SAVY(33)                               500720
YDOT(I+1) = R1*(CS1RO*(YANTH-YPRED(I+1))-XN*X1RO*(YPRED(I)+            500730
1        YAMPT*(SN*X1RO+X1R1))+YPRED(I+2)*X1R1)-R1*K*XFPHLD            500740
2        -R1*X1*(SAVY(25)*A+K*XFPHLD*B                                    500750
3        -SAVY(26)*YPRED(I+7)-SAVY(5)*K*XFZELD)                          500760
4        -X3*SAVY(34)                                                    500770
YDOT(I+2) = R1*(-YPRED(I+2)*CS1RO-YANTH*SN1RO-YPRED(I+1)*X1R1          500780
1        +XNSQ*YAMTH*X1ROSQ-2.0*XN*YAMPT*CS*X1ROSQ)+R1*K*              500790
2        (XN*XMPHLD*X1RO-XFZELD)-R1*X1*(SAVY(26)*A+K*XFZELD*          500800
3        B-SAVY(24)*YAOPH-SAVY(9)*K*                                      500810
4        XFTHLD+SAVY(25)*YPRED(I+7)+SAVY(5)*K*XFPHLD)                  500820
5        -X3*SAVY(35)                                                    500830
YDOT(I+3) = R1*(YAMTH*CS1RO-YPRED(I+3)*CS1RO-2.0*XN*YAMPT*X1RO+      500840
1        YAJPH+K*XMTHLD)                                                  500850
2        +X3*SAVY(36)                                                    500860
YDOT(I+6) = R1*(YPRED(I+7)-YPRED(I+5)*X1R1)                              500870
YDOT(I+7) = R1*(1.0/(XD22-XNUTP**2*XD11))*(-YPRED(I+3)+XNUTP*          500880
1        YAMTH-K*(XMTPH-XNUTP*XMTTH)-X2*(SAVY(14)-XNUTP*              500890
2        SAVY(13)))                                                       500900
3        +X3*SAVY(53)                                                    500910
GOTO 9005                                                                    500920
C EQUATIONS FOR CONE                                                         500930
152 CONTINUE                                                                    500940
YAOPH   = XN*YPRED(I+6)*X1CS/S-YPRED(I+4)*TAN/S                          500950
YANTH   = XNUTP*YPRED(I+1)+(XK11-XNUTP**2*XK22)*((X1CS/S)*(XN*          500960
1        YPRED(I+4)+YPRED(I+5)*CS-YPRED(I+6)*SN)+X1*YAOPH*              500970
2        SAVY(9))+K*(XNUTP*XNTPH-XNTTH)+X2*(XNUTP*SAVY(11)-            500980
3        SAVY(10))                                                         500990
4        +X3*SAVY(48)                                                     501000
YAMTH=XNUTP*YPRED(I+3)-(1.0/S)*X1CS*(XD11-XNUTP**2*XD22)*((1.0/S)*    501010
1        X1CS*(XN*YPRED(I+4)*SN-XNSQ*YPRED(I+6))+YPRED(I+7)*CS)-        501020
2        K*(XMTTH-XNUTP*XMTPH)                                             501030
3        +X2*(XNUTP*SAVY(14)-SAVY(13))                                    501040
4        +X3*SAVY(49)                                                     501050
YAMPT=(-1.0/((S*CS/XD33)+(SN*TN/(XK33*S))))*(-2.0*XN*YPRED(I+7)-        501060
1        YPRED(I+4)*SN/S+XN*YPRED(I+5)*TN/S+2.0*XN*YPRED(I+6)/S+YPRED    501070
2        (I)*SN/XK33+X2*(SAVY(12)*SN/XK33-SAVY(15))*S*CS/XD33)          501080
3        +SN*X1*(YAOPH*                                                  501090
4        SAVY(5)+SAVY(9)*YPRED(I+7)))                                      501100
5        +X3*SAVY(50)                                                     501110
YANPT   = YPRED(I)+YAMPT*TAN/S                                             501120
YAJPH   = YPRED(I+2)+X1*(SAVY(8)*YAOPH+YANPT*SAVY(9)-YPRED(I+1)*      501130
1        SAVY(5)-YPRED(I+7)*SAVY(6))                                       501140
YDOT(I+4)=(1.0/S)*(YPRED(I+4)+XN*YPRED(I+5)*X1CS+YAMPT*TN/XK33)          501150
1        +YPRED(I)/XK33+X2*SAVY(12)/XK33+X1*(YAOPH*SAVY(5)              501160
2        +YPRED(I+7)*SAVY(9))                                              501170
3        +X3*SAVY(51)                                                     501180
YDOT(I+5) = (1.0/(XK22-XNUTP**2*XK11))*(-YPRED(I+1)-XNUTP*YANTH+      501190
1        K*(XNTPH-XNUTP*XNTTH)+X2*(SAVY(11)-XNUTP*SAVY(10)))            501200
2        -YPRED(I+7)*X1*SAVY(5)                                           501210

```

```

3          +X3*SAVY(52) 501220
A =       YPRED(I+5)/S-YPRED(I+6)*TN/S+SAVY(9)*YAOPH+YDOT(I+5) 501230
1          +SAVY(5)*YPRED(I+7) 501240
B =       SAVY(1)/S-SAVY(3)*TN/S+0.5*(SAVY(9)*SAVY(9)+SAVY(5)* 501250
1          SAVY(5))+SAVY(2) 501260
YDOT(I)  =-2.0*YPRED(I)/S+XN*YANTH*X1CS/S-XN*YAMTH*SN*X1CS**2/S**2 501270
1          +YAMPT*TAN/S**2-K*(XFTHLD+XMPHLD*TAN/S)-X1*(SAVY(24)* 501280
2          A+K*XFTHLD*B+SAVY(25)*YDOT(I+4)+SAVY(4)*K*XFPHLD+ 501290
3          SAVY(26)*YAOPH+SAVY(9)*K*XFZELD+TAN/S*(YANTH*SAVY(9)+ 501300
4          YAOPH*SAVY(7)-YPRED(I+7)*SAVY(8)-YANPT*SAVY(5))-X3* 501310
5          SAVY(33) 501320
YDOT(I+1)=-YPRED(I+1)/S+YANTH/S-XN*YPRED(I)/(S*CS)-XN*YAMPT*SN/ 501330
1          (S*S*CS*CS)-K*XFPHLD-X1*(SAVY(25)*A+K*XFPHLD*B- 501340
2          SAVY(26)*YPRED(I+7)-SAVY(5)*K*XFZELD) 501350
3          -X3*SAVY(34) 501360
YDOT(I+2) = -YPRED(I+2)/S-YANTH*TAN/S+XNSQ*YAMTH/(S**2*CS**2) 501370
1          -2.0*XN*YAMPT/(S**2*CS)+K*(XN*XMPHLD*X1CS/S-XFZELD) 501380
2          -X1*(SAVY(26)*A+K*XFZELD*B-SAVY(24)*YAOPH-SAVY(9)*K* 501390
3          XFTHLD+SAVY(25)*YPRED(I+7)+SAVY(5)*K*XFPHLD) 501400
4          -X3*SAVY(35) 501410
YDOT(I+3)= YAMTH/S-YPRED(I+3)/S-2.0*XN*YAMPT/(S*CS)+YAJPH+XMTHLD 501420
1          *K 501430
2          +X3*SAVY(36) 501440
YDOT(I+6)=YPRED(I+7) 501450
YDOT(I+7)=(1.0/(XD22-XNUTP**2*XD11))*(-YPRED(I+3)+XNUTP*YAMTH- 501460
1          K*(XMPH-XNUTP*XMTTH)-X2*(SAVY(14)-XNUTP*SAVY(13))) 501470
2          +X3*SAVY(53) 501480
GO TO 9005 501490
C EQUATIONS FOR CYLINDER 501500
153 CONTINUE 501510
YAOPH = X1RO*(XN*YPRED(I+6)-YPRED(I+4)) 501520
YANTH = XNUTP*YPRED(I+1)+(XK11-XNUTP**2*XK22)*((X1RO*(XN* 501530
1          YPRED(I+4)-YPRED(I+6)))+X1*YAOPH*SAVY(9))+K*(XNUTP* 501540
2          XNTPH-XNTTH)+X2*(XNUTP*SAVY(11)-SAVY(10)) 501550
3          +X3*SAVY(48) 501560
YAMTH=XNUTP*YPRED(I+3)-(X1RO*(XD11-XNUTP**2*XD22))*((X1RO*(XN*YPRED 501570
1          (I+4)-XNSQ*YPRED(I+6)))+K*(XNUTP*XMPH-XMTTH) 501580
2          +X2*(XNUTP*SAVY(14)-SAVY(13))) 501590
3          +X3*SAVY(49) 501600
YAMPT=(-1.0/((RO/XD33)+(X1RO/XK33)))*(-2.0*XN*YPRED(I+7)+XN*X1RO* 501610
1          YPRED(I+5)+YPRED(I)/XK33+X2*(SAVY(12)/XK33-SAVY(15)* 501620
2          RO/XD33)+X1*(YAOPH*SAVY(5)+SAVY(9)*YPRED(I+7))) 501630
3          +X3*SAVY(50) 501640
YANPT = YPRED(I)+YAMPT*X1RO 501650
YAJPH = YPRED(I+2)+X1*(SAVY(8)*YAOPH+YANPT*SAVY(9)-YPRED(I+1) 501660
1          *SAVY(5)-YPRED(I+7)*SAVY(6)) 501670
YDOT(I+4) = XN*YPRED(I+5)*X1RO+YPRED(I)/XK33+X2*SAVY(12)/XK33+ 501680
1          YAMPT*X1RO/XK33+X1*(YAOPH*SAVY(5)+YPRED(I+7)*SAVY(9)) 501690
2          +X3*SAVY(51) 501700
YDOT(I+5) = (1.0/(XK22-XNUTP**2*XK11))*((YPRED(I+1)-XNUTP*YANTH+ 501710
1          K*(XNTPH-XNUTP*XNTTH)+X2*(SAVY(11)-XNUTP*SAVY(10)))- 501720
2          YPRED(I+7)*X1*SAVY(5) 501730
3          +X3*SAVY(52) 501740
A =       -YPRED(I+6)/RO+SAVY(9)*YAOPH+YDOT(I+5)+SAVY(5)* 501750
1          YPRED(I+7) 501760
B =       -SAVY(3)/RO+0.5*(SAVY(9)*SAVY(9)+SAVY(5)*SAVY(5))+ 501770
1          SAVY(2) 501780
YDOT(I)  = XN*YANTH*X1RO-XN*YAMTH*X1ROSQ-K*(XFTHLD+XMPHLD*X1RO) 501790
1          -X1*(SAVY(24)*A+K*XFTHLD*B+SAVY(25)*YDOT(I+4)+SAVY(4)* 501800
2          K*XFPHLD+SAVY(26)*YAOPH+SAVY(9)*K*XFZELD+(YANTH* 501810
3          SAVY(9)+YAOPH*SAVY(7)-YPRED(I+7)*SAVY(8)-YANPT* 501820
4          SAVY(5))/RO)-X3*SAVY(33) 501830

```

```

YDOT(I+1) = -XN*X1RO*YPRED(I)-XN*YAMPT*X1ROSQ-K*XFPHLD-X1*      501840
1 (SAVY(25)*A+K*XFPHLD*B-SAVY(26)*YPRED(I+7)-SAVY(5)*          501850
2 K*XFZELD)                                                       501860
3 -X3*SAVY(34)                                                    501870
YDOT(I+2) = -YANTH*X1RO+XNSQ*YAMTH*X1ROSQ+K*(XN*XMPHLD*X1RO-    501880
1 XFZELD)-X1*(SAVY(26)*A+K*XFZELD*B-SAVY(24)*YAOPH-          501890
2 SAVY(9)*K*XFTHLD+SAVY(25)*YPRED(I+7)+SAVY(5)*K*XFPHLD)    501900
3 -X3*SAVY(35)                                                    501910
YDOT(I+3) = -2.0*XN*YAMPT*X1RO+YAJPH+K*XMTHLD                    501920
1 +X3*SAVY(36)                                                    501930
YDOT(I+6)=YPRED(I+7)                                              501940
YDOT(I+7) = (1.0/(XD22-XNUTP**2*XD11))*(-YPRED(I+3)+XNUTP*YAMTH+ 501950
1 K*(XNUTP*XMTTH-XMTPH)-X2*(SAVY(14)-XNUTP*SAVY(13)))          501960
2 +X3*SAVY(53)                                                    501970
GO TO 9005.                                                         501980
7786 GO TO (4771,4772,4773),IGEOM                                  501990
C THE FOLLOWING EQUATIONS ARE THE 'ST10' SET                        502000
C EQUATIONS FOR SHELLS OF REVOLUTION ( PHI COORDINATE )          502010
4771 CONTINUE                                                       502020
YAOPH = XN*YPRED(I+6)*X1RO-YPRED(I+4)*SN1RO                       502030
YANTH = XK12*(1.0/(XK22+XC22**2/XD22))*(YPRED(I+1)+K*XNTPH+      502040
1 X2*SAVY(11)+(XC22/XD22)*(YPRED(I+3)+K*XMTPH+X2*              502050
1 SAVY(14)))-K*XNTTH-X2*SAVY(10)+(X1RO*XK11-                    502060
1 XK12*XK21*X1RO*(1.0/                                          502070
2 (XK22+XC22**2/XD22)))*(XN*YPRED(I+4)+YPRED(I+5)*CS-YPRED(I+ 502080
3 6)*SN+X1*RO*YAOPH*SAVY(9))-(XC11+XK12*XC22*XD21/XD22*      502090
3 (1.0/(XK22+XC22**2/XD22)))*                                  502100
4 (X1RO**2*(XN*YPRED(I+4)*SN-XN**2*YPRED(I+6))+YPRED(I+7)*CS* 502110
5 X1RO)                                                           502120
6 +X3*SAVY(48)                                                    502130
YAMTH = -XD12*(XC22/(XC22**2+XK22*XD22))*(YPRED(I+1)+K*XNTPH+ 502140
1 X2*SAVY(11))-K*XMTTH-X2*SAVY(13)+XD12*(XK22/(XC22**2+      502150
2 XK22*XD22))*(YPRED(I+3)+K*XMTPH+X2*SAVY(14))+(XC11*        502160
2 X1RO+XD12*XK21*X1RO*(XC22/(XC22**2+XK22*XD22)))*(XN*YPRED( 502170
3 I+4)+YPRED(I+5)*CS-YPRED(I+6)*SN+X1*RO*YAOPH*SAVY(9)))+ 502180
3 (XD11-XD12*XK22*XD21/(                                       502190
4 XC22**2+XK22*XD22))*(X1ROSQ*(XN*YPRED(I+4)*SN-XNSQ*YPRED 502200
5 (I+6))+YPRED(I+7)*CS*X1RO)                                    502210
6 +X3*SAVY(49)                                                    502220
YAMPT = (-1.0/(RO/XD33)+(SNSQ*X1RO/XK33))*(-2.0*XN*              502230
1 YPRED(I+7)+YPRED(I+4)*(CS1R1-CN1RO)+XN*YPRED(I+5)*          502240
2 (SN1RO+X1R1)+2.0*XN*YPRED(I+6)*CS1RO+YPRED(I)*SN/           502250
3 XK33+X2*(SAVY(12)*SN/XK33-SAVY(15)*RO/XD33)+SN*X1*         502260
4 (YAOPH*SAVY(5)+SAVY(9)*YPRED(I+7)))                          502270
5 +X3*SAVY(50)                                                    502280
YANPT = YPRED(I)+YAMPT*SN1RO                                       502290
YAJPH = YPRED(I+2)+X1*(SAVY(8)*YAOPH+YANPT*SAVY(9)-YPRED(I+1) 502300
1 *SAVY(5)-YPRED(I+7)*SAVY(6))                                  502310
YDOT(I+4) = R1*(YPRED(I+4)*CS1RO+XN*YPRED(I+5)*X1RO+YPRED(I)/XK33+ 502320
1 X2*SAVY(12)/XK33+YAMPT*SN1RO/XK33)+R1*X1*(YAOPH*           502330
2 SAVY(5)+YPRED(I+7)*SAVY(9))                                  502340
3 +X3*SAVY(51)                                                    502350
YDOT(I+5) = R1*(YPRED(I+6)*X1R1-X1*YPRED(I+7)*SAVY(5)+(1.0/(XK22+ 502360
1 XC22**2/XD22))*(YPRED(I+1)+K*XNTPH+X2*SAVY(11)+(XC22/      502370
1 XD22)*(YPRED(I+3)+K*XMTPH+X2*SAVY(14))-XK21*X1RO*(XN*      502380
2 YPRED(I+4)+YPRED(I+5)*CS-YPRED(I+6)*SN)-X1*XK12*YAOPH*    502390
2 SAVY(9)-(XC22*XD21/XD22                                       502400
3 )*(X1ROSQ*(XN*YPRED(I+4)*SN-XNSQ*YPRED(I+6))+YPRED(I+7)    502410
4 *CS*X1RO)))                                                    502420
5 +X3*SAVY(52)                                                    502430
A = YPRED(I+5)*CS1RO-YPRED(I+6)*SN1RO+SAVY(9)*YAOPH+          502440

```

```

1          YDOT(I+5)/R1-YPRED(I+6)/R1+SAVY(5)*YPRED(I+7)          502450
B =       SAVY(1)*CS1RO-SAVY(3)*SN1RO+.5*(SAVY(9)*SAVY(9)          502460
1         +SAVY(5)*SAVY(5))+(SAVY(2)-SAVY(3))/R1                    502470
YDOT(I)   = R1*(-2.0*YPRED(I)*CS1RO+XN*YANTH*X1RO-XN*YAMTH*SN*    502480
1         X1ROSQ-YAMPT*CS1RO*(X1R1-SN1RO))-R1*K*(XFTHLD+XMPHLD*    502490
2         SN1RO)-R1*X1*(SAVY(24)*A+K*XFTHLD*B+SAVY(25)*YDOT(I+4)    502500
3         /R1+SAVY(4)*K*XFPHLD/R1+SAVY(26)*YAOPH+SAVY(9)*K*        502510
4         XFZELD+SN/RD*(YANTH*SAVY(9)+YAOPH*SAVY(7)-YPRED(I+7)*    502520
5         SAVY(8)-YANPT*SAVY(5))-X3*SAVY(33)                          502530
YDOT(I+1) = R1*(CS1RO*(YANTH-YPRED(I+1))-XN*X1RO*(YPRED(I)+      502540
1         YAMPT*(SN*X1RO+X1R1))+YPRED(I+2)*X1R1)-R1*K*XFPHLD      502550
2         -R1*X1*(SAVY(25)*A+K*XFPHLD*B                               502560
3         -SAVY(26)*YPRED(I+7)-SAVY(5)*K*XFZELD)                    502570
4         -X3*SAVY(34)                                                502580
YDOT(I+2) = R1*(-YPRED(I+2)*CS1RO-YANTH*SN1RO-YPRED(I+1)*X1R1    502590
1         +XNSQ*YAMTH*X1ROSQ-2.0*XN*YAMPT*CS*X1ROSQ)+R1*K*        502600
2         (XN*XMPHLD*X1RO-XFZELD)-R1*X1*(SAVY(26)*A+K*XFZELD*    502610
3         B-SAVY(24)*YAOPH-SAVY(9)*K*                                502620
4         XFTHLD+SAVY(25)*YPRED(I+7)+SAVY(5)*K*XFPHLD)            502630
5         -X3*SAVY(35)                                                502640
YDOT(I+3) = R1*(YAMTH*CS1RO-YPRED(I+3)*CS1RO-2.0*XN*YAMPT*X1RO+  502650
1         YAJPH+K*XMTHLD)                                             502660
2         +X3*SAVY(36)                                                502670
YDOT(I+6) = R1*(YPRED(I+7)-YPRED(I+5)*X1R1)                          502680
YDOT(I+7) = R1*((-XC22/(XC22**2+XK22*XD22))*(YPRED(I+1)+K*XNTPH+  502690
1         X2*SAVY(11)-(XK21/RO)*(XN*YPRED(I+4)+YPRED(I+5)*CS-    502700
2         YPRED(I+6)*SN)-X1*XK12*YAOPH+SAVY(9)))+(XK22/(XC22**2+  502710
3         XK22*XD22))*(YPRED(I+3)+K*XNTPH+X2*SAVY(14))-XK22*    502720
4         XD21/(XC22**2+XK22*XD22))*(X1ROSQ*(XN*YPRED(I+4)*SN-XNSQ  502730
5         *YPRED(I+6))+YPRED(I+7)*CS*X1RO))                          502740
6         +X3*SAVY(53)                                                502750
GO TO 9005                                                              502760
C EQUATIONS FOR CONE                                                  502770
4772 CONTINUE                                                         502780
YAOPH     = XN*YPRED(I+6)*X1CS/S-YPRED(I+4)*TAN/S                    502790
YANTH     = XK12*(1.0/(XK22+XC22**2/XD22))*(YPRED(I+1)+K*XNTPH+    502800
1         X2*SAVY(11)+(XC22/XD22)*(YPRED(I+3)+K*XNTPH+X2*        502810
2         SAVY(14)))-K*XNTTH-X2*SAVY(10)+(1.0/(CS*S))              502820
3         *(XK11-XK12*XK21*(                                       502830
4         1.0/(XK22+XC22**2/XD22)))+(XN*YPRED(I+4)+YPRED(I+5)*CS-  502840
5         YPRED(I+6)*SN+X1*S*CS*YAOPH+SAVY(9))-(XC11+(XK12*XD21*  502850
6         XC22/XD22))*(1.0/(XK22+XC22*                               502860
7         *2/XD22)))*((1.0/(S**2*CS**2))*(XN*YPRED(I+4)*SN-XNSQ*YPRED  502870
8         (I+6))+YPRED(I+7)/S)                                         502880
9         +X3*SAVY(48)                                                502890
YAMTH     = -XD12*(XC22/(XC22**2+XK22*XD22))*(YPRED(I+1)+K*XNTPH+  502900
1         X2*SAVY(11))-K*XMTTH-X2*SAVY(13)+XD12*(XK22/(XC22**2+  502910
2         XK22*XD22))*(YPRED(I+3)+K*XNTPH+X2*SAVY(14)))+(XC11/    502920
3         (S*CS)+XD12*XK21/(S*CS))*(XC22/(XC22**2+XK22*XD22))*(XN*  502930
4         YPRED(I+4)+YPRED(I+5)*CS-YPRED(I+6)*SN+X1*S*CS*YAOPH*    502940
5         SAVY(9)))+(XD11-XD12*XK22*                                502950
6         XD21/(XC22**2+XK22*XD22))*((1.0/(S*CS)**2)*(XN*YPRED(I+4)*  502960
7         SN-XNSQ*YPRED(I+6))+YPRED(I+7)/S)                          502970
8         +X3*SAVY(49)                                                502980
YAMPT     = (-1.0/((S*CS/XD33)+(SN*TN/(XK33*S))))*(-2.0*XN*YPRED(I+7)-  502990
1         YPRED(I+4)*SN/S+XN*YPRED(I+5)*TN/S+2.0*XN*YPRED(I+6)/S+YPRED  503000
2         (I)*SN/XK33+X2*(SAVY(12)*SN/XK33-SAVY(15)*S*CS/XD33)    503010
3         +SN*X1*(YAOPH*                                            503020
4         SAVY(5)+SAVY(9)*YPRED(I+7)))                              503030
5         +X3*SAVY(50)                                                503040
YANPT     = YPRED(I)+YAMPT*TAN/S                                       503050
YAJPH     = YPRED(I+2)+X1*(SAVY(8)*YAOPH+YANPT*SAVY(9)-YPRED(I+1)*  503060

```

```

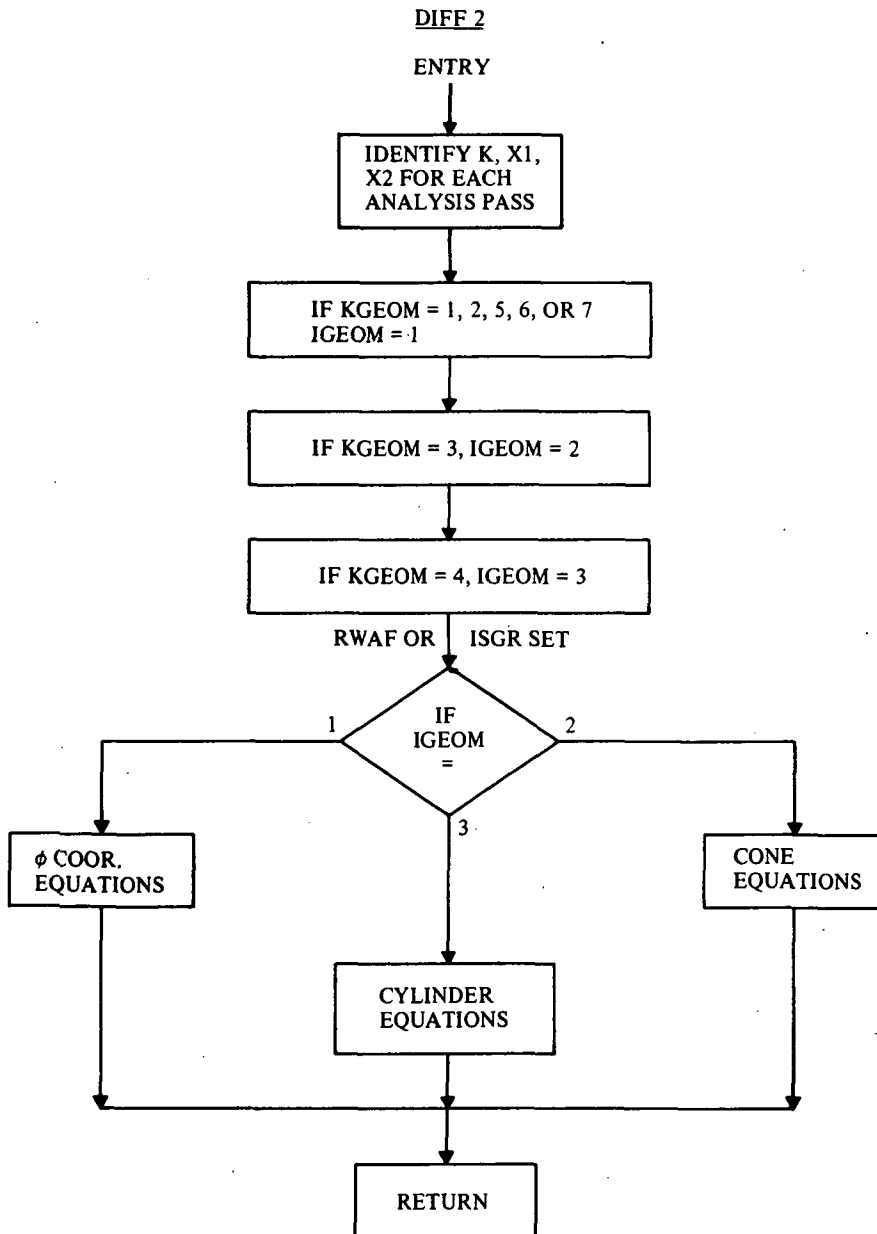
1          SAVY(5)-YPRED(I+7)*SAVY(6)
YDOT(I+4)=(1.0/S)*(YPRED(I+4)+XN*YPRED(I+5)*X1CS+YAMPT*TN/XK33)
1          +YPRED(I)/XK33+X2*SAVY(12)/XK33+X1*(YAOPH*SAVY(5)
2          +YPRED(I+7)*SAVY(9))
3          +X3*SAVY(51)
YDOT(I+5) = -X1*YPRED(I+7)*SAVY(5)+(1.0/(XK22+XC22**2/XD22))*
1          (YPRED(I+1)+K*XNTPH+X2*SAVY(11)+(XC22/XD22)*
2          (YPRED(I+3)+K*XMTPH+X2*SAVY(14))-(XK21/(S*CS))*(XN*
3          YPRED(I+4)+YPRED(I+5)*CS-YPRED(I+6)*SN)-X1*XK12*YAOPH*
4          SAVY(9)-(XC22*XD21/XD22))*((1.0/(S**2*CS**
3          2))*(XN*YPRED(I+4)*SN-XNSQ*YPRED(I+6))+YPRED(I+7)/S))
4          +X3*SAVY(52)
A = YPRED(I+5)/S-YPRED(I+6)*TN/S+SAVY(9)*YAOPH+YDOT(I+5)
1          +SAVY(5)*YPRED(I+7)
B = SAVY(1)/S-SAVY(3)*TN/S+0.5*(SAVY(9)*SAVY(9)+SAVY(5)*
1          SAVY(5))+SAVY(2)
YDOT(I)  = -2.0*YPRED(I)/S+XN*YANTH*X1CS/S-XN*YAMTH*SN*X1CS**2/S**2
1          +YAMPT*TAN/S**2-K*(XFTHLD+XMPHLD*TAN/S)-X1*(SAVY(24)*
2          A+K*XFTHLD*B+SAVY(25)*YDOT(I+4)+SAVY(4)*K*XFPHLD+
3          SAVY(26)*YAOPH+SAVY(9)*K*XFZELD+TAN/S*(YANTH*SAVY(9)+
4          YAOPH*SAVY(7)-YPRED(I+7)*SAVY(8)-YANPT*SAVY(5)))-X3*
5          SAVY(33)
YDOT(I+1) = -YPRED(I+1)/S+YANTH/S-XN*YPRED(I)/(S*CS)-XN*YAMPT*SN/
1          (S*S*CS*CS)-K*XFPHLD-X1*(SAVY(25)*A+K*XFPHLD*B-
2          SAVY(26)*YPRED(I+7)-SAVY(5)*K*XFZELD)
3          -X3*SAVY(34)
YDOT(I+2) = -YPRED(I+2)/S-YANTH*TAN/S+XNSQ*YAMTH/(S**2*CS**2)
1          -2.0*XN*YAMPT/(S**2*CS)+K*(XN*XMPHLD*X1CS/S-XFZELD)
2          +X1*(SAVY(26)*A+K*XFZELD*B-SAVY(24)*YAOPH-SAVY(9)*K*
3          XFTHLD+SAVY(25)*YPRED(I+7)+SAVY(5)*K*XFPHLD)
4          -X3*SAVY(35)
YDOT(I+3) = YAMTH/S-YPRED(I+3)/S-2.0*XN*YAMPT/(S*CS)+YAJPH+XMTHLD
1          *K
2          +X3*SAVY(36)
YDOT(I+6) = YPRED(I+7)
YDOT(I+7) = -(XC22/(XC22**2+XK22*XD22))*(YPRED(I+1)+K*XNTPH+X2*
1          SAVY(11)-XK21*(XN*YPRED(I+4)+YPRED(I+5)*CS-YPRED(I+6)*
1          SN)/(S*CS)-X1*XK12*YAOPH*SAVY(9))+(XK22/(XC22**2+XK22*
2          XD22))*(YPRED(I+3)+K*XMTPH+X2*SAVY(14))-(XK22*XD21
3          /XC22**2+XK22*XD22))*((1.0/(S*CS)**2)*(XN*YPRED(I+4)*SN
4          -XN**2*YPRED(I+6))+YPRED(I+7)/S)
5          +X3*SAVY(53)
GO TO 9005
C EQUATIONS FOR CYLINDER
4773 CONTINUE
YAOPH = X1RO*(XN*YPRED(I+6)-YPRED(I+4))
YANTH = XK12*(1.0/(XK22+XC22**2/XD22))*(YPRED(I+1)+K*XNTPH+
1          X2*SAVY(11)+
1          (XC22/XD22)*(YPRED(I+3)+K*XMTPH+X2*SAVY(14)))-K*XNTTH-
1          X2*SAVY(10)+(X1RO*(XK11-XK12*XK21*(1.0/(XK22+XC22**2/
2          XD22))))*(XN*YPRED(I+4)-YPRED(I+6)+X1RO*YAOPH*
2          SAVY(9))-(XC11+(
3          XK12*XC22*XD21/XD22)*(1.0/(XK22+XC22**2/XD22)))*(X1RO**2*(
4          XN*YPRED(I+4)-XNSQ*YPRED(I+6)))
5          +X3*SAVY(48)
YAMTH = -XD12*(XC22/(XC22**2+XK22*XD22))*(YPRED(I+1)+K*XNTPH+
1          X2*SAVY(11))-K*XMTTH-X2*SAVY(13)+XD12*(XK22/(XC22**2+
2          XK22*XD22))*(YPRED(I+3)+K*XMTPH+X2*SAVY(14))+(XC11*
2          X1RO+XD12*XK21*X1RO*(XC22/(XC22**2+XK22*XD22)))*(XN*YPRED
3          (I+4)-YPRED(I+6)+X1RO*YAOPH*SAVY(9))+(XD11-XD12*XK22*
3          XD21/(XC22**2+XK22*XD22)
503070
503080
503090
503100
503110
503120
503130
503140
503150
503160
503170
503180
503190
503200
503210
503220
503230
503240
503250
503260
503270
503280
503290
503300
503310
503320
503330
503340
503350
503360
503370
503380
503390
503400
503410
503420
503430
503440
503450
503460
503470
503480
503490
503500
503510
503520
503530
503540
503550
503560
503570
503580
503590
503600
503610
503620
503630
503640
503650
503660
503670

```

```

4      )*(X1ROSQ*(XN*YPRED(I+4)-XNSQ*YPRED(I+6)))          503680
5      +X3*SAVY(49)                                          503690
YAMPT=(-1.0/(IRO/XD33)+(X1RO/XK33))*(-2.0*XN*YPRED(I+7)+XN*X1RO*  503700
1      YPRED(I+5)+YPRED(I)/XK33+X2*(SAVY(12)/XK33-SAVY(15)*  503710
2      RO/XD33)+X1*(YAOPH*SAVY(5)+SAVY(9)*YPRED(I+7)))      503720
3      +X3*SAVY(50)                                          503730
YANPT = YPRED(I)+YAMPT*X1RO                                  503740
YAJPH = YPRED(I+2)+X1*(SAVY(8)*YAOPH+YANPT*SAVY(9)-YPRED(I+1)  503750
1      *SAVY(5)-YPRED(I+7)*SAVY(6))                        503760
YDOT(I+4) = XN*YPRED(I+5)*X1RO+YPRED(I)/XK33+X2*SAVY(12)/XK33+  503770
1      YAMPT*X1RO/XK33+X1*(YAOPH*SAVY(5)+YPRED(I+7)*SAVY(9))  503780
2      +X3*SAVY(51)                                          503790
YDOT(I+5) = -X1*YPRED(I+7)*SAVY(5)+(1.0/(XK22+XC22**2/XD22))*  503800
1      (YPRED(I+1)+K*XNTPH+X2*SAVY(11)+(XC22/XD22)*          503810
2      (YPRED(I+3)+K*XMTPH+X2*SAVY(14))-(XK21*X1RO))*(XN*    503820
3      YPRED(I+4)-YPRED(I+6))-X1*XK12*YAOPH*SAVY(9)-(XC22*  503830
4      XD21/XD22)*(X1ROSQ*(XN*(YPRED(I+4)-XN*YPRED(I+6))))    503840
5      +X3*SAVY(52)                                          503850
A = -YPRED(I+6)/RO+SAVY(9)*YAOPH+YDOT(I+5)+SAVY(5)*        503860
1      YPRED(I+7)                                          503870
B = -SAVY(3)/RO+0.5*(SAVY(9)*SAVY(9)+SAVY(5)*SAVY(5))+    503880
1      SAVY(2)                                              503890
YDOT(I) = XN*YANTH*X1RO-XN*YAMTH*X1ROSQ-K*(XFTHLD+XMPHLD*X1RO)  503900
1      -X1*(SAVY(24)*A+K*XFTHLD*B+SAVY(25)*YDOT(I+4)+SAVY(4)*  503910
2      K*XFPHLD+SAVY(26)*YAOPH+SAVY(9)*K*XFZELD+(YANTH*    503920
3      SAVY(9)+YAOPH*SAVY(7)-YPRED(I+7)*SAVY(8)-YANPT*    503930
4      SAVY(5))/RO)-X3*SAVY(33)                              503940
YDOT(I+1) = -XN*X1RO*YPRED(I)-XN*YAMPT*X1ROSQ-K*XFPHLD-X1*    503950
1      (SAVY(25)*A+K*XFPHLD*B-SAVY(26)*YPRED(I+7)-SAVY(5)*  503960
2      K*XFZELD)                                          503970
3      -X3*SAVY(34)                                          503980
YDOT(I+2) = -YANTH*X1RO+XNSQ*YAMTH*X1ROSQ+K*(XN*XMPHLD*X1RO-  503990
1      XFZELD)-X1*(SAVY(26)*A+K*XFZELD*B-SAVY(24)*YAOPH-    504000
2      SAVY(9)*K*XFTHLD+SAVY(25)*YPRED(I+7)+SAVY(5)*K*XFPHLD)  504010
3      -X3*SAVY(35)                                          504020
YDOT(I+3) = -2.0*XN*YAMPT*X1RO+YAJPH+K*XMTHLD                504030
1      +X3*SAVY(36)                                          504040
YDOT(I+6)=YPRED(I+7)                                          504050
YDOT(I+7) = -(XC22/(XC22**2+XK22*XD22))*(YPRED(I+1)+K*XNTPH+X2*  504060
1      SAVY(11)-XK21*X1RO*(XN*YPRED(I+4)-YPRED(I+6))-X1*XK12*  504070
2      YAOPH*SAVY(9))+(XC22/(XC22**2+XK22*XD22))*(YPRED(I+3)+  504080
1      K*XMTPH+X2*SAVY(14))-(XK22*XD21/(XC22**2+XK22*XD22))*  504090
3      X1ROSQ*(XN*YPRED(I+4)-XNSQ*YPRED(I+6)))              504100
4      +X3*SAVY(53)                                          504110
9005 CONTINUE                                               504120
      RETURN                                                 504130
      END                                                     504140

```



```

FOR,IS DIFF2,DIFF2
C ..... ROUTINE ** DIFF2 ** ABACUS UPDATED 01/11/74 ..... 600000
SUBROUTINE DIFF2 600010
INTEGER SAVJTC,SAVSTP,Q,THICK 600020
INTEGER XN1,XN 600030
REAL K 600040
DOUBLE PRECISION YPRED 600050
COMMON STORY(16),XMAT(270,10),STD(10),SADUS(30),RADUS(30) 600060
COMMON TADUS(30),UADUS(30),SAVTIC(900) 600070
COMMON XN,TEFREE,TIC,PHI,STOP,RESTOP,RTICK,G1,XNL(3),NH 600080
COMMON NST(30),NKL(30),NXMAT(20),SAVJTC(30),SAVSTP(30),JRTIC(30) 600090
COMMON JRSTOP(30),NREG,NMPT,NRC,NSC,NIX,IERROR,KGEOM,IGEOM,ISTTAB 600100
COMMON KELVIN,IBEGIN,NPROB,NSEG,NERROR,Q,THICK,NOJS,NLNKS,NLCASE 600110
COMMON NTSKL,NZ,NBCT,LINPUT,NTRKL,NPASS,XN1,KBC,NRINGS 600120
COMMON LODE,ICYCLE,LDISTL 600130
COMMON /EQUAZN/ YPRED(72),YDOT(72),YASAVE(72), 600140
1 YANTH,YAMTH,YAMPT,YAJPH, 600150
2 S,SN,CS,SNSQ,CSSQ,TAN,SEC,CN,X1CS,X1SN,TN, 600160
3 X1RO,X1ROSQ,X1SNRO,X1CSRO,CN1RO,SN1RO,CS1RO, 600170
4 X1R1,X1R2,CS1R1,CS1R2,SN1R1,X1R1SQ,R2SQ,RO,BESQ, 600180
5 ROSQ,XNSQ,BETA,R1,R2,S1,R1DOT, 600190
6 XNTTH,XNTPH,XMTTH,XMTPH,XFTHLD,XFPHLD,XFZELD, 600200
7 XMTHLD,XMPHLD,ETHET,EPHI,XGPT,ALPHTH,ALPHPH, 600210
8 XNUTP,XNUPT,XC11,XC22,XC15,XD33,XD22,XD21,XD12, 600220
9 XK11,XK12,XK21,XK22,XK33,XD11, 600230
A XNPHI,M,I,BETTA,ZETTA,XC16 600240
COMMON /PLS/ OMEGA,IWORD,XMERD,XPRES,XMONT 600250
COMMON /WOOD/ SAVY(53),NPLEV,NLPO,NPLA(21),STR(6),SIGMA(3,21), 600260
C SEPS(3,21),SALPH(3,21),SBAPH(3,21),STEPS(3,21), 600270
O EFF(21),STSRN(3),NPLAST(3),STSIG(3),STREPS(3), 600280
M STALPH(3),STBAPH(3),EFFST(3),NPLEVS(3) 600290
COMMON /COISP/ P,PMAX,DELP,DELP1,YEPS,ZEPS 600300
EQUIVALENCE (XNL(1),X1),(XNL(2),X2),(XNL(3),X3),(K,DELP) 600310
7447 GO TO (7341,7342,7343),IGEOM 600320
C THE FOLLOWING EQUATIONS ARE THE 'RWF' SET 600330
C EQUATIONS FOR SHELLS OF REVOLUTION ( PHI COORDINATE ) 600340
7341 CONTINUE 600350
YAOPH = XN*YPRED(I+6)*X1RO-YPRED(I+4)*SN1RO 600360
YANTH = (YPRED(I+1)+K*XNTPH+X2*SAVY(11))*(XC15*XC22+XD22*XK12) 600370
1 /(XK22*XD22+XC22**2)-K*XNTTH-X2*SAVY(10)+(XK12*XC22- 600380
1 XK22*XC15)*(YPRED(I+3)+K*XMTPH+X2*SAVY(14))/(XC22* 600390
2 XC22+XK22*XD22)+(X1RO*(XN*YPRED(I+4)+YPRED(I+5)*CS- 600400
2 YPRED(I+6)*SN)+X1*YAOPH*SAVY(9))*(XK11+(XC15*(XC15* 600410
3 XK22-2.0*XK12*XC22)-XK12*XK12* 600420
4 XD22)/(XK22*XD22+XC22*XC22)+(X1ROSQ*(XN*YPRED(I+4)*SN-XNSQ 600430
5 *YPRED(I+6))+X1RO*YPRED(I+7)*CS)*(-XC11+(XC15*XC15*XC22+ 600440
6 XC15*(XK12*XD22+XK22*XD12)-XK12*XD12*XC22)/(XK22*XD22+XC22*XC22)) 600450
7 +X3*SAVY(48) 600460
YAMTH= (YPRED(I+3)+K*XMTPH+X2*SAVY(14))*(XC15*XC22+XK22*XD12) 600470
1 /(XK22*XD22+XC22*XC22)+(YPRED(I+1)+K*XNTPH+X2*SAVY(11) 600480
2 )*(XD22*XC15-XD12*XC22)/(XD22*XK22+XC22**2)-K*XMTTH- 600490
3 X2*SAVY(13)+(X1ROSQ*(XN*YPRED(I+4)*SN-XNSQ*YPRED(I+6)) 600500
4 +X1RO*YPRED(I+7)*CS)*(XD11-(XD12*XD12*XK22+XC15*(2.0* 600510
5 XC22*XD12-XC15*XD22))/(XC22*XC22+XK22*XD22)+(X1RO* 600520
6 (XN*YPRED(I+4)+YPRED(I+5)*CS-YPRED(I+6)*SN)+X1*YAOPH* 600530
7 SAVY(9))*(XC11+(XD12*XC22*XK12-XC15*(XC15*XC22+XD12* 600540
8 XK22+XD22*XK12))/(XC22*XC22+XK22*XD22)) 600550
9 +X3*SAVY(49) 600560
YAMPT = (1.0/(XC16*SN*X1RO-XK33-SN*X1RO*(XD33*SN/(RO)-XC16))) 600570
1 *((XK33*XD33-XC16**2)*X1RO*(-2.0*XN*YPRED(I+7)+YPRED(I+4)* 600580

```



```

2      (CS*X1R1-CN1RO)+XN*YPRED(I+5)*(X1R1+SN1RO)+2.0*XN*YPRED      600590
3      (I+6)*CS*X1RO)+X1*SN*(YAOPH*SAVY(5)+YPRED(I+7)*SAVY(9)      600600
4      )+(YPRED(I)+X2*SAVY(12))*(XD33*SN*X1RO-XC16)+X2*      600610
5      SAVY(15)*(XK33-XC16*SN/RO))      600620
6      +X3*SAVY(50)      600630
YANPT      = YPRED(I)+YAMPT*SN1RO      600640
YAJPH      = YPRED(I+2)+X1*(SAVY(8)*YAOPH+YANPT*SAVY(9)-YPRED(I+1)      600650
1      *SAVY(5)-YPRED(I+7)*SAVY(6))      600660
YDOT(I+4)  = R1*(YPRED(I+4)*CS*X1RO+X1*(YAOPH*SAVY(5)+YPRED(I+7)*      600670
1      SAVY(9))      600680
1      +XN*YPRED(I+5)*X1RO+(1.0/(XK33-      600690
2      XC16**2/XD33))*(YPRED(I)+YAMPT*(SN*X1RO-XC16/XD33)+X2*      600700
3      (SAVY(12)-XC16*SAVY(15)/XD33)))      600710
4      +X3*SAVY(51)      600720
YDOT(I+5)  = YPRED(I+6)-R1*X1*YPRED(I+7)*SAVY(5)+R1*(XD22*(YPRED(I+      600730
1      1)+K*XNTPH+X2*SAVY(11))+XC22*(YPRED(I+3)+K*XMTPH+X2*      600740
2      SAVY(14))-(X1RO*(XN*YPRED(I+4)+YPRED(I+5)*CS-YPRED(I+6      600750
2      )*SN)+X1*YAOPH*SAVY(9))*      600760
3      (XK12*XD22+XC15*XC22)-(X1ROSQ*(XN*YPRED(I+4)-XNSQ*      600770
4      YPRED(I+6))+X1RO*YPRED(I+7)*CS)*(XC22*XD12-XC15*XD22))      600780
5      /(XK22*XD22+XC22**2)      600790
6      +X3*SAVY(52)      600800
A      = YPRED(I+5)*CS1RO-YPRED(I+6)*SN1RO+SAVY(9)*YAOPH+      600810
1      YDOT(I+5)/R1-YPRED(I+6)/R1+SAVY(5)*YPRED(I+7)      600820
B      = SAVY(1)*CS1RO-SAVY(3)*SN1RO+.5*(SAVY(9)*SAVY(9)      600830
1      +SAVY(5)*SAVY(5))+(SAVY(2)-SAVY(3))/R1      600840
YDOT(I)    = R1*(-2.0*YPRED(I)*CS1RO+XN*YANTH*X1RO-XN*YAMTH*SN*      600850
1      X1ROSQ-YAMPT*CS1RO*(X1R1-SN1RO))-R1*K*(XFTHLD+XMPHLD*      600860
2      SN1RO)-R1*X1*(SAVY(24)*A+K*XFTHLD*B+SAVY(25)*YDOT(I+4)      600870
3      /R1+SAVY(4)*K*XFPHLD/R1+SAVY(26)*YAOPH+SAVY(9)*K*      600880
4      XFZELD+SN/RO*(YANTH*SAVY(9)+YAOPH*SAVY(7)-YPRED(I+7)*      600890
5      SAVY(8)-YANPT*SAVY(5)))-X3*SAVY(33)      600900
YDOT(I+1)  = R1*(CS1RO*(YANTH-YPRED(I+1))-XN*X1RO*(YPRED(I)+      600910
1      YAMPT*(SN*X1RO+X1R1))+YPRED(I+2)*X1R1)-R1*K*XFPHLD      600920
2      -R1*X1*(SAVY(25)*A+K*XFPHLD*B      600930
3      -SAVY(26)*YPRED(I+7)-SAVY(5)*K*XFZELD)      600940
4      -X3*SAVY(34)      600950
YDOT(I+2)  = R1*(-YPRED(I+2)*CS1RO-YANTH*SN1RO-YPRED(I+1)*X1R1      600960
1      +XNSQ*YAMTH*X1ROSQ-2.0*XN*YAMPT*CS*X1ROSQ)+R1*K*      600970
2      (XN*XMPHLD*X1RO-XFZELD)-R1*X1*(SAVY(26)*A+K*XFZELD*      600980
3      B-SAVY(24)*YAOPH-SAVY(9)*K*      600990
4      XFTHLD+SAVY(25)*YPRED(I+7)+SAVY(5)*K*XFPHLD)      601000
5      -X3*SAVY(35)      601010
YDOT(I+3)  = R1*(YAMTH*CS1RO-YPRED(I+3)*CS1RO-2.0*XN*YAMPT*X1RO+      601020
1      YAJPH+K*XMTHLD)      601030
2      +X3*SAVY(36)      601040
YDOT(I+6)  = R1*(YPRED(I+7)-YPRED(I+5)*X1R1)      601050
YDOT(I+7)  = R1*(XK22*(YPRED(I+3)+K*XMTPH+X2*SAVY(14))-XC22*(YPRED(      601060
1      I+1)+K*XNTPH+X2*SAVY(11))+X1RO*(XN*YPRED(I+4)+      601070
1      YPRED(I+5)*CS-YPRED(I+6)*SN)+X1*YAOPH*SAVY(9))*(XK12*      601080
2      XC22-XK22*XC15)      601090
2      -(X1ROSQ*(XN*YPRED(I+4)*SN-XNSQ*YPRED(I+6))+X1RO*YPRED(I+7)*CS)*      601100
3      (XC15*XC22+XK22*XD12))/(XC22**2+XK22*XD22)      601110
3      +X3*SAVY(53)      601120
GO TO 9005      601130
C      EQUATIONS FOR CONE      601140
7342 CONTINUE      601150
YAOPH      = XN*YPRED(I+6)*X1CS/S-YPRED(I+4)*TAN/S      601160
YANTH      = (YPRED(I+1)+K*XNTPH+X2*SAVY(11))*(XC15*XC22+XD22*XK12)      601170
1      /(XK22*XD22+XC22**2)-K*XNTPH-X2*SAVY(10)+(XK12*XC22-      601180
1      XK22*XC15)*(YPRED(I+3)+K*XMTPH+X2*SAVY(14))/(XC22*      601190

```

```

2          XC22+XK22*XD22)+((XN*YPRED(I+4)+YPRED(I+5)*CS-      601200
3          YPRED(I+6)*SN)/(S*CS)+X1*YAOPH*SAVY(9))* (XK11+(XC15*      601210
3          (XC15*XK22-2.0*XK12*XC22)-XK12*XK12*      601220
4          XD22)/(XK22*XD22+XC22*XC22))+((XN*YPRED(I+4)*SN-XNSQ*      601230
5          YPRED(I+6))/(S*S*CSSQ)+YPRED(I+7)/S)*(-XC11+(XC15*XC15*XC22+      601240
6          XC15*(XK12*XD22+XK22*XD12)-XK12*XD12*XC22)/(XK22*XD22+XC22*XC22))      601250
7          +X3*SAVY(48)      601260
YAMTH =      (YPRED(I+3)+K*XMTPH+X2*SAVY(14))* (XC15*XC22+XK22*XD12)      601270
1          /(XK22*XD22+XC22**2)+(YPRED(I+1)+K*XNTPH+X2*SAVY(11))*      601280
1          (XD22*XC15-XD12*XC22)/(XD22*XK22+XC22**2)-K*XMTTH-X2*      601290
2          SAVY(13)+(1.0/(S*S*CSSQ))*(-XNSQ*YPRED(I+6)+XN*      601300
2          YPRED(I+4))*      601310
3          SN)+YPRED(I+7)/S)*(XD11-(XD12*XD12*XK22+XC15*(2.0*XC22*XD12-XC15*      601320
4          XD22))/(XC22*XC22+XK22*XD22))+((1.0/(S*CS))*(XN*      601330
5          YPRED(I+4)+YPRED(I+5)*CS-YPRED(I+6)*SN)+X1*YAOPH*      601340
6          SAVY(9))* (XC11+(XD12*XC22*XK12-XC15*(XC15*XC22+XD12*      601350
7          XK22+XD22*XK12))/(XC22*XC22+XK22*XD22))      601360
8          +X3*SAVY(49)      601370
YAMPT = ((XC16*TAN/S-XK33-(TAN/S)*(XD33*TAN/S-XC16))*(-1))*((XK33*      601380
1          XD33-XC16**2)*(1.0/(S*CS))*(-2.0*XN*YPRED(I+7)-YPRED(I+4)*      601390
2          SN/S+XN*YPRED(I+5)*TAN/S+2.0*XN*YPRED(I+6)/S)+X1*SN*      601400
3          (YAOPH*SAVY(5)+YPRED(I+7)*SAVY(9)))+(YPRED(I)+X2*      601410
4          SAVY(12))*(XD33*TAN/S-XC16)+X2*SAVY(15)*(XK33-XC16*      601420
5          TN/S))      601430
6          +X3*SAVY(50)      601440
YANPT      = YPRED(I)+YAMPT*TAN/S      601450
YAJPH =      YPRED(I+2)+X1*(SAVY(8)*YAOPH+YANPT*SAVY(9)-YPRED(I+1)*      601460
1          SAVY(5)-YPRED(I+7)*SAVY(6))      601470
YDOT(I+4) = YPRED(I+4)/S+X1*(YAOPH*SAVY(5)+YPRED(I+7)*SAVY(9))+XN*      601480
1          YPRED(I+5)/(S*CS)+(1.0/(XK33-XC16**2/      601490
2          XD33))*(YPRED(I)+YAMPT*(TAN/S-XC16/XD33)+X2*(SAVY(12)-      601500
3          XC16*SAVY(15)/XD33))      601510
4          +X3*SAVY(51)      601520
YDOT(I+5) = -X1*YPRED(I+7)*SAVY(5)+(XD22*(YPRED(I+1)+K*XNTPH+X2*      601530
1          SAVY(11))+XC22*(YPRED(I+3)+K*XMTPH+X2*SAVY(14))-(XK12*      601540
1          XD22+XC15*XC22))*((1.0/(S*CS))*(XN*YPRED(I+4)+YPRED(I+5)      601550
2          *CS-YPRED(I+6)*SN))+X1*YAOPH*SAVY(9))-(XC22*XD12-XC15*      601560
2          XD22)*((-XNSQ*      601570
3          YPRED(I+6)+XN*YPRED(I+4)*SN)/(S*S*CSSQ)+YPRED(I+7)/S))      601580
4          /(XK22*XD22+XC22*XC22)      601590
5          +X3*SAVY(52)      601600
A =      YPRED(I+5)/S-YPRED(I+6)*TN/S+SAVY(9)*YAOPH+YDOT(I+5)      601610
1          +SAVY(5)*YPRED(I+7)      601620
B =      SAVY(1)/S-SAVY(3)*TN/S+0.5*(SAVY(9)*SAVY(9)+SAVY(5)*      601630
1          SAVY(5))+SAVY(2)      601640
YDOT(I) = -2.0*YPRED(I)/S+XN*YANTH*X1CS/S-XN*YAMTH*SN*X1CS**2/S**2      601650
1          +YAMPT*TAN/S**2-K*(XFTHLD+XMPHLD*TAN/S)-X1*(SAVY(24)*      601660
2          A+K*XFTHLD*B+SAVY(25)*YDOT(I+4)+SAVY(4)*K*XFPHLD+      601670
3          SAVY(26)*YAOPH+SAVY(9)*K*XFZELD+TAN/S*(YANTH*SAVY(9)+      601680
4          YAOPH*SAVY(7)-YPRED(I+7)*SAVY(8)-YANPT*SAVY(5))-X3*      601690
5          SAVY(33)      601700
YDOT(I+1) = -YPRED(I+1)/S+YANTH/S-XN*YPRED(I)/(S*CS)-XN*YAMPT*SN/      601710
1          (S*S*CS*CS)-K*XFPHLD-X1*(SAVY(25)*A+K*XFPHLD*B-      601720
2          SAVY(26)*YPRED(I+7)-SAVY(5)*K*XFZELD)      601730
3          -X3*SAVY(34)      601740
YDOT(I+2) = -YPRED(I+2)/S-YANTH*TAN/S+XNSQ*YAMTH/(S**2*CS**2)      601750
1          -2.0*XN*YAMPT/(S**2*CS)+K*(XN*XMPHLD*X1CS/S-XFZELD)      601760
2          +X1*(SAVY(26)*A+K*XFZELD*B-SAVY(24)*YAOPH-SAVY(9)*K*      601770
3          XFTHLD+SAVY(25)*YPRED(I+7)+SAVY(5)*K*XFPHLD)      601780
4          -X3*SAVY(35)      601790
YDOT(I+3) = YAMTH/S-YPRED(I+3)/S-2.0*XN*YAMPT/(S*CS)+YAJPH+XMTHLD      601800

```

```

1          *K 601810
2          +X3*SAVY(36) 601820
YDOT(I+6)=YPRED(I+7) 601830
YDOT(I+7) = (XK22*(YPRED(I+3)+K*XMTPH+X2*SAVY(14))-XC22*
1          (YPRED(I+1)+K*XNTPH+X2*SAVY(11)))+(XK12*XC22-XK22*XC15) 601840
2          *((1.0/(S*CS))*(XN*YPRED(I+4)+YPRED(I+5)*CS-YPRED(I+6)* 601860
2          SN))+X1*YAOPH*SAVY(9))-(XC15*XC22+XK22*XD12)* 601870
3          ((-XNSQ*YPRED(I+6)+XN*YPRED(I+4)*SN)/(S*S*CSSQ)+ 601880
4          YPRED(I+7)/S))/(XK22*XD22+XC22*XC22) 601890
5          +X3*SAVY(53) 601900
GO TO 9005 601910
C EQUATIONS FOR CYLINDER 601920
7343 CONTINUE 601930
YAOPH = X1RO*(XN*YPRED(I+6)-YPRED(I+4)) 601940
YANTH = (YPRED(I+1)+K*XNTPH+X2*SAVY(11))*(XC15*XC22+XD22*XK12) 601950
1          /(XK22*XD22+XC22**2)-K*XNTTH-X2*SAVY(10)+(XK12*XC22- 601960
2          XK22*XC15)*(YPRED(I+3)+K*XMTPH+X2*SAVY(14))/(XC22* 601970
2          XC22+XK22*XD22)+(X1RO*(XN*YPRED(I+4)-YPRED(I+6))+X1* 601980
3          YAOPH*SAVY(9))*(XK11+(XC15*(XC15*XK22-2.0*XK12*XC22)- 601990
3          XK12*XK12* 602000
4          XD22)/(XK22*XD22+XC22*XC22))+(X1ROSQ*(XN*YPRED(I+4)-XNSQ 602010
5          *YPRED(I+6)))*(-XC11+(XC15*XC15*XC22+ 602020
6          XC15*(XK12*XD22+XK22*XD12)-XK12*XD12*XC22)/(XK22*XD22+XC22*XC22)) 602030
7          +X3*SAVY(48) 602040
YAMTH = (YPRED(I+3)+K*XMTPH+X2*SAVY(14))*(XC15*XC22+XK22*XD12) 602050
1          /(XK22*XD22+XC22**2)+(YPRED(I+1)+K*XNTPH+X2*SAVY(11))* 602060
2          (XD22*XC15-XD12*XC22)/(XD22*XK22+XC22**2)-K*XMTTH-X2* 602070
2          SAVY(13)+X1ROSQ*(XN*YPRED(I+4)-XNSQ*YPRED(I+6)) 602080
3          *(XD11-(XD12*XD12*XK22+XC15*(2.0*XC22*XD12-XC15* 602090
4          XD22))/(XC22*XC22+XK22*XD22))+(X1RO*(XN*YPRED(I+4)- 602100
5          YPRED(I+6))+X1*YAOPH*SAVY(9))*(XC11+(XD12*XC22*XK12- 602110
5          XC15*(XC15*XC22+XD12*XK22+ 602120
6          XD22*XK12))/(XC22*XC22+XK22*XD22)) 602130
7          +X3*SAVY(49) 602140
YAMPT=(1/(XC16*X1RO-XK33-X1RO*(XD33*X1RO-XC16)))*((XK33*XD33-XC16 602150
1          **2)*X1RO*(-2.0*XN*YPRED(I+7)+XN*X1RO*YPRED(I+5))+X1* 602160
2          (YAOPH*SAVY(5)+YPRED(I+7)*SAVY(9))+YPRED(I)+X2* 602170
3          SAVY(12))*(XD33*X1RO-XC16)+X2*SAVY(15)*(XK33-XC16/RO)) 602180
4          +X3*SAVY(50) 602190
YANPT = YPRED(I)+YAMPT*X1RO 602200
YAJPH = YPRED(I+2)+X1*(SAVY(8)*YAOPH+YANPT*SAVY(9)-YPRED(I+1) 602210
1          *SAVY(5)-YPRED(I+7)*SAVY(6)) 602220
YDOT(I+4) = X1*(YAOPH*SAVY(5)+YPRED(I+7)*SAVY(9))+XN*YPRED(I+5)/RO 602230
1          + 602240
1          (1.0/(XK33-XC16**2/XD33))*(YPRED(I)+ 602250
2          YAMPT*(X1RO-XC16/XD33)+X2*(SAVY(12)-XC16*SAVY(15)/ 602260
3          XD33)) 602270
4          +X3*SAVY(51) 602280
YDOT(I+5) = -X1*YPRED(I+7)*SAVY(5)+(XD22*(YPRED(I+1)+K*XNTPH+X2* 602290
1          SAVY(11))+XC22*(YPRED(I+3)+K*XMTPH+X2*SAVY(14))-(X1RO* 602300
1          (XN*YPRED(I+4)-YPRED(I+6))+X1*YAOPH*SAVY(9))*(XK12* 602310
2          XD22+XC15*XC22)-X1ROSQ*(XN*YPRED 602320
2          (I+4)-XNSQ*YPRED(I+6))*(XC22*XD12-XC15*XD22))/(XK22*XD22+XC22**2) 602330
3          +X3*SAVY(52) 602340
A = -YPRED(I+6)/RO+SAVY(9)*YAOPH+YDOT(I+5)+SAVY(5)* 602350
1          YPRED(I+7) 602360
B = -SAVY(3)/RO+0.5*(SAVY(9)*SAVY(9)+SAVY(5)*SAVY(5))+ 602370
1          SAVY(2) 602380
YDOT(I) = XN*YANTH*X1RO-XN*YAMTH*X1ROSQ-K*(XFTHLD+XMPHLD*X1RO) 602390
1          -X1*(SAVY(24)*A+K*XFTHLD*B+SAVY(25)*YDOT(I+4)+SAVY(4)* 602400
2          K*XFPHLD+SAVY(26)*YAOPH+SAVY(9)*K*XFZELD+(YANTH* 602410

```

3	SAVY(9)+YAOPH*SAVY(7)-YPRED(I+7)*SAVY(8)-YANPT*	602420
4	SAVY(5))/RO)-X3*SAVY(33)	602430
	YDOT(I+1) = -XN*X1RO*YPRED(I)-XN*YAMPT*X1ROSQ-K*XFPHLD-X1*	602440
1	(SAVY(25)*A+K*XFPHLD*B-SAVY(26)*YPRED(I+7)-SAVY(5)*	602450
2	K*XFZELD)	602460
3	-X3*SAVY(34)	602470
	YDOT(I+2) = -YANTH*X1RO+XNSQ*YAMTH*X1ROSQ+K*(XN*XMPHLD*X1RO-	602480
1	XFZELD)-X1*(SAVY(26)*A+K*XFZELD*B-SAVY(24)*YAOPH-	602490
2	SAVY(9)*K*XFTHLD+SAVY(25)*YPRED(I+7)+SAVY(5)*K*XFPHLD)	602500
3	-X3*SAVY(35)	602510
	YDOT(I+3) = -2.0*XN*YAMPT*X1RO+YAJPH+K*XMTHLD	602520
1	+X3*SAVY(36)	602530
	YDOT(I+6)=YPRED(I+7)	602540
	YDOT(I+7) = (XK22*(YPRED(I+3)+K*XMPH+X2*SAVY(14))-XC22*	602550
1	(YPRED(I+1)+K*XNTPH+X2*SAVY(11)))+(X1RO*(XN*YPRED(I+4)-	602560
1	YPRED(I+6))+X1*YAOPH*SAVY(9))*(XK12*XC22-XK22*XC15)-	602570
2	X1ROSQ*(XN*YPRED	602580
2	(I+4)-XNSQ*YPRED(I+6))*(XC15*XC22+XK22*XD12))/(XC22*2+XK22*XD22)	602590
3	+X3*SAVY(53)	602600
9005	CONTINUE	602610
	RETURN	602620
	END	602630

### SUBROUTINE SEGMAT

The results of the subroutine link, RIEMAN, are passed through the label common area, LYCORR, to this subroutine. SEGMAT places the elements of the YCORR array into several double-subscripted arrays, forms some coordinate transformation arrays, and calls subroutine SREVN2 for double precision matrix inversion.

As a result of appropriate matrix operations this subroutine produces a segment stiffness matrix, the XKS array, and a segment load matrix, the XLS array, for each segment. SEGMAT also orients each segment into the global coordinate system of the structure as a result of the matrix operations.

#### Subroutine SREVN2

SREVN2 is a subroutine called by SEGMAT to invert a real, double-precision, in-core matrix utilizing Gauss-Jordan elimination with partial pivoting.

FORTRAN CODE

ENGINEERING SYMBOLS (REF. 1)

SNi

si

SNj

sj

CSI

ci

CSJ

cj

A MATRIX

$$\left[ \begin{array}{c|c} \text{IFT} & 0 \\ \hline 0 & \text{JFT} \end{array} \right]$$

B MATRIX

$$\left[ \begin{array}{c|c|c|c} 0 & I_4 & & 0 \\ \hline X_1 & X_2 & & X_3 \end{array} \right]$$

C MATRIX

$$\left[ \begin{array}{c|c|c} I_4 & 0 & 0 \\ \hline 0 & Y_2^{-1} & 0 \\ \hline 0 & 0 & I_p \end{array} \right]$$

D MATRIX

$$\left[ \begin{array}{c|c|c} I_4 & 0 & 0 \\ \hline -Y_1 & \text{JDT}^T & -Y_3 \\ \hline 0 & 0 & I_p \end{array} \right]$$

E MATRIX

$$\left[ \begin{array}{c|c|c} \text{IDT}^T & 0 & 0 \\ \hline 0 & I_4 & 0 \\ \hline 0 & 0 & I_p \end{array} \right]$$

XKT MATRIX

$$[k \mid \ell]$$

XMAX MATRIX

$$\left[ \begin{array}{c|c} 2\pi r_0(i) & \\ \hline & 2\pi r_0(j) \end{array} \right]$$

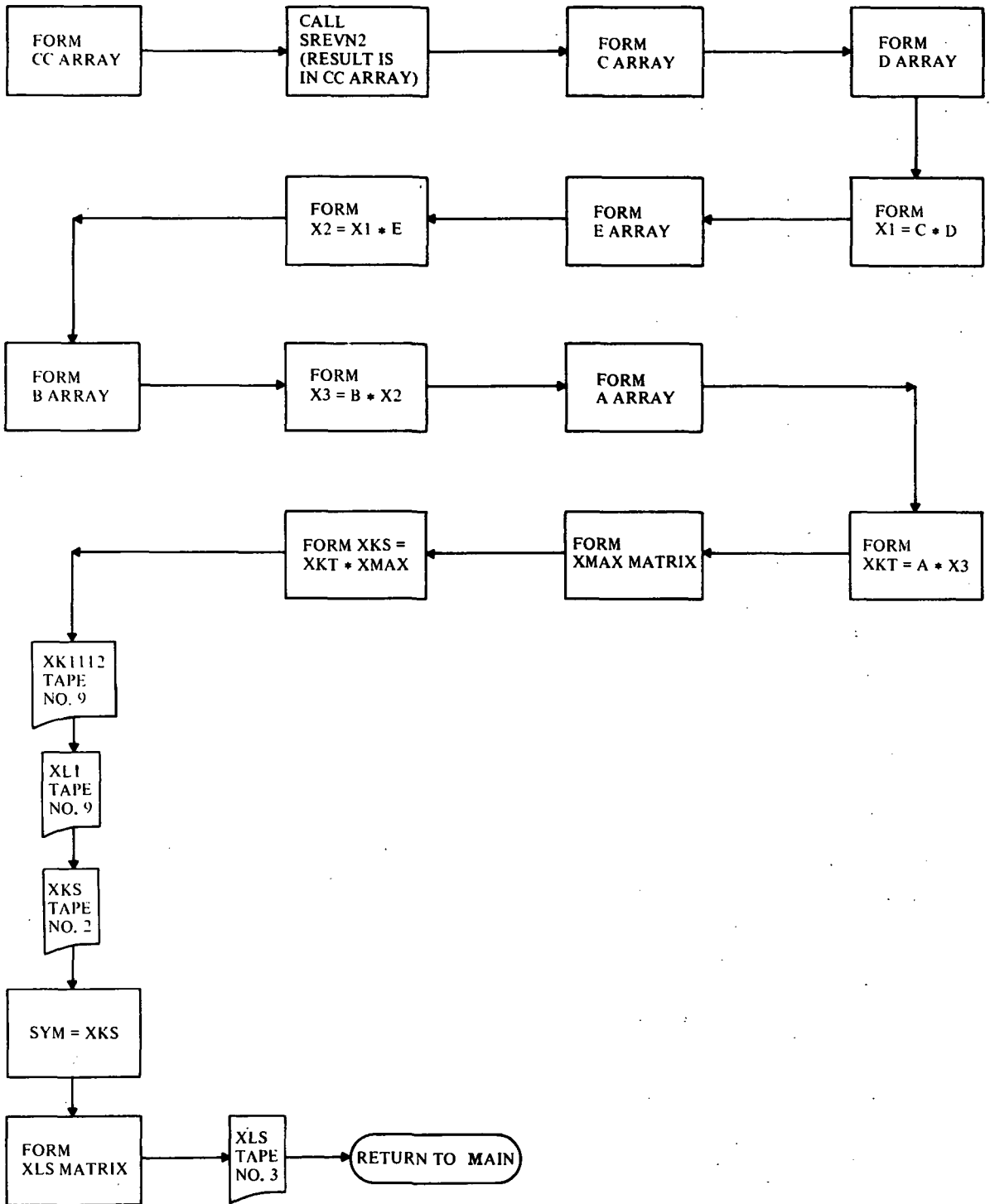
XKS MATRIX

$$s \begin{bmatrix} \hat{k} \\ \end{bmatrix} (n)$$

XLS MATRIX

$$s \begin{bmatrix} \hat{\ell} \\ \end{bmatrix} (n)$$

SEGMAT



```

FOR, IS SEGMA, SEGMA
SUBROUTINE SEGMA
INTEGER SAVJTC, SAVSTP, Q, THICK
INTEGER XN1, XN
DOUBLE PRECISION CC, ALABEL
COMMON STORY(16), XMAT(270, 10), STD(10), SADUS(30), RADUS(30)
COMMON TADUS(30), UADUS(30), SAVTIC(900)
COMMON XN, TEFREE, TIC, PHI, STOP, RESTOP, RTICK, G1, XNL(3), NH
COMMON NST(30), NKL(30), NXMAT(20), SAVJTC(30), SAVSTP(30), JRTIC(30)
COMMON JRSTOP(30), NREG, NMPT, NRC, NSC, NIX, IERROR, KGEOM, IGEOM, ISTTAB
COMMON KELVIN, IBEGIN, NPROB, NSEG, NERROR, Q, THICK, NOJS, NLINKS, NLCASE
COMMON NTSKL, NZ, NBCT, LINPUT, NTRKL, NPASS, XN1, KBC, NRINGS
COMMON LODE, ICYCLE, LDISTL
COMMON /LYCORR/ YCORR(72)
DIMENSION C(9,9), CC(4,4), D(9,9), E(9,9), B(8,9), A(8,8)
DIMENSION X1(9,9), X2(9,9), X3(8,9), XKT(8,9), XMAX(8,9)
DIMENSION XKS(8,9), XLS(8,1), SYM(8,9)
DIMENSION DEAD(4)
DIMENSION ALABEL(8)
EQUIVALENCE (C(1), E(1), X3(1), XMAX(1), XLS(1))
EQUIVALENCE (X2(1), D(1), A(1), XKS(1)), (X1(1), B(1), XKT(1), SYM(1))
DATA ALABEL/8HFORCE T1, 8HFORCE Z1, 8HFORCE R1, 8HMOMENT 1,
1 8HFORCE T2, 8HFORCE Z2, 8HFORCE R2, 8HMOMENT 2/
IF (NH.EQ.0) WRITE(6, 1726)
1726 FORMAT(1H1)
A1=G1
GOTO (601, 602, 603), IGEOM
601 SNI = SIN(TIC)
SNJ = SIN(STOP)
CSI = COS(TIC)
CSJ = COS(STOP)
GOTO 1
602 SNI = COS(1.570796-A1)
CSI = SIN(1.570796-A1)
IF (A1.NE.0.0) GO TO 604
SNI = 0.0
CSI = 1.0
604 SNJ = SNI
CSJ = CSI
GOTO 1
603 SNI = 1.0
SNJ = 1.0
CSI = 0.0
CSJ = 0.0
1 JJ = 8+NPROB
DO 111 J=1, JJ
DO 111 I=1, JJ
111 C(I, J)=0.0
K=28
DO 112 J=1, 4
K=K+8
L=K
DO 112 I=1, 4
L=L+1
112 CC(I, J)=YCORR(L)
CALL SREVN2 (CC, 4, DEAD, 4, NIX)
IF (NIX.NE.0) GOTO 8120
J1=0
DO 113 J=5, 8
J1=J1+1

```

```

800010
800020
800030
800040
800050
800060
800070
800080
800090
800100
800110
800120
800130
800140
800150
800160
800170
800180
800190
800200
800210
800220
800230
800240
800250
800260
800270
800280
800290
800300
800310
800320
800330
800340
800350
800360
800370
800380
800390
800400
800410
800420
800430
800440
800450
800460
800470
800480
800490
800500
800510
800520
800530
800540
800550
800560
800570
800580
800590

```



II=0	800600
DO 113 I=5,8	800610
II=II+1	800620
113 C(I,J)=CC(II,J1)	800630
DO 114 IJ=1,4	800640
114 C(IJ,IJ)=1.0	800650
DO 115 IJ=9,JJ	800660
115 C(IJ,IJ)=1.0	800670
DO 116 J=1,JJ	800680
DO 116 I=1,JJ	800690
116 D(I,J)=0.0	800700
DO 117 IJ=1,4	800710
117 D(IJ,IJ)=1.0	800720
I=5	800730
D(I,I)=1.0	800740
D(I+1,I+1)=-SNJ	800750
D(I+2,I+2)=-SNJ	800760
D(I+3,I+3)=1.0	800770
D(I+1,I+2)=CSJ	800780
D(I+2,I+1)=-CSJ	800790
DO 218 IJ=9,JJ	800800
218 D(IJ,IJ)=1.0	800810
K=-4	800820
DO 118 J=1,4	800830
K=K+8	800840
L=K	800850
DO 118 I=5,8	800860
L=L+1	800870
118 D(I,J)= -YCORR(L)	800880
K=60	800890
DO 119 J=9,JJ	800900
K=K+8	800910
L=K	800920
DO 119 I=5,8	800930
L=L+1	800940
119 D(I,J)=-YCORR(L)	800950
DO 120 J=1,JJ	800960
DO 120 I=1,JJ	800970
X1(I,J)=0.0	800980
DO 120 M=1,JJ	800990
120 X1(I,J)=X1(I,J)+C(I,M)*D(M,J)	801000
DO 121 J=1,JJ	801010
DO 121 I=1,JJ	801020
121 E(I,J)=0.0	801030
I=1	801040
E(I,I)=1.0	801050
E(I+1,I+1)=-SNI	801060
E(I+2,I+2)=-SNI	801070
E(I+3,I+3)=1.0	801080
E(I+1,I+2)=CSI	801090
E(I+2,I+1)=-CSI	801100
DO 122 J=5,JJ	801110
122 E(J,J)=1.0	801120
DO 123 J=1,JJ	801130
DO 123 I=1,JJ	801140
X2(I,J)=0.0	801150
DO 123 M=1,JJ	801160
123 X2(I,J)=X2(I,J)+X1(I,M)*E(M,J)	801170
DO 124 J=1,JJ	801180
DO 124 I=1,8	801190
124 B(I,J)=0.0	801200

J=4	801210
DO 125 I=1,4	801220
J = J+1	
125 B(I,J) = 1.0	
K = -8	
DO 126 J=1,4	
K = K+8	
L = K	
DO 126 I=5,8	801290
L=L+1	801300
126 B(I,J)=YCORR(L)	801310
K = 24	801320
DO 127 J=5,8	801330
K=K+8	801340
L=K	801350
DO 127 I=5,8	801360
L=L+1	801370
127 B(I,J)=YCORR(L)	801380
K=56	801390
DO 128 J=9,JJ	801400
K=K+8	801410
L=K	801420
DO 128 I=5,8	801430
L=L+1	801440
128 B(I,J)=YCORR(L)	801450
DO 129 J=1,JJ	801460
DO 129 I=1,8	801470
X3(I,J)=0.0	801480
DO 129 M=1,JJ	801490
129 X3(I,J)=X3(I,J)+B(I,M)*X2(M,J)	801500
DO 130 J=1,8	801510
DO 130 I=1,8	801520
130 A(I,J)=0.0	801530
I=1	801540
A(I,I)=-1.0	801550
A(I+1,I+1)=SNI	801560
A(I+2,I+2)=SNI	801570
A(I+1,I+2)=CSI	801580
A(I+2,I+1)=-CSI	801590
A(I+3,I+3)=1.0	801600
I=5	801610
A(I,I)=1.0	801620
A(I+1,I+1)=-SNJ	801630
A(I+2,I+2)=-SNJ	801640
A(I+3,I+3)=-1.0	801650
A(I+1,I+2)=-CSJ	801660
A(I+2,I+1)=CSJ	801670
DO 131 J=1,JJ	801680
DO 131 I=1,8	801690
XKT(I,J)=0.0	801700
DO 131 M=1,8	801710
131 XKT(I,J)=XKT(I,J)+A(I,M)*X3(M,J)	801720
PI=3.1415927	801730
RI=RTICK	801740
X2PIRI=2.0*PI*RI	801750
RJ=RESTOP	801760
X2PIRJ=2.0*PI*RJ	801770
DO 132 J=1,8	801780
DO 132 I=1,8	801790
132 XMAX(I,J)=0.0	801800
DO 133 I=1,4	801810

133	XMAX(I,I)=X2PIRI	801820
	DO 134 J=5,8	801830
134	XMAX(J,J)=X2PIRJ	801840
	DO 135 J=1,JJ	801850
	DO 135 I=1,8	801860
	XKS(I,J)=0.0	801870
	DO 135 M=1,8	801880
135	XKS(I,J)=XKS(I,J)+XMAX(I,M)*XKT(M,J)	801890
	WRITE(9) ((XKT(I,J),J=1,8),I=1,4),IGEOM,G1	801900
	WRITE(9) ((XKT(I,J),J=9,JJ),I=1,4)	801910
	IF (NH.NE.0.AND.IBEGIN.NE.1) GO TO 25	801920
	WRITE(6,781)	801930
781	FORMAT(/55X,22HSTIFFNESS COEFFICIENTS//14X,8HDELTA T1,7X,	801940
	1 8HDELTA Z1,7X,8HDELTA R1,7X,7HTHETA 1,8X,8HDELTA T2,7X,8HDELTA Z2	801950
	2 ,7X,8HDELTA R2,7X,7HTHETA 2)	801960
	III=0	801970
	DO 20 M=1,8	801980
	WRITE(6,23) ALABEL(M),(XKS(M,J),J=1,8)	801990
23	FORMAT(/1X,A8,1X,8(E14.7,1X))	802000
20	CONTINUE	802010
9968	FORMAT(1H ,8(E14.7,2X)/(5X,8(E14.7,2X)))	802020
25	CONTINUE	802030
	J1=8	802040
	ISEG=0	802050
	NRC1=NRC-1	802060
	IF(NRC1.EQ.0)GOTO 143	802070
	DO 244 I=1,NRC1	802080
244	ISEG=ISEG+NST(I)	802090
143	ISEG=ISEG+NSC	802100
	SAVTIC(ISEG)=TIC	802110
	WRITE(2) ((XKS(I,J),J=1,8),I=1,8)	802120
	DO 137 J=1,8	802130
	DO 137 I=1,8	802140
137	SYM(I,J)=0.0	802150
	INDEC=0	802160
	DO 138 I=1,8	802170
	DO 138 J=1,8	802180
	IF(J.NE.I)GO TO 138	802190
	IF(XKS(I,J).GE.0.0)GO TO 138	802200
	INDEC=1	802210
138	SYM(I,J)=XKS(I,J)	802220
	IF(INDEC.EQ.0)GO TO 151	802230
	WRITE(6,152)	802240
152	FORMAT(////' ***** WARNING - NEGATI	802250
	IVES APPEAR ON MAIN DIAGONAL. REVISE SIZING *****'//)	802260
151	JJ=2	802270
	N = 8	802280
	J = 1	802290
	DO 42 II=1,7	802300
	M = JJ	802310
	DO 43 I=M,N	802320
	ALPH = ABS(SYM(I,J)) - ABS(SYM(J,I))	802330
	IF(ALPH) 47,71,48	802340
47	IF(SYM(I,J).EQ.0.0) GOTO 71	802350
	SYM(I,J) = SYM(J,I) / SYM(I,J)	802360
	GOTO 43	802370
48	IF(SYM(J,I).EQ.0.0) GOTO 71	802380
	SYM(I,J) = SYM(I,J) / SYM(J,I)	802390
	GOTO 43	802400
71	SYM(I,J) = 1.0	802410
43	SYM(J,I) = 0.0	802420

JJ = JJ +1	802430
J = J+1	802440
42 CONTINUE	802450
IF (NH.NE.0.AND.IBEGIN.NE.1) GO TO 145	802460
WRITE(6,785)	802470
785 FORMAT(/55X,22HSEGMENT SYMMETRY CHECK,)	802480
DO 144 I=1,8	802490
144 WRITE(6,9968) (SYM(I,J),J=1,8)	802500
145 IF (NPROB.EQ.0) GO TO 9999	802510
DO 136 J=1,NPROB	802520
J1=J1+1	802530
DO 136 I=1,8	802540
136 XLS(I,J)=XKS(I,J1)	802550
WRITE(3)((XLS(I,J),J=1,NPROB),I=1,8)	802560
IF (NH.NE.0.AND.IBEGIN.NE.1) GO TO 9999	802570
WRITE(6,782)	802580
782 FORMAT(/55X,22HSEGMENT LOAD MATRICES ,)	802590
DO 840 I=1,8	802600
840 WRITE(6,9968)(XLS(I,J),J=1,NPROB)	802610
GOTO 9999	802620
8120 IERROR=8120	802630
NERROR=29	802640
8888 NIX=1	802650
9999 CONTINUE	802660
IF (NH.EQ.0.OR.IBEGIN.EQ.1) WRITE(6,795) RTICK,RESTOP	802670
795 FORMAT(/' RZERO(I) =',1PE15.6,10X,'RZERO(J) =',1PE15.6)	802680
RETURN	802690
END	802700

FOR, IS SREVN2, SREVN2	900010
SUBROUTINE SREVN2(A, M, LOC, MID, NIX)	900020
DOUBLE PRECISION A(MID, 1), PIVOT, TEMP1	900030
INTEGER LOC(1)	900040
100 N = M	900050
DO 190 K = 1, N	900060
PIVOT = 0.00	900070
DO 120 I = K, N	900080
IF (PIVOT - DABS(A(I, K))) 110, 110, 120	900090
110 PIVOT = DABS(A(I, K))	900100
L = I	900110
120 CONTINUE	900120
IF (PIVOT) 140, 130, 140	900130
130 NIX = -1	900140
GO TO 210	900150
140 LOC(K) = L	900160
DO 150 J = 1, N	900170
TEMP1 = A(K, J)	900180
A(K, J) = A(L, J)	900190
150 A(L, J) = TEMP1	900200
TEMP1 = A(K, K)	900210
A(K, K) = 1.00	900220
DO 160 J = 1, N	900230
160 A(K, J) = A(K, J) / TEMP1	900240
DO 190 I = 1, N	900250
IF (I - K) 170, 190, 170	900260
170 TEMP1 = -A(I, K)	900270
A(I, K) = 0.00	900280
DO 180 J = 1, N	900290
180 A(I, J) = A(I, J) + TEMP1 * A(K, J)	900300
190 CONTINUE	900310
DO 200 K = 1, N	900320
NK = N - K	900330
L = LOC(NK + 1)	900340
DO 200 I = 1, N	900350
TEMP1 = A(I, NK + 1)	900360
A(I, NK + 1) = A(I, L)	900370
200 A(I, L) = TEMP1	900380
NIX = 0	900390
210 RETURN	900400
END	

## SUBROUTINE REGMAT

The segment stiffness matrices, XKS, and the segment load matrices, XLS, are passed from SEGMAT to REGMAT via Tapes #2 and #3, and are placed in the XKRTOT array and the XLRTOT array, respectively. If kinematic links occur between segments in the region, the XKRTOT array and the XLRTOT array are modified to represent the situation. In the case of discrete rings the routine RINGER is called and provides the necessary matrices.

A horizontal and vertical partitioning of the XKRTOT array occurs while the XLRTOT array is subjected to a horizontal partitioning only. Appropriate matrix operations are performed upon the partitions of each array, thus reducing the size of the region stiffness and load matrices and resulting in increased program capacity. The results of these manipulations are the region stiffness matrix, XKR, and the region load matrix, XLR.

### Subroutines Called from REGMAT

Subroutine SYMSOC: Is the controlling routine for the solution of sparse, band-like, positive-definite, symmetric coefficient matrices.

Subroutine BANDIT: Is a routine called from SYMSOC which compacts a matrix into the special vector form required.

Subroutine LLTRAN: Is a routine called by SYMSOC for Cholesky factorization of sparse, band-like coefficient matrices.

Subroutine HOTDOT: (Alternate entry points PREFCE and FOREWD.) Is a small subroutine used repeatedly for efficiency in computing inner products.

Subroutine TRISLV: (Alternate entry point TRISOL.) Is a routine called by SYMSOC to carry out the solutions of sparse, bank-like, triangular coefficient matrices.

FORTTRAN CODE

ENGINEERING SYMBOLS (REF. 1)

SKL MATRIX

$$[SKL]$$

SKLTR MATRIX

$$[SKL]^T$$

XKRTOT MATRIX

$$\begin{bmatrix} K'_{11} & K'_{-12} \\ K'_{21} & K'_{22} \end{bmatrix}$$

XLRTOT MATRIX

$$\begin{bmatrix} L'_{iR1} \\ L'_{jR1} \\ L' \end{bmatrix}$$

SKL22 MATRIX

$$[SKL_{22}]$$

REGTOT MATRIX

$$\begin{bmatrix} K_{11} & K_{12} \\ K_{21} & K_{22} \end{bmatrix}$$

STORE MATRIX

$$\begin{bmatrix} L_{iR1} \\ L_{jR1} \\ L \end{bmatrix}$$

XK11 PARTITION

$$\left[ \overset{\wedge}{K}_{11} \right]$$

XK12 PARTITION

$$\left[ \overset{\wedge}{K}_{12} \right]$$

XK22 PARTITION

$$\left[ \overset{\wedge}{K}_{22} \right]$$

XK21 PARTITION

$$\left[ \overset{\wedge}{K}_{21} \right]$$

## FORTRAN CODE

## ENGINEERING SYMBOLS (REF. 1)

XL1 PARTITION

$$\left[ \begin{array}{c} \hat{L} \\ L_{R1} \end{array} \right]$$

XL2 PARTITION

$$\left[ \begin{array}{c} \hat{L} \\ L \end{array} \right]$$

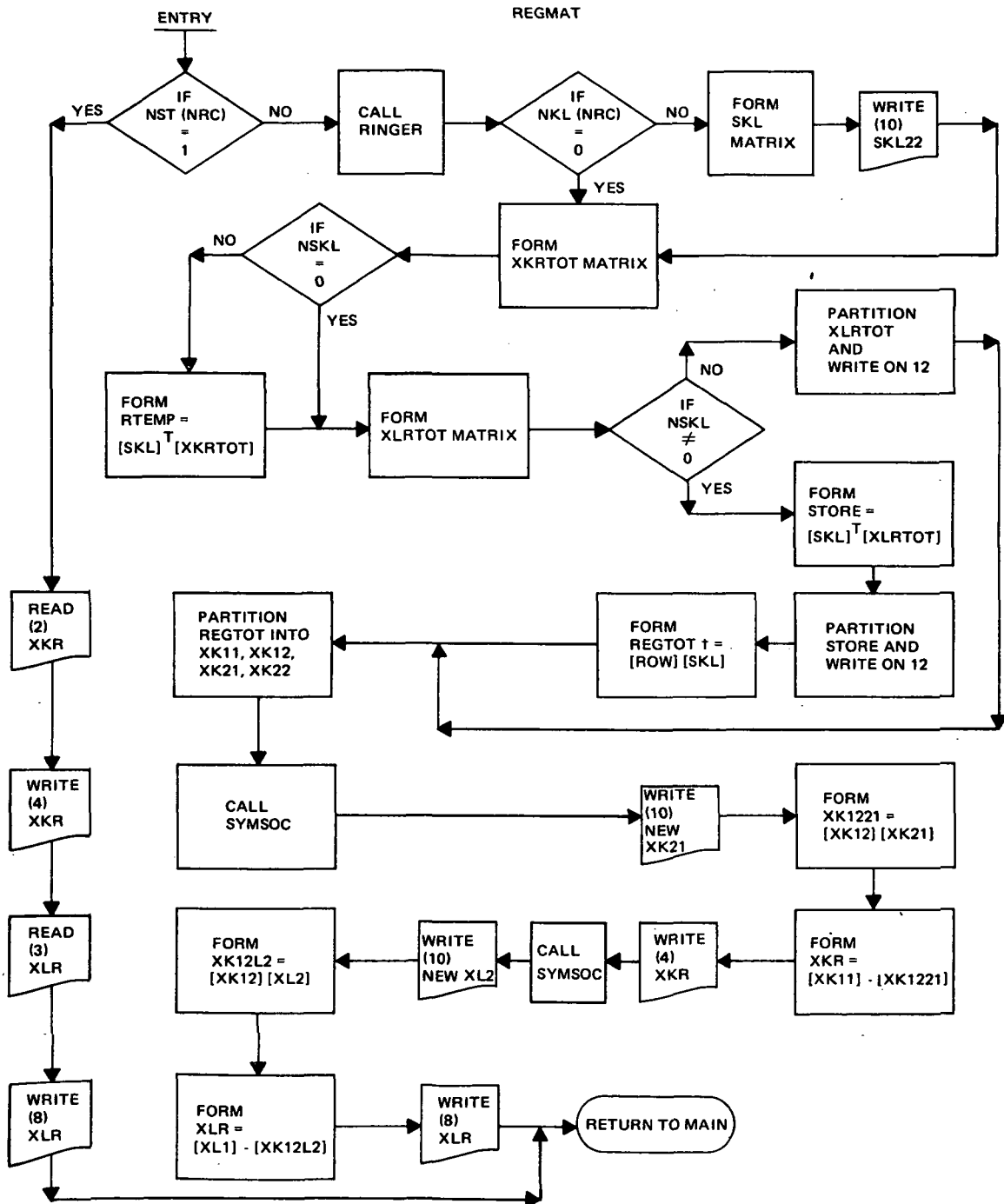
XKR MATRIX

$$\left[ \begin{array}{c} \hat{K} \\ K_R \end{array} \right]$$

XLR MATRIX

$$\left[ \begin{array}{c} \hat{L} \\ L_R \end{array} \right]$$





†NOTE: RTEMP = [ROW]

```

FOR, IS REGMAT, REGMAT
SUBROUTINE REGMAT
INTEGER SAVJTC, SAVSTP, Q, THICK
INTEGER XN1, XN
DOUBLE PRECISION ALABEL
COMMON STORY(16), XMAT(270, 10), STD(10), SADUS(30), RADUS(30)
COMMON TADUS(30), UADUS(30), SAVTIC(900)
COMMON XN, TEFREE, TIC, PHI, STOP, RESTOP, RTICK, G1, XNL(3), NH
COMMON NST(30), NKL(30), NXMAT(20), SAVJTC(30), SAVSTP(30), JRTIC(30)
COMMON JRSTOP(30), NREG, NMPT, NRC, NSC, NIX, IERROR, KGEOM, IGEOM, ISTTAB
COMMON KELVIN, IBEGIN, NPROB, NSEG, NERROR, Q, THICK, NOJS, NLINKS, NLCASE
COMMON NTSKL, NZ, NBCT, LINPUT, NTRKL, NPASS, XN1, KBC, NRINGS
COMMON LODE, ICYCLE, LDISTL
COMMON /OPT2/ PRINT
COMMON /ARING/ NRING(28), AMAT(30, 8), RSIG(12), REPS(12), RALPH(12),
C RBAPH(12)
COMMON /PLSTIC/ IO, JO, IOR, JOR, KORI, NEO
DIMENSION OPEN(4, 4)
DIMENSION XTEMP(8, 8), SKL(120, 120), SKLTR(120)
DIMENSION SYM(8, 8)
DIMENSION XKRTOT(120, 120), RTEMP(120), XLRTOT(120, 2), XKEEP(8, 2)
DIMENSION STORE(120, 2), ROW(120), REGTOT(120), HOLD(4, 120)
DIMENSION XK22(112, 112), XK11(8, 8), XK12(8, 112), XK21(112, 8)
DIMENSION XK1221(8, 8), XKR(8, 8), LEAD(8)
DIMENSION XL1(8, 1), XL2(112, 1), XK12L2(8, 1), XLR(8, 1)
DIMENSION JDEP(112), JIND(15), ANGLE(15)
DIMENSION RNGTOT(4, 4), RNLGLOD(4, 28), JTNO(28)
DIMENSION ALABEL(8)
EQUIVALENCE (SYM(1), XK12L2(1), XK1221(1), HOLD(1), JDEP(1))
EQUIVALENCE (SKL(1), XKRTOT(1), XK22(1), XLRTOT(1))
EQUIVALENCE (XKR(1), XK11(1), XTEMP(1), XLR(1), XL1(1), XKEEP(1),
1 RTEMP(1), ROW(1))
EQUIVALENCE (SKLTR(1), REGTOT(1), OPEN(1), XK12(1))
EQUIVALENCE (STORE(1), XL2(1), XK21(1))
DATA ALABEL/8HFORCE T1, 8HFORCE Z1, 8HFORCE R1, 8HMOMENT 1,
1 8HFORCE T2, 8HFORCE Z2, 8HFORCE R2, 8HMOMENT 2/
REWIND 2
REWIND 3
D = 0.0
PRINT = 0.0
NOJ = NST(NRC) + NKL(NRC) + 1
NOJ4 = NOJ*4
NSKL = NKL(NRC)
NH4=4
NJTNH4=NH4*NOJ
NJINK4 = (NOJ-NSKL)*4
M8=NJINK4-8
NKIV = NJINK4 - 8
IF (NST(NRC).EQ.1) GOTO 1
REWIND JO
IF (NH.NE.0.AND.IBEGIN.NE.1) GO TO 690
WRITE(6, 1726)
1726 FORMAT(1H1)
WRITE(6, 681) NRC, NOJ, NSKL
681 FORMAT(////51X31HINPUT DATA FOR SEGMENT COUPLING///25X14HREGION NU
1MBER ,12,5X25HNUMBER OF SEGMENT JOINTS ,13,5X,26HNUMBER OF KINEMAT
2IC LINKS ,13//)
WRITE(6, 682)
682 FORMAT(41X,7HSEGMENT,11X,8HJOINT(I),11X,8HJOINT(J)//)
DO 683 I=1,NSEG
100010
100020
100030
100040
100050
100060
100070
100080
100090
100100
100110
100120
100130
100140
100150
100160
100170
100180
100190
100200
100210
100220
100230
100240
100250
100260
100270
100280
100290
100300
100310
100320
100330
100340
100350
100360
100370
100380
100390
100400
100410
100420
100430
100440
100450
100460
100470
100480
100490
100500
100510
100520
100530
100540
100550
100560
100570
100580
100590

```

KTIC = SAVJTC(I)	1000600
KSTOP= SAVSTP(I)	1000610
WRITE(6,684) I,KTIC,KSTOP	1000620
684 FORMAT(43X,2(13,16X),I3)	1000630
683 CONTINUE	1000640
690 CONTINUE	1000650
NNT = NST(NRC)	1000660
DO 350 I=1,NOJ4	1000670
DO 350 J=1,NOJ4	1000680
350 XKRTOT(I,J)=0.0	1000690
591 FORMAT (3I5,16A4)	1000700
DO 701 NS=1,NNT	1000710
READ(2) ((XTEMP(I,J),J=1,8),I=1,8)	1000720
J1 = SAVJTC(NS)	1000730
J2 = SAVSTP(NS)	1000740
II = 4*(J1-1)	1000750
L = II	1000760
IF (J1.GT.J2) GOTO 950	1000770
DO 910 I = 1,8	1000780
JJ = L	1000790
II = II + 1	1000800
DO 910 J = 1,8	1000810
JJ = JJ + 1	1000820
910 XKRTOT(II,JJ)=XKRTOT(II,JJ)+XTEMP(I,J)	1000830
GOTO 701	1000840
950 JJ = 4*(J2-1)+1	1000850
II = II + 1	1000860
DO 960 JK = 1,4	1000870
GOTO (951,952,953,954) , JK	1000880
951 IX = II	1000890
IND = II	1000900
DO 961 I=1,4	1000910
DO 961 J=1,4	1000920
961 OPEN(I,J) = XTEMP(I,J)	1000930
GOTO 955	1000940
952 IX = II	1000950
IND = JJ	1000960
DO 962 I=1,4	1000970
DO 962 J=1,4	1000980
962 OPEN(I,J) = XTEMP(I,J+4)	1000990
GOTO 955	1001000
953 IX = JJ	1001010
IND = II	1001020
DO 963 I=1,4	1001030
DO 963 J=1,4	1001040
963 OPEN(I,J) = XTEMP(I+4,J)	1001050
GOTO 955	1001060
954 IX = JJ	1001070
IND = JJ	1001080
DO 964 I=1,4	1001090
DO 964 J=1,4	1001100
964 OPEN(I,J) = XTEMP(I+4,J+4)	1001110
955 DO 956 I=1,4	1001120
JX = IND	1001130
DO 957 J=1,4	1001140
XKRTOT(IX,JX) = XKRTOT(IX,JX) + OPEN(I,J)	1001150
957 JX = JX + 1	1001160
956 IX = IX + 1	1001170
960 CONTINUE	1001180
701 CONTINUE	1001190
NRNG = NRING(NRC)	1001200

	IF (NRING(NRC).EQ.0) GO TO 210	1001210
	IF (Q.EQ.5) WRITE(6,300)	1001220
300	FORMAT(///)	1001230
	MFLG = 1	1001240
	DO 211 J=1,NRNG	1001250
	CALL RINGER (Q,XN,RNGTOT,RNGLOD,J,RADUS,TADUS,SAVJTC,SAVSTP,JTNO,	1001260
1	KBC,XNL,MFLG,NSEG,ICYCLE,IBEGIN,LOISTL)	1001270
	JT = 4*(JTNO(J)-1)	1001280
	DO 220 I=1,4	1001290
	DO 220 IK=1,4	1001300
220	XKRTOT(JT+I,JT+IK) = XKRTOT(JT+I,JT+IK)+RNGTOT(I,IK)	1001310
211	CONTINUE	1001320
	IF (Q.NE.5) GO TO 210	1001330
	WRITE(6,300)	1001340
	READ(5,2000)	1001350
210	CONTINUE	1001360
	REWIND 2	1001370
	IF(NSKL.NE.0) GO TO 931	1001380
	DO 5504 I=1,NOJ4	1001390
	WRITE(2) (XKRTOT(I,J),J=1,NOJ4)	1001400
5504	CONTINUE	1001410
	GO TO 101	1001420
931	CONTINUE	1001430
	WRITE(JD) ((XKRTOT(I,J),J=1,NOJ4),I=1,NOJ4)	1001440
	REWIND JO	1001450
	DO 501 J=1,NJTNH4	1001460
	DO 501 I=1,NJTNH4	1001470
501	SKL(I,J)=0.0	1001480
	IF (NH.EQ.0) WRITE(6,685)	1001490
685	FORMAT(/60X13HSEGMENT LINKS//43X8HJOINT(J)5X8HJOINT(I)5X20HANGLE	1001500
	10F ORIENTATION//)	1001510
	DO 103 NRIG = 1,NSKL	1001520
	IF (Q.EQ.1) GO TO 566	1001530
	READ(5,503) JDEP(NRIG),JIND(NRIG),ANGLE(NRIG)	1001540
503	FORMAT (2I2,E14.7,15A4)	1001550
	WRITE(1) JDEP(NRIG),JIND(NRIG),ANGLE(NRIG)	1001560
	WRITE(6,686) JDEP(NRIG),JIND(NRIG),ANGLE(NRIG)	1001570
686	FORMAT(45X,I3,10X,I3,11X,E14.7)	1001580
	IF(JIND(NRIG).GE.JDEP(NRIG)) GO TO 8797	1001590
	GO TO 103	1001600
566	READ(1) JDEP(NRIG),JIND(NRIG),ANGLE(NRIG)	1001610
103	CONTINUE	1001620
	IF (Q.EQ.5) READ(5,2000)	1001630
2000	FORMAT(1X)	1001640
	J = -3	1001650
	N = 1	1001660
	DO 100 IJ = 1,NOJ	1001670
	I = 4*IJ-3	1001680
	IF(IJ.EQ.JDEP(N)) GOTO 11	1001690
	J = J + 4	1001700
	GOTO 12	1001710
11	JD = JDEP(N)	1001720
	JI = JIND(N)	1001730
	IF(N.LT.NRIG) N=N+1	1001740
	IF (SIN(ANGLE(N)).NE.0.0) GO TO 1829	1001750
	SKL(I,J) = 1.0	1001760
	SKL(I+1,J+3) = 0.0	1001770
	SKL(I+2,J+3) = 0.0	1001780
	GO TO 13	1001790
1829	CONTINUE	1001800
	COTAN = COS(ANGLE(N))/SIN(ANGLE(N))	1001810

SKL( I, J) = RADUS(JD)/RADUS(JI)	1001820
SKL(I+1,J+3) = -(RADUS(JD)-RADUS(JI))	1001830
SKL(I+2,J+3) = -SKL(I+1,J+3)*COTAN	1001840
GOTO 13	1001850
12 SKL( I, J) = 1.0	1001860
13 SKL(I+1,J+1) = 1.0	1001870
SKL(I+2,J+2) = 1.0	1001880
SKL(I+3,J+3) = 1.0	1001890
100 CONTINUE	1001900
5000 FORMAT(1H ,8(E14.7,2X)/(5X,8(E14.7,2X)))	1001910
II = NOJ4 - 4	1001920
JJ = NJINK4 - 4	1001930
WRITE(10) ((SKL(I,J),J=5,JJ),I=5,II)	1001940
DO 702 J=1,NJINK4	1001950
702 WRITE(2) (SKL(I,J),I=1,NOJ4)	1001960
WRITE(2) ((SKL(I,J),J=1,NJINK4),I=1,NOJ4)	1001970
REWIND 2	1001980
READ(JD) ((XKRTOT(I,J),J=1,NOJ4),I=1,NOJ4)	1001990
REWIND JO	1002000
1000 CONTINUE	1002010
DO 740 I=1,NJINK4	1002020
READ(2) (SKLTR(J),J=1,NOJ4)	1002030
DO 741 J=1,NOJ4	1002040
RTEMP (J)=0.0	1002050
DO 741 K=1,NOJ4	1002060
741 RTEMP (J)=RTEMP (J)+SKLTR(K)*XKRTOT(K,J)	1002070
WRITE(JO) (RTEMP(J),J=1,NOJ4)	1002080
740 CONTINUE	1002090
REWIND JO	1002100
101 IF (NPROB.EQ.0) GO TO 1001	1002110
REWIND 2	1002120
DO 436 I=1,NOJ4	1002130
DO 436 J=1,NPROB	1002140
436 XLRTOT(I,J)=0.0	1002150
DO 971 NS = 1,NNT	1002160
JTIC = SAVJTC(NS)	1002170
JSTOP= SAVSTP(NS)	1002180
READ (3) ((XKEEP(I,J),J=1,NPROB),I=1,8)	1002190
DO 971 N =1,2	1002200
GOTO (981,982),N	1002210
981 II = (JTIC-1)*4 + 1	1002220
III= II + 3	1002230
GOTO 983	1002240
982 II = (JSTOP-1)*4 +1	1002250
III= II + 3	1002260
983 DO 971 J=1,NPROB	1002270
I = 0	1002280
IF (N.EQ.2) I=4	1002290
DO 971 IL = II,III	1002300
I = I + 1	1002310
971 XLRTOT(IL,J) = XLRTOT(IL,J)+ XKEEP(I,J)	1002320
IF (NRNG.EQ.0) GO TO 230	1002330
DO 225 J=1,NRNG	1002340
JT = 4*(JTNO(J)-1)	1002350
DO 227 I=1,4	1002360
DO 226 IK=1,NPROB	1002370
226 XLRTOT(JT+I,IK) = XLRTOT(JT+I,IK)+RNGLOD(I,J)	1002380
227 CONTINUE	1002390
225 CONTINUE	1002400
230 CONTINUE	1002410
REWIND 3	1002420

IF (NSKL.NE.0) GOTO 147	1002430
DO 119 I=1,4	1002440
119 WRITE(3) (XLRTOT(I,J),J=1,NPROB)	1002450
M3=NJINK4-3	1002460
DO 118 I=M3,NJINK4	1002470
118 WRITE(3) (XLRTOT(I,J),J=1,NPROB)	1002480
M4=NJINK4-4	1002490
DO 117 I=5,M4	1002500
117 WRITE(3) (XLRTOT(I,J),J=1,NPROB)	1002510
REWIND 3	1002520
GOTO 102	1002530
147 DO 747 I=1,NJINK4	1002540
READ(2) (SKLTR(J),J=1,NOJ4)	1002550
DO 748 J=1,NPROB	1002560
STORE(I,J)=0.0	1002570
DO 748 K=1,NOJ4	1002580
748 STORE(I,J)=STORE(I,J)+SKLTR(K)*XLRTOT(K,J)	1002590
747 CONTINUE	1002600
DO 919 I=1,4	1002610
919 WRITE(3) (STORE(I,J),J=1,NPROB)	1002620
M3=NJINK4-3	1002630
DO 918 I=M3,NJINK4	1002640
918 WRITE(3) (STORE(I,J),J=1,NPROB)	1002650
M4=NJINK4-4	1002660
DO 917 I=5,M4	1002670
917 WRITE(3) (STORE(I,J),J=1,NPROB)	1002680
REWIND 3	1002690
1001 CONTINUE	1002700
IF (NSKL.EQ.0) GO TO 102	1002710
READ(2) ((SKL(I,J),J=1,NJINK4),I=1,NOJ4)	1002720
REWIND 2	1002730
DO 750 I=1,NJINK4	1002740
READ(JO) (ROW(J),J=1,NOJ4)	1002750
DO 751 J=1,NJINK4	1002760
REGTOT (J)=0.0	1002770
DO 751 K=1,NOJ4	1002780
751 REGTOT (J)=REGTOT (J) + ROW(K)*SKL(K,J)	1002790
750 WRITE(2) (REGTOT(J),J=1,NJINK4)	1002800
C THE 780 LOOP REARRANGES AND PARTITIONS THE REGION STIFFNESS MATRIX	1002810
102 NJINK = NJINK4/4	1002820
REWIND 2	1002830
DO 625 INK=1,8	1002840
DO 626 JAK=1,8	1002850
626 XK11(INK,JAK)=0.0	1002860
DO 625 KIX=1,M8	1002870
XK12(INK,KIX)=0.0	1002880
XK21(KIX,INK)=0.0	1002890
625 CONTINUE	1002900
DO 627 KIX=1,M8	1002910
DO 627 LAX=1,M8	1002920
627 XK22(KIX,LAX)=0.0	1002930
NREAD=0	1002940
KOUNT=-8	1002950
NJINK3=NJINK-1	1002960
DO 780 N=1,NJINK	1002970
NREAD=NREAD+1	1002980
KOUNT=KOUNT+4	1002990
DO 781 I=1,4	1003000
781 READ(2) (HOLD(I,J),J=1,NJINK4)	1003010
IF(NREAD.LE.2.OR.NREAD.GE.NJINK3)GO TO 790	1003020
KK=KOUNT+1	1003030

KKK=KOUNT+12	1003040
DO 785 L=KK,KKK	1003050
IROW=4*(NREAD-2)	1003060
J=L-4	1003070
DO 785 K=1,4	1003080
IROW=IROW+1	1003090
785 XK22(IROW,J)=HOLD(K,L)	1003100
GO TO 780	1003110
790 IF(NREAD.EQ.1)GO TO 791	1003120
IF(NREAD.EQ.2)GO TO 792	1003130
IF(NREAD.EQ.NJINK3)GO TO 793	1003140
IF(NREAD.EQ.NJINK)GO TO 794	1003150
791 DO 796 I=1,4	1003160
DO 796 J=1,4	1003170
XK11(I,J)=HOLD(I,J)	1003180
JJ=J+4	1003190
796 XK12(I,J)=HOLD(I,JJ)	1003200
GO TO 780	1003210
792 DO 797 I=1,4	1003220
DO 797 J=1,4	1003230
XK21(I,J)=HOLD(I,J)	1003240
JJ=J+4	1003250
XK22(I,J)=HOLD(I,JJ)	1003260
JJJ=J+8	1003270
IF(NNT.EQ.2) GO TO 795	1003280
XK22(I,JJ)=HOLD(I,JJJ)	1003290
GO TO 797	1003300
795 XK21(I,JJ)=HOLD(I,JJJ)	1003310
797 CONTINUE	1003320
GO TO 780	1003330
793 M11=NJINK4-11	1003340
M4=NJINK4-4	1003350
M8=NJINK4-8	1003360
KROW=M8-4	1003370
DO 798 I=1,4	1003380
KROW=KROW+1	1003390
KCOL=4	1003400
K8=M8-8	1003410
DO 798 J=M11,M8	1003420
K8=K8+1	1003430
XK22(KROW,K8)=HOLD(I,J)	1003440
JJ=J+4	1003450
KK=K8+4	1003460
XK22(KROW,KK) =HOLD(I,JJ)	1003470
JJJ=J+8	1003480
KCOL=KCOL+1	1003490
798 XK21(KROW,KCOL)=HOLD(I,JJJ)	1003500
GO TO 780	1003510
794 KEND=NJINK4-8	1003520
KROW=4	1003530
M4=NJINK4-4	1003540
M7=NJINK4-7	1003550
DO 799 I=1,4	1003560
KROW=KROW+1	1003570
K4=KEND-4	1003580
KCOL=4	1003590
DO 799 J=M7,M4	1003600
K4=K4+1	1003610
XK12(KROW,K4)=HOLD(I,J)	1003620
KCOL=KCOL+1	1003630
JJ=J+4	1003640

```

799 XK11(KROW,KCOL)=HOLD(I,JJ) 1003650
780 CONTINUE 1003660
7703 NSING=NKIV*(NKIV+1)/2 1003670
      N=NKIV 1003680
      IK=1 1003690
      DO 10 K=1,N 1003700
      DO 10 I=K,N 1003710
      XK22(I,K)=(XK22(I,K)+ XK22(K,I))/2. 1003720
10 CONTINUE 1003730
      DO 50 K=1,4 1003740
      LEAD(K) = 1 1003750
50 LEAD(K+4) = NJINK4-11 1003760
      CALL SYMSOC (XK22,XK22,N,0,XK21,8,LEAD,112,0.0,NIX) 1003770
      IF (NIX.LT.0) GOTO 8841 1003780
      WRITE (10) ((XK21(I,J),J=1,8),I=1,M8 ) 1003790
      WRITE ((10)(( SAVJTC(I), SAVSTP(I)),I=1,NNT) 1003800
      DO 81 J=1,8 1003810
      DO 81 I=1,8 1003820
      XK1221(I,J)=0.0 1003830
      DO 81 K=1,NKIV 1003840
81 XK1221(I,J)=XK1221(I,J)+XK12(I,K)*XK21(K,J) 1003850
      DO 82 J=1,8 1003860
      DO 82 I=1,8 1003870
82 XKR(I,J)=XK11(I,J)-XK1221(I,J) 1003880
      DO 650 J=1,7 1003890
      K = J+1 1003900
      DO 650 I=K,8 1003910
      XKR(I,J) = (XKR(I,J)+XKR(J,I))/2.0 1003920
650 XKR(J,I) = XKR(I,J) 1003930
      WRITE (4) ((XKR(I,J),J=1,8),I=1,8) 1003940
      IF (INH.NE.0.AND.IBEGIN.NE.1) GO TO 691 1003950
      WRITE(6,5011) 1003960
5011 FORMAT(////55X23HREGION STIFFNESS MATRIX//14X8HDELTA T17X8HDELTA Z 1003970
      11,7X,8HDELTA R1,7X,7HTHETA 1,8X,8HDELTA T2,7X,8HDELTA Z2,7X,8HDEL 1003980
      2A R2,7X,7HTHETA 2) 1003990
      III=0 1004000
      DO 687 M=1,8 1004010
      WRITE(6,688) ALABEL(M),(XKR(M,J),J=1,8) 1004020
688 FORMAT(/1X,A8,1X,8(E14.7,1X)) 1004030
687 CONTINUE 1004040
691 CONTINUE 1004050
      DO 137 J=1,8 1004060
      DO 137 I=1,8 1004070
137 SYM(I,J)=0.0 1004080
      INDEC=0 1004090
      DO 138 I=1,8 1004100
      DO 138 J=1,8 1004110
      IF(J.NE.I)GO TO 138 1004120
      IF(XKR(I,J).GE.0.0)GO TO 138 1004130
      INDEC=1 1004140
138 SYM(I,J)=XKR(I,J) 1004150
      IF(INDEC.EQ.0)GO TO 151 1004160
      WRITE(6,152) 1004170
152 FORMAT(////' ***** WARNING - NEGATI 1004180
      IVES APPEAR ON MAIN DIAGONAL. REVISE SIZING *****'//) 1004190
151 JJ=2 1004200
      N = 8 1004210
      J = 1 1004220
      DO 42 II=1,7 1004230
      M = JJ 1004240
      DO 43 I=M,N 1004250

```



ALPH = ABS(SYM(I,J)) - ABS(SYM(J,I))	1004260
IF(ALPH) 47,71,48	1004270
47 IF(SYM(I,J).EQ.0.0) GOTO 71	1004280
SYM(I,J) = SYM(J,I) / SYM(I,J)	1004290
GOTO 43	1004300
48 IF(SYM(J,I).EQ.0.0) GOTO 71	1004310
SYM(I,J) = SYM(I,J) / SYM(J,I)	1004320
GOTO 43	1004330
71 SYM(I,J) = 1.0	1004340
43 SYM(J,I) = 0.0	1004350
JJ = JJ +1	1004360
J = J+1	1004370
42 CONTINUE	1004380
IF (NH.NE.0.AND.IBEGIN.NE.1) GO TO 692	1004390
WRITE(6,157)	1004400
157 FORMAT(/56X,21HREGION SYMMETRY CHECK/)	1004410
DO 1730 I=1,8	1004420
WRITE(6,5000) (SYM(I,J),J=1,8)	1004430
1730 CONTINUE	1004440
692 CONTINUE	1004450
IF (NPROB.EQ.0) GO TO 150	1004460
DO 819 I=1,4	1004470
819 READ(3) (XL1(I,J),J=1,NPROB)	1004480
DO 818 I=5,8	1004490
818 READ(3) (XL1(I,J),J=1,NPROB)	1004500
D = 0.0	1004510
M8 = NJINK4-8	1004520
DO 817 I=1,M8	1004530
817 READ(3) (XL2(I,J),J=1,NPROB)	1004540
LEAD(1) = 1	1004550
CALL SYMSOC (XK22,XK22,M8,0,XL2,-1,LEAD,112,0.0,NIX)	1004560
IF (NIX.LT.0) GOTO 8842	1004570
WRITE (10) ((XL2(I,J),J=1,NPROB),I=1,M8 )	1004580
NL2=NPROB	1004590
DO 205 J=1,NPROB	1004600
DO 205 I=1,8	1004610
XK12L2(I,J)=0.0	1004620
DO 205 K=1,NKIV	1004630
205 XK12L2(I,J)=XK12L2(I,J)+XK12(I,K)*XL2(K,J)	1004640
DO 206 J=1,NPROB	1004650
DO 206 I=1,8	1004660
206 XLR(I,J)=XL1(I,J)-XK12L2(I,J)	1004670
WRITE(8) ((XLR(I,J),J=1,NPROB),I=1,8)	1004680
IF (NH.NE.0.AND.IBEGIN.NE.1) GO TO 150	1004690
WRITE(6,5012)	1004700
5012 FORMAT(/57X,18HREGION LOAD MATRIX/)	1004710
DO 5512 I=1,8	1004720
5512 WRITE(6,5000) (XLR(I,J),J=1,NPROB)	1004730
GOTO 150	1004740
8841 IERROR=8841	1004750
NERROR=30	1004760
GOTO 150	1004770
8797 IERROR = 8797	1004780
NERROR=33	1004790
GO TO 150	1004800
8842 IERROR=8842	1004810
NERROR=31	1004820
GOTO 150	1004830
1 READ (2) ((XKR(I,J),J=1,8),I=1,8)	1004840
DO 651 J=1,7	1004850
K = J+1	1004860

```
DO 651 I=K,8
XKR(I,J) = (XKR(I,J)+XKR(J,I))/2.0
651 XKR(J,I) = XKR(I,J)
WRITE(4) ((XKR(I,J),J=1,8),I=1,8)
IF (NPROB.EQ.0) GO TO 150
READ(3) ((XLR(I,J),J=1,NPROB),I=1,8)
WRITE(8) ((XLR(I,J),J=1,NPROB),I=1,8)
150 RETURN
END
```

```
1004870
1004880
1004890
1004900
1004910
1004920
1004930
1004940
1004950
```

```

FOR, IS SYMSOC, SYMSOC
SUBROUTINE SYMSOC (XMAT, A, M, BAND, Y, N, LEAD, MID, DET, NIX) 1100010
C 1100020
C SOLUTION OF LINEAR EQUATIONS A*X = Y, WITH POSDEF SYM BANDLIKE A, AND 1100030
C IN-CORE Y. Y MAY BE A STANDARD DOUBLE ARRAY (ROW DIM MID) OR A COMP- 1100040
C ACT SINGLE ARRAY (WITH MID=0). IN EITHER CASE, LEAD(K) IS THE FIRST 1100050
C NON-ZERO ELEMENT OF THE KTH Y-VECTOR. IF MID GT 0, THE SOLUTIONS ARE 1100060
C STACKED OVER THE RIGHT SIDES. IF MID = 0, THE ROUTINE IS PRINT-ONLY. 1100070
C 1100080
C 1100090
C SYMSOC CAN BE RE-ENTERED WITH NEW RIGHT SIDES BY SETTING N LT 0. 1100100
C 1100110
DIMENSION A(1), Y(1), X(128), XMAT(MID, 1), NUMBER(128) 1100120
DIMENSION LEAD(1) 1100130
INTEGER BAND 1100140
NP = IABS(N) 1100150
IF (N .LT. 0) GO TO 100 1100160
MM = M*(M+1)/2 1100170
CALL BANDIT (XMAT, A, M, MID, NUMBER) 1100180
CALL LLTRAN(A, M, BAND, NUMBER, DET, NIX) 1100190
IF (MID .EQ. 0) WRITE (6,10) NIX, M, DET 1100200
10 FORMAT('8ERROR CODE ='14,5X,'M ='14,5X,'DETERMINANT ='1PE16.6) 1100210
100 IF (NIX .LT. 0) RETURN 1100220
NIX = 0 1100230
M1 = M + 1 1100240
IF (MID .EQ. 0) GO TO 110 1100250
INCL = MID + 1 - M 1100260
IM = M - MID 1100270
GO TO 120 1100280
110 WRITE (6,20) N 1100290
20 FORMAT('8SOLUTIONS'9X,'N ='15) 1100300
INCL = 1 1100310
IM = 0 1100320
120 CALL TRISLV(A, M, BAND, NUMBER, X, LEAP, 1) 1100330
DO 170 K = 1, NP 1100340
LEAP = LEAD(K) 1100350
DO 130 J = 1, LEAP 1100360
X(J) = 0. 1100370
130 CONTINUE 1100380
IL = IM + INCL 1100390
IF (MID.GT.0) IL = IL+LEAP-1 1100400
IM = MAX0(MID, M1-LEAP) + IM 1100410
J = LEAP 1100420
DO 140 IJ = IL, IM 1100430
X(IJ) = Y(IJ) 1100440
J = J + 1 1100450
140 CONTINUE 1100460
CALL TRISOL (X, LEAP) 1100480
IF (MID .EQ. 0) GO TO 160 1100490
J = M 1100500
IJ = IM 1100510
150 Y(IJ) = X(J) 1100520
IJ = IJ - 1 1100530
J = J - 1 1100540
IF (J).170,170,150 1100550
160 WRITE (6,30) K, (X(J), J = 1, M) 1100560
30 FORMAT('0'15,1P8E15.6/(6X,8E15.6)) 1100570
170 CONTINUE 1100580
RETURN 1100590
END

```

FOR, IS BANDIT, BANDIT	1200010
SUBROUTINE BANDIT (XMAT, A, N, MID, NUMBER)	1200020
DIMENSION XMAT(MID, 1), NUMBER(1), A(1)	1200030
K = 0	1200040
DO 10 J=1, N	1200050
DO 30 I=1, J	1200060
IF (XMAT(I, J).EQ.0.0) GO TO 30	1200070
DO 20 L=I, J	1200080
K = K+1	1200090
20 A(K) = XMAT(L, J)	1200100
NUMBER(J) = J-I+1	1200110
GO TO 10	1200120
30 CONTINUE	1200130
NUMBER(J) = 0	1200140
10 CONTINUE	1200150
RETURN	1200160
END	

```

FOR, IS LLTRAN, LLTRAN
SUBROUTINE LLTRAN(A, M, BAND, NUMBER, DET, NIX)
CHOLESKY DECOMPOSITION OF A REAL IN-CORE POSITIVE DEFINITE MATRIX A.
C ROUTINE ASSUMES A IS STORED IN A TRIANGULAR ARRAY BY ROWS. EACH ROW
C STARTS WITH ITS 1ST NON-ZERO ELEMENT AND CONTINUES (WITH STORAGE OF
C INTERIOR ZEROS) TO ITS DIAGONAL ELEMENT. FULL LOWER TRIANGLES AND
C DIAGONAL MATRICES GIVE NO SPECIAL TROUBLE AND THE ROUTINE IS AIMED
C PARTICULARLY AT BAND MATRICES. THE PATTERN OF STORAGE IS SHOWN BY
C THE 6X6 MATRIX BELOW.
C
C      X
C      X X
C      O X X      STORED IN THE ORDER
C      O X O X
C      O O O X X
C      O X O X O X
C
C      1
C      2 3
C      * 4 5
C      * 6 7 8
C      * * * 9 A
C      * B C D E F
C
C WHERE A THROUGH F DENOTE 10 THROUGH 15.
C
C TO KEEP TRACK OF ZEROS, THE ROUTINE NEEDS TO BE TOLD THE NUMBER OF
C ELEMENTS STORED IN EACH ROW. THIS INFORMATION CAN BE GIVEN EXPLICIT-
C LY IN THE ARRAY NUMBER (SETTING BAND = 0) OR IMPLICITLY BY SETTING
C BAND TO THE NUMBER OF (COMPLETE) DIAGONALS. WITH THE 2ND CHOICE, THE
C ARRAY NUMBER IS NOT USED. IF A IS NOT POSITIVE DEFINITE, SOME LEAD-
C ING PRINCIPAL MINOR WILL HAVE A DETERMINANT LE 0, AND NIX WILL BE
C SET TO -I WHERE I IS THE FIRST SUCH MINOR. OTHERWISE L REPLACES A
C NIX = 1 INDICATES SUCCESSFUL FACTORIZATION WITH DETERMINANT OVERFLOW
C NIX = 0 INDICATES SUCCESSFUL FACTORIZATION AND THE DETERMINANT VALUE
C IS MEANINGFUL UNLESS IT HAS BEEN WIPED OUT BY UNDERFLOW.
C
C DIMENSION A(1), NUMBER(1), S(2)
C EQUIVALENCE (SUM, SUN, S(1)), (SUM1, S(2))
C INTEGER BAND
C LEALEA = 0
C LEAD1 = 0
C IK = 0
C DD 260 I = 1, M
C IF (BAND) 110, 100, 110
100 KOUNT = NUMBER(I)
C GO TO 120
110 KOUNT = MINO(I, BAND)
120 LEAD = I - KOUNT + 1
C IF (LEAD - LEAD1) 130, 190, 140
130 LAST = LEAD1
C LEAD1 = LEAD + 1
C LEALEA = -LEALEA
C GO TO 150
140 LAST = LEAD
C LEAD1 = LEAD1 + 1
150 CONTINUE
C DD 180 J = LEAD1, LAST
C IF (BAND) 170, 160, 170
160 LEALEA = NUMBER(J) + LEALEA
C GO TO 180
170 LEALEA = MINO(BAND, J) + LEALEA
180 CONTINUE
190 LEALEA = IABS(LEALEA)
C KK = LEALEA
C
C LP = 0
C LO = 1
C CALL PREFCE (LP, LO, A(IK+1), A(LEALEA), SUN, LEAST, INC, INDEX, KEY)
C K = LEAD
200 IK = IK + 1

```

```

1300010
1300020
1300030
1300040
1300050
1300060
1300070
1300080
1300090
1300100
1300110
1300120
1300130
1300140
1300150
1300160
1300170
1300180
1300190
1300200
1300210
1300220
1300230
1300240
1300250
1300260
1300270
1300280
1300290
1300310
1300320
1300330
1300340
1300350
1300360
1300370
1300380
1300390
1300400
1300410
1300420
1300430
1300440
1300450
1300460
1300470
1300480
1300490
1300500
1300510
1300520
1300530
1300540
1300550
1300560
1300570
1300590
1300600

```

	SUM = -A(IK)	1300610
	SUM1 = 0.	1300620
	K = K + 1	1300630
	LEAST = MAXO(1,K-INC-LEAD)	1300640
	IF (BAND) 220,210,220	1300650
210	JAZZ = NUMBER(K)	1300660
	GO TO 230	1300670
220	JAZZ = MINO(BAND,K)	1300680
230	INC = JAZZ - 1	1300690
	CALL HOTDOT (SUM,LEAST,INC)	1300700
	IF (K - I) 240,240,250	1300710
240	A(IK) = -SUM / A(KK)	1300720
	KK = KK + JAZZ	1300730
	GO TO 200	1300740
250	SUM = -SUM	1300750
	IF (SUM .LE. 0) GO TO 280	1300760
	DET = DET * SUM	1300770
	A(IK) = SQRT(SUM)	1300780
	LEAD1 = LEAD	1300790
260	CONTINUE	1300800
	NIX = 0	1300810
270	RETURN	1300820
280	NIX = -I	1300830
	GO TO 270	1300840
	END	1300850

FOR,IS HOTDOT,HOTDOT	1500010
SUBROUTINE HOTDOT (S,LOW,JUMP)	1500020
GO TO 250	1500030
C	1500040
FORTRAN VERSION NEEDS JUMP POSITIVE FOR SAFETY.	1500050
C	
ENTRY PREFCE (LAST,INC,FIX,VARY,S,LOW,JUMP,INDEX,KEY)	1500090
DIMENSION FIX(1),VARY(1)	1500100
C	1500110
INDEX = 1	1500120
KEY = 0	1500130
GO TO 99	1500140
250 CONTINUE	1500150
IF (LOW-LAST) 50,50,120	1500160
50 IJ = INDEX+LOW-1	1500170
IF (KEY) 200,100,99	1500180
100 DO 110 J=LOW,LAST	1500190
S = S+VARY(IJ)*FIX(J)	1500200
110 IJ = IJ+1	1500210
120 INDEX = INDEX+JUMP	1500220
LAST = LAST+INC	1500230
GO TO 99	
200 T = S	
DO 210 J=LOW,LAST	
FIX(J) = FIX(J)+VARY(IJ)*T	1500250
210 IJ = IJ+1	1500260
GO TO 120	1500270
ENTRY FOREWD (LAST,INC,FIX,VARY,S,LOW,JUMP,INDEX,KEY)	
INDEX = 1	1500290
KEY = -1	1500300
99 RETURN	1500310
END	1500320

```

FOR,IS TRISLV,TRISLV
SUBROUTINE TRISLV(A,M,BAND,NUMBER,Y,LEAP,LOP)
C SOLUTION OF LZ = Y, FOLLOWED BY SOLUTION OF LTX = Z. L IS A LOWER      1400020
C . TRIANGULAR MATRIX STORED BY (PARTIAL) ROWS IN THE ARRAY A. L IS AS- 1400030
C SUMED BANDLIKE, BUT BAND = 0 MEANS THAT THE NUMBER ARRAY GIVES THE 1400040
C NUMBER OF ELEMENTS STORED IN EACH ROW. FOR STORAGE ORDER SEE LLTRAN. 1400050
DIMENSION A(1),Y(1),NUMBER(1),S(2)
EQUIVALENCE (SUM,SUN,S(1)),(SUM1,S(2))
INTEGER BAND
M1 = M + 1
MM1 = M - 1
RETURN
ENTRY TRISOL (Y,LEAP)
LOW = LOP
LEAD = LEAP
LEAD1 = LEAD + 1
II = 0
DO 130 I = 1,LEAD
IF (BAND) 120,110,120
110 JAZZ = NUMBER(I)
GO TO 130
120 JAZZ = MINO(I,BAND)
130 II = II + JAZZ
IGO = II - LEAD + 1
LP = LEAD-1
CALL PREFCE (LP,1,Y,A(IGO),SUN,LEAST,INC,INDEX,KEY)
DO 170 I = LEAD1,M1
LEAST = MAXO(LEAD,I-JAZZ)
IF(BAND) 150,140,150
140 JAZZ = NUMBER(I)
GO TO 160
150 JAZZ = MINO(BAND,I)
160 INC = JAZZ - 1
SUM = -Y(I-1)
SUM1 = 0.
CALL HOTDOT (SUN,LEAST,INC)
Y(I-1) = -SUM/A(II)
II = II + JAZZ
170 CONTINUE
II = II - JAZZ
IGO = II - MM1
CALL FOREWD (MM1,-1,Y,A(IGO),SUN,LEAST,INC,INDEX,KEY)
I = M
180 SUM = -Y(I) / A(II)
Y(I) = -SUM
IF(BAND) 200,190,200
190 JAZZ = NUMBER(I)
GO TO 210
200 JAZZ = MINO(I,BAND)
210 INC = 1 - JAZZ
LEAST = MAXO(LOW,I+INC)
CALL HOTDOT (SUN,LEAST,INC)
II = II - JAZZ
I = I - 1
IF (I .GE. LOW) GO TO 180
RETURN
END

```



## SUBROUTINE RINGER

This subroutine reads the discrete ring geometric data, and temperatures, and forms the ring stiffness and thermal load matrices. These matrices are passed back to either of subroutines REGMAT or STRMAT (see next) as necessary, for incorporation into the region or structure matrices, respectively. The ring plasticity effects are calculated and the stresses and strains updated for each load increment.

The calculations in RINGER account for the eccentricity of the ring centroid from the base shell wall, and the offset of the ring centroid from the shear center.

### Subroutines Called from RINGER

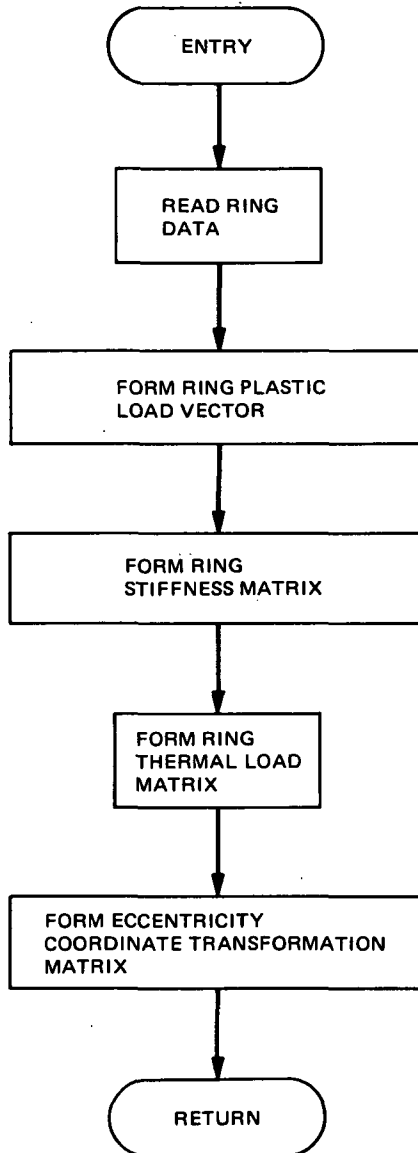
Subroutine RITEPS: Is a routine called by RINGER to calculate the thermal strains throughout the ring.

Subroutine RISULT: Is a routine called by RINGER to calculate ring stress resultants and moments.

Subroutine RGSRSE: Is a routine called by RINGER to calculate ring elastic stresses.

FORTRAN CODE	ENGINEERING SYMBOLS (REF. 1)
RNGTOT MATRIX	$\left[ k_R \right]$
TDEL MATRIX	$\left[ T_\Delta \right]$
RNGLOD MATRIX	$\left[ l_R \right]$
RC	$r_c$
RS	$r_s$
XC	$x_c$
YC	$y_c$

RINGER



e

```

FOR, IS RINGER, RINGER
SUBROUTINE RINGER (Q, XN, RNGTOT, RNLGLOD, J, ADUS, BADUS, JTIC, JSTOP,
1          JTNO, KBC, XNL, MFLG, NSEG, ICYCLE, IBEGIN, LDISTL)
INTEGER Q, XN
COMMON /ARING/ NRING(28), AMAT(30, 8), RSIG(12), REPS(12), RALPH(12),
C          RBAPH(12)
COMMON /PLS/ OMEGA, IWORD, XMERD, XPRES, XMONT
COMMON /PLSTIC/ IO, JO, IOR, JOR, KORI, NEO
COMMON /CDISP/ P, IMAX, DELP, DELP1, YEPS, ZEPS
DIMENSION RNGTOT(4, 4), RNLGLOD(4, 28), TDEL(4, 4), XKTOT(4, 4), XL(4)
DIMENSION ADUS(30), BADUS(30), JTIC(30), JSTOP(30), JTNO(28), XNL(3)
DIMENSION RNGSRN(2), RGSRS(3), NPLA(12), DSIG(12), DEPS(12)
DIMENSION RTEPS(12), TEPS(12), TEP SIN(3), ENTH(3), RGEOM(6), REPSIN(3)
DIMENSION AWORD(9), JIPR(9), REFF(12), HARD(3), SAVR(6)
EQUIVALENCE (TEPSIN(1), AMN), (TEPSIN(2), BN)
DATA AWORD /'SREC', 'ZSEC', 'ISEC', 'HREC', 'HTRI', 'CRRC', 'CHSC',
1          'TSEC', 'RASC'/
DATA HARD /'ISOT', 'KINE', 'PERF'/
DATA JIPR /9, 9, 9, 12, 9, 12, 9, 6, 6/
X1 = XNL(1)
X3 = XNL(3)
IF (Q.EQ.1) GO TO 212
READ(5, 213) JTNO(J), EA, E1Y, E1XY, E1X, E, WORD, PHI, SIGOX, RMOS, RMOSN,
1          ALPR, RC, XC, YC, XBAR, YBAR, TI, TO, ROJ, RHO, HARDEN, RGEOM
213 FORMAT(12, 5E14.7/A4, 2X, 4E14.7/6E12.5/4E14.7, 4X, A4/6E12.5)
DO 11 K=1, 9
IF (AWORD(K).EQ.WORD) GO TO 12
11 CONTINUE
12 NTP = K
NIPR = JIPR(NTP)
NPLEV = 0
DO 25 K=1, 3
IF (HARD(K).EQ.HARDEN) GO TO 26
25 CONTINUE
NERROR = 8013
GO TO 8888
26 KOR = K
KORIR = 0
IF (KOR.GT.1) KORIR = -1
IF (NEO.NE.0) GO TO 600
DO 20 K=1, 12
NPLA(K) = 0
RSIG(K) = 0.0
REPS(K) = 0.0
REFF(K) = SIGOX
RALPH(K) = 0.0
20 RBAPH(K) = 0.0
DO 21 K=1, 2
RNGSRN(K) = 0.0
REPSIN(K) = 0.0
21 RGSRS(K) = 0.0
RGSRS(3) = 0.0
REPSIN(3) = 0.0
C = 0.0
IPRINT = 0
D = 0.0
DELR = 0.0
DO 610 K=1, 6
610 SAVR(K) = 0.0
DO 240 K=1, 3

```

```

240 ENTH(K) = 0.0 2900600
CALL RITEPS (RTEPS, TI, TO, ALPR, NTYP, RGEOM) 2900610
IND = 0 2900620
CALL RISULT (TEPSIN, RTEPS, ENTH(3), NTYP, IND, RGEOM, PHI) 2900630
600 CONTINUE 2900640
WRITE(1) JTNO(J), EA, Eiy, EIXY, EIX, E, NTYP, NIPR, PHI, RC, XC, YC, 2900650
1 XBAR, YBAR, ROJ, RHO, RGEOM, ALPR 2900660
WRITE(6, 300) JTNO(J), EA, Eiy, EIXY, EIX, ALPR, E, RC, XC, YC, XBAR, YBAR, 2900670
1 ROJ, TI, TO, RHO 2900680
300 FORMAT(/55X, 'RING AT JOINT NO. ', I2// ' EA =', 1PE12.5, 6X, ' Eiy =', 2900690
1 1PE12.5, 5X, ' EIXY =', 1PE12.5, 4X, ' EIX =', 1PE12.5, 5X, ' ALPR =', 2900700
2 1PE12.5, 4X, ' E =', 1PE12.5// ' RC =', 1PE12.5, 6X, ' XC =', 1PE12.5, 6X, 2900710
3 ' YC =', 1PE12.5, 6X, ' XBAR =', 1PE12.5, 4X, ' YBAR =', 1PE12.5, 4X, ' RO =', 2900720
4 1PE12.5// ' TI =', 1PE12.5, 6X, ' TO =', 1PE12.5, 6X, ' RHO =', 1PE12.5) 2900730
GO TO 211 2900740
212 READ(1) JTNO(J), EA, Eiy, EIXY, EIX, E, NTYP, NIPR, PHI, RC, XC, YC, 2900750
1 XBAR, YBAR, ROJ, RHO, RGEOM, ALPR 2900760
211 CONTINUE 2900770
A = EA/E 2900780
ROM = RHO*OMEGA*DELPH 2900790
RS = RC+XC 2900800
RCS = RC*RS 2900810
RC2 = RC*RC 2900820
YC2 = YC*YC 2900830
TWOPI = 2.0*3.1415927 2900840
RNGTOT(1,1) = 1.0/RCS*(EA+Eiy/RC2) 2900850
RNGTOT(2,1) = 0.0 2900860
RNGTOT(3,1) = 0.0 2900870
RNGTOT(4,1) = 1.0/RCS*(-EA*YC-Eiy*YC/RC2-EIXY/RC) 2900880
RNGTOT(1,2) = 0.0 2900890
RNGTOT(2,2) = 0.0 2900900
RNGTOT(3,2) = 0.0 2900910
RNGTOT(4,2) = 0.0 2900920
RNGTOT(1,3) = 0.0 2900930
RNGTOT(2,3) = 0.0 2900940
RNGTOT(3,3) = 0.0 2900950
RNGTOT(4,3) = 0.0 2900960
RNGTOT(1,4) = RNGTOT(4,1) 2900970
RNGTOT(2,4) = 0.0 2900980
RNGTOT(3,4) = 0.0 2900990
RNGTOT(4,4) = 1.0/RCS*(YC2*EA+Eiy*YC+EIX+2.0*EIXY*YC/RC) 2901000
IF (NEO.NE.0) GO TO 50 2901010
IF (Q.NE.1) GO TO 400 2901020
50 READ(JOR) NPLEV, RNGSRN, RGSRS, NPLA, RSIG, REPS, RALPH, RBAPH, RTEPS, 2901030
1 SIGOX, RMOSS, RMOSN, REFF, KORIR, AMN, BN, OENTH3, ODELR, SAVR, 2901040
2 IPRINT 2901050
K = JTNO(J) 2901060
IF (MFLG.EQ.2) GO TO 102 2901070
ENTH(1) = (AMAT(K,1)*ROJ-YBAR*(AMAT(K,3)-OENTH3))/RS 2901080
ENTH(2) = (AMAT(K,3)-OENTH3)/RS
ENTH(3) = AMAT(K,3) 2901100
DELR = AMAT(K,4) 2901110
GO TO 101 2901120
102 ENTH(1) = (AMAT(K,5)*ROJ-YBAR*(AMAT(K,7)-OENTH3))/RS 2901130
ENTH(2) = (AMAT(K,7)-OENTH3)/RS
ENTH(3) = AMAT(K,7) 2901150
DELR = AMAT(K,8) 2901160
101 CONTINUE 2901170
IF (ICYCLE.NE.1) GO TO 180 2901180
IF (LDISTL.EQ.1) GO TO 185 2901190
READ(5, 215) SIGOX, RMOSS, RMOSN, TI, TO 2901200

```

215	FORMAT(5E14.7)	2901210
	CALL RITEPS (RTEPS, TI, TO, ALPR, NTPY, RGEOM)	2901220
	IND = 0	2901230
	CALL RESULT (TEPSIN, RTEPS, ENTH(3), NTPY, IND, RGEOM, PHI)	2901240
185	IF (DELP/ABS(DELP).EQ.DELP1/ABS(DELP1)) GO TO 180	2901250
	DO 181 I=1,12	2901260
	NPLA(I) = 0	2901270
181	RBAPH(I) = RSIG(I)	2901280
180	CONTINUE	2901290
	DDELR = DELR-ODELR	2901300
	DOMEG = ENTH(3)-DENTH3	2901310
	D1 = DELR-YBAR*ENTH(3)	2901320
	DD1 = DDELR-YBAR*DOMEG	2901330
	DF1 = RNGTOT(1,1)*DD1+RNGTOT(4,1)*DOMEG+SAVR(1)	2901340
	DF2 = RNGTOT(1,4)*DD1+RNGTOT(4,4)*DOMEG+SAVR(2)	2901350
	SAVR(5) = SAVR(5)+DF1	2901360
	SAVR(6) = SAVR(6)+DF2	2901370
	C = RNGTOT(1,1)*D1+RNGTOT(4,1)*ENTH(3)-SAVR(5)+SAVR(3)	2901380
	D = RNGTOT(1,4)*D1+RNGTOT(4,4)*ENTH(3)-SAVR(6)+SAVR(4)	2901390
	DO 483 L=1,2	2901400
483	RNGSRN(L) = RNGSRN(L)+ENTH(L)	2901410
	DO 484 II=1,NIPR	2901420
484	TEPS(II) = DELP * RTEPS(II)	2901430
	CALL RGSRSE (DSIG, ENTH, TEPS, E, NTPY, RGEOM, PHI)	2901440
	IF(NPLEV .EQ.0) GO TO 540	2901450
	DO 500 II=1,NIPR	2901460
	IF(NPLA(II) .LE.0) GO TO 496	2901470
	IF((RSIG(II)-RALPH(II))*DSIG(II) .LT. ZEPS) GO TO 495	2901480
	IF (RMOSN.NE.0.0) GO TO 485	2901490
	DEPS(II) = DSIG(II)/E	2901500
	REPS(II) = REPS(II) + DEPS(II)	2901510
	DSIG(II) = 0.0	2901520
	GO TO 500	2901530
485	IF (RMOSS.EQ.0.0) GO TO 490	2901540
	TOMP = 0.42857143*RMOSS*(ABS(RSIG(II)-RBAPH(II))/RMOSS)**(RMOSS-	2901550
	1 1.0)	2901560
	DSIG(II)=DSIG(II)/(1.+TOMP)	2901570
	RDSIG = DSIG(II)	2901580
	DEPS(II) = TOMP/E*DSIG(II)	2901590
	RSIG(II) = RSIG(II) + DSIG(II)	2901600
	REPS(II) = REPS(II) + DEPS(II)	2901610
	IF (KORIR.EQ.0) RDSIG = 0.0	2901620
	RALPH(II) = RALPH(II)+RDSIG	2901630
	IF (KORIR.EQ.0) REFF(II) = RSIG(II)	2901640
	GO TO 500	2901650
490	DSIG(II) = RMOSN*DSIG(II)	2901660
	RDSIG = DSIG(II)	2901670
	RSIG(II) = RSIG(II) + DSIG(II)	2901680
	DEPS(II) = DSIG(II)/E*((1.0-RMOSS)/RMOSS)	2901690
	REPS(II) = REPS(II) + DEPS(II)	2901700
	IF (KORIR.EQ.0) RDSIG = 0.0	2901710
	RALPH(II) = RALPH(II)+RDSIG	2901720
	IF (KORIR.EQ.0) REFF(II) = RSIG(II)	2901730
	GO TO 500	2901740
495	NPLA(II) = -II	2901750
496	RSIG(II) = RSIG(II) + DSIG(II)	2901760
	DEPS(II) = 0.0	2901770
	YCOND = YEPS	2901780
	IF (KORIR.EQ.0) YCOND = YCOND*REFF(II)/SIGOX	2901790
	IF (ABS((RSIG(II)-RALPH(II))/SIGOX).GE.YCOND) NPLA(II) = II	2901800
500	CONTINUE	2901810

```

507 IND = 0                                2901820
CALL RESULT (REPSIN,DEPS,ENTH(3),NTYP,IND,RGEOM,PHI) 2901830
GO TO 550                                    2901840
540 DO 545 II=1,NIPR                        2901850
RSIG(II) = RSIG(II) + DSIG(II)            2901860
IF (ABS(RSIG(II)/SIGOX).LT.YEPS) GO TO 545 2901870
NPLEV = 1.                                  2901880
NPLA(II) = II                               2901890
545 CONTINUE                                2901900
REPSIN(1) = 0.0                             2901910
REPSIN(2) = 0.0                             2901920
550 IND = 1                                  2901930
CALL RESULT (RGSRS,RSIG,ENTH(3),NTYP,IND,RGEOM,PHI) 2901940
IF (P.EQ.2.) GO TO 620                      2901950
IF (IPRINT.EQ.0) GO TO 322                 2901960
620 PP = P-1.0                               2901970
IF (MFLG.EQ.2) GO TO 320                   2901980
WRITE(6,301) JTNO(J),PP                   2901990
301 FORMAT(/34X,'RING AT REGION JOINT NO. ',I2,24X,'CYCLE = ',F5.0) 2902000
GO TO 321                                    2902010
320 WRITE(6,302) JTNO(J),PP                2902020
302 FORMAT(/32X,'RING AT STRUCTURE JOINT NO. ',I2,24X,'CYCLE = ',F5.0) 2902030
321 WRITE(6,303) RNGSRN,RGSRS              2902040
303 FORMAT(3X,'EPS THETA=',1PE12.5,4X,'K THETA=',1PE12.5,6X,'N THETA=' 2902050
1,1PE12.5,6X,'MR = ',1PE12.5,10X,'MZ = ',1PE12.5) 2902060
IF (NPLEV.EQ.0) GO TO 322                  2902070
WRITE(6,304) (RSIG(I),I=1,NIPR)           2902080
304 FORMAT(//' SIGMA = ',7X,1P9E13.5/15X,1P3E13.5) 2902090
WRITE(6,305) (REPS(I),I=1,NIPR)           2902100
305 FORMAT(/' EPSILON PLAS = ',1P9E13.5/15X,1P3E13.5) 2902110
322 CONTINUE                                2902120
400 CONTINUE                                2902130
TEMI = E/RS*AMN                             2902140
RNLGLOD(1,J) = DELP*TEMI+E/RS*REPSIN(1)-X3*C 2902150
RNLGLOD(2,J) = 0.0                          2902160
RNLGLOD(3,J) = 0.0                          2902170
RNLGLOD(4,J) =DELP*(-TEMI*YC-E/RS*BN)-E/RS*(YC*REPSIN(1)+REPSIN(2)) 2902180
1 -X3*D                                       2902190
SAVR(1) = RNLGLOD(1,J)                      2902200
SAVR(2) = RNLGLOD(4,J)                      2902210
SAVR(3) = SAVR(3)+SAVR(1)                   2902220
SAVR(4) = SAVR(4)+SAVR(2)                   2902230
IPRINT = 0                                    2902240
IF (IBEGIN.EQ.1.OR.(IMAX-1).EQ.ICYCLE) IPRINT = 1 2902250
WRITE(IOR) NPLEV,RNGSRN,RGSRS,NPLA,RSIG,REPS,RALPH,RBAPH,RTEPS, 2902260
1 SIGOX,RMOSS,RMOSN,REFF,KORIR,AMN,BN,ENTH(3),DELR,SAVR, 2902270
2 IPRINT                                       2902280
XBR5 = 1.0-XBAR/RS                          2902290
TDEL(1,1) = 0.0                             2902300
TDEL(2,1) = 0.0                             2902310
TDEL(3,1) = -1.0/XBR5                       2902320
TDEL(4,1) = 0.0                             2902330
TDEL(1,2) = 0.0                             2902340
TDEL(2,2) = -1.0                            2902350
TDEL(3,2) = 0.0                             2902360
TDEL(4,2) = 0.0                             2902370
TDEL(1,3) = -1.0                            2902380
TDEL(2,3) = 0.0                             2902390
TDEL(3,3) = 0.0                             2902400
TDEL(4,3) = 0.0                             2902410
TDEL(1,4) = -YBAR                           2902420

```

TDEL(2,4) = +XBAR	2902430
TDEL(3,4) = 0.0	2902440
TDEL(4,4) = -1.0	2902450
DO 813 L=1,4	2902460
DO 813 M=1,4	2902470
XKTOT(L,M) = 0.0	2902480
DO 813 N=1,4	2902490
813 XKTOT(L,M) = XKTOT(L,M)+RNGTOT(L,N)*TDEL(N,M)	2902500
DO 814 L=1,4	2902510
DO 814 M=1,4	2902520
RNGTOT(L,M) = 0.0	2902530
DO 814 N=1,4	2902540
814 RNGTOT(L,M) = RNGTOT(L,M)+TDEL(N,L)*XKTOT(N,M)	2902550
DO 815 L=1,4	2902560
XL(L) = 0.0	2902570
DO 815 N=1,4	2902580
815 XL(L) = XL(L)+TDEL(N,L)*RNGLOD(N,J)	2902590
DO 816 L=1,2	2902600
816 RNGLOD(L,J) = XL(L)	2902610
B = -ROM*RC*A	2902620
RNGLOD(3,J) = XL(3)+B	2902630
RNGLOD(4,J) = XL(4)+YBAR*B	2902640
DO 1100 L=1,NSEG	2902650
IF (JTNO(J).EQ.JTIC(L)) GO TO 1105	2902660
1100 CONTINUE	2902670
GO TO 1107	2902680
1105 M = JTIC(L)	2902690
RMULT = ADUS(M)*TWOPI	2902700
GO TO 1111	2902710
1107 DO 1101 L=1,NSEG	2902720
IF (JTNO(J).EQ.JSTOP(L)) GO TO 1106	2902730
1101 CONTINUE	2902740
1106 M = JSTOP(L)	2902750
RMULT = BADUS(M)*TWOPI	2902760
1111 CONTINUE	2902770
DO 820 L=1,4	2902780
DO 820 M=1,4	2902790
820 RNGTOT(L,M) = RNGTOT(L,M)*RMULT	2902800
DO 821 L=1,4	2902810
821 RNGLOD(L,J) = RNGLOD(L,J)*RMULT	2902820
402 RETURN	2902830
8888 NIX = 1	2902840
GO TO 402	2902850
END	2902860



```

FOR, IS RITEPS, RITEPS
SUBROUTINE RITEPS (RTEPS, TI, TO, ALPR, NTP, RGEOM)
COMMON /GINT/ AA(8,4), WW(8,4)
DIMENSION RTEPS(1), TEMP(4), RGEOM(1)
PI = 3.14159265
TEMP(1) = (TI-TO)/2.0
TEMP(2) = (TI+TO)/2.0
GO TO (100, 200, 300, 400, 500, 200, 600, 600), NTP
C
C SOLID RECTANGULAR SECTION
C
100 RTEPS(1) = ALPR*(TEMP(1)*AA(3,1)+TEMP(2))
RTEPS(2) = RTEPS(1)
RTEPS(3) = RTEPS(1)
RTEPS(4) = ALPR*(-TEMP(1)*AA(3,1)+TEMP(2))
RTEPS(5) = RTEPS(4)
RTEPS(6) = RTEPS(4)
RTEPS(7) = ALPR*TEMP(2)
RTEPS(8) = RTEPS(7)
RTEPS(9) = RTEPS(7)
GO TO 990
C
C Z-SECTION, I-SECTION OR CHANNEL SECTION
C
200 DENO=RGEOM(1)*RGEOM(4)+RGEOM(2)*RGEOM(5)+RGEOM(3)*RGEOM(6)
X1=RGEOM(2)/2.*(RGEOM(3)*RGEOM(6)-RGEOM(1)*RGEOM(4))/DENO
TEMP(3)=2.*TEMP(1)/RGEOM(2)
TEMP(4)=RGEOM(2)/2.-X1
RTEPS(7)=ALPR*TI
RTEPS(8)=RTEPS(7)
RTEPS(9)=RTEPS(7)
XT=RGEOM(2)/2.*AA(3,1)-X1
TT=TEMP(3)*(XT-TEMP(4))+TI
RTEPS(4)=ALPR*TT
XT=-RGEOM(2)/2.*AA(3,1)-X1
TT=TEMP(3)*(XT-TEMP(4))+TI
RTEPS(5)=ALPR*TT
XT=-X1
TT=TEMP(3)*(XT-TEMP(4))+TI
RTEPS(6)=ALPR*TT
RTEPS(1)=ALPR*TO
RTEPS(2)=RTEPS(1)
RTEPS(3)=RTEPS(1)
GO TO 990
C
C HOLLOW RECTANGULAR SECTION
C
300 X1=RGEOM(1)*RGEOM(2)/2.*(RGEOM(5)-RGEOM(3))/(RGEOM(1)*(RGEOM(3)
1 +RGEOM(5))+2.*RGEOM(2)*RGEOM(4))
TEMP(3)=2.*TEMP(1)/RGEOM(2)
TEMP(4)=RGEOM(2)/2.-X1
RTEPS(7)=ALPR*TI
RTEPS(8)=RTEPS(7)
RTEPS(9)=RTEPS(7)
XT=RGEOM(2)/2.*AA(3,1)-X1
TT=TEMP(3)*(XT-TEMP(4))+TI
RTEPS(4)=ALPR*TT
XT=-RGEOM(2)/2.*AA(3,1)-X1
TT=TEMP(3)*(XT-TEMP(4))+TI
RTEPS(5)=ALPR*TT
XT=-X1
TT=TEMP(3)*(XT-TEMP(4))+TI

```

```

3000010
3000020
3000030
3000040
3000050
3000060
3000070
3000080
3000090
3000100
3000110
3000120
3000130
3000140
3000150
3000160
3000170
3000180
3000190
3000200
3000210
3000220
3000230
3000330
3000340
3000350
3000360

```

	RTEPS(6)=ALPR*TT	
	RTEPS(1)=ALPR*TO	
	RTEPS(2)=RTEPS(1)	
	RTEPS(3)=RTEPS(1)	
	RTEPS(10) = RTEPS(4)	3000460
	RTEPS(11) = RTEPS(5)	3000470
	RTEPS(12) = RTEPS(6)	3000480
	GO TO 990	3000490
C		3000500
C	TRIANGULAR SECTION (ISOSCELES)	3000510
C		3000520
400	RTEPS(4) = TI*ALPR	3000530
	RTEPS(5) = RTEPS(4)	3000540
	RTEPS(6) = RTEPS(4)	3000550
	X1 = RGEOM(1)*RGEOM(1)*RGEOM(3)	3000560
	ST = RGEOM(2)/(2.0*RGEOM(1))	3000570
	CT = SQRT(1.0-ST*ST)	3000580
	X2 = 2.0*RGEOM(1)*RGEOM(3)+RGEOM(2)*RGEOM(4)	3000590
	X1 = X1*CT/X2	3000600
	X2 = -RGEOM(1)*CT*(RGEOM(1)*RGEOM(3)+RGEOM(2)*RGEOM(4))/X2	3000610
	TEMP(3) = (X1+X2)/2.0	3000620
	TEMP(4) = (X1-X2)/2.0	3000630
	X = TEMP(3)*AA(3,1)+TEMP(4)	3000640
	Q = TEMP(1)/TEMP(4)	3000650
	RTEPS(1) = (Q*(X-X1)+TI)*ALPR	3000660
	RTEPS(7) = RTEPS(1)	3000670
	X = -TEMP(3)*AA(3,1)+TEMP(4)	3000680
	RTEPS(2) = (Q*(X-X1)+TI)*ALPR	3000690
	RTEPS(8) = RTEPS(2)	3000700
	X = TEMP(4)	3000710
	RTEPS(3) = (Q*(X-X1)+TI)*ALPR	3000720
	RTEPS(9) = RTEPS(3)	3000730
	GO TO 990	3000740
		3000750
C		3000760
C	CRRC SECTION	3000770
C		3000780
500	RTEPS(1) = ALPR*TI	3000790
	RTEPS(2) = RTEPS(1)	3000800
	RTEPS(3) = RTEPS(1)	3000810
	X1 = (2.0*RGEOM(1)*RGEOM(1)+PI*RGEOM(2)*(RGEOM(1)+RGEOM(2)/PI))*	3000820
1	RGEOM(3)/(4.0*RGEOM(1)+PI*RGEOM(2))*RGEOM(3)+2.0*RGEOM(2)*	3000830
2	RGEOM(4))	3000840
	X = X1+RGEOM(2)/2.0*(AA(3,1)-1.0)	3000850
	X2 = X1-(RGEOM(1)+RGEOM(2)/2.0)	3000860
	TEMP(3) = (X1+X2)/2.0	3000870
	TEMP(4) = (X1-X2)/2.0	3000880
	Q = TEMP(1)/TEMP(4)	3000890
	RTEPS(4) = (Q*(X-X1)+TI)*ALPR	3000900
	RTEPS(7) = RTEPS(4)	3000910
	X = X1-RGEOM(2)/2.0*(AA(3,1)+1.0)	3000920
	RTEPS(5) = (Q*(X-X1)+TI)*ALPR	3000930
	RTEPS(8) = RTEPS(5)	3000940
	RTEPS(6) = (-Q*RGEOM(2)/2.0+TI)*ALPR	3000950
	RTEPS(9) = RTEPS(6)	3000960
	THETA = PI/2.0*(1.0+AA(3,1))	3000970
	X = X1-RGEOM(1)-RGEOM(2)/2.0*SIN(THETA)	3000980
	RTEPS(10) = (Q*(X-X1)+TI)*ALPR	3000990
	THETA = PI/2.0*(1.0-AA(3,1))	3001000
	X = X1-RGEOM(1)-RGEOM(2)/2.0*SIN(THETA)	3001010
	RTEPS(11) = (Q*(X-X1)+TI)*ALPR	3001020
	X = X1-RGEOM(1)-RGEOM(2)/2.0	

	RTEPS(12) = (Q*(X-X1)+T.I)*ALPR	3001030
	GO TO 990	3001040
C		3001050
C	T-SECTION OR RIGHT ANGULAR SECTION	3001060
C		3001070
	600 X1=RGEOM(2)/2.*(RGEOM(2)*RGEOM(4)+2.*RGEOM(1)*RGEOM(3))/(RGEOM(2)	
	1 *RGEOM(4)+RGEOM(1)*RGEOM(3))	
	TEMP(3)=2.*TEMP(1)/RGEOM(2)	
	RTEPS(1)=ALPR*TO	
	RTEPS(2) = RTEPS(1)	3001090
	RTEPS(3) = RTEPS(1)	3001100
	XT=RGEOM(2)/2.*(AA(3,1)-1.)+X1	
	TT=TEMP(3)*(XT-X1)+TI	
	RTEPS(4)=ALPR*TT	
	XT=-RGEOM(2)/2.*(AA(3,1)+1.)+X1	
	TT=TEMP(3)*(XT-X1)+TI	
	RTEPS(5)=ALPR*TT	
	XT=-RGEOM(2)/2.+X1	
	TT=TEMP(3)*(XT-X1)+TI	
	RTEPS(6)=ALPR*TT	
	990 RETURN	3001140
	END	3001150

```

FOR,IS RESULT,RESULT.
SUBROUTINE RESULT (RGSRS,SIG,ENTH,NTYP,IND,RGEOM,PHI)      3100010
COMMON /GINT/ AA(8,4),WW(8,4)                             3100020
DIMENSION RGSRS(1),SIG(1),TEMP(2),RGEOM(1)               3100030
II = 1                                                     3100040
PI = 3.14159265                                           3100050
ANG = PHI+ENTH                                             3100060
TEMP(1) = COS(ANG)                                         3100070
TEMP(2) = SIN(ANG)                                         3100080
RGSRS(1) = 0.0                                             3100090
RGSRS(2) = 0.0                                             3100100
IF (IND .NE.0) RGSRS(3) = 0.0                             3100110
GO TO (100,300,400,600,200,500,700,800,900),NTYP        3100120
C                                                         3100130
C SOLID RECTANGULAR SECTION                               3100140
C                                                         3100150
100 DO 140 L=1,2                                           3100160
    XT = RGEOM(1)/2.0*AA(3,L)                               3100170
110 DO 130 LL=1,2                                           3100180
    YT = RGEOM(2)/2.0*AA(3,LL)                             3100190
120 RGSRS(1) = RGSRS(1) + WW(3,L) * WW(3,LL) * SIG(II)   3100200
    RGSRS(2) = RGSRS(2) - WW(3,L) * WW(3,LL) * SIG(II) * (-XT*TEMP(1) + 3100210
1    YT * TEMP(2))
    IF (IND.NE.0) RGSRS(3) = RGSRS(3) - WW(3,L) * WW(3,LL)*SIG(II) * 3100220
1    (XT * TEMP(2) + YT * TEMP(1))
    II = II+1                                               3100230
    IF(YT .LE.0.0) GO TO 130                                3100240
    YT = -YT                                                3100250
    GO TO 120                                               3100260
130 CONTINUE                                               3100270
    IF(XT .LE. 0.0) GO TO 140                               3100280
    XT = -XT                                                3100290
    GO TO 110                                               3100300
140 CONTINUE                                               3100310
    FACT = RGEOM(1)*RGEOM(2)/4.0                           3100320
    RGSRS(1) = RGSRS(1) * FACT                             3100330
    RGSRS(2) = RGSRS(2) * FACT                             3100340
    IF(IND .NE.0) RGSRS(3) = RGSRS(3) * FACT              3100350
    GO TO 990                                               3100360
C                                                         3100370
C                                                         3100380
C TRIANGULAR SECTION (ISOSCELES)                          3100390
C                                                         3100400
C                                                         3100410
200 CONTINUE                                               3100420
    X1 = RGEOM(1)*RGEOM(1)*RGEOM(3)                       3100430
    ST = RGEOM(2)/2.0/RGEOM(1)                             3100440
    CT = SQRT(1.0-ST*ST)                                    3100450
    X2 = 2.0*RGEOM(1)*RGEOM(3)+RGEOM(2)*RGEOM(4)         3100460
    X1 = X1*CT/2.0                                          3100470
    X2 = RGEOM(1)*CT*(RGEOM(1)*RGEOM(3)+RGEOM(2)*RGEOM(4))/X2 3100480
    DO 230 L=1,2                                           3100490
    SI = AA(3,L)                                           3100500
210 RGSRS(1) = RGSRS(1)+WW(3,L)*((SIG(II)+SIG(II+6))*RGEOM(1)*RGEOM(3) 3100510
1    +SIG(II+3)*RGEOM(2)*RGEOM(4))/2.0
    YT = -RGEOM(2)/2.0*SI                                   3100520
    RGSRS(2) = RGSRS(2)-WW(3,L)*RGEOM(2)*RGEOM(4)*SIG(II+3)/2.0* 3100530
1    (-X1*TEMP(1)+YT*TEMP(2))
    XT = (X1-X2)/2.0-(X2+X1)/2.0*SI                       3100540
    YT = RGEOM(2)/2.0*(1.0-SI)                             3100550
    RGSRS(2) = RGSRS(2)-WW(3,L)*RGEOM(1)*RGEOM(3)*SIG(II)/2.0* 3100560
1    (-XT*TEMP(1)+YT*TEMP(2))                             3100570
    RGSRS(2) = RGSRS(2)-WW(3,L)*RGEOM(1)*RGEOM(3)*SIG(II)/2.0* 3100580
1    (-XT*TEMP(1)+YT*TEMP(2))                             3100590

```

	YT = -YT	3100600
	RGSRS(2) = RGSRS(2)-WW(3,L)*RGEOM(1)*RGEOM(3)*SIG(II+6)/2.0*	3100610
1	(-XT*TEMP(1)+YT*TEMP(2))	3100620
	IF (IND.EQ.0) GO TO 220	3100630
	YT = -RGEOM(2)/2.0*SI	3100640
	RGSRS(3) = RGSRS(3)-WW(3,L)*RGEOM(2)*RGEOM(4)*SIG(II+3)/2.0*	3100650
1	(X1*TEMP(2)+YT*TEMP(1))	3100660
	XT = (X1-X2)/2.0-(X2+X1)/2.0*SI	3100670
	YT = RGEOM(2)/2.0*(1.0-SI)	3100680
	RGSRS(3) = RGSRS(3)-WW(3,L)*RGEOM(1)*RGEOM(3)*SIG(II)/2.0*	3100690
1	(XT*TEMP(2)+YT*TEMP(1))	3100700
	YT = -YT	3100710
	RGSRS(3) = RGSRS(3)-WW(3,L)*RGEOM(1)*RGEOM(3)*SIG(II+6)/2.0*	3100720
1	(XT*TEMP(2)+YT*TEMP(1))	3100730
220	II = II+1	3100740
	IF (SI.LE.0.0) GO TO 230	3100750
	SI = -SI	3100760
	GO TO 210	3100770
230	CONTINUE	3100780
	GO TO 990	3100790
C		3100800
C	Z-SECTION	3100810
C		3100820
300	DENO=RGEOM(1)*RGEOM(4)+RGEOM(2)*RGEOM(5)+RGEOM(3)*RGEOM(6)	
	X1=RGEOM(2)/2.*(RGEOM(3)*RGEOM(6)-RGEOM(1)*RGEOM(4))/DENO	
	Y1=(RGEOM(1)**2*RGEOM(4)-RGEOM(3)**2*RGEOM(6))/2./DENO	
	X2=-RGEOM(2)/2.-X1	
	X3=RGEOM(2)/2.-X1	
	DO 330 L=1,2	
	SI = AA(3,L)	3100840
310	RGSRS(1) = RGSRS(1) + WW(3,L) * (SIG(II) * RGEOM(1) * RGEOM(4)	3100850
1	+ SIG(II+3) * RGEOM(2) * RGEOM(5)	3100860
2	+ SIG(II+6) * RGEOM(3) * RGEOM(6))/2.0	3100870
	YT=RGEOM(1)/2.*(1.+SI)-Y1	
	RGSRS(2) = RGSRS(2)-WW(3,L) * SIG(II) / 2.0*RGEOM(1) *	3100890
1	RGEOM(4)*(-X1*TEMP(1)+YT*TEMP(2))	
	YT=RGEOM(2)/2.*SI-X1	
	RGSRS(2) = RGSRS(2) + WW(3,L) * SIG(II+3) / 2.0 * RGEOM(2) *	3100920
1	RGEOM(5)*(-YT*TEMP(1)-Y1*TEMP(2))	
	YT=-RGEOM(3)/2.*(1.-SI)-Y1	
	RGSRS(2) = RGSRS(2) - WW(3,L) * SIG(II+6) / 2.0 * RGEOM(3) *	3100950
1	RGEOM(6)*(-X3*TEMP(1)+YT*TEMP(2))	
	IF (IND .EQ.0) GO TO 320	3100970
	YT=RGEOM(1)/2.*(1.+SI)-Y1	
	RGSRS(3) = RGSRS(3) - WW(3,L) * SIG(II) / 2.0 * RGEOM(1) *	3100990
1	RGEOM(4)*(X1*TEMP(2)+YT*TEMP(1))	
	YT=RGEOM(2)/2.*SI-X1	
	RGSRS(3) = RGSRS(3) - WW(3,L) * SIG(II+3) / 2.0 * RGEOM(2) *	3101020
1	RGEOM(5)*(YT*TEMP(2)-Y1*TEMP(1))	
	YT=-RGEOM(3)/2.*(1.-SI)-Y1	
	RGSRS(3) = RGSRS(3) - WW(3,L) * SIG(II+6) / 2.0 * RGEOM(3) *	3101050
1	RGEOM(6)*(X3*TEMP(2)+YT*TEMP(1))	
320	II = II + 1	3101070
	IF (SI .LE.0.0) GO TO 330	3101080
	SI = -SI	3101090
	GO TO 310	3101100
330	CONTINUE	3101110
	GO TO 990	3101120
C		3101130
C	I- SECTION	3101140
C		3101150

```

400 X1=RGEOM(2)/2.*(RGEOM(3)*RGEOM(6)-RGEOM(1)*RGEOM(4))/(RGEOM(1)*
1 RGEOM(4)+RGEOM(2)*RGEOM(5)+RGEOM(3)*RGEOM(6))
X2=RGEOM(2)/2.-X1
X3=-RGEOM(2)/2.-X1
DO 430 L=1,2
SI = AA(3,L)
410 RGSRS(1) = RGSRS(1) + WW(3,L) * (SIG(II) * RGEOM(1) * RGEOM(4)
1 + SIG(II+3) * RGEOM(2) * RGEOM(5)
2 + SIG(II+6) * RGEOM(3) * RGEOM(6)) / 2.0
YT = RGEOM(1) * SI / 2.0
RGSRS(2) = RGSRS(2) - WW(3,L) * SIG(II) / 2.0 * RGEOM(1) *
1 RGEOM(4)*(-X3*TEMP(1)+YT*TEMP(2))
YT=RGEOM(2)*SI/2.-X1
RGSRS(2) = RGSRS(2) + WW(3,L) * SIG(II+3) / 2.0 * RGEOM(2) *
1 RGEOM(5) * YT * TEMP(1)
YT = RGEOM(3) * SI / 2.0
RGSRS(2) = RGSRS(2) - WW(3,L) * SIG(II+6) / 2.0 * RGEOM(3) *
1 RGEOM(6)*(-X2*TEMP(1)+YT*TEMP(2))
IF (IND .EQ. 0) GO TO 420
YT = RGEOM(1) * SI / 2.0
RGSRS(3) = RGSRS(3) - WW(3,L) * SIG(II) / 2.0 * RGEOM(1) *
1 RGEOM(4)*(-X3*TEMP(2)+YT*TEMP(1))
YT=RGEOM(2)*SI/2.-X1
RGSRS(3) = RGSRS(3) - WW(3,L) * SIG(II+3) / 2.0 * RGEOM(2) *
1 RGEOM(5) * YT * TEMP(2)
YT = RGEOM(3) * SI / 2.0
RGSRS(3) = RGSRS(3) - WW(3,L) * SIG(II+6) / 2.0 * RGEOM(3) *
1 RGEOM(6)*(X2*TEMP(2)+YT*TEMP(1))
420 II = II+1
IF (SI .LE.0.0) GO TO 430
SI = -SI
GO TO 410
430 CONTINUE
GO TO 990

CRRC SECTION

500 CONTINUE
X1 = (2.0*RGEOM(1)*RGEOM(1)+PI*RGEOM(2)*(RGEOM(1)+RGEOM(2)/PI))*
1 RGEOM(3)/((4.0*RGEOM(1)+PI*RGEOM(2))*RGEOM(3)+2.0*RGEOM(2))*
2 RGEOM(4))
DO 530 L=1,2
SI = AA(3,L)
510 RGSRS(1) = RGSRS(1)+WW(3,L)/2.0*(SIG(II)*RGEOM(2)*RGEOM(4)+
1 (SIG(II+3)+SIG(II+6))*RGEOM(1)*RGEOM(3)+SIG(II+9)*
2 RGEOM(2)*RGEOM(3)*PI/2.0)
XT = X1
YT = -RGEOM(2)/2.0*SI
RGSRS(2) = RGSRS(2)-WW(3,L)*SIG(II)/2.0*RGEOM(2)*RGEOM(4)*
1 (-XT*TEMP(1)+YT*TEMP(2))
XT = RGEOM(1)/2.0*(SI-1.0)+X1
YT = RGEOM(2)/2.0
RGSRS(2) = RGSRS(2)-WW(3,L)*SIG(II+3)/2.0*RGEOM(1)*RGEOM(3)*
1 (-XT*TEMP(1)+YT*TEMP(2))
YT = -YT
RGSRS(2) = RGSRS(2)-WW(3,L)*SIG(II+6)/2.0*RGEOM(1)*RGEOM(3)*
1 (-XT*TEMP(1)+YT*TEMP(2))
THT = PI/2.0*(1.0+SI)
XT = X1-RGEOM(1)-RGEOM(2)/2.0*SIN(THT)
YT = RGEOM(2)/2.0*COS(THT)
RGSRS(2) = RGSRS(2)-WW(3,L)*SIG(II+9)/4.0*RGEOM(2)*RGEOM(3)*PI*

```

```

1          (-XT*TEMP(1)+YT*TEMP(2))
IF (IND.EQ.0) GO TO 520
XT = X1
YT = -RGEOM(2)/2.0*SI
RGSRS(3) = RGSRS(3)-WW(3,L)*SIG(II)/2.0*RGEOM(2)*RGEOM(4)*
1          (XT*TEMP(2)+YT*TEMP(1))
XT = RGEOM(1)/2.0*(SI-1.0)+RGEOM(1)
YT = RGEOM(2)/2.0
RGSRS(3) = RGSRS(3)-WW(3,L)*SIG(II+3)/2.0*RGEOM(1)*RGEOM(3)*
1          (XT*TEMP(2)+YT*TEMP(1))
YT = -YT
RGSRS(3) = RGSRS(3)-WW(3,L)*SIG(II+6)/2.0*RGEOM(1)*RGEOM(3)*
1          (XT*TEMP(2)+YT*TEMP(1))
XT = X1-RGEOM(1)-RGEOM(2)/2.0*SIN(THT)
YT = RGEOM(2)/2.0*COS(THT)
RGSRS(3) = RGSRS(3)-WW(3,L)*SIG(II+9)/4.0*RGEOM(2)*RGEOM(3)*
1          PI*(XT*TEMP(2)+YT*TEMP(1))
520 II = II+1
IF (SI.LE.0.0) GO TO 530
SI = -SI
GO TO 510
530 CONTINUE
GO TO 990
C
C          HOLLOW RECTANGULAR SECTION
C
600 X1=RGEOM(1)*RGEOM(2)/2.*(RGEOM(5)-RGEOM(3))/(RGEOM(1)*RGEOM(3)
1 +RGEOM(5))+2.*RGEOM(2)*RGEOM(4)
X2=RGEOM(2)/2.-X1
X3=-RGEOM(2)/2.-X1
DO 630 L=1,2
SI = AA(3,L)
610 RGSRS(1)=RGSRS(1)+WW(3,L)*(RGEOM(1)*RGEOM(3)*SIG(II)
1 +RGEOM(1)*RGEOM(5)*SIG(II+6)+RGEOM(2)*RGEOM(4)*(SIG(II+3)
2 +SIG(II+9)))/2.0
YT = RGEOM(1) * SI / 2.0
RGSRS(2)=RGSRS(2)-WW(3,L)*(SIG(II)*(-X3*TEMP(1)+YT*TEMP(2))*RGEOM
1 (3)+SIG(II+6)*(-X2*TEMP(1)+YT*TEMP(2))*RGEOM(5))*RGEOM(1)/2.
YT=RGEOM(2)*SI/2.-X1
RGSRS(2) = RGSRS(2) - WW(3,L) * (SIG(II+3) * (RGEOM(1) * TEMP(2) /
1 2.0 - YT * TEMP(1)) + SIG(II+9) * (-RGEOM(1) * TEMP(2)
2 / 2.0 - YT * TEMP(1))) * RGEOM(2) * RGEOM(4) / 2.0
IF (IND.EQ.0) GO TO 620
YT = RGEOM(1) * SI / 2.0
RGSRS(3)=RGSRS(3)-WW(3,L)*(SIG(II)*(X3*TEMP(2)+YT*TEMP(1))*
1 RGEOM(3)+SIG(II+6)*(X2*TEMP(2)+YT*TEMP(1))*RGEOM(5))*RGEOM(1)/2.
YT=RGEOM(2)*SI/2.-X1
RGSRS(3) = RGSRS(3) - WW(3,L) * (SIG(II+3) * (YT * TEMP(2) +
1 RGEOM(1)/2.*TEMP(1))+SIG(II+9)*(YT*TEMP(2)-
2 RGEOM(1)/2.*TEMP(1)))*RGEOM(2)*RGEOM(4)/2.
620 II = II+1
IF (SI.LE.0.0) GO TO 630
SI = -SI
GO TO 610
630 CONTINUE
GO TO 990
C
C          CHANNEL SECTION
C
700 CONTINUE
DENO=RGEOM(1)*RGEOM(4)+RGEOM(2)*RGEOM(5)+RGEOM(3)*RGEOM(6)

```

```

3101730
3101740
3101750
3101760
3101770
3101780
3101790
3101800
3101810
3101820
3101830
3101840
3101850
3101860
3101870
3101880
3101890
3101900
3101910
3101920
3101930
3101940
3101950
3101960
3101970
3101980
3102000
3102040
3102090
3102100
3102110
3102120
3102130
3102180
3102210
3102220
3102230
3102240
3102250
3102260
3102270
3102280
3102290
3102300

```

```

YI=(RGEOM(1)**2*RGEOM(4)+RGEOM(3)**2*RGEOM(6))/2./DENO
X1=RGEOM(2)/2.*(RGEOM(3)*RGEOM(6)-RGEOM(1)*RGEOM(4))/DENO
DO 730 L=1,2
SI = AA(3,L)
710 RGSRS(1)=RGSRS(1)+WW(3,L)/2.*(SIG(II)*RGEOM(1)*RGEOM(4)+SIG(II+3)
1 *RGEOM(2)*RGEOM(5)+SIG(II+6)*RGEOM(3)*RGEOM(6))
XT=-RGEOM(2)/2.-X1
YT = RGEOM(1)/2.0*(SI-1.0)+Y1
RGSRS(2)=RGSRS(2)-WW(3,L)*SIG(II)/2.0*RGEOM(1)*RGEOM(4)*
1 (-XT*TEMP(1)+YT*TEMP(2))
XT=RGEOM(2)/2.-X1
YT=RGEOM(3)/2.*(SI-1.0)+Y1
RGSRS(2)=RGSRS(2)-WW(3,L)*SIG(II+6)/2.*RGEOM(3)*RGEOM(6)*
1 (-XT*TEMP(1)+YT*TEMP(2))
XT=RGEOM(2)/2.*SI-Y1
RGSRS(2)=RGSRS(2)-WW(3,L)*SIG(II+3)/2.*RGEOM(2)*RGEOM(5)*
1 (-XT*TEMP(1)+Y1*TEMP(2))
IF (IND.EQ.0) GO TO 720
XT=-RGEOM(2)/2.-X1
YT=RGEOM(1)/2.*(SI-1.0)+Y1
RGSRS(3)=RGSRS(3)-WW(3,L)*SIG(II)/2.*RGEOM(1)*RGEOM(4)*
1 (XT*TEMP(2)+YT*TEMP(1))
XT=RGEOM(2)/2.-X1
YT=RGEOM(3)/2.*(SI-1.0)+Y1
RGSRS(3)=RGSRS(3)-WW(3,L)*SIG(II+6)/2.*RGEOM(3)*RGEOM(6)*
1 (XT*TEMP(2)+YT*TEMP(1))
XT=RGEOM(2)/2.*SI-Y1
RGSRS(3)=RGSRS(3)-WW(3,L)*SIG(II+3)/2.*RGEOM(2)*RGEOM(5)*
1 (XT*TEMP(2)+Y1*TEMP(1))
720 II = II+1
IF (SI.LE.0.0) GO TO 730
SI = -SI
GO TO 710
730 CONTINUE
C
C T-SECTION
C
800 CONTINUE
X1 = RGEOM(2)/2.0*(RGEOM(2)*RGEOM(4)+2.0*RGEOM(1)*RGEOM(3))/
1 (RGEOM(2)*RGEOM(4)+RGEOM(1)*RGEOM(3))
DO 830 L=1,2
SI = AA(3,L)
810 RGSRS(1) = RGSRS(1)+WW(3,L)*(SIG(II)*RGEOM(1)*RGEOM(3)+SIG(II+3)*
1 RGEOM(2)*RGEOM(4))/2.0
YT = RGEOM(1)/2.0*SI
XT = X1-RGEOM(2)
RGSRS(2) = RGSRS(2)-WW(3,L)*SIG(II)/2.0*RGEOM(1)*RGEOM(3)*
1 (-XT*TEMP(1)+YT*TEMP(2))
XT=RGEOM(2)/2.*(SI-1.0)+X1
RGSRS(2) = RGSRS(2)+WW(3,L)*SIG(II+3)/2.0*RGEOM(2)*RGEOM(4)*XT*
1 TEMP(1)
IF (IND.EQ.0) GO TO 820
XT = X1-RGEOM(2)
RGSRS(3) = RGSRS(3)-WW(3,L)*SIG(II)/2.0*RGEOM(1)*RGEOM(3)*
1 (XT*TEMP(2)+YT*TEMP(1))
XT = RGEOM(2)/2.0*(SI-1.0)+X1
RGSRS(3) = RGSRS(3)-WW(3,L)+SIG(II+3)/2.0*RGEOM(2)*RGEOM(4)*XT*
1 TEMP(2)
820 II = II+1
IF (SI.LE.0.0) GO TO 830
SI = -SI

```



	GO TO 810	3102890
830	CONTINUE	3102900
	GO TO 990	3102910
C		3102920
C	RIGHT ANGULAR SECTION	3102930
C		3102940
900	CONTINUE	3102950
	X1=RGEOM(2)/2.*(RGEOM(2)*RGEOM(4)+2.*RGEOM(1)*RGEOM(3))/(RGEOM(2)	
1	*RGEOM(4)+RGEOM(1)*RGEOM(3))	
	Y1=RGEOM(1)**2*RGEOM(3)/2./(RGEOM(1)*RGEOM(3)+RGEOM(2)*RGEOM(4))	
	DO 930 L=1,2	3102990
	SI = AA(3,L)	3103000
910	RGSRS(1) = RGSRS(1)+WW(3,L)/2.0*(SIG(II)*RGEOM(1)*RGEOM(3)+	3103010
1	SIG(II+3)*RGEOM(2)+RGEOM(4))	3103020
	XT = X1-RGEOM(2)	3103030
	YT = Y1+RGEOM(1)/2.0*(SI-1.0)	3103040
	RGSRS(2) = RGSRS(2)-WW(3,L)*SIG(II)*RGEOM(1)*RGEOM(3)/2.0*	3103050
1	(-XT*TEMP(1)+YT*TEMP(2))	3103060
	XT = X1+RGEOM(2)/2.0*(SI-1.0)	3103070
	YT = Y1	3103080
	RGSRS(2) = RGSRS(2)-WW(3,L)*SIG(II+3)*RGEOM(2)*RGEOM(4)/2.0*	3103090
1	(-XT*TEMP(1)+YT*TEMP(2))	3103100
	IF (IND.EQ.0) GO TO 920	3103110
	XT = X1-RGEOM(2)	3103120
	YT = Y1+RGEOM(1)/2.0*(SI-1.0)	3103130
	RGSRS(3) = RGSRS(3)-WW(3,L)*SIG(II)*RGEOM(1)*RGEOM(3)/2.0*	3103140
1	(XT*TEMP(2)+YT*TEMP(1))	3103150
	XT = X1+RGEOM(2)/2.0*(SI-1.0)	3103160
	YT = Y1	3103170
	RGSRS(3) = RGSRS(3)-WW(3,L)*SIG(II+3)*RGEOM(2)*RGEOM(4)/2.0*	3103180
1	(XT*TEMP(2)+YT*TEMP(1))	3103190
920	II = II+1	3103200
	IF (SI.LE.0.0) GO TO 930	3103210
	SI = -SI	3103220
	GO TO 910	3103230
930	CONTINUE	3103240
990	RETURN	3103250
	END	3103260
C	..... ROUTINE ** RGSRS ** ABACUS UPDATED 10/01/73 .....	3200000

FOR, IS RGSRSE, RGSRSE	3200010
SUBROUTINE RGSRSE (SIG, ENTH, REPS, E, NTP, RGEOM, PHI)	3200020
COMMON /GINT/ AA(8,4), WW(8,4)	3200030
DIMENSION SIG(1), TEMP(2), ENTH(1), REPS(1), RGEOM(1)	3200040
II = 1	3200050
PI = 3.14159265	3200060
ANG = PHI + ENTH(3)	3200070
TEMP(1) = COS(ANG)	3200080
TEMP(2) = SIN(ANG)	3200090
GO TO (100, 300, 400, 600, 200, 500, 700, 800, 900), NTP	3200100
C	3200110
SOLID RECTANGULAR SECTION	3200120
C	3200130
100 DO 150 L=1,2	3200140
XT = RGEOM(1) / 2.0 * AA(3,L)	3200150
110 DO 140 LL=1,2	3200160
YT = RGEOM(2) / 2.0 * AA(3,LL)	3200170
120 SIG(II) = E * (ENTH(1) - (-XT * TEMP(1) + YT * TEMP(2)) * ENTH(2) - REPS(II))	3200180
II = II+1	3200190
IF(YT .LE.0.0) GO TO 140	3200200
YT = -YT	3200210
GO TO 120	3200220
140 CONTINUE	3200230
IF(XT .LE.0.0) GO TO 150	3200240
XT = -XT	3200250
GO TO 110	3200260
150 CONTINUE	3200270
GO TO 990	3200280
C	3200290
TRIANGULAR SECTION (ISOSCELES)	3200300
C	3200310
200 CONTINUE	3200320
X1 = RGEOM(1)*RGEOM(1)*RGEOM(3)	3200330
ST = RGEOM(2)/(2.0*RGEOM(1))	3200340
CT = SQRT(1.0-ST*ST)	3200350
X2 = 2.0*RGEOM(1)*RGEOM(3)+RGEOM(2)*RGEOM(4)	3200360
X1 = X1*CT/X2	3200370
X2 = -RGEOM(1)*CT*(RGEOM(1)*RGEOM(3)+RGEOM(2)*RGEOM(4))/X2	3200380
DO 220 L=1,2	3200390
SI = AA(3,L)	3200400
210 CONTINUE	3200410
YT = -RGEOM(2)/2.0*SI	3200420
SIG(II+3) = E*(ENTH(1) - (-XT*TEMP(1) + YT*TEMP(2))*ENTH(2) - REPS(II+3))	3200440
XT = (X1-X2)/2.0 - (X2+X1)/2.0*SI	3200450
YT = RGEOM(2)/2.0*(1.0-SI)	3200460
SIG(II) = E*(ENTH(1) - (-XT*TEMP(1) + YT*TEMP(2))*ENTH(2) - REPS(II))	3200470
YT = -YT	3200490
SIG(II+6) = E*(ENTH(1) - (-XT*TEMP(1) + YT*TEMP(2))*ENTH(2) - REPS(II+6))	3200500
II = II+1	3200510
IF (SI.LE.0.0) GO TO 220	3200520
SI = -SI	3200530
GO TO 210	3200540
220 CONTINUE	3200550
GO TO 990	3200560
C	3200570
Z-SECTION	3200570
C	
300 DENO=RGEOM(1)*RGEOM(4)+RGEOM(2)*RGEOM(5)+RGEOM(3)*RGEOM(6)	
X1=RGEOM(2)/2.*(RGEOM(3)*RGEOM(6)-RGEOM(1)*RGEOM(4))/DENO	

```

Y1=(RGEOM(1)**2*RGEOM(4)-RGEOM(3)**2*RGEOM(6))/2./DEND
X2=-RGEOM(2)/2.-X1
X3=RGEOM(2)/2.-X1
DO 320 L=1,2
SI = AA(3,L)
310 YT=RGEOM(1)/2.*(1.0+SI)-Y1
SIG(II)=E*(ENTH(1)-(-X2*TEMP(1)+
1 YT * TEMP(2)) * ENTH(2) - REPS(II))
YT=RGEOM(2)*SI/2.-X1
SIG(II+3)=E*(ENTH(1)-(-YT*TEMP(1)-Y1*TEMP(2))*ENTH(2)-REPS(II+3))
YT=-RGEOM(3)/2.*(1.0-SI)-Y1
SIG(II+6)=E*(ENTH(1)-(-X3*TEMP(1)
1 + YT * TEMP(2)) * ENTH(2) - REPS(II+6))
II = II+1
IF(SI .LE.0.0) GO TO 320
SI = -SI
GO TO 310
320 CONTINUE
GO TO 990

C
C I-SECTION
C
400 X1=RGEOM(2)/2.*(RGEOM(3)*RGEOM(6)-RGEOM(1)*RGEOM(4))/(RGEOM(1)*
1 RGEOM(4)+RGEOM(2)*RGEOM(5)+RGEOM(3)*RGEOM(6))
X2=RGEOM(2)/2.-X1
X3=-RGEOM(2)/2.-X1
DO 430 L=1,2
SI = AA(3,L)
410 YT = RGEOM(1) * SI / 2.0
SIG(II)=E*(ENTH(1)-(-X3*TEMP(1)
1 + YT * TEMP(2)) * ENTH(2) - REPS(II))
YT=RGEOM(2)*SI/2.-X1
SIG(II+3) = E * (ENTH(1) + YT * TEMP(1) * ENTH(2) - REPS(II+3))
YT = RGEOM(3) * SI / 2.0
SIG(II+6)=E*(ENTH(1)-(-X2*TEMP(1)
1 + YT * TEMP(2)) * ENTH(2) - REPS(II+6))
II = II+1
IF(SI .LE.0.0) GO TO 430
SI = -SI
GO TO 410
430 CONTINUE
GO TO 990

C
C CRRC SECTION
C
500 CONTINUE
X1 = (2.0*RGEOM(1)*RGEOM(1)+PI*RGEOM(2)*(RGEOM(1)+RGEOM(2)/PI))*
1 RGEOM(3)/((4.0*RGEOM(1)+PI*RGEOM(2))*RGEOM(3)+2.0*RGEOM(2))*
2 RGEOM(4))
DO 520 L=1,2
SI = AA(3,L)
510 XT = X1
YT = -RGEOM(2)/2.0*SI
SIG(II) = E*(ENTH(1)-(-XT*TEMP(1)+YT*TEMP(2))*ENTH(2)-REPS(II))
XT = RGEOM(1)/2.0*(SI-1.0)+X1
YT = RGEOM(2)/2.0
SIG(II+3)=E*(ENTH(1)-(-XT*TEMP(1)+YT*TEMP(2))*ENTH(2)-REPS(II+3))
YT = -YT
SIG(II+6)=E*(ENTH(1)-(-XT*TEMP(1)+YT*TEMP(2))*ENTH(2)-REPS(II+6))
THT = PI/2.0*(1.0+SI)
XT = X1-RGEOM(1)-RGEOM(2)/2.0*SIN(THT)

```

```

      YT = RGEOM(2)/2.0*COS(THT)
      SIG(II+9)=E*(ENTH(1)-(-XT*TEMP(1)+YT*TEMP(2))*ENTH(2)-REPS(II+9))
      II = II+1
      IF (SI.LE.0.0) GO TO 520
      SI = -SI
      GO TO 510
520 CONTINUE
      GO TO 990

C
C HOLLOW RECTANGULAR SECTION
C
600 X1=RGEOM(1)*RGEOM(2)/2.*(RGEOM(5)-RGEOM(3))/(RGEOM(1)*(RGEOM(3)
1 +RGEOM(5))+2.*RGEOM(2)*RGEOM(4))
      X2=RGEOM(2)/2.-X1
      X3=-RGEOM(2)/2.-X1
      DO 620 L=1,2
      SI = AA(3,L)
610 YT = RGEOM(1) * SI / 2.0
      SIG(II)=E*(ENTH(1)-(-X3*TEMP(1)
1 + YT * TEMP(2)) * ENTH(2) - REPS(II))
      SIG(II+6)=E*(ENTH(1)-(-X2*TEMP(1)
1 +YT*TEMP(2))*ENTH(2)-REPS(II+6))
      YT=RGEOM(2)*SI/2.-X1
      SIG(II+3) = E * (ENTH(1) - (RGEOM(1) * TEMP(2) / 2.0
1 -YT*TEMP(1))*ENTH(2)-REPS(II+3))
      SIG(II+9) = E * (ENTH(1) - (-RGEOM(1) * TEMP(2) / 2.0
1 -YT*TEMP(1))*ENTH(2)-REPS(II+9))
      II = II+1
      IF (SI.LE.0.0) GO TO 620
      SI = -SI
      GO TO 610
620 CONTINUE
      GO TO 990

C
C CHANNEL SECTION
C
700 CONTINUE
      DENO=RGEOM(1)*RGEOM(4)+RGEOM(2)*RGEOM(5)+RGEOM(3)*RGEOM(6)
      Y1=(RGEOM(1)**2*RGEOM(4)+RGEOM(3)**2*RGEOM(6))/2./DENO
      X1=RGEOM(2)/2.*(RGEOM(3)*RGEOM(6)-RGEOM(1)*RGEOM(4))/DENO
      DO 720 L=1,2
      SI = AA(3,L)
710 YT = RGEOM(1)/2.0*(SI-1.0)+Y1
      XT=-RGEOM(2)/2.-X1
      SIG(II) = E*(ENTH(1)-(-XT*TEMP(1)+YT*TEMP(2))*ENTH(2)-REPS(II))
      XT=RGEOM(2)/2.-X1
      YT=RGEOM(3)/2.*(SI-1.0)+Y1
      SIG(II+6)=E*(ENTH(1)-(-XT*TEMP(1)+YT*TEMP(2))*ENTH(2)-REPS(II+6))
      XT=RGEOM(2)/2.*SI-Y1
      SIG(II+3)=E*(ENTH(1)-(-XT*TEMP(1)+Y1*TEMP(2))*ENTH(2)-REPS(II+3))
      II = II+1
      IF (SI.LE.0.0) GO TO 720
      SI = -SI
      GO TO 710
720 CONTINUE
      GO TO 990

C
C T-SECTION
C
800 CONTINUE
      X1 = RGEOM(2)/2.0*(RGEOM(2)*RGEOM(4)+2.0*RGEOM(1)*RGEOM(3))/

```

1	(RGEOM(2)*RGEOM(4)+RGEOM(1)*RGEOM(3))	3201670
	DO 820 L=1,2	3201680
	SI = AA(3,L)	3201690
810	XT = X1-RGEOM(2)	3201700
	YT = RGEOM(1)/2.0*SI	3201710
	SIG(II) = E*(ENTH(1)-(-XT*TEMP(1)+YT*TEMP(2))*ENTH(2)-REPS(II))	3201720
	XT = RGEOM(2)/2.0*(SI-1.0)+X1	3201730
	SIG(II+3)=E*(ENTH(1)+XT*TEMP(1)*ENTH(2)-REPS(II+3))	
	II = II+1	3201750
	IF (SI.LE.0.0) GO TO 820	3201760
	SI = -SI	3201770
	GO TO 810	3201780
820	CONTINUE	3201790
	GO TO 990	3201800
C		3201810
C	RIGHT ANGULAR SECTION	3201820
C		3201830
900	CONTINUE	3201840
	X1=RGEOM(2)/2.*(RGEOM(2)*RGEOM(4)+2.*RGEOM(1)*RGEOM(3))/(RGEOM(2)	
1	*RGEOM(4)+RGEOM(1)*RGEOM(3))	
	Y1=RGEOM(1)**2*RGEOM(3)/2./(RGEOM(1)*RGEOM(3)+RGEOM(2)*RGEOM(4))	
	DO 920 L=1,2	3201880
	SI = AA(3,L)	3201890
910	XT = X1-RGEOM(2)	3201900
	YT = RGEOM(2)/2.0*(SI-1.0)+Y1	3201910
	SIG(II) = E*(ENTH(1)-(-XT*TEMP(1)+YT*TEMP(2))*ENTH(2)-REPS(II))	3201920
	XT = RGEOM(2)/2.0*(SI-1.0)+X1	3201930
	YT = Y1	3201940
	SIG(II+3)=E*(ENTH(1)-(-XT*TEMP(1)+YT*TEMP(2))*ENTH(2)-REPS(II+3))	
	II = II+1	3201960
	IF (SI.LE.0.0) GO TO 920	3201970
	SI = -SI	3201980
	GO TO 910	3201990
920	CONTINUE	3202000
	GO TO 990	3202010
990	RETURN	3202020
	END	3202030

## SUBROUTINE STRMAT

The region stiffness matrices, XKR, and the region load matrices, XLR, are passed from REGMAT to STRMAT via Tape #4 and Tape #8, and are placed in the XKSTOT array and the XLSTOT array, respectively. A matrix, BCD, is formed to represent the boundary conditions, and, if kinematic links occur between regions, the RKL matrix is developed to represent this situation. The subroutine RINGER is again called for discrete ring matrices.

As a result of appropriate matrix operations, a reduced structure stiffness matrix is formed. The solution of the problem is obtained by again calling the routine SYMSOC. This produces the region end deflection array, DRE.

## FORTRAN CODE

## ENGINEERING SYMBOLS (REF. 1)

BCD MATRIX

 $[BC]$ 

BCT MATRIX

 $[BC]^T$ 

XST MATRIX

 $\hat{[K]}_T$ 

XKF MATRIX

 $\hat{[K]}_F$ 

A MATRIX

 $\hat{[A]}_F$ 

XSL MATRIX

 $\hat{[L]}_T$ 

XLS ARRAY

 $\hat{\{L\}}_F$ 

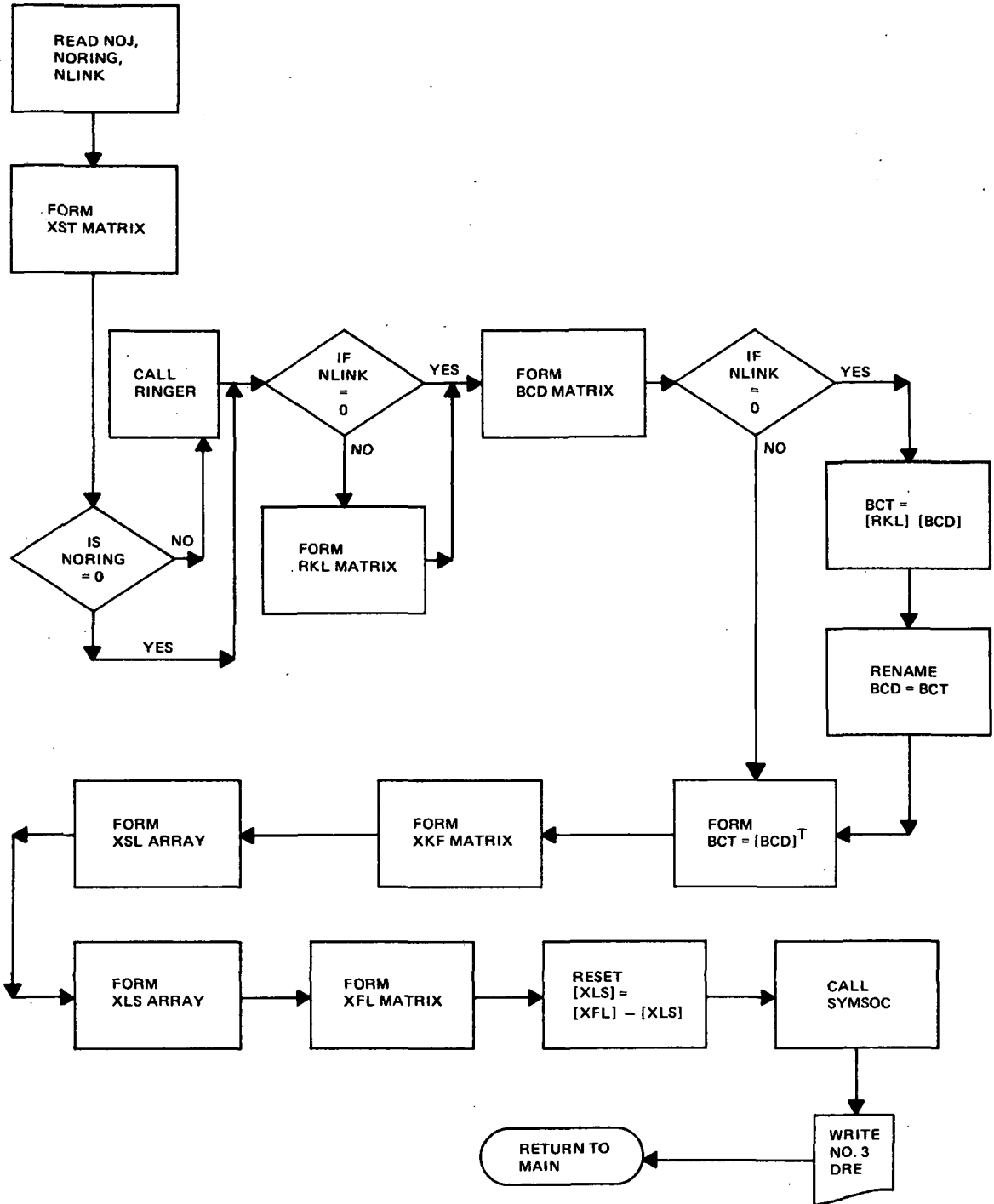
XFL ARRAY

 $\hat{\{F\}}_F$ 

DRE ARRAY

 $\hat{\{\Delta\}}_T$

STRMAT





```

FOR, IS STRMAT, STRMAT
SUBROUTINE STRMAT
INTEGER SAVJTC, SAVSTP, Q, THICK
INTEGER XN1, XN
COMMON STORY(16), XMAT(270,10), STD(10), SADUS(30), RADUS(30)
COMMON TADUS(30), UADUS(30), SAVTIC(900)
COMMON XN, TEFREE, TIC, PHI, STOP, RESTOP, RTICK, G1, XNL(3), NH
COMMON NST(30), NKL(30), NXMAT(20), SAVJTC(30), SAVSTP(30), JRTIC(30)
COMMON JRSTOP(30), NREG, NMPT, NRC, NSC, NIX, IERROR, KGEOM, IGEOM, ISTTAB
COMMON KELVIN, IBEGIN, NPROB, NSEG, NERROR, Q, THICK, NOJS, NLINKS, NLCASE
COMMON NTSKL, NZ, NBCT, LINPUT, NTRKL, NPASS, XN1, KBC, NRINGS
COMMON LODE, ICYCLE, LDISTL
COMMON /ARING/ NRING(28), AMAT(30,8), RSIG(12), REPS(12), RALPH(12),
C RBAPH(12)
COMMON /PLS/ OMEGA, IWORD, XMERD, XPRES, XMONT
COMMON /CDISP/ P, PMAX, DELP, DELP1, YEPS, ZEPS
DIMENSION SCLA(128), LOC(128)
DIMENSION ICOL(10)
DIMENSION RKL(120,120), OPEN(4,4)
DIMENSION DCP(4), BCD(124,124), TEMP(124), BCT(124), XKF(128), BC(128)
DIMENSION A(124,124), XSL(124,1), XFL(124,1), DRE(128,1), BCA(128)
DIMENSION XKR(8,8), XSTR(128), XLS(124,1), XLR(8,1)
DIMENSION XST(124,124), XSTBC(124,124), TEMP1(124)
DIMENSION RNGTHOT(4,4), RNGTHOD(4,28), JTNO(28)
DIMENSION COLTTL(2)
DIMENSION LEAD(1)
EQUIVALENCE (XST(1),BCD(1),A(1),XSTBC(1),RKL(1))
EQUIVALENCE (XSTR(1),XKF(1),XFL(1),XSL(1),DRE(1),SCLA(1),
1 TEMP(1),OPEN(1))
EQUIVALENCE (XKR(1),XLR(1),BC(1),BCT(1),BCA(1),TEMP1(1),LOC(1))
DATA COLTTL/4H CO,4HLUMN/
REWIND 2
REWIND 3
REWIND 4
REWIND 8
REWIND 9
REWIND 14
1 FORMAT(1H ,8(E14.7,2X)/(3X,8(E14.7,2X)))
101 FORMAT(3I5,16A4)
IF (NH.EQ.0.OR.IBEGIN.EQ.1) WRITE(6,1726)
1726 FORMAT(1H1)
IF (NH.NE.0) GO TO 1700
READ(5,101) NOJ,NORING,NLINK
NOJS = NOJ
NLINKS = NLINK
NRINGS = NORING
GO TO 1701
1700 NOJ = NOJS
NLINK = NLINKS
NORING = NRINGS
1701 CONTINUE
NH4=4
NH8=8
NJTNH4=NOJ*NH4
DO 102 J=1,NJTNH4
DO 102 I=1,NJTNH4
102 XST(I,J)=0.0
DO 100 NR=1,NREG
READ(4) ((XKR(I,J),J=1,8),I=1,8)
J1=JRTIC(NR)
J2=JRSTOP(NR)
II=4*(J1-1)
1600010
1600020
1600030
1600040
1600050
1600060
1600070
1600080
1600090
1600100
1600110
1600120
1600130
1600140
1600150
1600160
1600170
1600180
1600190
1600200
1600210
1600220
1600230
1600240
1600250
1600260
1600270
1600280
1600290
1600300
1600310
1600320
1600330
1600340
1600350
1600360
1600370
1600380
1600390
1600400
1600410
1600420
1600430
1600440
1600450
1600460
1600470
1600480
1600490
1600500
1600510
1600520
1600530
1600540
1600550
1600560
1600570
1600580
1600590
1600600
1600610

```

450	JJ=4*(J2-1)+1	1600620
	II=II+1	1600630
	DO 460 JK=1,4	1600640
	GO TO (451,452,453,454),JK	1600650
451	IX=II	1600660
	IND=II	1600670
	DO 461 I=1,4	1600680
	DO 461 J=1,4	1600690
461	OPEN(I,J)=XKR(I,J)	1600700
	GO TO 455	1600710
452	IX=II	1600720
	IND=JJ	1600730
	DO 462 I=1,4	1600740
	DO 462 J=1,4	1600750
462	OPEN(I,J)=XKR(I,J+4)	1600760
	GO TO 455	1600770
453	IX=JJ	1600780
	IND=II	1600790
	DO 463 I=1,4	1600800
	DO 463 J=1,4	1600810
463	OPEN(I,J)=XKR(I+4,J)	1600820
	GO TO 455	1600830
454	IX=JJ	1600840
	IND=JJ	1600850
	DO 464 I=1,4	1600860
	DO 464 J=1,4	1600870
464	OPEN(I,J)=XKR(I+4,J+4)	1600880
455	DO 456 I=1,4	1600890
	JX=IND	1600900
	DO 457 J=1,4	1600910
	XST(IX,JX)=XST(IX,JX)+OPEN(I,J)	1600920
457	JX=JX+1	1600930
456	IX=IX+1	1600940
460	CONTINUE	1600950
100	CONTINUE	1600960
	IF (NORING.EQ.0) GO TO 1170	1600970
	MFLG = 2	1600980
	DO 1211 J=1,NORING	1600990
	CALL RINGER (Q,XN,RNGTOT,RNGLOD,J,SADUS,UADUS,JRTIC,JRSTOP,JTNO,	1601000
	1 KBC,XNL,MFLG,NREG,ICYCLE,IBEGIN,LDISTL)	1601010
	JT = 4*(JTNO(J)-1)	1601020
	DO 1220 I=1,4	1601030
	DO 1220 IK=1,4	1601040
1220	XST(JT+I,JT+IK) = XST(JT+I,JT+IK)+RNGTOT(I,IK)	1601050
1211	CONTINUE	1601060
	IF (Q.NE.5) GO TO 1170	1601070
	WRITE(6,300)	1601080
300	FORMAT(///)	1601090
	READ(5,2000)	1601100
2000	FORMAT(1X)	1601110
1170	CONTINUE	1601120
	DO 107 I=1,NJTNM4	1601130
107	WRITE (2) (XST(I,J),J=1,NJTNM4)	1601140
	REWIND 2	1601150
	REWIND 4	1601160
	IF (NH.NE.0) GO TO 3200	1601170
C	GENERATION OF BC BOUNDARY CONDITION SCRAMBLING MATRIX	1601180
	WRITE(6,347) NOJ,NLINK	1601190
347	FORMAT(///51X30HINPUT DATA FOR REGION COUPLING///31X24HNUMBER OF	1601200
	1REGION JOINTS ,I3,14X26HNUMBER OF KINEMATIC LINKS ,I3///44X6HREGIO	1601210
	2N11X8HJOINT(I)11X8HJOINT(J)///)	1601220

DO 348 I=1,NREG	1601230
KTIC=JRTIC(I)	1601240
KSTOP=JRSTOP(I)	1601250
WRITE(6,349) I,KTIC,KSTOP	1601260
349 FORMAT(46X,I2,2(16X,I3))	1601270
348 CONTINUE	1601280
IF(NLINK.EQ.0) GO TO 3108	1601290
DO 756 I=1,NJTNH4	1601300
DO 756 J=1,NJTNH4	1601310
756 RKL(I,J)=0.0	1601320
DO 757 I = 1,NJTNH4	1601330
757 RKL(I,I) = 1.0	1601340
DO 789 I=1,4	1601350
DO 789 J=1,4	1601360
789 OPEN(I,J)=0.0	1601370
OPEN(2,2) = 1.0	1601380
OPEN(3,3) = 1.0	1601390
OPEN(4,4) = 1.0	1601400
WRITE(6,1824)	1601410
1824 FORMAT(//60X,12HREGION LINKS//43X,8HJOINT(J),5X,8HJDINT(I),	1601420
15X,20HANGLE OF ORIENTATION)	1601430
DO 502 NRIG=1,NLINK	1601440
READ(5,503) JD,JI,COTAN	1601450
503 FORMAT(2I2,E14.7)	1601460
WRITE(6,1828) JD,JI,COTAN	1601470
1828 FORMAT(46X,I2,11X,I2,11X,E14.7)	1601480
IF (SIN(COTAN).NE.0.0) GO TO 1829	1601490
OPEN(1,1) = 1.0	1601500
OPEN(2,4) = 0.0	1601510
OPEN(3,4) = 0.0	1601520
GO TO 1830	1601530
1829 CONTINUE	1601540
COTAN = COS(COTAN)/SIN(COTAN)	1601550
OPEN(1,1) = SADUS(JD) / SADUS(JI)	1601560
OPEN(2,4) = - (SADUS(JD)-SADUS(JI))	1601570
OPEN(3,4) = - OPEN(2,4)* COTAN	1601580
1830 CONTINUE	1601590
IXX= JD*4-3	1601600
DO 504 I=1,4	1601610
JXX= JI*4-3	1601620
DO 505 J=1,4	1601630
RKL(IXX,JXX)=OPEN(I,J)	1601640
505 JXX=JXX+1	1601650
504 IXX=IXX+1	1601660
502 CONTINUE	1601670
READ(5,2000)	1601680
DO 781 I=1,NJTNH4	1601690
781 WRITE(3) (RKL(I,J),J=1,NJTNH4)	1601700
REWIND 3	1601710
3108 CONTINUE	1601720
DO 108 J=1,NJTNH4	1601730
DO 108 I=1,NJTNH4	1601740
108 BCD(I,J)=0.0	1601750
ICR =1	1601760
WRITE(6,2372)	1601770
2372 FORMAT(/////57X19HBOUNDARY CONDITIONS//30X5HJOINTSX7HDELTA T,5X,7	1601780
1HDELTA Z,5X,7HDELTA R,5X,7H THETA ,7X,11HANGLE ALPHA)	1601790
DO 109 J=1,NOJ	1601800
READ (5,110) JN,DLP(1),DLP(2),DLP(3),DLP(4),ANGLE	1601810
110 FORMAT (I2,4F2.0,E14.1)	1601820
I1 = DLP(1)	1601830
I2 = DLP(2)	1601840

I3 = DLP(3)	1601850
I4 = DLP(4)	1601860
WRITE(6,2373) JN,I1,I2,I3,I4,ANGLE	1601870
2373 FORMAT(/31X,I3,9X,I2,10X,I2,10X,I2,10X,I2, 7X,E14.7)	1601880
II = (4*JN)-3	1601890
DO 121 I=1,4	1601900
IF(DLP(I)-1.0) 113,114,115	1601910
115 IF(DLP(I)-2.0) 116,116,117	1601920
114 BCD(II,ICR)=1.0	1601930
GOTO 118	1601940
116 BCD(II,ICR)=SIN(ANGLE)	1601950
BCD(II+1,ICR)= -COS(ANGLE)	1601960
GOTO 118	1601970
117 BCD(II-1,ICR)=COS(ANGLE)	1601980
BCD(II,ICR)=SIN(ANGLE)	1601990
118 ICR=ICR+1	1602000
113 II=II+1	1602010
121 CONTINUE	1602020
109 CONTINUE	1602030
READ(5,2000)	1602040
ICR=ICR-1	1602050
NZ=ICR	1602060
IF(NLINK.EQ.0) GO TO 3124	1602070
DO 783 N=1,NJTNH4	1602080
READ(3) (TEMP(M),M=1,NJTNH4)	1602090
DO 782 J=1,NZ	1602100
BCT(J)=0.0	1602110
DO 782 I=1,NJTNH4	1602120
782 BCT(J)=BCT(J)+TEMP(I)*BCD(I,J)	1602130
783 WRITE (4) (BCT(L),L=1, NZ)	1602140
REWIND 3	1602150
REWIND 4	1602160
DO 126 M=1,NJTNH4	1602170
126 READ(4) (BCD(M,N),N=1,NZ)	1602180
C AT THIS POINT THE BCD ARRAY IS THE PRODUCT OF RKL AND BCD ARRAYS	1602190
3124 CONTINUE	1602200
DO 124 J=1,NZ	1602210
124 WRITE(14) (BCD(I,J),I=1,NJTNH4)	1602220
DO 125 I=1,NJTNH4	1602230
125 WRITE(14) (BCD(I,J),J=1,NZ)	1602240
REWIND 14	1602250
REWIND 4	1602260
GO TO 3201	1602270
3200 DO 3300 J=1,NZ	1602280
3300 READ(14) (BCD(I,J),I=1,NJTNH4)	1602290
REWIND 14	1602300
3201 CONTINUE	1602310
DO 180 L=1,NJTNH4	1602320
READ (2) (XSTR(J),J=1,NJTNH4)	1602330
DO 184 M=1,NZ	1602340
TEMP1(M) = 0.0	1602350
DO 181 N=1,NJTNH4	1602360
181 TEMP1(M) = TEMP1(M)+XSTR(N)*BCD(N,M)	1602370
184 CONTINUE	1602380
WRITE(4) (TEMP1(I),I=1,NZ)	1602390
180 CONTINUE	1602400
REWIND 4	1602410
DO 183 II=1,NJTNH4	1602420
183 READ (4) (XSTBC(II,JJ),JJ=1,NZ)	1602430
REWIND 4	1602440
DO 182 N=1,NZ	1602450

READ(14) (BCT(J),J=1,NJTNH4)	1602460
DO 185 M=1,NZ	1602470
XKF(M)=0.0	1602480
DO 186 K=1,NJTNH4	1602490
186 XKF(M)=XKF(M)+BCT(K)*XSTBC(K,M)	1602500
185 CONTINUE	1602510
WRITE (4) (XKF(I),I=1,NZ)	1602520
182 CONTINUE	1602530
REWIND 2	1602540
REWIND 4	1602550
DO 187 I=1,NZ	1602560
187 READ(4) (A(I,J),J=1,NZ)	1602570
IF (IBEGIN.EQ.0.OR.LINPUT.EQ.0) GO TO 1750	1602580
WRITE(6,1726)	1602590
WRITE(6,2365)	1602600
2365 FORMAT(50X,29H THE REDUCED STIFFNESS MATRIX/)	1602610
NUMBER = 2	1602620
JJ = 0	1602630
JJJ = 0	1602640
1725 JJ = JJJ + 1	1602650
JJJ = JJJ + 8	1602660
MM = 8	1602670
IF (JJJ.GT.NZ) MM=8-(JJJ-NZ)	1602680
MMM = JJ	1602690
IF(JJJ.GT.NZ) JJJ=NZ	1602700
DO 1721 M=1,MM	1602710
ICOL(M)=MMM	1602720
1721 MMM = MMM + 1	1602730
NUMBER = NUMBER + 3	1602740
WRITE(6,1729) ((COLTTL,ICOL(M)),M=1,MM)	1602750
1729 FORMAT(/10H ROW ,8(2A4,1X,13,3X)/)	1602760
DO 1722 I=1,NZ	1602770
NUMBER = NUMBER + 1	1602780
WRITE(6,1728)I,(A(I,J),J=JJ,JJJ)	1602790
1728 FORMAT(3X,13,4X,8(E14.7,1X))	1602800
IF(NUMBER.LT.55) GO TO 1722	1602810
NUMBER = 3	1602820
WRITE(6,1726)	1602830
WRITE(6,1729) ((COLTTL,ICOL(M)),M=1,MM)	1602840
1722 CONTINUE	1602850
IF(JJJ.NE.NZ) GO TO 1725	1602860
1750 CONTINUE	1602870
REWIND 14	1602880
DO 991 J=1,NPROB	1602890
DO 991 I=1,NJTNH4	1602900
991 XSL(I,J) = 0.0	1602910
1001 DO 777 NR=1,NREG	1602920
J1 = JRTIC(NR)	1602930
J2 = JRSTOP(NR)	1602940
READ(8) ((XLR(I,J),J=1,NPROB),I=1,NH8)	1602950
DO 777 N2 = 1,2	1602960
GOTO (11,12),N2	1602970
11 II = (J1-1)*NH4+1	1602980
III= II+NH4-1	1602990
GOTO 3	1603000
12 II = (J2-1)*4+1	1603010
III= II+NH4-1	1603020
3 DO 777 J=1,NPROB	1603030
I=0	1603040
IF(N2.EQ.2) I=NH4	1603050
DO 777 IL=II,III	1603060
I=I+1	1603070

777	XSL(IL,J) = XSL(IL,J)+XLR(I,J)	1603080
	IF (NORING.EQ.0) GO TO 1150	1603090
	DO 1225 J=1,NORING	1603100
	JT = 4*(JTNO(J)-1)	1603110
	DO 1227 I=1,4	1603120
	DO 1226 IK=1,NPROB	1603130
1226	XSL(JT+I,IK) = XSL(JT+I,IK)+RNGLOD(I,J)	1603140
1227	CONTINUE	1603150
1225	CONTINUE	1603160
1150	CONTINUE	1603170
	DO 876 N=1,NZ	1603180
	READ(14) (BCT(J),J=1,NJTNH4)	1603190
	DO 717 M=1,NPROB	1603200
	XLS(N,M) = 0.0	1603210
	DO 806 K=1,NJTNH4	1603220
806	XLS(N,M) = XLS(N,M) + BCT(K)*XSL(K,M)	1603230
717	CONTINUE	1603240
876	CONTINUE	1603250
	DO 301 J=1,NPROB	1603260
	DO 301 I=1,NZ	1603270
301	XFL(I,J) = 0.0	1603280
	IF (LDISTL.EQ.1) GO TO 360	1603290
	READ(5,302) LINLOD,(STORY(I),I=1,16)	1603300
302	FORMAT(I4,16A4)	1603310
	WRITE(LODE) LINLOD	1603320
	GO TO 361	1603330
360	READ(LODE) LINLOD	1603340
361	CONTINUE	1603350
	IF (LINLOD.EQ.0) GO TO 303	1603360
	IF (ICYCLE.EQ.1.OR.NH.EQ.0) WRITE(6,341)	1603370
341	FORMAT(1H1///57X,19HEXTERNAL LINE LOADS///36X,14HPROBLEM NUMBER,7X	1603380
	120HPOINT OF APPLICATION,7X,12HAPPLIED LOAD//)	1603390
	IF (LDISTL.EQ.1) GO TO 362	1603400
	JEXT2 = 1	1603410
	DO 304 N=1,LINLOD	1603420
	READ(5,305) JEXT1,XFL(JEXT1,JEXT2)	1603430
305	FORMAT(5X,I5,E14.7)	1603440
	IF (ICYCLE.EQ.1.OR.IBEGIN.EQ.1)	1603450
	1WRITE(6,342) JEXT2,JEXT1,XFL(JEXT1,JEXT2)	1603460
342	FORMAT(41X,I3,22X,I3,15X,E14.7)	1603470
304	CONTINUE	1603480
	WRITE(LODE) ((XFL(I,J),I=1,NZ),J=1,NPROB)	1603490
	GO TO 303	1603500
362	READ(LODE) ((XFL(I,J),I=1,NZ),J=1,NPROB)	1603510
303	CONTINUE	1603520
	IF (LDISTL.NE.1) READ(5,2000)	1603530
306	CONTINUE	1603540
	DO 811 J=1,NPROB	1603550
	DO 811 I=1,NZ	1603560
811	XLS(I,J) = XFL(I,J)*DELP-XLS(I,J)	1603570
	DO 520 J=1,NPROB	1603580
	DO 530 I=1,NZ	1603590
	IF (XLS(I,J).NE.0.0) GO TO 540	1603600
530	CONTINUE	1603610
	LEAD(J) = NZ	1603620
	GO TO 520	1603630
540	LEAD(J) = I	1603640
520	CONTINUE	1603650
	CALL SYMSOC (A,A,NZ,0,XLS,NPROB,LEAD,124,0.0,NIX)	1603660
	IF (NIX.NE.0) GO TO 8777	1603670
	DO 812 J=1,NJTNH4	1603680

READ(14) (BC(K),K=1,NZ)	1603690
DO 813 M=1,NPROB	1603700
DRE(J,M)=0.0	1603710
DO 813 N=1,NZ	1603720
813 DRE(J,M) = DRE(J,M)+BC(N)*XLS(N,M)	1603730
812 CONTINUE	1603740
IF (NH.NE.0.AND.(LINPUT.NE.1.OR.IBEGIN.NE.1)) GO TO 1776	1603750
WRITE(6,1726)	1603760
WRITE(6,2368)	1603770
2368 FORMAT(31X,70HTHE EXPANDED REGION JOINT DISPLACEMENT MATRIX (REGIO	1603780
IN END DEFLECTIONS))	1603790
WRITE(6,1770)	1603800
1770 FORMAT(/,14X,5HJOINT,14X,7HPROBLEM,13X,7HDELTA T,13X,7HDELTA Z,13X	1603810
1,7HDELTA R,11X,11HOMEGA-THETA)	1603820
NUMBER = 4	1603830
KK=-3	1603840
DO 1735 J=1,NOJ	1603850
NUMBER = NUMBER + NPROB + 1	1603860
IF(NUMBER.LT.56) GO TO 1745	1603870
WRITE(6,1726)	1603880
WRITE(6,1770)	1603890
NUMBER=2+NPROB+3	1603900
1745 KK=KK+4	1603910
KKK=KK+3	1603920
WRITE(6,1739)	1603930
1739 FORMAT(1H )	1603940
DO 1764 L=1,NPROB	1603950
WRITE(6,1765) J,L,(DRE(K,L),K=KK,KKK)	1603960
1765 FORMAT(15X,12,18X,12,9X,4(3X,E14.7,3X))	1603970
1764 CONTINUE	1603980
1735 CONTINUE	1603990
1776 CONTINUE	1604000
DO 71 NR=1,NREG	1604010
DO 71 K=1,2	1604020
II =(JRTIC(NR) - 1) *4 +1	1604030
IF(K.EQ.2) II= JRSTOP(NR)*4-3	1604040
III= II + 3	1604050
DO 71 I = II,III	1604060
71 WRITE(3) (DRE(I,J),J=1,NPROB)	1604070
REWIND 2	1604080
REWIND 3	1604090
REWIND 4	1604100
GOTO 7	1604110
8777 IERROR =8777	1604120
NERROR=32	1604130
NIX=1	1604140
7 RETURN	1604150
END	1604160

### SUBROUTINE INITAL

As a result of the matrix operations performed in REGMAT, the SKI22, the XK2221, and the XK22L2 arrays for each region are passed to INITAL. The XK1112 and XL1 arrays for each segment, resulting from the matrix procedures in SEGMAT, are also passed to INITAL. The region end deflection matrices, DRE, which were formed in STRMAT are transmitted to INITAL.

Following appropriate matrix operations upon these arrays, the force initial conditions, the FICS array, and the deflections initial conditions, the DICS array, are produced. These arrays combine to form the YICS matrix, which contains the true initial conditions for the structure to be analyzed.

The pertinent counters in the subroutine are:

NS = segment counter

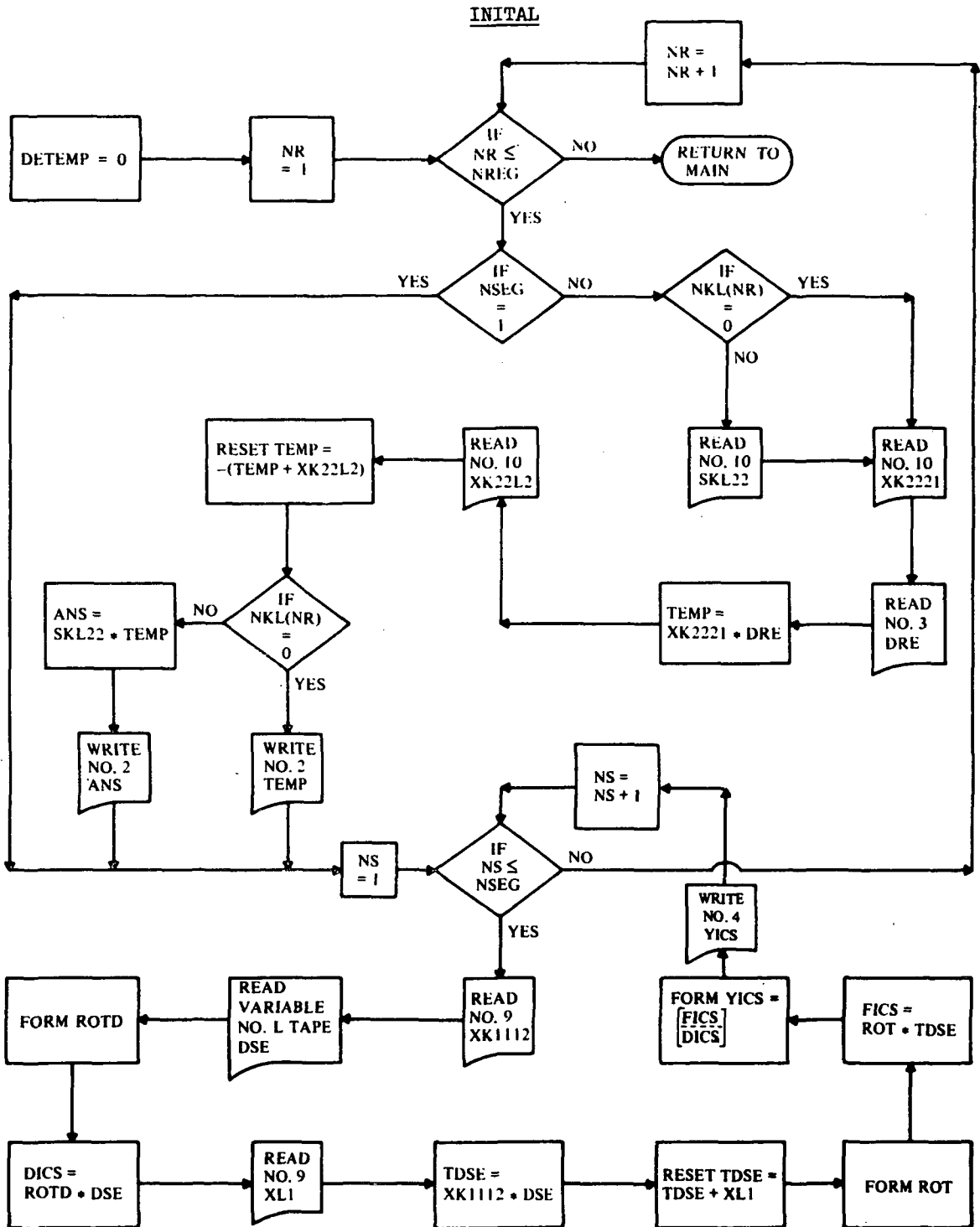
NR = region counter



FORTRAN CODE

ENGINEERING SYMBOLS (REF. 1)

XK2221 MATRIX	$\begin{bmatrix} \hat{K}_{22} \end{bmatrix}^{-1} \quad \begin{bmatrix} \hat{K}_{21} \end{bmatrix}$
XK22L2 MATRIX	$\begin{bmatrix} \hat{K}_{22} \end{bmatrix}^{-1} \quad \begin{bmatrix} \hat{L} \end{bmatrix}$
DSE ARRAY	$\{\Delta\}$
XK1112 MATRIX	$\begin{bmatrix} k_{ii} &   & k_{ij} \end{bmatrix}$
ROTD MATRIX	$[\text{IDT}]^T$
DICS ARRAY	$\{\delta(i)\}$
XL1 ARRAY	$\{\mathcal{L}(i)\}$
ROT MATRIX	$[\text{IFT}]^T$
FICS ARRAY	$\{f(i)\}$



```

FOR, IS INITAL, INITAL
SUBROUTINE INITAL
INTEGER SAVJTC, SAVSTP, Q, THICK
INTEGER XN1, XN
COMMON STORY(16), XMAT(270, 10), STD(10), SADUS(30), RADUS(30)
COMMON TADUS(30), UADUS(30), SAVTIC(900)
COMMON XN, TEFREE, TIC, PHI, STOP, RESTOP, RTICK, GI, XNL(3), NH
COMMON NST(30), NKL(30), NXMAT(20), SAVJTC(30), SAVSTP(30), JRTIC(30)
COMMON JRSTOP(30), NREG, NMPT, NRC, NSC, NIX, IERROR, KGEOM, IGEOM, ISTTAB
COMMON KELVIN, IBEGIN, NPROB, NSEG, NERROR, Q, THICK, NOJS, NLINKS, NLCASE
COMMON NTSKL, NZ, NBCT, LINPUT, NTRKL, NPASS, XN1, KBC, NRINGS
COMMON LODE, ICYCLE, LDISTL
DIMENSION XK2221(112, 8), DRE(8, 1), TEMP(112, 1), XK22L2(112, 1)
DIMENSION XK1112(4, 8), DSE(8, 1), ROTD(4, 4), DICS(4, 1)
DIMENSION TDSE(8, 1), YICS(8, 1)
DIMENSION XL1(4, 1), ROT(4, 4), FICS(4, 1), SKL22(112, 112), ANS(112, 1)
EQUIVALENCE (ROTD(1), ROTD(1)), (TIC, TICK)
EQUIVALENCE (DSE(1), DRE(1)), (XK2221(1), XK22L2(1))
EQUIVALENCE (SKL22(1), XK1112(1)), (YICS(1), TDSE(1))
NH4 = 4
NH41 = NH4 + 1
NH8 = 8
NH81 = NH8 + 1
REWIND 2
REWIND 3
REWIND 4
REWIND 8
REWIND 9
REWIND 10
DO 100 NR = 1, NREG
NOJ = NST(NR) + NKL(NR) + 1
ISKL22 = 4 * (NOJ - 2)
JSKL22 = 4 * (NOJ - 2 - NKL(NR))
NJTNH4 = NOJ * NH4
M8 = 4 * (NOJ - NKL(NR)) - 8
NSEG = NST(NR)
IF (NSEG.EQ.1) GOTO 703
IF (NKL(NR).EQ.0) GO TO 415
READ(10) ((SKL22(I, J), J = 1, JSKL22), I = 1, ISKL22)
415 READ(10) ((XK2221(I, J), J = 1, NH8), I = 1, M8)
READ(10) (SAVJTC(I), SAVSTP(I), I = 1, NSEG)
703 DO 91 K = 1, 2
II = 1
IF (K.EQ.2) II = 5
III = II + 3
DO 91 I = II, III
91 READ(3) (DRE(I, J), J = 1, NPROB)
IF (NSEG.EQ.1) GOTO 999
DO 101 J = 1, NPROB
DO 101 I = 1, M8
TEMP(I, J) = 0.0
DO 101 K = 1, NH8
TEMP(I, J) = TEMP(I, J) + XK2221(I, K) * DRE(K, J)
101 CONTINUE
READ(10) ((XK22L2(I, J), J = 1, NPROB), I = 1, M8)
DO 102 J = 1, NPROB
DO 102 I = 1, M8
102 TEMP(I, J) = -(TEMP(I, J) + XK22L2(I, J))
IF (NKL(NR).EQ.0) GO TO 435
DO 445 I = 1, ISKL22

```

DO 445 J=1,NPROB	1700600
ANS(I,J)=0.0	1700610
DO 445 K = 1,JSKL22	1700620
445 ANS(I,J)=ANS(I,J)+SKL22(I,K)*TEMP(K,J)	1700630
435 DO 391 N=1,NSEG	1700640
IF((N.EQ.1.OR.N.EQ.NSEG).AND.SAVJTC(N).GT.SAVSTP(N)) GO TO 370	1700650
DO 398 K=1,2	1700660
IF (N.NE.1.OR.K.NE.1) GOTO 393	1700670
DO 394 I= 1,4	1700680
394 WRITE (2) (DRE(I,J),J=1,NPROB)	1700690
GO TO 398	1700700
393 IF(N.EQ.NSEG.AND.K.EQ.2) GOTO 395	1700710
IF (K.EQ.1) II = SAVJTC(N)*4-7	1700720
IF (K.EQ.2) II = SAVSTP(N)*4-7	1700730
III = II + 3	1700740
DO 397 I=II,III	1700750
IF (NKL(NR).EQ.0) GOTO 392	1700760
WRITE (2) (ANS(I,J),J=1,NPROB)	1700770
GOTO 397	1700780
392 WRITE (2) (TEMP(I,J),J=1,NPROB)	1700790
397 CONTINUE	1700800
GO TO 398	1700810
395 DO 396 I=5,8	1700820
396 WRITE (2) (DRE(I,J),J=1,NPROB)	1700830
398 CONTINUE	1700840
GO TO 391	1700850
370 IF(N.EQ.NSEG) GO TO 380	1700860
IF(NKL(NR).EQ.0) GO TO 375	1700870
DO 371 I=1,4	1700880
371 WRITE(2) (ANS(I,J),J=1,NPROB)	1700890
GO TO 376	1700900
375 DO 372 I=1,4	1700910
372 WRITE(2) (TEMP(I,J),J=1,NPROB)	1700920
376 DO 373 I=1,4	1700930
373 WRITE(2) (DRE(I,J),J=1,NPROB)	1700940
GO TO 391	1700950
380 CONTINUE	1700960
DO 381 I=5,8	1700970
381 WRITE(2) (DRE(I,J),J=1,NPROB)	1700980
IF(NKL(NR).EQ.0) GO TO 385	1700990
II = ISKL22-3	1701000
III = ISKL22	1701010
DO 382 I=II,III	1701020
382 WRITE(2) (ANS(I,J),J=1,NPROB)	1701030
GO TO 391	1701040
385 II = M8-3	1701050
III = M8	1701060
DO 383 I=II,III	1701070
383 WRITE(2) (TEMP(I,J),J=1,NPROB)	1701080
391 CONTINUE	1701090
REWIND 2	1701100
999 DO 201 NS=1,NSEG	1701110
READ (9) ((XK1112(I,J),J=1,NH8),I=1,NH4),IGEOM,G1	1701120
ISEG=0	1701130
NR1=NR-1	1701140
IF(NR1.EQ.0)GOTO8	1701150
DO 7 I=1,NR1	1701160
7 ISEG=ISEG+NST(I)	1701170
8 ISEG=ISEG+NS	1701180
TIC= SAVTIC(ISEG)	1701190
GO TO (21,22,23),IGEOM	1701200

21	SN = SIN(TIC)	1701210
	CS = COS(TIC)	1701220
	GO TO 25	1701230
22	SN = COS(1.570796-G1)	1701240
	CS = SIN(1.570796-G1)	1701250
	IF (G1.NE.0.0) GO TO 25	1701260
	SN = 0.0	1701270
	CS = 1.0	1701280
	GO TO 25	1701290
23	SN = 1.0	1701300
	CS = 0.0	1701310
25	CONTINUE	1701320
	IF (NSEG.EQ.1) GO TO 80	1701330
	DO 78 I = 1,8	1701340
78	READ (2) (DSE(I,J),J=1,NPROB)	1701350
80	CONTINUE	1701360
	DO 302 J=1,NH4	1701370
	DO 302 I=1,NH4	1701380
302	ROTD(I,J)=0.0	1701390
	DO 305 J=1,NH4,4	1701400
	ROTD(J,J)=1.0	1701410
	ROTD(J+1,J+2)=CS	1701420
	ROTD(J+2,J+1)=-CS	1701430
	ROTD(J+1,J+1)=-SN	1701440
	ROTD(J+2,J+2)=-SN	1701450
305	ROTD(J+3,J+3)=1.0	1701460
	DO 306 J=1,NPROB	1701470
	DO 306 I=1,NH4	1701480
	DICS(I,J)=0.0	1701490
	DO 306 K=1,NH4	1701500
306	DICS(I,J)=DICS(I,J)+ROTD(I,K)*DSE(K,J)	1701510
	READ(9) ((XL1(I,J),J=1,NPROB),I=1,NH4)	1701520
	DO 202 J=1,NPROB	1701530
	DO 202 I=1,NH4	1701540
	TDSE(I,J)=0.0	1701550
	DO 202 K=1,NH8	1701560
202	TDSE(I,J)=TDSE(I,J)+XK1112(I,K)*DSE(K,J)	1701570
	DO 203 J=1,NPROB	1701580
	DO 203 I=1,NH4	1701590
203	TDSE(I,J)=TDSE(I,J)+XL1(I,J)	1701600
	DO 301 J=1,NH4	1701610
	DO 301 I=1,NH4	1701620
301	ROTD(I,J)=0.0	1701630
	DO 204 J=1,NH4,4	1701640
	ROT(J,J)=-1.0	1701650
	ROT(J+1,J+2)=-CS	1701660
	ROT(J+2,J+1)=CS	1701670
	ROT(J+1,J+1)=SN	1701680
	ROT(J+2,J+2)=SN	1701690
204	ROT(J+3,J+3)=1.0	1701700
	DO 205 J=1,NPROB	1701710
	DO 205 I=1,NH4	1701720
	FICS(I,J)=0.0	1701730
	DO 205 K=1,NH4	1701740
205	FICS(I,J)=ROT(I,K)*TDSE(K,J)+FICS(I,J)	1701750
	DO 402 J=1,NPROB	1701760
	DO 402 I=1,NH4	1701770
	II=I+NH4	1701780
	YICS(I,J)=FICS(I,J)	1701790
402	YICS(II,J)=DICS(I,J)	1701800
	WRITE(4) ((YICS(I,J),I=1,8),J=1,NPROB)	1701810

201 CONTINUE  
REWIND 2  
100 CONTINUE  
REWIND 1  
REWIND 4  
REWIND 8  
RETURN  
END

1701820  
1701830  
1701840  
1701850  
1701860  
1701870  
1701880  
1701890

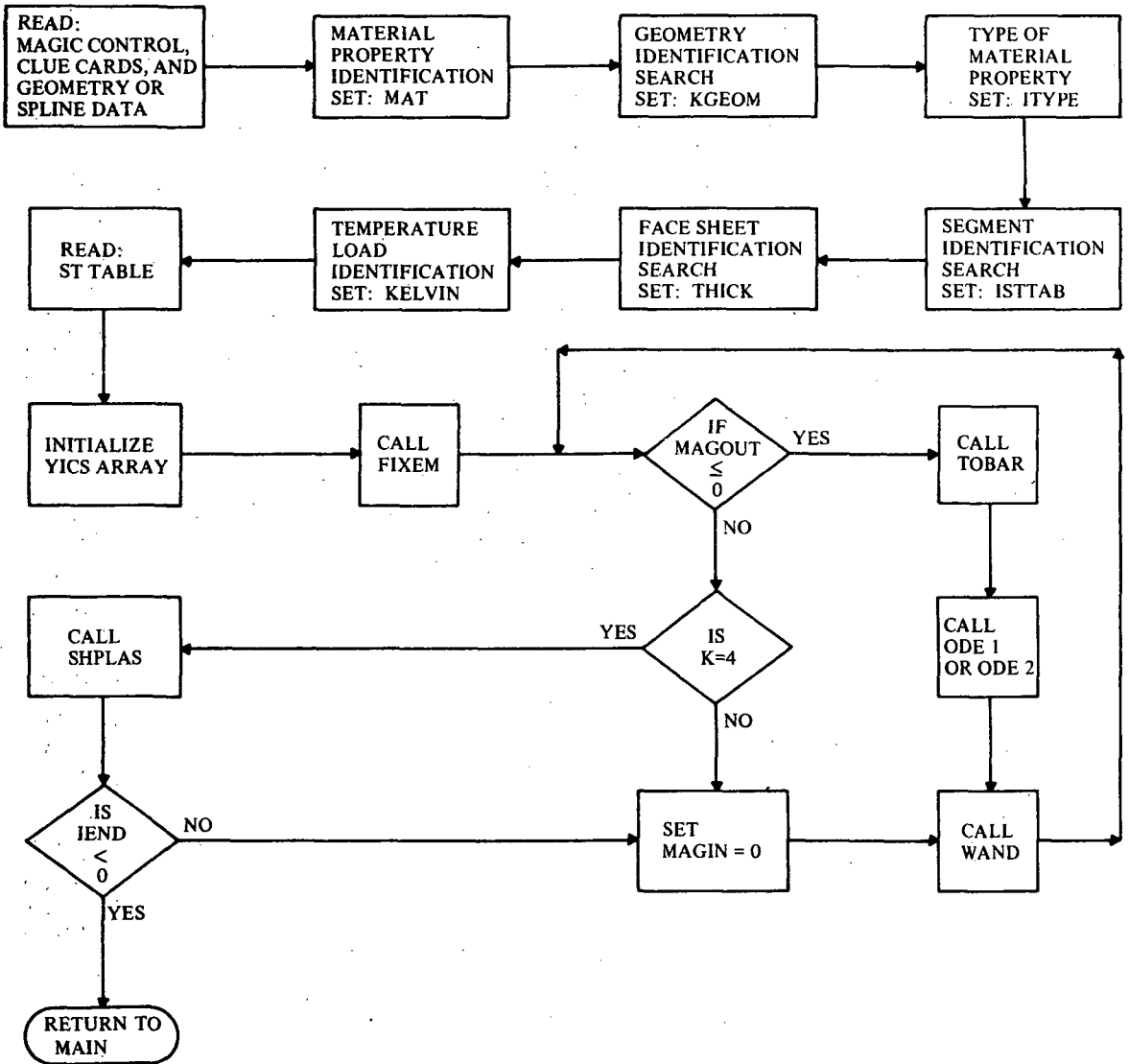
### SUBROUTINE LEBEGE

The subroutine link LEBEGE receives the YICS array for each segment from INITAL via Tape #4. The subroutine FIXEM is called to integrate the differential equations of each segment, under true load conditions. FIXEM is identical to subroutine SETUP, while WAND corresponds to subroutine MAGIC and only consideration of the OVERLAY structure dictates the change in names. The subroutines TOBAR, TEMOEG, PLYCO, and PLYNE are similarly equivalent to ROBOT, GEOMET, PLICO, and PLINE discussed previously.

The results of the final integration sequence are the forces and deflections at the beginning, intermediate, and end points of each segment. These are always the incremental values. The updating for current load step is accomplished in subroutine SHPLAS.

Subroutine GRAPH: This subroutine controls the system graphical routines. GRAPH prints the titles and passes the graphical display points to the necessary system routines, which utilize a Stromberg-Carlson 4020 plotter.

LEBEGE





```

FOR, IS LEBEGE, LEBEGE
SUBROUTINE LEBEGE
INTEGER SAVJTC, SAVSTP, Q, THICK
INTEGER XN
DOUBLE PRECISION YNEW, YPRED
COMMON STORY(16), XMAT(270, 10), STD(10), SADUS(30), RADUS(30)
COMMON TADUS(30), UADUS(30), SAVTIC(900)
COMMON XN, TEFREE, TIC, PHI, STOP, RESTOP, RTICK, G1, XNL(3), NH
COMMON NST(30), NKL(30), NXMAT(20), SAVJTC(30), SAVSTP(30), JRTIC(30)
COMMON JRSTOP(30), NREG, NMPT, NRC, NSC, NIX, IERROR, KGCOM, IGEOM, ISTTAB
COMMON KELVIN, IBEGIN, NPROB, NSEG, NERROR, Q, THICK, NOJS, NLINKS, NLCASE
COMMON NTSKL, NZ, NBCT, LINPUT, NTRKL, NPASS, XN1, KBC, NRINGS
COMMON LODE, ICYCLE, LDISTL
COMMON /ARING/ NRING(28), AMAT(30, 8), RSIG(12), REPS(12), RALPH(12),
C RBAPH(12)
COMMON /SNILPS/ ANG, PSI(100), RAD(100), CUR1(100), CUR2(100),
1 DR1DP(100), ZI(14), RI(14), NRZIN
COMMON /MAGIQ/ KKNT, TII, TIK, TOK, TOD
COMMON /LASTEQ/ YPRED(8), YDOT(8), YASAVE(8),
1 YANTH, YAMTH, YAMPT, YANPT, YAOPH, YAQPH, YAQTH, YAJPH,
2 S, SN, CS, SNSQ, CSSQ, TAN, SEC, CN, X1CS, X1SN, TN,
3 X1RO, X1ROSQ, X1SNRO, X1CSRO, CN1RO, SN1RO, CS1RO,
4 X1R1, X1R2, CS1R1, CS1R2, SN1R1, X1R1SQ, R2SQ, RO, BESQ,
5 ROSQ, XNSQ, BETA, R1, R2, S1, R1DOT, R1SQ,
6 XNTTH, XNTPH, XMTTH, XMTPH, XFTHLD, XFPHLD, XFZELD,
7 XMTHLD, XMPHLD, ETHET, EPHI, XGPT, ALPHTH, ALPHPH,
8 XNUTP, XNUPT, XC11, XC22, XC15, XD33, XD22, XD21, XD12,
9 XK11, XK12, XK21, XK22, XK33, XD11,
A H, I, SITIN, SITOUT, SIPIN, SIPOUT, TPTIN, TPTOUT,
B ZBRIN, ZBROUT, SCRIPA, SCRIP1, SIFIN, SIFOUT, TZEPH, TZETH
B ,XNPHI, BETTA, ZETTA, XC16
C ,RMOSS, RMOSN, YLDST, ROC, HP, FPLUH, GPLUH, TWON
D ,RMOSSY, RMOSNY, RMOSXY, RMONXY
D ,RMOSSNS, RMOSSS, SIGOXS, RMOSNR, RMOSSR, SIGOXR
COMMON /PLSTIC/ IO, JO, IOR, JOR, KORI, NEO
COMMON /PLS/ OMEGA, IWORD, XMERD, XPRES, XMONT
COMMON /WOOD/ SAVY(53), NPLEV, NLPO, NPLA(21), STR(6), SIGMA(3, 21),
C SEPS(3, 21), SALPH(3, 21), SBAPH(3, 21), STEPS(3, 21),
O EFF(21), STSRN(3), NPLAST(3), STSIG(3), STREPS(3),
M STALPH(3), STBAPH(3), EFFST(3), NPLEVS(3)
COMMON /CHAIN/ ZETA1(21), ZETA2(21), NODE, ALF(4), CE(4), NLRS, HI, HO, T
COMMON /CDISP/ P
COMMON /RWD/ ER, ES, CPH, CTH, APH, ATH, SPH, STH, ALPHS, ALPHR, TS, TR, SNB,
C CSB
COMMON /GRAFIX/ X(100), Y(100, 9), NGRAPH, LDEF(9), NGR, JCYC, NFLAG, JAM,
C JNSC
DIMENSION LST(13), YDEV(8), YICS(8), YNEW(8)
DIMENSION XKF(128), TBDEL(8), FWDEL(8), YCORR(8)
DIMENSION ST(30, 31), XLAYER(26)
EQUIVALENCE (YNEW(1), XKF(1))
REWIND 1
600 FORMAT(1H , 8(E14.7, 2X)/(3X, 8(E14.7, 2X)))
KSC = 0
JAM = 1
JNSC = 0
DO 451 I=1, NREG
451 KSC = KSC + NST(I)
LSC = 0
902 LSC = LSC + 1
JCYC = 0
1800010
1800020
1800030
1800040
1800050
1800060
1800070
1800080
1800090
1800100
1800110
1800120
1800130
1800140
1800150
1800160
1800170
1800180
1800190
1800200
1800210
1800220
1800230
1800240
1800250
1800260
1800270
1800280
1800290
1800300
1800310
1800320
1800330
1800340
1800350
1800360
1800370
1800380
1800390
1800400
1800410
1800420
1800430
1800440
1800450
1800460
1800470
1800480
1800490
1800500
1800510
1800520
1800530
1800540
1800550
1800560
1800570
1800580
1800590

```

XNTTH = 0.0	1800600
XNTPH = 0.0	1800610
XMTTH = 0.0	1800620
XMTPH = 0.0	1800630
NSC=LSC	1800640
JNSC=JNSC+1	1800650
IF(JNSC.LE.NST(JAM)) GO TO 1727	1800660
NRNG = NRNG(JAM)	1800670
IF (NRNG.EQ.0) GO TO 1900	1800680
DO 1901 I=1,NRNG	1800690
1901 READ(1) DUMLNK	1800700
1900 CONTINUE	1800710
NNSKL = NKL(JAM)	1800720
IF (NNSKL.EQ.0) GO TO 1724	1800730
DO 1725 I=1,NNSKL	1800740
1725 READ(1) DUMLNK	1800750
1724 CONTINUE	1800760
JAM=JAM+1	1800770
JNSC=1	1800780
1727 CONTINUE	1800790
READ(1) KGEOM,IGEOM,RGO,ANG,NLRS,STORY	1800800
READ(1) DTAU,DIFF,STEP,DELTA,NAPEX	1800810
IF (RGO.EQ.14.0) GO TO 182	1800820
READ(1) G1,G2,G3	1800830
GO TO 183	1800840
182 READ(1) NRZIN,(ZI(J),RI(J),J=1,NRZIN)	1800850
183 CONTINUE	1800860
READ(1) ITYPE,MAT,THICK,ISTTAB,KELVIN,KORI,TEFREE,NP,KLUE1,KLUE2,	1800870
1 IANLYZ,NROW	1800880
DIFF = 1.0E-04	1800890
EPSIL = 1.0E-05	1800900
ERR = 1.0 E-07	1800910
IF (NH.NE.0.AND.IBEGIN.NE.1) GO TO 1776	1800920
WRITE(6,1726)	1800930
1726 FORMAT(1H1)	1800940
IF(JNSC.EQ.1) WRITE(6,606) JAM,NST(JAM),NKL(JAM)	1800950
606 FORMAT(//58X,13HREGION NUMBER,I3//35X,10HTHERE ARE ,I2,14H SEGMENT	1800960
1S AND ,I2,35H KINEMATIC LINKS WITHIN THIS REGION)	1800970
I = RGO	1800980
WRITE(6,651) JNSC,I,NLRS	1800990
651 FORMAT(//13X,15HSEGMENT NUMBER ,I2,5X,13HSEGMENT CODE ,I2,5X,	1801000
1 14HNO. OF LAYERS ,I2)	1801010
1776 CONTINUE	1801020
NCONT = NROW	1801030
IF (NH.EQ.0.OR.IBEGIN.EQ.1) WRITE(6,655)	1801040
655 FORMAT(//42X,47HTABLE ORDER PHI OR S VS. CROSSECTION PROPERTIES)	1801050
DO 901 I=1,NROW	1801060
READ(1) (ST(I,J),J=1,NP)	1801070
IF (NH.NE.0.AND.IBEGIN.NE.1) GO TO 901	1801080
WRITE(6,600) (ST(I,J),J=1,NP)	1801090
901 CONTINUE	1801100
DO 750 JJ=1,12	1801110
750 LST(JJ) = 0	1801120
NLCS = NLCASE	1801130
NLPO = NLRS+1	1801140
KBC = NLPO	1801150
IF (THICK.NE.1) KBC = 2.0*NLPO	1801160
TAP1 = NLRS/2	1801170
DO 290 I=1,NLPO	1801180
TAP2 = I-1	1801190
ZETA1(I) = 1.0-TAP2/TAP1	1801200

```

290 ZETA2(I) = 1.0-FLOAT(I-1)/FLOAT(NLRS)      1801210
    K=NROW+1      1801220
    JJ=1          1801230
    JJJ=6        1801240
    MM=1         1801250
    DO 17 NLC=1,NLCS 1801260
    JT = JJ      1801270
    JTT= JJJ    1801280
    L=0         1801290
    READ(LODE) (LST(J),J=JJ,JJJ) 1801300
    IF(LST(JJ))8031,19,20 1801310
20 L = LST(JJ) 1801320
19 JJ=JJ+1     1801330
23 IF(LST(JJ))8031,22,21 1801340
21 L=L+1       1801350
22 IF(JJ.EQ.JJJ) GOTO 24 1801360
    JJ=JJ+1    1801370
    GOTO 23    1801380
24 IF (L.EQ.0) GO TO 668 1801390
    KK = K + L - 1 1801400
    DO 72 M=K,KK 1801410
    READ(LODE) (ST(M,J),J=1,NP) 1801420
72 CONTINUE    1801430
    IF (LST(JT).EQ.0) GO TO 660 1801440
    KZ = K + LST(1) -1 1801450
    K = KZ + 1 1801460
660 CONTINUE   1801470
    IF (NH.NE.0.AND.IBEGIN.NE.1) GO TO 665 1801480
    WRITE(6,661) 1801490
661 FORMAT(//31X,84HTABLE ORDER PHI OR S VS. DISTRIBUTED LOADS (F THE 1801500
    ITA, F PHI, F ZETA, M THETA, M PHI),) 1801510
    WRITE(6,1968) (LST(J),J=JT,JTT) 1801520
1968 FORMAT(27H LOAD IDENTIFICATION CLUES ,6I1/) 1801530
    DO 662 N=K,KK 1801540
662 WRITE(6,600) (ST(N,J),J=1,NP) 1801550
668 IF (NH.NE.0.AND.IBEGIN.NE.1) GO TO 665 1801560
    WRITE(6,7000) 1801570
7000 FORMAT(///3X,21HPHI (RAD. OR IN.) ,21HDEGRES 1801580
1      21HR ZERO ,21HBASE THICKNESS 1801590
2      21HSTEP ,21HEPSILON THETA IN / 1801600
3      3X,21HEPSILON THETA ,21HEPSILON PHI 1801610
4      21HGAMMA PHI THETA ,21HK PHI 1801620
5      21HK THETA ,21HEPSILON THETA OUT / 1801630
6      3X,21HU ,21HK PHI THETA 1801640
7      21HN THETA ,21HN PHI 1801650
8      21HN PHI THETA ,21HEPSILON PHI IN / 1801660
9      3X,21HV ,21HJ PHI STAR 1801670
A      21HM THETA ,21HM PHI 1801680
B      21HM PHI THETA ,21HEPSILON PHI OUT / 1801690
C      3X,21HW ,21HT PHI THETA 1801700
D      21HSIGMA THETA IN ,21HSIGMA PHI IN 1801710
E      21HTAU PHI THETA IN ,21HGAMMA PHI THETA IN / 1801720
F      3X,21HOMEGA THETA ,21HOMEGA PHI 1801730
G      21HSIGMA THETA OUT ,21HSIGMA PHI OUT 1801740
H      21HTAU PHI THETA OUT ,21HGAMMA PHI THETA OUT ) 1801750
    WRITE(6,7001) P 1801760
7001 FORMAT(///50X,'CYCLE',F8.0) 1801770
665 CONTINUE 1801780
71 K = K + L - LST(JT) 1801790
    JJ=JJJ+1 1801800
    JJJ=JJ+5 1801810

```

17	MM=MM+1	1801820
590	CONTINUE	1801830
	READ(1) IS,SAVJTC(1S),SAVSTP(1S),STORY	1801840
	NSAVE = NROW	1801850
	JJ=NPROB*6	1801860
	LT=0	1801870
	DO 15 J=1,JJ	1801880
15	LT=LT+LST(J)	1801890
	NTOTAL=LT+NSAVE	1801900
	NEQNS=8*NPROB	1801910
	TIC = ST(1,1)	1801920
	STOP = ST(1,NP)	1801930
	READ(4) (YICS(I),I=1,NEQNS)	1801940
	NCYC=0	1801950
	KKNT = 0	1801960
	NSAVE=NROW	1801970
	IEND=0	1801980
	NPR = 1	1801990
	PRINT=TIC	1802000
	DTA=DTAU	1802010
	DTAU=0.0	1802020
	READ(10) SAVY,NPLEV,NPLA,SIGMA,SALPH,SBAPH,STEPS,STR,EFF,STSRN,	1802030
	1 NPLAST,STSIG,STREPS,STALPH,STBAPH,NPLEVS,EFFST,SEPS	1802040
59	CALL FIXEM (MAGIN,MAGOUT,TIC,STEP,NEQNS,DTAU,EPSIL,DELTA,ERR,TIME,	1802050
	1 DTIME,YICS,YPRED,YCORR,YDOT,YNEW,YDEV,FWDDEL,TBDEL)	1802060
	GOTO 61	1802070
60	CALL WAND(MAGIN,MAGOUT,TIC,STEP,NEQNS,DTAU,EPSIL,DELTA,ERR,TIME,	1802080
	1 DTIME,YICS,YPRED,YCORR,YDOT,YNEW,YDEV,FWDDEL,TBDEL)	1802090
61	IF(MAGOUT.LE.0) GOTO 25	1802100
	IF(TIME.GT.STOP) GOTO 62	1802110
	IF(TIME.LT.STOP) GOTO 63	1802120
64	IEND=-1	1802130
	GOTO 67	1802140
62	IF(TIME.LE.(STOP+DIFF)) GOTO 64	1802150
	GOTO 8001	1802160
63	IF((STOP-DIFF).LE.TIME) GOTO 64	1802170
	IF((TIME+DTIME).GT.STOP) GOTO 65	1802180
	IF(PRINT.GT.TIME) GOTO 66	1802190
	PRINT=TIME+DTA	1802200
67	CONTINUE	1802210
	NPR = 1	1802220
	IF (TIME.EQ.TIC) NPR = 0	1802230
6450	IF(IEND.GT.0) GO TO 8002	1802240
	IF(IEND.LT.0) GOTO 150	1802250
	MAGIN = 0	1802260
	GO TO 60	1802270
66	MAGIN=0	1802280
	NPR = 0	1802290
	GOTO 60	1802300
65	DTIME=STOP-TIME	1802310
	DELTA=0.0	1802320
	GOTO 67	1802330
75	NCYC=NCYC+1	1802340
	IF (NCYC.NE.1.AND.KKNT.NE.4) GO TO 175	1802350
	IF ((TIME+STEP).GT.(STOP-DIFF)) NPR = 1	1802360
	CALL SHPLAS (NCYC,NAPEX,NPR,STEP)	1802370
	NPR = 0	1802380
175	MAGIN = -1	1802390
	GOTO 60	1802400
25	PHI=TIME	1802410
	ARG=PHI	1802420

	IF (KKNT.EQ.3)	1802430
	1 READ(IO) SAVY,NPLEV,NPLA,SIGMA,SALPH,SBAPH,STEPS,STR,EFF,STSRN,	1802440
	1 NPLAST,STSIG,STREPS,STALPH,STBAPH,NPLEVS,EFFST,SEPS	1802450
	LL=NP+1	1802460
	DO 51 I=1,NP	1802470
	IF (ARG-ST(1,I)) 52,55,51	1802480
	52 IF (I-1) 55,55,54	1802490
	51 CONTINUE	1802500
	I=NP	1802510
	GO TO 55	1802520
	54 DO 57 IK=2,NTOTAL	1802530
	57 ST(IK,LL)=ST(IK,I-1)+(ST(IK,I)-ST(IK,I-1))*(ARG-ST(1,I-1))/(ST(1,I	1802540
	1)-ST(1,I-1))	1802550
	GOTO 80	1802560
	55 DO 58 IK=2,NTOTAL	1802570
	58 ST(IK,LL)=ST(IK,I)	1802580
	80 CONTINUE	1802590
C	THE UPDATED INTERPOLATED VALUES OF THE MATERIAL PROPERTY COEFFIC	1802600
C	IENTS ARE FOUND IN THE XMAT TABLE AND STORED IN THE XLAYER ARRAY	1802610
	L=(MAT-1)*2+1	1802620
	II=NXMAT(L)	1802630
	III=NXMAT(L+1)	1802640
	LL=NP+1	1802650
	L=NROW + 1	1802660
	M=1	1802670
	GOTO (91,92,93,93),KELVIN	1802680
	91 ARG = (ST(L,LL)+ST(L+1,LL)+ST(L+2,LL)+ST(L+3,LL))/4.0	1802690
	GOTO 94	1802700
	93 CONTINUE	1802710
	ARG = ST(NROW+1,LL)	1802720
	94 DO 104 I = 2,10	1802730
	IF (ARG-XMAT(II,I)) 121,123,104	1802740
	121 IF (I-2) 8007,8007,124	1802750
	104 CONTINUE	1802760
	GOTO 8067	1802770
	123 L=II+1	1802780
	DO 122 J=L,III	1802790
	XLAYER(M)=XMAT(J,I)	1802800
	122 M=M+1	1802810
	GOTO 111	1802820
	124 L=II+1	1802830
	DO 125 J=L,III	1802840
	XLAYER(M)=XMAT(J,I-1)+(XMAT(J,I)-XMAT(J,I-1))*(ARG-XMAT(II,I-1))/	1802850
	1 (XMAT(II,I)-XMAT(II,I-1))	1802860
	125 M=M+1	1802870
	GOTO 111	1802880
	92 L = II + 1	1802890
	DO 922 J=L,III	1802900
	XLAYER(M)= XMAT(J,1)	1802910
	922 M=M+1	1802920
	111 CONTINUE	1802930
	115 GO TO(101,102,103),ITYPE	1802940
	101 ETHET = XLAYER(1)	1802950
	XNUTP =XLAYER(2)	1802960
	ALPHTH = XLAYER(3)	1802970
	EPHI = ETHET	1802980
	XNUPT= XNUTP	1802990
	ALPHPH = ALPHTH	1803000
	XGPT = ETHET/(2.0*(1.0+XNUPT))	1803010
	N = 4	1803020
	GO TO 105	1803030

102	ETHET = XLAYER(1)	1803040
	EPHI = XLAYER(2)	1803050
	XNUTP = XLAYER(3)	1803060
	ALPHTH = XLAYER(4)	1803070
	ALPHPH = XLAYER(5)	1803080
	XGPT = XLAYER(6)	1803090
	XNUPT = ETHET*XNUTP/EPHI	1803100
	N = 7	1803110
	GO TO 105	1803120
103	ETHET = XLAYER(1)	1803130
	EPHI = XLAYER(2)	1803140
	XNUTP = XLAYER(3)	1803150
	ALPHTH = XLAYER(4)	1803160
	ALPHPH = XLAYER(5)	1803170
	XGPT = XLAYER(6)	1803180
	ER = XLAYER(17)	1803190
	ES = XLAYER(18)	1803200
	ALPHR = XLAYER(19)	1803210
	ALPHS = XLAYER(20)	1803220
	RMOSSR = XLAYER(21)	1803230
	RMOSNR = XLAYER(22)	1803240
	SIGOXR = XLAYER(23)	1803250
	RMOSSS = XLAYER(24)	1803260
	RMOSNS = XLAYER(25)	1803270
	SIGOXS = XLAYER(26)	1803280
	XNUPT = ETHET*XNUTP/EPHI	1803290
	N = 7	1803300
105	CONTINUE	1803310
	RMOSS = XLAYER(N)	1803320
	RMOSN = XLAYER(N+1)	1803330
	SIGOX = XLAYER(N+2)	1803340
	IF (ITYPE.NE.1) GO TO 108	1803350
	SIGOY = SIGOX	1803360
	SIGOZ = SIGOX	1803370
	SIGXY = SIGOX/SQRT(3.0)	1803380
	GO TO 109	1803390
108	CONTINUE	1803400
	SIGOY = XLAYER(N+3)	1803410
	SIGOZ = XLAYER(N+4)	1803420
	SIGXY = XLAYER(N+5)	1803430
	RMOSSY = XLAYER(N+6)	1803440
	RMOSNY = XLAYER(N+7)	1803450
	RMOSXY = XLAYER(N+8)	1803460
	RMONXY = XLAYER(N+9)	1803470
	IF (KORI.GT.0) GO TO 227	1803480
109	CONTINUE	1803490
	IF (RMOSN.EQ.0.0) GO TO 225	1803500
	YLDST = SIGOX*SIGOX	1803510
	IF (RMOSS.NE.0.0) GO TO 224	1803520
	ROC = YLDST*EPHI*RMOSN/(1.0-RMOSN)	1803530
	GO TO 227	1803540
224	ROC = 2.333333*EPHI*YLDST/RMOSN	1803550
225	RMOSN = RMOSN-1.0	1803560
227	TEM1 = SIGOX*SIGOX	1803570
	TEM2 = SIGOY*SIGOY	1803580
	TEM3 = SIGOZ*SIGOZ	1803590
	TEM4 = 0.5/TEM1	1803600
	TEM5 = 0.5/TEM2	1803610
	TEM6 = 0.5/TEM3	1803620
	HP = TEM4+TEM5-TEM6	1803630
	TWON = 1.0/(SIGXY*SIGXY)	1803640

FPLUH = 1.0/TEM2	1803650
GPLUH = 1.0/TEM1	1803660
CALL TOBAR (ST,KLUE2,NROW,LL,E1,E2,HI,HO,T,TII,TOO,TIK,TOK,	1803670
1           DEGRES,G2,G3,TIME,NCONT)	1803680
IF (NIX.NE.0) GO TO 9999	1803690
LL=NP+1	1803700
IF(XK11.EQ.0.0) GOTO 8101	1803710
IF(ITYPE.EQ.3.AND.XK12.EQ.0.) GO TO 8102	1803720
IF(ITYPE.EQ.3.AND.XK21.EQ.0.) GO TO 8103	1803730
IF(XK22.EQ.0.0) GOTO 8104	1803740
IF(XK33.EQ.0.0) GOTO 8105	1803750
IF(XD11.EQ.0.0) GOTO 8106	1803760
IF(ITYPE.EQ.3.AND.XD12.EQ.0.) GO TO 8107	1803770
IF(ITYPE.EQ.3.AND.XD21.EQ.0.) GO TO 8108	1803780
IF(XD22.EQ.0.0) GOTO 8109	1803790
IF(XD33.EQ.0.0) GOTO 8110	1803800
NL=0	1803810
JF = NPROB	1803820
K = NROW	1803830
DO 7 M=1,JF	1803840
I = (M-1)*8 + 1	1803850
NL=NL+1	1803860
XFTHLD=0.0	1803870
XFPHLD=0.0	1803880
XFZELD=0.0	1803890
XMTHLD=0.0	1803900
XMPHLD=0.0	1803910
IR=NL*6-5	1803920
IF(LST(IR).NE.0) K=K+LST(IR)	1803930
IF (LST(IR+1).EQ.0) GOTO 44	1803940
K=K+1	1803950
XFTHLD=ST(K,LL)	1803960
44 IF(LST(IR+2).EQ.0) GOTO 45	1803970
K=K+1	1803980
XFPHLD = ST(K,LL)+XMERD*IWORD	1803990
45 IF(LST(IR+3).EQ.0) GOTO 46	1804000
K=K+1	1804010
XFZELD = ST(K,LL)+XPRES*IWORD	1804020
46 IF(LST(IR+4).EQ.0) GOTO 47	1804030
K=K+1	1804040
XMTHLD = ST(K,LL)+XMONT*IWORD	1804050
47 IF(LST(IR+5).EQ.0) GOTO 48	1804060
K=K+1	1804070
XMPHLD=ST(K,LL)	1804080
48 CONTINUE	1804090
50 IF (ISTTAB.GE.3.AND.ISTTAB.LE.9) GO TO 4002	1804100
CALL ODE1	1804110
GO TO 77	1804120
4002 CALL ODE2	1804130
77 CONTINUE	1804140
7 CONTINUE	1804150
GOTO 75	1804160
8001 IERROR=8001	1804170
NERROR = 11	1804180
GOTO 8888	1804190
8002 IERROR=8002	1804200
NERROR = 12	1804210
GOTO 8888	1804220
8007 IERROR=8007	1804230
NERROR = 15	1804240
GOTO 8888	1804250

8031	IERROR=8031	1804260
	NERROR = 9	1804270
8067	IERROR= 8067	1804280
	NERROR = 16	1804290
	GOTO 8888	1804300
8101	IERROR = 8101	1804310
	NERROR = 17	1804320
	GOTO 8888	1804330
8102	IERROR = 8102	1804340
	NERROR = 18	1804350
	GOTO 8888	1804360
8103	IERROR = 8103	1804370
	NERROR = 19	1804380
	GOTO 8888	1804390
8104	IERROR = 8104	1804400
	NERROR = 20	1804410
	GOTO 8888	1804420
8105	IERROR = 8105	1804430
	NERROR = 21	1804440
	GOTO 8888	1804450
8106	IERROR = 8106	1804460
	NERROR = 22	1804470
	GOTO 8888	1804480
8107	IERROR = 8107	1804490
	NERROR = 23	1804500
	GOTO 8888	1804510
8108	IERROR = 8108	1804520
	NERROR = 24	1804530
	GOTO 8888	1804540
8109	IERROR = 8109	1804550
	NERROR = 25	1804560
	GOTO 8888	1804570
8110	IERROR = 8110	1804580
	NERROR = 26	1804590
8888	NIX=1	1804600
	GO TO 9999	1804610
150	IF (NGR.EQ.1) CALL GRAPH (KGEOM)	1804620
	IF (LSC.LT.KSC) GO TO 902	1804630
9999	RETURN	1804640
	END	1804650



```

FOR, IS FIXEM, FIXEM
  SUBROUTINE FIXEM (MAGIN, MAGOUT, TIC, STEP, NEQNS, DTAU,
1      EPSIL, DELTA, ERR, TIME, DTIME, YICS, YPRED,
2      YCORR, YDOT, YNEW, YDEV, FWDEL, TBDEL)
C
  RUNGE KUTTA MAGIC (REVISED) SINGLE PRECISION          FORTRAN IV
  DIMENSION YICS( 1), YPRED( 1), YCORR( 1), YDOT( 1), YNEW( 1),
1      YDEV(1), FWDEL(1), TBDEL(1)
  DIMENSION C(3), D(3)
  COMMON /MAGIQ/ KKNT
  DOUBLE PRECISION YNEW, YPRED
  DATA C, D / .5, .5, 1.0, .5, .0, .5/
  MSET=1
  TIME = TIC
  TAU = TIC
  IF (DELTA) 200, 201, 200
200 DTIME = 0.0078125
  GO TO 225
201 DTIME = STEP
225 DO 102 I = 1, NEQNS
  YDEV(I) = 0.0
  YPRED(I) = YICS(I)
  YCORR(I) = YICS(I)
102 YNEW(I) = YICS(I)
  MAGOUT = -2
  GO TO 264
5555 CONTINUE
  ENTRY WAND (MAGIN, MAGOUT, TIC, STEP, NEQNS, DTAU,
1      EPSIL, DELTA, ERR, TIME, DTIME, YICS, YPRED,
2      YCORR, YDOT, YNEW, YDEV, FWDEL, TBDEL)
5556 CONTINUE
  MSET=2
  IF (MAGOUT) 305, 101, 101
101 IF (MAGIN) 21, 27, 14
  27 K = 0
  DO 202 I = 1, NEQNS
202 YNEW(I) = YPRED(I)
  21 K = K + 1
  KKNT = K
210 DO 2 I = 1, NEQNS
  GO TO (9, 6, 7, 4, 11), K
  9 FWDEL(I) = YDOT(I)
  GO TO 105
  6 TBDEL(I) = YDOT(I)
  GO TO 105
  7 TBDEL(I) = TBDEL(I) + YDOT(I)
105 YPRED(I) = YNEW(I) + C(K)*DTIME*YDOT(I)
  GO TO (2, 2, 400), K
400 YCORR(I) = YPRED(I)
  2 CONTINUE
  TIME = TIME + D(K)*DTIME
99 MAGOUT = 0.0
264 RETURN
  4 DO 8 I = 1, NEQNS
  YPRED(I) = YNEW(I) + DTIME*(FWDEL(I) + 2.*TBDEL(I) + YDOT(I))/6.
  8 YDEV(I) = YCORR(I) - YPRED(I)
  GO TO 99
11 IF (DELTA) 80, 5, 80
80 DO 13 I = 1, NEQNS
  IF (EPSIL*ABS(YCORR(I)) + ERR - ABS(YDEV(I))) 14, 13, 13
13 CONTINUE

```

IF (SIGB)15,15,205	1900580
205 SIGB = 0.0	1900590
GO TO 5	1900600
15 SIGB = 0.0	1900610
DO 207 I = 1,NEQNS	1900620
IF (ERR /100.+ DELTA*ABS(YCORR(I)) - ABS(YDEV(I))) 5,207,207	1900630
207 CONTINUE	1900640
DTIME = 2.*DTIME	1900650
5 DO 208 I = 1,NEQNS	1900660
208 YCORR(I) = YPRED(I)	1900670
305 IF (DTAU) 19,30,19	1900680
19 IF (TAU - TIME)20,20,27	1900690
20 TAU = TAU + DTAU	1900700
30 MAGOUT = 2	1900710
GO TO 264	1900720
14 DTIME = DTIME/2.0	1900730
25 IF (K-3)48,26,26	1900740
26 TIME = TIME - DTIME - DTIME	1900750
GO TO 47	1900760
48 TIME = TIME - DTIME	1900770
47 SIGB = +2.	1900780
DO 209 I = 1,NEQNS	1900790
209 YDOT(I) = FWDEL(I)	1900800
212 K = 0	1900810
GO TO 21	1900820
END	1900830

```

FOR, IS TOBAR, TOBAR
SUBROUTINE TOBAR (ST, KLUE2, NROW, LL, E1, E2, HI, HO, T, TII, TOO,
1 TIK, TOK, DEGRES, G2, G3, TIME, NCONT) 2200010
INTEGER SAVJTC, SAVSTP, Q, THICK 2200020
INTEGER XN1, XN2, XN 2200030
REAL*4 I2 2200050
DOUBLE PRECISION YPRED 2200060
COMMON STORY(16), XMAT(270, 10), STD(10), SADUS(30), RADUS(30) 2200070
COMMON TADUS(30), UACUS(30), SAVTIC(900) 2200080
COMMON XN, TEFREE, TIC, PHI, STOP, RESTOP, RTICK, G1, XNL(3), NH 2200090
COMMON NST(30), NKL(30), NXMAT(20), SAVJTC(30), SAVSTP(30), JRTIC(30) 2200100
COMMON JRSTOP(30), NREG, NMPT, NRC, NSC, NIX, IERROR, KGEOM, IGEOM, ISTTAB 2200110
COMMON KELVIN, IBEGIN, NPROB, NSEG, NERROR, Q, THICK, NOJS, NLINKS, NLCASE 2200120
COMMON NTSKL, NZ, NBCT, LINPUT, NTRKL, NPASS, XN1, KBC, NRINGS 2200130
COMMON LODE, ICYCLE, LDISTL 2200140
COMMON /LASTEQ/ YPRED(8), YDOT(8), YASAVE(8), 2200150
1 YANTH, YAMTH, YAMPT, YANPT, YAOPH, YAQPH, YAQTH, YAJPH, 2200160
2 S, SN, CS, SNSQ, CSSQ, TAN, SEC, CN, X1CS, X1SN, TN, 2200170
3 X1RO, X1ROSQ, X1SNRO, X1CSRO, CN1RO, SN1RO, CS1RO, 2200180
4 X1R1, X1R2, CS1R1, CS1R2, SN1R1, X1R1SQ, R2SQ, RO, BESQ, 2200190
5 ROSQ, XNSQ, BETA, R1, R2, S1, R1DOT, R1SQ, 2200200
6 XNTH, XNTPH, XMTTH, XMTPH, XFTHLD, XFPHL D, XFZELD, 2200210
7 XMTHLD, XMPHL D, ETHET, EPHI, XGPT, ALPHTH, ALPHPH, 2200220
8 XNUTP, XNUPT, XC11, XC22, XC15, XD33, XD22, XD21, XD12, 2200230
9 XK11, XK12, XK21, XK22, XK33, XD11, 2200240
A M, I, SITIN, SITOUT, SIPIN, SIPOUT, TPTIN, TPTOUT, 2200250
B ZBRIN, ZBROUT, SCRIPA, SCRIP1, SIFIN, SIFOUT, TZEPH, TZETH 2200260
B , XNPHI, BETTA, ZETTA, XC16 2200270
C , RMOSS, RMOSN, YLOST, ROCP, HP, FPLUH, GPLUH, TWON 2200280
D , RMOSSY, RMOSNY, RMOSXY, RMONXY
D , RMOSNS, RMOSSS, SIGOXS, RMOSNR, RMOSSR, SIGOXR 2200290
COMMON /SNILPS/ ANG, PSI(100), RAD(100), CURL(100), CUR2(100), 2200300
1 DR1DP(100), ZI(14), RI(14), NRZIN 2200310
COMMON /RWD/ ER, ES, CPH, CTH, APH, ATH, SPH, STH, ALPHS, ALPHR, TS, TR, SNB, 2200320
C CSB 2200330
COMMON /PLS/ OMEGA, IWORD, XMERD, XPRES, XMONT 2200340
COMMON /WOOD/ SAVY(53), NPLEV, NLPO, NPLA(21), STR(6), SIGMA(3, 21), 2200350
C SEPS(3, 21), SALPH(3, 21), SBAPH(3, 21), STEPS(3, 21), 2200360
D EFF(21), STSRN(3), NPLAST(3), STSIG(3), STREPS(3), 2200370
M STALPH(3), STBAPH(3), EFFST(3), NPLEVS(3) 2200380
DIMENSION ST(30, 31) 2200390
EQUIVALENCE (SINB, SNB), (COSB, CSB) 2200400
DATA A/'A '/ 2200410
GOTO (771, 772, 773, 774, 775, 776, 7077), KGEOM 2200420
C GEOMETRY FOR ELIPSE(G3=OFFSET DISTANCE ) 2200430
771 A=G1 2200440
BE=G2 2200450
BETA = BE 2200460
BESQ=B E**2 2200470
ASQ=A**2 2200480
SN = SIN(PHI) 2200490
CS = COS(PHI) 2200500
SNSQ = SN**2 2200510
CSSQ = CS**2 2200520
R2 = A*SQRT(1.0/(SNSQ+BESQ*CSSQ)) 2200530
R2SQ = R2**2 2200540
RO=R2*SN 2200550
R1=R2*R2SQ*BESQ/ASQ 2200560
BESQ=B E**2 2200570
R1DOT=0.0 2200580

```

```

      IF(KGEOM.EQ.1.AND.BETA.NE.1.0.AND.SN.NE.0.0)R1DOT=3.0*(R2*BETA/
1A) **2*(CS/SNSQ)*(R1*SN-RO)
      IF(SN.EQ. 0.0)GO TO 779
      R2 = R2-G3/SN
      R2SQ = R2**2
      RO = RO-G3
      GO TO 7775
779 IF(G3 .EQ. 0.0)GO TO 7775
      R1DOT = 3.0*G3
      RO = -G3
      GO TO 7775
C   GEOMETRY FOR OGIVE
772 R1=G1
      C=G2
      SN = SIN(PHI)
      CS = COS(PHI)
      IF (SN.EQ.0.0) GOTO 777
      R2=R1-C/SN
      GOTO 778
777 R2 = 1.0
778 RO = R1*SN-C
      R1DOT=0.0
      GOTO 7775
C   GEOMETRY FOR CONE
773 CS = COS(G1)
      SN=SIN(G1)
      S=PHI
      S1=1.0/S
      R2=CS*SN*PHI
      RO=PHI*CS
      R1DOT=0.0
      GOTO 7775
C   GEOMETRY FOR CYLINDER
774 RO = G1
      SN=1.0
      CS=1.0
      R1DOT=0.0
      GOTO 7775
C   MODIFIED ELLIPSE
775 XNEXP=G1
      A =G2
      XN1=1.0+XNEXP
      XN2=1.0/XN1
      XN3=XN1+1.0
      XN4=XN3+1.0
      XN5=XN4/XN1
      SN = SIN(PHI)
      CS = COS(PHI)
      R2= A*(2.0/(1.0+SN**XN1))**XN2
      R1=(A/2.0)*(R2/A)**XN3
      RO=R2*SN
      R1DOT=-XN3*A*(SN**XNEXP*CS/4.0)*(2.0/(1.0+SN**XN1))**XN5
      GOTO 7775
C   GENERAL GEOMETRY
776 SN = SIN(PHI)
      CS = COS(PHI)
      TAN = SN / CS
      SEC = 1.0 / CS
      IF (TIME.EQ.TIC) CALL TEMOEG
      ARG = PHI
      DO 204 J=1,100

```

```

2200590
2200600
2200610
2200620
2200630
2200640
2200650
2200660
2200670
2200680
2200690
2200700
2200710
2200720
2200730
2200740
2200750
2200760
2200770
2200780
2200790
2200800
2200810
2200820
2200830
2200840
2200850
2200860
2200870
2200880
2200890
2200900
2200910
2200920
2200930
2200940
2200950
2200960
2200970
2200980
2200990
2201000
2201010
2201020
2201030
2201040
2201050
2201060
2201070
2201080
2201090
2201100
2201110
2201120
2201130
2201140
2201150
2201160
2201170
2201180
2201190

```

PHO = PSI(J)	2201200
IF (ANG.EQ.A) IF (ARG-PHO) 221,223,204	2201210
IF (PHO-ARG) 221,223,204	2201220
221 IF (J-1) 8502,8502,224	2201230
204 CONTINUE	2201240
GO TO 8503	2201250
223 RO = RAD(J)	2201260
R1 = CUR1(J)	2201270
R2 = CUR2(J)	2201280
R1DOT = DR1DP(J)	2201290
GO TO 7775	2201300
8502 NERROR = 41	2201310
GO TO 8888	2201320
8503 NERROR = 42	2201330
8888 NIX = 1	2201340
GO TO 8889	2201350
224 SUB1 = ARG-PSI(J-1)	2201360
SUB2 = PSI(J)-PSI(J-1)	2201370
RO = RAD(J-1)+(RAD(J)-RAD(J-1))*SUB1/SUB2	2201380
R1 = CUR1(J-1)+(CUR1(J)-CUR1(J-1))*SUB1/SUB2	2201390
R2 = CUR2(J-1)+(CUR2(J)-CUR2(J-1))*SUB1/SUB2	2201400
R1DOT = DR1DP(J-1)+(DR1DP(J)-DR1DP(J-1))*SUB1/SUB2	2201410
GOTO 7775	2201420
C ISOTENSOID GEOMETRY	2201430
7077 CONTINUE	2201440
SN = SIN(PHI)	2201450
CS = COS(PHI)	2201460
A = G1	2201470
R2 = A / SQRT(SN)	2201480
R1 = 0.5 * R2	2201490
RO = R2 * SN	2201500
R1DOT = - ((A**2)*0.5)*(R1*CS)/RO**2	2201510
7775 TAN=SN/CS	2201520
DEGRES = 0.0	2201530
IF(IGEOM.EQ.1) DEGRES = PHI * 57.29578	2201540
ROSQ = RO**2	2201550
XNSQ=XN**2	2201560
CN=CS*SN	2201570
X1CS=1.0/CS	2201580
TN=SN/CS	2201590
X1RO=1.0/RO	2201600
X1ROSQ=1.0/RO**2	2201610
X1CSRO=1.0/(CS*RO)	2201620
CN1RO=CN/RO	2201630
SN1RO=SN/RO	2201640
CS1RO=CS/RO	2201650
SNSQ=SN**2	2201660
CSSQ=CS**2	2201670
IF(KGEOM.EQ.4.OR.KGEOM.EQ.3) GOTO 79	2201680
R1SQ = R1**2	2201690
R2SQ = R2**2	2201700
X1SN=1.0/SN	2201710
X1SNRO=1.0/(SN*RO)	2201720
X1R1=1.0/R1	2201730
X1R2=1.0/R2	2201740
CS1R1=CS/R1	2201750
CS1R2=CS/R2	2201760
SN1R1=SN/R1	2201770
X1R1SQ=1.0/R1**2	2201780
79 XNTTH=0.0	2201790
XNTPH=0.0	2201800

	XMTTH=0.0	2201810
	XMPH=0.0	2201820
C		2201830
C	COMPUTATION OF K AND D FOR MATERIAL PROPEY INPUT	2201840
C		2201850
	HO = 0.0	2201860
	T = 0.0	2201870
	HI = 0.0	2201880
	TS = 0.0	2201890
	TR = 0.0	2201900
	RHOR = 0.0	2201910
	RHOS = 0.0	2201920
	RHOI = 0.0	2201930
	RHOC = 0.0	2201940
	CTH = 0.0	2201950
	CPH = 0.0	2201960
	YBARI = 0.0	2201970
	YBARC = 0.0	2201980
	YBARO = 0.0	2201990
	GO TO (711,600,711,32,33,34,35,36,37,28,29,30),ISTTAB	2202000
C	THICK	2202010
	600 GO TO (703,702,701,701),THICK	2202020
	701 HO= ST(4,LL)	2202030
	702 T = ST(3,LL)	2202040
	RHOC = ST(NCONT-1,LL)	2202050
	703 HI= ST(2,LL)	2202060
	RHOI = ST(NCONT,LL)	2202070
	GO TO 40	2202080
C	ST11,ST12,ST13	2202090
	30 HO= ST(14,LL)	2202100
	29 T = ST(13,LL)	2202110
	RHOC = ST(NCONT-3,LL)	2202120
	28 HI= ST(12,LL)	2202130
	RHOI = ST(NCONT-2,LL)	2202140
	RHOS = ST(NCONT-1,LL)	2202150
	RHOR = ST(NCONT,LL)	2202160
	GJPH= ST(2,LL)	2202170
	GJTH= ST(3,LL)	2202180
	APH = ST(4,LL)	2202190
	ATH = ST(5,LL)	2202200
	CPH = ST(6,LL)	2202210
	CTH = ST(7,LL)	2202220
	XIPH = ST(8,LL)	2202230
	XITH= ST(9,LL)	2202240
	SPH = ST(10,LL)	2202250
	STH = ST(11,LL)	2202260
	IF (KELVIN.EQ.2.OR.KELVIN.EQ.4) GO TO 40	2202270
	ISTAB = ISTTAB-9	2202280
	TS = ST(ISTAB+12,LL)	2202290
	TR = ST(ISTAB+13,LL)	2202300
	GO TO 40	2202310
C	RWAF1,RWAF2,RWAF3	2202320
	34 HO = ST(10,LL)	2202330
	33 T = ST(9,LL)	2202340
	RHOC = ST(NCONT-2,LL)	2202350
	32 HI = ST(8,LL)	2202360
	RHOI = ST(NCONT-1,LL)	2202370
	RHOS = ST(NCONT,LL)	2202380
	APH = ST(2,LL)	2202390
	CPH = ST(3,LL)	2202400
	XIPH= ST(4,LL)	2202410

	SPH = ST(5,LL)	2202420
	BETTA=ST(6,LL)	2202430
	ZETTA = ST(7,LL)	2202440
	ATH = APH	2202450
	CTH = CPH	2202460
	XITH= XIPH	2202470
	STH = SPH	2202480
	RHOR = RHOS*IWORD	2202490
	IF (KELVIN.EQ.2.OR.KELVIN.EQ.4) GO TO 40	2202500
	ISTAB = ISTTAB-3	2202510
	TS = ST(ISTAB+8,LL)	2202520
	TR = TS	2202530
	GO TO 40	2202540
C	ISG1,ISG2,ISG3	2202550
	37 HO = ST(9,LL)	2202560
	36 T = ST(8,LL)	2202570
	RHOC = ST(NCONT-2,LL)	2202580
	35 HI = ST(7,LL)	2202590
	RHOI = ST(NCONT-1,LL)	2202600
	RHOS = ST(NCONT,LL)	2202610
	APH = ST(2,LL)	2202620
	CPH = ST(3,LL)	2202630
	XIPH = ST(4,LL)	2202640
	SPH = ST(5,LL)	2202650
	BETTA = ST(6,LL)	2202660
	ATH = APH	2202670
	CTH = CPH	2202680
	XITH = XIPH	2202690
	STH = SPH	2202700
	RHOR = RHOS*IWORD	2202710
	IF (KELVIN.EQ.2.OR.KELVIN.EQ.4) GO TO 40	2202720
	ISTAB = ISTTAB-6	2202730
	TS = ST(ISTAB+7,LL)	2202740
	TR = TS	2202750
	GO TO 40	2202760
	ST10,RWAF	2202770
C	RANKIN=THSTND MEANS INTERPOLATE, COMPUTE NTEMP, MTEMP	2202780
C	RANKIN=NOTHRM MEANS DO NOT INTERPOLATE, DO NOT COMPUTE NTEMP, MTEMP	2202790
C	RANKIN=THCNST MEANS DO NOT AVERAGE, BUT INTERPOLATE, COMPUTE	2202800
C	NTEMP, MTEMP	2202810
C	RANKIN=THINHO MEANS INTERPOLATE, BUT DO NOT COMPUTE NTEMP, MTEMP	2202820
C		2202830
	711 CONTINUE	2202840
	XK11=ST(2,LL)	2202850
	XK12=ST(3,LL)	2202860
	XK22 = ST(4,LL)	2202870
	XK33 = ST(5,LL)	2202880
	XD11 = ST(6,LL)	2202890
	XD12 = ST(7,LL)	2202900
	XD22 = ST(8,LL)	2202910
	XD33 = ST(9,LL)	2202920
	XC11 = ST(10,LL)	2202930
	XC22 = ST(11,LL)	2202940
	XC15 = ST(12,LL)	2202950
	XC16 = ST(13,LL)	2202960
	XMERD = ST(NCONT-2,LL)	2202970
	XPRES = ST(NCONT-1,LL)	2202980
	XMONT = ST(NCONT,LL)	2202990
	XK21 = XK12	2203000
	XD21 = XD12	2203010
	GO TO 103	2203020

C		2203030
	40 CONTINUE	2203040
	IF (IWORD.EQ.1) GO TO 140	2203050
	RHOR = 0.0	2203060
	RHOS = 0.0	2203070
	RHOI = 0.0	2203080
	RHOC = 0.0	2203090
	XNERD = 0.0	2203100
	XPRES = 0.0	2203110
	XMONT = 0.0	2203120
	140 CONTINUE	2203130
	TEMP3= (1.0-XNUPT * XNUTP)	2203140
	GO TO (42,47,49,41),THICK	2203150
	41 GO TO (103,42,103,42,47,49,42,47,49,42,47,49),ISTTAB	2203160
C		2203170
C	SINGLE SHEET	2203180
C		2203190
	42 TEMP1 = ETHET*HI	2203200
	TEMP2= TEMP1 * HI**2	2203210
	XK11= TEMP1/TEMP3	2203220
	XD11= TEMP2/(12.0* TEMP3)	2203230
	TEMP1 = EPHI*HI	2203240
	TEMP2= TEMP1*HI**2	2203250
	XK22= TEMP1/TEMP3	2203260
	XD22= TEMP2/(12.0* TEMP3)	2203270
	XK33 = XGPT*HI	2203280
	XD33= XK33*HI**2/12.0	2203290
	YBARI = 0.0	2203300
	YBARC = 0.0	2203310
	YBARO = 0.0	2203320
	GO TO 55	2203330
C		2203340
C	EQUAL SHEETS	2203350
C		2203360
	47 CONTINUE	2203370
	XK11 = 2.0*ETHET*HI/TEMP3	2203380
	XK22 = 2.0*EPHI*HI/TEMP3	2203390
	XK33 = 2.0*XGPT	2203400
	ZBR = HI+T/2.0	2203410
	ZBH = (ZBR-HI/2.0)**2	2203420
	XD33 = XGPT*HI*((HI**2)/6.0+2.0*ZBH)	2203430
	XD11 = HI*(XK11*HI/12.0+2.0*ETHET*ZBH/TEMP3)	2203440
	XD22 = HI*(XK22*HI/12.0+2.0*EPHI*ZBH/TEMP3)	2203450
	YBARI = ZBR-HI/2.0	2203460
	YBARC = ZBR-HI-T/2.0	2203470
	YBARO = HI/2.0-ZBR	2203480
	GO TO 55	2203490
C		2203500
C	UNEQUAL FACE SHEETS	2203510
C		2203520
	49 CONTINUE	2203530
	ZBR = (HI*HI+HO*HO+2.0*(HO*(HI+T)))/(2.0*(HI+HO))	2203540
	ZBHIN = (ZBR-HI/2.0)**2	2203550
	ZBHOUT = (ZBR-HO/2.0)**2	2203560
	XK11 = ETHET*(HI+HO)/TEMP3	2203570
	XK22 = EPHI*(HI+HO)/TEMP3	2203580
	XK33 = XGPT*(HI+HO)	2203590
	HIO3 = HI**3+HO**3	2203600
	XD33 = HIO3*XGPT/12.0+XGPT*(HI*ZBHIN+HO*ZBHOUT)	2203610
	D11 = ETHET*HIO3/12.0	2203620
	XD11 = (D11+ETHET*(HI*ZBHIN+HO*ZBHOUT))/TEMP3	2203630



	D22 = EPHI*HI03/12.0	2203640
	XD22 = (D22+EPHI*(HI*ZBHIN+HO*ZBHOUT))/TEMP3	2203650
	YBARI = ZBR-HI/2.0	2203660
	YBARC = ZBR-HI-T/2.0	2203670
	YBARO = HI/2.0-ZBR	2203680
C		2203690
C	DETERMINE COMPLETE CONSTANTS DEPENDENT ON REINFORCEMENT CLUE	2203700
C		2203710
	55 CONTINUE	2203720
	ROI = RO-YBARI*SN	2203730
	ROU = RO-YBARO*SN	2203740
	ROC = RO-YBARC*SN	2203750
	IF (THICK.EQ.2) HO = HI	2203760
	IF (ISTTAB.EQ.5.OR.ISTTAB.EQ.8.OR.ISTTAB.EQ.11) HO = HI	2203770
	D3 = RHOI*ROI*HI	2203780
	D4 = RHOC*ROC*T	2203790
	D5 = RHOI*ROU*HO	2203800
	DD = D3+D4+D5	2203810
	XMERD = DD*OMEGA*CS	2203820
	XPRES = -DD*OMEGA*SN	2203830
	XMONT = -(D3*YBARI+D4*YBARC+D5*YBARO)*OMEGA*CS	2203840
	IF(ISTTAB.EQ.2)GO TO 103	2203850
	TBARR = ATH/STH	2203860
	TBARS = APH/SPH	2203870
	ROR = RO-CTH*SN	2203880
	ROS = RO-CPH*SN	2203890
	EASTH=ER*ATH/STH	2203900
	EASPH=ES*APH/SPH	2203910
	EISPH= ES* XIPH/SPH	2203920
	EISTH= ER* XITH/STH	2203930
	D1 = RHOR*ROR*TBARR	2203940
	D2 = RHOS*ROS*TBARS	2203950
	DD = D1+D2+D3+D4+D5	2203960
	GO TO (58,60,100),KLUE2	2203970
C		2203980
C	ST CLUE (11,12,13)	2203990
C		2204000
	58 CONTINUE	2204010
	XK12= XK11*XNUTP	2204020
	XK11= XK11+ EASTH	2204030
	XK22= XK22+ EASPH	2204040
	XC11= EASTH*CTH	2204050
	XC22= EASPH*CPH	2204060
	XD22 = -XD22-EISPH	2204070
	XD33= XD33 + GJPH/(4.0*SPH)+ GJTH/(4.0*STH)	2204080
	XD12= -XD11*XNUTP	2204090
	XD11= -XD11- EISTH	2204100
	XK21 = XK12	2204110
	XD21 = XD12	2204120
	XMERD = DD*OMEGA*CS	2204130
	XPRES = -DD*OMEGA*SN	2204140
	XMONT = -(D1*CTH+D2*CPH+D3*YBARI+D4*YBARC+D5*YBARO)*OMEGA*CS	2204150
	GO TO 103	2204160
C	RWA CLUE (1,2,3)	2204170
C		2204180
	60 CONTINUE	2204190
	SINB =SIN(BETTA)	2204200
	COSB =COS(BETTA)	2204210
	SN2T04 = 2*(SINB**4.)	2204220
	D= STH*(COSB+SINB)	2204230
	ED = ER*ATH/D	2204240

	SINB2= SINB**2.	2204250
	HL = 2.0*(ABS(ZETTA)-ABS(CTH))	2204260
	I2=(ATH**3.)/(3* HL**2)	2204270
95	XC22 = 2.0*CTH*COB**3*ED	2204280
	XC15 = 2.0*CTH*COB*SINB2*ED	2204290
	XC16 = XC15	2204300
	GRI= ER* I2/(2.0*(1.0 + XNUTP)*D)	2204310
	XC11 = CTH*SN2TO4/COB*ED	2204320
	EDI = ER*XITH/D	2204330
	SN4TO2 = 4.*SINB2	2204340
	XD22 = -XD22-2.0*COB**3*EDI-SN4TO2*COB*GRI	2204350
	TB= 2.0* BETTA	2204360
	XD33 = XD33+((4.0*COB(TB)*	2204370
	1*2*GRI)/ COB) + (2.0*COB*SINB2*EDI)	2204380
	XD12 = -XD11*XNUTP-(2.0*COB	2204390
	1*SINB2*EDI)-(SN4TO2*COB*GRI )	2204400
	XK12= XK11*XNUTP + (2.0*COB*SINB2*ED)	2204410
	XK22=XK22+(2*COB**3*ED)	2204420
	XK33=XK33+(2*COB*SINB2*ED)	2204430
	XK11=XK11+(SN2TO4*ED/COB)	2204440
	XD11 = -XD11-SN2TO4*EDI/COB-(	2204450
	1 SN4TO2*COB*GRI)	2204460
	XK21 = XK12	2204470
	XD21 = XD12	2204480
	GO TO 108	2204490
C		2204500
C	ISG CLUE (1,2,3)	2204510
C		2204520
100	CONTINUE	2204530
	SNB =SIN(BETTA)	2204540
	CSB =COS(BETTA)	2204550
	TBETTA= 2.0*BETTA	2204560
	CS2B= COS(TBETTA)	2204570
	ONEC2B=(1.0+ CS2B)/2.	2204580
	SCB2 =(SNB-CS2B*SNB + 2.)/(2.0*CSB)	2204590
	SN2B =SIN(TBETTA) /2.	2204600
	XK12=XK11*XNUTP + (EASTH*SNB*ONEC2B/CSB)	2204610
	XK11=XK11+ EASTH*SCB2	2204620
	XK22=XK22+ EASTH*(CSB/SNB*ONEC2B)	2204630
	XK33=XK33+ EASTH* SN2B	2204640
	XC11= (EASTH*CTH* SCB2 )	2204650
	XC15=EASTH*CTH*( SNB* ONEC2B/CSB )	2204660
	XC16=EASTH*CTH*SN2B	2204670
	XC22= EASTH*CTH*( CSB/SNB * ONEC2B)	2204680
	XD12=-XD11*XNUTP- E1STH*(SNB*ONEC2B/CSB)	2204690
	XD11=-XD11- E1STH*SCB2	2204700
	XD22 = -XD22-E1STH*(CSB/SNB*ONEC2B)	2204710
	XD33= XD33+ E1STH*SN2B	2204720
	XK21 = XK12	2204730
	XD21 = XD12	2204740
C		2204750
C		2204760
108	XMERD = (DD-D2)*OMEGA*CS	2204770
	XPRES = -(DD-D2)*OMEGA*SN	2204780
	XMONT = -(D1*CTH+D3*YBARI+D4*YBARC+D5*YBARO)*OMEGA*CS	2204790
C		2204800
103	CONTINUE	2204810
	IF (KGEOM.NE.4) GO TO 105	2204820
	XMERD = 0.0	2204830
	XMONT = 0.0	2204840
105	CONTINUE	2204850

```

C
GOTO (716,714,715,714),KELVIN
716 TII = ST(NROW+1,LL)
TIK = ST(NROW+2,LL)
TOK = ST(NROW+3,LL)
TOO = ST(NROW+4,LL)
GOTO 717
715 TII = ST(NROW+1,LL)
TIK = TII
TOK = TII
TOO = TII

C
717 TEMP1 = ALPHTH+XNUTP*ALPHPH
TEMP2 = ALPHPH+XNUPT*ALPHTH
TEMP3 = 1-XNUPT*XNUTP
TEMP4 = HI/4.0
ETHK1 = ETHET*TEMP1/TEMP3
TEMP5 = HI**2/24.0
TEMP61= TII+ TIK-2* TEFREE
TEMP62= TOO+ TOK-2* TEFREE
TEMP71= 2.0* TII +TIK-3*TEFREE
TEMP72= 2.0* TOO +TOK-3*TEFREE
EPHK1 = EPHI*TEMP2/TEMP3
GO TO (811,812,813,814),THICK

C
814 GO TO (815,811,815,811,812,813,811,812,813,811,812,813),ISTTAB

C
811 XNTTH= ETHK1 * TEMP4 * (TEMP61+ TEMP62)
XNTPH= EPHK1 * TEMP4 * (TEMP61 + TEMP62)
XMTTH= ETHK1 * TEMP5 * (TEMP71- TEMP72)
XMTPH= EPHK1 * TEMP5 * (TEMP71 - TEMP72)
GO TO 816
812 TI = T/2.0
TEMP8= HI/2.0
XNTTH = ETHK1*TEMP8*(TEMP61+TEMP62)
XNTPH = EPHK1*TEMP8*(TEMP61+TEMP62)
XMTTH = ETHK1*TEMP8*(HI*(TEMP71-TEMP72)/3.0+TI*(TEMP61-TEMP62))
XMTPH = EPHK1*TEMP8*(HI*(TEMP71-TEMP72)/3.0+TI*(TEMP61-TEMP62))
GO TO 816
813 TI = (HO**2-HI**2+2.0*HO*T)/(2.0*(HI+HO))
TO = (HI**2-HO**2+2.0*HI*T)/(2.0*(HI+HO))
XNTTH = ETHK1/2.0*(HI*TEMP61+HO*TEMP62)
XNTPH = EPHK1/2.0*(HI*TEMP61+HO*TEMP62)
XMTTH = ETHK1/2.0*(HI**2*TEMP71/3.0-HO**2*TEMP72/3.0+TI*HI*TEMP61-
1 TO*HO*TEMP62)
XMTPH = EPHK1/2.0*(HI**2*TEMP71/3.0-HO**2*TEMP72/3.0+TI*HI*TEMP61-
1 TO*HO*TEMP62)
816 CONTINUE
IF (ISTTAB.EQ.2) GO TO 714
GO TO (817,818,819),KLUE2
817 XNTPH = XNTPH+ES*APH/SPH*ALPHS*TS
XNTTH = XNTTH+ER*ATH/STH*ALPHR*TR
XMTPH = XMTPH+CPH*ES*APH/SPH*ALPHS*TS
XMTTH = XMTTH+CTH*ER*ATH/STH*ALPHR*TR
GO TO 714
818 TEM = ES*APH/SPH*ALPHS*TS
XNTPH = XNTPH+TEM
XNTTH = XNTTH+TEM
XMTPH = XMTPH+CPH*TEM
XMTTH = XMTTH+CTH*TEM
GO TO 714

```

819	TEM = ES*APH/SPH*ALPHS*TS	2205470
	XNTPH = XNTPH+TEM*CSB/SNB	2205480
	XNTTH = XNTTH+TEM*(1.0+SNB)/CSB	2205490
	XMTPH = XMTPH+CPH*TEM*CSB/SNB	2205500
	XMTTH = XMTTH+CPH*TEM*(1.0+SNB)/CSB	2205510
	GO TO 714	2205520
815	TEMP10 = ((-XK11*XD11)**.5)/(48.0**.5)	2205530
	TEM11 = ((-XK22*XD22)**.5)/(48.0**.5)	2205540
	XNTTH = XK11/4.0*TEMP1*(TEMP61+TEMP62)	2205550
	XNTPH = XK22/4.0*TEMP2*(TEMP61+TEMP62)	2205560
	XMTTH = TEMP10*TEMP1*(TEMP71-TEMP72)	2205570
	XMTPH = TEM11*TEMP2*(TEMP71-TEMP72)	2205580
714	CONTINUE	2205590
8889	RETURN	2205600
	END	2205610

```

FOR,IS TEMOEG,TEMOEG
SUBROUTINE TEMOEG
THIS SUBROUTINE CALCULATES THE GEOMETRY FOR A SHELL SEGMENT.
THE INPUT VARIABLES ARE . . .
    RI(I) - - DISTANCE FROM AXIS OF REV. TO POINTS
                ON SHELL MERIDIAN.
    ZI(I) - - DISTANCE ALONG AXIS OF REV. TO THE
                INTERSECTION OF THE CORRESPONDING RI(I) AND
                THE AXIS OF REV.
    NRZIN - - NUMBER OF (RI,ZI) PAIRS READ AS INPUT.

COMMON /SNILPS/ ANG,PSI(100),RAD(100),CUR1(100),CUR2(100),
1   DR1OP(100),ZI(14),RI(14),NRZIN
DIMENSION CI(4,13),DRDZ(14),SOUT(14),S(101),RADD(100)

FUN(ARG) = SQRT(1.0 + ARG**2)

RADS = 3.1415926/180.0
DATA B/'B' '/'
AMULT = 1.0
IF (ANG.EQ.8) AMULT = -1.0

PASS SPLINE CURVE THROUGH INPUT POINTS ON SHELL MERIDIAN, AND
COMPUTE DR/DZ AT THESE POINTS.

CALL PLYCO (ZI,RI,NRZIN,CI)
NDELZ = NRZIN - 1
DO 60 I=1,NRZIN
CALL PLYNE (ZI,RI,NRZIN,CI,ZI(I),FAKE1,DRDZ(I),FAKE2)
60 CONTINUE

COMPUTE MERIDIONAL ARC LENGTH TO INTERPOLATED POINTS BY
NUMERICAL INTEGRATION (SIMPSONS RULE). SINCE SIMPSONS RULE
REQUIRES AN EVEN NUMBER OF PARTITIONS, INTERPOLATE A POINT
MIDWAY BETWEEN EACH PAIR OF POINTS USING SUBROUTINE PLINE.

SOUT(1) = 0.
DO 70 I=1,NDELZ
DZ2=(ZI(I+1)-ZI(I))/2.0
DZ6=DZ2/3.0
CALL PLYNE (ZI,RI,NRZIN,CI,ZI(I)+DZ2,FAKE1,DRDZM,FAKE2)
SOUT(I+1) = SOUT(I) + DZ6*(FUN(DRDZ(I)) + 4.0*FUN(DRDZM) +
1   FUN(DRDZ(I+1)))
70 CONTINUE

USE SPLICO TO REPRESENT RI(I) AS A FUNCTION OF SOUT(I). THEN USE
SPLINE TO INTERPOLATE RADD AND CORRESPONDING DERIVATIVES. FROM
THESE, COMPUTE THE TWO PRINCIPAL RADII OF CURVATURE,
    CUR1 = 1/R1
    CUR2 = 1/R2

OLDH1 = SOUT(NRZIN)/99.0
CALL PLYCO (SOUT,RI,NRZIN,CI)
DO 110 I=1,100
S(I) = FLOAT(I-1)*OLDH1
CALL PLYNE (SOUT,RI,NRZIN,CI,S(I),RAD(I),RADD(I),RADD2)
IF (ABS(RADD(I)).GT.1.0) RADD(I)=1.0
FACTOR = SQRT(1.0-RADD(I)**2)
CUR1(I) = -RADD2/FACTOR
CUR2(I) = FACTOR/RAD(I)

```

110 CONTINUE	2600600
DO 180 J=1,100	2600610
COSPSI = AMULT*RADD(J)	2600620
PSI(J) = ARCOS(COSPSI)	2600630
SINPSI = -AMULT*RAD(J)*CUR2(J)	2600640
IF (ANG.EQ.B) GO TO 179	2600650
PSI(J) = 2.0*3.1415926-PSI(J)	2600660
179 CONTINUE	2600670
CUR1(J) = -AMULT/CUR1(J)	2600680
CUR2(J) = -AMULT/CUR2(J)	2600690
IF (J.EQ.1) GO TO 180	2600700
I = 1	2600710
IF (J.EQ.2) GO TO 181	2600720
I = 2	2600730
181 IF (ANG.EQ.B) GO TO 190	2600740
DR1DP(J-1) = (CUR1(J)-CUR1(J-1))/(PSI(J)-PSI(J-1))	2600750
GO TO 180	2600760
190 DR1DP(J-1) = (CUR1(J-1)-CUR1(J))/(PSI(J-1)-PSI(J))	2600770
180 CONTINUE	2600780
DR1DP(100) = DR1DP(99)	2600790
DO 42 J=1,100	2600800
DR1DP(J) = DR1DP(J)*0.1	2600810
42 CONTINUE	2600820
RETURN	2600830
END	2600840

FOR, IS PLYCO, PLYCO	
SUBROUTINE PLYCO (X,Y,M,C)	2800010
C  SUBROUTINE TO DETERMINE C(1,K),C(2,K),C(3,K) AND C(4,K).	2800020
DIMENSION X(14),Y(14),A(14,3),B(14),Z(14)	2800030
DIMENSION D(13),P(13),E(13),C(4,13)	2800040
MM = M-1	2800050
DO 10 K=1,MM	2800060
D(K) = X(K+1) - X(K)	2800070
P(K) = D(K)/6.0	2800080
10  E(K) = (Y(K+1)-Y(K))/D(K)	2800090
DO 20 K=2,MM	2800100
20  B(K) = E(K) - E(K-1)	2800110
A(1,2) = -1.0-D(1)/D(2)	2800120
A(1,3) = D(1)/D(2)	2800130
A(2,3) = P(2)-P(1)*A(1,3)	2800140
A(2,2) = 2.0*(P(1)+P(2)) - P(1)*A(1,2)	2800150
A(2,3) = A(2,3)/A(2,2)	2800160
B(2) = B(2)/A(2,2)	2800170
DO 30 K=3,MM	2800180
A(K,2) = 2.0*(P(K-1)+P(K))-P(K-1)*A(K-1,3)	2800190
B(K) = B(K)-P(K-1)*B(K-1)	2800200
A(K,3) = P(K)/A(K,2)	2800210
30  B(K) = B(K)/A(K,2)	2800220
Q = D(M-2)/D(M-1)	2800230
A(M,1) = 1.0+Q+A(M-2,3)	2800240
A(M,2) = -Q-A(M,1)*A(M-1,3)	2800250
B(M) = B(M-2)-A(M,1)*B(M-1)	2800260
Z(M) = B(M)/A(M,2)	2800270
MN = M-2	2800280
DO 40 I=1,MN	2800290
K = M-I	2800300
40  Z(K) = B(K)-A(K,3)*Z(K+1)	2800310
Z(1) = -A(1,2)*Z(2)-A(1,3)*Z(3)	2800320
DO 50 K=1,MM	2800330
Q = 1.0/(6.0*D(K))	2800340
C(1,K) = Z(K)*Q	2800350
C(2,K) = Z(K+1)*Q	2800360
C(3,K) = Y(K)/D(K)-Z(K)*P(K)	2800370
50  C(4,K) = Y(K+1)/D(K)-Z(K+1)*P(K)	2800380
RETURN	2800390
END	2800400

FOR, IS PLYNE, PLYNE	
C SUBROUTINE PLYNE (X,Y,M,C,XINT,YINT,DYDX,D2YDX2)	2700010
C SUBROUTINE FOR SPLINE FIT INTERPOLATION IN THE TABLE OF VALUES	2700020
C (X1,Y1) TO (XM,YM), WHERE M MAY BE AS LARGE AS 100, HERE THE	2700030
C CONSTANTS C(1,K),C(2,K),C(3,K) AND C(4,K) ARE ALREADY COMPUTED	2700040
C AND STORED.	2700050
C SUBROUTINE ALSO COMPUTES DY/DX AND D2Y/DX2 AT XINT.	2700060
DIMENSION X(14),Y(14),C(4,13)	2700070
IF (XINT-X(1)) 80,10,20	2700080
10 YINT = Y(1)	2700090
K=1	2700100
GO TO 70	2700110
20 K = 1	2700120
30 IF (XINT-X(K+1)) 60,40,50	2700130
40 YINT = Y(K+1)	2700140
GO TO 70	2700150
50 K = K + 1	2700160
IF (M-K) 80,80,30	2700170
60 YINT = (X(K+1) - XINT)*(C(1,K)*(X(K+1)-XINT)**2+C(3,K))	2700180
YINT = YINT + (XINT-X(K))*(C(2,K)*(XINT-X(K))**2+C(4,K))	2700190
70 DYDX=-3.0*(C(1,K)*(X(K+1)-XINT)**2-C(2,K)*(XINT-X(K))**2)	2700200
1 -C(3,K)+C(4,K)	2700210
D2YDX2=6.0*(C(1,K)*(X(K+1)-XINT)+C(2,K)*(XINT-X(K)))	2700220
RETURN	2700230
80 WRITE (6,90)	2700240
90 FORMAT (31H OUT OF RANGE FOR INTERPOLATION)	2700250
RETURN	2700260
END	2700270



```

FOR,IS GRAPH,GRAPH
SUBROUTINE GRAPH (KGEOM)
COMMON /GRAFIX/ X(100),Y(100,9),NGRAPH,LDEF(9),NGR,JCYC,NFLAG,JAM,
C
COMMON /CDISP/ P
DIMENSION IDARY(22),YTITLE(12),YTIT(4,9),XTITLE(12)
DIMENSION TITLE(12),ALPHA(2)
DATA YTITLE/12* ' /
DATA TITLE/'REGION', ' NO.= ',2*6H ' , 'SEGMENT', 'T NO.= ',
1 2*6H ' , 'CYCLE ', 'NO.= ',2*6H /
DATA YTIT/'U ' ,3* ' ,
1 'V ' ,3* ' ,
2 'W ' ,3* ' ,
3 'SIGMA ' , 'THETA ' , 'IN ' , ' ' ,
4 'SIGMA ' , 'PHI IN', ' ' , ' ' ,
5 'TAU PH', 'I THET', 'A IN ' , ' ' ,
6 'SIGMA ' , 'THETA ' , 'OUT ' , ' ' ,
7 'SIGMA ' , 'PHI OU', 'T ' , ' ' ,
8 'TAU PH', 'I THET', 'A OUT ' , ' ' /
DATA XTITLE/'DISTAN', 'CE ALO', 'NG SEG', 'MENT (' /
DATA A/'PHI)'/,B/'S) ' /
EXTERNAL TABLIV
IF (NFLAG.NE.0) GO TO 1
CALL IDENT (9,IDARY)
NFLAG = 1
1 CONTINUE
CALL CHSIZV (2,2)
CALL RITSTV (13,19,TABLIV)
XMN = X(1)
XMX = X(1)
DO 20 J=1,JCYC
IF (X(J).LT.XMN) XMN = X(J)
IF (X(J).GT.XMX) XMX = X(J)
20 CONTINUE
CALL SCRND (XMX,XMN,XMAX,XMIN)
INDEX = 0
DO 100 K=1,9
IF (LDEF(K).EQ.0) GO TO 100
INDEX = INDEX+1
YMN = Y(1,INDEX)
YMX = Y(1,INDEX)
DO 30 L=1,JCYC
IF (Y(L,INDEX).LT.YMN) YMN = Y(L,INDEX)
IF (Y(L,INDEX).GT.YMX) YMX = Y(L,INDEX)
30 CONTINUE
CALL SCRND (YMX,YMN,YMAX,YMIN)
IF (KGEOM.EQ.3.OR.KGEOM.EQ.4) GO TO 1234
XTITLE(5) = A
GO TO 1235
1234 XTITLE(5) = B
1235 CONTINUE
DO 45 M=1,4
45 YTITLE(M) = YTIT(M,K)
CALL QUIK3L (-1,XMIN,XMAX,YMIN,YMAX,1H*,XTITLE,YTITLE,-JCYC,X,
1 Y(1,INDEX))
ENCODE (801,ALPHA) JAM,JNSC
801 FORMAT(2I6)
TITLE(3) = ALPHA(1)
TITLE(7) = ALPHA(2)
KCYC = P

```

```
      ENCODE (802,ALPHA) KCYC
802  FORMAT(I6)
      TITLE(11) = ALPHA(1)
      CALL RITE2V (46,1005,1023,90,1,72,1,TITLE,IERR)
      IF (IERR.NE.0) WRITE(6,800) IERR
800  FORMAT(' IERR =',I3,' CHARACTER COUNT WHERE WRITING WAS STOPPED')
100  CONTINUE
      RETURN
      END
```

## SUBROUTINES ODE1 AND ODE2

Subroutine LEBEGE calls either ODE1 or ODE2, as necessary, and various geometric and trigonometric clues, as well as the predicted values of the variables for the differential equations, are passed to this subprogram via label common area LASTEQ.

The equations in ODE1 and ODE2 are identical to those in subroutines DIF1 and DIFF2 respectively. Subroutines ODE1 and ODE2 perform the final integration for each segment in the structure utilizing the initial conditions previously obtained, and return these values to LEBEGE via label common area LASTEQ.

-----

The ODE1, ODE2 flow charts are identical to the DIF1, DIFF2 flow charts respectively.

FORTRAN CODE

ENGINEERING SYMBOLS (REF. 1)

YANPT

$N_{\phi\theta}$

YAQPH

$Q_{\phi}$

YAQTH

$Q_{\theta}$

YAOPH

$\Omega_{\phi}$

```

FOR, IS ODE1, ODE1
SUBROUTINE ODE1
INTEGER SAVJTC, SAVSTP, Q, THICK
INTEGER XN1, XN
REAL K
DOUBLE PRECISION YPRED
COMMON STORY(16), XMAT(270, 10), STD(10), SADUS(30), RADUS(30)
COMMON TADUS(30), UADUS(30), SAVTIC(900)
COMMON XN, TEFREE, TIC, PHI, STOP, RESTOP, RTICK, G1, XNL(3), NH
COMMON NST(30), NKL(30), NXMAT(20), SAVJTC(30), SAVSTP(30), JRTIC(30)
COMMON JRSTOP(30), NREG, NMPT, NRC, NSC, NIX, IERROR, KGEOM, IGEOM, I STTAB
COMMON KELVIN, IBEGIN, NPROB, NSEG, NERROR, Q, THICK, NOJS, NLINKS, NLCASE
COMMON NTSKL, NZ, NBCT, LINPUT, NTRKL, NPASS, XN1, KBC, NRINGS
COMMON LODE, ICYCLE, LDISTL
COMMON /LASTEQ/ YPRED(8), YDOT(8), YASAVE(8),
1 YANTH, YAMTH, YAMPT, YANPT, YAOPH, YAQPH, YAQTH, YAJPH,
2 S, SN, CS, SNSQ, CSSQ, TAN, SEC, CN, X1CS, X1SN, TN,
3 X1RO, X1ROSQ, X1SNRO, X1CSRO, CN1RO, SN1RO, CS1RO,
4 X1R1, X1R2, CS1R1, CS1R2, SN1R1, X1R1SQ, R2SQ, RO, BESQ,
5 ROSQ, XNSQ, BETA, R1, R2, S1, R1DOT, R1SQ,
6 XNTTH, XNTPH, XMTTH, XMPH, XFTHLD, XFPHLD, XFZELD,
7 XMTHLD, XMPHLD, ETHET, EPHI, XGPT, ALPHTH, ALPHPH,
8 XNUTP, XNUPT, XC11, XC22, XC15, XD33, XD22, XD21, XD12,
9 XK11, XK12, XK21, XK22, XK33, XD11,
A M, I, SITIN, SITOUT, SIPIN, SIPOUT, TPTIN, TPTOUT,
B ZBRIN, ZBROUT, SCRIPA, SCRIP1, SIFIN, SIFOUT, TZEPH, TZETH
B , XNPHI, BETTA, ZETTA, XC16
C , RMOS, RMOSN, YLDST, ROC, HP, FPLUH, GPLUH, TWON
D , RMOSY, RMOSNY, RMOSXY, RMONXY
D , RMOSNS, RMOSNS, SIGXNS, RMOSNR, RMOSNR, SIGXNR
COMMON /PLS/ OMEGA, IWORD, XMERD, XPRES, XMONT
COMMON /WOOD/ SAVY(53), NPLEV, NLPO, NPLA(21), STR(6), SIGMA(3, 21),
C SEPS(3, 21), SALPH(3, 21), SBAPH(3, 21), STEPS(3, 21),
O EFF(21), STSRN(3), NPLAST(3), STSIG(3), STREPS(3),
M STALPH(3), STBAPH(3), EFFST(3), NPLEVS(3)
COMMON /CDISP/ P, PMAX, DELP, DELP1, YEPS, ZEPS
EQUIVALENCE (XNL(1), X1), (XNL(2), X2), (XNL(3), X3), (K, DELP)
IF (ISTTAB.NE.2) GO TO 7786
C THE FOLLOWING EQUATIONS ARE THE 'THICK' SET
GO TO (151, 152, 153), IGEOM
C EQUATIONS FOR SHELLS OF REVOLUTION ( PHI COORDINATE )
151 CONTINUE
YAOPH = XN*YPRED(I+6)*X1RO-YPRED(I+4)*SN1RO
YANTH = XNUPT*YPRED(I+1)+(XK11-XNUPT**2*XK22)*((XN*YPRED(I+4)+
1 YPRED(I+5)*CS-YPRED(I+6)*SN)*X1RO+X1*YAOPH*SAVY(9))+K*
2 (XNUPT*XNTPH-XNTTH)+X2*(XNUPT*SAVY(11)-SAVY(10))
3 +X3*SAVY(48)
YAMTH = XNUPT*YPRED(I+3)-(XD11-XNUPT**2*XD22)*X1RO*(X1RO*(XN*
1 YPRED(I+4)*SN-XNSQ*YPRED(I+6))+YPRED(I+7)*CS)+K*
2 (XNUPT*XMPH-XMTTH)+X2*(XNUPT*SAVY(14)-SAVY(13))
3 +X3*SAVY(49)
YAMPT = (-1.0/((RO/XD33)+(SNSQ*X1RO/XK33)))*(-2.0*XN*
1 YPRED(I+7)+YPRED(I+4)*(CS1R1-CN1RO)+XN*YPRED(I+5)*
2 (SN1RO*X1R1)+2.0*XN*YPRED(I+6)*CS1RO+YPRED(I)*SN/
3 XK33+X2*(SAVY(12)*SN/XK33-SAVY(15)*RO/XD33)+SN*X1*
4 (YAOPH*SAVY(5)+SAVY(9)*YPRED(I+7)))
5 +X3*SAVY(50)
YANPT = YPRED(I)+YAMPT*SN1RO
YAJPH = YPRED(I+2)+X1*(SAVY(8)*YAOPH+YANPT*SAVY(9)-YPRED(I+1)
1 *SAVY(5)-YPRED(I+7)*SAVY(6))
YDOT(I+4) = R1*(YPRED(I+4)*CS1RO+XN*YPRED(I+5)*X1RO+YPRED(I)/XK33+

```

```

1      X2*SAVY(12)/XK33+YAMPT*SN1RO/XK33)+R1*X1*(YAOPH*      2000610
2      SAVY(5)+YPRED(I+7)*SAVY(9))      2000620
3      +X3*SAVY(51)      2000630
   YDOT(I+5) = R1*(YPRED(I+6)*X1R1+(1.0/(XK22-XNUTP**2*XK11))*      2000640
1      (YPRED(I+1)-XNUTP*YANTH+K*(XNTPH-XNUTP*XNTTH))+X2*      2000650
2      (SAVY(11)-XNUTP*SAVY(10))) -R1*YPRED(I+7)*X1*SAVY(5)      2000660
3      +X3*SAVY(52)      2000670
   A =      2000680
1      YPRED(I+5)*CS1RO-YPRED(I+6)*SN1RO+SAVY(9)*YAOPH+      2000690
   YDOT(I+5)/R1-YPRED(I+6)/R1+SAVY(5)*YPRED(I+7)
   B =      2000700
1      SAVY(1)*CS1RO-SAVY(3)*SN1RO+.5*(SAVY(9)*SAVY(9)      2000710
   +SAVY(5)*SAVY(5))+(SAVY(2)-SAVY(3))/R1
   YDOT(I) = R1*(-2.0*YPRED(I)*CS1RO+XN*YANTH*X1RO-XN*YAMTH*SN*      2000720
1      X1ROSQ-YAMPT*CS1RO*(X1R1-SN1RO))-R1*K*(XFTHLD+XMPHLD*      2000730
2      SN1RO)-R1*X1*(SAVY(24)*A+K*XFTHLD*B+SAVY(25)*YDOT(I+4)      2000740
3      /R1+SAVY(4)*K*XFPHLD/R1+SAVY(26)*YAOPH+SAVY(9)*K*      2000750
4      XFZELD+SN/RO*(YANTH*SAVY(9)+YAOPH*SAVY(7)-YPRED(I+7)*      2000760
5      SAVY(8)-YANPT*SAVY(5))) -X3*SAVY(33)      2000770
   YDOT(I+1) = R1*(CS1RO*(YANTH-YPRED(I+1))-XN*X1RO*(YPRED(I)+      2000780
1      YAMPT*(SN*X1RO+X1R1))+YPRED(I+2)*X1R1)-R1*K*XFPHLD      2000790
2      -R1*X1*(SAVY(25)*A+K*XFPHLD*B      2000800
3      -SAVY(26)*YPRED(I+7)-SAVY(5)*K*XFZELD)      2000810
4      -X3*SAVY(34)      2000820
   YDOT(I+2) = R1*(-YPRED(I+2)*CS1RO-YANTH*SN1RO-YPRED(I+1)*X1R1      2000830
1      +XNSQ*YAMTH*X1ROSQ-2.0*XN*YAMPT*CS*X1ROSQ)+R1*K*      2000840
2      (XN*XMPHLD*X1RO-XFZELD)-R1*X1*(SAVY(26)*A+K*XFZELD*      2000850
3      B-SAVY(24)*YAOPH-SAVY(9)*K*      2000860
4      XFTHLD+SAVY(25)*YPRED(I+7)+SAVY(5)*K*XFPHLD)      2000870
5      -X3*SAVY(35)      2000880
   YDOT(I+3) = R1*(YAMTH*CS1RO-YPRED(I+3)*CS1RO-2.0*XN*YAMPT*X1RO+      2000890
1      YAJPH+K*XMTHLD)      2000900
2      +X3*SAVY(36)      2000910
   YDOT(I+6) = R1*(YPRED(I+7)-YPRED(I+5)*X1R1)      2000920
   YDOT(I+7) = R1*(1.0/(XD22-XNUTP**2*XD11))*(-YPRED(I+3)+XNUTP*      2000930
1      YAMTH-K*(XNTPH-XNUTP*XMTTH)-X2*(SAVY(14)-XNUTP*      2000940
2      SAVY(13)))      2000950
3      +X3*SAVY(53)      2000960
   GOTO 9005      2000970
C      EQUATIONS FOR CONE      2000980
152 CONTINUE      2000990
   YAOPH = XN*YPRED(I+6)*X1CS/S-YPRED(I+4)*TAN/S      2001000
   YANTH =      2001010
1      XNUTP*YPRED(I+1)+(XK11-XNUTP**2*XK22)*((X1CS/S)*(XN*      2001020
2      YPRED(I+4)+YPRED(I+5)*CS-YPRED(I+6)*SN)+X1*YAOPH*      2001030
3      SAVY(9))+K*(XNUTP*XNTPH-XNTTH)+X2*(XNUTP*SAVY(11)-      2001040
4      SAVY(10))      2001050
   +X3*SAVY(48)
   YAMTH=XNUTP*YPRED(I+3)-(1.0/S)*X1CS*(XD11-XNUTP**2*XD22)*((1.0/S)*      2001060
1      X1CS*(XN*YPRED(I+4)*SN-XNSQ*YPRED(I+6))+YPRED(I+7)*CS)-      2001070
2      K*(XMTTH-XNUTP*XMTPH)      2001080
3      +X2*(XNUTP*SAVY(14)-SAVY(13))      2001090
4      +X3*SAVY(49)      2001100
   YAMPT=(-1.0/((S*CS/XD33)+(SN*TN/(XK33*S))))*(-2.0*XN*YPRED(I+7)-      2001110
1      YPRED(I+4)*SN/S+XN*YPRED(I+5)*TN/S+2.0*XN*YPRED(I+6)/S+YPRED      2001120
2      (I)*SN/XK33+X2*(SAVY(12)*SN/XK33-SAVY(15)*S*CS/XD33)      2001130
3      +SN*X1*(YAOPH*      2001140
4      SAVY(5)+SAVY(9)*YPRED(I+7)))      2001150
5      +X3*SAVY(50)      2001160
   YANPT = YPRED(I)+YAMPT*TAN/S      2001170
   YAJPH =      2001180
1      YPRED(I+2)+X1*(SAVY(8)*YAOPH+YANPT*SAVY(9)-YPRED(I+1))*      2001190
   SAVY(5)-YPRED(I+7)*SAVY(6))
   YDOT(I+4)=(1.0/S)*(YPRED(I+4)+XN*YPRED(I+5)*X1CS+YAMPT*TN/XK33)      2001200
1      +YPRED(I)/XK33+X2*SAVY(12)/XK33+X1*(YAOPH*SAVY(5)      2001210

```

```

2      +YPRED(I+7)*SAVY(9))      2001220
3      +X3*SAVY(51)      2001230
YDOT(I+5) = (1.0/(XK22-XNUTP**2*XK11))*(YPRED(I+1)-XNUTP*YANTH+
1      K*(XNTPH-XNUTP*XNTTH)+X2*(SAVY(11)-XNUTP*SAVY(10)))      2001240
2      -YPRED(I+7)*X1*SAVY(5)      2001250
3      +X3*SAVY(52)      2001260
A = YPRED(I+5)/S-YPRED(I+6)*TN/S+SAVY(9)*YAOPH+YDOT(I+5)      2001270
1      +SAVY(5)*YPRED(I+7)      2001280
B = SAVY(1)/S-SAVY(3)*TN/S+0.5*(SAVY(9)*SAVY(9)+SAVY(5)*
1      SAVY(5))+SAVY(2)      2001290
YDOT(I) = -2.0*YPRED(I)/S+XN*YANTH*X1CS/S-XN*YAMTH*SN*X1CS**2/S**2
1      +YAMPT*TAN/S**2-K*(XFTHLD+XMPHLD*TAN/S)-X1*(SAVY(24)*      2001300
2      A+K*XFTHLD*B+SAVY(25)*YDOT(I+4)+SAVY(4)*K*XFPHLD+      2001310
3      SAVY(26)*YAOPH+SAVY(9)*K*XFZELD*TAN/S*(YANTH*SAVY(9)+      2001320
4      YAOPH*SAVY(7)-YPRED(I+7)*SAVY(8)-YANPT*SAVY(5))-X3*      2001330
5      SAVY(33)      2001340
YDOT(I+1) = -YPRED(I+1)/S+YANTH/S-XN*YPRED(I)/(S*CS)-XN*YAMPT*SN/
1      (S*S*CS*CS)-K*XFPHLD-X1*(SAVY(25)*A+K*XFPHLD*B-      2001350
2      SAVY(26)*YPRED(I+7)-SAVY(5)*K*XFZELD)      2001360
3      -X3*SAVY(34)      2001370
YDOT(I+2) = -YPRED(I+2)/S-YANTH*TAN/S+XNSQ*YAMTH/(S**2*CS**2)
1      -2.0*XN*YAMPT/(S**2*CS)+K*(XN*XMPHLD*X1CS/S-XFZELD)      2001380
2      -X1*(SAVY(26)*A+K*XFZELD*B-SAVY(24)*YAOPH-SAVY(9)*K*      2001390
3      XFTHLD+SAVY(25)*YPRED(I+7)+SAVY(5)*K*XFPHLD)      2001400
4      -X3*SAVY(35)      2001410
YDOT(I+3) = YAMTH/S-YPRED(I+3)/S-2.0*XN*YAMPT/(S*CS)+YAJPH+XMTHLD
1      *K      2001420
2      +X3*SAVY(36)      2001430
YDOT(I+6) = YPRED(I+7)      2001440
YDOT(I+7) = (1.0/(XD22-XNUTP**2*XD11))*(-YPRED(I+3)+XNUTP*YAMTH-
1      K*(XNTPH-XNUTP*XMTTH)-X2*(SAVY(14)-XNUTP*SAVY(13)))      2001450
2      +X3*SAVY(53)      2001460
GO TO 9005      2001470
C EQUATIONS FOR CYLINDER      2001480
153 CONTINUE      2001490
YAOPH = X1RO*(XN*YPRED(I+6)-YPRED(I+4))      2001500
YANTH = XNUPT*YPRED(I+1)+(XK11-XNUPT**2*XK22)*((X1RO*(XN*
1      YPRED(I+4)-YPRED(I+6)))+X1*YAOPH*SAVY(9))+K*(XNUPT*
2      XNTPH-XNUTP*XNTTH)+X2*(XNUPT*SAVY(11)-SAVY(10))      2001510
3      +X3*SAVY(48)      2001520
YAMTH = XNUPT*YPRED(I+3)-(X1RO*(XD11-XNUPT**2*XD22))*((X1RO*(XN*YPRED
1      (I+4)-XNSQ*YPRED(I+6)))+K*(XNUPT*XMTPH-XMTTH)      2001530
2      +X2*(XNUPT*SAVY(14)-SAVY(13))      2001540
3      +X3*SAVY(49)      2001550
YAMPT = (-1.0/((RO/XD33)+(X1RO/XK33)))*(-2.0*XN*YPRED(I+7)+XN*X1RO*
1      YPRED(I+5)+YPRED(I)/XK33+X2*(SAVY(12)/XK33-SAVY(15))*      2001560
2      RO/XD33)+X1*(YAOPH*SAVY(5)+SAVY(9)*YPRED(I+7)))      2001570
3      +X3*SAVY(50)      2001580
YANPT = YPRED(I)+YAMPT*X1RO      2001590
YAJPH = YPRED(I+2)+X1*(SAVY(8)*YAOPH+YANPT*SAVY(9)-YPRED(I+1)
1      *SAVY(5)-YPRED(I+7)*SAVY(6))      2001600
YDOT(I+4) = XN*YPRED(I+5)*X1RO+YPRED(I)/XK33+X2*SAVY(12)/XK33+
1      YAMPT*X1RO/XK33+X1*(YAOPH*SAVY(5)+YPRED(I+7)*SAVY(9))
2      +X3*SAVY(51)      2001610
YDOT(I+5) = (1.0/(XK22-XNUTP**2*XK11))*(YPRED(I+1)-XNUTP*YANTH+
1      K*(XNTPH-XNUTP*XNTTH)+X2*(SAVY(11)-XNUTP*SAVY(10))-
2      YPRED(I+7)*X1*SAVY(5)      2001620
3      +X3*SAVY(52)      2001630
A = -YPRED(I+6)/RO+SAVY(9)*YAOPH+YDOT(I+5)+SAVY(5)*
1      YPRED(I+7)      2001640
B = -SAVY(3)/RO+0.5*(SAVY(9)*SAVY(9)+SAVY(5)*SAVY(5))+
2001650
2001660
2001670
2001680
2001690
2001700
2001710
2001720
2001730
2001740
2001750
2001760
2001770
2001780
2001790
2001800
2001810
2001820

```

```

1          SAVY(2) 2001830
YDOT(I) = XN*YANTH*XIRO-XN*YAMTH*XIROSQ-K*(XFTHLD+XMPHLD*XIRO) 2001840
1          -X1*(SAVY(24)*A+K*XFTHLD*B+SAVY(25)*YDOT(I+4)+SAVY(4)* 2001850
2          K*XFPHLD+SAVY(26)*YAOPH+SAVY(9)*K*XFZELD+(YANTH* 2001860
3          SAVY(9)+YAOPH*SAVY(7)-YPRED(I+7)*SAVY(8)-YANPT* 2001870
4          SAVY(5))/RO)-X3*SAVY(33) 2001880
YDOT(I+1) = -XN*XIRO*YPRED(I)-XN*YAMPT*XIROSQ-K*XFPHLD-X1* 2001890
1          (SAVY(25)*A+K*XFPHLD*B-SAVY(26)*YPRED(I+7)-SAVY(5)* 2001900
2          K*XFZELD) 2001910
3          -X3*SAVY(34) 2001920
YDOT(I+2) = -YANTH*XIRO+XNSQ*YAMTH*XIROSQ+K*(XN*XMPHLD*XIRO- 2001930
1          XFZELD)-X1*(SAVY(26)*A+K*XFZELD*B-SAVY(24)*YAOPH- 2001940
2          SAVY(9)*K*XFTHLD+SAVY(25)*YPRED(I+7)+SAVY(5)*K*XFPHLD) 2001950
3          -X3*SAVY(35) 2001960
YDOT(I+3) = -2.0*XN*YAMPT*XIRO+YAJPH+K*XMTHLD 2001970
1          +X3*SAVY(36) 2001980
YDOT(I+6)=YPRED(I+7) 2001990
YDOT(I+7) = (1.0/(XD22-XNUTP**2*XD11))*(-YPRED(I+3)+XNUTP*YAMTH+ 2002000
1          K*(XNUTP*XMTTH-XMTPH)-X2*(SAVY(14)-XNUTP*SAVY(13))) 2002010
2          +X3*SAVY(53) 2002020
GO TO 9005 2002030
7786 GO TO (4771,4772,4773),IGEOM 2002040
C THE FOLLOWING EQUATIONS ARE THE 'ST10' SET 2002050
C EQUATIONS FOR SHELLS OF REVOLUTION ( PHI COORDINATE ) 2002060
4771 CONTINUE 2002070
YAOPH = XN*YPRED(I+6)*XIRO-YPRED(I+4)*SNIRO 2002080
YANTH = XK12*(1.0/(XK22+XC22**2/XD22))*(YPRED(I+1)+K*XNTPH+ 2002090
1          X2*SAVY(11)+(XC22/XD22)*(YPRED(I+3)+K*XMTPH+X2* 2002100
1          SAVY(14)))-K*XNTTH-X2*SAVY(10)+(XIRO*XK11- 2002110
1          XK12*XK21*XIRO*(1.0/ 2002120
2          (XK22+XC22**2/XD22)))*(XN*YPRED(I+4)+YPRED(I+5)*CS-YPRED(I+ 2002130
3          6)*SN+X1*RO*YAOPH*SAVY(9))-(XC11+XK12*XC22*XD21/XD22* 2002140
3          (1.0/(XK22+XC22**2/XD22)))* 2002150
4          (XIRO**2*(XN*YPRED(I+4)*SN-XN**2*YPRED(I+6))+YPRED(I+7)*CS* 2002160
5          XIRO) 2002170
6          +X3*SAVY(48) 2002180
YAMTH = -XD12*(XC22/(XC22**2+XK22*XD22))*(YPRED(I+1)+K*XNTPH+ 2002190
1          X2*SAVY(11))-K*XMTTH-X2*SAVY(13)+XD12*(XK22/(XC22**2+ 2002200
2          XK22*XD22))*(YPRED(I+3)+K*XMTPH+X2*SAVY(14))+(XC11* 2002210
3          XIRO+XD12*XK21*XIRO*(XC22/(XC22**2+XK22*XD22)))*(XN*YPRED( 2002220
3          I+4)+YPRED(I+5)*CS-YPRED(I+6)*SN+X1*RO*YAOPH*SAVY(9))+ 2002230
3          (XD11-XD12*XK22*XD21/( 2002240
4          XC22**2+XK22*XD22))*(XIROSQ*(XN*YPRED(I+4)*SN-XNSQ*YPRED 2002250
5          (I+6))+YPRED(I+7)*CS*XIRO) 2002260
6          +X3*SAVY(49) 2002270
YAMPT = (-1.0/((RO/XD33)+(SNSQ*XIRO/XK33)))*(-2.0*XN* 2002280
1          YPRED(I+7)+YPRED(I+4)*(CS1R1-CN1RO)+XN*YPRED(I+5)* 2002290
2          (SNIRO+X1R1)+2.0*XN*YPRED(I+6)*CS1RO+YPRED(I)*SN/ 2002300
3          XK33+X2*(SAVY(12)*SN/XK33-SAVY(15)*RO/XD33)+SN*X1* 2002310
4          (YAOPH*SAVY(5)+SAVY(9)*YPRED(I+7))) 2002320
5          +X3*SAVY(50) 2002330
YANPT = YPRED(I)+YAMPT*SNIRO 2002340
YAJPH = YPRED(I+2)+X1*(SAVY(8)*YAOPH+YANPT*SAVY(9)-YPRED(I+1) 2002350
1          *SAVY(5)-YPRED(I+7)*SAVY(6)) 2002360
YDOT(I+4) = R1*(YPRED(I+4)*CS1RO+XN*YPRED(I+5)*XIRO+YPRED(I)/XK33+ 2002370
1          X2*SAVY(12)/XK33+YAMPT*SNIRO/XK33)+R1*X1*(YAOPH* 2002380
2          SAVY(5)+YPRED(I+7)*SAVY(9)) 2002390
3          +X3*SAVY(51) 2002400
YDOT(I+5) = R1*(YPRED(I+6)*X1R1-X1*YPRED(I+7)*SAVY(5)+(1.0/(XK22+ 2002410
1          XC22**2/XD22))*(YPRED(I+1)+K*XNTPH+X2*SAVY(11)+(XC22/ 2002420
1          XD22)*(YPRED(I+3)+K*XMTPH+X2*SAVY(14))-XK21*XIRO*(XN* 2002430

```



```

2          YPRED(I+4)+YPRED(I+5)*CS-YPRED(I+6)*SN)-X1*XK12*YAOPH* 2002440
2          SAVY(9)-(XC22*XD21/XD22 2002450
3          )*(X1ROSQ*(XN*YPRED(I+4)*SN-XNSQ*YPRED(I+6))+YPRED(I+7) 2002460
4          *CS*X1RO))) 2002470
5          +X3*SAVY(52) 2002480
A =        YPRED(I+5)*CS1RO-YPRED(I+6)*SN1RO+SAVY(9)*YAOPH+ 2002490
1          YDOT(I+5)/R1-YPRED(I+6)/R1+SAVY(5)*YPRED(I+7) 2002500
B =        SAVY(1)*CS1RO-SAVY(3)*SN1RO+.5*(SAVY(9)*SAVY(9) 2002510
1          +SAVY(5)*SAVY(5))+(SAVY(2)-SAVY(3))/R1 2002520
YDOT(I)   = R1*(-2.0*YPRED(I)*CS1RO+XN*YANTH*X1RO-XN*YAMTH*SN* 2002530
1          X1ROSQ-YAMPT*CS1RO*(X1R1-SN1RO))-R1*K*(XFTHLD+XMPHLD* 2002540
2          SN1RO)-R1*X1*(SAVY(24)*A+K*XFTHLD*B+SAVY(25)*YDOT(I+4) 2002550
3          /R1+SAVY(4)*K*XFPHLD/R1+SAVY(26)*YAOPH+SAVY(9)*K* 2002560
4          XFZELD+SN/RO*(YANTH*SAVY(9)+YAOPH*SAVY(7))-YPRED(I+7)* 2002570
5          SAVY(8)-YANPT*SAVY(5))-X3*SAVY(33) 2002580
YDOT(I+1) = R1*(CS1RO*(YANTH-YPRED(I+1))-XN*X1RO*(YPRED(I)+ 2002590
1          YAMPT*(SN*X1RO+X1R1))+YPRED(I+2)*X1R1)-R1*K*XFPHLD 2002600
2          -R1*X1*(SAVY(25)*A+K*XFPHLD*B 2002610
3          -SAVY(26)*YPRED(I+7)-SAVY(5)*K*XFZELD) 2002620
4          -X3*SAVY(34) 2002630
YDOT(I+2) = R1*(-YPRED(I+2)*CS1RO-YANTH*SN1RO-YPRED(I+1)*X1R1 2002640
1          +XNSQ*YAMTH*X1ROSQ-2.0*XN*YAMPT*CS*X1ROSQ)+R1*K* 2002650
2          (XN*XMPHLD*X1RO-XFZELD)-R1*X1*(SAVY(26)*A+K*XFZELD* 2002660
3          B-SAVY(24)*YAOPH-SAVY(9)*K* 2002670
4          XFTHLD+SAVY(25)*YPRED(I+7)+SAVY(5)*K*XFPHLD) 2002680
5          -X3*SAVY(35) 2002690
YDOT(I+3) = R1*(YAMTH*CS1RO-YPRED(I+3)*CS1RO-2.0*XN*YAMPT*X1RO+ 2002700
1          YAJPH+K*XMTHLD) 2002710
2          +X3*SAVY(36) 2002720
YDOT(I+6) = R1*(YPRED(I+7)-YPRED(I+5)*X1R1) 2002730
YDOT(I+7) = R1*((-XC22/(XC22**2+XK22*XD22))*(YPRED(I+1)+K*XNTPH+ 2002740
1          X2*SAVY(11)-(XK21/RO)*(XN*YPRED(I+4)+YPRED(I+5)*CS- 2002750
1          YPRED(I+6)*SN)-X1*XK12*YAOPH*SAVY(9))+XK22/(XC22**2+ 2002760
2          XK22*XD22))*(YPRED(I+3)+K*XNTPH+X2*SAVY(14))-(XK22* 2002770
3          XD21/(XC22**2+XK22*XD22))*(X1ROSQ*(XN*YPRED(I+4)*SN-XNSQ 2002780
4          *YPRED(I+6))+YPRED(I+7)*CS*X1RO)) 2002790
5          +X3*SAVY(53) 2002800
GO TO 9005 2002810
C          EQUATIONS FOR CONE 2002820
4772 CONTINUE 2002830
YAOPH     = XN*YPRED(I+6)*X1CS/S-YPRED(I+4)*TAN/S 2002840
YANTH     = XK12*(1.0/(XK22+XC22**2/XD22))*(YPRED(I+1)+K*XNTPH+ 2002850
1          X2*SAVY(11)+(XC22/XD22)*(YPRED(I+3)+K*XMTPH+X2* 2002860
1          SAVY(14))-K*XNTTH-X2*SAVY(10)+(1.0/ICS*S)) 2002870
1          *(XK11-XK12*XK21*( 2002880
2          1.0/(XK22+XC22**2/XD22))*(XN*YPRED(I+4)+YPRED(I+5)*CS- 2002890
3          YPRED(I+6)*SN+X1*S*CS*YAOPH*SAVY(9))-(XC11+(XK12*XD21* 2002900
3          XC22/XD22)*(1.0/(XK22+XC22* 2002910
4          *2/XD22)))*((1.0/(S**2*CS**2))*(XN*YPRED(I+4)*SN-XNSQ*YPRED 2002920
5          (I+6))+YPRED(I+7)/S) 2002930
6          +X3*SAVY(48) 2002940
YAMTH     = -XD12*(XC22/(XC22**2+XK22*XD22))*(YPRED(I+1)+K*XNTPH+ 2002950
1          X2*SAVY(11))-K*XMTTH-X2*SAVY(13)+XD12*(XK22/(XC22**2+ 2002960
1          XK22*XD22))*(YPRED(I+3)+K*XMTPH+X2*SAVY(14))+XC11/ 2002970
2          (S*CS)+XD12*XK21/(S*CS))*(XC22/(XC22**2+XK22*XD22))*(XN* 2002980
3          YPRED(I+4)+YPRED(I+5)*CS-YPRED(I+6)*SN+X1*S*CS*YAOPH* 2002990
3          SAVY(9))+(XD11-XD12*XK22* 2003000
4          XD21/(XC22**2+XK22*XD22))*((1.0/(S*CS)**2)*(XN*YPRED(I+4)* 2003010
5          SN-XNSQ*YPRED(I+6))+YPRED(I+7)/S) 2003020
6          +X3*SAVY(49) 2003030
YAMPT     = (-1.0/(S*CS/XD33)+(SN*TN/(XK33*S)))*(-2.0*XN*YPRED(I+7)- 2003040

```

```

1      YPRED(I+4)*SN/S+XN*YPRED(I+5)*TN/S+2.0*XN*YPRED(I+6)/S+YPRED 2003050
2      (I)*SN/XK33+X2*(SAVY(12)*SN/XK33-SAVY(15)*S*CS/XD33) 2003060
3      +SN*X1*(YAOPH* 2003070
4      SAVY(5)+SAVY(9)*YPRED(I+7)) 2003080
5      +X3*SAVY(50) 2003090
YANPT = YPRED(I)+YAMPT*TAN/S 2003100
YAJPH = YPRED(I+2)+X1*(SAVY(8)*YAOPH+YANPT*SAVY(9)-YPRED(I+1)* 2003110
1      SAVY(5)-YPRED(I+7)*SAVY(6)) 2003120
YDOT(I+4)=(1.0/S)*(YPRED(I+4)+XN*YPRED(I+5)*X1CS+YAMPT*TAN/XK33) 2003130
1      +YPRED(I)/XK33+X2*SAVY(12)/XK33+X1*(YAOPH*SAVY(5) 2003140
2      +YPRED(I+7)*SAVY(9)) 2003150
3      +X3*SAVY(51) 2003160
YDOT(I+5) = -X1*YPRED(I+7)*SAVY(5)+(1.0/(XK22+XC22**2/XD22))* 2003170
1      (YPRED(I+1)+K*XNTPH+X2*SAVY(11)+(XC22/XD22)* 2003180
2      (YPRED(I+3)+K*XMTPH+X2*SAVY(14))-(XK21/(S*CS))*(XN* 2003190
2      YPRED(I+4)+YPRED(I+5)*CS-YPRED(I+6)*SN)-X1*XK12*YAOPH* 2003200
3      SAVY(9)-(XC22*XD21/XD22)*((1.0/(S**2*CS** 2003210
3      2))*(XN*YPRED(I+4)*SN-XNSQ*YPRED(I+6))+YPRED(I+7)/S)) 2003220
4      +X3*SAVY(52) 2003230
A = YPRED(I+5)/S-YPRED(I+6)*TN/S+SAVY(9)*YAOPH+YDOT(I+5) 2003240
1      +SAVY(5)*YPRED(I+7) 2003250
B = SAVY(1)/S-SAVY(3)*TN/S+0.5*(SAVY(9)*SAVY(9)+SAVY(5)* 2003260
1      SAVY(5))+SAVY(2) 2003270
YDOT(I) = -2.0*YPRED(I)/S+XN*YANTH*X1CS/S-XN*YANTH*SN*X1CS**2/S**2 2003280
1      +YAMPT*TAN/S**2-K*(XFTHLD+XMPHLD*TAN/S)-X1*(SAVY(24)* 2003290
2      A*K*XFTHLD*B+SAVY(25)*YDOT(I+4)+SAVY(4)*K*XFPHLD+ 2003300
3      SAVY(26)*YAOPH+SAVY(9)*K*XFZELD+TAN/S*(YANTH*SAVY(9)+ 2003310
4      YAOPH*SAVY(7)-YPRED(I+7)*SAVY(8)-YANPT*SAVY(5))-X3* 2003320
5      SAVY(33) 2003330
YDOT(I+1) = -YPRED(I+1)/S+YANTH/S-XN*YPRED(I)/(S*CS)-XN*YAMPT*SN/ 2003340
1      (S*S*CS*CS)-K*XFPHLD-X1*(SAVY(25)*A+K*XFPHLD*B- 2003350
2      SAVY(26)*YPRED(I+7)-SAVY(5)*K*XFZELD) 2003360
3      -X3*SAVY(34) 2003370
YDOT(I+2) = -YPRED(I+2)/S-YANTH*TAN/S+XNSQ*YAMTH/(S**2*CS**2) 2003380
1      -2.0*XN*YAMPT/(S**2*CS)+K*(XN*XMPHLD*X1CS/S-XFZELD) 2003390
2      +X1*(SAVY(26)*A+K*XFZELD*B-SAVY(24)*YAOPH-SAVY(9)*K* 2003400
3      XFTHLD+SAVY(25)*YPRED(I+7)+SAVY(5)*K*XFPHLD) 2003410
4      -X3*SAVY(35) 2003420
YDOT(I+3) = YAMTH/S-YPRED(I+3)/S-2.0*XN*YAMPT/(S*CS)+YAJPH+XMTHLD 2003430
1      *K 2003440
2      +X3*SAVY(36) 2003450
YDOT(I+6)=YPRED(I+7) 2003460
YDOT(I+7) = -(XC22/(XC22**2+XK22*XD22))*(YPRED(I+1)+K*XNTPH+X2* 2003470
1      SAVY(11)-XK21*(XN*YPRED(I+4)+YPRED(I+5)*CS-YPRED(I+6)* 2003480
1      SN)/(S*CS)-X1*XK12*YAOPH*SAVY(9))+(XK22/(XC22**2+XK22* 2003490
2      XD22))*(YPRED(I+3)+K*XMTPH+X2*SAVY(14))-(XK22*XD21 2003500
3      /(XC22**2+XK22*XD22))*((1.0/(S*CS)**2)*(XN*YPRED(I+4)*SN 2003510
4      -XN**2*YPRED(I+6))+YPRED(I+7)/S) 2003520
5      +X3*SAVY(53) 2003530
GO TO 9005 2003540
C EQUATIONS FOR CYLINDER 2003550
4773 CONTINUE 2003560
YAOPH = X1RO*(XN*YPRED(I+6)-YPRED(I+4)) 2003570
YANTH = XK12*(1.0/(XK22+XC22**2/XD22))*(YPRED(I+1)+K*XNTPH+ 2003580
1      X2*SAVY(11)+ 2003590
1      (XC22/XD22)*(YPRED(I+3)+K*XMTPH+X2*SAVY(14)))-K*XNTTH- 2003600
1      X2*SAVY(10)+X1RO*(XK11-XK12*XK21*(1.0/(XK22+XC22**2/ 2003610
2      XD22)))*(XN*YPRED(I+4)-YPRED(I+6)+X1*RO*YAOPH* 2003620
2      SAVY(9))-(XC11+( 2003630
3      XK12*XC22*XD21/XD22)*(1.0/(XK22+XC22**2/XD22)))*(X1RO**2*( 2003640
4      XN*YPRED(I+4)-XNSQ*YPRED(I+6))) 2003650

```

```

5          +X3*SAVY(48) 2003660
YAMTH = -XD12*(XC22/(XC22**2+XK22*XD22))*(YPRED(I+1)+K*XNTPH+ 2003670
1          X2*SAVY(11))-K*XMTTH-X2*SAVY(13)+XD12*(XK22/(XC22**2+ 2003680
2          XK22*XD22))*(YPRED(I+3)+K*XMTPH+X2*SAVY(14))+(XC11* 2003690
2          X1RO+XD12*XK21*X1RO*(XC22/(XC22**2+XK22*XD22)))*(XN*YPRED 2003700
3          (I+4)-YPRED(I+6)+X1*RO*YAOPH*SAVY(9))+(XD11-XD12*XK22* 2003710
3          XD21/(XC22**2+XK22*XD22) 2003720
4          )*(X1ROSQ*(XN*YPRED(I+4)-XNSQ*YPRED(I+6))) 2003730
5          +X3*SAVY(49) 2003740
YAMPT=(-1.0/((RO/XD33)+(X1RO/XK33)))*(-2.0*XN*YPRED(I+7)+XN*X1RO* 2003750
1          YPRED(I+5)+YPRED(I)/XK33+X2*(SAVY(12)/XK33-SAVY(15)* 2003760
2          RO/XD33)+X1*(YAOPH*SAVY(5)+SAVY(9)*YPRED(I+7))) 2003770
3          +X3*SAVY(50) 2003780
YANPT = YPRED(I)+YAMPT*X1RO 2003790
YAJPH = YPRED(I+2)+X1*(SAVY(8)*YAOPH+YANPT*SAVY(9)-YPRED(I+1) 2003800
1          *SAVY(5)-YPRED(I+7)*SAVY(6)) 2003810
YDOT(I+4) = XN*YPRED(I+5)*X1RO+YPRED(I)/XK33+X2*SAVY(12)/XK33+ 2003820
1          YAMPT*X1RO/XK33+X1*(YAOPH*SAVY(5)+YPRED(I+7)*SAVY(9)) 2003830
2          +X3*SAVY(51) 2003840
YDOT(I+5) = -X1*YPRED(I+7)*SAVY(5)+(1.0/(XK22+XC22**2/XD22))* 2003850
1          (YPRED(I+1)+K*XNTPH+X2*SAVY(11)+(XC22/XD22)* 2003860
2          (YPRED(I+3)+K*XMTPH+X2*SAVY(14))-(XK21*X1RO)*(XN* 2003870
3          YPRED(I+4)-YPRED(I+6))-X1*XK12*YAOPH*SAVY(9)-(XC22* 2003880
4          XD21/XD22)*(X1ROSQ*(XN*(YPRED(I+4)-XN*YPRED(I+6)))) 2003890
5          +X3*SAVY(52) 2003900
A = -YPRED(I+6)/RO+SAVY(9)*YAOPH+YDOT(I+5)+SAVY(5)* 2003910
1          YPRED(I+7) 2003920
B = -SAVY(3)/RO+0.5*(SAVY(9)*SAVY(9)+SAVY(5)*SAVY(5))+ 2003930
1          SAVY(2) 2003940
YDOT(I) = XN*YANTH*X1RO-XN*YAMTH*X1ROSQ-K*(XFTHLD+XMPHLD*X1RO) 2003950
1          -X1*(SAVY(24)*A+K*XFTHLD*B+SAVY(25)*YDOT(I+4)+SAVY(4)* 2003960
2          K*XFPHLD+SAVY(26)*YAOPH+SAVY(9)*K*XFZELD+(YANTH* 2003970
3          SAVY(9)+YAOPH*SAVY(7)-YPRED(I+7)*SAVY(8)-YANPT* 2003980
4          SAVY(5))/RO)-X3*SAVY(33) 2003990
YDOT(I+1) = -XN*X1RO*YPRED(I)-XN*YAMPT*X1ROSQ-K*XFPHLD-X1* 2004000
1          (SAVY(25)*A+K*XFPHLD*B-SAVY(26)*YPRED(I+7)-SAVY(5)* 2004010
2          K*XFZELD) 2004020
3          -X3*SAVY(34) 2004030
YDOT(I+2) = -YANTH*X1RO+XNSQ*YAMTH*X1ROSQ+K*(XN*XMPHLD*X1RO- 2004040
1          XFZELD)-X1*(SAVY(26)*A+K*XFZELD*B-SAVY(24)*YAOPH- 2004050
2          SAVY(9)*K*XFTHLD+SAVY(25)*YPRED(I+7)+SAVY(5)*K*XFPHLD) 2004060
3          -X3*SAVY(35) 2004070
YDOT(I+3) = -2.0*XN*YAMPT*X1RO+YAJPH+K*XMTHLD 2004080
1          +X3*SAVY(36) 2004090
YDOT(I+6)=YPRED(I+7) 2004100
YDOT(I+7) = -(XC22/(XC22**2+XK22*XD22))*(YPRED(I+1)+K*XNTPH+X2* 2004110
1          SAVY(11)-XK21*X1RO*(XN*YPRED(I+4)-YPRED(I+6))-X1*XK12* 2004120
1          YAOPH*SAVY(9))+(XC22/(XC22**2+XK22*XD22))*(YPRED(I+3)+ 2004130
2          K*XMTPH+X2*SAVY(14))-(XK22*XD21/(XC22**2+XK22*XD22))*( 2004140
3          X1ROSQ*(XN*YPRED(I+4)-XNSQ*YPRED(I+6))) 2004150
4          +X3*SAVY(53) 2004160
9005 CONTINUE 2004170
      RETURN 2004180
      END 2004190

```

```

FOR, IS ODE2, ODE2
SUBROUTINE ODE2,
INTEGER SAVJTC, SAVSTP, Q, THICK
INTEGER XN1, XN
REAL K
DOUBLE PRECISION YPRED
COMMON STORY(16), XMAT(270, 10), STD(10), SADUS(30), RADUS(30)
COMMON TADUS(30), UADUS(30), SAVTIC(900)
COMMON XN, TEFREE, TIC, PHI, STOP, RESTOP, RTICK, G1, XNL(3), NH
COMMON NST(30), NKL(30), NXMAT(20), SAVJTC(30), SAVSTP(30), JRTIC(30)
COMMON JRSTOP(30), NREG, NMPT, NRC, NSC, NIX, IERROR, KGEOM, IGEOM, ISTAB
COMMON KELVIN, IBEGIN, NPROB, NSEG, NERROR, Q, THICK, NOJS, NLINKS, NLCASE
COMMON NTSKL, NZ, NBCT, LINPUT, NTRKL, NPASS, XN1, KBC, NRINGS
COMMON LODE, ICYCLE, LDISTL
COMMON /LASTEQ/ YPRED(8), YDOT(8), YASAVE(8),
1 YANTH, YAMTH, YAMPT, YANPT, YAOPH, YAQPH, YAQTH, YAJPH,
2 S, SN, CS, SNSQ, CSSQ, TAN, SEC, CN, X1CS, X1SN, TN,
3 X1RO, X1ROSQ, X1SNRO, X1CSRO, CN1RO, SN1RO, CS1RO,
4 X1R1, X1R2, CS1R1, CS1R2, SN1R1, X1R1SQ, R2SQ, RO, BESQ,
5 ROSQ, XNSQ, BETA, R1, R2, S1, R1DOT, R1SQ,
6 XNTTH, XNTPH, XMTTH, XMPH, XFTHLD, XFPHLD, XFZELD,
7 XMTHLD, XMPHLD, ETHET, EPHI, XGPT, ALPHTH, ALPHPH,
8 XNUTP, XNUPT, XC11, XC22, XC15, XD33, XD22, XD21, XD12,
9 XK11, XK12, XK21, XK22, XK33, XD11,
A M, I, SITIN, SITOUT, SIPIN, SIPOUT, TPTIN, TPTOUT,
B ZBRIN, ZBROUT, SCRIPA, SCRIP1, SIFIN, SIFOUT, TZEPH, TZETH
B , XNPHI, BETTA, ZETTA, XC16
C , RMOSS, RMOSEN, YLDST, ROC, HP, FPLUH, GPLUH, TWON
D , RMOSY, RMOSNY, RMOSXY, RMONXY
D , RMOSNS, RMOSSS, SIGOXS, RMOSNR, RMOSSR, SIGOXR
COMMON /PLS/ OMEGA, IWORD, XMERD, XPRES, XMONT
COMMON /WOOD/ SAVY(53), NPLEV, NLPD, NPLA(21), STR(6), SIGMA(3, 21),
C SEPS(3, 21), SALPH(3, 21), SBAPH(3, 21), STEPS(3, 21),
O EFF(21), STSRN(3), NPLAST(3), STSIG(3), STREPS(3),
M STALPH(3), STBAPH(3), EFFST(3), NPLEVS(3)
COMMON /CDISP/ P, PMAX, DELP, DELP1, YEPS, ZEPS
EQUIVALENCE (XNL(1), X1), (XNL(2), X2), (XNL(3), X3), (K, DELP)
GO TO (7341, 7342, 7343), IGEOM
C THE FOLLOWING EQUATIONS ARE THE 'RWF' SET
C EQUATIONS FOR SHELLS OF REVOLUTION ( PHI COORDINATE )
7341 CONTINUE
YAOPH = XN*YPRED(I+6)*X1RO-YPRED(I+4)*SN1RO
YANTH = (YPRED(I+1)+K*XNTPH+X2*SAVY(11))*(XC15*XC22+XD22*XK12)
1 / (XK22*XD22+XC22**2)-K*XNTTH-X2*SAVY(10)+(XK12*XC22-
1 XK22*XC15)*(YPRED(I+3)+K*XMTPH+X2*SAVY(14)) / (XC22*
2 XC22+XK22*XD22)+(X1RO*(XN*YPRED(I+4)+YPRED(I+5)*CS-
2 YPRED(I+6)*SN)+X1*YAOPH*SAVY(9))*(XK11+(XC15*(XC15*
3 XK22-2.0*XK12*XC22)-XK12*XK12*
4 XD22)/(XK22*XD22+XC22*XC22))+ (X1ROSQ*(XN*YPRED(I+4)*SN-XNSQ
5 *YPRED(I+6))+X1RO*YPRED(I+7)*CS)*(-XC11+(XC15*XC15*XC22+
6 XC15*(XK12*XD22+XK22*XD12)-XK12*XD12*XC22)/(XK22*XD22+XC22*XC22))
7 +X3*SAVY(48)
YANTH= (YPRED(I+3)+K*XMTPH+X2*SAVY(14))*(XC15*XC22+XK22*XD12)
1 / (XK22*XD22+XC22*XC22)+(YPRED(I+1)+K*XNTPH+X2*SAVY(11)
2 )*(XD22*XC15-XD12*XC22)/(XD22*XK22+XC22**2)-K*XMTTH-
3 X2*SAVY(13)+(X1ROSQ*(XN*YPRED(I+4)*SN-XNSQ*YPRED(I+6))
4 +X1RO*YPRED(I+7)*CS)*(XD11-(XD12*XD12*XK22+XC15*(2.0*
5 XK22*XD12-XC15*XD22)) / (XC22*XC22+XK22*XD22))+ (X1RO*
6 (XN*YPRED(I+4)+YPRED(I+5)*CS-YPRED(I+6)*SN)+X1*YAOPH*
7 SAVY(9))*(XC11+(XD12*XC22*XK12-XC15*(XC15*XC22+XD12*
8 XK22+XD22*XK12)) / (XC22*XC22+XK22*XD22))
9 +X3*SAVY(49)

```

```

YAMPT = (1.0/(XC16*SN*X1RO-XK33-SN*X1RO*(XD33*SN/(RO)-XC16))) 2100620
1 *((XK33*XD33-XC16**2)*X1RO*(-2.0*XN*YPRED(I+7)+YPRED(I+4)* 2100630
2 (CS*X1R1-CN1RO)+XN*YPRED(I+5)*(X1R1+SN1RO)+2.0*XN*YPRED 2100640
3 (I+6)*CS*X1RO)+X1*SN*(YAOPH*SAVY(5)+YPRED(I+7)*SAVY(9) 2100650
4 )+(YPRED(I)+X2*SAVY(12))*((XD33*SN*X1RO-XC16)+X2* 2100660
5 SAVY(15)*(XK33-XC16*SN/RO)) 2100670
6 +X3*SAVY(50) 2100680
YANPT = YPRED(I)+YAMPT*SN1RO 2100690
YAJPH = YPRED(I+2)+X1*(SAVY(8)*YAOPH+YANPT*SAVY(9)-YPRED(I+1) 2100700
1 *SAVY(5)-YPRED(I+7)*SAVY(6)) 2100710
YDOT(I+4) = R1*(YPRED(I+4)*CS*X1RO+X1*(YAOPH*SAVY(5)+YPRED(I+7)* 2100720
1 SAVY(9)) 2100730
1 +XN*YPRED(I+5)*X1RO+(1.0/(XK33- 2100740
2 XC16**2/XD33))*(YPRED(I)+YAMPT*(SN*X1RO-XC16/XD33)+X2* 2100750
3 (SAVY(12)-XC16*SAVY(15)/XD33)) 2100760
4 +X3*SAVY(51) 2100770
YDOT(I+5) = YPRED(I+6)-R1*X1*YPRED(I+7)*SAVY(5)+R1*(XD22*(YPRED(I+ 2100780
1 1)+K*XNTPH+X2*SAVY(11))+XC22*(YPRED(I+3)+K*XMTPH+X2* 2100790
2 SAVY(14))-(X1RO*(XN*YPRED(I+4)+YPRED(I+5)*CS-YPRED(I+6 2100800
2 )*SN)+X1*YAOPH*SAVY(9))* 2100810
3 (XK12*XD22+XC15*XC22)-(X1ROSQ*(XN*YPRED(I+4)-XNSQ* 2100820
4 YPRED(I+6))+X1RO*YPRED(I+7)*CS)*(XC22*XD12-XC15*XD22)) 2100830
5 /(XK22*XD22+XC22**2) 2100840
6 +X3*SAVY(52) 2100850
A = YPRED(I+5)*CS1RO-YPRED(I+6)*SN1RO+SAVY(9)*YAOPH+ 2100860
1 YDOT(I+5)/R1-YPRED(I+6)/R1+SAVY(5)*YPRED(I+7) 2100870
B = SAVY(1)*CS1RO-SAVY(3)*SN1RO+.5*(SAVY(9)*SAVY(9) 2100880
1 +SAVY(5)*SAVY(5))+(SAVY(2)-SAVY(3))/R1 2100890
YDOT(I) = R1*(-2.0*YPRED(I)*CS1RO+XN*YANTH*X1RO-XN*YAMTH*SN* 2100900
1 X1ROSQ-YAMPT*CS1RO*(X1R1-SN1RO))-R1*K*(XFTHLD+XMPHLD* 2100910
2 SN1RO)-R1*X1*(SAVY(24)*A+K*XFTHLD*B+SAVY(25)*YDOT(I+4) 2100920
3 /R1+SAVY(4)*K*XFPHLD/R1+SAVY(26)*YAOPH+SAVY(9)*K* 2100930
4 XFZELD+SN/RO*(YANTH*SAVY(9)+YAOPH*SAVY(7)-YPRED(I+7)* 2100940
5 SAVY(8)-YANPT*SAVY(5)))-X3*SAVY(33) 2100950
YDOT(I+1) = R1*(CS1RO*(YANTH-YPRED(I+1))-XN*X1RO*(YPRED(I)+ 2100960
1 YAMPT*(SN*X1RO+X1R1))+YPRED(I+2)*X1R1)-R1*K*XFPHLD 2100970
2 -R1*X1*(SAVY(25)*A+K*XFPHLD*B 2100980
3 -SAVY(26)*YPRED(I+7)-SAVY(5)*K*XFZELD) 2100990
4 -X3*SAVY(34) 2101000
YDOT(I+2) = R1*(-YPRED(I+2)*CS1RO-YANTH*SN1RO-YPRED(I+1)*X1R1 2101010
1 +XNSQ*YAMTH*X1ROSQ-2.0*XN*YAMPT*CS*X1ROSQ)+R1*K* 2101020
2 (XN*XMPHLD*X1RO-XFZELD)-R1*X1*(SAVY(26)*A+K*XFZELD* 2101030
3 B-SAVY(24)*YAOPH-SAVY(9)*K* 2101040
4 XFTHLD+SAVY(25)*YPRED(I+7)+SAVY(5)*K*XFPHLD) 2101050
5 -X3*SAVY(35) 2101060
YDOT(I+3) = R1*(YAMTH*CS1RO-YPRED(I+3)*CS1RO-2.0*XN*YAMPT*X1RO+ 2101070
1 YAJPH+K*XMTHLD) 2101080
2 +X3*SAVY(36) 2101090
YDOT(I+6) = R1*(YPRED(I+7)-YPRED(I+5)*X1R1) 2101100
YDOT(I+7) = R1*(XK22*(YPRED(I+3)+K*XMTPH+X2*SAVY(14))-XC22*(YPRED( 2101110
1 I+1)+K*XNTPH+X2*SAVY(11))+X1RO*(XN*YPRED(I+4)+ 2101120
1 YPRED(I+5)*CS-YPRED(I+6)*SN)+X1*YAOPH*SAVY(9))*((XK12* 2101130
2 XC22-XK22*XC15) 2101140
2-(X1ROSQ*(XN*YPRED(I+4)*SN-XNSQ*YPRED(I+6))+X1RO*YPRED(I+7)*CS)* 2101150
3(XC15*XC22+XK22*XD12))/(XC22**2+XK22*XD22) 2101160
3 +X3*SAVY(53) 2101170
GO TO 9005 2101180
C EQUATIONS FOR CONE 2101190
7342 CONTINUE 2101200
YAOPH = XN*YPRED(I+6)*X1CS/S-YPRED(I+4)*TAN/S 2101210
YANTH = (YPRED(I+1)+K*XNTPH+X2*SAVY(11))*((XC15*XC22+XD22*XK12) 2101220

```

```

1 / (XK22*XD22+XC22**2) - K*XNTTH - X2*SAVY(10) + (XK12*XC22 - 2101230
1 XK22*XC15) * (YPRED(I+3) + K*XMTPH + X2*SAVY(14)) / (XC22* 2101240
2 XC22 + XK22*XD22) + ((XN*YPRED(I+4) + YPRED(I+5)*CS - 2101250
3 YPRED(I+6)*SN) / (S*CS) + X1*YAOPH*SAVY(9)) * (XK11 + (XC15* 2101260
3 (XC15*XK22 - 2.0*XK12*XC22) - XK12*XK12* 2101270
4 XD22) / (XK22*XD22 + XC22*XC22)) + ((XN*YPRED(I+4)*SN - XNSQ* 2101280
5 YPRED(I+6)) / (S*S*CSSQ) + YPRED(I+7) / S) * (-XC11 + (XC15*XC15*XC22 + 2101290
6 XC15*(XK12*XD22 + XK22*XD12) - XK12*XD12*XC22) / (XK22*XD22 + XC22*XC22)) 2101300
7 + X3*SAVY(48) 2101310
YAMTH = (YPRED(I+3) + K*XMTPH + X2*SAVY(14)) * (XC15*XC22 + XK22*XD12) 2101320
1 / (XK22*XD22 + XC22**2) + (YPRED(I+1) + K*XNTPH + X2*SAVY(11)) * 2101330
1 (XD22*XC15 - XD12*XC22) / (XD22*XK22 + XC22**2) - K*XMTTH - X2* 2101340
2 SAVY(13) + (1.0 / (S*S*CSSQ)) * (-XNSQ*YPRED(I+6) + XN* 2101350
2 YPRED(I+4)* 2101360
3 SN) + YPRED(I+7) / S * (XD11 - (XD12*XD12*XK22 + XC15*(2.0*XC22*XD12 - XC15* 2101370
4 XD22)) / (XC22*XC22 + XK22*XD22)) + (1.0 / (S*CS)) * (XN* 2101380
5 YPRED(I+4) + YPRED(I+5)*CS - YPRED(I+6)*SN) + X1*YAOPH* 2101390
6 SAVY(9)) * (XC11 + (XD12*XC22*XK12 - XC15*(XC15*XC22 + XD12* 2101400
7 XK22 + XD22*XK12)) / (XC22*XC22 + XK22*XD22)) 2101410
8 + X3*SAVY(49) 2101420
YAMPT = ((XC16*TAN/S - XK33 - (TAN/S) * (XD33*TAN/S - XC16)) ** (-1)) * ((XK33* 2101430
1 XD33 - XC16**2) * (1.0 / (S*CS)) * (-2.0*XN*YPRED(I+7) - YPRED(I+4)* 2101440
2 SN/S + XN*YPRED(I+5)*TAN/S + 2.0*XN*YPRED(I+6) / S) + X1*SN* 2101450
3 (YAOPH*SAVY(5) + YPRED(I+7)*SAVY(9)) + (YPRED(I) + X2* 2101460
4 SAVY(12)) * (XD33*TAN/S - XC16) + X2*SAVY(15) * (XK33 - XC16* 2101470
5 TN/S)) 2101480
6 + X3*SAVY(50) 2101490
YANPT = YPRED(I) + YAMPT*TAN/S 2101500
YAJPH = YPRED(I+2) + X1*(SAVY(8)*YAOPH + YANPT*SAVY(9) - YPRED(I+1)* 2101510
1 SAVY(5) - YPRED(I+7)*SAVY(6)) 2101520
YDOT(I+4) = YPRED(I+4) / S + X1*(YAOPH*SAVY(5) + YPRED(I+7)*SAVY(9)) + XN* 2101530
1 YPRED(I+5) / (S*CS) + (1.0 / (XK33 - XC16**2) / 2101540
2 XD33)) * (YPRED(I) + YAMPT*(TAN/S - XC16/XD33) + X2*(SAVY(12) - 2101550
3 XC16*SAVY(15) / XD33)) 2101560
4 + X3*SAVY(51) 2101570
YDOT(I+5) = -X1*YPRED(I+7)*SAVY(5) + (XD22*(YPRED(I+1) + K*XNTPH + X2* 2101580
1 SAVY(11)) + XC22*(YPRED(I+3) + K*XMTPH + X2*SAVY(14)) - (XK12* 2101590
1 XD22 + XC15*XC22) * ((1.0 / (S*CS)) * (XN*YPRED(I+4) + YPRED(I+5) 2101600
2 *CS - YPRED(I+6)*SN)) + X1*YAOPH*SAVY(9)) - (XC22*XD12 - XC15* 2101610
2 XD22) * ((-XNSQ* 2101620
3 YPRED(I+6) + XN*YPRED(I+4)*SN) / (S*S*CSSQ) + YPRED(I+7) / S)) 2101630
4 / (XK22*XD22 + XC22*XC22) 2101640
5 + X3*SAVY(52) 2101650
A = YPRED(I+5) / S - YPRED(I+6)*TN/S + SAVY(9)*YAOPH + YDOT(I+5) 2101660
1 + SAVY(5)*YPRED(I+7) 2101670
B = SAVY(1) / S - SAVY(3)*TN/S + 0.5*(SAVY(9)*SAVY(9) + SAVY(5)* 2101680
1 SAVY(5)) + SAVY(2) 2101690
YDOT(I) = -2.0*YPRED(I) / S + XN*YANTH*X1CS/S - XN*YAMTH*SN*X1CS**2/S**2 2101700
1 + YAMPT*TAN/S**2 - K*(XFTHLD*XMPHLD*TAN/S) - X1*(SAVY(24))* 2101710
2 A + K*XFTHLD*B + SAVY(25)*YDOT(I+4) + SAVY(4)*K*XFPHLD + 2101720
3 SAVY(26)*YAOPH + SAVY(9)*K*XFZELD + TAN/S*(YANTH*SAVY(9) + 2101730
4 YAOPH*SAVY(7) - YPRED(I+7)*SAVY(8) - YANPT*SAVY(5)) - X3* 2101740
5 SAVY(33) 2101750
YDOT(I+1) = -YPRED(I+1) / S + YANTH/S - XN*YPRED(I) / (S*CS) - XN*YAMPT*SN/ 2101760
1 (S*S*CS*CS) - K*XFPHLD - X1*(SAVY(25)*A + K*XFPHLD*B - 2101770
2 SAVY(26)*YPRED(I+7) - SAVY(5)*K*XFZELD) 2101780
3 - X3*SAVY(34) 2101790
YDOT(I+2) = -YPRED(I+2) / S - YANTH*TAN/S + XNSQ*YAMTH / (S**2*CS**2) 2101800
1 - 2.0*XN*YAMPT / (S**2*CS) + K*(XN*XMPHLD*X1CS/S - XFZELD) 2101810
2 + X1*(SAVY(26)*A + K*XFZELD*B - SAVY(24)*YAOPH - SAVY(9)*K* 2101820
3 XFTHLD + SAVY(25)*YPRED(I+7) + SAVY(5)*K*XFPHLD) 2101830
4 - X3*SAVY(35) 2101840

```

```

YDOT(I+3)= YAMTH/S-YPRED(I+3)/S-2.0*XN*YAMPT/(S*CS)+YAJPH+XMTHLD 2101850
1      *K 2101860
2      +X3*SAVY(36) 2101870
YDOT(I+6)=YPRED(I+7) 2101880
YDOT(I+7) = (XK22*(YPRED(I+3)+K*XMTPH+X2*SAVY(14))-XC22* 2101890
1      (YPRED(I+1)+K*XNTPH+X2*SAVY(11)))+(XK12*XC22-XK22*XC15) 2101900
2      *((1.0/(S*CS))*(XN*YPRED(I+4)+YPRED(I+5)*CS-YPRED(I+6)* 2101910
2      SN))+X1*YAOPH*SAVY(9))-(XC15*XC22+XK22*XD12)* 2101920
3      ((-XNSQ*YPRED(I+6)+XN*YPRED(I+4)*SN)/(S*S*CSSQ)+ 2101930
4      YPRED(I+7)/S))/(XK22*XD22+XC22*XC22) 2101940
5      +X3*SAVY(53) 2101950
GO TO 9005 2101960
C EQUATIONS FOR CYLINDER 2101970
7343 CONTINUE 2101980
YAOPH = X1RO*(XN*YPRED(I+6)-YPRED(I+4)) 2101990
YANTH = (YPRED(I+1)+K*XNTPH+X2*SAVY(11))*(XC15*XC22+XD22*XK12) 2102000
1      /(XK22*XD22+XC22**2)-K*XNTTH-X2*SAVY(10)+(XK12*XC22- 2102010
2      XK22*XC15)*(YPRED(I+3)+K*XMTPH+X2*SAVY(14))/(XC22* 2102020
2      XC22+XK22*XD22)+(X1RO*(XN*YPRED(I+4)-YPRED(I+6))+X1* 2102030
3      YAOPH*SAVY(9))*(XK11+(XC15*(XC15*XK22-2.0*XK12*XC22)- 2102040
3      XK12*XK12* 2102050
4      XD22)/(XK22*XD22+XC22*XC22)))+(X1ROSQ*(XN*YPRED(I+4)-XNSQ 2102060
5      *YPRED(I+6)))*(-XC11+(XC15*XC15*XC22+ 2102070
6      XC15*(XK12*XD22+XK22*XD12)-XK12*XD12*XC22)/(XK22*XD22+XC22*XC22)) 2102080
7      +X3*SAVY(48) 2102090
YAMTH = (YPRED(I+3)+K*XMTPH+X2*SAVY(14))*(XC15*XC22+XK22*XD12) 2102100
1      /(XK22*XD22+XC22**2)+(YPRED(I+1)+K*XNTPH+X2*SAVY(11))* 2102110
2      (XD22*XC15-XD12*XC22)/(XD22*XK22+XC22**2)-K*XMTTH-X2* 2102120
2      SAVY(13)+X1ROSQ*(XN*YPRED(I+4)-XNSQ*YPRED(I+6)) 2102130
3      *(XD11-(XD12*XD12*XK22+XC15*(2.0*XC22*XD12-XC15* 2102140
4      XD22))/(XC22*XC22+XK22*XD22)))+(X1RO*(XN*YPRED(I+4)- 2102150
5      YPRED(I+6))+X1*YAOPH*SAVY(9))*(XC11+(XD12*XC22*XK12- 2102160
6      XC15*(XC15*XC22+XD12*XK22+ 2102170
7      XD22*XK12))/(XC22*XC22+XK22*XD22)) 2102180
      +X3*SAVY(49) 2102190
YAMPT=(1/(XC16*X1RO-XK33-X1RO*(XD33*X1RO-XC16)))*((XK33*XD33-XC16 2102200
1      **2)*X1RO*(-2.0*XN*YPRED(I+7)+XN*X1RO*YPRED(I+5))+X1* 2102210
2      (YAOPH*SAVY(5)+YPRED(I+7)*SAVY(9)))+(YPRED(I)+X2* 2102220
3      SAVY(12))*(XD33*X1RO-XC16)+X2*SAVY(15))*(XK33-XC16/RO)) 2102230
4      +X3*SAVY(50) 2102240
YANPT = YPRED(I)+YAMPT*X1RO 2102250
YAJPH = YPRED(I+2)+X1*(SAVY(8)*YAOPH+YANPT*SAVY(9)-YPRED(I+1) 2102260
1      *SAVY(5)-YPRED(I+7)*SAVY(6)) 2102270
YDOT(I+4) = X1*(YAOPH*SAVY(5)+YPRED(I+7)*SAVY(9))+XN*YPRED(I+5)/RO 2102280
1      + 2102290
1      (1.0/(XK33-XC16**2/XD33))*(YPRED(I)+ 2102300
2      YAMPT*(X1RO-XC16/XD33)+X2*(SAVY(12)-XC16*SAVY(15)/ 2102310
3      XD33)) 2102320
4      +X3*SAVY(51) 2102330
YDOT(I+5) = -X1*YPRED(I+7)*SAVY(5)+(XD22*(YPRED(I+1)+K*XNTPH+X2* 2102340
1      SAVY(11))+XC22*(YPRED(I+3)+K*XMTPH+X2*SAVY(14))-(X1RO* 2102350
1      (XN*YPRED(I+4)-YPRED(I+6))+X1*YAOPH*SAVY(9)))*(XK12* 2102360
2      XD22+XC15*XC22)-X1ROSQ*(XN*YPRED 2102370
2      (I+4)-XNSQ*YPRED(I+6))*(XC22*XD12-XC15*XD22))/(XK22*XD22+XC22**2) 2102380
3      +X3*SAVY(52) 2102390
A = -YPRED(I+6)/RO+SAVY(9)*YAOPH+YDOT(I+5)+SAVY(5)* 2102400
1      YPRED(I+7) 2102410
B = -SAVY(3)/RO+0.5*(SAVY(9)*SAVY(9)+SAVY(5)*SAVY(5))+ 2102420
1      SAVY(2) 2102430
YDOT(I) = XN*YANTH*X1RO-XN*YAMTH*X1ROSQ-K*(XFTHLD+XMPHLD*X1RO) 2102440
1      -X1*(SAVY(24)*A+K*XFTHLD*B+SAVY(25)*YDOT(I+4)+SAVY(4))* 2102450

```

2	K*XFPHLD+SAVY(26)*YAOPH+SAVY(9)*K*XFZELD+(YANTH*	2102460
3	SAVY(9)+YAOPH*SAVY(7)-YPRED(I+7)*SAVY(8)-YANPT*	2102470
4	SAVY(5))/RO)-X3*SAVY(33)	2102480
	YDOT(I+1) = -XN*X1RO*YPRED(I)-XN*YAMPT*X1ROSQ-K*XFPHLD-X1*	2102490
1	(SAVY(25)*A+K*XFPHLD*B-SAVY(26)*YPRED(I+7)-SAVY(5)*	2102500
2	K*XFZELD)	2102510
3	-X3*SAVY(34)	2102520
	YDOT(I+2) = -YANTH*X1RO+XNSQ*YAMTH*X1ROSQ+K*(XN*XMPHLD*X1RO-	2102530
1	XFZELD)-X1*(SAVY(26)*A+K*XFZELD*B-SAVY(24)*YAOPH-	2102540
2	SAVY(9)*K*XFTHLD+SAVY(25)*YPRED(I+7)+SAVY(5)*K*XFPHLD)	2102550
3	-X3*SAVY(35)	2102560
	YDOT(I+3) = -2.0*XN*YAMPT*X1RO+YAJPH+K*XMTHLD	2102570
1	+X3*SAVY(36)	2102580
	YDOT(I+6)=YPRED(I+7)	2102590
	YDOT(I+7) = {XK22*(YPRED(I+3)+K*XMTPH+X2*SAVY(14))-XC22*	2102600
1	(YPRED(I+1)+K*XNTPH+X2*SAVY(11))+(X1RO*(XN*YPRED(I+4)-	2102610
1	YPRED(I+6))+X1*YAOPH*SAVY(9))*(XK12*XC22-XK22*XC15)-	2102620
2	X1ROSQ*(XN*YPRED	2102630
2	(I+4)-XNSQ*YPRED(I+6))*(XC15*XC22+XK22*XD12))/(XC22**2+XK22*XD22)	2102640
3	+X3*SAVY(53)	2102650
	9005 CONTINUE	2102660
	RETURN	2102670
	END	2102680
	C ..... ROUTINE ** TOBAR ** ABACUS UPDATED 01/11/74 .....	2200000



## SUBROUTINE SHPLAS

Subroutine SHPLAS is called from LEBEGE and incremental stress resultants, deformations and geometric data are passed to the subroutine in the label common area LASTEQ. The routine SHPLAS updates all values to the current load increment and calls a series of routines to obtain the plasticity history of the shell.

### Subroutines Called from SHPLAS

Subroutine SHSRSE: Is a routine to calculate elastic stresses throughout the shell wall cross-section.

Subroutine SEPSIS: Is a routine to calculate the plastic strain increments and the shift in the yield surface. The total stresses and plastic strains are also obtained. For this routine the material must be isotropic and the hardening laws either kinematic or isotropic.

Subroutine LINEQU: Is a small simultaneous equation solver.

Subroutine ORTHKN: Performs the same function as SEPSIS, above, for orthotropic (kinematic hardening) plasticity.

Subroutine EPSIS: Performs the same function as SEPSIS, above, for perfectly plastic behavior.

Subroutine SMEAR: Is a routine to calculate the plasticity effects of smeared reinforcement.

Subroutine SAVXES: Is a routine which obtains an equilibrium and strain correction for each point in the shell, for a series of load steps.

Subroutine ARRAYS: If the clues are set for graphical display of results, the necessary information is passed to this subroutine, which in turn arranges the information to be plotted into proper arrays.

FORTRAN CODE

ENGINEERING SYMBOLS (REF. 1)

EPSITH

$\epsilon_{\theta}$

EPSIPH

$\epsilon_{\phi}$

GAPHTH

$\gamma_{\phi\theta}$

XKTH

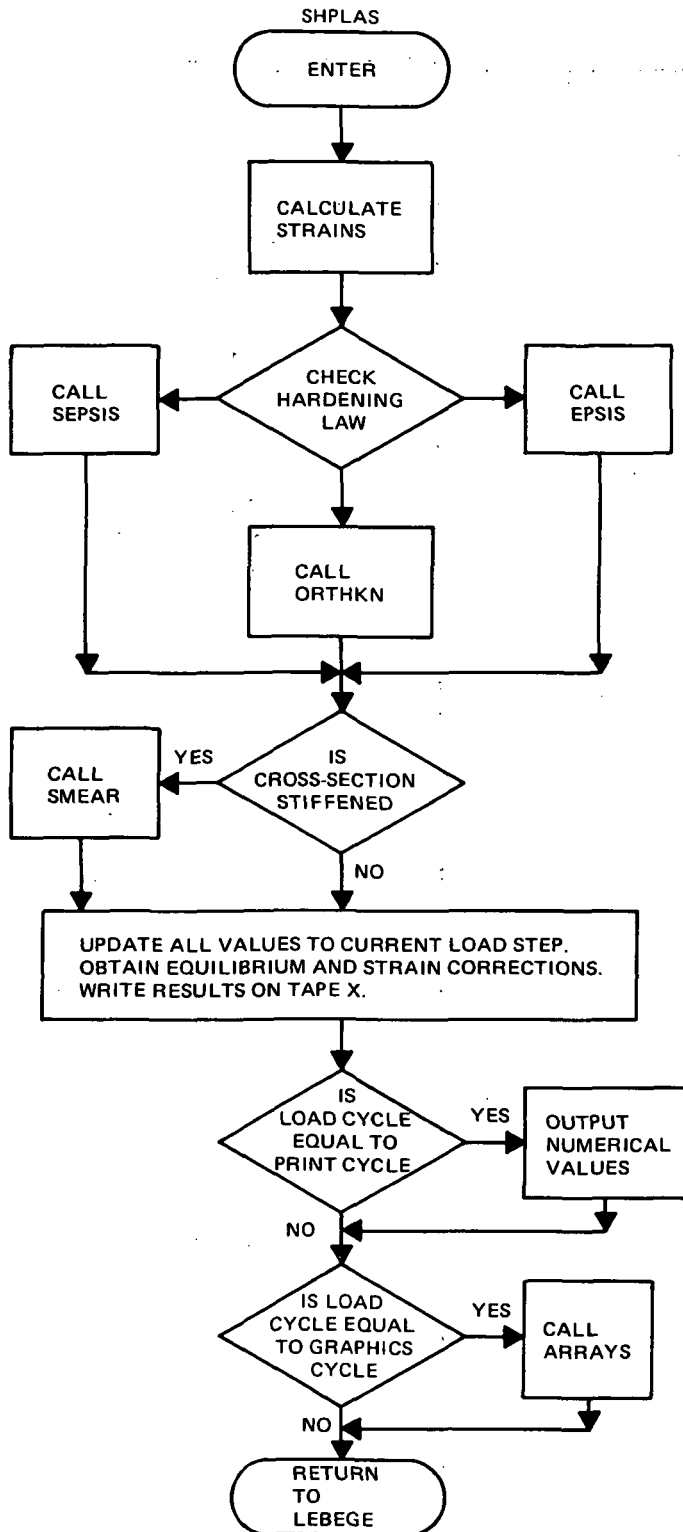
$k_{\theta}$

XKPH

$k_{\phi}$

XKPT

$k_{\phi\theta}$



```

FOR, IS SHPLAS, SHPLAS
SUBROUTINE SHPLAS (NCYC, NAPEX, NPR, STEP)
INTEGER SAVJTC, SAVSTP, Q, THICK
INTEGER XN
DOUBLE PRECISION YPRED
DOUBLE PRECISION YCORR
3300010
3300020
3300030
3300040
3300050
3300060
3300070
3300080
3300090
3300100
3300110
3300120
3300130
3300140
3300150
COMMON /LASTEQ/ YPRED(8), YDOT(8), YASAVE(8),
1 YANTH, YAMTH, YAMPT, YANPT, YAOPH, YAQPH, YAQTH, YAJPH,
2 S, SN, CS, SNSQ, CSSQ, TAN, SEC, CN, X1CS, X1SN, TN,
3 X1RO, X1ROSQ, X1SNRO, X1CSRO, CN1RO, SN1RO, CS1RO,
4 X1R1, X1R2, CS1R1, CS1R2, SN1R1, X1R1SQ, R2SQ, RO, BESQ,
5 ROSQ, XNSQ, BETA, R1, R2, S1, RIDOT, R1SQ,
6 XNTTH, XNTPH, XMTTH, XMPH, XFTHLD, XFPHL D, XFZELD,
7 XMTHLD, XMPHLD, ETHET, EPHI, XGPT, ALPHTH, ALPHPH,
8 XNUTP, XNUPPT, XC11, XC22, XC15, XD33, XD22, XD21, XD12,
9 XK11, XK12, XK21, XK22, XK33, XD11,
A M, I, SITIN, SITOUT, SIPIN, SIPOUT, TPTIN, TPTOUT,
B ZBRIN, ZBROUT, SCRIPA, SCRIP1, SIFIN, SIFOUT, TZEPH, TZETH
B , XNPHI, BETTA, ZETTA, XC16
3300270
C , RMOSS, RMOSN, YLDST, ROC, HP, FPLUH, GPLUH, TWON
3300280
D , RMOSSY, RMOSNY, RMOSSXY, RMONXY
3300290
D , RMOSSNS, RMOSSS, SIGOXS, RMOSNR, RMOSSR, SIGOXR
3300300
COMMON /WOOD/ SAVY(53), NPLEV, NLPO, NPLA(21), STR(6), SIGMA(3,21),
3300310
C SEPS(3,21), SALPH(3,21), SBAPH(3,21), STEPS(3,21),
3300320
O EFF(21), STSRN(3), NPLAST(3), STSIG(3), STREPS(3),
3300330
M STALPH(3), STBAPH(3), EFFST(3), NPLEVS(3)
3300340
COMMON /CDISP/ P, PMAX, DELP, DELP1, YEPS, ZEPS
3300350
COMMON /CMAIN/ ZETA1(21), ZETA2(21), NODE, ALF(4), CE(4), NLRS, HI, HO, T
3300360
COMMON /PLSTIC/ IO, JO, IOR, JOR, KOR, NEO
3300370
COMMON /MAGIQ/ KKNT, TII, TIK, TOK, TOD
3300380
COMMON /RWO/ ER, ES, CPH, CTH, APH, ATH, SPH, STH, ALPHS, ALPHR, TS, TR, SNB,
3300390
C CSB
3300400
COMMON /GRAFIX/ X(100), Y(100,9), NGRAPH, LDEF(9), NGR, JCYC, NFLAG, JAM,
3300410
C JNSC
3300420
DIMENSION SAVX(53), EPSTNT(3,2)
3300430
DIMENSION DSTR(6), EPSINT(3,2), TEMP(7), DSIG(3), DEPS(3), TEPS(3)
3300440
DIMENSION YCORR(16)
3300450
DIMENSION SIGMI(3), SIGMO(3), EPSI(3), EPSO(3)
3300460
DIMENSION DTOT(3), EE(2), DEN(3), DEM(3)
3300470
EQUIVALENCE (DSTR(1), EPSIPH), (DSTR(2), EPSITH), (DSTR(3), GAPHTH)
3300480
EQUIVALENCE (DSTR(4), XKPH), (DSTR(5), XKTH), (DSTR(6), XKPT)
3300490
EQUIVALENCE (YPRED(1), YCORR(1))
3300500
EQUIVALENCE (NERR, NIX)
3300510
EQUIVALENCE (XNL(1), X1), (XNL(2), X2), (XNL(3), X3)
3300520
EQUIVALENCE (RMOSSX, RMOSS), (RMOSNX, RMOSN)
3300530
13 FORMAT(1H0, 40X, 35HSTRAINS AND STRESSES SHELL ELEMENTS)
3300540
30 FORMAT(1H0, 45X, 4HNODE, I5, 10H OF MEMBER, I5, 12H NOT ON DISK)
3300550
50 FORMAT(1H0, 50X, 35HERROR IN LINEQU IN EPSIS CYCLE = ,F6.0)
3300560
55 FORMAT(1H0, 50X, 35HERROR IN LINEQU IN SEPSIS CYCLE = ,F6.0)
3300570
60 FORMAT(1H0, 50X, 35HERROR IN LINEQU IN ORTHKN CYCLE = ,F6.0)
3300580
JOISK = 6
3300590

```

.SIMP=.3333333/(NLPO-1)	3300600
IL = 1	3300610
IA = 1	3300620
IF (NH.EQ.0) GO TO 180	3300630
IF (LDISTL.EQ.1) GO TO 112	3300640
IF (KELVIN.EQ.1.OR.KELVIN.EQ.3) GO TO 110	3300650
DO 111 K=1,KBC	3300660
DO 111 J=1,3	3300670
111 STEPS(J,K) = 0.0	3300680
GO TO 112	3300690
110 IF (THICK.NE.1) GO TO 113	3300700
NLH = NLRS/2+1	3300710
DO 115 LR=1,NLH	3300720
TT = TOK+2.0*ZETA1(LR)*(TII-TOK)	3300730
STEPS(1,LR) = ALPHPH*TT	3300740
STEPS(2,LR) = ALPHTH*TT	3300750
115 STEPS(3,LR) = 0.0	3300760
NLH = NLH+1	3300770
DO 116 LR=NLH,NLPO	3300780
TT = TOK+2.0*ZETA1(LR)*(TOK-TOO)	3300790
STEPS(1,LR) = ALPHPH*TT	3300800
STEPS(2,LR) = ALPHTH*TT	3300810
116 STEPS(3,LR) = 0.0	3300820
GO TO 112	3300830
113 DO 200 K=1,2	3300840
DO 200 LR=1,NLPO	3300850
LRT = LR+(K-1)*NLPO	3300860
GO TO (300,400),K	3300870
300 TT = TIK+ZETA2(LR)*(TII-TIK)	3300880
GO TO 500	3300890
400 TT = TOK+ZETA2(LR)*(TOO-TOK)	3300900
500 STEPS(1,LRT) = ALPHPH*TT	3300910
STEPS(2,LRT) = ALPHTH*TT	3300920
200 STEPS(3,LRT) = 0.0	3300930
112 CONTINUE	3300940
IF (DELP/ABS(DELP).EQ.DELP1/ABS(DELP1)) GO TO 180	3300950
DO 181 K=1,KBC	3300960
NPLA(K) = 0	3300970
DO 181 J=1,3	3300980
181 SBAPH(J,K) = SIGMA(J,K)	3300990
DO 182 J=1,3	3301000
NPLAST(J) = 0	3301010
182 STBAPH(J) = STSIG(J)	3301020
180 CONTINUE	3301030
IF (NAPEX.EQ.0.OR.(NH.NE.0.AND.IBEGIN.NE.1)) GO TO 49	3301040
IF (NPR.EQ.0) GO TO 49	3301050
IF (PHI.NE.TIC) GO TO 49	3301060
WRITE(6,42)	3301070
42 FORMAT(/20X,'THIS IS AN APEX SEGMENT')	3301080
49 CONTINUE	3301090
356 GO TO (1781,1782,1783),IGEOM	3301100
C PHI COORDINATE	3301110
1781 EPSITH=X1R0*(YCORR(IL+5)*CS-YCORR(IL+6)*SN)	3301120
1 +X1*YAOPH*SAVY(9)	3301130
EPSIPH=X1R1*(YDOT(IL+5) - YCORR(IL+6))	3301140
1 +X1*YCORR(IL+7)*SAVY(5)	3301150
GAPHTH = YDOT(IL+4)*X1R1 - ( YCORR(IL+4)*CS)*X1R0	3301160
1 -X1*(YAOPH*SAVY(5)+YCORR(IL+7)*SAVY(9))	3301170
XKPH = YDOT(IL+7)*X1R1	3301180
XKTH = X1R0* YCORR(IL+7)*CS	3301190
XKPT = X1R0*0.5*(2.0*YAOPH*CS+X1R1*(	3301200

```

1 YDOT(IL+4) * SN + YCORR(IL+4) * CS          )) 3301210
GO TO 1785 3301220
C CONE 3301230
1782 EPSITH = (1.0/(S*CS)) * ( +YCORR(IL+5)*CS-SN*YCORR(IL+6)) 3301240
1 +X1*YAOPH*SAVY(9) 3301250
EPSIPH= YDOT(IL+5) 3301260
1 +X1*YCORR(IL+7)*SAVY(5) 3301270
GAPHTH = YDOT(IL+4) - 1.0/(S*CS) * ( +CS * YCORR(IL+4)) 3301280
1 -X1*(YAOPH*SAVY(5)+YCORR(IL+7)*SAVY(9)) 3301290
XKPH = YDOT(IL+7) 3301300
XKTH = 1.0/(S*CS) * YCORR(IL+7) * CS 3301310
XKPT = 1.0/(2.0*S*CS)*(2.0*YAOPH*CS+ 3301320
1 YDOT(IL+4) * SN) 3301330
GO TO 1785 3301340
C CYLINDER 3301350
1783 EPSITH= X1RO* ( - YCORR(IL+6)) 3301360
1 +X1*YAOPH*SAVY(9) 3301370
EPSIPH= YDOT(IL+5) 3301380
1 +X1*YCORR(IL+7)*SAVY(5) 3301390
GAPHTH= YDOT(IL+4) 3301400
1 -X1*(YAOPH*SAVY(5)+YCORR(IL+7)*SAVY(9)) 3301410
XKPH = YDOT(IL+7) 3301420
XKPT = 0.5*X1RO*YDOT(IL+4) 3301430
XKTH = 0.0 3301440
1785 CONTINUE 3301450
280 CONTINUE 3301460
CE(1) = EPHI/(1.0-XNUTP*XNUPT) 3301470
CE(2) = ETHET/(1.0-XNUTP*XNUPT) 3301480
CE(3) = XGPT 3301490
CE(4) = XNUPT*EPHI/(1.0-XNUTP*XNUPT) 3301500
ALF(1) = 1.0/EPHI 3301510
ALF(2) = 1.0/ETHET 3301520
ALF(3) = 1.0/XGPT 3301530
ALF(4) = -XNUPT/ETHET 3301540
C INITIALIZE EPSINT ARRAY 3301550
285 DO 290 JJ = 1,3 3301560
DO 290 JT = 1,2 3301570
290 EPSINT(JJ,JT) = 0.0 3301580
C 3301590
LIM = 2 3301600
IF (THICK.EQ.1) LIM = 1 3301610
DO 3800 IS=1,LIM 3301620
DO 2911 JJ=1,3 3301630
DO 2911 JT=1,2 3301640
2911 EPSTNT(JJ,JT) = 0.0 3301650
DO 380 LR = 1,NLPO 3301660
LRT = NLPO*(IS-1)+LR 3301670
GO TO (2901,2902),LIM 3301680
2901 TEMP(4) = ZETA1(LR)*HI/2.0 3301690
GO TO 292 3301700
2902 GO TO (2903,2904),IS 3301710
2903 TEMP(4) = ZETA2(LR)*HI+(2.0*T*HO+HO*HO-HI*HI)/2.0/(HI+HO) 3301720
GO TO 292 3301730
2904 TEMP(4) = ZETA2(LR)*HO-(2.0*HI*(HO+T)+HI*HI+HO*HO)/2.0/(HI+HO) 3301740
292 DO 293 II=1,3 3301750
293 TEPS(II) = DELP*STEPS(II,LRT) 3301760
C 3301770
CALL SHSRSE (DSIG,TEMP,DSTR,1,TEPS) 3301780
IF(NPLEV .EQ.0) GO TO 395 3301790
C 3301800
315 TEMP(5) = SIGMA(1,LRT)-SALPH(1,LRT) 3301810

```

TEMP(6) = SIGMA(2,LRT)-SALPH(2,LRT)	3301820
TEMP(7) = SIGMA(3,LRT)-SALPH(3,LRT)	3301830
IF (NPLA(LRT).LE.0) GO TO 375	3301840
C	3301850
IF (GPLUH*TEMP(5)*DSIG(1)+FPLUH*TEMP(6)*DSIG(2)-HP*(TEMP(5)*	3301860
1 DSIG(2)+TEMP(6)*DSIG(1))+TWON*TEMP(7)*DSIG(3).LT.ZEPS) GO TO 370	3301870
DO 318 JJ=1,3	3301880
318 TEMP(JJ) = TEMP(JJ)-TEPS(JJ)	3301890
IF (KORI.GT.0) GO TO 319	3301900
IF (RMOSN.EQ.-1.0) GO TO 320	3301910
CALL SEPSIS (TEMP,DEPS,SIGMA,DSIG,SEPS,SALPH,SBAPH,LRT,NERR,	3301920
1 RMOSN,RMOSS,ROC,YLDST,EFF,KORI)	3301930
IF(NERR .EQ.0) GO TO 335	3301940
WRITE(JDISK,55) P	3301950
GO TO 980	3301960
319 IF (RMOSNX.EQ.0.0) GO TO 320	3301970
CALL ORTHKN (TEMP,DEPS,DSIG,LRT,ALF,NERR)	3301980
IF (NERR.EQ.0) GO TO 335	3301990
WRITE(JDISK,60) P	3302000
GO TO 980	3302010
C	3302020
320 CALL EPSIS (TEMP,DEPS,SIGMA,DSIG,SEPS,LRT,NERR,GPLUH,FPLUH,HP,	3302030
1 TWON)	3302040
IF(NERR .EQ.0) GO TO 335	3302050
WRITE(JDISK,50) P	3302060
GO TO 980	3302070
335 IF(LR .EQ.2*(LR/2)) GO TO 360	3302080
IF(LR .EQ. 1 .OR. LR .EQ. NLPO) GO TO 350	3302090
DO 340 JJ = 1,3	3302100
EPSTNT(JJ,1) = EPSTNT(JJ,1)+2.0*DEPS(JJ)	3302110
340 EPSTNT(JJ,2) = EPSTNT(JJ,2)+2.0*TEMP(4)*DEPS(JJ)	3302120
GO TO 380	3302130
350 DO 355 JJ = 1,3	3302140
EPSTNT(JJ,1) = EPSTNT(JJ,1)+DEPS(JJ)	3302150
355 EPSTNT(JJ,2) = EPSTNT(JJ,2)+TEMP(4)*DEPS(JJ)	3302160
GO TO 380	3302170
360 DO 365 JJ = 1,3	3302180
EPSTNT(JJ,1) = EPSTNT(JJ,1)+4.0*DEPS(JJ)	3302190
365 EPSTNT(JJ,2) = EPSTNT(JJ,2)+4.0*TEMP(4)*DEPS(JJ)	3302200
GO TO 380	3302210
370 NPLA(LRT) = -LRT	3302220
375 DO 378 JJ = 1,3	3302230
SIGMA(JJ,LRT) = SIGMA(JJ,LRT)+DSIG(JJ)	3302240
378 TEMP(JJ+4) = TEMP(JJ+4) + DSIG(JJ)	3302250
YCOND = YEPS	3302260
IF (KORI.EQ.0) YCOND = YCOND*EFF(LRT)*EFF(LRT)/YLDST	3302270
IF (GPLUH*TEMP(5)*TEMP(5)+FPLUH*TEMP(6)*TEMP(6)-2.0*HP*TEMP(5)*	3302280
1 TEMP(6)+TWON*TEMP(7)*TEMP(7).GE.YCOND) NPLA(LRT) = LRT	3302290
GO TO 380	3302300
395 CONTINUE	3302310
DO 398 JJ=1,3	3302320
398 SIGMA(JJ,LRT) = SIGMA(JJ,LRT)+DSIG(JJ)	3302330
TEMP(1) = GPLUH*SIGMA(1,LRT)*SIGMA(1,LRT)+FPLUH*SIGMA(2,LRT)*	3302340
1 SIGMA(2,LRT)-2.0*HP*SIGMA(1,LRT)*SIGMA(2,LRT)+TWON*SIGMA(3,LRT)*	3302350
2 SIGMA(3,LRT)	3302360
IF (TEMP(1).LT.YEPS) GO TO 380	3302370
NPLA(LRT) = LRT	3302380
NPLEV = 1	3302390
380 CONTINUE	3302400
GO TO (3801,3802),IS	3302410
3801 DO 385 JJ=1,3	3302420

```

DO 385 JT=1,2
385 EPSINT(JJ,JT) = EPSINT(JJ,JT)+EPSTNT(JJ,JT)*SIMP*HI
GO TO 3800
3802 DO 386 JJ=1,3
DO 386 JT=1,2
386 EPSINT(JJ,JT) = EPSINT(JJ,JT)+EPSTNT(JJ,JT)*SIMP*HO
3800 CONTINUE
DO 435 JJ=1,6
435 STR(JJ) = STR(JJ) + DSTR(JJ)
DENPT = 0.0
DENPH = 0.0
DENTH = 0.0
DEMPH = 0.0
DEMTH = 0.0
DEMPT = 0.0
GO TO (5000,5000,5000,5250,5250,5250,5500,5500,5500,5750,5750,
1 5750),ISTTAB
C SMEARED RINGS AND STRINGER PLASTICITY
5750 IF (APH.EQ.0.0) GO TO 5850
DTOT(1) = EPSITH-CPH*XKPH
STSRN(1) = STSRN(1)+DTOT(1)
DTOT(1) = DTOT(1)-DELP*ALPHS*TS
CALL SMEAR (ES,NPLEVS(1),NPLAST(1),STSIG(1),STALPH(1),RMOSNS,
1 STREPS(1),RMOSSS,SIGDXS,STBAPH(1),EFFST(1),DENPH,
2 DEMPH,SPH,CPH,DTOT(1),APH)
5850 IF (ATH.EQ.0.0) GO TO 5000
DTOT(2) = EPSITH-CTH*XKTH
STSRN(2) = STSRN(2)+DTOT(2)
DTOT(2) = DTOT(2)-DELP*ALPHR*TR
CALL SMEAR (ER,NPLEVS(2),NPLAST(2),STSIG(2),STALPH(2),RMOSNR,
1 STREPS(2),RMOSSR,SIGDXR,STBAPH(2),EFFST(2),DENTH,
2 DEMTH,STH,CTH,DTOT(2),ATH)
GO TO 5000
C WAFFLE PLASTICITY
5250 IF (ATH.EQ.0.0) GO TO 5000
DTOT(1) = EPSIPH-CPH*XKPH
DTOT(2) = EPSITH-CPH*XKTH
DTOT(3) = GAPHTH-2.0*CPH*XKPT
EE(1) = DTOT(1)-CSB*CSB+DTOT(2)*SNB*SNB+DTOT(3)*SNB*CSB
STSRN(1) = STSRN(1)+EE(1)
EE(1) = EE(1)-DELP*ALPHS*TS
EE(2) = DTOT(1)*SNB*SNB+DTOT(2)*CSB*CSB-DTOT(3)*SNB*CSB
STSRN(2) = STSRN(2)+EE(2)
EE(2) = EE(2)-DELP*ALPHS*TS
DO 5300 II=1,2
CALL SMEAR (ES,NPLEVS(II),NPLAST(II),STSIG(II),STALPH(II),RMOSNS,
1 STREPS(II),RMOSSS,SIGDXS,STBAPH(II),EFFST(II),DEN(II),
2 DEM(II),SPH,CPH,EE(II),APH)
5300 CONTINUE
DENPH = (DEN(1)*CSB+DEN(2)*SNB)/(CSB+SNB)
DENTH = (DEN(1)*SNB+DEN(2)*CSB)/(CSB+SNB)
DEMPH = DENPH*CPH
DEMTH = DENTH*CPH
DENPT = (DEN(1)-DEN(2))/2.0
DEMPT = DENPT*CPH
GO TO 5000
C ISOGRID PLASTICITY
5500 IF (APH.EQ.0.0) GO TO 5000
DTOT(1) = EPSIPH-CPH*XKPH
DTOT(2) = EPSITH-CPH*XKTH
DTOT(3) = GAPHTH-2.0*CPH*XKPT

```



TEMP(1) = (DTOT(1)+DTOT(2))/2.0	3303040
TEMP(2) = (DTOT(2)-DTOT(1))/2.0	3303050
TEMP(3) = DTOT(2)	3303060
DTOT(1) = TEMP(1)-TEMP(2)*COS(2.0*BETTA)+DTOT(3)/2.0*SIN(2.0*	3303070
1 BETTA)	3303080
STSRN(1) = STSRN(1)+DTOT(1)	3303090
DTOT(1) = DTOT(1)-DELP*ALPHS*TS	3303100
DTOT(2) = TEMP(1)-TEMP(2)*COS(2.0*BETTA)-DTOT(3)/2.0*SIN(2.0*	3303110
1 BETTA)	3303120
STSRN(2) = STSRN(2)+DTOT(2)	3303130
DTOT(2) = DTOT(2)-DELP*ALPHS*TS	3303140
DTOT(3) = TEMP(3)	3303150
STSRN(3) = STSRN(3)+DTOT(3)	3303160
DTOT(3) = DTOT(3)-DELP*ALPHS*TS	3303170
DO 5525 II=1,3	3303180
CALL SMEAR (ES,NPLEVS,NPLAST(II),STSIG(II),STALPH(II),RMOSNS,	3303190
1 STREPS(II),RMOSSS,SIGOX,STBAPH(II),EFFST(II),DEN(II),	3303200
2 DEM(II),SPH,CPH,DTOT(II),APH)	3303210
5525 CONTINUE	3303220
DENPH = (DEN(1)*CSB+DEN(2)*CSB)/2.0/SNB	3303230
DENTH = (DEN(1)*SNB+DEN(2)*SNB+2.0*DEN(3))/2.0/CSB	3303240
DENPT = (DEN(1)-DEN(2))/2.0	3303250
DEMPH = DENPH*CPH	3303260
DEMT = DENTH*CPH	3303270
DEMP = DENPT*CPH	3303280
GO TO 5000	3303290
5000 CONTINUE	3303300
SAVX(1) = SAVY(1)+YPRED(I+5)	3303310
SAVX(2) = SAVY(2)+YDOT(I+5)	3303320
SAVX(3) = SAVY(3)+YPRED(I+6)	3303330
SAVX(4) = SAVY(4)+YDOT(I+4)	3303340
SAVX(5) = SAVY(5)+YPRED(I+7)	3303350
SAVX(6) = SAVY(6)+YPRED(I+1)	3303360
SAVX(7) = SAVY(7)+YANTH	3303370
SAVX(8) = SAVY(8)+YANPT	3303380
SAVX(9) = SAVY(9)+YAOPH	3303390
SAVX(10) = CE(2)*(EPSINT(2,1)+XNUTP*EPSINT(1,1))	3303400
1 +DENTH	3303410
SAVX(11) = CE(1)*(EPSINT(1,1)+XNUPT*EPSINT(2,1))	3303420
1 +DENPH	3303430
SAVX(12) = XGPT*EPSINT(3,1)	3303440
1 +DENPT	3303450
SAVX(13) = CE(2)*(EPSINT(2,2)+XNUTP*EPSINT(1,2))	3303460
1 +DEMT	3303470
SAVX(14) = CE(1)*(EPSINT(1,2)+XNUPT*EPSINT(2,2))	3303480
1 +DEMPH	3303490
SAVX(15) = XGPT*EPSINT(3,2)	3303500
1 +DEMP	3303510
SAVX(16) = SAVY(16)+YPRED(I)	3303520
SAVX(17) = SAVY(17)+YPRED(I+2)	3303530
SAVX(18) = SAVY(18)+YPRED(I+3)	3303540
SAVX(19) = SAVY(19)+YPRED(I+4)	3303550
SAVX(20) = SAVY(20)+YANTH	3303560
SAVX(21) = SAVY(21)+YAMPT	3303570
SAVX(22) = EPSITH	3303580
SAVX(23) = XKTH	3303590
SAVX(24) = SAVY(24)+DELP*XFTHLD	3303600
SAVX(25) = SAVY(25)+DELP*XFPHLD	3303610
SAVX(26) = SAVY(26)+DELP*XFZELD	3303620
SAVX(27) = SAVY(27)+DELP*XMTHLD	3303630
SAVX(28) = SAVY(28)+DELP*XMPLD	3303640

SAVX(29) = SAVY(29)+YDOT(I)	3303650
SAVX(30) = SAVY(30)+YDOT(I+1)	3303660
SAVX(31) = SAVY(31)+YDOT(I+2)	3303670
SAVX(32) = SAVY(32)+YDOT(I+3)	3303680
DO 120 J=6,8	3303690
120 IF (ABS(SAVX(J)).LT.1.E-5) SAVX(J) = 0.0	3303700
DO 121 J=10,18	3303710
121 IF (ABS(SAVX(J)).LT.1.E-5) SAVX(J) = 0.0	3303720
DO 122 J=20,21	3303730
122 IF (ABS(SAVX(J)).LT.1.E-5) SAVX(J) = 0.0	3303740
CALL SAVXES (SAVX)	3303750
WRITE(JO) SAVX,NPLEV,NPLA,SIGMA,SALPH,SBAPH,STEPS,STR,EFF,STSRN,	3303760
1 NPLAST,STSIG,STREPS,STALPH,STBAPH,NPLEVS,EFFST,SEPS	3303770
IF(NH.NE.0.AND.IBEGIN.NE.1.AND.NGR.EQ.0) GO TO 980	
IF (NPR.EQ.0.AND.NGR.EQ.0) GO TO 980	3303790
THK = 0.0	3303800
DO 540 J=1,3	3303810
SIGMI(J) = 0.0	3303820
SIGMO(J) = 0.0	3303830
EPSI(J) = 0.0	3303840
540 EPSO(J) = 0.0	3303850
GO TO (158,131,158,152,153,154,152,153,154,152,153,154),ISTTAB	3303860
131 GO TO (152,153,154,158),THICK	3303870
152 THK = HI	3303880
DO 542 J=1,3	3303890
SIGMO(J) = SIGMA(J,NLPO)	3303900
EPSI(J) = STR(J)+HI/2.0*STR(J+3)	3303910
542 EPSO(J) = STR(J)-HI/2.0*STR(J+3)	3303920
EPSI(3) = EPSI(3)+HI/2.0*STR(6)	3303930
EPSO(3) = EPSO(3)-HI/2.0*STR(6)	3303940
GO TO 157	3303950
153 THK = T+2.0*HI	3303960
GO TO 155	3303970
154 THK = T+HI+HO	3303980
155 CONTINUE	3303990
ZETAI = (HI*HI+HO*HO+2.0*HI*HO+2.0*HO*T)/(2.0*(HI+HO))	3304000
ZETAO = (HI*HI+HO*HO+2.0*HI*HO+2.0*HI*T)/(2.0*(HI+HO))	3304010
DO 543 J=1,3	3304020
SIGMO(J) = SIGMA(J,NLPO*2)	3304030
EPSI(J) = STR(J)+ZETAI*STR(J+3)	3304040
543 EPSO(J) = STR(J)-ZETAO*STR(J+3)	3304050
EPSI(3) = EPSI(3)+ZETAI*STR(6)	3304060
EPSO(3) = EPSO(3)-ZETAO*STR(6)	3304070
157 DO 541 J=1,3	3304080
541 SIGMI(J) = SIGMA(J,1)	3304090
158 CONTINUE	3304100
IF (NGR.EQ.1) CALL ARRAYS (SAVX(19),SAVX(1),SAVX(3),SIGMI(2),	3304110
1 SIGMI(1),SIGMI(3),SIGMO(2),SIGMO(1),SIGMO(3),PHI)	3304120
IF(NPR.EQ.0.OR.IBEGIN.NE.1) GO TO 980	
DEGRES = 0.0	3304140
IF (IGEOM.EQ.1) DEGRES = PHI*57.29578	3304150
WRITE(6,7001) PHI,DEGRES,RO,THK,STEP,EPSI(2),	3304160
1 STR(2),STR(1),(STR(I),I=3,5),EPSO(2),	3304170
2 SAVX(19),STR(6),SAVX(7),SAVX(6),SAVX(8),EPSI(1),	3304180
3 SAVX(1),SAVX(17),SAVX(20),SAVX(18),SAVX(21),EPSO(1),	3304190
4 SAVX(3),SAVX(16),SIGMI(2),SIGMI(1),SIGMI(3),EPSI(3),	3304200
5 SAVX(5),SAVX(9),SIGMO(2),SIGMO(1),SIGMO(3),EPSO(3)	3304210
7001 FORMAT(////(3X,6(1PE14.7,7X)))	3304220
IF (NPLEV.EQ.0) GO TO 515	3304230
WRITE(6,519) (NPLA(NL),NL=1,KBC)	3304240
519 FORMAT(//' NPLA =',8X,21I5)	3304250

WRITE(6,517) ((SIGMA(L3,NL),L3=1,3),NL=1,KBC)	3304260
517 FORMAT(/' SIGMA =',7X,1P9E13.5/(15X,1P9E13.5))	3304270
WRITE(6,518) ((SEPS(L3,NL),L3=1,3),NL=1,KBC)	3304280
518 FORMAT(/' EPSILON PLAS =',1P9E13.5/(15X,1P9E13.5))	3304290
515 CONTINUE	3304300
980 RETURN	3304310
END	3304320

FOR, IS SHSRSE,SHSRSE	
SUBROUTINE SHSRSE (DSIG,TEMP,STR,LL,EPS)	3500010
COMMON /CHAIN/ ZETA1(21),ZETA2(21),NODE,ALF(4),CE(4),NLRS,HI,HO,T	3500020
DIMENSION DSIG(3),TEMP(4),STR(1),EPS(1),ESR(3)	3500030
C    IF (ISTTAB.NE.2) GO TO 640	3500040
C 621 GO TO (610,650,650,640),THICK	3500050
610 CONTINUE	3500060
650 CONTINUE	3500070
640 CONTINUE	3500080
TEMP(1) = STR(LL)-TEMP(4)*STR(LL+3)	3500090
TEMP(2) = STR(LL+1)-TEMP(4)*STR(LL+4)	3500100
TEMP(3) = STR(LL+2)-2.0*TEMP(4)*STR(LL+5)	3500110
ESR(1)=TEMP(1)-EPS(1)	3500120
ESR(2)=TEMP(2)-EPS(2)	3500130
ESR(3)=TEMP(3)-EPS(3)	3500140
DSIG(1) = CE(1)*ESR(1)+CE(4)*ESR(2)	3500150
DSIG(2) = CE(4)*ESR(1)+CE(2)*ESR(2)	3500160
DSIG(3) = CE(3)*ESR(3)	3500170
RETURN	3500180
END	3500190

```

FOR, IS SEPSIS, SEPSIS
SUBROUTINE SEPSIS (DTOT, DEPS, SIGMA, DSIG, SEPS, SALPH, SBAPH, LR, NERR, 3600010
1 RMOSN, RMOSS, ROC, YLDST, EFF, KORI) 3600020
C STRAIN HARDENING- SHELL ELEMENTS. 3600030
C 3600040
C 3600050
COMMON /CHAIN/ ZETA1(21), ZETA2(21), NODE, ALF(4), CE(4), NLRS, HI, HO, T 3600060
DIMENSION DTOT(3), DEPS(3), SIGMA(3,1), DSIG(3), SEPS(3,1), 3600070
D SALPH(3,1), SBAPH(3,1), TEMP(3), SAG(3), R(3,3), CAPM(3) 3600080
DIMENSION EFF(1) 3600090
DO 100 I=1,3 3600100
SAG(I)=SIGMA(I,LR)-SALPH(I,LR) 3600110
100 TEMP(I)=SIGMA(I,LR)-SBAPH(I,LR) 3600120
C CHECK FOR ISOTROPIC HARDENING 3600130
IF (KORI.EQ.0) GO TO 301 3600140
C CHECK FOR LINEAR STRAIN HARDENING 3600150
IF (RMOSS.NE.0.0) GO TO 252 3600160
DEN = ROC 3600170
GO TO 254 3600180
C NON LINEAR 3600190
252 DEN = ROC*(RMOSS/SQRT(TEMP(1)*(TEMP(1)-TEMP(2))+TEMP(2)*TEMP(2))+ 3600200
1 3.0*TEMP(3)*TEMP(3))**RMOSN 3600210
GO TO 254
301 IF (RMOSS.NE.0.0) GO TO 352 3600220
DEN = -(RMOSN+1.0)/RMOSN/ALF(1) 3600230
GO TO 354 3600240
352 DEN = 2.333333/ALF(1)/(RMOSN+1.0)*(RMOSS/EFF(LR))**RMOSN 3600250
354 DEN = DEN*EFF(LR)*EFF(LR) 3600260
254 CAPM(1)=SAG(1)-0.5*SAG(2) 3600280
CAPM(2)=SAG(2)-0.5*SAG(1) 3600290
CAPM(3)=3.0*SAG(3) 3600300
C FORM R MATRIX RELATING TOTAL STRAIN AND STRESS INCREMENT 3600310
TEMP(1)=CAPM(1)/DEN 3600320
R(1,1) = ALF(1)+TEMP(1)*CAPM(1) 3600330
R(2,1) = ALF(4)+TEMP(1)*CAPM(2) 3600340
R(1,2)=R(2,1) 3600350
R(3,1)=TEMP(1)*CAPM(3) 3600360
R(1,3)=R(3,1) 3600370
TEMP(1)=CAPM(2)/DEN 3600380
R(2,2) = ALF(2)+TEMP(1)*CAPM(2) 3600390
R(3,2)=TEMP(1)*CAPM(3) 3600400
R(2,3)=R(3,2) 3600410
R(3,3) = ALF(3)+CAPM(3)*CAPM(3)/DEN 3600420
C SOLVE SYSTEM FOR STRESS INCREMENT 3600430
CALL LINEQU(R, DTOT, 3, 1, 3, NERR) 3600440
IF (NERR.EQ.0) GO TO 260 3600450
GO TO 990 3600460
260 DSIG(1)=DTOT(1) 3600470
DSIG(2)=DTOT(2) 3600480
DSIG(3)=DTOT(3) 3600490
C PLASTIC STRAIN INCREMENTS 3600500
TEMP(1)=CAPM(1)*DTOT(1)+CAPM(2)*DTOT(2)+CAPM(3)*DTOT(3) 3600510
TEMP(2) = TEMP(1)/YLDST 3600520
IF (KORI.EQ.0) TEMP(2) = 0.0 3600530
TEMP(1)=TEMP(1)/DEN 3600540
DO 270 I=1,3 3600550
DEPS(I)=CAPM(I)*TEMP(1) 3600560
SALPH(I,LR)=SALPH(I,LR)+SAG(I)*TEMP(2) 3600570
SIGMA(I,LR)=SIGMA(I,LR)+DSIG(I) 3600580
IF (KORI.EQ.0) EFF(LR) = SQRT(SIGMA(1,LR)**2+SIGMA(2,LR)**2- 3600590
1 SIGMA(1,LR)*SIGMA(2,LR)+3.0*SIGMA(3,LR)**2) 3600600
270 SEPS(I,LR)=SEPS(I,LR)+DEPS(I) 3600610

```

8888 CONTINUE  
CALL ETRAP  
STOP  
END

202440  
202450  
202460  
202470

14

FOR, IS LINEQU, LINEQU	3900010
SUBROUTINE LINEQU(A, Y, M, N, MID, NIX)	3900020
C	3900030
DIMENSION A(MID, MID), Y(MID, 1)	3900040
M1 = M - 1	3900050
DO 150 K = 1, M1	3900060
KP = K + 1	3900070
X = 0.	3900080
DO 110 I = K, M	3900090
IF(X - ABS(A(I, K))) 100, 110, 110	3900100
100 X = ABS(A(I, K))	3900110
L = I	3900120
110 CONTINUE	3900130
IF(X) 120, 120, 130	3900160
130 DO 140 J = 1, M	3900170
X = A(K, J)	3900180
A(K, J) = A(L, J)	3900190
140 A(L, J) = X	3900200
DO 143 J = 1, N	3900210
X = Y(K, J)	3900220
Y(K, J) = Y(L, J)	3900230
143 Y(L, J) = X	3900240
DO 150 I = KP, M	3900250
X = A(I, K) / A(K, K)	3900260
DO 146 J = 1, N	3900270
146 Y(I, J) = Y(I, J) - Y(K, J) * X	3900280
DO 150 J = KP, M	3900290
150 A(I, J) = A(I, J) - A(K, J) * X	3900300
T = ABS(A(M, M))	3900310
IF(T) 160, 120, 160	3900320
160 DO 165 J = 1, N	3900330
165 Y(M, J) = Y(M, J) / A(M, M)	3900340
K = M	3900350
DO 180 I = 1, M1	3900360
X = 0.	3900370
KP = K	3900380
K = K - 1	3900390
DO 180 L = 1, N	3900400
DO 170 J = KP, M	3900410
170 X = X + A(K, J) * Y(J, L)	3900420
180 Y(K, L) = (Y(K, L) - X) / A(K, K)	3900430
NIX = 0	
GO TO 190	
120 NIX = -(KP - 1)	3900440
190 RETURN	3900450
END	

```

FOR, IS ORTHKN, ORTHKN
SUBROUTINE ORTHKN (DTOT, DEPS, DSIG, LR, ALF, NERR)
COMMON /LASTEQ/ DUM(124), RMOSSX, RMOSNX, YLDST, ROC, HP, FPLUH, GPLUH,
C          TWON, RMOSSY, RMOSNY, RMOSSY, RMONXY
COMMON /WOOD/ SAVY(53), NPLEV, NLPO, NPLA(21), STR(6), SIGMA(3,21),
C          SEPS(3,21), SALPH(3,21), SBAPH(3,21), STEPS(3,21),
O          EFF(21), STSRN(3), NPLAST(3), STSIG(3), STREPS(3),
M          STALPH(3), STBAPH(3), EFFST(3), NPLEVS(3)
DIMENSION CAPM(4), TEMP(3), DEPS(1), DSIG(1), R(3,3), ALF(1), SAG(3)
DIMENSION DTOT(1)
DO 100 I=1,3
SAG(I) = SIGMA(I,LR)-SALPH(I,LR)
100 TEMP(I) = SIGMA(I,LR)-SBAPH(I,LR)
SIGB = FPLUH*TEMP(2)**2+GPLUH*TEMP(1)**2-2.0*HP*TEMP(1)*TEMP(2)+
1 TWON*TEMP(3)**2
IF (RMOSSX.NE.0.0) GO TO 205
CX=ALF(1)*(1.0-RMOSNX)/RMOSNX*(GPLUH**2+HP**2+(GPLUH-HP)**2)/
1 GPLUH**2
GO TO 210
205 CX=RMOSSX*ALF(1)/2.333333*(SQRT(SIGB/GPLUH)/RMOSSX)**(RMOSNX-1.0)
1 *(GPLUH**2+HP**2+(GPLUH-HP)**2)/GPLUH**2
210 IF (RMOSSY.NE.0.0) GO TO 215
CY=ALF(2)*(1.0-RMOSNY)/RMOSNY*(FPLUH**2+HP**2+(FPLUH-HP)**2)/
1 FPLUH**2
GO TO 220
215 CY=RMOSNY*ALF(2)/2.333333*(SQRT(SIGB/FPLUH)/RMOSSY)**(RMOSNY-1.0)
1 *(FPLUH**2+HP**2+(FPLUH-HP)**2)/FPLUH**2
220 IF (RMOSSY.NE.0.0) GO TO 225
CXY=0.5*ALF(3)*(1.0-RMONXY)/RMONXY
GO TO 230
225 CXY=RMONXY*ALF(3)/4.6666667*(SQRT(SIGB/TWON)/RMOSSY)**(RMONXY
1 -1.0)
230 ONDC=(GPLUH*SAG(1)**2-HP*SAG(1)*SAG(2))*CX+(FPLUH*SAG(2)**2
1 -HP*SAG(1)*SAG(2))*CY+TWON*SAG(3)**2*CXY
240 CAPM(1) = 2.0*(GPLUH*SAG(1)-HP*SAG(2))
CAPM(2) = 2.0*(FPLUH*SAG(2)-HP*SAG(1))
CAPM(3) = 2.0*TWON*SAG(3)
CAPM(4) = -2.0*((FPLUH-HP)*SAG(2)+(GPLUH-HP)*SAG(1))
DEN=(CAPM(1)**2+CAPM(2)**2+CAPM(3)**2/2.+CAPM(4)**2)/ONDC
TEMP(1) = CAPM(1)/DEN
R(1,1) = ALF(1)+TEMP(1)*CAPM(1)
R(2,1) = ALF(4)+TEMP(1)*CAPM(2)
R(1,2) = R(2,1)
R(3,1) = TEMP(1)*CAPM(3)
R(1,3) = R(3,1)
TEMP(1) = CAPM(2)/DEN
R(2,2) = ALF(2)+TEMP(1)*CAPM(2)
R(3,2) = TEMP(1)*CAPM(3)
R(2,3) = R(3,2)
R(3,3) = ALF(3)+CAPM(3)*CAPM(3)/DEN
C SOLVE SYSTEM FOR STRESS INCREMENT
CALL LINEQU (R,DTOT,3,1,3,NERR)
IF (NERR.EQ.0) GO TO 260
GO TO 990
260 DSIG(1) = DTOT(1)
DSIG(2) = DTOT(2)
DSIG(3) = DTOT(3)
C PLASTIC STRAIN INCREMENTS
TEMP(1) = CAPM(1)*DTOT(1)+CAPM(2)*DTOT(2)+CAPM(3)*DTOT(3)
TEMP(2) = TEMP(1)/DEN
DO 270 I=1,3
DEPS(I) = CAPM(I)*TEMP(2)

```



```
SALPH(I,LR) = SALPH(I,LR)+SAG(I)*TEMP(1)/2.0
SIGMA(I,LR) = SIGMA(I,LR)+DSIG(I)
270 SEPS(I,LR) = SEPS(I,LR)+DEPS(I)
990 RETURN
END
```

```
3800620
3800630
3800640
3800650
3800660
```

```

FOR,IS EPSIS,EP SIS
SUBROUTINE EPSIS (DTOT,DEPS,SIGMA,DSIG,SEPS,LR,NERR,
1          GPLUH,FPLUH,HP,TWON)
C
C   PERFECT PLASTICITY- SHELL ELEMENTS
C
COMMON /CMAIN/ ZETA1(21),ZETA2(21),NODE,ALF(4),CE(4),NLRS,HI,HQ,T
DIMENSION DTOT(1),DEPS(1),SIGMA(3,1),DSIG(1),SEPS(3,1),EUP(3,3),
D SMAM(3),ESTAR(3,3),CAPM(3)
CAPM(1) = GPLUH*SIGMA(1,LR)-HP*SIGMA(2,LR)
CAPM(2) = FPLUH*SIGMA(2,LR)-HP*SIGMA(1,LR)
CAPM(3) = TWON*SIGMA(3,LR)
TMAX = ABS(CAPM(1))
MMAX=1
IF(ABS(CAPM(2)).LT.TMAX) GO TO 110
MMAX = 2
TMAX=ABS(CAPM(2))
110 IF(ABS(CAPM(3)) .LT. TMAX) GO TO 140
MMAX = 3
140 TEMP = CAPM(MMAX)
C
C   INITIALIZE EUP,E UPPER BAR
152 DO 170 I =1,3
DO 160 J=1,3
160 EUP(I,J) = 0.0
170 EUP(I,I) = 1.0
C
C   SET SMAM AND COMPLETE EUP
DO 180 I = 1,3
SMAM(I) = CAPM(I) / TEMP
EUP(MMAX,I) = EUP(MMAX,I) - SMAM(I)
180 CONTINUE
EUP(MMAX,MMAX) = 0.0
C
C   ESTAR=ALF * EUP
DO 190 I =1,3
ESTAR(1,I) = ALF(1)*EUP(1,I)+ALF(4)*EUP(2,I)
ESTAR(2,I) = ALF(4)*EUP(1,I)+ALF(2)*EUP(2,I)
190 ESTAR(3,I) = ALF(3)*EUP(3,I)
C
C   ESTAR=ESTAR,+ E LOWER BAR
DO 200 I =1,3
200 ESTAR(I,MMAX) = ESTAR(I,MMAX) + SMAM(I)
C
C   SOLVE LINEAR SYSTEM FOR DSIG(I.NE.MMAX) AND DEPS(MMAX)
CALL LINEQU(ESTAR,DTOT,3,1,3,NERR)
IF(NERR .EQ.0) GO TO 210
GO TO 990
210 DO 220 I =1,3
220 DSIG(I) = DTOT(I)
C
C   SET DSIG(MMAX) AND DEPS(I.NE.MMAX)
DEPS(MMAX) = DSIG(MMAX)
DSIG(MMAX) = 0.0
DO 230 I =1,3
IF(I .EQ.MMAX) GO TO 230
DSIG(MMAX) = DSIG(MMAX) - SMAM(I) * DSIG(I)
DEPS(I) = SMAM(I) * DEPS(MMAX)
230 CONTINUE
DO 290 I =1,3
SIGMA(I,LR) = SIGMA(I,LR) + DSIG(I)
290 SEPS(I,LR) = SEPS(I,LR) + DEPS(I)

```

**C 990 RETURN  
END**

**3700620  
3700630  
3700640**



```

FOR, IS SAVXES, SAVXES
SUBROUTINE SAVXES (SAVX)
INTEGER SAVJTC, SAVSTP, Q, THICK
INTEGER XN
DOUBLE PRECISION YPRED
C
COMMON STORY(16), XMAT(270, 10), STD(10), SADUS(30), RADUS(30)
COMMON TADUS(30), UADUS(30), SAVTIC(900)
COMMON XN, TEFREE, TIC, PHI, STOP, RESTOP, RTICK, G1, XNL(3), NH
COMMON NST(30), NKL(30), NXMAT(20), SAVJTC(30), SAVSTP(30), JRTIC(30)
COMMON JRSTOP(30), NREG, NMPT, NRC, NSC, NIX, IERROR, KGEOM, IGEOM, ISTTAB
COMMON KELVIN, IBEGIN, NPROB, NSEG, NERROR, Q, THICK, NOJS, NLINKS, NLCASE
COMMON NTSKL, NZ, NBCT, LINPUT, NTRKL, NPASS, XN1, KBC, NRINGS
COMMON LODE, ICYCLE, LDISTL
COMMON /LASTEQ/ YPRED(8), YDOT(8), YASAVE(8),
1 YANTH, YAMTH, YAMPT, YANPT, YAOPH, YAQPH, YAQTH, YAJPH,
2 S, SN, CS, SNSQ, CSSQ, TAN, SEC, CN, X1CS, X1SN, TN,
3 X1RO, X1ROSQ, X1SNRO, X1CSRO, CN1RO, SN1RO, CS1RO,
4 X1R1, X1R2, CS1R1, CS1R2, SN1R1, X1R1SQ, R2SQ, RO, BESQ,
5 ROSQ, XNSQ, BETA, R1, R2, S1, R1DOT, R1SQ,
6 XNTH, XNTPH, XMTTH, XMTPH, XFTHLD, XFPHL D, XFZELD,
7 XMTHLD, XMPHL D, ETHET, EPHI, XGPT, ALPHTH, ALPHPH,
8 XNUTP, XNUPT, XC11, XC22, XC15, XD33, XD22, XD21, XD12,
9 XK11, XK12, XK21, XK22, XK33, XD11,
A M, I, SITIN, SITOUT, SIPIN, SIPOUT, TPTIN, TPTOUT,
B ZBRIN, ZBROUT, SCRIPA, SCRIP1, SIFIN, SIFOUT, TZEPH, TZETH
B ,XNPHI, BETTA, ZETTA, ZC16
C ,RMOSS, RMOSN, YLDST, ROC, HP, FPLUH, GPLUH, TWON
D ,RMOSSY, RMOSNY, RMOSXY, RMONXY
D ,RMOSSNS, RMOSSS, SIGOXS, RMOSNR, RMOSSR, SIGOXR
COMMON /WOOD/ SAVY(53), NPLEV, NLPO, NPLA(21), STR(6), SIGMA(3, 21),
C SEPS(3, 21), SALPH(3, 21), SBAPH(3, 21), STEPS(3, 21),
O EFF(21), STSRN(3), NPLAST(3), STSIG(3), STREPS(3),
M STALPH(3), STBAPH(3), EFFST(3), NPLEVS(3)
COMMON /CDISP/ P, PMAX, DELP, DELP1, YEPS, ZEPS
EQUIVALENCE (XNL(1), X1), (XNL(2), X2), (XNL(3), X3)
DIMENSION SAVX(1)
GO TO (101, 102, 103), IGEOM
101 CONTINUE
A = (SAVX(1)*CS - SAVX(3)*SN)/RO + 0.5*SAVX(9)*SAVX(9) + (SAVX(2) -
1 SAVX(3))/R1 + 0.5*SAVX(5)*SAVX(5)
SAVX(33) = -(SAVX(29) - R1*(CS/RO*(-2.0*SAVX(16) - SAVX(21)*(1.0/R1 -
1 SN/RO)) - X1*(SAVX(24)*A + SAVX(25)*SAVX(4)/R1 + SAVX(26)*
2 SAVX(9)) - SN/RO*(SAVX(28) + X1*(SAVX(7)*SAVX(9) - SAVX(8)*
3 SAVX(5))) - SAVX(24)))
SAVX(34) = -(SAVX(30) - R1*(CS/RO*(-SAVX(6) + SAVX(7)) + SAVX(17)/R1 -
1 X1*(SAVX(25)*A - SAVX(26)*SAVX(5)) - SAVX(25)))
SAVX(35) = -(SAVX(31) + R1*((SAVX(17)*CS + SAVX(7)*SN)/RO + SAVX(6)/R1 +
1 X1*(SAVX(26)*A - SAVX(24)*SAVX(9) + SAVX(25)*SAVX(5)) +
2 SAVX(26)))
SAVX(36) = SAVX(32) - R1*((CS/RO*(SAVX(20) - SAVX(18))) + SAVX(17) +
1 X1*(SAVX(8)*SAVX(9) - SAVX(6)*SAVX(5)) + SAVX(27))
GO TO 105
102 CONTINUE
A = (SAVX(1) - SAVX(3)*TN)/S + 0.5*(SAVX(9)*SAVX(9) + SAVX(5)*
1 SAVX(5)) + SAVX(2)
SAVX(33) = -2.0*SAVX(16)/S + SAVX(21)*TN/(S*S) - X1*(SAVX(24)*A +
1 SAVX(25)*SAVX(4) + SAVX(26)*SAVX(9)) - SAVX(28)*TN/S -
1 TN/S*X1*(SAVX(7))*
2 SAVX(9) - SAVX(8)*SAVX(5)) - SAVX(29) - SAVX(24)

```

```

    SAVX(34) = -(SAVX(6)-SAVX(7))/S-X1*(SAVX(25)*A-SAVX(26)*SAVX(5))- 3400600
1     SAVX(30)-SAVX(25) 3400610
    SAVX(35) = -(SAVX(17)+SAVX(7)*TN)/S-X1*(SAVX(26)*A-SAVX(24)* 3400620
1     SAVX(9)+SAVX(25)*SAVX(5))-SAVX(31)-SAVX(26) 3400630
    SAVX(36) = -(SAVX(20)-SAVX(18))/S+SAVX(17)+X1*(SAVX(8)*SAVX(9)- 3400640
1     SAVX(6)*SAVX(5))+SAVX(27)-SAVX(32)) 3400650
    GO TO 105 3400660
103 CONTINUE 3400670
    A = -SAVX(3)/RO+0.5*(SAVX(9)*SAVX(9)+SAVX(5)*SAVX(5))+SAVX(2) 3400680
    SAVX(33) = -X1*(SAVX(24)*A+SAVX(25)*SAVX(4)+SAVX(26)*SAVX(9))- 3400690
1     SAVX(28)/RO-X1*(SAVX(7)*SAVX(9)-SAVX(8)*SAVX(5))/RO- 3400700
2     SAVX(29)-SAVX(24) 3400710
    SAVX(34) = -X1*(SAVX(25)*A-SAVX(26)*SAVX(5))-SAVX(30)-SAVX(25) 3400720
    SAVX(35) = -SAVX(7)/RO-X1*(SAVX(26)*A-SAVX(24)*SAVX(9)+SAVX(25)* 3400730
1     SAVX(5))-SAVX(31)-SAVX(26) 3400740
    SAVX(36) = -(SAVX(17)+X1*(SAVX(8)*SAVX(9)-SAVX(6)*SAVX(5))+ 3400750
1     SAVX(27))+SAVX(32) 3400760
105 CONTINUE 3400770
    SAVX(37) = SAVY(37)+SAVX(10) 3400780
    SAVX(38) = SAVY(38)+SAVX(11) 3400790
    SAVX(39) = SAVY(39)+SAVX(12) 3400800
    SAVX(40) = SAVY(40)+SAVX(13) 3400810
    SAVX(41) = SAVY(41)+SAVX(14) 3400820
    SAVX(42) = SAVY(42)+SAVX(15) 3400830
    SAVX(43) = SAVY(43)+DELP*XNTPH 3400840
    SAVX(44) = SAVY(44)+DELP*XNTTH 3400850
    SAVX(45) = SAVY(45)+DELP*XMTPH 3400860
    SAVX(46) = SAVY(46)+DELP*XMTTH 3400870
    SAVX(47) = SAVY(47)+YDOT(I+7) 3400880
    IF (ISTTAB.NE.2) GO TO 7776 3400890
    GO TO (151,152,153),IGEOM 3400900
151 CONTINUE 3400910
    SAVX(48) = SAVX(7)-(XNUPT*SAVX(6)+(XK11-XNUPT**2*XK22)*((SAVX(1)* 3400920
1     CS-SAVX(3)*SN)*X1RO+X1*SAVX(9)**2*0.5)+XNUPT*SAVX(43)- 3400930
2     SAVX(44)+X2*(XNUPT*SAVX(38)-SAVX(37))) 3400940
    SAVX(49) = SAVX(20)-(XNUPT*SAVX(18)-(XD11-XNUPT**2*XD22)*X1RO* 3400950
1     SAVX(5)*CS+(XNUPT*SAVX(45)-SAVX(46))+X2*(XNUPT*SAVX(41) 3400960
2     -SAVX(40))) 3400970
    SAVX(50) = SAVX(21)-((-1.0/((RO/XD33)+(SNSQ*X1RO/XK33)))*(SAVX(19) 3400980
1     *(CS1R1-CN1RO)+SAVX(16)*SN/XK33+X2*(SAVX(39)*SN/XK33- 3400990
2     SAVX(42)*RO/XD33)+SN*X1*SAVX(9)*SAVX(5))) 3401000
    SAVX(51) = SAVX(4)-(R1*(SAVX(19)*CS1RO+SAVX(16)/XK33+X2*SAVX(39)/ 3401010
1     XK33+SAVX(21)*SN1RO/XK33)+R1*X1*SAVX(9)*SAVX(5) 3401020
    SAVX(52) = SAVX(2)-(R1*(SAVX(3)*X1R1+(1.0/(XK22-XNUTP**2*XK11))* 3401030
1     (SAVX(6)-XNUTP*SAVX(7)+SAVX(43)-XNUTP*SAVX(44))+X2* 3401040
2     (SAVX(38)-XNUTP*SAVX(37))))-R1*SAVX(5)**2*X1*0.5 3401050
    SAVX(53) = SAVX(47)-(R1*(1.0/(XD22-XNUTP**2*XD11))*(-SAVX(18)+ 3401060
1     XNUTP*SAVX(20)-SAVX(45)+XNUTP*SAVX(46)-X2*(SAVX(41)- 3401070
2     XNUTP*SAVX(40)))) 3401080
    GO TO 175 3401090
152 CONTINUE 3401100
    SAVX(48) = SAVX(7)-(XNUPT*SAVX(6)+(XK11-XNUPT**2*XK22)*((X1CS/S)* 3401110
1     (SAVX(1)*CS-SAVX(3)*SN)+X1*SAVX(9)**2*0.5)+XNUPT* 3401120
2     SAVX(43)-SAVX(44)+X2*(XNUPT*SAVX(38)-SAVX(37))) 3401130
    SAVX(49) = SAVX(20)-(XNUPT*SAVX(18)-(1.0/S)*X1CS*(XD11-XNUPT**2* 3401140
1     XD22)*SAVX(5)*CS-SAVX(46)+XNUPT*SAVX(45)+X2*(XNUPT* 3401150
2     SAVX(41)-SAVX(40))) 3401160
    SAVX(50) = SAVX(21)-((-1.0/((S*CS/XD33)+(SN*TN/(XK33*S))))*(- 3401170
1     SAVX(19)*SN/S+SAVX(16)*SN/XK33+X2*(SAVX(39)*SN/XK33- 3401180
2     SAVX(42)*S*CS/XD33)+SN*X1*SAVX(9)*SAVX(5))) 3401190
    SAVX(51) = SAVX(4)-((1.0/S)*(SAVX(19)+SAVX(21)*TN/XK33)+SAVX(16)/ 3401200

```

```

1          XK33+X2*SAVX(39)/XK33+X1*SAVX(9)*SAVX(5)          3401210
SAVX(52) = SAVX(2)-((1.0/(XK22-XNUTP**2*XK11))*(SAVX(6)-XNUTP* 3401220
1          SAVX(7)+SAVX(43)-XNUTP*SAVX(44)+X2*(SAVX(38)-XNUTP* 3401230
2          SAVX(37)))-X1*SAVX(5)*SAVX(5)*0.5)                3401240
SAVX(53) = SAVX(47)-((1.0/(XD22-XNUTP**2*XD11))*(-SAVX(18)+XNUTP* 3401250
1          SAVX(20)-SAVX(45)+XNUTP*SAVX(46)-X2*(SAVX(41)-XNUTP* 3401260
2          SAVX(40))))                                          3401270
GO TO 175                                                    3401280
153 CONTINUE                                                3401290
SAVX(48) = SAVX(7)-(XNUPT*SAVX(6)+(XK11-XNUTP**2*XK22)*(-X1RO* 3401300
1          SAVX(3)+X1*SAVX(9)**2*0.5)+XNUTP*SAVX(43)-SAVX(44)+ 3401310
2          X2*(XNUPT*SAVX(38)-SAVX(37)))                      3401320
SAVX(49) = SAVX(20)-(XNUPT*SAVX(18)+(XNUPT*SAVX(45)-SAVX(46))+ 3401330
1          X2*(XNUPT*SAVX(41)-SAVX(40)))                      3401340
SAVX(50) = SAVX(21)-((-1.0/(RO/XD33)+(X1RO/XK33)))*(SAVX(16)/XK33 3401350
1          +X2*(SAVX(39)/XK33-SAVX(42)*RO/XD33)+X1*SAVX(9)*SAVX(5) 3401360
2          ))                                                  3401370
SAVX(51) = SAVX(4)-(SAVX(16)/XK33+X2*SAVX(39)/XK33+SAVX(21)*X1RO/ 3401380
1          XK33+X1*SAVX(9)*SAVX(5))                          3401390
SAVX(52) = SAVX(2)-((1.0/(XK22-XNUTP**2*XK11))*(SAVX(6)-XNUTP* 3401400
1          SAVX(7)+(SAVX(43)-XNUTP*SAVX(44))+X2*(SAVX(38)-XNUTP* 3401410
2          SAVX(37)))-X1*SAVX(5)*SAVX(5)*0.5)                3401420
SAVX(53) = SAVX(47)-((1.0/(XD22-XNUTP**2*XD11))*(-SAVX(18)+XNUTP* 3401430
1          SAVX(20)+(XNUTP*SAVX(46)-SAVX(45))-X2*(SAVX(41)-XNUTP* 3401440
2          SAVX(40))))                                          3401450
GO TO 175                                                    3401460
7776 IF (ISTTAB.GE.3.AND.ISTTAB.LE.9) GO TO 7777          3401470
GO TO (161,162,163),IGEOM                                3401480
161 CONTINUE                                                3401490
SAVX(48) = SAVX(7)-(XK12*(1.0/(XK22+XC22**2/XD22)))*(SAVX(6)+ 3401500
1          SAVX(43)+X2*SAVX(38)+XC22/XD22*(SAVX(18)+SAVX(45)+X2* 3401510
2          SAVX(41))-SAVX(44)-X2*SAVX(37)+(X1RO*XK11-XK12*XK21* 3401520
3          X1RO*(1.0/(XK22+XC22**2/XD22)))*(SAVX(5)*CS-SAVX(3)*SN+ 3401530
4          X1*RO*SAVX(9)**2*0.5)-(XC11+XK12*XC22*XD21/XD22*(1.0/ 3401540
5          (XK22+XC22**2/XD22)))*SAVX(5)*CS*X1RO)            3401550
SAVX(49) = SAVX(20)-(-XD12*(XC22/(XC22**2+XK22*XD22))*(SAVX(6)+ 3401560
1          SAVX(43)+X2*SAVX(38))-SAVX(46)-X2*SAVX(40)+XD12*(XK22/ 3401570
2          (XC22**2+XK22*XD22))*(SAVX(18)+SAVX(45)+X2*SAVX(41))+ 3401580
3          (XC11*X1RO+XD12*XK21*X1RO*(XC22/(XC22**2+XK22*XD22)))* 3401590
4          (SAVX(1)*CS-SAVX(3)*SN+X1*RO*SAVX(9)**2*0.5)+(XD11- 3401600
5          XD12*XK22*XD21/(XC22**2+XK22*XD22))*SAVX(5)*CS*X1RO) 3401610
SAVX(50) = SAVX(21)-((-1.0/(RO/XD33)+(SNSQ*X1RO/XK33))*(SAVX(19) 3401620
1          *(CS1R1-CN1RO)+SAVX(16)*SN/XK33+X2*(SAVX(39)*SN/XK33- 3401630
2          SAVX(42)*RO/XD33)+SN*X1*SAVX(9)*SAVX(5)))          3401640
SAVX(51) = SAVX(4)-(R1*(SAVX(19)*CS1RO+SAVX(16)/XK33+X2*SAVX(39)/ 3401650
1          XK33+SAVX(21)*SN1RO/XK33)+R1*X1*SAVX(9)*SAVX(5)) 3401660
SAVX(52) = SAVX(2)-(R1*(SAVX(3)*X1R1-X1*SAVX(5)**2*0.5+(1.0/(XK22 3401670
1          +XC22**2/XD22))*(SAVX(6)+SAVX(43)+X2*SAVX(38)+(XC22/ 3401680
2          XD22)*(SAVX(18)+SAVX(45)+X2*SAVX(41))-XK21*X1RO* 3401690
3          (SAVX(1)*CS-SAVX(3)*SN)-X1*XK12*SAVX(9)**2*0.5-(XC22* 3401700
4          XD21/XD22)*SAVX(5)*CS*X1RO)))                      3401710
SAVX(53) = SAVX(47)-(R1*(-XC22/(XC22**2+XK22*XD22))*(SAVX(6)+ 3401720
1          SAVX(43)+X2*SAVX(38)-(XK21/RO)*(SAVX(1)*CS-SAVX(3)*SN)- 3401730
2          X1*XK12*SAVX(9)**2*0.5)+(XK22/(XC22**2+XK22*XD22))* 3401740
3          (SAVX(18)+SAVX(45)+X2*SAVX(41))-(XK22*XD21/(XC22**2+ 3401750
4          XK22*XD22))*SAVX(5)*CS*X1RO))                      3401760
GO TO 175                                                    3401770
162 CONTINUE                                                3401780
SAVX(48) = SAVX(7)-(XK12*(1.0/(XK22+XC22**2/XD22)))*(SAVX(6)+ 3401790
1          SAVX(43)+X2*SAVX(38)+(XC22/XD22)*(SAVX(18)+SAVX(45)+ 3401800
2          X2*SAVX(41))-SAVX(44)-X2*SAVX(37)+(1.0/(CS*S))*(XK11- 3401810

```

```

3          XK12*XK21*(1.0/(XK22+XC22**2/XD22)))*(SAVX(1)*CS-      3401820
4          SAVX(3)*SN+X1*S*CS*SAVX(9)**2*0.5)-(XC11+(XK12*XD21*      3401830
5          XC22/XD22)*(1.0/(XK22+XC22**2/XD22)))*SAVX(5)/S)      3401840
SAVX(49) = SAVX(20)-(-XD12*(XC22/(XC22**2+XK22*XD22)))*(SAVX(6)+      3401850
1          SAVX(43)+X2*SAVX(38))-SAVX(46)-X2*SAVX(40)+XD12*(XK22/      3401860
2          (XC22**2+XK22*XD22))*(SAVX(18)+SAVX(45)+X2*SAVX(41))+      3401870
3          (XC11/(S*CS)+XD12*XK21/(S*CS))*(XC22/(XC22**2+XK22*      3401880
4          XD22))*(SAVX(1)*CS-SAVX(3)*SN+X1*S*CS*SAVX(9)**2*0.5)      3401890
5          +(XD11-XD12*XK22*XD21/(XC22**2+XK22*XD22))*SAVX(5)/S)      3401900
SAVX(50) = SAVX(21)-((-1.0/((S*CS/XD33)+(SN*TN/(XK33*S))))*(-      3401910
1          SAVX(19)*SN/S+SAVX(16)*SN/XK33+X2*(SAVX(39)*SN/XK33-      3401920
2          SAVX(42)*S*CS/XD33)+SN*X1*SAVX(9)*SAVX(5)))      3401930
SAVX(51) = SAVX(4)-((1.0/S)*(SAVX(19)+SAVX(21)*TN/XK33)+SAVX(16)/      3401940
1          XK33+X2*SAVX(39)/XK33+X1*SAVX(9)*SAVX(5))      3401950
SAVX(52) = SAVX(2)-(-X1*SAVX(5)**2*0.5+(1.0/(XK22+XC22**2/XD22))*      3401960
1          (SAVX(6)+SAVX(43)+X2*SAVX(38)+(XC22/XD22)*(SAVX(18)+      3401970
2          SAVX(45)+X2*SAVX(41))-(XK21/(S*CS))*(SAVX(1)*CS-SAVX(3)      3401980
3          *SN)-X1*XK12*SAVX(9)**2*0.5-(XC22*XD21/XD22)*SAVX(5)/      3401990
4          S))      3402000
SAVX(53) = SAVX(47)-(-(XC22/(XC22**2+XK22*XD22))*(SAVX(6)+SAVX(43)      3402010
1          +X2*SAVX(38)-XK21*(SAVX(1)*CS-SAVX(3)*SN)/(S*CS)-X1*      3402020
2          XK12*SAVX(9)**2*0.5)+(XK22/(XC22**2+XK22*XD22))*      3402030
3          (SAVX(18)+SAVX(45)+X2*SAVX(41))-(XK22*XD21/(XC22**2+      3402040
4          XK22*XD22))*SAVX(5)/S)      3402050
GO TO 175      3402060
163 CONTINUE      3402070
SAVX(48) = SAVX(7)-(XK12*(1.0/(XK22+XC22**2/XD22))*(SAVX(6)+      3402080
1          SAVX(43)+X2*SAVX(38)+(XC22/XD22)*SAVX(18)+SAVX(45)+X2*      3402090
2          SAVX(41))-SAVX(44)-X2*SAVX(37)+(X1RO*(XK11-XK12*XK21*      3402100
3          (1.0/(XK22+XC22**2/XD22))))*(-SAVX(3)+X1*RO*SAVX(9)*      3402110
4          SAVX(9)*0.5))      3402120
SAVX(49) = SAVX(20)-(-XD12*(XC22/(XC22**2+XK22*XD22)))*(SAVX(6)+      3402130
1          SAVX(43)+X2*SAVX(38))-SAVX(46)-X2*SAVX(40)+XD12*(XK22/      3402140
2          (XC22**2+XK22*XD22))*(SAVX(18)+SAVX(45)+X2*SAVX(41))+      3402150
3          (XC11*X1RO+XD12*XK21*X1RO*(XC22/(XC22**2+XK22*XD22)))*      3402160
4          (-SAVX(3)+X1*RO*SAVX(9)*SAVX(9)*0.5))      3402170
SAVX(50) = SAVX(21)-((-1.0/((RO/XD33)+(X1RO/XK33)))*(SAVX(16)/XK33      3402180
1          +X2*(SAVX(39)/XK33-SAVX(42)*RO/XD33)+X1*SAVX(9)*SAVX(5)      3402190
2          ))      3402200
SAVX(51) = SAVX(4)-(SAVX(16)/XK33+X2*SAVX(39)/XK33+SAVX(21)*X1RO/      3402210
1          XK33+X1*SAVX(9)*SAVX(5))      3402220
SAVX(52) = SAVX(2)-(-X1*SAVX(5)**2*0.5+(1.0/(XK22+XC22**2/XD22))*      3402230
1          (SAVX(6)+SAVX(43)+X2*SAVX(38)+(XC22/XD22)*(SAVX(18)+      3402240
2          SAVX(45)+X2*SAVX(41))-(XK21*X1RO)*(-SAVX(3))-X1*XK12*      3402250
3          SAVX(9)*SAVX(9)*0.5))      3402260
SAVX(53) = SAVX(47)-(-(XC22/(XC22**2+XK22*XD22))*(SAVX(6)+SAVX(43)      3402270
1          +X2*SAVX(38)-XK21*X1RO*(-SAVX(3))-X1*XK12*SAVX(9)*      3402280
2          SAVX(9)*0.5)+(XK22/(XC22**2+XK22*XD22))*(SAVX(18)+      3402290
3          SAVX(45)+X2*SAVX(41)))      3402300
GO TO 175      3402310
7777 GO TO (171,172,173),IGEOM      3402320
171 CONTINUE      3402330
SAVX(48) = SAVX(7)-((SAVX(6)+SAVX(43)+X2*SAVX(38))*(XC15*XC22+XD22      3402340
1          *XK12)/(XK22*XD22+XC22**2)-SAVX(44)-X2*SAVX(37)+(XK12*      3402350
2          XC22-XK22*XC15)*(SAVX(18)+SAVX(45)+X2*SAVX(41))/(XC22      3402360
3          *XC22+XK22*XD22)+(X1RO*(SAVX(1)*CS-SAVX(3)*SN)+X1*      3402370
4          SAVX(9)**2*0.5)*(XK11+(XC15*(XC15*XK22-2.0*XK12*XC22)-      3402380
5          XK12*XK12*XD22)/(XK22*XD22+XC22*XC22))+X1RO*SAVX(5)*CS*      3402390
6          (-XC11+(XC15*XC15*XC22+XC15*(XK12*XD22+XK22*XD12)-XK12      3402400
7          *XD12*XC22)/(XK22*XD22+XC22*XC22)))      3402410
SAVX(49) = SAVX(20)-((SAVX(18)+SAVX(45)+X2*SAVX(41))*(XC15*XC22+      3402420

```



```

1      XK22*XD12)/(XK22*XD22+XC22*XC22)+(SAVX(6)+SAVX(43)+X2* 3402430
2      SAVX(38))*(XD22*XC15-XD12*XC22)/(XD22*XK22+XC22*XC22)- 3402440
3      SAVX(46)-X2*SAVX(40)+X1RO*SAVX(5)*CS*(XD11-(XD12*XD12* 3402450
4      XK22+XC15*(2.0*XC22*XD12-XC15*XD22))/(XC22*XC22+XK22* 3402460
5      XD22)+(X1RO*(SAVX(1)*CS-SAVX(3)*SN)+X1*SAVX(9)* 3402470
6      SAVX(9)*0.5)*(XC11+(XD12*XC22*XK12-XC15*(XC15*XC22+ 3402480
7      XD12*XK22+XD22*XK12)))/(XC22*XC22+XK22*XD22))) 3402490
SAVX(50) = SAVX(21)-((1.0/(XC16*SN*X1RO-XK33-SN*X1RO*(XD33*SN/RO- 3402500
1      XC16)))*((XK33*XD33-XC16*XC16)*X1RO*SAVX(19)+(CS*X1R1- 3402510
2      CN1RO)+X1*SN*SAVX(9)*SAVX(5)+(SAVX(16)+X2*SAVX(39))* 3402520
3      (XD33*SN*X1RO-XC16)+X2*SAVX(42)*(XK33-XC16*SN/RO))) 3402530
SAVX(51) = SAVX(4)-(R1*(SAVX(19)*CS*X1RO+X1*SAVX(9)*SAVX(5)+(1.0/ 3402540
1      (XK33-XC16*XC16/XD33))*((SAVX(16)+SAVX(21))*(SN*X1RO-XC16 3402550
2      /XD33)+X2*(SAVX(39)-XC16*SAVX(42)/XD33))) 3402560
SAVX(52) = SAVX(2)-(SAVX(3)-R1*X1*SAVX(5)*SAVX(5)+0.5+R1*(XD22* 3402570
1      (SAVX(6)+SAVX(43)+X2*SAVX(38))+XC22*(SAVX(18)+SAVX(45)+ 3402580
2      X2*SAVX(41)-(X1RO*(SAVX(1)*CS-SAVX(3)*SN)+X1*SAVX(9)* 3402590
3      SAVX(9)*0.5)*(XK12*XD22+XC15*XC22)-X1RO*SAVX(5)*CS* 3402600
4      (XC22*XD12-XC15*XD22))/(XK22*XD22+XC22*XC22)) 3402610
SAVX(53) = SAVX(47)-(R1*(XK22*(SAVX(18)+SAVX(45)+X2*SAVX(41))-XC22 3402620
1      *(SAVX(6)+SAVX(43)+X2*SAVX(38))+(X1RO*(SAVX(1)*CS- 3402630
2      SAVX(3)*SN)+X1*SAVX(9))*2*0.5)*(XK12*XC22-XK22*XC15)- 3402640
3      X1RO*SAVX(5)*CS*(XC15*XC22+XK22*XD12))/(XC22**2+XK22* 3402650
4      XD22)) 3402660
GO TO 175 3402670
172 CONTINUE 3402680
SAVX(48) = SAVX(7)-((SAVX(6)+SAVX(43)+X2*SAVX(38))*(XC15*XC22+XD22 3402690
1      *XK12)/(XK22*XD22+XC22**2)-SAVX(44)-X2*SAVX(37)+(XK12* 3402700
2      XC22-XK22*XC15)*(SAVX(18)+SAVX(45)+X2*SAVX(41))/(XC22* 3402710
3      XC22+XK22*XD22)+(SAVX(1)*CS-SAVX(3)*SN)/(S*CS)+X1* 3402720
4      SAVX(9)**2*0.5)*(XK11+(XC15*(XC15*XK22-2.0*XK12*XC22)- 3402730
5      XK12*XK12*XD22)/(XK22*XD22+XC22*XC22))+SAVX(5)/S*(-XC11 3402740
6      +(XC15*XC15*XC22+XC15*(XK12*XD22+XK22*XD12)-XK12*XD12* 3402750
7      XC22)/(XC22*XC22+XK22*XC22))) 3402760
SAVX(49) = SAVX(20)-((SAVX(18)+SAVX(45)+X2*SAVX(41))*(XC15*XC22+ 3402770
1      XK22*XD12)/(XK22*XD22+XC22*XC22)+(SAVX(6)+SAVX(43)+X2* 3402780
2      SAVX(38))*(XD22*XC15-XD12*XC22)/(XD22*XK22+XC22*XC22)- 3402790
3      SAVX(46)-X2*SAVX(40)+SAVX(5)/S*(XD11-(XD12*XD12*XK22+ 3402800
4      XC15*(2.0*XC22*XD12-XC15*XD22))/(XC22*XC22+XK22*XD22))+ 3402810
5      (1.0/(S*CS))*(SAVX(1)*CS-SAVX(3)*SN)+X1*SAVX(9)**2*0.5) 3402820
6      *(XC11+(XD12*XC22*XK12-XC15*(XC15*XC22+XD12*XK22+XD22* 3402830
7      XK12))/(XC22*XC22+XK22*XC22))) 3402840
SAVX(50) = SAVX(21)-(1.0/(XC16*TN/S-XK33-(TN/S)*(XD33*TN/S-XC16))* 3402850
1      ((XK33*XD33-XC16*XC16)*(1.0/(S*CS))*(-SAVX(19)*SN/S)+ 3402860
2      X1*SN*SAVX(9)*SAVX(5)+(SAVX(16)+X2*SAVX(39))*(XD33*TN/S 3402870
3      -XC16)+X2*SAVX(42)*(XK33-XC16*TN/S))) 3402880
SAVX(51) = SAVX(4)-(SAVX(19)/S+X1*SAVX(9)*SAVX(5)+(1.0/(XK33-XC16* 3402890
1      XC16/XD33))*(SAVX(16)+SAVX(21))*(TN/S-XC16/XD33)+X2* 3402900
2      (SAVX(39)-XC16*SAVX(42)/XD33))) 3402910
SAVX(52) = SAVX(2)-(-X1*SAVX(5)**2*0.5+(XD22*(SAVX(6)+SAVX(43)+ 3402920
1      X2*SAVX(38))+XC22*(SAVX(18)+SAVX(45)+X2*SAVX(41))-(XK12 3402930
2      *XD22+XC15*XC22)*((1.0/(S*CS))*(SAVX(1)*CS-SAVX(3)*SN))+ 3402940
3      X1*SAVX(9)**2*0.5)-(XC22*XD12-XC15*XD22)*SAVX(5)/S/ 3402950
4      (XK22*XD22+XC22*XC22)) 3402960
SAVX(53) = SAVX(47)-((XK22*(SAVX(18)+SAVX(45)+X2*SAVX(41))-XC22* 3402970
1      (SAVX(6)+SAVX(43)+X2*SAVX(38))+(XK12*XC22-XK22*XC15)* 3402980
2      ((1.0/(S*CS))*(SAVX(1)*CS-SAVX(3)*SN))+X1*SAVX(9)* 3402990
3      SAVX(9)*0.5)-(XC15*XC22+XK22*XD12)*SAVX(5)/S)/(XK22* 3403000
4      XD22+XC22*XC22)) 3403010
GO TO 175 3403020
173 CONTINUE 3403030

```

```

SAVX(48) = SAVX(7)-((SAVX(6)+SAVX(43)+X2*SAVX(38))*(XC15*XC22+XD22 3403040
1 *XK12)/(XK22*XD22+XC22*XC22)-SAVX(44)-X2*SAVX(37)+(XK12 3403050
2 *XC22-XK22*XC15)*(SAVX(18)+SAVX(45)+X2*SAVX(41))/(XC22* 3403060
3 XC22+XK22*XD22)+(X1RO*(-SAVX(3))+X1*SAVX(9)**2*0.5)* 3403070
4 (XK11+(XC15*(XC15*XK22-2.0*XK12*XC22)-XK12*XK12*XD22)/ 3403080
5 (XK22*XD22+XC22*XC22))) 3403090
SAVX(49) = SAVX(20)-((SAVX(18)+SAVX(45)+X2*SAVX(41))*(XC15*XC22+ 3403100
1 XK22*XD12)/(XK22*XD22+XC22*XC22)+(SAVX(6)+SAVX(43)+X2* 3403110
2 SAVX(38))*(XD22*XC15-XD12*XC22)/(XD22*XK22+XC22*XC22)- 3403120
3 SAVX(46)-X2*SAVX(40)+(X1RO*(-SAVX(3))+X1*SAVX(9))* 3403130
4 SAVX(9)*0.5)*(XC11+(XD12*XC22*XK12-XC15*(XC15*XC22+ 3403140
5 XD12*XK22+XD22*XK12))/(XC22*XC22+XK22*XD22))) 3403150
SAVX(50) = SAVX(21)-((1.0/(XC16*X1RO-XK33-X1RO*(XD33*X1RO-XC16)))* 3403160
1 (X1*SAVX(9)*SAVX(5)+(SAVX(16)+X2*SAVX(39))*(XD33*X1RO- 3403170
2 XC16)+X2*SAVX(15)*(XK33-XC16/RO))) 3403180
SAVX(51) = SAVX(4)-(X1*SAVX(9)*SAVX(5)+(1.0/(XK33-XC16/XD33)) 3403190
1 *(SAVX(16)+SAVX(21)*(X1RO-XC16/XD33))+X2*(SAVX(39)-XC16* 3403200
2 SAVX(42)/XD33))) 3403210
SAVX(52) = SAVX(2)-(-X1*SAVX(5)**2*0.5+(XD22*(SAVX(6)+SAVX(43)+X2 3403220
1 *SAVX(38))+XC22*(SAVX(18)+SAVX(45)+X2*SAVX(41))-(X1RO* 3403230
2 (-SAVX(3))+X1*SAVX(9)**2*0.5)*(XK12*XD22+XC15*XC22))/ 3403240
3 (XK22*XD22+XC22*XC22)) 3403250
SAVX(53) = SAVX(47)-((XK22*(SAVX(18)+SAVX(45)+X2*SAVX(41))-XC22* 3403260
1 (SAVX(6)+SAVX(43)+X2*SAVX(38)))+(X1RO*(-SAVX(3))+X1* 3403270
2 SAVX(9)**2*0.5)*(XK12*XC22-XK22*XC15))/(XC22*XC22+XK22 3403280
3 *XD22)) 3403290
175 CONTINUE 3403300
RETURN 3403310
END 3403320

```

```

FOR, IS ARRAYS, ARRAYS
SUBROUTINE ARRAYS (A, B, C, D, E, F, G, H, O, PHI) 4200010
COMMON /GRAFIX/ X(100), Y(100, 9), NGRAPH, LDEF(9), NGR, JCYC, NFLAG, JAM, 4200020
C JNSC 4200030
DIMENSION Z(9) 4200040
Z(1) = A 4200050
Z(2) = B 4200060
Z(3) = C 4200070
Z(4) = D 4200080
Z(5) = E 4200090
Z(6) = F 4200100
Z(7) = G 4200110
Z(8) = H 4200120
Z(9) = O 4200130
INDEX = 0 4200140
JCYC = JCYC+1 4200150
DO 100 J=1,9 4200160
IF (LDEF(J).EQ.0) GO TO 100 4200170
INDEX = INDEX+1 4200180
Y(JCYC, INDEX) = Z(J) 4200190
100 CONTINUE 4200200
X(JCYC) = PHI 4200210
RETURN 4200220
END 4200230

```

## SUBROUTINE ETRAP

This is an error trap subroutine which can be called by the MAIN routine at various stages of program execution. If the indicator NIX is not equal to zero, MAIN will call ETRAP and indicate the proper error message to be printed.

```

FOR,IS ETRAP,ETRAP
SUBROUTINE ETRAP
INTEGER SAVJTC,SAVSTP,Q,THICK
INTEGER XN
COMMON STORY(16),XMAT(270,10),STD(10),SADUS(30),RADUS(30)
COMMON TADUS(30),UADUS(30),SAVTIC(900)
COMMON XN,TEFREE,TIC,PHI,STOP,RESTOP,RTICK,G1,XNL(3),NH
COMMON NST(30),NKL(30),NXMAT(20),SAVJTC(30),SAVSTP(30),JRTIC(30)
COMMON JRSTOP(30),NREG,NMPT,NRC,NSC,NIX,IERROR,KGEOM,IGEOM,ISTTAB
COMMON KELVIN,IBEGIN,NPROB,NSEG,NERROR,Q,THICK,NOJS,NLINKS,NLCASE
COMMON NTSKL,NZ,NBCT,LINPUT,NTRKL,NPASS,XN1,KBC,NRINGS
COMMON LODE,ICYCLE,LDISTL
WRITE(6,1726)
1726 FORMAT(1H1)
GO TO (8000,8036,8086,8087,8089,8090,8013,8009,8031,8008,8001,
1 8002,8003,8006,8007,8067,8101,8102,8103,8104,8105,8106,
2 8107,8108,8109,8110,8088,110,8120,8841,8842,8777,8797,
3 8787),NERROR
8000 WRITE(6,1)
1 FORMAT(/ 4X,'ONE OF THE MATERIAL PROPERTY TABLES CANNOT BE IDENTI
1FIED AS ISOT, ORTH, OR STIF. '//)
GO TO 505
8036 WRITE(6,2)
2 FORMAT(/ 4X,'A MATERIAL PROPERTY TABLE NAME FOR A SEGMENT CANNOT
1BE FOUND IN THE TABLE LIST. '//)
GO TO 505
8086 WRITE(6,3)
3 FORMAT(/ 4X,'THE TYPE OF GEOMETRY OF A SEGMENT CANNOT BE IDENTIFI
1ED AS ONE HANDLED BY THE PROGRAM. '//)
GO TO 505
8087 WRITE(6,4)
4 FORMAT(/ 4X,'THE TYPE OF MATERIAL PROPERTY TABLE FOR A SEGMENT CA
1NNOT BE IDENTIFIED AS ISOT, ORTH, OR STIF. '//)
GO TO 505
8089 WRITE(6,5)
5 FORMAT(/ 4X,'THE WALL CONSTRUCTION OF A SEGMENT CANNOT BE IDENTIF
1IED AS SING, EQUA, UNEQ, OR BLAN. '//)
GO TO 505
8090 WRITE(6,6)
6 FORMAT(/ 4X,'THE TYPE OF TEMPERATURE INPUT FOR A SEGMENT CANNOT B
1E IDENTIFIED AS THST, NOTH, THCN, OR THIN. '//)
8013 WRITE(6,7)
7 FORMAT(/ 4X,'THE PROGRAM CANNOT RECOGNIZE THE HARDENING CLUF AS B
1EING EITHER ISOT, KINE OR PERF. '//)
8009 GO TO 505
8031 WRITE(6,9)
9 FORMAT(/ 4X,'THE LOAD INDICATOR CLUES CAN ONLY BE ZERO, BLANK, ON
1E, OR FOUR. '//)
GO TO 505
8008 WRITE(6,10)
10 FORMAT(/ 4X,'THE COMBINATION OF AN ORTHOTROPIC MATERIAL AND THE I
1SOTROPIC HARDENING RULE IS NOT PRESENTLY ALLOWED. '//)
GO TO 505
8001 WRITE(6,11)
11 FORMAT(/ 4X,'THE MAGIC CYCLE HAS GONE PAST STOP BY MORE THAN THE
1PERMITTED VALUE. CHECK TO SEE IF FIXED STEP SIZE IS TOO LARGE. '//)
GO TO 505
8002 WRITE(6,12)
12 FORMAT(/ 4X,'THE RIEMAN VARIABLE, IEND, WHICH SIGNALS THE END OF
1A SEGMENT SHOULD ONLY BE ZERO OR NEGATIVE ONE. '//)

```

8003	GO TO 505	4000600
8006	GO TO 505	4000610
8007	WRITE(6,15)	4000620
15	FORMAT(/ 4X,'THE INTERPOLATED VALUE OF TEMPERATURE FOR THE MATERIAL PROPERTY TABLE IS LESS THAN THE SECOND TEMPERATURE VALUE.')	4000630
	GO TO 505	4000640
8067	WRITE(6,16)	4000650
16	FORMAT(/ 4X,'THE INTERPOLATED VALUE OF TEMPERATURE FOR THE MATERIAL PROPERTY TABLE IS GREATER THAN THE LAST VALUE OF TEMPERATURE.')	4000660
	2/)	4000670
	GO TO 505	4000680
8101	WRITE(6,17)	4000690
17	FORMAT(/ 4X,'THE K11 STIFFNESS PARAMETER IS ZERO.')	4000700
	GO TO 505	4000710
8102	WRITE(6,18)	4000720
18	FORMAT(/ 4X,'THE K12 STIFFNESS PARAMETER IS ZERO.')	4000730
	GO TO 505	4000740
8103	WRITE(6,19)	4000750
19	FORMAT(/ 4X,'THE K21 STIFFNESS PARAMETER IS ZERO.')	4000760
	GO TO 505	4000770
8104	WRITE(6,20)	4000780
20	FORMAT(/ 4X,'THE K22 STIFFNESS PARAMETER IS ZERO.')	4000790
	GO TO 505	4000800
8105	WRITE(6,21)	4000810
21	FORMAT(/ 4X,'THE K33 STIFFNESS PARAMETER IS ZERO.')	4000820
	GO TO 505	4000830
8106	WRITE(6,22)	4000840
22	FORMAT(/ 4X,'THE D11 STIFFNESS PARAMETER IS ZERO.')	4000850
	GO TO 505	4000860
8107	WRITE(6,23)	4000870
23	FORMAT(/ 4X,'THE D12 STIFFNESS PARAMETER IS ZERO.')	4000880
	GO TO 505	4000890
8108	WRITE(6,24)	4000900
24	FORMAT(/ 4X,'THE D21 STIFFNESS PARAMETER IS ZERO.')	4000910
	GO TO 505	4000920
8109	WRITE(6,25)	4000930
25	FORMAT(/ 4X,'THE D22 STIFFNESS PARAMETER IS ZERO.')	4000940
	GO TO 505	4000950
8110	WRITE(6,26)	4000960
26	FORMAT(/ 4X,'THE D33 STIFFNESS PARAMETER IS ZERO.')	4000970
	GO TO 505	4000980
8088	WRITE(6,27)	4000990
27	FORMAT(/ 4X,'THE PROGRAM CANNOT DETERMINE WHETHER THE PROBLEM INPUT IS THIC, RWA1, RWA2, RWA3, ST10, ST11, ST12, ST13, ISG1, 2ISG2, OR ISG3.')	4001000
110	GO TO 505	4001010
8120	WRITE(6,29)	4001020
29	FORMAT(/ 4X,'THE Y2 BLOCK IN THE SEGMENT MAGIC OUTPUT IS SINGULAR 1.')	4001030
	GO TO 505	4001040
8841	WRITE(6,30)	4001050
30	FORMAT(/ 4X,'IN THE COMPUTATION OF THE REGION STIFFNESSES, THE K212 MATRIX WAS NOT POSITIVE DEFINITE.')	4001060
	GO TO 505	4001070
8842	WRITE(6,31)	4001080
31	FORMAT(/ 4X,'IN THE COMPUTATION OF THE REGION LOADS, THE K22 MATRIX WAS NOT POSITIVE DEFINITE.')	4001090
	GO TO 505	4001100
8777	WRITE(6,32)	4001110
32	FORMAT(/ 4X,'IN THE COMPUTATION OF THE REDUCED FLEXIBILITY MATRIX 1, THE REDUCED STIFFNESS MATRIX IS SINGULAR.')	4001120
		4001130
		4001140
		4001150
		4001160
		4001170
		4001180
		4001190
		4001200

GO TO 505,	4001210
8797 WRITE(6,33)	4001220
33 FORMAT(/ 4X, 'FOR KINEMATIC LINKS BETWEEN SEGMENTS, THE DEPENDENT	4001230
1JOINT NUMBER MUST BE GREATER THAN THE INDEPENDENT JOINT NUMBER.'/)	4001240
GO TO 505	4001250
8787 WRITE(6,34)	4001260
34 FORMAT(/ 4X, 'THE NUMBER OF POINTS IN THE ST TABLE MUST BE BETWEEN	4001270
1 2 AND 30.'/)	4001280
505 RETURN	4001290
END	4001300

## REFERENCES

1. Svalbonas, V., "Numerical Analysis of Stiffened Shells of Revolution-Vol. I: Theory", NASA CR-2273, September 1973.
2. Svalbonas, V., and Levine, H., "Numerical Nonlinear Inelastic Analysis of Stiffened Shells of Revolution-Vol. I: Theory", NASA CR-2559





709 001 C1 U D 750711 S00903DS  
DEPT OF THE AIR FORCE  
AF WEAPONS LABORATORY  
ATTN: TECHNICAL LIBRARY (SUL)  
KIRTLAND AFB NM 87117

POSTMASTER: If Undeliverable (Section 158  
Postal Manual) Do Not Return

*"The aeronautical and space activities of the United States shall be conducted so as to contribute . . . to the expansion of human knowledge of phenomena in the atmosphere and space. The Administration shall provide for the widest practicable and appropriate dissemination of information concerning its activities and the results thereof."*

—NATIONAL AERONAUTICS AND SPACE ACT OF 1958

## NASA SCIENTIFIC AND TECHNICAL PUBLICATIONS

**TECHNICAL REPORTS:** Scientific and technical information considered important, complete, and a lasting contribution to existing knowledge.

**TECHNICAL NOTES:** Information less broad in scope but nevertheless of importance as a contribution to existing knowledge.

**TECHNICAL MEMORANDUMS:** Information receiving limited distribution because of preliminary data, security classification, or other reasons. Also includes conference proceedings with either limited or unlimited distribution.

**CONTRACTOR REPORTS:** Scientific and technical information generated under a NASA contract or grant and considered an important contribution to existing knowledge.

**TECHNICAL TRANSLATIONS:** Information published in a foreign language considered to merit NASA distribution in English.

**SPECIAL PUBLICATIONS:** Information derived from or of value to NASA activities. Publications include final reports of major projects, monographs, data compilations, handbooks, sourcebooks, and special bibliographies.

**TECHNOLOGY UTILIZATION PUBLICATIONS:** Information on technology used by NASA that may be of particular interest in commercial and other non-aerospace applications. Publications include Tech Briefs, Technology Utilization Reports and Technology Surveys.

Details on the availability of these publications may be obtained from:

**SCIENTIFIC AND TECHNICAL INFORMATION OFFICE**

**NATIONAL AERONAUTICS AND SPACE ADMINISTRATION**

Washington, D.C. 20546