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California Institute of Technology

FINAL TECHNICAL REPORT

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MARINER 6 AND 7 PICTURE ANALYSIS

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This report summarizes the status and results of analytical studies of Mariner 6 and 7 far-encounter (FE) pictures, carried out during the period July, 1970 to September, 1973. The purpose of the studies was to devise ways to combine digital data from the full set of FE pictures so as to improve surface resolution, distinguish clouds and haze patches from permanent surface topographic markings, deduce improved values for radius, oblateness, and spin-axis orientation, and produce a composite photographic "map" of Mars at the 1969 epoch suitable for comparison with later or earlier data.

The general status of the work at the end of the period was that the attempts to measure and correct camera distortions, locate each image in the frame, and convert image coordinates to martian surface coordinates were highly successful - residual uncertainties in location were considerably less than one pixel (picture element). However, the analysis of the data to improve the radius, figure, and axial tilt was curtailed because of the huge mass of superior data provided by the follow-on Mariner 9 spacecraft.

The procedures for superposition of successive frames to produce a composite map had been only partially worked out when the effort was suspended. All of the data, programs, and intermediate results are still available (1976) and could be carried forward with little difficulty given sufficient need and the necessary technical support.

The greater part of this report is devoted to a brief summary of the problems faced, the solutions found, and the conclusions reached in analyzing the picture data.

#### THE DATA

Mariner 6 returned 49 far-encounter pictures over a 2-day period, and Mariner 7 returned 92 FE pictures over a 3-day period prior to closest approach. The picture frame format comprised 700 lines having 945 pixels per line. Each pixel was represented by a digitized intensity on a scale of 0-255, called data-numbers (DN). We are not concerned here with the degree of linearity of the actual relationship between DN and intensity, but simply treat DN's as approximately linear in intensity.

The image diameters, in pixels, ranged from 145 to more than 1000, with corresponding scale factors of  $\sim 100$  km/pixel to  $\sim 10$  km/pixel. These scales, while far inferior to those obtained at near-encounter and by Mariner 9, are substantially

superior in resolution to earth-based pictures and thus provide valuable intermediate-resolution data. The possible importance of such data in connection with studies of variable martian features prompted the program described here.

### TECHNICAL OBJECTIVES

In order to derive the best possible resolution, intensity discriminability, and geometric fidelity, it was taken as a goal to superimpose images such that any given point on Mars, visible in a particular image, be defined within a fraction - say a tenth - of a pixel. To achieve this goal entailed a considerable analysis and correction of camera distortions, and required the invention of highly sensitive procedures for defining the boundaries of each image. The principal factors which entered the problem were these:

1. Camera optics. The focal length and geometrical distortions of each camera system had to be determined with sufficient accuracy, both for intercomparing the results from Mariners 6 and 7, or for combining the two data sets should this prove desirable.
2. Vidicon distortion. The vidicon TV sensor used in the cameras, while being quite satisfactorily distortion-free for ordinary purposes, did possess measurable distortions (of electronic origin) analogous to the optical distortions familiar in camera systems. A complicating factor here was that the electronic distortions were to some extent intensity-dependent.
3. Image geometry. The problem of defining the location and size of each image was complicated by the frequent occurrence of haze layers around the limb and perhaps near the terminator. The oblique view (phase angle approximately  $25^{\circ}$ ) also made it necessary to work with the relatively poorly-defined sunrise terminator line on half of the image rather than with a relatively sharp limb-sky boundary. This problem could be alleviated somewhat if one knew the focal length precisely and were able to assume a radius, oblateness, and distance for Mars. At the start of this project it was hoped that the data might yield improved values for the radius and oblateness, so that it was deemed necessary to face the image measurement problem in its most general form.

### PROCEDURES

The procedures used to evaluate the system parameters, correct for aberrations, and define the image shape will be discussed under the following headings:

## Focal Lengths and Image Scale

## Image Distortions and Their Correction

## Limb Detection

## Image Superposition

1. Focal Lengths and Image Scale.

The focal lengths of the cameras were defined by direct measurement in the laboratory, by viewing a calibrated illuminated reticle in the focal plane of an autocollimator using a theodolite, and then measuring the image of this reticle in the camera focal plane using a travelling microscope.

(L. Adams: JPL memo of 1 July, 1969, "Narrow Angle Optics Focal Length Determination").

The present author reviewed the procedures and the data, and reduced the data using a maximum-likelihood procedure. If the various angles subtended by the cross-lines of the reticle, as viewed in the theodolite, are  $A_i$  ( $i = 1, 2, \dots$ ) and the corresponding linear positions of these lines as viewed in the focal plane are  $X_i$  ( $i = 1, 2, \dots$ ), then the focal length  $F$  may be defined in terms of these values as the best-fit value in the relation

$$(X_i - \bar{X}) = F(A_i - \bar{A})$$

where  $\bar{X}$ ,  $\bar{A}$  are the means of  $X_i$  and  $A_i$ , respectively.

The quantities  $X_i$  and  $A_i$  were both subject to uncertainties,  $\sigma_X$  and  $\sigma_A$ , which were taken into account in finding the best fit  $F$ . (Each measurement of  $X_i$  and  $A_i$  was made four times in independent runs, so that  $\sigma_X$  and  $\sigma_A$  could be evaluated:  $\sigma_X = 0.003$  mm and  $\sigma_A = 0.7$  arc sec.) The resulting values for  $F$  were

M6 Camera B:  $F = 505.44 \pm .07$  mm

M7 Camera B:  $F = 502.66 \pm .07$  mm

To define the linear scale of the image on the face of the vidicon, a 7 x 9 array of small, square marks was vacuum deposited through a carefully prepared mask on the inner face of each vidicon tube during manufacture. Each tube was later measured to verify the actual location of each such reseau mark. These marks were visible as black dots covering a few pixels of the image, and were not visible in unilluminated areas. Each Mars picture had at least one mark visible on it, and the later, larger images had many.

A drawing of the picture area and reseau marks is shown in Fig. 1. The reseau marks were spaced 1.8008 mm apart except for those around the edge where the spacing perpendicular to the edge was modified for frame-formatting purposes.

## 2. Image Distortions and Their Correction.

On the basis of uniform-illumination pictures taken during bench calibration of the systems, it was known that the recorded reseau mark locations in line-number and element-number (L,E) coordinates were not uniformly spaced but showed small, systematic departures from rectilinearity. These departures remained substantially constant throughout the tests, but varied somewhat with illumination intensity and shutter position during readout.

The first task in treating the data was thus to find the actual reseau mark locations in the flight pictures and, if sufficiently well-defined systematic behavior were found, to use the observed reseau pattern as a basis for geometric correction of the flight pictures.

All of the pictures were examined visually, the visible reseau marks were identified as to row and column (I,J), and a table of nominal (integral pixel) coordinates was made. A computer program was written which stored the local (10 x 10 pixel) neighborhood of each visible reseau mark of a picture and found the line-and element (L,E) coordinates of the darkest pixel in that neighborhood. Then, the DN values of the surrounding pixels were least-square fitted to a paraboloid of revolution

$$DN(L,E) = DNO + A*((L - XL)^2 + (E - YE)^2)$$

The fractional-pixel part of the mark location was taken as the real quantities (XL, YE) corresponding to the best fit.

The accuracy with which a given reseau mark in a given frame could be located was approximately 0.3 pixel rms, and the average over several frames was well within 0.1 pixel.

Because of a weak magnetic field associated with the spring steel shutter blade, the reseau grid was not the same for each picture. The shutter was of the flip-flop type, so that two different, but respectively constant, patterns were evident, corresponding to the two positions of the shutter during readout. These patterns differed by as much as 3 pixels at the edge of the frame, the greatest effect being a relative rotation of some 0.4 degree.

The reseau-mark-locating program thus yielded four tables of average mark locations - one for each spacecraft and shutter-blade orientation. The mark offsets varied smoothly from point to point on the vidicon target, and provided a good basis for correcting the individual picture distortions by interpolation.

Various possible schemes for utilizing the reseau shift data were considered, including a least-square polynomial fit in two-dimensions and step-wise linear, quadratic, and cubic interpolation. A bi-cubic "spline" interpolation formula seemed to have significant advantages in accuracy and economy and was the method actually used. The formulas are given in appendix A.

Using the bi-cubic interpolation formula, the pictures were transformed to a new format in which the reseau marks fell upon a precisely rectilinear grid having exactly 135 pixels between reseau marks (for those marks not lying along a picture edge). The corrected picture format had 770 lines of 935 elements each, and reseau marks fell at the element and line numbers given in Table 1. Fig. 1 shows this adopted standard reseau pattern. The curvilinear grid in this figure shows the offsets (magnified 22.5 X) of corresponding points in the original pictures. The grid lines were drawn by computer, using the bi-cubic spline interpolation scheme based upon the measured reseau mark shifts.

Table 1

Line and element numbers of Reseau Marks in corrected pictures

| Row | Line   | Column         | Element |
|-----|--------|----------------|---------|
| 1   | 32.11  | 1(L mask edge) | 7.29    |
| 2   | 120.00 | 2              | 65.00   |
| 3   | 255.00 | 3              | 200.00  |
| 4   | 390.00 | 4              | 335.00  |
| 5   | 525.00 | 5              | 470.00  |
| 6   | 660.00 | 6              | 605.00  |
| 7   | 747.89 | 7              | 740.00  |
|     |        | 8              | 875.00  |
|     |        | 9(R mask edge) | 932.71  |

MARINER 7 TOP SHUTTER  
RESIDUALS AFTER LEAST-SQUARES FIT

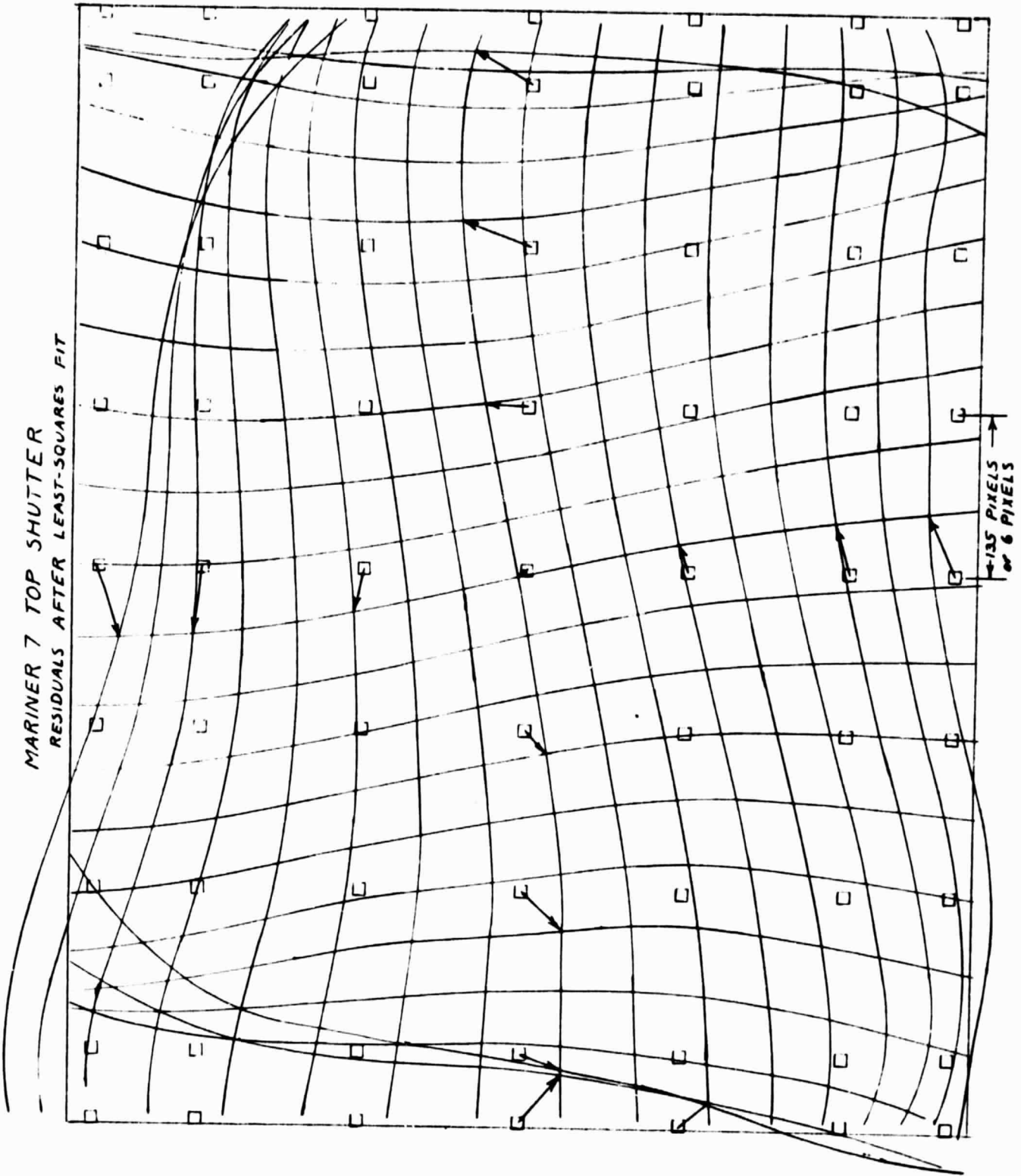


Figure 1



The transformation was carried out as follows: For each integral pixel location (LC, EC) of the corrected picture, non-integral line-and-element coordinates ( $L + \lambda$ ,  $E + \epsilon$ ) of the corresponding point in the "raw" picture were calculated by iteration, where  $0 \leq \lambda < 1$  and  $0 \leq \epsilon < 1$  are the fractional parts of the coordinates. A weighted DN value was assigned to the pixel by the formula

$$\begin{aligned} \text{DN}(\text{LC}, \text{EC}) = & (1 - \lambda)(1 - \epsilon)\text{DN}(\text{L}, \text{E}) \\ & + \lambda(1 - \epsilon)\text{DN}(\text{L} + 1, \text{E}) \\ & + (1 - \lambda)\epsilon\text{DN}(\text{L}, \text{E} + 1) \end{aligned}$$

This method introduces approximately one-half pixel of smearing on the average, which was considered acceptable.

The result to this point is that all pictures were transformed into a true rectilinear form, as if they had been taken by a distortion-free optical system. In the following, all references to picture coordinates are in the corrected system.

3. Limb Detection. The next step toward superimposability of images was to define the image location in each frame. (The spacecraft and camera platform orientations were known well enough to assure that the image would be inside the camera field, but pointing uncertainties of many pixels remained. The angular image orientation (roll) was sufficiently accurately known from spacecraft data that it was not deemed necessary to determine it from the image itself.)

The easiest problem was approached first - namely, to find the sharp edge of the planet image (limb). The approximate (L,E) coordinates of the extreme boundaries of each image were estimated by eye, using pictures with (L,E) grid lines superimposed by computer. Each image edge was then mapped into eight overlapping elongated "BLOCKS", each containing about  $45^\circ$  of the limb or terminator. Block coordinates were (L,E) coordinates for four of the blocks and were quasi-rectangular coordinates at  $45^\circ$  to (L,E) coordinates for the other four. The purpose of this procedure was to permit the use of a single, simple procedure for detecting the image edge.

The principal problem was to define the "edge" of the planet in a physically reasonable, operationally simple, and yet sufficiently sensitive and reproducible manner. Several criteria were devised and tested. All used

data averaged over a number of pixels "parallel" to the (computed) local limb so as to reduce noise. Five successive lines of data were averaged, using a suitable linear interpolation between pixels in a given line to accommodate the local "tilt" of the image edge. Each resulting line of data thus represented an "edge function" which ideally should start at sky-background level, rise rapidly as the edge is crossed, and quickly level off to the local disk intensity value inside the edge. Indeed, many actual cases showed just such behavior, but often there were also some complicating factors: a) Haze layers, which would show an irregular rise from sky to disk; b) the polar cap, which showed quite marked limb darkening; c) local disk markings, which often modified or confused the ideally expected behavior. Nevertheless, at almost all points two or more of the edge-defining criteria would give concordant results. Fig. 2 shows examples of edge functions taken from one image frame.

The edge functions tended to fall into four categories:

- 1) A sharp rise from near-zero DN values to a plateau, within a span of 4 or 5 pixels.
- 2) A more gradual rise over 5-20 pixels, sometimes with an intermediate maximum (haze layers).
- 3) A steep rise for 3-4 pixels, followed by a more gradual but substantial further rise (polar cap).
- 4) A gradual, irregular rise over many pixels (terminator and north-polar limb region).

Several criteria were devised for locating the sharp edge characterized by edge functions of the first type, to fractional - pixel accuracy: 1) A correlation procedure to match the observed edge profile with that expected on the basis of a plausible edge smearing-function was devised. A gaussian smearing function having approximately a 2-pixel FWHM was correlated with the first difference function of the edge function, and the (fractional-pixel) location of the maximum of the correlation was determined. 2) A definition of the location of the planet edge in the presence of a haze layer was the position of the innermost maximum of the correlation function used in 1) above. This criterion was not fully refined and tested under conditions where a clearly visible haze layer was present, and it sometimes gave wildly discordant results in those cases where it was tried. 3) A linear least-squares

7a

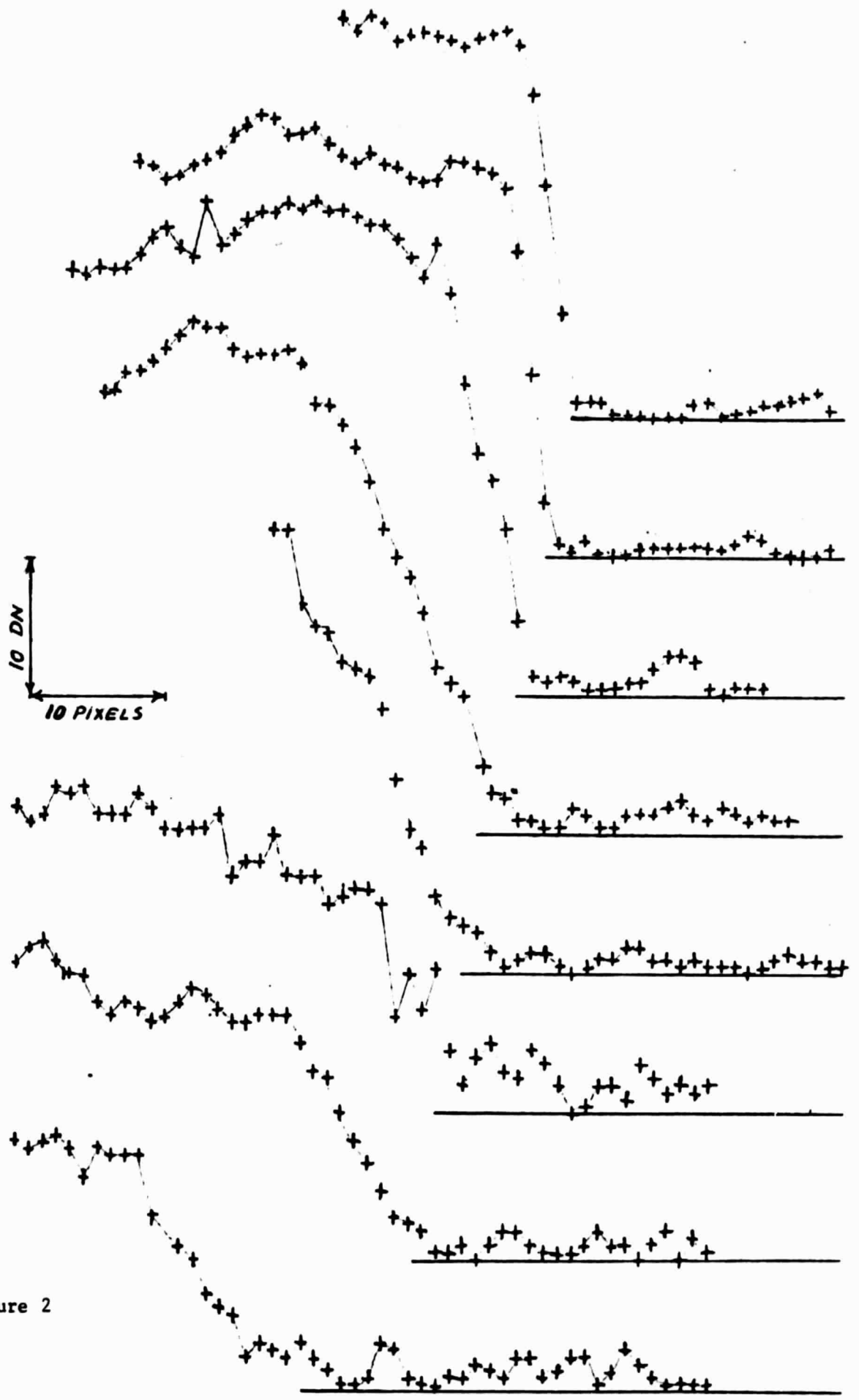


Figure 2

fit to a few consecutive points surrounding the maximum DN "jump", extrapolated to zero and the intercept point moved toward the planet by a fixed amount (approximately 1.25 pixel), gave another measure of the point of maximum slope. 4) Along the terminator and in certain other areas where it seemed appropriate, an extended linear or quadratic least-squares fit, similar to criterion 3) above, was used. In the case of a very gradual rise, the identification and rejection of "sky" background was a crucial part of the procedure. The simplest way to do this was to reject all data outside that point where any DN value was less than some threshold value.

The mutual consistency, and the sometimes systematic disagreement, of the various edge locators is shown in Fig. 3. Over most of the span, four out of five methods gave the same value within 0.2 pixel out of an image radius of about 100 pixels. Systematic departures of two of the methods are also seen, associated with the polar cap. The "gradual-rise" linear least squares fit systematically falls outside any of the other edge values, usually by about the expected "edge-smear" amount. All in all, the edge-locating procedures were considered to be of excellent accuracy wherever the edge was reasonably sharp, and of acceptable accuracy elsewhere, provided some judgement was used in selecting among the various methods for a given case.

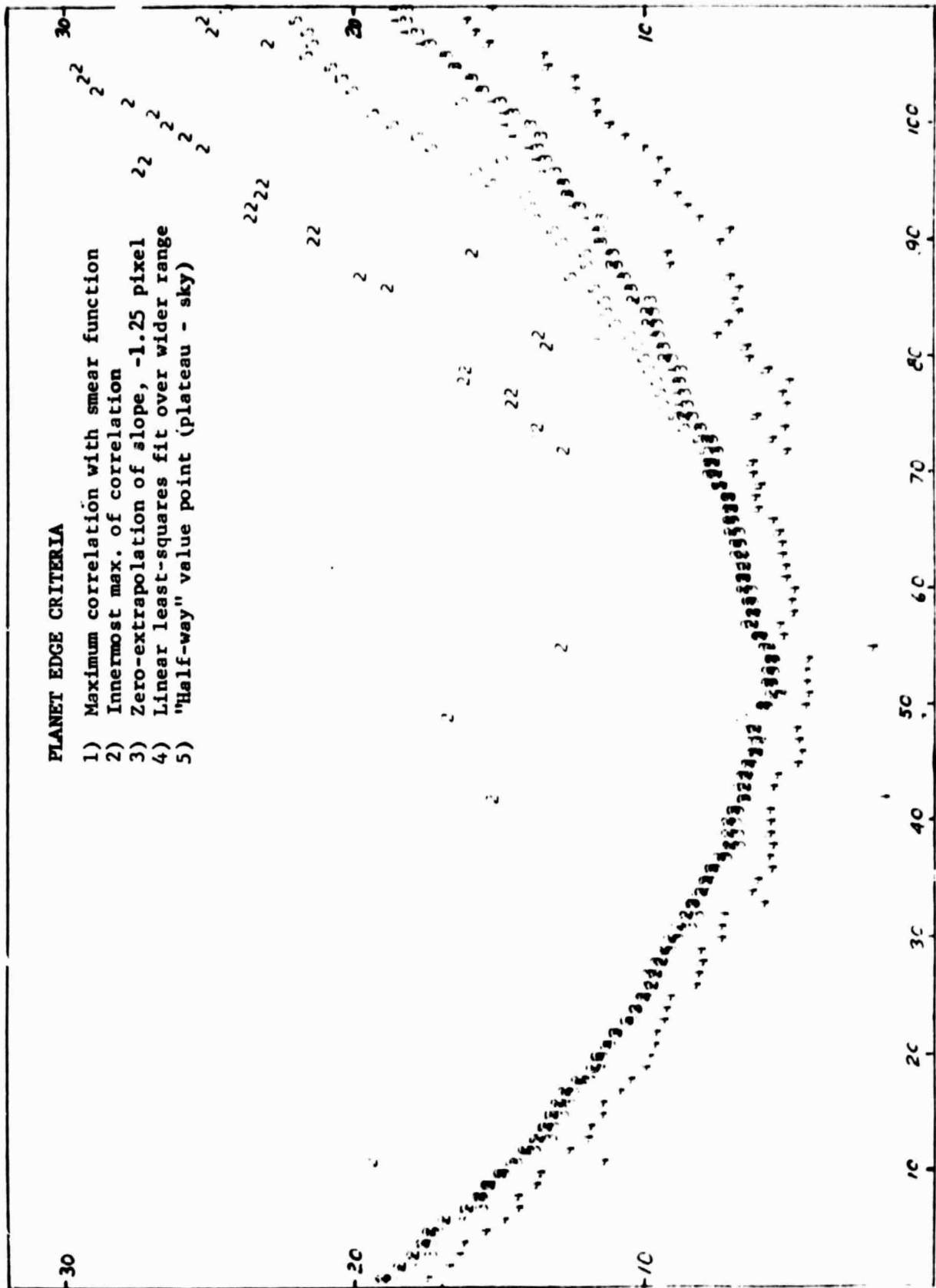
#### 4. Image Superposition.

Given suitable means of locating the bright limb and the terminator of the planet, the coordinates of the center of the planet can be estimated. If the full disc were illuminated, this would simply require a fit to an ellipsoidal arc of known "tilt" in the frame. The  $26^\circ$  phase angle of the solar illumination was a complication, but by use of a suitable side-illuminated-ellipsoid model and careful assignment of relative weights to limb and terminator data, a good fit could still be expected because of the large number of available points and the small number of parameters.

Before it was decided to abandon the objective of finding accurate values for the polar and equatorial radii of Mars, the question of how to deal with systematic errors was examined. It was reasonable to believe that the camera properties were not changing with time during the few-day far-encounter period. The image "smear" in pixels, from all instrumental causes, should be independent of image size. Thus a given systematic effect, related

PLANET EDGE CRITERIA

- 1) Maximum correlation with smear function
- 2) Innermost max. of correlation
- 3) Zero-extrapolation of slope, -1.25 pixel
- 4) Linear least-squares fit over wider range
- 5) "Half-way" value point (plateau - sky)



PIXELS ALONG LIMB

Figure 3

to the camera point-spread function, should be constant (in pixels) and should have a greater effect on small images than on large ones. Data from one spacecraft, analyzed in this way, did seem to show qualitatively such an effect, but no reliable quantitative results were obtained.

Even though reliable independent radius values were not obtained, it was still felt worthwhile to attempt a superposition of frames to yield a quasi-mercator strip-map of the lower latitudes. Two alternative procedures were devised. In the first, coordinates of the planet center for a given image, deduced from a best-fit of limb and terminator data to a constant ellipsoidal model for the Mars figure, were used to define the image point corresponding to the ephemeris latitude and longitude of the planet center based on spacecraft orbital and orientation data as it applied to that image. Then, using the appropriate image scale, a matrix of standard latitudes and longitudes at one of three chosen linear resolutions, was filled with (interpolated) DN values from that image. These partial mappings were called "strips". Two strips were formed from each image - one centered somewhat east of the planet center, and the other an equal distance (in longitude) west of the planet center. The purpose of the two mappings at different local solar times was to search the resulting maps, later, for evidences of diurnal cloud, frost, haze, or other albedo effects. This is still a good idea and could give valuable results.

The strips corresponding to a given local time, from the full set of images, constituted an overlapping set which could be combined directly, point by point, by simple averaging.

The second procedure, for producing a high-resolution map, started from the strip data just discussed. However, on the assumption that the adopted center location of each image might be slightly in error, a procedure for improving the centering was set up: for each given strip, a correlation function for this strip with the corresponding averaged data from all other strips contributing to the same area was to be evaluated, and the maximum of the correlation function was to be found by inspection as well as by analytic means. Using the individual corrections so obtained, new strips were to be formed from the images and the process repeated if necessary.

The above procedure was carried through to the point of producing a "raw" strip map, which showed considerable promise. (Fig. 4) Programs to evaluate correlations of "strip" with the "map-minus-strip" were written and debugged,



but corrected centers were not obtained.

#### SUMMARY

Procedures were successfully devised to combine data from separate, uncorrected pictures in a coherent way so as to produce an averaged data set having finer resolution and better signal-to-noise value than any of the original images. It was demonstrated that images can be corrected for geometric distortions; that they can be located in a frame; and that rectified strips produced from such images can be combined: all within an accuracy of from about a tenth to about half a pixel.



A POLYNOMIAL INTERPOLATION EXPRESSION FOR A  
SMOOTH FUNCTION DEFINED ON A RECTANGULAR POINT GRID

R. B. Leighton

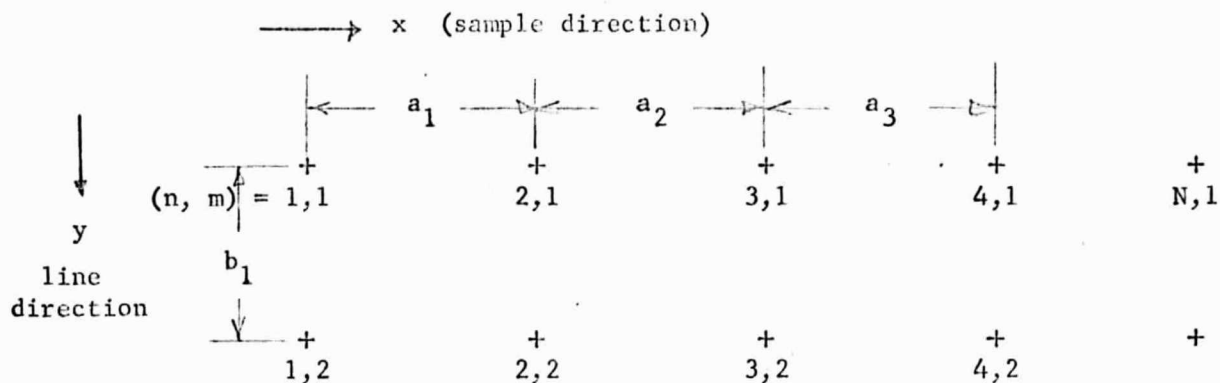
18 July 1969

Corrected 23 March 1970, 20 February 1976

Given a rectangular grid of points whose coordinates are  $x_n, y_m$  where

$n = 1, 2, \dots, N$  and  $m = 1, 2, \dots, M$

( $n =$  sample number,  $m =$  line number)



let the x-spacing of the points be  $a_r = x_{r+1} - x_r$   $r = 1, 2, \dots, N-1$

and the y-spacing be  $b_s = y_{s+1} - y_s$   $s = 1, 2, \dots, M-1$ .

Let  $f(x,y)$  be a function whose value  $f_{nm}$  is known only at the points  $x_n, y_m$ . We wish to approximate this function by interpolation. We do this by developing a polynomial expression for  $f(x,y)$  which will be used within a given rectangle whose corners are at  $(x_n, y_m), (x_{n+1}, y_m), (x_n, y_{m+1}), (x_{n+1}, y_{m+1})$ . This polynomial joins on to the corresponding expressions in neighboring domains in such a way that  $f$  and its first derivative are continuous across the boundaries.

We must first define the derivatives of  $f$  at the corner points of each rectangle. For such points interior to the array we do this by passing a parabola through three successive points. The resulting slopes are

$$f_{nm}^x = \left. \frac{\partial f}{\partial x} \right|_{\substack{x = x_n \\ y = y_m}} = \frac{a_{n-1}^2 (f_{n+1,m} - f_{n,m}) + a_n^2 (f_{n,m} - f_{n-1,m})}{a_n a_{n-1} (a_n + a_{n-1})}$$

and

$$f_{nm}^y = \left. \frac{\partial f}{\partial y} \right|_{\substack{x = x_n \\ y = y_m}} = \frac{b_m^2 (f_{n,m+1} - f_{n,m}) + b_{m-1}^2 (f_{n,m} - f_{n,m-1})}{b_m b_{m-1} (b_m + b_{m-1})}$$

Along the outermost edges of the entire grid, the derivatives perpendicular to the edge at a grid point may be defined as the slope of a parabola through the three points including the edge. (Other definitions may be used if some special symmetry is present or if there is other information.) These slopes are:

$$f_{1m}^x = f_{1,m} \left( -\frac{1}{a_1} - \frac{1}{a_1+a_2} \right) + f_{2m} \left( \frac{1}{a_1} + \frac{1}{a_2} \right) + f_{3m} \left( \frac{-a_1}{a_2(a_1+a_2)} \right)$$

$$f_{Nm}^x = f_{N-2,m} \left( \frac{a_{N-1}}{a_{N-2} (a_{N-2} + a_{N-1})} \right) - f_{N-1,m} \left( \frac{1}{a_{N-2}} + \frac{1}{a_{N-1}} \right) + f_{N,m} \left( \frac{1}{a_{N-1}} + \frac{1}{a_{N-2} + a_{N-1}} \right)$$

$$f_{n1}^y = f_{n,1} \left( -\frac{1}{b_1} - \frac{1}{b_1+b_2} \right) + f_{n2} \left( \frac{1}{b_1} + \frac{1}{b_2} \right) + f_{n3} \left( \frac{-b_1}{b_2(b_1 + b_2)} \right)$$

$$f_{nM}^y = f_{n,M-2} \left( \frac{b_{M-1}}{b_{M-2} (b_{M-2} + b_{M-1})} \right) - f_{n,M-1} \left( \frac{1}{b_{M-2}} + \frac{1}{b_{M-1}} \right) + f_{n,M} \left( \frac{1}{b_{M-1}} + \frac{1}{b_{M-2} + b_{M-1}} \right)$$

With all displacements and slopes now defined, the polynomial expression

$$\begin{aligned}
 f(x,y) = & f_{00} (1 + 2X) (1-X)^2 (1+2Y) (1-Y)^2 \\
 & + f_{01} (1+2X) (1-X)^2 Y^2 (3-2Y) \\
 & + f_{10} X^2 (3-2X) (1+2Y) (1-Y)^2 \\
 & + f_{11} X^2 (3-2X) Y^2 (3-2Y) \\
 & + a_n f_{00}^x X(1-X)^2 (1+2Y) (1-Y)^2 \\
 & + a_n f_{01}^x X(1-X)^2 Y^2 (3-2Y) \\
 & - a_n f_{10}^x X^2(1-X) (1+2Y) (1-Y)^2 \\
 & - a_n f_{11}^x X^2(1-X) Y^2 (3-2Y) \\
 & + b_m f_{00}^y (1+2X) (1-X)^2 Y (1-Y)^2 \\
 & - b_m f_{01}^y (1+2X) (1-X)^2 Y^2 (1-Y) \\
 & + b_m f_{10}^y X^2 (3-2X) Y (1-Y)^2 \\
 & - b_m f_{11}^y X^2 (3-2X) Y^2 (1-Y)
 \end{aligned}$$

meets the desired conditions, where

$$f_{00} = f_{nm}, \quad f_{01} = f_{n, m+1} \quad \text{etc.}$$

and 
$$X = \frac{x-x_n}{a_{1i}}, \quad Y = \frac{y-y_m}{b_m}$$