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**CUBIC SPLINE FUNCTION INTERPOLATION IN ATMOSPHERE
MODELS FOR THE SOFTWARE DEVELOPMENT LABORATORY:
FORMULATION AND DATA**

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LYNDON B. JOHNSON SPACE CENTER
HOUSTON, TEXAS 77058**



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16. Abstract A tabulation of selected altitude-related values of pressure, density, speed of sound, and coefficient of viscosity for each of U.S.A. models of the atmosphere is presented in block data format. Interpolation for the desired atmospheric parameters is performed by using cubic spline functions. The recursive relations necessary to compute the cubic spline function coefficients are derived and implemented in subroutine form. Three companion subprograms, which form the preprocessor and processor, are also presented. These subprograms, together with the data element, compose the spline fit atmosphere package. Detailed FLOWGM flow charts and FORTRAN listings of the atmosphere package are presented in the appendix.			
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James C. Kirkpatrick
Lyndon B. Johnson Space Center
Houston, Texas 77058

**CUBIC SPLINE FUNCTION INTERPOLATION IN ATMOSPHERE
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**By James C. Kirkpatrick
Lyndon B. Johnson Space Center**

SUMMARY

Six standard reference atmosphere models for the years 1962, 1963 (Patrick Air Force Base), and 1966 (for July and January at latitudes 30° and 60° N) are presented in tabular form. The tabulation, which is presented in block data format, is adequate for the accurate representation of the atmospheric parameters of pressure, density, speed of sound, and coefficient of viscosity as functions of altitude. The range of tabulated altitudes extends from 0 to 205 kilometers. Interpolation for the desired parameters is performed by using cubic spline functions. The recursive relations necessary to compute the cubic spline function coefficients are derived and implemented in subroutine form. Detailed FLOWGM flow charts and FORTRAN listings of the atmosphere package are presented in the appendix.

INTRODUCTION

This report presents a tabulation in block data format of selected altitude-correlated values of pressure, density, speed of sound, and coefficient of viscosity for each of six atmosphere models. These values were selected such that they adequately represent their respective functions for accurate interpolation by cubic spline functions throughout the range of tabulated altitudes. Three companion subprograms, which form the preprocessor (subroutines SDAT and SPLN1) and processor (subroutine ATMSPL), are presented. These subprograms, together with the data element, compose the spline fit atmosphere package. In the preprocessor, the data for the desired atmosphere model are selected and processed for proper order and unit consistency before SPLN1 is used to compute the spline function coefficients. In the processor, the data table is searched to establish the interval in which the desired altitude lies, and then the values of the previously mentioned parameters are computed by using the cubic spline function coefficients for the appropriate altitude interval.

The cubic spline technique provides an effective, easy-to-use method for the unerring reproduction of a function from tabulated data. The method also ensures continuity in the function and in its first and second derivatives. After

the cubic spline function coefficients have been computed, they may be stored for repeated use as long as the tabulated data remain unchanged.

SYMBOLS

a, b, c, d	edges of the beam
a_k	defined in equation (37)
b_k	defined in equation (38)
C_1, C_2	arbitrary constants of integration
c_k	defined in equation (39)
$c_1(k)$	defined in equation (68)
$c_2(k)$	defined in equation (69)
$c_3(k)$	defined in equation (70)
dA	differential element of a cross-sectional area of a beam
ds	differential element of arc length
dx	differential element of the length of the beam
$d\theta$	differential element of the angle through which a cross-sectional surface of a beam is rotated under load
d_k	defined in equation (49)
E	modulus of elasticity of the beam
EI	flexural rigidity (can be taken as unity for any plane curve without loss of generality)
ef	original unstressed length of the fiber
gh	typical fiber of the beam
hk	defined in equation (1)
I	area moment of inertia
l	distance from the neutral surface to a deformed fiber of a loaded beam

$M(x)$	bending moment as a function of the distance x measured from the end of the beam
M_k	bending moment at the k th section of the beam or an approximation to the second derivative at the k th section
P	load that acts upon the beam
Q_k	defined in equation (44)
R_1, R_2	support reactions of the beam
S	stress
s	arc length of a curve
U_k	defined in equation (46)
V_k	shear force at the k th section of the beam
$y(k)$	defined in equation (24)
$y(x)$	defined in equation (23)
y'	slope of the deformation curve
$y'(x)$	defined in equation (22)
ϵ	strain (change in length per unit of length)
ρ	radius of curvature of the neutral surface
φ	angle that the tangent to a curve makes with the axis of abscissas

SPLINE FIT ATMOSPHERE MODEL PACKAGE

Model History

The spline fit atmosphere package discussed in this report, was originally developed for the space vehicle dynamic simulator (SVDS) program in November 1972. In February 1973, the package was incorporated with appreciable modification, into the Shuttle optimal abort program (SOAP). The package presented here is from an early version of the SOAP. For implementation into the SOAP, the SVDS version was modified, at the expense of storage, to improve its performance and execution requirements. The spline fit atmosphere package has performed accurately in both programs.

Description of the Models

The spline fit atmosphere package consists of six atmosphere models:

1. The 1962 standard reference atmosphere
2. The 1966 standard reference atmosphere for July at latitude 30° N
3. The 1966 standard reference atmosphere for January at latitude 30° N
4. The 1966 standard reference atmosphere for July at latitude 60° N
5. The 1966 standard reference atmosphere for January at latitude 60° N
6. The 1963 Patrick Air Force Base (AFB) reference atmosphere

Each model consists of a tabulation of altitude-correlated values of the atmospheric parameters of pressure, density, speed of sound, and coefficient of viscosity. All six models are correlated to the same table of altitudes and tabulated in the foregoing sequence. All tabulated atmospheric parameter values are expressed in the meter-kilogram-second (MKS) system of units. Altitude values are given in meters, pressure values are given in millibars, density values are given in kilograms per cubic meter, speed of sound values are given in meters per second, and coefficient of viscosity values are given in kilograms per meter per second. Each atmospheric parameter is represented as a function of altitude by 123 data points. These data have been selected on best-fit considerations, with particular emphasis on those regions in which the tabulation shows that the function is discontinuous in its first derivative. Each model is represented in the 0- to 205-kilometer altitude range. The tabulation was compiled from references 1 to 3.

Because the tabulation for the 1966 atmosphere extends only to 118 kilometers, the last data point is repeated to 205 kilometers for model consistency. If the model altitude boundaries are exceeded, the package returns the last tabulated parameter values at the violated boundary.

Assumptions and Approximations

The spline fit atmosphere model package was developed to accommodate the needs and restrictions of the SVDS program. As a result, temperature, an important atmospheric parameter, was not included in the list of parameters modeled when the package was built. This parameter can be added to any model desired at the cost of tabulating the parameter values required.

The tabulation was performed in the MKS system of units because this system was common to all the references used. A common system of units is advantageous because a single set of conversion factors can be used to place all models in any desired working units. The British engineering system of units was used to convert the atmospheric data in this package (i.e., pressure in pounds-force per square foot, density in slugs per cubic foot, speed of sound in feet per second, and coefficient of viscosity in pounds-mass seconds per square foot).

Atmospheric parameter function values were selected at various altitudes. The increment of altitude was varied as a function of altitude as follows.

<u>Altitude range, km</u>	<u>Altitude increment, m</u>
0 to 3	250
3 to 5	500
5 to 20	1000
20 to 160	2000
160 to 204	4000
204 to 205	1000

Additional data points were added to mark the location in which the atmospheric parameter functions undergo first-derivative discontinuities. These discontinuities occur only in the speed of sound and coefficient of viscosity functions, which are affected because of temperature variations. As a result, when temperature is added to the atmosphere models, the choice of altitudes should accommodate discontinuities in the first derivative of the temperature functions. Because of the need to intersperse additional points, an ordering scheme is included in the pre-processor SDAT to place all altitude values and associated function values in ascending order of the independent variable. This order must be established before calling subroutine SPLN1 to compute the cubic spline coefficients.

The small altitude increment used at the extremes of the tabulation permitted the approximation of the first derivatives of the function at the initial and terminal boundaries by forming the difference quotient. This assumption of linearity at the extremes of the tabulated function is the only assumption made in the model. (The theoretical arguments on which the algorithm is based result in the additional assumption that the curvature of the function can be represented by its second derivative. The data sample selected is expected to comply with this assumption.)

DERIVATION OF THE RECURSIVE RELATIONS FOR COMPUTING THE COEFFICIENTS OF THE CUBIC SPLINE FUNCTIONS

The mathematical spline is a formal analog of the draftsman's spline, a flexible beam device used to fair out a smooth curve between specified data points. The mechanical spline is anchored on the drawing board at each plotted data point. The curvature of the spline results from the bending moments applied to the beam.

In deriving the recursive relations of the spline algorithm, the elementary theory of elasticity is useful. Consider a simply supported beam (i.e., ends

unrestrained) under the action of an applied load, however distributed. For an elementary analysis, the following assumptions are made:

1. Sections of the beam, which were originally plane, remain plane.
2. The material of the beam is homogeneous and obeys Hooke's law (the deformation is proportional to the applied load).
3. The moduli of elasticity for tension and for compression are equal.
4. The beam is initially straight and is of constant cross section.

Figure 1 shows a uniform homogeneous beam under the action of the load P . The beam is simply supported and is in static equilibrium under the action of the support reactions R_1 and R_2 . The differential element of length dx , bounded by the edges a , b , c , and d , is bent or deformed under load into the exaggerated shape shown in figure 2 where c and d are deflected to c' and d' . The sections ab and cd are shown rotated relative to each other through an angle $d\theta$, but they remain undistorted in accordance with assumption 1. The fibers in the region of ac are contracted, or shortened, in compression, whereas those in the region bd are elongated, or lengthened, in tension. Because the beam is uniform and homogeneous in going from contraction to elongation, a region conceivably exists in which the fibers maintain their original unstressed length. This surface of unstressed fibers is referred to as the neutral surface. In the deformation of a typical fiber gh located at distance ℓ from the neutral surface, the elongation hk is the arc of a circle of radius ℓ , which subtends the angle $d\theta$ and is given by the relation

$$hk = \ell d\theta \quad (1)$$

The strain ϵ (the change in length per unit of length) is found by dividing the deformation hk by the original unstressed length of the fiber ef .

$$\epsilon = \frac{hk}{ef} = \frac{\ell d\theta}{ef} \quad (2)$$

If the radius of curvature of the neutral surface is ρ , the curved length of ef is equal to $\rho d\theta$. The strain can then be expressed as

$$\epsilon = \frac{\ell d\theta}{\rho d\theta} = \frac{\ell}{\rho} \quad (3)$$

Because the material is assumed to be homogeneous and to obey Hooke's law, the stress (force per unit area) in the fiber gh is given by

$$S = E \epsilon = \frac{E}{\rho} \ell \quad (4)$$

where E is the modulus of elasticity defined as the ratio of the stress S to the strain ϵ . Clearly, the sign of S varies with the sign of ℓ : negative or compressive stress for ℓ negative and positive or tensile stress for ℓ positive.

The beam in figure 1 is shown in static equilibrium. As a result, the algebraic sum of all forces and moments acting on the beam must be zero. The bending moment $M(x)$ must be balanced by the resisting moment. The resisting moment is the sum of all stresses S acting on each differential area element of cross section dA multiplied by its moment arm ℓ measured from the neutral axis as shown in figure 3. Hence, the bending moment is

$$M(x) = \int \ell (S \, dA) \quad (5)$$

Replacing S with $E\ell/\rho$ from equation (4) gives

$$M(x) = EI/\rho \quad (6)$$

where I is the area moment of inertia.

$$\frac{1}{\rho} = \frac{M(x)}{EI} \quad (7)$$

The reciprocal of ρ , the radius of curvature of the beam, is called the curvature of the curve. For plane curves, the curvature is defined as the rate at which the tangent to the curve turns compared with the description of arc. Therefore, if φ is the angle that the tangent to a curve makes with the axis of abscissas and s is the element of arc length, then the curvature is defined as

$$\frac{1}{\rho} = \frac{d\varphi}{ds} \quad (8)$$

The slope of the tangent to the curve is

$$y' = \frac{dy}{dx} = \tan \varphi$$

or

$$\varphi = \arctan y' \quad (10)$$

and

$$d\varphi = \frac{dy'}{(1+y'^2)^{\frac{3}{2}}} dx = \frac{y''}{(1+y'^2)^{\frac{3}{2}}} dx \quad (11)$$

The differential element of arc length ds is defined as

$$ds = (1+y'^2)^{\frac{1}{2}} dx \quad (12)$$

Therefore,

$$\frac{1}{\rho} = \frac{d\varphi}{ds} = \frac{y''}{(1+y'^2)^{\frac{3}{2}}} \quad (13)$$

and

$$\frac{y''}{(1+y'^2)^{\frac{3}{2}}} = \frac{M(x)}{EI} \quad (14)$$

The assumption is usually made that the slope of the deformation curve y' is small so that y'^2 can be ignored compared to unity. When this assumption is made, the differential equation of the deformation curve can be written as

$$M(x) = EIy''(x) \quad (15)$$

The assumption concerning the elastic behavior of a beam made at the beginning of this discussion can be realized by a mathematical function of one variable. The assumption that the slope of the curve is small and that its square can be neglected can be realized by an arbitrary mathematical function only over relatively short intervals. Under this condition, the curvature can be approximated by the second derivative of the function. This point must be remembered when selecting a set of data points to represent a function for spline fit. Sufficient data points must be chosen in the appropriate concentration such that in the regions where the curvature is large, each section of the curve can be considered as a simply supported beam (adequately supported so that the slope of the deformation curve is negligible).

The following definitions are required for the discussion that follows.

1. The shear at a section of a beam is the algebraic sum of all external forces acting on one side of the section.

2. The bending moment at a section of a beam is the algebraic sum of the moments of all the external forces on one side of the section.

Hence, if a mathematical function is represented in a region of definition by n data points, the region of definition will have been divided into $n - 1$ sections (fig. 4). If each section of the curve between given data points is considered to be a beam deflected under load, then the bending moment in the k th section between the k th and $(k + 1)$ th data points will be given by the equation

$$M(x) = \int_{x_k}^x V_k dx + M_k \quad (16)$$

where V_k and M_k are the shear and bending moments at the k th section. Therefore,

$$M(x) = V_k(x - x_k) + M_k \quad (17)$$

Clearly, where $x = x_k$, $M(x_k) = M_k$ and where $x = x_{k+1}$, $M(x_{k+1}) = M_{k+1}$ or

$$M_{k+1} = V_k(x_{k+1} - x_k) + M_k \quad (18)$$

Solving for V_k gives

$$V_k = \frac{M_{k+1} - M_k}{x_{k+1} - x_k} = \frac{\Delta M_k}{\Delta x_k} \quad (19)$$

Substituting equation (19) into equation (17) gives

$$\begin{aligned}
 M(x) &= \frac{(M_{k+1} - M_k)}{(x_{k+1} - x_k)} (x - x_k) + M_k \\
 &= M_{k+1} \frac{(x - x_k)}{(x_{k+1} - x_k)} + M_k \frac{(x_{k+1} - x)}{(x_{k+1} - x_k)}
 \end{aligned} \tag{20}$$

Substituting the bending moment $M(x)$ by its equivalent from equation (15) (the product EI is known as the flexural rigidity and can be taken as unity for any plane curve without loss of generality) in equation (20) gives

$$y''(x) = M_{k+1} \frac{(x - x_k)}{\Delta x_k} + M_k \frac{(x_{k+1} - x)}{\Delta x_k} \tag{21}$$

where $\Delta x_k = x_{k+1} - x_k$. Integrating twice gives

$$y'(x) = M_{k+1} \frac{(x - x_k)^2}{2\Delta x_k} - M_k \frac{(x_{k+1} - x)^2}{2\Delta x_k} + C_1 \tag{22}$$

$$y(x) = M_{k+1} \frac{(x - x_k)^3}{6\Delta x_k} + M_k \frac{(x_{k+1} - x)^3}{6\Delta x_k} + C_1 x + C_2 \tag{23}$$

where C_1 and C_2 are constants of integration. At $x = x_k$, $y(x_k) = y_k$; at $x = x_{k+1}$, $y(x_{k+1}) = y_{k+1}$. Substituting y_k and y_{k+1} in equation (23) gives

$$y_k = M_k \frac{\Delta x_k^2}{6} + C_1 x_k + C_2 \tag{24}$$

and

$$y_{k+1} = M_{k+1} \frac{\Delta x_k^2}{6} + C_1 x_{k+1} + C_2 \tag{25}$$

Subtracting equation (24) from equation (25) gives

$$y_{k+1} - y_k = (M_{k+1} - M_k) \frac{\Delta x_k^2}{6} + C_1 \Delta x_k \quad (26)$$

Solving for C_1 from equation (26) gives

$$\begin{aligned} C_1 &= \frac{y_{k+1} - y_k}{\Delta x_k} - \frac{(M_{k+1} - M_k) \Delta x_k}{6} \\ &= \left(\frac{y_{k+1}}{\Delta x_k} - \frac{M_{k+1} \Delta x_k}{6} \right) - \left(\frac{y_k}{\Delta x_k} - \frac{M_k \Delta x_k}{6} \right) \end{aligned} \quad (27)$$

Substituting for C_1 from equation (27) in equation (25) and solving for C_2 gives

$$C_2 = x_{k+1} \left(\frac{y_k}{\Delta x_k} - \frac{M_k \Delta x_k}{6} \right) - x_k \left(\frac{y_{k+1}}{\Delta x_k} - \frac{M_{k+1} \Delta x_k}{6} \right) \quad (28)$$

Substituting the expressions for C_1 and C_2 from equations (27) and (28) in equations (22) and (23) gives the expression for the cubic spline function in the k th interval as

$$\begin{aligned} y(x) &= M_{k+1} \frac{(x - x_k)^3}{6\Delta x_k} + M_k \frac{(x_{k+1} - x)^3}{6\Delta x_k} \\ &+ \left(\frac{y_{k+1}}{\Delta x_k} - \frac{M_{k+1} \Delta x_k}{6} \right) (x - x_k) + \left(\frac{y_k}{\Delta x_k} - \frac{M_k \Delta x_k}{6} \right) (x_{k+1} - x) \end{aligned} \quad (29)$$

and its first derivative is given by

$$\begin{aligned}
 y'(x) = & M_{k+1} \frac{(x - x_k)^2}{2\Delta x_k} - M_k \frac{(x_{k+1} - x)^2}{2\Delta x_k} \\
 & + \left(\frac{y_{k+1}}{\Delta x_k} - \frac{M_{k+1}\Delta x_k}{6} \right) - \left(\frac{y_k}{\Delta x_k} - \frac{M_k\Delta x_k}{6} \right)
 \end{aligned} \tag{30}$$

Equations (21), (29), and (30) provide expressions for the values of the cubic spline function and its first and second derivatives in the k th interval. These expressions can be written for the cubic spline function and its first and second derivatives in the $(k - 1)$ th interval by replacing k with $k - 1$. Therefore, in the $(k - 1)$ th interval,

$$\begin{aligned}
 y(x) = & M_k \frac{(x - x_{k-1})^3}{6\Delta x_{k-1}} + M_{k-1} \frac{(x_k - x)^3}{6\Delta x_{k-1}} \\
 & + \left(\frac{y_k}{\Delta x_{k-1}} - \frac{M_k\Delta x_{k-1}}{6} \right) (x - x_{k-1}) \\
 & + \left(\frac{y_{k-1}}{\Delta x_{k-1}} - \frac{M_{k-1}\Delta x_{k-1}}{6} \right) (x_k - x)
 \end{aligned} \tag{31}$$

$$\begin{aligned}
 y'(x) = & M_k \frac{(x - x_{k-1})^2}{2\Delta x_{k-1}} - M_{k-1} \frac{(x_k - x)^2}{2\Delta x_{k-1}} \\
 & + \left(\frac{y_k}{\Delta x_{k-1}} - \frac{M_k\Delta x_{k-1}}{6} \right) - \left(\frac{y_{k-1}}{\Delta x_{k-1}} - \frac{M_{k-1}\Delta x_{k-1}}{6} \right)
 \end{aligned} \tag{32}$$

$$y''(x) = M_k \frac{(x - x_{k-1})}{\Delta x_{k-1}} + M_{k-1} \frac{(x_k - x)}{\Delta x_{k-1}} \tag{33}$$

A cursory inspection of equations (29) and (31) and equations (21) and (33) will show that neither the cubic spline function nor its second derivative will experience discontinuity in going from the $(k - 1)$ th to the k th interval. This may be shown simply by replacing x with x_k in these expressions. To ensure that the cubic spline functions will experience no discontinuity in the first derivative in going from the $(k - 1)$ th to the k th interval, replace x with x_k in equations (30) and (32) and equate the results. Thus,

$$\begin{aligned} M_k \frac{\Delta x_{k-1}}{2} + \left(\frac{y_k}{\Delta x_{k-1}} - \frac{M_k \Delta x_{k-1}}{6} \right) - \left(\frac{y_{k-1}}{\Delta x_{k-1}} - \frac{M_{k-1} \Delta x_{k-1}}{6} \right) \\ = -M_k \frac{\Delta x_k}{2} + \left(\frac{y_{k+1}}{\Delta x_k} - \frac{M_{k+1} \Delta x_k}{6} \right) - \left(\frac{y_k}{\Delta x_k} - \frac{M_k \Delta x_k}{6} \right) \end{aligned} \quad (34)$$

or

$$\frac{\Delta x_{k-1}}{6} M_{k-1} + \frac{\Delta x_{k-1} + \Delta x_k}{3} M_k + \frac{\Delta x_k}{6} M_{k+1} = \frac{\Delta y_k}{\Delta x_k} - \frac{\Delta y_{k-1}}{\Delta x_{k-1}} \quad (35)$$

where $\Delta y_k = y_{k+1} - y_k$ and $\Delta y_{k-1} = y_k - y_{k-1}$. Equation (35) permits the writing of k equations for the solution of $k + 2$ unknown values of M . Clearly, two second derivative values must be supplied at any two of the tabulated data points. However, if the second derivatives are not known, first derivative values may be used through equation (30). Further, if both the first and second derivatives of the function are known at any one of the tabulated points, the set of simultaneous equations given by equation (35) can still be solved.

Solving for M_{k+1} in equation (35) gives

$$\begin{aligned} M_{k+1} &= -\frac{2(\Delta x_k + \Delta x_{k-1})M_k}{\Delta x_k} - \frac{\Delta x_{k-1}}{\Delta x_k} M_{k-1} + \frac{6}{\Delta x_k} \left(\frac{\Delta y_k}{\Delta x_k} - \frac{\Delta y_{k-1}}{\Delta x_{k-1}} \right) \\ &= a_k M_k + b_k M_{k-1} + c_k \end{aligned} \quad (36)$$

where

$$a_k = -\frac{2(\Delta x_k + \Delta x_{k-1})}{\Delta x_k} \quad (37)$$

$$b_k = -\frac{\Delta x_{k-1}}{\Delta x_k} \quad (38)$$

$$c_k = \frac{6}{\Delta x_k} \left(\frac{\Delta y_k}{\Delta x_k} - \frac{\Delta y_{k-1}}{\Delta x_{k-1}} \right) \quad (39)$$

Assume a solution of the form

$$M_{k+1} = \frac{1}{Q_k} (M_k - U_k) \quad (40)$$

so that in the $(k - 1)$ th interval

$$M_{k-1} = Q_{k-1} M_k + U_{k-1} \quad (41)$$

Substituting equation (41) in equation (36) gives

$$\begin{aligned} M_{k+1} &= a_k M_k + b_k (Q_{k-1} M_k + U_{k-1}) + c_k \\ &= (a_k + b_k Q_{k-1}) M_k + b_k U_{k-1} + c_k \end{aligned} \quad (42)$$

Comparing equations (40) and (42) gives

$$\frac{1}{Q_k} = a_k + b_k Q_{k-1} \quad (43)$$

or

$$Q_k = \frac{1}{a_k + b_k Q_{k-1}} \quad (44)$$

and

$$-\frac{U_k}{Q_k} = b_k U_{k-1} + c_k \quad (45)$$

or

$$U_k = -Q_k (b_k U_{k-1} + c_k) \quad (46)$$

Substituting equations (37), (38), and (39) in equations (44) and (46) gives

$$Q_k = -\frac{\Delta x_k}{2(\Delta x_k + \Delta x_{k-1}) + \Delta x_{k-1} Q_{k-1}} = -\frac{\Delta x_k}{2(x_{k+1} - x_{k-1}) + \Delta x_{k-1} Q_{k-1}} \quad (47)$$

$$\begin{aligned} U_k &= -Q_k \left[-\frac{\Delta x_{k-1}}{\Delta x_k} U_{k-1} + \frac{6}{\Delta x_k} \left(\frac{\Delta y_k}{\Delta x_k} - \frac{\Delta y_{k-1}}{\Delta x_{k-1}} \right) \right] \\ &= \frac{Q_k}{\Delta x_k} \left[\Delta x_{k-1} U_{k-1} + 6 \left(\frac{\Delta y_{k-1}}{\Delta x_{k-1}} - \frac{\Delta y_k}{\Delta x_k} \right) \right] \end{aligned} \quad (48)$$

Equations (40), (41), (47), and (48) are the recursive relations that will be used for the solution of the set of simultaneous linear equations given by equation (35). Before this is done, equations (29) and (30) will be put in a more convenient form by using the following difference operators.

$$d_k = x - x_k \quad (49)$$

$$d_{k+1} = x - x_{k+1} \quad (50)$$

Adding and subtracting x_k to the right-hand side of equation (50) gives

$$d_{k+1} = x - x_{k+1} + x_k - x_k = d_k - \Delta x_k \quad (51)$$

Substituting equations (49) and (50) in equations (29) and (30) gives

$$y(x) = M_{k+1} \frac{d_k^3}{6\Delta x_k} - M_k \frac{d_{k+1}^3}{6\Delta x_k} + \left(\frac{y_{k+1}}{\Delta x_k} - \frac{M_{k+1}\Delta x_k}{6} \right) d_k - \left(\frac{y_k}{\Delta x_k} - \frac{M_k\Delta x_k}{6} \right) d_{k+1} \quad (52)$$

$$\begin{aligned} y'(x) &= M_{k+1} \frac{d_k^2}{2\Delta x_k} - M_k \frac{d_{k+1}^2}{2\Delta x_k} + \left(\frac{y_{k+1}}{\Delta x_k} - \frac{M_{k+1}\Delta x_k}{6} \right) - \left(\frac{y_k}{\Delta x_k} - \frac{M_k\Delta x_k}{6} \right) \\ &= M_{k+1} \frac{d_k^2}{2\Delta x_k} - M_k \frac{d_{k+1}^2}{2\Delta x_k} + \frac{\Delta y_k}{\Delta x_k} - \frac{\Delta M_k \Delta x_k}{6} \end{aligned} \quad (53)$$

where $\Delta M_k = M_{k+1} - M_k$.

From equations (49), (50), and (51), when $x = x_k$, then $d_k = 0$ and $d_{k+1} = -\Delta x_k$; when $x = x_{k+1}$, then $d_k = \Delta x_k$ and $d_{k+1} = 0$. Substituting these results in equation (53) gives, for $x = x_k$,

$$\begin{aligned} y'(x_k) &= -M_k \frac{\Delta x_k}{2} + \left(\frac{y_{k+1}}{\Delta x_k} - \frac{M_{k+1}\Delta x_k}{6} \right) - \left(\frac{y_k}{\Delta x_k} - \frac{M_k\Delta x_k}{6} \right) \\ &= \frac{\Delta y_k}{\Delta x_k} - \frac{\Delta x_k}{6} (M_{k+1} + 2M_k) \end{aligned} \quad (54)$$

and, for $x = x_{k+1}$,

$$\begin{aligned} y'(x_{k+1}) &= M_{k+1} \frac{\Delta x_k}{2} + \left(\frac{y_{k+1}}{\Delta x_k} - \frac{M_{k+1}\Delta x_k}{6} \right) - \left(\frac{y_k}{\Delta x_k} - \frac{M_k\Delta x_k}{6} \right) \\ &= \frac{\Delta y_k}{\Delta x_k} + \frac{\Delta x_k}{6} (M_k + 2M_{k+1}) \end{aligned} \quad (55)$$

The use of these recursive relations is described in the following six cases.

Case 1: Solution of the set of simultaneous equations given by equation (35) when the second derivatives of the function are known at the initial and terminal tabulated boundaries. In this case, $y''(x_1) = M_1$ and $y''(x_n) = M_n$. From equation (41) with $k = 2$, if $Q_1 = 0$, then $M_1 = U_1$. By using these values for Q_1 and U_1 , equations (47) and (48) can be used to generate values of Q_k and U_k , recursively, for all values of k ranging from 2 to $n - 1$. After these values are available, then all values of M_k can be computed by using equation (40) written in the form of equation (41)

$$M_k = Q_k M_{k+1} + U_k \quad (56)$$

and propagating the solution backwards with k ranging from $n - 1$ to 2. As M_n and M_1 are known, all n second-derivative values will be available.

Case 2: Solution of the set of simultaneous equations given by equation (35) when the first derivatives of the function are known at the initial and terminal tabulated boundaries. In this case, $y'(x_1) = D_1$ and $y'(x_n) = D_n$. Substitute $k = 1$ in equation (54) for M_{k+1} from equation (40) and solve for U_1 to get

$$\left. \begin{aligned} y'(x_1) = D_1 &= \frac{\Delta y_1}{\Delta x_1} - \frac{\Delta x_1}{6} \left(\frac{M_1 - U_1}{Q_1} + 2M_1 \right) \\ U_1 &= Q_1 \left[M_1 \left(2 + \frac{1}{Q_1} \right) + \frac{6}{\Delta x_1} \left(D_1 - \frac{\Delta y_1}{\Delta x_1} \right) \right] \end{aligned} \right\} \quad (57)$$

If $Q_1 = -1/2$, then from equation (57),

$$U_1 = \frac{3}{\Delta x_1} \left(\frac{\Delta y_1}{\Delta x_1} - D_1 \right) \quad (58)$$

By using $Q_1 = -1/2$ and the value obtained for U_1 from equation (58), compute all values of Q_k and U_k from equations (47) and (48) for values of k ranging from 2 to $n - 1$. With the value of Q_{n-1} and U_{n-1} thus computed, substitute

equation (41) in equation (55) for M_{n-1} such that at $x = x_n$,

$$y'(x_n) = D_n = \frac{\Delta y_{n-1}}{\Delta x_{n-1}} + \frac{\Delta x_{n-1}}{6} \left(Q_{n-1} M_{n-1} + U_{n-1} + 2M_n \right) \quad (59)$$

Solving for M_n from equation (59) gives

$$M_n = \frac{\frac{6}{\Delta x_{n-1}} \left(D_n - \frac{\Delta y_{n-1}}{\Delta x_{n-1}} \right) - U_{n-1}}{2 + Q_{n-1}} \quad (60)$$

With the value of M_n known, the solution can be propagated backward by using equation (41) with k ranging from $n - 1$ to 1. Thus, M_1 will be computed as the last value.

Case 3: Solution of the set of simultaneous equations given by equation (35) when the first and second derivatives of the function are known, respectively, at the initial and terminal tabulated boundaries. In this case, $y'(x_1) = D_1$ and $y''(x_n) = M_n$. Proceed as in case 2 excluding the computation for M_n , which is not needed.

Case 4: Solution of the set of simultaneous equations given by equation (35) when the first and second derivatives of the function are known, respectively, at the terminal and initial tabulated boundaries. In this case, $y'(x_n) = D_n$ and $y''(x_1) = M_1$. Proceed as in case 1 and compute the value of M_n as in case 2.

Case 5: Solution of the set of simultaneous equations given by equation (35) when the first and second derivatives of the function are known at the initial tabulated boundary. In this case, $y'(x_1) = D_1$ and $y''(x_1) = M_1$. From equation (56), if $Q_1 = 1$, then

$$U_1 = 3M_1 + \frac{6}{\Delta x_1} \left(D_1 - \frac{\Delta y_1}{\Delta x_1} \right) \quad (61)$$

With the value of $Q_1 = 1$ and the value of U_1 given by equation (61), compute all values of Q_k and U_k from equations (47) and (48) for $k = 2$ to $n - 1$. With these values of Q_k and U_k known, compute values for the second derivative from equation (40) by propagating the solution forward for k ranging from 1 to $n - 1$. The last value thus computed is M_n .

Case 6: Solution of the set of simultaneous equations given by equation (35) when the first and second derivatives of the function are known at the terminal tabulated boundary. In this case, $y'(x_n) = D_n$ and $y''(x_n) = M_n$. In equation (55), substitute M_k in equation (41) with $k = n - 1$ and solve for U_{n-1} to get

$$\left. \begin{aligned} y'(x_n) = D_n &= \frac{\Delta y_{n-1}}{\Delta x_{n-1}} + \frac{\Delta x_{n-1}}{6} (Q_{n-1} M_n + U_{n-1} + 2M_n) \\ U_{n-1} &= \frac{6}{\Delta x_{n-1}} \left(D_n - \frac{\Delta y_{n-1}}{\Delta x_{n-1}} \right) - M_n (2 + Q_{n-1}) \end{aligned} \right\} \quad (62)$$

If $Q_{n-1} = 1$, then from equation (62),

$$U_{n-1} = \frac{6}{\Delta x_{n-1}} \left(D_n - \frac{\Delta y_{n-1}}{\Delta x_{n-1}} \right) - 3M_n \quad (63)$$

Solving for Q_{k-1} and U_{k-1} from equations (47) and (48) gives

$$Q_{k-1} = -\frac{1}{\Delta x_{k-1}} \left[\frac{\Delta x_k}{Q_k} + 2(\Delta x_k + \Delta x_{k-1}) \right] = -\frac{1}{\Delta x_{k-1}} \left[\frac{\Delta x_k}{Q_k} + 2(x_{k+1} - x_{k-1}) \right] \quad (64)$$

$$U_{k-1} = \frac{1}{\Delta x_{k-1}} \left[U_k \frac{\Delta x_k}{Q_k} - 6 \left(\frac{\Delta y_{k-1}}{\Delta x_{k-1}} - \frac{\Delta y_k}{\Delta x_k} \right) \right] \quad (65)$$

With $Q_{n-1} = 1$ and U_{n-1} given by equation (63), compute all values of Q_{k-1} and U_{k-1} from equations (64) and (65) for values of k ranging from $n - 1$ to 2. With the values of Q_k and U_k known, compute values for the second derivatives from equation (40) by propagating the solution backwards for k ranging from $n - 1$ to 1. The last value thus computed will be M_1 .

Clearly, the solutions for case 5 and case 6 could have been obtained from equations (54) and (55). In the solution for case 5, M_{k+1} can be obtained from equation (54) and $y'(x_{k+1})$ from equation (55). The solution can be propagated forward recursively with k ranging from 1 to $n - 1$. In the solution for case 6, M_k can be obtained from equation (55) and $y'(x_k)$ from equation (54). The solution can be propagated backward recursively with k ranging from $n - 1$ to 1.

If equation (52) is written with d_{k+1} replaced by its equivalent $d_{k+1} = d_k - \Delta x_k$ given by equation (51), the result is

$$\begin{aligned}
 y(x) = & M_{k+1} \frac{d_k^3}{6\Delta x_k} - M_k \frac{(d_k - \Delta x_k)^3}{6\Delta x_k} + \left(\frac{y_{k+1}}{\Delta x_k} - \frac{M_{k+1}\Delta x_k}{6} \right) d_k \\
 & - \left(\frac{y_k}{\Delta x_k} - \frac{M_k\Delta x_k}{6} \right) (d_k - \Delta x_k) = y_k + \left[\frac{\Delta y_k}{\Delta x_k} - \frac{\Delta x_k}{6} (M_{k+1} + 2M_k) \right] d_k \\
 & + \frac{M_k}{2} d_k^2 + \frac{\Delta M_k}{6\Delta x_k} d_k^3
 \end{aligned} \tag{66}$$

Equation (66) is the equation for the cubic spline function coefficients in the k th interval. If there are n data points in the tabulation, there will be $n - 1$ intervals and $n - 1$ cubic spline functions to cover the range of tabulated data.

For computation purposes, equation (67) is usually written as

$$y(x) = y_k + \left\{ \left[c_3(k)d_k + c_2(k) \right] d_k + c_1(k) \right\} d_k \tag{67}$$

where

$$c_1(k) = \frac{\Delta y_k}{\Delta x_k} - \frac{\Delta x_k}{6} (M_{k+1} + 2M_k) \tag{68}$$

$$c_2(k) = \frac{M_k}{2} \tag{69}$$

$$c_3(k) = \frac{\Delta M_k}{6\Delta x_k} \tag{70}$$

Equations (67) through (70) show that the coefficients are functions of the interval; however, the coefficients need to be computed only once. After the computation is made, the set pertaining to the interval in which the value of the independent variable lies can be brought in to compute the value of the dependent variable needed. Because there are three coefficients for each interval, if there are n data points, there will be $n - 1$ intervals and $3(n - 1)$ coefficients.

CONCLUDING REMARKS AND RECOMMENDATIONS

The atmosphere package for the 1962 and 1966 standard atmosphere models is recommended without reservation. When these models were built, it was possible to conduct comparison checks with the layered versions of these models in 250-meter increments. In both packages, these tests revealed errors that were properly corrected. The package for the 1963 Patrick Air Force Base reference standard model was not subjected to such strenuous tests because the layered version of this model was not available. However, with the other models so thoroughly tested, the choice of altitudes was established as adequate, and the only requirement for the Patrick Air Force Base reference standard model was to ensure that the data were tabulated correctly. The laborious task of comparing (digit for digit) each tabulated number in the model printouts with the numbers in the reference source was performed as carefully as possible, and all errors found were corrected. As a result, the accuracy of this model is reasonably ensured.

To test the accuracy of these models after they have been recoded for use in the Software Development Laboratory, the only requirement is to have the package reproduce the tabulated data. Because the interpolation is to be performed in a different set of units, the output must be converted to the units of the tabulated data for ease of comparison. The results should agree within an error of no greater than 10^{-8} . Additional verification can be obtained by evaluating the parameters of the models at various altitudes and comparing the results with those obtained from established operational sources, such as the space vehicle dynamic simulator and the Shuttle optimal abort programs. These tests should be performed for all models.

It is recommended that where the first and second derivatives are known at the same data point the cubic spline functions be used to interpolate data only in a small neighborhood of this point and not be extended for interpolation over the entire range of tabulated data.

Lyndon B. Johnson Space Center
National Aeronautics and Space Administration
Houston, Texas, June 4, 1976
986-16-00-00-72

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1. United States Committee on Extension to the Standard Atmosphere: U. S. Standard Atmosphere, 1962. U. S. Government Printing Office, 1962.
2. United States Committee on Extension to the Standard Atmosphere: U. S. Standard Atmosphere Supplements, 1966. U. S. Government Printing Office, 1966.
3. Smith, O. E.; and Weidner, Don K.: A Reference Atmosphere for Patrick Air Force Base, Florida, Annual (1963 Revision). NASA TM X-53139, 1964.

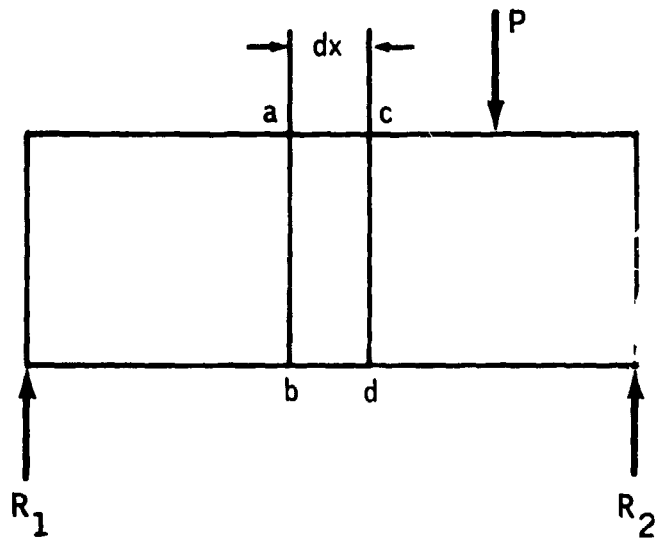


Figure 1.- Undeformed beam.

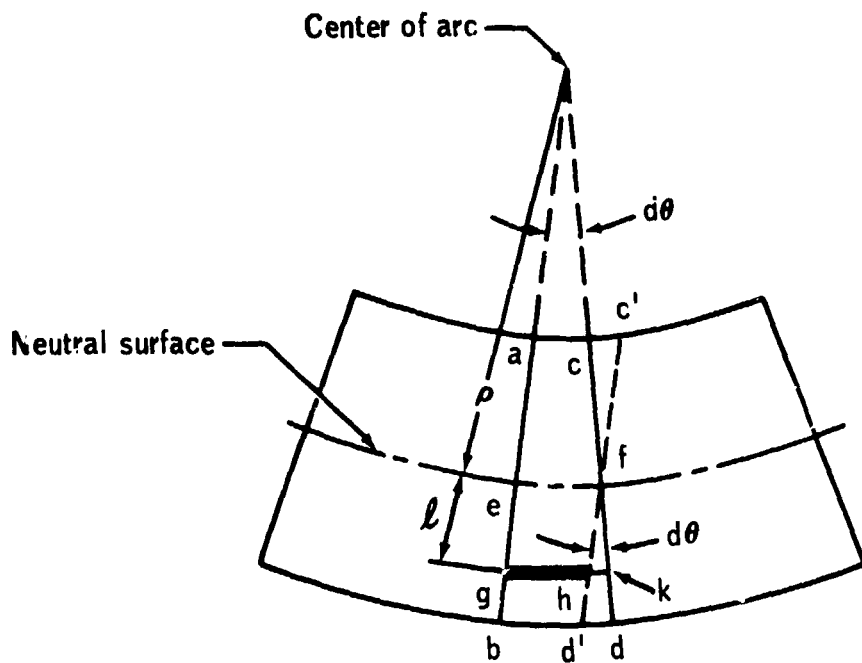


Figure 2.- Deformed section of a beam.

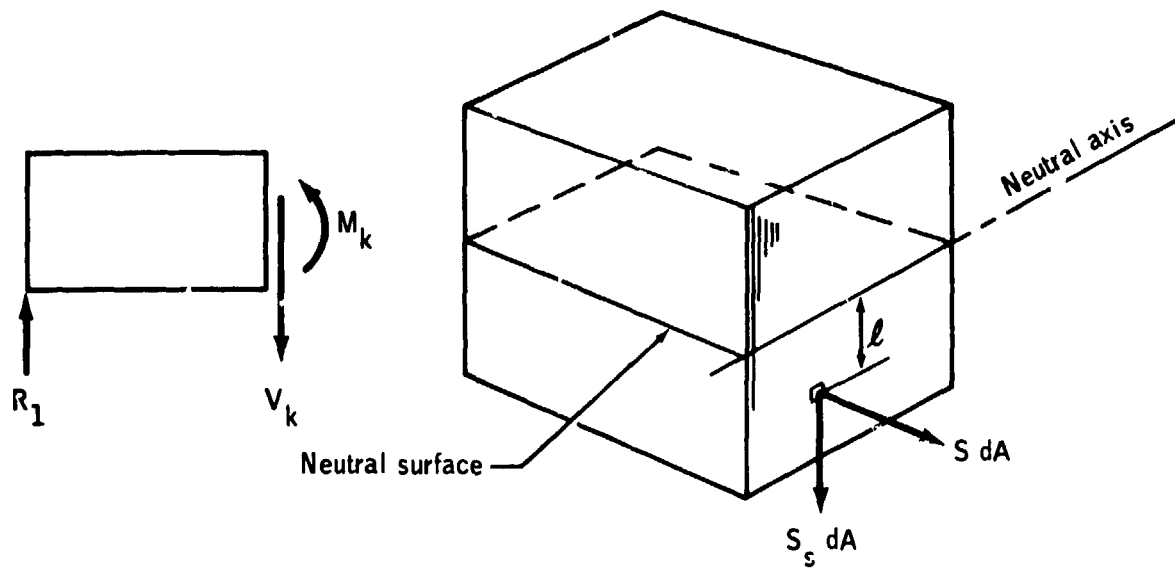


Figure 3.- Element of the cross section of a beam.

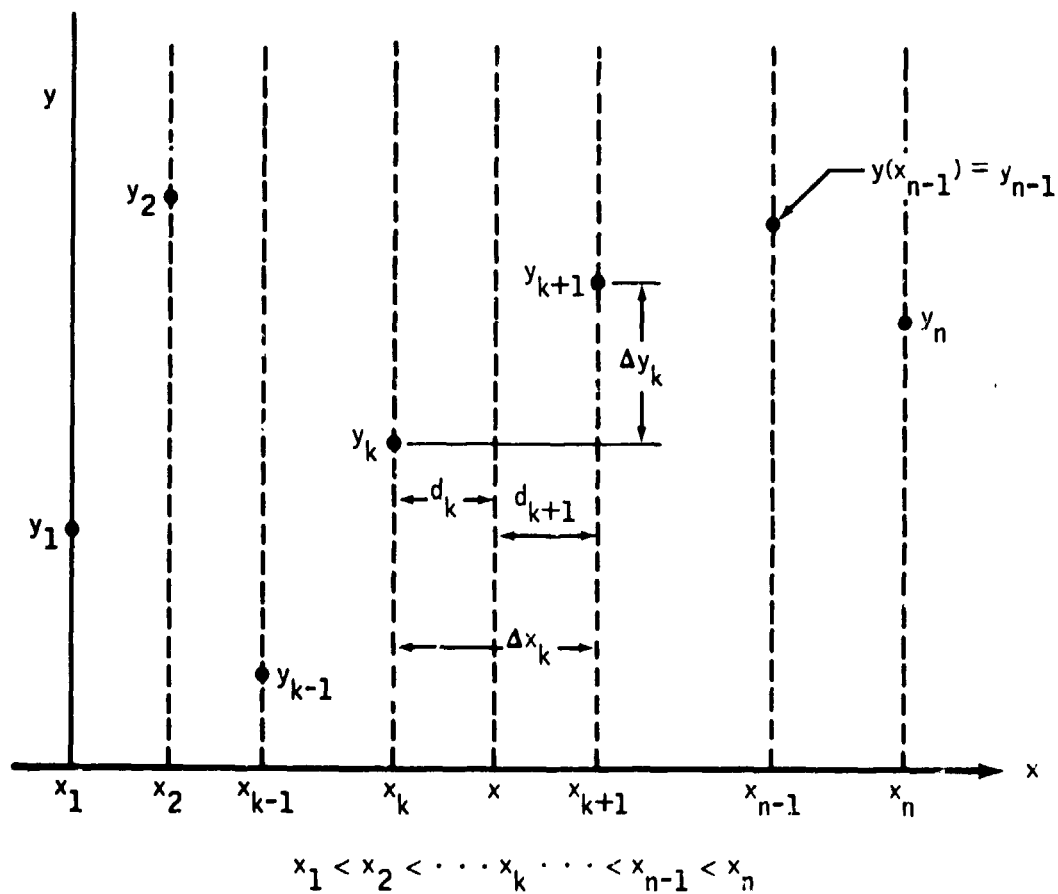


Figure 4.- Graph of a tabulated set of data for cubic spline interpolation.

APPENDIX

PROGRAM FLOW CHARTS AND LISTINGS

Definitions of the symbols used in the program flow charts and listings are as follows.

SYMBOLS USED IN SUBROUTINE SDAT (IOP)

- IOP** an integer parameter used to designate the desired atmosphere based on the following set of values:
- IOP = 0** 1962 standard atmosphere
 - IOP = 1** 1966 standard atmosphere for July at latitude 30° N
 - IOP = 2** 1966 standard atmosphere for January at latitude 30° N
 - IOP = 3** 1966 standard atmosphere for July at latitude 60° N
 - IOP = 4** 1966 standard atmosphere for January at latitude 60° N
 - IOP = 5** 1963 Patrick Air Force Base reference standard atmosphere
- NF** an integer variable used to specify the number of data points used to describe each atmospheric parameter in each model (equal to 123)
- NP64** an integer variable used to specify the total number of data points used to describe all atmospheric parameters in each atmosphere model (equal to $6 \cdot NP$ or $6 \times 123 = 738$)
- NP34** an integer variable used to specify the total number of cubic spline coefficients for each atmospheric parameter (equal to $3 \cdot (NP - 1)$ or $3 \cdot (123 - 1) = 366$)
- PRSLST** a column vector array dimensioned by NP64 or 738 containing all pressure data values (in millibars) for all atmosphere models tabulated
- RHOLST** a column vector array dimensioned by NP64 or 738 containing all density data values (in kilograms per cubic meter) for all atmosphere models tabulated
- SONLST** a column vector array dimensioned by NP64 or 738 containing all speed of sound data values (in meters per second) for all atmosphere models tabulated

VISLST a column vector array dimensioned by NP64 or 738 containing all coefficient of viscosity data values (in kilograms per meter per second) for all atmosphere models tabulated

ALTLST a column vector array dimensioned by NP or 123 containing the altitude data values (in meters) for all atmosphere models tabulated

WORK a column vector array dimensioned by NP or 123 used as a working array for subroutine SPLN1

D a column vector array dimensioned by 2 containing the values of the first (or second) derivative of the function at either or both of the tabulated terminal boundaries (only first-derivative values are used for the atmosphere package)

ALTTAB a column vector array dimensioned by NP or 123 containing altitude values in the working units of the program (feet)

PRSTAB a column vector array dimensioned by NP or 123 containing pressure data values for the selected atmosphere model in the working units of the program (pounds-force per square foot)

RHOTAB a column vector array dimensioned by NP or 123 containing density data values for the selected atmosphere model in the working units of the program (slugs per cubic foot)

SONTAB a column vector array dimensioned by NP or 123 containing speed of sound data values for the selected atmosphere model in the working units of the program (feet per second)

VISTAB a column vector array dimensioned by NP or 123 containing the coefficient of viscosity data values for the selected atmosphere model in the working units of the program (pounds-mass seconds per square foot)

CP a column vector array dimensioned by NP34 or 366 containing the cubic spline function coefficients for the interpolation for pressure in pounds-force per square foot

CR a column vector array dimensioned by NP34 or 366 containing the cubic spline function coefficients for the interpolation for density in slugs per cubic foot

CS a column vector array dimensioned by NP34 or 366 containing the cubic spline function coefficients for the interpolation for the speed of sound in feet per second

- CV** a column vector array dimensioned by NP34 or 366 containing the cubic spline function coefficients for the interpolation for the coefficient of viscosity in pounds-mass seconds per square foot
- J1** an integer variable used to designate the order of the derivative of the function supplied at the initial tabulated boundary (except when $J1 = 4$). It can have the following values:
- J1 = 1** The first derivative of the function at the first tabulated point is supplied in D(1).
- J1 = 2** The second derivative of the function at the first tabulated point is supplied in D(1).
- J1 = 3** The first and second derivatives of the function at the first tabulated point are supplied in D(1) and D(2), respectively.
- J1 = 4** The first and second derivatives of the function at the last tabulated point are supplied in D(1) and D(2), respectively.
- JN** an integer variable used to designate the order of the derivatives of the function supplied at the last tabulated boundary. It can have the following values:
- JN = 1** The first derivative of the function at the last tabulated point is supplied in D(2).
- JN = 2** The second derivative of the function at the last tabulated point is supplied in D(2).
- xs, ys1, ys2, ys3, ys4** Variables used for temporary storage in the ordering process for altitude, pressure, density, speed of sound, and coefficient of viscosity, respectively

SYMBOLS USED IN SUBROUTINE SPLN1(N,X,Y,J1,JN,D,C,W)

- N** an integer variable used to specify the number of data points used to represent the function in the region of definition
- X** a column vector array dimensioned by at least N in the calling element containing the values of the independent variable in ascending order
- Y** a column vector array dimensioned by at least N in the calling element containing the values of the dependent variable in sequence with the values in the X array
- J1** same as J1 defined in SDAT

- JN** same as JN defined in SDAT
- D** same as D defined in SDAT
- C** a column vector array dimensioned by at least $3*(N-1)$ in the calling element containing the cubic spline function coefficients for the first-, second-, and third-degree terms for each interval. A portion of the array is also used to compute and store the values of one of the recursive functions used in the computation of the second derivatives and in the computation of the second-derivative values.
- W** a column vector array dimensioned by at least N in the calling element used as a working array to compute and store the values of one of the recursive functions used in the computation of the second derivatives and in the computation of the cubic spline function coefficients

SYMBOLS USED IN SUBROUTINE ATMSPL(V,FANS)

- V** a real variable used to specify the altitude from the calling element containing the equations of motion at which values of the atmospheric parameters are desired
- IS** an integer variable used to save the interval number in which the specified altitude lies
- FANS** a column vector array dimensioned by 8 containing the following:
- FANS(1) the interpolated value for pressure at V altitude in pounds-force per square foot
 - FANS(2) the interpolated value for density at V altitude in slugs per cubic foot
 - FANS(3) the interpolated value for speed of sound at V altitude in feet per second
 - FANS(4) the interpolated value for coefficient of viscosity at V altitude in pounds-mass seconds per square foot
 - FANS(5) the ratio of the pressure at V altitude and the pressure at 0 altitude
 - FANS(6) the ratio of the density at V altitude and the density at 0 altitude
 - FANS(7) the ratio of the speed of sound at V altitude and the speed of sound at 0 altitude

**FANS(8) the ratio of the coefficient of viscosity at V altitude and the
coefficient of viscosity at 0 altitude**

All other variables are defined in subroutine SDAT.

SUBROUTINE SDAT(IOP)
PARAMETER NP = 123. NP64 = 6*NP. NP34 = 3*NP - 3
DATA J1,JN /1.1/

C IOP.....AN INTEGER VARIABLE RANGING FROM 0 TO 5 USED TO DESIGNATE
C THE ATMOSPHERE MODEL TO BE USED
C IOP = 0 - 1962 STANDARD ATMOSPHERE
C IOP = 1 - 1966 STANDARD FOR JULY AT 30 DEG. N. LATITUDE
C IOP = 2 - 1966 STANDARD FOR JAN. AT 30 DEG. N. LATITUDE
C IOP = 3 - 1966 STANDARD FOR JULY AT 60 DEG. N. LATITUDE
C IOP = 4 - 1966 STANDARD FOR JAN. AT 60 DEG. N. LATITUDE
C IOP = 5 - 1963 PATRICK AFB REFERENCE STANDARD

C SELECT DESIRED ATMOSPHERE INDEX ADJUSTOR

IOP1 = IOP*NP

C TRANSFER PERTINENT ATMOSPHERE DATA FROM STORAGE ARRAY TO WORKING
C ARRAY AND CONVERT TO DESIRED WORKING UNITS (BRITISH ENGINEERING)

DO 1 I = 1, NP - - - - > 2

C TRANSFER ALTITUDE VALUES LIST TO WORKING ARRAY

ALTTAB(I) = ALTLST(I)/0.3048

C TRANSFER PRESSURE VALUES LIST TO WORKING ARRAY

PRSTAB(I) = PRSLST(IOP1 + I)*2.11622/1.01325

C TRANSFER DENSITY VALUES LIST TO WORKING ARRAY

RHOTAB(I) = RHOLST(IOP1 + I)*7.6474E-2/(1.225*32.174049)

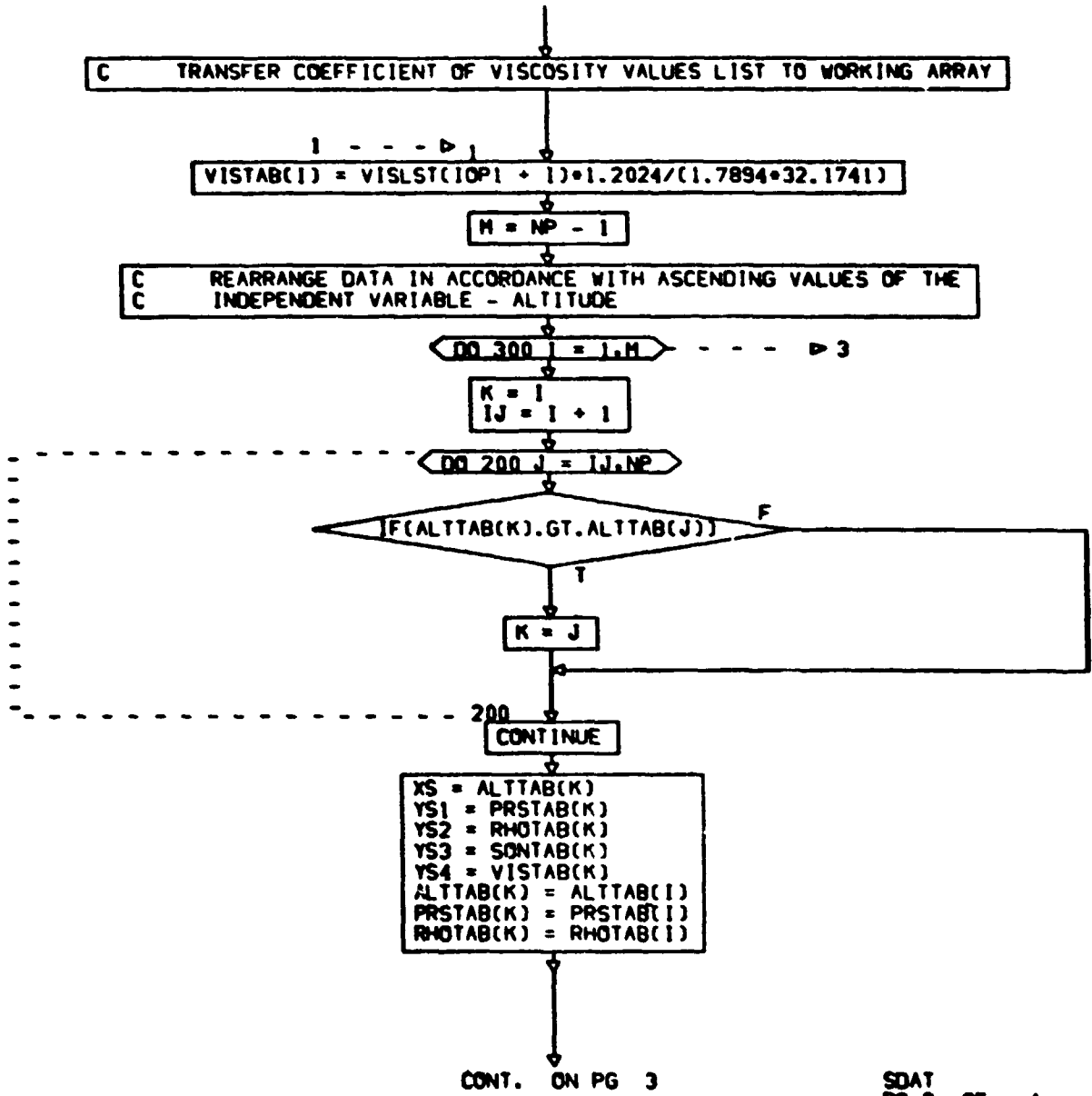
C TRANSFER SPEED OF SOUND VALUES LIST TO WORKING ARRAY

SONTAB(I) = SONLST(IOP1 + I)/0.3048

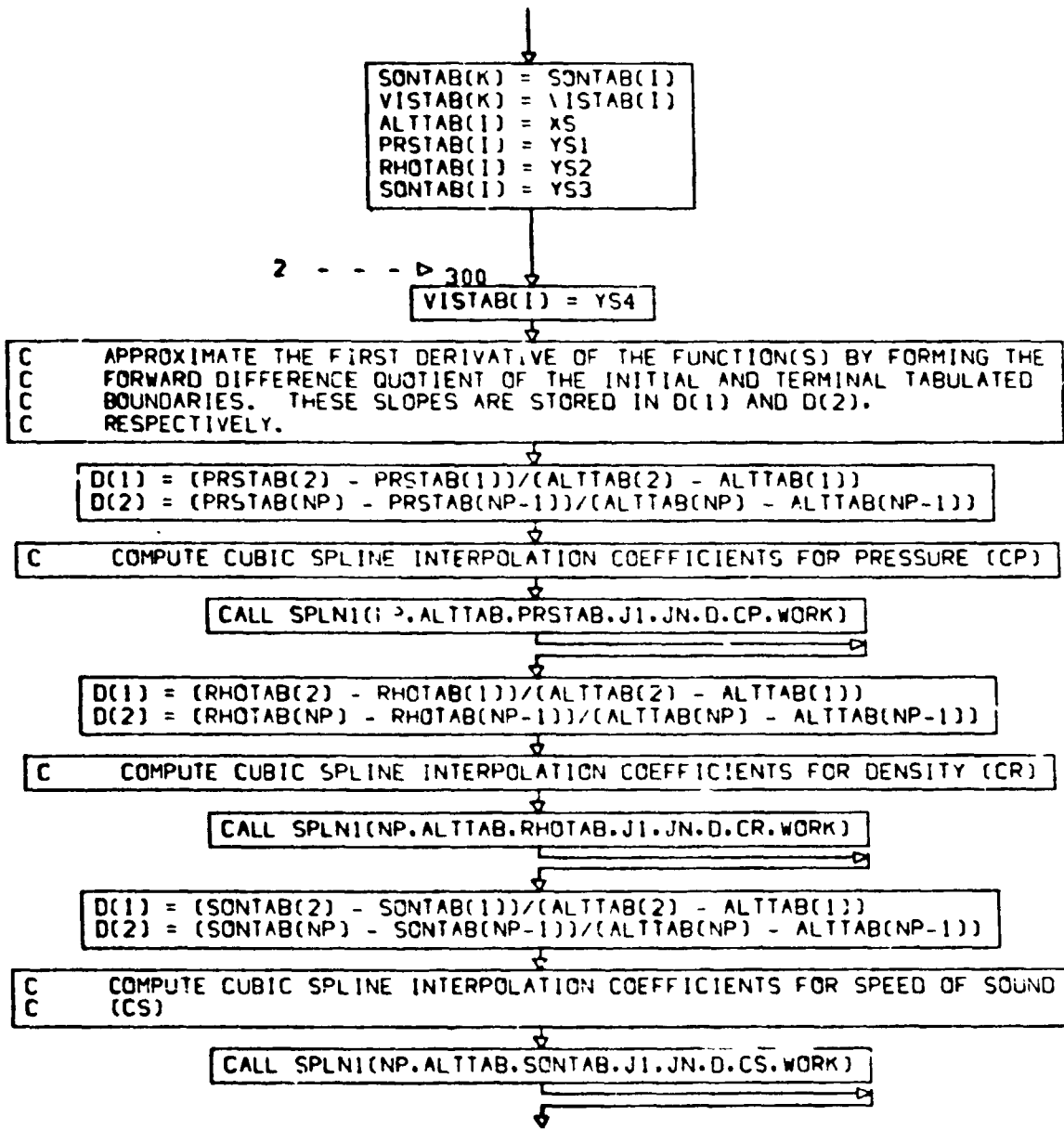
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SDAT
PG 1 OF 4

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SDAT
PG 2 OF 4

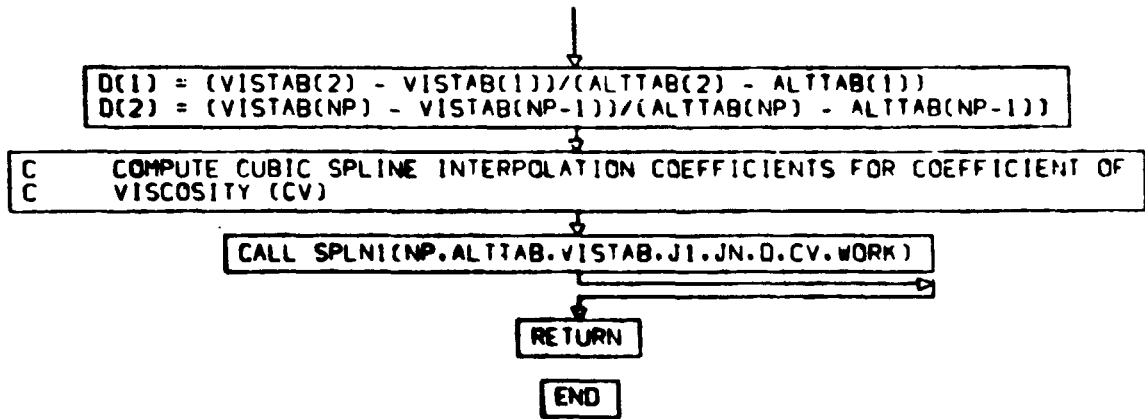


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PG 3 OF 4

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SUBROUTINE SPLN1(N,X,Y,J1,JN,D,C,W)

C N - AN INTEGER DENOTING THE NUMBER OF DATA POINTS USED TO
 C REPRESENT THE FUNCTION IN THE REGION OF DEFINITION
 C X - A ONE-DIMENSIONAL ARRAY DIMENSIONED BY N CONTAINING THE
 C VALUES OF THE INDEPENDENT VARIABLE IN ASCENDING ORDER
 C Y - A ONE-DIMENSIONAL ARRAY DIMENSIONED BY N CONTAINING THE
 C VALUES OF THE DEPENDENT VARIABLE CORRESPONDING IN
 C SEQUENCE TO THE VALUES IN THE X ARRAY
 C J1,JN - INTEGERS DEFINED AS FOLLOWS

C J1 = 1 - FIRST DERIVATIVE OF THE FUNCTION AT THE FIRST TABULATED
 C DATA POINT IS SUPPLIED IN D(1)
 C J1 = 2 - SECOND DERIVATIVE OF THE FUNCTION AT THE FIRST TABULATED
 C DATA POINT IS SUPPLIED IN D(1)
 C J1 = 3 - FIRST AND SECOND DERIVATIVES OF THE FUNCTION AT THE FIRST
 C DATA POINT ARE SUPPLIED IN D(1) AND D(2), RESPECTIVELY
 C J1 = 4 - FIRST AND SECOND DERIVATIVES OF THE FUNCTION AT THE LAST
 C DATA POINT ARE SUPPLIED IN D(1) AND D(2), RESPECTIVELY

C JN = 1 - FIRST DERIVATIVE OF THE FUNCTION AT THE LAST TABULATED
 C DATA POINT IS SUPPLIED IN D(2)
 C JN = 2 - SECOND DERIVATIVE OF THE FUNCTION AT THE LAST TABULATED
 C DATA POINT IS SUPPLIED IN D(2)
 C D - A ONE-DIMENSIONAL ARRAY DIMENSIONED BY 2 CONTAINING THE
 C VALUES OF THE DERIVATIVES OF THE FUNCTION SPECIFIED IN
 C ACCORDANCE WITH J2 AND JN
 C C - A ONE-DIMENSIONAL ARRAY DIMENSIONED BY 3*(N-1) CONTAINING

C THE CUBIC SPLINE INTERPOLATING COEFFICIENTS FOR EACH
 C INTERVAL
 C W - A ONE-DIMENSIONAL ARRAY DIMENSIONED BY N USED AS A WORKING
 C ARRAY ONLY
 C COMPUTE THE INITIAL VALUES OF THE RECURSIVE RELATIONS IN
 C ACCORDANCE WITH THE SPECIFIED PROPERTY OF THE FUNCTION AT THE
 C INITIAL BOUNDARY

GO TO (1,2,3,4),J1

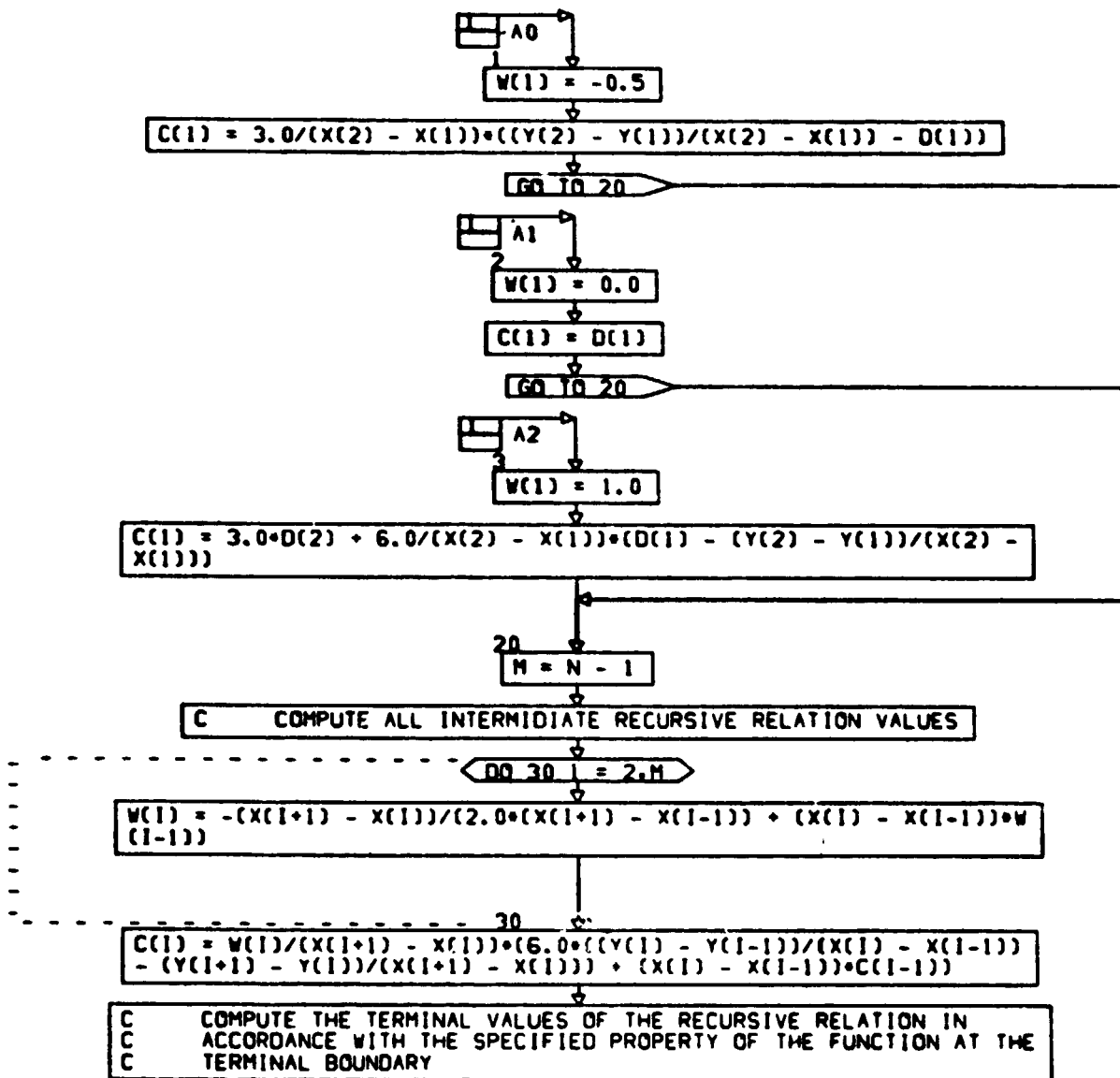
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A1	A1	A2	A3

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SPLN1
 PG 1 OF 5

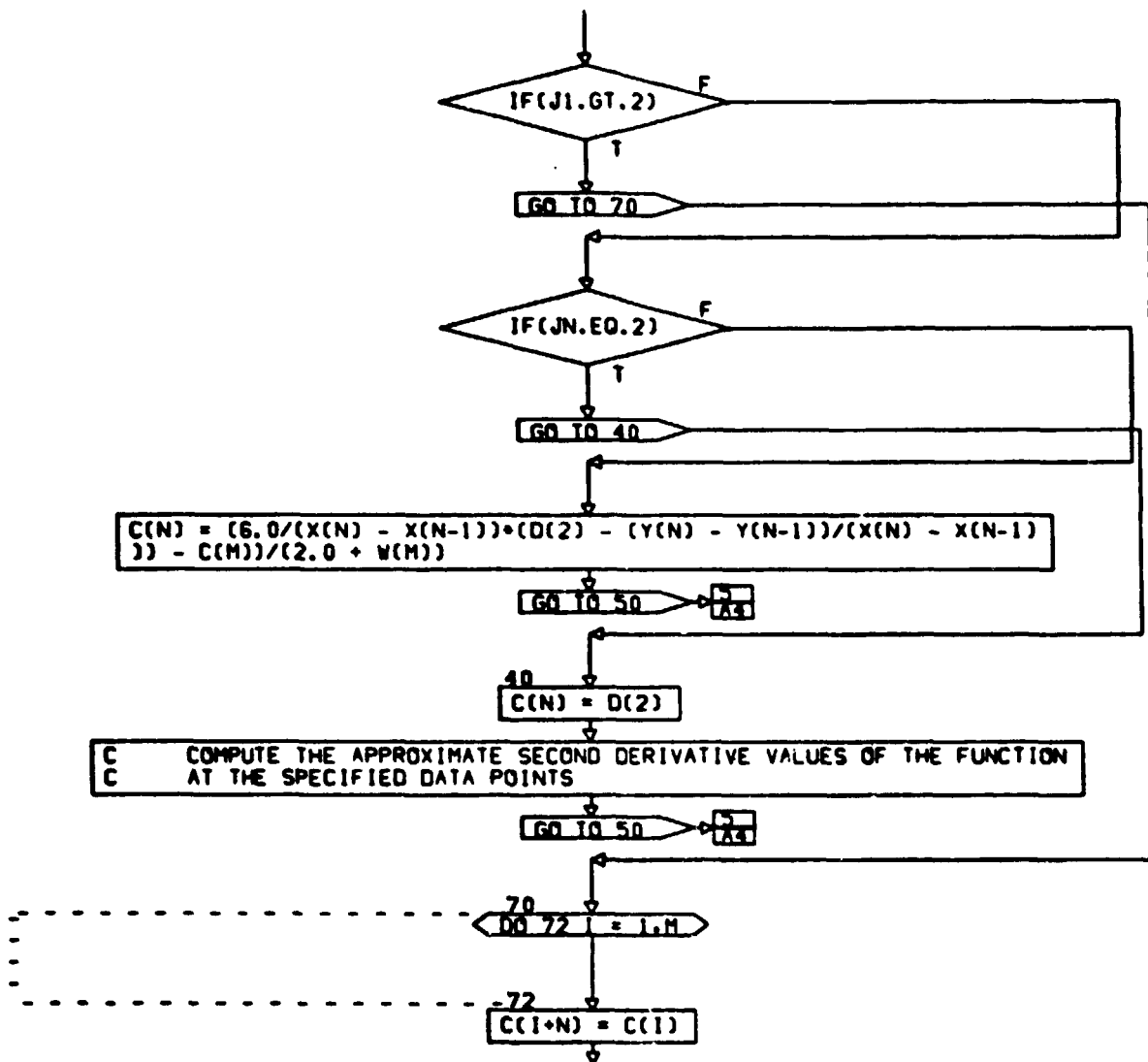
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APPENDIX



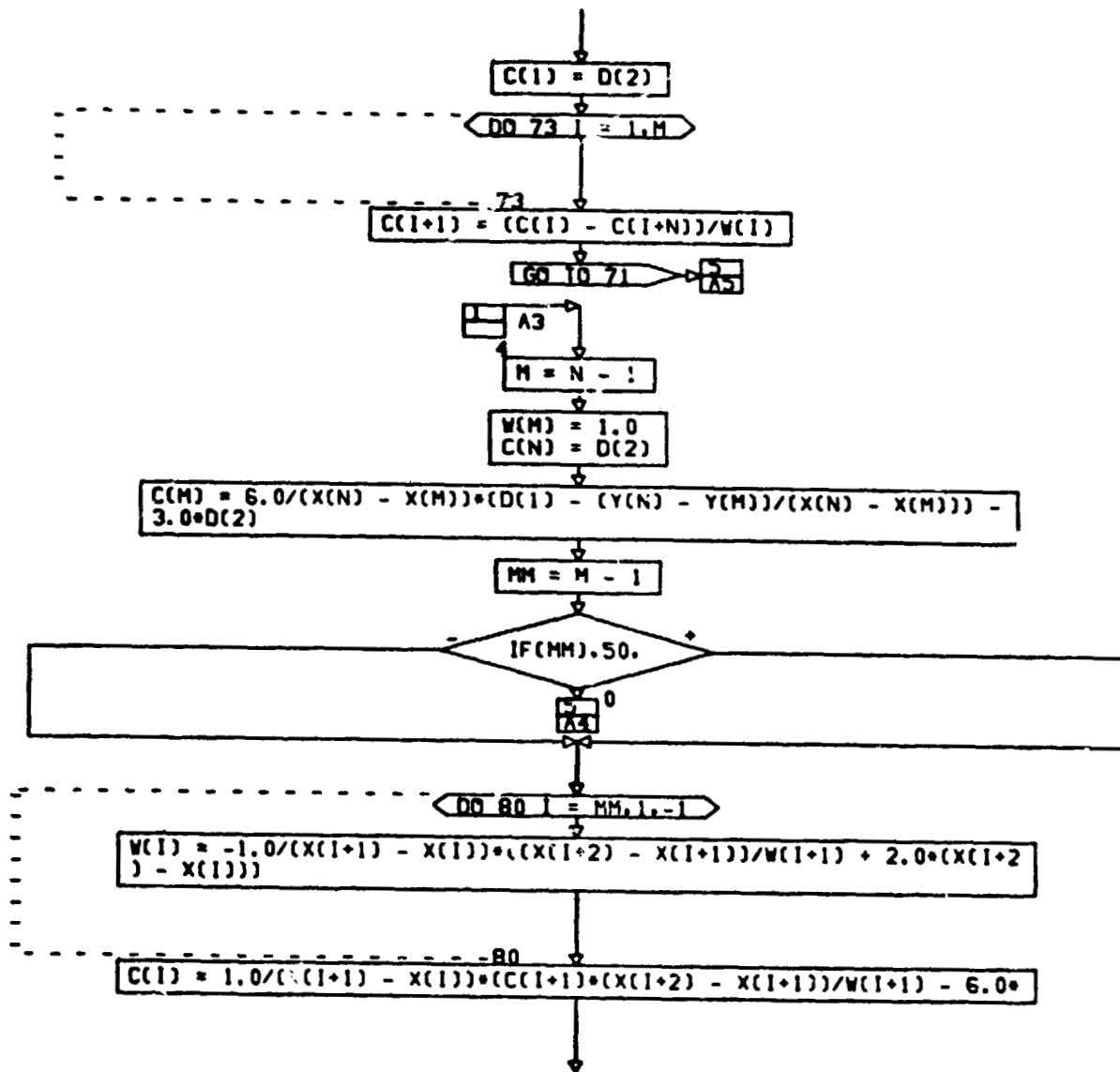
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SPLNI
PG 2 OF 5



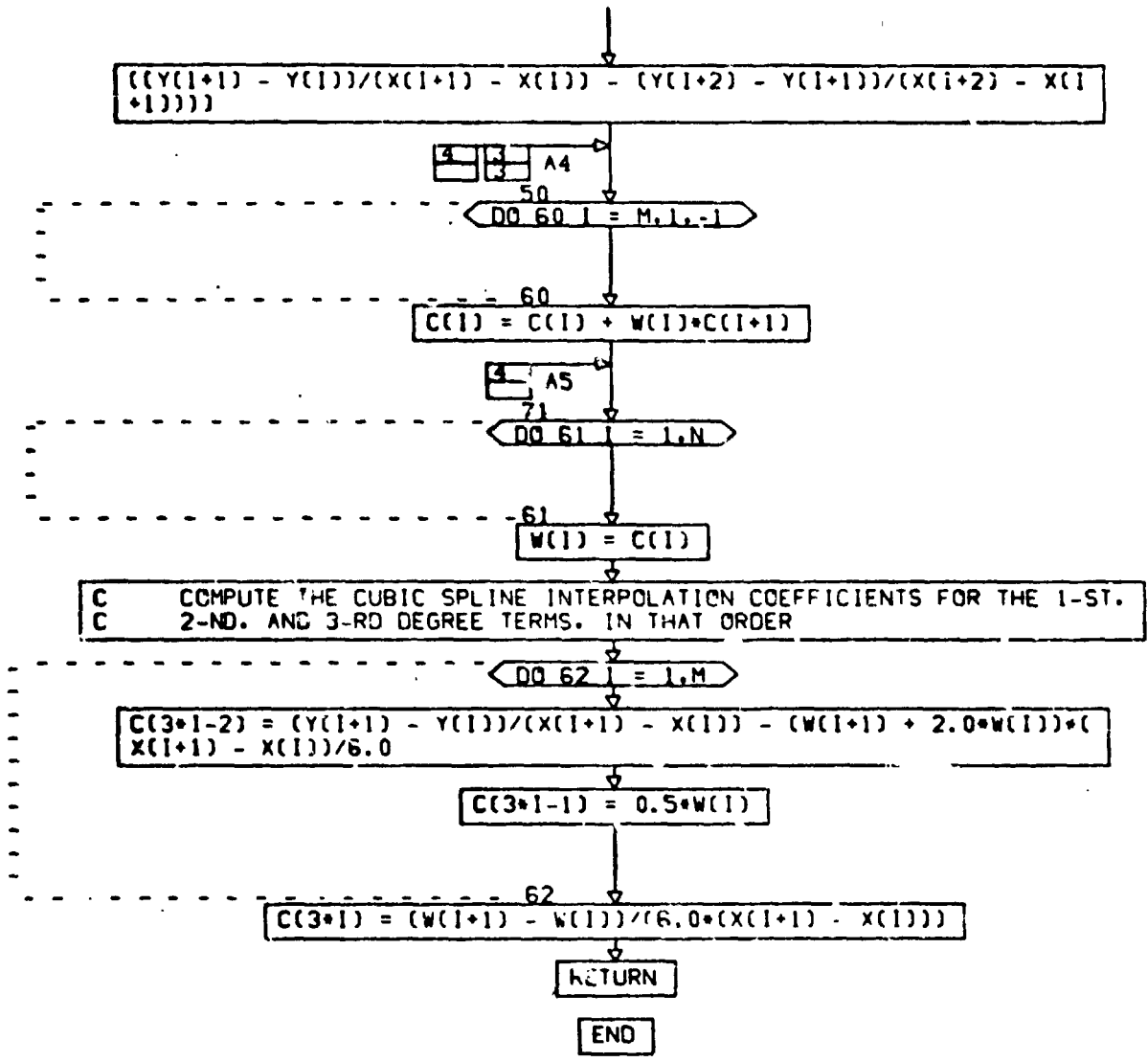
CONT. ON PG 4

SPLN1
PG 3 OF 5



CONT. ON PG 5

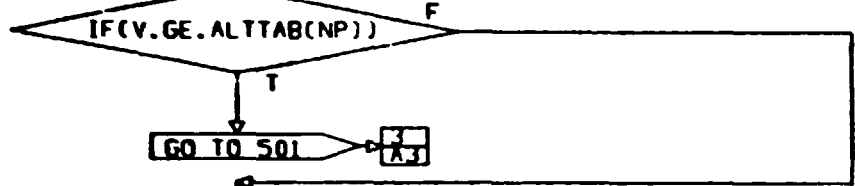
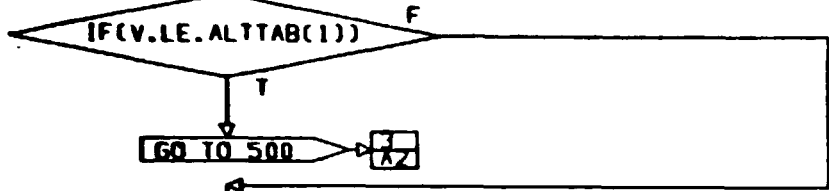
SPLN1
PG 4 OF 5



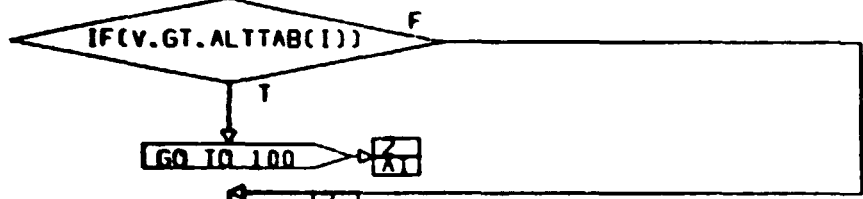
SPLN1
PG 5 FINAL

SUBROUTINE ATMSPL(V,FANS)
PARAMETER NP = 123, MP = 3*NP - 3
DATA IS / 1 /

C ESTABLISH THE INTERVAL IN WHICH THE SPECIFIED ALTITUDE LIES



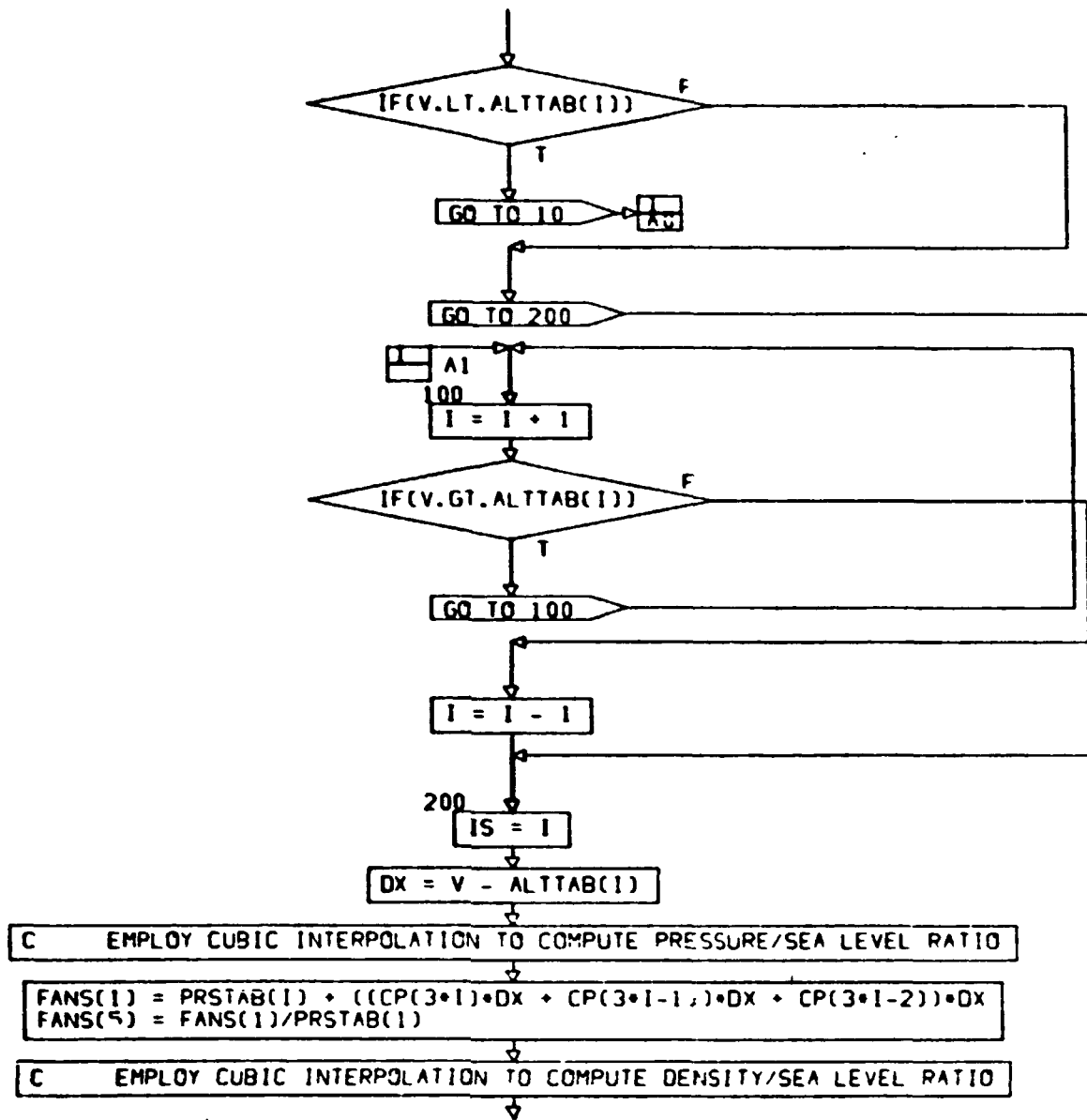
I = IS



I = I - 1

CONT. ON PG 2

ATMSPL
PG 1 OF 4



CONT. ON PG 3

ATMSPL
PG 2 OF 4

FANS(2) = RHOTAB(1) + ((CR(3*1)*DX + CR(3*1-1))*DX + CR(3*1-2))*DX
FANS(6) = FANS(2)/RHOTAB(1)

C EMPLOY CUBIC INTERPOLATION TO COMPUTE SPEED OF SOUND/SEA LEVEL RATIO
C

FANS(3) = SONTAB(1) + ((CS(3*1)*DX + CS(3*1-1))*DX + CS(3*1-2))*DX
FANS(7) = FANS(3)/SONTAB(1)

C EMPLOY CUBIC INTERPOLATION TO COMPUTE COEFFICIENT OF VISCOSITY/SEA LEVEL RATIO
C

FANS(4) = VISTAB(1) + ((CV(3*1)*DX + CV(3*1-1))*DX + CV(3*1-2))*DX
FANS(8) = FANS(4)/VISTAB(1)

RETURN

C INITIAL BOUNDARY VALUES - FUNCTION/SEA LEVEL RATIO

A2
500

FANS(1) = PRSTAB(1)

FANS(2) = RHOTAB(1)
FANS(3) = SONTAB(1)
FANS(4) = VISTAB(1)
FANS(5) = 1.0
FANS(6) = 1.0
FANS(7) = 1.0
FANS(8) = 1.0

RETURN

C TERMINAL BOUNDARY VALUES - FUNCTION/SEA LEVEL RATIO

A3
501

FANS(1) = PRSTAB(NP)

FANS(2) = RHOTAB(NP)

CONT. ON PG 4

ATMSPL
PG 3 OF 4

ORIGINAL PAGE IS
OF POOR QUALITY

FANS(3) = SONTAB(NP)
FANS(4) = VISTAB(NP)
FANS(5) = FANS(1)/PRSTAB(1)
FANS(6) = FANS(2)/RHOTAB(1)
FANS(7) = FANS(3)/SONTAB(1)
FANS(8) = FANS(4)/VISTAB(1)

RETURN

END

ATMSPL
PG 4 FINAL

BLOCK DATA
 PARAMETER NP = 123
 PARAMETER NP11 = 1, NP12 = 114, NP13 = 115, NP14 = 'P'
 PARAMETER NP21=NP11+NP, NP22=NP12+NP, NP23=NP13+NP, NP24=NP14+NP
 PARAMETER NP31=NP21+NP, NP32=NP22+NP, NP33=NP23+NP, NP34=NP24+NP
 PARAMETER NP41=NP31+NP, NP42=NP32+NP, NP43=NP33+NP, NP44=NP34+NP
 PARAMETER NP51=NP41+NP, NP52=NP42+NP, NP53=NP43+NP, NP54=NP44+NP
 PARAMETER NP61=NP51+NP, NP62=NP54+95, NP63=NP54+96, NP64=NP54+NP

C ALTITUDE TABULATION IN METERS

DATA (ALTLIST(I), I=NP11, NP12)/

C	1	2	3	4	5	6
	0.0E0.	2.5E2.	5.0E2.	7.5E2.	1.0E3.	1.25E3.
C	7	8	9	10	11	12
	1.5E3.	1.75E3.	2.0E3.	2.25E3.	2.5E3.	2.75E3.
C	13	14	15	16	17	18
	3.0E3.	3.5E3.	4.0E3.	4.5E3.	5.0E3.	6.0E3.
C	19	20	21	22	23	24
	7.0E3.	8.0E3.	9.0E3.	1.0E4.	1.1E4.	1.2E4.
C	25	26	27	28	29	30
	1.3E4.	1.4E4.	1.5E4.	1.6E4.	1.7E4.	1.8E4.
C	31	32	33	34	35	36
	1.9E4.	2.0E4.	2.2E4.	2.4E4.	2.6E4.	2.8E4.
C	37	38	39	40	41	42

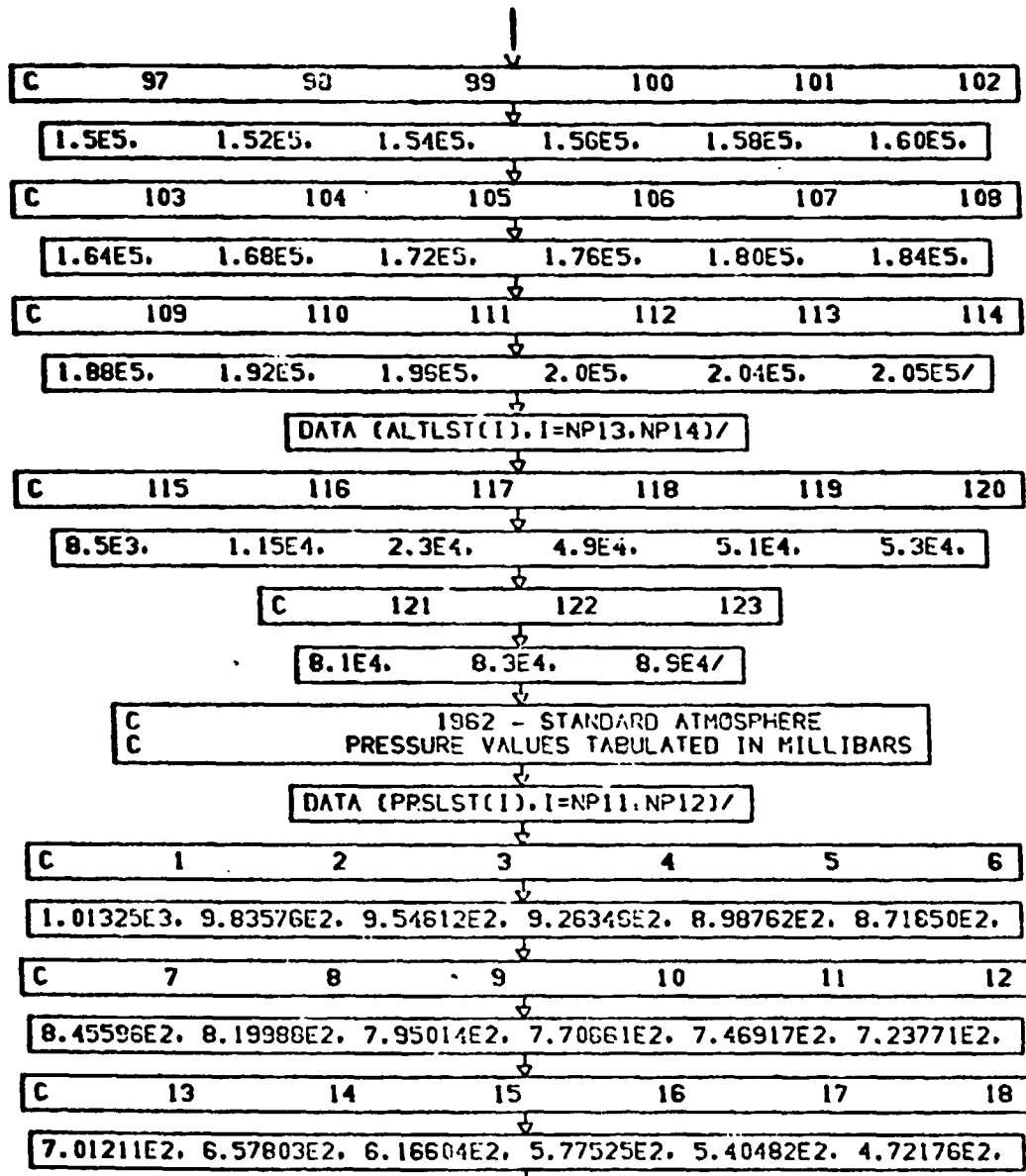
CONT. ON PG 2

PARTS
PG 1 OF 52

	3.0E4.	3.2E4.	3.4E4.	3.6E4.	3.8E4.	4.0E4.
C	43	44	45	46	47	48
	4.2E4.	4.4E4.	4.6E4.	4.8E4.	5.0E4.	5.2E4.
C	49	50	51	52	53	54
	5.4E4.	5.6E4.	5.8E4.	6.0E4.	6.2E4.	6.4E4.
C	55	56	57	58	59	60
	6.6E4.	6.8E4.	7.0E4.	7.2E4.	7.4E4.	7.6E4.
C	61	62	63	64	65	66
	7.8E4.	8.0E4.	8.2E4.	8.4E4.	8.6E4.	8.8E4.
C	67	68	69	70	71	72
	9.0E4.	9.2E4.	9.4E4.	9.6E4.	9.8E4.	1.0E5.
C	73	74	75	76	77	78
	1.02E5.	1.04E5.	1.06E5.	1.08E5.	1.1E5.	1.12E5.
C	79	80	81	82	83	84
	1.14E5.	1.16E5.	1.18E5.	1.20E5.	1.22E5.	1.24E5.
C	85	86	87	88	89	90
	1.26E5.	1.28E5.	1.3E5.	1.32E5.	1.34E5.	1.36E5.
C	91	92	93	94	95	96
	1.38E5.	1.4E5.	1.42E5.	1.44E5.	1.46E5.	1.48E5.

CONT. ON PG 3

PARTS
PG 2 OF 52



CONT. ON PG 4

PARTS
PG 3 OF 52

C	19	20	21	22	23	24
4.11052E2, 3.56516E2, 3.08007E2, 2.64999E2, 2.26999E2, 1.93994E2,						
C	25	26	27	28	29	30
1.65796E2, 1.41704E2, 1.21118E2, 1.03528E2, 8.84971E1, 7.56522E1,						
C	31	32	33	34	35	36
6.46748E1, 5.52930E1, 4.04749E1, 2.97174E1, 2.18837E1, 1.61619E1,						
C	37	38	39	40	41	42
1.19703E1, 8.89063E0, 6.63412E0, 4.9P522E0, 3.77138E0, 2.87143E0,						
C	43	44	45	46	47	48
2.19967E0, 1.69496E0, 1.31340E0, 1.02296E0, 7.97790E-1, 6.22263E-1,						
C	49	50	51	52	53	54
4.84917E-1, 3.76572E-1, 2.91373E-1, 2.24606E-1, 1.72457E-1, 1.31504E-1,						
C	55	56	57	58	59	60
9.94067E-2, 7.44483E-2, 5.52047E-2, 4.05013E-2, 2.93758E-2, 2.1045E-2,						
C	61	62	63	64	65	66
1.4877E-2, 1.0366E-2, 7.1691E-3, 4.9592E-3, 3.4313E-3, 2.3740E-3,						
C	67	68	69	70	71	72
1.6438E-3, 1.1449E-3, 8.0683E-4, 5.7403E-4, 4.1377E-4, 3.0075E-4,						
C	73	74	75	76	77	78

CONT. ON PG 5

PARTS
PG 4 OF 52

	2.2123E-4	1.6500E-4	1.2462E-4	9.5225E-5	7.3544E-5	5.7623E-5
C	79	80	81	82	83	84
	4.5919E-5	3.7137E-5	3.0426E-5	2.5217E-5	2.1210E-5	1.8139E-5
C	85	86	87	88	89	90
	1.5726E-5	1.3791E-5	1.2214E-5	1.0909E-5	9.8151E-6	8.8882E-6
C	91	92	93	94	95	96
	6.0950E-6	7.4194E-6	6.8148E-6	6.2931E-6	5.8331E-6	5.4252E-6
C	97	98	99	100	101	102
	5.0617E-6	4.7345E-6	4.4375E-6	4.1671E-6	3.9202E-6	3.6943E-6
C	103	104	105	106	107	108
	3.2932E-6	2.9475E-6	2.6479E-6	2.3851E-6	2.1536E-6	1.9491E-6
C	109	110	111	112	113	114
	1.7680E-6	1.6070E-6	1.4630E-6	1.3339E-6	1.2179E-6	1.1907E-6
	DATA (PRSLST(I),I=NP13,NP14)/					
C	115	116	117	118	119	120
	3.31541E2	2.09848E2	3.46686E1	9.03367E-1	7.04580E-1	5.49540E-1
C	121	122	123			
	8.6204E-3	5.9624E-3	1.9756E-3			
C	DENSITY VALUES TABULATED IN KILOGRAMS PER CUBIC METER					

CONT. ON PG 6

PARTS
PG 5 OF 52

DATA (RHOLST(I), I=NP11, NP12)/

C	1	2	3	4	5	6
1.2250E0, 1.1959E0, 1.1673E0, 1.1392E0, 1.1117E0, 1.0846E0.						
C	7	8	9	10	11	12
1.0581E0, 1.0321E0, 1.0066E0, 9.8151E-1, 9.5695E-1, 9.3287E-1.						
C	13	14	15	16	17	18
9.0925E-1, 8.6340E-1, 8.1935E-1, 7.7704E-1, 7.3643E-1, 6.6011E-1.						
C	19	20	21	22	23	24
5.9002E-1, 5.2579E-1, 4.6706E-1, 4.1351E-1, 3.6480E-1, 3.1194E-1.						
C	25	26	27	28	29	30
2.6660E-1, 2.2786E-1, 1.9475E-1, 1.6647E-1, 1.4230E-1, 1.2165E-1.						
C	31	32	33	34	35	36
1.0400E-1, 8.8910E-2, 6.4510E-2, 4.6936E-2, 3.4257E-2, 2.5076E-2.						
C	37	38	39	40	41	42
1.8410E-2, 1.3555E-2, 9.8874E-3, 7.2579E-3, 5.3666E-3, 3.9957E-3.						
C	43	44	45	46	47	48
2.9948E-3, 2.2589E-3, 1.7141E-3, 1.3167E-3, 1.0269E-3, 8.0097E-4.						
C	49	50	51	52	53	54
6.3137E-4, 4.9762E-4, 3.9086E-4, 3.0592E-4, 2.3931E-4, 1.8837E-4.						

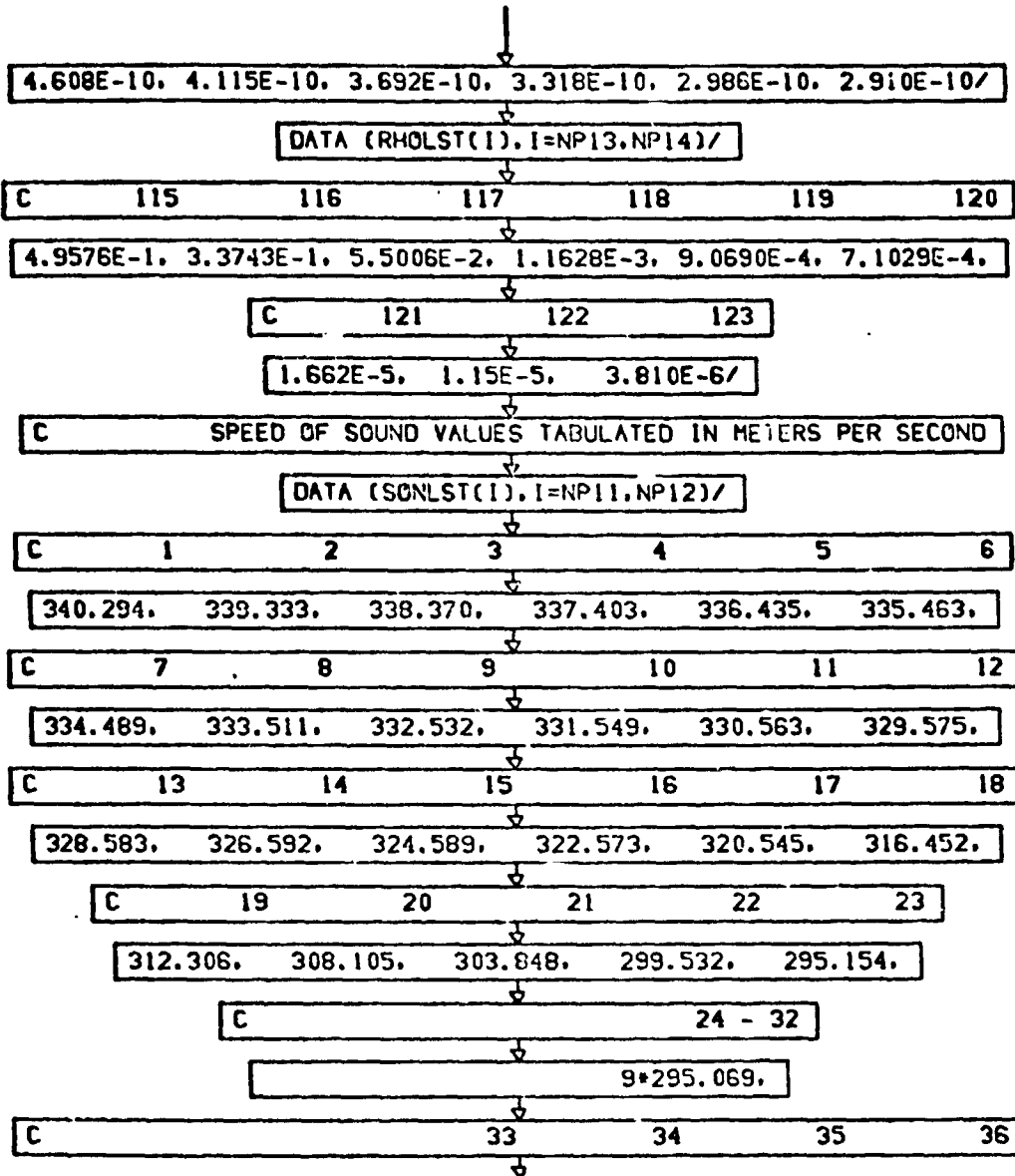
CONT. ON PG 7

PARTS
PG 6 OF 52

C	55	56	57	58	59	60
1.4713E-4, 1.1399E-4, 8.7535E-5, 6.6593E-5, 5.0151E-5, 3.736E-5,						
C	61	62	63	64	65	66
2.750E-5, 1.999E-5, 1.382E-5, 9.563E-6, 6.617E-6, 4.579E-6,						
C	67	68	69	70	71	72
3.170E-6, 2.137E-6, 1.459E-6, 1.008E-6, 7.044E-7, 4.974E-7,						
C	73	74	75	76	77	78
3.493E-7, 2.492E-7, 1.804E-7, 1.323E-7, 9.829E-8, 7.153E-8,						
C	79	80	81	82	83	84
5.321E-8, 4.035E-8, 3.112E-8, 2.436E-8, 1.844E-8, 1.434E-8,						
C	85	86	87	88	89	90
1.140E-8, 9.226E-9, 7.589E-9, 6.327E-9, 5.337E-9, 4.549E-9,						
C	91	92	93	94	95	96
3.913E-9, 3.394E-9, 2.965E-9, 2.608E-9, 2.307E-9, 2.053E-9,						
C	97	98	99	100	101	102
1.836E-9, 1.665E-9, 1.515E-9, 1.382E-9, 1.264E-9, 1.159E-9,						
C	103	104	105	106	107	108
9.970E-10, 8.624E-10, 7.532E-10, 6.633E-10, 5.858E-10, 5.189E-10,						
C	109	110	111	112	113	114

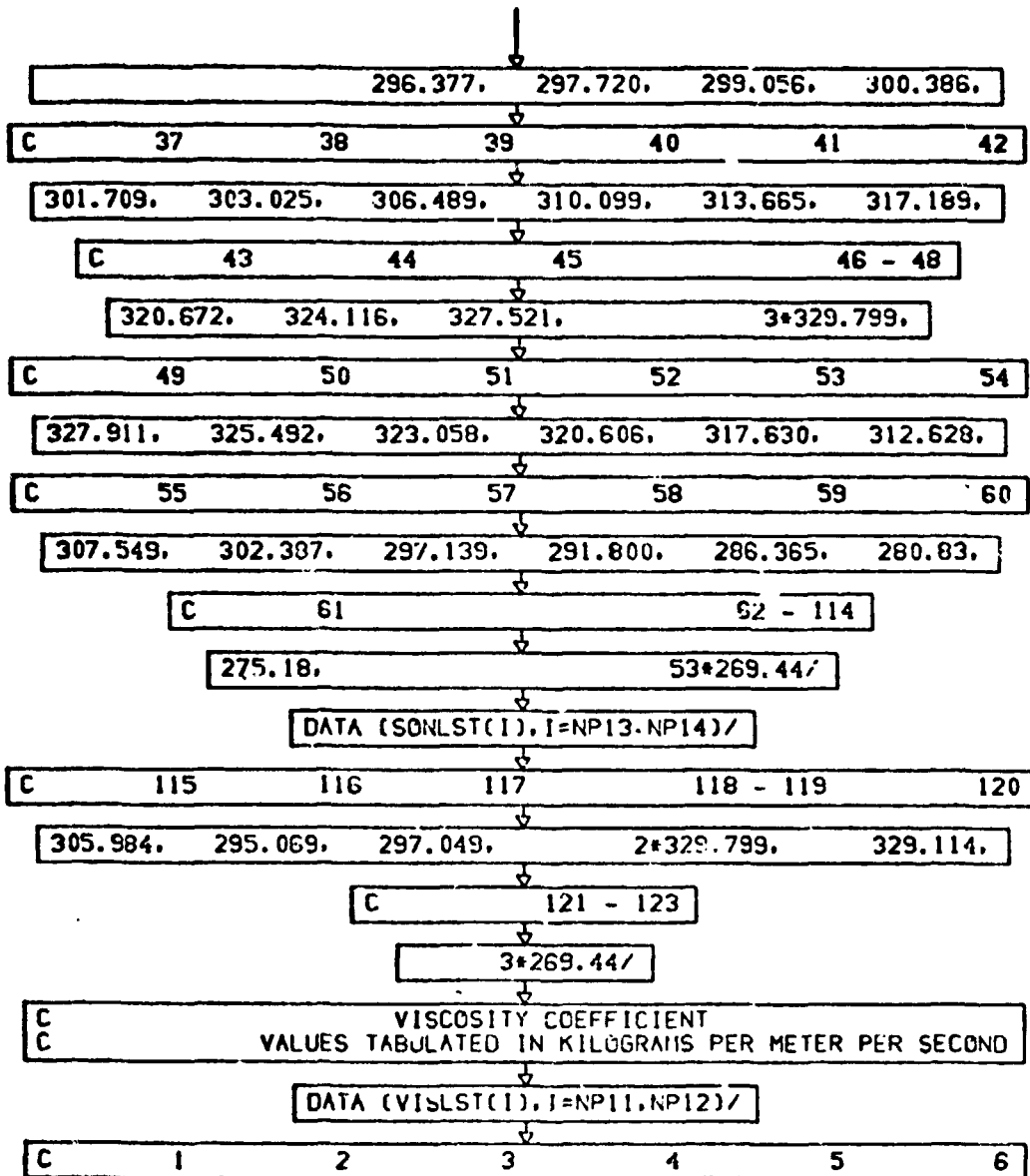
CONT. ON PG 8

PARTS
PG 7 OF 52



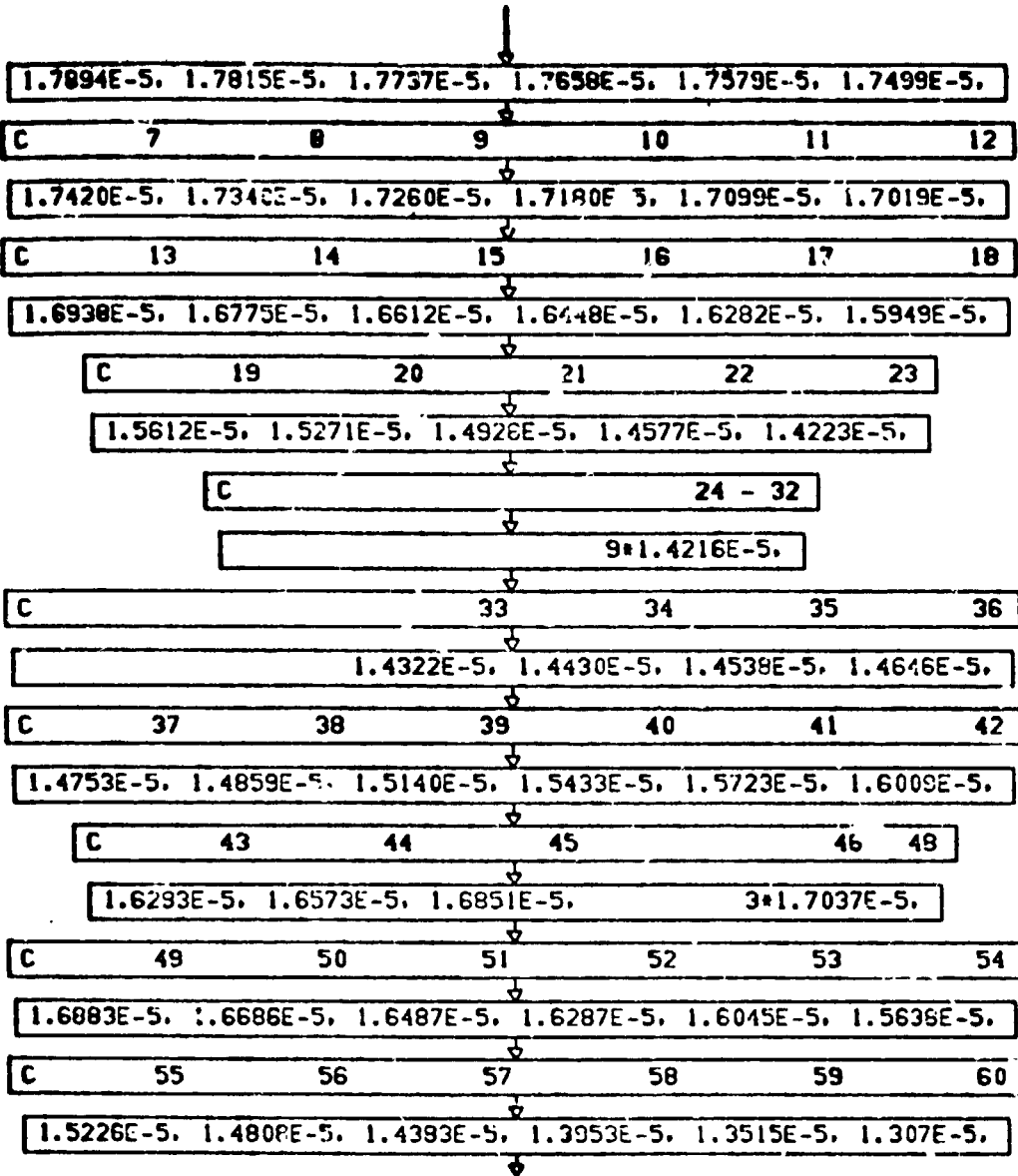
CONT. ON PG 9

PARTS
PG 8 OF 52



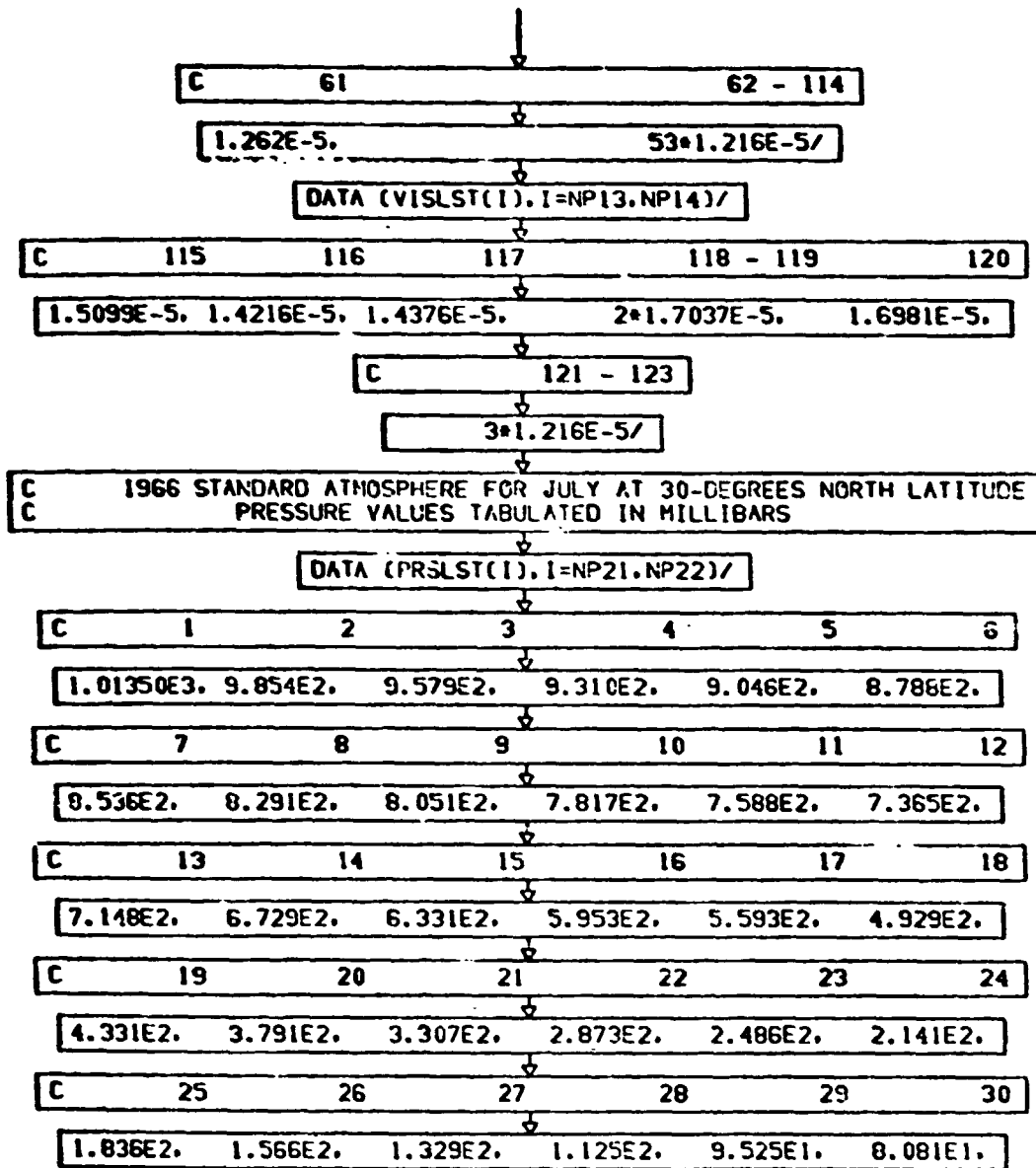
CONT. ON PG 10

PARTS
PG 9 OF 52



CONT. ON PG 11

PARTS
PG 10 OF 52



CONT. ON PG 12

PARTS
PG 11 OF 52

C	31	32	33	34	35	36
	6.067E1.	5.846E1.	4.258E1.	3.121E1.	2.300E1.	1.705E1.
C	37	38	39	40	41	42
	1.270E1.	9.513E0.	7.163E0.	5.425E0.	4.131E0.	3.162E0.
C	43	44	45	46	47	48
	2.433E0.	1.881E0.	1.461E0.	1.140E0.	8.908E-1.	6.959E-1.
C	49	50	51	52	53	54
	5.424E-1.	4.212E-1.	3.259E-1.	2.512E-1.	1.924E-1.	1.462E-1.
C	55	56	57	58	59	60
	1.102E-1.	8.226E-2.	6.083E-2.	4.450E-2.	3.224E-2.	2.306E-2.
C	61	62	63	64	65	66
	1.629E-2.	1.135E-2.	7.792E-3.	5.301E-3.	3.607E-3.	2.455E-3.
C	67	68	69	70	71	72
	1.671E-3.	1.142E-3.	7.877E-4.	5.488E-4.	3.859E-4.	2.737E-4.
C	73	74	75	76	77	78
	1.958E-4.	1.427E-4.	1.005E-4.	8.104E-5.	6.276E-5.	4.935E-5.
C	79	80	81 - 114			
	3.955E-5.	3.240E-5.	34*2.702E-5/			
	DATA (PRSLST(I), I=NP23, NP24)/					

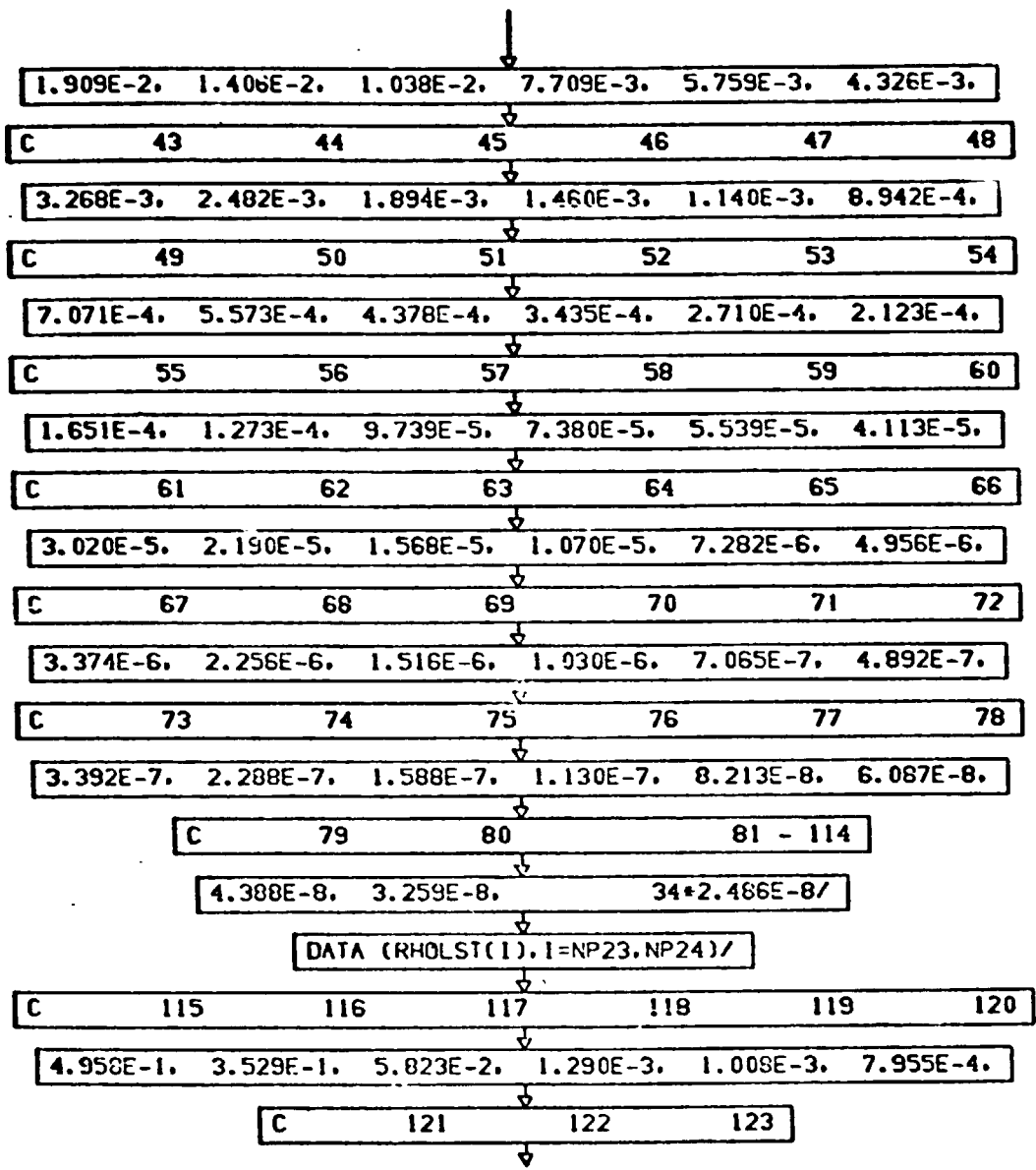
CONT. CN PG 13

PARTS
PG 12 OF 52

C	115	116	117	118	119	120
	3.542E2.	2.308E2.	3.643E1.	1.008E0.	7.874E-1.	6.146E-1.
C	121	123	123			
	9.423E-3.	6.427E-3.	2.025E-3/			
C	DENSITY VALUES TABULATED IN KILOGRAMS PER CUBIC METER					
	DATA (RHOLST(I), I=NP21, NP22)/					
C	1	2	3	4	5	6
	1.159E0.	1.135E0.	1.112E0.	1.089E0.	1.066E0.	1.041E0.
C	7	8	9	10	11	12
	1.016E0.	9.923E-1.	9.666E-1.	9.452E-1.	9.222E-1.	8.997E-1.
C	13	14	15	16	17	18
	8.776E-1.	8.348E-1.	7.937E-1.	7.540E-1.	7.159E-1.	6.443E-1.
C	19	20	21	22	23	24
	5.814E-1.	5.232E-1.	4.634E-1.	4.199E-1.	3.742E-1.	3.324E-1.
C	25	26	27	28	29	30
	2.941E-1.	2.592E-1.	2.275E-1.	1.929E-1.	1.617E-1.	1.357E-1.
C	31	32	33	34	35	36
	1.142E-1.	9.618E-2.	6.870E-2.	4.944E-2.	3.579E-2.	2.607E-2.
C	37	38	39	40	41	42

CONT. ON PG 14

PARTS
PG 13 OF 52



CONT. ON PG 15

PARTS
PG 14 OF 52

↓
1.856E-5, 1.298E-5, 4.089E-6/

C SPEED OF SOUND VALUES TABULATED IN METERS PER SECOND

↓
DATA (SONLST(I), I=NP21, NP22)/

C 1 2 3 4 5 6

↓
349.9, 348.6, 347.3, 346.0, 344.7, 343.8.

C 7 8 9 10 11 12

↓
342.9, 342.0, 341.1, 340.3, 339.4, 338.5.

C 13 14 15 16 17 18

↓
337.7, 335.9, 334.2, 332.5, 330.7, 327.3.

C 19 20 21 22 23 24

↓
322.9, 318.5, 314.0, 309.5, 304.9, 303.3.

C 25 26 27 28 29 30

↓
295.6, 290.9, 286.0, 285.7, 287.2, 288.7.

C 31 32 33 34 35 36

↓
290.2, 291.7, 294.6, 297.3, 299.9, 302.6.

C 37 38 39 40 41 42

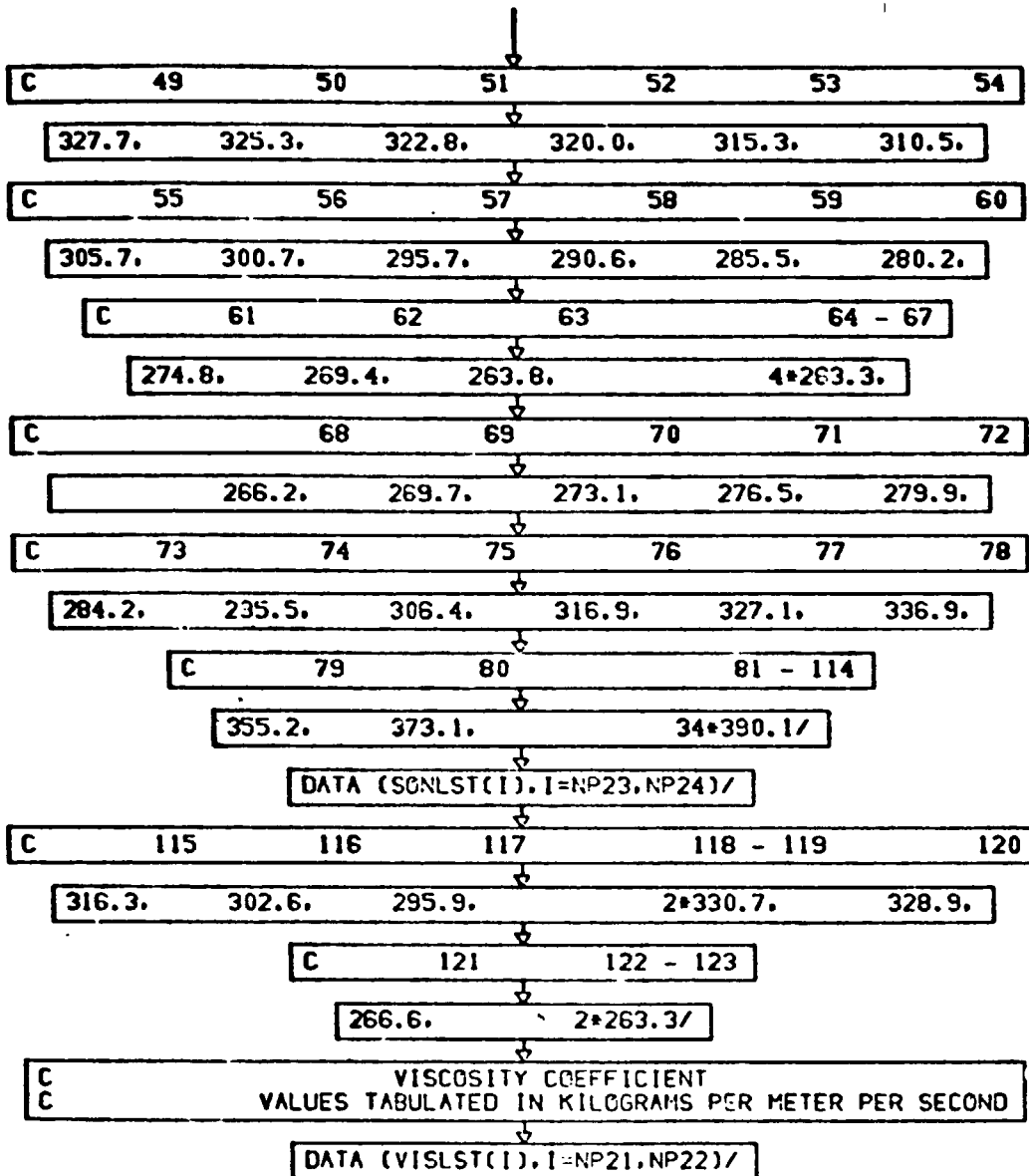
↓
305.2, 307.8, 310.8, 313.9, 316.9, 319.9.

C 43 44 45 46 - 47 48

↓
322.8, 325.8, 328.7, 2*330.7, 330.1.

↓
CONT. ON PG 16

PARTS
PG 15 OF 52



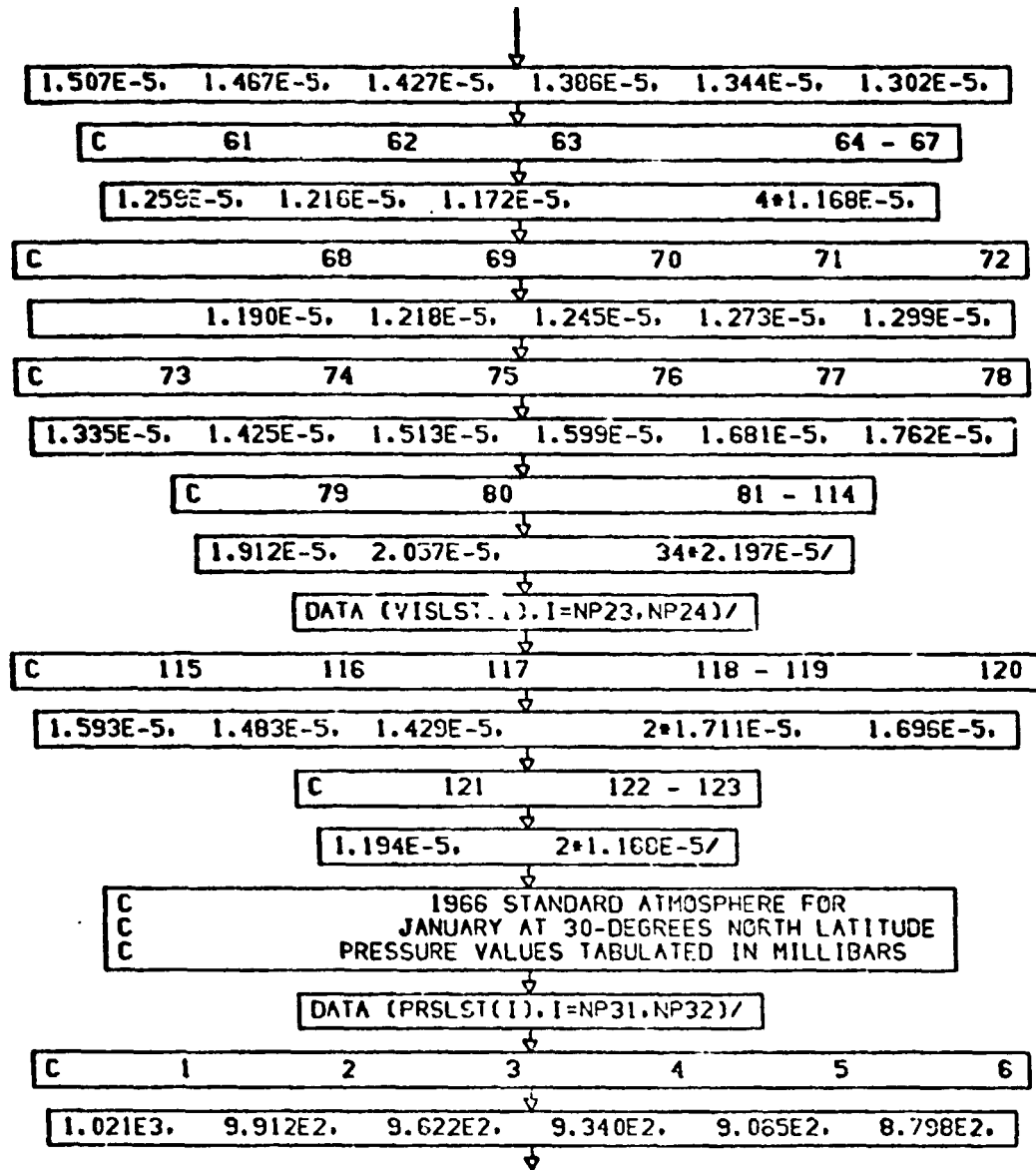
CONT. ON PG 17

PARTS
PG 16 OF 52

C	1	2	3	4	5	6
1.868E-5, 1.857E-5, 1.846E-5, 1.836E-5, 1.825E-5, 1.818E-5,						
C	7	8	9	10	11	12
1.811E-5, 1.803E-5, 1.796E-5, 1.789E-5, 1.782E-5, 1.775E-5,						
C	13	14	15	16	17	18
1.768E-5, 1.754E-5, 1.739E-5, 1.725E-5, 1.711E-5, 1.683E-5,						
C	19	20	21	22	23	24
1.648E-5, 1.612E-5, 1.575E-5, 1.539E-5, 1.501E-5, 1.464E-5,						
C	25	26	27	28	29	30
1.426E-5, 1.389E-5, 1.349E-5, 1.346E-5, 1.358E-5, 1.370E-5,						
C	31	32	33	34	35	36
1.302E-5, 1.395E-5, 1.418E-5, 1.439E-5, 1.461E-5, 1.482E-5,						
C	37	38	39	40	41	42
1.504E-5, 1.525E-5, 1.549E-5, 1.574E-5, 1.599E-5, 1.623E-5,						
C	43	44	45	46 - 47	48	
1.647E-5, 1.671E-5, 1.694E-5, 2*1.711E-5, 1.706E-5,						
C	49	50	51	52	53	54
1.687E-5, 1.677E-5, 1.647E-5, 1.624E-5, 1.595E-5, 1.547E-5,						
C	55	56	57	58	59	60

CONT. ON PG 18

PARTS
PG 17 OF 52



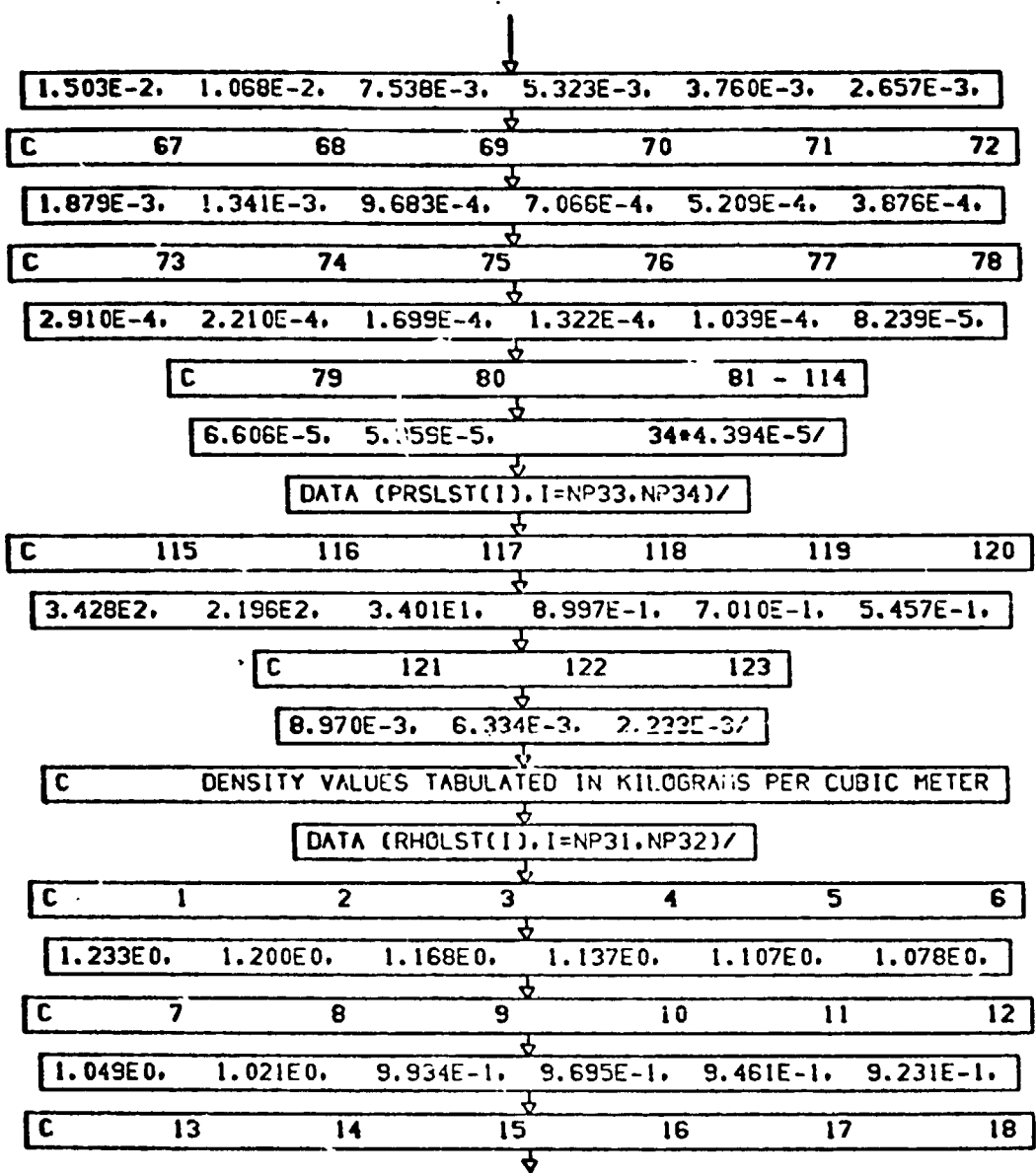
CONT. ON PG 19

PARTS
PG 18 OF 52

C	7	8	9	10	11	12
	8.538E2.	8.285E2.	8.038E2.	7.798E2.	7.564E2.	7.335E2.
C	13	14	15	16	17	18
	7.112E2.	6.682E2.	6.274E2.	5.886E2.	5.517E2.	4.837E2.
C	19	20	21	22	23	24
	4.226E2.	3.679E2.	3.191E2.	2.757E2.	2.372E2.	2.032E2.
C	25	26	27	28	29	30
	1.734E2.	1.478E2.	1.257E2.	1.067E2.	9.040E1.	7.650E1.
C	31	32	33	34	35	36
	6.479E1.	5.499E1.	3.984E1.	2.907E1.	2.134E1.	1.575E1.
C	37	38	39	40	41	42
	1.169E1.	8.723E0.	6.544E0.	4.939E0.	3.748E0.	2.860E0.
C	43	44	45	46	47	48
	2.194E0.	1.691E0.	1.310E0.	1.019E0.	7.941E-1.	6.187E-1.
C	49	50	51	52	53	54
	4.808E-1.	3.723E-1.	2.872E-1.	2.207E-1.	1.687E-1.	1.281E-1.
C	55	56	57	58	59	60
	9.659E-2.	7.231E-2.	5.372E-2.	3.959E-2.	2.893E-2.	2.095E-2.
C	61	62	63	64	65	66

CONT. ON PG 20

PARTS
PG 19 OF 52



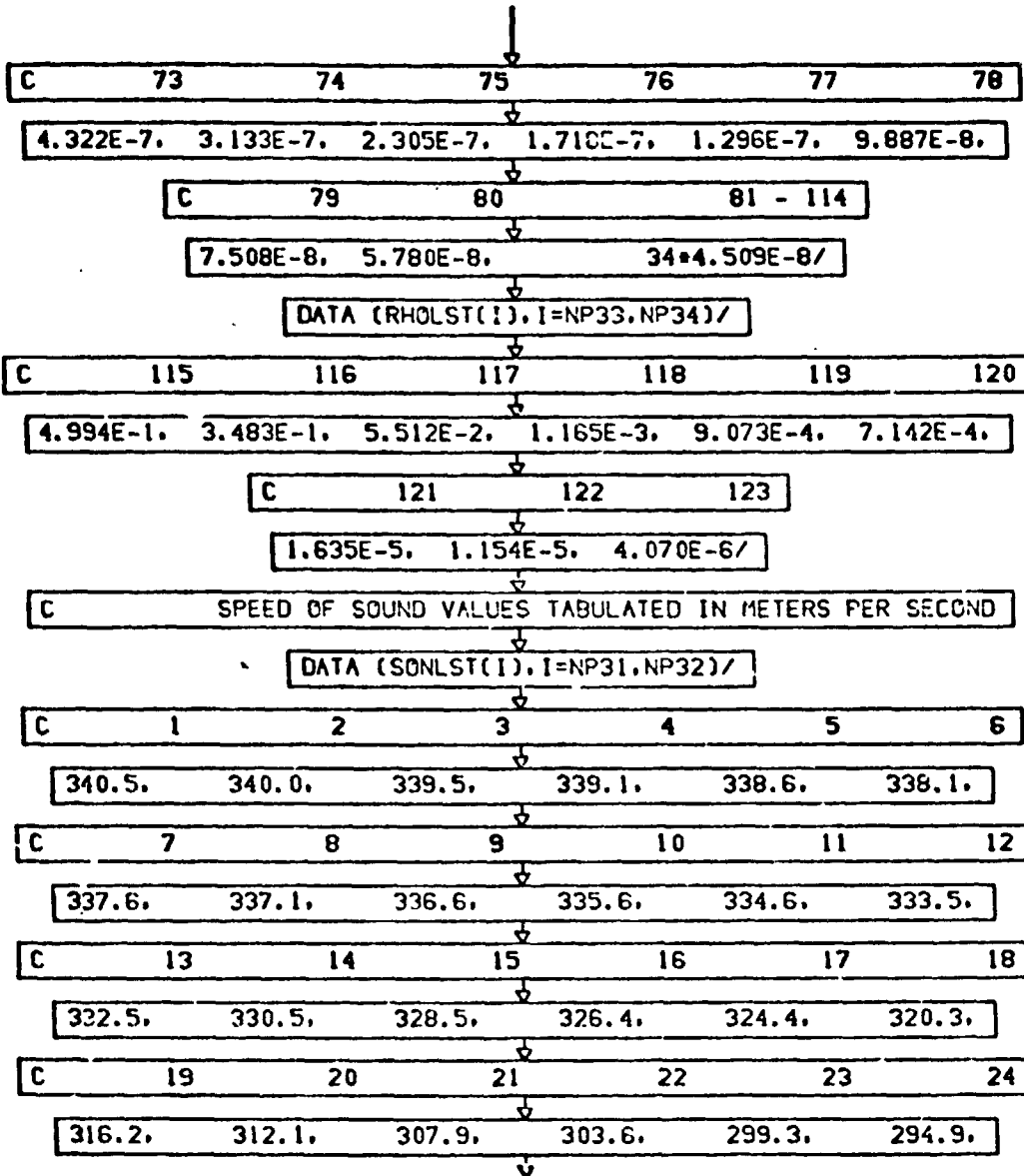
CONT. ON PG 21

PARTS
PG 20 OF 52

	9.005E-1,	8.565E-1,	8.142E-1,	7.733E-1,	7.340E-1,	6.599E-1,
C	19	20	21	22	23	24
	5.916E-1,	5.288E-1,	4.713E-1,	4.187E-1,	3.707E-1,	3.270E-1,
C	25	26	27	28	29	30
	2.828E-1,	2.439E-1,	2.101E-1,	1.805E-1,	1.549E-1,	1.312E-1,
C	31	32	33	34	35	36
	1.099E-1,	9.213E-2,	6.520E-2,	4.669E-2,	3.385E-2,	2.440E-2,
C	37	38	40	40	41	42
	1.780E-2,	1.306E-2,	9.603E-3,	7.05E-3,	5.289E-3,	3.960E-3,
C	43	44	45	46	47	48
	2.981E-3,	2.257E-3,	1.717E-3,	1.319E-3,	1.028E-3,	8.038E-4,
C	49	50	51	52	53	54
	6.340E-4,	4.983E-4,	3.903E-4,	3.051E-4,	2.389E-4,	1.860E-4,
C	55	56	57	58	59	60
	1.439E-4,	1.106E-4,	8.441E-5,	6.396E-5,	4.809E-5,	3.596E-5,
C	61	62	63	64	65	66
	2.651E-5,	1.942E-5,	1.374E-5,	9.702E-6,	6.853E-6,	4.842E-6,
C	67	68	69	70	71	72
	3.386E-6,	2.335E-6,	1.630E-6,	1.152E-6,	8.231E-7,	5.942E-7,

CONT. ON PG 22

PARTS
PG 21 OF 52



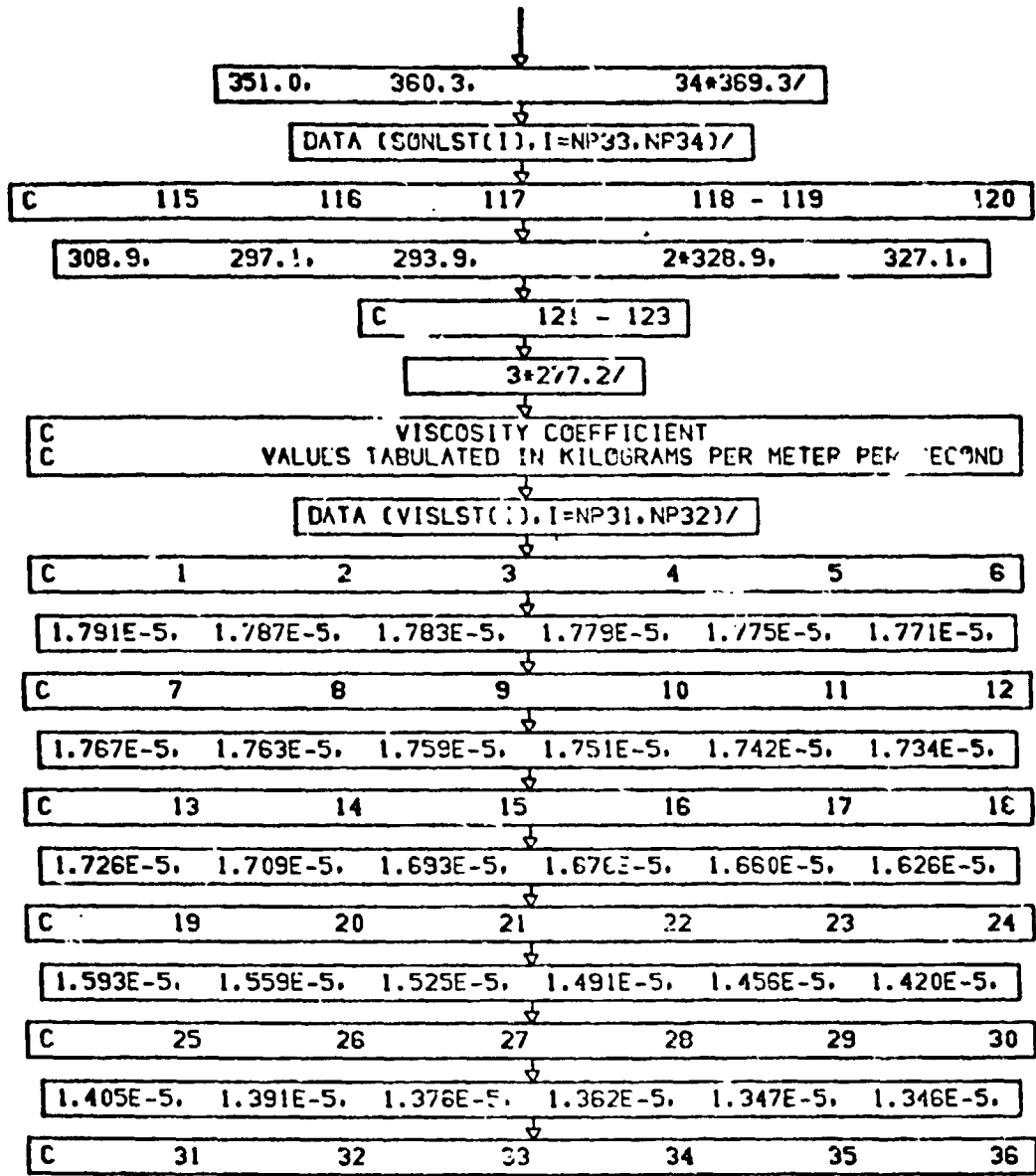
CONT. ON PG 23

PARTS
PG 22 OF 52

C	25	26	27	28	29	30
	293.0.	291.3.	289.5.	287.7.	285.9.	285.7.
C	31	32	33	34	35	36
	287.3.	289.1.	292.5.	295.2.	297.9.	300.6.
C	37	38	39	40	41	42
	303.2.	305.8.	308.9.	311.9.	315.0.	318.0.
C	43	44	45	46 - 47		48
	321.0.	323.9.	326.8.	2*328.9.		328.3.
C	49	50	51	52	53	54
	325.8.	323.4.	321.0.	316.3.	314.4.	310.5.
C	55	56	57	58	59	60
	306.5.	302.5.	298.5.	294.4.	290.2.	286.0.
C		61	62			63 - 66
		281.7.	277.4.			4*277.2.
C	67	68	69	70	71	72
	278.7.	283.6.	288.4.	293.0.	297.7.	302.2.
C	73	74	75	76	77	78
	307.0.	314.3.	321.3.	328.2.	335.0.	341.6.
C		79	80			81 - 114

CONT. ON PG 24

PARTS
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CONT. ON PG 25

PARTS
PG 24 OF 52

	1.359E-5.	1.373E-5.	1.401E-5.	1.423E-5.	1.445E-5.	1.466E-5.
C	37	38	39	40	41	42
	1.408E-5.	1.509E-5.	1.533E-5.	1.558E-5.	1.583E-5.	1.607E-5.
C	43	44	45	46 - 47		48
	1.632E-5.	1.656E-5.	1.679E-5.	2*1.696E-5.	1.691E-5.	
C	49	50	51	52	53	54
	1.671E-5.	1.652E-5.	1.632E-5.	1.610E-5.	1.578E-5.	1.547E-5.
C	55	56	57	58	59	60
	1.514E-5.	1.482E-5.	1.449E-5.	1.416E-5.	1.383E-5.	1.349E-5.
C	61	62	63 - 66			
	1.314E-5.	1.280E-5.	4*1.278E-5.			
C	67	68	69	70	71	72
	1.290E-5.	1.329E-5.	1.368E-5.	1.405E-5.	1.443E-5.	1.475E-5.
C	73	74	75	76	77	78
	1.518E-5.	1.577E-5.	1.634E-5.	1.691E-5.	1.746E-5.	1.800E-5.
C	79	80	81 - 114			
	1.877E-5.	1.953E-5.	34*2.027E-5/			
	DATA (VISLST(1),I=NP33, NP34)/					
C	115	116	117	118 - 119		120

CONT. ON PG 26

PARTS
PG 25 OF 52

ORIGINAL PAGE IS
OF POOR QUALITY

A-43

↓
1.542E-5, 1.438E-5, 1.412E-5, 2*1.696E-5, 1.681E-5,

C 121 - 123

3*1.278E-5/

C 1966 STANDARD ATMOSPHERE FOR JULY AT 60-DEGREES NORTH LATITUDE
C PRESSURE VALUES TABULATED IN MILLIBARS

DATA (PRSLST(I), I=NP41, NP42)/

C 1 2 3 4 5 6

1.010E3, 9.804E2, 9.516E2, 9.234E2, 8.960E2, 8.692E2,

C 7 8 9 10 11 12

8.432E2, 8.177E2, 7.930E2, 7.688E2, 7.453E2, 7.224E2,

C 13 14 15 16 17 18

7.000E2, 6.571E2, 6.164E2, 5.779E2, 5.414E2, 4.740E2,

C 19 20 21 22 23 24

4.134E2, 3.592E2, 3.108E2, 2.677E2, 2.301E2, 1.978E2,

C 25 26 27 28 29 30

1.700E2, 1.461E2, 1.256E2, 1.080E2, 9.285E1, 7.983E1,

C 31 32 33 34 35 36

6.864E1, 5.902E1, 4.364E1, 3.229E1, 2.398E1, 1.788E1,

C 37 38 39 40 41 42

1.338E1, 1.005E1, 7.593E0, 5.775E0, 4.421E0, 3.406E0,

↓
CONT. ON PG 27

PARTS
PG 26 OF 52

C	43	44	45	46	47	48
2.640E0, 2.057E0, 1.607E0, 1.259E0, 9.872E-1, 7.742E-1,						
C	49	50	51	52	53	54
6.072E-1, 4.751E-1, 3.704E-1, 2.877E-1, 2.218E-1, 1.694E-1,						
C	55	56	57	58	59	60
1.281E-1, 9.576E-2, 7.075E-2, 5.160E-2, 3.710E-2, 2.627E-2,						
C	61	62	63	64	65	66
1.829E-2, 1.249E-2, 8.380E-3, 5.536E-3, 3.667E-3, 2.430E-3,						
C	67	68	69	70	71	72
1.610E-3, 1.075E-3, 7.297E-4, 5.027E-4, 3.512E-4, 2.485E-4,						
C	73	74	75	76	77	78
1.782E-4, 1.310E-4, 9.889E-5, 7.633E-5, 6.004E-5, 4.801E-5,						
C	79	80	81 - 114			
3.903E-5, 3.224E-5, 34*2.700E-5/						
DATA (PRSLST(I), I=NP43, NP44)/						
C	115	116	117	118	119	120
3.343E2, 2.133E2, 3.753E1, 1.115E0, 8.742E-1, 6.857E-1,						
C	121	122	123			
1.025E-2, 6.803E-3, 1.978E-3/						

CONT. ON PG 28

PARTS
PG 27 OF 52

ORIGINAL PAGE IS
OF POOR QUALITY

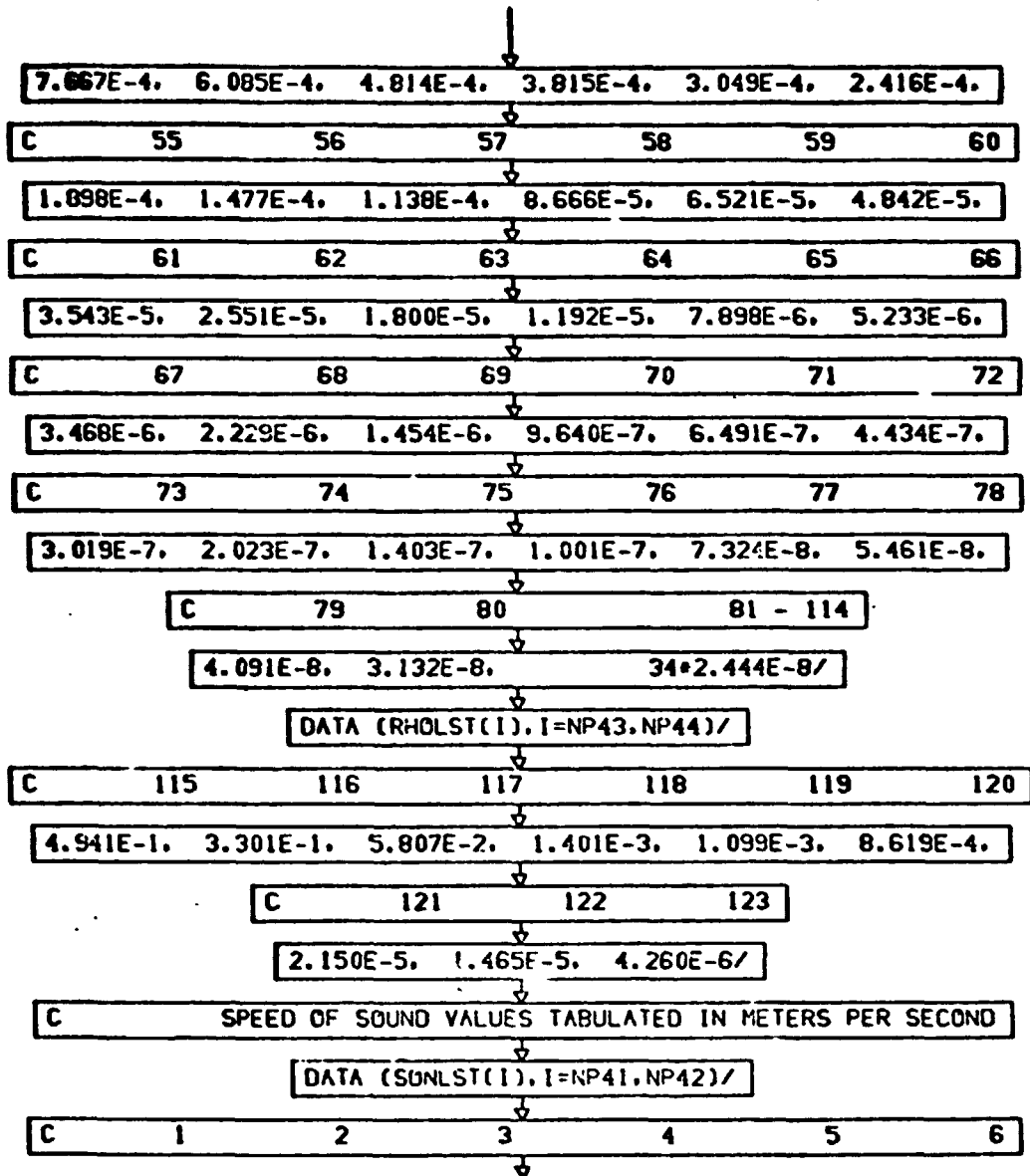
↓

C	DENSITY VALUES TABULATED IN KILOGRAMS PER CUBIC METER					
	DATA (RHOLST(I), I=NP41, NP42)/					
C	1	2	3	4	5	6
	1.220E0.	1.190E0.	1.161E0.	1.132E0.	1.104E0.	1.077E0.
C	7	8	9	10	11	12
	1.050E0.	1.023E0.	9.971E-1.	9.716E-1.	9.467E-1.	9.223E-1.
C	13	14	15	16	17	18
	8.984E-1.	8.521E-1.	8.077E-1.	7.651E-1.	7.244E-1.	6.519E-1.
C	19	20	21	22	23	24
	5.849E-1.	5.231E-1.	4.683E-1.	4.142E-1.	3.560E-1.	3.060E-1.
C	25	26	27	28	29	30
	2.631E-1.	2.261E-1.	1.944E-1.	1.671E-1.	1.437E-1.	1.235E-1.
C	31	32	33	34	35	36
	1.062E-1.	9.132E-2.	6.753E-2.	4.965E-2.	3.639E-2.	2.678E-2.
C	37	38	39	40	41	42
	1.979E-2.	1.469E-2.	1.083E-2.	8.041E-3.	6.013E-3.	4.528E-3.
C	43	44	45	46	47	48
	3.431E-3.	2.630E-3.	2.039E-3.	1.584E-3.	1.241E-3.	9.732E-4.
C	49	50	51	52	53	54

↓

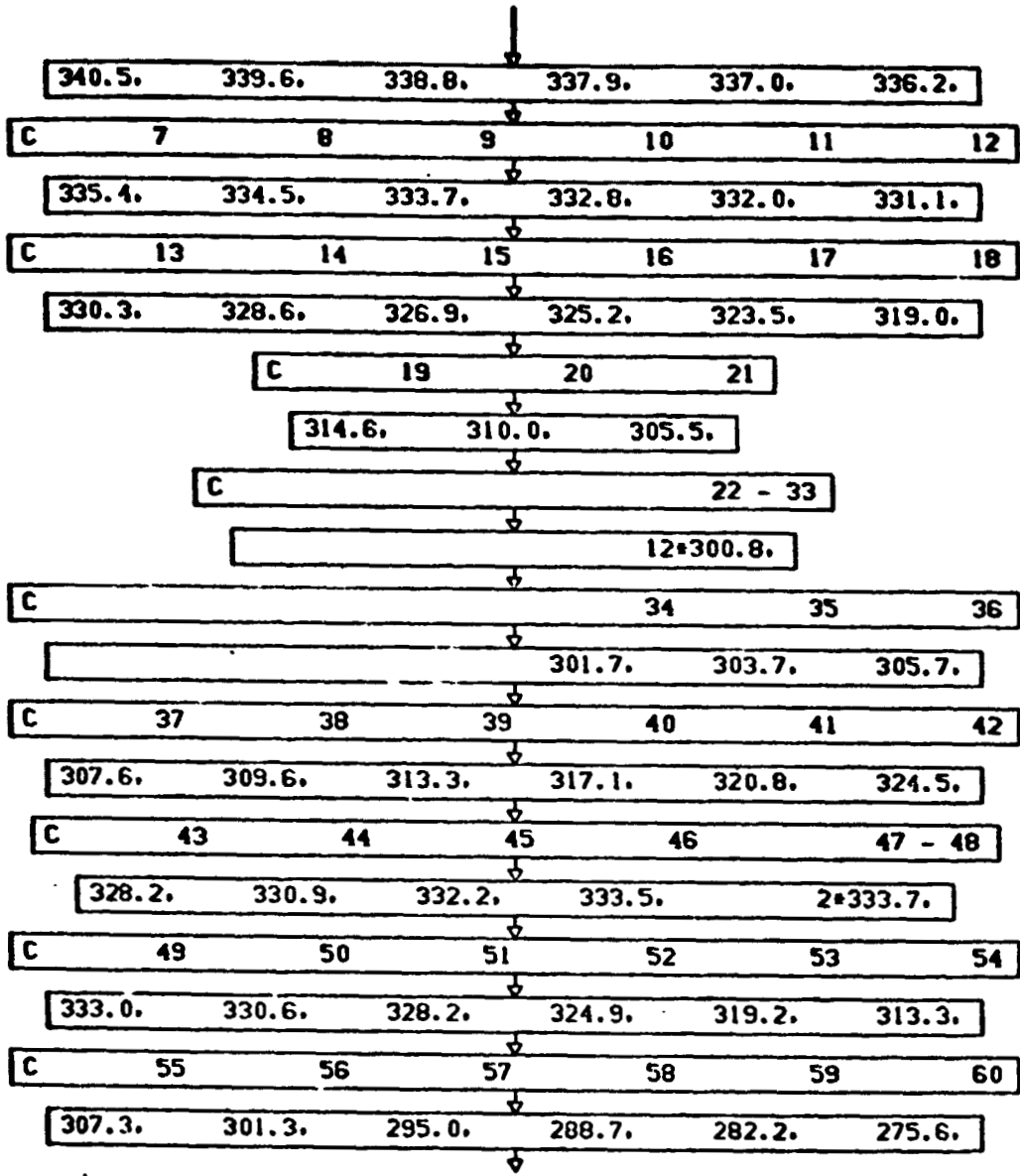
CONT. ON PG 29

PARTS
PG 28 OF 52



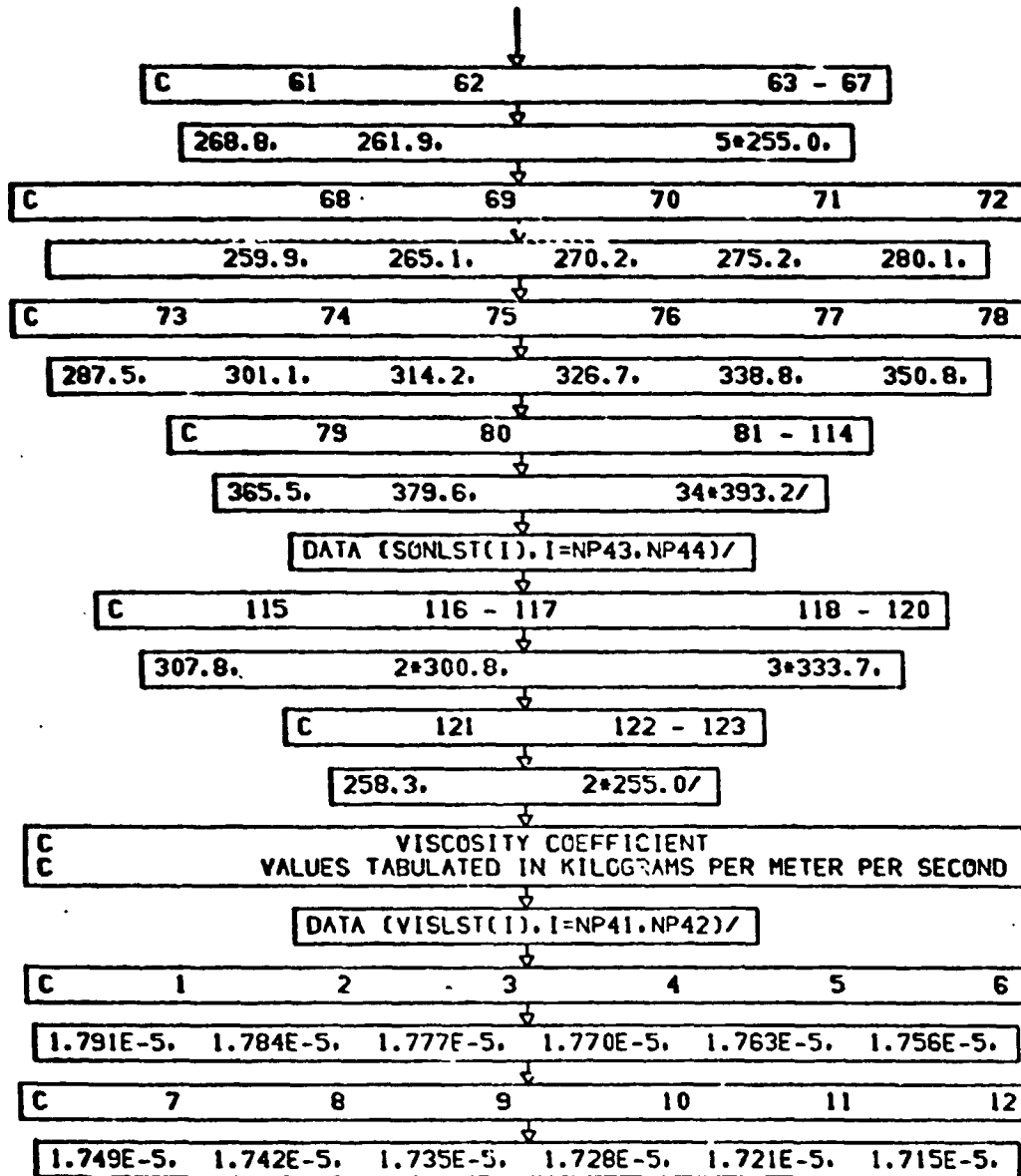
CONT. ON PG 30

PARTS
PG 29 OF 52



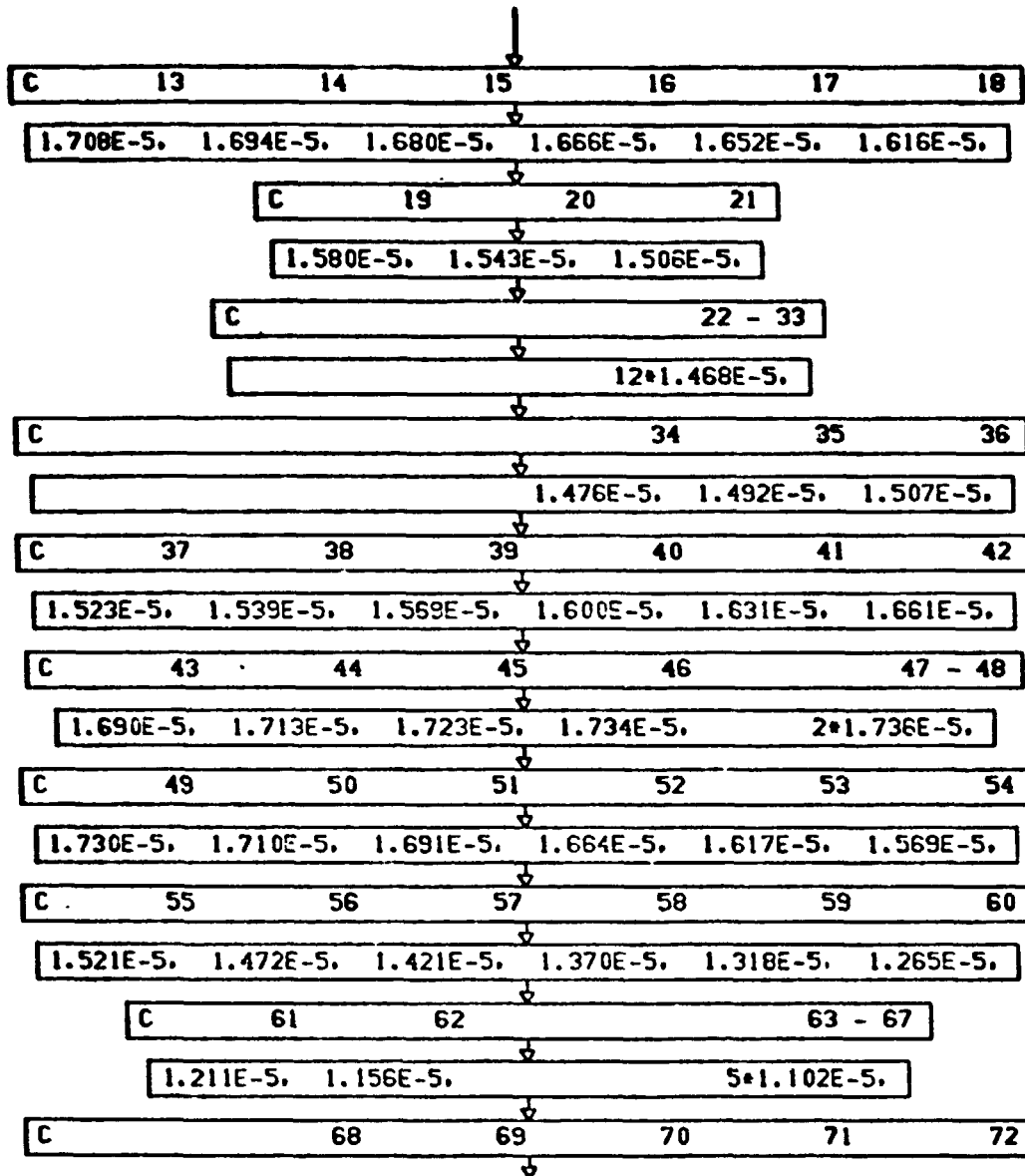
CONT. ON PG 31

PARTS
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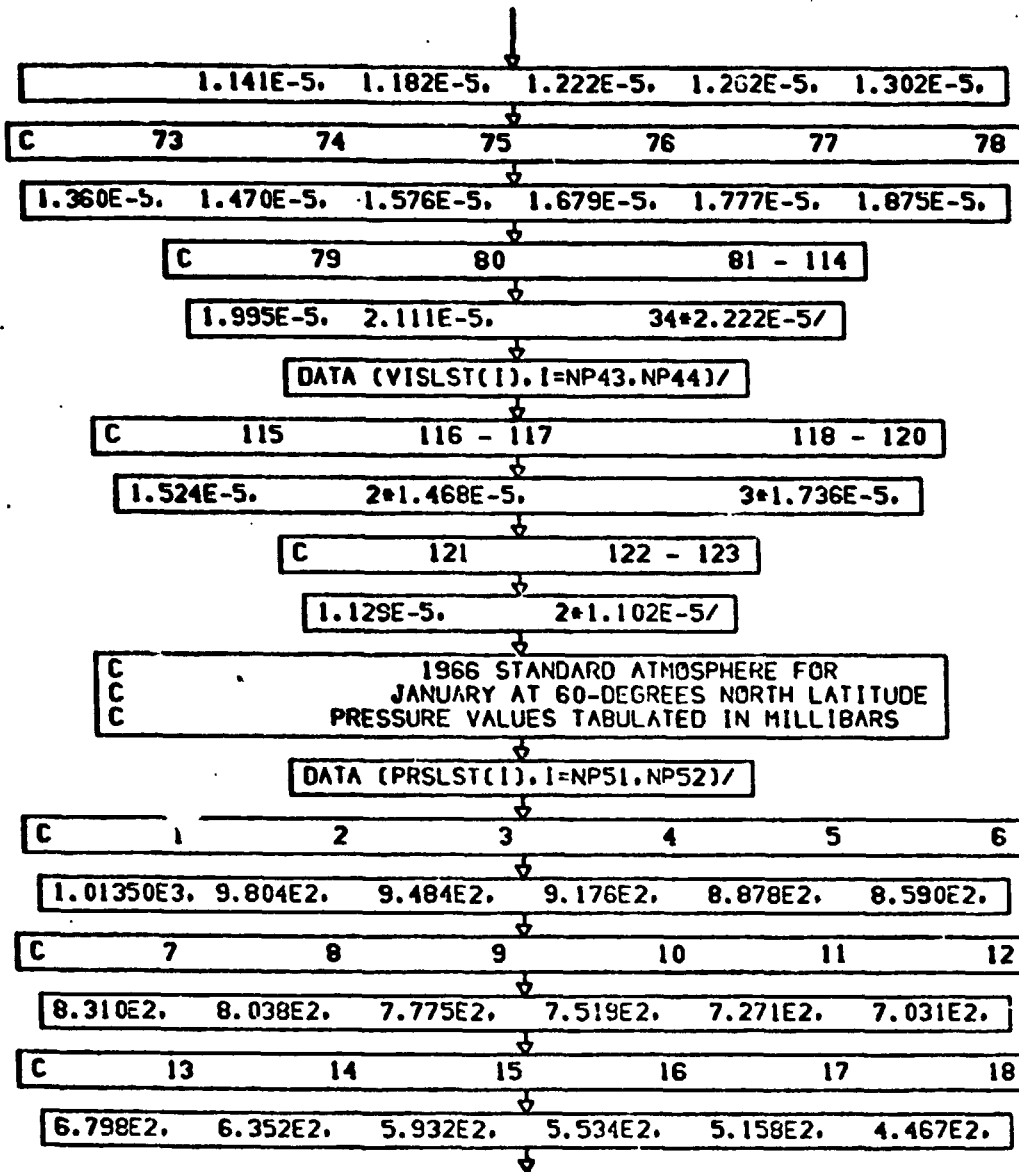
CONT. ON PG 32

PARTS
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CONT. ON PG 33

PARTS
PG 32 OF 52



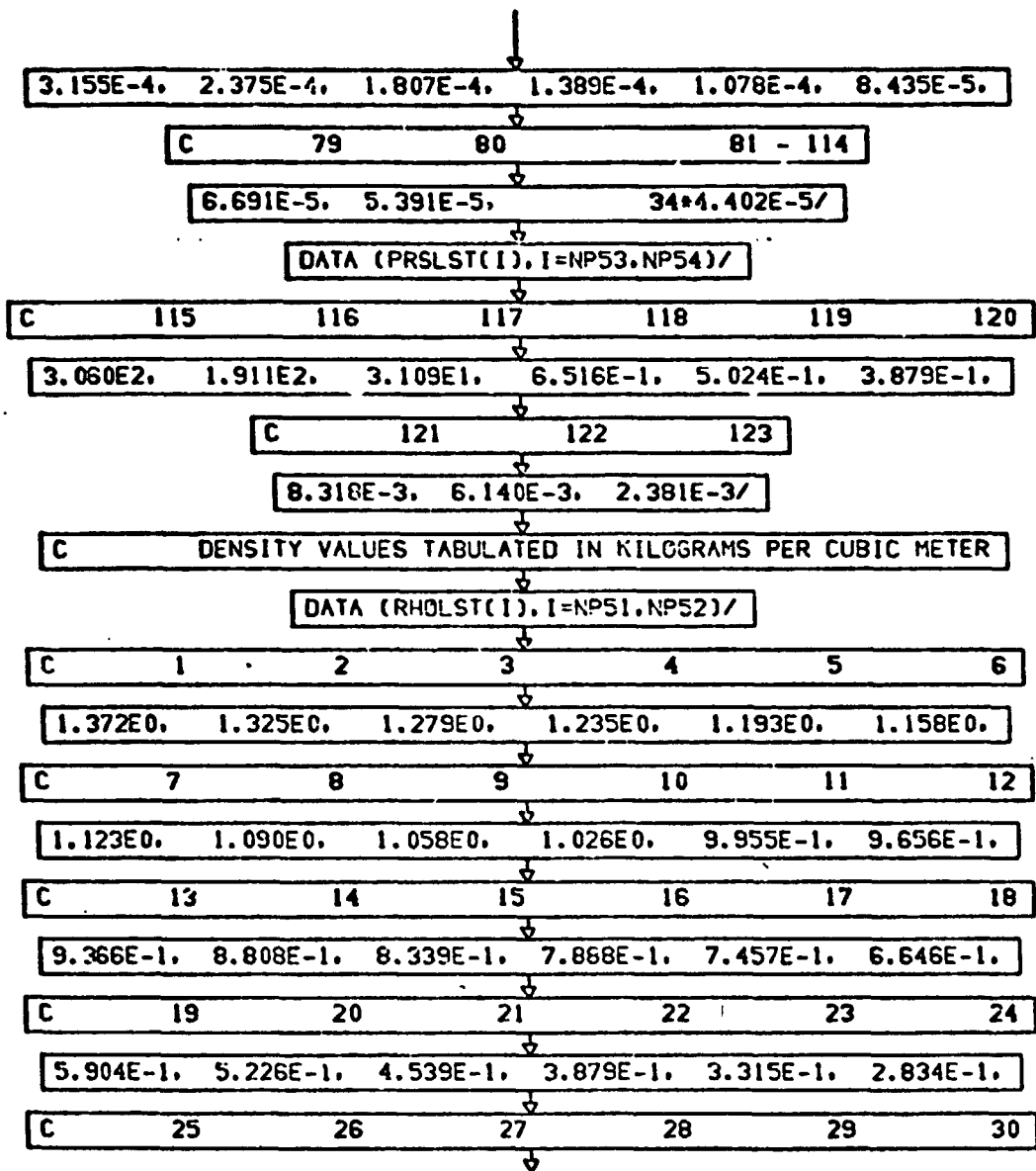
CONT. ON PG 34

PARTS
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C	19	20	21	22	23	24
	3.853E2.	3.308E2.	2.829E2.	2.418E2.	2.067E2.	1.766E2.
C	25	26	27	28	29	30
	1.510E2.	1.291E2.	1.103E2.	9.431E1.	8.058E1.	6.882E1.
C	31	32	33	34	35	36
	5.875E1.	5.014E1.	3.647E1.	2.649E1.	1.922E1.	1.398E1.
C	37	38	39	40	41	42
	1.020E1.	7.464E0.	5.479E0.	4.041E0.	3.001E0.	2.243E0.
C	43	44	45	46	47	48
	1.687E0.	1.277E0.	9.714E-1.	7.434E-1.	5.719E-1.	4.414E-1.
C	49	50	51	52	53	54
	3.408E-1.	2.629E-1.	2.021E-1.	1.548E-1.	1.184E-1.	9.050E-2.
C	55	56	57	58	59	60
	6.909E-2.	5.271E-2.	4.017E-2.	3.051E-2.	2.306E-2.	1.735E-2.
C	61	62	63	64	65	66
	1.298E-2.	9.661E-3.	7.152E-3.	5.263E-3.	3.851E-3.	2.800E-3.
C	67	68	69	70	71	72
	2.022E-3.	1.460E-3.	1.061E-3.	7.762E-4.	5.715E-4.	4.234E-4.
C	73	74	75	76	77	78

CONT. ON PG 35

PARTS
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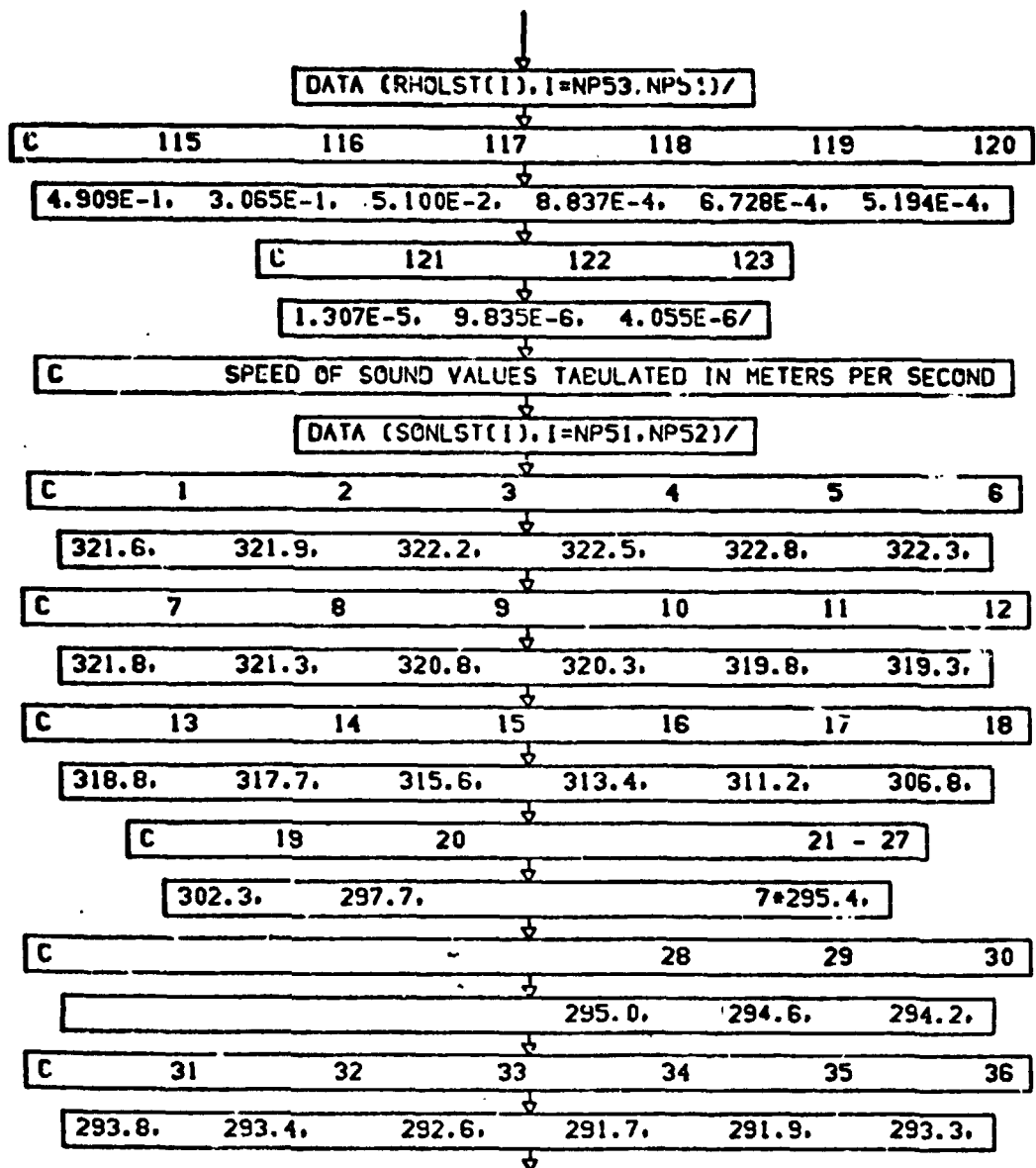
CONT. ON PG 36

PARTS
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	2.422E-1.	2.071E-1.	1.770E-1.	1.517E-1.	1.300E-1.	1.113E-1.
C	31	32	33	34	35	36
	9.530E-2.	8.156E-2.	5.966E-2.	4.357E-2.	3.157E-2.	2.275E-2.
C	37	38	39	40	41	42
	1.645E-2.	1.193E-2.	8.676E-3.	6.264E-3.	4.551E-3.	3.330E-3.
C	43	44	45	46	47	48
	2.453E-3.	1.819E-3.	1.357E-3.	1.018E-3.	7.682E-4.	5.911E-4.
C	49	50	51	52	53	54
	4.564E-4.	3.559E-4.	2.774E-4.	2.150E-4.	1.651E-4.	1.266E-4.
C	55	56	57	58	59	60
	9.708E-5.	7.435E-5.	5.701E-5.	4.408E-5.	3.392E-5.	2.599E-5.
C	61	62	63	64	65	66
	1.981E-5.	1.503E-5.	1.134E-5.	8.516E-6.	6.357E-6.	4.717E-6.
C	67	68	69	70	71	72
	3.480E-6.	2.467E-6.	1.757E-6.	1.260E-6.	9.093E-7.	6.607E-7.
C	73	74	75	76	77	78
	4.803E-7.	3.479E-7.	2.550E-7.	1.891E-7.	1.417E-7.	1.067E-7.
C	79	80	81 - 114			
	7.890E-8.	5.950E-8.	34*4.567E-8/			

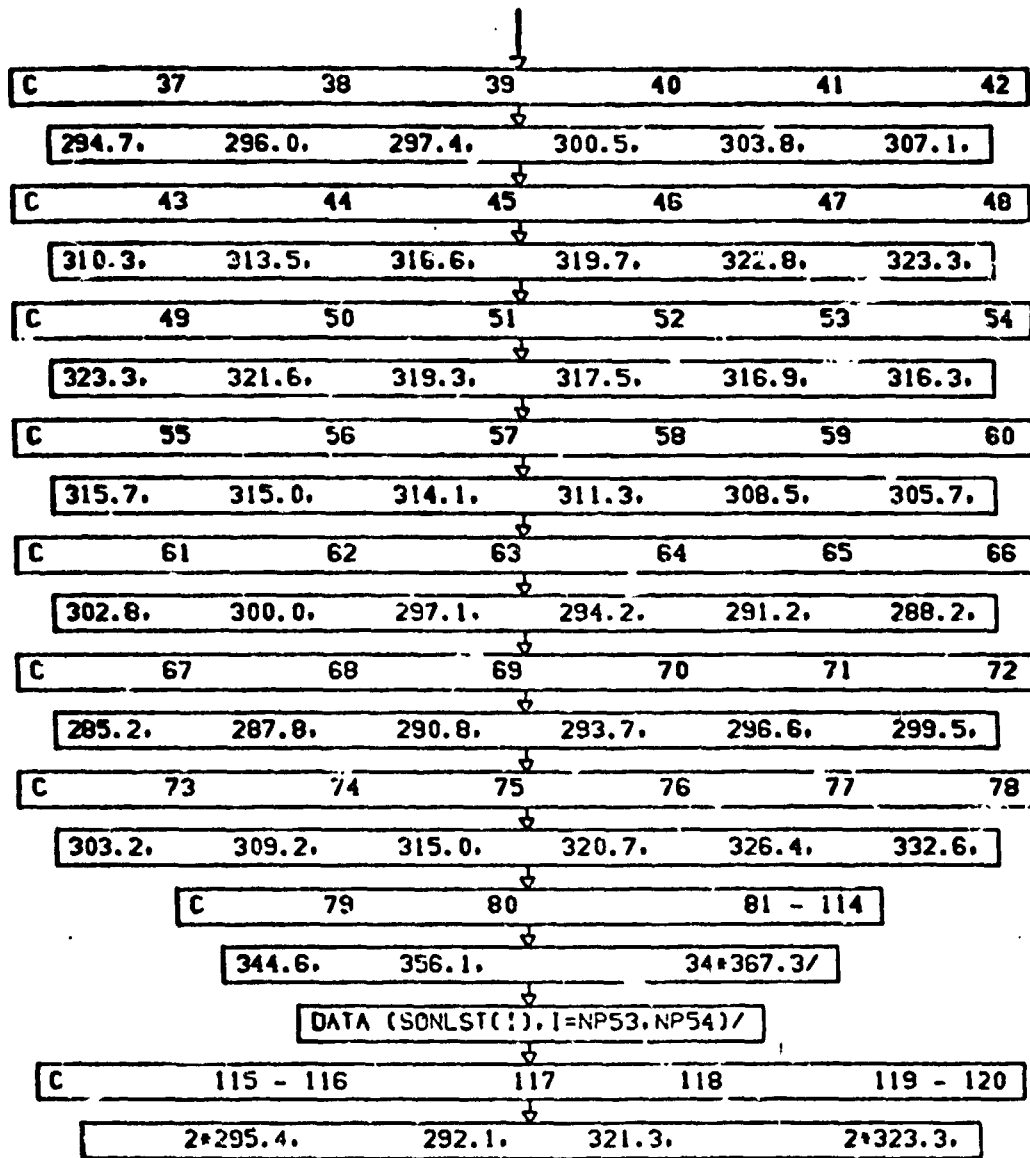
CONT. ON PG 37

PARTS
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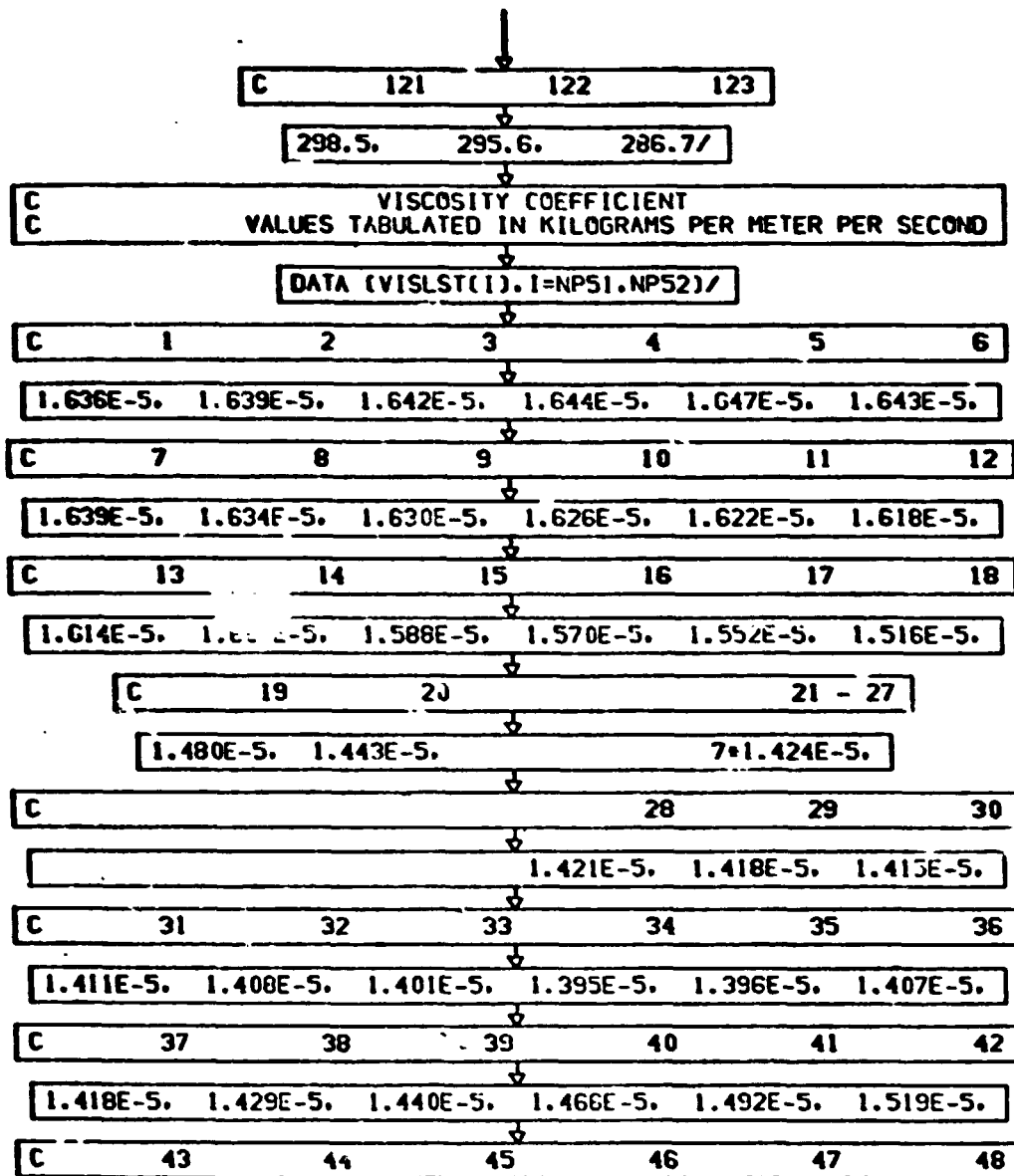
CONT. ON PG 38

PARTS
PG 37 OF 52



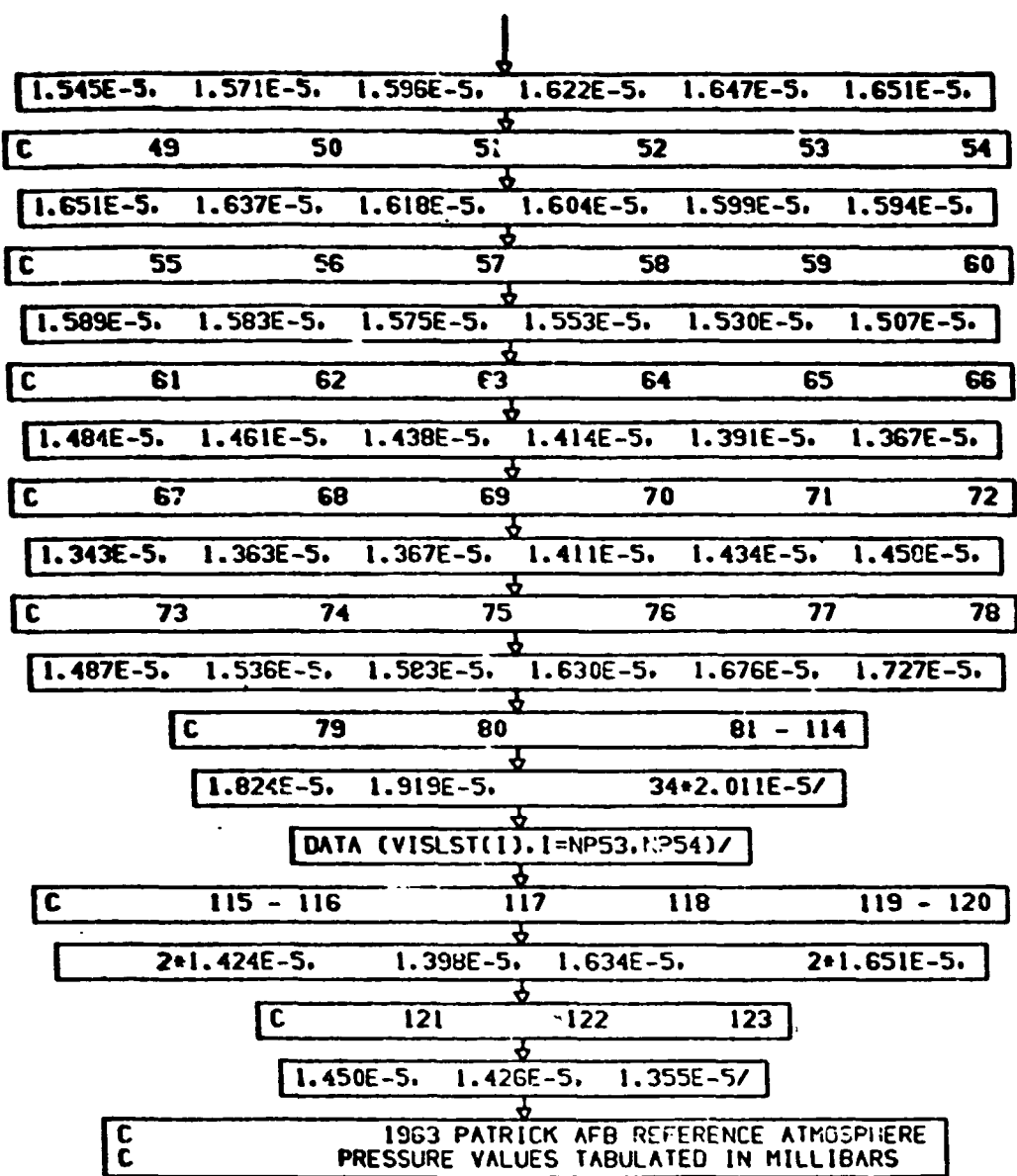
CONT. ON PG 39

PARTS
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CONT. ON PG 40

PARTS
PG 39 OF 52



CONT. ON PG 41

PARTS
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DATA (PRSLST(1),I=NP61, NP62)/

C	1	2	3	4	5
1.0170147E+3.9.8829373E+2.9.6022651E+2.9.3280664E+2.9.0603418E+2.					
C	6	7	8	9	10
8.7989596E+2.8.5409573E+2.8.2949430E+2.8.0521168E+2.7.8152728E+2.					
C	11	12	13	14	15
7.5843002E+2.7.3590840E+2.7.1395065E+2.6.7167869E+2.6.3151745E+2.					
C	16	17	18	19	20
5.9337050E+2.5.5714348E+2.4.9009912E+2.4.2967959E+2.3.7532040E+2.					
C	21	22	23	24	25
3.2649869E+2.2.8277555E+2.2.4373144E+2.2.0909281E+2.1.7861068E+2.					
C	26	27	28	29	30
1.5199026E+2.1.2892856E+2.1.0911841E+2.9.2252642E+1.7.8097365E+1.					
C	31	32	33	34	35
6.6260092E+1.5.6315652E+1.4.0899191E+1.2.9918759E+1.2.2038159E+1.					
C	36	37	38	39	40
1.6327363E+1.1.2146273E+1.9.0905080E+0.6.8429914E+0.5.1807184E+0.					
C	41	42	43	44	45
3.9447995E+0.3.0209180E+0.2.3262411E+0.1.8004513E+0.1.3994781E+0.					

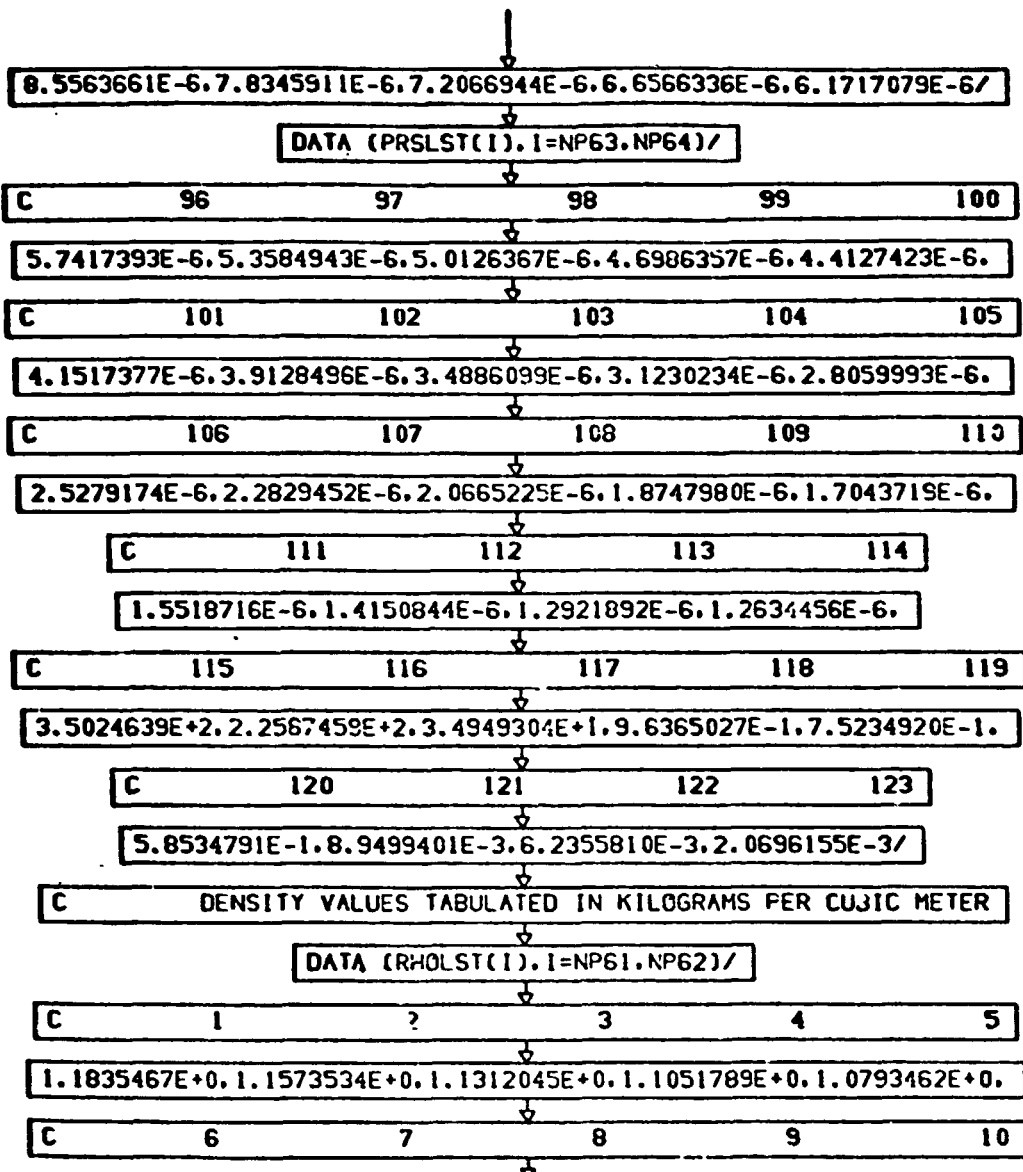
CONT. ON PG 42

PARTS
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C	46	47	48	49	50
↓					
1.0910568E+0.8.5180215E-1.6.6393197E-1.5.1553130E-1.3.9852059E-1.					
C	51	52	53	54	55
↓					
3.0651143E-1.2.3442082E-1.1.7818466E-1.1.3454170E-1.1.0086976E-1.					
C	56	57	58	59	60
↓					
7.5059128E-2.5.5414297E-2.4.0576003E-2.2.9458738E-2.2.1200623E-2.					
C	61	62	63	64	65
↓					
1.5119931E-2.1.0684305E-2.7.4793850E-3.5.1678215E-3.3.5914714E-3.					
C	66	67	68	69	70
↓					
2.4869045E-3.1.7224435E-3.1.2093941E-3.8.4635721E-4.6.0330423E-4.					
C	71	72	73	74	75
↓					
4.3449711E-4.3.1597170E-4.2.3253935E-4.1.7351145E-4.1.3111039E-4.					
C	76	77	78	79	80
↓					
1.0022554E-4.7.7438980E-5.6.0696757E-5.4.8386073E-5.3.9145232E-5.					
C	81	82	83	84	85
↓					
3.2082435E-5.2.6597710E-5.2.2377934E-5.1.9141913E-5.1.6599345E-5.					
C	86	87	88	89	90
↓					
1.4560872E-5.1.2898417E-5.1.1522650E-5.1.0369626E-5.9.3925204E-6.					
C	91	92	93	94	95
↓					

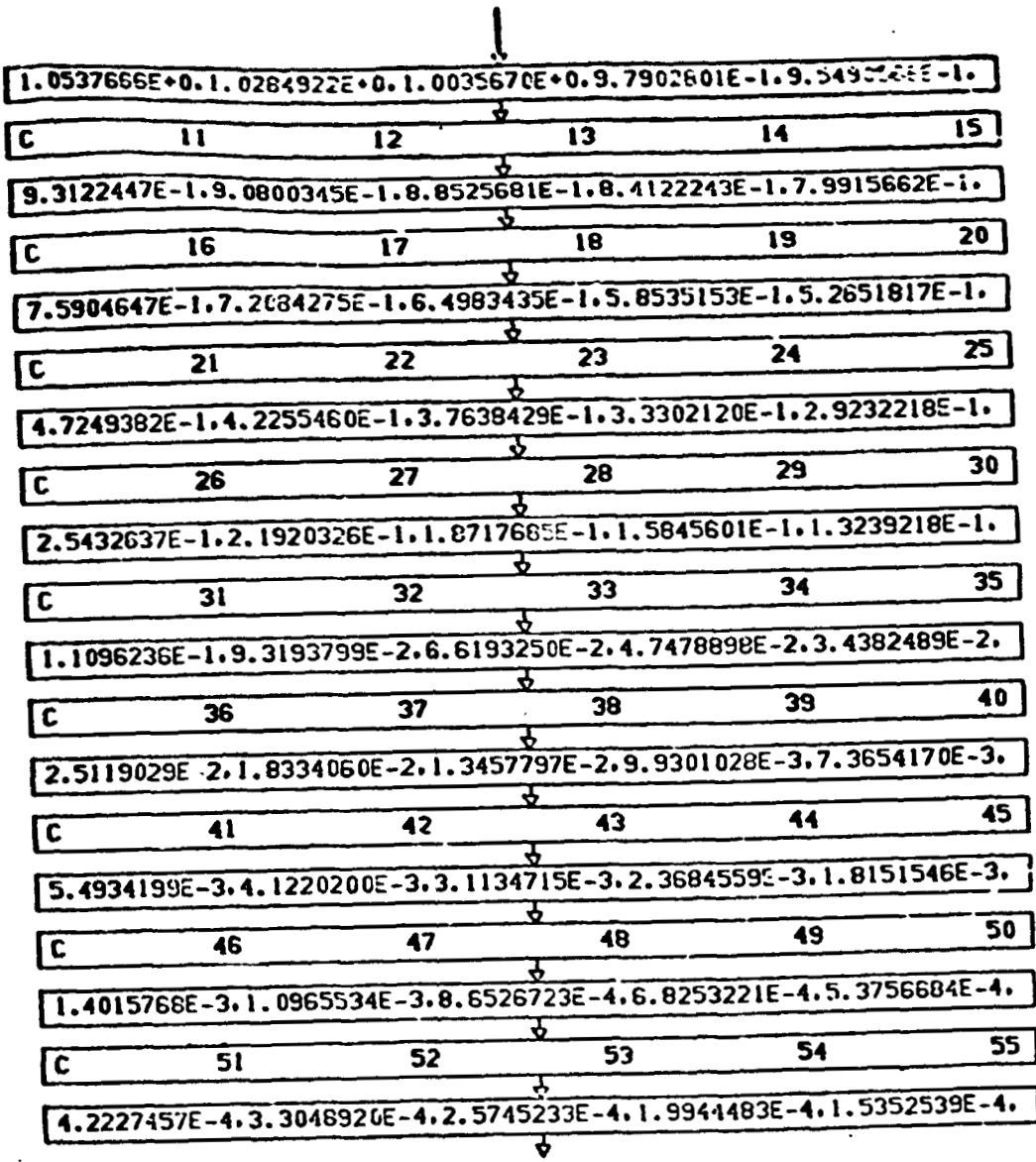
CONT. ON PG 43

PARTS
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CONT. CN PG 44

PARTS
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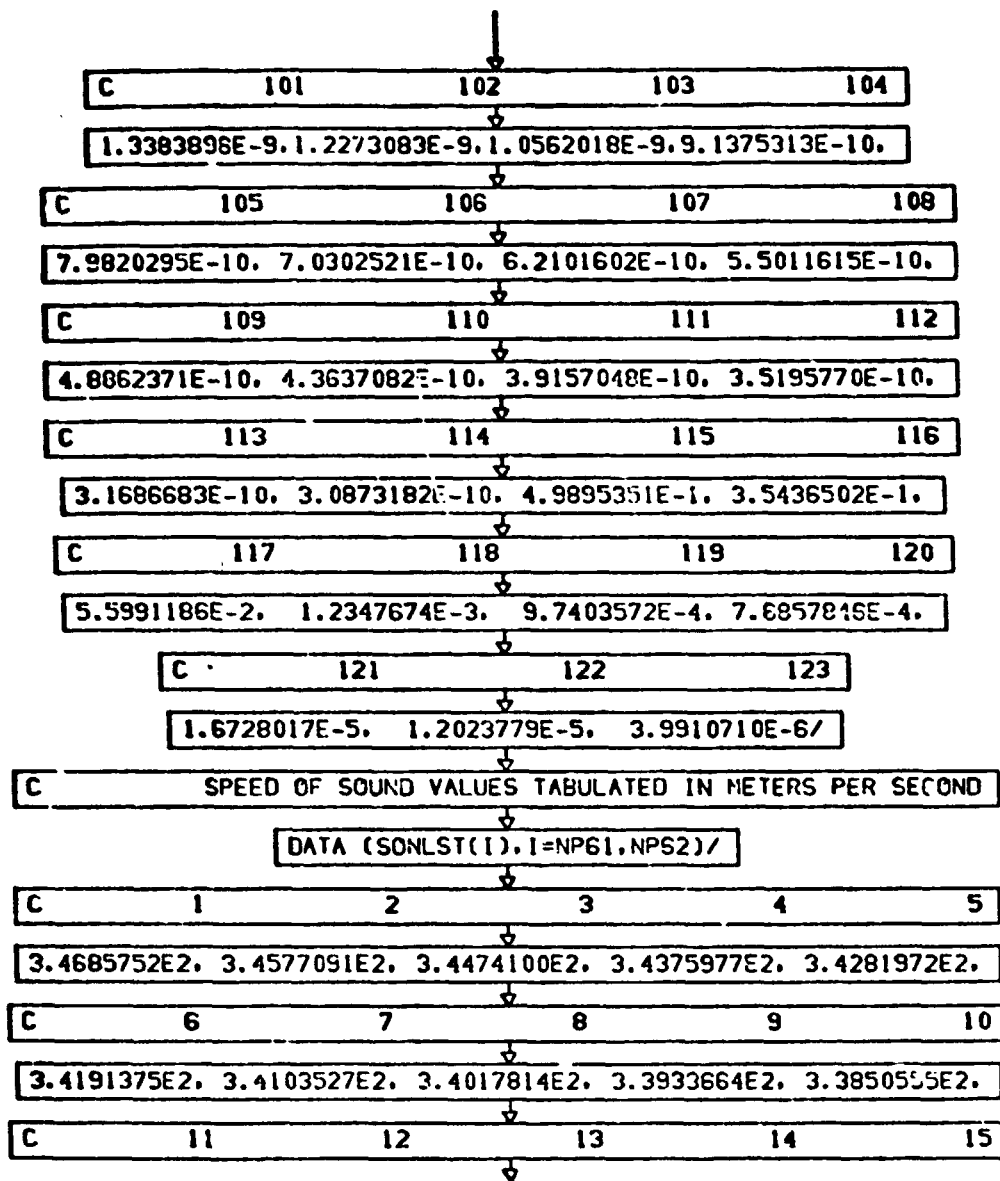
CONT. ON PG 45

PARTS
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C	56	57	58	59	60
1.1734238E-4.0.6997903E-5.6.6949356E-5.4.9935490E-5.3.6923403E-5.					
C	61	62	63	64	65
2.7067399E-5.1.9677408E-5.1.4194402E-5.1.0004200E-5.6.9259360E-6.					
C	66	67	68	69	70
4.7957760E-6.3.3215805E-6.2.2404228E-6.1.5304616E-6.1.0579997E-6.					
C	71	72	73	74	75
7.3902724E-7.5.2254595E-7.3.6173880E-7.2.6206711E-7.1.8979684E-7.					
C	76	77	78	79	80
1.3929915E-7.1.0349983E-7.7.5342182E-8.5.6095657E-8.4.2529020E-8.					
C	81	82	83	84	85
3.2809278E-8.2.5691890E-8.1.9457748E-8.1.5133149E-8.1.2030946E-8.					
C	86	87	88	89	90
9.7426983E-9.8.0146089E-9.6.6829568E-9.5.6387136E-9.4.8072428E-9.					
C	91	92	93	94	95
4.1362113E-9.3.5031390E-9.3.1356758E-9.2.7585267E-9.2.4414047E-9/					
DATA (RHOLST(I), I=NP63, NP64)/					
C	96	97	98	99	100
2.1726345E-9.1.9431903E-9.1.7627216E-9.1.6037353E-9.1.4631480E-9.					

CONT. ON PG 46

PARTS
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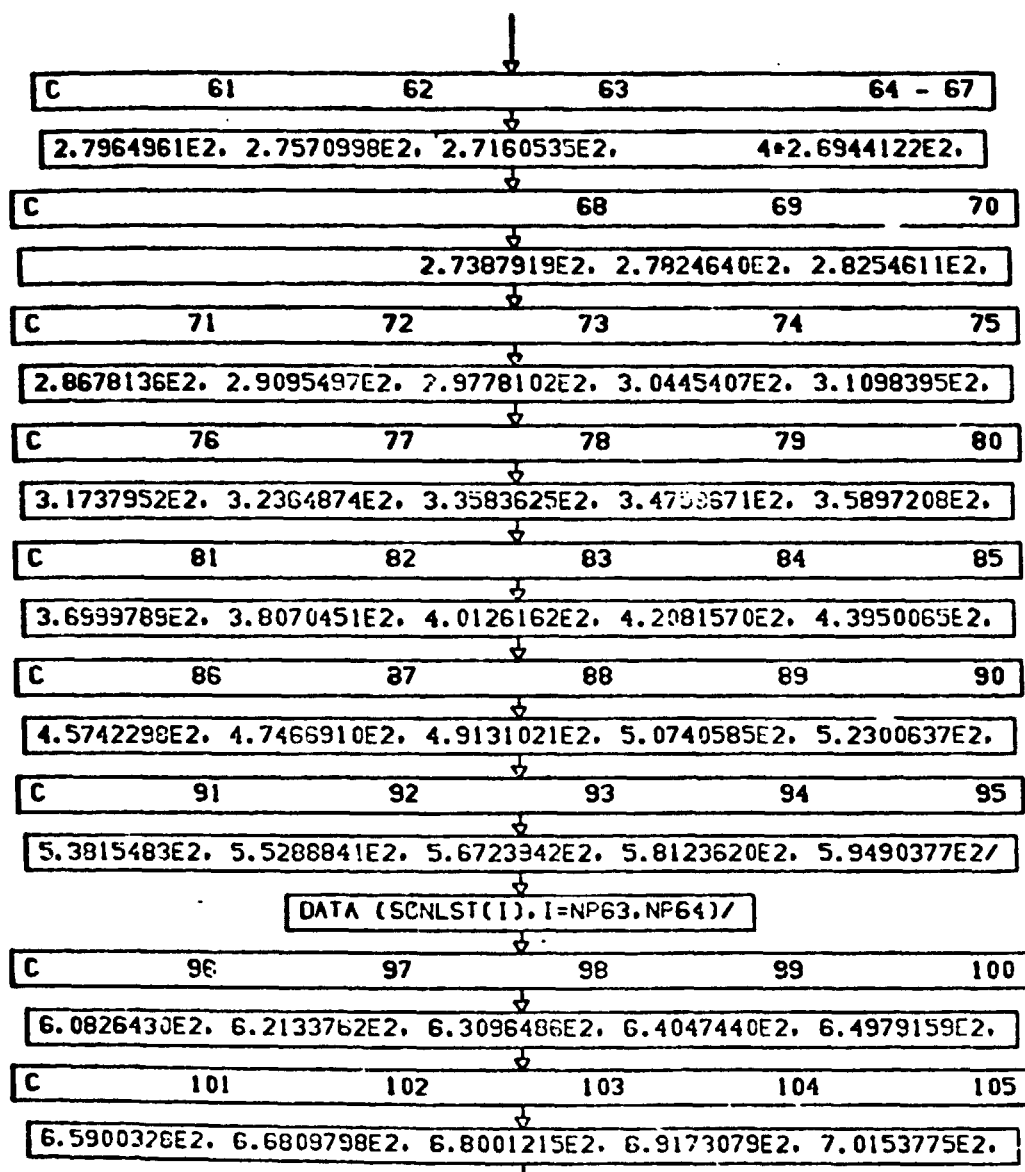
CONT. ON PG 47

PARTS
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3	8	9	10	11	12
4	13	14	15	16	17
5	18	19	20	21	22
6	23	24	25	26	27
7	28	29	30	31	32
8	33	34	35	36	37
9	38	39	40	41	42
10	43	44	45	46	47
11	48	49	50	51	52
12	53	54	55	56	57
13	58	59	60	61	62

CONT. ON PG 48

PARTS
PG 47 OF 52



CONT. ON PG 49

PARTS
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C	106	107	108	109	110
7.0951229E2, 7.1739818E2, 7.2519835E2, 7.3291548E2, 7.3946609E2.					
C	111	112	113	114	115
7.4488092E2, 7.5025666E2, 7.5559417E2, 7.5692267E2, 3.1349187E2.					
C	116	117	118	119	120
2.9879332E2, 2.9577557E2, 3.3054537E2, 3.2884119E2, 3.2653283E2.					
C	121	122	123		
2.7368549E2, 2.6945229E2, 2.6944122E2/					
C	VISCOSITY COEFFICIENT VALUES TABULATED IN KILOGRAMS PER METER PER SECOND				
C	DATA (VISLST(I), I=NP61, NP62)/				
C	1	2	3	4	5
1.8302431E-5, 1.8224157E-5, 1.8149999E-5, 1.8079299E-5, 1.8011441E-5.					
C	6	7	8	9	10
1.7945850E-5, 1.7881991E-5, 1.7819367E-5, 1.7757524E-5, 1.7696042E-5.					
C	11	12	13	14	15
1.7634541E-5, 1.7572676E-5, 1.7510139E-5, 1.7381977E-5, 1.7248245E-5.					
C	16	17	18	19	20
1.7107621E-5, 1.6959239E-5, 1.6637781E-5, 1.6284601E-5, 1.5905319E-5.					
C	21	22	23	24	25

CONT. ON PG 50

PARTS
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	1.5509244E-5, 1.5108096E-5, 1.4707842E-5, 1.4335282E-5, 1.4108886E-5,				
C	26	27	28	29	30
	1.3745403E-5, 1.3558590E-5, 1.3457958E-5, 1.3447579E-5, 1.3585386E-5,				
C	31	32	33	34	35
	1.3724675E-5, 1.3867977E-5, 1.4145944E-5, 1.4389370E-5, 1.4587102E-5,				
C	36	37	38	39	40
	1.4748972E-5, 1.4982730E-5, 1.5223539E-5, 1.5474160E-5, 1.5734080E-5,				
C	41	42	43	44	45
	1.5999574E-5, 1.6263778E-5, 1.6516764E-5, 1.6745577E-5, 1.6934206E-5,				
C	46	47	48	49	50
	1.7063446E-5, 1.7034883E-5, 1.6870136E-5, 1.6660460E-5, 1.6414072E-5,				
C	51	52	53	54	55
	1.6138668E-5, 1.5841407E-5, 1.5528854E-5, 1.5206885E-5, 1.4880579E-5,				
C	56	57	58	59	60
	1.4554073E-5, 1.4230412E-5, 1.3911371E-5, 1.3597275E-5, 1.3286809E-5,				
C	61	62	63	64 - 67	
	1.2976813E-5, 1.2662082E-5, 1.2335131E-5, 4*1.2163172E-5,				
C			68	69	70
	1.2516126E-5, 1.2864314E-5, 1.3208747E-5,				

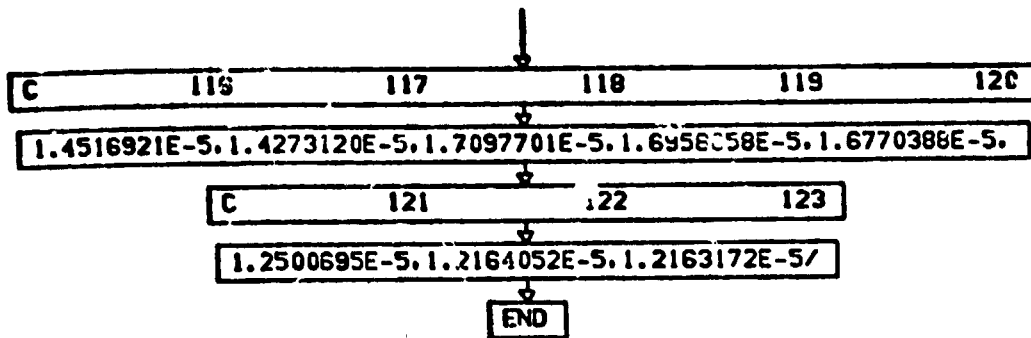
CONT. ON PG 51

PARTS
PG 50 OF 52

C	71	72	73	74	75
1.3540638E-5, 1.3884397E-5, 1.4435101E-5, 1.4975097E-5, 1.5504842E-5,					
C	76	77	78	79	80
1.6024767E-5, 1.6535285E-5, 1.7529632E-5, 1.8490756E-5, 1.9421230E-5,					
C	81	82	83	84	85
2.0323355E-5, 2.1199197E-5, 2.2879253E-5, 2.4474125E-5, 2.5994216E-5,					
C	86	87	88	89	90
2.7448117E-5, 2.8842997E-5, 3.0184890E-5, 3.1478926E-5, 3.2729499E-5,					
C	91	92	93	94	95
3.3940400E-5, 3.5114925E-5, 3.6255956E-5, 3.7366033E-5, 3.8447395E-5/					
DATA (VISLST(1), I=NP63, NP64)/					
C	96	97	98	99	100
3.9502050E-5, 4.0531768E-5, 4.1288666E-5, 4.2033057E-5, 4.2765514E-5,					
C	101	102	103	104	105
4.3486565E-5, 4.4196706E-5, 4.5127375E-5, 4.6040465E-5, 4.6803460E-5,					
C	106	107	108	109	110
4.7423142E-5, 4.8035293E-5, 4.8640170E-5, 4.9238014E-5, 4.9745032E-5,					
C	111	112	113	114	115
5.0163831E-5, 5.0579335E-5, 5.0991617E-5, 5.1094193E-5, 5.15708689E-5,					

CONT. ON PG 52

PARTS
PG 51 OF 52



PARTS
Pg. 52 FINAL

W FOR SDAT,SDAT
 UNITAC 1104 FURTHER Y EXEC 11 LEVEL 25A -1E2EEN LLVEL 212010012A1
 THIS COMPILATION WAS ON JUN 11 FEB 74 AT 20:52:09

11 FEB 74

20:52:09.02

SUBROUTINE SDAT ENTRY POINT 000275

STORAGE USED: (CODE) 000311; (DATA) 000059; BLANK COMMON(2) 000000

COMMON BLOCKS:

0003 ATDATA 004200
 0004 SPLDAT 004037

EXTERNAL REFERENCES (BLOCK, NAME)

C: 1 SPLN1
 C: 14 DEFPSA

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0001 000010 I124	0001 000090 I294	0001 00005C I226	0003 R 005410 ALTLST	0004 R 000000 ALTTAB
0004 R 001497 CP	0004 R 001725 CR	0004 R 001503 CS	0004 R 003241 CV	0003 R 004174 D
0000 I 006003 I	0000 I 000004 IJ	0000 000027 INJPS	0000 I 000002 IOP1	0000 I 000007 J
0000 I 000001 JH	0000 I 000000 JI	0000 I 000005 A	0000 I 000004 R	0003 R 000000 PASLST
0004 R 000173 PRSTAB	0003 R 001342 RHOLST	0004 R 000364 RHOTAB	0003 R 002200 S0NLST	0004 R 000541 S0NTAB
0003 R 004244 VISLST	0004 R 030754 /1STAB	0003 R 004003 PORC	0000 R 000010 R3	0000 R 000011 Y31
0000 R 000012 Y32	0000 R 000013 Y33	0000 R 000014 Y34		

00101	10		SUBROUTINE SDAT(TOP)
00101	20	C	
00103	30		PARAMETER NP = 123, NPA = 0*NP, NP3 = 3*NP - 3
00103	40	C	
00104	50		COMMON/ATDATA/
00104	60		(PRSLST(INP4), RHOLST(INP4), S0NLST(INP4), VISLST(INP4),
00104	70		ZAL(LST(INP4), R0NC(INP4), D1Z,
00104	80	C	
00105	90		COMMON /SPLDAT/
00105	100		(ALTTAB(INP), PRSTAB(INP), RHOTAB(INP), S0NTAB(INP), Y1STAB(INP),
00105	110		CP(INP3), CR(INP3), CS(INP3), CV(INP3)
00105	120	C	
00106	130		DATA JI, JH /1, 1/
00106	140	C	
00106	150	C	
00106	160	C	
00106	170	C	TOP.....AN INTEGER VARIABLE RANGING FROM 0 TO 5 USED TO DESIGNATE
00106	180	C	THE ATMOSPHERE MODEL TO BE USED
00106	190	C	
00106	200	C	TOP = 0 - 1962 STANDARD ATMOSPHERE
00106	210	C	
00106	220	C	TOP = 1 - 1964 STANDARD FOR JULY AT 30 DEG. N. LATITUDE
00106	230	C	

ORIGINAL PAGE IS
 OF POOR QUALITY

C2

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00106 240 C IOP = 2 - 1966 STANDARD FOR JAN. AT 30 DEG. N. LATITUDE
00106 250 C
00106 260 C IOP = 3 - 1966 STANDARD FOR JULY AT 60 DEG. N. LATITUDE
00106 270 C
00106 280 C IOP = 4 - 1966 STANDARD FOR JAN. AT 60 DEG. N. LATITUDE
00106 290 C
00106 300 C IOP = 5 - 1963 PATRICK AFB REFERENCE STANDARD
00106 310 C
00106 320 C
00106 330 C
00106 340 C SELECT DESIRED ATMOSPHERE INDEX ADJUSTOR
00106 350 C
00111 360 C IOP1 = IOP*NP
00111 370 C
00111 380 C TRANSFER PERTINENT ATMOSPHERE DATA FROM STORAGE ARRAY TO WORKING
00111 390 C ARRAY AND CONVERT TO DESIRED WORKING UNITS (BRITISH ENGINEERING)
00111 400 C
00112 410 C DO 1 I = 1, NP
00112 420 C
00112 430 C TRANSFER ALTITUDE VALUES LIST TO WORKING ARRAY
00112 440 C
00115 450 C ALTYAB(I) = ALTST(I)/0.3048
00115 460 C
00115 470 C TRANSFER PRESSURE VALUES LIST TO WORKING ARRAY
00115 480 C
00116 490 C PRSYAB(I) = PRSLST(IOP1 + 1)/2.11622/1.01325
00116 500 C
00116 510 C TRANSFER DENSITY VALUES LIST TO WORKING ARRAY
00116 520 C
00117 530 C RHOYAB(I) = RHO1ST(IOP1 + 1)/7.6479E-2/(1.225*32.17409)
00117 540 C
00117 550 C TRANSFER SPEED OF SOUND VALUES LIST TO WORKING ARRAY
00117 560 C
00120 570 C SONTAB(I) = SONLST(IOP1 + 1)/0.3048
00120 580 C
00120 590 C TRANSFER COEFFICIENT OF VISCOSITY VALUES LIST TO WORKING ARRAY
00120 600 C
00121 610 C VISTAB(I) = VISLST(IOP1 + 1)/1.02029/(1.7897*32.1741)
00123 620 C M = NP - 1
00123 630 C
00123 640 C REARRANGE DATA IN ACCORDANCE WITH ASCENDING VALUES OF THE
00123 650 C INDEPENDENT VARIABLE - ALTITUDE
00123 660 C
00124 670 C
00127 680 C DO 300 I = 1, M
00130 690 C K = 1
00131 700 C IJ = 1 + 1
00134 710 C DO 200 J = IJ, NP
00136 720 C IF (ALTYAB(K).GT.ALTYAB(IJ)) K = J
00140 730 C 200 CONTINUE
00141 740 C AS = ALTYAB(K)
00142 750 C YS1 = PRSYAB(K)
00143 760 C YS2 = RHOYAB(K)
00144 770 C YS3 = SONTAB(K)
00145 780 C YS4 = VISTAB(K)
00146 790 C ALTYAB(K) = ALTYAB(IJ)
00147 800 C PRSYAB(K) = PRSYAB(IJ)
00147 810 C RHOYAB(K) = RHOYAB(IJ)
00150 810 C SONTAB(K) = SONTAB(IJ)

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00151      82°      VISTAB(K) = VISTAB(I)
00152      83°      ALTTAB(I) = AS
00153      84°      PRSTAB(I) = YS1
00154      85°      RHOTAB(I) = YS2
00155      86°      SONTAB(I) = YS3
00156      87°      300 VISTAB(I) = YS4
00156      88°      C
00156      89°      C
00156      90°      C
00156      91°      C
00156      92°      C
00156      93°      C
00156      94°      C
00156      95°      C
00156      96°      C
00156      97°      C
00160      98°      D(1) = (PRSTAB(2) - PRSTAB(1))/(ALTTAB(2) - ALTTAB(1))
00161      99°      D(2) = (PRSTAB(NP) - PRSTAB(NP-1))/(ALTTAB(NP) - ALTTAB(NP-1))
00161     100°      C
00161     101°      C
00161     102°      C
00162     103°      CALL SPLN(INP,ALTTAB,PRSTAB,JI,JN,D,CP,WORK)
00162     104°      C
00162     105°      C
00163     106°      D(1) = (RHOTAB(2) - RHOTAB(1))/(ALTTAB(2) - ALTTAB(1))
00164     107°      D(2) = (RHOTAB(NP) - RHOTAB(NP-1))/(ALTTAB(NP) - ALTTAB(NP-1))
00164     108°      C
00164     109°      C
00164     110°      C
00165     111°      CALL SPLN(INP,ALTTAB,RHOTAB,JI,JN,D,CR,WORK)
00165     112°      C
00165     113°      C
00166     114°      D(1) = (SONTAB(2) - SONTAB(1))/(ALTTAB(2) - ALTTAB(1))
00167     115°      D(2) = (SONTAB(NP) - SONTAB(NP-1))/(ALTTAB(NP) - ALTTAB(NP-1))
00167     116°      C
00167     117°      C
00167     118°      C
00167     119°      C
00170     120°      CALL SPLN(INP,ALTTAB,SONTAB,JI,JN,D,CS,WORK)
00170     121°      C
00170     122°      C
00171     123°      D(1) = (VISTAB(2) - VISTAB(1))/(ALTTAB(2) - ALTTAB(1))
00172     124°      D(2) = (VISTAB(NP) - VISTAB(NP-1))/(ALTTAB(NP) - ALTTAB(NP-1))
00172     125°      C
00172     126°      C
00172     127°      C
00172     128°      C
00173     129°      CALL SPLN(INP,ALTTAB,VISTAB,JI,JN,D,CV,WORK)
00173     130°      C
00173     131°      C
00174     132°      RETURN
00175     133°      END

```

END OF COMPILATION! NO DIAGNOSTICS.

W FOR ATMSPL,ATMSPL
 -NIVAL 1100 FORTSAR V L2EC 11 LEVEL 25A -124ECB LEVEL 112010010A
 THIS COMPILATION WAS DONE ON 11 FEB 74 AT 20:52:11

11 FEB 74

20152111. 13

SUBROUTINE ATMSPL ENTRY POINT 000211

STORAGE USED: CODE(1); 000227; DATA(8); 000021; BLANK COMMON(2); 000000

COMMON BLOCKS:

0003 S PLOAT 000037

EXTERNAL REFERENCES (BLOCK, NAME):

0004 REF225

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME):

0001	000023	10L	0001	000035	100L	0001	000050	200L	0001	200131	500L	0001	000151	501L	
0002	R	000000	ALTTAB	0002	R	001147	CP	0002	R	001725	CR	0002	R	001725	CS
0000	R	000002	ZI	0000	I	000001	I	0000	000000	INJPS	0000	I	0000	IS	
0002	R	000240	RHDTAB	0002	R	000261	SOHTAB	0002	R	000754	VISTAB	0002	R	000773	PRSTAB

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00101 10      SUBROUTINE ATMSPL(V,PANS)
00101 20      C
00102 30      C   PARAMETER NP = 123, NP = JUMP + 3
00103 40      C
00104 50      C   DIMENSION
00104 60      C   IFANS(8)
00104 70      C
00105 80      C   COMMON /SPLDAT/
00105 90      C   (ALTTAB(NP), PRSTAB(NP), RHDTAB(NP), SOHTAB(NP), VISTAB(NP),
00105 100     C   ZCP(NP), CR(NP), CS(NP), CV(NP))
00105 110     C
00106 120     C   DATA IS / 1 /
00106 130     C
00106 140     C
00106 150     C   ESTABLISH THE INTERVAL IN WHICH THE SPECIFIED ALTITUDE LIES
00106 160     C
00106 170     C
00110 180     C   IF(V-LE-ALTTAB(1))GO TO 500
00112 190     C   IF(V-GE-ALTTAB(NP))GO TO 501
00114 200     C   I = 15
00115 210     C   IF(V-GT-ALTTAB(1))GO TO 100
00117 220     C   I = I - 1
00120 230     C   IF(V-LT-ALTTAB(1))GO TO 10
00122 240     C   GO TO 200
00123 250     C   100 I = I + 1
00124 260     C   IF(V-GT-ALTTAB(1))GO TO 100
00126 270     C   I = I - 1
00127 280     C   200 IS = I
  
```

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00130 290      DX = V - ALTTAB(I)
00130 300      C
00130 310      C   EMPLOY CUBIC INTERPOLATION TO COMPUTE PRESSURE/SEA LEVEL RATIO
00130 320      C
00131 330      FANS(1) = PRSTAB(I) + ((CP(3*1)*DX + CP(3*1-1)*DX + CP(3*1-2))*DX
00132 340      FANS(5) = FANS(1)/PRSTAB(I)
00132 350      C
00132 360      C   EMPLOY CUBIC INTERPOLATION TO COMPUTE DENSITY/SEA LEVEL RATIO
00132 370      C
00133 380      FANS(2) = RHOTAB(I) + ((CR(3*1)*DX + CR(3*1-1)*DX + CR(3*1-2))*DX
00134 390      FANS(6) = FANS(2)/RHOTAB(I)
00134 400      C
00134 410      C   EMPLOY CUBIC INTERPOLATION TO COMPUTE SPEED OF SOUND/SEA LEVEL
01 34 420      C   RATIO
00134 430      C
00135 440      FANS(3) = SONTAB(I) + ((CS(3*1)*DX + CS(3*1-1)*DX + CS(3*1-2))*DX
00136 450      FANS(7) = FANS(3)/SONTAB(I)
00136 460      C
00136 470      C   EMPLOY CUBIC INTERPOLATION TO COMPUTE COEFFICIENT OF VISCOSITY/SEA
00136 480      C   LEVEL RATIO
00136 490      C
00137 500      FANS(4) = VISTAB(I) + ((CV(3*1)*DX + CV(3*1-1)*DX + CV(3*1-2))*DX
00140 510      FANS(8) = FANS(4)/VISTAB(I)
00141 520      RETURN
00141 530      C
00141 540      C
00141 550      C   INITIAL BOUNDARY VALUES - FUNCTION/SEA LEVEL RATIO
00141 560      C
00142 570      500 FANS(1) = PRSTAB(I)
00143 580      FANS(2) = RHOTAB(I)
00144 590      FANS(3) = SONTAB(I)
00145 600      FANS(4) = VISTAB(I)
00146 610      FANS(5) = 1.0
00147 620      FANS(6) = 1.0
00150 630      FANS(7) = 1.0
00151 640      FANS(8) = 1.0
00152 650      RETURN
00152 660      C
00152 670      C
00152 680      C   TERMINAL BOUNDARY VALUES - FUNCTION/SEA LEVEL RATIO
00152 690      C
00153 700      501 FANS(1) = PRSTAB(NP)
00154 710      FANS(2) = RHOTAB(NP)
00155 720      FANS(3) = SONTAB(NP)
00156 730      FANS(4) = VISTAB(NP)
00157 740      FANS(5) = FANS(1)/PRSTAB(I)
00160 750      FANS(6) = FANS(2)/RHOTAB(I)
00161 760      FANS(7) = FANS(3)/SONTAB(I)
00162 770      FANS(8) = FANS(4)/VISTAB(I)
00162 780      C
00162 790      C
00163 800      RETURN
00164 810      END

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END OF COMPILATION: NO DIAGNOSTICS.

M FOR SPLM1,SPLM1
 UNITAC 1100 PONTIAC V LABC 11 LEVEL 264 -IERECC LEVEL [120100100]
 THIS COMPILATION WAS DONE ON 11 FEB 74 AT 20152:12

11 FEB 74

20152112-667

SUBROUTINE SPLM1 ENTRY POINT 000676

SOURCE USL01 (00L11) 0007371 DATA(0) 0001101 BLANK (COMMON:2) 000000

EXTERNAL REFERENCES (BLOCK, NAME)

0002 HERR20
 0004 HERR20

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0001	000130	1L	0001	000230	1176	0001	000291	1356	0001	000301	1436	0001	000473	1616
0001	000557	1A76	0001	000579	1706	0001	000152	2L	0001	000205	2AL	0001	000610	2016
0001	000161	3L	0001	000367	4L	0001	000320	40L	0001	000540	5AL	0001	000731	70L
0001	000569	71L	0000	000000	1	0000	000019	14JPS	0000	000000	4	0000	000002	4H

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00101 10 SUBROUTINE SPLM1(M,X,T,J1,JN,D,C,0)
00101 20 C
00103 30 DIMENSION R(1),Y(1),D(2),D(1),C(1)
00103 40 C
00103 50 C
00103 60 C M - AN INTEGER DENOTING THE NUMBER OF DATA POINTS USED TO
00103 70 C REPRESENT THE FUNCTION IN THE REGION OF DEFINITION
00103 80 C
00103 90 C X - A ONE-DIMENSIONAL ARRAY DIMENSIONED BY M CONTAINING THE
00103 100 C VALUES OF THE INDEPENDENT VARIABLE IN ASCENDING ORDER
00103 110 C
00103 120 C Y - A ONE-DIMENSIONAL ARRAY DIMENSIONED BY M CONTAINING THE
00103 130 C VALUES OF THE DEPENDENT VARIABLE CORRESPONDING IN
00103 140 C SEQUENCE TO THE VALUES IN THE X ARRAY
00103 150 C
00103 160 C J1,JN - INTEGERS DEFINED AS FOLLOWS
00103 170 C
00103 180 C J1 = 1 - FIRST DERIVATIVE OF THE FUNCTION AT THE FIRST TABULATED
00103 190 C DATA POINT IS SUPPLIED IN D(1)
00103 200 C
00103 210 C J1 = 2 - SECOND DERIVATIVE OF THE FUNCTION AT THE FIRST TABULATED
00103 220 C DATA POINT IS SUPPLIED IN D(1)
00103 230 C
00103 240 C J1 = 3 - FIRST AND SECOND DERIVATIVES OF THE FUNCTION AT THE FIRST
00103 250 C DATA POINT ARE SUPPLIED IN D(1) AND D(2), RESPECTIVELY
00103 260 C
00103 270 C J1 = 4 - FIRST AND SECOND DERIVATIVES OF THE FUNCTION AT THE LAST
00103 280 C DATA POINT ARE SUPPLIED IN D(1) AND D(2), RESPECTIVELY
00103 290 C
00103 300 C JN = 1 - FIRST DERIVATIVE OF THE FUNCTION AT THE LAST TABULATED
00103 310 C DATA POINT IS SUPPLIED IN D(2)

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00103 320 C
00105 330 C JN = 2 = SECOND DERIVATIVE OF THE FUNCTION AT THE LAST TABULATED
00103 340 C DATA POINT IS SUPPLIED IN D(2)
00103 350 C
00103 360 C D = A ONE-DIMENSIONAL ARRAY DIMENSIONED BY 2 CONTAINING THE
00103 370 C VALUES OF THE DERIVATIVES OF THE FUNCTION SPECIFIED IN
00103 380 C ACCORDANCE WITH J2 AND JN
00103 390 C C = A ONE-DIMENSIONAL ARRAY DIMENSIONED BY 3*(N-1) CONTAINING
00103 400 C THE CUBIC SPLINE INTERPOLATING COEFFICIENTS FOR EACH
00103 410 C INTERVAL
00103 420 C
00103 430 C * = A ONE-DIMENSIONAL ARRAY DIMENSIONED BY N USED AS A WORKING
00103 440 C ARRAY ONLY
00103 450 C
00103 460 C
00103 470 C COMPUTE THE INITIAL VALUES OF THE RECURSIVE RELATIONS IN
00103 480 C ACCORDANCE WITH THE SPECIFIED PROPERTY OF THE FUNCTION AT THE
00103 490 C INITIAL BOUNDARY
00103 500 C
00103 510 C
00104 520 GO TO (1,2,3,4),J1
00105 530 1 R(1) = -0.5
00106 540 C(1) = 3.0/(X(2) - X(1))*(Y(2) - Y(1))/(X(2) - X(1)) - D(1)
00107 550 GO TO 20
00110 560 2 R(1) = 0.0
00111 570 C(1) = D(1)
00112 580 GO TO 20
00113 590 3 R(1) = 1.0
00114 600 C(1) = 3.0*D(2) + 6.0/(X(2) - X(1))*(D(1) - (Y(2) - Y(1))/(X(2) -
00114 610 X(1)))
00115 620 20 N = N - 1
00115 630 C
00116 640 C COMPUTE ALL INTERMEDIATE RECURSIVE RELATION VALUES
00116 650 C
00116 660 DO 30 I = 2,N
00121 670 R(I) = -(X(I+1) - X(I))/(2.0*(X(I+1) - X(I-1)) + (X(I) - X(I-1))*R
00121 680 X(I-1))
00122 690 30 C(I) = R(I)/(X(I+1) - X(I))*16.0*((Y(I) - Y(I-1))/(X(I) - X(I-1))
00122 700 X = (Y(I+1) - Y(I))/(X(I+1) - X(I)) + (X(I) - X(I-1))*C(I-1))
00122 710 C
00122 720 C COMPUTE THE TERMINAL VALUES OF THE RECURSIVE RELATION IN
00122 730 C ACCORDANCE WITH THE SPECIFIED PROPERTY OF THE FUNCTION AT THE
00122 740 C TERMINAL BOUNDARY
00122 750 C
00124 760 IF(J1.GT.2)GO TO 70
00124 770 IF(JN.EQ.2)GO TO 40
00130 780 C(N) = 16.0/(X(N) - X(N-1))*(D(2) - (Y(N) - Y(N-1))/(X(N) - X(N-1)
00130 790 X) - C(N))/(2.0 + R(N))
00130 800 C
00131 810 GO TO 50
00132 820 40 C(N) = D(2)
00132 830 C
00132 840 C COMPUTE THE APPROXIMATE SECOND DERIVATIVE VALUES OF THE FUNCTION
00132 850 C AT THE SPECIFIED DATA POINTS
00132 860 C
00133 870 GO TO 50
00134 880 70 DO 72 I = 1,N
00137 890 72 C(I+N) = C(I)

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ORIGINAL PAGE
OF POOR QUALITY


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00141  90°      C(I) = D(2)
00142  91°      DO 73 I = 1,M
00145  92°      73 C(I+1) = (C(I) - C(I+M))/M(I)
00147  93°      GO TO 71
00150  94°      * M = M - 1
00151  95°      M(M) = 1.0
00152  96°      C(M) = D(2)
00153  97°      C(M) = 6.0/(X(M) - X(M-1))*(D(1) - (Y(M) - Y(M-1))/(X(M) - X(M-1)) -
00153  98°      X3.0*D(2))
00154  99°      MM = M - 1
00155  100°     IF(MM).50,
00160  101°     DO 80 I = MM,1,-1
00163  102°     W(I) = -1.0/(X(I+1) - X(I))*(X(I+2) - X(I+1))/W(I+1) + 2.0*(X(I+2)
00163  103°     X) - X(I))
00164  104°     80 C(I) = 1.0/(X(I+1) - X(I))*(C(I+1)*(X(I+2) - X(I+1))/W(I+1) - 6.0*
00164  105°     X((Y(I+1) - Y(I))/(X(I+1) - X(I)) - (Y(I+2) - Y(I+1))/(X(I+2) - X(I)
00164  106°     X*1)))
00166  107°     50 DO 60 I = M,1,-1
00171  108°     60 C(I) = C(I) + W(I)*C(I+1)
00173  109°     71 DO 61 I = 1,M
00176  110°     61 W(I) = C(I)
00176  111°     C
00176  112°     C   COMPUTE THE CUBIC SPLINE INTERPOLATION COEFFICIENTS FOR THE 1-ST,
00176  113°     C   2-ND, AND 3-RD DEGREE TERMS, IN THAT ORDER
00176  114°     C
00200  115°     DO 62 I = 1,M
00203  116°     C(2+I-2) = (Y(I+1) - Y(I))/(X(I+1) - X(I)) - (W(I+1) + 2.0*W(I))*C
00203  117°     IX(I+1) - X(I))/6.0 ,
00204  118°     C(3+I-1) = 0.5*W(I),
00205  119°     62 C(3+I) = (W(I+1) - W(I))/6.0*(X(I+1) - X(I))
00205  120°     C
00207  121°     RETURN
00210  122°     END

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END OF COMPILATION: NO DIAGNOSTICS.

FOR SPARE PARTS, ETC
 UNITAL 1100 FURNISH Y LALC 11 LEVEL 25A -11RECH, LEVEL E12010010A1
 THIS COMPILATION WAS DONE ON 12 DEC 73 AT 13:00:50

12 DEC 73

131 618022

BLOCK DATA

STORAGE USED: (00E11) 000000: DATA0; 000001: BLANK COMMON2; 000000

COMMON BLOCKS:

0003 ATDATA 000200

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0003 R 005010 ALTLST 0003 R 000170 D 0000 I 000000 I 0003 R 000000 PRSLST 0003 R 001302 RWLST
 0003 R 002700 SOLST 0003 R 000200 VISLST 0003 R 000000 WGR

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00101 10  BLOCK DATA
00101 20  C
00102 30  PARAMETER NP = 123
00103 40  PARAMETER NP11 = 1, NP12 = 119, NP13 = 115, NP14 = NP
00104 50  PARAMETER NP21=NP11+NP, NP22=NP12+NP, NP23=NP13+NP, NP24=NP14+NP
00105 60  PARAMETER NP31=NP21+NP, NP32=NP22+NP, NP33=NP23+NP, NP34=NP24+NP
00106 70  PARAMETER NP41=NP31+NP, NP42=NP32+NP, NP43=NP33+NP, NP44=NP34+NP
00107 80  PARAMETER NP51=NP41+NP, NP52=NP42+NP, NP53=NP43+NP, NP54=NP44+NP
00108 90  PARAMETER NP61=NP51+NP, NP62=NP52+NP, NP63=NP53+NP, NP64=NP54+NP
00110 100 C
00111 110 COMMON/ATDATA/
00111 120 (PRSLSTINP(1), RWLSTINP(1), SOLSTINP(1), VISLSTINP(1),
00111 130 2ALTLSTINP(1), WGRINP, 0121)
00111 140 C
00111 150 C
00111 160 C
00111 170 C
00112 180 DATA (ALTLST(1), NP11, NP12)/
00112 190 1 2 3 4 5 6
00112 200 C 20 2000, 2.5E3, 5.0E3, 7.5E3, 1.0E4, 1.25E4. 1
00112 210 7 8 9 10 11 12
00112 220 C 22 2200, 2.75E3, 2.0E3, 2.25E3, 2.5E3, 2.75E3. 2
00112 230 C 13 14 15 16 17 18
00112 240 C 24 2400, 3.5E3, 4.0E3, 4.5E3, 5.0E3, 6.0E3. 3
00112 250 C 19 20 21 22 23 24
00112 260 C 26 2600, 8.0E3, 9.0E3, 1.0E4, 1.1E4, 1.2E4. 4
00112 270 C 25 28 29 30
00112 280 C 28 2800, 1.4E4, 1.5E4, 1.6E4, 1.7E4, 1.8E4. 5
00112 290 C 31 32 33 34 35 36
00112 300 C 30 3000, 2.4E4, 2.2E4, 2.0E4, 2.6E4, 2.8E4. 6
00112 310 C 37 38 39 40 41 42
00112 320 C 32 3200, 3.2E4, 3.4E4, 3.6E4, 3.8E4, 4.0E4. 7
00112 330 C 43 44 45 46 47 48
00112 340 C 34 3400, 4.4E4, 4.6E4, 4.8E4, 5.0E4, 5.2E4. 8
00112 350 C 49 50 51 52 53 54
00112 360 C 36 3600, 5.4E4, 5.6E4, 5.8E4, 6.0E4, 6.2E4. 9
00112 370 C 55 56 57 58 59 60
  
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00112	30°		X6.0E4,	6.0E4,	7.0E4,	7.2E4,	7.4E4,	7.6E4,	10	
00112	30°	C	01	02	03	04	05	06		
00112	40°		X7.0E4,	8.0E4,	8.2E4,	8.4E4,	8.6E4,	8.8E4,	11	
00112	40°	C	07	08	09	10	11	12		
00112	42°		X9.0E4,	9.2E4,	9.4E4,	9.6E4,	9.8E4,	1.0E5,	12	
00112	42°	C	13	14	15	16	17	18		
00112	44°		X1.0E5,	1.0E5,	1.06E5,	1.08E5,	1.1E5,	1.12E5,	13	
00112	44°	C	19	20	21	22	23	24		
00112	46°		X1.1E5,	1.1E5,	1.18E5,	1.20E5,	1.22E5,	1.24E5,	14	
00112	46°	C	25	26	27	28	29	30		
00112	48°		X1.2E5,	1.2E5,	1.3E5,	1.32E5,	1.34E5,	1.36E5,	15	
00112	48°	C	31	32	33	34	35	36		
00112	50°		X1.3E5,	1.3E5,	1.42E5,	1.44E5,	1.46E5,	1.48E5,	16	
00112	50°	C	37	38	39	40	41	42		
00112	52°		X1.5E5,	1.52E5,	1.54E5,	1.56E5,	1.58E5,	1.60E5,	17	
00112	52°	C	43	44	45	46	47	48		
00112	54°		X1.6E5,	1.6E5,	1.72E5,	1.74E5,	1.76E5,	1.78E5,	18	
00112	54°	C	49	50	51	52	53	54		
00112	56°		X1.8E5,	1.8E5,	1.96E5,	2.0E5,	2.04E5,	2.08E5,	19	
00112	56°	C	55	56	57	58	59	60		
00114	58°		DATA (ALTLST(1),INP13,INP14)/							
00114	58°	C	115	116	117	118	119	120		
00114	60°		X0.5E3,	1.15E4,	2.3E4,	4.9E4,	5.1E4,	5.3E4,		
00114	60°	C	121	122	123					
00114	62°		X0.1E4,	8.3E4,	8.9E4,					
00114	62°	C								
00114	64°		1962 - STANDARD ATMOSPHERE							
00114	64°	C								
00114	66°		PRESSURE VALUES TABULATED IN MILLIBARS							
00114	66°	C								
00114	68°		DATA (PRSLST(1),INP11,INP12)/							
00114	68°	C	1	2	3	4	5	6		
00114	70°		X1.01325E3,	9.83576E2,	9.59612E2,	9.26346E2,	8.98762E2,	8.71850E2,		
00114	70°	C	7	8	9	10	11	12		
00114	72°		X0.55596E2,	8.19988E2,	7.95014E2,	7.70001E2,	7.46917E2,	7.23771E2,		
00114	72°	C	13	14	15	16	17	18		
00114	74°		X7.01211E2,	6.57403E2,	6.16609E2,	5.77525E2,	5.40482E2,	5.02176E2,		
00114	74°	C	19	20	21	22	23	24		
00114	76°		X4.11052E2,	3.56516E2,	3.08007E2,	2.64999E2,	2.26999E2,	1.93999E2,		
00114	76°	C	25	26	27	28	29	30		
00114	78°		X1.65796E2,	1.41704E2,	1.21110E2,	1.03528E2,	8.84971E1,	7.56527E1,		
00114	78°	C	31	32	33	34	35	36		
00114	80°		X0.46748E1,	5.52930E1,	4.04749E1,	2.97174E1,	2.18837E1,	1.61619E1,		
00114	80°	C	37	38	39	40	41	42		
00114	82°		X1.19703E1,	8.89043E0,	6.63412E0,	4.98522E0,	3.77138E0,	2.87143E0,		
00114	82°	C	43	44	45	46	47	48		
00114	84°		X2.19967E0,	1.67496E0,	1.31340E0,	1.02246E0,	7.97790E-1,	6.22283E-1,		
00114	84°	C	49	50	51	52	53	54		
00114	86°		X4.84917E-1,	3.78572E-1,	2.91373E-1,	2.24606E-1,	1.72457E-1,	1.31509E-1,		
00114	86°	C	55	56	57	58	59	60		
00114	88°		X9.94067E-2,	7.44448E-2,	5.52047E-2,	4.05013E-2,	2.93758E-2,	2.1045E-2,		
00114	88°	C	61	62	63	64	65	66		
00114	90°		X1.4877E-2,	1.0366E-2,	7.1691E-3,	4.9542E-3,	3.4313E-3,	2.3746E-3,		
00114	90°	C	67	68	69	70	71	72		
00114	92°		X1.6438E-3,	1.1449E-3,	8.0683E-4,	5.7448E-4,	4.1377E-4,	3.0075E-4,		
00114	92°	C	73	74	75	76	77	78		
00114	94°		X2.2123E-4,	1.6597E-4,	1.2462E-4,	9.5225E-5,	7.0544E-5,	5.7623E-5,		
00114	94°	C	79	80	81	82	83	84		

00110	96°		X4.5919E-5	3.7137E-5	3.0426E-5	2.5217E-5	2.1210E-5	1.8139E-5
00110	97°	C	85	86	87	88	89	90
00110	98°		X1.5720E-5	1.3791E-5	1.2214E-5	1.0909E-5	9.8151E-6	8.8882E-6
00110	99°	C	91	92	93	94	95	96
00110	100°		X8.0950E-6	7.4104E-6	6.8148E-6	6.2931E-6	5.8331E-6	5.4252E-6
00110	101°	C	97	98	99	100	101	102
00110	102°		X5.0617E-6	4.7345E-6	4.4375E-6	4.1671E-6	3.9202E-6	3.6943E-6
00110	103°	C	103	104	105	106	107	108
00110	104°		X3.2932E-6	2.9475E-6	2.6479E-6	2.3851E-6	2.1536E-6	1.9491E-6
00110	105°	C	109	110	111	112	113	114
00110	106°		X1.740E-6	1.6070E-6	1.4630E-6	1.3339E-6	1.2179E-6	1.1070E-6
00110	107°	C						
00120	108°		DATA (PMSLST(1),I,NP13,NP14)/					
00120	109°	C	115	116	117	118	119	120
00120	110°		X3.3154E-2	2.0964E-2	3.4668E-2	9.03367E-1	7.04580E-1	5.49540E-1
00120	111°	C	121	122	123			
00120	112°		X8.6204E-3	5.9624E-3	1.9756E-3			
00120	113°	C						
00120	114°	C						
00120	115°	C						
00120	116°	C						
00122	117°		DATA (RMOLST(1),I,NP11,NP12)/					
00122	118°	C	1	2	3	4	5	6
00122	119°		X1.2250E0	1.1959E0	1.1673E0	1.1392E0	1.1117E0	1.0846E0
00122	120°	C	7	8	9	10	11	12
00122	121°		X1.0561E0	1.0321E0	1.0066E0	9.8151E-1	9.5695E-1	9.3287E-1
00122	122°	C	13	14	15	16	17	18
00122	123°		X9.0925E-1	8.6340E-1	8.1935E-1	7.7704E-1	7.3643E-1	6.9601E-1
00122	124°	C	19	20	21	22	23	24
00122	125°		X5.9002E-1	5.2579E-1	4.6706E-1	4.1351E-1	3.6480E-1	3.1194E-1
00122	126°	C	25	26	27	28	29	30
00122	127°		X2.6660E-1	2.2780E-1	1.9475E-1	1.6647E-1	1.4230E-1	1.2165E-1
00122	128°	C	31	32	33	34	35	36
00122	129°		X1.0400E-1	8.8910E-2	6.4510E-2	4.6930E-2	3.4257E-2	2.5076E-2
00122	130°	C	37	38	39	40	41	42
00122	131°		X1.8410E-2	1.3555E-2	9.8874E-3	7.2579E-3	5.3666E-3	3.9957E-3
00122	132°	C	43	44	45	46	47	48
00122	133°		X2.9948E-3	2.2589E-3	1.7141E-3	1.3167E-3	1.0269E-3	8.0097E-4
00122	134°	C	49	50	51	52	53	54
00122	135°		X6.3137E-4	4.9762E-4	3.9086E-4	3.0592E-4	2.3931E-4	1.8837E-4
00122	136°	C	55	56	57	58	59	60
00122	137°		X1.4713E-4	1.1399E-4	8.7535E-5	6.6593E-5	5.0151E-5	3.736E-5
00122	138°	C	61	62	63	64	65	66
00122	139°		X2.750E-5	1.999E-5	1.382E-5	9.563E-6	6.617E-6	4.579E-6
00122	140°	C	67	68	69	70	71	72
00122	141°		X3.170E-6	2.137E-6	1.459E-6	1.008E-6	7.044E-7	4.974E-7
00122	142°	C	73	74	75	76	77	78
00122	143°		X3.493E-7	2.492E-7	1.604E-7	1.132E-7	8.029E-8	5.843E-8
00122	144°	C	79	80	81	82	83	84
00122	145°		X5.321E-8	4.035E-8	3.112E-8	2.436E-8	1.844E-8	1.434E-8
00122	146°	C	85	86	87	88	89	90
00122	147°		X1.140E-8	9.224E-9	7.589E-9	6.327E-9	5.337E-9	4.549E-9
00122	148°	C	91	92	93	94	95	96
00122	149°		X3.413E-9	3.394E-9	2.965E-9	2.608E-9	2.307E-9	2.053E-9
00122	150°	C	97	98	99	100	101	102
00122	151°		X1.836E-9	1.666E-9	1.515E-9	1.382E-9	1.264E-9	1.159E-9
00122	152°	C	103	104	105	106	107	108
00122	153°		X9.71E-10	8.624E-10	7.532E-10	6.433E-10	5.450E-10	4.589E-10

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00122 154° C      109      110      111      114      113      114
00122 155°      X4.008E-10; 4.115E-10; 3.692E-10; 3.318E-10; 2.986E-10; 2.910E-10/
00122 156° C
00124 157°      DATA (MOLST(1),I=NP13,NP14)/
00124 158° C      115      116      117      118      119      120
00124 159°      X4.9576E-10; 3.3743E-10; 5.5006E-10; 1.1628E-09; 9.0690E-10; 7.1029E-10;
00124 160° C      121      122      123
00124 161°      X1.662E-05; 1.15E-05; 3.810E-06/
00124 162° C
00124 163° C
00124 164° C
00124 165° C
00126 166°      DATA (SONLST(1),I=NP11,NP12)/
00126 167° C      1      2      3      4      5      6
00126 168°      X340.294; 339.323; 338.370; 337.403; 336.435; 335.463;
00126 169° C      7      8      9      10      11      12
00126 170°      X334.489; 333.511; 332.532; 331.549; 330.563; 329.575;
00126 171° C      13      14      15      16      17      18
00126 172°      X328.583; 328.592; 327.589; 326.573; 325.545; 324.452;
00126 173° C      19      20      21      22      23
00126 174°      X312.306; 308.105; 303.848; 299.532; 295.154;
00126 175° C      24 - 32
00126 176°      X      9.295.069;
00126 177° C      33      34      35      36
00126 178°      X      206.377; 297.720; 259.056; 300.386;
00126 179° C      37      38      39      40      41      42
00126 180°      X301.709; 303.025; 306.489; 310.099; 313.665; 317.189;
00126 181° C      43      44      45      46 - 48
00126 182°      X320.672; 324.116; 327.521;      3329.799;
00126 183° C      49      50      51      52      53      54
00126 184°      X327.911; 325.492; 323.058; 320.606; 317.630; 312.628;
00126 185° C      55      56      57      58      59      60
00126 186°      X307.549; 302.387; 297.139; 291.800; 286.365; 280.83;
00126 187° C      61      62 - 114
00126 188°      X275.18;      53*269.44/
00126 189° C
00130 190°      DATA (SONLST(1),I=NP13,NP14)/
00130 191° C      115      116      117      118 - 119      120
00130 192°      X305.984; 295.069; 297.049;      2*329.799; 329.114;
00130 193° C      121 - 123
00130 194°      X      3*269.44/
00130 195° C
00130 196° C
00130 197° C
00130 198° C
00130 199° C
00132 200°      DATA (VISLST(1),I=NP11,NP12)/
00132 201° C      1      2      3      4      5      6
00132 202°      X1.7894E-5; 1.7615E-5; 1.7337E-5; 1.7658E-5; 1.7579E-5; 1.7499E-5;
00132 203° C      7      8      9      10      11      12
00132 204°      X1.7420E-5; 1.7340E-5; 1.7260E-5; 1.7180E-5; 1.7099E-5; 1.7019E-5;
00132 205° C      13      14      15      16      17      18
00132 206°      X1.6938E-5; 1.6775E-5; 1.6612E-5; 1.6448E-5; 1.6282E-5; 1.5949E-5;
00132 207° C      19      20      21      22      23
00132 208°      X1.5612E-5; 1.5271E-5; 1.4926E-5; 1.4577E-5; 1.4223E-5;
00132 209° C      24 - 32
00132 210°      X      9.14218E-5;
00132 211° C      33      34      35      36

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00132	2120	X	1.4322E-5	1.4538E-5	1.4646E-5
00132	2130	C	37	38	42
00132	2140	C	38	41	42
00132	2150	C	43	46	48
00132	2160	C	43	45	48
00132	2170	C	49	50	54
00132	2180	C	49	52	54
00132	2190	C	49	52	54
00132	2200	C	55	58	60
00132	2210	C	55	57	60
00132	2220	C	61	64	66
00132	2230	C	61	63	66
00132	2240	C	67	70	72
00132	2250	C	67	65	72
00132	2260	C	72	75	78
00132	2270	C	79	80	81
00132	2280	C	80	81	81
00132	2290	C	80	81	81
00132	2300	C	80	81	81
00132	2310	C	80	81	81
00132	2320	C	80	81	81
00132	2330	C	80	81	81
00132	2340	C	80	81	81
00132	2350	C	80	81	81
00132	2360	C	80	81	81
00132	2370	C	80	81	81
00132	2380	C	80	81	81
00132	2390	C	80	81	81
00132	2400	C	80	81	81
00132	2410	C	80	81	81
00132	2420	C	80	81	81
00132	2430	C	80	81	81
00132	2440	C	80	81	81
00132	2450	C	80	81	81
00132	2460	C	80	81	81
00132	2470	C	80	81	81
00132	2480	C	80	81	81
00132	2490	C	80	81	81
00132	2500	C	80	81	81
00132	2510	C	80	81	81
00132	2520	C	80	81	81
00132	2530	C	80	81	81
00132	2540	C	80	81	81
00132	2550	C	80	81	81
00132	2560	C	80	81	81
00132	2570	C	80	81	81
00132	2580	C	80	81	81
00132	2590	C	80	81	81
00132	2600	C	80	81	81
00132	2610	C	80	81	81
00132	2620	C	80	81	81
00132	2630	C	80	81	81
00132	2640	C	80	81	81
00132	2650	C	80	81	81
00132	2660	C	80	81	81
00132	2670	C	80	81	81
00132	2680	C	80	81	81
00132	2690	C	80	81	81
00132	2700	C	80	81	81
00132	2710	C	80	81	81
00132	2720	C	80	81	81
00132	2730	C	80	81	81
00132	2740	C	80	81	81
00132	2750	C	80	81	81
00132	2760	C	80	81	81
00132	2770	C	80	81	81
00132	2780	C	80	81	81
00132	2790	C	80	81	81
00132	2800	C	80	81	81
00132	2810	C	80	81	81
00132	2820	C	80	81	81
00132	2830	C	80	81	81
00132	2840	C	80	81	81
00132	2850	C	80	81	81
00132	2860	C	80	81	81
00132	2870	C	80	81	81
00132	2880	C	80	81	81
00132	2890	C	80	81	81
00132	2900	C	80	81	81
00132	2910	C	80	81	81
00132	2920	C	80	81	81
00132	2930	C	80	81	81
00132	2940	C	80	81	81
00132	2950	C	80	81	81
00132	2960	C	80	81	81
00132	2970	C	80	81	81
00132	2980	C	80	81	81
00132	2990	C	80	81	81
00132	3000	C	80	81	81

1966 STANDARD ATMOSPHERE FOR JULY AT 30-DEGREES NORTH LATITUDE
 PRESSURE VALUES TABULATED IN MILLIBARS

00132	2280	X	1.0121E-5	1.0229E-5	1.0337E-5
00132	2290	C	1	1	1
00132	2300	C	1	1	1
00132	2310	C	1	1	1
00132	2320	C	1	1	1
00132	2330	C	1	1	1
00132	2340	C	1	1	1
00132	2350	C	1	1	1
00132	2360	C	1	1	1
00132	2370	C	1	1	1
00132	2380	C	1	1	1
00132	2390	C	1	1	1
00132	2400	C	1	1	1
00132	2410	C	1	1	1
00132	2420	C	1	1	1
00132	2430	C	1	1	1
00132	2440	C	1	1	1
00132	2450	C	1	1	1
00132	2460	C	1	1	1
00132	2470	C	1	1	1
00132	2480	C	1	1	1
00132	2490	C	1	1	1
00132	2500	C	1	1	1
00132	2510	C	1	1	1
00132	2520	C	1	1	1
00132	2530	C	1	1	1
00132	2540	C	1	1	1
00132	2550	C	1	1	1
00132	2560	C	1	1	1
00132	2570	C	1	1	1
00132	2580	C	1	1	1
00132	2590	C	1	1	1
00132	2600	C	1	1	1
00132	2610	C	1	1	1
00132	2620	C	1	1	1
00132	2630	C	1	1	1
00132	2640	C	1	1	1
00132	2650	C	1	1	1
00132	2660	C	1	1	1
00132	2670	C	1	1	1
00132	2680	C	1	1	1
00132	2690	C	1	1	1
00132	2700	C	1	1	1
00132	2710	C	1	1	1
00132	2720	C	1	1	1
00132	2730	C	1	1	1
00132	2740	C	1	1	1
00132	2750	C	1	1	1
00132	2760	C	1	1	1
00132	2770	C	1	1	1
00132	2780	C	1	1	1
00132	2790	C	1	1	1
00132	2800	C	1	1	1
00132	2810	C	1	1	1
00132	2820	C	1	1	1
00132	2830	C	1	1	1
00132	2840	C	1	1	1
00132	2850	C	1	1	1
00132	2860	C	1	1	1
00132	2870	C	1	1	1
00132	2880	C	1	1	1
00132	2890	C	1	1	1
00132	2900	C	1	1	1
00132	2910	C	1	1	1
00132	2920	C	1	1	1
00132	2930	C	1	1	1
00132	2940	C	1	1	1
00132	2950	C	1	1	1
00132	2960	C	1	1	1
00132	2970	C	1	1	1
00132	2980	C	1	1	1
00132	2990	C	1	1	1
00132	3000	C	1	1	1

00132	2900	X	1.0430E-5	1.0538E-5	1.0646E-5
00132	2910	C	1	1	1
00132	2920	C	1	1	1
00132	2930	C	1	1	1
00132	2940	C	1	1	1
00132	2950	C	1	1	1
00132	2960	C	1	1	1
00132	2970	C	1	1	1
00132	2980	C	1	1	1
00132	2990	C	1	1	1
00132	3000	C	1	1	1

00132	3000	X	1.0753E-5	1.0861E-5	1.0969E-5
00132	3010	C	1	1	1
00132	3020	C	1	1	1
00132	3030	C	1	1	1
00132	3040	C	1	1	1
00132	3050	C	1	1	1
00132	3060	C	1	1	1
00132	3070	C	1	1	1
00132	3080	C	1	1	1
00132	3090	C	1	1	1
00132	3100	C	1	1	1

00132	3100	X	1.1096E-5	1.1204E-5	1.1312E-5
00132	3110	C	1	1	1
00132	3120	C	1	1	1
00132	3130	C	1	1	1
00132	3140	C	1	1	1
00132	3150	C	1	1	1
00132	3160	C	1	1	1
00132	3170	C	1	1	1
00132	3180	C	1	1	1
00132	3190	C	1	1	1
00132	3200	C	1	1	1

00140 270° C
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 00146 327° C

DENSITY VALUES TABULATED IN KILOGRAMS PER CUBIC METER

DATA (RMOLST(1), I=NP21, NP221/

	1	2	3	4	5	6
X1.159E0,	1.135E0,	1.112E0,	1.089E0,	1.066E0,	1.041E0,	
X1.016E0,	9.923E-1,	9.686E-1,	9.452E-1,	9.222E-1,	8.997E-1,	
X8.776E-1,	8.348E-1,	7.937E-1,	7.540E-1,	7.159E-1,	6.793E-1,	
X5.419E-1,	5.232E-1,	4.894E-1,	4.199E-1,	3.742E-1,	3.324E-1,	
X2.941E-1,	2.592E-1,	2.275E-1,	1.929E-1,	1.617E-1,	1.357E-1,	
X1.142E-1,	9.618E-2,	6.870E-2,	4.944E-2,	3.579E-2,	2.607E-2,	
X1.909E-2,	1.406E-2,	1.038E-2,	7.709E-3,	5.759E-3,	4.326E-3,	
X3.268E-3,	2.482E-3,	1.894E-3,	1.460E-3,	1.140E-3,	8.942E-4,	
X7.071E-4,	5.573E-4,	4.378E-4,	3.435E-4,	2.710E-4,	2.123E-4,	
X1.651E-4,	1.273E-4,	9.739E-5,	7.380E-5,	5.539E-5,	4.113E-5,	
X3.020E-5,	2.190E-5,	1.568E-5,	1.070E-5,	7.282E-6,	4.956E-6,	
X3.379E-6,	2.256E-6,	1.516E-6,	1.030E-6,	7.065E-7,	4.892E-7,	
X3.392E-7,	2.288E-7,	1.588E-7,	1.130E-7,	8.213E-8,	6.087E-8,	
X4.388E-8,	3.259E-8,		81 - 114 39*2.486E-8/			

DATA (RMOLST(1), I=NP23, NP241/

	115	116	117	118	119	120
X4.958E-1,	3.529E-1,	5.823E-2,	1.290E-3,	1.008E-3,	7.955E-4,	
X1.456E-5,	1.298E-5,	4.089E-6/				

SPEED OF SOUND VALUES TABULATED IN METERS PER SECOND

DATA (SMOLST(1), I=NP21, NP221/

	1	2	3	4	5	6
X349.9,	378.8,	347.3,	346.0,	344.7,	343.8,	
X342.9,	342.0,	341.1,	340.3,	339.4,	338.5,	
X337.7,	335.9,	334.2,	332.5,	330.7,	327.3,	
X322.9,	318.5,	314.0,	309.5,	304.9,	303.3,	
X295.6,	290.9,	285.0,	285.7,	287.2,	288.7,	
X290.2,	291.7,	294.6,	297.3,	299.9,	302.6,	
X305.2,	307.8,	310.8,	313.9,	316.9,	319.9,	

00140	320°	C	43	44	45	46 - 47	48
00140	329°		X322+0.	325+0.	327+0.	2+330+7.	330+1.
00140	330°	C	49	50	51	52	53
00140	331°		X327+7.	325+3.	322+0.	320+0.	315+3.
00140	332°	C	55	56	57	58	59
00140	333°		X305+7.	300+7.	295+7.	290+0.	285+5.
00140	334°	C	61	62	63	64 - 67	
00140	335°		X274+0.	269+4.	2A3+0.		2+263+3.
00140	336°	C	68	69	70	71	72
00140	337°		X	266+2.	2A9+7.	273+1.	270+5.
00140	338°	C	73	74	75	76	77
00140	339°		X284+2.	295+5.	3+6+7.	316+9.	327+1.
00140	340°	C	79	80		81 - 114	336+9.
00140	341°		X355+2.	373+1.		34+390+17	
00140	342°	C					
00150	343°		DATA (SOMLST(1),1+NP23,1+P241/				
00150	344°	C	115	116	117	118 - 119	120
00150	345°		X310+3.	302+6.	295+9.	2+330+7.	328+9.
00150	346°	C	121	122 - 123			
00150	347°		X266+6.	2+263+3/			
00150	348°	C					
00150	349°	C					
00150	350°	C					
00150	351°	C					
00150	352°	C					

VISCOSITY COEFFICIENT
VALUES TABULATED IN KILOGRAMS PER METER PER SECOND

00152	353°		DATA (VISLST(1),1+NP21,1+P221/				
00152	354°	C	1	2	3	4	5
00152	355°		X1+060E-5.	1+057E-5.	1+046E-5.	1+038E-5.	1+025E-5.
00152	356°	C	7	8	9	10	11
00152	357°		X1+011E-5.	1+003E-5.	1+796E-5.	1+789E-5.	1+782E-5.
00152	358°	C	13	14	15	16	17
00152	359°		X1+768E-5.	1+754E-5.	1+739E-5.	1+725E-5.	1+711E-5.
00152	360°	C	19	20	21	22	23
00152	361°		X1+648E-5.	1+612E-5.	1+575E-5.	1+539E-5.	1+501E-5.
00152	362°	C	25	26	27	28	29
00152	363°		X1+424E-5.	1+388E-5.	1+349E-5.	1+306E-5.	1+258E-5.
00152	364°	C	31	32	33	34	35
00152	365°		X1+382E-5.	1+335E-5.	1+291E-5.	1+239E-5.	1+196E-5.
00152	366°	C	37	38	39	40	41
00152	367°		X1+504E-5.	1+525E-5.	1+549E-5.	1+574E-5.	1+599E-5.
00152	368°	C	43	44	45	46 - 47	48
00152	369°		X1+647E-5.	1+671E-5.	1+694E-5.	2+1+711E-5.	1+706E-5.
00152	370°	C	49	50	51	52	53
00152	371°		X1+687E-5.	1+677E-5.	1+647E-5.	1+624E-5.	1+585E-5.
00152	372°	C	55	56	57	58	59
00152	373°		X1+507E-5.	1+467E-5.	1+427E-5.	1+386E-5.	1+344E-5.
00152	374°	C	61	62	63	64 - 67	
00152	375°		X1+259E-5.	1+216E-5.	1+172E-5.	4+1+168E-5.	
00152	376°	C	68	69	70	71	72
00152	377°		X	1+190E-5.	1+218E-5.	1+245E-5.	1+273E-5.
00152	378°	C	73	74	75	76	77
00152	379°		X1+335E-5.	1+425E-5.	1+513E-5.	1+599E-5.	1+681E-5.
00152	380°	C	79	80		81 - 114	1+762E-5.
00152	381°		X1+912E-5.	2+057E-5.		34+2+197E-5/	
00152	382°	C					
00154	383°		DATA (VISLS (1),1+NP23,1+P241/				
00154	384°	C	115	116	117	118 - 119	120
00154	385°		X1+593E-5.	1+403E-5.	1+429E-5.	2+1+711E-5.	1+696E-5.

00154 306° C
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 11-199E-5 2*1-168E-5/

1966 STANDARD ATMOSPHERE FOR
 JANUARY AT 30-DEGREES NORTH LATITUDE

PRESSURE VALUES TABULATED IN MILLIBARS

DATA (PRSLST(1),1=NP31,WP321/

	1	2	3	4	5	6
11-021E3	9-912E2	9-622E2	9-370E2	9-065E2	8-798E2	
80-530E2	8-206E2	8-038E2	7-798E2	7-569E2	7-335E2	
17-112E2	6-682E2	6-274E2	5-886E2	5-517E2	4-837E2	
17-226E2	3-679E2	3-191E2	2-757E2	2-372E2	2-032E2	
11-739E2	1-478E2	1-257E2	1-067E2	9-090E1	7-650E1	
10-479E1	5-799E1	3-984E1	2-907E1	2-139E1	1-575E1	
11-169E1	8-723E0	6-544E0	4-939E0	3-748E0	2-860E0	
12-199E0	1-691E0	1-310E0	1-019E0	7-941E-1	6-187E-1	
19-008E-1	3-723E-1	2-872E-1	2-207E-1	1-687E-1	1-281E-1	
19-659E-2	7-231E-2	5-372E-2	3-959E-2	2-893E-2	2-095E-2	
11-503E-2	1-068E-2	7-538E-3	5-323E-3	3-760E-3	2-657E-3	
11-879E-3	1-341E-3	9-683E-4	7-066E-4	5-209E-4	3-876E-4	
12-910E-4	2-210E-4	1-699E-4	1-322E-4	1-039E-4	8-239E-5	
10-606E-5	8-359E-5		81 - 114			

DATA (PRSLST(1),1=NP33,WP341/

	115	116	117	118	119	120
13-428E2	2-196E2	3-901E1	8-997E-1	7-010E-1	5-457E-1	
10-970E-3	6-334E-3	2-233E-3/				

DENSITY VALUES TABULATED IN KILOGRAMS PER CUBIC METER

DATA (NMOLST(1),1=NP31,WP321/

	1	2	3	4	5	6
11-233E0	1-200E0	1-168E0	1-137E0	1-107E0	1-078E0	
11-049E0	1-021E0	9-934E-1	9-695E-1	9-461E-1	9-231E-1	
17-005E-1	8-565E-1	8-142E-1	7-733E-1	7-340E-1	6-599E-1	
15-916E-1	5-248E-1	4-713E-1	4-187E-1	3-707E-1	3-270E-1	

00162	444°		X2.020E-1.	2.439E-1.	2.101E-1.	1.805E-1.	1.549E-1.	1.312E-1.
00162	445°	C	31	32	33	34	35	36
00162	446°		X1.099E-1.	9.213E-2.	6.520E-2.	4.669E-2.	3.065E-2.	2.440E-2.
00162	447°	C	37	38	40	40	41	42
00162	448°		X1.780E-2.	1.306E-2.	9.603E-3.	7.105E-3.	5.289E-3.	3.960E-3.
00162	449°	C	43	44	45	46	47	48
00162	450°		X2.981E-3.	2.257E-3.	1.717E-3.	1.319E-3.	1.028E-3.	8.038E-4.
00162	451°	C	49	50	51	52	53	54
00162	452°		X6.340E-4.	4.983E-4.	3.903E-4.	3.051E-4.	2.3A9E-4.	1.860E-4.
00162	453°	C	55	56	57	58	59	60
00162	454°		X1.739E-4.	1.136E-4.	8.441E-5.	6.396E-5.	4.809E-5.	3.586E-5.
00162	455°	C	61	62	63	64	65	66
00162	456°		X2.651E-5.	1.942E-5.	1.374E-5.	9.702E-6.	6.853E-6.	4.842E-6.
00162	457°	C	67	68	69	70	71	72
00162	458°		X3.384E-6.	2.335E-6.	1.630E-6.	1.152E-6.	8.231E-7.	5.942E-7.
00162	459°	C	73	74	75	76	77	78
00162	460°		X4.322E-7.	3.133E-7.	2.305E-7.	1.718E-7.	1.296E-7.	9.887E-8.
00162	461°	C	79	80		81 - 114		
00162	462°		X7.509E-8.	5.780E-8.		3494.509E-8/		
00162	463°	C						
00164	464°		DATA (RMOLST(1),1=NP33,4=NP34)/					
00164	465°	C	115	116	117	118	119	120
00164	466°		X4.994E-1.	3.483E-1.	5.512E-2.	1.165E-3.	9.073E-4.	7.142E-4.
00164	467°	C	121	122	123			
00164	468°		X1.635E-5.	1.154E-5.	8.070E-6/			
00164	469°	C						
00164	470°	C						
00164	471°	C						
00164	472°	C						
00164	473°		DATA (SONLST(1),1=NP31,2=NP32)/					
00166	474°	C	1	2	3	4	5	6
00166	475°		X340.5.	340.0.	339.5.	339.1.	338.6.	338.1.
00166	476°	C	7	8	9	10	11	12
00166	477°		X337.6.	337.1.	336.6.	336.0.	335.6.	335.5.
00166	478°	C	13	14	15	16	17	18
00166	479°		X332.5.	330.5.	328.5.	326.4.	324.4.	320.3.
00166	480°	C	19	20	21	22	23	24
00166	481°		X316.2.	312.1.	307.9.	303.6.	299.3.	294.9.
00166	482°	C	25	26	27	28	29	30
00166	483°		X293.0.	291.3.	289.5.	287.7.	285.9.	285.7.
00166	484°	C	31	32	33	34	35	36
00166	485°		X287.3.	289.1.	282.5.	285.2.	297.9.	300.6.
00166	486°	C	37	38	39	40	41	42
00166	487°		X303.2.	305.9.	308.9.	311.9.	315.0.	318.0.
00166	488°	C	43	44	45		46 - 47	48
00166	489°		X321.0.	323.9.	326.8.		20328.9.	328.3.
00166	490°	C	49	50	51	52	53	54
00166	491°		X325.8.	323.4.	321.0.	318.3.	314.9.	310.5.
00166	492°	C	55	56	57	58	59	60
00166	493°		X306.5.	302.5.	298.5.	294.4.	290.2.	286.0.
00166	494°	C	61	62		63 - 64		
00166	495°		X281.7.	277.4.		40277.2.		
00166	496°	C	67	68	69	70	71	72
00166	497°		X278.7.	283.6.	288.4.	293.0.	297.7.	302.2.
00166	498°	C	73	74	75	76	77	78
00166	499°		X307.0.	314.3.	321.3.	328.2.	335.0.	341.6.
00166	500°	C	79	80		81 - 114		
00166	501°		X351.0.	340.3.		340369.3/		

ORIGINAL PAGE IS
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00170 502° C
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DATA (SONLST(1),1,4NP33,4NP34)/
 115 116 117 118 - 119 120
 2308.9, 297.1, 293.9, 20328.9, 327.1
 121 - 123
 30277.27

VISCOSITY COEFFICIENT
 VALUES TABULATED IN KILOGRAMS PER METER PER SECOND

DATA (VISLST(1),1,4NP33,4NP32)/
 1 2 3 4 5 6
 11.791E-5, 1.787E-5, 1.783E-5, 1.779E-5, 1.775E-5, 1.771E-5,
 7 8 9 10 11 12
 11.767E-5, 1.763E-5, 1.759E-5, 1.755E-5, 1.751E-5, 1.739E-5,
 13 14 15 16 17 18
 11.726E-5, 1.722E-5, 1.693E-5, 1.676E-5, 1.660E-5, 1.626E-5,
 19 20 21 22 23 24
 11.593E-5, 1.559E-5, 1.525E-5, 1.491E-5, 1.456E-5, 1.420E-5,
 25 26 27 28 29 30
 11.405E-5, 1.391E-5, 1.376E-5, 1.362E-5, 1.347E-5, 1.346E-5,
 31 32 33 34 35 36
 11.359E-5, 1.337E-5, 1.401E-5, 1.423E-5, 1.445E-5, 1.466E-5,
 37 38 39 40 41 42
 11.488E-5, 1.509E-5, 1.533E-5, 1.558E-5, 1.583E-5, 1.607E-5,
 43 44 45 46 - 47 48
 11.632E-5, 1.656E-5, 1.679E-5, 2.1.696E-5, 1.691E-5,
 49 50 51 52 53 54
 11.671E-5, 1.652E-5, 1.632E-5, 1.610E-5, 1.578E-5, 1.547E-5,
 55 56 57 58 59 60
 11.514E-5, 1.492E-5, 1.449E-5, 1.416E-5, 1.383E-5, 1.349E-5,
 61 62 63 - 66
 11.319E-5, 1.280E-5, 4.1.278E-5,
 67 68 69 70 71 72
 11.290E-5, 1.329E-5, 1.368E-5, 1.405E-5, 1.443E-5, 1.479E-5,
 73 74 75 76 77 78
 11.518E-5, 1.577E-5, 1.634E-5, 1.691E-5, 1.746E-5, 1.800E-5,
 79 80 81 - 114
 11.877E-5, 1.953E-5, 3.92.027E-5/

DATA (VISLST(1),1,4NP33,4NP34)/
 115 116 117 118 - 119 120
 11.542E-5, 1.436E-5, 1.412E-5, 2.1.696E-5, 1.681E-5,
 121 - 123
 3.1.278E-5/

1966 STANDARD ATMOSPHERE FOR JULY AT 60-DEGREES NORTH LATITUDE

PRESSURE VALUES TABULATED IN MILLIBARS

DATA (PRSLST(1),1,4NP41,4NP42)/
 1 2 3 4 5 6
 11.010E2, 9.834E2, 9.516E2, 9.234E2, 8.960E2, 8.692E2,
 7 8 9 10 11 12
 8.432E2, 8.177E2, 7.930E2, 7.688E2, 7.453E2, 7.224E2,
 13 14 15 16 17 18

00176	560°		X7.000E2:	6.571E2:	6.164E2:	5.779E2:	5.414E2:	4.740E2:
00176	561°	C	19	25	21	22	23	24
00176	562°		X4.134E2:	3.592E2:	3.108E2:	2.677E2:	2.301E2:	1.978E2:
00176	563°	C	25	26	27	28	29	30
00176	564°		X1.700E2:	1.401E2:	1.256E2:	1.080E2:	9.285E1:	7.983E1:
00176	565°	C	31	32	33	34	35	36
00176	566°		X6.064E1:	5.902E1:	4.364E1:	3.229E1:	2.398E1:	1.788E1:
00176	567°	C	37	38	39	40	41	42
00176	568°		X1.338E1:	1.009E1:	7.593E0:	5.775E0:	4.421E0:	3.406E0:
00176	569°	C	43	44	45	46	47	48
00176	570°		X2.040E0:	2.057E0:	1.807E0:	1.259E0:	9.872E-1:	7.742E-1:
00176	571°	C	49	50	51	52	53	54
00176	572°		X6.072E-1:	4.751E-1:	3.704E-1:	2.877E-1:	2.218E-1:	1.694E-1:
00176	573°	C	55	56	57	58	59	60
00176	574°		X1.281E-1:	9.578E-2:	7.075E-2:	5.160E-2:	3.710E-2:	2.627E-2:
00176	575°	C	61	62	63	64	65	66
00176	576°		X1.829E-2:	1.249E-2:	8.360E-3:	5.530E-3:	3.447E-3:	2.430E-3:
00176	577°	C	67	68	69	70	71	72
00176	578°		X1.610E-3:	1.075E-3:	7.297E-4:	5.027E-4:	3.5.2E-4:	2.485E-4:
00176	579°	C	73	74	75	76	77	78
00176	580°		X1.782E-4:	1.310E-4:	9.889E-5:	7.633E-5:	6.004E-5:	4.801E-5:
00176	581°	C	79	80	81 - 114			
00176	582°		X3.903E-5:	3.224E-5:		34*2.700E-5/		
00176	583°	C						
00200	584°		DATA (PRSLST(I),I=NP43, NP44)/					
00200	585°	C	115	116	117	118	119	120
00200	586°		X3.343E2:	2.133E2:	3.753E1:	1.115E0:	8.742E-1:	6.857E-1:
00200	587°	C	121	122	123			
00200	588°		X1.025E-2:	6.803E-3:	1.978E-3/			
00200	589°	C						
00200	590°	C						
00200	591°	C						
00200	592°	C						
00200	593°	C						
00200	594°		DATA (KHOLST(I),I=NP41, NP42)/					
00200	595°	C	1	2	3	4	5	6
00200	596°		X1.220E0:	1.190E0:	1.161E0:	1.132E0:	1.104E0:	1.077E0:
00200	597°	C	7	8	9	10	11	12
00200	598°		X1.050E0:	1.023E0:	9.971E-1:	9.716E-1:	9.467E-1:	9.223E-1:
00200	599°	C	13	14	15	16	17	18
00200	600°		X8.984E-1:	8.521E-1:	8.077E-1:	7.651E-1:	7.244E-1:	6.851E-1:
00200	601°	C	19	20	21	22	23	24
00200	602°		X5.849E-1:	5.231E-1:	4.663E-1:	4.142E-1:	3.660E-1:	3.200E-1:
00200	603°	C	25	26	27	28	29	30
00200	604°		X2.631E-1:	2.261E-1:	1.944E-1:	1.671E-1:	1.437E-1:	1.235E-1:
00200	605°	C	31	32	33	34	35	36
00200	606°		X1.062E-1:	9.132E-2:	8.753E-2:	8.965E-2:	8.639E-2:	8.278E-2:
00200	607°	C	37	38	39	40	41	42
00200	608°		X1.979E-2:	1.469E-2:	1.083E-2:	8.091E-3:	6.013E-3:	4.528E-3:
00200	609°	C	43	44	45	46	47	48
00200	610°		X3.431E-3:	2.600E-3:	2.039E-3:	1.584E-3:	1.241E-3:	9.732E-4:
00200	611°	C	49	50	51	52	53	54
00200	612°		X7.867E-4:	6.085E-4:	4.814E-4:	3.815E-4:	3.049E-4:	2.416E-4:
00200	613°	C	55	56	57	58	59	60
00200	614°		X1.898E-4:	1.477E-4:	1.138E-4:	8.666E-5:	6.521E-5:	4.842E-5:
00200	615°	C	61	62	63	64	65	66
00200	616°		X3.543E-5:	2.501E-5:	1.800E-5:	1.192E-5:	7.998E-6:	5.233E-6:
00200	617°	C	67	68	69	70	71	72
00200	617°		X3.464E-6:	2.729E-6:	1.554E-6:	9.640E-7:	6.491E-7:	4.434E-7:

DENSITY VALUES TABULATED IN KILOGRAMS PER CUBIC METER

DATA (KHOLST(I),I=NP41, NP42)/

1	2	3	4	5	6
X1.220E0:	1.190E0:	1.161E0:	1.132E0:	1.104E0:	1.077E0:
7	8	9	10	11	12
X1.050E0:	1.023E0:	9.971E-1:	9.716E-1:	9.467E-1:	9.223E-1:
13	14	15	16	17	18
X8.984E-1:	8.521E-1:	8.077E-1:	7.651E-1:	7.244E-1:	6.851E-1:
19	20	21	22	23	24
X5.849E-1:	5.231E-1:	4.663E-1:	4.142E-1:	3.660E-1:	3.200E-1:
25	26	27	28	29	30
X2.631E-1:	2.261E-1:	1.944E-1:	1.671E-1:	1.437E-1:	1.235E-1:
31	32	33	34	35	36
X1.062E-1:	9.132E-2:	8.753E-2:	8.965E-2:	8.639E-2:	8.278E-2:
37	38	39	40	41	42
X1.979E-2:	1.469E-2:	1.083E-2:	8.091E-3:	6.013E-3:	4.528E-3:
43	44	45	46	47	48
X3.431E-3:	2.600E-3:	2.039E-3:	1.584E-3:	1.241E-3:	9.732E-4:
49	50	51	52	53	54
X7.867E-4:	6.085E-4:	4.814E-4:	3.815E-4:	3.049E-4:	2.416E-4:
55	56	57	58	59	60
X1.898E-4:	1.477E-4:	1.138E-4:	8.666E-5:	6.521E-5:	4.842E-5:
61	62	63	64	65	66
X3.543E-5:	2.501E-5:	1.800E-5:	1.192E-5:	7.998E-6:	5.233E-6:
67	68	69	70	71	72
X3.464E-6:	2.729E-6:	1.554E-6:	9.640E-7:	6.491E-7:	4.434E-7:

ORIGINAL PAGE IS
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00202 018° C      73      74      75      76      77      78
00202 019° C      X3.019E-7, 2.023E-7, 1.703E-7, 1.001E-7, 7.324E-8, 5.901E-8,
00202 020° C      79      80      81 - 119
00202 021° C      X9.091E-8, 3.132E-8, 34*2.994E-8/
00202 022° C
00204 023° C      DATA (MHO LST(1),I=NP43,4P44)/
00204 024° C      115      116      117      118      119      120
00204 025° C      X4.941E-1, 3.301E-1, 5.407E-2, 1.701E-3, 1.099E-3, 8.619E-4,
00204 026° C      121      122      123
00204 027° C      X2.150E-5, 1.465E-5, 4.263E-6/
00204 028° C
00204 029° C
00204 030° C
00204 031° C
00204 032° C
00206 033° C      DATA (SONLST(1),I=NP41,4P42)/
00206 034° C      1      2      3      4      5      6
00206 035° C      X340.5, 339.8, 338.8, 337.9, 337.0, 336.2,
00206 036° C      7      8      9      10      11      12
00206 037° C      X335.4, 334.5, 333.7, 332.8, 332.0, 331.1,
00206 038° C      13      14      15      16      17      18
00206 039° C      X330.3, 328.6, 326.9, 325.2, 323.5, 319.0,
00206 040° C      19      20      21
00206 041° C      X314.8, 310.0, 307.5,
00206 042° C      R      22 - 33
00206 043° C      X      12*300.0,
00206 044° C      R      34      35      36
00206 045° C      X      301.7, 303.7, 305.7,
00206 046° C      37      38      39      40      41      42
00206 047° C      X307.8, 309.6, 313.3, 317.1, 320.8, 324.5,
00206 048° C      43      44      45      46      47 - 48
00206 049° C      X328.2, 330.9, 332.2, 333.5, 2*333.7,
00206 050° C      49      50      51      52      53      54
00206 051° C      X333.0, 330.6, 328.2, 324.9, 319.2, 313.3,
00206 052° C      55      56      57      58      59      60
00206 053° C      X307.3, 301.3, 295.0, 288.7, 282.2, 275.6,
00206 054° C      61      62      63 - 67
00206 055° C      X268.8, 261.9, 5*255.0,
00206 056° C      R      68      69      70      71      72
00206 057° C      X      259.9, 245.1, 270.2, 275.2, 280.1,
00206 058° C      73      74      75      76      77      78
00206 059° C      X287.5, 301.1, 314.2, 326.7, 338.8, 350.8,
00206 060° C      79      80      81 - 119
00206 061° C      X365.5, 379.6, 34*393.2/
00210 062° C      DATA (SONLST(1),I=NP43,4P44)/
00210 063° C      115      116 - 117      118 - 120
00210 064° C      X307.8, 2*300.0, 3*333.7,
00210 065° C      121      122 - 123
00210 066° C      X258.3, 2*255.0/
00210 067° C
00210 068° C
00210 069° C
00210 070° C
00210 071° C
00212 072° C      DATA (VISLST(1),I=NP41,4P42)/
00212 073° C      1      2      3      4      5      6
00212 074° C      X1.791E-5, 1.704E-5, 1.777E-5, 1.770E-5, 1.743E-5, 1.756E-5,
00212 075° C      7      8      9      10      11      12

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00216	7340	C	X6.709E-2,	5.271E-2,	4.017E-2,	3.051E-2,	2.396E-2,	1.735E-2,
00216	7350		61	62	63	64	65	66
00216	7360	C	X1.278E-2,	9.661E-3,	7.152E-3,	5.263E-3,	3.851E-3,	2.800E-3,
00216	7370		67	68	69	70	71	72
00216	7380	C	X2.022E-3,	1.460E-3,	1.061E-3,	7.762E-4,	5.715E-4,	4.234E-4,
00216	7390		73	74	75	76	77	78
00216	7400	C	X3.156E-4,	2.375E-4,	1.807E-4,	1.389E-4,	1.078E-4,	8.435E-5,
00216	7410		79	80	81 - 114			
00216	7420	C	X6.691E-5,	5.391E-5,		3494.402E-5/		
00216	7430							
00220	7440		DATA (P)SLST(1), (M)P53, (N)P54/					
00220	7450	C	115	116	117	118	119	120
00220	7460		X3.060E2,	1.911E2,	3.109E1,	6.516E-1,	5.029E-1,	3.879E-1,
00220	7470	C	121	122	123			
00220	7480		X8.310E-3,	6.199E-3,	2.381E-3/			
00220	7490	C						
00220	7500	C						
00220	7510	C	DENSITY VALUES TABULATED IN KILOGRAMS PER CUBIC METER					
00220	7520	C						
00222	7530		DATA (R)HOLST(1), (M)P51, (N)P52/					
00222	7540	C	1	2	3	4	5	6
00222	7550		X1.372E0,	1.325E0,	1.279E0,	1.235E0,	1.193E0,	1.158E0,
00222	7560	C	7	8	9	10	11	12
00222	7570		X1.123E0,	1.090E0,	1.058E0,	1.026E0,	9.955E-1,	9.656E-1,
00222	7580	C	13	14	15	16	17	18
00222	7590		X9.366E-1,	8.808E-1,	8.339E-1,	7.888E-1,	7.457E-1,	6.646E-1,
00222	7600	C	19	20	21	22	23	24
00222	7610		X6.909E-1,	5.226E-1,	4.539E-1,	3.879E-1,	3.315E-1,	2.834E-1,
00222	7620	C	25	26	27	28	29	30
00222	7630		X2.422E-1,	2.071E-1,	1.770E-1,	1.517E-1,	1.300E-1,	1.113E-1,
00222	7640	C	31	32	33	34	35	36
00222	7650		X9.530E-2,	8.156E-2,	5.966E-2,	4.357E-2,	3.157E-2,	2.275E-2,
00222	7660	C	37	38	39	40	41	42
00222	7670		X1.845E-2,	1.193E-2,	8.676E-3,	6.264E-3,	4.551E-3,	3.330E-3,
00222	7680	C	43	44	45	46	47	48
00222	7690		X2.453E-3,	1.819E-3,	1.357E-3,	1.010E-3,	7.682E-4,	5.911E-4,
00222	7700	C	49	50	51	52	53	54
00222	7710		X4.564E-4,	3.559E-4,	2.774E-4,	2.150E-4,	1.651E-4,	1.266E-4,
00222	7720	C	55	56	57	58	59	60
00222	7730		X9.708E-5,	7.435E-5,	5.701E-5,	4.400E-5,	3.302E-5,	2.599E-5,
00222	7740	C	61	62	63	64	65	66
00222	7750		X1.981E-5,	1.503E-5,	1.134E-5,	8.516E-6,	6.357E-6,	4.717E-6,
00222	7760	C	67	68	69	70	71	72
00222	7770		X3.480E-6,	2.467E-6,	1.757E-6,	1.260E-6,	9.093E-7,	6.607E-7,
00222	7780	C	73	74	75	76	77	78
00222	7790		X4.805E-7,	3.479E-7,	2.550E-7,	1.891E-7,	1.417E-7,	1.047E-7,
00222	7800	C	79	80	81 - 114			
00222	7810		X7.890E-8,	5.950E-8,		3494.567E-8/		
00222	7820	C						
00224	7830		DATA (R)HOLST(1), (M)P53, (N)P54/					
00224	7840	C	115	116	117	118	119	120
00224	7850		X4.909E-1,	3.065E-1,	5.100E-2,	8.837E-3,	6.728E-3,	5.194E-3,
00224	7860	C	121	122	123			
00224	7870		X1.307E-5,	9.835E-6,	4.055E-6/			
00224	7880	C						
00224	7890	C						
00224	7900	C						
00224	7910	C	SPEED OF SOUND VALUES TABULATED IN METERS PER SECOND					

00224	792°		DATA (SONLST(1),I=NP51,NP52)/					
00224	793°	C	1	2	3	4	5	6
00224	794°		X321.4,	321.9,	322.2,	322.5,	322.8,	322.3,
00224	795°	C	7	8	9	10	11	12
00224	796°		X321.8,	321.3,	320.8,	320.3,	319.8,	319.3,
00224	797°	C	13	14	15	16	17	18
00224	798°		X318.8,	317.7,	315.6,	313.4,	311.2,	308.8,
00224	799°	C	19	20			21 - 27	
00224	800°		X302.3,	297.7,			7*295.4,	
00224	801°	C				28	29	30
00224	802°		X			295.0,	294.6,	294.2,
00224	803°	C	31	32	33	34	35	36
00224	804°		X293.8,	293.4,	292.6,	291.7,	291.9,	293.3,
00224	805°	C	37	38	39	40	41	42
00224	806°		X294.7,	296.0,	297.4,	300.5,	303.8,	307.1,
00224	807°	C	43	44	45	46	47	48
00224	808°		X310.3,	313.5,	316.6,	319.7,	322.8,	323.3,
00224	809°	C	49	50	51	52	53	54
00224	810°		X323.3,	321.6,	319.3,	317.5,	316.9,	316.3,
00224	811°	C	55	56	57	58	59	60
00224	812°		X315.7,	315.0,	314.1,	311.3,	308.5,	305.7,
00224	813°	C	61	62	63	64	65	66
00224	814°		X302.8,	300.0,	297.1,	294.2,	291.2,	288.2,
00224	815°	C	67	68	69	70	71	72
00224	816°		X285.2,	287.8,	290.8,	293.7,	296.6,	299.5,
00224	817°	C	73	74	75	76	77	78
00224	818°		X303.2,	309.2,	315.0,	320.7,	325.4,	332.6,
00224	819°	C	79	80		81 - 114		
00224	820°		X344.6,	356.1,		34*367.3/		
00224	821°	C						
00230	822°		DATA (SONLST(1),I=NP53,NP54)/					
00230	823°	C	115 - 116		117	118		119 - 120
00230	824°		X	2*295.4,	292.1,	321.3,		2*323.3,
00230	825°	C	121	122	123			
00230	826°		X298.5,	295.6,	286.7/			
00230	827°	C						
00230	828°	C						
00230	829°	C						
00230	830°	C						
00230	831°	C						
00232	832°		DATA (VISLST(1),I=NP51,NP52)/					
00232	833°	C	1	2	3	4	5	6
00232	834°		X1.638E-5,	1.639E-5,	1.642E-5,	1.644E-5,	1.647E-5,	1.643E-5,
00232	835°	C	7	8	9	10	11	12
00232	836°		X1.639E-5,	1.638E-5,	1.630E-5,	1.626E-5,	1.622E-5,	1.618E-5,
00232	837°	C	13	14	15	16	17	18
00232	838°		X1.619E-5,	1.605E-5,	1.588E-5,	1.570E-5,	1.552E-5,	1.516E-5,
00232	839°	C	19	20			21 - 27	
00232	840°		X1.480E-5,	1.443E-5,			7*1.424E-5,	
00232	841°	C				28	29	30
00232	842°		X			1.421E-5,	1.418E-5,	1.415E-5,
00232	843°	C	31	32	33	34	35	36
00232	844°		X1.411E-5,	1.408E-5,	1.401E-5,	1.395E-5,	1.396E-5,	1.407E-5,
00232	845°	C	37	38	39	40	41	42
00232	846°		X1.418E-5,	1.429E-5,	1.440E-5,	1.466E-5,	1.492E-5,	1.519E-5,
00232	847°	C	43	44	45	46	47	48
00232	848°		X1.545E-5,	1.571E-5,	1.596E-5,	1.622E-5,	1.647E-5,	1.651E-5,
00232	849°	C	49	50	51	52	53	54

VISCOSITY COEFFICIENT
 VALUES TABULATED IN KILOGRAMS PER METER PER SECOND

00232	850°		X1.031E-5,	1.637E-5,	1.618E-5,	1.604E-5,	1.599E-5,	1.594E-5,
00232	850°	C	55	56	57	58	59	60
00232	852°		X1.589E-5,	1.583E-5,	1.575E-5,	1.553E-5,	1.530E-5,	1.507E-5,
00232	853°	C	61	62	63	64	65	66
00232	854°		X1.484E-5,	1.461E-5,	1.438E-5,	1.414E-5,	1.391E-5,	1.367E-5,
00232	855°	C	67	68	69	70	71	72
00232	856°		X1.343E-5,	1.363E-5,	1.387E-5,	1.411E-5,	1.434E-5,	1.458E-5,
00232	857°	C	73	74	75	76	77	78
00232	858°		X1.487E-5,	1.536E-5,	1.583E-5,	1.630E-5,	1.676E-5,	1.727E-5,
00232	859°	C	79	80	81 - 114			
00232	860°		X1.024E-5,	1.919E-5,	3432.011E-5/			
00232	861°	C						
00234	862°		DATA (V1SLST11), I=NP53, W=PS41/					
00234	863°	C	115 - 116	117	118	119 - 120		
00234	864°		X 2.01424E-5,	1.398E-5,	1.634E-5,	2.91.651E-5,		
00234	865°	C	121	122	123			
00234	866°		X1.450E-5,	1.426E-5,	1.355E-5/			
00234	867°	C						
00234	868°	C						
00234	869°	C						
00234	870°	C						
00234	871°	C						
00234	872°	C						
00236	873°		DATA (PRSLST11), I=NP61, W=P62/					
00236	874°	C	1	2	3	4	5	
00236	875°		X1.0170147E+3.9.0829373E+2.9.0022651E+2.9.3280864E+2.9.0603418E+2.					
00236	876°	C	6	7	8	9	10	
00236	877°		X8.7989596E+2.8.5438573E+2.8.2949430E+2.8.0521168E+2.7.8152728E+2.					
00236	878°	C	11	12	13	14	15	
00236	879°		X7.58433002E+2.7.3590840E+2.7.1395065E+2.6.7167869E+2.6.3151745E+2.					
00236	880°	C	16	17	18	19	20	
00236	881°		X5.9337050E+2.5.5714348E+2.4.9008912E+2.4.2967959E+2.3.7532040E+2.					
00236	882°	C	21	22	23	24	25	
00236	883°		X3.2649869E+2.2.8277555E+2.2.4373144E+2.2.0909281E+2.1.7861068E+2.					
00236	884°	C	26	27	28	29	30	
00236	885°		X1.5199024E+2.1.2852856E+2.1.0911341E+2.9.2252642E+1.7.8097365E+1.					
00236	886°	C	31	32	33	34	35	
00236	887°		X6.6260092E+1.5.6315652E+1.4.0899191E+1.2.9918759E+1.2.2038159E+1.					
00236	888°	C	36	37	38	39	40	
00236	889°		X1.6327363E+1.1.2146273E+1.9.0905300E+0.6.8429914E+0.5.1807184E+0.					
00236	890°	C	41	42	43	44	45	
00236	891°		X3.9447995E+0.3.0209180E+0.2.3262411E+0.1.6004513E+0.1.399781E+0.					
00236	892°	C	46	47	48	49	50	
00236	893°		X1.0910568E+0.8.5180215E-1.6.6393197E-1.5.1553130E-1.3.9852059E-1.					
00236	894°	C	51	52	53	54	55	
00236	895°		X3.0651143E-1.2.3442082E-1.1.7818466E-1.1.3454170E-1.1.0086976E-1.					
00236	896°	C	56	57	58	59	60	
00236	897°		X7.5059128E-2.5.5414297E-2.4.0576003E-2.2.9458748E-2.2.1200623E-2.					
00236	898°	C	61	62	63	64	65	
00236	899°		X1.5119031E-2.1.0688305E-2.7.4793850E-3.5.1878215E-3.3.5914714E-3.					
00236	900°	C	66	67	68	69	70	
00236	901°		X2.4869045E-3.1.7224435E-3.1.2003841E-3.8.4635721E-4.6.0330423E-4.					
00236	902°	C	71	72	73	74	75	
00236	903°		X4.3449711E-4.3.1597170E-4.2.3253935E-4.1.7351148E-4.1.3111039E-4.					
00236	904°	C	76	77	78	79	80	
00236	905°		X1.0027554E-4.7.7438980E-5.6.0696757E-5.4.8080073E-5.3.9145232E-5.					
00236	906°	C	81	82	83	84	85	
00236	907°		X3.2082435E-5.2.6597710E-5.2.2377934E-5.1.9141913E-5.1.6599345E-5.					

00236	908°	C	86	87	88	89	90
00236	909°		X1.4560872E-5	1.2898417E-5	1.1522650E-5	1.0369426E-5	9.3925204E-6
00236	910°	C	91	92	93	94	95
00236	911°		X8.5583661E-6	7.8345911E-6	7.2066944E-6	6.6566336E-6	6.1717079E-6
00236	912°	C					
00240	913°		DATA (PRSLST(1),1,NP63,NP64)/				
00240	914°	C	96	97	98	99	100
00240	915°		X5.7417393E-6	5.3584943E-6	5.0126367E-6	4.6986357E-6	4.4127423E-6
00240	916°	C	101	102	103	104	105
00240	917°		X4.1517377E-6	3.9128496E-6	3.69886099E-6	3.51230234E-6	3.359993E-6
00240	918°	C	106	107	108	109	110
00240	919°		X2.5279174E-6	2.2829452E-6	2.0665225E-6	1.8747980E-6	1.7093719E-6
00240	920°	C	111	112	113	114	
00240	921°		X1.5518716E-6	1.4150844E-6	1.2921892E-6	1.2634456E-6	
00240	922°	C	115	116	117	118	119
00240	923°		X3.5024639E-6	2.22587459E-6	2.34949304E-6	1.96365027E-6	1.75234920E-6
00240	924°	C	120	121	122	123	
00240	925°		X5.8534791E-6	5.89499401E-6	5.62355810E-6	5.20696155E-6	
00240	926°	C					
00240	927°	C					
00240	928°	C	DENSITY VALUES TABULATED IN KILOGRAMS PER CUBIC METER				
00240	929°	C					
00242	930°		DATA (RHOLST(1),1,NP61,NP62)/				
00242	931°	C	1	2	3	4	5
00242	932°		X1.1835467E+0	1.1573534E+0	1.1312045E+0	1.1051789E+0	1.0793462E+0
00242	933°	C	6	7	8	9	10
00242	934°		X1.0537666E+0	1.0284922E+0	1.0035670E+0	9.7902801E-1	9.5490568E-1
00242	935°	C	11	12	13	14	15
00242	936°		X9.3122447E-1	9.000345E-1	8.8525681E-1	8.64122243E-1	8.449915662E-1
00242	937°	C	16	17	18	19	20
00242	938°		X7.5904447E-1	7.2084275E-1	6.8983435E-1	6.58535153E-1	6.2651817E-1
00242	939°	C	21	22	23	24	25
00242	940°		X4.7249382E-1	4.225460E-1	3.7638429E-1	3.3302120E-1	2.9232218E-1
00242	941°	C	26	27	28	29	30
00242	942°		X2.5432637E-1	2.1920326E-1	1.8717895E-1	1.5845601E-1	1.3239218E-1
00242	943°	C	31	32	33	34	35
00242	944°		X1.1096236E-1	9.3193799E-2	8.6193250E-2	7.978898E-2	7.39382489E-2
00242	945°	C	36	37	38	39	40
00242	946°		X2.5119029E-2	2.18334060E-2	1.9457797E-2	1.799301028E-2	1.703654170E-2
00242	947°	C	41	42	43	44	45
00242	948°		X5.4934199E-3	4.220200E-3	3.1134715E-3	2.3684559E-3	1.8151546E-3
00242	949°	C	46	47	48	49	50
00242	950°		X1.4015768E-3	1.0965534E-3	8.6526723E-4	6.8253221E-4	5.3756684E-4
00242	951°	C	51	52	53	54	55
00242	952°		X4.2227457E-4	3.3048920E-4	2.5745233E-4	1.9944483E-4	1.5352539E-4
00242	953°	C	56	57	58	59	60
00242	954°		X1.1734236E-4	8.8997983E-5	6.6949356E-5	4.9935490E-5	3.6923403E-5
00242	955°	C	61	62	63	64	65
00242	956°		X2.7067389E-5	1.9677466E-5	1.4194402E-5	1.0004256E-5	7.2583360E-6
00242	957°	C	66	67	68	69	70
00242	958°		X4.7957760E-6	3.3215805E-6	2.2404228E-6	1.5304616E-6	1.0579997E-6
00242	959°	C	71	72	73	74	75
00242	960°		X7.3962724E-7	5.2254595E-7	3.6173880E-7	2.6206711E-7	1.8979684E-7
00242	961°	C	76	77	78	79	80
00242	962°		X1.3929915E-7	1.0349963E-7	7.5342182E-8	5.606657E-8	4.2529020E-8
00242	963°	C	81	82	83	84	85
00242	964°		X3.2809278E-8	2.510940E-8	1.9457748E-8	1.5133149E-8	1.12030946E-8
00242	965°	C	86	87	88	89	90

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00242	966°		X9.7426983E-9.8.0146089E-9.6.6029560E-9.5.638713	-8J72428E-9.
00242	967°	L	91 92 93 94 95	
00242	968°		X4.1362113E-9.3.5481306E-9.3.1356750E-9.2.7585267.	14047E-9/
00242	969°	C		
00244	970°		DATA (MMOLST(1),I=NP63,NP64)/	
00244	971°	C	96 97 98 99 100	
00244	972°		X2.1726345E-9.1.9431903E-9.1.7627216E-9.1.6037353E-9.1.4631550E-9.	
00244	973°	C	101 102 103 104	
00244	974°		X1.3383898E-9.1.2273083E-9.1.0562018E-9.9.1375313E-10.	
00244	975°	C	105 106 107 108	
00244	976°		X7.9820295E-10.7.0302521E-10.6.2101002E-10.5.5011615E-10.	
00244	977°	C	109 110 111 112	
00244	978°		X4.4002371E-10.4.3637082E-10.3.9157098E-10.3.5195770E-10.	
00244	979°	C	113 114 115 116	
00244	980°		X3.1696683E-10.3.0873182E-10.4.9895351E-10.3.5436502E-10.	
00244	981°	C	117 118 119 120	
00244	982°		X5.6991186E-2.1.2347674E-3.9.7403572E-4.7.6857846E-4.	
00244	983°	C	121 122 123	
00244	984°		X1.6728017E-5.1.2023770E-5.3.9910710E-6/	
00244	985°	C		
00244	986°	C		
00244	987°	C		
00244	988°	C		
00244	989°	C		
00244	990°		SPEED OF SOUND VALUES TABULATED IN METERS PER SECOND	
00244	991°		DATA (SONLST(1),I=NP61,NP62)/	
00244	992°	C	1 2 3 4 5	
00244	993°		X3.4685752E2.3.4577091E2.3.4474100E2.3.4375977E2.3.4281972E2.	
00244	994°	C	6 7 8 9 10	
00244	995°		X3.4191375E2.3.4103527E2.3.4017814E2.3.3933604E2.3.3850555E2.	
00244	996°	C	11 12 13 14 15	
00244	997°		X3.3768001E2.3.3685564E2.3.3602846E2.3.3535175E2.3.3462585E2.	
00244	998°	C	16 17 18 19 20	
00244	999°		X3.3083264E2.3.2891940E2.3.2794679E2.3.2057962E2.3.1891021E2.	
00244	1000°	C	21 22 23 24 25	
00244	1001°		X3.1103836E2.3.0609732E2.3.0115374E2.2.9654540E2.2.9250004E2.	
00244	1002°	C	26 27 28 29 30	
00244	1003°		X2.8922838E2.2.86490521E2.2.8565248E2.2.8552323E2.2.8723862E2.	
00244	1004°	C	31 32 33 34 35	
00244	1005°		X2.6897076E2.2.9075108E2.2.9419972E2.2.9721502E2.2.9966127E2.	
00244	1006°	C	36 37 38 39 40	
00244	1007°		X3.0166194E2.3.0454826E2.3.0751834E2.3.1060615E2.3.1380529E2.	
00244	1008°	C	41 42 43 44 45	
00244	1009°		X3.1706789E2.3.2031579E2.3.2342147E2.3.2622854E2.3.2854145E2.	
00244	1010°	C	46 47 48 49 50	
00244	1011°		X3.3012557E2.3.277550E2.3.275595E2.3.2518452E.3.2216108E2.	
00244	1012°	C	51 52 53 54 55	
00244	1013°		X3.1877907E2.3.1512538E2.3.1121960E2.3.0731304E2.3.0328736E2.	
00244	1014°	C	56 57 58 59 60	
00244	1015°		X2.9925283E2.2.9524650E2.2.9128985E2.2.8738653E2.2.8351977E2.	
00244	1016°	C	61 62 63 64 67	
00244	1017°		X2.7964461E2.2.7570998E2.2.7180535E2.4.2.6944122E2.	
00244	1018°	C	68 69 70	
00244	1019°		X 2.7387919E2.2.7824640E2.2.8254611E2.	
00244	1020°	C	71 72 73 74 75	
00244	1021°		X2.8678136E2.2.909549752.2.9778102E2.3.0445407E2.3.1098395E2.	
00244	1022°	C	76 77 78 79 80	
00244	1023°		X3.1737952E2.3.2364874E2.3.3583625E2.3.475967E2.3.5897208E2.	
00244	1024°	C	81 82 83 84 85	
00244	1025°		X3.6999789E2.3.4070451E2.4.0126162E2.4.2081570E2.4.3950065E2.	

			36	87	88	89	90
00246	1024°	C	X4.5742298E2	4.7466910E2	4.9131021E2	5.0740585E2	5.2300637E2
00246	1025°	C	91	92	93	94	95
00246	1026°	C	X5.3815483E2	5.5288841E2	5.6711742E2	5.812320E2	5.94900377E2
00250	1029°		DATA (SONLST(1),1,0NP63,1,0P64)				
00250	1030°	C	96	97	98	99	100
00250	1031°	C	X6.082610E2	6.2133762E2	6.3096486E2	6.4004440E2	6.4979159E2
00250	1032°	C	101	102	103	104	105
00250	1033°	C	X6.5900328E2	6.6600798E2	6.8001215E2	6.9173079E2	7.0153775E2
00250	1034°	C	106	107	108	109	110
00250	1035°	C	X7.0951229E2	7.1739818E2	7.2519035E2	7.3291548E2	7.3946609E2
00250	1036°	C	111	112	113	114	115
00250	1037°	C	X7.4488092E2	7.5025666E2	7.5559417E2	7.5692267E2	7.5349118E2
00250	1039°	C	116	117	118	119	120
00250	1039°	C	X2.9579332E2	2.9577557E2	3.0054537E2	3.02884119E2	3.02853783E2
00250	1040°	C	121	122	123		
00250	1041°	C	X2.7368549E2	2.6545229E2	2.6944122E2		
00250	1042°	C					
00250	1043°	C					
00250	1044°	C					
00250	1045°	C					
00250	1046°	C					
00252	1047°	C					
00252	1048°	C					
00252	1049°	C					
00252	1050°	C					
00252	1051°	C					
00252	1052°	C					
00252	1053°	C					
00252	1054°	C					
00252	1055°	C					
00252	1056°	C					
00252	1057°	C					
00252	1058°	C					
00252	1059°	C					
00252	1060°	C					
00252	1061°	C					
00252	1062°	C					
00252	1063°	C					
00252	1064°	C					
00252	1065°	C					
00252	1066°	C					
00252	1067°	C					
00252	1068°	C					
00252	1069°	C					
00252	1070°	C					
00252	1071°	C					
00252	1072°	C					
00252	1073°	C					
00252	1074°	C					
00252	1075°	C					
00252	1076°	C					
00252	1077°	C					
00252	1078°	C					
00252	1079°	C					
00252	1080°	C					
00252	1081°	C					

VISCOSITY COEFFICIENT
VALUES TABULATED IN KILOGRAMS PER METER PER SECOND

			1	2	3	4	5
00252	1047°	C	X1.0302431E-5	1.03224157E-5	1.03499999E-5	1.038079299E-5	1.0414441E-5
00252	1049°	C	6	7	8	9	10
00252	1051°	C	X1.7745850E-5	1.7881991E-5	1.7819367E-5	1.775524E-5	1.7696042E-5
00252	1052°	C	11	12	13	14	15
00252	1053°	C	X1.7634541E-5	1.7572676E-5	1.7510139E-5	1.7381977E-5	1.7248245E-5
00252	1054°	C	16	17	18	19	20
00252	1055°	C	X1.7107621E-5	1.6859239E-5	1.6637791E-5	1.6284601E-5	1.5905319E-5
00252	1056°	C	21	22	23	24	25
00252	1057°	C	X1.5509244E-5	1.5108096E-5	1.4707842E-5	1.4335282E-5	1.4008886E-5
00252	1058°	C	26	27	28	29	30
00252	1059°	C	X1.3745403E-5	1.3553590E-5	1.3457958E-5	1.3344759E-5	1.3358386E-5
00252	1060°	C	31	32	33	34	35
00252	1061°	C	X1.03724675E-5	1.0387977E-5	1.04145944E-5	1.04389370E-5	1.04587102E-5
00252	1062°	C	36	37	38	39	40
00252	1063°	C	X1.4748972E-5	1.4982730E-5	1.5223539E-5	1.5474160E-5	1.5734080E-5
00252	1064°	C	41	42	43	44	45
00252	1065°	C	X1.5999574E-5	1.6263778E-5	1.6516764E-5	1.6745577E-5	1.6954206E-5
00252	1066°	C	46	47	48	49	50
00252	1067°	C	X1.7063446E-5	1.7034883E-5	1.6870136E-5	1.6660460E-5	1.6414072E-5
00252	1068°	C	51	52	53	54	55
00252	1069°	C	X1.38668E-5	1.5841407E-5	1.552885E-5	1.5206885E-5	1.4860579E-5
00252	1070°	C	56	57	58	59	60
00252	1071°	C	X1.4554073E-5	1.4230412E-5	1.3911371E-5	1.3597275E-5	1.3288099E-5
00252	1072°	C	61	62	63	64	67
00252	1073°	C	X1.2976813E-5	1.2662082E-5	1.2335131E-5		1.2163172E-5
00252	1074°	C					
00252	1075°	C					
00252	1076°	C					
00252	1077°	C					
00252	1078°	C					
00252	1079°	C					
00252	1080°	C					
00252	1081°	C					

ORIGINAL FAC
IF MORE QD

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00252 1002° C          86          87          88          89          90
00252 1003° C          91          92          93          94          95
00252 1004° C          96          97          98          99          100
00252 1005° C          101         102         103         104         105
00252 1006° C          106         107         108         109         110
00252 1007° C          111         112         113         114         115
00252 1008° C          116         117         118         119         120
00252 1009° C          121         122         123
00252 1010° C          124         125
00252 1011° C          126         127         128         129         130
00252 1012° C          131         132         133         134         135
00252 1013° C          136         137         138         139         140
00252 1014° C          141         142         143         144         145
00252 1015° C          146         147         148         149         150
00252 1016° C          151         152         153         154         155
00252 1017° C          156         157         158         159         160
00252 1018° C          161         162         163         164         165
00252 1019° C          166         167         168         169         170
00252 1020° C          171         172         173         174         175
00252 1021° C          176         177         178         179         180
00252 1022° C          181         182         183         184         185
00252 1023° C          186         187         188         189         190
00252 1024° C          191         192         193         194         195
00252 1025° C          196         197         198         199         200
00252 1026° C          201         202         203         204         205
00252 1027° C          206         207         208         209         210
00252 1028° C          211         212         213         214         215
00252 1029° C          216         217         218         219         220
00252 1030° C          221         222         223         224         225
00252 1031° C          226         227         228         229         230
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00252 1078° C          461         462         463         464         465
00252 1079° C          466         467         468         469         470
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00252 1082° C          481         482         483         484         485
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00252 1085° C          496         497         498         499         500
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00252 1088° C          511         512         513         514         515
00252 1089° C          516         517         518         519         520
00252 1090° C          521         522         523         524         525
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00252 1093° C          536         537         538         539         540
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00252 1098° C          561         562         563         564         565
00252 1099° C          566         567         568         569         570
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00252 1101° C          576         577         578         579         580
00252 1102° C          581         582         583         584         585
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00252 1105° C          596         597         598         599         600
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00252 1107° C          606         607         608         609         610
00252 1108° C          611         612         613         614         615
00252 1109° C          616         617         618         619         620
00252 1110° C          621         622         623         624         625
00252 1111° C          626         627         628         629         630
00252 1112° C          631         632         633         634         635
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00252 1114° C          641         642         643         644         645
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00252 1137° C          756         757         758         759         760
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00252 1140° C          771         772         773         774         775
00252 1141° C          776         777         778         779         780
00252 1142° C          781         782         783         784         785
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00252 1144° C          791         792         793         794         795
00252 1145° C          796         797         798         799         800
00252 1146° C          801         802         803         804         805
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00252 1148° C          811         812         813         814         815
00252 1149° C          816         817         818         819         820
00252 1150° C          821         822         823         824         825
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00252 1154° C          841         842         843         844         845
00252 1155° C          846         847         848         849         850
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00252 1164° C          891         892         893         894         895
00252 1165° C          896         897         898         899         900
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00252 1167° C          906         907         908         909         910
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00252 1169° C          916         917         918         919         920
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00252 1173° C          936         937         938         939         940
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00252 1175° C          946         947         948         949         950
00252 1176° C          951         952         953         954         955
00252 1177° C          956         957         958         959         960
00252 1178° C          961         962         963         964         965
00252 1179° C          966         967         968         969         970
00252 1180° C          971         972         973         974         975
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00252 1183° C          986         987         988         989         990
00252 1184° C          991         992         993         994         995
00252 1185° C          996         997         998         999         1000
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00252 1187° C          1006        1007        1008        1009        1010
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00252 1258° C          1361        1362        1363        1364        1365
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00252 1294° C          1541        1542        1543        1544        1545
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00252 1297° C          1556        1557        1558        1559        1560
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00252 1302° C          1581        1582        1583        1584        1585
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00252 1311° C          1626        1
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