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TESTS OF GULTON INDUSTRIES, FD, 9.0 AMPERE-HOUR NICKEL-CADMIUM CELLS WITH (Naval Weapons Support 63)

INCOF

# EVALUATION PROGRAM for

## SECONDARY SPACECRAFT CELLS

INITIAL EVALUATION TESTS

OF

GULTON INDUSTRIES, INC.

9.0 AMPERE-HOUR NICKEL-CADMIUM SPACECRAFT CELLS

WITH AUXILIARY ELECTRODES

FOR THE

SMALL ASTRONOMY SATELLITE (SAS-C)

prepared for GODDARD SPACE FLIGHT CENTER

CONTRACT S-53742AG

WEAPONS QUALITY ENGINEERING CENTER

NAVAL WEAPONS SUPPORT CENTER, CRANE, INDIANA

# DEFARTMENT OF THE NAVY NAVAL WEAPONS SUPPORT CENTER CHARE, INDIANA 47922

3053-JDH:jsf

2 9 JUL 1975

From: Commanding Officer, Naval Weapons Support Center, Crane, Indiana To: National Aeronautics and Space Administration, Goddard Space

Flight Center (711.2), Greenbelt, MD 20771

Subj: Report WQEC/C 75-165; Evaluation program for secondary spacecraft cells; initial evaluation tests of 9.0 ampere-hour nickel-cadmium spacecraft cells with auxiliary electrodes for the Small Astronomy Satellite (SAS-C) manufactured by Gulton Industries, Inc.

Ref: (a) NASA Purchase Order S-53742AG

Encl: (1) Report WQEC/C 75-165

1. In compliance with reference (a), enclosure (1) is forwarded for information and retention.

D. G. MILEY
By direction

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# DEPARTMENT OF THE NAVY NAVAL WEAPONS SUPPORT CENTER WEAPONS QUALITY ENGINEERING CENTER CRANE, INDIANA 47522

EVALUATION PROGRAM
FOR
SECONDARY SPACECRAFT CELLS

INITIAL EVALUATION TESTS
OF
GULTON INDUSTRIES, INC.
9.0 AMPERE-HOUR NICKEL-CADMIUM SPACECRAFT CELLS
WITH AUXILIARY ELECTRODES
FOR THE
SMALL ASTRONOMY SATELLITE (SAS-C)

WQEC/C 75-165

2 JULY 1975

PREPARED BY

J. D. HARKNESS

PREPARED UNDER THE DIRECTION OF

DO THE ...

D. E. MAINS, Manager Satellite & Shipboard Battery Branch **APPROVED** 

By direction

#### REPORT BRIEF

INITIAL EVALUATION TESTS

GULTON INDUSTRIES, INC.

9.0 AMPERE-HOUR NICKEL-CADMIUM SPACECRAFT CELLS
WITH AUXILIARY ELECTRODES
FOR THE
SMALL ASTRONOMY SATELLITE (SAS-C)

(a) NASA Purchase Order S-53742AG

(b) Initial Evaluation Test Procedure for Nickel-Cadmium Sealed Space Cells: NAD 3053-TP324, 10 April 1973

#### TEST ASSIGNMENT BRIEF

Ref:

- A. The purpose of this evaluation test program is to insure that all cells put into the life cycle program are of high quality by the screening of cells found to have electrolyte leakage, internal shorts, low capacity, or inability of any cell to recover its open-circuit voltage above 1.150 volts during the internal short test.
- B. The 12 cells were provided by the National Aeronautics and Space Administration, Goddard Space Flight Center, to NAD Crane for evaluation on life test. The cells were procured by the Applied Physics Laboratory (APL), to APL Specification 7217-9014-A for the Small Astronomy Satellite (SAS-C), from Gulton Industries, Inc., Metuchen, New Jersey. These cells are from the same lot of cells that are being flown in the satellite which was launched in May 1975. Ten cells had no auxiliary electrode and were identified by the manufacturer's model number VO9HS and part number 805051. The remaining two, with auxiliary electrodes, had model number VO9HSAD and part number 805052. The auxiliary electrode cells and two of the other cells have pressure gauges. These cells are rated at 9.0 ampere-hours and contain double ceramic seals. The auxiliary electrode is Gulton's standard adhydrode (U-fold). The auxiliary resistor used throughout the test was 47 ohms. Testing was funded in accordance with reference (a).
- C. Test limits specify those values in which a cell is to be terminated from a particular charge or discharge. Requirements are referred to as normally expected values based on past performance of aerospace nickel-cadmium cells with demonstrated life characteristics. A requirement does not constitute a limit for discontinuance from test.

#### II. SUMMARY OF RESULTS

- A. The cells exceeded the maximum voltage requirement of 1.480 volts during their charges at 20°C.
- B. One cell exceeded the test limit of 1.560 volts for a continuous time period of 2 hours during the 0°C overcharge test. The other cells exceeded 1.560 volts during charge; but did not exceed the time period.
- C. Average end-of-charge voltages and capacity output in amperehours (ah) were as follows:

| Charge            |          | Volts | ah Out |
|-------------------|----------|-------|--------|
| c/20 for 48 hours | at 25°C  | 1.429 | 12.3   |
| c/10 for 24 hours | at 25°C  | 1.443 | 12.3   |
| c/10 for 24 hours | at 20°C  | 1.469 | 12.0   |
| c/10 for 24 hours | at 20°C* | 1.471 | 10.8   |
| c/40 for 20 hours | at 20°C  | 1.373 | 3.0**  |
| c/20 for 60 hours | at 0°C   | 1.553 | 13.0   |
| c/10 for 24 hours | at 35°C  | 1.403 | 10.1   |

\*Charge retention test.

- D. The average cell voltage at the end of one week open-circuit, during the charge retention test, was 1.305 volts.
- E. The 24-hour average cell voltage, following a 16-hour short period, was 7.221 volts.
- F. One of the auxiliary electrode cells reached its pressure limit of 20 psia with 12.8 ampere-hours input, and a voltage of 1.541 volts, during the pressure versus capacity test. The other three cells reached their voltage limit of 1.550 volts with an average input of 13.5 ampere-hours. Three cells exhibited pressure decay of 1 psia during the last 30 minutes of the 1-hour open-circuit stand. Average capacity out was 11.4 ampere-hours.

#### III. RECOMMENDATIONS

A. It was recommended that these cells be placed on life test simulating that which the spacecraft will require of the flight batteries.

<sup>\*\*</sup>This value represents 66.7 percent of the input capacity (charge efficiency test)

B. On 4 April 1975, one 10-cell pack (Pack 18G) began life test on a 1.48-hours orbit (1.00-hour charge) with a voltage limit control (1.447 V/C) at  $20^{\circ}\text{C}$  and a depth of discharge of 25 percent.

#### RESULTS OF INITIAL EVALUATION TESTS OF

GULTON INDUSTRIES, INC.

9.0 AMPERE-HOUR NICKEL- ADMIUM SPACECRAFT CELLS
WITH AUXILIARY ELECTRODES
FOR THE

#### SMALL ASTRONOMY SATELLITE (SAS-C)

#### I. TEST CONDITIONS AND PROCEDURE

- A. All evaluation tests were performed at room ambient (RA) pressure and temperature ( $25^{\circ} \pm 2^{\circ}$ C), with discharges at the 2-hour rate, and in accordance with reference (b), unless otherwise specified, and consisted of the following:
  - 1. Phenolphthalein leak tests (2).
- 2. Three capacity tests, third at 20°C; with internal resistance measurements during second charge/discharge.
  - 3. Auxiliary electrode characterization test.
  - 4. Charge retention test, 20°C.
  - 5. Internal short test.
  - 6. Charge efficiency test, 20°C.
  - 7. Overcharge tests, 0° and 35°C.
  - 8. Pressure versus capacity test.
  - 9. Phenolphthalein leak test.

(See Appendix I for summary of test procedure.)

#### II. CELL IDENTIFICATION AND DESCRIPTION

A. Ten of the twelve cells were manufactured without auxiliary electrodes. The cells were identified by the Applied Physics Laboratory part numbers 7217-9040A and also by the manufacturer as follows:

| Model    | Part Number | Serial Number             |
|----------|-------------|---------------------------|
| V09HS    | 805051      | 2049-2082 (not inclusive) |
| VO9HSAD* | 805052      | 109, 112                  |

\*Cells with auxiliary electrodes and pressure gauges. Two cells without auxiliary electrodes also had pressure gauges. The cells were placed in a temporary pack configuration for initial testing.

B. The 9.0 ampere-hour cell is rectangular with average weight and physical dimensions as follows:

| Weight (g)* | Overall<br>Height (in) | Length (in) | Width (in) |
|-------------|------------------------|-------------|------------|
| 404.5       | 3.696                  | 2.967       | .877       |

<sup>\*</sup> Does not include those cells with pressure gauges.

- C. The cell containers and covers are made of stainless steel. The positive and negative terminals are insulated from the cell cover by ceramic seals and protrude through the cover as solder-type terminals.
  - D. The auxiliary electrode in Gulton's standard adhydrode (U-fold).
- III. RESULTS--The following was condensed from tables I through VII.
- A. The cells exceeded the maximum voltage requirement of 1.480 voltages during their charges at 20°C.
- B. One cell, S/N 2069, exceeded the test limit of 1.560 volts for a continuous time period of 2 hours during the 0°C overcharge test. The other cells exceeded 1.560 volts during charge; but did not exceed the time period.
- C. Average end-of-charge (EOC) voltages and capacity output in ampere-hours (ah) were as follows:

| Charge                                    | Volts | ah Out |
|---|-------|--------|
| c/20 for 48 hours at 25°C                 | 1.429 | 12.3   |
| c/10 for 24 hours at 25°C                 | 1.443 | 12.3   |
| c/10 for 24 hours at $20^{\circ}\text{C}$ | 1.469 | 12.0   |
| c/10 for 24 hours at 20°C*                | 1.471 | 10.8   |
| c/40 for 20 hours at $20^{\circ}\text{C}$ | 1.373 | 3.0**  |
| c/20 for 60 hours at $0^{\circ}$ C        | 1.553 | 13.0   |
| c/10 for 24 hours at 35°C                 | 1.403 | 10.1   |

<sup>\*</sup> Charge retention test.

<sup>\*\*</sup> This value represents 66.7 percent of the input capacity (charge efficiency test).

#### D. Average Internal Resistance Measurements (milliohms):

| Measurement laken                       | Resistance |
|---|------------|
| 30 min before and-of-charge (Cycle 1)   | 4.41       |
| 1 Hr after start-of-discharge (Cycle 2) | 4.25       |
| 2 Hr after start-of-discharge (Cycle 2) | 4.42       |

- E. Maximum power was obtained with a 50-ohm resistance; but a 47-ohm resistance was used throughout the tests as instructed by the Goddard Space Flight Centers' Technical Officer.
- F. The average cell voltage at the end of one week open-circuit during the charge retention test, was 1.305 volts.
- G. The 24-hour average cell voltage, following a 16-hour short period, was 1.221 volts.
- H. One of the auxiliary electrode calls reached its pressure limit of 20 psia with 12.8 ampere-hours input, with a voltage of 1.541 volts, during the pressure versus capacity test. The other three cells reached their voltage limit of 1.550 volts with an average input of 13.5 ampere-hours. Three cells exhibited pressure decay of 1 psia during the last 30 minutes of the 1-hour open-circuit stand. Average capacity out was 11.4 ampere-hours.

APPENDIX I

#### APPENDIX I

#### TEST PROCEDURE

#### A. Phenolphthalein Leak Tests:

- 1. This test is a determination of the condition of the welds and ceramic seals on receipt of the cells and following the last discharge of the cells (Cycle #8).
- 2. The cells were initially checked with a one-half of one percent phenolphthalein solution applied with a cotton swab and then placed in a vacuum chamber and exposed to a vacuum of 40 microns of mercury or less for 24 hours. Upon removal they were rechecked for leaks and then received a final check following test completion. The requirement is no red or pink discoloration which indicates a leak.

#### B. Capacity Tests:

- 1. The capacity test is a determination of the cells' capacity at the C/2 discharge rate to 0.75 volt per cell, where C is the manufacturer's rated capacity. This type discharge follows all charges of this evaluation test.
  - 2. The charges for the capacity tests are as follows:
- a. C/20, 48 hours, room ambient (RA), Cycle 0, with a test limit of 1.52 volts or pressure of 100 psia.
- b. C/10, 24 hours, RA, Cycle 1, with a test limit of 1.52 volts or 100 psia pressure and a requirement of maximum voltage (1.48) or pressure (65 psia).
- c. C/10, 24 hours,  $20^{\circ}C$ , Cycle 2, with the same limits and requirements as the charge of Cycle 1.
- C. Special Resistance Characterization Tests for Auxiliary Electrode Cells:
- 1. The purpose of this test is to determine the resistance to be placed across the cell's auxiliary electrode and negative terminal which will provide maximum signal when the cell is fully charged.
- 2. The cells are charged at C/10 for 24 hours at the room ambient temperature following their initial charge/discharge cycle. Following this the cells are continued on charge with the current reduced, if necessary, to maintain the cell's voltage below 1.520 volts

and to stabilize the pressure between 10--20 psia. Resistance values, between 10--000 ohms and 0.1 ohm are then placed between the auxiliary electrode and the negative terminal. The cells are allowed a minimum of 5 minutes, at each resistance value, to obtain an equilibrium voltage across this resistance. This voltage value is then recorded and by calculation using the equation  $P = E^2/R$  the resistance that produces maximum power is determined.

#### D. Internal Resistance:

1. Measurements are taken across the cell terminals 1/2 hour before the end-of-charge (EOC) on Cycle 1 and 1 and 2 hours after the start-of-discharge of Cycle 2. These measurements were made with a Hewlett-Packard milliohmmeter (Model 4328A).

#### E. Special Charge Retention Test, 20°C:

- 1. This test is to establish the capacity retention of each cell following a 7 day open-circuit-stand in a charge mode.
- 2. The cells are charged at c/10 for 24 hours with a test limit of 1.52 volts or 100 psia pressure. They then stand on open-circuit for 7 days, with the requirement that the open-circuit voltage of each cell, following this period, is within  $\pm 5$  millivolts of the average cell voltage. The cells are then discharged and 80 percent capacity out of that obtained in Cycle 3 is required.

#### F. Internal Short Test:

- 1. This test is a means of detecting slight shorting conditions which may exist because of imperfections in the insulating materials, or damage to element in handling or assembly.
- 2. Following completion of the third capacity discharge, the cells are shunted with a 0.5-ohm, 3-watt resistor for 16 hours. At the end of 16 hours the resistors are removed and the cells stand on open-circuit-voltage (OCV) for 24 hours. A minimum voltage of 1.15 is required at the end of 24 hours.

#### G. Charge Efficiency Test, 20°C:

- 1. This test is a measurement of the cells' charge efficiency when charged at a low current rate.
- 2. The cells are charged at C/40 for 20 hours with a test limit of 1.52 volts or 100 psia pressure. They are then discharged and the requirement is that the minimum capacity out equals 55 percent of capacity in during the preceding charge.

#### H. Overcharge Test #1, 0°C:

- The purpose of this test is to determine the degree to which the cells will maintain a balanced voltage, and to determine the cells' capability to be overcharged without overcharging the negative electrode.
- 2. The cells are charged at C/20 for 60 hours. The test limits are cell voltages of 1 56 or greater for a continuous time period of ? hours or pressures of 100 psia. The requirement is a voltage of 1.520 or a pressure of 65 psia. The cells are then discharged and 85 percent capacity out of that obtained in Cycle 3 is required.

#### I. Overcharge Test #2, 35°C:

- 1. This test is a measurement of the cells' capacity at a higher temperature when compared to its capacity at 20°C. This test also determines the cells' capability of reaching a point of pressure equivibrium; oxygen recombination at the negative plate at the same rate it is being generated at the positive plate.
- 2. The cells are charged C/10 for 24 hours with a test limit of 1.52 volts or 100 psia pressure and a requirement of 1.45 volts or 65 psia pressure. The cells are then discharged with a requirement that capacity out equals 55 percent capacity out as obtained in Cycle 3.

#### J. Pressure versus Capacity Test:

- 1. The purpose of this test is to determine the capacity to a pressure and the pressure decay during charge and open circuit stand respectively.
- 2. Each cell is charged at C/2 to either a pressure of 20 psia or a voltage of 1.550. Recordings are taken on each cell when it reaches 5, 10, 15 and 20 psia pressure. The cells then stand OCV for 1 hour with 30-minute recordings and then are discharged, shorted out and leak tested.

WQEC/C 75-165

MEASUREMENT AND LEAK TEST DATA TARIF I

| SERIAL   HEIGHT   H   | -    | Jun-und          | (6) /          |                 |                 |                   |           |       |   | PHENOL | PHTHAL  | EIN LE | PHENOLPHTHALEIN LEAK TESTS |            |        |         |        |
|--|------|------------------|----------------|-----------------|-----------------|-------------------|-----------|-------|---|--------|---------|--------|----------------------------|------------|--------|---------|--------|
| SERIAL WEIGHT HEIGHT LENGTH WIDTH Terminals Fill Other Inches) (Inches) (In | _    |                  |                |                 |                 |                   | I         | itial |   | Ä      | ollowin | ng Hi  | /ac                        | Followi    | ing Te | st Comp | letion |
| 109 778.5 3.70c 2.770 .878 112 794.4 3.696 2.968 .887 2049 464.6 3.696 2.968 .877 2052 781.5 3.691 2.968 .872 2054 464.7 3.496 2.966 .860 2054 464.7 3.496 2.966 .879 2054 464.3 3.707 2.965 .877 2072 403.3 3.696 2.965 .877 2072 403.3 3.696 2.965 .877 2072 403.3 3.696 2.965 .877 2072 403.3 3.696 2.965 .877 2082 783.7 3.695 2.968 .879  |      | SERIAL<br>NUMBER | WEIGHT (Grams) | HEIGHT (Inches) | LENGTH (Inches) | WIDTH<br>(Inches) | Terminals | -     | - | - Term |         | Fill   | Other O                    | Termi<br>+ | na ls  |         | Other  |
| 1/2 7944 3.696 2.968 .877  2049 4040 3.688 2.968 .877  2052 788.5 3.48/1 2.968 .872  2054 4047 3.494 2.946 .880  2054 404.3 3.70/ 2.974 .877  2072 403.3 3.692 2.965 .877  2072 403.3 3.692 2.965 .877  2078 404.8 3.49 2.968 .877  2082 783.7 3.675 2.968 .877  | -    | 109              | 798.5          | 3.706           | 2.970           | .878              |           |       |   |        |         |        |                            |            |        |         |        |
| 2052 78.5 3.67/ 2.968 .877 2052 78.5 3.67/ 2.968 .872 2059 4647 3.696 .860 2061 404.9 3.704 2.965 .889 2063 404.8 3.704 2.967 .877 2064 406.3 3.692 2.965 .877 2072 403.3 3.692 2.965 .877 2072 403.4 3.692 2.965 .877 2072 403.5 3.692 2.965 .877 2082 783.7 3.675 2.968 .877   | -    | 112              | 794.4          | 3.696           | 7.964           | .88 %             |           |       |   |        |         |        |                            |            |        |         |        |
| 2052     78.5     3.64     2.96     .672       2059     404.7     3.64     2.96     .860       2061     404.9     3.74     2.96     .880     No tears       2063     402.8     3.70     2.94     .877       2072     406.3     3.69     2.94     .877       2073     406.3     3.69     2.96     .875       2074     405.6     3.69     2.96     .877       2078     403.6     3.69     2.96     .877       2082     783.7     3.69     2.96     .877  |      | 2049             | 404.0          | 3.688           | 2.96.8          | .877              |           |       |   |        |         |        |                            |            |        |         |        |
| 2059 404.7 3.496 2.966 .880 No Leaks No Leaks 2061 404.9 3.704 2.965 .880 No Leaks 2063 402.8 3.701 2.967 .877 2069 406.3 3.701 2.974 .877 2072 403.3 3.692 2.965 .875 2072 403.3 3.692 2.965 .877 2078 403.6 3.692 2.968 .877 2082 783.7 3.695 2.968 .879   |      | 2052             | 781.5          | 3.691           | 2.968           | .872              |           |       |   |        |         |        |                            |            |        |         |        |
| 404.9       3.704       2.965       .880       N0 Leaks       N0 Leaks         402.8       3.701       2.947       .877       N0 Leaks       N0 Leaks         406.3       3.701       2.945       .877       N0 Leaks       N0 Leaks         403.3       3.672       2.965       .877       N0 Leaks       N0 Leaks         403.3       3.692       2.965       .879       N0 Leaks         783.7       3.695       2.968       .879       N0 Leaks  |      | 2059             | 404.7          | 3.696           | 2.966           | .880              |           |       |   |        |         |        |                            |            |        |         |        |
| 2063 402.8 3.701 2.967<br>2069 406.3 3.701 2.975<br>2072 403.3 3.696 2.965<br>2073 406.3 3.692 2.965<br>2078 403.6 3.690 2.964<br>2082 783.7 3.695 2.968   |      | 2061             | 404.9          | 3.704           | 2.965           | .880              | No        | Leak  | 4 |        | No      | Leaks  |                            |            | NO     | Leaks   |        |
| 2069 406.3 3.701 2.974<br>2072 403.3 3.696 2.965<br>2073 406.3 3.692 2.965<br>2078 403.6 3.690 2.968<br>2082 783.7 3.695 2.968   |      | 2063             | 402.8          | 3.701           | 2.967           | .8 79             |           |       |   |        |         |        |                            |            |        |         |        |
| 2072 403.3 3.6% 2.965<br>2073 406.3 3.692 2.965<br>2078 403.6 3.690 2.964<br>2082 783.7 3.695 2.968  |      | 2069             | 406.3          | 3.701           | 2.974           | .877              |           |       |   |        |         |        |                            |            |        |         |        |
| 2073     406.3     3.692     2.965       2078     403.6     3.690     2.964       2082     783.7     3.695     2.968   |      | 2072             | 403.           | 3.6%            | 2.965           | .875              |           |       |   |        |         |        |                            |            |        |         |        |
| 2078 403.6 3.690 2.964   |      | 2073             | -              | 3.692           | 2.965           | .877              |           |       |   |        |         |        |                            |            |        |         |        |
| 2082 783.7 3.695 2.968   |      | 2078             | 403.6          | 3.690           | 2.964           | 418.              |           |       |   |        |         |        |                            |            |        |         |        |
|  |      | 2082             | 783.7          | 3.695           | 2.968           | .879              |           |       |   |        |         |        |                            |            |        |         |        |
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|          |              |                 |        |        |             |        |         | S               | Capacity Data | Data   |            |       |          |                      | 10000   |               |              |        |
|----------|--------------|-----------------|--------|--------|-------------|--------|---------|-----------------|---------------|--------|------------|-------|----------|----------------------|---------|---------------|--------------|--------|
|          | Capacit      | Capacity Test 1 | 200    | JU UNJ | OF DECOMPOS | 1900   | Capaci  | Capacity Test 2 | 5             | CMA    | OF DI CON  | 3000  | Capacity | Capacity lest 3 ZUTL | 77.07   | FMD           | OF DISONA    | PER    |
| SERIAL   | _            | AUX             | PRESS  | CAPAC- | AUX         | PRES   | _       | AUX             | PRESS         | CAPAC- | CAPAC- AUX | PFESS | СЕП      | AUX                  | P RE SS | CAPAC-<br>ITY | ITY ELECT PR | PRESS  |
|          | (Volts)      | (Volts)         | (PSIA) | (ak)   | (Volts)     | (PSIA) | (Volts) | (Volts)         | (PSIA)        | ( AP ) | (Volts)    |       | (Volts)  | (Volts)              | (PS:4)  | <b>%</b>      | (Volts)      | (PSIA) |
| 109      | 1.431        | .466            | 12     | 12.1   | .042        | 3      | 1. 143  | . 578           | 22            | 12.2   | .036       | 4     | 1.462    | 869.                 | 65      | 11.5          | .4.2         | 13     |
| 112      | 1.431        | 479             | 15     | 12.2   | +20.        | 5      | 1.444   | .590            | 27            | 12.2   | .045       | 5     | 1764     | .727                 | 75      | 4.11          | 374.         | 19     |
| 2049     | 1.432        |                 |        |        |             |        | 1.448   |                 |               | 12.5   |            |       | 1.475    |                      |         | 12.2          |              |        |
| 2052     | 1427         |                 | 10     | 12.3   |             | 5      | 1.442   |                 | 17            | 12.4   |            | 6     | 1.469    |                      | 19      | 1.1           |              | 5      |
| 2059     | 1.427        |                 |        | /2.3   |             |        | 1.442   |                 |               | 12.3   |            |       | 1.469    |                      |         | 12.2          |              |        |
| 2061     | 1.427        |                 |        | 12.2   |             |        | 1,442   |                 |               | 12.2   |            |       | 1.468    |                      |         | 11.9          |              |        |
| 2063     | 1.428        |                 |        | 12.1   |             |        | 1.441   |                 |               | 12.3   |            |       | 1.466    |                      |         | 12.0          |              |        |
| 2069     | 1.428        |                 |        | 12.4   |             |        | 1.444   |                 |               | 12.5   |            |       | 1472     |                      |         | 12.2          |              |        |
| 2072     | -            |                 |        | 12.3   |             |        | 1.440   |                 |               | 12.4   |            |       | 1.470    |                      |         | 12.2          |              |        |
| 2073     | +-           |                 |        | 12.4   |             |        | 1.443   |                 |               | 12.5   |            |       | 1.470    |                      |         | 12.2          |              |        |
| 2078     | 1429         |                 |        | 12.2   |             |        | 1.443   |                 |               | 12.2   |            |       | 1.469    |                      |         | 12.1          |              | I      |
| 2082     | 1.431        |                 | 6      | 12.2   |             | 4      | 1.446   |                 | 16            | 12.3   |            | +     | 1.472    |                      | 18      | 12.1          |              | 5      |
|          |              |                 |        |        |             |        |         |                 |               |        |            |       |          |                      |         |               |              |        |
|          |              |                 |        |        |             |        |         |                 |               |        |            |       |          |                      |         |               |              |        |
|          |              |                 |        |        |             |        |         |                 |               |        |            |       |          |                      |         |               |              |        |
|          |              |                 | _      |        |             |        |         |                 |               |        |            |       |          |                      |         |               |              |        |
|          |              |                 | 1      |        |             |        |         |                 |               |        |            |       |          |                      |         |               |              |        |
|          |              |                 | -      |        |             |        |         |                 |               |        |            |       |          |                      |         |               |              |        |
|          |              |                 | -      |        |             |        |         |                 |               |        |            |       |          |                      |         |               |              |        |
|          |              |                 | L      |        |             |        |         |                 |               |        |            |       |          |                      |         |               |              |        |
|          |              |                 | -      |        |             |        |         |                 |               |        |            |       |          |                      |         |               |              |        |
|          |              |                 | _      |        | Ö,          | _      |         |                 |               |        |            |       |          |                      |         |               |              |        |
|          |              |                 | -      |        | R           |        |         |                 |               |        |            |       |          |                      |         |               |              |        |
|          |              |                 |        |        | GI<br>PO    |        |         |                 |               |        |            |       |          |                      |         |               |              |        |
|          |              |                 |        |        | $N_A$ $0R$  |        |         |                 |               |        |            |       |          |                      |         |               |              |        |
|          |              |                 | -      |        | L           |        |         |                 |               |        |            |       |          |                      |         |               |              |        |
| SED-KADO | c (sp 11/73) | 73)             |        |        | F.          |        |         |                 |               |        |            |       |          |                      |         |               |              |        |

### TABLE III INTERNAL RESISTANCE AND SHORT TEST DATA

9ND-NADC (SP 11/73)

|                  | IN            | TERNAL RESISTANCE (M                 | ILLIOHMS)                             |                      | AL SHORT           |       |
|------------------|---------------|--------------------------------------|---------------------------------------|----------------------|--------------------|-------|
| SERIAL<br>NUMBER | END-OF-CHARGE | ONE HOUR AFTER<br>START-OF-DISCHARGE | TWO HOURS AFTER<br>START-OF-DISCHARGE | AFTER 16<br>HR SHORT | AFTER 24<br>OCV ST |       |
|                  |               |                                      |                                       | CELL                 | CELL               | PRESS |
| 109              | 4.8           | 4.4                                  | 4.2                                   | .028                 | 1.223              | 4     |
| 112              | 4.4           | 4.2                                  | 4.5                                   | ,027                 | 1.218              | 6     |
| 2049             | 4.2           | 4.2                                  | 4.2                                   | .012                 | 1.219              |       |
| 2052             | 4.4           | 4.1                                  | 4.2                                   | .016                 | 1.222              | 5     |
| 2059             | 4.3           | 4.3                                  | 4.3                                   | .014                 | 1.223              |       |
| 2061             | 4.3           | 4.1                                  | 4.4                                   | .015                 | 1.223              |       |
| 2063             | 5.0           | 4.3                                  | 4.6                                   | .013                 | 1.223              |       |
| 2069             | 4.3           | 4.6                                  | 4.6                                   | .012                 | 1.220              |       |
| 2072             | 4.2           | 4.1                                  | 4.6                                   | .012                 | 1.221              |       |
| 2073             | 4.6           | 4.2                                  | 4.4                                   | .014                 | 1.221              |       |
| 2078             | 4.3           | 4.3                                  | 4.6                                   | .014                 | 1,222              |       |
| 2082             | 4.1           | 4.2                                  | 4.4                                   | . 012                | 1.222              | 4     |
|                  |               |                                      |                                       |                      |                    |       |
|                  |               |                                      |                                       |                      |                    |       |
|                  |               |                                      |                                       |                      |                    |       |
|                  |               |                                      | 10                                    |                      |                    |       |

#### TABLE IV CHARGE RETENTION TEST DATA

|                  | END-   | OF-CHAR                   | GE               | 24             | HR. OC                   | v                | 1 W             | EEK OC                   | 1                | END-0                 | F-DISCH | ARGE   |
|------------------|--|---------------------------|------------------|----------------|--------------------------|------------------|-----------------|--------------------------|------------------|-----------------------|---------|--------|
| SERIAL<br>NUMBER | CELL<br>(VOLTS)                                  | AUX.<br>ELECT.<br>(VOLTS) | PRESS.<br>(PSIA) | CELL<br>(VOLTS | AUX.<br>ELECT.<br>(VOLTS | PRESS.<br>(PSIA) | CELL<br>(VOLTS) | AUX.<br>ELECT<br>(VOLTS) | PRESS.<br>(PSIA) | CAPAC-<br>ITY<br>(AH) |         | PRESS. |
| 109              | 1.474  | .682                      | 65               | 1.346          | .063                     | 5                | 1.307           | .013                     | 3                | 10.6                  | 164     | 3      |
| 112              | 1.475  | .686                      | 7/               | 1349           | .060                     | 6                | 1.307           | .008                     | 4                | 10.7                  | 143     | 4      |
| 2049             | 1.475  |                           |                  | 1.348          |                          |                  | 1.305           |                          |                  | 11.0                  |         |        |
| 2052             |  |                           | 36               | 1349           |                          | 5                | 1.307           |                          | 5                | 11.0                  |         | 5      |
| 2059             | 1470   |                           |                  | 1.349          |                          |                  | 1.306           |                          |                  | 10.7                  |         |        |
| 2061             | 1470   |                           |                  | 1347           |                          |                  | 1304            |                          |                  | 10.7                  |         |        |
| 2063             | 1469   |                           |                  | 1348           |                          |                  | 1.305           |                          |                  | 10.7                  |         |        |
| 2069             | 1.477  |                           |                  | 1349           |                          |                  | 1305            |                          |                  | 10.9                  |         |        |
| 2072             | 1469   |                           |                  | 1.347          |                          |                  | 1303            |                          |                  | 10.7                  |         |        |
| 2073             | 1466   |                           |                  | 1.349          |                          |                  | 1306            |                          |                  | 10.8                  |         | -      |
| 2078             | 1468   |                           |                  | 1.346          |                          |                  | 1304            |                          |                  | 10.8                  |         |        |
| 2082             | 1.471  |                           | 33               | 1347           |                          | 5                | 1303            |                          | 5                | 10.8                  |         | 5      |
|                  |  |                           |                  |                |                          |                  |                 |                          |                  |                       |         | -      |
|                  |  |                           |                  |                |                          |                  |                 |                          |                  |                       |         | -      |
|                  |  |                           |                  |                |                          |                  |                 |                          |                  |                       |         |        |
|                  |  |                           |                  |                |                          |                  |                 |                          |                  |                       |         |        |
|                  |  |                           |                  |                |                          |                  |                 |                          |                  |                       |         |        |
|                  |  |                           |                  |                |                          |                  |                 |                          |                  |                       |         |        |
|                  |  |                           |                  |                |                          |                  |                 |                          |                  |                       |         |        |
|                  |  |                           |                  |                |                          |                  |                 |                          |                  |                       |         |        |
|                  |  |                           |                  |                |                          |                  |                 |                          |                  |                       |         |        |
|                  |  |                           |                  |                |                          |                  |                 |                          |                  |                       |         |        |
|                  |  |                           |                  |                |                          |                  |                 |                          |                  |                       |         |        |
|                  |  |                           |                  |                |                          |                  |                 |                          |                  |                       |         |        |
|                  |  |                           |                  |                |                          |                  |                 |                          |                  |                       |         |        |
|                  |  |                           |                  |                |                          |                  |                 |                          |                  |                       |         |        |
|                  |  |                           |                  |                |                          |                  |                 |                          |                  |                       |         |        |
|                  |  |                           |                  |                |                          |                  |                 |                          |                  |                       |         |        |
|                  |  |                           |                  |                |                          |                  |                 |                          |                  |                       |         |        |
|                  |  |                           |                  |                |                          |                  |                 |                          |                  |                       |         |        |
| ·                |  |                           |                  |                |                          |                  |                 |                          |                  |                       |         |        |
| -                |  |                           |                  |                |                          | 11               |                 |                          |                  |                       |         |        |
|                  | <del>                                     </del> |                           |                  |                |                          |                  |                 |                          |                  |                       |         |        |
|                  | <b>†</b>   |                           |                  |                | 1                        |                  |                 |                          |                  |                       |         |        |

| THE CELL ELECT PRESS THY ELECT PRESS THY (VOIES) (PSIA)  (270 (2012) (VOIES) (PSIA) (an) (VOIES) (PSIA)  (270 (272 (28 2.97 2.9 2.97 2.9 2.9 2.9 2.9 2.9 2.9 2.9 2.9 2.9 2.9   | Control   Cont   |                | -         | . 661-100               | 10001           | -                     |                         |                 | 0vercha      | Overcharge Test (00)   | (00) |                        |                        |        | Overcha | Overcharge Test | (3200)          |      |                  |   |
|--|--|----------------|-----------|-------------------------|-----------------|-----------------------|-------------------------|-----------------|--------------|------------------------|------|------------------------|------------------------|--------|---------|-----------------|-----------------|------|------------------|---|
| CELL   ELECT   PRESS   CELL   ELECT   PRESS   CELL   CHOICAL   C   | Call      |                | Charge    | LTTICIENC               | 300             | END                   | OF-DISCH                | 1P.CE           | EN           | D-CF-CHAR              |      | - T - T                | 01-10                  | 7      | . 7     | 441 C-1 C-      | 44              | 3    | OF - JIS CHI     | 10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00<br>10.00 |
| 370  | 370   066   3   29   000   3   1558   N#   9   136   034   19   190   100      | ERIAL<br>UMBER |           | Aux<br>ELECT<br>(Volts) | PRESS<br>(PSIA) | CAPAC-<br>1TY<br>(ah) | AUX<br>ELECT<br>(Volts) | PRESS<br>(PSIA) | CELL (Volts) | AUX<br>ELECT<br>Volts) | E.S  | CAPAC-<br>1-TV<br>(ah) | LEGI<br>LEGI<br>Nolts) | (PSIA) | (701ts) |                 | PRESS<br>(PSIA) | (#)  | CLECT<br>(Volts) | PRES:   |
| 574   295   4 35   272   255   300   274   7468   688   57   112   226   2           | 374   695   4   35   1072   5   551   308   36   130   014   24   1466   686   57   112   123   1374   1466   14   | 0              | 1 270     | 276                     | ~               |                       | 010                     | 8               | 1.558        | NA                     | 6    | n                      | .034                   | 61     | 1410    | .701            | 6               | 112  | .226             | - 1   |
| 1373   5 3 5   | 1374   2.8   | 12             |           | .095                    | 1               |                       | 0                       | 5               | 1551         | ,308                   |      | m                      | +10.                   | 24     | 8041    | 889.            |                 |      | .226             | 28  |
| 1373   5 35  | 1 373  | 0              |           | 2                       |                 | 1 7                   |                         |                 | 1555         |                        |      |                        |                        |        | 1403    |                 |                 | 0.01 |                  |   |
| 373   35   1553   132   1319   95   1373   1373   1254   1254   124   1403      | 373   35   1553   132   1349   1373   2.9   1554   124   1465   1373   2.9   1556   124   1465   1373   2.9   1556   124   1463   1373   2.9   1556   124   1463   1373   2.9   1557   125   124   1463   1373   4 29   4 1555   124   1463   1373   4 29   4 1555   124   1463   1373   4 29   4 1555   124   1463   1373   1373   4 29   4 1555   124   1463   1373   | 17             |           |                         | V               | 200                   |                         | 7               | 1543         |                        | 3/   | 12.8                   |                        | 61     | 1.401   |                 | 20              | 1.01 |                  |   |
| 373   2.9   1556   19.3   1379   19.4   19.5   1373   1373   2.9   1526   12.6   12.6   14.65   10.4   13.7   13   | 373   2.9  | 70             |           |                         |                 | 24 (                  |                         |                 | 1553         |                        |      |                        |                        |        | 1399    |                 |                 | 95   |                  |   |
| 373   2.9   1521   124   1405   164   1373   1373   124   1405   164     | 373   29   1531   124   1465   1373   25   1562   1562   1562   1563     | 17             | 1373      |                         |                 |                       |                         |                 | 1556         |                        |      |                        |                        |        | 1.399   |                 |                 | 24   |                  |   |
| 2.7 (40.5) (40.5 | 1373 2.7 1562 135 1463<br>1373 2.9 1566 126 136<br>1373 4 29 4 555 22 126 11 1405<br>1373 4 29 4 1555 22 126 11 1405   | 27             | 1         |                         | -               |                       |                         |                 | 1531         |                        |      |                        |                        |        | 1.405   |                 |                 | 401  |                  | 1   |
| 2 2.9 (25) (26) (136) (1 | 1373   | 64             | 16        |                         |                 | 27                    |                         |                 | 1.562        |                        |      | 135                    |                        |        | 1403    |                 |                 | 66   |                  | 1   |
| 1372   | CRIGINAL PAGE IS 12.2 1.2.4 1.463 1.3.5 1. | 172            | 16        |                         | -               | 1 - '                 |                         |                 | 1558         |                        |      |                        |                        |        | 1 398   |                 |                 | 9.3  |                  | 1   |
| CRICINAL DOR DOR OF POOR QUALITY   | 0 POOR QUALITY  9 23 34 6 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7  | 33             | 1272      |                         | _               | 1.                    |                         |                 | 1550         |                        |      |                        |                        |        | 1403    |                 |                 |      |                  | 1   |
| ORIGINAL PAGE OF ROOR QUALITY  | ORIGINAL PAGE IS OF POOR QUALITY   | 100            | 1278      |                         | -               |                       |                         |                 | 1557         |                        |      |                        |                        |        | 1.399   |                 |                 |      |                  | -   |
| ORIGINAL PAGE OF POOR QUALIT   | OF POOR QUALITY  | 82             | 1373      |                         | 7               |                       |                         | 7               | 1555         |                        | 22   |                        |                        | //     | 1405    |                 |                 | 10.3 |                  | 7   |
| ORIGINAL PAGE OF POOR QUALITY  | ORIGINAL PAGE IS OF POOR QUALITY   |                |           |                         |                 |                       |                         | 1               |              |                        |      |                        |                        |        |         |                 |                 |      |                  | Ц   |
| ORIGINAL PAGE OF POOR QUALITY  | ORIGINAL PAGE IS OF POOR QUALITY   |                |           |                         |                 |                       |                         |                 |              |                        |      |                        |                        |        |         |                 |                 |      |                  | -   |
| ORIGINAL PAGE OF POOR QUALITY  | ORIGINAL PAGE IS OF POOR QUALITY   |                |           |                         | -               | -                     |                         |                 |              | _                      |      |                        |                        |        |         |                 |                 |      |                  | 1   |
| OR GOVAL PAGE OUALITY  | ORIGINAL PAGE IS OF POOR QUALITY   |                |           |                         | -               |                       |                         |                 |              |                        |      |                        |                        |        |         |                 |                 |      |                  | 1   |
| ORIGINAL PAGE OF POOR QUALIT   | ORIGINAL PAGE IS OF POOR QUALITY   |                |           |                         | -               |                       |                         |                 |              |                        |      |                        |                        |        |         |                 | 1               |      |                  | +   |
| ORIGINAL PAGE OF POOR QUALIT   | ORIGINAL PAGE IS OF POOR QUALITY   |                |           |                         |                 |                       |                         |                 |              |                        |      |                        |                        | -      |         |                 | _               |      |                  | 1   |
| ORIGINAL PAGE QUALIT   | ORIGINAL PAGE IS OF POOR QUALITY   |                |           |                         | 1               |                       |                         | 1               |              |                        | 1    |                        |                        | -      |         |                 |                 |      |                  |   |
| POOR QUALITY   | POOR QUALITY   |                |           | OR                      | 1               |                       |                         | 1               |              |                        |      |                        |                        |        |         |                 |                 |      |                  | +   |
| NAL PAGE<br>OR QUALIT  | NAL PAGE IS<br>OR QUALITY  |                | Po        | G                       | +               |                       |                         |                 |              |                        |      |                        |                        |        |         |                 | _               |      |                  | -   |
| L PAGE<br>QUALIT   | L PAGE IS<br>QUALITY   | 1              | OR        | N <sub>A</sub>          |                 |                       |                         |                 |              |                        |      |                        |                        | -      |         |                 |                 |      |                  | +   |
| PAGE   | PAGE IS  |                | Q         | 7                       | +               | 1                     |                         | 1               | 1            | -                      | -    |                        | 1                      | +      | 1       | -               | +               |      | -                | -   |
| GE   | GE IS<br>LITY  |                | JA.       | 7                       | -               | _                     | _                       |                 |              |                        |      |                        |                        |        |         |                 |                 |      |                  |   |
|  | I.S. Y.  |                | GE<br>LII |                         |                 |                       |                         |                 |              |                        |      |                        |                        |        |         |                 |                 |      |                  |   |

9ND-NADC (SP 11/73)

ORIGINAL PAGE IS OF POOR QUALITY TABLE VI PRESSURE VS. CAPACITY TEST DATA 1.382 2082 1.550 1.401 1.517 13.8 11.4 13.8 8/10 N/A 12 13.1 17 4/2 4/4 8/1 4/2 0 % 17 15 386 2052 400 1.531 11.5 4/1 1.44 7.5 22 13.3 4/4 15 61 6 1/2 13. 1.541 1.389 1.492 440. 1.402 033 142 7117 124 .136 11.3 20 4/4 WA 1 13 1/2 12. 2 NOT APPLICABLE +91. 389 .063 1.515 .075 206 5 4.17 14.3 WIR ø 61 13 Press AH fn to V/L (1.55V) Start-of-Charge, AH in to 20 PSIA AH in to 10 PSIA AH in to 15 PSIA 30 Min OCV, Cell hour OCY. Cell .. W/N AH in to 5 PSIA Aux (volts) Press (PSIA) Cell (volts) Press (PSIA) Cell (volts) Press (PSIA) Cell (volts) Cell (volts) Press (PSIA) Aux (volts) EOD AH out Serial No.

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SPECIAL RESISTANCE CHARACTERISTIC DATA ON THE AUXILIARY ELECTRODES TABLE VII

| SERIAL 40. | 109   | 6     | 112   | 2     |       |       |       |       |       |       | AVERAGE | GE         |
|------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|---------|------------|
| CHINS      | VOLTS | PRESS | VOLTS   | MILLIWATTS |
| 10,000     | .835  | 20    | .860  | 20    |       |       |       |       |       |       | 8+7     | .072       |
| 5,000      | .837  | 20    | .855  | 20    |       |       |       |       |       |       | .846    | ./43       |
| 2,000      | .837  | 20    | 748.  | 20    |       |       |       |       |       |       | .842    | .354       |
| 1,000      | .830  | 20    | .833  | 20    |       |       |       |       |       |       | .83/    | .69/       |
| 200        | +08.  | 20    | .807  | 61    |       |       |       |       |       |       | .805    | 1.2%       |
| 200        | .683  | 61    | .675  | 19    |       |       |       |       |       |       | .679    | 2.305      |
| 100        | .595  | 19    | .572  | 19    |       |       |       |       |       |       | . 583   | 3.349      |
| 50         | .475  | 81    | .433  | 61    |       |       |       |       |       |       | .454    | 4.122      |
| 20         | .298  | 91    | .260  | 61    |       |       |       |       |       |       | .279    | 3.892      |
| 10         | 881.  | 18    | 165   | 8/    |       |       |       |       |       |       | .176    | 3.097      |
| 5          | ./33  | 17    | 00/.  | 8/    |       |       |       |       |       |       | 9//     | 2.691      |
| 2          | 150.  | 17    | ,050  | 18    |       |       |       |       |       |       | .053    | 1.405      |
| -          | ,031  | 17    | .028  | 8/    |       |       |       |       |       |       | .029    | .81        |
| 0.5        | 910.  | 9/    | 210.  | 18    |       |       |       |       |       |       | .015    | .450       |
| 0.2        | 800.  | 16    | 700.  | 8     |       |       |       |       |       |       | 1.00.   | . 245      |
| 0.1        | ,006  | ,6    | 500.  | 8/    |       |       |       |       |       |       | .005    | .250       |
|            |       |       |       |       |       |       |       |       |       |       |         |            |

Note: All pressures in PSIA.

: Milliwatts  $POWER = \frac{V^2}{R}$  Watts  $10^3$  Milliwatts