

(NASA-CR-144320) EXPANSION AND IMPROVEMENT  
OF THE FORMA SYSTEM FOR RESPONSE AND LOAD  
ANALYSIS. VOLUME 2C: LISTINGS, FINITE  
ELEMENT FORMA SUBROUTINES (MARTIN MARIETTA  
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EXPANSION AND IMPROVEMENT OF THE FORMA  
SYSTEM FOR RESPONSE AND LOAD ANALYSIS

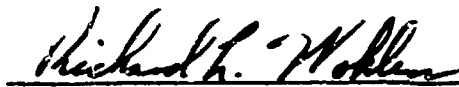
Volume IIC - Listings, Finite Element FORMA Subroutines

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FOREWORD

This report presents results of the expansion and improvement of the FORMA system for response and load analysis. The acronym FORMA stands for FORTRAN Matrix Analysis. The study, performed from 16 May 1975 through 17 May 1976 was conducted by the Analytical Mechanics Department, Martin Marietta Corporation, Denver Division, under the contract NAS8-31370. The program was administered by the National Aeronautics and Space Administration, George C. Marshall Space Flight Center, Huntsville, Alabama under the direction of Dr. John R. Admire, Structural Dynamics Division, Systems Dynamics Laboratory.

This report is published in seven volumes:

Volume I - Programming Manual,  
Volume IIA - Listings, Dense FORMA Subroutines,  
Volume IIB - Listings, Sparse FORMA Subroutines,  
Volume IIC - Listings, Finite Element FORMA Subroutines,  
Volume IIIA - Explanations, Dense FORMA Subroutines,  
Volume IIIB - Explanations, Sparse FORMA Subroutines, and  
Volume IIIC - Explanations, Finite Element FORMA Subroutines.

CONTENTS

	<u>Page</u>
Foreword . . . . .	ii
Contents . . . . .	iii
Abstract . . . . .	iv
Acknowledgements . . . . .	v
I. Introduction . . . . .	I-1
II. Subroutine Listings (Subroutine Names in Alphabetical Order, Numbers Coming Before Letters) . . . . .	II-1

ABSTRACT

This report presents techniques for the solution of structural dynamic systems on an electronic digital computer using FORMA (FORTRAN Matrix Analysis).

FORMA is a library of subroutines coded in FORTRAN IV for the efficient solution of structural dynamics problems. These subroutines are in the form of building blocks that can be put together to solve a large variety of structural dynamics problems. The obvious advantage of the building block approach is that programming and checkout time are limited to that required for putting the blocks together in the proper order.

The FORMA method has advantageous features such as:

1. subroutines in the library have been used extensively for many years and as a result are well checked out and debugged;
2. method will work on any computer with a FORTRAN IV compiler;
3. incorporation of new subroutines is no problem;
4. basic FORTRAN statements may be used to give extreme flexibility in writing a program.

Two programming techniques are used in FORMA: dense and sparse.

ACKNOWLEDGMENTS

The editor expresses his appreciation to those individuals whose assistance was necessary for the successful completion of this report. Dr. John R. Admire was instrumental in the definition of the program scope and contributed many valuable suggestions. Messrs. Carl Bodley, Wilcomb Benfield, Darrell Devers, Richard Hruda, Roger Philippus, and Herbert Wilkening, all of the Analytical Mechanics Department, Denver Division of Martin Marietta Corporation, have contributed ideas, as well as subroutines, in the formulation of the FORMA library.

The editor also expresses his appreciation to those persons who developed FORTRAN, particularly the subroutine concept of that programming tool.

## I. INTRODUCTION

A listing of the source deck of each finite element FORMA subroutine is given in this volume to remove the "black box" aura of the subroutines so that the analyst may better understand the detailed operations of each subroutine.

The FORTRAN IV programming language is used in all finite element FORMA subroutines.

II. SUBROUTINE LISTINGS

The subroutines are given in alphabetical order with numbers coming before letters.



```

SUBROUTINE AXIAL (XYZ,JDOF,EUL,NUTEL,NJ,
*             NUTMX,NUTKX,NUTLT,NUTST,
*             W,T,S,KX,KJ,KE,KW)
DIMENSION XYZ(KX,1),JDOF(KJ,1),EUL(KE,1),W(KW,1),T(KW,1),S(KW,1)
DIMENSION CJ(3,2), E1(3,2), IVE1(6)
DATA NAME1/6HAXIAL /, NRW,NRLT/6,2/, IBLNK/6H      /, KCJ/3/
DATA NIT,NOT/5,6/

```

```

C
C SUBROUTINE TO CALCULATE (ON OPTION) FINITE ELEMENT ...
C MASS MATRICES AND IVECS (ON NUTMX),
C STIFFNESS MATRICES (SAME AS GLOBAL LOAD TRANSFORMATION MATRICES)
C AND IVECS (ON NUTKX),
C LOCAL LOAD TRANSFORMATION MATRICES AND IVECS (ON NUTLT),
C STRESS TRANSFORMATION MATRICES AND IVECS (ON NUTST)
C FOR AXIAL ROD ELEMENTS.
C MASS, STIFFNESS MATRICES ARE IN GLOBAL COORDINATE DIRECTIONS.
C GLOBAL COORDINATE ORDER FOR EACH ELEMENT IS
C (U,V,W) JOINT 1, THEN JOINT 2.
C WHERE U,V,W ARE TRANSLATIONS.
C IVEC GIVES ELEMENT DOF INTO GLOBAL DOF. EXAMPLES...
C IVEC(6)=834 PLACES ELEMENT DOF 6 INTO GLOBAL DOF 834.
C IVEC(3)=0 OMTS ELEMENT DOF 3 FROM GLOBAL DOF. THIS CONSTRAINS
C ELEMENT DOF 3 TO ZERO MOTION.
C GLOBAL LOAD TRANSFORMATION MATRIX RELATES LOADS AT ROD ENDS IN GLOBAL
C COORDINATE DIRECTIONS TO DEFLECTIONS IN THE GLOBAL COORDINATE
C DIRECTIONS.
C ROW ORDER IN GLOBAL LOAD TRANSFORMATION MATRIX IS
C (PU,PV,PW) JOINT 1, THEN JOINT 2.
C WHERE P IS FORCE.
C LOCAL LOAD TRANSFORMATION MATRIX RELATES LOADS AT ROD ENDS IN LOCAL
C COORDINATE SYSTEM TO DEFLECTIONS IN THE GLOBAL COORDINATE
C DIRECTIONS.
C ROW ORDER IN LOCAL LOAD TRANSFORMATION MATRIX IS
C PX1,PX2
C WHERE PX IS AXIAL FORCE.
C PX1(-), PX2(+) IS TENSION. PX1(+), PX2(-) IS COMPRESSION.
C STRESS TRANSFORMATION MATRIX RELATES STRESS AT ROD ENDS IN LOCAL
C COORDINATE SYSTEM TO DEFLECTIONS IN THE GLOBAL COORDINATE DIRECTIONS.
C ROW ORDER IN STRESS TRANSFORMATION MATRIX IS
C SIGMA-X1, SIGMA-X2
C WHERE SIGMA IS NORMAL STRESS.
C SX1(-), SX2(+) IS TENSION. SX1(+), SX2(-) IS COMPRESSION.
C DATA APRANGEMENT ON NUTMX, NUTKX, NUTLT, NUTST FOR EACH FINITE
C ELEMENT IS (W=M,K,LT,ST)
C WRITE (NUTWX) NAMEW,NEL,NR,NC,NAMEL,(IBLNK,I=1,5),
C ((W(I,J),I=1,NR),J=1,NC),(IVEC(I),I=1,NC)
C CALLS FORMA SUBROUTINES MASIA, PAGEHD, STF1A, ZZBOMB.
C DEVELOPED BY WA BENFIELD, CS BODLEY, RL WOHLN. JANUARY 1973.
C LAST REVISION BY WA BENFIELD. MARCH 1976.
C
C *****
C INPUT DATA READ IN THIS SUBROUTINE FROM NUTEL. IF NUTEL = 5, DATA IS
C READ FROM CAPDS.
C NAMEM,NAMEK,NAMELT,NAMEST          FORMAT (4(A6,4X)
C RO,E                                FORMAT (2(5X,E10))

```

```

C 20 NEL,J1,J2,A1,A2                                FORMAT (3I5,2E10)
C   IF (J1 .EQ. 0) RETURN
C   GO TO 20
C
C DEFINITION OF INPUT VARIABLES.
C NAMEM = TYPE OF MASS MATRIX WANTED.
C       = M1, DIAGONAL LUMPED.
C       = M2, CONSISTENT.
C       = 6H      OR 6HNUMASS, NO MASS MATRIX CALCULATED.
C NAMEK = TYPE OF STIFFNESS MATRIX WANTED.
C       = K1, CONSTANT AXIAL FORCE ASSUMED.
C       = 6H      OR 6HNUSTIF, NO STIFFNESS MATRIX CALCULATED.
C NAMELT = IDENTIFICATION NAME FOR LOAD TRANSFORMATION MATRICES.
C        = 6H      OR 6HNOLOAD, NO LOAD TRANSFORMATIONS CALCULATED.
C NAMEST = IDENTIFICATION NAME FOR STRESS TRANSFORMATION MATRICES.
C        = 6H      OR 6HNOSTRS, NO STRESS TRANSFORMATIONS CALCULATED.
C RO     = MASS DENSITY.
C E      = YOUNGS MODULUS OF ELASTICITY.
C NEL    = FINITE ELEMENT NUMBER. FOR REFERENCE ONLY, NOT USED IN
C          CALCULATIONS. WRITTEN ON NUTMX, ETC.
C J1     = JOINT NUMBER AT ROD END 1.
C J2     = JOINT NUMBER AT ROD END 2.
C A1     = CROSS-SECTION AREA AT ROD END 1.
C A2     = CROSS-SECTION AREA AT ROD END 2.
C
C EXPLANATION OF INPUT FORMATS. NUMBER INDICATES CARD COLUMNS USED.
C   I = INTEGER DATA, RIGHT ADJUSTED.
C   F = DECIMAL POINT DATA, ANYWHERE IN FIELD. EXPONENT RIGHT ADJUSTED.
C   X = CARD COLUMNS SKIPPED.
C *****
C
C SUBROUTINE ARGUMENTS (ALL INPUT)
C XYZ   = MATRIX OF JOINT GLOBAL X,Y,Z LOCATIONS. ROWS CORRESPOND
C        TO JOINT NUMBERS. COLUMNS 1,2,3 CORRESPOND TO THE JOINT
C        X,Y,Z LOCATIONS RESPECTIVELY. SIZE(NJ,3).
C JDOF  = MATRIX OF JOINT GLOBAL DEGREES OF FREEDOM. ROWS CORRESPOND
C        TO JOINT NUMBERS. COLUMNS 1,2,3 CORRESPOND TO THE JOINT
C        TRANSLATION DOFS AND COLUMNS 4,5,6 CORRESPOND TO THE JOINT
C        ROTATION DOFS. SIZE(NJ,6).
C EUL   = MATRIX OF JOINT EULER ANGLES (DEGREES). ROWS CORRESPOND
C        TO JOINT NUMBERS. COLUMNS 1,2,3 CORRESPOND TO THE
C        GLOBAL X,Y,Z PERMUTATION. SIZE(NJ,3).
C NUTEL = LOGICAL NUMBER OF TAPE CONTAINING ELEMENT INPUT DATA FOR
C        THIS SUBROUTINE. IF NUTEL = 5, DATA IS READ FROM CARDS.
C NJ    = NUMBER OF JOINTS OR ROWS IN MATRICES (XYZ), (JDOF), (EUL).
C NUTMX = LOGICAL NUMBER OF UTILITY TAPE ON WHICH ELEMENT
C        MASS MATRICES AND IVECS ARE OUTPUT.
C        NUTMX MAY BE ZERO IF MASS MATRIX IS NOT FORMED.
C        USES FORTRAN READ, WRITE.
C NUTKX = LOGICAL NUMBER OF UTILITY TAPE ON WHICH ELEMENT
C        STIFFNESS MATRICES (SAME AS GLOBAL LOADS TRANSFORMATION
C        MATRICES) AND IVECS ARE OUTPUT.
C        NUTKX MAY BE ZERO IF STIFFNESS MATRIX IS NOT FORMED.
C        USES FORTRAN READ, WRITE.
C NUTLT = LOGICAL NUMBER OF UTILITY TAPE ON WHICH ELEMENT LOCAL

```

```

C          LOAD TRANSFORMATION MATRICES AND IVECS ARE OUTPUT.
C          NUTLT MAY BE ZERO IF LOAD TRANSFORMATIONS ARE NOT FORMED.
C          USES FORTRAN READ, WRITE.
C  NUTST  = LOGICAL NUMBER OF UTILITY TAPE ON WHICH ELEMENT
C          STRESS TRANSFORMATION MATRICES AND IVECS ARE OUTPUT.
C          NUTST MAY BE ZERO IF STRESS TRANSFORMATIONS ARE NOT FORMED.
C          USES FORTRAN READ, WRITE.
C  W      = MATRIX WORK SPACE. MIN SIZE(6,6).
C  T      = MATRIX WORK SPACE. MIN SIZE(6,6).
C  S      = MATRIX WORK SPACE. MIN SIZE(6,6).
C  KX     = ROW DIMENSION OF XYZ IN CALLING PROGRAM.
C  KJ     = ROW DIMENSION OF JDOF IN CALLING PROGRAM.
C  KE     = ROW DIMENSION OF EUL IN CALLING PROGRAM.
C  KW     = ROW DIMENSION OF W, T, AND S IN CALLING PROGRAM. MIN=6.

```

```

C
C  NERROR EXPLANATION
C  1 = JOINT NUMBER GREATER THAN NUMBER OF JOINTS.
C  2 = MASS MATRIX FORMED, NUTMX .LE. ZERO.
C  3 = STIFFNESS MATRIX FORMED, NUTKX .LE. ZERO.
C  4 = LT MATRIX FORMED, NUTLT .LE. ZERO.
C  5 = ST MATRIX FORMED, NUTST .LE. ZERO.

```

```

C
1001 FORMAT (4(A6,4X))
1002 FORMAT (2(5X,E10.0))
1003 FORMAT (3I5,4E10.0)
2001 FORMAT (/ /46X 29HINPUT DATA FOR AXIAL ELEMENTS)
2002 FORMAT (/ /40X 41HINPUT DATA FOR AXIAL ELEMENTS (CONTINUED))
2003 FORMAT (/ 16X7HMASS = A6, 9X7HSTIF = A6, 9X13HLOAD TRANS = A6,
*           6X15HSTRESS TRANS = A6,
*           / 18X4HRO = E10.3, 9X3HE = E10.3,
*           / /16X7HELEMENT 13X7HJOINT 1 13X7HJOINT 2 15X4HAREA
*           16X4HAREA / 16X6HNUMBER 55X7HJOINT 1 13X7HJOINT 2 /)
2004 FORMAT (1X 3I20, 14X E10.3, 10X E10.3)

```

```

C
C  READ AND WRITE FINITE ELEMENT DATA.
      NLINE = 0
      CALL PAGEHD
      WRITE (NOT,2001)
      READ (NUTEL,1001) NAMEM,NAMEK,NAMELT,NAMEST
      READ (NUTEL,1002) RO,E
      WRITE (NOT,2003) NAMEM,NAMEK,NAMELT,NAMEST,RO,E
20  READ (NUTEL,1003) NEL,J1,J2,A1,A2
      IF (J1 .LE. 0) RETURN
      NLINE = NLINE + 1
      IF (NLINE .LE. 42) GO TO 30
      CALL PAGEHD
      WRITE (NOT,2002)
      WRITE (NOT,2003) NAMEM,NAMEK,NAMELT,NAMEST,RO,E
      NLINE = 0
30  WRITE (NOT,2004) NEL,J1,J2,A1,A2

```

NERROR=1

```

C          IF (J1 .GT. NJ .OR. J2 .GT. NJ ) GO TO 999
C
C  FORM FINITE ELEMENT COORDINATE LOCATIONS, EULER ANGLES. REVADD IVEC.
      DO 42 I=1,3

```

```

CJ(I,1) = XYZ(J1,I)
CJ(I,2) = XYZ(J2,I)
EJ(I,1) = FUL(J1,I)
EJ(I,2) = FUL(J2,I)
IV1(I)   = JDOF(J1,I)
IV1(I+3) = JDOF(J2,I)
C
C FORM MASS MATRIX (W).
  IF (NAMEM .EQ. 6H .OR. NAMEM .EQ. 6HNOMASS) GO TO 110
  CALL MASIA (CJ,EJ,A1,A2,RO,NAMEM,W,KCJ,KCJ,KW)
  IF (NUTMX .LE. 0) GO TO 999
  WRITE (NUTMX) NAMEM,NEL,NRW,NRW,NAMEL,(IBLNK,I=1,5),
*          ((W(I,J),I=1,NRW),J=1,NRW),(IV1(I),I=1,NRW)
  NERROR=2
C
C FORM STIFFNESS MATRIX (W), LOCAL LOAD TRANSFORMATION MATRIX (T),
C STRESS TRANSFORMATION MATRIX (S).
110 IF (NAMEK .EQ. 6H .OR. NAMEK .EQ. 6HNOSTIF) GO TO 20
  CALL STFIA (CJ,EJ,A1,A2,E,NAMEK,NAMEST,W,T,S,NRST,
*          KCJ,KCJ,KW,KW,KW)
  IF (NUTKX .LE. 0) GO TO 999
  WRITE (NUTKX) NAMEK,NEL,NRW,NRW,NAMEL,(IBLNK,I=1,5),
*          ((W(I,J),I=1,NRW),J=1,NRW),(IV1(I),I=1,NRW)
  IF (NAMELT .EQ. 6H .OR. NAMELT .EQ. 6HNOLOAD) GO TO 115
  NERROR=4
  IF (NUTLT .LE. 0) GO TO 999
  WRITE (NUTLT) NAMELT,NEL,NRLT,NRW,NAMEL,(IBLNK,I=1,5),
*          ((T(I,J),I=1,NRLT),J=1,NRW),(IV1(I),I=1,NRW)
115 IF (NAMEST .EQ. 6H .OR. NAMEST .EQ. 6HNOSTRS) GO TO 20
  NERROR=5
  IF (NUTST .LE. 0) GO TO 999
  WRITE (NUTST) NAMEST,NEL,NRST,NRW,NAMEL,(IBLNK,I=1,5),
*          ((S(I,J),I=1,NRST),J=1,NRW),(IV1(I),I=1,NRW)
  GO TO 20
C
999 CALL ZZBOME (6HAXIAL,NERROR)
  END

```

B1A1

```
      SUBROUTINE B1A1 (RL,Z,KZ)
      DIMENSION Z(KZ,2)
C
C  SUBROUTINE TO CALCULATE FINITE ELEMENT...
C  BUCKLING MATRIX
C  FOR AN AXIAL ROD ELEMENT WITH UNRESTRAINED BOUNDARIES.
C  BUCKLING MATRIX IS BASED ON UNIT AXIAL LOAD.
C  BUCKLING MATRIX IS IN LOCAL COORDINATE SYSTEM.
C  THE LOCAL COORDINATE SYSTEM ASSUMES THE ROD TO LIE IN THE X-Z PLANE
C  WITH JOINT 1 AT THE ORIGIN, JOINT 2 ALONG THE POSITIVE X AXIS.
C  LOCAL COORDINATE ORDER IS
C    DZ1,DZ2
C  WHERE DZ IS TRANSLATION.
C  DEVELOPED BY RL WOHLER. AUGUST 1973.
C  LAST REVISION BY RL WOHLER. SEPTEMBER 1973.
C
C  SUBROUTINE ARGUMENTS
C  RL = INPUT ROD LENGTH.
C  Z = OUTPUT BUCKLING MATRIX. SIZE(2,2).
C  KZ = INPUT ROW DIMENSION OF Z IN CALLING PROGRAM. MIN=2.
C
      C = 1./RL
      Z(1,1) = C
      Z(1,2) = -C
      Z(2,1) = -C
      Z(2,2) = C
C
      RETURN
      END
```

B1A2

```
      SUBROUTINE B1A2  (RL,Z,KZ)
      DIMENSION Z(KZ,1)
C
C  SUBROUTINE TO CALCULATE FINITE ELEMENT...
C  BUCKLING MATRIX
C  FOR A BEAM ELEMENT WITH UNRESTRAINED BOUNDARIES.
C  BUCKLING MATRIX IS BASED ON UNIT AXIAL LOAD.
C  BUCKLING MATRIX IS IN LOCAL COORDINATE SYSTEM.
C  THE LOCAL COORDINATE SYSTEM ASSUMES THE BEAM TO LIE IN THE X-Z PLANE.
C  WITH JOINT 1 AT THE ORIGIN, JOINT 2 ALONG THE POSITIVE X AXIS.
C  LOCAL COORDINATE ORDER IS
C  DZ1,DZ2,TY1,TY2
C  WHERE DZ IS TRANSLATION AND TY IS ROTATION.
C  DEVELOPED BY RL WOHLER.  AUGUST 1973.
C  LAST REVISION BY RL WOHLER.  SEPTEMBER 1973.
C
C  SUBROUTINE ARGUMENTS
C  RL = INPUT  ROD LENGTH.
C  Z  = OUTPUT BUCKLING MATRIX.  SIZE(4,4).
C  KZ = INPUT  ROW DIMENSION OF Z IN CALLING PROGRAM.  MIN=4.
C
      C1 = 6./(5.*RL)
      C2 = .1
      C3 = (2.*RL)/15.
      Z(1,1) = C1
      Z(1,2) = -C1
      Z(1,3) = -C2
      Z(1,4) = -C2
      Z(2,2) = C1
      Z(2,3) = C2
      Z(2,4) = C2
      Z(3,3) = C3
      Z(3,4) = -RL/30.
      Z(4,4) = C3
      DO 10 I=1,4
      DO 10 J=1,4
10  Z(J,I) = Z(I,J)
C
      RETURN
      END
```

```

SUBROUTINE BAR      (XYZ,JDOF,EUL,NUTEL,NJ,
*                  NUTMX,NUTKX,NUTRX,NUTLT,NUTST,
*                  W,T,S,KX,KJ,KE,KW)
DIMENSION XYZ(KX,1),JDOF(KJ,1),EUL(KE,1),W(KW,1),T(KW,1),S(KW,1)
DIMENSION CJ(3,3),EJ(3,2),IV1(12),TR(12,12),TD(24,24)
DIMENSION KODEK(4),KODEB(2),IFPIN(4),IV2(4)
DATA NAMEL / 6HEAP /
DATA NRW,NRLT/12,12/,IBLNK/6H      /,KCJ/3/,KTR/12/,KTD/24/
DATA NIT,NOT/5,6/

C
C SUBROUTINE TO CALCULATE (ON OPTION) FINITE ELEMENT ...
C MASS MATRICES AND IVECS (ON NUTMX),
C STIFFNESS MATRICES (SAME AS GLOBAL LOAD TRANSFORMATION MATRICES)
C AND IVECS (ON NUTKX),
C UNIT LOAD BUCKLING MATRICES AND IVECS (ON NUTBX),
C LOCAL LOAD TRANSFORMATION MATRICES AND IVECS (ON NUTLT),
C STRESS TRANSFORMATION MATRICES AND IVECS (ON NUTST)
C FOR COMBINED AXIAL-TORSION-BENDING BAR ELEMENTS.
C MASS, STIFFNESS, BUCKLING MATRICES ARE IN GLOBAL COORDINATE
C DIRECTIONS.
C GLOBAL COORDINATE ORDER FOR EACH ELEMENT IS
C (U,V,W,P,Q,R) JOINT 1, THEN JOINT 2
C WHERE U,V,W ARE TRANSLATIONS AND P,Q,R ARE ROTATIONS.
C IVEC GIVES ELEMENT DOF INTO GLOBAL DOF. EXAMPLES...
C IVEC(6)=834 PLACES ELEMENT DOF 6 INTO GLOBAL DOF 834.
C IVEC(3)=0  OMTS ELEMENT DOF 3 FROM GLOBAL DOF. THIS CONSTRAINS
C ELEMENT DOF 3 TO ZERO MOTION.
C GLOBAL LOAD TRANSFORMATION MATRIX RELATES LOADS AT BAR ENDS IN GLOBAL
C COORDINATE DIRECTIONS TO DEFLECTIONS IN THE GLOBAL COORDINATE
C DIRECTIONS.
C ROW ORDER IN GLOBAL LOAD TRANSFORMATION MATRIX IS
C (PU,PV,PW,MP,MQ,MR) JOINT 1, THEN JOINT 2.
C WHERE P IS FORCE AND M IS MOMENT.
C LOCAL LOAD TRANSFORMATION MATRIX RELATES LOADS AT BAR ENDS IN LOCAL
C COORDINATE SYSTEM TO DEFLECTIONS IN THE GLOBAL COORDINATE DIRECTIONS.
C ROW ORDER IN LOCAL LOAD TRANSFORMATION MATRIX IS
C PX1,PX2,MX1,MX2,FY1,PY2,MZ1,MZ2,PZ1,PZ2,MY1,MY2
C WHERE P IS FORCE AND M IS MOMENT.
C STRESS TRANSFORMATION MATRIX RELATES STRESS AT BAR ENDS IN LOCAL
C COORDINATE SYSTEM TO DEFLECTIONS IN THE GLOBAL COORDINATE DIRECTIONS.
C ROW ORDER IN STRESS TRANSFORMATION MATRIX IS
C PX1/A1,PX2/A2, MX1*R1/TJ1,MX2*R2/TJ2,
C PY1/A1,PY2/A2,MZ1*CY1/BIZ1,MZ2*CY2/BIZ2,
C PZ1/A1,PZ2/A2,MY1*CZ1/EIY1,MY2*CZ2/EIY2
C WHERE P IS FORCE AND M IS MOMENT.
C DATA ARRANGEMENT ON NUTMX, NUTKX, NUTEX, NUTLT, NUTST FOR EACH
C FINITE ELEMENT IS (W=M,K,B,LT,ST)
C WRITE (NUTWX) NAMEW,NEL,NR,NC,NAMEL,(IBLNK,I=1,5),
C ((W(I,J),I=1,NR),J=1,NC),(IVEC(I),I=1,NC)
C CALLS FORMS SUBROUTINES EUCIE, MASIE, PAGEHD, STF18, ZZBOMB.
C DEVELOPED BY WA BENFIELD, CS BODLEY, RL WOHLER. FEBRUARY 1973.
C LAST REVISION BY RL WOHLER. APRIL 1976.
C
C *****
C INPUT DATA READ IN THIS SUBROUTINE FROM NUTEL. IF NUTEL = 5, DATA IS

```

```

C READ FROM CARDS.
C   NAMEM,NAMEK,NAMELT,NAMEST,NAMEB,      FORMAT (5(A6,4X),
C   (KODEK(I),I=1,4),(KODEB(I),I=1,2)      A1,A1,A2,A2,4X,A2,A2)
C   RO,E,G                                  FORMAT (3(5X,E10))
C 20 NEL,J1,J2,JREF,A1,PI1,TJ1,BIZ1,BIY1,SF,
C   IFPY1,IFPZ1,IFPY2,IFPZ2,IFTAPR        FORMAT (4I5,5E10,E5,5A1)
C   IF (J1 .EQ. 0) RETURN
C   IF (IFTAPR .EQ. 1HT) A2,PI2,TJ2,BIZ2,BIY2  FORMAT (20X,5E10)
C 30 IF (NAMEST .EQ. 6H                    .OR. NAMEST .EQ. 6HNOSTRS) GO TO 20
C   R1,CY1,CZ1,R2,CY2,CZ2                FORMAT (20X,6E10)
C   GO TO 20

```

INPUT DATA REQUIREMENTS

	AXIAL ALONG LOCAL X	TORSION ABOUT LOCAL X	BENDING ABOUT LOCAL Z	BENDING ABOUT LOCAL Y
MASS	A,RO	PI,RO	A,RO	A,RO
STIF, LOAD TRANS	A,F	TJ,G	PIZ,A,SF,E,G	BIY,A,SF,E,G
BUCKLING	NONE	NONE	NONE	NONE
STRESS TRANS	SEE STIF	STIF+R	STIF+CY	STIF+CZ

FOR NO SHEAR DEFORMATION IN BENDING, SET ANY OF A (NOT IF AXIAL USED), SF, OF G (NOT IF TORSION IS USED) TO ZERO. IF BENDING STRESS TRANSFORMATION IS WANTED, A MUST NOT BE ZERO.

DEFINITION OF INPUT VARIABLES.

```

C NAMEM = TYPE OF MASS MATRIX WANTED.
C       = M1, DIAGONAL LUMPED.
C       = M2, CONSISTENT.
C       = 6H      OR 6HNOMASS, NO MASS MATRIX CALCULATED.
C NAMEK = TYPE OF STIFFNESS MATRIX WANTED.
C       = K1, CONSTANT FORCE FOR AXIAL, CONSTANT TORQUE FOR TORSION,
C         CONSTANT SHEAR AND LINEAR MOMENT FOR BENDING.
C       = 6H      OR 6HNCSTIF, NO STIFFNESS MATRIX CALCULATED.
C NAMELT = IDENTIFICATION NAME FOR LOAD TRANSFORMATION MATRICES.
C        = 6H      OR 6HNCLOAD, NO LOAD TRANSFORMATIONS CALCULATED.
C NAMEST = IDENTIFICATION NAME FOR STRESS TRANSFORMATION MATRICES.
C        = 6H      OR 6HNOSTRS, NO STRESS TRANSFORMATIONS CALCULATED.
C NAMEB = TYPE OF BUCKLING MATRIX WANTED.
C       = E1, AXIAL ROD.
C       = E2, BEAM.
C       = 6H      OR 6HNCBUCK, NO BUCKLING MATRIX CALCULATED.
C KODEK = OPTION CODE FOR AXIAL, TORSION, BENDING Z, BENDING Y LOCAL
C        STIFFNESS. IF BLANK, ALL FOUR ARE CALCULATED. SIZE(4).
C        KODEK(1)=A , LOCAL STIF MATRIX IS CALCULATED FOR AXIAL
C          (ALONG LOCAL X-AXIS).
C        KODEK(2)=T , LOCAL STIF MATRIX IS CALCULATED FOR TORSION
C          (ABOUT LOCAL X-AXIS).
C        KODEK(3)=EZ, LOCAL STIF MATRIX IS CALCULATED FOR BENDING
C          (ABOUT LOCAL Z-AXIS).
C        KODEK(4)=EY, LOCAL STIF MATRIX IS CALCULATED FOR BENDING
C          (ABOUT LOCAL Y-AXIS).
C KODEB = OPTION CODE FOR BUCKLING IN LOCAL Y OR Z DIRECTION.
C       IF BLANK, BOTH ARE CALCULATED. SIZE(2).
C       KODEB(1)=EY, LOCAL BUCKLING MATRIX IS CALCULATED FOR

```



C DEFLECTION IN LOCAL Y DIRECTION.  
 C KODEE(2)=E2, LOCAL BUCKLING MATRIX IS CALCULATED FOR  
 C DEFLECTION IN LOCAL Z DIRECTION.  
 C RO = MASS DENSITY.  
 C E = YOUNGS MODULUS OF ELASTICITY.  
 C G = SHEAR MODULUS OF ELASTICITY.  
 C NEL = FINITE ELEMENT NUMBER. FOR REFERENCE ONLY, NOT USED IN  
 C CALCULATIONS. WRITTEN ON NUTMX, ETC.  
 C J1 = JOINT NUMBER AT BAR END 1. LOCAL X-AXIS ORIGINATES AT J1.  
 C J2 = JOINT NUMBER AT BAR END 2. LOCAL X-AXIS GOES FROM J1 TO J2.  
 C JREF = REFERENCE POINT. LOCAL Z-AXIS IS DEFINED BY VECTOR (J1,J2)  
 C CPUSSED INTO VECTOR (J1,JREF). LOCAL Y-AXIS LIES IN XY PLANE  
 C DEFINED BY J1,J2,JREF.  
 C A1 = CROSS-SECTION AREA AT BAR END 1.  
 C A2 = SAME AS A1 AT BAR END 2.  
 C PI1 = CROSS-SECTION POLAR AREA MOMENT OF INERTIA FOR MASS  
 C CALCULATIONS AT BAR END 1.  
 C PI2 = SAME AS PI1 AT BAR END 2.  
 C TJ1 = CROSS-SECTION SAINT VENANTS TORSION CONSTANT (J) IN JG FOR  
 C TORSION STIFFNESS AT BAR END 1.  
 C TJ2 = SAME AS TJ1 AT BAR END 2.  
 C BIZ1 = CROSS-SECTION AREA MOMENT OF INERTIA ABOUT LOCAL Z-AXIS  
 C (FOR BENDING) AT BAR END 1.  
 C BIZ2 = SAME AS BIZ1 AT BAR END 2.  
 C BIY1 = CROSS-SECTION AREA MOMENT OF INERTIA ABOUT LOCAL Y-AXIS  
 C (FOR BENDING) AT BAR END 1.  
 C BIY2 = SAME AS BIY1 AT BAR END 2.  
 C SF = SHAPE FACTOR (K) FOR SHEAR IN KAG.  
 C USE SF=0.0 FOR NO SHEAR DEFORMATION IN BENDING.  
 C SF=1.0 FOR A SOLID CIRCULAR CYLINDER.  
 C SF=.5 FOR A THIN WALLED CIRCULAR CYLINDER.  
 C IFPY1 = PIN JOINT OPTION FOR LOCAL COORDINATE THETA Y AT BAR END 1.  
 C = 1H, MOMENT JOINT.  
 C = 1PP, PIN JOINT.  
 C IFPY2 = SAME AS IFPY1 AT BAR END 2.  
 C IFPZ1 = PIN JOINT OPTION FOR LOCAL COORDINATE THETA Z AT BAR END 1.  
 C = 1H, MOMENT JOINT.  
 C = 1PP, PIN JOINT.  
 C IFPZ2 = SAME AS IFPZ1 AT BAR END 2.  
 C IFTAPR = OPTION FOR TAPERED BAR.  
 C = 1H, CONSTANT SECTION PROPERTIES.  
 C = 1HT, LINEAR TAPER SECTION PROPERTIES.  
 C R1 = DISTANCE FROM LOCAL X-AXIS TO OUTER FIBER FOR TORSION  
 C STRESS CALCULATION AT BAR END 1.  
 C R2 = SAME AS R1 AT BAR END 2.  
 C CY1 = DISTANCE FROM LOCAL XZ PLANE TO OUTER FIBER FOR BENDING  
 C STRESS CALCULATION AT BAR END 1. LOCAL Y DIRECTION.  
 C CY2 = SAME AS CY1 AT BAR END 2.  
 C CZ1 = DISTANCE FROM LOCAL XY PLANE TO OUTER FIBER FOR BENDING  
 C STRESS CALCULATION AT BAR END 1. LOCAL Z DIRECTION.  
 C CZ2 = SAME AS CZ1 AT BAR END 2.  
 C  
 C EXPLANATION OF INPUT FORMATS. NUMBER INDICATES CARD COLUMNS USED.  
 C I = INTEGER DATA, RIGHT ADJUSTED.  
 C E = DECIMAL POINT DATA, ANYWHERE IN FIELD. EXPONENT RIGHT ADJUSTED.

```

C      X = CARD COLUMNS SKIPPED.
C      *****
C
C      SUBROUTINE ARGUMENTS (ALL INPUT)
C      XYZ      = MATRIX OF JOINT GLOBAL X,Y,Z LOCATIONS. ROWS CORRESPOND
C                TO JOINT NUMBERS. COLUMNS 1,2,3 CORRESPOND TO THE JOINT
C                X,Y,Z LOCATIONS RESPECTIVELY. SIZE(NJ,3).
C      JDOF     = MATRIX OF JOINT GLOBAL DEGREES OF FREEDOM. ROWS CORRESPOND
C                TO JOINT NUMBERS. COLUMNS 1,2,3 CORRESPOND TO THE JOINT
C                TRANSLATION DOFS AND COLUMNS 4,5,6 CORRESPOND TO THE JOINT
C                ROTATION DOFS. SIZE(NJ,6).
C      EUL      = MATRIX OF JOINT EULER ANGLES (DEGREES). ROWS CORRESPOND
C                TO JOINT NUMBERS. COLUMNS 1,2,3 CORRESPOND TO THE
C                GLOBAL X,Y,Z PERMUTATION. SIZE(NJ,3).
C      NUTEL    = LOGICAL NUMBER OF TAPE CONTAINING ELEMENT INPUT DATA FOR
C                THIS SUBROUTINE. IF NUTEL = 5, DATA IS READ FROM CARDS.
C      NJ       = NUMBER OF JOINTS OR ROWS IN MATRICES (XYZ), (JDOF), (EUL).
C      NUTMX    = LOGICAL NUMBER OF UTILITY TAPE ON WHICH ELEMENT
C                MASS MATRICES AND IVECS ARE OUTPUT.
C                NUTMX MAY BE ZERO IF MASS MATRIX IS NOT FORMED.
C                USES FORTRAN READ, WRITE.
C      NUTKX    = LOGICAL NUMBER OF UTILITY TAPE ON WHICH ELEMENT
C                STIFFNESS MATRICES (SAME AS GLOBAL LOADS TRANSFORMATION
C                MATRICES) AND IVECS ARE OUTPUT.
C                NUTKX MAY BE ZERO IF STIFFNESS MATRIX IS NOT FORMED.
C                USES FORTRAN READ, WRITE.
C      NUTBX    = LOGICAL NUMBER OF UTILITY TAPE ON WHICH ELEMENT UNIT LOAD
C                BUCKLING MATRICES AND IVECS ARE OUTPUT.
C                NUTBX MAY BE ZERO IF BUCKLING MATRIX IS NOT FORMED.
C                USES FORTRAN READ, WRITE.
C      NUTLT    = LOGICAL NUMBER OF UTILITY TAPE ON WHICH ELEMENT LOCAL
C                LOAD TRANSFORMATION MATRICES AND IVECS ARE OUTPUT.
C                NUTLT MAY BE ZERO IF LOAD TRANSFORMATIONS ARE NOT FORMED.
C                USES FORTRAN READ, WRITE.
C      NUTST    = LOGICAL NUMBER OF UTILITY TAPE ON WHICH ELEMENT
C                STRESS TRANSFORMATION MATRICES AND IVECS ARE OUTPUT.
C                NUTST MAY BE ZERO IF STRESS TRANSFORMATIONS ARE NOT FORMED.
C                USES FORTRAN READ, WRITE.
C      W        = MATRIX WORK SPACE. MIN SIZE(12,12).
C      T        = MATRIX WORK SPACE. MIN SIZE(12,12).
C      S        = MATRIX WORK SPACE. MIN SIZE(12,12).
C      KX       = ROW DIMENSION OF XYZ IN CALLING PROGRAM.
C      KJ       = ROW DIMENSION OF JDOF IN CALLING PROGRAM.
C      KE       = ROW DIMENSION OF EUL IN CALLING PROGRAM.
C      KW       = ROW DIMENSION OF W, T, AND S IN CALLING PROGRAM. MIN=12.
C
C      NERROR  EXPLANATION
C      1 = JOINT NUMBER GREATER THAN NUMBER OF JOINTS.
C      2 = STIFFNESS MATRIX FORMED, NUTKX .LE. ZERO.
C      3 = LOAD TRANSFORMATION MATRIX FORMED, NUTLT .LE. ZERO.
C      4 = STRESS TRANSFORMATION MATRIX FORMED, NUTST .LE. ZERO.
C      5 = MASS MATRIX FORMED, NUTMX .LE. ZERO.
C      6 = BUCKLING MATRIX FORMED, NUTBX .LE. ZERO.
C
C      1001 FORMAT (5(A6,4X),A1,A1,A2,A2, 4X A2,A2)

```

```

1002 FORMAT (3(5X,E10.0))
1003 FORMAT (4I5,5E10.0,E5.0,5A1)
1004 FORMAT (20X,6E10.0)
2001 FORMAT (//46X 27HINPUT DATA FOR BAR ELEMENTS)
2002 FORMAT (//40X 39HINPUT DATA FOR BAR ELEMENTS (CONTINUED))
2003 FORMAT ( 45X,8HKODEK = A1,A1,A2,A2, 4X 8HKODEB = A2,A2,
*           / 10X7HMASS = A6, 6X7HSTIF = A6, 6X13HLOAD TRANS = A6,
*           3X15HSTRESS TRANS = A6. 3X11HBUCKLING = A6,
*           / 12X4HRC = E10.3, 6X3HE = E10.3, 80X7HI I I I,
*           / 32X3HG = E10.3, 80X7HF F F F,
*           / 125X7HP P P P,
*           / 1X7HELEMENT 2X5HJOINT 2X5HJOINT 3X3HREF 5X4HAREA
*           7X5HPOLAR 5X7HTORSION 3X9HZ BENDING 2X9HY BENDING
*           2X5HSHEAR 3X6HSTRESS 5X6HSTRESS 5X6HSTRESS 3X7HY Z Y Z
*           / 1X6HNUMBER 5X1H1 6X1H2 4X5HPOINT
*           14X 7HINERTIA 5X5HCONST 5X7HINERTIA
*           4X7HINERTIA 3X6HFACTOR 5X1HR 9X2HCY 9X2HCZ 5X7HI 1 2 2/)
2004 FORMAT (1X I5, I8, 2I7, 1X 5E11.3, F7.3, 3E11.3, 4(1XA1))
2005 FORMAT (29X,5E11.3,7X,3E11.3)

```

C

C READ AND WRITE FINITE ELEMENT DATA.

```

R1 = 0.0
CY1 = 0.0
CZ1 = 0.0
NLINE = 0
CALL PAGEHD
WRITE (NOT,2001)
READ (NUTEL,1001) NAMEM,NAMEK,NAMELT,NAMEST,NAMEB,
*           (KODEK(I),I=1,4),(KODEB(I),I=1,2)
READ (NUTEL,1002) RO,E,G
WRITE (NOT,2003) (KODEK(I),I=1,4),(KODEB(I),I=1,2),
*           NAMEM,NAMEK,NAMELT,NAMEST,NAMEB,RO,E,G
20 READ (NUTEL,1003) NEL,J1,J2,JREF,A1,PI1,TJ1,BIZ1,BIY1,SF,
*           IFPIN,IFTAPR
IF (J1 .LE. 0) RETURN
IF (IFTAPR .EQ. 1HT) READ (NUTEL,1004) A2,PI2,TJ2,BIZ2,BIY2
IF (NAMEST .EQ. 6H .OR. NAMEST .EQ. 6HNOSTRS) GO TO 25
READ (NUTEL,1004) R1,CY1,CZ1,R2,CY2,CZ2
25 NLINE = NLINE + 1
IF (IFTAPR .EQ. 1HT) NLINE=NLINE+1
IF (NLINE .LE. 42) GO TO 30
CALL PAGEHD
WRITE (NOT,2002)
WRITE (NOT,2003) (KODEK(I),I=1,4),(KODEB(I),I=1,2),
*           NAMEM,NAMEK,NAMELT,NAMEST,NAMEB,RO,E,G
NLINE = 0
30 WRITE (NOT,2004) NEL,J1,J2,JREF,A1,PI1,TJ1,BIZ1,BIY1,SF,
*           R1,CY1,CZ1,IFPIN
NERROR=1
IF (J1 .GT. NJ .OR. J2 .GT. NJ .OR. JREF .GT. NJ) GO TO 999
IF (IFTAPR .EQ. 1HT) WRITE (NOT,2005) A2,PI2,TJ2,BIZ2,BIY2,R2,
*           CY2,CZ2

```

C

C FORM FINITE ELEMENT COORDINATE LOCATIONS, EULER ANGLES, REVADD IVEC.  
DO 42 I=1,3

```

      CJ(I,1) = XYZ(J1,I)
      CJ(I,2) = XYZ(J2,I)
      CJ(I,3) = XYZ(JREF,I)
      EJ(I,1) = EUL(J1,I)
42    EJ(I,2) = EUL(J2,I)
      DO 44 I=1,6
      IV1(I) = JDOF(J1,I)
44    IV1(I+6) = JDOF(J2,I)
C
C  FORM DATA FOR UNIFORM ELEMENT.
      IF (IFTAPR .EQ. 1HT) GO TO 50
      A2 = A1
      P12 = P11
      TJ2 = TJ1
      B122 = B121
      BIY2 = BIY1
      R2 = R1
      CY2 = CY1
      CZ2 = CZ1
C
C  FORM PINNING IVEC.
50    NPIN = 0
      DO 55 I=1,4
      IF (IFPIN(I) .NE. 1HP) GO TO 55
      NPIN = NPIN + 1
      IF (I .EQ. 1) IV2(NPIN) = 11
      IF (I .EQ. 2) IV2(NPIN) = 7
      IF (I .EQ. 3) IV2(NPIN) = 12
      IF (I .EQ. 4) IV2(NPIN) = 8
55    CONTINUE
C
C  FORM STIFFNESS MATRIX (W), LOCAL LOAD TRANSFORMATION MATRIX (T),
C  STRESS TRANSFORMATION MATRIX (S).
100   IF (NAMEK .EQ. 6H .OR. NAMEK .EQ. 6HNOSTIF) GO TO 110
      CALL STF1B (CJ,EJ,KODEK,A1,A2,TJ1,TJ2,B121,B122,BIY1,BIY2,R1,R2,
      *          CY1,CY2,CZ1,CZ2,SF,E,G,NAMEK,NAMEST,W,T,S,NRST,
      *          KCJ,KCJ,KW,KW,KW)
C
C  PIN STIFFNESS MATRIX.
      IF (NPIN .EQ. 0) GO TO 105
      CALL DCOS1B (CJ,EJ,W,KCJ,KCJ,KW)
      CALL TRANS (W,TR,NRW,NRW,KW,KTR)
      CALL MULTA (T,TR,NRLT,NRW,NRW,KW,KTR)
      CALL SPED3 (T,IV2,T,TD,NRW,NPIN,1,KW)
      CALL MULTA (TD,W,NRW,NRW,NRW,KTD,KW)
      CALL MULTA (TR,TD,NRW,NRW,NRW,KTR,KTD)
      CALL MULTA (T,W,NRLT,NRW,NRW,KW,KW)
      CALL ATXPA1 (W,T,NRW,NRW,KW,KW)
      IF (NAMEST .EQ. 6H .OR. NAMEST .EQ. 6HNOSTRS) GO TO 105
      CALL MULTA (S,TR,NRST,NRW,NRW,KW,KTR)
105   IF (NUTKX .LE. 0) GO TO 999
      WRITE (NUTKX) NAMEK,NEL,NRW,NRW,NAMEL,(IBLNK,I=1,5),
      *          ((W(I,J),I=1,NRW),J=1,NRW),(IV1(I),I=1,NRW)
      IF (NAMELT .EQ. 6H .OR. NAMELT .EQ. 6HNOLOAD) GO TO 115

```

NERROR=2

NERROR=3

```

IF (NUTLT .LE. 0) GO TO 999
WRITE (NUTLT) NAMELT,NEL,NRLT,NRW,NAMEL,(IBLNK,I=1,5),
*      ((T(I,J),I=1,NRLT),J=1,NRW),(IV1(I),I=1,NRW)
115 IF (NAMEST .EQ. 6H      .OR. NAMEST .EQ. 6HNOSTRS) GO TO 110

```

NERROR=4

```

IF (NUTST .LE. 0) GO TO 999
WRITE (NUTST) NAMEST,NEL,NRST,NRW,NAMEL,(IBLNK,I=1,5),
*      ((S(I,J),I=1,NRST),J=1,NRW),(IV1(I),I=1,NRW)

```

C

C FORM MASS MATRIX (W).

```

110 IF (NAMEM .EQ. 6H      .OR. NAMEM .EQ. 6HNOMASS) GO TO 140
CALL MASIB (CJ,EJ,A1,A2,PI1,PI2,RO,NAMEM,W,T,KCJ,KCJ,KW,KW)

```

C

C PIN MASS MATRIX.

```

IF (NPIN .GT. 0) CALL BTABA (W,TR,NRW,NRW,KW,KTR)

```

NERROR=5

```

IF (NUTMX .LE. 0) GO TO 999
WRITE (NUTMX) NAMEM,NEL,NRW,NRW,NAMEL,(IBLNK,I=1,5),
*      ((W(I,J),I=1,NRW),J=1,NRW),(IV1(I),I=1,NRW)

```

C

C FORM UNIT LOAD BUCKLING MATRIX (W).

```

140 IF (NAMEB .EQ. 6H      .OR. NAMEB .EQ. 6HNOBUCK) GO TO 20
CALL BUCIB (CJ,EJ,KODEB,NAMEB,W,S,KCJ,KCJ,KW,KW)

```

NERROR=6

```

IF (NUTPX .LE. 0) GO TO 999
WRITE (NUTBX) NAMEB,NEL,NRW,NRW,NAMEL,(IBLNK,I=1,5),
*      ((W(I,J),I=1,NRW),J=1,NRW),(IV1(I),I=1,NRW)
GO TO 20

```

C

```

999 CALL ZZBOMB (6HBAR ,NERROR)
END

```



```
IF (KODEB(1) .NE. 2HBZ) KODEBY = 0
IF (KODEB(2) .NE. 2HBZ) KODEBZ = 0
10 IF (NAMEB .EQ. 6HB1 ) GO TO 110
IF (NAMEB .EQ. 6HB2 ) GO TO 120
```

NERROR=2

GO TO 999

```
C
110 IF (KODEBY .EQ. 1) CALL B1A1 (RL,Z(5,5),KZ)
IF (KODEBZ .EQ. 1) CALL B1A1 (RL,Z(9,9),KZ)
GO TO 300
```

```
C
120 IF (KODEBY .EQ. 1) CALL B1A2 (RL,Z(5,5),KZ)
DO 125 J=7,8
DO 125 I=5,6
Z(I,J) =-Z(I,J)
125 Z(J,I) =-Z(J,I)
IF (KODEBZ .EQ. 1) CALL B1A2 (RL,Z(9,9),KZ)
```

```
C
300 CALL DCOSIB (CJ,EJ,W,KCJ,KEJ,KW)
CALL PTABA (Z,W, 12,12, KZ,KW)
RETURN
```

```
C
999 CALL ZZBOMB (6HBUC1B ,NERROR)
END
```

```

SUBROUTINE DCOS1A (CJ,EJ,2,KCJ,KEJ,KZ)
DIMENSION CJ(KCJ,1), EJ(KEJ,1), Z(KZ,1)
DIMENSION P(3), T(3,3)

```

```

C
C SUBROUTINE TO CALCULATE FINITE ELEMENT...
C DIRECTION COSINE MATRIX
C FOR AN AXIAL ROD ELEMENT.
C THE DIRECTION COSINE MATRIX RELATES LOCAL COORDINATE DISPLACEMENTS
C TO GLOBAL COORDINATE DISPLACEMENTS.
C THE LOCAL COORDINATE SYSTEM ASSUMES THE ROD TO LIE ALONG THE X AXIS
C WITH JOINT 1 AT THE ORIGIN, JOINT 2 ALONG THE POSITIVE X AXIS.
C ROW ORDER (LOCAL COORDINATE ORDER) OF DIRECTION COSINE MATRIX IS
C DX1,DX2
C WHERE DX IS TRANSLATION.
C COLUMN ORDER (GLOBAL COORDINATE ORDER) OF DIRECTION COSINE MATRIX IS
C (U,V,W) JOINT 1, THEN JOINT 2.
C WHERE U,V,W ARE TRANSLATIONS.
C EULER ANGLE CONVENTION IS GLOBAL X,Y,Z PERMUTATION.
C CALLS FORMA SUBROUTINES EULER,MULTB,ZZBOMB.
C DEVELOPED BY RL WOHLER. SEPTEMBER 1972.
C LAST REVISION BY WA BENFIELD. MARCH 1976.
C
C SUBROUTINE ARGUMENTS
C CJ = INPUT MATRIX OF GLOBAL X,Y,Z COORDINATES AT ROD JOINTS.
C ROWS 1,2,3 CORRESPOND TO X,Y,Z COORDINATES.
C COLS 1,2 CORRESPOND TO JOINTS 1,2. SIZE(3,2).
C EJ = INPUT MATRIX OF EULER ANGLES (DEGREES) AT ROD JOINTS.
C ROWS 1,2,3 CORRESPOND TO GLOBAL X,Y,Z PERMUTATION.
C COLS 1,2 CORRESPOND TO JOINTS 1,2. SIZE(3,2).
C Z = OUTPUT DIRECTION COSINE MATRIX. SIZE(2,6).
C KCJ = INPUT ROW DIMENSION OF CJ IN CALLING PROGRAM.
C KEJ = INPUT ROW DIMENSION OF EJ IN CALLING PROGRAM.
C KZ = INPUT ROW DIMENSION OF Z IN CALLING PROGRAM. MIN=2.
C
C NEPROR EXPLANATION
C 1 = DIMENSION SIZE LESS THAN 2.
C

```

NERROR = 1

```

IF (KZ .LT. 2) GO TO 999
PX = CJ(1,2)-CJ(1,1)
PY = CJ(2,2)-CJ(2,1)
PZ = CJ(3,2)-CJ(3,1)
PL = SQRT(PX**2 + PY**2 + PZ**2)
P(1) = PX/PL
P(2) = PY/PL
P(3) = PZ/PL
DO 10 I=1,2
DO 10 J=1,6
10 Z(I,J) = 0.0
CALL EULER (EJ(1,1),T,3)
CALL MULTB (P,T, 1,3,3, 1,3)
DO 22 J=1,3
22 Z(1,J) = T(1,J)
CALL EULER (EJ(1,2),T,3)
CALL MULTB (P,T, 1,3,3, 1,3)

```



```
DO 24 J=1,3  
24 Z(2,J+3) = T(1,J)  
RETURN
```

C

```
999 CALL ZZBOMB (6HDCOSIA,NERROR)  
END
```

```

SUBROUTINE DCOS1B (CJ,EJ,Z,KCJ,KEJ,KZ)
DIMENSION CJ(KCJ,1), EJ(KEJ,1), Z(KZ,1)
DIMENSION W(3,3), T(3,3)

C
C SUBROUTINE TO CALCULATE FINITE ELEMENT...
C DIRECTION COSINE MATRIX
C FOR A COMBINED AXIAL-TORSION-BENDING BAR ELEMENT.
C THE DIRECTION COSINE MATRIX RELATES LOCAL COORDINATE DISPLACEMENTS
C TO GLOBAL COORDINATE DISPLACEMENTS.
C THE LOCAL COORDINATE SYSTEM ASSUMES THE BAR TO LIE IN THE X-Y PLANE
C WITH JOINT 1 AT THE ORIGIN, JOINT 2 ALONG THE POSITIVE X AXIS,
C REFERENCE POINT 3 (TO DEFINE THE LOCAL X-Y PLANE) IS IN THE
C POSITIVE Y DIRECTION.
C ROW ORDER (LOCAL COORDINATE ORDER) OF DIRECTION COSINE MATRIX IS
C DX1,DX2, TX1, TX2, DY1,DY2, TZ1, TZ2, DZ1, DZ2, TY1, TY2
C WHERE DX,DY,DZ ARE TRANSLATIONS AND TX, TY, TZ ARE ROTATIONS.
C COLUMN ORDER (GLOBAL COORDINATE ORDER) OF DIRECTION COSINE MATRIX IS
C (U,V,W,P,Q,R) JOINT 1, THEN JOINT 2
C WHERE U,V,W ARE TRANSLATIONS AND P,Q,R ARE ROTATIONS.
C EULER ANGLE CONVENTION IS GLOBAL X,Y,Z PERMUTATION.
C CALLS FORMA SUBROUTINES EULER,MULTB,ZZBOMB.
C DEVELOPED BY RL WOHLER. FEBRUARY 1973.
C LAST REVISION BY WA BENFIELD. MARCH 1976.
C
C SUBROUTINE ARGUMENTS
C CJ = INPUT MATRIX OF GLOBAL X,Y,Z COORDINATES AT BAR JOINTS.
C ROWS 1,2,3 CORRESPOND TO X,Y,Z COORDINATES.
C COLS 1,2 CORRESPOND TO JOINTS 1,2. COL 3 CORRESPONDS
C TO REFERENCE POINT TO DEFINE LOCAL XY PLANE. SIZE(3,3).
C EJ = INPUT MATRIX OF EULER ANGLES (DEGREES) AT BAR JOINTS.
C ROWS 1,2,3 CORRESPOND TO GLOBAL X,Y,Z PERMUTATION.
C COLS 1,2 CORRESPOND TO JOINTS 1,2. SIZE(3,2).
C Z = OUTPUT DIRECTION COSINE MATRIX. SIZE(12,12).
C KCJ = INPUT ROW DIMENSION OF CJ IN CALLING PROGRAM.
C KEJ = INPUT ROW DIMENSION OF EJ IN CALLING PROGRAM.
C KZ = INPUT ROW DIMENSION OF Z IN CALLING PROGRAM. MIN=12.
C
C NERROR EXPLANATION
C I = DIMENSION SIZE LESS THAN 12.
C
C NERROR = 1

IF (KZ .LT. 12) GO TO 999
PX = CJ(1,2)-CJ(1,1)
PY = CJ(2,2)-CJ(2,1)
PZ = CJ(3,2)-CJ(3,1)
PL = SQRT(PX**2 + PY**2 + PZ**2)
RX = PY*(CJ(3,3)-CJ(3,1)) - PZ*(CJ(2,3)-CJ(2,1))
RY = PZ*(CJ(1,3)-CJ(1,1)) - PX*(CJ(3,3)-CJ(3,1))
RZ = PX*(CJ(2,3)-CJ(2,1)) - PY*(CJ(1,3)-CJ(1,1))
RL = SQRT(RX**2 + RY**2 + RZ**2)
QX = RY*PZ - RZ*PY
QY = RZ*PX - RX*PZ
QZ = RX*PY - RY*PX
QL = SQRT(QX**2 + QY**2 + QZ**2)
W(1,1) = PX/PL

```

```
W(1,2) = PY/PL
W(1,3) = PZ/PL
W(2,1) = QX/QL
W(2,2) = QY/QL
W(2,3) = QZ/QL
W(3,1) = RX/RL
W(3,2) = RY/RL
W(3,3) = RZ/RL
DO 10 J=1,12
DO 10 I=1,12
10 Z(I,J) = 0.0
CALL EULER (EJ(1,1),T,3)
CALL MULTB (W,T, 3,3,3, 3,3)
DO 22 J=1,3
Z(1,J) = T(1,J)
Z(5,J) = T(2,J)
Z(9,J) = T(3,J)
JP3 = J+3
Z( 3,JP3) = T(1,J)
Z( 7,JP3) = T(3,J)
22 Z(11,JP3) = T(2,J)
CALL EULER (EJ(1,2),T,3)
CALL MULTB (W,T, 3,3,3, 3,3)
DO 24 J=1,3
JP6 = J+6
Z( 2,JP6) = T(1,J)
Z( 6,JP6) = T(2,J)
Z(10,JP6) = T(3,J)
JP9 = J+9
Z( 4,JP9) = T(1,J)
Z( 8,JP9) = T(3,J)
24 Z(12,JP9) = T(2,J)
RETURN
999 CALL ZZBOMB (6HDCOS1B,NERRGR)
END
```



```
W(1,3) = PZ/PL
W(2,1) = QX/QL
W(2,2) = QY/QL
W(2,3) = QZ/QL
W(3,1) = RX/RL
W(3,2) = RY/RL
W(3,3) = RZ/RL
DO 10 J=1,18
DO 10 I=1,18
10 Z(I,J) = 0.0
DO 50 NW=1,3
CALL EULER (EJ(1,NW),T,3)
CALL MULTF (W,T,3,3,3,3,3)
IZZ = 3*(NW-1)
JZZ = 6*(NW-1)
DO 50 JW=1,3
JZ = JZZ+JW
Z(IZZ+ 1,JZ) = T(1,JW)
Z(IZZ+ 2,JZ) = T(2,JW)
Z(IZZ+10,JZ) = T(3,JW)
JZ = JZ+3
Z(IZZ+ 3,JZ) = T(3,JW)
Z(IZZ+11,JZ) = T(1,JW)
50 Z(IZZ+12,JZ) = T(2,JW)
RETURN
C
999 CALL ZZSOME (6HDCOS2 ,NERROR)
END
```



```
DO 10 J=1,12
DO 10 I=1,8
10 Z(I,J) = 0.0
DO 50 IJNT=1,4
CALL EULER (EJ(I,IJNT),T,3)
CALL MULTP (W,T, 2,3,3, 2,3)
JZZ = 3*(IJNT-1)
DO 50 JW=1,3
JZ = JZZ+JW
Z(IJNT ,JZ) = T(1,JW)
50 Z(IJNT+4,JZ) = T(2,JW)
RETURN
```

```
C
999 CALL ZZBOMB (6HDCOS3C,NERROR)
END
```

EULER

SUBROUTINE EULER (E,R,KR)  
DIMENSION E(1),R(KR,1)

C  
C CALCULATE EULER ANGLE ROTATION TRANSFORMATION MATRIX.  
C EULER ANGLE CONVENTION IS GLOBAL X,Y,Z PERMUTATION.  
C DEVELOPED BY C. BODLEY. MARCH 1973.  
C  
C SUBROUTINE ARGUMENTS  
C E = INPUT VECTOR OF JOINT EULER ANGLES (DEGREES).  
C LOCATIONS 1,2,3 CORRESPOND TO THE GLOBAL X,Y,Z  
C PERMUTATION. SIZE(3).  
C R = OUTPUT EULER ROTATION TRANSFORMATION MATRIX. SIZE(3,3).  
C KR = INPUT ROW DIMENSION OF R IN CALLING PROGRAM.  
C  
C DTOR = ATAN2(1.,1.)/45.  
C  
C C1 = COS(E(1)\*DTOR)  
C C2 = COS(E(2)\*DTOR)  
C C3 = COS(E(3)\*DTOR)  
C S1 = SIN(E(1)\*DTOR)  
C S2 = SIN(E(2)\*DTOR)  
C S3 = SIN(E(3)\*DTOR)  
C  
C R(1,1) = C2\*C3  
C R(1,2) = -C2\*S3  
C R(1,3) = S2  
C R(2,1) = C1\*S3 + S1\*S2\*C3  
C R(2,2) = C1\*C3 - S1\*S2\*S3  
C R(2,3) = -S1\*C2  
C R(3,1) = S1\*S3 - C1\*S2\*C3  
C R(3,2) = S1\*C3 + C1\*S2\*S3  
C R(3,3) = C1\*C2  
C  
C RETURN  
C END



```

SUBROUTINE FINEL (XYZ,JDOF,EUL,NUTEL,NJ,
*           NUTM,NUTK,NUTLT,NUTST,NUTB,V,LV,KV,
*           KRX,KRJ,KRE,NUTMX,NUTKX,NUT1,NUT2,NUT3)
DIMENSION XYZ(KRX,1), JDOF(KRJ,1), EUL(KRE,1), V(1), LV(1)
DIMENSION W1(24,24), W2(24,24), W3(24,24)
DATA KW/24/, IBLANK/6H      /, 11/1/
DATA NIT,NOT/5,6/

C
C SUBROUTINE TO CALCULATE (ON OPTION) FINITE ELEMENT...
C   ASSEMBLED MASS MATRIX (ON NUTM),
C   ASSEMBLED STIFFNESS MATRIX (ON NUTK),
C   ELEMENT LOCAL LOAD TRANSFORMATION MATRICES, IVECS (ON NUTLT),
C   ELEMENT GLOBAL LOAD TRANSFORMATION MATRICES, IVECS (ON NUTKX),
C   ELEMENT STRESS TRANSFORMATION MATRICES, IVECS (ON NUTST),
C   ELEMENT UNIT LOAD BUCKLING MATRICES, IVECS (ON NUTB).
C IVEC GIVES ELEMENT DOF INTO GLOBAL DOF. EXAMPLES...
C   IVEC(6)=834 PLACES ELEMENT DOF 6 INTO GLOBAL DOF 834.
C   IVEC(3)=0  OMTS ELEMENT DOF 3 FROM GLOBAL DOF. THIS CONSTRAINS
C             ELEMENT DOF 3 TO ZERO MOTION.
C DATA ARRANGEMENT ON NUTM, NUTK FOR THE ASSEMBLED MATRICES IS IN
C SPARSE (Y) FORMA SUBROUTINE FORMAT.
C DATA ARRANGEMENT ON NUTLT, NUTKX, NUTST, NUTB FOR EACH FINITE
C ELEMENT (WRITTEN IN SUBROUTINE AXIAL, BAR, ETC) IS
C   WRITE (NUTW) NAMEW,NEL,NP,NC,NAMEL (IBLANK,I=1,5),
C             ((W(I,J),I=1,NP),J=1,NC),(IVEC(I),I=1,NC)
C   NAMEW = NAMELT,NAMEKX,NAMEST, OR NAMEB.
C   NAMEL = AXIAL,BAR,ETC.
C LAST RECORD (TO DENOTE TERMINATION) IS,
C   WRITE (NUTW) IBLANK,(11,I=1,30)
C THE FOLLOWING UTILITY TAPES USE BASIC FORTRAN READ, WRITE. DO NOT
C USE THESE TAPES IN SPARSE (Y) FORMA SUBROUTINES WHICH USE FORMA
C SUBROUTINES YIN, YOUT (BECAUSE THEY USE BUFFER IN, BUFFER OUT).
C   NUTLT, NUTST, NUTMX, NUTKX, NUTB.
C THE FOLLOWING UTILITY TAPES USE FORMA YIN, YOUT.
C   NUTM, NUTK, NUT1, NUT2, NUT3.
C CALLS FORMA SUBROUTINES AXIAL ,BAR ,FLUID ,GRAVITY,PAGEHD,QUAD ,
C             RECTSP,TRNGL ,YRVAD2,ZZBCMB.
C DEVELOPED BY WA BENFIELD, CS BODLEY, RL WOHLER. JANUARY 1973.
C LAST REVISION BY  RL WOHLER.  MAY 1976.
C
C *****
C INPUT DATA READ IN THIS SUBROUTINE FROM NUTEL. IF NUTEL = 5, DATA IS
C READ FROM CARDS.
C 50 NAMEL                                FORMAT (A6)
C   IF (NAMEL .EQ. 6HRETURN) RETURN
C   IF (NAMEL .EQ. 6HAXIAL ) CALL AXIAL (SEE SUBRT FOR INPUT)
C   IF (NAMEL .EQ. 6HBAR   ) CALL BAR  (SEE SUBRT FOR INPUT)
C   IF (NAMEL .EQ. 6HFLUID ) CALL FLUID (SEE SUBRT FOR INPUT)
C   IF (NAMEL .EQ. 6HGRAVTY) CALL GRAVTY (SEE SUBRT FOR INPUT)
C   IF (NAMEL .EQ. 6HQUAD  ) CALL QUAD  (SEE SUBRT FOR INPUT)
C   IF (NAMEL .EQ. 6HRECTSP) CALL RECTSP (SEE SUBRT FOR INPUT)
C   IF (NAMEL .EQ. 6HTRNGL ) CALL TRNGL  (SEE SUBRT FOR INPUT)
C   GO TO 50
C
C DEFINITION OF INPUT VARIABLES.

```

C NAMEL = AXIAL, BAR, ETC AS SHOWN ABOVE. GIVES SUBROUTINE CALLED.  
 C  
 C EXPLANATION OF INPUT FORMATS. NUMBER INDICATES CARD COLUMNS USED.  
 C A = ANY KEYPUNCH SYMBOL.  
 C X = CARD COLUMNS SKIPPED.  
 C \*\*\*\*\*  
 C  
 C SUBROUTINE ARGUMENTS (ALL INPUT)  
 C XYZ = MATRIX OF JOINT GLOBAL X,Y,Z LOCATIONS. ROWS CORRESPOND  
 C TO JOINT NUMBERS. COLUMNS 1,2,3 CORRESPOND TO THE JOINT  
 C X,Y,Z LOCATIONS RESPECTIVELY. SIZE(NJ,3).  
 C MAY BE EQUIVALENCED TO V(1) IN CALLING PROGRAM.  
 C JDOF = MATRIX OF JOINT GLOBAL DEGREES OF FREEDOM. ROWS CORRESPOND  
 C TO JOINT NUMBERS. COLUMNS 1,2,3 CORRESPOND TO THE JOINT  
 C TRANSLATION DOFS AND COLUMNS 4,5,6 CORRESPOND TO THE JOINT  
 C ROTATION DOFS. SIZE(NJ,6).  
 C MAY BE EQUIVALENCED TO LV(1) IN CALLING PROGRAM.  
 C EUL = MATRIX OF JOINT EULER ANGLES (DEGREES). ROWS CORRESPOND  
 C TO JOINT NUMBERS. COLUMNS 1,2,3 CORRESPOND TO THE  
 C GLOBAL X,Y,Z PERMUTATION. SIZE(NJ,3). MAY BE  
 C EQUIVALENCED TO VKRX\*(XYZ COL DIM)+1) IN CALLING PROGRAM.  
 C NUTEL = LOGICAL NUMBER OF TAPE CONTAINING ELEMENT INPUT DATA FOR  
 C THIS SUBROUTINE AND SUBROUTINES AXIAL, ETC GIVEN BY NAMEL.  
 C IF NUTEL = 5, DATA WILL BE READ FROM CARDS.  
 C NJ = NUMBER OF JOINTS OR ROWS IN MATRICES (XYZ), (JDOF), (EUL).  
 C NUTM = LOGICAL NUMBER OF UTILITY TAPE ON WHICH ASSEMBLED  
 C MASS MATRIX IS OUTPUT IN SPARSE NOTATION.  
 C NUTM MAY BE ZERO IF MASS MATRIX IS NOT FORMED.  
 C USES FORMA YIN, YOUT.  
 C NUTK = LOGICAL NUMBER OF UTILITY TAPE ON WHICH ASSEMBLED  
 C STIFFNESS MATRIX IS OUTPUT IN SPARSE NOTATION.  
 C NUTK MAY BE ZERO IF STIFFNESS MATRIX IS NOT FORMED.  
 C USES FORMA YIN, YOUT.  
 C NUTLT = LOGICAL NUMBER OF UTILITY TAPE ON WHICH ELEMENT LOCAL  
 C LOAD TRANSFORMATION MATRICES AND IVECS ARE OUTPUT.  
 C NUTLT MAY BE ZERO IF LOAD TRANSFORMATIONS ARE NOT FORMED.  
 C USES FORTRAN READ, WRITE.  
 C NUTST = LOGICAL NUMBER OF UTILITY TAPE ON WHICH ELEMENT  
 C STRESS TRANSFORMATION MATRICES AND IVECS ARE OUTPUT.  
 C NUTST MAY BE ZERO IF STRESS TRANSFORMATIONS ARE NOT FORMED.  
 C USES FORTRAN READ, WRITE.  
 C NUTB = LOGICAL NUMBER OF UTILITY TAPE ON WHICH ELEMENT UNIT LOAD  
 C BUCKLING MATRICES AND IVECS ARE OUTPUT.  
 C NUTB MAY BE ZERO IF BUCKLING MATRICES ARE NOT FORMED.  
 C USES FORTRAN READ, WRITE.  
 C V = VECTOR WORK SPACE.  
 C LV = VECTOR WORK SPACE.  
 C KV = DIMENSION SIZE OF V,LV IN CALLING PROGRAM.  
 C KRX = ROW DIMENSION OF XYZ IN CALLING PROGRAM.  
 C KRJ = ROW DIMENSION OF JDOF IN CALLING PROGRAM.  
 C KRE = ROW DIMENSION OF EUL IN CALLING PROGRAM.  
 C NUTMX = LOGICAL NUMBER OF UTILITY TAPE ON WHICH ELEMENT  
 C MASS MATRICES AND IVECS ARE STORED.  
 C NUTMX MAY BE ZERO IF MASS MATRIX IS NOT FORMED.  
 C USES FORTRAN READ, WRITE.  
 C

```

C NUTKX = LOGICAL NUMBER OF UTILITY TAPE ON WHICH ELEMENT
C STIFFNESS MATRICES (SAME AS GLOBAL LOADS TRANSFORMATION
C MATRICES) AND IVECS ARE STORED.
C NUTKX MAY BE ZERO IF STIFFNESS MATRIX IS NOT FORMED.
C USES FORTRAN READ, WRITE.
C NUT1 = LOGICAL NUMBER OF UTILITY TAPE. USES FORMS YIN, YOUT.
C NUT2 = LOGICAL NUMBER OF UTILITY TAPE. USES FORMS YIN, YOUT.
C NUT3 = LOGICAL NUMBER OF UTILITY TAPE. USES FORMS YIN, YOUT.
C
C ERROR EXPLANATION
C 1 = NAMEL IMPROPERLY DEFINED.
C
1001 FORMAT (A6)
2001 FORMAT (//41X 35HJOINT DATA USED IN SUBROUTINE FINEL)
2002 FORMAT (//35X 47HJOINT DATA USED IN SUBROUTINE FINEL (CONTINUED))
2003 FORMAT ( /16X 18HDEGREES OF FREEDOM
* 18X 28HGLOBAL CARTESIAN COORDINATES
* 12X 22HEULER ANGLES (DEGREES)
* /14X 11HTRANSLATION 8X 8HROTATION
* / 2X5HJOINT 6X1HU 5X1HV 5X1HW 5X1HP 5X1HQ 5X1HR
* 11X1HX 11X1HY 11X1HZ 14X1HX 10X1HY 10X1HZ /)
2004 FORMAT (1X I5, 3X 6I6, 3X 3F12.4, 4X 3F11.4)
C
IF (NUTMX .GT. 0) REWIND NUTMX
IF (NUTKX .GT. 0) REWIND NUTKX
IF (NUTE .GT. 0) REWIND NUTE
IF (NUTLT .GT. 0) REWIND NUTLT
IF (NUTST .GT. 0) REWIND NUTST
C
C DETERMINE SIZE OF FINAL MASS-STIFFNESS MATRIX FROM THE MAXIMUM DOF
C NUMBER IN JDOF.
NDOF = JDOF(1,1)
DO 35 I=1,NJ
DO 35 J=1,6
IF (JDOF(I,J) .GT. NDOF) NDOF=JDOF(I,J)
35 CONTINUE
C
C PRINT JOINT DOF, XYZ COORDINATES, EULER ANGLES.
CALL PAGEHD
WRITE (NOT,2001)
WRITE (NOT,2003)
NLINE = 0
DO 40 IJ=1,NJ
NLINE = NLINE+1
IF (NLINE .LE. 42) GO TO 40
CALL PAGEHD
WRITE (NOT,2002)
WRITE (NOT,2003)
NLINE = 1
40 WRITE (NOT,2004) IJ, (JDOF(IJ,J), J=1,6), (XYZ(IJ,J), J=1,3),
* (EUL(IJ,J), J=1,3)
C
C READ FINITE ELEMENT TYPE.
50 READ (NUTEL,1001) NAMEL
IF (NAMEL .EQ. 6HRETURN) GO TO 50C

```

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IF (NAMEL .EQ. 6HAXIAL ) GO TO 110
IF (NAMEL .EQ. 6HEAR ) GO TO 140
IF (NAMEL .EQ. 6PTRNGL ) GO TO 150
IF (NAMEL .EQ. 6HFLUID ) GO TO 151
IF (NAMEL .EQ. 6HQUAD ) GO TO 160
IF (NAMEL .EQ. 6HRECTSP) GO TO 162
IF (NAMEL .EQ. 6HGRAVTY) GO TO 171

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NERROR=1
GO TO 999

```

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C BAR FINITE ELEMENT (AXIAL ONLY).
110 CALL AXIAL (XYZ,JDOF,EUL,NUTEL,NJ,
*           NUTMX,NUTKX,NUTLT,NUTST,
*           W1,W2,W3,KRX,KRJ,KRE,KW)
GO TO 50
C BAR FINITE ELEMENT (COMBINED AXIAL, TORSION, BENDING).
140 CALL BAR (XYZ,JDOF,EUL,NUTEL,NJ,
*           NUTMX,NUTKX,NUTB,NUTLT,NUTST,
*           W1,W2,W3,KRX,KRJ,KRE,KW)
GO TO 50
C TRIANGULAR PLATE ELEMENT.
150 CALL TRNGL (XYZ,JDOF,EUL,NUTEL,NJ,
*           NUTMX,NUTKX,NUTB,NUTLT,NUTST,
*           W1,W2,W3,KRX,KRJ,KRE,KW)
GO TO 50
C FLUID ELEMENT.
151 CALL FLUID (XYZ,JDOF,EUL,NUTEL,NJ,
*           NUTMX,NUTKX, NUTLT,NUTST,
*           W1,W2,W3,KRX,KRJ,KRE,KW)
GO TO 50
C QUADRILATERAL PLATE ELEMENT.
160 CALL QUAD (XYZ,JDOF,EUL,NUTEL,NJ,
*           NUTMX,NUTKX,NUTB,NUTLT,NUTST,
*           W1,W2,W3,KRX,KRJ,KRE,KW)
GO TO 50
C RECTANGULAR SHEAR PANEL.
162 CALL RECTSP (XYZ,JDOF,EUL,NUTEL,NJ,
*           NUTMX,NUTKX,NUTLT,NUTST,
*           W1,W2,W3,KRX,KRJ,KRE,KW)
GO TO 50
C GRAVITY ELEMENT.
171 CALL GRAVTY (XYZ,JDOF,EUL,NUTEL,NJ,
*           NUTKX,
*           W1,W2,W3,KRX,KRJ,KRE,KW)
GO TO 50
C
C TERMINATE FINITE ELEMENT DATA ON STORAGE DISKS.
500 IF (NUTMX .GT. 0) WRITE (NUTMX) IBLANK, (11,I=1,30)
IF (NUTKX .GT. 0) WRITE (NUTKX) IBLANK, (11,I=1,30)
IF (NUTB .GT. 0) WRITE (NUTB) IBLANK, (11,I=1,30)
IF (NUTLT .GT. 0) WRITE (NUTLT) IBLANK, (11,I=1,30)
IF (NUTST .GT. 0) WRITE (NUTST) IBLANK, (11,I=1,30)
C
C SUM FINITE ELEMENT MATRICES.
IF (NUTM.GT.0) CALL YZERO (NUTM,NDOF,NDOF)
IF (NUTK.GT.0) CALL YZERO (NUTK,NDOF,NDOF)

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```
IF (NUTMX .GT. 0) CALL YRVAD2 (NUTMX,NUTM,NDOF,W1,KW,V,LV,KV,  
* NUT1,NUT2,NUT3)  
IF (NUTKX .GT. 0) CALL YRVAD2 (NUTKX,NUTK,NDOF,W1,KW,V,LV,KV,  
* NUT1,NUT2,NUT3)  
RETURN
```

```
C  
999 CALL ZZBOMB (6HFINEL ,NERRGR)  
END
```

```

SUBROUTINE FLUID (XYZ,JDOF,EUL,NUTEL,NJ,
*   NUTMX,NUTKX,      NUTLT,NUTST,
*   W, T, S, KX, KJ, KE, KW)
DIMENSION XYZ(KX,1),JDOF(KJ,1), EUL(KE,1), W(KW,1),
*   T(KW,1), S(KW,1)
DIMENSION CJ(3,8),EJ(3,8),IV1(24),IVTET(12),JM(4,16),VL(10),
*   DV(12),DIST(12,12),TV(24)
DATA NRW,NRST/24,1/, IBLNK/6H      /,J1ST /0/
DATA NIT,NOT/ 5,6 /
DATA NAMEL / 6HFLUID /
DATA KCJ / 3 /,KJM / 4 /
DATA KDIST / 12 / , IFBAD / 1 /
DATA JM/1,2,3,4, 3,6,4,2, 2,6,4,5, 3,5,1,2,
*   1,3,6,5, 1,6,4,5, 2,7,4,5, 1,2,4,5,
*   4,7,8,5, 5,2,7,6, 4,2,3,7, 1,3,8,6,
*   1,6,8,5, 1,3,4,8, 1,2,3,6, 8,3,7,6 /

C
C SUBROUTINE TO CALCULATE (ON OPTION) FINITE ELEMENT ...
C MASS MATRICES AND IVECS (ON NUTMX),
C STIFFNESS MATRICES (SAME AS GLOBAL LOAD TRANSFORMATION MATRICES)
C AND IVECS (ON NUTKX),
C PRESSURE TRANSFORMATION MATRICES AND IVECS (ON NUTST),
C FOR FLUID ELEMENTS.
C ELEMENT SHAPE MAY BE TETRAHEDRON, PENTAHEDRON, OR HEXAHEDRON.
C MASS, STIFFNESS MATRICES ARE IN GLOBAL COORDINATE DIRECTIONS.
C GLOBAL COORDINATE ORDER IS
C (U,V,W) JOINT 1, THEN JOINT 2,3,4,(5,6,7,8).
C WHERE U,V,W ARE TRANSLATIONS.
C IVEC GIVES ELEMENT DOF INTO GLOBAL DOF. EXAMPLES...
C IVEC(6)=834 PLACES ELEMENT DOF 6 INTO GLOBAL DOF 834.
C IVEC(3)=0 OMTS ELEMENT DOF 3 FROM GLOBAL DOF. THIS CONSTRAINS
C ELEMENT DOF 3 TO ZERO MOTION.
C PRESSURE TRANSFORMATION MATRICES RELATE CHANGE IN PRESSURE (DUE TO
C COMPRESSIBILITY) TO DEFLECTIONS IN THE GLOBAL COORDINATE DIRECTIONS.
C PRESSURE CHANGE WITHIN THE FLUID ELEMENT IS CONSTANT. STATIC PRESSURE
C DUE TO GRAVITY AND FLUID HEIGHT IS NOT INCLUDED.
C DATA ARRANGEMENT ON NUTMX, NUTKX, NUTST FOR EACH FINITE ELEMENT IS
C (W=M,K,ST)
C WRITE (NUTWX) NAMEW,NEL,NP,NC,NAMEL,(IBLNK,I=1,5),
C ((W(I,J),I=1,NR),J=1,NC),(IVEC(I),I=1,NC)
C CALLS FORMA SUBROUTINES TEGEOM,VCROSS,VDOT ,ZZBOMB.
C DEVELOPED BY C S BODLEY. FEBRUARY 1974.
C LAST REVISION BY WA BENFIELD. MARCH 1976.
C
C INPUT DATA READ IN THIS SUBROUTINE FROM NUTEL. IF NUTEL = NIT, DATA IS
C READ FROM CARDS.
C NAMEM,NAMEK,NAMELT,NAMEST          FORMAT (4(A6,4X)
C RC,EKM                             FOPMAT (2(5X,E10))
C 20 NEL,J1,J2,J3,J4,J5,J6,J7,J8    FORMAT (9I5)
C IF (J1 .EQ. 0) RETURN
C GO TO 20
C
C DEFINITION OF INPUT VARIABLES.
C NAMEM = TYPE OF MASS MATRIX WANTED.
C = M1, LUMPED MASS MATRIX.

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C = M2, QUASI-IRROTATIONAL CONSISTENT MASS MATRIX.  
 C = M3, IRROTATIONAL MASS MATRIX.  
 C = 6H OR 6HNO MASS, NO MASS MATRIX CALCULATED.  
 C NAMEK = TYPE OF STIFFNESS MATRIX WANTED.  
 C = K1, LINEAR DISPLACEMENT ASSUMED.  
 C = 6H OR 6HNO STIF, NO STIFFNESS MATRIX CALCULATED.  
 C NAMELT = IDENTIFICATION NAME FOR LOAD TRANSFORMATION MATRICES. (NOT YET).  
 C NAMEST = IDENTIFICATION NAME FOR PRESSURE TRANSFORMATION MATRICES.  
 C = 6H OR 6HNO STRS, NO PRESSURE TRANSFORMATIONS CALCULATED.  
 C RO = MASS DENSITY.  
 C BKM = BULK MODULUS.  
 C NEL = FINITE ELEMENT NUMBER. FOR REFERENCE ONLY, NOT USED IN  
 C CALCULATIONS. WRITTEN ON NUTMX, ETC.  
 C J1 = JOINT NUMBER AT ELEMENT VERTEX 1.  
 C J2 = JOINT NUMBER AT ELEMENT VERTEX 2.  
 C J3 = JOINT NUMBER AT ELEMENT VERTEX 3.  
 C J4 = JOINT NUMBER AT ELEMENT VERTEX 4.  
 C FOR A TETRAHEDRON. FACE 1,2,3 MUST BE NUMBERED CLOCKWISE AS  
 C VIEWED FROM OUTSIDE THE ELEMENT.  
 C J5 = JOINT NUMBER AT ELEMENT VERTEX 5. (USED FOR PENTAHEDRON AND  
 C HEXAHEDRON).  
 C J6 = JOINT NUMBER AT ELEMENT VERTEX 6. (USED FOR PENTAHEDRON AND  
 C HEXAHEDRON).  
 C FOR A PENTAHEDRON, FACE 1,2,3 MUST BE NUMBERED CLOCKWISE AS  
 C VIEWED FROM OUTSIDE THE ELEMENT. FACE 4,5,6 IS NUMBERED IN  
 C THE SAME ORDER AS FACE 1,2,3. A LINE JOINING JOINTS 1 AND 4  
 C MUST FORM AN EDGE OF THE PENTAHEDRON.  
 C J7 = JOINT NUMBER AT ELEMENT VERTEX 7. (USED FOR HEXAHEDRON).  
 C J8 = JOINT NUMBER AT ELEMENT VERTEX 8. (USED FOR HEXAHEDRON).  
 C FOR A HEXAHEDRON, FACE 1,2,3,4 MUST BE NUMBERED CLOCKWISE  
 C AS VIEWED FROM OUTSIDE THE ELEMENT. FACE 5,6,7,8 IS NUMBERED  
 C IN THE SAME ORDER AS FACE 1,2,3,4. A LINE JOINING JOINTS 1  
 C AND 5 MUST FORM AN EDGE OF THE HEXAHEDRON.  
 C  
 C EXPLANATION OF INPUT FORMATS. NUMBER INDICATES CARD COLUMNS USED.  
 C I = INTEGER DATA, RIGHT ADJUSTED.  
 C E = DECIMAL POINT DATA, ANYWHERE IN FIELD. EXPONENT RIGHT ADJUSTED.  
 C X = CARD COLUMNS SKIPPED.  
 C  
 C SUBROUTINE ARGUMENTS (ALL INPUT)  
 C XYZ = MATRIX OF JOINT GLOBAL X,Y,Z LOCATIONS. ROWS CORRESPOND  
 C TO JOINT NUMBERS. COLUMNS 1,2,3 CORRESPOND TO THE JOINT  
 C X,Y,Z LOCATIONS RESPECTIVELY. SIZE(NJ,3).  
 C JDOF = MATRIX OF JOINT GLOBAL DEGREES OF FREEDOM. ROWS CORRESPOND  
 C TO JOINT NUMBERS. COLUMNS 1,2,3 CORRESPOND TO THE JOINT  
 C TRANSLATION DOFS AND COLUMNS 4,5,6 CORRESPOND TO THE JOINT  
 C ROTATION DOFS. SIZE(NJ,6).  
 C EUL = MATRIX OF JOINT EULER ANGLES (DEGREES). ROWS CORRESPOND  
 C TO JOINT NUMBERS. COLUMNS 1,2,3 CORRESPOND TO THE  
 C GLOBAL X,Y,Z PERMUTATION. SIZE(NJ,3).  
 C NUTEL = LOGICAL NUMBER OF TAPE CONTAINING ELEMENT INPUT DATA FOR  
 C THIS SUBROUTINE. IF NUTEL = NIT, DATA IS READ FROM CARDS.  
 C NJ = NUMBER OF JOINTS OR ROWS IN MATRICES (XYZ), (JDOF), (EUL).  
 C NUTMX = LOGICAL NUMBER OF UTILITY TAPE ON WHICH ELEMENT  
 C MASS MATRICES AND IVECS ARE OUTPUT.

```

C          NUTMX MAY BE ZERO IF MASS MATRIX IS NOT FORMED.
C          USES FORTRAN READ, WRITE.
C  NUTKX  = LOGICAL NUMBER OF UTILITY TAPE ON WHICH ELEMENT
C          STIFFNESS MATRICES (SAME AS GLOBAL LOADS TRANSFORMATION
C          MATRICES) AND IVECS ARE OUTPUT.
C          NUTKX MAY BE ZERO IF STIFFNESS MATRIX IS NOT FORMED.
C          USES FORTRAN READ, WRITE.
C  NUTLT  = LOGICAL NUMBER OF UTILITY TAPE ON WHICH ELEMENT LOAD
C          TRANSFORMATION MATRICES AND IVECS ARE OUTPUT. (NOT YET).
C  NUTST  = LOGICAL NUMBER OF UTILITY TAPE ON WHICH ELEMENT
C          PRESSURE TRANSFORMATION MATRICES AND IVECS ARE OUTPUT.
C          NUTST MAY BE ZERO IF PRESSURE TRANSFORMATIONS ARE NOT FORMED.
C          USES FORTRAN READ, WRITE.
C  W      = MATRIX WORK SPACE. MIN SIZE(24,24).
C  T      = MATRIX WORK SPACE. MIN SIZE(24,24).
C  S      = MATRIX WORK SPACE. MIN SIZE(24,24).
C  KX     = ROW DIMENSION OF XYZ IN CALLING PROGRAM.
C  KJ     = ROW DIMENSION OF JDOF IN CALLING PROGRAM.
C  KE     = ROW DIMENSION OF EUL IN CALLING PROGRAM.
C  KW     = ROW DIMENSION OF W, T, AND S IN CALLING PROGRAM. MIN=24.
C
C  ERROR EXPLANATION
C  1 = INCORRECT TETRAHEDRON GEOMETRY.
C  2 = INPUT JOINT NUMBER EXCEEDS MAXIMUM ALLOWABLE NUMBER OF JOINTS.
C  3 = NUTMX NOT POSITIVE.
C  4 = NUTKX NOT POSITIVE.
C  5 = NUTST NOT POSITIVE.
C
1001 FORMAT (5(A6,4X))
1002 FORMAT (3(5X,E10.0))
1003 FORMAT (9I5)
2001 FORMAT (/25X 38HINPUT DATA FOR FLUID (TETRA, PENTA, OR
* 21H HEXAHEDRON) ELEMENTS)
2002 FORMAT (/20X 38HINPUT DATA FOR FLUID (TETRA, PENTA, OR
* 33H HEXAHEDRON) ELEMENTS (CONTINUED))
2003 FORMAT (/12X7HMASS = A6,13X7HSTIF = A6,6X13HLOAD TRANS = A6,
* 3X15HSTRESS TRANS = A6, 3X
* / 15X,4HRC = E10.3, 13X7HBULKM = E10.3,
* // 9X7HELEMENT 6 HJOINT 1 6X7HJOINT 2 6X7HJOINT 3 6X7HJOINT 4
* 6X7HJOINT 5 6X7HJOINT 6 6X7HJOINT 7 6X7HJOINT 8
* / 9X6HNUMBER)
2004 FORMAT (3X,9(8X,15))
3001 FORMAT (51H * * * * * UNCONVENTIONAL JOINT NUMBERING * * * * * , /
* 9I5)
C
C
IF (IIST .EQ. 1) GO TO 3
IIST = 1
DO 4 I=1,4
I1 = 3*I - 2
DO 4 J=1,4
J1 = 3*J - 2
4 CALL UNITY (DIST(I1,J1),3,KDIST)
C
3 NLINE = 0

```



```

CALL PAGEHD
WRITE (NOT,2001)
READ (NUTEL,1001) NAMEM,NAMEK,NAMELT,NAMEST
READ (NUTEL,1002) RO, BKM
WRITE (NOT,2003) NAMEM,NAMEK,NAMELT,NAMEST,
*      RO, BKM
IF (NAMEM .NE. 6HM3 ) GO TO 20
DO 2 I=1,12
2 DIST(I,I) = 2.
C
20 READ (NUTEL,1003) NEL,J1,J2,J3,J4,J5,J6,J7,J8
NERROR=1
IF (J1.LE.0 .AND. IFRAD.EQ.-1) GO TO 999
IF (J1 .LE. 0) RETURN
NLINE = NLINE + 1
IF (NLINE .LE. 42) GO TO 30
CALL PAGEHD
WRITE (NOT,2002)
WRITE (NOT,2003) NAMEM,NAMEK,NAMELT,NAMEST,
*      RO, BKM
NLINE = 0
30 WRITE (NOT,2004) NEL,J1,J2,J3,J4,J5,J6,J7,J8
NERROR=2
IF (J1.GT.NJ .OR. J2.GT.NJ .OR. J3.GT.NJ .OR. J4.GT.NJ) GO TO 999
IF (J5.GT.NJ .OR. J6.GT.NJ .OR. J7.GT.NJ .OR. J8.GT.NJ) GO TO 999
C
C FORM FINITE ELEMENT COORDINATE LOCATIONS,EULER ANGLES, REVADD IVEC.
C
LR = 10
NJN = 8
IF (J7 .NE. 0) GO TO 38
LR = 6
NJN = 6
IF (J5 .NE. 0) GO TO 38
LR = 1
NJN = 4
C
38 NCCL = 3*NJN
DO 5 I=1,NCCL
DO 5 J=1,NCCL
W(I,J) = 0.
S(I,J) = 0.
5 T(I,J) = 0.
C
DO 40 I=1,3
CJ(I,1) = XYZ(J1,I)
CJ(I,2) = XYZ(J2,I)
CJ(I,3) = XYZ(J3,I)
CJ(I,4) = XYZ(J4,I)
EJ(I,1) = EUL(J1,I)
EJ(I,2) = EUL(J2,I)
EJ(I,3) = EUL(J3,I)
EJ(I,4) = EUL(J4,I)
IV1(I) = JDOF(J1,I)
IV1(I+3) = JDOF(J2,I)

```

```

IV1(I+6) = JDOF(J3,I)
40 IV1(I+9) = JDOF(J4,I)
   IF (LR .EQ. 1) GO TO 50
C
   DO 42 I=1,3
   CJ(I,5) = XYZ(J5,I)
   CJ(I,6) = XYZ(J6,I)
   EJ(I,5) = EUL(J5,I)
   EJ(I,6) = EUL(J6,I)
   IV1(I+12) = JDOF(J5,I)
42 IV1(I+15) = JDOF(J6,I)
   IF (LR .EQ. 6) GO TO 50
C
   DO 44 I=1,3
   CJ(I,7) = XYZ(J7,I)
   CJ(I,8) = XYZ(J8,I)
   EJ(I,7) = EUL(J7,I)
   EJ(I,8) = EUL(J8,I)
   IV1(I+18) = JDOF(J7,I)
44 IV1(I+21) = JDOF(J8,I)
C
50 DO 52 L=1,LR
   LA = L
   IF (LR.EQ.10) LA=L+6
   DO 52 I=1,4
   JNO = JM(I,LA)
   LI = 3*I - 2
   IVTET(LI ) = 3*JNO - 2
   IVTET(LI+1) = 3*JNO - 1
53 IVTET(LI+2) = 3*JNO
C
   CALL TEGEOM (CJ,JM(1,LA ),VL(L),DV,      KCJ,IFEAD)
   IF (IFBAD.NE.0) GO TO 51
   WRITE (NOI,3001) NEL,J1,J2,J3,J4,J5,J6,J7,J8
   IFBAD = -1
51 SM = RO*VL(L)/16.0
   IF (NAMEM .EQ. 6HMB ) SM=RO*VL(L)/20.0
   IF (LR .GT. 1) SM = SM/2.
   CALL REVADD (1.,DV,L,IVTET,T,?,12,LR,NCOL,1,KW)
52 CALL REVADD (SM,DIST,IVTET,IVTET,W,12,12,NCOL,NCOL,KDIST,KW)
C
   IF (NAMEM .NE. 6HMI ) GO TO 220
   DO 210 I=1,NCOL
   SAVE = 0.0
   DO 215 J=1,NCOL
   SAVE = SAVE + W(I,J)
215 W(I,J) = 0.0
210 W(I,I) = SAVE
C
220 IF (LR .EQ. 1) GO TO 60
   DO 55 I=2,LR
   VL(I) = VL(I) + VL(I)
   DO 55 J=1,NCOL
55 T(I,J) = T(I,J) + T(I,J)
   VL(I) = VL(I)/2.

```

```

      DO 56 J=1,NCOL
56  T(1,J) = T(1,J)/2.
C
60  DO 61 J=1,NCOL
61  TV(J) = T(1,J)
      DO 65 J=1,NJN
          J1 = 3*J - 2
65  CALL EULER (EJ(1,J),S(J1,J1),KW)
      IF (NAMEST .EQ. 6H .OR. NAMEST .EQ. 6HNOSTRS) GO TO 90
      CALL PRESS (CJ,T,NJN,NCOL,KCJ,KW)
      CALL MULTA (T,S,NJN,NCOL,NCOL,KW,KW)
90  CALL BTAPA (W,S,NCOL,NCOL,KW,KW)
      CALL MULTA (TV,S,1,NCOL,NCOL,1,KW)
      BOV = BKM/VL(1)
      DO 70 I=1,NCOL
      DO 70 J=1,NCOL
          S(I,J) = BOV*TV(I)*TV(J)
70  S(J,I) = S(I,J)
C
      IF (NAMEM .EQ. 6H .OR. NAMEM .EQ. 6HNOMASS) GO TO 110
                                                    NERROR=3
      IF (NUTMX .LE. 0) GO TO 999
      WRITE (NUTMX) NAMEM,NEL,NCOL,NCOL,NAMEL,(IBLNK,I=1,5),
*      ((W(I,J),I=1,NCOL),J=1,NCOL), (IV1(I),I=1,NCOL)
C
110 IF (NAMEK .EQ. 6H .OR. NAMEK .EQ. 6HNOSTIF) GO TO 120
                                                    NERROR=4
      IF (NUTKX .LE. 0) GO TO 999
      WRITE (NUTKX) NAMEK,NEL,NCOL,NCOL,NAMEL,(IBLNK,I=1,5),
*      ((S(I,J),I=1,NCOL),J=1,NCOL), (IV1(I),I=1,NCOL)
C
120 IF (NAMEST .EQ. 6H .OR. NAMEST .EQ. 6HNOSTRS) GO TO 20
                                                    NERROR=5
      IF (NUTST .LE. 0) GO TO 999
      NJNPI = NJN + 1
      CALL MULT (T,S,T(NJNPI,1),NJN,NCOL,NCOL,KW,KW)
      CALL MULTA (T,W,NJN,NCOL,NCOL,KW,KW)
      NRST = 2*NJN
      WRITE (NUTST) NAMEST,NEL,NRST,NCOL,NAMEL,VL(1),(YBLNK,I=1,4),
*      ((T(I,J),I=1,NRST),J=1,NCOL), (IV1(I),I=1,NCOL)
      GO TO 20
C
999 CALL ZZBOMB (6HFLUID ,NERROR)
      END

```

```

SUBROUTINE GRAVITY (XYZ,JDOF,EUL,NUTEL,NJ,
*      NUTKX,
*      W, T, S, KX, KJ, KE, KW)
DIMENSION XYZ(KX,1),JDOF(KJ,1), EUL(KE,1), W(KW,1),
*      (KW,1), S(KW,1)
DIMENSION CJ(3,4),EJ(3,4),IV1(12),IVTRI(9),JM(3,4),GV(3),EV(3)
DATA IBLNK/6H /
DATA NIT,NOT/ 5,6 /
DATA NAMEL / 6HGRAVITY /
DATA KCJM / 3 /
DATA JM / 1,2,3, 1,3,4, 1,2,4, 4,2,3 /

C
C SUBROUTINE TO CALCULATE (ON OPTION) FINITE ELEMENT ...
C STIFFNESS MATRICES (SAME AS GLOBAL LOAD TRANSFORMATION MATRICES)
C AND IVECS (ON NUTKX),
C FOR GRAVITY ELEMENTS.
C STIFFNESS MATRICES ARE 9- GLO21- 300R49-1T 4IR 090-58
C GLOBAL COORDINATE ORDER IS
C (U,V,W) JOINT 1, THEN JOINT 2,3,(4).
C WHERE U,V,W ARE TRANSLATIONS.
C IVEC GIVES ELEMENT DOF INTO GLOBAL DOF. EXAMPLES...
C IVEC(6)=834 PLACES ELEMENT DOF 6 INTO GLOBAL DOF 834.
C IVEC(3)=0 OMMITS ELEMENT DOF 3 FROM GLOBAL DOF. THIS CONSTRAINS
C ELEMENT DOF 3 TO ZERO MOTION.
C DATA ARRANGEMENT ON NUTKX FOR EACH FINITE ELEMENT IS
C (W=K)
C WRITE (NUTWX) NAMEW,NEL,NR,NC,NAMEL,(IBLNK,I=1,5),
C ((W(I,J),I=1,NR),J=1,NC),(IVEC(I),I=1,NC)
C CALLS FORMA SUBROUTINES KGRAV ,MULTA ,MULTE ,VCROSS,ZZBOMB.
C DEVELOPED BY C S BODLEY. FEBRUARY 1974.
C LAST REVISION BY WA BENFIELD. MARCH 1976.
C
C *****
C INPUT DATA READ IN THIS SUBROUTINE FROM NUTEL. IF NUTEL = NIT, DATA IS
C READ FROM CARDS.
C NAMEM,NAMEK          FORMAT (2(A6,4X)
C RO                   FORMAT (5X,E10)
C (GV(I),I=1,3)        FORMAT (3(5X,E10))
C 20 NEL,J1,J2,J3,J4   FORMAT (5I5)
C IF (J1 .EQ. 0) RETURN
C GO TO 20
C
C DEFINITION OF INPUT VARIABLES.
C NAMEM = TYPE OF MASS MATRIX WANTED.
C        = 6H          OR 6HNO MASS, NO MASS MATRIX CALCULATED.
C NAMEK = TYPE OF STIFFNESS MATRIX WANTED.
C        = K1, LINEAR DISPLACEMENT ASSUMED.
C        = 6H          OR 6HNO STIF, NO STIFFNESS MATRIX CALCULATED.
C RO    = MASS DENSITY.
C GV    = GRAVITY VECTOR.
C NEL   = FINITE ELEMENT NUMBER. FOR REFERENCE ONLY, NOT USED IN
C        CALCULATIONS. WRITTEN ON NUTKX.
C J1    = JOINT NUMBER AT ELEMENT VERTEX 1.
C J2    = JOINT NUMBER AT ELEMENT VERTEX 2.
C J3    = JOINT NUMBER AT ELEMENT VERTEX 3.

```

C J4 = JOINT NUMBER AT ELEMENT VERTEX 4. (USED FOR QUADRILATERAL).  
 C THE ELEMENT MUST BE NUMBERED CLOCKWISE AS VIEWED FROM THE FLUID SIDE  
 C OF THE ELEMENT.

C  
 C EXPLANATION OF INPUT FORMATS. NUMBER INDICATES CARD COLUMNS USED.  
 C I = INTEGER DATA, RIGHT ADJUSTED.  
 C E = DECIMAL POINT DATA, ANYWHERE IN FIELD. EXPONENT RIGHT ADJUSTED.  
 C X = CARD COLUMNS SKIPPED.

C \*\*\*\*\*

C  
 C SUBROUTINE ARGUMENTS (ALL INPUT)  
 C XYZ = MATRIX OF JOINT GLOBAL X,Y,Z LOCATIONS. ROWS CORRESPOND  
 C TO JOINT NUMBERS. COLUMNS 1,2,3 CORRESPOND TO THE JOINT  
 C X,Y,Z LOCATIONS RESPECTIVELY. SIZE(NJ,3).  
 C JDOF = MATRIX OF JOINT GLOBAL DEGREES OF FREEDOM. ROWS CORRESPOND  
 C TO JOINT NUMBERS. COLUMNS 1,2,3 CORRESPOND TO THE JOINT  
 C TRANSLATION DOFS AND COLUMNS 4,5,6 CORRESPOND TO THE JOINT  
 C ROTATION DOFS. SIZE(NJ,6).  
 C EUL = MATRIX OF JOINT EULER ANGLES (DEGREES). ROWS CORRESPOND  
 C TO JOINT NUMBERS. COLUMNS 1,2,3 CORRESPOND TO THE  
 C GLOBAL X,Y,Z PERMUTATION. SIZE(NJ,3).  
 C NUTEL = LOGICAL NUMBER OF TAPE CONTAINING ELEMENT INPUT DATA FOR  
 C THIS SUBROUTINE. IF NUTEL = NIT, DATA IS READ FROM CARDS.  
 C NJ = NUMBER OF JOINTS OR ROWS IN MATRICES (XYZ), (JDOF), (EUL).  
 C NUTKX = LOGICAL NUMBER OF UTILITY TAPE ON WHICH ELEMENT  
 C STIFFNESS MATRICES (SAME AS GLOBAL LOADS TRANSFORMATION  
 C MATRICES) AND IVECS ARE OUTPUT.  
 C NUTKX MAY BE ZERO IF STIFFNESS MATRIX IS NOT FORMED.  
 C USES FORTRAN READ, WRITE.  
 C W = MATRIX WORK SPACE. MIN SIZE(12,12).  
 C T = MATRIX WORK SPACE. MIN SIZE(12,12).  
 C S = MATRIX WORK SPACE. MIN SIZE(12,12).  
 C KX = ROW DIMENSION OF XYZ IN CALLING PROGRAM.  
 C KJ = ROW DIMENSION OF JDOF IN CALLING PROGRAM.  
 C KE = ROW DIMENSION OF EUL IN CALLING PROGRAM.  
 C KW = ROW DIMENSION OF W, T, AND S IN CALLING PROGRAM. MIN=12.

C  
 C NERROR EXPLANATION  
 C 1 = INPUT JOINT NUMBER EXCEEDS MAXIMUM ALLOWABLE NUMBER OF JOINTS.  
 C 2 = NUTKX NOT POSITIVE.

C  
 C 1001 FORMAT (5(A6,4X))  
 C 1002 FORMAT (3(5X,E10.0))  
 C 1003 FORMAT (5I5)  
 C 2001 FORMAT (//25X 45HINPUT DATA FOR GRAVITY STIFFNESS (TRIANGLE OR  
 C \* 24H QUADRILATERAL) ELEMENTS)  
 C 2002 FORMAT (//20X 45HINPUT DATA FOR GRAVITY STIFFNESS (TRIANGLE OR  
 C \* 36H QUADRILATERAL) ELEMENTS (CONTINUED))  
 C 2003 FORMAT (//12X7HMASS = A6,13X7HSTIF = A6,6X  
 C \* / 15X,4HRG = E10.3, 13X5HGVX = E10.3, 13X5HGVY = E10.3,  
 C \* 13X5HGVZ = E10.3,  
 C \* //15X7HELEMENT 13X7HJOINT 1 13X7HJOINT 2 13X7HJOINT 3  
 C \* 13X7HJOINT 4  
 C \* /15X6HNUMBER)  
 C 2004 FORMAT (18X,9(I5,15X))

```

C
C
NLINE = 0
CALL PAGEHD
WRITE (NOT,2001)
READ (NUTEL,1001) NAMEM,NAMEK
READ (NUTEL,1002) RO
READ (NUTEL,1002) (GV(I),I=1,3)
WRITE (NOT,2003) NAMEM,NAMEK,
*      RO, (GV(I),I=1,3)
C
.20 READ (NUTEL,1003) NEL,J1,J2,J3,J4
IF (J1 .LE. 0) RETURN
NLINE = NLINE + 1
IF (NLINE .LE. 42) GO TO 30
CALL PAGEHD
WRITE (NOT,2002)
WRITE (NOT,2003) NAMEM,NAMEK,
*      RO, (GV(I),I=1,3)
NLINE = 0
30 WRITE (NOT,2004) NEL,J1,J2,J3,J4
                                                    NERROR=1
IF (J1.GT.NJ .OR. J2.GT.NJ .OR. J3.GT.NJ .OR. J4.GT.NJ) GO TO 999
C
C FORM FINITE ELEMENT COORDINATE LOCATIONS,EULER ANGLES, REVADD IVEC.
C
LP = 4
NJN = 4
IF (J4 .NE. 0) GO TO 38
LP = 1
NJN = 3
38 NCOL = 3*NJN
DO 5 I=1,NCOL
DO 5 J=1,NCOL
W(I,J) = 0.
S(I,J) = 0.
5 T(I,J) = 0.
C
DO 40 I=1,3
CJ(I,1) = XYZ(J1,I)
CJ(I,2) = XYZ(J2,I)
CJ(I,3) = XYZ(J3,I)
EJ(I,1) = EUL(J1,I)
EJ(I,2) = EUL(J2,I)
EJ(I,3) = EUL(J3,I)
IV1(I ) = JDOF(J1,I)
IV1(I+3) = JDOF(J2,I)
40 IV1(I+6) = JDOF(J3,I)
IF (LP .EQ. 1) GO TO 50
C
DO 42 I=1,3
CJ(I,4) = XYZ(J4,I)
EJ(I,4) = EUL(J4,I)
42 IV1(I+9) = JDOF(J4,I)
C

```

```

50 G = SQRT(GV(1)**2 + GV(2)**2 + GV(3)**2)
DO 51 I=1,3
51 EV(I) = -GV(I)/G
DO 52 L=1,LR
CALL KGRAV (CJ,JM(1,L),EV,A,W,KW,KCJM)

```

C

```

DO 53 I=1,3
JNO = JM(I,L)
L1 = 3*I - 2
IVTRI(L1 ) = 3*JNO - 2
IVTRI(L1+1) = 3*JNO - 1
53 IVTRI(L1+2) = 3*JNO
SS = RO*G*A/24.
IF (LR .GT. 1) SS = SS/2.
52 CALL REVADD (SS,W,IVTRI,IVTRI,S,9,9,NCOL,NCOL,KW,KW)

```

C

```

DO 65 J=1,NJN
J1 = 3*J - 2
65 CALL EULEP (EJ(1,J),T(J1,J1),KW)
CALL BTABA (S,T,NCOL,NCOL,KW,KW)

```

C

```

IF (NAMEK .EQ. 6H .CR. NAMEK .EQ. 6HNOSTIF) GO TO 20
NERRCR=2
IF (NUTKY .LE. 0) GO TO 999
WRITE (NUTKX) NAMEK,NEL,NCOL,NCOL,NAMEL,(IBLNK,I=1,5),
* ((S(I,J),I=1,NCOL),J=1,NCOL), (IV(I),I=1,NCOL)

```

C

```

GO TO 20

```

C

```

999 CALL ZZBOMB (6HGRAVITY,NERRCR)
END

```

K1A1

SUBROUTINE K1A1 (A1,A2,RL,E,Z,TS,KZ,KTS)  
DIMENSION Z(KZ,1), TS(KTS,1)

C  
C SUBROUTINE TO CALCULATE FINITE ELEMENT...  
C STIFFNESS MATRIX,  
C STRESS TRANSFORMATION MATRIX,  
C FOR AN AXIAL ROD ELEMENT WITH UNRESTRAINED BOUNDARIES.  
C ROD MAY BE LINEARLY TAPERED OR UNIFORM.  
C CONSTANT FORCE ASSUMED.  
C STIFFNESS MATRIX IS IN LOCAL COORDINATE SYSTEM.  
C STRESS TRANSFORMATION MATRIX RELATES STRESS AT ROD ENDS IN LOCAL  
C COORDINATE SYSTEM TO DEFLECTIONS IN LOCAL COORDINATE SYSTEM.  
C ROW ORDER IN STRESS TRANSFORMATION MATRIX IS  
C SIGMA-X1, SIGMA-X2  
C WHERE SIGMA IS NORMAL STRESS.  
C SX1(-), SX2(+) IS TENSION. SX1(+), SX2(-) IS COMPRESSION.  
C THE LOCAL COORDINATE SYSTEM ASSUMES THE ROD TO LIE ALONG THE X AXIS  
C WITH JOINT 1 AT THE ORIGIN, JOINT 2 ALONG THE POSITIVE X AXIS.  
C LOCAL COORDINATE ORDER IS  
C DX1,DX2  
C WHERE DX IS TRANSLATION.  
C DEVELOPED BY RL WOHLFN. SEPTEMBER 1972.  
C LAST REVISION BY RL WOHLFN. SEPTEMBER 1973.  
C  
C SUBROUTINE ARGUMENTS  
C A1 = INPUT CROSS-SECTION AREA AT ROD END 1.  
C A2 = INPUT CROSS-SECTION AREA AT ROD END 2.  
C RL = INPUT ROD LENGTH.  
C E = INPUT YOUNGS MODULUS OF ELASTICITY.  
C Z = OUTPUT STIFFNESS MATRIX. SIZE(2,2).  
C TS = OUTPUT STRESS TRANSFORMATION MATRIX. SIZE(2,2).  
C KZ = INPUT ROW DIMENSION OF Z IN CALLING PROGRAM. MIN=2.  
C KTS = INPUT ROW DIMENSION OF TS IN CALLING PROGRAM. MIN=2.  
C  
C S = A1\*E/RL  
C R = A2/A1  
C IF (ABS(R-1.) .GT. .01) S = (A2-A1)\*E / (RL\*ALOG(R))  
C STIFFNESS MATRIX.  
C Z(1,1) = S  
C Z(1,2) = -S  
C Z(2,1) = -S  
C Z(2,2) = S  
C  
C STRESS TRANSFORMATION MATRIX.  
C TS(1,1) = Z(1,1)/A1  
C TS(1,2) = Z(1,2)/A1  
C TS(2,1) = Z(2,1)/A2  
C TS(2,2) = Z(2,2)/A2  
C  
C RETURN  
C END



```

SUBROUTINE K1B1 (B11,B12,C1,C2,A1,A2,SF,RL,E,G,Z,TS,KZ,KTS)
DIMENSION Z(KZ,1), TS(KTS,1)
DATA EPS/1.E-15/

C
C SUBROUTINE TO CALCULATE FINITE ELEMENT...
C STIFFNESS MATRIX,
C STRESS TRANSFORMATION MATRIX,
C FOR A BENDING (PLUS SHEAR) BEAM ELEMENT WITH UNRESTRAINED BOUNDARIES.
C BEAM MAY BE LINEARLY TAPERED OR UNIFORM.
C UNIFORM SHEAR AND LINEAR BENDING MOMENT VARIATION IS ASSUMED.
C SHEAR STIFFNESS USES SF*A1*G AND SF*A2*G. IF ANY OF THESE VARIABLES
C ARE ZERO, THERE IS NO SHEAR DEFORMATION IN BENDING.
C STIFFNESS MATRIX IS IN LOCAL COORDINATE SYSTEM.
C STRESS TRANSFORMATION MATRIX RELATES STRESS AT BEAM ENDS IN LOCAL
C COORDINATE SYSTEM TO DEFLECTIONS IN LOCAL COORDINATE SYSTEM.
C ROW ORDER IN STRESS TRANSFORMATION MATRIX IS
C TAU-X1,TAU-X2,SIGMA-X1,SIGMA-X2
C WHERE SIGMA IS NORMAL STRESS (MC/I) AND TAU IS SHEAR STRESS (P/A).
C THE LOCAL COORDINATE SYSTEM ASSUMES THE BEAM TO LIE IN THE X-Z PLANE
C WITH JOINT 1 AT THE ORIGIN, JOINT 2 ALONG THE POSITIVE X AXIS.
C LOCAL COORDINATE ORDER IS
C DZ1,DZ2,TY1,TY2
C WHERE DZ IS TRANSLATION AND TY IS ROTATION.
C DEVELOPED BY RL WOHLER. FEBRUARY 1973.
C LAST REVISION BY RL WOHLER. APRIL 1976.
C
C SUBROUTINE ARGUMENTS
C B11 = INPUT CROSS-SECTION AREA MOMENT OF INERTIA AT BEAM END 1.
C B12 = INPUT SAME AS B11 AT BEAM END 2.
C C1 = INPUT DISTANCE FROM BENDING NEUTRAL AXIS TO OUTER FIBER
C AT BEAM END 1.
C C2 = INPUT SAME AS C1 AT BEAM END 2.
C A1 = INPUT CROSS-SECTION AREA AT BEAM END 1. CAN BE ZERO FOR NO
C SHEAR DEFORMATION IN BENDING. SHEAR STRESS IN STRESS
C TRANSFORMATION WILL BE SET TO ZERO.
C A2 = INPUT SAME AS A1 AT BEAM END 2.
C SF = INPUT SHAPE FACTOR (K) FOR SHEAR IN KAG.
C USE SF=0.0 FOR NO SHEAR DEFORMATION IN BENDING.
C SF=1.0 FOR A SOLID CIRCULAR CYLINDER.
C SF=.5 FOR A THIN WALLED CIRCULAR CYLINDER.
C RL = INPUT ROD LENGTH.
C E = INPUT YOUNGS MODULUS OF ELASTICITY.
C G = INPUT SHEAR MODULUS OF ELASTICITY. CAN BE ZERO FOR NO SHEAR
C DEFORMATION IN BENDING.
C Z = OUTPUT STIFFNESS MATRIX. SIZE(4,4).
C TS = OUTPUT STRESS TRANSFORMATION MATRIX. SIZE(4,4).
C KZ = INPUT ROW DIMENSION OF Z IN CALLING PROGRAM. MIN=4.
C KTS = INPUT ROW DIMENSION OF TS IN CALLING PROGRAM. MIN=4.
C
C BENDING FLEXIBILITY.
RPI = B12/B11
REIMI = RPI-1.
IF (ABS(REIMI) .LT. .01) GO TO 15
EPS = E*B11*RPI*REIMI
REILN = ALOG(RPI)

```

```

F11 = (.5 - 1./RBIM1 + RBILN/RBIM1**2) * (RL**3) / EBR
F12 = (1. - RBILN/RBIM1) * (RL**2) / EBR
F22 = RL* RBILN / EBR
GO TO 20
15 F11 = RL**3 / (3.*E*BII)
F12 = RL**2 / (2.*E*BII)
F22 = RL/ (E*BII)
C SHEAR FLEXIBILITY.
20 IF (SF.LT.EPS .OR. A1.LT.EPS .OR. A2.LT.EPS .OR. G.LT.EPS)GO TO 30
RA = A2/A1
IF (ABS(RA-1.) .LT. .01) GO TO 25
F11 = F11 + RL * ALOG(RA) / (SF*G*(A2-A1))
GO TO 30
25 F11 = F11 + RL/(SF*A1*G)
C
C BENDING + SHEAR STIFFNESS MATRIX.
30 D = F11*F22 - F12**2
Z(1,1) = F22/D
Z(1,2) = -Z(1,1)
Z(1,3) = -F12/D
Z(1,4) = (-RL*F22 + F12)/D
Z(2,2) = Z(1,1)
Z(2,3) = -Z(1,3)
Z(2,4) = -Z(1,4)
Z(3,3) = F11/D
Z(3,4) = (RL*F12 - F11)/D
Z(4,4) = (F22*RL**2 - 2.*RL*F12 + F11)/D
C SYMMETRIZE LOWER HALF.
DO 40 J=1,4
DO 40 I=J,4
40 Z(I,J) = Z(J,I)
C
C STRESS TRANSFORMATION MATRIX.
DO 55 J=1,4
TS(1,J) = 0.0
TS(2,J) = 0.0
IF (A1 .GT. 0.0) TS(1,J) = Z(1,J)/A1
IF (A2 .GT. 0.0) TS(2,J) = Z(2,J)/A2
TS(3,J) = Z(3,J)*C1/B11
55 TS(4,J) = Z(4,J)*C2/B12
C
RETURN
END

```

```

SUBROUTINE K1C1 (TJ1,TJ2,R1,R2,RL,G,Z,TS,KZ,KTS)
DIMENSION Z(KZ,1), TS(KTS,1)
C
C SUBROUTINE TO CALCULATE FINITE ELEMENT...
C STIFFNESS MATRIX,
C STRESS TRANSFORMATION MATRIX,
C FOR A TORSION ROD ELEMENT WITH UNRESTRAINED BOUNDARIES.
C ROD MAY BE LINEARLY TAPERED OR UNIFORM.
C CONSTANT TORQUE ASSUMED.
C STIFFNESS MATRIX IS IN LOCAL COORDINATE SYSTEM.
C STRESS TRANSFORMATION MATRIX RELATES STRESS AT ROD ENDS IN LOCAL
C COORDINATE SYSTEM TO ROTATIONS IN LOCAL COORDINATE SYSTEM.
C ROW ORDER IN STRESS TRANSFORMATION MATRIX IS
C TAU-X1,TAU-X2
C WHERE TAU IS SHEAR STRESS.
C STRESS IS + OR - AS RIGHT HAND AXIS BETWEEN END POINTS 1 AND 2.
C THE LOCAL COORDINATE SYSTEM ASSUMES THE ROD TO LIE ALONG THE X AXIS
C WITH JOINT 1 AT THE ORIGIN, JOINT 2 ALONG THE POSITIVE X AXIS.
C LOCAL COORDINATE ORDER IS
C TX1,TX2
C WHERE TX IS ROTATION.
C DEVELOPED BY RL WOHLER. FEBRUARY 1973.
C LAST REVISION BY RL WOHLER. SEPTEMBER 1973.
C
C SUBROUTINE ARGUMENTS
C TJ1 = INPUT CROSS-SECTION SAINT VENANTS TORSION CONSTANT (J) IN JG
C AT ROD END 1. E.G., TJ1=.5*PI*R1**4 FOR A SOLID CIRCULAR
C CYLINDER. TJ1=2.*PI*T*R1**3 FOR A THIN WALLED CIRCULAR
C CYLINDER.
C TJ2 = INPUT CROSS-SECTION SAINT VENANTS TORSION CONSTANT (J) IN JG
C AT ROD END 2.
C R1 = INPUT DISTANCE FROM TORSION AXIS TO OUTER FIBER AT ROD END 1.
C R2 = INPUT DISTANCE FROM TORSION AXIS TO OUTER FIBER AT ROD END 2.
C RL = INPUT ROD LENGTH.
C G = INPUT SHEAR MODULUS OF ELASTICITY.
C Z = OUTPUT STIFFNESS MATRIX. SIZE(2,2).
C TS = OUTPUT STRESS TRANSFORMATION MATRIX. SIZE(2,2).
C KZ = INPUT ROW DIMENSION OF Z IN CALLING PROGRAM. MIN=2.
C KTS = INPUT ROW DIMENSION OF TS IN CALLING PROGRAM. MIN=2.
C
S = TJ1*G/RL
R = TJ2/TJ1
IF (ABS(R-1.) .GT. .01) S = (TJ2-TJ1)*G / (RL*ALOG(R))
C STIFFNESS MATRIX.
Z(1,1) = S
Z(1,2) = -S
Z(2,1) = -S
Z(2,2) = S
C
C STRESS TRANSFORMATION MATRIX.
TS(1,1) = Z(1,1)*R1/TJ1
TS(1,2) = Z(1,2)*R1/TJ1
TS(2,1) = Z(2,1)*R2/TJ2
TS(2,2) = Z(2,2)*R2/TJ2
C

```

K1C1 -- 2 / 2

RETURN  
END

```

SUBROUTINE K2A1 (X2,X3,Y3,TH,E,ANU,Z,T,P,KZ,KT,KR)
DIMENSION Z(KZ,1),T(KT,1),R(KR,1)
DIMENSION XE(3),ET(3)

```

```

C
C SUBROUTINE TO CALCULATE FINITE ELEMENT...
C STIFFNESS MATRIX,
C STRESS TRANSFORMATION MATRIX,
C FOR A MEMBRANE TRIANGLE PLATE ELEMENT WITH UNRESTRAINED BOUNDARIES.
C QUADRATIC DISPLACEMENT (LINEAR STRAIN) FIELD IS USED.
C STIFFNESS MATRIX IS IN LOCAL COORDINATE SYSTEM.
C STRESS TRANSFORMATION MATRIX RELATES STRESS AT TRIANGLE VERTICES
C IN LOCAL COORDINATE SYSTEM TO DEFLECTIONS IN THE LOCAL SYSTEM.
C ROW ORDER IN STRESS TRANSFORMATION MATRIX IS
C (SIGMA-X,SIGMA-Y,TAU-XY) JOINT 1, THEN JOINT 2, 3.
C WHERE SIGMA IS NORMAL STRESS AND TAU IS SHEAR STRESS.
C THE LOCAL COORDINATE SYSTEM ASSUMES THE PLATE TO LIE IN AN X-Y PLANE
C WITH JOINT 1 AT THE X-Y ORIGIN, JOINT 2 LIES ALONG THE POSITIVE
C X AXIS, AND JOINT 3 IS IN THE POSITIVE Y DIRECTION.
C LOCAL COORDINATE ORDER IS
C (DX,DY,TZ) JOINT 1, THEN JOINT 2, 3.
C WHERE DX,DY ARE TRANSLATION AND TZ IS ROTATION.
C CALLS FOR SUBROUTINES BTABA AND MULTA.
C DEVELOPED BY CS BODLEY, WA BENFIELD. MARCH 1973.
C LAST REVISION BY CS BODLEY. SEPTEMBER 1973.

```

```

C
C SUBROUTINE ARGUMENTS
C X2 = INPUT LOCAL X COORDINATE LOCATION OF JOINT 2.
C X3 = INPUT LOCAL X COORDINATE LOCATION OF JOINT 3.
C Y3 = INPUT LOCAL Y COORDINATE LOCATION OF JOINT 3.
C TH = INPUT PLATE THICKNESS.
C E = INPUT YOUNGS MODULUS OF ELASTICITY.
C ANU = INPUT POISSONS RATIO. (E/2G)-1.
C Z = OUTPUT STIFFNESS MATRIX. SIZE(9,9).
C T = OUTPUT STRESS TRANSFORMATION MATRIX. SIZE(9,9).
C R = INPUT MATRIX WORK SPACE. SIZE(8,9).
C KZ = INPUT ROW DIMENSION OF Z IN CALLING PROGRAM. MIN=9.
C KT = INPUT ROW DIMENSION OF T IN CALLING PROGRAM. MIN=9.
C KR = INPUT ROW DIMENSION OF R IN CALLING PROGRAM. MIN=8.

```

```

C
DO 5 I=1,9
DO 5 J=1,9
5 T(I,J) = 0.0
DO 10 I=1,9
DO 10 J=1,9
10 Z(I,J) = 0.0
IF (TH .LE. 0.0) RETURN
X22 = X2*X2
Y32 = Y3*Y3
X2Y3 = X2*Y3
SE1 = X3/X2
G = E/(2. + 2.*ANU)
DD = E*TH/(1. - ANU**2)
DNU = DD*ANU
DG = G*TH

```

```

C

```

```

DO 15 I=1,8
DC 15 J=1,9
15 R(I,J) = 0.

```

C

```

F00 = X2Y3/2.
F10 = X2Y3*(1. + SE1)/6.
F01 = X2Y3/6.
F20 = X2Y3*(1. + SE1 + SE1**2)/12.
F11 = X2Y3*(1. + 2.*SE1)/24.
F02 = X2Y3/12.

```

C

```

Z(1,1) = DD*F00/X22
Z(1,3) = DD*F01/X22
Z(1,6) = DNU*F00/X2Y3
Z(1,8) = DNU*F10/X2Y3
Z(2,2) = DG*F00/Y32
Z(2,3) = DG*F10/Y32
Z(2,4) = 2.*DG*F01/Y32
Z(2,5) = DG*F00/X2Y3
Z(2,7) = 2.*DG*F10/X2Y3
Z(2,8) = DG*F01/X2Y3
Z(3,3) = DD*F02/X22 + DG*F20/Y32
Z(3,4) = 2.*DG*F11/Y32
Z(3,5) = DG*F10/X2Y3
Z(3,6) = DNU*F01/X2Y3
Z(3,7) = 2.*DG*F20/X2Y3
Z(3,8) = DNU*F11/X2Y3 + DG*F11/X2Y3
Z(4,4) = 4.*DG*F02/Y32
Z(4,5) = 2.*DG*F01/X2Y3
Z(4,7) = 4.*DG*F11/X2Y3
Z(4,8) = 2.*DG*F02/X2Y3
Z(5,5) = DG*F00/X22
Z(5,7) = 2.*DG*F10/X22
Z(5,8) = DG*F01/X22
Z(6,6) = DD*F00/Y32
Z(6,8) = DD*F10/Y32
Z(7,7) = 4.*DG*F20/X22
Z(7,8) = 2.*DG*F11/X22
Z(8,8) = DD*F20/Y32 + DG*F02/X22

```

```

DO 20 I=1,8

```

```

DC 20 J=1,8

```

```

20 Z(J,I) = Z(I,J)

```

C

```

R(1,1) = -1.
R(1,2) = 1.
R(2,1) = SE1 - 1.
R(2,3) = -Y3
R(2,4) = -SE1
R(2,7) = 1.
R(2,9) = Y3
R(3,3) = Y3
R(3,6) = -Y3
R(4,3) = Y3*(1. - SE1)
R(4,6) = Y3*SE1
R(4,9) = -Y3

```

```

R(5,2) = -1.
R(5,3) = X2
R(5,5) = 1.
R(5,6) = -X2
R(6,2) = SE1 - 1.
R(6,5) = -SE1
R(6,6) = X3
R(6,8) = 1.
R(6,9) = -X3
R(7,3) = -X2
R(7,6) = X2
R(8,3) = X2*(SE1 - 1.)
R(8,6) = -X3
R(8,9) = X2

```

C

```
CALL BTABA (Z,R,8,9,KZ,KR)
```

C

```

D11 = DD/TH
D12 = ANU*D11
D33 = G
XE(1) = 0.
XE(2) = 1.
XF(3) = SE1
ET(1) = 0.
ET(2) = 0.
ET(3) = 1.
DO 30 I=1,3
K1 = 3*I - 2
K2 = K1 + 1
K3 = K1 + 2
T(K1,1) = D11/X2
T(K1,3) = D11*ET(I)/X2
T(K1,6) = D12/Y3
T(K1,8) = D12*XF(I)/Y3
T(K2,1) = D12/X2
T(K2,3) = D12*ET(I)/X2
T(K2,6) = D11/Y3
T(K2,8) = D11*XF(I)/Y3
T(K3,2) = D33/Y3
T(K3,3) = D33*XF(I)/Y3
T(K3,4) = 2.*D33*ET(I)/Y3
T(K3,5) = D33/X2
T(K3,7) = 2.*D33*XE(I)/X2
30 T(K3,8) = 2.*D33*ET(I)/X2
CALL MULT. (T,R,9,8,9,KT,KR)

```

C

```

RETURN
END

```

```

SUBROUTINE K2B1 (X2,X3,Y3,TH,E,ANU,Z,TS,T,KZ,KTS,KT)
DIMENSION Z(KZ,9),TS(KTS,1),T(KT,1)
DIMENSION R(10,10),IVEC(10),COEF(9),XE(3),ET(3)
C
C SUBROUTINE TO CALCULATE FINITE ELEMENT...
C STIFFNESS MATRIX,
C STRESS TRANSFORMATION MATRIX,
C FOR A BENDING TRIANGLE PLATE ELEMENT WITH UNRESTRAINED BOUNDARIES.
C CUBIC DISPLACEMENT (LINEAR CURVATURE) FIELD IS USED.
C STIFFNESS MATRIX IS IN LOCAL COORDINATE SYSTEM.
C STRESS TRANSFORMATION MATRIX RELATES STRESS AT JOINTS IN LOCAL
C COORDINATE SYSTEM TO DEFLECTIONS IN THE LOCAL SYSTEM.
C ROW ORDER IN STRESS TRANSFORMATION MATRIX IS
C (SIGMA-X,SIGMA-Y,TAU-XY) FOR (Z=TH/2) AT JOINT 1, THEN JOINT 2,3,
C (SIGMA-X,SIGMA-Y,TAU-XY) FOR (Z=-TH/2) AT JOINT 1, THEN JOINT 2,3.
C WHERE SIGMA IS NORMAL STRESS AND TAU IS SHEAR STRESS.
C THE LOCAL COORDINATE SYSTEM ASSUMES THE PLATE TO LIE IN AN X-Y PLANE
C WITH JOINT 1 AT THE X-Y ORIGIN, JOINT 2 LIES ALONG THE POSITIVE
C X AXIS, AND JOINT 3 IS IN THE POSITIVE Y DIRECTION.
C LOCAL COORDINATE ORDER IS
C (DZ,TX,TY) JOINT 1, THEN JOINT 2, 3.
C WHERE DZ IS TRANSLATION AND TX,TY ARE ROTATIONS.
C CALLS FORMER SUBROUTINES FTAE6 AND MULTA.
C DEVELOPED BY CS EODLEY. MARCH 1973.
C LAST REVISION BY CS EODLEY. SEPTEMBER 1973.
C
C SUBROUTINE ARGUMENTS
C X2 = INPUT LOCAL X COORDINATE LOCATION OF JOINT 2.
C X3 = INPUT LOCAL X COORDINATE LOCATION OF JOINT 3.
C Y3 = INPUT LOCAL Y COORDINATE LOCATION OF JOINT 3.
C TH = INPUT PLATE THICKNESS.
C E = INPUT YOUNG'S MODULUS OF ELASTICITY.
C ANU = INPUT POISSON'S RATIO. (E/2G)-1.
C Z = OUTPUT STIFFNESS MATRIX. SIZE(9,9).
C TS = OUTPUT LOCAL STRESS TRANSFORMATION MATRIX. SIZE(18,9).
C T = INPUT MATRIX WORK SPACE. SIZE(10,10).
C KZ = INPUT ROW DIMENSION OF Z IN CALLING PROGRAM. MIN=9.
C KTS = INPUT ROW DIMENSION OF TS IN CALLING PROGRAM. MIN=18.
C KT = INPUT ROW DIMENSION OF T IN CALLING PROGRAM. MIN=10.
C
DO 10 I=1,9
DO 10 J=1,9
10 Z(I,J) = 0.0
DO 11 I=1,18
DO 11 J=1,9
11 TS(I,J) = 0.0
IF (TH .LE. 0.0) RETURN
C
DO 12 I=1,10
DO 12 J=1,10
12 T(I,J) = 0.0
X22 = X2*X2
X24 = X22*X22
Y32 = Y3*Y3
Y34 = Y32*Y32

```



```

SE1 = X3/X2
SE2 = SE1*SE1
SE3 = SE2*SE1
SE4 = SE3*SE1
SEC1 = (1. + SE1)/3.
SEC2 = SEC1**2
SEC3 = SEC1**3
G = E/(2. + 2.*ANU)
DD = (E*TH**3)/(12.*(1.-ANU**2))
DNU = DD*ANU
DG = (G*TH**3)/12.
AL = DD/X1
BE = DNU/(X22*Y32)
GA = DD/Y34
DE = 4.*DG/(X22*Y32)

```

C

```

T(1,1) = 1.
T(2,3) = 1.
T(3,2) = 1.
T(4,1) = 1.
T(4,2) = 1.
T(4,4) = 1.
T(4,7) = 1.
T(5,3) = 1.
T(5,5) = 1.
T(5,8) = 1.
T(6,2) = 1.
T(6,4) = 2.
T(6,7) = 3.
T(7,1) = 1.
T(7,2) = SE1
T(7,3) = 1.
T(7,4) = SE2
T(7,5) = SE1
T(7,6) = 1.
T(7,7) = SE3
T(7,8) = SE2
T(7,9) = SE1
T(7,10) = 1.
T(8,3) = 1.
T(8,5) = SE1
T(8,6) = 2.
T(8,8) = SE2
T(8,9) = 2.*SE1
T(8,10) = 3.
T(9,2) = 1.
T(9,4) = 2.*SE1
T(9,5) = 1.
T(9,7) = 3.*SE2
T(9,8) = 2.*SE1
T(9,9) = 1.
T(10,1) = 1.
T(10,2) = SEC1
T(10,3) = 1./3.
T(10,4) = SEC2

```

```

T(10,5) = SEC1/3.
T(10,6) = 1./9.
T(10,7) = SEC3
T(10,8) = SEC2/3.
T(10,9) = SEC1/9.
T(10,10) = 1./27.

```

C

```

DO 5 I=1,10
DO 7 J=1,10
7 R(I,J) = 0.
5 R(I,I) = 1.

```

C

```

DO 100 L=1,10
JEIG = 1
A1 = ABS(T(L,1))
DO 15 J=2,10
A2 = ABS(T(L,J))
IF (A2 .LT. A1) GO TO 15
A1 = A2
JEIG = J
15 CONTINUE
IVEC(L) = JEIG
ALJFIG = T(L,JEIG)
DO 17 J=1,10
T(L,J) = T(L,J)/ALJFIG
17 R(L,J) = R(L,J)/ALJFIG
DO 25 I=1,10
AIJFIG = T(I,JEIG)
IF (I .EQ. L) GO TO 25
DO 30 J=1,10
T(I,J) = T(I,J) - AIJFIG*T(L,J)
30 R(I,J) = R(I,J) - AIJFIG*R(L,J)
25 CONTINUE
100 CONTINUE

```

C

```

DO 40 I=1,10
IP = IVEC(I)
DO 40 J=1,10
40 T(IP,J) = R(I,J)
DO 50 I=1,10
DO 50 J=1,10
50 R(I,J) = T(I,J)

```

C

```

DO 20 I=1,10
R(I,2) = Y3*R(I,2)
R(I,3) = -X2*R(I,2)
R(I,5) = Y3*R(I,5)
R(I,6) = -X2*R(I,5)
R(I,8) = Y3*R(I,8)
20 R(I,9) = -X2*R(I,8)

```

C

```

COEF(1) = 1./3.
COEF(2) = Y3/18.
COEF(3) = -(X2+X2)/18.
COEF(4) = 1./3.

```

```

COEF(5) = Y3/18.
COEF(6) = (2.*X2 - X3)/18.
COEF(7) = 1./3.
COEF(8) = -Y3/6.
COEF(9) = (2.*X3 - X2)/18.
DO 80 I=1,10
DO 80 J=1,9
80 R(I,J) = R(I,J) + R(I,10)*COEF(J).
C
DO 55 I=1,10
DO 55 J=1,10
55 T(I,J) = 0.
C
F00 = X2*Y3/2.
F10 = X2*Y3*(1. + SE1)/6.
F01 = X2*Y3/6.
F20 = X2*Y3*(1. + SE1 + SE2)/12.
F11 = X2*Y3*(1. + 2.*SE1)/24.
F02 = X2*Y3/12.
C
T(4,4) = 4.*AL*F00
T(4,6) = 4.*BE*F00
T(4,7) = 12.*AL*F10
T(4,8) = 4.*AL*F01
T(4,9) = 4.*BE*F10
T(4,10) = 12.*BE*F01
T(5,5) = DE*F00
T(5,8) = 2.*DE*F10
T(5,9) = 2.*DE*F01
T(6,6) = 4.*GA*F00
T(6,7) = 12.*EE*F10
T(6,8) = 4.*EE*F01
T(6,9) = 4.*GA*F10
T(6,10) = 12.*GA*F01
T(7,7) = 36.*AL*F20
T(7,8) = 12.*AL*F11
T(7,9) = 12.*BE*F20
T(7,10) = 36.*BE*F11
T(8,8) = 4.*AL*F02 + 4.*DE*F20
T(8,9) = 4.*BE*F11 + 4.*DE*F11
T(8,10) = 12.*EE*F02
T(9,9) = 4.*GA*F20 + 4.*DE*F02
T(9,10) = 12.*GA*F11
T(10,10) = 36.*GA*F02
C
DO 60 I=1,10
DO 60 J=1,10
60 T(J,I) = T(I,J)
CALL ETABA (T,F,10,9,KT,10)
DO 85 I=1,9
DO 85 J=1,9
85 Z(I,J) = T(I,J)
C
DO 73 I=1,9
DO 73 J=1,10

```

```
73 T(I,J) = 0.0
   D11 = -6.*DD/((X2*TH)**2)
   D21 = ANU*D11
   D22 = -6.*DD/((Y3*TH)**2)
   D12 = ANU*D22
   D33 = -12.*DG/((X2*Y3)*TH**2)
   XE(1) = 0.
   XE(2) = 1.
   XE(3) = SE1
   ET(1) = 0.
   ET(2) = 0.
   ET(3) = 1.
   DO 75 I=1,3
   K1 = 3*I - 2
   K2 = K1 + 1
   K3 = K1 + 2
   T(K1,4) = 2.*D11
   T(K1,6) = 2.*D12
   T(K1,7) = 6.*D11*XE(I)
   T(K1,8) = 2.*D11*ET(I)
   T(K1,9) = 2.*D12*XE(I)
   T(K1,10) = 6.*D12*ET(I)
   T(K2,4) = 2.*D21
   T(K2,6) = 2.*D22
   T(K2,7) = 6.*D21*XE(I)
   T(K2,8) = 2.*D21*ET(I)
   T(K2,9) = 2.*D22*XE(I)
   T(K2,10) = 6.*D22*ET(I)
   T(K3,5) = D33
   T(K3,8) = 2.*D33*XE(I)
75 T(K3,9) = 2.*D33*ET(I)
   CALL MULTA (T,R,9,10,9,KT,10)
   DO 77 I=1,9
   IP9 = I + 9
   DO 77 J=1,9
   TS(I,J) = T(I,J)
77 TS(IP9,J) = -TS(I,J)
C
   RETURN
   END
```

SUBROUTINE K3C1 (X3,Y3,TH,G,Z,T,KZ,KT)  
 DIMENSION Z(KZ,1), T(KT,1)

C  
 C SUBROUTINE TO CALCULATE FINITE ELEMENT...  
 C STIFFNESS MATRIX,  
 C STRESS TRANSFORMATION MATRIX,  
 C FOR A RECTANGULAR SHEAR PANEL ELEMENT WITH UNRESTRAINED BOUNDARIES.  
 C LINEAR DISPLACEMENT (CONSTANT STRAIN) FIELD IS USED.  
 C STIFFNESS MATRIX IS IN LOCAL COORDINATE SYSTEM.  
 C STRESS TRANSFORMATION MATRIX RELATES PANEL SHEAR STRESS (CONSTANT)  
 C IN LOCAL COORDINATE SYSTEM TO DEFLECTIONS IN THE LOCAL SYSTEM.  
 C THE LOCAL COORDINATE SYSTEM ASSUMES THE PANEL TO LIE IN AN X-Y PLANE  
 C WITH JOINT 1 AT THE X-Y ORIGIN, JOINT 2 LIES ALONG THE POSITIVE  
 C X AXIS, JOINT 3 IS IN THE POSITIVE X,Y DIRECTION, AND JOINT 4 LIES  
 C ALONG THE POSITIVE Y AXIS.  
 C LOCAL COORDINATE ORDER IS  
 C DX1,DX2,DX3,DX4, DY1,DY2,DY3,DY4  
 C WHERE DX,DY ARE TRANSLATIONS.  
 C DEVELOPED BY RL WOHLER. APRIL 1974.  
 C  
 C SUBROUTINE ARGUMENTS  
 C X3 = INPUT LOCAL X COORDINATE LOCATION OF JOINT 3.  
 C Y3 = INPUT LOCAL Y COORDINATE LOCATION OF JOINT 3.  
 C TH = INPUT PANEL THICKNESS.  
 C G = INPUT SHEAR MODULUS OF ELASTICITY.  
 C Z = OUTPUT STIFFNESS MATRIX. SIZE(8,8).  
 C T = OUTPUT STRESS TRANSFORMATION MATRIX. SIZE(1,8).  
 C KZ = INPUT ROW DIMENSION OF Z IN CALLING PROGRAM. MIN=8.  
 C KT = INPUT ROW DIMENSION OF T IN CALLING PROGRAM. MIN=1.  
 C  
 C STIFFNESS MATRIX.  
 C = TH\*G/4.  
 A = C\*X3/Y3  
 B = C\*Y3/X3  
 Z(1,1) = A  
 Z(1,2) = A  
 Z(1,3) = -A  
 Z(1,4) = -A  
 Z(1,5) = C  
 Z(1,6) = -C  
 Z(1,7) = -C  
 Z(1,8) = C  
 Z(2,2) = A  
 Z(2,3) = -A  
 Z(2,4) = -A  
 Z(2,5) = C  
 Z(2,6) = -C  
 Z(2,7) = -C  
 Z(2,8) = C  
 Z(3,5) = A  
 Z(3,4) = A  
 Z(3,5) = -C  
 Z(3,6) = C  
 Z(3,7) = C  
 Z(3,8) = -C

```
Z(4,4) = A
Z(4,5) = -C
Z(4,6) = C
Z(4,7) = C
Z(4,8) = -C
Z(5,5) = F
Z(5,6) = -F
Z(5,7) = -E
Z(5,8) = B
Z(6,6) = F
Z(6,7) = B
Z(6,8) = -E
Z(7,7) = B
Z(7,8) = -F
Z(8,8) = F
C SYMMETRIZE LOWER HALF.
  DO 10 J=1,8
  DC 10 I=J,8
  10 Z(I,J) = Z(J,I)
C
C STRESS TRANSFORMATION MATRIX.
  DO 20 J=1,8
  20 T(1,J) = 2.*Z(3,J)/(TH*X3)
C
  RETURN
  END
```

KGRAV

```
SUBROUTINE KGRAV (CJ, JM ,EV,A,W,KW,KCJ)
DIMENSION CJ(KCJ ,1), JM( 1), EV(1), W(KW,1)
DIMENSION E(3,4),R12(3),R13(3),VN(3),F(3,3)
DATA KEF / 3 /

C
C SUBROUTINE TO DERIVE STIFFNESS MATRIX FOR A TRIANGULAR GRAVITY ELEMENT.
C CALLS FORMA SUBROUTINES MULTA ,MULTB ,VCROSS.
C DEVELOPED BY C S BODLEY. FEBRUARY 1974.
C LAST REVISION BY C S BODLEY. NOVEMBER 1974.
C SUBROUTINE ARGUMENTS
C CJ = INPUT MATRIX OF JOINT COORDINATES. SIZE (3,4).
C JM = INPUT VECTOR OF JOINTS DEFINING A TRIANGLE. SIZE (3).
C EV = INPUT VECTOR NORMALIZED GRAVITY. SIZE = 3.
C A = OUTPUT AREA.
C W = OUTPUT STIFFNESS MATRIX.
C KW = INPUT ROW DIMENSION SIZE OF W IN CALLING PROGRAM. MIN=9.
C KCJ = INPUT ROW DIMENSION OF CJ IN CALLING PROGRAM. MIN=3.
C
      J1 = JM(1 )
      J2 = JM(2 )
      J3 = JM(3 )
      DO 5 I=1,9
      DO 5 J=1,3
      W(I,J) = 0.
      5 E(J,I) = 0.
      DO 7 I=1,3
      R12(I) = CJ(I,J2) - CJ(I,J1)
      R13(I) = CJ(I,J3) - CJ(I,J1)
      DO 8 J=1,3
      8 F(1,J) = 1.
      7 F(1,I) = 2.
C
      CALL VCROSS (R12,R13,VN,VAMAG,VBMAG,A,SINAB)
      DO 10 I=1,3
      10 VN(I) = VN(I)/A
      ACUM = 0.0
      DO 15 I=1,3
      I1 = 3*I - 3
      ACUM = ACUM + VN(I)*EV(I)
      DO 15 J=1,2
      E(I,I1+J) = VN(J)
      15 W(I1+J,I) = VN(J)
      CALL MULTB (F,E,3,3,0,KEF,KEF)
      CALL MULTA (W,F,0,3,9,KW,KEF)
      A = A*ACUM*ACUM*ACUM
C
      RETURN
      END
```

MIA1

```
SUBROUTINE MIA1 (A1,A2,RL,RO,Z,KZ)
DIMENSION Z(KZ,1)

C
C SUBROUTINE TO CALCULATE FINITE ELEMENT...
C LUMPED MASS MATRIX
C FOR AN AXIAL ROD ELEMENT WITH UNRESTRAINED BOUNDARIES.
C ROD MAY BE LINEARLY TAPERED OR UNIFORM.
C MASS MATRIX IS IN LOCAL COORDINATE SYSTEM.
C THE LOCAL COORDINATE SYSTEM ASSUMES THE ROD TO LIE ALONG THE X AXIS
C WITH JOINT 1 AT THE ORIGIN, JOINT 2 ALONG THE POSITIVE X AXIS.
C LOCAL COORDINATE ORDER IS
C DX1,DX2
C WHERE DX IS TRANSLATION.
C DEVELOPED BY RL WOHLN. JANUARY 1973.
C LAST REVISION BY RL WOHLN. SEPTEMBER 1973.
C
C SUBROUTINE ARGUMENTS
C A1 = INPUT CROSS-SECTION AREA AT ROD END 1.
C A2 = INPUT CROSS-SECTION AREA AT ROD END 2.
C RL = INPUT ROD LENGTH.
C RO = INPUT MASS DENSITY.
C Z = OUTPUT MASS MATRIX. SIZE(2,2).
C KZ = INPUT ROW DIMENSION OF Z IN CALLING PROGRAM. MIN=2.
C
W1 = A1*RL*RO/6.
W2 = A2*RL*RO/6.
Z(1,1) = 2.*W1 + W2
Z(1,2) = 0.
Z(2,1) = 0.
Z(2,2) = W1 + 2.*W2

C
RETURN
END
```



MIA2

```
-----
SUBROUTINE MIA2 (A1,A2,RL,RO,Z,KZ)
  DIMENSION Z(KZ,1)
C
C SUBROUTINE TO CALCULATE FINITE ELEMENT...
C CONSISTENT MASS MATRIX
C FOR AN AXIAL ROD ELEMENT WITH UNRESTRAINED BOUNDARIES.
C ROD MAY BE LINEARLY TAPERED OR UNIFORM.
C LINEAR DISPLACEMENT FUNCTION ASSUMED.
C MASS MATRIX IS IN LOCAL COORDINATE SYSTEM.
C THE LOCAL COORDINATE SYSTEM ASSUMES THE ROD TO LIE ALONG THE X AXIS
C WITH JOINT 1 AT THE ORIGIN, JOINT 2 ALONG THE POSITIVE X AXIS.
C LOCAL COORDINATE ORDER IS
C DX1,DX2
C WHERE DX IS TRANSLATION.
C DEVELOPED BY RL WOHLER. SEPTEMBER 1972.
C LAST REVISION BY RL WOHLER. SEPTEMBER 1973.
C
C SUBROUTINE ARGUMENTS
C A1 = INPUT CROSS-SECTION AREA AT ROD END 1.
C A2 = INPUT CROSS-SECTION AREA AT ROD END 2.
C RL = INPUT ROD LENGTH.
C RO = INPUT MASS DENSITY.
C Z = OUTPUT MASS MATRIX. SIZE(2,2).
C KZ = INPUT ROW DIMENSION OF Z IN CALLING PROGRAM. MIN=2.
C
  W1 = A1*RL*RO/12.
  W2 = A2*RL*RO/12.
  Z(1,1) = 3.*W1 + W2
  Z(1,2) = W1 + W2
  Z(2,1) = Z(1,2)
  Z(2,2) = W1 + 3.*W2
C
  RETURN
  END
```

MIB1

```

SUBROUTINE MIB1 (A1,A2,RL,RO,Z,KZ)
DIMENSION Z(KZ,1)
C
C SUBROUTINE TO CALCULATE FINITE ELEMENT...
C LUMPED MASS MATRIX
C FOR A BENDING BEAM ELEMENT WITH UNRESTRAINED BOUNDARIES.
C BEAM MAY BE LINEARLY TAPERED OR UNIFORM.
C MASS MATRIX IS IN LOCAL COORDINATE SYSTEM.
C THE LOCAL COORDINATE SYSTEM ASSUMES THE BEAM TO LIE IN THE X-Z PLANE
C WITH JOINT 1 AT THE ORIGIN, JOINT 2 ALONG THE POSITIVE X AXIS.
C LOCAL COORDINATE ORDER IS
C DZ1,DZ2,TY1,TY2
C WHERE DZ IS TRANSLATION AND TY IS ROTATION.
C DEVELOPED BY RL WOHLIN. FEBRUARY 1973.
C LAST REVISION BY RL WOHLIN. SEPTEMBER 1973.
C
C SUBROUTINE ARGUMENTS
C A1 = INPUT CROSS-SECTION AREA AT BEAM END 1.
C A2 = INPUT CROSS-SECTION AREA AT BEAM END 2.
C RL = INPUT BEAM LENGTH.
C RO = INPUT MASS DENSITY.
C Z = OUTPUT MASS MATRIX. SIZE(4,4).
C KZ = INPUT ROW DIMENSION OF Z IN CALLING PROGRAM. MIN=4.
C
      W1 = A1*RL*RO/6.
      W2 = A2*RL*RO/6.
      DO 10 J=1,4
      DO 10 I=1,4
10 Z(I,J) = 0.0
      Z(1,1) = 2.*W1 + W2
      Z(2,2) = W1 + 2.*W2
      Z(3,3) = (A1*RO*RL**3)/24.
      Z(4,4) = (A2*RO*RL**3)/24.
C
      RETURN
      END

```

```
      SUBROUTINE M1B2 (A1,A2,RL,RO,Z,KZ)
      DIMENSION Z(KZ,1)
C
C  SUBROUTINE TO CALCULATE FINITE ELEMENT...
C  CONSISTENT MASS MATRIX
C  FOR A BENDING BEAM ELEMENT WITH UNRESTRAINED BOUNDARIES.
C  BEAM MAY BE LINEARLY TAPERED OR UNIFORM.
C  CUBIC DISPLACEMENT FUNCTION ASSUMED.
C  MASS MATRIX IS IN LOCAL COORDINATE SYSTEM.
C  THE LOCAL COORDINATE SYSTEM ASSUMES THE BEAM TO LIE IN THE X-Z PLANE
C  WITH JOINT 1 AT THE ORIGIN, JOINT 2 ALONG THE POSITIVE X AXIS.
C  LOCAL COORDINATE ORDER IS
C    DZ1,DZ2,TY1,TY2
C  WHERE DZ IS TRANSLATION AND TY IS ROTATION.
C  DEVELOPED BY RL WOHLER. FEBRUARY 1973.
C  LAST REVISION BY RL WOHLER. SEPTEMBER 1973.
C
C  SUBROUTINE ARGUMENTS
C  A1 = INPUT  CROSS-SECTION AREA AT BEAM END 1.
C  A2 = INPUT  CROSS-SECTION AREA AT BEAM END 2.
C  RL = INPUT  BEAM LENGTH.
C  RO = INPUT  MASS DENSITY.
C  Z  = OUTPUT MASS MATRIX. SIZE(4,4).
C  KZ = INPUT  ROW DIMENSION OF Z IN CALLING PROGRAM. MIN=4.
C
      W1 = A1*RL*RO/840.
      W2 = A2*RL*RO/840.
      RL2 = RL**2
      Z(1,1) = 240.*W1 + 72.*W2
      Z(1,2) = 54.*W1 + 54.*W2
      Z(2,2) = 72.*W1 + 240.*W2
      Z(1,3) = -( 30.*W1 + 14.*W2)*RL
      Z(1,4) = ( 14.*W1 + 12.*W2)*RL
      Z(2,3) = -( 12.*W1 + 14.*W2)*RL
      Z(2,4) = ( 14.*W1 + 30.*W2)*RL
      Z(3,3) = ( 5.*W1 + 3.*W2)*RL2
      Z(3,4) = -( 3.*W1 + 3.*W2)*RL2
      Z(4,4) = ( 3.*W1 + 5.*W2)*RL2
      DO 10 J=1,4
      DO 10 I=J,4
10  Z(I,J) = Z(J,I)
C
      RETURN
      END
```

MIC1

```

SUBROUTINE MIC1 (PI1,PI2,RL,RO,Z,KZ)
  DIMENSION Z(KZ,1)
C
C SUBROUTINE TO CALCULATE FINITE ELEMENT...
C LUMPED MASS MATRIX
C FOR A TORSION ROD ELEMENT WITH UNRESTRAINED BOUNDARIES.
C ROD MAY BE LINEARLY TAPERED OR UNIFORM.
C MASS MATRIX IS IN LOCAL COORDINATE SYSTEM.
C THE LOCAL COORDINATE SYSTEM ASSUMES THE ROD TO LIE ALONG THE X AXIS
C WITH JOINT 1 AT THE ORIGIN, JOINT 2 ALONG THE POSITIVE X AXIS.
C LOCAL COORDINATE ORDER IS
C TX1, TX2
C WHERE TX IS ROTATION.
C DEVELOPED BY RL WOHLN. FEBRUARY 1973.
C LAST REVISION BY RL WOHLN. SEPTEMBER 1973.
C
C SUBROUTINE ARGUMENTS
C PI1 = INPUT CROSS-SECTION POLAR AREA MOMENT OF INERTIA AT ROD END 1.
C PI2 = INPUT CROSS-SECTION POLAR AREA MOMENT OF INERTIA AT ROD END 2.
C RL = INPUT ROD LENGTH.
C RO = INPUT MASS DENSITY.
C Z = OUTPUT MASS MATRIX. SIZE(2,2).
C KZ = INPUT ROW DIMENSION OF Z IN CALLING PROGRAM. MIN=2.
C
  W1 = PI1*RL*RO/6.
  W2 = PI2*RL*RO/6.
  Z(1,1) = 2.*W1 + W2
  Z(1,2) = 0.
  Z(2,1) = 0.
  Z(2,2) = W1 + 2.*W2
C
  RETURN
  END

```

MIC2

```
      SUBROUTINE MIC2 (PI1,PI2,RL,RO,Z,KZ)
      DIMENSION Z(KZ,1)
C
C SUBROUTINE TO CALCULATE FINITE ELEMENT...
C CONSISTENT MASS MATRIX
C FOR A TORSION ROD ELEMENT WITH UNRESTRAINED BOUNDARIES.
C ROD MAY BE LINEARLY TAPERED OR UNIFORM.
C LINEAR DISPLACEMENT FUNCTION ASSUMED.
C MASS MATRIX IS IN LOCAL COORDINATE SYSTEM.
C THE LOCAL COORDINATE SYSTEM ASSUMES THE ROD TO LIE ALONG THE X AXIS
C WITH JOINT 1 AT THE ORIGIN, JOINT 2 ALONG THE POSITIVE X AXIS.
C LOCAL COORDINATE ORDER IS
C TX1, TX2
C WHERE TX IS ROTATION.
C DEVELOPED BY RL WOHLER. FEBRUARY 1973.
C LAST REVISION BY RL WOHLER. SEPTEMBER 1973.
C
C SUBROUTINE ARGUMENTS
C PI1 = INPUT CROSS-SECTION POLAR AREA MOMENT OF INERTIA AT ROD END 1.
C PI2 = INPUT CROSS-SECTION POLAR AREA MOMENT OF INERTIA AT ROD END 2.
C RL = INPUT ROD LENGTH.
C RO = INPUT MASS DENSITY.
C Z = OUTPUT MASS MATRIX. SIZE(2,2).
C KZ = INPUT ROW DIMENSION OF Z IN CALLING PROGRAM. MIN=2.
C
      W1 = PI1*RO*RL/12.
      W2 = PI2*RO*RL/12.
      Z(1,1) = 3.*W1 + W2
      Z(1,2) = W1 + W2
      Z(2,1) = Z(1,2)
      Z(2,2) = W1 + 3.*W2
C
      RETURN
      END
```

M2A1

```
SUBROUTINE M2A1 (X2,Y3,TH,RO,Z,KZ)
DIMENSION Z(KZ,1)
C
C SUBROUTINE TO CALCULATE FINITE ELEMENT...
C LUMPED MASS MATRIX,
C FOR A MEMBRANE TRIANGLE PLATE ELEMENT WITH UNRESTRAINED BOUNDARIES.
C MASS MATRIX IS IN LOCAL COORDINATE SYSTEM.
C THE LOCAL COORDINATE SYSTEM ASSUMES THE PLATE TO LIE IN AN X-Y PLANE
C WITH JOINT 1 AT THE X-Y ORIGIN, JOINT 2 LIES ALONG THE POSITIVE
C X AXIS, AND JOINT 3 IS IN THE POSITIVE Y DIRECTION.
C LOCAL COORDINATE ORDER IS
C (DX,DY,TZ) JOINT 1, THEN JOINT 2, 3.
C WHERE DX,DY ARE TRANSLATIONS AND TZ IS ROTATION.
C DEVELOPED BY WA BENFIELD. FEBRUARY 1973.
C LAST REVISION BY RL WOHLER. SEPTEMBER 1973.
C
C SUBROUTINE ARGUMENTS
C X2 = INPUT LOCAL X COORDINATE LOCATION OF JOINT 2.
C Y3 = INPUT LOCAL Y COORDINATE LOCATION OF JOINT 3.
C TH = INPUT PLATE THICKNESS.
C RO = INPUT MASS DENSITY.
C Z = OUTPUT MASS MATRIX. SIZE(9,9).
C KZ = INPUT ROW DIMENSION OF Z IN CALLING PROGRAM. MIN=9.
C
AREA = 0.5*X2*Y3
CM = (RO*TH*AREA)/3.0
DO 10 I=1,9
DO 10 J=1,9
10 Z(I,J) = 0.0
DO 20 I=1,9
20 Z(I,I) = CM
RETURN
END
```

```

SUBROUTINE M2A2 (X2,X3,Y3,TH,RHO,Z,T,R,KZ,KT,KR)
DIMENSION Z(KZ,1),T(KT,1),R(KR,1)

```

```

C
C SUBROUTINE TO CALCULATE FINITE ELEMENT...
C CONSISTENT MASS MATRIX,
C FOR A MEMBRANE TRIANGLE PLATE ELEMENT WITH UNRESTRAINED BOUNDARIES.
C QUADRATIC DISPLACEMENT (LINEAR STRAIN) FIELD IS USED.
C MASS MATRIX IS IN LOCAL COORDINATE SYSTEM.
C THE LOCAL COORDINATE SYSTEM ASSUMES THE PLATE TO LIE IN AN X-Y PLANE
C WITH JOINT 1 AT THE X-Y ORIGIN, JOINT 2 LIES ALONG THE POSITIVE
C X AXIS, AND JOINT 3 IS IN THE POSITIVE Y DIRECTION.
C LOCAL COORDINATE ORDER IS
C (DX,DY,TZ) JOINT 1, THEN JOINT 2, 3.
C WHERE DX,DY ARE TRANSLATIONS AND TZ IS ROTATION.
C CALLS FOPMA SUBROUTINES ETAL.
C DEVELOPED BY CS BODLEY. MARCH 1973.
C LAST REVISION BY WA BENFIELD. SEPTEMBER 1973.

```

```

C
C SUBROUTINE ARGUMENTS
C X2 = INPUT LOCAL X COORDINATE LOCATION OF JOINT 2.
C X3 = INPUT LOCAL X COORDINATE LOCATION OF JOINT 3.
C Y3 = INPUT LOCAL Y COORDINATE LOCATION OF JOINT 3.
C TH = INPUT PLATE THICKNESS.
C RHO = INPUT MASS DENSITY.
C Z = OUTPUT MASS MATRIX. SIZE(9,9).
C T = INPUT MATRIX WORK SPACE. SIZE(10,10).
C R = INPUT MATRIX WORK SPACE. SIZE(10,10).
C KZ = INPUT ROW DIMENSION OF Z IN CALLING PROGRAM. MIN=9.
C KT = INPUT ROW DIMENSION OF T IN CALLING PROGRAM. MIN=10.
C KR = INPUT ROW DIMENSION OF R IN CALLING PROGRAM. MIN=10.

```

```

C
SE1 = X2/X2
SE2 = SE1*SE1
SE3 = SE2*SE1
SE4 = SE3*SE1
X2Y3 = X2*Y3*RHO*TH

```

```

C
DO 10 I=1,10
DO 10 J=1,10
T(I,J) = 0.
10 R(I,J) = 0.

```

```

C
F00 = X2Y3/2.
F10 = X2Y3*(1. + SE1)/6.
F01 = X2Y3/6.
F20 = X2Y3*(1. + SE1 + SE2)/12.
F11 = X2Y3*(1. + 2.*SE1)/24.
F02 = X2Y3/12.
F30 = X2Y3*(1. + SE1 + SE2 + SE3)/20.
F21 = X2Y3*(1. + 2.*SE1 + 3.*SE2)/60.
F12 = X2Y3*(1. + 3.*SE1)/60.
F03 = X2Y3/20.
F40 = X2Y3*(1. + SE1 + SE2 + SE3 + SE4)/30.
F31 = X2Y3*(1. + 2.*SE1 + 3.*SE2 + 4.*SE3)/120.
F22 = X2Y3*(1. + 3.*SE1 + 6.*SE2)/180.

```

```

F13 = X2Y3*(1. + 4.*SE1)/120.
F04 = X2Y3/30.
T(1,1) = F00
T(1,2) = F10
T(1,3) = F01
T(1,4) = F11
T(1,5) = F02
T(2,2) = F20
T(2,3) = F11
T(2,4) = F21
T(2,5) = F12
T(3,3) = F02
T(3,4) = F12
T(3,5) = F03
T(4,4) = F22
T(4,5) = F13
T(5,5) = F04
T(6,6) = F00
T(6,7) = F10
T(6,8) = F01
T(6,9) = F20
T(6,10) = F11
T(7,7) = F20
T(7,8) = F11
T(7,9) = F30
T(7,10) = F21
T(8,8) = F02
T(8,9) = F21
T(8,10) = F12
T(9,9) = F40
T(9,10) = F31
T(10,10) = F22
DO 30 I=1,10
DO 30 J=1,10
30 T(J,I) = T(I,J)

```

C

```

F(1,1) = 1.
R(2,1) = -1.
R(2,4) = 1.
P(3,1) = SE1 - 1.
R(3,3) = -Y3
F(3,4) = -SE1
F(3,7) = 1.
R(3,9) = Y3
P(4,3) = Y2
R(4,6) = -Y3
R(5,3) = Y3*(1. - SE1)
P(5,6) = Y3*SE1
R(5,9) = -Y3
R(6,2) = 1.
P(7,2) = -1.
P(7,3) = Y2
P(7,5) = 1.
R(7,6) = -Y2
R(8,2) = SE1 - 1.

```



```
R(8,5) = -SE1  
R(8,6) = X3  
R(8,8) = 1.  
F(8,9) = -Y3  
R(9,3) = -X2  
F(9,6) = X2  
F(10,2) = X2*(SE1 - 1.)  
R(10,6) = -X3  
R(10,9) = X2
```

C

```
CALL PTABA (T,R,10,9,KT,KB)  
DC 40 I=1,0  
DC 40 J=1,0  
40 Z(I,J) = T(I,J)
```

C

```
RETURN  
END
```

M2B1

SUBROUTINE M2B1 (X2,Y3,TH,RO,Z,KZ)  
DIMENSION Z(KZ,1)

C  
C SUBROUTINE TO CALCULATE FINITE ELEMENT...  
C LUMPED MASS MATRIX.  
C FOR A BENDING TRIANGLE PLATE ELEMENT WITH UNRESTRAINED BOUNDARIES.  
C MASS MATRIX IS IN LOCAL COORDINATE SYSTEM.  
C THE LOCAL COORDINATE SYSTEM ASSUMES THE PLATE TO LIE IN AN X-Y PLANE  
C WITH JOINT 1 AT THE X-Y ORIGIN, JOINT 2 LIES ALONG THE POSITIVE  
C X AXIS, AND JOINT 3 IS IN THE POSITIVE Y DIRECTION.  
C LOCAL COORDINATE ORDER IS  
C (DZ, TX, TY) JOINT 1, THEN JOINT 2, 3.  
C WHERE DZ IS TRANSLATION AND TX, TY ARE ROTATIONS.  
C DEVELOPED BY WA BENFIELD. FEBRUARY 1973.  
C LAST REVISION BY RL WOHLER. SEPTEMBER 1973.

C  
C SUBROUTINE ARGUMENTS  
C X2 = INPUT LOCAL X COORDINATE LOCATION OF JOINT 2.  
C Y3 = INPUT LOCAL Y COORDINATE LOCATION OF JOINT 3.  
C TH = INPUT PLATE THICKNESS.  
C RO = INPUT MASS DENSITY.  
C Z = OUTPUT MASS MATRIX. SIZE(9,9).  
C KZ = INPUT ROW DIMENSION OF Z IN CALLING PROGRAM. MIN=9.

C  
C AREA = 0.5\*X2\*Y3  
C CM = (RO\*TH\*AREA)/3.0  
C DO 10 I=1,9  
C DO 10 J=1,9  
10 Z(I,J) = 0.0  
C DO 20 I=1,9  
20 Z(I,J) = CM  
C RETURN  
C END

```

SUBROUTINE M2F2 (X2,X3,Y3,TH,RHO,Z,T,R,KZ,KT,KR)
DIMENSION Z(KZ,1),T(KT,1),R(KR,1)
DIMENSION IVEC(10),COEF(9)

```

```

C
C SUBROUTINE TO CALCULATE FINITE ELEMENT...
C CONSISTENT MASS MATRIX,
C FOR A BENDING TRIANGLE PLATE ELEMENT WITH UNRESTRAINED BOUNDARIES.
C CUBIC DISPLACEMENT (LINEAR CURVATURE) FIELD IS USED.
C THIS IS NOT THE SO CALLED STRICKLAND ELEMENT.
C MASS MATRIX IS IN LOCAL COORDINATE SYSTEM.
C THE LOCAL COORDINATE SYSTEM ASSUMES THE PLATE TO LIE IN AN X-Y PLANE
C WITH JOINT 1 AT THE X-Y ORIGIN, JOINT 2 LIES ALONG THE POSITIVE
C X AXIS, AND JOINT 3 IS IN THE POSITIVE Y DIRECTION.
C LOCAL COORDINATE ORDER IS
C (DZ, TX, TY) JOINT 1, THEN JOINT 2, 3.
C WHERE DZ IS TRANSLATION AND TX, TY ARE ROTATIONS.
C CALLS FOR SUBROUTINES BTABA.
C DEVELOPED BY CAFL FODLEY MARCH 1973.
C LAST REVISION BY WA BENFIELD. SEPTEMBER 1973.

```

```

C
C SUBROUTINE ARGUMENTS
C X2 = INPUT LOCAL X COORDINATE LOCATION OF JOINT 2.
C X3 = INPUT LOCAL X COORDINATE LOCATION OF JOINT 3.
C Y3 = INPUT LOCAL Y COORDINATE LOCATION OF JOINT 3.
C TH = INPUT PLATE THICKNESS.
C RHO = INPUT MASS DENSITY.
C Z = OUTPUT MASS MATRIX. SIZE(9,9).
C T = INPUT MATRIX WORK SPACE. SIZE(10,10).
C R = INPUT MATRIX WORK SPACE. SIZE(10,10).
C KZ = INPUT ROW DIMENSION OF Z IN CALLING PROGRAM. MIN=9.
C KT = INPUT ROW DIMENSION OF T IN CALLING PROGRAM. MIN=10.
C KR = INPUT ROW DIMENSION OF R IN CALLING PROGRAM. MIN=10.

```

```

C
C SF1 = X3/Y3
C SF2 = SF1*SF1
C SF3 = SF2*SF1
C SF4 = SF3*SF1
C SF5 = SF4*SF1
C SF6 = SF5*SF1
C SEC1 = (1. + SF1)/3.
C SEC2 = SEC1**2
C SEC3 = SEC1**3

```

```

C
C DO 10 I=1,10
C DO 10 J=1,10
10 T(I,J) = 0.

```

```

C
C T(1,1) = 1.
C T(2,2) = 1.
C T(3,2) = 1.
C T(4,1) = 1.
C T(4,2) = 1.
C T(4,4) = 1.
C T(4,7) = 1.
C T(5,3) = 1.

```

T(5,5) = 1.  
T(5,8) = 1.  
T(6,2) = 1.  
T(6,4) = 2.  
T(6,7) = 3.  
T(7,1) = 1.  
T(7,2) = SE1  
T(7,3) = 1.  
T(7,4) = SE2  
T(7,5) = SE1  
T(7,6) = 1.  
T(7,7) = SE3  
T(7,8) = SE2  
T(7,9) = SE1  
T(7,10) = 1.  
T(8,3) = 1.  
T(8,5) = SE1  
T(8,6) = 2.  
T(8,8) = SE2  
T(8,9) = 2.\*SE1  
T(8,10) = 3.  
T(9,2) = 1.  
T(9,4) = 2.\*SE1  
T(9,5) = 1.  
T(9,7) = 3.\*SE2  
T(9,8) = 2.\*SE1  
T(9,9) = 1.  
T(10,1) = 1.  
T(10,2) = SEC1  
T(10,3) = 1./3.  
T(10,4) = SEC2  
T(10,5) = SEC1/3.  
T(10,6) = 1./9.  
T(10,7) = SEC3  
T(10,8) = SEC2/3.  
T(10,9) = SEC1/9.  
T(10,10) = 1./27.

C

DO 5 I=1,10  
DO 7 J=1,10  
7 R(I,J) = 0.  
5 R(I,I) = 1.

C

DO 100 L=1,10  
JBIG = 1  
A1 = ABS(T(L,1))  
DO 15 J=2,10  
A2 = ABS(T(L,J))  
IF (A2 .LT. A1) GO TO 15  
A1 = A2  
JBIG = J  
15 CONTINUE  
IVEC(L) = JBIG  
ALJBIG = T(L,JBIG)  
DO 17 J=1,10

```

T(L,J) = T(L,J)/ALJFIG
17 R(L,J) = F(L,J)/ALJFIG
DO 25 I=1,10
  AIJFIG = T(I,J)FIG
  IF (I .EQ. L) GO TO 25
  DO 30 J=1,10
    T(I,J) = T(I,J) - AIJFIG*T(L,J)
30 R(I,J) = R(I,J) - AIJFIG*R(L,J)
25 CONTINUE
100 CONTINUE

```

```

C
DO 40 I=1,10
  IF = IVEC(I)
  DO 40 J=1,10
40 T(IR,J) = R(I,J)
  DO 50 I=1,10
  DO 50 J=1,10
50 R(I,J) = T(I,J)

```

```

C
DO 20 I=1,10
  R(I,2) = Y3*P(I,2)
  R(I,3) = -X2*R(I,3)
  R(I,5) = Y3*R(I,5)
  R(I,6) = -X2*R(I,6)
  R(I,8) = Y3*P(I,8)
20 R(I,9) = -X2*R(I,9)

```

```

C
COEF(1) = 1./3.
COEF(2) = Y3/18.
COEF(3) = -(X2+X3)/18.
COEF(4) = 1./3.
COEF(5) = Y3/18.
COEF(6) = (2.*X2 - X3)/18.
COEF(7) = 1./3.
COEF(8) = -Y3/9.
COEF(9) = (2.*X3 - X2)/18.
DO 80 I=1,10
  DO 80 J=1,9
80 R(I,J) = R(I,J) + R(I,10)*COEF(J)

```

```

C
DO 55 I=1,10
  DO 55 J=1,10
55 T(I,J) = 0.

```

```

C
X2Y3 = X2*Y3*TH*RHO
FO0 = X2Y3/2.
FO1 = X2Y3*(1. + SE1)/6.
FO2 = X2Y3/6.
FO3 = X2Y3*(1. + SE1 + SE2)/12.
FO4 = X2Y3*(1. + 2.*SE1)/24.
FO5 = X2Y3/12.
FO6 = X2Y3*(1. + SE1 + SE2 + SE3)/20.
FO7 = X2Y3*(1. + 2.*SE1 + 3.*SE2)/60.
FO8 = X2Y3*(1. + 3.*SE1)/60.
FO9 = X2Y3/20.

```

$F40 = X2Y3*(1. + SE1 + SE2 + SE3 + SE4)/30.$   
 $F31 = X2Y3*(1. + 2.*SE1 + 3.*SE2 + 4.*SE3)/120.$   
 $F22 = X2Y3*(1. + 3.*SE1 + 6.*SE2)/180.$   
 $F13 = X2Y3*(1. + 4.*SE1)/120.$   
 $F04 = X2Y3/30.$   
 $F50 = X2Y3*(1. + SE1 + SE2 + SE3 + SE4 + SE5)/42.$   
 $F41 = X2Y3*(1. + 2.*SE1 + 3.*SE2 + 4.*SE3 + 5.*SE4)/210.$   
 $F32 = X2Y3*(1. + 3.*SE1 + 6.*SE2 + 10.*SE3)/420.$   
 $F23 = X2Y3*(1. + 4.*SE1 + 10.*SE2)/420.$   
 $F14 = X2Y3*(1. + 5.*SE1)/210.$   
 $F05 = X2Y3/42.$   
 $F60 = X2Y3*(1. + SE1 + SE2 + SE3 + SE4 + SE5 + SE6)/56.$   
 $F51 = X2Y3*(1.+2.*SE1+3.*SE2+4.*SE3+5.*SE4+6.*SE5)/336.$   
 $F42 = X2Y3*(1.+3.*SE1+6.*SE2+10.*SE3+15.*SE4)/840.$   
 $F33 = X2Y3*(1.+4.*SE1+10.*SE2+20.*SE3)/1120.$   
 $F24 = X2Y3*(1.+5.*SE1+15.*SE2)/840.$   
 $F15 = X2Y3*(1.+6.*SE1)/336.$   
 $F06 = X2Y3/56.$

C.

$T(1,1) = F00$   
 $T(1,2) = F10$   
 $T(1,3) = F01$   
 $T(1,4) = F20$   
 $T(1,5) = F11$   
 $T(1,6) = F02$   
 $T(1,7) = F30$   
 $T(1,8) = F21$   
 $T(1,9) = F12$   
 $T(1,10) = F03$   
 $T(2,2) = F20$   
 $T(2,3) = F11$   
 $T(2,4) = F30$   
 $T(2,5) = F21$   
 $T(2,6) = F12$   
 $T(2,7) = F40$   
 $T(2,8) = F31$   
 $T(2,9) = F22$   
 $T(2,10) = F13$   
 $T(3,3) = F02$   
 $T(3,4) = F21$   
 $T(3,5) = F12$   
 $T(3,6) = F03$   
 $T(3,7) = F31$   
 $T(3,8) = F22$   
 $T(3,9) = F13$   
 $T(3,10) = F04$   
 $T(4,4) = F40$   
 $T(4,5) = F31$   
 $T(4,6) = F22$   
 $T(4,7) = F50$   
 $T(4,8) = F41$   
 $T(4,9) = F32$   
 $T(4,10) = F23$   
 $T(5,5) = F22$   
 $T(5,6) = F13$

T(5,7) = F41  
T(5,8) = F32  
T(5,9) = F23  
T(5,10) = F14  
T(6,6) = F04  
T(6,7) = F32  
T(6,8) = F23  
T(6,9) = F14  
T(6,10) = F05  
T(7,7) = F60  
T(7,8) = F51  
T(7,9) = F42  
T(7,10) = F33  
T(8,8) = F42  
T(8,9) = F33  
T(8,10) = F24  
T(9,9) = F24  
T(9,10) = F15  
T(10,10) = F06

C

DO 60 I=1,10  
DO 60 J=I,10  
60 T(J,I) = T(I,J)  
CALL RTAPA (T,R,10,9,KT,KR)  
DO 85 I=1,9  
DO 85 J=1,9  
85 Z(I,J) = T(I,J)

C

RETURN  
END

```
SUBROUTINE M3C1 (X3,Y3,TH,RO,Z,KZ)
DIMENSION Z(KZ,1)
```

```
C
C SUBROUTINE TO CALCULATE FINITE ELEMENT...
C LUMPED MASS MATRIX
C FOR A RECTANGULAR SHEAR PANEL ELEMENT WITH UNRESTRAINED BOUNDARIES.
C MASS MATRIX IS IN LOCAL COORDINATE SYSTEM.
C THE LOCAL COORDINATE SYSTEM ASSUMES THE PANEL TO LIE IN AN X-Y PLANE
C WITH JOINT 1 AT THE X-Y ORIGIN, JOINT 2 LIES ALONG THE POSITIVE
C X AXIS, JOINT 3 IS IN THE POSITIVE X,Y DIRECTION, AND JOINT 4 LIES
C ALONG THE POSITIVE Y AXIS.
C LOCAL COORDINATE ORDER IS
C DX1,DX2,DX3,DX4, DY1,DY2,DY3,DY4
C WHERE DX,DY ARE TRANSLATIONS.
C DEVELOPED BY RL WOHLER. APRIL 1974.
C
C SUBROUTINE ARGUMENTS
C X3 = INPUT LOCAL X COORDINATE LOCATION OF JOINT 3.
C Y3 = INPUT LOCAL Y COORDINATE LOCATION OF JOINT 3.
C TH = INPUT PANEL THICKNESS.
C RO = INPUT MASS DENSITY.
C Z = OUTPUT MASS MATRIX. SIZE(8,8).
C KZ = INPUT ROW DIMENSION OF Z IN CALLING PROGRAM. MIN=8.
C
C CM = RO*TH*X3*Y3/4.0
C DO 10 J=1,8
C DO 10 I=1,8
10 Z(I,J) = 0.0
C DO 20 I=1,8
20 Z(I,1) = CM
C
C RETURN
C END
```





```
DO 114 I=4,6
114 Z(I,J) = W(2,2) -
RETURN
C
C CONSISTENT.
120 CALL MIA2 (A1,A2,RL,RO,W,2)
DO 122 I=1,3
122 Z(I,I) = W(1,1)
CALL EULER (EJ(1,1),E1,3)
CALL EULER (EJ(1,2),E2,3)
CALL ATXBB (E1,E2, 3,3,3, 3,3)
DO 124 I=1,3
DO 124 J=4,6
Z(I,J) = W(1,2)*E2(I,J-3)
124 Z(J,I) = Z(I,J)
DO 126 I=4,6
126 Z(I,1) = W(2,2)
RETURN
C
999 CALL ZZBUMB (6HMASIA ,NERROR)
END.
```



```
GO TO 999
C
C AXIAL=MIA1 (LUMPED), TORSION=MIC1 (LUMPED), BENDING=MIB1 (LUMPED).
110 CALL MIA1 (A1,A2,RL,RC,Z,KZ)
CALL MIC1 (PI1,PI2,RL,RC,Z(3,3),KZ)
CALL MIB1 (A1,A2,RL,RC,Z(5,5),KZ)
CALL MIB1 (A1,A2,RL,RC,Z(9,9),KZ)
GO TO 300
C
C AXIAL=MIA2 (LINEAR DISP), TORSION=MIC2 (LINEAR DISP),
C BENDING=MIB2 (CUBIC DISP).
120 CALL MIA2 (A1,A2,RL,RC,Z,KZ)
CALL MIC2 (PI1,PI2,RL,RC,Z(3,3),KZ)
CALL MIB2 (A1,A2,RL,RC,Z(5,5),KZ)
DO 125 J=7,8
DO 125 I=5,6
Z(I,J) =-Z(I,J)
125 Z(J,I) =-Z(J,I)
CALL MIB2 (A1,A2,RL,RC,Z(9,9),KZ)
C
300 CALL DDCS1F (CJ,EJ,W,KCJ,KEJ,KW)
CALL HTABA (Z,W,12,12,KZ,KW)
RETURN
C
999 CALL ZZBOMB (6PMAS1B ,NERROP)
END
```

```

SUBROUTINE MAS2 (CJ,EJ,TMAS,RO,NAMEM,Z,W1,W2,KCJ,KEJ,KZ,KW1,KW2)
DIMENSION CJ(KCJ,1), EJ(KEJ,1), Z(KZ,1), W1(KW1,1), W2(KW2,1)
DIMENSION IVEC(18)
DATA IVEC/1,2,6,7,8,12,13,14,18, 3,4,5,9,10,11,15,16,17/

```

```

C
C SUBROUTINE TO CALCULATE FINITE ELEMENT...
C MASS MATRIX
C FOR A COMBINED MEMBRANE-BENDING TRIANGLE PLATE ELEMENT WITH
C UNRESTRAINED BOUNDARIES.
C MASS MATRIX IS IN GLOBAL COORDINATE DIRECTIONS.
C GLOBAL COORDINATE ORDER IS
C (U,V,W,P,Q,R) JOINT 1, THEN JOINT 2, 3.
C WHERE U,V,W ARE TRANSLATIONS AND P,Q,R ARE ROTATIONS.
C EULER ANGLE CONVENTION IS GLOBAL X,Y,Z PERMUTATION.
C CALLS FORMA SUBROUTINES STABA,DCOS2,M2A1,M2A2,M2B1,M2B2,ZZBOMB.
C DEVELOPED BY WA BENFIELD, FL WOHLER. FEBRUARY 1973.
C LAST REVISION BY WA BENFIELD. MARCH 1976.
C
C SUBROUTINE ARGUMENTS
C CJ = INPUT MATRIX OF GLOBAL X,Y,Z COORDINATES AT TRIANGLE JOINTS.
C ROWS 1,2,3 CORRESPOND TO X,Y,Z COORDINATES.
C COLS 1,2,3 CORRESPOND TO JOINTS 1,2,3. SIZE(3,3).
C EJ = INPUT MATRIX OF EULER ANGLES (DEGREES) AT TRIANGLE JOINTS.
C ROWS 1,2,3 CORRESPOND TO GLOBAL X,Y,Z PERMUTATION.
C COLS 1,2,3 CORRESPOND TO JOINTS 1,2,3. SIZE(3,3).
C TMAS = INPUT EFFECTIVE MASS THICKNESS.
C RO = INPUT MASS DENSITY.
C NAMEM = INPUT TYPE OF MASS MATRIX WANTED.
C = M1, LUMPED.
C = M2, CONSISTENT.
C Z = OUTPUT MASS MATRIX. SIZE(18,18).
C W1 = INPUT WORK SPACE MATRIX. SIZE(18,18).
C W2 = INPUT WORK SPACE MATRIX. SIZE(10,10).
C KCJ = INPUT ROW DIMENSION OF CJ IN CALLING PROGRAM. MIN=3.
C KEJ = INPUT ROW DIMENSION OF EJ IN CALLING PROGRAM. MIN=3.
C KZ = INPUT ROW DIMENSION OF Z IN CALLING PROGRAM. MIN=18.
C KW1 = INPUT ROW DIMENSION OF W1 IN CALLING PROGRAM. MIN=18.
C KW2 = INPUT ROW DIMENSION OF W2 IN CALLING PROGRAM. MIN=10.
C
C NEPROR EXPLANATION
C 1 = DIMENSION SIZE EXCEEDED (KZ,KW1,KW2).
C 2 = NAMEM IMPROPERLY DEFINED.
C

```

NEPROR=1

```

IF (KZ .LT. 18 .OR. KW1 .LT. 18 .OR. KW2 .LT. 10) GO TO 999
DO 5 J=1,18
DO 5 I=1,18
5 Z(I,J) = 0.0
SL12 = SQRT((CJ(1,2)-CJ(1,1))**2 + (CJ(2,2)-CJ(2,1))**2
* (CJ(3,2)-CJ(3,1))**2)
SL23 = SQRT((CJ(1,3)-CJ(1,2))**2 + (CJ(2,3)-CJ(2,2))**2
* (CJ(3,3)-CJ(3,2))**2)
SL13 = SQRT((CJ(1,3)-CJ(1,1))**2 + (CJ(2,3)-CJ(2,1))**2
* (CJ(3,3)-CJ(3,1))**2)
X3 = (SL13**2+SL12**2-SL23**2)/(2.0*SL12)

```

```

Y3 = SQRT(SL13**2-X3**2)
IF (NAMEM .EQ. 6HM1 ) GO TO 110
IF (NAMEM .EQ. 6HM2 ) GO TO 120

```

NERROR=2

```

GO TO 999

```

```

C
C MEMBRANE = M2A1 (LUMPED), BENDING = M2F1 (LUMPED).

```

```

110 CALL M2A1 (SL12,Y3,TMAS,RO,W1,KW1)
CALL M2F1 (SL12,Y3,TMAS,RO,W1(10,10),KW1)
DO 115 IW=1,18
IZ = IVEC(IW)
115 Z(IZ,IZ) = W1(IW,IW)
RETURN

```

```

C
C MEMBRANE = M2A2 (CONSISTENT), BENDING = M2E2 (CONSISTENT).

```

```

120 CALL M2A2 (SL12,X3,Y3,TMAS,RO,Z,W1,W2,KZ,KW1,KW2)
CALL M2E2 (SL12,X3,Y3,TMAS,PO,Z(10,10),W1,W2,KZ,KW1,KW2)
CALL DCOS2 (CJ,EJ,W1,KCJ,KEJ,KW1)
CALL RTABA (Z,W1,18,18,KZ,KW1)
RETURN

```

```

C
999 CALL ZZEOMB (FMAS2 ,NERROR)
END

```

```

SUBROUTINE MAS3 (CJ,EJ,TMAS,RC,NAMEM,Z,W1,W2,KCJ,KEJ,KZ,KW1,KW2)
DIMENSION CJ(KCJ,1),EJ(KEJ,1),Z(KZ,1),W1(KW1,1),W2(KW2,1)
DIMENSION CW(3,3),EW(3,3),IV1(18),IV2(18),IV3(18),IV4(18),
* W3(10,10)
DATA IV1/ 1, 2, 3, 4, 5, 6, 7, 8, 9,10,11,12,13,14,15,16,17,18/,
* IV2/ 1, 2, 3, 4, 5, 6,13,14,15,16,17,18,19,20,21,22,23,24/,
* IV3/ 1, 2, 3, 4, 5, 6, 7, 8, 9,10,11,12,19,20,21,22,23,24/,
* IV4/ 7, 8, 9,10,11,12,13,14,15,16,17,18,19,20,21,22,23,24/
C
C SUBROUTINE TO CALCULATE FINITE ELEMENT...
C MASS MATRIX
C FOR A COMBINED MEMBRANE-BENDING QUADRILATERAL PLATE ELEMENT WITH
C UNRESTRAINED BOUNDARIES.
C MASS MATRIX IS IN GLOBAL COORDINATE DIRECTIONS.
C GLOBAL COORDINATE ORDER IS
C (U,V,W,P,Q,R) JOINT 1, THEN JOINT 2, 3, 4.
C WHERE U,V,W ARE TRANSLATIONS AND P,Q,R ARE ROTATIONS.
C EULER ANGLE CONVENTION IS GLOBAL X,Y,Z PERMUTATION.
C CALLS FORMA SUBROUTINES MAS2,EFVADD,ZZBOMB.
C DEVELOPED BY WA BENFIELD, RL WOHLER. FEBRUARY 1973.
C LAST REVISION BY WA BENFIELD. MARCH 1976.
C
C SUBROUTINE ARGUMENTS
C CJ = INPUT MATRIX OF GLOBAL X,Y,Z COORDINATES AT QUAD JOINTS.
C ROWS 1,2,3 CORRESPOND TO X,Y,Z COORDINATES.
C COLS 1,2,3,4 CORRESPOND TO JOINTS 1,2,3,4. SIZE(3,4).
C EJ = INPUT MATRIX OF EULER ANGLES (DEGREES) AT QUAD JOINTS.
C ROWS 1,2,3 CORRESPOND TO GLOBAL X,Y,Z PERMUTATION.
C COLS 1,2,3,4 CORRESPOND TO JOINTS 1,2,3,4. SIZE(3,4).
C TMAS = INPUT EFFECTIVE MASS THICKNESS.
C RC = INPUT MASS DENSITY.
C NAMEM = INPUT TYPE OF MASS MATRIX WANTED.
C = M1, LUMPED. 4 TRIANGLES, OVERLAP AVERAGE.
C = M2, CONSISTENT. 4 TRIANGLES, OVERLAP AVERAGE.
C Z = OUTPUT MASS MATRIX. SIZE(24,24).
C W1 = INPUT WORK SPACE MATRIX. SIZE(18,18).
C W2 = INPUT WORK SPACE MATRIX. SIZE(18,18).
C KCJ = INPUT ROW DIMENSION OF CJ IN CALLING PROGRAM. MIN=3.
C KEJ = INPUT ROW DIMENSION OF EJ IN CALLING PROGRAM. MIN=3.
C KZ = INPUT ROW DIMENSION OF Z IN CALLING PROGRAM. MIN=24.
C KW1 = INPUT ROW DIMENSION OF W1 IN CALLING PROGRAM. MIN=18.
C KW2 = INPUT ROW DIMENSION OF W2 IN CALLING PROGRAM. MIN=18.
C
C NERROR EXPLANATION
C 1 = DIMENSION SIZE EXCEEDED (KZ,KW1,KW2).
C 2 = NAMEM IMPROPERLY DEFINED.
C
C NERROR=1
IF (KZ .LT. 24 .OR. KW1 .LT. 18 .OR. KW2 .LT. 18) GO TO 999
DO 5 J=1,24
DO 5 I=1,24
5 Z(I,J) = 0.0
IF (NAMEM .EQ. 6HM1 ) GO TO 110
IF (NAMEM .EQ. 6HM2 ) GO TO 110
C NERROR=2

```

GO TO 990

C

```
110 DO 112 I=1,3
    CW(I,1) = CJ(I,1)
    EW(I,1) = EJ(I,1)
    CW(I,2) = CJ(I,2)
    EW(I,2) = EJ(I,2)
    CW(I,3) = CJ(I,3)
112 EW(I,3) = EJ(I,3)
    CALL MAS2 (CW,EW,TMAS,RO,NAMEM,W1,W2,W3,3,3,KW1,KW2,10)
    CALL REVADD (.5,W1,IV1,IV1,Z, 18,18,24,24, KW1,KZ)
    DO 113 I=1,3
    CW(I,1) = CJ(I,1)
    EW(I,1) = EJ(I,1)
    CW(I,2) = CJ(I,3)
    EW(I,2) = EJ(I,3)
    CW(I,3) = CJ(I,4)
113 EW(I,3) = EJ(I,4)
    CALL MAS2 (CW,EW,TMAS,RO,NAMEM,W1,W2,W3,3,3,KW1,KW2,10)
    CALL REVADD (.5,W1,IV2,IV2,Z, 18,18,24,24, KW1,KZ)
    DO 114 I=1,3
    CW(I,1) = CJ(I,1)
    EW(I,1) = EJ(I,1)
    CW(I,2) = CJ(I,2)
    EW(I,2) = EJ(I,2)
    CW(I,3) = CJ(I,4)
114 EW(I,3) = EJ(I,4)
    CALL MAS2 (CW,EW,TMAS,RO,NAMEM,W1,W2,W3,3,3,KW1,KW2,10)
    CALL REVADD (.5,W1,IV3,IV3,Z, 18,18,24,24, KW1,KZ)
    DO 115 I=1,3
    CW(I,1) = CJ(I,2)
    EW(I,1) = EJ(I,2)
    CW(I,2) = CJ(I,3)
    EW(I,2) = EJ(I,3)
    CW(I,3) = CJ(I,4)
115 EW(I,3) = EJ(I,4)
    CALL MAS2 (CW,EW,TMAS,RO,NAMEM,W1,W2,W3,3,3,KW1,KW2,10)
    CALL REVADD (.5,W1,IV4,IV4,Z, 18,18,24,24, KW1,KZ)
    RETURN
```

C

```
999 CALL ZZBOMB (5HMAS3 ,NERFOR)
    END
```





```
IZ = 3*(IW-1)
Z(IZ+1, IZ+1) = W1(IW, IW)
Z(IZ+2, IZ+2) = W1(IW, IW)
115 Z(IZ+3, IZ+3) = W1(IW, IW)
RETURN
```

```
C
999 CALL ZZBOMB (6HMAS3A ,NERROR)
END
```

```

SUBROUTINE PRESS (CJ,T,NJN,NCOL,KCJ,KW)
DIMENSION CJ(KCJ,1),T(KW,1)
DIMENSION A(8,8),JNM(3,42),VN(3),C(3,9),IV(3),JV(9)

```

```

C
C
C *** SUBROUTINE TO CALCULATE FLUID ELEMENT PRESSURE TRANSFORMATION
C *** MORE DESCRIPTIVE COMMENT CARDS TO BE ADDED AT A LATER DATE.
C *** DEVELOPED BY CAPT BODLEY, OCTOBER 1974.
C LAST REVISION BY C. S. BODLEY. NOVEMBER 1974.
C

```

```

DATA JNM /
* 1,2,3, 2,4,3, 3,4,1, 1,4,2, 1,2,3, 6,5,4,
* 2,6,3, 2,5,6, 4,5,2, 4,2,1, 3,6,4, 3,4,1,
* 3,5,6, 3,2,5, 4,5,1, 1,5,2, 1,3,6, 1,6,4,
* 1,5,2, 5,6,2, 5,8,7, 5,7,6, 4,7,8, 4,3,7,
* 1,2,4, 2,3,4, 1,4,5, 4,8,5, 2,6,7, 2,7,3,
* 1,5,6, 1,6,2, 5,8,6, 6,8,7, 3,7,8, 3,8,4,
* 1,2,3, 1,3,4, 1,8,5, 1,4,8, 2,6,3, 6,7,3 /

```

```

C
CALL ZERO (T,NJN,NCOL,KW)
LC = 18
NTF = 24
IF (NJN .EQ. 8) GO TO 5
LC = 4
NTF = 14
IF (NJN .EQ. 6) GO TO 5
LC = 0
NTF = 4
5 CONTINUE

```

```

C
DO 20 N=1,NTF
LOC = N + LC
J1 = JNM(1,LOC)
J2 = JNM(2,LOC)
J3 = JNM(3,LOC)
VN(1)=(CJ(2,J2)-CJ(2,J1))*(CJ(3,J3)-CJ(3,J1))
* -(CJ(3,J2)-CJ(3,J1))*(CJ(2,J3)-CJ(2,J1))
VN(2)=(CJ(3,J2)-CJ(3,J1))*(CJ(1,J3)-CJ(1,J1))
* -(CJ(1,J2)-CJ(1,J1))*(CJ(3,J3)-CJ(3,J1))
VN(3)=(CJ(1,J2)-CJ(1,J1))*(CJ(2,J3)-CJ(2,J1))
* -(CJ(2,J2)-CJ(2,J1))*(CJ(1,J3)-CJ(1,J1))
AC = SQRT(VN(1)*VN(1) + VN(2)*VN(2) + VN(3)*VN(3))
DO 25 I=1,3
25 VN(I) = VN(I)/AC
AC = AC/48.
IF (LOC .LT. 6) AC = 2.*AC
DO 30 I=1,3
IV(I) = JNM(1,LOC)
DO 30 J=1,3
JI = 3*I - 3 + J
JL = (IV(I) - 1)*3 + J
30 JV(JI) = JL

```

```

C
DO 35 L=1,3
DO 35 I=1,3

```

```
IL = I + 3*(L - 1)
DO 35 J=1,3
F = 1.
IF (L .EQ. J) F = 2.
35 C(J,IL) = F*VN(I)
CALL REVADD (AC,C,IV,JV,T,3,9,NJN,NCOL,3,KW)
20 CONTINUE
C
DO 40 I=1,NJN
DO 40 J=I,NJN
A(I,J) = 0.
DO 40 K=1,NCOL
40 A(I,J) = A(I,J) + T(I,K)*T(J,K)
CALL INVINP (A,A,NJN,8)
CALL MULTE (A,T,NJN,NJN,NCOL,8,KW)
C
RETURN
END
```

```

SUBROUTINE QUAD (XYZ,JDOF,EUL,NUTEL,NJ,
                NUTMX,NUTKX,NUTBX,NUTLT,NUTST,
                W,T,S,KX,KJ,KE,KW)
DIMENSION XYZ(KX,1),JDOF(KJ,1),EUL(KE,1),W(KW,1),T(KW,1),S(KW,1)
DIMENSION CJ(3,4),EJ(3,4),IV(24)
DATA NAMEL/6HQAD /,NRW,NRLT/24,24/, IBLNK/6H /, KCJ/3,
DATA NIT,NOT/5,6/
C
C SUBROUTINE TO CALCULATE (CN OPTION) FINITE ELEMENT ...
C MASS MATRICES AND IVECS (CN NUTMX),
C STIFFNESS MATRICES (SAME AS GLOBAL LOAD TRANSFORMATION MATRICES)
C AND IVECS (CN NUTKX),
C UNIT LOAD BUCKLING MATRICES AND IVECS (CN NUTBX), (NOT YET)
C LOCAL LOAD TRANSFORMATION MATRICES AND IVECS (CN NUTLT), (NOT YET)
C STRESS TRANSFORMATION MATRICES AND IVECS (CN NUTST), (NOT YET)
C FOR COMBINED MEMBRANE-BENDING QUADRILATERAL PLATE ELEMENTS.
C MASS, STIFFNESS, BUCKLING MATRICES ARE IN GLOBAL COORDINATE
C DIRECTIONS.
C GLOBAL COORDINATE ORDER IS
C (U,V,W,P,Q,R) JOINT 1, THEN JOINT 2, 3, 4.
C WHERE U,V,W ARE TRANSLATIONS AND P,Q,R ARE ROTATIONS.
C IVEC GIVES ELEMENT DOF INTO GLOBAL DOF. EXAMPLES...
C IVEC(6)=834 PLACES ELEMENT DOF 6 INTO GLOBAL DOF 834.
C IVEC(3)=0 OMTS ELEMENT DOF 3 FROM GLOBAL DOF. THIS CONSTRAINS
C ELEMENT DOF 3 TO ZERO MOTION.
C GLOBAL LOAD TRANSFORMATION MATRIX RELATES LOADS AT QUAD VERTICES IN
C GLOBAL COORDINATE DIRECTIONS TO DEFLECTIONS IN THE GLOBAL COORDINATE
C DIRECTIONS.
C ROW ORDER IN GLOBAL LOAD TRANSFORMATION MATRIX IS
C (PU,PV,PW,MP,MQ,MR) JOINT 1, THEN JOINT 2,3,4.
C WHERE P IS FORCE AND M IS MOMENT.
C LOCAL LOAD TRANSFORMATION MATRICES RELATES LOAD AT QUAD VERTICES IN
C LOCAL COORDINATE SYSTEM TO DEFLECTIONS IN THE GLOBAL COORDINATE
C DIRECTIONS.
C STRESS TRANSFORMATION MATRICES RELATES STRESS AT QUAD VERTICES IN
C LOCAL COORDINATE SYSTEM TO DEFLECTIONS IN THE GLOBAL COORDINATE
C DIRECTIONS.
C DATA ARRANGEMENT ON NUTMX, NUTKX, NUTBX, NUTLT, NUTST FOR EACH FINITE
C ELEMENT IS (W=M,K,P,LT,ST)
C WRITE (NUTWX) NAMEW,NEL,NR,NC,NAMEL,(IBLNK,I=1,5),
C ((W(I,J),I=1,NR),J=1,NC),(IVEC(I),I=1,NC)
C CALLS FORMA SUBROUTINES MAS3, PAGEHD, STF3, ZZPOMB.
C DEVELOPED BY WA BENFIELD, CS BODLFY, RL WOHLN. MARCH 1973.
C LAST REVISION BY RL WOHLN. MAY 1976.
C
C *****+*****
C INPUT DATA READ IN THIS SUBROUTINE FROM NUTEL. IF NUTEL = 5, DATA IS
C READ FROM CARDS.
C NAMEM,NAMEK,NAMELT,NAMEST,NAMEF FORMAT (5(A6,4X)
C PG,F,ANU FORMAT (3(5X,E10))
C TMACC,TMEMC,TRENC FORMAT (3(5X,E10))
C 20 NEL,J1,J2,J3,J4,TMASV,TMEMV,TEENV FORMAT (5I5,.E10)
C IF (J1 .EQ. 0) RETURN
C GO TO 20
C

```

C DEFINITION OF INPUT VARIABLES.

C NAMEM = TYPE OF MASS MATRIX WANTED.

C = M1, DIAGONAL LUMPED. OVERLAP AVERAGE OF FOUR TRIANGLES.

C = M2, CONSISTENT. OVERLAP AVERAGE OF FOUR TRIANGLES.

C = 6H OR 6HNO MASS, NO MASS MATRIX CALCULATED.

C NAMEK = TYPE OF STIFFNESS MATRIX WANTED.

C = K1, OVERLAP AVERAGE OF FOUR TRIANGLES.

C = 6H OR 6HNO STIF, NO STIFFNESS MATRIX CALCULATED.

C NAMELT = IDENTIFICATION NAME FOR LOAD TRANSFORMATION MATRICES.

C = 6H OR 6HNO LOAD, NO LOAD TRANSFORMATIONS CALCULATED.

C NAMEST = IDENTIFICATION NAME FOR STRESS TRANSFORMATION MATRICES.

C = 6H OR 6HNO STRS, NO STRESS TRANSFORMATIONS CALCULATED.

C NAMEB = TYPE OF BUCKLING MATRIX WANTED.

C = 6H OR 6HNO BUCK, NO BUCKLING MATRIX CALCULATED.

C RO = MASS DENSITY.

C E = YOUNGS MODULUS OF ELASTICITY.

C ANU = POISSONS RATIO. (E/2G)-1.

C TMASC = EFFECTIVE MASS THICKNESS, (CONSTANT).

C TMASV = EFFECTIVE MASS THICKNESS, (VARIABLE).

C IF .LE. 0., TMASC IS USED.

C TMEC = EFFECTIVE MEMBRANE THICKNESS, (CONSTANT).

C TMEMV = EFFECTIVE MEMBRANE THICKNESS, (VARIABLE).

C IF .LE. 0., TMEC IS USED.

C TBENC = EFFECTIVE BENDING THICKNESS, (CONSTANT).

C TBENV = EFFECTIVE BENDING THICKNESS, (VARIABLE).

C IF .LE. 0., TBENC IS USED.

C NEL = FINITE ELEMENT NUMBER. FOR REFERENCE ONLY, NOT USED IN  
CALCULATIONS. WRITTEN ON NUTMX, ETC.

C J1 = JOINT NUMBER AT QUADRILATERAL VERTEX 1.

C J2 = JOINT NUMBER AT QUADRILATERAL VERTEX 2.

C J3 = JOINT NUMBER AT QUADRILATERAL VERTEX 3.

C J4 = JOINT NUMBER AT QUADRILATERAL VERTEX 4.

C

C EXPLANATION OF INPUT FORMATS. NUMBER INDICATES CARD COLUMNS USED.

C I = INTEGER DATA, RIGHT ADJUSTED.

C E = DECIMAL POINT DATA, ANYWHERE IN FIELD. EXPONENT RIGHT ADJUSTED

C X = CARD COLUMNS SKIPPED.

C \*\*\*\*\*

C

C SUBROUTINE ARGUMENTS (ALL INPUT)

C XYZ = MATRIX OF JOINT GLOBAL X,Y,Z LOCATIONS. ROWS CORRESPOND  
TO JOINT NUMBERS. COLUMNS 1,2,3 CORRESPOND TO THE JOINT  
X,Y,Z LOCATIONS RESPECTIVELY. SIZE(NJ,3).

C JDOF = MATRIX OF JOINT GLOBAL DEGREES OF FREEDOM. ROWS CORRESPOND  
TO JOINT NUMBERS. COLUMNS 1,2,3 CORRESPOND TO THE JOINT  
TRANSLATION DOFS AND COLUMNS 4,5,6 CORRESPOND TO THE JOINT  
ROTATION DOFS. SIZE(NJ,6).

C EUL = MATRIX OF JOINT EULER ANGLES (DEGREES). ROWS CORRESPOND  
TO JOINT NUMBERS. COLUMNS 1,2,3 CORRESPOND TO THE  
GLOBAL X,Y,Z PERMUTATION. SIZE(NJ,3).

C NUTEL = LOGICAL NUMBER OF TAPE CONTAINING ELEMENT INPUT DATA FOR  
THIS SUBROUTINE. IF NUTEL = 5, DATA IS READ FROM CARDS.

C NJ = NUMBER OF JOINTS OR ROWS IN MATRICES (XYZ), (JDOF), (EUL).

C NUTMX = LOGICAL NUMBER OF UTILITY TAPE ON WHICH ELEMENT  
MASS MATRICES AND IVECS ARE OUTPUT.

C

```

C          NUTMX MAY BE ZERO IF MASS MATRIX IS NOT FORMED.
C          USES FORTRAN READ, WRITE.
C  NUTKX   = LOGICAL NUMBER OF UTILITY TAPE ON WHICH ELEMENT
C          STIFFNESS MATRICES (SAME AS GLOBAL LOADS TRANSFORMATION
C          MATRICES) AND IVECS ARE OUTPUT.
C          NUTKX MAY BE ZERO IF STIFFNESS MATRIX IS NOT FORMED.
C          USES FORTRAN READ, WRITE.
C  NUTBX   = LOGICAL NUMBER OF UTILITY TAPE ON WHICH ELEMENT UNIT LOAD
C          BUCKLING MATRICES AND IVECS ARE OUTPUT.
C          NUTEX MAY BE ZERO IF BUCKLING MATRIX IS NOT FORMED.
C          USES FORTRAN READ, WRITE.
C  NUTLT   = LOGICAL NUMBER OF UTILITY TAPE ON WHICH ELEMENT LOCAL
C          LOAD TRANSFORMATION MATRICES AND IVECS ARE OUTPUT.
C          NUTLT MAY BE ZERO IF LOAD TRANSFORMATIONS ARE NOT FORMED.
C          USES FORTRAN READ, WRITE.
C  NUTST   = LOGICAL NUMBER OF UTILITY TAPE ON WHICH ELEMENT
C          STRESS TRANSFORMATION MATRICES AND IVECS ARE OUTPUT.
C          NUTST MAY BE ZERO IF STRESS TRANSFORMATIONS ARE NOT FORMED.
C          USES FORTRAN READ, WRITE.
C  W       = MATRIX WORK SPACE. MIN SIZE(24,24).
C  T       = MATRIX WORK SPACE. MIN SIZE(24,24).
C  S       = MATRIX WORK SPACE. MIN SIZE(24,24).
C  KX      = ROW DIMENSION OF XYZ IN CALLING PROGRAM.
C  KJ      = ROW DIMENSION OF JDOF IN CALLING PROGRAM.
C  KE      = ROW DIMENSION OF EUL IN CALLING PROGRAM.
C  KW      = ROW DIMENSION OF W, T, AND S IN CALLING PROGRAM. MIN=24.
C
C  ERROR  EXPLANATION
C  1 = JOINT NUMBER GREATER THAN NUMBER OF JOINTS.
C  2 = MASS MATRIX FORMED, NUTMX .LE. ZERO.
C  3 = STIFFNESS MATRIX FORMED, NUTKX .LE. ZERO.
C  4 = LT MATRIX FORMED, NUTLT .LE. ZERO.
C  5 = ST MATRIX FORMED, NUTST .LE. ZERO.
C
C 1001 FORMAT (5(A6,4X))
C 1002 FORMAT (3(FX,F10.0))
C 1003 FORMAT (5I5,3E10.0)
C 2001 FORMAT (/25X 40HINPUT DATA FOR COMBINED MEMBRANE-BENDING
C          *          20H QUADRILATERAL PLATE ELEMENTS)
C 2002 FORMAT (/20X 40HINPUT DATA FOR COMBINED MEMBRANE-BENDING
C          *          41H QUADRILATERAL PLATE ELEMENTS (CONTINUED))
C 2003 FORMAT (/ 13X7HMASS = A6, 13X7HSTIF = A6, 6X13HLOAD TRANS = A6,
C          *          3X15HSTRESS TRANS = A6, 3X11HBUCKLING = A6,
C          *          / 15X4HEC = E10.3, 13X3HE = E10.3,
C          *          / 10X9HT(MASS) = E10.3, 12X4HNU = E10.3,
C          *          / 32X13HT(MEMBRANE) = E10.3,
C          *          / 33X12HT(BENDING) = E10.3,
C          *          /12X 7HELEMENT 5X 7HJOINT 1 5X 7HJOINT 2 5X 7HJOINT 3
C          *          5X 7HJOINT 4 5X 7HT(MASS) 6X 11HT(MEMBRANE)
C          *          5X 10HT(BENDING)
C          *          /12X 8HNUMBER 48X 3(5X 10H(VARIABLE) ) )
C 2004 FORMAT (12X 5(I5,7X),3(F10.0,5X) )
C 2005 FORMAT (12X 5(I5,7X) )
C
C READ AND WRITE FINITE ELEMENT DATA.

```

```

NLINE = 0
CALL PAGEHD
WRITE (NOT,2001)
READ (NUTEL,1001) NAMEM,NAMEK,NAMELT,NAMEST,NAMEB
READ (NUTEL,1002) RO,E,ANU
READ (NUTEL,1002) TMASC,TMEMC,TEENC
WRITE (NOT,2003) NAMEM,NAMEK,NAMELT,NAMEST,NAMEB,
* RO,E, TMASC,ANU, TMEMC,TEENC
20 READ (NUTEL,1003) NEL,J1,J2,J3,J4,TMASV,TMEMV,TEENV
NO THIK = 1
IF (TMASV.LE.0. .AND. TMEMV.LE.0. .AND. TEENV.LE.0.) NO THIK=0
IF (J1 .LE. 0) RETURN
NLINE = NLINE + 1
IF (NLINE .LE. 42) GO TO 30
CALL PAGEHD
WRITE (NOT,2002)
WRITE (NOT,2003) NAMEM,NAMEK,NAMELT,NAMEST,NAMEB,
* RO,E, TMASC,ANU, TMEMC,TEENC
NLINE = 0
30 IF (NO THIK.EQ.1)
*WRITE (NOT,2004) NEL, J1,J2,J3,J4,TMASV,TMEMV,TEENV
IF (NO THIK.EQ.0) WRITE (NOT,2005) NEL,J1,J2,J3,J4
NERROR=1
IF (J1.GT.NJ .OR. J2.GT.NJ .OR. J3.GT.NJ .OR. J4.GT.NJ) GO TO 999
C
C SET THICKNESSES.
TMAS = TMASC
TMEM = TMEMC
TEEN = TEENC
IF (TMASV.GT.0.) TMAS=TMASV
IF (TMEMV.GT.0.) TMEM=TMEMV
IF (TEENV.GT.0.) TEEN=TEENV
C
C FORM FINITE ELEMENT COORDINATE LOCATIONS, EULER ANGLES, REVADD IVEC.
DO 42 I=1,3
CJ(I,1) = XYZ(J1,I)
CJ(I,2) = XYZ(J2,I)
CJ(I,3) = XYZ(J3,I)
CJ(I,4) = XYZ(J4,I)
EJ(I,1) = -EUL(1,I)
EJ(I,2) = EUL(2,I)
EJ(I,3) = EUL(3,I)
42 EJ(I,4) = EUL(J4,I)
DO 44 I=1,6
IV1(I) = JDOF(J1,I)
IV1(I+6) = JDOF(J2,I)
IV1(I+12) = JDOF(J3,I)
44 IV1(I+18) = JDOF(J4,I)
C
C FORM MASS MATRIX (W).
IF (NAMEM.NE.6H .OR. NAMEM.EQ.6HNDMASS) GO TO 110
CALL MASS(CJ,EJ,TMAS,FC,NAMEM,W,I,S,KCJ,KCJ,KW,KW,KW)
NERROR=2
IF (NOIMX .LE. 0) GO TO 999
WRITE (NUTMX) NAMEM,NEL,NRW,NEW-NAMEL,(IPLNK,I=1,3),

```



```

C          ((W(I,J),I=1,NRW),J=1,NRW),(IV1(I),I=1,NRW)
C FORM STIFFNESS MATRIX (W), LOCAL LOAD TRANSFORMATION MATRIX (T),
C STRESS TRANSFORMATION MATRIX (S).
110 IF (NAMEK .EQ. 6H          .OR. NAMEK .EQ. 6HNOSTIF) GO TO 20
    CALL STFB (CJ,EJ,TEEM,TEEN,E,ANU,NAMEK,NAMEST,W,T,S,NRST,
*           K,CJ,KCJ,KW,KW,KW)
                                           NERROR=3
    IF (NUTKX .LE. 0) GO TO 999
    WRITE (NUTKX) NAMEK,NEL,NRW,NRW,NAMEL,(IBLNK,I=1,5),
*           ((W(I,J),I=1,NRW),J=1,NRW),(IV1(I),I=1,NRW)
    IF (NAMELT .EQ. 6H          .OR. NAMELT .EQ. 6HNOLOAD) GO TO 115
                                           NERROR=4
    IF (NUTLT .LE. 0) GO TO 999
    WRITE (NUTLT) NAMELT,NEL,NRST,NRW,NAMEL,(IBLNK,I=1,5),
*           ((T(I,J),I=1,NRST),J=1,NRW),(IV1(I),I=1,NRW)
115 IF (NAMEST .EQ. 6H          .OR. NAMEST .EQ. 6HNOSTRS) GO TO 20
                                           NERROR=5
    IF (NUTST .LE. 0) GO TO 999
    WRITE (NUTST) NAMEST,NEL,NRST,NRW,NAMEL,(IBLNK,I=1,5),
*           ((S(I,J),I=1,NRST),J=1,NRW),(IV1(I),I=1,NRW)
    GO TO 20
C
999 CALL ZZPOMP (6HQUAD ,NERROR)
    END

```

```

SUBROUTINE RECTSP (XYZ,JDOF,EUL,NUTFL,NJ,
*           NUTMX,NUTKX,NUTLT,NUTST,
*           W,T,S,KX,KJ,KE,KW)
DIMENSION XYZ(KX,1),JDOF(KJ,1),EUL(KE,1),W(KW,1),T(KW,1),S(KW,1)
DIMENSION CJ(3,4),FJ(3,4),IVI(12)
DATA NAMEL/6HRECTSP/,NRW,NRLT/12,8/,IBLNK/6H      /,KCJ/3/
DATA NIT,NOT/5,6/

C
C SUBROUTINE TO CALCULATE (ON OPTION) FINITE ELEMENT ...
C MASS MATRICES AND VECs (ON NUTMX),
C STIFFNESS MATRICES (SAME AS GLOBAL LOAD TRANSFORMATION MATRICES)
C AND IVECS (ON NUTKX),
C LOCAL LOAD TRANSFORMATION MATRICES AND IVECS (ON NUTLT),
C STRESS TRANSFORMATION MATRICES AND IVECS (ON NUTST),
C FOR RECTANGULAR SHEAR PANEL ELEMENTS.
C MASS, STIFFNESS MATRICES ARE IN GLOBAL COORDINATE DIRECTIONS.
C GLOBAL COORDINATE ORDER IS
C (U,V,W) JOINT 1, THEN JOINT 2, 3, 4.
C WHERE U,V,W ARE TRANSLATIONS.
C IVEC GIVES ELEMENT DOF INTO GLOBAL DOF. EXAMPLES...
C IVEC(6)=834 PLACES ELEMENT DOF 6 INTO GLOBAL DOF 834.
C IVEC(3)=0  OMITs ELEMENT DOF 3 FROM GLOBAL DOF. THIS CONSTRAINS
C ELEMENT DOF 3 TO ZERO MOTION.
C GLOBAL LOAD TRANSFORMATION MATRIX RELATES LOADS AT PANEL VERTICES IN
C GLOBAL COORDINATE DIRECTIONS TO DEFLECTIONS IN THE GLOBAL COORDINATE
C DIRECTIONS.
C ROW ORDER IN GLOBAL LOAD TRANSFORMATION MATRIX IS
C (PU,PV,PW) JOINT 1, THEN JOINT 2, 3, 4.
C WHERE P IS FORCE.
C LOCAL LOAD TRANSFORMATION MATRICES RELATES LOAD AT PANEL VERTICES IN
C LOCAL COORDINATE SYSTEM TO DEFLECTIONS IN THE GLOBAL COORDINATE
C DIRECTIONS.
C STRESS TRANSFORMATION MATRICES RELATES PANEL SHEAR STRESS (CONSTANT)
C IN LOCAL COORDINATE SYSTEM TO DEFLECTIONS IN THE GLOBAL COORDINATE
C DIRECTIONS.
C DATA ARRANGEMENT ON NUTMX, NUTKX, NUTLT, NUTST FOR EACH FINITE
C ELEMENT IS (W=M,K,LT,ST)
C WRITE (NUTWX) NAMEW,NEL,NR,NC,NAMEL,(IBLNK,I=1,5),
C           (IW(I,J),I=1,NP),J=1,NC),(IVEC(I),I=1,NC)
C CALLS FORMA SUBROUTINES MAS3A, PAGEHD, STF3A, ZZBOMB.
C DEVELOPED BY PL WOHLER. APRIL 1974.
C LAST REVISION BY WA BENFIELD. MARCH 1976.
C
C *****
C INPUT DATA READ IN THIS SUBROUTINE FROM NUTEL. IF NUTEL = 5, DATA IS
C READ FROM CARDS.
C NAMEM,NAMEK,NAMELT,NAMEST          FORMAT (4(A6,4X))
C PD,G                                FORMAT (2(5X,E10))
C TMS,TSTF                            FORMAT (2(5X,E10))
C 20 NEL,J1,J2,J3,J4                  FORMAT (5I5)
C IF (J1 .EQ. 0) RETURN
C GO TO 20
C
C DEFINITION OF INPUT VARIABLES.
C NAMEM = TYPE OF MASS MATRIX WANTED.

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C = M1, DIAGONAL LUMPED.  
 C = M2, CONSISTENT.  
 C = 6H OR 6HNO MASS, NO MASS MATRIX CALCULATED.  
 C NAMEK = TYPE OF STIFFNESS MATPIX WANTED.  
 C = K1, LINEAR DISPLACEMENT (CONSTANT STRAIN).  
 C = 6H OR 6HNO STIF, NO STIFFNESS MATRIX CALCULATED.  
 C NAMELT = IDENTIFICATION NAME FOR LOAD TRANSFORMATION MATRICES.  
 C = 6H OR 6HNO LOAD, NO LOAD TRANSFORMATIONS CALCULATED.  
 C NAMEST = IDENTIFICATION NAME FOR STRESS TRANSFORMATION MATRICES.  
 C = 6H OR 6HNO STRS, NO STRESS TRANSFORMATIONS CALCULATED.  
 C RD = MASS DENSITY.  
 C G = SHEAR MODULUS OF ELASTICITY.  
 C TMS = EFFECTIVE MASS THICKNESS.  
 C TSTF = EFFECTIVE STIFFNESS THICKNESS.  
 C NEL = FINITE ELEMENT NUMBER. FOR REFERENCE ONLY, NOT USED IN  
 C CALCULATIONS. WRITTEN ON NUTMX, ETC.  
 C J1 = JOINT NUMBER AT PANEL VERTEX 1.  
 C J2 = JOINT NUMBER AT PANEL VERTEX 2.  
 C J3 = JOINT NUMBER AT PANEL VERTEX 3.  
 C J4 = JOINT NUMBER AT PANEL VERTEX 4.  
 C  
 C EXPLANATION OF INPUT FORMATS. NUMBER INDICATES CARD COLUMNS USED.  
 C I = INTEGER DATA, RIGHT ADJUSTED.  
 C E = DECIMAL POINT DATA, ANYWHERE IN FIELD. EXPONENT RIGHT ADJUSTED.  
 C X = CARD COLUMNS SKIPPED.  
 C \*\*\*\*\*  
 C  
 C SUBROUTINE ARGUMENTS (ALL INPUT)  
 C XYZ = MATRIX OF JOINT GLOBAL X,Y,Z LOCATIONS. ROWS CORRESPOND  
 C TO JOINT NUMBERS. COLUMNS 1,2,3 CORRESPOND TO THE JOINT  
 C X,Y,Z LOCATIONS RESPECTIVELY. SIZE(NJ,3).  
 C JDOF = MATRIX OF JOINT GLOBAL DEGREES OF FREEDOM. ROWS CORRESPOND  
 C TO JOINT NUMBERS. COLUMNS 1,2,3 CORRESPOND TO THE JOINT  
 C TRANSLATION DOFS AND COLUMNS 4,5,6 CORRESPOND TO THE JOINT  
 C ROTATION DOFS. SIZE(NJ,6).  
 C EUL = MATRIX OF JOINT EULER ANGLES (DEGREES). ROWS CORRESPOND  
 C TO JOINT NUMBERS. COLUMNS 1,2,3 CORRESPOND TO THE  
 C GLOBAL X,Y,Z PERMUTATION. SIZE(NJ,3).  
 C NUTEL = LOGICAL NUMBER OF TAPE CONTAINING ELEMENT INPUT DATA FOR  
 C THIS SUBROUTINE. IF NUTEL = 5, DATA IS READ FROM CARDS.  
 C NJ = NUMBER OF JOINTS OR ROWS IN MATRICES (XYZ), (JDOF), (EUL).  
 C NUTMX = LOGICAL NUMBER OF UTILITY TAPE ON WHICH ELEMENT  
 C MASS MATRICES AND IVECS ARE OUTPUT.  
 C NUTMX MAY BE ZERO IF MASS MATRIX IS NOT FORMED.  
 C USES FORTRAN READ, WRITE.  
 C NUTKX = LOGICAL NUMBER OF UTILITY TAPE ON WHICH ELEMENT  
 C STIFFNESS MATRICES (SAME AS GLOBAL LOADS TRANSFORMATION  
 C MATRICES) AND IVECS ARE OUTPUT.  
 C NUTKX MAY BE ZERO IF STIFFNESS MATRIX IS NOT FORMED.  
 C USES FORTRAN READ, WRITE.  
 C NUTLT = LOGICAL NUMBER OF UTILITY TAPE ON WHICH ELEMENT LOCAL  
 C LOAD TRANSFORMATION MATRICES AND IVECS ARE OUTPUT.  
 C NUTLT MAY BE ZERO IF LOAD TRANSFORMATIONS ARE NOT FORMED.  
 C USES FORTRAN READ, WRITE.  
 C NUTST = LOGICAL NUMBER OF UTILITY TAPE ON WHICH ELEMENT

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C          STRESS TRANSFORMATION MATRICES AND IVECS ARE OUTPUT.
C          NUTST MAY BE ZERO IF STRESS TRANSFORMATIONS ARE NOT FORMED.
C          USES FORTRAN READ, WRITE.
C  W       = MATFIX WORK SPACE. MIN SIZE(12,12).
C  T       = MATFIX WORK SPACE. MIN SIZE(12,12).
C  S       = MATFIX WORK SPACE. MIN SIZE(12,12).
C  KX      = ROW DIMENSION OF XYZ IN CALLING PROGRAM.
C  KJ      = ROW DIMENSION OF JOOF IN CALLING PROGRAM.
C  KE      = ROW DIMENSION OF EUL IN CALLING PROGRAM.
C  KW      = ROW DIMENSION OF W, T, AND S IN CALLING PROGRAM. MIN=12.
C
C          NERROR  EXPLANATION
C  1 = INPUT JOINT NUMBER EXCEEDS MAXIMUM ALLOWABLE NUMBER OF JOINTS.
C  2 = NUTMX NON POSITIVE.
C  3 = NUTKX NON POSITIVE.
C  4 = NUTLT NON POSITIVE.
C  5 = NUTST NON POSITIVE.
C
1001 FORMAT (4(A6,4X))
1002 FORMAT (2(5X,E10.0))
1003 FORMAT (5I5)
2001 FORMAT (/ / 38X 47HINPUT DATA FOR RECTANGULAR SHEAR PANEL ELEMENTS)
2002 FORMAT (/ / 32X 47HINPUT DATA FOR RECTANGULAR SHEAR PANEL ELEMENTS
*           12H (CONTINUED))
2003 FORMAT (/ 14X7HMASS = A6, 14X7HSTIF = A6, 11X13HLOAD TRANS = A6,
*           8X15HSTRESS TRANS = A6,
*           / 16X4HRO = E10.3, 14X3HG = E10.3,
*           / 11X9HT(MASS) = E10.3, 8X9HT(STIF) = E10.3,
*           / / 18X7HELEMENT 13X7HJOINT 1 13X7HJOINT 2 13X7HJOINT 3
*           13X7HJOINT 4 / 18X6HNUMBER)
2004 FORMAT (18X,5(15,15X))
C
C  READ AND WRITE FINITE ELEMENT DATA.
      NLINE = 0
      CALL PAGEHD
      WRITE (NCT,2001)
      READ (NUTFL,1001) NAMEM,NAMEK,NAMELT,NAMEST
      READ (NUTFL,1002) RO,G
      READ (NUTFL,1002) TMAS,TSTF
      WRITE (NCT,2003) NAMEM,NAMEK,NAMELT,NAMEST,RO,G,TMAS,TSTF
20  READ (NUTFL,1003) NEL,J1,J2,J3,J4
      IF (J1 .LE. 0) RETURN
      NLINE = NLINE + 1
      IF (NLINE .LE. 42) GO TO 30
      CALL PAGEHD
      WRITE (NCT,2002)
      WRITE (NCT,2003) NAMEM,NAMEK,NAMELT,NAMEST,RO,G,TMAS,TSTF
      NLINE = 0
30  WRITE (NCT,2004) NEL,J1,J2,J3,J4
                                                    NERROR=1
      IF (J1.GT.NJ .OR. J2.GT.NJ .OR. J3.GT.NJ .OR. J4.GT.NJ) GO TO 999
C
C  FORM FINITE ELEMENT COORDINATE LOCATIONS, EULER ANGLES, REVADD IVEC.
      DD 42 I=1,3
      CJ(I,1) = XYZ(J1,I)

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CJ(I,2) = XYZ(J2,I)
CJ(I,3) = XYZ(J3,I)
CJ(I,4) = XYZ(J4,I)
EJ(I,1) = EUL(J1,I)
EJ(I,2) = EUL(J2,I)
EJ(I,3) = EUL(J3,I)
42 EJ(I,4) = EUL(J4,I)
DO 44 I=1,3
  IV1(I)   = JDOF(J1,I)
  IV1(I+3) = JDOF(J2,I)
  IV1(I+6) = JDOF(J3,I)
44 IV1(I+9) = JDOF(J4,I)
C
C FORM MASS MATRIX (W).
  IF (NAMEM .EQ. 6H      .OR. NAMEM .EQ. 6HNCMASS) GO TO 110
  CALL MASBA (CJ,EJ,TMAS,RO,NAMEM,W,T,S,KCJ,KCJ,KW,KW,KW)
                                                                NERROR=2
  IF (NUTMX .LE. 0) GO TO 999
  WRITE (NUTMX) NAMEM,NEL,NRW,NRW,NAMEL,(IBLNK,I=1,5),
*           ((W(I,J),I=1,NRW),J=1,NRW),(IV1(I),I=1,NRW)
C
C FORM STIFFNESS MATRIX (W), LOCAL LOAD TRANSFORMATION MATRIX (T),
C STRESS TRANSFORMATION MATRIX (S).
110 IF (NAMEK .EQ. 6H      .OR. NAMEK .EQ. 6HNCSTIF) GO TO 20
  CALL STFBA (CJ,EJ,TSTF,G,NAMEK,NAMEST,W,T,S,NRST,
*           KCJ,KCJ,KW,KW,KW)
                                                                NERROR=3
  IF (NUTKX .LE. 0) GO TO 999
  WRITE (NUTKX) NAMEK,NEL,NRW,NRW,NAMEL,(IBLNK,I=1,5),
*           ((W(I,J),I=1,NRW),J=1,NRW),(IV1(I),I=1,NRW)
  IF (NAMELT .EQ. 6H      .OR. NAMELT .EQ. 6HNCLOAD) GO TO 115
                                                                NERROR=4
  IF (NUTLT .LE. 0) GO TO 999
  WRITE (NUTLT) NAMELT,NEL,NRST,NRW,NAMEL,(IBLNK,I=1,5),
*           ((T(I,J),I=1,NRST),J=1,NRW),(IV1(I),I=1,NRW)
115 IF (NAMEST .EQ. 6H      .OR. NAMEST .EQ. 6HNCSTRS) GO TO 20
                                                                NERROR=5
  IF (NUTST .LE. 0) GO TO 999
  WRITE (NUTST) NAMEST,NEL,NRST,NRW,NAMEL,(IBLNK,I=1,5),
*           ((S(I,J),I=1,NRST),J=1,NRW),(IV1(I),I=1,NRW)
  GO TO 20
C
999 CALL ZZBOME (6HRECTSP,NERRGR)
  END

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SUBROUTINE STF1A (CJ,EJ,A1,A2,E,NAMEK,NAMEST,S,TL,TS,NRST,
*              KCJ,KEJ,KS,KTL,KTS)
DIMENSION CJ(KCJ,1), EJ(KEJ,1), S(KS,1), TL(KTL,1), TS(KTS,1)
C
C SUBROUTINE TO CALCULATE FINITE ELEMENT...
C STIFFNESS MATRIX (SAME AS GLOBAL LOAD TRANSFORMATION MATRIX),
C LOCAL LOAD TRANSFORMATION MATRIX,
C STRESS TRANSFORMATION MATRIX,
C FOR AN AXIAL ROD ELEMENT WITH UNRESTRAINED BOUNDARIES.
C ROD MAY BE LINEARLY TAPERED OR UNIFORM.
C STIFFNESS MATRIX IS IN GLOBAL COORDINATE DIRECTIONS.
C GLOBAL COORDINATE ORDER IS
C (U,V,W) JOINT 1, THEN JOINT 2.
C WHERE U,V,W ARE TRANSLATIONS.
C GLOBAL LOAD TRANSFORMATION MATRIX RELATES LOADS AT ROD ENDS IN GLOBAL
C COORDINATE DIRECTIONS TO DEFLECTIONS IN THE GLOBAL COORDINATE
C DIRECTIONS.
C ROW ORDER IN GLOBAL LOAD TRANSFORMATION MATRIX IS
C (PU,PV,PW) JOINT 1, THEN JOINT 2.
C WHERE P IS FORCE.
C LOCAL LOAD TRANSFORMATION MATRIX RELATES LOADS AT ROD ENDS IN LOCAL
C COORDINATE SYSTEM TO DEFLECTIONS IN THE GLOBAL COORDINATE DIRECTIONS.
C ROW ORDER IN LOCAL LOAD TRANSFORMATION MATRIX IS
C PX1,PX2
C WHERE PX IS AXIAL FORCE.
C PX1(-), PX2(+) IS TENSION. PX1(+), PX2(-) IS COMPRESSION.
C STRESS TRANSFORMATION MATRIX RELATES STRESS AT ROD ENDS IN LOCAL
C COORDINATE SYSTEM TO DEFLECTIONS IN THE GLOBAL COORDINATE DIRECTIONS.
C ROW ORDER IN STRESS TRANSFORMATION MATRIX IS
C SIGMA-X1, SIGMA-X2
C WHERE SIGMA IS NORMAL STRESS.
C SX1(-), SX2(+) IS TENSION. SX1(+), SX2(-) IS COMPRESSION.
C EULER ANGLE CONVENTION IS GLOBAL X,Y,Z PERMUTATION.
C CALLS FOR SUBROUTINES ATXBA1, DCOS1A, KIA1, MULTA, ZZ60MB.
C DEVELOPED BY RL WOHLER. SEPTEMBER 1972.
C LAST REVISION BY WA BENFIELD. MARCH 1976.
C
C SUBROUTINE ARGUMENTS
C CJ = INPUT MATRIX OF GLOBAL X,Y,Z COORDINATES AT ROD JOINTS.
C ROWS 1,2,3 CORRESPOND TO X,Y,Z COORDINATES.
C COLS 1,2 CORRESPOND TO JOINTS 1,2. SIZE(3,2).
C EJ = INPUT MATRIX OF EULER ANGLES (DEGREES) AT ROD JOINTS.
C ROWS 1,2,3 CORRESPOND TO GLOBAL X,Y,Z PERMUTATION.
C COLS 1,2 CORRESPOND TO JOINTS 1,2. SIZE(3,2).
C A1 = INPUT CROSS-SECTION AREA AT ROD END 1.
C A2 = INPUT CROSS-SECTION AREA AT ROD END 2.
C E = INPUT YOUNG'S MODULUS OF ELASTICITY.
C NAMEK = INPUT TYPE OF STIF MATRIX WANTED.
C = K1, CONSTANT AXIAL FORCE ASSUMED.
C NAMEST = INPUT OPTION FOR STRESS TRANSFORMATION.
C = 6H OR 6HNOSTRS ,NO STRESS TRANS CALCULATED.
C S = OUTPUT STIFFNESS MATRIX (SAME AS GLOBAL LOAD TRANSFORMATION
C MATRIX). SIZE(6,6).
C TL = OUTPUT LOCAL LOAD TRANSFORMATION MATRIX. SIZE(2,6).
C TS = OUTPUT STRESS TRANSFORMATION MATRIX. SIZE(NRST,6).

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C NRST = OUTPUT NUMBER OF ROWS IN STRESS TRANSFORMATION MATRIX.
C KCJ = INPUT ROW DIMENSION OF CJ IN CALLING PROGRAM. MIN=3.
C KEJ = INPUT ROW DIMENSION OF EJ IN CALLING PROGRAM. MIN=3.
C KS = INPUT ROW DIMENSION OF S IN CALLING PROGRAM. MIN=6.
C KTL = INPUT ROW DIMENSION OF TL IN CALLING PROGRAM. MIN=2.
C KTS = INPUT ROW DIMENSION OF TS IN CALLING PROGRAM. MIN=NRST.
C
C ERROR EXPLANATION
C 1 = SIZE LIMITATION EXCEEDED.
C 2 = NAMEK IMPROPERLY DEFINED.
C
C NRST = 2
C
C NERROR=1
IF (KS .LT. 6 .OR. KTL .LT. 2 .OR. KTS .LT. NRST) GO TO 999
RL = SQRT((CJ(1,2)-CJ(1,1))**2 + (CJ(2,2)-CJ(2,1))**2
* + (CJ(3,2)-CJ(3,1))**2)
IF (NAMEK .EQ. 6HK1 ) GO TO 110
C NERROR=2
GO TO 999
110 CALL KIA1 (A1,A2,RL,E,TL,TS,KTL,KTS) TL=K
C
CALL DCOS1A (CJ,EJ,S,KCJ,KEJ,KS) S=DC
CALL MULTA (TL,S, 2,2,6, KTL,KS)
IF (NAMEST .EQ. 6H .OR. NAMEST .EQ. 6HNOSTRS) GO TO 210
CALL MULTA (TS,S,NRST,2,6, KTS,KS)
210 CALL ATXBA1 (S,TL, 2,6, KS,KTL)
RETURN
C
999 CALL ZZBOMB (6HSTF1A ,NERROR)
END

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SUBROUTINE STF1B (CJ,EJ,KODE,A1,A2,TJ1,TJ2,R1Z1,B1Z2,B1Y1,B1Y2,
*           R1,R2,CY1,CY2,CZ1,CZ2,SF,E,G,NAMEK,NAMEST,
*           S,TL,TS,NFST,KCJ,KEJ,KS,KTL,KTS)
DIMENSION CJ(KCJ,1),EJ(KEJ,1),KODE(1),S(KS,1),TL(KTL,1),TS(KTS,1)
C
C SUBROUTINE TO CALCULATE FINITE ELEMENT...
C STIFFNESS MATRIX (SAME AS GLOBAL LOAD TRANSFORMATION MATRIX),
C LOCAL LOAD TRANSFORMATION MATRIX,
C STRESS TRANSFORMATION MATRIX,
C FOR A COMBINED AXIAL-TORSION-BENDING BAR ELEMENT WITH UNRESTRAINED
C BOUNDARIES.
C BAR MAY BE LINEARLY TAPERED OR UNIFORM.
C STIFFNESS MATRIX IS IN GLOBAL COORDINATE DIRECTIONS.
C GLOBAL COORDINATE ORDER IS
C (U,V,W,P,Q,R) JOINT 1, THEN JOINT 2
C WHERE U,V,W ARE TRANSLATIONS AND P,Q,R ARE ROTATIONS.
C GLOBAL LOAD TRANSFORMATION MATRIX RELATES LOADS AT BAR ENDS IN GLOBAL
C COORDINATE DIRECTIONS TO DEFLECTIONS IN THE GLOBAL COORDINATE
C DIRECTIONS.
C ROW ORDER IN GLOBAL LOAD TRANSFORMATION MATRIX IS
C (PU,PV,PW,MP,MQ,MR) JOINT 1, THEN JOINT 2.
C WHERE P IS FORCE AND M IS MOMENT.
C LOCAL LOAD TRANSFORMATION MATRIX RELATES LOADS AT BAR ENDS IN LOCAL
C COORDINATE SYSTEM TO DEFLECTIONS IN THE GLOBAL COORDINATE DIRECTIONS.
C ROW ORDER IN LOCAL LOAD TRANSFORMATION MATRIX IS
C PX1,PX2,MX1,MX2,PY1,PY2,MZ1,MZ2,PZ1,PZ2,MY1,MY2
C WHERE P IS FORCE AND M IS MOMENT.
C STRESS TRANSFORMATION MATRIX RELATES STRESS AT BAR ENDS IN LOCAL
C COORDINATE SYSTEM TO DEFLECTIONS IN THE GLOBAL COORDINATE DIRECTIONS.
C ROW ORDER IN STRESS TRANSFORMATION MATRIX IS
C PX1/A1,PX2/A2, MX1*R1/TJ1,MX2*R2/TJ2,
C PY1/A1,PY2/A2,MZ1*CY1/B1Z1,MZ2*CY2/B1Z2,
C PZ1/A1,PZ2/A2,MY1*CZ1/B1Y1,MY2*CZ2/B1Y2
C WHERE P IS FORCE AND M IS MOMENT.
C EULER ANGLE CONVENTION IS GLOBAL X,Y,Z PERMUTATION.
C CALLS FORMA SUBROUTINES ATXBA1,DCOS1B,K1A1,K1B1,K1C1,MULTA,ZZBOMB.
C DEVELOPED BY RL WOHLER. FEBRUARY 1973.
C LAST REVISION BY RL WOHLER. APRIL 1976.
C
C SUBROUTINE ARGUMENTS
C CJ = INPUT MATRIX OF GLOBAL X,Y,Z COORDINATES AT BAR JOINTS.
C ROWS 1,2,3 CORRESPOND TO X,Y,Z COORDINATES.
C COLS 1,2 CORRESPOND TO JOINTS 1,2. COL 3 CORRESPONDS
C TO REFERENCE POINT TO DEFINE LOCAL XY PLANE. SIZE(3,3).
C EJ = INPUT MATRIX OF EULER ANGLES (DEGREES) AT BAR JOINTS.
C ROWS 1,2,3 CORRESPOND TO GLOBAL X,Y,Z PERMUTATION.
C COLS 1,2 CORRESPOND TO JOINTS 1,2. SIZE(3,2).
C KODE = INPUT OPTION CODE FOR AXIAL, TORSION, BENDING 2, BENDING Y
C LOCAL STIFFNESS. IF BLANK, ALL FOUR ARE CALCULATED.
C SIZE(4).
C KODE(1)=A , LOCAL STIFFNESS MATRIX IS CALCULATED
C FOR AXIAL (ALONG LOCAL X-AXIS).
C KODE(2)=T , LOCAL STIFFNESS MATRIX IS CALCULATED
C FOR TORSION (ABOUT LOCAL X-AXIS).
C KODE(3)=BZ, LOCAL STIFFNESS MATRIX IS CALCULATED

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5 TS(I,J) = 0.0
  RL = SQRT((CJ(1,2)-CJ(1,1))**2 + (CJ(2,2)-CJ(2,1))**2
*          + (CJ(3,2)-CJ(3,1))**2)
  KODEA = 1
  KODET = 1
  KODEBZ = 1
  KODEBY = 1
  IF (KODE(1).EQ.1H .AND. KODE(2).EQ.1H .AND.
*     KODE(3).EQ.2H .AND. KODE(4).EQ.2H ) GO TO 10
  IF (KODE(1) .NE. 1HA ) KODEA = 0
  IF (KODE(2) .NE. 1HT ) KODET = 0
C LAST HALF OF NEXT TWO CARDS ALLOW FOR OLD DATA. INSERTED APRIL 1976.
  IF (KODE(3) .NE. 2HBZ .AND. KODE(3) .NE. 2HBY) KODEBZ = 0
  IF (KODE(4) .NE. 2HBY .AND. KODE(4) .NE. 2HBZ) KODEBY = 0
10 IF (NAMEK .EQ. 6HK1 ) GO TO 110
                                                    NERROR=2
  GO TO 999

C
C AXIAL = K1A1 (CONSTANT FORCE), TORSION = K1C1 (CONSTANT TORQUE),
C BENDING = K1B1 (CONSTANT SHEAR, LINEAR BENDING MOMENT).
110 IF (KODEA .EQ. 1) CALL K1A1 (A1,A2,RL,F,TL,TS,KTL,KTS)
  IF (KODET .EQ. 1) CALL K1C1 (TJ1,TJ2,R1,R2,RL,G,TL(3,3),TS(3,3),
*                               KTL,KTS)
  IF (KODEBZ .EQ. 1) CALL K1B1 (BI21,BI22,CY1,CY2,A1,A2,SF,RL,E,G,
*                               TL(5,5),TS(5,5),KTL,KTS)
  DO 115 J=7,8
  DO 115 I=5,6
  TL(I,J) =-TL(I,J)
  TS(I,J) =-TS(I,J)
  TL(J,I) =-TL(J,I)
115 TS(J,I) =-TS(J,I)
  IF (KODEBY .EQ. 1) CALL K1B1 (BIY1,BIY2,CZ1,CZ2,A1,A2,SF,RL,E,G,
*                               TL(9,9),TS(9,9),KTL,KTS)
                                                    TL=K

C
  CALL DCOS1B (CJ,EJ,S,KCJ,KEJ,KS)
                                                    S=DC
  CALL MULTA (TL,S, 12,12,12, KTL,KS)
  IF (NAMEST .EQ. 6H .OR. NAMEST .EQ. 6HNOSTRS) GO TO 210
  CALL MULTA (TS,S, NRST,12,12, KTS,KS)
210 CALL ATXBA1 (S,TL, 12,12, KS,KTL)
  RETURN

C
999 CALL ZZBCMB (6HSTF1B ,NERROR)
  END

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SUBROUTINE STF2 (CJ,EJ,TMEM,TBEN,E,ANU,NAMEK,NAMEST,S,TL,TS,NRST,
*              KCJ,KEJ,KS,KTL,KTS)
DIMENSION CJ(KCJ,1), EJ(KEJ,1), S(KS,1), TL(KTL,1), TS(KTS,1)
C
C SUBROUTINE TO CALCULATE FINITE ELEMENT...
C STIFFNESS MATRIX (SAME AS GLOBAL LOAD TRANSFORMATION MATRIX),
C LOCAL LOAD TRANSFORMATION MATRIX,
C STRESS TRANSFORMATION MATRIX,
C FOR A COMBINED MEMBRANE-BENDING TRIANGLE PLATE ELEMENT WITH
C UNRESTRAINED BOUNDARIES.
C STIFFNESS MATRIX IS IN GLOBAL COORDINATE DIRECTIONS.
C GLOBAL COORDINATE ORDER IS
C (U,V,W,P,Q,R) JOINT 1, THEN JOINT 2, 3.
C WHERE U,V,W ARE TRANSLATIONS AND P,Q,R ARE ROTATIONS.
C GLOBAL LOAD TRANSFORMATION MATRIX RELATES LOADS AT TRNGL VERTICES IN
C GLOBAL COORDINATE DIRECTIONS TO DEFLECTIONS IN THE GLOBAL COORDINATE
C DIRECTIONS.
C ROW ORDER IN GLOBAL LOAD TRANSFORMATION MATRIX IS
C (PU,PV,PW,MP,MQ,MR) JOINT 1, THEN JOINT 2,3.
C WHERE P IS FORCE AND M IS MOMENT.
C LOCAL LOAD TRANSFORMATION MATRIX RELATES LOADS AT TRNGL VERTICES IN
C LOCAL COORDINATE SYSTEM TO DEFLECTIONS IN THE GLOBAL COORDINATE
C DIRECTIONS.
C ROW ORDER IN LOCAL LOAD TRANSFORMATION MATRIX IS
C (PX,PY,MZ) JOINT 1 THEN 2,3, NEXT
C (PZ,MX,MY) JOINT 1 THEN 2,3.
C WHERE P IS FORCE AND M IS MOMENT.
C STRESS TRANSFORMATION MATRIX RELATES STRESS AT TRNGL VERTICES IN LOCAL
C COORDINATE SYSTEM TO DEFLECTIONS IN THE GLOBAL COORDINATE DIRECTIONS.
C ROW ORDER IN STRESS TRANSFORMATION MATRIX IS
C (SIGMA-X,SIGMA-Y,TAU-XY) FOR (Z=TBEN/2) AT JOINT 1,
C THEN JOINT 2,3.
C (SIGMA-X,SIGMA-Y,TAU-XY) FOR (Z=-TBEN/2) AT JOINT 1,
C THEN JOINT 2,3.
C WHERE SIGMA IS NORMAL STRESS AND TAU IS SHEAR STRESS.
C EULER ANGLE CONVENTION IS GLOBAL X,Y,Z PERMUTATION.
C CALLS FORMA SUBROUTINES ATXBA1,DCOS2,K2A1,K2B1,MULTA,ZZBOMB.
C DEVELOPED BY WA BENFIELD. FEBRUARY 1973.
C LAST REVISION BY WA BENFIELD. MARCH 1976.
C
C SUBROUTINE ARGUMENTS
C CJ = INPUT MATRIX OF GLOBAL X,Y,Z COORDINATES AT TRIANGLE JOINTS.
C ROWS 1,2,3 CORRESPOND TO X,Y,Z COORDINATES.
C COLS 1,2,3 CORRESPOND TO JOINTS 1,2,3. SIZE(3,3).
C EJ = INPUT MATRIX OF EULER ANGLES (DEGREES) AT TRIANGLE JOINTS.
C ROWS 1,2,3 CORRESPOND TO GLOBAL X,Y,Z PERMUTATION.
C COLS 1,2,3 CORRESPOND TO JOINTS 1,2,3. SIZE(3,3).
C TMEM = INPUT EFFECTIVE MEMBRANE THICKNESS.
C TBEN = INPUT EFFECTIVE BENDING THICKNESS.
C E = INPUT YOUNGS MODULUS OF ELASTICITY.
C ANU = INPUT POISSONS RATIO. (E/2G)-1.
C NAMEK = INPUT TYPE OF STIF MATRIX WANTED.
C = K1, USES K2A1 FOR MEMBRANE, K2B1 FOR BENDING.
C NAMEST = INPUT OPTION FOR STRESS TRANSFORMATION.
C = 6H OR 6HNDSTRS ,NO STRESS TRANS CALCULATED.

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C S      = OUTPUT STIFFNESS MATRIX (SAME AS GLOBAL LOAD TRANSFORMATION
C          MATRIX). SIZE(18,18).
C TL     = OUTPUT LOCAL LOAD TRANSFORMATION MATRIX. SIZE(18,18).
C TS     = OUTPUT STRESS TRANSFORMATION MATRIX. SIZE(NRST,18).
C NRST   = OUTPUT NUMBER OF ROWS IN STRESS TRANSFORMATION MATRIX.
C KCJ    = INPUT ROW DIMENSION OF CJ IN CALLING PROGRAM.
C KEJ    = INPUT ROW DIMENSION OF EJ IN CALLING PROGRAM.
C KS     = INPUT ROW DIMENSION OF S IN CALLING PROGRAM. MIN=18.
C KTL    = INPUT ROW DIMENSION OF TL IN CALLING PROGRAM. MIN=18.
C KTS    = INPUT ROW DIMENSION OF TS IN CALLING PROGRAM. MIN=NRST.
C
C      NERROR EXPLANATION
C 1 = SIZE LIMITATION EXCEEDED.
C 2 = NAMEK IMPROPERLY DEFINED.
C
      NRST = 18
                                                    NERROR=1
      IF (KS .LT. 18 .OR. KTL .LT. 18 .OR. KTS .LT. NRST) GO TO 999
      DO 5 J=1,18
      DO 5 I=1,18
      TL(I,J) = 0.0
5  TS(1,J) = 0.0
      SL12 = SQRT((CJ(1,2)-CJ(1,1))**2 + (CJ(2,2)-CJ(2,1))**2
      *          + (CJ(3,2)-CJ(3,1))**2)
      SL23 = SQRT((CJ(1,3)-CJ(1,2))**2 + (CJ(2,3)-CJ(2,2))**2
      *          + (CJ(3,3)-CJ(3,2))**2)
      SL13 = SQRT((CJ(1,3)-CJ(1,1))**2 + (CJ(2,3)-CJ(2,1))**2
      *          + (CJ(3,3)-CJ(3,1))**2)
      X3   = (SL13**2+SL12**2-SL23**2)/(2.0*SL12)
      Y3   = SQRT(SL13**2-X3**2)
      IF (NAMEK .EQ. 6HK1      ) GO TO 110
                                                    NERROR=2
      GO TO 999
C
C MEMBRANE = K2A1 (BODLEY, BENFIELD), FENDING = K2B1 (BODLEY).
110 CALL K2A1 (SL12,X3,Y3,TMEM,F,ANU,TL,TS,S,KTL,KTS,KS)      TL=K
      CALL K2B1 (SL12,X3,Y3,TBEN,E,ANU,TL(10,10),TS(1,10),S,
      *          KTL,KTS,KS)
      DO 111 I=1,9
      II = I+9
      DO 111 J=1,9
111 TS(II,J) = TS(I,J)
C
      CALL DCOS2 (CJ,EJ,S,KCJ,KEJ,KS)      S=DC
      CALL MULTA (TL,S,18,18,18,KTL,KS)
      IF (NAMEST .EQ. 6H      .OR. NAMEST .EQ. 6HNOSTRS) GO TO 210
      CALL MULTA (TS,S,NRST,18,18,KTS,KS)
210 CALL ATXBA1 (S,TL,18,18,KS,KTL)
      RETURN
C
999 CALL ZZBOMB (5HSTF2 ,NERROR)
      END

```

```

SUBROUTINE STF3 (CJ,EJ,TMEM,TBEN,E,ANU,NAMEK,NAMEST,S,TL,TS,NRST,
*           KCJ,KEJ,KS,KTL,KTS)
DIMENSION CJ(KCJ,1),EJ(KEJ,1),S(KS,1),TL(KTL,1),TS(KTS,1)
DIMENSION CW(3,3),EW(3,3),W1(18,18),
*           IV1(18),IV2(18),IV3(18),IV4(18)
DATA KCW,KW1 / 3,18 /
DATA IV1/ 1, 2, 3, 4, 5, 6, 7, 8, 9,10,11,12,13,14,15,16,17,18/,
*       IV2/ 1, 2, 3, 4, 5, 6,13,14,15,16,17,18,19,20,21,22,23,24/,
*       IV3/ 1, 2, 3, 4, 5, 6, 7, 8, 9,10,11,12,19,20,21,22,23,24/,
*       IV4/ 7, 8, 9,10,11,12,13,14,15,16,17,18,19,20,21,22,23,24/
C
C SUBROUTINE TO CALCULATE FINITE ELEMENT...
C STIFFNESS MATRIX (SAME AS GLOBAL LOAD TRANSFORMATION MATRIX),
C LOCAL LOAD TRANSFORMATION MATRIX (NOT YET),
C STRESS TRANSFORMATION MATRIX (NOT YET),
C FOR A COMBINED MEMBRANE-BENDING QUADRILATERAL PLATE ELEMENT WITH
C UNRESTRAINED BOUNDARIES.
C STIFFNESS MATRIX IS IN GLOBAL COORDINATE DIRECTIONS.
C GLOBAL COORDINATE ORDER IS
C (U,V,W,P,Q,R) JOINT 1, THEN JOINT 2, 3, 4.
C WHERE U,V,W ARE TRANSLATIONS AND P,Q,R ARE ROTATIONS.
C GLOBAL LOAD TRANSFORMATION MATRIX RELATES LOADS AT QUAD VERTICES IN
C GLOBAL COORDINATE DIRECTIONS TO DEFLECTIONS IN THE GLOBAL COORDINATE
C DIRECTIONS.
C ROW ORDER IN GLOBAL LOAD TRANSFORMATION MATRIX IS
C (PU,PV,PW,MP,MQ,MR) JOINT 1, THEN JOINT 2,3,4.
C WHERE P IS FORCE AND M IS MOMENT.
C LOCAL LOAD TRANSFORMATION MATRIX RELATES LOADS AT QUAD VERTICES
C IN LOCAL COORDINATE SYSTEM TO DEFLECTIONS IN THE GLOBAL COORDINATE
C DIRECTION.
C STRESS TRANSFORMATION MATRIX RELATES STRESS AT QUAD VERTICES IN LOCAL
C COORDINATE SYSTEM TO DEFLECTIONS IN THE GLOBAL COORDINATE DIRECTION.
C EULER ANGLE CONVENTION IS GLOBAL X,Y,Z PERMUTATION.
C CALLS FORMA SUBROUTINES STF2,REVADD,ZZBOMB.
C DEVELOPED BY WA BENFIELD, RL WOHLER. FEBRUARY 1973.
C LAST REVISION BY WA BENFIELD. MARCH 1976.
C
C SUBROUTINE ARGUMENTS
C CJ = INPUT MATRIX OF GLOBAL X,Y,Z COORDINATES AT QUAD JOINTS.
C ROWS 1,2,3 CORRESPOND TO X,Y,Z COORDINATES.
C COLS 1,2,3,4 CORRESPOND TO JOINTS 1,2,3,4. SIZE(3,4).
C EJ = INPUT MATRIX OF EULER ANGLES (DEGREES) AT QUAD JOINTS.
C ROWS 1,2,3 CORRESPOND TO GLOBAL X,Y,Z PERMUTATION.
C COLS 1,2,3,4 CORRESPOND TO JOINTS 1,2,3,4. SIZE(3,4).
C TMEM = INPUT EFFECTIVE MEMBRANE THICKNESS.
C TBEN = INPUT EFFECTIVE BENDING THICKNESS.
C E = INPUT YOUNGS MODULUS OF ELASTICITY.
C ANU = INPUT POISSONS RATIO. (E/2G)-1.
C NAMEK = INPUT TYPE OF STIF MATRIX WANTED.
C = K1, USES 4 TRIANGLES, OVERLAP AVERAGE.
C NAMEST = INPUT OPTION FOR STRESS TRANSFORMATION.
C = 6H OR 6HNOSTRS ,NO STRESS TRANS CALCULATED.
C S = OUTPUT STIFFNESS MATRIX (SAME AS GLOBAL LOAD TRANSFORMATION
C MATRIX). SIZE(24,24).
C TL = OUTPUT LOCAL LOAD TRANSFORMATION MATRIX. SIZE(24,24).

```



```
CW(I,2) = CJ(I,3)
EW(I,2) = EJ(I,3)
CW(I,3) = CJ(I,4)
205 EW(I,3) = EJ(I,4)
CALL STF2 (CW,EW,TMEM,TBEN,E,ANU,NAMEK,NAMEST,W1,TL,TS,NRSTX,
*         KCW,KCW,KW1,KTL,KTS)
CALL REVADD (.5,W1,IV4,IV4,S, 18,18,24,24, 18,KS)
C
DO 300 J=1,24
DO 300 I=1,24
TL(I,J) = 0.0
300 TS(I,J) = 0.0
RETURN
C
999 CALL ZZBOMB (4HSTF3 ,NERROR)
END
```

```

SUBROUTINE STF3A (CJ,EJ,TH,G,NAMEK,NAMEST,S,TL,TS,NRST,
*              KCJ,KEJ,KS,KTL,KTS)
  DIMENSION CJ(KCJ,1), EJ(KEJ,1), S(KS,1), TL(KTL,1), TS(KTS,1)
C
C  SUBROUTINE TO CALCULATE FINITE ELEMENT...
C  STIFFNESS MATRIX (SAME AS GLOBAL LOAD TRANSFORMATION MATRIX),
C  LOCAL LOAD TRANSFORMATION MATRIX,
C  STRESS TRANSFORMATION MATRIX,
C  FOR A RECTANGULAR SHEAR PANEL ELEMENT WITH UNRESTRAINED BOUNDARIES.
C  STIFFNESS MATRIX IS IN GLOBAL COORDINATE DIRECTIONS.
C  GLOBAL COORDINATE ORDER IS
C  (U,V,W) JOINT 1, THEN JOINT 2, 3, 4.
C  WHERE U,V,W ARE TRANSLATIONS.
C  GLOBAL LOAD TRANSFORMATION MATRIX RELATES LOADS AT PANEL VERTICES IN
C  GLOBAL COORDINATE DIRECTIONS TO DEFLECTIONS IN THE GLOBAL COORDINATE
C  DIRECTIONS.
C  ROW ORDER IN GLOBAL LOAD TRANSFORMATION MATRIX IS
C  (PU,PV,PW) JOINT 1, THEN JOINT 2, 3, 4.
C  WHERE P IS FORCE.
C  LOCAL LOAD TRANSFORMATION MATRIX RELATES LOADS AT PANEL VERTICES IN
C  LOCAL COORDINATE SYSTEM TO DEFLECTIONS IN THE GLOBAL COORDINATE
C  DIRECTIONS.
C  ROW ORDER IN LOCAL LOAD TRANSFORMATION MATRIX IS
C  PX1,PX2,PX3,PX4, PY1,PY2,PY3,PY4
C  WHERE P IS FORCE. X GOES FROM 1 TO 2. Y GOES FROM 1 TO 4.
C  STRESS TRANSFORMATION MATRIX RELATES PANEL SHEAR STRESS (CONSTANT) IN
C  LOCAL COORDINATE SYSTEM TO DEFLECTIONS IN THE GLOBAL COORD DIRECTIONS.
C  EULER ANGLE CONVENTION IS GLOBAL X,Y,Z PERMUTATION.
C  CALLS FORMER SUBROUTINES ATXBA1,DCOS3C,K3C1,MULTA,ZZBOMB.
C  DEVELOPED BY RL WOHLER. APRIL 1974.
C  LAST REVISION BY WA BENFIELD. MARCH 1976.
C
C  SUBROUTINE ARGUMENTS
C  CJ      = INPUT  MATRIX OF GLOBAL X,Y,Z COORDINATES AT PANEL JOINTS.
C           ROWS 1,2,3 CORRESPOND TO X,Y,Z COORDINATES.
C           COLS 1,2,3,4 CORRESPOND TO JOINTS 1,2,3,4.  SIZE(3,4).
C  EJ      = INPUT  MATRIX OF EULER ANGLES (DEGREES) AT PANEL JOINTS.
C           ROWS 1,2,3 CORRESPOND TO GLOBAL X,Y,Z PERMUTATION.
C           COLS 1,2,3,4 CORRESPOND TO JOINTS 1,2,3,4.  SIZE(3,4).
C  TH      = INPUT  PANEL THICKNESS.
C  G       = INPUT  SHEAR MODULUS OF ELASTICITY.
C  NAMEK   = INPUT  TYPE OF STIF MATRIX WANTED.
C           = K1, USES K3C1.
C  NAMEST  = INPUT  OPTION FOR STRESS TRANSFORMATION.
C           = 6H      OF 6HNDSTRS ,NO STRESS TRANS CALCULATED.
C  S       = OUTPUT STIFFNESS MATRIX (SAME AS GLOBAL LOAD TRANSFORMATION
C           MATRIX).  SIZE(12,12).
C  TL      = OUTPUT LOCAL LOAD TRANSFORMATION MATRIX.  SIZE(6,12).
C  TS      = OUTPUT STRESS TRANSFORMATION MATRIX.  SIZE(1,12).
C  NRST    = OUTPUT NUMBER OF ROWS (1) IN STRESS TRANSFORMATION MATRIX.
C  KCJ     = INPUT  ROW DIMENSION OF CJ IN CALLING PROGRAM.
C  KEJ     = INPUT  ROW DIMENSION OF EJ IN CALLING PROGRAM.
C  KS      = INPUT  ROW DIMENSION OF S IN CALLING PROGRAM.  MIN=12.
C  KTL     = INPUT  ROW DIMENSION OF TL IN CALLING PROGRAM.  MIN=8.
C  KTS     = INPUT  ROW DIMENSION OF TS IN CALLING PROGRAM.  MIN=1.

```





TEGEOM

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SUBROUTINE TEGEOM (CJ,JM,    VL,DV,    KCJ,    IFBAD)
  DIMENSION CJ(KCJ,1), JM(    1),    DV(1)
  DIMENSION    R12(3),R13(3),R14(3)
  DATA EPS / 1.E-5 /

C
C  SUBROUTINE TO DETERMINE THE VOLUME AND VOLUME CHANGE COEFFICIENTS OF
C  A TETRAHEDRON.
C  CALLS FORMA SUBROUTINES VCROSS,VDOT .
C  DEVELOPED BY C S BODLEY.  FEBRUARY 1974.
C  LAST REVISION BY R A PHILIPPUS.  AUGUST 1974.
C  SUBROUTINE ARGUMENTS
C  CJ    = INPUT  MATRIX OF JOINT COORDINATES.  SIZE(3,8).
C  JM    = INPUT  VECTOR OF JOINTS DEFINING A TETRAHEDRON.  SIZE (4).
C  VL    = OUTPUT VOLUME OF TETRAHEDRON DEFINED BY JM.
C  DV    = OUTPUT VECTOR OF VOLUME CHANGE COEFFICIENTS.
C  KCJ   = INPUT  ROW DIMENSION SIZE OF CJ IN CALLING PROGRAM.  MIN = 3.
C  IFBAD = OUTPUT
C          = 0 , THE TETRAHEDRON VERTICIES ARE NOT NUMBERED ACCORDING
C          TO THE ESTABLISHED CONVENTION, OR LIE IN A PLANE.
C
      J1 = JM(1  )
      J2 = JM(2  )
      J3 = JM(3  )
      J4 = JM(4  )
      DO 5 I=1,3
      R12(I) = CJ(I,J2) - CJ(I,J1)
      R13(I) = CJ(I,J3) - CJ(I,J1)
5  R14(I) = CJ(I,J4) - CJ(I,J1)

C
      CALL VCROSS (R12,R13,DV(10),VAMAG,VPMAG,VZMAG,SINAB)
      CALL VDOT   (DV(10),R14,VOL,VAMAG,VBMAG,COSAB)
      IF (VOL.LE.EPS) IFBAD=0
      VL    = VOL/6.

C
      CALL VCROSS (R13,R14,DV(4), VAMAG,VPMAG,VZMAG,SINAB)
      CALL VCROSS (R14,R12,DV(7), VAMAG,VBMAG,VZMAG,SINAB)
      DO 10 I=1,3
10  DV(I) = -DV(I+3) - DV(I+6) - DV(I+9)
      DO 15 I=1,12
15  DV(I) = DV(I)/6.

C
      RETURN
      END

```

```

SUBROUTINE TRNGL (XYZ,JDOF,EUL,NUTEL,NJ,
*             NUTMX,NUTKX,NUTBX,NUTLT,NUTST,
*             W,T,S,KX,KJ,KE,KW)
DIMENSION XYZ(KX,1),JDOF(KJ,1),EUL(KE,1),W(KW,1),T(KW,1),S(KW,1)
DIMENSION CJ(3,3), EJ(3,3), IVE(18)
DATA MANSI/6HTRNGL /, NRW,NRLT/18,18/, IBLNK/6H      /, KCJ/3/
DATA NIT,NCT/5,6/

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```

C
C SUBROUTINE TO CALCULATE (ON OPTION) FINITE ELEMENT ...
C MASS MATRICES AND IVECS (ON NUTMX),
C STIFFNESS MATRICES (SAME AS GLOBAL LOAD TRANSFORMATION MATRICES)
C AND IVECS (ON NUTKX);
C UNIT LOAD BUCKLING MATRICES AND IVECS (ON NUTBX), (NOT YET)
C LOCAL LOAD TRANSFORMATION MATRICES AND IVECS (ON NUTLT),
C STRESS TRANSFORMATION MATRICES AND IVECS (ON NUTST),
C FOR COMBINED MEMBRANE-BENDING TRIANGLE PLATE ELEMENTS.
C MASS, STIFFNESS, BUCKLING MATRICES ARE IN GLOBAL COORDINATE
C DIRECTIONS.
C GLOBAL COORDINATE ORDER IS
C (U,V,W,P,Q,R) JOINT 1, THEN JOINT 2, 3.
C WHERE U,V,W ARE TRANSLATIONS AND P,Q,R ARE ROTATIONS.
C IVEC GIVES ELEMENT DOF INTO GLOBAL DOF. EXAMPLES...
C IVEC(6)=834 PLACES ELEMENT DOF 6 INTO GLOBAL DOF 834.
C IVEC(3)=0 OMMITS ELEMENT DOF 3 FROM GLOBAL DOF. THIS CONSTRAINS
C ELEMENT DOF 3 TO ZERO MOTION.
C GLOBAL LOAD TRANSFORMATION MATRIX RELATES LOADS AT TRNGL VERTICES IN
C GLOBAL COORDINATE DIRECTIONS TO DEFLECTIONS IN THE GLOBAL COORDINATE
C DIRECTIONS.
C ROW ORDER IN GLOBAL LOAD TRANSFORMATION MATRIX IS
C (PU,PV,PW,MP,MQ,MR) JOINT 1, THEN JOINT 2,3.
C WHERE P IS FORCE AND M IS MOMENT.
C LOCAL LOAD TRANSFORMATION MATRIX RELATES LOADS AT TRNGL VERTICES IN
C LOCAL COORDINATE SYSTEM TO DEFLECTIONS IN THE GLOBAL COORDINATE
C DIRECTIONS.
C ROW ORDER IN LOCAL LOAD TRANSFORMATION MATRIX IS
C (PX,PY,PZ) JOINT 1 THEN 2,3, NEXT
C (MX,MY,MZ) JOINT 1 THEN 2,3.
C WHERE P IS FORCE AND M IS MOMENT.
C STRESS TRANSFORMATION MATRIX RELATES STRESS AT TRNGL VERTICES IN LOCAL
C COORDINATE SYSTEM TO DEFLECTIONS IN THE GLOBAL COORDINATE DIRECTIONS.
C ROW ORDER IN STRESS TRANSFORMATION MATRIX IS
C (SIGMA-X,SIGMA-Y,TAU-XY) FOR (Z=TBEN/2) AT JOINT 1,
C THEN JOINT 2,3.
C (SIGMA-X,SIGMA-Y,TAU-XY) FOR (Z=-TBEN/2) AT JOINT 1,
C THEN JOINT 2,3.
C WHERE SIGMA IS NORMAL STRESS AND TAU IS SHEAR STRESS.
C DATA ARRANGEMENT ON NUTMX, NUTKX, NUTBX, NUTLT, NUTST FOR EACH
C FINITE ELEMENT IS (W=M,K,B,LT,ST)
C WRITE (NUTWX) N,M,W,NFL,NR,NC,NAMFL,(IBLNK,I=1,5),
C ((W(I,J),I=1,NR),J=1,NC),(IVEC(I),I=1,NC)
C CALLS FORMA SUBROUTINES MAS2, PAGEHD, STF2, ZZBOMB.
C DEVELOPED BY WA BENFIELD, CS BODLEY, RL WOHLER. FEBRUARY 1973.
C LAST REVISION BY RL WOHLER. MAY 1976.
C
C *****

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```

C INPUT DATA READ IN THIS SUBROUTINE FROM NUTEL. IF NUTEL = 5, DATA IS
C READ FROM CARDS.
C   NAMEM,NAMEK,NAMELT,NAMEST,NAMEB      FORMAT (5(A6,4X)
C   RO,E,ANU                             FORMAT (3(5X,E10))
C   TMASC,TMEMC,TBENC                     FORMAT (3(5X,E10))
C 20 NEL,J1,J2,J3,TMASV,TMEMV,TBENV      FORMAT (4I5,3E10)
C   IF (J1 .EQ. 0) RETURN
C   GO TO 20

```

```

C DEFINITION OF INPUT VARIABLES.
C NAMEM = TYPE OF MASS MATRIX WANTED.
C       = M1, DIAGONAL LUMPED.
C       = M2, CONSISTENT.
C       = 6H      OR 6HNDMASS, NO MASS MATRIX CALCULATED.
C NAMEK = TYPE OF STIFFNESS MATRIX WANTED.
C       = K1, QUADRATIC DISPLACEMENT FOR MEMBRANE, CUBIC
C         DISPLACEMENT FOR BENDING.
C       = 6H      OR 6HNOSTIF, NO STIFFNESS MATRIX CALCULATED.
C NAMELT = IDENTIFICATION NAME FOR LOAD TRANSFORMATION MATRICES.
C        = 6H      OR 6HNLOAD, NO LOAD TRANSFORMATIONS CALCULATED.
C NAMEST = IDENTIFICATION NAME FOR STRESS TRANSFORMATION MATRICES.
C        = 6H      OR 6HNOSTPS, NO STRESS TRANSFORMATIONS CALCULATED.
C NAMEB = TYPE OF PUCKLING MATRIX WANTED.
C        = 6H      OR 6HNOBUCK, NO BUCKLING MATRIX CALCULATED.
C RO    = MASS DENSITY.
C E     = YOUNGS MODULUS OF ELASTICITY.
C ANU   = POISSONS RATIO. (E/2G)-1.
C TMASC = EFFECTIVE MASS THICKNESS, (CONSTANT).
C TMASV = EFFECTIVE MASS THICKNESS, (VARIABLE).
C       IF .LE. 0., TMASC IS USED.
C TMEMC = EFFECTIVE MEMBRANE THICKNESS, (CONSTANT).
C TMEMV = EFFECTIVE MEMBRANE THICKNESS, (VARIABLE).
C       IF .LE. 0., TMEMC IS USED.
C TBENC = EFFECTIVE BENDING THICKNESS, (CONSTANT).
C TBENV = EFFECTIVE BENDING THICKNESS, (VARIABLE).
C       IF .LE. 0., TBENC IS USED.
C NEL   = FINITE ELEMENT NUMBER. FOR REFERENCE ONLY, NOT USED IN
C        CALCULATIONS. WRITTEN ON NUTMX, ETC.
C J1    = JOINT NUMBER AT TRIANGLE VERTEX 1.
C J2    = JOINT NUMBER AT TRIANGLE VERTEX 2.
C J3    = JOINT NUMBER AT TRIANGLE VERTEX 3.

```

```

C EXPLANATION OF INPUT FORMATS. NUMBER INDICATES CARD COLUMNS USED.
C   I = INTEGER DATA, RIGHT ADJUSTED.
C   E = DECIMAL POINT DATA, ANYWHERE IN FIELD. EXPONENT RIGHT ADJUSTED.
C   X = CARD COLUMNS SKIPPED.

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C SUBROUTINE ARGUMENTS (ALL INPUT)
C XYZ = MATRIX OF JOINT GLOBAL X,Y,Z LOCATIONS. ROWS CORRESPOND
C      TO JOINT NUMBERS. COLUMNS 1,2,3 CORRESPOND TO THE JOINT
C      X,Y,Z LOCATIONS RESPECTIVELY. SIZE(NJ,3).
C JDOF = MATRIX OF JOINT GLOBAL DEGREES OF FREEDOM. ROWS CORRESPOND
C       TO JOINT NUMBERS. COLUMNS 1,2,3 CORRESPOND TO THE JOINT
C       TRANSLATION DOFS AND COLUMNS 4,5,6 CORRESPOND TO THE JOINT

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*          / 33X12HT(BENDING) = E10.3,
*          //18X 7HELEMENT 5X 7HJOINT 1 5X 7HJOINT 2 5X 7HJOINT 3
*          5X 7HT(MASS) 6X 11HT(MEMBRANE) 5X 10HT(BENDING)
*          /18X 6HNUMBER 36X 3(5X 10H(VARIABLE) ) )
2004 FORMAT (18X 4(15,7X),3(E10.3,5X) )
2005 FORMAT (18X 4(15,7X) )

```

C

C READ AND WRITE FINITE ELEMENT DATA.

```

NLINE = 1
CALL PAGEHD
WRITE (NOT,2001)
READ (NUTEL,1001) NAMEM,NAMEK,NAMELT,NAMEST,NAMEB
READ (NUTEL,1002) RO,E,ANU
READ (NUTEL,1002) TMASC,TMEMC,TBENC
WRITE (NOT,2003) NAMEM,NAMEK,NAMELT,NAMEST,NAMEB,
*          RO,E,TMASC,ANU,TMEMC,TBENC
20 READ (NUTEL,1003) NEL,J1,J2,J3,TMASV,TMEMV,TBENV
NO THIK = 1
IF (TMASV.LE.0. .AND. TMEMV.LE.0. .AND. TBENV.LE.0.) NO THIK=0
IF (J1 .LE. 0) RETURN
NLINE = NLINE + 1
IF (NLINE .LE. 42) GO TO 30
CALL PAGEHD
WRITE (NOT,2002)
WRITE (NOT,2003) NAMEM,NAMEK,NAMELT,NAMEST,NAMEB,
*          RO,E,TMASC,ANU,TMEMC,TBENC
NLINE = 0
30 IF (NO THIK.EQ.1)
*WRITE (NOT,2004) NFL,J1,J2,J3,TMASV,TMEMV,TBENV
IF (NO THIK.EQ.0) WRITE (NOT,2005) NEL,J1,J2,J3
NERROR=1
IF (J1 .GT. NJ .OR. J2 .GT. NJ .OR. J3 .GT. NJ) GO TO 999

```

C

C SET THICKNESSES.

```

TMAS = TMASC
TMEM = TMEMC
TBEN = TBENC
IF (TMASV.GT.0.) TMAS=TMASV
IF (TMEMV.GT.0.) TMEM=TMEMV
IF (TBENV.GT.0.) TBEN=TBENV

```

C

C FORM FINITE ELEMENT COORDINATE LOCATIONS, EULER ANGLES, REVADD IVEC.

```

DO 42 I=1,3
CJ(I,1) = XYZ(J1,I)
CJ(I,2) = XYZ(J2,I)
CJ(I,3) = XYZ(J3,I)
EJ(I,1) = EUL(J1,I)
EJ(I,2) = EUL(J2,I)
42 EJ(I,3) = EUL(J3,I)
DO 44 I=1,6
IV1(I) = JDDF(J1,I)
IV1(I+6) = JDDF(J2,I)
44 IV1(I+12) = JDDF(J3,I)

```

C

C FORM MASS MATRIX (W).

```

IF (NAMEM .EQ. 6H .OR. NAMEM .EQ. 6HNDMASS) GO TO 110
CALL MAS2 (CJ,EJ,TMAS,RO,NAMEM,W,T,S,KCJ,KCJ,KW,KW,KW)
                                                                    NERROR=2
IF (NUTMX .LE. 0) GO TO 999
WRITE (NUTMX) NAMEM,NEL,NRW,NRW,NAMEL,(IBLNK,I=1,5),
* ((W(I,J),I=1,NRW),J=1,NRW),(IV1(I),I=1,NRW)
C
C FORM STIFFNESS MATRIX (W), LOCAL LOAD TRANSFORMATION MATRIX (T),
C STRESS TRANSFORMATION MATRIX (S).
110 IF (NAMEK .EQ. 6H .OR. NAMEK .EQ. 6HNOSTIF) GO TO 20
CALL STF2 (CJ,EJ,TMEM,TBEN,F,ANU,NAMEK,NAMEST,W,T,S,NRST,
* KCJ,KCJ,KW,KW,KW)
                                                                    NERROR=3
IF (NUTKX .LE. 0) GO TO 999
WRITE (NUTKX) NAMEK,NEL,NRW,NRW,NAMEL,(IBLNK,I=1,5),
* ((W(I,J),I=1,NRW),J=1,NRW),(IV1(I),I=1,NRW)
IF (NAMELT .EQ. 6H .OR. NAMELT .EQ. 6HNOLOAD) GO TO 115
                                                                    NERROR=4
IF (NUTLT .LE. 0) GO TO 999
WRITE (NUTLT) NAMELT,NEL,NRST,NRW,NAMEL,(IBLNK,I=1,5),
* ((T(I,J),I=1,NRST),J=1,NRW),(IV1(I),I=1,NRW)
115 IF (NAMEST .EQ. 6H .OR. NAMEST .EQ. 6HNOSTRS) GO TO 20
                                                                    NERROR=5
IF (NUTST .LE. 0) GO TO 999
WRITE (NUTST) NAMEST,NEL,NRST,NRW,NAMEL,(IBLNK,I=1,5),
* ((S(I,J),I=1,NRST),J=1,NRW),(IV1(I),I=1,NRW)
GO TO 20
C
999 CALL Z2BOMB (6HTRNGL ,NERROR)
END

```