



AAFE RADSCAT DATA REDUCTION PROGRAMS
USER'S GUIDE

CRES Technical Report 186-9

(NASA-CR-144992)	AAFE RADSCAT DATA	N76-22643
	REDUCTION PROGRAMS USER'S GUIDE (Kansas	
	Univ. Center for Research, Inc.) 146 p HC	
\$6.00	CSSL 04B	Unclas
		63/43 27389

John P. Classen



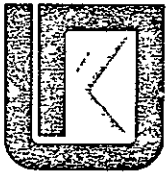
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Langley Research Center
Hampton, Virginia
CONTRACT NAS 1-10048



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2385 Irving Hill Rd.— Campus West Lawrence, Kansas 66044

1. Report No. <i>NASA CR-144992</i>	2. Government Accession No.	3. Recipient's Catalog No.	
4. Title and Subtitle AAFE RADSCAT Data Reduction Programs User's Guide		5. Report Date	
		6. Performing Organization Code	
7. Author(s) John P. Claassen		8. Performing Organization Report No. Technical Report 186-9	
		10. Work Unit No.	
9. Performing Organization Name and Address University of Kansas Center for Research, Inc. Space Technology Center, 2291 Irving Hill Road - Campus West Lawrence, Kansas 66044		11. Contract or Grant No. NAS 1-10048	
		13. Type of Report and Period Covered	
12. Sponsoring Agency Name and Address National Aeronautics and Space Administration Langley Research Center Hampton, Virginia 23365		14. Sponsoring Agency Code	
		15. Supplementary Notes	
16. Abstract <p>The theory, design and operation of the computer programs which automate the reduction of joint radiometer and scatterometer observations conducted by the AAFE RADSCAT instrument is presented. The programs reduce scatterometer measurements to the normalized scattering coefficient; whereas the radiometer measurements are converted into antenna temperatures. The programs are both investigator and user oriented. Supplementary parameters are provided to aid in the interpretation of the observations. A hierarchy of diagnostics is available to evaluate the operation of the instrument, the conduct of the experiments and the quality of the records.</p> <p>General descriptions of the programs and their data products are also presented. This document therefore serves as a user's guide to the programs and is therefore intended to serve both the experimenter and the program operator.</p>			
17. Key Words (Suggested by Author(s)) Data Reduction Radiometer Measurements Scatterometer Measurements Remote Sensing Earth Resources		18. Distribution Statement Unclassified-Unlimited	
19. Security Classif. (of this report) UNCLASSIFIED	20. Security Classif. (of this page) UNCLASSIFIED	21. No. of Pages 144	22. Price*



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FOREWORD

The value of microwave scatterometers and radiometers as remote sea wind sensors has been independently demonstrated by a number of investigators. However, near-simultaneous observations by a composite radiometer and scatterometer (RADSCAT) instrument have been proposed as a method of making improved wind estimates. The improvement is derived from the complementary as well as supplementary features of the sensors. To demonstrate this potential a joint effort among New York University, General Electric Space Division, the University of Kansas and NASA Langley Research Center was undertaken through the Advanced Application Flight Experiment program of NASA. This document is submitted in support of these efforts.

Specifically, this document was prepared by the Remote Sensing Laboratory of the University of Kansas Center For Research, Inc. under NASA Contract NAS 1-10048. The principal investigator under the contract is Dr. R. K. Moore and project engineer is Dr. A. K. Fung. Several individuals rendered valuable assistance in the development of the computer programs. The control and integration of the routines were partially achieved by Glen E. Elliott of the University of Kansas. John L. Mitchell of LTV operated the programs repeatedly on the CDC-6600 while they were under final scrutiny by the author.

ABSTRACT

The theory, design and operation of the computer programs which automate the reduction of joint radiometer and scatterometer observations conducted by the AAFE RADSCAT instrument is presented. The programs reduce scatterometer measurements to the normalized scattering coefficient; whereas the radiometer measurements are converted into antenna temperatures. The programs are both investigator and user oriented. Supplementary parameters are provided to aid in the interpretation of the observations. A hierarchy of diagnostics is available to evaluate the operation of the instrument, the conduct of the experiments and the quality of the records.

General description of the programs and their data products are also presented. This document therefore serves as a user's guide to the programs and is therefore intended to serve both the experimenter and the program operator.

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I. INTRODUCTION

The AAFE RADSCAT* Data Reduction Package, as prepared by the University of Kansas, is a family of computer programs** which together form a basis for automated reduction and presentation of scatterometer and radiometer measurements taken by the RADSCAT instrument. The primary member in the family validates the raw RADSCAT data records and uses instrument and aircraft parameters to yield emission and scattering characteristics of the scene represented by the data. The scatterometer data is reduced to the normalized scattering coefficient whereas the radiometer data is reduced to the antenna temperature. Other programs in the family are employed to maintain a file of instrument characteristics, list the output (reduced data), and prepare duplicate output tapes for use on other computing machines. Two engineering routines are also provided to compute certain antenna parameters essential to the reduction of the microwave data; these routines are not employed regularly. The programs were written in FORTRAN IV, developed on a HW 635 system and then modified and demonstrated on a CDC-6600.

The program outputs provide a comprehensive basis from which to interpret the results of RADSCAT experiments. The basic output parameters have been augmented with others to reconstruct the influence of the aircraft attitude on the experiment, to validate the measurements, and to reflect the status of the RADSCAT instrument. Full evaluation of the data is accomplished by examining contents of an activity report as well as the output records. A fuller data base from which to analyze RADSCAT data is only provided when these outputs are augmented with sea/ground truth and certain aircraft parameters available from other sources. The programs are therefore largely experimenter oriented.

Attempts have been made to generalize the reduction algorithms so as to easily adapt the programs for changes in the character or operation of the instrument. In doing so the user is expected to provide many more of the calibration and

* A composite radiometer and scatterometer sensor.

** The family of programs does not include a merge and edit routine which prepares the raw input data. This routine was developed by the Flight Instrumentation Division of NASA Langley Research Center.

data parameters than would otherwise be required. For this reason a historical file is maintained on the instrument parameters. It is also provided to trace the development, modifications and aging of the instrument.

No attempts have been made to develop efficient coding; rather extensive efforts have been made to develop programs which will, to some degree, document themselves. Self documentation is provided by a liberal insertion of comment cards. This approach had been instituted with the full realization that the programs are likely to undergo changes as experience or changes in the instrument dictate them. It is hopeful that this approach together with this document will ease the insertion of program modifications. However, the authors can assume no responsibility for changes made without their knowledge. It is strongly recommended that changes to the reduction algorithms be made only with the approval of an engineer who is thoroughly familiar with the operation of the instrument, the theory behind the algorithms and the needs of the investigators.

Some strides have been made to design production type programs. External directives give the users the ability to select the files to be processed or the service function to be executed. Unrecognized directives will halt the execution of the program. Data entries are also validated and when too many bad files are encountered the job is aborted. Activity reports and termination statements are provided so that the user can trace the progress of the job.

The details on the use, theory and design of these programs are presented in the remainder of this document. To place these programs in context with RADSCAT experiments the technical background is briefly described in Section II. The experimenter and programmer will find Section III helpful in understanding the general features and data products of the programs. He may wish to refer to Section IV and the Appendices for more specific information. The program operator will find Section IV essential to the operation of the programs. Again he may wish to consult the appendices for specific help. The cognizant engineer will want to become familiar with all aspects of this document to develop a thorough understanding of the program content. To a large extent this document assumes some knowledge of the operation of the RADSCAT instrument*. The programmer and cognizant

* A description of the instrument may be found in "Field Service Procedure Handbook," vol. 1, prepared by General Electric Space Division, Philadelphia, Pennsylvania under NASA Contract NAS 1-10161.

engineer will also want to consult the document which describes the merge and edit routine which prepares the raw data records. This document is in preparation at NASA Langley Research Center. Those wishing to learn the details on the theory and design of the various routines in the family of programs will find the appendices helpful.

II. TECHNICAL BACKGROUND

A. Introduction

This section is primarily written for the investigator or programmer not familiar with scatterometric or radiometric measurements. The motivation for joint measurements is presented and the elementary theory behind the measurements is discussed. The instrument and its relation to the C-130 aircraft is also briefly described. It is hoped that this section will place the AAFE RADSCAT Data Reduction Programs in context of experiments.

B. Motivation for Joint Measurements

In recent years a strong interest has developed in interpreting the microwave signatures of natural surfaces. In these efforts a number of potential earth resources and scientific applications have been demonstrated by measuring the emission or scattering properties of various scenes. The scatterometer is employed to measure the scattering characteristic whereas the radiometer is used to measure the emission properties. To date the investigations have been largely conducted with one instrument or the other. However, several investigators have proposed that joint scattering and emission measurements would form a stronger-interpretational basis, because each sensor measures a different aspect of the bi-static scattering characteristic of the surface. From an entirely different viewpoint the sensors are complementary in nature. It is known that the radiometer is very sensitive to clouds and rain whereas the scatterometer is relatively insensitive to clouds and rain. Over the ocean this property has potential in correcting the scatterometer measurements for small attenuations caused by clouds.

C. Description of the RADSCAT Sensor

The AAFE RADSCAT instrument is a composite sensor consisting of a pencil-beam microwave scatterometer and radiometer. It was designed to conduct measurements from an aircraft and is capable of operating at either of two frequencies, 9.3 GHz or 13.9 GHz. In three of its four modes of operation it makes scatterometer and radiometer measurements on a near-simultaneous basis. In the fourth mode it makes radiometer measurements only. Observations can be conducted at any one of six adjustable angles covering the sector between nadir and 60 degrees.

The AAFE RADSCAT instrument was primarily designed to perform experiments over the ocean to verify the remote anemometric capability of the composite sensor. Although primarily designed for oceanographic work, the extension to observations of agrarian or urban scenes is straightforward. The instrument is capable of conducting experiments at one of four altitudes, viz, 2000, 5000, 10,000 and 20,000 feet*. The wide range of altitudes is provided to study atmospheric effects such as humidity, temperature, clouds and rains. To avoid difficulties introduced by operating from behind a radome, the RADSCAT instrument mounts on the tail gate of the NASA/MSC C-130 aircraft. The Litton Navigator LTN-51 aboard the C-130 aircraft is extremely useful to the interpretation and reduction of the RADSCAT observations. It provides aircraft attitude and location information from which the point of observation on the surface may be established. The attitude parameters are especially useful when measurements are performed from a roll maneuver, since these parameters enable one to compute the incident angle. The radar altimeter information provided by the aircraft is essential to the inversion of the scatterometer measurements.

D. Estimating the Scattering and Emission Properties from Measurements

The scatterometer is a radar which is capable of accurately measuring the backscatter properties of a rough surface. The backscatter ability of the surface is denoted by the normalized scattering coefficient σ^0 which is given in terms of the scattering cross-section per unit area. In general it is dependent upon the point of observation, the incident angle, frequency, polarization, etc. It is well known that the radar return is predicted by (see Figure 1).

$$P_r = \frac{\lambda^2}{(4\pi)^3} P_t \iint_{4\pi} \frac{g^2(\theta, \phi) \sigma^0(\theta', \phi')}{R^4} dA \quad (1)$$

where σ^0 = normalized scattering coefficient
 P_r = received power
 P_t = transmitted power
 λ = wavelength
 g = antenna gain function
 R = radar range to elemental area dA

*The radiometer by itself can operate at any altitude.

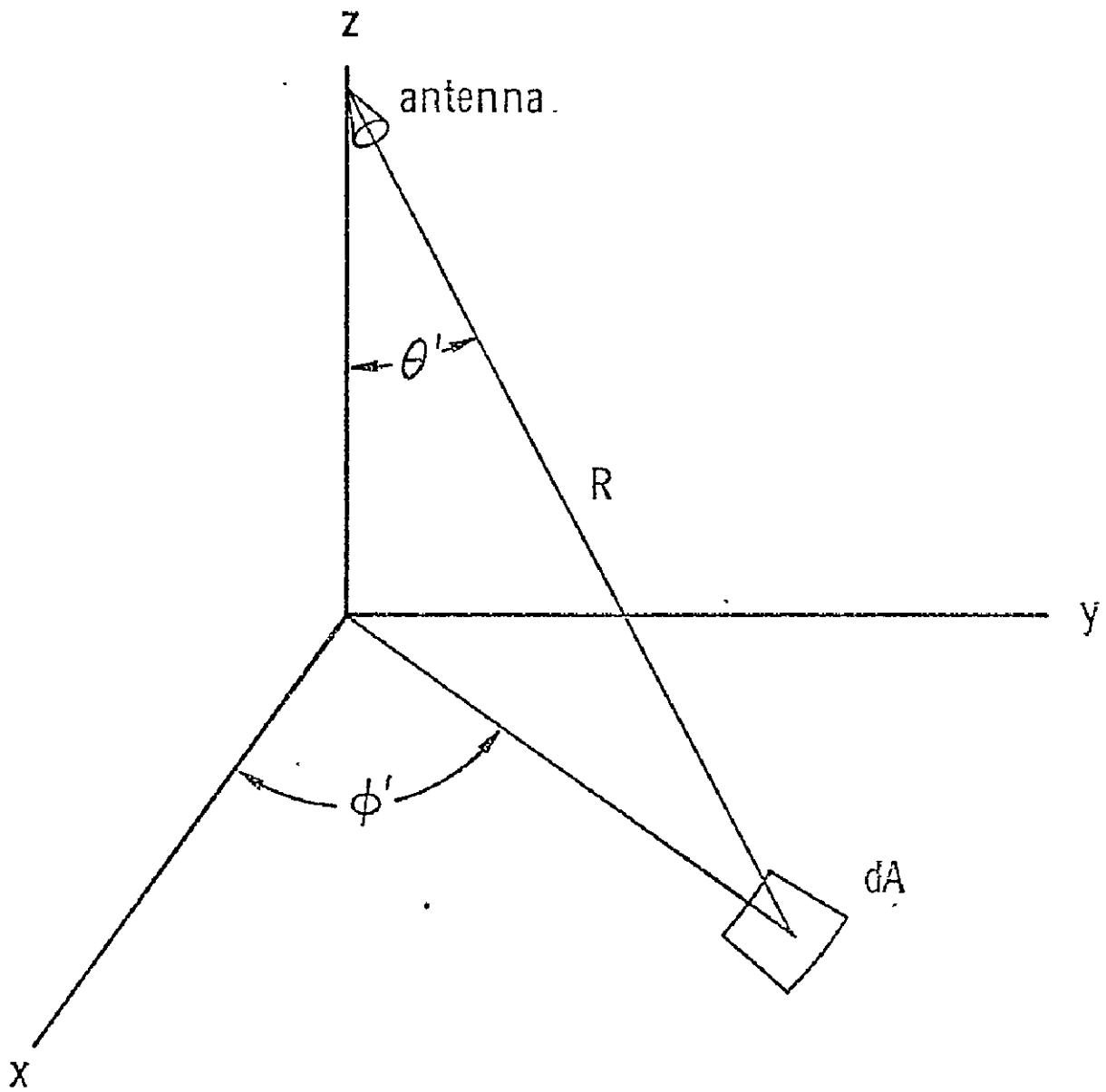


FIGURE 1. RADAR GEOMETRY

For narrow (or equivalently narrow) beam scatterometers the above integral expression may be inverted rather simply for σ^0 . As a consequence the problem of accurately determining σ^0 reduces to the problem of accurately measuring the transmitted and receiver powers, the pattern function, look angle, and radar range. The area of illumination may be shown to be related to the pattern function, look angle, and radar range. The scatterometer provides outputs which are measures of P_r and P_t . The power transfer function of scatterometer completes the association between the outputs to yield P_r and P_t^* . A member of the family of programs actually employs the scatterometer transfer function and an algebraic approximation of equation (1) to estimate σ^0 .

The radiometer, on the other hand, is a very sensitive receiver capable of measuring very low level emissions which emanate naturally from objects. In the microwave region the natural emission is governed by the Jeans-Rayleigh law which states that the power emitted is proportional to the physical temperature T of the body. In actuality, however, different objects at different temperatures emit different powers depending until their relative ability to absorb energy. Better absorbers emit more efficiently than poor ones. The relative ability to emit is described in terms of a parameter called emissivity ϵ . The emitted power per unit bandwidth in direction θ is given by^{**}

$$P(\theta) = \frac{4\pi k \epsilon(\theta) T}{\lambda^2} \quad (2)$$

where k is Boltzmann's constant.

We may now suppose that the surface emits in accord with this relation. Then a radiometer whose antenna gain function is given by $g(\theta, \phi)$ will measure (ignoring atmospheric contributions) a total power per unit bandwidth given by^{***}

$$P_a = \frac{1}{\Omega} \int \int_{4\pi} g(\theta, \phi) k T_B(\theta) d\Omega \quad (3)$$

* Actually only the ratio P_r/P_t is needed.

** For one polarization.

*** This relation is only representative of the nature of the problem. See Claassen, J. P. and A. K. Fung, "An Efficient Method for Inverting Antenna Temperatures for the Apparent Temperature Distribution" University of Kansas Center For Research, Inc., TR 186-8, January 1973, for a precise relationship.

where

$$\Omega = \iint_{4\pi} g(\theta, \phi) d\Omega \quad (4)$$

and

$$T_B = \epsilon(\theta) T \quad (5)$$

The antenna power may be related to antenna temperature by $P_a = kT_a$. For narrow beam, efficient antennas the antenna temperature is an approximate measure of the brightness temperature T_B in the look direction. The radiometer therefore must accurately measure the antenna power. The RADSCAT data reduction programs use the calibration data and radiometer transfer function to estimate T_a for each polarization.

III. GENERAL DESCRIPTION

A. Introduction

This section is primarily written to familiarize the investigator or programmer with the family of RADSCAT data reduction programs. The functions of the particular programs and the relationships between the programs are presented. Input and output data products are described to various degrees.

B. Summary of Programs

The AAFE RADSCAT Data Reduction Package consists of a family of six programs:

1. Conversion Program (CONVERT)
2. Output Program (OUTPUT)
3. Program for the Storage and Retrieval of Instrument Characteristics (ICHAR)
4. Output Translation and Duplication Program (TDUPE)
5. Equivalent Beamwidth Program (WIDTH)
6. Antenna Gain and Efficiency Program (GAIN)

The actual reduction of data is accomplished in CONVERT. The input data for CONVERT is prepared by an edit and merge routine developed by NASA Langley Research Center. The merged tape consists of RADSCAT and aircraft data. To assist in the computations, program ICHAR prepares a historical file of instrument characteristics. CONVERT selects a particular set of characteristics from the file and applies them to the input data. The computed results are stored on an output tape. Program OUTPUT will list the contents of the output tape. To prepare duplicate output tapes for use on other computing machines program TDUPE may be employed.

WIDTH and GAIN are special routines which compute several antenna parameters. The parameters are employed as elements of the instrument characteristics. Both programs require antenna pattern information to compute the parameters. Their use will seldom be required unless the antenna pattern changes.

Of the six programs the initial four programs are production types and the last two are engineering application programs.

C. Conversion Program

The reduction of RADSCAT data is performed entirely in CONVERT. By means of external directives, physical files of a specified type are processed with a designated set of instrument characteristics withdrawn from a separate file source. External directives permit the user to initiate processing of input files by type or sequentially regardless of type. The files are organized by flight runs and are labeled in accord with a procedure instituted by the Flight Operations Division of NASA/MSC.

Directive options are given by MISFLT, FLTLIN, SPECIF, or ALL. When the first directive is appended with mission and flight numbers, all files from that mission and flight are processed in the order that they appear on the tape. Mission, flight and line numbers must appear with the second directive option. Files of the designated line type will thus be processed. Consecutive directives which exhaust the line types will order the output files by line type. This feature is helpful to the interpreter who often associates an experiment condition with a line type. The third directive is employed when a specific file designated by mission, flight, line and run is to be processed. This directive is appropriate for a quick or selective look at the experiment results. The last directive (ALL) will initiate processing of all files regardless of type. Combinations of directives may be employed; however, indiscriminant use of the processing types is cautioned against since duplicate processing of files may occur. For each directive the file search is effectively conducted from the beginning of the tape.

Each of the above directives must include a designator which selects a set of instrument characteristics from a historical file of characteristics or which permits them to be read from cards. It is likely that the most current characteristics will be chosen; however, any set on the file may be selected. Alternatively, characteristics may be entered from the card reader. However, operation under this latter option is restricted to one data file per directive. Entry through the card reader is mainly reserved for testing a set of instrument characteristics before storage on the historical file. Also as a part of the same directive the number of files to be processed of the indicated type and the line density of the activity report must be designated on the control card. The latter parameter can be used to limit the number of data records on which reports are given.

During processing CONVERT generates a conversion report. The report routinely issues statements on the calibration parameters and critical receiver temperatures as they are computed from the input file. It will also routinely state that a record had been reduced. The reports are appended with record numbers. Other special statements are generated whenever critical situations are encountered in the records. When these special situations occur, the record is normally processed regardless; however, that record is flagged by an interpretational code which becomes a part of the output record. In some cases, such as invalid data, the record is bypassed and an appropriate error message is generated. When an excessive number of bad records is encountered, the file is bypassed and an appropriate message printed. These messages are primarily intended to reflect the status of the processing, the condition of the instrument, the conduct of the experiment, and the quality of the data. A sample listing of the conversion report is illustrated in Figure 2.

As processing progresses output records are accumulated in blocks (arrays) and the blocks are written to the output tape. A description of the contents of the output tape appears in the following subsection.

D. Output Program

Program OUTPUT will list the processed records produced in the conversion program. External directives similar to those in CONVERT permit listing files of designated types or all files regardless of type. Again general directives are given by MISFLT, FLTLIN, SPECIF or ALL. The appropriate mission, flight, line and run designators must accompany the directives.

A sample listing produced by OUTPUT is shown in Figure 3. A double page of output consists of the file label, column headings, 80 records and a key. The set of instrument characteristics which produced the results is identified by set number and date in the last entry of the file label. Each measurement record occupies one line on the listing. A record number is appended to each line and should agree with the number assigned in the conversion report. The time of measurement in mean Greenwich time is presented in the second column. It is to be read in hours, minutes, seconds and 1/10th seconds. The measurement can therefore be associated with data from other sources. The mode from which the instrument conducted the measurement is reflected in column 3. The incident and cross-tracks angles appear in the next two columns. They were computed from aircraft attitude parameters and the RADSCAT view angle with respect to the aircraft platform. The cross-track angle is that angle

CONVERSION REPORT

MISSION-207 FLIGHT-12 DATE- 7 25 1972 FLT LINE- 2 RUA- J FREQUENCY- 13.9 FEED- WG SW IPAN- 1 2 1 73

RECORD NO.	MESSAGE	PARAMETERS
	CALIBRATION DATA	CHAN 1= .270 CHAN 2= .410 CHAN 3= 1.190 CHAN 4= 1.285 RCAL= 2.406 RBASE= .160 NCAL= 6 HNCAL= 6 LOCATION NO. 1 TEMPERATURE =337.8 KELVIN WARM= 311.8 HCT= 415.0 OMT= 312.1 Sh= 311.3 AIR= 288.0 GDE= 312.7 DEFOL= .021
1	* RECVR TEMP NOT WITHIN OPERATING RANGE *	ANTENNA TEMP= 266.6 SCATTERING COEF=7.720366E+00 CHANNEL= 2 DOP BAND= 7 LOCATION NO. 1 TEMPERATURE =337.8 KELVIN
1	* CRITICAL TEMPERATURES *	WARM= 311.8 HCT= 415.0 OMT= 312.1 Sh= 311.3 AIR= 288.0 GDE= 312.7
1	* EXCESSIVE DEPOLARIZATION *	ANTENNA TEMP= 248.6 SCATTERING COEF=6.311449E+00 CHANNEL= 2 DOP BAND= 7 DEFOL= .022
1	** COMPLETED RECCRC COMPUTATIONS **	LOCATION NO. 1 TEMPERATURE =337.8 KELVIN
2	* RECVR TEMP NOT WITHIN OPERATING RANGE *	WARM= 311.8 HCT= 415.0 OMT= 312.1 Sh= 311.3 AIR= 288.0 GDE= 312.7
2	* CRITICAL TEMPERATURES *	ANTENNA TEMP= 248.6 SCATTERING COEF=6.311449E+00 CHANNEL= 2 DOP BAND= 7 DEFOL= .022
2	** COMPLETED RECCRC COMPUTATIONS **	LOCATION NO. 1 TEMPERATURE =337.8 KELVIN
3	* RECVR TEMP NOT WITHIN OPERATING RANGE *	WARM= 311.8 HCT= 415.0 OMT= 312.1 Sh= 311.3 AIR= 288.0 GDE= 312.7
3	* CRITICAL TEMPERATURES *	ANTENNA TEMP= 268.4 SCATTERING COEF=5.924877E+00 CHANNEL= 2 DOP BAND= 7 DEFOL= .020
3	** COMPLETED RECCRC COMPUTATIONS **	LOCATION NO. 1 TEMPERATURE =337.8 KELVIN
4	* RECVR TEMP NOT WITHIN OPERATING RANGE *	WARM= 311.8 HCT= 415.0 OMT= 312.1 Sh= 311.3 AIR= 288.0 GDE= 312.7
4	* CRITICAL TEMPERATURES *	ANTENNA TEMP= 248.6 SCATTERING COEF=7.028195E+00 CHANNEL= 2 DOP BAND= 7 DEFOL= .022
4	** COMPLETED RECCRC COMPUTATIONS **	LOCATION NO. 1 TEMPERATURE =337.8 KELVIN
5	* RECVR TEMP NOT WITHIN OPERATING RANGE *	WARM= 311.8 HCT= 415.0 OMT= 312.1 Sh= 311.3 AIR= 288.0 GDE= 312.7
5	* CRITICAL TEMPERATURES *	ANTENNA TEMP= 249.4 SCATTERING COEF=6.206822E+00 CHANNEL= 2 DOP BAND= 7 DEFOL= .022
5	** COMPLETED RECCRC COMPUTATIONS **	LOCATION NO. 1 TEMPERATURE =337.8 KELVIN
6	* RECVR TEMP NOT WITHIN OPERATING RANGE *	WARM= 311.8 HCT= 415.0 OMT= 312.1 Sh= 311.3 AIR= 287.6 GDE= 312.7
6	* CRITICAL TEMPERATURES *	ANTENNA TEMP= 249.1 SCATTERING COEF=5.944944E+00 CHANNEL= 2 DOP BAND= 7 DEFOL= .020
6	** COMPLETED RECCRC COMPUTATIONS **	LOCATION NO. 1 TEMPERATURE =337.8 KELVIN
7	* RECVR TEMP NOT WITHIN OPERATING RANGE *	WARM= 311.8 HCT= 415.0 OMT= 312.2 Sh= 311.3 AIR= 287.9 GDE= 312.7
7	* CRITICAL TEMPERATURES *	ANTENNA TEMP= 248.2 SCATTERING COEF=7.501535E+00 CHANNEL= 2 DOP BAND= 7 DEFOL= .020
7	** COMPLETED RECCRC COMPUTATIONS **	LOCATION NO. 1 TEMPERATURE =337.8 KELVIN
8	* RECVR TEMP NOT WITHIN OPERATING RANGE *	WARM= 311.8 HCT= 415.0 OMT= 312.2 Sh= 311.3 AIR= 288.0 GDE= 312.7
8	* CRITICAL TEMPERATURES *	ANTENNA TEMP= 269.0 SCATTERING COEF=7.141555E+00 CHANNEL= 2 DOP BAND= 7 DEFOL= .020
8	** COMPLETED RECCRC COMPUTATIONS **	LOCATION NO. 1 TEMPERATURE =337.8 KELVIN
9	* RECVR TEMP NOT WITHIN OPERATING RANGE *	WARM= 311.8 HCT= 415.0 OMT= 312.1 Sh= 311.3 AIR= 288.0 GDE= 312.7
9	* CRITICAL TEMPERATURES *	ANTENNA TEMP= 249.2 SCATTERING COEF=8.071541E+00 CHANNEL= 2 DOP BAND= 7 DEFOL= .020
9	** COMPLETED RECCRC COMPUTATIONS **	LOCATION NO. 1 TEMPERATURE =337.8 KELVIN
10	* RECVR TEMP NOT WITHIN OPERATING RANGE *	WARM= 311.8 HCT= 415.0 OMT= 312.1 Sh= 311.3 AIR= 288.0 GDE= 312.7
10	* CRITICAL TEMPERATURES *	ANTENNA TEMP= 268.6 SCATTERING COEF=7.145143E+00 CHANNEL= 2 DOP BAND= 7 DEFOL= .020
10	** COMPLETED RECCRC COMPUTATIONS **	LOCATION NO. 1 TEMPERATURE =338.0 KELVIN
11	* RECVR TEMP NOT WITHIN OPERATING RANGE *	WARM= 311.8 HCT= 415.0 OMT= 312.1 Sh= 311.3 AIR= 288.1 GDE= 312.7
11	* CRITICAL TEMPERATURES *	ANTENNA TEMP= 243.5 SCATTERING COEF=5.522865E+00 CHANNEL= 2 DOP BAND= 7 DEFOL= .020
11	** COMPLETED RECCRC COMPUTATIONS **	LOCATION NO. 1 TEMPERATURE =338.0 KELVIN

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FIGURE 2. SAMPLE OF THE CONVERSION REPORT

MICROWAVE DATA

MISSION-201 FLIGHT- 12 GATE- 7 25 1972 FLT LINE- 2 RUN- 3 FREQUENCY- 13.4 FEED- NO SW IPAR- 1 2 1 73

RECORD NO.	TIME	MODE	INCL ANGLE (DEG)	CROSS ANGLE (CEG)	XMIT PGL	REC POL	S INT TIME (SEC)	SCAT	SCAT CB	RAD (DEG R)	DEPOL FACTOR	S/R CCDE	ALTITUDE (FEET)	FLT DIRECT (CEG)
1	151746.7	F.A.	13.7	-11.4	H	H	.555	7.7204E+00	8.9	246.8	.021	110000	9966	2.5
2	151748.2	F.A.	13.8	-10.3	H	H	.555	6.3114E+00	8.0	248.6	0.000	100000	9959	2.7
3	151750.4	F.A.	13.8	-9.0	H	H	.555	5.9249E+00	7.7	248.4	0.000	100000	9957	2.6
4	151751.1	F.A.	13.7	-9.9	H	H	.555	7.0282E+00	8.5	249.8	0.000	100000	9956	2.3
5	151751.9	F.A.	13.6	-10.7	H	H	.555	6.2068E+00	7.9	249.4	.021	110000	9956	2.0
6	151752.6	F.A.	13.6	-10.0	H	H	.555	5.9449E+00	7.7	249.1	-.022	110000	9959	1.9
7	151753.3	F.A.	13.5	-10.5	H	H	.555	7.5075E+00	8.8	248.2	-.020	110000	9958	1.8
8	151754.1	F.A.	13.5	-9.7	H	H	.555	7.1420E+00	8.5	249.0	0.000	100000	9955	1.8
9	151754.8	F.A.	13.3	-6.9	H	H	.555	8.0719E+00	9.1	249.2	0.000	100000	9953	1.8
10	151756.3	F.A.	13.4	-8.6	H	H	.555	7.1891E+00	8.6	2 8.6	0.000	100000	9956	1.6
11	151757.8	F.A.	13.5	-9.5	V	V	.555	5.5229E+00	7.4	243.5	0.000	100000	9956	1.3
12	151758.5	F.A.	13.6	-9.3	V	V	.555	5.5486E+00	7.4	244.0	0.000	100000	9954	1.2
13	151759.2	F.A.	13.5	-8.9	V	V	.555	5.3070E+00	7.3	242.9	0.000	100000	9955	1.2
14	151800.0	F.A.	13.4	-8.2	V	V	.555	5.6805E+00	7.5	244.0	0.000	100000	9955	1.1
15	151800.7	F.A.	13.4	-7.4	V	V	.555	5.7777E+00	7.6	243.4	0.000	100000	9955	1.1
16	151802.2	F.A.	13.3	-7.2	V	V	.555	5.7537E+00	7.6	243.2	0.000	100000	9953	.9
17	151804.4	F.A.	13.3	-7.8	V	V	.555	7.1411E+00	8.5	249.4	0.000	100000	9951	.6
18	151805.1	F.A.	13.4	-7.6	V	V	.555	5.3751E+00	7.3	242.7	0.000	100000	9952	.6
19	151809.9	F.A.	13.3	-7.1	V	V	.555	7.2444E+00	8.6	243.7	0.000	100000	9956	.6
20	151806.6	F.A.	13.2	-6.7	V	V	.555	7.6415E+00	8.8	244.4	0.000	100000	9956	.6
21	151815.4	F.A.	43.0	-2.5	V	V	.555	3.2273E-01	-4.9	250.1	0.000	100000	9951	103.4
22	151816.7	F.A.	43.0	-2.8	V	V	.802	2.4405E-01	-6.1	250.1	0.000	100000	9953	359.8
23	151818.6	F.A.	42.9	-2.6	V	V	.802	2.4335E-01	-6.1	250.4	0.000	100000	9952	359.9
24	151820.5	F.A.	42.7	-2.2	V	V	.802	2.4358E-01	-6.1	249.7	0.000	100000	9952	359.8
25	151821.4	F.A.	42.8	-2.2	V	V	.802	2.4347E-01	-6.1	249.3	0.000	100000	9953	359.7
26	151822.4	F.A.	42.8	-2.4	V	V	.802	2.0886E-01	-6.8	250.5	0.000	100000	9952	359.7
27	151823.3	F.A.	42.8	-2.5	V	V	.802	2.0911E-01	-6.8	250.5	0.000	100000	9953	359.6
28	151824.3	F.A.	42.7	-2.5	V	V	.802	2.0958E-01	-6.8	250.1	0.000	100000	9957	359.6
29	151825.2	F.A.	42.8	-2.2	V	V	.802	2.0990E-01	-6.8	250.1	0.000	100000	9957	359.7
30	151827.1	F.A.	42.7	-1.9	V	V	.802	2.0854E-01	-6.8	249.3	0.000	100000	9961	359.6
31	151828.0	F.A.	42.8	-1.8	V	V	.802	2.0997E-01	-6.8	249.5	0.000	100000	9960	359.6
32	151829.9	F.A.	43.0	-1.9	V	V	.802	2.4451E-01	-6.1	249.3	0.000	100000	9963	359.4
33	151830.9	F.A.	43.0	-2.0	V	V	.802	2.4449E-01	-6.1	249.3	0.000	100000	9963	359.4
34	151831.8	F.A.	43.0	-1.9	V	V	.802	2.4402E-01	-6.1	250.1	0.000	100000	9961	359.4
35	151832.8	F.A.	42.9	-1.8	V	V	.802	2.4336E-01	-6.1	250.5	0.000	100000	9962	359.5
36	151833.7	F.A.	42.9	-1.6	V	V	.802	2.4434E-01	-6.1	249.7	0.000	100000	9958	359.5
37	151835.6	F.A.	42.8	-1.2	H	H	.802	7.2189E-04	-30.5	247.0	0.000	100000	9959	359.4
38	151836.5	F.A.	42.8	-1.2	H	H	.802	7.5444E-04	-31.0	246.0	0.000	100000	9957	359.3
39	151837.5	F.A.	42.8	-1.3	H	H	.802	7.4506E-04	-31.3	246.8	0.000	100000	9960	359.3
40	151838.4	F.A.	42.8	-1.3	H	H	.802	6.5443E-04	-31.8	246.2	0.000	100000	9960	359.3
41	151839.4	F.A.	42.8	-1.4	H	H	.802	7.7676E-04	-31.1	246.4	0.000	100000	9960	359.4
42	151840.3	F.A.	42.7	-1.3	H	H	.802	7.2853E-04	-31.4	245.0	0.000	100000	9960	359.5
43	151842.2	F.A.	42.9	-1.0	H	H	.802	8.5995E-04	-30.7	246.0	0.000	100000	9960	359.4
44	151844.1	F.A.	42.9	-1.1	H	H	.802	6.8271E-04	-31.7	247.0	0.000	100000	9960	359.4
45	151846.0	F.A.	42.9	-1.3	H	H	.802	6.8509E-04	-31.6	245.2	0.000	100000	9963	359.4
46	151847.9	F.A.	42.9	-1.1	H	H	.802	7.5142E-04	-31.2	247.2	0.000	100000	9966	359.6
47	151848.8	F.A.	43.0	-1.0	H	H	.802	7.4572E-04	-31.3	247.8	0.000	100000	9964	359.5
48	151857.8	F.A.	13.3	-2.2	H	H	.555	5.6747E+00	7.5	247.6	0.000	100000	9960	359.7
49	151858.5	F.A.	13.1	-2.3	H	H	.555	5.5253E+00	7.4	248.3	0.000	100000	9960	359.7
50	151859.3	F.A.	13.1	-2.1	H	H	.555	7.4050E+00	8.7	249.1	0.000	100000	9962	359.8
51	151900.7	F.A.	13.2	-1.5	H	H	.555	6.7056E+00	8.3	248.9	0.000	100000	9959	359.8
52	151901.5	F.A.	13.3	-1.1	H	H	.555	5.6748E+00	7.5	245.7	0.000	100000	9961	359.9
53	151902.2	F.A.	13.3	-1.0	H	H	.555	6.4946E+00	8.1	248.5	0.000	100000	9961	359.9
54	151903.7	F.A.	13.3	-1.4	H	H	.555	5.5778E+00	7.5	248.2	0.000	100000	9960	359.8
55	151904.4	F.A.	13.2	-1.4	H	H	.555	6.0552E+00	7.8	249.5	0.000	100000	9961	359.8
56	151905.2	F.A.	13.3	-1.5	H	H	.555	6.0606E+00	7.8	249.3	0.000	100000	9961	359.9
57	151906.6	F.A.	13.2	-1.5	H	H	.555	5.4558E+00	7.4	247.8	0.000	100000	9959	360.0
58	151907.4	F.A.	13.3	-1.4	H	H	.555	5.8421E+00	7.7	248.4	0.000	100000	9960	360.0
59	151908.1	F.A.	13.2	-1.3	H	H	.555	5.4304E+00	7.3	248.4	0.000	100000	9960	213.1
60	151909.6	F.A.	13.3	-1.1	H	H	.555	6.9278E+00	8.4	248.5	0.000	100000	9960	.1
61	151910.3	F.A.	13.2	-1.2	H	H	.555	5.7202E+00	7.6	249.3	0.000	100000	9959	.1
62	151911.8	F.A.	13.2	-1.2	H	H	.555	6.7520E+00	8.3	247.6	0.000	100000	9957	.1
63	151912.5	F.A.	13.2	-1.3	V	V	.555	5.9210E+00	7.7	244.2	0.000	100000	9958	.2
64	151913.3	F.A.	13.2	-1.3	V	V	.555	4.7140E+00	6.7	244.4	0.000	100000	9956	.3
65	151914.0	F.A.	13.3	-1.2	V	V	.555	4.8754E+00	6.9	244.6	0.000	100000	9954	.3
66	151915.5	F.A.	13.3	-1.1	V	V	.555	4.5261E+00	6.9	243.4	0.000	100000	9954	.5
67	151916.2	F.A.	13.2	-1.2	V	V	.555	5.9873E+00	7.8	244.4	0.000	100000	9954	.5
68	151917.7	F.A.	13.3	-1.3	V	V	.555	4.4515E+00	6.5	245.0	0.000	100000	9951	.4
69	151918.4	F.A.	13.2	-1.3	V	V	.555	5.3231E+00	7.3	243.4	0.000	100000	9950	.4
70	151919.2	F.A.	13.2	-1.3	V	V	.555	5.7957E+00	7.6	243.6	0.000	100000	9951	.5
71	151920.6	F.A.	13.3	-1.0	V	V	.555	5.5595E+00	7.5	244.2	0.000	100000	9950	.6
72	151921.4	F.A.	13.3	-.6	V	V	.555	5.2076E+00	7.2	244.0	0.000	100000	9951	.8
73	151922.1	F.A.	13.2	-.4	V	V	.555	5.0653E+00	7.0	245.0	0.000	100000	9952	.9
74	151923.6	F.A.	13.2	-.4	V	V	.555	4.7133E+00	6.7	244.0	0.000	100000	9955	.9
75	151924.3	F.A.	13.3	-.7	V	V	.555	4.5975E+00	7.0	243.6	0.000	100000	9954	.9
76	151925.1	F.A.	13.2	-1.1	V	V	.555	6.0345E+00	7.8	244.2	0.000	100000	9954	.9
77	151925.8	F.A.	13.2	-1.4	V	V	.555	5.9154E+00	7.7	243.6	0.000	100000	9953	.9
78	151926.5	F.A.	13.2	-1.4	V	V	.555	5.1604E+00	7.1	244.2	0.000	100000	9954	1.1
79	151927.3	F.A.	13.1	-1.5	V	V	.555	5.3982E+00	7.3	243.3	0.000	100000	9958	1.1
80	151928.0	F.A.	13.1	-1.4	V	V	.555	4.6694E+00	6.7	244.2	0.000	100000	9961	1.2

KEY TO CODES-

0 REC FLAG
 1 FCSSIBLY OUTSIDE RANGE GATE
 10 OUTSIDE DYNAMIC RANGE
 100 EXCESSIVE COUPLER
 1000 POLAR REVERSAL
 10000 EXCESSIVE DEPOL
 100000 REC TEMP ANOMAL
 1000000 WARM LOAD TEMP ESTIMATED
 COMBINATIONS OF FLAGS CAN OCCUR.

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FIGURE 3. SAMPLE LISTING OF OUTPUT RECORDS

between the "negative" flight direction and the azimuthal look direction. The positive cross-track angle is defined to the right of the aircraft when looking aft. It is induced by aircraft roll and drift angle. The incident and cross-track angles are precisely computed for any aircraft attitude. The angles enable the investigator to locate the illumination area. The scatterometer transmit polarization and the scatterometer and radiometer receive polarization are presented in the next two columns, respectively. The scatterometer integration time is indicated in the following column. The radiometer integration time is not listed since it is constant (128 milliseconds) regardless of mode or angle. The normalized scattering coefficient (m^2/m^2) is shown in decimal as well as dB units. The radiometer antenna temperature is shown in column 11.

A depolarization factor appears in column 12. The depolarization factor when expressed as a percentage indicates the percent power transmitted at the opposite surface polarization. Whenever DEPOL exceeds 50 per cent a polarization reversal flag is generated under the S/R validation code (column 13) and the complementary depolarization factor (1-DEPOL) is posted in column 12. If a reversal is indicated and the (complementary) depolarization factor is small, the polarization designators in columns 6 and 7 may indeed be regarded in the opposite state. Polarization reversals will frequently occur when observations are conducted from an aircraft roll condition. When DEPOL exceeds 2 per cent a flag in the S/R code is raised.

Other flag conditions can occur under the S/R code. The flags are used as a quick indicator of an abnormal condition. The interpretations of flags are given in a key at the bottom of every double page. The range gate flag is specifically set whenever the aircraft is not within ± 300 feet of the range gate setting. On some occasions this condition may be purposely generated to check the scatterometer zeros. A dynamic range flag is set whenever the scatterometer return is above or below the dynamic capability of the scatterometer receiver. If any of the receiver temperatures are not within the proper operating range a flag is set. Whenever the receiver temperature data is missing for long periods of time (data drop out), the receiver temperatures are estimated and a flag is generated. The other keys are self-explanatory. For additional assistance in diagnosing the flagged condition the conversion report may be consulted.

The latter two columns denote aircraft radar altitude and flight direction. Other aircraft parameters are available from the listings of the aircraft mission tape.

Not listed but present on the tape is the ambient air temperature at altitude. This latter parameter is available should the investigator wish to use it to estimate the apparent temperature distribution*.

E. Program ICHAR

Program ICHAR maintains a historical tape file of RADSCAT instrument characteristics. The historical file will (eventually) consist of many sets of instrument parameters which have been entered chronologically and labeled numerically. The historical file is maintained to chart the changes in the instrument parameters as may occur through updating, instrument modifications or simply aging. The Conversion Program withdraws an appropriate set of parameters from the historical file and applies the withdrawn parameters to reduce the measurements.

ICHAR performs several useful functions. It will initially establish the file. Once the file has been established it will permit the user to append new sets of characteristics. To assist in the maintenance of the file, ICHAR may be used to print and punch old sets of characteristics. The punched sets may be modified, for example, and submitted to ICHAR as a new set to be appended to file.

F. Program TDUPE

Program TDUPE provides a master duplicate tape of the output tape formed by the Conversion Program for use on other computing machines. The bit conversion problem between machines is avoided by scaling and integerizing all the numerical data before transferring the output data to the duplicate tape. This technique has been successfully applied to tapes prepared by a CDC-6600 and read on a Honeywell 635. The CDC 6600 is a 60 bit machine which performs "ones complement" arithmetic whereas the Honeywell is a 36 bit machine which performs "twos complement" arithmetic. The scale factors may be withdrawn from the listing of TDUPE shown in Figure D-2. Each output file consists of a header label (a flight run), the instrument characteristics applied to the data, and the output data records.

* See for example, Claassen, J. P. and A. K. Fung, "An Efficient Technique for Estimating the Apparent Temperature Distribution," University of Kansas Center for Research, Inc., Technical Report 186-8, January 1973.

Additional integerized tapes may be prepared from the master duplicate tape by using system utility programs.

G. Special Programs

In addition to the above production type programs two engineering routines WIDTH and GAIN are included in the reduction package. Program WIDTH computes the equivalent beamwidth when it is presented with the mainbeam antenna pattern. The equivalent beamwidth parameter is essential to the inversion of the scatterometer data. The program GAIN computes the beam solid angle and directivity. The initial factor is important to the inversion of the radiometer measurements whereas the second is required in the inversion of the scatterometer measurements.

Functional representations of the antenna pattern are required by both programs.

IV. OPERATING INSTRUCTIONS

A. Introduction

General operating requirements, preparation of data input files, construction of the job deck, descriptions of the data products, flags and aborts, etc., are treated in this section. It is primarily written for the user having little or no knowledge of the theory and design of the programs. The reader will find that Section II and Section III will be helpful in understanding the contents of this section. Supplementary as well as detailed information on these programs may be found in the Appendices. Sufficient information is intended to permit the user to operate the primary programs CONVERT, OUTPUT, ICHAR and TDUPE. The remaining programs WIDTH and GAIN are engineering routines and should be handled by an engineer (or equivalent) familiar with the RADSCAT antenna. However, it is also strongly advised that a competent engineer, thoroughly familiar with the RADSCAT instrument, be involved in the preparation of the data and in the operation of the primary programs.

System control cards are not specified. It is presumed that this section together with sufficient knowledge of the operating system will dictate the necessary system control cards.

B. Conversion Program (CONVERT)

1. General

This program reduces 50 word input records to 20 word output records. Various computational algorithms described in detail in the Appendices are applied to the input records to yield data products of interest to the investigator. The input records are members of a file having an indefinite number of records. The files are elements of a multi-file tape. Each file is labeled with the entries shown in Table 1. The files are footed with an "end of file" mark. It is anticipated that files (flight runs) from several missions can be stored on a single tape. Tapes of this type are designated Raw Data Tapes.

To initiate processing of any of the files or all of them, processing directives are employed. The directives permit seeking files of certain types and must appear as data cards in the job deck. Each processing directive must be accompanied with a file referral argument to select a set of instrument parameters from the Instrument

Characteristics Tape* on which sets of instrument parameters are indexed numerically (and presumably stored chronologically). A set of these parameters is employed by CONVERT to reduce the raw data records. Alternatively, the instrument parameters can be entered from the card reader should the file index be set at zero. Files processed under a particular directive are transferred to the Output Tape. Various processing directives may be applied successively. In each instance the file search is effectively initiated from the beginning of the tape. Processing continues until all directives have been exhausted.

Other types of directives perform service functions. The directive POST permits newly processed files to be appended to an old Output Tape. This directive, when used, must precede all processing directives. The PRINT and PUNCH commands will list and punch, respectively, a set or several consecutive sets of instruments parameters from the Instrument Characteristics Tape. When the PUNCH command is employed, a listing of the set is also generated.

The composition of a CONVERT job deck is illustrated in Figure 4.

2. Preparation of the Raw Data Tape

As mentioned above each file is identified by a header label. The first seven items in the label (Table 1) are integer variables. The integer variables must be right justified. Note that the date requires three words. The sixth and seventh items are appended to the label to assist in selecting the proper subset of instrument characteristics from the set index designated on the processing directive card. See Section IV D for a description of the instrument characteristic files. The frequency is specified in GHz. The feed type is declared in the seventh word and is an alphanumeric word.

Presently two feed types are employed by the RADSCAT instrument. One feed uses a mechanical waveguide switch and the other a ferrite circulator. The abbreviations WG SW and CIRC are recommended as designators. To establish a convention, they should be left justified. The label must be created with an unformatted WRITE statement.

Beneath the header label are a sequence of raw data records each a mixture of real and integer words. The records are blocked by groups of 10 records. The blocks

* This tape is physically separate from the Raw Data Tape.

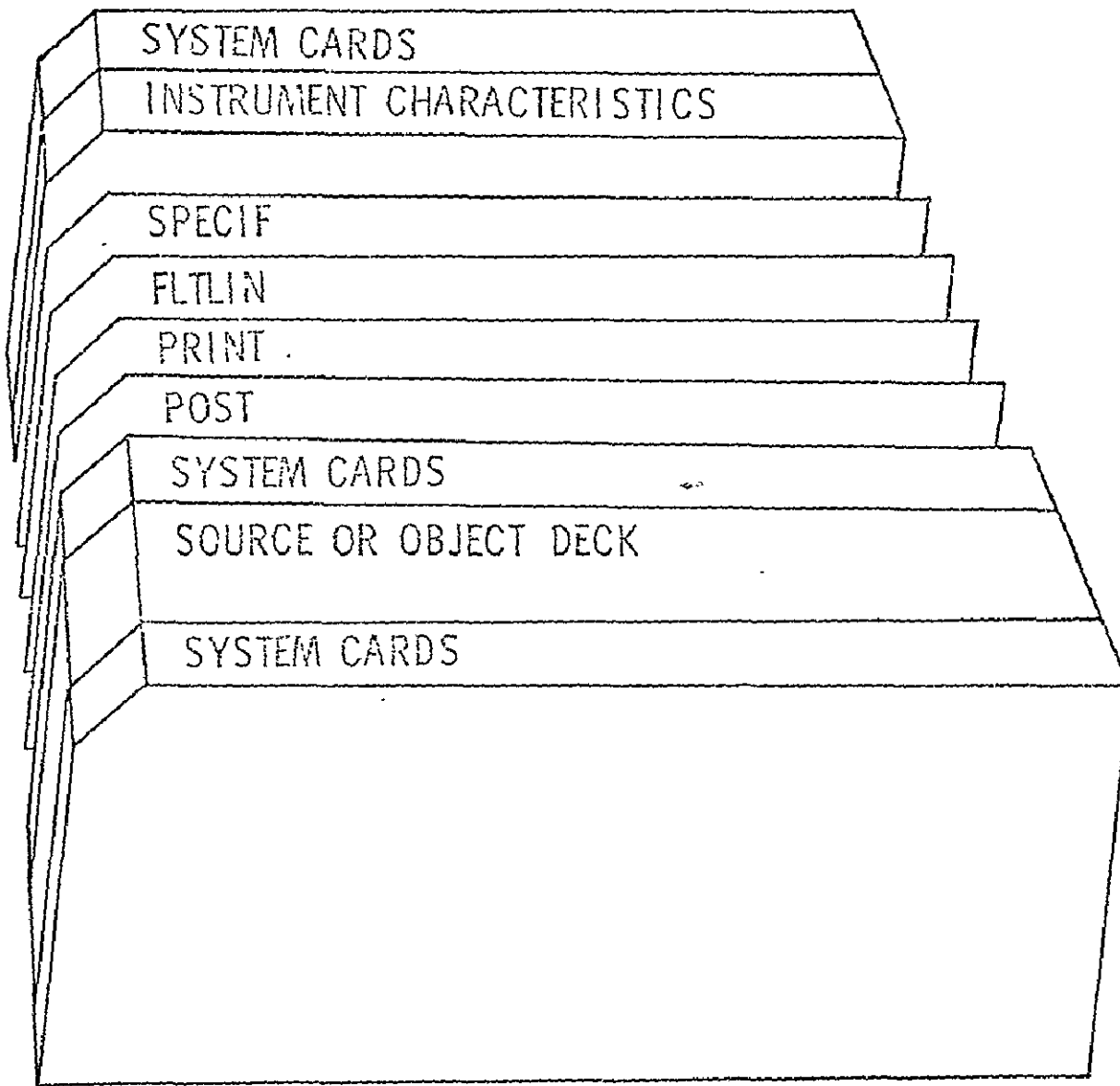


FIGURE 4. JOB DECK FOR PROGRAM CONVERT

Table I . File Label Entries Illustrated

<u>Position</u>	<u>Name</u>	<u>Entry</u>
1	Mission	207
2	Flight	.11
3	Month	7
4	Day	21
5	Year	1972
6	Line	4
7	Run	9
8	Frequency	13.9
9	Feed	WG SW

must be created by unformatted WRITE statements. When insufficient records exist to fill the last block on a file, the remaining records must be filled with 99999.0 (floating point). These entries are used to flag the end of the records (file). In addition an EOF is appended to the foot of the file. As many files as practical may be created on the tape. The end of the files must be flagged with the label END OF REEL which fills the beginning of a nine word array and in effect is another file label.

The files are composed of three record types:

1. Normal Calibration
2. Baseline Calibration
3. Measurements

Calibration records may appear anywhere in the file and as frequently as desired. In a properly constructed file both types of calibrations should appear in the first records. However, should one (or both) type(s) of calibration be missing from the top of the file, the program will search for calibration records deeper in the file. Records bypassed in the search are transferred to a scratch unit for subsequent processing. Once found, the calibration information is extracted and applied to the bypassed records. Records following the calibration records are also treated with the same parameters until new calibration records are encountered. When the calibration information is totally missing or incomplete, the file is bypassed and an appropriate error message is printed.

The entries in the records are shown in Table II. Type and units of the variables are indicated. Parenthetical designators behind some of the entry names describe the computed results stored in those positions during processing. The integer

TABLE II RAW DATA VECTOR

NAME : DATA

<u>POSITION</u>	<u>ENTRY</u>	<u>TYPE</u>	<u>UNITS</u>
1	TIME	R	HR MIN SEC
2	FREQUENCY INDICATOR	I	—
3	MODE INDICATOR	I	—
4	DATA TYPE INDICATOR	I	—
5	ANGLE DESIGNATOR	I	—
6	TRANS POL INDICATOR	I	—
7	REC POL INDICATOR	I	—
8	SCAT 1 (OR CONVERTED SCAT)	R	VOLTS
9	SCAT 2	"	"
10	SCAT 3	"	"
11	SCAT 4	"	"
12	RAD POL INDICATOR	I	—
13	RAD (OR CONVERTED RAD)	R	VOLTS
14	SCAT ANGLE (OR INCID ANGLE)	R	"
15	RAD ANGLE (OR X-TRACK ANGLE)	R	"
16	RANGE GATE INDICATOR	I	—
17	T ₁ ' 9.3 DICKE SWITCH	R	VOLTS
18	T ₂ ' TRIPLEXER	R	"
19	T ₃ ' T/R CIRCULATOR	R	"
20	T ₄ ' 13.9 DICKE SWITCH	R	"
21	T ₅ ' 9.3 TDA	R	"
22	T ₆ ' 9.3 WARM LOAD	R	"
23	T ₇ ' 9.3 LIMITER	R	"
24	T ₈ ' BRACKET	R	"
25	T ₉ ' COMMON T/R GUIDE	R	"
26	T ₁₀ ' 11.7 DICKE SWITCH	R	"
27	T ₁₁ ' 13.9 WARM LOAD	R	"
28	T ₁₂ ' POLAR SWITCH OR CIRC.	R	"
29	T ₁₃ ' SCAT CALIB SWITCH	R	"
30	T ₁₄ ' 9.3 IMAGE REJECTION FILTER	R	"

TABLE II RAW DATA VECTOR (continued)

NAME : DATA

<u>POSITION</u>	<u>ENTRY</u>	<u>TYPE</u>	<u>UNITS</u>
31	T ₁₅ , BASEPLATE	R	VOLTS
32	T ₁₆ , OMT	R	"
33	T ₁₇ , HOT LOAD	R	VOLTS
34	V _{agc}	R	VOLTS
35	V _{supply}	R	"
36	FLAG (T ₁₁ MISSING)	I	-
37	EMPTY		
38	"		
39	"		
40	"		
41	RADAR ALTITUDE	R	FEET
42	GRD SPEED	R	FT/SEC
43	PITCH	R	DEGREES
44	DRIFT	R	DEGREES
45	ROLL	R	DEGREES
46	AMBIENT AIR TEMP	R	°C
47	FLIGHT DIRECTION	R	DEGREES
48	EMPTY		
49			
50			

indicator variables are defined in Table III. These indicators are employed to cue certain program actions or to index variables and must be right justified. Items 2 through 13 and 16 are extracted from the RADSCAT microwave data channel. Items 17 through 32 are retrieved from the RADSCAT ATM channel. Item 33 is presently entered by hand but may eventually appear on the ATM channel. Items 34 and 35 are presently ignored but may also eventually appear on the ATM channel. Item 36 is presently entered by hand and is used to flag missing temperature data (DATA(17) - DATA(32)). Items 41 to 45 and 47 are provided by the Litton Navigator LTN-51 aboard the C-130. Item 46 is provided by an external sensor aboard the aircraft.

The measurement records must be completed as shown in Table II. However, the calibration records may be abbreviated to include only the data type indicator (DATA(4)) and the calibration entries in the appropriate SCAT and/or in the RAD position. The normal calibration records must be ordered by SCAT channels (one through four) with the normal RAD calibration occurring in the fourth record (containing the SCAT channel 4 calibration). The routine which extracts calibration data will orient itself on the calibration record for SCAT channel 1 in an attempt to meet contingencies where calibration record drop-outs occur. Any number of normal calibration sequences (calibrations on channels one through four in each sequence) may occur successively. All will be averaged. Typically the instrument produces three sequences of normal calibrations. The baseline calibration record simply requires the appropriate RAD baseline calibration in the DATA(13) position (as well as the type indicator in DATA(4)) and may occur anywhere in the file except within a sequence of normal calibrations. It is essential that the baseline and normal calibrations be grouped by three or more consecutive records to assure that a statistically significant average will be established. The program will average consecutive baseline records, even if they are interspersed with sets of normal calibrations. The normal calibrations will also be averaged in this circumstance.

A routine prepared by Langley Research Center actually merges data from several sources to meet the above specifications.

3. Preparation and Use of the Control Cards

There are four types of processing directives and three service directives. The directives consist of a control word and some arguments. All control words are left justified; the arguments are right justified. Sample directives and their formats are defined in Table IV.

TABLE III. DEFINITION OF INTEGER INDICATOR VARIABLES

	0	1	2	3	4	5	6
Frequency Indicator		9.3 GHz	11.4*GHz	13.9 GHz			
Data Type	Measurement	Normal Calibration	Base Calibration				
Angle Designator		X	X	X	X	X	X
Polarization Indicator	Horizontal	Vertical					
Range Gate	2000 ft.	5000 ft.	10,000 ft.	20,000 ft.			
Mode Indicator**	R.O.	S.S.	F.A.	A.A.			

* NOT OPERATIONAL

** R.O. = RADIOMETER ONLY

S.S. = SHORT SCAT

F.A. = FIXED ANGLE

A.A. = ALTERNATING ANGLE

TABLE IV. CONTROL CARD OPTIONS ILLUSTRATED

CONTROL WORD	ARGUMENTS						
	MISSION	FLIGHT	LINE	RUN	LINE PRINT MODULUS	ICHAR SET NO.	FILES TO BE PROCESSED
A6, 4X	15	15	15	15	15	15	15
SPECIF	207	12	2	3	1	2	1
FLTLIN	208	1	4	--	5	3	81
MISFLT	209	4	--	--	10	3	10
ALL	--	--	--	--	10	2	999
POST	--	--	--	--	--	--	--
PRINT	--	--	--	--	--	2	2
PUNCH	--	--	--	--	--	1	1

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The control word for the processing directives designates the classification of the file search to be conducted. The search is conducted by comparing the arguments, mission, flight, line and run on the directive with the file labels on the Raw Data Tape. The depth of comparison in the label will depend on the type of processing directive. ALL will process all files on the tape, MISFLT will process all lines and runs under the designated mission and flight, FLTLIN will process all runs from the specified mission, flight, and line. SPECIF will process only a particular file labeled by the specified mission, flight, line and run. When consecutive processing directives are employed, the file search is effectively conducted from the beginning of the tape.

Arguments other than the mission, flight, line and run must also be provided. The sixth word LNPMOD controls the density of records on which reports will be made in the activity report. The use of this parameter will limit the amount of print out acquired during the reduction of records. It will not affect the density of output records.

The set of instrument characteristics (ICU) to be applied to the specified files is designated in the seventh word. The entry specifies the file position on a master tape of characteristics. If a zero is entered, the program will expect instrument parameters to be read from cards appended behind the program control card. When characteristics are read from the card reader, processing is limited to one physical file regardless of the directive. This control option is primarily reserved to test a set of instrument characteristics. See Section IVD for a description of the format required for the instrument characteristics. If 999 is specified, the last set of characteristics on the master (historical) tape will be used.

The last (eighth) entry NFP on the control card specifies the number of files to be processed under the directive. To process all files under the directive simply make NFP sufficiently large.

The special service command POST may be used to position a previously produced output tape to a point behind the last file on the tape. The use of this command will, therefore, permit new files to be appended to an old output tape. This command, when used, must appear before any processing directives. There are no arguments with this directive.

The two service directives PRINT and PUNCH are provided to list and list and punch a designated set of instrument characteristics, respectively. The desired

set number is entered in columns 36 through 40 of the directive card. If $n-1$ sets behind the designated set are to be listed or punched also, NFP should be set to n ; otherwise it is set equal to one. NFP appears in column 41 through 45 of the directive card.

4. Peripheral and Memory Requirement

The input and output unit requirements are illustrated in Figure 5. Under a processing directive units 01, 02, 04, 06, 08 are required; under the service directives PRINT or PUNCH units 04, 06, and 43 are required. Unit 08 is a scratch unit, either disc or tape, preferably disc. It is used to temporarily store bypassed records when it is necessary to search for calibration data.

Approximately 17000 decimal words of memory were required to load this program on a CDC-6600 to include buffer space and system routines.

5. Flags and Aborts

The activity report produced by the program conveys various messages to indicate the status of the processing. It is normal for the program to echo check the directives, to list the progress on the processing, and to indicate a normal termination. The Conversion Report will also make regular statements reflecting the progress of the processing and the quality of the measurements. A sample listing of the Conversion Report is shown in Figure 2 of Section III. In some instances however, improper use of the program or construction of the data will result in an error message or an abort.

When an abort condition is encountered, an error message is generated, an abort code is given, an end of file mark is appended to the output tape on unit 02, an END OF REEL statement is appended, and control is yielded to the system. Table V defines the various abort conditions. When invalid data records are encountered, an error message will identify the improper element and the entire record will be dumped in octal. The message will appear within the Conversion Report. When more than 10 bad records are encountered in a file, the remaining records in the file are bypassed and processing is directed to the next internal activity. When more than three bad files are encountered the processing is aborted.

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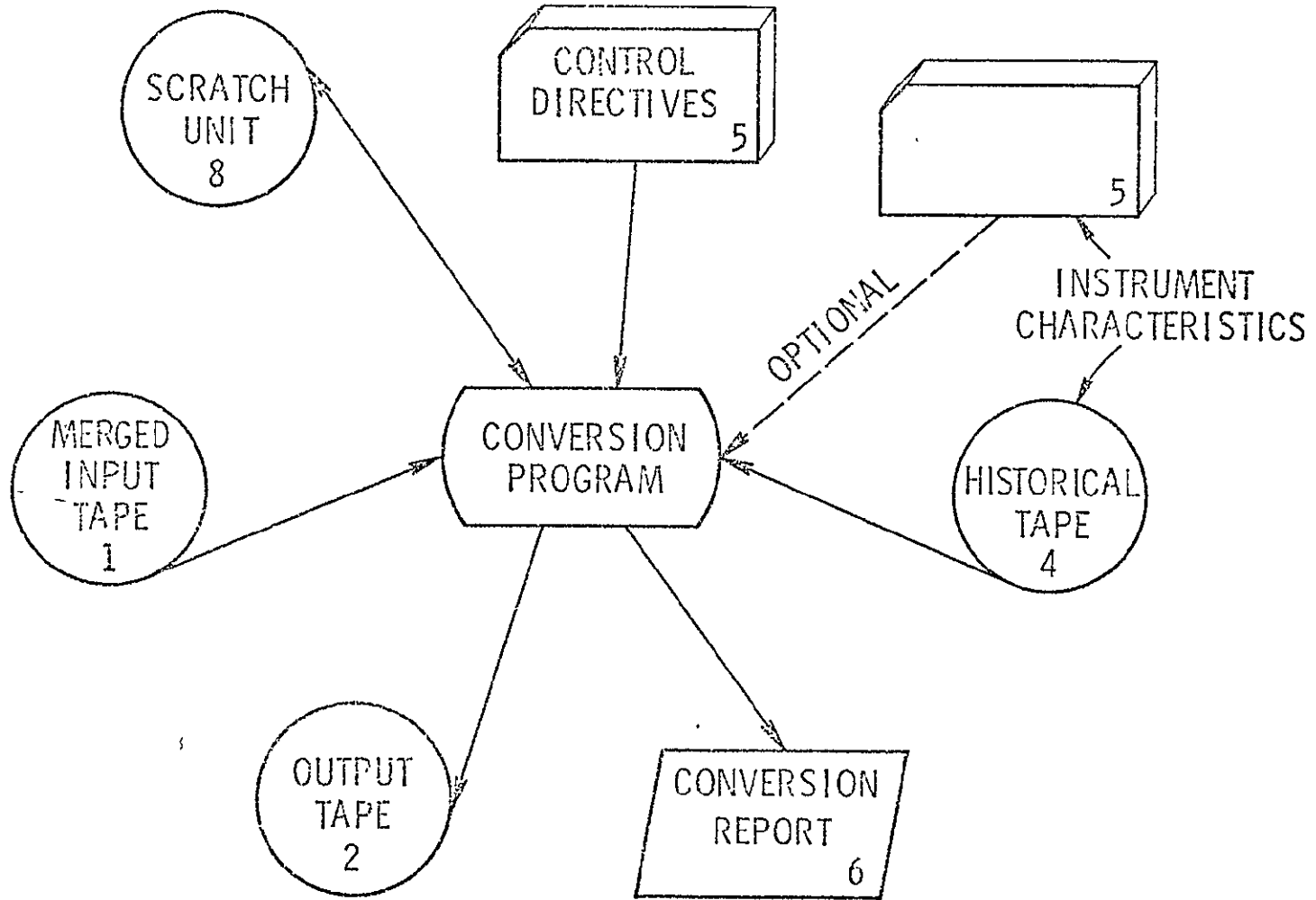


FIGURE 5. PERIPHERAL REQUIREMENTS FOR THE PROGRAM CONVERT

Table V. Definition of Abort Codes

UD	= <u>U</u> nrecognized <u>D</u> irective
IC	= <u>I</u> nstrument <u>C</u> haracteristic Missing
MF	= <u>M</u> issing Raw Data <u>F</u> ile
FF	= Unable to Find Instrument Characteristics with the <u>F</u> eed and <u>F</u> requency Designated
ER	= Too Many File <u>E</u> rrors
NFP	= NFP less than 1

6. Description of the Data Products

Normally two data products are generated by CONVERT, an activity report and an output tape. When the PUNCH option is employed a set or sets of punched instrument parameters can also occur. The character of the punched output is identical to that described in Section III D. The activity report reflects the program progress and largely contains items in the Conversion Report. See Figure 2 of Section III for an illustration of the Conversion Report. The Output Tape, however, will be described.

The output file structure is similar to that of the input raw data files. The file consists of the file label and blocks of output records. However, occurring between the label and output record blocks is the set of instrument parameters that had been used to process the input records. The entries in the file label are the same as that for the input files shown in Table I. The label and instrument parameters are created with separate unformatted WRITE statements. The entries in the instrument characteristics are described in Section III D. The output records occurring beneath the instrument parameters are blocked in 20 records groups. Each block is created with a binary WRITE statement. The elements in the output records consist of mixed integer and floating point entries. The entries are defined in Table VI. When insufficient records exist to fill the the last block in the file, the remaining entries are filled with integer zeros. An "end of file" mark is created after the last block in the file.

When all directives have been exhausted or the program aborted an "end of reel" statement is appended behind the last output file.

TABLE VI OUTPUT DATA VECTOR

<u>POSITION</u>	<u>ENTRY</u>	<u>TYPE</u>	<u>UNITS</u>
1.	TIME	R	HR, MIN, SEC
2.	MODE	I	—
3.	INCIDENCE ANGLE	R	DEGREES
4.	CROSS TRACK ANGLE	R	DEGREES
5.	TRANSMIT POLARIZATION	I	—
6.	RECEIVE POLARIZATION	I	—
7.	SCAT INTEGRATION TIME	R	SECONDS
8.	NORMALIZE SCATTERING COEF.	R	M^2/M^2
9.	NORMALIZE SCATTERING COEF.	R	dB
10.	ANTENNA TEMPERATURE	R	DEGREES KELVIN
11.	DEPOLARIZATION FACTOR	R	—
12.	DATA VALIDATION CODE	I	—
13.	ALTITUDE		FEET
14.	FLIGHT DIRECTION		DEGREES wrt TRUE NORTH
15.	AMBIENT AIR TEMP		DEGREES KELVIN
16-20.	EMPTY		

C. Output Program

1. General

The Output Program simply lists the output records prepared by program CONVERT. The output listings are organized by files which are selected by external directives similar to those described for the Conversion Program. A sample of a listing is illustrated in Figure 3 of Section III. The file heading together with instrument characteristic identifiers compose the page heading. Beneath the heading are listed 80 record images; each image consists of the first fourteen entries in an output record as defined in Table VI. The fifteenth entry is not printed but is available on tape should the investigator choose to use it to further reduce the radiometer data. Each line of print-out is appended with the record number. The record number corresponds to those used in the Conversion Report. The 80 records are intended to fill two consecutive pages of print-out where the page size is 8-1/2" by 15". Appended to the foot of each double page is a key defining the S/R validation code in column 13.

The instrument characteristics although present on the output tape are not listed. The set which has produced the data is identified in the heading on the right by the set number and date. No option is provided to print the characteristics.

The job deck for the program OUTPUT is organized identically to the conversion program (however, no instrument characteristics must appear in the data deck). File types are selected from the output by proper use of the directives:

1. ALL
2. MISFLT
3. FLTLIN
4. SPECIF

The meaning and use of these directives have been presented in Sections III B.1 and III B.2. The format of these control cards is identical to those described above. In the argument field of the control card the appropriate file identifiers must be present. No provision is made to limit the number of files to be processed, nor can the record density be controlled through a line print modulus. It is, of course, meaningless to specify the instrument characteristics ICU.

2. Program Messages

In addition to listing the output file, OUTPUT will keep the user posted on its internal activity as it searches for the specified files. The directive is initially echo checked, bypassed files are identified and the user is notified when the reel is encountered. Unrecognized directives will terminate the processing.

3. Peripheral and Memory Requirement

Peripheral requirements are illustrated in Figure 6. The program required approximately 7000 decimal words of memory on a CDC 6600 to include buffer space and system routines.

D. Program ICHAR

1. General

The primary purpose of program ICHAR is to maintain a file of instrument characteristics. The file is maintained not only to serve as a source of parameters to reduce raw data records but also to serve as a history of the changes undergone by the RADSCAT instrument. The file can consist of many sets of instrument parameters which are appended to the file numerically. The user may also identify the set by a date which is entered with the parameters.

Each set of instrument characteristics can consist of four subsets. The four subsets permit characterizing the instrument for a combination of two feeds and two frequencies. Each subset is composed of a set of radiometer parameters and a set of scatterometer parameters. The subsets are identified by feed and frequency. These identifiers are used by the Conversion Program to select the appropriate subset of characteristics.

This file maintenance program is operated by means of external control cards. Four directive (processing) options are offered:

1. INITIALIZE
2. APPEND
3. PRINT
4. PUNCH

They must be left justified and occupy columns 1 through 10 of the control card. INITIALIZE will create the historical file by storing the first set of characteristics on the tape. The set must appear behind the control card. APPEND will permit other sets to be added to the existing historical file. The characteristics set to be appended must appear behind the APPEND command card. When several sets are added at one operation, each set must be led by an APPEND card and intervening PRINT or PUNCH commands are not permitted. When sets are appended to the file, the old sets are transferred from the old tape to a new tape and the new sets are then

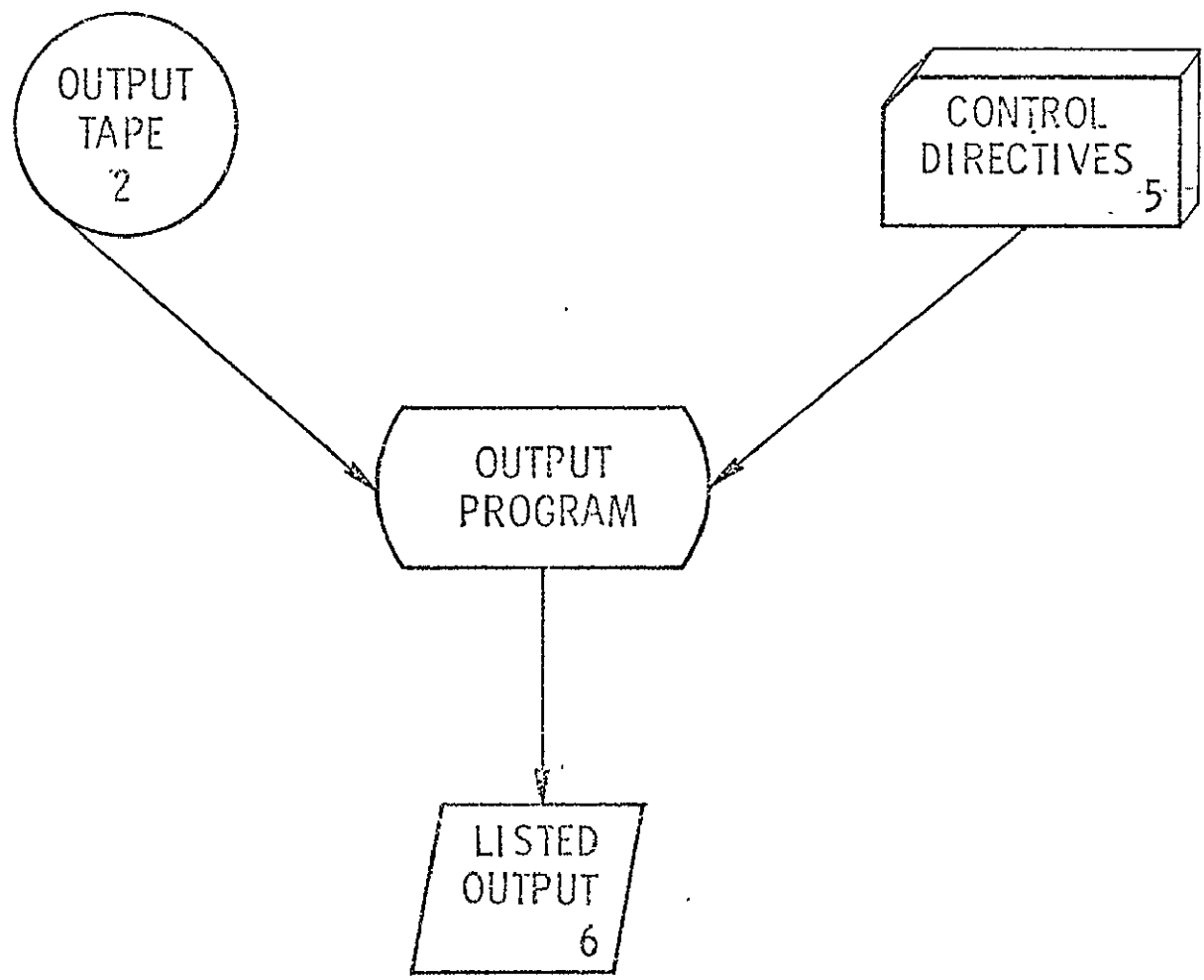


FIGURE 6. PERIPHERAL REQUIREMENTS FOR THE PROGRAM OUTPUT

added to the new tape. Before appending a new set of characteristics, it is advisable to have tested them in the Conversion Program by entering them from the card reader.

The PRINT and PUNCH commands perform the same service as they do in the Conversion Program. However, one command must be used for each set to be printed or punched. The set to be printed or punched must be specified on the control card in columns 11 through 15. The set number must be right justified. A listing accompanies the punched output. The PRINT or PUNCH may precede or follow a set of APPEND commands but must not intermingle with them. These commands are provided so that new sets may be formed easily from old sets of characteristics.

A sample deck is illustrated in Figure 7.

2. Preparation of the Instrument Characteristics

The instrument parameters cards must be prepared in groups of four subsets. When insufficient data exists to complete one of the subsets, a complete subset may be repeated an appropriate number of times to fill the requirement. A sample subset is shown in Figure 8. The lines actually represent card images (except for the word SET). The entries in the upper half are radiometer parameters whereas the entries in the lower half are scatterometer parameters. This subset would be used for measurements taken at 13.9 GHz with a waveguide switch (WG SW) as the polarization switch. The radiometer and scatterometer parameters are identified with the set number of which it is a member and with a date of entry (origin). The first line of radiometer or scatterometer parameters must be punched with the format 4I5, 10X, E10.3, A10, E10.3 whereas the remaining lines must be punched according to the format 7E10.3. Excluding the set number and date, the radiometer parameters array consist of 75 words and the scatterometer parameter array consists of 85 words. Not all words are necessarily filled.

The entries in the radiometer and scatterometer arrays are defined in Tables VII and VIII, respectively. Many of the entries can be clarified by referring to a description of the reduction algorithms in the Appendices. These algorithms have been developed from the transfer and calibration characteristics of the RADSCAT instrument. As a consequence the entries may change (and perhaps the program algorithms) when the instrument is modified. Many of the entries must be based on special calibrations and measurements. Explanations are required for some of the

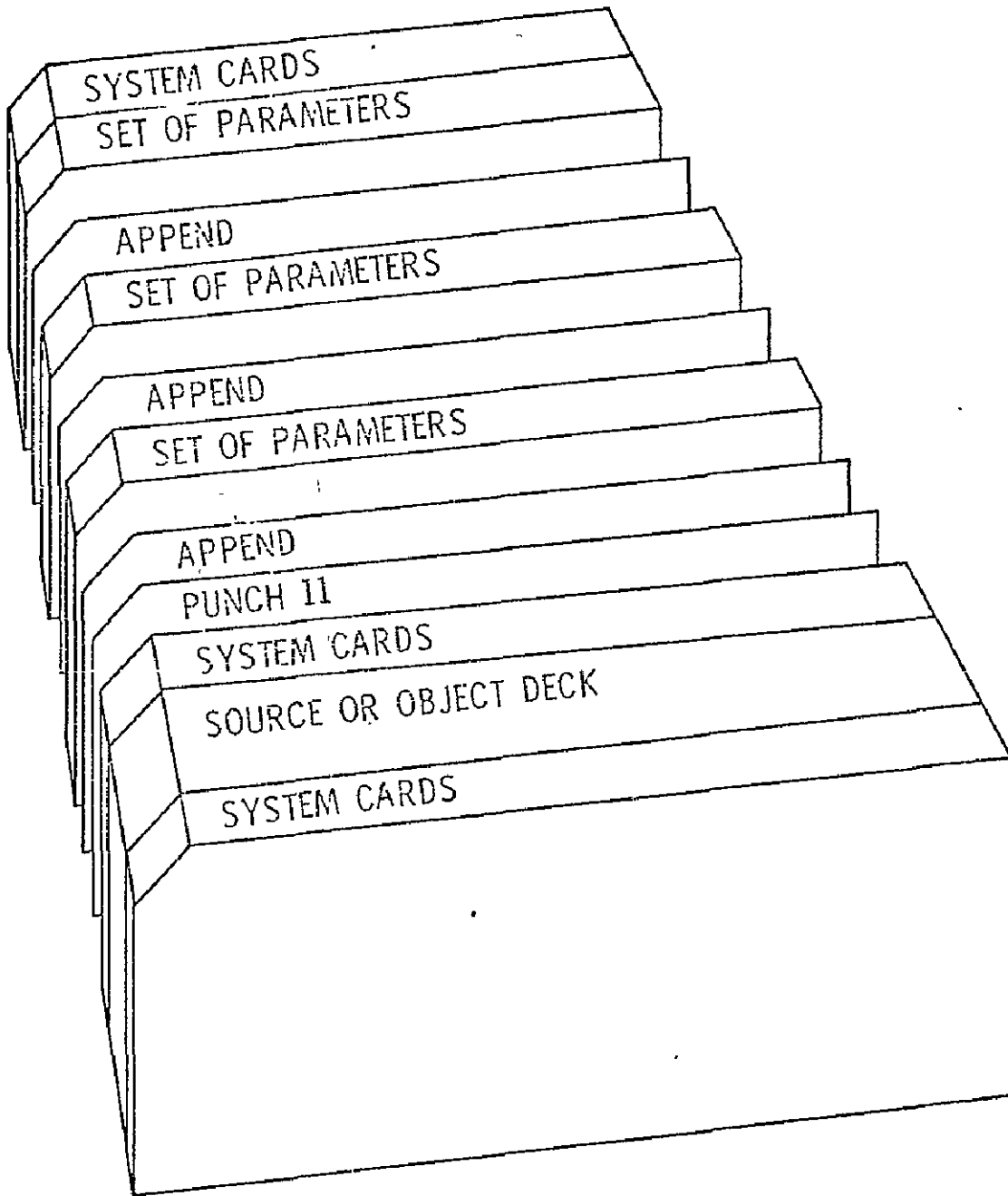


FIGURE 7. JOB DECK FOR PROGRAM ICHAR

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SET	1	DATE	10	23	72	1.3900E+10	WG SW	0.	0.	0.	0.
0.			3.9900E+02			1.0540E+00	1.9950E+02	4.0000E-01	8.0000E-02	8.0000E-02	8.0000E-02
1.0200E-02			1.0150E-02			6.0000E-02	6.0000E-02	0.	0.	0.	-0.
-0.			1.2800E-01			1.0000E-01	3.2500E+02	3.0500E+02	-8.7800E+00	-8.7800E+00	7.9924E+01
-8.7800E+00			7.9871E+01			-8.7800E+00	7.9169E+01	-8.7800E+00	7.8879E+01	7.8879E+01	-8.7800E+00
7.9476E+01			-8.7800E+00			7.8730E+01	-8.7800E+00	7.9415E+01	-8.7800E+00	-8.7800E+00	7.9704E+01
-8.7800E+00			7.9388E+01			-8.7800E+00	7.9889E+01	-8.7800E+00	8.0178E+01	8.0178E+01	-8.7800E+00
7.8826E+01			-8.7800E+00			7.9757E+01	-8.7800E+00	7.9709E+01	-8.7800E+00	-8.7800E+00	7.9573E+01
-8.7800E+00			7.9379E+01			1.0000E+00	-2.7318E+02	-0.	-0.	-0.	-0.
-0.			-0.			-0.	-0.	-0.	-0.	-0.	-0.
-0.			-0.			-0.	-0.	-0.	-0.	-0.	-0.
-0.			-0.			-0.	-0.	-0.	-0.	-0.	-0.

SET	1	DATE	10	23	72	1.3900E+10	WG SW	1.0000E-01	1.0000E-01	1.0000E-01	1.0000E-01
5.8000E-01			5.9500E-01			6.3700E-01	7.0700E-01	8.0200E-01	9.2400E-01	9.2400E-01	3.0000E-01
3.7568E-01			3.7916E-01			0.	0.	4.9753E-01	5.0213E-01	5.0213E-01	2.0893E-01
1.0000E+00			1.0000E-02			3.1623E-04	3.1623E-04	-8.0000E+03	3.0000E+03	3.0000E+03	2.5000E+02
1.4125E+04			1.4125E+04			1.4000E+00	1.0500E+01	1.4000E-01	-6.3400E+00	-6.3400E+00	5.0000E+01
2.2514E-01			2.2514E-02			0.	0.	4.6000E-02	7.1000E-02	7.1000E-02	9.6000E-02
1.3000E-01			1.6500E-01			2.1300E-01	2.6200E-01	2.8600E-01	3.0000E-01	3.0000E-01	6.4200E-01
5.1500E-01			6.0000E-01			7.6900E-01	8.8500E-01	1.0000E+00	1.1730E+00	1.1730E+00	1.3460E+00
1.3460E+00			1.3460E+00			1.2500E+00	1.1540E+00	1.0960E+00	1.0380E+00	1.0380E+00	1.0190E+00
1.0000E+00			1.0560E+00			1.1120E+00	1.2170E+00	1.3230E+00	1.3730E+00	1.3730E+00	1.4230E+00
1.4850E+00			1.5380E+00			1.4420E+00	1.3460E+00	1.1570E+00	9.0900E-01	9.0900E-01	7.6000E-01
5.5000E-01			4.2100E-01			2.9200E-01	2.3300E-01	1.7300E-01	1.4400E-01	1.4400E-01	1.1500E-01
1.0000E-01			8.5000E-02			-0.	-0.	-0.	-0.	-0.	-0.

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FIGURE 8. SAMPLE OF INSTRUMENT CHARACTERISTICS

TABLE VII RADIOMETER PARAMETERS

VARIABLE NAME : RPAR

<u>POSITION</u>	<u>ENTRY</u>		<u>TYPE</u>	<u>UNITS</u>
1	FREQUENCY		R	GHZ
2	FEED (WG SW OR CIRC)		A	UNITLESS
3	CROSS FEED CONSTANT	ϵ_{HV}	R	"
4	" "	ϵ_{VH}	R	"
5	HOT LOAD REFERENCE CONST	σ_1	R	$^{\circ}K$
6	WARM LOAD REFERENCE CONST	σ_2	R	"
7	HOT LOAD BIAS FACTOR	σ_3	R	"
8	WARM LOAD BIAS FACTOR	σ_4	R	UNITLESS
9	SWITCH COMPENSATION FACTOR	ρ_{1H}	R	UNITLESS
10	" " "	ρ_{1V}	R	"
11	OMT " "	ρ_{2H}	R	"
12	" " "	ρ_{2V}	R	"
13	CUTLER FEED " "	ρ_{3H}	R	"
14	" " "	ρ_{3V}	R	"
15	INPUT GUIDE " "	ρ_{4H}	R	"
16		ρ_{4V}	R	"
17	RESIDUAL " "	ρ_{5H}	R	
18	"	ρ_{5V}	R	
19	MEASUREMENT PERIOD	τ	R	SEC
20	CALIBRATION PERIOD	τ_C	R	SEC
21	UPPER TEMP LIMIT	UP	R	$^{\circ}K$
22	LOWER TEMP LIMIT	LOW	R	$^{\circ}K$
23	THERMISTOR CONVERSION FACTOR	α_1	R	$^{\circ}C/VOLT$
24	" " "	β_1	R	$^{\circ}C$
25	" " "	α_2	R	$^{\circ}C/VOLT$
26	" " "	β_2	R	$^{\circ}C$
27	" " "	α_3	R	$^{\circ}C/VOLT$
28	" " "	β_3	R	$^{\circ}C$
29	" " "	α_4	R	$^{\circ}C/VOLT$
30	" " "	β_4	R	$^{\circ}C$

TABLE VII RADIOMETER PARAMETERS (continued)

<u>POSITION</u>	<u>ENTRY</u>		<u>TYPE</u>	<u>UNITS</u>
31	THERMISTOR CONVERSION FACTOR	α_5	F6.2	$^{\circ}\text{C}/\text{VOLT}$
32	"	"	"	$^{\circ}\text{C}$
33	"	"	"	$^{\circ}\text{C}/\text{VOLT}$
34	"	"	"	$^{\circ}\text{C}$
35	"	"	"	$^{\circ}\text{C}/\text{VOLT}$
36	"	"	"	$^{\circ}\text{C}$
37	"	"	"	$^{\circ}\text{C}/\text{VOLT}$
38	"	"	"	$^{\circ}\text{C}$
39	"	"	"	$^{\circ}\text{C}/\text{VOLT}$
40	"	"	"	$^{\circ}\text{C}$
41	"	"	"	$^{\circ}\text{C}/\text{VOLT}$
42	"	"	"	$^{\circ}\text{C}$
43	"	"	"	$^{\circ}\text{C}/\text{VOLT}$
44	"	"	"	$^{\circ}\text{C}$
45	"	"	"	$^{\circ}\text{C}/\text{VOLT}$
46	"	"	"	$^{\circ}\text{C}$
47	"	"	"	$^{\circ}\text{C}/\text{VOLT}$
48	"	"	"	$^{\circ}\text{C}$
49	"	"	"	$^{\circ}\text{C}/\text{VOLT}$
50	"	"	"	$^{\circ}\text{C}$
51	"	"	"	$^{\circ}\text{C}/\text{VOLT}$
52	"	"	"	$^{\circ}\text{C}$
53	"	"	"	$^{\circ}\text{C}/\text{VOLT}$
54	"	"	"	$^{\circ}\text{C}$
55	"	"	"	$^{\circ}\text{C}/\text{VOLT}$
56	"	"	"	$^{\circ}\text{C}$
57	EMPTY			
.	.			
.	.			
.	.			
75	EMPTY			

TABLE VIII SCATTEROMETER PARAMETERS

<u>POSITION</u>	<u>ENTRY</u>		<u>TYPE</u>	<u>UNITS</u>
1	FREQ		R	HZ
2	FEED (WG SW OR CIRC)		A	—
3	CALIBRATION PERIOD	C	R	SEC
4	INT. TIME #1	1	R	"
5	INT. TIME #2	2	R	"
6	INT. TIME #3	3	R	"
7	INT. TIME #4	4	R	"
8	INT. TIME #5	5	R	"
9	INT. TIME #6	6	R	"
10	SHORT SCAT INT TIME	7	R	"
11	TRANSFER FUNCTION	G_{HT}	R	—
12	" "	G_{VT}	R	—
13	" "	G_{VHT}	R	—
14	" "	G_{HVT}	R	—
15	" "	G_{HR}	R	—
16	" "	G_{VR}	R	—
17	" "	G_C	R	—
18	CAL ATTN CHAN 1	A_1	R	—
19	" " " 2	A_2	R	—
20	" " " 3	A_3	R	—
21	" " " 4	A_4	R	—
22	FILTER LOWER LIMIT (NEG)		R	HZ
23	FILTER UPPER LIMIT (POS)		R	HZ
24	FILTER RESOLUTION		R	HZ
25	ANT GAIN H	Γ_H	R	—
26	ANT GAIN V	Γ_V	R	—
27	CHAN #1 SATURATION LEVEL		R	VOLTS
28	EMPTY			—
29	MINIMUM SQUARE LAW LEVEL FOR ALL CHANNELS		R	VOLTS
30	ANGLE CONVERSION FACTOR		R	DEG/VOLT

TABLE VIII SCATTEROMETER PARAMETERS (continued)

<u>POSITION</u>	<u>ENTRY</u>	<u>TYPE</u>	<u>UNITS</u>
31	ANGLE CORRECTION FACTOR*	R	DEG.
32	EQUIVALENT BEAMWIDTH H θ_{eq}	R	RADIANS
33	EQUIVALENT BEAMWIDTH V θ_{eq}	R	"
34	EMPTY		—
35	"		—
36	"		—
37	"		—
38	RELATIVE FILTER GAIN, $f=$ 3000	R	—
39	" $f=$ 2750	R	—
40	" $f=$ 2500	R	—
41	" $f=$ 2250	R	—
42	" $f=$ 2000	R	—
43	" $f=$ 1750	R	—
44	" $f=$ 1500	R	—
45	" $f=$ 1250	R	—
46	" $f=$ 1000	R	—
47	" $f=$ 750	R	—
48	" $f=$ 500	R	—
49	" $f=$ 250	R	—
50	" $f=$ 0	R	—
51	" $f=$ -250	R	—
52	" $f=$ -500	R	—
53	" $f=$ -750	R	—
54	" $f=$ -1000	R	—
55	" $f=$ -1250	R	—
56	" $f=$ -1500	R	—
57	" $f=$ -1750	R	—
58	" $f=$ -2000	R	—
59	" $f=$ -2250	R	—
60	" $f=$ -2500	R	—

* Includes relative pitch between aircraft frame and antenna gimbal.

TABLE VIII SCATTEROMETER PARAMETERS (continued)

<u>POSITION</u>	<u>ENTRY</u>		<u>TYPE</u>	<u>UNITS</u>
61	RELATIVE FILTER GAIN,	f=-2750	R	—
62	"	f=-3000	R	—
63	"	f=-3250	R	—
64	"	f=-3500	R	—
65	"	f=-3750	R	—
66	"	f=-4000	R	—
67	"	f=-4250	R	—
68	"	f=-4500	R	—
69	"	f=-4750	R	—
70	"	f=-5000	R	—
71	"	f=-5250	R	—
72	"	f=-5500	R	—
73	"	f=-5750	R	—
74	"	f=-6000	R	—
75	"	f=-6250	R	—
76	"	f=-6500	R	—
77	"	f=-6750	R	—
78	"	f=-7000	R	—
79	"	f=-7250	R	—
80	"	f=-7500	R	—
81	"	f=-7750	R	—
82	"	f=-8000	R	—
83	EMPTY			
84	"			
85	"			

entries. The thermistor conversion factors in RPAR(23) through RPAR(56) convert the thermistor voltages in DATA(17) through DATA(33) to temperature in centigrade (see Table II). A sampled representation of the scatterometer doppler filter frequency characteristic appears in SPAR(34) through SPAR(85). The sample frequency interval is designated in SPAR(24) and the frequency domain of the doppler filter is specified in SPAR(22) and SPAR(23).

3. Peripheral and Memory Requirements

The peripheral requirements are illustrated in Figure 9. To load the program required approximately 10,000 decimal words of memory on a CDC-6600 to include buffer space and system routines.

E. Program TDUPE

Program TDUPE scales and integerizes output files prepared by program CONVERT and transfers the result to another tape. The resulting tape serves as a master tape which may be duplicated and sent to the investigator for use on another type of computing machine.

The scaling and transferring of an output tape is implemented by an external control card appended to the source or object deck. The card simply states the files by mission and flight which are to be transferred. The control card requires a 2I10 format. The input files must be located on tape unit 01. The specified file types are transferred to a tape on unit 02. An activity report, stating the status on the transfers, is generated. The program requires approximately 8000 decimal words on a CDC-6600. The peripheral requirements are illustrated in Figure 10.

F. Special Programs

Several engineering application programs are provided to compute and/or verify certain antenna parameters employed in the instrument parameters. Program WIDTH computes the equivalent pencil beamwidth, an important parameter to the inversion of the scatterometer data (SPAR(32) and SPAR(33)). The program GAIN computes the antenna gains SPAR(25) and SPAR(26) and the beam solid angle.

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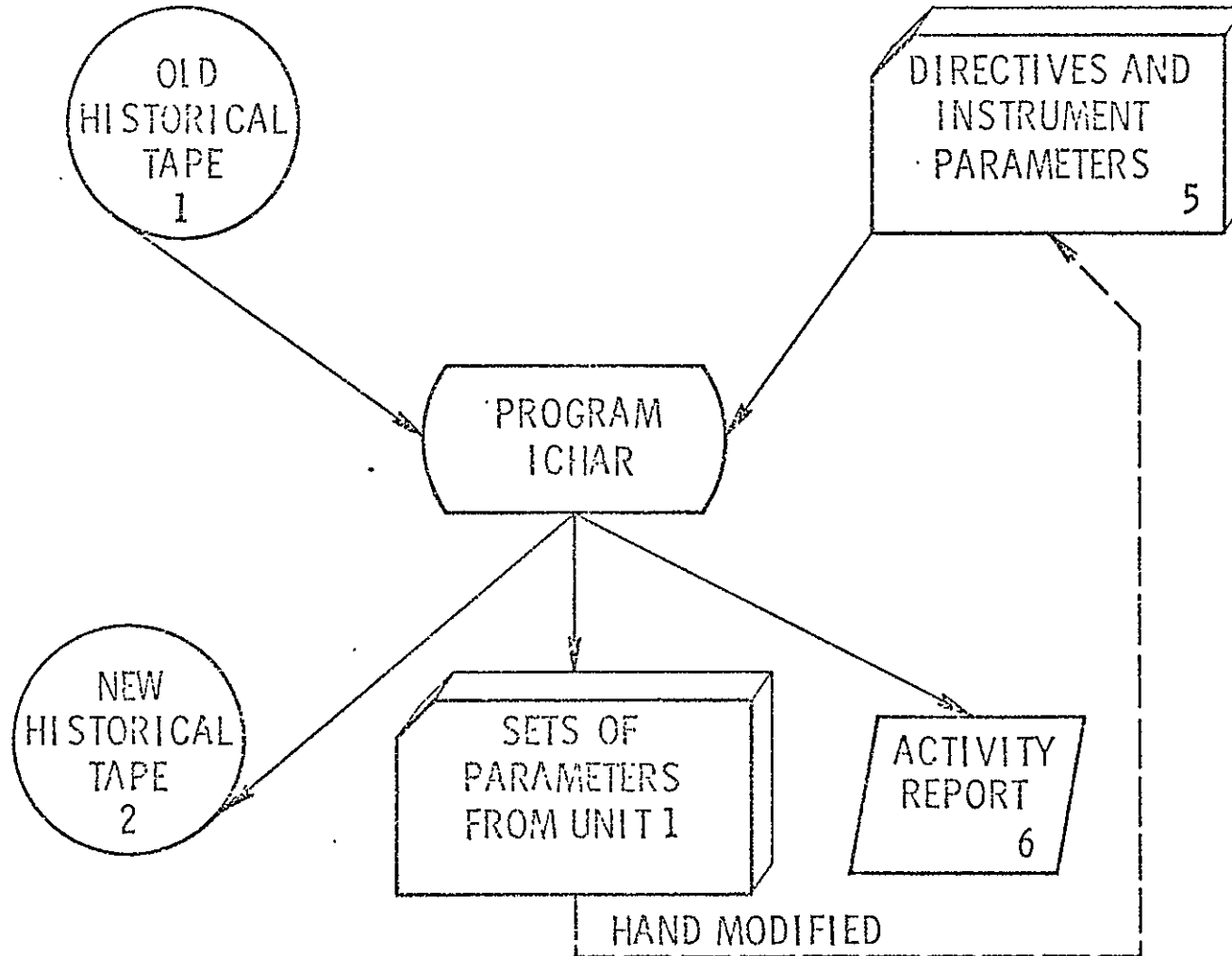


FIGURE 9. PERIPHERAL REQUIREMENTS FOR PROGRAM ICHAR

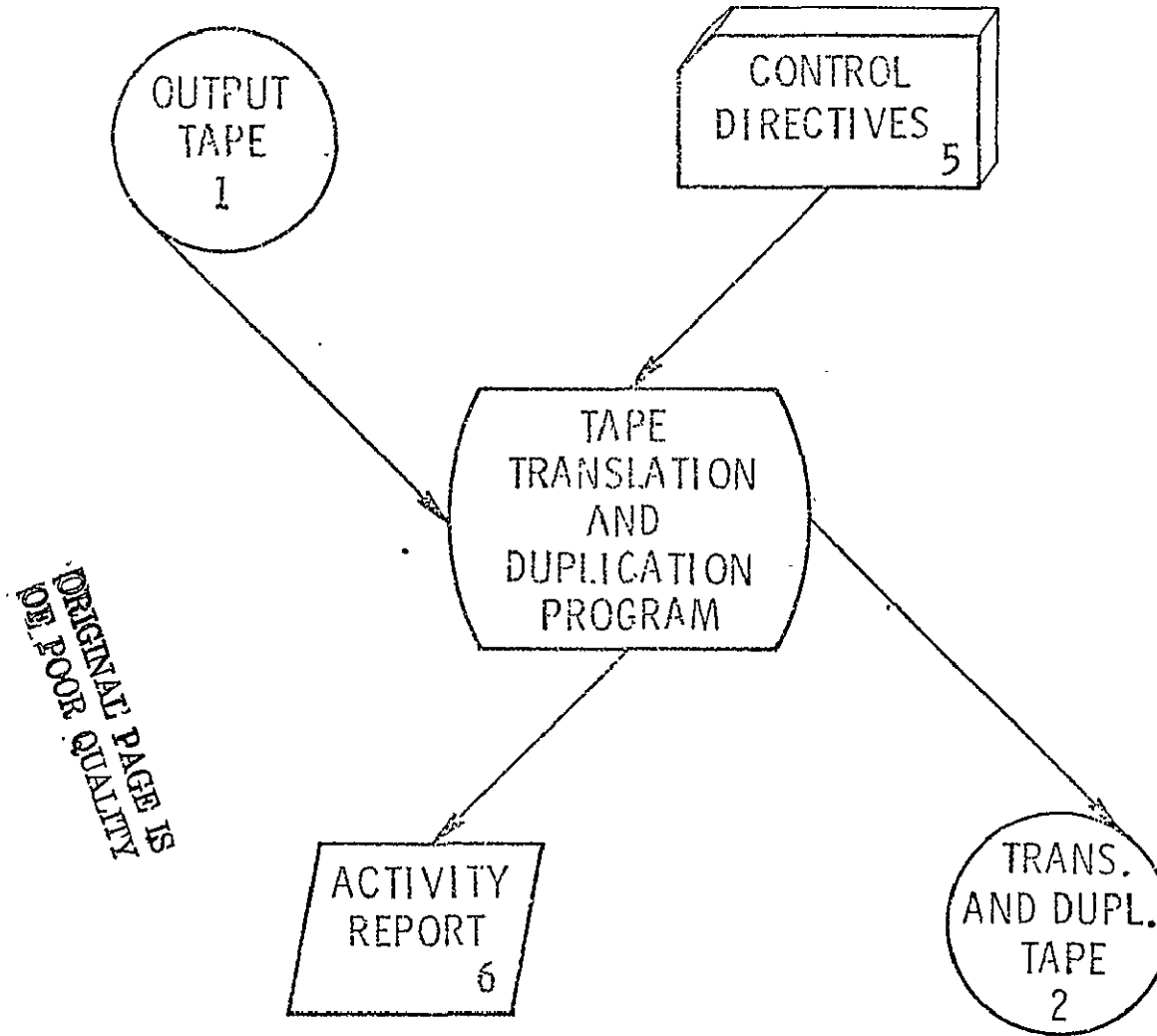


FIGURE 10. PERIPHERAL REQUIREMENTS FOR PROGRAM TDUPE

Program WIDTH is self sufficient when antenna pattern information is provided in the FUNCTION subroutine FUN. Presently functional representations of the main beam out to 6 degrees from boresight are provided. This routine may be replaced by a sampled version of the main beam. However, interpolation between sampled values must be provided since a double integration routine requires values dictated by the Gaussian Legendre quadrature technique.

Program GAIN requires both polarized and cross polarized power patterns. Functional representations of the polarized pattern is now given in FUN1 and the cross polarized pattern in FUN2. These may be replaced with sampled valued representation, if desired. Again, interpolation will be required.

For more specific information see Appendix E.

APPENDICES

APPENDIX A

CONVERSION PROGRAM

I. INTRODUCTION

The conversion program (CONVERT) applies many reduction algorithms to the raw RADSCAT data to provide the investigator with a set of comprehensive data products with which to interpret the scattering and emission characteristics of the scene represented by the data. CONVERT consists of the Control Section and the following subroutines:

- | | |
|-----------|------------|
| 1. IREAD | 7. CALIB |
| 2. READ1 | 8. RCONV |
| 3. WRITE2 | 9. ANGLE |
| 4. ABORT | 10. DOPCHK |
| 5. SEARCH | 11. SCONV |
| 6. CRUNCH | 12. THERMO |

The theory and design of these routines are treated in this appendix.

II. GENERAL OVERVIEW

The Control Section reads and interprets external directives. On the basis of the directive, the appropriate files are retrieved and presented to the processing subroutines. Subroutine SEARCH executes entry into the data records of the file in search of the appropriate calibration records. When found, the calibration information is extracted and averaged in subroutine CALIB. When sufficient calibration data cannot be found, the file is bypassed. The actual processing is performed by subroutine CRUNCH which applies various algorithms and calibration information to reduce the data. Many of the algorithms are embodied in subroutines, bearing descriptive names, which are called from CRUNCH.

Subroutine ANGLE computes the incident and cross-track angles using aircraft attitude and look angle information. Subroutine THERMO checks internal

receiver temperatures . The antenna temperature is computed in RCONV using the transfer function of the RADSCAT radiometer, the temperatures developed in THERMO and RAD calibration parameters . When scatterometer data is present, the maximum on-scale measurement is selected from the four SCAT channels with an in-line routine in CRUNCH . Using aircraft ground speed, DOPCHK computes the doppler shift in the scatterometer signal . The doppler filter gain is chosen accordingly . The scatterometer transfer function is applied in subroutine SCONV to compute the scatterometer normalized input power . An in-line routine in CRUNCH applies antenna inversion parameters to the input power to compute the normalized scattering coefficient .

When additional calibration records are encountered, the old calibration information is replaced by the new calibration information by subroutine CALIB .

Subroutine IREAD and READ1 perform the file read functions, whereas subroutine WRITE2 performs the write functions .

Subroutine ABORT is employed by the CONTROL Section to abort the job when an abnormal condition is encountered .

III. CONTROL SECTION

A. Theory and Design

The control section was developed to give the user a large amount of flexibility in the choice of the instruments characteristics and the files to be processed . As many or as few files of a particular type can be processed . Some files can be treated with one set of instrument characteristics and others with another . These features permit the user to (1) test a set instrument parameters, (2) group the files by type, (3) process different types of files with different instrument parameters, (4) etc . The flexibility in the choice of parameters was incorporated with the full realization that the instrument would undergo modifications .

Control of the program is executed by the choice of appropriate directives entered as data cards . The types of controls have already been discussed in Section II and III of the text and will not be treated here again . The method by which control cards are read and files are retrieved is shown in the logic diagram of Figure A-1 .

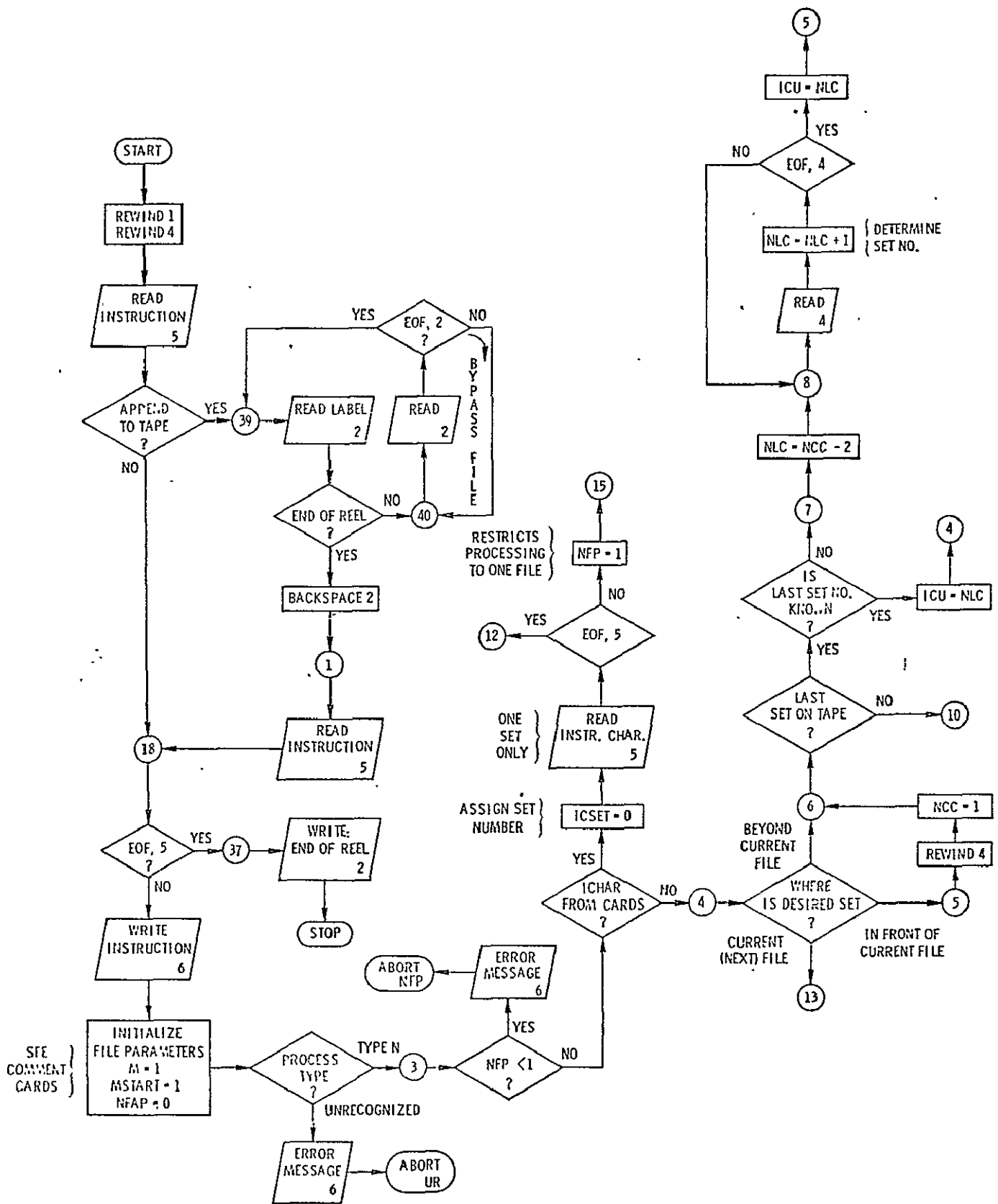
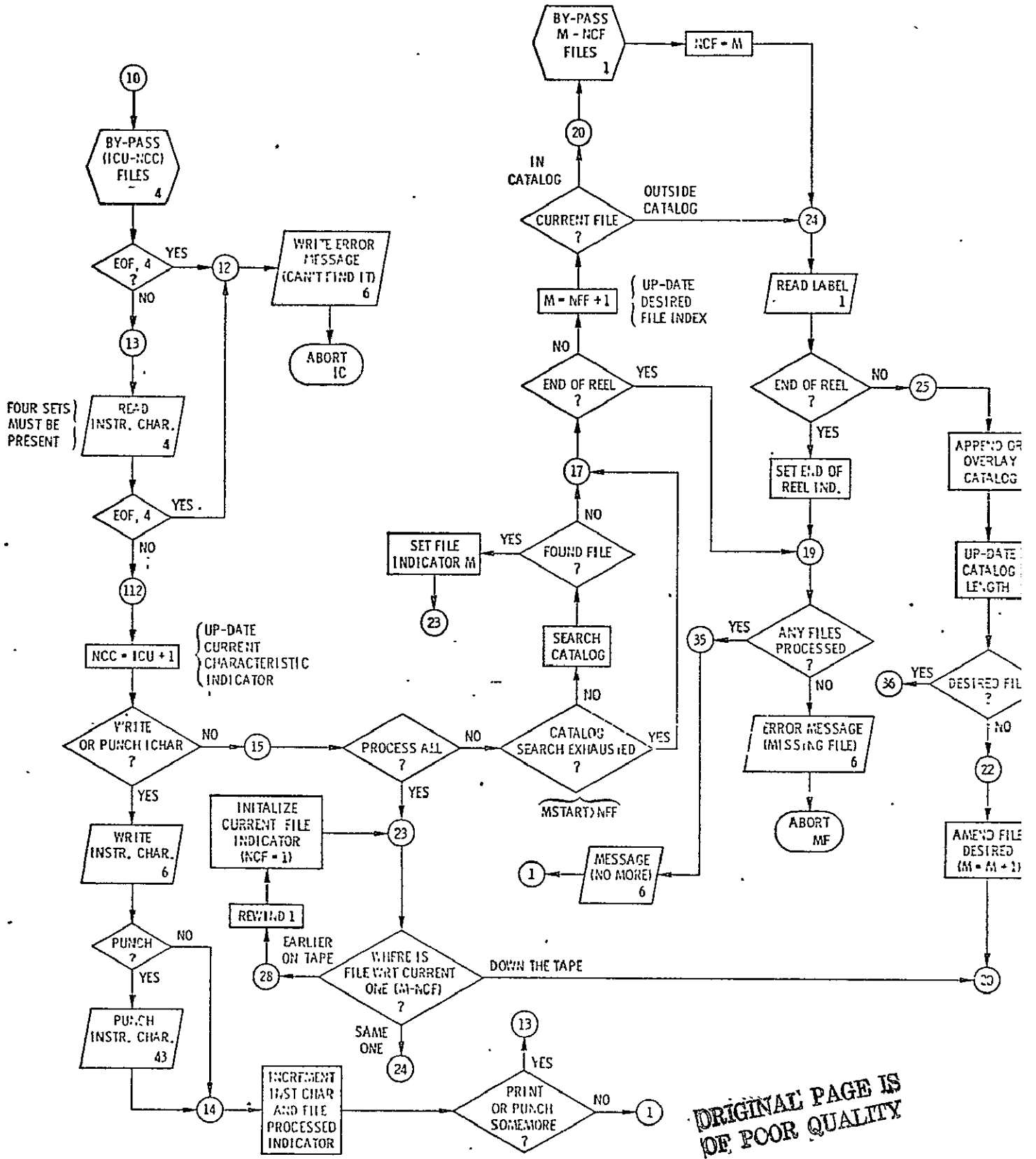


FIGURE A-1(a). DESCRIPTIVE LOGIC DIAGRAM FOR THE CONTROL SECTION

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FIGURE A-1. (b) DESCRIPTIVE LOGIC DIAGRAM FOR THE CONTROL SECTION

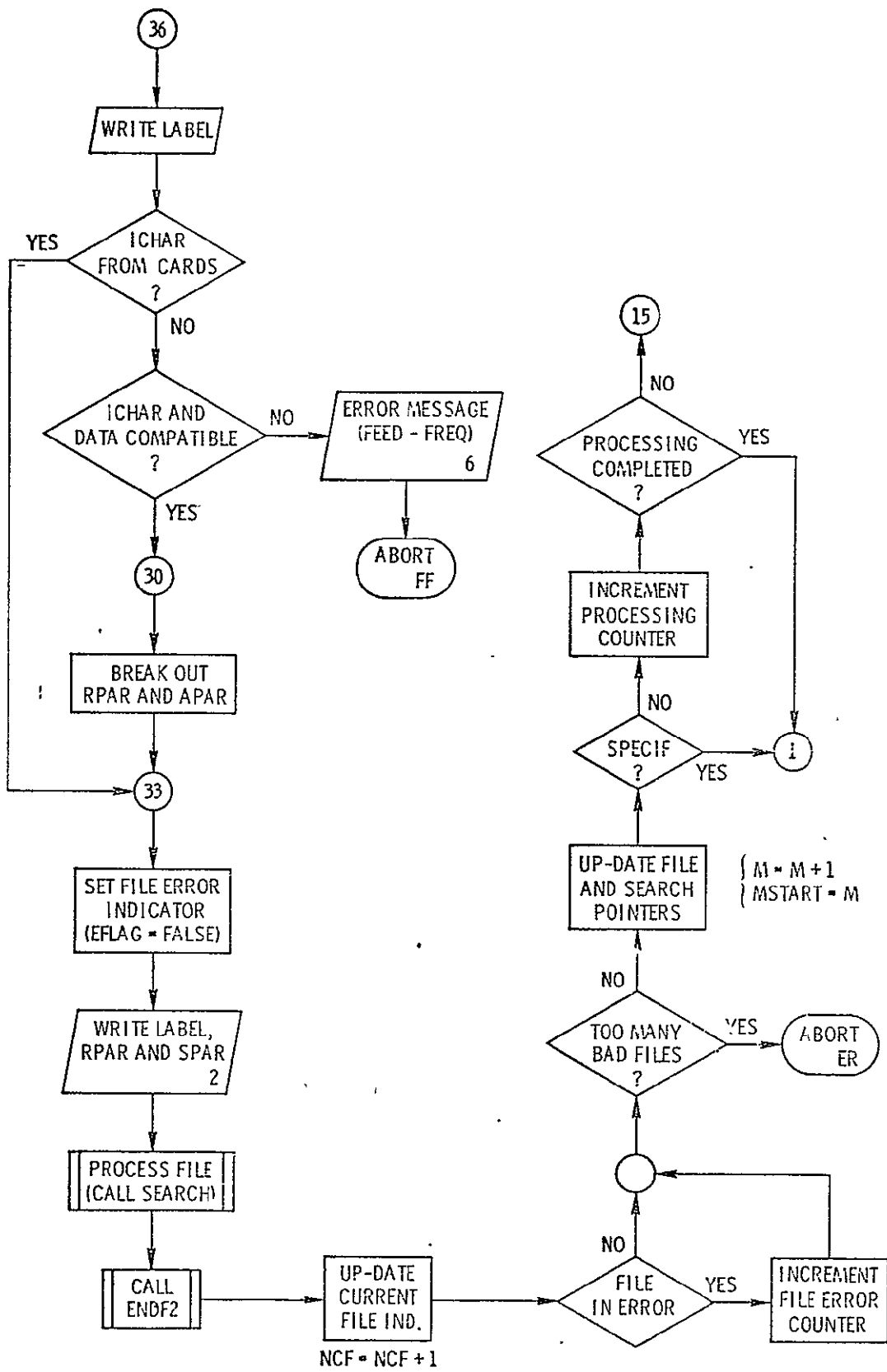


FIGURE A-1. (c) DESCRIPTIVE LOGIC DIAGRAM FOR THE CONTROL SECTION

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The numbers on the connecting points coincide with the statement numbers of the text shown in Figure A-2.

An instruction is read from the card reader. If it is POST, the files on an old output tape are bypassed in statements between 39 and 1 of the diagram. Another instruction is then read. The instruction is echo checked, file parameters are initialized and in the subsequent blocks of Figure A-1, the processing type is identified. Thereafter the specified instrument characteristic is read from unit 04 or 05. If the last set of characteristics on a file code 04 is desired and its file number is not known (ICU=999), the last file number is determined in statements between 6 and 5. If, on the other hand, they are to be read from cards (ICU=0), the appropriate action is taken and control is advanced to statement 15. If a specific file is designated, an appropriate number of files is bypassed until tape unit 04 is positioned on the correct file (see steps between statements 10 and 13).

If the set is to be punched or printed, the appropriate action is taken in steps preceding statement 14. If $NFP > 1$, $NFP - 1$ subsequent sets are also punched or printed. (See steps between 112 and 13). When completed, the next control card is read.

When the control card is a processing directive, the instrument characteristic tape will have been positioned to the correct file (set of parameters) or the set will have been entered from cards. Steps following 15 search for the appropriate data file. The search is governed by the type of directive. Bypassed files are cataloged in steps between 25 and 22. If the desired file is in the catalog and the current file is strictly in the catalog, the appropriate number of files are bypassed in steps between 22 and 24. If the file is beyond the catalog, the catalog is updated as the program advances the tape in search of the file.

Once found, the file label is listed and the appropriate subset of instrument parameters is withdrawn from tape if they weren't entered from the reader. SEARCH is then called to find the calibration data. SEARCH in turn calls CRUNCH to process the measurement records. Once completed control returns to the Control Section where additional files are sought or another directive is read.

B. Program Listing

The Control Section Listing is shown in Figures A-2(a) through A-2(e). The variables are defined in the listing.

```

PROGRAM CONVERT (INPUT,OUTPUT,PUNCH,TAPE1,TAPE2,TAPE4,TAPE5,
* TAPE5=INPUT,TAPE6=OUTPUT,TAPE43=PUNCH)
CCCCS  CCONVRSICK CONTROL SECTION
C
C      THIS PROGRAM WAS PREPARED BY
C
C      JOHN P. CLAASSEN
C      GLEN E. ELLIOTT
C
C      UNIVERSITY OF KANSAS CENTER FOR RESEARCH
C
C      PROGRAM DESCRIPTION.
C      FILE CODES USED.
C
C      01 -- INPUT RAW DATA.
C      02 -- OUTPUT PROCESSED DATA.
C      04 -- INPUT INSTRUMENT CHARACTERISTICS FILE.
C      05 -- SYSTEM INPUT - DIRECTIVE CARDS.
C      06 -- SYSTEM OUTPUT - PRINT LINES.
C      08 -- SCRATCH FILE - USED BY COMPLETION SECTION.
C      43 -- SYSTEM CLIPUT - PUNCHED CARDS.
C
C      VARIABLE NAMES USED.
C
C      LBLTBL #LABEL TABLE#. TABLE CONTAINING
C      LABEL INFORMATION (MISSION, FLIGHT, LINE, RUN) FOR ALL
C      DATA FILES BYPASSED SO FAR.
C
C      NWPST #NEXT POSITION#. ARRAY CONTAINING LABEL INFO (M,F,L,R)
C      OF NEXT FILE TO BE PROCESSED.
C
C      NCF #NUMBER OF CURRENT FILE#. POSITION POINTER FOR
C      FILE CODE 01.
C
C      NFF #NUMBER OF FINAL FILE#. INDEX OF LAST ENTRY IN
C      #LBLTBL# TABLE.
C
C      NSTART STARTING POINT FOR SEARCH IN #LBLTBL# TABLE.
C
C      MI #INPUT FILE TO USE. RELATIVE POSITION ON FILE CODE 01.
C
C      EOR1 #END OF REEL INDICATOR#. LOGICAL VARIABLE, SET TRUE
C      WHEN END OF REEL ON FILE CODE 01 IS DETECTED, INDICATING
C      #LBLTBL# TABLE IS COMPLETE.
C
C      IEOR INTEGER ARRAY CONTAINING WORDS #END OF REEL#.
C
C      IPTYPE INTEGER #PROCESSING TYPE# ARRAY, CONTAINING RECOGNIZED
C      PROCESSING TYPES.
C
C      JPTYPE INPUT DESIRED PROCESSING TYPE.
C
C      N INDEX OF POSITION OF #JPTYPE# IN #IPTYPE#.
C
C      ICU #INSTRUMENT CHARACTERISTICS TO USE#. NUMBER OF THE I.C.
C      SET TO BE USED. REFLECTS THE POSITION OF THE SET ON
C      FILE CODE 04.
C      0 INDICATES I.C. TO BE READ FROM CARDS (FC=05),
C      999 MEANS USE THE LAST SET ON FILE 04.
C
C      NCC #NUMBER OF CURRENT CHARACTERISTICS#. REFLECTS POSITION
C      FILE CODE 04.
C
C      NLC #NUMBER OF LAST CHARACTERISTIC#. USED WHEN ICU=999.
C      NLC=0 INDICATES THIS VALUE IS YET UNKNOWN.
C
C      RPAR #RADIOMETER PARAMETERS#.
C      SPAR #SCATERMETER PARAMETERS#.
C
C      PAK #PARAMETERS# ARRAY CONTAINING UP TO 4 SETS OF RACSCAT
C      INSTR PARAMETERS READ FROM FILE CODE 04 OR 05. RAC
C      PARAMETERS COMPOSE THE FIRST 75 ENTRIES OF PAK AND SCAT
C      PARAMETERS OCCUPY THE NEXT 85 ENTRIES IN EACH SUBSET.
C      THE APPROPRIATE SUBSET OF PARAMETERS IS SELECTED ON THE
C      BASIS OF FREQUENCY AND FEED.
C
C      NFP #NUMBER OF FILES TO PROCESS# USING THE PROCESSING TYPE
C      GIVEN BY #JPTYPE# AND DESCRIPTION IN #NWPST#.
C      NFP IS IGNORED IF JTYPL = SPECIF. IF ICU = 0,
C      NFP IS SET TO 1.
C
C      NFA #NUMBER OF FILES ALREADY PROCESSED#. COMPARED TO #NFP#
C      TO CHECK FOR TERMINATE CONDITION.

```

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FIGURE A-2. (a) LISTING OF CONTROL SECTION


```

C      LNPMOD  #LINE PRINTING MODULUS#. USED TO REDUCE OUTPUT          C0000102
C      FROM COMPUTATION SECTION. 0 IS TAKEN AS 1.                    CCCC0103
C      NERR    #NUMBER OF ERRORS#. NUMBER OF TIMES COMPUTATION SECTION C0000104
C      RETURNED ERROR CONDITION. NERR = 4 CAUSES ABORT.             C0000105
C      ERRFLG  BAD FILE ERROR FLAG.                                   C0000106
C
C      DIRECTIVE CARD USAGE
C
C      PROCESSING ----- MEANING -----
C      TYPE
C      ALL     START FROM FIRST OF INPUT FILE AND PROCESS WITHOUT    C0000107
C      REGARD TO LABEL INFORMATION.                                     C0000108
C
C      MISFLT  CHECK LABEL ONLY FOR CORRECT MISSION AND FLIGHT.      C0000109
C
C      FLTLIN  CHECK FOR CORRECT MISSION, FLIGHT, AND FLIGHT LINE.   C0000110
C
C      SPECIF  CHECK FOR MISSION, FLIGHT, FLT. LINE, AND RUN.        C0000111
C
C      PRINT   PRINT OUT VALUES OF INSTRUMENT CHARACTERISTICS.      C0000112
C
C      PUNCH   PRINT AND PUNCH I.C.#S.                                C0000113
C
C      POST    MAY BE USED AS THE FIRST PROCESSING TYPE. IF SO,      C0000114
C      THE PROGRAM WILL SPACE DOWN THE OUTPUT TAPE SEARCHING        C0000115
C      FOR THE END OF REEL. POST IS ILLEGAL EXCEPT ON THE        C0000116
C      FIRST DIRECTIVE CARD.                                         C0000117
C
C      DIRECTIVE CARD FORMAT.                                         C0000118
C
C      JPTYPE  MISS  FLT  LINE  RUN  LNPM  ICU  NFP
C      A6  4X  15  15  15  15  15  15
C
C      ALL     *      *      *      *      1      3      6
C      MISFLT  207  12  *      *      5      3      2
C      FLTLIN  207  12  1      *      10     3      5
C      SPECIF  207  12  1      2      1      3      1
C      PUNCH   *      *      *      *      *      4      6
C      PRINT   *      *      *      *      *      5      7
C      POST    *      *      *      *      *      *      *
C
C      * INDICATES FIELD IS IGNORED BY PROGRAM.                       C0000126
C
C      DIMENSION NWPST(4), LBLTBL(4,300), IEGR(2), RPAR(75), SPAR(85), C0000127
C      * PAR(160,4), IPTYPE(6), IDAT(3)                               CCCC0128
C      DIMENSION LBL(9)                                             C0000129
C      EQUIVALENCE (LBL(8),FREQ),(LBL(9),FEED)                    C0000130
C      EQUIVALENCE (IDAT(1),ID1),(ICAT(2),ID2),(ICAT(3),ID3)      C0000131
C      LOGICAL EGRI, ERRFLG                                         C0000132
C      DATA IEGR /10*END OF REE,1HL/                               C0000133
C      DATA IPTYPE/6HFLTLIN,6HMISFLT,6HSPECIF,3HALL,5HPRINT,5HPUNCH/
C      DATA IPUST/4HPOST/
C      DATA EGRI/.FALSE./, NLC,NCC/O,1/, NCF,NFF/1,0/, NERR/O/
C      REWIND 1
C      REWIND 4
C      READ(5,500) JPTYPE, NWPST, LNPMOD, ICU, NFP
C      IF(JPTYPE.NE.IPCST) GO TO 18
C      READ(2) LBL1,LBL2
C      IF(LBL1.NE.IEGR(1)) GO TO 40
C      IF(LBL2.NE.IEGR(2)) GO TO 40
C      BACKSPACE 2
C      GO TO 1
C      READ(2) REAL(2)
C      IF(EGRI) 39, 40
C
C      READ DIRECTIVES
C
C      READ(5,500) JPTYPE, NWPST, LNPMOD, ICU, NFP
C      FORMAT(A6,4X,7I5)
C      IF(LEUF,5) 37,41
C      WRITE(6,600) JPTYPE, NWPST, LNPMOD, ICU, NFP
C      FORMAT(1H1, //10X,17H CCNTRCL CARD IS ,
C      * A6,4X,7I5)
C
C      WHAT MANNER TO PROCESS
C
C      M=1
C      MSTART=1
C      NFP=0
C      DU 2 N=1,6
C      IF(JPTYPE.EQ.IPTYPE(N)) GO TO 3
C      WRITE(6,601)

```

FIGURE A-2. (b) LISTING OF CONTROL SECTION

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000126 001  FORMAT(10A,30H) IN CONTROLLED PROCESSING (J&M)
000126 CALL ABLRT(2HIC)
000130 3  IF(NFP.EQ.1) GO TO 59
000133 WRITE(6,61) NFP
000140 610  FORMAT(//10A,*NFP LT 1*,5X,*NFP = *,15//)
000140 CALL ABLRT(3HNF)

C
C          FIND INSTRUMENT CHAR.
C
000142 59  IF(ICL.NE.0) GO TO 4
C          READ FROM CARDS
000143      ICSET=0
000144      READ(5,4303) NUMBER, ID1, IC2, ID3, RPAR(1), RPAR(2), RPAR(3)
000166      IF(EOF,5) 12, 60
000171 60  WRITE(6,603) ICSET, ID1, ID2, ID3, RPAR(1), RPAR(2), RPAR(3)
000213      DO 61 J=4, 75, 7
000215          L=J+6
000217          IF(L.GT.75) L=75
000222      READ(5,4304) (RPAR(K), K=J, L)
000235      IF(EOF,5) 12, 61
000240 61  WRITE(6,604) (RPAR(K), K=J, L)
000255      READ(5,4303) ALPBEK, ID1, IC2, ID3, SPAR(1), SPAR(2), SPAR(3)
000277      IF(EOF,5) 12, 62
000302 62  WRITE(6,603) ICSET, ID1, IC2, ID3, SPAR(1), SPAR(2), SPAR(3)
000324      DO 63 J=4, 85, 7
000326          L=J+6
000330          IF(L.GT.85) L=85
000333      READ(5,4304) (SPAR(K), K=J, L)
000346      IF(EOF,5) 12, 63
000351 63  WRITE(6,604) (SPAR(K), K=J, L)
000366      NFP=1
000367      GO TO 15
000370 4  IF(ICU.NE.0) 5, 13, 6
000375 5  REWIND 4
000375      NCC=1
000376 6  IF(ICU.NE.999) GO TO 10
C          FIND LAST SET ON FILE.
000400      IF(NLC.EQ.0) GO TO 7
000401 +2  ICU=NLC
000403      GO TO 4
000403 7  NLC=NCC-2
000405 8  READ(4)
000410 9  NLC=NLC+1

000412      IF(EOF,4) 45, 8
000415 +3  ICU=NLC
000417      GO TO 5
C          POSITION TO THE SET
000417 10  NCL=NCC+1
000421      DO 11 I=NCL, ICL
000422      READ(4)
000425      IF(EOF,4) 12, 11
000430 11  CONTINUE
000433      GO TO 13
000433 12  WRITE(6,602)
000437 602  FORMAT(10X,34HNO SUCH INSTRUMENT CHARACTERISTICS)
000437      CALL ABLRT(2HIC)
C          READ THEM
000441 13  READ(4) ICSET, ID1, ID2, IC3, PAR
000456      IF(EOF,4) 12, 112
000461 112  NCC=ICU+1
000463      IF(N.LT.5) GO TO 15
C
C          WRITE (AND PUNCH) INST. CHAR.
C
000466      DO 55 I=1, 4
000467          WRITE(6,603) ICU, ID1, IC2, ID3, PAR(1, I), PAR(2, I), PAR(3, I)
000515 603  FORMAT(// * SET*, 15, * DATE*, 315, E15.4, 5X, A10, E15.4)
000515      DO 54 J=4, 75, 7
000517          L=J+6
000521          IF(L.GT.75) L=75
000524 54  WRITE(6,604) (PAR(K, I), K=J, L)
000543 604  FORMAT(7E15.4)
000543      WRITE(6,603) ICU, ID1, ID2, ID3, PAR(76, I), PAR(77, I), PAR(78, I)
000572      DO 55 J=75, 160, 7
000574          L=J+6
000576          IF(L.GT.160) L=160
000601 55  WRITE(6,604) (PAR(K, I), K=J, L)
000622 112  IF(N.NE.6) GO TO 14
000624      DO 57 I=1, 4
000626          LL=I
000627          WRITE(4,4303) ICU, ID1, ID2, ID3, PAR(1, I), PAR(2, I), PAR(3, I),
*          ICU, I, LL
000664 4303  FORMAT(4I5, 10X, E10.3, A10, E10.3, 12X, 12, 11, 15)
000664      DO 56 J=4, 75, 7
000666          LL=LL+1
000670          L=J+6

```

```

CCCC172
C000173
C000174

CCCC175
0000176
C000177
C000178
C000179
C000180
0000181
CC00182
0000183
C000184
C000185
C000186
C000187
0000188
C000189
0000190
CC00191
0000192
C000193
CC00194
C000195
CC00196
0000197
C000198
C000199
0000200
0000201
C000202
C000203
C000204
CC00205
0000206
CC00207
0000208
0000209
C000210
C000211

C000212
0000213
C000214
C000215
C000216
C000217
CC00218
0000219
C000220

0000221
C000222
0000223
C000224
C000225
CC00226
0000227
C000228
C000229
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C000231
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C000252
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FIGURE A-2. (c) LISTING OF CONTROL SECTION

```

00072 56 WRITE(43,4304)(PAR(K,1),K=J,L),ICU,1,LL C0000254
000715 4304 (ORCAT(1E10.3,2X,12,11,15) 00000255
000715 LL=LL+1 C0000256
000717 WRITE(43,4303) ICU,ICAT,PAR(76,1),PAR(77,1),PAR(78,1), C0000257
* ICU,1,LL C0000258
000747 DU 57 J=79,100,7 C0000259
000751 LL=LL+1 C0000260
000753 L=J+6 C0000261
000755 57 WRITE(43,4304)(PAR(K,1),K=J,L),ICU,1,LL C0000262
001002 14 ICU=ICU+1 C0000263
001004 NFAP=NFAP+1 C0000264
001005 IF(NFAP.LI.NFP) GO TO 13 C0000265
001007 GO TO 1 C0000266
C C0000267
C FIND THE DATA RECORD. C0000268
C C0000269
001010 15 IF(N.EQ.4) GO TO 23 C0000270
001012 IF(MSTART.CT.NFF) GO TO 17 C0000271
C C0000272
C SEE IF WE'VE BEEN BY IT ALREADY. C0000273
C C0000274
001016 DU 16 M=MSTART,NFF C0000275
001017 IF(NWPST(1).NE.LBLTBL(1,M)) GO TO 16 C0000276
001022 IF(NWPST(2).NE.LBLTBL(2,M)) GO TO 16 C0000277
001025 IF(N.FU.2) GO TO 23 C0000278
001027 IF(NWPST(3).NE.LBLTBL(3,M)) GO TO 16 C0000279
001032 IF(N.FU.1) GO TO 23 C0000280
001033 IF(NWPST(4).NE.LBLTBL(4,M)) GO TO 16 C0000281
001036 GO TO 23 C0000282
001041 16 CONTINUE C0000283
17 IF(EUR) GO TO 19 C0000284
C C0000285
C GOSS IT'S FURTHER DOWN THE TAPE. C0000286
C C0000287
001043 M=NFF+1 C0000288
001045 IF(NCF.GT.NFF) GO TO 24 C0000289
001050 20 M1=M-1 C0000290
001052 DU 27 I=NCF,M1 C0000291
001054 26 READ(1) C0000292
001057 IF(EUF,1) 27, 26 C0000293
001062 27 CONTINUE C0000294
001065 NCF=M C0000295
001066 24 READ(1) LBL C0000296

001073 IF(LBL(1).NE.IEGR(1)) GO TO 25 C0000297
001075 IF(LBL(2).NE.IEGR(2)) GO TO 25 C0000298
001077 EOKI=.TRUE. C0000299
001100 19 IF(NFAP.NE.0) GO TO 35 C0000300
001101 WRITE(6,606) C0000301
001105 606 FORMAT (10X,19HNO SUCH DATA RECORD) C0000302
001105 CALL ABORT(2HMF) C0000303
001107 35 WRITE(6,607) NFAP C0000304
001115 607 FORMAT(10X,13,32H FILES FOUND. CAN FIND NO MORE.) C0000305
001115 GO TO 1 C0000306
001116 LBLTBL(1,NCF)=LBL(1) C0000307
001121 LBLTBL(2,NCF)=LBL(2) C0000308
001124 LBLTBL(3,NCF)=LBL(6) C0000309
001126 LBLTBL(4,NCF)=LBL(7) C0000310
001130 NFF=MAX0(NFF,NCF) C0000311
001133 IF(N.EQ.4) GO TO 36 C0000312
001135 IF(NWPST(1).NE.LBLTBL(1,M)) GO TO 22 C0000313
001140 IF(NWPST(2).NE.LBLTBL(2,M)) GO TO 22 C0000314
001143 IF(N.EQ.2) GO TO 36 C0000315
001144 IF(NWPST(3).NE.LBLTBL(3,M)) GO TO 22 C0000316
001147 IF(N.EQ.1) GO TO 36 C0000317
001150 IF(NWPST(4).NE.LBLTBL(4,M)) GO TO 22 C0000318
001153 GO TO 36 C0000319
001153 22 M=M+1 C0000320
001155 GO TO 20 C0000321
001155 23 IF(M-NCF) 28, 24, 20 C0000322
001160 28 REWIND 1 C0000323
001162 NCF=1 C0000324
001163 GO TO 23 C0000325
C FOUND IT. IT'S THIS ONE. C0000326
001164 36 WRITE(6,608) LBL, ICSET, ID1, ID2, ID3 C0000327
001202 608 FORMAT(1H1,51X,17HCONVERSION REPORT, C0000328
* //10X,8HMISSION-,13,9H FLIGHT-,13,
* 7H DATE-,213,15,2X,11H FLT LINE-,1X, 15,6H RUN-,13,
* 13H FREQUENCY-,F5.1,7H FEED-,2X,A6,
* 6F IPAR=,12,313////)
001202 IF(ICU.EQ.0) GO TO 33 C0000333
C GET CORRECT INST. CHAR. C0000334
001203 DU 29 K=1,4 C0000335
001205 IF(AUS(FREC-PAK(K)/1.0.E9).GT.1.0) GO TO 29 C0000336
001215 IF(ILED.EQ.PAR(2,K)) GO TO 30 C0000337
001221 29 CONTINUE C0000338
001223 WRITE(6,605) FREU, FEED C0000339

```

FIGURE A-2. (d) LISTING OF CONTROL SECTION

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001233	605	FORMAT (10X,17H-KL SUCH FREQ-FEED,F10.5,1X,A10)	C0000340
001233		CALL ABORT(2HFF)	C0000341
001235	30	DO 31 I=1,75	C0000342
001237	31	RPAR(I)=PAR(I,K)	C0000343
001246		DO 32 I=1,65	C0000344
001247	32	SPAR(I)=PAR(I+75,K)	C0000345
	C	CALL COMPUTATION SECTION.	C0000346
001256	33	ERRFLG=.FALSE.	C0000347
	C	LABEL OUTPUT TAPE	C0000348
001257		WRITE(2) LCL	C0000349
001264		WRITE(2) ICSET, ID1, ID2, ID3, RPAR, SPAR	C0000350
001303		CALL SEARCH(SPAR,RPAR,LNPMOD,ERRFLG)	C0000351
001306		CALL ENDF2	C0000352
001307		NCF=NCF+1	C0000353
001311		IF(ERRFLG) NERR=NERR+1	C0000354
001313		IF(NERR.GT.3) CALL ABORT(2HER)	C0000355
001317		M=M+1	C0000356
001321		MSTART=M	C0000357
	C	MORE FILES TO PROCESS	C0000358
001322		IF(N.EQ.3) GO TO 1	C0000359
001324		NFAP=NFAP+1	C0000360
001325		IF(NFAP.GE.NFP) GO TO 1	C0000361
001327		GO TO 15	C0000362
	C		C0000363
	C	TERMINATIONS.	C0000364
001330	37	WRITE(2) IECR, (I,I=3,9)	C0000365
001342		WRITE(6, /00)	
001346	700	FORMAT(1H1,///11X,10(1H*),10HNORMAL TERMINATION,10(1H*))	C0000366
001346		STOP	C0000367
001350		ENC	

FIGURE A-2. (e) LISTING OF CONTROL SECTION

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C. Peripheral Requirements

UNIT 01	RADSCAT Raw Data Tape
UNIT 02	Output Tape
UNIT 04	Characteristics Tape
UNIT 05	Card Reader
UNIT 06	Printer
UNIT 08	Scratch Unit (Preferably Disc)
UNIT 43	Punch

IV. SUBROUTINES

A. Subroutine Search

1. Theory and Design

This routine serves as an entry and exit point for the selected file. One of its primary purposes is to find calibration data of both kinds. It anticipates that both NORMAL and BASELINE calibrations are in the opening records of the file. If this is the case the processing of the remainder of the file is given to CRUNCH. Otherwise, a search for the missing calibrations is conducted deeper into the file. The bypassed files are stored on a scratch unit (08) for subsequent processing. When both types of calibrations are found, the bypassed records on file code 08 are processed by CRUNCH and the remainder of the records on file code 01 are also.

If the return from CRUNCH is without an error flag, control is simply returned to the Control Section. If not, an error message is given and the remainder of the file bypassed before returning.

See Figure A-3 for a descriptive logic diagram of SEARCH.

2. Program Listing and Variables

The listing for SEARCH is shown in Figure A-4(a) and A-4(b). The definitions of the variables are given in Table A-1. The entries in DATA were defined in Section III B.

Table A-1 Definition of Variable Used in SEARCH

DATA	=	Vector Containing Raw RADSCAT DATA
IDATA	=	Integer Equivalent of DATA
SCAL	=	SCAT Calibration Vector (Channels 1-4)


```

SUBROUTINE SEARCH(SPAR,RPAR,LNPMOD,EFLAG)                                00000438
CSEARCH      CALIB SEARCH ROUTINE                                    00000439
C      SUBROUTINE SEARCH(SPAR,RPAR,LNPMOD,EFLAG)                    00000440
C      THIS PROGRAM WAS PREPARED BY                                00000441
C      JOHN P. CLAASSEN                                           00000442
C      GLEN E. ELLIOTT                                           00000443
C      UNIVERSITY OF KANSAS CENTER FOR RESEARCH                   00000444
C      THIS SUBROUTINE EXECUTES ENTRY INTO THE CONTENTS OF THE    00000445
C      FILE AND SEEKS CALIBRATION INFORMATION, BOTH NORMAL AND   00000446
C      BASELINE. THE PROGRAM ANTICIPATES THAT BOTH TYPES OF     00000447
C      CALIBRATIONS ARE PRESENT IN THE INITIAL RECORDS. HOWEVER 00000448
C      WHEN THIS NOT THE CASE, THE FILE IS SEARCHED UNTIL BOTH   00000449
C      TYPES ARE FOUND. BY-PASSED RECORDS ARE STORED ON UNIT 8   00000450
C      SUBSEQUENT PROCESSING.                                     00000451
C      DIMENSION DATA(50), IDATA(50),                            00000452
C      SPAR(85), RPAR(15), SCAL(4), RCAL(2)                       00000453
C      COMMON /INPLT/ EGF1, DATA                                 00000454
C      EQUIVALENCE (DATA(1),ICATA(1))                            00000455
C      LOGICAL EFLAG, ECF1, EOF8                                 00000456
C      LOGICAL NORMAL, BASE                                      00000457
C      READ DATA RECORD FROM TAPE UNIT 1                         00000458
C      IPASS=0                                                    00000459
C      WRITE(6,66)                                                00000460
C      60 FORMAT(12F RECCRD NO.*,13X,7HMESSACE,19X,1H*,20X,      00000461
C      * 10HPARAMETERS//)                                        00000462
C      CALL READ1                                                00000463
C      IF(EOF1) GO TO 130                                         00000464
C      CHECK IF RECORD IS CALIB DATA                             00000465
C      10 IF (IDATA(4) .EQ. 0 .OR. ICATA(4) .EQ. 2) GO TO 50     00000466
C      PREPARE DISC FOR BY-PASSED RECORDS                       00000467
C      REWIND 8                                                  00000468
C      IPASS=1                                                    00000469
C      ERROR MESSAGE                                             00000470
C      WRITE(6,26) ICATA(4)                                       00000471
C      20 FORMAT(5X,1H*,5X,27HFILE STRUCTURE INCOMPATIBLE,7X,1H*,5X, 00000472
C      * 33HFIRST RECORD NOT CALIBRATION DATA,5X, 6HMODE= ,13/) 00000473
C      WRITE(6,120) DATA .                                       00000474
C      SEARCH FOR CALIBRATION RECORD                             00000475
C      30 WRITE(8) DATA                                           00000476
C      35 CALL READ1                                               00000477
C      IF(EOF1) GO TO 100                                         00000478
C      CHECK IF CALIB DATA                                     00000479
C      40 IF (ICATA(4) .NE. 0 .AND. IDATA(4) .NE. 2) GO TO 30   00000480
C      50 ICOUNT=0                                                00000481
C      IL=0                                                        00000482
C      WITHDRAW CALIBRATION INFORMATION                          00000483
C      NORMAL = .FALSE.                                          00000484
C      BASE = .FALSE.                                             00000485
C      65 CALL CALIE(SCAL,RCAL,RPAR,NORMAL,BASE)                  00000486
C      IF (.NOT. NORMAL .AND. .NOT. BASE) GO TO 35               00000487
C      IF (.NOT. NORMAL) GO TO 160                                00000488
C      IF (.NOT. BASE) GO TO 180                                  00000489
C      IF(IPASS.EQ.0) GO TO 70                                     00000490
C      ENDFILE c                                                 00000491
C      REWIND 8                                                  00000492
C      CALL CRUNCH(8,LATA, IDATA, IL, ICOUNT, SCAL, RCAL,         00000493
C      * SPAR, RPAR, LNPMOD, EFLAG, EOF8)                         00000494
C      70 IF(EOF1) GO TO 80                                       00000495
C      CALL CRUNCH(1, DATA, ICATA, IL, ICOUNT, SCAL, RCAL,      00000496
C      * SPAR, RPAR, LNPMOD, EFLAG, EOF1)                         00000497
C      80 IF(EFLAG) GO TO 190                                     00000498
C      NORMAL TERMINATION MESSAGE                                00000499
C      90 WRITE (6,90) IL, ICOUNT                                00000500

```

FIGURE A-4. (a) SOURCE LISTING FOR SUBROUTINE SEARCH

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000166 90  FORMAT (10,5X,1H*,2X,36HCCOMPLETED COMPLETIONS FOR THIS FILE,
*          1X,1H*,5X,10HTHERE WERE,15,
*          24H WARNING FLAGS GENERATED)
000166      RETURN
      C
      C          ERRCR MESSAGE
      C
000167 100  WRITE (6,110)
000173 110  FORMAT (11X,1H*,5X,27HFILE STRUCTURE INCOMPATIBLE,7X,1H*,5X,
*          25HUNABLE TO FIND CALIB DATA)
000173      WRITE(6,120) DATA
000201 120  FCKMAT(/10(5022//))
      C
      C          ABORT FILE AND SEEK NEXT INSTRUCTION
      C
000201      EFLAG=.TRUE.
000204      RETURN
000205 130  WRITE(6,140)
000211 140  FORMAT(11H EMPTY FILE)
000211      LFLAG=.TRUE.
000214      RETURN
      C
      C          SEARCH FOR MISSING CALIB DATA
      C
000215 150  WRITE(8) DATA
000222 160  CALL READ1
000223      IF(EOF1) GO TC 100
000227 165  IF (ICATA(4) .NE. 0) GO TO 150
000230      GO TO 65
000231 170  WRITE (8) DATA
000236 180  CALL READ1
000237      IF(EOF1) GO TC 100
000243 185  IF (ICATA(4) .NE. 2) GO TC 170
000245      GO TO 65
000246 190  WRITE(6,195)
000252 195  FORMAT(///11X,1H*,5X,28H EXCESSIVE NO. OF BAD RECORDS,6X,1H*)
000252      IF(EOF1) RETURN
000257 200  READ(1)
000262      IF(EOF,1) 250,200
000270 250  RETURN
000271      END

```

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FIGURE A-4. (b) SOURCE LISTING FOR SUBROUTINE SEARCH

(Continued)

Table A-1 Definition of Variable Used in SEARCH entries in DATA

RCAL	=	RAD Calibrations (NORMAL, BASE)
EOF1	=	End of File for Unit 1
EOF8	=	End of File for Unit 8
EFLAG	=	File Error Flag
IPASS	=	Flag for Data on Unit 8
NORMAL	=	Flag for Normal RAD Cals
BASE	=	Flag for Baseline RAD Cals
ICOUNT	=	RADSCAT Performance Error Counter
IL	=	Record Counter

B. Subroutine CRUNCH

1. Theory and Design

The reduction algorithms are applied in or from subroutine CRUNCH. The routine was designed to process RADSCAT data whether it consisted of radiometer measurements (RAD only mode) or both scatterometer and radiometer measurements (alternating angles, fixed angle, or short SCAT modes). In processing the records on an independent basis, there is a tacit assumption that coupling between polarization is negligible. It was also necessary to equip the routine with the ability to read records from file code 01 (raw data tape) or file code 08 (scratch unit). A description of the internal operation of CRUNCH is shown in the logic diagram of Figure A-5.

In the opening steps of CRUNCH the data record is extracted from the file and verified by an in-line routine. The first sixteen entries in the data record are checked for type and magnitude. If an invalid entry is present, an error message identifying the bad entry is given and a bad record counter is incremented (NGR). If more than 10 bad records are encountered, an error flag (EFLAG) is set and control is returned to SEARCH. If not, the next record is read (statement 100) and the process repeated. If the record is valid, it is further examined to determine if it is a calibration record. If it is, CALIB is called (statement 220) to extract and average the calibrations. The next record is then read and the process

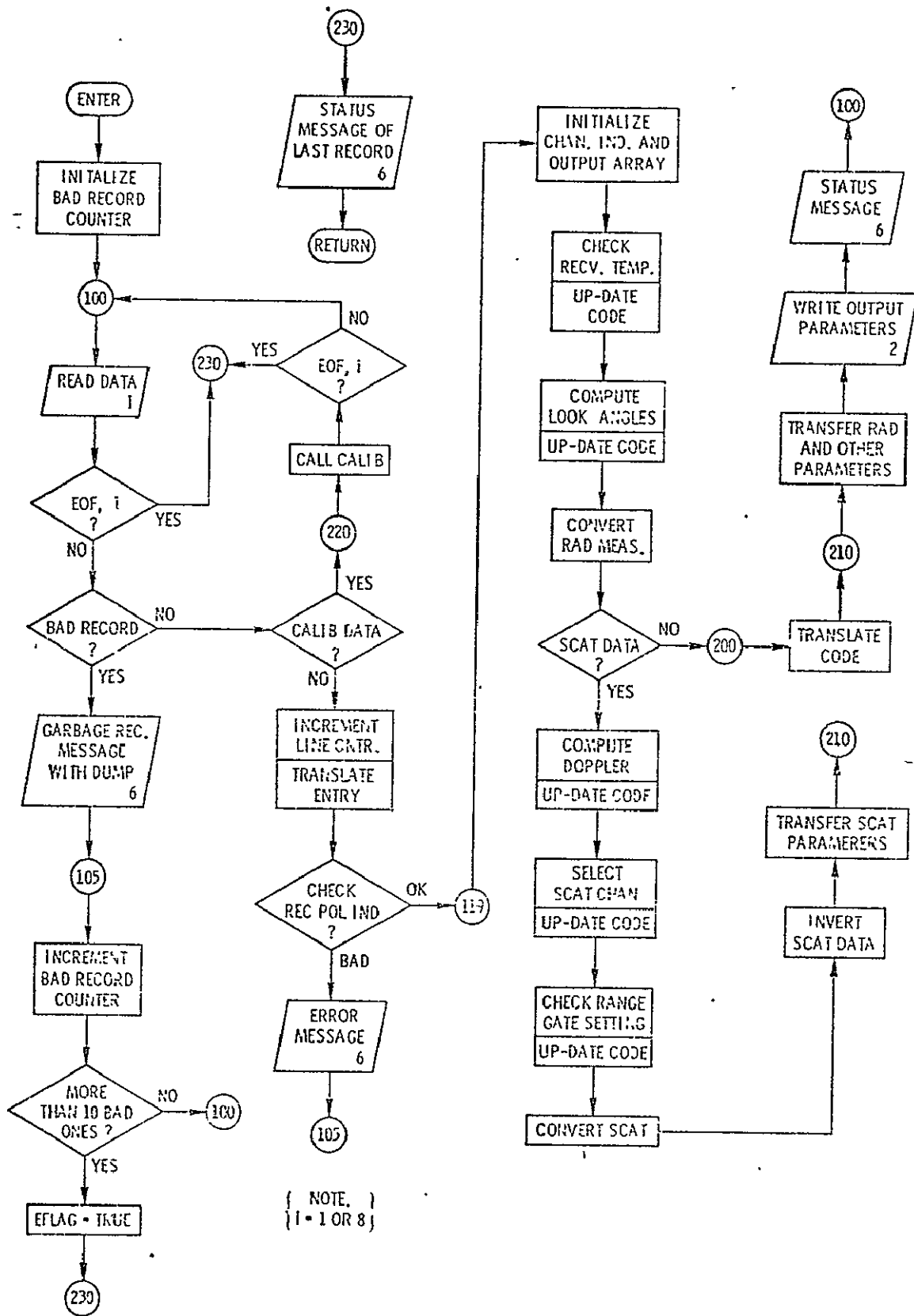


FIGURE A-5. DESCRIPTIVE LOGIC DIAGRAM FOR SUBROUTINE CRUNCH

repeated. If it is not calibration data, the mode entry is translated and the SCAT and RAD receiver polarization are checked for agreement when the instrument is not in the "RAD only" mode. If they disagree the record is declared invalid and treated as a bad record.* If the measurement occurred in the "RAD only" mode or the polarization agree, the record is then processed in the steps following and including statement number 119.

Initially the record counter is incremented, the SCAT channel indicator initialized and the output array cleared. CRUNCH then calls THERMO to compute and check receiver temperatures. An interpretation code is updated after which subroutine ANGLE is called. ANGLE computes the incident and cross-track angles and again the interpretational code is updated. Subroutine RCONV (radiometer convert) is called to compute the antenna temperature. If no scatterometer data is present, control advances to statement 200 where the computed results are transferred to the output array. Otherwise when SCAT data is present, DOPCHK is called to compute the doppler shift and set the doppler filter band index. The interpretational code is then updated.

In the following statements (up to number 170), the maximum on-scale SCAT measurement is selected from the four output channels (DATA(8) through DATA(11)). To select the appropriate channel output, the channels are tested for an output in excess of a value that would cause the output to saturate on the next higher sensitivity channel. Note that channel 1 (DATA(8)) is least sensitive whereas channel 4 (DATA (11)) is most sensitive. The selected measurement is stored in DATA(8) after scaling it with some channel dependent parameters. If the SCAT return fell below or above the channels, an interpretational flag is set in statements between 170 and 175.

Following the channel selection, the range gate setting is compared with the aircraft altitude. If the altitude is not within 300 feet of the range gate setting, an interpretation flag is set.

Subroutine SCONV (SCAT convert) is then called to compute the normalized input power. Once computed, the scatterometer measurement is inverted for antenna pattern effects with an in-line statement (number 190). The antenna inversion is based on the notion of an equivalent pencil beam replacing the actual main beam

*The implication is that the instrument didn't operate correctly.

antenna pattern. Computer simulations have shown that the method is extremely accurate (errors ≤ 0.1 dB) for narrow beam antennas. Briefly the equivalent beam-width notion is based on the fact that the normalized input power

$$I(\theta_0) = \iint \frac{P^2(\theta, \phi) \sigma^0(\theta') dA}{R^4}$$

where

- = normalized scattering coefficient
- = radar range to elemental area dA
- = normalized antenna pattern
- = elemental area

can be approximated by an algebraic expression through the following considerations. For narrow beam antenna

$$I(\theta_0) = \iint \frac{P^2(\theta, \phi) \sigma^0(\theta') \sin \theta R^2 d\theta d\phi}{R^4 (\cos \theta')}$$

where $\cos \theta'$ is a projection factor, may be approximated by

$$I(\theta_0) \cong \frac{\sigma^0(\theta_0)}{R^2 (\cos \theta_0)} \iint P^2(\theta, \phi) \sin \theta d\theta d\phi$$

The integral may be computed numerically from a description of the antenna pattern and equated to the effect produced by a pencil beam of width θ_{eq} , i.e.,

$$\begin{aligned} \iint P^2(\theta, \phi) \sin \theta d\theta d\phi &= \int_0^{2\pi} \int_0^{\theta_{eq}/2} \sin \theta d\theta d\phi \\ &\cong \frac{\pi \theta_{eq}^2}{4} \end{aligned}$$

Therefore the normalized scattering coefficient is given by

$$\sigma^{\circ}(\theta_0) = \frac{4 I(\theta_0) R^2 \cos \theta_0}{\pi \theta_{eq}^2}$$

But note that $R = h / \cos \theta_0$ so that

$$\sigma^{\circ}(\theta_0) = \frac{4 I(\theta_0) h^2}{\pi \theta_{eq}^2 \cos \theta_0}$$

where h is the aircraft altitude. The entry θ_{eq} is computed by the engineering routine WIDTH described in Appendix E as well as Section IV F of the text.

The scatterometer and radiometer products are then stored in the output array and the output array is transferred to the output tape (unit 02).

The next data record is then read (statement 100) and the sequence of events repeated. If an end of file is encountered on the input tape, control is returned to SEARCH.

2. Program Listing and Variables

The source listing for CRUNCH is shown in Figures A-6(a) through A-6(d). The variables employed in CRUNCH are defined in Table A-2. Entries in SPAR

Table A-2 Definition of Variables Used in CRUNCH

DATA	=	Input Raw Data Vector
IDATA	=	Integer Equivalent of DATA
SPAR	=	SCAT Parameters
RPAR	=	RAD Parameter
SCAL	=	SCAT Calibration Vector (Channel 1 to 4)
RCAL	=	RAD Calibration Vector (Normal and Base)
VERI	=	Data Validation Parameters
IVERI	=	Integer Equivalent of VERI
EOFIFC	=	End of File Indicator for FC 01
EFLAG	=	File Verification Indicator
IL	=	Record Count

```

SUBROUTINE CRUNCH(IIC,DATA,ICDATA,IL,ICOUNT,SCAL,RCAL,
* SPAR,RPAR,LNFMLD,EFLAG,EOFIFC)
C CRUNCH
C
C THIS PROGRAM WAS PREPARED BY
C
C JOHN P. CLAASSEN
C GLEN E. ELLIOTT
C
C UNIVERSITY OF KANSAS CENTER FOR RESEARCH
C
C THE PRIMARY FUNCTION OF THIS ROUTINE IS TO CONVERT SCATTER-
C METER AND RADIOMETER OUTPUT VOLTAGES INTO THEIR RESPECTIVE
C NORMALIZED INPUT POWERS. THE CONVERTED SCAT DATA IS
C SUBSEQUENTLY INVERTED FOR THE SCATTERING COEFFICIENT.
C PRIMARY COMPUTATIONS ARE PERFORMED IN SUBROUTINE CRUNCH
C WHICH CALLS A NUMBER OF IMPORTANT ROUTINES. FROM CRUNCH
C INTERNAL CALIBRATION INFORMATION IS WITHDRAWN FROM THE DATA
C RECORDS AND APPLIED TO SUBSEQUENT MEASUREMENTS. THE VIEW
C ANGLE IS CORRECTED FOR AIRCRAFT ORIENTATION. A WARNING FLAG
C IS GIVEN WHEN THE RCLL ANGLE CAUSES EXCESSIVE DEPOLARIZATION.
C A FLAG IS ALSO GENERATED WHEN THE DOPPLER SHIFT EXCEEDS
C THE DOPPLER FILTER BANDWIDTH. THERMISTOR DATA IS
C CHECKED FOR REASONABLE TEMPERATURES AND TEMPERATURES OF
C CRITICAL COMPONENTS ARE WITHDRAWN FOR SUBSEQUENT USE IN
C CONVERTING RADIOMETER MEASUREMENTS.
C
000017 DIMENSION DATA(50), ICATA(50), SPAR(85), RPAR(75), SCAL(4),
* RCAL(2), ARRAY(20), IARRAY(20), ALT(4)
000017 DIMENSION ICHG(3)
000017 DIMENSION VERR(15,2), IVERI(15,2)
000017 DIMENSION VMAX(15), VMIN(15), IVMAX(15), IVMIN(15)
000017 EQUIVALENCE (VMAX(1),IVMAX(1)),(VMIN(1),IVMIN(1))
000017 EQUIVALENCE (VERI(1,1),VMIN(1)),(VERI(1,2),VMAX(1))
000017 EQUIVALENCE (VERI(1,1),IVERI(1,1))
000017 EQUIVALENCE (ARRAY(1),IARRAY(1))
000017 LOGICAL EOFIFC
000017 DATA (IVMIN(I),I=1,6)/1,0,0,1,0,0/
000017 DATA (IVMAX(I),I=1,6)/3,4,2,6,1,1/
000017 DATA (VMIN(I),I=7,10),(VMAX(I),I=7,10)/4*0.0, 4*10.5/
000017 DATA IVERI(1,1),IVERI(1,2)/0,1/
C
000017 DATA (VMIN(I),I=12,14),(VMAX(I),I=12,14)/3*0.0, 10.5, 10.5, 10.5/
000017 DATA IVERI(15,1), IVERI(15,2)/0,3/
000017 DATA ICHG/1,0,2/
000017 DATA ALT/2030.0, 5000.0, 10000.0, 20000.0/
C
C READ IN NEXT RECORD
C
000017 NGR=0
000020 100 IF(IREAD(IFC).NE.0) GO TO 230
000026 101 I=12
C
C VERIFY CONTENTS OF RECORD
C
000027 IF(ICATA(I).LT.IVERI(I-1,1).OR.
* ICATA(I).GT.IVERI(I-1,2)) GO TO 115
000041 I=16
000042 IF(IDATA(I).LT.IVERI(I-1,1).OR.
* ICATA(I).GT.IVERI(I-1,2)) GO TO 115
000054 DO 111 I=2,7
000055 111 IF(IDATA(I).LT.IVERI(I-1,1).OR.
* ICATA(I).GT.IVERI(I-1,2)) GO TO 115
000071 DO 112 I=8,11
000072 112 IF(IDATA(I).LT.IVERI(I-1,1).OR.
* ICATA(I).GT.IVERI(I-1,2)) GO TO 115
000106 DO 113 I=13,15
000107 113 IF(ICATA(I).LT.IVERI(I-1,1).OR.
* ICATA(I).GT.IVERI(I-1,2)) GO TO 115
000123 GO TO 118
000123 115 WRITE(6,116) I
000131 116 FORMAT(/'11X,1F*,11H BAD RECORD,28X,1H*,5X,9HCOMPONENT,13,
* 12H IS GARBAGE./)
000131 WRITE(6,117) DATA
000143 117 FORMAT(/'10(5022)/')
000143 100 NGR = NGR + 1
000145 IF(NGR.LE.10) GO TO 100
000152 EFLAG = .TRUE.
000153 GO TO 230
C
C BRANCH IF CALIB DATA
C
000154 118 IF (IDATA(4) .EQ. 0 .OR. IDATA(4).EQ.2) GO TO 220
C
C TRANSLATE CERTAIN ENTRIES IN FILE

```

FIGURE A-6. (a) SOURCE LISTING FOR CRUNCH

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000163      C      IDATA(3)=ICATA(3)-1      00000642
*          *      IJK=IUAATA(4)      00000643
*          *      ICATA(4)=1-CHL(IJK+1)      00000644
*          *      IDATA(6)=1-IDATA(6)      00000645
C          C      CHECK FOR AGREEMENT IN RECEIVE PGL      00000646
C          C      00000647
C          C      00000648
C          C      00000649
000165      C      IF(IIDATA(7).EQ.IIDATA(12).OR.IIDATA(3).EQ.0) GO TO 119      00000650
000175      C      WRITE(6,1000) IIDATA(7), IIDATA(12)      00000651
000212      1000      C      FORMAT(/11X,1H*,31H RECEIVE POLARIZATIONS DISAGREE,8X,1H*,5X,      00000652
*          *      9HSCAT REC=,13,5X,8HRAD REC=,13//)      00000653
000212      C      GO TO 105      00000654
C          C      00000655
C          C      INITIALIZE CHANNEL INDICATOR FLAG AND CLEAR OUTPUT ARRAY.      00000656
C          C      00000657
000216      119      C      ICHAN=0      00000658
000217      C      DO 120 I=1,20      00000659
000221      120      C      IARRAY(I)=0      00000660
000224      C      IL = IL + 1      00000661
C          C      00000662
C          C      CHECK TEMPERATURES OF CRITICAL ELEMENTS      00000663
C          C      00000664
000226      C      CALL THERMC (DATA, IDATA, RPAR, IL, LNPCC, IFLAG, IWARM)      00000665
C          C      00000666
C          C      FORM ERROR CODE MESSAGE FOR SCAT AND RAD      00000667
C          C      00000668
000234      C      IARRAY(12) = IWARM      00000669
000236      C      ICCOUNT = ICCOUNT + IWARM      00000670
000242      C      IARRAY(12) = IARRAY(12)*10 + IFLAG      00000671
000245      C      ICCOUNT=ICCOUNT + IFLAG      00000672
C          C      00000673
C          C      COMPUTE LCCK ANGLES.      00000674
C          C      00000675
000246      C      CALL ANGLE (DATA, SPAR, IL, LNPMD, IFLAG)      00000676
C          C      00000677
C          C      AMEND ERROR CODE      00000678
C          C      00000679
000252      C      ICCOUNT=ICCOUNT+IFLAG/10      00000680
000262      C      IARRAY(12) = IARRAY(12)*100+IFLAG      00000681
C          C      00000682
C          C      CONVERT RADIOMETER DATA      00000683
C          C      00000684
000264      C      CALL RCONV (DATA, IDATA, RPAR, RCAL, IL)      00000685
C          C      00000686
C          C      BRANCH IF RAD ONLY DATA      00000687
000270      C      IF (IIDATA(3) .EQ. 0) GO TO 200      00000688
C          C      00000689
C          C      CHECK DOPPLER      00000690
C          C      00000691
000275      C      CALL DOPCHK (DATA, SPAR, IL, IBAND, LNPMD, IFLAG)      00000692
C          C      00000693
C          C      AMEND INDICATOR      00000694
C          C      00000695
000301      C      IARRAY(12) = IARRAY(12) *10+IFLAG      00000696
000304      C      ICCOUNT=ICCOUNT+IFLAG      00000697
C          C      00000698
C          C      SELECT SCAT CHANNEL OUTPUT      00000699
C          C      00000700
C          C      00000701
C          C      THIS SECTION SELECTS THE MAXIMUM CN-SCALE SCAT CHANNEL OUTPUT      00000702
C          C      AND TRANSFORMS IT TO A NORMALIZED RECEIVER INPUT POWER.      00000703
C          C      WHERE READING FALLS OUTSIDE OF DYNAMIC RANGE OF THE FOUR      00000704
C          C      CHANNELS, THE DATA IS YET SELECTED, HOWEVER, A FLAG      00000705
C          C      ACCOMPANIES THE VALUE. THE TRANSFORMED VALUE IS FOUND      00000706
C          C      IN DATA(8).      00000707
C          C      00000708
C          C      INITIALIZE FLAG      00000709
C          C      00000710
000310      C      IFLAG =0      00000711
C          C      00000712
C          C      DETERMINE WHAT CHANNEL MEASUREMENT FELL IN      00000713
C          C      00000714
000311      C      IF (DATA (8) .GE. SPAR(25)) GO TO 140      00000715
000314      C      IF (DATA (9) .GE. SPAR(29)) GO TO 150      00000716
000317      C      IF (DATA (10).GE. SPAR(29)) GO TO 160      00000717
000322      C      IF (DATA (11).GE. SPAR(29)) GO TO 130      00000718
C          C      00000719
C          C      DATA FELL BENEATH RANGE      00000720
C          C      00000721
000326      C      DATA(11)=DATA(11)+1.0 E-10      00000722
000330      C      IFLAG =1      00000723
C          C      00000724
C          C      APPLY SCALE FACTORS      00000725
C          C      00000726

```

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FIGURE A-6. (b) SOURCE LISTING FOR CRUNCH

```

000331 130 DATA (8) = DATA (11)*SPAR(21)/SCAL(4)
000336 ICHAN=4
000337 GO TO 170
C
C DATA FELL ABOVE RANGE
C
000337 140 IF (DATA(8) .GE. SPAR(27)) IFLAG=1
C
C APPLY SCALE FACTORS
C
000344 DATA (8) = DATA (6)*SPAR(18)/SCAL(1)
000350 ICHAN=1
000351 GO TO 170
000351 150 DATA (8) = DATA(9)*SPAR(19)/SCAL(2)
000356 ICHAN=2
000357 GO TO 170
000357 160 DATA (8) = DATA(10)*SPAR(20)/SCAL(3)
000364 ICHAN=3
C
C END SFLECTION OF SCAT CHANNEL.
C
C AMEND ERROR INCICATGR
C
000365 170 IARRAY(12)=IARRAY(12)*10+IFLAG
000370 ICOUNT=ICOUNT+IFLAC
000371 IF(IFLAG.NE.1) GO TO 175
000373 IF(MOD(11,LNFMCD).EQ.0) WRITE(6,1700) IL
000410 1700 FORMAT(16,5X,2F* 22HEXCEEDED DYNAMIC RANGE,16X,1H*)
C
C CHECK RANGE GATE SETTING
C
000410 175 IFLAG = 0
000411 IALT = ICATA(16)+1
000414 CHECK=ALT(IALT)
000416 IF(DATA(41) .LT. CHECK+300. .AND. DATA(41) .GT. CHECK-300.)
* GO TO 177
000431 IFLAG = 1
000432 WRITE(6,1760) CHECK,DATA(41)
000445 1760 FORMAT(16,5X,2F* ,32HNOT WITHIN 300 FT. OF RANGE GATE,6X,1F*,
* 5X,11HRANGE GATE=,F7.0,5X,9HALTITUDE=,F7.0)
000445 177 IARRAY(12) = IARRAY(12)*10 + IFLAG,
000450 ICOUNT=ICOUNT+IFLAC
C
C COMPLETE CONVERSION OF SCAT DATA
C
000454 180 CALL SCUNV (DATA, IDATA, SPAR, IBAND)
C
C SCAT INVERSION.
C
C
C
C COMPARE SCAT POLARIZATIONS.
C
000457 IXMT=IDATA(6)
000464 IREC=IDATA(7)
000466 IF(IXMT.EQ.IREC) GO TO 190
C
C ERROR MESSAGE
C
000467 IF(MOD(11,LNFMCC).EQ.0) WRITE(6,1800) IL, IXMT, IREC
000511 1800 FORMAT(16,5X,2F* ,37HUNABLE TO HANDLE CROSS POLARIZED DATA,
* 1X,2H* ,4X,26HWILL ASSUME POLARIZED DATA, 5X,
* 10HXMIT PUL.=,12,5X,10HREC. PCL.=,12)
C
C INVERT SCAT DATA
C
000511 190 DATA(8) = 4.0*DATA(8)*DATA(41)*DATA(41)/(CCS(0.017453293*
* DATA(14))*3.14159265*SPAR(IXMT+32)*SPAR(IREC+32)*
* 5.250304)
C
C TRANSFER SCAT INT PERIOD
C
000533 IND=IDATA(5)
000535 IARRAY(7)*SPAR(IND+3)
000537 IF(IDATA(3).FC.1) IARRAY(7)=SPAR(10)
C
C TRANSFER SCAT LATA TO OUTPUT ARRAY
C
000544 IARRAY(5) = IDATA (6)
000546 IARRAY(6) = IDATA (7)
000547 IARRAY(8) = DATA (8)
000551 IARRAY(9) = 10.0*ALOG10(DATA(8))
000562 GO TO 210
C
C TRANSFER RAD DATA TO OUTPUT ARRAY
C
000562 200 IARRAY(12)=IARRAY(12)*1000

```

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FIGURE A-6. (c) SOURCE LISTING FOR CRUNCH


```

000565 210  ARRAY (10)= DATA (13)                CCCC0808
C                                               CC000809
C           TRANSFER OTHER SELECTED DATA        C0000810
C                                               00000811
000567  -   ARRAY(1)=DATA(1)                      C0000812
000570  -   IARRAY(2)=IDATA(3)                    00000813
000572  -   ARRAY(3)=DATA(14)                   C0000814
000573  -   ARRAY(4)= DATA(15)                  C0000815
000575  -   ARRAY(11)=DATA(40)                  C0000816
000576  -   ARRAY (13)= DATA(41)                00000817
000600  -   ARRAY (14)= DATA (47)              C0000818
000601  -   ARRAY (15)= DATA (46)              C0000819
C                                               CC000820
C           WRITE TC OUTPUT TAPE                00000821
C                                               C0000822
000603  -   CALL WRITE2(ARRAY)                  00000823
C                                               C0000824
C           INTERMEDIATE PRINT-OUT             00000825
C                                               C0000826
000604  -   IF(MOD(IL,(NPPCD).EQ.0) WRITE(6,2000) IL, ARRAY(10), ARRAY(8),
*           ICHAN, IEANC                        00000827
000643  2000  * FORMAT(I6,5X,2H**,4X,29HCOMPLETED RECCRD CCMPLTATIONS,4X,2H**,
*           4X,14H ANTENNA TEMP=,F6.1,2X,16HSCATTERING COEF=,E12.6,
*           2X,8HCHANNEL=,12,2X,9HDOP BANC=,13) CCCC0828
000643  -   GO TO 100                            C0000829
000644  220  CALL CALIB(SCAL,RCAL,RPAR,NORMAL,BASE) 00000830
000650  -   IF(.NOT.ECFIFC) GO TO 100            C0000831
000656  230  WRITE(6,2000) IL, ARRAY(10), ARRAY(8), ICHAN, IBAND C0000832
000702  -   RETURN                                00000833
000703  -   END                                  C0000834
                                               C0000835
                                               C0000836
                                               00000837

```

FIGURE A-6. (d) SOURCE LISTING FOR CRUNCH

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Table A-2 Definition of Variables Used in CRUNCH (Continued)

ICOUNT	=	Number of Interpretational Flags
LNPMOD	=	Line Print Modulus
IFC	=	Unit Code Number (1 or 8)
NGR	=	Number of Bad Records
ALT	=	Range Gate Settings
CHECK	=	One of Gate Settings
IXMT	=	Transmit Polarization Indicator
IREC	=	Receive Polarization Indicator
IND	=	SCAT Integration Selector
ARRAY	=	Output Array
IARRAY	=	Integer Equivalent

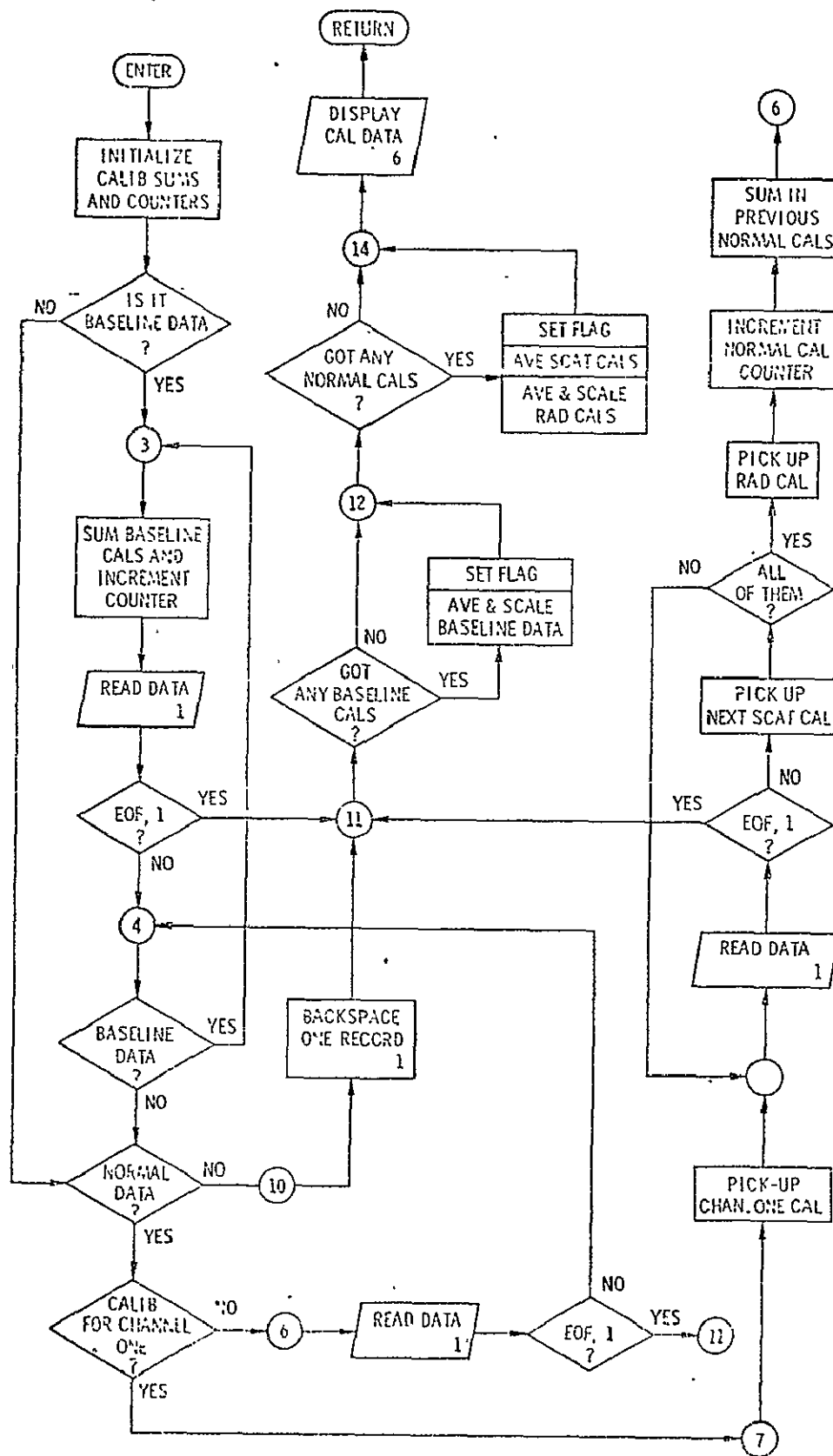
and RRAR are defined in Section III D; whereas, the entries in ARRAY are defined in Section III C.

C. Subroutine CALIB

1. Theory and Design

Subroutine CALIB extracts, averages and displays calibration parameters from calibration records. CALIB was designed to anticipate calibration records in a format generated by the RADSCAT instrument. Although additional flexibility is provided so that baseline records, which are entered by hand, may be inserted in almost any fashion. The baseline records may occur anywhere in the file except within a group of four normal calibration records. In regards to sequences of normal calibrations, the subroutine will orient itself on a set of four by interrogating whether the first normal calibration record causes SCAT outputs to saturate in channels 2, 3 and 4. This feature was embedded in the routine when it became apparent that the RADSCAT instrument would occasionally drop calibrations on the first few SCAT channels. A descriptive logic diagram for subroutine CALIB is shown in Figure A-7.

The baseline (BCAL) and normal calibration counters are initialized upon entry into the routine. Also the SCAT channel (CAL1(I), I = 1,4) and RAD accumulators (CAL1(5), RCL) are cleared. If the type of calibration record (normal or baseline, see Section III B) is normal (IDATA(4) = 0), processing is directed to statements including and following 4. Otherwise, if it is a baseline record, it is accumulated in RCL, the baseline counter is incremented, and the next record is



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FIGURE A-7. DESCRIPTIVE LOGIC DIAGRAM
FOR SUBROUTINE CALIB

read. In statement 4 and the one following, the type of record is again determined. If additional baselines records are present (IDATA(4) = 2), the above processing is repeated; if it is normal calibration data, the record is examined to determine whether the calibration indeed occurred on channel 1 (see DO loop terminating in statement 5). If not, the next record is read and the type is again determined. Once the program is aligned on the calibration for channel one, it extracts it in statement 7 and pulls the SCAT calibrations from the subsequent records for channels 2, 3 and 4 and the normal RAD calibration from the last SCAT calibration record (Channel 4). The normal cal counter is incremented and the calibration accumulator update.

The next record is read and the type determined again. If it is a calibration record the above steps are repeated. If not (measurement record), the unblocking routine READI is called to backspace a record (statement 10). The steps 11 through 60 determine what kinds of calibrations were present and how many. The accumulated calibrations are averaged and scaled accordingly. The types of calibrations present are reflected by setting the logical variables NORMAL and BASE to TRUE. The calibration parameters are then printed and control is returned to the calling routine, either SEARCH or CRUNCH.

2. Program Listing and Variables

The source listing for CALIB is shown in Figure A-8. The definitions of the variables are listed in Table A-3.

Table A-3 Variables Used in CALIB

DATA	=	Input Raw Data Vector
IDATA	=	Integer Equivalent of DATA
SCAL	=	SCAT Calibration Vector
RCAL	=	RAD Calibration Vector
RPAR	=	RAD Parameters
NORMAL	=	Normal Cal Indicator
BASE	=	Baseline Cal Indicator
BCAL	=	Baseline Cal Record Counter
CAL	=	Normal Cal Record Counter
RCAL	=	Baseline Cal Accumulator
CALI	=	Normal Cal Accumulator

```

SUBROUTINE CALIB(SCAL,RCAL,RPAP,NORMAL,BASE)
CALIB
C
C      THIS PROGRAM WAS PREPARED BY
C
C      JOHN P. CLAASSEN
C      GLEN E. ELLIOTT
C
C      UNIVERSITY OF KANSAS CENTER FOR RESEARCH
C
C      THIS SUBROUTINE EXTRACTS CALIBRATION INFORMATION FROM
C      THE RADSCAT DATA FILE AND DISPLAYS IT.
C
C000010 COMMON /INPUT/ EOF1, DATA
C000010 LOGICAL NORMAL, BASE, EOF1
C000010 DIMENSION DATA(50), ICATA(1), SCAL(1), RCAL(1), RPAP(1)
C000010 DIMENSION CAL1(5), CAL2(5)
C000010 EQUIVALENCE (DATA(1),ICATA(1))
C
C      INITIALIZE CAL COUNTERS
C
C000010 BCAL=0.0
C000011 RCL=0.0
C000012 CAL=0.0
C
C      CLEAR CAL ACCUMULATORS
C
C000013 DO 1 I=1,5
C000014 CAL1(I)=0.0
C
C      BRANCH WHEN NOT BASELINE
C
C000017 IF(ICATA(4).NE.2) GO TO 4
C
C      EXTRACT BASELINE
C
C000021 RCL=RCL+DATA(13)
C
C      UPDATE ECAL COUNT
C
C000023 BCAL=BCAL+1.0
C
C      READ NEXT RECORD
C
C000025 CALL READ1
C000026 IF(EOF1) GO TO 11
C000033 IF(ICATA(4).EQ.2) GO TO 3
C
C      EXIT WHEN NO MORE CAL DATA
C
C000035 IF(ICATA(4).NE.C) GO TO 10
C
C      CHECK IF RECORD CONTAINS CAL CN
C      FIRST SCAT CHANNEL
C
C000036 DO 5 I=2,4
C000037 IF(DATA(I+7).LT.9.0) GO TO 6
C000044 GO TO 7
C
C      FIND FIRST SCAT CAL
C
C000044 CALL READ1
C000045 IF(EOF1) 11,4
C
C      EXTRACT SCAT 1
C
C000053 CAL2(1)=DATA(8)
C
C      EXTRACT REMAINDER OF CALS
C
C000055 DO 8 I=2,4
C000056 CALL READ1
C000057 IF(EOF1) GO TO 11
C000064 IF(ICATA(4).NE.0) GO TO 4
C000065 CAL2(I)=DATA(I+7)
C000071 CAL2(5)=DATA(13)
C000073 CAL=CAL+1.0
C
C      ACCUMULATE REPETITIVE CALS
C
C000075 DO 9 I=1,5
C000076 CAL1(I)=CAL1(I)+CAL2(I)
C000102 GO TO 6
C
C      REPOSITION DATA RECORD
C0000838
C0000839
C0000840
C0000841
C0000842
C0000843
C0000844
C0000845
C0000846
C0000847
C0000848
C0000849
C0000850
C0000851
C0000852
C0000853
C0000854
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C0000864
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C0000905
C0000906
C0000907
C0000908
C0000909
C0000910
C0000911
C0000912
C0000913
C0000914
C0000915
C0000916
C0000917
C0000918
C0000919
C0000920
C0000921
C0000922

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FIGURE A-8. (a) FORTRAN LISTING FOR CALIB

000102	C	10	CALL BCKSP1	C0000923
	C			C0000924
	C		CHECK FOR PRESENCE OF BASELINE CAL	C0000925
	C			C0000926
000103	C	11	IF(BCAL.LT.1.0) GO TO 12	C0000927
000111	C		BASE = .TRUE.	00000928
	C			C0000929
	C		AVERAGE AND TRANSLATE BASELINE	C0000930
	C			C0000931
000111	C		KCAL(1)=(RCL/BCAL)*RPAR(19)/RPAR(20)	00000932
	C			C0000933
	C		CHECK FOR PRESENCE OF NORMAL CAL	C0000934
	C			C0000935
000115	C	12	IF(CAL.LT.1.0) GO TO 14	C0000936
000120	C		NORMAL = .TRUE.	C0000937
000120	C		DO 13 I=1,4	C0000938
	C			00000939
	C		AVERAGE SCAT CALS	C0000940
	C			C0000941
000122	C	13	SCAL(I)=CAL(I)/CAL	C0000942
	C			C0000943
	C		AVERAGE AND TRANSLATE RAD CAL	C0000944
	C			C0000945
000126	C		RCAL(2)=(CAL(5)/CAL)*RPAR(19)/RPAR(20)	C0000946
	C			C0000947
	C		DISPLAY CAL DATA	C0000948
	C			C0000949
000122	C	14	WRITE (6,100) (I,SCAL(I),I=1,4),RCAL(2), RCAL(1), CAL, BCAL	C0000950
000167	C	100	FORMAT (11X,1H*10X,16FCALIBRATION DATA,13X,1H*,3X,	00000951
	C	*	4(2X,4HCHAN,12,1H=,F7.3),	C0000952
	C	*	/51X,1H*,5X,5HRCAL=F7.3,2X,6HRBASE=,F7.3,	C0000953
	C	*	7F NCAL=,F6.0,5H NCAL=,F6.0)	C0000954
000167	C	60	RETURN	C0000955
000170	C		END	C0000956
				00000959

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FIGURE A-8. (b) (continued)

D. Subroutine ANGLE

1. Introduction

This routine computes the incident angle and cross track angle both of which are required to define the beam position on the surface with respect to the aircraft flight vector. When roll or pitch becomes excessive, as the case may be, so as to make the polarization difficult to interpret a flag is generated. Irrespective of the flagged condition the data is reduced in the standard way. The theory by which these angles are computed and the method by which the angles are applied to determine the polarization break-up at the surface are described below.

2. Theory and Design

a. Incident and Cross-Track Angles - Suppose the aircraft is vectored along the positive x axis of an unprimed coordinate system where the z axis corresponds to the local vertical. The orientation of the aircraft is represented in a primed coordinate system where x' axis is located along the fore-aft axis of the aircraft. They are related to the unprimed system by a drift angle ϕ_d about the z axis, a pitch angle θ_p with respect to the x, y plane and a roll angle ϕ_r about the x' axis (Figure A-9).*

The antenna points at an angle θ_a with respect to the $-z'$ axis. θ_a is assumed to be corrected for the relative angle between aircraft and antenna platforms. The true incident angle θ on the ground is desired. The incident angle may be derived from relation

$$\cos \theta = - \bar{\tau}_r \cdot \bar{z}_z \quad (1)$$

where $\bar{\tau}_r$ is a unit vector in the boresight direction. Also of interest is the cross track angle ϕ_c measured in the x, y plane with respect to the $-x$ axis as shown in Figure A-10. Clearly we have

$$\tan \phi_c = \frac{\bar{\tau}_r \cdot \bar{z}_y}{-\bar{\tau}_r \cdot \bar{z}_x} \quad (2)$$

* It should be noted that these definitions of roll, pitch and drift coincide with those provided by the Litton Navigator LTN-51.

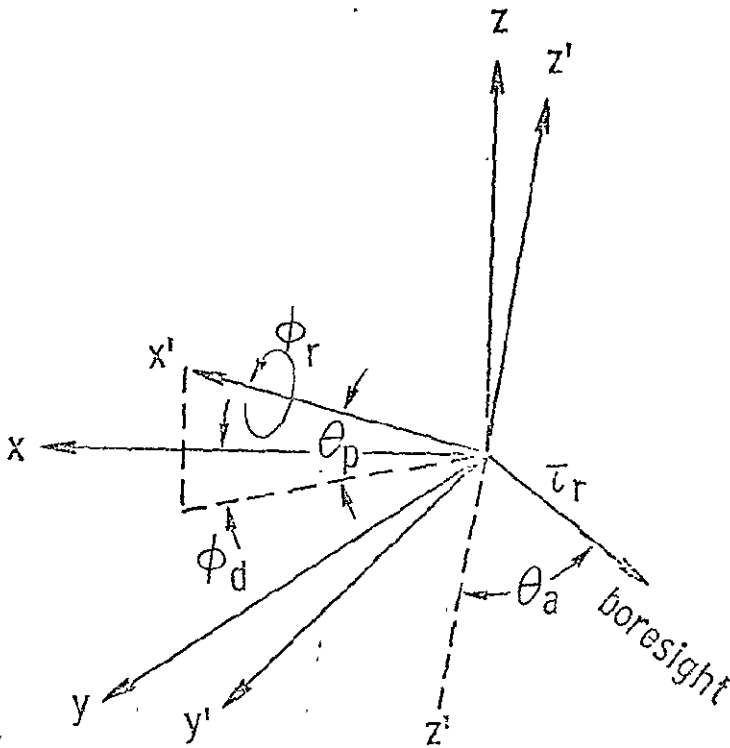


Figure A-9. Aircraft Flight Geometry

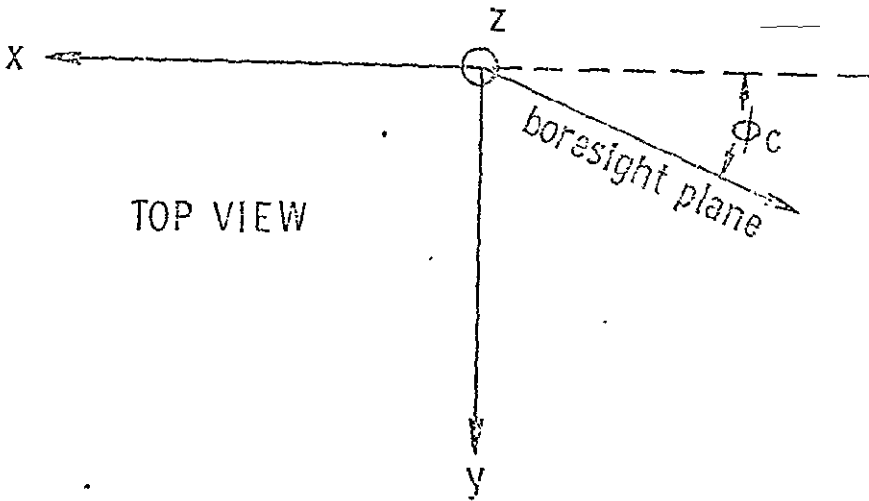


Figure A-10. Geometry Defining the Cross-Track Angle.

Now in the primed coordinate system the boresight axis is described by

$$\bar{r}_r = -\sin \theta_a \bar{r}_{x'} - \cos \theta_a \bar{r}_{z'} \quad (3)$$

The primed and unprimed coordinate systems are related by the following successive transformation

$$\begin{pmatrix} \bar{x}_{x'} \\ \bar{x}_{y'} \\ \bar{x}_{z'} \end{pmatrix} = ABC \begin{pmatrix} \bar{x}_x \\ \bar{x}_y \\ \bar{x}_z \end{pmatrix} \quad (4)$$

where

$$A = \begin{pmatrix} 1 & 0 & 0 \\ 0 & \cos \phi_r & \sin \phi_r \\ 0 & -\sin \phi_r & \cos \phi_r \end{pmatrix}$$

$$B = \begin{pmatrix} \cos \theta_p & 0 & \sin \theta_p \\ 0 & 1 & 0 \\ -\sin \theta_p & 0 & \cos \theta_p \end{pmatrix}$$

$$C = \begin{pmatrix} \cos \phi_d & \sin \phi_d & 0 \\ -\sin \phi_d & \cos \phi_d & 0 \\ 0 & 0 & 1 \end{pmatrix}$$

Substitution of (3) and (4) into (1) yields

$$\cos \theta = \sin \theta_p \sin \theta_a + \cos \theta_p \cos \theta_a \cos \phi_r \quad (5)$$

which reduces to the expected result when $\phi_r = 0$, namely, $\cos (\theta_p + \theta_a)$.

When the drift angle is considered zero, a similar approach will yield

$$\tan \phi_c (\phi_d = 0) = \frac{\sin \phi_r \cos \theta_a}{\sin \theta_a \cos \theta_p - \sin \theta_p \cos \theta_a \cos \phi_r} \quad (6)$$

When $\phi_d = 0$, it is clear from Figure A-11 that the correction for ϕ_d is simply given by

$$\phi_c (\phi_d = 0) = - [\phi_d - \phi_c (\phi_d = 0)] \quad (7)$$

or

$$\phi_c (\phi_d = 0) = -\phi_d + \tan^{-1} \left[\frac{\sin \phi_r \cos \theta_a}{\sin \theta_a \cos \theta_p - \sin \theta_p \cos \theta_a \cos \phi_r} \right] \quad (8)$$

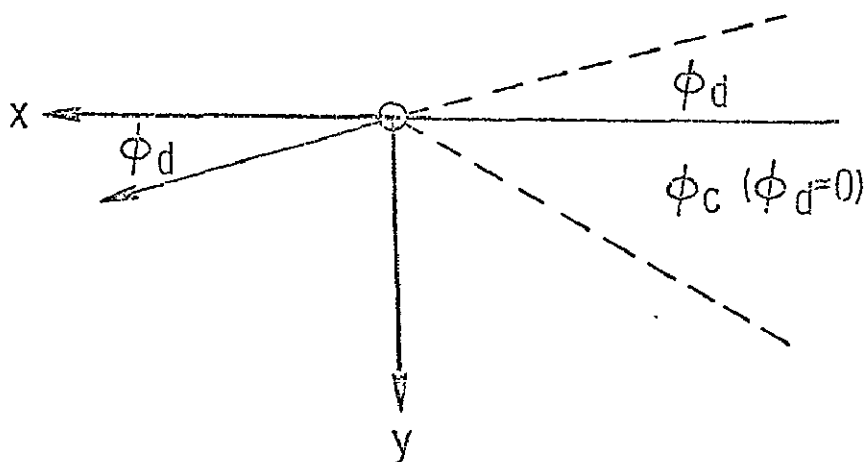


Figure A-11. Cross-Track Angle Correction for Drift.

Equations 5 and 8 thus define the beam position on the sea with respect to the aircraft trajectory.

b. Polarization Decomposition - When the aircraft pitches and rolls, the incident polarization can decompose into vertically and horizontally polarized components. When the unwanted component becomes excessive, the measurement becomes difficult to interpret; and, consequently, the reduced data should be flagged.* To determine the size of the undesired component, the degree of "de-polarization" is computed from considerations similar to those above.

* Correction for this situation is possible when polarized measurements are considered jointly.

Without loss of generality we may assume that the aircraft is vectored along the $-x$ axis with zero drift. It is pitched at an angle of θ with respect to the $-x$ axis and a positive roll of ϕ_r is induced about the $-x'$ axis. The x, y plane forms the local horizontal and the z axis is pointed at nadir. See Figure A-12.

The antenna is boresighted in the x', z' plane with an angle θ_a from the z' axis. The vertical polarization emitted by the antenna is described by

$$\bar{\tau}_{\theta'} = \cos \theta_a \bar{\tau}_{x'} - \sin \theta_a \bar{\tau}_{z'} \quad (9)$$

along the boresight axis. The horizontal surface polarization at the boresight point is described as

$$\bar{\tau}_{\phi} = -\sin \phi_c \bar{\tau}_x + \cos \phi_c \bar{\tau}_y \quad (10)$$

where ϕ_c corresponds to the cross-track angle for the zero drift condition. Now the percent power de-polarization is approximately given by $100 |\bar{\tau}_{\theta'} \cdot \bar{\tau}_{\phi}|^2$ for points illuminated by the main beam.

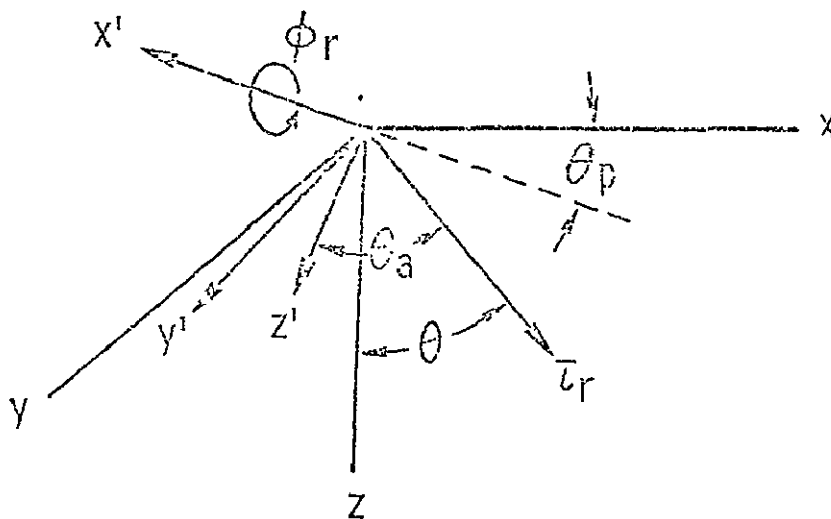


Figure A-12. "Depolarization" Geometry.

Now the transformation between the coordinates is given by

$$\begin{pmatrix} \bar{x}' \\ \bar{y}' \\ \bar{z}' \end{pmatrix} = \begin{pmatrix} 1 & 0 & 0 \\ 0 & \cos \phi_r & -\sin \phi_r \\ 0 & \sin \phi_r & \cos \phi_r \end{pmatrix} \begin{pmatrix} \cos \theta_p & 0 & \sin \theta_p \\ 0 & 1 & 0 \\ -\sin \theta_p & 0 & \cos \theta_p \end{pmatrix} \begin{pmatrix} \bar{x} \\ \bar{y} \\ \bar{z} \end{pmatrix} \quad (11)$$

or

$$\begin{pmatrix} \bar{x}' \\ \bar{y}' \\ \bar{z}' \end{pmatrix} = \begin{pmatrix} \cos \theta_p & 0 & \sin \theta_p \\ \sin \phi_r \sin \theta_p & \cos \phi_r & -\sin \phi_r \cos \theta_p \\ -\cos \phi_r \sin \theta_p & \sin \phi_r & \cos \phi_r \cos \theta_p \end{pmatrix} \begin{pmatrix} \bar{x} \\ \bar{y} \\ \bar{z} \end{pmatrix} \quad (12)$$

With the help of (12) we may thus write

$$\begin{aligned} |\bar{\tau}_{\theta'} \cdot \bar{\tau}_{\phi}| &= |\sin \phi_c (\cos \theta_a \cos \theta_p + \sin \theta_a \cos \phi_r \sin \theta_p) \\ &\quad + \cos \phi_r \sin \theta_a \sin \phi_r| \end{aligned} \quad (13)$$

Now a suitable criterion for excessive polarization may be formed by requiring that

$$|\bar{\tau}_{\theta'} \cdot \bar{\tau}_{\phi}|^2 < \epsilon \quad (14)$$

where $0 < \epsilon < 1$. However, when the aircraft roll becomes excessive so that $|\bar{\tau}_{\theta'} \cdot \bar{\tau}_{\phi}|^2 > 0.5$ the interpretation of the incident polarization should be reversed from that defined by the instrument. Under this circumstance the polarization criterion should be written as

$$1 - |\bar{\tau}_{\theta'} \cdot \bar{\tau}_{\phi}|^2 < \epsilon \quad (15)$$

where $0 < \epsilon < 1$. This latter criterion should be useful when RADSCAT observations are conducted from an aircraft in a roll (blank) attitude.

From Section IV.B.1 we noted that for zero drift

$$\tan \phi_c = \frac{\sin \phi_r \cos \theta_a}{\sin \theta_a \cos \theta_p + \sin \theta_p \cos \theta_a \cos \phi_r} \quad (16)$$

The drift angle does not influence the polarization decomposition as a little thought will substantiate. This is fortunate since drift angle is not well defined in a roll maneuver. As a consequence the criterion is now formed on the basis of measured and computed parameters.

Relationships (13), (14), (15) and (16) establish the depolarization parameters and the polarization reversal criterion.

3. Program Listing and Variables

The FORTRAN listing for ANGLE is shown in Figure A-13. The comment statements are sufficient to establish the logic of the program. The variables defined in Table A-4 should be helpful.

Table A-4 Definition of Variables in Subroutine ANGLE

DATA	=	Input Raw Data Vector
SPAR	=	SCAT Parameters
IL	=	Record Count
LNPMOD	=	Line Print Modulus
IFLAG	=	Excessive Depolarization and Reversal Flag
DEGRAD	=	Degress to Radians Conversion Factor
ANTA	=	Antenna Angle
PITCH	=	Aircraft Pitch
DRIFT	=	Aircraft Drift
ROLL	=	Aircraft Roll
THETA	=	Incident Angle
ARG1, ARG2	=	Intermediate Storage
PHI	=	Cross-track Angle
DEPOL	=	Depolarization Factor

```

SUBROUTINE ANGLE (DATA,SPAR,IL,LAMPCL,IFLAG)
CANGLE      COMPUTE INCIDENCE ANGLE
C           SUBROUTINE ANGLE (DATA,SPAR,IL,LAMPCL,IFLAG)
C
C           THIS PROGRAM WAS PREPARED BY
C
C           JOHN P. CLAASSEN
C           GLEN E. ELLIOTT
C
C           UNIVERSITY OF KANSAS CENTER FOR RESEARCH
C
C           THIS ROUTINE COMPUTES THE INCIDENT ANGLE THETA FROM AIRCRAFT
C           AND ANTENNA PARAMETERS. CORRECTION IS MADE FOR THE RELATIVE
C           ANGLE BETWEEN THE AIRCRAFT AND ANTENNA PLATFORM.
C           THE BORESIGHT CROSS-TRACK ANGLE PHI IS ALSO COMPUTED.
C           WHEN THE ROLL OR PITCH ANGLE BECOMES EXCESSIVE, AS THE CASE
C           MAY BE, SO AS TO MAKE THE RETURN OR EMISSION POLARIZATION
C           DIFFICULT TO INTERPRET, A FLAG IS GENERATED.
000010      DIMENSION DATA(1), SPAR(1)
C
C           DEGREE-RADIAN CONVERSION FACTOR.
000010      DATA DEGRAD/0.0174532525/
C
C           INITIALIZE FLAG
000010      IFLAG=0
C
C           AVERAGE SCAT AND RAC ANGLES
000010      DATA(14)=(DATA(14)+DATA(15))/2.0
C
C           CONVERT TO DEGREES
000013      DATA(14)=DATA(14)*SPAR(30)
C
C           COMPENSATE FOR ANTENNA PITCH RELATIVE TO AIRCRAFT
000015      DATA(14)=DATA(14)+SPAR(31)
C
C           CONVERT TO RADIANS
C
C           ANTA= DATA(14)*DEGRAD
000017      ANTA= DATA(14)*DEGRAD
000021      PITCH=DATA(43)*DEGRAD
000022      DRIFT=DATA(44)*DEGRAD
000024      ROLL =DATA(45)*DEGRAD
C
C           COMPUTE INCIDENT ANGLE
000025      THETA = SIN(ANTA)*SIN(PITCH)+COS(PITCH)*COS(ANTA)*COS(ROLL)
000043      THETA = ACOS(THETA)
C
C           CONVERT TO DEGREES.
000046      DATA(14)=THETA/DEGRAD
C
C           COMPUTE CROSS TRACK ANGLE
000052      ARG1=SIN(ROLL)*COS(ANTA)
000057      ARG2=SIN(ANTA)*COS(PITCH)-SIN(PITCH)*COS(ANTA)*COS(ROLL)
000075      IF (ABS(ARG2).LT.1.E-07) GO TO 30
000104      IF (ABS(ARG1).LT.1.0E-07) GO TO 10
000107      PHI=ATAN2(ARG1,ARG2)
000112      GO TO 40
000115      PHI=0.
000116      IF (ARG2.LT.0.0) PHI=3.14159265
000121      GO TO 40
000122      PHI=SIGN(1.57079633,ARG1)
000125      DATA(15)=PHI/DEGRAD-DATA(44)
C
C           COMPUTE THE DEPOLARIZATION
000130      DEPOL= SIN(PHI)*
*           [COS(ANTA)*COS(PITCH)+SIN(ANTA)*COS(ROLL)*SIN(PITCH)]+
*           [COS(PHI)*SIN(ANTA)*SIN(ROLL)]
C
C           CHECK FOR POLARIZATION REVERSALS.
000162      DEPOL = DEPOL*DEPOL
000163      IF(DEPOL.GT.0.500) GO TO 50
000172      GO TO 60
000172      50      DEPOL = 1.0 - DEPOL
C
C           IFLAG REVERSAL

```

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FIGURE A-15. (a) FORTRAN LISTING FOR SUBROUTINE ANGLE

000174	C	IF(MOD(IL,LNPPCD).EQ.0) WRITE(6,500) IL	00001279
000210	>00	FORMAT(16,5X,2H* 2HPOLARIZATION REVERSAL,17X,1H*)	00001280
000210		IFLAG=1	00001281
	C		00001282
	C	FLAG EXCESSIVE DEPOL.	00001283
	C		00001284
000211	>0	IF(DEPOL.GT.0.02) GO TO 70	00001285
000215		RETURN	00001286
000215	/0	IFLAG=IFLAG+10	00001287
000216		IF(MOD(IL,LNPPCD).EQ.0) WRITE(6,700) IL, DEPOL	00001288
000235	700	FORMAT(16,5X,2H* 2HEXCESSIVE DEPOLARIZATION,14X,1H*,	00001289
	*	5X,6HDEPOL=,F7.3)	00001290
000235		DATA(40)=DEPOL	00001291
000237		RETURN	00001292
000240		END	00001293

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FIGURE A-13. (b) FORTRAN LISTING FOR SUBROUTINE ANGLE

E. Subroutine THERMO

Temperatures within the RADSCAT microwave assembly are monitored at various points. Certain of these temperatures are essential to the reduction of the radiometer data. All of the temperatures should be checked to determine whether the instrument is operating within its temperature limits.

The temperatures are monitored by means of thermistors. Above 283° the thermistor output voltages are linearly proportional to temperature. This routine converts the recorded thermistor voltages, DATA(17) through DATA(33), to degrees Kelvin by using linear conversion constants, RPAR(23) through RPAR(56). Once converted the computed temperatures are examined to see that they appear in the operating temperature range specified by RPAR(21) and RPAR(22). Those that fall outside this range are flagged with a message in the Conversion Report. A flag is also generated in the S/R validation code appearing in the output files. Routinely the temperatures critical to the conversion of radiometer data are reported by this routine.

The above steps are reflected in the FORTRAN listing for THERMO shown in Figure A-14. The variables employed in the routine are defined in Table A-5.

Table A-5 Definition of Variables Used in THERMO

DATA	=	Raw Data Vector
IDATA	=	Integer Equivalent of DATA
RPAR	=	Radiometer Parameters
IL	=	Record Number
LNPMOD	=	Line Print Modulus
IFLAG	=	Abnormal Receiver Temperature Flag
IWARM	=	Warm Load Temperature Estimate Flag

F. Subroutine RCONV

1. Introduction

This routine converts the radiometer output voltage into an antenna (input) temperature. Radiometer baseline calibration RCAL(1) and normal calibrations RCAL(2) are employed to properly scale the output voltage DATA(13) to a receiver input temperature. Thermal noise contributions from front-end elements are subtracted


```

SUBROUTINE THERMO (DATA, IDATA, RPAR, IL, LNPMOD, IFLAG, IWARM)      C0001068
C                                                                    00001069
CTHERMO                    CHECKS TEMPERATURE                       C0001070
C                                                                    00001071
C      ----- THIS PROGRAM WAS PREPARED BY                        00001072
C                                                                    00001073
C              JOHN P. CLAASSEN                                    00001074
C              GLEN E. ELLICTT                                    00001075
C                                                                    00001076
C      ----- UNIVERSITY OF KANSAS CENTER FOR RESEARCH          00001077
C                                                                    00001078
C      THIS ROUTINE EXAMINES ATM VOLTAGES AND CONVERTS THEM TO    C0001079
C      TEMPERATURES. THE TEMPERATURE VALUES ARE CHECKED TO SEE  00001080
C      IF THEY OCCUR IN THE PERMISSIBLE OPERATING RANGE. WHEN    00001081
C      THEY FALL OUTSIDE THE RANGE A FLAG IS GENERATED AND AN ERROR 00001082
C      MESSAGE DISCLOSES THE BAD VALUE AND MONITORING LOCATION    00001083
C      IS PRINTED. THE VOLTAGE TO TEMPERATURE PARAMETERS ARE     00001084
C      ENTERED FROM RPAR. THE STARRED STATEMENT IS TO BE         00001085
C      USED WHEN THE HOT LOAD TEMP IS AVAILABLE.                  00001086
C                                                                    00001087
C00012    DIMENSION DATA(1), RPAR(1), IDATA(1)                    C0001088
C                                                                    00001089
C              INITIALIZE FLAGS                                     00001090
C                                                                    00001091
C00012    IFLAG=0                                                  00001092
C00012    IWARM = 0 .                                              00001093
C                                                                    00001094
C              CONVERT TO TEMPERATURES                            00001095
C                                                                    00001096
C00013    J = 22                                                  00001097
C00014    DO 20 I= 1,17                                           00001098
C00016    K=I+J                                                    00001099
C00020    DATA(I+16)=RPAR(K)*DATA(I+16)+RPAR(K+1)+273.18        00001100
C00025    T=DATA(I+16)                                            00001101
C00027    J = J+1                                                 00001102
C00031    IF(I.EQ.17) GO TO 20                                    00001103
C00033    IF (T.LT.RPAR(21) .AND. T.GT. RPAR(22)) GO TO 20      00001104
C                                                                    00001105
C              FLAG AND PRINT MESSAGE WHEN NOT IN LIMITS.        00001106
C                                                                    00001107
C00043    10  IFLAG=1                                             00001107
C00044    IF(MOD(IL, LNPMOD).EQ.0) WRITE (6,100) IL,I,T          00001108
C                                                                    00001109
C00066    100  FORMAT(16,5X,41H* RECVR TEMP NOT WITHIN OPERATING RANGE *, 00001109
C      * 5X,12HLLOCATION NO. 13,5X,                                00001110
C00066    20  * 13HTEMPERATURE =,F5.1,7H KELVIN)                  00001111
C      CONTINUE                                                  00001112
C                                                                    00001113
C              CHANGE AIR TEMP TO KELVIN                          00001114
C                                                                    00001115
C00070    DATA(46) = DATA(46) + 273.18                          00001116
C                                                                    00001117
C              CHECKS FOR ESTIMATED WARM LOAD TEMPERATURE        00001118
C                                                                    00001119
C00072    IF (IDATA(36) .EQ. 0) GO TO 30                          00001120
C00074    IWARM = 1                                               00001121
C00074    IF (MOD(IL, LNPMOD) .EQ. 0) WRITE(6,150) IL           00001122
C00113    150  FORMAT (16,5X,2H* ,31HWARM LOAD TEMPERATURE ESTIMATED,7X,,1H*) 00001123
C                                                                    00001124
C              LIST CRITICAL TEMPERATURES                        00001125
C                                                                    00001126
C00113    30  IF(MOD(IL, LNPMOD).EQ.0) WRITE (6,200) IL, DATA(27), DATA(33), 00001126
C      * DATA(32), DATA(28), DATA(46), DATA(25)              00001127
C00167    200  FORMAT (16,5X,2H* 21HCRITICAL TEMPERATURES,17X,  00001128
C      * 1H*,5X,5HWARM=,F6.1,2X,4HHOT=,F6.1,2X,4HOMT=,F6.1,    00001129
C      * 2X,3HSHW=,F6.1,2X,4HAIR=,F6.1,2X,4HGDE=,F6.1)         00001130
C00167    RETURN                                                  00001131
C00170    END                                                    00001132

```

FIGURE A-14. FORTRAN LISTING FOR SUBROUTINE THERMO

out to refer the receiver input temperature to the antenna terminals with the help of conversion constants RPAR and temperatures of input elements, DATA (17) to DATA (33).

2. Theory and Design

The radiometer conversion model was developed in TM 186-3^{*}. In view of the involvement in the derivation, only an outline of the derivation will be presented here.

During baseline calibration an output proportional to a zero receiver input temperature is generated

$$V_b = -\frac{\tau_c}{RC} \left[V_r + \frac{G}{4(T_{1r} - T_{2r})} (T_{1r} + T_{2r} - T_{1r} - T_{2r}) \right] \quad (1)$$

where

τ_c = calibration integration period

RC = output integrator time constant

G = receiver gain established by AGC circuit

V_r = output reference bias

T_{1r} = hot load temperature referred to receiver input

T_{2r} = warm load temperature referred to receiver input

During a normal calibration sequence the output integration produces a voltage given by

$$V_m = -\frac{\tau_c}{RC} \left[V_r - \frac{G}{4(T_{1r} - T_{2r})} (2T_{1r} - 2T_{2r}) \right] \quad (2)$$

This result yields the unknown gain factor

$$G = \frac{2RC}{\tau_c} (V_m - V_b) \quad (3)$$

where (1) has been employed. A measurement cycle yields an output voltage given by

$$V_m = -\frac{\tau}{RC} \left[V_r + \frac{G(2T_{ar} - T_{1r} - T_{2r})}{4(T_{1r} - T_{2r})} \right] \quad (4)$$

^{*} Claassen, J. P., "The RADSCAT Radiometer Transfer Function and Its Application to the Reduction of RADSCAT Data," University of Kansas Center for Research, Inc. Lawrence, Kansas, December 1971.

where T_{ar} is the temperature at the antenna port of the Dicke switch. This result may be written as

$$T_{ar} = \frac{T_{1r} + T_{2r}}{2} - \rho_m (T_{1r} - T_{2r}) \quad (5)$$

where

$$\rho_m = \frac{V_m - V_b \tau/\tau_c}{(V_m - V_b) \tau/\tau_c} \quad (6)$$

and where (1) and (3) have been employed. From pages 8-11 of TM 186-3 it is noted that certain leakages at the Dicke switch require that certain terms in (5) be modified with reflection factors R_a and R_c so that the modeling equation actually becomes

$$T_{ar} (1 - R_L) = \frac{T_{1r} + T_{2r}}{2} (1 - R_a) - \rho_m (T_{1r} - T_{2r}) \quad (7)$$

Now the temperature at the antenna port of the Dicke switch can be described by

$$(1 - R_a) T_{ar} = \beta_1 T_a + \beta_2 T_g + \beta_3 T_s + \beta_4 T_F + \beta_5 T_o + \beta_6 T_c + \beta_7 + \beta_8 T_L \quad (8)$$

where

T_a = desired antenna temperature

T_L = leakage from opposite port

T_g = internal guide temperature

T_s = temperature of polarization switch

T_F = temperature of feed between switch and OMT

T_o = temperature of OMT

T_c = temperature of cutler feed

β_i = referral constants $i = 1, 2, \dots, 8$

It should be noted that the factor β_7 simply accounts for small but unknown contributions originating from front-end elements not well defined physically. Now let

$$\frac{T_{1r} + T_{2r}}{2} (1 - R_a) = \sqrt{1} T_1 + \sqrt{2} T_2 \quad (9)$$

and

$$\rho_m (T_{1r} - T_{2r}) = \rho_m (v_3 T_1 - v_4 T_2) \quad (10)$$

Then (7) may be written as

$$\begin{aligned} \beta_1 T_a + \beta_8 T_L = & v_1 T_1 + v_2 T_2 - \rho_m (v_3 T_1 - v_4 T_2) \\ & - \beta_2 T_g - \beta_3 T_s - \beta_4 T_F - \beta_5 T_o \\ & - \beta_6 T_c - \beta_7 \end{aligned} \quad (11)$$

or after division by β_1 as

$$\begin{aligned} T_a + \epsilon_c T_L = & \sigma_1 T_1 + \sigma_2 T_2 - \rho_m (\sigma_3 T_1 - \sigma_4 T_2) \\ & - \eta_1 T_g + \eta_2 T_s - \eta_3 T_F - \eta_4 T_o \\ & - \eta_5 T_c - \eta_6 \end{aligned} \quad (12)$$

Now since T_F is not monitored it will be assumed that $T_F = a_o T_s + a_i T_o$ where $a_o + a_s = 1$. In this case the conversion model simplifies to the form

$$\begin{aligned} T_a + \epsilon_c T_L = & \sigma_1 T_1 + \sigma_2 T_2 - \rho_m (\sigma_3 T_1 - \sigma_4 T_2) - \sigma_5 T_g \\ & - \sigma_6 T_s - \sigma_7 T_o - \sigma_8 T_c - \sigma_9 \end{aligned} \quad (13)$$

The leakage term T_L is actually the antenna temperature at the opposite polarization. This term can be estimated from measurements at that polarization. There is no guarantee that it is always available; however, over the sea it can be estimated from T_o with reasonable accuracy when the sky is clear. Hollinger* has shown that the polarized temperatures are related by

$$T_{av} = \frac{1-c}{1+c} T_{ah}$$

where

$$C = 0.00012 \theta^2$$

θ = observation angle in degrees

*Hollinger, J. P., "Passive Microwave Measurements of the Sea Surface," Journal of Geophysical Research, vol. 75, no. 27, pp. 5209-5213, September 1970.

The latter estimating technique is employed by the subroutine since temperatures at the opposite polarization are not always available. Fortunately ξ_c is small (estimated at .004) so that under some circumstances the leakage term can be ignored (by setting $\xi_c = 0$).

The above model is incorporated in RCONV. The listing for the subroutine is shown in Figure A-15. The variables are defined in Table A-6.

Table A-6 Definition of Variables in Subroutine RCONV

I	=	Receive Polarization Index
J	=	Frequency Indicator
RPAR(5)	=	σ_1
RPAR(6)	=	σ_2
RPAR(7)	=	σ_3
RPAR(8)	=	σ_4
RPAR(I+9)	=	σ_6
RPAR(I+11)	=	σ_7
RPAR(I+13)	=	σ_8
RPAR(I+15)	=	σ_5
RPAR(17)	=	σ_9
EST	=	$\epsilon_c T_L$
DATA(28)	=	T_S
DATA(32)	=	T_0
DATA(46)	=	T_c
DATA(18)	=	T_g

G. Subroutine DOPCHK

1. Introduction

This subroutine computes the doppler frequency shift induced by the relative motion between aircraft and sea. The doppler shift is compared with the doppler filter characteristic to determine whether the shift is within the bandpass. When it is, a frequency index IBAND, which is employed to locate the filter gain, is computed. When the doppler shift lies outside the defined doppler filter characteristic, the band index is set at the appropriate extreme and a flag is set.

```

SUBROUTINE RCONV (DATA, IDATA, RPAR, RCAL, IL)
C      CONVERT RADIOMETER
C      SUBROUTINE RCONV (DATA, IDATA, RPAR, RCAL, IL)
C      THIS PROGRAM WAS PREPARED BY
C      JOHN P. CLAASSEN
C      GLEN E. ELLICOTT
C      UNIVERSITY OF KANSAS CENTER FOR RESEARCH
C      THIS PROGRAM CONVERTS RADIOMETER OUTPUT VOLTAGES TO ANTENNA
C      TEMPERATURE.
C00010 DIMENSION DATA(1), IDATA(1), RPAR(1), RCAL(1)
C      FOR POLARIZATION AND FREQUENCY INDEX.
C00010 I=IDATA(1)
C00011 J=IDATA(2)
C      EXTRACT LOAD TEMPERATURES
C00012 T1 = DATA(3)
C00014 T2=DATA(2)
C00015 IF (J.EQ.3) T2=DATA(27)
C      FORM MEASUREMENT PARAMETER.
C00021 DATA(13)=-((DATA(15)-RCAL(1))/(RCAL(2)-RCAL(1)))
C      APPLY TEMPERATURE FACTORS.
C00026 DATA(13)=DATA(13)*(RPAR(5)*T1-RPAR(6)*T2)+RPAR(7)*T1+RPAR(8)*T2-
* RPAR(11)*DATA(28)-RPAR(11)*DATA(32)-RPAR(11)*
* DATA(46) - RPAR(15)*DATA(18)
C      APPROXIMATE MISSING DATA
C      APPROXIMATING PARAMETER
C00062 C=0.00012*DATA(14)*DATA(14)
C      FOR HORIZONTAL POLARIZATION
C00065 EST=DATA(13)*(1.0+C)/(1.0-C)
C      FOR VERTICAL POLARIZATION
C00071 IF (I.EQ.1) EST = DATA (13)*(1.0-C)/(1.0+C)
C      FORM ANTENNA TEMPERATURES
C00100 DATA(13) = DATA(13) - EST*RPAR(I+3)
C00104 RETURN
C00105 END

```

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FIGURE A-15. FORTRAN LISTING FOR SUBROUTINE RCONV
90

2. Theory and Design

For non-relativistic speeds the two way doppler frequency shift is known to be given by

$$f_d = 2 \langle \vec{v} \cdot \vec{r}_r \rangle \frac{f}{c} \quad (1)$$

where \vec{r}_r = boresight unit vector
 \vec{v} = aircraft velocity
 f = operating frequency
 c = speed of light

Denote ϕ_c as the cross-track angle and θ as the incident angle (see subroutine ANGLE). Then the boresight vector is given by

$$\vec{r}_r = -\sin \theta \cos \phi_c \vec{r}_x + \sin \theta \sin \phi_c \vec{r}_y - \cos \theta \vec{r}_z \quad (2)$$

Also

$$\vec{v} = v \vec{r}_x \quad (3)$$

So

$$\vec{v} \cdot \vec{r}_r = -v \sin \theta \cos \phi_c \quad (4)$$

and

$$f_d = -2 \frac{f v}{c} \sin \theta \cos \phi_c \quad (5)$$

Expression (5) is the desired result.

Now the computer routine determines whether the doppler shift falls in the doppler bandwidth as defined by the upper and lower limits, SPAR(23) and SPAR(22), respectively. If f_d is between SPAR(22) and SPAR(23), f_d is divided by the doppler filter gain sample interval SPAR(24) and the result rounded off to determine the band index (IBAND) from the center frequency. When the shift is outside the bandpass, the band index is set at the appropriate extreme and a flag is set. An error message is also appended to the Conversion Report. A listing of DOPCHK is shown in Figure A-16. The variables employed by the routine are defined in Table A-7.

```

SUBROUTINE DOPCHK (DATA,SPAR,IL,IBAND,LNPMOD,IFLAG)
C DOPCHK      CHECK DOPPLER SHIFT
C      SUBROUTINE DOPCHK (DATA,SPAR,IL,IBAND,LNPMOD,IFLAG)
C      ---
C      THIS PROGRAM WAS PREPARED BY
C      JOHN P. CLAASSEN
C      GLEN E. ELLIOTT
C      UNIVERSITY OF KANSAS CENTER FOR RESEARCH
C
C      THIS SUBROUTINE COMPUTES THE DOPPLER SHIFT INDUCED BY THE
C      RELATIVE MOTION BETWEEN AIRCRAFT AND SEA. THE DOPPLER SHIFT
C      IS COMPARED WITH THE DOPPLER FILTER CHARACTERISTIC TO
C      DETERMINE WHETHER SHIFT IS WITHIN THE BANDPASS AND WHEN
C      IT IS TO SELECT THE DOPPLER FILTER GAIN RELATIVE TO THE
C      CALIBRATION SIGNAL.
C00011      DIMENSION DATA(1), SPAR(1)
C00011      DATA DEGRAD/0.0174532525/
C      INITIALIZE FLAG
C00011      IFLAG=0
C      CONVERT AIRCRAFT SPEED TO METERS/SEC
C00011      VEL=DATA (42)/3.048
C      CONVERT TO RADIAN
C00013      THETA = DATA (14)*DEGRAD
C00015      PHI=DATA(15)*DEGRAD
C      COMPUTE THE DOPPLER SHIFT
C00017      DOP=-2.0*SPAR(1)*VEL/299793000.0*SIN(THETA)*COS(PHI)
C      IF DOPPLER SHIFT EXCESSIVE FORM FLAG
C00036      IF(DOP.LT.SPAR(22)) GO TO 10
C00041      IF(DOP.GT.SPAR(23)) GO TO 20
C      FORM DOPPLER BAND INDEX
C00044      IBAND=-DOP/SPAR(24)+0.5
C00047      IF (DOP.GT.0.0) IBAND= -DOP/SPAR(24)-0.5
C00053      RETURN
C      FORM FLAG AND ASSIGN BAND
C00054      10  IBAND = -SPAR(22)/SPAR(24)
C00057      GO TO 30
C00060      <0  IBAND = -SPAR(23)/SPAR(24)
C00063      >0  IFLAG=1
C00064      IF(MOD(IL,LNPMOD).EQ.0) WRITE (6,40) IL,DATA(42),DATA(14),DOP
000115      40  FORMAT (14,5X,1H*,1X,17HEXCESSIVE DOPPLER,21X,1H*,5X,
*          13HAIRCRAFT SPD=,F5.1,5X,11HVIEW ANGLE=,F5.1,5X,
*          14HDOPPLER SHIFT=,F6.0)
C00115      RETURN
000116      END

```

FIGURE A-16. FORTRAN LISTING OF SUBROUTINE DOPCHK

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Table A-7 Definition of Variables

IFLAG	=	Flag for Excessive Doppler
VEL	=	Aircraft Ground Velocity
THETA	=	Incident Angle
PHI	=	Cross-track Angle
DOP	=	Doppler Shift
IBAND	=	Doppler Band Index
SPAR(22)	=	Lower Doppler Filter Limit
SPAR(23)	=	Upper Doppler Filter Limit
SPAR(24)	=	Doppler Filter Sample Interval

H. Subroutine SCONV

1. Introduction

SCONV converts scatterometer output measurements into a normalized input power. The scatterometer transfer function is employed to perform the conversion. The transfer function is developed below. Certain significant simplifications arise when SCAT normal calibrations are employed.

2. Theory and Design

The block diagram for the RADSCAT scatterometer is shown in Figure A-17. The front-end elements have been decomposed into a calibration element G_c , transmission elements G_{VT} , G_{HVT} , G_{HT} , and G_{VHT} and reception elements G_{VR} , G_{HVR} , G_{HR} and G_{VHR} for ease in analysis and reduction of data. The transfer functions account for mis-match and loss. Calibration attenuators A_1 through A_4 are employed to calibrate the output channels 1 through 4, respectively.

During calibration transmitter power is routed sequentially through A_1 , A_2 , A_3 and A_4 and the respective channel output is noted. The resulting output voltage for the i^{th} channel is thus given by

$$V_i^{(c)} = d^2 P_x G_c G_R A_i \alpha_i I_i \tau_c \quad (1)$$

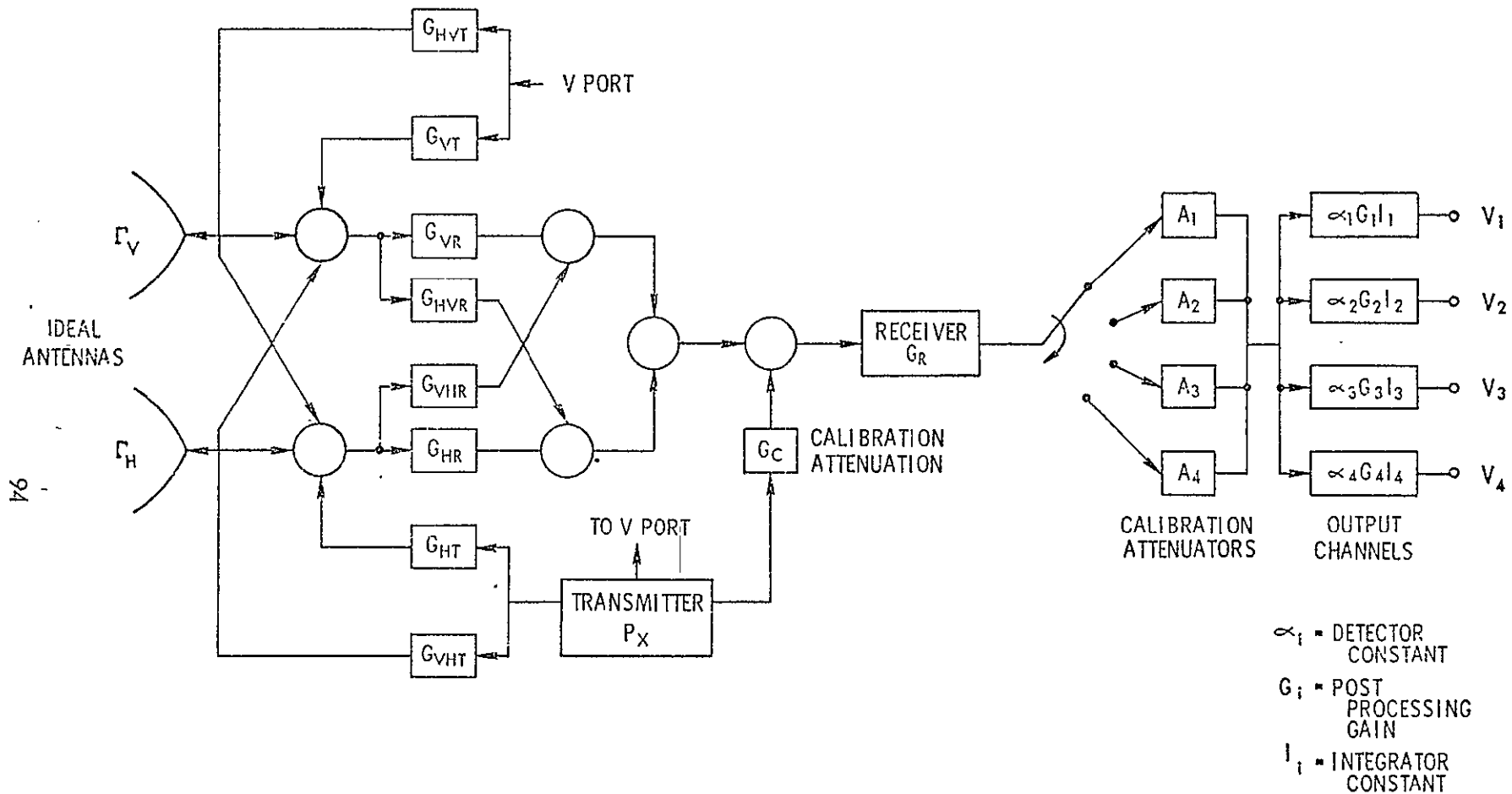


FIGURE A-17. BLOCK DIAGRAM FOR SCATTEROMETER

where d = the effective duty factor
 P_x = transmitter peak power
 τ_c = calibration integration period

The factor d^2 occurs in the above expression since only the center frequency of the power spectrum is sampled by the receiver. The calibrations thus serve as a measure of the transmitted power

$$P_x = \frac{V_L^{(c)}}{d^2 G_c G_R A_i \alpha_i G_i I_i \tau_c} \quad (2)$$

During measurements at VV polarization and incident angle θ_0 , the power arriving at the receiver input is given by

$$P_{VV}(\theta_0) = \frac{\lambda^2}{(4\pi)^3} d^2 P_x \left[G_{VV} \Gamma_V I_{VV}(\theta_0) \Gamma_V G_{VT} \right. \\ \left. + G_{VHR} \Gamma_H I_{HV}(\theta_0) \Gamma_V G_{VT} + G_{HVR} \Gamma_H I_{HH}(\theta_0) \Gamma_H G_{HVT} \right. \\ \left. + G_{VR} \Gamma_V I_{VH}(\theta_0) \Gamma_H G_{HVT} \right] \quad (3)$$

where

$$I_{mn} = \iint_{4\pi} \frac{P_m(\chi, \psi) P_n(\chi, \psi) \sigma_{mn}(\theta)}{R^4} dA \quad (4)$$

σ_{mn} = normalized scattering coefficient for transmission at polarization n and reception at polarization m

R = range to scattering element dA

P_m = normalized antenna pattern

Γ_m = antenna directivity at polarization m

λ = operating wavelength

Similarly for observations at HH polarization the power at the receiver input is given by

$$P_{HH}(\theta_0) = \frac{\lambda^2}{(4\pi)^3} d^2 P_x \left[G_{HR} \Gamma_H I_{HH}(\theta_0) \Gamma_H G_{HT} \right. \\ \left. + G_{HVR} \Gamma_V I_{VH}(\theta_0) \Gamma_H G_{HT} + G_{VHR} \Gamma_V I_{VV}(\theta_0) \Gamma_V G_{VHT} \right. \\ \left. + G_{HR} \Gamma_H I_{HV}(\theta_0) \Gamma_V G_{VHT} \right] \quad (5)$$

The latter three terms in expressions (3) and (5) may be neglected since products such as $G_{HVR} I_{VH}$, $G_{VHR} G_{VHT}$, $I_{HV} G_{VHT}$, etc., are extremely small. Therefore (3) and (5) simplify to:

$$P_{VV}(\theta_0) = \frac{\lambda^2 d^2 G_x}{(4\pi)^3} G_{VR} \Gamma_V I_{VV}(\theta_0) \Gamma_V G_{VT} \quad (6)$$

and

$$P_{HH}(\theta_0) = \frac{\lambda^2 d^2 G_x}{(4\pi)^3} G_{HR} \Gamma_H I_{HH}(\theta_0) \Gamma_H G_{HT} \quad (7)$$

The corresponding on-scale output voltage for these measurements occur on say, channels j and k , respectively. The outputs are given by

$$V_{jm} = P_{VV}(\theta_0) G_R \alpha_j G_j I_j \tau_m \quad (8)$$

and

$$V_{km} = P_{HH}(\theta_0) G_R \alpha_k G_k I_k \tau_m \quad (9)$$

where τ_m = measurement integration time
 $m = 1, 2, \dots, 7$

A subscript is employed on τ to identify the different integration periods associated with six angle indicators (1 through 6) for the ALTERNATING and FIXED ANGLE MODES and the integration period τ_7 unique to the SHORT SCAT mode.

Now equations(8) and (9) may be employed to express the receiver input power. Thus we may write

$$\frac{V_{jm}}{G_R \alpha_j G_j I_j \tau_m} = \frac{\lambda^2 d^2 P_x}{(4\pi)^3} G_{VR} G_{VT} \Gamma_V^2 I_{VV}(\theta_0) \quad (10)$$

$$\frac{V_{km}}{G_R \alpha_k G_k I_k \tau_m} = \frac{\lambda^2 d^2 P_x}{(4\pi)^3} G_{HR} G_{HT} \Gamma_H^2 I_{HH}(\theta_0) \quad (11)$$

Now P_x may be replaced by expression (2) for the corresponding output channel to yield the desired results

$$I_{VV}(\theta_o)_j = \frac{V_{jm}}{V_i^{(c)}} \frac{\tau_c}{\tau_m} \frac{G_c A_j}{G_{VR} G_{VT} \Gamma_v^2} \frac{(4\pi)^3}{\lambda^2} \quad (12)$$

and

$$I_{HH}(\theta_o)_k = \frac{V_{km}}{V_k^{(c)}} \frac{\tau_c}{\tau_m} \frac{G_c A_k}{G_{HR} G_{HT} \Gamma_H^2} \frac{(4\pi)^3}{\lambda^2} \quad (13)$$

It is noted that the receiver gain terms have dropped out.

Subroutine SCONV implements the algebraic expressions for I_{VV} and I_{HH} . Actually the SCAT channel selection routine in CRUNCH applies the factors A_m and $V_m^{(c)}$ ($m = j$ or k) since they are channel dependent. Missing from these algebraic expressions is the doppler filter gain factor which is a function of the doppler frequency shift. The gain is normalized with respect to the gain at zero doppler since the calibrations are made there. An equally spaced sample version of this filter characteristic must appear in the lower part of SPAR. The filter gain at zero doppler must appear at SPAR(50). Down doppler filter gains must be stored in entries between SPAR(51) and SPAR(85) whereas entries for the up-doppler gain must appear between SPAR(34) and SPAR(50). Presently the gain function is sampled at 250 Hz intervals. To compensate the measurement, the relative doppler gain must divide the measurement, DATA(8).

The FORTRAN coding for SCONV is shown in Figure A-18. The variables are defined in Table A-8.

Table A-8		Definition of Variables
DATA(8)	=	Selected Channel Output, V_{jm}
INT	=	Integration Period Index
IDATA(3)	=	RADSCAT Mode
SPAR(3)	=	Calibration Period
SPAR(INT+3)	=	Measurement Period
SPAR(IBAND+50)	=	Relative Doppler Filter Gain
SPAR(17)	=	Calibration Attenuation, G_c

	SUBROUTINE SCCNV (DATA, IDATA, SPAR, IBAND)	00001019
CSCONV	SCAT CONVERSION	00001020
C	SUBROUTINE SCGNV (DATA, IDATA, SPAR, IBAND)	00001021
C	-----	00001022
C	THIS PROGRAM WAS PREPARED BY	00001023
C		00001024
C	JOHN P. CLAASSEN	00001025
C	GLEN E. ELLIOTT	00001026
C		00001027
C	UNIVERSITY OF KANSAS CENTER FOR RESEARCH	00001028
C		00001029
C		00001030
C	THIS SUBROUTINE CONVERTS A SCATTEROMETER NORMALIZED OUTPUT	00001031
C	VOLTAGE TO THE SCATTERING INTEGRAL. THE RESULT IS LEFT	00001032
C	IN DATA(8).	00001033
C		00001034
C00007	DIMENSION DATA(1), IDATA(1), SPAR(1)	00001035
C00007	DATA PI/3.1415927/	00001036
C		00001037
C		00001038
C	APPLY CONVERSION PARAMETERS	00001039
C		00001040
C00007	DATA(8) = DATA(8)*(4.*PI)**3/(299793000./SPAR(1))**2	00001041
C		00001042
C	SET INTEGRATION TIME INDEX	00001043
C		00001044
C00014	INT = IDATA (5)	00001045
C00015	IF (IDATA (5) .EQ. 1) INT = 7	00001046
C		00001047
C	COMPENSATE FOR INTEGRATION TIMES	00001048
C		00001049
C00020	DATA(8) = DATA(8)*SPAR(3)/SPAR(INT+3)	00001050
C		00001051
C	SET POLARIZATION INDICES	00001052
C		00001053
C00024	IXMIT = IDATA (6)	00001054
C00025	IREC = ILATA (7)	00001055
C		00001056
C	COMPENSATE FOR DOPPLER FILTER CHARACTERISTIC	00001057
C		00001058
C00027	DATA(8) = DATA(8)/SPAR(1BAND+50)	00001059
C		00001060
C		00001061
C	APPLY GAIN FACTORS	00001062
C		00001063
C00031	DATA(8) = DATA(8)*SPAR(17)/(SPAR(IXMIT+11)*SPAR(IXMIT+25)*	00001064
	* SPAR(IREC+15)*SPAR(IREC+25))	00001065
C00041	RETURN	00001066
C00042	END	00001067

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FIGURE A-18. SOURCE LISTING FOR SUBROUTINE SCGNV

Table A-8 Definition of Variables (Continued)

IXMIT	=	Transmit Polarization Index
IREC	=	Receive Polarization Index
SPAR(IXMIT+11)	=	Transmit Transfer Function
SPAR(IREC+15)	=	Receive Transfer Function
SPAR(IXMIT+25)	=	Transmit Antenna Gain
SPAR(IREC+25)	=	Receive Antenna Gain

V. SPECIAL ROUTINES

A. Tape Read Routines

FUNCTION subroutine IREAD and subroutine READ1 are employed to read the Input Raw Data records. IREAD permits CRUNCH to read records from either file code 01 or 08. IREAD calls READ1 to unblock records from file code 01. The records on the scratch unit (08) are not blocked and so can be read from IREAD. A second entry point in READ1 permits subroutine CALIB to backspace one physical record (DATA). Read functions on unit 1 may be performed by simply calling READ1. The source listings for IREAD and READ1 are shown in Figures A-19 and A-20, respectively.

B. Tape Write Routine

Subroutine WRITE2 performs WRITE functions on file code 02. Output records (IARRAY) are accumulated in IBLOCK until it is full at which time IBLOCK is written to file code 02. A second entry point in WRITE2 performs the END OF FILE function. However, the remainder of IBLOCK is first filled with zeros before putting an EOF mark on file code 02. See the listing for WRITE2 in Figure A-21 for further insight.

C. Subroutine ABORT

To purposely stop the execution of the program and abort the job, an abort function was provided. The circumstances under which an abort is executed are described in Section III B. If the system has an abort routine available that dumps more registers and memory than this fatal execution will, it is advisable to replace the one provided. A listing of subroutine ABORT is shown in Figure A-22.

C
C
C
C
C
C
C
C
C
C

THIS PROGRAM WAS PREPARED BY
 GLEN E. ELLIOTT
 UNIVERSITY OF KANSAS CENTER FOR RESEARCH, INC.

THIS SUBROUTINE READS BLOCKS OF 10 PHYSICAL RECORDS AND
 SEPARATES THEM. RECORDS FILLED WITH 99999. ARE BY-PASSED
 UNTIL AN ECF IS ENCOUNTERED. A SECONDARY ENTRY POINT
 IS PROVIDED TO PERMIT BACKSPACING INDIVIDUAL RECORDS
 WITHIN A BLOCK.

C00002		COMMON/INPUT/IECF,DATA(50)	C0000393
C00002		LOGICAL IECF	00000394
C00002		DIMENSION BLOCK(50,10)	00000395
C00002		DATA NDX,NUT/0,1/	00000396
C00002		IECF=.FALSE.	00000397
C00003		IF(NDX.NE.0) GO TO 10	00000398
C00004		NDX=1	00000399
C00005		READ(NUT) BLOCK	00000400
C00012		IF(EOF,NUT) GO TO 10	00000401
C00015	10	IF(BLOCK(1,NDX).EQ.99999.) GO TO 90	00000402
C00022		DO 20 I = 1,10	00000403
C00023	20	DATA(I) = BLOCK(I,NDX)	00000404
C00033		NDX=NDX+1	00000405
C00034		IF(NDX.GT.10) NDX=0	00000406
C00037		RETURN	00000407
C00040	90	READ(NUT)	00000408
C00043		IF(EOF,NUT) GO TO 90	00000409
C00046	100	IECF=.TRUE.	00000410
C00047		NDX=0	00000411
C00050		RETURN	00000412
C00051		ENTRY BACKSP1	00000413
C00050		IF(NDX.LT.1) NDX=11	00000414
C00052		NDX=NDX-1	00000415
C00053		RETURN	00000416
C00064		END	00000417

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FIGURE A-20. LISTING FOR READ1

SUBROUTINE WRITE2 (IARRAY)

C0000418

C
C
C
C
C
C
C
C
C
C
C

THIS PROGRAM WAS PREPARED BY
GLEN E. ELLIOTT
UNIVERSITY OF KANSAS CENTER FOR RESEARCH, INC.

THIS ROUTINE BLOCKS 20 WORD RECORDS INTO 20 RECORD
GROUPS (BLOCKS) AND WRITES THE BLOCK OUT TO FILE UNIT
02. WHEN INSUFFICIENT RECORDS EXIST TO FILL A BLOCK
THE REMAINING PORTION IS FILLED WITH ZEROES AS PROVIDED
AT THE SECONDARY ENTRY POINT. AN EOF IS APPENDED
TO THE FILE THEREAFTER.

C00003		DIMENSION IBLCK(20,20), IARRAY(1)	00000419
C00003		DATA INDEX /1/	00000420
C00003		DC 20 I = 1,20	00000421
C00005	20	IBLOCK(I,INDEX) = IARRAY(I)	00000422
000015		INDEX = INDEX + 1	00000423
C00016		IF (INDEX .LE. 20) RETURN	00000424
000021		WRITE (2) IBLCK	00000425
C00026		INDEX = 1	00000426
000027		RETURN	00000427
C00030		ENTRY ENDF2	00000428
C00036		IF (INDEX .LE. 1) GO TO 30	00000429
C00042		DO 25 I = INDEX,20	00000430
C00043		DO 25 J = 1,20	00000431
C00044	25	IBLOCK(J,I) = 0	00000432
C00054		WRITE (2) IBLCK	00000433
C00061		INDEX=1	00000434
C00062	30	ENDFILE 2	00000435
000064		RETURN	00000436
C00065		END	00000437

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FIGURE A-21. LISTING FOR WRITE2

		SUBROUTINE ABCRT(A)	C0000368
	C	HALT PROGRAM IN CASE OF ERROR	00000369
C00005		DIMENSION IECR(2)	00000370
C00006		DATA IECR/10HEND OF REE,1HL/	00000371
C00007		WRITE (6,100) A	00000372
C00011	100	FORMAT (10X,10-ABCRT CODE,1X,A10)	00000373
C00011		CALL ENDF2	00000374
C00012		WRITE(2) IECR,(1,1=3,9)	00000375
C00024		B=A/0.0+1.0	00000376
C00030		STOP	00000377
C00032		END	00000378

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FIGURE A-22. LIST FOR SUBROUTINE ABCRT

APPENDIX B

OUTPUT PROGRAM

I. INTRODUCTION

The output program (OUTPUT) lists groups of output files produced by the conversion program. External directives permit the user to select file types to be listed. This appendix describes the operation of OUTPUT. In the description below it will be helpful to refer to the logic diagram of Figure B-1 and the listing of Figure B-2.

II. DESIGN AND OPERATION

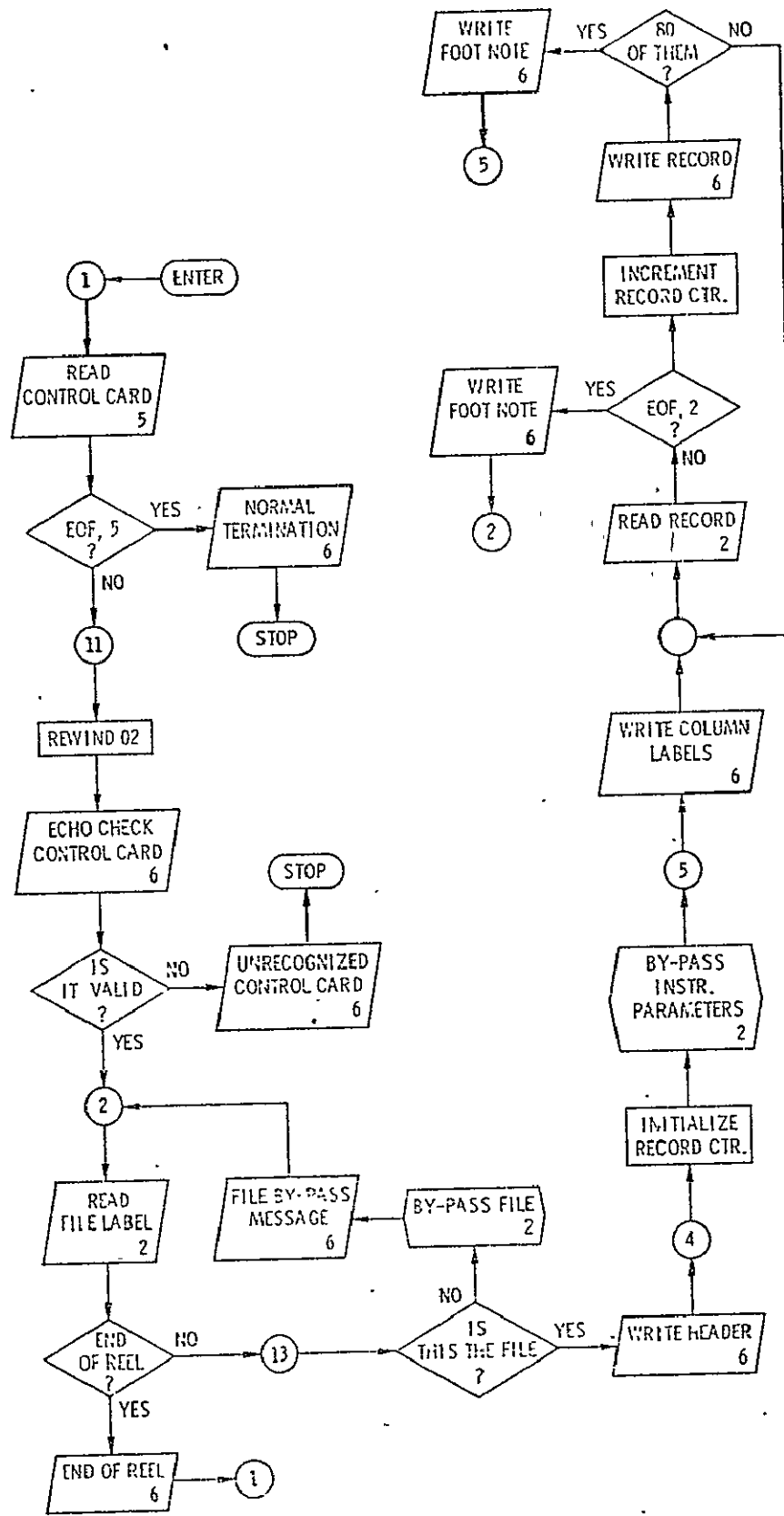
Upon entry into OUTPUT a control card is read. The format and content of the control card is treated in Section III C. The card content is printed and its validity is checked. An invalid command terminates the program. The tape on unit 2 is also rewound. The file label is read and compared with the validated directive. If the file label does not agree with the label, the file is bypassed and a bypass message is printed. The search continues until the appropriate file is found; if in the search the end of reel is encountered, a message to that effect is printed and another control card is read (statement 1).

Specified file types are listed 80 records at a time. Each record is identified with a record number. The listing continues until the file is exhausted (EOF) at which time another file of the same type is sought.

The variables employed in OUTPUT are defined in Table B-1.

Table B-1 Definition of Variables

MISSD	=	Directed Mission Number
FLTD	=	Directed Flight Number
LIND	=	Directed Line Number
RUND	=	Directed Run Number



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FIGURE B-1. DESCRIPTIVE LOGIC DIAGRAM FOR OUTPUT PROGRAM

```

PROGRAM CLIPUT(INPUT,OUTPUT,TAPE2,TAPE5=INPUT,TAPE6=OUTPUT)
COOUTPUT          OUTPUT PROGRAM
C
C      . . . . . THIS PROGRAM WAS PREPARED BY
C
C              JOHN P. CLAASSEN
C              GLEN E. ELLICOTT
C
C              UNIVERSITY OF KANSAS CENTER FOR RESEARCH
C
C00003      INTEGER FLTD, RUND, FLT, RUN
C00003      DIMENSION DATA(20), DATE(3)
C00003      DIMENSION LSTYP(4), IMODE(4), IPL(2)
C00003      DIMENSION IEOR(2)
C00003      LOGICAL ECF2
C00003      EQUIVALENCE (MCGE, DATA(2)),
C          *      (IP1, DATA(5)), (IP2, DATA(6))
C00003      DATA IEOR/10HEND OF REE, IHL/
C00003      DATA IMODE/4HR.C., 4HS.S., 4HF.A., 4FA.A./, IFL/1HM, 1HV/
C00003      DATA LSTYP/6HFLTLIN, 6HMISFLT, 6HMSPECIF, 3HALL/
C          C      GET DIRECTIVE AND FILE ID.
C00003      1      REAL(5,100) LTYPE, MISSD, FLTD, LIND, RUND
C00021      100     FORMAT(A6,4X,4I5)
C00021      IF(EOF,5) 10,11
C00024      11      REWIND 2
C00026      WRITE(6,200) LTYPE, MISSD, FLTD, LIND, RUND
C00044      200     FORMAT(1H1,///10X13HCCNTROL CARU=,3X,A6,4X,4I5//)
C00044      DO 20 I = 1,4
C00046      20      IF(LTYPE.EQ.LSTYP(I)) GO TO 2
C00052      WRITE(6,700)
C00055      700     FORMAT(1H1,///10X22HUNRECCGNIZED DIRECTIVE)
C00055      STOP
C          C      FIND THE FILE.
C00057      2      CONTINUE
C00057      WRITE(6,300)
C00063      300     FORMAT(1H1)
C00063      READ(2) MISS, FLT, DATE, LIN, RUN, FREQ, FEED
C00104      IF(MISS.NE.IEOR(1)) GO TO 13
C00106      IF(FLT.NE.IEOR(2)) GO TO 13
C00110      WRITE(6,400)
C00114      400     FORMAT(///10X10(1H*),11HEND OF REEL,10(1H*)//)
C00114      GO TO 1
C          C      CONTINUE
C00115      13     CONTINUE
C00115      IF(LTYPE.EQ.LSTYP(4)) GO TO 4
C00117      IF(MISS.NE.MISSD) GO TO 3
C00121      IF(FLT.NE.FLTD) GO TO 3
C00123      IF(LTYPE.EQ.LSTYP(2)) GO TO 4
C00125      IF(LIN.NE.LIND) GO TO 3
C00127      IF(LTYPE.NE.LSTYP(3)) GO TO 4
C00131      IF(RUN.EQ.RUND) GO TO 4
C00133      WRITE(6,500) MISS, FLT, LIN, RUN
C00146      500     FORMAT(//10X13H-BYPASSED FILE,4I5)
C00146      3      READ(2)
C00151      IF(EOF,2) 2,3
C          C      FOUND IT, OUTPUT HEADINGS.
C00154      4      CONTINUE
C00154      WRITE(6,604)
C00160      604     FORMAT(1H1,53X,14HMICROWAVE DATA)
C00160      LINEN=0
C          C      BYPASS IC RECCRD.
C00161      READ(2) ICSET, ID1, ID2, ID3
C00174      WRITE(6,600) MISS, FLT, DATE, LIN, RUN, FREQ, FEED,
C          *      ICSET, ID1, ID2, ID3
C00226      600     FORMAT(/9H MISSICN-,13,5H FLIGHT-,13,
C          *      7H DATE-,2I3,15,2X,11H FLT LINE-,1X,16,6H RUN-,13,
C          *      13H FREQUENCY-,F5.1,7H FEED-,2X,A6,8H IPAR=,I2,3I3/)
C00226      WRITE(6,605)
C00232      605     FORMAT(/
C          *      62H RECORD TIME MODE INCIID CROSS XMIT REC S INT
C          *      >3HSCAT SCAT RAD DEPCL S/R ALTITUDE,
C          *      11H FLT /,
C          *      62H NO. ANGLE ANGLE POL POL TIME
C          *      52H DE FACTOR CODE ,
C          *      11H DIRECT /,
C          *      62H (DEG) (DEG) (SEC)
C          *      >3H (DEG K) (FEET),
C          *      12H (DEG) -- //)
C          C      OUTPUT ONE DOUBLE COMPUTER PAGE.
C00232      DO 6 I=1,60
C00234      CALL READ2(DATA, EOF2)
C00236      IF(EOF2) GO TO 7
C00240      12     LINFN=LINEN+1
C00242      MUDE=IMODE(MODE+1)
C00243      IP1=IPL(IP1+1)
C00245      IP2=IPL(IP2+1)

```

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FIGURE B-2. SOURCE LISTING FOR PROGRAM OUTPUT
106

```

000246      6      WRITE(6,601) LINE#, (LATA(I), I = 1,14)
000264      601      FORMAT
C
*          MATCH HEADING WITH FORMATS.
*          # LINE      TIME      MODE      INCID CRCSX      XMIT REC      S INT
*          # NO.      ANGLE ANGLE      PCL      PUL      TIME
*          #          (DEG) (DEG)
*          * (1X,14, 2X,F8.1,3X, A6, F5.1,2X, F5.1,6X, A5, A1,4X, F5.3,2X,
C
*          #SCAT      SCAT      RAD DEPOL S/R      ALTITUDE#,
*          #          DB          FACTOR CODE      #,
*          #          (DEG K)          (FEET)#,
*          * E11.4, 2X,F6.1,2X, F7.1, F8.3, 19, F10.0,
C
*          # FLT      #/,
*          # DIREC    #/,
*          # (DEG)    #)
*          * F9.1)
C
C          FOOT PAGE WITH CODE KEY.
000264      WRITE(6,602)
000270      602      FORMAT(/,14H KEY TC CODES-/,
*          25X,32H 0 NO FLAG          #,5X,
*          21H 1000 POLAR REVERSAL/,
*          25X,* 1 POSSIBLY OUTSIDE RANGE GATE*,5X,
*          22H 10000 EXCESSIVE DEPOL/,
*          25X,32H 10 OUTSIDE DYNAMIC RANGE      #,5X,
*          24H100000 REC TEMP ABNORMAL/,
*          25X,* 100 EXCESSIVE DOPPLER          #,4X,
*          *1000000 WARM LOAD TEMP ESTIMATED*/,
*          25X,37H COMBINATIONS OF FLAGS CAN OCCUR./,14H)
000270      GO TO 5
C          FOOT PARTIAL PAGE
000271      7      WRITE(6,602)
000275      IF(LTYPE.EQ.LSTYP(3)) GO TO 1
000277      GO TO 2
000300      10     STOP
000302      END

```

```

: CC0C1367
00001368
00001369
*,00001370
*,00001371
*,00001372
00001373
00001374
00001375
00001376
00001377
00001378
CC001379
00001380
00001381
00001382
CC001383
00001384
00001385
00001386
00001387
00001388
00001389
00001390
00001391
00001392
00001393
00001394
00001395
00001396
00001397
00001398
00001399
CC0C1400
00001401
CC001402
CC0C1403

```

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Figure B-2. (Continued)

Table B-1 Definition of Variables (Continued)

MISS	=	File Mission Number
FLT	=	File Flight Number
LIN	=	File Line Number
RUN	=	File Run Number
LTYPE	=	Control Directive
LSTYPE	=	Program Recognized Directives
IEOR	=	10H End of Reel
DATA	=	Output Data
EOF2	=	EOF Indicator on File Code 02

III. SUBROUTINE READ2

READ2 performs the record retrieval function for OUTPUT. Output files are blocked in 20 record groups. READ2 retrieves these blocks and withdraws records as required by OUTPUT. The end of the file indicator EOF2 is generated by READ2. A listing for this routine appears in Figure B-3.

		SUBROUTINE READ2(ILATA,EOF2)	00001404
C			
C		THIS PROGRAM WAS PREPARED BY	
C		GLEN E. ELLIOTT	
C		UNIVERSITY OF KANSAS CENTER FOR RESEARCH, INC.	
C			
C		THIS ROUTINE UNBLOCKS 20 RECORD BLOCKS AND PROVIDES	
C		AN END OF FILE INDICATOR, EOF2.	
C			
000005		DIMENSION IADATA(20), IBLOCK(20,20)	00001405
000005		LOGICAL LGF2	00001406
000005		DATA NDEX/0/	00001407
000005		EOF2=.FALSE.	00001408
000005		IF(NDEX.NE.0) GO TO 10	00001409
000006		NDEX=1	00001410
000007		REAL(2) IBLOCK	00001411
000014		IF(EOF,2) 100,10	00001412
000020	10	IF(1BLOCK(1,NDEX).EQ.0) GO TO 90	00001413
000023		DO 20 I=1,20	00001414
000025	20	IADATA(I)=IBLOCK(I,NDEX)	00001415
000035		NDEX=NDEX+1	00001416
000036		IF(NDEX.GT.20) NDEX=0	00001417
000041		RETURN	00001418
000042	90	READ(2)	00001419
000045		IF(EOF,2) 100,90	00001420
000051	100	EOF2=.TRUE.	00001421
000052		NDEX=0	00001422
000053		RETURN	00001423
000054		END	00001424

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FIGURE B-3. SOURCE LISTING FOR SUBROUTINE READ2

APPENDIX C

INSTRUMENT CHARACTERISTICS MAINTENANCE PROGRAM (ICHAR)

I. INTRODUCTION

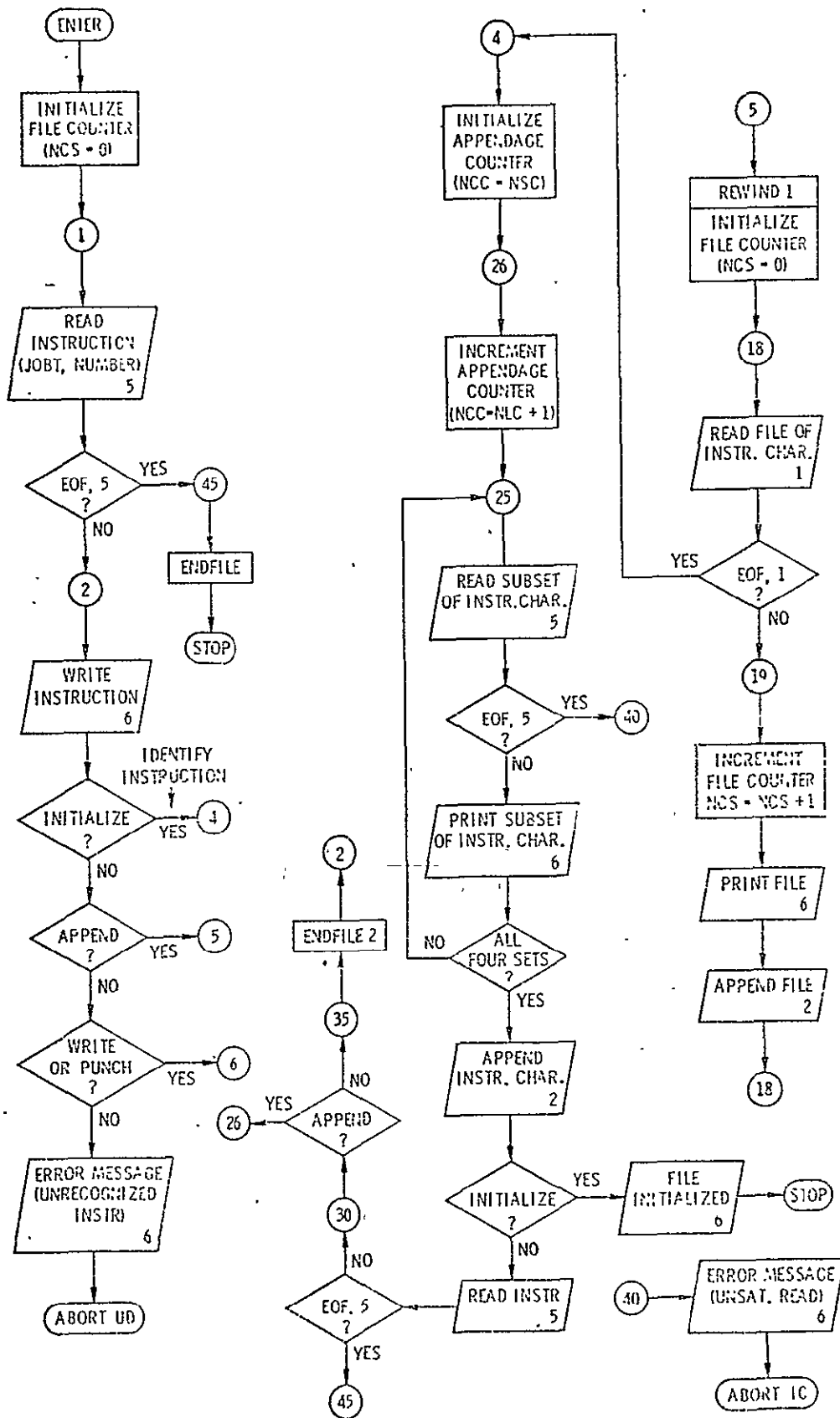
Program ICHAR maintains a historical file of RADSCAT instrument characteristics. New sets of instrument parameters may be submitted to ICHAR for storage; old sets may be printed or punched. The design and operation of ICHAR is treated in this appendix. The reader will find it helpful to refer to the logic diagram (Figure C-1) and listing (Figure C-2) for ICHAR.

II. DESIGN AND OPERATION

The files on the historical parameter tape are identified numerically. So upon entry into the program the file pointer is initialized to zero. An instruction is read and echo checked. The instruction is then identified as one of three types. If the instruction is INITIALIZE, the file appendage counter (NNC) is set equal to one and four subsets of instrument parameters are read and transferred to file code 02. The format and entry for the parameters were described in Section III D of the text. The program is then halted.

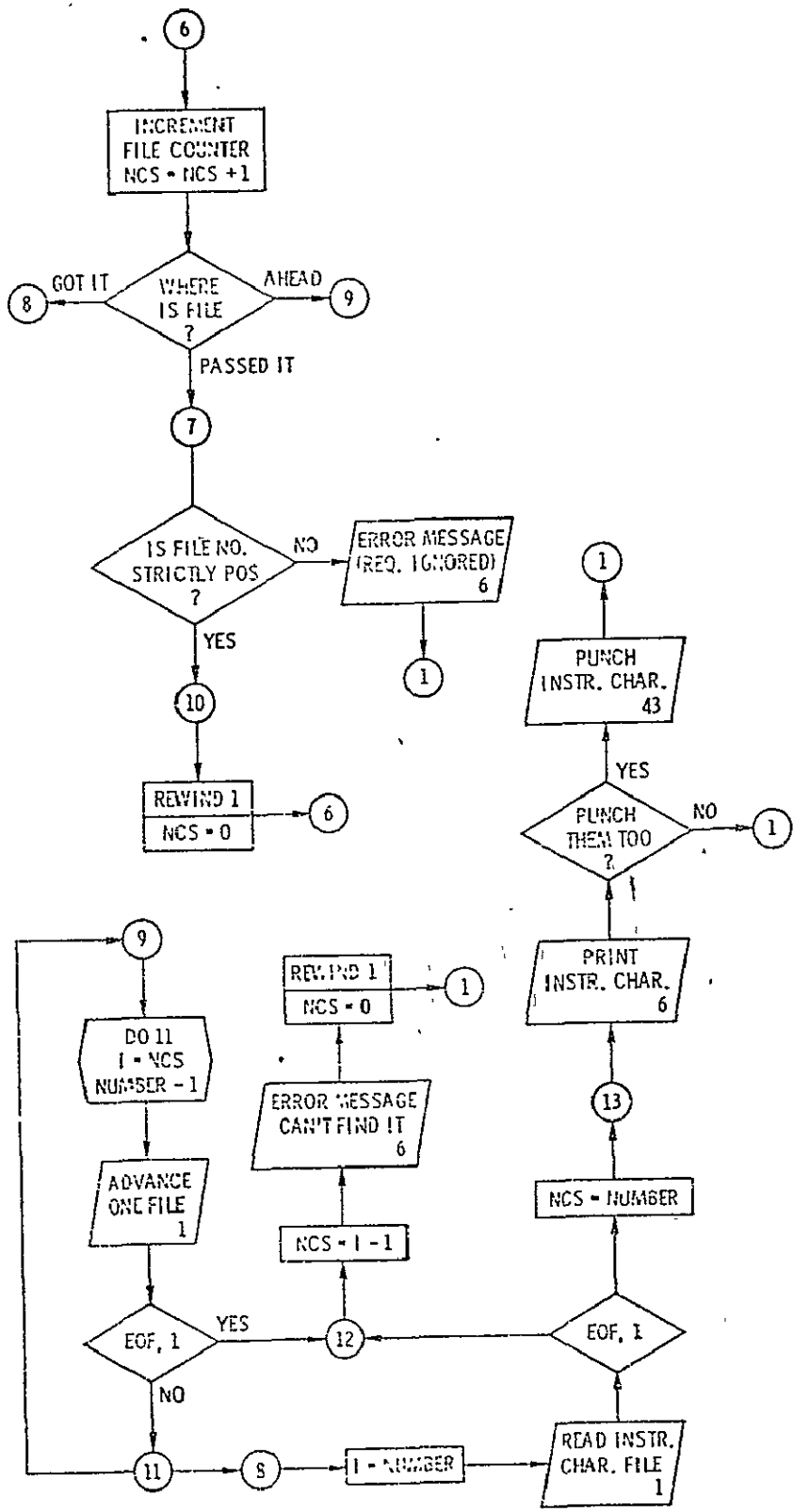
If the historical tape had been initialized already and the command was APPEND, the old historical tape would have been rewound (Statement 5) and the contents of that tape transferred to another one (Statements between 5 and 18). Once transferred, the new set would be appended to the new file (Statements 26 through 23). When insufficient parameters are presented to fill the new file, the program is aborted. Otherwise the next control card is read; if it is APPEND, the process is repeated until all APPEND commands have been executed.

If the (next) command had been PRINT or PUNCH, the program would have advanced to statement 6 and executed the instruction. The program continues until all control cards have been exhausted.



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FIGURE C-1. DESCRIPTIVE FLOW CHART
FOR PROGRAM ICHAR



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FIGURE C-1. (continued)

```

PROGRAM ICHAR(INPUT,OUTPUT,PUNCH,TAPE1,TAPE2,
* TAPE5=INPUT,TAPE6=OUTPUT,TAPE4)=PUNCH)
C ICHAR          MAINTAIN ICHAR FILE.
C
C              THIS PROGRAM WAS PREPARED BY
C
C              JOHN P. CLAASSEN
C              GLEN E. ELLIOTT
C
C              UNIVERSITY OF KANSAS CENTER FOR RESEARCH, INC.
C
C              THIS PROGRAM WILL STORE RADSCAT INSTRUMENT
C              CHARACTERISTICS ON A HISTORICAL TAPE. THE HISTORICAL
C              TAPE IS INITIALLY PREPARED BY USING THE DIRECTIVE
C              *INITIALIZE* . TO APPEND NEW SETS OF CHARACTERISTICS THE
C              COMMAND *APPEND* WILL TRANSFER OLD SETS FROM TAPE UNIT
C              1 TO TAPE UNIT 2 AND APPEND THE NEW SET . NEW SETS ARE
C              READ FROM CARDS. PREVIOUSLY STORED SETS MAY
C              BE PRINTED OR PUNCHED BY USING THE COMMANDS PRINT OR
C              PUNCH RESPECTIVELY. THE SET NO. MUST BE DESIGNATED .
C              THE SETS WILL HAVE BEEN STORED NUMERICALLY IN ORDER ON
C              THE TAPE. TO MAINTAIN THE INSTRUMENT CHARACTERISTICS
C              IT IS ADVISABLE TO RETAIN THE OLD TAPE WHEN A
C              NEW ONE IS PREPARED. OLDER VERSIONS MAY BE DISCARDED.
C              IT IS ADVISABLE ALSO TO USE A TAPE COMPARISON UTILITY
C              PROGRAM TO VERIFY THE TRANSFER.
C
C              NCS = FILE COUNTER FOR THE OLD TAPE ALSO SERVES AS
C              A FILE POINTER ON UNIT 1
C              NCC = FILE COUNTER FOR THE APPENDED SETS
C              JOPT = EXTERNAL DIRECTIVE. SEE DATA STATEMENT
C              NUMBEP = NUMBER OF THE REQUESTED FILE
C              PAR = INSTRUMENT PARAMETERS
C              IDAT = DATE
C              NUM2 = SET NO. AS READ FROM TAPE
C
000003          DIMENSION PAR(160,4), IDAT(3), IOPT(4)
000003          DATA IOPT/10#INITIALIZE,6#APPEND,5#PRINT,5#PUNCH/, NCS/0/
C              READ DIRECTIVE AND SET NUMBER.
000003          1  READ(5,500) JOPT, NUMBER
000013          IF (FOF,5) 45,2
000016          500  FORMAT(A10,15)

000016          2  WRITE(6,600) JOPT,NUMBEP
000026          600  FORMAT(IH1,///# DIRECTIVE IS *,A10,15)
C              CHECK DIRECTIVE
000026          DO 3 N=1,4
000030          IF (JOPT.EQ. IOPT(N)) GO TO(4,5,6,6)*N
000041          3  CONTINUE
000043          WRITE(6,601)
000047          601  FORMAT(///# UNRECOGNIZED DIRECTIVE*//)
000047          CALL ABORT(2#H0)
C              FIND FILE
000051          6  NCS = NCS+1
000053          IF (NUMBER-NCS) 7,8,9
000055          7  IF (NUMBER.GE.1) GO TO 10
000060          WRITE(6,602) NUMBER
000065          602  FORMAT(///# IC SET NUMBEP*,15,* DOES NOT EXIST.*,
* REQUEST IGNORED,*//)
000065          GO TO 1
000066          10  REWIND 1
000070          NCS = 0
000071          GO TO 6
000072          12  NCS = I-1
000074          WRITE(6,608) NCS,NUMBER
000104          608  FORMAT(///# THERE ARE ONLY*15,* FILES.*
* CANT FIND FILE*15//)
000104          REWIND 1
000106          NCS = 0
000107          GO TO 1
C              FORWARD SPACE TO CORRECT SET.
000110          9  NUM=NUMBER-1
000112          DO 11 I=NCS,NUM
000114          READ(1)
000117          IF (FOF,1) 12,11
000122          11  CONTINUE
C              READ INSTRUMENT CHARACTERISTICS
000125          8  I = NUMBEP
000127          READ(1) NUM2,IDAT,PAR
000140          IF (FOF,1) 12,13
000143          13  NCS=NUMBER
C              WRITE INSTRUMENT CHARACTERISTICS.
000145          WRITE(6,610)
000150          610  FORMAT(IH1,///)
000150          DO 15 I=1,4
000152          WRITE(6,603) NUM2 ,IDAT,PAR(1,1),PAR(2,1),PAR(3,1)

```

FIGURE C-2. SOURCE LISTING FOR PROGRAM ICHAR

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```

000174 60J  FORMAT(// * SET*, I5, * DATE*, J15, F15, 4, 5X, A10, E15, 4)
000174 DO 14 J=4,75,7
000176 L=J+6
000200 IF (L.GT.75) L=75
000203 14  WRITE (6,604) (PAR(K,I),K=J,L)
000222 604  FORMAT(7E15,4)
000222 WRITE (6,603) NU 12 , IDAT, PAR(76,I), PAR(77,I), PAR(78,I)
000245 DO 15 J=79,160,7
000247 L=J+6
000251 IF (L.GT.160) L=160
000254 15  WRITE (6,604) (PAR(K,I),K=J,L)
000275 IF (N.EQ.3) GO TO 1
C          PUNCH IC#S.
000277 DO 17 I=1,4
000301 LL=1
000302 WRITE (43,4303)  NUM2, IDAT , PAR(1,I), PAR(2,I), PAR(3,I),
*          NUMBER, I, LL
000333 4303 FORMAT(4I5,10X,E10,3,A10,E10,3,12X,12,11,15)
000333 DO 16 J=4,75,7
000335 LL=LL+1
000337 L=J+6
000341 16  WRITE (43,4304) (PAR(K,I),K=J,L), NUMBER, I, LL
000364 4304 FORMAT(7E10,3,2X,12,11,15)
000364 LL=LL+1
000366 * WRITE (43,4303)  NUM2, IDAT , PAR(1,I), PAR(2,I), PAR(3,I),
*          NUMBER, I, LL
000416 DO 17 J=79,160,7
000420 LL=LL+1
000422 L=J+6
000424 17  WRITE (43,4304) (PAR(K,I),K=J,L), NUMBER, I, LL
000451 GO TO 1
C
C          COPY OLD IC#S
C
000452 5  REWIND 1
000454 * NCS = 0
000455 WRITE (6,605)
000461 605  FORMAT(1H1, * THE FOLLOWING IC SETS WERE COPIED FROM *,
* THE OLD FILE*, /
* * SET NUMBER ID NUMBER DATE*)
000461 18  READ(1) NUM2, IDAT, PAR
000472 IF (EOF,1) 4,19
000475 19  NCS = NCS+1

000477 WRITE (6,606) NCS, NUM2, IDAT
000510 606  FORMAT(3X, I5, 9X, I5, 3X, J15)
000510 WRITE (2) NUM2, IDAT, PAR
000521 GO TO 18
C          READ NEW SETS.
000522 4  NCC = NCS
000524 26  NCC = NCC+1
000526 WRITE (6,607)
000531 607  FORMAT(1H1, * THE FOLLOWING IC SETS WERE APPENDED TO *
* THE OUTPUT FILE.*)
000531 25  DO 23 I=1,4
000533 READ (5,4303) NUMBER, IDAT, PAR(1,I), PAR(2,I), PAR(3,I)
000555 IF (FOF,5) 40,20
000560 20  WRITE (6,603) NCC, IDAT, PAR(1,I), PAR(2,I), PAR(3,I)
000603 DO 21 J=4,75,7
000605 L=J+6
000607 IF (L.GT.75) L=75
000612 READ (5,4304) (PAR(K,I),K=J,L)
000627 IF (FOF,5) 40,21
000632 21  WRITE (6,604) (PAR(K,I),K=J,L)
000651 READ (5,4303) NUMBER, IDAT, PAR(76,I), PAR(77,I), PAR(78,I)
000674 IF (EOF,5) 40,22
000677 22  WRITE (6,603) NCC, IDAT, PAR(76,I), PAR(77,I), PAR(78,I)
000722 DO 23 J=79,160,7
000724 L=J+6
000726 IF (L.GT.160) L=160
000731 READ (5,4304) (PAR(K,I),K=J,L)
000746 IF (FOF,5) 40,23
000751 23  WRITE (6,604) (PAR(K,I),K=J,L)
C          APPEND IC#S
000772 WRITE (2) NCC, IDAT, PAR
001003 IF (JOBT.NE.IOPT(1)) GO TO 29
001005 WRITE (6,800)
001011 800  FORMAT(//10X * FILE INITIALIZED*//)
001011 STOP
001013 29  READ (5,500) JOBT, NUMBER
001023 IF (FOF,5) 45,35
001026 30  IF (JOBT.EQ. IOPT(2) ) 26,35
001033 35  E=FILE 2
001035 GO TO 2
001036 40  WRITE (6,609)
001042 609  FORMAT (// * UNSATISFIED READ, *
* * INCOMPLETE SET OF CHARACTERISTICS*//)

```

Figure C-2. (continued)

```
001042      CALL ABORT, (2HIC)
001044      45  ENDFILE 2
001046      STOP
001050      END
```

```
00001622
00001623
```

```
          SUBROUTINE ABORT(A)
C
C      HALT PROGRAM IN CASE OF ERROR
C
000003      WRITE (6,100) A
000011      100  FORMAT (10X,10HABORT CODE,1X,A10)
000011      ENDFILE 2
000013      R=A/0.0+1.0
000017      STOP
000021      END
```

Figure C-2. (Continued)

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III. DEFINITION OF VARIABLES

The variables employed by ICHAR are defined in Table C-1.

Table C-1 Definition of Variables

NSC	=	File Pointer for File Code 01
NCC	=	File Pointer for File Code 02
JOBT	=	Job Instruction
NUMBER	=	File Number to be Printed or Punched
IOPT	=	Array of Recognized Instructions
IDAT	=	Date in Parameters
NUM2	=	Set Number as Read from File Code 01
PAR	=	Set of Instrument Parameters

APPENDIX D

PROGRAM TDUPE

I. INTRODUCTION

Program TDUPE is a translation and duplication program which prepares an integer version of the output tape. It is intended that copies of the integerized tape be sent to the investigators upon request for use on other computing machines. A utility program may be used to prepare additional copies. This appendix describes the design and operation of TDUPE. Helpful to the reader are the flow charts of Figure D-1 and the program listing of Figure D-2.

II. DESIGN AND OPERATION

Action in TDUPE is initiated by an external control card specifying the files, by mission and flight, which are to be copied. A file counter is initialized, file unit 1 is rewound, and the instruction is listed. The labels on the files are examined and compared with the instruction. Files not having the designated mission and flight are bypassed until one is found. At this time a record counter is initialized. Then the instrument parameters are read, scaled, and integerized. The file heading and instrument parameters are transferred to file unit 2. The file heading is also listed on the printer and the file counter is incremented.

Consecutive records are then read, scaled and integerized. In each instance the record counter is incremented. The records are accumulated in blocks by subroutine WRITE2 and transferred to tape unit 2 when the block is filled. The terminating block is filled with integer zeroes when there are insufficient records to fill it. When the file has been exhausted, an EOF is appended to the transferred file and a message is given to indicate the number of records which have been transferred.

The search for additional files continues until the end of the reel is encountered. At this point another instruction is sought. The program terminates

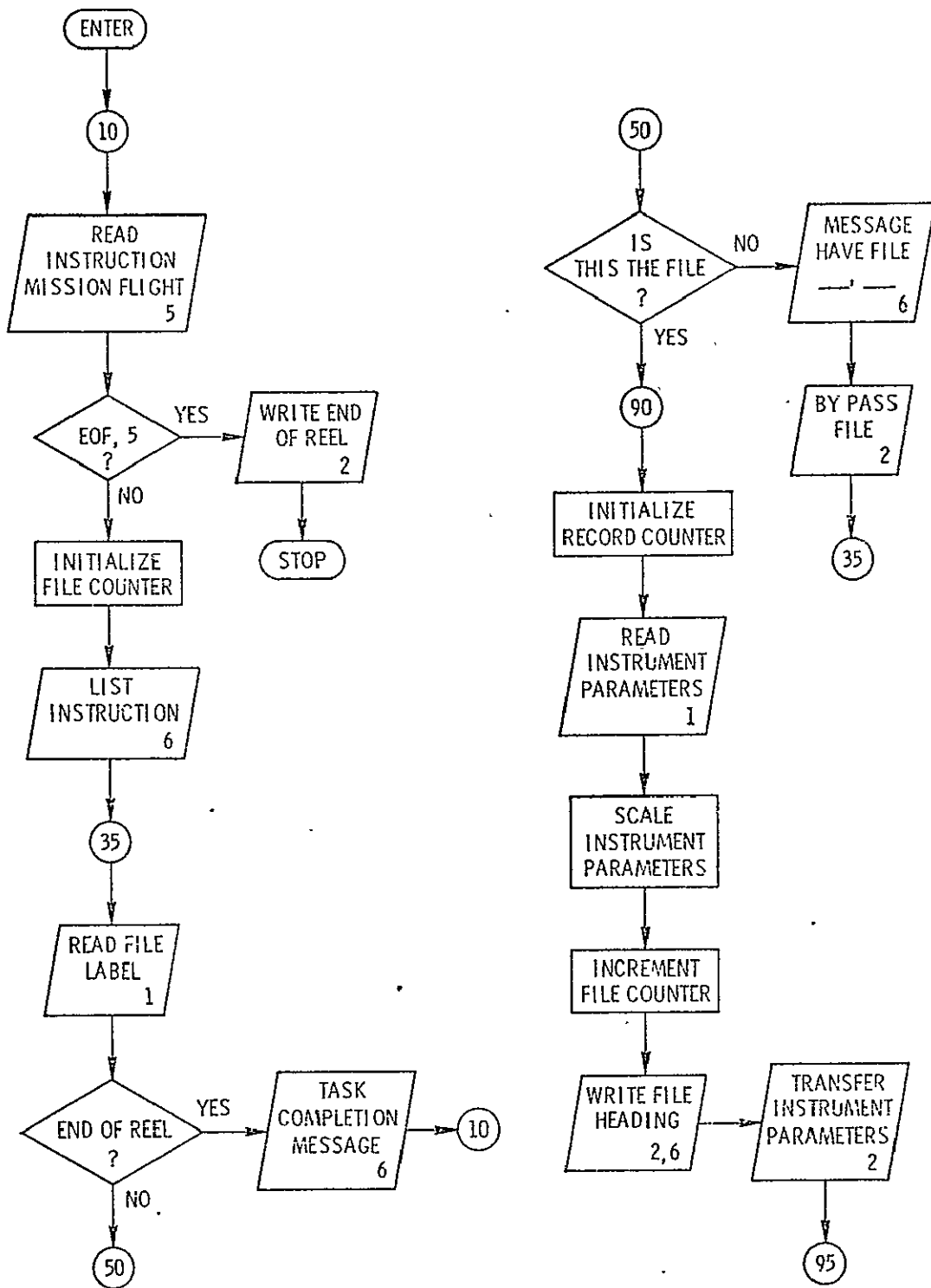
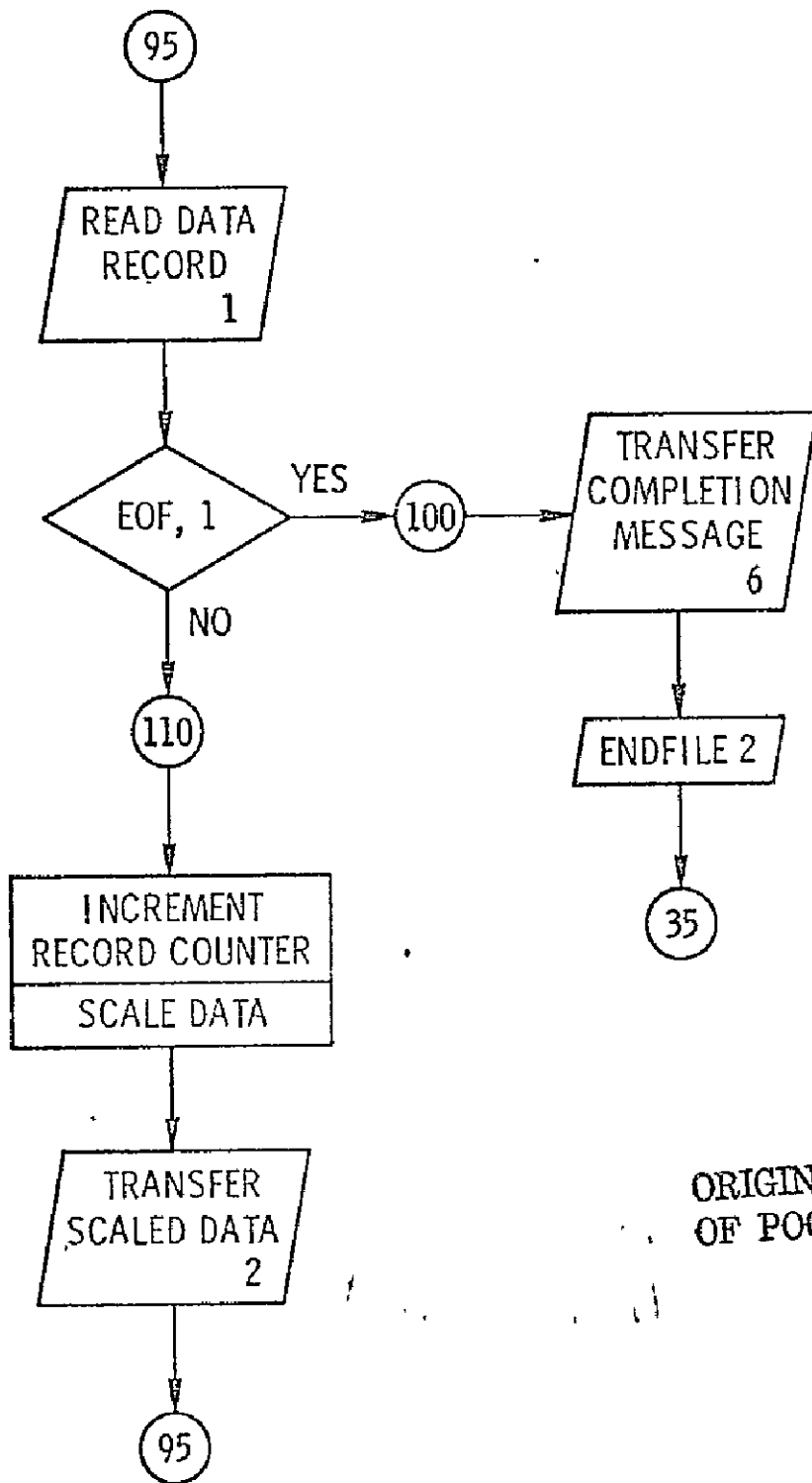


FIGURE D-1. DESCRIPTIVE LOGIC DIAGRAM FOR PROGRAM TDUPE

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FIGURE D-1. (continued)


```

000104 4000 FORMAT (11X, *FILE HEADING * 215 * DOES NOT AGREE WITH DIRECTIVE 00001421
      * *215) 00001422
C 00001423
C BY-PASS UNWANTED FILE 00001424
C 00001425
000104 80 READ (1) 00001426
000107 IF (EOF,1) 35,80 00001427
C 00001428
C INITIALIZE RECORD COUNT 00001429
C 00001430
000112 90 IREC = 0 00001431
000113 READ (1) LCHAR, ICHAR 00001432
C 00001433
C SCALE AND TRANSFER INSTR. PARAMETERS 00001434
C 00001435
000122 ICHAR(1)=RPAR(1)*1.0E-6 00001436
000125 DO 91 I=3,20 00001437
000127 91 ICHAR(I)=RPAR(I)*1.0E4 00001438
000134 ICHAR(21)=RPAR(21)*10.0 00001439
000137 ICHAR(22)=RPAR(22)*10.0 00001440
000142 DO 92 I=23,75 00001441
000143 92 ICHAR(I)=RPAR(I)*1.0E4 00001442
000150 ICHAR(76)=SPAR(1)*1.0E-6 00001443
000153 DO 93 I=3,16 00001444
000155 93 ICHAR(I+75)=SPAR(I)*1.0E4 00001445
000162 DO 96 I=17,31 00001446
000164 96 ICHAR(I+75)=SPAR(I)*SFAC(I-16) 00001447
000171 DO 97 I=32,85 00001448
000173 97 ICHAR(I+75)=SPAR(I)*1.0E4 00001449
000200 WRITE (6,5000) (IHEAD(I),I=1,7) 00001450
000212 5000 FORMAT (/11X,*HAVE MISSION*15,* FLT*14,* DATE*315* FLT LINE*A6, 00001451
      * * RUN*13) 00001452
C 00001453
C UPDATE FILE COUNTER. 00001454
C 00001455
000212 NOF = NOF + 1 00001456
000214 WRITE(2) IHEAD 00001457
000221 WRITE(2) LCHAR, ICHAR 00001458
000230 95 CALL READ1(DATA,EOF1)
000232 IF (.NOT.EOF1) GO TO 110
000234 100 WRITE (6,6000) IREC,NOF 00001461
000244 6000 FORMAT (/11X,I4* RECORDS HAVE BEEN TRANSFERRED FROM FILE* I3//) 00001462
000244 CALL ENDF2

000245 GO TO 35 00001464
C 00001465
C UPDATE RECORD COUNTER. 00001466
C 00001467
000246 110 IREC = IREC + 1 00001468
C 00001469
C SCALE AND TRANSFER RADSCAT MEASUREMENTS. 00001470
C 00001471
000250 IARRAY(1)=DATA(1)*100.0 00001472
000253 IARRAY(2)=IDATA(2) 00001473
000254 IARRAY(3)=DATA(3)*100.0 00001474
000257 IARRAY(4)=DATA(4)*100.0 00001475
000261 IARRAY(5)=IDATA(5) 00001476
000263 IARRAY(6)=IDATA(6) 00001477
000264 IARRAY(7)=DATA(7)*10000.0 00001478
000267 IF (DATA(8) .LT. 1.0E-03) GO TO 120 00001479
000272 IARRAY(8) = DATA(8)*1.0 E06 00001480
000275 IARRAY(9)=1000000 00001481
000276 GO TO 130 00001482
000277 120 IARRAY(8)=DATA(8)*1.0E+09 00001483
000302 IARRAY(9)= 1000000000 00001484
000304 130 IARRAY(10)=DATA(9)*100.0 00001485
000307 IARRAY(11)=DATA(10)*100.0 00001486
000312 IARRAY(12) = DATA(11)*10000.0 00001487
000315 IARRAY(13)=IDATA(12) 00001488
000316 IARRAY(14)=DATA(13)*10.0 00001489
000321 IARRAY(15)=DATA(14)*100.0 00001490
000324 IARRAY(16)=DATA(15)*100.0 00001491
000327 CALL WRITE2(IARRAY)
000330 GO TO 95 00001493
000331 END 00001494

```

Figure D-2. (Continued)

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```

SUBROUTINE READ1(IDATA,EOF1)
000005 DIMENSION IDATA(20), IBLOCK(20,20)
000005 LOGICAL FOF1
000005 DATA NDEX/0/
000005 EOF1=.FALSE.
000005 IF(NDEX.NE.0) GO TO 10
000006 NDEX=1
000007 READ(1) IBLOCK
000014 IF(EOF.1) 100,10
000020 10 IF(IBLOCK(1,NDEX).EQ.0) GO TO 90
000023 DO 20 I=1,20
000025 20 IDATA(I)=IBLOCK(1,NDEX)
000035 NDEX=NDEX+1
000036 IF(NDEX.GT.20) NDEX=0
000041 RETURN
000042 90 READ(1)
000045 IF(EOF.1) 100,90
000051 100 EOF1=.TRUE.
000052 NDEX=0
000053 RETURN
000054 END

```

```

SUBROUTINE WRITE2 (IARRAY)
000003 DIMENSION IBLOCK(20,20), IARRAY(1)
000003 DATA INDEX /1/
000003 DO 20 I = 1,20
000005 20 IBLOCK(I,INDEX) = IARRAY(I)
000015 INDEX = INDEX + 1
000016 IF (INDEX .LE. 20) RETURN
000021 WRITE (2) IBLOCK
000026 INDEX = 1
000027 RETURN
000030 ENTRY ENDF 2
000036 IF (INDEX .LE. 1) GO TO 30
000042 DO 25 I = INDEX,20
000043 DO 25 J= 1,20
000044 25 IBLOCK(J,I) = 0
000054 WRITE (2) IBLOCK
000061 INDEX=1
000062 30 ENDFILE 2
000064 RETURN
000065 END

```

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when there are no additional instructions. However, before terminating an end of reel statement is written on file unit 2.

The variables are defined in Table D-1.

IHEAD	=	File Label
LCHAR	=	Instrument Parameters Label
ICHR	=	Instrument Parameters
DATA	=	Input Records
IDATA	=	Integer Equivalent
IARRAY	=	Output Records
IEOR	=	11HEND of Reel
SFACT	=	Scale Factors

APPENDIX E

SPECIAL PROGRAMS

I. INTRODUCTION

Two special engineering routines WIDTH and GAIN prepare several antenna parameters essential to the reduction of the scatterometer data. WIDTH computes the equivalent beamwidth of the RADSCAT antenna; whereas GAIN computes the antenna directivity. Other parameters of special interest to antenna engineers are also computed in GAIN. These programs are provided with the realization that the antenna pattern may eventually change through an alteration of the antenna. In this case the equivalent beamwidth and gain should then be recomputed based on new pattern information and the instrument parameters changed accordingly.

Each of the programs are described below. Operating instructions are given in Section IV F of the main text.

II. PROGRAM WIDTH

The theory for this program was described in Appendix A, Section III B. In that development it is apparent that the equivalent beamwidth is given by

$$\theta_{eq} = \sqrt{\frac{4}{\pi} \int_0^{2\pi} \int_0^{\pi} P^2(\theta, \phi) \sin \theta \, d\theta \, d\phi} \quad (1)$$

where $P(\theta, \phi)$ is the normalized power pattern function described in the standard spherical coordinate system (r, θ, ϕ) . When the pattern is elliptically symmetric, the integration may be limited to one quadrant in which case

$$\theta_{eq} = \sqrt{\frac{16}{\pi} \int_0^{\pi} \int_0^{\pi/2} P^2(\theta, \phi) \sin \theta \, d\theta \, d\phi} \quad (2)$$

Here it is assumed that the main beam lies on the x-axis as shown in Figure E-1. It is convenient to work in terms of elevation angle ϵ rather than polar angle in which case

$$\theta_{eq} = \sqrt{\frac{16}{\pi} \int_0^{\pi} \int_0^{\pi/2} P^2(\theta, \phi) \cos \epsilon \, d\epsilon \, d\phi} \quad (3)$$

Since quadrature techniques usually require rectangular domains of integration, it is necessary to apply the transformation

$$\psi = \sin \epsilon \quad (4)$$

so that

$$\theta_{eq} = \sqrt{\frac{16}{\pi} \int_0^{\pi} \int_0^1 P^2(\psi, \phi) \, d\psi \, d\phi} \quad (5)$$

The full limits of integration are not necessary since the integral converges rapidly over the main beam. Program WIDTH whose listing is shown in Figure E-2 use this property to advantage. As shown in the driver routine, the upper limits of integration are progressively increased by 1/2 degree intervals in ϵ . The convergence of the equivalent beamwidth can then be observed as the domain increases to include more of the beam.

A Gaussian-Legendre quadrature technique is employed to perform the double integration. This technique is embodied in RINTEG. The reader is referred to Klerer and Korn* or any other advanced text on numerical techniques for a discussion of this technique.

The main beam of the RADSCAT antenna pattern is functionally represented in the FUNCTION subroutine FUN. RINTEG calls FUN repeatedly to evaluate the pattern function squared.

* Klerer, M. and Korn, G. A., "Digital Computer User's Handbook," McGraw-Hill Book Company, 1970.

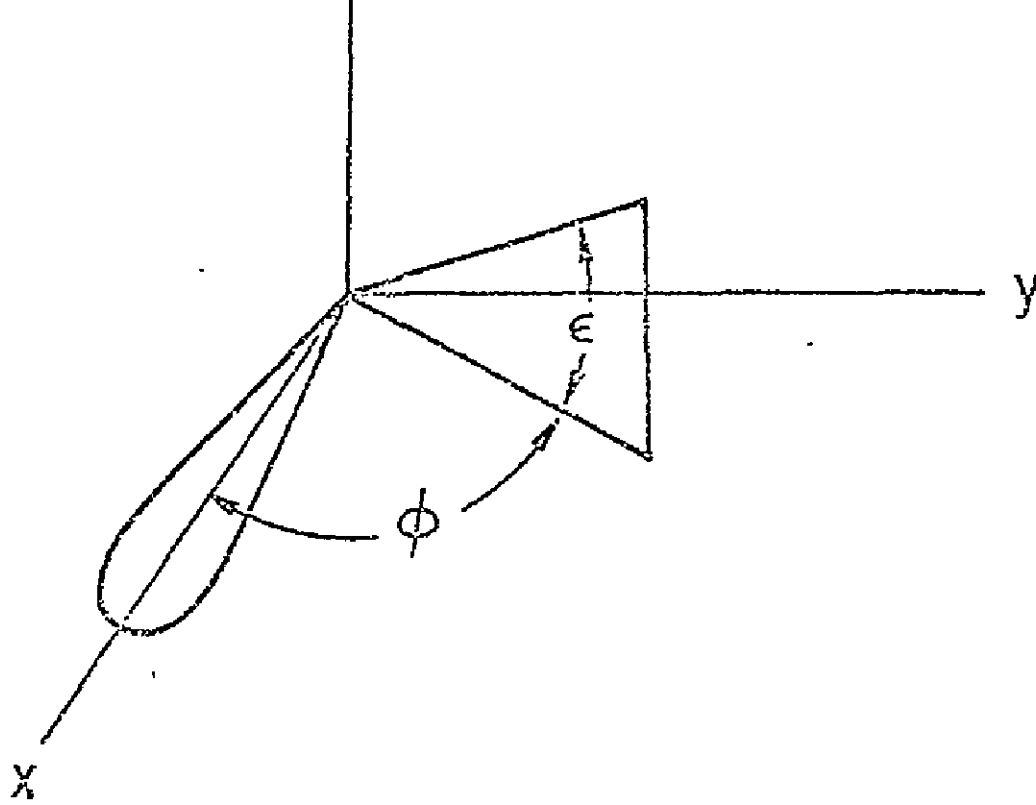


FIGURE E-1. ANTENNA PATTERN GEOMETRY FOR WIDTH

```

PROGRAM WIDTH(OUTPUT,TAPE6=OUTPUT)                                00000001
C                                                                    00000002
C                                                                    00000003
C      THIS ROUTINE DETERMINES THE EQUIVALENT (PENCIL)           00000004
C      BEAMWIDTH FOR AN ANTENNA WHOSE PATTERN IS SPECIFIED      00000005
C      IN SUBROUTINE FUN. SUBROUTINE RINTEG INTEGRATES           00000006
C      THE PATTERN BY A QUASSIAN (LEGENDRE) QUADRATURE METHOD.   00000007
C      INTEGRATION ARE REPETIVELY PERFORMED AT ONE DEGREE      00000008
C      INTERVALS OUT TO SIX DEGREES. THE EQUIVALENT             00000009
C      BEAMWIDTH IS CHOSEN FROM THE LISTING AT THE POINT AT    00000010
C      WHICH THE VALUES BEGIN TO CONVERGE                       00000011
C                                                                    00000012
C      THIS PROGRAM WAS PREPARED BY                               00000013
C                                                                    00000014
C      JOHN P. CLAASSEN                                          00000015
C                                                                    00000016
C      UNIVERSITY OF KANSAS                                       00000017
C      CENTER FOR RESEARCH.                                       00000018
C                                                                    00000019
C                                                                    00000020
000003      EXTERNAL-FUN                                          00000021
000003      DATA PI/3.14159265/                                  00000022
000003      WRITE (6,300)                                         00000023
000007      300  FORMAT (1H1//)                                    00000024
000007      WRITE (6,100)                                          00000025
000013      100  FORMAT(30X,5(1H*),*SEARCH FOR THE EQUIVALENT BEAMWIDTH*5(1H*)//) 00000026
000013      DO 20 I=1,6                                           00000027
000015      X2 = 0.0174532925*FLOAT(I)*0.50                     00000028
000017      Y2 = X2                                               00000029
000021      X2 = SIN(X2)                                          00000030
000023      X1 = 0.0                                              00000031
000024      Y1 = 0.0                                              00000032
000025      IX = 10*I                                             00000033
000030      CALL RINTEG (FUN, Z, X2, X1, Y2, Y1, IX, IX, 4, 4)   00000034
000041      RFAW = SQRT (16.0*Z/PI)/0.0174532925                00000035
000047      WRITE (6,200) I, BEAM                                00000036
000056      200  FORMAT (10X,*ACTIVE BEAMWIDTH IS *I3,* DEGREES, WHEREAS*, 00000037
* THE EQUIVALENT BEAMWIDTH IS*F5.2,* DEGREES*)
000056      20  CONTINUE                                          00000038
000060      STOP                                                  00000039
000062      END                                                  00000040

000056      DO 30 I = 1,MP                                        00000083
000057      SY(I) = SAMPLE(MP,I)*HDELY                            00000084
000066      30  CONTINUE                                          00000085
000070      DO 50 I = 1,NP                                        00000086
000071      DO 40 J = 1,MP                                        00000087
000072      C(I,J) = COEF(NP,1)*COEF(MP,J)                       00000088
000106      40  CONTINUE                                          00000089
000110      50  CONTINUE                                          00000090
000112      DO 40 N=1,NX                                         00000091
000114      X1=X2                                                00000092
000116      X2=X1+DELX                                           00000093
000120      XM = X1 + HDELX                                       00000094
000121      Y2 = Y1P                                              00000095
000122      DO 80 M=1,MY                                         00000096
000124      Y1 = Y2                                               00000097
000126      Y2 = Y1 + DELY                                       00000098
000130      YM = Y1 + HDELY                                       00000099
000131      DO 70 I=1,MP                                          00000100
000133      X=SX(I)+XM                                           00000101
000136      DO 60 J=1,MP                                          00000102
000137      Y=SY(J)+YM                                           00000103
000142      SUM = SUM+C(I,J)*FUN(X,Y)                             00000104
000160      60  CONTINUE                                          00000105
000162      70  CONTINUE                                          00000106
000164      80  CONTINUE                                          00000107
000167      90  CONTINUE                                          00000108
000171      ZZ = SUM*DELX*DELY*0.250                             00000109
000174      RETURN                                              00000110
000175      END                                                  00000111

```

FIGURE E-2. SOURCE LISTING FOR WIDTH

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```

SUBROUTINE RINTEG (FUN,ZZ,X2P,X1P,Y2P,Y1P,NNX,MMY,NNP,MMP)      00000041
THIS ROUTINE EMPLOYS A GAUSSIAN LEGENDER QUADRATURE           00000042
INTEGRATION PROCEDURE. INTEGRATION OVER X-Y SEGMENTS        00000043
ARE PERFORMED AFTER TRANSLATION TO (-1,1)x(-1,1).           00000044
FUN= INTEGRAND FUNCTION                                       00000045
ZZ = EITHER A PARAMETER FOR FUN OR THE INTEGRATED RESULT    00000046
OR BOTH                                                        00000047
X2P,X1P = UPPER AND LOWER LIMITS ON X                        00000048
Y2P,Y1P = UPPER AND LOWER LIMITS ON Y                       00000049
NX,MY = SEGMENTS IN X AND Y, RESPECTIVELY                   00000050
NP,MP = DEGREE OF PRECISION IN X AND Y, RESPECTIVELY        00000051
DIMENSION SAMPLE(5,5),COEF(5,5),SX(5),SY(5),C(5,5),SV(25),CV(25) 00000052
EQUIVALENCE (SV(1),SAMPLE(1,1)), (CV(1),COEF(1,1))          00000053
DATA SV/                                                       00000054
* 1.0, -0.577350269, -0.774596669, -0.861136312, -0.906179846, 00000055
* 1.0, 0.577350269, 0.0, -0.339981044, -0.538469310, 00000056
* 1.0, 0.0, .774596669, 0.339981044, 0.0, 00000057
* 1.0, 0.0, 0.0, 0.861136312, 0.538469310, 00000058
* 1.0, 0.0, 0.0, 0.0, 0.906179846/ 00000059
DATA CV/                                                       00000060
* 1.0, 1.0, 0.555555556, 0.347854845, 0.236926885, 00000061
* 1.0, 1.0, 0.888888889, 0.652145155, 0.478628670, 00000062
* 1.0, 0.0, 0.555555556, 0.652145155, 0.568888888, 00000063
* 1.0, 0.0, 0.0, 0.347854845, 0.478628670, 00000064
* 1.0, 0.0, 0.0, 0.0, 0.236926885/ 00000065
SUM = 0.0 00000066
X1 = X1P 00000067
X2 = X2P 00000068
Y1 = Y1P 00000069
Y2 = Y2P 00000070
NX = NNX 00000071
MY = MMY 00000072
NP = NNP 00000073
MP = MMP 00000074
DELX = (X2-X1)/FLOAT(NX) 00000075
DELY = (Y2-Y1)/FLOAT(MY) 00000076
HDELX = DELX*0.50 00000077
HDELY = DELX*0.50 00000078
X2 = X1 00000079
DO 20 I = 1, NP 00000080
SX(I) = SAMPLE(NP,I)*HDELX 00000081
20 CONTINUE 00000082

```

```

FUNCTION FUN (XX,YY) 00000112
THIS ROUTINE DEFINES THE SQUARE OF THE ANTENNA 00000113
PATTERN OVER THE MAIN BEAM. 00000114
FSP = XX 00000115
ESP = ATAN(ESP,SORT(1.0-ESP*ESP)) 00000116
PHIP = YY 00000117
AMXEP = AMAX1 (ESP,PHIP) 00000118
IF (AMXEP .LE. 0.0291 ) GO TO 10 00000119
IF (AMXEP .LE. 0.0349 ) GO TO 20 00000120
IF (AMXEP .LE. 0.0611 ) GO TO 30 00000121
IF (AMXEP .LE. 0.105 ) GO TO 40 00000122
IF (AMXEP .LE. 0.628) GO TO 50 00000123
FUN = 10.0F-39 00000124
10 FUN = EXP ( -4690.*ESP*ESP -3280.*PHIP*PHIP ) 00000125
FUN = FUN*FUN 00000126
RETURN 00000127
20 FUN = EXP(-121.1*ESP-3280.*PHIP*PHIP) 00000128
FUN = FUN*FUN 00000129
RETURN 00000130
30 FUN = 0.0398*EXP(-821.*ESP*ESP-1072.*PHIP*PHIP) 00000131
FUN = FUN*FUN 00000132
RETURN 00000133
40 FUN = 0.0159*EXP(-486.*ESP*ESP-53.6*PHIP) 00000134
FUN = FUN*FUN 00000135
RETURN 00000136
50 FUN = 0.000159*EXP(-8.59*SORT(ESP*ESP+PHIP*PHIP)) 00000137
FUN = FUN*FUN 00000138
RETURN 00000139
END 00000140

```

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Figure E-2. (Continued)

III. PROGRAM GAIN

A. Introduction

Program GAIN computes the antenna directivity, beam solid angle and, antenna efficiency. The theory and design of the program is described below.

B. Theory

The antenna beam solid angle is given by

$$\Omega = \int_0^{2\pi} \int_0^{\pi} p(\theta, \phi) \sin \theta \, d\theta \, d\phi \quad (6)$$

where

$p(\theta, \phi)$ = normalized antenna pattern

θ = polar angle

ϕ = azimuthal angle

$p(\theta, \phi)$ represents the normalized power in the antenna pattern. It can be shown that the antenna directivity Γ is related to Ω by the following expression

$$\Gamma = \frac{4\pi}{\Omega} \quad (7)$$

The antenna efficiency, on the otherhand, is the ratio of the power in the main beam to that in the entire pattern. Clearly then, the efficiency is given by

$$\eta_i = \int_0^{2\pi} \int_0^{\theta_i} p(\theta, \phi) \sin \theta \, d\theta \, d\phi \quad (8)$$

where θ_i is a polar angle which subdivides the main beam. In the above expression it is tacitly assumed that the main beam lies on the positive z axis as illustrated in Figure E-3. θ_i is chosen somewhat arbitrarily. Commonly θ_i is chosen at the -3 dB point or at the first null of the antenna pattern. For narrow beam antenna, the latter is most appropriate for radiometric work.

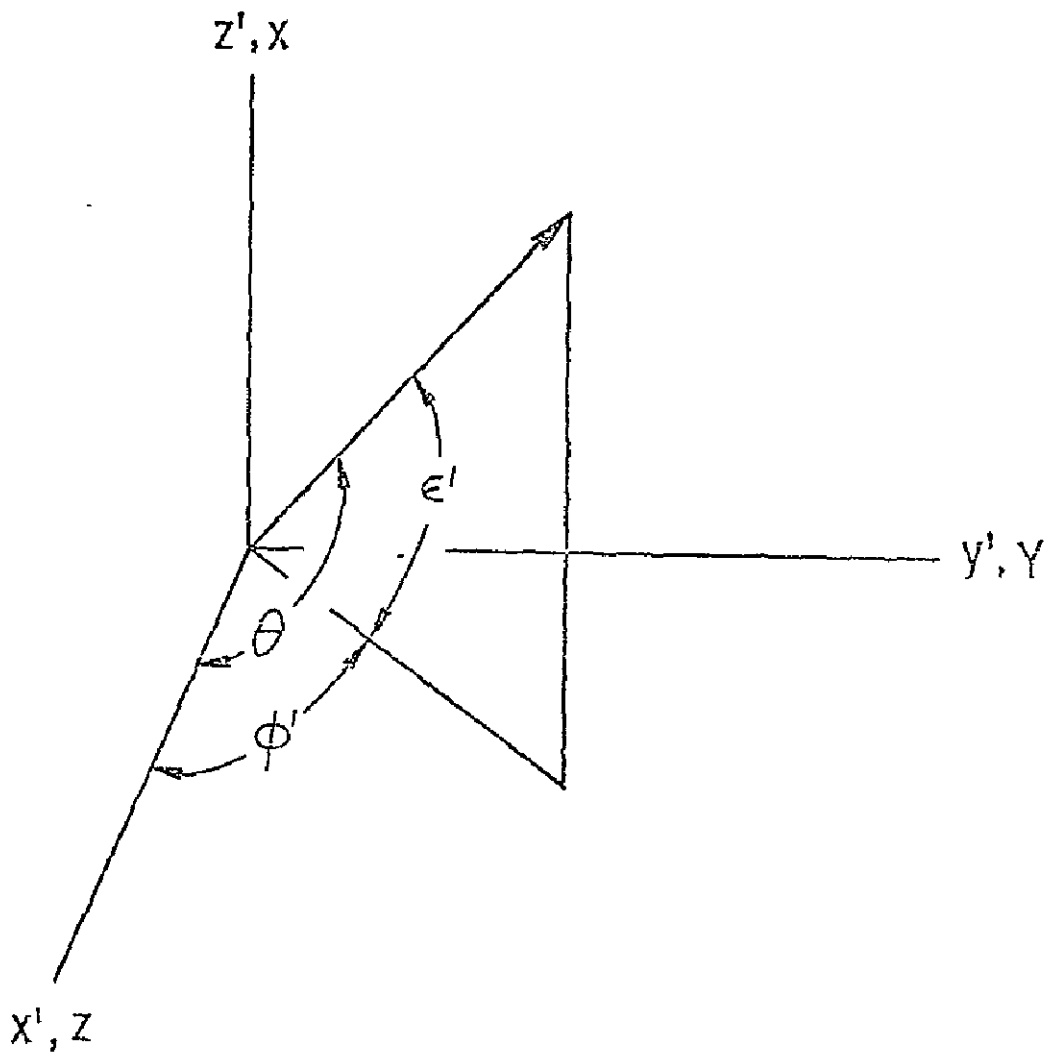


FIGURE E-3. ANTENNA PATTERN GEOMETRY FOR GAIN

C. Design and Operation of GAIN

In the discussion which follows it will be helpful to examine the FORTRAN listing for GAIN as shown in Figure E-4. Upon entry into GAIN, an array BEAM in which various polarized beam solid angle factors will be stored, is cleared. The main beam solid angles are then computed for various θ_i spaced at 1/2 degree intervals. The integration of the antenna pattern is performed by RINTEG which in turn calls for polarized pattern information from FUN1. The results are stored in BEAM. The accumulated solid beam angle is stored in TOTAL. The remainder of the polarized beam solid angle is then computed in the following statements.

At this point the antenna gain is computed and the gain and beam solid angle are printed.

In the remainder of the program the power content in the cross-polarized pattern (FUN2) is computed and added to TOTAL. A DO loop terminating on 30 then computes the antenna efficiency at one degree intervals out to 8 degrees. The result is listed.

Finally, the total beam solid angle, including polarized and cross-polarized contributions, is printed.

D. Subroutines FUN1 and FUN2

The antenna patterns described in FUN1 and FUN2 are actually represented in terms of another coordinate system. The relationship between the two coordinate systems is illustrated in Figure E-3. In the primed system the pattern is described in terms of the elevation angle ϵ and azimuth ϕ as shown in Figure E-1. The necessary transformations between the two are performed in the opening statements of FUN1 and FUN2. The latter statements simply evaluate the pattern over one of six domains in FUN1 and over five domains in FUN2.

```

PROGRAM GAIN (OUTPUT,TAPE6=OUTPUT)
C
C
C THIS PROGRAM COMPUTES THE ANTENNA GAIN AND EFFECIENCY FROM
C ANTENNA (POWER) PATTERNS DESCRIBED IN FUN1 AND FUN2.
C FUN1 DESCRIBES THE POLARIZED PATTERN WHEREAS FUN2 DESCRIBES THE
C CROSS-POLARIZED PATTERN.
C
C THIS PROGRAM WAS PREPARED BY
C
C JOHN P. CLAASSEN
C
C UNIVERSITY OF KANSAS CENTER FOR RESEARCH, INC.
C
000003 DIMENSION BEAM(10), EFF(10)
000003 EXTERNAL FUN1
000003 EXTERNAL FUN2
000003 DATA PI/3.14159265/
000003 DATA FACTOR/0.0174532925/
000003 WRITE (6,500)
000007 500 FORMAT (1H1//)
000007 TOTAL = 0.0
000010 DO 10 I = 1,10
000012 BEAM(I) = 0.0
000013 10 CONTINUE
000015 Y2 = PI/2.0
000016 Y1 = 0.0
000017 WRITE (6,100)
000023 100 FORMAT(30X,'ANTENNA GAIN AND EFFICIENCY FACTORS',//)
C
C COMPUTE THE MAIN BEAM SOLID ANGLE
C
000023 DO 20 I = 1,8
000025 X1 = COS(FLOAT(I)*FACTOR*0.50)
000031 X2 = COS(FLOAT(I-1)*FACTOR*0.50)
000040 CALL RINTEG (FUN1, Z, X2, X1, Y2, Y1, 2, 90, 3, 3)
000051 BEAM (I+1) = BEAM (I) + 4.0*Z
000055 TOTAL = TOTAL + 4.0*Z
000057 20 CONTINUE
C
C COMPUTE THE REMAINDER BEAM SOLID ANGLE
C
000061 X2 = COS(4.0*FACTOR)
C
000064 X1 = COS(120.0*FACTOR)
000071 CALL RINTEG (FUN1, Z, X2, X1, Y2, Y1, 115, 90, 3, 3)
000102 TOTAL = TOTAL + 4.0*Z
C
C COMPUTE GAIN
C
000105 GAIN1 = 4.0*PI/TOTAL
000107 GAIN2 = 10.0*ALOG10(GAIN1)
000113 WRITE (6,200) TOTAL, GAIN1, GAIN2
000124 200 FORMAT (5X,'POLARIZED BEAM SOLID ANGLE=*E14.6/
* 5X,'POLARIZED GAIN=*E14.6,* OR*F6.1,* DB*//)
C
C COMPUTE THE CONTRIBUTION FROM THE CROSS PATTERN
C
000124 Y2 = 1.0
000125 X1 = COS (FACTOR*5.0)
000132 CALL RINTEG(FUN2,Z,X2,X1,Y2,Y1,5,40,4,4)
000143 TOTAL = TOTAL + 4.0*Z
C
C COMPUTE BEAM EFFICIENCY
C
000146 DO 30 I = 1,8
000150 EFF(I) = BEAM(I+1)/TOTAL
000152 WRITE (6,300) I, EFF(I)
000162 300 FORMAT(5X,'ACTIVE BEAMWIDTH IS *13,* DEGREES.*,
* * CORRESPONDING EFFICIENCY IS*F6.3* .*)
000162 30 CONTINUE
C
C WRITE THE BEAM SOLID ANGLE
C
000164 WRITE (6,400) TOTAL
000172 400 FORMAT (75X,'TOTAL BEAM SOLID ANGLE=*E14.6)
000172 STOP
000174 ENH

```

FIGURE E-4. SOURCE LISTING FOR GAIN

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```

SUBROUTINE RINTEG (FUN, Z2,X2P,X1P,Y2P,Y1P,NNX,MHY,NNP,MMP)
C THIS ROUTINE EMPLOYS A GAUSSIAN LEGENDRE QUADRATURE
C INTEGRATION PROCEDURE. INTEGRATION OVER X-Y SEGMENTS
C ARE PERFORMED AFTER TRANSLATION TO (-1,1)X(-1,1).
C FUN= INTEGRAND FUNCTION
C Z2 = EITHER A PARAMETER FOR FUN OR THE INTEGRATED RESULT
C OR BOTH
C X2P,X1P = UPPER AND LOWER LIMITS ON X
C Y2P,Y1P = UPPER AND LOWER LIMITS ON Y
C NX,MHY = SEGMENTS IN X AND Y, RESPECTIVELY
C NNP,MMP = DEGREE OF PRECISION IN X AND Y, RESPECTIVELY
000015 DIMENSION SAMPLE(S,5),COEF(S,5),SX(S),SY(S),C(S,5),SV(25),CV(25)
000015 FOURVALENCE (SV(1),SAMPLE(1,1)), (CV(1),COEF(1,1))
DATA SV/
* 1.0, -0.577350269, -0.774596669, -0.861136312, -0.906179846,
* 1.0, 0.577350269, 0.0, -0.339981044, -0.538469310,
* 1.0, 0.0, .774596669, 0.339981044, 0.0,
* 1.0, 0.0, 0.0, 0.861136312, 0.538469310,
* 1.0, 0.0, 0.0, 0.0, 0.906179846/
000015 DATA CV/
* 1.0, 1.0, 0.555555556, 0.347854845, 0.236926885,
* 1.0, 1.0, 0.888888889, 0.652145155, 0.478628670,
* 1.0, 0.0, 0.555555556, 0.652145155, 0.568888888,
* 1.0, 0.0, 0.0, 0.347854845, 0.478628670,
* 1.0, 0.0, 0.0, 0.0, 0.236926885/
C CLEAR SUMMING VARIABLE
000015 SUM = 0.0
C RE-ASSIGN INPUT ARGUMENTS
000016 X1 = X1P
000017 X2 = X2P
000020 Y1 = Y1P
000021 Y2 = Y2P
000022 NX = NNX
000023 MY = MHY
000025 NP = NNP
000026 MP = MMP
C COMPUTE LENGTH OF CELL SIDES
C
C
000030 DELX = (X2-X1)/FLOAT(NX)
000033 DELY = (Y2-Y1)/FLOAT(MY)
000037 HDELX = DELX*0.50
000041 HDELY = DELX*0.50
C FORM SAMPLE FACTOR FOR X
000042 DO 20 I = 1, NP
000043 SX(I) = SAMPLE(NP,I)*HDELX
000052 20 CONTINUE
C FORM SAMPLE FACTOR FOR Y
000054 DO 30 I = 1, MP
000055 SY(I) = SAMPLE(MP,I)*HDELY
000064 30 CONTINUE
C FORM GAUSSIAN WEIGHTS
000066 DO 50 I = 1, NP
000067 DO 40 J = 1, MP
000070 C(I,J) = COEF(NP,I)*COEF(MP,J)
000104 40 CONTINUE
000106 50 CONTINUE
C INTEGRATE IN STRIPS OF DELX
000110 X2 = X1
000112 DO 90 N=1,NX
000113 X1=X2
000115 X2=X1+DELX
000117 XM = X1 + HDELX
C INTEGRATE ALONG Y
000120 Y2 = Y1P
000121 DO 80 M=1,MY
000123 Y1 = Y2
000125 Y2 = Y1 + DELY
000127 YM = Y1 + HDELY
C TRANSFORM TO CELL (-1,1)X(-1,1)

```

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Figure E-4. (Continued)

```

C
000130 DO 70 I=1,NP
000132 X=SX(I)*XM
000135 DO 60 J=1,MP

C
C FORM PARTIAL SUM
C
000136 Y=SY(J)*YM
000141 SUM = SUM+C(I,J)*FUN(X,Y)
000157 60 CONTINUE
000161 70 CONTINUE
000163 80 CONTINUE
000166 90 CONTINUE

C
C APPLY JACOBIAN
C
000170 ZZ = SUM*DELT*X*DELT*0.250
000173 RETURN
000174 END

FUNCTION FUN1 (X,Y)
C
C POLARIZED PATTERN
C THIS FUNCTION SUBROUTINE EVALUATES THE PATTERN INTENSITY
C IN THE PRIMED COORDINATE SYSTEM. THE PATTERN IS
C EXPRESSED IN TERMS OF ELEVATION AND AZIMUTH IN THAT
C COORDINATE SYSTEM. THE INPUT ARGUMENTS, HOWEVER, ARE
C DESCRIBED IN AN UNPRIMED COORDINATE SYSTEM RELATED
C TO THE PRIMED SYSTEM BY A ROTATION ABOUT THE
C Y AXIS. THE BORE SIGHT IS ON THE X-PRIME AXIS IN
C THE PRIMED SYSTEM AND ON THE Z AXIS IN THE UNPRIMED
C SYSTEM.
C
C TRANSFORM TO PATTERN COORDINATES
C
000005 SINX = SQRT(1.0 - X*X)
000013 COSY = COS(Y)
000016 SINY=SQRT(1.0-COSY*COSY)
000022 COSTP =-SINX*COSY
000024 SINTP = SQRT(1.0-COSTP*COSTP)
000031 THETAP=ATAN2(SINTP,COSTP)
000034 PHIP= ATAN2(SINX*SINY,X)
000045 APHIP = ABS(PHIP)
000046 AESPP = ABS(1.57079633-THETAP)
000051 ESQ = AESPP*AESPP
000052 PSQ = PHIP*PHIP

C
C EVALUATE THE PATTERN FUNCTIONS
C
000054 AMXEP = AMAX1(AESPP,PHIP)
000057 IF (AMXEP .LE. 0.0291 ) GO TO 100
000062 IF (AMXEP .LE. 0.0349 ) GO TO 200
000064 IF (AMXEP .LE. 0.0611 ) GO TO 300
000067 IF (AMXEP .LE. 0.105 ) GO TO 400
000071 IF (AMXEP .LE. 0.628 ) GO TO 500
000074 XI = -SINTP*COS(PHIP)
000077 XI = ATAN2(SQRT(1.0-XI*XI),XI)
000106 XID = XI*57.2957796
000110 IF (XID .LT. 100. .AND. XID .GT. 60. ) GO TO 600
000123 FUN1 = 0.0
000124 RETURN
000124 100 FUN1 = EXP ( -4690.*ESQ -3280.*PSQ )
000133 RETURN
000133 200 FUN1 =EXP(- 121.1*AESPP-3280.*PSQ)
000142 RETURN
000142 300 FUN1 = 0.0398*EXP(-820.7*ESQ-1072.*PSQ)
000152 HFTURN
000152 400 FUN1 = 0.0159*EXP(-486.*ESQ-53.6*APHIP)
000162 RFTURN
000162 500 FUN1 = 0.000159*EXP(-8.59*SQRT(FSQ+PSQ))
000173 RFTURN
000173 600 TANPSI = SINTP/COSTP*SIN(PHIP)
000177 PSI = ATAN(TANPSI)
000201 COSPS = COS(PSI)**2
000204 SINPS = SIN(PSI)**2
000207 FUN1 = (3.16E-05*COSPS + 6.31E-06*SINPS)*
* EXP(-(XID-80.)*2/(100.*COSPS + 36.*SINPS))
000224 RFTURN
000225 END

```

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Figure E-4. (Continued)

```

FUNCTION FUN2 (X,Y)                                00000382
C                                                    00000383
C                                                    00000384
C          CROSS-POLARIZED PATTERN                 00000385
C          THIS FUNCTION SUBROUTINE EVALUATES THE PATTERN INTENSITY 00000386
C          IN THE PRIMED COORDINATE SYSTEM. THE PATTERN IS          00000387
C          EXPRESSED IN TERMS OF ELEVATION AND AZIMTH IN THAT        00000388
C          COORDINATE SYSTEM. THE INPUT ARGUMENTS, HOWEVER, ARE     00000389
C          DESCRIBED IN AN UNPRIMED COORDINATE SYSTEM RELATED      00000390
C          TO THE PRIMED SYSTEM BY A ROTATION ABOUT THE              00000391
C          Y AXIS. THE BORE SIGHT IS ON THE X-PRIME AXIS IN         00000392
C          THE PRIMED SYSTEM AND ON THE Z AXIS IN THE UNPRIMED      00000393
C          SYSTEM.                                                  00000394
C                                                    00000395
C          TRANSFORM TO PATTERN COORDINATES                    00000396
C                                                    00000397
000005      SINX = SQRT(1.0 - X*X)                          00000398
000013      COSY = COS(Y)                                    00000399
000016      SINY=SQRT(1.0-COSY*COSY)                        00000400
000022      COSTP =-SINX*COSY                               00000401
000024      SINTP = SQRT(1.0-COSTP*COSTP)                  00000402
000031      THETAP=ATAN2(SINTP,COSTP)                       00000403
000034      PHIP= ATAN2(SINX*SINY,X)                       00000404
000045      APHIP = ABS(PHIP)                               00000405
000046      AESPP = ABS(1.57079633-THETAP)                 00000406
000051      ESQ = AESPP*AESPP                               00000407
000052      PSQ = PHIP*PHIP                                 00000408
C                                                    00000409
C          EVALUATE THE PATTERN FUNCTIONS                    00000410
C                                                    00000411
000054      AMXEP = AMAX1(AESPP,PHIP)                       00000412
000057      IF (AMXEP .LE. 0.0291 ) GO TO 100              00000413
000062      IF (AMXEP .LE. 0.0349 ) GO TO 200              00000414
000064      IF (AMXEP .LE. 0.0611 ) GO TO 300              00000415
000067      IF (AMXEP .LE. 0.105 ) GO TO 400               00000416
000071      FUN2 = 0.0                                       00000417
000072      RETURN                                           00000418
000073      100 FUN2 = 0.0063*EXP (-4690.*ESQ-3280.*PSQ)    00000419
000103      RETURN                                           00000420
000103      200 FUN2 = 0.0063*EXP ( -4690.*ESQ -3280.*PSQ ) 00000421
000113      RETURN                                           00000422
000113      300 FUN2 = 0.00025*EXP (-821.*PSQ-821.*ESQ)    00000423

000123      RETURN                                           00000424
000123      400 FUN2 = 0.00025*EXP (-821.*PSQ-821.*ESQ)    00000425
000133      RETURN                                           00000426
000133      END                                              00000427

```

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Figure E-4. (Continued)

CRINC LABORATORIES

Chemical Engineering Low Temperature Laboratory

Remote Sensing Laboratory

Flight Research Laboratory

Chemical Engineering Heat Transfer Laboratory

Nuclear Engineering Laboratory

Environmental Health Engineering Laboratory

Information Processing Laboratory

Water Resources Institute

Technology Transfer Laboratory

CRINC

