NASA TECHNICAL NOTE

NASA TN D-8247

NASA TN D-8247

THEORETICAL AND EXPERIMENTAL STUDY OF TWISTED AND CAMBERED DELTA WINGS DESIGNED FOR A MACH NUMBER OF 3.5

Russell B. Sorrells III and Emma Jean Landrum

Langley Research Center
Hampton, Va. 23665

NATIONAL AERONAUTICS AND SPACE ADMINISTRATION • WASHINGTON, D. C. • AUGUST 1976

1. Report No. NASA TN D-8247	2. Government Accession No.	3. Recipient's Catalog No.
4. Title and Subtitle THEORETICAL AND EXPERIMENTAL STUDY OF TWISTED AND CAMBERED DELTA WINGS DESIGNED FOR A MACH NUMBER OF 3.5		5. Report Date August 1976 6. Performing Organization Code
7. Author(s) Russell B. Sorrells III and Emma Jean Landrum		8. Performing Organization Report No. L-10823
9. Performing Organization Name and Address NASA Langley Research Center Hampton, Va. 23665		10. Work Unit No. 505-11-15-01 11. Contract or Grant No.
12. Sponsoring Agency Name and Address National Aeronautics and Space Administration Washington, D.C. 20546		13. Type of Report and Period Covered Technical Note 14. Sponsoring Agency Code
15. Supplementary Notes		

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17. Key Words (Suggested by Author(s)) Aerodynamics Delta wing Pressure distributions Force data Supersonic	18. Distribution Statement Unclassified – Unlimited Subject Category 02

19. Security Classif. (of this report) Unclassified	20. Security Classif. (of this page) Unclassified	21. No. of Pages 236	22. Price* $7.50

*For sale by the National Technical Information Service, Springfield, Virginia 22161

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SUMMARY

This investigation provided data for the evaluation of the aerodynamic performance of a series of twisted and cambered delta wings designed for a Mach number of 3.5. Systematic force and pressure data are also presented for comparison with theory.

Force tests were made at Mach numbers of 2.3, 3.0, 3.5, 4.0, and 4.6. Design lift coefficients of 0.0 and 0.1 were employed on the 55° and 68° sweep wings, and design lift coefficients of 0.0, 0.05, and 0.1 were employed on the 76° sweep wings. Pressure tests were conducted on the 55° and 76° sweep flat wings and on the 0.1 design lift coefficient 76° sweep wing.

The results indicate that for the sweep angles tested, an increase in the zero-lift pitching-moment coefficient is the primary benefit of twist and camber at a Mach number of 3.5. Comparison of the experimental results with results obtained from several lift theories indicates that the Carlson-Middleton linear theory method gave the best overall agreement. The pressure data indicate, however, that there is a fortuitous cancellation of error at high angle of attack where the lower surface pressures are significantly underpredicted over the inboard region of the wing and where the upper and lower surface pressures are overpredicted over the outboard region of the wing.

INTRODUCTION

The performance benefits of twist and camber applied to swept wings with subsonic leading edges at moderate supersonic speeds have been demonstrated both theoretically (refs. 1 to 5) and experimentally (refs. 6 to 8). The benefits at moderate supersonic speeds are a higher lift-drag ratio relative to that for a flat wing and a positive zero-lift pitching moment. The positive zero-lift pitching moment has provided for self-trimming configurations with little or no trim drag at supersonic speeds. It is not known, however, whether twist and camber provide similar benefits in the high supersonic speed range.

Reference 9 indicates that the benefits are minimal for delta wings at Mach numbers above about 3.0, but that double delta planforms might provide some benefits up to about Mach 4.5.

The purpose of this investigation was to provide data for the evaluation of the aerodynamic performance of a series of twisted and cambered delta wings designed for a Mach number of 3.5; the investigation also provided systematic force, pressure, and flow-visualization data in the Mach number range from 2.3 to 4.6. The wings tested were not intended to represent optimum aerodynamic designs for a Mach number of 3.5, but were intended to provide data which could lead to optimum design.

The purpose of the pressure investigation was to aid in the analysis of the force data and to provide, insofar as possible, systematic and detailed data for comparison with theory. To date, no analytical technique has been developed to predict accurately the detailed loading at high angles of attack. It is essential that high angle-of-attack pressure data through a Mach number range on a series of wings, as provided by this investigation, be available if such a technique is to be developed.

Force tests were made on seven wings; detailed pressure data were taken on three of the seven wings at Mach numbers of 2.3, 3.0, 3.5, 4.0, and 4.6 through an angle-of-attack range from about -5° to 23°. These data are tabulated in appendixes A and B which follow the figures. Boundary-layer transition was fixed and all tests were conducted at a free-stream Reynolds number of 8.1×10^6 per meter.

SYMBOLS

The results are referred to the stability-axis system. The moment reference point is at 56.9 percent of the overall length for all models. Angle of attack is referenced to the center line of the strain-gage balance.

b	span
C_D	drag coefficient, $\frac{\text{Drag}}{q_\infty S}$
$C_{D,C}$	zero-lift camber drag coefficient
$C_{D,W}$	zero-lift wave drag coefficient
C_L	lift coefficient, $\frac{\text{Lift}}{q_\infty S}$
$C_{L,des}$	design lift coefficient

$C_{L,p}$ potential lift coefficient

C_{L_α} $= \frac{C_L}{\Delta\alpha}$, per deg

C_m pitching-moment coefficient, $\frac{\text{Pitching moment}}{q_\infty S\bar{c}}$

$C_{m,0}$ pitching-moment coefficient at zero lift

C_N normal-force coefficient, $\frac{\text{Normal force}}{q_\infty S}$

C_{N_α} $\approx \frac{C_N}{\Delta\alpha}$, per deg

C_p local pressure coefficient, $\frac{p - p_\infty}{q_\infty}$; Cp in computer-generated tables and plots

ΔC_p total lifting pressure coefficient $\left(C_{p,\text{lower}} - C_{p,\text{upper}}\right)$

c local chord

$\bar{c}$ mean geometric chord

c_n section normal-force coefficient, $\int_0^{1.0} \Delta C_p \, d\left(\frac{x}{c}\right)$

L/D lift-drag ratio

$(L/D)_{max}$ maximum lift-drag ratio

M free-stream Mach number

p local pressure, N/m^2

p_∞ free-stream static pressure, N/m^2

q_∞ free-stream dynamic pressure, N/m^2

S reference wing area, 0.2045 m^2

x longitudinal distance measured from model apex, cm

y spanwise distance measured from model center line, cm

α angle of attack, deg

β $= \sqrt{M^2 - 1}$

Λ leading-edge sweep angle, deg

μ Mach angle, deg

Abbreviations:

L.S. lower surface

U.S. upper surface

MODEL TESTS

Model Design

The three sweep angles employed were selected to cover the three basic leading-edge conditions at the design Mach number of 3.5: subsonic, supersonic with detached leading-edge shock, and supersonic with attached leading-edge shock. The 76° sweep wing had a subsonic leading edge at a Mach number of 3.5, the 68° sweep wing was estimated to have a detached shock at angles of attack above 3°, and the 55° sweep wing was estimated to have a detached shock at angles of attack above 15°.

The cambered and twisted wings were designed by using a computer program based on the method described in reference 3. This program determines the wing camber and twist which supports an optimum combination of three specified loadings so that the wing has minimum drag for a given lift coefficient. A body of revolution was added symmetrically about the wing center line to provide a housing for the strain-gage balance. The base diameter was 5.08 cm for all wings and was the minimum diameter required to house the balance. For the 76° leading-edge sweep models, the root chord incidence as given by the computer program exceeded that incidence believed practical. Accordingly, for these wings the mean camber surface was significantly modified in the root chord region. For example, the z-ordinate at the trailing edge of the root chord for the $C_{L,des} = 0.1$ wing was changed from 11.4 cm to 6.8 cm. The $C_{L,des} = 0.05$ wing was designed by using the option of reference 10; in this option, the z-ordinate of the trailing edge at the model center line is constrained to a specified value. For this wing a value of 4.45 cm was used for the constraint, and the root chord was refaired so that the trailing-edge ordinate was 3.82 cm. The root chord camber as defined by the numerical program was left unchanged for the 68° and 55° sweep-angle wings. It should

be mentioned, however, that all the wings depart from the true theoretical optimum which displays a root chord singularity. The finite solution at the wing root is the result of the numerical techniques used in the computer program. The airfoils for all the cambered wings were sheared vertically so that the mean chord lines are flat across the span at 50 percent of the root chord.

Models

Force models.- The models had clipped delta wings of equal planform area and employed three leading-edge sweep angles: 76°, 68°, and 55°. (See figs. 1 and 2.) One flat and one cambered and twisted wing designed to have minimum drag at $C_{L,des} = 0.1$ and a Mach number of 3.5 were tested for each sweep angle. In addition, a 76° sweep wing cambered and twisted to have minimum drag at $C_{L,des} = 0.05$ and a Mach number of 3.5 was tested. All the wings had 4-percent-thick circular-arc airfoils. A minimum-volume body housed the strain-gage balance and provided for minimum departure from the prescribed optimum loading distribution. The body base diameter of 5.08 cm for all models permitted sting mounting from the rear on the main support system of the tunnel. All models except the $C_{L,des} = 0.05$ wing were measured on a three-dimensional digitizer. The resulting numerical configuration data (in the form described in ref. 11) are presented in tables I to VI.

Pressure models.- Three of the force models were duplicated as pressure models: the 76° sweep at $C_{L,des} = 0.1$, the 76° sweep flat, and the 55° sweep flat. The pressure tubes were integrally cast into the models to permit a greater number of more closely spaced pressure measurements. (See appendix B for pressure orifice locations.) On the 76° sweep cambered and the 76° sweep flat wings, the upper and lower surface orifices were serviced by the same pressure tube; this technique required taping one surface while the other surface was being tested. The models were sting mounted from the rear on the main support system of the tunnel.

Tunnel Description

Tests were conducted in the high Mach number test section of the Langley Unitary Plan wind tunnel which is a variable Mach number, variable pressure, continuous-flow tunnel. The test section is approximately 1.22 m square. (See ref. 12 for a more detailed description of this facility.)

Test Measurements and Corrections

All tests were conducted at a free-stream Reynolds number of 8.1×10^6 per meter. The stagnation temperature was maintained at 338 K for Mach numbers of 2.3, 3.0, and 3.5, and at 352 K for Mach numbers of 4.0 and 4.6. Transition strips composed of

number 40 carborundum grit (0.0460 ± 0.0041 cm) were fixed at a position 1.016 cm aft of the leading edge in a streamwise direction. The grit was individually spaced so as to be three diameters apart on centers.

Aerodynamic forces and moments were measured by means of a six-component electrical strain-gage balance housed within the model. All pitching moments were referenced to a point which would provide a subsonic static margin of $0.05\bar{c}$ as calculated by a Langley subsonic aerodynamic computer program based on the method of reference 13.

Angle of attack for all the models is defined as the strain-gage balance angle of attack and has been corrected for tunnel flow angularities and sting and balance deflection due to aerodynamic loads. The data have been adjusted to represent the condition of free-stream static pressure acting over the base of the body.

Pressures were measured by four scanning values. All pressure coefficients were referenced to free-stream static pressure.

Accuracy

Force data.- Given the balance accuracy of 0.5 percent of maximum load, the various parameters can be estimated to be accurate within the following limits:

C_D	±0.0005
C_L	±0.006
C_m	±0.006 (76^o sweep)
	±0.007 (68^o sweep)
	±0.01 (55^o sweep)

The accuracies are based on a dynamic pressure of 14 100 N/m^2 (the nominal dynamic pressure for a Mach number of 4.60).

Pressure data.- The accuracy of the scanning valve system is better than 1 percent of the gage range of 34 kN/m^2. When expressed as pressure coefficient, this accuracy varies from 0.01 at a Mach number of 2.3 to 0.03 at a Mach number of 4.6.

RESULTS AND DISCUSSION

For the convenience of the reader, the large volume of basic experimental data is placed in appendixes A and B. Only summary data, selected theoretical-experimental correlations, and discussions of oil-flow photographs are presented in the main body of the text. The longitudinal aerodynamic characteristics α, C_L, C_D, and C_m for seven wings and five Mach numbers are given in tables A-1 to A-7 of appendix A. Upper and lower surface pressure coefficients for the three pressure wings tested are given in tables B-1 to B-15 of appendix B.

Comparison of Various Theoretical Results With Experimental Force Results

The experimental data for Mach numbers 2.3, 3.5, and 4.6 are compared with data obtained by several theoretical methods (figs. 6 and 7) used for calculating lift, drag, and pitching moment. The theoretical methods used include: small angle linear potential theory (Carlson-Middleton method, ref. 16); Polhamus leading-edge suction analogy for vortex lift (refs. 15 and 17); the Woodward linear potential theory (refs. 18, 19, and 20); and several hypersonic theories which are options in the Douglas hypersonic arbitrary-body computer program (ref. 21). All the methods shown in figure 7 include skin-friction values based on reference 22. For the theories which do not calculate their own wave drag (Carlson-Middleton and Polhamus suction analogy), the method of reference 23 was used.

Carlson-Middleton theory.- This theory calculates the lift, pitching moment, and drag due to lift numerically by the use of a planar grid system (51 × 100 on right-hand wing panel). The local surface slope of a point on a lifting surface is related to the pressure at the point, the influence of pressures upstream of the specified point being taken into account (ref. 16). A small angle assumption is used in this method so that the lift coefficient is given by $C_L = C_{N_\alpha} \alpha$. A problem with this method is that pressures are allowed to exceed vacuum.

The agreement of this theory with experiment is generally good throughout the Mach number range for all the wings, but is better for the 55^o and the 68^o sweep wings. The generally good agreement obtained with this method may be caused in part by compensating errors between the use of the small angle approximation and by permitting pressures to exceed vacuum (discussed further in the section on pressure measurements).

Polhamus leading-edge suction analogy.- The Mach 2.3 data of figures 7(a) and 7(b) are unique in that they are the only data obtained for the case where the leading edge is sufficiently subsonic to generate a significant amount of vortex lift. The experimental values of lift slightly exceed those predicted by the Carlson-Middleton method as expected, although this fact in itself is not conclusive evidence that there is vortex lift present. The lift, pitching moment, and drag due to lift were calculated by using the vortex-lift theory described in references 15 and 17. This vortex-lift theory is based on the assumption that when leading-edge suction is lost, it is converted into a normal force or vortex lift. The total lift is assumed to be the vortex-lift increment plus the potential lift. The potential lift is defined as the linear potential theory lift (or Carlson-Middleton) described previously but without the small angle assumption. Therefore, the equation for potential lift is given by:

$$C_{L,p} = C_{N_\alpha} \sin \alpha \cos^2 \alpha$$

where C_{N_α} is the linear potential theory C_{L_α} used in the Carlson-Middleton method.

The vortex lift was calculated by using the computer program described in reference 24. This program calculates the section leading-edge thrust at several spanwise stations and integrates them to obtain an overall leading-edge suction (vortex lift). The subsonic leading-edge cases shown in figure 7 indicate, however, that the assumption of 100-percent leading-edge suction is not justified because the lift is consistently overpredicted. For the supersonic leading-edge cases (where there is no vortex lift), the Carlson-Middleton method generally agrees as well as the Polhamus analogy even though the latter corrects for the small angle assumption. Furthermore, the pressure data (to be discussed later) indicate no significant increment in lift on the upper surface relative to linear theory; however, the data do indicate a strong increment of lift on the lower surface relative to linear theory.

The pitching moment was found by summing the potential pitching moment and the contribution to pitching moment from the vortex lift. The vortex-lift contribution to pitching moment is found by assuming that the vortex lift acts along the leading edge normal to the wing surface and by integrating the section pitching moment due to vortex lift along the leading edge.

Woodward.- The unified approach to the aerodynamic analysis of wing-body-tail configurations presented in references 18 and 19 has been extended in reference 20 by the introduction of several aerodynamic singularity distributions. These distributions improve the capability to represent arbitrary shapes.

The configuration surface is subdivided into a large number of panels, each of which contains an aerodynamic singularity distribution. A constant source distribution is used on the body panels, and a vortex distribution with a linear variation in the streamwise direction is used on the wing and tail. The normal components of velocity induced at specified control points make up the coefficients of a system of linear equations relating the strengths of the singularities to the magnitude of the normal velocities. A matrix inversion procedure is used to solve this system of equations for the singularity strengths which satisfy the boundary conditions of tangential flow at the control points for a given Mach number and angle of attack. From these singularity strengths, pressure coefficients are calculated, and the forces and moments acting on the configuration are determined by numerical integration. This method, although it uses linearized theory, does not make the small angle assumptions and limits pressures to vacuum after all the pressures have been calculated.

In figure 7, the agreement between theoretical data and experimental data is generally good except at high lift and high Mach number. This exception could be a result of the failure to apply the pressure-limiting feature until all pressures have been calculated.

Douglas hypersonic arbitrary-body computer program.- This program provides for the option of selecting the theory to be used for surfaces under compression and the surfaces under expansion (ref. 21). In this study, the Prandtl-Meyer expansion was used for the expansion surfaces, and three different theories were used for the surfaces under compression: modified Newtonian, tangent wedge, and tangent cone. All three of these methods first calculated the pressure coefficients and then calculated the lift, drag due to lift, pitching moment, and drag due to volume. The tangent-wedge option agreed very well with experiment for the higher values of $\beta \cot \Lambda$.

Zero-lift drag component comparison.- The zero-lift camber and wave drag are shown in figure 6. The zero-lift wave drag was calculated by using the Harris wave-drag program (ref. 23) by describing the entire model as a wing and using 50 cutting plane angles. A special version of the program which allows the wing to have finite thickness at the trailing edge was used.

The camber drag predictions of the Carlson-Middleton and Woodward methods appear to agree equally well at all Mach numbers for the 76° sweep wing. However, for the 68° and 55° sweep wings the Woodward program predicts negative camber drag whereas the Carlson-Middleton program predicts positive camber drag with reasonably good accuracy for all three sweeps. The tangent-wedge predictions at higher Mach numbers agree with experiment reasonably well at all sweep angles although the predictions for the 68° sweep are somewhat high.

The Woodward program overpredicts the zero-lift wave drag at the lower Mach numbers for the 68° and 55° sweep wings while comparing very well with experiment for the 76° sweep wing. The zero-lift drag predictions of the Harris program are low for the 55° sweep wing for all Mach numbers and at the high Mach numbers for the 68° sweep wing. At the higher Mach numbers the tangent wedge predicts the wave drag reasonably well except for the 68° sweep wing.

Comparison of Various Theories With Pressure Tests

Comparisons of experimental pressure data for representative angles of attack with data obtained from both the Woodward theory (ref. 20) and the Middleton theory (ref. 25) are presented in figures 8 to 16. Pressure data for the 76° sweep wings (figs. 8 to 13) were integrated to obtain the spanwise lift distributions shown in figure 17.

The Woodward theory shown in figures 8 to 16 employs a pressure-limiting feature which limits pressures to vacuum after all the pressures have been calculated. The

Middleton method, on the other hand, allows the user to select the fraction of vacuum he wishes to use, and the pressure limiting is applied as the pressures are calculated. For figures 8 to 16 a vacuum fraction of 0.7 was used. This limit appears to work very well for the upper surface, but since the program in its present form constrains the total lifting pressure, it unnecessarily limits the lower surface pressures. As a result, the lower surface pressures are consistently underpredicted at the higher angles of attack. The numerical model used for the Middleton method was an all wing description.

The data shown in figure 12(b) represent the $C_{L,des} = 0.1$ design case for the 76° sweep wing. The camber was designed with technology similar to that of the Middleton method without pressure limiting. By assuming that the pressures do not exceed vacuum, the data would be expected to agree more closely with the Middleton method without pressure limiting than they do. In general, it appears that the outboard section of the wing does not lift as much as expected. This outboard section is the area of the wing where camber and twist are expected to provide a thrust component. The experimental pressures on the lower surface near the leading edge are considerably overpredicted and show no inclination to follow the theoretical predictions at the leading edge. The exception to the overprediction on the lower surface is the center-line station (fig. 12(b)) where the pressures were underpredicted near the leading edge. This underprediction was apparently caused by the groove (see fig. 2) on the lower surface center line (which resulted from shearing the camber lines) since the flat wings do not show this phenomenon at moderate angles of attack. Comparison of data obtained by the Middleton without pressure limiting method with the data of the two outboard stations (figs. 9(b) and 12(b)) indicates boundary-layer separation which is substantiated by the oil-flow photographs of this region (figs. 4(a) and 4(b)).

At the high angles of attack tested for each wing, linear theory appears to be totally inadequate, especially for the lower surface where the experimental pressures are much higher (except at the tip) than the estimates. In view of this large discrepancy for the lower surface, the question arises as to the significance of a relatively small vortex-lift correction which is assumed to occur on the upper surface only. Figures 8(c) and 11(c) indicate a small amount of vortex lift at $2y/b = 0.2$. However, the lower surface pressures indicate that if lift greater than that predicted by linear theory exists, it would be caused by lower surface effects and not by vortex lift. The lower surface pressures also indicate that the force data correlation with theory (Carlson-Middleton) is fortuitous at the highest angles of attack because underprediction of lift at the inboard stations is canceled by overprediction of lift at the outboard stations. (See fig. 17.) Since the zero-thickness linear theory prediction assumes equal pressure coefficients of opposite sign on the upper and lower surfaces, the high pressure coefficients measured on the lower surface (approximately twice those measured on the upper surface) could not be obtained theoretically. Pressure limiting as applied in the Middleton method would tend to magnify

this discrepancy further since the limits are applied to the loading parameter ΔC_p. Thus, the assumption of equal pressures of opposite sign on the upper and lower surfaces would result in even lower pressures than those obtained without pressure limiting.

Reference 26 compares pressure data with linear theory on a series of delta wings at Mach numbers from 1.62 to 2.41. This reference shows the same underprediction of lower surface pressure coefficient at an angle of attack as low as 7°.

CONCLUDING REMARKS

The experimental results indicate that for the wings tested, an increase in the pitching-moment coefficient at zero lift is the primary benefit of twist and camber at a Mach number of 3.5.

Comparison of the experimental force data results with results obtained from several lift theories indicates that the Carlson-Middleton method gave the best overall agreement at all conditions. It is thus concluded that linear theories can be used with good accuracy to estimate lift, drag due to lift, and pitching moment on slender wing-body configurations up to a Mach number of 4.6 at moderate angles of attack. The pressure data, however, indicate that there is a fortuitous cancellation of error at high angle of attack where the lower surface pressures are significantly underpredicted over the inboard region of the wing and where the upper and lower surface pressures are overpredicted over the outboard region of the wing.

It appears from both the force and the pressure data that any proper correction made to the theory for vortex lift would be small.

Langley Research Center
National Aeronautics and Space Administration
Hampton, Va. 23665
May 10, 1976

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TABLE I.- NUMERICAL CONFIGURATION DATA FOR WING WITH 76° SWEEP,

$C_{L,des} = 0.0$

[See ref. 11]

1 1			19 20							
2045.16										REFA
0.	.5	.75	1.25	2.5	5.	7.5	10.	15.	20.	XAF 10
25.	30.	35.	40.	50.	60.	70.	80.	90.	100.	XAF 20
-.061	.003	0.000	90.548							WAFORG 1
.686	.216	0.000	89.797							WAFORG 2
1.516	.432	0.000	88.966							WAFORG 3
2.362	.648	0.000	88.120							WAFORG 4
3.223	.864	0.000	87.259							WAFORG 5
4.094	1.082	0.000	86.388							WAFORG 6
4.950	1.290	0.000	85.534							WAFORG 7
6.665	1.727	0.000	83.820							WAFORG 8
8.352	2.154	0.000	82.151							WAFORG 9
9.863	2.540	0.000	80.630							WAFORG10
16.965	4.305	0.000	73.492							WAFORG11
25.557	6.457	0.000	64.902							WAFORG12
34.229	8.611	0.000	56.241							WAFORG13
42.857	10.765	0.000	47.612							WAFORG14
51.483	12.918	0.000	38.994							WAFORG15
60.117	15.070	0.000	30.363							WAFORG16
68.760	17.224	0.000	21.732							WAFORG17
77.450	19.378	0.000	13.038							WAFORG18
86.106	21.488	0.000	4.379							WAFORG19
0.000	-.008	-.013	-.008	-.010	-.013	-.008	-.008	-.003	0.000	TZORD 1
.005	.005	.008	.005	-.010	-.025	-.023	-.020	-.013	.010	TZORD 1
0.000	-.003	-.005	-.010	-.008	-.003	0.000	-.003	-.005	-.010	TZORD 2
-.005	-.003	0.000	0.000	-.015	-.028	-.028	-.025	-.018	.008	TZORD 2
-.010	-.003	-.003	-.003	-.003	.003	.008	.008	0.000	-.015	TZORD 3
-.015	-.010	-.008	-.008	-.025	-.033	-.033	-.028	-.020	.005	TZORD 3
-.008	-.003	0.000	.003	0.000	.003	.008	.005	-.003	-.020	TZORD 4
-.020	-.018	-.015	-.015	-.033	-.036	-.033	-.033	-.023	.005	TZORD 4
-.020	0.000	.005	0.000	.005	.005	.010	.010	-.008	-.028	TZORD 5
-.033	-.030	-.028	-.030	-.043	-.041	-.038	-.036	-.025	.003	TZORD 5
-.015	.005	.008	.003	.003	.005	.010	.005	-.010	-.041	TZORD 6
-.046	-.043	-.041	-.043	-.048	-.043	-.048	-.038	-.030	-.003	TZORD 6
-.018	-.003	.003	.008	.003	.003	.013	.008	-.005	-.023	TZORD 7
-.048	-.051	-.051	-.058	-.061	-.053	-.053	-.046	-.038	.003	TZORD 7
-.015	-.003	.003	.005	.005	.010	.010	.008	.003	.003	TZORD 8
.013	.015	.005	-.036	-.058	-.056	-.069	-.066	-.043	.020	TZORD 8
-.003	.005	.005	.005	.005	.008	.005	.003	.013	.018	TZORD 9
.025	.041	.056	.048	.030	.018	-.003	-.051	-.056	.003	TZORD 9
-.020	-.005	0.000	-.003	.003	.005	.008	.005	.015	.023	TZORD 10
.030	.046	.056	.053	.038	.028	.020	.015	.028	.025	TZORD 10
-.033	-.020	-.018	-.013	-.010	-.003	.003	.008	.018	.025	TZORD 11
.036	.036	.036	.036	.036	.023	.013	.015	.033	.025	TZORD 11
-.028	-.013	-.008	-.005	-.005	.003	.008	.015	.025	.025	TZORD 12
.020	.018	.025	.036	.033	.013	.008	.013	.028	.028	TZORD 12
-.013	-.003	0.000	0.000	.005	.010	.013	.010	.008	.008	TZORD 13
.010	.020	.025	.028	.020	.008	.003	.008	.020	.030	TZORD 13
-.005	-.005	-.005	-.008	-.010	-.010	-.010	-.010	-.008	-.003	TZORD 14
.003	.013	.018	.018	.013	.003	.003	.005	.015	.028	TZORD 14
-.018	-.013	-.008	-.005	-.005	-.010	-.015	-.015	-.013	-.005	TZORD 15
-.003	.003	.008	.010	.005	0.000	-.005	0.000	.010	.028	TZORD 15

TABLE I.- Concluded

-.018	-.013	-.010	-.008	-.008	-.005	-.010	-.013	-.013	-.010	TZORD 16
-.010	-.005	.003	.003	0.000	-.008	-.008	0.000	.013	.036	TZORD 16
-.025	-.023	-.020	-.020	-.020	-.018	-.018	-.020	-.018	-.018	TZORD 17
-.015	-.013	-.010	-.008	-.005	-.008	-.005	.010	.023	.041	TZORD 17
-.038	-.036	-.036	-.033	-.028	-.025	-.025	-.025	-.025	-.023	TZORD 18
-.020	-.015	-.010	-.005	0.000	0.000	.010	.023	.033	.025	TZORD 18
-.028	-.025	-.023	-.020	-.015	-.013	-.015	-.013	-.005	-.003	TZORD 19
0.000	.008	.010	.013	.025	.025	.025	.025	.020	.041	TZORD 19
0.000	.083	.102	.141	.230	.396	.570	.747	1.097	1.453	WAFORD 1
1.800	2.078	2.299	2.486	2.723	2.775	2.786	2.812	2.834	2.828	WAFORD 1
0.000	.080	.101	.137	.235	.426	.606	.785	1.145	1.504	WAFORD 2
1.846	2.116	2.335	2.516	2.747	2.791	2.803	2.828	2.846	2.845	WAFORD 2
0.000	.068	.094	.134	.236	.436	.623	.806	1.164	1.528	WAFORD 3
1.864	2.132	2.349	2.529	2.750	2.785	2.796	2.822	2.837	2.834	WAFORD 3
0.000	.065	.091	.132	.237	.443	.632	.810	1.167	1.523	WAFORD 4
1.855	2.118	2.338	2.519	2.728	2.756	2.769	2.793	2.806	2.806	WAFORD 4
0.000	.064	.090	.131	.239	.446	.636	.812	1.161	1.497	WAFORD 5
1.818	2.081	2.299	2.484	2.686	2.705	2.716	2.742	2.751	2.754	WAFORD 5
0.000	.070	.095	.138	.249	.453	.640	.816	1.140	1.443	WAFORD 6
1.751	2.014	2.237	2.422	2.615	2.626	2.636	2.666	2.672	2.673	WAFORD 6
0.000	.063	.092	.141	.249	.451	.640	.818	1.125	1.390	WAFORD 7
1.662	1.922	2.143	2.321	2.500	2.509	2.526	2.552	2.557	2.544	WAFORD 7
0.000	.060	.088	.141	.252	.458	.640	.811	1.097	1.339	WAFORD 8
1.558	1.758	1.933	2.051	2.175	2.170	2.170	2.202	2.204	2.171	WAFORD 8
0.000	.065	.092	.137	.256	.455	.636	.795	1.078	1.327	WAFORD 9
1.545	1.735	1.864	1.924	1.977	1.914	1.754	1.593	1.554	1.494	WAFORD 9
0.000	.063	.089	.133	.256	.452	.627	.780	1.067	1.323	WAFORD10
1.550	1.739	1.863	1.924	1.973	1.901	1.679	1.292	.846	.317	WAFORD10
0.000	.059	.086	.134	.239	.425	.595	.753	1.047	1.316	WAFORD11
1.564	1.753	1.882	1.965	2.015	1.950	1.714	1.275	.721	0.0	WAFORD11
0.000	.049	.071	.111	.217	.400	.567	.727	1.032	1.304	WAFORD12
1.537	1.720	1.854	1.949	2.013	1.958	1.716	1.268	.722	0.0	WAFORD12
0.000	.046	.067	.109	.210	.393	.558	.717	1.012	1.275	WAFORD13
1.495	1.688	1.825	1.920	2.008	1.966	1.712	1.264	.716	0.0	WAFORD13
0.000	.051	.076	.120	.224	.406	.564	.716	1.006	1.261	WAFORD14
1.478	1.667	1.819	1.916	2.008	1.961	1.701	1.266	.723	0.0	WAFORD14
0.000	.047	.075	.119	.228	.421	.584	.732	1.012	1.260	WAFORD15
1.475	1.658	1.812	1.920	2.003	1.960	1.702	1.271	.738	0.0	WAFORD15
0.000	.051	.075	.118	.225	.413	.582	.730	1.006	1.251	WAFORD16
1.462	1.639	1.781	1.883	1.977	1.929	1.693	1.282	.779	0.0	WAFORD16
0.000	.035	.053	.091	.195	.394	.577	.739	1.012	1.254	WAFORD17
1.464	1.627	1.756	1.851	1.967	1.941	1.723	1.349	.854	0.0	WAFORD17
0.000	.057	.085	.137	.238	.432	.634	.813	1.110	1.342	WAFORD18
1.527	1.666	1.793	1.889	1.984	1.969	1.841	1.530	.973	0.0	WAFORD18
0.000	.075	.112	.185	.352	.565	.649	.826	.973	1.275	WAFORD19
1.396	1.640	1.758	1.998	2.077	2.181	2.066	1.797	1.202	0.0	WAFORD19

TABLE II.- NUMERICAL CONFIGURATION DATA FOR WING WITH 76° SWEEP,

$C_{L,des} = 0.1$

[See ref. 11]

1 1			19 20							
2045.16										REFA
0.0	0.5	.75	1.25	2.5	5.0	7.5	10.	15.	20.	XAF 10
25.	30.	35.	40.	50.	60.	70.	80.	90.	100.0	XAF 20
0.000	0.000	0.000	90.731							WAFORG 1
.058	.218	0.000	90.655							WAFORG 2
.889	.432	0.000	89.812							WAFORG 3
1.740	.648	0.000	88.928							WAFORG 4
2.664	.864	0.000	87.988							WAFORG 5
3.553	1.080	0.000	87.092							WAFORG 6
4.359	1.298	0.000	86.286							WAFORG 7
6.020	1.727	0.000	84.607							WAFORG 8
7.826	2.154	0.000	82.789							WAFORG 9
9.431	2.540	0.000	81.178							WAFORG10
16.754	4.305	0.000	73.889							WAFORG11
25.326	6.459	0.000	65.303							WAFORG12
34.039	8.611	0.000	56.563							WAFORG13
42.710	10.765	0.000	47.854							WAFORG14
51.377	12.918	0.000	39.134							WAFORG15
60.030	15.070	0.000	30.437							WAFORG16
68.732	17.224	0.000	21.671							WAFORG17
77.401	19.378	0.000	12.959							WAFORG18
85.933	21.397	0.000	4.348							WAFORG19
5.606	5.580	5.568	5.542	5.461	5.258	5.024	4.780	4.204	3.607	TZORD 1
2.974	2.385	1.908	1.473	.665	.046	-.328	-.460	-.320	-.041	TZORD 1
5.634	5.608	5.596	5.565	5.481	5.281	5.052	4.806	4.221	3.617	TZORD 2
2.982	2.390	1.910	1.478	.665	.051	-.330	-.457	-.315	.028	TZORD 2
5.443	5.418	5.403	5.370	5.276	5.098	4.905	4.666	4.092	3.493	TZORD 3
2.865	2.301	1.834	1.412	.617	.020	-.340	-.452	-.312	-.056	TZORD 3
5.171	5.144	5.128	5.090	4.983	4.831	4.666	4.455	3.917	3.330	TZORD 4
2.725	2.197	1.750	1.336	.561	-.013	-.353	-.450	-.312	-.023	TZORD 4
4.864	4.818	4.796	4.752	4.651	4.514	4.361	4.168	3.691	3.129	TZORD 5
2.568	2.080	1.651	1.250	.500	-.053	-.368	-.452	-.310	-.015	TZORD 5
4.524	4.465	4.442	4.402	4.321	4.176	4.023	3.848	3.432	2.921	TZORD 6
2.410	1.969	1.565	1.173	.447	-.089	-.381	-.457	-.310	-.069	TZORD 6
4.155	4.125	4.110	4.077	3.985	3.840	3.698	3.543	3.180	2.723	TZORD 7
2.273	1.872	1.488	1.120	.414	-.109	-.389	-.457	-.307	.008	TZORD 7
3.515	3.493	3.475	3.434	3.348	3.233	3.122	3.010	2.715	2.362	TZORD 8
2.012	1.674	1.361	1.041	.389	-.094	-.366	-.439	-.284	.076	TZORD 8
2.891	2.880	2.873	2.860	2.814	2.733	2.667	2.573	2.316	2.047	TZORD 9
1.778	1.496	1.229	.950	.391	-.066	-.345	-.495	-.254	.071	TZORD 9
2.443	2.436	2.431	2.421	2.395	2.357	2.306	2.217	2.014	1.824	TZORD 10
1.598	1.359	1.118	.866	.348	-.112	-.391	-.437	-.239	.008	TZORD 10
.983	.996	1.001	1.013	1.044	1.105	1.153	1.184	1.179	1.105	TZORD 11
1.008	.892	.742	.582	.257	-.084	-.396	-.691	-.947	-1.234	TZORD 11
.386	.434	.447	.460	.478	.564	.617	.658	.704	.732	TZORD 12
.721	.673	.617	.533	.315	.086	-.155	-.424	-.691	-.960	TZORD 12
.259	.287	.297	.318	.351	.424	.485	.536	.638	.706	TZORD 13
.742	.744	.719	.668	.546	.404	.279	.043	-.178	-.399	TZORD 13
.612	.638	.650	.673	.709	.767	.831	.886	.983	1.054	TZORD 14
1.090	1.097	1.092	1.082	1.052	.986	.902	.787	.617	.353	TZORD 14
1.247	1.262	1.270	1.285	1.313	1.351	1.389	1.430	1.511	1.577	TZORD 15
1.626	1.669	1.704	1.725	1.755	1.768	1.717	1.638	1.521	1.308	TZORD 15

TABLE II.- Concluded

1.831	1.852	1.862	1.875	1.897	1.933	1.974	2.014	2.096	2.164	TZORD 16
2.230	2.286	2.332	2.365	2.416	2.433	2.441	2.418	2.350	2.195	TZORD 16
2.431	2.441	2.446	2.456	2.479	2.517	2.550	2.583	2.652	2.718	TZORD 17
2.720	2.842	2.860	2.908	2.977	3.023	3.053	3.058	3.040	2.954	TZORD 17
3.007	3.012	3.018	3.023	3.040	3.071	3.096	3.117	3.160	3.205	TZORD 18
3.254	3.299	3.340	3.373	3.444	3.505	3.538	3.551	3.551	3.510	TZORD 18
3.564	3.566	3.569	3.571	3.576	3.589	3.602	3.612	3.630	3.653	TZORD 19
3.675	3.696	3.713	3.734	3.780	3.820	3.856	3.889	3.914	3.909	TZORD 19
0.000	.071	.104	.161	.251	.439	.619	.788	1.179	1.562	WAFORD 1
1.904	2.180	2.392	2.563	2.786	2.869	2.875	2.901	2.864	2.632	WAFORD 1
0.000	.071	.105	.163	.248	.422	.603	.778	1.167	1.547	WAFORD 2
1.895	2.166	2.375	2.552	2.769	2.859	2.869	2.892	2.856	2.697	WAFORD 2
0.000	.075	.105	.151	.232	.426	.624	.814	1.217	1.593	WAFORD 3
1.925	2.177	2.379	2.547	2.752	2.863	2.869	2.889	2.857	2.607	WAFORD 3
0.000	.061	.089	.133	.214	.412	.611	.822	1.244	1.616	WAFORD 4
1.924	2.162	2.353	2.508	2.709	2.834	2.847	2.866	2.836	2.605	WAFORD 4
0.000	.053	.079	.125	.212	.388	.588	.816	1.250	1.622	WAFORD 5
1.903	2.124	2.303	2.451	2.641	2.782	2.798	2.822	2.792	2.575	WAFORD 5
0.000	.070	.095	.127	.190	.357	.572	.806	1.237	1.602	WAFORD 6
1.858	2.062	2.237	2.374	2.557	2.711	2.720	2.749	2.720	2.438	WAFORD 6
0.000	.061	.088	.127	.182	.352	.561	.784	1.204	1.558	WAFORD 7
1.803	1.991	2.156	2.284	2.459	2.612	2.621	2.645	2.617	2.404	WAFORD 7
0.000	.071	.094	.122	.184	.371	.570	.778	1.149	1.448	WAFORD 8
1.678	1.850	2.005	2.115	2.254	2.334	2.311	2.347	2.307	2.177	WAFORD 8
0.000	.051	.076	.122	.213	.389	.591	.771	1.094	1.367	WAFORD 9
1.579	1.764	1.911	2.003	2.066	2.027	1.907	2.000	1.796	1.615	WAFORD 9
0.000	.061	.090	.136	.218	.396	.579	.738	1.042	1.320	WAFORD10
1.536	1.734	1.867	1.952	2.010	1.923	1.714	1.546	1.187	.618	WAFORD10
0.000	.042	.062	.103	.193	.370	.559	.731	1.032	1.308	WAFORD11
1.544	1.721	1.842	1.927	2.025	1.910	1.667	1.268	.742	0.	WAFORD11
0.000	.093	.124	.164	.238	.453	.628	.787	1.062	1.325	WAFORD12
1.557	1.722	1.854	1.952	2.032	1.917	1.697	1.293	.782	0.	WAFORD11
0.000	.079	.111	.161	.242	.420	.598	.764	1.094	1.353	WAFORD13
1.572	1.758	1.899	1.988	2.038	1.938	1.675	1.326	.808	0.	WAFORD13
0.000	.058	.087	.139	.246	.426	.607	.785	1.104	1.374	WAFORD14
1.598	1.752	1.863	1.955	2.039	1.962	1.721	1.282	.768	0.	WAFORD14
0.000	.062	.093	.152	.279	.473	.651	.816	1.123	1.376	WAFORD15
1.574	1.750	1.902	2.016	2.075	1.920	1.693	1.272	.755	0.	WAFORD15
0.000	.064	.095	.150	.259	.454	.638	.808	1.113	1.372	WAFORD16
1.588	1.770	1.914	1.991	2.049	1.969	1.729	1.321	.779	0.	WAFORD16
0.000	.052	.078	.130	.252	.465	.656	.819	1.096	1.323	WAFORD17
1.783	1.636	1.890	1.944	2.030	1.986	1.754	1.355	.829	0.	WAFORD17
0.000	.050	.075	.124	.246	.475	.669	.841	1.178	1.461	WAFORD18
1.656	1.829	1.983	2.079	2.213	2.067	1.828	1.466	.997	0.	WAFORD18
0.000	.057	.086	.143	.282	.542	.756	.913	1.128	1.366	WAFORD19
1.618	1.740	1.787	1.868	2.039	2.077	2.003	1.771	1.247	0.	WAFORD19

TABLE III.- NUMERICAL CONFIGURATION DATA FOR WING WITH 68° SWEEP,

$C_{L,des} = 0.0$

[See ref. 11]

```
  1  1                    20 21
2045.16                                                                  REFA
0.      .5      .75     1.25    2.5      5.      7.5     10.     15.     20.     XAF   10
25.     30.     35.     40.     50.     60.     70.     80.     90.     99.     XAF   20
100.                                                                     XAF   21
   .051   0.000   0.000 71.237                                           WAFORG 1
   .386    .213   0.000 70.907                                           WAFORG 2
   .909    .429   0.000 70.388                                           WAFORG 3
  1.445    .648   0.000 69.858                                           WAFORG 4
  1.976    .864   0.000 69.327                                           WAFORG 5
  2.553  1.077    0.000 68.750                                           WAFORG 6
  3.053  1.295    0.000 68.245                                           WAFORG 7
  4.110  1.727    0.000 67.175                                           WAFORG 8
  5.171  2.159    0.000 66.106                                           WAFORG 9
  6.093  2.535    0.000 65.176                                           WAFORG10
  6.520  2.705    0.000 64.765                                           WAFORG11
 13.216  5.408    0.000 58.016                                           WAFORG12
 19.926  8.115    0.000 51.293                                           WAFORG13
 26.640 10.818    0.000 44.577                                           WAFORG14
 33.343 13.528    0.000 37.876                                           WAFORG15
 40.488 16.383    0.000 30.731                                           WAFORG16
 46.860 18.933    0.000 24.366                                           WAFORG17
 53.614 21.646    0.000 17.615                                           WAFORG18
 60.340 24.348    0.000 10.889                                           WAFORG19
 67.104 27.056    0.000  4.097                                           WAFORG20
  -.079  -.048    -.051  -.056  -.053  -.061  -.066  -.066  -.051  -.033 TZORD  1
  -.033  -.043    -.028  -.003   .015   .030   .041   .051   .023   .030 TZORD  1
   .030                                                                  TZORD  1
  -.069  -.043    -.043  -.048  -.056  -.061  -.064  -.089  -.048  -.028 TZORD  2
  -.028  -.033    -.018   .003   .020   .030   .046   .053   .030   .041 TZORD  2
   .041                                                                  TZORD  2
  -.058  -.046    -.048  -.051  -.056  -.064  -.066  -.056  -.043  -.018 TZORD  3
  -.023  -.033    -.015   .005   .023   .028   .048   .056   .030   .043 TZORD  3
   .043                                                                  TZORD  3
  -.051  -.046    -.043  -.046  -.053  -.061  -.061  -.053  -.033   .005 TZORD  4
  -.003  -.018     .003   .015   .030   .033   .058   .056   .033   .053 TZORD  4
   .053                                                                  TZORD  4
  -.053  -.043    -.043  -.048  -.056  -.064  -.061  -.053  -.033   .008 TZORD  5
   .015  -.008     .005   .018   .030   .030   .058   .061   .036   .058 TZORD  5
   .051                                                                  TZORD  5
  -.104  -.053    -.043  -.051  -.053  -.061  -.061  -.053  -.030   .005 TZORD  6
   .018   .010     .023   .025   .043   .036   .061   .064   .036   .061 TZORD  6
   .061                                                                  TZORD  6
  -.053  -.043    -.043  -.048  -.053  -.064  -.058  -.051  -.028   .003 TZORD  7
   .015   .008     .028   .030   .033   .028   .066   .064   .033   .064 TZORD  7
   .064                                                                  TZORD  7
  -.056  -.048    -.046  -.048  -.056  -.061  -.058  -.051  -.033  -.010 TZORD  8
   .003   .013     .028   .030   .036   .028   .071   .066   .041   .081 TZORD  8
   .081                                                                  TZORD  8
  -.056  -.046    -.046  -.048  -.053  -.061  -.058  -.051  -.033  -.018 TZORD  9
  -.008   .008     .020   .015   .010   .015   .074   .081   .061   .124 TZORD  9
   .124                                                                  TZORD  9
  -.053  -.046    -.043  -.041  -.051  -.058  -.056  -.048  -.033  -.020 TZORD 10
  -.013   .005     .015   .008   .005  0.000   .010  -.008   .028   .084 TZORD 10
   .084                                                                  TZORD 10
```

TABLE III.- Continued

```
  -.053   -.046   -.043   -.041   -.051   -.058   -.056   -.048   -.036   -.023  TZORD 11
  -.013    .005    .010    .005    .003   -.003   -.003   -.030   -.025   -.005  TZORD 11
   .005                                                                         TZORD 11
  -.043   -.038   -.036   -.036   -.038   -.046   -.051   -.051   -.048   -.038  TZORD 12
  -.026   -.025   -.025   -.023   -.010   -.003   -.013   -.053   -.069   -.064  TZORD 12
   .064                                                                         TZORD 12
  -.033   -.028   -.025   -.023   -.028   -.036   -.043   -.048   -.048   -.046  TZORD 13
  -.041   -.038   -.036   -.038   -.025   -.015   -.036   -.066   -.074   -.064  TZORD 13
   .064                                                                         TZORD 13
  -.010   -.010   -.013   -.013   -.020   -.028   -.038   -.043   -.043   -.041  TZORD 14
  -.041   -.041   -.041   -.041   -.036   -.036   -.056   -.066   -.069   -.071  TZORD 14
   .071                                                                         TZORD 14
  -.005   -.005   -.008   -.008   -.010   -.020   -.025   -.033   -.036   -.038  TZORD 15
  -.041   -.043   -.043   -.043   -.043   -.051   -.058   -.058   -.064   -.076  TZORD 15
  -.076                                                                         TZORD 15
   .005   -.003   -.005   -.008   -.008   -.015   -.020   -.025   -.036   -.038  TZORD 16
  -.041   -.041   -.041   -.041   -.043   -.048   -.053   -.051   -.056   -.081  TZORD 16
  -.081                                                                         TZORD 16
  -.003   -.003   -.003   -.003   -.003   -.010   -.013   -.018   -.023   -.025  TZORD 17
  -.025   -.025   -.028   -.028   -.033   -.043   -.043   -.038   -.046   -.069  TZORD 17
  -.069                                                                         TZORD 17
   .003    .005    .005    .005    .005   0.000   -.005   -.005   -.008   -.010  TZORD 18
  -.010   -.013   -.015   -.018   -.025   -.028   -.028   -.023   -.030   -.043  TZORD 18
  -.025                                                                         TZORD 18
   .013    .015    .015    .018    .020    .023    .018    .018    .015    .010  TZORD 19
   .008    .005    .003   0.000   -.008   -.008   -.005   -.003   -.010   -.013  TZORD 19
  -.013                                                                         TZORD 19
   .043    .043    .043    .043    .043    .043    .046    .043    .043    .038  TZORD 20
   .036    .033    .030    .028    .030    .041    .028    .030    .038    .064  TZORD 20
   .064                                                                         TZORD 20
  0.000    .092    .110    .147    .252    .451    .645    .822   1.148   1.541  WAFORD 1
  1.914   2.232   2.528   2.810   3.218   3.478   3.687   3.743   3.737   3.582  WAFORD 1
3.582                                                                           WAFORD 1
  0.000    .077    .102    .158    .279    .493    .691    .909   1.192   1.574  WAFORD 2
  1.945   2.256   2.551   2.832   3.239   3.494   3.697   3.752   3.745   3.583  WAFORD 2
3.583                                                                           WAFORD 2
  0.000    .079    .107    .163    .283    .501    .699    .873   1.193   1.573  WAFORD 3
  1.946   2.261   2.561   2.838   3.240   3.499   3.694   3.747   3.740   3.579  WAFORD 3
3.579                                                                           WAFORD 3
  0.000    .074    .106    .162    .276    .497    .695    .869   1.180   1.503  WAFORD 4
  1.882   2.206   2.511   2.799   3.202   3.467   3.654   3.711   3.705   3.537  WAFORD 4
3.537                                                                           WAFORD 4
  0.000    .072    .105    .161    .282    .500    .695    .866   1.173   1.470  WAFORD 5
  1.764   2.118   2.435   2.729   3.139   3.410   3.597   3.645   3.642   3.458  WAFORD 5
3.458                                                                           WAFORD 5
  0.000    .091    .121    .168    .288    .507    .702    .873   1.180   1.460  WAFORD 6
  1.677   1.977   2.315   2.611   3.027   3.317   3.513   3.556   3.554   3.358  WAFORD 6
3.358                                                                           WAFORD 6
```

TABLE III.- Concluded

```
  0.000   .076   .110   .166   .284   .503   .694   .864  1.172  1.446  WAFORD 7
  1.647  1.872  2.135  2.436  2.888  3.194  3.379  3.422  3.422  3.234  WAFORD 7
3.234                                                                  WAFORD 7
  0.000   .077   .111   .168   .284   .502   .693   .863  1.172  1.434  WAFORD 8
  1.636  1.815  1.982  2.110  2.402  2.764  2.964  3.006  3.012  2.804  WAFORD 8
2.804                                                                  WAFORD 8
  0.000   .076   .111   .168   .285   .501   .690   .861  1.166  1.423  WAFORD 9
  1.626  1.805  1.963  2.078  2.148  2.172  2.218  2.250  2.258  2.042  WAFORD 9
2.042                                                                  WAFORD 9
  0.000   .076   .110   .165   .281   .497   .687   .856  1.161  1.417  WAFORD10
  1.620  1.799  1.958  2.071  2.132  2.080  1.879  1.549  1.227   .653  WAFORD10
.853                                                                   WAFORD10
  0.000   .076   .109   .169   .282   .497   .686   .856  1.160  1.414  WAFORD11
  1.620  1.796  1.956  2.069  2.130  2.076  1.853  1.475   .997   .292  WAFORD11
.292                                                                   WAFORD11
  0.000   .074   .107   .159   .274   .484   .669   .838  1.123  1.368  WAFORD12
  1.586  1.782  1.938  2.037  2.111  2.044  1.790  1.375   .786  0.0    WAFORD12
0.                                                                     WAFORD12
  0.000   .065   .095   .151   .262   .465   .649   .815  1.105  1.359  WAFORD13
  1.587  1.782  1.935  2.031  2.125  2.039  1.772  1.331   .724  0.0    WAFORD13
0.                                                                     WAFORD13
  0.000   .057   .085   .139   .254   .452   .639   .807  1.115  1.378  WAFORD14
  1.601  1.790  1.938  2.041  2.112  2.020  1.743  1.293   .687  0.0    WAFORD14
0.                                                                     WAFORD14
  0.000   .058   .085   .136   .245   .458   .644   .822  1.130  1.390  WAFORD15
  1.608  1.784  1.925  2.021  2.081  1.980  1.697  1.254   .661  0.0    WAFORD15
0.                                                                     WAFORD15
  0.000   .075   .108   .159   .266   .476   .670   .838  1.135  1.397  WAFORD16
  1.607  1.777  1.907  1.991  2.051  1.940  1.654  1.208   .637  0.0    WAFORD16
0.                                                                     WAFORD16
  0.000   .068   .101   .161   .283   .497   .677   .852  1.155  1.413  WAFORD17
  1.625  1.789  1.916  1.994  2.030  1.899  1.608  1.179   .619  0.0    WAFORD17
0.                                                                     WAFORD17
  0.000   .061   .091   .149   .276   .488   .688   .858  1.169  1.426  WAFORD18
  1.634  1.804  1.917  1.987  2.006  1.871  1.585  1.161   .642  0.0    WAFORD18
0.                                                                     WAFORD18
  0.000   .068   .101   .167   .318   .537   .721   .888  1.187  1.456  WAFORD19
  1.675  1.837  1.955  2.031  2.047  1.905  1.617  1.186   .643  0.0    WAFORD19
0.                                                                     WAFORD19
  0.000   .044   .065   .109   .215   .407   .572   .735  1.096  1.408  WAFORD20
  1.619  1.772  1.886  1.925  1.818  1.410  1.324   .959   .489  0.0    WAFORD20
0.                                                                     WAFORD20
```

TABLE IV.- NUMERICAL CONFIGURATION DATA FOR WING WITH 68° SWEEP,

$C_{L,des} = 0.1$

[See ref. 11]

1 1			20 21							
2045.16										REFA
0.0	0.5	.75	1.25	2.5	5.0	7.5	10.	15.	20.	XAF 10
25.	30.	35.	40.	50.	60.	70.	80.	90.	99.	XAF 20
100.										XAF 21
.003	0.000	0.000	72.283							WAFORG 1
.417	.216	0.000	71.869							WAFORG 2
.919	.432	0.000	71.361							WAFORG 3
1.448	.645	0.000	70.830							WAFORG 4
1.956	.864	0.000	70.317							WAFORG 5
2.489	1.080	0.000	69.769							WAFORG 6
3.033	1.293	0.000	69.212							WAFORG 7
4.155	1.725	0.000	68.049							WAFORG 8
5.273	2.159	0.000	66.860							WAFORG 9
6.281	2.535	0.000	65.763							WAFORG10
6.789	2.703	0.000	65.217							WAFORG11
13.907	5.413	0.000	57.942							WAFORG12
20.660	8.120	0.000	51.153							WAFORG13
27.371	10.820	0.000	44.409							WAFORG14
34.082	13.531	0.000	37.663							WAFORG15
41.092	16.391	0.000	30.592							WAFORG16
47.386	18.943	0.000	24.247							WAFORG17
54.000	21.646	0.000	17.590							WAFORG18
60.670	24.351	0.000	10.884							WAFORG19
66.980	26.848	0.000	4.519							WAFORG20
1.928	1.943	1.948	1.963	1.989	1.986	1.948	1.892	1.745	1.549	TZORD 1
1.344	1.158	.988	.815	.505	.206	-.010	-.102	-.056	.046	TZORD 1
.046										TZORD 1
1.935	1.951	1.956	1.969	1.984	1.969	1.928	1.877	1.730	1.537	TZORD 2
1.328	1.148	.975	.805	.498	.201	-.015	-.104	-.051	.048	TZORD 2
.048										TZORD 2
1.890	1.915	1.925	1.935	1.941	1.928	1.887	1.839	1.702	1.521	TZORD 3
1.318	1.140	.960	.795	.483	.193	-.018	-.104	-.046	.058	TZORD 3
.058										TZORD 3
1.867	1.864	1.862	1.862	1.864	1.857	1.826	1.781	1.661	1.494	TZORD 4
1.306	1.130	.953	.787	.470	.183	-.023	-.104	-.043	.061	TZORD 4
.061										TZORD 4
1.745	1.745	1.745	1.748	1.763	1.763	1.742	1.699	1.598	1.450	TZORD 5
1.283	1.113	.945	.782	.460	.178	-.028	-.104	-.043	.053	TZORD 5
.053										TZORD 5
1.605	1.613	1.615	1.623	1.636	1.643	1.626	1.595	1.511	1.387	TZORD 6
1.247	1.092	.940	.782	.455	.170	-.033	-.104	-.041	.071	TZORD 6
.071										TZORD 6
1.427	1.443	1.448	1.461	1.478	1.491	1.481	1.463	1.397	1.298	TZORD 7
1.181	1.046	.914	.770	.452	.157	-.038	-.099	-.033	.076	TZORD 7
.076										TZORD 7
1.036	1.039	1.039	1.041	1.052	1.087	1.110	1.120	1.105	1.059	TZORD 8
.989	.897	.808	.699	.432	.137	-.046	-.107	-.028	.089	TZORD 8
.089										TZORD 8
.505	.495	.490	.483	.505	.587	.648	.691	.732	.742	TZORD 9
.729	.678	.625	.546	.373	.127	-.038	-.107	-.023	.056	TZORD 9
.056										TZORD 9
.010	.008	.008	.008	.033	.132	.206	.267	.343	.399	TZORD 10
.437	.442	.424	.389	.325	.213	.117	.089	.201	.368	TZORD 10
.368										TZORD 10

TABLE IV.- Continued

-.191	-.193	-.196	-.193	-.152	-.056	.030	.089	.170	.246	TZORD 11
.307	.333	.333	.325	.305	.246	.203	.213	.328	.533	TZORD 11
.533										TZORD 11
-1.519	-1.504	-1.499	-1.483	-1.443	-1.356	-1.260	-1.156	-.958	-.757	TZORD 12
-.566	-.399	-.239	-.081	.196	.452	.714	.986	1.257	1.501	TZORD 12
1.501										TZORD 12
-1.280	-1.260	-1.250	-1.229	-1.179	-1.074	-.975	-.879	-.696	-.521	TZORD 13
-.353	-.193	-.036	.119	.414	.696	.963	1.227	1.504	1.773	TZORD 13
1.773										TZORD 13
-.762	-.747	-.739	-.721	-.681	-.602	-.523	-.442	-.290	-.137	TZORD 14
.005	.145	.290	.434	.716	.980	1.219	1.471	1.722	1.979	TZORD 14
1.979										TZORD 14
-.145	-.137	-.132	-.122	-.086	-.015	.053	.117	.244	.366	TZORD 15
.488	.610	.739	.866	1.107	1.334	1.542	1.768	1.994	2.233	TZORD 15
2.233										TZORD 15
.625	.625	.627	.638	.678	.737	.795	.853	.963	1.067	TZORD 16
1.173	1.275	1.377	1.473	1.664	1.847	2.029	2.220	2.390	2.563	TZORD 16
2.563										TZORD 16
1.458	1.455	1.455	1.458	1.478	1.529	1.570	1.613	1.699	1.786	TZORD 17
1.869	1.953	2.035	2.113	2.261	2.400	2.553	2.695	2.817	2.939	TZORD 17
2.939										TZORD 17
2.337	2.342	2.344	2.352	2.367	2.400	2.436	2.469	2.532	2.593	TZORD 18
2.652	2.710	2.766	2.824	2.934	3.040	3.142	3.231	3.315	3.366	TZORD 18
3.366										TZORD 18
3.282	3.284	3.284	3.287	3.292	3.312	3.327	3.348	3.386	3.424	TZORD 19
3.459	3.495	3.528	3.564	3.630	3.688	3.731	3.777	3.818	3.838	TZORD 19
3.838										TZORD 19
4.155	4.145	4.140	4.135	4.122	4.125	4.138	4.145	4.153	4.166	TZORD 20
4.171	4.181	4.188	4.199	4.216	4.237	4.249	4.257	4.262	4.272	TZORD 20
4.272										TZORD 20
0.000	.064	.095	.153	.254	.391	.551	.711	1.067	1.446	WAFORD 1
1.826	2.169	2.467	2.722	3.089	3.368	3.500	3.530	3.564	3.499	WAFORD 1
3.499										WAFORD 1
0.000	.081	.118	.181	.266	.412	.574	.737	1.099	1.483	WAFORD 2
1.866	2.206	2.504	2.750	3.108	3.377	3.501	3.532	3.572	3.502	WAFORD 2
3.502										WAFORD 2
0.000	.109	.149	.200	.257	.422	.580	.737	1.097	1.475	WAFORD 3
1.859	2.203	2.507	2.745	3.106	3.367	3.486	3.519	3.560	3.473	WAFORD 3
3.473										WAFORD 3
0.000	.069	.103	.164	.268	.421	.569	.726	1.074	1.433	WAFORD 4
1.818	2.160	2.470	2.705	3.071	3.334	3.444	3.480	3.519	3.438	WAFORD 4
3.438										WAFORD 4

TABLE IV.- Concluded

```
  0.000   .086   .124   .182   .259   .409   .545   .700  1.026  1.364  WAFORD 5
  1.737  2.079  2.385  2.618  2.997  3.258  3.369  3.406  3.445  3.355  WAFORD 5
3.355                                                                  WAFORD 5
  0.000   .064   .095   .154   .264   .394   .524   .669   .972  1.283  WAFORD 6
  1.637  1.975  2.272  2.496  2.885  3.154  3.264  3.298  3.342  3.261  WAFORD 6
3.261                                                                  WAFORD 6
  0.000   .083   .121   .184   .267   .383   .502   .635   .917  1.225  WAFORD 7
  1.547  1.864  2.145  2.359  2.724  2.997  3.114  3.142  3.191  3.105  WAFORD 7
3.105                                                                  WAFORD 7
  0.000   .080   .118   .181   .254   .341   .453   .570   .822  1.111  WAFORD 8
  1.411  1.696  1.932  2.109  2.355  2.538  2.641  2.663  2.732  2.656  WAFORD 8
2.656                                                                  WAFORD 8
  0.000   .066   .098   .154   .234   .335   .448   .552   .771  1.044  WAFORD 9
  1.328  1.600  1.809  1.942  2.089  2.043  1.951  1.897  1.899  1.896  WAFORD 9
1.896                                                                  WAFORD 9
  0.000   .060   .089   .144   .250   .378   .497   .596   .796  1.049  WAFORD10
  1.317  1.572  1.757  1.876  2.020  1.942  1.701  1.438  1.152   .611  WAFORD10
.611                                                                   WAFORD10
  0.000   .081   .119   .185   .274   .404   .514   .618   .824  1.079  WAFORD11
  1.334  1.579  1.751  1.863  2.008  1.938  1.687  1.346   .950   .295  WAFORD11
.295                                                                   WAFORD11
  0.000   .055   .082   .135   .249   .405   .557   .711  1.001  1.272  WAFORD12
  1.496  1.668  1.801  1.904  2.027  1.967  1.723  1.308   .764   .015  WAFORD12
0.0                                                                    WAFORD12
  0.000   .076   .112   .181   .310   .455   .610   .756  1.019  1.255  WAFORD13
  1.474  1.654  1.805  1.925  2.032  1.955  1.696  1.286   .748   .003  WAFORD13
0.0                                                                    WAFORD13
  0.000   .076   .112   .179   .298   .445   .599   .745  1.020  1.280  WAFORD14
  1.492  1.677  1.830  1.935  2.001  1.918  1.670  1.270   .740  -.017  WAFORD14
0.0                                                                    WAFORD14
  0.000   .103   .145   .204   .286   .476   .638   .782  1.048  1.288  WAFORD15
  1.499  1.679  1.818  1.912  1.988  1.912  1.680  1.277   .750  -.024  WAFORD15
0.0                                                                    WAFORD15
  0.000   .100   .143   .211   .313   .469   .616   .762  1.022  1.250  WAFORD16
  1.461  1.634  1.781  1.886  1.989  1.922  1.660  1.235   .699   .023  WAFORD16
0.0                                                                    WAFORD16
  0.000   .107   .158   .247   .391   .554   .690   .811  1.044  1.259  WAFORD17
  1.441  1.605  1.749  1.860  1.975  1.924  1.655  1.246   .686   .029  WAFORD17
0.0                                                                    WAFORD17
  0.000   .091   .137   .225   .425   .665   .760   .872  1.085  1.255  WAFORD18
  1.422  1.559  1.675  1.782  1.930  1.935  1.713  1.274   .730   .186  WAFORD18
0.0                                                                    WAFORD18
  0.000   .126   .188   .307   .552   .756   .879   .993  1.189  1.377  WAFORD19
  1.538  1.675  1.773  1.864  1.985  2.000  1.774  1.340   .804  -.070  WAFORD19
0.0                                                                    WAFORD19
  0.000   .287   .425   .676  1.105  1.321  1.279  1.340  1.542  1.608  WAFORD20
  1.692  1.676  1.756  1.843  1.886  1.886  1.720  1.462  1.267   .155  WAFORD20
0.0                                                                    WAFORD20
```

TABLE V.- NUMERICAL CONFIGURATION DATA FOR WING WITH 55° SWEEP,

$C_{L,des} = 0.0$

[See ref. 11]

```
  1  1                    20 20
2045.16                                                                  REFA
0.      .5      .75     1.25    2.5     5.      7.5     10.     15.     20.      XAF   10
25.     30.     35.     40.     50.     60.     70.     80.     90.     100.     XAF   20
  0.000   0.000   0.000  54.130                                                   WAFORG 1
   .259    .216   0.000  53.906                                                   WAFORG 2
   .546    .432   0.000  53.617                                                   WAFORG 3
   .856    .648   0.000  53.320                                                   WAFORG 4
  1.130    .864   0.000  53.043                                                   WAFORG 5
  1.466   1.080   0.000  52.695                                                   WAFORG 6
  1.991   1.448   0.000  52.169                                                   WAFORG 7
  2.393   1.727   0.000  51.768                                                   WAFORG 8
  3.018   2.159   0.000  51.145                                                   WAFORG 9
  3.564   2.540   0.000  50.597                                                   WAFORG10
  4.930   3.495   0.000  49.218                                                   WAFORG11
  9.898   6.988   0.000  44.219                                                   WAFORG12
 14.856  10.478   0.000  39.273                                                   WAFORG13
 19.820  13.975   0.000  34.315                                                   WAFORG14
 24.869  17.473   0.000  29.279                                                   WAFORG15
 29.873  20.963   0.000  24.280                                                   WAFORG16
 34.877  24.458   0.000  19.274                                                   WAFORG17
 39.888  27.953   0.000  14.252                                                   WAFORG18
 44.935  31.445   0.000   9.187                                                   WAFORG19
 49.977  34.940   0.000   4.128                                                   WAFORG20
  -.023   -.025   -.030   -.030   -.023   -.036   -.051   -.076   -.097   -.104  TZORD  1
  -.112   -.119   -.117   -.112   -.102   -.094   -.084   -.074   -.058   -.046  TZORD  1
  -.046   -.041   -.036   -.030   -.028   -.046   -.061   -.084   -.112   -.122  TZORD  2
  -.130   -.132   -.127   -.122   -.112   -.102   -.089   -.079   -.061   -.048  TZORD  2
  -.036   -.030   -.030   -.025   -.030   -.048   -.066   -.081   -.114   -.137  TZORD  3
  -.145   -.145   -.137   -.132   -.117   -.107   -.094   -.081   -.064   -.053  TZORD  3
  -.033   -.028   -.028   -.028   -.033   -.053   -.069   -.081   -.099   -.127  TZORD  4
  -.145   -.157   -.152   -.142   -.124   -.112   -.099   -.084   -.064   -.061  TZORD  4
  -.010   -.020   -.023   -.028   -.036   -.053   -.069   -.081   -.094   -.104  TZORD  5
  -.122   -.147   -.160   -.155   -.132   -.114   -.102   -.086   -.061   -.051  TZORD  5
  -.028   -.020   -.025   -.030   -.038   -.058   -.071   -.081   -.094   -.099  TZORD  6
  -.107   -.124   -.147   -.165   -.147   -.124   -.104   -.089   -.061   -.069  TZORD  6
  -.028   -.023   -.028   -.033   -.043   -.061   -.076   -.084   -.094   -.097  TZORD  7
  -.104   -.109   -.107   -.130   -.170   -.147   -.114   -.099   -.069   -.086  TZORD  7
  -.036   -.025   -.028   -.033   -.046   -.066   -.079   -.089   -.097   -.097  TZORD  8
  -.104   -.109   -.107   -.117   -.135   -.157   -.137   -.109   -.076   -.102  TZORD  8
  -.015   -.023   -.028   -.036   -.049   -.071   -.084   -.091   -.099   -.099  TZORD  9
  -.107   -.109   -.112   -.122   -.119   -.117   -.127   -.137   -.112   -.069  TZORD  9
```

TABLE V.- Continued

-.018	-.030	-.036	-.041	-.051	-.076	-.089	-.097	-.102	-.102	TZORD 10
-.107	-.112	-.114	-.122	-.122	-.119	-.119	-.109	-.084	-.030	TZORD 10
-.043	-.038	-.043	-.048	-.064	-.086	-.099	-.104	-.104	-.107	TZORD 11
-.112	-.117	-.119	-.124	-.124	-.122	-.130	-.127	-.112	-.076	TZORD 11
-.097	-.089	-.086	-.084	-.089	-.099	-.102	-.104	-.109	-.109	TZORD 12
-.109	-.114	-.119	-.127	-.124	-.117	-.119	-.117	-.119	-.099	TZORD 12
-.094	-.086	-.084	-.081	-.091	-.099	-.107	-.109	-.112	-.107	TZORD 13
-.104	-.109	-.114	-.117	-.112	-.104	-.102	-.104	-.114	-.084	TZORD 13
-.130	-.114	-.112	-.114	-.114	-.114	-.114	-.114	-.112	-.112	TZORD 14
-.112	-.109	-.109	-.109	-.104	-.104	-.102	-.102	-.099	-.086	TZORD 14
-.142	-.117	-.109	-.107	-.112	-.112	-.114	-.114	-.112	-.109	TZORD 15
-.107	-.104	-.104	-.104	-.102	-.099	-.094	-.099	-.097	-.086	TZORD 15
-.112	-.086	-.089	-.091	-.091	-.094	-.097	-.097	-.099	-.102	TZORD 16
-.102	-.099	-.097	-.091	-.084	-.084	-.089	-.099	-.102	-.097	TZORD 16
-.094	-.074	-.074	-.076	-.079	-.081	-.084	-.086	-.089	-.091	TZORD 17
-.089	-.086	-.084	-.081	-.079	-.081	-.086	-.091	-.097	-.086	TZORD 17
-.081	-.071	-.069	-.069	-.074	-.074	-.076	-.076	-.081	-.081	TZORD 18
-.084	-.084	-.084	-.084	-.079	-.076	-.071	-.069	-.066	-.056	TZORD 18
-.094	-.079	-.074	-.074	-.071	-.069	-.071	-.071	-.074	-.074	TZORD 19
-.074	-.074	-.071	-.069	-.064	-.053	-.041	-.030	-.015	.003	TZORD 19
-.076	-.064	-.058	-.051	-.048	-.048	-.046	-.041	-.036	-.033	TZORD 20
-.028	-.025	-.023	-.018	-.013	-.008	-.008	-.008	-.005	-.005	TZORD 20
0.000	.077	.104	.145	.261	.458	.627	.800	1.193	1.588	WAFORD 1
1.983	2.365	2.729	3.071	3.652	4.052	4.357	4.562	4.670	4.694	WAFORD 1
0.000	.061	.099	.142	.259	.464	.634	.798	1.171	1.566	WAFORD 2
1.953	2.333	2.709	3.051	3.641	4.048	4.352	4.560	4.666	4.686	WAFORD 2
0.000	.066	.096	.146	.257	.460	.627	.776	1.114	1.485	WAFORD 3
1.864	2.244	2.640	2.996	3.602	4.011	4.318	4.529	4.637	4.658	WAFORD 3
0.000	.065	.095	.145	.254	.455	.621	.767	1.058	1.378	WAFORD 4
1.721	2.098	2.508	2.889	3.514	3.934	4.246	4.463	4.574	4.554	WAFORD 4
0.000	.060	.088	.136	.244	.445	.613	.757	1.036	1.300	WAFORD 5
1.574	1.892	2.282	2.695	3.359	3.797	4.121	4.343	4.456	4.439	WAFORD 5
0.000	.075	.096	.141	.248	.448	.617	.765	1.041	1.287	WAFORD 6
1.509	1.740	2.054	2.436	3.145	3.617	3.953	4.195	4.311	4.315	WAFORD 6
0.000	.075	.096	.142	.246	.444	.615	.763	1.044	1.289	WAFORD 7
1.496	1.652	1.809	2.019	2.591	3.140	3.532	3.801	3.933	3.903	WAFORD 7
0.000	.078	.101	.143	.246	.443	.613	.763	1.044	1.288	WAFORD 8
1.498	1.654	1.786	1.910	2.174	2.601	3.040	3.348	3.507	3.460	WAFORD 8
0.000	.066	.093	.141	.244	.439	.609	.761	1.042	1.287	WAFORD 9
1.498	1.664	1.797	1.902	1.997	2.002	2.034	2.247	2.438	2.524	WAFORD 9
0.000	.078	.105	.146	.241	.436	.605	.757	1.037	1.287	WAFORD10
1.502	1.674	1.807	1.910	1.999	1.932	1.720	1.436	1.125	.698	WAFORD10

TABLE V.- Concluded

0.000	.076	.099	.140	.239	.426	.592	.744	1.029	1.284	WAFORD11
1.509	1.693	1.828	1.922	2.001	1.937	1.684	1.278	.741	0.0	WAFORD11
0.000	.063	.093	.146	.238	.405	.573	.727	1.017	1.285	WAFORD12
1.515	1.702	1.836	1.933	2.015	1.956	1.721	1.300	.787	0.0	WAFORD12
0.000	.067	.097	.146	.230	.402	.573	.731	1.024	1.278	WAFORD13
1.508	1.699	1.832	1.925	2.013	1.962	1.717	1.310	.794	0.0	WAFORD13
0.000	.098	.134	.175	.265	.430	.583	.732	1.012	1.274	WAFORD14
1.515	1.708	1.846	1.934	2.014	1.961	1.702	1.310	.795	0.0	WAFORD14
0.000	.121	.166	.216	.284	.452	.603	.754	1.052	1.323	WAFORD15
1.547	1.714	1.837	1.932	2.025	1.942	1.695	1.320	.819	0.0	WAFORD15
0.000	.142	.155	.192	.284	.457	.614	.765	1.046	1.301	WAFORD16
1.519	1.704	1.846	1.948	2.022	1.931	1.696	1.338	.821	0.0	WAFORD16
0.000	.148	.171	.202	.290	.453	.607	.752	1.031	1.287	WAFORD17
1.520	1.706	1.841	1.939	1.995	1.906	1.681	1.291	.753	0.0	WAFORD17
0.000	.127	.174	.225	.291	.451	.610	.756	1.023	1.267	WAFORD18
1.482	1.650	1.788	1.884	1.975	1.922	1.699	1.315	.777	0.0	WAFORD18
0.000	.187	.221	.228	.290	.445	.605	.742	1.005	1.260	WAFORD19
1.478	1.684	1.845	1.977	2.127	2.091	1.863	1.432	.892	0.0	WAFORD19
0.000	.308	.437	.617	.716	.708	.859	.993	1.175	1.396	WAFORD20
1.531	1.658	1.782	1.901	2.046	2.061	1.781	1.419	.850	0.0	WAFORD20

TABLE VI.- NUMERICAL CONFIGURATION DATA FOR WING WITH 55° SWEEP,

$C_{L,des} = 0.1$

[See ref. 11]

```
  1  1                  20 20
2045.16                                                                  REFA
0.      .5      .75     1.25    2.5     5.      7.5     10.     15.     20.      XAF   10
25.     30.     35.     40.     50.     60.     70.     80.     90.     100.     XAF   20
  0.000   0.000   0.000 54.529                                                   WAFORG 1
   .295    .216   0.000 54.224                                                   WAFORG 2
   .597    .432   0.000 53.917                                                   WAFORG 3
   .907    .648   0.000 53.612                                                   WAFORG 4
  1.219    .864   0.000 53.299                                                   WAFORG 5
  1.537   1.080   0.000 52.982                                                   WAFORG 6
  2.065   1.448   0.000 52.448                                                   WAFORG 7
  2.469   1.727   0.000 52.045                                                   WAFORG 8
  3.104   2.159   0.000 51.372                                                   WAFORG 9
  3.665   2.540   0.000 50.785                                                   WAFORG10
  5.032   3.495   0.000 49.329                                                   WAFORG11
 10.066   6.988   0.000 44.232                                                   WAFORG12
 15.098  10.483   0.000 39.210                                                   WAFORG13
 20.089  13.975   0.000 34.224                                                   WAFORG14
 25.070  17.470   0.000 29.258                                                   WAFORG15
 30.061  20.963   0.000 24.239                                                   WAFORG16
 35.016  24.458   0.000 19.261                                                   WAFORG17
 39.995  27.950   0.000 14.232                                                   WAFORG18
 44.961  31.445   0.000  9.220                                                   WAFORG19
 49.903  34.940   0.000  4.209                                                   WAFORG20
   .079    .076    .079    .089    .114    .168    .203    .213    .198    .185  TZORD  1
   .142    .076    .020   -.010   -.048   -.104   -.135   -.140   -.071    .071  TZORD  1
   .076    .099    .104    .109    .132    .183    .203    .203    .191    .180  TZORD  2
   .140    .071    .018   -.013   -.053   -.107   -.137   -.142   -.074    .066  TZORD  2
   .081    .084    .089    .104    .127    .155    .165    .175    .178    .170  TZORD  3
   .135    .064    .018   -.013   -.048   -.107   -.137   -.145   -.076    .071  TZORD  3
   .056    .058    .064    .076    .099    .124    .132    .127    .132    .137  TZORD  4
   .117    .058    .010   -.015   -.053   -.107   -.137   -.147   -.079    .066  TZORD  4
   .033    .033    .038    .046    .069    .094    .104    .102    .089    .089  TZORD  5
   .081    .038   0.000   -.020   -.058   -.112   -.142   -.152   -.084    .069  TZORD  5
  -.008    .003    .005    .013    .033    .061    .079    .079    .071    .058  TZORD  6
   .033   -.003   -.023   -.030   -.064   -.117   -.145   -.155   -.089    .074  TZORD  6
  -.048   -.058   -.053   -.043   -.028    .010    .036    .046    .051    .043  TZORD  7
   .020   -.041   -.102   -.117   -.086   -.124   -.142   -.155   -.086    .066  TZORD  7
  -.056   -.102   -.094   -.084   -.069   -.025    .008    .023    .036    .033  TZORD  8
   .015   -.033   -.097   -.152   -.168   -.147   -.142   -.155   -.084    .069  TZORD  8
  -.145   -.155   -.155   -.155   -.127   -.076   -.038   -.013    .015    .020  TZORD  9
 0.000    -.048   -.102   -.155   -.234   -.279   -.259   -.193   -.099    .076  TZORD  9
  -.201   -.213   -.206   -.198   -.175   -.117   -.079   -.043   -.008    .008  TZORD 10
  -.020   -.061   -.107   -.150   -.229   -.282   -.307   -.272   -.213    .013  TZORD 10
  -.320   -.330   -.328   -.312   -.279   -.221   -.170   -.132   -.079   -.058  TZORD 11
  -.071   -.089   -.112   -.124   -.165   -.180   -.165   -.127   -.038    .109  TZORD 11
  -.561   -.579   -.579   -.566   -.549   -.511   -.470   -.427   -.348   -.262  TZORD 12
  -.173   -.094   -.020    .064    .203    .323    .432    .528    .612    .691  TZORD 12
  -.437   -.429   -.419   -.409   -.378   -.328   -.287   -.244   -.173   -.112  TZORD 13
  -.046    .030    .099    .168    .282    .378    .475    .569    .643    .726  TZORD 13
  -.229   -.216   -.211   -.203   -.188   -.157   -.130   -.104   -.048   -.003  TZORD 14
   .046    .097    .145    .185    .262    .340    .419    .480    .559    .648  TZORD 14
```

TABLE VI.- Concluded

-.038	-.030	-.030	-.030	-.028	-.018	-.003	.015	.058	.097	TZORD 15
.137	.168	.201	.234	.312	.373	.417	.465	.508	.566	TZORD 15
.513	.516	.518	.521	.523	.533	.544	.554	.579	.602	TZORD 16
.627	.653	.671	.686	.714	.749	.777	.792	.820	.881	TZORD 16
1.041	1.049	1.054	1.057	1.054	1.064	1.072	1.082	1.100	1.118	TZORD 17
1.133	1.151	1.168	1.184	1.204	1.207	1.214	1.229	1.240	1.285	TZORD 17
1.544	1.570	1.575	1.575	1.577	1.585	1.593	1.600	1.621	1.641	TZORD 18
1.659	1.674	1.687	1.694	1.702	1.699	1.694	1.681	1.684	1.689	TZORD 18
2.073	2.093	2.098	2.106	2.106	2.113	2.116	2.118	2.123	2.126	TZORD 19
2.129	2.131	2.131	2.134	2.131	2.121	2.113	2.108	2.118	2.118	TZORD 19
2.631	2.631	2.634	2.634	2.634	2.634	2.631	2.624	2.616	2.611	TZORD 20
2.606	2.601	2.598	2.591	2.581	2.576	2.578	2.593	2.596	2.593	TZORD 20
0.000	.068	.102	.160	.286	.525	.746	.938	1.301	1.666	WAFORD 1
2.020	2.361	2.708	3.059	3.641	4.079	4.365	4.576	4.715	4.621	WAFORD 1
0.000	.078	.110	.171	.309	.543	.755	.959	1.333	1.691	WAFORD 2
2.035	2.376	2.724	3.070	3.640	4.090	4.373	4.586	4.726	4.657	WAFORD 2
0.000	.068	.091	.127	.229	.423	.622	.844	1.260	1.631	WAFORD 3
1.970	2.322	2.678	3.021	3.612	4.054	4.344	4.561	4.700	4.637	WAFORD 3
0.000	.059	.085	.132	.225	.383	.537	.706	1.101	1.489	WAFORD 4
1.839	2.200	2.572	2.922	3.526	3.973	4.271	4.496	4.644	4.579	WAFORD 4
0.000	.063	.089	.134	.227	.376	.513	.662	1.006	1.337	WAFORD 5
1.663	2.015	2.394	2.758	3.384	3.848	4.163	4.386	4.541	4.495	WAFORD 5
0.000	.060	.087	.134	.224	.369	.506	.658	.978	1.253	WAFORD 6
1.490	1.802	2.148	2.519	3.176	3.667	3.998	4.234	4.394	4.361	WAFORD 6
0.000	.052	.083	.127	.206	.358	.508	.666	.972	1.210	WAFORD 7
1.406	1.600	1.786	2.045	2.695	3.208	3.579	3.843	4.027	4.012	WAFORD 7
0.000	.028	.056	.121	.188	.339	.503	.667	.969	1.201	WAFORD 8
1.395	1.588	1.734	1.860	2.265	2.743	3.092	3.400	3.608	3.619	WAFORD 8
0.000	.035	.056	.096	.185	.339	.509	.668	.963	1.213	WAFORD 9
1.408	1.604	1.745	1.850	1.963	2.055	2.149	2.375	2.646	2.612	WAFORD 9
0.000	.026	.063	.106	.187	.344	.514	.666	.954	1.215	WAFORD10
1.424	1.612	1.754	1.863	1.947	1.903	1.808	1.541	1.373	.953	WAFORD10
0.000	.024	.048	.101	.190	.345	.495	.646	.944	1.210	WAFORD11
1.447	1.638	1.784	1.867	1.957	1.867	1.654	1.219	.712	0.0	WAFORD11
0.000	.012	.035	.056	.139	.306	.479	.654	.970	1.227	WAFORD12
1.463	1.641	1.776	1.883	1.993	1.925	1.722	1.286	.769	0.0	WAFORD12
0.000	.028	.061	.096	.174	.315	.455	.601	.915	1.206	WAFORD13
1.437	1.624	1.775	1.887	1.965	1.928	1.708	1.304	.766	0.0	WAFORD13
0.000	.062	.089	.135	.218	.370	.512	.656	.939	1.219	WAFORD14
1.438	1.621	1.779	1.880	2.017	1.922	1.640	1.285	.723	0.0	WAFORD14
0.000	.067	.091	.135	.228	.374	.524	.678	.959	1.219	WAFORD15
1.460	1.653	1.832	1.980	2.068	1.951	1.731	1.344	.846	0.0	WAFORD15
0.000	.055	.078	.119	.200	.353	.503	.655	.933	1.191	WAFORD16
1.420	1.611	1.760	1.878	1.950	1.889	1.697	1.344	.791	0.0	WAFORD16
0.000	.103	.145	.210	.315	.477	.622	.771	1.026	1.247	WAFORD17
1.456	1.621	1.756	1.868	1.942	1.835	1.644	1.321	.815	0.0	WAFORD17
0.000	.212	.263	.301	.403	.575	.716	.847	1.127	1.375	WAFORD18
1.563	1.723	1.842	1.928	2.008	1.988	1.835	1.448	.960	0.0	WAFORD18
0.000	.251	.338	.430	.504	.705	.849	.977	1.207	1.405	WAFORD19
1.609	1.785	1.916	2.034	2.165	2.141	1.954	1.634	1.201	0.0	WAFORD19
0.000	.108	.162	.268	.529	.994	1.338	1.560	1.816	2.033	WAFORD20
2.294	2.506	2.634	2.829	3.039	3.112	2.797	1.965	1.044	0.0	WAFORD20

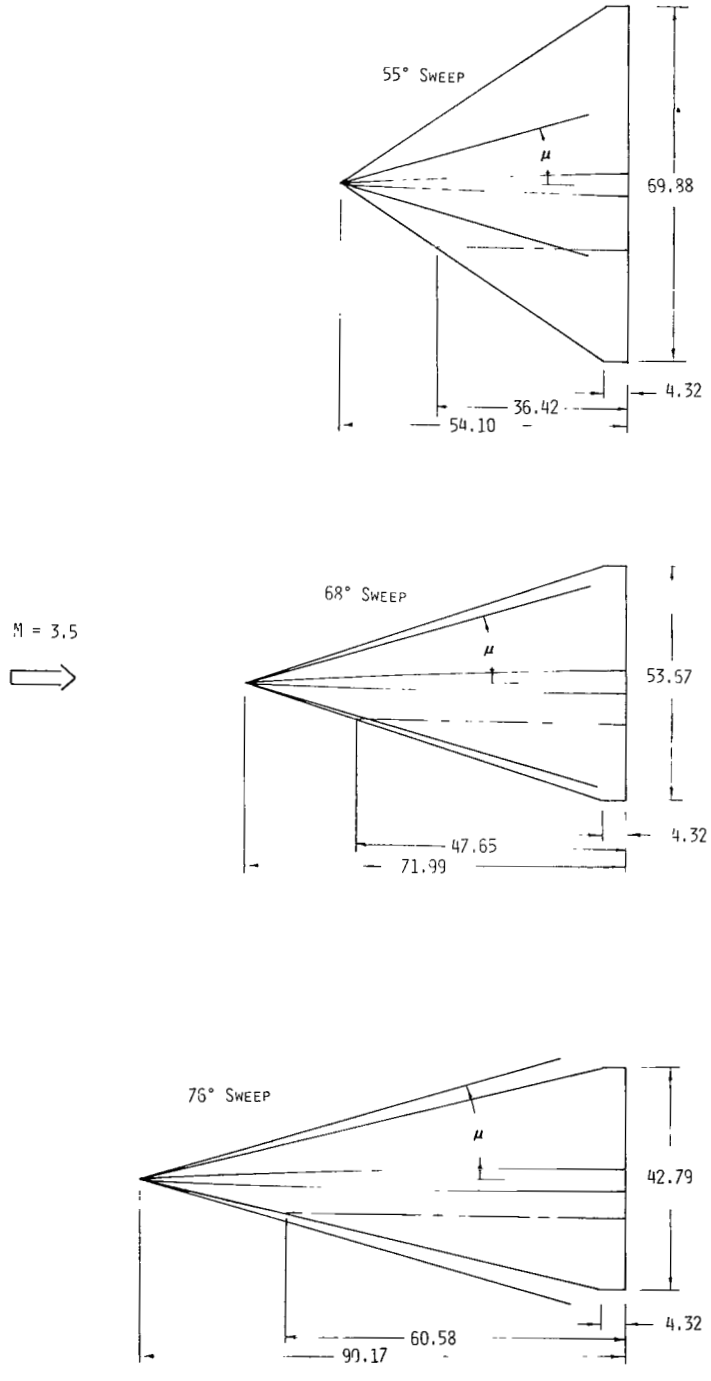
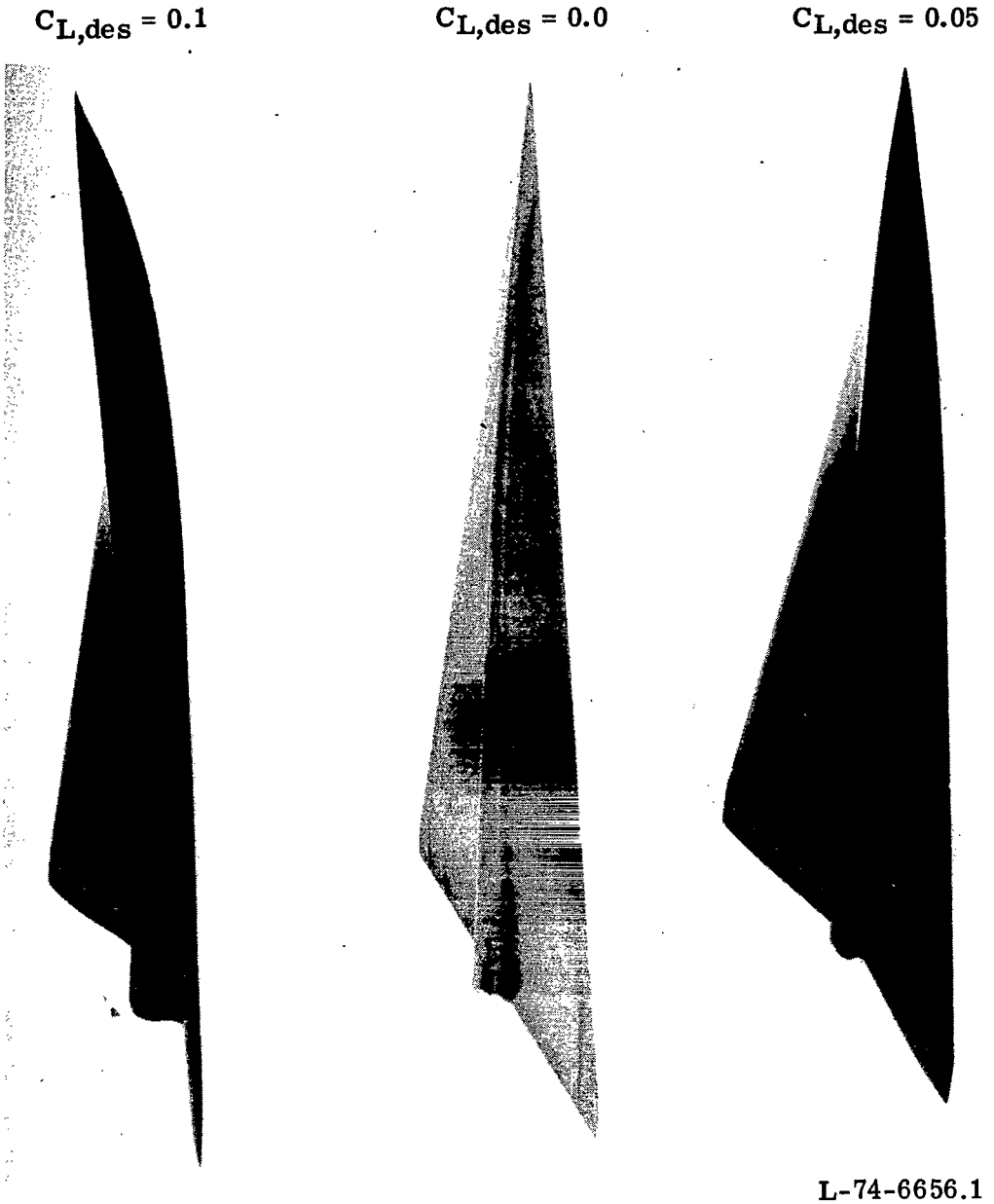


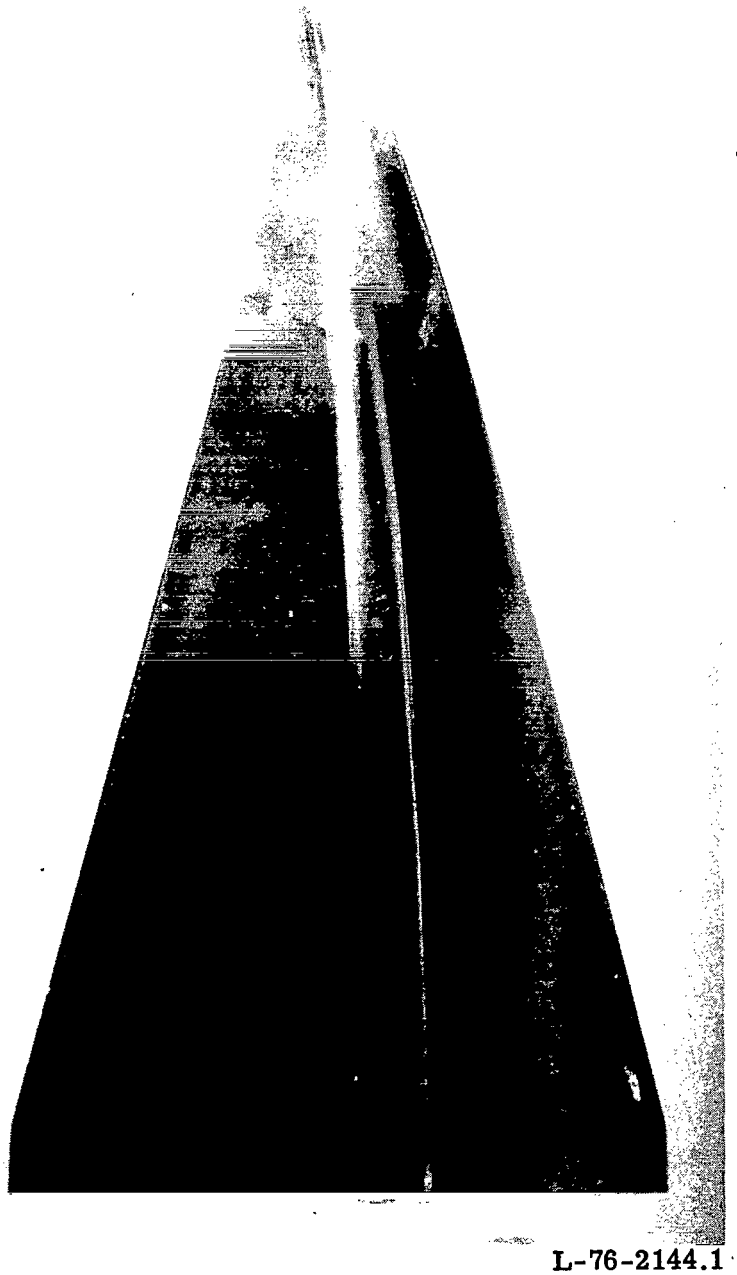
Figure 1.- Model planforms. All dimensions are in cm.



(a) 76° sweep (upper surface).

Figure 2.- Photographs of the models.

$C_{L,des} = 0.1$

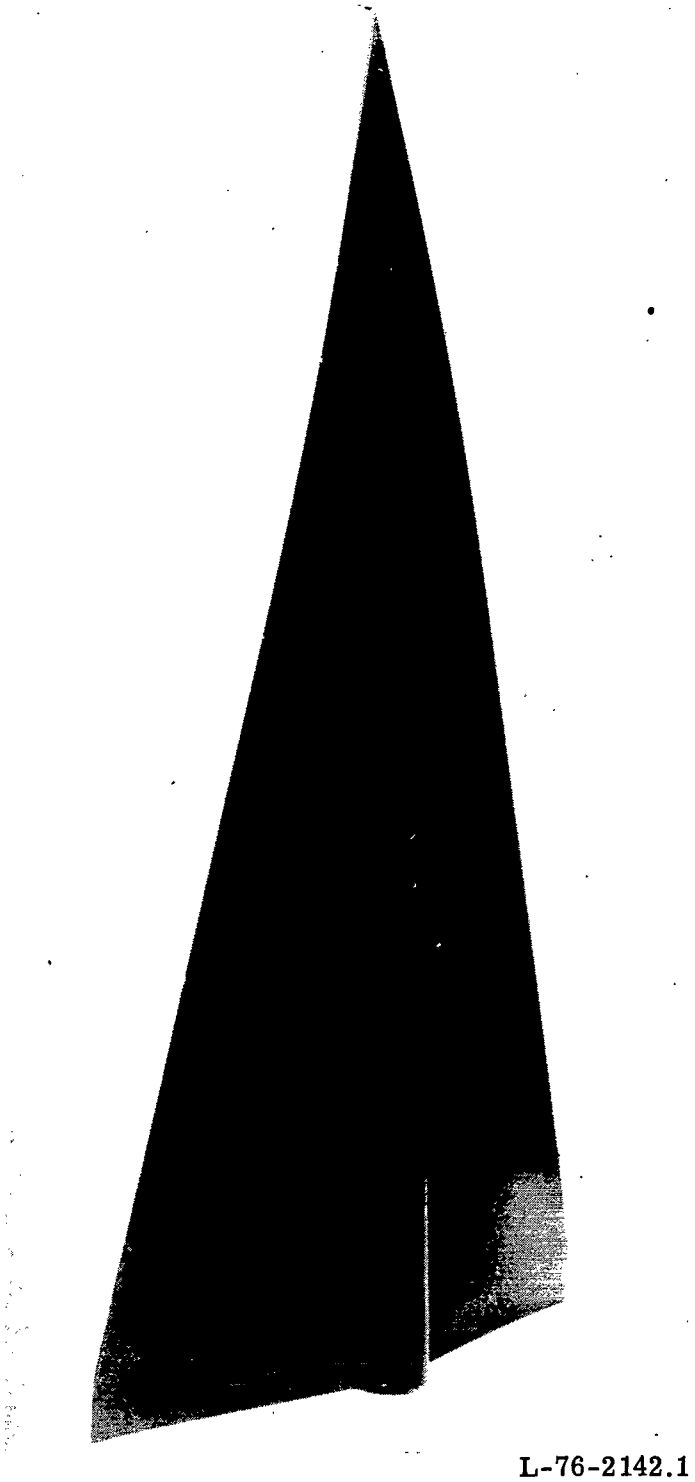


L-76-2144.1

(b) 76° sweep (lower surface).

Figure 2.- Continued.

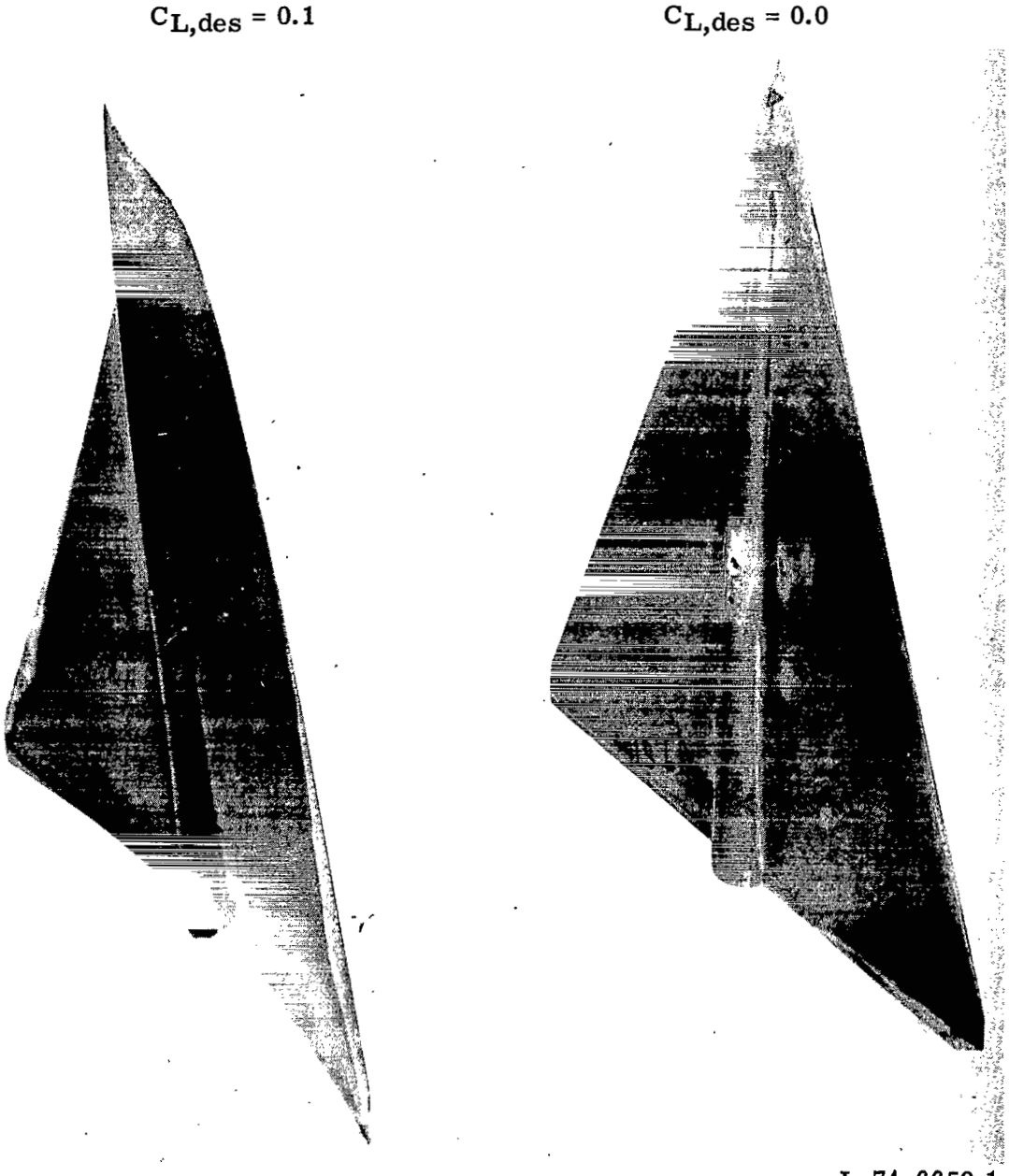
$C_{L,des} = 0.05$



L-76-2142.1

(b) Concluded.

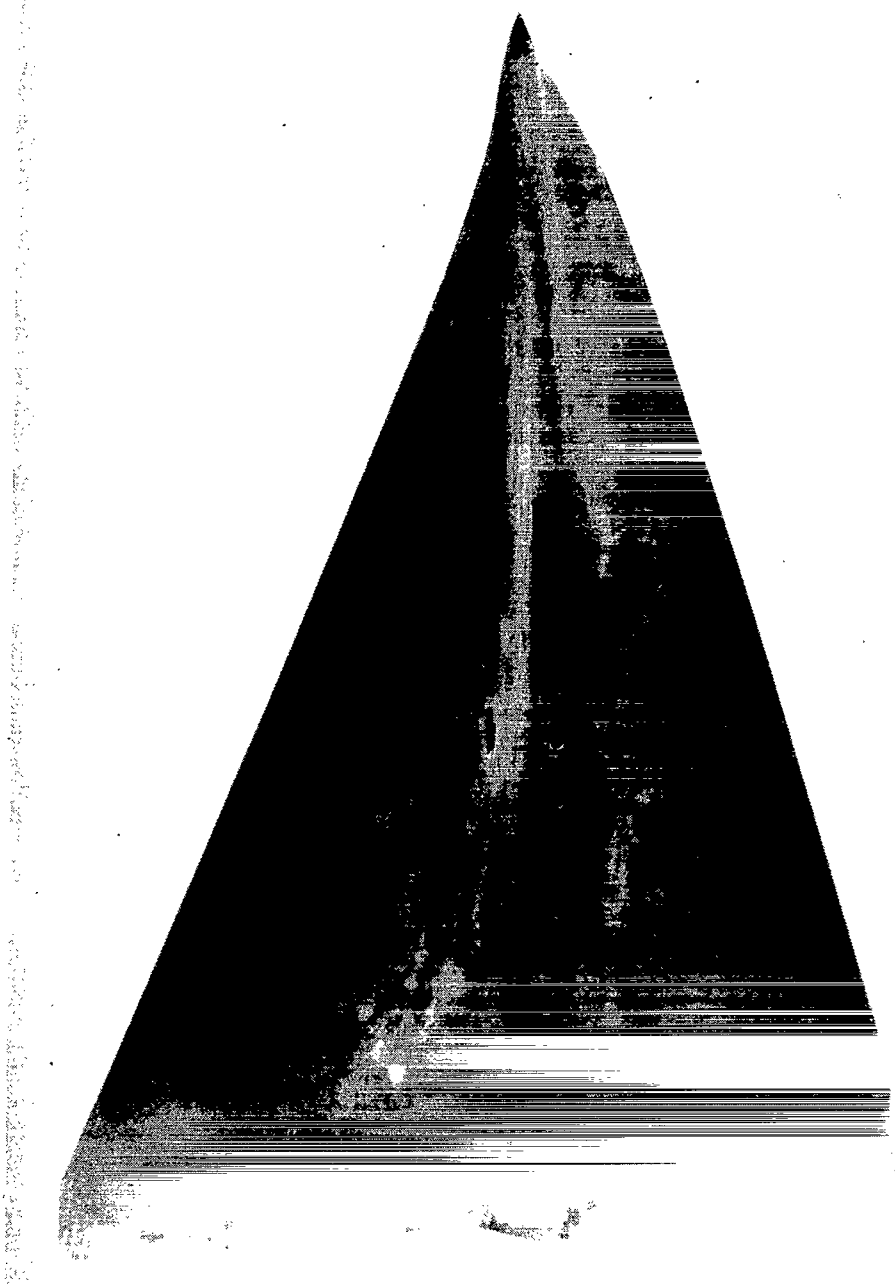
Figure 2.- Continued.



(c) 68° sweep (upper surface).

Figure 2.- Continued.

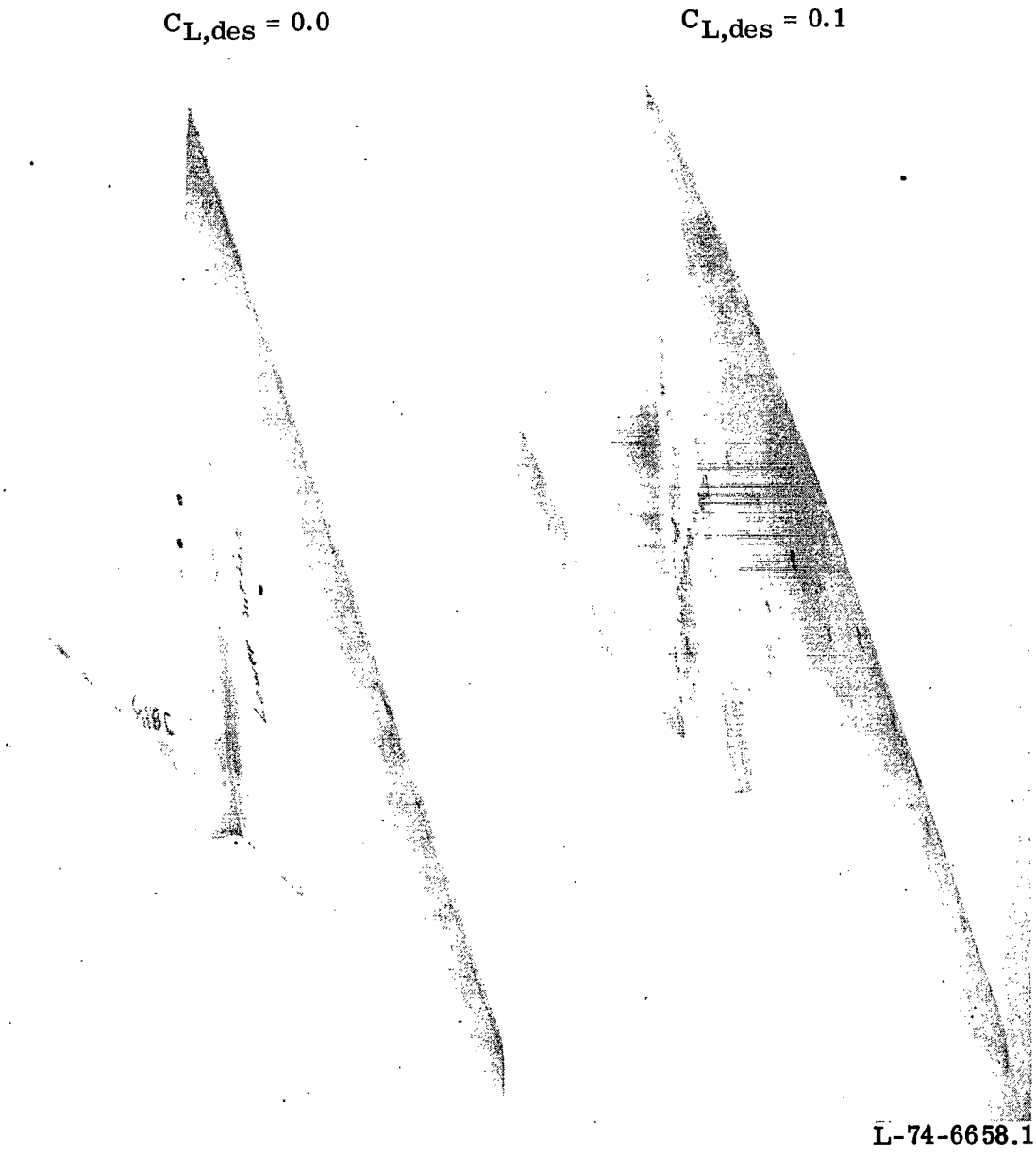
$C_{L,des} = 0.1$



L-76-2141.1

(d) 68° sweep (lower surface).

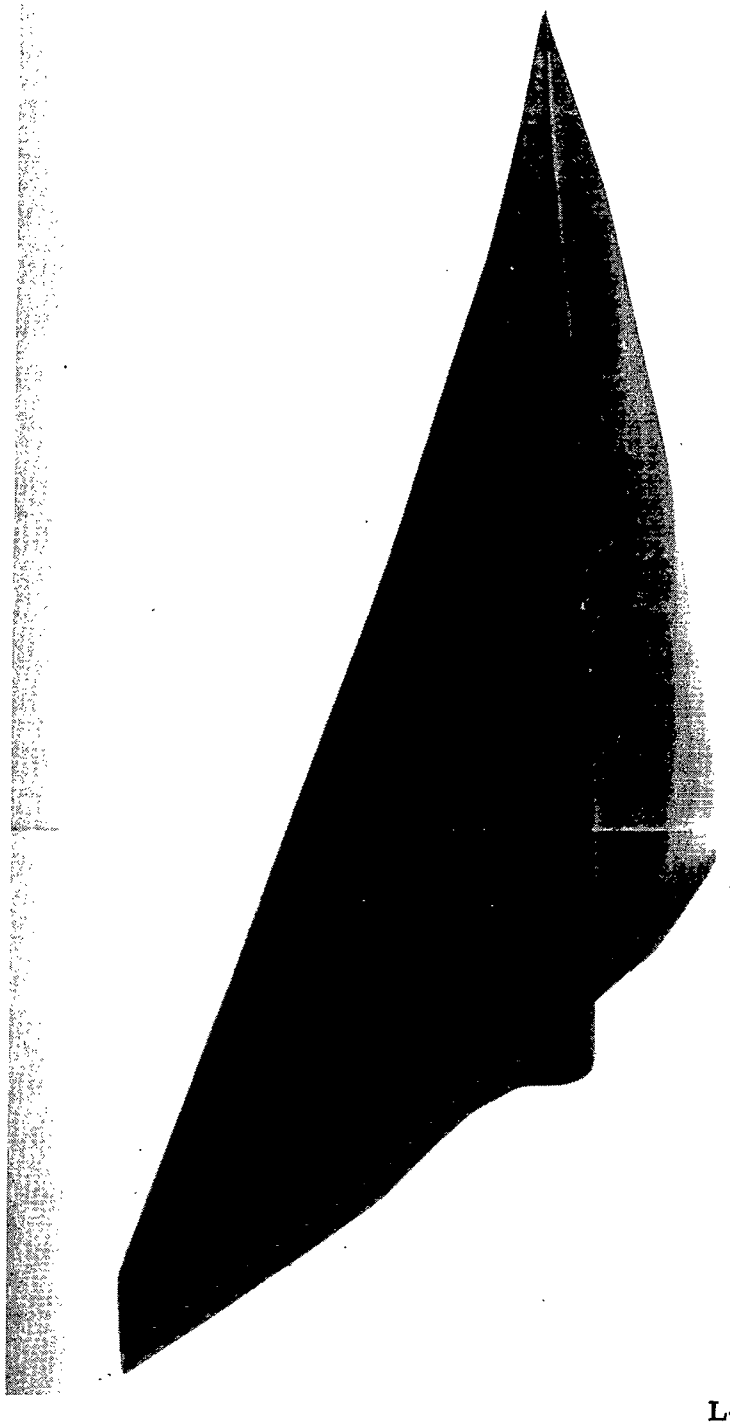
Figure 2.- Continued.



(e) 55° sweep (upper surface).

Figure 2.- Continued.

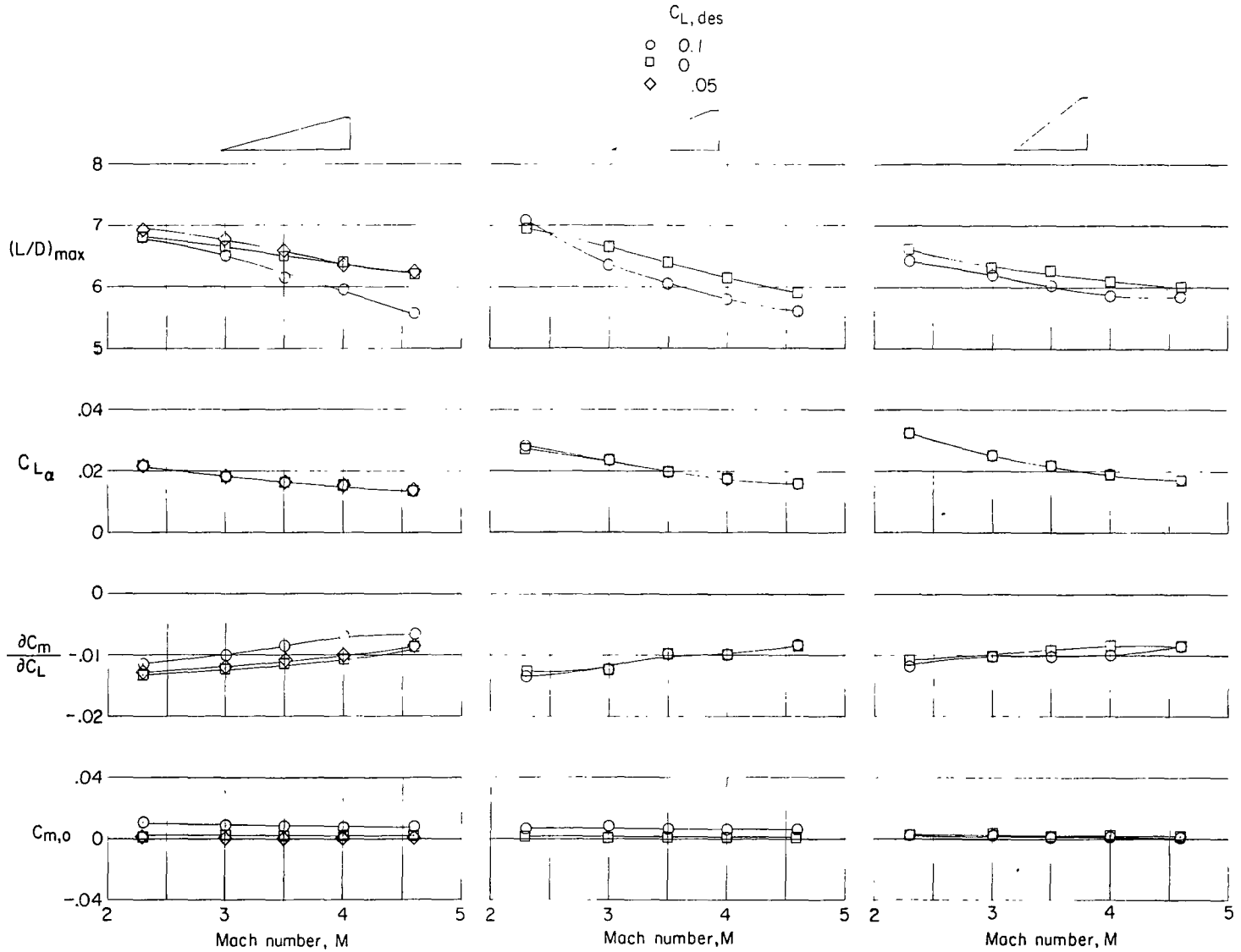
$C_{L,des} = 0.1$



L-76-2143.1

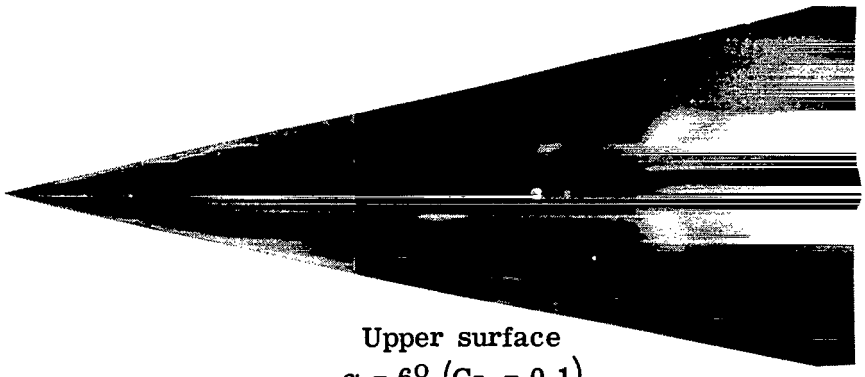
(f) 55^{o} sweep (lower surface).

Figure 2.- Concluded.

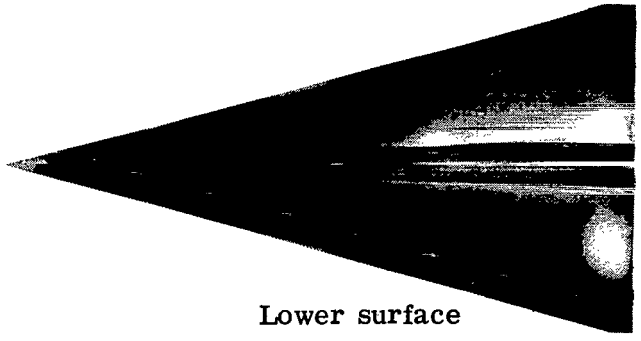


(a) $\Lambda = 76^o$. (b) $\Lambda = 68^o$. (c) $\Lambda = 55^o$.

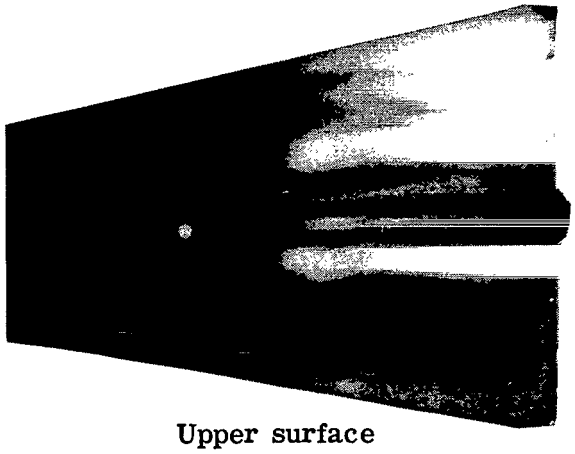
Figure 3.- Summary of longitudinal aerodynamic characteristics.



Upper surface
$\alpha = 6^{o}$ $(C_L = 0.1)$



Lower surface
$\alpha = 6^{o}$

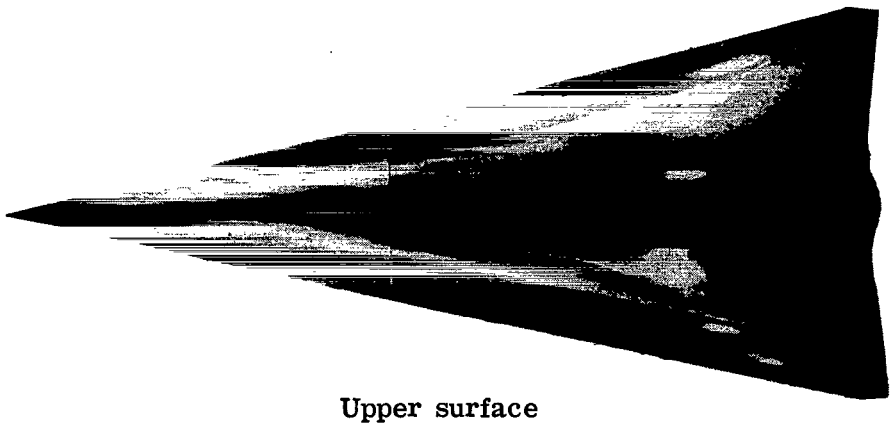


Upper surface
$\alpha = 9^{o}$

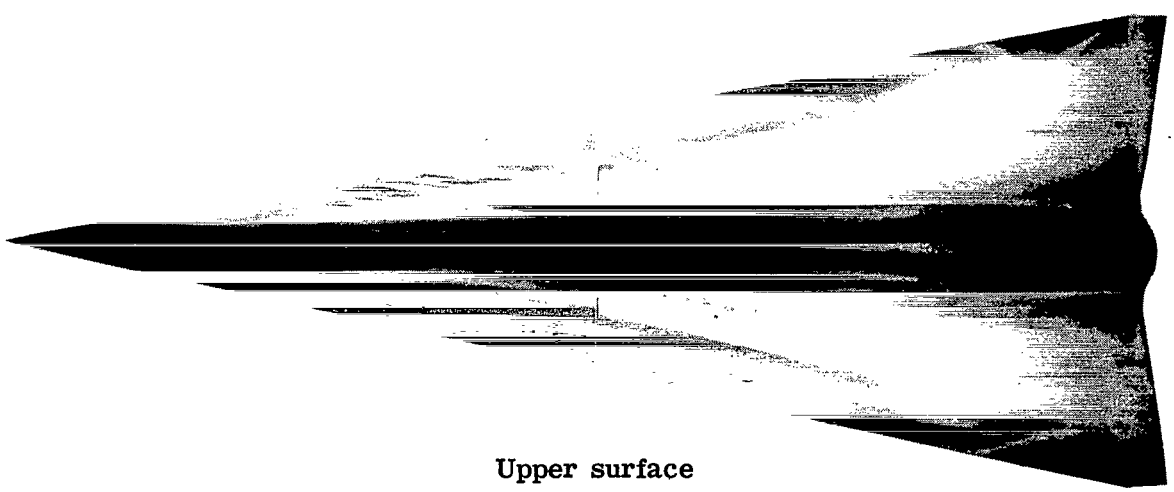
L-76-196

(a) 76^{o} sweep flat wing.

Figure 4.- Oil-flow photographs.



Upper surface
$\alpha = 4.5^{o}$ $(C_L = 0.1)$

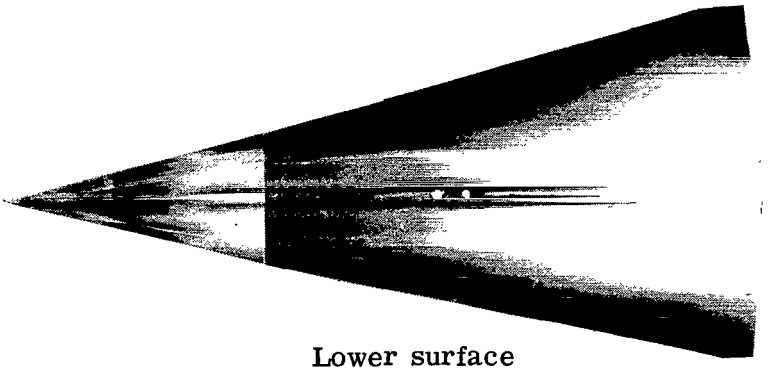


Upper surface
$\alpha = 9^{o}$

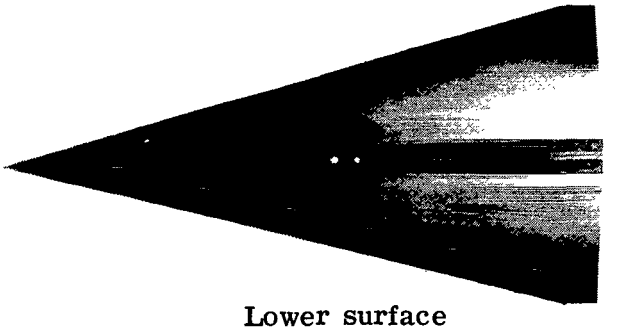
L-76-197

(b) 76^{o} sweep cambered wing.

Figure 4.- Continued.



Lower surface
$\alpha = 4.5^{o}$ $(C_L = 0.1)$

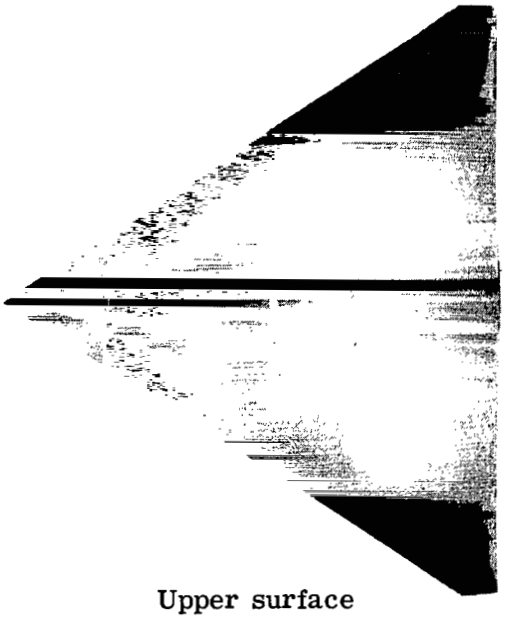


Lower surface
$\alpha = 9^{o}$

L-76-198

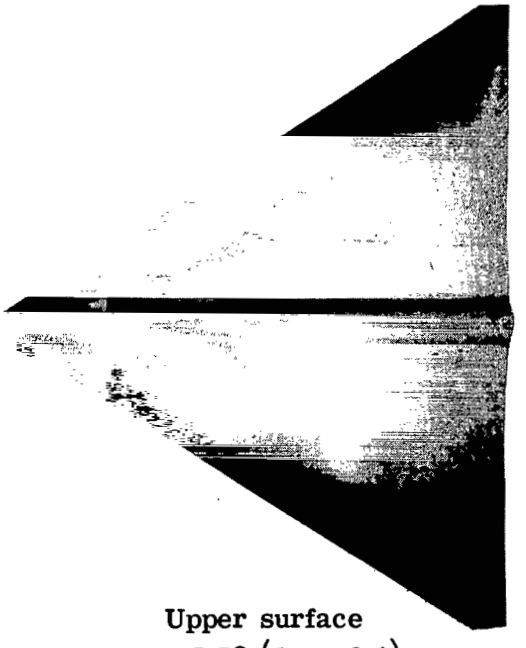
(b) Concluded.

Figure 4.- Continued.



Upper surface

$\alpha = 3^{o}$



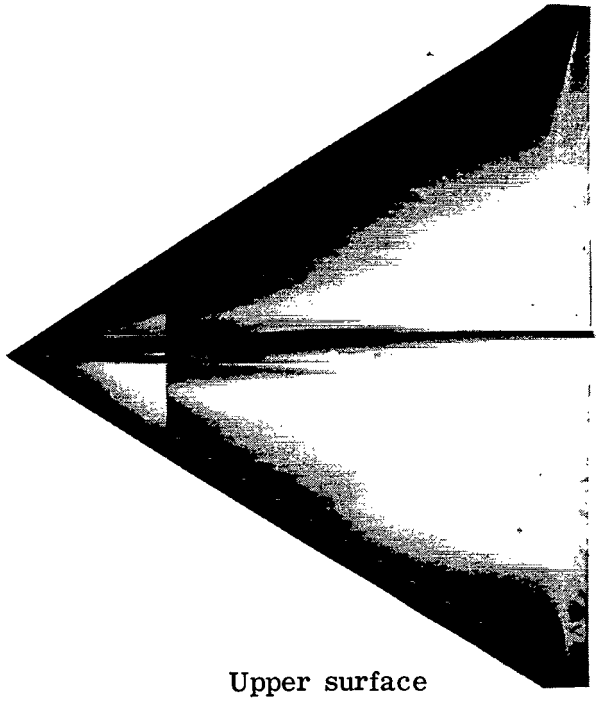
Upper surface

$\alpha = 5.5^{o}$ $(C_L = 0.1)$

L-76-199

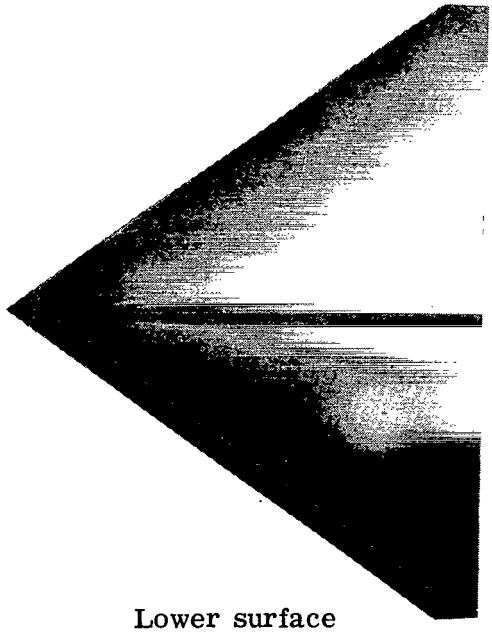
(c) 55^{o} sweep flat wing.

Figure 4.- Continued.



Upper surface

$\alpha = 8^{o}$

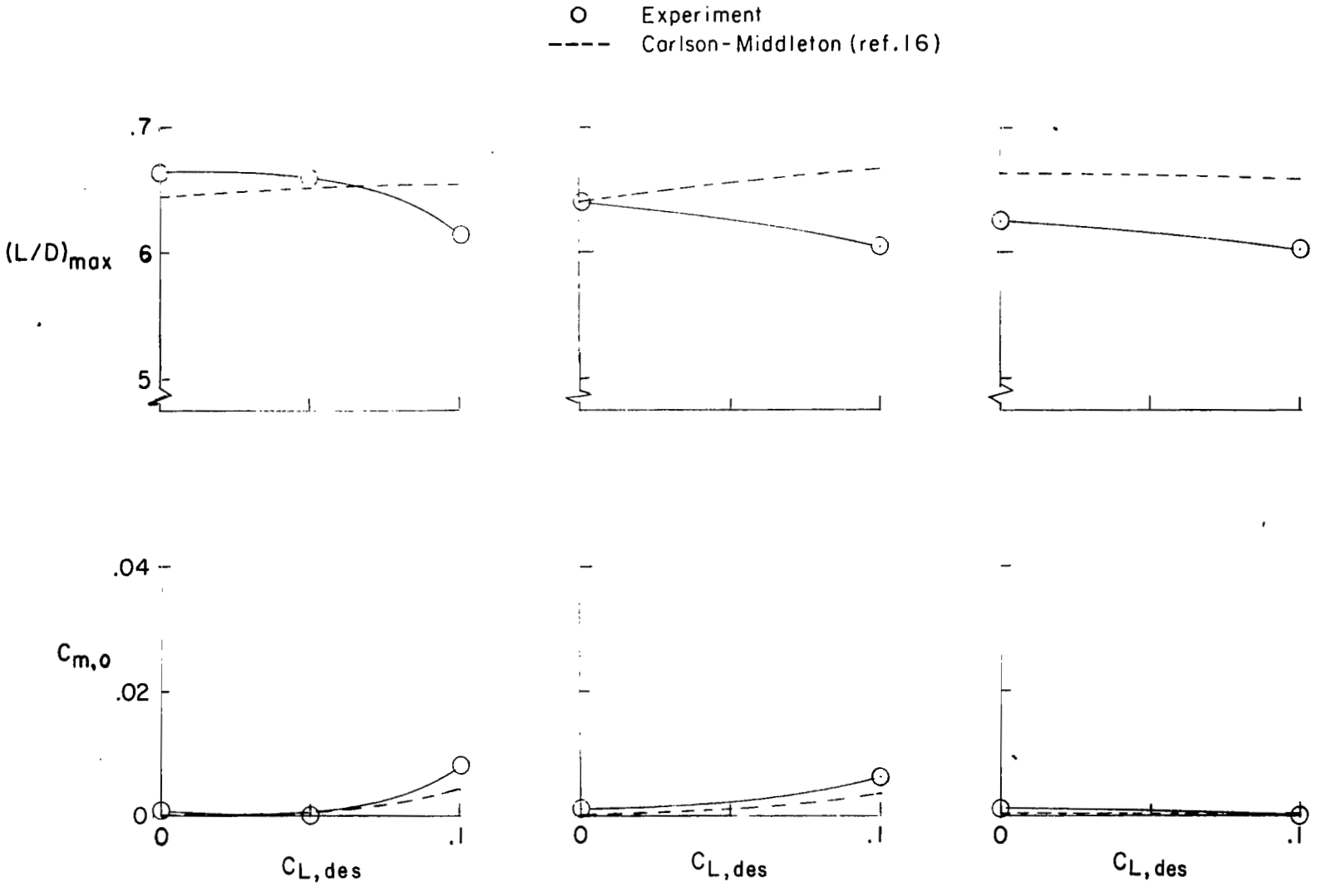


Lower surface

$\alpha = 5.5^{o}$ $(C_L = 0.1)$ L-76-200

(c) Concluded.

Figure 4.- Concluded.



(a) $\Lambda = 76^{o}$. (b) $\Lambda = 68^{o}$. (c) $\Lambda = 55^{o}$.

Figure 5.- Effect of design lift coefficient on $(L/D)_{max}$ and $C_{m,0}$ at design Mach number of 3.5.

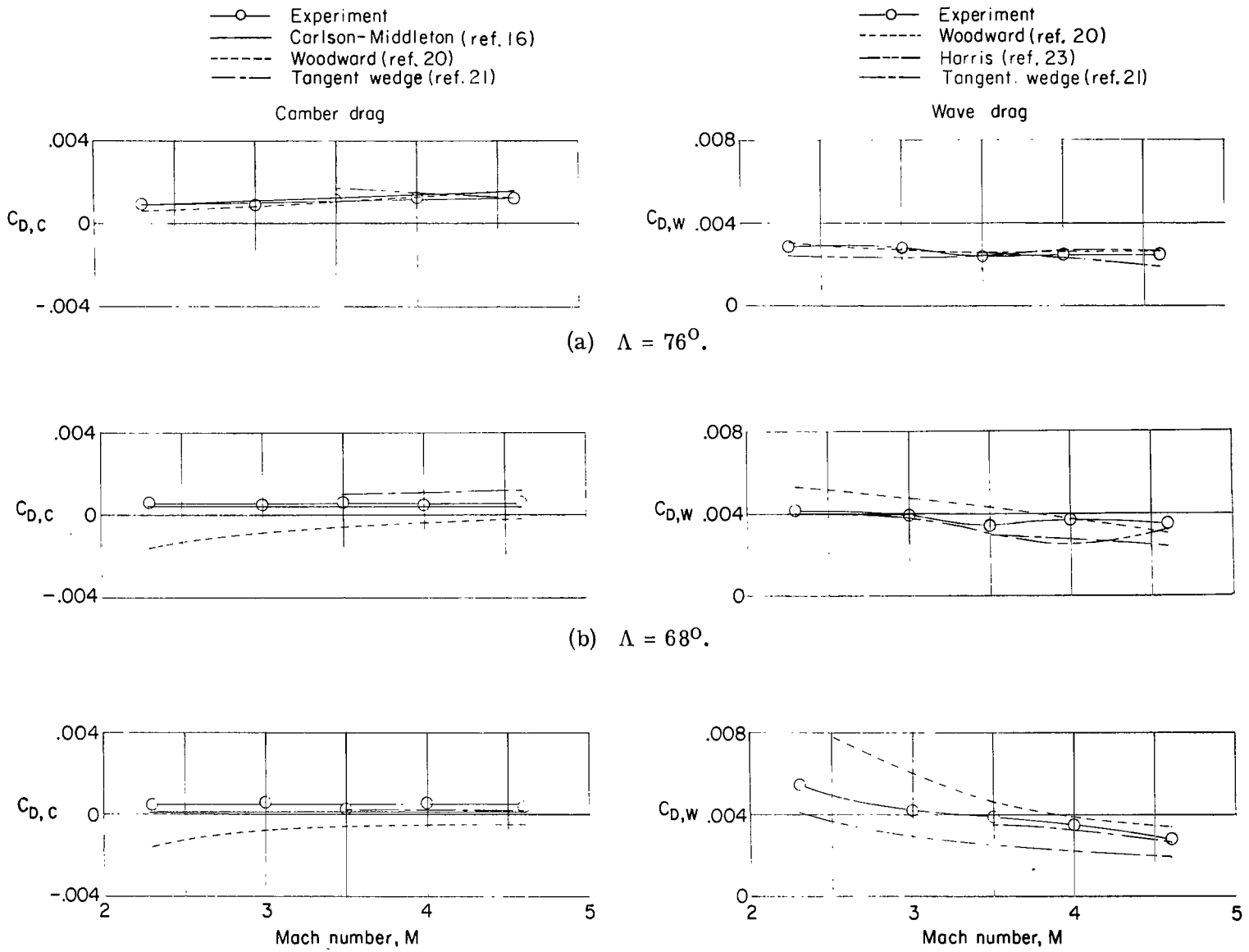
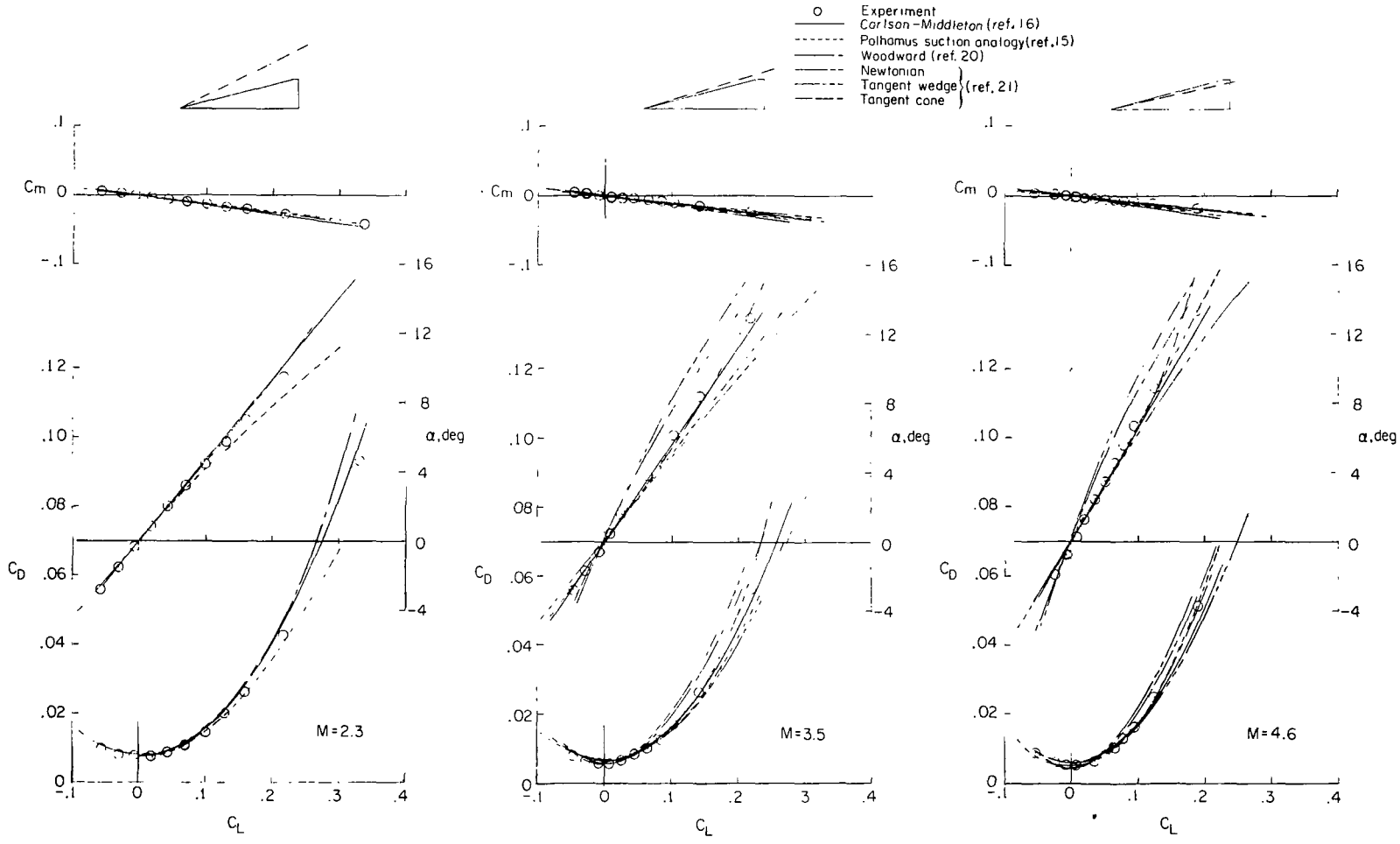
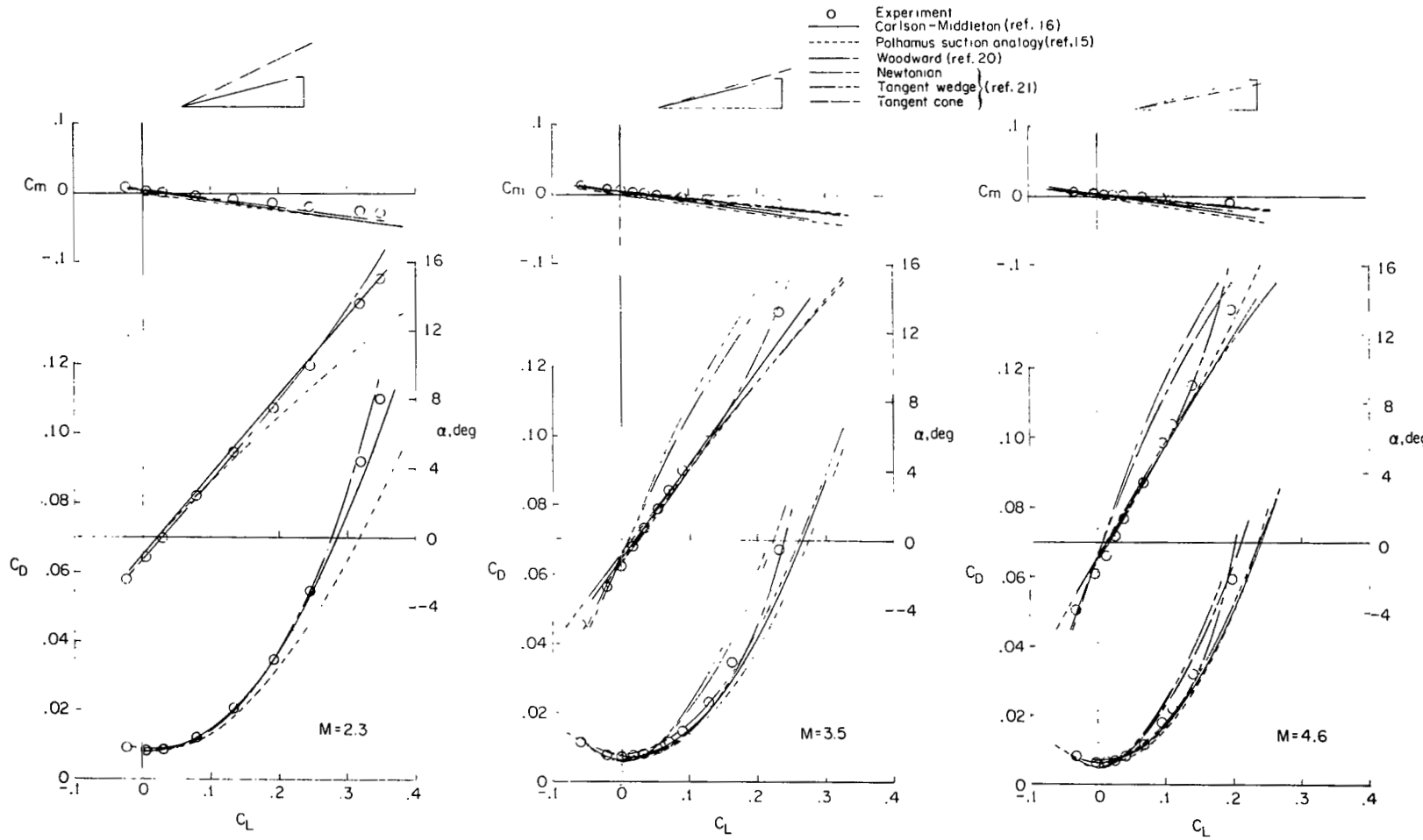


Figure 6.- Effect of Mach number on camber and wave drag. $C_{L,des} = 0.1$.



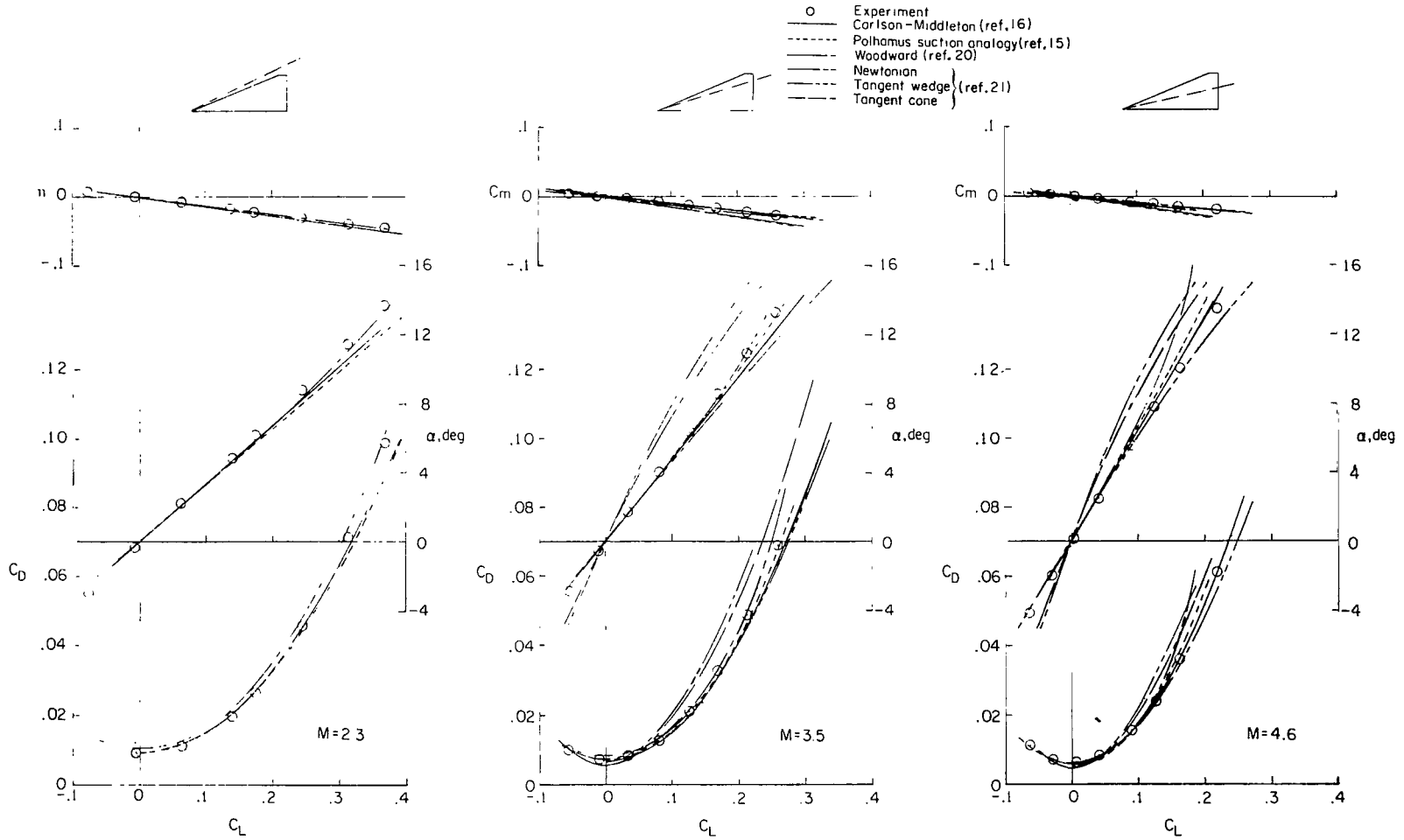
(a) 76° sweep; $C_{L,des} = 0.0$.

Figure 7.- Comparison of experimental and theoretical results.



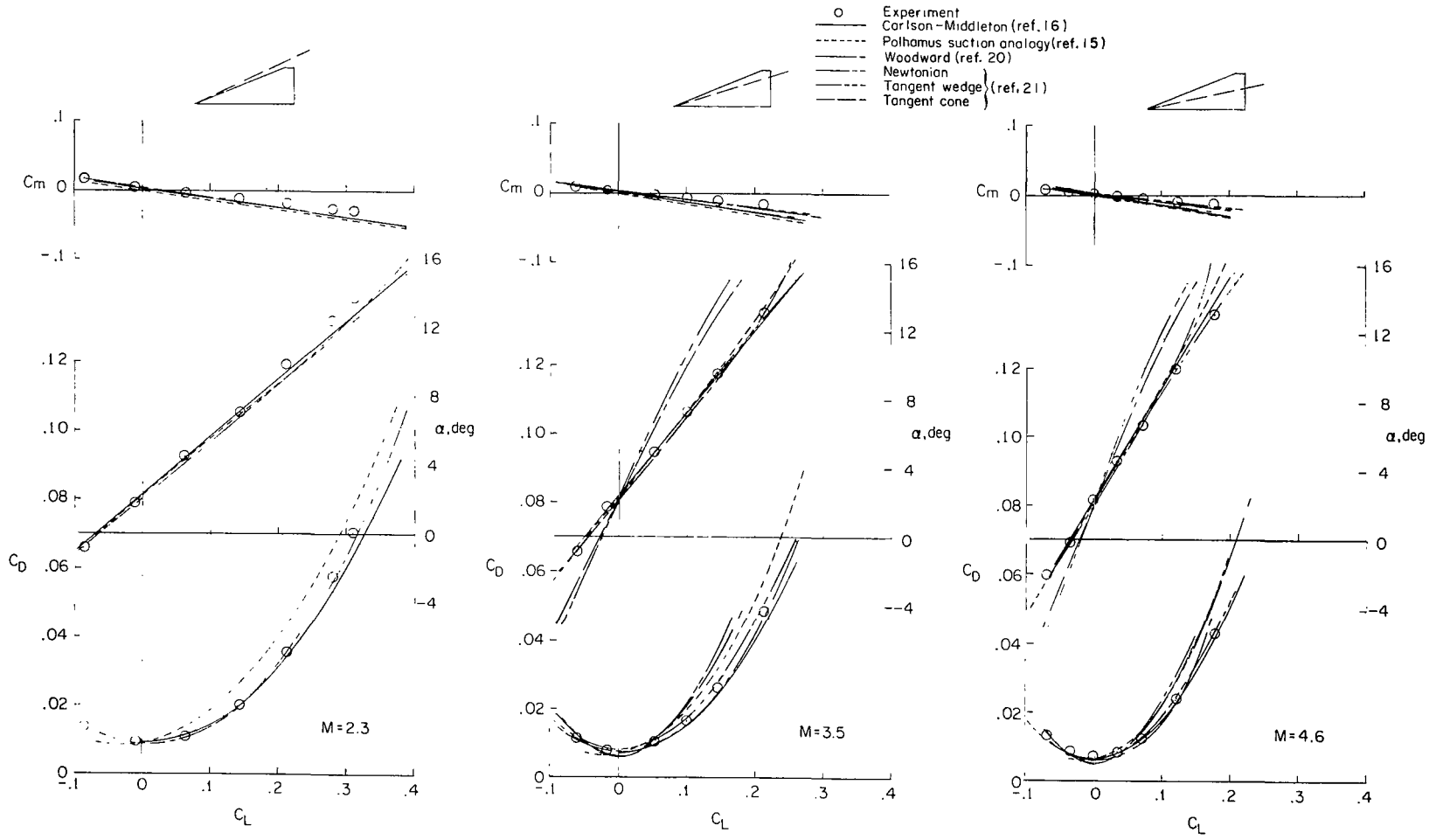
(b) 76° sweep; $C_{L,des} = 0.1$.

Figure 7.- Continued.



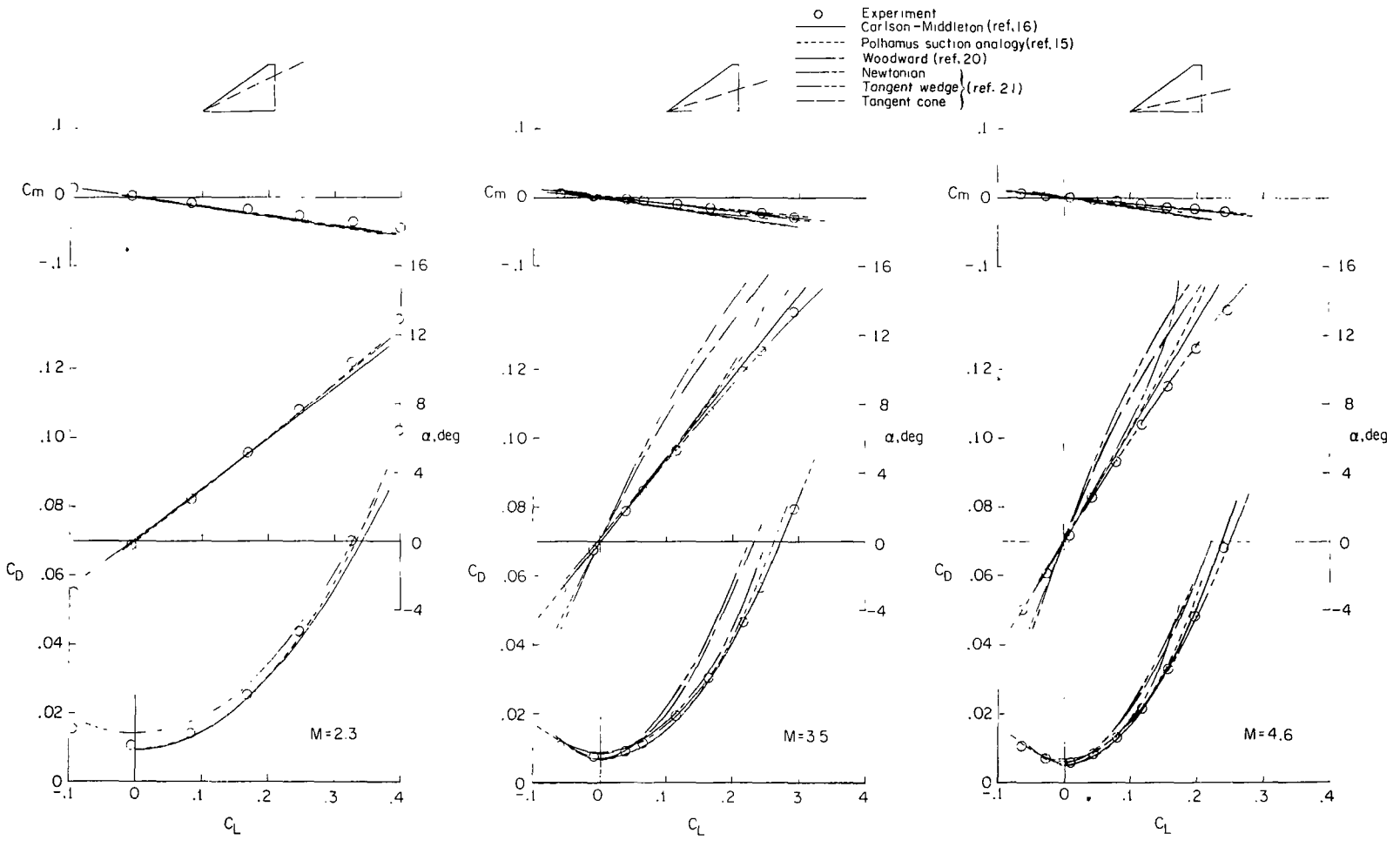
(c) 68^{o} sweep; $C_{L,des} = 0.0$.

Figure 7.- Continued.



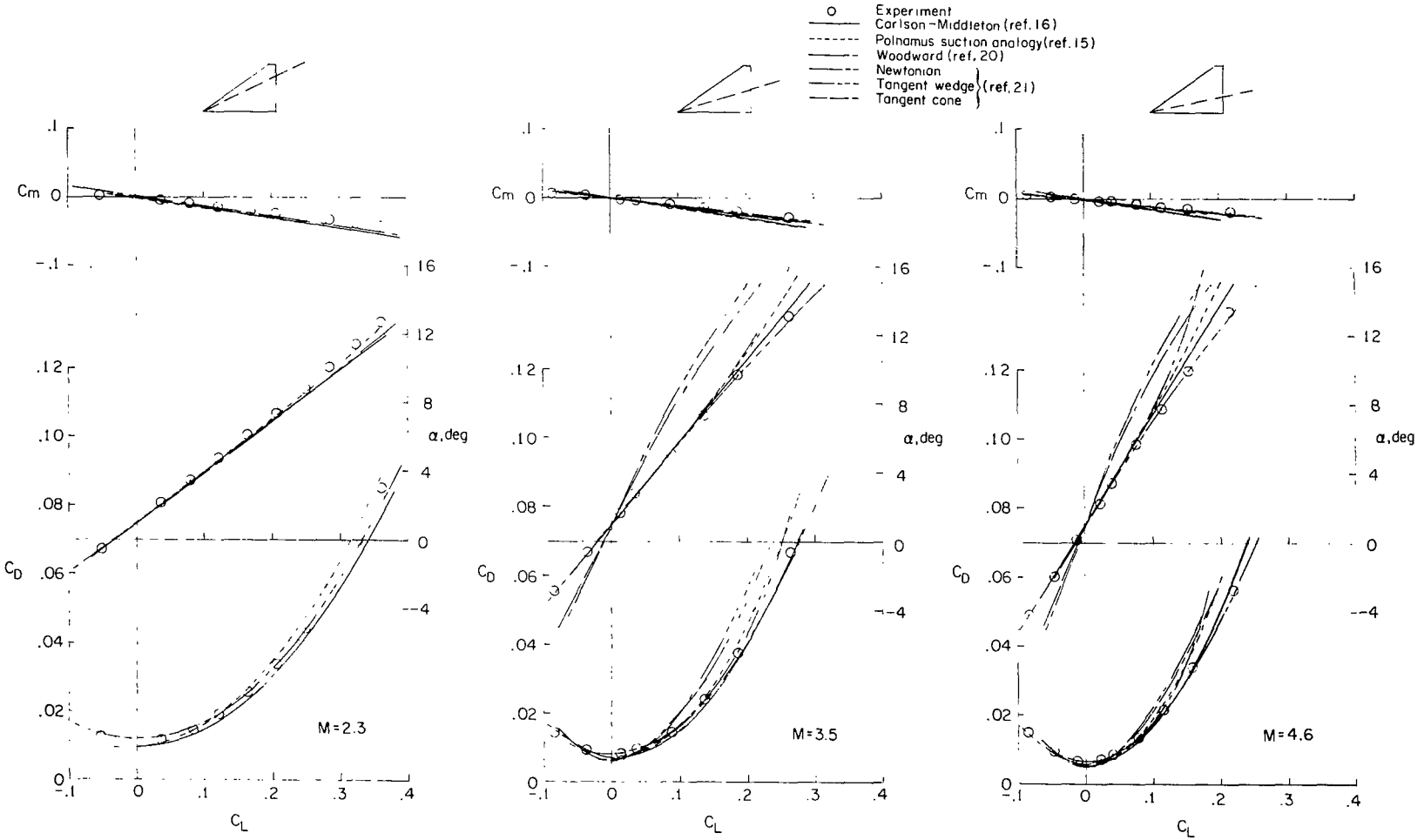
(d) 68° sweep; $C_{L,des} = 0.1$.

Figure 7.- Continued.



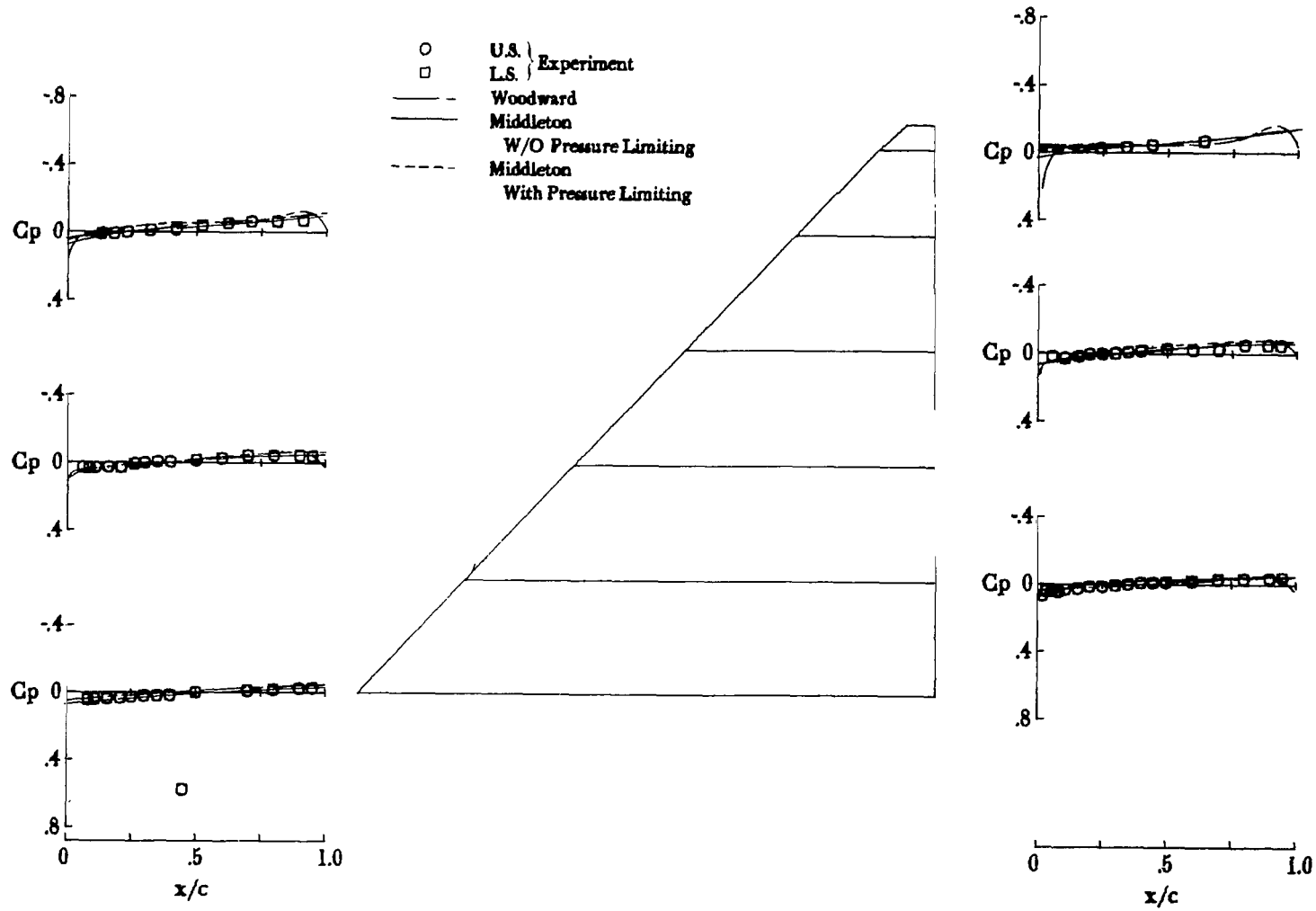
(e) 55° sweep; $C_{L,des} = 0.0$.

Figure 7.- Continued.



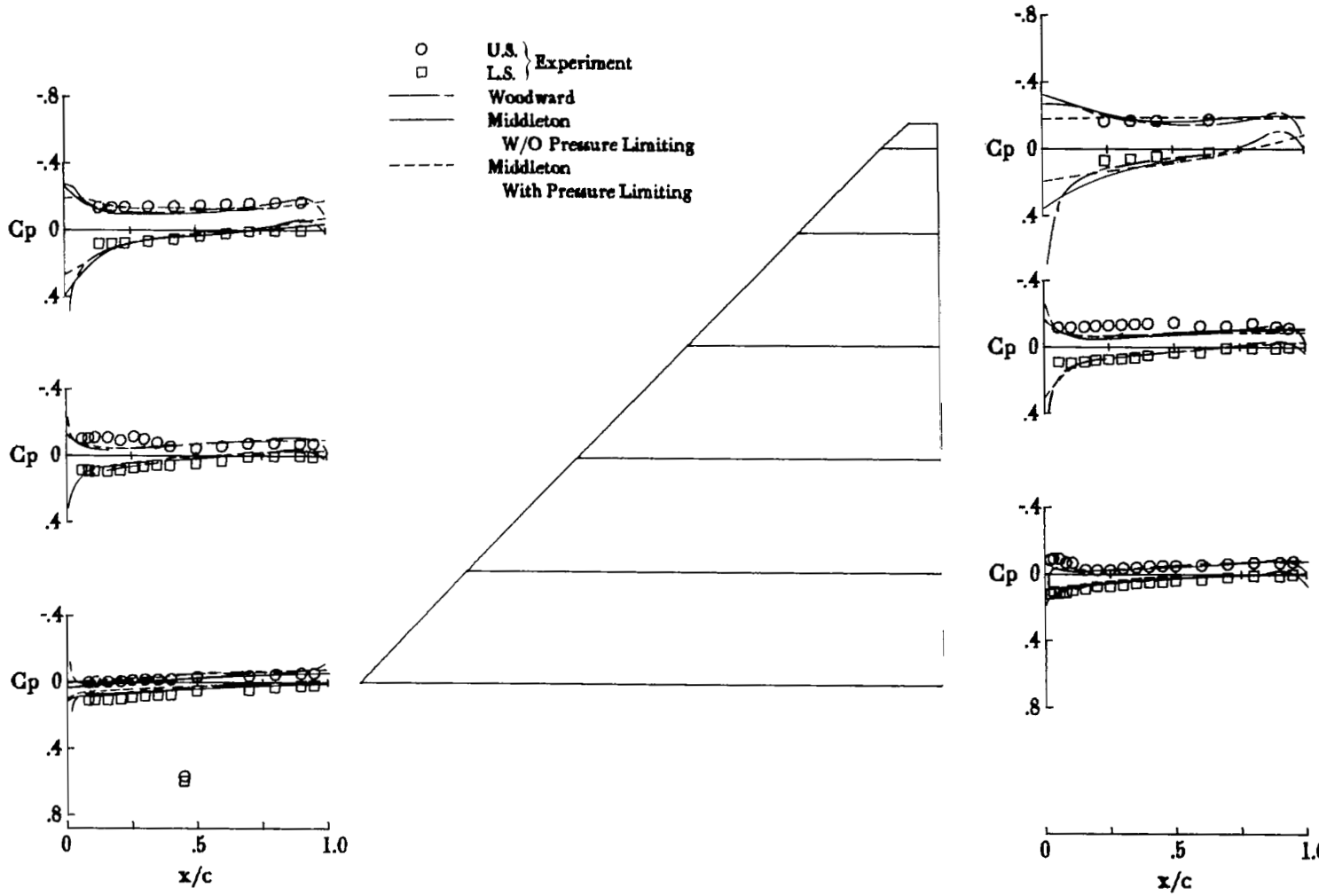
(f) 55° sweep; $C_{L,des} = 0.1$.

Figure 7.- Concluded.



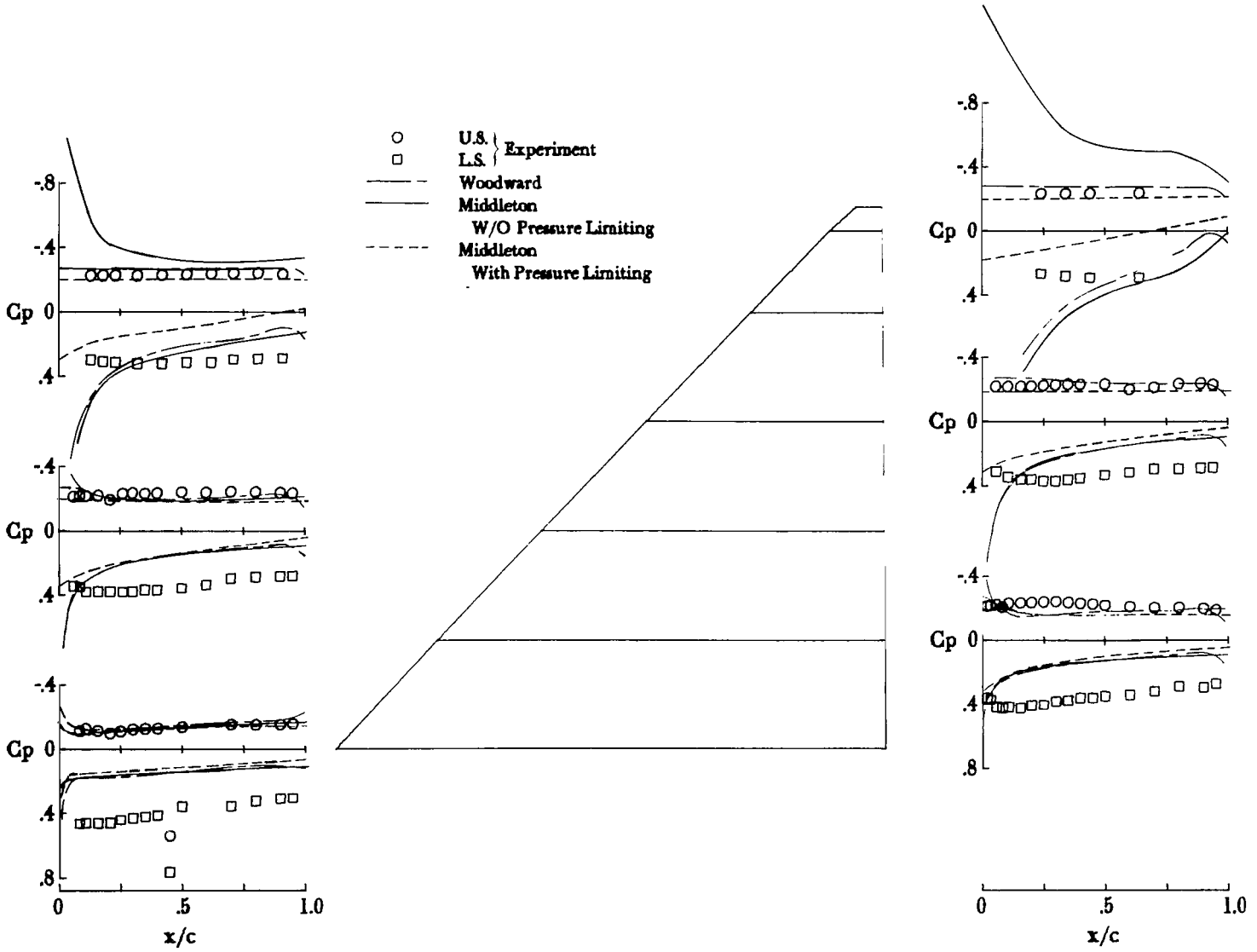
(a) $\alpha = -0.06^{o}$.

Figure 8.- Experimental and theoretical pressure distributions at $\Lambda = 76^{o}$, $C_{L,des} = 0.0$, and $M = 2.3$.



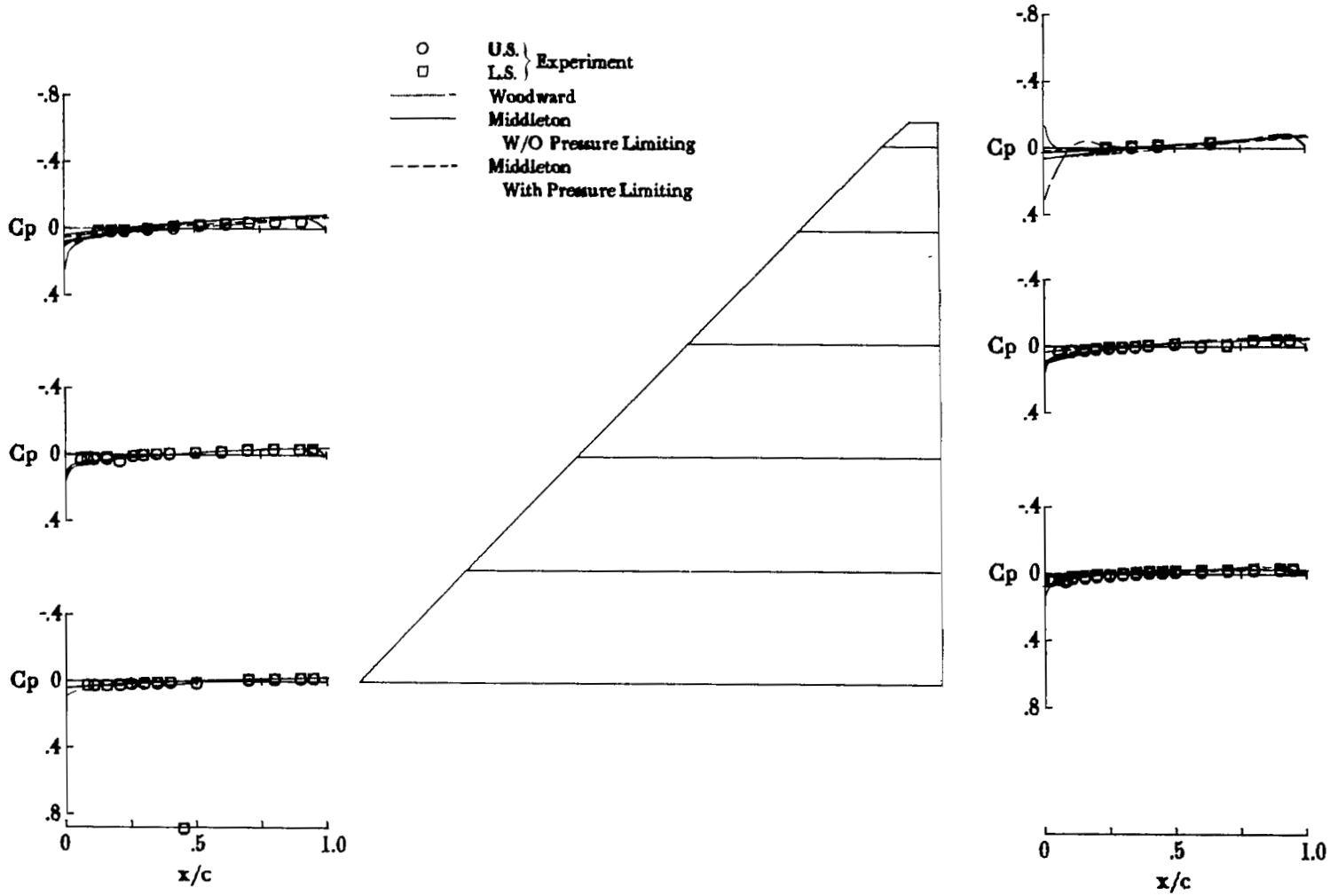
(b) $\alpha = 4.95^{O}$.

Figure 8.- Continued.



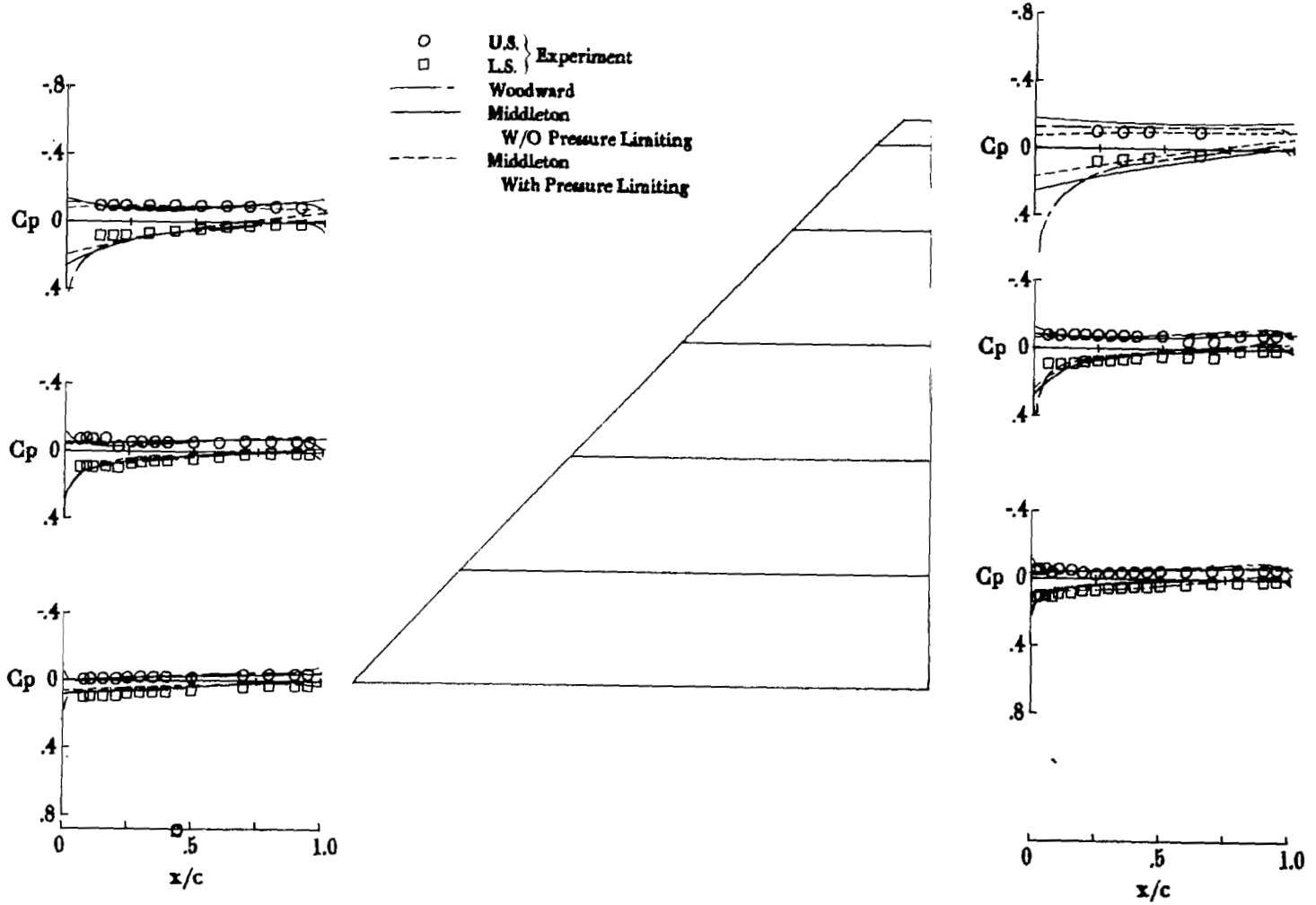
(c) $\alpha = 19.94^{\circ}$.

Figure 8.- Concluded.



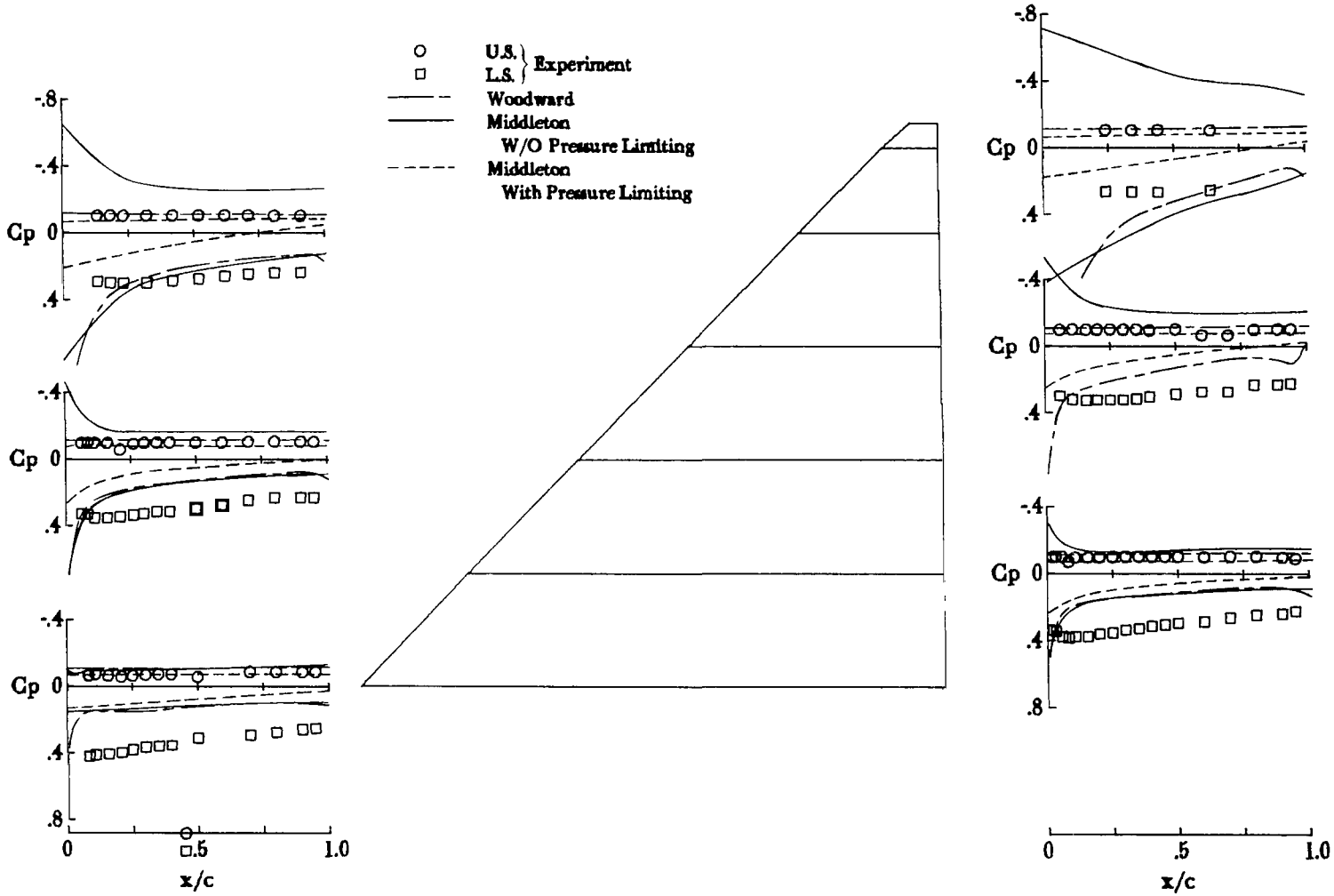
(a) $\alpha = -0.27^{\circ}$.

Figure 9.- Experimental and theoretical pressure distributions at $\Lambda = 76^{\circ}$, $C_{L,des} = 0.0$, and $M = 3.5$.



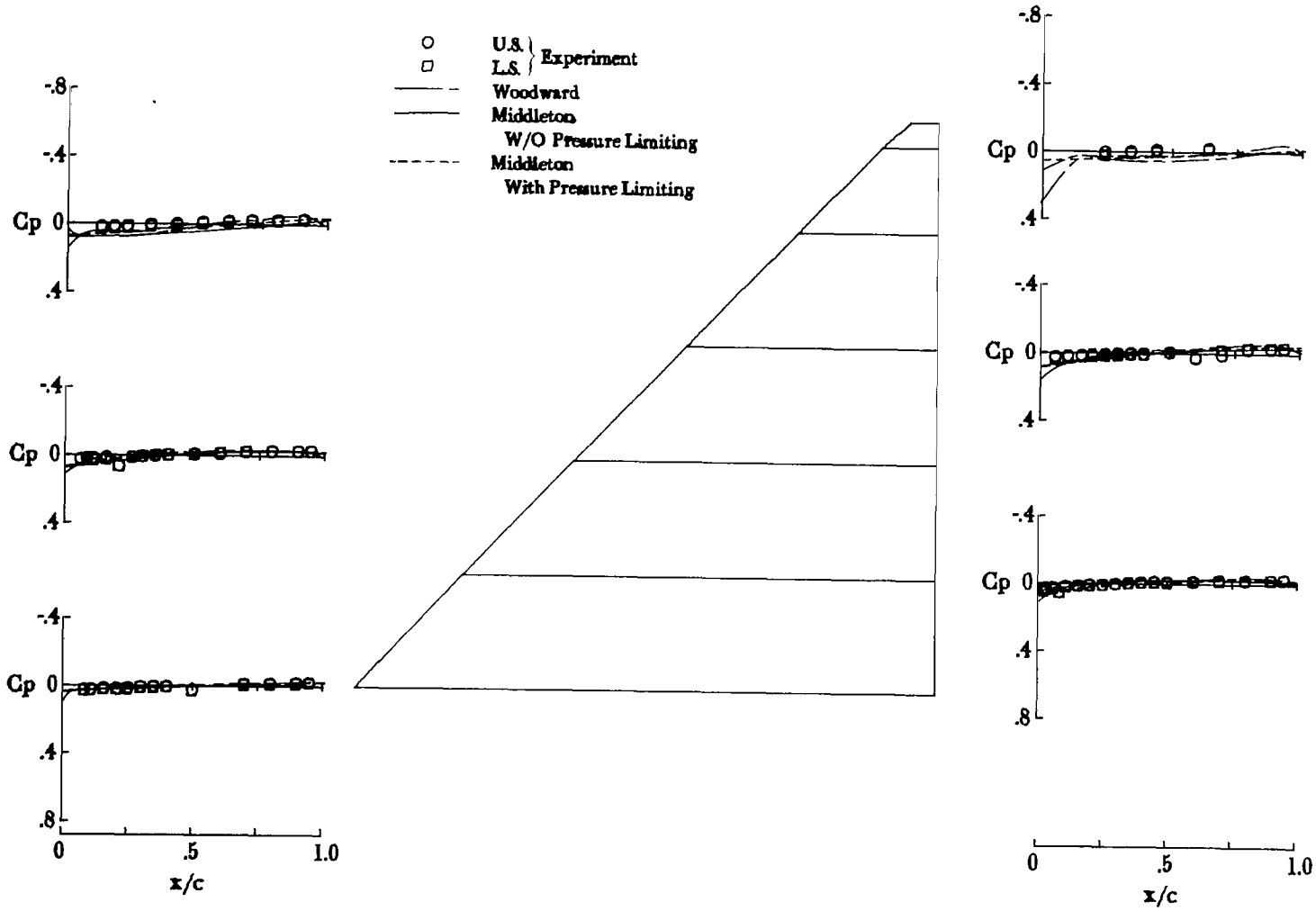
(b) $\alpha = 5.73^{\circ}$.

Figure 9.- Continued.



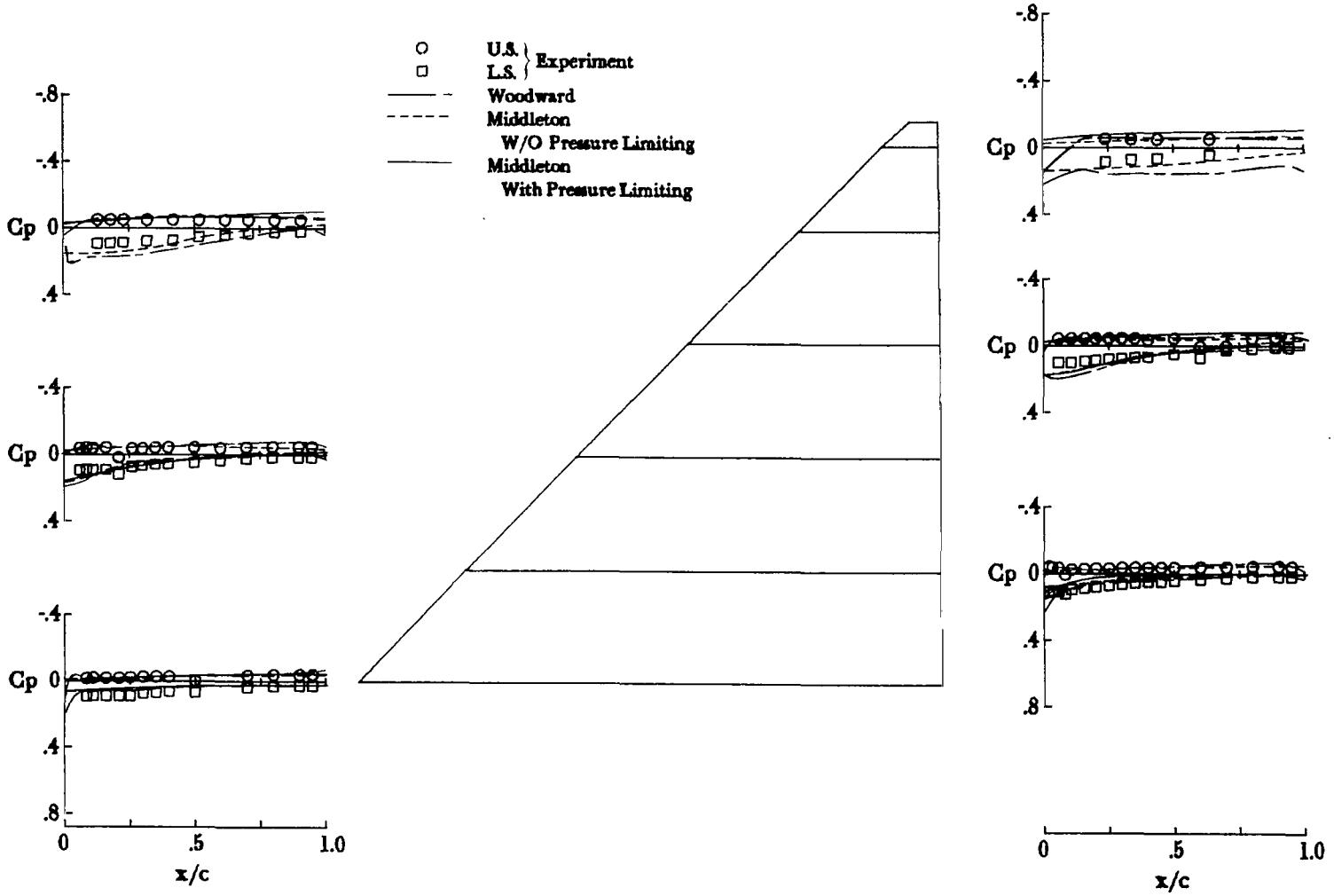
(c) $\alpha = 19.74^{O}$.

Figure 9.- Concluded.



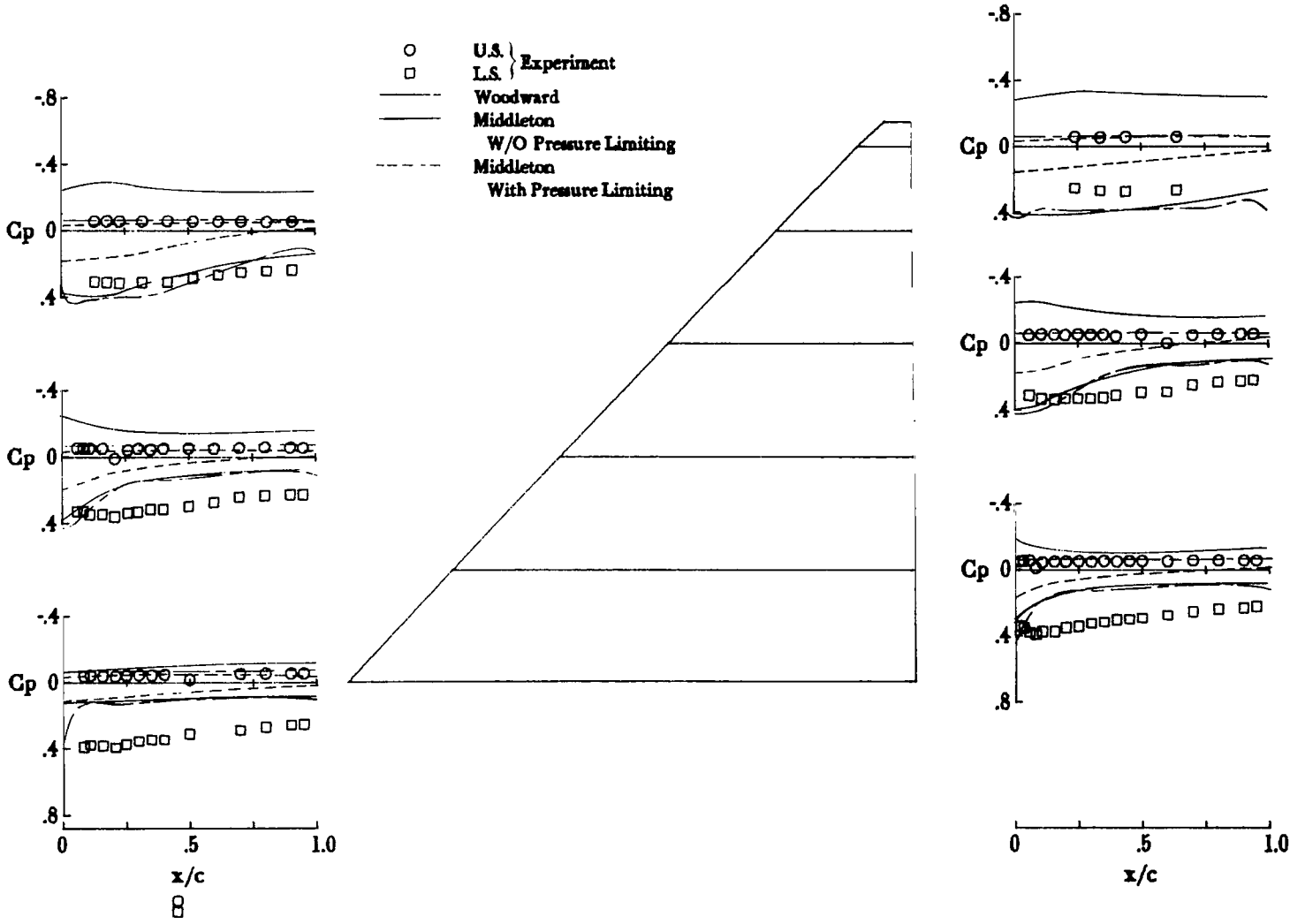
(a) $\alpha = 0.56^{o}$.

Figure 10.- Experimental and theoretical pressure distributions at $\Lambda = 76^{o}$, $C_{L,des} = 0.0$, and $M = 4.6$.



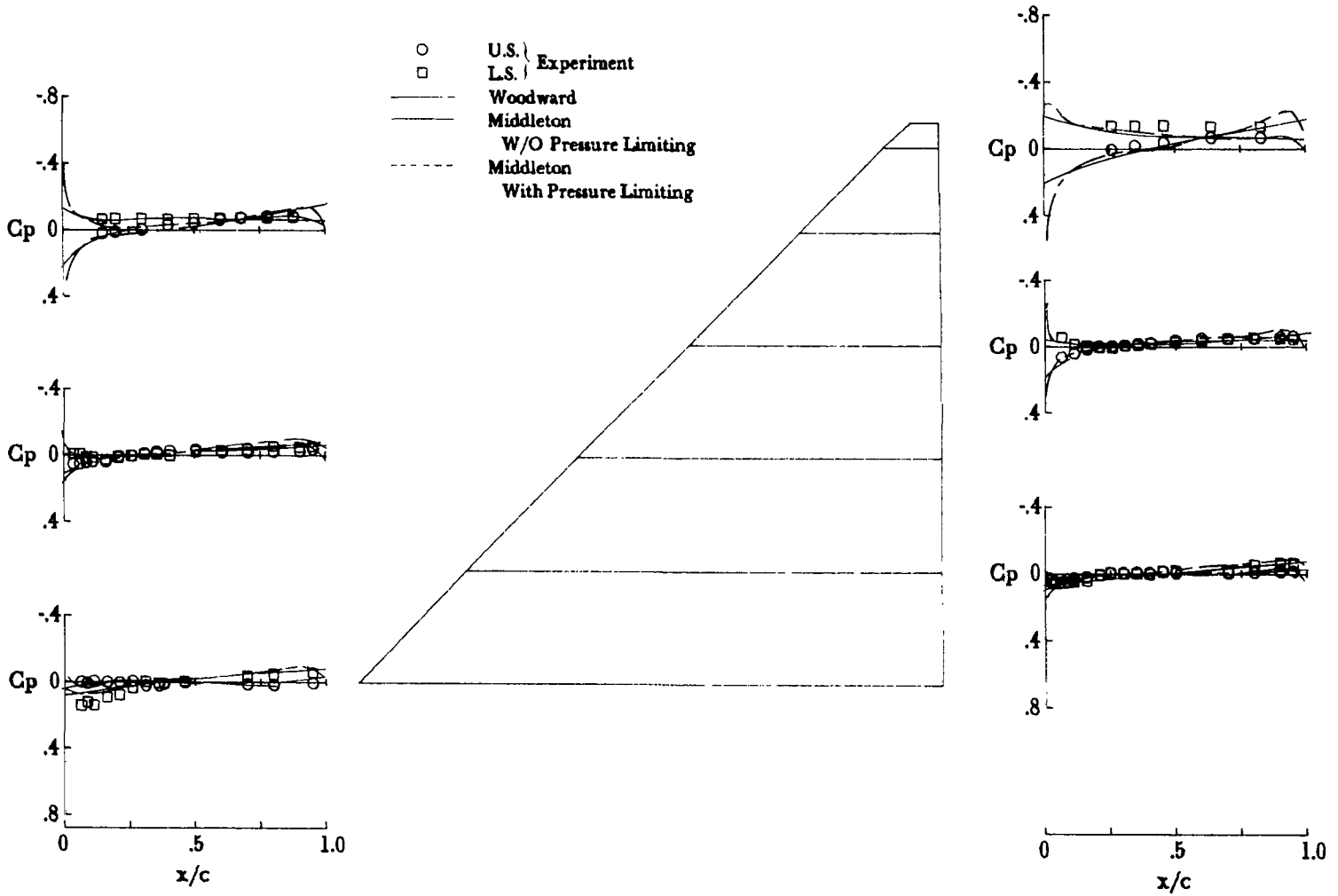
(b) $\alpha = 6.56^{o}$.

Figure 10.- Continued.



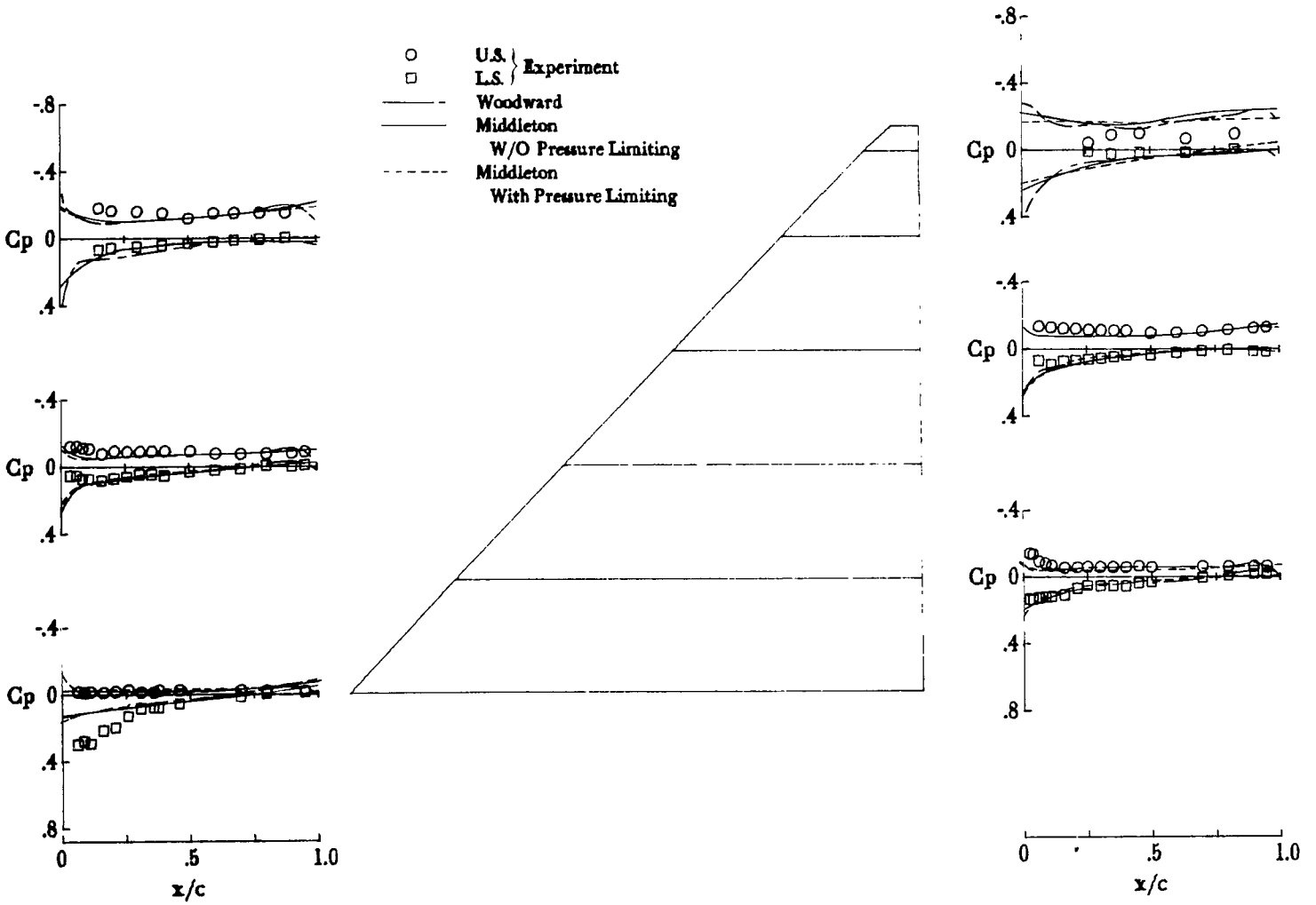
(c) $\alpha = 20.56^{o}$.

Figure 10.- Concluded.



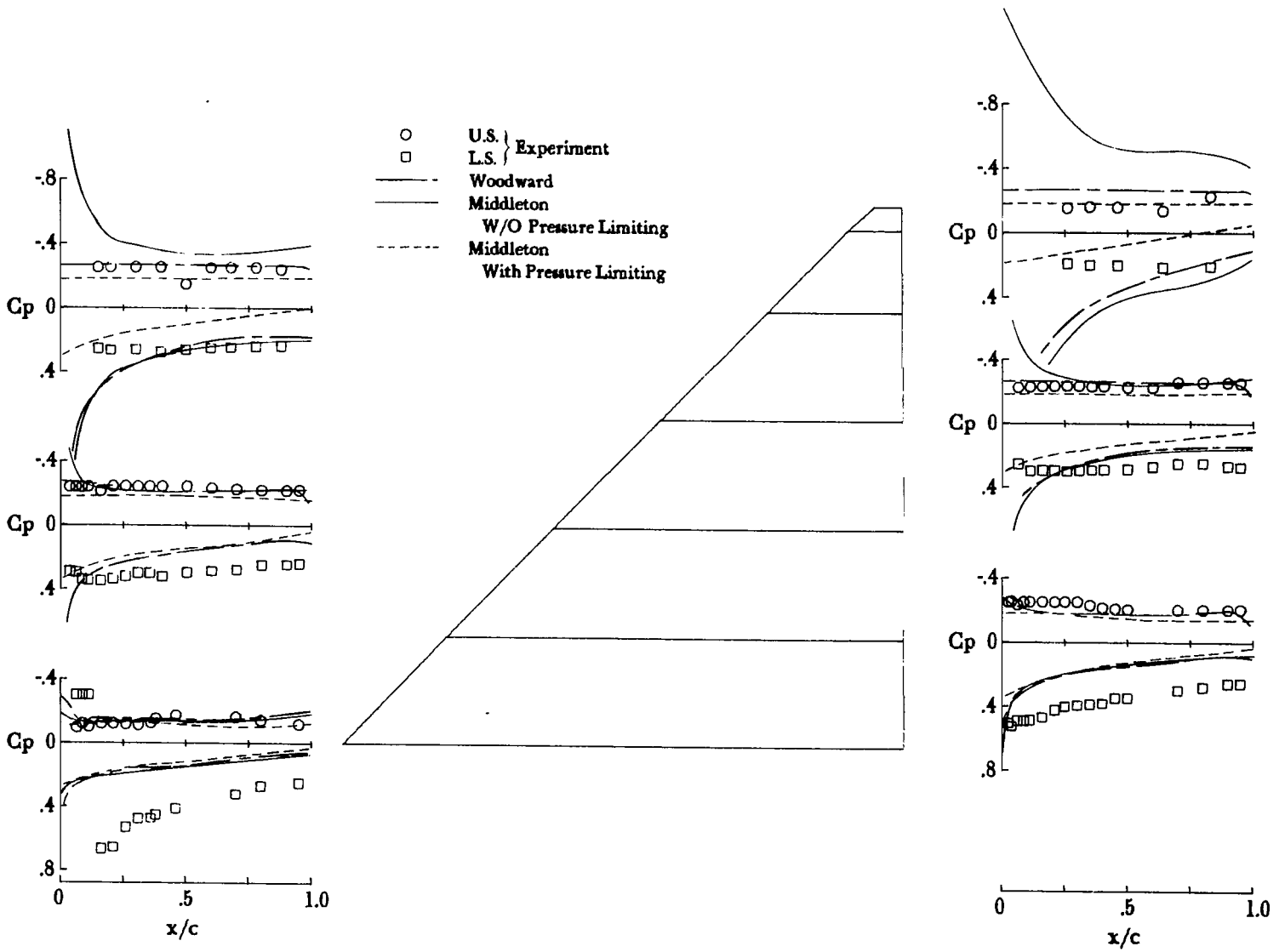
(a) $\alpha = -2.05^{o}$.

Figure 11.- Experimental and theoretical pressure distributions at $\Lambda = 76^{o}$, $C_{L,des} = 0.1$, and $M = 2.3$.



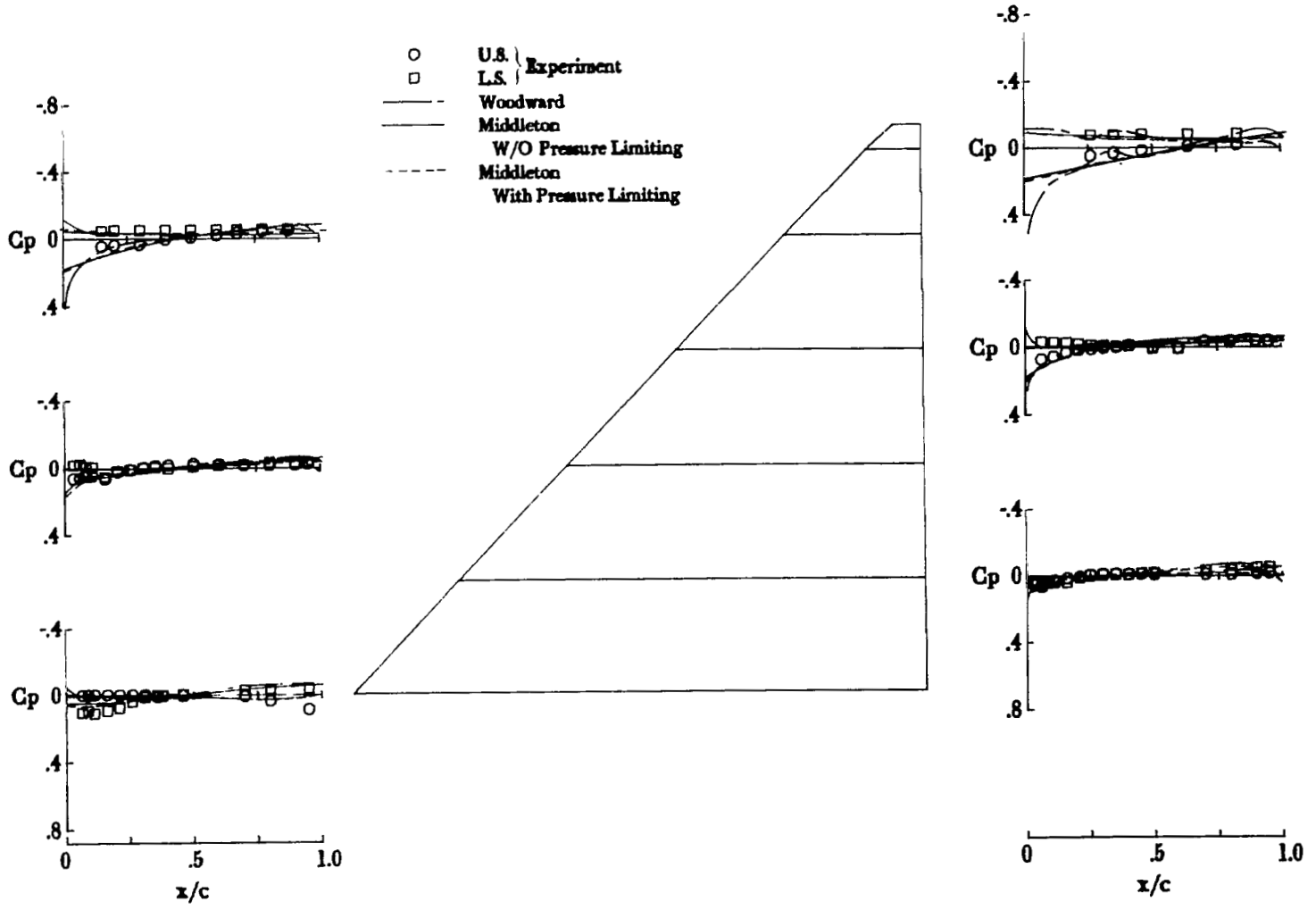
(b) $\alpha = 3.95^{o}$.

Figure 11.- Continued.



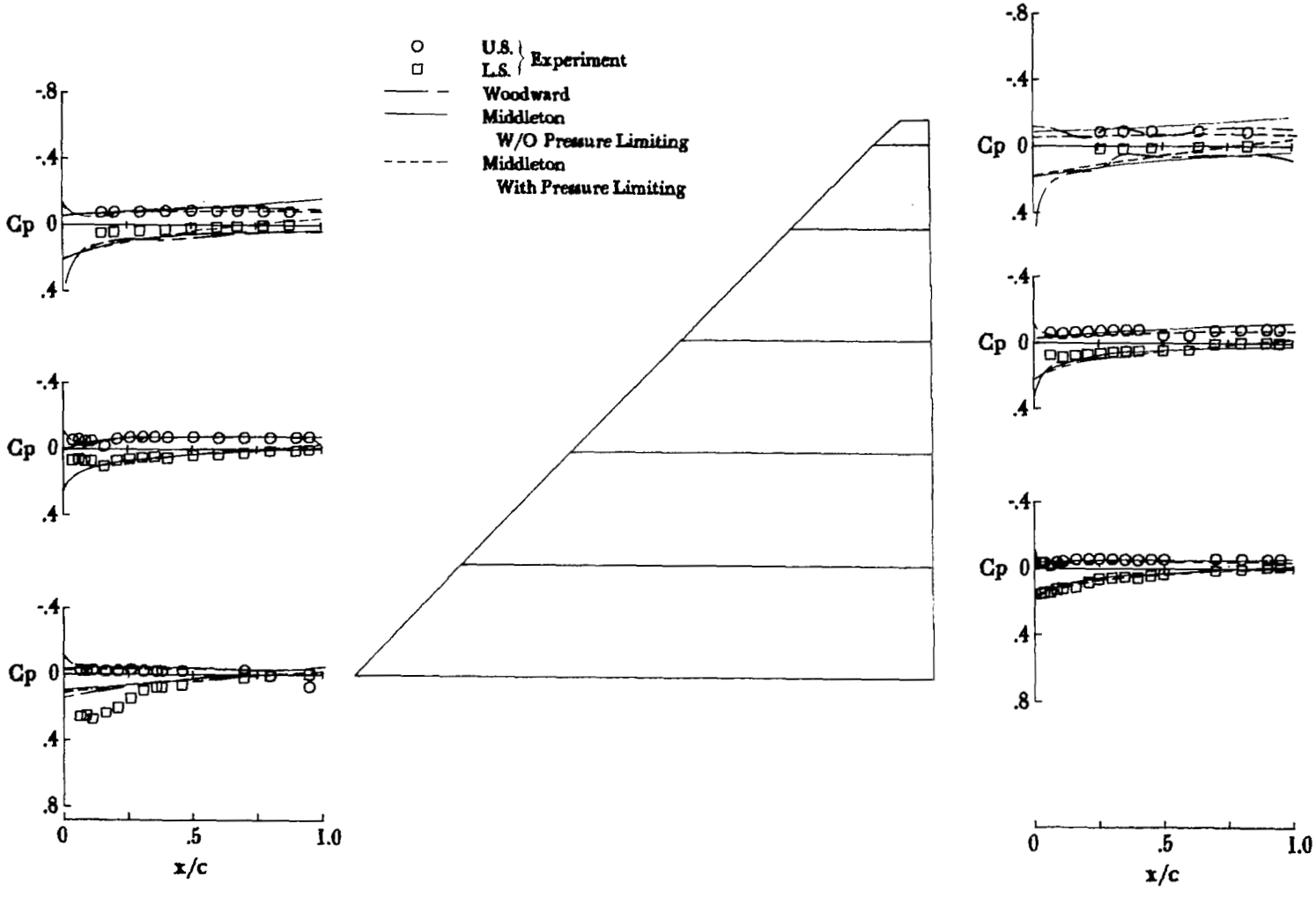
(c) $\alpha = 19.95^{o}$.

Figure 11.- Concluded.



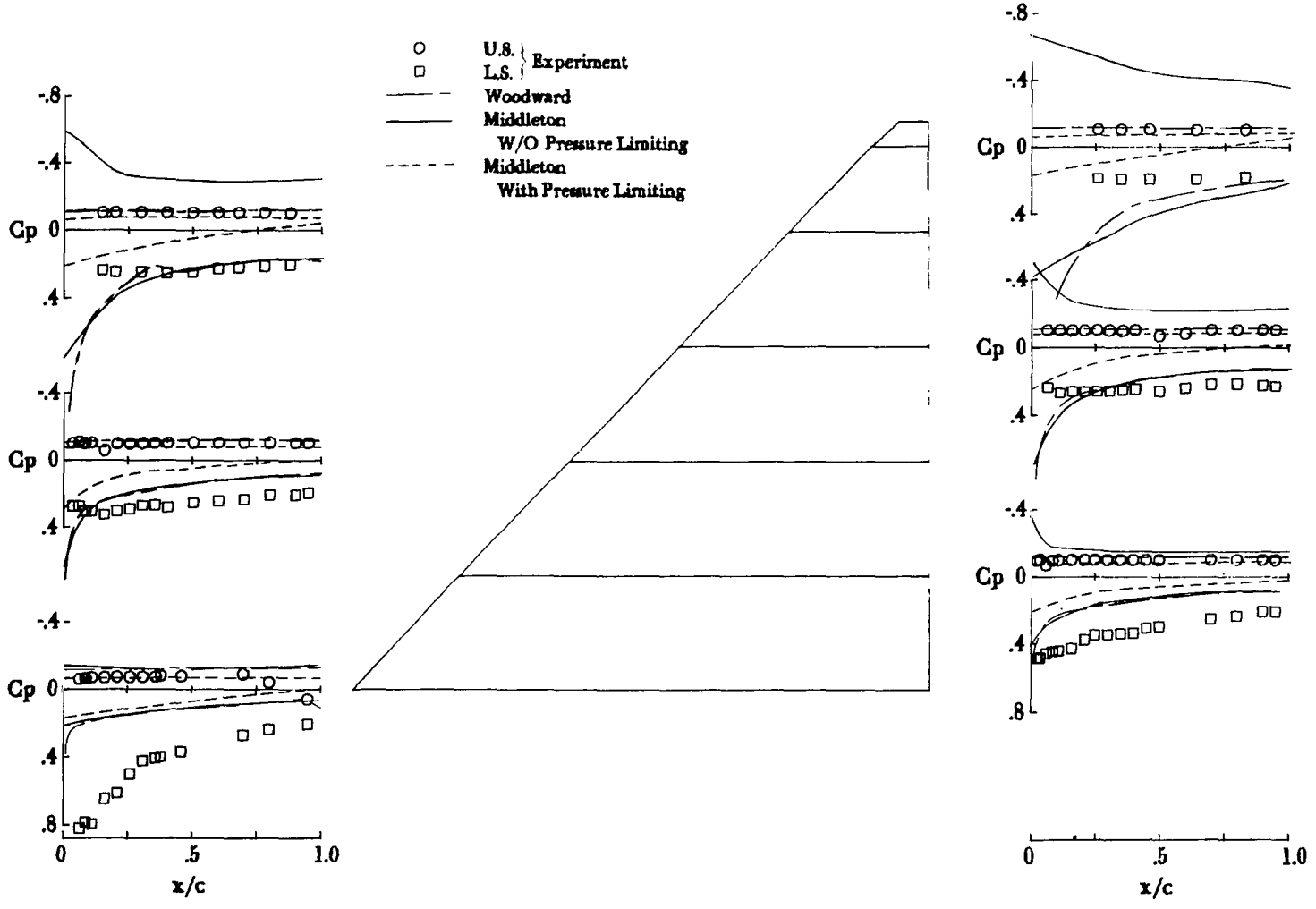
(a) $\alpha = -2.30^{o}$.

Figure 12.- Experimental and theoretical pressure distributions at $\Lambda = 76^{o}$, $C_{L,des} = 0.1$, and $M = 3.5$.



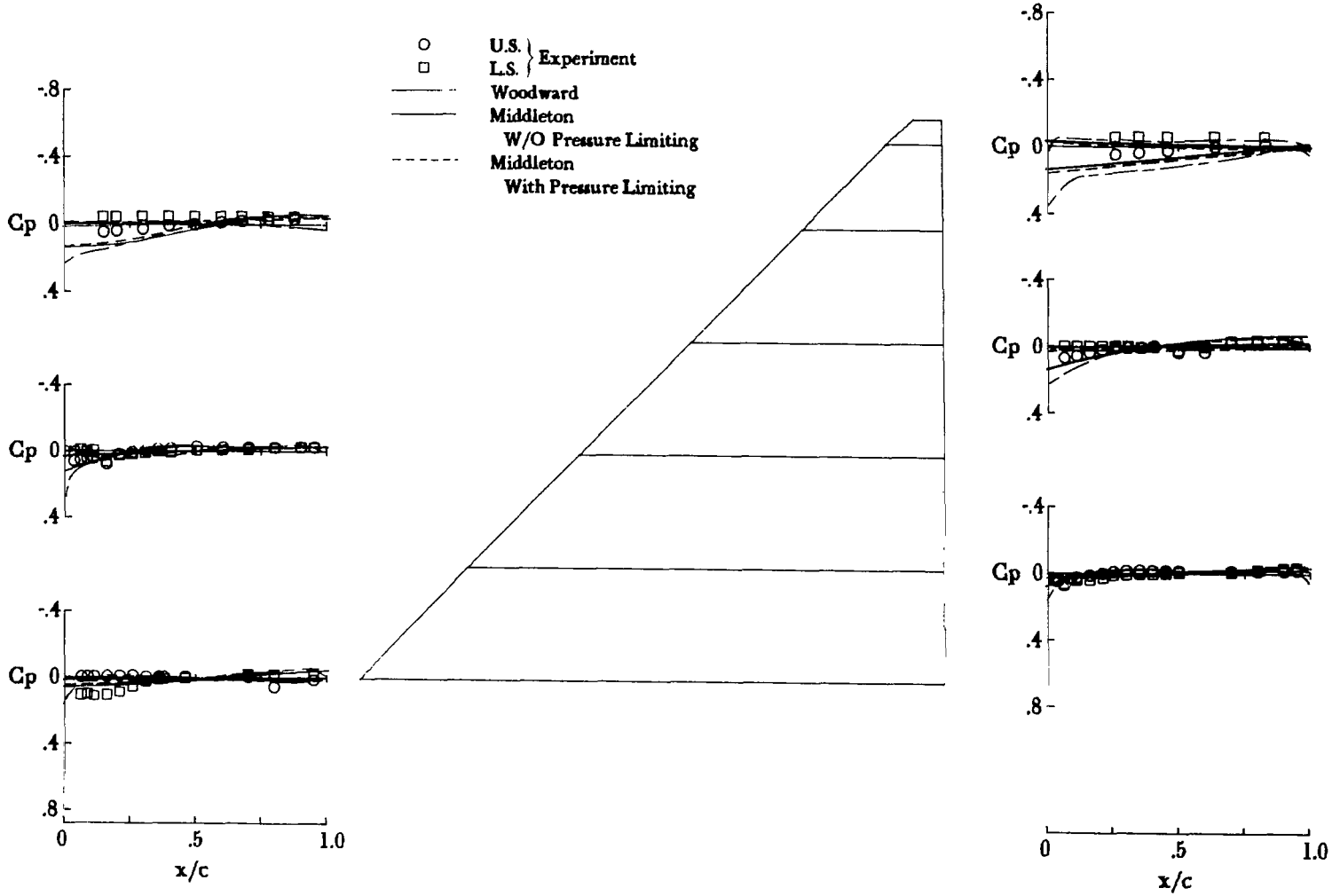
(b) $\alpha = 4.70^{\circ}$.

Figure 12.- Continued.



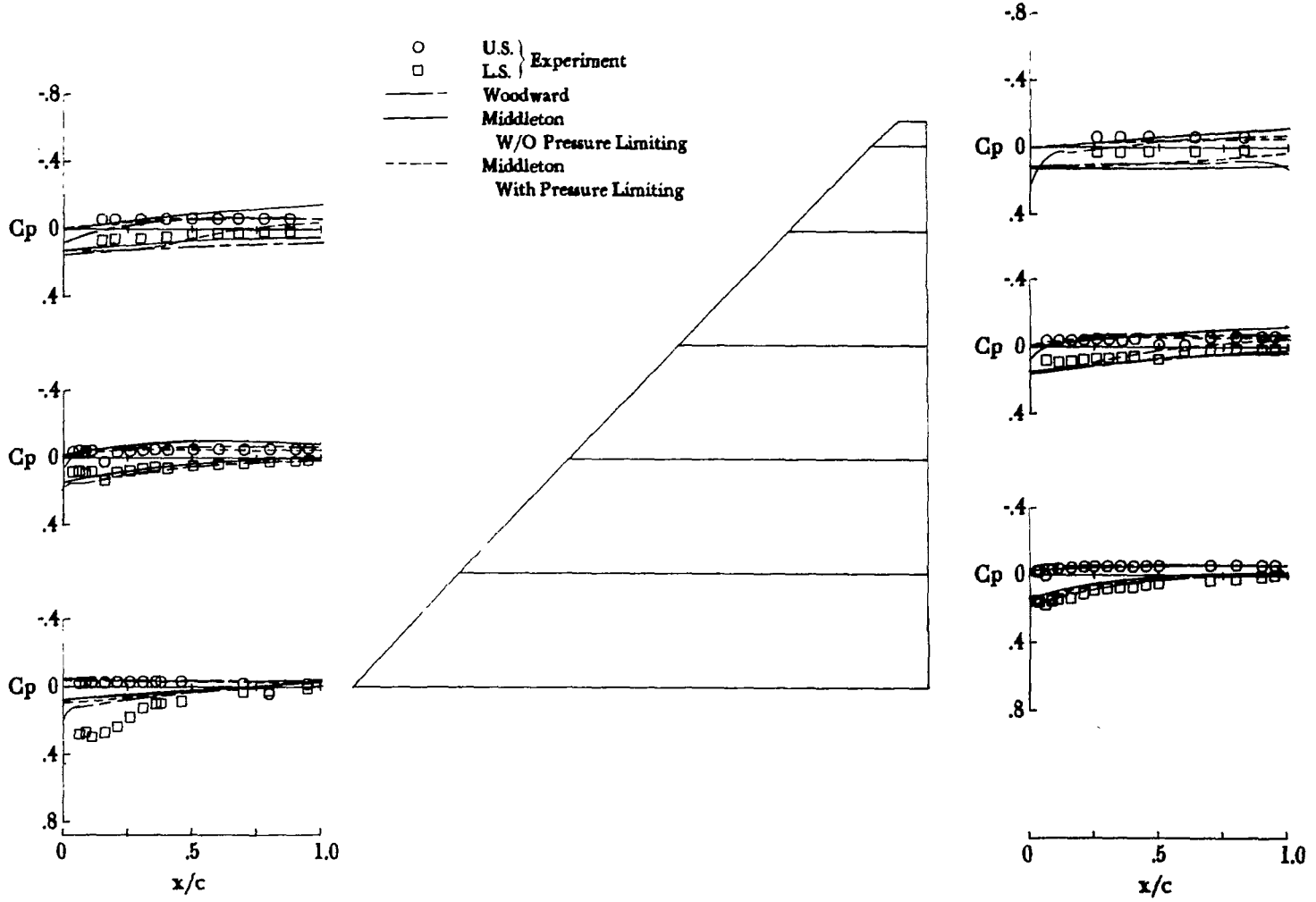
(c) $\alpha = 19.70^{O}$.

Figure 12.- Concluded.



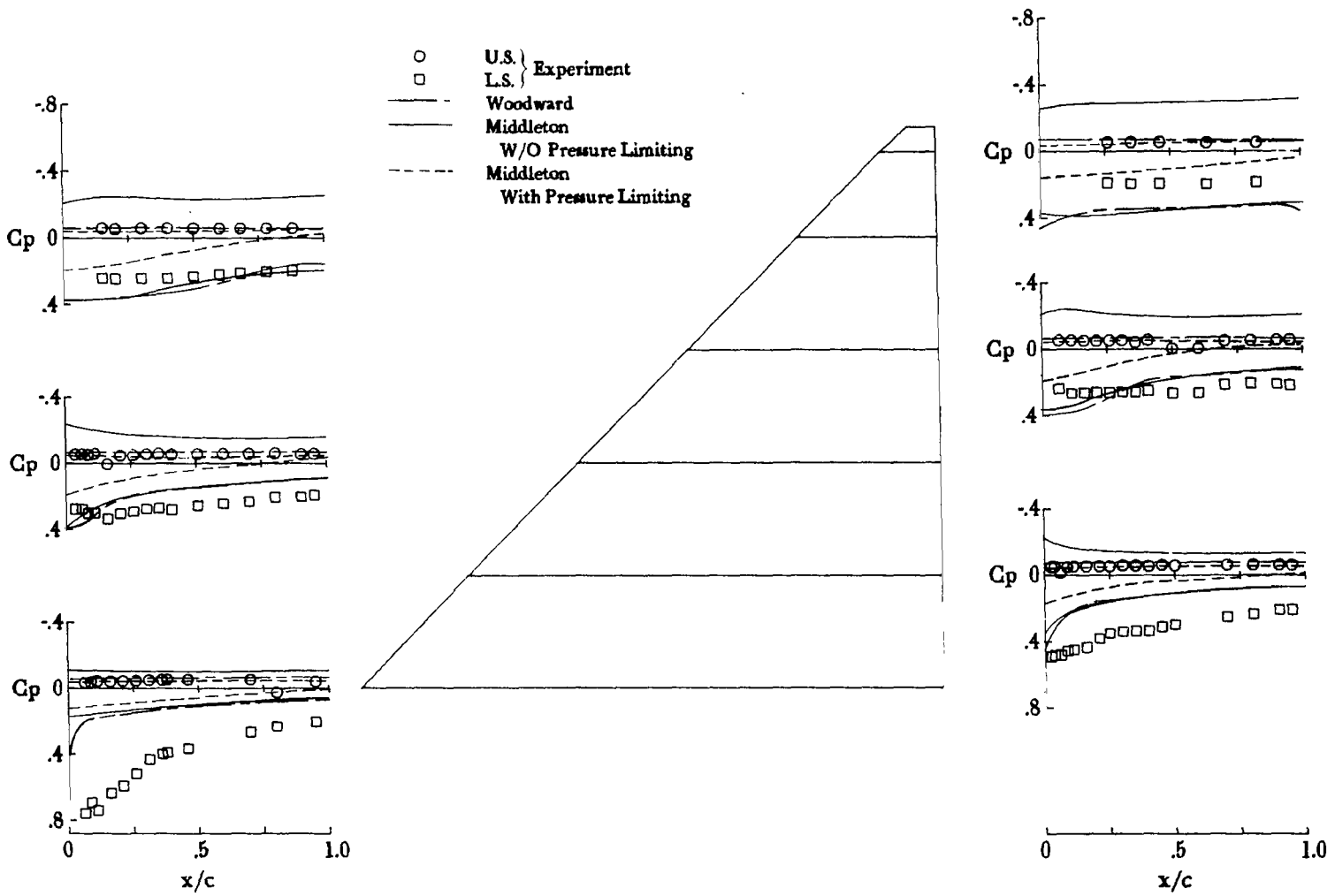
(a) $\alpha = -1.46^{o}$.

Figure 13.- Experimental and theoretical pressure distributions at $\Lambda = 76^{o}$, $C_{L,des} = 0.1$, and $M = 4.6$.



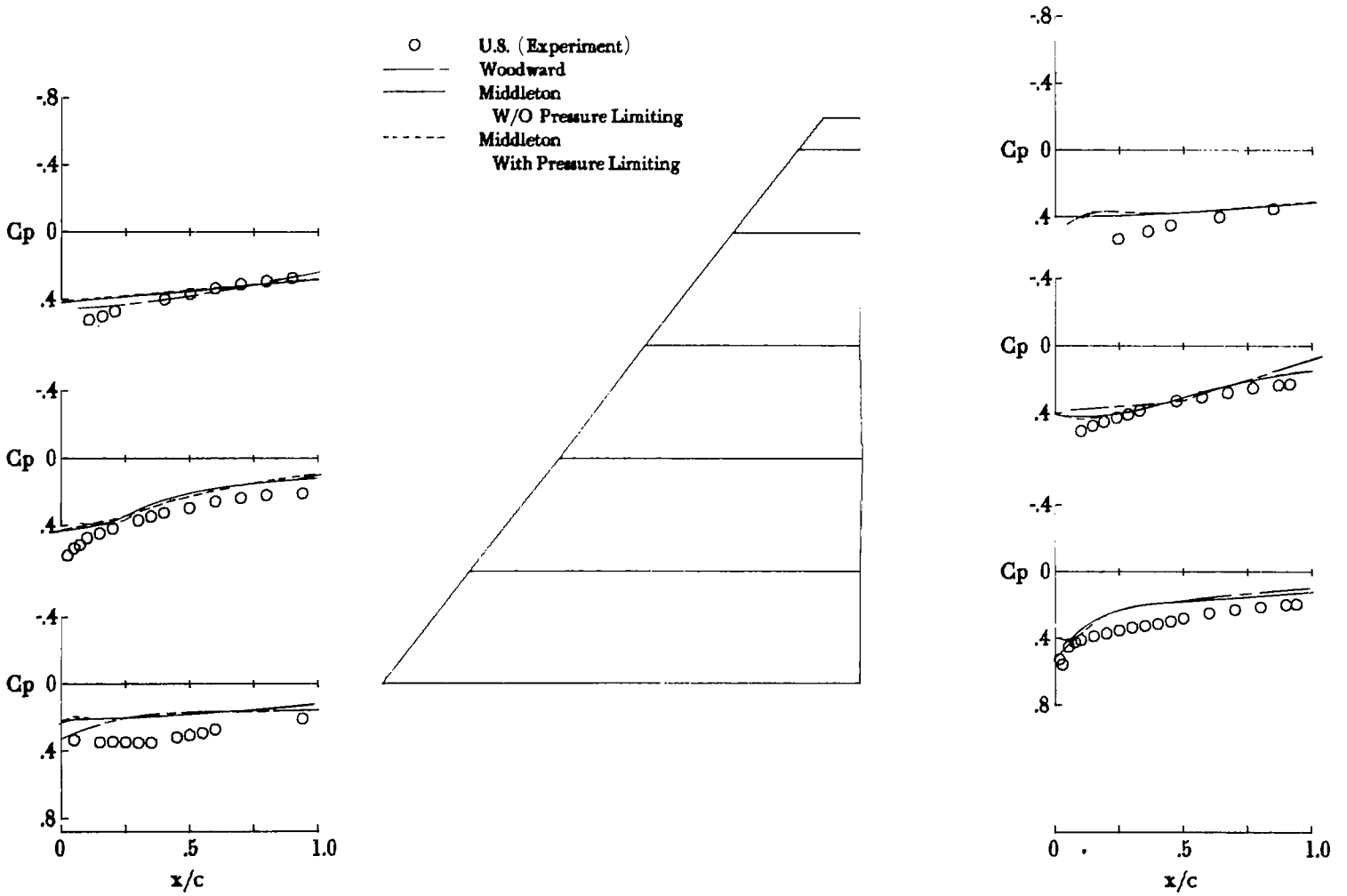
(b) $\alpha = 6.54^{o}$.

Figure 13.- Continued.



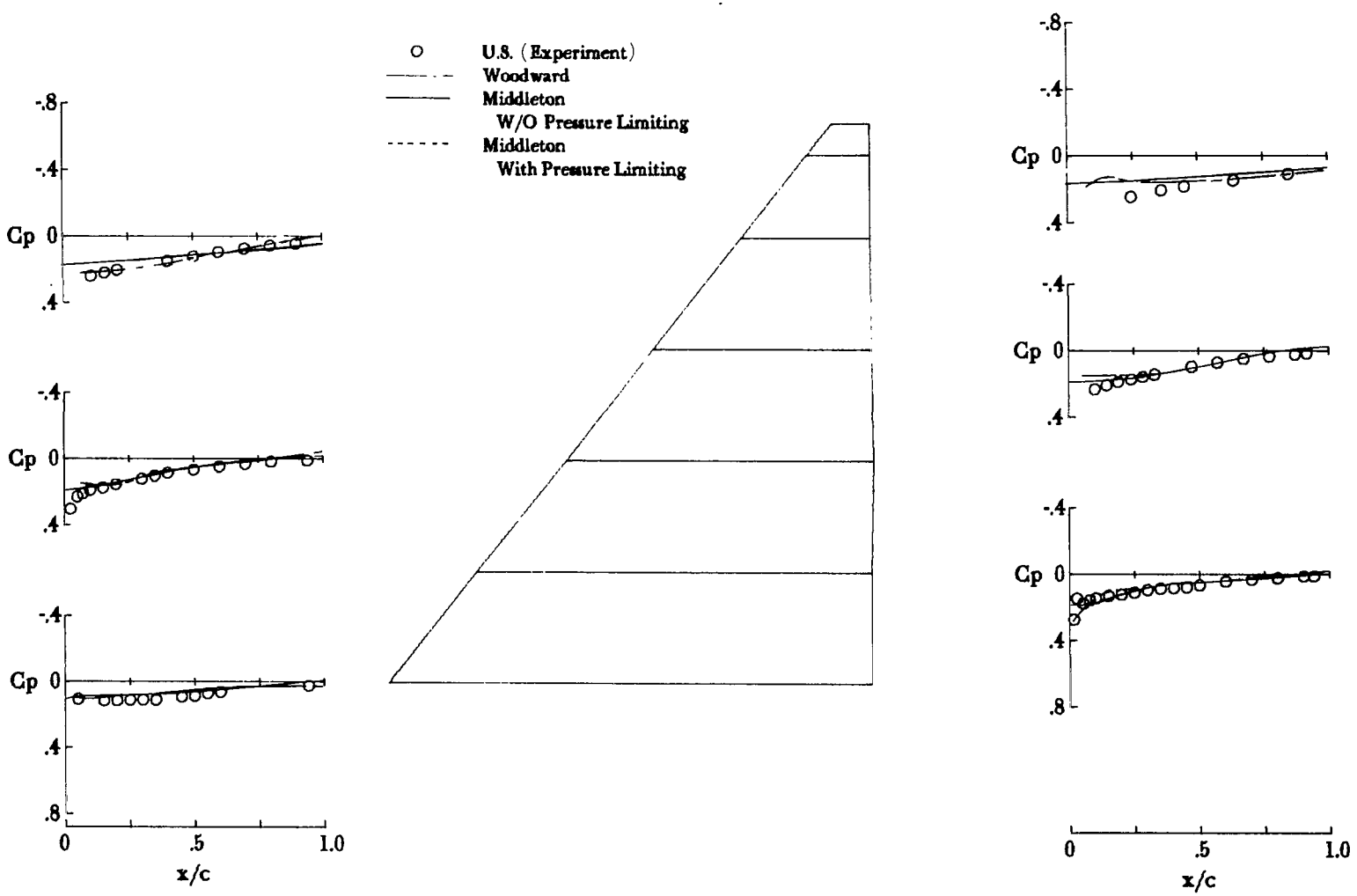
(c) $\alpha = 20.54^{o}$.

Figure 13.- Concluded.



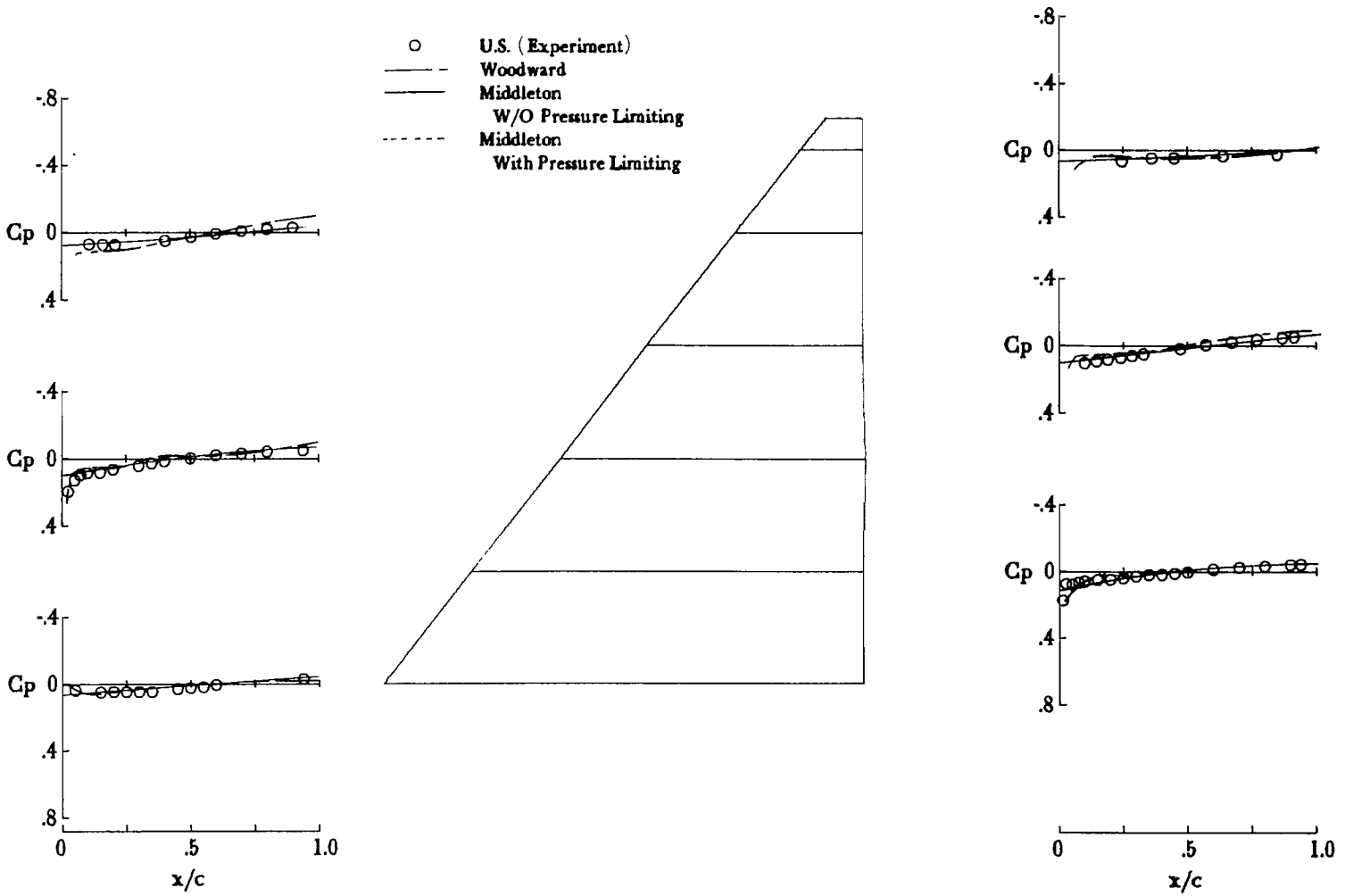
(a) $\alpha = -14.30^{o}$.

Figure 14.- Experimental and theoretical pressure distributions at $\Lambda = 55^{o}$, $C_{L,des} = 0.0$, and $M = 2.3$.



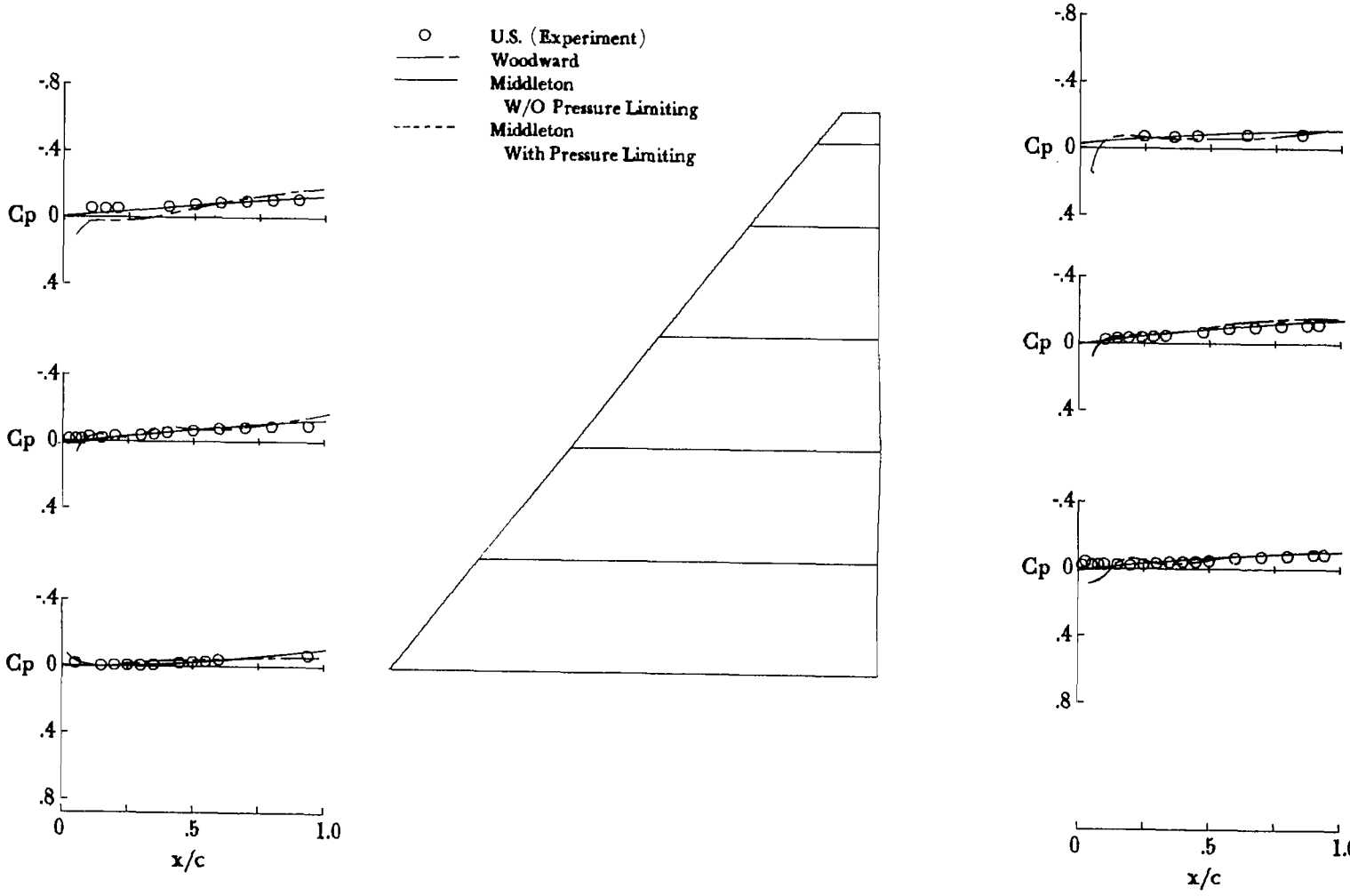
(b) $\alpha = -4.19^{o}$.

Figure 14.- Continued.



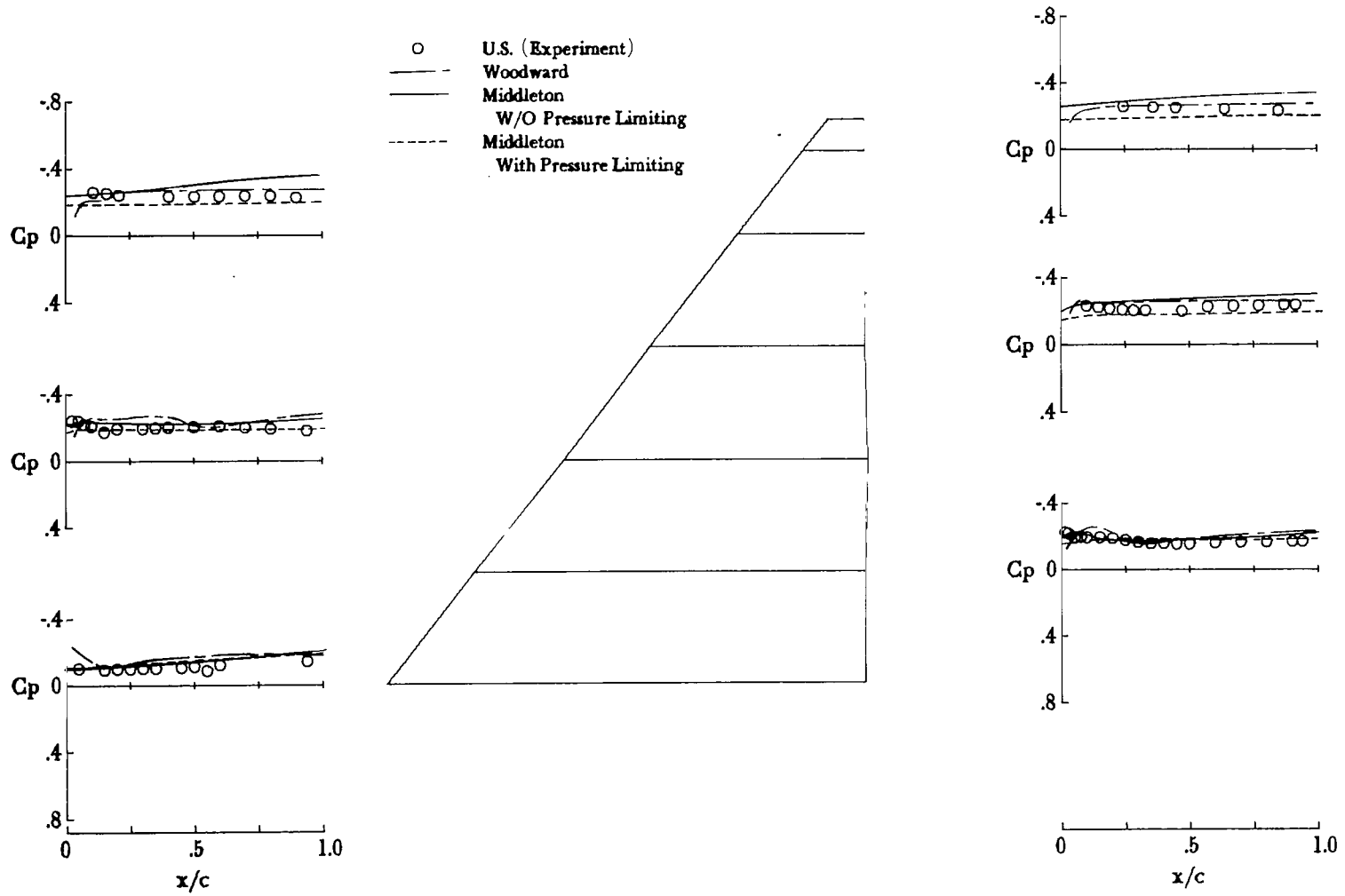
(c) $\alpha = -0.19^{o}$.

Figure 14.- Continued.



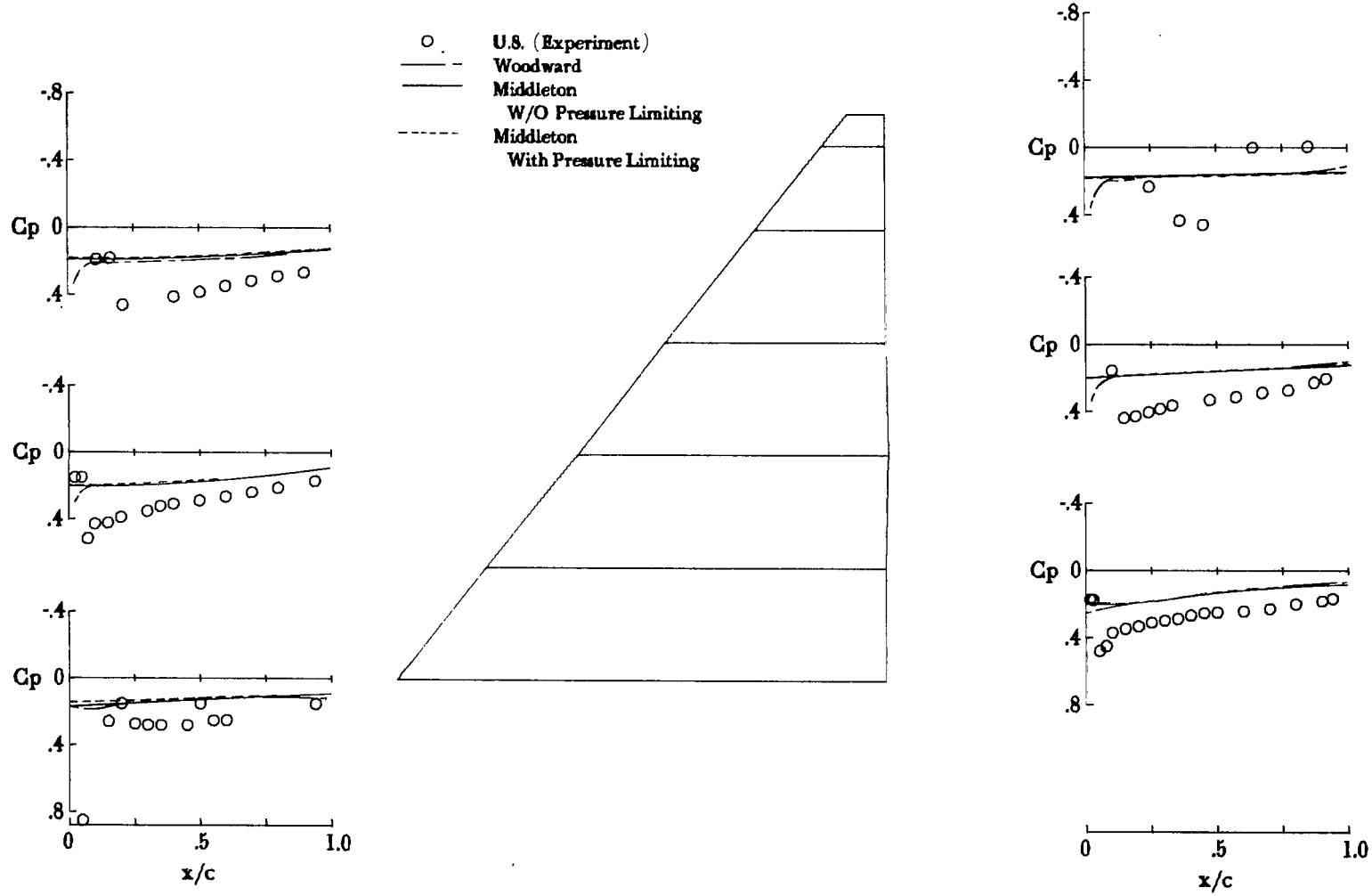
(d) $\alpha = 3.82^{o}$.

Figure 14.- Continued.



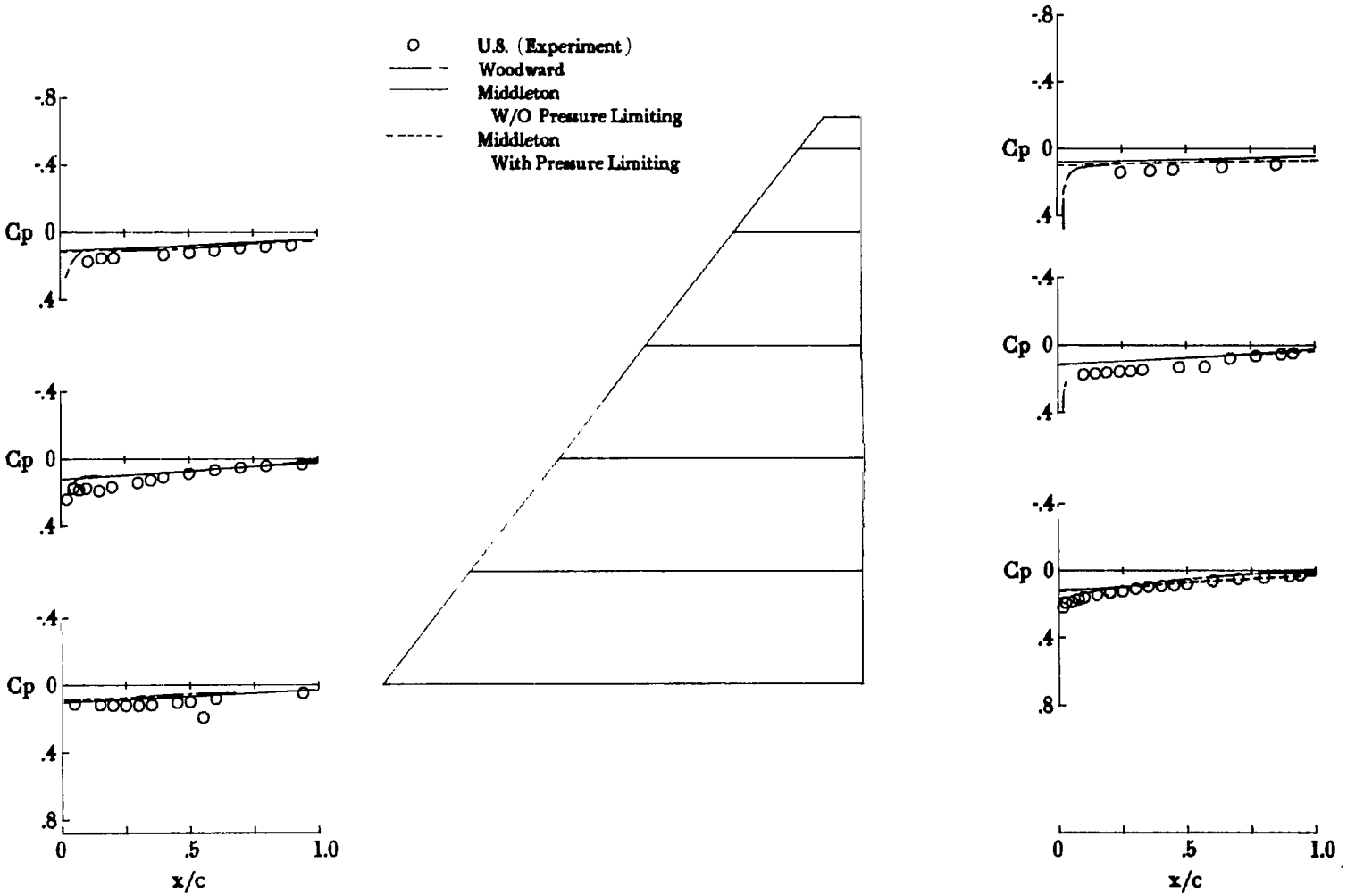
(e) $\alpha = 13.82^{o}$.

Figure 14.- Concluded.



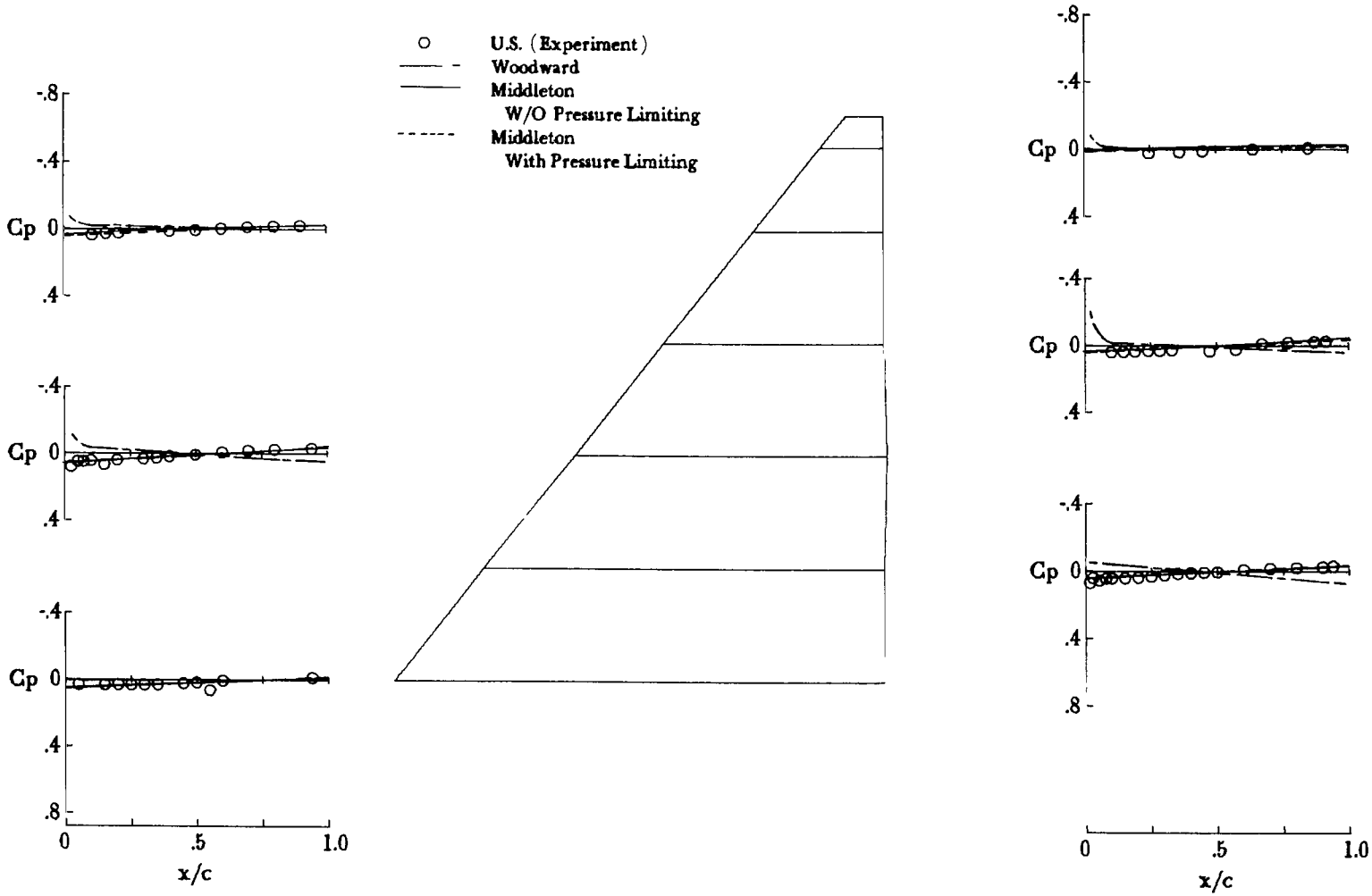
(a) α = -14.40°.

Figure 15.- Experimental and theoretical pressure distributions at $\Lambda = 55^{\circ}$, $C_{L,des} = 0.0$, and $M = 3.5$.



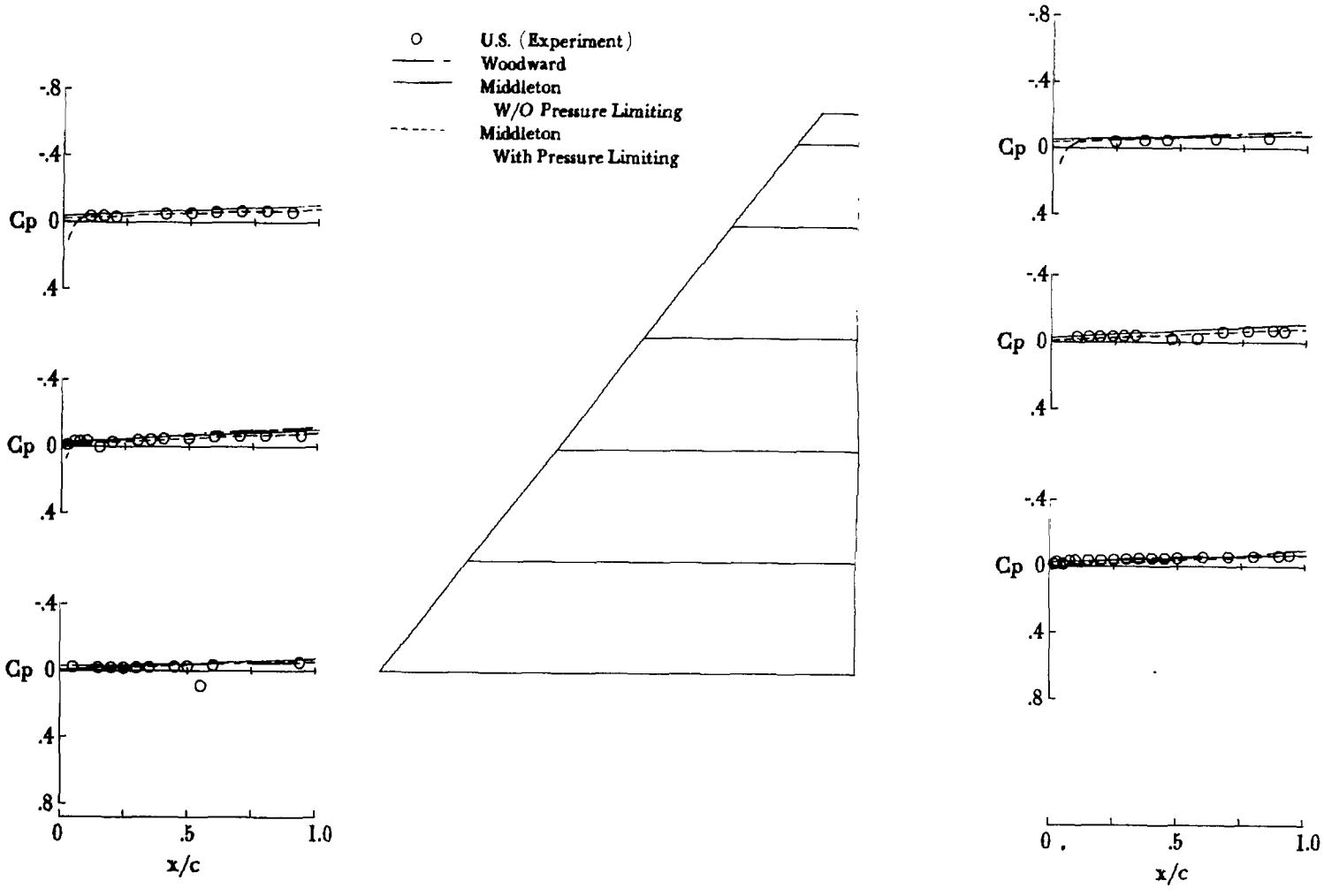
(b) $\alpha = -6.39^{o}$.

Figure 15.- Continued.



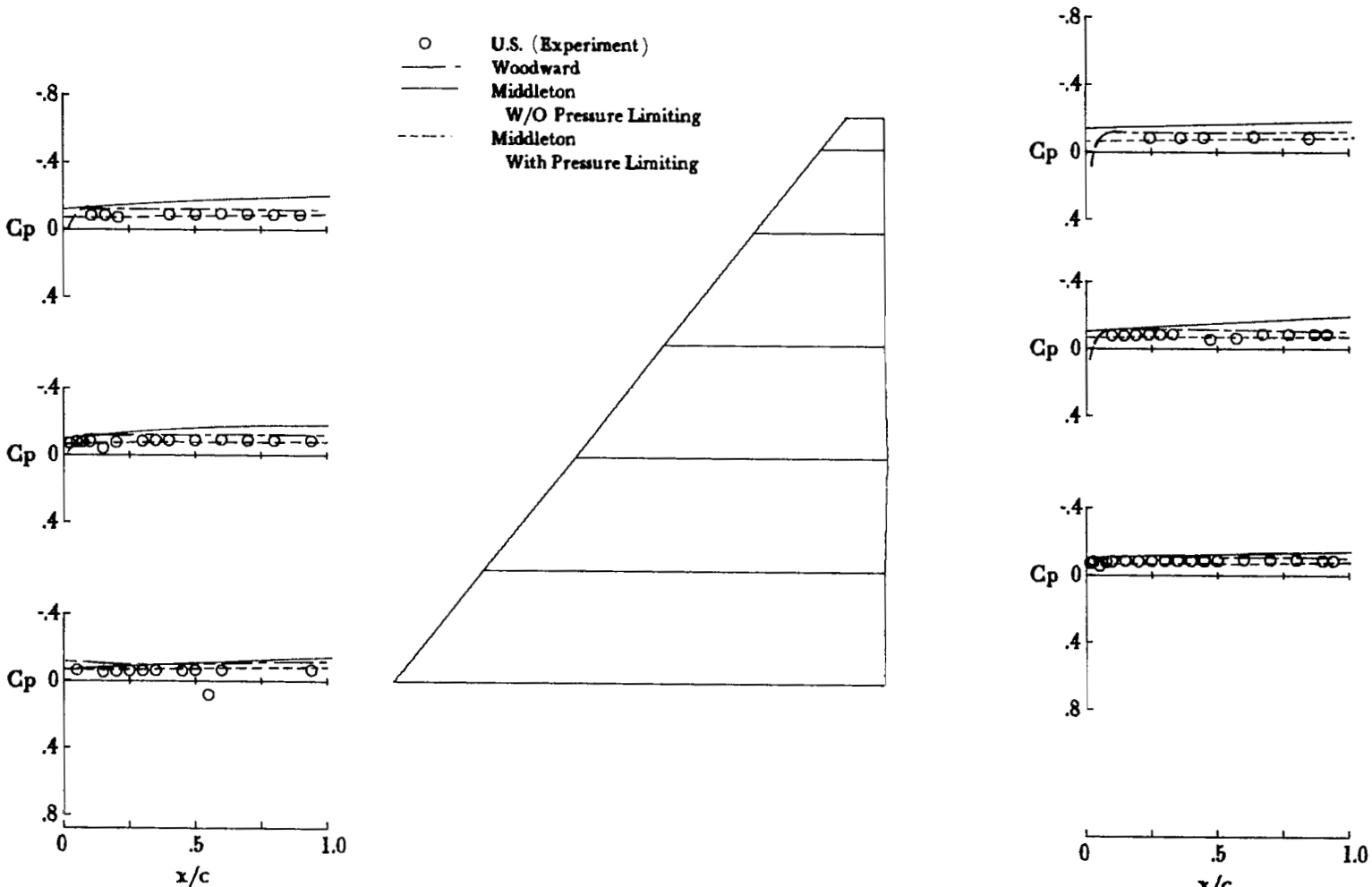
(c) $\alpha = -0.11^{o}$.

Figure 15.- Continued.



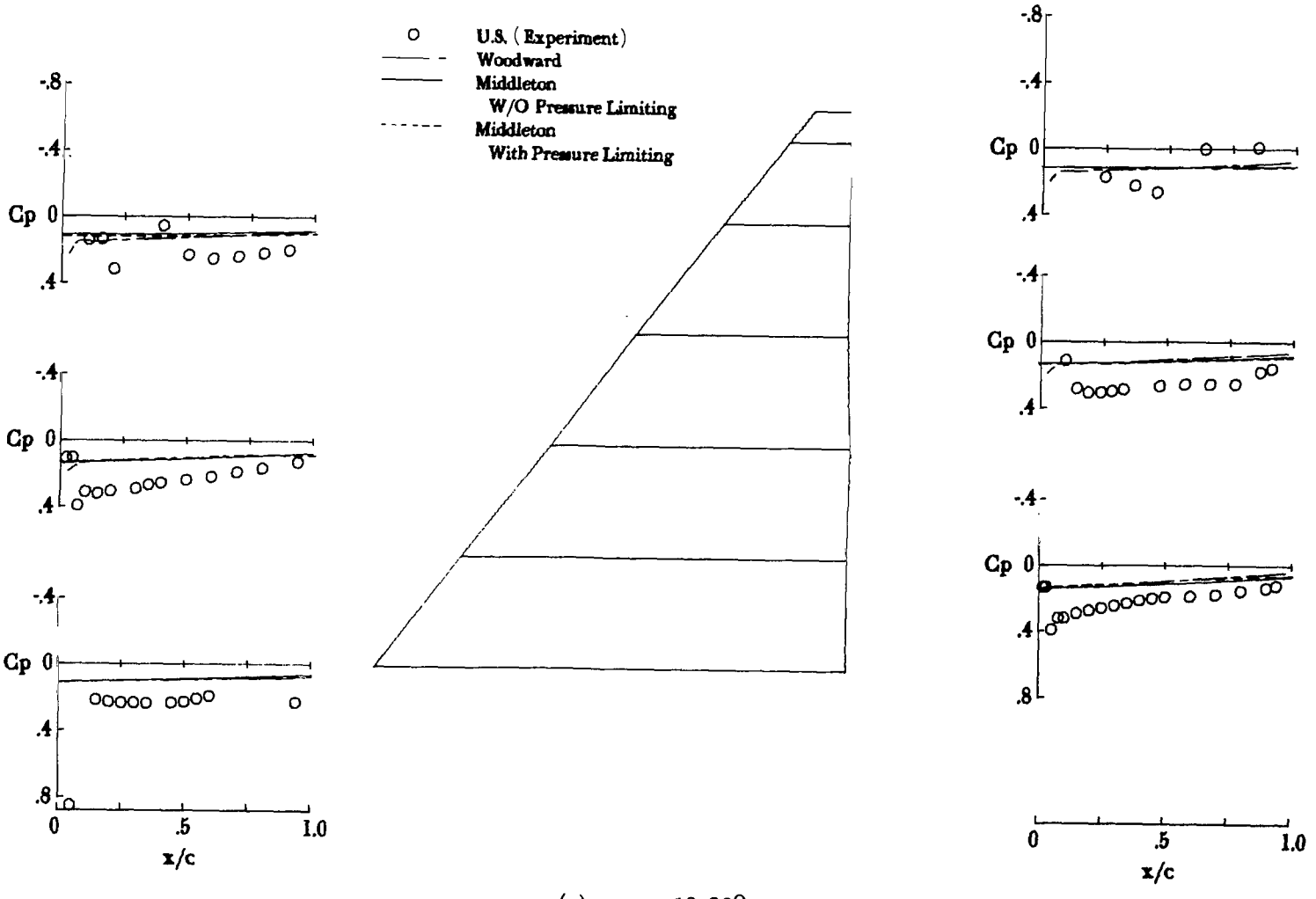
(d) $\alpha = 5.61^{o}$.

Figure 15.- Continued.



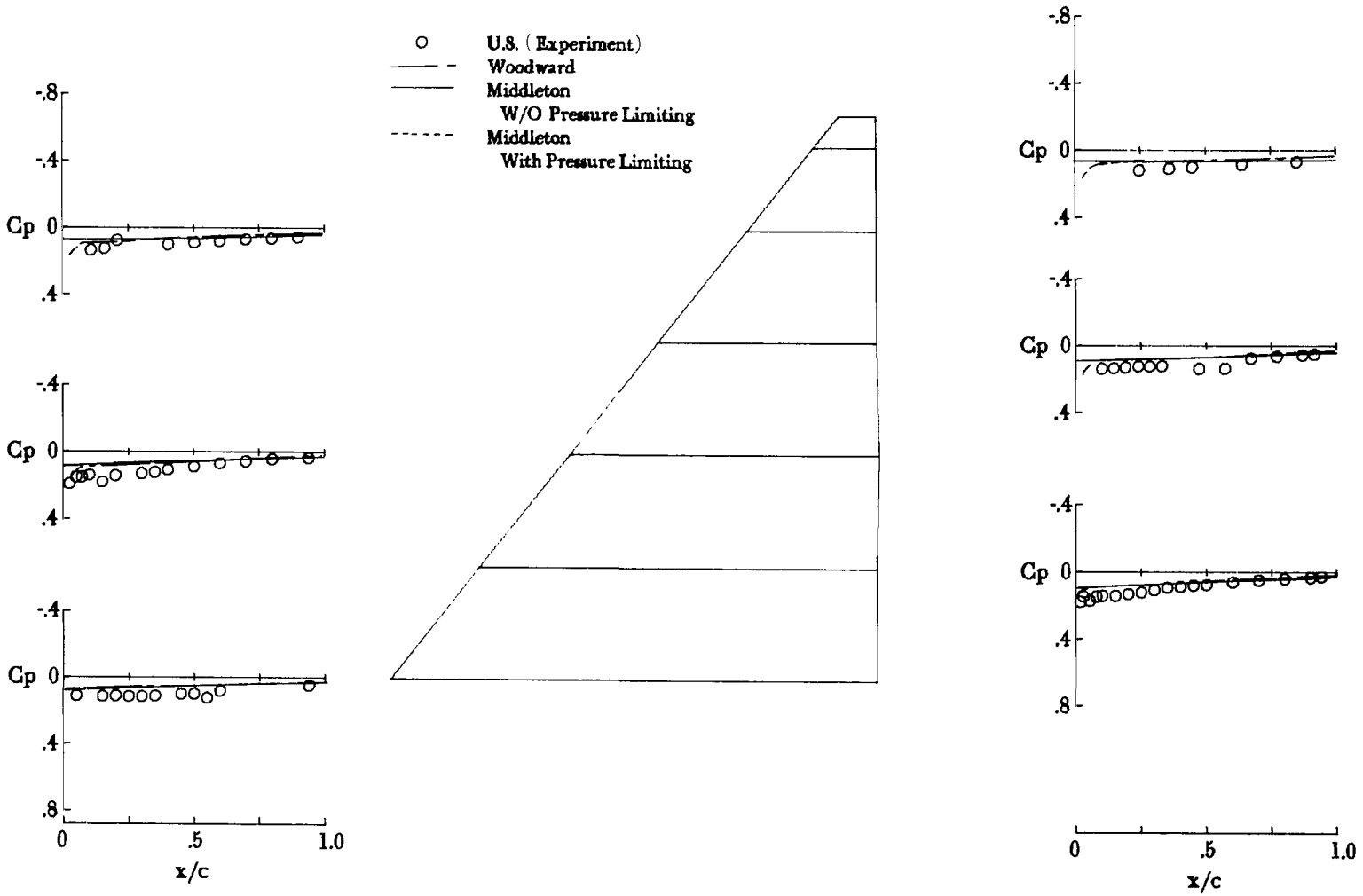
(e) $\alpha = 13.61^{o}$.

Figure 15.- Concluded.



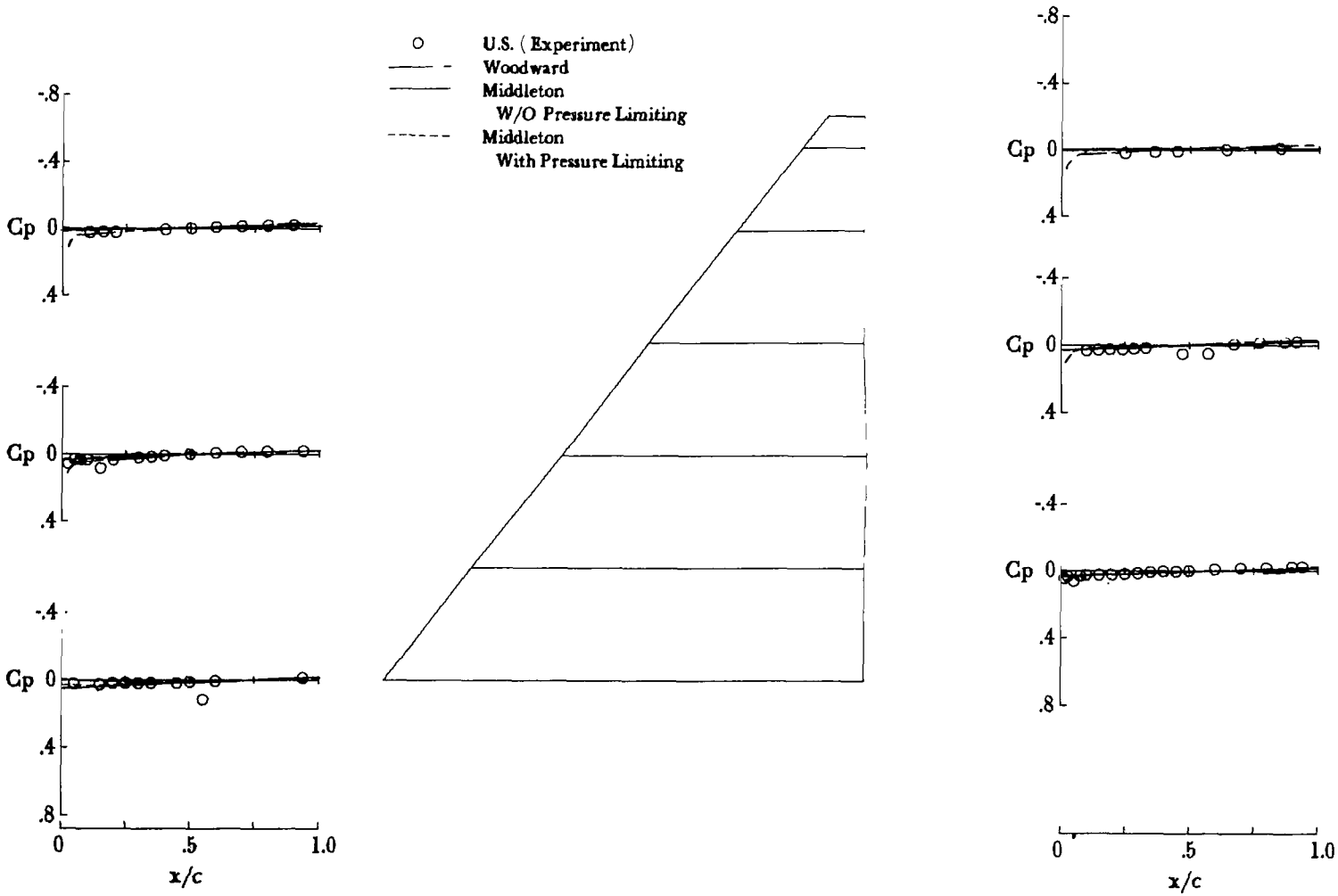
(a) α = -13.20°.

Figure 16.- Experimental and theoretical pressure distributions at $\Lambda = 55^{\circ}$, $C_{L,des} = 0.0$, and $M = 4.6$.



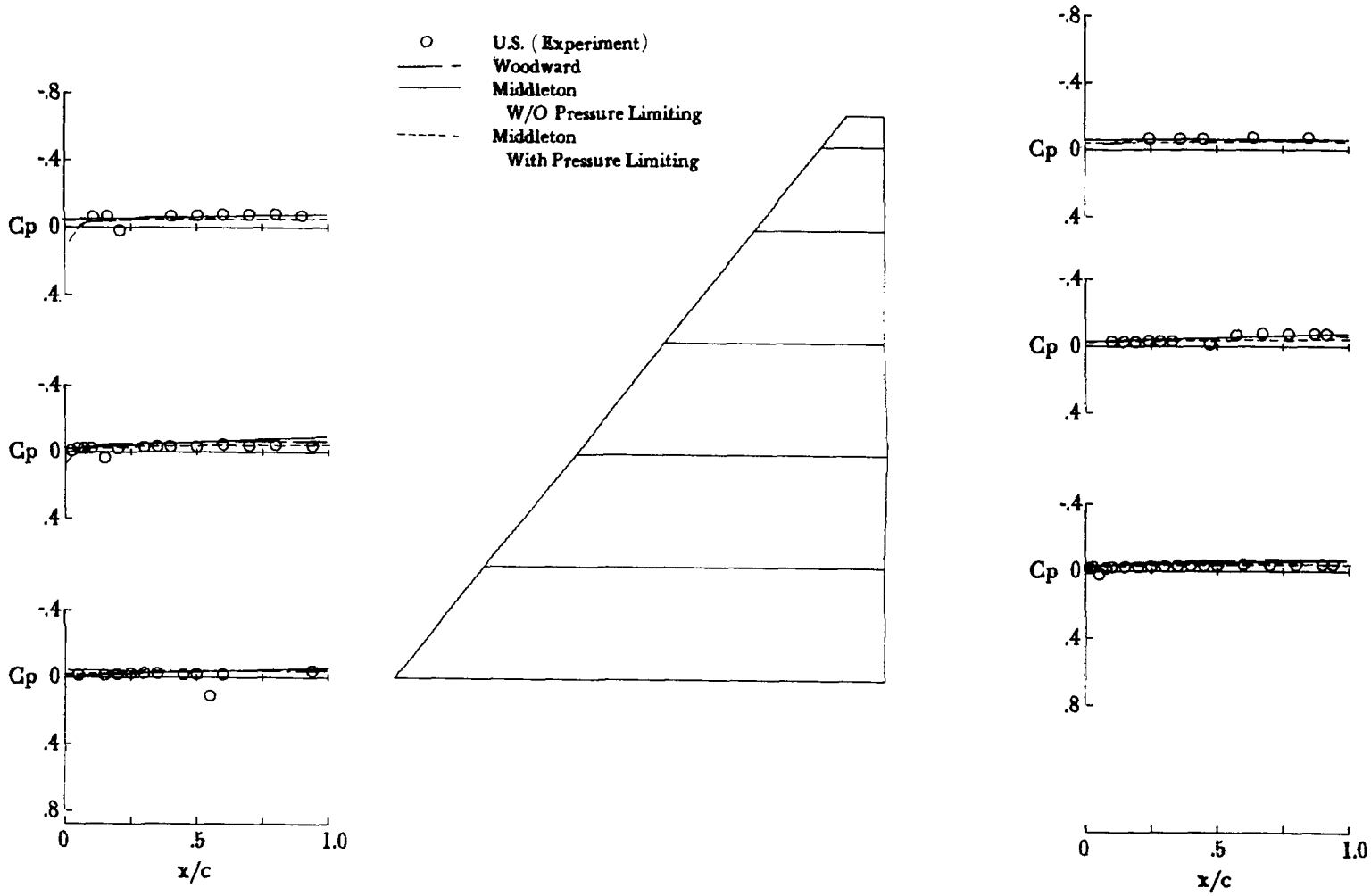
(b) $\alpha = -7.21^{o}$.

Figure 16.- Continued.



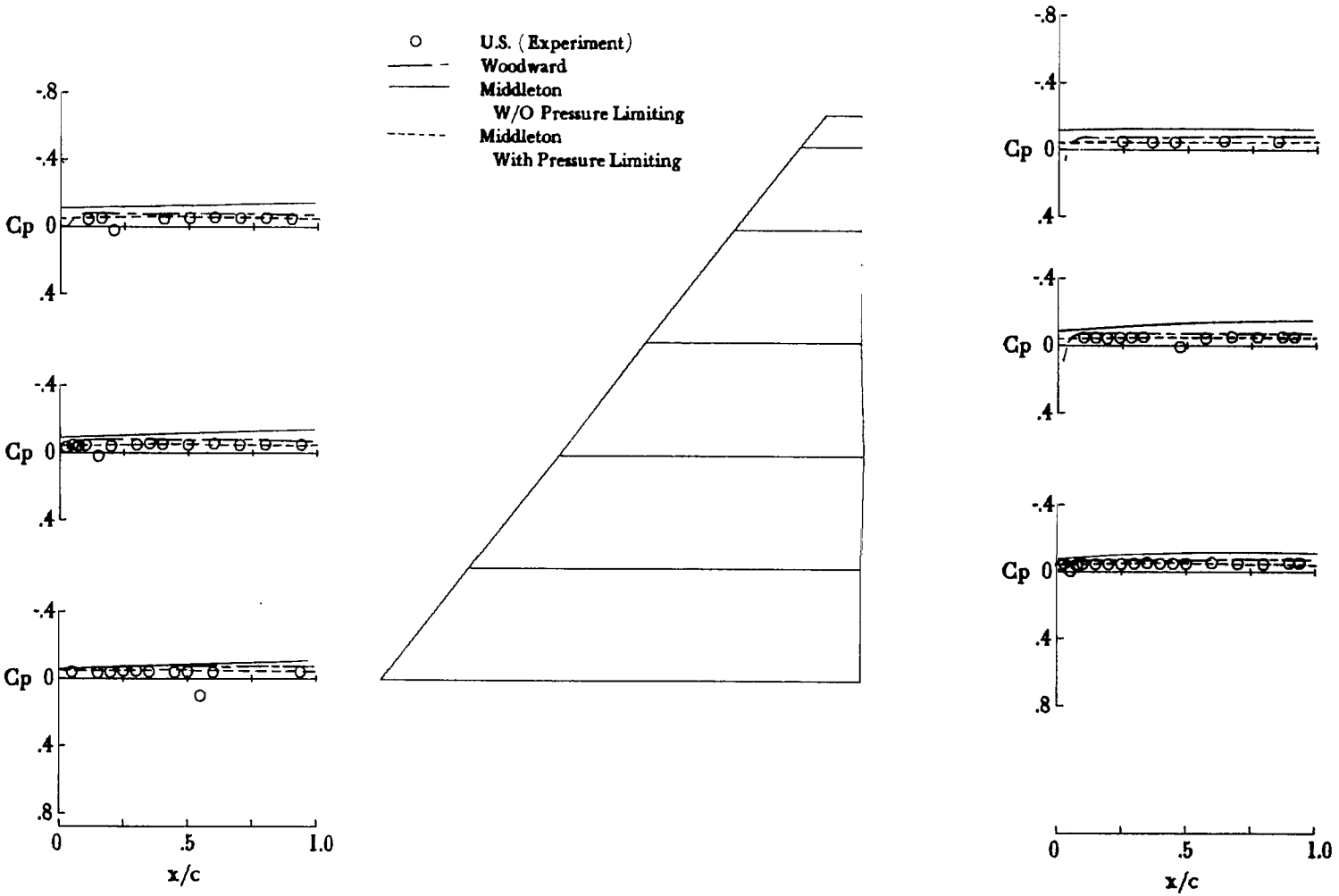
(c) $\alpha = -0.29^{O}$.

Figure 16.- Continued.



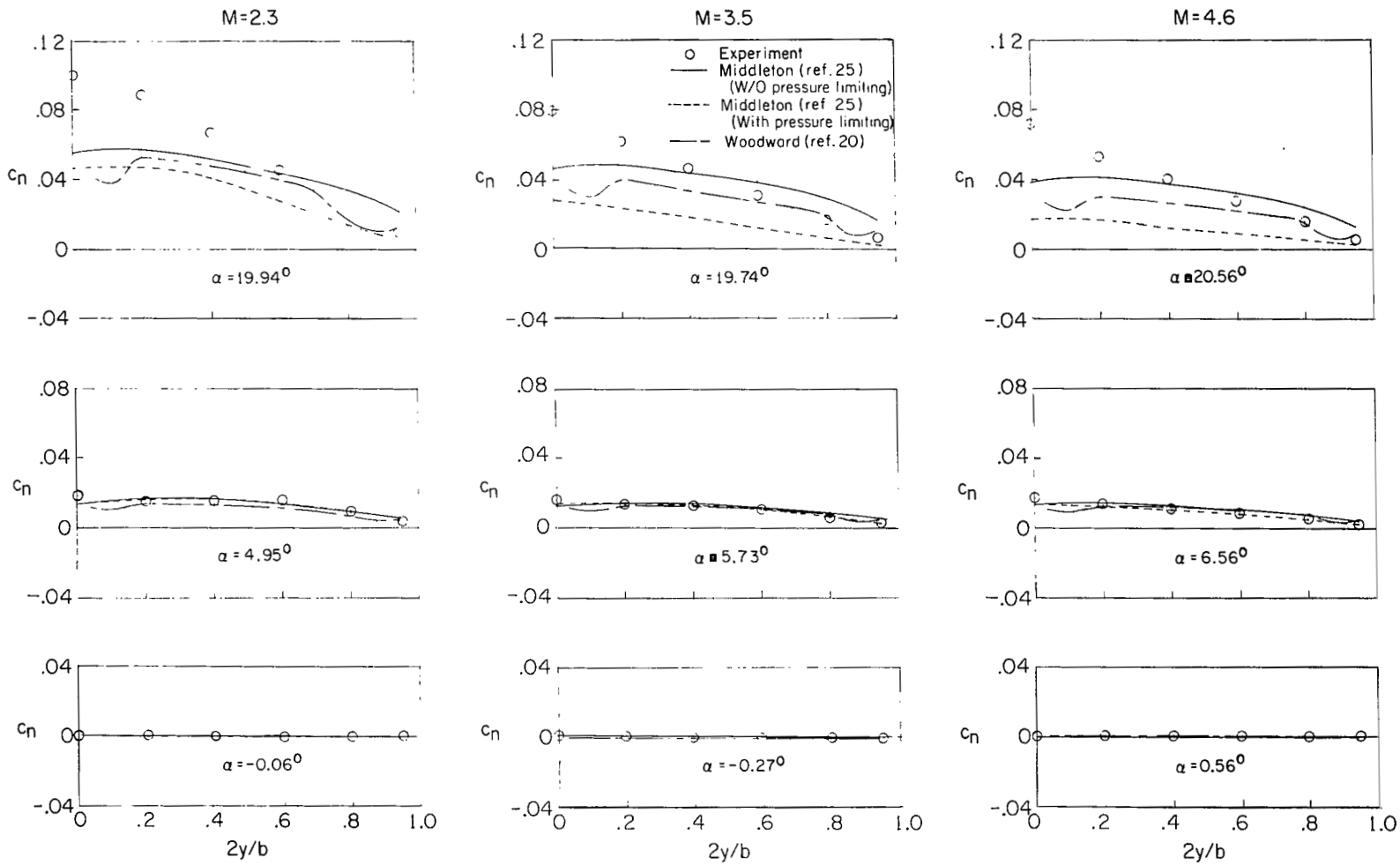
(d) $\alpha = 6.78^{o}$.

Figure 16.- Continued.



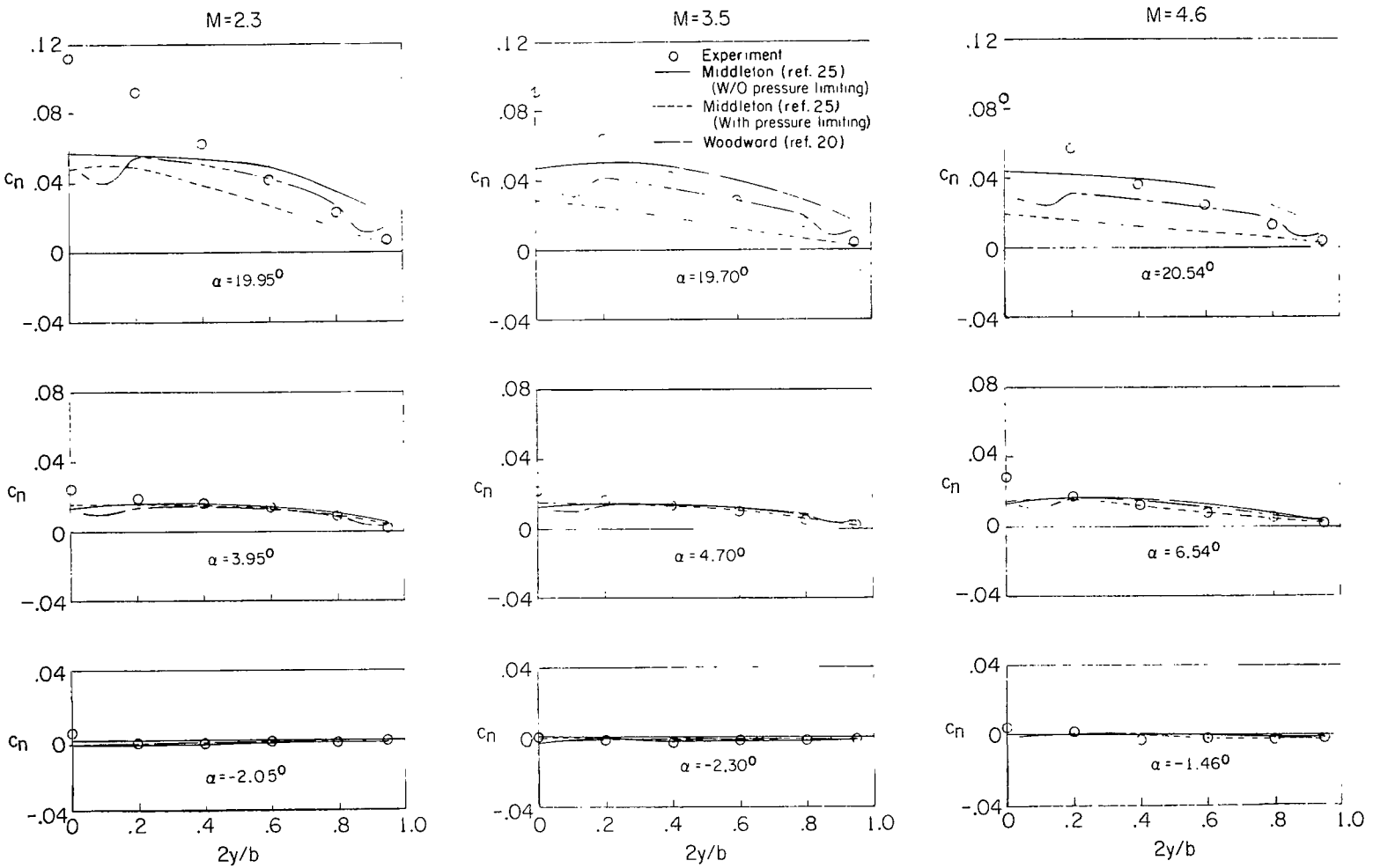
(e) $\alpha = 14.79^{o}$.

Figure 16.- Concluded.



(a) 76° sweep; $C_{L,des} = 0.0$.

Figure 17.- Comparison of experimental and theoretical spanwise lift distributions.



(b) 76^0 sweep; $C_{L,des} = 0.1$.

Figure 17.- Concluded.

APPENDIX A

STABILITY-AXIS COEFFICIENTS

Stability-axis force coefficients for the seven wings tested are given in tables A-1 to A-7 for each of the five test Mach numbers.

APPENDIX A

TABLE A-1.- STABILITY-AXIS FORCE COEFFICIENTS FOR WING WITH 76° SWEEP, $C_{L,des} = 0.0$

M = 2.3

α, deg	C_L	C_D	C_m
-5.34	-.1169	.0176	.0158
-2.80	-.0579	.0100	.0082
-1.50	-.0304	.0083	.0042
-.37	-.0073	.0078	.0010
.81	.0171	.0079	-.0023
2.04	.0424	.0090	-.0058
3.20	.0697	.0111	-.0094
4.45	.0995	.0148	-.0131
5.75	.1305	.0199	-.0169
6.97	.1595	.0262	-.0204
9.47	.2175	.0428	-.0276
14.52	.3328	.0930	-.0421
19.61	.4423	.1645	-.0566
22.29	.4973	.2110	-.0652

M = 3.0

α, deg	C_L	C_D	C_m
-5.14	-.0975	.0146	.0123
-2.62	-.0485	.0085	.0061
-1.57	-.0282	.0073	.0033
-.41	-.0077	.0068	.0007
.67	.0113	.0068	-.0017
1.86	.0326	.0076	-.0043
2.96	.0539	.0091	-.0070
4.11	.0777	.0117	-.0098
5.40	.1024	.0157	-.0126
6.44	.1229	.0198	-.0149
8.87	.1693	.0324	-.0201
13.52	.2565	.0683	-.0305
18.28	.3476	.1218	-.0429
23.08	.4404	.1953	-.0576

M = 3.5

α, deg	C_L	C_D	C_m
-5.07	-.0858	.0131	.0098
-2.81	-.0465	.0080	.0053
-1.71	-.0282	.0067	.0032
-.60	-.0098	.0062	.0010
.51	.0076	.0061	-.0011
1.62	.0250	.0066	-.0029
2.72	.0438	.0079	-.0050
3.85	.0639	.0100	-.0072
4.99	.0840	.0129	-.0094
6.12	.1032	.0166	-.0113
8.36	.1407	.0264	-.0151
12.90	.2184	.0564	-.0238
17.51	.2999	.1019	-.0336
22.09	.3856	.1648	-.0458

M = 4.0

α, deg	C_L	C_D	C_m
-4.62	-.0662	.0108	.0070
-2.29	-.0332	.0067	.0035
-1.23	-.0158	.0060	.0015
-.15	.0008	.0058	-.0005
.94	.0164	.0059	-.0022
2.05	.0335	.0068	-.0039
3.12	.0498	.0083	-.0056
4.20	.0660	.0104	-.0072
5.29	.0838	.0132	-.0090
6.41	.1012	.0170	-.0107
8.62	.1345	.0263	-.0140
13.14	.2065	.0550	-.0217
17.65	.2836	.0981	-.0309
22.10	.3672	.1581	-.0427

M = 4.6

α, deg	C_L	C_D	C_m
-3.98	-.0540	.0090	.0050
-1.88	-.0237	.0062	.0022
-.76	-.0080	.0056	.0006
.33	.0067	.0055	-.0008
1.36	.0201	.0058	-.0020
2.51	.0364	.0067	-.0034
3.51	.0497	.0083	-.0045
4.61	.0649	.0105	-.0059
5.63	.0792	.0131	-.0071
6.72	.0951	.0166	-.0087
8.88	.1248	.0253	-.0115
13.34	.1893	.0515	-.0183
17.82	.2606	.0916	-.0272
22.01	.3375	.1454	-.0386

APPENDIX A

TABLE A-2.- STABILITY-AXIS FORCE COEFFICIENTS FOR WING WITH 76° SWEEP, $C_{L,des} = 0.05$

M = 2.3

α, deg	C_L	C_D	C_m
-5.42	-.1533	.0269	.0222
-2.97	-.0959	.0161	.0144
-1.75	-.0691	.0125	.0108
-.53	-.0391	.0099	.0065
.69	-.0115	.0088	.0026
1.88	.0134	.0085	-.0010
3.06	.0374	.0091	-.0044
4.26	.0628	.0106	-.0080
5.46	.0877	.0130	-.0115
6.68	.1150	.0165	-.0150
9.15	.1727	.0288	-.0217
11.65	.2307	.0467	-.0283
19.21	.3937	.1322	-.0463
20.86	.4272	.1569	-.0507

M = 3.0

α, deg	C_L	C_D	C_m
-5.29	-.1265	.0226	.0173
-2.99	-.0820	.0140	.0111
-1.85	-.0602	.0110	.0085
-.70	-.0377	.0089	.0055
.46	-.0152	.0077	.0026
1.60	.0067	.0073	-.0003
2.75	.0275	.0077	-.0028
3.88	.0481	.0089	-.0055
5.02	.0682	.0107	-.0078
6.17	.0905	.0133	-.0107
8.50	.1355	.0218	-.0156
10.84	.1803	.0350	-.0202
17.81	.3066	.0962	-.0340
22.52	.3919	.1582	-.0449

M = 3.5

α, deg	C_L	C_D	C_m
-5.26	-.1116	.0204	.0139
-3.03	-.0735	.0129	.0092
-1.91	-.0551	.0103	.0072
-.80	-.0358	.0084	.0048
.30	-.0172	.0072	.0026
1.42	.0021	.0067	.0002
2.53	.0201	.0069	-.0016
3.63	.0380	.0078	-.0036
4.75	.0564	.0093	-.0055
5.86	.0756	.0115	-.0077
8.10	.1137	.0184	-.0114
10.35	.1518	.0289	-.0150
17.11	.2624	.0800	-.0253
21.69	.3409	.1333	-.0340

M = 4.0

α, deg	C_L	C_D	C_m
-4.70	-.0913	.0166	.0112
-2.51	-.0581	.0107	.0073
-1.43	-.0415	.0086	.0052
-.32	-.0247	.0072	.0033
.75	-.0080	.0065	.0012
1.86	.0088	.0064	-.0007
2.98	.0256	.0068	-.0023
4.02	.0416	.0079	-.0040
5.11	.0582	.0095	-.0057
6.22	.0756	.0119	-.0073
8.41	.1092	.0187	-.0105
10.61	.1423	.0285	-.0132
17.25	.2455	.0764	-.0226
21.77	.3230	.1278	-.0308

M = 4.6

α, deg	C_L	C_D	C_m
-4.18	-.0766	.0141	.0086
-2.07	-.0473	.0092	.0054
-1.01	-.0326	.0076	.0036
.06	-.0178	.0065	.0023
1.11	-.0030	.0060	.0008
2.19	.0118	.0060	-.0004
3.26	.0267	.0066	-.0017
4.33	.0415	.0077	-.0030
5.40	.0561	.0093	-.0043
6.45	.0706	.0115	-.0057
8.61	.1005	.0179	-.0081
10.77	.1307	.0270	-.0106
17.25	.2250	.0704	-.0190
21.64	.2983	.1178	-.0274

TABLE A-3.- STABILITY-AXIS FORCE COEFFICIENTS FOR WING WITH 76° SWEEP, $C_{L,des} = 0.1$

M = 2.3

α, deg	C_L	C_D	C_m
-4.93	-.0841	.0146	.0187
-2.44	-.0252	.0094	.0107
-1.17	.0022	.0086	.0064
.01	.0277	.0089	.0027
1.22	.0531	.0102	-.0003
2.45	.0776	.0124	-.0029
3.66	.1045	.0155	-.0057
4.91	.1333	.0206	-.0083
6.20	.1628	.0274	-.0110
7.43	.1905	.0351	-.0132
9.97	.2450	.0549	-.0179
13.57	.3189	.0922	-.0251
18.15	.4068	.1527	-.0342
22.73	.4912	.2289	-.0441

M = 3.0

α, deg	C_L	C_D	C_m
-4.74	-.0644	.0121	.0142
-2.43	-.0198	.0083	.0063
-1.29	.0016	.0077	.0056
-.13	.0231	.0080	.0030
1.01	.0439	.0091	.0006
2.19	.0648	.0109	-.0016
3.34	.0862	.0135	-.0035
4.52	.1088	.0171	-.0055
5.66	.1305	.0216	-.0073
6.83	.1521	.0275	-.0091
9.17	.1920	.0417	-.0121
13.90	.2705	.0810	-.0186
18.68	.3502	.1363	-.0264
23.36	.4302	.2081	-.0361

M = 3.5

α, deg	C_L	C_D	C_m
-4.90	-.0584	.0114	.0123
-2.68	-.0200	.0079	.0077
-1.51	-.0004	.0073	.0055
-.41	.0178	.0074	.0036
.70	.0354	.0082	.0019
1.81	.0536	.0098	.0002
2.93	.0718	.0119	-.0014
4.01	.0899	.0147	-.0027
5.28	.1100	.0188	-.0043
6.29	.1271	.0231	-.0055
8.61	.1621	.0348	-.0077
13.15	.2311	.0673	-.0124
17.81	.3035	.1145	-.0178
22.43	.3803	.1783	-.0255

M = 4.0

α, deg	C_L	C_D	C_m
-4.37	-.0421	.0096	.0094
-2.17	-.0092	.0072	.0060
-1.04	.0072	.0069	.0043
.09	.0244	.0073	.0024
1.12	.0401	.0084	.0011
2.27	.0566	.0101	-.0001
3.34	.0722	.0124	-.0014
4.47	.0893	.0154	-.0027
5.60	.1055	.0191	-.0037
6.68	.1214	.0234	-.0048
8.84	.1522	.0339	-.0064
13.34	.2161	.0646	-.0100
17.89	.2863	.1093	-.0154
22.48	.3620	.1710	-.0224

M = 4.6

α, deg	C_L	C_D	C_m
-3.86	-.0323	.0085	.0078
-1.84	-.0031	.0069	.0051
-.68	.0116	.0067	.0040
.40	.0253	.0072	.0032
1.43	.0399	.0084	.0020
2.56	.0546	.0101	.0011
3.53	.0682	.0123	.0004
4.67	.0817	.0150	-.0004
5.75	.0961	.0183	-.0012
6.82	.1102	.0222	-.0019
9.04	.1400	.0322	-.0035
13.43	.1968	.0597	-.0065
17.60	.2599	.0986	-.0113
22.14	.3291	.1536	-.0183

TABLE A-4.- STABILITY-AXIS FORCE COEFFICIENTS FOR WING WITH 68° SWEEP, $C_{L,des} = 0.0$

M = 2.3				M = 3.0			
α, deg	C_L	C_D	C_m	α, deg	C_L	C_D	C_m
-5.62	-.1512	.0224	.0169	-5.18	-.1145	.0177	.0121
-2.97	-.0772	.0125	.0081	-2.72	-.0601	.0107	.0060
-.37	-.0073	.0093	-.0002	-.41	-.0089	.0083	.0004
2.27	.0628	.0113	-.0085	1.99	.0455	.0095	-.0057
4.87	.1378	.0198	-.0173	4.39	.1009	.0153	-.0117
6.20	.1744	.0269	-.0217	5.65	.1294	.0203	-.0149
7.55	.2117	.0360	-.0259	6.80	.1548	.0259	-.0176
8.83	.2441	.0459	-.0298	8.01	.1810	.0329	-.0206
10.17	.2794	.0581	-.0339	9.26	.2076	.0415	-.0235
11.51	.3123	.0716	-.0378	10.40	.2322	.0503	-.0263
12.79	.3458	.0866	-.0420	11.66	.2578	.0611	-.0292
13.74	.3690	.0989	-.0451	14.04	.3071	.0851	-.0350
18.47	.4831	.1706	-.0601	18.95	.4081	.1495	-.0484
23.14	.5867	.2606	-.0757	21.14	.4523	.1846	-.0549
M = 3.5				M = 4.0			
α, deg	C_L	C_D	C_m	α, deg	C_L	C_D	C_m
-5.14	-.0996	.0159	.0094	-4.51	-.0780	.0128	.0070
-2.85	-.0551	.0101	.0050	-2.31	-.0394	.0086	.0033
-.57	-.0112	.0078	.0006	-.08	-.0007	.0071	-.0004
1.71	.0337	.0084	-.0040	2.19	.0383	.0083	-.0040
4.02	.0801	.0126	-.0084	4.40	.0780	.0127	-.0079
5.15	.1024	.0161	-.0107	5.53	.0981	.0162	-.0098
6.33	.1259	.0210	-.0132	6.61	.1166	.0204	-.0114
7.46	.1465	.0263	-.0151	7.77	.1371	.0258	-.0136
8.59	.1683	.0328	-.0173	8.91	.1568	.0318	-.0154
9.84	.1920	.0408	-.0199	10.08	.1770	.0390	-.0175
10.93	.2133	.0489	-.0222	11.15	.1969	.0466	-.0195
13.25	.2577	.0689	-.0270	13.41	.2369	.0649	-.0238
17.95	.3494	.1227	-.0378	18.05	.3242	.1155	-.0341
22.66	.4437	.1961	-.0510	22.64	.4160	.1848	-.0465
M = 4.6							
α, deg	C_L	C_D	C_m				
-4.11	-.0640	.0113	.0048				
-1.97	-.0296	.0076	.0019				
.20	.0049	.0066	-.0007				
2.48	.0406	.0083	-.0036				
4.54	.0734	.0125	-.0063				
5.64	.0905	.0156	-.0078				
6.83	.1095	.0200	-.0095				
7.86	.1255	.0243	-.0110				
8.99	.1442	.0301	-.0129				
10.04	.1618	.0361	-.0147				
11.09	.1782	.0426	-.0163				
13.51	.2188	.0610	-.0204				
17.73	.2943	.1039	-.0295				
22.04	.3779	.1644	-.0413				

APPENDIX A

TABLE A-5.- STABILITY-AXIS FORCE COEFFICIENTS FOR WING WITH 68° SWEEP, $C_{L,des} = 0.1$

M = 2.3

α, deg	C_L	C_D	C_m
-6.05	-.2290	.0430	.0356
-3.45	-.1597	.0255	.0264
-.79	-.0851	.0140	.0166
1.86	-.0108	.0097	.0071
4.50	.0632	.0117	-.0016
5.86	.1018	.0151	-.0059
7.09	.1417	.0201	-.0106
8.55	.1779	.0272	-.0146
9.85	.2119	.0355	-.0184
11.19	.2463	.0457	-.0220
12.54	.2802	.0578	-.0259
13.80	.3097	.0702	-.0288
18.34	.4129	.1270	-.0407
22.83	.5076	.1994	-.0531

M = 3.0

α, deg	C_L	C_D	C_m
-5.49	-.1748	.0327	.0261
-3.12	-.1225	.0203	.0189
-.67	-.0696	.0121	.0123
1.73	-.0132	.0087	.0057
4.16	.0439	.0100	-.0006
5.36	.0714	.0122	-.0037
6.57	.0987	.0155	-.0066
7.85	.1254	.0201	-.0093
8.98	.1526	.0257	-.0120
10.22	.1794	.0328	-.0145
11.41	.2047	.0406	-.0170
13.85	.2537	.0599	-.0215
18.76	.3487	.1123	-.0310
19.36	.3596	.1198	-.0321

M = 3.5

α, deg	C_L	C_D	C_m
-5.39	-.1505	.0289	.0214
-3.10	-.1072	.0184	.0159
-.80	-.0626	.0116	.0107
1.76	-.0176	.0080	.0058
3.79	.0296	.0090	.0008
4.96	.0528	.0106	-.0014
6.08	.0765	.0132	-.0038
7.28	.1002	.0167	-.0061
8.43	.1224	.0210	-.0079
9.60	.1450	.0264	-.0097
10.76	.1675	.0329	-.0117
13.10	.2118	.0488	-.0154
17.81	.2977	.0924	-.0219
22.45	.3804	.1511	-.0298

M = 4.0

α, deg	C_L	C_D	C_m
-4.74	-.1227	.0235	.0172
-2.55	-.0842	.0151	.0125
-.27	-.0469	.0098	.0084
1.98	-.0070	.0077	.0041
4.20	.0329	.0088	-.0000
5.33	.0533	.0105	-.0019
6.46	.0742	.0130	-.0039
7.60	.0950	.0165	-.0059
8.73	.1149	.0207	-.0075
9.86	.1347	.0257	-.0089
11.18	.1550	.0320	-.0105
13.13	.1946	.0459	-.0133
17.85	.2751	.0866	-.0192
22.37	.3571	.1426	-.0261

M = 4.6

α, deg	C_L	C_D	C_m
-4.19	-.1051	.0202	.0139
-2.02	-.0708	.0132	.0101
.16	-.0370	.0089	.0069
2.35	-.0010	.0072	.0034
4.53	.0340	.0084	.0004
5.61	.0515	.0100	-.0011
6.71	.0697	.0126	-.0026
7.84	.0887	.0161	-.0044
8.90	.1058	.0198	-.0056
9.97	.1227	.0243	-.0069
11.11	.1413	.0299	-.0082
13.33	.1769	.0431	-.0105
17.72	.2520	.0798	-.0162
22.23	.3291	.1316	-.0230

APPENDIX A

TABLE A-6.- STABILITY-AXIS FORCE COEFFICIENTS FOR WING WITH 55° SWEEP, $C_{L,des} = 0.0$

M = 2.3

α, deg	C_L	C_D	C_m
-5.61	-.1806	.0278	.0210
-2.94	-.0960	.0154	.0115
-.23	-.0073	.0109	.0021
2.46	.0819	.0143	-.0076
3.74	.1221	.0187	-.0120
5.15	.1665	.0256	-.0170
6.49	.2085	.0343	-.0217
7.72	.2460	.0438	-.0260
9.06	.2871	.0562	-.0308
10.39	.3257	.0701	-.0351
11.67	.3612	.0849	-.0393
12.97	.3990	.1021	-.0439
15.66	.4733	.1428	-.0530
18.61	.5514	.1966	-.0637
23.23	.6633	.2961	-.0800

M = 3.0

α, deg	C_L	C_D	C_m
-5.12	-.1305	.0208	.0145
-2.70	-.0684	.0122	.0079
-.29	-.0078	.0089	.0018
2.17	.0555	.0112	-.0044
3.32	.0857	.0141	-.0077
4.54	.1167	.0187	-.0108
5.74	.1479	.0244	-.0142
6.94	.1776	.0314	-.0173
8.18	.2083	.0398	-.0207
9.37	.2373	.0491	-.0238
10.60	.2663	.0598	-.0270
11.76	.2948	.0715	-.0302
14.18	.3515	.0992	-.0366
19.06	.4652	.1720	-.0513
23.97	.5767	.2684	-.0680

M = 3.5

α, deg	C_L	C_D	C_m
-5.07	-.1086	.0175	.0111
-2.78	-.0587	.0106	.0061
-.48	-.0098	.0078	.0017
1.78	.0385	.0090	-.0027
2.96	.0650	.0113	-.0052
4.08	.0894	.0145	-.0076
5.29	.1149	.0188	-.0097
6.37	.1395	.0240	-.0122
7.55	.1646	.0305	-.0146
8.71	.1901	.0381	-.0171
9.88	.2161	.0469	-.0199
11.03	.2418	.0568	-.0227
13.37	.2929	.0798	-.0283
18.08	.3970	.1411	-.0404
22.81	.5022	.2239	-.0545

M = 4.0

α, deg	C_L	C_D	C_m
-4.43	-.0809	.0134	.0075
-2.20	-.0390	.0085	.0036
.02	.0024	.0071	-.0001
2.25	.0437	.0089	-.0036
3.35	.0647	.0111	-.0054
4.47	.0873	.0143	-.0076
5.58	.1079	.0183	-.0093
6.70	.1302	.0234	-.0112
7.85	.1525	.0294	-.0134
8.95	.1746	.0362	-.0153
10.10	.1980	.0444	-.0175
11.21	.2219	.0535	-.0201
13.51	.2695	.0752	-.0251
18.11	.3675	.1323	-.0366
22.73	.4706	.2107	-.0504

M = 4.6

α, deg	C_L	C_D	C_m
-3.98	-.0646	.0108	.0058
-1.80	-.0281	.0070	.0029
.39	.0077	.0060	.0001
2.54	.0424	.0082	-.0024
3.60	.0616	.0104	-.0042
4.69	.0798	.0133	-.0054
5.77	.0980	.0170	-.0068
6.87	.1175	.0216	-.0085
7.97	.1373	.0270	-.0100
9.03	.1564	.0330	-.0117
10.15	.1775	.0403	-.0136
11.25	.1982	.0484	-.0155
13.51	.2418	.0681	-.0201
17.96	.3340	.1202	-.0313
22.39	.4290	.1904	-.0443

APPENDIX A

TABLE A-7.- STABILITY-AXIS FORCE COEFFICIENTS FOR WING WITH 55° SWEEP, $C_{L,des} = 0.1$

M = 2.3

α, deg	C_L	C_D	C_m
-5.53	-.2095	.0348	.0238
-3.26	-.1399	.0214	.0153
-.58	-.0537	.0127	.0053
2.09	.0347	.0120	-.0045
3.43	.0775	.0145	-.0094
4.76	.1213	.0191	-.0142
6.10	.1634	.0256	-.0190
7.42	.2056	.0339	-.0237
8.81	.2480	.0447	-.0286
10.06	.2850	.0560	-.0327
11.40	.3238	.0699	-.0373
12.70	.3613	.0852	-.0414
15.33	.4321	.1206	-.0495

M = 3.0

α, deg	C_L	C_D	C_m
-5.37	-.1641	.0283	.0178
-2.94	-.1023	.0167	.0106
-.55	-.0412	.0105	.0039
1.86	.0202	.0096	-.0026
3.08	.0512	.0112	-.0057
4.29	.0838	.0142	-.0094
5.46	.1128	.0183	-.0123
6.67	.1426	.0238	-.0155
7.90	.1735	.0307	-.0189
9.09	.2029	.0387	-.0220
10.32	.2327	.0481	-.0252
11.49	.2611	.0584	-.0281
13.95	.3199	.0838	-.0345
18.84	.4338	.1507	-.0481
22.19	.5092	.2088	-.0582

M = 3.5

α, deg	C_L	C_D	C_m
-5.23	-.1363	.0236	.0133
-2.90	-.0860	.0142	.0079
-.63	-.0365	.0093	.0029
1.66	.0126	.0083	-.0018
2.79	.0356	.0094	-.0040
3.94	.0614	.0114	-.0065
5.08	.0866	.0145	-.0089
6.22	.1113	.0186	-.0113
7.39	.1367	.0239	-.0139
8.51	.1605	.0300	-.0162
9.68	.1862	.0374	-.0188
10.83	.2123	.0461	-.0215
13.17	.2635	.0668	-.0268
17.88	.3675	.1227	-.0380
22.56	.4703	.1983	-.0506

M = 4.0

α, deg	C_L	C_D	C_m
-4.52	-.1040	.0180	.0096
-2.34	-.0632	.0113	.0053
-.13	-.0220	.0078	.0012
2.14	.0202	.0078	-.0027
3.22	.0405	.0091	-.0046
4.33	.0614	.0111	-.0066
5.47	.0846	.0144	-.0088
6.55	.1053	.0183	-.0105
7.69	.1273	.0232	-.0126
8.85	.1500	.0292	-.0147
9.91	.1710	.0356	-.0167
11.13	.1963	.0442	-.0191
13.38	.2442	.0636	-.0241
17.99	.3419	.1162	-.0344
22.56	.4423	.1880	-.0467

M = 4.6

α, deg	C_L	C_D	C_m
-4.15	-.0854	.0151	.0067
1.94	-.0482	.0094	.0036
.21	-.0126	.0067	.0007
2.37	.0220	.0070	-.0020
3.44	.0402	.0084	-.0037
4.53	.0585	.0104	-.0052
5.64	.0777	.0134	-.0067
6.65	.0946	.0166	-.0081
7.78	.1151	.0213	-.0097
8.94	.1355	.0268	-.0118
9.99	.1539	.0325	-.0132
11.13	.1743	.0398	-.0152
13.27	.2165	.0566	-.0194
17.79	.3089	.1047	-.0295
22.20	.4031	.1695	-.0414

APPENDIX B

PRESSURE COEFFICIENTS

Pressure coefficients for the three wings tested are given in tables B-1 to B-15 for the upper and lower surfaces. The 55° sweep wing had pressure orifices on one side only. The tunnel flow angularity made it difficult to obtain data at the same angle of attack for the lower and upper surfaces. Consequently, the experimental data for the 55° sweep wing are presented as upper surface pressures through a complete positive and negative angle-of-attack range.

APPENDIX B

TABLE B-1.- PRESSURE COEFFICIENTS FOR WING WITH 76° SWEEP,

$C_{L,des} = 0.0$, $M = 2.3$

(a) $\alpha = -4.06°$

Cp at 2y/b of:																	
0.00			0.20			0.40			0.60			0.80			0.95		
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower
			.020	.1043	-.0941	.035			.056	.0768	-.1050	.130	.0690	-.1252	.200		
.032			.032	.0902	-.0523	.060	.0776	-.0887	.105	.0804	-.1050	.180	.0725	-.1252	.240	.0619	-.1552
.058			.058	.0937	-.0275	.085	.0776	-.0905	.157	.0715	-.1086	.230	.0672	-.1252	.340	.0496	-.1570
.083	.0849	.0095	.083	.0936	-.0051	.110	.0811	-.0833	.200	.0591	-.1068	.320	.0531	-.1287	.440	.0337	-.1588
.108	.0796	.0078	.108	.0811	-.0140	.160	.0811	-.0833	.250	.0574	-.1068	.420	.0513	-.1305	.640	.0072	-.1640
.157	.0778	.0042	.157	.0776	-.0105	.209	.0751	-.0270	.300	.0538	-.1050	.520	.0248	-.1340			
.207	.0761	.0024	.207	.0705	-.0158	.260	.0574	-.0341	.350	.0450	-.1033	.620	.0072	-.1411			
.250	.0690	-.0045	.250	.0634	-.0193	.300	.0485	-.0359	.400	.0361	-.1015	.710	-.0016	-.1464			
.300	.0655	-.0081	.300	.0510	-.0262	.350	.0397	-.0412	.500	.0220	-.0962	.810	-.0086	-.1499			
.350	.0637	-.0116	.350	.0421	-.0318	.400	.0343	-.0430	.600	.0195	-.0722	.910	-.0104	-.1535			
.400	.0602	-.0134	.400	.0350	-.0389	.500	.0308	-.0483	.700	.0195	-.0811						
.450			.450	.0332	-.0407	.600	.0166	-.0572	.800	-.0086	-.0864						
.500	.0372	-.0293	.500	.0297	-.0460	.700	-.0010	-.0713	.890	-.0086	-.0828						
.600			.600	.0226	-.0460	.800	-.0063	-.0731	.940	-.0086	-.0828						
.700	.0319	-.0346	.700	.0137	-.0549	.900	-.0045	-.0696									
.800	.0195	-.0435	.800	.0049	-.0620	.950	-.0027	-.0678									
.900	.0125	-.0505	.900	.0013	-.0638												
.950	.0089	-.0541	.950	-.0057	-.0691												

TABLE B-1.- Continued

(b) $\alpha = -0.06^{o}$

Cp at 2y/b of:																	
0.00			0.20			0.40			0.60			0.80			0.95		
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower
			.020	.0697	.0679	.035			.056	.0191	.0208	.130	.0096	.0107	.200		
.032			.032	.0432	.0449	.060	.0304	.0289	.105	.0244	.0279	.180	.0096	.0107	.240	-.0222	-.0193
.058			.058	.0450	.0467	.085	.0268	.0289	.157	.0155	.0190	.230	.0043	.0036	.340	-.0310	-.0281
.083	.0414	.0467	.083	.0499	.0467	.110	.0304	.0289	.200	.0049	.0066	.320	-.0098	-.0104	.440	-.0434	-.0422
.108	.0397	.0414	.108	.0339	.0324	.160	.0268	.0289	.250	.0013	.0030	.420	-.0133	-.0246	.640	-.0700	-.0652
.157	.0397	.0396	.157	.0304	.0289	.209	.0279	.0296	.300	-.0039	-.0022	.520	-.0346	-.0369			
.207	.0361	.0361	.207	.0179	.0182	.260	.0049	.0101	.350	-.0092	-.0093	.620	-.0505	-.0510			
.250	.0290	.0272	.250	.0161	.0146	.300	-.0004	.0048	.400	-.0163	-.0181	.710	-.0611	-.0599			
.300	.0220	.0219	.300	.0055	.0075	.350	-.0057	-.0040	.500	-.0287	-.0270	.810	-.0647	-.0616			
.350	.0202	.0219	.350	.0019	.0022	.400	-.0057	-.0040	.600	-.0222	-.0210	.910	-.0664	-.0634			
.400	.0149	.0184	.400	-.0069	-.0066	.500	-.0128	-.0164	.700	-.0222	-.0316						
.450			.450	-.0104	-.0102	.600	-.0252	-.0288	.800	-.0523	-.0528						
.500	.0007	.0024	.500	-.0104	-.0120	.700	-.0412	-.0412	.890	-.0523	-.0510						
.600			.600	-.0158	-.0191	.800	-.0429	-.0448	.940	-.0523	-.0510						
.700	-.0063	-.0099	.700	-.0229	-.0298	.900	-.0394	-.0412									
.800	-.0151	-.0169	.800	-.0318	-.0315	.950	-.0394	-.0394									
.900	-.0222	-.0240	.900	-.0335	-.0333												
.950	-.0257	-.0276	.950	-.0389	-.0422												

TABLE B-1.- Continued

(c) $\alpha = 4.95^{o}$

Cp at 2y/b of:																	
0.00			0.20			0.40			0.60			0.80			0.95		
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower
			.020	-.0824	.1211	.035			.056	-.1193	.0901	.130	-.1358	.0814	.200		
.032			.032	-.0895	.1087	.060	-.1029	.0891	.105	-.1193	.0954	.180	-.1358	.0814	.240	-.1641	.0708
.058			.058	-.0877	.1158	.085	-.1047	.0891	.157	-.1228	.0883	.230	-.1376	.0779	.340	-.1658	.0620
.083	-.0024	.1123	.083	-.0656	.1122	.110	-.1100	.0962	.200	-.1281	.0776	.320	-.1411	.0655	.440	-.1658	.0478
.108	-.0006	.1087	.108	-.0638	.0998	.160	-.1100	.0962	.250	-.1299	.0741	.420	-.1411	.0549	.640	-.1729	.0249
.157	-.0010	.1052	.157	-.0229	.0926	.209	-.0927	.0901	.300	-.1352	.0705	.520	-.1482	.0372			
.207	-.0046	.1017	.207	-.0212	.0784	.260	-.1157	.0741	.350	-.1370	.0634	.620	-.1552	.0196			
.250	-.0116	.0893	.250	-.0212	.0766	.300	-.0997	.0670	.400	-.1423	.0510	.710	-.1605	.0090			
.300	-.0170	.0822	.300	-.0318	.0677	.350	-.0785	.0581	.500	-.1476	.0333	.810	-.1641	.0037			
.350	-.0170	.0786	.350	-.0372	.0589	.400	-.0554	.0581	.600	-.1252	.0337	.910	-.1676	.0019			
.400	-.0187	.0751	.400	-.0443	.0517	.500	-.0430	.0457	.700	-.1252	.0072						
.450			.450	-.0460	.0482	.600	-.0572	.0297	.800	-.1411	.0037						
.500	-.0329	.0521	.500	-.0460	.0429	.700	-.0749	.0084	.890	-.1217	.0037						
.600			.600	-.0514	.0375	.800	-.0767	.0049	.940	-.1146	.0019						
.700	-.0382	.0450	.700	-.0585	.0215	.900	-.0731	.0049									
.800	-.0470	.0308	.800	-.0656	.0126	.950	-.0714	.0067									
.900	-.0541	.0220	.900	-.0674	.0126												
.950	-.0559	.0185	.950	-.0727	.0037												

TABLE B-1.- Continued

(d) $\alpha = 5.94^{o}$

Cp at 2y/b of:																	
0.00			0.20			0.40			0.60			0.80			0.95		
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower
			.020	-.0988	.1330	.035			.056	-.1320	.0989	.130	-.1467	.0916	.200	-.1802	
.032			.032	-.1059	.1207	.060	-.1175	.0993	.105	-.1338	.1060	.180	-.1467	.0916	.240	-.1732	.0810
.058			.058	-.1094	.1295	.085	-.1193	.0993	.157	-.1373	.1007	.230	-.1485	.0898	.340	-.1732	.0739
.083	-.0053	.1277	.083	-.1016	.1277	.110	-.1229	.1100	.200	-.1409	.0900	.320	-.1520	.0775	.440	-.1749	.0616
.108	-.0070	.1224	.108	-.1122	.1135	.160	-.1246	.1100	.250	-.1427	.0865	.420	-.1538	.0704	.640	-.1802	.0386
.157	-.0088	.1207	.157	-.0732	.1082	.209	-.1108	.1007	.300	-.1480	.0829	.520	-.1591	.0510			
.207	-.0106	.1171	.207	-.0218	.0940	.260	-.1462	.0865	.350	-.1550	.0758	.620	-.1661	.0334			
.250	-.0194	.1048	.250	-.0183	.0904	.300	-.1462	.0794	.400	-.1603	.0652	.710	-.1714	.0210			
.300	-.0229	.0959	.300	-.0325	.0798	.350	-.1338	.0705	.500	-.1727	.0457	.810	-.1749	.0175			
.350	-.0229	.0924	.350	-.0413	.0727	.400	-.1108	.0687	.600	-.1485	.0457	.910	-.1802	.0157			
.400	-.0247	.0888	.400	-.0502	.0638	.500	-.0613	.0581	.700	-.1503	.0192						
.450			.450	-.0520	.0602	.600	-.0560	.0404	.800	-.1820	.0157						
.500	-.0388	.0641	.500	-.0537	.0567	.700	-.0754	.0191	.890	-.1732	.0157						
.600			.600	-.0573	.0496	.800	-.0825	.0138	.940	-.1661	.0139						
.700	-.0459	.0570	.700	-.0644	.0336	.900	-.0790	.0138									
.800	-.0547	.0429	.800	-.0715	.0229	.950	-.0772	.0155									
.900	-.0600	.0340	.900	-.0732	.0229												
.950	-.0635	.0305	.950	-.0785	.0141												

TABLE B-1.- Continued

(e) $\alpha = 7.94^{o}$

Cp at 2y/b of:																	
0.00			0.20			0.40			0.60			0.80			0.95		
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower
			.020	-.1287	.1560	.035			.056	-.1549	.1250	.130	-.1678	.1131	.200		
.032			.032	-.1340	.1471	.060	-.1440	.1259	.105	-.1549	.1321	.180	-.1678	.1149	.240	-.1872	.1008
.058			.058	-.1393	.1595	.085	-.1440	.1241	.157	-.1585	.1286	.230	-.1695	.1131	.340	-.1872	.0955
.083	-.0209	.1648	.083	-.1352	.1614	.110	-.1493	.1383	.200	-.1638	.1137	.320	-.1713	.1061	.440	-.1889	.0884
.108	-.0192	.1595	.108	-.1600	.1490	.160	-.1618	.1383	.250	-.1673	.1179	.420	-.1731	.0990	.640	-.1925	.0672
.157	-.0227	.1560	.157	-.1635	.1437	.209	-.1372	.1339	.300	-.1709	.1162	.520	-.1766	.0796			
.207	-.0227	.1524	.207	-.1263	.1277	.260	-.1762	.1179	.350	-.1744	.1091	.620	-.1836	.0619			
.250	-.0298	.1383	.250	-.0518	.1224	.300	-.1815	.1109	.400	-.1779	.0949	.710	-.1889	.0495			
.300	-.0333	.1312	.300	-.0429	.1117	.350	-.1850	.1020	.500	-.1850	.0772	.810	-.1907	.0460			
.350	-.0368	.1277	.350	-.0464	.1046	.400	-.1850	.1020	.600	-.1642	.0725	.910	-.1925	.0442			
.400	-.0386	.1206	.400	-.0571	.0957	.500	-.1673	.0896	.700	-.1872	.0478						
.450			.450	-.0606	.0922	.600	-.1319	.0719	.800	-.2154	.0442						
.500	-.0510	.0941	.500	-.0642	.0868	.700	-.1107	.0488	.890	-.2189	.0425						
.600			.600	-.0677	.0780	.800	-.1018	.0453	.940	-.2189	.0407						
.700	-.0598	.0870	.700	-.0713	.0638	.900	-.0965	.0435									
.800	-.0686	.0693	.800	-.0855	.0495	.950	-.0947	.0453									
.900	-.0739	.0605	.900	-.0872	.0495												
.950	-.0775	.0570	.950	-.0908	.0389												

TABLE B-1.- Continued

(f) $\alpha = 9.94^{o}$

Cp at 2y/b of:																	
0.00			0.20			0.40			0.60			0.80			0.95		
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower
			.020	-.1482	.1841	.035			.056	-.1727	.1466	.130	-.1819	.1390	.200		
.032			.032	-.1535	.1771	.060	-.1616	.1537	.105	-.1727	.1608	.180	-.1819	.1426	.240	-.1978	.1267
.058			.058	-.1588	.1841	.085	-.1634	.1537	.157	-.1727	.1591	.230	-.1819	.1426	.340	-.1995	.1249
.083	-.0369	.2071	.083	-.1545	.1945	.110	-.1687	.1697	.200	-.1762	.1520	.320	-.1837	.1390	.440	-.1995	.1196
.108	-.0299	.2018	.108	-.1811	.1839	.160	-.1705	.1679	.250	-.1815	.1520	.420	-.1854	.1320	.640	-.2031	.1002
.157	-.0352	.1965	.157	-.1953	.1803	.209	-.1408	.1644	.300	-.1886	.1484	.520	-.1907	.1108			
.207	-.0334	.1912	.207	-.2025	.1662	.260	-.1815	.1520	.350	-.1939	.1431	.620	-.1960	.0832			
.250	-.0440	.1788	.250	-.1687	.1591	.300	-.1921	.1449	.400	-.1939	.1289	.710	-.1995	.0826			
.300	-.0475	.1718	.300	-.1225	.1466	.350	-.2028	.1360	.500	-.1939	.1094	.810	-.2048	.0808			
.350	-.0493	.1647	.350	-.0887	.1413	.400	-.2045	.1360	.600	-.1678	.1055	.910	-.2083	.0791			
.400	-.0511	.1594	.400	-.0816	.1307	.500	-.2151	.1236	.700	-.1890	.0808						
.450			.450	-.0816	.1271	.600	-.1957	.1059	.800	-.2066	.0773						
.500	-.0634	.1276	.500	-.0851	.1218	.700	-.1886	.0793	.890	-.2119	.0756						
.600			.600	-.0905	.1112	.800	-.1621	.0757	.940	-.2154	.0738						
.700	-.0758	.1240	.700	-.0976	.0952	.900	-.1461	.0739									
.800	-.0811	.1028	.800	-.1029	.0810	.950	-.1408	.0739									
.900	-.0881	.0922	.900	-.1047	.0810												
.950	-.0934	.0887	.950	-.1136	.0686												

TABLE B-1.- Concluded

(g) $\alpha = 19.94^{o}$

Cp at 2y/b of:																	
0.00			0.20			0.40			0.60			0.80			0.95		
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower
			.020	-.2117	.3642	.035			.056	-.2222	.3107	.130	-.2259	.2993	.200		
.032			.032	-.2134	.3731	.060	-.2132	.3440	.105	-.2204	.3444	.180	-.2259	.3099	.240	-.2312	.2694
.058			.058	-.2205	.4190	.085	-.2150	.3475	.157	-.2204	.3585	.230	-.2259	.3152	.340	-.2312	.2835
.083	-.1109	.4632	.083	-.2043	.4238	.110	-.2167	.3795	.200	-.2222	.3585	.320	-.2259	.3223	.440	-.2330	.2941
.108	-.1250	.4596	.108	-.2274	.4203	.160	-.2185	.3777	.250	-.2257	.3674	.420	-.2277	.3223	.640	-.2347	.2923
.157	-.1127	.4614	.157	-.2292	.4256	.209	-.1920	.3780	.300	-.2310	.3674	.520	-.2312	.3134			
.207	-.0968	.4579	.207	-.2327	.4096	.260	-.2310	.3798	.350	-.2346	.3603	.620	-.2365	.3134			
.250	-.1091	.4402	.250	-.2363	.4061	.300	-.2346	.3780	.400	-.2328	.3497	.710	-.2400	.2958			
.300	-.1215	.4296	.300	-.2380	.3866	.350	-.2310	.3656	.500	-.2346	.3302	.810	-.2418	.2923			
.350	-.1250	.4190	.350	-.2327	.3777	.400	-.2346	.3674	.600	-.2012	.3134	.910	-.2347	.2888			
.400	-.1268	.4119	.400	-.2274	.3635	.500	-.2399	.3568	.700	-.2153	.2923						
.450			.450	-.2221	.3635	.600	-.2381	.3355	.800	-.2365	.2923						
.500	-.1356	.3589	.500	-.2150	.3528	.700	-.2434	.2966	.890	-.2400	.2888						
.600			.600	-.2061	.3440	.800	-.2417	.2859	.940	-.2312	.2852						
.700	-.1516	.3554	.700	-.1990	.3227	.900	-.2381	.2824									
.800	-.1498	.3218	.800	-.2007	.2925	.950	-.2346	.2806									
.900	-.1516	.3077	.900	-.1954	.2978												
.950	-.1551	.3041	.950	-.1848	.2765												

TABLE B-2.- PRESSURE COEFFICIENTS FOR WING WITH 76° SWEEP,

$C_{L,des}$ = 0.0, M = 3.0

(a) α = -4.10°

Cp at 2y/b of:																	
0.00			0.20			0.40			0.60			0.80			0.95		
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower
			.020	.0946	-.0383	.035			.056	.0824	-.0782	.130	.0790	-.1016	.200		
.032			.032	.0840	-.0404	.060	.0809	-.0611	.105	.0824	-.0782	.180	.0769	-.0995	.240	.0685	-.1228
.058			.058	.0861	-.0341	.085	.0766	-.0611	.157	.0740	-.0638	.230	.0727	-.0932	.340	.0538	-.1228
.083	.0735	.0039	.083	.0957	.0110	.110	.0830	-.0547	.200	.0634	-.0655	.320	.0601	-.0890	.440	.0432	-.1228
.108	.0713	.0018	.108	.0745	-.0080	.160	.0787	-.0568	.250	.0592	-.0634	.420	.0474	-.0911	.640	.0201	-.1270
.157	.0692	.0018	.157	.0724	-.0080	.209	.0930	.0063	.300	.0549	-.0613	.520	.0306	-.0911			
.207	.0671	-.0003	.207	.0639	-.0144	.260	.0592	-.0274	.350	.0486	-.0613	.620	.0180	-.0911			
.250	.0629	-.0066	.250	.0597	-.0165	.300	.0507	-.0317	.400	.0422	-.0613	.710	.0075	-.0953			
.300	.0587	-.0087	.300	.0512	-.0208	.350	.0422	-.0359	.500	.0274	-.0634	.810	.0032	-.0953			
.350	.0587	-.0108	.350	.0448	-.0271	.400	.0401	-.0359	.600	.0453	-.0341	.910	-.0009	-.0953			
.400	.0566	-.0129	.400	.0384	-.0314	.500	.0295	-.0422	.700	.0432	-.0362						
.450			.450	.0342	-.0314	.600	.0190	-.0486	.800	-.0009	-.0763						
.500	.0439	-.0150	.500	.0300	-.0335	.700	.0020	-.0571	.890	-.0051	-.0784						
.600			.600	.0236	-.0377	.800	-.0000	-.0571	.940	-.0051	-.0784						
.700	.0291	-.0298	.700	.0130	-.0441	.900	-.0000	-.0571									
.800	.0228	-.0319	.800	.0088	-.0462	.950	-.0000	-.0549									
.900	.0143	-.0383	.900	.0045	-.0505												
.950	.0122	-.0383	.950	.0003	-.0526												

TABLE B-2.- Continued

(b) $\alpha = -0.11^{o}$

Cp at 2y/b of:																	
0.00			0.20			0.40			0.60			0.80			0.95		
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower
			.020	.0608	.0567	.035			.056	.0295	.0275	.130	.0224	.0183	.200		
.032			.032	.0460	.0440	.060	.0363	.0322	.105	.0317	.0296	.180	.0203	.0183	.240	.0013	-.0006
.058			.058	.0460	.0440	.085	.0321	.0301	.157	.0232	.0212	.230	.0161	.0141	.340	-.0091	-.0006
.083	.0355	.0335	.083	.0554	.0555	.110	.0321	.0301	.200	.0147	.0127	.320	.0034	.0014	.440	-.0196	-.0196
.108	.0333	.0335	.108	.0321	.0301	.160	.0300	.0279	.250	.0105	.0106	.420	-.0070	-.0027	.640	-.0386	-.0406
.157	.0333	.0313	.157	.0300	.0258	.209	.0486	.0487	.300	.0063	.0042	.520	-.0218	-.0238			
.207	.0333	.0313	.207	.0215	.0173	.260	.0126	.0106	.350	.0020	.0000	.620	-.0323	-.0343			
.250	.0249	.0229	.250	.0172	.0152	.300	.0063	.0064	.400	-.0042	-.0062	.710	-.0407	-.0406			
.300	.0207	.0187	.300	.0088	.0067	.350	-.0000	.0000	.500	-.0148	-.0168	.810	-.0428	-.0428			
.350	.0186	.0166	.350	.0024	.0025	.400	-.0021	-.0041	.600	.0055	.0035	.910	-.0449	-.0449			
.400	.0165	.0144	.400	-.0017	-.0017	.500	-.0084	-.0105	.700	.0034	-.0027						
.450			.450	-.0039	-.0038	.600	-.0190	-.0189	.800	-.0407	-.0406						
.500	.0101	.0102	.500	-.0081	-.0080	.700	-.0317	-.0317	.890	-.0428	-.0428						
.600			.600	-.0102	-.0123	.800	-.0317	-.0338	.940	-.0428	-.0428						
.700	-.0024	-.0045	.700	-.0187	-.0186	.900	-.0317	-.0317									
.800	-.0088	-.0108	.800	-.0230	-.0250	.950	-.0317	-.0317									
.900	-.0151	-.0150	.900	-.0251	-.0271												
.950	-.0151	-.0171	.950	-.0293	-.0292												

TABLE B-2.- Continued

(c) $\alpha = 4.90^{o}$

Cp at 2y/b of:																	
0.00			0.20			0.40			0.60			0.80			0.95		
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower
			.020	-.0510	.1072	.035			.056	-.0889	.0909	.130	-.1060	.0877	.200		
.032			.032	-.0531	.0967	.060	-.0761	.0872	.105	-.0910	.0930	.180	-.1060	.0856	.240	-.1187	.0793
.058			.058	-.0552	.1009	.085	-.0782	.0851	.157	-.0889	.0846	.230	-.1060	.0814	.340	-.1187	.0666
.083	.0016	.0925	.083	-.0316	.1084	.110	-.0740	.0893	.200	-.0846	.0761	.320	-.1060	.0687	.440	-.1208	.0540
.108	-.0004	.0904	.108	-.0358	.0872	.160	-.0761	.0872	.250	-.0825	.0719	.420	-.1081	.0582	.640	-.1229	.0308
.157	-.0025	.0882	.157	-.0189	.0830	.209	-.0191	.0994	.300	-.0825	.0676	.520	-.1081	.0413			
.207	-.0046	.0840	.207	-.0210	.0745	.260	-.0529	.0697	.350	-.0825	.0613	.620	-.1081	.0266			
.250	-.0109	.0756	.250	-.0210	.0703	.300	-.0508	.0613	.400	-.0783	.0528	.710	-.1081	.0161			
.300	-.0151	.0692	.300	-.0274	.0597	.350	-.0487	.0528	.500	-.0825	.0401	.810	-.1081	.0119			
.350	-.0151	.0671	.350	-.0316	.0533	.400	-.0466	.0528	.600	-.0471	.0519	.910	-.1081	.0076			
.400	-.0172	.0650	.400	-.0358	.0448	.500	-.0487	.0422	.700	-.0660	.0519						
.450			.450	-.0380	.0427	.600	-.0529	.0295	.800	-.0892	.0076						
.500	-.0194	.0523	.500	-.0401	.0384	.700	-.0614	.0126	.890	-.0892	.0034						
.600			.600	-.0422	.0342	.800	-.0635	.0084	.940	-.0892	.0034						
.700	-.0320	.0418	.700	-.0485	.0236	.900	-.0614	.0084									
.800	-.0384	.0312	.800	-.0528	.0151	.950	-.0592	.0084									
.900	-.0405	.0249	.900	-.0528	.0130												
.950	-.0405	.0228	.950	-.0570	.0088												

TABLE B-2.- Continued

(d) $\alpha = 5.90^{o}$

Cp at 2y/b of:																		
0.00			0.20			0.40			0.60			0.80			0.95		
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower
			.020	-.0658	.1142	.035			.056	-.0952	.1036	.130	-.1123	.0982	.200		
.032			.032	-.0679	.1036	.060	-.0866	.0978	.105	-.0994	.1057	.180	-.1123	.0961	.240	-.1208	.0877
.058			.058	-.0700	.1099	.085	-.0866	.0978	.157	-.0994	.0973	.230	-.1123	.0940	.340	-.1229	.0772
.083	-.0067	.1036	.083	-.0505	.1190	.110	-.0866	.1021	.200	-.0994	.0888	.320	-.1123	.0814	.440	-.1229	.0666
.108	-.0088	.0994	.108	-.0696	.0999	.160	-.0866	.0999	.250	-.0973	.0846	.420	-.1166	.0687	.640	-.1250	.0456
.157	-.0088	.0994	.157	-.0442	.0978	.209	-.0360	.1121	.300	-.0973	.0803	.520	-.1145	.0540			
.207	-.0088	.0930	.207	-.0336	.0872	.260	-.0783	.0824	.350	-.0973	.0740	.620	-.1166	.0392			
.250	-.0151	.0846	.250	-.0293	.0830	.300	-.0783	.0740	.400	-.0952	.0655	.710	-.1187	.0287			
.300	-.0194	.0782	.300	-.0315	.0724	.350	-.0762	.0655	.500	-.0994	.0528	.810	-.1187	.0224			
.350	-.0215	.0761	.350	-.0336	.0660	.400	-.0719	.0634	.600	-.0639	.0645	.910	-.1187	.0182			
.400	-.0215	.0761	.400	-.0399	.0575	.500	-.0677	.0528	.700	-.0913	.0624						
.450			.450	-.0421	.0554	.600	-.0635	.0422	.800	-.1102	.0182						
.500	-.0236	.0592	.500	-.0442	.0512	.700	-.0656	.0253	.890	-.1123	.0140						
.600			.600	-.0484	.0448	.800	-.0656	.0190	.940	-.1123	.0140						
.700	-.0384	.0486	.700	-.0527	.0342	.900	-.0635	.0190									
.800	-.0405	.0401	.800	-.0569	.0257	.950	-.0593	.0190									
.900	-.0447	.0295	.900	-.0569	.0236												
.950	-.0447	.0295	.950	-.0611	.0172												

TABLE B-2.- Continued

(e) $\alpha = 7.90^{o}$

Cp at 2y/b of:																	
0.00			0.20			0.40			0.60			0.80			0.95		
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower
			.020	-.0869	.1410	.035			.056	-.1079	.1269	.130	-.1187	.1232	.200		
.032			.032	-.0911	.1347	.060	-.1015	.1232	.105	-.1100	.1311	.180	-.1187	.1232	.240	-.1271	.1126
.058			.058	-.0911	.1431	.085	-.1036	.1211	.157	-.1121	.1247	.230	-.1187	.1211	.340	-.1271	.1042
.083	-.0173	.1389	.083	-.0634	.1508	.110	-.1036	.1296	.200	-.1121	.1163	.320	-.1208	.1105	.440	-.1271	.0937
.108	-.0194	.1368	.108	-.0909	.1296	.160	-.1057	.1275	.250	-.1121	.1120	.420	-.1250	.0958	.640	-.1292	.0748
.157	-.0194	.1326	.157	-.0888	.1254	.209	-.0550	.1374	.300	-.1121	.1078	.520	-.1229	.0832			
.207	-.0194	.1304	.207	-.0867	.1148	.260	-.1037	.1099	.350	-.1121	.1015	.620	-.1250	.0685			
.250	-.0257	.1178	.250	-.0824	.1105	.300	-.1058	.1036	.400	-.1100	.0951	.710	-.1271	.0558			
.300	-.0299	.1114	.300	-.0697	.0999	.350	-.1079	.0930	.500	-.1164	.0782	.810	-.1271	.0516			
.350	-.0299	.1093	.350	-.0464	.0936	.400	-.1100	.0909	.600	-.0786	.0895	.910	-.1292	.0474			
.400	-.0320	.1072	.400	-.0443	.0851	.500	-.1143	.0824	.700	-.0976	.0895						
.450			.450	-.0443	.0830	.600	-.1100	.0676	.800	-.1250	.0453						
.500	-.0320	.0882	.500	-.0507	.0787	.700	-.1143	.0486	.890	-.1292	.0411						
.600			.600	-.0528	.0724	.800	-.1037	.0422	.940	-.1313	.0390						
.700	-.0468	.0777	.700	-.0613	.0596	.900	-.0846	.0422									
.800	-.0489	.0671	.800	-.0634	.0512	.950	-.0783	.0422									
.900	-.0531	.0587	.900	-.0634	.0469												
.950	-.0552	.0566	.950	-.0676	.0405												

TABLE B-2.- Continued

(f) $\alpha = 9.90^{o}$

Cp at 2y/b of:																	
0.00			0.20			0.40			0.60			0.80			0.95		
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower
			.020	-.1017	.1662	.035			.056	-.1185	.1500	.130	-.1271	.1486	.200		
.032			.032	-.1038	.1620	.060	-.1120	.1503	.105	-.1185	.1585	.180	-.1250	.1486	.240	-.1292	.1339
.058			.058	-.1059	.1746	.085	-.1142	.1482	.157	-.1185	.1542	.230	-.1250	.1465	.340	-.1292	.1255
.083	-.0257	.1746	.083	-.0781	.1821	.110	-.1142	.1609	.200	-.1206	.1458	.320	-.1250	.1381	.440	-.1313	.1192
.108	-.0299	.1704	.108	-.1057	.1652	.160	-.1163	.1588	.250	-.1206	.1437	.420	-.1292	.1234	.640	-.1313	.1002
.157	-.0299	.1683	.157	-.1099	.1609	.209	-.0656	.1669	.300	-.1206	.1394	.520	-.1292	.1128			
.207	-.0299	.1641	.207	-.1142	.1461	.260	-.1164	.1437	.350	-.1206	.1331	.620	-.1292	.0939			
.250	-.0342	.1535	.250	-.1142	.1419	.300	-.1185	.1352	.400	-.1206	.1246	.710	-.1313	.0834			
.300	-.0384	.1451	.300	-.1142	.1313	.350	-.1206	.1246	.500	-.1248	.1098	.810	-.1313	.0770			
.350	-.0384	.1430	.350	-.0972	.1249	.400	-.1248	.1246	.600	-.0871	.1149	.910	-.1313	.0728			
.400	-.0405	.1409	.400	-.0845	.1165	.500	-.1291	.1119	.700	-.0871	.1149						
.450			.450	-.0718	.1122	.600	-.1291	.0971	.800	-.1313	.0707						
.500	-.0405	.1177	.500	-.0612	.1080	.700	-.1333	.0760	.890	-.1355	.0665						
.600			.600	-.0633	.1016	.800	-.1291	.0696	.940	-.1355	.0644						
.700	-.0553	.1071	.700	-.0718	.0868	.900	-.1206	.0675									
.800	-.0595	.0966	.800	-.0739	.0762	.950	-.1164	.0696									
.900	-.0637	.0860	.900	-.0760	.0741												
.950	-.0637	.0839	.950	-.0802	.0657												

TABLE B-2.- Concluded

(g) $\alpha = 19.90^{o}$

Cp at 2y/b of:																	
0.00			0.20			0.40			0.60			0.80			0.95		
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower
			.020	-.1354	.3395	.035			.056	-.1375	.3131	.130	-.1397	.3110	.200		
.032			.032	-.1396	.3480	.060	-.1354	.3311	.105	-.1375	.3364	.180	-.1397	.3194	.240	-.1418	.2836
.058			.058	-.1396	.3775	.085	-.1354	.3311	.157	-.1375	.3448	.230	-.1397	.3237	.340	-.1418	.2878
.083	-.0867	.4240	.083	-.1014	.3905	.110	-.1354	.3587	.200	-.1375	.3427	.320	-.1397	.2984	.440	-.1418	.2921
.108	-.0931	.4134	.108	-.1332	.3841	.160	-.1375	.3587	.250	-.1396	.3470	.420	-.1439	.3215	.640	-.1397	.2815
.157	-.0825	.4092	.157	-.1354	.3863	.209	-.0846	.3639	.300	-.1375	.3470	.520	-.1418	.3068			
.207	-.0761	.4050	.207	-.1354	.3714	.260	-.1312	.3575	.350	-.1375	.3427	.620	-.1418	.2878			
.250	-.0846	.3902	.250	-.1375	.3672	.300	-.1375	.3491	.400	-.1354	.3322	.710	-.1439	.2773			
.300	-.0910	.3796	.300	-.1375	.3502	.350	-.1354	.3385	.500	-.1418	.3152	.810	-.1397	.2710			
.350	-.0952	.3754	.350	-.1375	.3439	.400	-.1375	.3385	.600	-.0976	.3089	.910	-.1397	.2668			
.400	-.0952	.3733	.400	-.1375	.3332	.500	-.1418	.3258	.700	-.1060	.2773						
.450			.450	-.1375	.3311	.600	-.1396	.3046	.800	-.1418	.2689						
.500	-.0888	.3289	.500	-.1375	.3226	.700	-.1439	.2750	.890	-.1439	.2689						
.600			.600	-.1354	.3120	.800	-.1460	.2644	.940	-.1418	.2605						
.700	-.1121	.3226	.700	-.1332	.2908	.900	-.1439	.2602									
.800	-.1142	.3036	.800	-.1311	.2739	.950	-.1418	.2602									
.900	-.1142	.2888	.900	-.1247	.2717												
.950	-.1142	.2825	.950	-.1120	.2569												

TABLE B-3.- PRESSURE COEFFICIENTS FOR WING WITH 76° SWEEP,

$C_{L,des}$ = 0.0, M = 3.5

(a) α = -1.28°

Cp at 2y/b of:																	
0.00			0.20			0.40			0.60			0.80			0.95		
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower
			.020	.0935	-.0271	.035			.056	.0790	-.0617	.130	.0735	.0797	.200		
.032			.032	.0845	-.0271	.060	.0770	0470	.105	.0790	-.0631	.180	.0690	-.0797	.240	.0646	-.0900
.058			.058	.0845	-.0286	.085	.0726	-.0515	.157	.0715	-.0631	.230	.0661	-.0797	.340	.0528	-.0900
.083	.0696	.0011	.083	.0918	-.0086	.110	.0756	-.0411	.200	.0627	-.0631	.320	.0528	-.0797	.440	.0410	-.0915
.108	.0681	-.0033	.108	.0711	-.0189	.160	.0741	-.0441	.250	.0567	-.0602	.420	.0469	-.0812	.640	.0204	-.0915
.157	.0666	-.0018	.157	.0667	-.0086	.209	.0834	.0095	.300	.0523	-.0572	.520	.0278	-.0797			
.207	.0637	-.0033	.207	.0578	-.0145	.260	.0552	.0246	.350	.0478	-.0557	.620	.0160	-.0797			
.250	.0562	-.0077	.250	.0549	-.0160	.300	.0493	-.0290	.400	.0404	-.0513	.710	.0071	-.0782			
.300	.0517	-.0107	.300	.0460	-.0219	.350	.0404	-.0335	.500	.0271	-.0557	.810	.0027	-.0768			
.350	.0517	-.0122	.350	.0416	-.0249	.400	.0375	-.0349	.600	.0366	-.0296	.910	-.0016	-.0753			
.400	.0488	-.0137	.400	.0342	-.0293	.500	.0286	-.0394	.700	.0160	-.0311						
.450			.450	.0327	-.0293	.600	.0182	-.0409	.800	-.0031	-.0635						
.500	.0443	-.0092	.500	.0282	-.0323	.700	.0049	-.0513	.890	-.0075	-.0664						
.600			.600	.0223	-.0352	.800	-.0010	-.0557	.940	-.0075	-.0664						
.700	.0264	-.0286	.700	.0135	-.0397	.900	-.0010	-.0528									
.800	.0204	-.0316	.800	.0075	-.0441	.950	.0004	-.0528									
.900	.0145	-.0346	.900	.0061	.0456												
.950	.0145	-.0361	.950	.0031	-.0470												

TABLE B-3.- Continued

(b) $\alpha = -0.27^{O}$

Cp at 2y/b of:																	
0.00			0.20			0.40			0.60			0.80			0.95		
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower
			.020	.0490	.0445	.035			.056	.0316	.0258	.130	.0249	.0145	.200		
.032			.032	.0416	.0370	.060	.0357	.0216	.105	.0316	.0243	.180	.0205	.0130	.240	.0102	-.0016
.058			.058	.0386	.0325	.085	.0313	.0186	.157	.0242	.0183	.230	.0175	.0086	.340	.0013	-.0105
.083	.0267	.0266	.083	.0520	.0395	.110	.0328	.0216	.200	.0168	.0109	.320	.0072	-.0001	.440	-.0060	-.0164
.108	.0267	.0251	.108	.0313	.0201	.160	.0298	.0186	.250	.0124	.0050	.420	-.0001	-.0119	.640	-.0251	-.0340
.157	.0281	.0251	.157	.0283	.0157	.209	.0435	.0391	.300	.0079	.0020	.520	-.0148	-.0208			
.207	.0267	.0221	.207	.0195	.0082	.260	.0124	.0080	.350	.0049	-.0023	.620	-.0251	-.0311			
.250	.0207	.0161	.250	.0165	.0053	.300	.0064	.0020	.400	-.0009	-.0068	.710	-.0325	-.0385			
.300	.0162	.0116	.300	.0076	-.0006	.350	.0005	-.0038	.500	-.0128	-.0172	.810	-.0355	-.0414			
.350	.0147	.0101	.350	.0047	-.0065	.400	-.0024	-.0068	.600	.0028	-.0016	.910	-.0369	-.0444			
.400	.0117	.0087	.400	-.0012	-.0110	.500	-.0083	-.0112	.700	-.0104	-.0031						
.450			.450	-.0026	-.0140	.600	-.0128	-.0201	.800	-.0340	-.0399						
.500	.0132	.0101	.500	-.0071	-.0155	.700	-.0246	-.0305	.890	-.0369	-.0429						
.600			.600	-.0086	-.0199	.800	-.0306	-.0335	.940	-.0384	-.0444						
.700	-.0046	-.0092	.700	-.0145	-.0259	.900	-.0291	-.0335									
.800	-.0091	-.0136	.800	-.0189	-.0303	.950	-.0276	-.0335									
.900	-.0136	-.0181	.900	-.0219	-.0318												
.950	-.0150	-.0196	.950	-.0233	-.0348												

TABLE B-3.- Continued

(c) $\alpha = 4.74^{o}$

Cp at 2y/b of:																	
0.00			0.20			0.40			0.60			0.80			0.95		
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower
			.020	-.0375	.0997	.035			.056	-.0691	.0852	.130	-.0827	.0764	.200		
.032			.032	-.0390	.0922	.060	-.0574	.0817	.105	-.0691	.0852	.180	-.0827	.0735	.240	-.0915	.0691
.058			.058	-.0405	.0937	.085	-.0589	.0788	.157	-.0706	.0762	.230	-.0827	.0705	.340	-.0900	.0573
.083	-.0002	.0848	.083	-.0130	.0995	.110	-.0515	.0803	.200	-.0721	.0673	.320	-.0827	.0588	.440	-.0930	.0470
.108	-.0032	.0818	.108	-.0337	.0788	.160	-.0559	.0803	.250	-.0706	.0629	.420	-.0856	.0440	.640	-.0915	.0263
.157	-.0032	.0803	.157	-.0130	.0743	.209	-.0038	.0866	.300	-.0691	.0584	.520	-.0827	.0337			
.207	-.0047	.0758	.207	-.0160	.0640	.260	-.0335	.0599	.350	-.0676	.0510	.620	-.0827	.0204			
.250	-.0106	.0654	.250	-.0175	.0595	.300	-.0335	.0525	.400	-.0617	.0451	.710	-.0827	.0116			
.300	-.0136	.0594	.300	-.0234	.0506	.350	-.0364	.0466	.500	-.0631	.0317	.810	-.0812	.0072			
.350	-.0151	.0549	.350	-.0264	.0447	.400	-.0364	.0421	.600	-.0325	.0411	.910	-.0797	.0042			
.400	-.0166	.0549	.400	-.0308	.0388	.500	-.0409	.0347	.700	-.0399	.0352						
.450			.450	-.0323	.0358	.600	-.0424	.0199	.800	-.0679	.0013						
.500	-.0106	.0490	.500	-.0337	.0329	.700	-.0528	.0080	.890	-.0709	-.0031						
.600			.600	-.0367	.0255	.800	-.0557	.0020	.940	-.0709	-.0045						
.700	-.0300	.0311	.700	-.0411	.0166	.900	-.0542	.0020									
.800	-.0345	.0236	.800	-.0441	.0107	.950	-.0542	.0020									
.900	-.0360	.0176	.900	-.0456	.0062												
.950	-.0375	.0161	.950	-.0485	.0033												

TABLE B-3.- Continued

(d) $\alpha = 5.73^{o}$

Cp at 2y/b of:																	
0.00			0.20			0.40			0.60			0.80			0.95		
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower
			.020	-.0509	.1130	.035			.056	-.0780	.0940	.130	-.0915	.0869	.200		
.032			.032	-.0509	.1041	.060	-.0707	.0935	.105	-.0780	.0955	.180	-.0915	.0854	.240	-.0989	.0795
.058			.058	-.0524	.1056	.085	-.0736	.0920	.157	-.0809	.0880	.230	-.0930	.0810	.340	-.0974	.0677
.083	-.0046	.0981	.083	-.0322	.1127	.110	-.0707	.0950	.200	-.0809	.0791	.320	-.0915	.0707	.440	-.0989	.0574
.108	-.0061	.0951	.108	-.0529	.0920	.160	-.0751	.0920	.250	-.0795	.0747	.420	-.0959	.0559	.640	-.0974	.0382
.157	-.0091	.0937	.157	-.0455	.0876	.209	-.0260	.0999	.300	-.0780	.0702	.520	-.0915	.0441			
.207	-.0106	.0892	.207	-.0322	.0772	.260	-.0557	.0717	.350	-.0780	.0643	.620	-.0915	.0308			
.250	-.0151	.0787	.250	-.0248	.0728	.300	-.0542	.0643	.400	-.0735	.0554	.710	-.0915	.0220			
.300	-.0196	.0698	.300	-.0292	.0624	.350	-.0542	.0584	.500	-.0765	.0435	.810	-.0900	.0161			
.350	-.0196	.0683	.350	-.0322	.0565	.400	-.0527	.0554	.600	-.0443	.0500	.910	-.0886	.0131			
.400	-.0196	.0653	.400	-.0366	.0506	.500	-.0513	.0450	.700	-.0458	.0500						
.450			.450	-.0381	.0476	.600	-.0527	.0317	.800	-.0812	.0102						
.500	-.0151	.0593	.500	-.0396	.0432	.700	-.0602	.0183	.890	-.0841	.0058						
.600			.600	-.0425	.0358	.800	-.0617	.0109	.940	-.0841	.0043						
.700	-.0345	.0400	.700	-.0470	.0269	.900	-.0602	.0094									
.800	-.0375	.0325	.800	-.0439	.0195	.950	-.0602	.0109									
.900	-.0405	.0265	.900	-.0529	.0151												
.950	-.0419	.0250	.950	-.0544	.0121												

TABLE B-3.- Continued

(e) $\alpha = 7.73^{o}$

Cp at 2y/b of:																	
0.00			0.20			0.40			0.60			0.80			0.95		
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower
			.020	-.0673	.1369	.035			.056	-.0869	.1177	.130	-.0944	.1088	.200		
.032			.032	-.0703	.1309	.060	-.0810	.1187	.105	-.0869	.1207	.180	-.0944	.1073	.240	-.0974	.0999
.058			.058	-.0703	.1369	.085	-.0825	.1157	.157	-.0869	.1133	.230	-.0944	.1044	.340	-.0974	.0911
.083	-.0136	.1324	.083	-.0455	.1394	.110	-.0825	.1201	.200	-.0869	.1058	.320	-.0944	.0940	.440	-.0989	.0823
.108	-.0151	.1309	.108	-.0677	.1216	.160	-.0855	.1187	.250	-.0884	.0999	.420	-.0974	.0852	.640	-.0974	.0616
.157	-.0196	.1309	.157	-.0648	.1172	.209	-.0394	.1236	.300	-.0884	.0969	.520	-.0959	.0690			
.207	-.0196	.1280	.207	-.0618	.1039	.260	-.0735	.0984	.350	-.0869	.0895	.620	-.0959	.0543			
.250	-.0226	.1086	.250	-.0588	.0994	.300	-.0750	.0895	.400	-.0839	.0821	.710	-.0959	.0439			
.300	-.0270	.1071	.300	-.0588	.0891	.350	-.0765	.0821	.500	-.0869	.0673	.810	-.0959	.0395			
.350	-.0270	.0966	.350	-.0544	.0817	.400	-.0765	.0821	.600	-.0546	.0719	.910	-.0959	.0351			
.400	-.0285	.0937	.400	-.0544	.0757	.500	-.0780	.0702	.700	-.0590	.0381						
.450			.450	-.0529	.0728	.600	-.0750	.0554	.800	-.0900	.0322						
.500	-.0226	.0817	.500	-.0499	.0683	.700	-.0839	.0391	.890	-.0944	.0277						
.600			.600	-.0499	.0595	.800	-.0854	.0332	.940	-.0944	.0248						
.700	-.0420	.0638	.700	-.0529	.0491	.900	-.0869	.0302									
.800	-.0450	.0549	.800	-.0559	.0417	.950	-.0854	.0317									
.900	-.0479	.0474	.900	-.0574	.0358												
.950	-.0494	.0459	.950	-.0588	.0313												

TABLE B-3.- Continued

(f) $\alpha = 9.74^{o}$

Cp at 2y/b of:																	
0.00			0.20			0.40			0.60			0.80			0.95		
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower
			.020	-.0793	.1639	.035			.056	-.0928	.1416	.130	-.0974	.1340	.200		
.032			.032	-.0807	.1594	.060	-.0869	.1466	.105	-.0928	.1475	.180	-.0974	.1325	.240	-.0989	.1222
.058			.058	-.0807	.1684	.085	-.0869	.1451	.157	-.0928	.1416	.230	-.0959	.1310	.340	-.0989	.1148
.083	-.0196	.1684	.083	-.0558	.1747	.110	-.0884	.1511	.200	-.0928	.1341	.320	-.0959	.1222	.440	-.0989	.1074
.108	-.0240	.1639	.108	-.0781	.1555	.160	-.0899	.1496	.250	-.0943	.1297	.420	-.0989	.1074	.640	-.0989	.0868
.157	-.0270	.1594	.157	-.0766	.1525	.209	-.0483	.1505	.300	-.0943	.1267	.520	-.0989	.0956			
.207	-.0255	.1564	.207	-.0766	.1392	.260	-.0854	.1297	.350	-.0928	.1208	.620	-.0989	.0809			
.250	-.0300	.1430	.250	-.0781	.1333	.300	-.0854	.1208	.400	-.0884	.1119	.710	-.0989	.0706			
.300	-.0360	.1326	.300	-.0810	.1200	.350	-.0884	.1119	.500	-.0943	.0941	.810	-.0989	.0632			
.350	-.0375	.1261	.350	-.0825	.1126	.400	-.0884	.1104	.600	-.0605	.0971	.910	-.0989	.0602			
.400	-.0375	.1251	.400	-.0825	.1037	.500	-.0913	.0985	.700	-.0620	.0809						
.450			.450	-.0781	.1022	.600	-.0839	.0822	.800	-.0959	.0558						
.500	-.0285	.1087	.500	-.0736	.0963	.700	-.0958	.0629	.890	-.0989	.0514						
.600			.600	-.0633	.0875	.800	-.0988	.0555	.940	-.0989	.0499						
.700	-.0494	.0923	.700	-.0633	.0756	.900	-.1002	.0555									
.800	-.0524	.0818	.800	-.0662	.0667	.950	-.0973	.0555									
.900	-.0554	.0729	.900	-.0677	.0623												
.950	-.0569	.0714	.950	-.0692	.0549												

TABLE B-3.- Concluded

(g) $\alpha = 19.74^{o}$

Cp at 2y/b of:																	
0.00			0.20			0.40			0.60			0.80			0.95		
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower
			.020	-.0972	.3399	.035			.056	-.0988	.2993	.130	-.1018	.2916	.200		
.032			.032	-.0987	.3459	.060	-.0973	.3300	.105	-.1017	.3201	.180	-.1033	.2975	.240	-.1033	.2651
.058			.058	-.0987	.3772	.085	-.0973	.3314	.157	-.1002	.3260	.230	-.1018	.3005	.340	-.1018	.2680
.083	-.0643	.4205	.083	-.0677	.3847	.110	-.0973	.3536	.200	-.1002	.3215	.320	-.1033	.2975	.440	-.1033	.2695
.108	-.0733	.4100	.108	-.0929	.3773	.160	-.0973	.3521	.250	-.1017	.3230	.420	-.1048	.2857	.640	-.1018	.2577
.157	-.0629	.4056	.157	-.0929	.3788	.209	-.0572	.3453	.300	-.1002	.3215	.520	-.1048	.2739			
.207	-.0584	.3966	.207	-.0944	.3625	.260	-.0928	.3349	.350	-.1017	.3156	.620	-.1048	.2577			
.250	-.0629	.3787	.250	-.0958	.3566	.300	-.0988	.3260	.400	-.0958	.3037	.710	-.1048	.2459			
.300	-.0688	.3623	.300	-.0973	.3373	.350	-.1002	.3141	.500	-.1017	.2889	.810	-.1018	.2386			
.350	-.0718	.3563	.350	-.0988	.3300	.400	-.1002	.3141	.600	-.0649	.2739	.910	-.1018	.2356			
.400	-.0733	.3519	.400	-.0973	.3152	.500	-.1002	.2978	.700	-.0664	.2739						
.450			.450	-.0988	.3078	.600	-.1002	.2755	.800	-.1003	.2327						
.500	-.0569	.3101	.500	-.0973	.2989	.700	-.1032	.2458	.890	-.1033	.2297						
.600			.600	-.0944	.2871	.800	-.1062	.2309	.940	-.1033	.2253						
.700	-.0852	.2937	.700	-.0973	.2649	.900	-.1047	.2294									
.800	-.0852	.2758	.800	-.0973	.2471	.950	-.1032	.2294									
.900	-.0852	.2579	.900	-.0929	.2397												
.950	-.0867	.2519	.950	-.0855	.2264												

TABLE B-4.- PRESSURE COEFFICIENTS FOR WING WITH 76° SWEEP,

$C_{L,des} = 0.0$, $M = 4.0$

(a) $\alpha = -3.90°$

Cp at 2y/b of:																	
0.00			0.20			0.40			0.60			0.80			0.95		
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower
			.020	.0825	-.0142	.035			.056	.0733	-.0411	.130	.0705	-.0546	.200		
.032			.032	.0742	-.0125	.060	.0678	-.0247	.105	.0716	-.0394	.180	.0656	-.0529	.240	.0640	-.0645
.058			.058	.0725	-.0108	.085	.0645	-.0330	.157	.0633	-.0394	.230	.0623	-.0529	.340	.0508	-.0661
.083	.0558	.0008	.083	.0860	.0150	.110	.0661	-.0214	.200	.0567	-.0394	.320	.0508	-.0529	.440	.0409	-.0661
.108	.0558	-.0025	.108	.0595	-.0098	.160	.0645	-.0263	.250	.0517	-.0377	.420	.0508	-.0579	.640	.0211	-.0678
.157	.0558	-.0025	.157	.0545	-.0098	.209	.0832	.0203	.300	.0467	-.0377	.520	.0277	-.0579			
.207	.0525	-.0025	.207	.0479	-.0131	.260	.0467	-.0195	.350	.0417	-.0377	.620	.0145	-.0595			
.250	.0458	-.0058	.250	.0446	-.0147	.300	.0401	-.0228	.400	.0384	-.0328	.710	.0063	-.0612			
.300	.0391	-.0108	.300	.0380	-.0164	.350	.0334	-.0278	.500	.0235	-.0377	.810	.0013	-.0628			
.350	.0391	-.0108	.350	.0330	-.0197	.400	.0301	-.0278	.600	.0409	-.0067	.910	-.0019	-.0628			
.400	.0375	-.0125	.400	.0264	-.0230	.500	.0218	-.0328	.700	.0030	-.0084						
.450			.450	.0248	-.0247	.600	.0135	-.0377	.800	-.0035	-.0513						
.500	.0425	.0008	.500	.0215	-.0263	.700	.0019	-.0444	.890	-.0085	-.0546						
.600			.600	.0165	-.0296	.800	-.0030	-.0461	.940	-.0101	-.0562						
.700	.0191	-.0258	.700	.0099	-.0346	.900	-.0030	-.0461									
.800	.0158	-.0292	.800	.0066	-.0379	.950	-.0013	-.0461									
.900	.0108	-.0325	.900	.0033	-.0412												
.950	.0091	-.0325	.950	.0000	-.0412												

TABLE B-4.- Continued

(b) $\alpha = 0.11^{O}$

Cp at 2y/b of:																	
0.00			0.20			0.40			0.60			0.80			0.95		
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower
			.020	.0458	.0509	.035			.056	.0253	.0336	.130	.0227	.0261	.200		
.032			.032	.0341	.0409	.060	.0265	.0331	.105	.0253	.0302	.180	.0211	.0228	.240	.0095	.0113
.058			.058	.0291	.0359	.085	.0216	.0298	.157	.0203	.0253	.230	.0161	.0179	.340	.0013	.0014
.083	.0224	.0276	.083	.0464	.0530	.110	.0232	.0298	.200	.0136	.0170	.320	.0079	.0063	.440	-.0052	-.0035
.108	.0191	.0242	.108	.0216	.0282	.160	.0199	.0265	.250	.0103	.0136	.420	.0046	-.0018	.640	-.0200	-.0199
.157	.0191	.0242	.157	.0183	.0232	.209	.0468	.0518	.300	.0070	.0086	.520	-.0101	-.0150			
.207	.0191	.0226	.207	.0116	.0149	.260	.0103	.0120	.350	.0037	.0037	.620	-.0200	-.0232			
.250	.0141	.0159	.250	.0083	.0116	.300	.0037	.0053	.400	-.0012	.0020	.710	-.0266	-.0298			
.300	.0091	.0109	.300	.0034	.0050	.350	-.0029	.0003	.500	-.0112	-.0095	.810	-.0316	-.0315			
.350	.0091	.0109	.350	-.0015	.0000	.400	-.0045	-.0012	.600	.0128	.0113	.910	-.0332	-.0364			
.400	.0041	.0092	.400	-.0048	-.0032	.500	-.0095	-.0079	.700	-.0266	.0047						
.450			.450	-.0065	-.0048	.600	-.0162	-.0195	.800	-.0316	-.0348						
.500	.0158	.0175	.500	-.0098	-.0065	.700	-.0261	-.0261	.890	-.0349	-.0397						
.600			.600	-.0114	-.0098	.800	-.0294	-.0294	.940	-.0349	-.0397						
.700	-.0075	-.0074	.700	-.0181	-.0181	.900	-.0294	-.0294									
.800	-.0108	-.0107	.800	-.0197	-.0197	.950	-.0294	-.0294									
.900	-.0158	-.0158	.900	-.0230	-.0263												
.950	-.0158	-.0174	.950	-.0247	-.0263												

TABLE B-4.- Continued

(c) $\alpha = 5.12^{O}$

Cp at 2y/b of:																	
0.00			0.20			0.40			0.60			0.80			0.95		
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower
			.020	-.0309	.1010	.035			.056	-.0527	.0867	.130	-.0562	.0822	.200		
.032			.032	-.0325	.0944	.060	-.0445	.0861	.105	-.0544	.0850	.180	-.0579	.0789	.240	-.0661	.0723
.058			.058	-.0309	.0944	.085	-.0479	.0811	.157	-.0544	.0784	.230	-.0579	.0740	.340	-.0678	.0608
.083	-.0042	.0843	.083	-.0015	.1060	.110	-.0429	.0845	.200	-.0544	.0701	.320	-.0579	.0624	.440	-.0678	.0509
.108	-.0092	.0810	.108	-.0263	.0811	.160	-.0479	.0811	.250	-.0544	.0634	.420	-.0612	.0492	.640	-.0661	.0311
.157	-.0075	.0793	.157	-.0263	.0778	.209	.0037	.0967	.300	-.0544	.0618	.520	-.0612	.0377			
.207	-.0092	.0760	.207	-.0263	.0662	.260	-.0328	.0634	.350	-.0527	.0568	.620	-.0645	.0261			
.250	-.0125	.0676	.250	-.0247	.0629	.300	-.0361	.0551	.400	-.0494	.0502	.710	-.0645	.0162			
.300	-.0158	.0610	.300	-.0230	.0530	.350	-.0361	.0468	.500	-.0527	.0369	.810	-.0645	.0113			
.350	-.0158	.0593	.350	-.0247	.0480	.400	-.0361	.0435	.600	-.0149	.0509	.910	-.0645	.0080			
.400	-.0158	.0560	.400	-.0280	.0398	.500	-.0361	.0352	.700	-.0529	.0492						
.450			.450	-.0297	.0365	.600	-.0361	.0203	.800	-.0579	.0047						
.500	-.0058	.0543	.500	-.0313	.0331	.700	-.0461	.0120	.890	-.0595	-.0002						
.600			.600	-.0346	.0282	.800	-.0477	.0053	.940	-.0595	-.0035						
.700	-.0292	.0342	.700	-.0379	.0199	.900	-.0494	.0037									
.800	-.0309	.0276	.800	-.0429	.0149	.950	-.0477	.0037									
.900	-.0342	.0209	.900	-.0445	.0100												
.950	-.0359	.0192	.950	-.0445	.0067												

TABLE B-4.- Continued

(d) $\alpha = 6.11^{o}$

Cp at 2y/b of:																	
0.00			0.20			0.40			0.60			0.80			0.95		
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower
			.020	-.0375	.1127	.035			.056	-.0627	.0967	.130	-.0678	.0938	.200		
.032			.032	-.0392	.1077	.060	-.0528	.0977	.105	-.0627	.0967	.180	-.0678	.0905	.240	-.0727	.0839
.058			.058	-.0392	.1077	.085	-.0561	.0961	.157	-.0610	.0900	.230	-.0678	.0872	.340	-.0711	.0707
.083	-.0092	.0977	.083	-.0131	.1192	.110	-.0545	.0977	.200	-.0610	.0817	.320	-.0678	.0740	.440	-.0711	.0624
.108	-.0125	.0960	.108	-.0379	.0961	.160	-.0561	.0961	.250	-.0610	.0751	.420	-.0694	.0591	.640	-.0694	.0410
.157	-.0125	.0944	.157	-.0396	.0911	.209	-.0062	.1100	.300	-.0610	.0718	.520	-.0694	.0476			
.207	-.0125	.0910	.207	-.0412	.0812	.260	-.0444	.0751	.350	-.0610	.0668	.620	-.0694	.0360			
.250	-.0175	.0810	.250	-.0363	.0745	.300	-.0444	.0668	.400	-.0560	.0618	.710	-.0694	.0261			
.300	-.0192	.0727	.300	-.0346	.0646	.350	-.0444	.0585	.500	-.0593	.0468	.810	-.0694	.0212			
.350	-.0209	.0710	.350	-.0330	.0580	.400	-.0444	.0552	.600	-.0233	.0624	.910	-.0694	.0179			
.400	-.0209	.0677	.400	-.0346	.0514	.500	-.0444	.0452	.700	-.0612	.0608						
.450			.450	-.0346	.0481	.600	-.0444	.0352	.800	-.0661	.0146						
.500	-.0092	.0660	.500	-.0363	.0447	.700	-.0494	.0203	.890	-.0678	.0080						
.600			.600	-.0396	.0381	.800	-.0527	.0136	.940	-.0678	.0064						
.700	-.0325	.0426	.700	-.0429	.0298	.900	-.0527	.0136									
.800	-.0359	.0359	.800	-.0446	.0232	.950	-.0527	.0136									
.900	-.0375	.0309	.900	-.0479	.0199												
.950	-.0375	.0276	.950	-.0479	.0149												

TABLE B-4.- Continued

(e) $\alpha = 8.12^{o}$

Cp at 2y/b of:																	
0.00			0.20			0.40			0.60			0.80			0.95		
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower
			.020	-.0525	.1412	.035			.056	-.0676	.1200	.130	-.0711	.1170	.200		
.032			.032	-.0525	.1345	.060	-.0534	.1226	.105	-.0693	.1200	.180	-.0711	.1137	.240	-.0727	.1038
.058			.058	-.0525	.1379	.085	-.0611	.1193	.157	-.0676	.1150	.230	-.0711	.1120	.340	-.0727	.0939
.083	-.0141	.1312	.083	-.0213	.1474	.110	-.0611	.1243	.200	-.0660	.1067	.320	-.0711	.0988	.440	-.0727	.0840
.108	-.0158	.1278	.108	-.0478	.1243	.160	-.0611	.1210	.250	-.0709	.1017	.420	-.0727	.0873	.640	-.0727	.0641
.157	-.0175	.1262	.157	-.0512	.1210	.209	-.0144	.1333	.300	-.0693	.0984	.520	-.0727	.0724			
.207	-.0191	.1212	.207	-.0512	.1077	.260	-.0560	.1001	.350	-.0693	.0918	.620	-.0727	.0592			
.250	-.0242	.1095	.250	-.0495	.1027	.300	-.0576	.0934	.400	-.0610	.0851	.710	-.0727	.0476			
.300	-.0275	.1011	.300	-.0478	.0912	.350	-.0560	.0834	.500	-.0693	.0718	.810	-.0711	.0427			
.350	-.0275	.0994	.350	-.0512	.0845	.400	-.0576	.0785	.600	-.0282	.0823	.910	-.0711	.0377			
.400	-.0275	.0961	.400	-.0512	.0762	.500	-.0593	.0702	.700	-.0661	.0542						
.450			.450	-.0512	.0729	.600	-.0560	.0569	.800	-.0694	.0344						
.500	-.0141	.0878	.500	-.0512	.0680	.700	-.0643	.0419	.890	-.0727	.0295						
.600			.600	-.0512	.0597	.800	-.0676	.0336	.940	-.0727	.0262						
.700	-.0392	.0660	.700	-.0512	.0498	.900	-.0676	.0336									
.800	-.0408	.0594	.800	-.0512	.0431	.950	-.0676	.0336									
.900	-.0425	.0510	.900	-.0528	.0382												
.950	-.0442	.0477	.950	-.0528	.0315												

TABLE B-4.- Continued

(f) $\alpha = 10.12^{o}$

Cp at 2y/b of:																	
0.00			0.20			0.40			0.60			0.80			0.95		
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower
			.020	-.0532	.1680	.035			.056	-.0693	.1433	.130	-.0727	.1417	.200		
.032			.032	-.0625	.1629	.060	-.0644	.1524	.105	-.0710	.1483	.180	-.0744	.1401	.240	-.0744	.1252
.058			.058	-.0609	.1713	.085	-.0644	.1475	.157	-.0710	.1433	.230	-.0744	.1368	.340	-.0744	.1170
.083	-.0191	.1680	.083	-.0296	.1789	.110	-.0677	.1541	.200	-.0693	.1350	.320	-.0744	.1269	.440	-.0744	.1087
.108	-.0225	.1646	.108	-.0561	.1574	.160	-.0661	.1524	.250	-.0726	.1316	.420	-.0760	.1186	.640	-.0744	.0906
.157	-.0225	.1613	.157	-.0578	.1541	.209	-.0195	.1615	.300	-.0710	.1283	.520	-.0760	.0988			
.207	-.0242	.1563	.207	-.0578	.1408	.260	-.0593	.1300	.350	-.0710	.1200	.620	-.0760	.0840			
.250	-.0308	.1429	.250	-.0578	.1359	.300	-.0643	.1233	.400	-.0627	.1134	.710	-.0760	.0724			
.300	-.0342	.1329	.300	-.0578	.1226	.350	-.0627	.1117	.500	-.0710	.1001	.810	-.0744	.0658			
.350	-.0342	.1312	.350	-.0594	.1143	.400	-.0660	.1100	.600	-.0315	.1071	.910	-.0744	.0625			
.400	-.0358	.1279	.400	-.0594	.1061	.500	-.0660	.0967	.700	-.0694	.0790						
.450			.450	-.0611	.1011	.600	-.0660	.0835	.800	-.0744	.0592						
.500	-.0191	.1145	.500	-.0611	.0961	.700	-.0693	.0668	.890	-.0760	.0526						
.600			.600	-.0594	.0878	.800	-.0726	.0585	.940	-.0760	.0493						
.700	-.0458	.0928	.700	-.0594	.0746	.900	-.0726	.0552									
.800	-.0458	.0844	.800	-.0594	.0663	.950	-.0726	.0552									
.900	-.0475	.0761	.900	-.0594	.0614												
.950	-.0492	.0727	.950	-.0594	.0564												

TABLE B-4.- Concluded

(g) $\alpha = 20.12^{O}$

Cp at 2y/b of:																	
0.00			0.20			0.40			0.60			0.80			0.95		
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower
			.020	-.0726	.3243	.035			.056	-.0743	.3108	.130	-.0760	.3011	.200		
.032			.032	-.0742	.3276	.060	-.0710	.3360	.105	-.0776	.3291	.180	-.0777	.3077	.240	-.0760	.2781
.058			.058	-.0742	.3793	.085	-.0727	.3360	.157	-.0743	.3341	.230	-.0760	.3110	.340	-.0760	.2781
.083	-.0492	.4160	.083	-.0379	.3922	.110	-.0710	.3575	.200	-.0743	.3324	.320	-.0760	.3061	.440	-.0760	.2781
.108	-.0559	.4127	.108	-.0661	.3806	.160	-.0710	.3575	.250	-.0776	.3324	.420	-.0777	.3044	.640	-.0760	.2616
.157	-.0475	.4093	.157	-.0677	.3806	.209	-.0261	.3590	.300	-.0743	.3291	.520	-.0777	.2830			
.207	-.0459	.4010	.207	-.0677	.3624	.260	-.0660	.3424	.350	-.0759	.3241	.620	-.0777	.2649			
.250	-.0509	.3776	.250	-.0677	.3558	.300	-.0726	.3341	.400	-.0676	.3091	.710	-.0777	.2501			
.300	-.0559	.3626	.300	-.0644	.3376	.350	-.0676	.3208	.500	-.0776	.2925	.810	-.0760	.2418			
.350	-.0559	.3610	.350	-.0694	.3293	.400	-.0726	.3175	.600	-.0348	.2830	.910	-.0760	.2369			
.400	-.0592	.3526	.400	-.0677	.3178	.500	-.0726	.2992	.700	-.0727	.2468						
.450			.450	-.0710	.3111	.600	-.0726	.2743	.800	-.0760	.2369						
.500	-.0392	.3143	.500	-.0710	.3029	.700	-.0776	.2444	.890	-.0777	.2336						
.600			.600	-.0677	.2863	.800	-.0809	.2328	.940	-.0777	.2253						
.700	-.0675	.2943	.700	-.0710	.2615	.900	-.0776	.2311									
.800	-.0675	.2742	.800	-.0710	.2433	.950	-.0793	.2311									
.900	-.0709	.2609	.900	-.0710	.2416												
.950	-.0709	.2542	.950	-.0694	.2300												

APPENDIX B

TABLE B-5.- PRESSURE COEFFICIENTS FOR WING WITH 76° SWEEP,

$C_{L,des} = 0.0$, $M = 4.6$

(a) $\alpha = -3.45°$

Cp at 2y/b of:																	
0.00			0.20			0.40			0.60			0.80			0.95		
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower
			.020	.0852	-.0035	.035			.056	.0680	-.0243	.130	.0652	-.0307	.200		
.032			.032	.0749	-.0055	.060	.0695	-.0121	.105	.0659	-.0222	.180	.0631	-.0307	.240	.0590	-.0409
.058			.058	.0708	-.0035	.085	.0634	-.0183	.157	.0597	-.0222	.230	.0570	-.0307	.340	.0468	-.0429
.083	.0563	.0026	.083	.0941	.0267	.110	.0634	-.0121	.200	.0495	-.0222	.320	.0468	-.0327	.440	.0386	-.0429
.108	.0522	.0006	.108	.0614	-.0040	.160	.0614	-.0162	.250	.0433	-.0243	.420	.0407	-.0348	.640	.0202	-.0470
.157	.0522	-.0014	.157	.0552	-.0081	.209	.0926	.0373	.300	.0392	-.0243	.520	.0243	-.0388			
.207	.0522	-.0035	.207	.0470	-.0101	.260	.0433	-.0140	.350	.0351	-.0264	.620	.0121	-.0429			
.250	.0439	-.0076	.250	.0429	-.0121	.300	.0372	-.0202	.400	.0330	-.0222	.710	.0039	-.0429			
.300	.0377	-.0097	.300	.0327	-.0162	.350	.0289	-.0222	.500	.0187	-.0325	.810	-.0001	-.0470			
.350	.0357	-.0117	.350	.0286	-.0203	.400	.0248	-.0243	.600	.0188	.0122	.910	-.0042	-.0450			
.400	.0336	-.0138	.400	.0225	-.0224	.500	.0166	-.0284	.700	.0468	-.0368						
.450			.450	.0204	-.0224	.600	.0084	-.0284	.800	-.0062	-.0429						
.500	.0439	.0068	.500	.0163	-.0244	.700	-.0018	-.0366	.890	-.0103	-.0429						
.600			.600	.0122	-.0265	.800	-.0079	-.0387	.940	-.0123	-.0429						
.700	.0130	-.0241	.700	.0061	-.0306	.900	-.0100	-.0407									
.800	.0088	-.0282	.800	.0020	-.0326	.950	-.0079	-.0387									
.900	.0026	-.0282	.900	-.0040	-.0367												
.950	.0006	-.0303	.950	-.0040	-.0347												

TABLE B-5.- Continued

(b) $\alpha = 0.56^{o}$

Cp at 2y/b of:																	
0.00			0.20			0.40			0.60			0.80			0.95		
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower
			.020	.0419	.0543	.035			.056	.0229	.0353	.130	.0183	.0306	.200		
.032			.032	.0315	.0419	.060	.0246	.0349	.105	.0188	.0333	.180	.0162	.0285	.240	.0040	.0224
.058			.058	.0274	.0377	.085	.0185	.0308	.157	.0147	.0271	.230	.0122	.0244	.340	-.0000	.0101
.083	.0253	.0295	.083	.0554	.0595	.110	.0185	.0308	.200	.0105	.0209	.320	.0040	.0142	.440	-.0082	.0060
.108	.0233	.0274	.108	.0205	.0267	.160	.0144	.0287	.250	.0064	.0189	.420	-.0000	.0122	.640	-.0184	-.0102
.157	.0171	.0233	.157	.0185	.0205	.209	.0619	.0662	.300	.0023	.0147	.520	-.0123	-.0041			
.207	.0171	.0233	.207	.0123	.0164	.260	.0126	.0127	.350	.0003	.0086	.620	-.0184	-.0123			
.250	.0130	.0171	.250	.0103	.0123	.300	.0064	.0065	.400	.0023	.0086	.710	-.0225	-.0204			
.300	.0068	.0109	.300	.0041	.0062	.350	.0023	.0003	.500	-.0079	-.0057	.810	-.0266	-.0225			
.350	.0047	.0109	.350	-.0019	.0021	.400	-.0017	-.0016	.600	.0285	.0265	.910	-.0286	-.0266			
.400	.0047	.0088	.400	-.0060	-.0019	.500	-.0099	-.0057	.700	.0081	-.0225						
.450			.450	-.0081	-.0040	.600	-.0099	-.0160	.800	-.0245	-.0307						
.500	.0212	.0253	.500	-.0101	-.0040	.700	-.0222	-.0242	.890	-.0307	-.0327						
.600			.670	-.0121	-.0101	.800	-.0284	-.0263	.940	-.0327	-.0327						
.700	-.0117	-.0055	.700	-.0183	-.0142	.900	-.0284	-.0263									
.800	-.0158	-.0097	.800	-.0203	-.0183	.950	-.0284	-.0263									
.900	-.0179	-.0138	.900	-.0224	-.0203												
.950	-.0200	-.0158	.950	-.0244	-.0224												

TABLE B-5.- Continued

(c) $\alpha = 5.56^{o}$

Cp at 2y/b of:																	
0.00			0.20			0.40			0.60			0.80			0.95		
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower
			.020	-.0220	.1040	.035			.056	-.0366	.0888	.130	-.0368	.0837	.200		
.032			.032	-.0220	.0978	.060	-.0285	.0861	.105	-.0366	.0868	.180	-.0368	.0817	.240	-.0429	.0776
.058			.058	-.0220	.0957	.085	-.0326	.0820	.157	-.0366	.0785	.230	-.0388	.0776	.340	-.0429	.0653
.083	-.0035	.0771	.083	.0205	.1127	.110	-.0306	.0820	.200	-.0387	.0724	.320	-.0388	.0653	.440	-.0450	.0571
.108	-.0076	.0751	.108	-.0121	.0820	.160	-.0326	.0820	.250	-.0407	.0662	.420	-.0409	.0633	.640	-.0450	.0387
.157	-.0076	.0751	.157	-.0142	.0758	.209	.0292	.1074	.300	-.0407	.0621	.520	-.0429	.0408			
.207	-.0076	.0751	.207	-.0162	.0656	.260	-.0242	.0621	.350	-.0387	.0559	.620	-.0450	.0306			
.250	-.0117	.0647	.250	-.0203	.0615	.300	-.0284	.0538	.400	-.0345	.0538	.710	-.0450	.0203			
.300	-.0158	.0585	.300	-.0224	.0513	.350	-.0325	.0456	.500	-.0407	.0374	.810	-.0450	.0162			
.350	-.0179	.0585	.350	-.0244	.0451	.400	-.0345	.0415	.600	.0122	.0612	.910	-.0450	.0122			
.400	-.0200	.0544	.400	-.0285	.0390	.500	-.0366	.0353	.700	.0040	.0101						
.450			.450	-.0285	.0369	.600	-.0345	.0168	.800	-.0388	.0040						
.500	.0047	.0585	.500	-.0285	.0328	.700	-.0407	.0106	.890	-.0429	-.0000						
.600			.600	-.0306	.0267	.800	-.0448	.0065	.940	-.0429	-.0021						
.700	-.0282	.0296	.700	-.0326	.0205	.900	-.0448	.0045									
.800	-.0303	.0234	.800	-.0347	.0144	.950	-.0448	.0045									
.900	-.0324	.0172	.900	-.0367	.0103												
.950	-.0344	.0151	.950	-.0367	.0082												

TABLE B-5.- Continued

(d) $\alpha = 6.56^{o}$

Cp at 2y/b of:																	
0.00			0.20			0.40			0.60			0.80			0.95		
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower
			.020	-.0406	.1123	.035			.056	-.0449	.1010	.130	-.0491	.0939	.200		
.032			.032	-.0344	.1081	.060	-.0367	.0984	.105	-.0449	.1010	.180	-.0491	.0919	.240	-.0511	.0878
.058			.058	-.0323	.1081	.085	-.0388	.0943	.157	-.0449	.0928	.230	-.0491	.0878	.340	-.0491	.0755
.083	-.0137	.0937	.083	.0082	.1230	.110	-.0367	.0963	.200	-.0449	.0866	.320	-.0491	.0776	.440	-.0491	.0674
.108	-.0179	.0916	.108	-.0224	.0963	.160	-.0408	.0922	.250	-.0449	.0804	.420	-.0491	.0735	.640	-.0491	.0469
.157	-.0158	.0895	.157	-.0265	.0902	.209	.0208	.1135	.300	-.0469	.0743	.520	-.0491	.0530			
.207	-.0158	.0895	.207	-.0285	.0799	.260	-.0346	.0743	.350	-.0449	.0702	.620	-.0491	.0408			
.250	-.0199	.0895	.250	-.0285	.0738	.300	-.0346	.0681	.400	-.0366	.0660	.710	-.0491	.0306			
.300	-.0241	.0730	.300	-.0326	.0636	.350	-.0407	.0539	.500	-.0449	.0496	.810	-.0491	.0244			
.350	-.0261	.0709	.350	-.0326	.0574	.400	-.0428	.0558	.600	.0040	.0714	.910	-.0491	.0203			
.400	-.0261	.0647	.400	-.0347	.0492	.500	-.0428	.0475	.700	.0019	.0244						
.450			.450	-.0347	.0472	.600	-.0387	.0352	.800	-.0450	.0162						
.500	-.0013	.0689	.500	-.0347	.0431	.700	-.0449	.0229	.890	-.0491	.0101						
.600			.600	-.0367	.0369	.800	-.0469	.0167	.940	-.0491	.0081						
.700	-.0344	.0379	.700	-.0367	.0287	.900	-.0469	.0147									
.800	-.0385	.0317	.800	-.0408	.0205	.950	-.0469	.0147									
.900	-.0385	.0255	.900	-.0408	.0205												
.950	-.0406	.0255	.950	-.0408	.0164												

TABLE B-5.- Continued

(e) $\alpha = 8.56^{o}$

Cp at 2y/b of:																	
0.00			0.20			0.40			0.60			0.80			0.95		
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower
			.020	-.0427	.1389	.035			.056	-.0510	.1213	.130	-.0511	.1185	.200		
.032			.032	-.0427	.1348	.060	-.0429	.1230	.105	-.0510	.1254	.180	-.0532	.1164	.240	-.0532	.1082
.058			.058	-.0427	.1368	.085	-.0429	.1209	.157	-.0489	.1193	.230	-.0511	.1123	.340	-.0511	.1001
.083	-.0199	.1265	.083	.0000	.1516	.110	-.0429	.1230	.200	-.0489	.1131	.320	-.0511	.1021	.440	-.0511	.0898
.108	-.0261	.1245	.108	-.0326	.1230	.160	-.0429	.1189	.250	-.0510	.1070	.420	-.0532	.0960	.640	-.0511	.0694
.157	-.0220	.1224	.157	-.0326	.1189	.209	.0147	.1439	.300	-.0510	.1008	.520	-.0532	.0755			
.207	-.0220	.1203	.207	-.0347	.1066	.260	-.0387	.1008	.350	-.0489	.0967	.620	-.0532	.0612			
.250	-.0261	.1079	.250	-.0367	.1004	.300	-.0448	.0946	.400	-.0407	.0885	.710	-.0532	.0510			
.300	-.0282	.0997	.300	-.0367	.0902	.350	-.0448	.0844	.500	-.0510	.0741	.810	-.0511	.0419			
.350	-.0303	.0976	.350	-.0408	.0820	.400	-.0469	.0803	.600	.0019	.0919	.919	-.0511	.0408			
.400	-.0323	.0955	.400	-.0408	.0738	.500	-.0489	.0700	.700	-.0000	.0449						
.450			.450	-.0408	.0697	.600	-.0469	.0556	.800	-.0470	.0346						
.500	-.0055	.0914	.500	-.0408	.0676	.700	-.0489	.0433	.890	-.0511	.0306						
.600			.600	-.0408	.0595	.800	-.0551	.0351	.940	-.0532	.0265						
.700	-.0385	.0625	.700	-.0449	.0492	.900	-.0551	.0330									
.800	-.0406	.0563	.800	-.0449	.0410	.950	-.0531	.0330									
.900	-.0427	.0481	.900	-.0449	.0369												
.950	-.0427	.0460	.950	-.0449	.0349												

TABLE B-5.- Continued

(f) $\alpha = 10.57^{o}$

Cp at 2y/b of:																	
0.00			0.20			0.40			0.60			0.80			0.95		
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower
			.020	-.0489	.1678	.035			.056	-.0490	.1483	.130	-.0532	.1430	.200		
.032			.032	-.0489	.1616	.060	-.0470	.1516	.105	-.0510	.1524	.180	-.0552	.1430	.240	-.0532	.1307
.058			.058	-.0489	.1657	.085	-.0470	.1475	.157	-.0490	.1483	.230	-.0532	.1409	.340	-.0532	.1225
.083	-.0261	.1637	.083	-.0040	.1824	.110	-.0511	.1516	.200	-.0490	.1400	.320	-.0532	.1287	.440	-.0532	.1144
.108	-.0323	.1596	.108	-.0388	.1537	.160	-.0470	.1496	.250	-.0531	.1359	.420	-.0552	.1246	.640	-.0532	.0939
.157	-.0282	.1575	.157	-.0408	.1516	.209	-.0125	.1709	.300	-.0490	.1298	.520	-.0552	.1021			
.207	-.0261	.1534	.207	-.0429	.1373	.260	-.0387	.1298	.350	-.0510	.1257	.620	-.0552	.0878			
.250	-.0303	.1410	.250	-.0429	.1332	.300	-.0469	.1215	.400	-.0408	.1174	.710	-.0532	.0755			
.300	-.0323	.1306	.300	-.0408	.1209	.350	-.0449	.1113	.500	-.0510	.1010	.810	-.0532	.0694			
.350	-.0344	.1286	.350	-.0449	.1107	.400	-.0469	.1092	.600	-.0000	.1164	.910	-.0532	.0653			
.400	-.0365	.1245	.400	-.0429	.1025	.500	-.0490	.0989	.700	-.0286	.0674						
.450			.450	-.0449	.0984	.600	-.0469	.0804	.800	-.0511	.0532						
.500	-.0096	.1183	.500	-.0449	.0922	.700	-.0531	.0660	.890	-.0532	.0530						
.600			.600	-.0449	.0840	.800	-.0551	.0578	.940	-.0552	.0490						
.700	-.0427	.0873	.700	-.0490	.0717	.900	-.0551	.0558									
.800	-.0447	.0811	.800	-.0511	.0636	.950	-.0551	.0558									
.900	-.0447	.0749	.900	-.0511	.0595												
.950	-.0468	.0728	.950	-.0490	.0554												

TABLE B-5.- Concluded

(g) $\alpha = 20.56^{O}$

Cp at 2y/b of:																	
0.00			0.20			0.40			0.60			0.80			0.95		
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower
			.020	-.0509	.3433	.035			.056	-.0510	.3127	.130	-.0552	.3065	.200		
.032			.032	-.0530	.3557	.060	-.0531	.3278	.105	-.0551	.3333	.180	-.0572	.3106	.240	-.0552	.2534
.058			.058	-.0530	.3825	.085	-.0531	.3278	.157	-.0531	.3353	.230	-.0552	.3147	.340	-.0532	.2697
.083	-.0365	.3908	.083	-.0101	.3934	.110	-.0511	.3463	.200	-.0510	.3312	.320	-.0552	.3106	.440	-.0552	.2738
.108	-.0427	.3763	.108	-.0429	.3750	.160	-.0511	.3442	.250	-.0551	.3312	.420	-.0572	.3086	.640	-.0552	.2656
.157	-.0365	.3805	.157	-.0470	.3750	.209	-.0105	.3579	.300	-.0531	.3312	.520	-.0552	.2840			
.207	-.0365	.3929	.207	-.0470	.3524	.260	-.0428	.3353	.350	-.0531	.3250	.620	-.0552	.2636			
.250	-.0406	.3722	.250	-.0490	.3442	.300	-.0510	.3292	.400	-.0428	.3107	.710	-.0552	.2493			
.300	-.0448	.3516	.300	-.0449	.3258	.350	-.0449	.3148	.500	-.0551	.2922	.810	-.0532	.2411			
.350	-.0427	.3433	.350	-.0511	.3176	.400	-.0510	.3148	.600	-.0021	.2902	.910	-.0552	.2350			
.400	-.0468	.3433	.400	-.0470	.3032	.500	-.0531	.2963	.700	-.0491	.2493						
.450			.450	-.0511	.3012	.600	-.0510	.2716	.800	-.0552	.2309						
.500	-.0179	.3103	.500	-.0511	.2930	.700	-.0551	.2408	.890	-.0572	.2247						
.600			.600	-.0490	.2787	.800	-.0592	.2305	.940	-.0572	.2186						
.700	-.0509	.2876	.700	-.0531	.2561	.900	-.0572	.2264									
.800	-.0530	.2690	.800	-.0531	.2397	.950	-.0551	.2264									
.900	-.0530	.2566	.900	-.0531	.2336												
.950	-.0530	.2545	.950	-.0531	.2233												

TABLE B-6.- PRESSURE COEFFICIENTS FOR WING WITH 76° SWEEP,

$C_{L,des} = 0.1$, $M = 2.3$

(a) $\alpha = -2.05°$

Cp at 2y/b of:																	
0.00			0.20			0.40			0.60			0.80			0.95		
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower
.029	-.0052	.0977	.025	.0585	.0406	.036	.0542	-.0065	.064	.0627	-.0569	.104	.0281	-.0634	.206	.0109	-.1259
.038	-.0063	.1368	.037	.0510	.0628	.061	.0510	-.0034	.112	.0393	-.0155	.150	.0135	-.0603	.260	.0076	-.1344
.064	.0000	.1410	.061	.0542	.0579	.085	.0436	.0156	.161	.0127	-.0028	.200	.0109	-.0603	.350	-.0159	-.1302
.087	.0074	.1220	.056	.0351	.0526	.110	.0383	.0188	.209	-.0031	.0014	.300	-.0019	-.0592	.460	-.0353	-.1323
.112	-.0042	.1410	.110	.0287	.0484	.160	.0393	.0289	.259	-.0063	.0056	.400	-.0278	-.0571	.640	-.0655	-.1249
.162	.0011	.0924	.160	.0213	.0431	.209	.0085	.0162	.307	-.0105	-.0038	.500	-.0407	-.0634	.830	-.0655	-.1259
.210	.0042	.0797	.210	.0096	.0092	.259	.0032	.0077	.358	-.0180	-.0091	.600	-.0612	-.0677			
.260	-.0052	.0343	.250	.0000	-.0055	.309	-.0084	-.0028	.406	-.0233	-.0176	.680	-.0730	-.0677			
.310	.0213	.0015	.300	-.0042	.0008	.356	-.0201	-.0038	.500	-.0407	-.0253	.780	-.0827	-.0687			
.360	.0213	.0089	.350	-.0052	.0018	.406	-.0244	.0035	.600	-.0515	-.0370	.880	-.0838	-.0719			
.380	.0106	.0068	.400	-.0042	.0039	.505	-.0318	-.0219	.700	-.0493	-.0465						
.460	.0042	-.0037	.450	-.0116	-.0118	.604	-.0169	-.0282	.800	-.0536	-.0539						
.510	.0011	-.0100	.500	-.0031	-.0182	.703	-.0159	-.0325	.900	-.0601	-.0465						
.600	-.0020	-.0385	.600	-.0095	.1690	.802	-.0222	-.0494	.950	-.0644	-.0423						
.700	.0138	-.0343	.700	-.0042	-.0362	.902	-.0265	-.0473									
.800	.0191	-.0459	.800	-.0063	-.0383	.952	-.0382	-.0505									
.900	-.0180	-.0554	.900	-.0116	-.0594												
.950	.0064	-.0544	.950	-.0127	-.0594												

TABLE B-6.- Continued

(b) $\alpha = -0.05^{o}$

Cp at 2y/b of:																		
0.00			0.20			0.40			0.60			0.80			0.95		
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower
.029			.025	.0079	.0724	.036	.0188	.0236	.064	.0245	.0288	.104			.206		
.038			.037	.0121	.0840	.061	.0156	.0215	.112	.0000	.0499	.150	-.0259	.0104	.260	.0063	-.0530
.064	-.0005	.1904	.061	.0305	.0783	.085	.0093	.0394	.161	-.0286	.0362	.200	-.0345	.0019	.350	-.0151	-.0424
.087	-.0005	.1683	.056	.0103	.0731	.110	.0029	.0383	.209	-.0456	.0309	.300	-.0496	-.0054	.460	-.0345	-.0488
.112	-.0047	.1852	.110	.0039	.0699	.160	.0043	.0489	.259	-.0456	.0256	.400	-.0700	-.0149	.640	-.0614	-.0456
.162	-.0016	.1314	.160	-.0045	.0636	.209	-.0265	.0351	.307	-.0467	.0161	.500	-.0807	-.0265	.830	-.0625	-.0530
.210	-.0005	.1146	.210	-.0130	.0299	.259	-.0286	.0267	.358	-.0520	.0098	.600	-.0990	-.0339			
.260	-.0069	.0566	.250	-.0204	.0131	.309	-.0382	.0140	.406	-.0563	-.0017	.680	-.1098	-.0382			
.310	.0111	.0208	.300	-.0236	.0183	.356	-.0446	.0119	.500	-.0668	-.0107	.780	-.1152	-.0424			
.360	.0100	.0281	.350	-.0236	.0194	.406	-.0488	.0204	.600	-.0764	-.0212	.880	-.1130	-.0477			
.380	-.0016	.0292	.400	-.0225	.0226	.505	-.0520	-.0038	.700	-.0721	-.0318						
.460	-.0069	.0134	.450	-.0268	.0057	.604	-.0361	-.0112	.800	-.0743	-.0392						
.510			.500	-.0204	-.0005	.703	-.0339	-.0186	.900	-.0797	-.0318						
.600			.600			.802	-.0414	-.0366	.950	-.0840	-.0276						
.700	.0015	-.0213	.700	-.0246	-.0216	.902	-.0467	-.0334									
.800	.0058	-.0350	.800	-.0268	-.0321	.952	-.0563	-.0376									
.900			.900	-.0310	-.0447												
.950	.0058	-.0413	.950	-.0321	-.0458												

TABLE B-6.- Continued

(c) $\alpha = 2.95^{o}$

Cp at 2y/b of:																	
0.00			0.20			0.40			0.60			0.80			0.95		
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower
.029			.025	-.1079	.1168	.036	-.0963	.0475	.064	-.0832	.0641	.104			.206		
.038			.037	-.0921	.1220	.061	-.0889	.0465	.112	-.0757	.0853	.150	-.1323	.0465	.260	-.0042	-.0099
.064	-.0126	.2738	.061	-.0603	.1130	.085	-.0624	.0665	.161	-.0906	.0652	.200	-.1248	.0369	.350	-.0548	.0038
.087	-.0116	.2496	.056	-.0539	.1098	.110	-.0592	.0655	.209	-.1033	.0599	.300	-.1312	.0273	.460	-.0494	-.0067
.112	-.0126	.2622	.110	-.0444	.1066	.160	-.0418	.0747	.259	-.1012	.0557	.400	-.1452	.0188	.640	-.0602	-.0056
.162	-.0105	.1937	.160	-.0402	.0971	.209	-.0662	.0620	.307	-.1002	.0472	.500	-.1248	.0060	.830	-.0871	-.0270
.210	-.0105	.1747	.210	-.0444	.0592	.259	-.0662	.0514	.358	-.0991	.0409	.600	-.1538	-.0014			
.260	-.0211	.1094	.250	-.0497	.0423	.309	-.0715	.0377	.406	-.0991	.0292	.680	-.1538	-.0110			
.310	-.0073	.0588	.300	-.0518	.0465	.356	-.0768	.0377	.500	-.0979	.0134	.780	-.1517	-.0184			
.360	-.0073	.0630	.350	-.0486	.0465	.406	-.0779	.0451	.600	-.1054	.0028	.880	-.1473	-.0259			
.380	-.0169	.0651	.400	-.0476	.0486	.505	-.0779	.0229	.700	-.1011	-.0099						
.460	-.0222	.0461	.450	-.0539	.0317	.604	-.0651	.0144	.800	-.1043	-.0174						
.510			.500	-.0497	.0264	.703	-.0662	.0059	.900	-.1108	-.0088						
.600			.600			.802	-.0726	-.0130	.950	-.1151	-.0046						
.700	-.0169	.0019	.700	-.0529	.0022	.902	-.0789	-.0109									
.800	-.0105	-.0138	.800	-.0518	-.0104	.952	-.0895	-.0151									
.900			.900	-.0518	-.0231												
.950	-.0094	-.0212	.950	-.0539	-.0241												

TABLE B-6.- Continued

(d) $\alpha = 3.95^{o}$

Cp at 2y/b of:																	
0.00			0.20			0.40			0.60			0.80			0.95		
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower
.029			.025	-.1397	.1351	.036	-.1217	.0537	.064	-.1371	.0689	.104			.206		
.038			.037	-.1385	.1383	.061	-.1227	.0527	.112	-.1297	.0921	.150	-.1796	.0679	.260	-.0404	.0137
.064	-.0157	.2982	.061	-.0909	.1276	.085	-.1121	.0738	.161	-.1233	.0731	.200	-.1626	.0585	.350	-.0872	.0272
.087	-.0125	.2783	.056	-.0793	.1234	.110	-.1079	.0738	.209	-.1222	.0668	.300	-.1584	.0502	.460	-.0967	.0189
.112	-.0168	.2919	.110	-.0645	.1212	.160	-.0776	.0826	.259	-.1148	.0625	.400	-.1488	.0429	.640	-.0638	.0189
.162	-.0115	.2130	.160	-.0528	.1117	.209	-.0935	.0699	.307	-.1116	.0562	.500	-.1159	.0314	.830	-.0935	-.0029
.210	-.0178	.1962	.210	-.0539	.0717	.259	-.0893	.0594	.358	-.1095	.0478	.600	-.1488	.0231			
.260	-.0263	.1288	.250	-.0570	.0548	.309	-.0903	.0467	.406	-.1095	.0372	.680	-.1499	.0126			
.310	-.0125	.0814	.300	-.0560	.0580	.356	-.0925	.0467	.500	-.0957	.0366	.780	-.1509	.0053			
.360	-.0125	.0804	.350	-.0560	.0569	.406	-.0935	.0541	.600	-.0967	.0241	.880	-.1520	-.0029			
.380	-.0231	.0783	.400	-.0549	.0590	.505	-.0925	.0309	.700	-.1074	.0126						
.460	-.0253	.0562	.450	-.0613	.0411	.604	-.0776	.0214	.800	-.1137	.0064						
.510			.500	-.0549	.0358	.703	-.0755	.0140	.900	-.1244	.0147						
.600			.600			.802	-.0787	-.0049	.950	-.1286	.0189						
.700	-.0231	.0151	.700	-.0592	.0105	.902	-.0808	-.0028									
.800	-.0210	-.0048	.800	-.0592	-.0010	.952	-.0893	-.0071									
.900			.900	-.0602	-.0147												
.950	-.0168	-.0132	.950	-.0623	-.0158												

TABLE B-6.- Continued

(e) $\alpha = 4.95^{o}$

Cp at 2y/b of:																	
0.00			0.20			0.40			0.60			0.80			0.95		
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower
.029			.025	-.1662	.1514	.036	-.1512	.0624	.064	-.1529	.0790	.104			.206		
.038			.037	-.1683	.1566	.061	-.1533	.0624	.112	-.1572	.1022	.150	-.1763	.0756	.260	-.0857	.0201
.064	-.0200	.3258	.061	-.1183	.1455	.085	-.1544	.0834	.161	-.1551	.0821	.200	-.1741	.0662	.350	-.1155	.0327
.087	-.0168	.3069	.056	-.1003	.1413	.110	-.1523	.0834	.209	-.1529	.0779	.300	-.1741	.0588	.460	-.1166	.0232
.112	-.0221	.3248	.110	-.0865	.1382	.160	-.1210	.0937	.259	-.1487	.0737	.400	-.1709	.0515	.640	-.0910	.0253
.162	-.0147	.2376	.160	-.0696	.1287	.209	-.1381	.0811	.307	-.1455	.0663	.500	-.1198	.0379	.830	-.1262	.0044
.210	-.0221	.2186	.210	-.0632	.0877	.259	-.1327	.0695	.358	-.1444	.0589	.600	-.1763	.0295			
.260	-.0306	.1493	.250	-.0632	.0698	.309	-.1253	.0568	.406	-.1434	.0494	.680	-.1816	.0190			
.310	-.0168	.0999	.300	-.0632	.0729	.356	-.1210	.0579	.500	-.1326	.0442	.780	-.1848	.0117			
.360	-.0168	.0967	.350	-.0621	.0719	.406	-.1157	.0663	.600	-.1358	.0316	.880	-.1890	.0023			
.380	-.0285	.0946	.400	-.0611	.0719	.505	-.0987	.0420	.700	-.1560	.0190						
.460	-.0327	.0746	.450	-.0653	.0529	.604	-.0721	.0336	.800	-.1635	.0127						
.510			.500	-.0611	.0487	.703	-.0699	.0252	.900	-.1677	.0222						
.600			.600			.802	-.0774	.0051	.950	-.1677	.0253						
.700	-.0295	.0252	.700	-.0674	.0214	.902	-.0827	.0083									
.800	-.0263	.0042	.800	-.0674	.0098	.952	-.0923	.0030									
.900			.900	-.0685	-.0038												
.950	-.0253	-.0030	.950	-.0706	-.0048												

TABLE B-6.- Continued

(f) $\alpha = 5.95^{o}$

Cp at 2y/b of:																	
0.00			0.20			0.40			0.60			0.80			0.95		
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower
.029			.025	-.1842	.1672	.036	-.1725	.0732	.064	-.1638	.0853	.104			.206		
.038			.037	-.1895	.1735	.061	-.1746	.0732	.112	-.1691	.1085	.150	-.1838	.0814	.260	-.1145	.0245
.064	-.0233	.3532	.061	-.1449	.1635	.085	-.1767	.0963	.161	-.1712	.0916	.200	-.1838	.0729	.350	-.1220	.0382
.087	-.0201	.3364	.056	-.1184	.1593	.110	-.1788	.0953	.209	-.1723	.0874	.300	-.1838	.0645	.460	-.1220	.0298
.112	-.0265	.3543	.110	-.1025	.1562	.160	-.1521	.1043	.259	-.1701	.0832	.400	-.1838	.0603	.640	-.1167	.0309
.162	-.0191	.2607	.160	-.0845	.1457	.209	-.1733	.0927	.307	-.1712	.0758	.500	-.1220	.0466	.830	-.1795	.0109
.210	-.0254	.2428	.210	-.0739	.1047	.259	-.1691	.0800	.358	-.1733	.0684	.600	-.1891	.0361			
.260	-.0339	.1682	.250	-.0707	.0858	.309	-.1627	.0653	.406	-.1765	.0600	.680	-.1933	.0256			
.310	-.0212	.1178	.300	-.0686	.0879	.356	-.1595	.0674	.500	-.1699	.0508	.780	-.1987	.0182			
.360	-.0233	.1146	.350	-.0675	.0879	.406	-.1521	.0769	.600	-.1806	.0382	.880	-.2051	.0109			
.380	-.0339	.1115	.400	-.0644	.0869	.505	-.1096	.0526	.700	-.2019	.0256						
.460	-.0381	.0904	.450	-.0697	.0669	.604	-.0735	.0452	.800	-.2061	.0203						
.510			.500	-.0665	.0627	.703	-.0788	.0347	.900	-.1976	.0298						
.600			.600			.802	-.0851	.0136	.950	-.1870	.0340						
.700	-.0381	.0358	.700	-.0750	.0344	.902	-.0905	.0168									
.800	-.0328	.0148	.800	-.0750	.0218	.952	-.0990	.0125									
.900			.900	-.0771	.0071												
.950	-.0318	.0011	.950	-.0792	.0060												

TABLE B-6.- Continued

(g) $\alpha = 9.96^{o}$

Cp at 2y/b of:																	
0.00			0.20			0.40			0.60			0.80			0.95		
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower
.029			.025	-.2233	.2473	.036	-.2105	.1188	.064	-.1956	.1173	.104			.206		
.038			.037	-.2276	.2536	.061	-.2116	.1199	.112	-.1977	.1426	.150	-.2079	.1173	.260	-.1264	.0642
.064	-.0505	.4482	.061	-.2116	.2379	.085	-.2127	.1441	.161	-.1998	.1300	.200	-.2068	.1162	.350	-.1339	.0725
.087	-.0409	.4524	.056	-.2180	.2337	.110	-.2127	.1441	.209	-.2020	.1258	.300	-.2100	.1152	.460	-.1339	.0683
.112	-.0452	.4745	.110	-.2127	.2295	.160	-.1871	.1563	.259	-.2041	.1258	.400	-.2154	.1121	.640	-.1264	.0735
.162	-.0335	.3693	.160	-.1691	.2179	.209	-.2169	.1437	.307	-.2062	.1184	.500	-.1286	.0954	.830	-.2186	.0600
.210	-.0399	.3409	.210	-.1596	.1726	.259	-.2200	.1310	.358	-.2094	.1131	.600	-.2314	.0829			
.260	-.0473	.2505	.250	-.1532	.1515	.309	-.2222	.1152	.406	-.2169	.1058	.680	-.2400	.0746			
.310	-.0377	.1989	.300	-.1373	.1515	.356	-.2296	.1152	.500	-.2164	.1058	.780	-.2432	.0683			
.360	-.0420	.1958	.350	-.1107	.1494	.406	-.2349	.1279	.600	-.2154	.0912	.880	-.2357	.0621			
.380	-.0536	.1874	.400	-.1001	.1483	.505	-.2115	.1005	.700	-.2443	.0777						
.460	-.0600	.1621	.450	-.1065	.1252	.604	-.1743	.0931	.800	-.2464	.0746						
.510			.500	-.1065	.1220	.703	-.1520	.0815	.900	-.2411	.0850						
.600			.600			.802	-.1361	.0636	.950	-.2357	.0850						
.700	-.0780	.0980	.700	-.1129	.0862	.902	-.1361	.0658									
.800	-.0674	.0675	.800	-.1150	.0735	.952	-.1424	.0594									
.900			.900	-.1160	.0535												
.950	-.0727	.0549	.950	-.1171	.0535												

TABLE B-6.- Concluded

(h) $\alpha = 19.95^{o}$

Cp at 2y/b of:																	
0.00			0.20			0.40			0.60			0.80			0.95		
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower
.029			.025	-.2478	.5067	.036	-.2392	.2893	.064	-.2264	.2520	.104			.206		
.038			.037	-.2520	.5257	.061	-.2392	.2935	.112	-.2296	.2954	.150	-.2528	.2541	.260	-.1503	.1912
.064	-.0953	-.2385	.061	-.2297	.4919	.085	-.2382	.3389	.161	-.2328	.2933	.200	-.2528	.2636	.350	-.1530	.2017
.087	-.1207	-.2385	.056	-.2477	.4919	.110	-.2392	.3442	.209	-.2360	.2933	.300	-.2538	.2604	.460	-.1568	.2028
.112	-.1027	-.2385	.110	-.2488	.4888	.160	-.2126	.3462	.259	-.2370	.2975	.400	-.2538	.2741	.640	-.1342	.2143
.162	-.1207	.6661	.160	-.2488	.4708	.209	-.2423	.3346	.307	-.2370	.2933	.500	-.1482	.2594	.830	-.2236	.2091
.210	-.1218	.6555	.210	-.2477	.4233	.259	-.2434	.3176	.358	-.2328	.2901	.600	-.2506	.2489			
.260	-.1186	.5299	.250	-.2488	.4012	.309	-.2413	.2986	.406	-.2349	.2880	.680	-.2538	.2437			
.310	-.1133	.4740	.300	-.2477	.3938	.356	-.2423	.2986	.500	-.2280	.2846	.780	-.2538	.2384			
.360	-.1249	.4719	.350	-.2276	.3874	.406	-.2423	.3208	.600	-.2269	.2678	.880	-.2420	.2353			
.380	-.1525	.4508	.400	-.2116	.3811	.505	-.2423	.2933	.700	-.2603	.2489						
.460	-.1715	.4107	.450	-.2053	.3473	.604	-.2328	.2848	.800	-.2603	.2468						
.510			.500	-.2010	.3473	.703	-.2253	.2763	.900	-.2592	.2636						
.600			.600			.802	-.2200	.2456	.950	-.2560	.2709						
.700	-.1620	.3199	.700	-.2000	.2998	.902	-.2179	.2446									
.800	-.1419	.2692	.800	-.2010	.2808	.952	-.2200	.2382									
.900			.900	-.2010	.2566												
.950	-.1175	.2502	.950	-.2031	.2566												

TABLE B-7.- PRESSURE COEFFICIENTS FOR WING WITH 76° SWEEP,

$C_{L,des} = 0.1$, M = 3.0

(a) $\alpha = -2.08°$

Cp at 2y/b of:																	
0.00			0.20			0.40			0.60			0.80			0.95		
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower
.029			.025	.0552	.0418	.036	.0605	-.0195	.064	.0674	-.0360	.104			.206		
.038			.037	.0577	.0519	.061	.0567	-.0220	.112	.0470	-.0285	.150	.0408	-.0489	.260	.0358	-.0893
.064	.0008	.1150	.061	.0681	.0602	.085	.0504	.0146	.161	.0216	-.0183	.200	.0333	-.0477	.350	.0181	-.0918
.087	.0008	.1049	.056	.0428	.0475	.110	.0466	.0121	.209	.0051	-.0120	.300	.0194	-.0489	.460	.0105	-.0931
.112	.0008	.1213	.110	.0288	.0412	.160	.0534	.0448	.259	.0013	-.0019	.400	-.0058	-.0477	.640	.0093	-.0918
.162	.0008	.0960	.160	.0187	.0399	.209	.0127	.0182	.307	-.0037	-.0006	.500	-.0058	-.0515	.830	-.0475	-.0931
.210	-.0020	.0784	.210	.0098	.0159	.259	.0038	.0106	.358	-.0100	.0005	.600	-.0311	-.0527			
.260	-.0020	.0431	.250	-.0028	.0020	.309	-.0075	.0018	.406	-.0164	-.0057	.680	-.0424	-.0540			
.310	-.0134	.0090	.300	-.0053	-.0005	.356	-.0164	-.0019	.500	-.0058	-.0010	.780	-.0526	-.0552			
.360	-.0185	.0039	.350	-.0078	-.0030	.406	-.0202	.0056	.600	-.0058	-.0237	.880	-.0576	-.0578			
.380	-.0122	.0077	.400	-.0053	.0020	.505	-.0291	-.0095	.700	-.0374	-.0325						
.460	-.0071	.0002	.450	-.0091	-.0068	.604	-.0202	-.0171	.800	-.0387	-.0388						
.510			.500	-.0053	-.0131	.703	-.0164	-.0209	.900	-.0412	-.0363						
.600			.600			.802	-.0202	-.0335	.950	-.0437	-.0325						
.700	-.0122	-.0250	.700	-.0053	-.0296	.902	-.0227	-.0335									
.800	-.0299	-.0351	.800	-.0066	-.0384	.952	-.0291	-.0373									
.900			.900	-.0104	-.0473												
.950	-.0261	-.0401	.950	-.0129	-.0486												

TABLE B-7.- Continued

(b) $\alpha = -0.08^{o}$

Cp at 2y/b of:																	
0.00			0.20			0.40			0.60			0.80			0.95		
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower
.029			.025	.0222	.0719	.036	.0349	.0280	.064	.0368	.0297	.104			.206		
.038			.037	.0260	.0769	.061	.0298	.0255	.112	.0178	.0448	.150	.0069	.0096	.260	.0043	-.0435
.064	-.0030	.1564	.061	.0475	.0810	.085	.0184	.0381	.161	-.0075	.0360	.200	-.0019	.0046	.350	-.0006	-.0295
.087	-.0030	.1475	.056	.0222	.0684	.110	.0134	.0356	.209	-.0241	.0322	.300	-.0171	-.0004	.460	.0005	-.0321
.112	-.0068	.1627	.110	.0096	.0608	.160	.0266	.0600	.259	-.0304	.0259	.400	-.0398	-.0105	.640	.0018	-.0321
.162	-.0005	.1286	.160	-.0005	.0583	.209	-.0126	.0347	.307	-.0368	.0195	.500	-.0487	-.0245	.830	-.0537	-.0371
.210	-.0030	.1085	.210	-.0093	.0318	.259	-.0241	.0259	.358	-.0393	.0170	.600	-.0601	-.0283			
.260	-.0093	.0694	.250	-.0207	.0166	.309	-.0329	.0145	.406	-.0444	.0107	.680	-.0702	-.0283			
.310	.0020	.0303	.300	-.0245	.0154	.356	-.0393	.0132	.500	-.0310	.0071	.780	-.0790	-.0295			
.360	.0045	.0227	.350	-.0220	.0128	.406	-.0418	.0208	.600	-.0310	-.0156	.880	-.0828	-.0295			
.380	-.0005	.0265	.400	-.0194	.0154	.505	-.0456	.0044	.700	-.0563	-.0270						
.460	-.0055	.0164	.450	-.0245	.0065	.604	-.0368	-.0031	.800	-.0563	-.0409						
.510			.500	-.0194	.0002	.703	-.0329	-.0069	.900	-.0575	-.0308						
.600			.600			.802	-.0368	-.0221	.950	-.0588	-.0270						
.700	-.0005	-.0125	.700	-.0207	-.0161	.902	-.0380	-.0221									
.800	.0184	-.0238	.800	-.0245	-.0287	.952	-.0444	-.0246									
.900			.900	-.0258	-.0363												
.950	.0222	-.0301	.950	-.0296	-.0388												

TABLE B-7.- Continued

(c) $\alpha = 2.92^{O}$

Cp at 2y/b of:																	
0.00			0.20			0.40			0.60			0.80			0.95		
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower
.029			.025	-.0345	.1246	.036	-.0371	.0531	.064	-.0265	.0624	.104			.206		
.038			.037	-.0333	.1221	.061	-.0383	.0518	.112	-.0328	.0750	.150	-.0474	.0620	.260	-.0209	.0196
.064	-.0168	.2241	.061	-.0092	.1174	.085	-.0257	.0632	.161	-.0544	.0637	.200	-.0512	.0570	.350	-.0765	.0221
.087	-.0117	.2128	.056	-.0206	.1035	.110	-.0295	.0619	.209	-.0684	.0573	.300	-.0563	.0545	.460	-.0866	.0158
.112	-.0155	.2342	.110	-.0257	.0959	.160	-.0138	.0826	.259	-.0748	.0523	.400	-.0854	.0370	.640	-.0196	.0146
.162	-.0117	.1889	.160	-.0320	.0934	.209	-.0506	.0586	.307	-.0786	.0485	.500	-.0929	.0246	.830	-.1081	.0046
.210	-.0142	.1586	.210	-.0371	.0632	.259	-.0570	.0497	.358	-.0811	.0447	.600	-.1031	.0183			
.260	-.0219	.1133	.250	-.0447	.0455	.309	-.0646	.0384	.406	-.0862	.0371	.680	-.1094	.0133			
.310	-.0117	.0692	.300	-.0434	.0430	.356	-.0684	.0371	.500	-.0639	.0470	.780	-.1132	.0083			
.360	-.0104	.0591	.350	-.0409	.0405	.406	-.0672	.0434	.600	-.0790	.0246	.880	-.1106	.0021			
.380	-.0168	.0591	.400	-.0383	.0430	.505	-.0646	.0257	.700	-.0790	.0146						
.460	-.0206	.0478	.450	-.0421	.0304	.604	-.0570	.0194	.800	-.0765	.0071						
.510	-.0231	.0390	.500	-.0396	.0241	.703	-.0557	.0144	.900	-.0790	.0083						
.600			.600			.802	-.0595	-.0020	.950	-.0803	.0108						
.700	-.0142	.0087	.700	-.0472	.0039	.902	-.0621	-.0032									
.800	.0034	-.0050	.800	-.0472	-.0061	.952	-.0672	-.0058									
.900			.900	-.0459	-.0187												
.950	.0237	-.0126	.950	-.0497	-.0187												

TABLE B-7.- Continued

(d) $\alpha = 3.92^{o}$

Cp at 2y/b of:																	
0.00			0.20			0.40			0.60			0.80			0.95		
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower
.029			.025	-.0534	.1396	.036	-.0861	.0641	.064	-.0837	.0686	.104			.206		
.038			.037	-.0534	.1371	.061	-.0861	.0628	.112	-.0710	.0825	.150	-.0980	.0709	.260	-.0246	.0259
.064	-.0229	.2492	.061	-.0326	.1321	.085	-.0619	.0729	.161	-.0698	.0699	.200	-.0954	.0634	.350	-.1081	.0309
.087	-.0166	.2379	.056	-.0454	.1208	.110	-.0645	.0729	.209	-.0786	.0648	.300	-.0967	.0621	.460	-.1157	.0234
.112	-.0216	.2618	.110	-.0492	.1119	.160	-.0240	.0901	.259	-.0850	.0610	.400	-.0992	.0459	.640	-.1106	.0234
.162	-.0166	.2102	.160	-.0492	.1082	.209	-.0621	.0674	.307	-.0888	.0547	.500	-.1030	.0334	.830	-.1119	.0110
.210	-.0204	.1850	.210	-.0517	.0767	.259	-.0685	.0585	.358	-.0901	.0522	.600	-.1119	.0272			
.260	-.0267	.1296	.250	-.0556	.0591	.309	-.0723	.0459	.406	-.0939	.0446	.680	-.1157	.0209			
.310	-.0178	.0817	.300	-.0556	.0553	.356	-.0748	.0459	.500	-.0689	.0534	.780	-.1157	.0160			
.360	-.0166	.0729	.350	-.0517	.0528	.406	-.0736	.0522	.600	-.0828	.0309	.880	-.1119	.0072			
.380	-.0229	.0729	.400	-.0517	.0553	.505	-.0710	.0333	.700	-.0828	.0209						
.460	-.0280	.0603	.450	-.0556	.0427	.604	-.0647	.0269	.800	-.0841	.0135						
.510			.500	-.0530	.0339	.703	-.0634	.0231	.900	-.0879	.0147						
.600			.600			.802	-.0685	.0067	.950	-.0891	.0185						
.700	-.0204	.0175	.700	-.0619	.0150	.902	-.0710	.0042									
.800	-.0026	.0037	.800	-.0594	.0037	.952	-.0761	.0004									
.900			.900	-.0568	-.0088												
.950	.0214	-.0051	.950	-.0594	-.0101												

TABLE B-7.- Continued

(e) $\alpha = 4.92^{o}$

Cp at 2y/b of:																	
0.00			0.20			0.40			0.60			0.80			0.95		
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower
.029			.025	-.0650	.1560	.036	-.1017	.0749	.064	-.1130	.0759	.104			.206		
.038			.037	-.0663	.1522	.061	-.1029	.0724	.112	-.1104	.0698	.150	-.1233	.0714	.260	-.1195	.0261
.064	-.0220	.2781	.061	-.0421	.1490	.085	-.0890	.0849	.161	-.1130	.0784	.200	-.1221	.0651	.350	-.1271	.0311
.087	-.0220	.2630	.056	-.0561	.1377	.110	-.0903	.0837	.209	-.1155	.0734	.300	-.1258	.0613	.460	-.1271	.0248
.112	-.0220	.2894	.110	-.0611	.1301	.160	-.0495	.0999	.259	-.1117	.0696	.400	-.1258	.0475	.640	-.1208	.0261
.162	-.0220	.2315	.160	-.0586	.1251	.209	-.0787	.0772	.307	-.1079	.0633	.500	-.1208	.0361	.830	-.1208	.0122
.210	-.0207	.2051	.210	-.0561	.0912	.259	-.0774	.0683	.358	-.1028	.0608	.600	-.1233	.0299			
.260	-.0220	.1484	.250	-.0573	.0724	.309	-.0799	.0545	.406	-.1041	.0545	.680	-.1233	.0236			
.310	-.0195	.0980	.300	-.0561	.0698	.356	-.0799	.0545	.500	-.0715	.0537	.780	-.1246	.0173			
.360	-.0207	.0867	.350	-.0548	.0661	.406	-.0799	.0633	.600	-.0779	.0336	.880	-.1258	.0085			
.380	-.0258	.0880	.400	-.0548	.0686	.505	-.0787	.0431	.700	-.0918	.0210						
.460	-.0309	.0741	.450	-.0586	.0560	.604	-.0736	.0355	.800	-.0943	.0135						
.510			.500	-.0586	.0472	.703	-.0723	.0317	.900	-.0961	.0173						
.600			.600			.802	-.0749	.0141	.950	-.0993	.0198						
.700	-.0245	.0275	.700	-.0662	.0246	.902	-.0799	.0116									
.800	-.0068	.0124	.800	-.0624	.0146	.952	-.0838	.0078									
.900			.900	-.0573	.0020												
.950	.0209	.0024	.950	-.0599	-.0004												

TABLE B-7.- Continued

(f) $\alpha = 5.92^{o}$

Cp at 2y/b of:																	
0.00			0.20			0.40			0.60			0.80			0.95		
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower
.029			.025	-.0776	.1724	.036	-.1193	.0817	.064	-.1256	.0838	.104			.206		
.038			.037	-.0776	.1661	.061	-.1193	.0792	.112	-.1256	.0989	.150	-.1296	.0883	.260	-.1258	.0409
.064	-.0232	.3059	.061	-.0583	.1610	.085	-.1142	.0918	.161	-.1256	.0876	.200	-.1283	.0821	.350	-.1271	.0459
.087	-.0206	.2870	.056	-.0723	.1497	.110	-.1167	.0918	.209	-.1256	.0825	.300	-.1309	.0759	.460	-.1258	.0397
.112	-.0244	.3159	.110	-.0761	.1434	.160	-.0685	.1103	.259	-.1206	.0787	.400	-.1283	.0634	.640	-.1233	.0409
.162	-.0219	.2542	.160	-.0761	.1384	.209	-.1002	.0876	.307	-.1193	.0737	.500	-.1258	.0522	.830	-.1246	.0284
.210	-.0244	.2253	.210	-.0697	.1031	.259	-.0977	.0787	.358	-.1142	.0699	.600	-.1271	.0459			
.260	-.0308	.1661	.250	-.0672	.0830	.309	-.0926	.0661	.406	-.1155	.0623	.680	-.1271	.0397			
.310	-.0232	.1132	.300	-.0659	.0805	.356	-.0913	.0648	.500	-.0854	.0696	.780	-.1283	.0334			
.360	-.0232	.1019	.350	-.0659	.0779	.406	-.0901	.0724	.600	-.1144	.0621	.880	-.1283	.0247			
.380	-.0295	.1031	.400	-.0659	.0792	.505	-.0888	.0509	.700	-.1170	.0384						
.460	-.0333	.0880	.450	-.0697	.0654	.604	-.0824	.0459	.800	-.1208	.0297						
.510			.500	-.0697	.0565	.703	-.0812	.0421	.900	-.1233	.0347						
.600			.600			.802	-.0812	.0244	.950	-.1233	.0372						
.700	-.0295	.0389	.700	-.0761	.0339	.902	-.0850	.0206									
.800	-.0118	.0225	.800	-.0697	.0225	.952	-.0888	.0168									
.900			.900	-.0536	.0087												
.950	.0249	.0112	.950	-.0646	.0074												

TABLE B-7.- Continued

(g) $\alpha = 9.93^{o}$

Cp at 2y/b of:																	
0.00			0.20			0.40			0.60			0.80			0.95		
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower
.029			.025	-.1092	.2522	.036	-.1371	.1252	.064	-.1307	.1198	.104			.206		
.038			.037	-.1118	.2459	.061	-.1345	.1226	.112	-.1320	.1388	.150	-.1321	.1249	.260	-.1296	.0761
.064	-.0459	.4299	.061	-.0926	.2312	.085	-.1371	.1403	.161	-.1320	.1274	.200	-.1309	.1211	.350	-.1309	.0824
.087	-.0395	.3946	.056	-.1091	.2186	.110	-.1371	.1391	.209	-.1320	.1248	.300	-.1347	.1161	.460	-.1309	.0774
.112	-.0408	.4312	.110	-.1117	.2148	.160	-.1002	.1565	.259	-.1332	.1211	.400	-.1321	.1099	.640	-.1296	.0811
.162	-.0332	.3543	.160	-.1129	.2085	.209	-.1307	.1362	.307	-.1320	.1173	.500	-.1309	.0986	.830	-.1309	.0686
.210	-.0345	.3240	.210	-.1041	.1681	.259	-.1320	.1274	.358	-.1282	.1122	.600	-.1321	.0899			
.260	-.0433	.2497	.250	-.0990	.1441	.309	-.1320	.1135	.406	-.1320	.1059	.680	-.1334	.0824			
.310	-.0383	.1866	.300	-.1002	.1416	.356	-.1332	.1109	.500	-.1043	.1136	.780	-.1347	.0724			
.360	-.0383	.1690	.350	-.1041	.1391	.406	-.1332	.1211	.600	-.1334	.1074	.880	-.1334	.0636			
.380	-.0446	.1652	.400	-.1079	.1391	.505	-.1320	.0983	.700	-.1372	.0799						
.460	-.0446	.1551	.450	-.1104	.1201	.604	-.1294	.0907	.800	-.1372	.0724						
.510			.500	-.1091	.1113	.703	-.1282	.0869	.900	-.1397	.0786						
.600			.600			.802	-.1282	.0666	.950	-.1384	.0824						
.700	-.0497	.0908	.700	-.1015	.0835	.902	-.1218	.0628									
.800	-.0319	.0706	.800	-.0837	.0709	.952	-.1180	.0577									
.900			.900	-.0799	.0532												
.950	.0237	.0555	.950	-.0837	.0532												

TABLE B-7.- Concluded

(h) $\alpha = 19.91^{o}$

Cp at 2y/b of:																	
0.00			0.20			0.40			0.60			0.80			0.95		
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower
.029			.025	-.1346	.4774	.036	-.1397	.2799	.064	-.1384	.2449	.104			.206		
.038			.037	-.1397	.4825	.061	-.1409	.2824	.112	-.1384	.2803	.150	-.1435	.2539	.260	-.1410	.2050
.064	-.0941	.7382	.061	-.1156	.4647	.085	-.1397	.3164	.161	-.1384	.2778	.200	-.1423	.2589	.350	-.1423	.2137
.087	-.0979	.7596	.056	-.1359	.4559	.110	-.1397	.3227	.209	-.1384	.2753	.300	-.1448	.2639	.460	-.1410	.2100
.112	-.0865	.7873	.110	-.1384	.4534	.160	-.1066	.3360	.259	-.1434	.2765	.400	-.1435	.2702	.640	-.1359	.2137
.162	-.0878	.6462	.160	-.1397	.4408	.209	-.1384	.3183	.307	-.1409	.2727	.500	-.1423	.2564	.830	-.1385	.1999
.210	-.0865	.6147	.210	-.1371	.3905	.259	-.1396	.3031	.358	-.1384	.2715	.600	-.1423	.2463			
.260	-.0865	.4976	.250	-.1384	.3654	.309	-.1422	.2841	.406	-.1447	.2677	.680	-.1423	.2388			
.310	-.0827	.4321	.300	-.1397	.3629	.356	-.1447	.2854	.500	-.1144	.2727	.780	-.1423	.2300			
.360	-.0903	.4258	.350	-.1384	.3579	.406	-.1422	.3006	.600	-.1397	.2714	.880	-.1397	.2225			
.380	-.0979	.4144	.400	-.1346	.3566	.505	-.1447	.2727	.700	-.1448	.2388						
.460	-.0979	.3842	.450	-.1359	.3264	.604	-.1447	.2639	.800	-.1448	.2325						
.510			.500	-.1333	.3214	.703	-.1434	.2601	.900	-.1448	.2413						
.600			.600			.802	-.1447	.2335	.950	-.1448	.2476						
.700	-.1143	.2960	.700	-.1333	.2761	.902	-.1422	.2272									
.800	-.0764	.2557	.800	-.1346	.2648	.952	-.1422	.2196									
.900			.900	-.1346	.2347												
.950	.0223	.2305	.950	-.1359	.2347												

TABLE B-8.- PRESSURE COEFFICIENTS FOR WING WITH 76° SWEEP,

$C_{L,des} = 0.1$, $M = 3.5$

(a) $\alpha = -2.30°$

Cp at 2y/b of:																	
0.00			0.20			0.40			0.60			0.80			0.95		
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower
.029			.025	.0493	.0291	.036	.0597	-.0193	.064	.0703	-.0309	.104			.206		
.038			.037	.0508	.0364	.061	.0567	-.0237	.112	.0540	-.0279	.150	.0444	-.0475	.260	.0473	-.0740
.064	-.0010	.1042	.061	.0656	.0543	.085	.0464	-.0090	.161	.0302	-.0250	.200	.0370	-.0490	.350	.0311	-.0740
.087	-.0024	.0924	.056	.0419	.0410	.110	.0449	-.0060	.209	.0154	-.0206	.300	.0311	-.0505	.460	.0178	-.0769
.112	-.0039	.1071	.110	.0286	.0410	.160	.0629	.0517	.259	.0080	-.0132	.400	.0015	-.0490	.640	-.0087	-.0769
.162	-.0039	.0909	.160	.0152	.0396	.209	.0184	.0177	.307	.0006	-.0102	.500	-.0102	-.0505	.830	-.0191	-.0798
.210	-.0039	.0732	.210	.0078	.0130	.259	.0065	.0104	.358	-.0038	-.0058	.600	-.0220	-.0519			
.260	-.0039	.0408	.250	-.0069	-.0001	.309	-.0038	.0000	.406	-.0127	-.0102	.680	-.0338	-.0519			
.310	-.0039	.0099	.300	-.0099	-.0031	.356	-.0157	-.0043	.500	.0030	.0067	.780	-.0427	-.0534			
.360	.0078	.0011	.350	-.0113	-.0090	.406	-.0186	.0015	.600	.0030	.0082	.880	-.0471	-.0549			
.380	.0049	.0026	.400	-.0084	-.0060	.505	-.0261	-.0102	.700	-.0353	-.0314						
.460	.0019	-.0017	.450	-.0113	-.0134	.604	-.0216	-.0161	.800	-.0383	-.0372						
.510			.500	-.0084	-.0178	.703	-.0172	-.0191	.900	-.0398	-.0372						
.600			.600			.802	-.0186	-.0324	.950	-.0398	-.0343						
.700	.0064	-.0268	.700	-.0084	-.0296	.902	-.0201	-.0339									
.800	.0345	-.0327	.800	-.0084	-.0311	.952	-.0246	-.0353									
.900			.900	-.0128	-.0458												
.950	.0864	-.0385	.950	-.0143	-.0488												

TABLE B-8.- Continued

(b) $\alpha = -0.30^{o}$

Cp at 2y/b of:																		
0.00			0.20			0.40			0.60			0.80			0.95			
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	
.029			.025	.0225	.0557	.036	.0362	.0243	.064	.0436	.0089	.104			.206			
.038			.037	.0240	.0646	.061	.0347	.0139	.112	.0258	.0163	.150	.0178	-.0229	.260	.0163	-.0630	
.064	-.0055	.1412	.061	.0392	.0801	.085	.0184	.0346	.161	.0050	.0310	.200	.0104	-.0229	.350	.0030	-.0616	
.087	-.0055	.1294	.056	.0169	.0655	.110	.0154	.0317	.209	-.0112	.0295	.300	.0030	-.0199	.460	-.0102	-.0601	
.112	-.0085	.1471	.110	.0065	.0596	.160	.0377	.0650	.259	-.0186	.0222	.400	-.0235	-.0199	.640	-.0324	-.0586	
.162	-.0070	.1250	.160	-.0053	.0552	.209	-.0067	.0310	.307	-.0246	.0177	.500	-.0338	-.0303	.830	-.0442	-.0511	
.210	-.0070	.1014	.210	-.0127	.0331	.259	-.0157	.0251	.358	-.0275	.0148	.600	-.0442	-.0348				
.260	-.0114	.0646	.250	-.0231	.0199	.309	-.0260	.0148	.406	-.0349	.0089	.680	-.0530	-.0378				
.310	-.0040	.0292	.300	-.0260	.0155	.356	-.0364	.0089	.500	-.0176	.0052	.780	-.0619	-.0422				
.360	.0003	.0174	.350	-.0260	.0111	.406	-.0394	.0148	.600	-.0383	.0052	.880	-.0663	-.0452				
.380	-.0040	.0204	.400	-.0246	.0126	.505	-.0409	.0000	.700	-.0530	-.0348							
.460	-.0070	.0130	.450	-.0260	.0052	.604	-.0349	-.0043	.800	-.0530	-.0422							
.510			.500	-.0246	-.0005	.703	-.0305	-.0073	.900	-.0530	-.0407							
.600			.600			.802	-.0320	-.0220	.950	-.0516	-.0378							
.700	-.0025	-.0164	.700	-.0246	-.0152	.902	-.0335	-.0235										
.800	.0270	-.0252	.800	-.0260	-.0255	.952	-.0379	-.0265										
.900	-.0159	-.0340	.900	-.0290	-.0343													
.950	.0788	-.0311	.950	-.0305	-.0358													

TABLE B-8.- Continued

(c) $\alpha = 2.70^{o}$

Cp at 2y/b of:																	
0.00			0.20			0.40			0.60			0.80			0.95		
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower
.029			.025	-.0115	.1145	.036	-.0057	.0537	.064	-.0083	.0574	.104			.206		
.038			.037	-.0100	.1145	.061	-.0086	.0508	.112	-.0186	.0663	.150	-.0280	.0371	.260	-.0398	.0016
.064	-.0174	.2087	.061	.0090	.1198	.085	-.0205	.0611	.161	-.0379	.0574	.200	-.0339	.0327	.350	-.0472	.0076
.087	-.0144	.1999	.056	-.0160	.1037	.110	-.0234	.0581	.209	-.0498	.0515	.300	-.0413	.0238	.460	-.0546	-.0012
.112	-.0189	.2190	.110	-.0249	.0949	.160	.0005	.0870	.259	-.0543	.0456	.400	-.0605	.0164	.640	-.0694	-.0042
.162	-.0144	.1866	.160	-.0338	.0905	.209	-.0409	.0545	.307	-.0617	.0397	.500	-.0694	.0046	.830	-.0797	-.0116
.210	-.0159	.1601	.210	-.0382	.0640	.259	-.0498	.0471	.358	-.0617	.0368	.600	-.0767	-.0012			
.260	-.0218	.1115	.250	-.0426	.0464	.309	-.0572	.0353	.406	-.0691	.0294	.680	-.0826	-.0057			
.310	-.0159	.0659	.300	-.0426	.0420	.356	-.0632	.0309	.500	-.0413	.0357	.780	-.0871	-.0101			
.360	-.0129	.0512	.350	-.0412	.0376	.406	-.0617	.0368	.600	-.0472	.0327	.880	-.0900	-.0145			
.380	-.0174	.0512	.400	-.0367	-.0005	.505	-.0587	.0206	.700	-.0723	-.0057						
.460	-.0218	.0438	.450	-.0397	.0126	.604	-.0543	.0147	.800	-.0694	-.0131						
.510			.500	-.0367	.0214	.703	-.0498	.0102	.900	-.0694	-.0116						
.600			.600			.802	-.0528	-.0030	.950	-.0694	-.0101						
.700	-.0144	.0026	.700	-.0426	.0038	.902	-.0543	-.0044									
.800	.0151	-.0076	.800	-.0426	-.0049	.952	-.0572	-.0089									
.900	-.0263	-.0223	.900	-.0426	-.0152												
.950	.0713	-.0150	.950	-.0456	-.0196												

TABLE B-8.- Continued

(d) $\alpha = 3.70^{o}$

Cp at 2y/b of:																	
0.00			0.20			0.40			0.60			0.80			0.95		
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower
.029			.025	-.0247	.1353	.036	-.0307	.0640	.064	-.0364	.0652	.104			.206		
.038			.037	-.0232	.1294	.061	-.0337	.0596	.112	-.0378	.0740	.150	-.0531	.0419	.260	-.0649	.0093
.064	-.0217	.2311	.061	-.0055	.1345	.085	-.0307	.0684	.161	-.0497	.0652	.200	-.0531	.0359	.350	-.0678	.0093
.087	-.0173	.2237	.056	-.0277	.1168	.110	-.0337	.0684	.209	-.0616	.0593	.300	-.0575	.0285	.460	-.0723	.0033
.112	-.0217	.2443	.110	-.0366	.1080	.160	-.0126	.0933	.259	-.0705	.0519	.400	-.0693	.0211	.640	-.0826	.0004
.162	-.0188	.2075	.160	-.0440	.1021	.209	-.0557	.0622	.307	-.0720	.0460	.500	-.0767	.0093	.830	-.0826	-.0084
.210	-.0202	.1780	.210	-.0470	.0757	.259	-.0631	.0533	.358	-.0720	.0445	.600	-.0826	.0033			
.260	-.0262	.1279	.250	-.0514	.0566	.309	-.0676	.0415	.406	-.0794	.0371	.680	-.0855	-.0025			
.310	-.0202	.0778	.300	-.0500	.0507	.356	-.0705	.0386	.500	-.0442	.0359	.780	-.0826	-.0069			
.360	-.0173	.0631	.350	-.0470	.0463	.406	-.0705	.0445	.600	-.0457	.0359	.880	-.0796	-.0114			
.380	-.0217	.0616	.400	-.0440	.0493	.505	-.0676	.0282	.700	-.0752	-.0025						
.460	-.0262	.0528	.450	-.0470	.0390	.604	-.0616	.0193	.800	-.0767	-.0114						
.510		.0439	.500	-.0455	.0317	.703	-.0586	.0179	.900	-.0796	-.0084						
.600		.0027	.600			.802	-.0616	.0016	.950	-.0796	-.0069						
.700	-.0188	.0100	.700	-.0514	.0096	.902	-.0646	.0001									
.800	.0108	-.0002	.800	-.0500	.0008	.952	-.0676	-.0042									
.900	-.0321	-.0178	.900	-.0500	-.0094												
.950	.0775	-.0090	.950	-.0514	-.0123												

TABLE B-8.- Continued

(e) $\alpha = 4.70^{o}$

Cp at 2y/b of:																	
0.00			0.20			0.40			0.60			0.80			0.95		
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower
.029			.025	-.0337	.1541	.036	-.0544	.0690	.064	-.0617	.0736	.104			.206		
.038			.037	-.0337	.1482	.061	-.0574	.0645	.112	-.0602	.0839	.150	-.0767	.0493	.260	-.0826	.0167
.064	-.0248	.2557	.061	-.0145	.1441	.085	-.0455	.0749	.161	-.0661	.0736	.200	-.0782	.0448	.350	-.0856	.0181
.087	-.0204	.2498	.056	-.0367	.1279	.110	-.0485	.0734	.209	-.0721	.0677	.300	-.0811	.0359	.460	-.0870	.0122
.112	-.0248	.2719	.110	-.0441	.1191	.160	-.0172	.1031	.259	-.0750	.0618	.400	-.0856	.0285	.640	-.0870	.0093
.162	-.0204	.2321	.160	-.0529	.1132	.209	-.0617	.0721	.307	-.0795	.0559	.500	-.0870	.0196	.830	-.0826	-.0010
.210	-.0219	.2012	.210	-.0559	.0837	.259	-.0706	.0633	.358	-.0780	.0529	.600	-.0870	.0122			
.260	-.0278	.1468	.250	-.0574	.0645	.309	-.0736	.0515	.406	-.0825	.0470	.680	-.0870	.0078			
.310	-.0219	.0953	.300	-.0544	.0572	.356	-.0736	.0485	.500	-.0472	.0433	.780	-.0841	.0033			
.360	-.0204	.0776	.350	-.0515	.0542	.406	-.0736	.0544	.600	-.0472	.0419	.880	-.0841	-.0040			
.380	-.0204	.0761	.400	-.0515	.0557	.505	-.0721	.0382	.700	-.0782	.0048						
.460	-.0204	.0643	.450	-.0544	.0439	.604	-.0691	.0294	.800	-.0811	-.0040						
.510		.0555	.500	-.0529	.0351	.703	-.0676	.0264	.900	-.0841	-.0025						
.600		.0099	.600			.802	-.0691	.0117	.950	-.0841	.0004						
.700	-.0219	.0202	.700	-.0589	.0145	.902	-.0721	.0087									
.800	.0076	.0084	.800	-.0574	.0056	.952	-.0750	.0043									
.900	-.0337	-.0121	.900	-.0529	-.0061												
.950	.0727	-.0018	.950	-.0574	-.0090												

TABLE B-8.- Continued

(f) $\alpha = 5.70^{o}$

Cp at 2y/b of:																	
0.00			0.20			0.40			0.60			0.80			0.95		
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower
.029			.025	-.0468	.1717	.036	-.0707	.0827	.064	-.0810	.0779	.104			.206		
.038			.037	-.0483	.1643	.061	-.0722	.0798	.112	-.0795	.0912	.150	-.0914	.0762	.260	-.0929	.0412
.064	-.0319	.2820	.061	-.0205	.1649	.085	-.0634	.0901	.161	-.0839	.0824	.200	-.0914	.0704	.350	-.0944	.0426
.087	-.0260	.2761	.056	-.0441	.1487	.110	-.0663	.0886	.209	-.0869	.0765	.300	-.0944	.0645	.460	-.0929	.0382
.112	-.0305	.2997	.110	-.0501	.1399	.160	-.0261	.1133	.259	-.0884	.0706	.400	-.0929	.0543	.640	-.0900	.0368
.162	-.0275	.2555	.160	-.0574	.1341	.209	-.0661	.0824	.307	-.0899	.0662	.500	-.0914	.0455	.830	-.0885	.0236
.210	-.0305	.2232	.210	-.0634	.1018	.259	-.0765	.0735	.358	-.0810	.0632	.600	-.0914	.0397			
.260	-.0349	.1643	.250	-.0634	.0813	.309	-.0780	.0617	.406	-.0854	.0558	.680	-.0914	.0339			
.310	-.0275	.1114	.300	-.0589	.0754	.356	-.0780	.0588	.500	-.0515	.0675	.780	-.0914	.0280			
.360	-.0245	.0922	.350	-.0574	.0695	.406	-.0765	.0647	.600	-.0515	.0675	.880	-.0900	.0222			
.380	-.0305	.0908	.400	-.0574	.0725	.505	-.0765	.0470	.700	-.0655	.0309						
.460	-.0319	.0790	.450	-.0589	.0607	.604	-.0765	.0396	.800	-.0900	.0236						
.510	-.0334	.0672	.500	-.0604	.0519	.703	-.0750	.0352	.900	-.0929	.0251						
.600			.600			.802	-.0765	.0190	.950	-.0929	.0266						
.700			.700	-.0648	.0300	.902	-.0780	.0160									
.800	-.0008	.0172	.800	-.0634	.0197	.952	-.0810	.0131									
.900	-.0409	-.0062	.900	-.0560	.0080												
.950	.0704	.0069	.950	-.0589	.0050												

TABLE B-8.- Continued

(g) $\alpha = 9.70^{o}$

Cp at 2y/b of:																	
0.00			0.20			0.40			0.60			0.80			0.95		
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower
.029			.025	-.0722	.2500	.036	-.1003	.1192	.064	-.0988	.1121	.104			.206		
.038			.037	-.0737	.2411	.061	-.1003	.1162	.112	-.0988	.1268	.150	-.1018	.1122	.260	-.0988	.0743
.064	-.0396	.4060	.061	-.0528	.2297	.085	-.0988	.1295	.161	-.0988	.1180	.200	-.1003	.1108	.350	-.0988	.0758
.087	-.0322	.3328	.056	-.0765	.2106	.110	-.1003	.1295	.209	-.0973	.1135	.300	-.1018	.1035	.460	-.0988	.0714
.112	-.0367	.4222	.110	-.0810	.2032	.160	-.0543	.1549	.259	-.0988	.1106	.400	-.1018	.0976	.640	-.0959	.0729
.162	-.0381	.3516	.160	-.0810	.1958	.209	-.0914	.1268	.307	-.0988	.1047	.500	-.1003	.0860	.830	-.0974	.0627
.210	-.0381	.3192	.210	-.0810	.1575	.259	-.0958	.1180	.358	-.0928	.1017	.600	-.1003	.0801			
.260	-.0455	.2470	.250	-.0795	.1324	.309	-.0958	.1032	.406	-.0988	.0944	.680	-.1018	.0743			
.310	-.0426	.1808	.300	-.0780	.1266	.356	-.0988	.1017	.500	-.0648	.1049	.780	-.1018	.0685			
.360	-.0337	.1601	.350	-.0810	.1207	.406	-.0988	.1076	.600	-.0663	.1049	.880	-.0988	.0612			
.380	-.0381	.1557	.400	-.0839	.1221	.505	-.0988	.0870	.700	-.0988	.0714						
.460	-.0411	.1395	.450	-.0854	.1059	.604	-.0988	.0781	.800	-.1018	.0641						
.510	-.0396	.1248	.500	-.0884	.0971	.703	-.0958	.0752	.900	-.1033	.0656						
.600			.600			.802	-.0973	.0575	.950	-.1033	.0699						
.700			.700	-.0914	.0691	.902	-.0988	.0530									
.800	-.0086	.0586	.800	-.0899	.0573	.952	-.1003	.0471									
.900	-.0485	.0262	.900	-.0825	.0411												
.950	.0609	.0438	.950	-.0869	.0396												

TABLE B-8.- Concluded

(h) $\alpha = 19.70^{o}$

Cp at 2y/b of:																	
0.00			0.20			0.40			0.60			0.80			0.95		
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower
.029			.025	-.0943	.4859	.036	-.1032	.2733	.064	-.1047	.2347	.104			.206		
.038			.037	-.1002	.4829	.061	-.1092	.2748	.112	-.1047	.2657	.150	-.1048	.2363	.260	-.1018	.1882
.064	-.0601	.8218	.061	-.0677	.4587	.085	-.1018	.3027	.161	-.1017	.2584	.200	-.1048	.2465	.350	-.1018	.1955
.087	-.0646	.7849	.056	-.0944	.4455	.110	-.1032	.3042	.209	-.1017	.2584	.300	-.1062	.2465	.460	-.1033	.1926
.112	-.0691	.7967	.110	-.0958	.4425	.160	-.0587	.3248	.259	-.1047	.2584	.400	-.1048	.2509	.640	-.0988	.1969
.162	-.0705	.6450	.160	-.0973	.4278	.209	-.0988	.3026	.307	-.1032	.2539	.500	-.1048	.2480	.830	-.1003	.1838
.210	-.0735	.6126	.210	-.0973	.3763	.259	-.1003	.2894	.358	-.0988	.2510	.600	-.1048	.2261			
.260	-.0735	.4977	.250	-.0973	.3483	.309	-.1017	.2687	.406	-.1047	.2451	.680	-.1048	.2188			
.310	-.0735	.4196	.300	-.0988	.3454	.356	-.1047	.2657	.500	-.0708	.2567	.780	-.1048	.2101			
.360	-.0750	.4048	.350	-.0988	.3395	.406	-.1032	.2730	.600	-.0841	.2392	.880	-.1018	.2028			
.380	-.0794	.3960	.400	-.0988	.3366	.505	-.1062	.2524	.700	-.1048	.2174						
.460	-.0780	.3665	.450	-.0988	.3057	.604	-.1047	.2421	.800	-.1048	.2130						
.510	-.0794	.3459	.500	-.0988	.2954	.703	-.1047	.2333	.900	-.1062	.2217						
.600		.2325	.600			.802	-.1062	.2067	.950	-.1062	.2261						
.700		.2693	.700	-.0988	.2512	.902	-.1047	.2052									
.800	-.0408	.2340	.800	-.0988	.2365	.952	-.1047	.1949									
.900	-.0616	.1765	.900	-.0988	.2071												
.950	.0585	.2045	.950	-.0988	.2071												

TABLE B-9.- PRESSURE COEFFICIENTS FOR WING WITH 76° SWEEP,

$C_{L,des} = 0.1$, M = 4.0

(a) $\alpha = -1.85°$

Cp at 2y/b of:																	
0.00			0.20			0.40			0.60			0.80			0.95		
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower
.029			.025	.0401	.0326	.036	.0582	-.0070	.064	.0670	-.0166	.104			.206		
.038			.037	.0418	.0359	.061	.0516	-.0135	.112	.0521	-.0149	.150	.0359	-.0266	.260	.0359	-.0513
.064	-.0062	.1067	.061	.0599	.0555	.085	.0433	-.0037	.161	.0304	-.0116	.200	.0292	-.0266	.350	.0208	-.0497
.087	-.0062	.0968	.056	.0350	.0390	.110	.0383	-.0070	.209	.0171	-.0050	.300	.0275	-.0299	.460	.0091	-.0513
.112	-.0079	.1116	.110	.0251	.0390	.160	.0670	.0625	.259	.0088	-.0017	.400	-.0058	-.0266	.640	-.0125	-.0513
.162	-.0096	.0984	.160	.0118	.0341	.209	.0155	.0246	.307	.0022	-.0017	.500	-.0158	-.0282	.830	-.0141	-.0563
.210	-.0096	.0803	.210	.0019	.0176	.259	.0038	.0180	.358	-.0011	.0031	.600	-.0275	-.0299			
.260	-.0112	.0474	.250	-.0080	.0061	.309	-.0061	.0064	.406	-.0094	-.0017	.680	-.0375	-.0299			
.310	-.0029	.0177	.300	-.0146	.0012	.356	-.0160	.0031	.500	.0041	.0294	.780	-.0475	-.0315			
.360	.0020	.0046	.350	-.0146	-.0004	.406	-.0210	.0064	.600	.0041	.0261	.880	-.0525	-.0315			
.380	-.0013	.0046	.400	-.0130	-.0004	.505	-.0277	-.0050	.700	-.0458	-.0167						
.460	-.0029	.0013	.450	-.0146	-.0070	.604	-.0227	-.0116	.800	-.0508	-.0233						
.510			.500	-.0113	-.0119	.703	-.0194	-.0133	.900	-.0508	-.0216						
.600			.600			.802	-.0194	-.0232	.950	-.0508	-.0216						
.700	.0020	-.0217	.700	-.0096	-.0201	.902	-.0210	-.0282									
.800	.0401	-.0266	.800	-.0096	-.0316	.952	-.0244	-.0298									
.900			.900	-.0146	-.0382												
.950	.0186	-.0349	.950	-.0179	-.0432												

TABLE B-9.- Continued

(b) $\alpha = 0.16^{o}$

Cp at 2y/b of:																		
0.00			0.20			0.40			0.60			0.80			0.95		
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower
.029			.025	.0233	.0575	.036	.0399	.0289	.064	.0438	.0165	.104			.206		
.038			.037	.0250	.0624	.061	.0333	.0224	.112	.0288	.0214	.150	.0249	.0035	.260	.0216	-.0312
.064	-.0064	.1466	.061	.0416	.0864	.085	.0217	.0371	.161	.0072	.0281	.200	.0166	.0018	.350	.0116	-.0312
.087	-.0080	.1334	.056	.0134	.0700	.110	.0184	.0322	.209	-.0060	.0314	.300	.0116	.0001	.460	.0000	-.0296
.112	-.0097	.1515	.110	.0068	.0634	.160	.0455	.0743	.259	-.0127	.0297	.400	-.0148	.0035	.640	-.0197	-.0263
.162	-.0097	.1334	.160	-.0047	.0601	.209	-.0043	.0347	.307	-.0193	.0214	.500	-.0230	-.0047	.830	-.0247	-.0296
.210	-.0114	.1119	.210	-.0130	.0388	.259	-.0143	.0264	.358	-.0193	.0181	.600	-.0330	-.0097			
.260	-.0130	.0740	.250	-.0230	.0256	.309	-.0227	.0165	.406	-.0293	.0132	.680	-.0412	-.0130			
.310	-.0064	.0393	.300	-.0246	.0207	.356	-.0326	.0115	.500	.0034	.0333	.780	-.0479	-.0163			
.360	-.0047	.0245	.350	-.0246	.0158	.406	-.0360	.0165	.600	.0017	.0333	.880	-.0528	-.0213			
.380	-.0064	.0228	.400	-.0213	.0158	.505	-.0393	.0049	.700	-.0445	-.0114						
.460	-.0097	.0179	.450	-.0230	.0092	.604	-.0343	-.0016	.800	-.0479	-.0180						
.510			.500	-.0213	.0043	.703	-.0310	-.0049	.900	-.0479	-.0196						
.600			.600			.802	-.0326	-.0165	.950	-.0479	-.0163						
.700	-.0047	-.0100	.700	-.0213	-.0071	.902	-.0326	-.0181									
.800	.0366	-.0183	.800	-.0213	-.0186	.952	-.0360	-.0214									
.900			.900	-.0246	-.0252												
.950	.0134	-.0265	.950	-.0296	-.0301												

TABLE B-9.- Continued

(c) $\alpha = 3.16^{o}$

Cp at 2y/b of:																	
0.00			0.20			0.40			0.60			0.80			0.95		
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower
.029			.025	-.0064	.1040	.036	.0034	.0587	.064	.0022	.0580	.104			.206		
.038			.037	-.0048	.1122	.061	-.0031	.0521	.112	-.0094	.0680	.150	-.0453	.0544	.260	-.0554	.0230
.064	-.0147	.2097	.061	.0200	.1278	.085	-.0081	.0636	.161	-.0243	.0537	.200	-.0504	.0511	.350	-.0605	.0247
.087	-.0147	.1981	.056	-.0081	.1080	.110	-.0130	.0603	.209	-.0360	.0547	.300	-.0554	.0445	.460	-.0673	.0181
.112	-.0164	.2196	.110	-.0164	.0998	.160	.0205	.0978	.259	-.0410	.0498	.400	-.0740	.0346	.640	-.0774	.0147
.162	-.0164	.1965	.160	-.0263	.0932	.209	-.0293	.0597	.307	-.0460	.0431	.500	-.0791	.0247	.830	-.0808	.0081
.210	-.0180	.1667	.210	-.0329	.0702	.259	-.0393	.0498	.358	-.0443	.0398	.600	-.0842	.0181			
.260	-.0213	.1188	.250	-.0379	.0521	.309	-.0460	.0365	.406	-.0526	.0332	.680	-.0875	.0147			
.310	-.0180	.0742	.300	-.0395	.0455	.356	-.0526	.0349	.500	-.0436	.0594	.780	-.0909	.0098			
.360	-.0147	.0561	.350	-.0379	.0406	.406	-.0526	.0365	.600	-.0740	.0577	.880	-.0926	.0048			
.380	-.0164	.0527	.400	-.0362	.0406	.505	-.0526	.0249	.700	-.0892	.0147						
.460	-.0180	.0461	.450	-.0362	.0324	.604	-.0493	.0183	.800	-.0892	.0065						
.510			.500	-.0362	.0242	.703	-.0460	.0150	.900	-.0892	.0065						
.600			.600			.802	-.0476	.0017	.950	-.0892	.0081						
.700	-.0130	.0081	.700	-.0395	.0110	.902	-.0510	-.0015									
.800	.0283	-.0017	.800	-.0395	-.0004	.952	-.0526	-.0048									
.900	-.0213	-.0182	.900	-.0395	-.0103												
.950	-.0048	-.0116	.950	-.0462	-.0136												

TABLE B-9.- Continued

(d) $\alpha = 4.16^{o}$

Cp at 2y/b of:

0.00			0.20			0.40			0.60			0.80			0.95		
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower
.029			.025	-.0131	.1251	.036	-.0131	.0641	.064	-.0160	.0661	.104			.206		
.038			.037	-.0131	.1301	.061	-.0197	.0592	.112	-.0210	.0760	.150	-.0458	.0626	.260	-.0558	.0296
.064	-.0197	.2324	.061	.0100	.1383	.085	-.0180	.0691	.161	-.0343	.0661	.200	-.0475	.0577	.350	-.0592	.0296
.087	-.0180	.2208	.056	-.0164	.1185	.110	-.0230	.0658	.209	-.0427	.0611	.300	-.0508	.0511	.460	-.0642	.0246
.112	-.0197	.2439	.110	-.0246	.1103	.160	.0121	.1041	.259	-.0493	.0562	.400	-.0642	.0411	.640	-.0692	.0213
.162	-.0180	.2175	.160	-.0329	.1037	.209	-.0377	.0677	.307	-.0526	.0496	.500	-.0692	.0312	.830	-.0692	.0131
.210	-.0213	.1878	.210	-.0396	.0773	.259	-.0476	.0562	.358	-.0493	.0479	.600	-.0725	.0246			
.260	-.0246	.1367	.250	-.0429	.0592	.309	-.0526	.0446	.406	-.0576	.0413	.680	-.0759	.0197			
.310	-.0197	.0888	.300	-.0429	.0526	.356	-.0576	.0413	.500	-.0341	.0643	.780	-.0759	.0147			
.360	-.0164	.0674	.350	-.0429	.0460	.406	-.0576	.0446	.600	-.0658	.0610	.880	-.0759	.0098			
.380	-.0197	.0658	.400	-.0412	.0476	.505	-.0576	.0314	.700	-.0742	.0180						
.460	-.0213	.0559	.450	-.0429	.0361	.604	-.0576	.0264	.800	-.0742	.0114						
.510			.500	-.0429	.0295	.703	-.0576	.0214	.900	-.0759	.0114						
.600			.600			.802	-.0576	.0082	.950	-.0759	.0131						
.700	-.0147	.0146	.700	-.0462	.0130	.902	-.0576	.0049									
.800	.0249	.0047	.800	-.0462	.0014	.952	-.0593	.0016									
.900			.900	-.0462	-.0100												
.950	-.0097	-.0067	.950	-.0495	-.0117												

TABLE B-9.- Continued

(e) $\alpha = 5.15^{o}$

Cp at 2y/b of:																	
0.00			0.20			0.40			0.60			0.80			0.95		
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower
.029			.025	-.0213	.1499	.036	-.0345	.0767	.064	-.0377	.0727	.104			.206		
.038			.037	-.0213	.1515	.061	-.0411	.0735	.112	-.0393	.0843	.150	-.0593	.0605	.260	-.0643	.0255
.064	-.0213	.2555	.061	-.0013	.1590	.085	-.0328	.0833	.161	-.0460	.0744	.200	-.0593	.0555	.350	-.0676	.0272
.087	-.0197	.2456	.056	-.0278	.1376	.110	-.0378	.0800	.209	-.0493	.0677	.300	-.0626	.0488	.460	-.0693	.0222
.112	-.0213	.2720	.110	-.0361	.1277	.160	.0055	.1124	.259	-.0543	.0628	.400	-.0676	.0405	.640	-.0693	.0189
.162	-.0213	.2390	.160	-.0428	.1228	.209	-.0410	.0760	.307	-.0576	.0578	.500	-.0709	.0288	.830	-.0709	.0105
.210	-.0230	.2093	.210	-.0461	.0948	.259	-.0526	.0677	.358	-.0543	.0545	.600	-.0726	.0222			
.260	-.0280	.1548	.250	-.0494	.0751	.309	-.0576	.0545	.406	-.0626	.0496	.680	-.0726	.0172			
.310	-.0230	.1037	.300	-.0494	.0669	.356	-.0610	.0496	.500	-.0293	.0605	.780	-.0726	.0122			
.360	-.0180	.0822	.350	-.0494	.0619	.406	-.0593	.0545	.600	-.0593	.0488	.880	-.0709	.0072			
.380	-.0230	.0789	.400	-.0494	.0619	.505	-.0610	.0413	.700	-.0709	.0172						
.460	-.0230	.0690	.450	-.0494	.0521	.604	-.0610	.0330	.800	-.0726	.0072						
.510			.500	-.0511	.0422	.703	-.0610	.0297	.900	-.0742	.0072						
.600			.600			.802	-.0626	.0148	.950	-.0742	.0105						
.700	-.0180	.0245	.700	-.0560	.0258	.902	-.0626	.0115									
.800	.0216	.0130	.800	-.0560	.0143	.952	-.0659	.0082									
.900			.900	-.0527	.0027												
.950	-.0131	-.0001	.950	-.0577	.0011												

TABLE B-9.- Continued

(f) $\alpha = 6.16^{o}$

Cp at 2y/b of:																		
0.00			0.20			0.40			0.60			0.80			0.95			
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower
.029			.025	-.0280	.1764	.036	-.0462	.0838	.064	-.0526	.0810	.104			.206		
.038			.037	-.0296	.1681	.061	-.0495	.0805	.112	-.0526	.0909	.150	-.0892	.0808	.260	-.0909	.0445
.064	-.0247	.2820	.061	-.0048	.1711	.085	-.0412	.0903	.161	-.0560	.0827	.200	-.0892	.0759	.350	-.0943	.0445
.087	-.0213	.2737	.056	-.0313	.1513	.110	-.0462	.0870	.209	-.0593	.0777	.300	-.0892	.0676	.460	-.0943	.0395
.112	-.0230	.3001	.110	-.0379	.1414	.160	.0005	.1240	.259	-.0626	.0711	.400	-.0926	.0594	.640	-.0926	.0379
.162	-.0230	.2605	.160	-.0429	.1349	.209	-.0477	.0843	.307	-.0626	.0661	.500	-.0943	.0494	.830	-.0926	.0280
.210	-.0263	.2308	.210	-.0462	.1052	.259	-.0560	.0761	.358	-.0576	.0645	.600	-.0943	.0412			
.260	-.0296	.1731	.250	-.0495	.0838	.309	-.0610	.0628	.406	-.0659	.0579	.680	-.0943	.0379			
.310	-.0247	.1169	.300	-.0495	.0772	.356	-.0626	.0595	.500	-.0521	.0792	.780	-.0943	.0313			
.360	-.0213	.0971	.350	-.0511	.0706	.406	-.0626	.0645	.600	-.0825	.0775	.880	-.0926	.0247			
.380	-.0247	.0938	.400	-.0511	.0706	.505	-.0626	.0479	.700	-.0909	.0346						
.460	-.0247	.0823	.450	-.0528	.0590	.604	-.0626	.0413	.800	-.0926	.0263						
.510			.500	-.0528	.0491	.703	-.0626	.0380	.900	-.0943	.0280						
.600			.600			.802	-.0659	.0231	.950	-.0943	.0296						
.700	-.0213	.0344	.700	-.0578	.0310	.902	-.0659	.0198									
.800	.0183	.0229	.800	-.0594	.0195	.952	-.0693	.0149									
.900	-.0280	-.0018	.900	-.0545	.0079												
.950	-.0164	.0080	.950	-.0578	.0046												

TABLE B-9.- Continued

(g) $\alpha = 10.16^{o}$

Cp at 2y/b of:																	
0.00			0.20			0.40			0.60			0.80			0.95		
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower
.029			.025	-.0495	.2571	.036	-.0726	.1296	.064	-.0709	.1140	.104			.206		
.038			.037	-.0495	.2456	.061	-.0742	.1247	.112	-.0709	.1273	.150	-.0760	.1171	.260	-.0760	.0775
.064	-.0329	.3390	.061	-.0276	.2448	.085	-.0726	.1395	.161	-.0693	.1206	.200	-.0760	.1155	.350	-.0760	.0791
.087	-.0280	.3940	.056	-.0559	.2201	.110	-.0726	.1362	.209	-.0693	.1157	.300	-.0776	.1105	.460	-.0760	.0742
.112	-.0362	.4221	.110	-.0609	.2119	.160	-.0177	.1669	.259	-.0726	.1107	.400	-.0776	.1022	.640	-.0726	.0742
.162	-.0362	.3676	.160	-.0626	.2037	.209	-.0610	.1322	.307	-.0693	.1074	.500	-.0776	.0907	.830	-.0743	.0659
.210	-.0379	.3264	.210	-.0626	.1658	.259	-.0643	.1223	.358	-.0643	.1041	.600	-.0760	.0841			
.260	-.0412	.2538	.250	-.0643	.1428	.309	-.0693	.1074	.406	-.0726	.0958	.680	-.0760	.0775			
.310	-.0412	.1878	.300	-.0676	.1345	.356	-.0709	.1041	.500	-.0361	.1171	.780	-.0760	.0632			
.360	-.0379	.1647	.350	-.0693	.1279	.406	-.0693	.1091	.600	-.0361	.1155	.880	-.0760	.0626			
.380	-.0396	.1614	.400	-.0659	.1279	.505	-.0726	.0892	.700	-.0743	.0742						
.460	-.0379	.1433	.450	-.0726	.1131	.604	-.0726	.0810	.800	-.0760	.0659						
.510			.500	-.0709	.1000	.703	-.0726	.0777	.900	-.0776	.0676						
.600			.600			.802	-.0743	.0611	.950	-.0793	.0692						
.700	-.0313	.0789	.700	-.0759	.0753	.902	-.0743	.0562									
.800	.0117	.0641	.800	-.0759	.0637	.952	-.0759	.0512									
.900	-.0379	.0294	.900	-.0709	.0489												
.950	-.0280	.0459	.950	-.0726	.0456												

TABLE B-9.- Concluded

(h) α = 20.17°

Cp at 2y/b of:																	
0.00			0.20			0.40			0.60			0.80			0.95		
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower
.029			.025	-.0677	.5029	.036	-.0776	.2806	.064	-.0776	.2414	.104			.206		
.038			.037	-.0694	.4947	.061	-.0776	.2790	.112	-.0759	.2695	.150	-.1010	.2425	.260	-.0976	.1927
.064	-.0429	.8428	.061	-.0394	.4714	.085	-.0759	.3070	.161	-.0743	.2645	.200	-.0993	.2441	.350	-.0976	.1977
.087	-.0478	.7785	.056	-.0676	.4566	.110	-.0776	.3086	.209	-.0726	.2629	.300	-.0993	.2441	.460	-.0993	.1944
.112	-.0512	.7983	.110	-.0710	.4500	.160	-.0260	.3340	.259	-.0793	.2629	.400	-.0993	.2441	.640	-.0960	.1977
.162	-.0528	.6762	.160	-.0726	.4352	.209	-.0693	.3092	.307	-.0743	.2595	.500	-.0993	.2309	.830	-.0960	.1861
.210	-.0561	.6283	.210	-.0710	.3826	.259	-.0709	.2976	.358	-.0693	.2579	.600	-.0993	.2242			
.260	-.0578	.5128	.250	-.0726	.3546	.309	-.0743	.2777	.406	-.0759	.2496	.680	-.0993	.2159			
.310	-.0594	.4271	.300	-.0759	.3481	.356	-.0793	.2744	.500	-.0590	.2591	.780	-.0993	.2076			
.360	-.0627	.4056	.350	-.0759	.3415	.406	-.0743	.2693	.600	-.0590	.2441	.880	-.0976	.1993			
.380	-.0644	.3957	.400	-.0710	.3415	.505	-.0793	.2579	.700	-.0960	.2143						
.460	-.0644	.3693	.450	-.0776	.3152	.604	-.0776	.2447	.800	-.0976	.2093						
.510			.500	-.0759	.3037	.703	-.0776	.2347	.900	-.0993	.2159						
.600			.600			.802	-.0793	.2132	.950	-.0993	.2192						
.700	-.0661	.2720	.700	-.0793	.2560	.902	-.0793	.2083									
.800	-.0081	.2357	.800	-.0793	.2379	.952	-.0793	.1967									
.900	-.0396	.1763	.900	-.0759	.2132												
.950	-.0578	.2076	.950	-.0776	.2116												

TABLE B-10.- PRESSURE COEFFICIENTS FOR WING WITH 76° SWEEP,

$C_{L,des} = 0.1$, M = 4.6

(a) $\alpha = -1.46°$

Cp at 2y/b of:																	
0.00			0.20			0.40			0.60			0.80			0.95		
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower
.029			.025	.0469	.0340	.036	.0612	.0033	.064	.0659	-.0063	.104			.206		
.038			.037	.0489	.0381	.061	.0551	-.0067	.112	.0535	-.0043	.150	.0468	-.0407	.260	.0488	-.0551
.064	-.0021	.1051	.061	.0714	.0661	.085	.0469	.0053	.161	.0330	-.0063	.200	.0406	-.0407	.350	.0365	-.0572
.087	-.0041	.0990	.056	.0367	.0377	.110	.0428	-.0027	.209	.0187	-.0063	.300	.0284	-.0469	.460	.0243	-.0572
.112	-.0041	.1112	.110	.0264	.0418	.160	.0802	.0670	.259	.0104	-.0043	.400	.0080	-.0448	.640	.0018	-.0572
.162	-.0062	.1051	.160	.0142	.0418	.209	.0187	.0262	.307	.0043	-.0043	.500	-.0001	-.0448	.830	-.0144	-.0592
.210	-.0082	.0889	.210	.0019	.0276	.259	.0063	.0180	.358	.0043	.0038	.600	-.0123	-.0448			
.260	-.0102	.0564	.250	-.0082	.0134	.309	-.0038	.0099	.406	-.0059	.0017	.680	-.0205	-.0448			
.310	-.0041	.0238	.300	-.0143	.0073	.356	-.0141	.0038	.500	.0325	.0231	.780	-.0287	-.0469			
.360	-.0021	.0096	.350	-.0164	.0053	.406	-.0182	.0058	.600	.0325	.0005	.880	-.0328	-.0469			
.380	-.0021	.0076	.400	-.0143	.0033	.505	-.0285	-.0043	.700	-.0287	-.0345						
.460	-.0041	.0035	.450	-.0143	-.0006	.604	-.0244	-.0084	.800	-.0348	-.0407						
.510			.500	-.0143	-.0047	.703	-.0223	-.0104	.900	-.0368	-.0407						
.600			.600			.802	-.0244	-.0206	.950	-.0368	-.0407						
.700	-.0041	-.0187	.700	-.0123	-.0067	.902	-.0244	-.0247									
.800	.0551	-.0207	.800	-.0143	-.0209	.952	-.0264	-.0247									
.900			.900	-.0164	-.0270												
.950	.0121	-.0289	.950	-.0205	-.0310												

TABLE B-10.- Continued

(b) $\alpha = 0.53^{o}$

Cp at 2y/b of:																	
0.00			0.20			0.40			0.60			0.80			0.95		
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower
.029			.025	.0266	.0585	.036	.0411	.0257	.064	.0416	.0201	.104			.206		
.038			.037	.0287	.0626	.061	.0349	.0176	.112	.0313	.0242	.150	.0029	.0117	.260	.0029	-.0166
.064	-.0060	.1419	.061	.0534	.0905	.085	.0226	.0338	.161	.0107	.0262	.200	-.0053	.0117	.350	-.0094	-.0146
.087	-.0081	.1338	.056	.0165	.0622	.110	.0165	.0277	.209	-.0036	.0282	.300	-.0177	.0077	.460	-.0198	-.0146
.112	-.0101	.1500	.110	.0062	.0622	.160	.0621	.0873	.259	-.0098	.0303	.400	-.0322	.0097	.640	-.0384	-.0126
.162	-.0101	.1399	.160	-.0019	.0601	.209	.0004	.0384	.307	-.0160	.0242	.500	-.0384	.0036	.830	-.0503	-.0146
.210	-.0142	.1195	.210	-.0121	.0419	.259	-.0098	.0282	.358	-.0119	.0242	.600	-.0467	-.0004			
.260	-.0142	.0809	.250	-.0224	.0297	.309	-.0181	.0201	.406	-.0242	.0160	.680	-.0530	-.0024			
.310	-.0122	.0443	.300	-.0265	.0216	.356	-.0283	.0160	.500	-.0011	.0545	.780	-.0592	-.0065			
.360	-.0101	.0260	.350	-.0265	.0155	.406	-.0325	.0160	.600	-.0011	.0545	.880	-.0633	-.0105			
.380	-.0101	.0219	.400	-.0265	.0155	.505	-.0366	.0058	.700	-.0571	-.0004						
.460	-.0122	.0178	.450	-.0244	.0095	.604	-.0366	-.0002	.800	-.0633	-.0085						
.510			.500	-.0244	.0034	.703	-.0345	-.0022	.900	-.0633	-.0105						
.600			.600			.802	-.0366	-.0124	.950	-.0654	-.0085						
.700	-.0122	-.0126	.700	-.0244	-.0026	.902	-.0366	-.0165									
.800	.0512	-.0166	.800	-.0244	-.0148	.952	-.0366	-.0185									
.900			.900	-.0265	-.0229												
.950	.0061	-.0248	.950	-.0306	-.0269												

TABLE B-10.- Continued

(c) $\alpha = 3.54^{o}$

Cp at 2y/b of:																	
0.00			0.20			0.40			0.60			0.80			0.95		
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower
.029			.025	-.0020	.1012	.036	.0062	.0581	.064	.0085	.0568	.104			.206		
.038			.037	.0000	.1033	.061	.0000	.0500	.112	-.0038	.0670	.150	-.0081	.0412	.260	-.0163	.0104
.064	-.0163	.2110	.061	.0307	.1311	.085	-.0060	.0622	.161	-.0161	.0608	.200	-.0143	.0350	.350	-.0225	.0104
.087	-.0163	.1948	.056	-.0040	.1068	.110	-.0081	.0581	.209	-.0243	.0547	.300	-.0225	.0289	.460	-.0265	.0063
.112	-.0184	.2192	.110	-.0122	.1027	.160	.0414	.1098	.259	-.0305	.0486	.400	-.0327	.0207	.640	-.0368	.0022
.162	-.0184	.1388	.160	-.0204	.0966	.209	-.0161	.0608	.307	-.0325	.0445	.500	-.0368	.0104	.830	-.0409	-.0059
.210	-.0204	.1724	.210	-.0285	.0743	.259	-.0264	.0506	.358	-.0284	.0425	.600	-.0429	.0043			
.260	-.0245	.1256	.250	-.0326	.0581	.309	-.0325	.0405	.406	-.0387	.0343	.680	-.0450	.0001			
.310	-.0225	.0809	.300	-.0326	.0480	.356	-.0407	.0343	.500	.0081	.0555	.780	-.0470	-.0039			
.360	-.0204	.0606	.350	-.0347	.0419	.406	-.0428	.0364	.600	-.0020	.0555	.880	-.0470	-.0080			
.380	-.0225	.0565	.400	-.0367	.0419	.505	-.0449	.0242	.700	-.0450	.0001						
.460	-.0245	.0463	.450	-.0367	.0318	.604	-.0449	.0180	.800	-.0470	-.0080						
.510			.500	-.0367	.0257	.703	-.0428	.0160	.900	-.0490	-.0100						
.600			.600			.802	-.0449	.0038	.950	-.0490	-.0080						
.700	-.0184	.0077	.700	-.0388	.0135	.902	-.0449	-.0002									
.800	.0470	-.0024	.800	-.0408	.0014	.952	-.0469	-.0043									
.900			.900	-.0408	-.0067												
.950	-.0061	-.0126	.950	-.0408	-.0127												

TABLE B-10.- Continued

(d) $\alpha = 4.53^{o}$

Cp at 2y/b of:																	
0.00			0.20			0.40			0.60			0.80			0.95		
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower
.029			.025	-.0101	.1195	.036	-.0120	.0662	.064	-.0079	.0671	.104			.206		
.038			.037	-.0101	.1216	.061	-.0202	.0601	.112	-.0141	.0753	.150	-.0365	.0646	.260	-.0427	.0341
.064	-.0204	.2314	.061	.0167	.1473	.085	-.0202	.0723	.161	-.0244	.0671	.200	-.0386	.0606	.350	-.0468	.0341
.087	-.0204	.2192	.056	-.0181	.1230	.110	-.0243	.0662	.209	-.0305	.0630	.300	-.0427	.0524	.460	-.0510	.0301
.112	-.0224	.2456	.110	-.0264	.1169	.160	.0330	.1181	.259	-.0367	.0549	.400	-.0510	.0443	.640	-.0551	.0260
.162	-.0245	.2212	.160	-.0346	.1108	.209	-.0244	.0691	.307	-.0408	.0508	.500	-.0551	.0341	.830	-.0592	.0178
.210	-.0265	.1927	.210	-.0387	.0865	.259	-.0346	.0589	.358	-.0326	.0508	.600	-.0592	.0280			
.260	-.0285	.1419	.250	-.0428	.0662	.309	-.0408	.0467	.406	-.0428	.0426	.680	-.0613	.0240			
.310	-.0285	.0951	.300	-.0449	.0601	.356	-.0449	.0426	.500	-.0097	.0789	.780	-.0633	.0178			
.360	-.0265	.0728	.350	-.0449	.0520	.406	-.0469	.0447	.600	-.0097	.0768	.880	-.0633	.0138			
.380	-.0285	.0687	.400	-.0469	.0520	.505	-.0469	.0324	.700	-.0592	.0219						
.460	-.0285	.0585	.450	-.0469	.0419	.604	-.0469	.0243	.800	-.0633	.0138						
.510			.500	-.0469	.0338	.703	-.0469	.0222	.900	-.0633	.0138						
.600			.600			.802	-.0469	.0100	.950	-.0633	.0158						
.700	-.0204	.0158	.700	-.0490	.0196	.902	-.0490	.0059									
.800	.0430	.0056	.800	-.0510	.0054	.952	-.0510	.0039									
.900			.900	-.0490	-.0006												
.950	-.0122	-.0044	.950	-.0490	-.0067												

TABLE B-10.- Continued

(e) $\alpha = 5.53^{o}$

Cp at 2y/b of:																	
0.00			0.20			0.40			0.60			0.80			0.95		
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower
.029			.025	-.0183	.1340	.036	-.0163	.0784	.064	-.0243	.0732	.104			.206		
.038			.037	-.0183	.1381	.061	-.0245	.0723	.112	-.0264	.0834	.150	-.0368	.0710	.260	-.0388	.0384
.064	-.0224	.2521	.061	.0184	.1635	.085	-.0184	.0824	.161	-.0325	.0753	.200	-.0347	.0670	.350	-.0409	.0384
.087	-.0245	.2419	.056	-.0163	.1372	.110	-.0245	.0763	.209	-.0366	.0712	.300	-.0409	.0588	.460	-.0429	.0343
.112	-.0265	.2704	.110	-.0225	.1311	.160	.0311	.1263	.259	-.0407	.0651	.400	-.0429	.0506	.640	-.0450	.0323
.162	-.0265	.2439	.160	-.0306	.1250	.209	-.0284	.0773	.307	-.0449	.0589	.500	-.0470	.0405	.830	-.0470	.0242
.210	-.0285	.2114	.210	-.0327	.0986	.259	-.0407	.0671	.358	-.0366	.0569	.600	-.0470	.0343			
.260	-.0326	.1584	.250	-.0368	.0804	.309	-.0449	.0549	.406	-.0469	.0508	.680	-.0490	.0303			
.310	-.0306	.1075	.300	-.0388	.0703	.356	-.0469	.0508	.500	.0020	.0833	.780	-.0511	.0242			
.360	-.0285	.0831	.350	-.0388	.0642	.406	-.0469	.0549	.600	.0000	.0812	.880	-.0490	.0201			
.380	-.0306	.0790	.400	-.0388	.0622	.505	-.0469	.0406	.700	-.0470	.0282						
.460	-.0326	.0688	.450	-.0409	.0520	.604	-.0490	.0324	.800	-.0490	.0201						
.510		.0566	.500	-.0409	.0419	.703	-.0469	.0304	.900	-.0511	.0180						
.600		.0118	.600			.802	-.0490	.0161	.950	-.0511	.0201						
.700	-.0204	.0220	.700	-.0450	.0257	.902	-.0510	.0141									
.800	.0410	.0118	.800	-.0470	.0135	.952	-.0531	.0100									
.900			.900	-.0450	.0054												
.950	-.0142	-.0003	.950	-.0450	.0014												

TABLE B-10.- Continued

(f) $\alpha = 6.54^{o}$

Cp at 2y/b of:																	
0.00			0.20			0.40			0.60			0.80			0.95		
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower
.029		.2538	.025	-.0204	.1541	.036	-.0346	.0865	.064	-.0367	.0812	.104			.206		
.038		.2395	.037	-.0204	.1622	.061	-.0407	.0824	.112	-.0367	.0914	.150	-.0572	.0660	.260	-.0572	.0310
.064	-.0225	.2802	.061	.0064	.1817	.085	-.0366	.0926	.161	-.0408	.0853	.200	-.0551	.0598	.350	-.0592	.0331
.087	-.0245	.2680	.056	-.0284	.1554	.110	-.0407	.0865	.209	-.0408	.0771	.300	-.0572	.0557	.460	-.0613	.0269
.112	-.0265	.2965	.110	-.0346	.1473	.160	.0248	.1363	.259	-.0469	.0710	.400	-.0613	.0454	.640	-.0613	.0228
.162	-.0265	.2700	.160	-.0407	.1392	.209	-.0326	.0873	.307	-.0469	.0670	.500	-.0613	.0331	.830	-.0613	.0167
.210	-.0286	.2354	.210	-.0449	.1128	.259	-.0408	.0771	.358	-.0387	.0649	.600	-.0613	.0269			
.260	-.0306	.1785	.250	-.0469	.0926	.309	-.0449	.0649	.406	-.0490	.0568	.680	-.0633	.0228			
.310	-.0306	.1236	.300	-.0490	.0824	.356	-.0490	.0588	.500	-.0119	.0742	.780	-.0633	.0167			
.360	-.0306	.0992	.350	-.0490	.0763	.406	-.0469	.0629	.600	-.0119	.0269	.880	-.0633	.0125			
.380	-.0306	.0951	.400	-.0490	.0743	.505	-.0490	.0486	.700	-.0592	.0187						
.460	-.0327	.0850	.450	-.0510	.0622	.604	-.0510	.0405	.800	-.0613	.0125						
.510			.500	-.0510	.0520	.703	-.0490	.0364	.900	-.0633	.0105						
.600			.600			.802	-.0531	.0242	.950	-.0633	.0125						
.700	-.0204	.0321	.700	-.0551	.0338	.902	-.0531	.0201									
.800	.0409	.0219	.800	-.0572	.0236	.952	-.0551	.0160									
.900			.900	-.0551	.0115												
.950	-.0163	.0097	.950	-.0551	.0054												

TABLE B-10.- Continued

(g) $\alpha = 10.54^{o}$

Cp at 2y/b of:																	
0.00			0.20			0.40			0.60			0.80			0.95		
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower
.029			.025	-.0327	.2561	.036	-.0510	.1290	.064	-.0490	.1140	.104			.206		
.038			.037	-.0327	.2418	.061	-.0551	.1249	.112	-.0490	.1283	.150	-.0778	.1158	.260	-.0778	.0771
.064	-.0265	.3843	.061	-.0057	.2506	.085	-.0510	.1371	.161	-.0469	.1201	.200	-.0778	.1118	.350	-.0778	.0791
.087	-.0265	.3843	.056	-.0386	.2222	.110	-.0531	.1371	.209	-.0469	.1160	.300	-.0778	.1077	.460	-.0778	.0751
.112	-.0306	.4067	.110	-.0448	.2121	.160	.0146	.1793	.259	-.0531	.1120	.400	-.0778	.0995	.640	-.0758	.0730
.162	-.0286	.3701	.160	-.0489	.2060	.209	-.0387	.1324	.307	-.0490	.1058	.500	-.0778	.0893	.830	-.0778	.0649
.210	-.0327	.3253	.210	-.0489	.1716	.259	-.0449	.1222	.358	-.0428	.1038	.600	-.0778	.0812			
.260	-.0347	.2540	.250	-.0510	.1472	.309	-.0469	.1099	.406	-.0510	.0956	.680	-.0778	.0751			
.310	-.0368	.1869	.300	-.0531	.1371	.356	-.0510	.1058	.500	-.0259	.1240	.780	-.0778	.0690			
.360	-.0347	.1624	.350	-.0531	.1290	.406	-.0490	.1079	.600	-.0321	.1240	.880	-.0778	.0628			
.380	-.0368	.1584	.400	-.0510	.1290	.505	-.0531	.0916	.700	-.0737	.0710						
.460	-.0388	.1421	.450	-.0572	.1148	.604	-.0531	.0814	.800	-.0758	.0628						
.510			.500	-.0551	.1006	.703	-.0510	.0773	.900	-.0778	.0628						
.600			.600			.802	-.0551	.0610	.950	-.0778	.0649						
.700	-.0327	.0770	.700	-.0592	.0743	.902	-.0551	.0569									
.800	.0389	.0607	.800	-.0613	.0642	.952	-.0551	.0528									
.900			.900	-.0592	.0500												
.950	-.0224	.0423	.950	-.0592	.0459												

TABLE B-10.- Concluded

(h) $\alpha = 20.54^{o}$

Cp at 2y/b of:																	
0.00			0.20			0.40			0.60			0.80			0.95		
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower
.029			.025	-.0470	.4916	.036	-.0531	.2786	.064	-.0551	.2384	.104			.206		
.038			.037	-.0470	.4834	.061	-.0552	.2766	.112	-.0551	.2670	.150	-.0572	.2449	.260	-.0532	.1918
.064	-.0327	.7559	.061	-.0122	.4830	.085	-.0531	.3029	.161	-.0531	.2629	.200	-.0532	.2469	.350	-.0532	.1979
.087	-.0368	.6928	.086	-.0449	.4587	.110	-.0552	.3049	.209	-.0510	.2609	.300	-.0572	.2449	.460	-.0532	.1959
.112	-.0409	.7416	.110	-.0490	.4506	.160	.0063	.3384	.259	-.0551	.2609	.400	-.0572	.2449	.640	-.0511	.1979
.162	-.0389	.6359	.160	-.0511	.4365	.209	-.0469	.3037	.307	-.0531	.2588	.500	-.0572	.2326	.830	-.0511	.1877
.210	-.0429	.5891	.210	-.0511	.3818	.259	-.0490	.2915	.358	-.0428	.2568	.600	-.0552	.2224			
.260	-.0429	.5180	.250	-.0511	.3494	.309	-.0551	.2751	.406	-.0551	.2486	.680	-.0552	.2143			
.310	-.0470	.4306	.300	-.0552	.3413	.356	-.0572	.2711	.500	-.0062	.2653	.780	-.0552	.2041			
.360	-.0491	.4001	.350	-.0552	.3353	.406	-.0531	.2813	.600	-.0062	.2633	.880	-.0552	.1979			
.380	-.0511	.3879	.400	-.0511	.3353	.505	-.0572	.2568	.700	-.0511	.2122						
.460	-.0511	.3635	.450	-.0572	.3110	.604	-.0572	.2445	.800	-.0532	.2041						
.510			.500	-.0552	.2988	.703	-.0572	.2323	.900	-.0552	.2102						
.600			.600			.802	-.0593	.2058	.950	-.0572	.2163						
.700	-.0511	.2659	.700	-.0593	.2523	.902	-.0551	.2037									
.800	.0264	.2313	.800	-.0593	.2361	.952	-.0572	.1935									
.900			.900	-.0572	.2098												
.950	-.0409	.2049	.950	-.0593	.2077												

TABLE B-11.- PRESSURE COEFFICIENTS FOR WING WITH 55° SWEEP,

$C_{L,des} = 0.0$, $M = 2.3$

(a) $\alpha = -14.30°$

Cp at 2y/b of:																	
0.00			0.20			0.40			0.60			0.80			0.95		
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower
.024			.016	.5243		.024			.055	.5178		.107	.5228		.194		
.050	.3345		.028	.5572		.050	.5345		.100	.5050		.160	.5018		.246	.5280	
.076			.052	.4479		.072	.5155		.146	.4732		.208	.4713		.362	.4818	
.100			.077	.4226		.100	.4733		.190	.4498		.306			.450	.4471	
.150	.3472		.100	.4089		.150	.4456		.240	.4254		.403	.4009		.640	.3999	
.200	.3451		.150	.3856		.200	.4169		.284	.4052		.503	.3694		.850	.3505	
.250	.3472		.200	.3687		.250	.3808		.330	.3840		.600	.3358				
.300	.3504		.250	.3508		.300	.3691		.374			.700	.3117				
.350	.3504		.300	.3328		.350	.3458		.473	.3264		.800	.2917				
.400			.350	.3233		.400	.3245		.572	.3033		.900	.2739				
.450	.3186		.400	.3117		.500	.2958		.672	.2770							
.500	.3058		.450	.2959		.600	.2566		.771	.2497							
.550	.2931		.500	.2790		.700	.2364		.870	.2329							
.600	.2719		.600	.2463		.800	.2183		.915	.2266							
.700			.700	.2273		.900	.2098										
.800			.800	.2114		.940	.2088										
.900			.900	.1966													
.940	.2082		.940	.1935													

TABLE B-11.- Continued

(b) α = -10.20°

Cp at 2y/b of:																		
0.00			0.20			0.40			0.60			0.80			0.95		
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower
.024			.016	.4162		.024			.055	.4198		.107	.4138		.194		
.050	.2332		.028	.4204		.050	.4034		.100	.3997		.160	.3937		.246	.4307	
.076			.052	.3317		.072	.3876		.146	.3637		.208	.3672		.362	.3767	
.100			.077	.3085		.100	.3559		.190	.3393		.306			.450	.3418	
.150	.2438		.100	.2917		.150	.3329		.240	.3170		.403	.2963		.640	.2931	
.200	.2428		.150	.2727		.200	.3043		.284	.3001		.503	.2613		.850	.2444	
.250	.2470		.200	.2579		.250	.2704		.330	.2789		.600	.2285				
.300	.2449		.250			.300	.2587		.374			.700	.2031				
.350	.2417		.300	.2253		.350	.2365		.473	.2190		.800	.1841				
.400			.350	.2137		.400	.2163		.572	.1989		.900	.1682				
.450	.2121		.400	.2073		.500	.1941		.672	.1735							
.500	.2036		.450	.1936		.600	.1623		.771	.1523							
.550	.1783		.500	.1799		.700	.1443		.870	.1364							
.600	.1761		.600	.1536		.800	.1284		.915	.1279							
.700			.700	.1378		.900	.1220										
.800			.800	.1230		.940	.1210										
.900			.900	.1104													
.940	.1264		.940	.1093													

TABLE B-11.- Continued

(c) α = -8.19°

Cp at 2y/b of:																	
0.00			0.20			0.40			0.60			0.80			0.95		
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower
.024			.016	.3664		.024			.055	.3643		.107	.3615		.194		
.050	.1877		.028	.3347		.050	.3843		.100	.3339		.160	.3415		.246	.3731	
.076			.052	.2768		.072	.3253		.146	.3134		.208	.3152		.362	.3225	
.100			.077	.2558		.100	.3011		.190	.2911		.306			.450	.2839	
.150	.1993		.100	.2389		.150	.2794		.240	.2699		.403	.2499		.640	.2457	
.200	.1983		.150	.2220		.200	.2550		.284	.2508		.503	.2173		.850	.1994	
.250	.1962		.200	.2094		.250	.2221		.330	.2327		.600	.1857				
.300	.1930		.250			.300	.2105		.374			.700	.1604				
.350	.1919		.300	.1757		.350	.1871		.473	.1783		.800	.1404				
.400			.350	.1662		.400	.1691		.572	.1773		.900	.1257				
.450	.1676		.400	.1620		.500	.1500		.672	.1320							
.500	.1602		.450	.1504		.600	.1224		.771	.1131							
.550	.1306		.500	.1377		.700	.1033		.870	.0983							
.600	.1359		.600	.1145		.800	.0895		.915	.0910							
.700			.700	.0987		.900	.0821										
.800			.800	.0840		.940	.0810										
.900			.900														
.940	.0883		.940	.0734													

TABLE B-11.- Continued

(d) $\alpha = -6.18^{o}$

Cp at 2y/b of:																	
0.00			0.20			0.40			0.60			0.80			0.95		
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower
.024			.016	.3172		.024			.055	.2914		.107	.3187		.194		
.050	.1458		.028	.2410		.050	.3273		.100	.2871		.160	.2821		.246	.3114	
.076			.052	.2251		.072	.2672		.146	.2596		.208	.2622		.362	.2674	
.100			.077	.2051		.100	.2440		.190	.2405		.306			.450	.2381	
.150	.1574		.100	.1914		.150	.2268		.240	.2215		.403	.2024		.640	.1983	
.200	.1542		.150	.1745		.200	.2034		.284	.2045		.503	.1710		.850	.1542	
.250	.1521		.200	.1640		.250	.1759		.330	.1865		.600	.1427				
.300	.1500		.250			.300	.1653		.374			.700	.1186				
.350	.1479		.300	.1324		.350	.1441		.473	.1364		.800	.0998				
.400			.350	.1229		.400	.1251		.572	.1123		.900	.0851				
.450	.1288		.400	.1187		.500	.1070		.672	.0914							
.500	.1214		.450	.1123		.600	.0837		.771	.0736							
.550	.1035		.500	.1007		.700	.0668		.870	.0610							
.600	.0892		.600	.0765		.800	.0520		.915	.0558							
.700			.700	.0607		.900	.0456										
.800			.800	.0512		.940	.0445										
.900			.900														
.940	.0558		.940	.0407													

TABLE B-11.- Continued

(e) α = -4.19°

Cp at 2y/b of:																	
0.00			0.20			0.40			0.60			0.80			0.95		
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower
.024			.016	.2724		.024			.055	.2073		.107	.2399		.194		
.050	.1064		.028	.1455		.050	.2289		.100	.2306		.160	.2210		.246	.2430	
.076			.052	.1742		.072	.2110		.146	.2063		.208	.2042		.362	.2042	
.100			.077	.1552		.100	.1889		.190	.1883		.306			.450	.1811	
.150	.1169		.100	.1436		.150	.1756		.240	.1724		.403	.1517		.640	.1454	
.200	.1148		.150	.1289		.200	.1555		.284	.1565		.503	.1234		.850	.1077	
.250	.1127		.200	.1205		.250	.1322		.330	.1417		.600	.0972				
.300	.1106		.250			.300	.1227		.374			.700	.0762				
.350	.1106		.300	.0931		.350	.1036		.473	.0961		.800	.0583				
.400			.350	.0847		.400	.0856		.572	.0699		.900	.0447				
.450	.0926		.400	.0826		.500	.0676		.672	.0489							
.500	.0863		.450	.0763		.600	.0475		.771	.0332							
.550	.0725		.500	.0647		.700	.0316		.870	.0216							
.600	.0641		.600	.0415		.800	.0178		.915	.0164							
.700			.700	.0299		.900	.0115										
.800			.800	.0205		.940	.0104										
.900			.900														
.940	.0249		.940	.0099													

TABLE B-11.- Continued

(f) $\alpha = -2.19^{o}$

Cp at 2y/b of:																	
0.00			0.20			0.40			0.60			0.80			0.95		
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower
.024			.016	.2281		.024			.055	.1077		.107	.1687		.194		
.050	.0684		.028	.0567		.050	.1353		.100	.1724		.160	.1507		.246	.1613	
.076			.052	.1237		.072	.1553		.146	.1512		.208	.1401		.362	.1306	
.100			.077	.1090		.100	.1374		.190	.1342		.306			.450	.1157	
.150	.0800		.100	.0974		.150	.1278		.240	.1225		.403	.0945		.640	.0871	
.200	.0779		.150	.0858		.200	.1087		.284	.1087		.503	.0702		.850	.0532	
.250	.0800		.200	.0805		.250			.330	.0960		.600	.0468				
.300	.0768		.250	.0711		.300	.0822		.374			.700	.0278				
.350	.0768		.300	.0584		.350	.0642		.473	.0490		.800	.0140				
.400			.350	.0500		.400	.0483		.572	.0246		.900	.0013				
.450	.0599		.400	.0479		.500	.0313		.672	.0055							
.500	.0535		.450	.0416		.600	.0111		.771	-.0114							
.550	.0123		.500	.0321		.700	-.0015		.870	-.0209							
.600	.0334		.600	.0110		.800	-.0143		.915	-.0251							
.700			.700	.0005		.900											
.800			.800	-.0078		.940	-.0206										
.900			.900	-.0162													
.940	-.0035		.940	-.0173													

TABLE B-11.- Continued

(g) $\alpha = -0.19^{o}$

Cp at 2y/b of:																	
0.00			0.20			0.40			0.60			0.80			0.95		
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower
.024			.016	.1707		.024			.055			.107	.0719		.194		
.050	.0375		.028	.0714		.050	.1267		.100	.1018		.160	.0750		.246	.0645	
.076			.052	.0751		.072	.0941		.146	.0923		.208	.0761		.362	.0478	
.100			.077	.0635		.100	.0835		.190	.0817		.306			.450	.0478	
.150	.0502		.100	.0562		.150	.0817		.240	.0711		.403	.0509		.640	.0341	
.200	.0481		.150	.0478		.200	.0636		.284	.0605		.503	.0299		.850	.0268	
.250	.0471		.200	.0457		.250			.330	.0499		.600	.0100				
.300	.0471		.250	.0383		.300	.0425		.374			.700	-.0056				
.350	.0471		.300	.0257		.350	.0287		.473	.0184		.800	-.0182				
.400			.350	.0183		.400	.0149		.572	-.0056		.900	-.0277				
.450	.0301		.400	.0162		.500	-.0030		.672	-.0224							
.500	.0249		.450	.0109		.600	-.0200		.771	-.0371							
.550	.0185		.500	.0025		.700	-.0305		.870	-.0455							
.600	.0058		.600	-.0153		.800	-.0422		.915	-.0508							
.700			.700	-.0248		.900											
.800			.800	-.0321		.940	-.0486										
.900			.900	-.0416													
.940	-.0279		.940	-.0437													

TABLE B-11.- Continued

(h) $\alpha = 1.81^{o}$

Cp at 2y/b of:																							
0.00			0.20			0.40			0.60			0.80			0.95		
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower
.024			.016	.0511		.024			.055			.107	.0155		.194		
.050	.0089		.028	.0268		.050	.0497		.100	.0384		.160	.0134		.246	.0040	
.076			.052	.0276		.072	.0350		.146	.0278		.208	.0145		.362	-.0095	
.100			.077	.0192		.100	.0276		.190	.0204		.306			.450	-.0147	
.150	.0226		.100	.0129		.150	.0310		.240	.0140		.403	-.0053		.640	-.0241	
.200	.0205		.150	.0129		.200	.0151		.284	.0087		.503	-.0199		.850	-.0377	
.250	.0205		.200	.0118		.250			.330	.0003		.600	-.0356				
.300	.0194		.250	.0066		.300	.0024		.374			.700	-.0482				
.350	.0173		.300	-.0049		.350	-.0071		.473	-.0199		.800	-.0566				
.400			.350	-.0133		.400	-.0198		.572	-.0419		.900	-.0639				
.450	.0025		.400	-.0154		.500	-.0346		.672	-.0555							
.500	-.0037		.450	-.0186		.600	-.0516		.771	-.0670							
.550	-.0058		.500	-.0238		.700	-.0601		.870	-.0743							
.600	-.0185		.600	-.0417		.800	-.0686		.915	-.0775							
.700			.700	-.0491		.900											
.800			.800	-.0575		.940	-.0739										
.900			.900	-.0649													
.940	-.0492		.940	-.0659													

TABLE B-11.- Continued

(i) $\alpha = 3.82^{o}$

Cp at 2y/b of:																		
0.00			0.20			0.40			0.60			0.80			0.95			
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	
.024			.016	-.0215		.024			.055			.107	-.0535		.194			
.050	-.0152		.028	-.0437		.050	-.0152		.100	-.0233		.160	-.0492		.246	-.0714		
.076			.052	-.0247		.072	-.0152		.146	-.0318		.208	-.0503		.362	-.0683		
.100			.077	-.0258		.100	-.0279		.190	-.0339		.306			.450	-.0735		
.150	-.0014		.100	-.0279		.150	-.0202		.240	-.0360		.403	-.0630		.640	-.0809		
.200	-.0035		.150	-.0247		.200	-.0318		.284	-.0403		.503	-.0756		.850	-.0830		
.250	-.0046		.200	-.0205		.250			.330	-.0466		.600	-.0873					
.300	-.0056		.250	-.0258		.300	-.0382		.374			.700	-.0968					
.350	-.0078		.300	-.0331		.350	-.0456		.473	-.0672		.800	-.1042					
.400			.350	-.0394		.400	-.0540		.572	-.0883		.900	-.1084					
.450	-.0194		.400	-.0405		.500	-.0646		.672	-.0978								
.500	-.0247		.450	-.0426		.600	-.0784		.771	-.1063								
.550	-.0278		.500	-.0479		.700	-.0847		.870	-.1105								
.600	-.0395		.600	-.0637		.800	-.0911		.915	-.1137								
.700			.700	-.0721		.900												
.800			.800	-.0784		.940	-.0964											
.900			.900	-.0858														
.940	-.0691		.940	-.0868														

TABLE B-11.- Continued

(j) $\alpha = 5.81^{o}$

Cp at 2y/b of:																		
0.00			0.20			0.40			0.60			0.80			0.95		
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower
.024			.016	-.0755		.024			.055	-.1194		.107	-.1119		.194		
.050	-.0342		.028	-.0945		.050	-.0942		.100	-.0918		.160	-.1014		.246	-.1320	
.076			.052	-.0711		.072	-.0742		.146	-.0801		.208	-.0993		.362	-.1151	
.100			.077	-.0732		.100	-.0753		.190	-.0812		.306			.450	-.1151	
.150	-.0237		.100	-.0732		.150	-.0610		.240	-.0833		.403	-.1046		.640	-.1235	
.200	-.0258		.150	-.0637		.200	-.0780		.284	-.0865		.503	-.1130		.850	-.1235	
.250	-.0279		.200	-.0542		.250			.330	-.0897		.600	-.1235				
.300	-.0290		.250	-.0542		.300	-.0844		.374			.700	-.1320				
.350	-.0290		.300	-.0595		.350	-.0886		.473	-.1004		.800	-.1372				
.400			.350	-.0637		.400	-.0939		.572	-.1225		.900	-.1415				
.450	-.0406		.400	-.0648		.500	-.0950		.672	-.1320							
.500	-.0459		.450	-.0658		.600	-.1045		.771	-.1404							
.550	-.0438		.500	-.0700		.700	-.1098		.870	-.1446							
.600	-.0607		.600	-.0837		.800	-.1151		.915	-.1457							
.700			.700	-.0911		.900											
.800			.800	-.0974		.940	-.1173										
.900			.900	-.1048													
.940	-.0871		.940	-.1058													

TABLE B-11.- Continued

(k) $\alpha = 7.81^{o}$

Cp at 2y/b of:																	
0.00			0.20			0.40			0.60			0.80			0.95		
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower
.024			.016	-.1302		.024			.055	-.1628		.107	-.1598		.194		
.050	-.0561		.028	-.1281		.050	-.1508		.100	-.1331		.160	-.1472		.246	-.1671	
.076			.052	-.1150		.072	-.1203		.146	-.1278		.208	-.1419		.362	-.1556	
.100			.077	-.1171		.100	-.1224		.190	-.1246		.306			.450	-.1535	
.150	-.0455		.100	-.1139		.150	-.0970		.240	-.1225		.403	-.1388		.640	-.1566	
.200	-.0486		.150	-.1087		.200	-.1140		.284	-.1235		.503	-.1440		.850	-.1577	
.250	-.0486		.200	-.0929		.250			.330	-.1267		.600	-.1514				
.300	-.0497		.250	-.0855		.300	-.1225		.374			.700	-.1587				
.350	-.0518		.300	-.0855		.350	-.1278		.473	-.1272		.800	-.1640				
.400			.350	-.0886		.400	-.1341		.572	-.1493		.900	-.1682				
.450	-.0603		.400	-.0886		.500	-.1352		.672	-.1566							
.500	-.0666		.450	-.0897		.600	-.1331		.771	-.1640							
.550	-.0603		.500	-.0929		.700	-.1331		.870	-.1703							
.600	-.0804		.600	-.1045		.800	-.1373		.915	-.1724							
.700			.700	-.1118		.900											
.800			.800	-.1171		.940	-.1384										
.900			.900	-.1224													
.940	-.1048		.940	-.1245													

TABLE B-11.- Continued

(1) $\alpha = 9.81^{o}$

Cp at 2y/b of:																	
0.00			0.20			0.40			0.60			0.80			0.95		
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower
.024			.016	-.1748		.024			.055	-.1980		.107	-.2046		.194		
.050	-.0733		.028	-.1632		.050	-.1834		.100	-.1747		.160	-.1908		.246	-.2046	
.076			.052	-.1432		.072	-.1643		.146	-.1620		.208	-.1792		.362	-.1961	
.100			.077	-.1496		.100	-.1538		.190	-.1567		.306			.450	-.1919	
.150	-.0606		.100	-.1485		.150	-.1249		.240	-.1567		.403	-.1761		.640	-.1908	
.200	-.0637		.150	-.1443		.200	-.1419		.284	-.1535		.503	-.1771		.850	-.1856	
.250	-.0648		.200	-.1326		.250			.330	-.1546		.600	-.1813				
.300	-.0659		.250	-.1179		.300	-.1482		.374			.700	-.1877				
.350	-.0669		.300	-.1126		.350	-.1535		.473	-.1550		.800	-.1919				
.400			.350	-.1115		.400	-.1599		.572	-.1792		.900	-.1951				
.450	-.0764		.400	-.1115		.500	-.1652		.672	-.1856							
.500	-.0817		.450	-.1126		.600	-.1652		.771	-.1919							
.550	-.0669		.500	-.1136		.700	-.1578		.870	-.1951							
.600	-.0934		.600	-.1231		.800	-.1567		.915	-.1972							
.700			.700	-.1295		.900											
.800			.800	-.1337		.940	-.1535										
.900			.900	-.1390													
.940	-.1177		.940	-.1390													

TABLE B-11.- Concluded

(m) $\alpha = 13.82^{o}$

Cp at 2y/b of:																	
0.00			0.20			0.40			0.60			0.80			0.95		
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower
.024			.016	-.2267		.024			.055	-.2403		.107	-.2572		.194		
.050	-.1019		.028	-.2193		.050	-.2415		.100	-.2319		.160	-.2509		.246	-.2572	
.076			.052	-.1928		.072	-.2193		.146	-.2234		.208	-.2381		.362	-.2519	
.100			.077	-.1892		.100	-.2097		.190	-.2149		.306			.450	-.2477	
.150	-.0924		.100	-.1960		.150	-.1746		.240	-.2096		.403	-.2296		.640	-.2402	
.200	-.0977		.150	-.1960		.200	-.1937		.284	-.2054		.503	-.2296		.850	-.2307	
.250	-.0987		.200	-.1897		.250			.330	-.2043		.600	-.2317				
.300	-.0998		.250	-.1791		.300	-.1948		.374			.700	-.2339				
.350	-.1008		.300	-.1664		.350	-.1979		.473	-.2009		.800	-.2339				
.400			.350	-.1579		.400	-.2022		.572	-.2264		.900	-.2222				
.450	-.1051		.400	-.1569		.500	-.2054		.672	-.2307							
.500	-.1104		.450	-.1558		.600	-.2096		.771	-.2328							
.550	-.0860		.500	-.1558		.700	-.2001		.870	-.2360							
.600	-.1209		.600	-.1622		.800	-.1927		.915	-.2360							
.700			.700	-.1664		.900											
.800			.800	-.1674		.940	-.1739										
.900			.900	-.1685													
.940	-.1400		.940	-.1706													

APPENDIX B

TABLE B-12.- PRESSURE COEFFICIENTS FOR WING WITH 55° SWEEP,

$C_{L,des} = 0.0$, $M = 3.0$

(a) $\alpha = -14.20°$

Cp at 2y/b of:																	
0.00			0.20			0.40			0.60			0.80			0.95		
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower
.024			.016	.4835		.024			.055			.107	.5049		.194		
.050	.2816		.028	.5100		.050	.5589		.100	.4761		.160	.4811		.246	.4798	
.076			.052	.3877		.072	.4670		.146	.4432		.208	.4498		.362	.4623	
.100			.077	.3625		.100	.4267		.190	.4204		.306			.450	.4272	
.150	.2904		.100	.3474		.150	.4103		.240	.3939		.403	.3784		.640	.3797	
.200	.2955		.150	.3272		.200	.3850		.284	.3749		.503	.3471		.850	.3784	
.250	.2980		.200	.3159		.250			.330	.3572		.600	.3145				
.300	.2980		.250	.3083		.300	.3370		.374			.700	.2870				
.350	.2993		.300	.2907		.350	.3142		.473	.3008		.800	.2670				
.400			.350	.2806		.400	.2902		.572	.2895		.900	.2532				
.450	.2766		.400	.2769		.500	.2636		.672	.2444							
.500	.2740		.450	.2655		.600	.2295		.771	.2219							
.550	.2400		.500	.2517		.700	.2054		.870	.2056							
.600	.2425		.600	.2202		.800	.1852		.915	.1993							
.700			.700	.1975		.900											
.800			.800	.1799		.940	.1751										
.900			.900	.1648													
.940	.1882		.940	.1648													

TABLE B-12.- Continued

(b) α = -10.10°

Cp at 2y/b of:																	
0.00			0.20			0.40			0.60			0.80			0.95		
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower
.024			.016	.4072		.024			.055			.107	.3722		.194		
.050	.1937		.028	.2998		.050	.4393		.100	.3527		.160	.3571		.246	.3722	
.076			.052	.2973		.072	.3450		.146	.3274		.208	.3358		.362	.3371	
.100			.077	.2734		.100	.3161		.190	.3084		.306			.450	.3096	
.150	.2013		.100	.2596		.150	.3034		.240	.2882		.403	.2745		.640	.2732	
.200	.2076		.150	.2395		.200	.2780		.284	.2730		.503	.2482		.850	.2519	
.250	.2114		.200	.2282		.250			.330	.2565		.600	.2206				
.300	.2126		.250	.2156		.300	.2363		.374			.700	.1981				
.350	.2126		.300	.1993		.350	.2135		.473	.2119		.800	.1806				
.400			.350	.1867		.400	.1932		.572	.1818		.900	.1643				
.450	.1886		.400	.1817		.500	.1679		.672	.1580							
.500	.1836		.450	.1742		.600	.1426		.771	.1392							
.550	.2366		.500	.1603		.700	.1248		.870	.1255							
.600	.1558		.600	.1314		.800	.1084		.915	.1192							
.700			.700	.1164		.900											
.800			.800	.1025		.940	.0995										
.900			.900	.0925													
.940	.1116		.940	.0912													

TABLE B-12.- Continued

(c) $\alpha = -8.14^{o}$

Cp at 2y/b of:																	
0.00			0.20			0.40			0.60			0.80			0.95		
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower
.024			.016	.3604		.024			.055			.107	.3070		.194		
.050	.1583		.028	.2442		.050	.3500		.100	.2937		.160	.2907		.246	.2835	
.076			.052	.2495		.072	.2859		.146	.2709		.208	.2732		.362	.2669	
.100			.077	.2269		.100	.2620		.190	.2544		.306			.450	.2469	
.150	.1659		.100	.2118		.150	.2506		.240	.2379		.403	.2256		.640	.2156	
.200	.1684		.150	.1942		.200	.2252		.284	.2265		.503	.2006		.850	.1893	
.250	.1646		.200	.1842		.250			.330	.2100		.600	.1755				
.300	.1646		.250	.1741		.300	.1898		.374			.700	.1555				
.350	.1671		.300	.1565		.350	.1707		.473	.1718		.800	.1380				
.400			.350	.1440		.400	.1505		.572	.1430		.900	.1242				
.450	.1482		.400	.1377		.500	.1289		.672	.1192							
.500	.1431		.450	.1314		.600	.1048		.771	.1016							
.550	.1924		.500	.1201		.700	.0896		.870	.0904							
.600	.1179		.600	.0962		.800	.0757		.915	.0841							
.700			.700	.0812		.900											
.800			.800	.0724		.940	.0655										
.900			.900	.0623													
.940	.0787		.940	.0598													

TABLE B-12.- Continued

(d) α = -6.15°

Cp at 2y/b of:																	
0.00			0.20			0.40			0.60			0.80			0.95		
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower
.024			.016	.3074		.024			.055			.107	.2173		.194		
.050	.1267		.028	.1659		.050	.2311		.100	.2286		.160	.2135		.246	.1858	
.076			.052	.2060		.072	.2286		.146	.2135		.208	.2072		.362	.1846	
.100			.077	.1846		.100	.2072		.190	.2021		.306			.450	.1733	
.150	.1330		.100	.1707		.150	.2033		.240	.1894		.403	.1733		.640	.1556	
.200	.1356		.150	.1531		.200	.1780		.284	.1805		.503	.1519		.850	.1343	
.250	.1343		.200	.1443		.250			.330	.1666		.600	.1292				
.300	.1330		.250	.1330		.300	.1489		.374			.700	.1104				
.350	.1305		.300	.1167		.350	.1324		.473	.1317		.800	.0953				
.400			.350	.1041		.400	.1134		.572	.1267		.900	.0840				
.450	.1116		.400	.1003		.500	.0932		.672	.0827							
.500	.1065		.450	.0953		.600	.0704		.771	.0651							
.550	.1899		.500	.0865		.700	.0577		.870	.0538							
.600	.0863		.600	.0651		.800	.0451		.915	.0487							
.700			.700	.0525		.900											
.800			.800	.0450		.940	.0362										
.900			.900	.0336													
.940	.0497		.940	.0324													

TABLE B-12.- Continued

(e) $\alpha = -4.15^{o}$

Cp at 2y/b of:																	
0.00			0.20			0.40			0.60			0.80			0.95		
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower
.024			.016	.2276		.024			.055			.107	.1482		.194		
.050	.0338		.028	.1708		.050	.1633		.100	.1618		.160	.1355		.246	.1152	
.076			.052	.1593		.072	.1719		.146	.1554		.208	.1330		.362	.1063	
.100			.077	.1429		.100	.1580		.190	.1504		.306			.450	.0974	
.150	.0988		.100	.1291		.150	.1605		.240	.1428		.403	.1101		.640	.0835	
.200	.1013		.150	.1140		.200	.1390		.284	.1364		.503	.0949		.850	.0683	
.250	.1001		.200	.1040		.250			.330	.1263		.600	.0784				
.300	.0976		.250	.0964		.300	.1124		.374			.700	.0632				
.350	.0950		.300	.0813		.350	.0972		.473	.0898		.800	.0518				
.400			.350	.0713		.400	.0819		.572	.0607		.900	.0429				
.450	.0786		.400	.0675		.500	.0617		.672	.0429							
.500	.0736		.450	.0625		.600	.0414		.771	.0264							
.550	.1291		.500	.0562		.700	.0287		.870	.0175							
.600	.0572		.600	.0386		.800	.0173		.915	.0112							
.700			.700	.0273		.900											
.800			.800	.0197		.940	.0097										
.900			.900	.0097													
.940	.0256		.940	.0084													

TABLE B-12.- Continued

(f) $\alpha = -2.15^{\circ}$

Cp at 2y/b of:																	
0.00			0.20			0.40			0.60			0.80			0.95		
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower
.024			.016	.1432		.024			.055			.107	.0798		.194		
.050	.0649		.028	.0977		.050	.1117		.100	.1047		.160	.0836		.246	.0710	
.076			.052	.1155		.072	.1117		.146	.1009		.208	.0823		.362	.0596	
.100			.077	.1016		.100	.1029		.190	.0958		.306			.450	.0520	
.150	.0687		.100	.0928		.150	.1160		.240	.0920		.403	.0646		.640	.0394	
.200	.0699		.150	.0765		.200	.0983		.284	.0882		.503	.0520		.850	.0306	
.250	.0674		.200	.0702		.250			.330	.0819		.600	.0394				
.300	.0662		.250	.0626		.300	.0781		.374			.700	.0268				
.350	.0649		.300	.0501		.350	.0641		.473	.0609		.800	.0192				
.400			.350	.0400		.400	.0502		.572	.0331		.900	.0116				
.450	.0510		.400	.0375		.500	.0325		.672	.0179							
.500	.0472		.450	.0350		.600	.0147		.771	.0041							
.550	.1281		.500	.0287		.700	.0021		.870	-.0047							
.600	.0320		.600	.0123		.800	-.0067		.915	-.0085							
.700			.700	.0010		.900											
.800			.800	-.0052		.940	-.0130										
.900			.900	-.0127													
.940	.0042		.940	-.0140													

TABLE B-12.- Continued

(g) $\alpha = -0.15^{o}$

Cp at 2y/b of:																	
0.00			0.20			0.40			0.60			0.80			0.95		
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower
.024			.016	.0899		.024			.055			.107	.0479		.194		
.050	.0381		.028	.0470		.050	.0994		.100	.0550		.160	.0429		.246	.0366	
.076			.052	.0692		.072	.0616		.146	.0550		.208	.0416		.362	.0279	
.100			.077	.0579		.100	.0553		.190	.0525		.306			.450	.0203	
.150	.0419		.100	.0553		.150	.0740		.240	.0500		.403	.0304		.640	.0091	
.200	.0419		.150	.0453		.200	.0550		.284	.0449		.503	.0304		.850	.0028	
.250	.0419		.200	.0390		.250			.330	.0386		.600	.0078				
.300	.0394		.250	.0327		.300	.0449		.374			.700	-.0021				
.350	.0381		.300	.0226		.350	.0335		.473	.0329		.800	-.0096				
.400			.350	.0138		.400	.0209		.572	.0091		.900	-.0146				
.450	.0280		.400	.0113		.500	.0057		.672	-.0034							
.500	.0243		.450	.0087		.600	-.0119		.771	-.0146							
.550	.0003		.500	.0050		.700	-.0220		.870	-.0221							
.600	.0078		.600	-.0113		.800	-.0296		.915	-.0259							
.700			.700	-.0201		.900											
.800			.800	-.0239		.940	-.0334										
.900			.900	-.0315													
.940	-.0148		.940	-.0340													

TABLE B-12.- Continued

(h) $\alpha = 1.86^{o}$

Cp at 2y/b of:																	
0.00			0.20			0.40			0.60			0.80			0.95		
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower
.024			.016	.0470		.024			.055			.107	.0164		.134		
.050	.0129		.028	.0167		.050	.0534		.100	.0158		.160	.0089		.246	-.0185	
.076			.052	.0295		.072	.0232		.146	.0120		.208	.0051		.362	-.0048	
.100			.077	.0207		.100	.0207		.190	.0120		.306			.450	-.0098	
.150	.0167		.100	.0182		.150	.0386		.240	.0107		.403	-.0035		.640	-.0210	
.200	.0167		.150	.0157		.200	.0171		.284	.0082		.503	-.0123		.850	-.0223	
.250	.0167		.200	.0119		.250			.330	.0044		.600	-.0223				
.300	.0167		.250	.0069		.300	.0095		.374			.700	-.0311				
.350	.0142		.300	-.0005		.350	.0032		.473	.0051		.800	-.0373				
.400	.1240		.350	-.0080		.400	-.0069		.572	-.0223		.900	-.0398				
.450	.0053		.400	-.0105		.500	-.0208		.672	-.0323							
.500	.0015		.450	-.0131		.600	-.0347		.771	-.0398							
.550	.0571		.500	-.0168		.700	-.0436		.870	-.0448							
.600	-.0110		.600	-.0294		.800	-.0499		.915	-.0473							
.700			.700	-.0357		.900											
.800			.800	-.0407		.940	-.0524										
.900			.900	-.0470													
.940	-.0324		.940	-.0482													

TABLE B-12.- Continued

(i) $\alpha = 3.86^{o}$

Cp at 2y/b of:																	
0.00			0.20			0.40			0.60			0.80			0.95		
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower
.024			.016	.0092		.024			.055			.107	-.0147		.194		
.050	-.0072		.028	-.0109		.050	-.0064		.100	-.0133		.160	-.0185		.246	-.0448	
.076			.052	-.0014		.072	-.0102		.146	-.0146		.208	-.0210		.362	-.0323	
.100			.077	-.0127		.100	-.0114		.190	-.0184		.306			.450	-.0360	
.150	-.0046		.100	-.0140		.150	.0093		.240	-.0209		.403	-.0323		.640	-.0460	
.200	-.0046		.150	-.0140		.200	-.0146		.284	-.0209		.503	-.0410		.850	-.0473	
.250	-.0021		.200	-.0165		.250			.330	-.0247		.600	-.0485				
.300	-.0034		.250	-.0190		.300	-.0209		.374			.700	-.0560				
.350	-.0046		.300	-.0253		.350	-.0259		.473	-.0198		.800	-.0611				
.400	.1266		.350	-.0303		.400	-.0335		.572	-.0473		.900	-.0636				
.450	-.0122		.400	-.0328		.500	-.0436		.672	-.0560							
.500	-.0173		.450	-.0341		.600	-.0550		.771	-.0623							
.550	.0559		.500	-.0366		.700	-.0613		.870	-.0686							
.600	-.0274		.600	-.0467		.800	-.0664		.915	-.0698							
.700			.700	-.0530		.900											
.800			.800	-.0567		.940	-.0689										
.900			.900	-.0618													
.940	-.0476		.940	-.0655													

TABLE B-12.- Continued

(j) $\alpha = 5.85^{o}$

Cp at 2y/b of:																	
0.00			0.20			0.40			0.60			0.80			0.95		
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower
.024			.016	-.0210		.024			.055			.107	-.0454		.194		
.050	-.0248		.028	-.0412		.050	-.0341		.100	-.0408		.160	-.0492		.246	-.0592	
.076			.052	-.0278		.072	-.0378		.146	-.0408		.208	-.0492		.362	-.0605	
.100			.077	-.0403		.100	-.0403		.190	-.0434		.306			.450	-.0655	
.150	-.0197		.100	-.0403		.150	-.0155		.240	-.0446		.403	-.0630		.640	-.0743	
.200	-.0210		.150	-.0416		.200	-.0408		.284	-.0484		.503	-.0693		.850	-.0743	
.250	-.0197		.200	-.0416		.250			.330	-.0510		.600	-.0756				
.300	-.0197		.250	-.0441		.300	-.0484		.374			.700	-.0819				
.350	-.0223		.300	-.0492		.350	-.0522		.473	-.0466		.800	-.0869				
.400	.1317		.350	-.0517		.400	-.0586		.572	-.0466		.900	-.0907				
.450	-.0286		.400	-.0529		.500	-.0662		.672	-.0819							
.500	-.0336		.450	-.0517		.600	-.0738		.771	-.0882							
.550	.0547		.500	-.0542		.700	-.0801		.870	-.0920							
.600	-.0412		.600	-.0617		.800	-.0852		.915	-.0932							
.700			.700	-.0668		.900											
.800			.800	-.0706		.940	-.0839										
.900			.900	-.0756													
.940	-.0602		.940	-.0781													

TABLE B-12.- Continued

(k) $\alpha = 7.85^{o}$

Cp at 2y/b of:																	
0.00			0.20			0.40			0.60			0.80			0.95		
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower
.024			.016	-.0475		.024			.055			.107	-.0737		.194		
.050	-.0400		.028	-.0652		.050	-.0531		.100	-.0611		.160	-.0788		.246	-.0876	
.076			.052	-.0455		.072	-.0606		.146	-.0624		.208	-.0788		.362	-.0876	
.100			.077	-.0606		.100	-.0606		.190	-.0636		.306			.450	-.0902	
.150	-.0349		.100	-.0631		.150	-.0345		.240	-.0662		.403	-.0902		.640	-.0991	
.200	-.0362		.150	-.0644		.200	-.0624		.284	-.0687		.503	-.0952		.850	-.0991	
.250	-.0349		.200	-.0644		.250			.330	-.0725		.600	-.1016				
.300	-.0362		.250	-.0669		.300	-.0700		.374			.700	-.1079				
.350	-.0387		.300	-.0681		.350	-.0750		.473	-.0711		.800	-.1117				
.400	.1393		.350	-.0694		.400	-.0801		.572	-.1029		.900	-.1079				
.450	-.0425		.400	-.0694		.500	-.0864		.672	-.1092							
.500	-.0475		.450	-.0669		.600	-.0928		.771	-.1130							
.550	.0534		.500	-.0669		.700	-.0979		.870	-.1168							
.600	-.0539		.600	-.0732		.800	-.1004		.915	-.1181							
.700			.700	-.0782		.900											
.800			.800	-.0807		.940	-.0991										
.900			.900	-.0858													
.940	-.0715		.940	-.0883													

TABLE B-12.- Continued

(l) $\alpha = 9.86^{o}$

Cp at 2y/b of:																	
0.00			0.20			0.40			0.60			0.80			0.95		
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower
.024			.016	-.0716		.024			.055			.107	-.0918		.194		
.050	-.0539		.028	-.0804		.050	-.0769		.100	-.0802		.160	-.0918		.246	-.0968	
.076			.052	-.0656		.072	-.0781		.146	-.0815		.208	-.0905		.362	-.0993	
.100			.077	-.0819		.100	-.0794		.190	-.0828		.306			.450	-.1019	
.150	-.0463		.100	-.0832		.150	-.0511		.240	-.0840		.403	-.1006		.640	-.1082	
.200	-.0476		.150	-.0844		.200	-.0790		.284	-.0866		.503	-.1069		.850	-.1069	
.250	-.0488		.200	-.0844		.250			.330	-.0891		.600	-.1120				
.300	-.0501		.250	-.0844		.300	-.0878		.374			.700	-.1170				
.350	-.0526		.300	-.0870		.350	-.0916		.473	-.0817		.800	-.1183				
.400	.1480		.350	-.0895		.400	-.0954		.572	-.1120		.900	-.1069				
.450	-.0539		.400	-.0895		.500	-.1017		.672	-.1183							
.500	-.0602		.450	-.0882		.600	-.1081		.771	-.1221							
.550	.0521		.500	-.0870		.700	-.1119		.870	-.1132							
.600	-.0640		.600	-.0882		.800	-.1131		.915	-.1107							
.700			.700	-.0907		.900											
.800			.800	-.0932		.940	-.1093										
.900			.900	-.0958													
.940	-.0804		.940	-.0995													

TABLE B-12.- Concluded

(m) $\alpha = 13.84^{o}$

Cp at 2y/b of:																	
0.00			0.20			0.40			0.60			0.80			0.95		
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower
.024			.016	-.1095		.024			.055			.107	-.1434		.194		
.050	-.0754		.028	-.1095		.050	-.1222		.100	-.1157		.160	-.1396		.246	-.1459	
.076			.052	-.0907		.072	-.1108		.146	-.1119		.208	-.1268		.362	-.1434	
.100			.077	-.1096		.100	-.1108		.190	-.1119		.306			.450	-.1421	
.150	-.0653		.100	-.1108		.150	-.0765		.240	-.1119		.403	-.1370		.640	-.1421	
.200	-.0703		.150	-.1133		.200	-.1068		.284	-.1144		.503	-.1408		.850	-.1357	
.250	-.0703		.200	-.1108		.250			.330	-.1144		.600	-.1447				
.300	-.0703		.250	-.1108		.300	-.1131		.374			.700	-.1447				
.350	-.0716		.300	-.1108		.350	-.1157		.473	-.1115		.800	-.1370				
.400	.1681		.350	-.1133		.400	-.1195		.572	-.1434		.900	-.1332				
.450	-.0716		.400	-.1133		.500	-.1220		.672	-.1459							
.500	-.0792		.450	-.1133		.600	-.1271		.771	-.1396							
.550	-.0034		.500	-.1146		.700	-.1258		.870	-.1383							
.600	-.0817		.600	-.1184		.800	-.1245		.915	-.1370							
.700			.700	-.1209		.900											
.800			.800	-.1209		.940	-.1093										
.900			.900	-.1222													
.940	-.0918		.940	-.1259													

TABLE B-13.- PRESSURE COEFFICIENTS FOR WING WITH 55° SWEEP, $C_{L,des} = 0.0$, M = 3.5

(a) $\alpha = -14.40°$

Cp at 2y/b of:																	
0.00			0.20			0.40			0.60			0.80			0.95		
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower
.024			.016	.4765		.024			.055			.107	.4610		.194		
.050	.2670		.028	.4485		.050	.4263		.100	.4275		.160	.4376		.246	.4552	
.076			.052	.3676		.072	.4204		.146	.4024		.208	.4113		.362	.4186	
.100			.077	.3441		.100	.3867		.190	.3832		.306			.450	.3894	
.150	.2729		.100	.3294		.150	.3728		.240	.3625		.403	.3470		.640	.3484	
.200	.2788		.150	.3074		.200	.3492		.284	.3462		.503	.3177		.850	.3089	
.250	.2803		.200	.2957		.250			.330	.3299		.600	.2899				
.300	.2803		.250	.2839		.300	.3063		.374			.700	.2665				
.350	.2803		.300	.2649		.350	.2856		.473	.2855		.800	.2461				
.400			.350	.2517		.400	.2619		.572	.2724		.900	.2300				
.450	.2522		.400	.2473		.500	.2368		.672	.2256							
.500	.2493		.450	.2399		.600	.2102		.771	.2036							
.550	.1932		.500	.2267		.700	.1895		.870	.1890							
.600	.2183		.600	.1974		.800	.1687		.915	.1817							
.700			.700	.1798		.900											
.800			.800	.1651		.940	.1569										
.900			.900	.1504													
.940	.1740		.940	.1489													

TABLE B-13.- Continued

(b) $\alpha = -10.30^{o}$

Cp at 2y/b of:																	
0.00			0.20			0.40			0.60			0.80			0.95		
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower
.024			.016	.3733		.024			.055	.2492		.107	.3052		.194		
.050	.1830		.028	.2849		.050	.2987		.100	.3025		.160	.2891		.246	.2744	
.076			.052	.2692		.072	.2987		.146	.2862		.208	.2788		.362	.2657	
.100			.077	.2442		.100	.2766		.190	.2744		.306			.450	.2495	
.150	.1874		.100	.2324		.150	.2758		.240	.2595		.403	.2408		.640	.2276	
.200	.1904		.150	.2147		.200	.2536		.284	.2492		.503	.2202		.850	.2012	
.250	.1919		.200	.2015		.250			.330	.2358		.600	.1968				
.300	.1919		.250	.1912		.300	.2181		.374			.700	.1778				
.350	.1904		.300	.1750		.350	.1988		.473	.2012		.800	.1617				
.400			.350	.1632		.400	.1796		.572	.1924		.900	.1485				
.450	.1682		.400	.1588		.500	.1559		.672	.1455							
.500	.1653		.450	.1529		.600	.1307		.771	.1265							
.550	.1919		.500	.1440		.700	.1129		.870	.1133							
.600	.1461		.600	.1175		.800	.0981		.915	.1075							
.700			.700	.1013		.900											
.800	.1476		.800	.0910		.940	.0877										
.900	.1033		.900	.0792													
.940	.1048		.940	.0778													

TABLE B-13.- Continued

(c) $\alpha = -8.39^{o}$

Cp at 2y/b of:																	
0.00			0.20			0.40			0.60			0.80			0.95		
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower
.024			.016	.3022		.024			.055	.1731		.107	.2218		.134		
.050	.1429		.028	.2639		.050	.2347		.100	.2366		.160	.2144		.246	.1938	
.076			.052	.2273		.072	.2479		.146	.2277		.208	.2056		.362	.1806	
.100			.077	.2067		.100	.2303		.190	.2218		.306			.450	.1732	
.150	.1488		.100	.1950		.150	.2337		.240	.2100		.403	.1865		.640	.1585	
.200	.1518		.150	.1759		.200	.2071		.284	.2026		.503	.1688		.850	.1423	
.250	.1532		.200	.1656		.250			.330	.1923		.600	.1482				
.300	.1518		.250	.1568		.300	.1775		.374			.700	.1335				
.350	.1503		.300	.1406		.350	.1598		.473	.1615		.800	.1188				
.400			.350	.1288		.400	.1420		.572	.1585		.900	.1085				
.450	.1341		.400	.1229		.500	.1198		.672	.1070							
.500	.1296		.450	.1185		.600	.0962		.771	.0894							
.550	.1916		.500	.1097		.700	.0799		.870	.0761							
.600	.1090		.600	.0891		.800	.0681		.915	.0702							
.700			.700	.0744		.900											
.800	.1473		.800	.0656		.940	.0592										
.900	.0736		.900	.0553													
.940	.0736		.940	.0539													

TABLE B-13.- Continued

(d) α = -6.39°

Cp at 2y/b of:																	
0.00			0.20			0.40			0.60			0.80			0.95		
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower
.024			.016	.2197		.024			.055	.1394		.107	.1721		.194		
.050	.1120		.028	.1917		.050	.1745		.100	.1765		.160	.1530		.246	.1398	
.076			.052	.1848		.072	.1848		.146	.1691		.208	.1516		.362	.1296	
.100			.077	.1701		.100	.1760		.190	.1646		.306			.450	.1222	
.150	.1165		.100	.1583		.150	.1898		.240	.1572		.403	.1340		.640	.1091	
.200	.1179		.150	.1422		.200	.1676		.284	.1557		.503	.1222		.850	.0959	
.250	.1194		.200	.1304		.250			.330	.1468		.600	.1076				
.300	.1194		.250	.1216		.300	.1409		.374			.700	.0944				
.350	.1165		.300	.1069		.350	.1261		.473	.1325		.800	.0856				
.400			.350	.0951		.400	.1098		.572	.1296		.900	.0768				
.450	.1017		.400	.0907		.500	.0876		.672	.0797							
.500	.0973		.450	.0848		.600	.0669		.771	.0651							
.550	.1302		.500	.0789		.700	.0521		.870	.0534							
.600	.0811		.600	.0598		.800	.0417		.915	.0490							
.700			.700	.0466		.900											
.800	.1460		.800	.0407		.940	.0329										
.900	.0486		.900	.0304													
.940	.0486		.940	.0275													

TABLE B-13.- Continued

(e) $\alpha = -4.39^{o}$

Cp at 2y/b of:																	
0.00			0.20			0.40			0.60			0.80			0.95		
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower
.024			.016	.1623		.024			.055	.1023		.107	.1148		.194		
.050	.0841		.028	.1180		.050	.1290		.100	.1186		.160	.1089		.246	.0957	
.076			.052	.1423		.072	.1305		.146	.1200		.208	.1030		.362	.0869	
.100			.077	.1290		.100	.1231		.190	.1156		.306			.450	.0781	
.150	.0856		.100	.1217		.150	.1452		.240	.1126		.403	.0913		.640	.0664	
.200	.0856		.150	.1070		.200	.1245		.284	.1097		.503	.0796		.850	.0547	
.250	.0885		.200	.0952		.250			.330	.1008		.600	.0664				
.300	.0885		.250	.0878		.300	.1052		.374			.700	.0562				
.350	.0856		.300	.0761		.350	.0919		.473	.0957		.800	.0474				
.400			.350	.0658		.400	.0786		.572	.0943		.900	.0415				
.450	.0723		.400	.0599		.500	.0594		.672	.0503							
.500	.0678		.450	.0555		.600	.0401		.771	.0386							
.550	.1889		.500	.0511		.700	.0283		.870	.0283							
.600	.0531		.600	.0349		.800	.0165		.915	.0239							
.700			.700	.0246		.900											
.800	.1461		.800	.0172		.940	.0091										
.900	.0265		.900	.0084													
.940	.0250		.940	.0054													

TABLE B-13.- Continued

(f) $\alpha = -2.39^{o}$

Cp at 2y/b of:																	
0.00			0.20			0.40			0.60			0.80			0.95		
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower
.024			.016	.1135		.024			.055	.0680		.107	.0766		.134		
.050	.0574		.028	.0810		.050	.0846		.100	.0783		.160	.0649		.246	.0605	
.076			.052	.0934		.072	.0904		.146	.0724		.208	.0649		.362	.0532	
.100			.077	.0846		.100	.0816		.190	.0739		.306			.450	.0444	
.150	.0589		.100	.0816		.150	.1049		.240	.0709		.403	.0546		.640	.0327	
.200	.0559		.150	.0757		.200	.0812		.284	.0680		.503	.0444		.850	.0209	
.250	.0604		.200	.0669		.250			.330	.0650		.600	.0327				
.300	.0604		.250	.0596		.300	.0709		.374			.700	.0239				
.350	.0574		.300	.0478		.350	.0620		.473	.0649		.800	.0166				
.400			.350	.0376		.400	.0488		.572	.0634		.900	.0107				
.450	.0471		.400	.0332		.500	.0325		.672	.0224							
.500	.0427		.450	.0302		.600	.0163		.771	.0122							
.550	.1858		.500	.0258		.700	.0030		.870	.0048							
.600	.0323		.600	.0111		.800	-.0058		.915	.0019							
.700			.700	.0023		.900	-.0087										
.800	.1459		.800	-.0035		.940	-.0102										
.900	.0073		.900	-.0108													
.940	.0058		.940	-.0137													

TABLE B-13.- Continued

(g) $\alpha = -0.11^{o}$

Cp at 2y/b of:																	
0.00			0.20			0.40			0.60			0.80			0.95		
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower
.024			.016	.0678		.024			.055			.107	.0373		.194		
.050	.0295		.028	.0398		.050	.0463		.100	.0400		.160	.0270		.246	.0241	
.076			.052	.0551		.072	.0463		.146	.0370		.208	.0256		.362	.0168	
.100			.077	.0433		.100	.0419		.190	.0340		.306			.450	.0109	
.150	.0324		.100	.0419		.150	.0680		.240	.0296		.403	.0138		.640	.0006	
.200	.0295		.150	.0404		.200	.0400		.284	.0296		.503	.0080		.850	-.0066	
.250	.0309		.200	.0360		.250			.330	.0267		.600	-.0007				
.300	.0309		.250	.0301		.300	.0326		.374			.700	-.0095				
.350	.0295		.300	.0213		.350	.0267		.473	.0329		.800	-.0154				
.400			.350	.0125		.400	.0178		.572	.0226		.900	-.0198				
.450	.0221		.400	.0096		.500	.0075		.672	-.0110							
.500	.0176		.450	.0066		.600	-.0072		.771	-.0183							
.550	.0649		.500	.0037		.700	-.0176		.870	-.0227							
.600	.0058		.600	-.0094		.800	-.0250		.915	-.0257							
.700			.700	-.0168		.900											
.800			.800	-.0212		.940	-.0309										
.900			.900	-.0270													
.940	-.0133		.940	-.0314													

TABLE B-13.- Continued

(h) $\alpha = 1.61^{o}$

Cp at 2y/b of:																	
0.00			0.20			0.40			0.60			0.80			0.95		
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower
.024			.016	.0397		.024	.0479		.055	.0076		.107	.0122		.194		
.050	-.0132		.028	.0206		.050	.0214		.100	-.0135		.160	-.0063		.246	-.0049	
.076			.052	.0302		.072	.0200		.146	-.0120		.208	-.0078		.362	-.0024	
.100			.077	.0170		.100	.0170		.190	-.0090		.306			.450	-.0068	
.150	-.0147		.100	.0155		.150	.0445		.240	-.0076		.403	-.0068		.640	-.0170	
.200	-.0132		.150	.0155		.200	.0164		.284	-.0031		.503	-.0126		.850	-.0272	
.250	-.0132		.200	.0111		.250			.330	-.0016		.600	-.0199				
.300	-.0147		.250	.0082		.300	.0061		.374			.700	-.0272				
.350	-.0147		.300	.0009		.350	.0016		.473	-.0151		.800	-.0331				
.400			.350	-.0049		.400	-.0057		.572	-.0136		.900	-.0375				
.450	-.0073		.400	-.0093		.500	-.0130		.672	-.0272							
.500	-.0029		.450	-.0108		.600	-.0249		.771	-.0331							
.550	-.0929		.500	-.0137		.700	-.0337		.870	-.0390							
.600	-.0044		.600	-.0240		.800	-.0411		.915	-.0404							
.700			.700	-.0299		.900	-.0441										
.800	-.1460		.800	-.0343		.940	-.0441										
.900	-.0221		.900	-.0402													
.940	-.0251		.940	-.0431													

TABLE B-13.- Continued

(i) $\alpha = 3.61^{o}$

Cp at 2y/b of:																	
0.00			0.20			0.40			0.60			0.80			0.95		
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower
.024			.016	-.0102		.024	-.0170		.055	-.0175		.107	-.0126		.194		
.050	-.0059		.028	-.0059		.050	-.0035		.100	-.0116		.160	-.0141		.246	-.0185	
.076			.052	.0096		.072	-.0050		.146	-.0131		.208	-.0141		.362	-.0243	
.100			.077	-.0079		.100	-.0079		.190	-.0131		.306			.450	-.0287	
.150	-.0015		.100	-.0094		.150	.0223		.240	-.0160		.403	-.0273		.640	-.0375	
.200	-.0045		.150	-.0108		.200	-.0101		.284	-.0190		.503	-.0346		.850	-.0434	
.250	-.0045		.200	-.0108		.250			.330	-.0219		.600	-.0419				
.300	-.0030		.250	-.0138		.300	-.0175		.374			.700	-.0463				
.350	-.0045		.300	-.0196		.350	-.0234		.473	-.0039		.800	-.0507				
.400			.350	-.0270		.400	-.0293		.572	-.0141		.900	-.0536				
.450	-.0074		.400	-.0285		.500	-.0353		.672	-.0463							
.500	-.0133		.450	-.0299		.600	-.0426		.771	-.0522							
.550	.0928		.500	-.0314		.700	-.0486		.870	-.0566							
.600	-.0192		.600	-.0402		.800	-.0560		.915	-.0580							
.700			.700	-.0446		.900	-.0589										
.800	.1459		.800	-.0475		.940	-.0574										
.900	-.0354		.900	-.0519													
.940	-.0384		.940	-.0549													

TABLE B-13.- Continued

(j) $\alpha = 5.61^{o}$

Cp at 2y/b of:																		
0.00			0.20			0.40			0.60			0.80			0.95		
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower
.024			.016	-.0133		.024	-.0120		.055	-.0382		.107	-.0330		.194		
.050	-.0207		.028	-.0266		.050	-.0311		.100	-.0308		.160	-.0360		.246	-.0389	
.076			.052	-.0149		.072	-.0311		.146	-.0338		.208	-.0316		.362	-.0448	
.100			.077	-.0326		.100	-.0341		.190	-.0338		.306			.450	-.0477	
.150	-.0163		.100	-.0355		.150	-.0031		.240	-.0353		.403	-.0477		.640	-.0550	
.200	-.0192		.150	-.0370		.200	-.0293		.284	-.0382		.503	-.0536		.850	-.0594	
.250	-.0177		.200	-.0370		.250			.330	-.0397		.600	-.0594				
.300	-.0177		.250	-.0400		.300	-.0382		.374			.700	-.0638				
.350	-.0192		.300	-.0444		.350	-.0427		.473	-.0213		.800	-.0667				
.400			.350	-.0473		.400	-.0471		.572	-.0228		.900	-.0580				
.450	-.0222		.400	-.0488		.500	-.0530		.672	-.0624							
.500	-.0266		.450	-.0488		.600	-.0604		.771	-.0682							
.550	.0898		.500	-.0517		.700	-.0648		.870	-.0711							
.600	-.0310		.600	-.0562		.800	-.0678		.915	-.0653							
.700			.700	-.0606		.900	-.0722										
.800	.1488		.800	-.0621		.940	-.0707										
.900	-.0458		.900	-.0665													
.940	-.0502		.940	-.0694													

TABLE B-13.- Continued

(k) $\alpha = 7.61^{o}$

Cp at 2y/b of:																	
0.00			0.20			0.40			0.60			0.80			0.95		
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower
.024			.016	-.0339		.024	-.0299		.055	-.0530		.107	-.0505		.194		
.050	-.0339		.028	-.0472		.050	-.0416		.100	-.0485		.160	-.0535		.246	-.0564	
.076			.052	-.0269		.072	-.0460		.146	-.0500		.208	-.0476		.362	-.0608	
.100			.077	-.0475		.100	-.0475		.190	-.0500		.306			.450	-.0637	
.150	-.0295		.100	-.0475		.150	-.0130		.240	-.0530		.403	-.0637		.640	-.0711	
.200	-.0310		.150	-.0490		.200	-.0471		.284	-.0544		.503	-.0681		.850	-.0667	
.250	-.0310		.200	-.0490		.250			.330	-.0559		.600	-.0740				
.300	-.0310		.250	-.0519		.300	-.0530		.374			.700	-.0769				
.350	-.0324		.300	-.0549		.350	-.0574		.473	-.0358		.800	-.0755				
.400			.350	-.0563		.400	-.0618		.572	-.0358		.900	-.0667				
.450	-.0324		.400	-.0593		.500	-.0648		.672	-.0769							
.500	-.0398		.450	-.0593		.600	-.0722		.771	-.0799							
.550	.0885		.500	-.0622		.700	-.0766		.870	-.0740							
.600	-.0413		.600	-.0651		.800	-.0796		.915	-.0711							
.700			.700	-.0681		.900	-.0722										
.800	.1519		.800	-.0710		.940	-.0692										
.900	-.0531		.900	-.0725													
.940	-.0590		.940	-.0769													

TABLE B-13.- Continued

(l) $\alpha = 9.61^{o}$

Cp at 2y/b of:

0.00			0.20			0.40			0.60			0.80			0.95		
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower
.024			.016	-.0501		.024	-.0461		.055	-.0648		.107	-.0638		.194		
.050	-.0471		.028	-.0619		.050	-.0578		.100	-.0619		.160	-.0667		.246	-.0682	
.076			.052	-.0372		.072	-.0593		.146	-.0633		.208	-.0579		.362	-.0711	
.100			.077	-.0607		.100	-.0622		.190	-.0648		.306			.450	-.0741	
.150	-.0398		.100	-.0622		.150	-.0249		.240	-.0663		.403	-.0755		.640	-.0799	
.200	-.0412		.150	-.0637		.200	-.0589		.284	-.0678		.503	-.0785		.850	-.0726	
.250	-.0412		.200	-.0622		.250			.330	-.0678		.600	-.0829				
.300	-.0427		.250	-.0637		.300	-.0678		.374			.700	-.0843				
.350	-.0457		.300	-.0652		.350	-.0707		.473	-.0433		.800	-.0785				
.400			.350	-.0681		.400	-.0737		.572	-.0638		.900	-.0741				
.450	-.0442		.400	-.0681		.500	-.0752		.672	-.0843							
.500	-.0501		.450	-.0696		.600	-.0826		.771	-.0829							
.550	.0657		.500	-.0710		.700	-.0811		.870	-.0799							
.600	-.0516		.600	-.0769		.800	-.0766		.915	-.0770							
.700			.700	-.0784		.900	-.0752										
.800	.1551		.800	-.0813		.940	-.0752										
.900	-.0619		.900	-.0813													
.940	-.0693		.940	-.0828													

TABLE B-13.- Concluded

(m) $\alpha = 13.61^{o}$

Cp at 2y/b of:																	
0.00			0.20			0.40			0.60			0.80			0.95		
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower
.024			.016	-.0723		.024	-.0725		.055	-.0825		.107	-.0814		.194		
.050	-.0634		.028	-.0797		.050	-.0813		.100	-.0811		.160	-.0829		.246	-.0844	
.076			.052	-.0563		.072	-.0798		.146	-.0811		.208	-.0697		.362	-.0844	
.100			.077	-.0798		.100	-.0828		.190	-.0825		.306			.450	-.0858	
.150	-.0531		.100	-.0828		.150	-.0426		.240	-.0840		.403	-.0873		.640	-.0902	
.200	-.0575		.150	-.0857		.200	-.0781		.284	-.0855		.503	-.0888		.850	-.0829	
.250	-.0605		.200	-.0828		.250			.330	-.0870		.600	-.0932				
.300	-.0605		.250	-.0842		.300	-.0855		.374			.700	-.0902				
.350	-.0619		.300	-.0857		.350	-.0899		.473	-.0566		.800	-.0873				
.400			.350	-.0872		.400	-.0899		.572	-.0654		.900	-.0858				
.450	-.0590		.400	-.0857		.500	-.0899		.672	-.0888							
.500	-.0649		.450	-.0872		.600	-.0929		.771	-.0873							
.550	.0826		.500	-.0872		.700	-.0885		.870	-.0888							
.600	-.0649		.600	-.0931		.800	-.0885		.915	-.0873							
.700			.700	-.0931		.900	-.0899										
.800	.1638		.800	-.0931		.940	-.0885										
.900	-.0605		.900	-.0886													
.940	-.0664		.940	-.0901													

TABLE B-14.- PRESSURE COEFFICIENTS FOR WING WITH 55° SWEEP,

$C_{L,des} = 0.0$, $M = 4.0$

(a) $\alpha = -13.90°$

Cp at 2y/b of:																		
0.00			0.20			0.40			0.60			0.80			0.95			
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	
.024			.016	.4461		.024			.055			.107	.3731		.194			
.050	.2412		.028	.3552		.050	.4064		.100	.3616		.160	.3665		.246	.3583		
.076			.052	.3323		.072	.3669		.146	.3484		.208	.3501		.362	.3436		
.100			.077	.3059		.100	.3389		.190	.3335		.306			.450	.3239		
.150	.2478		.100	.2928		.150	.3351		.240	.3169		.403	.3058		.640	.2944		
.200	.2511		.150	.2747		.200	.3086		.284	.3053		.503	.2812		.850	.2763		
.250	.2544		.200	.2598		.250			.330	.2937		.600	.2583					
.300	.2527		.250	.2483		.300	.2705		.374			.700	.2370					
.350	.2494		.300	.2318		.350	.2522		.473	.2616		.800	.2189					
.400			.350	.2170		.400	.2323		.572	.2599		.900	.2058					
.450	.2230		.400	.2104		.500	.2074		.672	.1993								
.500	.2180		.450	.2038		.600	.1809		.771	.1796								
.550	.0660		.500	.1939		.700	.1627		.870	.1648								
.600	.1866		.600	.1676		.800	.1461		.915	.1599								
.700			.700	.1511		.900												
.800			.800	.1396		.940	.1345											
.900			.900	.1281														
.940	.1519		.940	.1248														

TABLE B-14.- Continued

(b) α = -9.94°

Cp at 2y/b of:																	
0.00			0.20			0.40			0.60			0.80			0.95		
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower
.024			.016	.2825		.024			.055			.107	.2390		.194		
.050	.1585		.028	.2610		.050	.2611		.100	.2340		.160	.2193		.246	.2045	
.076			.052	.2348		.072	.2381		.146	.2273		.208	.2160		.362	.1963	
.100			.077	.2183		.100	.2282		.190	.2224		.306			.450	.1848	
.150	.1668		.100	.2068		.150	.2456		.240	.2141		.403	.1947		.640	.1684	
.200	.1668		.150	.1903		.200	.2207		.284	.2108		.503	.1799		.850	.1536	
.250	.1668		.200	.1772		.250			.330	.2025		.600	.1635				
.300	.1651		.250	.1673		.300	.1942		.374			.700	.1487				
.350	.1618		.300	.1525		.350	.1776		.473	.1848		.800	.1372				
.400			.350	.1393		.400	.1594		.572	.1848		.900	.1290				
.450	.1470		.400	.1344		.500	.1362		.672	.1290							
.500	.1437		.450	.1295		.600	.1113		.771	.1126							
.550	.0677		.500	.1229		.700	.0964		.870	.1011							
.600	.1255		.600	.1015		.800	.0848		.915	.0945							
.700			.700	.0867		.900											
.800			.800	.0785		.940	.0748										
.900			.900	.0702													
.940	.0908		.940	.0670													

TABLE B-14.- Continued

(c) α = -7.94°

Cp at 2y/b of:																				
0.00			0.20			0.40			0.60			0.80			0.95		
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower
.024			.016	.2130		.024			.055			.107	.1624		.194		
.050	.1238		.028	.1800		.050	.2150		.100	.1740		.160	.1557		.246	.1441	
.076			.052	.1936		.072	.1903		.146	.1723		.208	.1475		.362	.1342	
.100			.077	.1739		.100	.1755		.190	.1706		.306			.450	.1243	
.150	.1271		.100	.1689		.150	.1988		.240	.1657		.403	.1342		.640	.1077	
.200	.1271		.150	.1525		.200	.1756		.284	.1624		.503	.1210		.850	.0961	
.250	.1304		.200	.1426		.250			.330	.1557		.600	.1044				
.300	.1304		.250	.1344		.300	.1541		.374			.700	.0928				
.350	.1288		.300	.1196		.350	.1408		.473	.1375		.800	.0829				
.400	.1701		.350	.1081		.400	.1259		.572	.1011		.900	.0763				
.450	.1155		.400	.1015		.500	.1044		.672	.0845							
.500	.1106		.450	.0982		.600	.0845		.771	.0696							
.550	.0693		.500	.0916		.700	.0680		.870	.0597							
.600	.0908		.600	.0735		.800	.0564		.915	.0547							
.700			.700	.0620		.900											
.800			.800	.0538		.940	.0498										
.900			.900	.0455													
.940	.0643		.940	.0423													

TABLE B-14.- Continued

(d) α = -5.94°

Cp at 2y/b of:																	
0.00			0.20			0.40			0.60			0.80			0.95		
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower
.024			.016	-.1634		.024			.055			.107	-.1336		.194		
.050	-.0324		.028	-.1271		.050	-.1607		.100	-.1262		.160	-.1238		.246	-.1139	
.076			.052	-.1426		.072	-.1409		.146	-.1262		.208	-.1221		.362	-.1057	
.100			.077	-.1311		.100	-.1311		.190	-.1262		.306			.450	-.0959	
.150	-.0957		.100	-.1311		.150	-.1543		.240	-.1245		.403	-.1025		.640	-.0812	
.200	-.0940		.150	-.1228		.200	-.1295		.284	-.1228		.503	-.0926		.850	-.0664	
.250	-.1007		.200	-.1113		.250			.330	-.1145		.600	-.0812				
.300	-.1007		.250	-.1031		.300	-.1195		.374			.700	-.0697				
.350	-.0990		.300	-.0916		.350	-.1079		.473	-.1139		.800	-.0615				
.400	-.1684		.350	-.0784		.400	-.0947		.572	-.1025		.900	-.0549				
.450	-.0858		.400	-.0735		.500	-.0781		.672	-.0664							
.500	-.0825		.450	-.0702		.600	-.0582		.771	-.0549							
.550	-.0709		.500	-.0653		.700	-.0449		.870	-.0467							
.600	-.0676		.600	-.0488		.800	-.0333		.915	-.0418							
.700			.700	-.0373		.900											
.800			.800	-.0324		.940	-.0267										
.900			.900	-.0242													
.940	-.0412		.940	-.0209													

TABLE B-14.- Continued

(e) $\alpha = -3.94^{o}$

Cp at 2y/b of:																	
0.00			0.20			0.40			0.60			0.80			0.95		
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower
.024			.016	-.1222		.024			.055	.0845		.107	.0838		.194		
.050	-.0660		.028	-.0908		.050	-.1212		.100	.0945		.160	.0805		.246	.0722	
.076			.052	-.1081		.072	-.1015		.146	.0879		.208	.0772		.362	.0623	
.100			.077	-.0916		.100	-.0949		.190	.0862		.306			.450	.0557	
.150	-.0693		.100	-.0916		.150	-.1210		.240	.0829		.403	.0590		.640	.0426	
.200	-.0676		.150	-.0867		.200	-.0912		.284	.0829		.503	.0508		.850	.0294	
.250	-.0709		.200	-.0834		.250			.330	.0796		.600	.0393				
.300	-.0726		.250	-.0752		.300	-.0845		.374	.0746		.700	.0310				
.350	-.0693		.300	-.0653		.350	-.0763		.473	.0805		.800	.0244				
.400			.350	-.0538		.400	-.0663		.572	.0475		.900	.0195				
.450	-.0610		.400	-.0488		.500	-.0514		.672	.0294							
.500	-.0561		.450	-.0456		.600	-.0365		.771	.0195							
.550	-.0709		.500	-.0406		.700	-.0216		.870	.0145							
.600	-.0445		.600	-.0275		.800	-.0117		.915	.0112							
.700			.700	-.0176		.900											
.800			.800	-.0127		.940	-.0051										
.900			.900	-.0044													
.940	-.0214		.940	-.0011													

TABLE B-14.- Continued

(f) $\alpha = -1.96^{O}$

Cp at 2y/b of:																	
0.00			0.20			0.40			0.60			0.80			0.95		
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower
.024			.016	.0858		.024			.055	.0531		.107	.0421		.194		
.050	.0445		.028	.0610		.050	.0775		.100	.0614		.160	.0338		.246	.0268	
.076			.052	.0742		.072	.0610		.146	.0580		.208	.0387		.362	.0221	
.100			.077	.0544		.100	.0561		.190	.0564		.306			.450	.0155	
.150	.0478		.100	.0528		.150	.0912		.240	.0514		.403	.0171		.640	.0038	
.200	.0445		.150	.0528		.200	.0580		.284	.0481		.503	.0071		.850	-.0094	
.250	.0445		.200	.0495		.250			.330	.0448		.600	-.0011				
.300	.0462		.250	.0445		.300	.0514		.374	.0415		.700	-.0094				
.350	.0445		.300	.0362		.350	.0465		.473	.0421		.800	-.0144				
.400			.350	.0247		.400	.0382		.572	.0022		.900	-.0194				
.450	.0395		.400	.0197		.500	.0282		.672	-.0077							
.500	.0362		.450	.0164		.600	.0133		.771	-.0144							
.550	.0709		.500	.0131		.700	-.0034		.870	-.0210							
.600	.0280		.600	.0032		.800	-.0064		.915	-.0227							
.700			.700	-.0066		.900											
.800			.800	-.0099		.940	-.0114										
.900			.900	-.0182													
.940	.0032		.940	-.0198													

TABLE B-14.- Continued

(g) $\alpha = 0.05^{o}$

Cp at 2y/b of :																	
0.00			0.20			0.40			0.60			0.80			0.95		
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower
.024			.016	.0529		.024			.055			.107	.0320		.194		
.050	.0231		.028	.0363		.050	.0478		.100	.0332		.160	.0270		.246	.0238	
.076			.052	.0478		.072	.0312		.146	.0299		.208	.0320		.362	.0172	
.100			.077	.0279		.100	.0279		.190	.0282		.306			.450	.0106	
.150	.0264		.100	.0263		.150	.0679		.240	.0265		.403	.0123		.640	.0008	
.200	.0231		.150	.0230		.200	.0299		.284	.0216		.503	.0041		.850	-.0089	
.250	.0231		.200	.0230		.250			.330	.0199		.600	-.0040				
.300	.0248		.250	.0197		.300	.0216		.374			.700	-.0106				
.350	.0248		.300	.0114		.350	.0183		.473	.0385		.800	-.0155				
.400			.350	.0032		.400	.0116		.572	.0369		.900	-.0188				
.450	.0198		.400	-.0017		.500	.0050		.672	-.0073							
.500	.0181		.450	-.0017		.600	-.0048		.771	-.0138							
.550	.0678		.500	-.0050		.700	-.0131		.870	-.0204							
.600	.0099		.600	-.0149		.800	-.0214		.915	-.0220							
.700			.700	-.0215		.900											
.800			.800	-.0265		.940	-.0263										
.900			.900	-.0298													
.940	-.0132		.940	-.0347													

TABLE B-14.- Continued

(h) $\alpha = 2.05^{o}$

Cp at 2y/b of:																	
0.00			0.20			0.40			0.60			0.80			0.95		
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower
.024			.016	.0264		.024			.055			.107	.0074		.194		
.050	.0066		.028	.0116		.050	.0144		.100	.0085		.160	.0041		.246	.0008	
.076			.052	.0309		.072	.0111		.146	.0068		.208	.0123		.362	-.0056	
.100			.077	.0078		.100	.0078		.190	.0051		.306			.450	-.0089	
.150	.0099		.100	.0062		.150	.0466		.240	.0035		.403	-.0089		.640	-.0187	
.200	.0066		.150	.0045		.200	.0085		.284	.0002		.503	-.0155		.850	-.0269	
.250	.0049		.200	.0029		.250			.330	-.0014		.600	-.0237				
.300	.0066		.250	.0012		.300	.0002		.374			.700	-.0269				
.350	.0066		.300	-.0053		.350	-.0064		.473	.0205		.800	-.0335				
.400			.350	-.0102		.400	-.0097		.572	.0139		.900	-.0351				
.450	.0049		.400	-.0135		.500	-.0146		.672	-.0269							
.500	.0000		.450	-.0151		.600	-.0246		.771	-.0335							
.550	.0678		.500	-.0184		.700	-.0296		.870	-.0384							
.600	-.0049		.600	-.0250		.800	-.0345		.915	-.0384							
.700			.700	-.0300		.900											
.800			.800	-.0333		.940	-.0395										
.900			.900	-.0382													
.940	-.0264		.940	-.0415													

TABLE B-14.- Continued

(i) $\alpha = 4.05^{o}$

Cp at 2y/b of:																	
0.00			0.20			0.40			0.60			0.80			0.95		
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower
.024			.016	.0033		.024			.055			.107	-.0137		.194		
.050	-.0082		.028	-.0082		.050	-.0003		.100	-.0114		.160	-.0170		.246	-.0203	
.076			.052	.0111		.072	-.0086		.146	-.0131		.208	-.0072		.362	-.0252	
.100			.077	-.0102		.100	-.0135		.190	-.0131		.306			.450	-.0285	
.150	-.0049		.100	-.0135		.150	.0282		.240	-.0147		.403	-.0285		.640	-.0367	
.200	-.0082		.150	-.0135		.200	-.0098		.284	-.0197		.503	-.0334		.850	-.0416	
.250	-.0082		.200	-.0151		.250			.330	-.0214		.600	-.0400				
.300	-.0082		.250	-.0168		.300	-.0180		.374			.700	-.0433				
.350	-.0082		.300	-.0217		.350	-.0230		.473	.0042		.800	-.0482				
.400			.350	-.0267		.400	-.0280		.572	.0042		.900	-.0433				
.450	-.0098		.400	-.0300		.500	-.0313		.672	-.0416							
.500	-.0132		.450	-.0300		.600	-.0396		.771	-.0466							
.550	.0661		.500	-.0316		.700	-.0429		.870	-.0515							
.600	-.0181		.600	-.0398		.800	-.0495		.915	-.0482							
.700			.700	-.0431		.900											
.800			.800	-.0464		.940	-.0495										
.900			.900	-.0481													
.940	-.0363		.940	-.0514													

TABLE B-14.- Continued

(j) $\alpha = 6.06^{o}$

Cp at 2y/b of:																	
0.00			0.20			0.40			0.60			0.80			0.95		
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower
.024			.016	-.0164		.024			.055			.107	-.0301		.194		
.050	-.0181		.028	-.0247		.050	-.0184		.100	-.0295		.160	-.0334		.246	-.0351	
.076			.052	-.0003		.072	-.0250		.146	-.0295		.208	-.0186		.362	-.0383	
.100			.077	-.0250		.100	-.0299		.190	-.0312		.306			.450	-.0416	
.150	-.0164		.100	-.0266		.150	.0151		.240	-.0329		.403	-.0416		.640	-.0482	
.200	-.0181		.150	-.0299		.200	-.0246		.284	-.0345		.503	-.0449		.850	-.0498	
.250	-.0198		.200	-.0299		.250			.330	-.0362		.600	-.0515				
.300	-.0198		.250	-.0316		.300	-.0329		.374			.700	-.0531				
.350	-.0214		.300	-.0349		.350	-.0395		.473	-.0055		.800	-.0564				
.400			.350	-.0398		.400	-.0412		.572	-.0072		.900	-.0482				
.450	-.0198		.400	-.0398		.500	-.0428		.672	-.0531							
.500	-.0247		.450	-.0415		.600	-.0528		.771	-.0564							
.550	.0645		.500	-.0431		.700	-.0544		.870	-.0564							
.600	-.0264		.600	-.1238		.800	-.0561		.915	-.0515							
.700			.700	-.0514		.900											
.800			.800	-.0546		.940	-.0511										
.900			.900	-.0563													
.940	-.0462		.940	-.0563													

TABLE B-14.- Continued

(k) $\alpha_c = 8.06^o$

Cp at 2y/b of:																		
0.00			0.20			0.40			0.60			0.80			0.95		
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower
.024			.016	-.0313		.024			.055			.107	-.0417		.194		
.050	-.0297		.028	-.0396		.050	-.0333		.100	-.0412		.160	-.0450		.246	-.0466	
.076			.052	-.0119		.072	-.0382		.146	-.0412		.208	-.0302		.362	-.0483	
.100			.077	-.0382		.100	-.0399		.190	-.0429		.306			.450	-.0499	
.150	-.0264		.100	-.0399		.150	-.0034		.240	-.0429		.403	-.0515		.640	-.0564	
.200	-.0297		.150	-.0415		.200	-.0362		.284	-.0445		.503	-.0532		.850	-.0532	
.250	-.0313		.200	-.0415		.250			.330	-.0462		.600	-.0581				
.300	-.0297		.250	-.0432		.300	-.0445		.374			.700	-.0597				
.350	-.0313		.300	-.0448		.350	-.0478		.473	-.0138		.800	-.0581				
.400			.350	-.0481		.400	-.0495		.572	-.0155		.900	-.0532				
.450	-.0297		.400	-.0481		.500	-.0528		.672	-.0614							
.500	-.0363		.450	-.0481		.600	-.0611		.771	-.0614							
.550	.0628		.500	-.0498		.700	-.0578		.870	-.0581							
.600	-.0363		.600	-.0547		.800	-.0578		.915	-.0564							
.700			.700	-.0563		.900											
.800			.800	-.0580		.940	-.0545										
.900			.900	-.0580													
.940	-.0528		.940	-.0580													

TABLE B-14.- Continued

(l) $\alpha = 10.05^{o}$

Cp at 2y/b of:																	
0.00			0.20			0.40			0.60			0.80			0.95		
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower
.024			.016	-.0429		.024			.055			.107	-.0531		.194		
.050	-.0396		.028	-.0512		.050	-.0448		.100	-.0527		.160	-.0564		.246	-.0564	
.076			.052	-.0201		.072	-.0481		.146	-.0527		.208	-.0383		.362	-.0564	
.100			.077	-.0465		.100	-.0498		.190	-.0511		.306			.450	-.0564	
.150	-.0346		.100	-.0498		.150	-.0062		.240	-.0544		.403	-.0580		.640	-.0646	
.200	-.0380		.150	-.0498		.200	-.0477		.284	-.0544		.503	-.0613		.850	-.0580	
.250	-.0396		.200	-.0498		.250			.330	-.0560		.600	-.0662				
.300	-.0396		.250	-.0514		.300	-.0544		.374			.700	-.0646				
.350	-.0413		.300	-.0530		.350	-.0594		.473	-.0235		.800	-.0629				
.400			.350	-.0563		.400	-.0594		.572	-.0235		.900	-.0580				
.450	-.0363		.400	-.0547		.500	-.0594		.672	-.0662							
.500	-.0429		.450	-.0563		.600	-.0677		.771	-.0646							
.550	-.0612		.500	-.0563		.700	-.0627		.870	-.0646							
.600	-.0429		.600	-.0629		.800	-.0610		.915	-.0629							
.700			.700	-.0613		.900											
.800			.800	-.0613		.940	-.0594										
.900			.900	-.0613													
.940	-.0479		.940	-.0629													

TABLE B-14.- Concluded

(m) $\alpha = 14.06^{o}$

Cp at 2y/b of:																	
0.00			0.20			0.40			0.60			0.80			0.95		
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower
.024			.016	-.0529		.024			.055			.107	-.0809		.194		
.050	-.0496		.028	-.0612		.050	-.0563		.100	-.0644		.160	-.0859		.246	-.0859	
.076			.052	-.0317		.072	-.0596		.146	-.0644		.208	-.0626		.362	-.0842	
.100			.077	-.0580		.100	-.0596		.190	-.0594		.306			.450	-.0842	
.150	-.0446		.100	-.0613		.150	-.0163		.240	-.0644		.403	-.0859		.640	-.0909	
.200	-.0463		.150	-.0596		.200	-.0577		.284	-.0644		.503	-.0892		.850	-.0859	
.250	-.0512		.200	-.0613		.250			.330	-.0677		.600	-.0909				
.300	-.0512		.250	-.0613		.300	-.0660		.374			.700	-.0876				
.350	-.0512		.300	-.0629		.350	-.0710		.473	-.0493		.800	-.0892				
.400			.350	-.0679		.400	-.0693		.572	-.0576		.900	-.0842				
.450	-.0463		.400	-.0629		.500	-.0677		.672	-.0876							
.500	-.0496		.450	-.0646		.600	-.0727		.771	-.0876							
.550	.0610		.500	-.0662		.700	-.0644		.870	-.0892							
.600	-.0496		.600	-.0711		.800	-.0677		.915	-.0876							
.700			.700	-.0662		.900											
.800			.800	-.0646		.940	-.0677										
.900			.900	-.0662													
.940	-.0479		.940	-.0662													

TABLE B-15.- PRESSURE COEFFICIENTS FOR WING WITH 55° SWEEP,

$C_{L,des} = 0.0$, $M = 4.6$

(a) $\alpha = -13.20°$

Cp at 2y/b of:																	
0.00			0.20			0.40			0.60			0.80			0.95		
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower
.024			.016	.3906		.024			.055			.107	.3181		.194		
.050	.2229		.028	.3190		.050	.3092		.100	.3056		.160	.2816		.246	.2613	
.076			.052	.3194		.072	.3194		.146	.3015		.208	.0563		.362	.2511	
.100			.077	.2888		.100	.3051		.190	.2933		.306			.450	.2389	
.150	.2331		.100	.2725		.150	.3261		.240	.2830		.403	.2511		.640	.2186	
.200	.2331		.150	.2542		.200	.2892		.284	.2748		.503	.2369		.850	.2004	
.250	.2352		.200	.2399		.250			.330	.2646		.600	.2166				
.300	.2331		.250	.2277		.300	.2543		.374			.700	.1963				
.350	.2311		.300	.2114		.350	.2358		.473	.2511		.800	.1821				
.400			.350	.1972		.400	.2153		.572	.2491		.900	.1699				
.450	.2086		.400	.1911		.500	.1866		.672	.1760							
.500	.1922		.450	.1850		.600	.1620		.771	.1557							
.550	.1227		.500	.1748		.700	.1415		.870	.1415							
.600	.1493		.600	.1503		.800	.1251		.915	.1354							
.700			.700	.1320		.900											
.800			.800	.1198		.940	.1128										
.900			.900	.1055													
.940	.1309		.940	.1035													

TABLE B-15.- Continued

(b) $\alpha = -9.21^{o}$

Cp at 2y/b of:																	
0.00			0.20			0.40			0.60			0.80			0.95		
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower
.024			.016	.2270		.024			.055			.107	.1742		.194		
.050	.1452		.028	.1922		.050	.1890		.100	.1828		.160	.1681		.246	.1580	
.076			.052	.2094		.072	.2013		.146	.1767		.208	.0706		.362	.1458	
.100			.077	.1911		.100	.1890		.190	.1746		.306			.450	.1377	
.150	.1472		.100	.1850		.150	.2239		.240	.1726		.403	.1397		.640	.1194	
.200	.1493		.150	.1768		.200	.1910		.284	.1685		.503	.1316		.850	.1031	
.250	.1534		.200	.1626		.250			.330	.1623		.600	.1194				
.300	.1493		.250	.1544		.300	.1726		.374			.700	.1072				
.350	.1452		.300	.1402		.350	.1582		.473	.1702		.800	.0970				
.400			.350	.1239		.400	.1418		.572	.1702		.900	.0909				
.450	.1329		.400	.1157		.500	.1213		.672	.1052							
.500	.1329		.450	.1096		.600	.0966		.771	.0909							
.550	.1227		.500	.1035		.700	.0802		.870	.0808							
.600	.1124		.600	.0852		.800	.0679		.915	.0767							
.700			.700	.0689		.900											
.800			.800	.0607		.940	.0576										
.900			.900	.0506													
.940	.0736		.940	.0485													

TABLE B-15.- Continued

(c) α = -7.21°

Cp at 2y/b of:																		
0.00			0.20			0.40			0.60			0.80			0.95			
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	
.024			.016	-.1759		.024			.055			.107	-.1354		.194			
.050	-.1124		.028	-.1452		.050	-.1503		.100	-.1377		.160	-.1253		.246	-.1171		
.076			.052	-.1687		.072	-.1503		.146	-.1336		.208	-.0766		.362	-.1070		
.100			.077	-.1442		.100	-.1402		.190	-.1295		.306			.450	-.0989		
.150	-.1145		.100	-.1402		.150	-.1808		.240	-.1233		.403	-.1009		.640	-.0847		
.200	-.1124		.150	-.1402		.200	-.1418		.284	-.1233		.503	-.0908		.850	-.0684		
.250	-.1145		.200	-.1300		.250			.330	-.1213		.600	-.0806					
.300	-.1145		.250	-.1198		.300	-.1295		.374			.700	-.0705					
.350	-.1124		.300	-.1055		.350	-.1213		.473	-.1374		.800	-.0644					
.400			.350	-.0913		.400	-.1069		.572	-.1354		.900	-.0583					
.450	-.1002		.400	-.0852		.500	-.0884		.672	-.0745								
.500	-.0981		.450	-.0791		.600	-.0679		.771	-.0623								
.550	-.1227		.500	-.0750		.700	-.0556		.870	-.0542								
.600	-.0797		.600	-.0587		.800	-.0433		.915	-.0502								
.700			.700	-.0465		.900												
.800			.800	-.0383		.940	-.0351											
.900			.900	-.0302														
.940	-.0470		.940	-.0261														

TABLE B-15.- Continued

(d) $\alpha = -5.22^{o}$

Cp at 2y/b of:																	
0.00			0.20			0.40			0.60			0.80			0.95		
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower
.024			.016	.1329		.024			.055			.107	.0666		.194		
.050	-.0838		.028	.1084		.050	.1076		.100	.1005		.160	.0625		.246	.0542	
.076			.052	.1300		.072	.1116		.146	.0964		.208	.0542		.362	.0459	
.100			.077	.1055		.100	.1035		.190	.0944		.306			.450	.0377	
.150	-.0838		.100	.1015		.150	.1456		.240	.0903		.403	.0418		.640	.0253	
.200	-.0818		.150	.0994		.200	.1005		.284	.0862		.503	.0315		.850	.0109	
.250	-.0818		.200	.0954		.250			.330	.0821		.600	.0212				
.300	-.0838		.250	.0892		.300	.0903		.374			.700	.0109				
.350	-.0818		.300	.0770		.350	.0841		.473	.0810		.800	.0047				
.400			.350	.0648		.400	.0739		.572	.0521		.900	-.0014				
.450	-.0736		.400	.0587		.500	.0636		.672	.0171							
.500	-.0736		.450	.0526		.600	.0452		.771	.0067							
.550	-.1227		.500	.0485		.700	.0329		.870	.0005							
.600	-.0593		.600	.0343		.800	.0226		.915	-.0035							
.700			.700	.0261		.900											
.800			.800	.0180		.940	.0144										
.900			.900	.0119													
.940	-.0265		.940	.0078													

TABLE B-15.- Continued

(e) α = -3.22°

Cp at 2y/b of:																	
0.00			0.20			0.40			0.60			0.80			0.95		
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower
.024			.016	.0940		.024			.055			.107	.0433		.194		
.050	-.0572		.028	.0736		.050	.0750		.100	.0677		.160	.0412		.246	.0330	
.076			.052	.0994		.072	.0770		.146	.0657		.208	.0638		.362	.0268	
.100			.077	.0709		.100	.0689		.190	.0636		.306			.450	.0207	
.150	-.0613		.100	.0668		.150	.1190		.240	.0595		.403	.0227		.640	.0084	
.200	-.0552		.150	.0648		.200	.0677		.284	.0575		.503	.0145		.850	-.0038	
.250	-.0531		.200	.0607		.250			.330	.0534		.600	.0043				
.300	-.0531		.250	.0567		.300	.0554		.374			.700	-.0038				
.350	-.0531		.300	.0485		.350	.0513		.473	.0617		.800	-.0100				
.400			.350	.0383		.400	.0431		.572	.0412		.900	-.0141				
.450	.0490		.400	.0343		.500	.0370		.672	.0002							
.500	.0470		.450	.0302		.600	.0247		.771	-.0059							
.550	.1227		.500	.0262		.700	.0144		.870	-.0141							
.600	.0347		.600	.0159		.800	.0062		.915	-.0162							
.700			.700	.0078		.900											
.800			.800	.0017		.940	-.0019										
.900			.900	-.0043													
.940	.0081		.940	-.0084													

TABLE B-15.- Continued

(f) $\alpha = -1.22^{o}$

Cp at 2y/b of:																	
0.00			0.20			0.40			0.60			0.80			0.95		
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower
.024			.016	.0613		.024			.055			.107	.0360		.194		
.050	.0368		.028	.0490		.050	.0425		.100	.0392		.160	.0339		.246	.0278	
.076			.052	.0731		.072	.0446		.146	.0371		.208	.0786		.362	.0217	
.100			.077	.0425		.100	.0405		.190	.0351		.306			.450	.0157	
.150	.0388		.100	.0364		.150	.0946		.240	.0330		.403	.0177		.640	.0055	
.200	.0327		.150	.0364		.200	.0412		.284	.0289		.503	.0116		.850	-.0005	
.250	.0306		.200	.0344		.250			.330	.0268		.600	.0014				
.300	.0306		.250	.0303		.300	.0289		.374			.700	-.0025				
.350	.0306		.300	.0242		.350	.0227		.473	.0623		.800	-.0086				
.400			.350	.0160		.400	.0166		.572	.0563		.900	-.0127				
.450	.0306		.400	.0119		.500	.0125		.672	-.0005							
.500	.0286		.450	.0099		.600	.0002		.771	-.0066							
.550	.1206		.500	.0058		.700	-.0059		.870	-.0127							
.600	.0204		.600	-.0022		.800	-.0120		.915	-.0147							
.700			.700	-.0083		.900	-.0162										
.800			.800	-.0145		.940	-.0162										
.900			.900	-.0185													
.940	-.0061		.940	-.0226													

TABLE B-15.- Continued

(g) α = -0.29°

Cp at 2y/b of:																	
0.00			0.20			0.40			0.60			0.80			0.95		
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower
.024			.016	.0471		.024			.055			.107	.0240		.194		
.050	.0266		.028	.0348		.050	.0343		.100	.0289		.160	.0219		.246	.0158	
.076			.052	.0648		.072	.0343		.146	.0268		.208	.0728		.362	.0118	
.100			.077	.0343		.100	.0322		.190	.0248		.306			.450	.0057	
.150	.0287		.100	.0282		.150	.0843		.240	.0227		.403	.0077		.640	-.0024	
.200	.0225		.150	.0261		.200	.0330		.284	.0186		.503	-.0003		.850	-.0105	
.250	.0205		.200	.0261		.250			.330	.0166		.600	-.0064				
.300	.0205		.250	.0220		.300	.0207		.374			.700	-.0125				
.350	.0205		.300	.0159		.350	.0145		.473	.0525		.800	-.0166				
.400			.350	.0078		.400	.0084		.572	.0504		.900	-.0207				
.450	.0205		.400	.0058		.500	.0022		.672	-.0085							
.500	.0184		.450	.0037		.600	-.0079		.771	-.0166							
.550	.1167		.500	-.0003		.700	-.0141		.870	-.0227							
.600	.0103		.600	-.0084		.800	-.0203		.915	-.0227							
.700			.700	-.0125		.900											
.800			.800	-.0166		.940	-.0223										
.900			.900	-.0227													
.940	-.0142		.940	-.0247													

TABLE B-15.- Continued

(h) $\alpha = 2.78^{o}$

Cp at 2y/b of:																	
0.00			0.20			0.40			0.60			0.80			0.95		
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower
.024			.016	.0123		.024			.055	-.0038		.107	-.0324		.194		
.050	.0062		.028	.0041		.050	.0037		.100	-.0038		.160	-.0365		.246	-.0386	
.076			.052	.0383		.072	.0037		.146	-.0038		.208	.0377		.362	-.0406	
.100			.077	.0058		.100	.0017		.190	-.0059		.306			.450	-.0448	
.150	.0062		.100	.0017		.150	.0597		.240	-.0059		.403	-.0427		.640	-.0530	
.200	.0021		.150	-.0023		.200	.0063		.284	-.0079		.503	-.0468		.850	-.0551	
.250	-.0040		.200	-.0003		.250			.330	-.0100		.600	-.0551				
.300	-.0040		.250	-.0043		.300	-.0059		.374			.700	-.0551				
.350	-.0040		.300	-.0084		.350	-.0120		.473	.0067		.800	-.0633				
.400			.350	-.0145		.400	-.0162		.572	.0067		.900	-.0613				
.450	.0000		.400	-.0145		.500	-.0162		.672	-.0551							
.500	.0000		.450	-.0166		.600	-.0285		.771	-.0571							
.550	.1147		.500	-.0186		.700	-.0285		.870	-.0654							
.600	-.0019		.600	-.0267		.800	-.0326		.915	-.0633							
.700			.700	-.0267		.900											
.800			.800	-.0328		.940	-.0346										
.900			.900	-.0349													
.940	-.0306		.940	-.0349													

TABLE B-15.- Continued

(i) $\alpha = 4.78^{o}$

Cp at 2y/b of:																	
0.00			0.20			0.40			0.60			0.80			0.95		
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower
.024			.016	-.0060		.024			.055			.107	-.0468		.194		
.050	-.0081		.028	-.0122		.050	-.0125		.100	-.0162		.160	-.0510		.246	-.0510	
.076			.052	-.0261		.072	-.0125		.146	-.0162		.208	-.0315		.362	-.0510	
.100			.077	-.0084		.100	-.0145		.190	-.0182		.306			.450	-.0551	
.150	-.0040		.100	-.0125		.150	-.0453		.240	-.0203		.403	-.0551		.640	-.0633	
.200	-.0101		.150	-.0166		.200	-.0079		.284	-.0203		.503	-.0571		.850	-.0633	
.250	-.0163		.200	-.0145		.250			.330	-.0244		.600	-.0654				
.300	-.0163		.250	-.0166		.300	-.0182		.374			.700	-.0633				
.350	-.0163		.300	-.0206		.350	-.0264		.473	-.0035		.800	-.0675				
.400			.350	-.0267		.400	-.0264		.572	-.0551		.900	-.0633				
.450	-.0101		.400	-.0247		.500	-.0264		.672	-.0675							
.500	-.0122		.450	-.0267		.600	-.0387		.771	-.0675							
.550	.1126		.500	-.0267		.700	-.0367		.870	-.0716							
.600	-.0122		.600	-.0349		.800	-.0408		.915	-.0675							
.700			.700	-.0349		.900											
.800			.800	-.0349		.940	-.0387										
.900			.900	-.0410													
.940	-.0347		.940	-.0390													

TABLE B-15.- Continued

(j) $\alpha = 6.78^{o}$

Cp at 2y/b of:																	
0.00			0.20			0.40			0.60			0.80			0.95		
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower
.024			.016	-.0184		.024			.055			.107	-.0613		.194		
.050	-.0143		.028	-.0245		.050	-.0247		.100	-.0285		.160	-.0654		.246	-.0654	
.076			.052	.0159		.072	-.0227		.146	-.0264		.208	.0193		.362	-.0654	
.100			.077	-.0186		.100	-.0247		.190	-.0264		.306			.450	-.0654	
.150	-.0122		.100	-.0247		.150	.0351		.240	-.0305		.403	-.0654		.640	-.0737	
.200	-.0163		.150	-.0267		.200	-.0203		.284	-.0305		.503	-.0695		.850	-.0716	
.250	-.0245		.200	-.0247		.250			.330	-.0326		.600	-.0757				
.300	-.0225		.250	-.0267		.300	-.0285		.374			.700	-.0757				
.350	-.0225		.300	-.0308		.350	-.0346		.473	-.0137		.800	-.0778				
.400			.350	-.0349		.400	-.0346		.572	-.0675		.900	-.0695				
.450	-.0163		.400	-.0328		.500	-.0346		.672	-.0778							
.500	-.0204		.450	-.0349		.600	-.0469		.771	-.0757							
.550	.1124		.500	-.0349		.700	-.0408		.870	-.0757							
.600	-.0184		.600	-.0410		.800	-.0449		.915	-.0737							
.700			.700	-.0390		.900											
.800			.800	-.0390		.940	-.0408										
.900			.900	-.0430													
.940	-.0409		.940	-.0430													

TABLE B-15.- Continued

(k) $\alpha = 8.78^{o}$

Cp at 2y/b of:																	
0.00			0.20			0.40			0.60			0.80			0.95		
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower
.024			.016	-.0286		.024			.055			.107	-.0654		.194		
.050	-.0225		.028	-.0347		.050	-.0349		.100	-.0367		.160	-.0695		.246	-.0695	
.076			.052	.0078		.072	-.0328		.146	-.0367		.208	.0130		.362	-.0675	
.100			.077	-.0288		.100	-.0328		.190	-.0326		.306			.450	-.0675	
.150	-.0204		.100	-.0328		.150	.0310		.240	-.0367		.403	-.0675		.640	-.0778	
.200	-.0225		.150	-.0328		.200	-.0264		.284	-.0367		.503	-.0737		.850	-.0737	
.250	-.0306		.200	-.0328		.250			.330	-.0408		.600	-.0778				
.300	-.0306		.250	-.0349		.300	-.0367		.374			.700	-.0778				
.350	-.0306		.300	-.0369		.350	-.0449		.473	-.0179		.800	-.0778				
.400			.350	-.0410		.400	-.0428		.572	-.0695		.900	-.0695				
.450	-.0225		.400	-.0369		.500	-.0408		.672	-.0799							
.500	-.0266		.450	-.0390		.600	-.0490		.771	-.0778							
.550	.1084		.500	-.0390		.700	-.0428		.870	-.0778							
.600	-.0245		.600	-.0471		.800	-.0449		.915	-.0757							
.700			.700	-.0430		.900											
.800			.800	-.0410		.940	-.0449										
.900			.900	-.0451													
.940	-.0368		.940	-.0451													

TABLE B-15.- Continued

(l) $\alpha = 10.79^{o}$

Cp at 2y/b of:

0.00			0.20			0.40			0.60			0.80			0.95		
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower
.024			.016	-.0368		.024			.055			.107	-.0411		.194		
.050	-.0327		.028	-.0429		.050	-.0410		.100	-.0449		.160	-.0471		.246	-.0471	
.076			.052	.0017		.072	-.0390		.146	-.0428		.208	.0279		.362	-.0431	
.100			.077	-.0369		.100	-.0390		.190	-.0408		.306			.450	-.0431	
.150	-.0306		.100	-.0410		.150	.0248		.240	-.0449		.403	-.0431		.640	-.0512	
.200	-.0347		.150	-.0410		.200	-.0346		.284	-.0449		.503	-.0471		.850	-.0471	
.250	-.0388		.200	-.0410		.250			.330	-.0449		.600	-.0532				
.300	-.0388		.250	-.0410		.300	-.0449		.374			.700	-.0492				
.350	-.0388		.300	-.0451		.350	-.0490		.473	.0056		.800	-.0512				
.400			.350	-.0471		.400	-.0469		.572	-.0451		.900	-.0451				
.450	-.0306		.400	-.0451		.500	-.0469		.672	-.0532							
.500	-.0347		.450	-.0451		.600	-.0531		.771	-.0492							
.550	.1024		.500	-.0471		.700	-.0449		.870	-.0512							
.600	-.0327		.600	-.0532		.800	-.0469		.915	-.0492							
.700			.700	-.0471		.900											
.800			.800	-.0491		.940	-.0490										
.900			.900	-.0491													
.940	-.0368		.940	-.0471													

TABLE B-15.- Concluded

(m) α = 14.79°

Cp at 2y/b of:																	
0.00			0.20			0.40			0.60			0.80			0.95		
x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower	x/c	Upper	Lower
.024			.016	-.0409		.024			.055			.107	-.0431		.194		
.050	-.0388		.028	-.0491		.050	-.0471		.100	-.0490		.160	-.0492		.246	-.0492	
.076			.052	-.0043		.072	-.0451		.146	-.0469		.208	.0238		.362	-.0451	
.100			.077	-.0410		.100	-.0451		.190	-.0428		.306			.450	-.0451	
.150	-.0347		.100	-.0471		.150	.0186		.240	-.0490		.403	-.0451		.640	-.0533	
.200	-.0368		.150	-.0451		.200	-.0408		.284	-.0490		.503	-.0492		.850	-.0492	
.250	-.0450		.200	-.0451		.250			.330	-.0510		.600	-.0533				
.300	-.0450		.250	-.0471		.300	-.0490		.374			.700	-.0492				
.350	-.0409		.300	-.0491		.350	-.0572		.473	.0075		.800	-.0512				
.400			.350	-.0552		.400	-.0531		.572	-.0451		.900	-.0451				
.450	-.0368		.400	-.0491		.500	-.0490		.672	-.0533							
.500	-.0388		.450	-.0491		.600	-.0551		.771	-.0512							
.550	.1022		.500	-.0491		.700	-.0469		.870	-.0533							
.600	-.0368		.600	-.0552		.800	-.0510		.915	-.0512							
.700			.700	-.0491		.900											
.800			.800	-.0471		.940	-.0510										
.900			.900	-.0532													
.940	-.0409		.940	-.0532													

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