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STUDY OF LH₂ FUELED SUBSONIC PASSENGER TRANSPORT AIRCRAFT

by G. D. Brewer & R. E. Morris

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FOREWORD

This is the final report of work performed as an addendum to a previously completed study of hydrogen fueled subsonic transport aircraft (Reference 1). This work was performed under Modification No. 4 of Contract NAS 1-12972 for NASA - Langley Research Center. The report is documentation of the substance of work performed during the period 20 June through 20 December, 1975.

The study was performed within the Advanced Design Division of the Science and Technology Organization at Lockheed - California Company, Burbank, California. G. Daniel Brewer was study manager and Robert E. Morris was project engineer. Other participants were

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All computations were performed in U.S. Customary units and then converted to S.I. units.

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NOMENCLATURE

AR	=	Aspect Ratio
ATA	=	Air Transport Association
b	=	Wing Span
BPR	=	Bypass Ratio
Btu	=	British Thermal Unit
C_v	=	Velocity Coefficient
CPR	=	Compressor Pressure Ratio
DOC	=	Direct Operating Cost
DTAM	=	Deviation from std. ambient Temperature
FAR	=	Federal Air Regulation
F_N	=	Net Thrust
FPR	=	Fan Pressure Ratio
GH_2	=	Gaseous Hydrogen
HP	=	High Pressure
Jet A	=	Conventional Hydrocarbon Fuel

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NOMENCLATURE (Continued)

KEAS	=	Knots Equivalent Airspeed
L/D	=	Lift-to-Drag Ratio
LH ₂	=	Liquid Hydrogen
LP	=	Low Pressure
M	=	Mach Number
MAC	=	Mean Aerodynamic Chord
OPR	=	Overall Pressure Ratio
Pax.	=	Passenger
Sw	=	Wing Reference Area
SFC	=	Specific Fuel Consumption
SLS	=	Sea Level Static
T/W	=	Thrust to Weight Ratio
TIT	=	Turbine Inlet Temperature
t_c	=	Wing Thickness Ratio
\bar{v}	=	Tail Volume Coefficient
V _{app}	=	Landing Approach Velocity

NOMENCLATURE (Continued)

- V_o = Flight Velocity
- V_r = Takeoff Rotate Velocity
- V_2 = Takeoff Safety Speed
- V_s = Stall Velocity
- $W_a \frac{\sqrt{\theta_{T_2}}}{\delta_{P_2}}$ = Engine Corrected Airflow
- W_g = Gross Weight
- W_{pod} = Engine Pod Weight
- W/S = Wing Loading (weight/wing area)
- δ_{P_2} = Delta $P_2 = P_{T_2}$ PSIA/14.7
- θ_{T_2} = Theta $T_2 = T_{T_2}$ °K/288.2

STUDY OF LH₂ FUELED SUBSONIC PASSENGER
TRANSPORT AIRCRAFT

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SUMMARY

The work reported herein is supplemental to an original study performed for NASA - Langley Research Center in 1974 (Reference 1). In that study two different LH₂ passenger aircraft designs were established, one of which carried the fuel within the fuselage in tanks located both forward and aft of the passenger compartment; the other, in tanks mounted on short pylons above the wing at about midspan. Versions of these internal and external tank LH₂ airplane designs were configured to carry 400 passengers two different ranges: 5560 km (3000 n.mi.) and 10,190 km (5500 n.mi.).

The present study extended the scope of missions considered for the LH₂ fueled aircraft as follows:

130 passengers	2780 km	(1500 n.mi.)
200 passengers	5560 km	(3000 n.mi.)
400 passengers	9265 km	(5000 n.mi.) radius

As noted, the longer range mission was specified as a radius. The aircraft was designed to fly 9265 km, land, and return to point of origin without refueling, carrying full design payload both directions and providing for specified reserve fuel for both landings.

Both internal tank and external tank LH₂ designs were defined for the short and medium range missions. Only the internal tank concept was considered for the long range requirement. For all three missions, equivalent designs of conventionally fueled aircraft were identified to provide a basis for comparison and evaluation.

One of the objectives of the work was to determine if the external tank LH₂ design concept would begin to show design advantages, or at least design equivalence, with the internal tank concept at the low fuel load missions. It apparently does not. Even for the short range mission the external tank design was clearly not competitive. This stems from the dual, but incompatible, needs to design the external tanks with a high fineness ratio for aerodynamic acceptability on the one hand, but with a low surface-to-volume ratio on the other to achieve low heat leak with minimum insulation thickness and weight. On small aircraft the external tanks account for an increasing percentage of total aircraft drag.

A summary of selected data for the preferred, internal tank LH₂ aircraft and for the corresponding Jet A fueled designs for all three of the subject missions is presented in the table on page 3.

One of the objectives of the study was to determine if a crossover point could be predicted, i.e., a design mission requiring such a small amount of Jet A fuel that an equivalent LH₂ fueled aircraft would offer no advantage. The short range mission of this study appears to be at or near that crossover point. The internal tank LH₂ aircraft and the corresponding Jet A design are virtual standoffs. Since the LH₂ aircraft designed for the longer range, larger payload missions do show advantage over corresponding aircraft, it is presumed that for a mission requiring even less energy than the short range mission of this study, the Jet A airplane would be preferred.

As in the previous study, the results show that use of LH₂ fuel provides significant advantages in long range aircraft. The more energy required to perform the mission, the greater the advantage to be gained by using a high energy fuel. The long range LH₂ aircraft of this study are lighter; require smaller wing area and shorter span but larger, longer fuselages; use smaller engines; can operate from shorter runways; and use 25 percent less energy to perform the mission. Further, the LH₂ airplane would cost less both to develop and to produce. A differential of \$1.00 more per GJ ($\$1.05/10^6$ Btu) can be paid for LH₂, relative to a current price

S.I. Units

		Short Range [130 Passengers] 2780 km		Medium Range [200 Passengers] 5560 km		Long Range [400 Passengers] 9285 km radius	
		LH ₂	Jet A	LH ₂	Jet A	LH ₂	Jet A
Gross Weight	kg	44,800	49,300	81,400	88,400	266,400	450,200
Total Fuel Wt.	kg	3,380	8,940	9,480	27,720	68,500	238,000
Operating Empty Wt.	kg	28,300	27,400	51,900	50,700	158,100	172,600
Thrust/Weight	N/kg	3.43	3.43	3.33	2.75	2.65	1.96
Number of Engines	-	2	2	4	4	4	4
Thrust per Engine	N	75,600	84,100	66,700	68,100	175,300	221,100
Wing Area	m ²	84.7	85.3	148.8	154.8	486	662
Span	m	29.3	30.8	37.5	38.7	68.3	85.3
Fuselage Length	m	42.7	34.4	52.7	44.2	77.4	68.6
FAR T.O. Distance	m	2,410	2,430	1,640	2,432	2,106	3,650
Price per Aircraft	\$10 ⁶	7.85	7.51	13.95	13.33	38.90	40.0
Noise Sideline	EPNdB	86	86	86	86	94	93
Flyover	EPNdB	79	79	82	86	93	100
Energy Utilization	$\frac{\text{kJ}}{\text{Seat km}}$	763	734	631	876	950	1,210

U.S. Customary Units

		Short Range [130 Passengers] 1500 n.mi.		Medium Range [200 Passengers] 3000 n.mi.		Long Range [400 Passengers] 5000 n.mi. radius	
		LH ₂	Jet A	LH ₂	Jet A	LH ₂	Jet A
Gross Weight	lb	98,300	108,700	179,500	216,900	587,400	992,500
Total Fuel Wt.	lb	7,400	19,700	20,900	61,100	150,900	524,000
Operating Empty Wt.	lb	62,300	60,400	114,500	111,900	348,500	380,500
Thrust/Weight	-	0.35	0.35	0.34	0.28	0.27	0.20
Number of Engines	-	2	2	4	4	4	4
Thrust per Engine	lb	17,000	18,900	15,000	15,300	39,400	49,600
Wing Area	ft ²	912	929	1,602	1,664	5,020	7,125
Span	ft	96	101	123	127	224	280
Fuselage Length	ft	140	113	173	145	254	225
FAR T.O. Distance	ft	7,890	7,970	5,380	7,980	6,910	11,970
Price per Aircraft	\$10 ⁶	7.85	7.51	13.95	13.33	38.90	40.00
Noise Sideline	EPNdB	86	86	86	86	94	93
Flyover	EPNdB	79	79	82	86	93	100
Energy Utilization	$\frac{\text{BTU}}{\text{Seat n.mi.}}$	1,340	1,290	1,460	1,540	1,870	2,120

for Jet A, and still have equal direct operating cost. The LH₂ design is 6 EPNdB quieter in flyover noise, but slightly noisier in sideline and approach compared to the Jet A counterpart.

Advantages for the LH₂ aircraft not reassessed in this supplementary study, but which nevertheless pertain, are the significant reduction in noxious exhaust products reported in Reference 1, and the fact that aircraft designed for initial operation in 1990-1995 will have normal service life long after Jet A - type fuel is expected to become increasingly unavailable and expensive around the world.

1. INTRODUCTION

This work is an addendum to a study performed in 1974 for NASA-Langley Research Center to evaluate the feasibility, practicability, and desirability of using liquid hydrogen (LH₂) as fuel in subsonic transport aircraft. NASA CR-132558 and 132559 (Reference 1), dated January 1975, are the Summary and Final reports, respectively, of the original study. That work involved investigation of both passenger and cargo type aircraft. The passenger vehicles were all capable of carrying 400 passengers plus appropriate cargo for a total of 36,300 kg (88,000 lb) of payload. Aircraft designed for two ranges, 5560 km (3000 n.mi.) and 10,190 km (5500 n.mi.) and for cruise speeds of Mach 0.80, 0.85, and 0.90 were evaluated. In addition, aircraft capable of carrying 600 and 800 passengers were also investigated for both ranges but for only Mach 0.85 cruise speed. Cargo aircraft capable of carrying 56,700 kg (125,000 lb) and 113,400 kg (250,000 lb) were designed for ranges of 5560 km (3000 n.mi.) and 10,190 km (5500 n.mi.), respectively. All cargo aircraft were designed for Mach 0.85 cruise speed.

In the present study, the payload and range spectrum of the passenger aircraft was enlarged to involve aircraft of the following capability, all designed to cruise at Mach 0.85:

	Passengers	Range	
		km	(n.mi.)
Short range mission	130	2780	(1500)
Medium range mission	200	5560	(3000)
Long range mission	400	9265 radius	(5000) radius

For the short and medium range missions, LH₂ fueled aircraft using both internal and external tank design concepts illustrated by the artist's rendering in Figure 1, taken from Reference 1, were parametrically evaluated.

The long range mission was different in that the range requirement was stated as an unrefueled radius capability. The aircraft was intended to fly

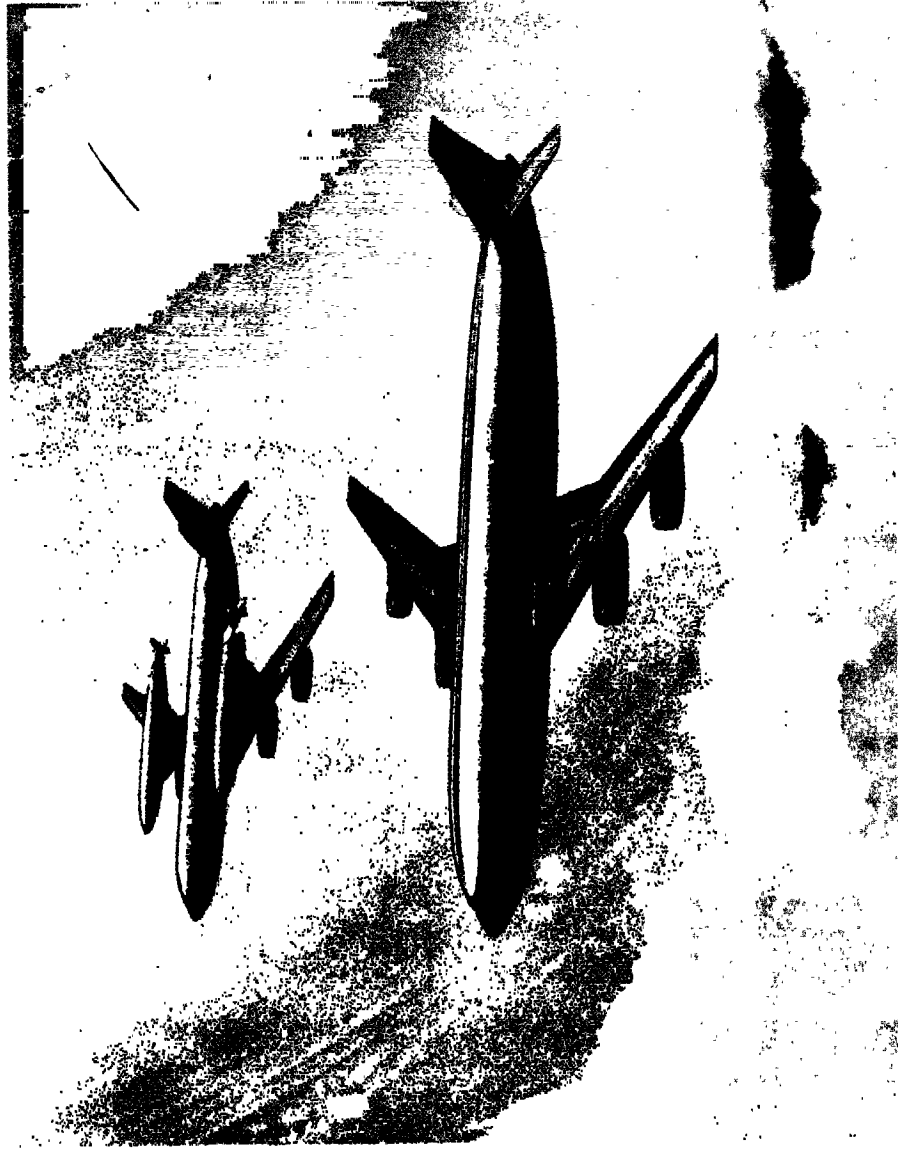


Figure 1. Illustration of External and Internal Tank LH₂ Aircraft

9265 km (5000 n.mi.), land, and then return to the point of origin unrefueled with full payload and with full allowances for reserve fuel for both landings. For this mission, only the internal tank design of LH₂ fueled aircraft was investigated.

For all missions, as in the case of the original study, reference aircraft using conventional (Jet A) fuel were designed to the same guidelines and technology to provide a basis for valid comparison.

All aircraft incorporate such advanced technology concepts as are forecast to be available for designs which might be ready for initial operational use in 1990-1995.

Since the subject work is a "follow-on" to an earlier study and uses the basic LH₂ airplane design concepts developed and described in Reference 1, only revisions and modifications to the designs and the results derived therefrom are reported in full in this report. The reader interested in the background leading to derivation of the original airplane design concepts should refer to NASA CR-132559 (Reference 1).

2. TECHNICAL APPROACH

This investigation expanded the matrix of passenger aircraft missions which were studied under the original contract (Reference 1). The complete list of aircraft evaluated herein is shown in Table I.

As noted, the long range aircraft were designed to fly 9256 km (5000 n.mi.) carrying full allowance for reserve fuel (per ATA international definition), land, takeoff without refueling, fly 9265 km (5000 n.mi.) and land with final reserves calculated on the basis of the airplane weight at the end of cruise for the second leg.

TABLE I. AIRCRAFT DESIGNS REQUIRED

Aircraft Number	Passenger Load	Range		Fuel	Configuration
		km	(n.mi.)		
<u>Short Range</u>					
1	130	2780	(1500)	LH ₂	Internal Tank
2	130	2780	(1500)	LH ₂	External Tank
3	130	2780	(1500)	Jet A	Conventional
<u>Medium Range</u>					
4	200	5560	(3000)	LH ₂	Internal Tank
5	200	5560	(3000)	LH ₂	External Tank
6	200	5560	(3000)	Jet A	Conventional
<u>Long Range</u>					
7	400	9265 radius	(5000) radius	LH ₂	Internal Tank
8	400	9265 radius	(5000) radius	Jet A	Conventional

Guidelines used in the present study were the same as those which served as a basis for the work in the original study (Reference 1) with the exception that the short and medium range aircraft used reserve fuel quantities as defined by the ATA for domestic flights. The long range aircraft continued to use the ATA international reserve definition. The same differences in basis for calculating direct operating costs applied; the short and medium range aircraft were treated as domestic flights per the 1967 ATA equations, while the long range aircraft were treated as international carriers. For convenience, Table II presents the complete list of updated guidelines which were used in the present study. It should be noted that the allowable runway length for the long range aircraft was extended to 3600 m (12,000 ft). The basis for this revision is discussed in Section 6.

The technical approach employed was essentially the same as that described in Reference 1 for the original study. Preliminary sizing and conceptual design studies established baseline sizes, weights, and configurations for each of the eight aircraft. The resulting preliminary configuration drawings were then used as a basis for assessment of

- stability and control requirements
- structural and weight relationships
- drag characteristics
- propulsion requirements
- tank insulation requirements

as required for the various aircraft.

The results of these analyses, plus the preliminary sizing data, provided input to the ASSET (Advanced System Synthesis Evaluation Technique) computer program for parametric determination of preferred vehicle design characteristics. The performance capability, weight, and cost of aircraft designs derived for each of the specified set of requirements were determined by detail analysis of the carpet-type Autoplots produced from ASSET printout data. The criterion used as an ultimate basis for selecting

TABLE II. BASIC GUIDELINES

Fuel: Liquid Hydrogen (assumed available at airport for this study)	
Initial Operational Capability: 1990-95	
Advanced Aircraft Technologies:	
<ul style="list-style-type: none"> ● Supercritical aerodynamics ● Composite materials ● Active controls ● Terminal area features 	
Advanced Engines: Contractor-derived performance for both LH ₂ and Jet A fueled turbofans	
Noise Goal: 5.18 km ² (2 mi ²) area for 90 EPNdB contour (sum of takeoff + approach)	
Emission Limit Goals:	
● Ground Idle	CO 14 gm/kg fuel burned UHC 2 gm/kg fuel burned
● Takeoff Power	NO _x 13 gm/kg fuel burned Smoke SAE 1179 Number 25
Landing and Takeoff: 32.2°C (90°F) day, 304.8 m (1000 ft) altitude. 2410 m (8000 ft) runway for short and medium range aircraft. 3660 m (12,000 ft) runway for long range aircraft.	
Fuel Reserves: ATA guidelines (Reference 2)	
<ul style="list-style-type: none"> ● Use domestic definition for short and medium range aircraft ● Use international definition for long range aircraft 	
Direct Operating Cost:	
● Utilization:	Short Range - 3300 hrs/yr Medium Range - 3600 hrs/yr Long Range - 7000 hrs/yr
● 1967 ATA equations	international basis for long range aircraft. domestic basis for short and medium range aircraft.
● 1973 Dollars	
● 350 aircraft production base	
● Baseline fuel costs	
	LH ₂ = \$2.85/GJ (\$3/10 ⁶ Btu = 15.48¢/lb)
	Jet A = \$1.90/GJ (2/10 ⁶ Btu = 24.8¢/gal = 3.68¢/lb)

preferred vehicle design characteristics was minimum direct operating cost (DOC). Final design three-view general and interior arrangement drawings of each of the eight aircraft were then made to reflect the results of the analysis. Noise levels for preferred LH₂ aircraft and the Jet A counterpart for each mission were then determined.

The characteristics of the eight aircraft were compared to the extent possible. Since this study was simply an evaluation of a matrix of aircraft designed to perform specified payload/range combinations, and was not planned specifically as a study to determine performance trends, there was little which could be concluded by comparing aircraft of the various missions. Comparisons were basically limited to evaluating internal tank versus external tank LH₂ designs within each of the three range categories, and then comparing the preferred LH₂ design with the corresponding Jet A airplane. The only exception to this was an opportunity to establish a three-point curve and thus provide a basis for comparison between range categories involving the 400 passenger aircraft. Aircraft from the long range mission of the present study were correlated with final design 400 passenger aircraft of the original study (Reference 1). In order to make this comparison valid the conventional oneway range capability of the aircraft from the current study were determined, as contrasted with their mission radius capability.

3. TECHNOLOGY MODIFICATIONS

3.1 Propulsion

The high bypass ratio turbofan engine data developed for the original LH₂ subsonic aircraft study (Reference 1) were based on predictions of component efficiencies and weight for advanced (1985-1990) state-of-the-art technology. The baseline engine size for that study was set at 155.7 kN (35,000 lb) for the sea level static (SLS) design point. This was achieved with a 1.51 fan pressure ratio (FPR) and a 35.0 overall pressure ratio (OPR). The engine data used was estimated to be scaleable to approximately 70 percent of the base engine size without changes in component efficiencies or overall cruise specific fuel consumption (SFC).

The same engine data were used in the present study, within limits of scale. For a description of the basis for derivation of the point design engine cycle parameters, and for a tabulation of the engine design and performance characteristics, see Section 3.2, starting on Page 30, Reference 1.

In addition to the baseline engine, the current study required that engine data be developed for smaller aircraft which would otherwise require scaling the baseline engines to approximately 35-45 percent. Such scaling would obviously result in some degradation of component efficiencies and, therefore, overall engine performance. This is basically due to the effects of reducing the size of the high pressure (HP) module of the engine. Specifically, the problem is related to the ratio of the HP compressor and turbine blade tip clearances to the blade height becoming relatively large compared to the baseline engine size - thereby making the originally assumed HP rotor pressure ratios and component efficiencies very difficult to achieve.

Because of this size (efficiency) problem, a new baseline engine cycle was defined for the smaller aircraft. It was sized to produce 53.4 kN (12,000 lb) thrust (SLS) and has a more moderate overall pressure ratio of 25.0, achieved with the same 1.51 FPR and a 16.67 compressor pressure ratio (CPR). The average pressure rise per axial stage would be approximately the

same (1.37) as the large engine, however, only nine axial stages are required to achieve the lower compressor pressure ratio. The estimated polytropic efficiency for the design point HP compressor of such a configuration is 90 percent (decreased from 92 percent), and the estimated turbine adiabatic efficiency is 89.5 percent (decreased from 91 percent) to account for size effects at the lower design pressure ratio.

The small engine design point cycle characteristics are presented in Table III for both the LH₂ and Jet A fueled engines. Some weight and dimensional characteristics of a typical installation of the 53.4 kN (12,000 lb) thrust size engine are shown in Tables IV and V. Table IV presents the wing pod weight buildup and Table V defines the nacelle dimensions. Nacelle scaling, resulting from small engine thrust perturbations, are referenced to the 53.4 kN (12,000 lb) thrust size and scaled with the equations provided in Table V.

The reduction in overall engine pressure ratio from 35.0 to 25.0 results in a 4.5 percent increase in cruise specific fuel consumption (SFC) and the decrease in HP component efficiency increases the SFC an additional 1.5 percent. Therefore, the total cruise SFC increase for both the LH₂ and Jet A fueled engines is approximately 6 percent, relative to the large thrust engine. A typical cruise SFC comparison for the LH₂ fueled engines is shown in Figure 2. All rated power thrust levels were scaled directly by the thrust change.

3.2 Hydrogen Tankage

The wide range of sizes of aircraft investigated in this study necessitated a review of the work done on hydrogen tankage in the previous contract (Reference 1). In particular, the smaller aircraft were examined with regard to tank, insulation, and cover weights as the tanks (internal and external)

TABLE III. SMALL ENGINE DESIGN POINT DATA, SEA LEVEL STANDARD - STANDARD DAY

I. Base Size Engine	Hydrogen Fueled		Jet A Fueled	
Installed Net Thrust	53.4 kN	(12,000 lb)	53.4 kN	(12,000 lb)
Installed S.F.C.	0.086 kg/hr/daN	(0.100 lb/hr/lb)	0.292 kg/hr/daN	(0.296 lb/hr/lb)
Turbine Inlet Temperature	1416°C	(3040°R)	1416°C	(3040°R)
Bypass Ratio		12.8		10.8
Overall Pressure Ratio				
Jet Exhaust Velocity	254.5 m/sec	25.0 (836 ft/sec) (V _j FRI & V _j duct matched @ SLS)	254.5 m/s	25.0 (836 ft/sec)
II. Fan Design				
Stages		1		1
Airflow - $W_a \sqrt{\theta T_2 / \delta P_2}$	212 kg/sec	(468 lb/sec)	212 kg/sec	(468 lb/sec)
Pressure Ratio		1.51		1.51
Polytropic Efficiency		91%		91%
Diameter	1.26	(149.6 in.)	1.26 m	(149.6 in.)
Tip Velocity	249 m/sec	(817 ft/sec)	249 m/sec	(817 ft/sec)
Fan Face Mach No.		0.56		0.56
Hub/Tip Ratio		0.36		0.36
III. Compressor Design				
Compressor Pressure Ratio		16.7		16.7
Polytropic Efficiency		90.0%		90.0%
Airflow	15.2 kg/sec	(33.4 lb/sec)	17.8 kg/sec	(39.3 lb/sec)
IV. Combustor				
Efficiency		100%		100%
Total Pressure Loss		4.5%		4.5%
V. High Pressure Turbine				
Pressure Ratio		3.2		3.8
Stages		2		2
Adiabatic Efficiency		89.5%		88.5%
Cooling Air		0		5%
VI. Low Pressure Turbine				
Pressure Ratio		6.5		6.4
Stages		4		4
Adiabatic Efficiency		91%		91%
Cooling Air		0		0
VII. Nozzle Design				
Configuration		Coplanar, fixed convergent nozzle		Same
Performance - (Vel. Coef.)				
A. Prin wry C _y		0.995		0.995
B. Fan C _y		0.995		0.995
VIII. Acoustic Treatment				
A. Inlet		{ Variable geometry throat - Throat Mach = 0.8 during takeoff and approach, inlet wall treatment }		Same
B. Exhaust -				
1. Fan Duct		All treatment on both core engine and outer wall, one treated duct ring		Same
2. Primary		Wall treatment		Same
IX. Nozzle Geometry				
Maximum Diameter	1.26 m	(62 in.)		
Overall Length	4.22 m	(168 in.)		
Inlet Highlight Diameter	1.26 m	(51 in.)		Same
Inlet Throat Diameter	1.17 m	(46 in.)		
Cruise Throat Mach Number		0.73		

TABLE IV. SMALL ENGINE PROPULSION SYSTEM WEIGHT

Base Thrust = 53.4 kN (12,000 lb) (SLS, Installed)

TIT = 1416°C (3040°R), OPR = 25.0

Fan Pressure Ratio = 1.51

Item	kg	lb
Bare Engine	839.2	1850
Accessories and Gear Box	74.8	165
Inlet, Variable Geometry	156.5	345
Mounting Brackets and Pylon Splitter Fairing	31.8	70
Nacelle	154.2	340
Gas Generator Cowl and Tail Pipe	79.4	175
Fan Duct Acoustic Ring	43.1	95
Thrust Reverser	97.5	215
Total Pod Weight (per Engine)	1476.5	3255

TABLE V. SMALL ENGINE NACELLE DESIGN CHARACTERISTICS

Base Thrust = 53.4 kN (12,000 lb) (SLS, Installed)

Fan Hub/Tip Ratio	= 0.35
Fan Tip Diameter	= 1.26m (49.6 in.)
Max Nacelle Diameter	= 1.58m (62.2 in.)
Max Nacelle Length	= 4.22m (168.1 in.)
<u>NACELLE SCALING DATA</u>	
WT. POD	= $WT_{POD(REF)} \left(\frac{F_{N_{SLS}}}{F_{N_{SLS(REF)}}} \right)^{1.07}$
DIA.	= $DIA_{(REF)} \left(\frac{F_{N_{SLS}}}{F_{N_{SLS(REF)}}} \right)^{0.50}$
LENGTH	= $LENGTH_{(REF)} \left(\frac{F_{N_{SLS}}}{F_{N_{SLS(REF)}}} \right)^{0.45}$

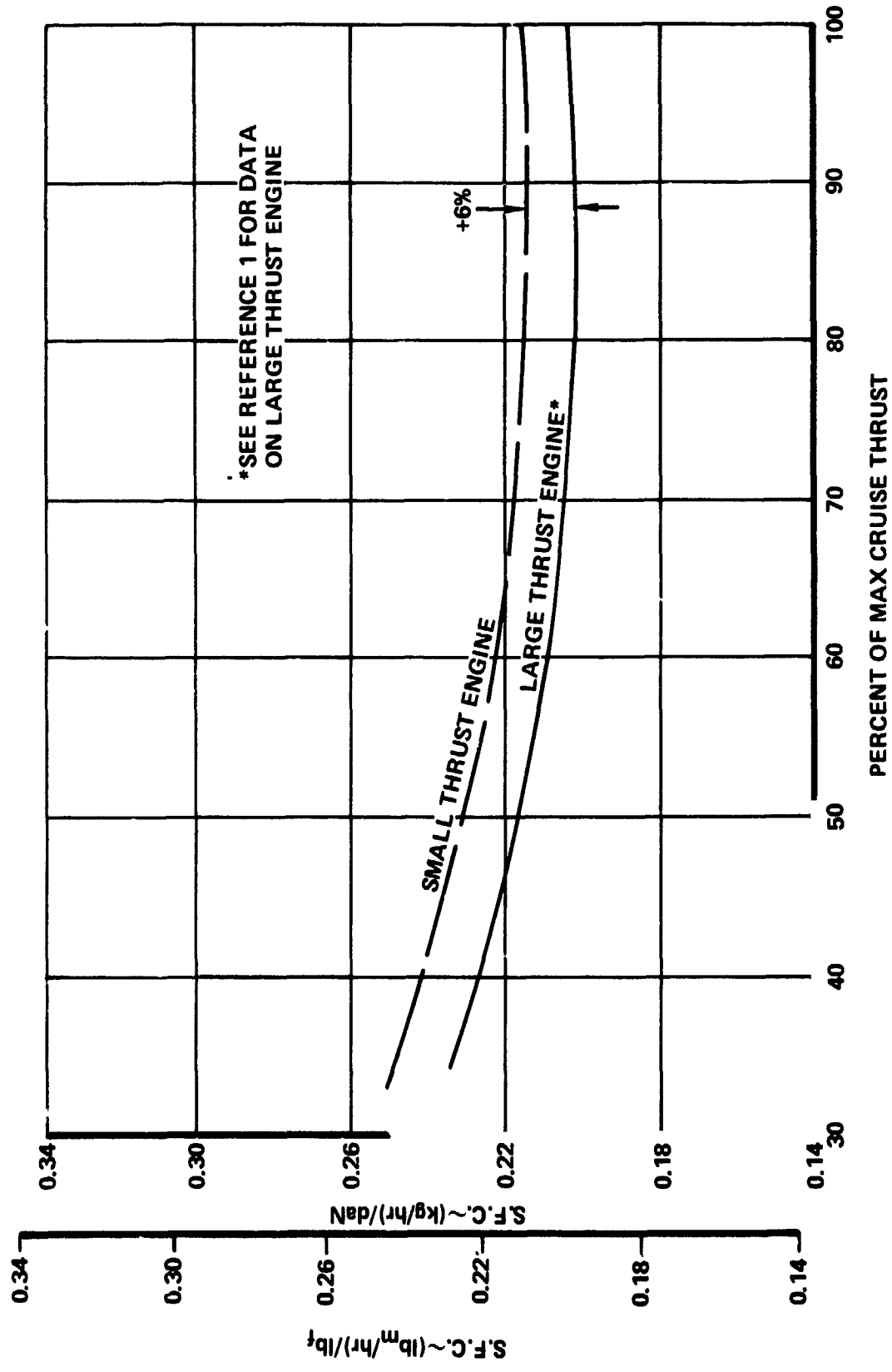


Figure 2. Installed Cruise SFC Versus Percent Maximum Rated Thrust
10,668 m (35,000 ft), Mach 0.85, Standard Day (LH₂ Fueled Engines)

became smaller. A preliminary analysis was made to examine trends based on the following assumptions:

- Range of gross weights: 45,360 to 181,440 kg (100,000 to 400,000 lb)
- 3780 km (1,500 n.mi.) range
- Constant fuel fractions
- External tank length-to-diameter ratio (l/d) = 6.5
- Constant wing loading of 527 kg/m^2 (108 lb/ft^2)

It was further assumed that the percent boil-off remained constant. This required an increase in insulation thickness as the ratio of tank wetted area-to-volume increased since boil-off is approximately proportional to this ratio. Figure 3 shows the results of this investigation and indicates that:

1. The external tank has a higher ratio of wetted area-to-volume than the internal tank.
2. This results in the much higher ratio of insulation and cover weight fractions as indicated. (Note, tank weight not included).
3. The effect of the addition of the tank wetted areas on the aircraft L/D is shown at the top of the figure compared to a clean (no tank) configuration. The internal tank aircraft L/D decreases 4.1 percent while the external tank L/D reduction is 15.8 percent over the gross weight range from 45,360 to 181,440 kg (100,000 to 400,000 lb).

These results show that the insulation thickness and weight must be adjusted as the size of the tanks decreases. This was done in providing the input data to ASSET for the parametric aircraft study. The results also indicate that the external tank aircraft will suffer more severe weight and aerodynamic penalties relative to the internal tank design as the aircraft size is decreased.

3.3 Weight Allowances

The aircraft designs which were considered in the present study represent a wide range of passenger requirements. This necessitated adjustment of those items of equipment associated with providing services to passengers. The

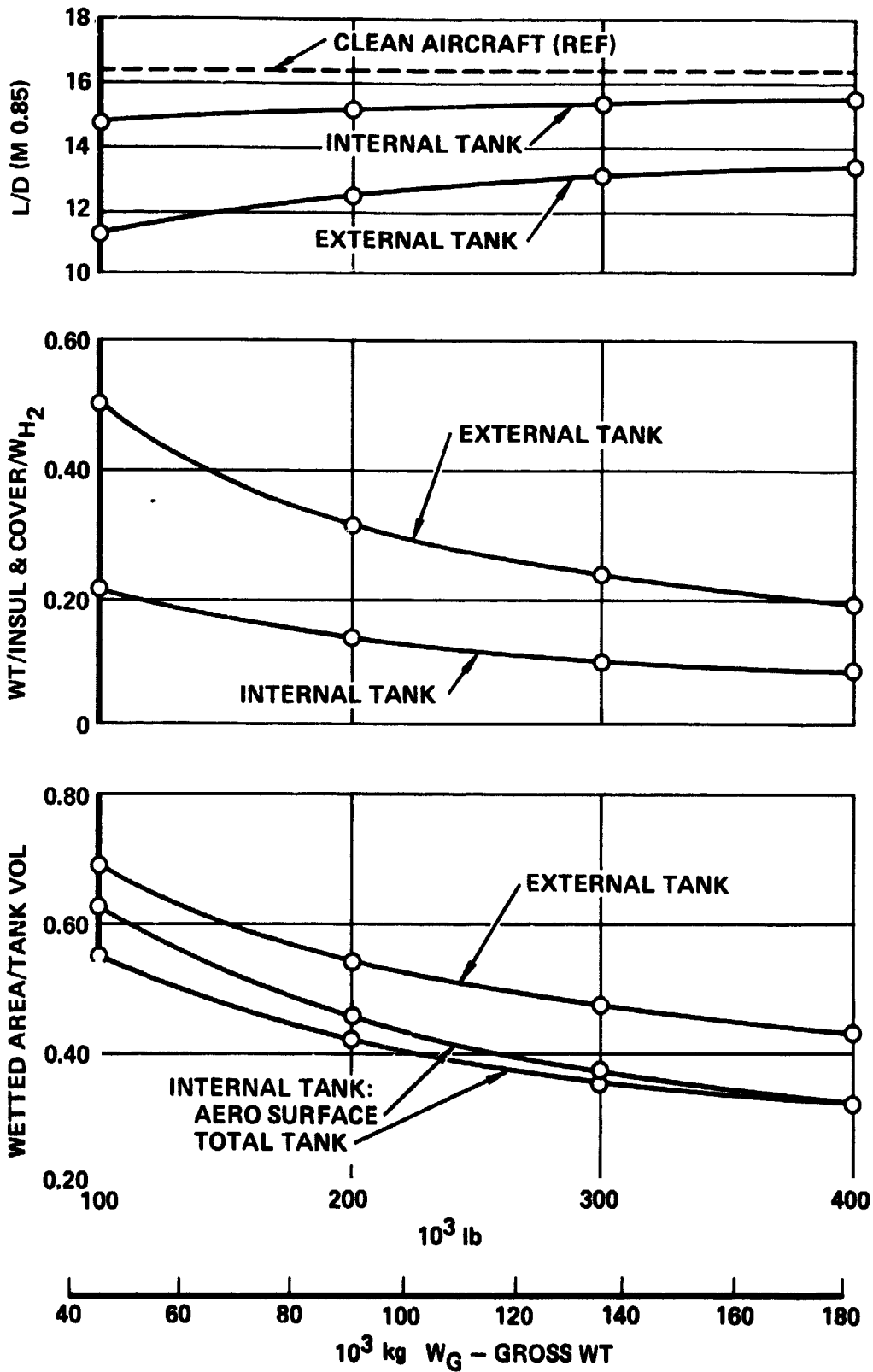


Figure 3. Results of Analysis of Hydrogen Tanks

adjustment is basically a function of the number of passengers carried, and the design range. As previously defined, the short range aircraft carry 130 passengers 2780 km (1500 n.mi.), the medium range aircraft carry 200 passengers 5560 km (3000 n.mi.), and the long range aircraft carry 400 passengers 9265 km (5000 n.mi.) each way, out and back. Table VI shows values which were used for these items which required such adjustment.

There was also a small adjustment in the weight of escape slide/rafts as a result of the fact the LH₂ aircraft designed for the long range mission is double decked. Its conventionally fueled counterpart is not, all 400 passengers are carried on a single deck. Accordingly, as shown on the table, the weight of escape slide/rafts provided for the LH₂ airplane is 810 kg (1786 lb) while that for the Jet A design is 623 kg (1374 lb).

Other weight changes to the short range aircraft include addition of air stairs (2) and deletion of certain navigation and communication equipment not required for short, over-land flight.

TABLE VI. PASSENGER SERVICE EQUIPMENT

	Short Range	Medium Range	Long Range
Escape Slide/Rafts kg (lb)	160 (353)	203 (448)	810 (1786)-LH ₂ 623 (1374)-Jet A
Food Allowance/Pass. kg (lb)	3.74 (8.24)	4.65 (10.24)	6.91 (15.24)
Water Allowance/Pass. kg (lb)	0.73 (1.6)	0.91 (2.0)	1.42 (3.12)
Pass. Serv. Equip./ Pass. kg (lb)	0.95 (2.1)	1.27 (2.8)	1.81 (4.0)
Cargo Containers-Total kg (lb)	0.0	1470 (3240)	1960 (4320)
Serving Carts-Total kg (lb)	330 (726.)	494 (1090)	989 (2180)
No. of Cabin Attendants	4.0	5.0	8.0
No. of Lavatories	3.0	4.0	7.0

4. SHORT RANGE AIRCRAFT

4.1 Design Requirements

The short range aircraft are designed to meet the following requirements and constraints:

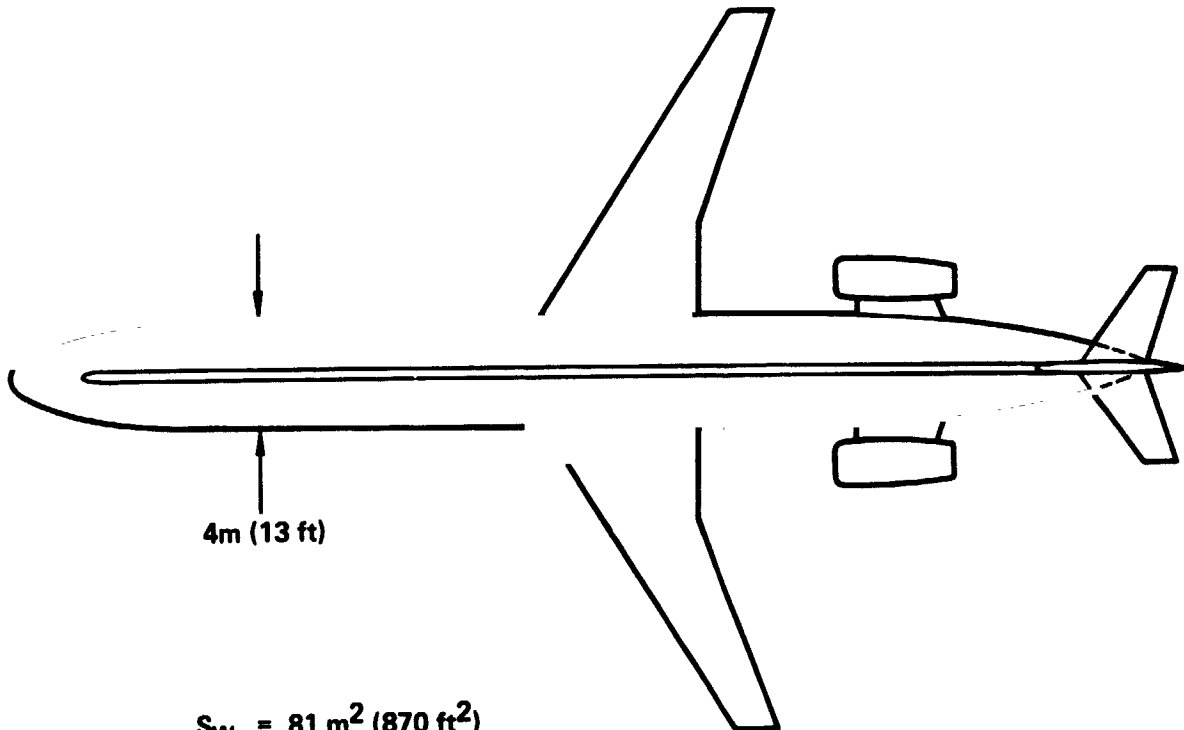
- 2780 km (1500 nmi) design range
- 130 passengers plus baggage and cargo for a total payload of 12,970 kg (28,600 lb)
- Maximum FAR takeoff field length of 2438 m (8000 ft)
- Minimum initial cruise altitude of 10,360 m (34,000 ft)
- Reserve fuel per ATA domestic regulations.
- Maximum approach speed of 69.4 m/s (135 KEAS) for aircraft weight corresponding to end of design range

4.2 Configuration Selection

Because of the small size and range of the aircraft, extended over-water operation was not envisioned and a two-engined configuration was selected. This requires an engine-out second segment climb gradient of at least 2.4 percent during takeoff.

The short range two-engined aircraft, in contrast to the medium and long range version which were investigated in the original study (Reference 1), offered the most possibilities for variations in configuration. Some of the variations investigated were:

1. Aft mounted engines as shown in Figure 4 for the internal tank hydrogen fuel version and in Figure 5 for the external. This is a viable configuration for the internal tank aircraft but presents some aerodynamic, and structural dynamic problems in the external tank version.



$S_W = 81 \text{ m}^2 (870 \text{ ft}^2)$
 $AR = 8 \quad \lambda = .3$
 $b = 25 \text{ m} (83.5 \text{ ft})$
 $T/W = .28$

$L_{FUS} = 42 \text{ m} (136.5 \text{ ft})$
 $\bar{V}_{VT} = .0853$
 $\bar{V}_{HT} = .59$

130 PAX 6 A/B @ 0.86m (34 in)

LH₂ - INT FUEL, 130 PAX, 2,780 km (1500 n.mi.)

W_G = 39,463 kg (87,000 lb)

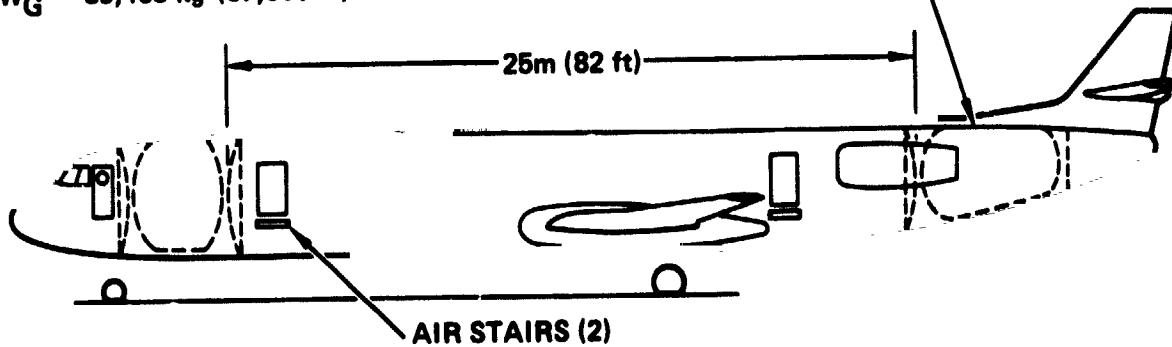
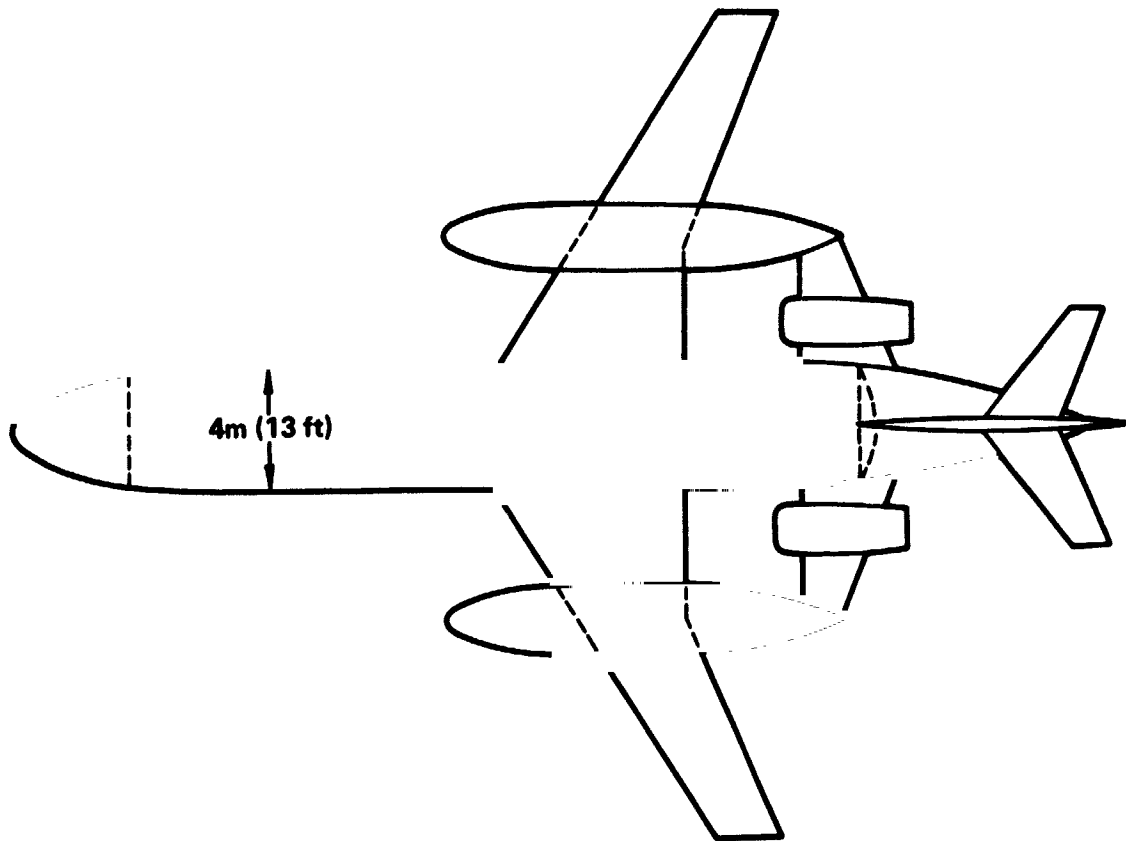


Figure 4. Candidate Configuration - Internal Tanks, Aft Mounted Engines



$S_W = 85 \text{ m}^2 (910 \text{ ft}^2)$

$AR = 8 \quad \lambda = .4$

$b = 26\text{m} (85.5 \text{ ft})$

$T/W = .32 \quad W/S = 488 \text{ kg/m}^2 (100 \text{ lb/ft}^2)$

$L_{FUS} = 34\text{m} (113 \text{ ft})$

$\nabla_{HT} = .59$

$\nabla_{VT} = .0858$

$LH_2 - \text{EXT FUEL, 130 PAX, 2,780 km (1500 n.mi.)}$

$W_G = 48,776 \text{ kg (91,000 lb)}$

130 PAX, 6 A/B @ 0.86m (34 in)

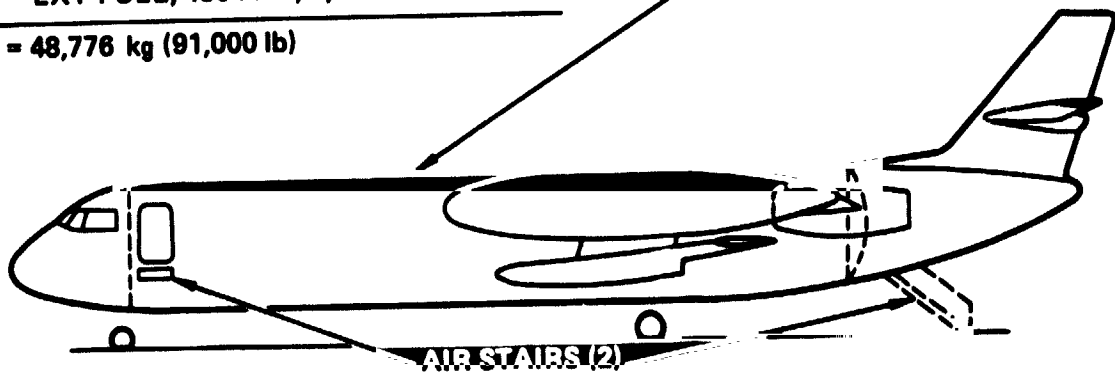


Figure 5. Candidate Configuration - External Tanks, Aft Mounted Engines

2. A high-winged configuration with underwing mounted engines for both internal and external tanks. This configuration presented no advantage over the low wing aircraft and had the problem of landing gear location and storage and also vulnerability of the internal fuel tanks to a wheels-up landing due to having no heavy wing box for protection as is the case with low winged aircraft. Another disadvantage is the passenger cabin exposure to an engine burst due to absence of the wing box.
3. A version of the aft-engined internal tank hydrogen fuel aircraft in which all fuel is carried in a single aft tank was also considered. This arrangement has the advantage of placing all fuel and propulsion in a package aft of the passengers. The obvious disadvantage with this concept is the excessive c.g. travel, estimated at 75 percent of MAC. This requires a horizontal tail approximately twice as large as is the case when the fuel is located fore and aft. Other disadvantages are the exposure of the tank to damage, and structural weight penalties due to the cantilevered tank and tail junction.

The concept chosen for analysis was a conventional low-winged design with under-wing mounted engines as described in the following sections. This configuration allows for maximum flexibility in going from the internal to the external hydrogen tanks and is adaptable to the Jet A version as well. This insures a high degree of commonality between all the designs for comparison purposes.

4.3 LH₂ Internal Tank Airplane (Aircraft No. 1)

The parametric study was conducted using the ASSET vehicle synthesis program described in Section 4.3, Reference 1. In the previous study, a comprehensive investigation was made to determine the influence of wing geometry (thickness ratio, taper ratio, and sweep) on vehicle performance. Those characteristics found to be optimum for Mach 0.85 cruise were retained for this study. The primary consideration in the present work was selection of wing aspect ratio as described below.

4.3.1 Aspect Ratio Selection. - From a matrix of some 64 aircraft generated by the vehicle synthesis program, i.e., 16 aircraft for each of four candidate aspect ratios (8,10,12, and 14) one aircraft which met all the performance constraints was selected for each aspect ratio. The variation of the selection

criteria; DOC, gross weight, price, and block fuel for these point design aircraft is presented in Figure 6 as a function of aspect ratio. This figure indicates that if the selection criteria were minimum airplane purchase price and gross weight an aspect ratio of 8 would be chosen. If minimum block fuel were desired, it would be 14. Since minimum DOC was specified as the ultimate selection criterion to be used in event of conflict, an aspect ratio of 10 was selected. Following this choice, all synthesis program input data was reviewed, revised where required, and the final point design aircraft was generated. This method of selecting the final configuration was used for each of the study aircraft.

Since two-engined aircraft are critical with regard to field length and climb gradient with one engine out, a subroutine of ASSET was used to determine the optimum takeoff flap setting and overspeed (V_2/V_S) ratio to meet these constraints with any given combination of thrust-to-weight, aspect ratio, and wing loading.

4.3.2 Configuration Description. -- A general arrangement drawing of the LH₂ internal tank, Mach 0.85, 2280 km (1500 n.mi.), 130 passenger aircraft is shown in Figure 7. The passenger compartment is located in the central section of the fuselage. Liquid hydrogen fuel tanks are located fore and aft of the passenger compartment. They occupy the full available cross section of the fuselage, except for provision for protective, crushable structure around the bottom areas. No provision was made for a passageway through or around the forward tank to permit movement between flight station and passenger compartment. The flight station is provided with separate lavatory and galley facilities.

Passenger accommodations, shown in Figure 8, use 6 abreast seating and seat spacing of 0.8 m (34 in.). The arrangement provides doors, lavatory and galley facilities in accordance with requirements of FAR 25 and current wide-body standards. Air stairs are provided at both portside doors. All cargo is contained in the pressurized fuselage below the cabin floor where space is provided for cargo containers and for loose cargo. Further details of the design are as follows:

$V_{APPR} = 69.4 \text{ m/s (135 KEAS)}$
 2nd SEG GRAD > 0.24
 FAR T.O. FIELD LENGTH $< 2438 \text{ m (8000 ft)}$

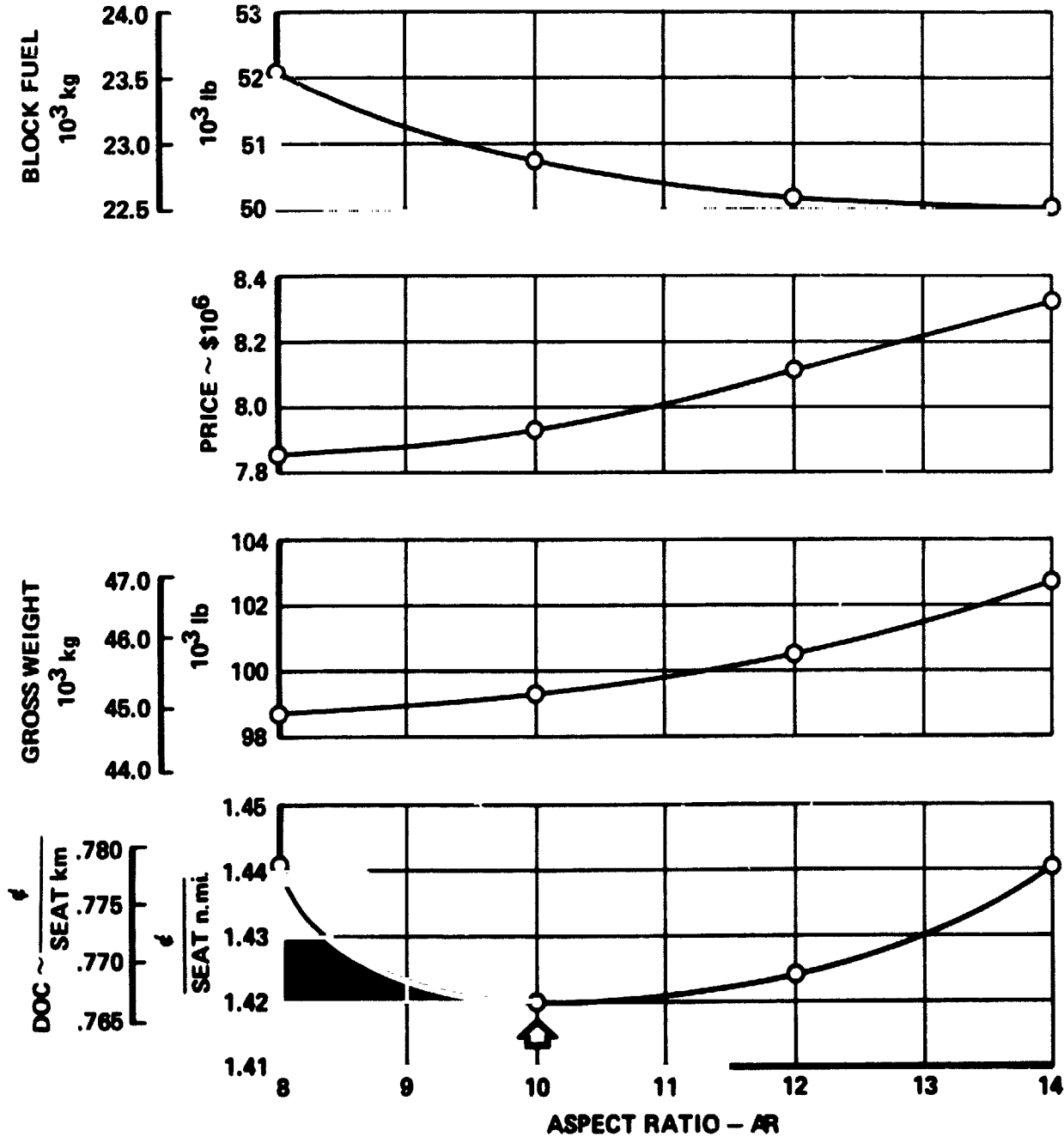


Figure 6. Aspect Ratio Selection - Aircraft No. 1

Wing: The wing has an aspect ratio of 10, thickness ratio of 10 percent and a sweep angle of 30°. The high lift devices include 15 percent leading edge slats and 35 percent double-slotted flaps, as shown. This high lift system is typical for all study configurations. Spoilers are used in flight for direct lift control, and for landing ground run deceleration. Conventional ailerons are fitted outboard of the flaps.

Landing gear: The landing gear consists of two two-wheel main gears mounted aft of the rear spar. They retract inward into the fuselage. The space between the retracted gear contains the hydraulic service center. The forward gear has two-wheels mounted on a strut which retracts forward under the pilot's compartment.

Hydrogen tank and systems: The hydrogen tank structural concept selected for purposes of this study is the integral type described in Reference 1, Section 3.1.2. All aircraft structural loads in addition to the fuel dynamic and pressure loads are taken by the tank shell. Loads are transferred from the vehicle structure to the tank at both ends by low heat-leak boron-reinforced fiberglass tubes arranged in an interconnect truss structure. Eight inches of closed-cell plastic foam insulation e.g., Rohacel 41S, covers the tank, in accordance with the scaling relationship discussed in Section 3.2. The foam insulation is then wrapped by a vapor shield (Kapton) to prevent cryopumping in event a crack develops in the foam insulation. A fiberglass reinforced composite layer covers the entire tank section to provide a smooth aerodynamic surface, and protection from physical damage.

The tank is thus generally protected from mechanical damage by the foam insulation and its fiberglass cover. Further special protection from foreign object damage and damage from aircraft maneuvers such as overrotation or tail scrape is provided on the bottom of the tank, as shown in Figure 7, by an energy absorbing, aluminum honeycomb structure supported from the tank bottom. Protection is also provided by this structure for plumbing, electrical, and control systems which would be routed adjacent to the tank.

The tank and mounting is designed for both inflight structural and fatigue loads (fail safe considerations) and to withstand the emergency crash load requirements of FAR 25 with full fuel load.

4.3.3 Vehicle Data. - All weight, performance, and cost data are presented in Section 4.6.

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CHARACTERISTICS	WING	HORIZ. TAIL	VERT. TAIL
AREA M ² (SQ FT)	84.68 (911.5)	8.73 (94)	8.36 (90)
ASPECT RATIO	10	4.5	1.6
SPAN M (FT)	29.11 (95.5)	6.28 (20.6)	3.66 (12.0)
ROOT CHORD M (IN)	4.49 (176.5)	2.14 (84.4)	3.52 (139.5)
TIP CHORD M (IN)	1.34 (52.88)	0.64 (25.3)	1.05 (41.5)
TAPER RATIO	0.3	0.3	0.3
MAC M (IN)	3.13 (125.64)	1.53 (60.1)	2.51 (98.7)
SWEEP ANG. (DEG)	0.524 (30)	0.524 (30)	0.524 (30)
T/C ROOT (%)	10	9	9
T/C TIP (%)	10	9	9

DESIGN GROSS WT. - 44,563 KG. (98,257 LB.)

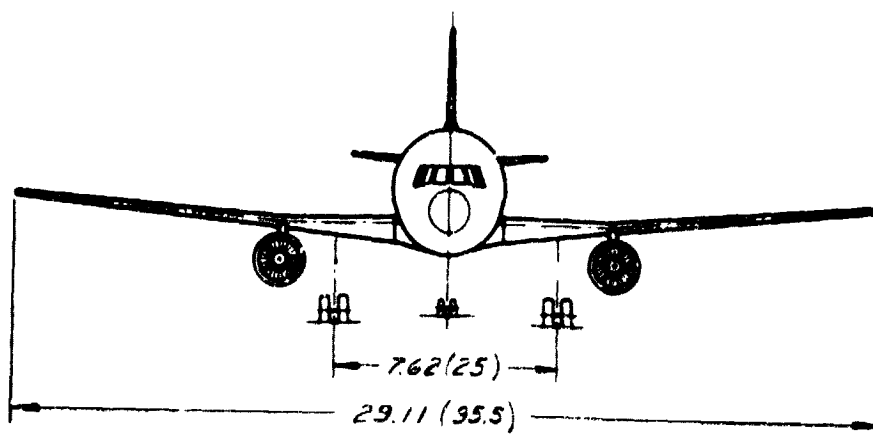
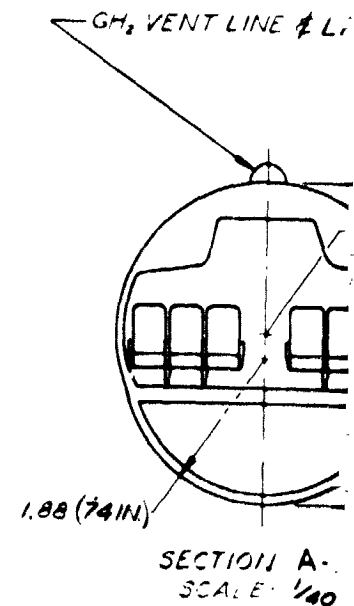
POWER PLANT - 2, TURBOFANS

INSTALLED THRUST EA. - 75,389 N. (16,943 LB.)

PASSENGERS - 130

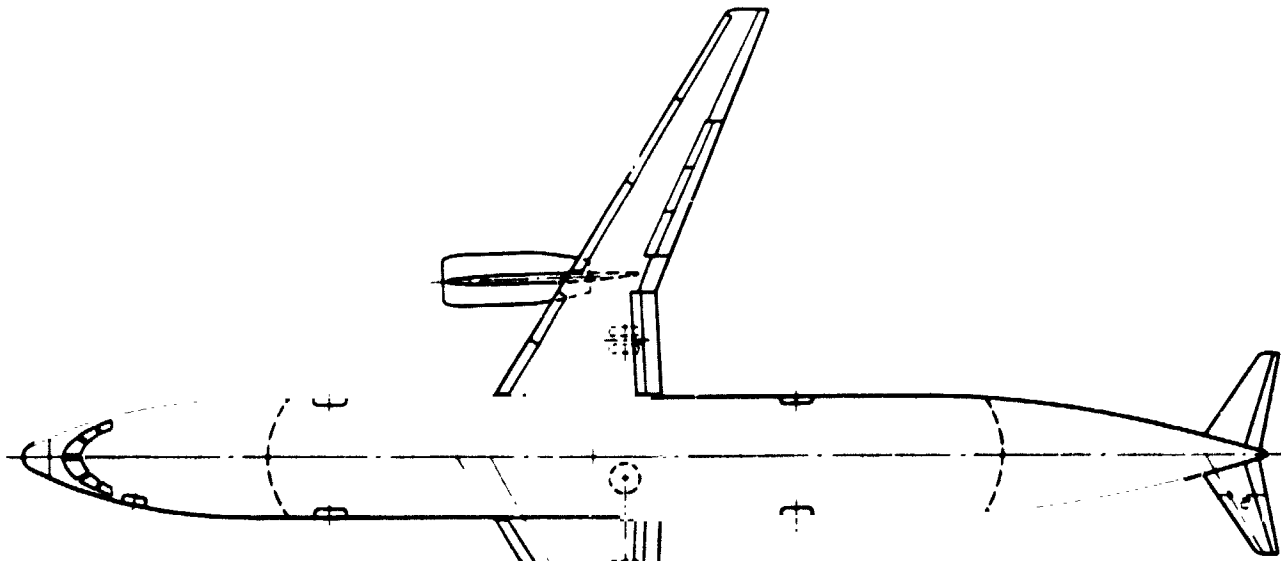
FUEL (LH₂) - 3,463 KG. (7,634 LB.)

RANGE - 2,780 KM. (1,500 N.M.)

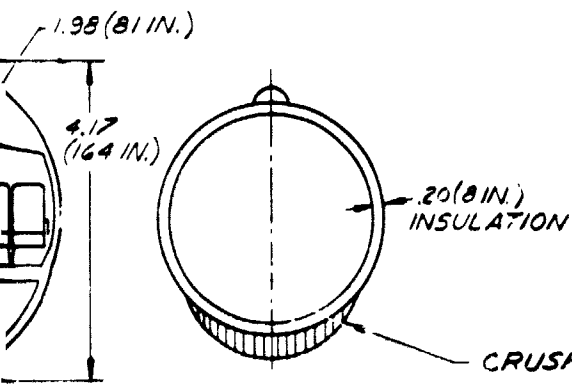


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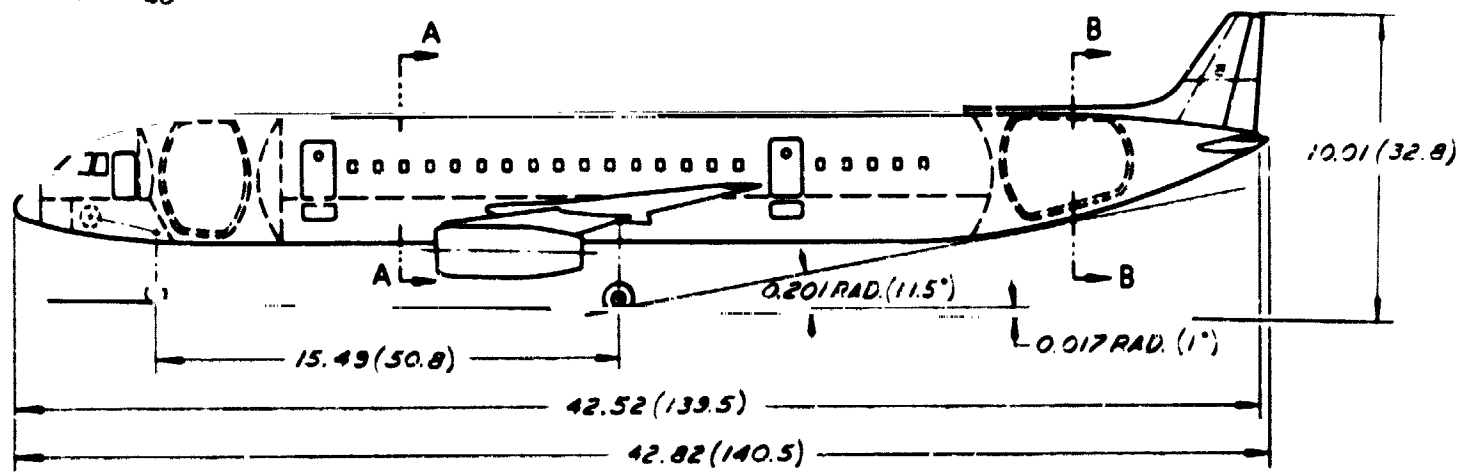


FUELING LINE

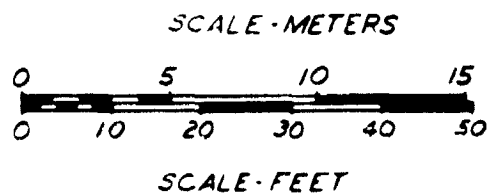
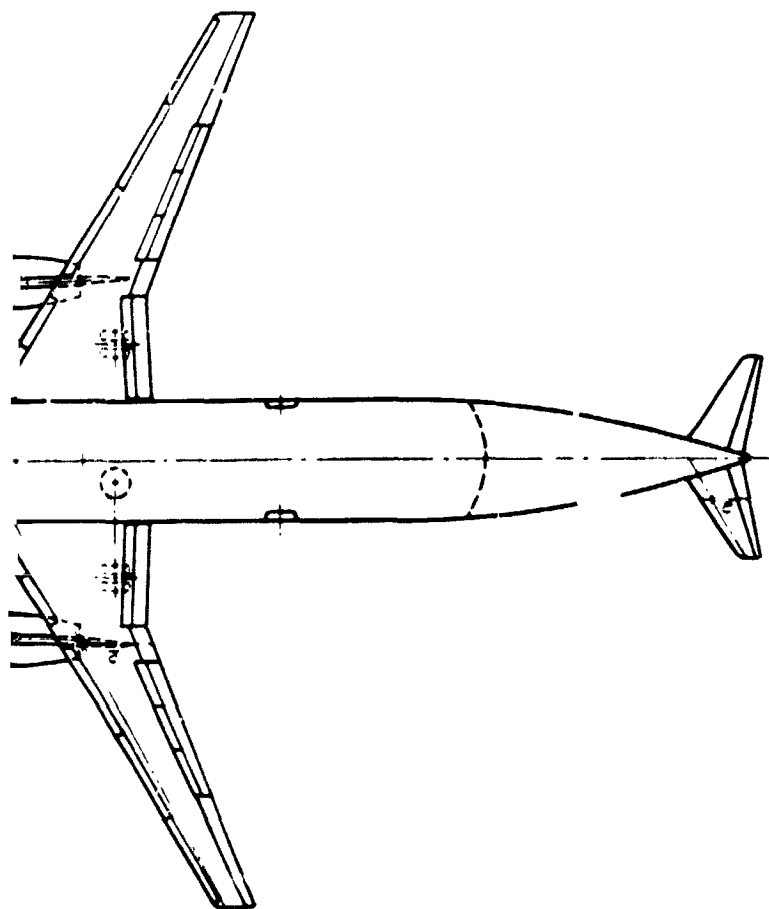


CRUSHABLE MATERIAL FOR TANK PROTECTION

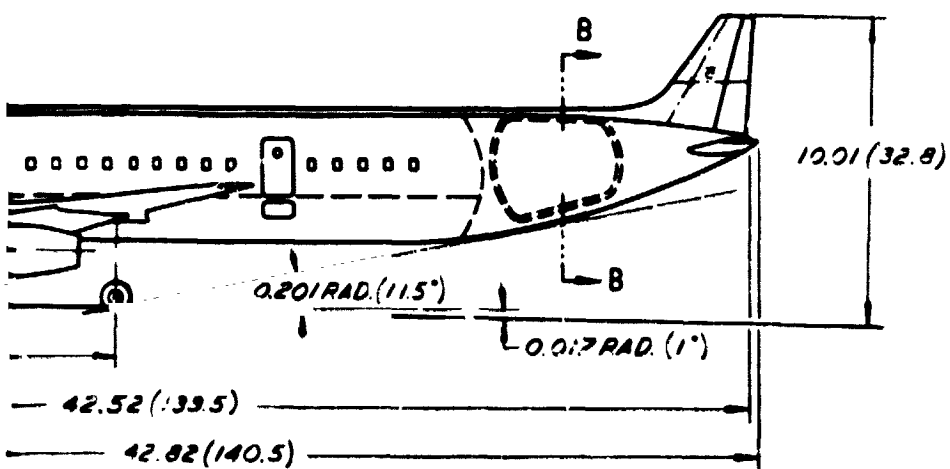
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FOLDOUT FRAME 2



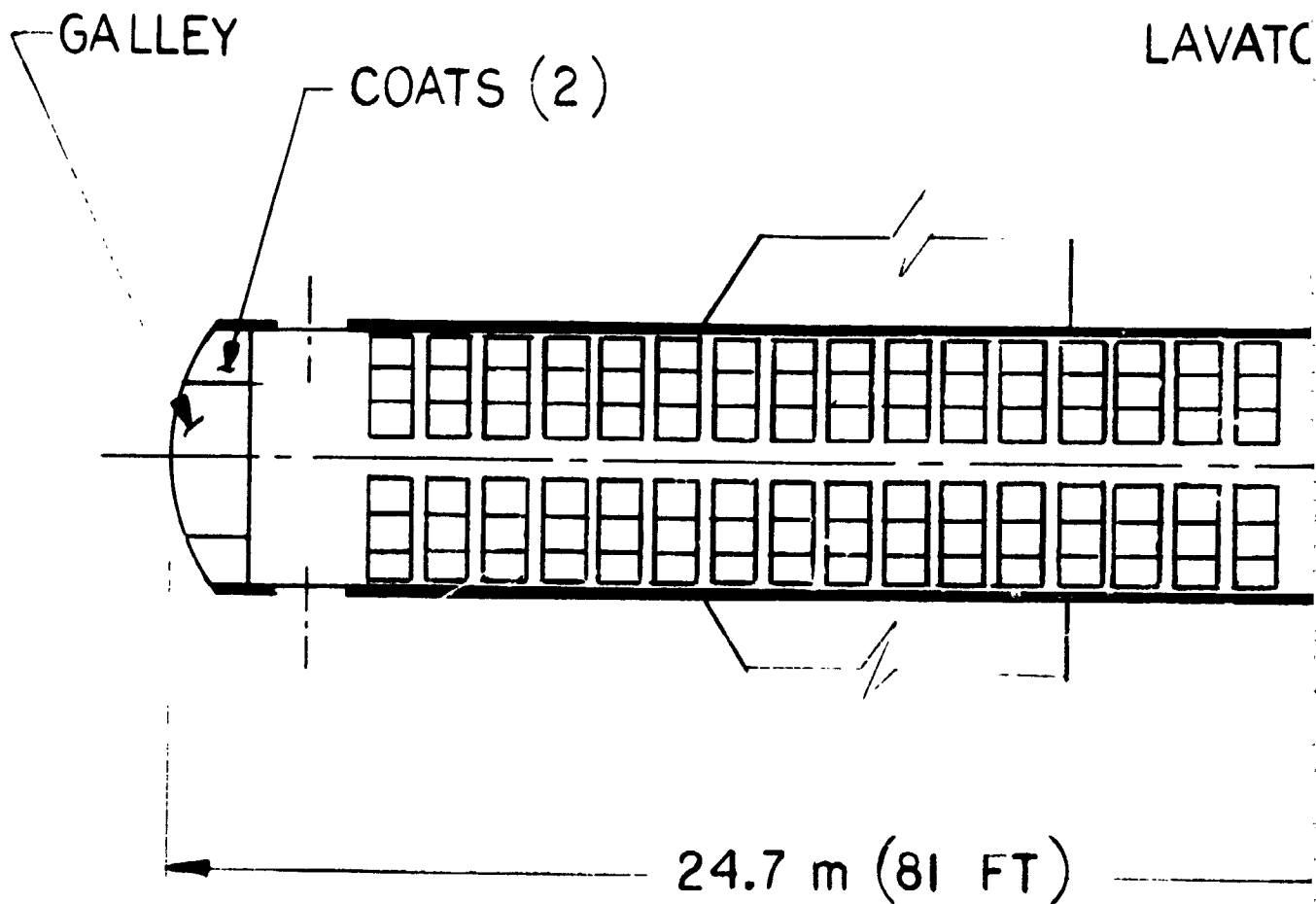
MATERIAL FOR TANK PROTECTION



1 DIM. IN METERS (FEET), OR NOTED
NOTE:

Figure 7. General Arrangement:
Short Range, LH₂
Internal Tank Transport

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130 PAX , 6 A/B , .86 m (34 IN) SPACING

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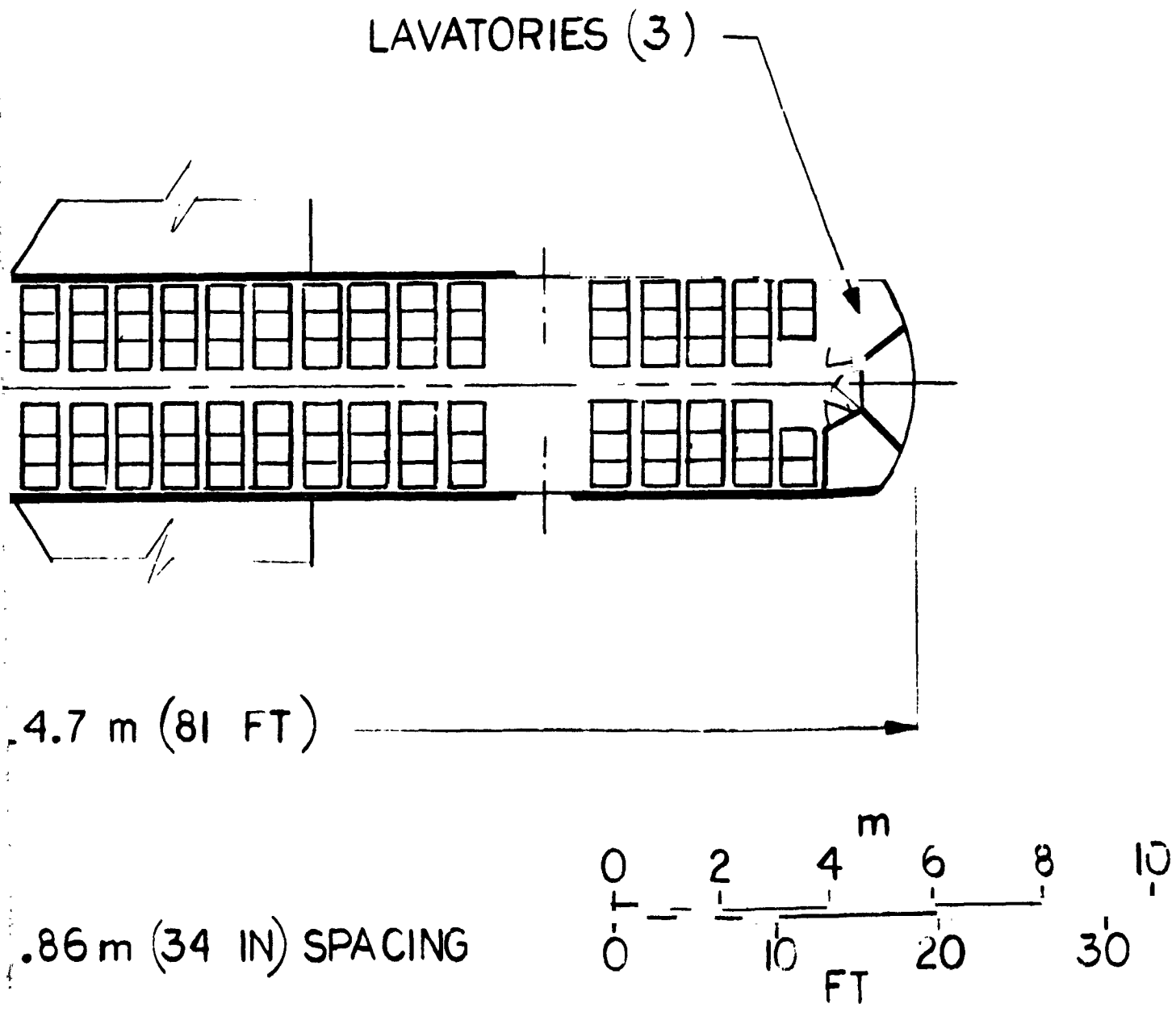


Figure 8. Interior Arrangement:
130 Pax Aircraft

4.4 LH₂ External Tank Airplane (Aircraft No. 2)

4.4.1 Aspect Ratio Selection. - The procedure for selecting aircraft characteristics from the parametric matrix generated by use of ASSET is the same as that described in Section 4.3.1 for the internal tank configuration. Figure 9 shows the effect of the various selection criteria on choice of aspect ratio. Based on minimum DOC, an aspect ratio of 9.5 was selected for the final point design aircraft.

4.4.2 Configuration Description. - The most obvious feature of the external tank LH₂ aircraft design shown in Figure 10 is of course the large wing-mounted tanks. Their physical size prevents mounting below the wing. To reduce drag to an acceptable level the tank is supported on a pylon with a height of approximately one-third the tank diameter. The tank is of integral construction covered with eight inches of closed-cell plastic foam insulation protected by a vapor proof barrier film and an external fiberglass reinforced composite cover.

The fuselage length of this aircraft has been reduced compared to the internal tank version by removal of the hydrogen fuel tanks. Six abreast seating is provided with a 0.86 m (34 in.) seat pitch for 130 passengers. Cargo volume, lavatory, and galley facilities are equivalent to those on the internal tank aircraft.

The tank arrangement of this aircraft simplifies the fuel system arrangement since only one engine crossfeed line and refuel line are carried across the aircraft fuselage in the wing box.

Air stairs are provided at both entry doors on the left hand side of the aircraft.

4.4.3 Vehicle Data. - All weight, performance, and cost data for this aircraft are presented in Section 4.6.

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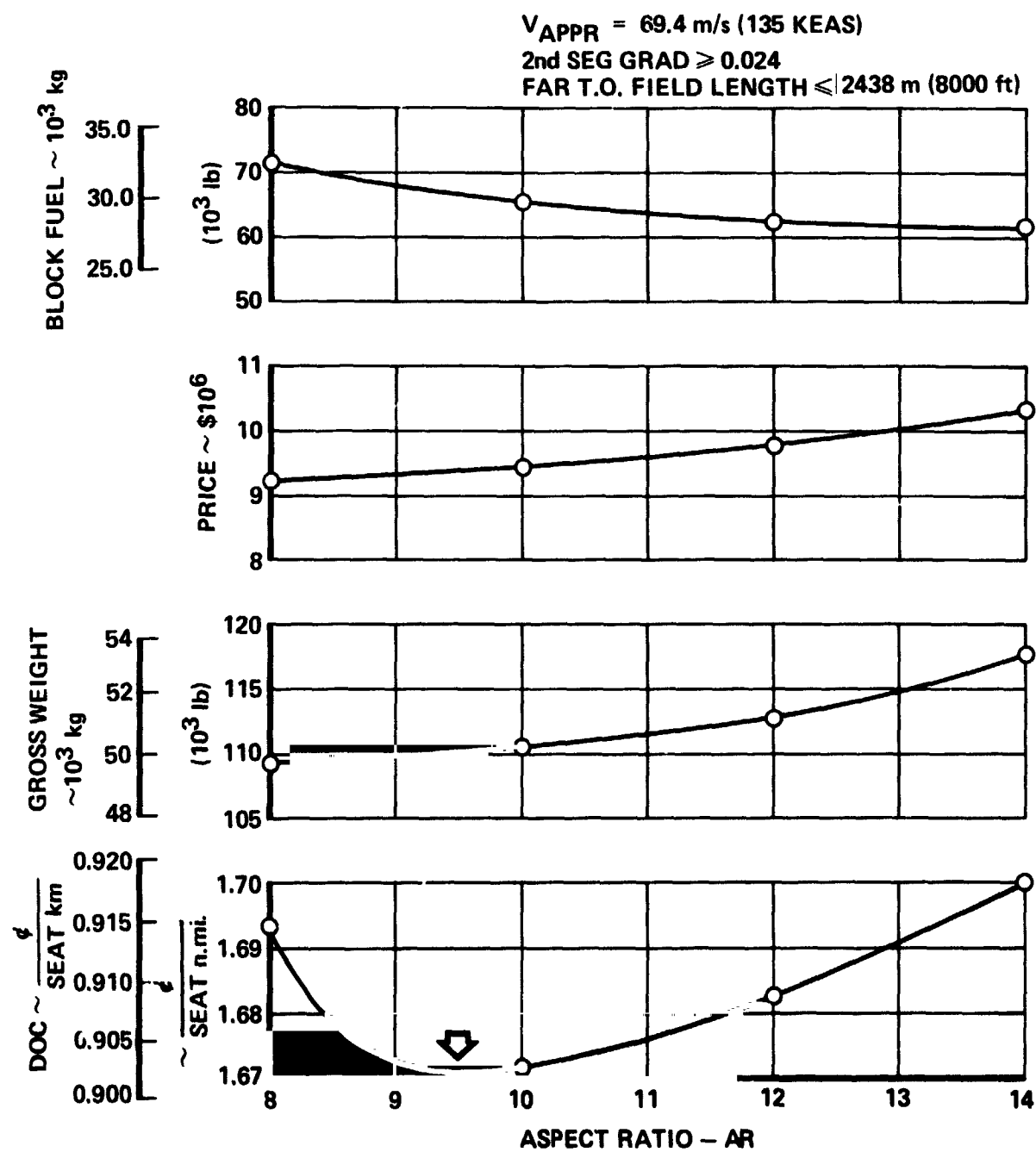


Figure 9. Aspect Ratio Selection - Aircraft No. 2

CHARACTERISTICS	WING	HORIZ. TAIL	VERT. TAIL
AREA M ² (SQ FT)	94.54 (1017.6)	15.16 (163.2)	12.89 (138.8)
ASPECT RATIO	9.5	4.5	1.6
SPAN M (FT)	29.97 (98.3)	8.26 (27.1)	4.54 (14.9)
ROOT CHORD M (IN)	4.51 (177.4)	2.82 (111.1)	4.37 (172.0)
TIP CHORD M (IN)	1.80 (71.0)	0.85 (33.3)	1.31 (51.6)
TAPER RATIO	0.4	0.3	0.3
MAC M (IN)	3.35 (131.5)	2.01 (79.2)	3.11 (122.6)
SWEEP RAD. (DEG)	0.524 (30)	0.524 (30)	0.524 (30)
T/C ROOT (°)	10	9	9
T/C TIP (°)	10	9	9

DESIGN GROSS WT. - 43,851 KG. (109,901 LB.)

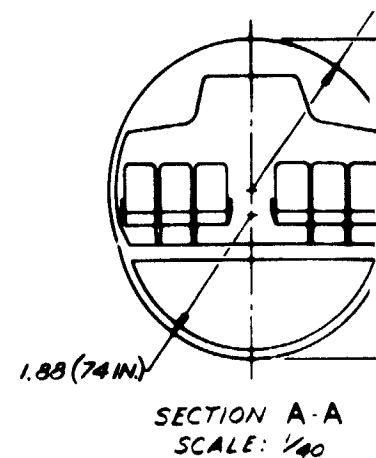
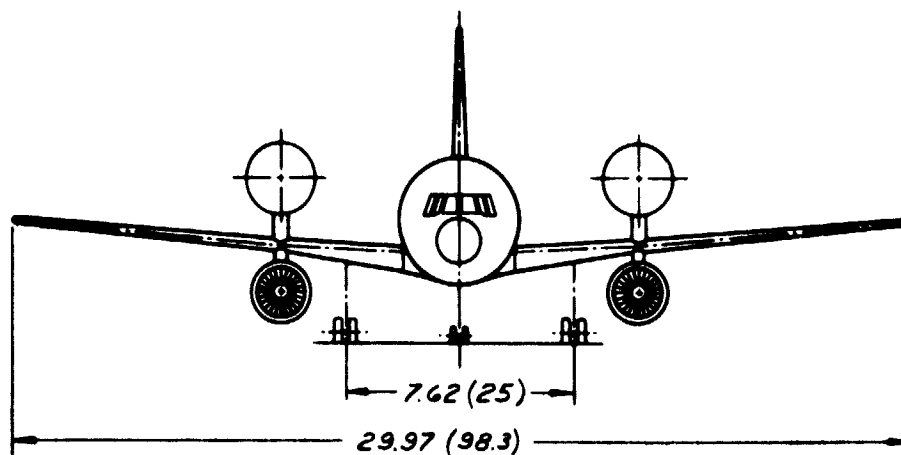
POWER PLANT - (2) TURBOFANS

INSTALLED THRUST (EA.) - 109,986 N. (24,727 LB.)

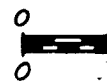
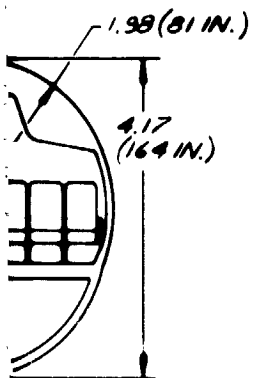
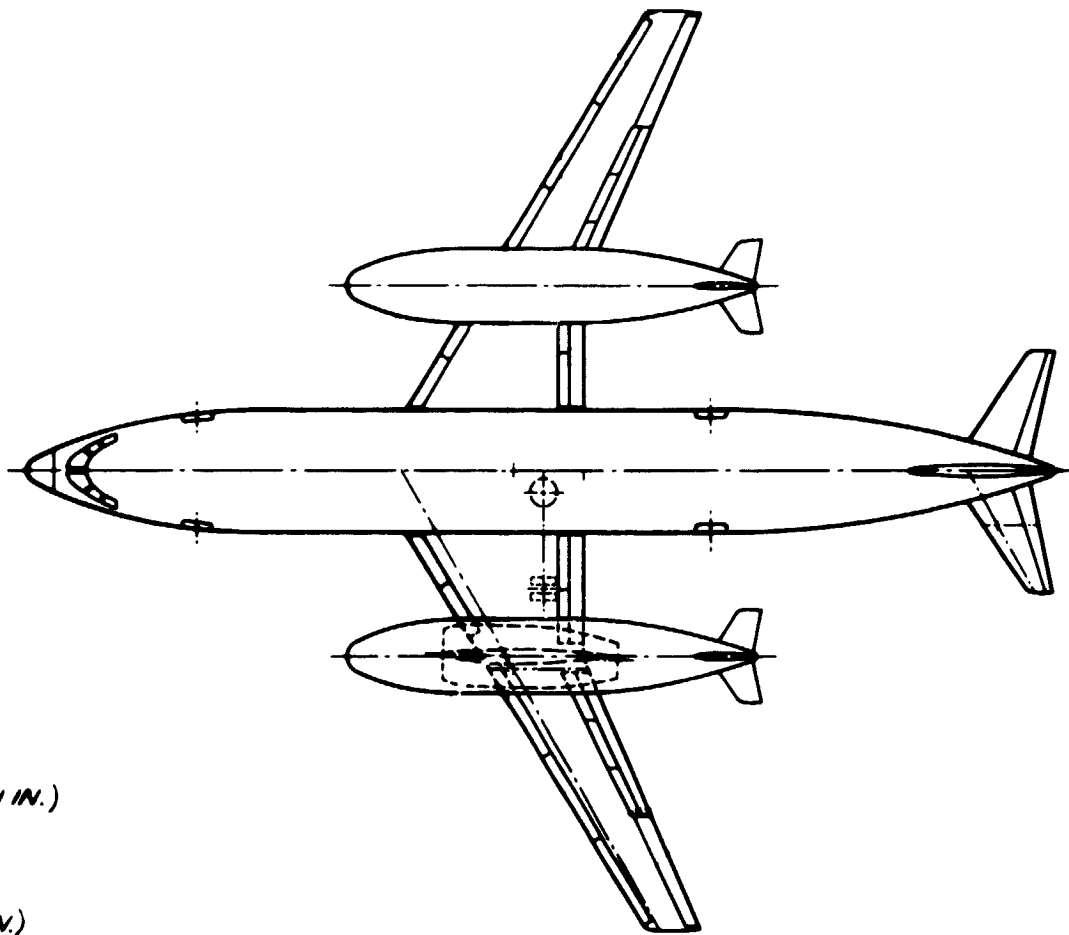
PASSENGERS - 130

FUEL (LH₂) - 4,361 KG. (9,615 LB.)

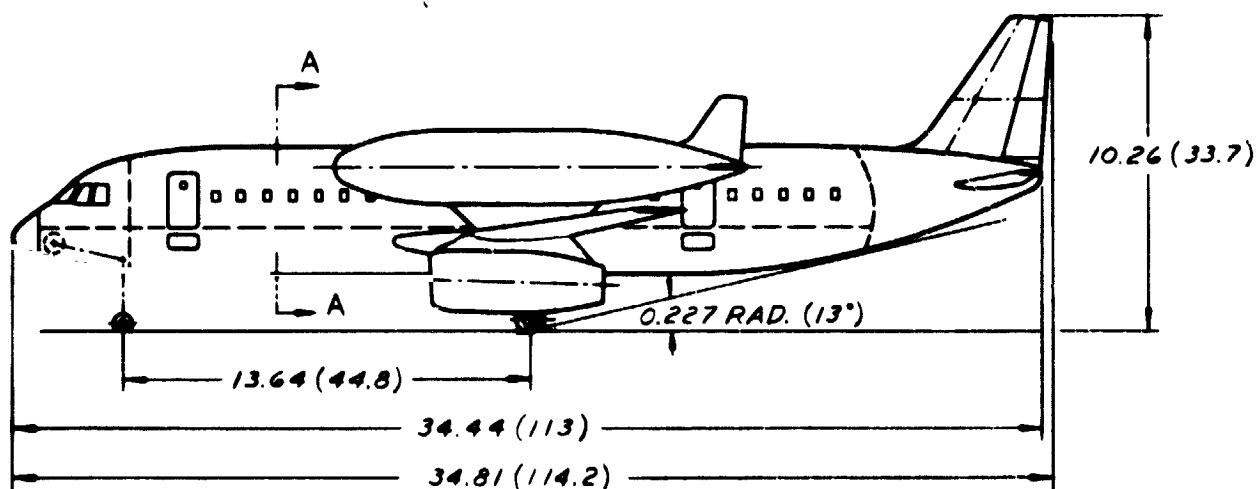
RANGE - 2,780 KM. (1,500 N.M.)



FOLDOUT FRAME (



-A
90

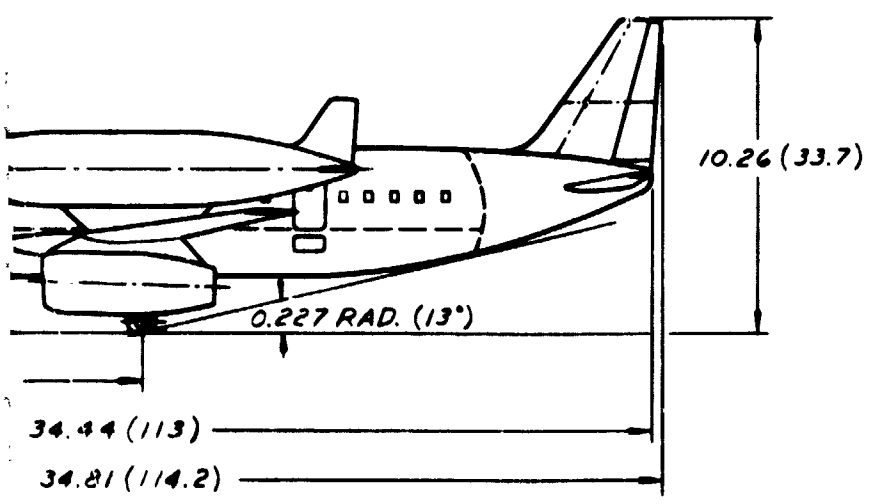
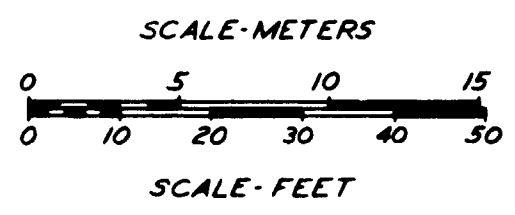
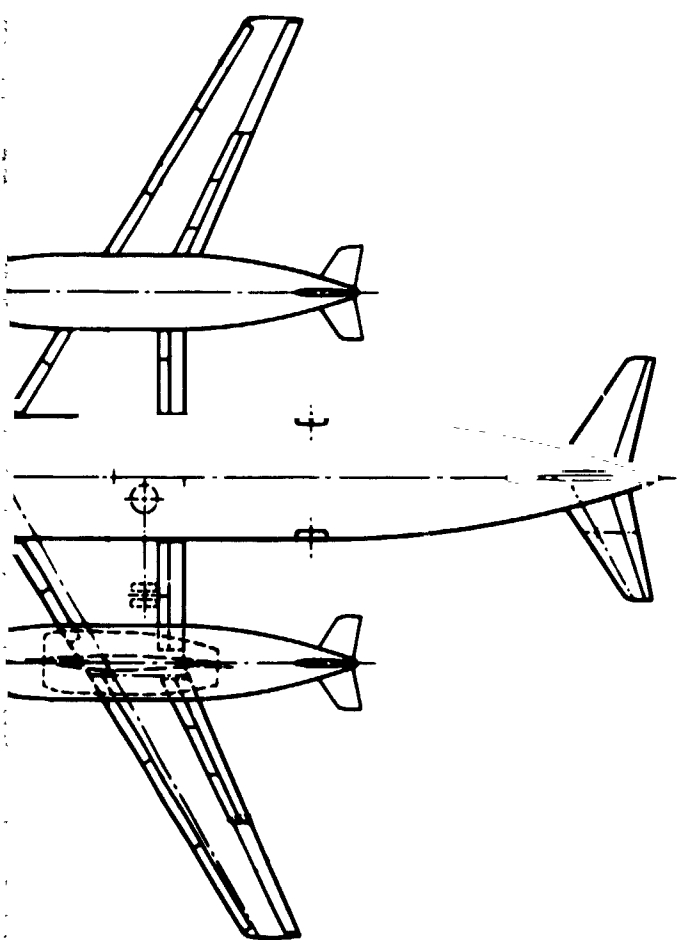


1. DIM
NOTE

Figur

FOLDOUT FRAME

2



1. DIM. IN METERS (FEET), OR NOTED
NOTE:

Figure 10. General Arrangement:
Short Range, LH₂
External Tank Transport

4.5 Jet A Airplane (Aircraft No. 3)

4.5.1 Aspect Ratio Selection. - Figure 11 shows the various selection criteria versus aspect ratio and indicates a choice of 11 to provide minimum DOC.

4.5.2 Configuration Description. - The general arrangement of the Jet A fueled aircraft is shown in Figure 12. The fuselage and interior arrangement is the same as that of the external tank hydrogen aircraft described in Section 4.4. All fuel is contained in the wing box structure resulting in some load relief for this wing compared to the internal tank hydrogen design. Air stairs are provided on both left hand entry doors.

4.5.3 Vehicle Data. - All weight, performance, and cost data for this aircraft are presented in Section 4.6.

4.6 Comparison of Short Range Aircraft

Table VII presents a summary of the characteristics of the three short range aircraft. These are the final point designs meeting all performance constraints and selected on the basis of minimum DOC. For convenience in comparing the designs, ratios of the more significant values are shown.

Comparison of the external to the internal tank LH_2 aircraft designs shows that in spite of the short range involved, and therefore a relatively small fuel load, the drag of the external tanks resulted in a lift/drag ratio 15 percent poorer for that aircraft design compared to the internal tank aircraft. This is due to the rapid increase of external tank wetted area (and weight) compared to the internal tank, as discussed in Section 3.2. The lower L/D in turn, requires more cruise thrust and results in use of larger engines.

Use of larger engines accounts for the shorter takeoff distance and the higher initial cruise altitude of the external tank design. However, the combination of lower L/D and larger engines causes a significant penalty in fuel weight, aircraft price, and DOC. These disadvantages led to selection of the

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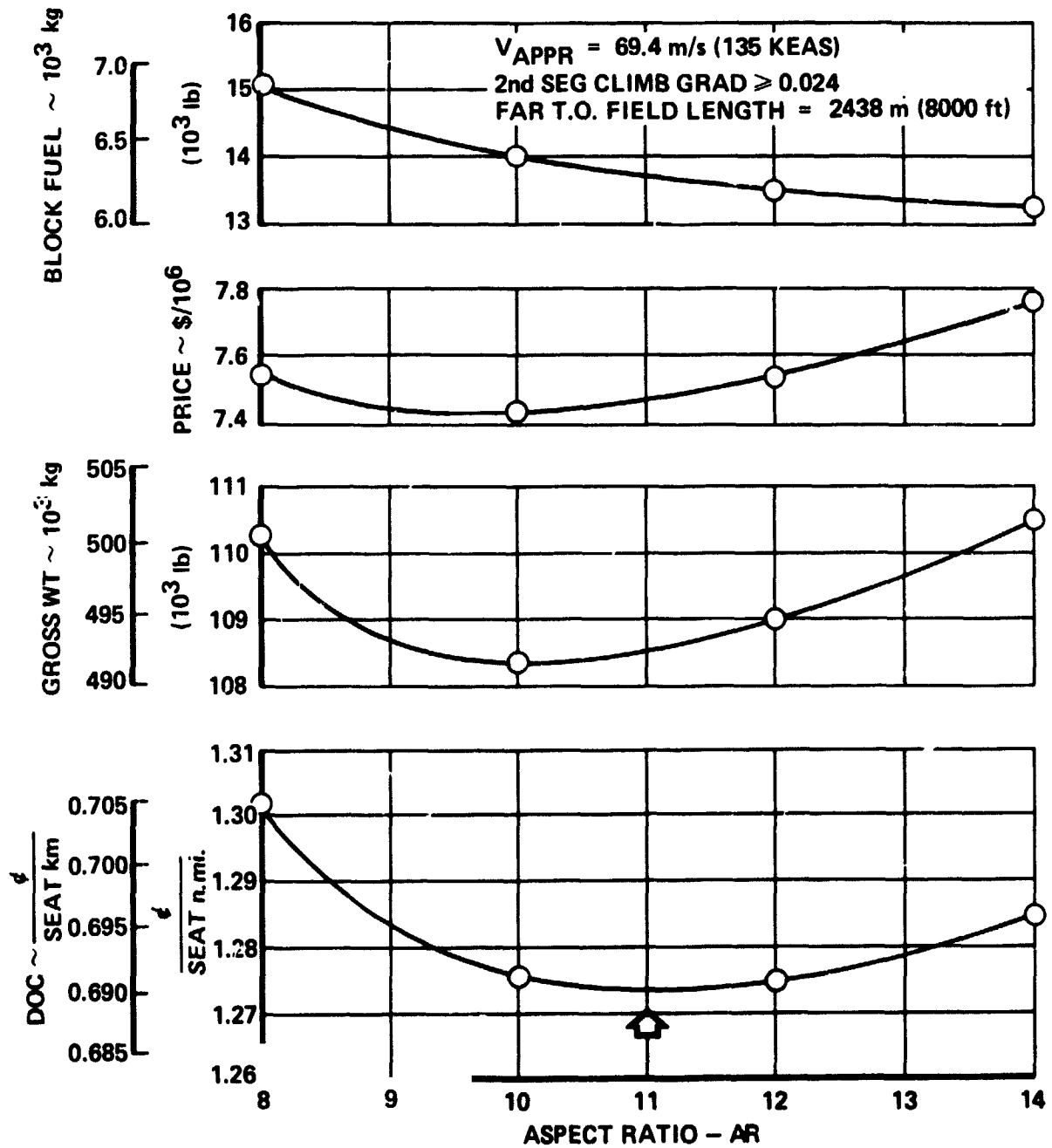


Figure 11. Aspect Ratio Selection - Aircraft No. 3

CHARACTERISTICS	WING	HORIZ. TAIL	VERT. TAIL
AREA M ² (SQ FT)	86.3 (928.7)	12.3 (132.1)	11.6 (125.4)
ASPECT RATIO	11	4.5	1.6
SPAN M (FT)	30.81 (101.1)	7.43 (24.4)	4.32 (14.2)
ROOT CHORD M (IN)	4.31 (169.6)	2.54 (99.9)	4.14 (162.9)
TIP CHORD M (IN)	1.29 (50.9)	0.76 (30.0)	1.24 (48.9)
TAPER RATIO	0.3	0.3	0.3
MAC M (IN)	3.07 (120.9)	1.81 (71.2)	2.95 (116.1)
SWEEP RAD. (DEG)	0.524 (30)	0.524 (30)	0.524 (30)
T/C ROOT (%)	10	9	9
T/C TIP (%)	10	9	9

DESIGN GROSS WT. - 49,287 KG. (108,657 LB.)

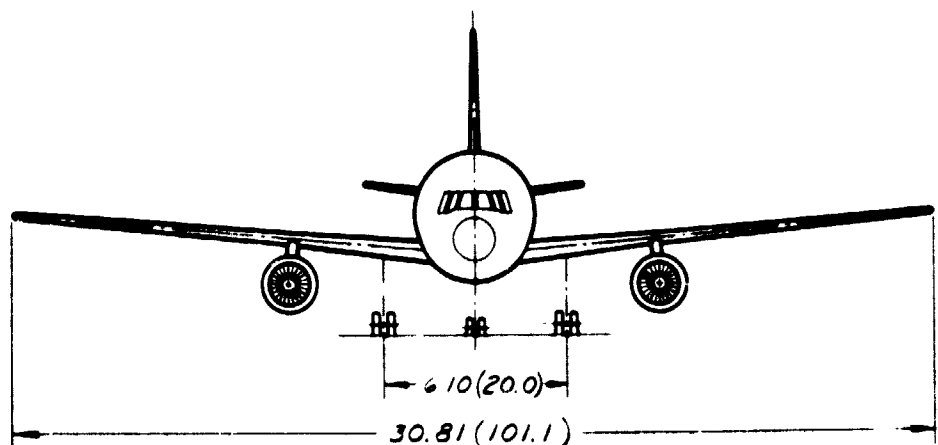
POWER PLANT - (2) TURBOFANS

INSTALLED THRUST (EA) - 84,094 N. (18,906 LB.)

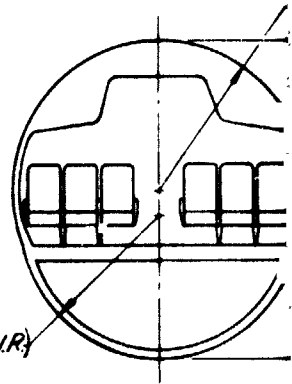
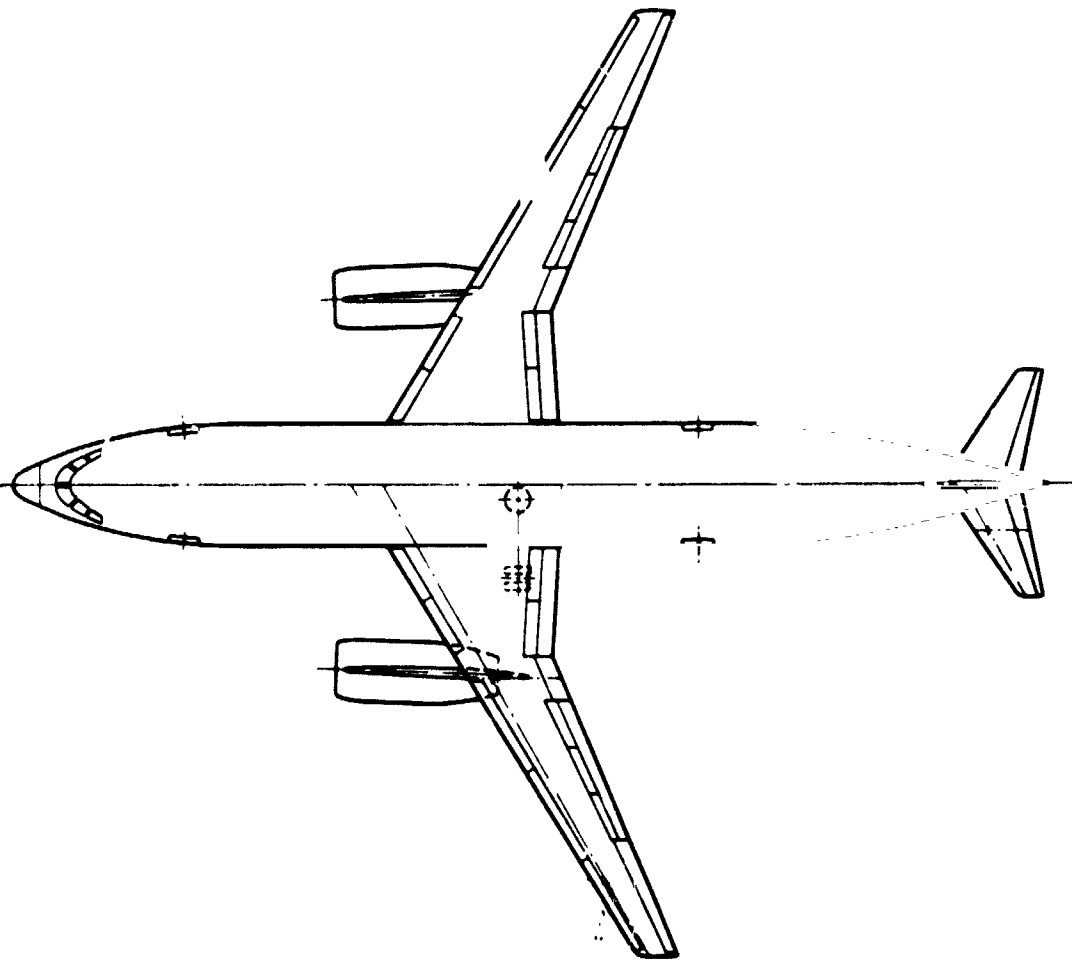
PASSENGERS - 130

FUEL (JET A) - 8,938 KG (19,704 LB.)

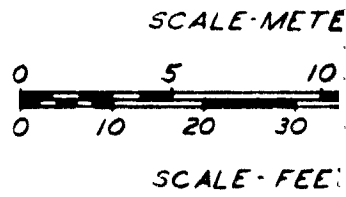
RANGE - 2,780 KM. (1,500 N.M.)



BOLDOUT FRAME 1



SECTION A -
SCALE: 1/40



1. DIM. IN METERS (FEET)
NOTE:

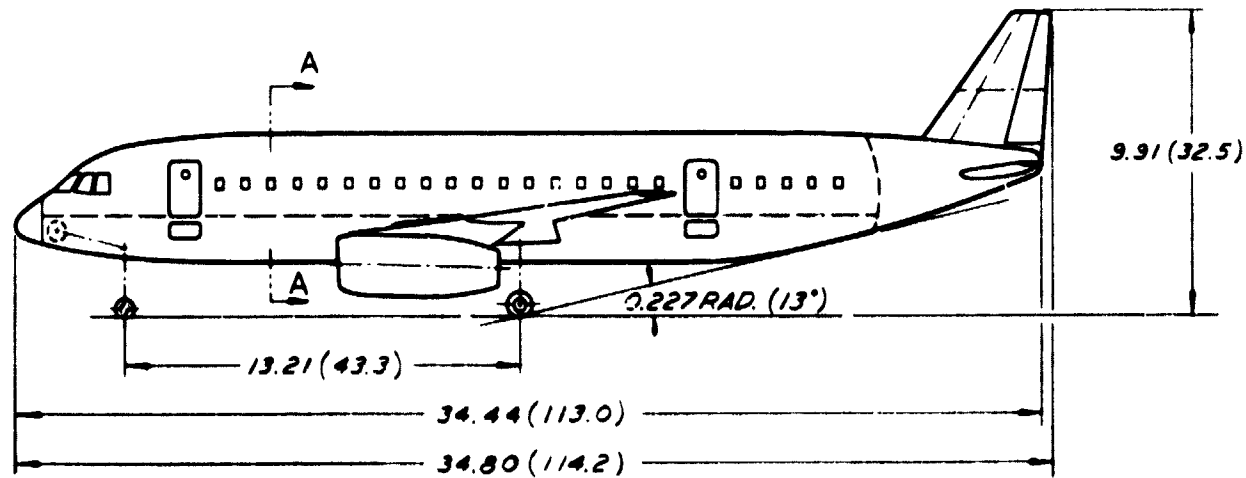
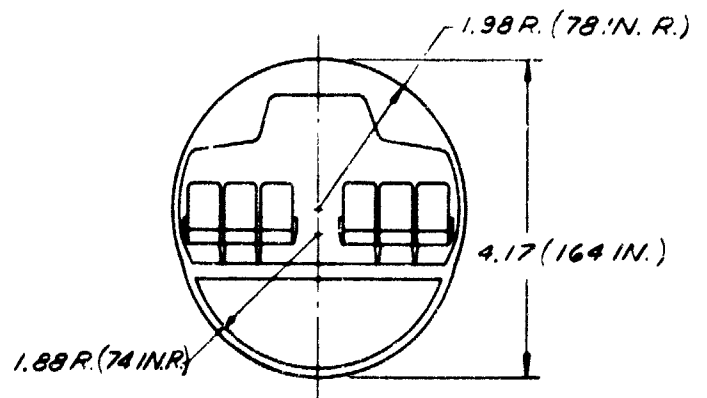
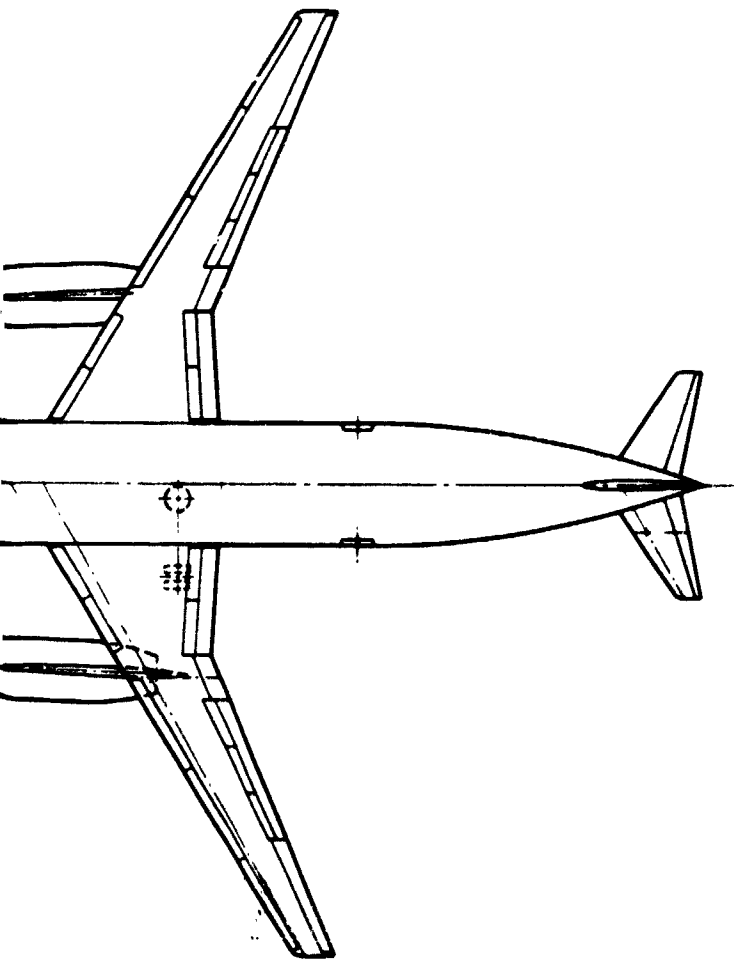


Figure 12. General
Short Range
Fuel Transport

WORLDWIDE FRAME 2



SECTION A-A
SCALE: 1/40

SCALE-METERS



SCALE- FEET

1. DIM. IN METERS (FEET), OR NOTED.
NOTE:

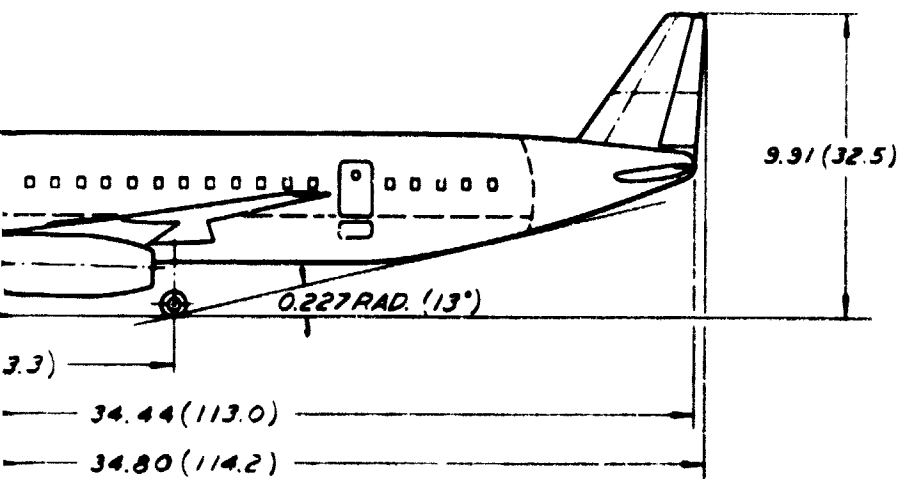


Figure 12. General Arrangement:
Short Range, Jet A
Fuel Transport

TABLE VII. COMPARISON OF FINAL DESIGN SHORT RANGE AIRCRAFT

(S.I. UNITS)

(2780 km Range - 130 Pax. - Mach 0.85)

Payload = 12,973 kg

		Aircraft No. 1 (Int LH ₂)	Aircraft No. 2 (Ext LH ₂)	Ratio (<u>Ext</u> <u>Int</u>)	Aircraft No. 3 (Jet A)	Ratio (<u>Jet A</u> <u>Int LH₂</u>)
Gross Weight	kg	44,570	49,850	1.118	49,290	1.11
Total Fuel	kg	3,340	4,360	1.31	8,940	2.68
Block Fuel	kg	2,296	3,015	1.31	0,190	2.70
Operating Empty Wt	kg	28,260	32,520	1.15	27,380	0.97
Empty Wt	kg	26,290	30,520	1.16	25,460	0.97
Aspect Ratio		10	9.5		11	
Wing Area	m ²	85	94.5	1.11	86.3	1.02
Sweep	degrees	30	30		30	
Span	m	29.1	30.0	1.03	30.8	1.06
Fus. Length	m	42.5	34.4	0.81	34.4	0.81
L/D - Cruise		13.9	11.7	0.846	16.3	1.18
SFC - Cruise	kg/hr /daN	0.215	0.215		0.629	2.93
Initial Cruise Altitude	m	10,970	11,580		12,190	
Wing Loading	kg/m ²	526.3	527.3		571.2	
Thrust/Weight	N/kg	3.38	4.41	1.3	3.41	1.0
No. Engines		2	2		2	
Thrust Per Engine	N	75,390	109,990	1.46	84,090	1.12
FAR T.O. Distance	m	2,403	1,420	0.59	2,429	1.02
FAR Ldg. Distance	m	1,746	1,753		1,754	
2nd Seg Climb		0.0276	0.0583	2.11	0.0365	1.32
Grad. (Eng. Climb)						
Approach Speed	m/s	69	69		69	
Weight Fractions	percent					
Fuel		7.5	8.8		18.1	
Payload		29.1	26.0		26.3	
Structure		28.3	27.6		26.1	
Propulsion (Includes Fuel System)		12.8	17.6		9.2	
Equipment and Operating Items		22.3	20.0		20.3	
Price	\$10 ⁶	7.85	9.34	1.19	7.51	0.95
DOC	seat km	0.783 ¹	0.901 ¹	1.18	0.689 ²	0.90
Energy Utilization	<u>kJ</u> seat km	762	1001	1.32	733	0.96

¹DOC based on LH₂ cost = \$2.85/GJ

²DOC based on Jet A cost = \$1.90/GJ

TABLE VII. COMPARISON OF FINAL DESIGN SHORT RANGE AIRCRAFT

(U.S. CUSTOMARY UNITS)

(1500 n.mi. Range - 130 Pax. - Mach 0.85)

Payload = 28,600 lb

		Aircraft No. 1 (Int LH ₂)	Aircraft No. 2 (Ext LH ₂)	Ratio ($\frac{\text{Ext}}{\text{Int}}$)	Aircraft No. 3 (Jet A)	Ratio ($\frac{\text{Jet A}}{\text{Int LH}_2}$)
Gross Weight	lb	98,280	109,900	1.118	108,660	1.11
Total Fuel	lb	7,364	9,616	1.31	19,704	2.68
Block Fuel	lb	5,060	6,647	1.31	13,645	2.70
Operating Empty Wt	lb	62,290	71,680	1.15	60,350	0.97
Empty Wt	lb	57,970	67,270	1.16	56,130	0.97
Aspect Ratio		10	9.5		11	
Wing Area	ft ²	911.5	1,018	1.12	928.7	1.02
Sweep	deg	30	30		30	
Span	ft	95.5	98.3	1.03	101.1	1.06
Fus. Length	ft	139.5	113.0	0.81	113.0	0.81
L/D - Cruise		13.9	11.7	0.846	16.3	1.18
SFC - Cruise	hr lb	0.211	0.211		0.614	2.93
Initial Cruise Altitude	ft	38,000	38,000		40,000	
Wing Loading	lb/ft ²	107.8	108.0		117.0	
Thrust/Weight		0.345	0.450	1.3	0.348	1.0
No. Engines		2	2		2	
Thrust Per Engine	lb	16,950	24,730	1.46	18,910	1.12
FAR T.O. Distance	ft	7,885	4,770	0.59	7,970	1.02
FAR Ldg. Distance	ft	5,728	5,752		5,754	
2nd Sg. Climb		0.0276	0.0583	2.11	0.0385	1.32
Grad. (Enj. Out)						
Approach Speed	KEAS	135	135		135	
Weight Fractions	percent					
Fuel		7.5	8.8		18.1	
Payload		29.1	28.0		28.3	
Structure		28.3	27.6		28.1	
Propulsion (includes Fuel System)		12.8	17.6		9.2	
Equipment and Operating Items		22.3	20.0		20.3	
Price	\$10 ⁶	7.85	9.34	1.19	7.51	0.95
DOC	$\frac{\$}{\text{seat n.mi.}}$	1.413 ¹	1.689 ¹	1.18	1.276 ²	0.90
Energy Utilization	$\frac{\text{Btu}}{\text{seat n.mi.}}$	1,339	1,759	1.32	1,288	0.96

¹ DOC based on LH₂ cost = \$3/10⁶ Btu

² DOC based on Jet A cost = \$2/10⁶ Btu = 24.8 /gal

internal tank design for comparison with the Jet A fueled airplane. For a description of the complete rationale leading to selection of internal tank over external tank designs, see Section 4.6 of the final report of the original study (Reference 1).

As might be expected from the low fuel fraction involved in this small payload, short-range mission, the advantage of using hydrogen fuel is largely mitigated by the penalties involved, i.e., tank, insulation weight, and drag increase due to more wetted area. The factor of 2.93 advantage in specific fuel consumption offered by the LH₂ fueled design, operating on the small fuel weight involved, is not sufficient to overcome the 18 percent disadvantage in L/D. Table VII shows almost equal empty weights for the internal tank LH₂ (Aircraft No. 1) and Jet A (Aircraft No. 3) designs and only an 11 percent higher gross weight for the Jet A fueled design. The purchase price of Aircraft No. 3 is lower by 4 percent and energy used in performing the mission is lower by 4 percent.

Table VIII presents a breakdown of costs for the three aircraft. Note that DOC is calculated on the basis of the prescribed fuel costs. Figure 13 shows the DOC versus the fuel cost in \$/GJ ($\$/10^6$ Btu) across the lower edge, and for Jet A fuel in ϕ /gallon at the top. It indicates the high DOC of the external tank LH₂ and almost equal DOC's for the internal LH₂ and the Jet A aircraft for the same fuel price. In other words, for these aircraft LH₂ cannot cost more than Jet A for equal DOC's.

Selected pages of ASSET computer printouts for the internal tank LH₂, external tank LH₂, and Jet A point design aircraft are reproduced in Appendix A-1, A-2 and A-3, respectively.

4.6.1 Noise. - A comparison of noise generated by the two aircraft is presented numerically in Table IX and graphically in Figure 14. The analysis was made using the takeoff and approach paths generated for the respective aircraft in the ASSET program, and using engine parameters and procedures described in Section 4.8.2 of the final report of the previous study (Reference 1).

TABLE VIII. COST COMPARISON OF FINAL DESIGN SHORT RANGE AIRCRAFT

2,780 km (1500 n.mi.) - 130 Pax. - M 0.85

		Aircraft No. 1 (Int. LH ₂)	Aircraft No. 2 (Ext. LH ₂)	Aircraft No. 3 (Jet A)
<u>Development</u>	\$10 ⁶			
Airframe		21.62	27.47	23.68
Engine (Amortized in prod. cost)		0	0	0
TOTAL		21.62	27.47	23.68
<u>Production</u>	\$10 ⁶			
Airframe Cost		5.482	6.222	5.210
Engine (including R&D)		1.530	2.113	1.340
Avionics		0.220	0.220	0.220
R&D Amortization (Airframe)		0.618	0.785	0.677
TOTAL Aircraft Price		7.850	9.340	7.507
<u>Direct Operating Cost</u>	$\frac{\$}{\text{km}}$ ($\frac{\$}{\text{n.mi.}}$)			
Crew		0.228 (0.422)	0.227 (0.420)	0.228 (0.423)
Maintenance				
Airframe Labor (Including Burden)		0.072 (0.134)	0.078 (0.145)	0.070 (0.129)
Engine Labor (Including Burden)		0.029 (0.053)	0.035 (0.064)	0.045 (0.084)
Airframe Material		0.037 (0.069)	0.043 (0.079)	0.036 (0.067)
Engine Material		0.037 (0.069)	0.051 (0.095)	0.051 (0.095)
Fuel* and Oil	$\frac{\$}{\text{km}}$ ($\frac{\$}{\text{n.mi.}}$)	0.296 (0.549)	0.389 (0.721)	0.185 (0.342)
Insurance		0.060 (0.111)	0.071 (0.132)	0.058 (0.107)
Depreciation		0.332 (0.430)	0.278 (0.514)	0.222 (0.412)
TOTAL DOC		0.992 (1.837)	1.17 (2.170)	0.896 (1.659)
TOTAL Unit DOC	$\frac{\$}{\text{seat km}}$ ($\frac{\$}{\text{seat n.mi.}}$)	0.763 (1.413)	0.901 (1.670)	0.689 (1.276)

*Fuel Cost:

Jet A = \$1.90/GJ ($\$2/10^6$ Btu = 24.8¢/gal = 3.68¢/lb)

LH₂ = \$2.85/GJ ($\$3/10^6$ Btu = 15.48¢/lb)

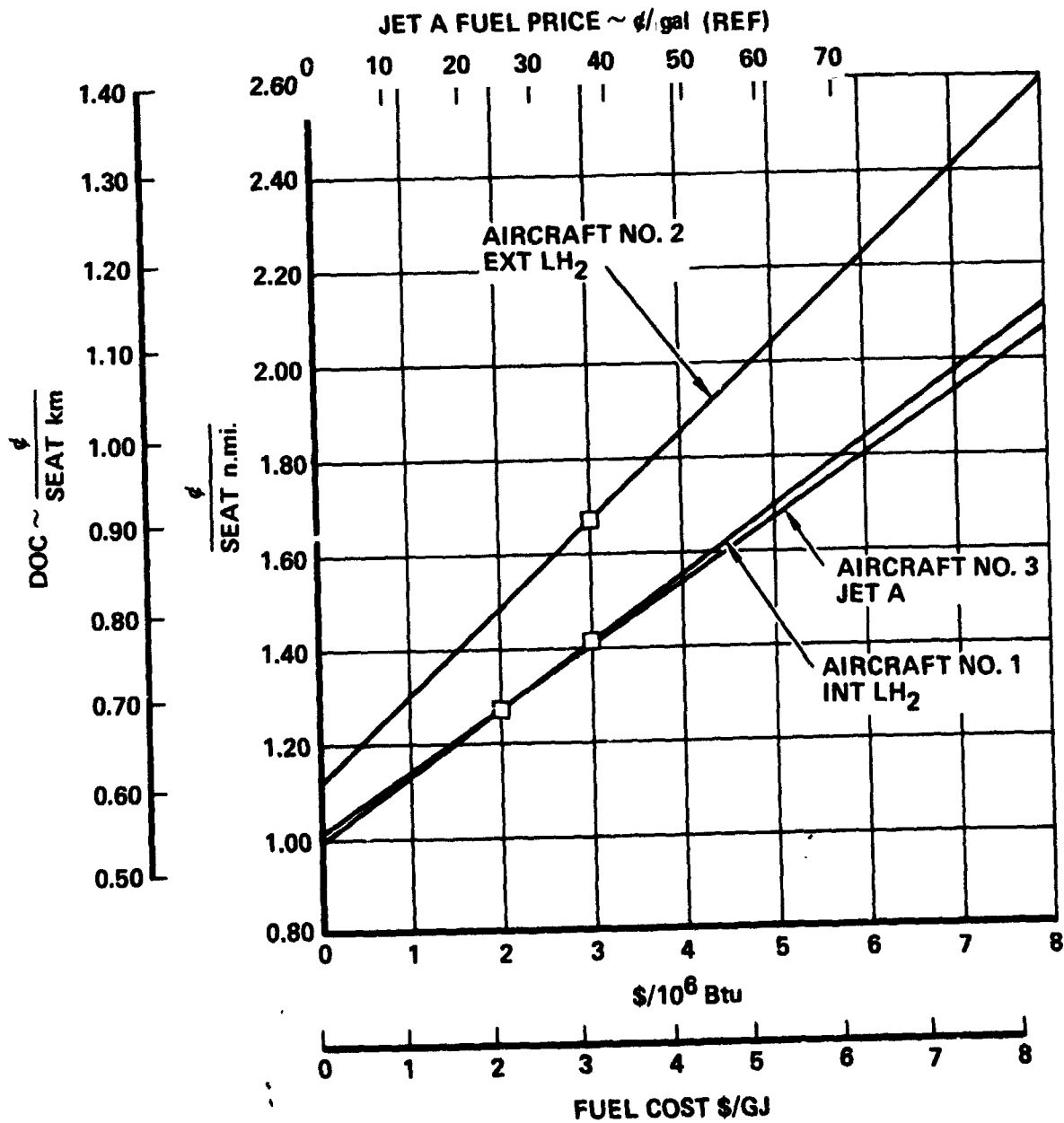
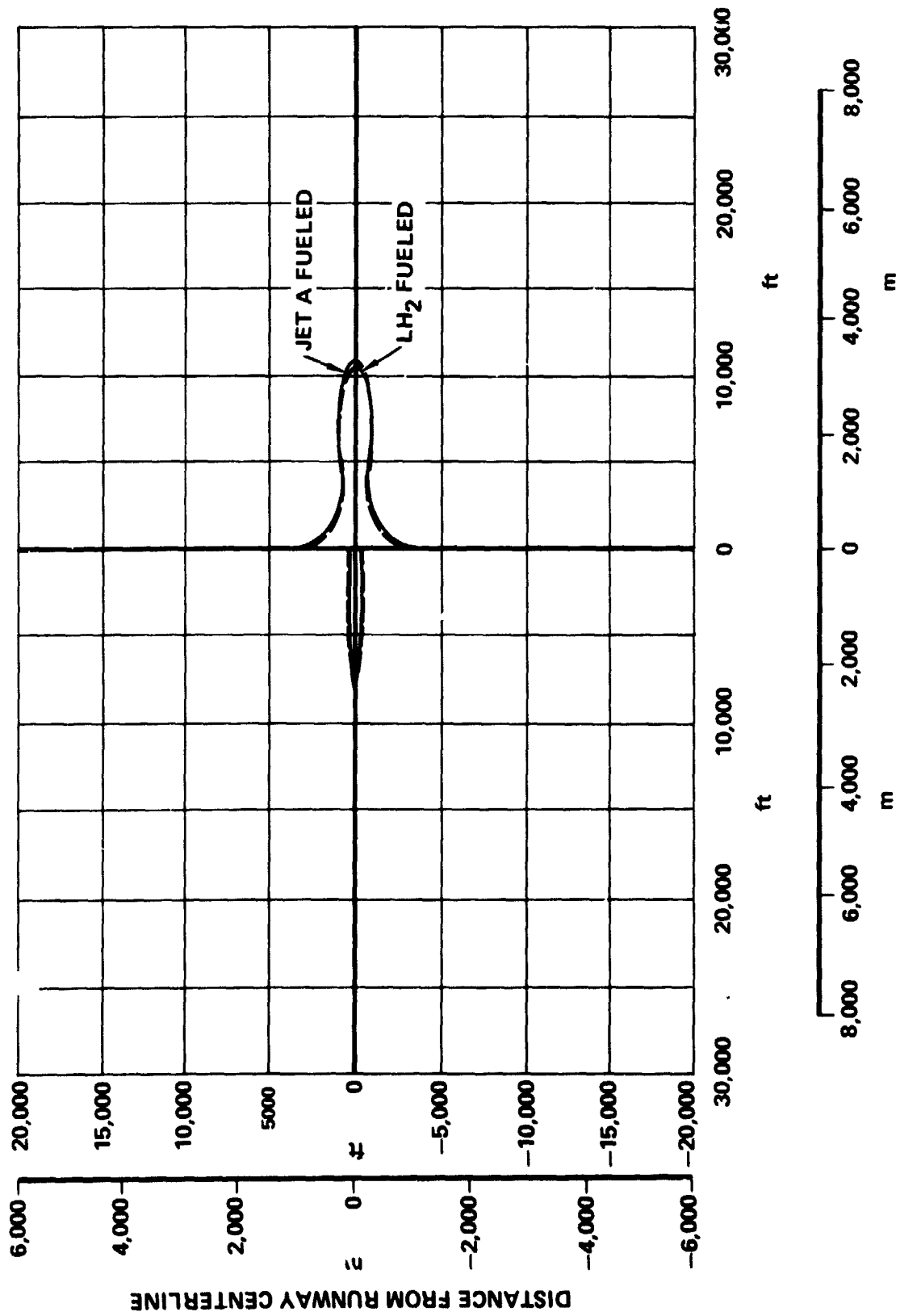


Figure 13. DOC Versus Fuel Cost - 1500 n.mi., 130 Pax Aircraft

TABLE IX. NOISE EVALUATION - SHORT RANGE AIRCRAFT

Airplane No.	1	3
Number of Engines	2	2
Fuel	LH ₂	Jet A
Gross Weight	kg (lb.) 44,570 (98,260)	49,288 (108,660)
FAR 36 <u>Flyover</u> Level (EPNdB)	79.2	79.2
Limit Per NPRM 75-37	87.6	88.2
FAR 36 <u>Sideline</u> Level (EPNdB)	85.5	85.7
Limit Per NPRM 75-37	93.7	94.0
FAR 36 <u>Approach</u> Level (EPNdB)	91.1	90.3
Limit Per NPRM 75-37	98.8	99.1
Enclosed "Footprint" Contour Area		
	<u>km²</u>	<u>st.mi.²</u>
80 EPNdB - Takeoff	8.03	3.10
- Approach	<u>6.32</u>	<u>2.44</u>
- Total	14.35	5.54
90 EPNdB - Takeoff	1.92	0.74
- Approach	<u>.47</u>	<u>0.18</u>
- Total	2.39	0.92
	<u>km²</u>	<u>st.mi.²</u>
	7.56	2.92
	<u>5.36</u>	<u>2.07</u>
	12.92	4.99
	1.94	0.75
	<u>.36</u>	<u>0.14</u>
	2.30	0.89



DISTANCE TO THRESHOLD DISTANCE FROM BRAKE RELEASE

Figure 14. 90 EPNdB Contour Comparison - Short Range Aircraft

Noise limits which are listed in the table for comparison with the values calculated for the subject aircraft are calculated according to the recently published Notice of Proposed Rule Making (NPRM) (Reference 3) for revision of the FAR Part 36 noise certification requirements. The final format and limits of a revised FAR Part 36 will probably be fairly close to the NPRM.

The airplane takeoff performance conditions of 305 m (1000 ft) elevation runway, 32.2°C (90°F) day, are not consistent with the sea level, 25°C (77°F), reference conditions of FAR Part 36, or the proposed change thereto. This will tend to make some of the results conservative. The approach noise predictions, however, are probably slightly too low because airframe noise was not included.

The aircraft designed for the short range mission are essentially equal in noise characteristics. Both are significantly quieter than the limit noise calculated by the proposed standard; viz., 8.4 and 9 EPNdB quieter in flyover, 8.2 and 8.3 EPNdB quieter in sideline, and 7.7 and 8.8 EPNdB quieter in approach respectively, for the LH₂ and Jet A aircraft.

The LH₂ airplane is slightly noisier in approach for reasons explained in Reference 1. Compared to the Jet A design, it has smaller engines, lower L/D, and in approach it has approximately equal weight. Consequently, the LH₂ aircraft is required to operate its engines at more advanced throttle setting to maintain the 3 degree glide slope. This accounts for the fact Aircraft No. 1 has a slightly larger footprint area, for both the 80 and the 90 EPNdB contours. The area of the 90 EPNdB contour for the LH₂ airplane is 2.39 km² (0.92 mi²) vs 2.30 km² (0.89 mi²) for the Jet A design. These areas are the total of approach plus takeoff. They are less than half the noise goal specified in the study guidelines.

5. MEDIUM RANGE AIRCRAFT

5.1 Design Requirements

The medium range aircraft are designed to meet the following requirements and constraints:

- 5560 km (3000 n.mi.) design range
- 200 passengers plus baggage and cargo for a total payload of 19,960 kg (44,000 lb)
- Maximum FAR takeoff field length of 2438 m (8000 ft)
- Minimum initial cruise altitude of 10,360 m (34,000 ft)
- Reserve fuel per ATA domestic regulations
- Maximum approach speed of 69.4 m/s (135 KEAS) for aircraft weight corresponding to end of design range.

5.2 Configuration Selection

Based on the study of alternate configurations reported in Section 4.2 on Reference 1, the medium range configurations are low-winged aircraft of conventional appearance with four wing-mounted engines. This requires a minimum 2.7 percent gradient during the critical second segment climb with an engine out. The external tank LH₂ design (Aircraft No. 5) has tanks mounted above the wing at the inboard engine position. The internal tank LH₂ aircraft (No. 4) has tanks located fore and aft of the passenger compartment.

5.3 LH₂ Internal Tank Airplane (Aircraft No. 4)

5.3.1 Aspect Ratio Selection. - The method of generation of data for the parametric aircraft evaluation, and the basis for selection of an aspect ratio of 9.5 for minimum DOC, is the same as previously described for the short range aircraft in Section 4.3.

5.3.2 Configuration Description. - A general arrangement drawing of the LH₂ internal tank, Mach 0.85, 5560 km (3000 n.mi.), 200 passenger aircraft is shown in Figure 15. Specific features of the design are as follows:

Fuselage: The passenger compartment is located in the central section of the fuselage. Liquid hydrogen fuel tanks are located fore and aft of the passenger compartment. They occupy the full available cross section of the fuselage, except for provision for protective, crushable structure around the bottom areas. No provision was made for a passageway through or around the forward tank to permit movement between flight station and passenger compartment. The flight station is provided with special lavatory and galley facilities.

Passenger accommodations are shown in Figure 16 which illustrates the 10/90 percent class mix and seat spacing of 0.965 m (38 in.) and 0.86 m (34 in.), respectively, for first class and coach. Six abreast seating is used in first class and eight in coach. Provision for doors, lavatory, and galley facilities is in accordance with the requirements of FAR 25 and current widebody standards. Separate galleys are provided for first class and coach sections.

All cargo is contained in the pressurized fuselage below the cabin floor where space is provided for nine cargo containers plus additional space for loose cargo.

Wing: The wing has an aspect ratio of 9.5, thickness ratio of 10 percent and a sweep angle of 30°. The high lift devices include 15 percent leading edge slats and 35 percent double-slotted flaps where shown. Spoilers are used in flight for direct lift control, and for landing ground run deceleration. Conventional ailerons are fitted outboard of the flaps.

Landing Gear: The main gear consists of two four-wheel bogies mounted aft of the rear spar. They retract inward into the fuselage. The space between the retracted gear contains the hydraulic service center. The forward gear is a forward retracting two-wheel strut arrangement.

Hydrogen Tank and Systems: The hydrogen tank structural concept is the integral type. All aircraft structural loads in addition to the fuel dynamic and pressure loads are taken by the tank shell. Loads are transferred from the vehicle structure to the tank at each end by low heat-leak boron-reinforced fiberglass tubes arranged in an interconnect truss structure. Six-and-one-half inches of closed-cell plastic foam insulation, e.g., Rohacell 41S, covers the tank. This is wrapped by a vapor shield (Kapton) which is to prevent cryopumping in event a crack develops in the foam insulation. A fiberglass reinforced composite layer covers the entire tank section to provide a smooth aerodynamic surface, and protection from physical damage.

CHARACTERISTICS	WING	HORIZ. TAIL	VERT. TAIL
AREA M ² (SQ FT)	48.8 (1602.3)	19.8 (212.9)	15.6 (167.7)
ASPECT RATIO	9.5	4.5	1.6
SPAN M (FT)	37.61 (123.4)	9.43 (31.0)	4.99 (16.4)
ROOT CHORD M (IN)	6.09 (239.7)	3.22 (126.8)	4.80 (188.8)
TIP CHORD M (IN)	1.83 (71.9)	0.97 (38.0)	1.44 (56.6)
TAPER RATIO	0.3	0.3	0.3
MAC Y (IN)	4.34 (170.9)	2.30 (90.4)	3.42 (134.6)
SWEEP RAD (DEG)	0.524 (30)	0.524 (30)	0.524 (30)
T/C ROOT (%)	10	9	9
T/C TIP (%)	10	9	9

DESIGN GROSS WT. - 81,403 KG. (179,459 LB.)

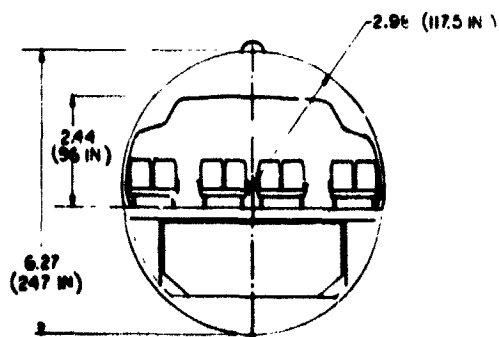
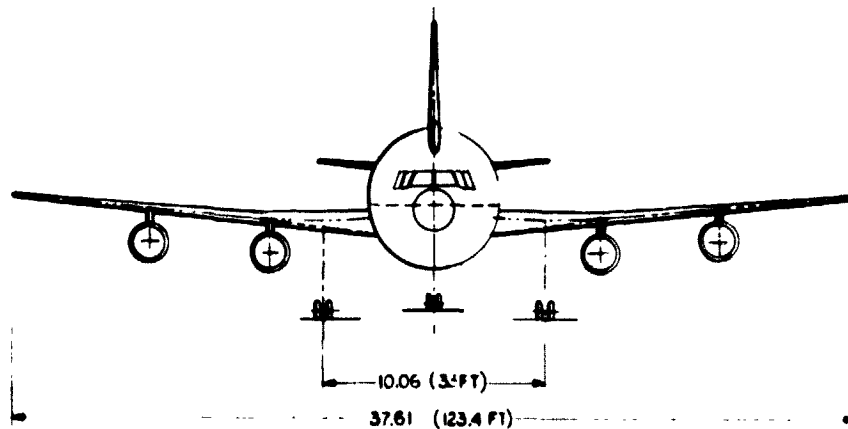
POWER PLANT - (2) TURBOFAN

INSTALLED THRUST (EA.) - 66,849 N. (15,029 LB.)

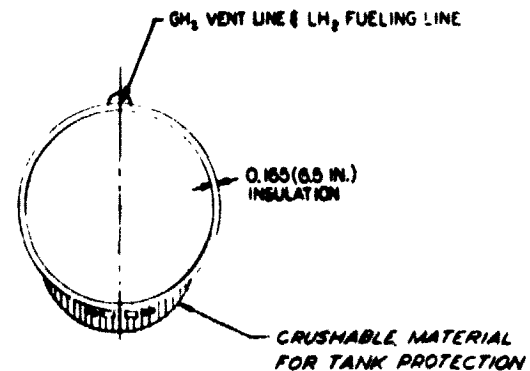
PASSENGERS - 200

FUEL LH₂ - 9,492 KG (20,924 LB.)

RANGE - 5,559 KM. (3,000 NM.)



SECTION A-A
SCALE 1/30



SECTION B-B
SCALE 1/30

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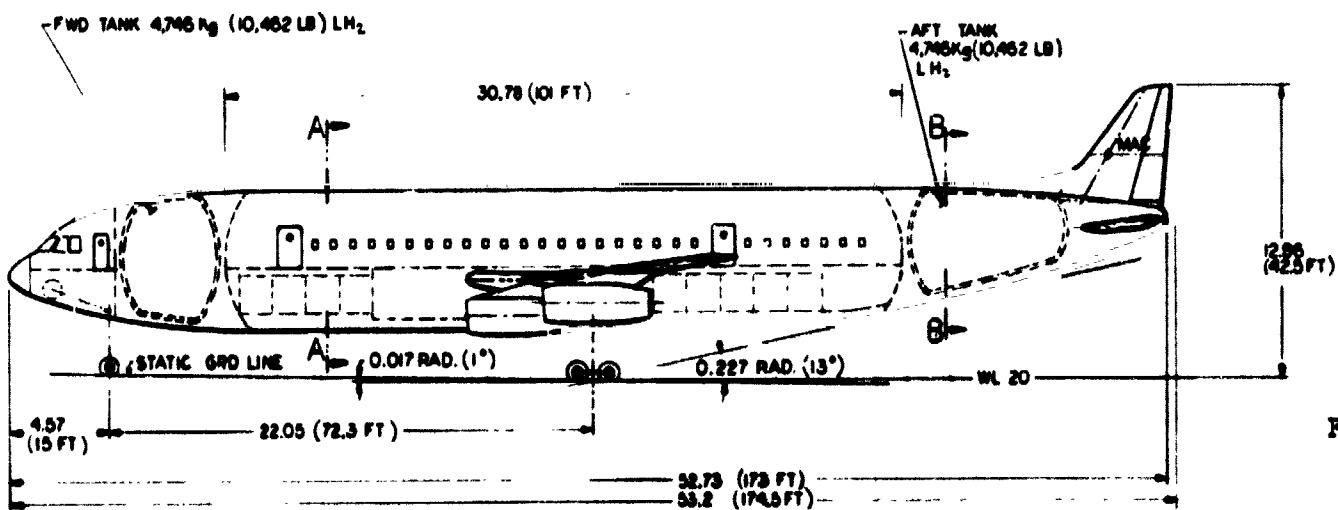
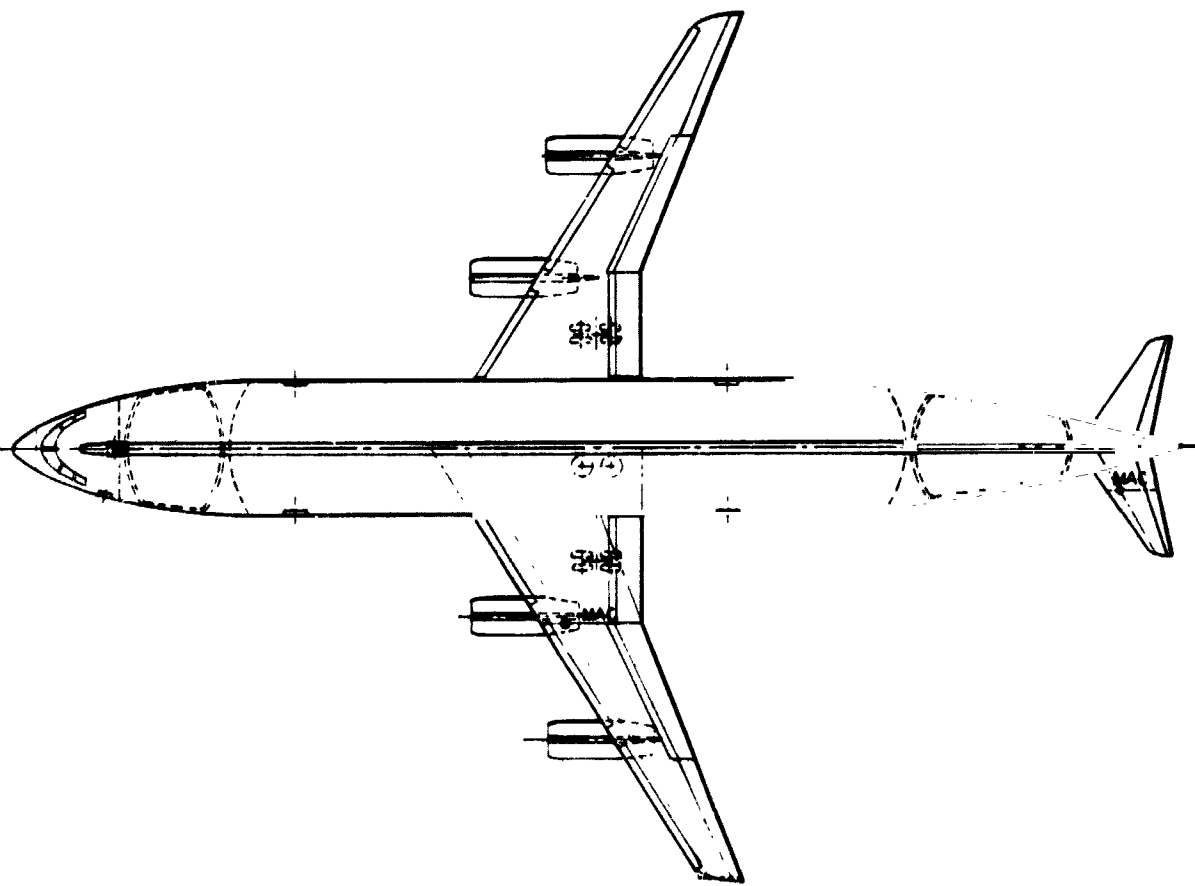
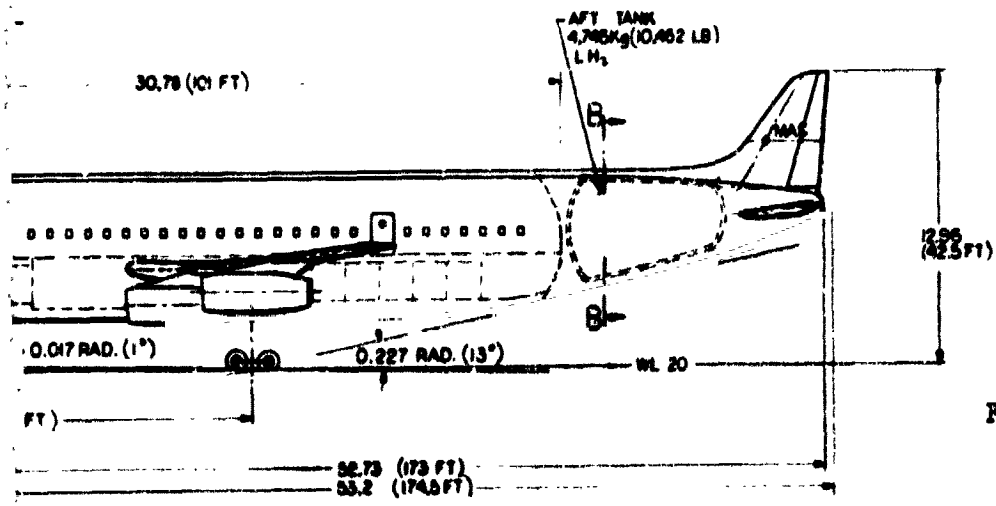
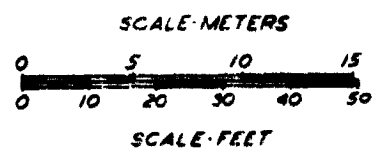
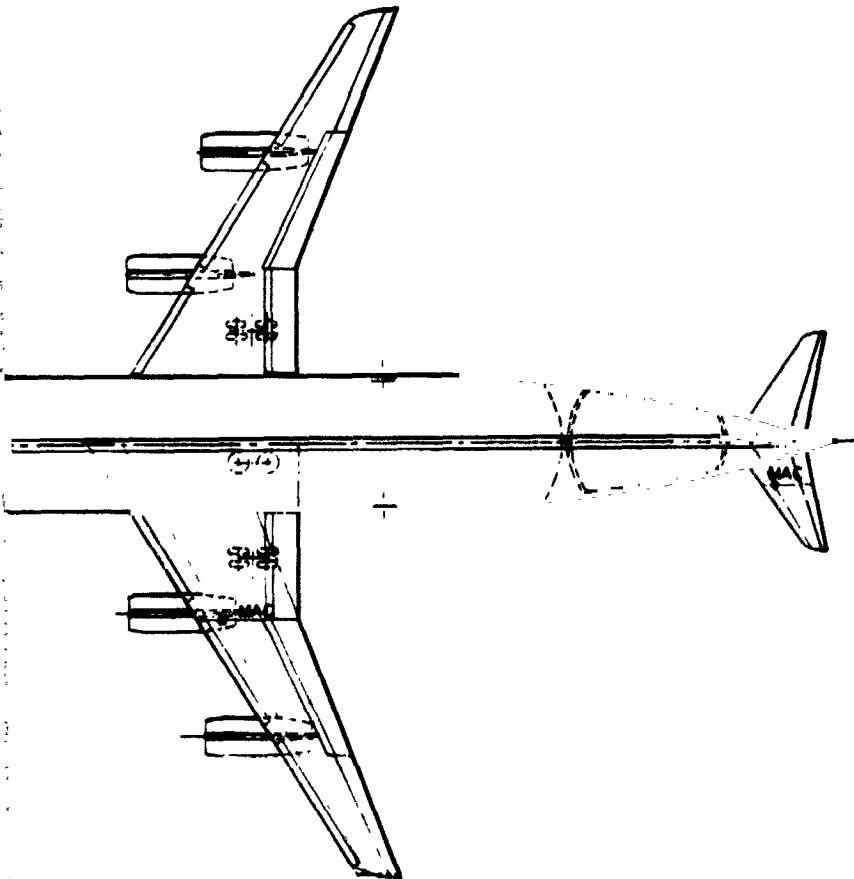


Figure 15. General Medium Internal

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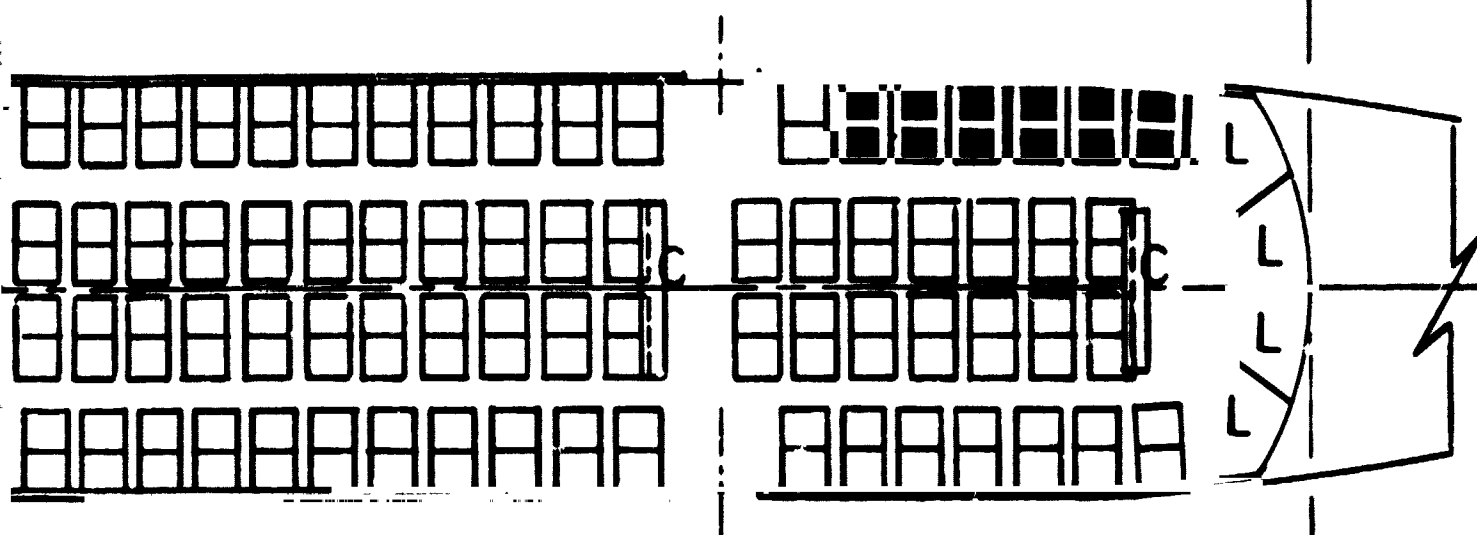
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Figure 15. General Arrangement:
Medium Range, LH₂
Internal Tank Transport

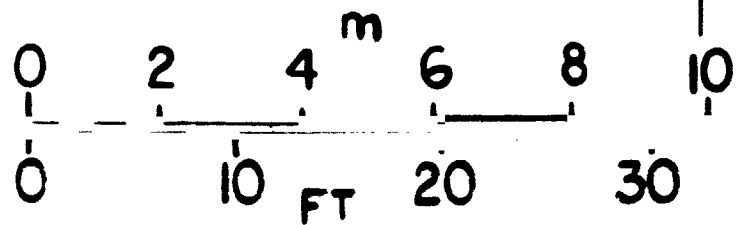
49
FOLDOUT FRAMES

COACH CLASS

8 A/B



0.78 m (101 FT)



SPACING
SPACING

Figure 16. Interior Arrangement:
200 Pax Transport, LH₂
Internal Tank

51
FOLDOUT PAGE 2

5.3.3 Vehicle Data. - All weight, performance, and cost data are presented in Section 5.6.

5.4 LH₂ External Tank Airplane (Aircraft No. 5)

5.4.1 Aspect Ratio Selection. - The aspect ratio selected for this aircraft is 9.5 based on minimum DOC.

5.4.2 Configuration Description. - The general arrangement of this aircraft design is shown in Figure 17. This configuration is similar to the short range external tank LH₂ aircraft described in Section 4.4.2, with the exception that this design has four engines. Also, since the ratio of tank wetted area to volume is more favorable, only 6.5 inches of tank insulation are required to restrict boil-off to the desired fraction. The seating arrangement is shown in Figure 18. A 10/90 percent first-to-coach class mix is used with a seat spacing of 0.965 m (38 in.) in first, and 0.86 m (34 in.) in coach class. Six abreast seating is used in first class and eight in coach. An under-floor galley is used in this configuration, with elevators as shown to provide access. Five lavatories and provision for overhead coat storage is also shown.

5.4.3 Vehicle Data. - For performance, weight, and cost data see Section 5.6.

5.5 Jet A Airplane (Aircraft No. 6)

5.5.1 Aspect Ratio Selection. - The aspect ratio which provides minimum DOC for this aircraft is 9.75.

5.5.2 Configuration Description. - The general arrangement is shown in Figure 19. The aircraft design is conventional with all fuel carried in the wing box. The fuselage size and arrangement is the same as that of the external tank LH₂ aircraft described in Section 5.4.2.

5.5.3 Vehicle Data. - All weight, performance, and cost data is presented in Section 5.6.

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5.6 Comparison of Medium Range Aircraft

Table X presents a summary of the characteristics of the three medium range, minimum DOC aircraft which meet the specified performance requirements.

Comparison of the external to the internal tank LH₂ aircraft shows that the internal tank version is superior in every significant respect. Aircraft No. 5 is 16 percent heavier in gross weight, 20 percent heavier in empty weight, costs 22 percent more in price and DOC, and uses 20 percent more fuel. Consequently the internal tank LH₂ design (Aircraft No. 4) was selected for comparison with the Jet A aircraft (Aircraft No. 6).

The comparison of the internal tank LH₂ aircraft and the corresponding Jet A fueled design for the medium range mission is also presented in Table X. The LH₂ fueled aircraft shows marginally superior characteristics compared to the Jet A design. It is considerably lighter in gross weight but slightly heavier in empty weight. The purchase price of the Jet A design is 4 percent less, but the LH₂ vehicle uses 5 percent less energy in performing the design mission.

Table XI shows a cost comparison breakdown for the three aircraft indicating a slightly higher price for the internal LH₂ compared to Jet A. Note that the DOC values shown in the table reflect use of arbitrarily selected values of fuel costs. Figure 20 shows the DOC versus fuel cost in \$/GJ ($\$/10^6$ Btu.). Equivalent cost of Jet A fuel expressed in ¢/gallon is shown at the top of the figure. The figure indicates the higher DOC of the external compared to the internal tank LH₂ aircraft and a slight advantage for the internal LH₂ compared to the Jet A design for equal fuel cost. Also shown is the average price paid by domestic truck airlines for Jet A fuel in September 1975 (28.6 ¢/gallon). At that price a differential of \$.133/GJ ($\$.14/10^6$ Btu's) more could be paid for LH₂ and still maintain equal DOC's. This would increase slightly as the cost of Jet A increases.

Detailed ASSET computer printouts for aircraft No's. 4, 5, and 6 are shown in Appendix A-4, A-5 and A-6, respectively.

CHARACTERISTICS	WING	HORIZ. TAIL	VERT. TAIL
AREA M ² (SQ FT)	174.2 (1874.7)	32.4 (349.2)	24.6 (264.6)
ASPECT RATIO	9.5	4.5	1.6
SPAN METERS (FT)	40.67 (133.4)	12.08 (39.6)	6.28 (20.6)
ROOT CHORD M (IN)	6.12 (240.8)	4.14 (162.8)	6.02 (237.1)
TIP CHORD M (IN)	2.45 96.3	1.24 48.8	1.81 71.1
TAPER RATIO	0.4	0.3	0.3
MAC METERS (IN)	4.54 (178.9)	2.95 (116.0)	4.29 (169.0)
SWEEP RAD (DEG)	0.524 (30)	0.524 (30)	0.524 (30)
T/C ROOT (°)	10	9	9
T/C TIP (°)	10	9	9

DESIGN GROSS WT. - 94,052 KG (207,346 LB.)

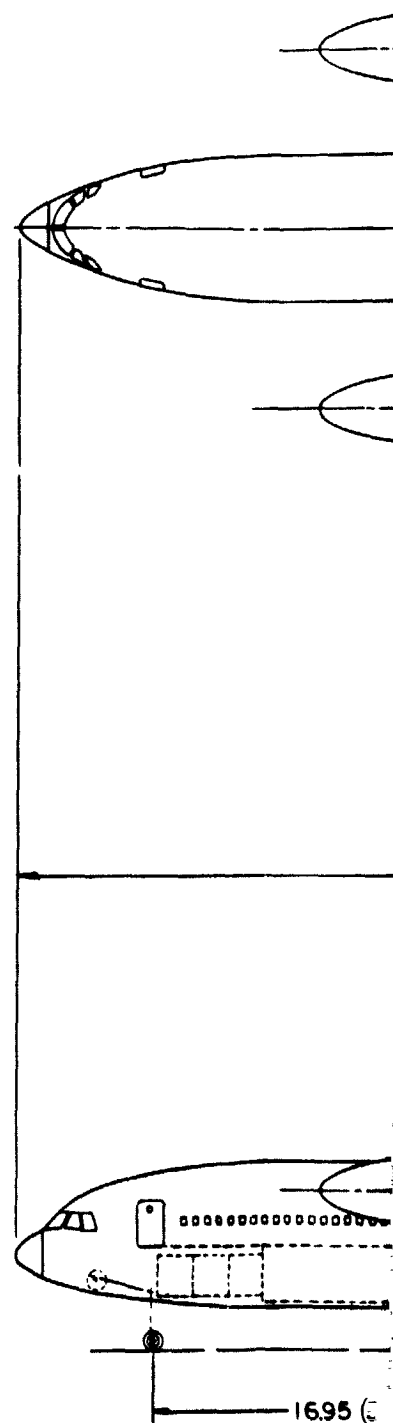
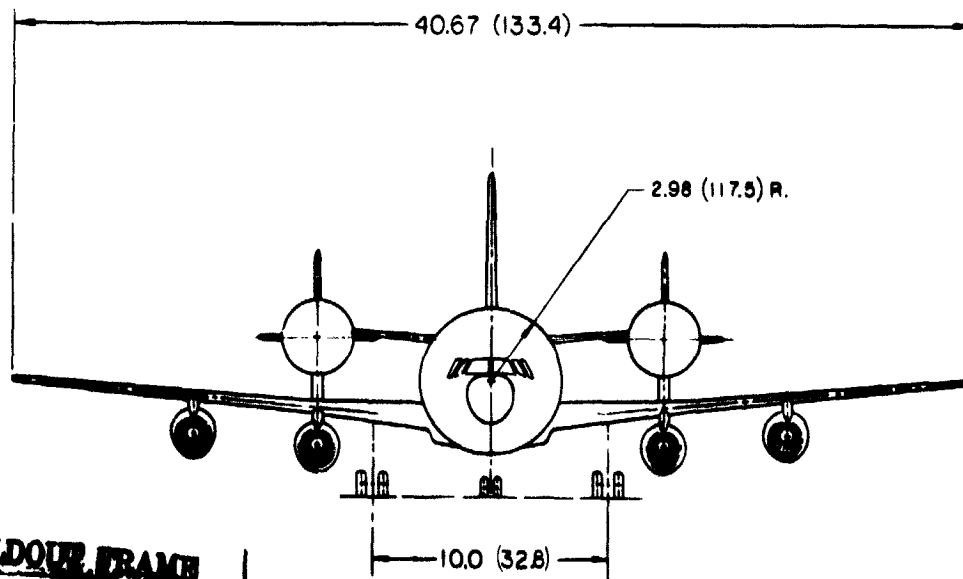
POWER PLANT - 2 TURBOFAN

INSTALLED THRUST (EA.) - 99,141 N. (22,289 LB.)

PASSENGERS - 200

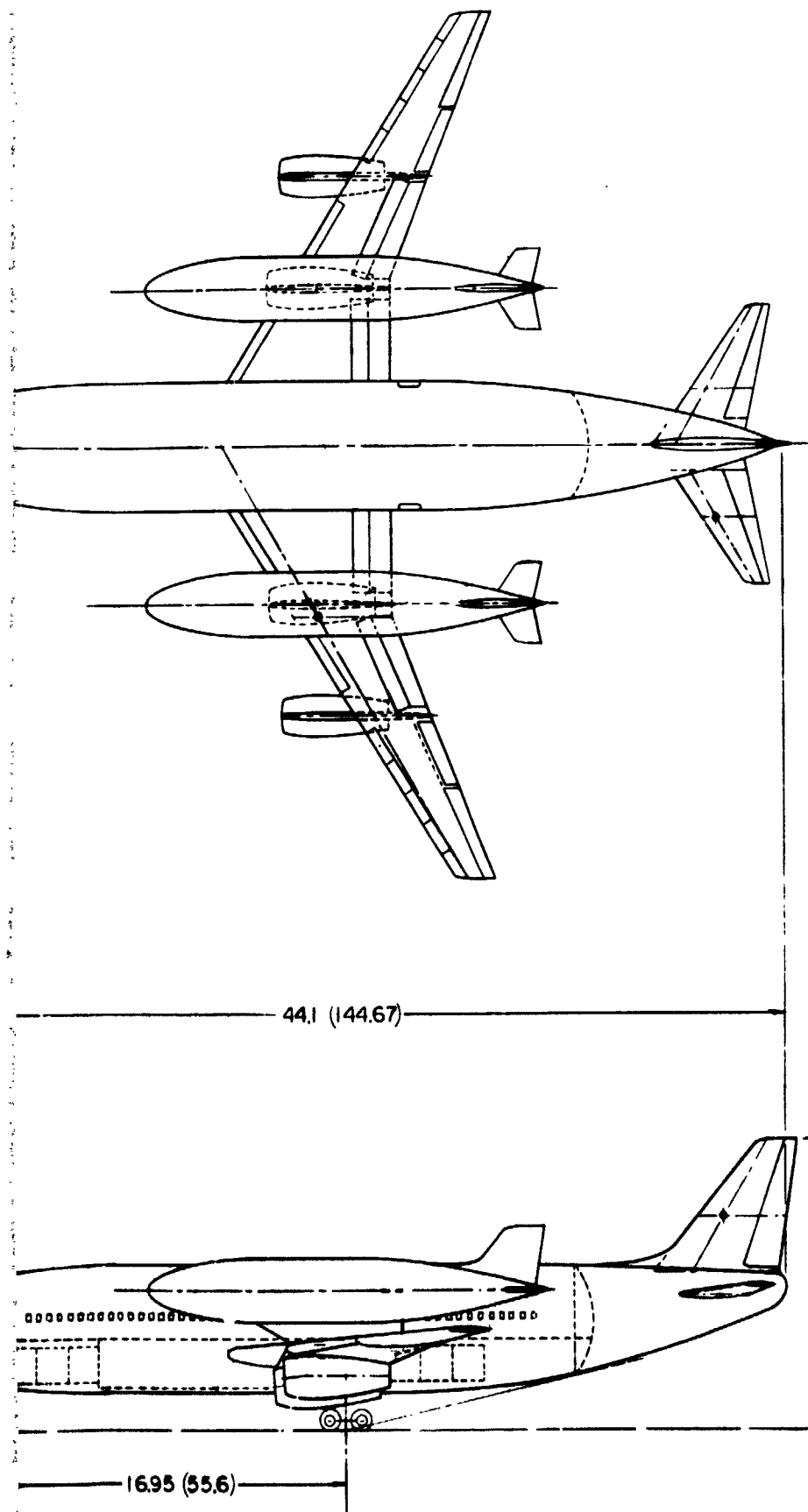
FUEL LH₂ - 12,351 KG. (27,229 LB.)

RANGE - 5,559 KM. (3,000 N.M.)



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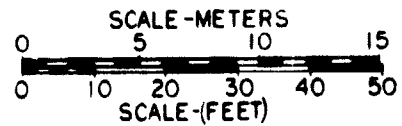
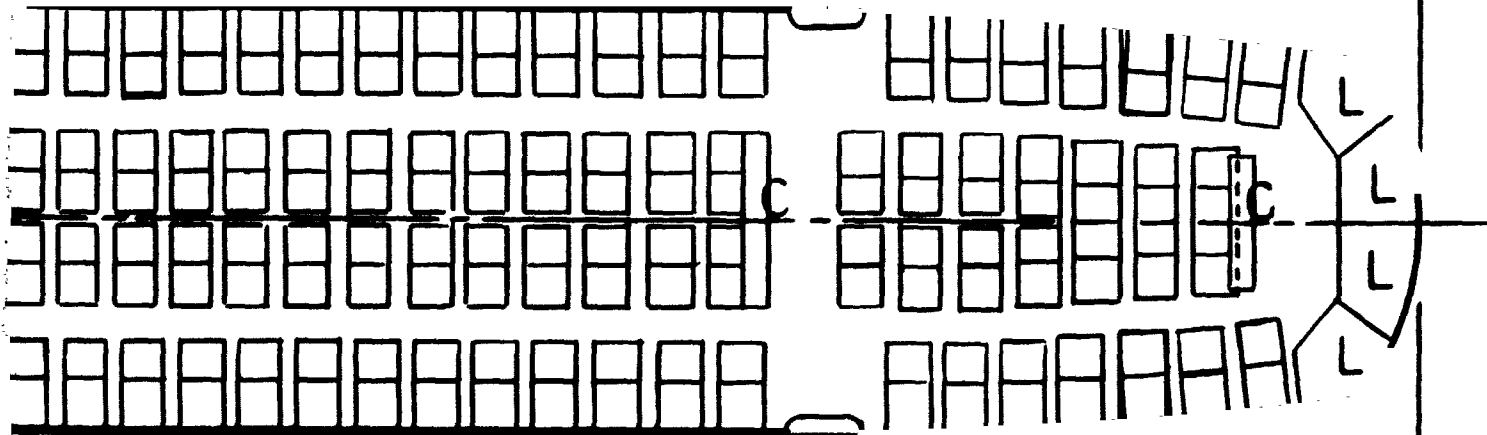


Figure 17. General Arrangement:
Medium Range, LH₂
External Tank Transport

COACH CLASS

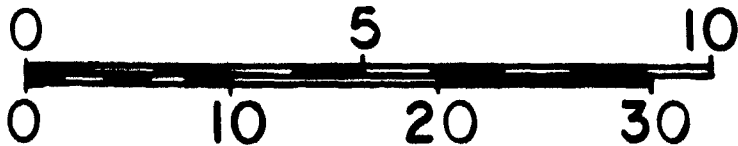
8 A/B



30.9 M (101.4 FT)

IN) SPACING
IN) SPACING

SCALE-METERS



SCALE FEET

Figure 18. Internal Arrangement:
200 Pax Transport, LH₂
External Tank

BOLDOUT FRAME 2

CHARACTERISTICS	WING	HORIZ. TAIL	VERT. TAIL
AREA M ² (SQ FT)	154.5 (1663.5)	27.5 (296.3)	20.6 (221.6)
ASPECT RATIO	9.75	4.5	1.6
SPAN M (FT)	38.82 (127.4)	11.13 (36.5)	5.74 (18.8)
ROOT CHORD M (IN)	6.12 (241.1)	3.81 (149.9)	5.52 (217.3)
TIP CHORD M (IN)	1.84 (72.3)	1.14 (45.0)	1.66 (65.2)
TAPER RATIO	0.3	0.3	0.3
MAC M (IN)	4.73 (171.9)	2.71 (106.8)	3.93 (154.9)
SWEEP RAD. (DEG)	0.524 (30)	0.524 (30)	0.524 (30)
T/C ROOT (°)	10	9	9
T/C TIP (°)	10	9	9

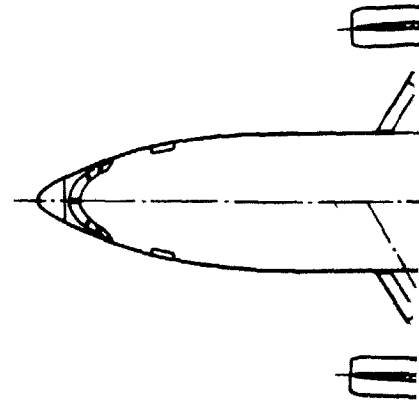
DESIGN GROSS WT. - 98,396 KG. (216,923 LB.)

POWER PLANT - (2) TURBOFANS
 INSTALLED THRUST (EA.) - 68,023 N. (15,293 LB.)

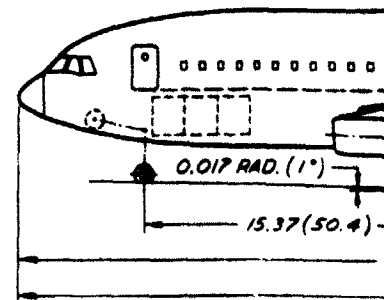
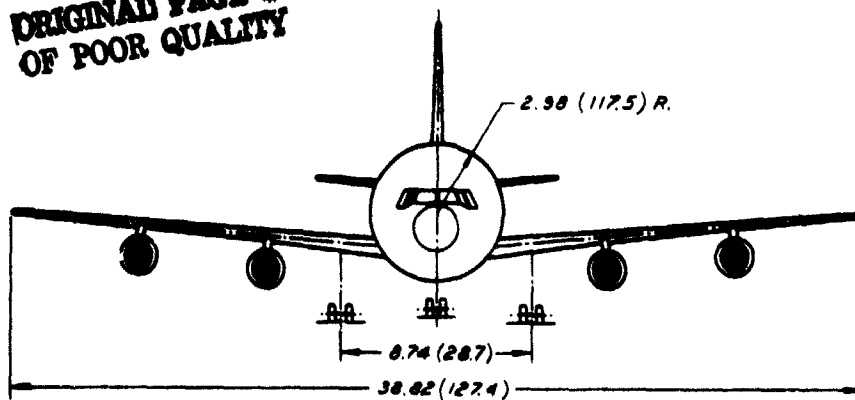
PASSENGERS - 200

FUEL (JET A) - 27,731 KG. (61,136 LB.)

RANGE - 5,559 KM. (3,000 N.M.)

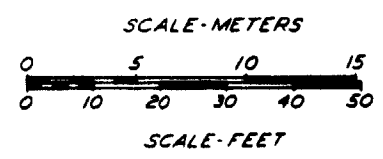
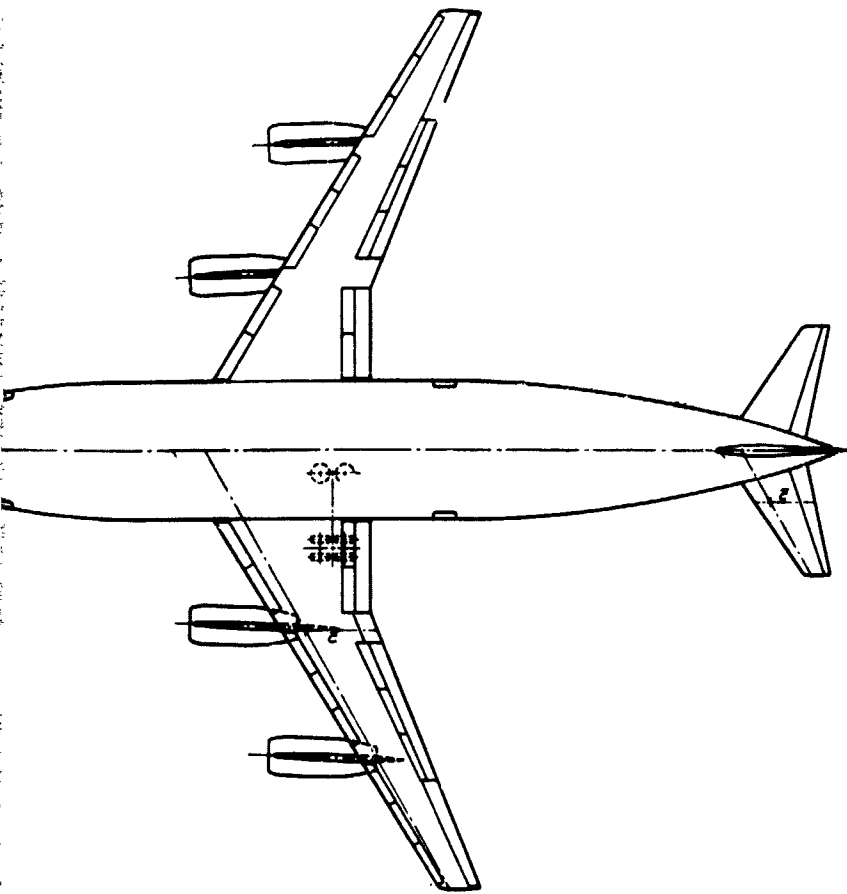


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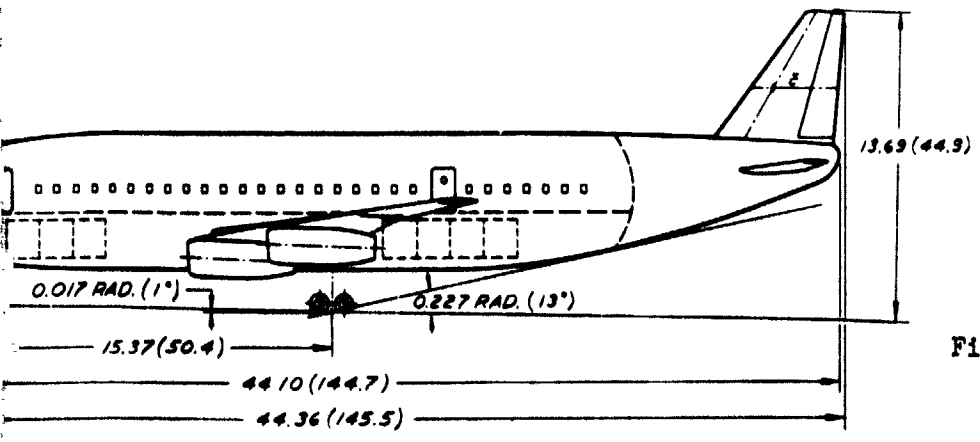


Figure 19. General Arrangement:
Medium Range, Jet Fuel

HOLD ON FRAME 2

TABLE X. COMPARISON OF FINAL DESIGN MEDIUM RANGE AIRCRAFT
(S.I. UNITS)
(5560 km RANGE - 200 PAX - Mach 0.85)

$W_{pay} = 19,960 \text{ kg}$

		Aircraft No. 4 (Int. LH ₂)	Aircraft No. 5 (Ext. LH ₂)	Ratio: (Ext.) (Int.)	Aircraft No. 6 (Jet A)	Ratio: (Jet A) (Int. LH ₂)
Gross Wt	kg	81,400	94,050	1.16	98,400	1.21
Total Fuel	kg	9,490	12,350	1.30	27,730	2.92
Block Fuel	kg	7,724	10,000	1.29	22,710	2.94
Operating Empty Wt	kg	51,950	61,740	1.19	50,710	0.98
Empty Wt	kg	47,420	57,050	1.20	46,270	0.98
Aspect Ratio		9.50	9.50		9.75	
Wing Area	m ²	149	174	1.17	155	1.04
Sweep	deg	30	30		30	
Span	m	38	41	1.08	39	1.03
Fus Length	m	53	44	0.83	44	0.83
L/D - Cruise		13.8	12.3	0.89	15.3	1.11
SFC - Cruise	kg/daN hr	.215	.215		.627	2.92
Initial Cruise Altitude	m	10,670	11,580		10,360	
Wing Loading	kg/m ²	547	540		637	
Thrust/Weight	N/kg	3.28	4.21	1.28	2.76	0.84
No. Engines		4	4		4	
Thrust Per Engine	N	66,850	99,140	1.48	68,020	1.02
FAR T.O. Distance	m	1,640	1,290	0.79	2,430	1.48
FAR Ldg. Distance	m	1,760	1,755		1,757	
2nd Seg. Climb Grad. (Eng out)		0.094	0.146	1.55	0.066	0.70
Approach Speed	m/s	69	69		69	
Weight Fractions - Percent						
Fuel		11.7	13.1		28.2	
Payload		24.5	21.2		20.3	
Structure		31.0	30.7		27.5	
Propulsion (Includes Fuel System)		12.5	17.2		7.1	
Equipment and Operating Items		20.3	17.8		16.9	
Price	\$10 ⁶	13.95	17.07	1.22	13.33	0.96
DOC	$\frac{\$}{\text{seat km}}$	0.723 ¹	0.878 ¹	0.122	0.850 ²	0.90
Energy Utilization	$\frac{\text{kJ}}{\text{seat km}}$	833	1,078	1.29	875	1.05

¹DOC based of LH₂ cost = \$2.85/GJ

²DOC based on Jet A cost = \$1.90/GJ

TABLE X. COMPARISON OF FINAL DESIGN MEDIUM RANGE AIRCRAFT
(U.S. CUSTOMARY UNITS)

(3000 n. mi. RANGE - 200 PAX - Mach 0.85)

$W_{pay} = 44,000$ lbs

		Aircraft No. 4 (Int. LH ₂)	Aircraft No. 5 (Ext. LH ₂)	Ratio (Ext.) (Int.)	Aircraft No. 6 (Jet A)	Ratio (Jet A) (Int. LH ₂)
Gross Wt.	lb	179,460	207,350	1.16	216,920	1.21
Total Fuel	lb	20,920	27,230	1.30	61,140	2.92
Block Fuel	lb	17,030	22,040	1.29	50,080	2.94
Operating Empty Wt	lb	114,540	136,120	1.19	111,790	0.98
Empty Wt	lb	104,530	125,770	1.20	102,000	0.98
Aspect Ratio		9.50	9.50		9.75	
Wing Area	ft ²	1,602	1,875	1.17	1,664	1.04
Sweep	deg	30	30		30	
Span	ft	123.4	133.5	1.08	127.4	1.03
Fus Length	ft	173.4	144.7	0.83	144.7	0.83
L/D - Cruise		13.8	12.3	0.89	15.3	1.11
SFC - Cruise	lb/hr / lb	0.211	0.211		0.516	2.92
Initial Cruise Altitude	ft	35,000	38,000		34,000	
Wing Loading	lb/ft ²	112.0	110.6		130.4	
Thrust/Weight		0.335	0.430	1.28	0.282	0.84
No. Engines		4	4		4	
Thrust per Engine	lb	15,030	22,290	1.48	15,290	1.02
FAR T.O. Distance	ft	5,382	4,235	0.79	7,975	1.48
FAR Ldg. Distance	ft	5,779	5,757		5,763	
2nd Seg. Climb		0.094	0.148	1.55	0.066	0.70
Grad. (Eng out)						
Approach Speed	KEAS	135	135		135	
Weight Fractions - Percent						
Fuel		11.7	13.1		28.2	
Payload		24.5	21.2		20.3	
Structure		31.0	30.7		27.4	
Propulsion (Includes Fuel System)		12.5	17.2		7.2	
Equipment and Operating Items		20.3	17.8		16.9	
Price	\$10 ⁶	13.95	17.07	1.22	13.33	0.96
DOC	¢ seat n.mi	1.338 ¹	1.626 ¹	1.22	1.203 ²	0.90
Energy Utilization	Btu seat n.mi.	1,464	1,895	1.29	1,537	1.05

¹DOC based on LH₂ cost = \$3/10⁶ BTU = 15.48 ¢/lb

²DOC based on Jet A cost = \$2/10⁶ Btu = 24.8¢/gal

TABLE XI. COST COMPARISON OF FINAL DESIGN MEDIUM RANGE AIRCRAFT

5560 km (3000 n.mi.) - 200 Pax - Mach 0.85

	Aircraft No. 4 (Int. LH ₂)	Aircraft No. 5 (Ext. LH ₂)	Aircraft No. 6 (Jet A)
<u>Development</u> $\$10^6$			
Airframe	362.24	469.40	390.66
Engine (Amortized in prod. cost)	0	0	0
TOTAL	362.24	469.40	390.66
<u>Production</u> $\$10^6$			
Airframe Cost	9.880	11.674	9.561
Engine (Including R&D)	2.540	3.559	2.148
Avionics	0.500	0.500	0.500
R&D Amortization (Airframe)	1.035	1.341	1.116
TOTAL Aircraft Price	13.955	17.074	13.325
<u>Direct Operating Cost</u> $\frac{\$}{\text{km}} \left(\frac{\$}{\text{n.mi.}} \right)$			
Crew	0.213 (0.395)	0.213 (0.395)	0.214 (0.396)
Maintenance			
Airframe Labor (Including Burden)	0.092 (0.170)	0.103 (0.191)	0.090 (0.167)
Engine Labor (Including Burden)	0.048 (0.089)	0.058 (0.107)	0.072 (0.134)
Airframe Material	0.053 (0.098)	0.063 (0.116)	0.052 (0.096)
Engine Material	0.054 (0.100)	0.076 (0.141)	0.069 (0.128)
Fuel* and Oil	0.499 (0.924)	0.645 (1.195)	0.339 (0.628)
Insurance	0.10 (0.185)	0.123 (0.227)	0.096 (0.177)
Depreciation	0.386 (0.714)	0.475 (0.879)	0.367 (0.679)
TOTAL DOC	1.445 (2.675)	1.756 (3.251)	1.299 (2.405)
TOTAL Unit DOC $\frac{\$}{\text{seat km}} \left(\frac{\$}{\text{seat n.mi.}} \right)$	0.723 (1.338)	0.878 (1.626)	0.650 (1.203)

*Fuel Cost:

Jet A = \$1.90/GJ ($\$2/10^6$ Btu = 24.8¢/gal = 3.68¢/lb)

LH₂ = \$2.85/GJ ($\$3/10^6$ Btu = 15.48¢/lb)

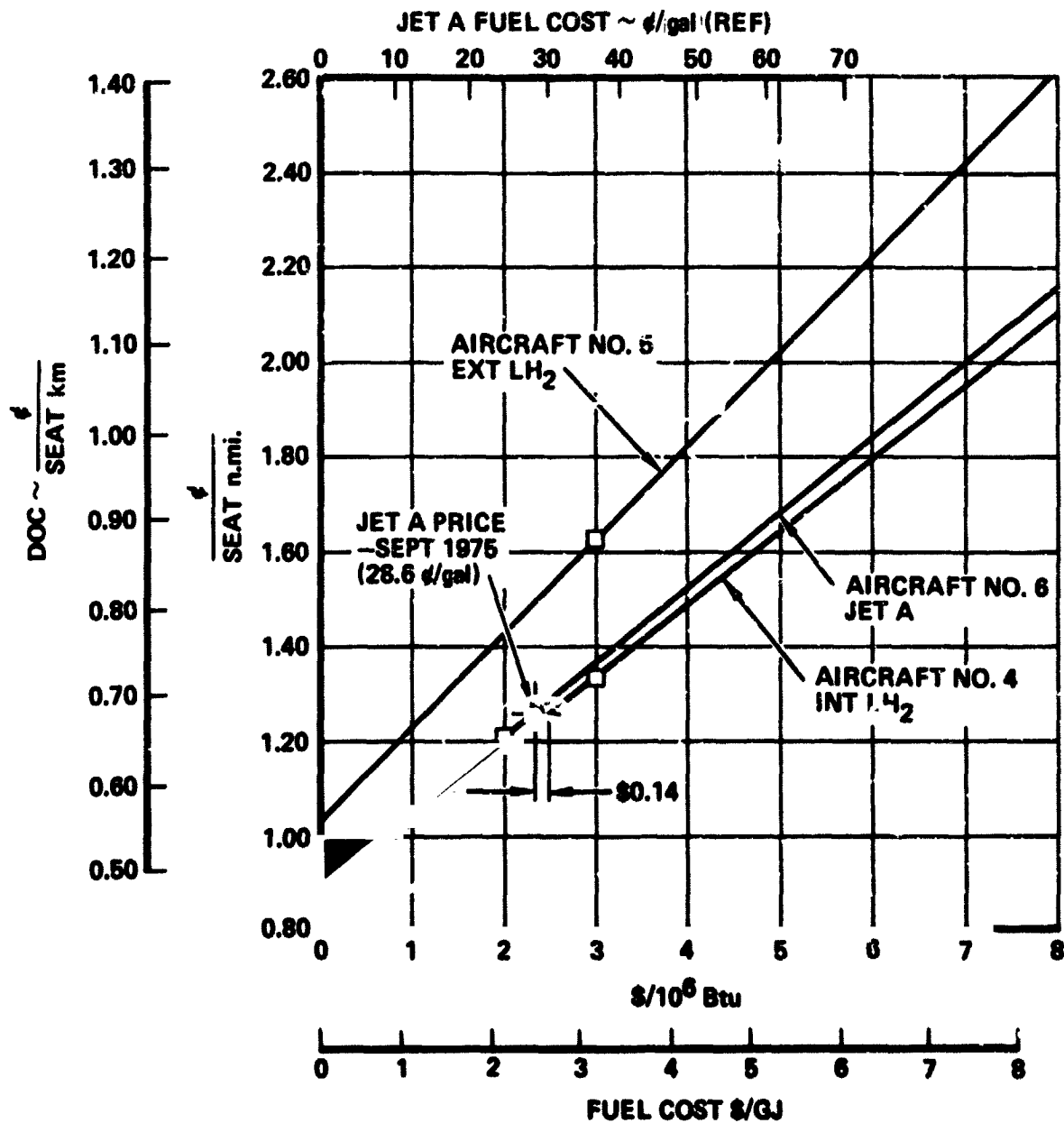


Figure 20. DOC Versus Fuel Cost - 3000 n.mi., 200 Pax Aircraft

5.6.1 Noise. - A comparison of noise generated by the two aircraft is presented numerically in Table XII and graphically in Figure 21. The analysis was made using the takeoff and approach paths generated for the respective aircraft in the ASSET program, and using engine parameters and procedures described in section 4.8.2 of the final report of the previous study (Reference 1).

As noted in section 4.6.1, noise limits which are listed in the table for comparison with the values calculated for the subject aircraft are those according to the recently published Notice of Proposed Rule Making (Reference 3) for revision of the FAR Part 36 noise certification requirements.

The LH₂ aircraft designed for the medium range mission is appreciably quieter in flyover, but slightly noisier in sideline and during approach than its Jet A fueled counterpart. Both are significantly quieter than the limit noise calculated by the proposed standard. The differences are 15.2 and 12.2 EPNdB quieter in flyover, 12.2 and 13.1 EPNdB quieter in sideline, and 7.4 and 8.3 EPNdB quieter in approach, respectively, for the LH₂ and Jet A aircraft.

The LH₂ airplane is slightly noisier in approach for reasons explained in Reference 1 and reviewed in section 4.6.1. As shown in Table XII, the area of the 90 EPNdB contour for the LH₂ airplane is 3.21 km² (1.24 mi²) vs 3.75 km² (1.45 mi²) for the Jet A design. These areas are the total of approach plus takeoff. They are both less than the noise goal listed in the study guidelines, Table II.

TABLE XII. NOISE EVALUATION - MEDIUM RANGE AIRCRAFT

Airplane No.	4	6		
Number of Engines	4	6		
Fuel	LH ₂	Jet A		
Gross Weight - kg (lb)	81,403 (179,460)	98,395 (216,920)		
FAR 36 <u>Flyover</u> Level (EPNdB)	81.8	85.9		
Limit per NPRM 75-37	97.0	98.1		
FAR 36 <u>Sideline</u> Level	86.4	86.0		
Limit Per NPRM 75-37	98.6	99.1		
FAR 36 <u>Approach</u> Level (EPNdB)	93.1	92.8		
Limit Per NPRM 75-37	100.5	101.1		
Enclosed "Footprint" Contour Area				
	<u>km²</u>	<u>st.mi.²</u>	<u>km²</u>	<u>st.mi.²</u>
80 EPNdB - Takeoff	10.33	3.99	12.48	4.82
- Approach	<u>8.08</u>	<u>3.12</u>	<u>7.85</u>	<u>3.03</u>
- Total	18.41	7.11	20.33	7.85
90 EPNdB - Takeoff	2.41	0.93	3.00	1.16
- Approach	<u>.80</u>	<u>0.31</u>	<u>.75</u>	<u>0.29</u>
- Total	3.21	1.24	3.75	1.45

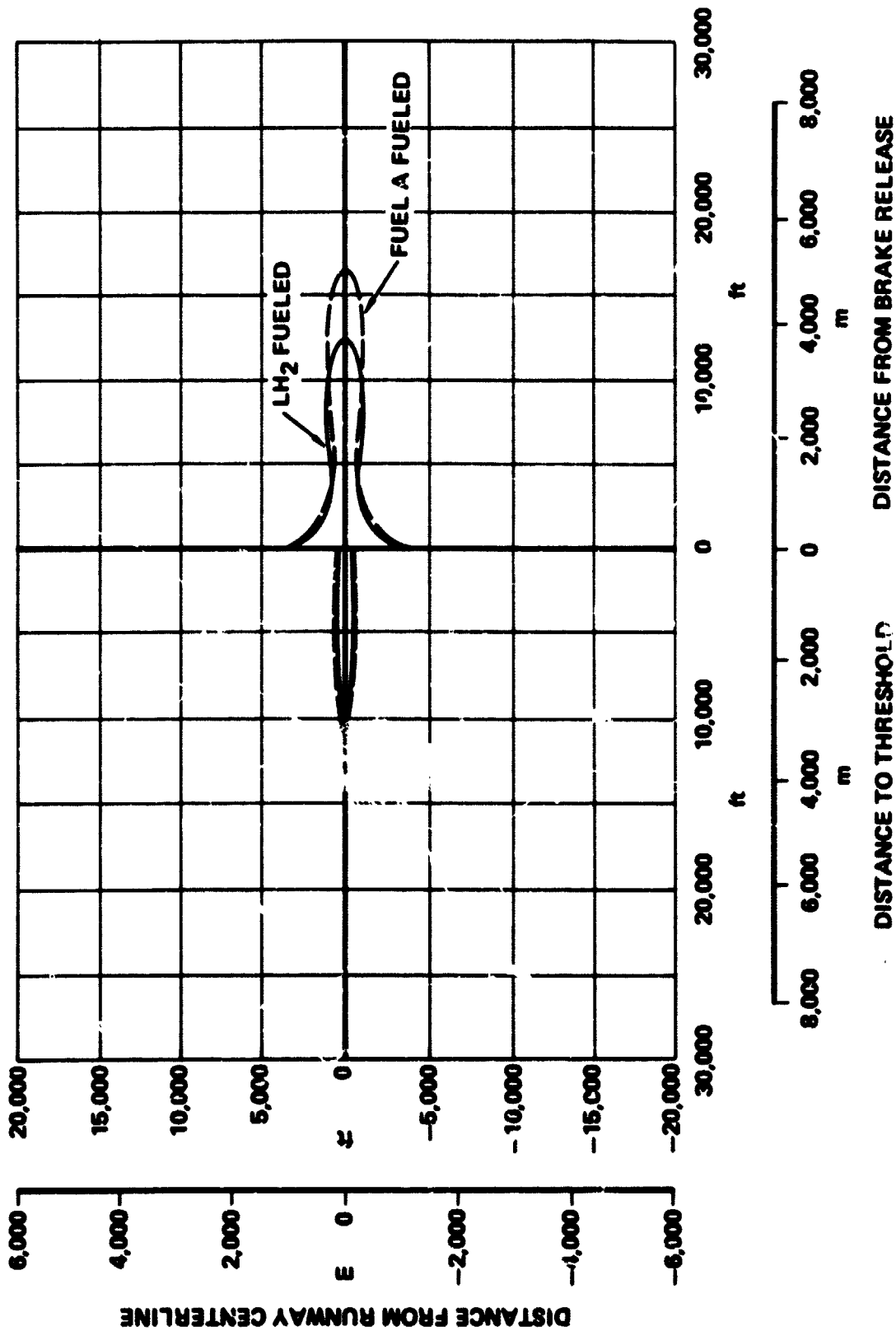


Figure 21. 90 EPNdB Contour Comparison - Medium Range Aircraft

6. LONG RANGE AIRCRAFT

6.1 Design Requirements

The long range aircraft are designed to provide the following performance and meet the specified constraints:

- 9265 km (5000 n.mi.) radius. With full payload and ATA international reserves for each segment, fly 9265 km, land, takeoff unrefueled, and fly another 9265 km segment.
- 400 passengers plus baggage and cargo for a total payload of 39,920 kg (88,000 lb)
- Maximum FAR takeoff field length of 3658 m (12,000 ft)
- Minimum initial cruise altitude of 10,360 m (34,000 ft)
- Maximum approach speed of 69.4 m/s (135 KEAS) at a landing weight equivalent to that at the end of the first 9265 km (5000 n.mi.) segment.

6.2 Configuration Selection

An external tank LH_2 configuration was not evaluated for this long range mission because the work done in Reference 1 had confirmed that the high drag and weight penalties associated with this design concept would be noncompetitive.

Designs of the internal tank LH_2 and the Jet A aircraft are similar to the medium range aircraft described in Section 5.0 with the exception that the passenger cabin of the internal LH_2 aircraft is a two deck arrangement. It is described in a following section.

Both the long range LH_2 and Jet A aircraft have relatively high growth factors because of the high fuel fraction required for the very long, unrefueled flight. During the initial parametric investigation of these aircraft, the constraints imposed on each aircraft were examined to determine which were critical in sizing the aircraft. The results indicated that initial cruise altitude was the principal design constraint for the LH_2

design, and that takeoff field length was most significant for the Jet A aircraft. Consequently, an investigation of the sensitivity of each aircraft to these parameters was made. Results are described below for the LH₂ aircraft and in Section 6.4.1 for the Jet A.

6.3 LH₂ Internal Tank Airplane (Aircraft No. 7)

6.3.1 Parametric Investigation. - Results of the study to determine the effect of initial cruise altitude on characteristics of aircraft No. 7 are shown in Table VIII. The data are plotted in Figures 22 and 23. Note that each airplane design listed in Table XIII represents the combination of wing loading (W/S) and thrust-to-weight ratio (T/W) which meets all design constraints, i.e., approach speed, 2nd segment climb gradient, and FAR takeoff field length, and achieves the specified initial cruise altitude. In Figure 22 these results are plotted to determine the minimum direct operating cost (DOC) for each aspect ratio. The locus of minima is indicated by the broken line. It shows that changing the initial cruise altitude of the long range hydrogen-fueled airplane from 10,360 m (34,000 ft) would not result in a significant decrease in DOC. Accordingly, this altitude was retained as a design constraint for the long range aircraft in this study. Also, as shown in Figure 22 the aspect ratio selected for this aircraft on the basis of minimum DOC is 10.

Following this initial investigation, corrections to the ASSET input were made as required due to the reduction of the actual gross weight over the preliminary estimates, and the final aircraft data was generated.

6.3.2 Configuration Description. - A general arrangement drawing of the LH₂ internal tank, Mach 0.85, 9265 km (5000 n.mi.) radius 400 passenger aircraft is shown in Figure 24.

Fuselage: As in the previous LH₂ fueled aircraft the passenger compartment is located in the central section of the fuselage in a double deck arrangement. Liquid hydrogen fuel tanks are located fore and aft of the passenger compartment. They occupy the full available cross section of the fuselage, except for provision for protective, crushable structure around the bottom areas.

TABLE XIII. EFFECT OF INITIAL CRUISE ALTITUDE ON LH₂ AIRCRAFT

(S.I. UNITS)
(Aircraft No. 7)

Initial Cruise Alt.-10 ³ m		Aspect Ratio			
		8	9	10	12
11.58	W/S - kg/m ²	575	571	569	565
	T/W - N/kg	0.33	0.32	0.31	0.29
	DOC - $\frac{g}{seat\ km}$.803	.784	.776	.788
	W _G - kg	282,050	278,740	278,420	284,320
	Cost - \$10 ⁶	41.63	41.56	41.8	43.3
	FAR T.O. - m	1,646	1,670	1,707	1,798
	2nd Seg. Grad.	0.079	0.0823	0.085	0.085
	V(Appr.) - m/s	69	69	69	69
10.97	W/S - kg/m ²	575	573	570	566
	T/W - N/kg	0.31	0.30	0.29	0.27
	DOC - $\frac{g}{seat\ km}$.786	.772	.767	.777
	W _G - kg	277,510	275,290	275,930	283,860
	Cost - 10 ⁶	40.53	40.54	40.96	42.7
	FAR T.O. - m	1,774	1,804	1,847	1,963
	2nd Seg. Grad.	0.067	0.0715	0.073	0.073
	V(Appr.) - m/s	69	69	69	69
10.36	W/S - kg/m ²	576	574	571	568
	T/W - N/kg	0.29	0.28	0.27	0.25
	DOC - $\frac{g}{seat\ km}$.776	.766	.761	.781
	W _G - kg	274,880	273,970	274,750	285,630
	Cost - \$10 ⁶	39.7	39.86	40.28	42.42
	FAR T.O. - m	1,914	1,959	2,012	2,149
	2nd Seg. Grad.	0.056	0.0605	0.062	0.062
	V(Appr.) m/s	69	69	69	69
9.75	W/S - kg/m ²	578	575	574	570
	T/W - N/kg	0.27	0.26	0.25	0.24
	DOC - $\frac{g}{seat\ km}$.769	.764	.767	.789
	W _G - kg	273,430	274,340	277,470	288,800
	Cost - \$10 ⁶	38.98	39.37	40.1	42.56
	FAR T.O. - m	2,088	2,143	2,210	2,282
	2nd Seg. Grad.	0.045	0.048	0.05	0.0565
	V(Appr.) - m/s	69	69	69	69
9.14	W/S - kg/m ²	579	577	575	571
	T/W - N/kg	0.256	0.25	0.24	0.233
	DOC - $\frac{g}{seat\ km}$.772	.766	.774	.795
	W _G - kg	275,240	275,520	280,640	291,670
	Cost - \$10 ⁶	38.83	39.28	40.18	42.75
	FAR T.O. - m	2,234	2,251	2,338	2,359
	2nd Seg. Grad.	0.0364	0.043	0.045	0.0525
	V(Appr.) m/s	69	69	69	69
8.53	W/S - kg/m ²	580	578	577	572
	T/W - N/kg	0.25	0.247	0.235	0.23
	DOC - $\frac{g}{seat\ km}$.775	.768	.780	.798
	W _G - kg	276,520	276,240	282,590	292,570
	Cost - \$10 ⁶	38.2	39.3	42.8	42.82
	FAR T.O. - m	2,304	2,292	2,377	2,393
	2nd Seg. Grad.	0.033	0.0413	0.042	0.051
	V(Appr.) - m/s	69	69	69	69

TABLE XIII. EFFECT OF INITIAL CRUISE ALTITUDE ON LH₂ AIRCRAFT
(U.S. CUSTOMARY UNITS)
(Aircraft No. 7)

Initial Cruise Alt.-10 ³ m		Aspect Ratio			
		8	9	10	12
38	W/S - lb/ft ²	117.7	117	116.5	115.7
	T/W	0.33	0.32	0.31	0.29
	DOC - $\frac{\$}{\text{Seat n.mi.}}$	1.4867	1.4527	1.437	1.46
	W _G - lb	621,800	614,500	613,800	626,800
	Cost - \$10 ⁶	41.63	41.56	41.8	43.3
	FAR T.O. - ft	5,400	5,480	5,600	5,900
	2nd Seg. Grad.	0.079	0.082	0.085	0.085
	V(Appr.) - KEAS	135	135	135	135
36	W/S - lb/ft ²	117.82	117.3	116.7	116
	T/W	0.31	0.30	0.29	0.27
	DOC - $\frac{\$}{\text{Seat n.mi.}}$	1.456	1.43	1.42	1.438
	W _G - lb	611,800	606,900	608,300	625,800
	Cost - \$10 ⁶	40.53	40.54	40.96	42.7
	FAR T.O. - ft	5,820	5,920	6,060	6,440
	2nd Seg. Grad.	0.067	0.072	0.073	0.073
	V(Appr.) - KEAS	135	135	135	135
34	W/S - lb/ft ²	118	117.5	117	116.4
	T/W	0.29	0.28	0.27	0.25
	DOC - $\frac{\$}{\text{Seat n.mi.}}$	1.437	1.418	1.410	1.446
	W _G - lb	606,000	604,000	605,700	629,700
	Cost - \$10 ⁶	39.7	39.86	40.28	42.42
	FAR T.O. - ft	6,280	6,426	6,600	7,050
	2nd Seg. Grad.	0.056	0.060	0.062	0.062
	V(Appr.) - KEAS	135	135	135	135
32	W/S - lb/ft ²	118.3	117.8	117.5	116.75
	T/W	0.27	0.26	0.25	0.24
	DOC - $\frac{\$}{\text{Seat n.mi.}}$	1.4243	1.415	1.42	1.462
	W _G - lb	602,800	604,000	611,700	636,700
	Cost - \$10 ⁶	38.98	39.37	40.1	42.56
	FAR T.O. - ft	6,850	7,030	7,250	7,420
	2nd Seg. Grad.	0.045	0.048	0.05	0.056
	V(Appr.) - KEAS	135	135	135	135
30	W/S - lb/ft ²	118.5	118.1	117.8	117
	T/W	0.256	0.25	0.24	0.233
	DOC - $\frac{\$}{\text{Seat n.mi.}}$	1.429	1.418	1.4325	1.473
	W _G - lb	606,800	607,400	618,700	643,000
	Cost - \$10 ⁶	38.83	39.28	40.18	42.75
	FAR T.O. - ft	7,330	7,385	7,670	7,740
	2nd Seg. Grad.	0.036	0.043	0.045	0.052
	V(Appr.) - KEAS	135	135	135	135
28	W/S - lb/ft ²	118.8	118.3	118.2	117.1
	T/W	0.25	0.247	0.235	0.23
	DOC - $\frac{\$}{\text{Seat n.mi.}}$	1.4345	1.422	1.445	1.478
	W _G - lb	609,600	609,000	623,000	645,000
	Cost - \$10 ⁶	38.2	39.3	42.8	42.82
	FAR T.O. - ft	7,560	7,520	7,800	7,850
	2nd Seg. Grad.	0.033	0.041	0.042	0.051
	V(Appr.) - KEAS	135	135	135	135

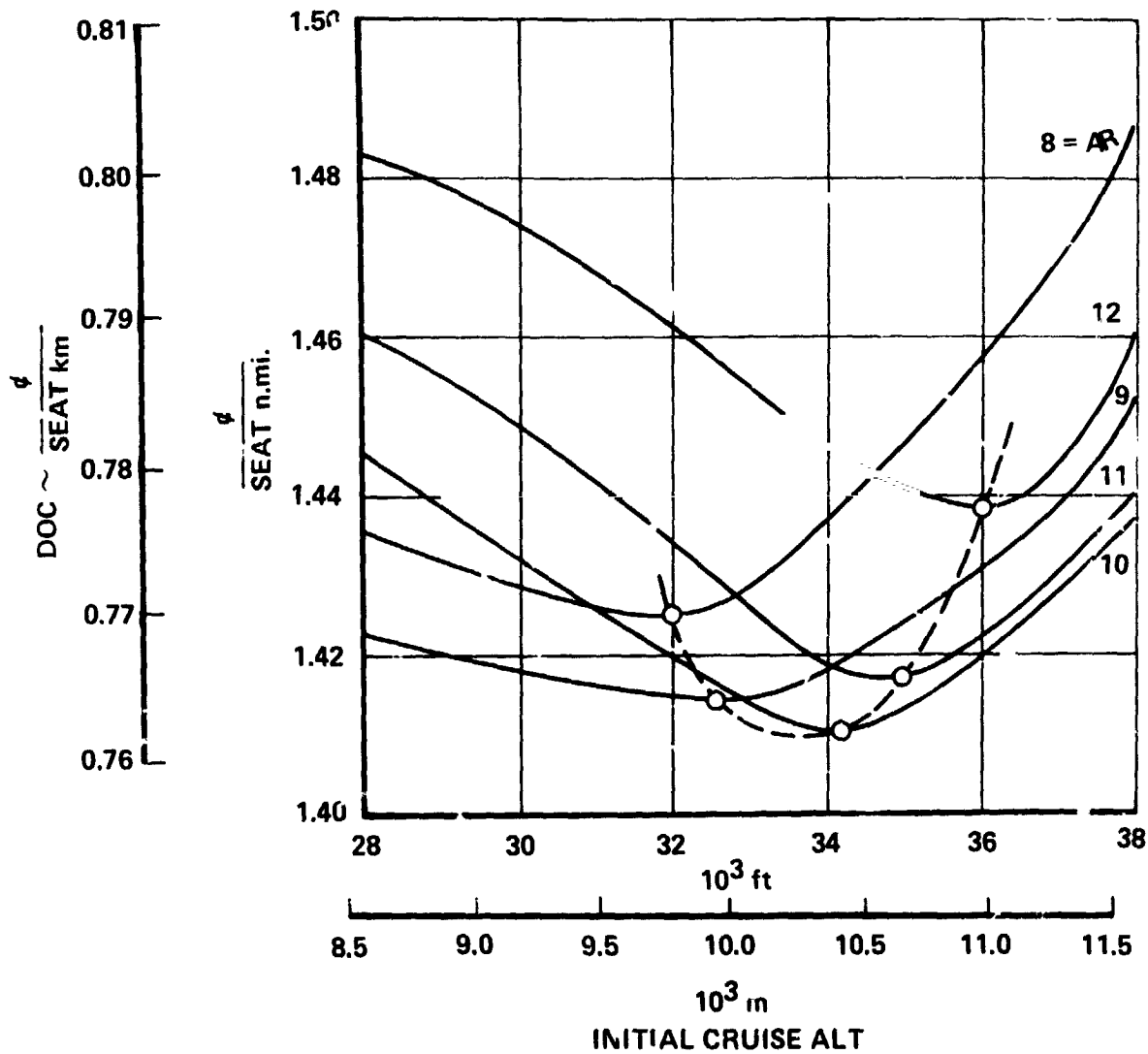


Figure 22. Effect of Aspect Ratio and Initial Cruise Altitude on Direct Operating Cost of the Long Range LH₂ Aircraft

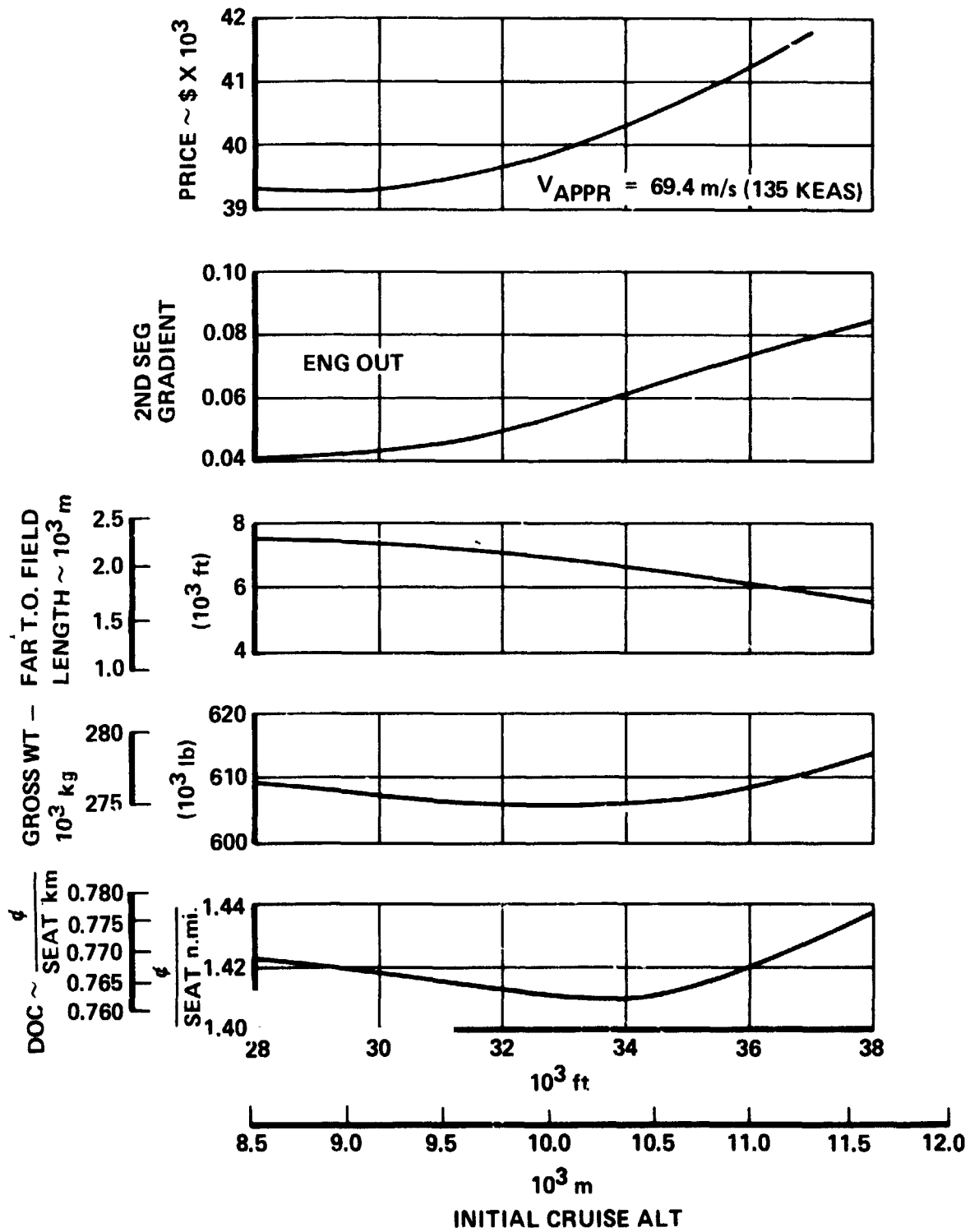


Figure 23. Effect of Initial Cruise Altitude on Performance and Cost of the Long Range LH₂ Aircraft

No provision was made for a passageway through or around the forward tank to permit movement between flight station and passengers. In the absence of such communication, the flight station is provided with special lavatory and galley facilities.

Passenger accommodations are shown in Figure 25 which shows the 10/90 percent class mix and seat spacing of 0.965 m (38 in.) and 0.86 m (34 in.) respectively, for first class and coach. Seven abreast seating is used in first class and 10 abreast in coach. The arrangement includes doors, lavatory and galley facilities in keeping with the requirements of FAR 25 and current widebody standards. Stairwells at each end of the cabin allow access to either deck in flight.

All cargo is contained in the pressurized fuselage, below the lower deck, where space is provided for cargo containers plus an additional 17 m^3 (600 ft^3) for loose cargo.

Wings: The wing has an aspect ratio of 10, and a sweep of 30° . The high lift devices include 15 percent leading edge slats and 35 percent double-slotted flaps where shown. Spoilers are used in flight for direct lift control, and for landing ground run deceleration. Conventional ailerons are fitted outboard of the flaps.

Landing Gear: The main gear consists of two six-wheel bogies mounted aft of the rear spar. They retract inward into the fuselage. The space between the retracted gear contains the hydraulic service center. The forward gear is a two-wheel strut arrangement retracting forward under the flight station.

Hydrogen Tank and Systems: The hydrogen tank structural concept selected for purposes of this study is the integral type described in Section 3.1.2. All aircraft structural loads in addition to the fuel dynamic and pressure loads are taken by the tank shell. Loads are transferred from the vehicle structure to the tank at each end by low heat-leak boron reinforced fiberglass tubes arranged in an interconnect truss structure. Seven inches of closed-cell plastic foam insulation, e.g., Rohacell 41S, covers the tank. This is then wrapped by a vapor shield (Kapton) which is to prevent cryopumping in event a crack develops in the foam insulation. A fiberglass reinforced composite layer covers the entire tank section to provide a smooth aerodynamic surface and protection from physical damage.

The tank is thus generally protected from mechanical damage by the foam insulation and its fiberglass cover. Further special protection from both foreign object damage and damage from maneuvers such as over-rotation or tail scrape is provided on the bottom of the tank. An energy absorbing, aluminum honeycomb structure is supported from

	WING	HORIZ. TAIL	VERT. TAIL
WING AREA (SQ FT)	466.4 (5020.2)	65.0 (699.6)	68.6 (738.0)
WING ASPECT RATIO	10	4.5	1.6
SPAN M (FT)	68.29 (224.1)	17.10 (56.1)	10.47 (34.4)
ROOT CHORD M (IN)	10.51 (413.6)	5.85 (230.2)	10.06 (396.1)
TIP CHORD M (IN)	3.15 (124.1)	1.75 (69.1)	3.02 (118.8)
TAPER RATIO	0.3	0.3	0.3
MAC M (IN)	7.49 (294.8)	4.17 (164.1)	7.17 (282.3)
SWEEP RAD. (DEG)	0.524 (30)	0.524 (30)	0.524 (30)
T/C ROOT (°)	10	9	9
T/C TIP (°)	10	9	9

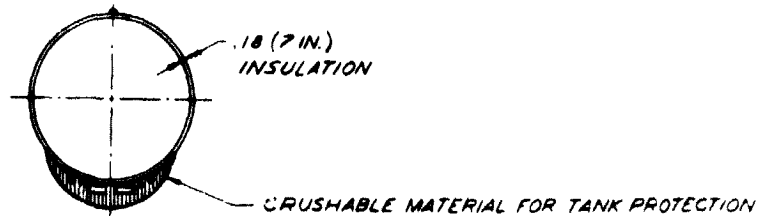
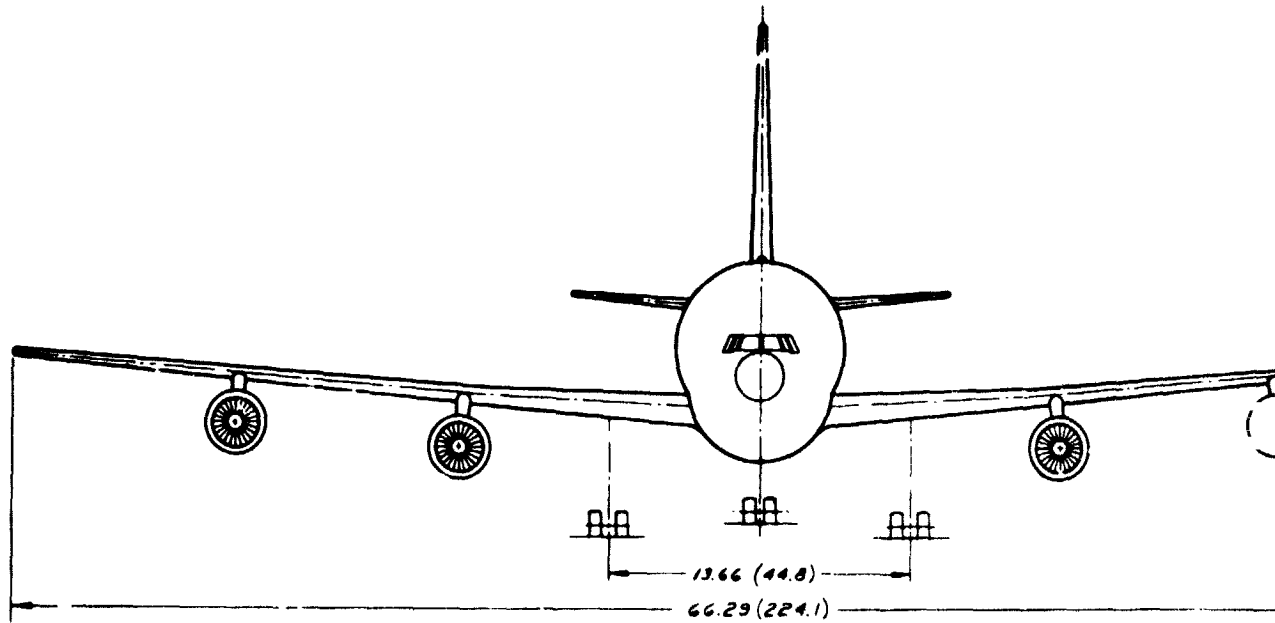
DESIGN GROSS WT - 266,429 KG (587,365 LB.)

POWER PLANT - (2) TURBOFANS
 INSTALLED THRUST (EA.) - 175,000 N (39,353 LB.)

PASSENGERS - 400

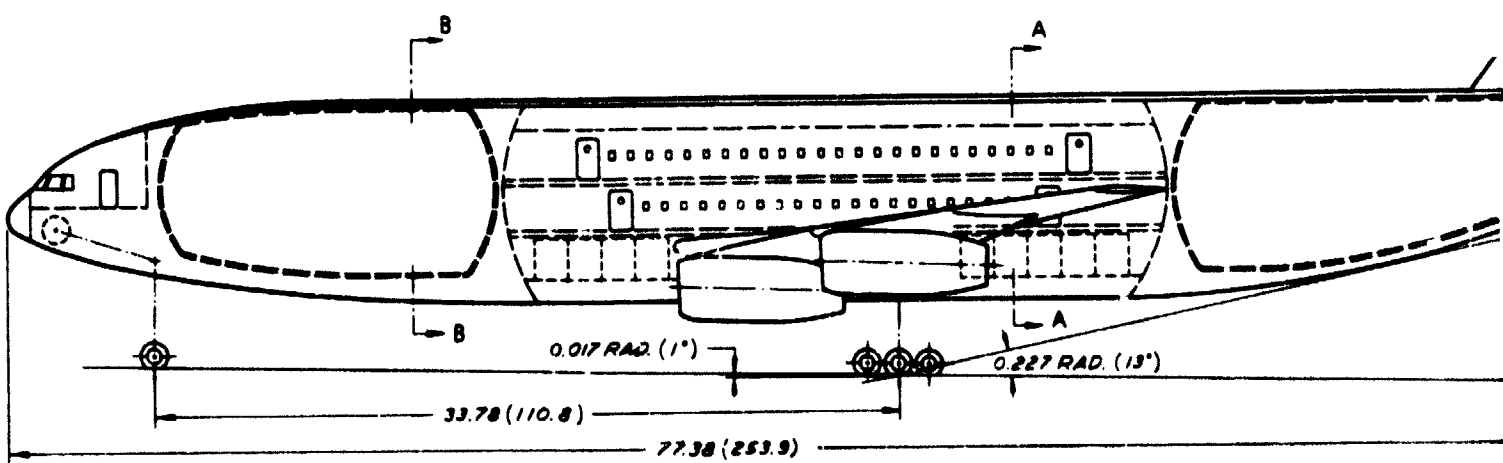
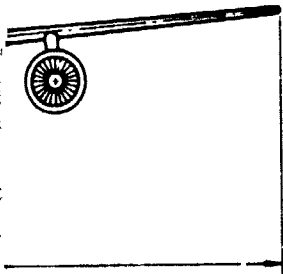
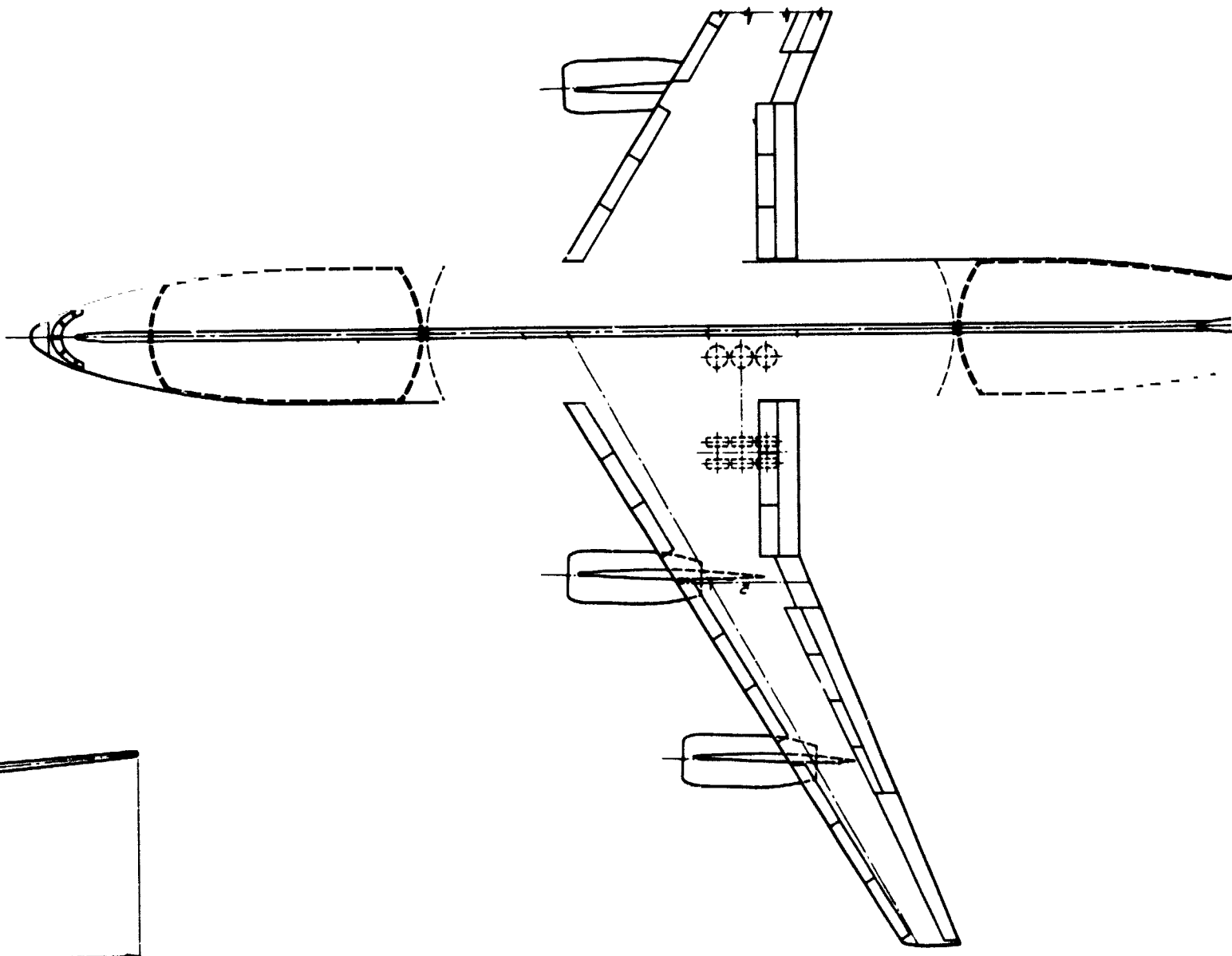
FUEL (LH₂) - 68,424 KG. (150,847 LB.)

RANGE - 9,265 KM RADIUS (5,000 N.M. RADIUS)

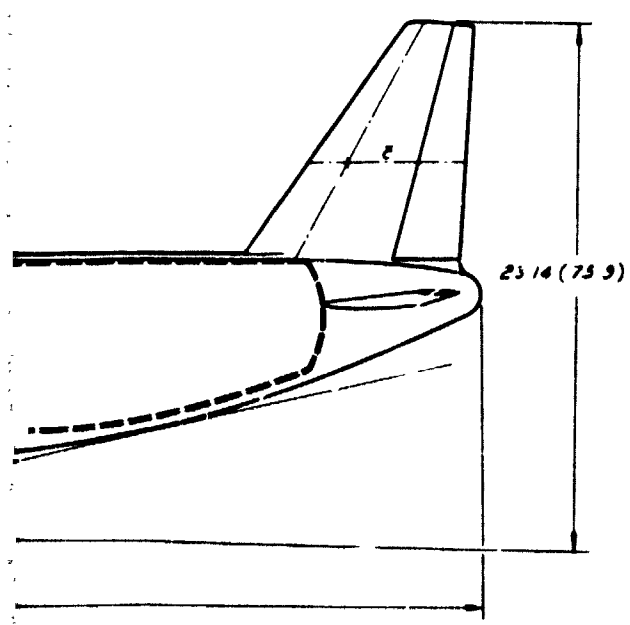
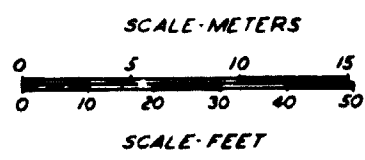
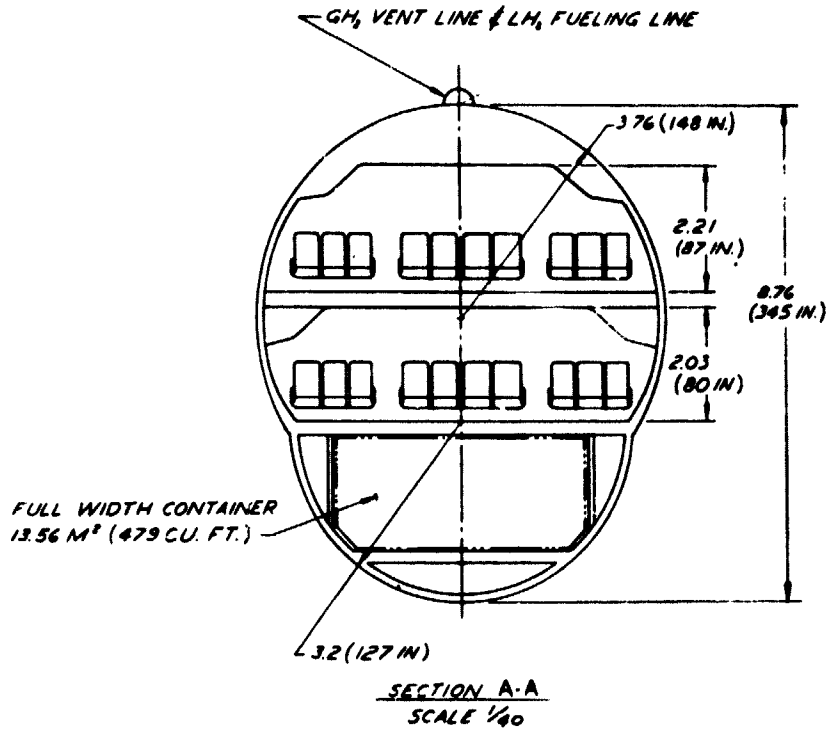
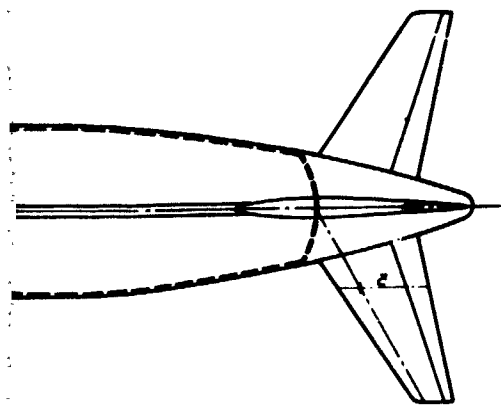


SECTION B-B

BUILDER FRAME 1



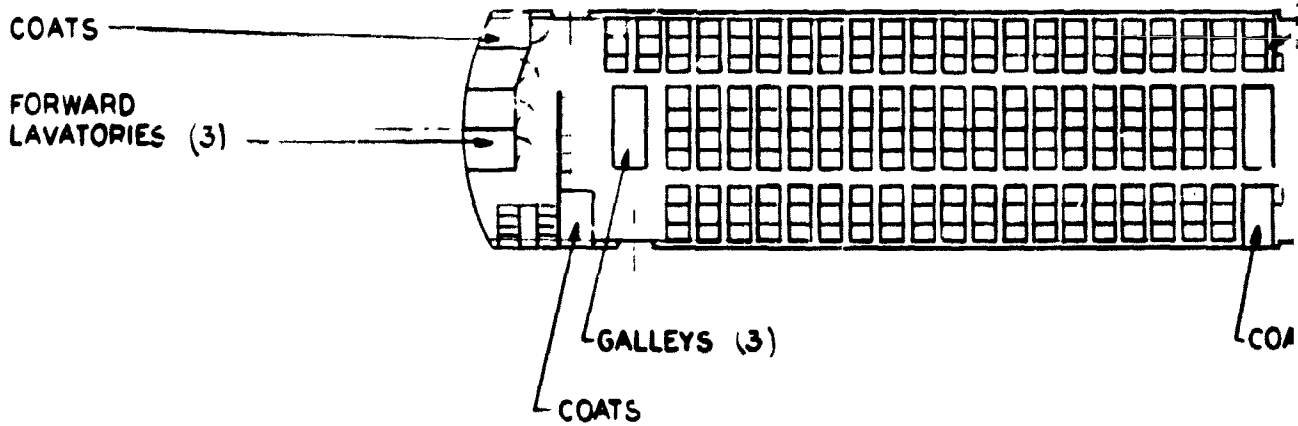
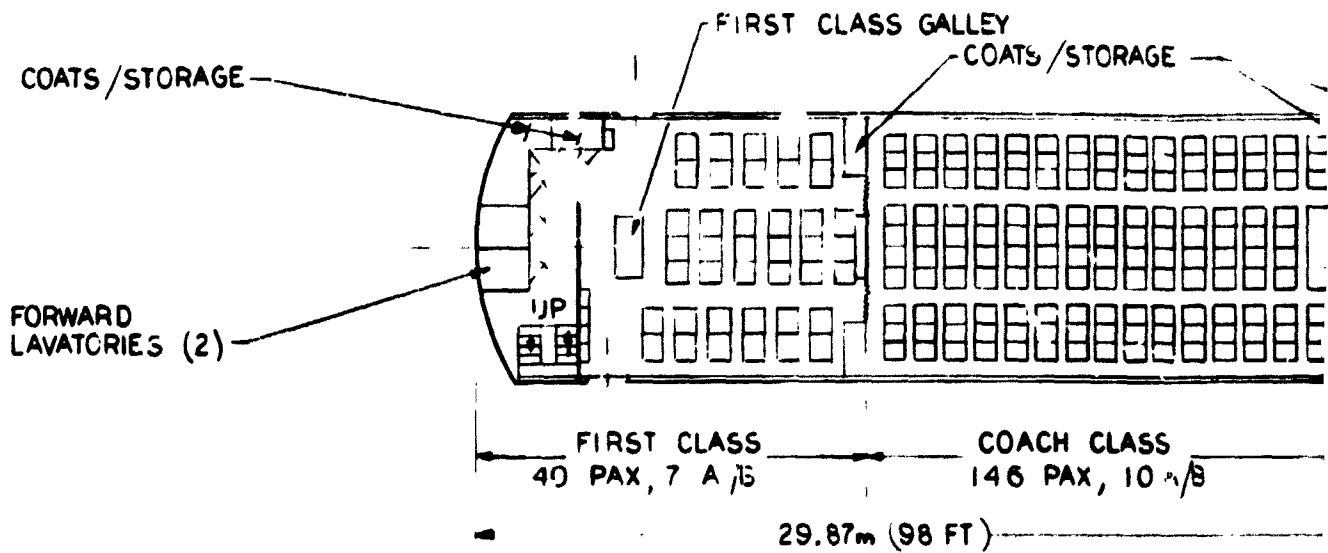
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1. DIM. IN METERS (FEET), OR NOTED
NOTE:

Figure 24. General Arrangement:
Long Range, Internal
Tank LH₂ Transport

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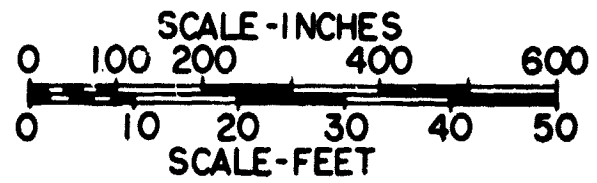
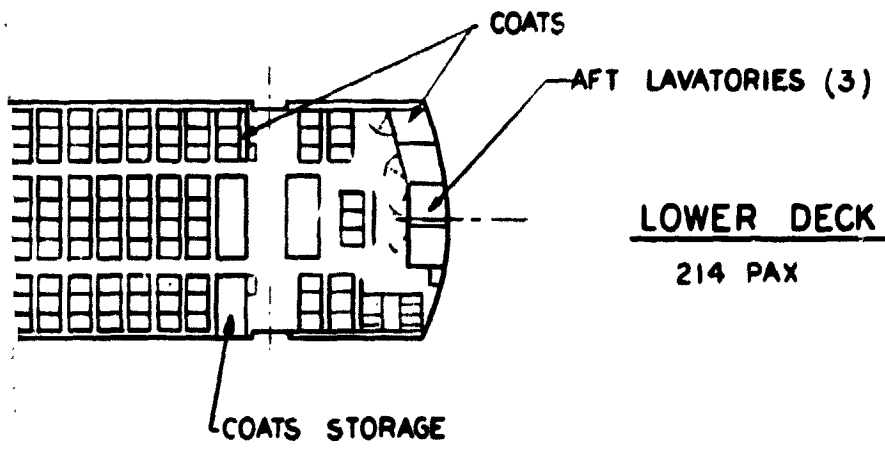
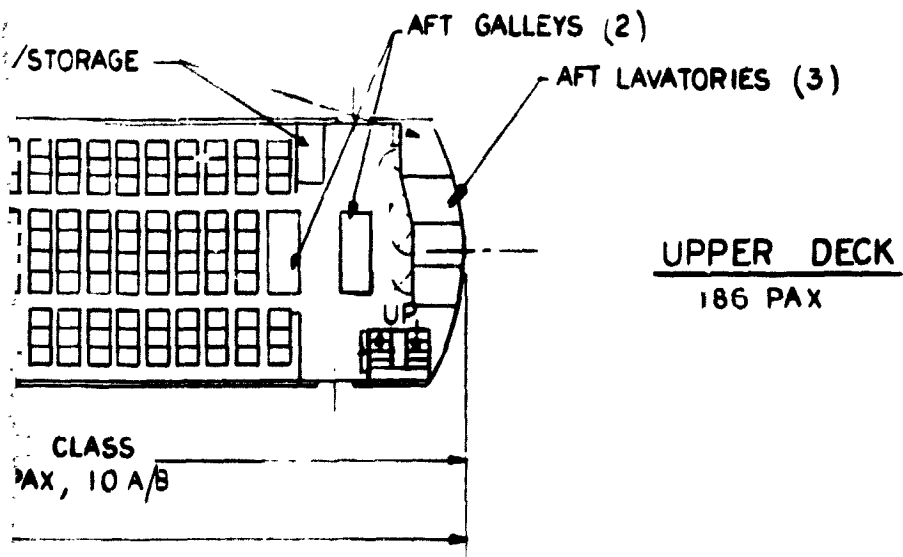
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SEATING ARRANGEMENT

TOTAL PASSENGERS = 400
 FIRST CLASS = 40/.96m (38 IN)S
 COACH CLASS = 360/.86m (34 IN)S

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ARRANGEMENT

- 3 - 400
- 0.96 m (38 IN) SPACING
- 0.86 m (34 IN) SPACING

Figure 25. Interior Arrangement:
400 Pax Transport,
LH₂ Fuel

FOLDOUT FRAME 2

the tank bottom. In this manner protection is also provided for plumbing, electrical wiring, and control systems routed adjacent to the tank.

The tank and mounting is designed for both inflight structural and fatigue loads (fail safe considerations) and to withstand the emergency crash load requirements of FAR 25 with a full fuel load.

6.3.3 Vehicle Data. - All weight, performance, and cost data are presented in Section 6.5.

6.4 Jet A Airplane (Aircraft No. 8)

6.4.1 Parametric Investigation. - The results of the preliminary parametric investigation are shown in Figure 26. The data show that the takeoff field length is critical since it exceeds the original constraint of 3048 m (10 000 ft). It also indicates that minimum DOC is achieved with an aspect ratio of 11. This aspect ratio was then used for the following tradeoff study. It should be noted that because the original preliminary assessment of the design characteristics of aircraft No. 7 indicated it might have a gross weight well in excess of 453,600 kg (1 million lb), it was planned that the airplane would have six engines. Subsequently, the final design was changed to four engines when it became apparent the thrust requirement could be met without resorting to excessively large engines.

At the conclusion of the initial parametric investigation, the question of the validity of the original takeoff field length specification of 3048 m (10,000 ft) was raised by the NASA technical monitor as perhaps being unduly restrictive. For an aircraft of this size and purpose, it is logical to assume it would characteristically operate from the major airports of the world where long, modern runways would be available. Accordingly, a special study was made to determine the effect various field lengths ranging from 2740 m (9000 ft) to almost 4880 m (16,000 ft) would have on the long range Jet A aircraft design and performance. Figure 27 presents the results of this investigation. A series of aircraft designs was generated, each of which meets the guideline constraints, except for the specified field length. For each, the DOC, gross weight, initial cruise altitude, second

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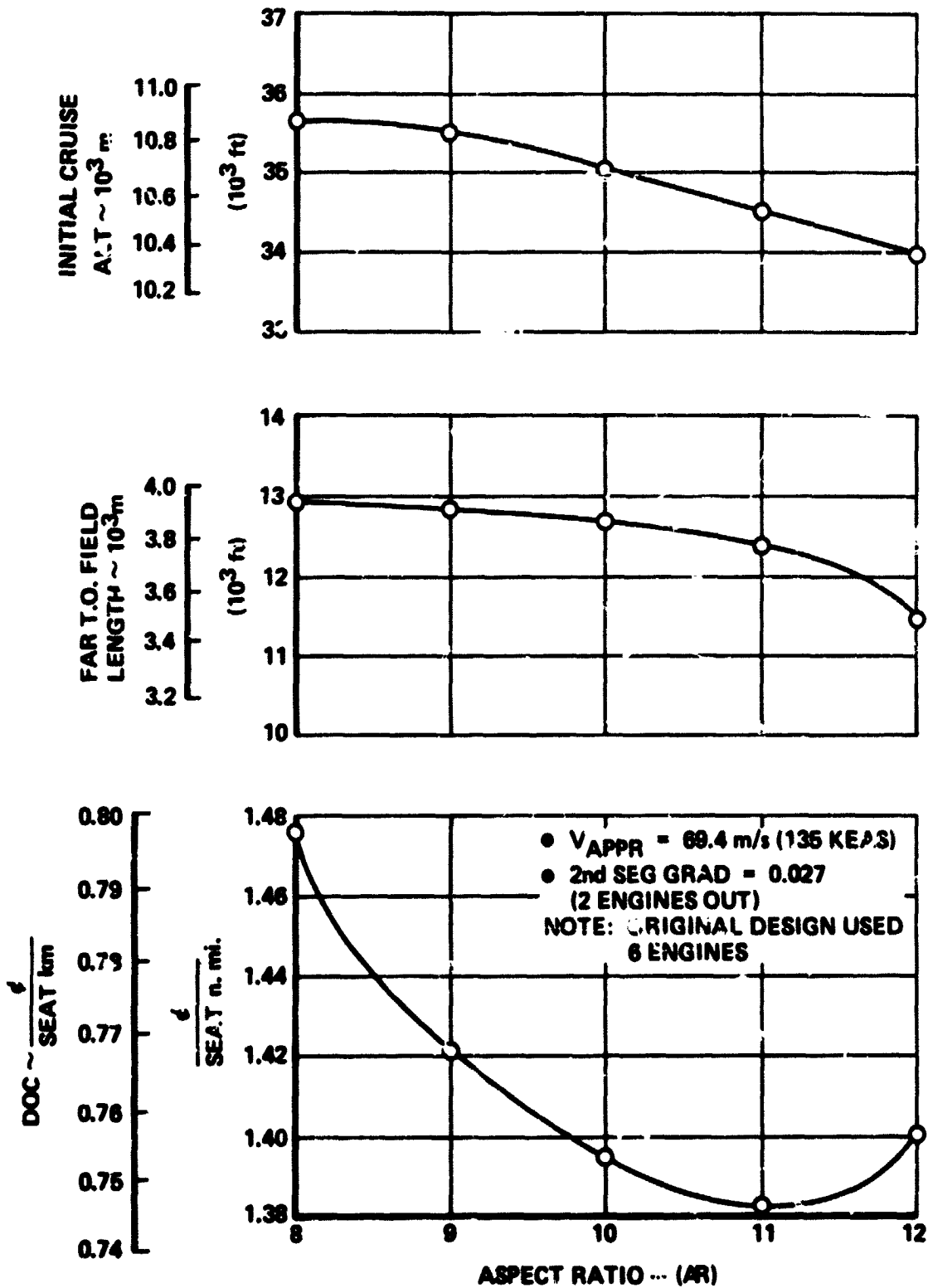


Figure 26. Aspect Ratio Selection for Long Range Jet A Aircraft

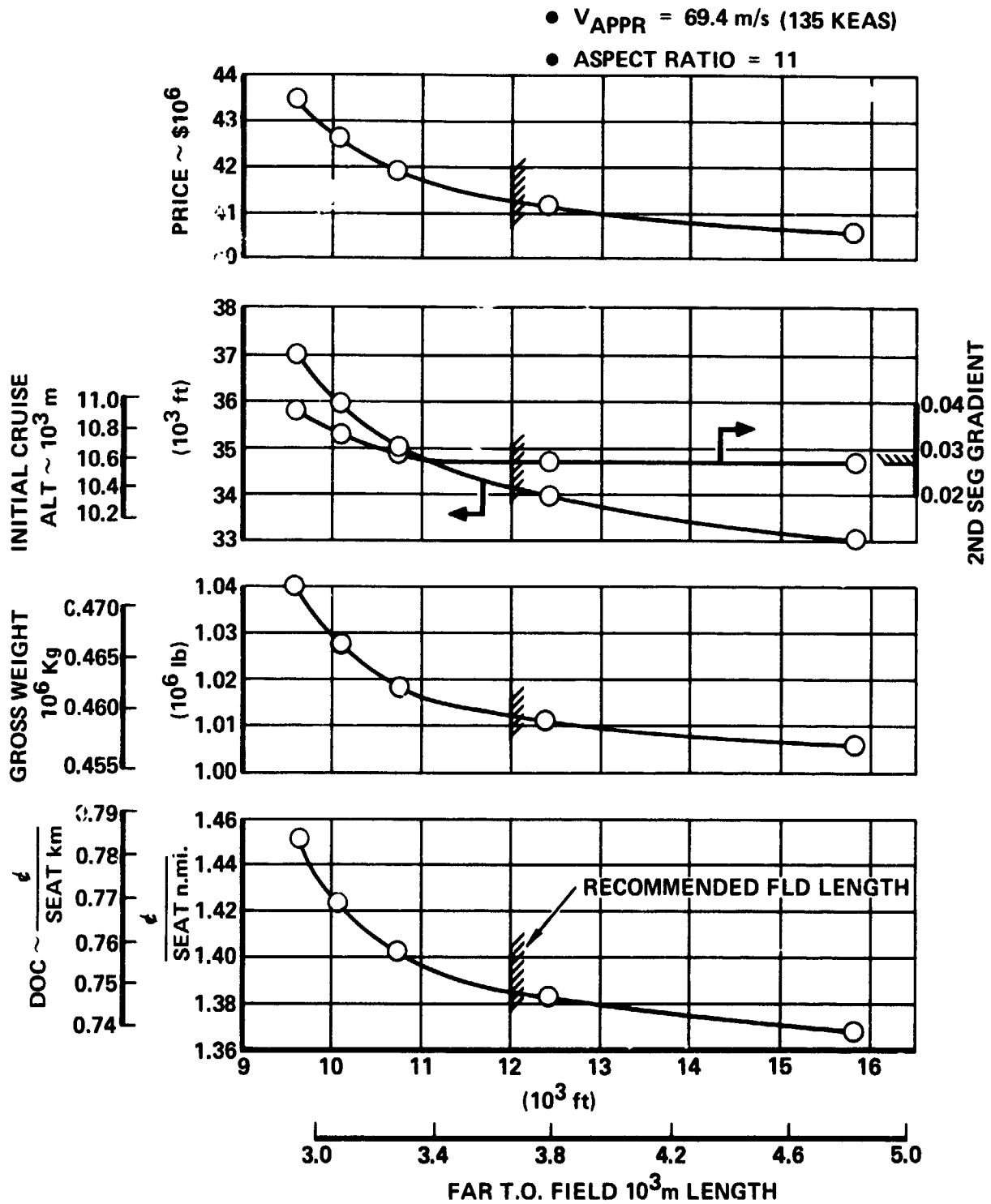


Figure 27. Recommended Field Length for the Long Range, Jet A Aircraft

C.2

segment climb gradients, and aircraft production price are all plotted to show the effect of FAR takeoff field length.

In addition, data on existing runway lengths and reference conditions of some of the major airports in the world which have high traffic densities was compiled and tabulated. These results are shown in Table XIV. Evaluation of these data showed that all the airports marked with an asterisk could be used if the subject airplane was capable of taking off from Miami which has a runway length of 3048 m (10,000 ft), elevation of 3 m (10 ft), and a reference temperature of 28.9°C. If these runway conditions are translated to the conditions of this study, i.e., 304.8 m (1000 ft) elevation and 32.2°C (90°F), the equivalent maximum allowable takeoff distance becomes approximately 3658 m (12,000 ft). This recommended field length is indicated on Figure 27.

Examination of the figure shows that considerable improvement in all of the vehicle parameters can result from increasing takeoff field length to 3658 m (12,000 ft), from the 3048 m (10,000 ft) originally proposed, and that not a great deal of further improvement would be realized if the field length requirement increased still further at the cost of eliminating the capability of operating from many of the world's major airports. Accordingly, a change to the design constraint of 3658 m (12,000 ft) FAR takeoff distance was adapted for the Jet A long range aircraft of this study.

The characteristics of the final vehicle design were generated using this constraint after modifying the ASSET inputs as required by the reduction in the vehicle size from the original estimate. For example, four engines were specified instead of the original six.

6.4.2 Configuration Description. - The general arrangement of this aircraft is shown in Figure 28. The arrangement is conventional with the exception of the main gear which consists of four six-wheel bogies mounted aft of the rear spar. The outboard bogies retract inward into the fuselage, while the inboard bogies retract aft into the fuselage. The nose gear consists of dual wheels which retract forward. All fuel is carried in the wing box and wing center section.

TABLE XIV. MAJOR AIRPORT RUNWAY LENGTHS AND REFERENCE CONDITIONS

	Runway Length		Elevation		Ref. Temp. †	
	m	(ft)	m	(ft)	°C	(°F)
ATLANTA	3,048.	(10,000)	313.	(1,026)	30.0	(86.0)
* CHICAGO	3,556.	(11,667)	203.	(666)	23.7	(74.7)
* DALLAS - FT. WORTH	3,477.	(11,408)	183.	(600)	30.8	(87.4)
* HONOLULU	3,771.	(12,373)	4.	(13)	26.5	(79.7)
* LOS ANGELES	3,685.	(12,090)	38.	(126)	23.7	(74.7)
* MIAMI	3,200.	(10,500)	3.	(10)	28.9	(84.0)
MINNEAPOLIS	3,048.	(10,000)	256.	(840)	29.0	(84.2)
NEW ORLEANS	2,812.	(9,226)	.9	(3)	29.6	(85.3)
* NEW YORK (JFK)	4,441.	(14,571)	4.	(13)	24.8	(76.6)
* SAN FRANCISCO	3,225.	(10,581)	3.	(10)	17.8	(64.0)
* WASHINGTON (DULLES)	3,505.	(11,500)	95.	(312)	26.9	(80.4)
* AMSTERDAM	3,452.	(11,326)	4.	(13)	17.8	(64.0)
* BRUSSELS	3,638.	(11,936)	55.	(180)	19.1	(66.4)
* COPENHAGEN	3,599.	(11,808)	5.	(16)		
* FRANKFURT	3,899.	(12,792)	112.	(367)	20.9	(69.6)
* GENEVA	3,898.	(12,790)	430.	(1,411)	21.5	(70.7)
* LONDON	3,657.	(12,000)	24.	(79)	19.0	(66.2)
* MOSCOW	3,499.	(11,480)	204.	(670)	21.0	(69.8)
* MUNICH	3,998.	(13,120)	530.	(1,740)	19.2	(66.6)
* PARIS (ORLY)	3,649.	(11,972)	89.	(292)	21.0	(69.8)
* ROME	3,899.	(12,792)	2.	(7)	25.4	(77.7)

† REF. TEMP. = Mean 24-hour temperature for hottest month of year plus one-third of difference between maximum daily mean and 24-hour mean temperature.

*Airports from which subject aircraft could operate if designed to 365^R m (12,000 ft) FAR runway length, specified conditions.

The interior arrangement is shown in Figure 29 with a 10/90 percent first-to-coach class mix with 6 abreast, 0.96 m (38 in.) seat spacing in first class and 8 abreast, 0.86 m (34 in.) spacing in coach. A below-deck galley is used. Doors and lavatories are provided in accordance with requirements of FAR 25 and current industry standards. Storage for carry-on luggage and passenger belongings suitable for a 400 passenger aircraft is also provided.

6.4.3 Vehicle Data. - All performance, weight, and cost data is shown in Section 6.5.

6.5 Comparison of Long Range Aircraft

Table XV presents a summary of significant design and performance data for the LH₂ and Jet A long range aircraft. The table also shows a ratio which compares the value of each significant parameter listed for the Jet A design with that of the LH₂ fueled airplane. Copies of pertinent sheets of the ASSET computer printouts for each of these final design aircraft are presented in Appendix A-7 and A-8 for more detailed information.

Generally, comparing the values listed in the columns of Table XV, it is seen that the LH₂ aircraft offers significant advantage in almost every category of comparison for this long range mission. The LH₂ aircraft is lighter, requires a smaller wing but a larger fuselage, uses smaller engines, can takeoff in shorter distances, and uses 25 percent less energy per seat mile in performing its mission.

The penalties occasioned by the density and cryogenic nature of liquid hydrogen, reflected in the values shown for Lift/Drag are more than overcome by the advantage of the heating value of the fuel, indicated by the values shown for specific fuel consumption (SFC).

The heating values of the fuels used in this study are 42,760 kJ/kg (18,400 Btu/lb) for Jet A, and 119,900 kJ/kg (51,590 Btu/lb) for hydrogen. This is a ratio of 2.8 in favor of hydrogen which accounts for the principle portion of the difference in specific fuel consumptions (SFC) listed in the

CHARACTERISTICS	WING	HORIZ TAIL	VERT. TAIL
AREA M ² (SQ FT)	661.91 (7125)	10.32 (757)	70.84 (7266)
ASPECT RATIO	11	4.5	16
SPAN M (FT)	85.34 (280.0)	17.60 (584)	10.64 (349)
ROOT CHORD M (IN)	11.93 (469.8)	6.08 (239.4)	10.24 (403.1)
TIP CHORD M (IN)	3.58 (141.0)	1.82 (71.8)	3.07 (120.9)
TAPER RATIO	0.3	0.3	0.3
MAC M (IN)	8.51 (334.9)	4.34 (170.7)	7.34 (287.3)
SWEEP = Λ (DEG)	0.524 (30)	0.524 (30)	0.524 (30)
T/C ROOT (%)	10	9	9
T/C TIP (%)	10	9	9

DESIGN GROSS WT - 450,206 KG (997,517 LB)

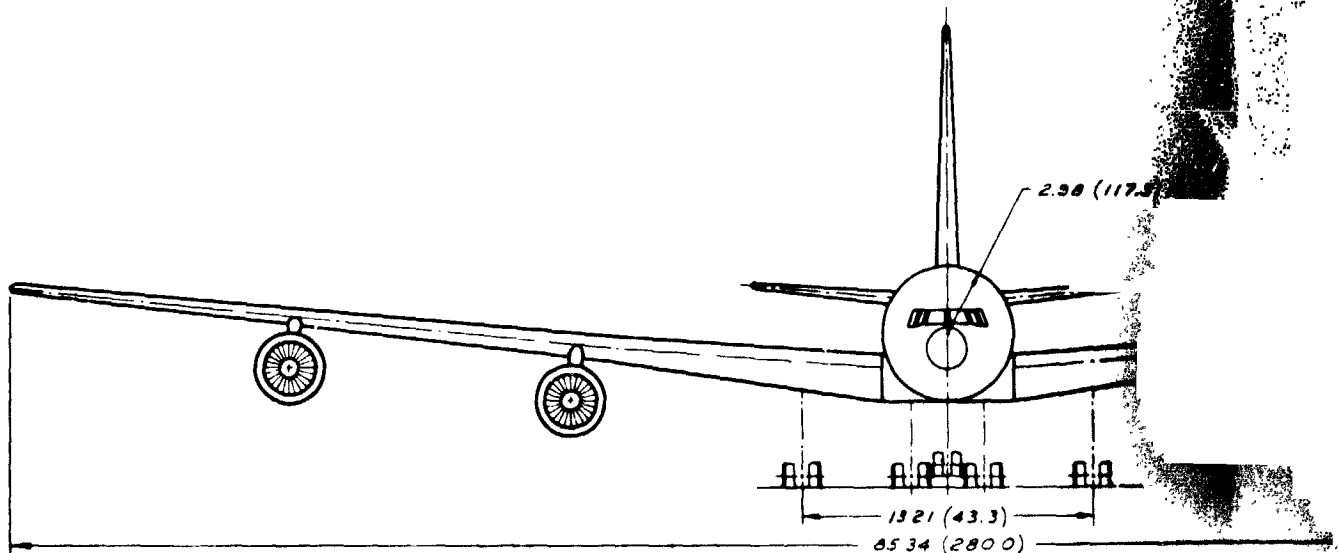
POWER PLANT - (4) TURBOFANS

INSTALLED THRUST (EA) - 220,723 N (49,625 LB)

PASSENGERS - 400

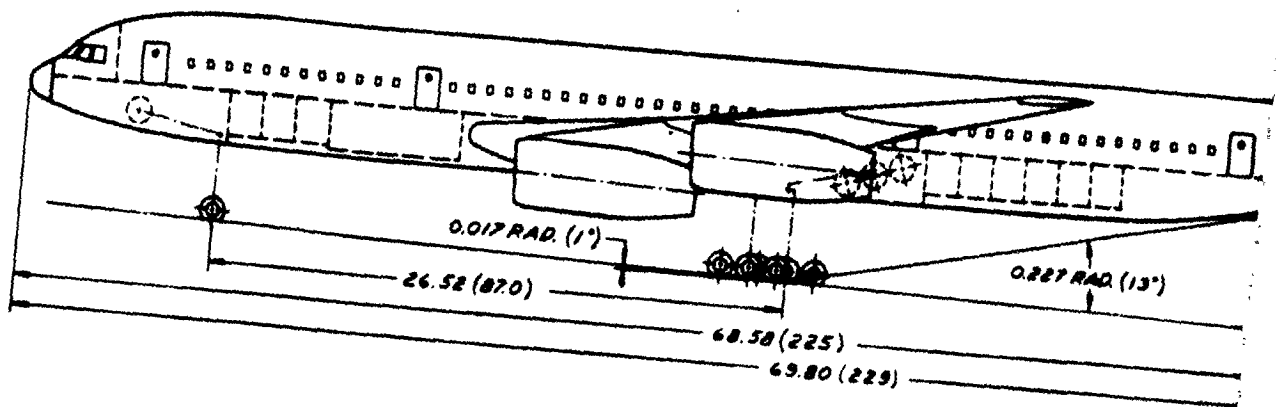
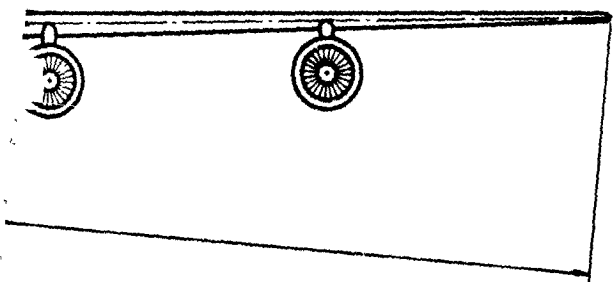
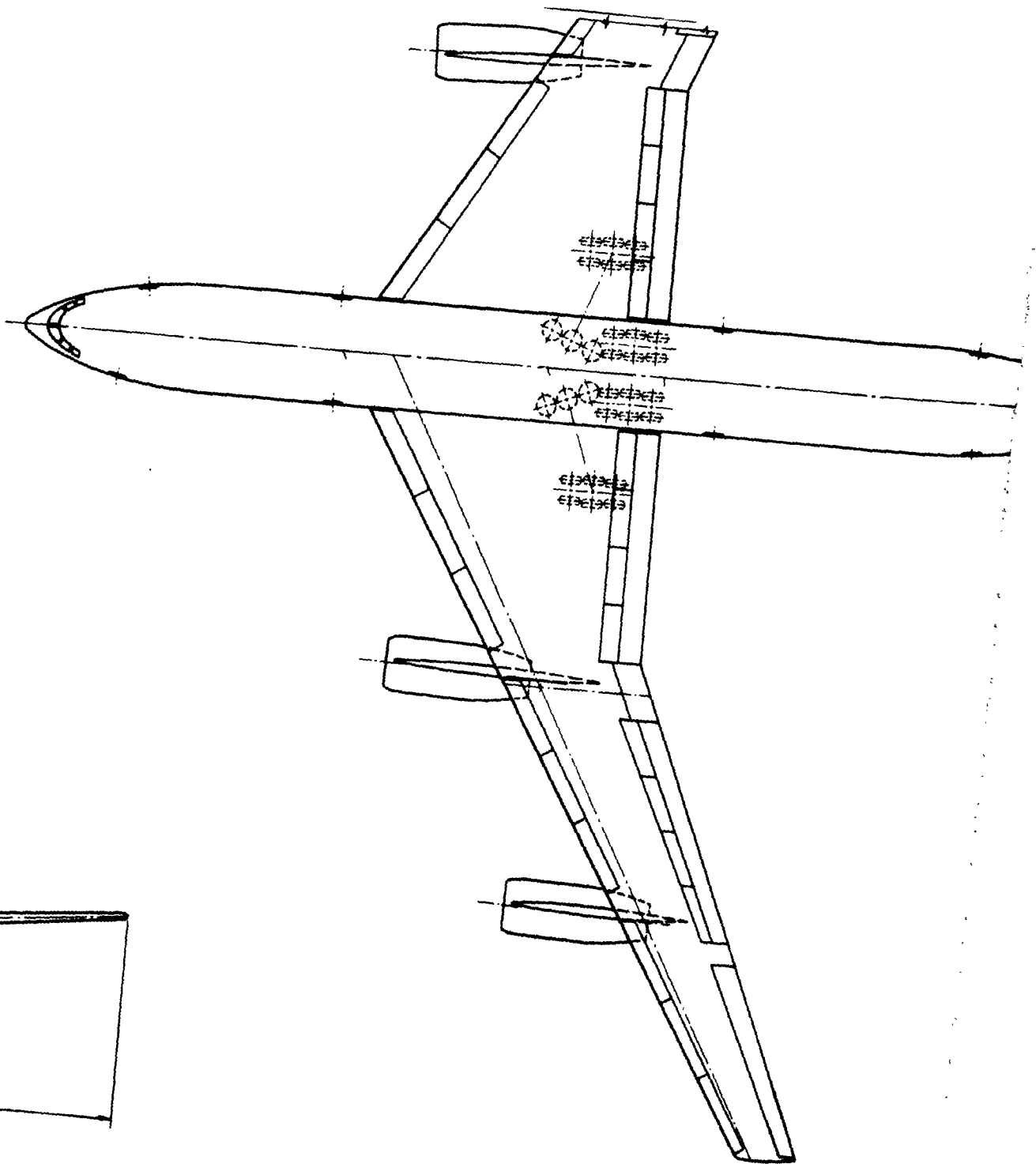
FUEL (JET A) - 237,685 KG (523,996 LB)

RANGE - 9,265 KM RADIUS (5,000 N.M. RADIUS)

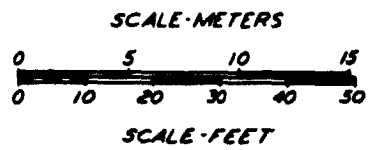
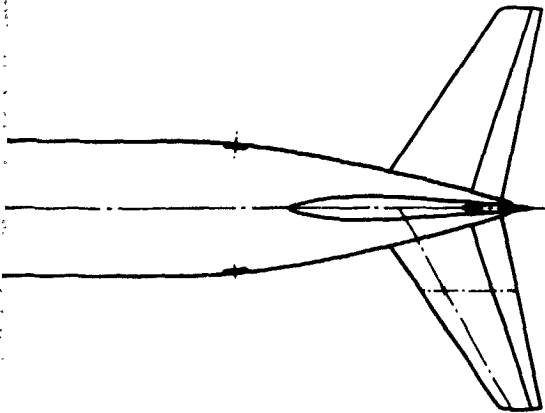


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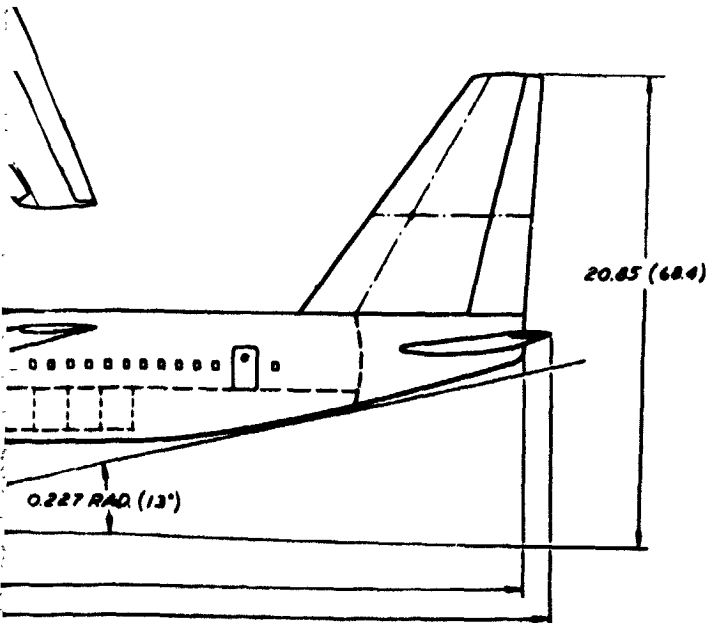
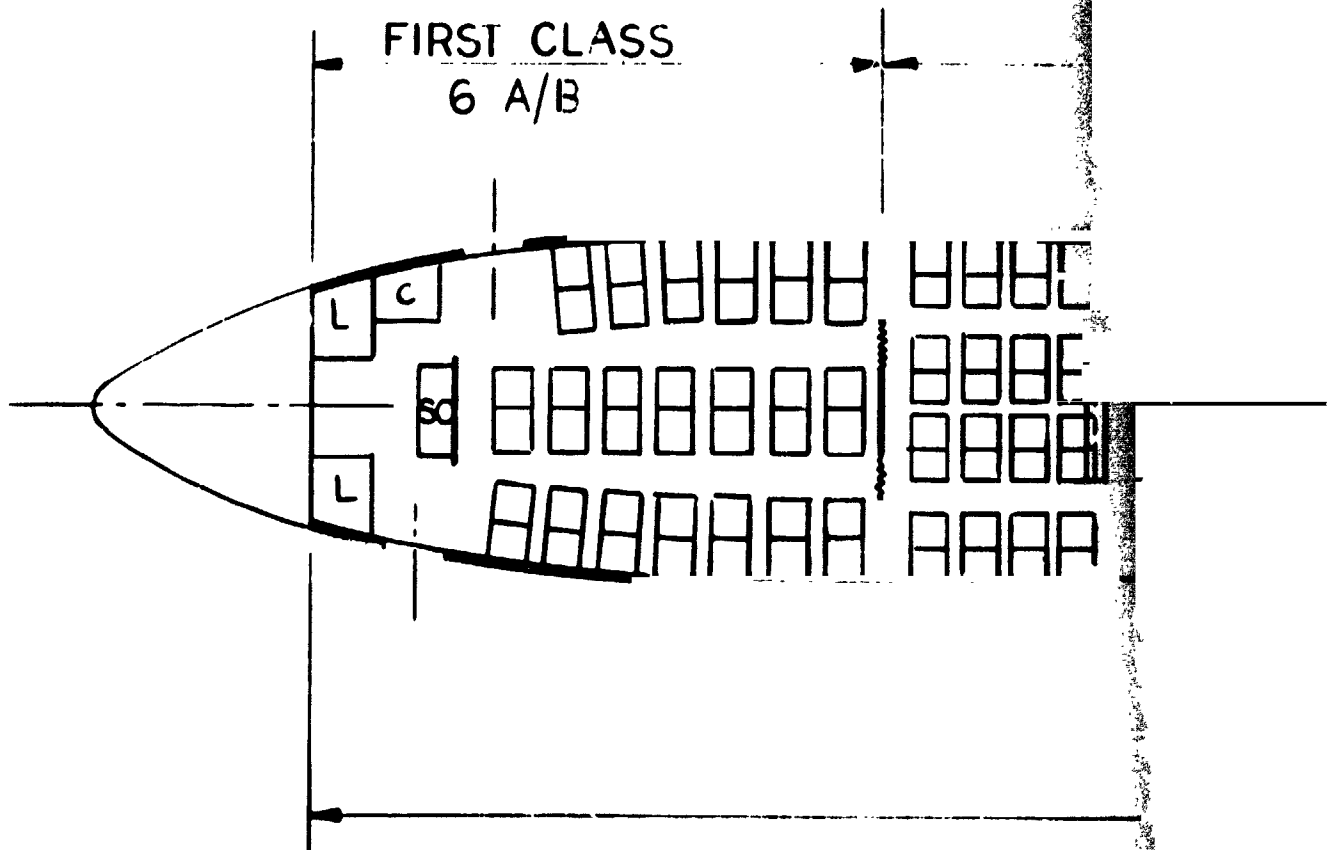


Figure 28. General Arrangement:
Long Range, Jet A
Fuel Transport

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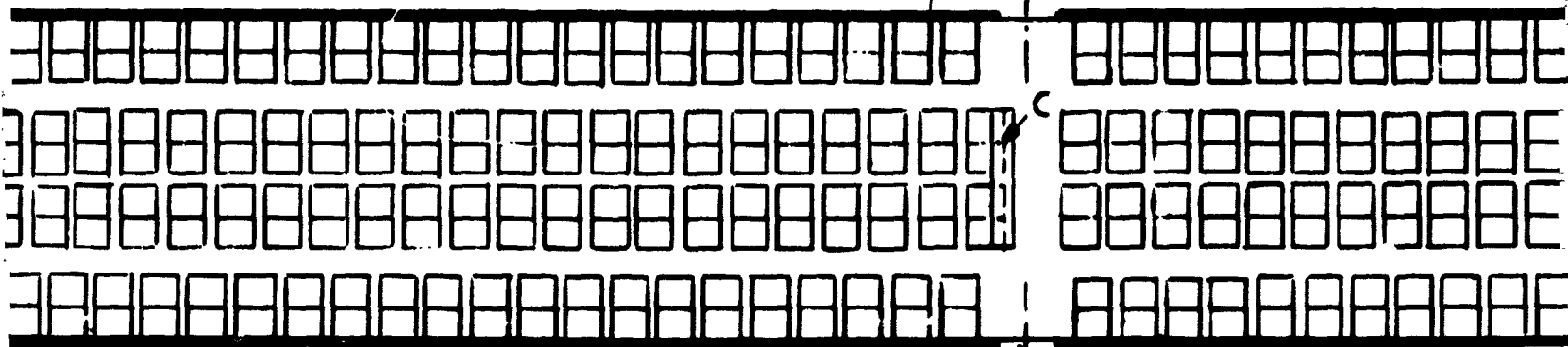


L - LAVATORY
 C - COATS
 E - ELEVATOR TO BELOW FLOOR KITCHEN
 S - SERVICE CART
 SC - SERVICE CENTER

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COACH CLASS

8 A/B



57.15 m (187.5 FT)

FIRST CLASS : 40 PAX , .96 m (38 IN) SPACING
COACH CLASS : 360 PAX , .86 m (34 IN) SPACING

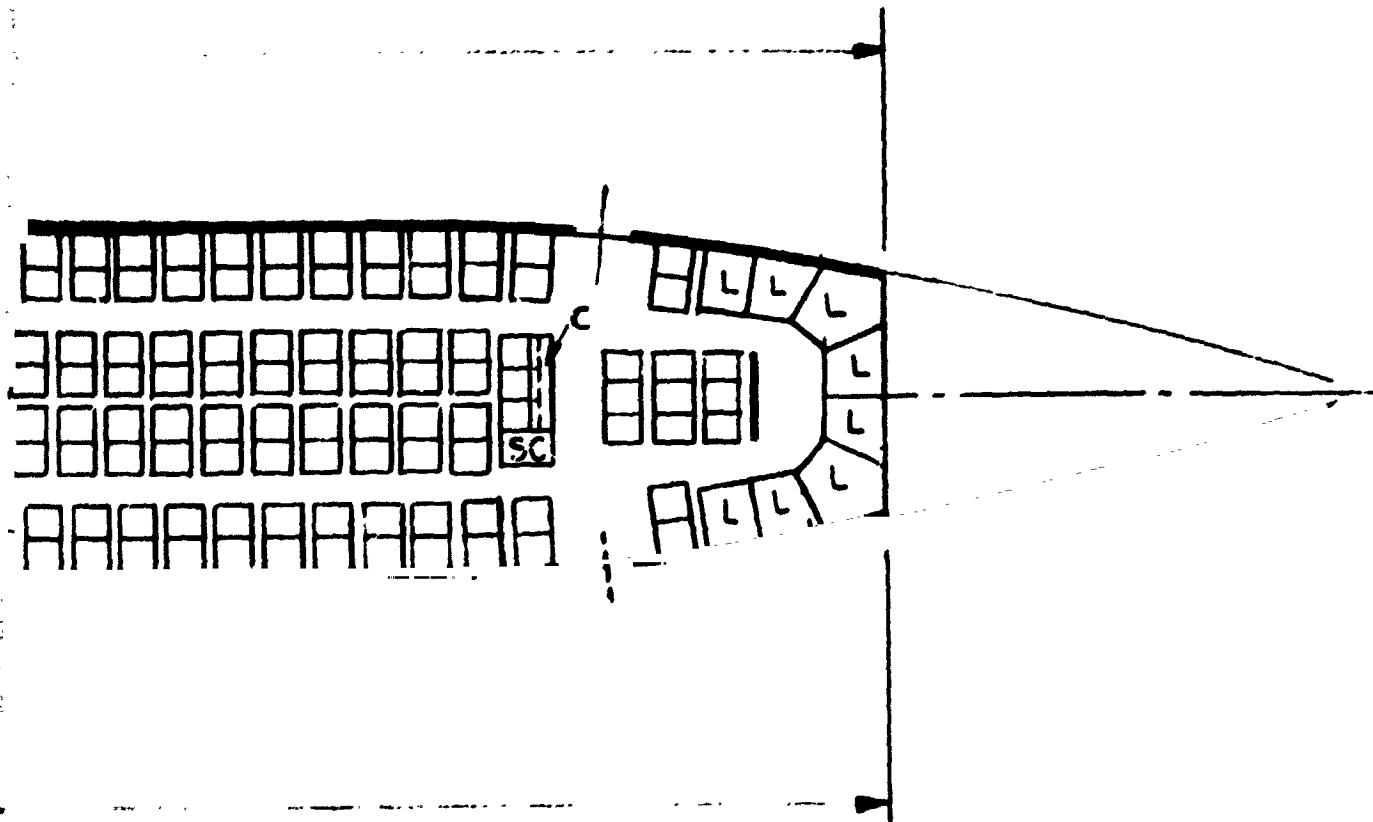


Figure 29. Interior Arrangement:
400 Pax Transport,
Jet A Fuel

TABLE XV. COMPARISON OF FINAL DESIGN LONG RANGE AIRCRAFT
(S.I. UNITS)

(9265 km radius - 400 PAX. - Mach 0.85)
(Payload - 39,920 kg)

		Aircraft No. 7 (Int. LH ₂)	Aircraft No. 8 (Jet A)	Ratio (Jet A) (Int. LH ₂)
Gross Wt	kg	266,430	450,200	1.69
Total Fuel Wt	kg	68,430	237,690	3.47
Block Fuel Wt	kg	59,610	208,720	3.50
Operating Empty Wt	kg	158,090	172,600	1.09
Empty Wt	kg	147,700	159,280	1.08
Aspect Ratio		10	11	
Wing Area	m ²	466	662	1.42
Sweep	deg	30	30	
Span	m	68	85	1.25
Fuselage Length	m	77	69	0.89
L/D - Cruise		16.8	20.3	1.21
SFC - Cruise	$\frac{\text{kg}}{\text{hr}} / \text{daN}$	0.203	0.593	2.93
Initial Cruise Altitude	m	10,360	10,060	
Wing Loading	kg/m ²	571	680	
Thrust/Weight	N/kg	2.63	1.96	0.75
No. Engines		4	4	
Thrust Per Engine	N	175,000	220,700	1.26
FAR T.O. Distance	m	2,107	3,649	1.73
FAR Ldg. Distance	m	1,795	1,788	
2nd Seg Climb Grad. (Eng Out)		0.066	0.034	0.52
Approach Speed	m/s	69	69	
Weight Fractions	percent			
Fuel		25.7	52.8	
Payload		15.0	8.9	
Structure		32.6	24.6	
Propulsion (Includes Fuel System)		14.3	5.3	
Equipment and Operating Items		12.4	8.4	
Price	$\$10^6$	38.89	39.99	1.03
DOC	$\frac{\phi}{\text{seat km}}$	0.738 ¹	0.723 ²	0.98
Energy Utilization	$\frac{\text{kJ}}{\text{seat km}}$	964	1207	1.25
Max. Nonstop Range ³	km	19,590	19,980	1.02

¹DOC based on LH₂ cost = \$2.85/GJ

²DOC based on Jet A cost = \$1.90/GJ

³Including reserve fuel requirement.

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TABLE XV. COMPARISON OF FINAL DESIGN LONG RANGE AIRCRAFT
(U.S. CUSTOMARY UNITS)

(5000 n.mi. radius - 400 PAX. - Mach 0.85)
(Payload = 88,000 lb)

		Aircraft No. 7 (Int. LH ₂)	Aircraft No. 8 (Jet A)	Ratio (Jet A) (Int LH ₂)
Gross Wt	lb	587,370	992,520	1.69
Total Fuel Wt	lb	150,850	524,000	3.47
Block Fuel Wt	lb	131,420	460,150	3.50
Operating Empty Wt	lb	348,520	380,520	1.09
Empty Wt	lb	325,630	351,150	1.08
Aspect Ratio		10	11	
Wing Area	ft ²	5020	7125	1.42
Sweep	deg	30	30	
Span	ft	224.1	279.9	1.25
Fuselage Length	ft	253.9	225.0	.89
L/D - Cruise		16.8	20.3	1.21
SFC - Cruise	(lb/hr)/lb	0.199	0.583	2.93
Initial Cruise Altitude	ft	34,000	33,000	
Wing Loading	lb/ft ²	117.0	139.3	
Thrust/Weight		0.268	0.200	0.75
No. Engines		4	4	
Thrust Per Engine	lb	39,350	49,630	1.26
FAR T.O Distance	ft	6914	11,970	1.73
FAR Ldg. Distance	ft	5890	5867	
2nd Seg Climb Grad. (Eng Out)		0.066	0.034	0.52
Approach Speed	KEAS	135	135	
Weight Fractions	percent			
Fuel		25.7	52.8	
Payload		15.9	8.9	
Structure		32.6	24.6	
Propulsion (Includes Fuel System)		14.3	5.3	
Equipment and Operating Items		12.4	8.4	
Price	\$10 ⁶	38.89	39.99	1.03
DOC	$\frac{\$}{\text{seat n.mi.}}$	1.366 ¹	1.339 ²	0.98
ENERGY UTILIZATION	$\frac{\text{Btu}}{\text{seat n.mi.}}$	1695	2122	1.25
Max Nonstop Range ³	n.mi.	10,571	10,780	1.02

¹ DOC based on LH₂ cost = \$3/10⁶ Btu = 15.48¢/lb

² DOC based on Jet A cost = \$2/10⁶ Btu = 24.8¢/gal

³ Including reserve fuel requirement

tables. The ratio of cruise SFC's, Jet A-to-LH₂, listed in Table XV is 2.93. The extra advantage given the hydrogen system over the factor of 2.8 expected from comparison of the heating values, is mostly due to the requirement to cool the high pressure turbine stages of the Jet A engine with air bled from its compressor---air on which energy has been expended and which is not available for performing useful work.

The ratio of block fuel consumed by aircraft using each type of fuel is in the ratio of 3.50. It might normally be expected that the fuel used to perform a mission would be in approximately the same ratio as the SFC's realized in cruise. Actually, there is a leverage factor which works to the advantage of the LH₂ aircraft. Because that aircraft uses less fuel, it has a lower gross weight to accelerate and to lift to cruise conditions. This advantage, reduced somewhat by the lower L/D of the hydrogen fueled aircraft, produces an iterative fuel saving which compounds to produce the final block fuel weight relationship listed. The lower gross weight also permits a reduction in structure and propulsion weight in spite of the hydrogen tankage and insulation weight penalties.

For purposes of providing data for plotting in a later section (Section 8), the conventional, non-stop range capability of both the long range aircraft was calculated and the results are shown as the bottom entry of Table X'.

Table XVI is a summary of costs calculated for the subject aircraft. The basis for these cost estimates was presented in Sections 4.4 and 4.7 of Reference I. In the comparison shown the LH₂ aircraft are seen to cost less, both to develop and to produce, than the Jet A. The price of the Jet A aircraft is 3 percent greater than the LH₂ airplane.

In considering the development costs, it should be noted that the cost of basic hydrogen technology development was assumed to be funded separate and apart from the traditional aircraft development costs represented in the table. As discussed in the Reference 1 report, Section 6.0, a six year program is suggested during which such technology development

TABLE XVI. COST COMPARISON OF FINAL DESIGN
LONG RANGE AIRCRAFT

9265 km (5000 n.mi. radius - 200 Pax. - Mach 0.85)

	Aircraft No. 7 (Int LH ₂)		Aircraft No. 8 (Jet A)	
Development - \$10 ⁶				
Airframe	919.64		1221.79	
Engine (Amortized in prod. cost)	0		0	
TOTAL	919.64		1221.79	
Production - \$10 ⁶				
Airframe Cost	29.975		30.111	
Engine (Including R&D)	5.789		5.884	
Avionics	0.500		0.500	
R&D Amortization (Airframe)	2.628		3.491	
TOTAL AIRCRAFT PRICE	38.892		39.986	
Direct Operating Cost - $\frac{\$}{\text{km}}$ ($\frac{\$}{\text{n.mi.}}$)				
Crew	0.208	(0.385)	0.208	(0.386)
Maintenance				
Airframe Labor (Including Burden)	0.194	(0.359)	0.204	(0.377)
Engine Labor (Including Burden)	0.073	(0.135)	0.129	(0.238)
Airframe Material	0.126	(0.234)	0.131	(0.242)
Engine Material	0.113	(0.209)	0.173	(0.320)
Fuel* and Oil	1.154	(2.137)	0.933	(1.728)
Insurance	0.225	(0.416)	0.232	(0.429)
Depreciation	0.858	(1.589)	0.883	(1.635)
TOTAL DOC -	2.951	(5.465)	2.892	(5.355)
TOTAL UNIT DOC - $\frac{\$}{\text{seat km}}$ ($\frac{\$}{\text{seat n.mi.}}$)	0.738	(1.366)	0.723	(1.339)

*Fuel Cost:

Jet A = \$1.90/GJ ($\frac{\$}{10^6}$ Btu = 24.8¢/gal = 3.68¢/lb)

LH₂ = \$2.85/GJ ($\frac{\$}{10^6}$ Btu = 15.48¢/lb)

would occur before a decision need be made to proceed with development of a commercial transport airplane. The cost of this basic technology development is not included in the costs shown in Table XV.

Direct operating cost (DOC) is very sensitive to fuel cost. As noted in Table XVI, the fuel prices which were specified for use in this study to establish baseline DOC's were \$1.90 per GJ for Jet A (equivalent to $\$2/10^6$ Btu= 24.8ϕ /gal or 3.68ϕ /lb), and \$2.85 per GJ for LH₂ (equivalent to $\$3/10^6$ Btu's or 15.48ϕ /lb). The sensitivity of DOC to fuel cost is shown in Figure 30 for the long range vehicles. The price of Jet A fuel expressed in cents per gallon is shown for reference across the top of the grid.

To provide perspective for these comparisons, in September, 1975, U.S. international air carriers paid an average of 36.6ϕ /gal for Jet A fuel. The horizontal dotted line in Figure 30, shows that from the Jet A price of 36.6ϕ /gal, airlines could afford to pay \$1.00 more per GJ ($\$1.05/10^6$ Btu) for LH₂ and still operate at equal DOC. This price differential increases with fuel costs as shown by the divergence of the fuel cost lines.

6.5.1 Noise. - A comparison of noise generated by the two aircraft is presented numerically in Table XVII and graphically in Figure 31. The analysis was made using the takeoff and approach paths generated for the respective aircraft in the ASSET program, and using engine parameters and procedures described in section 4.8.2 of the final report of the previous study (Reference 1).

The LH₂ aircraft designed for the long range mission is appreciably quieter in flyover, but slightly noisier in sideline and approach, compared with its Jet A fueled counterpart. The LH₂ airplane is slightly noisier in approach for reasons previously explained. Both are significantly quieter than the limit noise calculated by the proposed standard, NPRM 75-37. The differences are 10.1 and 6.5 EPNdb quieter in flyover, 8.1 and 10.2 EPNdb quieter in sideline, and 6.0 and 9.5 EPNdb quieter in approach respectively, for the LH₂ and Jet A aircraft.

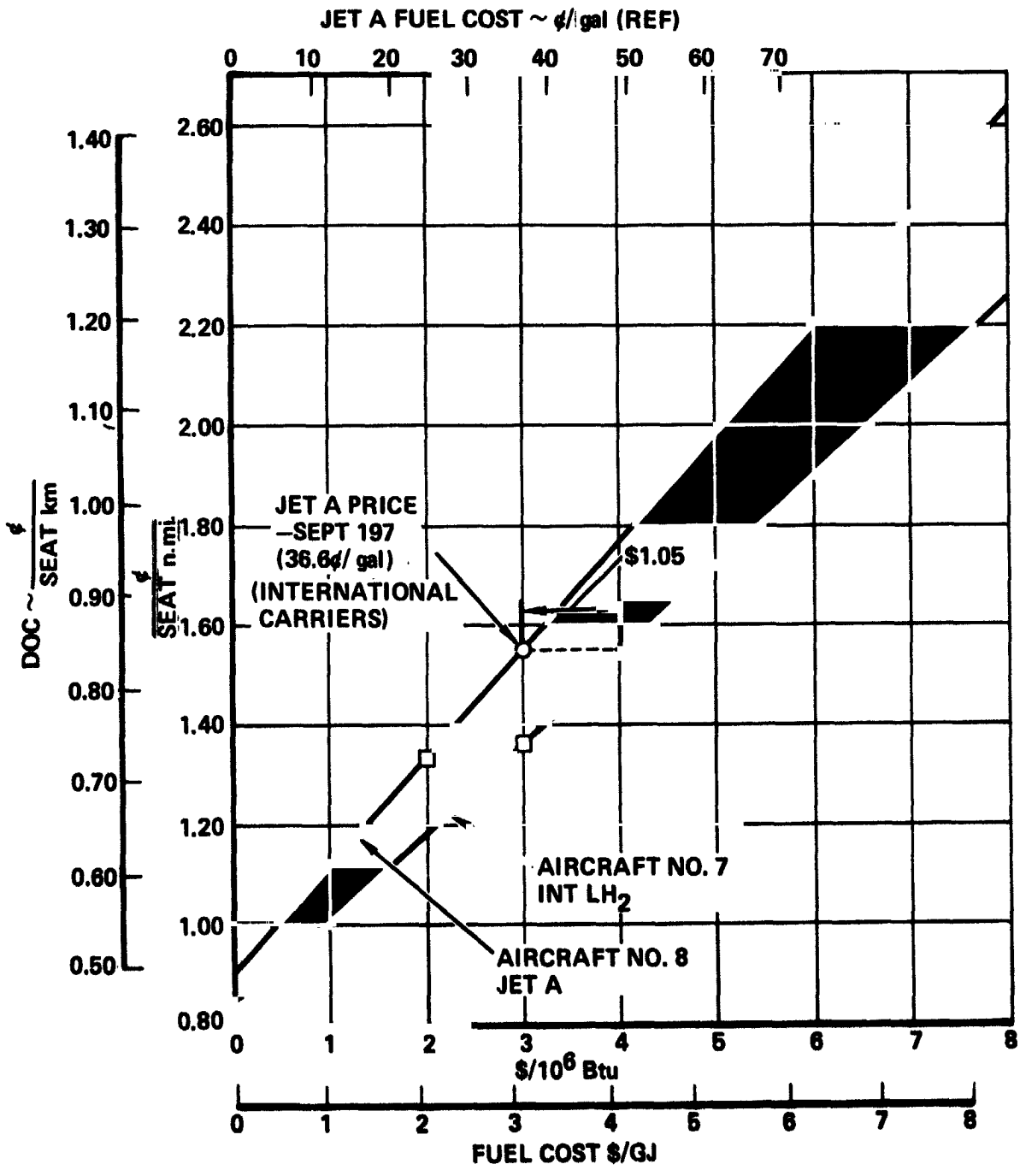


Figure 30. DOC vs Fuel Cost - 5000 n.mi. radius, 400 Pax Aircraft

TABLE XVII. NOISE EVALUATION - LONG RANGE AIRCRAFT

Airplane No.	7	8		
Number of Engines	4	4		
Fuel	LH ₂	Jet A		
Gross Weight kg (lb)	266,430 (587,370)	450,210 (992,520)		
Far 36 Flyover Level (EPNdB)	93.3	99.5		
Limit Per NPRM 75-37	103.4	106.0		
FAR 36 Sideline Level (EPNdB)	93.9	92.8		
Limit Per NPRM 75-37	102.0	103.0		
FAR 36 Approach Level (EPNdB)	97.9	95.5		
Limit Per NPRM 75-37	103.9	105.0		
Enclosed "Footprint" Contour Area				
	<u>km²</u>	<u>st.mi.²</u>	<u>km²</u>	<u>st.mi.²</u>
80 EPNdB - Takeoff	35.74	13.80	50.38	19.45
- Approach	<u>25.66</u>	<u>9.91</u>	<u>18.31</u>	<u>7.07</u>
- Total	61.40	23.71	68.69	26.52
90 EPNdB - Takeoff	8.52	3.29	11.16	4.31
- Approach	<u>3.13</u>	<u>1.21</u>	<u>1.84</u>	<u>0.71</u>
- Total	11.65	4.50	13.00	5.02

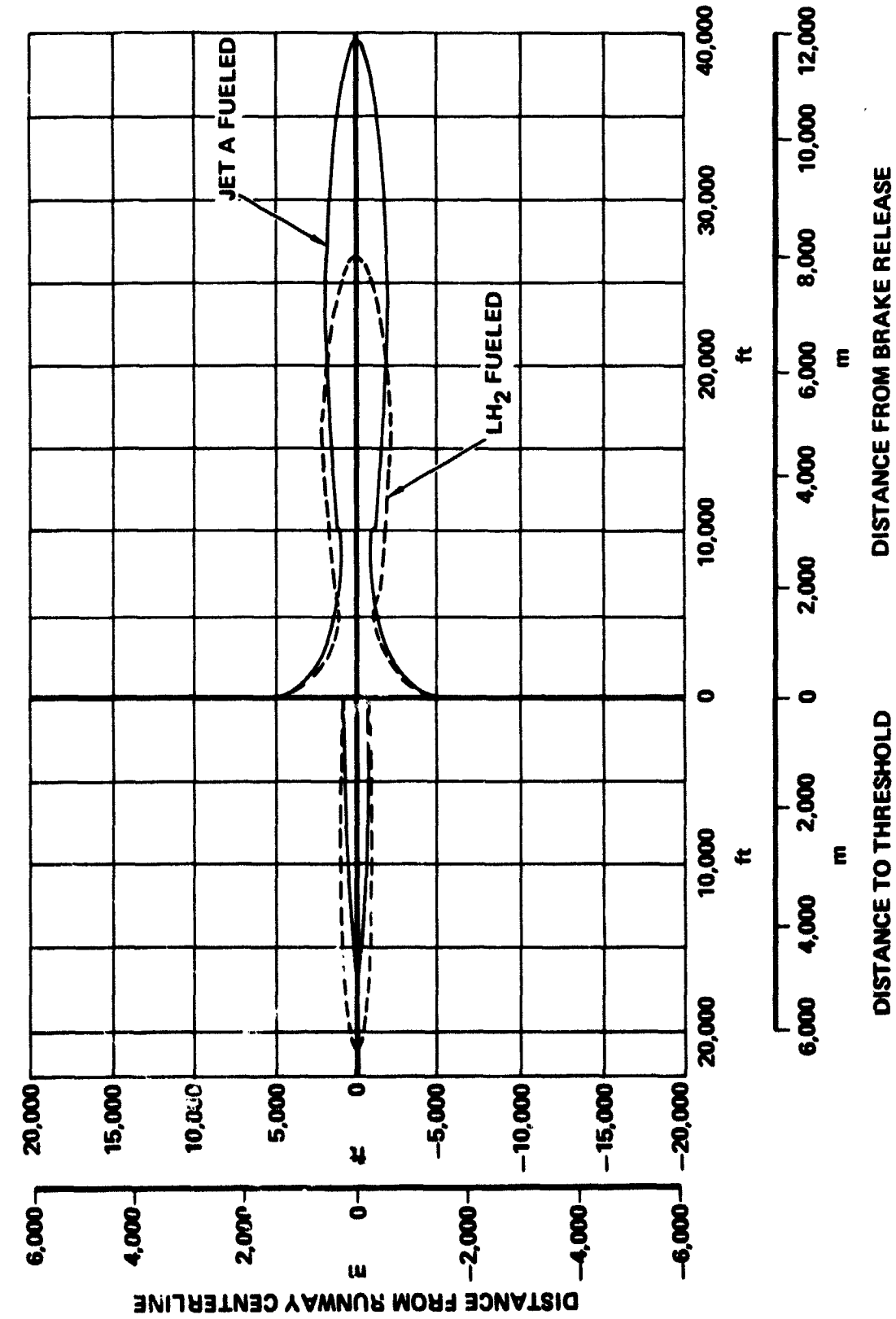


Figure 31. 9 EPNdB Contour Comparison - Long Range Aircraft

Aircraft No. 7 has a smaller total footprint area, for both the 80 and 90 EPNdb contours. As shown in Table XVII, the area of the 90 EPNdb contour for the LH₂ airplane is 11.65 km² (4.5 mi²) vs 13.0 km² (5.02 mi²) for the Jet A design. These areas are the total of approach plus takeoff.

6.6 Sensitivity Factors

The sensitivity of the large aircraft to increases in inert weight was briefly explored. Tables XVIII and XIX present the data which were generated for Aircraft Nos. 7 and 8, respectively. In each case, data for the base-line aircraft are presented, followed by columns representing changes in the parameters which would result from modifications in the design of the aircraft assuming 4536 kg (10,000 lb), was added to the inert weight before design freeze. For example, if detail design of the aircraft indicated that the structure was going to be 4536 kg (10,000 lb) heavier than the original allocation, in order to perform the design mission the aircraft would have to grow. The results are shown in the tables for selected parameters for both the LH₂ and the Jet A fueled aircraft.

The effect of this type of change is indicated in terms of growth factors in the tables. Gross weight and block fuel weight changes are expressed per unit of inert weight increase which caused the change. The change in airplane purchase price is also evaluated per unit of original inert weight increase. Changes in direct operating cost and energy utilization are both expressed in terms of the total inert weight change which perturbed the original design. Each of these growth factors is an expression of the rate of change of the given parameter as a function of a specified unit change in the variable.

The significant conclusion from this exercise follows from comparing growth factors for the LH₂ airplane from Table XVIII with corresponding factors for the Jet A design from Table XIX. The Jet A airplane is significantly more sensitive to changes in each of the parameters than is the LH₂ design. For instance, the gross weight of the Jet A airplane must increase 2.48 kg (5.49 lb) for every kilogram (pound) increase in inert weight, whereas the LH₂ design only requires 1.27 kg (2.8 lb) increase in gross weight to

TABLE XVIII. SENSITIVITY TO INERT WEIGHT INCREASE - BEFORE DESIGN FREEZE - AIRCRAFT NO. 7

		BASELINE		EFFECT OF 4536 kg (10,000 lb)	
		Increase in Inert Weight			
Basic Data					
Gross Weight	kg (lb)	266,430	(587,370)	279,170	(615,480)
Total Fuel Weight	kg (lb)	69,430	(150,850)	70,980	(156,470)
Block Fuel Weight	kg (lb)	59,610	(131,420)	61,770	(136,180)
Empty Weight	kg (lb)	147,700	(325,630)	153,290	(337,940)
Price	\$10 ⁶	38.89		40.27	
DOC	$\frac{\$}{\text{seat km}} \left(\frac{\$}{\text{seat n.mi.}} \right)$	0.738	(1.366)	0.762	(1.412)
Energy Utilization	$\frac{\text{kJ}}{\text{seat km}} \left(\frac{\text{Btu}}{\text{seat n.mi.}} \right)$	964	(1695)	999	(1756)
Growth Factors					
Gross Weight	$\left(\frac{\text{kg}}{\text{kg}} \frac{\text{lb}}{\text{lb}} \right)$			1.27	(2.8)
Block Fuel Weight	$\left(\frac{\text{kg}}{\text{kg}} \frac{\text{lb}}{\text{lb}} \right)$			0.22	(0.48)
Price	\$/kg \$/lb			304.	(138)
DOC	$\frac{\$}{\text{seat km}/4536 \text{ kg}} \left(\frac{\$}{\text{seat n.mi.}/10,000 \text{ lb}} \right)$.025	(0.046)
Energy Utilization	$\frac{\text{kJ}}{\text{seat km}/4536 \text{ kg}} \left(\frac{\text{Btu}}{\text{seat n.mi.}/10,000 \text{ lb}} \right)$			35.0	(61)

compensate for an unexpected 0.454 kg (1 lb) increase in inert weight. The increase in block fuel required by the Jet A vehicle is 1.01 kg (2.23 lb) per pound of inert weight increase; the value for the LH₂ airplane is only 0.22 kg (0.48 lb). For every 0.454 kg (pound) increase in inert weight the purchase price of the Jet A airplane goes up \$197; the LH₂ design, \$138. The growth factors for DOC and energy utilization are expressed in terms of 4536 kg (10,000 lb) increase of inert weight because these parameters are relatively insensitive.

TABLE XIX. SENSITIVITY TO INERT WEIGHT INCREASE - BEFORE DESIGN
FREEZE - AIRCRAFT NO. 8

		BASELINE		EFFECT OF 4536 kg (10,000 lb)	
				Increase in Inert Weight	
Basic Data					
Gross Weight	kg (lb)	450,200	(992,520)	475,300	(1,047,800)
Total Fuel Weight	kg (lb)	237,880	(524,000)	248,520	(550,100)
Block Fuel Weight	kg (lb)	208,720	(460,150)	218,820	(482,400)
Empty Weight	kg (lb)	159,280	(351,150)	167,570	(369,400)
Price	\$10 ⁶	39.99		41.99	
DOC	$\frac{\phi}{\text{seat km}} \left(\frac{\phi}{\text{seat n.mi.}} \right)$	0.723	(1.339)	0.755	(1.398)
Energy Utilization	$\frac{\text{kJ}}{\text{seat km}} \left(\frac{\text{Btu}}{\text{seat n.mi.}} \right)$	1,205.	(2117)	1,263.	(2219)
Growth Factors					
Gross Weight	$\frac{\text{kg}}{\text{kg}} \left(\frac{\text{lb}}{\text{lb}} \right)$	(0)		2.49	(5.49)
Block Fuel Weight	$\frac{\text{kg}}{\text{kg}} \left(\frac{\text{lb}}{\text{lb}} \right)$	(0)		1.01	(2.23)
Price	\$/kg (\$/lb)	(0)		434	(197)
DOC	$\frac{\phi}{\text{seat km}/4536 \text{ kg}} \left(\frac{\phi}{\text{seat n.mi.}/10,000 \text{ lb}} \right)$	(0)		0.032	(0.069)
Energy Utilization	$\frac{\text{kJ}}{\text{seat km}/4536 \text{ kg}} \left(\frac{\text{Btu}}{\text{seat n.mi.}/10,000 \text{ lb}} \right)$	(0)		95.	(102)

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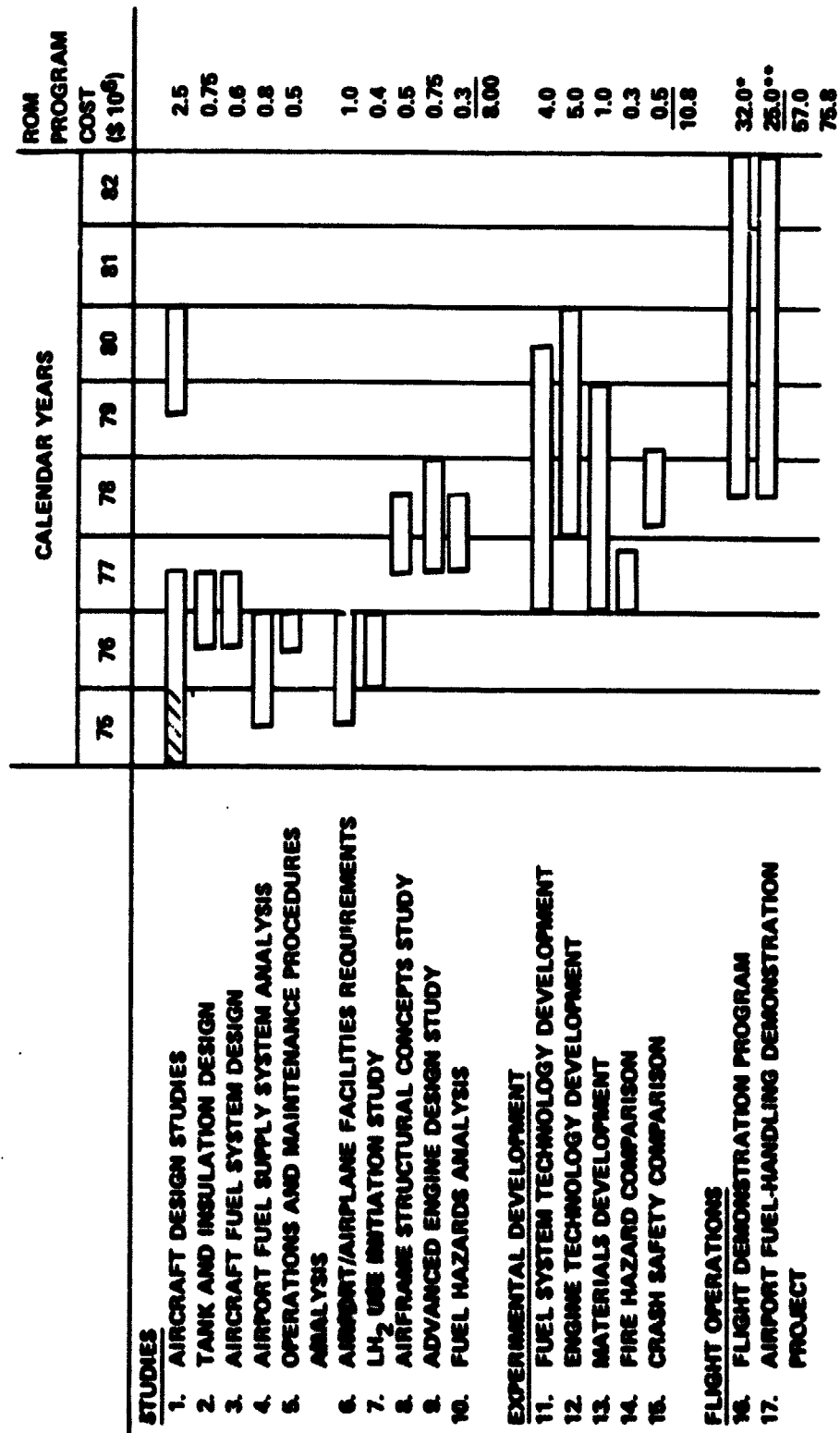
7. RESEARCH AND DEVELOPMENT RECOMMENDATIONS

Technology development required for LH₂ fueled transport aircraft is essentially as described in the final report of the previous study (Reference 1). For convenience, the recommended development program schedule from that report (Figure 99, p 302 from Reference 1) has been updated and is presented as Figure 32. Of the items recommended, a preliminary assessment of task 4, "Airport Fuel Supply System Analysis" has been funded and the work is in progress.

In addition to the technology development listed in Figure 32, a very significant event for which there is an immediate need is an assessment of the impact the initiation of use of hydrogen as fuel for commercial transport aviation would have on society in general.* In a sense this effort would be a preliminary study of task 9, Figure 32, since one output would be a hypothetical but realistic scenario depicting the transition to hydrogen. In addition, the economic ramifications, the institutional barriers and incentives, and the social dislocations and opportunities of all major stakeholder classes in society would be disclosed. Stakeholder classes whose participation in the evolutionary scenario would be described include the following:

- airlines
- aircraft manufacturers
- fuel suppliers
- airport operators
- consumers
- government regulators
- work forces
- general public

*This study suggested by Stanford Research Institute, September 26, 1975.



*COST ESTIMATE FROM REFERENCE 30

**COST ESTIMATE FROM REFERENCE 31

Figure 32. Technology Development Program

While not classified as a "technology development," this study would provide important input and an order of priorities for the technical work. In addition it would acquaint, and hopefully convince, many stakeholders of the need for early conversion of commercial aviation to hydrogen fuel.

8. CONCLUSIONS AND RECOMMENDATIONS

This study explored an enlarged matrix of passenger/range mission requirements to determine the comparative desirability of LH₂ vs Jet A fuel, relative to the missions studied in the original program (Reference 1).

The analysis showed that even for short range missions the internal tank arrangement for LH₂ fueled aircraft is clearly preferred from a performance and cost point of view over the design concept which uses external tanks. In order to provide a fineness ratio for the externally mounted tanks which is aerodynamically acceptable, the surface-to-volume ratio of the tanks is increased to the point that insulation must be both thick and therefore heavy to achieve acceptable boiloff percentages.

The results of the study of small payload - short range aircraft, designed to carry 130 passengers 2780 km (1500 n.mi.), showed that use of LH₂ offers no performance advantage compared to a Jet A fueled design. This mission appears to represent an approximate crossover point. Payload/range requirements which involve use of larger Jet A fuel loads show increasing advantage for using LH₂ fuel. It is probable that aircraft designed for even shorter ranges and smaller payloads would begin to show net disadvantages for LH₂ fueled aircraft. The advantages of using the higher energy fuel are mitigated by the penalties involved: weight of tanks, insulation, and fuel system, plus the increased drag due to the larger volume required for the LH₂ fuel and the insulation surrounding the tanks. The aircraft are essentially equal insofar as noise is concerned. They are both significantly quieter than limits calculated according to the newly proposed change to the noise standard (Reference 3).

Analysis of aircraft designs for the medium range mission, which involves carrying 200 passengers 5560 km (3000 n.mi.), showed the internal tank LH₂ aircraft to have marginally superior characteristics, compared with the Jet A design. It is considerably lighter in gross weight but slightly heavier in empty weight. The Jet A aircraft requires 9 percent more energy to perform

the design mission. The LH₂ design is 4 EPNdB quieter in flyover but slightly noisier in sideline and approach than its Jet A counterpart. Its 90 EPNdB contour is slightly smaller.

The long range mission involved a requirement for carrying 400 passengers 9265 km (5000 n.mi.), landing, then taking off without refueling and flying another 9265 km segment with full payload. Full reserve fuel calculated by ATA international definition was provided for each segment. The LH₂ fueled aircraft showed important advantages over the Jet A design for this mission. It is lighter, requires a smaller wing but a larger fuselage, uses smaller engines, can operate from shorter runways, and uses 25 percent less energy per seat mile in performance of the design mission. The LH₂ airplane would cost less both to develop and to produce. A differential of \$1.00 more per GJ (\$1.05/10⁶ Btu) can be paid for LH₂, relative to a current price for Jet A, and still provide equal DOC. The LH₂ airplane is nearly 6 EPNdB quieter in flyover, but slightly noisier in sideline and approach compared to the Jet A design. Both aircraft are significantly quieter than the noise limit calculated according to the pending revision to FAR 36. The LH₂ airplane has a slightly smaller 90 EPNdB contour.

A study of sensitivities of the long range aircraft to increases in inert weight before design freeze showed the LH₂ design to be considerably less sensitive.

Results of analyses from the previous study of subsonic passenger transport aircraft (Reference 1) are combined with those from the present work and are plotted in Figures 33 and 34. The total energy (represented by the energy content of the block fuel) required to perform various payload-range missions is displayed as a function of the mission requirements (expressed in available seats times design range in Figure 33). Two characteristics are plotted, the trend of energy requirement for aircraft of a given passenger capacity - with range as the variable, and the energy requirement of aircraft designed for a given range - with passenger capacity as the variable.

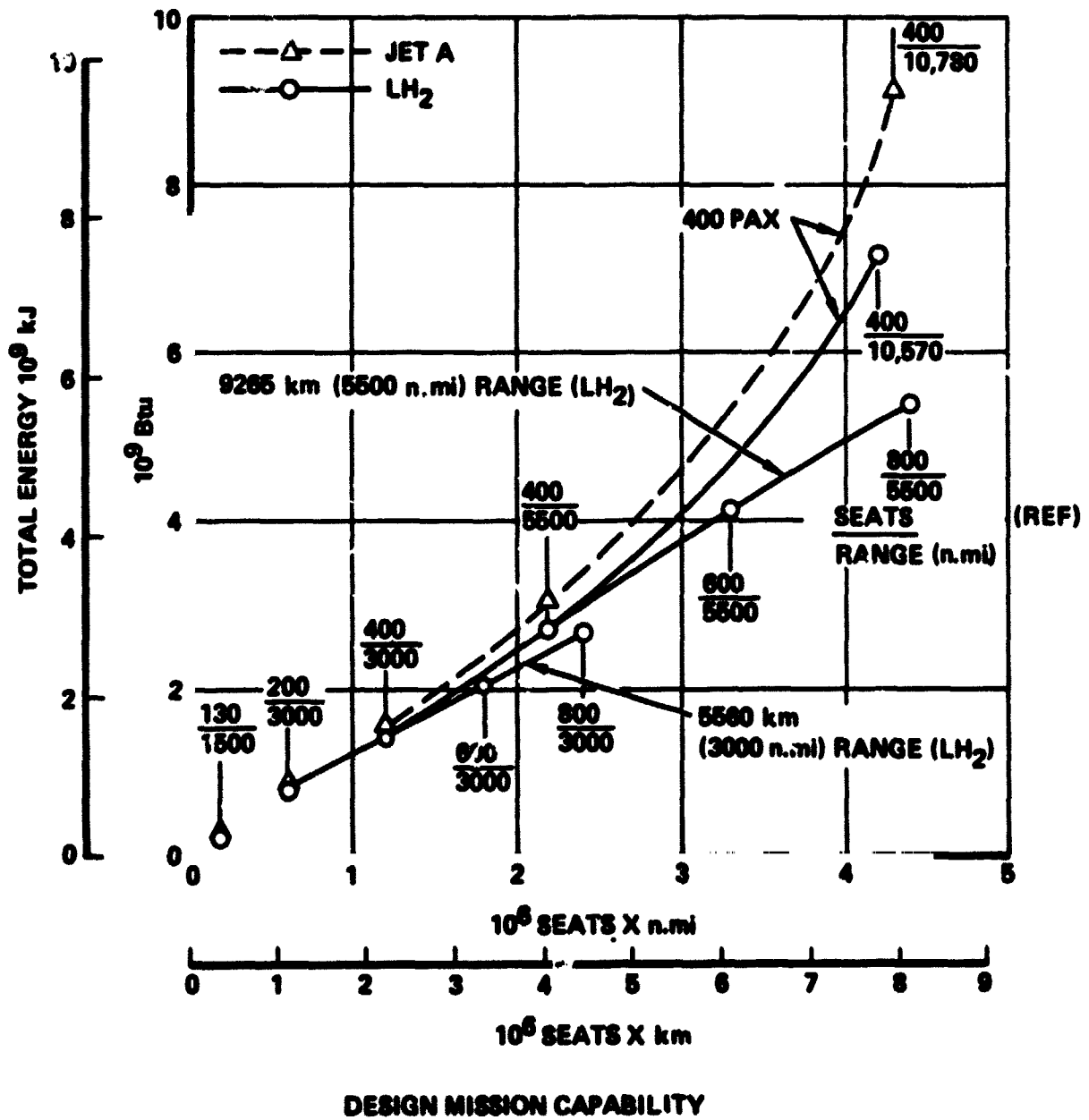


Figure 33. Total Energy vs Design Mission Capability .

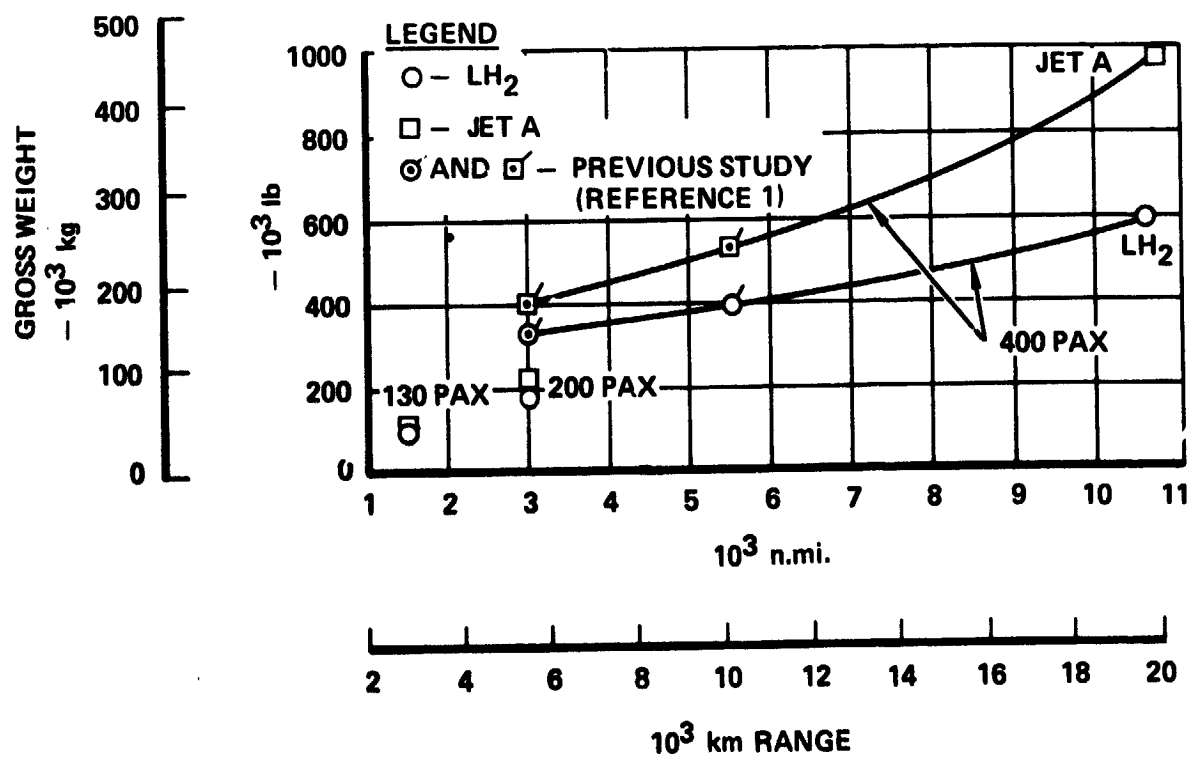
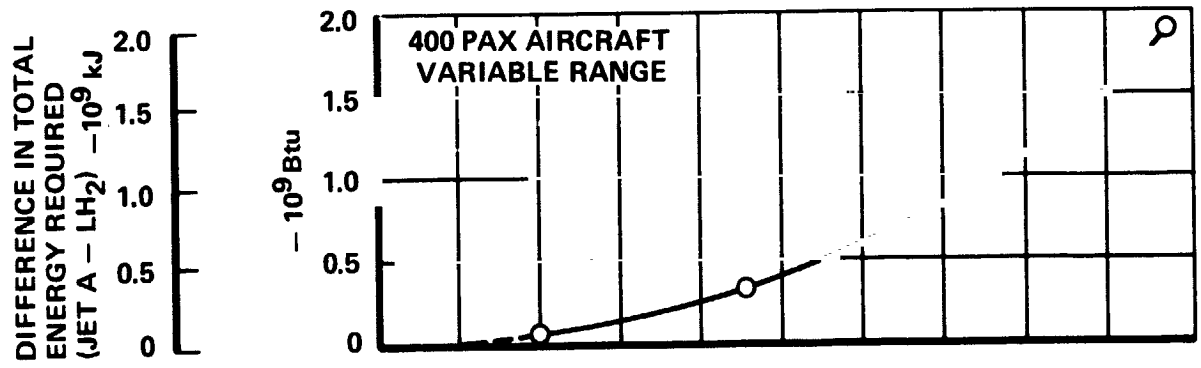
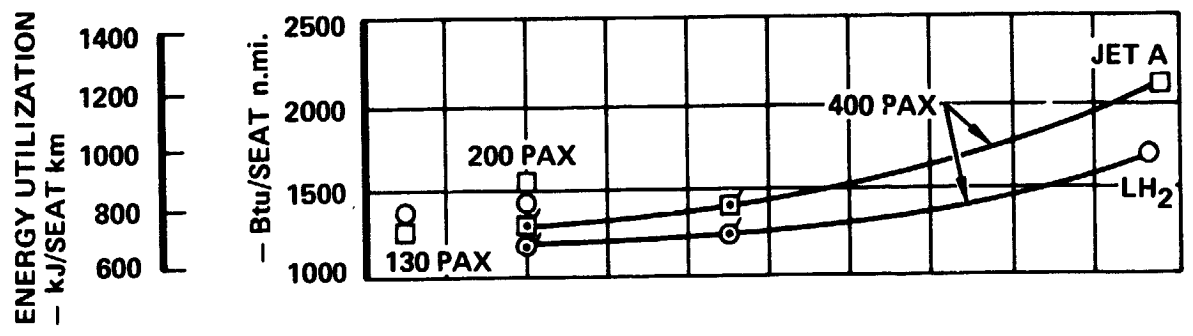


Figure 34. Growth Characteristics

The figure shows that the energy requirement varies almost linearly as passenger capacity increases from 400 to 800 seats in aircraft designed for a given range. On the other hand, as the range requirement changes in aircraft designed for a constant number of passengers, the energy requirement varies exponentially. In other words, more energy is required to increase the mission capability (seats x distance) of a given aircraft configuration by increasing its range than by adding to its passenger seating capacity. It is also apparent that the energy requirement for Jet A fueled aircraft increases substantially faster than for aircraft fueled with LH₂.

Three additional relationships for the 400 passenger aircraft are plotted in Figure 34. Gross weight, energy utilization, and the difference in energy required by the Jet A fueled aircraft - relative to the LH₂ - to perform the various design missions, are all plotted vs range. For reference, points representing the 130 passenger and 200 passenger aircraft design are also shown.

The advantage of using LH₂ as fuel in transport aircraft increases with the amount of energy required to perform the mission. The crossover point, above which LH₂ can be used to advantage, and below which Jet A is more energy efficient, seems to vary somewhat with the passenger load. For the 130 passenger Mach 0.85 aircraft shown in the lower left corner of Figure 33 the crossover point is approximately the 2780 km (1500 n.mi.) design range, which requires about 0.264 kJ (0.25×10^9 Btu). For a 400 passenger Mach 0.85 aircraft the crossover appears to be just under 3700 km (2000 n.mi.) design range, a mission which needs approximately 1.054 kJ (10^9 Btu).

In view of the obvious advantages of LH₂ fuel in long range aircraft an aggressive program of technology investigation and development is recommended. In particular, a societal impact study is recommended for immediate undertaking.

APPENDIX A

SELECTED PAGES OF ASSET COMPUTER PRINTOUT FOR
EIGHT AIRCRAFT

A-1	Internal Tank LH ₂		
A-2	External Tank LH ₂	}	Short Range Aircraft
A-3	Jet A		
A-4	Internal Tank LH ₂	}	Medium Range Aircraft
A-5	External Tank LH ₂		
A-6	Jet A		
A-7	Internal Tank LH ₂	}	Long Range Aircraft
A-8	Jet A		

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LIQUID HYDROGEN---BASIC DESIGN MISSION/130 PASS/ 1500 N MI MISS INT. L.H.L.

T/C T/R AR LAM W/S T/W
 10.60 0.30 10.00 30.00 107.8 0.345

C O N F I G U R A T I O N G E O M E T R Y

WING-- AREA(SQ.FT) SPAN(FT) TAPER RATIO C/4 SWEEP (DEC) L.F. SWEEP (DEC) L.F.P/CHORD
 911.5 94.47 0.300 30.000 32.260 0.0
 CR(FT) CY(FT) MAC(FT) CRE(FT) S MET(SO.FT) REF L(FT)
 14.69 4.41 10.47 13.29 1468.6 10.47

WING TANK-- CHAR1(FT) CHAR2(FT) FTL(FT) FWMING(CU FT) FVROX(CU FT)
 13.29 5.15 17.77 0.00 0.00

FUSELAGE-- LENGTH(FT) S MET(SQ FT) BW(FT) EQUIV D(FT) SPI(SO FT)
 139.47 5100.5 13.00 13.32 146.30

RW(FT) BW(FT) SBW(SO FT) FVB(CU FT)
 13.00 13.66 5100.49 1407.29

TAIL-- SMT(SO.FT) SMTX(SO.FT) HT REF L(FT) SVT(SO.FT) SVTX(SO.FT) VT REF L(FT)
 94.04 77.54 4.68 89.96 89.96 8.25

PROPULSION-- ENG L(FT) ENG D(FT) POD L(FT) POD D(FT) POD S MET (SO. FT) NO. PODS INLET L(FT)
 7.22 4.91 16.16 5.37 545.04 2. 0.0

A-1
 Aircraft No. 1
 LH2 Internal Tank
 130 PAX, 1500 n mi range
 Mach 0.85

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LIQUID HYDROGEN----BASIC DESIGN MISSION/130 PASS/ 1500 N M J MISS

T/C T/R AR LAM W/S T/W
 10.00 0.30 10.00 30.00 107.8 0.345

	POUNDS	O/O	POUNDS	O/O
DESIGN GROSS WEIGHT	98257.	100.00		
FUEL	7364.	7.49		
PAYLOAD	28600.	29.11		
OPERATING WEIGHT EMPTY	2871.	2.92		
STANDARD ITEMS	1457.	1.48		
EMPTY WEIGHT-MFG.				
WING	7923.	8.06		
TAIL	904.	0.92		
BODY	11665.	11.87		
LANDING GEAR	3762.	3.83		
FLIGHT CONTROLS	1530.	1.56		
MACELLES	2031.	2.07		
PROPULSION SYSTEM	12530.	12.76		
ENGINE	6815.			
AIR INTAKE	787.			
EXHAUST	617.			
COOLING	0.			
OIL SYSTEM (LESS OIL)	11.			
ENGINE CONTROLS	38.			
ENGINE STARTING	118.			
TANKS	1588.			
INSULATION	1603.			
FUEL-PLUMBING	960.			
INSTRUMENTS			831.	0.85
HYDRAULICS			948.	0.96
ELECTRICAL			2586.	2.63
ELECTRONICS			688.	0.70
FURNISHINGS AND EQUIP.			9440.	9.61
AIR CONDITIONING			1873.	1.91
ANTI-ICING			137.	0.14
AUXILIARY POWER UNIT			430.	0.44
MISCELLANEOUS			0.	0.0
DESIGN RESERVE			0.	0.0

NO. OF PASSENGERS 130.
 NO. OF CREW 7.
 STRUCTURAL T/C 12.50
 FUEL VOLUME REQD 1761.0
 WING FUEL VOLUME AVAILABLE 0.0

M I S S I O N S U M M A R Y

LIQUID HYDROGEN--BASIC DESIGN MISSION/130 PASS/ 1500 N MI MISS

SEGMENT	INIT ALTITUDE (FT)	INIT MACH NO	INIT WEIGHT (LB)	SECTY FUEL (LB)	TOTAL FUEL (LN)	SFGT DIST (N MI)	TOTAL DIST (N MI)	SEGMT TIME (MIN)	TOTAL TIME (MIN)	EXTERN STORE TAB ID	ENGINE THRUST TAB ID	EXTERN F TANK TAB ID	AVG L/D RATIO	AVG SFC (FF/7)
TAKEOFF														
POWER 1	0.	0.0	98257.	49.	49.	0.	0.	14.0	14.0	0.	-83101.	0.	0.0	0.124
POWER 2	0.	0.0	98208.	56.	105.	0.	0.	1.0	15.0	0.	83401.	0.	0.0	0.100
CLIMB	0.	0.378	98152.	154.	260.	13.	13.	2.9	17.9	0.	83101.	0.	15.75	0.161
ACCEL	10000.	0.456	97998.	58.	318.	7.	20.	1.2	14.1	0.	83101.	0.	13.00	0.184
CLIMB	10000.	0.638	97439.	1386.	1703.	332.	352.	40.7	59.8	0.	83101.	0.	11.93	0.212
CRUISE	36000.	0.850	96554.	2668.	4372.	898.	1250.	110.4	170.2	0.	-83101.	0.	13.87	0.211
DESCENT	36000.	0.850	93886.	43.	4415.	51.	1201.	6.5	176.7	0.	83301.	0.	11.01	-1.716
DECEL	10000.	0.638	93842.	13.	4428.	8.	1309.	1.4	178.0	0.	83301.	0.	13.13	47.336
DESCENT	10000.	0.456	93829.	74.	4508.	32.	1341.	7.2	185.2	0.	83301.	0.	15.50	0.847
CRUISE	36000.	0.850	93751.	469.	4975.	149.	1500.	19.6	204.8	0.	-83101.	0.	13.75	0.211
LOITER	1500.	0.248	93282.	86.	5061.	0.	1500.	6.0	210.8	0.	-83101.	0.	16.07	0.148
RESET	0.	0.0	93196.	0.	5061.	0.	1500.	0.0	210.8	0.	0.	0.	0.0	0.0
RESET	0.	0.0	93196.	0.	5061.	-1506.	0.	-210.8	0.0	0.	0.	0.	0.0	0.0
CRUISE	36000.	0.850	93196.	1429.	6490.	0.	0.	60.0	60.0	0.	-83101.	0.	13.67	0.211
RESET	0.	0.0	91767.	0.	6490.	0.	0.	0.0	60.0	0.	0.	0.	0.0	0.0
CLIMB	0.	0.378	91767.	142.	6632.	12.	12.	2.7	62.7	0.	83101.	0.	15.27	0.161
ACCEL	10000.	0.456	91625.	23.	6654.	3.	15.	0.5	63.2	0.	83101.	0.	13.95	0.175
CLIMB	10000.	0.547	91603.	393.	7048.	70.	84.	10.4	73.6	0.	83101.	0.	13.15	0.193
CRUISE	30000.	0.650	91209.	44.	7091.	15.	100.	2.4	76.0	0.	-83101.	0.	15.67	0.169
DESCENT	30000.	0.700	91166.	50.	7141.	47.	147.	7.1	83.1	0.	83301.	0.	12.97	-5.275
DECEL	10000.	0.547	91116.	7.	7148.	4.	151.	0.8	83.8	0.	83301.	0.	14.01	1.705
DESCENT	10000.	0.456	91109.	57.	7205.	25.	175.	5.4	89.2	0.	83301.	0.	15.29	0.889
CRUISE	30000.	0.650	91052.	70.	7274.	25.	200.	3.8	93.0	0.	-83101.	0.	15.64	0.169
LOITER	1500.	0.245	90993.	84.	7358.	0.	200.	6.0	99.0	0.	-83101.	0.	16.04	0.148

TDCMTC 98257.3 FUEL A= 7364.4 FUEL R= 7358.2

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LIQUID PROPELLANT--BASIC MISSION MISSION/30 PASS/ 1500 N MI MISS BRT LM₂

T/C T/F BP LAM M/S T/M
 10.00 0.20 0.50 50.00 100.0 0.450

C O N F I G U R A T I O N C E L L M I T O V

WING-- AREA(CU FT) SPAN(FT) T. PER RATIO C/4 SWEEP L.E. SWEEP L.E.-R/CHORD
 (DEG) (DEG)
 1017.0 96.32 0.260 30.000 31.901 0.0
 CG(FT) CT(FT) MAC(FT) CR(FT) S MET(SQ-FT) PFF(FT)
 14.70 5.91 10.98 13.61 1792.2 10.98

WING TANK-- CG(FT) CFAR2(FT) FT(LIFT) FWMING(CU FT) FVEX(CU FT)
 13.61 6.56 30.10 0.00 0.00

FUSELAGE-- LUNGH(FT) S MET(SQ FT) GWH(FT) FQUIV P(FT) SPIISC FT)
 113.00 4077.0 13.00 13.32 130.30

GH(FT) SHWISC FT) FVRI(CU FT)
 13.00 13.66 4077.00 0.00

TAIL-- SWY(SC FT) SWY(SC FT) HY PFF L(FT) SWY(SC FT) SWY(SC FT) VY EFF L(FT)
 163.16 170.66 6.12 130.7P 130.7P 10.20

REPPUSION-- FW L(FT) ENG L(FT) PCD L(FT) PCD R(FT) PCD S MET (SQ. FT)
 0.55 5.93 14.16 6.48 780.37 2.0

FUEL PINS-- VOL(CU FT) LFN(HT) SPIISC FT) S MET(SQ FT) MC PDS
 200.21 45.68 107.00 2200.5 2.0

A-2
 Aircraft No. 2
 LH₂ External Tank
 130 PAX, 1500 n mi range
 Mach 0.85

LIQUID MARGIN—BASIC DESIGN MISSION/130 PASS/ 1500 M MI MISS

T/C T/A AR LAM W/S T/M
 10.00 1.40 0.50 30.00 108.0 0.450

	POUNDS	0/N	POUNDS	0/N
DESIGN GROSS WEIGHT	100002.	100.00		
FUEL	9616.	8.75		
ZERO FUEL WEIGHT			100286.	
PAVLOAD	29600.	26.02	71686.	65.23
OPERATING WEIGHT EMPTY	2296.	2.63		
OPERATIONAL ITEMS	1578.	1.50		
STANDARD ITEMS				
EMPTY WEIGHT—MFC.				
WING	0157.	0.51		
TAIL	1505.	1.37		
NOSE	10791.	9.82		
LANDING GEAR	3037.	3.58		
FLIGHT CONTROLS	1686.	1.53		
WHEELS	3063.	2.77		
PROMUSION SYSTEM	10393.	17.64		
ENGINE				
AIR INTAKE	10200.			
EXHAUST	1170.			
COILING	025.			
OIL SYSTEM (LESS OIL)	6.			
ENGINE CONTROLS	11.			
ENGINE STARTING	57.			
TEMP.	172.			
INSULATION	265.			
FUEL—PUMPING	3702.			
780.				
INSTRUMENTS				
HYDRAULICS	842.	0.77		
ELECTRICAL	1077.	0.93		
ELECTRONICS	2400.	2.27		
FURNISHING AND EQUIP.	918.	0.84		
AIR CONDITIONING	0440.	0.59		
ANTI-ICING	1073.	1.20		
AUXILIARY POWER UNIT	144.	0.13		
MISCELLANEOUS	870.	0.76		
DESIGN RESERVE	0.	0.00		
	0.	0.00		

NO. OF PASSENGERS 120.
 NO. OF CREW 7.
 STRUCTURAL T/C 17.50
 FUEL VOLUME REQD 2296.00
 WING FUEL VOLUME AVAILABLE 0.0

M I S S I O N S U M M A R Y

LIQUID HYDROGEN---BASIC DESIGN MISSION/130 PASS/ 1500 N MI MISS

SEGMENT	INIT ALTITUDE (FT)	INIT MACH NO	INIT WEIGHT (LB)	SEGMT FUEL (LR)	SEGMT FUEL (LR)	SEGMT DIST (N MI)	SEGMT TIME (MIN)	TOTAL TIME (MIN)	EXTERN STORE TAB IN	ENGINE THRUST TAB IN	EXTERN F TANK TAB IN	AVG L/D RATIO	AVG SFC (PP/7)
TAKEOFF													
POWER 1	0.	0.0	100002.	71.	71.	0.	14.0	14.0	0.	-83101.	0.	0.0	0.124
POWER 2	0.	0.0	100031.	82.	153.	0.	1.0	15.0	0.	83401.	0.	0.0	0.100
CLIMB	0.	0.378	100748.	108.	321.	10.	2.2	17.2	0.	83101.	0.	12.77	0.161
ACCEL	10000.	0.454	100580.	67.	385.	5.	0.8	18.1	0.	83101.	0.	10.35	0.184
CLIMB	10000.	0.634	100517.	147.	1056.	251.	30.9	49.0	0.	83101.	0.	9.79	0.212
CRUISE	20000.	0.850	100045.	2846.	5703.	984.	121.1	170.0	0.	-83101.	0.	11.74	0.211
DESCENT	30000.	0.850	100100.	52.	4754.	43.	4.5	175.5	0.	93301.	0.	8.82	-1.058
DECEL	10000.	0.630	100148.	15.	4769.	6.	1.1	176.6	0.	83401.	0.	10.30	46.587
DESCENT	10000.	0.454	100133.	94.	5462.	26.	5.9	182.5	0.	83401.	0.	12.52	0.847
CRUISE	10000.	0.450	100000.	675.	6537.	175.	150.	203.9	0.	-83101.	0.	11.61	0.211
LOITER	1400.	0.243	100364.	110.	6647.	0.	4.0	204.9	0.	-83101.	0.	14.29	0.152
RESET	0.	0.0	100254.	0.	6647.	0.	0.0	204.9	0.	0.	0.	0.0	0.0
RESET	0.	0.0	100254.	0.	6647.	-1500.	-200.9	0.0	0.	0.	0.	0.0	0.0
CRUISE	50000.	0.850	100254.	1054.	8482.	0.	60.0	60.0	0.	-83101.	0.	11.78	0.211
RESET	0.	0.0	101420.	0.	8482.	0.	0.0	60.0	0.	0.	0.	0.0	0.0
CLIMB	0.	0.378	101420.	153.	8634.	0.	2.0	6.0	0.	83101.	0.	12.22	0.161
ACCEL	10000.	0.454	101267.	24.	9059.	2.	0.2	62.3	0.	83101.	0.	11.11	0.175
CLIMB	10000.	0.447	101243.	411.	9049.	50.	7.4	64.0	0.	83101.	0.	10.35	0.192
CRUISE	20000.	0.607	100832.	150.	9420.	40.	6.6	76.3	0.	-83101.	0.	13.49	0.184
DESCENT	30000.	0.700	100682.	57.	9276.	37.	5.6	81.4	0.	83301.	0.	10.19	-5.262
DECEL	10000.	0.447	100625.	8.	9284.	3.	0.6	92.7	0.	93301.	0.	11.10	1.701
DESCENT	10000.	0.454	100617.	67.	9341.	20.	4.4	97.0	0.	93301.	0.	12.24	0.889
CRUISE	20000.	0.605	100550.	152.	9404.	60.	6.7	93.5	0.	-83101.	0.	13.47	0.184
LOITER	1000.	0.240	100300.	107.	9611.	0.	4.0	94.5	0.	-83101.	0.	14.28	0.153
TOTALS	100001.0		FUEL AT 0615.8					FUEL R= 6610.9					

C O S T S U M M A R Y

WING 626710.00
 TAIL 121045.04
 BODY 040618.62
 LANDING GEAR 040370.24
 FLIGHT CONTROLS 115182.63
 MACULLES 362150.56
 ENGINE 14051.32
 AIR INTUCTION 100526.60
 FUEL SYSTEM 413026.14
 START SYSTEM 2740.50
 ENGINE CONTROLS 1100.14
 INSTRUMENTS 125214
 LIFE SYSTEM 2176.15
 TOTAL PROPULSION 734907.04
 INSTRUMENTS 120402.13
 HYDRAULICS 71185.56
 ELECTRICAL 214102.60
 ELECTRONIC BACKS 47967.66
 PUBLISHING 21116.13
 AIR COMPETITION 143462.10
 AIRCRAFT 11114.62
 APU 40242.00
 SVS. INTEGRATION 01741.71

6221401.00

6220245.00

SUSTAINING ENGINEER 270000.00
 TECHNICAL DATA 0.00
 PROG. TOOLING MAINT. 367471.13
 MISC. 102000.00
 ENG. CHANGE ORDER 303618.60
 QUALITY ASSURANCE
 AIRFRAME MAINT 0.00
 AIRFRAME PFE 0.00
 AIRCRAFT COST 303618.60
 ENGINE WARRANTY
 ENGINE FEE
 ENGINE COST
 AVIONICS COST
 RESEARCH AND DEVELOPMENT
 TOTAL FLY AWAY COST

DIRECT OPERATING COST-COLLARS/M. MILE 0.00
 CREW 10.35
 AIRFRAME LACK AND BURDEN PAINT. 6.4100
 ENGINE LACK AND BURDEN PAINT. 6.1440
 AIRFRAME MATERIAL PAINT. 0.1043
 ENGINE MATERIAL PAINT. 0.1715
 AIRFRAME MATERIAL PAINT. 0.0042
 FUEL AND OIL 0.7200
 INSULANCE 0.1170
 DEPRECIATION (INCLUDING SPARE) 0.0140
 TOTAL MC 1/M. MILE 2.1406 100.00

R AND D
 DEVELOPMENT TECHNICAL DATA 4010023.
 DESIGN ENGINEERING 15,373172.
 DEVELOPMENT TOOLING 5,002,032.
 DEVELOPMENT TEST ARTICLE 2,659,752.
 FLIGHT TEST 141,000.78.
 SPECIAL SUPPORT EQUIPMENT 184,200.
 DEVELOPMENT SPARE 1,870,000.
 ENGINE DEVELOPMENT 0.
 AVIONICS DEVELOPMENT 0.
 TOTAL R AND D 774660252.

0330716.00

0330716.00

657. 707. 1074. 1219. 1340. 1500.
 2,0051 1,8007 1,7713 1,7293 1,6940 1,6689
 1,7006 2,0570 2,0224 2,0224 3,2107 3,4091
 1712. 1049. 2447. 2746. 2947. 3254.

ORIGINAL PAGE 11
OF POOR QUALITY

JP FUEL REFERENCE BASELINE DESIGN / 130 PAS' / 1400 N MI MISS JETA
 T/C T/R AR LAM M/S T/W
 IC.OC 6.70 11.00 10.00 117.6 0.348

C O N F I G U R A T I O N G E O M E T R Y

WING--	AREALISO (FT)	SPAN (FT)	TAPER RATIO	C/4 SWEEP (DEG)	L.F. WEEP (DEG)	L.E.R/CHORD (DEG)
	428.7	101.07	0.300	30.000	12.050	0.0
	CR (FT)	MC (FT)	CR (FT)	S W (ISO, FT)	REF L (FT)	
	16.14	4.24	10.00	12.86	1402.8	10.00
WING TANK--	CGAR (FT)	CHARZ (FT)	FL (FT)	FWING (CU FT)	WV (NOXICU FT)	
	12.06	6.06	40.37	333.00	46.64	
FUSELAGE--	LFMC (FT)	S W (ISO FT)	BM (FT)	FOUR (NFT)	SPISO (FT)	
	113.00	4077.0	13.00	13.32	139.30	
	FW (FT)	SMISO (FT)	FW (CU FT)			
	13.00	13.64	4077.00	99000.00		
TAIL--	SMTISO (FT)	MT REF L (FT)	SVTISO (FT)	SVTISO (FT)	VT REF L (FT)	
	132.64	46.24	125.38	125.38	0.70	
PROPULSION--	ENG LIFT	ENG DIFT	PD LIFT	PD DIFT	PD S WFT (SO, FT)	NO. PODS INLET L (FT)
	7.50	5.17	17.87	5.63	632.64	2. 0.0

A-3
 Aircraft No. 3
 JET A Fueled
 130 PAS, 1500 n mi range
 Mach 0.85

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 OF POOR QUALITY

JP FUEL REFERENCE PARCEL DESIGN / 130 PASS / 1500 N MI MISS

T/C 10.00 T/F 0.70 AR 11.00 LAM W/S 30.00 T/W 117.0 MISS 0.348

POUNDS 0/G
 88953.
 60353. 55.54
 56128.

POUNDS 0/G
 108659. 100.00
 19704. 18.13
 28600. 26.32
 2875. 2.65
 1351. 1.24

DESIGN GROSS WEIGHT
 FUEL ZERO FUEL WEIGHT
 PAYLOAD OPERATING WEIGHT EMPTY
 OPERATIONAL ITEMS
 STANDARD ITEMS
 EMPTY WEIGHT-MFG.

WING 8455. 7.78
 TAIL 1278. 1.18
 FITY 10760. 9.91
 LANDING GEAR 3892. 3.58
 FLIGHT CONTROLS 1668. 1.53
 NACELLE 2283. 2.10
 PROPULSION SYSTEM 10018. 9.22

ENGINE 7660.
 AIR INTAKE 85.
 EXHAUST 694.
 COOLING 0.
 OIL SYSTEM (LESS OIL) 11.
 ENGINE CONTROLS 43.
 ENGINE STARTING 132.
 TANKS 201.
 INSULATION 0.
 FUEL-PLUMBING 393.

841. 0.77
 1010. 0.94
 2409. 2.31
 924. 0.85
 0440. 4.06
 2058. 1.89
 143. 0.13
 830. 0.76
 0. 0.0
 0. 0.0

INSTRUMENTS
 HYDRAULICS
 ELECTRICAL
 ELECTRONICS
 FURNISHINGS AND EQUIP.
 AIR CONDITIONING
 ANTI-ICING
 AUXILIARY POWER UNIT
 MISCELLANEOUS
 DESIGN RESERVE

130.
 7.
 12.50
 393.2
 428.4

NO. OF PASSENGERS
 NO. OF CREW
 STRUCTURAL T/C
 FUEL VOLUME REQD
 WING FUEL VOLUME AVAILABLE

M I S S I O N S U M M A R Y

JP FUEL REFERENCE BASELINE DESIGN / 130 PASS / 1500 N MI MISS

SEGMENT	INIT ALTITUDE (FT)	INIT MACH NO	INIT WEIGHT (LE)	SEGMT FUEL (LE)	TOTAL FUEL (LR)	SEGMT DIST (IN MI)	TOTAL DIST (IN MI)	SEGMT TIME (MIN)	TOTAL TIME (MIN)	EXTERN STORE TAB ID	ENGINE THRUST TAB ID	EXTERN F TANK TAB ID	AVG L/D RATIO	AVG SFC (PP/T)
TAKEOFF														
POWER 1	0.	0.0	108658.	205.	205.	0.	0.	14.0	14.0	0.	-81101.	0.	0.0	0.465
POWER 2	0.	0.0	108443.	188.	393.	0.	0.	15.0	15.0	0.	81401.	0.	0.0	0.298
CLIMB	0.	0.379	108765.	485.	877.	12.	12.	2.8	17.8	0.	81101.	0.	17.57	0.482
ACCEL	10000.	0.458	107780.	148.	1045.	6.	18.	1.0	18.8	0.	81101.	0.	14.83	0.544
CLIMB	10000.	0.628	107613.	3187.	4212.	254.	272.	31.5	50.1	0.	81101.	0.	14.29	0.619
CRUISE	40000.	0.910	104446.	7646.	11851.	978.	1250.	120.3	170.5	0.	-81101.	0.	16.30	0.618
DESCENT	41000.	0.850	96800.	163.	12021.	67.	1717.	8.5	179.0	0.	81301.	0.	12.58	-4.507
DECEL	10000.	0.828	96637.	43.	12064.	9.	1375.	1.5	180.4	0.	81301.	0.	14.27	131.889
DESCENT	10000.	0.450	96543.	275.	12340.	36.	1761.	8.0	188.5	0.	81301.	0.	16.04	2.372
CRUISE	41000.	0.850	96318.	1045.	13384.	139.	1500.	17.1	205.5	0.	-81101.	0.	16.13	0.618
LOITER	1500.	0.247	95273.	260.	13645.	0.	1500.	6.0	211.5	0.	-81101.	0.	17.54	0.481
RESET	0.	0.0	95013.	0.	13645.	0.	1500.	0.0	211.5	0.	0.	0.	0.0	0.0
RESET	0.	0.0	95012.	0.	13645.	-1500.	0.	-211.5	0.0	0.	0.	0.	0.0	0.0
CRUISE	41000.	0.850	95013.	1560.	17204.	0.	0.	60.0	60.0	0.	-81101.	0.	16.19	0.618
RESET	0.	0.0	91443.	0.	17204.	0.	0.	0.0	60.0	0.	0.	0.	0.0	0.0
CLIMB	0.	0.376	91453.	395.	17599.	10.	10.	2.2	62.2	0.	81101.	0.	16.30	0.482
ACCEL	10000.	0.456	91058.	60.	17659.	2.	12.	0.4	62.6	0.	81101.	0.	14.84	0.516
CLIMB	10000.	0.547	90900.	916.	18575.	48.	60.	7.2	64.8	0.	81101.	0.	13.86	0.568
CRUISE	30000.	0.650	90802.	216.	18891.	40.	100.	6.1	75.6	0.	-81101.	0.	16.59	0.571
DESCENT	30000.	0.700	89766.	167.	19051.	49.	147.	7.5	83.4	0.	81301.	0.	13.66	-16.768
DECEL	10000.	0.547	89603.	23.	19078.	4.	151.	0.6	84.2	0.	81301.	0.	14.81	4.771
DESCENT	10000.	0.456	89575.	194.	19270.	27.	180.	5.9	90.1	0.	81301.	0.	16.24	2.491
CRUISE	30000.	0.645	89386.	144.	19426.	20.	200.	3.0	93.1	0.	-81101.	0.	16.64	0.569
LOITER	1500.	0.247	89332.	247.	19673.	0.	200.	6.0	99.1	0.	-81101.	0.	17.47	0.485

TOTGWT= 108457.7 FUEL A= 19704.4 FUEL P= 19672.0

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C O S T S U M M A R Y

WING	618464.00
TAIL	103664.14
BODY	956650.34
LANDING GEAR	94240.61
FLIGHT CONTROLS	114513.04
WHEELS	250598.38
PROPULSION	
ENGINE	10456.41
AIR INDUCTION	7431.75
FUEL SYSTEM	109440.40
START SYSTEM	2087.33
ENGINE CONTROLS	729.19
EXHAUST/THRUST PIV.	949.64
LUBR SYSTEM	2189.64
TOTAL PROPULSION	202444.56
INSTRUMENTS	129454.75
HYDRAULIC	71042.66
ELECTRICAL	217456.56
ELECTRONIC RACKS	58792.23
PUMPISHING	212434.94
AIR CONDITIONING	170197.63
ANTI ICING	11926.72
APU	90577.38
SYS. INTEGRATION	70039.81

TOTAL EMPTY WFG. COST 3390401.00

SUSTAINING ENGINEERY	227943.75
TECHNICAL DATA	0.00
PROD. TOOLING MAINT.	300161.44
MISC.	82399.63
ENG. CHANGE ORDER	0.00
QUALITY ASSURANCE	313187.81
AIRFRAME WARRANTY	217754.00
AIRFRAME FEE	674625.14
AIRFRAME COST	5210460.00
ENGINE WARRANTY	50506.50
ENGINE FEE	140963.75
ENGINE COST	1799663.00
AVIONICS COST	220000.00
RESEARCH AND DEVELOPMENT	678571.19
TOTAL FLY AWAY COST	7504644.00

PERFECT OPERATING COST-COLLARS/P. MILE	0.00
CREW	0.4231
AIRFRAME LAPOE AND BURDEN MAINT.	2.50
ENGINE LAPOE AND BURDEN MAINT.	0.1266
AIRFRAME MATERIAL MAINT.	0.0844
ENGINE MATERIAL MAINT.	0.0667
FUEL AIR OIL	0.0945
INSURANCE	0.3420
DEPRECIATION (INCLUDING SPARES)	0.1069
TOTAL DOC S/PN. MILE	0.4120

DEVELOPMENT TECHNICAL DATA	5278414.
DESIGN ENGINEERING	117298996.
DEVELOPMENT TOOLING	65516176.
DEVELOPMENT TEST ARTICLE	16988560.
FLIGHT TEST	16059858.
SPECIAL SUPPORT EQUIPMENT	1407576.
ENGINE DEVELOPMENT SPARES	14251270.
AVIONICS DEVELOPMENT	0.
TOTAL R AND D	236789904.

802.	641.	1081.	1221.	1360.	1500.
1.588	1.4087	1.3628	1.3274	1.2993	1.2764
1.8047	7.3797	7.6662	2.9577	3.2392	3.5257.
1.741.	1724.	1015.	2106.	2296.	2489.

LIQUID HYDROGEN---BASIC DESIGN MISSION/200 PASS/ 3600 N MI MISS INT. LM₂

T/C T/R AR LAM W/S T/W
 10.00 0.30 9.50 30.00 112.0 0.335

C O N F I G U R A T I O N G E O M E T R Y

WING--- AREA(SQ.FT) SPAN(FT) TAPER RATIO C/4 SWEEP L.E. SWEEP L.E.R./CHORD
 (DEG) (DEG) (DEC)
 1602.3 123.38 0.300 30.000 3.176 0.0
 CR(FT) CT(FT) MAC(FT) CRE(FT) S WET(SQ.FT) REF L(FT)
 19.98 5.99 14.24 17.76 2638.7 14.24

WING TANK--- CRAP1(FT) CAR2(FT) FTL(FT) FVJMG(CU FT) FVRDX(CU FT)
 17.76 7.01 47.43 0.01 0.00

FUSELAGE--- LENGTH(FT) S WET(SQ FT) AMW(FT) EQUIV D(FT) SPI(SQ FT)
 173.35 9306.3 19.48 20.13 318.20

FW(FT) RW(FT) SPW(SQ FT) FVR(CU FT)
 19.58 20.58 9306.31 5131.63

TAIL--- SMT(SQ.FT) SMTX(SQ.FT) MT REF L(FT) SVT(SQ.FT) SVTX(SQ.FT) VT REF L(FT)
 232.93 157.56 5.68 167.71 167.71 11.21

PROPULSION--- ENG L(FT) ENG D(FT) POD L(FT) POD D(FT) POD S WET (SQ. FT) NO. PODS INLET L(FT)
 6.84 4.62 16.12 5.07 1027.51 4. 0.6

A-4
 Aircraft No. 4
 LH₂ Internal Tank
 200 PAX, 3000 n mi range
 Mach 0.85

LIQUID HYDROGEN---BASIC DESIGN MISSION/200 PASS/ 3000 N MI MISS

T/C 10.00 T/R 0.30 AR 9.50 L4M 30.00 W/S 112.0 T/W 0.335

POUNDS 0/0 POUNDS 0/0
 179460. 100.00
 70924. 11.66
 44000. 24.52
 7777. 4.33
 2225. 1.24
 14889. 8.30
 2014. 1.12
 25033. 13.95
 7676. 4.28
 2461. 1.43
 3465. 1.93
 22405. 12.48

DESIGN GROSS WEIGHT
 FUEL
 PAYLOAD ZERO FUEL WEIGHT
 OPERATING WEIGHT EMPTY
 OPERATIONAL ITEMS
 STANDARD ITEMS
 EMPTY WEIGHT-MFG.
 WING
 TAIL
 BODY
 LANDING GEAR
 FLIGHT CONTROLS
 MACELLES
 PROPULSION SYSTEM
 ENGINE
 AIR INTAKE
 EXHAUST
 CYCLING
 OIL SYSTEM (LESS OIL)
 ENGINE CONTROLS
 ENGINE STARTING
 TANKS
 INSULATION
 FUEL-PLUMBING
 INSTRUMENTS
 HYDRAULICS
 ELECTRICAL
 ELECTRONICS
 FURNISHINGS AND EQUIP.
 AIR CONDITIONING
 ANTI-ICING
 AUXILIARY POWER UNIT
 MISCELLANEOUS
 DESIGN RESERVE

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NO. OF PASSENGERS 200.
 NO. OF CREW 8.
 STRUCTURAL T/C 12.50
 FUEL VOLUME REQD 5000.3
 WING FUEL VOLUME AVAILABLE 0.0

M I S S I O N S U M M A R Y

L I Q U I D H Y D R O G E N --- B A S I C D E S I G N M I S S I O N / 2 0 0 P A S S / 3 0 0 0 N M I M I S S

SECTMT	INIT ALTITUDE (FT)	INIT MACH NO	INIT WEIGHT (LB)	SEGMT FUEL (LB)	TOTAL FUEL (LB)	SEGMT DIST (N MI)	TOTAL DIST (N MI)	SEGMT TIME (MIN)	TOTAL TIME (MIN)	EXTRN STORE TAB ID	ENGINE THRUST TAB ID	EXTRN F TANK TAB ID	AVG L/D RATIO	AVG SFC (FF/FT)
TAREOFF														
POWER 1	0.	0.0	179460.	87.	87.	0.	0.	14.0	14.0	0.	-83101.	0.	0.0	0.124
POWER 2	0.	0.0	179373.	100.	186.	0.	0.	1.0	15.0	0.	83401.	0.	0.0	0.100
CLIMB	0.	0.378	179273.	285.	472.	14.	14.	3.1	18.1	0.	83101.	0.	15.81	0.161
ACCEL	10000.	0.456	178988.	107.	579.	7.	21.	1.2	19.3	0.	83101.	0.	13.35	0.184
CLIMB	10000.	0.638	178881.	2061.	2640.	260.	281.	31.9	51.2	0.	83101.	0.	11.99	0.213
CRUISE	35000.	0.850	178820.	13170.	15010.	2469.	2750.	303.1	354.2	0.	-83101.	0.	13.79	0.211
DESCENT	36000.	0.850	163649.	76.	18886.	51.	2801.	6.4	360.6	0.	83301.	0.	10.95	-1.716
CECEL	10000.	0.638	163573.	22.	15909.	8.	2808.	1.4	362.0	0.	83301.	0.	13.03	47.438
DESCENT	10000.	0.456	163551.	138.	16047.	32.	2840.	7.1	369.1	0.	83301.	0.	15.33	0.847
CRUISE	36000.	0.850	163412.	828.	16875.	160.	3000.	19.7	388.8	0.	-83101.	0.	13.63	0.211
LITTER	1500.	0.247	162585.	154.	17028.	0.	3000.	6.0	394.8	0.	-83101.	0.	15.59	0.147
RESET	0.	0.0	162431.	0.	17028.	0.	3000.	0.0	394.8	0.	0.	0.	0.0	0.0
RESET	0.	0.6	162431.	0.	17028.	-3000.	0.	-394.8	0.0	0.	0.	0.	0.0	0.0
CRUISE	36000.	0.850	162431.	1643.	18472.	0.	0.	40.0	40.0	0.	-83101.	0.	13.84	0.211
RESET	0.	0.0	160788.	0.	18472.	0.	0.	0.0	40.0	0.	0.	0.	0.0	0.0
CLIMB	0.	0.378	160788.	248.	18920.	12.	12.	2.7	42.7	0.	83101.	0.	14.14	0.161
ACCEL	10000.	0.456	160539.	39.	18959.	2.	14.	0.5	43.1	0.	83101.	0.	13.88	0.175
CLIMB	10000.	0.547	160500.	681.	19640.	68.	82.	10.1	53.3	0.	83101.	0.	13.11	0.193
CRUISE	30000.	0.655	159819.	87.	19727.	17.	100.	2.7	57.4	0.	-83101.	0.	15.43	0.190
DESCENT	30000.	0.700	159732.	88.	19815.	47.	146.	7.1	63.0	0.	83401.	0.	12.93	-5.277
DFCEL	10000.	0.547	159644.	12.	19827.	4.	150.	0.7	63.8	0.	83301.	0.	13.93	1.706
DESCENT	10000.	0.456	159612.	100.	19927.	24.	175.	5.4	69.1	0.	83301.	0.	15.16	0.889
CRUISE	30000.	0.655	159532.	125.	20052.	25.	200.	3.8	72.9	0.	-83101.	0.	15.42	0.190
LITTER	1500.	0.246	159407.	890.	20950.	0.	200.	36.0	108.9	0.	-83101.	0.	15.66	0.147

T O T A L W T = 179499.6 FUEL A = 20924.1 FUEL R = 20950.3

C O S T S U M M A R Y

WING 976538.75
 TAIL 156938.44
 BODY 2160814.00
 LANDING GEAR 183804.81
 FLIGHT CONTROLS 173523.75
 MACELLES 382040.50
 PROPULSION
 ENGINE 15594.38
 AIP INDUCTION 112060.44
 FUEL SYSTEM 713234.81
 START SYSTEM 3120.31
 ENGINE CONTROLS 1239.55
 EXH/AIRUST. REV. 1389.69
 LUBE SYSTEM 2137.05
 TOTAL PROPULSION 848776.06
 INSTRUMENTS 152981.56
 HYDRAULICS 102395.00
 ELECTRICAL 329401.31
 ELECTRONIC RACKS 98400.44
 PURRISHING 316431.00
 AIR CONDITIONING 252521.31
 ANTI ICING 15153.31
 APU 89491.00
 SYS. INTEGRATION 141984.81

4383688.00

TOTAL EMPTY MFG. COST

SUSTAINING ENGINEER 443379.63
 TECHNICAL DATA 0.0
 PROD. TOOLING MAINT. 583052.13
 MISC. 162203.38
 ENG. CHANGE ORDER 0.0
 QUALITY ASSURANCE 609190.19
 AIRFRAME WARRANTY
 AIRFRAME PEE
 AIRFRAME COST 107985.88
 ENGINE WARRANTY 272124.19
 ENGINE FEE
 ENGINE COST
 AVIONICS COST
 RESEARCH AND DEVELOPMENT
 TOTAL FLY AWAY COST -

R AND D
 DEVELOPMENT TECHNICAL DATA 8206321.
 DESIGN ENGINEERING 182362704.
 DEVELOPMENT TOOLING 88812128.
 DEVELOPMENT TEST ARTICLE 32720032.
 FLIGHT TEST 21019664.
 SPECIAL SUPPORT EQUIPMENT 2188352.
 DEVELOPMENT SPARES 26927328.
 ENGINE DEVELOPMENT 0.
 AVIONICS DEVELOPMENT 0.
 TOTAL R AND D 362235392.

13954926.00

DIRECT OPERATING COST-DOLLARS/M. MILE 0/0
 CREW 14.76
 AIRFRAME LABR AND BURDEN MAINT. 6.36
 ENGINE LABR AND BURDEN MAINT. 3.31
 AIRFRAME MATERIAL MAINT. 3.67
 ENGINE MATERIAL MAINT. 3.76
 FUEL AND OIL 34.53
 INSURANCE 6.93
 DEPRECIATION (INCLUDING SPARES) 0.7139
 TOTAL DOC \$/M. MILE 2.6793 100.00

PERCENTAGE
 RANGE
 M. MI
 DOC
 C/ASM
 TA-HR
 S/TRP
 1.6195 1.5055 1.4018 1.3738 1.3533 1.3376
 1589. 1942. 2295. 2647. 3000.
 3.6932 4.4147 5.1363 6.5794
 4583. 5444. 7145. 8026.

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T A K E O F F P E R F O R M A N C E

POWER	EMCOP	OVERSPO	WEIGHT	FLAP	DCRSTA	CMRT	DCLSP0	CLST	CLST1	DCDSPA	CDST
CLRN	CDRNI	DCDSTA	CPRN	CLRT	CL2	TM2	LD2	XTD	FIELD	GRAD	
CLTD	TMTO	LOTO	CLCLMB	TMCLMB	XG1	XROT	XOB				
VSTALL	V1	VROT	VTD	V2	YG						
89401.	4.00	1.00	179460.	18.00							
0.28184	0.11295	0.01063	0.12357	1.96987	0.16235	0.17298	-0.57424	-0.29240	0.12411	0.07308	0.197719
2.06046	0.25809	12.12550	1.88959	0.25489	12.08684	0.25489	11.12763	4638.78	5334.59	0.1672	
112.06	130.21	130.21	140.07	146.88	3158.51	686.27	796.01				
89401.	3.00	1.00	179460.	18.00							
0.28184	0.11295	0.01063	0.12357	1.91480	0.15815	0.16878	-0.57424	-0.29240	0.12411	0.07308	0.197719
1.92117	0.19357	12.11145	1.78633	0.19157	11.94464	0.19157	10.88595	5382.75	5382.75	0.0937	
112.06	129.86	134.27	140.07	145.67	3137.52	694.54	1121.53				

B R A K I N G R U M C D E F F I E M T S---L A N D I N G
 CLRN DCLSP0 CLGRD CDGRD1 DCDSPO DCDSPA CDGRD
 0.75479 -0.76500 -0.01021 0.19626 0.06850 0.01960 0.28436

L A N D I N G P E R F O R M A N C E

LANDING WT	XOB, FT	XROLL, FT	XBRAKE, FT	TOT DIST, FT	FIELD L	VAPPR, KTS
162631.13	1139.08	227.82	2100.50	3467.40	5779.00	134.98
182831.13	1166.62	241.44	2349.13	3756.98	6261.63	143.05
170486.56	1150.05	233.40	2200.61	3584.06	5973.44	138.29

LIQUID HYDROGEN--BASIC DESIGN MISSION/200 PASS/ 3000 N M) MISS - EXTERNAL TANK

T/C T/R AR LAM W/S T/M
 10.00 0.40 9.50 30.00 110.6 0.0-30

C O N F I G U R A T I O N G E O M E T R Y

WING--	AREA(SQ.FT)	SPAN(FT)	TAPER RATIO	C/4 SWEEP (DEG)	L.E. SWEEP (DEG)	L.E.R/CHORD
	1674.7	133.45	0.400	30.000	31.901	0.0
	CR (FT)	CT (FT)	MAC (FT)	CRE (FT)	S MET(SO.FT)	REF L (FT)
	20.07	8.03	14.91	18.90	3223.2	14.91
WING TANK--	CDAR(1FT)	CBAR(2FT)	FIL (FT)	FWMING(CU FT)	FVBOX(CU FT)	
	18.30	8.90	52.10	0.01	0.00	
FUSELAGE--	LENG IN (FT)	S MET(SO FT)	BHW(FT)	EQUIV D(FT)	SPI(SO FT)	
	144.70	7580.0	19.58	20.13	318.20	
	BW(FT)	HW(FT)	SRW(SG FT)	FVW(CU FT)		
	19.58	20.58	7580.00	0.0		
TAIL--	SMT(SO.FT)	SMTX(SO.FT)	MT REF L(FT)	SVT(SO.FT)	SVTX(SO.FT)	VT REF L(FT)
	349.22	251.34	8.09	264.14	264.64	14.10
PROPULSION--	ENG L(FT)	ENG D(FT)	POD L(FT)	POD D(FT)	POD S MET (SO. FT)	MO. PODS INLET L(FT)
	8.10	5.63	19.25	6.13	1483.21	4. 0.0
FUEL PODS--	VOL (CU FT)	LENGTH(FT)	SPI(SO FT)	S MET(SO FT)	MO PODS	
	6076.41	63.71	181.15	4008.8	2.	

A-5
 Aircraft No. 5
 LH₂ External Tank
 200 PAX, 3000 n mi range

L IQUID HYDROGEN---BASIC DESIGN MISSION/20G PASS/ 300G M M3 MISS

T/C T/M AR LAM W/S T/M
 10.00 0.40 9.50 20.00 110.6 0.430

	POUNDS	O/U	POUNDS	O/U
DESIGN GROSS WEIGHT	207346.	100.00		
FUEL	27229.	13.13		
PAYLOAD	44000.	21.22		
ZERO FUEL WEIGHT			180117.	
OPERATING WEIGHT EMPTY	7805.	3.76	136117.	65.65
OPERATIONAL ITEMS	2541.	1.23		
EMPTY WEIGHT-MFG.			125772.	
WING	19603.	9.45		
TAIL	3312.	1.60		
BODY	24329.	11.73		
LANDING GEAR	8203.	3.94		
FLIGHT CONTROLS	2898.	1.40		
RACELLES	5283.	2.55		
PROPULSION SYSTEM	35540.	17.14		
ENGINE	17727.			
AIR INTAKE	2048.			
EXHAUST	1606.			
COOLING	0.			
OIL SYSTEM (LESS OIL)	11.			
ENGINE CONTROLS	49.			
ENGINE STARTING	304.			
TANKS	7523.			
INSULATION	4973.			
FUEL-PLUMBING	1247.			
INSTRUMENTS			1642.	0.70
HYDRAULICS			1690.	0.82
ELECTRICAL			3608.	1.84
ELECTRONICS			1554.	0.75
FURNISHINGS AND EQUIP.			14353.	6.92
AIR CONDITIONING			3122.	1.51
ANTI-ICING			205.	0.10
AUXILIARY POWER UNIT			830.	0.40
MISCELLANEOUS			0.	0.0
DESIGN RESERVE			0.	0.0
NO. OF PASSENGERS			200.	
NO. OF CREW			8.	
STRUCTURAL T/C			12.50	
FUEL VOLUME REQD			6365.6	
WING FUEL VOLUME AVAILABLE			0.0	

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MISSION SUMMARY

LIQUID HYDROGEN--EASIL DESIGN MISSION/200 PASS/3000 RPM MISS

SEGMENT	INIT ALTITUDE (FT)	INIT WGT (LE)	INIT WGT (LE)	SEGMENT FUEL (LE)	TOTAL FUEL (LE)	SEGMENT FUEL (LE)	TOTAL FUEL (LE)	SEGMENT WGT (LE)	TOTAL WGT (LE)	SEGMENT TIME (MIN)	TOTAL TIME (MIN)	EXTERN STCPE TAB ID	EXTERN F TANK TAB ID	AVG L/D RATIO	AVG SFC (FF/FT)
TAREOFF POWER 1	0.	0.0	267346.	124.	124.	0.	0.	14.0	14.0	0.	0.	-F3101.	0.	0.0	0.124
POWER 2	0.	0.0	217217.	148.	272.	0.	0.	1.0	15.0	0.	0.	F3401.	0.	0.0	0.100
CLIMB	0.	0.378	17064.	317.	544.	10.	16.	2.3	17.3	0.	0.	F3101.	0.	13.37	0.161
ACCEL	10000.	0.456	26752.	118.	712.	5.	16.	0.9	16.2	0.	0.	F3101.	0.	10.94	0.104
CLIMB	10000.	0.434	26634.	2316.	3026.	208.	224.	25.6	43.8	0.	0.	F3101.	0.	10.35	0.212
CRUISE	36000.	0.850	264316.	17360.	20406.	2526.	2750.	310.4	344.7	0.	0.	-F3101.	0.	12.30	0.211
DESCENT	39000.	0.850	186937.	97.	20506.	46.	2746.	5.6	340.5	0.	0.	F3301.	0.	9.13	-1.635
WCELL	10000.	0.636	16840.	27.	20533.	6.	2802.	1.1	361.6	0.	0.	F3301.	0.	10.60	44.520
DESCENT	10000.	0.454	16613.	173.	20766.	27.	2824.	6.1	367.6	0.	0.	F3301.	0.	12.78	0.847
CRUISE	39000.	0.850	186640.	1136.	21842.	171.	3060.	21.0	368.7	0.	0.	-F3101.	0.	12.11	0.211
LOITER	1500.	0.241	18504.	195.	22037.	0.	3000.	4.0	344.7	0.	0.	-F3101.	0.	14.53	0.153
RESET	0.	0.0	185304.	0.	22037.	0.	3000.	0.0	344.7	0.	0.	0.	0.	0.0	0.0
RESET	0.	0.0	185304.	0.	22037.	-3000.	0.	-344.7	0.0	0.	0.	0.	0.	0.0	0.0
CRUISE	39000.	0.850	185309.	3108.	25235.	0.	0.	60.0	40.0	0.	0.	-F3101.	0.	12.13	0.211
RESET	0.	0.0	182111.	0.	25235.	0.	0.	0.0	40.0	0.	0.	0.	0.	0.0	0.0
CLIMB	0.	0.378	162111.	272.	25506.	9.	9.	2.0	62.0	0.	0.	F3101.	0.	12.48	0.161
ACCEL	10000.	0.456	181034.	43.	25549.	2.	11.	0.3	62.3	0.	0.	F3101.	0.	11.29	0.175
CLIMB	10000.	0.567	181796.	714.	26263.	48.	58.	7.1	69.4	0.	0.	F3101.	0.	10.56	0.192
CRUISE	36000.	0.605	181082.	277.	26540.	41.	100.	6.9	76.3	0.	0.	-F3101.	0.	13.79	0.184
DESCENT	30000.	0.700	180805.	105.	26645.	37.	137.	5.7	62.0	0.	0.	F3301.	0.	10.41	-5.261
DFCFL	10000.	0.547	180701.	15.	26654.	3.	140.	0.6	82.6	0.	0.	F3301.	0.	11.34	1.700
DESCENT	10000.	0.456	180686.	124.	26783.	20.	161.	4.5	87.1	0.	0.	F3301.	0.	12.55	0.809
CRUISE	36000.	0.605	180562.	260.	27043.	34.	260.	6.4	93.5	0.	0.	-F3101.	0.	13.77	0.184
LOITER	1500.	0.239	180303.	190.	27233.	0.	200.	6.0	99.5	0.	0.	-F3101.	0.	14.46	0.153

TURBINE 2073-0-1 ULL 4- 27229-1 FUEL 6- 27233-0

C O S T S U M M A R Y

WING	1274539.00				
TAIL	254304.88				
BODY	2062172.00				
LANDING GEAR	145907.88				
FLIGHT CONTROLS	145537.56				
WHEELS	577160.38				
PROPULSION					
ENGINE	23516.38				
AIR INDUCTION	169304.88				
FUEL SYSTEM	1199342.00				
START SYSTEM	4735.46				
ENGINE CONTROLS	1881.14				
ENGINE/THRUST REV.	2095.85				
LUBE SYSTEM	2121.73				
TOTAL PROPULSION	1462795.60				
INSTRUMENTS	156409.69				
HYDRAULICS	144608.19				
ELECTRICAL	342269.56				
ELECTRONIC RACKS	95511.06				
PUMP/ENGINE	314515.38				
AIR CONDITIONING	250876.50				
ANTI ICEING	14457.43				
APU	29171.75				
SYS. INTEGRATION	164037.13				
TOTAL EMPTY WFG. COST	7514423.00				
SUSTAINING ENGINEER	530796.81				
TECHNICAL DATA	0.0				
PROD. TOOLING MAINT.	4987.494				
RISC.	194183.56				
ENG. CHANGE ORDER	0.0				
QUALITY ASSURANCE	729299.63				
AIRFRAME WARRANTY					
AIRFRAME P/E					
AIRFRAME COST					
ENGINE WARRANTY					
ENGINE P/E					
ENGINE COST					
AERONAUTICS COST					
RESEARCH AND DEVELOPMENT					
TOTAL FLY AWAY COST	11673679.00				
	3558861.00				
	500000.00				
	1341131.00				
	17073666.00				
DIRECT OPERATING COST-DOLLARS/M. MILE	0/0				
CREW	0.3447				
AIRFRAME LABOR AND BURDEN MAINT.	12.14				
ENGINE LABOR AND BURDEN MAINT.	0.1913				
AIRFRAME LABOR AND BURDEN MAINT.	0.1047				
ENGINE MATERIAL MAINT.	0.1162				
FUEL AND OIL	0.1409				
INSURANCE	1.1952				
DEPRECIATION (INCLUDING SPARE)	0.2249				
TOTAL DOC 8/M. MILE	0.8793				
	27.05				
	6.98				
	34.76				
	C/ASM				
	4.33				
	DOC				
	3.57				
	M. MI				
	RANGE				
	5.88				
	C-1913				
	0.1047				
	3.26				
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	0.1162				
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JET A

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C O N F I G U R A T I O N C O M P L E T E

WING--	AREA(SQ.FT)	SPAN(FT)	TAPER RATIO	C/S	SWEEP (D/C)	L.F. SWEEP (D/C)	L.F. SWEEP (D/C)	L.F. SWEEP (D/C)
	1663.4	127.56	0.500	30.000	32.314	0.0	0.0	0.0
	LE(FT)	CT(FT)	MAC(FT)	CR(FT)	S MET(SQ.FT)	REF L(FT)	REF L(FT)	REF L(FT)
	20.10	0.03	14.33	17.52	2782.1	14.33	14.33	14.33
WING TANK--	CFAP(FT)	CHARZ(FT)	HTL(FT)	FVWIK(CU FT)	FVRC(CU FT)			
	17.93	7.05	49.27	797.48	277.04			
FUSELAGE--	LENGTH(FT)	S MET(SQ.FT)	BW(FT)	LGUV(CFT)	SPI(SQ.FT)			
	144.70	7560.0	19.58	20.13	318.20			
	BW(FT)	BW(FT)	SRW(SQ.FT)	FVP(CU FT)				
	19.58	20.58	7580.00	60990.00				
TAIL--	SMT(SQ.FT)	SMTX(SQ.FT)	HT REF L(FT)	SVT(SQ.FT)	SVTX(SQ.FT)	VT REF L(FT)		
	296.30	203.11	7.36	221.56	221.56	12.91		
PROPULSION--	ENG L(FT)	ENG D(FT)	POD L(FT)	POD D(FT)	POD S MET (SQ.FT)	NU. PODS	INLET L(FT)	
	6.89	4.65	16.25	5.07	1034.05	4.	0.0	

A-6
 Aircraft No. 6
 JET A Fueled
 200 PAX, 3000 n mi range
 Mach 0.85

ORIGINAL PAGE IS
 OF POOR QUALITY

OPERATIONAL WEIGHTS - MAXIMUM DESIGN / 30000 LBS / 30000 LBS

T/C 10.00 W/A 0.50 AR 5.75 L/G 140.5 T/W 1.00

PCUNLS 0.70
155187.
111707. 51.52
102006.

PCUNLS 0.70

214924. 100.00
81157. 21.18
44606. 20.20
7778. 4.55
2003. 0.82
17112. 7.91
2012. 1.30
24434. 11.25
8542. 4.0
3012. 1.30
2620. 1.63
1521. 0.71

DESIGN GROSS WEIGHT
FUEL
ZERO FUEL WEIGHT
PAYLOAD
OPERATING WEIGHT EMPTY
STANDARD ITEMS
EMPTY WEIGHT-MFG.
WING
TAIL
BODY
LANDING GEAR
FLIGHT CONTROLS
FACILITIES
PROPULSION SYSTEM
ENGINE
AIR INTAKE
EXHAUST
COOLING
OIL SYSTEM (LESS OIL)
ENGINE CONTROLS
ENGINE STARTING
TANKS
INSULATION
FUEL-PLUMBING
INSTRUMENTS
HYDRAULICS
ELECTRICAL
ELECTRONICS
FURNISHINGS AND EQUIP.
AIR CONDITIONING
ANTI-ICING
AUXILIARY POWER UNIT
MISCELLANEOUS
DESIGN RESERVE

11846.
1369.
1073.
0.
11.
66.
204.
320.
0.
632.

1052. 0.48
1755. 0.81
3779. 1.74
1542. 0.71
14353. 6.62
3431. 1.58
211. 0.10
890. 0.38
C. 0.0
0. 0.0

NO. OF PASSENGERS
NO. OF CREW
STRUCTURAL T/C
FUEL VOLUME REQD
WING FUEL VOLUME AVAILABLE

200.
8.
12.50
1219.4
1074.9

AIRCRAFT HYDROGEN--BASIC DESIGN MISSION/400 PASSES/10000 N MI MISS WT. LBS
 T/C 1/A AS LAM W/S 1/A
 10.00 0.30 10.00 20.00 117.0 0.20

C O N F I D E N T I A L P L E C I T Y

WING-- AREA(SQ.FT) SPAN(FT) TAPER RATIO L/W SWEEP L-t. SWEET L-E.R/CHORD (LEG) (DEG)
 5027.2 224.06 0.300 30.700 32.260 0.0
 CRIFT) CT(FT) MAC(FT) CRF(FT) S WPT(SQ.FT) REF LIFT) REF LIFT)
 34.47 10.34 24.57 31.81 0166.4 24.57

WING TANK-- LEAR(FT) CRACK(FT) FTL(FT) FWMING(CU FT) FVX(CU FT)
 31.81 12.09 01.56 0.05 0.06

FUSELAGE-- LENGTH(FT) S WPT(SQ FT) BW(FT) EQUIV D(FT) SPI(SQ FT)
 253.87 18129.6 24.66 26.5 552.00

BW(FT) SW(SQ FT) FV(CU FT)
 24.66 26.75 18124.55 36006.96

TAIL-- SHY(SQ.FT) SMTR(SQ.FT) MT REF LIFT) SVT(SQ.FT) SVTX(SQ.FT) VT REF LIFT)
 699.64 522.64 12.71 737.97 737.97 23.03

PROPULSION-- ENG LIFT) ENG D(FT) POD LIFT) POD D(FT) POD S WPT (SQ. FT) NC. PODS INLET LIFT)
 10.54 7.45 24.80 6.13 2534.04 4. 0.0

A-7
 Aircraft No. 7
 LH2 Internal Tank
 400 PAX, 5000 n mi radius
 Mach 0.85

LIQUID HYDROGEN---MAGIC DESIGN MISSION/400 PASS/REGUL N MI MISS

T/C 10.00 T/R 0.250 A/R 16.00 LAM M/S 117.0 T/W 0.285

	POUNDS	G/G	POUNDS	G/G
DESIGN GROSS WEIGHT	587366	166.00		
FUEL	150040	25.68		
PAYLOAD	46538			
ZERO FUEL WEIGHT	430826	129.32		
OPERATING WEIGHT EMPTY	348114	59.34		
STANDARD ITEMS	325627			
EMPTY WEIGHT-MFG.				
WING	71300	12.15		
TAIL	6186	1.05		
BODY	64247	10.94		
LANDING GEAR	33666	5.70		
FLIGHT CONTROLS	7058	1.20		
WHEELS	9252	1.58		
PROPULSION SYSTEM	84217	14.34		
ENGINE	31644			
AIR INTAKE	3507			
EXHAUST	2813			
COOLING	0			
OIL SYSTEM (LESS OIL)	11			
ENGINE CONTROLS	174			
ENGINE STARTING	536			
TANKS	30962			
INSULATION	11920			
FUEL-PLUMBING	3171			
INSTRUMENTS	1324	0.23		
HYDRAULICS	4274	0.73		
ELECTRICAL	5463	1.02		
ELECTRONICS	2381	0.41		
FURNISHINGS AND EQUIP.	28400	4.84		
AIR CONDITIONING	5926	1.01		
ANTI-ICING	443	0.08		
AUXILIARY POWER UNIT	1116	0.19		
MISCELLANEOUS	0	0.0		
DESIGN RESERVE	0	0.0		
NO. OF PASSENGERS	400			
NO. OF CREW	11			
STRUCTURAL T/C	12.50			
FUEL VOLUME REQD	34049.9			
WING FUEL VOLUME AVAILABLE	0.0			

ORIGINAL PAGE IS
OF POOR QUALITY

M I S S I O N S U M M A R Y

LIQUID FUEL/GEN-8500 GECION MISSION/400 PASS/10000 K.M. WISE

STAGANT	INIT ALTITUDE (FT)	INIT MACH	INIT WEIGHT (LBS)	FUEL (LBS)	TOTAL FUEL (LBS)	SEGMENT FUEL (LBS)	TOTAL DIST (NM)	SEGMENT DIST (NM)	TOTAL TIME (MIN)	SEGMENT TIME (MIN)	EXTERN SYCAL TAB ID	ENGINE THRUST TAB ID	EXTERN F TANK TAB ID	AVL L/D RATIO	AVG SFC (FF/T)
TAKOFF POWER 1	0	0.0	517300	429	429	0	0	0	24.1	24.1	0	-83101	0	0.0	0.117
POWER 2	0	0.0	516937	493	922	0	0	0	30.0	30.0	0	83301	0	0.0	0.094
LLIMB	0	0.374	516444	894	1816	17	17	17	33.6	33.6	0	83101	0	19.30	0.152
ACCEL	10000	0.456	515500	324	2140	9	26	26	35.4	35.4	0	83101	0	16.90	0.173
CLIMB	10000	0.638	514226	6799	8939	365	39	39	44.7	44.7	0	83101	0	15.33	0.201
CRUISE	34000	0.851	514427	57887	66826	4358	475	475	614.5	614.5	0	-83101	0	16.85	0.199
DESCENT	35000	0.850	516540	749	67574	114	446	464	633.7	633.7	0	83301	0	16.68	-5.977
CRUISE	36000	0.850	519790	1724	69299	136	500	500	650.4	650.4	0	-83101	0	16.66	0.199
LOITER	1500	0.277	517066	402	69701	0	500	500	649.4	649.4	0	-83101	0	18.64	0.145
RESET	0	0.0	517669	0	69701	0	500	500	646.4	646.4	0	0	0	0.0	0.0
CLIMB	0	0.378	517665	756	70456	15	5015	5015	659.7	659.7	0	83101	0	18.62	0.152
ACCEL	10000	0.456	516909	274	70730	8	5022	5022	661.0	661.0	0	83101	0	15.78	0.173
CLIMB	10000	0.638	516636	4737	75467	244	5272	5272	699.7	699.7	0	83101	0	14.53	0.200
CRUISE	37000	0.850	511898	53276	128743	4478	9750	9750	551.1	551.1	0	-83101	0	16.64	0.199
DESCENT	35000	0.850	458622	708	129451	107	9857	9857	18.1	18.1	0	83301	0	15.69	-5.807
CRUISE	39000	0.850	457914	1610	131061	143	10000	10000	17.6	17.6	0	-83101	0	16.61	0.199
LOITER	1500	0.259	456303	356	131418	0	10000	10000	6.0	6.0	0	-83101	0	18.53	0.145
RESET	0	0.0	455947	0	131418	0	10000	10000	0.0	0.0	0	0	0	0.0	0.0
RESET	0	0.0	455947	0	131418	-10000	0	0	0.0	0.0	0	0	0	0.0	0.0
CRUISE	39000	0.850	455947	10415	141833	0	0	0	115.0	115.0	0	-83101	0	16.52	0.199
RESET	0	0.0	455522	0	141833	0	0	0	0.0	0.0	0	0	0	0.0	0.0
CLIMB	0	0.378	455532	2311	144143	78	78	78	12.7	12.7	0	83101	0	15.70	0.174
CRUISE	30000	0.650	443222	1389	145532	122	200	200	146.3	146.3	0	-83101	0	17.85	0.181
DESCENT	30000	0.700	441833	611	146143	90	290	290	16.1	16.1	0	83301	0	16.15	-2.140
CRUISE	36000	0.650	441222	1254	147397	110	400	400	16.8	16.8	0	-83101	0	17.82	0.181
LOITER	1500	0.254	439068	3433	150829	0	400	400	60.0	60.0	0	-83101	0	18.50	0.145

JP FUEL REFERENCE CASSETTE DESIGN / 4000 PAX / HIGH P.M. JET
 T/C T/R AR LAM W/S T/M W/RS W/RS JET
 10.00 6.20 11.00 30.00 129.2 0.700

C O N F I G U R A T I O N G E O M E T R Y

WING--	AREA(SQ.FT)	SPAN(FT)	TAPER RATIO	C/A	SHEEP (NIC)	L.F. SHEEP (FT)	L.F. R/CM/POD
	7125.0	279.46	0.306	30.000	32.050	0.0	
	CP(FT)	CT(FT)	MC(FT)	CKE(FT)	S MET(ISO.FT)	REF L(FT)	
	30.14	11.74	27.01	37.24	13482.9	27.01	
WING TANK--	CFAR(FT)	CFAR2(FT)	FTL(FT)	FWING(CU FT)	FVOLUME(FT)		
	37.24	13.73	120.04	R178.20	1104.03		
FUSELAGE--	LENGTH(FT)	S MET(ISO.FT)	MM(FT)	EQUIV D(FT)	SP(ISO.FT)		
	225.00	14435.0	19.58	19.56	301.10		
	HM(FT)	BM(FT)	SM(ISO.FT)	FV(FCU FT)			
	19.58	19.58	14435.00	99009.00			
TAIL--	SM(ISO.FT)	SM(ISO.FT)	MT REF L(FT)	SVT(ISO.FT)	SVT(ISO.FT)	VT REF L(FT)	
	757.05	411.04	15.01	767.67	767.67	23.92	
PROPULSION--	ENG LIFT	ENG D(FT)	POD LIFT	POD D(FT)	POD S MFT (ISO.FT)	NO. PODS	MLIFT L(FT)
	11.70	8.37	27.59	9.12	3103.09	4.	0.0

A-8
 Aircraft No. 8
 JET A Fueled
 400 PAX, 5000 n mi radius
 Mach 0.85

ORIGINAL PAGE IS
 OF POOR QUALITY

JP FUEL REFERENCE MAXIMUM DESIGN / 400 P.S.I. / 10,000 + WT MISS
 T/C 7/4 AR 1AM M/S 7/4
 10.00 0.30 11.00 24.00 134.5 6.200

	PIKUPS	WT	POUNDS	0/20
DESIGN GROSS WEIGHT	90257.	100.00		
FUEL	23986.	57.70		44821.
PAYLOAD	8800.	6.37		34021.
OPERATING WEIGHT EMPTY	15499.	1.56		351146.
OPERATIONAL ITEMS	13875.	1.40		
STANDARD ITEMS				
EMPTY WEIGHT-MFG.				
WING	104437.	10.77		
TAIL	7013.	0.71		
BODY	54378.	5.44		
LANDING GEAR	53142.	5.35		
FLIGHT CONTROLS	11054.	1.11		
WACELLS	1177.	1.19		
PROPULSION SYSTEM	53007.	5.34		
ENGINE	39788.			
AIR INTAKE	4547.			
EXHAUST	3605.			
COOLING	0.			
OIL SYSTEM (LFS OIL)	11.			
ENGINE CONTROLS	223.			
ENGINE STARTING	686.			
TANKS	2222.			
INSULATION	0.			
FUEL-PLUMBING	1879.			
INSTRUMENTS	1532.	0.15		
HYDRAULICS	7029.	0.71		
ELECTRICAL	4085.	0.41		
ELECTRONICS	2420.	0.24		
PUMPS/TANKS AND EQUIP.	28400.	2.86		
AIR CONDITIONING	6982.	0.70		
ANTI-ICING	696.	0.70		
AUXILIARY POWER UNIT	1116.	0.11		
MISCELLANEOUS	0.	0.00		
DESIGN RESERVE	0.	0.00		
NO. OF PASSENGERS	400.			
NO. OF CREW	11.			
STRUCTURAL T/C	12.50			
FUEL VOLUME REQD	10454.8			
WING FUEL VOLUME AVAILABLE	4372.8			

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2. Anon., Standard Method of Estimating Comparative Direct Operating Costs of Turbine Powered Transport Airplanes, Air Transport Association of America, December 1967.
3. Anon., Subsonic Transport Category Large Airplanes and Subsonic Turbojet Powered Airplanes - Proposed Noise Reduction Stages and Acoustical Change Requirements, Notice No. 75-37, Federal Register, Vol. 40, No. 214, Nov. 5, 1975.

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