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TECHNICAL REPORT

CR-151230

FEASIBILITY STUDY OF AUTOMATIC CONTROL
OF CREW COMFORT IN THE SHUTTLE
EXTRAVEHICULAR MOBILITY UNIT (EMU)

Job Order 81-107

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Prepared By

Lockheed Electronics Company, Inc.
Aerospace Systems Division
Houston, Texas

Contract NAS 9-15200

For

CREW SYSTEMS DIVISION

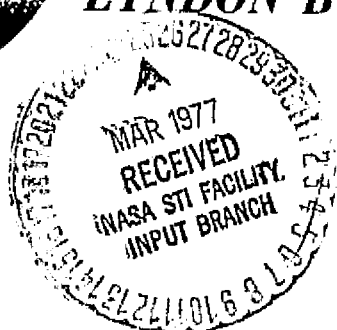


National Aeronautics and Space Administration
LYNDON B. JOHNSON SPACE CENTER

Houston, Texas

February 22, 1977

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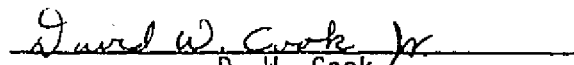


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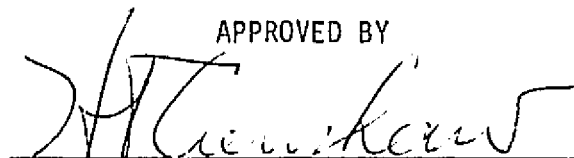
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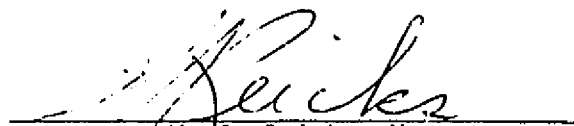
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1. INTRODUCTION

During the Apollo project, crew comfort in the Apollo Extravehicular Mobility Unit (EMU) was maintained by manual manipulation of a valve that controlled the inlet coolant temperature to the liquid cooled garment (LCG). Four inlet temperature selections were possible ranging approximately from 45⁰F to 80⁰F. During Skylab, similar comfort control was achieved by manually operating a valve which varied LCG coolant flow rate.

The Shuttle EMU design proposal includes an 11-position manual valve to vary inlet coolant temperature similar to the method used in Apollo. Eleven inlet temperatures would be available for selection vs. the four previously available.

Apollo experience indicates that some training is necessary to enhance the crewman's comfort and optimize his ability to carry a workload. Several tendencies were noted during lunar and Skylab extravehicular activities (EVA's):

- a. Some crewmen precooled themselves in anticipation of a high activity level and left the valve in the valve position selected prior to the activity. A high level of training is needed for such anticipation.
- b. Some crewmen tended to work at rates that were conducive to their comfort at some intermediate cooling level. They would slow down or stop and rest if they became too hot, or they would speed up or hurry to the next activity if they were too cool.
- c. At times, preoccupation with a task would cause a crewman to forget comfort until excessive sweating or fatigue became imminent, and ground controllers would suggest valve changes.

It was proposed that the manual control valve be replaced with an automatic one as a product improvement item for the Shuttle program. The automatic valve proposed would sense the normally measured parameters of LCG inlet coolant temperature and LCG coolant inlet and outlet temperature difference (LCG ΔT) for use in controlling comfort. It was further proposed that if computer

simulations gave encouraging results, that tests would be run on Apollo hardware in which the controller logic was simulated by real-time calculations.

LEC/ASD was tasked with determining the feasibility of such a controller using Program J196 on the 1110 computer and to develop suggested control logic for testing. This memorandum contains the results of that effort.

This concludes the requirements outlined by Action Item 46, Project 3030. The study was conducted by LEC/ASD, Dept. 641-11.

2. DISCUSSION

2.1 CONTROLLER LOGIC

2.1.1 GENERAL

Using Program J196, the 41-node man program (ref. 1), a map of comfort can be plotted at steady state. Heat stored at steady state can be calculated for a grid of metabolic rates and inlet coolant temperatures at a given inlet gas dry bulb temperature, dewpoint temperature, and flow rate, and at a given suit heat leak. LCG coolant temperature difference (LCG ΔT) as calculated at steady state by the program can be plotted vs. metabolic rate for constant inlet coolant temperatures. At each plotted point, the heat stored at steady state can be noted. When the grid is completed, comfort boundaries can be interpolated between the heat storage value as follows:

$$\text{Stored heat at comfort (Btu)} = \frac{\text{Metabolic rate (Btu/hr)} - 278 \pm 65}{13.2}$$

A series of these comfort maps have been plotted. An example of such a study is found in reference 2. An example of this type of plot is shown in figure 1.

From plots such as figure 1, a relationship between inlet coolant temperature and LCG ΔT at steady-state comfort is established (figure 2). It was established by averaging together results from several comfort curves such as in figure 1 and modifying them to get better results while developing the controller logic.

To develop logic for this controller, however, some transient data was needed in order to input to the controller how much variation in LCG ΔT was due to previous inlet temperature adjustments and how much was due to changes in the activity level of the crewman (metabolic rate). Therefore, a controller was simulated on the 41-node man program which adjusted inlet LCG temperature by the heat storage of the body. This would be the ideal controller, but the hardware is not practical. Changes in ΔT vs. changes in inlet temperature

were determined as the simulated man remained at perfect comfort while being stepped from one metabolic rate to another. These points were then plotted and an average curve drawn through the points (fig. 3). This curve represents the expected changes in ΔT for every change in inlet temperature if the controller is perfectly tracking comfort during a transient in metabolic rate.

2.1.2 METHOD 1 - USE OF FIGURE 2

The logic of the controller using figure 2 was developed as follows:

$$\Delta T_{in_1} = K_1 (T_{in}' - \bar{T}_{in_1}) \quad (1)$$

where ΔT_{in_1} = the adjustment signal to the final control element, T_{in}' (set point for the inlet coolant temperature to the LCG), calculated from the method using figure 2.

K_1 = The proportional gain constant for the method using figure 2.

T_{in}' = The current inlet temperature to the LCG.

\bar{T}_{in_1} = The inlet temperature at steady state comfort read off figure 2 as a function of the currently measured ΔT .

2.1.3 METHOD 2 - USE OF FIGURE 3

The logic of the controller using figure 3 was as follows:

$$\Delta T_{in_2} = K_2 (\overline{\Delta T}_{in_2}) \quad (2)$$

where

ΔT_{in_2} = The adjustment signal to the final control element T_{in} calculated from the method using figure 2.

K_2 = The proportional gain constant for this method.

$\overline{\Delta T}_{in_2}$ = The changes in the inlet temperature based on figure 3.

$\overline{\Delta T}_{in2}$ is read from figure 3 in the following manner. dT_{in}/dt is calculated (the changes in inlet temperature with time). $d\Delta T/dt$ is read from figure 3 as the expected change in ΔT ($\overline{\Delta\Delta T}$) during the same period of time. Since the same period of time is used, $\overline{\Delta\Delta T}$ is read as a function of ΔT_{in} . The actual change in ΔT ($\Delta\Delta T'$) from the expected $\overline{\Delta\Delta T}$ is then calculated. A calculation of the deviation ($\delta\Delta\Delta T$) of the actual $\Delta\Delta T'$ from the expected $\overline{\Delta\Delta T}$ is made as follows:

$$\delta\Delta\Delta T = \Delta\Delta T' - \overline{\Delta\Delta T} \quad (3)$$

$\delta\Delta\Delta T$ is the main error signal for this method. Error derivative and error integral compensation were also added:

$$\delta\Delta\Delta T = (\Delta\Delta T' - \overline{\Delta\Delta T}) + K_3 \frac{d(\delta\Delta\Delta T)}{dt} + K_4 \int \delta\Delta\Delta T dt \quad (4)$$

where

$$\delta\Delta\Delta T = \Delta\Delta T' - \overline{\Delta\Delta T} \text{ (eq. (3))}.$$

K_3 = the gain constant for error derivative compensation.

$\frac{d(\delta\Delta\Delta T)}{dt}$ = the error derivative compensation.

K_4 = the gain constant for the error integral compensation.

$\delta\Delta\Delta T dt$ = the error integral compensation.

The total error signal $\delta\Delta\Delta T$ is then used on the $\Delta\Delta T/\Delta T$ curve (fig. 3) to determine the adjustment to the final control element, T_{in} , by reading $\overline{\Delta T}_{in2}$. $\overline{\Delta T}_{in2}$ is then applied in eq. (2) to determine the adjustment to the final control element supplied by this method.

2.1.4 FINAL TOTAL CONTROLLER SIGNAL COMBINED FROM FIGURE 2 AND FIGURE 3 METHODS

The two methods described in eqs. (1) and (2) are then combined to give a final calculated value to the final control element, T_{in} :

$$T_{in} = T_{in}' + \left(\frac{\Delta T_{in1} + \Delta T_{in2}}{2} \right)$$

where T_{in}' is the current value of the final control element, the inlet LCG coolant temperature set point.

2.1.5 NEGLECTED CONTROLLER CONSIDERATIONS

Sensor response times, controller deadband, and speed of the final control element were neglected. It should be pointed out that the final control element is the set point for the inlet temperature to the LCG. Another controller would be required to operate the diverter valve bypassing coolant flow around the sublimator in the portable life support system (PLSS) to control the actual LCG inlet temperature. The delay and logic of this controller was neglected in the program and the inlet temperature of the LCG was set instantly to the set point required.

Output differential and integral compensation were attempted in both methods (eqs. 1 and 2). Lack of time prevented the development of gain constants that would improve controller results and these items were not incorporated into the test logic. Error differential and integral compensation in method 1 was never tried for lack of time.

Controller logic was based on Reference 3, pages 6-SERVO-1 through 6-SERVO-20.

2.1.6 PROGRAM CODE AND SAMPLE INPUT

Appendix A shows the program edits used to add the controller logic to Program J196. A nomenclature list is included.

Appendix B shows the input used to develop the necessary calculations from program J196 to do the required pretest predictions.

2.2 CONTROLLER LOGIC VERIFICATION AND PRETEST PREDICTIONS

A 40-hour metabolic profile was run on the J196 program, and values for the gain constants K_1 , K_2 , K_3 and K_4 were varied to obtain optimum controller action. Figures 4 and 5 show the best results that were obtained before an actual hardware test of a simulated controller was run. Figure 4 shows the metabolic profile vs. time. On the same graph, the controller selected inlet temperature and the resulting LCG ΔT are plotted. Figure 5 shows the resulting heat stored vs. time and how it compares to the comfort limits. On the same graph, controller action is shown by a plot of LCG inlet temperature vs. time.

The best values for the controller parameters resulting from these computer runs were as follows:

- a. Values for the inlet temperature vs. LCG ΔT at steady state comfort were taken from figure 2.
- b. Values for $\Delta \Delta T$ vs. ΔT while tracking perfect comfort were taken from figure 3.
- c. Values for K_1 , K_2 , K_3 and K_4 were set at 0.085, 2.6, 0.0000001, and 0.01, respectively.

Pretest predictions of the controller test profile were run using the best controller logic achieved to that point. Metabolic rate levels were proposed to be 15 minutes each of 800, 2000, 400, and 1600 Btu/hr. Results are shown in figure 6. This graph shows heat stored vs. comfort limits. Valve action is shown by plotting inlet LCG temperature for expected test conditions. Recommendations for the test simulated controller included the following:

- a. Set point values for the two curves were set at the figure 2 and 3 values as before.
- b. K_1 , K_2 , K_3 , and K_4 values were set at 0.0952, 2.912, 0.0000001, and 0.01, respectively.

3. CONCLUSIONS AND RECOMMENDATIONS

3.1 CONCLUSIONS

It can be concluded from computer simulation that crewman comfort can be assured by using automatic control of the inlet temperature of the coolant into the LCG when input to the controller consists of measurements of the LCG inlet temperature and ΔT . Subsequent tests using a facsimile of the control logic developed in the computer program confirmed the feasibility of such a design scheme.

Automatic comfort control has been demonstrated as a desirable product improvement. It is not a design requirement.

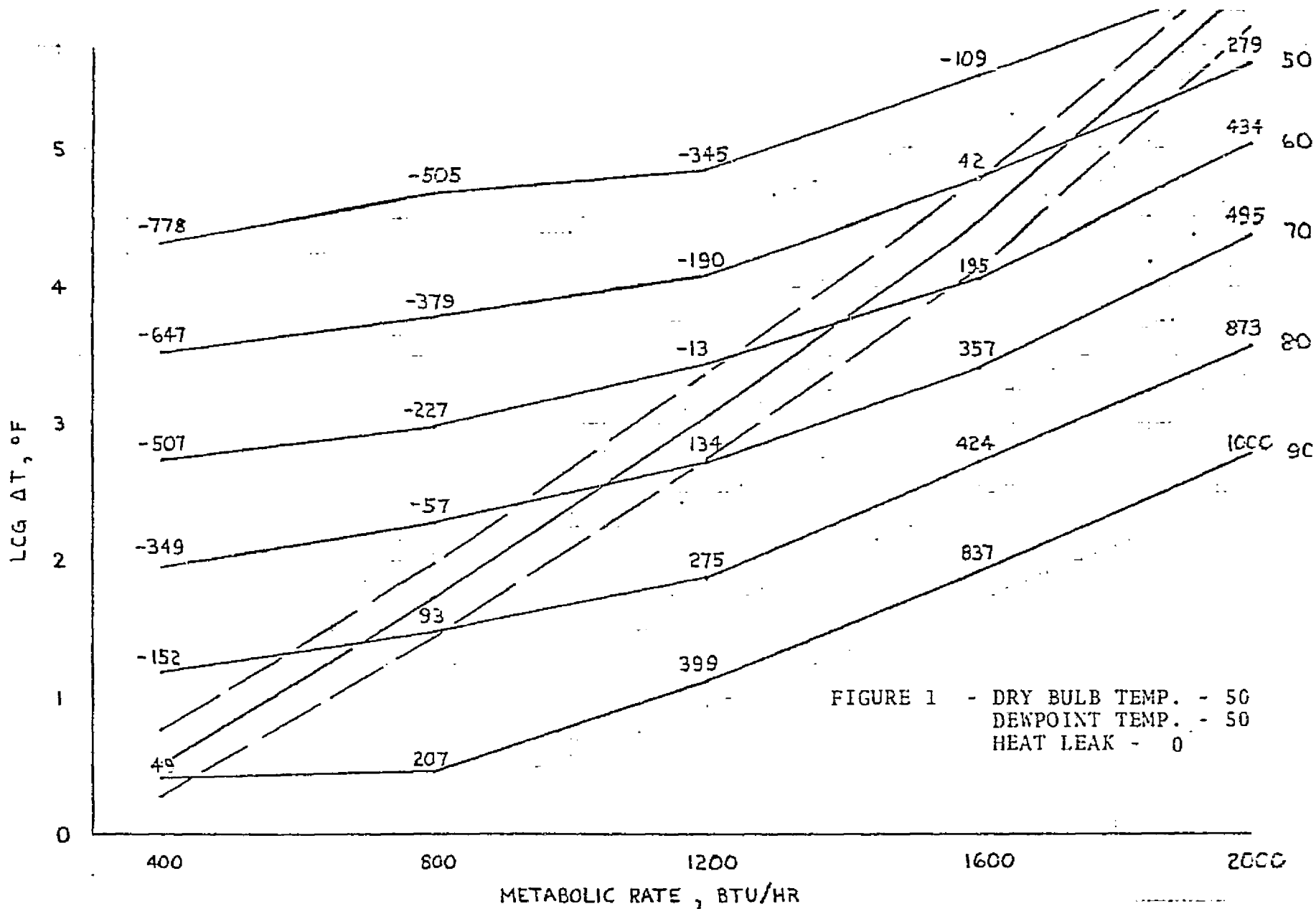
3.2 RECOMMENDATIONS

This controller should be fabricated and tested if funds can be made available for product improvement or if some reason is discovered that makes the inclusion of the device mandatory.

Design of the controller should include manual adjustment for shifting the curves from figures 2 and 3 to conform to physical changes such as a heat leak or inlet suit ventilation conditions and to compensate for personal preferences in comfort level. Design provisions should also be included in the PLSS hardware to allow that the controller be bypassed and that manual control of the diverter valve be available.

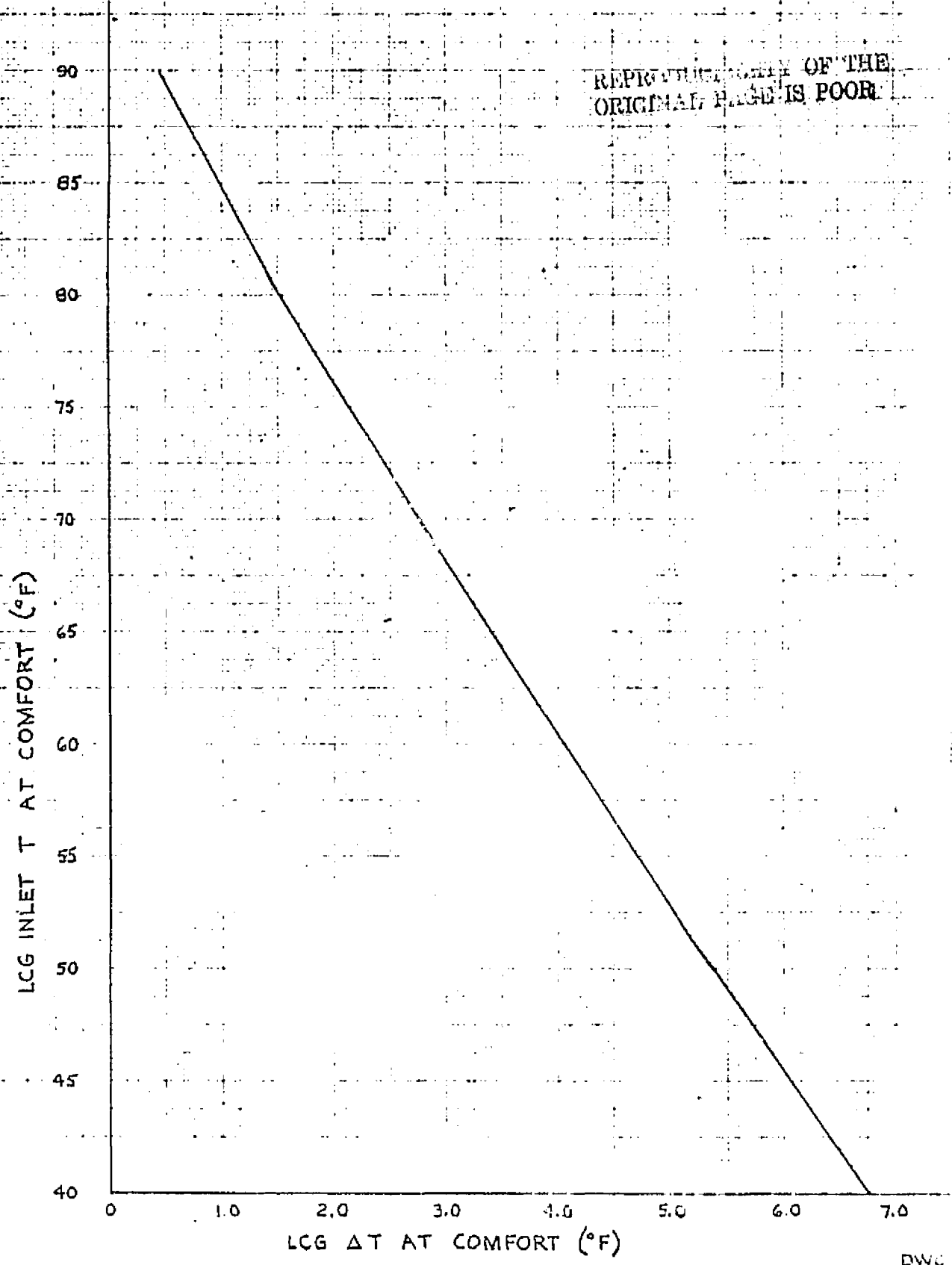
Final values of K_1 , K_2 , K_3 , and K_4 should be determined by test. Final values for curves 2 and 3 can also be fine-tuned in testing. Output differential and integral compensation should be tested on both methods and error differential and integral compensation tried on method 1.

Recommendations for controller logic considerations were taken from reference 3, pages 6-SERVO-1 through 6-SERVO-20.



LCG INLET TEMPERATURE VS ΔT AT COMFORT

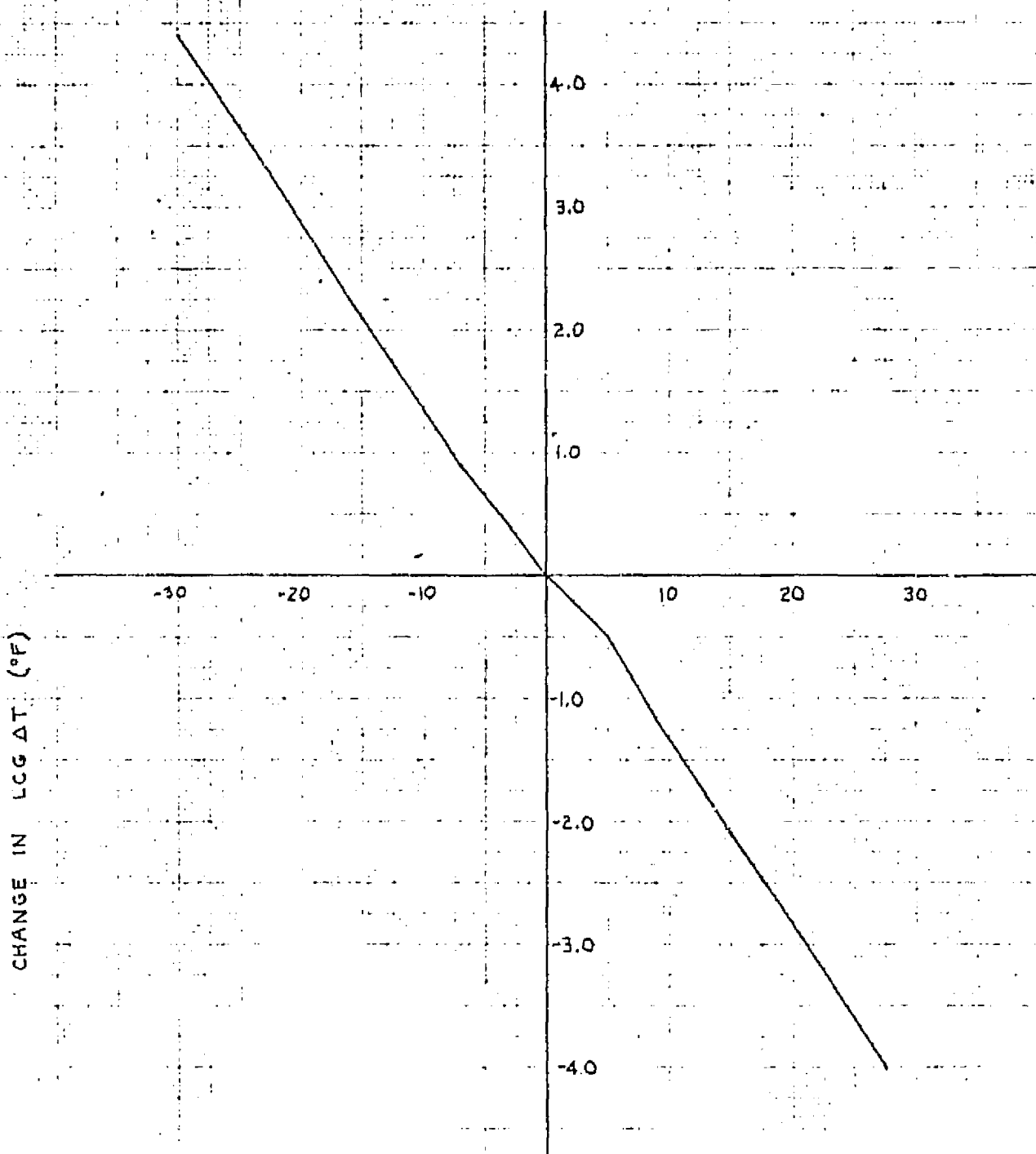
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CHANGE IN LCG ΔT VS CHANGE IN LCG INLET TEMPERATURE WHILE TRACKING COMFORT

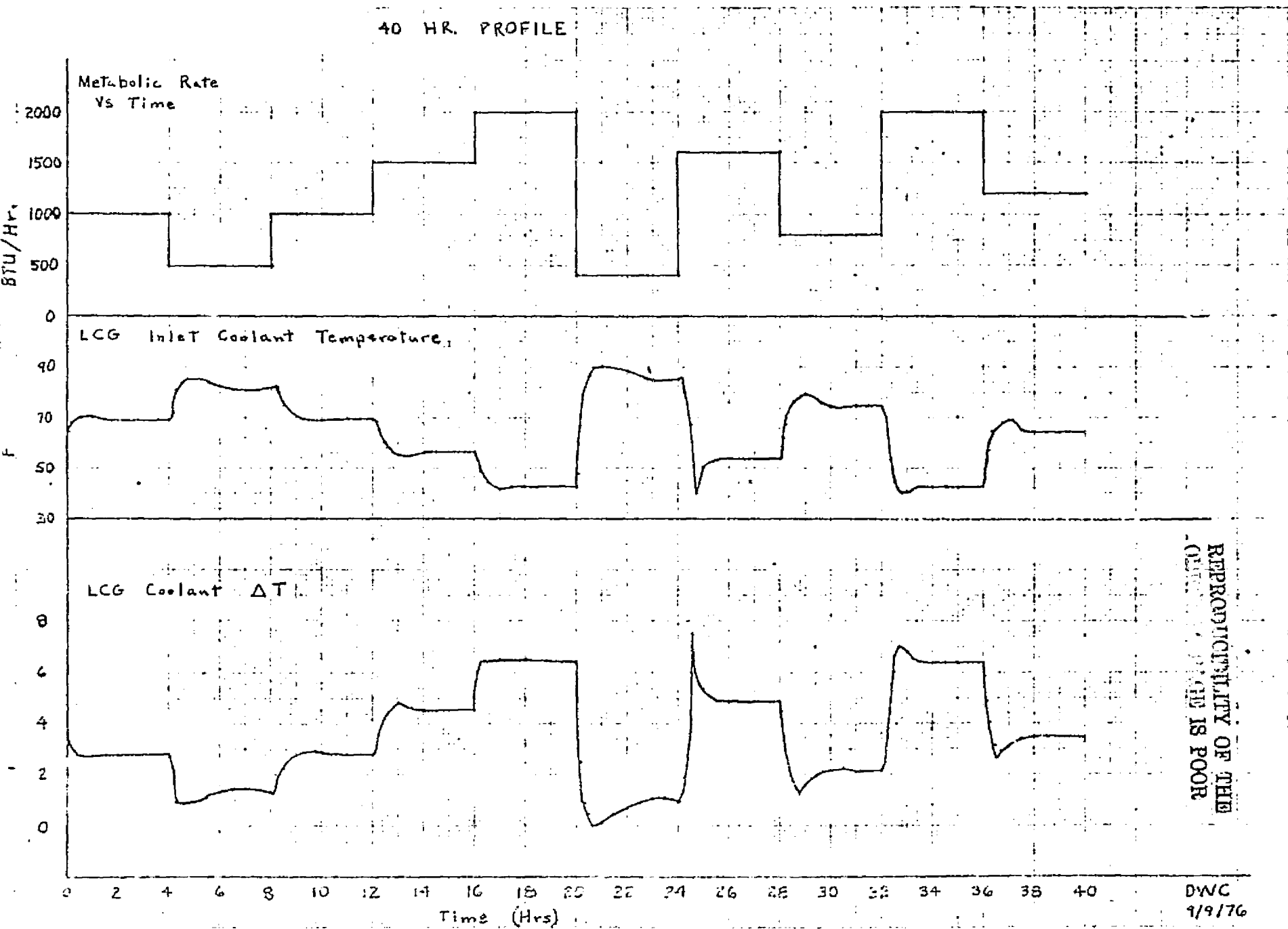


CHANGE IN LCG INLET T (°F)

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FIGURE 4

40 HR. PROFILE

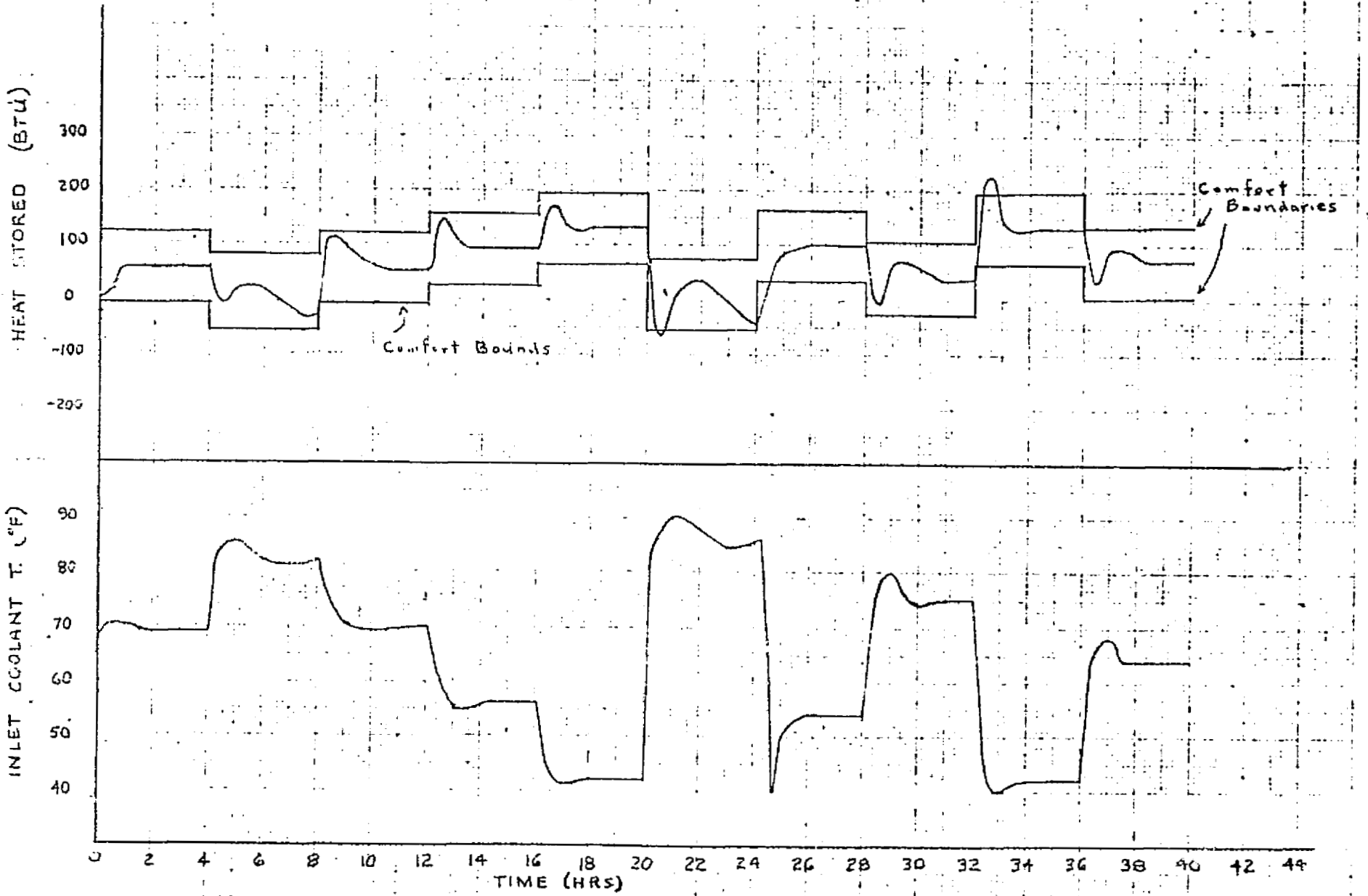


FIGURE 5

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Shuttle EMU Simulated
Controller Test

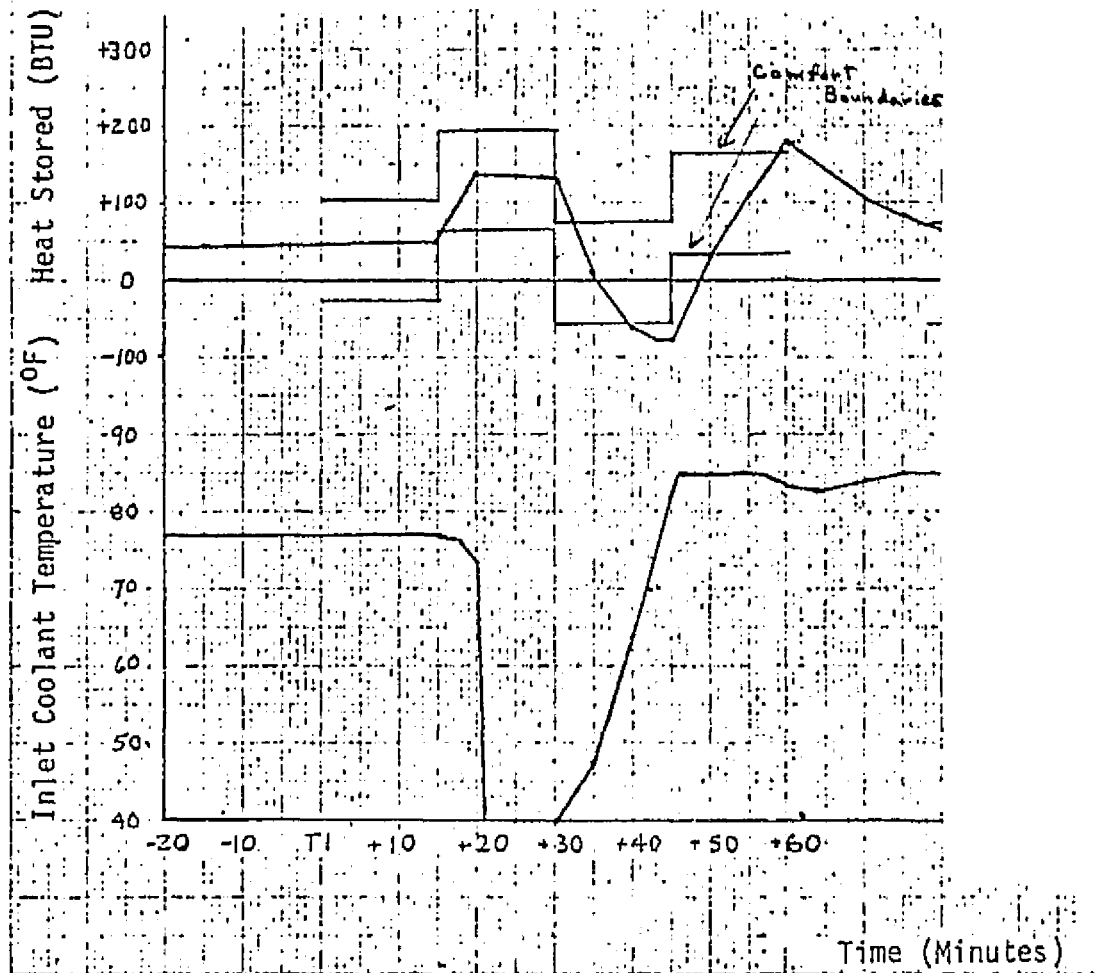


FIGURE 6

REFERENCES

1. Morgan, Lois W., et al: 41-Node Transient Metabolic Man Program, LEC/672-23-030031, May 1970.
2. Cook, D. W.: EMU Comfort Reference Data, TM-675-44-00103, August 25, 1970
3. Barker, R. S., et al: G-189A Generalized Environmental/Thermal Control and Life Support Systems Computer Program, McDonnell Douglas Contract NAS9-10330, September 1971.

APPENDIX A

PROGRAM EDITS TO MODEL THE
PROPOSED CONTROLLER
(NOMENCLATURE LIST IS INCLUDED)


```
00302 302* C SO THAT CRANE CAN STEP MORE ACCURATELY 000220
00304 303* CALL DISCON 000222
00305 304* 245 CONTINUE 000225
00306 305* ENDONX=.TRUE. 000225
00307 306* JT=JT+1 000226
00310 307* XHATAR(JT)=SETI/60. 000231
00311 308* IF(JT.EQ.1)GO TO 247 000235
00311 309* C PUT THE XHAT VALUES IN ASCENDING ORDER 000235
00313 310* CALL ASCEND(XHATAR,JT) 000240
00314 311* 247 CONTINUE 000245
00315 312* XHAT=XHATAR(1) 000245
00316 313* IXH=1 000246
00317 314* PREC=5. 000250
00320 315* IF(ICOND.EQ.0) PREC=3. 000252
00322 316* QLGT=-1. 000256
00323 317* DTIME=DT/60. 000260
00324 318* MIN=3 000263
00325 319* VPPCAB = VPP(TDE,C) 000265
00326 320* SPHCAB=VPPCAB*18/(PCAB*29.) 000271
00327 321* TOTCO2=0.0 000276
00330 322* TOTO2=0.0 000277
00331 323* TOTWCN=0.0 000300
00332 324* FOWTR=0.0 000301
00333 325* 837 CONTINUE 000303
00334 326* H=DTIME 000303
00335 327* INITL=0 000304
00336 328* HC=H NEW 000305
00337 329* AP=ARI 000307
00340 330* IF(MODE.GT.0) AR=AC 000311
00342 331* IF(MODE-1)21,22,23 000316
00345 332* 21 WRITE(6,117) 000322
00347 333* 117 FORMAT(16X,17HSHIRTSLEEVES MODE/) 000327
00350 334* GO TO 26 000327
00351 335* 22 WRITE(6,118) 000331
00353 336* 118 FORMAT(18X,18HNORMAL SUITED MODE/) 000335
00354 337* GO TO 26 000335
00355 338* 23 IF (MODE.GT.2) GO TO 24 000337
00357 339* EVA = .TRUE. 000342
00360 340* WRITE(6,119) 000344
00362 341* 119 FORMAT(21X, 8HEVA MODE/) 000351
00363 342* GO TO 26 000351
00364 343* 24 WRITE(6,120) 000353
00366 344* 120 FORMAT(13X,27HSUITED WITH HELMET OFF MODE/) 000360
00367 345* 26 IF (IPL0P) WRITE(6,1001) 000366
00372 346* 1001 FORMAT(18X,12HPOST LANDING) 000366
00373 347* IF(.NOT. IPL0P) GO TO 1210 000366
00375 348* *WRITE(6,1702)PLAS,TATH,VOLCAB,POZA,PNZA,CPA,NUMEN,PA,AREAW, 000370
00378 349* * TDE=AC,CFMC 000370
00412 350* 170. FORMAT(' ATMOSPHERIC GAS CONSTANT, Lbf-ft/(lBM-DEG R)-----',F9.3/ 000411
00412 351* 1 ' DRYJULB TEMP. OF ATMOSPHERE, DEG.F-----',F9.3/ 000411
00412 352* 2 ' VOLUME OF CAPIN, CU FT-----',F9.3/ 000411
00412 353* 3 ' ATMOSPHERIC OXYGEN PARTIAL PRESSURE, PSIA-----',F9.3/ 000411
00412 354* 4 ' ATMOSPHERIC NITROGEN PARTIAL PRESSURE, PSIA-----',F9.3/ 000411
00412 355* 5 ' SPECIFIC HEAT OF ATMOSPHERE, BTU/(LBM-DEG F)-----',F9.3/ 000411
00412 356* 6 ' NUMBER OF MEN-----',I9/ 000411
00412 357* 7 ' ATMOSPHERIC PRESSURE, PSIA-----',F9.3/ 000411
00412 358* 8 ' CABIN WALL AREA, SQ FT-----',F9.3/ 000411
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1002 587* WRITE(6,99)
1004 588* MODEG=MODE
1005 589* MODE=MODEC
1006 590* EVA=.FALSE.
1007 591* GO TO 887
1010 592* 888 CONTINUE
1011 593* IF (CTCIN) CALL LAGIN (1,CCTGIN,NPTGIN,2,TIME,TGIN)
1012 594* IF (CTDEW) CALL LAGIN (2,CCTDEW,NPTDEW,2,TIME,TDEW)
1013 595* IF (CTWI) CALL LAGIN (3,CCTWI,NPTWI,2,TIME,TWI)
1017 596* IF (CPCAB) CALL LAGIN (4,CCPCAB,NPPCAB,2,TIME,PCAB)
1021 597* IF (CPGC) CALL LAGIN (5,CCPGC,NPPGC,2,TIME,PG)
1023 598* IF (CP02) CALL LAGIN (6,CCP02,NPP02,2,TIME,P02)
1025 599* IF (CRM) CALL LAGIN (7,CCRM,NPRM,2,TIME,RM)
1027 600* IF (CUEFF) CALL LAGIN (8,CCUEFF,NPUEFF,2,TIME,UEFF)
1031 601* IF (.NOT. CWF) GO TO 380
1033 602* WFOLD=.F
1034 603* CALL LAGIN(9,CCWF,NPWF,2,TIME,WF)
1035 604* WDOT1=WDOT1+WF/WFOLD
1036 605* 380 CONTINUE
1037 606* IF (CCFMS) CALL LAGIN (10,CCCFMS,NPCFMS,2,TIME,CFMS)
1041 607* IF (.NOT. CAKS) GO TO 725
1043 608* CALL LAGIN (11,CCAKS,NPAKS,2,TIME,AKST)
1044 609* DO 725 I=1,IG
1047 610* AKS(I)=AKST
1050 611* 725 CONTINUE
1052 612* IF (DAKS) CALL LAGIN(12,DDAKS,UPAKS,2,TIME,AKS(I))
1054 613* 730 IF (.NOT. COASRB) GO TO 400
1055 614* DO 726 I=1,IG
1056 615* CALL LAGIN(13,CCQASR(I,I),NPQASR,2,TIME,QASRB(I))
1062 616* 726 CONTINUE
1064 617* 430 CONTINUE
1065 618* IF (TRAN .OR. IO.EQ. 0) GO TO 430
1067 619* CALL TRATRX
1070 620* 430 CONTINUE
1071 621* DLTAT1=DLTAT
1072 622* WILDLT=WILDLT
1073 623* CALL SUT
1074 624* DELTAT=TWO-TWI
1075 625* TWI=TWI
1076 626* OLDLT=DLTAT-DLTAT1
1077 627* EDLDT=EDLDT+H/H0
1078 628* WOLDLT=OLDLT-EDLDT
1081 629* EDLDT=EDLDT+(WOLDLT-WILDLT)*H/H0
1082 630* WOLDLT=WOLDLT+EDLDT+H
1083 631* WOLDLT=WOLDLT+DDELDT+DDELDT+DDELDT
1084 632* CALL LAGIN(9,CCDELDT,8,7,DELDT,TWI)
1085 633* TWI=TWI+2.6*DT*W
1086 634* CALL LAGIN(9,CCDELDT,8,2,DELDT,TWI2)
1087 635* TWI2=TWI+0.035*(TWI2-TWI)
1088 636* TWI=(TWI+TWI2)/2.0
1089 637* IF (TWI.GT.93.0) TWI=93.0
1090 638* IF (TWI.LT.40.0) TWI=40.0
1091 639* DT*I=TWI-TWI1
1092 640* CALL LAGIN(10,CCDTWI,8,2,DTWI,EDLDT)
1093 641* HO=H
1094 642* CO2RATE= (0.001708-(1.0-0.707)/0.293*0.000123)*RM
1095 643* CO2RAT=CO2RATE+44.0/32.0*RL

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1244 701* KOUNTR = KOUNTR+24
1245 702* 704 IF (IMPAIP .AND. OSTOR .GT. 1000) GO TO 706
C1247 703* GO TO 705
C1250 704* 706 IF (KOUNTR .GT. 24) GO TO 709
C1252 705* WRITE (6,632)
1254 706* WRITE (6,601)
1255 707* GO TO 714
1257 708* 709 WRITE (6,99)
C1261 709* WRITE (6,601)
C1263 710* 714 WRITE (6,608)
C1265 711* TERM=.TRUE.
1266 712* GO TO 14
1267 713* 705 CONTINUE
1270 714* WRITE (6,113) PTIM,IGOUTS,SHSO,T(1),T(72),TISAV,TOSAV,QTSUIT,SOUG,
C1271 715* ICEVAP,TOTL,STORAT,OSHTV,OSTOR
C1272 716* SUBOT = SUBOUT - SUBIN
1273 717* OTPP=760.0/14.7*PH20SO
1274 718* TDEWOT=DEWPT (OTPR)
1275 719* OTPRI=PG*SHSO*32.0/16.0*760.0/14.7
1276 720* TOWOT1=DEWPT (OTPRI)
C1277 721* SATPRS=VPP (IGOUTS)
C1278 722* HELPM=PH20SO/SATPRS
C1279 723* IF (LCG) WRITE (6,999) T*1,T*0,DELTA T,IDEW,TGIN,TOTCO2,TOTCO2,TOTWCN,
1280 724* FDNTR,RM,WF
1281 725* NAMELIST/NO1/T*1,DLTAT1,DLDT,DLDTL,WDLDT,DT*1,EDLDT,TW12
1282 726* WRITE (6,901)
C1283 727* IF (MODE .EQ. 1 .OR. MODE .EQ. 2) WRITE (6,2032) HCO2MH
C1284 728* IF (IPLOP) WRITE (6,1033) TCAO,TDEWC,CO2MMH
C1285 729* 1605 FORMAT (15H CABIN TEMP =,F7.2, 6H DEG F,18H DEWPOINT TEMP =,
1286 730* F7.2, 5H DEG F,17H CO2 PRESSURE =,F7.2, 6H MM HG/)
C1287 731* OLATR = OLAT(1) + OLAT(5) + OLAT(2) + OLAT(3) + OLAT(6)
1288 732* IF (IPLOP) GO TO 1605
C1289 733* IF (KOUNTR .EQ. 48) GO TO 1606
1290 734* KOUNTR = KOUNTR + 3
1291 735* GO TO 1608
C1292 736* 1606 WRITE (6,112)
C1293 737* KOUNTR = 0
C1294 738* GO TO 1608
C1295 739* 1605 IF (KOUNTR .EQ. 48) GO TO 1607
C1296 740* KOUNTR = KOUNTR + 4
1297 741* GO TO 1608
C1298 742* 1607 WRITE (6,112)
C1299 743* KOUNTR = 0
1300 744* 1605 IF (TRAN) GO TO 490
1301 745* ASSIGN 14 TO IJM
C1302 746* ASSIGN 12 TO IJMP
C1303 747* GO TO 780
C1304 748* 49. CONTINUE
C1305 749* IF (JT .EQ. 0 .OR. ENDONX) GO TO 915
C1306 750* IXH=IXH+1
C1307 751* IF (IXH .LE. JT) GO TO 910
1308 752* JT=C
1309 753* GO TO 915
C1310 754* 91. ENDONX=.TRUE.
C1311 755* XHAT=XHATAR (IXH)
C1312 756* 915 CONTINUE
C1313 757* C CHECK IF CRANE HAS SET THE FLAG ENDONX TO FALSE TO INDICATE THE

```

```

002135
002141
002151
002153
002156
002163
002170
002172
002176
002204
002210
002212
002214
002214
002214
-01002236
002241
002244
002250
002257
002263
002267
002272
002272
NEW002314
NEW002314
002320
002342
002354
002354
002354
002362
002364
002367
002372
002374
002400
002401
002403
002405
002410
002412
002416
002420
002421
002423
002425
002427
002427
002434
002437
002442
002443
002445
002447
002452
002452

```

NOMENCLATURE OF VARIABLES APPEARING IN CONTROLLER EDITS

<u>Program name</u>	<u>Document engineering symbol</u>	<u>Description</u>
CCDELT	Figure 2	Curve of LCG ΔT vs. inlet temperature at comfort (both in $^{\circ}F$).
CCDLDL	Figure 3	Curve of change in LCG ΔT vs. change in LCG inlet temperature while tracking perfect comfort with the changes in inlet temperature as the dependent variable (all $^{\circ}F$).
CCDLDP	not currently used.	
CCDTWI	Figure 3	Curve of change in LCG ΔT vs. change in LCG inlet temperature while tracking perfect comfort with the change in LCG ΔT as the dependent variable (all $^{\circ}F$).
DELTAT	LCG ΔT	Difference in the liquid cooled garment inlet and outlet coolant temperature ($^{\circ}F$).
DDLDT	$d\Delta T/dt$	Error differential compensation ($^{\circ}F/hr$).
DLDLT	$\Delta\Delta T$ or $d\Delta T/dt$	Change in LCG ΔT with respect to time. (Time cancels out on the $\Delta\Delta T$ vs. ΔT curve) ¹ ($^{\circ}F/hr$ or $^{\circ}F$).
DLTAT1	-----	Difference in the liquid cooled garment inlet and outlet coolant temperatures calculated in previous time step ($^{\circ}F$).
DTWI (first appearance)	ΔT_{in2}	The adjustment signal to the final control element using method 2, figure 3, eq. (2).
DTWI (second appearance)	-----	Final complete adjustment signal to the final control element, T_{in} .

NOMENCLATURE OF VARIABLES APPEARING IN CONTROLLER EDITS (Continued)

<u>Program name</u>	<u>Document engineering symbol</u>	<u>Description</u>
DTWI (second appearance)	dT_{in}/dt	Changes in LCG inlet temperature between current time increment and last ($^{\circ}F/hr$).
EDLDT	$\overline{\Delta\Delta T}$	Expected change in LCG ΔT ($d\Delta T/dt$) that would accompany a change in LCG inlet temperature if perfect comfort were being tracked ($^{\circ}F/hr$).
H	dt	Current time increment (hr).
HO	-----	Previous time increment (hr).
RDLDT	$\int \delta\Delta T dt$	Summation of $\delta\Delta T$ times the time increment ($^{\circ}F/hr$).
TWI (first appearance)	-----	New position of the final control element as calculated by method 2, figure 3, eq. (2) ($^{\circ}F$).
TWI (second appearance)	T_{in}	New position of the final control element ($^{\circ}F$).
TWI1	-----	Position of the final control element at the previous time increment ($^{\circ}F$).
TWI2	-----	Position of the final control element as calculated by method 1, figure 2, eq. (1).
WDLDT	$\delta\Delta T$	Deviation of the actual change in LCG ΔT from the expected change in LCG ΔT
WILDLT	-----	WDLDT at the previous time increment.

APPENDIX B
INPUT TO PROGRAM J196 TO BRING ABOUT
THE NECESSARY CONTROLLER PRETEST PREDICTIONS
AND EVALUATIONS

ELT,ULL DATA

ELT007 RL71-3 09/18/76 08:20:50 (1,2)

00001 000 \$INPUT
00002 000 MODE=2,
00003 NEW 002 MODE=1,
00004 000 RM=1200.,
00005 NEW 002 RM=1000.0,
00006 000 UEFF=0.,
00007 000 AC=19.5,
00008 NEW 002 API=19.5,
00009 -01 000 G=C.,
00010 000 ALUG=0.0141,
00011 000 AKUG=.046,
00012 000 EUG=0.9,
00013 001 ACSUIT=9.22,2.91,2.91,6.38,6.38,0.77,0.77,1.19,1.19,1.85,
00014 001 ARSUIT=7.34,2.22,2.32,5.07,5.07,0.62,0.62,0.96,0.96,1.47,
00015 001 ALS=9*.0078,.021,
00016 001 AKS=9*.000383,.02155,
00017 001 EOS=9*0.91,.62,
00018 001 EIS=16*0.90,
00019 001 WS=15.60,4.89,4.89,10.82,10.82,1.22,1.22,1.95,1.95,2.75,
00020 001 CPS=9*0.22,0.30,
00021 000 GASKE=10*308.,
00022 NEW 002 GASRB=10*120.0,
00023 000 VF=0.0,
00024 000 VOLHMT=0.1968,
00025 000 CFMS=6.,
00026 NEW 002 CFMS=5.90,
00027 000 TGIN=80.,
00028 NEW 002 TGIN=45.0,
00029 000 TDE=50.,
00030 NEW 002 TDE=43.0,
00031 000 CPG=0.22,
00032 000 PG=3.85,
00033 NEW 002 PG=4.0,
00034 000 P02=3.85,
00035 NEW 002 P02=4.0,
00036 NEW 002 LCG=1,
00037 -01 000 WF=240.,
00038 000 TWI=40.,
00039 NEW 002 TWI=72.0,
00040 000 CPW=1.0,
00041 000 UAG=43.5,
00042 000 DT=0.05,
00043 000 PRINTI=5.0,
00044 000 SETI=600.,
00045 NEW 002 SETI=240.0,
00046 NEW 002 MCASES=20.0,
00047 NEW 002 STLPE=.TRUE.,
00048 NEW 002 RM=800.0,
00049 NEW 002 TWI=75.0,
00050 NEW 002 PRINTI=1.0,
00051 000 \$END
00052 NEW 002 \$INPUT
00053 NEW 002 RM=500.0,
00054 NEW 002 SETI=15.0,
00055 NEW 002 RM=800.0,

```
L00056 NEW 002 $END
L00057 NEW 002 $INPUT
L00058 NEW 002 RM=1000.0,
L00059 NEW 002 SETI=450.0,
L00060 NEW 002 SETI=30.0,
L00061 NEW 002 RM=2000.0,
L00062 NEW 002 $END
L00063 NEW 002 $INPUT
L00064 NEW 002 RM=1500.0,
L00065 NEW 002 SETI=720.0,
L00066 NEW 002 SETI=45.0,
L00067 NEW 002 RM=900.0,
L00068 NEW 002 $END
L00069 NEW 002 $INPUT
L00070 NEW 002 RM=2000.0,
L00071 NEW 002 SETI=960.0,
L00072 NEW 002 SETI=60.0,
L00073 NEW 002 RM=1600.0,
L00074 NEW 002 $END
L00075 -15 000 @PHD,B
```

END ELT.

PLP
URPUR 0026-09/18-08:20