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School of ENGINEERING DUKE UNIVERSITY

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COMPUTER-AIDED DESIGN PROGRAMS FOR
INDUCTOR-ENERGY-STORAGE dc-TO-dc ELECTRONIC
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USER'S MANUAL -- COMPUTER-AIDED DESIGN PROGRAMS
FOR INDUCTOR-ENERGY-STORAGE DC-TO-DC
ELECTRONIC POWER CONVERTERS

BY

STEPHEN D. HUFFMAN

PREPARED UNDER CONTRACT NO. NAS5-22475

30 JUNE 1977



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**USER'S MANUAL -- COMPUTER-AIDED DESIGN PROGRAMS
FOR INDUCTOR-ENERGY-STORAGE DC-TO-DC
ELECTRONIC POWER CONVERTERS**

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16. Abstract Detailed instructions on the use of two computer-aided-design programs for designing the energy-storage-inductor for single-winding and two-winding dc-to-dc converters are provided. Step-by-step procedures are given to illustrate the formatting of user input data. The procedures are illustrated by eight sample design problems which include the user input and the computer program output.		
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PREFACE

This special report contains detailed instructions on the use of two computer-aided design programs for use in designing the energy-storage reactor for both single-winding and two-winding dc-to-dc converters. Step-by-step procedures are given to illustrate the formatting of user input data. These procedures are illustrated by eight sample design problems and computer runs which include user input and computer program output.

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INTRODUCTION

1.1 DESCRIPTION OF PROGRAMS

DC1DC is a program for the computer-aided design of the reactor element and/or the evaluation of the steady-state operating characteristics of any member of a family of single-winding energy-storage dc-to-dc electronic power converters. Any one of the three converter circuits shown in Figure 1 may be coupled with any one of three types of controllers--constant frequency, constant transistor on-time or constant transistor off-time--for a total of nine possible systems.

DC2DC is a similar program for the design of the reactor element and/or the evaluation of the steady-state operating characteristics of the two-winding voltage step-up/current step-up converter circuit shown in Figure 2. This converter circuit may be coupled with any of the three previously mentioned types of controllers to yield three distinct converter systems.

The design of the reactor and the steady-state evaluation of the converter are based on models of the converter circuits which make certain simplifying assumptions. These assumptions are given in Section 1.2.

User inputs to the programs include the type of converter/controller combination desired and a set of design requirements which the system must meet. In executing a design or evaluation

request, the program makes use of a stored data base consisting of a catalog of magnetic core data (usually from manufacturers' catalogs) and a table listing available sizes of magnet wire. The reactor design(s) produced by the program include core catalog information, number of turns, wire sizes and various other design parameters.

In addition to the reactor design routine, an algorithm is included in the programs to assist in the evaluation of certain steady-state operating characteristics of the converter/controller combination. This evaluation algorithm may be used to automatically evaluate the computer generated design(s) or it may be used independently to evaluate a previously generated design or a design computed by hand. Outputs from the evaluation algorithm include: minimum, maximum, average and RMS values for the reactor current(s), the RMS value of the current through the capacitor, pulse widths and frequency of operation, power losses in the various components and the converter efficiency. These output variables are computed over the user specified operating range of the converter in increments of input voltage and output power also specified by the user.

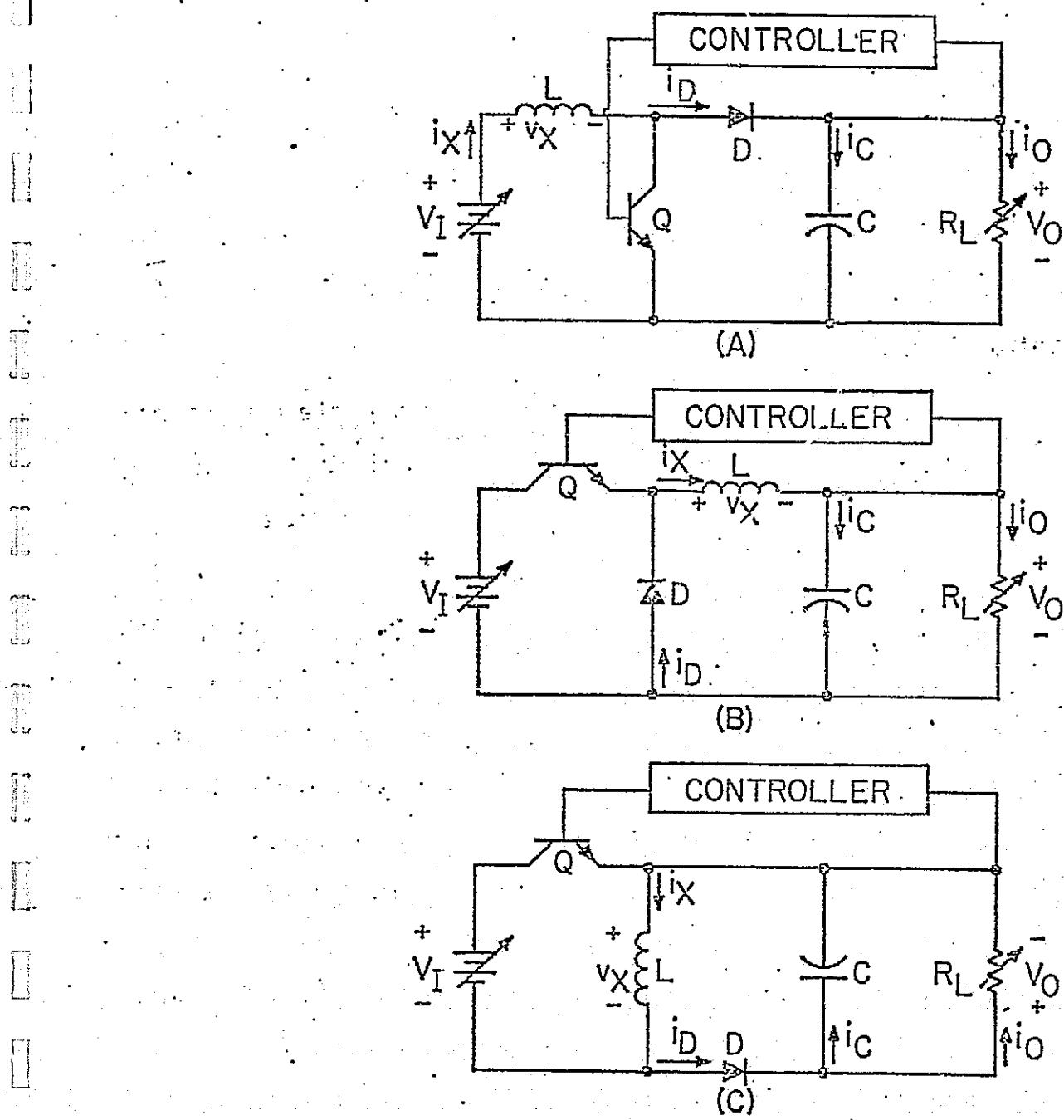


Figure 1. Three Single-Winding Converters

- (A) Voltage Step-up
- (B) Current Step-up
- (C) Voltage Step-up/Current Step-up

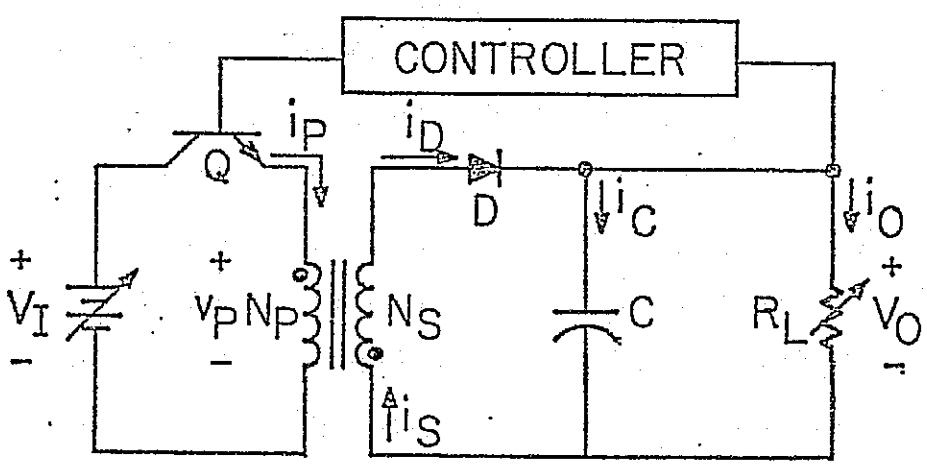


Figure 2. Two-Winding Voltage Step-up/
Current Step-up Converter

1.2 DEVICE MODELS

The design and evaluation algorithms used by the programs are based on circuit models which make certain simplifying assumptions [1]. The following discussion of device models applies to all three converter circuits shown in Figure 1 as well as to the two-winding circuit shown in Figure 2.

1.2.1 Transistor Model

For the design algorithm, the transistor collector-emitter is modeled as a switch with a constant forward voltage drop (switch closed) and infinite reverse resistance (switch open) as indicated by the equivalent circuit and V-I characteristic shown in Figure 3. It is further assumed that the transistor base current is negligible. During the transistor on-time (T_{ON}) the switch is closed. At the end of this interval, the switch opens and remains open during the transistor off-time (T_{OFF}). It is assumed that switching takes place over a negligible time interval.

For design evaluation purposes, the transistor collector-emitter is modeled as a lumped linear saturation resistance as shown in Figure 4. The power loss in the collector is computed by taking the product of the saturation resistance and the square of the RMS value of the collector current.

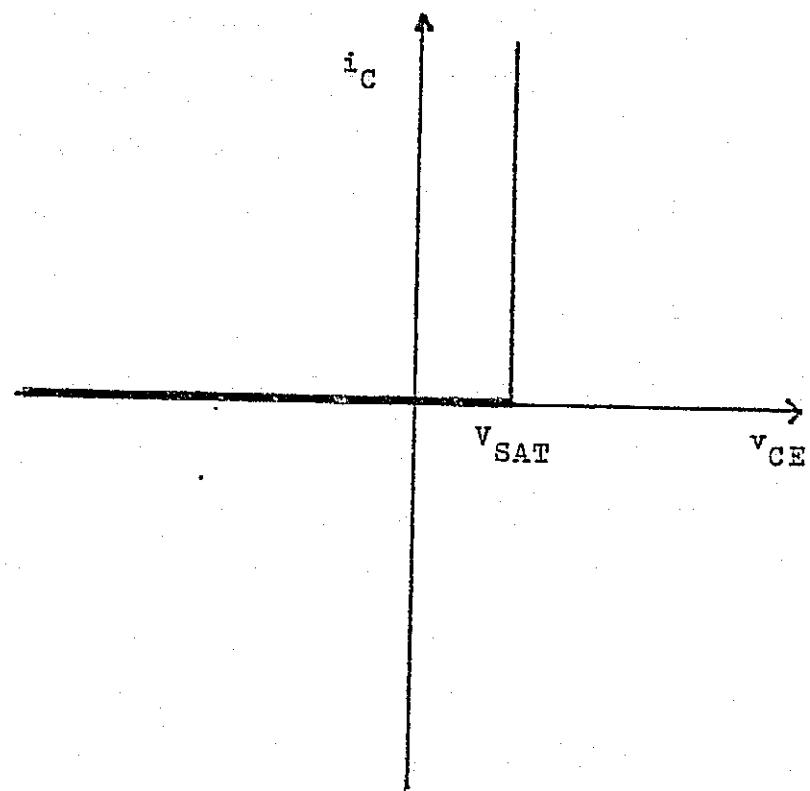
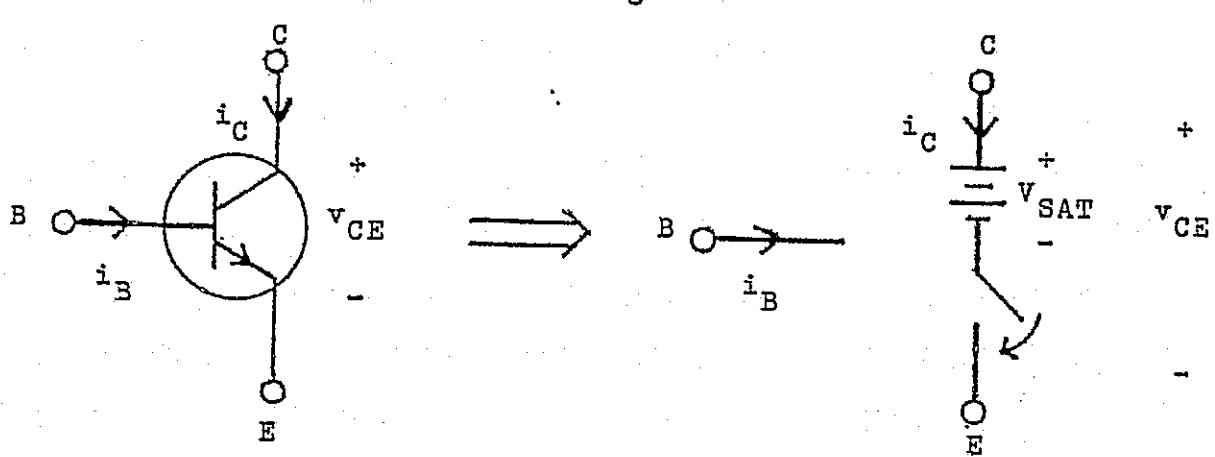


Figure 3. Transistor Model--Design Procedure

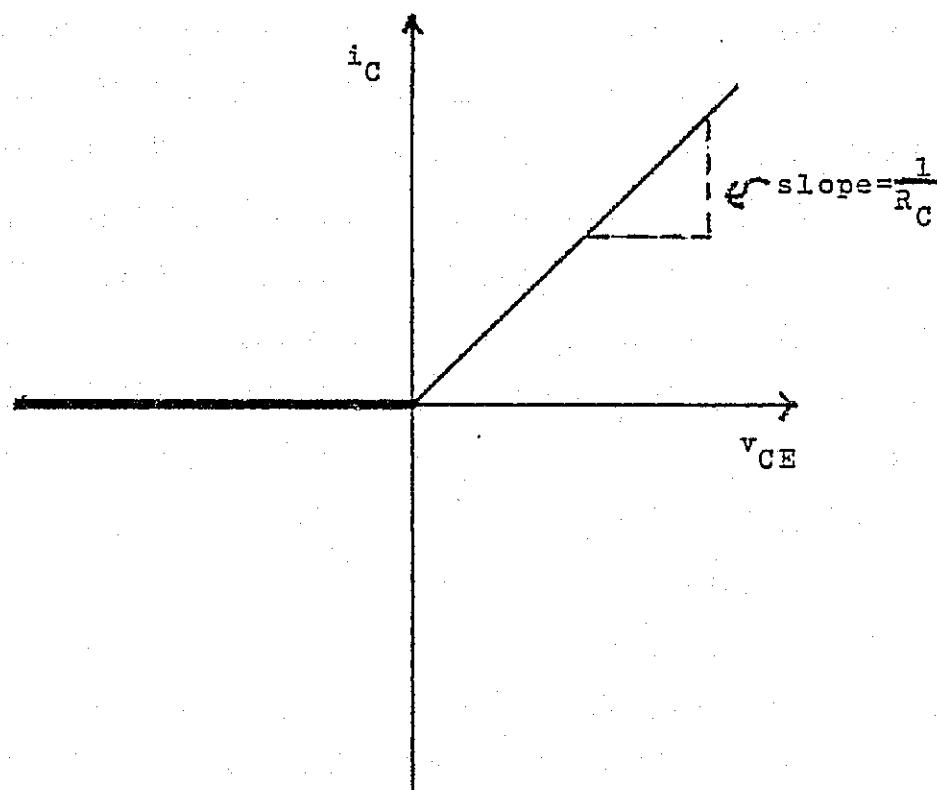
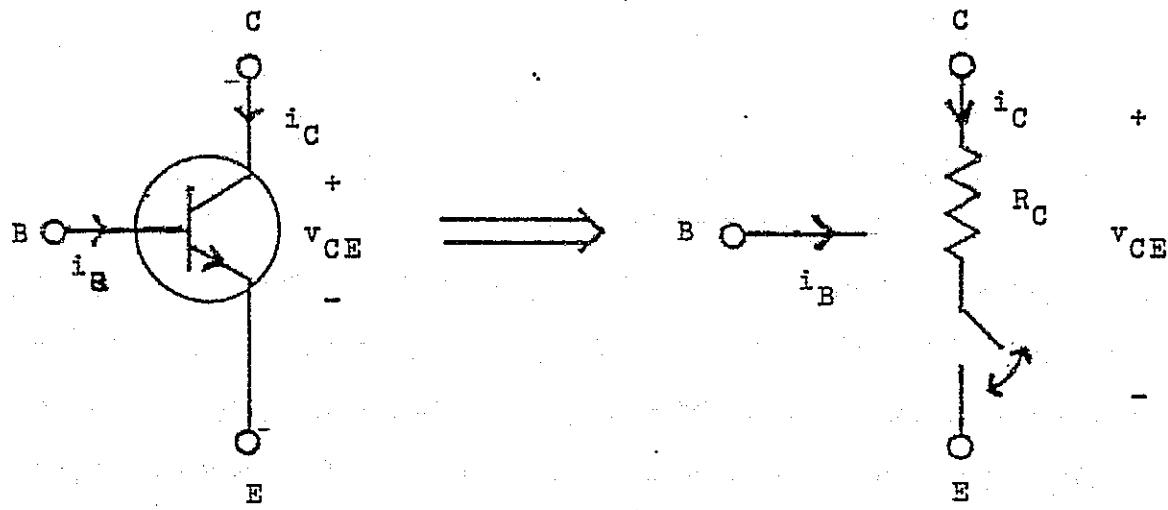


Figure 4. Transistor Model--Evaluation Procedure

1.2.2 Diode Model

Both the design routine and the evaluation algorithm assume the diode acts as a constant voltage source in series with an ideal diode as indicated by the equivalent circuit and V-I characteristic shown in Figure 5. Again, it is assumed that switching takes place over a negligible time interval.

1.2.3 Reactor Element Model

It is assumed that the magnetic core is operated in the linear range of constant permeability as shown in the B-H characteristic in Figure 6. The design routine is carried out assuming that winding resistance is negligible. The evaluation algorithm assumes a lumped linear winding resistance (equal to the product of the computed winding length (meters) and the resistivity (ohms/meter) of the wire size) in calculating the power loss in the winding(s). The winding losses are computed by multiplying the winding resistance by the square of the RMS value of the current in the winding. Power losses in the magnetic core are approximated by use of Legg's equation [2]. Total core loss is computed as the sum of three frequency dependent components, hysteresis loss, eddy current loss and residual loss. These three loss components are related to the core loss resistance by Legg's equation in modified form:

$$R_{ac} = \mu_r L (a \Delta B 10^4 f + cf + ef^2)$$

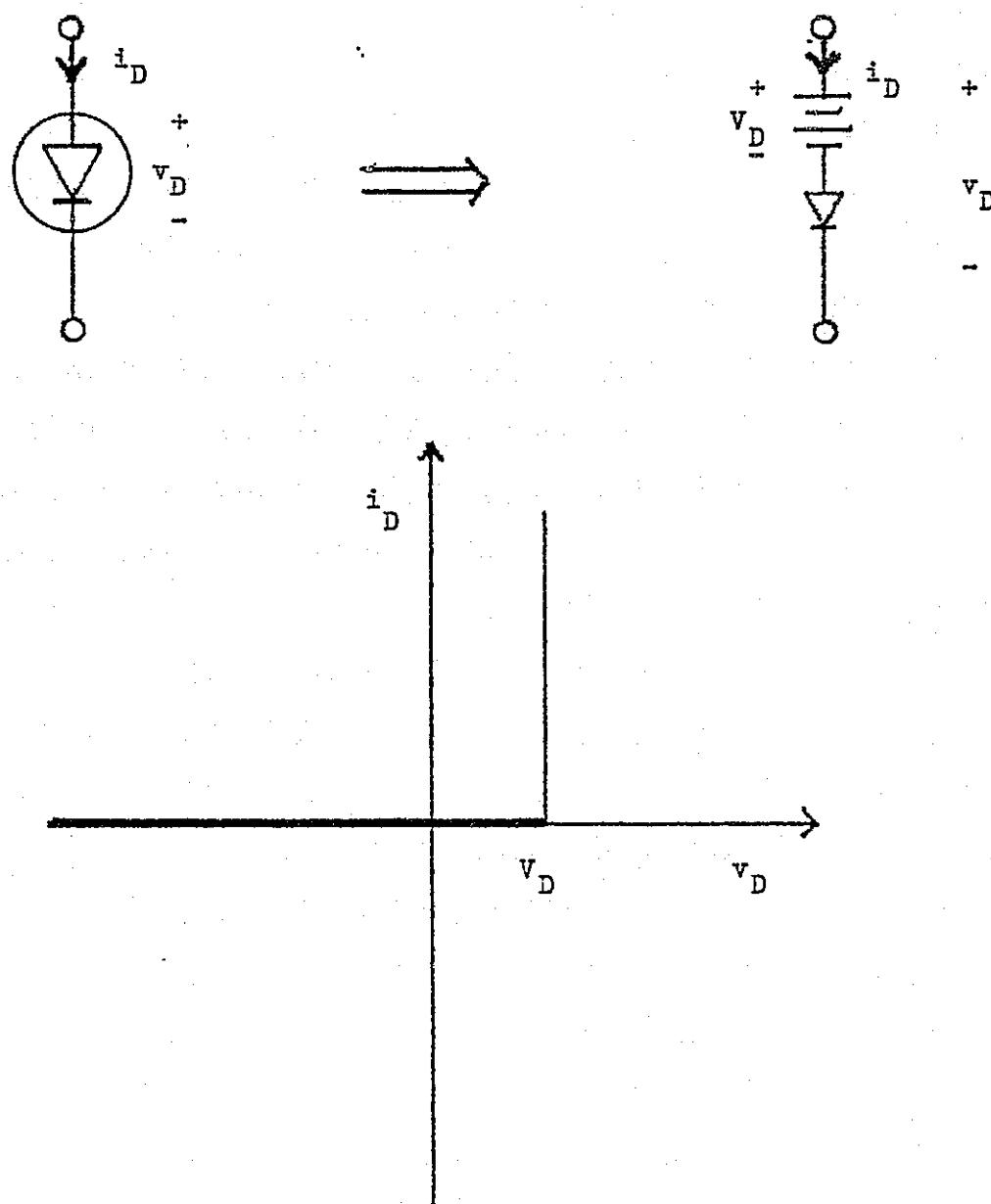


Figure 5. Diode Model

where:

- R_{ac} = core loss resistance
- μ_r = relative permeability
- L = inductance (henries)
- a = hysteresis loss coefficient
- c = residual loss coefficient
- e = eddy current loss coefficient
- ΔB = flux density excursion (tesla)
- f = frequency (Hz)

The hysteresis, residual and eddy current loss coefficients are available from manufacturers' data sheets. Power loss in the core is approximated by multiplying the core loss resistance by the square of the RMS value of the fundamental component of the winding current. Legg's equation is strictly valid only under the conditions of sinusoidal flux and low flux-density excursions. Although these conditions are seldom met in the converter operation, Legg's equation is the best approximation given the presently available core data.

1.2.4 Capacitor Model

It is assumed that the capacitor is so large that there is negligible ripple voltage at the converter output. To approximate power loss in the capacitor, the evaluation algorithm assumes that the capacitor has a lumped linear effective series resistance (ESR). Power loss in the capacitor is approximated by taking the product of the ESR and the square of the RMS value of current through the capacitor.

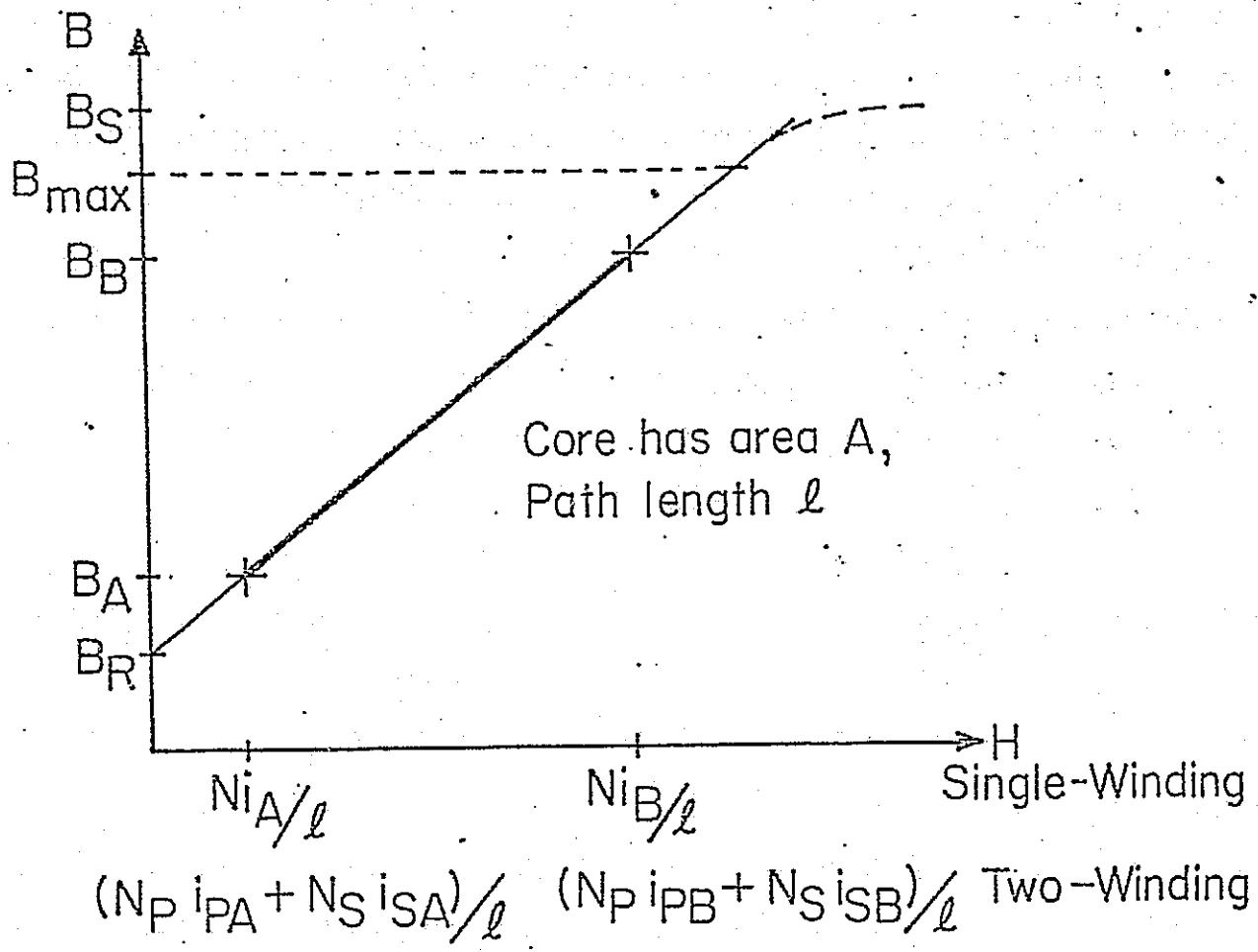


Figure 6. Magnetic Core Characteristics

1.2.5 Controller Model

The controller is assumed to be ideal in that it draws no current from the load and it operates with negligible time delay.

1.2.6 Input Voltage Magnitude

The minimum input voltage is assumed to be always larger than the transistor saturation voltage drop.

1.3 THE DATA BASE

The data base consists of two sections, a core catalog and a wire-size table. The programs use the data base along with the design-requirement data in executing an assigned task. Unlike the design-requirement data, the data base will be modified infrequently. Thus, once the data base is constructed and stored in some fashion which allows the computer to access the information (i.e. cards, magnetic disk, etc.), the user need not concern himself with the data base until such time as he desires to make revisions or additions to this data. Part II of this manual deals with construction and revision of the data base.

1.3.1 The Core Catalog

The Core Catalog consists of data concerning the available magnetic cores. It contains core dimensional data, manufacturers' catalog numbers and loss coefficients (see Section 1.2.3) for

the values of relative permeability available. The data in the core catalog is usually obtained from manufacturers' core catalogs.

1.3.2 The Wire Table

The Wire Table gives the cross-sectional area and resistivity of the available sizes of magnet wire. The area of each wire size is listed for bare wire as well as for single, heavy, triple and quad synthetic insulated wire. The wire-table data is usually obtained from wire manufacturers' data sheets.

PART I -- USE OF THE PROGRAMSPRELIMINARY INFORMATION

The designer, in using either Program DC1DC or DC2DC, must input a set of design requirements which the program will use along with a stored data base in executing the assigned task. Part I of this manual deals with the use of the program for carrying out design and evaluation problems and centers on the input of design-requirement data. It is assumed in Part I that the stored data base is already available for use. Part II deals with the construction of the data base.

2.1 PROGRAM PROCEDURES

DC1DC and DC2DC offer three design/evaluation procedures to the user. Procedure DSN1 produces a list of up to fifty usable reactor designs for a given set of design requirements, and evaluates as many of these designs as the user desires. Procedure DSN2 allows the designer to have a single design computed and evaluated using a specified magnetic core. The third procedure, EVAL, may be used to evaluate any previously completed design.

2.1.1 Procedure DSN1

In Procedure DSN1, the user inputs to the program the type of converter/controller combination desired and a set of specifications for the system. All cores in the core catalog are checked by the program for windability under the constraints

imposed by the design specifications. A list of up to fifty usable designs is printed out, including manufacturers' core numbers, value of relative permeability, value(s) of inductance, number of turns, wire size(s), winding factor, and various operating parameters. Beginning with the smallest volume core, each of these designs, up to a user specified maximum, is evaluated under steady-state conditions over a user specified range of input voltage and output power. Outputs include: minimum, maximum and RMS values for the winding current(s), RMS value of the capacitor current, pulse widths and frequency of operation, power losses in the core, wire, transistor, diode and capacitor, and the estimated converter efficiency.

2.1.2 Procedure DSN2

Under Procedure DSN2, the user may specify that a design be computed and evaluated for a specific core. The designer simply enters the integer core number from the core catalog along with the relative permeability and the design requirements. By entering dimensional information, the user is also allowed to request that a design be generated for a core which is not in the core catalog. Also, if a value of relative permeability other than a catalog value is required, the user may enter loss coefficient information and request a design for a particular core having the entered value of relative permeability. If loss coefficients are not supplied, default values will be assumed (see Section 3.4.3). The outputs under Procedure DSN2 are the same as those under Procedure DSN1, except that only

the specified core can appear in the windable core list. If the core entered should fail to meet the design specifications, a message to this effect will be printed by the programs.

2.1.3 Procedure EVAL

Under Procedure EVAL, the user may enter a completed design of a reactor element and request that an evaluation be performed. The evaluation is performed under steady-state conditions over a specified range of input voltage and output power. As in Procedure DSN2, the core size and relative permeability need not be in the core catalog in order for a design to be evaluated. However, the wire size used must be in the wire table. To use Procedure EVAL, the designer must input the core number (integer) of the core used, the relative permeability of the core, the number(s) of turns, the AWG wire size(s) and the number of cores in the stack. If a core which is not in the catalog is used, dimensional information must be supplied. Similarly, if a value of relative permeability which is not in the catalog is used, information of the loss coefficients may be given. If loss coefficients are not supplied, default values will be assumed (see Section 3.4.3). The outputs from Procedure EVAL include: minimum, maximum and RMS values for the winding current(s), RMS value of the capacitor current, pulse widths and frequency fo operation, power losses in the various components and the converter efficiency.

2.2 INPUT FORMAT

The input data for the programs is entered in the form of eighty-character records. In the instructions for preparing the data, each such record will be referred to as a "card" although the input data may not necessarily be in the form of computer cards. For example, it may be convenient to store the data base on magnetic disk or tape to reduce the number of punched cards which must be handled. Each record, or "card", is divided into a varying number of data fields with each data field containing the value of a particular variable. The field descriptor, or format, indicates what type of data is contained in a particular field. The field descriptors for each of the variables on a card are given in the instructions and are one of the standard FORTRAN IV field descriptors discussed in the following sections [3].

2.2.1 I Format

The form of the I format is: I_m where m is an integer greater than zero. The integer m indicates the number of spaces allocated to the field. Variables which take on integer values in the program are read in under the I format. Any column within the field which is left blank will be read as a zero. Thus, it is important that all variables read in under the I format be right justified. Characters other than digits, plus and minus are invalid in I fields. For an example of the use of the I format, see Figure 7.

100

OR

1

Figure 7. The Integer 100 Read Under An I5 Format

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2.2.2 F Format

The form of the F format is: Fm.n where m is an integer greater than zero and n is an integer greater than or equal to zero. The letter F indicates that this variable is a fixed point decimal number. The integer m indicates the number of spaces allocated to the field and the integer n indicates the number of decimal places present in the number. Placing a decimal point within the field overrides the value on n and is suggested. Use of a decimal point allows the placement of the number anywhere within the m spaces. Characters other than digits, plus, minus, and decimal point are invalid under the F format. For an example of the use of the F format, see Figure 8.

2.2.3 E Format

The form of the E format is: Em.n where m is an integer greater than zero and n is an integer greater than or equal to zero. The E format is used to read floating point decimal numbers with integer exponents. The integer m gives the number of spaces allocated to the field and the integer n indicates the number of decimal places present in the number. Use of a decimal point within the field overrides the value of n and is suggested. Exponents are entered by placing either an "E" or a space between the mantissa and the exponent. Blank columns are read as zeros, so the exponent should be right justified in order for its value to be read properly. For an example of the use of the E format, see Figure 9.

100

OR

三

Figure 8. The Number 100.0 Read Under An F5.0 Format

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5, 067E-07

OR

5, US7 - 07

Figure 9. The Number 5.067×10^{-7} Read Under An E10.3 Format

2.2.4 A Format

The form of the A format is: Am where m is an integer greater than zero. The letter A indicates that this is an alphanumeric field. All keyboard characters are valid under the A format. The integer m gives the number of spaces allocated for the field. The A format is used to input variables which are words or groups of symbols, such as the name of a magnetic core manufacturer. For an example of the use of the A format, see Figure 10.

2.2.5 Characters

Use of characters within designated fields other than those listed below will usually result in severe errors which will either terminate the program or give invalid results.

<u>FORMAT</u>	<u>VALID CHARACTERS</u>
I	Digits, +, -
F	Digits, +, -, decimal point
E	Digits, +, -, decimal point, E
A	All keyboard characters

2.3 THE DATA DECK

The Data Deck is the total set of inputs to the program, and consists of the data base and the control cards. The programs read the data base first, followed by the control cards as shown in Figure 11. Section 3. discusses the control cards.

NAME

Figure 10. The Word "NAME" Read Under An A4 Format

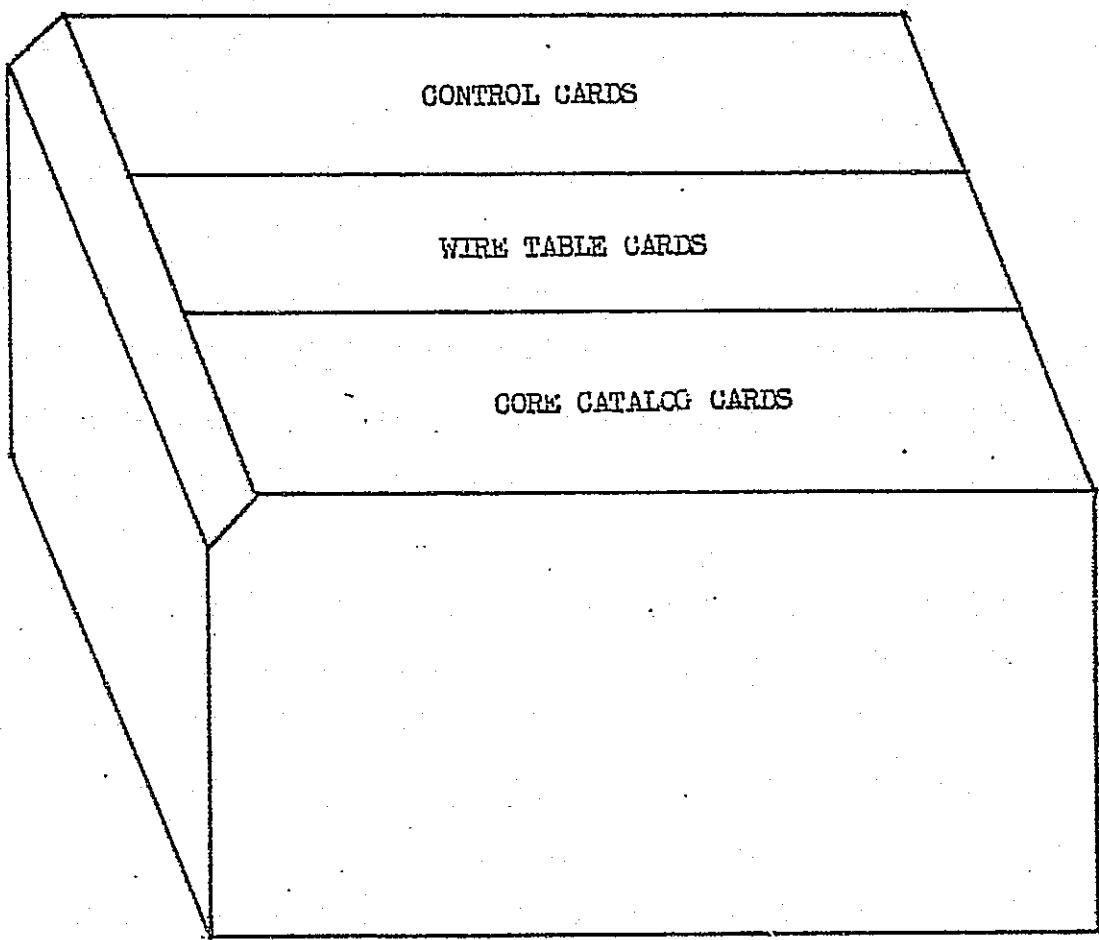
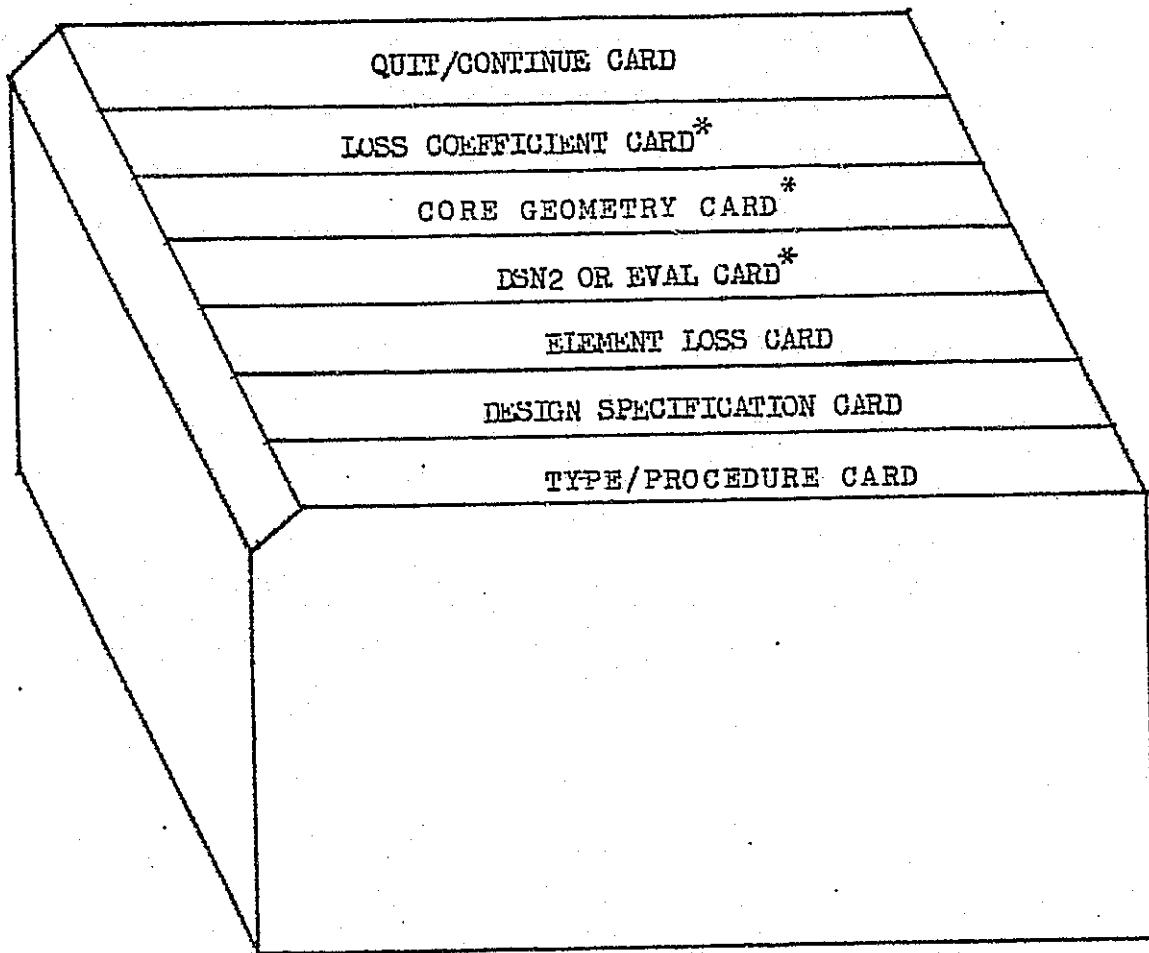


Figure 11. Order of The Data Deck

CONTROL CARDS

The control cards are read immediately after the data base and are the means by which the user inputs converter design specifications and indicates which of the three program procedures is desired. There are seven types of control cards, although all seven types need not be used on a given run. The names and order of the control cards are shown in Figure 12. Sections 3.1-3.5 give instructions for preparing the control cards for Program DC1DC. The number, order and function of the control cards for Program DC2DC are the same as those for Program DC1DC. However, in several of these cards--specifically the Type/Procedure Card, the Design Specification Card and the EVAL Card--there are slight differences between programs. Sections 3.6-3.9 give instructions for preparing the Control Cards for Program DC2DC.

In the instructions which follow (Sections 3.1-3.12), sections which apply to only one of the two programs will have titles which include the relevant program name as illustrated in the title of Section 3.1. Titles of sections which apply to both programs will not contain any reference to the program name as seen in the title of Section 3.1.2.



*(if needed)

Figure 12. Order of The Control Cards

3.1 TYPE/PROCEDURE CARD--PROGRAM DC1DC

The Type/Procedure Card is the first card in the control deck. It specifies the type of converter/controller combination desired, controls the listing of the catalog, specifies the program procedure desired and gives certain parameters used in the design evaluation algorithm. The format of the Type/Procedure Card for Program DC1DC is given below (see also Figure 13). A sample card is shown in Figure 14.

<u>COLUMNS</u>	<u>FORMAT</u>	<u>PARAMETER</u>
2-5	A4	Converter/Controller Type
7-8	A2	Catalog Print Feature
10-13	A4	Program Procedure
14-20	I7	Maximum Number of Evaluations to be Performed (DSN1)
21-25	F5.0	Input Voltage Increment (volts)
26-30	F5.0	Output Power Increment (watts)

PARAMETER	FORMAT
CONVERTER/CONTROLLER TYPE	A4
CATALOG PRINT FEATURE	A2
PROGRAM PROCEDURE	A4
MAXIMUM NO. OF EVALUATIONS	I7
INPUT VOLTAGE INCREMENT	F5.0
OUTPUT POWER INCREMENT	F5.0

Figure 13. Type/Procedure Card--Program DC1DC

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Figure 14. Example: Type/Procedure Card
Program DC1DC

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3.1.1 Converter/Controller Types--Program DC1DC

The type of converter/controller combination that is to be designed and/or evaluated is indicated on the Type/Procedure Card by the use of the proper converter/controller code. DC1DC may be used to aid in the design of any one of the three circuit configurations shown in Figure 1 in conjunction with any one of three different types of controllers. The correct converter/controller code for each of the nine possible converter systems is given below.

<u>CODE</u>	<u>CONVERTER TYPE</u>	<u>CONTROLLER TYPE</u>
FQVU	Voltage Step-up	Constant Frequency
TNVU	Voltage Step-up	Constant On-time
TFVU	Voltage Step-up	Constant Off-time
FQCU	Current Step-up	Constant Frequency
TNCU	Current Step-up	Constant On-time
TFCU	Current Step-up	Constant Off-time
FQUD	Voltage Step-up/ Current Step-up	Constant Frequency
TNUD	Voltage Step-up/ Current Step-up	Constant On-time
TFUD	Voltage Step-up/ Current Step-up	Constant Off-time

3.1.4 Evaluation Parameters

The Input Voltage Increment and the Output Power Increment determine the conditions under which the design will be evaluated. First, the input voltage is set to its minimum value and the design is evaluated first for the minimum output power, then for the minimum power plus the power increment. The power is incremented until the maximum output power is reached or exceeded. Then, the input voltage is increased by the input voltage increment and the process is repeated. When the input voltage reaches or exceeds its maximum value, the evaluation routine is terminated. If the Input Voltage Increment and/or the Output Power Increment are set equal to zero, the program will assume a default value. The default value for the Input Voltage Increment is one third of the specified input voltage range and the default value for the Output Power Increment is one fifth of the specified output power range. The minimum and maximum values for the input voltage and the output power are specified on the Design Specification Card.

3.2 DESIGN SPECIFICATION CARD--PROGRAM DC1DC

The second card in the control deck is the Design Specification Card. The design specifications are entered on this card in the format given below (see also Figure 15). A sample Design Specification Card is shown in Figure 16. The meaning of the design specifications is discussed in Section

3.2.1.

<u>COLUMNS</u>	<u>FORMAT</u>	<u>PARAMETER</u>
1-5	F5.0	Output Voltage (volts)
6-10	F5.0	Minimum Input Voltage (volts)
11-15	F5.0	Maximum Input Voltage (volts)
16-20	F5.0	Minimum Output Power (watts)
21-25	F5.0	Maximum Output Power (watts)
26-30	F5.0	On-time, Off-time or Freq. (depending on Controller) (usec or KHz)
31-35	F5.0	Residual Flux Density (tesla)
36-40	F5.0	Minimum Flux Density (tesla)
41-45	F5.0	Maximum Flux Density (tesla)
46-50	F5.0	Maximum Winding Factor
51-55	I5	Min. No. of Cores in Stack
56-60	I5	Max. No. of Cores in Stack
61-70	E10.3	Reciprocal Current Density (m ² /ampere)
72-75	A4	Wire Type
76-80	I5	Min. No. of Strands of Wire

3.2.1 Design Specifications

The maximum flux density specification sets an upper limit for the flux excursion. The computer design algorithm is such that the peak flux density of a computed design will reach this specified maximum at some point within the design range of input voltage and output power.

Figure 15. Design Specification Card
Program DC1DC

Figure 16. Example: Design Specification Card
Program DC1DC

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The minimum flux density establishes a lower limit for the flux excursion. The design algorithm insures that the minimum instantaneous flux density of a computed design will exceed or equal this specified minimum at every point within the design range. This specification may not be chosen to be less than the specified residual flux density of the magnetic material. If the minimum flux density specification is chosen to be greater than the residual flux density, all computer generated designs will operate in Mode 1 (continuous conduction mode) over their entire design range. However, if the minimum flux density specification is chosen to be equal to the residual, then the generated designs may operate in Mode 1 over the entire design range; or, in Mode 2 (discontinuous conduction mode) over the entire range; or, in Mode 1 over some portion of the range and in Mode 2 elsewhere. It should be noted however, that while it is possible to force completely Mode 1 operation by choosing the minimum flux density specification to be greater than the residual, it is not possible to force the program to generate designs which operate in Mode 2 over the entire design range of input voltage and output power.

The maximum winding factor determines which cores are acceptable designs. The winding factor is computed by taking the area of the winding(s) (based on the cross-sectional area of the insulated wire) and dividing by the window area of the magnetic core. This corresponds to the fractional part of the core window which is filled by the winding(s). Cores which require winding factors greater than the specified maximum are

rejected. This parameter is ignored in the evaluation portion of the programs. Winding factors greater than one are not allowed in Procedures DSN1 and DSN2.

The minimum number of cores in the stack and the maximum number of cores in the stack allow designs with stacked cores to be generated. If fifty usable designs are not found for the specified minimum core stack, the stack height is automatically increased by one and the design procedure is repeated. The stack height will be increased in this fashion until fifty designs are found or until the specified maximum number of cores in the stack is reached.

Often, it may be desired to use more than one strand of wire for the core winding(s). The minimum strands of wire parameter(s) allows designs to be made with stranded wire. If the largest wire size in the wire table will not meet the reciprocal current density specification with the specified minimum number of strands, the number of strands is automatically increased by the design algorithm until this specification is met. There is an internal default value of one for the minimum number of strands. When using Procedure EVAL, the minimum strands of wire parameter must be set equal to the number of strands actually used in the design being evaluated. In Program DC2DC, there is a minimum strands of wire specification for both primary and secondary windings of the two-winding reactor (see Section 3.7).

3.2.2 Wire Types

Four types of wire coating are available in the program. The user selects the desired type by entering the correct wire type code in the field provided for this purpose on the Design Specification Card. The wire type codes are given in the table below.

<u>CODE</u>	<u>WIRE TYPE</u>
SING	Single Coating--Synthetic Film Insulation
HEAV	Double Coating--Synthetic Film Insulation
TRIP	Triple Coating--Synthetic Film Insulation
QUAD	Quad Coating--Synthetic Film Insulation

3.3 ELEMENT LOSS CARD

The Element Loss Card gives parameters used to calculate approximate power losses in the elements of the converter circuit other than the magnetic core. The format for this card is given in the table below (see also Figure 17). A sample Element Loss Card is shown in Figure 18. Section 1.2 discusses the device models and power loss calculations. If any of the parameters on the Element Loss Card are entered as zero (or left blank), the program will assume that the corresponding device is lossless.

<u>COLUMNS</u>	<u>FORMAT</u>	<u>PARAMETER</u>
1-5	F5.0	Transistor Saturation Voltage (volts)
6-10	F5.0	Collector Current for above (amperes)
11-15	F5.0	Diode Forward Drop (volts)
16-20	F5.0	Capacitor Effective Series Resistance (ohms)

3.4 DSN2 CARD AND EVAL CARD

3.4.1 DSN2 Card

In Procedure DSN2, the program attempts to compute a design using a specified magnetic core. The DSN2 card is used only if the DSN2 procedure has been specified on the Type/Procedure Card (see Section 3.1). It contains the integer size number and the relative permeability of the core for which a design is desired. The integer core number may be obtained from the catalog listing produced by the program. This information is found on the catalog listing under the heading "SIZE NO.". The format of the DSN2 Card is given in the table below (see also Figure 19). A sample DSN2 Card is shown in Figure 20.

<u>COLUMNS</u>	<u>FORMAT</u>	<u>PARAMETER</u>
1-5	I5	Core Size Number from Catalog
6-10	F5.0	Relative Permeability of Core
11-15	I5	Number of Cores in Stack

PARAMETER	FORMAT
TRANSISTOR SATURATION VOLTAGE (VOLTS)	F5.0
COLLECTOR CURRENT (AMPS)	F5.0
DIODE FORWARD DROP (VOLTS)	F5.0
CAPACITOR KVAR	F5.0

Figure 17. Element Loss Card

1.1 10. .65 .1

Figure 18. Example: Element Loss Card

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Figure 19. DSN2 Card

19 800. 1

Figure 20. Example: DSN2 Card

3.4.2 EVAL Card--Program DC1DC

In Procedure EVAL, Program DC1DC evaluates a design entered by the user. The EVAL card is used only if the EVAL procedure was specified on the Type/Procedure Card (see Section 3.1). The EVAL Card contains the integer size number of the core, the relative permeability, the number of turns, wire size and number of cores in the stack. The integer core number may be obtained from the catalog listing produced by the program. This information is found on the catalog listing under the heading "SIZE NO.". The format of the EVAL Card for Program DC1DC is given in the table below (see also Figure 21). A sample EVAL Card for Program DC1DC is shown in Figure 22.

<u>COLUMNS</u>	<u>FORMAT</u>	<u>PARAMETER</u>
1-5	I5	Core Size Number from Catalog
6-10	F5.0	Relative Permeability of Core
11-15	I5	Number of Cores in Stack
16-20	I5	Number of Turns of Wire
21-25	I5	Wire Size (AWG number)

Figure 21. EVAL Card--Program DC1DC

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13 200^a 1 80 16

Figure 22. Example: EVAL Card
Program DC1DC

3.4.3 Procedures DSN2 and EVAL with Cores not in the Catalog

If either a core size or a relative permeability value (or both) is not in the catalog, it is still possible to use Procedures DSN2 and EVAL. Simply enter a zero or blank for the core size and/or permeability on the DSN2 or EVAL Card. If a zero (or blank) was entered for the core size number, an additional card must be added immediately following the DSN2 or EVAL Card which gives the dimensional information for the core used. If a zero (or blank) was entered for the value of relative permeability, an additional card must be added giving loss coefficient information on the entered core and its value of relative permeability. If both parameters are entered as zero (or blank), then both extra cards are needed. The dimensional data card follows the DSN2 or EVAL Card and the loss coefficient data card follows the dimensional data card. The formats of these extra cards are the same as those of the Core Geometry Card (Section 6.4.2) and the Loss-Coefficient Card (Section 6.3). The loss coefficient information is used only in the evaluation algorithm. If loss coefficients for an entered value of relative permeability are given as zero (or left blank), the programs will use values from the catalog which are for the cataloged value of relative permeability which is closest to the entered value.

3.5 QUIT/CONTINUE CARD

The final card in the control deck should have a zero in column one. If more than one design and/or evaluation is desired on a given run, use a card with a one in column one followed by another set of control cards. This may be repeated for as many design and/or evaluation requests as desired.

PROGRAM DC2DC

3.6 TYPE/PROCEDURE CARD--PROGRAM DC2DC

The Type/Procedure Card is the first card in the Control Deck for Program DC2DC. It specifies the type of controller desired, controls the listing of the catalog and gives the desired design constraint option and the design constraint. In addition, the Type/Procedure card lists the evaluation parameters described in Section 3.1.4. The format of the Type/Procedure Card is given in the table below (see also Figure 23). A sample Type/Procedure Card for Program DC2DC is shown in Figure 24.

<u>COLUMNS</u>	<u>FORMAT</u>	<u>PARAMETER</u>
2-6	A5	Converter/Controller Type
8-9	A2	Catalog Print Feature
11-14	A4	Program Procedure

<u>COLUMNS</u>	<u>FORMAT</u>	<u>PARAMETER</u>
15-20	I6	Design Constraint Option
21-25	F5.0	Design Constraint Value
26-30	I5	Max. No. of Evaluations to be performed (DSN1)
31-35	F5.0	Input Voltage Increment (volts)
36-40	F5.0	Output Power Increment (watts)

3.6.1 Converter/Controller Types--Program DC2DC

Program DC2DC may be used for the design of the reactor element and/or the evaluation of the operating characteristics of the two-winding voltage step-up/current step-up converter configuration shown in Figure 2. This converter circuit may be coupled with any one of three types of controllers--constant frequency, constant transistor on-time or constant transistor off-time. The converter/controller code indicates which of these three possible systems is to be designed and/or evaluated. The correct converter/controller code for each possible type of controller is given below.

<u>CODE</u>	<u>TYPE OF CONTROLLER</u>
FQ2UD	Constant Frequency
TN2UD	Constant On-time
TF2UD	Constant Off-time

PARAMETER	FORMAT
CONVERTER / CONTROLLER TYPE	A 5
CATALOG PRINT FEATURE	A 2
PROGRAM PROCEDURE	A 4
DESIGN CONSTRAINT OPTION	I 6
DESIGN CONSTRAINT VALUE	F5.0
MAXIMUM NO. OF EVALUATIONS	I 5
INPUT VOLTAGE INCREMENT	F5.0
OUTPUT POWER INCREMENT	F5.0

Figure 23. Type/Procedure Card
Program DC2DC

Figure 24. Example: Design Specification Card
Program DC2DC

3.6.2 Catalog Print Feature

On request, Program DC2DC will print out a listing of the core catalog and wire table. The use of this feature is identical to that of the Catalog Print Feature in Program DCLDC and is discussed in Section 3.1.2.

3.6.3 Program Procedure Codes

The Program Procedure Codes indicate which program procedure is desired. These codes are identical to those for Program DCLDC and are given in Section 3.1.4. The Program Procedures are discussed in Section 2.1.

3.6.4 Design Constraint Options--Program DC2DC

For the two-winding voltage step-up/current step-up circuit configuration shown in Figure 2, knowledge of the converter operating range and the magnetic core parameters is not sufficient to uniquely determine values for N_S and N_P [4]. This provides an additional degree of freedom in the design which may be useful to the designer. Program DC2DC makes use of this extra degree of freedom by allowing the user to select any one of ten Design Constraint Options. Each of these options places a constraint on the allowable values of certain converter system parameters. The actual numerical value of the particular constraint is referred to as the Design Constraint Value. The user specifies the desired Design Constraint Option by entering the integer option number from the list below in the field provided on the Type/Procedure Card (see Section 3.6). The Design Constraint Value, U_i , is also entered on the Type/Procedure Card.

<u>OPTION NO.</u>	<u>DESIGN CONSTRAINT OPTION</u>
-------------------	---------------------------------

1	Duty Cycle* Centered at U_1
2	Minimum Duty Cycle = U_2
3	Range of Duty Cycle Variation = U_3
4	Max. Transistor Collector-Emitter Voltage = U_4 volts
5	Max Reverse Diode Voltage = U_5 volts
6	Max. Peak Transistor Current = U_6 amps
7	Max. Peak Diode Current = U_7 amps
8	Maximum Duty Cycle = U_8
9	Total Number of Turns = $N_S + N_P = U_9$
10	Turns Ratio = $N_S/N_P = U_{10}$

*Duty Cycle is defined as the ratio of transistor on-time to the total period.

3.6.5 Evaluation Parameters

The Evaluation Parameters consist of the Input Voltage Increment and the Output Power Increment. These Parameters are discussed in Section 3.1.4 and serve the same function in both Program DC1DC and DC2DC.

3.7 DESIGN SPECIFICATION CARD--PROGRAM DC2DC

The design specifications are entered on the Design Specification Card as indicated in the table below (see also Figure 25). A sample Design Specification Card for Program DC2DC is shown in Figure 26.

<u>COLUMNS</u>	<u>FORMAT</u>	<u>PARAMETER</u>
1-5	F5.0	Output Voltage (volts)
6-10	F5.0	Minimum Input Voltage (volts)
11-15	F5.0	Maximum Input Voltage (volts)
16-20	F5.0	Minimum Output Power (watts)
21-25	F5.0	Maximum Output Power (watts)
26-30	F5.0	On-time, Off-time or Freq. (depending on controller) (usec or KHz)
31-35	F5.0	Residual Flux Density (tesla)
36-40	F5.0	Minimum Flux Density (tesla)
41-45	F5.0	Maximum Flux Density (tesla)
46-50	F5.0	Maximum Winding Factor
51-55	I5	Minimum No. of Cores in Stack
56-60	I5	Maximum No. of Cores in Stack
61-70	E10.3	Reciprocal Current Density $(m^2/ampere)$
72-75	A4	Wire Type
77-78	I2	Min. No. Strands--Primary
79-80	I2	Min. No. Strands--Secondary

FORMAT	PARAMETER	TYPE	FORMAT
	OUTPUT VOLTAGE (VOLTS)	F5.0	
	MINIMUM INPUT VOLTAGE (VOLTS)	F5.0	
	MAXIMUM INPUT VOLTAGE (VOLTS)	F5.0	
	MINIMUM OUTPUT POWER (WATTS)	F5.0	
	MAXIMUM OUTPUT POWER (WATTS)	F5.0	
	ON-TIME, OFF-TIME OR FREQ. (USEC OR KHZ)	F5.0	
	RESIDUAL FLUX DENSITY (TESLA)	F5.0	
	MINIMUM FLUX DENSITY (TESLA)	F5.0	
	MAXIMUM FLUX DENSITY (TESLA)	F5.0	
	MAXIMUM WINDING FACTOR	F5.0	
	MINIMUM NUMBER OF CORES IN STACK	I5	
	MAXIMUM NUMBER OF CORES IN STACK	I5	
	RECIPROCAL CURRENT DENSITY (M ² /AMPERE)	E10.3	
	WIRE TYPE CODE	A4	
	MIN. NO. PRI. WIRE STRANDS	I5	
	MIN. NO. SEC. WIRE STRANDS	I5	

Figure 25. Design Specification Card
Program DC2DC

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Figure 26. Example: Design Specification
Card---Program DC2DC

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3.7.1 Design Specifications

The meaning of certain of the design specifications is discussed in Section 3.2.1.

3.7.2 Wire Types

Four types of wire coating are available in the program. The user selects the desired type by entering the correct wire type code in the field provided for this purpose on the Design Specification Card. The wire type codes are given in Section 3.2.2 and are identical to those used in Program DC1DC.

3.8 ELEMENT LOSS CARD

The Element Loss Card gives parameters used in computing approximate power loss in the transistor, diode and capacitor. The format of this card is given in Section 3.3 and is the same as that used in Program DC1DC.

3.9 DSN2 AND EVAL CARD

3.9.1 DSN2 Card

In Procedure DSN2, the program attempts to compute a design using a specific magnetic core. The DSN2 Card is used only if the DSN2 procedure was specified on the Type/Procedure Card (Section 3.6). The format of the DSN2 Card is identical to that used in Program DC1DC and is discussed in Section 3.4.1.

3.9.2 EVAL Card--Program DC2DC

In Procedure EVAL, the program evaluates a design entered by the user. The EVAL Card is used only if the EVAL procedure was specified on the Type/Procedure Card (Section 3.6). The EVAL Card gives the integer size number of the core, the relative permeability, the number of cores in the stack, the wire sizes, and the number of primary and secondary turns. The integer core size number may be obtained from the "SIZE NO." column on the catalog listing produced by the program. The format of the EVAL Card is given in the table below (see also Figure 27). A sample EVAL Card is shown in Figure 28.

<u>COLUMNS</u>	<u>FORMAT</u>	<u>PARAMETER</u>
1-5	I5	Core Size Number from Catalog
6-10	F5.0	Relative Permeability of Core
11-15	I5	Number of Cores in Stack
16-20	I5	Number of Primary Turns
21-25	I5	Wire Size of Primary Winding
26-30	I5	Number of Secondary Turns
31-35	I5	Wire Size of Secondary Winding

FORMAT	PARAMETER	CORE SIZE NUMBER (INTEGER)	I5
	RELATIVE PERMEABILITY	F5.0	
	NUMBER OF CORES IN STACK	I5	
	NUMBER OF PRIMARY TURNS	I5	
	PRIMARY WIRE SIZE	I5	
	NUMBER OF SECONDARY TURNS	I5	
	SECONDARY WIRE SIZE	I5	

Figure 27. EVAL Card--Program DC2DC

22 185. 1 48 19 . 84 22

Figure 28. Example: EVAL Card--Program DC2DC

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3.9.3 Procedures DSN2 and EVAL with Cores not in the Catalog

If either a core size or a relative permeability value (or both) is not in the catalog, it is still possible to use Procedures DSN2 and EVAL. The method for using this feature is identical to that used in Program DC1DC and is discussed in Section 3.4.3.

3.10 QUIT/CONTINUE CARD

The final card in the control deck should have a zero in column one. If more than one design or evaluation is desired on a given run, a card with a one in column one may be used followed by another set of control cards. This may be repeated if desired. This feature is identical to that used in Program DC1DC.

3.11 ASSEMBLING THE CONTROL CARDS

The Control Cards for Programs DC1DC and DC2DC should be placed in the following order as shown before in Figure 12:

1. Type/Procedure Card -- For Program desired (DC1DC or DC2DC)
2. Design Specification Card -- For Program desired (DC1DC or DC2DC)
3. Element Loss Card
4. DSN2 or EVAL Card -- Only used if Procedure DSN2 or Procedure EVAL was specified on the Type/Procedure Card
5. Core Geometry Card -- Only used in Procedures DSN2 and EVAL when the core size is not in the Catalog

6. Loss-Coefficient Card--Only used in Procedures DSN2 and
EVAL when the value of relative
permeability is not in the catalog

7. Quit/Continue Card

3.12 ASSEMBLING THE DATA DECK

The data cards should be placed in the following order as shown before in Figure 11:

1. Core Catalog Cards]
 2. Wire Table Cards]
 3. Control Cards
-] The Data Base

PROGRAM OUTPUT

Figures 29 and 30 show sample outputs from Programs DC1DC and DC2DC respectively. The values of the output variables in these figures have been replaced by integer note numbers. Section 4.1 relates the integer note number to the meaning of the output variable or symbol. The output variables and symbols are also defined in the Appendix. Many of the output variables have the same meaning in both programs. Thus, in these cases, the particular variable in Figures 29 and 30 will be referenced to the same note number in Section 4.1. If a note applies to only one of the programs, the correct program will be clearly indicated in the text of the note. Otherwise, program names will not appear in the note.

(1) --CONSTANT

(2)

STEP-UP CONVERTER DESIGN

I/O IN VOLTS, AMPERES, WATTS, TESLAS, MICROSEC, KHZ, OHMS

CONVERTER SPECIFICATIONS

V OUT	V IN MIN	V IN MAX	P OUT MIN	P OUT MAX	I SAT	I COLL.	V DIODE	CAP ESR	B RESIDUAL	B MIN	B MAX	WIND FACTOR	MAT CORES	
(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	(12)	(13)	(14)	(15)	(16)	(17)	(18)

WIRE TYPE=

(19) MIN. STRANDS= (21) RECIPROCAL CURRENT DENSITY= (20) SG. M/INCH

THE FOLLOWING CORES MATCH THE CONSTRAINTS WHEN USED IN A -CORE STACK

SIZE NO.	MAGNETICS	ARNOLD	MU	N	AWG	IND. MH	VDG FAC	DSN MODE	OP MODE	IB MAX	IXRMS MAX	ICPMS MAX
(25)	(26)	(27)	(28)	(29)	(31)	(33)	(38)	(39)	(40)	(41)	(44)	(47)

DESIGN EVALUATION

MAX. NO. OF EVALUATIONS =

EVALIGATION FOR DESIGN NO.

SIZE NO.	MAGNETICS	ARNOLD	MU	N	AWG	IND. MH	VDG FAC	DSN MODE	OP MODE	IB MAX	IXRMS MAX	ICPMS MAX
(25)	(26)	(27)	(28)	(29)	(31)	(33)	(38)	(39)	(40)	(41)	(44)	(47)
REACTOR AREA SQ.M	PATH LENGTH M	CORE WH. AREAL SQ.M	REACTOR LENGTH/TURN M	STACK HEIGHT M	REACTOR MASS KG	REACTOR WIRE LENGTH M	REACTOR WIRE RES. OHMS					
(48)	(49)	(50)	(51)	(52)	(53)	(54)	(56)					
V IN=	PO WATTS	IA AMPS	IB AMPS	FREQ KHZ	IXAVER AMPS	IXRMS AMPS	ICRMS AMPS	TRANS DIODE LOSSES (WATTS)	VIRE CORE CAPAC TOTAL	EFF %	EPE/MASS X/EG	
(60)	(61)	(64)	(67)	(68)	(70)	(71)	(74)	(75)	(76)	(77)	(78)	(81)
												(82)

Figure 29. Output of Program DC1DC

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(1) --CONSTANT (3) TWO-WINDING VOLTAGE STEP-UP/CURRENT STEP-UP CONVERTER DESIGN
 I/O IN VOLTS, AMPERES, WATTS, TESLAS, MICROSEC, KHZ, OHMS

CONVERTER SPECIFICATIONS

V OUT	V IN MIN	V IN MAX	P OUT MIN	P OUT MAX	V SAT	I COLL.	V DIODE	CAP ESR	B RESIDUAL	B MIN	B MAX	WIND FACTOR	R IX CCIES	
4	5	6	7	8	9	10	11	12	13	14	15	16	17	18

WIRE TYPE = (19) MIN. PRI. STRANDS = (22) MIN. SEC. STRANDS = (23) RECIPROCAL CURRENT DENSITY = (20) SQ.M/Amp

(24)

THE FOLLOWING CORES MATCH THE CONSTRAINTS WHEN USED IN A -CORE STACK

SIZE MAGNETICS NO.	ARNOLD	HU	NP	Avg PRI. IND. PRI.	NS	Avg SEC. IND. MM	WDG OF FAC NODE	IBP MAX	IBS MAX	IPRMS MAX	ISRMS MAX	ICRS MAX				
25	26	27	28	30	32	34	35	36	37	38	40	42	43	45	46	47

DESIGN EVALUATION

MAX. NO. OF EVALUATIONS =

EVALUATION FOR DESIGN NO.

SIZE MAGNETICS NO.	ARNOLD	HU	NP	Avg PRI. IND. PRI.	NS	Avg SEC. IND. MM	WDG OF FAC NODE	IBP MAX	IBS MAX	IPRMS MAX	ISRMS MAX	ICRS MAX					
25	26	27	28	30	32	34	35	36	37	38	40	42	43	45	46	47	
REACTOR AREA SQ.R	PATH LENGTH M	CORE WH. AREA SQ.M	REACTOR LENGTH/TURN 8	STACK HEIGHT 8	REACTOR MASS KG	REACTOR PRI. WIRE LENGTH, M	REACTOR PRI. WIRE RES, OHMS	REACTOR SEC. WIRE LENGTH, M	REACTOR SEC. WIRE RES, OHMS								
48	49	50	51	52	53	54	55	56	57	58	59						
Y IN=	PO WATTS	IPM AMPS	IBS AMPS	IBP AMPS	IPRMS AMPS	ISRMS AMPS	ICRMS AMPS	TRANS CAPAC	DIODE TOTAL	LOSSSES (WATTS)	EPP/MASS X/KG						
60	62	63	65	66	68	72	73	74	75	76	77	78	79	80	81	82	

Figure 30. Output of Program DC2DC

PRODUCIBILITY OF THE
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4.1 PROGRAM OUTPUT VARIABLES AND SYMBOLS

<u>NOTE NO.</u>	<u>OUTPUT VARIABLE</u>	<u>NOTE</u>
1	Converter/Controller Code	See Sections 3.1.1 & 3.6.1
2	Type of Converter/Controller (Program DC1DC)	See Section 3.1.1
3	Type of Controller (DC2DC)	See Section 3.6.1
4	V OUT	The regulated converter output voltage (volts)
5	V IN MIN	The specified minimum input voltage (volts)
6	V IN MAX	The specified maximum input voltage (volts)
7	P OUT MIN	The specified minimum output power (watts)
8	P OUT MAX	The specified maximum output power (watts)
9	V SAT	The transistor saturation voltage (volts)
10	I COLL	The current in the collector of the transistor at which the saturation voltage was measured (amperes)
11	V DIODE	The diode forward drop (volts)
12	CAP ESR	The effective series resistance (ESR) of the capacitor (ohms)
13	T ON, T OFF or FREQ (depending on controller)	The constant parameter of the controller, either transistor on-time, transistor off-time or frequency (usec or KHz)
14	B RESIDUAL	The residual flux density of the core material (tesla)

<u>NOTE NO.</u>	<u>OUTPUT VARIABLE</u>	<u>NOTE</u>
15	B MIN	The specified minimum flux density (tesla)
16	B MAX	The specified maximum flux density (tesla)
17	WIND FACTOR	The specified maximum allowable winding factor
18	MAX CORES	The specified maximum allowable number of cores in the stack
19	WIRE TYPE	See Section 3.2.2
20	RECIPROCAL CURRENT DENSITY	The specified minimum reciprocal current density ($m^2/ampere$)
21	MIN STRANDS	The specified minimum no. of strands of wire to be used in the winding (DC1DC)
22	MIN PRI. STRANDS	The specified minimum no. of strands of wire to be used in the primary winding (DC2DC)
23	MIN SEC. STRANDS	The specified minimum no. of strands of wire to be used in the secondary winding (DC2DC)
24	DESIGN CONSTRAINT	See Section 3.6.4 (DC2DC)
25	SIZE NO.	The integer core size no. from the catalog (see Section 6.4)
26	MANUFACTURER'S NO.	The particular core number from the catalog of the first core manufacturer (in this case, Magnetics)
27	MANUFACTURER'S NO.	The particular core number from the catalog of the second core manufacturer (in this case, Arnold Engineering)

<u>NOTE NO.</u>	<u>OUTPUT VARIABLE</u>	<u>NOTE</u>
28	MU	The value of relative permeability of the core
29	N	The number of turns of wire in the winding (DC1DC)
30	NP	The number of turns of wire in the primary winding (DC2DC)
31	AWG	The AWG wire size used in the winding (DC1DC)
32	AWG PRI.	The AWG wire size used in the primary winding (DC2DC)
33	IND	The computed value of inductance (mh) (DC1DC)
34	PRI. IND	The computed value of primary inductance (mh) (DC2DC)
35	NS	The number of turns of wire in the secondary winding (DC2DC)
36	AWG SEC.	The AWG wire size used in the secondary winding (DC2DC)
37	SEC. IND	The computed value of the secondary inductance (mh) (DC2DC)
38	WDG FAC	The computed value of the winding factor, defined as the ratio of the area of the core window filled by the winding(s) to the total window area of the core
39	DSN MODE	The mode of operation which occurs at the design point in the PO-VI plane [4]. A "1" denotes Mode 1 operation (continuous conduction) and a "2" implies Mode 2 (discontinuous conduction) operation. (DC1DC) (see Section 3.2.1)

<u>NOTE NO.</u>	<u>OUTPUT VARIABLE</u>	<u>NOTE</u>
40	OP MODE	A value of "1" for this variable indicates that the converter operates in Mode 1 (continuous conduction) everywhere within the design range. A value of "2" indicates that the converter operates in Mode 2 (discontinuous conduction) at least somewhere within the design range
41	IB MAX	The maximum value that the peak reactor current takes on over the entire design range of the converter (DC1DC)
42	IBP MAX	The maximum value that the peak primary current takes on over the entire design range of the converter (DC2DC)
43	IBS MAX	The maximum value that the peak secondary current takes on over the entire design range of the converter (DC2DC)
44	IXRMS MAX	The maximum value that the RMS reactor current takes on over the entire design range of the converter (DC1DC)
45	IPRMS MAX	The maximum value that the RMS primary current takes on over the entire design range of the converter (DC2DC)
46	ISRMS MAX	The maximum value that the RMS secondary current takes on over the entire design range of the converter (DC2DC)

<u>NOTE NO.</u>	<u>OUTPUT VARIABLE</u>	<u>NOTE</u>
47	ICRMS MAX	The maximum value that the RMS capacitor current takes on over the entire design range of the converter
48	REACTOR AREA	The cross-sectional area of the magnetic material in the core stack used (m^2)
49	PATH LENGTH	The mean magnetic path length of the core used (m)
50	CORE WN. AREA	The area of the core window (m^2)
51	REACTOR LENGTH/TURN	The mean length/turn of the wound reactor, computed on the same basis as the core length/turn parameter (see Sec. 6.4.2) (m)
52	REACTOR HEIGHT	The height in meters of the core stack
53	REACTOR MASS	The mass of the wound reactor, neglecting the mass of the wire insulation (kg)
54	WIRE LENGTH	The length in meters of the wire used in the winding, based on a 40% winding factor (DC1DC)
55	PRI. WIRE LENGTH	The length in meters of the wire used in the primary winding, based on a 40% winding factor (DC2DC)
56	WIRE RES.	The resistance in ohms of the winding (DC1DC)
57	PRI. WIRE RES.	The resistance in ohms of the primary winding (DC2DC)
58	SEC. WIRE LENGTH	The length in meters of the wire used in the secondary winding, based on a 40% winding factor (DC2DC)

<u>NOTE NO.</u>	<u>OUTPUT VARIABLE</u>	<u>NOTE</u>
59	SEC. WIRE RES	The resistance in ohms of the secondary winding (DC2DC)
60	PO	The converter output power (watts)
61	IA	The minimum value of the reactor current over a cycle (amperes) (DC1DC)
62	IAP	The value in amperes that the primary current takes on at the beginning of the transistor on-time (DC2DC)
63	IAS	The value in amperes that the secondary current takes on at the beginning of the transistor on-time (DC2DC)
64	IB	The maximum value in amperes that the reactor current takes on over a cycle (DC1DC)
65	IBP	The maximum value in amperes that the primary current takes on over a cycle (DC2DC)
66	IBS	The maximum value in amperes that the secondary current takes on over a cycle (DC2DC)
67	T ON or T'OFF (depending on controller)	The transistor on-time (T ON), or that portion of the transistor off-time during which the reactor current is greater than zero (T'OFF). (DC1DC) (usec)
68	FREQ	The converter frequency (KHz) (DC1DC)
69	FREQ or T ON (depending on controller)	The converter frequency in KHz (FREQ) or the transistor on-time (T ON) in usec (DC2DC)
70	IXAVE	The average value (amperes) of the reactor current (DC1DC)

<u>NOTE NO.</u>	<u>OUTPUT VARIABLE</u>	<u>NOTE</u>
71	IXRMS	The RMS value (amperes) of the reactor current (DC1DC)
72	IPRMS	The RMS value (amperes) of the primary current (DC2DC)
73	ISRMS	The RMS value (amperes) of the secondary current (DC2DC)
74	ICRMS	The RMS value (amperes) of the current in the capacitor
75	LOSSES TRANS	Estimated power loss (watts) in the transistor (see Sec. 1.2.1)
76	LOSSES DIODE	Estimated power loss (watts) in the diode (see Sec. 1.2.2)
77	LOSSES WIRE	Estimated power loss (watts) in the reactor winding(s) (see Sec. 1.2.3)
78	LOSSES CORE	Estimated power loss (watts) in the magnetic core material (see Sec. 1.2.3)
79	LOSSES CAPAC	Estimated power loss (watts) in the capacitor (see Sec. 1.2.4)
80	LOSSES TOTAL	Estimated total power loss (watts). Computed as the sum of the transistor, diode, wire, core and capacitor losses
81	EFF	Estimated converter efficiency (%). Computed as the ratio of the output power to output power plus losses
82	EFF/MASS	The estimated converter efficiency divided by the mass of the wound reactor

SAMPLE PROGRAMS

The five sample programs given in Sections 5.2-5.6 offer possible uses of Program DC1DC in the solution to a hypothetical design problem. The same design problem is attacked through the use of Program DC2DC in Sections 5.7-5.9. These sets of programs begin with specified design requirements and work toward two completed reactor element designs (a single-winding design from Program DC1DC and a two-winding design from Program DC2DC) using the computer programs as tools. The procedure followed in completing these designs is structured so as to illustrate all of the available program procedures and is not intended to be illustrative of a "typical" design procedure. A single design problem was chosen so that similarities and differences in the program output could be more readily compared across the set of program procedures. Also, the use of a single design problem serves to more clearly illustrate some of the possible advantages offered by the Design Constraint Options provided by Program DC2DC. In the following sections, the previously adopted convention of including the relevant program name in the title of each section will be continued. Sections whose titles do not mention a particular program name (i.e. DC1DC or DC2DC) apply to both sets of sample programs.

5.1 SAMPLE PROBLEM

Design a reactor element for a voltage step-up/current step-up converter with a constant frequency controller which will meet the following set of design requirements:

Output Voltage	24.0 volts
Input Voltage Range	6.0 to 16.0 volts
Output Power Range	10.0 to 20.0 watts
Converter Frequency	10.0 KHz

Also given are the following parameter values for the circuit components:

Transistor Saturation Voltage	1.0 volt @ 10.0 amperes
Diode Forward Drop	0.6 volt
Capacitor ESR	0.10 ohm

By consulting manufacturers' core catalogs, it is determined that the Residual Flux Density of the core material is on the order of 0.01 tesla. From manufacturer's data a value should also be selected for the maximum operating flux density so that the program assumption that the core operates in its linear region is satisfied. Assume that a value of 0.36 tesla will satisfy this assumption.

Finally, assume the commonly used values of 0.4 for the maximum allowable winding factor, $5.067 \times 10^{-7} \text{ m}^2/\text{ampere}$ ($= 1000$ circular mils/ampere) reciprocal current density and that heavy coated wire will be used for the winding(s). The maximum value

of the winding factor is determined largely by the technique used for winding the core and the wire size. Experience is the best guide for choosing a maximum allowable winding factor. The reciprocal current density value chosen may vary with application and type of package or other criteria and the type of wire coating chosen depends on turn-to-turn voltage level and possibly other factors.

5.2 SAMPLE PROGRAM #1 --- PROGRAM DC1DC

As a starting point, Sample Program #1 uses the DSN1 procedure of Program DC1DC to obtain a list of usable single-winding reactor designs for the circuit of Figure 1-c. By referring to Sections 3.1 - 3.6 it can be seen that most of the required input data has been given in Section 5.1. Now the minimum number of cores in the stack, the minimum number of strands of wire, the minimum value of flux density, and a set of parameters for use in the evaluation must be selected.

Setting the minimum flux density equal to the residual flux density insures that both designs which operate only in Mode 1 (continuous conduction mode) and those which operate both in Mode 1 and Mode 2 (discontinuous conduction mode) will be produced. Unless space or wire stiffness is a problem, designs with only one core and one strand of wire would normally be desired. Choosing a one core minimum stack and the minimum number of strands = 1 will allow such designs to be computed. Also, assume that designs which have a stack height of two cores or less are required.

For illustration, the first three designs are evaluated in Sample Program #1. Since both the input voltage range and the output power range cover 10 units, setting the input voltage increment and the output power increment equal to 2.0 units gives evaluations at six values of output power for each one of six values of input voltage, i.e. thirty-six evaluation points.

5.2.1 Design Requirement Input Data--Sample Program #1 (DC1DC)

The following is a complete summary of the input data:

Converter/Controller Code	FQUD
Catalog Print Code	NP
Program Procedure	DSN1
Output Voltage	24.0 volts
Input Voltage Range	6.0 to 16.0 volts
Output Power Range	10.0 to 20.0 watts
Converter Frequency	10.0 KHz
Residual Flux Density	0.01 tesla
Minimum Flux Density	0.01 tesla
Maximum Flux Density	0.36 tesla
Maximum Winding Factor	0.4
Wire Type Code	HEAV
Reciprocal Current Density	$5.067 * 10^{-7} \text{ m}^2/\text{ampere}$
Minimum No. of Cores in Stack	1
Maximum No. of Cores in Stack	2
Minimum No. of Strands of Wire	1
Transistor Saturation Voltage	1.0 volt @ 10.0 amperes

Diode Forward Drop	0.6 volt
Capacitor ESR	0.1 ohm
Maximum No. of Evaluations	3
Input Voltage Increment	2.0 volts
Output Power Increment	2.0 watts

5.2.2 Control Cards--Sample Program #1 (Program DC1DC)

The control cards for Sample Program #1 are shown below. Sections 3.1-3.6 give instructions for preparing these cards.

FQUD NF DSN1 3 2. 2. .01 .01 .36 .4 1 2 5.067E-07 HEAVY 1
84. 6. 16. 10. 20. 10. .01 .01 .36 .4 1 2 5.067E-07 HEAVY 1
1.0 10. .60 .1

5.2.3 Results of Sample Program #1--Program DC1DC

The results of Sample Program #1 are given on the following pages. Program DC1DC has produced a list of fifty single-winding reactor designs which will meet the design requirements. The list of designs gives the manufacturers' catalog numbers, relative permeability, number of turns, wire size, and winding factor for each usable design as well as other parameters. Note from the print out that all of the designs generated use only one core in the stack. Also, many of the designs operate in Mode 2

(discontinuous conduction mode) over some portion of the operating range. This can be seen from the "OP MODE" column of the design list. Note also that the actual winding factor, as seen in the "WDG FAC" column, is less than the specified maximum of 0.4 for all the listed designs. By noting the RMS value of the reactor current from the "IXRMS MAX" column and applying the reciprocal current density constraint, it can be seen that the program has chosen the correct wire size in all cases.

In the design evaluations, the output gives the same design information as was given in the design list. However, additional information on the reactor is also given. As desired, thirty-six evaluation points have been produced with six values of output power for each of six values of input voltage. Note that the value of IA is equal to zero over some part of the design range for those designs whose "OP MODE" is equal to two. The last two columns in the evaluation output give estimates of the converter efficiency and the efficiency/mass. The EFF/MASS column may be particularly useful in comparing designs in terms of performance-to-weight.

FOUND—CONSTANT FREQ VOLTAGE STEP-UP/CURRENT STEP-UP CONVERTER DESIGN
I/O IN VOLTS, AMPERE, WATTS, TESLAS, MICROSEC, KHZ, OHMS

CONVERTER SPECIFICATIONS

T _{OUT}	V _{IN} MIN	V _{IN} MAX	P _{OUT} MIN	P _{OUT} MAX	I _{SAT}	C _{COLL.}	I _{DICDE}	C _{AV} ESR	C _{CCV} FREQ	E _{RESIDUAL}	B _{MIN}	B _{MAX}	WIND FACTOR	MAX CORES
24.0	6.0	16.0	10.0	20.0	1.00	10.0C	0.60	0.10	10.0	1.000E-02	1.000E-02	3.600E-01	0.40	2

WIRE TYPE= HELY MIN. STRANDS= 1 RECIPROCAL CURRENT DENSITY= 5.067E-07 SQ.M/AMP

THE FOLLOWING CORES MATCH THE CONSTRAINTS WHEN USED IN A 1-CORE STACK

SIZE NO.	MAGNETICS	ARMOLD	BU	X	1WG	IND. MH	Wdg FAC	DSH NODE	OP CODE	IS MAX	ITEMS MAX	ICORES MAX
21	55548	1-588127	125.	22	12	0.063	0.278	1	2	8.256	1	2.009
23	555324	1-229117	125.	28	13	0.093	0.228			7.168		1.823
25	555294	1-254168	125.	38	13	0.247	0.264	1	1	5.776	1	1.659
26	555295	1-151198	187.	38	13	0.193	0.215			0.01455		1.659
28	555252	1-306215	160.	28	13	0.171	0.194			0.398		1.671
28	555249	1-179233	173.	25	13	0.168	0.178			0.162		1.678
28	55251	1-214276	200.	20	13	0.109	0.139			0.157		1.678
28	55089	1-378336	250.	12	13	0.049	0.104			0.308		1.678
28	55089	1-089178	125.	48	13	0.418	0.233			0.308		1.678
28	55088	1-153210	187.	50	13	0.301	0.175			0.308		1.678
28	55087	1-216228	160.	36	13	0.273	0.150			0.308		1.678
28	55082	1-195266	173.	33	13	0.212	0.131			0.308		1.678
28	55086	1-326228	200.	21	13	0.160	0.102			0.308		1.678
28	55084	1-402287	250.	16	13	0.073	0.078			0.308		1.678
26	55715	1-023498	350.	12	13	0.418	0.205			0.308		1.678
26	55714	1-715152	350.	22	13	0.301	0.187			0.308		1.678
26	55713	1-217198	160.	52	13	0.201	0.168			0.308		1.678
26	55709	1-181210	173.	50	13	0.173	0.147			0.308		1.678
26	55712	1-217194	173.	52	13	0.154	0.118			0.308		1.678
26	55710	1-404288	160.	52	13	0.107	0.067			0.308		1.678
27	55109	1-109108	173.	50	13	0.063	0.068			0.308		1.678
27	55108	1-109108	173.	50	13	0.063	0.068			0.308		1.678
27	55107	1-109108	173.	50	13	0.063	0.068			0.308		1.678
27	55103	1-109108	173.	50	13	0.063	0.068			0.308		1.678
27	55106	1-109108	173.	50	13	0.063	0.068			0.308		1.678
27	55106	1-326228	200.	22	13	0.231	0.131			0.308		1.678
28	55438	1-402287	250.	15	13	0.184	0.084			0.308		1.678
28	55436	1-152430	173.	38	13	0.592	0.056			0.308		1.678
28	55436	1-325366	160.	38	13	0.496	0.264			0.308		1.678
28	55435	1-180396	173.	32	13	0.414	0.222			0.308		1.678
28	55435	1-215462	200.	27	13	0.341	0.168			0.308		1.678
28	55433	1-379562	250.	21	13	0.256	0.146			0.308		1.678
28	55433	1-501674	200.	16	13	0.179	0.111			0.308		1.678
28	55433	1-422787	250.	13	13	0.138	0.090			0.308		1.678
28	55433	1-423068	60.	185	13	0.108	0.052			0.308		1.678
28	55433	1-866142	125.	87	13	0.052	0.143			0.308		1.678
28	55433	1-156167	167.	73	13	0.052	0.120			0.308		1.678
28	55433	1-183197	173.	62	13	0.052	0.102			0.308		1.678
28	55433	1-219233	205.	55	13	0.052	0.084			0.308		1.678
28	55433	1-725112	160.	55	13	0.052	0.064			0.308		1.678
28	554228	1-542228	125.	94	13	0.052	0.114			0.308		1.678
28	554228	1-157268	173.	80	13	0.052	0.097			0.308		1.678
28	554228	1-1008316	173.	67	13	0.052	0.081			0.308		1.678
31		1-220374	205.	67	13	1.647	0.051			0.308		1.678

THE MAXIMUM OF 50 WINDABILITY CHECKS HAS BEEN REACHED

PRODUCIBILITY OF THE
FINAL PAGE IS POOR.

DESIGN EVALUATION

MAX. NO. OF EVALUATIONS = 3

EVALUATION FOR DESIGN NO. 1

SIZE NO.	MAGNETICS			ARNOLD		H.U.	N	ANG	IND. HR	WDG FAC	DSW MODE	OP MODE	IS MAX	IIRMS MAX	ICFMS MAX
	55548	A-548127	125.	22	12										
21.															
REACTOR AREA SQ.M	PATH LENGTH M	CORE VN. AREA SQ.M	REACTOR LENGTH/TURN M	STACK HEIGHT M	REACTOR MASS KG	REACTOR WIRE LEN. M	REACTOR WIRE RES. CHMS								
6.720E-05	8.150E-02	2.927E-04	4.270E-02	1.160E-02	7.379E-02	9.394E-01	4.993E-03								
V IN= 6.0															
PO WATTS	IA AMPS	IB AMPS	T ON USEC	FREQ KHZ	IXAVE AMPS	IIRMS AMPS	ICRMS AMPS	TRANS DIODE	LOSSES WIRE2	(WATTS) CORE	CAPAC	TOTAL	EPP %	EPP/MASS %	
10.0	0.0	5.72	71.7	10.00	2.467	3.067	1.189	0.782	0.250	0.047	0.757	0.141	1.977	83.5	1.132E 03
12.0	0.0	6.26	78.5	10.00	2.950	3.516	1.356	1.027	0.300	0.062	0.989	0.184	2.562	82.4	1.112E 03
14.0	0.0	6.77	83.1	10.00	3.953	3.947	1.514	1.295	0.350	0.078	1.167	0.229	3.120	81.4	1.108E 03
16.0	0.0	7.26	83.1	10.00	4.386	4.835	1.675	1.599	0.400	0.096	1.167	0.281	3.542	81.1	1.108E 03
18.0	0.0	7.75	83.1	10.00	4.890	5.291	1.840	1.943	0.450	0.117	1.167	0.339	4.015	81.1	1.108E 03
20.0	0.0	8.25	83.1	10.00	4.933	2.009	2.327	0.500	0.140	0.167	0.404	0.537	4.537	81.1	1.108E 03
V IN= 8.0															
PO WATTS	IA AMPS	IB AMPS	T ON USEC	FREQ KHZ	IXAVE AMPS	IIRMS AMPS	ICRMS AMPS	TRANS DIODE	LOSSES WIRE	(WATTS) CORE	CAPAC	TOTAL	EPP %	EPP/MASS %	
10.0	0.0	5.72	51.2	10.00	1.881	2.678	1.189	0.558	0.250	0.036	0.757	0.141	1.743	85.2	1.154E 03
12.0	0.0	6.26	56.1	10.00	2.257	3.070	1.356	0.738	0.300	0.047	0.989	0.184	2.250	84.3	1.141E 03
14.0	0.0	6.77	60.6	10.00	2.633	3.447	1.514	0.925	0.350	0.059	1.240	0.229	2.803	83.3	1.129E 03
16.0	0.0	7.23	64.8	10.00	3.010	3.810	1.664	1.130	0.400	0.072	1.508	0.277	3.387	82.3	1.118E 03
18.0	0.0	7.67	68.7	10.00	3.385	4.161	1.809	1.348	0.450	0.086	1.793	0.327	4.005	81.6	1.109E 03
20.0	0.0	8.09	72.4	10.00	3.762	4.504	1.949	1.579	0.500	0.101	2.094	0.380	4.654	81.1	1.099E 03
V IN= 10.0															
PO WATTS	IA AMPS	IB AMPS	T ON USEC	FREQ KHZ	IXAVE AMPS	IIRMS AMPS	ICRMS AMPS	TRANS DIODE	LOSSES WIRE	(WATTS) CORE	CAPAC	TOTAL	EPP %	EPP/MASS %	
10.0	0.0	5.72	39.8	10.00	1.556	2.935	1.189	0.436	0.250	0.030	0.757	0.141	1.613	86.1	1.167E 03
12.0	0.0	6.26	43.6	10.00	1.867	2.792	1.356	0.571	0.300	0.039	0.989	0.184	2.082	85.1	1.155E 03
14.0	0.0	6.77	47.1	10.00	2.178	3.134	1.514	0.719	0.350	0.049	1.240	0.229	2.567	84.1	1.144E 03
16.0	0.0	7.23	50.4	10.00	2.465	3.464	1.664	0.879	0.400	0.060	1.508	0.277	3.124	83.1	1.133E 03
18.0	0.0	7.67	53.4	10.00	2.800	3.784	1.809	1.049	0.450	0.072	1.793	0.327	3.690	82.1	1.125E 03
20.0	0.0	8.09	56.3	10.00	3.111	4.096	1.949	1.223	0.500	0.084	2.094	0.380	4.285	81.1	1.116E 03
V IN= 12.0															
PO WATTS	IA AMPS	IB AMPS	T ON USEC	FREQ KHZ	IXAVE AMPS	IIRMS AMPS	ICRMS AMPS	TRANS DIODE	LOSSES WIRE	(WATTS) CORE	CAPAC	TOTAL	EPP %	EPP/MASS %	
10.0	0.0	5.72	32.6	10.00	1.368	2.267	1.189	0.355	0.250	0.026	0.757	0.141	1.530	86.7	1.175E 03
12.0	0.0	6.26	35.7	10.00	1.618	2.600	1.356	0.467	0.300	0.034	0.989	0.184	1.973	85.6	1.164E 03
14.0	0.0	6.77	39.6	10.00	1.868	2.918	1.514	0.582	0.350	0.043	1.240	0.229	2.450	84.6	1.153E 03
16.0	0.0	7.23	43.1	10.00	2.178	3.226	1.664	0.719	0.400	0.052	1.508	0.277	2.956	83.6	1.142E 03
18.0	0.0	7.67	45.7	10.00	2.427	3.524	1.809	0.854	0.450	0.062	1.793	0.327	3.490	82.6	1.132E 03
20.0	0.0	8.09	46.1	10.00	2.697	3.813	1.949	1.005	0.500	0.073	2.094	0.380	4.051	81.6	1.127E 03
V IN= 14.0															
PO WATTS	IA AMPS	IB AMPS	T ON USEC	FREQ KHZ	IXAVE AMPS	IIRMS AMPS	ICRMS AMPS	TRANS DIODE	LOSSES WIRE	(WATTS) CORE	CAPAC	TOTAL	EPP %	EPP/MASS %	
10.0	0.0	5.72	27.6	10.00	1.205	2.143	1.189	0.301	0.250	0.023	0.757	0.141	1.472	87.2	1.181E 03
12.0	0.0	6.26	30.2	10.00	1.446	2.458	1.356	0.395	0.300	0.030	0.989	0.184	2.098	86.3	1.170E 03
14.0	0.0	6.77	32.6	10.00	1.687	2.759	1.514	0.498	0.350	0.038	1.240	0.229	2.555	85.6	1.160E 03
16.0	0.0	7.23	34.9	10.00	1.928	3.028	1.664	0.603	0.400	0.046	1.508	0.277	3.040	84.9	1.151E 03
18.0	0.0	7.67	37.0	10.00	2.169	3.231	1.809	0.705	0.450	0.055	1.793	0.327	3.352	83.7	1.142E 03
20.0	0.0	8.09	39.0	10.00	2.410	3.605	1.949	0.850	0.500	0.065	2.094	0.380	3.889	82.7	1.135E 03
V IN= 16.0															
PO WATTS	IA AMPS	IB AMPS	T ON USEC	FREQ KHZ	IXAVE AMPS	IIRMS AMPS	ICRMS AMPS	TRANS DIODE	LOSSES WIRE	(WATTS) CORE	CAPAC	TOTAL	EPP %	EPP/MASS %	
10.0	0.0	5.72	23.9	10.00	1.100	2.048	1.189	0.261	0.250	0.021	0.757	0.141	1.430	87.5	1.186E 03
12.0	0.0	6.26	26.2	10.00	1.320	2.348	1.356	0.382	0.300	0.028	0.989	0.184	2.043	86.7	1.179E 03
14.0	0.0	6.77	28.3	10.00	1.540	2.636	1.514	0.432	0.350	0.035	1.240	0.229	2.285	86.3	1.169E 03
16.0	0.0	7.23	30.2	10.00	1.760	2.913	1.664	0.527	0.400	0.042	1.508	0.277	2.755	85.5	1.159E 03
18.0	0.0	7.67	32.1	10.00	1.980	3.182	1.809	0.629	0.450	0.051	1.793	0.327	3.250	84.7	1.150E 03
20.0	0.0	8.09	33.8	10.00	2.200	3.444	1.949	0.737	0.500	0.059	2.094	0.380	3.770	84.1	1.140E 03

SIZE NO.	SYNTHESIS FOR DESIGN NO. 2		ARNOLD	NU	X	ANG. MH.	IND. MH.	Wdg FAC	DSK NODE	OP NODE	ID MAX	ITEMS MAX				
	MAGNETICS															
23	55324	1-324117	125.	28	13	0.093	0.228	1	2	7.168	5.099	1.923				
REACTOR AREA SQ.F.	BARTH LENGTH IN	CORE AREA SQ.F.	REACTOR LENGTH/TUBE IN	STACK HEIGHT IN	REACTOR ROSS KG	REACTOR WIRE LEN. M	REACTOR WIRE RES. CRMS									
6.780E-05	8.980E-02	3.644E-04	4.340E-02	1.130E-02	7.952E-02	1.215E 00	8.133E-03									
T IX= 6.0	PO WATTS	IA AMPS	IB AMPS	T ON USEC	FREQ KHZ	IXAVE AMPS	IXAMS AMPS	ICRMS AMPS	TRANS DIODE	LOSSSES WIRE	(WATTS) CORE	***** CAPAC	EFF %	EFF/MASS %		
10.0	0.0	0.23	0.70	83.1	10.00	2.467	2.784	1.063	0.644	0.250	0.663	0.624	0.114	1.695	85.6	1.075E 03
12.0	0.0	0.23	0.19	83.1	10.00	2.460	2.259	1.229	0.566	0.250	0.295	0.624	0.151	2.027	85.6	1.073E 03
14.0	0.0	0.22	0.69	83.1	10.00	2.453	2.086	1.398	1.129	0.250	0.111	0.624	0.196	2.110	85.6	1.068E 03
16.0	0.0	0.21	0.18	83.1	10.00	2.447	1.952	1.571	1.433	0.250	0.180	0.624	0.247	2.044	85.6	1.061E 03
18.0	0.0	0.21	0.67	83.1	10.00	2.440	1.828	1.746	1.777	0.250	0.178	0.624	0.305	3.930	85.6	1.054E 03
20.0	0.0	0.20	0.17	83.1	10.00	4.933	5.099	1.923	2.161	0.500	0.211	0.624	0.370	3.867	85.6	1.054E 03
T IX= 8.0	PO WATTS	IA AMPS	IB AMPS	T ON USEC	FREQ KHZ	IXAVE AMPS	IXAMS AMPS	ICRMS AMPS	TRANS DIODE	LOSSSES WIRE	(WATTS) CORE	***** CAPAC	EFF %	EFF/MASS %		
10.0	0.0	0.23	0.70	62.4	10.00	1.881	2.327	1.063	0.458	0.250	0.668	0.721	0.113	1.591	86.3	1.085E 03
12.0	0.0	0.23	0.18	68.3	10.00	2.453	2.082	1.210	0.603	0.300	0.663	0.941	0.146	2.053	86.3	1.074E 03
14.0	0.0	0.22	0.56	73.8	10.00	2.447	1.953	1.389	0.759	0.350	0.378	1.380	0.182	2.050	86.3	1.058E 03
16.0	0.0	0.21	0.56	77.8	10.00	2.440	1.829	1.689	0.924	0.400	0.397	1.380	0.220	2.020	86.3	1.062E 03
18.0	0.0	0.20	0.33	77.8	10.00	3.386	3.785	1.750	1.175	0.450	0.117	1.380	0.307	3.050	86.3	1.064E 03
20.0	0.0	0.19	0.69	77.8	10.00	3.762	4.125	1.732	1.323	0.500	0.138	1.380	0.307	3.050	86.3	1.064E 03
T IX= 10.0	PO WATTS	IA AMPS	IB AMPS	T ON USEC	FREQ KHZ	IXAVE AMPS	IXAMS AMPS	ICRMS AMPS	TRANS DIODE	LOSSSES WIRE	(WATTS) CORE	***** CAPAC	EFF %	EFF/MASS %		
10.0	0.0	0.23	0.70	88.5	10.00	1.556	2.207	1.063	0.367	0.250	0.380	0.721	0.113	1.580	87.1	1.095E 03
12.0	0.0	0.23	0.18	88.5	10.00	1.857	2.530	1.210	0.600	0.300	0.380	0.941	0.146	2.009	87.1	1.076E 03
14.0	0.0	0.22	0.56	87.8	10.00	2.178	2.360	1.349	0.752	0.350	0.356	1.180	0.182	2.036	87.1	1.067E 03
16.0	0.0	0.21	0.56	87.8	10.00	2.189	2.360	1.349	0.752	0.400	0.356	1.180	0.220	2.036	87.1	1.059E 03
18.0	0.0	0.20	0.30	85.1	10.00	3.010	3.629	1.509	1.061	0.450	0.396	1.706	0.259	3.371	87.1	1.052E 03
20.0	0.0	0.19	0.64	88.6	10.00	3.111	3.711	1.731	1.009	0.500	0.112	1.992	0.299	3.912	87.1	1.052E 03
T IX= 12.0	PO WATTS	IA AMPS	IB AMPS	T ON USEC	FREQ KHZ	IXAVE AMPS	IXAMS AMPS	ICRMS AMPS	TRANS DIODE	LOSSSES WIRE	(WATTS) CORE	***** CAPAC	EFF %	EFF/MASS %		
10.0	0.0	0.23	0.70	39.7	10.00	1.348	2.056	1.063	0.292	0.250	0.334	0.721	0.113	1.410	87.6	1.102E 03
12.0	0.0	0.23	0.18	87.5	10.00	1.618	2.356	1.210	0.383	0.300	0.340	0.941	0.146	1.816	87.6	1.067E 03
14.0	0.0	0.22	0.56	87.5	10.00	1.888	2.688	1.349	0.482	0.350	0.356	1.180	0.182	2.252	87.6	1.059E 03
16.0	0.0	0.21	0.56	89.0	10.00	2.158	2.920	1.383	0.593	0.400	0.369	1.425	0.220	2.269	87.6	1.051E 03
18.0	0.0	0.20	0.30	86.1	10.00	2.827	3.435	1.609	0.703	0.450	0.393	1.706	0.297	3.713	87.6	1.061E 03
20.0	0.0	0.19	0.64	86.1	10.00	2.697	3.435	1.731	0.825	0.500	0.397	1.992	0.299	3.713	87.6	1.061E 03
T IX= 14.0	PO WATTS	IA AMPS	IB AMPS	T ON USEC	FREQ KHZ	IXAVE AMPS	IXAMS AMPS	ICRMS AMPS	TRANS DIODE	LOSSSES WIRE	(WATTS) CORE	***** CAPAC	EFF %	EFF/MASS %		
10.0	0.0	0.23	0.70	23.6	10.00	1.205	1.542	1.063	0.247	0.250	0.231	0.721	0.113	1.362	88.0	1.107E 03
12.0	0.0	0.23	0.18	89.0	10.00	1.645	2.227	1.210	0.328	0.300	0.280	0.941	0.146	1.753	88.0	1.089E 03
14.0	0.0	0.22	0.56	89.0	10.00	1.687	2.500	1.349	0.482	0.350	0.357	1.180	0.182	2.220	88.0	1.074E 03
16.0	0.0	0.21	0.56	89.0	10.00	2.129	2.763	1.482	0.593	0.400	0.369	1.435	0.220	2.615	88.0	1.067E 03
18.0	0.0	0.20	0.35	87.5	10.00	2.129	2.763	1.482	0.696	0.500	0.387	1.992	0.299	3.576	88.0	1.067E 03
T IX= 16.0	PO WATTS	IA AMPS	IB AMPS	T ON USEC	FREQ KHZ	IXAVE AMPS	IXAMS AMPS	ICRMS AMPS	TRANS DIODE	LOSSSES WIRE	(WATTS) CORE	***** CAPAC	EFF %	EFF/MASS %		
10.0	0.0	0.23	0.70	29.1	10.00	1.100	1.956	1.063	0.214	0.250	0.228	0.721	0.113	1.326	88.3	1.110E 03
12.0	0.0	0.23	0.14	31.9	10.00	1.320	2.128	1.210	0.281	0.300	0.237	0.941	0.146	1.706	88.3	1.091E 03
14.0	0.0	0.22	0.56	34.4	10.00	1.550	2.380	1.349	0.353	0.350	0.246	1.180	0.182	2.113	88.3	1.080E 03
16.0	0.0	0.21	0.56	36.8	10.00	1.950	2.680	1.482	0.433	0.400	0.267	1.435	0.220	2.544	88.3	1.074E 03
18.0	0.0	0.20	0.30	39.0	10.00	1.953	2.684	1.609	0.517	0.450	0.268	1.706	0.258	2.999	88.3	1.067E 03
20.0	0.0	0.19	0.64	41.2	10.00	2.200	3.121	1.731	0.605	0.500	0.379	1.992	0.299	3.475	88.3	1.071E 03

REPRODUCIBILITY OF THE
ORIGINAL PAGE IS POOR

EVALUATION FOR DESIGN NO. 3														
SIZE NO.	MAGNETICS			ARNOLD	HU	N	AWG	IND. MH	Wdg FAC	DSH MODE	OP MODE	IB MAX	IIRMS MAX	ICRMS MAX
24	55254			1-254168	125.	38	13	0.247	0.264	1	2	5.776	4.957	1.859
REACTOR AREA SQ.M	PATH LENGTH M	CORE HN. AREA SQ.M	REACTOR LENGTH/TURNS	STACK HEIGHT M	REACTOR HASS KG	REACTOR WIRE LEN. M	REACTOR WIRE RES. OMHS							
1.070E-04	9.840E-02	4.270E-04	5.400E-02	1.540E-02	1.385E-01	2.052E 00	1.373E-02							
V IN= 6.0														
PO WATTS	IA AMPS	IB AMPS	T ON USEC	FREQ KHZ	IXAVE AMPS	IIrms AMPS	ICRMS AMPS	***** TRANS DIODE	LOSSES WIRE CORE	***** CAPAC	***** TOTAL	EPP %	EPP/MASS %/KG	
10.0	1.62	3.31	83.1	10.00	2.467	2.514	0.946	0.525	0.250	0.087	0.121	0.069	1.072	
12.0	2.12	3.80	83.1	10.00	2.960	3.000	1.127	0.748	0.300	0.124	0.121	0.127	1.419	
14.0	2.61	4.30	83.1	10.00	3.453	3.487	1.309	1.011	0.350	0.167	0.121	0.171	1.820	
16.0	3.10	4.79	83.1	10.00	3.947	3.977	1.492	1.310	0.400	0.217	0.121	0.223	2.275	
18.0	3.59	5.28	83.1	10.00	4.440	4.487	1.676	1.658	0.450	0.274	0.121	0.281	2.783	
20.0	4.08	5.78	83.1	10.00	4.933	4.957	1.859	2.042	0.500	0.337	0.121	0.346	3.346	
V IN= 8.0														
PO WATTS	IA AMPS	IB AMPS	T ON USEC	FREQ KHZ	IXAVE AMPS	IIrms AMPS	ICRMS AMPS	***** TRANS DIODE	LOSSES WIRE CORE	***** CAPAC	***** TOTAL	EPP %	EPP/MASS %/KG	
10.0	0.78	2.99	77.8	10.00	1.884	1.986	0.837	0.307	0.250	0.058	0.261	0.070	0.942	
12.0	1.15	3.36	77.8	10.00	2.351	2.346	0.984	0.429	0.300	0.076	0.261	0.087	1.162	
14.0	1.53	3.74	77.8	10.00	2.833	2.709	1.134	0.571	0.350	0.101	0.261	0.128	1.473	
16.0	1.90	4.11	77.8	10.00	3.310	3.445	1.285	0.737	0.400	0.130	0.261	0.163	1.693	
18.0	2.28	4.49	77.8	10.00	3.786	3.816	1.591	1.133	0.500	0.200	0.261	0.205	2.348	
20.0	2.66	4.87	77.8	10.00	3.762	3.816								
V IN= 10.0														
PO WATTS	IA AMPS	IB AMPS	T ON USEC	FREQ KHZ	IXAVE AMPS	IIrms AMPS	ICRMS AMPS	***** TRANS DIODE	LOSSES WIRE CORE	***** CAPAC	***** TOTAL	EPP %	EPP/MASS %/KG	
10.0	0.22	2.89	73.2	10.00	1.556	1.736	0.796	0.221	0.250	0.041	0.451	0.063	1.027	
12.0	0.30	3.20	73.2	10.00	1.867	2.020	0.918	0.252	0.300	0.056	0.451	0.084	1.190	
14.0	0.38	3.51	73.2	10.00	2.178	2.310	1.044	0.391	0.350	0.073	0.451	0.109	1.374	
16.0	0.46	3.82	73.2	10.00	2.489	2.606	1.172	0.497	0.400	0.093	0.451	0.137	1.579	
18.0	0.54	4.12	73.2	10.00	2.800	2.904	1.303	0.618	0.450	0.116	0.451	0.170	1.804	
20.0	0.62	4.45	73.2	10.00	3.111	3.205	1.434	0.752	0.500	0.141	0.451	0.206	2.050	
V IN= 12.0														
PO WATTS	IA AMPS	IB AMPS	T ON USEC	FREQ KHZ	IXAVE AMPS	IIrms AMPS	ICRMS AMPS	***** TRANS DIODE	LOSSES WIRE CORE	***** CAPAC	***** TOTAL	EPP %	EPP/MASS %/KG	
10.0	0.0	2.88	64.6	10.00	1.343	1.510	0.792	0.179	0.250	0.036	0.562	0.063	1.090	
12.0	0.08	3.16	69.1	10.00	1.613	1.847	0.896	0.236	0.300	0.047	0.682	0.080	1.445	
14.0	0.35	3.43	69.1	10.00	1.888	2.087	1.003	0.301	0.350	0.060	0.682	0.101	1.697	
16.0	0.52	3.70	69.1	10.00	2.158	2.354	1.113	0.376	0.400	0.075	0.682	0.124	1.936	
18.0	0.69	3.97	69.1	10.00	2.427	2.595	1.226	0.462	0.450	0.092	0.682	0.150	2.030	
20.0	1.16	4.24	69.1	10.00	2.697	2.840	1.341	0.557	0.500	0.111	0.682	0.180	2.030	
V IN= 14.0														
PO WATTS	IA AMPS	IB AMPS	T ON USEC	FREQ KHZ	IXAVE AMPS	IIrms AMPS	ICRMS AMPS	***** TRANS DIODE2	LOSSSES WIRE CORE	***** CAPAC	***** TOTAL	EPP %	EPP/MASS %/KG	
10.0	0.0	2.88	59.7	10.00	1.205	1.522	0.792	0.152	0.250	0.032	0.562	0.063	1.059	
12.0	0.0	3.16	65.9	10.00	1.546	1.765	0.896	0.239	0.300	0.042	0.682	0.080	1.354	
14.0	0.0	3.41	66.7	10.00	1.567	1.959	0.993	0.251	0.400	0.050	0.946	0.099	1.669	
16.0	0.20	3.65	66.7	10.00	1.928	2.170	1.088	0.308	0.400	0.078	0.946	0.141	1.837	
18.0	0.44	3.89	65.4	10.00	2.159	2.387	1.186	0.373	0.450	0.093	0.946	0.160	1.988	
20.0	0.68	4.13	65.4	10.00	2.410	2.608	1.287	0.445	0.500	0.093	0.946	0.180	2.150	
V IN= 16.0														
PO WATTS	IA AMPS	IB AMPS	T ON USEC	FREQ KHZ	IXAVE AMPS	IIrms AMPS	ICRMS AMPS	***** TRANS DIODE	LOSSSES WIRE CORE	***** CAPAC	***** TOTAL	EPP %	EPP/MASS %/KG	
10.0	0.0	2.88	47.4	10.00	1.100	1.454	0.792	0.131	0.250	0.029	0.562	0.063	1.036	
12.0	0.0	3.16	51.9	10.00	1.320	1.667	0.896	0.173	0.300	0.038	0.733	0.080	1.324	
14.0	0.0	3.61	56.1	10.00	1.580	1.871	0.993	0.219	0.350	0.048	0.917	0.099	1.631	
16.0	0.0	3.65	60.0	10.00	1.760	2.069	1.089	0.266	0.400	0.059	1.114	0.118	1.956	
18.0	0.09	3.87	62.1	10.00	1.993	2.260	1.172	0.373	0.450	0.070	1.235	0.137	2.210	
20.0	0.31	4.09	62.1	10.00	2.200	2.455	1.261	0.375	0.500	0.083	1.235	0.159	2.351	

REPRODUCIBILITY OF THE
ORIGINAL PAGE IS POOR

5.3 SAMPLE PROGRAM #2--PROGRAM DC1DC

Now suppose that to the design requirements given in Section 5.1 the constraint that all designs operate in Mode 1 (continuous conduction mode) over the entire design range is added. This is satisfied simply by making the minimum flux density greater than the residual flux density. Let the minimum flux density be 0.011 tesla and make another run using the DSN1 procedure of Program DC1DC. All other design requirements will remain the same as those used in Sample Program #1.

5.3.1 Control Cards--Sample Program #2 (Program DC1DC)

The control cards for Sample Program #2 are shown below. Sections 3.1-3.6 give instructions for preparing these cards.

FQUD MP DSN1 3 2. 2.
 24. 6. 16. 10. 20. 10. .01 .011 .36 .4 1 2 5.067E-07 HEAVY 1
 1.0 10. .60 .1
 0

5.3.2 Results of Sample Program #2--Program DC1DC

The results of Sample Program #2 are given on the following pages. Program DC1DC has again produced a list of fifty usable designs. However, note from the "OP MODE" column that all of these designs operate in Mode 1 (continuous conduction mode) over the entire operating range. Note also that the program has added a core to the stack in order to produce fifty designs. By comparing the output to that from Sample Program #1, it can be seen that most of the Mode 1 designs produced by Sample Program #1 have also been produced by Sample Program #2. This is due to the fact that the total allowable flux density range is almost, but not quite, the same in both cases.

Note from the evaluation output that the value of IA is greater than zero over the entire design range of the converter. Also, since larger core sizes have been used, the efficiency/mass of the designs evaluated in Sample Program #2 is less than that for the designs evaluated in Sample Program #1.

FQUD—CONSTANT FREQUENCY VOLTAGE STEP-UP/CURRENT STEP-UP CONVERTER DESIGN

CONVERTER SPECIFICATIONS

T _{OUT}	T _{IN}	T _{IN} MAX	P _{OUT}	P _{OUT} MIN	P _{OUT} MAX	SAT	COLL.	DICDE	C1P	CCRV	FREQ	RESIDUAL	B _{MIN}	B _{MAX}	WIND FACTS	RAD COEFS
24.0	6.0	16.0	10.0	20.0	1.00	10.0C	0.60	0.10	10.0	1.000E-02	1.100E-02	3.600E-01	0.40	2		

WIRE TYPE= HELV MIN. STRANDS= 1 RECIPROCAL CURRENT DENSITY= 5.067E-07 SC-B-14

THE FOLLOWING CODES MATCH THE CONSTRAINTS WHEN USED IN A 1-CORE STICK.

SIZE NO.	MAGNETICS	IRONOID	MS	M	IRG	IND. MH	WDG FAC	DSH CODE	OP CODE	IS MAX	IXR55 MAX	ICBNS MAX
27	65109	A-109156	125	60	12	0.569	0.188	1	1	4	638	1
27	65108	A-159185	167	60	12	0.466	0.156	1	1	4	630	1
28	65107	A-430281	125	60	12	0.592	0.313	1	1	4	650	1
28	65106	A-159330	167	38	12	0.496	0.264	1	1	4	677	1
29	65436	A-325360	160	34	12	0.432	0.236	1	1	4	650	1
		A-123066	60	165	12	0.284	0.304	1	1	4	650	1
		A-861642	125	87	12	0.052	0.120	1	1	4	650	1
		A-156167	167	73	12	0.871	0.102	1	1	4	650	1
		A-183197	173	62	12	0.740	0.084	1	1	4	650	1
		A-219233	205	51	12	0.593	0.077	1	1	4	650	1
		A-125112	60	38	12	0.879	0.187	1	1	4	650	1
		A-547222	125	111	12	0.766	0.081	1	1	4	650	1
		A-157276	167	94	12	0.984	0.081	1	1	4	650	1
		A-184316	173	80	12	1.647	0.081	1	1	4	650	1
		A-220222	205	67	12	0.607	0.081	1	1	4	650	1
		A-123124	60	11	12	1.547	0.095	1	1	4	650	1
		A-158222	125	149	12	0.606	0.080	1	1	4	650	1
		A-189242	167	126	12	0.717	0.068	1	1	4	650	1
		A-221242	173	107	12	0.503	0.057	1	1	4	650	1
		A-221245	205	90	12	0.356						

THE FOLLOWING CORES MATCH THE CONSTRAINTS WHEN USED IN A 2-CORE STACK

THE MAXIMUM OF 50 VERIFIABILITY CHECKS HAS BEEN REACHED.

REPRODUCIBILITY OF THE ORIGINAL PAGE IS POOR

DESIGN EVALUATION

MAX. NO. OF EVALUATIONS = 3

EVALUATION PCB DESIGN NO. 1

SIZE NO.	MAGNETICS		ARNOLD		MU	N	AWG	IND. MH	Bdg PAC	DSW MODE	OP NODES	IB MAX	IXBRs MAX	ICRMS MAX
27		55109		A-109156	125.	60	13	0.569	0.188	1	1	5.248	4.938	1.850
	REACTOR AREA SQ.M	PATH LENGTH M	CORE RH AREA SQ.M	REACTOR LENGTH/TURN M	STACK HEIGHT M				REACTOR MASS KG	REACTOR WIRE LENS. M			REACTOR WIRE RES. OMS	
1.440E-04	1.430E-01	9.480E-04		6.230E-02	1.490E-02				2.666E-01	3.738E-01			2.501E-02	
V IN= 6.0	PO WATTS	IA AMPS	IB AMPS	T ON USEC	FREQ KHZ	IXAVE AMPS	IXEMS AMPS	ICRMS AMPS	TRANS DIODE	LOSSSES WIRE	(WATTS) CORE	CAFAC TOTAL	EFP %	EFP/MASS X/KG
10.0	2.10	2.83	83.1	10.00	2.867	2.476	0.928	0.509	0.250	0.153	0.029	0.026	1.028	3.479E-02
12.0	2.32	3.21	83.1	10.00	2.960	2.467	1.122	0.732	0.300	0.220	0.029	0.124	1.405	3.391E-02
14.0	2.53	3.52	83.1	10.00	3.453	2.460	1.257	0.995	0.350	0.299	0.029	0.168	1.842	3.348E-02
16.0	2.74	3.83	83.1	10.00	3.947	2.452	1.481	1.089	0.400	0.391	0.029	0.219	2.238	3.305E-02
18.0	2.95	4.13	83.1	10.00	4.880	2.445	1.684	1.584	0.450	0.494	0.029	0.277	2.893	3.264E-02
20.0	3.16	4.43	83.1	10.00	4.933	2.438	1.850	2.026	0.500	0.610	0.029	0.342	3.508	
V IN= 8.0	PO WATTS	IA AMPS	IB AMPS	T ON USEC	FREQ KHZ	IXAVE AMPS	IXEMS AMPS	ICRMS AMPS	TRANS DIODE	LOSSSES WIRE	(WATTS) CORE	CAFAC TOTAL	EFP %	EFP/MASS X/KG
10.0	1.46	2.36	77.8	10.00	1.881	1.901	0.792	0.281	0.250	0.090	0.061	0.063	0.746	3.715E-02
12.0	1.78	2.74	77.8	10.00	2.257	2.274	0.946	0.403	0.300	0.120	0.061	0.090	0.983	3.668E-02
14.0	2.19	3.11	77.8	10.00	2.633	2.648	1.101	0.546	0.350	0.175	0.061	0.121	1.558	3.619E-02
16.0	2.60	3.49	77.8	10.00	3.010	3.022	1.257	0.711	0.400	0.228	0.061	0.158	1.558	3.565E-02
18.0	2.91	3.86	77.8	10.00	3.388	3.397	1.412	0.898	0.450	0.299	0.061	0.199	1.527	3.446E-02
20.0	3.22	4.24	77.8	10.00	3.762	3.772	1.568	1.108	0.500	0.356	0.061	0.246	2.270	
V IN= 10.0	PO WATTS	IA AMPS	IB AMPS	T ON USEC	FREQ KHZ	IXAVE AMPS	IXEMS AMPS	ICRMS AMPS	TRANS DIODE	LOSSSES WIRE	(WATTS) CORE	CAFAC TOTAL	EFP %	EFP/MASS X/KG
10.0	0.98	2.13	73.2	10.00	1.555	1.591	0.710	0.185	0.250	0.063	0.103	0.050	0.653	3.022E-02
12.0	1.29	2.45	73.2	10.00	1.957	2.006	0.845	0.263	0.350	0.190	0.103	0.071	0.828	
14.0	1.60	2.76	73.2	10.00	2.178	2.203	0.980	0.355	0.350	0.211	0.103	0.096	1.026	
16.0	1.91	3.07	73.2	10.00	2.489	2.511	1.115	0.463	0.400	0.258	0.103	0.124	1.247	
18.0	2.22	3.38	73.2	10.00	2.950	2.920	1.252	0.555	0.450	0.399	0.103	0.157	1.491	3.327E-02
20.0	2.53	3.69	73.2	10.00	3.111	3.129	1.369	0.717	0.500	0.245	0.103	0.193	1.758	
V IN= 12.0	PO WATTS	IA AMPS	IB AMPS	T ON USEC	FREQ KHZ	IXAVE AMPS	IXEMS AMPS	ICRMS AMPS	TRANS DIODE	LOSSSES WIRE	(WATTS) CORE	CAFAC TOTAL	EFP %	EFP/MASS X/KG
10.0	0.68	2.02	69.1	10.00	1.348	1.402	0.659	0.136	0.250	0.049	0.154	0.043	0.623	3.608E-02
12.0	0.99	2.30	69.1	10.00	1.618	1.663	0.778	0.191	0.300	0.069	0.154	0.060	0.775	3.597E-02
14.0	1.30	2.58	69.1	10.00	1.888	1.927	0.898	0.257	0.350	0.093	0.154	0.091	0.938	
16.0	1.60	2.86	69.1	10.00	2.158	2.192	1.020	0.332	0.400	0.120	0.154	0.104	1.110	3.567E-02
18.0	1.89	3.14	69.1	10.00	2.427	2.458	1.152	0.417	0.450	0.151	0.154	0.130	1.303	
20.0	2.03	3.36	69.1	10.00	2.697	2.724	1.264	0.513	0.500	0.186	0.154	0.160	1.513	
V IN= 14.0	PO WATTS	IA AMPS	IB AMPS	T ON USEC	FREQ KHZ	IXAVE AMPS	IXEMS AMPS	ICRMS AMPS	TRANS DIODE	LOSSSES WIRE	(WATTS) CORE	CAFAC TOTAL	EFP %	EFP/MASS X/KG
10.0	0.46	1.95	65.4	10.00	1.205	1.280	0.627	0.107	0.250	0.041	0.212	0.039	0.649	3.603E-02
12.0	0.70	2.19	65.4	10.00	1.646	1.503	0.733	0.149	0.300	0.057	0.212	0.054	0.772	
14.0	0.94	2.43	65.4	10.00	1.687	1.731	0.882	0.198	0.350	0.076	0.212	0.071	0.907	3.594E-02
16.0	1.18	2.68	65.4	10.00	1.928	1.976	1.062	0.250	0.400	0.122	0.212	0.091	1.056	
18.0	1.42	2.92	65.4	10.00	2.169	2.212	1.174	0.392	0.500	0.150	0.212	0.113	1.217	3.587E-02
V IN= 16.0	PO WATTS	IA AMPS	IB AMPS	T ON USEC	FREQ KHZ	IXAVE AMPS	IXEMS AMPS	ICRMS AMPS	TRANS DIODE	LOSSSES WIRE	(WATTS) CORE	CAFAC TOTAL	EFP %	EFP/MASS X/KG
10.0	0.28	1.92	62.1	10.00	1.100	1.197	0.608	0.089	0.250	0.036	0.275	0.037	0.686	3.590E-02
12.0	0.44	2.14	62.1	10.00	1.320	1.402	0.703	0.122	0.300	0.049	0.275	0.049	0.795	
14.0	0.60	2.36	62.1	10.00	1.540	1.611	0.802	0.161	0.350	0.065	0.275	0.064	0.915	3.581E-02
16.0	0.76	2.56	62.1	10.00	1.760	1.822	0.902	0.206	0.400	0.098	0.275	0.081	1.045	
18.0	1.06	2.80	62.1	10.00	2.000	2.036	1.106	0.315	0.500	0.127	0.275	0.122	1.186	3.596E-02
20.0	1.36	3.02	62.1	10.00	2.200	2.250	1.106							

REPRODUCIBILITY OF THE
ORIGINAL PAGE IS POOR

C-2

EVALUATION FOR DESIGN NO. 2											Wdg Fac	DSK Mode	Op Mode	IP Mix	I _{IRMS} Max	ICRMS Max
Size No.	MAGNETICS			ARNOLD	No	N	Awg	I _{HD} Amp	WDG Fac							
27		55108		R-155185	147.	50	13	0.465	0.156	1	1	5.380	4.940	1.851		
	REACTOR REL. SO.H	PATH LENTH M	CORE WH-AREA SQ.R	REACTOR LENGTH/TURN M	STACK HEIGHT M										REACTOR WIRE RES. OHMS	
1.440E-04	1.430E-01	9.480E-04	6.230E-02	1.490E-02	2.465E-01	3.115E 00									2.085E-02	
V I _H = 6.0																
PO WATTS	IA AMPS	IB AMPS	T _{ON} USC	FREQ KHZ	I _{XAVG} AMPS	I _{IRMS} AMPS	ICRMS AMPS	T _{BANS} DIODE	LOSSSES WIRE	(WATTS)	CORE	CAPAC	TOTAL	EPP %	EPE/MASS %	KG
10.0	2.02	2.91	83.1	10.00	2.467	2.480	0.930	0.511	0.250	0.128	0.048	0.087	1.024	90.7	3.679E 02	
12.0	2.05	2.91	83.1	10.00	2.460	2.571	1.118	0.734	0.380	0.144	0.048	0.124	1.390	85.6	3.635E 02	
14.0	2.08	2.91	83.1	10.00	2.463	2.563	1.298	0.997	0.380	0.144	0.048	0.169	1.813	88.0	3.591E 02	
16.0	2.10	2.91	83.1	10.00	2.460	2.563	1.483	1.300	0.400	0.131	0.048	0.220	2.294	82.7	3.540E 02	
18.0	2.12	2.91	83.1	10.00	2.460	2.567	1.667	1.644	0.480	0.132	0.048	0.278	2.832	86.5	3.460E 02	
20.0	2.14	2.91	83.1	10.00	2.463	2.560	1.851	2.028	0.500	0.109	0.048	0.343	3.426	89.4	3.400E 02	
V I _H = 8.0																
PO WATTS	IA AMPS	IB AMPS	T _{ON} USC	FREQ KHZ	I _{XAVG} AMPS	I _{IRMS} AMPS	ICRMS AMPS	TRANS DIODE	LOSSSES WIRE	(WATTS)	CORE	CAPAC	TOTAL	EPP %	EPE/MASS %	KG
10.0	1.30	2.47	77.8	10.00	1.881	1.911	0.797	0.284	0.250	0.076	0.102	0.064	0.776	92.8	3.764E 02	
12.0	1.37	2.84	77.8	10.00	2.257	2.633	0.951	0.406	0.300	0.109	0.102	0.090	1.020	97.7	3.723E 02	
14.0	2.05	3.22	77.8	10.00	3.010	3.386	1.105	0.549	0.350	0.147	0.102	0.122	1.270	99.1	3.692E 02	
16.0	2.42	3.57	77.8	10.00	3.762	3.777	1.260	0.714	0.400	0.191	0.102	0.169	1.566	90.0	3.650E 02	
18.0	2.80	3.87	77.8	10.00	3.765	3.777	1.411	0.901	0.450	0.241	0.102	0.200	1.895	89.9	3.589E 02	
20.0	3.18	4.35	77.8	10.00	3.762	3.777	1.570	1.111	0.500	0.297	0.102	0.287	2.257			
V I _H = 10.0																
PO WATTS	IA AMPS	IB AMPS	T _{ON} USC	FREQ KHZ	I _{XAVG} AMPS	I _{IRMS} AMPS	ICRMS AMPS	TRANS DIODE	LOSSSES WIRE	(WATTS)	CORE	CAPAC	TOTAL	EPP %	EPE/MASS %	KG
10.0	0.85	2.26	73.2	10.00	1.556	1.608	0.721	0.189	0.250	0.054	0.174	0.052	0.719	93.3	3.784E 02	
12.0	1.16	2.58	73.2	10.00	1.867	1.911	0.853	0.267	0.300	0.076	0.174	0.097	0.890	93.1	3.776E 02	
14.0	1.47	2.89	73.2	10.00	2.178	2.216	0.983	0.359	0.350	0.102	0.174	0.124	1.083	92.2	3.752E 02	
16.0	1.78	3.20	73.2	10.00	2.489	2.522	1.123	0.466	0.400	0.133	0.174	0.156	1.298	92.1	3.730E 02	
18.0	2.09	3.51	73.2	10.00	2.800	2.830	1.293	0.586	0.450	0.167	0.174	0.194	1.585	91.0	3.722E 02	
20.0	2.40	3.82	73.2	10.00	2.111	3.138	1.392	0.721	0.500	0.205	0.174	0.274	1.794			
V I _H = 12.0																
PO WATTS	IA AMPS	IB AMPS	T _{ON} USC	FREQ KHZ	I _{XAVG} AMPS	I _{IRMS} AMPS	ICRMS AMPS	TRANS DIODE	LOSSSES WIRE	(WATTS)	CORE	CAPAC	TOTAL	EPP %	EPE/MASS %	KG
10.0	0.53	2.17	69.1	10.00	1.348	1.429	0.676	0.141	0.250	0.043	0.260	0.046	0.739	93.1	3.777E 02	
12.0	0.86	2.44	69.1	10.00	1.678	1.686	0.795	0.196	0.300	0.059	0.260	0.063	0.878	93.0	3.777E 02	
14.0	1.07	2.71	69.1	10.00	1.888	1.946	0.911	0.267	0.350	0.079	0.260	0.083	1.033	92.8	3.755E 02	
16.0	1.34	2.97	69.1	10.00	2.126	2.209	1.031	0.400	0.400	0.102	0.260	0.104	1.206	92.6	3.732E 02	
18.0	1.61	3.21	69.1	10.00	2.467	2.573	1.152	0.523	0.450	0.127	0.260	0.134	1.596	92.4	3.712E 02	
20.0	1.88	3.51	69.1	10.00	2.667	2.738	1.274	0.518	0.500	0.156	0.260	0.162	1.596			
V I _H = 14.0																
PO WATTS	IA AMPS	IB AMPS	T _{ON} USC	FREQ KHZ	I _{XAVG} AMPS	I _{IRMS} AMPS	ICRMS AMPS	TRANS DIODE	LOSSSES WIRE	(WATTS)	CORE	CAPAC	TOTAL	EPP %	EPE/MASS %	KG
10.0	0.29	2.12	65.4	10.00	1.205	1.216	0.652	0.113	0.250	0.036	0.358	0.042	0.799	92.6	3.756E 02	
12.0	0.40	2.36	65.4	10.00	1.486	1.580	0.755	0.155	0.300	0.059	0.358	0.057	1.051	92.5	3.757E 02	
14.0	0.57	2.60	65.4	10.00	1.687	1.699	0.860	0.204	0.350	0.089	0.358	0.074	1.234	92.4	3.743E 02	
16.0	0.72	2.88	65.4	10.00	1.928	1.999	0.968	0.261	0.400	0.108	0.358	0.096	1.496	92.3	3.730E 02	
18.0	0.85	3.08	65.4	10.00	2.160	2.233	1.077	0.326	0.450	0.128	0.358	0.116	1.354	92.2	3.719E 02	
20.0	1.00	3.32	65.4	10.00	2.410	2.567	1.168	0.398	0.500	0.127	0.358	0.141	1.524			
V I _H = 16.0																
PO WATTS	IA AMPS	IB AMPS	T _{ON} USC	FREQ KHZ	I _{XAVG} AMPS	I _{IRMS} AMPS	ICRMS AMPS	TRANS DIODE	LOSSSES WIRE	(WATTS)	CORE	CAPAC	TOTAL	EPP %	EPE/MASS %	KG
10.0	0.10	2.10	62.1	10.00	1.100	1.243	0.641	0.096	0.250	0.032	0.464	0.051	0.883	91.9	3.777E 02	
12.0	0.13	2.32	62.1	10.00	1.320	1.484	0.733	0.129	0.300	0.054	0.464	0.054	0.990	92.4	3.777E 02	
14.0	0.17	2.56	62.1	10.00	1.540	1.681	0.828	0.168	0.350	0.089	0.464	0.068	1.234	92.3	3.767E 02	
16.0	0.20	2.86	62.1	10.00	1.760	1.883	0.925	0.213	0.400	0.108	0.464	0.086	1.372	92.2	3.750E 02	
18.0	0.23	3.08	62.1	10.00	1.980	2.083	1.024	0.264	0.450	0.128	0.464	0.105	1.520	92.1	3.730E 02	
20.0	1.20	3.20	62.1	10.00	2.200	2.275	1.125	0.321	0.500	0.132	0.464	0.127	1.520			

EVALUATION FOR DESIGN NO. 3

SIZE NO.	MAGNETICS			ARNOLD		MU	N	AWG	IND. MH	Wdg FAC	DSN MODE	OP MODE	ID MAX	IXBMS MAX	ICRMS MAX
28	55438	A-438281	125.	45	13	0.592	0.313	1	1	5.245	4.937	1.650			
REACTOR AREA SQ.M	PATH M	CORE WN. AREA SQ.M	REACTOR LENGTH/TURN M	STACK HEIGHT M	SECTOR MASS KG	REACTOR WIRE LENGTH M	REACTOR WIRE RES. OHMS								
1.990E-04	1.070E-01	4.270E-04	6.780E-02	1.890E-02	2.511E-01	3.051E 00	2.042E-02								
V IN= 6.0															
PO WATTS	TA AMPS	TB AMPS	T _{ON} USEC	FREQ KHZ	IXAVE AMPS	IXBMS AMPS	ICRMS AMPS	TRANS DIODE	LOSSES WIRE (WATTS)	CORE CAPAC	TOTAL	EPP %	EPP/MASS %/KG		
10.0	2.12	2.82	83.1	10.00	2.467	2.475	0.928	0.509	0.250	0.125	0.027	0.066	0.998	90.9	
12.0	2.61	3.31	83.1	10.00	2.950	2.967	1.112	0.732	0.300	0.180	0.027	0.124	1.362	89.8	
14.0	3.10	3.80	83.1	10.00	3.453	3.459	1.297	0.995	0.350	0.248	0.027	0.168	1.784	88.7	
16.0	3.60	4.30	83.1	10.00	4.040	4.045	1.481	1.298	0.400	0.319	0.027	0.209	2.264	87.6	
18.0	4.09	4.79	83.1	10.00	4.933	4.937	1.666	1.542	0.450	0.403	0.027	0.277	3.000	86.5	
20.0	4.58	5.28	83.1	10.00			2.026	0.500	0.498	0.027	0.342	3.394		85.5	
V IN= 8.0															
PO WATTS	TA AMPS	TB AMPS	T _{ON} USEC	FREQ KHZ	IXAVE AMPS	IXBMS AMPS	ICRMS AMPS	TRANS DIODE	LOSSES WIRE (WATTS)	CORE CAPAC	TOTAL	EPP %	EPP/MASS %/KG		
10.0	1.42	2.34	77.8	10.00	1.881	1.900	0.791	0.281	0.250	0.074	0.057	0.063	0.724	93.2	
12.0	1.80	2.72	77.8	10.00	2.257	2.273	0.946	0.402	0.300	0.105	0.057	0.089	0.954	92.0	
14.0	2.19	3.09	77.8	10.00	2.633	2.647	1.101	0.505	0.350	0.143	0.057	0.121	1.217	90.2	
16.0	2.57	3.47	77.8	10.00	3.010	3.021	1.256	0.711	0.450	0.186	0.057	0.158	1.512	89.1	
18.0	2.95	3.85	77.8	10.00	3.386	3.396	1.412	0.898	0.500	0.236	0.057	0.199	1.840	88.7	
20.0	3.33	4.22	77.8	10.00	3.762	3.771	1.567	1.107	0.500	0.290	0.057	0.246	2.200	86.1	
V IN= 10.0															
PO WATTS	TA AMPS	TB AMPS	T _{ON} USEC	FREQ KHZ	IXAVE AMPS	IXBMS AMPS	ICRMS AMPS	TRANS DIODE	LOSSSES (WATTS)	CORE CAPAC	TOTAL	EPP %	EPP/MASS %/KG		
10.0	1.00	2.11	73.2	10.00	1.556	1.598	0.709	0.185	0.250	0.052	0.097	0.050	0.633	94.0	
12.0	1.31	2.42	73.2	10.00	2.057	2.094	0.843	0.263	0.300	0.073	0.097	0.071	0.800	94.7	
14.0	1.62	2.73	73.2	10.00	2.578	2.601	0.979	0.355	0.350	0.099	0.097	0.096	0.906	93.4	
16.0	1.93	3.05	73.2	10.00	3.089	3.110	1.115	0.461	0.400	0.129	0.097	0.124	1.211	92.0	
18.0	2.24	3.36	73.2	10.00	3.600	3.818	1.251	0.582	0.450	0.162	0.097	0.167	1.447	91.6	
20.0	2.55	3.57	73.2	10.00	3.111	3.128	1.388	0.716	0.500	0.200	0.097	0.193	1.705	92.1	
V IN= 12.0															
PO WATTS	TA AMPS	TB AMPS	T _{ON} USEC	FREQ KHZ	IXAVE AMPS	IXBMS AMPS	ICRMS AMPS	TRANS DIODE	LOSSSES (WATTS)	CORE CAPAC	TOTAL	EPP %	EPP/MASS %/KG		
10.0	0.71	1.99	69.1	10.00	1.348	1.399	0.656	0.135	0.250	0.040	0.144	0.043	0.613	95.2	
12.0	0.98	2.26	69.1	10.00	1.618	1.660	0.776	0.190	0.300	0.056	0.144	0.060	0.780	94.7	
14.0	1.25	2.53	69.1	10.00	1.888	1.924	0.896	0.256	0.350	0.076	0.144	0.050	0.906	93.9	
16.0	1.53	2.80	69.1	10.00	2.158	2.189	1.018	0.321	0.400	0.098	0.144	0.053	1.021	92.0	
18.0	1.80	3.07	69.1	10.00	2.427	2.455	1.140	0.417	0.400	0.123	0.144	0.130	1.264	91.4	
20.0	2.05	3.34	69.1	10.00	2.697	2.722	1.263	0.512	0.500	0.151	0.144	0.160	1.467	90.2	
V IN= 14.0															
PO WATTS	TA AMPS	TB AMPS	T _{ON} USEC	FREQ KHZ	IXAVE AMPS	IXBMS AMPS	ICRMS AMPS	TRANS DIODE	LOSSSES (WATTS)	CORE CAPAC	TOTAL	EPP %	EPP/MASS %/KG		
10.0	0.49	1.92	65.4	10.00	1.205	1.275	0.623	0.106	0.250	0.033	0.198	0.039	0.626	94.1	
12.0	0.73	2.17	65.4	10.00	1.446	1.509	0.730	0.148	0.300	0.046	0.198	0.046	0.746	93.1	
14.0	0.97	2.41	65.4	10.00	1.687	1.737	0.839	0.198	0.350	0.062	0.198	0.070	0.873	92.1	
16.0	1.21	2.65	65.4	10.00	1.923	1.972	0.949	0.255	0.400	0.079	0.198	0.090	1.022	91.1	
18.0	1.45	2.89	65.4	10.00	2.163	2.239	1.060	0.319	0.450	0.100	0.198	0.112	1.179	90.8	
20.0	1.69	3.13	65.4	10.00	2.410	2.446	1.172	0.391	0.500	0.122	0.198	0.137	1.349	93.7	
V IN= 16.0															
PO WATTS	TA AMPS	TB AMPS	T _{ON} USEC	FREQ KHZ	IXAVE AMPS	IXBMS AMPS	ICRMS AMPS	TRANS DIODE	LOSSSES (WATTS)	CORE CAPAC	TOTAL	EPP %	EPP/MASS %/KG		
10.0	0.31	1.89	62.1	10.00	1.100	1.190	0.603	0.088	0.250	0.029	0.257	0.036	0.660	93.8	
12.0	0.49	2.01	62.1	10.00	1.320	1.396	0.699	0.121	0.300	0.060	0.297	0.049	0.766	94.0	
14.0	0.67	2.11	62.1	10.00	1.540	1.606	0.798	0.160	0.350	0.093	0.297	0.064	0.883	94.1	
16.0	0.85	2.29	62.1	10.00	1.760	1.818	0.898	0.205	0.400	0.067	0.297	0.081	1.010	94.1	
18.0	1.03	2.47	62.1	10.00	1.980	2.032	1.000	0.258	0.450	0.100	0.198	0.122	1.147	94.0	
20.0	1.21	2.99	62.1	10.00	2.200	2.246	1.103	0.314	0.500	0.103	0.257	0.122	1.295	93.9	

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5.4 SAMPLE PROGRAM #3--PROGRAM DC1DC

Note from the results of Sample Program #2 that core size number 24 is the smallest usable size even in a two core stack. To use core size #23 with a relative permeability of 125.0 in a design which will operate in Mode 1 (continuous conduction mode) over the entire design range, Sample Program #3 uses Procedure DSN2 of Program DC1DC to compute a design using core size #23 in a three core stack. Again, the minimum flux density is set equal to 0.011 tesla to insure that only a Mode 1 design will be produced. All other design specifications will remain the same as those used in Sample Program #1. If the program cannot produce a design which meets the constraints using the core size and stack height indicated, a message to this effect will be printed out instead of a design.

5.4.1 Control Cards--Sample Program #3 (Program DC1DC)

The control cards for Sample Program #3 are shown below. Sections 3.1-3.6 give instructions for preparing these cards.

FQUD NP ISDN2 1 2. 2. 1.01 1.011 1.36 .4 1 2 5.067E-07 HEAVY 1
 84. 6. 16. 10. 20. 10. 1.01 1.011 1.36 .4 1 2 5.067E-07 HEAVY 1
 1.0 10. .60 .1
 23 125. 3

11

5.4.2 Results of Sample Program #3--Program DC1DC

The results of Sample Program #3 are given on the following page. Note from the last column under "Converter Specifications" that the number of cores, or stack height, is equal to three. Program DC1DC was able to produce a design using core size #23 in a three core stack. This design operates in Mode 1 (continuous conduction mode) over its entire design range as can be seen from the "OP MODE" column of the print out. Note that the program has taken the integer core size number which was entered as a part of the design specifications and related it to the manufacturers' core numbers form the core catalog. Also, in addition to the design information, an evaluation of the design was produced automatically.

FQUD--CONSTANT FREQUENCY VOLTAGE STEP-UP/CURRENT STEP-UP CONVERTER DESIGN

CONVERTER SPECIFICATIONS

V_{IN} V_{IN} V_{IN} P_{OUT} P_{OUT} V_{MAX} SAT COLL. DIODE CAP CONV FREQ RESIDUAL BIM B MAX WIND FACTOR NO. OUT MIN MAX MAX RIN. MAX SAT ESR FREQ BIM . B MAX CORES

WIRE TYPE= HEAT MIN. STRANDS= 1 RECIPROCAL CURRENT FENSITY= 5.067E-07 SQ-IN/ARE

DESIGN EVALUATION

EVALUATION ZCB DESIGN NO. 1

SIZE NO. **MAGNETICS** **ARNOLD** **HU** **N** **ANG** **IND. MM** **WDG FAC** **DSH MODE** **GP MODE** **IE MIX** **ITEMS MAX** **ICBMS MAX**

REACTOR AREA	PATH LENGTH	CORE AREA	REACTOR LENGTH/TURN	STACK HEIGHT	REACTOR MASS KG	REACTOR WIRE LENGTH	REACTOR WIRE RES. OHMS
SQ.M	M	SQ.M	M	M	KG	M	OMS
2.038E-04	8.880E-02	3.684E-04	8.860E-02	3.390E-02	2.302E-01	3.278E-00	2.194E-02

T IN= 6.0		FREQUENCY										CAPACITIVE				EPP		EFF/MASS	
PO WATTS	TA AMPS	TB AMPS	T USEC	FREQ KHZ	IXATE AMPS	IXBMS AMPS	ICRMS AMPS	TRANS	DIODE	LOSSES WIRE	(WATTS) CORE	CAPAC TOTAL	X	%	KG				
10.0	2.0	2.89	83.7	10.00	2.467	2.479	0.930	0.511	0.250	0.135	0.038	0.066	1.020	60.7	3.942	02			
12.0	2.0	3.39	83.7	10.00	2.467	2.479	0.733	0.733	0.300	0.194	0.038	0.124	1.388	3.895	02	3.395			
14.0	2.0	3.89	83.7	10.00	2.467	2.479	0.562	1.294	0.995	0.350	0.038	0.168	1.815	3.849	02	3.349			
16.0	2.0	4.39	83.7	10.00	2.467	2.479	0.494	1.667	1.300	0.400	0.038	0.220	2.300	3.795	02	3.379			
18.0	2.0	4.87	83.7	10.00	2.467	2.479	0.427	1.667	1.643	0.450	0.038	0.278	2.843	3.755	02	3.355			
20.0	2.0	5.36	83.7	10.00	2.467	2.479	0.360	1.667	2.028	0.500	0.038	0.343	3.443	3.708	02	3.308			

V IN=	E.O	EQUIPMENT												SPP	EPP/MASS
PO	IA	IB	T ON	FREQ	I _{MAX}	I _{MAX}	ICRMS	*****	LOSSSES	(WATTS)	*****	CAPAC	TOTAL	%	EPP/MASS
WATTS	AMPS	AMPS	USC	KHZ	AMPS	AMPS	AMPS	TRANS	DIODE	WIRE	CORE				%/KG
10.0	1.32	2.44	77.8	10.00	1.881	1.598	0.796	0.284	0.250	0.380	0.079	0.063	0.756	93.0	4.0388 02
12.0	1.76	2.82	77.8	10.00	2.280	2.050	0.850	0.405	0.300	0.114	0.079	0.090	0.988	92.4	3.1320 002
15.0	2.07	3.23	77.8	10.00	2.653	2.453	1.104	0.588	0.350	0.154	0.079	0.122	1.254	91.2	3.9876 002
18.0	2.39	3.63	77.8	10.00	3.010	2.727	1.295	0.713	0.460	0.201	0.079	0.159	1.552	90.2	3.9328 002
20.0	2.67	3.91	77.8	10.00	3.386	3.011	1.414	0.900	0.550	0.254	0.079	0.200	1.884	89.5	3.8525 002
22.0	2.95	4.19	77.8	10.00	3.762	3.276	1.510	1.110	0.500	0.313	0.079	0.245	2.248	88.9	3.8052 002

V IN= 10.0																	
WATTS	AMPS	AMPS	AMPS	USEC	KHZ	AMPS	AMPS	AMPS	TRANS	DIODES	WIRE	(WATTS)	CORE	CAPAC	TOTAL	EFF	EFF/MASS %/KG
10.0	0.000	2.23	73.2	10.00	1.556	1.604	0.718	0.188	0.250	0.056	0.135	0.052	0.681	93.6	0.066	0.2	
12.0	0.000	2.23	73.2	10.00	1.557	1.607	0.719	0.266	0.300	0.080	0.135	0.072	0.854	93.4	0.051	0.2	
14.0	0.000	2.23	73.2	10.00	1.558	1.607	0.719	0.266	0.300	0.080	0.135	0.072	0.854	93.4	0.051	0.2	
16.0	0.000	2.23	73.2	10.00	1.559	1.608	0.720	0.267	0.300	0.081	0.135	0.073	0.854	93.4	0.051	0.2	
18.0	0.000	2.23	73.2	10.00	1.560	1.609	0.721	0.267	0.300	0.081	0.135	0.073	0.854	93.4	0.051	0.2	

V IN= 14.0														
PO WATTS	IA AMPS	IB AMPS	T OH USEC	FREQ KHZ	IXAVZ AMPS	IISMS AMPS	ICRMS AMPS	TRANS DIODE	LOSSES WIRE	(WATTS) CORE	***** CAPAC	***** TOTAL	EPP I	EPP/MASS KG
10.0	0.33	2.08	65.4	10.00	1.205	1.306	0.645	0.112	0.250	0.237	0.278	0.042	0.719	93.0
12.0	0.57	2.32	65.4	10.00	1.446	1.531	0.845	0.150	0.300	0.251	0.278	0.056	0.839	94.0
14.0	0.81	2.56	65.4	10.00	1.687	1.761	0.855	0.203	0.350	0.268	0.278	0.066	0.958	95.0
16.0	1.06	2.80	65.4	10.00	2.192	2.493	0.944	0.260	0.400	0.287	0.288	0.076	1.178	96.0
18.0	1.30	3.04	65.4	10.00	2.169	2.227	1.073	0.324	0.450	0.309	0.288	0.086	1.277	97.0

Y IN = 16.0												EFF/MASS %/KG			
PO WATTS	IA AMP	IB AMP	T ON SEC	FREQ KHZ	IXAVE AMP	IXBMS AMP	ICRMS AMP	TRANS	DIODE	LOSSZS WATT	(WATTS) CORE	CAPAC	TOTAL	EFF %	EFF/MASS %/KG
10.0	0.15	2.06	62.1	10.00	1.100	1.231	0.633	0.094	0.250	0.033	0.361	0.040	0.778	92.8	4.030E-02
12.0	0.16	2.28	62.1	10.00	1.120	1.431	0.725	0.127	0.302	0.045	0.361	0.053	0.885	93.1	4.045E-02
14.0	0.18	2.50	62.1	10.00	1.140	1.636	0.821	0.166	0.350	0.059	0.361	0.067	1.003	93.3	4.055E-02
16.0	0.20	2.72	62.1	10.00	1.160	1.832	0.919	0.211	0.406	0.075	0.361	0.084	1.132	93.6	4.055E-02
18.0	0.22	2.94	62.1	10.00	1.180	2.036	1.019	0.262	0.460	0.093	0.361	0.104	1.270	93.9	4.057E-02

5.5 SAMPLE PROGRAM #4---PROGRAM DC1DC

Now assume that by some criteria it is decided that the design produced in Sample Program #3 is close to the desired result for a single-winding design. However, there is available from a different manufacturer a core with slightly different dimensions from core size #23. Also, this core has a relative permeability value of 128. Sample Program #4 uses Procedure DSN2 of Program DC1DC to produce a design for this new core size and relative permeability using a three core stack to see if any changes in number of turns or wire size must be made due to the change in core. Also, since AWG #13 wire is fairly stiff, it is decided to use two strands of smaller wire to make winding easier. Assume that the dimensions of the new core size are as follows:

Cross-Sectional Area	$7.00 * 10^{-5}$ m ²
Mean Magnetic Path Length	$9.00 * 10^{-2}$ m
Window Area	$3.704 * 10^{-4}$ m ²
Length/Turn of Wire (40% Wdg. Factor)	$4.50 * 10^{-2}$ m
Height	$1.15 * 10^{-2}$ m
Mass	$5.50 * 10^{-2}$ kg

The relative permeability value of 128.0 is close to the catalog value of 125.0. Thus, if no loss-coefficient information is entered, the program will use the loss coefficients for the catalog value of 125.0.

5.5.1 Control Cards--Sample Program #4 (Program DC1DC)

The control cards for Sample Program #4 are shown below. Sections 3.1-3.6 give instructions for preparing these cards.

FQUD NP DSM2 1 2. 2.
 84. 6. 16. 10. 20. 10. .01 .011 .36 .4 1 2 5.067E-07 HEAVY 2
 1.0 10. .60 .1
 3
 7.00E-5 9.00E-2 3.704E-4 4.50E-2 1.15E-2 5.50E-2
 123.
 0

5.5.2 Results of Sample Program #4--Program DC1DC

The results of Sample Program #4 are given on the next page. Note that the change in core dimensions and permeability did not change the number of turns for the design. However, by using two strands of wire, the wire size has been reduced to AWG #16. By comparing the results to those of Sample Program #3, slight differences can be noted in the evaluation portion of the print out. For example, the efficiency/mass is slightly less in Sample Program #4. However, basically the same design and performance is found in both cases except for the number of strands of wire.

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PQUD—CONSTANT FREQ VOLTAGE STEP-UP/CURRENT STEP-UP CONVERTER DESIGN
I/O IN VOLTS, AMPERES, WATTS, TESLAS, MICROSEC, KHZ, OHMS

CONVERTER SPECIFICATIONS

T OUT	V IN MIN	V IN MAX	P OUT MIN	P OUT MAX	I SAT	C CELL.	I DIODE	C CAP ESR	G COV FREQ	R RESIDUAL	S MIN	S MAX	B FACTOR	WIND COSES
24.0	6.0	16.0	10.0	20.0	1.00	10.00	0.60	0.10	10.0	1.00E-02	1.100E-02	3.600E-01	0.40	3

WIRE TYPE= HEAVY MIN. STRANDS= 2 RECIPROCAL CURRENT DENSITY= 5.067E-07 SQ. M/AMP

DESIGN EVALUATION

EVALUATION FOR DESIGN NO. 0

CORRECT WIRE SIZE NOT AVAILABLE OR MULTIPLE STRANDS SPECIFIED, 2 STRANDS USED

SIZE NO.	CORE NOT IN CATALOG				MU	N	AWG	IND. MH	WDG PAC	DSH MODE	OP MODE	IB MAX	IYMAX	ICRMS MAX
	REACTOR AREA SC.M	PATH LENGTH M	CORE WH. AREA SQ.M	REACTOR LENGTH/TURN M										
33				128.	37	16	0.514	0.304	1	1	5.338	4.939	1.851	
2.100E-04	9.000E-02	3.704E-04	9.100E-02	3.450E-02										
V IN= 6.0														
PO WATTS	IA AMPS	IB AMPS	T ON USEC	FREQ KHZ	IXAVE AMPS	IXEMS AMPS	ICRMS AMPS	TRANS DIODE	LOSSSES WIRE CORE	CAPAC	TOTAL	EPP %	EPP/HASS %/KG	
10.0	2.06	2.87	83.1	10.00	2.467	2.478	0.929	0.510	0.250	0.139	0.036	0.086	1.021	90.7
12.0	2.55	3.36	83.1	10.00	2.960	2.559	1.113	0.733	0.300	0.200	0.036	0.124	1.392	90.2
14.0	3.04	3.86	83.1	10.00	3.453	3.661	1.297	0.996	0.350	0.271	0.036	0.168	1.821	90.2
16.0	3.53	4.35	83.1	10.00	3.947	3.654	1.482	1.299	0.400	0.354	0.036	0.220	2.308	90.7
18.0	4.02	4.84	83.1	10.00	4.440	4.539	1.666	1.643	0.450	0.448	0.036	0.278	2.854	90.2
20.0	4.52	5.34	83.1	10.00	4.933	4.539	1.851	2.027	0.500	0.552	0.036	0.343	3.458	90.2
V IN= 8.0														
PO WATTS	IA AMPS	IB AMPS	T ON USEC	FREQ KHZ	IXAVE AMPS	IXEMS AMPS	ICRMS AMPS	TRANS DIODE	LOSSSES WIRE CORE	CAPAC	TOTAL	EPP %	EPP/HASS %/KG	
10.0	1.35	2.41	77.8	10.00	1.881	1.906	0.794	0.283	0.250	0.082	0.075	0.063	0.753	93.0
12.0	1.73	2.79	77.8	10.00	2.257	2.278	0.948	0.504	0.300	0.117	0.075	0.090	0.987	93.0
14.0	2.10	3.16	77.8	10.00	2.633	2.651	1.104	0.547	0.350	0.159	0.075	0.122	1.253	93.0
16.0	2.48	3.54	77.8	10.00	3.010	3.029	1.298	0.712	0.400	0.267	0.075	0.158	1.706	93.0
18.0	2.86	3.92	77.8	10.00	3.385	3.390	1.470	0.900	0.450	0.326	0.075	0.200	2.096	93.0
20.0	3.23	4.29	77.8	10.00	3.762	3.774	1.569	1.109	0.500	0.323	0.075	0.246	2.453	93.0
V IN= 10.0														
PO WATTS	IA AMPS	IB AMPS	T ON USEC	FREQ KHZ	IXAVE AMPS	IXEMS AMPS	ICRMS AMPS	TRANS DIODE	LOSSSES WIRE CORE	CAPAC	TOTAL	EPP %	EPP/HASS %/KG	
10.0	0.91	2.20	73.2	10.00	1.556	1.599	0.715	0.187	0.250	0.058	0.128	0.051	0.674	93.7
12.0	1.23	2.51	73.2	10.00	1.867	1.903	0.849	0.265	0.300	0.082	0.128	0.072	0.847	93.4
14.0	1.54	2.82	73.2	10.00	2.178	2.209	0.983	0.357	0.350	0.111	0.128	0.097	1.042	93.7
16.0	1.86	3.13	73.2	10.00	2.429	2.416	1.192	0.464	0.400	0.143	0.128	0.125	1.260	92.7
18.0	2.16	3.43	73.2	10.00	2.800	2.824	1.391	0.584	0.450	0.181	0.128	0.157	1.500	92.3
20.0	2.47	3.75	73.2	10.00	3.111	3.133	1.591	0.719	0.500	0.222	0.128	0.193	1.762	91.9
V IN= 12.0														
PO WATTS	IA AMPS	IB AMPS	T ON USEC	FREQ KHZ	IXAVE AMPS	IXEMS AMPS	ICRMS AMPS	TRANS DIODE	LOSSSES WIRE CORE	CAPAC	TOTAL	EPP %	EPP/HASS %/KG	
10.0	0.61	2.09	69.1	10.00	1.348	1.514	0.667	0.138	0.250	0.045	0.191	0.044	0.569	93.7
12.0	0.88	2.36	69.1	10.00	1.618	1.574	0.786	0.195	0.300	0.063	0.191	0.062	0.810	93.7
14.0	1.15	2.63	69.1	10.00	1.882	1.936	0.904	0.259	0.350	0.085	0.191	0.082	0.967	93.5
16.0	1.42	2.90	69.1	10.00	2.158	2.198	1.025	0.334	0.400	0.110	0.191	0.105	1.140	93.3
18.0	1.69	3.17	69.1	10.00	2.427	2.469	1.146	0.420	0.450	0.139	0.191	0.131	1.333	93.0
20.0	1.96	3.44	69.1	10.00	2.697	2.731	1.269	0.515	0.500	0.169	0.191	0.161	1.536	92.9
V IN= 14.0														
PO WATTS	IA AMPS	IB AMPS	T ON USEC	FREQ KHZ	IXAVE AMPS	IXEMS AMPS	ICRMS AMPS	TRANS DIODE	LOSSSES WIRE CORE	CAPAC	TOTAL	EPP %	EPP/HASS %/KG	
10.0	0.38	2.03	65.4	10.00	1.205	1.296	0.638	0.110	0.250	0.038	0.263	0.041	0.702	93.4
12.0	0.65	2.27	65.4	10.00	1.446	1.523	0.743	0.152	0.300	0.053	0.263	0.055	0.822	93.6
14.0	0.86	2.56	65.4	10.00	1.617	1.754	0.850	0.201	0.350	0.070	0.263	0.072	0.956	93.6
16.0	1.10	2.76	65.4	10.00	1.922	1.987	0.959	0.258	0.400	0.089	0.263	0.092	1.102	93.6
18.0	1.34	3.00	65.4	10.00	2.169	2.221	1.069	0.323	0.450	0.112	0.263	0.119	1.262	93.6
20.0	1.58	3.24	65.4	10.00	2.410	2.457	1.180	0.395	0.500	0.137	0.263	0.139	1.434	93.3
V IN= 16.0														
PO WATTS	IA AMPS	IB AMPS	T ON USEC	FREQ KHZ	IXAVE AMPS	IXEMS AMPS	ICRMS AMPS	TRANS DIODE	LOSSSES WIRE CORE	CAPAC	TOTAL	EPP %	EPP/HASS %/KG	
10.0	0.19	2.01	62.1	10.00	1.100	1.218	0.623	0.092	0.250	0.034	0.341	0.039	0.756	93.0
12.0	0.41	2.23	62.1	10.00	1.329	1.250	0.717	0.125	0.300	0.064	0.341	0.051	0.863	93.3
14.0	0.63	2.45	62.1	10.00	1.549	1.414	0.814	0.164	0.300	0.076	0.341	0.066	0.981	93.3
16.0	0.85	2.67	62.1	10.00	1.760	1.746	0.913	0.202	0.400	0.076	0.341	0.081	1.110	93.2
18.0	1.07	2.89	62.1	10.00	1.970	2.021	1.017	0.261	0.450	0.095	0.341	0.103	1.249	93.2
20.0	1.29	3.11	62.1	10.00	2.200	2.261	1.115	0.318	0.500	0.116	0.341	0.124	1.399	93.0

5.6 SAMPLE PROGRAM #5 -- PROGRAM DC1DC

Sample Program #5 evaluates the reactor element design produced in Sample Program #4 under a different set of operating conditions. A reactor element design for a single-winding voltage step-up/current step-up converter has been produced. From the design specifications it can be seen that this converter has been designed for voltage step-up operation since the specified output voltage of 24.0 volts is greater than the maximum input voltage of 16.0 volts. To determine how the design will perform when the controller is changed to regulate the output at 5.0 volts, Procedure EVAL of Program DC1DC is used. On the Design Specification Card, the output voltage is set equal to 5.0 volts. All of the other parameters will remain the same and the completed design will be entered on the EVAL card. Note that since we are requesting an evaluation rather than a design, the minimum and maximum flux density specifications, the maximum winding factor, and the reciprocal current density specification are not needed. Thus, it is not necessary to enter these parameters on the Design Specification Card when using Procedure EVAL.

5.61 Control Cards--Sample Program #5 (Program DC1DC)

The Control Cards for Sample Program #5 are given below. Sections 3.1-3.6 give instructions for preparing these cards.

FQUD NP EVAL 1 2. 2.
 5. 6. 16. 10. 20. 10. .01
 1.0 10. .60 .1
 3 32 16
 7.00E-5 9.00E-2 3.704E-4 4.50E-2 1.15E-2 5.50E-6
 128.
 0

5.6.2 Results of Sample Program #5 -- Program DC1DC

The results of Sample Program #5 are given on the next page. Note that the converter operates in Mode 1 (continuous conduction mode) over its entire operating range. However, the peak value of the reactor current, I_B , is about 60% higher than in Sample Program #4. The same is true for the values of all the currents given in the evaluation. Thus, if the converter is used under these operating conditions as well as under those of the original problem, it will be necessary to use a larger wire size if the reciprocal current density specification of $5.067 * 10^{-7} \text{ m}^2/\text{A}$ is to be met. Also, the maximum operating flux density, given by

$$B_{\max} = (N/l) \mu_0 I B_{\max}$$

where

N = Number of Turns

ℓ = Mean Magnetic Path Length

μ = Permeability

$I_{B_{max}}$ = Peak Value of Reactor Current

should be checked to determine whether or not this value exceeds the saturation flux density of the magnetic material. For this case, the

maximum operating flux density would be approximately 0.578 tesla.

Note also that the increase in current values has led to increased losses in the transistor, diode, wire and capacitor. The core loss has decreased due to the fact that the total flux density excursion given by

$$(N/l)(IB - IA)\mu$$

has decreased by about 40%. Since total core loss as given by Legg's equation (see Section 1.2.3) is directly to the flux density excursion, the core loss varies directly with this excursion. The increase in total power loss over that of Sample Program #4 can also be noted in the decreased efficiency in Sample Program #5. Thus, this single-winding reactor design will work for an output voltage of 5.0 volts, but not as well as for the design output voltage of 24.0 volts.

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**FQUD--CONSTANT FREQ VOLTAGE STEP-UP/CURRENT STEP-DOWN CONVERTER DESIGN
I/O IN VOLTS, AMPERES, WATTS, TESLAS, MICROSEC, MHZ, OHMS**

CONVERTER SPECIFICATIONS

V OUT	V IN	V OUT	P OUT	V MIN	P OUT	V MAX	I SAT	COLL.	V DIODE	CAP ESR	CCNV FREQ	P RESIDUAL	B MHD	B MAX	WIND FACTOR	NO. CORES
5.0	6.0	16.0	10.0	20.0	1.00	10.00	0.60	0.10	10.0	1.00E-02						3

WIRE TYPE= HEAVY NO. STRANDS= 2

DESIGN EVALUATION

EVALUATION FOR DESIGN ENTERED

CORRECT WIRE SIZE NOT AVAILABLE OR MULTIPLE STRANDS SPECIFIED, 2 STRANDS USED

SIZE NO.	CORE NOT IN CATALOG				H.U.	N	AWG	IND. MH	Wdg Pac	DSN MODE	OP MODE	IB MAX	IXAMS MAX	ICRMS MAX	
	REACTOR AREA SQ.M	PATH LENGTH M	CORE W.H. AREA SQ.M	REACTOR LENGTH/TURN											
2.100E-04	9.000E-02	3.704E-04	9.100E-02	3.450E-02	2.409E-01	3.367E-00									2.264E-02
V IN= 6.0															
PO WATTS	IA AMPS	IB AMPS	T ON USEC	FREQ KHZ	IXAVE AMPS	IXAMS AMPS	ICRMS AMPS	TRANS DIODE	LOSSSES WIRE	(WATTS) CORE	CAFAC TOTAL	EPP %	EPP/MASS %/KG		
10.0	3.96	4.50	52.8	10.00	4.240	4.243	2.119	0.951	1.200	0.408	0.011	0.449	3.018	16.6	3.189E-02
12.0	4.02	4.55	52.8	10.00	4.089	4.090	2.084	1.369	1.440	0.587	0.011	0.648	3.052	17.1	3.103E-02
14.0	4.07	4.59	52.8	10.00	4.089	4.090	2.084	1.863	1.680	0.798	0.011	0.879	3.231	22.0	3.224E-02
16.0	4.12	4.64	52.8	10.00	4.784	4.786	3.388	2.433	1.920	1.043	0.011	1.148	3.321	26.6	3.458E-02
18.0	4.17	4.79	52.8	10.00	7.532	7.533	3.811	3.078	2.160	1.319	0.011	1.453	3.321	69.2	3.718E-02
20.0	4.22	4.74	52.8	10.00	8.480	8.481	4.234	3.800	2.400	1.629	0.011	1.793	9.633	67.5	3.102E-02
V IN= 8.0															
PO WATTS	IA AMPS	IB AMPS	T ON USEC	FREQ KHZ	IXAVE AMPS	IXAMS AMPS	ICRMS AMPS	TRANS DIODE	LOSSSES WIRE	(WATTS) CORE	CAFAC TOTAL	EPP %	EPP/MASS %/KG		
10.0	3.30	3.90	44.4	10.00	3.600	3.604	1.794	0.577	1.200	0.294	0.016	0.322	2.410	5.6	3.345E-02
12.0	4.02	4.62	44.4	10.00	4.320	4.324	2.151	0.831	1.440	0.423	0.016	0.462	3.173	7.1	3.287E-02
14.0	4.74	5.38	44.4	10.00	5.050	5.053	2.508	1.130	1.680	0.576	0.016	0.629	4.031	7.6	3.239E-02
16.0	5.46	6.16	44.4	10.00	5.760	5.763	2.865	1.476	1.920	0.752	0.016	0.821	4.985	76.6	3.165E-02
18.0	6.18	6.94	44.4	10.00	6.480	6.482	3.223	1.868	2.160	1.038	0.016	1.038	6.034	3.009E-02	
20.0	6.90	7.50	44.4	10.00	7.200	7.202	3.580	2.305	2.400	1.175	0.016	1.282	7.178	73.6	3.055E-02
V IN= 10.0															
PO WATTS	IA AMPS	IB AMPS	T ON USEC	FREQ KHZ	IXAVE AMPS	IXAMS AMPS	ICRMS AMPS	TRANS DIODE	LOSSSES WIRE	(WATTS) CORE	CAFAC TOTAL	EPP %	EPP/MASS %/KG		
10.0	2.91	3.58	38.4	10.00	3.244	3.250	1.585	0.405	1.200	0.239	0.022	0.251	2.117	6.5	3.126E-02
12.0	3.26	4.03	38.4	10.00	4.093	4.099	2.398	0.583	1.440	0.344	0.022	0.361	2.749	6.0	3.081E-02
14.0	4.21	4.86	38.4	10.00	4.542	4.546	2.414	0.793	1.680	0.468	0.022	0.490	3.451	6.2	3.308E-02
16.0	4.96	5.53	38.4	10.00	5.191	5.195	2.549	1.035	1.920	0.611	0.022	0.639	4.227	7.9	3.280E-02
18.0	5.50	6.18	38.4	10.00	5.893	5.893	2.849	1.310	2.160	0.773	0.022	0.809	5.073	78.0	3.289E-02
20.0	6.15	6.82	38.4	10.00	6.489	6.492	3.159	1.616	2.400	0.954	0.022	0.998	5.990	77.0	3.194E-02
V IN= 12.0															
PO WATTS	IA AMPS	IB AMPS	T ON USEC	FREQ KHZ	IXAVE AMPS	IXAMS AMPS	ICRMS AMPS	TRANS DIODE	LOSSSES WIRE	(WATTS) CORE	CAFAC TOTAL	EPP %	EPP/MASS %/KG		
10.0	2.66	3.38	33.7	10.00	3.018	3.025	1.437	0.309	1.200	0.207	0.026	0.207	1.949	83.7	3.474E-02
12.0	3.26	3.98	33.7	10.00	4.622	4.628	1.721	0.444	1.440	0.298	0.026	0.295	2.504	82.7	3.434E-02
14.0	4.86	5.59	33.7	10.00	6.225	6.231	2.005	0.604	1.680	0.405	0.026	0.402	3.177	81.8	3.295E-02
16.0	5.47	6.19	33.7	10.00	6.829	6.834	2.290	0.788	1.920	0.529	0.026	0.524	3.768	80.0	3.256E-02
18.0	6.07	6.79	33.7	10.00	7.433	7.437	2.574	0.997	2.160	0.669	0.026	0.653	4.555	80.0	3.119E-02
20.0	6.68	7.40	33.7	10.00	8.036	8.040	2.859	1.231	2.400	0.826	0.026	0.817	5.300	79.1	3.081E-02
V IN= 14.0															
PO WATTS	IA AMPS	IB AMPS	T ON USEC	FREQ KHZ	IXAVE AMPS	IXAMS AMPS	ICRMS AMPS	TRANS DIODE	LOSSSES WIRE	(WATTS) CORE	CAFAC TOTAL	EPP %	EPP/MASS %/KG		
10.0	2.48	3.24	30.1	10.00	2.862	2.867	1.325	0.248	1.200	0.187	0.030	0.176	1.840	84.5	3.506E-02
12.0	3.05	3.91	30.1	10.00	3.474	3.481	1.686	0.356	1.440	0.268	0.030	0.262	2.346	83.6	3.426E-02
14.0	4.08	4.93	30.1	10.00	4.006	4.012	1.847	0.483	1.680	0.365	0.030	0.344	2.901	82.0	3.405E-02
16.0	4.77	5.53	30.1	10.00	5.151	5.155	2.170	0.800	2.160	0.602	0.030	0.562	4.154	81.2	3.373E-02
20.0	5.34	6.10	30.1	10.00	5.723	5.727	2.632	0.988	2.400	0.743	0.030	0.693	4.853	80.5	3.340E-02
V IN= 16.0															
PO WATTS	IA AMPS	IB AMPS	T ON USEC	FREQ KHZ	IXAVE AMPS	IXAMS AMPS	ICRMS AMPS	TRANS DIODE	LOSSSES WIRE	(WATTS) CORE	CAFAC TOTAL	EPP %	EPP/MASS %/KG		
10.0	2.35	3.14	27.2	10.00	2.747	2.756	1.238	0.207	1.200	0.172	0.034	0.153	1.766	84.0	3.528E-02
12.0	2.90	3.69	27.2	10.00	3.295	3.304	1.574	0.297	1.440	0.247	0.034	0.219	2.237	85.3	3.449E-02
14.0	3.47	4.24	27.2	10.00	3.845	3.852	1.722	0.403	1.680	0.336	0.034	0.297	2.750	83.6	3.470E-02
16.0	4.00	4.79	27.2	10.00	4.192	4.197	1.965	0.526	1.920	0.432	0.034	0.346	3.105	82.9	3.407E-02
18.0	4.55	5.34	27.2	10.00	4.944	4.949	2.208	0.666	2.160	0.555	0.034	0.408	3.902	82.2	3.412E-02
20.0	5.10	5.89	27.2	10.00	5.493	5.498	2.452	0.822	2.400	0.685	0.034	0.601	4.641	81.5	3.383E-02

5.7 SAMPLE PROGRAM #6 -- PROGRAM DC2DC

As mentioned in Section 3.6.4, Program DC2DC allows the user to select from ten Design Constraint Options which may be useful in a converter design. Sample Program #6 illustrates the use of one of these options in the design of a two-winding voltage step-up/current step-up converter with a constant frequency controller to meet the specifications given in Sections 5.1 and 5.2. For convenience, these specifications are repeated in Section 5.7.1.

Note from the output of Sample Program #4 (Section 5.5.2) that the single-winding reactor design produced by Program DC1DC requires a maximum transistor on-time (T_{ON}) of 83.1 μ sec. Since the converter frequency is 10.0 KHz, the maximum duty cycle is, therefore, 0.83. Suppose that the controller circuit which must be used in the system will produce an output with a maximum duty cycle of 0.75. With this limitation on the controller, the single-winding design produced in Sample Program #4 could not meet the design constraints. However, if Program DC2DC is used to produce a two-winding reactor design, the additional constraint that the maximum duty cycle be less than 0.75 can easily be handled. If a value of 0.74 is chosen for the Design Constraint Value, the maximum duty cycle for the designs produced by Program DC2DC will always be strictly less than 0.75. Since the program is allowed to choose only an integer number of turns, the Design Constraint value should be chosen to be slightly less than the desired maximum of 0.75. Sample Program #6 uses a value of 0.74 for the Design Constraint option.

5.7.1 Design Requirement Input Data--Sample Program #6 (DC2DC)

As in Sample Program #2, it is desired that the converter operate in Mode 1 (continuous mmf mode) over the entire design range. This is accomplished by making the specified minimum flux density greater than the residual flux density of the core material. The following is a complete summary of the input data to Program DC2DC for Sample Program #6.

Converter/Controller Code	FQ2UD
Catalog Print Code	NP
Program Procedure	DSN1
Output Voltage	24.0 volts
Input Voltage Range	6.0 to 16.0 volts
Output Power Range	10.0 to 20.0 watts
Converter Frequency	10.0 KHz
Residual Flux Density	0.01 tesla
Minimum Flux Density	0.011 tesla
Maximum Flux Density	0.36 tesla
Wire Type Code	HEAV
Reciprocal Current Density	$5.067 * 10^{-7} \text{ m}^2/\text{amp}$
Minimum No. of Cores in Stack	1
Maximum No. of Cores in Stack	2
Min. Strands of Wire--Primary	1
Min. Strands of Wire--Secondary	1
Transistor Saturation Voltage	1.0 volt @ 10.0 amps
Diode Forward Drop	0.60 volts
Capacitor ESR	0.10 ohm

Maximum No. of Evaluations	3
Input Voltage Increment	2.0 volts
Output Power Increment	2.0 watts
Design Constraint Option	8 (Restrict Max. Duty Cycle)
Design Constraint Value	0.74

5.7.2 Control Cards--Sample Program #6 (Program DC2DC)

The Control Cards for Sample Program #6 are shown below.
Sections 3.6-3.10 give instructions for preparing these cards.

F92UD MP BSN1 8 .74 3 2. 2.
 24. 6. 16. 10. 20. 10. .01 .011 .36 .4 1 8 5.067E-07 HEAV 1 1
 1.0 10. .60 .1
 0

5.7.3 Results of Sample Program #6--Program DC2DC

The following four pages give the results of Sample Program #6. Procedure DSNI of Program DC2DC has produced a list of fifty usable reactor element designs. Note from the "OP MODE" column of the design list that all of the designs operate in Mode 1 (continuous mmf mode) over the entire design range as desired. Also note that the stack height was increased to two cores by DC2DC in order to produce fifty designs. From the design evaluation portion of the printout, it can be seen that the maximum transistor on-time (T_{ON}) over the design range is less than 75.0 μ sec for all the designs evaluated. Since the converter frequency is 10.0 KHz, this corresponds to a maximum duty cycle of 0.75 as desired. Also, the efficiency and the efficiency/mass of these designs are comparable to those of the single-winding designs produced in Sample Program #2 (section 5.2).

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FQ2UD--CONSTANT FREQ TWO-WINDING VOLTAGE STEP-UP/CURRENT STEP-UP CONVERTER DESIGN
I/O IN VOLTS, AMPERES, WATTS, TESLAS, MICROSEC, KHZ, OHMS

CONVERTER SPECIFICATIONS

V _{OUT}	I _{IN}	V _{IN}	P _{OUT}	P _{OUT}	V _{SAT}	I _{COLL.}	V _D	CAP ESS	COY FREQ	B _{RESIDUAL}	B _{MIN}	B _{MAX}	WIND FACTOR	MAI COSTS
24.0	6.0	16.0	10.0	20.0	1.00	10.00	0.60	0.10	10.0	1.000E-02	1.100E-02	3.600E-01	0.40	2

HIRE TYPE= HEAV MIN. PRI. STRANDS= 1 MIN. SEC. STRANDS= 1 RECIPROCAL CURRENT DENSITY= 5.067E-07 SQ.M/AMP

BESTRICTING THE MAX. DUTY CYCLE= 0.740

THE FOLLOWING CORES MATCH THE CONSTRAINTS WHEN USED IN A 1-CORE STACK

SIZE NO.	MAGNETICS	ARNOLD	MU	NP	Avg Pri.	Pri. Ind.	HS	Avg Sec.	Sec. Ind.	WDG	OP	I _{BP}	I _{BS}	I _{PRES}	I _{CRMS}	I _{CREM}
					PHI.	SH			SH	PAC MODE	MAX	MAX	MAX	MAX	MAX	MAX
25	55089	A-089178	125	42	13	0.320	72	17	0.941	0.348	1	6.108	3.563	4.770	1.642	1.415
26	55175	A-1506156	125	46	13	0.327	79	17	0.965	0.310	1	6.098	3.551	4.770	1.641	1.414
27	55109	A-1506176	125	48	13	0.348	91	17	1.310	0.284	1	5.948	3.564	4.766	1.640	1.413
27	55108	A-1506200	147	54	13	0.360	76	17	1.074	0.236	1	6.053	3.553	4.772	1.637	1.409
27	55107	A-1506200	160	50	13	0.324	69	17	0.964	0.214	1	6.109	3.561	4.773	1.638	1.409
27	55103	A-1506218	173	57	13	0.300	63	17	0.869	0.197	1	6.139	3.565	4.767	1.647	1.411
28	55107	A-1506230	147	54	13	0.378	57	17	1.116	0.309	1	6.034	3.563	4.768	1.637	1.409
28	55106	A-1506236	160	50	13	0.337	51	17	0.973	0.322	1	6.093	3.564	4.770	1.641	1.411
28	55106	A-1506390	173	58	13	0.317	68	17	0.932	0.322	1	6.093	3.564	4.763	1.641	1.411
29	55114	A-156142	125	77	13	0.28	133	17	0.932	0.322	1	6.093	3.564	4.766	1.641	1.411
29	55116	A-156167	147	65	13	0.291	112	17	0.932	0.322	1	6.093	3.564	4.766	1.641	1.411
29	55117	A-183197	173	54	13	0.351	93	17	0.932	0.322	1	6.093	3.564	4.766	1.641	1.411
29	55118	A-219233	205	85	13	0.562	77	17	1.161	0.514	1	6.093	3.564	4.766	1.641	1.411
29	55119	A-542228	125	99	12	2.192	171	17	1.656	0.286	1	6.093	3.564	4.766	1.641	1.411
29	55120	A-157268	147	63	13	0.313	163	17	0.932	0.322	1	6.093	3.564	4.766	1.641	1.411
29	55121	A-184316	173	71	13	1.1	120	17	0.932	0.322	1	6.093	3.564	4.766	1.641	1.411
31	55124	A-220374	205	59	13	1.1	107	17	0.932	0.322	1	6.093	3.564	4.766	1.641	1.411
32	55125	A-129124	60	277	13	1.1	107	17	0.932	0.322	1	6.093	3.564	4.766	1.641	1.411
32	55126	A-172259	125	132	13	1.1	129	17	0.932	0.322	1	6.093	3.564	4.766	1.641	1.411
32	55127	A-159304	147	113	13	1.1	129	17	0.932	0.322	1	6.093	3.564	4.766	1.641	1.411
32	55128	A-185358	173	107	13	1.1	129	17	0.932	0.322	1	6.093	3.564	4.766	1.641	1.411
32	55129	A-221425	205	80	13	1.1	138	17	0.932	0.322	1	6.093	3.564	4.766	1.641	1.411

THE FOLLOWING CORES MATCH THE CONSTRAINTS WHEN USED IN A 2-CORE STACK

SIZE NO.	MAGNETICS	ARNOLD	MU	NP	Avg Pri.	Pri. Ind.	HS	Avg Sec.	Sec. Ind.	WDG	OP	I _{BP}	I _{BS}	I _{PRES}	I _{CRMS}	I _{CREM}
					PHI.	SH			SH	PAC MODE	MAX	MAX	MAX	MAX	MAX	MAX
24	55253	A-1511198	147	30	13	0.362	51	17	1.045	0.355	1	6.031	3.547	4.763	1.647	1.415
24	55254	A-3062233	160	28	13	0.393	48	17	1.007	0.332	1	6.069	3.540	4.762	1.640	1.413
24	55255	A-179233	173	25	13	0.295	43	17	0.874	0.297	1	6.160	3.552	4.773	1.651	1.423
24	55256	A-089178	125	48	13	0.373	63	17	0.906	0.366	1	6.037	3.542	4.767	1.649	1.417
24	55257	A-153210	147	37	13	0.364	63	17	0.994	0.306	1	6.057	3.557	4.769	1.651	1.421
24	55258	A-326228	160	34	13	0.337	63	17	1.111	0.257	1	6.099	3.563	4.771	1.653	1.423
24	55259	A-195286	173	31	13	0.483	53	17	1.411	0.229	1	6.084	3.555	4.763	1.649	1.417
24	55260	A-216292	200	27	13	0.323	123	17	1.111	0.257	1	6.099	3.563	4.771	1.653	1.423
24	55261	A-380056	250	21	13	0.320	36	17	0.941	0.229	1	6.084	3.555	4.763	1.649	1.417
25	55715	A-715152	125	48	13	0.712	82	17	0.979	0.322	1	6.084	3.555	4.763	1.649	1.417
25	55714	A-155179	147	63	13	0.611	70	17	0.782	0.288	1	6.084	3.555	4.763	1.649	1.417
25	55713	A-327195	160	47	13	0.642	63	17	0.751	0.288	1	6.084	3.555	4.763	1.649	1.417
25	55709	A-181210	173	50	13	0.616	63	17	0.440	0.288	1	6.084	3.555	4.763	1.649	1.417
25	55712	A-217249	200	50	13	0.327	100	17	1.041	0.288	1	6.084	3.555	4.763	1.649	1.417
25	55109	A-109156	250	31	13	0.327	100	17	1.041	0.288	1	6.084	3.555	4.763	1.649	1.417
25	55108	A-155185	147	48	13	0.717	78	17	0.979	0.322	1	6.084	3.555	4.763	1.649	1.417
25	55107	A-182218	173	52	13	0.789	78	17	1.056	0.322	1	6.084	3.555	4.763	1.649	1.417
25	55103	A-218259	200	50	13	0.667	87	17	1.701	0.322	1	6.084	3.555	4.763	1.649	1.417
25	55106	A-383312	200	48	13	0.420	88	17	0.981	0.322	1	6.084	3.555	4.763	1.649	1.417
25	55106	A-402374	200	50	13	0.420	88	17	0.981	0.322	1	6.084	3.555	4.763	1.649	1.417
28	55436	A-326260	160	50	13	0.666	55	17	0.262	0.380	1	5.774	3.560	4.764	1.639	1.411
28	55432	A-180190	173	52	13	0.666	55	17	1.729	0.297	1	5.850	3.401	4.766	1.646	1.416
28	55435	A-215262	200	50	13	0.654	43	17	1.351	0.237	1	5.914	3.479	4.760	1.644	1.414
28	55433	A-401674	300	16	13	0.359	27	17	1.022	0.189	1	6.025	3.570	4.768	1.655	1.423

THE MAXIMUM CP 50 WINDABILITY CHECKS HAS BEEN REACHED

DESIGN EVALUATION

MAX. NO. OF EVALUATIONS = 3

EVALUATION PCB DESIGN NO. 1

SIZE NO.	MAGNETICS	ARNOLD	HU	NF	AVG. PRI. IND.	NS	AVG. SEC. IND.	WDG. OF	IBP	IHS	IPMS	ISRMS	ICRMS
					MH		MH	FAC MODE	MAX	MAX	MAX	MAX	MAX
25	55G89	1-089178	125.	42	13	0.320	72	17	0.941	0.348	1	6.108	3.563
	REACTOR AREA	PATH LENGTH	CORE WH. AREA	REACTOR LENGTH/TURN	STACK HEIGHT	REACTOR MASS	REACTOR PRI. WIRE LENGTH, M	REACTOR PRI. WIRE RES, OHMS	REACTOR SEC. WIRE LENGTH, M	REACTOR SEC. WIRE RES, OHMS			
1.340E-04	1.160E-01	6.111E-04	5.920E-02	1.610E-02	2.255E-01	2.486E 00	1.664E-02	4.262E 00	7.102E-02				

V IN= 6.0

PO WATTS	TAP AMPS	IAS AMPS	IBP AMPS	IHS AMPS	T ON USEC	IPMS AMPS	ISRMS AMPS	ICRMS AMPS	TRANS DIODE	LOSSSES WIRE	(WATTS) CORE	***** CAPAC	EPP TOTAL %	EFF MASS %/KG	
10.00	2.19	1.27	3.34	1.95	74.16	2.40	0.83	0.71	0.575	0.495	0.145	0.052	0.051	1.318	86.4 3.92E 02
12.00	2.74	1.60	3.90	2.27	74.16	2.67	0.89	0.85	0.824	0.933	0.208	0.052	0.073	1.750	87.3 3.87E 02
14.00	3.29	1.92	4.45	2.60	74.16	2.95	1.12	0.99	1.119	0.991	0.282	0.052	0.099	2.242	86.2 3.82E 02
16.00	3.84	2.24	5.00	2.92	74.16	3.23	1.13	1.459	0.789	0.367	0.052	0.129	2.796	85.1 3.77E 02	
18.00	4.40	2.56	5.55	3.24	74.16	3.50	1.18	1.844	0.987	0.464	0.052	0.162	3.410	84.1 3.73E 02	
20.00	4.95	2.89	6.11	3.56	74.16	3.77	1.64	1.42	2.275	0.985	0.573	0.052	0.200	4.086	83.0 3.68E 02

V IN= 8.0

PO WATTS	TAP AMPS	IAS AMPS	IBP AMPS	IHS AMPS	T ON USEC	IPMS AMPS	ISRMS AMPS	ICRMS AMPS	TRANS DIODE	LOSSSES WIRE	(WATTS) CORE	***** CAPAC	EPP TOTAL %	EFF MASS %/KG	
10.00	1.48	0.84	2.91	1.70	67.21	1.82	0.74	0.61	0.331	0.445	0.095	0.101	0.038	1.009	90.8 4.03E 02
12.00	1.86	1.10	3.35	1.95	67.21	2.17	0.89	0.73	0.471	0.531	0.135	0.101	0.053	1.291	90.7 4.00E 02
14.00	2.24	1.35	3.78	2.21	67.21	2.52	1.03	0.85	0.637	0.617	0.182	0.101	0.072	1.609	90.6 3.98E 02
16.00	2.62	1.60	4.22	2.46	67.21	2.88	1.17	0.96	0.829	0.704	0.237	0.101	0.093	1.964	90.5 3.95E 02
18.00	3.00	1.86	4.66	2.72	67.21	3.23	1.32	1.08	1.086	0.790	0.299	0.101	0.117	2.353	90.4 3.92E 02
20.00	3.38	2.11	5.09	2.97	67.21	3.59	1.46	1.20	1.288	0.877	0.368	0.101	0.144	2.779	90.3 3.89E 02

V IN= 10.0

PO WATTS	TAP AMPS	IAS AMPS	IBP AMPS	IHS AMPS	T ON USEC	IPMS AMPS	ISRMS AMPS	ICRMS AMPS	TRANS DIODE	LOSSSES WIRE	(WATTS) CORE	***** CAPAC	EPP TOTAL %	EFF MASS %/KG	
10.00	0.98	0.58	2.72	1.59	61.46	1.50	0.70	0.56	0.226	0.417	0.072	0.159	0.031	0.906	91.7 4.07E 02
12.00	1.37	0.79	3.09	1.80	61.46	1.75	0.83	0.66	0.219	0.495	0.102	0.159	0.063	1.119	91.5 4.06E 02
14.00	1.76	1.01	3.45	2.02	61.46	2.07	1.06	0.76	0.299	0.374	0.137	0.159	0.058	1.357	91.3 4.04E 02
16.00	2.14	1.23	3.83	2.26	61.46	2.36	1.29	0.86	0.356	0.553	0.178	0.159	0.074	1.620	90.9 4.03E 02
18.00	2.52	1.44	4.20	2.50	61.46	2.66	1.43	1.07	0.860	0.813	0.224	0.159	0.093	1.908	90.4 4.01E 02
20.00	2.89	1.66	4.57	2.67	61.46	2.93	1.55				0.275	0.159	0.114	2.221	90.3 3.99E 02

V IN= 12.0

PO WATTS	TAP AMPS	IAS AMPS	IBP AMPS	IHS AMPS	T ON USEC	IPMS AMPS	ISRMS AMPS	ICRMS AMPS	TRANS DIODE	LOSSSES WIRE	(WATTS) CORE	***** CAPAC	EPP TOTAL %	EFF MASS %/KG	
10.00	0.67	0.39	2.62	1.53	56.61	1.31	0.57	0.52	0.171	0.401	0.061	0.223	0.027	0.883	91.6 4.07E 02
12.00	1.00	0.58	2.95	1.72	56.61	1.55	0.79	0.61	0.239	0.473	0.085	0.223	0.037	1.057	91.4 4.08E 02
14.00	1.33	0.78	3.28	1.91	56.61	1.78	0.91	0.70	0.318	0.547	0.113	0.223	0.049	1.250	91.2 4.06E 02
16.00	1.66	0.97	3.61	2.10	56.61	2.03	1.03	0.79	0.411	0.621	0.145	0.223	0.063	1.450	90.9 4.05E 02
18.00	2.00	1.16	3.94	2.30	56.61	2.27	1.16	0.88	0.515	0.733	0.182	0.223	0.078	1.656	91.1 4.03E 02
20.00	2.32	1.35	4.26	2.49	56.61	2.51	1.28	0.98	0.631	0.770	0.224	0.223	0.095	1.945	91.1 4.04E 02

V IN= 14.0

PO WATTS	TAP AMPS	IAS AMPS	IBP AMPS	IHS AMPS	T ON USEC	IPMS AMPS	ISRMS AMPS	ICRMS AMPS	TRANS DIODE	LOSSSES WIRE	(WATTS) CORE	***** CAPAC	EPP TOTAL %	EFF MASS %/KG	
10.00	0.44	0.26	2.57	1.50	52.47	1.18	0.65	0.50	0.138	0.392	0.054	0.289	0.025	0.898	91.8 4.07E 02
12.00	0.74	0.43	2.87	1.57	52.47	1.38	0.77	0.58	0.190	0.460	0.074	0.289	0.034	1.047	92.0 4.08E 02
14.00	1.04	0.61	3.17	1.85	52.47	1.58	0.88	0.66	0.252	0.529	0.098	0.289	0.044	1.212	92.0 4.08E 02
16.00	1.34	0.78	3.47	2.02	52.47	1.78	1.00	0.74	0.323	0.599	0.126	0.289	0.055	1.392	92.0 4.08E 02
18.00	1.64	0.96	3.77	2.19	52.47	1.98	1.12	0.83	0.404	0.669	0.157	0.289	0.068	1.587	91.9 4.08E 02
20.00	1.94	1.13	4.07	2.37	52.47	2.22	1.23	0.91	0.494	0.740	0.192	0.289	0.083	1.798	91.8 4.07E 02

V IN= 16.0

PO WATTS	TAP AMPS	IAS AMPS	IBP AMPS	IHS AMPS	T ON USEC	IPMS AMPS	ISRMS AMPS	ICRMS AMPS	TRANS DIODE	LOSSSES WIRE	(WATTS) CORE	***** CAPAC	EPP TOTAL %	EFF MASS %/KG	
10.00	0.26	0.15	2.54	1.48	48.89	1.08	0.64	0.49	0.117	0.387	0.049	0.356	0.028	0.933	91.5 4.06E 02
12.00	0.41	0.31	2.82	1.65	48.89	1.26	0.75	0.56	0.159	0.451	0.067	0.356	0.032	1.064	91.0 4.07E 02
14.00	0.61	0.47	3.10	1.81	48.89	1.44	0.86	0.63	0.209	0.517	0.088	0.356	0.040	1.269	92.0 4.08E 02
16.00	0.79	0.64	3.38	1.97	48.89	1.63	0.97	0.71	0.266	0.583	0.112	0.356	0.050	1.369	92.1 4.08E 02
18.00	1.07	0.80	3.66	2.14	48.89	1.82	1.08	0.78	0.331	0.651	0.140	0.356	0.061	1.559	92.1 4.08E 02
20.00	1.35	0.96	3.94	2.30	48.89	2.01	1.20	0.86	0.403	0.719	0.170	0.356	0.074	1.724	92.1 4.08E 02

**REPRODUCIBILITY OF THE
ORIGINAL PAGE IS POOR**

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EVALUATION FOR DESIGN NO. 2

SIZE NO.	MAGNETICS	ARNOLD	NU	XP	ANG.	PRI. IND.	VS	AVG. SEC.	SEC. IND.	Wdg. Fac.	Op. Mode	I _P S MAX	I _B S MAX	I _P RMS MAX	I _S RMS MAX	I _C RMS MAX	
26	55715	A-715152	125.	46	13	0.327	79	17	0.965	0.310	1	6.098	3.551	4.770	1.641	1.814	
REACTOR AREA SQ.M	PATH LENGTH M	CORE AREA SQ.M	REACTOR LENGTH/TUBE M	STACK HEIGHT M	REACTOR MASS KG	REACTOR PRI.WIRE RES.OHMS	REACTOR SEC.WIRE RES.OHMS	REACTOR LENGTH,M	REACTOR SEC.WIRE RES.OHMS	REACTOR SEC.WIRE RES.OHMS	REACTOR SEC.WIRE RES.OHMS						
1.250E-04	1.270E-01	7.519E-04	5.770E-02	1.400E-02	2.340E-01	2.654E 00	1.776E-02	4.558E 00	7.702E-02								
V IN= 6.0																	
PO WATTS	I _A P AMPS	I _A S AMPS	I _B P AMPS	I _B S AMPS	T ON USEC	I _P RMS AMPS	I _S RMS AMPS	I _C RMS AMPS	TRANS	DIODE	LOSSSES	(WATTS)	CORE	CAPAC	TOTAL	EFF %	
10.00	2.20	1.28	3.33	1.98	74.13	2.85	0.82	0.71	0.575	0.495	0.155	0.050	0.051	1.325	86.3	3.77E 02	
12.00	2.75	1.60	3.89	2.26	74.13	2.85	0.99	0.73	0.824	0.593	0.222	0.050	0.073	1.561	87.3	3.73E 02	
14.00	3.37	2.04	4.44	2.58	74.13	2.85	1.15	0.73	0.99	0.691	0.301	0.050	0.050	0.098	2.159	88.0	3.70E 02
16.00	4.06	2.52	5.00	2.91	74.13	2.85	1.31	0.73	1.119	0.789	0.392	0.050	0.128	2.518	88.0	3.69E 02	
18.00	4.81	3.09	5.59	3.23	74.13	2.85	1.48	0.73	1.27	0.887	0.612	0.050	0.162	3.422	88.0	3.68E 02	
20.00	5.66	3.69	6.10	3.55	74.13	2.85	1.64	0.73	1.41	1.276	0.985	0.200	0.200	4.122	88.0	3.66E 02	
V IN= 8.0																	
PO WATTS	I _A P AMPS	I _A S AMPS	I _B P AMPS	I _B S AMPS	T ON USEC	I _P RMS AMPS	I _S RMS AMPS	I _C RMS AMPS	TRANS	DIODE	LOSSSES	(WATTS)	CORE	CAPAC	TOTAL	EFF %	
10.00	1.45	0.85	2.90	1.69	67.17	1.85	0.74	0.61	0.331	0.444	0.101	0.097	0.037	1.110	90.9	3.38E 02	
12.00	1.90	1.10	3.33	1.94	67.17	1.85	0.88	0.73	0.471	0.530	0.144	0.097	0.053	1.617	90.9	3.36E 02	
14.00	2.33	1.36	3.77	2.20	67.17	1.85	1.03	0.73	0.637	0.516	0.194	0.097	0.072	1.875	90.9	3.35E 02	
16.00	2.77	1.61	4.21	2.45	67.17	1.85	1.17	0.73	0.829	0.703	0.253	0.097	0.093	2.175	90.9	3.34E 02	
18.00	3.21	1.87	4.64	2.70	67.17	1.85	1.32	0.73	0.946	0.790	0.319	0.097	0.117	2.576	90.9	3.33E 02	
20.00	3.64	2.12	5.08	2.96	67.17	1.85	1.46	0.73	1.20	1.288	0.877	0.393	0.097	0.154	2.799	90.7	3.32E 02
V IN= 10.0																	
PO WATTS	I _A P AMPS	I _A S AMPS	I _B P AMPS	I _B S AMPS	T ON USEC	I _P RMS AMPS	I _S RMS AMPS	I _C RMS AMPS	TRANS	DIODE	LOSSSES	(WATTS)	CORE	CAPAC	TOTAL	EFF %	
10.00	1.01	0.59	2.70	1.57	61.41	1.50	0.60	0.55	0.226	0.316	0.077	0.153	0.021	0.503	91.7	3.92E 02	
12.00	1.36	0.89	3.07	1.73	61.41	1.50	0.62	0.60	0.319	0.394	0.109	0.153	0.032	1.108	91.1	3.91E 02	
14.00	1.71	1.20	3.48	2.00	61.41	1.50	0.66	0.76	0.529	0.571	0.186	0.153	0.052	1.308	91.0	3.90E 02	
16.00	2.14	1.54	3.81	2.22	61.41	1.50	0.70	0.86	0.629	0.699	0.209	0.153	0.072	1.506	91.0	3.89E 02	
18.00	2.59	1.87	4.18	2.48	61.41	1.50	0.74	0.96	0.799	0.759	0.239	0.153	0.092	1.704	91.0	3.88E 02	
20.00	2.98	2.20	4.55	2.69	61.41	1.50	0.78	0.97	0.859	0.872	0.294	0.153	0.114	2.111	91.0	3.86E 02	
V IN= 12.0																	
PO WATTS	I _A P AMPS	I _A S AMPS	I _B P AMPS	I _B S AMPS	T ON USEC	I _P RMS AMPS	I _S RMS AMPS	I _C RMS AMPS	TRANS	DIODE	LOSSSES	(WATTS)	CORE	CAPAC	TOTAL	EFF %	
10.00	0.70	0.41	2.60	1.51	56.56	1.31	0.67	0.52	0.171	0.400	0.064	0.214	0.027	0.576	91.9	3.93E 02	
12.00	1.03	0.60	2.93	1.70	56.56	1.31	0.79	0.61	0.238	0.872	0.090	0.214	0.037	1.551	91.9	3.93E 02	
14.00	1.36	0.79	3.26	1.90	56.56	1.31	0.91	0.70	0.318	0.546	0.120	0.214	0.049	1.471	91.9	3.92E 02	
16.00	1.68	0.98	3.59	2.09	56.56	1.31	1.03	0.79	0.410	0.620	0.155	0.214	0.062	1.551	91.9	3.92E 02	
18.00	2.01	1.17	3.92	2.28	56.56	1.31	1.16	0.88	0.514	0.694	0.195	0.214	0.078	1.747	91.4	3.91E 02	
20.00	2.34	1.36	4.25	2.47	56.56	1.31	1.28	0.97	0.631	0.769	0.239	0.214	0.095	1.947	91.1	3.90E 02	
V IN= 14.0																	
PO WATTS	I _A P AMPS	I _A S AMPS	I _B P AMPS	I _B S AMPS	T ON USEC	I _P RMS AMPS	I _S RMS AMPS	I _C RMS AMPS	TRANS	DIODE	LOSSSES	(WATTS)	CORE	CAPAC	TOTAL	EFF %	
10.00	0.46	0.27	2.55	1.48	52.42	1.17	0.55	0.50	0.138	0.390	0.057	0.277	0.025	0.387	91.9	3.93E 02	
12.00	0.76	0.44	2.85	1.66	52.42	1.17	0.68	0.66	0.200	0.490	0.104	0.277	0.033	1.376	91.9	3.93E 02	
14.00	1.06	0.62	3.15	1.83	52.42	1.17	0.88	0.66	0.251	0.528	0.104	0.277	0.043	1.576	91.9	3.92E 02	
16.00	1.36	0.82	3.45	2.01	52.42	1.17	1.00	0.76	0.323	0.608	0.134	0.277	0.055	1.776	91.9	3.92E 02	
18.00	1.67	0.97	3.75	2.18	52.42	1.17	1.11	0.82	0.403	0.668	0.167	0.277	0.068	1.976	91.9	3.92E 02	
20.00	1.97	1.15	4.05	2.36	52.42	1.17	1.23	0.91	0.493	0.739	0.205	0.277	0.082	2.196	91.9	3.92E 02	
V IN= 16.0																	
PO WATTS	I _A P AMPS	I _A S AMPS	I _B P AMPS	I _B S AMPS	T ON USEC	I _P RMS AMPS	I _S RMS AMPS	I _C RMS AMPS	TRANS	DIODE	LOSSSES	(WATTS)	CORE	CAPAC	TOTAL	EFF %	
10.00	0.20	0.16	2.52	1.47	49.95	1.09	0.59	0.49	0.116	0.385	0.052	0.341	0.026	0.518	91.6	3.92E 02	
12.00	0.36	0.33	2.89	1.63	49.95	1.09	0.75	0.66	0.158	0.495	0.071	0.341	0.031	1.511	91.6	3.92E 02	
14.00	0.52	0.49	3.26	1.80	49.95	1.09	0.98	0.66	0.208	0.595	0.094	0.341	0.050	1.707	91.6	3.92E 02	
16.00	0.71	0.69	3.60	1.96	49.95	1.09	1.07	0.76	0.268	0.615	0.120	0.341	0.060	1.907	91.6	3.92E 02	
18.00	0.90	0.89	3.92	2.12	49.95	1.09	1.23	0.86	0.330	0.690	0.149	0.341	0.071	2.106	91.6	3.92E 02	
20.00	1.08	0.98	4.20	2.28	49.95	1.09	1.37	0.96	0.403	0.778	0.182	0.341	0.074	2.276	91.6	3.92E 02	

EVALUATION FOR DESIGN NO. 3													IAMS MAX			
SIZE MAGNETICS NO.	ARNOLD	MU	HP	Avg. PRI. IND. PH	NS	SEC. SEC: PH	Vdg. Fac. Mode	Op. Max	IIP	IAMS MAX	IERRMS MAX	ITEMS MAX	IAMS MAX			
27	55109	A-109156	125.	53	13	0.444	91	17	1.310	0.284	1	5.948	3.464	4.766	1.640	1.412
REACTOR AREA SQ.M	REACTOR PATH LENGTH M	CORE WH. AREA SQ.M	REACTOR LENGTH/TURN M	STACK HEIGHT M	REACTOR MASS KG	REACTOR PRI. WIRE LENGTH, M	REACTOR SECOND. WIRE LENGTH, M	REACTOR RES. OHMS								
1.440E-04	1.430E-01	9.480E-04	6.230E-02	1.490E-02	3.016E-01	3.302E-00	2.210E-02	5.669E-00	9.579E-02							
V IN= 6.0															EFF/EFF A/KG	
PO WATTS	IAP AMPS	IAS AMPS	IBP AMPS	IBS AMPS	T ON USEC	IPRMS AMPS	ISRMS AMPS	ICRMS AMPS	TRANS DIODE	LOSSES WIRE	(WATTS)	CORE	CAPAC	TOTAL	EFF/EFF A/KG	
10.00	2.35	1.37	3.18	1.86	74.13	2.39	0.82	0.71	0.571	0.493	0.191	0.030	0.050	1.336	87.7	2.938 02
12.00	2.80	1.69	3.74	2.18	74.13	2.86	0.99	0.85	0.821	0.591	0.274	0.036	0.072	2.306	89.9	2.958 02
14.00	3.45	2.01	4.29	2.50	74.13	3.34	1.15	0.99	1.145	0.589	0.373	0.030	0.098	2.306	87.7	2.812 02
16.00	4.51	2.33	4.84	2.82	74.13	4.28	1.31	1.13	1.456	0.788	0.487	0.030	0.129	2.306	87.7	2.776 02
18.00	5.66	2.63	5.39	3.14	74.13	4.77	1.48	1.27	1.844	0.886	0.616	0.030	0.162	2.306	87.7	2.742 02
20.00	5.11	2.98	5.95	3.46	74.13	4.77	1.64	1.41	2.272	0.984	0.760	0.030	0.200	4.145	87.7	2.742 02
V IN= 8.0															EFF/EFF A/KG	
PO WATTS	IAP AMPS	IAS AMPS	IBP AMPS	IBS AMPS	T ON USEC	IPRMS AMPS	ISRMS AMPS	ICRMS AMPS	TRANS DIODE	LOSSES WIRE	(WATTS)	CORE	CAPAC	TOTAL	EFF/EFF A/KG	
10.00	1.65	0.96	2.71	1.58	67.18	1.80	0.73	0.60	0.325	0.441	0.124	0.057	0.037	0.554	91.0	3.022 02
12.00	2.22	1.22	3.14	1.83	67.18	2.16	0.88	0.72	0.466	0.527	0.177	0.057	0.052	1.179	89.4	2.952 02
14.00	2.87	1.47	3.58	2.09	67.18	2.51	1.02	0.84	0.632	0.614	0.240	0.057	0.071	1.514	89.4	2.952 02
16.00	3.52	1.72	4.02	2.34	67.18	2.87	1.17	0.96	0.323	0.701	0.303	0.057	0.092	1.595	89.4	2.952 02
18.00	4.17	1.98	4.46	2.59	67.18	3.23	1.31	1.08	1.040	0.768	0.395	0.057	0.116	2.397	87.5	2.908 02
20.00	3.83	2.23	4.89	2.85	67.18	3.58	1.46	1.20	1.283	0.875	0.487	0.057	0.143	2.645	87.5	2.908 02
V IN= 10.0															EFF/EFF A/KG	
PO WATTS	IAP AMPS	IAS AMPS	IBP AMPS	IBS AMPS	T ON USEC	IPRMS AMPS	ISRMS AMPS	ICRMS AMPS	TRANS DIODE	LOSSES WIRE	(WATTS)	CORE	CAPAC	TOTAL	EFF/EFF A/KG	
10.00	1.23	0.72	2.48	1.64	61.42	1.48	0.68	0.54	0.219	0.410	0.093	0.090	0.029	0.754	91.2	3.068 02
12.00	1.66	1.03	2.85	1.66	61.42	1.77	0.82	0.64	0.422	0.569	0.173	0.090	0.055	1.179	89.3	3.028 02
14.00	2.07	1.35	3.22	1.87	61.42	2.05	0.95	0.79	0.546	0.649	0.233	0.090	0.091	1.595	89.3	2.988 02
16.00	2.72	1.37	3.59	2.09	61.42	2.34	1.08	0.85	0.692	0.729	0.294	0.090	0.112	2.196	89.3	2.988 02
18.00	3.25	1.58	3.96	2.31	61.42	2.63	1.35	1.06	0.853	0.809	0.362	0.090	0.143	2.645	89.3	2.988 02
V IN= 12.0															EFF/EFF A/KG	
PO WATTS	IAP AMPS	IAS AMPS	IBP AMPS	IBS AMPS	T ON USEC	IPRMS AMPS	ISRMS AMPS	ICRMS AMPS	TRANS DIODE	LOSSES WIRE	(WATTS)	CORE	CAPAC	TOTAL	EFF/EFF A/KG	
10.00	0.95	0.55	2.35	1.37	56.57	1.28	0.65	0.50	0.163	0.391	0.077	0.125	0.025	0.750	91.8	3.085 02
12.00	1.28	0.74	2.68	1.56	56.57	1.52	0.82	0.64	0.230	0.489	0.133	0.090	0.041	1.167	89.5	3.038 02
14.00	1.61	0.94	3.01	1.94	56.57	1.75	1.02	0.75	0.310	0.539	0.186	0.090	0.055	1.595	89.5	3.028 02
16.00	1.94	1.13	3.34	2.12	56.57	2.01	1.12	0.87	0.402	0.689	0.259	0.090	0.091	2.196	89.5	3.028 02
18.00	2.26	1.32	3.67	2.33	56.57	2.25	1.27	0.96	0.523	0.764	0.293	0.090	0.126	2.645	89.5	3.035 02
20.00	2.59	1.51	3.99	2.53	56.57	2.50	1.42	1.06	0.623	0.764	0.323	0.090	0.167	3.034	89.5	3.035 02
V IN= 14.0															EFF/EFF A/KG	
PO WATTS	IAP AMPS	IAS AMPS	IBP AMPS	IBS AMPS	T ON USEC	IPRMS AMPS	ISRMS AMPS	ICRMS AMPS	TRANS DIODE	LOSSES WIRE	(WATTS)	CORE	CAPAC	TOTAL	EFF/EFF A/KG	
10.00	0.74	0.43	2.27	1.32	52.43	1.14	0.63	0.47	0.129	0.378	0.066	0.161	0.022	0.757	93.0	3.088 02
12.00	1.04	0.60	2.57	1.50	52.43	1.39	0.80	0.75	0.181	0.448	0.093	0.161	0.031	1.614	89.6	3.088 02
14.00	1.38	0.78	2.87	1.67	52.43	1.64	0.96	0.86	0.243	0.519	0.125	0.161	0.041	1.614	89.6	3.078 02
16.00	1.72	0.95	3.17	1.85	52.43	1.99	1.08	0.98	0.348	0.590	0.162	0.161	0.052	1.614	89.6	3.066 02
18.00	2.04	1.13	3.47	2.02	52.43	2.20	1.22	0.89	0.465	0.733	0.250	0.161	0.080	1.614	89.6	3.056 02
20.00	2.24	1.31	3.77	2.20	52.43	2.20	1.42	0.98	0.589	0.733	0.321	0.161	0.108	1.614	89.6	3.056 02
V IN= 16.0															EFF/EFF A/KG	
PO WATTS	IAP AMPS	IAS AMPS	IBP AMPS	IBS AMPS	T ON USEC	IPRMS AMPS	ISRMS AMPS	ICRMS AMPS	TRANS DIODE	LOSSES WIRE	(WATTS)	CORE	CAPAC	TOTAL	EFF/EFF A/KG	
10.00	0.57	0.33	2.22	1.29	48.85	1.03	0.52	0.45	0.107	0.369	0.060	0.198	0.021	0.754	93.0	3.088 02
12.00	0.65	0.50	2.50	1.62	48.85	1.22	0.63	0.53	0.199	0.436	0.093	0.198	0.028	1.682	93.0	3.088 02
14.00	1.13	0.69	2.78	1.78	48.85	1.41	0.85	0.60	0.260	0.504	0.141	0.198	0.036	1.682	93.0	3.088 02
16.00	1.41	0.82	3.06	1.95	48.85	1.60	1.07	0.68	0.256	0.572	0.144	0.198	0.046	1.696	93.0	3.078 02
18.00	1.65	0.99	3.34	2.11	48.85	1.79	1.18	0.84	0.393	0.640	0.180	0.198	0.058	1.696	93.0	3.078 02
20.00	1.87	1.15	3.62	2.11	48.85	1.98	1.38	0.84	0.493	0.709	0.221	0.198	0.070	1.696	93.0	3.078 02

5.8 SAMPLE PROGRAM #7 -- PROGRAM DC2DC

It can be seen from the output of Sample Program #6 that core size #24 is the smallest core in the core catalog which will meet the design constraints when used in a stack of two cores or less. Sample Program #7 uses Procedure DSN2 of Program DC2DC to attempt to produce a design using core size #23 with a relative permeability of 125.0 in a three-core stack. All other design requirements remain the same as in Sample Program #6.

5.8.1 Control Cards--Sample Program #7 (Program DC2DC)

The Control Cards for Sample Program #7 are shown below.
Sections 3.6-3.10 give instructions for preparing these cards.

F02UD NP DSN2 8 .74 1 2. 2.
24. 6. 16. 10. 20. 10. .01 .011 .36 .4 1 2 5.067E-07 HEAVY 1 1
1.0 10. .60 .1
23 125. 3

5.8.2 Results of Sample Program #7--Program DC2DC

The results of Sample Program #7 are shown below. It can be seen from the print out that core size #23 with a relative permeability of 125.0 used in a three core stack will not meet the design requirement regarding maximum winding factor. Thus, the design is rejected by the program. The actual computed winding factor of 0.46 is shown on the program output.

 FQ2UD--CONSTANT FREQ TWO-WINDING VOLTAGE STEP-UP/CURRENT STEP-UP CONVERTER DESIGN
 I/O IN VOLTS, AMPERES, WATTS, TESLAS, MICROSEC, KHZ, OHMS

CONVERTER SPECIFICATIONS

I _{OUT}	V _{IN} MIN	V _{IN} MAX	P _{OUT} MIN	P _{OUT} MAX	V _{SAT}	I _{COLL.}	I _{DIGDE}	CAP _{ESR}	CONV _{FREQ}	B _{RESIDUAL}	B _{MIN}	B _{MAX}	WIND FACTOR	NO. COEFS
24.0	6.0	16.0	10.0	20.0	1.00	10.00	0.60	0.10	0.10	1.000E-02	1.100E-02	3.600E-01	0.40	3

 WIRE TYPE= EEA
 MIN. PRI. STRANDS= 1 MIN. SEC. STRANDS= 1 RECIEFEOCAL CURRENT DENSITY= 5.067E-07 SQ. IN/AMP

 RESTRICTING THE MAX. DUTY CYCLE= 0.740

DESIGN EVALUATION

 EVALUATION PCB DESIGN NO. 0

 CCBE ENTERED IS NOT WINDABLE--WF= 0.460

5.9 SAMPLE PROGRAM #8 -- PROGRAM DC2DC

Sample Program #8 uses Procedure DSN2 of Program DC2DC to attempt to produce a design for the same core size, relative permeability and stack height as used in Sample Program #7. In Sample Program #7, the reactor design produced was rejected because the winding factor of 0.46 was greater than the maximum winding factor of 0.40. Sample Program #8 uses the same design requirement data as Sample Program #7 except that the Reciprocal Current Density Specification is lowered to $3.8 \times 10^{-7} \text{ m}^2/\text{ampere}$ (≈ 750 circular mils/ampere) to allow smaller wire to be used. Also, it is desired that a minimum of two strands of wire be used for the primary winding. A minimum of one strand of wire is to be used for the secondary winding.

5.9.1 Control Cards--Sample Program #8 (Program DC2DC)

The Control Cards for Sample Program #8 are shown below.
Sections 3.6-3.10 give instructions for preparing these cards.

EQ2UP MP DSME 8 .74 1 84. 8.
 84. 6. 16. 10. 20. 10. .01 .011 .36 .4 1 8 3.800E-07 HEAV 2 1
 1.0 10. .60 .1
 23 125. 3

5.9.2 Results of Sample Program #8--Program DC2DC

The results of Sample Program #8 are given on the following page. Lowering the Reciprocal Current Density Specification allowed Program DC2DC to use wire of smaller cross-sectional area in the windings. Thus, the winding factor was lowered to 0.346 which is less than the specified maximum winding factor. Therefore, the design was acceptable. The smaller wire area has, however, caused a slight increase in the winding resistances over the designs evaluated in Sample Program #6.

POZUD--CONSTANT FREQ TWO-WINDING VOLTAGE STEP-UP/CURRENT STEP-UP CONVERTER DESIGN
I/O IN VOLTS, AMPERES, WATTS, TESLAS, MICROSEC, KHZ, OHMS

CONVERTER SPECIFICATIONS

T OUT	V IN	V IN	P OUT	P OUT	V SAT	I COLL.	T DIODE	C CAP	C CHV	E ESR	F FREQ	R RESIDUAL	B MIN	H MAX	W FACTOR	N CORES
24.0	6.0	16.0	10.0	20.0	1.00	10.00	0.60	0.10	10.0	1.000E-02	1.100E-02	3.600E-01	0.40	3		

WIRE TYPE= EBYT MIN. PRI. STRANDS= 2 MIN. SEC. STRANDS= 1 RECIPROCAL CURRENT DENSITY= 3.800E-07 SC.M/AMP

RESTRICTING THE MAX. DUTY CYCLE= 0.740

DESIGN EVALUATION

EVALUATION FOR DESIGN NO. 0

CORRECT WIRE SIZES NOT AVAILABLE OR MULTIPLE STRANDS SPECIFIED. 2 STRANDS USED FOR PRIMARY WINDING

SIZE MAGNETICS	ARNOOLD	NU	NP	Avg. PRI. IND.	HS	Avg. SEC.	SEC. IND.	RDG	OP	IPS	IPS	IPSMS	IPSMS	ICRMS		
23	55326	A-324117	125.	33	17	0.387	57	19	1.156	0.346	1	6.017	3.484	4.772	1.637	1.409

REACTOR AREA	PATH LENGTH	CORE	REACTOR LENGTH/TURNS	STACK HEIGHT	REACTOR MASS	REACTOR PRI. WIRE LENGTH, M	REACTOR SEC. WIRE LENGTH, M	REACTOR LENGTH, M	REACTOR MASS, OHMS
2.034E-04	8.980E-02	3.644E-04	8.860E-02	3.390E-02	2.368E-01	2.924E 00	2.470E-02	5.050E 00	1.360E-01

V IN= 6.0

PO	IAP	IAS	IBP	IBS	T ON	IPMS	ISMS	ICRMS	TRANS	DIODE	LOSSSES	(WATTS)	CORE	CAPAC	TOTAL	EPP	EPP/MASS
10.00	2.29	1.33	3.25	1.88	74.02	2.39	0.82	0.71	0.573	0.493	0.233	0.037	0.050	1.327	67.0	3.718	02
12.00	2.55	1.65	3.80	2.20	74.02	2.87	0.98	0.85	0.623	0.591	0.355	0.037	0.052	1.342	69.0	3.807	02
14.00	2.80	1.97	4.36	2.52	74.02	3.38	1.15	0.99	1.118	0.588	0.455	0.037	0.048	1.357	72.0	3.897	02
16.00	3.05	2.29	5.91	2.88	74.02	3.82	1.31	1.13	1.459	0.786	0.554	0.037	0.127	1.372	75.0	3.984	02
18.00	3.31	2.61	6.46	3.16	74.02	4.30	1.47	1.27	1.845	0.884	0.751	0.037	0.161	1.379	77.0	4.071	02
20.00	3.56	2.93	6.02	3.48	74.02	4.77	1.64	1.41	2.277	0.982	0.927	0.037	0.198	1.422	79.0	4.158	02

V IN= 8.0

PO	IAP	IAS	IBP	IBS	T ON	IPMS	ISMS	ICRMS	TRANS	DIODE	LOSSSES	(WATTS)	CORE	CAPAC	TOTAL	EPP	EPP/MASS
10.00	1.58	0.91	2.79	1.62	67.05	1.81	0.75	0.61	0.328	0.441	0.155	0.072	0.037	1.032	90.0	3.838	02
12.00	1.72	1.17	3.23	1.87	67.05	2.16	0.88	0.72	0.469	0.527	0.221	0.072	0.052	1.341	89.0	3.828	02
14.00	1.86	1.52	3.66	2.12	67.05	2.53	1.02	0.84	0.635	0.614	0.299	0.072	0.071	1.650	88.0	3.755	02
16.00	2.00	1.67	4.10	2.37	67.05	2.98	1.17	0.96	0.827	0.700	0.390	0.072	0.092	2.061	87.0	3.745	02
18.00	2.14	1.93	4.54	2.63	67.05	3.43	1.31	1.08	1.248	0.787	0.492	0.072	0.116	2.511	87.0	3.718	02
20.00	2.37	2.18	4.97	2.88	67.05	3.89	1.46	1.19	1.287	0.874	0.606	0.072	0.143	2.982	87.0	3.672	02

V IN= 10.0

PO	IAP	IAS	IBP	IBS	T ON	IPMS	ISMS	ICRMS	TRANS	DIODE	LOSSSES	(WATTS)	CORE	CAPAC	TOTAL	EPP	EPP/MASS
10.00	1.15	0.66	2.57	1.49	61.28	1.48	0.69	0.54	0.222	0.411	0.119	0.113	0.030	0.895	91.0	3.888	02
12.00	1.30	0.80	3.05	1.70	61.28	1.78	0.82	0.70	0.315	0.490	0.169	0.120	0.052	1.129	91.0	3.868	02
14.00	1.45	0.95	3.51	1.92	61.28	2.08	0.95	0.75	0.425	0.569	0.228	0.123	0.058	1.391	90.0	3.848	02
16.00	1.60	1.09	4.00	2.16	61.28	2.40	1.08	0.86	0.506	0.649	0.329	0.123	0.073	1.682	90.0	3.828	02
18.00	1.75	1.24	4.43	2.39	61.28	2.73	1.21	1.00	0.656	0.729	0.373	0.123	0.091	2.002	90.0	3.798	02
20.00	1.90	1.74	4.83	2.60	61.28	3.03	1.35	1.06	0.857	0.808	0.459	0.123	0.112	2.348	90.0	3.768	02

V IN= 12.0

PO	IAP	IAS	IBP	IBS	T ON	IPMS	ISMS	ICRMS	TRANS	DIODE	LOSSSES	(WATTS)	CORE	CAPAC	TOTAL	EPP	EPP/MASS
10.00	0.85	0.49	2.45	1.42	56.42	1.23	0.56	0.51	0.166	0.393	0.099	0.158	0.026	0.842	92.2	3.898	02
12.00	1.16	0.69	2.78	1.61	56.42	1.53	0.73	0.60	0.224	0.467	0.140	0.158	0.033	1.033	92.1	3.896	02
14.00	1.35	0.87	3.11	1.80	56.42	1.82	0.89	0.69	0.315	0.525	0.228	0.169	0.047	1.246	91.0	3.876	02
16.00	1.54	1.07	3.44	1.99	56.42	2.12	1.05	0.78	0.406	0.596	0.329	0.181	0.061	1.483	91.0	3.856	02
18.00	1.71	1.26	3.77	2.18	56.42	2.42	1.21	0.87	0.511	0.690	0.308	0.192	0.076	1.740	90.0	3.836	02
20.00	1.90	1.43	4.10	2.38	56.42	2.51											

V IN= 14.0

PO	IAP	IAS	IBP	IBS	T ON	IPMS	ISMS	ICRMS	TRANS	DIODE	LOSSSES	(WATTS)	CORE	CAPAC	TOTAL	EPP	EPP/MASS
10.00	0.63	0.37	2.39	1.38	52.22	1.15	0.64	0.48	0.132	0.382	0.088	0.204	0.023	0.829	92.3	3.808	02
12.00	0.93	0.54	2.69	1.56	52.22	1.36	0.75	0.56	0.185	0.451	0.122	0.204	0.031	0.992	92.4	3.806	02
14.00	1.23	0.71	3.09	1.73	52.22	1.57	0.87	0.64	0.246	0.521	0.163	0.204	0.041	1.176	92.4	3.804	02
16.00	1.44	0.89	3.29	1.90	52.22	1.78	0.99	0.73	0.318	0.592	0.211	0.208	0.051	1.377	92.4	3.802	02
18.00	1.64	1.06	3.59	2.08	52.22	2.00	1.10	0.81	0.399	0.663	0.264	0.204	0.066	1.595	91.9	3.784	02
20.00	1.84	1.24	3.89	2.25	52.22	2.21	1.22	0.90	0.489	0.734	0.324	0.204	0.080	1.831	91.6	3.762	02

V IN= 16.0

PO	IAP	IAS	IBP	IBS	T ON	IPMS	ISMS	ICRMS	TRANS	DIODE	LOSSSES	(WATTS)	CORE	CAPAC	TOTAL	EPP	EPP/MASS
10.00	0.86	0.27	2.35	1.36	48.70	1.05	0.62	0.46	0.110	0.374	0.080	0.250	0.022	0.837	92.3	3.908	02
12.00	1.22	0.43	2.63	1.52	48.70	1.21	0.73	0.54	0.182	0.440	0.111	0.250	0.029	0.982	92.4	3.906	02
14.00	1.43	0.59	2.91	1.68	48.70	1.42	0.85	0.61	0.202	0.507	0.147	0.250	0.037	1.144	92.4	3.904	02
16.00	1.63	0.76	3.19	1.85	48.70	1.61	0.96	0.69	0.260	0.575	0.189	0.250	0.047	1.321	92.4	3.902	02
18.00	1.83	0.92	3.42	2.01	48.70	1.80	1.07	0.76	0.325	0.643	0.216	0.250	0.059	1.513	92.2	3.889	02
20.00	1.88	1.08	3.75	2.17	48.70	1.99	1.19	0.84	0.398	0.711	0.289	0.250	0.071	1.719	92.1	3.869	02

PART II -- THE DATA BASETHE DATA BASE

The first block of data read by the programs forms the data base for the execution of design and evaluation tasks. The data base is a group of cards (records) divided into two sections. The first section, the core catalog, contains information on the magnetic cores and includes catalog numbers, dimensional data, relative permeability and loss coefficient information. The second section consists of a table of wire data containing the cross-sectional area and resistivity information on the available sizes of magnet wire. Usually, once the data base has been constructed, the information in it will not be changed often. Thus, it may be advantageous to store the data base on magnetic disk or tape. Additions to the core catalog or the wire table may be made at any time without having to construct an entirely new data base.

THE CORE CATALOG

The core catalog cards list the necessary data on the magnetic cores and are the first cards read by the program. The core catalog cards are ordered as shown in Figure 31.

6.1 HEADING CARDS

The first two cards in the core catalog are used to generate headings for the output. They are the Title Card and the Manufacturers' Names Card.

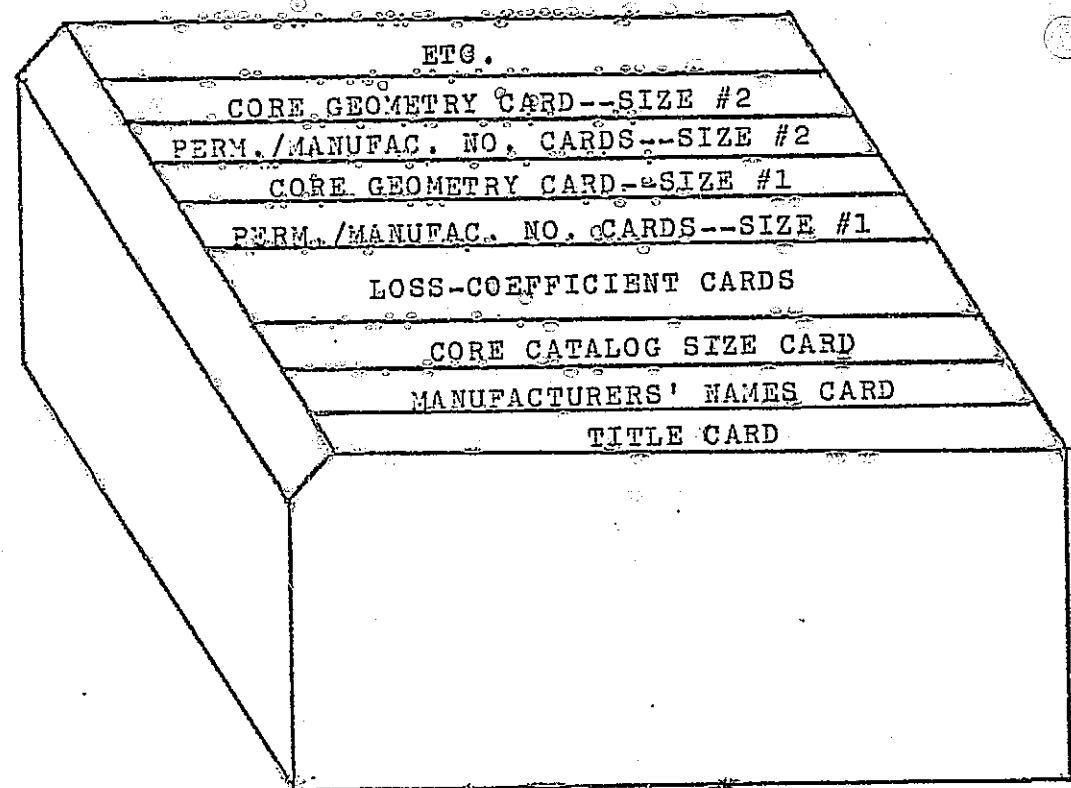


Figure 31. Order of the Core Catalog Cards

6.1.1 Title Card

The Title Card is read as a block of twenty consecutive A4 formats to provide for a user specified title up to eighty characters in length. It may be used to list identifying information such as manufacturers' names, date of catalog and etc. This information is used as a heading for the catalog list (see Section 3.1.2). A sample Title Card is shown in Figure 32.

6.1.2 Manufacturers' Names Card

The Manufacturers' Names Card is read as two A10 formats. Thus, two manufacturers' names may be used, with ten spaces allocated for each name. This information is used to provide headings for the lists of manufacturers' core catalog numbers which appear on the output. A sample Manufacturers' Names Card is shown in Figure 34. Figure 33 shows the format of the card.

6.2 CORE CATALOG SIZE CARD

The Core Catalog Size Card is read as two I5 formats. Columns 1-5 give the number of core sizes available and columns 6-10 give the number of relative permeability values available. (see Figure 35). These numbers are read in as integers and must be right justified. The catalog may contain up to forty core sizes and up to fifteen values of relative permeability. A sample Core Catalog Size Card is shown in Figure 36.

115

Figure 32. Example: Title Card

Figure 33. Manufacturers' Names Card

Figure 34. Example: Manufacturers' Names Card

Figure 35. Core Catalog Size Card

32 14

Figure 36. Example: Core Catalog Size Card

6.3 LOSS-COEFFICIENT CARDS

Core losses are estimated in the program by the use of Legg's equation [2]. One Loss-Coefficient Card should be used for each value of relative permeability in the core catalog. These cards should be arranged in order from lowest to highest value of relative permeability. Loss-Coefficient Cards are formated as follows (see also Figure 37). Figure 38 shows a sample Loss-Coeffiecint Card.

<u>COLUMNS</u>	<u>FORMAT</u>	<u>PARAMETER</u>
1-5	F5.0	Relative Permeability
6-15	E10.3	Eddy Current Loss Coefficient
16-25	E10.3	Hysteresis Loss Coefficient
26-35	E10.3	Residual Loss Coefficient

6.4 PERMEABILITY/CORE GEOMETRY CARDS

The Permeability/Core Geometry Cards consist of a subgroup of cards for each core size and relate the size number and relative permeability of a core to its specific catalog number(s) and actual dimensions. As a general rule, core manufacturers supply cores of several sizes and a core of a given size may be available in different values of relative permeability.

Figure 37. Loss-Coefficient Card

230. 37.0E-9 1.2E-6 2.60E-6

Figure 38. Example: Loss-Coefficient Card

Thus, in the instructions that follow, the "core size number" will uniquely identify a set of core dimensions and the pair (core size number, relative permeability) will uniquely identify one particular core. In order for the program to work most effectively, it is assumed that the core sizes are ordered by assending volume: i.e. the volume of core size number n is less than that of core size number n+1. If this assumption is violated when assembling the catalog, all designs generated will be valid. However, some possible design of lower size and mass may be "overlooked." Because the integer core size number is assigned by the program, new core sizes may be added to the catalog at any time. However, these additions should be made so as to maintain the ordering by volume of the core sizes. Presently, both programs DC1DC and DC2DC will allow up to forty core sizes and up to fifteen values of relative permeability. Thus, the core catalog may contain up to six hundred cores with each core being identified by up to two numbers from manufacturers' catalogs or other identifiers. The Permeability/ Manufacturers' Numbers Card(s) and the Core Geometry Card give complete information on each core.

6.4.1 Permeability/Manufacturers' Numbers Card(s)

For a given core size, the Permeability/Manufacturers' Numbers Card(s) list the available values of relative permeability and their respective manufacturers' catalog numbers. The format of these cards is 4(F3.0,4A4). This format allows the user to list four cores on a single card with three spaces for the

relative permeability and two groups of eight spaces for numbers from manufacturers' catalogs or other identifiers. The manufacturers' catalog numbers should be listed in the same order as the names on the Manufacturers' Names Card. Continue listing cores in the same fashion, using as many cards as needed, until all the cores for a particular core size have been listed. On the last card used, place a "1" in column 80 to indicate the end of the listing for that core size and that a Core Geometry Card is to be read next. The Permeability/Manufacturers' Numbers Card is formated as shown in the table below (see also Figure 39). A sample Permeability/Manufacturers' Numbers Card is shown in Figure 40.

<u>COLUMN</u>	<u>FORMAT</u>	<u>PARAMETER</u>
1-3	F3.0	Relative Permeability--Core A
4-11	A8	Catalog Number--Manufacturer 1
12-19	A8	Catalog Number--Manufacturer 2
20-22	F3.0	Relative Permeability--Core B
23-30	A8	Catalog Number--Manufacturer 1
31-38	A8	Catalog Number--Manufacturer 2
39-41	F3.0	Relative Permeability--Core C
42-49	A8	Catalog Number--Manufacturer 1
50-57	A8	Catalog Number--Manufacturer 2
58-60	F3.0	Relative Permeability--Core D
61-68	A8	Catalog Number--Manufacturer 1
69-76	A8	Catalog Number--Manufacturer 2

Figure 39. Permeability/Manufacturer's Numbers Card

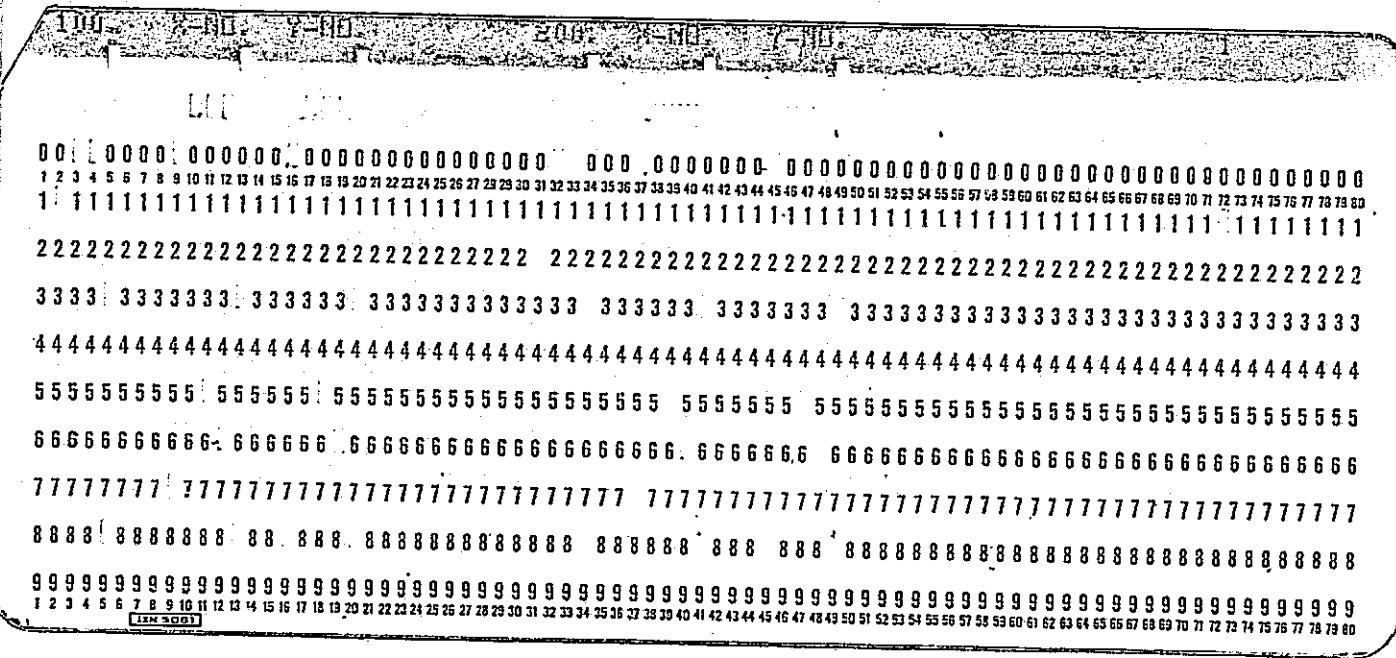


Figure 40. Example: Permeability/Manufacturers' Numbers Card

6.4.2 Core Geometry Card

A Core Geometry Card immediately follows the Permeability/ Manufacturers' Numbers Card(s) for each core size and gives the core cross-sectional area, mean magnetic path length, window area, length/turn of wire, height, and mass of the core size. These parameters are usually readily found in manufacturers' core catalogs. The length/turn of wire is usually given assuming a 40% winding factor. The format of the Core Geometry Card is as follows (see also Figure 41). A sample Core Geometry Card is shown in Figure 42.

<u>COLUMN</u>	<u>FORMAT</u>	<u>PARAMETER</u>
1-10	E10.3	Core Cross-Sectional Area (m^2)
11-20	E10.3	Mean Magnetic Path Length (m)
21-30	E10.3	Window Area (m^2)
31-40	E10.3	Length/Turn of Wire (m)
41-50	E10.3	Height (m)
51-60	E10.3	Mass (kg)

Figure 41. Core Geometry Card

8.85E-5 1.06E-2 2.923E-5 1.02E-3 3.30E-3 3.50E-4

Figure 42. Example: Core Geometry Card

6.5 ASSEMBLING THE CORE CATALOG

As shown in Figure 31, the Core Catalog Cards should be arranged as follows:

1. Title Card--one card containing any desired information.
 2. Manufacturers' Names Card--one card containing the names of up to two manufacturers.
 3. Core Catalog Size Card--one card giving the number of core sizes and the number of values of relative permeability in the catalog.
 4. Loss-Coefficient Cards--one card for each value of relative permeability in the catalog listing loss coefficients.
 5. Permeability/Manufacturers' Names Card(s)--for Core Size #1 (smallest volume).
 6. Core Geometry Card--one card giving the dimensions of core size #1.
 7. Permeability/Manufacturers' Names Card(s)--for Core Size #2 (next to smallest volume).
 8. Core Geometry Card--one card giving the dimensions of core size #2.

Permeability/Manufacturers' Names Card(s)--for Core Size #n (largest volume).

Core Geometry Card--one card giving the dimensions of core size #n.

THE WIRE TABLE

The Wire Table immediately follows the core catalog cards. The first card in the wire table is in a (I2,1x,I2) format. The first variable gives the largest wire size (smallest AWG number) and the second variable gives the smallest wire size (largest AWG number). The format of this Wire Table Size Card is shown in Figure 43. A sample Wire Table Size Card is shown in Figure 44.

The remaining cards in the Wire Table give the cross-sectional area and resistivity of each wire size. These Wire Data Cards should be arranged in order of increasing AWG number (decreasing wire cross-sectional area). One Wire Data Card should be used for each wire size. The format of the Wire Data Cards is shown in the table below (see also Figure 45). A sample Wire Data Card is shown in Figure 46.

<u>COLUMNS</u>	<u>FORMAT</u>	<u>PARAMETER</u>
1-12	E12.5	Area of Bare Wire (m^2)
13-24	E12.5	Area of Single Coated Wire (m^2)
25-36	E12.5	Area of Double Coated Wire (m^2)
37-48	E12.5	Area of Triple Coated Wire (m^2)
49-60	E12.5	Area of Quad Coated Wire (m^2)
61-72	E12.5	Resistivity of Wire Size (ohms/meter)

If a wire size is not available in a particular coating, indicate this by entering zero (or blank) for the cross-sectional area of the unavailable wire type. This insures that the unavailable wire type will not be chosen for a design.

Figure 43. Wire Table Size Card

Figure 44. Example: Wire Table Size Card

Figure 45. Wire Data Card

Figure 46. Example: Wire Data Card

PROGRAM INSTALLATION INSTRUCTIONS

Programs DC1DC and DC2DC described in this user's manual are written in FORTRAN IV and have been used on an IBM 370 model 165 operating under the control of the IBM Operating System Multiprogramming with a Variable number of Tasks (OS MVT). The two programs DC1DC and DC2DC are separate, stand-alone programs, each with its own separate identical data base. Program DC1DC consists of approximately 1050 statements, while program DC2DC consists of approximately 1075 statements. The data base, consisting of magnetic core loss, permeability and dimensional data, occupies approximately 260 cards. The total core requirement to compile and produce an executable module, including arrays, is 250 K on the IBM system described above.

The programs read only from the card reader and write only to the line printer. The logical unit number for the card reader on the system for which the programs were developed is 1 (one); the line printer unit number is 3 (three). These input/output unit numbers must be adapted by appropriate job control language or the programs must be edited to conform to the conventions of the system on which the programs are to be installed.

The installer may wish to copy the data base cards to a disk or tape file and assign the corresponding logical unit number for the read operations associated with the data base. These data base reads occur only once during the program execution at the beginning of the program. The control cards which describe the design specifications and control operations must be read by the card reader.

APPENDIX

LIST OF SYMBOLS

The following symbols may appear on the program output:

<u>SYMBOL</u>	<u>MEANING</u>
AREA (or CORE AREA)	The cross-sectional area of the magnetic core (m^2).
AWG	Wire size given by AWG numbers. (Program DC1DC).
AWG PRI.	Wire Size of the primary winding (Program DC2DC).
AWG SEC.	Wire size of the secondary winding (Program DC2DC).
B MAX	The maximum allowable flux density, given in tesla.
B MIN	The minimum allowable flux density, given in tesla.
B RESIDUAL	The residual flux density of the core material, given in tesla.
CAP ESR	The effective series resistance of the capacitor (ohms).
CONV FREQ	The frequency of operation of the converter system (KHz).
CORE PATH LENGTH	The mean magnetic path length of the core (m).

<u>SYMBOL</u>	<u>MEANING</u>
DSN MODE	The mode of operation of the converter at the design point in the PO-VI plane. A "1" implies continuous conduction, a "2" implies discontinuous conduction (Program DC1DC).
EFF	The efficiency of the converter (%).
EFF/MASS	The efficiency of the converter divided by the mass of the reactor element, (%/KG).
HEIGHT	The height of the magnetic core (m).
IA	The minimum value of reactor current over a cycle (amperes) (Program DC1DC).
IAP	The value in amperes that the primary current takes on at the beginning of the transistor on-time (Program DC2DC).
IAS	The value in amperes that the secondary current takes on at the beginning of the transistor on-time (Program DC2DC).
IB	The maximum value of reactor current over a cycle (amperes) (Program DC1DC).
IBP	The maximum value of primary current over a cycle (amperes) (Program DC2DC).
IBS	The maximum value of secondary current over a cycle (amperes) (Program DC2DC).

<u>SYMBOL</u>	<u>MEANING</u>
IB MAX	The maximum value that IB takes on over the design range of the converter. (Program DC1DC)
IBP MAX	The maximum value that IBP takes on over the design range of the converter. (Program DC2DC)
IBS MAX	The maximum value that IBS takes on over the design range of the converter. (Program DC2DC)
I COLL	Current in the collector of the transistor at which the saturation voltage was measured (amperes).
IC RMS	The RMS value of current in the capacitor (amperes).
IC RMS MAX	The maximum value that IC RMS takes on over the design range of the converter.
IND	The inductance of the single-winding reactor (mh) (Program DC1DC).
IP RMS	The RMS value of primary current (amperes) (Program DC2DC).
IS RMS	The RMS value of secondary current (amperes) (Program DC2DC).
IP RMS MAX	The maximum value that IP RMS takes on over the design range of the converter.

<u>SYMBOL</u>	<u>MEANING</u>
IS RMS MAX	The maximum value that IS RMS takes on over the design range of the converter (Program DC2DC).
IX AVE	The average value of the single-grounding neutral current over a cycle (Program DC1DC).
IX RMS	The RMS value of the single-grounding neutral current (Program DC1DC).
IX RMS MAX	The maximum value that IX RMS takes on over the design range of the converter (Program DC1DC).
MASS	The mass of the magnetic core (KG).
MAX CORES	The maximum allowable stack height.
N _T	Relative Permeability
N ₁	Number of turns of wire for the single-grounding reactor (Program DC1DC).
N ₂	Number of primary turns for the two-grounding reactor (Program DC2DC).
N ₃	Number of secondary turns for the two-grounding reactor (Program DC2DC).
OP MODE	Set if the converter operates in the continuous mmf mode over its option range, "2" otherwise.

<u>SYMBOL</u>	<u>MEANING</u>
P0	The output power (watts).
P OUT MIN	The minimum output power of the converter (watts).
P OUT MAX	The maximum output power of the converter (watts).
PRI. IND.	The inductance of the primary of the two-winding reactor (mh) (Program DC2DC).
PRI. WIRE LEN.	The length of wire used in the primary winding of the two-winding reactor (m) (Program DC2DC).
PRI. WIRE RES.	The resistance (ohms) of the primary winding of the two-winding reactor (Program DC2DC).
REACTOR AREA	The cross-sectional area of the magnetic material in the reactor (m^2).
REACTOR LENGTH/TURN	The length of wire per turn of the reactor, based on a 40% winding factor (m).
REACTOR MASS	The mass of the wound reactor (KG).
SEC. IND.	The inductance of the secondary of the two-winding reactor (mh) (Program DC2DC).

<u>SYMBOL</u>	<u>MEANING</u>
SEC. WIRE LEN.	The length of wire used in the secondary winding of the two-winding reactor (m) (Program DC2DC).
SEC. WIRE RES.	The resistance (ohms) of the secondary winding of the two-winding reactor (Program DC2DC).
STACK HEIGHT	The height in meters of the core stack.
T ON	The transistor on-time (μ sec).
T OFF	The transistor off-time (μ sec).
V DIODE	The diode forward drop (volts).
V IN	The input voltage (volts).
V IN MIN	The specified minimum input voltage (volts).
V IN MAX	The specified maximum input voltage (volts).
V OUT	The regulated converter output voltage (volts).
V SAT	The transistor saturation voltage (volts).
WIRE LENGTH	The length of wire used in the single-winding reactor (m) (Program DC1DC).

SYMBOLMEANING

WIRE RESISTANCE

The resistance (ohms) of the wire used in the winding of the single-winding reactor (Program DCIDC).

WN. AREA

The area of the window of the core (m^2).

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