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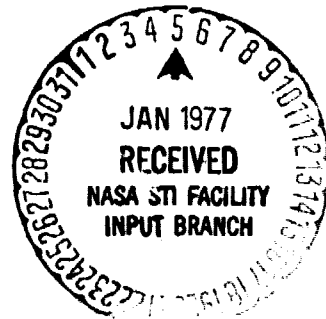
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**STANDARDIZED PERFORMANCE TESTS OF COLLECTORS  
OF SOLAR THERMAL ENERGY - AN EVACUATED FLAT-  
PLATE COPPER COLLECTOR WITH A SERPENTINE  
FLOW DISTRIBUTION**

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# STANDARDIZED PERFORMANCE TESTS OF COLLECTORS OF SOLAR

## THERMAL ENERGY - AN EVACUATED FLAT-PLATE COPPER

### COLLECTOR WITH A SERPENTINE FLOW DISTRIBUTION

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#### INTRODUCTION

An area that has been investigated by the NASA Lewis Research Center in its efforts to aid in the utilization of alternate energy sources is the use of solar energy for the heating and cooling of buildings. An important part of this effort was the evaluation of solar collectors which have the potential to be efficient, economical, and reliable.

This preliminary data report gives basic test results of a collector whose performance was determined in the NASA-Lewis solar simulator. In the interest of providing performance data on this collector to the technical community as quickly as possible, the basic test results reported herein are presented without evaluation. Detailed analyses and interpretation of these results may be presented in subsequent papers or reports by this Center. Some of the results contained in this report may be changed as warranted by reviews and evaluations, or by obtaining additional data on this collector.

Reference 1 describes the solar-simulator test facility, as well as the basic test procedure.

#### COLLECTOR DESCRIPTION

The Solarvak flat plate solar collector was manufactured by Solar Systems, Inc. of Tyler, Texas. The collector is designed to be evacuated but the particular collector tested had an internal pressure only slightly less than atmospheric (28.5 inches of mercury). Wooden dowels separate the 1/4 inch thick acrylic top and bottom sheets. These two acrylic sheets form the box-like construction of the collector with nuts and bolts holding the assembly together at the flanges. The absorber plate is copper with a selective surface copper oxide coating and is suspended and held in place by several 1 inch diameter wooden dowels. The fluid flow is serpentine configuration with 3/8 inch

O.D. copper tubes soldered to the underside of the absorber plate. Aluminum foil is placed on the bottom and directly behind the flow tubes to reduce energy lost by radiation from the back of the absorber plate. No insulation is present in the collector. A photograph of the collector on the test stand is shown in figure 1.

#### COLLECTOR TEST RESULTS

Basic test results are given in Table I. Since this collector was larger than the area of radiation provided by the solar simulator, it was necessary to use a "shield" approach as explained in Reference 1. This technique allows one to determine the efficiency of the entire collector even though only a portion of it is actually exposed to radiation. By using the analytical method outlined in Reference 1 for a collector tested with a "shield", the results given for the flow rate in Table I were used for a determination of the performance correlation given in Figure 2.

In addition to the basic test performed on the collector, a series of incident angle tests were run to help predict changes of sun incidence angles throughout the period of one solar day. Table II lists the collector efficiency at various rotation and incident angles, along with  $K_{qT}$  values. One analytical method for interpreting and using these data can be found in Reference 1.

#### REFERENCES

1. Simon, Frederick F.: Flat-Plate Collector Performance with a Solar Simulator as a Basis for Collector Selection and Performance Prediction. NASA TMX-71793, 1975.

TABLE I - BASIC EXPERIMENTAL DATA

50/50 Water and Ethylene Glycol  
 Incident Angel = 0°  
 Tilt Angle = 57° Above Horizontal

| Flow Per Radiated Surface Area<br>lb/hr ft <sup>2</sup> | Flow Gal/Min | Incident Radiation Flux<br>Btu/hr ft <sup>2</sup> | Fluid Outlet Temp., °F | Fluid Inlet Temp., °F | Ambient Temp. | Efficiency |
|---|--------------|---|------------------------|-----------------------|---------------|------------|
| 19.305  | 0.49469      | 202.27  | 96.447                 | 85.993                | 84.144        | 0.81975    |
| 19.370  | 0.45620      | 195.31  | 97.675                 | 85.538                | 83.659        | 0.58080    |
| 19.157  | 0.50251      | 195.08  | 126.22                 | 120.39                | 80.897        | 0.47981    |
| 19.141  | 0.50281      | 287.41  | 130.09                 | 120.89                | 81.416        | 0.51403    |
| 19.222  | 0.50610      | 194.23  | 165.66                 | 161.94                | 79.390        | 0.31617    |
| 19.271  | 0.50612      | 292.82  | 168.11                 | 161.16                | 79.834        | 0.39142    |

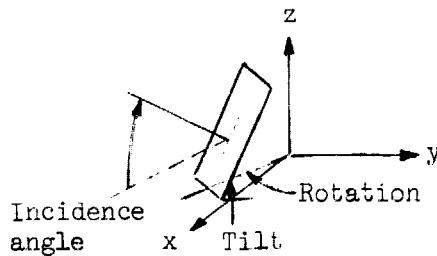
TABLE II. - INCIDENT ANGLE MODIFIER DATA

| Tilt <sup>a</sup><br>angle,<br>deg | Rotation<br>angle,<br>deg | Incidence<br>angle,<br>deg | Efficiency | $K_{\alpha\tau}$ |
|------------------------------------|---------------------------|----------------------------|------------|------------------|
| 57                                 | 0                         | 0                          | 0.820      | 1.0              |
| 57                                 | 50                        | 41.5                       | 0.816      | 0.995            |
| 57                                 | 70                        | 57.5                       | 0.769      | 0.938            |
| 57                                 | 80                        | 65.2                       | 0.720      | 0.878            |

<sup>a</sup>Tilt angle - the angle between the horizontal and the plane of the collector.

Rotation angle - the angle that is measured in relation to the X-axis when the collector is rotated around the Z-axis.

Incidence angle - the angle that is measured between the beam of light and the normal to the plane of the collector.



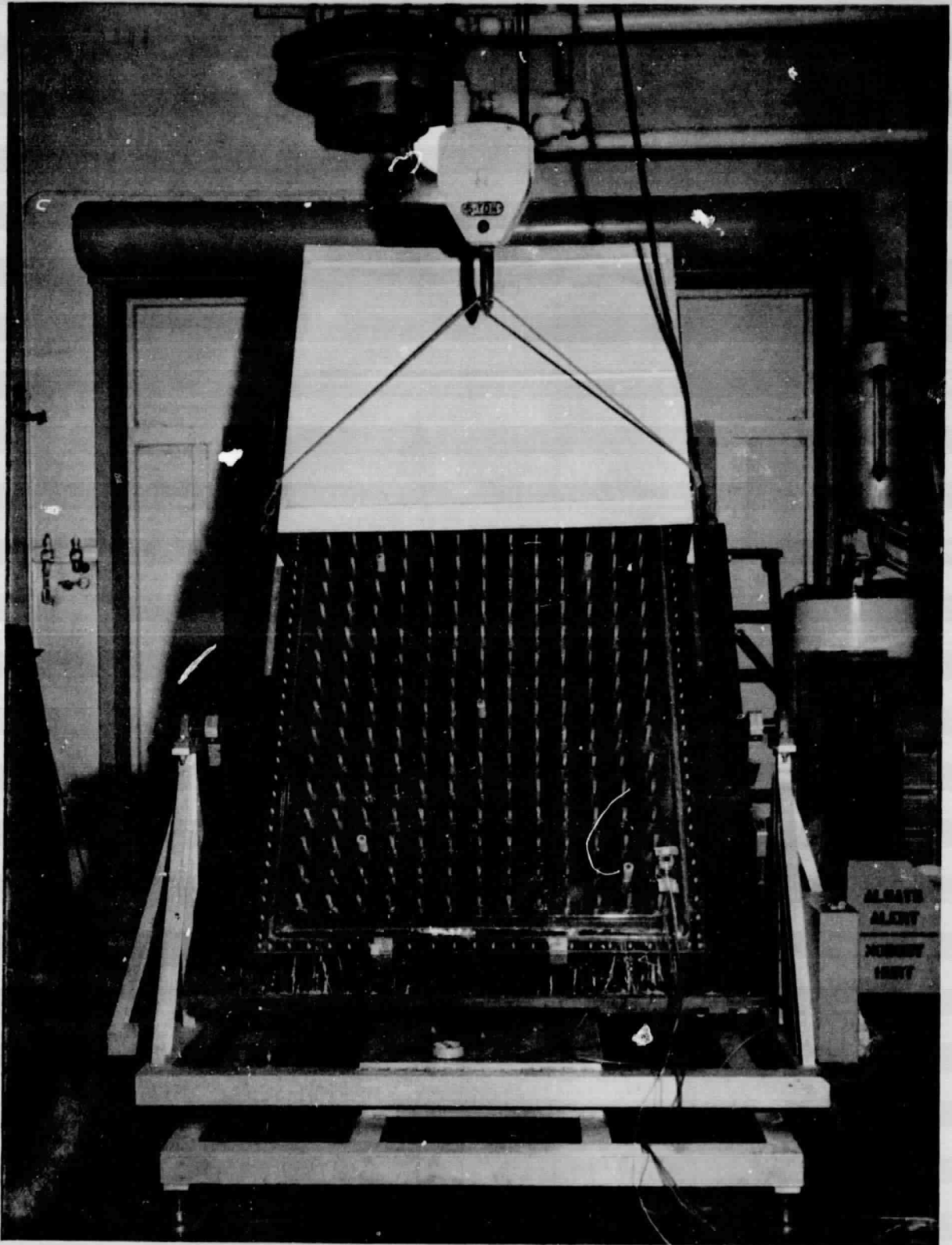
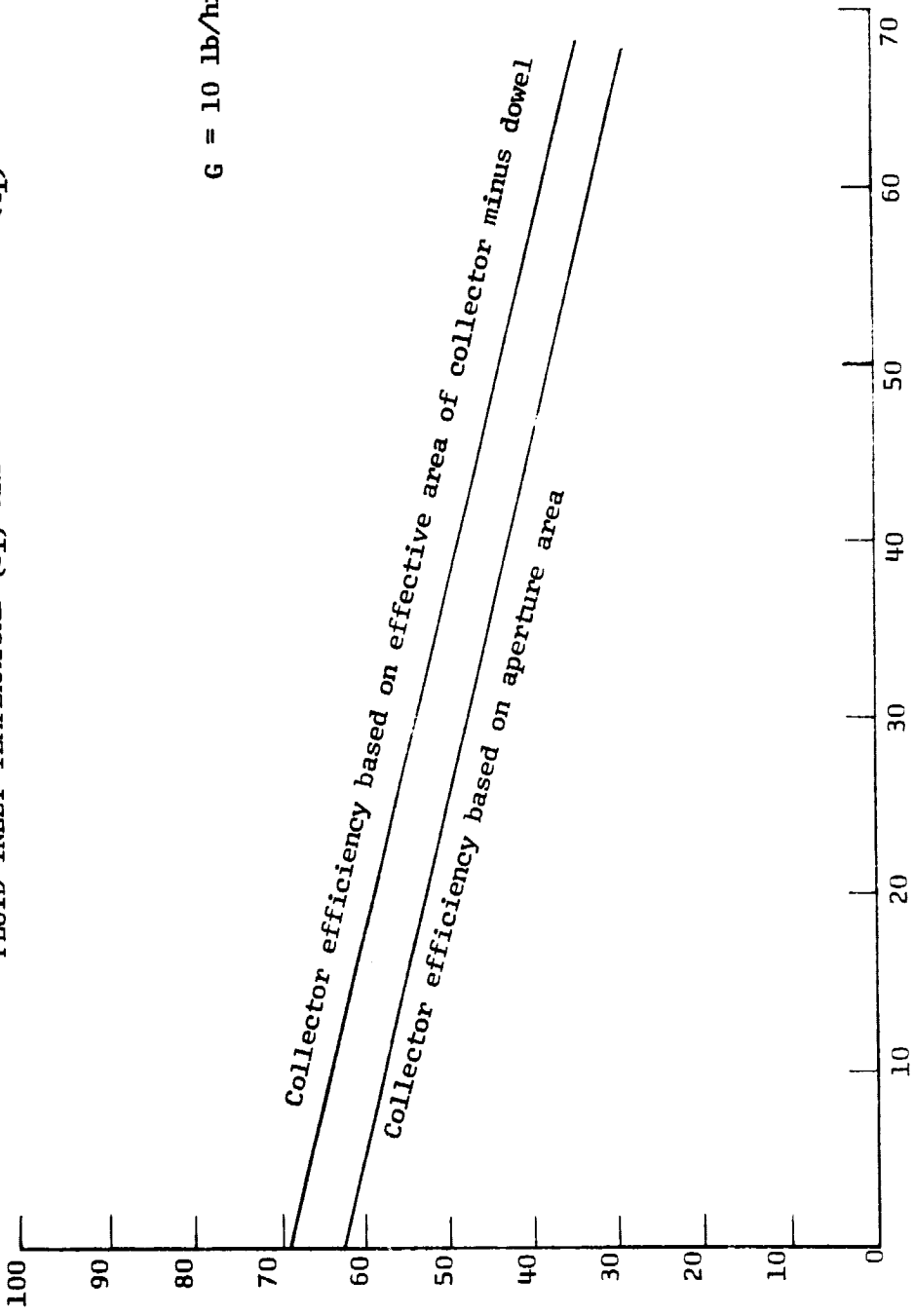


Figure 1. - Collector on Test Stand



COLLECTOR EFFICIENCY ( $\eta$ ) AS A FUNCTION  
 FLUID INLET TEMPERATURE ( $T_i$ ) AND INCIDENT FLUX ( $q_i$ )



$$\frac{T_i - T_{\text{ambient}}}{q_i} \times 10^2 \left( \frac{\text{BTU}}{\text{HR FT}^2 \text{ °F}} \right)^{-1}$$

Figure 2. - Collector Performance Correlation