## General Disclaimer One or more of the Following Statements may affect this Document

- This document has been reproduced from the best copy furnished by the organizational source. It is being released in the interest of making available as much information as possible.
- This document may contain data, which exceeds the sheet parameters. It was furnished in this condition by the organizational source and is the best copy available.
- This document may contain tone-on-tone or color graphs, charts and/or pictures, which have been reproduced in black and white.
- This document is paginated as submitted by the original source.
- Portions of this document are not fully legible due to the historical nature of some of the material. However, it is the best reproduction available from the original submission.

Produced by the NASA Center for Aerospace Information (CASI)

## NATIONAL AERONAUTITS AND SPACE ADMINISTRATION


(NASA-CR-151058) RESULTS CF PHASE CHANGE HEAT TRARSEEE TEST OHS1 USING $0.006-S C A L E ~ H C ~ A \delta 3 / M F A O I ~$ AND EABTIAL ING O.0175-SCALE HODEL 64-0 IN UnClas THE LABC 31-INCH CFHT (Chrysler Corp.) 4! FG3/16 22929

## SPACE ShUTTLE

## AEROTHERMODYNAMIC DATA REPORT

JOHNSON SPACE CENTER

HOUSTON, TEXAS

DATA $\triangle A N$ agement services
chersics CORPOAATION
DMS-DR-2368
NASA CR-151,058
results of phase change heat transfer test oh5l USING 0.006-SCALE SPACE SHUTTLE ORBITER MODELS 46-0 AND 90-0 AND PARTIAL WING 0.0175-SCALE MODEL 64-O IN THE LaRC 31-INCH CFHT

by<br>J. W. Curmings Shuttle Aero Sciences Rockwell International Space Division

Prepared under NASA Contract Number NAS9-13247

by<br>Data Management Services Úhrysler Corporation Michoud Defense-Space Division New Orleans, La. 70139

for
Engineering Analysis Division

Johnson Space Center
National Aeronautics and Space Administration Houston, Texas

WIND TUNNEL TEST SPECIFICS:
Test Number: LaRC CFHT 112
NASA Series Number: OH51
Model Number: $\quad 46-0,64-0,90-0$
Test Dates:
June 17 through July 3, 1974
Occupancy Hours:
40

FACILITY COORDINATOR:
B. Spencer, Jr.

Mail Stop 365
Langley Research Center
Langley Station
Hampton, Virginia 23665
Phone: (804) 827-3911

PROJECT ENGINEERS:
J. W. Cummings

Mail Code An38
Rockwell International
Space Division
12214 Lakewood Blvd.
Downey, California 90241
Phone: (213) 922-4600

AEROHEATING ANALYSIS ENGINEER:
C. W. Craig

Mail Code AC78
Rockwell International
Space Division
12214 Lakewood B7vd.
Downey, California 90241
Phone: (213) 922-1558

DATA MANAGEMENT SERVICES:
Prepared by: Liaison--D. W. Hersey Operations--Maurice Moser, Jr.

Reviewed by: G. E McDonald

Approved:


Chrysler Corporation Michoud Defense-Space Division assumes no responsibility for the data presented other than publication and distribution.

# RESULTS OF PHASE CHANGE HEAT TRANSFER TEST OH51 USING 0.006-SCALE SPACE SHUTTLE ORBITER MODELS <br> 46-0 AND 90-0 AND PARTIAL WING 0.0175-SCALE <br> MODEL 64-0 IN THE LaRC 31-INCH CFHT <br> by 

J. W. Curmings, Rockwell International Space Division

## ABSTRACT

Test procedures and results of OH 51 are described in this report. Test 0 OH 51 was a phase change paint test conducted in the LaRC 31 -inch CFHT utilizing models $46-0,64-0$, and $90-0$. Model 46-0 represented the Space Shuttle configuration 139 Orbiter. Model 90-0 represented the configuration 140 Orbiter. Model 64-0 represented the forward $45 \%$ portion of the Orbiter wing. The partial wing was tested with a shock generator located at various positions relative to the wing. The test was conducted at Mach 10.0 , angles of attack from $27.5^{\circ}$ through $37.5^{\circ}$, and Reynolds numbers of 0.5 and 1.5 million per foot.
Page
ABSTRACT ..... iii
INDEX OF MODEL FIGURES ..... 2
NOMENCLATURE ..... 3
CONFIGURATIONS INVESTIGATED ..... 4
TEST FACILITY DESCRIPTION ..... 8
DATA REDUCTION ..... 9
REFERENCES ..... 10
TABLES
I. TEST CONDITIONS ..... 11
II. TEST PROGRAM ..... 12
III. MODEL DIMENSIONAL DATA ..... 15
MODEL FIGURES ..... 30

## INDEX OF MODEL FIGURES

Figure Title ..... Page

1. Axis systems. ..... 30
2. Model Sketches.
a. Orbiter Configuration ..... 31
b. Model 64-0 Partial Wing. ..... 32
c. Partial Wing Installation With Shock Generator ..... 33
3. Model Photographs.
a. Orbiter Grid Model Installed in Tunnel ..... 34
b. Partial Wing Model Installed in Tunnel ..... 35
C. Partial Wing Model Mounting Assembly ..... 36
d. Partial Wing Model With Shock Generator ..... 37

## NOMENCLATURE

| Symbol | Definition |
| :---: | :---: |
| M | freestream Mach number |
| $P_{0}$ | freestream stagnation pressure, psia |
| $\mathrm{Re} / \mathrm{ft}$ | freestream unit Reynolds number, million per foot |
| $\mathrm{T}_{0}$ | freestream total temperature, ${ }^{\circ} \mathrm{F}$ |
| $\mathrm{T}_{\mathrm{pc}}$ | paint phase change temperature, ${ }^{\circ} \mathrm{F}$ |
| X | longitudinal distance between shock generator leading edge and wing model reference point as defined in figure 2 c , in . |
| $x_{0}$ | Orbiter longitudinal coordinate, in. |
| $Y$ | lateral distance between shock generator centerline and wing model reference point as defined in figure $2 c$, in. |
| $Y_{0}$ | Orbiter lateral coordinate, in. |
| Z | vertical distance between shock generator and wing model reference system as defined in figure 2c, in. |
| $Z_{0}$ | Orbiter vertical coordinate, in. |
| $\alpha$ | angle of attack, deg. |
| $\beta$ | angle of sideslip, deg. |
| $\mathrm{T}_{\mathbf{i}}$ | initial model temperature before model is injected into tunnel, ${ }^{\circ} \mathrm{F}$ |
| b/2 | semi-span |
| C | local chord, inches |
| IML | inner mold line |
| OML | outer mold line |

## CONFIGURATIONS INVESTIGATED

Three different configurations were investigated. Model 64-0 was a partial model of the Orbiter wing. Model 46-0 represented the Orbiter - 139 configuration. Model 90-0 represented the Orbiter - 140 configuration. The shock generator edge model was cut from an existing 0.0175 -scale, Grumman built, Material "G", Orbiter paint model 21-0. Two identical models were fabricated: one for testing at $\alpha=30^{\circ}$ and the other for testing at $\alpha=35^{\circ}$. The model was cut from the left hand wing to have dimensions from the $35 \%$ semi-span to the wing tip and cut along a line three i:aches from the leading edge and parallel to the $45^{\circ}$ sweep angle. The model was sting mounted directly to the tunnel support system. A removable thin metal plate was attached at the $35 \%$ semi-span. A third leading edge model was fabricated and painted with strips to be used as a grid reference system. The model was defined by Rockwell drawing SS-H-01304 and is shown in figures $2 b$ and $3 c$.

The leading edge wing model was sting mounted to the tunnel support system and positioned to be visible in the Schlieren window. The shock generator consisted of a series of sharp nose cones attached to a strut and located forward of the wing leading edge model. Six cones were provided which had half angles of $25^{\circ}, 27^{\circ}, 28^{\circ}, 29^{\circ}, 30^{\circ}$, and $32^{\circ}$. All cones were made from 17-4 PH stainless steel and all were removable. The shock generator was attached to the injection system floor. Shock strength and location were varied by changing cones and location of the generator. It was defined by Rockwell drawing SS-H-01305. Figures

## CONFIGURATIONS INVESTIGATED (Continued)

2c and 3d show the shock generator installation with the partial wing model.
The 0.006 paint model $46-0$ was sting mounted to the tunnel support system utilizing the $W$ - $118 S A$ bent sting adapter. The model was rolled $90^{\circ}$ clockwise from the conventional position and located in the Schlieren window in the same general location as the leading edge wing model. The n.nn6 paint model 90-0 was stinq mounted to the tunnel support system and rolled $90^{\circ}$ utilizing the SS-H-00386-1 bent sting adapter. A reference arid model was available for each configuration. All models were leveled in pitch and roll prior to testing. Figure 2a shows the general Orbiter configuration. Figure 3a shows an Orbiter grid model mounted in the tunnel.

Two $35-\mathrm{mm}$ cameras were aligned and focused on the model in the tunnel, one from the top and one from the side. When taking paint data, both cameras operated together. When Schlieren coverage was required, the side camera was "cranked" down out of the way. When testing the leading edge wing model, the initial location of the shock generator was positioned at pre-determined values. Upon evaluation of the Schlieren photographs, the shock generator was adjusted as required to position shock impingement. Any movement in the shock generator was noted and recorded as given in Table II.

Before each run, the initial temperature of the model was determined by a digital contact thermometer. This thermometer was mounted on the end of a probe, which was placed against the model surface for a reading. Before and after a run, the model was in the injection chamber outside

## CONFIGURATIONS INVESTIGATED (Continued)

of the test section. Only after flow was established was the model and support system injected. Continuous pictures were taken throughout the test period. At the end of the test period, the model was withdrawn. The test period was determined by the paint-melt temperature and estimated heating rates. ifter the model was removed from the injection chamber and replaced by a freshly painted model, specific areas of interest on the tested model were photographed at various angles with a Polaroid camera. After all photographs were completed, the model was washed with a solvent to remove the remaining paint. Fresh paint was then sprayed on to prepare the model for another run.

The models were denoted as follows:

| Configuration <br> Designation | Model | Component Designation |
| :--- | :--- | :--- |
| Wing | $64-0$ | $W_{123}$ |
| 139 ORB | $46-0$ | $B_{17} C_{7} F_{5} M_{4} V_{7} W_{103} E_{22}$ |
|  |  | $R_{5}$ |
| 140 ORB | $90-0$ | $B_{26} C_{9} F_{8} M_{7} V_{8} W_{116} E_{22}$ |
|  |  | $R_{5}$ |

Where individual component designations were as follows:
Nomenclature Description
${ }^{B} 17$
Body (46-0)

| Nomenclature | Description |
| :---: | :---: |
| $\mathrm{B}_{26}$ | Body (90-0) |
| $C_{7}$ | Canopy ( $46-0$ ) |
| $c_{9}$ | Canopy (90-0) |
| $\mathrm{F}_{5}$ | Body Flap (46-0) |
| $\mathrm{F}_{8}$ | Body Flap (90-0) |
| $M_{4}$ | OMS Pods ( $46-0$ ) |
| $\mathrm{M}_{7}$ | OMS Pods (90-0) |
| $v_{7}$ | Vertical Tail (46-0) |
| $V_{8}$ | Vertical Tail (90-0) |
| $W_{103}$ | Wing used with body $\mathrm{B}_{17},(46-0)$ |
| $W_{116}$ | Wing used with body $\mathrm{B}_{2} .(90-0)$ |
| $W_{123}$ | Partial wing fabr:cated from left wing of model 21-0, (64-9) |
| $E_{22}$ | elevon |
| $\mathrm{R}_{5}$ | rudder |

The Mach 10 nozzle of the Langley Continuous Flow Hypersonic Tunnel is designed to operate at stagnation pressures of 15 to 150 atmospheres at temperatures up to $1960^{\circ}$ R. Air is preheated electrically by passing it through a multi-tube heater. The nozzle has a 31 -inch square test section which incorporates a movable second minimum. Continuous operation is achieved by passing the air through a series of compressors. Additional information on this facility is given in NASA TM X-1130 entitled, "Characteristics of Major Active Wind Tunnels at the Langley Research Center," by William T. Schaefer, Jr.

Recorded data consisted of motion picture film recorded by the cameras outside the tunnel. These data are retained by:

James C. Dunavant
Mail Stop 408
Langley Research Center
Hampton, Va. 23665
Phone: (804) 827-3984
Use of the data should be obtained through contact with the abjve person.

1. SD74-SH-0017, "Pretest Information For Tests of an 0.0175-Scale Leading Edge Wing Model (64-0) and a 0.006 Scale Paint Model (46-0 and 90-0) in the Langley Research Center, Variable Density, Mach Wind Tunnel (Test OH51)," By D. G. Walstad, March 6, 1974.
2. Jones, R. A. and Jaeger, Hunt: "Use of Temperature Indicators for Obtaining Quantitative Aerodynamic Heat Transfer Data." NASA-TRR-230 (Feb. 1966).
3. Carslaw, H. S. and Jaeger J. C.: "Conduction of Heat in Solids." Oxford Clarenden Press (1959).
4. SAS/WT0/74-407, Trip Report for Test OH51, Model 64-0, Wing and Shock Generator Including Two (2) 0.006-Scale Full Span Orbiters. By J. W. Cummings, dated July 23, 1974.

TABLE 1.

TEST : OH51 (LaRC CFHT 112)
DATE: Po.st-test
TEST CONDITIONS

| MACH MUMBER | REYNOLDS NUMBER <br> (per foot) | DYMAMIC PRESSURE <br> (pounds/sq. inch) | STAGNATION TEMPERATURE <br> (degrees Fahrenheit) |
| :---: | :---: | :---: | :---: |
| 10.0 | $1.5 \times 10^{6}$ | 7.788 | 1375 |
| 10.0 | $0.5 \times 10^{6}$ | 2.424 | 1350 |
|  |  |  |  |
|  |  |  |  |
|  |  |  |  |
|  |  |  |  |
|  |  |  |  |
|  |  |  |  |
|  |  |  |  |
|  |  |  |  |
|  |  |  |  |
|  |  |  |  |
|  |  |  |  |
|  |  |  |  |
|  |  |  |  |
|  |  |  |  |
|  |  |  |  |
|  |  |  |  |
|  |  |  |  |
|  |  |  |  |
|  |  |  |  |
|  |  |  |  |
|  |  |  |  |
|  |  |  |  |

BALANCE UTILIZED: $\qquad$
CAPACITY:
ACCURACY:
COEFFICIENT
TOLERANCE:


COMMENTS:

TABLE II. - TEST PROGRAM


TABLE II. - Continued.

| Config. | $\begin{gathered} \alpha \\ (\operatorname{deg}) \end{gathered}$ | $\begin{aligned} & \mathrm{Re} / \mathrm{ft} \\ & \text { (million/ft) } \end{aligned}$ | $\stackrel{\mathrm{P}_{0}}{(\text { psia) }}$ | $\begin{gathered} \left.\mathrm{T}_{\mathrm{o}}^{\mathrm{F}}\right) \end{gathered}$ | $\left({ }^{T}{ }_{\left({ }^{\circ}+\right.}^{F}\right)$ | $\begin{gathered} \mathrm{T} \mathrm{pc} \\ (\mathrm{O}) \end{gathered}$ | Cone half angle (deg) | X | tion Y | Z | Run No. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Wing | 30 | 0.5 | 375 | 1350 | 78 | 350 |  |  |  |  | 24 |
|  | 37.5 | . |  | 1350 | 78 | $0{ }^{1}$ |  |  |  |  | 25 |
|  | 30 |  |  | 1350 | 78 | 250 |  |  |  |  | 26 |
|  | 30 |  |  | 1355 | 79 | 011 |  |  |  |  | 27 |
|  | 35 |  |  | 1360 | 79 | 350 |  |  |  |  | 28 |
|  | 27.5 |  |  | 1370 | 80 | 350 |  |  |  |  | 29 |
|  |  |  |  | 1370 | 80 | 250 |  |  |  |  | 30 |
|  | 27.5 |  |  | 1370 | 80 | 250 |  |  |  |  | 31 |
|  | 35 |  |  | 1375 | 80 | $0 i 1$ |  |  |  |  | 32 |
|  | 27.5 |  |  | 1380 | 80 | $0 i 1$ |  |  |  |  | 33 |
|  | 32.5 | $\downarrow$ | $\downarrow$ | 1385 | 80 | $0 i 1$ |  |  |  |  | 34 |
|  |  | SHOCK GENER | ATOR IN | L3LED |  |  |  |  |  |  |  |
|  |  | T | $T$ | 1350 | 75 | 350 | 25 |  |  |  | $35$ |
|  | I |  |  | 1405 1340 | 75 75 | 250 0.1 | I | I | $\downarrow$ | $J$ | 36 37 |
|  | 35 | $1$ |  | 1330 | 75 | 350 |  |  |  |  | 38 |
|  | 30 |  | $\downarrow$ | 1335 | 77 | 350 | I | T | I | I | 39 |
|  | 35 | 0.5 | 375 | 1360 | 77 | 250 | 28 | 5.0 | 2.79 | 1.32 | 40 |
|  | 30 |  |  | 1360 | 77 | 250 | T | T |  | T | 41 |
|  | 35 |  |  | 1375 | 78 | $0 i 1$ |  |  |  |  | 42 |
|  | 30 |  |  | 1375 | 78 | $0 i 1$ | $\downarrow$ | $\downarrow$ | $\downarrow$ |  | 43 |
|  | 30 |  |  | 1380 | 78 | 350 | 29 | 5.0 | 2.93 | 1.34 | 44 |
|  | 30 |  |  | 1385 | 80 | 250 |  |  |  | I | 45 |
|  | 30 |  |  | 1335 | 80 | 0 il | $\downarrow$ | 1 | $\downarrow$ | $\downarrow$ | 46 |
|  | 35 |  |  | 1320 | 80 | 350 | 30 | 5.0 | 3.07 | 1.36 | 47 |
|  | 30 |  |  | 1300 | 80 | 350 | T | T | T | T | 48 |
|  | 35 |  |  | 1330 | 80 | 250 |  |  |  |  | 49 |
|  | 30 | , |  | 1350 | 80 | 250 |  |  | - |  | 50 |
|  | 35 30 | $\downarrow$ | $\downarrow$ | 1345 1360 | 75 75 | $0 i 1$ $0 i 1$ | $\downarrow$ | $\downarrow$ | $\downarrow$ | $\downarrow$ | 51 52 |

TABLE II. - Concluded.


TABLE III. - MODEL DIMENSIONAL DATA

| MODEL COMPONENT: $\frac{\text { Body }\left(B_{17}\right)}{1}$ |
| :--- |
| GENERAL DESCRIPTION: $\quad$ Basic fuselage for models $46-1,-2,-3,-4$. |

Model Scale $=0.00593$
DRAWING NUMBER

## V170-000139

DIMENSION:
Lemath~in.
Max Width~in.
Max Depth~in.
Fineriess Ratio
Areo $\sim \mathrm{ft}^{2}$
Mux Cross-Sectional
Planform
Wetted
Bose

FULL SCALE MODEL SCALE
$\xrightarrow{1290.3} \quad 7.65148$ $267.6 \quad 1.58687$
$244.5 \quad 1.44988$

- 82175 (172175
$\qquad$
$\qquad$
—

HOLEL CO:PCHERT: BODY - $B_{26}$

GERERAL OESCRIPTIOR: Orbiter Fuselage Configuration $140 \mathrm{~A} / \mathrm{B}$
NOTE: B2indentimal to B2, except underside of fuselage refaired to accept $\mathrm{N}_{116}$.

Model Scale $=0.006$
VL70.000193
DRAWIK RU: SER:
VL70-0001401

DIMENSIOUS:

Length (Bodj; Fwd Sta $X_{0}=235$ ) - in.
Mix. Kidth (at $X_{0}=1520$ ) - in.

Max. Depth (at $X_{0}-1464$ ) - in.
FULL-SCALE MODEL SCALE

Fineness katio


Arca - $\mathrm{rt}^{2}$

| Man. Cross-Sectional |  |
| :--- | :--- |
| Planform |  |
| Ketted |  |
| Base |  |

TABLE III. - Continued.

| MODEL COMPONENT: Canopy ( $C_{7}$ ) |  |  |
| :---: | :---: | :---: |
| GENERAL DESCRIPTION: 3 configurations per lines VL70-000139. InsufficientInformation to complete dimensional data at this time. |  |  |
|  |  |  |
| Model Scale $=0.006$ |  |  |
| DRAWING NUMBER VL70-000139 |  |  |
| DIMENSION: | FULL SCALE | MODEL SCALE |
| Length (Sta. Fwd. Bulkhead) | 432.70 | 3.0309 |
| Mox Width (T.E. Bulkhead) | 571.40 | 3.997 |
| Max Depth (WPZ $=\ldots$ to $Z_{0}=501$ ) |  |  |
| Fineness Ratio |  |  |
| Area |  |  |
| Max Cross-Sectional |  |  |
| Planform |  |  |
| - Wetted |  |  |
| Base |  |  |

MODEL DIMENSIONAL DATA - Continued.

MODEL COMPONENT : Canopr (C9)
GENERAL DESCRIPTION : Configuration_14OB

Model Scale $=0.006$
VL70-000140B
DRAWING NUMBER: VL70-000143A

DIMENSIONS


TABLE III. - Continued.

MODEL COMPONENT: ELEVON E22

GENERAL OESCRIPTION: Design configuration 3, right wing only

Mode1 Scale: 0.006

DRAWING NUMBER:
VL70-000139

DIMENSIONS:
Area- $\mathrm{Ft}^{2}$
Span (equivalent) - In.
Inb'd equivalent chord - In.
Outb'd equivalent chord - In.
Ratio movable surface chord/ total surface chord

At Inb'd equiv. chord
At Outb'd equiv. chord
Sweep Back Angles, degrees
Leading Edge
Tailing Edge
Hingeline
Area Moment (Normal to hinge line)

| FULL-SCALE |  |
| :--- | :--- |
| $\frac{205.52}{353.34}$ |  |
| $\frac{114.78}{55.00}$ |  |

$\frac{0.208}{0.400} \quad \frac{0.208}{0.400}$

| Leading Edge | 0.00 | -0.00 |
| :--- | :--- | :--- |
| Tailing Edge | -10.24 | -10.24 |
| Hingeline | -0.00 |  |
| Area Moment (Normal to hinge line) |  |  |

GENERAL DESCRIPTION: Body flap located on the lower aft end of the orbiter fuselage.,

Model Scale * 0.00593

DRAWING NUMBER
V170-000139
DIMENSION:
FULL SCALE MODEL SCALE
Length.~in.
Max Width~in.


Area $\sim \mathrm{ft}^{2}$
Max Cross-Sectional
Platform

| -142.5195 |
| :---: |
| -0.00501 |

TABLE III. - Continued.

MODEL COMPONENT: Body Flap - Fs

GENERAL DESCRIPTION: Confiruration 4

| Model Scale - 0.006 DRAWING NUMBER | VL70-000140B, V1.70-000200 |  |
| :---: | :---: | :---: |
| DIMENSION: | FULL SCALE | MODEL SCALE |
| Length in. | 84.7 | . 508 |
| Max Width in. | 262.308 | 1.574 |
| Max Depth in. | 23.000 | . 138 |
| Fineness Ratio |  | - |
| Areo - $\mathrm{ft}^{\mathbf{2}}$ | . |  |
| Max Cross-Sectional | - |  |
| Planform | 158.85350 | . 0057 |
| Wetted |  |  |
| Base | 41.89642 | . 00151 |


$\angle$ of OUS Pod
$W P=463.9$ in. F.S.: WP $400+63.9=463.9$
$B P=80.0$ in. F.S.
Length 1214.0 to $1560.0=346.0$ in. F.S.
NOTE: $M_{4}$ identical to $M_{3}$ of $2 A$ configuration except intersection to body.

TABLE III. - Continued.

MODEL COMCNENT: ONS POD.MT
CENERAL DESCRIYIION: Configuration 140B Orbiter ONS Pod

MODEL SCALE: 0.006

| DRP:IIHG NUMBER: $\quad 170000140 \mathrm{Na}$ |  |  |
| :---: | :---: | :---: |
| DIENSIONS: | FULL SCALE | MODEL ECRLE |
| Length (ONS Fwd Sta $X_{0}=1233.0$ ) - IN. | 327.000 | 1.962 |
| Max Whdth (@ $\mathrm{X}_{0}=1450.0$ ) - IN. | 94.5 | . 567 |
| Max. Depth ( $\mathrm{K}_{0}=1493.0$ ) - In. | 109.000 | . 654 |

Area
Max Max Cross-Sectional
Planforn
Wetted
Base

MODEL COMPONENT: $\quad$ RUDDER $R_{5}$

GENERAL DESCRIPTION: Design configurations 2A, 3 and 3A

MODEL SCALE: 0.006

DRAWING NUMBER: VL70-0001.46A -000095 -000139

| DIMENSIONS: | FULL-SCALE | MODEL SCALE |
| :---: | :---: | :---: |
| Area - $\mathrm{Ft}^{2}$ | 100.15 | 0.036 |
| Span (equivalent)-In. | 201.00 | 1.206 |
| Inb'd equivalent chord - In. | 91.585 | 0.5495 |
| Outb'd equivalent chord - In. | 50.833 | 0.305 |
| Ratio movable surface chord/ total surface chord |  |  |

At Inb'd equiv. chord
At Outb'd equiv. chord

| $-\frac{0.400}{0.400} \quad \underline{0.400}$ |
| :--- |

Sweep Back Angles, degrees
Leading Edge
3:.83
34.83

Tailing Edge
Hingeline 3433 26.25
$\qquad$
34.83

Area Moment (Normal to hinge line)
Mean aerodynamic chord - In.

$$
73.2
$$

MODEL COMPONENT:
Vertical ( $V_{7}$ )-Lightweight orbiter configuration.
GENERAL DESCRIPTION: Centerline vertical tail, double-wedgeairfoil with


Model Scale $=0.00593$

| DRAWING NUMBER: | VL70-0000139 <br> VL70-000095 |  |
| :--- | :--- | :--- | :--- |
| DIMENSIONS: |  | FULL-SCALE |

TOTAL DATA
Area, (Theo.) $\mathrm{ft}^{2}$
Planform
Span. (Theo.) in.
Aspect Ratio
Rate of Taper
Taper Ratio
Sweepback Angles, degrees
Leading Edge
Trailing Edge
0.25 Element Line

Chords:
Root, (Theo.) WP
Tip, (Theo.) WP
MAC
Fus. Sta. of 0.25 MAC
W.P. of 0.25 MAC
B.L. of 0.25 MAC

Airfoil Section
Leading Wedge Angle, degrees
Trailing Wesdge Angle, degrees
Leading Edge Radius ~in.
Void Area
Blanketed Area

| 425.92 | $0.01498{ }^{\circ}$ |
| :---: | :---: |
| 315.72 | 1.87222 |
| 1.675 | 1.675 |
| 0.507 | 0.507 |
| 0.404 | 0.404 |
| 45.000 | 45.000 |
| 26.249 | 26.249 |
| 41.130 | 41.130 |
| 268.50 | 1.59220 |
| 108.47 | 0.64323 |
| 199.81 | 1.18487 |
| 1463.50 | 8.67856 |
| 635.522 | 3.76864 |
| 0.00 | 0.00 |
| 10.000 | 10.000 |
| 14.920 | 14.920 |
| 2.00 | 0.01186 |
| 13.17 | 0.00046 |

table III. - Continued.
MODEL COAPONENT: VERTICAL - VB
GENERAL DESCRIPTION: Conflpuration 14OB Orbitor Vertical Tail
NOTE: Similar to V5 with ridius of T.E. upper corner and L.E. corner
where vertical moats fuselage.
MODEL SCALE $=0.006$
DRAWING NUPBER:
DIMENSIONS:
FULL -SCALE
MODEL SCALE
TOTAL DATA

| Area (Theo) $\mathrm{Ft}^{2}$ | 413.253 | . 0148 |
| :---: | :---: | :---: |
| Planform |  |  |
| Span (Theo) In | 315.72 | 1.894 |
| Aspect Ratio | 1.675 | 2.675 |
| Rate of Taper | 0.507 | 0.507 |
| Taper Ratio | 0.404 | 0.404 |
| Sweep Back Angles, degrees |  |  |
| Leading Edge | 45.00 | 45.00 |
| Trailing Edge | 25.947 | 25.947 |
| 0.25 Element Line | 41.130 | 42.130 |
| Chords: |  |  |
| Root (Theo) WP | 268.500 | 1.621 |
| Tip (Theo) WP | 108.470 | 0.651 |
|  | 199.807 | 1.198 |
| Fus. Sta. of . 25 MAC | $\underline{14.63 .50}$ | 8.781 |
| W. P. of . 25 MAC | 635.52 | 3.813 |
| B. L. of . 25 MAC | 0.00 | 0,00 |
| Alrfoll Section |  |  |
| Leading Wedge Angle Deg | 10.00 | 10.00 |
| Trailing Wedge Angle Deg | -14.920 | 24.92 |
| Ledding Edge Radius | 2.00 | 2.00 |
| Void Área | 13.17 | 13.17 |
| Blanketed Area | 0.0 | 0.00 |

GENERAL DESCRIPTION: Configuration 3 Orbiter per lines VL.70-000139

NOTE: Same planform as W87, except dihedral at TE

Scale Model $=0.006$

DRAWING NUMBER: VL70-000139

```
DIMENSIONS:
FULL-SCALE
MODEL SCALE
```

TOTAL DATA

| $\begin{aligned} & \text { Area (Theo.) - } \mathrm{Ft}^{2} \\ & \text { Planform } \\ & \text { Wetted } \end{aligned}$ | 2690.00 | 0.09684 |
| :---: | :---: | :---: |
| Span (Theo In.) | 936.68 | 5.62 |
| Aspect Ratio | 2.265 | 2.265 |
| Rate of Taper | 1.177 | 1.177 |
| Taper Ratio | 0.200 | 0.200 |
| Dihedral Angle, degrees ( $¢$ TE of Elevon) | 3.500 | 3.500 |
| Incidence Angle, degrees | 3.000 | 3.000 |
| Aerodynamic Twist, degrees | +3.600 | +3.000 |
| Toe-In Angle |  |  |
| Cant Angle |  |  |
| Sweep Back Angles, degrees |  |  |
| Leading Edge | 45,000 | 45.000 |
| Trailing Edge | -10.24 | -10.24 |
| 0.25 Element Line | 35,209 | 35,209 |
| Chords: (Theo) |  |  |
| Root (Theo) B.P.0.0. | 689.24 | 4.135 |
| Tip, (Theo) B.P. | 137.85 | 0.8271 |
| MAC | 474.81 | 2.849 |
| Fus. Sta. of . 25 MAC | 1136.89 | 6.8213 |
| W.P. of . 25 MAC | 299.20 | 1.7952 |
| B.L. of . 25 MAC | 182.13 | 1.09278 |
| Airfoil Section |  |  |
| Root |  |  |
| Tip |  |  |
| EXPOSED DATA |  |  |
| Area (Theo) $\mathrm{Ft}^{2}$ | 1752.29 | 0.06211 |
| Span, (Theo) In. BP 108 | 720.68 | 4.32408 |
| Aspect Ratio | 2.058 |  |
| Taper Ratio | 0.2451 |  |
| Chords |  |  |
| Root BP108 | 562.40 | 3.3744 |
| Tip 1.00 b | 137.85 | . 8271 |
| MAC 2 | 393.03 | 2.35818 |
| Fus. Sta. of . 25 MAC | 1185.31 | 7.11186 |
| W.P. of . 25 MAC | 300.20 | 1.8012 |
| B.L. of . 25 MAC | 251.75 | 1.57056 |

MODEL COAPONENT: WING-W 16
GENERAL DESCRIPTiAN.: Configuration 4
NOTE: Identical to : except airfoil thickness. Dihedral angle is along trailing edge of wing.

Model Scale $=0.006$
IEST NO.


TOTAL DATA
Area (Theo.)
Planform
Span (Theo In.
Aspect Ratio
Rate of Taper
Taper Ratio
Dihedral Angle, degrees(at $X_{0}=1506.623, Y_{0}=$
Incidence Angle, degrees $105, \mathrm{z}_{\mathrm{O}}=282.75$ )
Aerodynamic Twist, degrees
Sweep Back Angles, degrees
Leading Edge
$F t^{2}$

Trailing Edge
0.25 Element Line

Chords:
Root (Theo) B.P.0.0.
Tip, (Theo) B.P.
MAC
Fus. Sta, of . 25 MAC
W.P. of . 25 : 1 AC
B.L. of . 25 :1AC

| $\frac{2690.00}{936.6816}$ |
| :---: |
| $\frac{2.265}{2.1 .177}$ |
| $\frac{0.200}{3.500}$ |
| 0.500 |
| +3.000 |
| 45.00 |
| 10.056 |
| 35.209 |


| .09684 |
| :---: |
| $\frac{5.620}{2.265}$ |
| 1.177 <br> 0.200 <br> 3.500 <br> 0.500 <br> +3.000 <br> 45.00 <br> -10.056 <br> 35.209 |
| 4.135 |
| .8 .827 |
| 6.760 |
| 6.746 |

EXPOSED DATA
Area (Tneo ) $\mathrm{Ft}^{2}$
Span, (heo) In. EP 108
Aspect Ratio
Taper Ratio
Chords
Rodt BP 108
Tip $1.00 \frac{b}{2}$
Fus. Sta. of . 25 MAC
W.P. of . 25 :1AC
B.L. of . 25 HAC

Airfoil Section (rockrell fod IIASA) XXXXX-64
Root $\frac{b}{2}=0.425$
$\operatorname{Tip} \frac{b}{2}=1.00$
$\frac{0.113}{0.12} \quad \frac{0.113}{0.12}$

Data for (1) of (2) Sides
Leading Edge Cuff
Planform Area ${ }^{2}$
Leading Edge Intersects Fus M. L. © Sta Leading Edge Intersects Wing e Sta
$\frac{718.33}{\frac{505.0}{1003.5}} \frac{-00426}{3.030}$

MDDEL *2vporict


and parallel to the $45 x^{\prime}$ element line.
NOTE: Dihedral anple is defined at the lower surface of the nin at the
75.33\% element line profected into a plane 1 to the FRL.
-

Model Scale $=0.0175$

DIMENS:ONS:

?lanform
Span! Theo In.
Aspec: Qatio
Rate of Taper
Taper Ratio
Dinedral Anc̣ie, degrees
Incidence Argie, degrees
Ae rodynamic Twist, degrees
Sweep Eack Angies, decrees Leading Edge Trailing Edge 0.25 Element Line

Chords:
Root (Theo) 3.P.0.0.
Tio, (Theo) B.P.
MAC
Fus. Sta. of . 25 MAC
W.P. of . 25 MAC
B.L. of .25 MAC

EXPOSED DATA
Area (Tneo) $\mathrm{Ft}^{2}$
Span, (Theo) In. BP 108
Aspect Ratio
Taper Ratic
Chords
Root BP108
Tip $1.00 \frac{b}{2}$
MAC
Fus. Sta. of . 25 MAC
W.P. of . 25 MAC
B.L. of . 25 MAC

Airfoil Section (Rociwell Mod NASA) XXXX-64
Root $\frac{b}{2}=$
TiD $\frac{b}{2}{ }^{=}$

$\frac{.10}{.12}$

Jata for (!) of (2) Sides

DWG. NO. VL7O-COD3O

Full-Scale
Model Scale


| 689.24 |
| ---: |
| 137.85 |
| 474.81 |
| 1136.89 |
| 299.20 |
| 182.13 |


| $\frac{0.82381}{16.39190}$ |
| :--- |
| $\frac{2.265}{1.177}$ |
| $\frac{.200}{3.507}$ |
| $\frac{3.000}{+3.000}$ |
| 45.000 |
| -71.24 |
| $\frac{35.209}{12.0617}$ |
| $\frac{2.41238}{8.30918}$ |
| 19.39558 |
| $\frac{5.2360}{3.18728}$ |


| $\frac{1752.29}{\frac{720.68}{2.05 \%}}$ |
| :--- |
| $\frac{0.2451}{562.40}$ |
| $\frac{137.85}{393.03}$ |
| $\frac{1185.31}{360.2 \pi}$ |
| $\frac{143.76}{12.6119}$ |


| .10 |
| :---: |

$$
\begin{aligned}
& \text { Leading Edge Cuft } \\
& \text { Lanform aqea rt } \\
& \text { Leading Edge intersects Fus M. L. © Sto } \\
& \text { Leading Edge Intersects whnc e Sto }
\end{aligned}
$$

$$
\quad 12 n .33
$$

550.0
1035.0
$\frac{0.03685}{\frac{9.8}{13.1125}}$


Figure 1. Axis Systems.

a. Orbiter Configuration

Figure 2. - Model Sketches.

b. Model 64-0 Partial Wing

Figure 2. - Continued.


Figure 2. - Concluded.

a. Orbiter Grid Model Installed in Tunnel

Figure 3. - Model Photographs.

b. Partial Wing Model Installed in Tunnel

Figure 3. - Continued.

C. Partial Wing Model Mounting Assembly

Figure 3. - Continued.

d. Partial Wing Model With Shock Generator

Figure 3. - Concluded.

