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TRANSIENT HEAT TRANSFER COMPUTER CODE  
UTILIZING EIGENVECTORS AND EIGENVALUES  
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## CAVE3 — A General Transient Heat Transfer Computer Code Utilizing Eigenvectors and Eigenvalues

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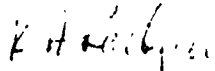
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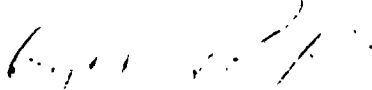
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Enclosed is a corrected copy of "CAVE3-A General Transient Heat Transfer Computer Code Utilizing Eigenvector and Eigenvalues". The previous copy of the report you received had an erroneous report and contract number printed on the cover. Please discard it and replace it with this corrected copy. Please accept our apologies for any inconveniences.

Sincerely,

GRUMMAN AEROSPACE CORPORATION

  
Dr. Kenneth A. Rathjen

  
Joseph V. Palmieri

Enc.

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## SUMMARY

This report describes a digital computer code CAVE3 (Conduction Analysis Via Eigenvalues for Three Dimensional Geometries) which provides a convenient and economical tool for predicting the transient temperature response of structures. This code is an extension of the work done under contract NAS1-13655 for two-dimensional geometries. CAVE3 is written in FORTRAN IV and is operational on both the IBM 370/165 and CDC 6600 computers.

The method of solution is a hybrid analytical-numerical technique which utilizes eigenvalues (thermal frequencies) and eigenvectors (thermal mode vectors). The method is inherently stable, permitting large time steps even with the best of conductors with the finest of mesh sizes, which can provide a factor-of-five reduction in machine time compared to conventional explicit finite difference methods when structures with small time constants are analyzed over long time periods. This code will find utility in analyzing hypersonic missile and aircraft structures which fall naturally into this class.

The code is a completely general one in that problems involving any geometry, boundary conditions and materials can be analyzed. This is made possible by requiring the user to establish the thermal network, e.g., node capacitances, conductances between nodes, etc. Dynamic storage allocation is used to minimize core storage requirements.

This report is primarily a user's manual for the CAVE3 code. Input and output formats are presented and explained. Sample problems are included which illustrate the usage of the code as well as establish the validity and accuracy of the method.

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Section 1

INTRODUCTION

The computer code CAVE3 (Conduction Analysis Via Eigenvalues for Three Dimensional Geometries) provides a convenient and economical tool for predicting the transient temperature response of structures. It will find special utility in the analysis of thermal protection systems for hypersonic missiles and aircraft where the flight trajectory time is large in comparison to the time constants of the structures.

The method employed by CAVE3 to solve the partial differential heat conduction equation is a hybrid analytical-numerical (HAN) technique which was developed under a previous NASA contract NAS1-13655 (Ref. 1).

Mr. James L. Hunt, of the High Speed Aerodynamics Division, Langley Research Center, Virginia, served as the NASA technical monitor for that program.

In the HAN method, spatial derivatives are replaced by appropriate finite difference representations and the temporal derivatives are retained as ordinary derivatives. In effect the problem is subdivided into a number of uniform temperature systems or nodes that are coupled and changing in temperature. The problem is thereby specified by a set of first order, linear, ordinary differential equations whose solution is expressed in terms of eigenvectors (thermal mode vectors for the system) and eigenvalues (thermal frequencies of the system). The complete solution for a system involving  $N$  nodes contains  $N$  eigenvalues and  $N$  eigenvectors. The determination of all  $N$  eigenvalues and eigenvectors involves formidable computations for typical heat transfer problems involving hundreds of nodes - however the accuracy requirements of most problems do not require the determination of all  $N$  eigenvalues and eigenvectors. In fact, a small number say 10 or so are sufficient when the heat flux response is contained in the first few thermal modes (characteristic of materials with high thermal diffusivity) or if the response for a large number of time increments is required, which is precisely the situation in predicting the temperatures throughout the flight trajectory of a hypersonic vehicle. A reduction by a factor of five in computer time can be expected over conventional explicit finite difference codes for typical flight trajectory analyses. The savings in computer time is due to the HAN method

being inherently stable and, therefore, permitting large time steps in comparison to an explicit algorithm.

This report is basically a user's manual for CAVE3. The next section discusses the overall operation and running of CAVE3 while Section 3 describes the input data format. Sections 4 and 5 present two sample problems provided by the contract monitor. These problems are used to illustrate the input data and output of CAVE3 and to establish the validity and accuracy of the code. Section 6 provides the programmer oriented documentation of CAVE3, i. e., list of subroutines, variables and logic diagrams.

Mr. Charles B. Johnson, of the High Speed Aerodynamics Division, Langley Research Center, Virginia, served as the NASA technical monitor for the program.

At Grumman, the contract was administered by the Advanced Development office, under Fred Berger, Manager of Advanced Development System Engineering. The Study Manager was Dr. Kenneth A. Rathjen. Mr. Joseph V. Palmieri developed much of the code and Mr. Michael J. Rossi developed the matrix routines.

## Section 2

### DESCRIPTION OF CAVE3 CODE OPERATION

This section provides an overview of the CAVE3 code capabilities, method of solution and input/output.

CAVE3 has been designed to be a completely general digital computer code for operation on the CDC 6600 and IBM 370/165 computers. Operation of CAVE3 requires the following type of information from the user:

- Initial temperatures of nodes
- Capacitance (mass times specific heat) of each node
- Conductance (and convection) links between nodes
- Radiation links between nodes
- Heat generated at a node
- Boundary conditions (e. g. adiabatic wall temperature or recovery temperature and convective heat transfer coefficient)
- Thermal properties as a function of temperature
- Initial and final time
- Time steps (which can be variable)

The user may assign any node numbering system desired; CAVE3 establishes a node labeling array that is packed to ensure efficient matrix operations. The input for CAVE3 has been designed to be totally generalized and options have been provided to minimize the amount of input. The data is structured in blocks and resides on one data file. A detailed description of the input is provided in Section 3.

The user, via input, establishes the overall core size available. CAVE3 dynamically allocates storage for the individual arrays based on the data input. In this fashion the user does not pay for excess overhead by executing a program designed for a large scale problem with fixed storage when running a smaller problem. The code is designed so that the data storage is set-up and maintained in the main program and the program flow is controlled by subroutine CAVE3. The program is modular in structure which aids the user to understand the logic and make changes if desired.

A description of each subroutine and its specific task, along with flow charts, is presented in Section 6.

The main advantage of CAVE3 over other general thermal analyzer codes is in execution time. CAVE3 will prove economical in solving transient heat conduction problems involving structures with time constants that are small compared to the time period of interest (e.g. flight trajectory). The method employed in CAVE3 is a hybrid analytical-numerical technique that is inherently stable permitting large time steps in comparison to explicit finite difference methods. It is noted that there is a significant amount of computer time required to determine the eigenvectors and eigenvalues of the solution, and therefore the method is not advantageous compared to conventional explicit schemes for problems involving a short time period (e.g. total time of interest on the order of 100 times the maximum permissible time step).

A detailed description of the method is presented in Ref. (1) and therefore only a brief overview is presented here. The transient heat conduction problem being solved is characterized by the following system of  $n$  first-order linear differential equations with constant coefficients

$$C_i \frac{dT_i}{dt} = \sum_j K_{ij} (T_j - T_i) + H_i (T_{AW,i} - T_i) + \dot{Q}_i \quad i = 1, n \quad \text{Eq. (1)}$$

where

- $C_i$  = thermal capacitance of node  $i$
- $K_{ij}$  = conductive coupling between nodes  $i$  and  $j$
- $T_i$  = temperature of node  $i$
- $T_j$  = temperature of node  $j$  which is adjacent to node  $i$
- $H_i$  = convective coupling between node  $i$  and the fluid (for interior nodes  $H_i = 0$ )
- $t$  = time
- $T_{AW,i}$  = adiabatic wall temperature of the fluid in contact with node  $i$
- $\dot{Q}_i$  = heat generated at node  $i$

There are  $n$  such coupled differential equations, one for each of the  $n$  nodes. It is noted that radiation between nodes is considered via a linearization process described in Appendix C of Ref. (1) which leads to modified conductive and/or convective couplings.

The system of equations given in Eq. (1) has the following exact solution for a particular time-subinterval (Appendix F of Ref. (1) gives the details):

$$T_i = T_{\infty i} + \sum_{j=1}^n c_{ij} \exp(\lambda_j t) \quad \text{Eq. (2)}$$

where

- $T_i$  = temperature at node i at time t seconds into the time subinterval
- $T_{\infty i}$  = steady-state temperature at node i for the particular time subinterval
- $c_{ij}$  = constants that depend on the  $T_{\infty i}$ , a set of eigenvectors of a matrix A, and the temperatures of the nodes at the start of the time subinterval
- $\lambda_j$  = the eigenvalues of a matrix A
- t = time into the particular time subinterval. If  $\tau$  represents the time in the flight trajectory, and if  $\tau_s$  and  $\tau_e$  represent the time at the start and end of a time subinterval, then the following relationships hold:

$$0 \leq t \leq \tau_e - \tau_s \text{ and } \tau = \tau_s + t \text{ for } \tau_s \leq t \leq \tau_e$$

A = symmetric matrix whose elements depend on the  $C_i$ ,  $K_{ij}$  and  $H_i$  of Eq. (1). (Refer to Appendixes A and F of Ref. (1).)

Considering a thermal network with n nodes, there are then n eigenvalues and eigenvectors to be determined and used in Eq. (2). Considerable machine time can be saved by calculating only those eigenvalues and eigenvectors that are "significant" or "dominant". This was noted very aptly by Maise and Rossi in NASA CR-2435 and used by them in the CAPE code for the inverse heat transfer problem of finding the boundary conditions given the temperature history, and it was used in Ref. (1). When the series in Eq. (2) is truncated to the "dominant" terms, we obtain:

$$T_i = T_{\infty i} + \sum_{j=1}^{ne} c_{ij} \exp(\lambda_j t) \quad \text{Eq. (3)}$$

where ne is a number substantially less than n. It represents the number of dominant eigenvalues and eigenvectors that will be found and utilized by the code. This is an input number decided upon by the user. Appendix A of Ref. (1) discusses the effect of ne on solution accuracy.

It may be interesting to digress for a moment to note that the usual thermal analyzers take equation (1) a step further and replace the ordinary derivative  $\frac{dT_i}{dt}$  with a finite difference approximation. Depending on the form of the approximation either an explicit or implicit algorithm is obtained. In the common explicit and implicit formulations, the  $T_i$ 's and  $T_j$ 's are taken to be constant during the time step interval. In the current HAN method, the ordinary derivative is retained and the  $T_i$ 's and  $T_j$ 's are treated as time-dependent variables in Eq. (1). This leads to a more accurate solution with no limitation on the time step from a stability standpoint. However, in solving Eq. (1), the HAN method treats the  $C_i$ ,  $K_{ij}$ ,  $H_i$  and  $T_{AW,i}$  as constants. This is necessary, as discussed in Appendix E of Ref. (1), for an eigenvalue solution to exist. The technique used within CAVE3 to handle variations in these parameters is to subdivide the total time interval (e.g., the flight trajectory) and take these parameters to be piecewise constant within each time subinterval.

Thus, the single problem of determining the temperature distribution in the structure where the boundary conditions are varying is solved by considering a number of subproblems where the boundary conditions are piecewise constant. These subproblems are interconnected in that the temperature at the end of one time subinterval becomes the initial temperature for the next time subinterval. It should be noted that the time subintervals, or time steps in the HAN method, are typically of the order of seconds or tens of seconds which is probably 100 to 1000 times larger than is permissible with the explicit method.

CAVE3 uses the convective coefficient and adiabatic wall temperatures at the beginning of the time interval for the entire time interval. Therefore in selecting the time subintervals, the user should be guided by the variation in the boundary conditions with particular concern for abrupt changes that affect the convective heating. For those problems in which the temperature dependency of the material properties plays a dominant role for some reason, or if radiation heat transfer is of great importance, a second run with smaller subintervals should be made to determine the effect of subinterval selection on the predicted temperatures.

The problem solution is accomplished in CAVE3 using the following sequence:

1. Storage requirements for the various arrays are determined and allocated.
2. Initial conditions are printed out.



Then for each time step the following are done:

3. Using the temperature distribution at the start of the time step, the thermal properties of the materials are determined, followed by the capacitances and conductances for the network. This step is not exercised if the material properties are independent of temperature.
4. The convective heat transfer and conduction couplings are then modified to account for radiation if it is being considered. Appendix C of Ref. (1) gives the details of the linearized treatment that is given to the radiation heat transfer.
5. Set up a matrix A in compact form which depends on the  $C_i$ ,  $K_{ij}$  and  $H_i$  of Eq. (1) (Refer to Appendix F of Ref. (1).)
6. Obtain the ne dominant eigenvectors and eigenvalues of matrix A using Jennings<sup>(2)</sup> method of simultaneous vector iteration.
7. Determine the steady-state solution to Eq. (1).
8. Calculate the  $c_{ij}$  of Eq. (3) for  $i = 1, 2, \dots, n$  and  $j = 1, 2, \dots, ne$ .
9. Calculate the temperatures of the nodes at the end of the time subinterval using Eq. (3).
10. Set the initial temperatures for the next time subinterval equal to the final temperature of the present subinterval. Increment time.
11. Print temperatures.
12. Repeat steps 3 through 11 until the final time has been reached. The solution is then completed.

The following sections describe in detail the input data format for CAVE3 and two sample problems which will enable the reader to use CAVE3.

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### Section 3

#### INPUT DATA FORMAT

The input to CAVE3 consists of one data file containing 3 control cards, 4 title cards and 9 distinct blocks of information. The unit input is general in that any set of consistent units can be used. The general format is displayed in Figure 3-1 and a more detailed set of descriptions is presented in Figure 3-2.

##### First Control Card:

This card consists of 11 variables describing the storage size, the degree of accuracy and the input output options. The variable NUMBND indicates the number of boundary nodes, NUMITR, the number of iterated nodes, NUMCON, the number of conductors, which includes conduction and convection links, NUMRAD, indicates the number of radiators, NUMNOD, the highest node number, NUMFLX, number of heat fluxes. These variables are used to determine the size of the data array. Care should be taken to minimize the size of each variable to truly represent the problem to be solved for excess size will cause a need for excessive core storage and increase the running time. Variable NSTR, is a storage parameter which indicates the size of the problem. The program will compute the value during execution and output the input value versus the computed value, thereby allowing the user to modify NSTR to the proper value. NEVALU is used to indicate the number of eigenvalues to be used to solve the problem. The higher the number of eigenvalues used the more accurate the solution and the longer the execution time. The user should investigate the proper size of NEVALU and minimize its size. Generally the smaller the size problem the smaller the number of eigenvalues needed to obtain the proper solution. IDIAG, is the diagnostic flag. If the user wants a more detailed output indicating the steady state solution at each time step and the dominant eigenvectors the user should set IDIAG equal to 1. Leaving IDIAG blank or setting it to 0 indicates the user wants only the temperature time history written out. IFLUX is also an output flag. If IFLUX is equal to one it indicates that the user wants the cumulative fluxes printed out for each node at each time step; a zero indicates no fluxes should be written out.

### Title Block:

The user can use four cards to describe the problem (four cards are required). The title block will be printed out in the output.

### Second Control Card:

This card consists of two variables KODE and NMTRIC. KODE should be left blank. NMTRIC is a flag indicating the units of input; 0 indicating degrees Fahrenheit; 1, degrees Rankine; 2, degrees Centigrade and 3, degrees Kelvin.

### Third Control Card:

This card consists of variables KODE, TIME, DTIME, FTIME, and SIG. KODE again should be left blank, TIME indicates the initial time, DTIME indicates the time step, FTIME, the final time and SIG the Stefan-Boltzmann constant. If SIG is left blank or set to zero it indicates that the Stefan-Boltzmann constant has been folded into the radiation couplings.

### Initial Temperature Block for Iterated Nodes:

This block of data establishes the initial temperature values for each of the iterated nodes. Variables II and JJ, the multiple parameter input are used to condense the input where the user numbering scheme allows. This Multiple Parameter Input option is explained at the end of this section.

### Temperature Block for Boundary and/or Specified Temperature Nodes:

This block of data consists of the temperature values of boundary nodes and/or nodes within the structure with specified temperatures. The multiple parameter input is available to minimize the input. These values can be made to vary with time by using the proper table format (discussed in Table Block).

### Capacitance Block

Within this block the node thermal capacitance (mass times specific heat) is stored in the CAP(N) array for each node N. Again the multiple parameter option is available.

### Conductance Block

The nodal conductance (and convection) values are contained in this block of data. The program requires a conductance sequence number N, the two node numbers I and J that are linked and the conductance value COND(N). The conductance value represents

an overall UA and therefore is associated with both conduction and convection links. Note the link need only be established in one direction i.e., if a conductor is input from node 6 to 12 it need not be listed again from 12 to 6.

#### Radiation Coupling Block

The radiation links are stored in this block of data. Similar to the conductance block, N represents the radiation sequence number, followed by I and J the node numbers connected by the radiation link, followed by the radiation coupling value. (As with the conductor links it should only be input once.) This value can contain the Stefan-Boltzmann constant or can be computed without it, but the SIG flag must indicate which option the user selected.

#### Heat Source Block

The heat source or sinks are stored in this block. The heat source sequence number (N) should be input followed by (I) the number of the node to which the source is applied and  $Q(I)$ , the heat source value.

#### Conductor Constant Block

This block contains the parameter  $A/\Delta X$ , the conductor constant. This parameter is used when adjusting the conductance to represent the effect of changing thermal properties. The symbol A represents the cross sectional area perpendicular to the flow of heat. The  $\Delta X$  term represents the distance from the node center to the node boundary. The parameter is stored as a function of the conductor number it is associated with (N). DIS1(N) represents the value of the constant associated with the node from which the conductance is emanating from. DIS2(N) represents the value of the constant associated with node to which the conductance is emanating to. Figure 3-3 is presented to demonstrate the computation of the conductance term and the geometric positions of variables A and  $\Delta X$ .

#### Table Block

The table format is simple and permits convenient manipulation. Tables are assigned consecutive table numbers according to their position in the input data array. Each table starts with a header card specifying the table dimensions, i.e., the number of values of the independent variable and the number of dependent variables, followed by a table index which indicates the type of table, and then an optional title. A list of table types and their descriptions are listed in Figure 3-2 in the Table Block section and explained below. The values of the independent variable are specified on the next

card. These values are listed consecutively, up to 7 per line as required. The dependent variables follow with all values of each variable being specified consecutively. The tables make no use of sequence numbers to identify variables or records. No blank record or delimiter is used at the end of a table; the next table or the 11100 record (to indicate the end of the table block) follows immediately.

The LFLAG index, as mentioned previously, is used to distinguish the use of each table. The table options are broken up in seven segments. The user has the option to vary: (1) the time step as a function of time (LFLAG equal to 1), (2) the boundary temperature with time ( $10000 < \text{LFLAG} < 20000$ ), (3) heat sources or sinks with time ( $20000 < \text{LFLAG} < 30000$ ), (4) conductance value versus temperature ( $30000 < \text{LFLAG} < 40000$ ), (5) conductance value versus time ( $40000 < \text{LFLAG} < 50000$ ), (6) capacitance value versus temperature ( $50000 < \text{LFLAG} < 60000$ ) and (7) thermal properties versus temperature (LFLAG = 99999). In all cases except the first and last, LFLAG also related the node number, or conductor number with the changing parameter it was associated with i.e., if node 99 was a boundary node and its temperature was a function of time the user would have input a value of 10099 for LFLAG indicating boundary temperature (node number 10099-10000) was changing with time and at every new time step a new value would be extracted from the table. If the user wants to adjust the time step he must input in the first table the desired time steps as a function of increment. Note the first time step is set by the initial input in control card 3. An example would be if the user input an initial DTIME equal to .001 and wanted it increased by .001 four times. The user would have put in the first table of his input a L1 = 4, L2 = 1, and LFLAG = 1 followed by a card with the increments 1., 2., 3., and 4., and finally a card with .002, .003, .004, and .005. The program would have understood this to mean the first time step should be .001, the second .002, the third .003, the fourth .004 and the fifth .005. The final LFLAG segment is used when conductivity and/or specific heat are changing with temperature. This option assumes the first dependent variable input in the table is specific heat and the second the conductivity. When this table option is activated an additional block of information has to be input. That is a node table number correspondence table. A value must be entered for each node whose property changes with time and the table number associated with the properties of that node. If all iterated node properties are represented by a single table (same material), the user can set the variable J1(1)=0 and J2(1)=table number. The program will then automatically assign the table number stored in J2(1) to all nodes.

Termination Card:

The last data entry must be a 11100, card indicating data termination.

First Control Card  
Title Block (4 cards)  
Second Control Card  
Third Control Card  
Initial Temperature Block for Iterated Nodes  
11100  
Temperature Block for Boundary and/or Fixed Temperature Nodes  
11100  
Capacitance Block  
11100  
Conductance Block  
11100  
Radiator Block  
11100  
Heat Source Block  
11100  
Conductor Constant Block  
11100  
Table Block  
11100  
Node/Table Information  
11100  
Termination

Figure 3-1. General Data Format

First Control Card (1015)

NUMBND = Number of boundary nodes  
NUMITR = Number of iterated nodes  
NUMCON = Number of conductors  
NUMRAD = Number of radiators  
NUMNOD = Highest node number  
NUMFLX = Number of fluxes  
NSTR = Storage parameter  
NEVALU = Number of eigenvalues  
IDIAG = Diagnostic flag (0, no diagnostic; 1, diagnostics)  
IFLUX = Flux option (0, fluxes not to be printed; 1, fluxes to be printed out)

Title Block

4 Title Cards (any format)

Second Control Card

KODE, NMTRIC (I5, 15X, I5)

KODE = 0 or blank  
NMTRIC = 0, input in degrees Fahrenheit  
= 1, input in degrees Rankine  
= 2, input in degrees Centigrade  
= 3, input in degrees Kelvin

**Figure 3-2. Detailed Input Description (Sheet 1 of 6)**

Third Control Card

KODE, TIME, DTIME, FTIME, SIG (15, 4E10.0)

- KODE = 0 or blank
- TIME = initial time
- DTIME = computing interval
- FTIME = end of computing time
- SIG = Stefan-Boltzmann constant

Values for the Stefan-Boltzmann constant, in various units are given in the following table. It should be noted that if a zero is input or no Stefan-Boltzmann constant is input the program assumes it will be included in the radiation links.

Stefan-Boltzmann Constants

$0.1714 \times 10^{-8}$	BTU/h. - sq. ft. - $^{\circ}\text{R}^4$
$5.673 \times 10^{-12}$	Watts/sq. cm. - $^{\circ}\text{K}^4$
$1.355 \times 10^{-12}$	Cal/sec - sq. cm. - $^{\circ}\text{K}^4$
$5.669 \times 10^{-5}$	ergs/sec - sq. cm. - $^{\circ}\text{K}^4$

Initial Temperature Block for Iterated Nodes

KODE, N, T(N), II, JJ (215, E10.0, 215)

11100 (15)

- KODE = 0 or blank
- N = node number
- T(N) = node initial temperature
- II = limit for multiple parameter input
- JJ = spacing for multiple parameter input

Figure 3-2. Detailed Input Description (Sheet 2 of 6)



Temperature Block for Boundary and/or Fixed Temperature Nodes

KODE, N, T (N), II, JJ (215, E10 0, 215)

11100 (15)

- KODE = 0 or blank
- N = node number
- T (N) = boundary node temperature
- II = limit for multiple parameter input
- JJ = spacing for multiple parameter input

Capacitance Block (for iterated nodes)

KODE, N, CAP (N), II, JJ (215, E10 0, 215)

11100 (15)

- KODE = 0 or blank
- N = node number
- CAP (N) = node capacitance (mass x specific heat)
- II = limit for multiple parameter input
- JJ = spacing for multiple parameter input

Conductance Block

KODE, N, I, J, COND (N), II, JJ (415, E10.0, 215)

11100 (15)

- KODE = 0 or blank
- N = conductance sequence number
- I = first connected node number
- J = second connected node number
- COND (N) = conductance value (overall UA)
- II = limit for multiple parameter input
- JJ = spacing for multiple parameter input

Figure 3-2. Detailed Input Description (Sheet 3 of 6)

Radiation Coupling Block

KODE, N, I, J, RAD(N), II, JJ (415, E10.0, 215)

11100 (15)

- KODE = 0 or blank
- N = radiation coupling sequence number
- I = first connected node number
- J = second connected node number
- RAD(N) = radiation coupling value (Stefan-Boltzmann constant must be input either in the second control card or in each value for radiators)
- II = limit for multiple parameter input
- JJ = spacing for multiple parameter input

Heat Source Block

KODE, N, I,  $\dot{Q}(I)$  (315, E10.0)

11100 (15)

- KODE = 0 or blank
- N = heat source sequence number
- I = number of node to which source is applied
- $\dot{Q}(I)$  = heat source value

Conductive Constant Block

KODE, N, DIS1 (N), DIS2 (N) (215, 2F15.5)

1110

- KODE = 0 or blank
- N = Conductor number constant is associated with
- DIS1 (N) = Constant  $\frac{A}{\Delta X}$  for conductor N associated with node NCOND (1, N)
- DIS2 (N) = Constant  $\frac{A}{\Delta X}$  for conductor N associated with node NCOND (2, N)

Figure 3-2. Detailed Input Description (Sheet 4 of 6)

Table Block

KODE, L1, L2, LFLAG, Title	(415, A60)
X(1), X(2), X(3), X(4), X(5), X(6), X(7)	(7E10.0)
X(8), . . . . X(L1)	(7E10.0)
Y1 (1), Y1 (2), Y1 (3), . . . . , Y1(7)	(7E10.0)
Y1(8) . . . . , Y1 (L1)	(7E10.0)
Y2(1), Y2(2), Y2(3), . . . . , Y2(7)	(7E10.0)
Y2(8), . . . . , Y2(L1)	(7E10.0)
.	
.	
.	
YL2(1), . . . . . , YL2(L1)	(7E10.0)

Repeat above cards for each table with no blank or additional records between tables. Tables are numbered consecutively starting with 1 by the program.

11100 (at end of table block only) (15)

KODE = 0, or blank  
 L1 = number of values of independent variable  
 L2 = number of dependent variables  
 LFLAG = index indicating type of table and node number associated with table

= 1	DTIME vs. TIME
> 10000:	Boundary Temperature vs. Time
< 20000	for node # = LFLAG - 10000
> 20000	Heat Sources vs. Time
< 30000	for node # = LFLAG - 20000
> 30000	Conductance vs. Temperature
< 40000	for node # = LFLAG - 30000
> 40000	Conductance vs. Time
< 50000	for node # = LFLAG - 40000
> 50000	Capacitance vs. Temperature
< 50000	for node # = LFLAG - 50000
= 99999	Variable Properties
	C <sub>p</sub> (T) 1st Table
	K (T) 2nd Table

Node Number vs. Table Number Block

KODE, (J1(I), J2(I), I = 1, 7)	15, 7(215)
.	
.	
.	
11100	

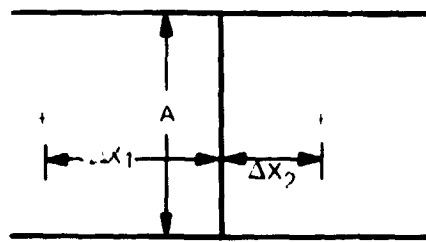
Figure 3-2. Detailed Input Description (Sheet 5 of 6)

KODE		0, or blank
J1(I)		Node number
J2(I)		Table number associated with node number J1(I)
IF J1(1)	=	0 indicates all nodes are associated with J2(1) (table number)

Termination Card

KODE = 11100 Job is terminated

Figure 3-2. Detailed Input Description (Sheet 6 of 6)



COND (N)

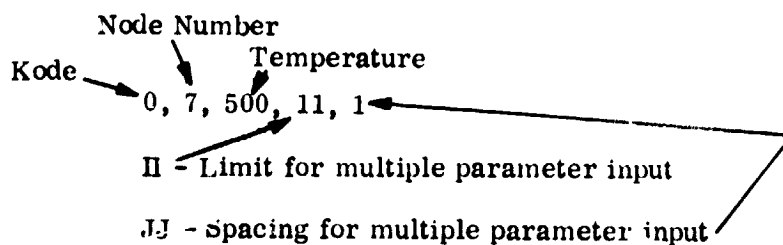


COND (N)	$\frac{\frac{K_1 A}{\Delta X_1} \times \frac{K_2 A}{\Delta X_2}}{\frac{K_1 A}{\Delta X_1} + \frac{K_2 A}{\Delta X_2}}$	$\frac{K_1 \text{ DIS1(N)} \times K_2 \text{ DIS2(N)}}{K_1 \text{ DIS1(N)} + K_2 \text{ DIS2(N)}}$
----------	--	--

Figure 3-3. Parameter A/  $\Delta X$

### Multiple Parameter Input

This option permits specification of the same value for a series of parameters, with a single data line. For temperatures or capacitances the node number is incremented by the spacing (JJ) until the limit (II) is reached. Each node so specified is assigned the same temperature or capacitance. An example follows showing an application of this feature in the Temperature Block.

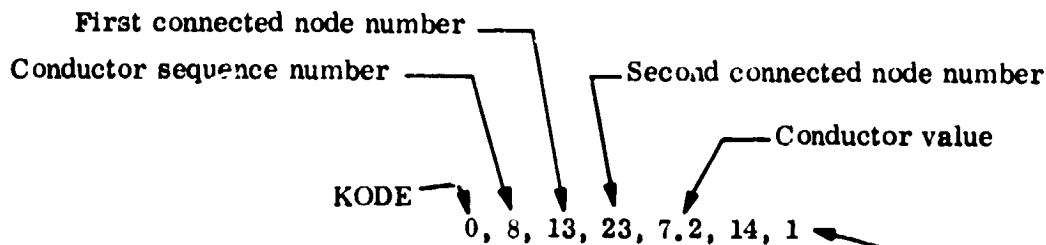


Equivalent to:

0, 7, 500,  
0, 8, 500,  
0, 9, 500,  
0, 10, 500,  
0, 11, 500,

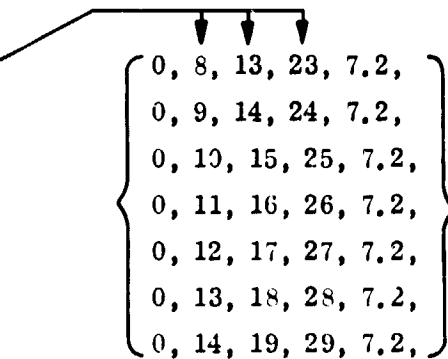
The node number in this case is increased by one to the limit 11, spaced by one.

For conductances or radiation couplings the feature is similar except that the parameter number (N) and the two node numbers (I and J) are incremented by the spacing until the parameter number reaches the limit value. Again the same value is assigned to each parameter. An example follows showing application of this feature in the Conductance Block.



This single card using Multiple Parameter Input is equivalent to the following seven cards.

NOTE: The conductor  
sequence no. , and both  
node numbers advance  
by JJ interval



0, 8, 13, 23, 7.2,  
0, 9, 14, 24, 7.2,  
0, 10, 15, 25, 7.2,  
0, 11, 16, 26, 7.2,  
0, 12, 17, 27, 7.2,  
0, 13, 18, 28, 7.2,  
0, 14, 19, 29, 7.2,

The conductor  
sequence number,  
the first node number  
and the second node  
number are incremented  
by 1 until the limit  
conductor is reached.

If the value of JJ (spacing) was 2, the equivalent would be:

0, 8, 13, 23, 7.2,  
0, 10, 15, 25, 7.2,  
0, 12, 17, 27, 7.2,  
0, 14, 19, 29, 7.2,

## Section 4

### SAMPLE PROBLEM NO. 1

The first sample problem provided by the Technical Monitor was a Lockalloy structure with a one inch diameter perturbation. The structure is depicted in Figure 4-1. As shown, it is horseshoe shaped and symmetric about axis A. The model for this structure is comprised of a number of rectangular and circular segmented nodes. It is three layers deep except for the perturbation. The node numbering scheme was provided by the Technical Monitor. Figure 4-2 shows the external boundary conditions and material properties. Note that the heat transfer coefficients vary near the rod. A math model was created representing the structure and is highlighted in Figure 4-3. The model contains 181 iterated nodes, 2 boundary nodes, 181 capacitances, 488 conductors, 60 radiators, 488 conductor constants, a table of physical properties versus temperature and a node/table correspondence block. The first data card is used to set the core allocation for the program; the values just mentioned and the requested 18 eigenvalues for this solution are shown on this card. This input data file was created and executed on the Grumman Cyber 173 computer. The solution is displayed in Figure 4-4. Note the output option taken in this problem was the briefest one (i. e., no heat fluxes, steady-state temperatures or eigenvalues). The initial conditions and the temperatures of each node at each time step were written out. This same problem was run using the Grumman Thermal Analyzer, which employs a forward difference technique. A comparison plot is presented in Figure 4-5. The solid symbols represent the CAVE results while the open symbols represent the thermal analyzer results. The comparison between the two techniques is excellent.



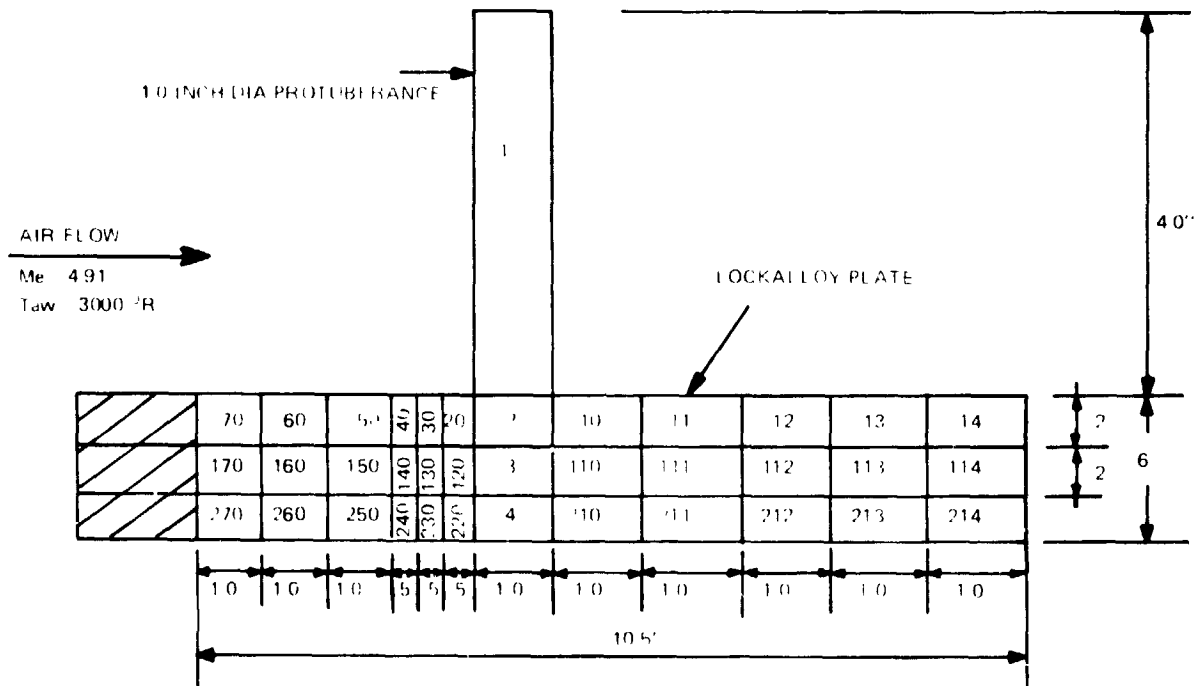
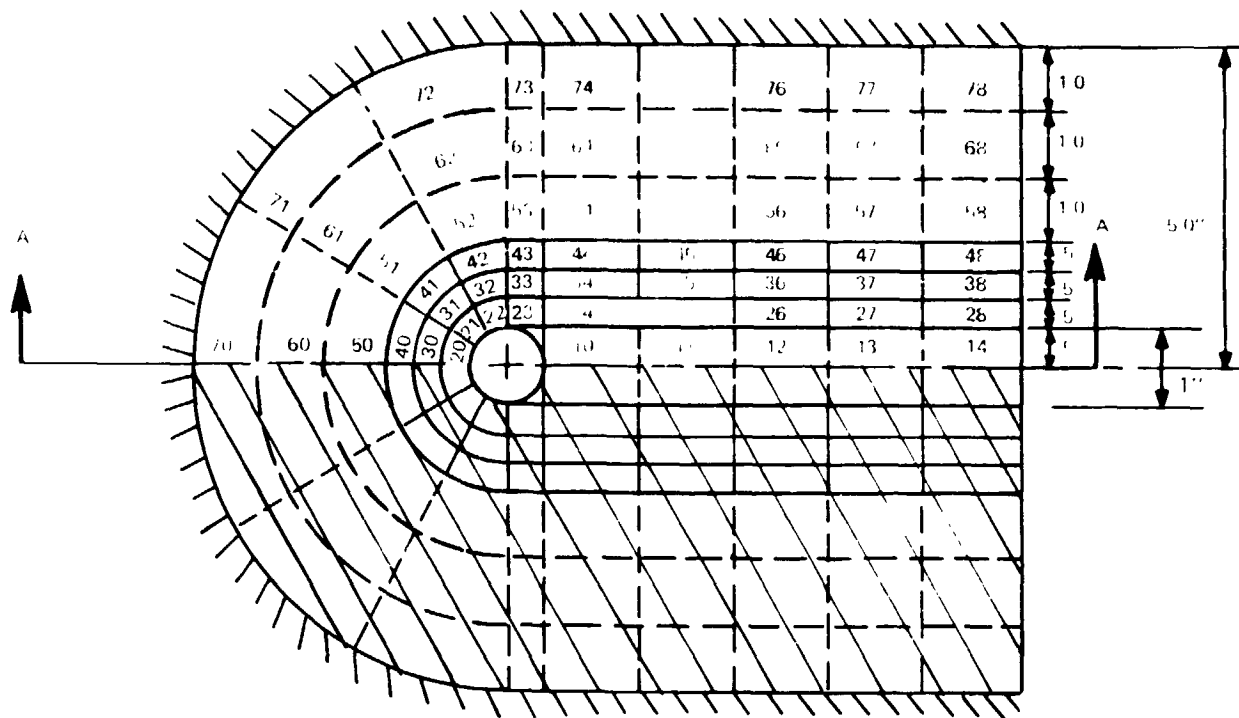


Figure 4-1. Sample Problem No. 1 Geometry Configuration

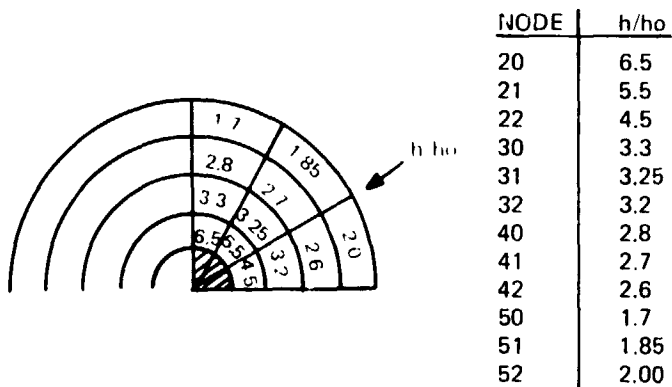
$T_{aw} = 3000^{\circ}R$   
 $T_{initial} = 960^{\circ}R$  (time = 0)  
 Start time = 0  
 Final time = 40 sec  
 Lockalloy Emissivity = 0.8  
 View Factor = 1.0  
 Background Temperature =  $519^{\circ}R$

Convection Nodes Surface: 10 to 14, 23 to 28, 33 to 38  
 43 to 48, 53 to 58, 60 to 68  
 and 70 to 78 have

$$h/h_o = 1.0$$

$$\text{where } h_o = 24.5 \text{ BTU/hr ft}^2 \text{ }^{\circ}R$$

The interference heating to the remaining surface nodes is listed below: (See NASA TND-1372)



Physical Properties

	$540^{\circ}R$	$860^{\circ}R$	$1060^{\circ}R$	$1260^{\circ}R$
$\rho$ (lbm/in <sup>3</sup> )	.0756	.0756	.0756	.0756
$C_p$ (Btu/lbm $^{\circ}R$ )	.395	.511	.548	.562
$K$ BTU/(HR FT <sup>2</sup> $^{\circ}R$ /FT)	123.0	99.5	89.0	81.5

Figure 4-2. Sample Problem No. 1 Boundary Conditions and Properties

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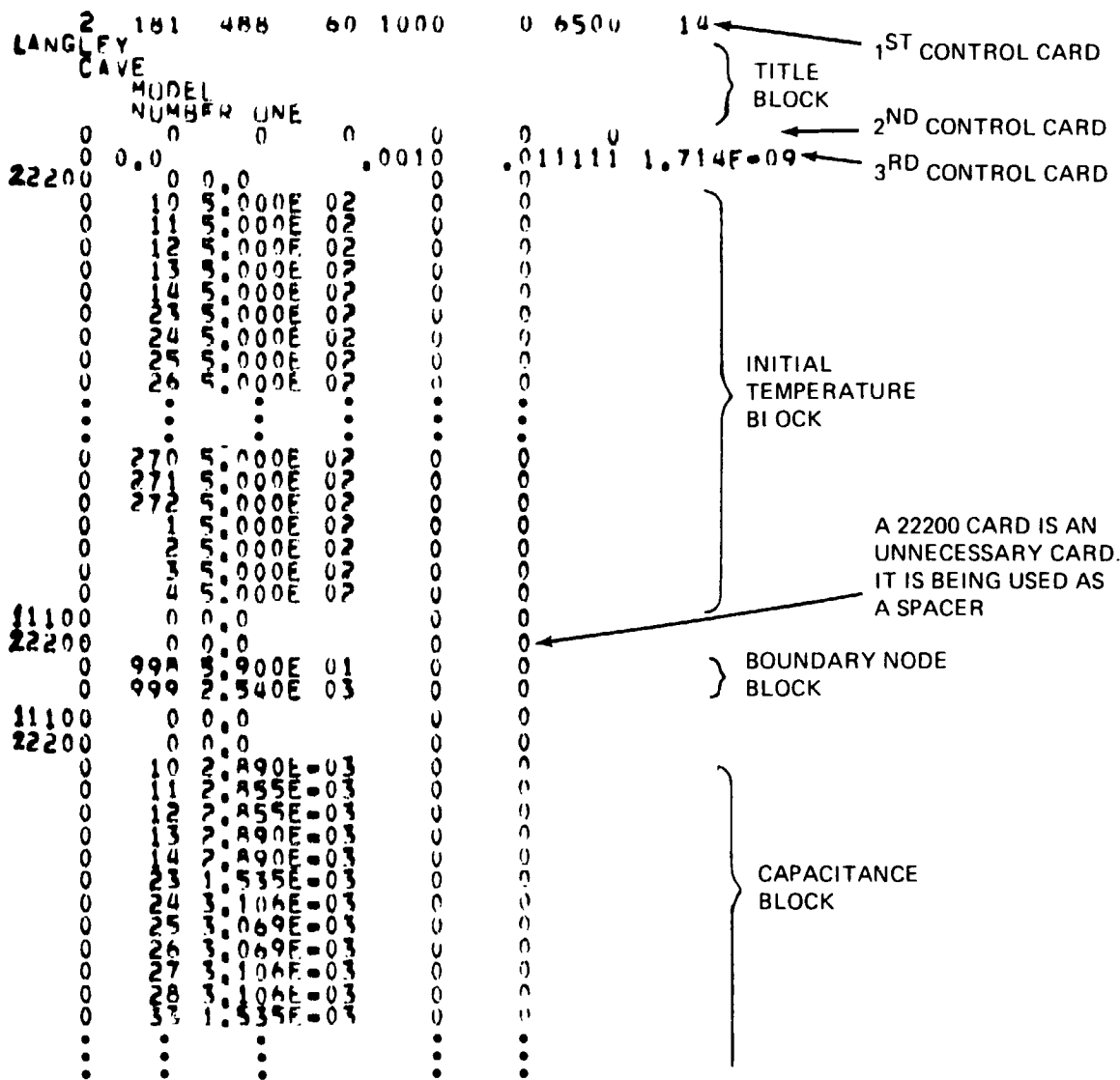


Figure 4-3. Input File for Sample Problem No. 1 (Sheet 1 of 3)



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41100 00000000  
 41100  
 22200

99A 99A 99A 99A 99A 99A  
 0 0 0 0 0 0

30  
 7.5  
 7.5  
 7.5  
 7.5  
 7.5  
 7.5

800  
 200  
 200  
 200  
 200  
 200  
 200  
 200

RADIATION BLOCK

NOTE ABSENCE OF HEAT SOURCE BLOCK  
 ==AHEAD==

679  
 679  
 679  
 679  
 200  
 7.850

CONDUCTANCE CONSTANT BLOCK

11100  
 0  
 10.25  
 0  
 0  
 0

299999  
 80  
 395  
 10.25  
 0  
 1 } NODE/TABLE BLOCK

TEMP VS PROPERTIES  
 400 600  
 511 548  
 6.29 7.42

800  
 562  
 6.79

5000 } TABLE BLOCK  
 59  
 6.0

11100 } TERMINATION  
 11100  
 11100  
 11100

Figure 4-3. Input File for Sample Problem No. 1 (Sheet 3 of 3)



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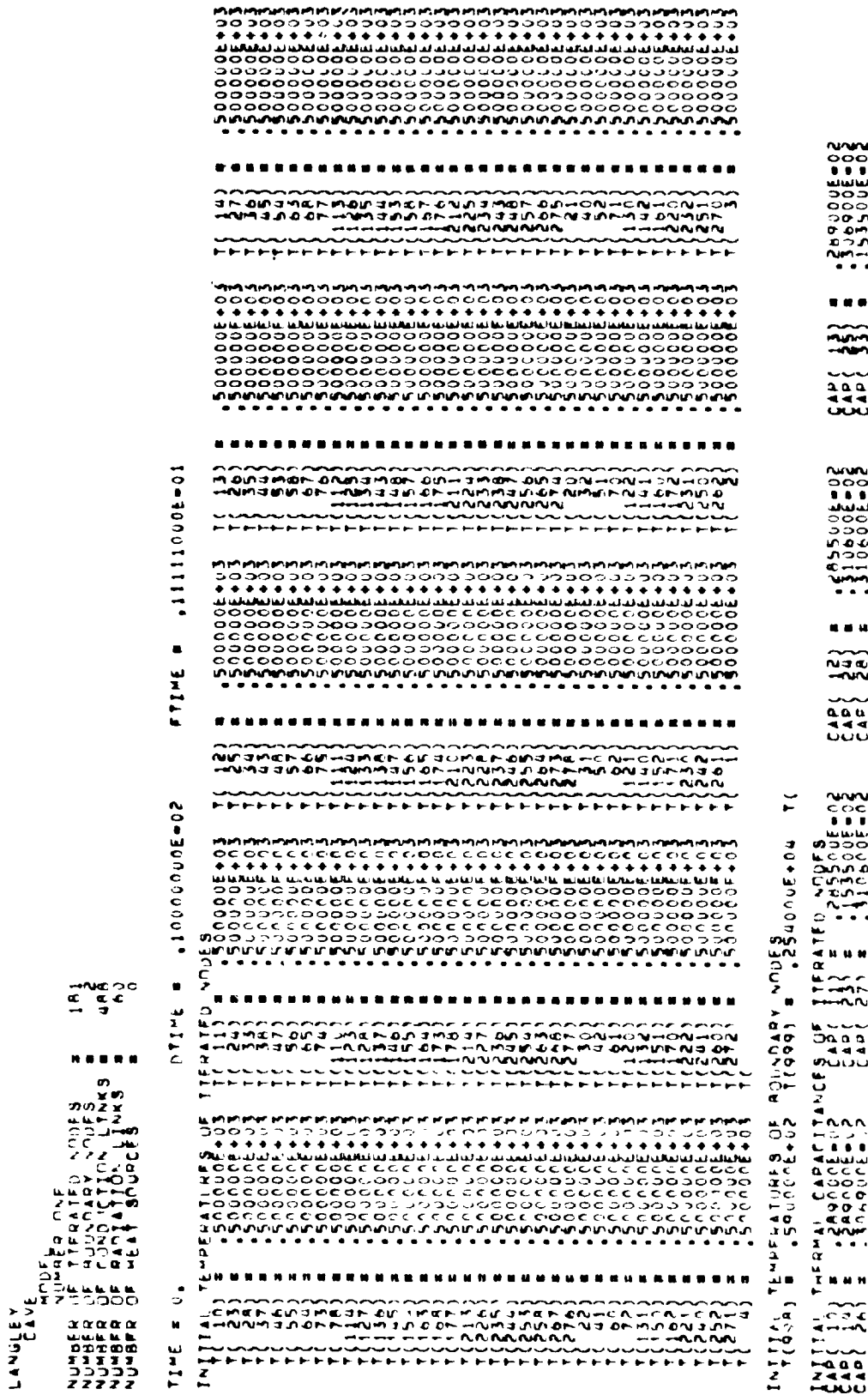


Figure 4-1. Output for Sample Problem No. 1 (Sheet 2 of 14)

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Figure 4-4. Output for Sample Problem No. 1 (Sheet 3 of 14)



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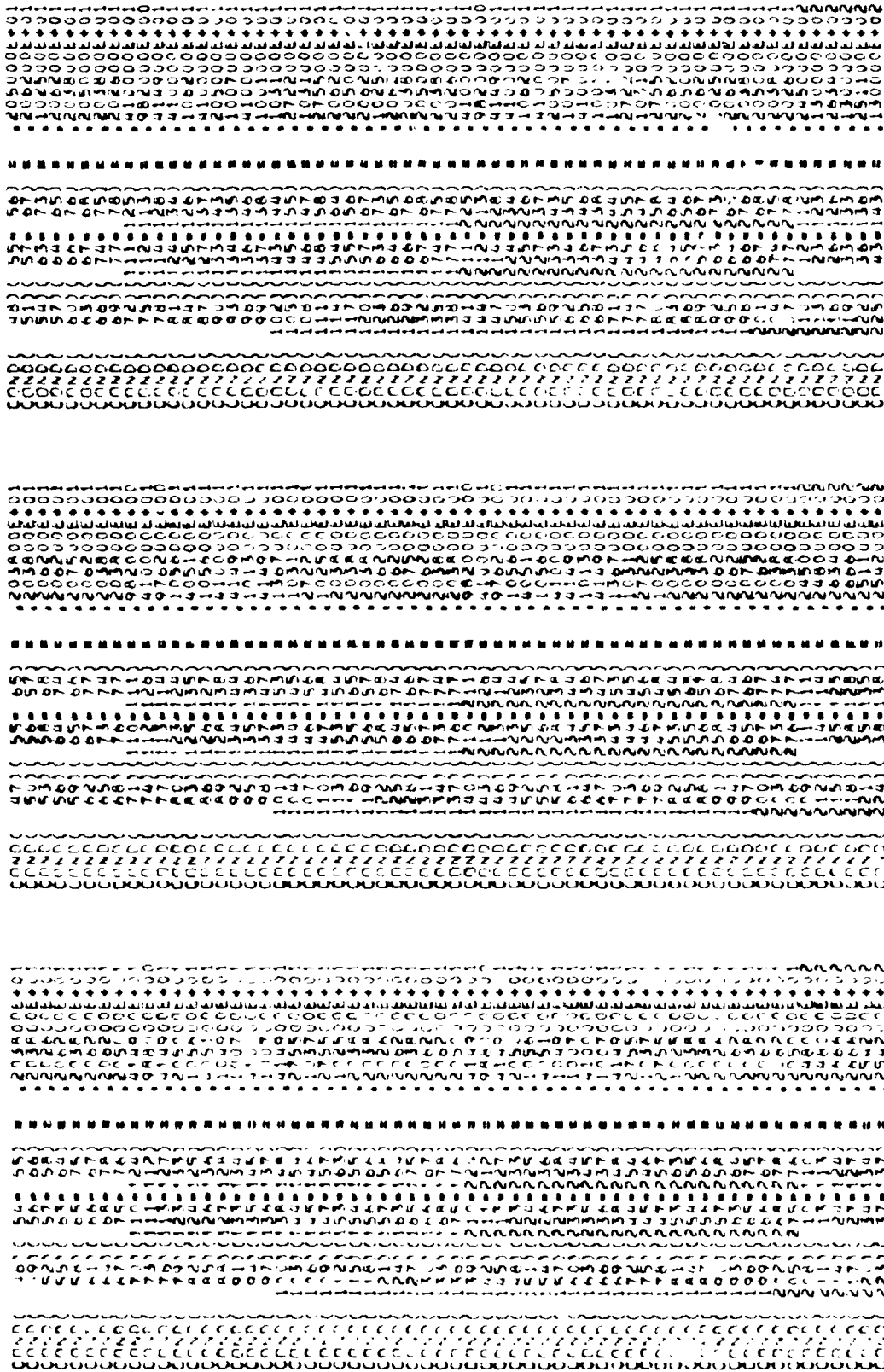


Figure 4-4. Output for Sample Problem No. 1 (Sheet 4 of 14)

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Figure 4-1. Output for Sample Problem No. 1 (Sheet 5 of 14)

# REPRODUCIBILITY OF THE ORIGINAL PAGE IS POOR

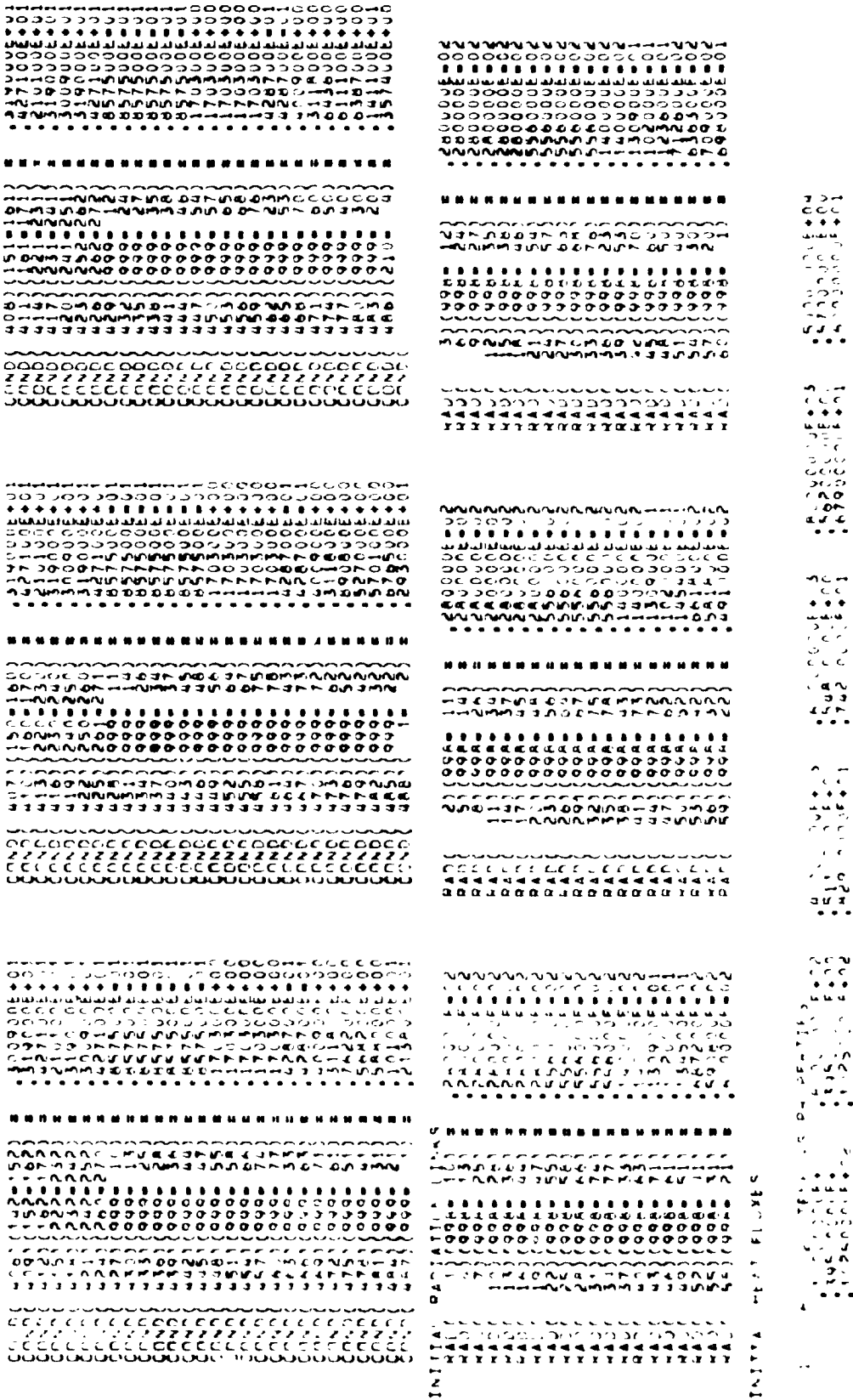


Figure 4-4. Output for Sample Problem No. 1 (Sheet 6 of 14)

REPRODUCTION OF ORIGINAL

RESERVED STORAGE IS 6500. REQUIRED IS 12. OCCURS  
MAXIMUM ITERATION 12 OCCURS

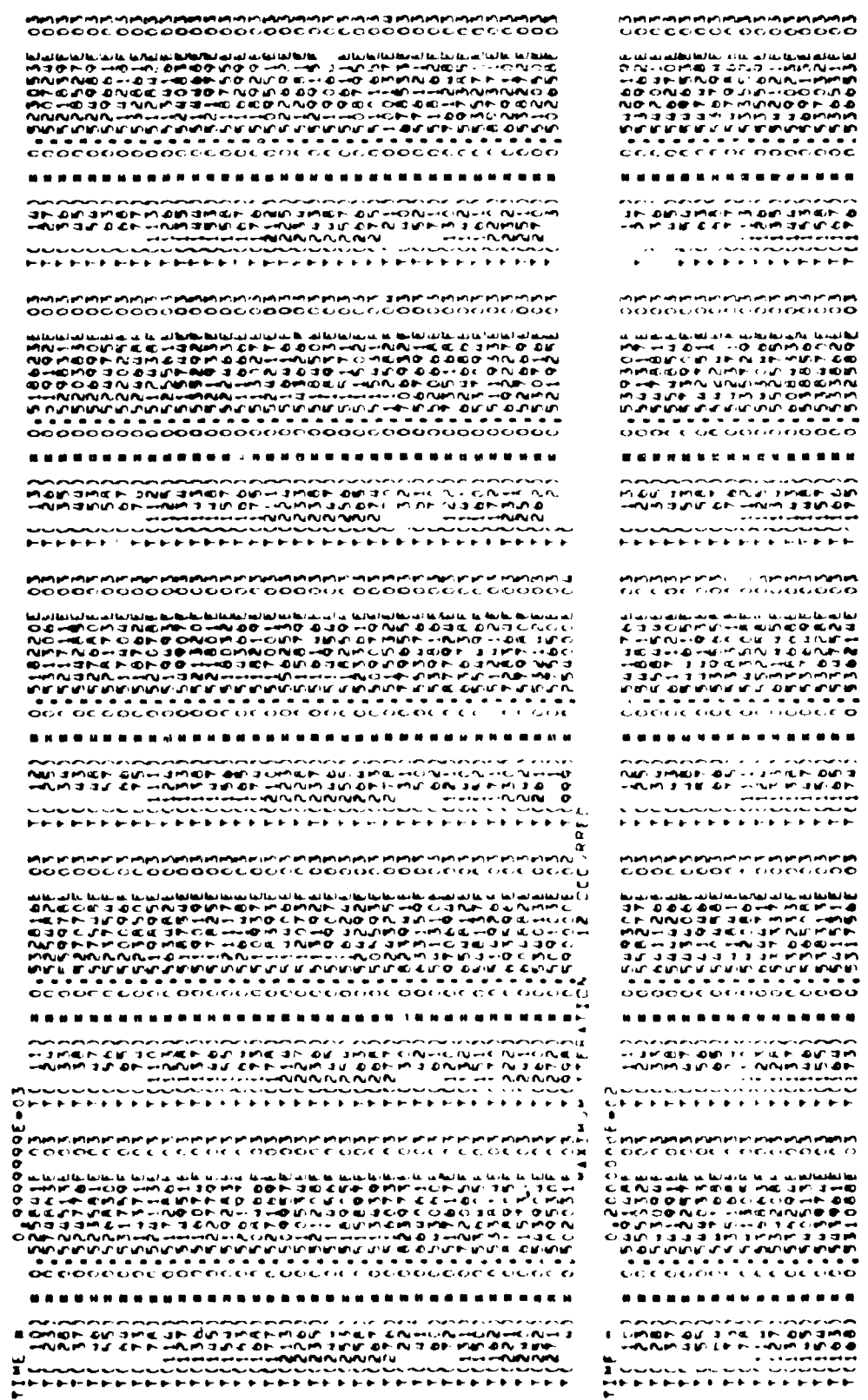


Figure 1-4. Output for Sample Problem No. 1 (Sheet 7 of 14)

REPRODUCIBILITY OF THE  
ORIGINAL PAGE IS POOR

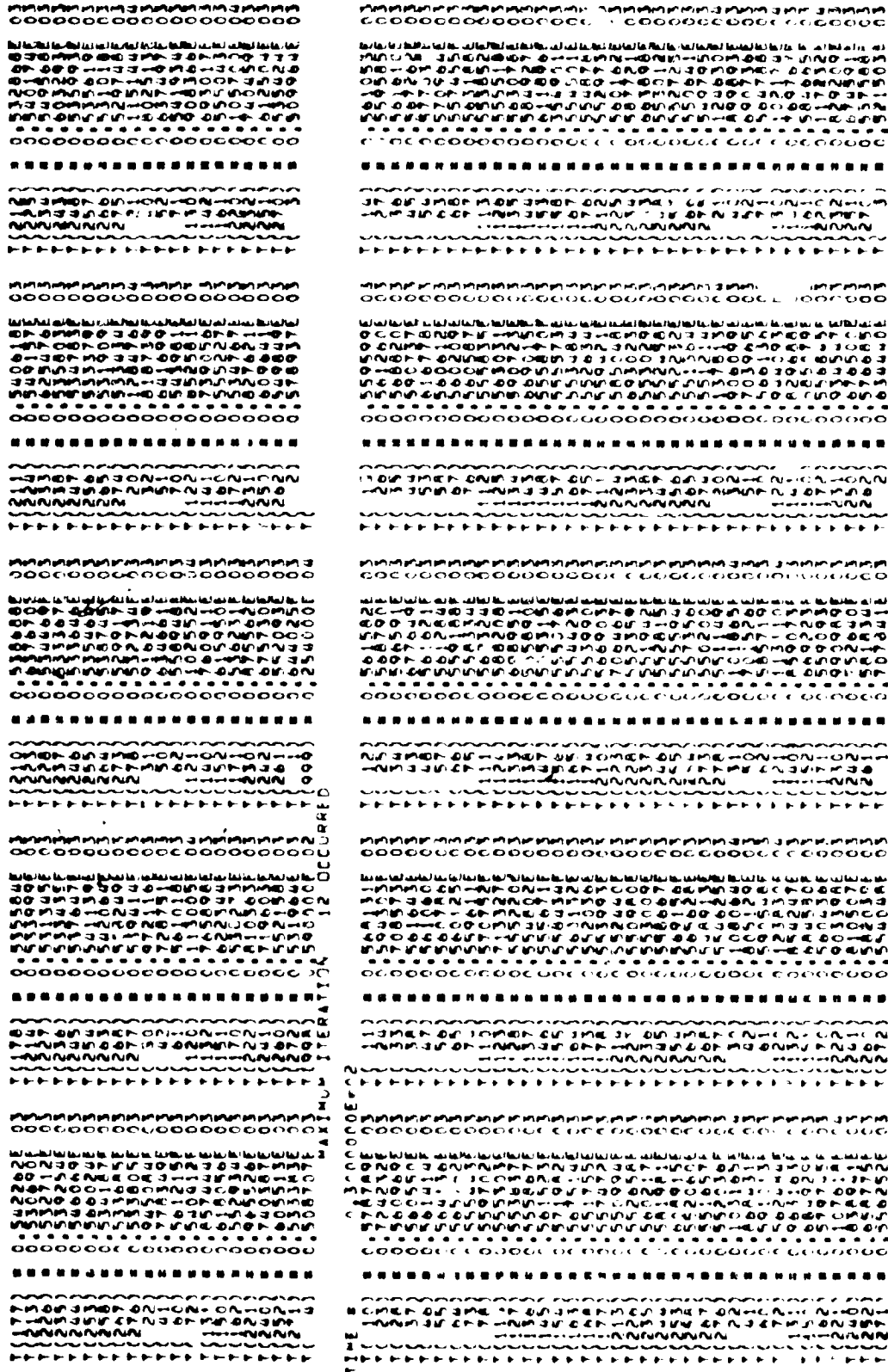


Figure 4-4. Output for Sample Problem No. 1 (Sheet 5 of 14)

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GENERAL PAGE IS POOR

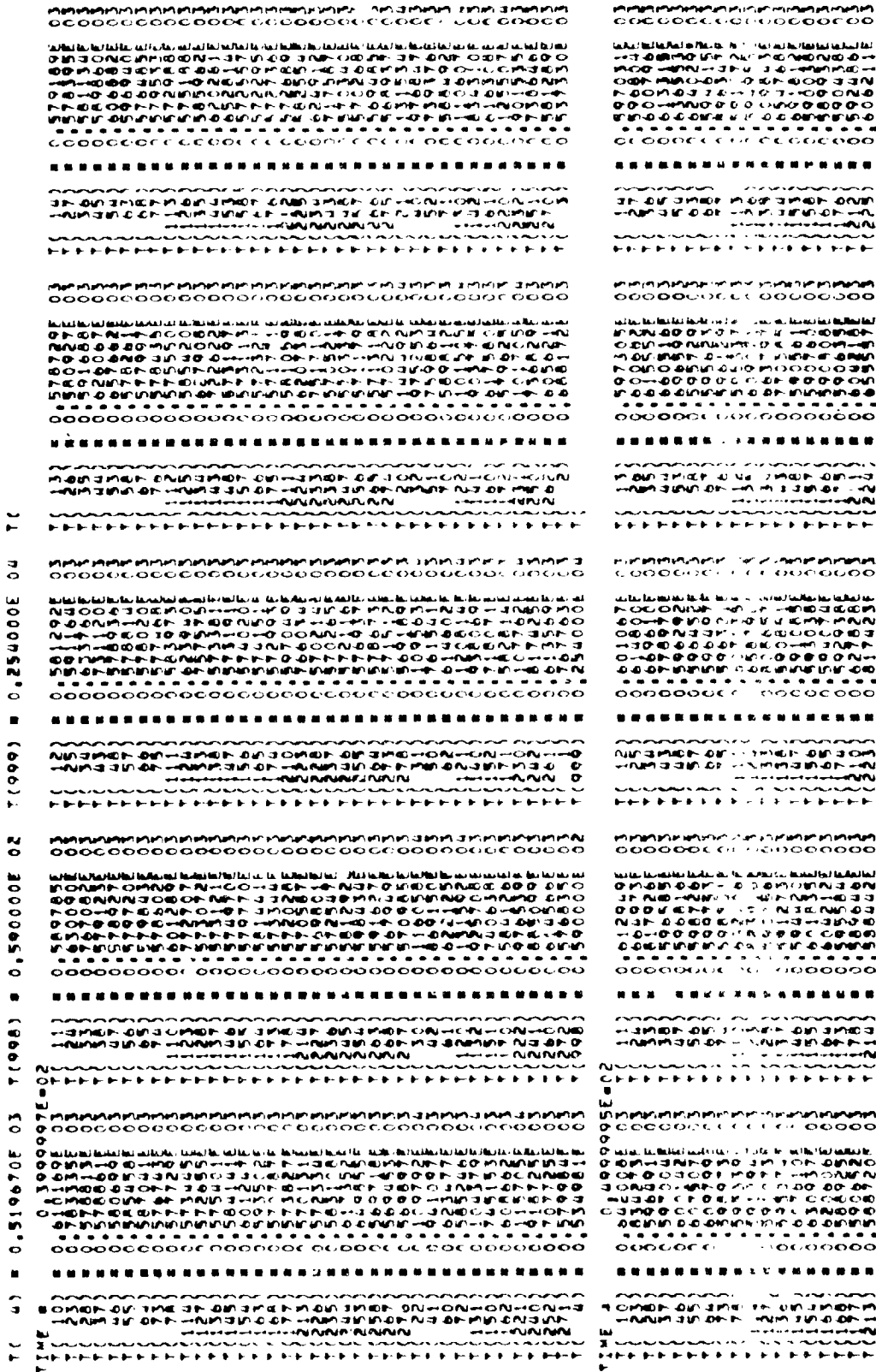


Figure 1-4. Output for Sample Problem No. 1 (Sheet 9 of 14)



Output for Sample Problem No. 1 (Sheet 11 of 14)

Figure 4-4. Output for Sample Problem No. 1 (Sheet 11 of 14)



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Figure 4-4. Output for Sample Problem No. 1 (Sheet 12 of 14)





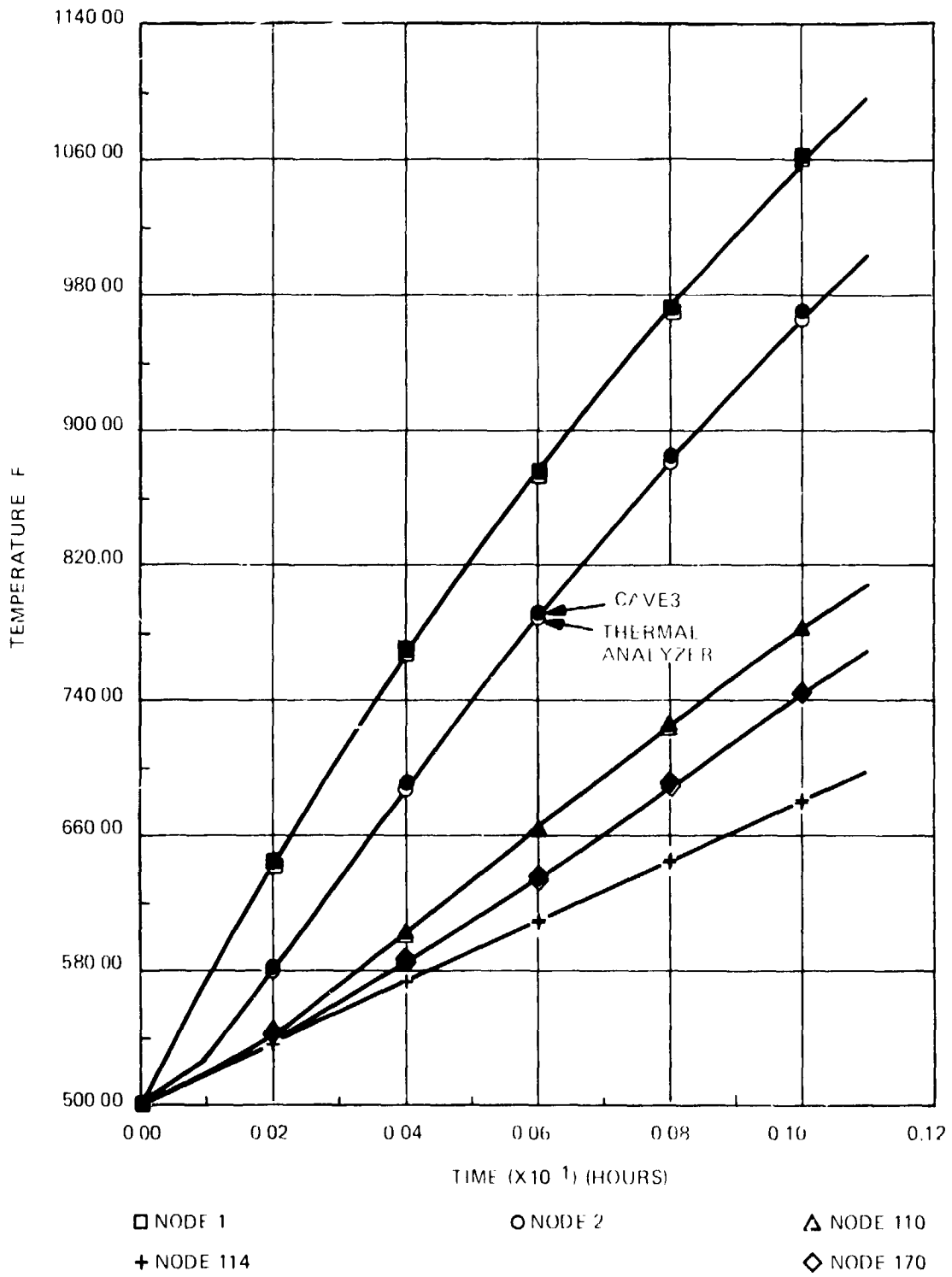


Figure 4-5. CAVE3 Model 1 Verification Plot

## Section 5

### SAMPLE PROBLEM NO. 2

Sample problem No. 2 is displayed in Figures 5-1 to 5-4; it is actually three problems. The first problem, or Model 2A, is a 160 node model (flat plate) exposed to the given top surface boundary conditions shown in Figure 5-1 and 5-3 with all other surfaces being adiabatic. The entire model is made of Lockalloy and its physical properties are displayed in Figure 5-4. The geometry and node breakdown are presented in Figure 5-1. The geometry consists of three distinct regions, A, B, and C. These regions represent areas of buildup for problems Model 2A & B and 2C. Model 2B is constructed by adding an additional Lockalloy layer under regions A and B. This creates a 256 node model, with Model 2A being the basic core. Model 2C is made up of Model 2B and an additional layer of Lockalloy under region A resulting in a 272 node model. Figure 5-2 depicts the nodal arrangement for each of the three models. Note that only the additions are represented, i.e., Model 2B uses the Model 2A numbering plus the layers shown for Model 2B. An input data set has been created for each of the models presented and is displayed in Figures 5, 6 and 7. The data format is essentially identical in each case, so a discussion of the Model 2A data input will be addressed while noting any differences in the remaining model input.

The first control card informs the program that the model consists of two boundary nodes, 160 iterated nodes, 444 conductors, 80 radiators, the highest node number is 1000 (actually 999 in the model), and 0 heat sources. Models 2B and 2C have increased the number of iterated nodes and conductors on this card. An estimate of reserved storage was made at 12500 words. This number is based on the data size and a user "feel" for its estimated size which comes with program use. It should be noted that the output displays the actual reserve storage needed and in this case it was 7269 words. Therefore the input value could have been less. The user also chose to use 14 eigenvalues and employed both the diagnostic option and the flux option. Models 2B and 2C used the default output option which displays only the initial conditions and the temperature time history. The user then input the desired title. Note four lines must be used. The example shows three lines of text and a blank line. On the second control card the user indicates the inputs are to be in degrees Fahrenheit. The third control card indicated an

initial time of zero, a time step of 0.01 and a final time of 0.1. The unit of time in this case is hours which is specified implicitly in the choice of units for thermal conductivity and radiation couplings. The Stephan-Boltzmann constant has also been included as an input which indicates that the values for the radiation couplings do not have this value folded into them. The 22200 is used as a comment card and in this case it is used as a separator. The next block encountered is the initial temperature block and indicates that all 160 nodes are initially at 500°F. The block is terminated by the 11100 card. Note in Figure 5-6 and 5-7 that the initial temperature block has been increased to 256 nodes and 272 nodes for Model 2B and Model 2C respectively. The boundary nodes 998 and 999 are displayed next at 2390°F and 59°F. This data is followed by the capacitance block (mass times specific heat) for each iterated node. Again note the additional capacitances listed for Models 2B and 2C. The conductance links are established next and represent an overall UA computation. Both conduction links (iterated node to iterated node) and convective links (iterated node to boundary node) are represented. The number of conductance links increased dramatically from model to model (444 to 695 to 727) due to the increase in the nodal definition. Note the use of the multiple parameter option in the conductance blocks of Model 2B and Model 2C to minimize the input. The user set-up conductance values for 48 conductors with just 5 lines of input (Figure 5-6). The radiation block follows with the first surface only represented (80 nodes) since it is the only surface exposed to the radiation boundary condition. This block is followed by the conductance constant block and represents the value of  $A/\Delta X$  for each iterated conductance link, i. e., all links not exposed to boundary nodes. The final 2 blocks deal with table descriptions. The first represents the change in specific heat and conductivity with temperature. Note the units in this case are °F and inches. The node/table correspondence uses this table to describe the property changes and relates table to node number. The final card entered is the termination card.

Figures 5-8 to 5-10 represent the resulting output for each of these three executions. Figure 5-8 is the output from the Model 2A run. It includes the output from the diagnostic and flux options. Figures 5-9 and 5-10 represent the default output which is the initial conditions plus the temperature time history of Model 2B and 2C. Referring to Figure 5-8 after the initial conditions are printed the program displays the steady state temperature solution followed by the eigenvectors for the number of dominant eigenvalues requested. The nodal temperatures and the cumulative heat flux from node to node at the end of the first time step are printed next. This process is repeated at each time step.

Finally, Figures 5-11 to 5-13 represent a comparison of the CAVE3 execution to a Ciumman Thermal Analyzer execution for these three models. The solid symbols represent CAVE3 and the open ones the Thermal Analyzer. Note the excellent agreement in all cases thus establishing the validity and accuracy of CAVE3.

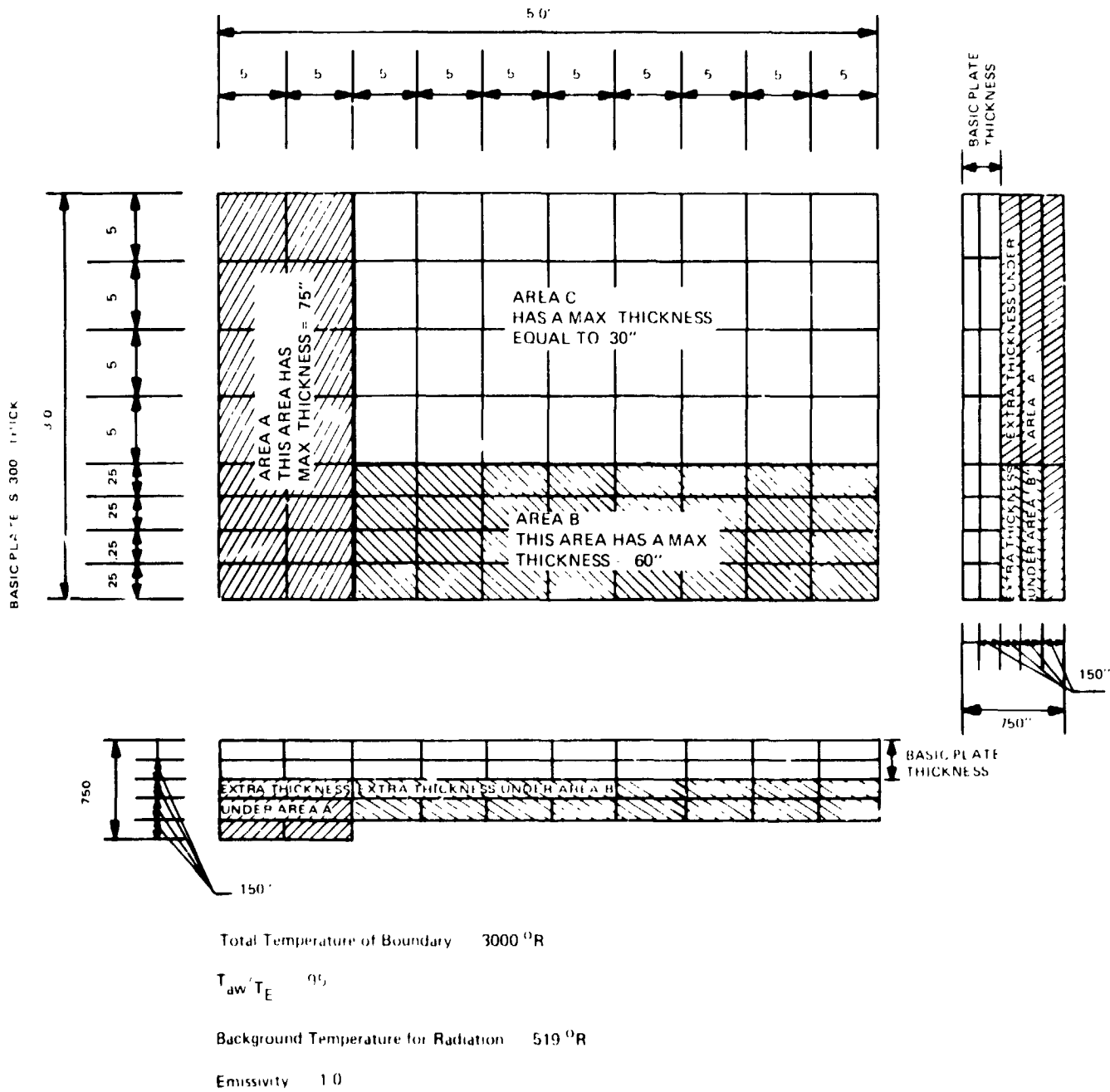


Figure 5-1. Sample Problem No. 2 Geometry Configuration



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MODEL 2A

71,151	72,152	73,153	74,154	75,155	76,156	77,157	78,158	79,159	80,160
61,141	62,142	63,143	64,144	65,145	66,146	67,147	68,148	69,149	70,150
51,131	52,132	53,133	54,134	55,135	56,136	57,137	58,138	59,139	60,140
41,121	42,122	43,123	44,124	45,125	46,126	47,127	48,128	49,129	50,130
31,111	32,112	33,113	34,114	35,115	36,116	37,117	38,118	39,119	40,120
21,101	22,102	23,103	24,104	25,105	26,106	27,107	28,108	29,109	30,110
11,91	12,92	13,93	14,94	15,95	16,96	17,97	18,98	19,99	20,100
1,81	2,82	3,83	4,84	5,85	6,86	7,87	8,88	9,89	10,90

MODEL 2B

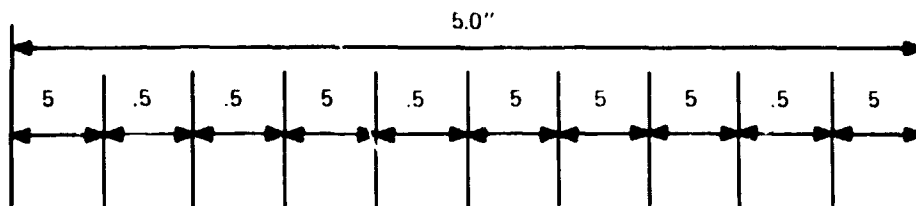
207,255	208,256								
205,253	206,254								
203,251	204,252								
201,249	202,250								
191,239	192,240	193,241	194,242	195,243	196,244	197,245	198,246	199,247	200,248
181,229	182,230	183,231	184,232	185,233	186,234	187,235	188,236	189,237	190,238
171,219	172,220	173,221	174,222	175,223	176,224	177,225	178,226	179,227	180,228
161,209	162,210	163,211	164,212	165,213	166,214	167,215	168,216	169,217	170,218

MODEL 2C

271	272
269	270
267	268
265	266
263	264
261	262
259	260
257	258

Figure 5-2. Sample Problem No. 2 Node Configuration

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SURFACE BLOCKS

$h_{ho}$	13	5	2	1	1	1	1	1	1
17	12	5	3	4	3	3	1	1	1
17	12	5	4	9	9	8	7	1	1
17	11	6	6	9	10	10	9	3	2
17	11	5	5	9	11	11	11	9	7
17	10	5	4	6	7	8	11	11	9
17	10	4	4	4	4	5	7	9	9
17	10	5	5	5	5	6	7	9	9


$$h_o = 13.2 \frac{\text{BTU}}{\text{ft}^2 \text{hr}^\circ\text{R}}$$

Figure 5-3. Sample Problem No. 2 Convective Heat Transfer Rates

	540 °R	860 °R	1060 °R	1260 °R
$\rho$ (lbm/in <sup>3</sup> )	0.756	0.756	0.756	0.756
$C_p$ (BTU/lbm °R)	395	511	548	562
$K$ $\frac{\text{BTU}}{\text{hr ft}^2 \text{R/ft}}$	123.0	99.5	89.0	81.5

Figure 5-4. Physical Properties of Lockalloy





LANGLEY	2	260	700	80	1000	015000	14
	MODEL	TWO	SECTION				
	RUN 2	SECTION					
222000	0.0	0	0	0	0	0	.1 1.714E-09
000000	1	0	0	0	0	0	
000000	2	0	0	0	0	0	
000000	3	0	0	0	0	0	
000000	4	0	0	0	0	0	
000000	5	0	0	0	0	0	
000000	6	0	0	0	0	0	
000000	7	0	0	0	0	0	
000000	8	0	0	0	0	0	
000000	9	0	0	0	0	0	
111000	0	0	0	0	0	0	
222000	999	0	0	0	0	0	
000000	0	0	0	0	0	0	
111000	999	0	0	0	0	0	
222000	0	0	0	0	0	0	
000000	1	7.311E-04	0	0	0	0	
000000	2	7.440E-04	0	0	0	0	
000000	3	7.568E-04	0	0	0	0	
000000	4	7.696E-04	0	0	0	0	
000000	5	7.824E-04	0	0	0	0	
000000	6	7.952E-04	0	0	0	0	
000000	7	8.080E-04	0	0	0	0	
000000	8	8.208E-04	0	0	0	0	
000000	9	8.336E-04	0	0	0	0	
000000	0	8.464E-04	0	0	0	0	
111000	0	0	0	0	0	0	
222000	0	0	0	0	0	0	
000000	1	1.110E-03	0	0	0	0	
000000	2	1.220E-03	0	0	0	0	
000000	3	1.330E-03	0	0	0	0	
000000	4	1.440E-03	0	0	0	0	
000000	5	1.550E-03	0	0	0	0	
000000	6	1.660E-03	0	0	0	0	
000000	7	1.770E-03	0	0	0	0	
000000	8	1.880E-03	0	0	0	0	
000000	9	1.990E-03	0	0	0	0	
000000	0	2.100E-03	0	0	0	0	
000000	1	2.210E-03	0	0	0	0	
000000	2	2.320E-03	0	0	0	0	
000000	3	2.430E-03	0	0	0	0	
000000	4	2.540E-03	0	0	0	0	
000000	5	2.650E-03	0	0	0	0	
000000	6	2.760E-03	0	0	0	0	
000000	7	2.870E-03	0	0	0	0	
000000	8	2.980E-03	0	0	0	0	
000000	9	3.090E-03	0	0	0	0	
000000	0	3.200E-03	0	0	0	0	
000000	1	3.310E-03	0	0	0	0	
000000	2	3.420E-03	0	0	0	0	
000000	3	3.530E-03	0	0	0	0	
000000	4	3.640E-03	0	0	0	0	
000000	5	3.750E-03	0	0	0	0	
000000	6	3.860E-03	0	0	0	0	
000000	7	3.970E-03	0	0	0	0	
000000	8	4.080E-03	0	0	0	0	
000000	9	4.190E-03	0	0	0	0	
000000	0	4.300E-03	0	0	0	0	

INITIAL TEMPERATURES

BOUNDARY TEMPERATURES

CAPACITANCE BLOCK

CONDUCTANCE BLOCK

Figure 5-6. Model 2B Input (Sheet 1 of 2)









REPRODUCIBILITY OF THE  
ALL PAGE IS POOR

```

SSURE
NUMND = 2,
NUMTR = 160,
NUMCON = 444,
NUMTCN = 1648,
NUMND = 1000,
NUMFLX = 0,
NBTH = 12500,
NEVALU = 14,
NUMTOT = 162,
NUMSCH = 1487,
NUMRAD = 80,
SEND

THIS RUN REQUIRES A DATA AREA OF
1 162 24015 444
0 162 160 2094 444
162 160 444 444
3209 121 445 1000
22362 3091 3703 3799
HIGHEST MEMORY IN HEXADECIIMAL IS 23124 23572
162 160 1000 0 1487 12500

```

Parameter	Value	Value	Value	Value	Value	Value
NUMND	2	162	160	444	444	0
NUMTR	160	162	160	444	444	12500
NUMCON	444	162	445	1000	3799	3299
NUMTCN	1648	445	3703	3799	3799	22200
NUMND	1000	3703	23124	23572	1487	12500
NUMFLX	0	23124	0	1487	12500	0
NBTH	12500	0	1487	12500	1000	1487
NEVALU	14	1487	12500	1000	1487	12500
NUMTOT	162	1487	12500	1000	1487	12500
NUMSCH	1487	1000	1487	12500	1000	1487
NUMRAD	80	1000	1487	12500	1000	1487

Figure 5-8. Model 2A Output (Sheet 1 of 49)











ITERATION NUMBER 13 MAXIMUM ABSOLUTE ERROR = 6.30

EST ABS FWD  
 ROW / COL 0. 11 -7.405E+06 5.081E+06 3.051E+00 1.174E+00 6.303E+00 7.213E+06 1.077E+02 6.797E+02 4.083E+03

ROW / COL 1.038E+05 3.417E+00 6.025E+04 7.783E+04

RAYLEIGH QUOTIENTS  
 ROW / COL -2.184E+01 -4.306E+01 -3.803E+01 -1.75E+02 -1.405E+02 -1.508E+02 -5.720E+01 -1.231E+02 -1.193E+02 -1.088E+02

ROW / COL -7.370E+01 -1.507E+02 -8.800E+01 -9.307E+01

DOMINANT EIGENVALUES  
 ROW / COL -2.184E+01 -4.306E+01 -5.720E+01 -7.370E+01 -9.307E+01 -11.009E+01 -1.193E+02 -1.231E+02

ROW / COL -1.405E+02 -1.508E+02 -1.508E+02 -1.508E+02 -1.508E+02 -1.508E+02 -1.508E+02 -1.508E+02

MAXIMUM ITERATION 12 IN ATJEN MFACTED

TIME = .100E-01 NUMBER OF DOMINANT EIGENVALUES = 14

TEMP / COL	1	2	3	4	5	6	7	8	9	10	11	12	13	14
ROW / COL	1.012E+03	1.508E+03	1.100E+03	1.026E+03	1.001E+03	1.000E+03	1.000E+03	1.000E+03	1.000E+03	1.000E+03	1.000E+03	1.000E+03	1.000E+03	1.000E+03
ROW / COL	1.410E+03	1.508E+03	1.045E+03	9.321E+02	9.301E+02	9.557E+02	1.113E+03	1.113E+03	1.113E+03	1.113E+03	1.113E+03	1.113E+03	1.113E+03	1.113E+03
ROW / COL	1.404E+03	1.512E+03	1.111E+03	9.583E+02	1.055E+03	1.144E+03	1.144E+03	1.144E+03	1.144E+03	1.144E+03	1.144E+03	1.144E+03	1.144E+03	1.144E+03
ROW / COL	1.404E+03	1.512E+03	1.111E+03	1.088E+03	1.088E+03	1.088E+03	1.088E+03	1.088E+03	1.088E+03	1.088E+03	1.088E+03	1.088E+03	1.088E+03	1.088E+03
ROW / COL	1.404E+03	1.512E+03	1.111E+03	1.192E+03	1.192E+03	1.192E+03	1.192E+03	1.192E+03	1.192E+03	1.192E+03	1.192E+03	1.192E+03	1.192E+03	1.192E+03
ROW / COL	1.404E+03	1.512E+03	1.111E+03	9.715E+02	1.273E+03	1.273E+03	1.273E+03	1.273E+03	1.273E+03	1.273E+03	1.273E+03	1.273E+03	1.273E+03	1.273E+03
ROW / COL	1.404E+03	1.512E+03	1.111E+03	9.307E+02	8.275E+02	8.275E+02	8.275E+02	8.275E+02	8.275E+02	8.275E+02	8.275E+02	8.275E+02	8.275E+02	8.275E+02
ROW / COL	1.404E+03	1.512E+03	1.111E+03	8.938E+02	7.074E+02	7.074E+02	7.074E+02	7.074E+02	7.074E+02	7.074E+02	7.074E+02	7.074E+02	7.074E+02	7.074E+02
ROW / COL	1.404E+03	1.512E+03	1.111E+03	8.938E+02	9.352E+02	9.352E+02	9.352E+02	9.352E+02	9.352E+02	9.352E+02	9.352E+02	9.352E+02	9.352E+02	9.352E+02
ROW / COL	1.404E+03	1.512E+03	1.111E+03	9.091E+02	9.103E+02	9.103E+02	9.103E+02	9.103E+02	9.103E+02	9.103E+02	9.103E+02	9.103E+02	9.103E+02	9.103E+02
ROW / COL	1.404E+03	1.512E+03	1.111E+03	9.114E+02	9.114E+02	9.114E+02	9.114E+02	9.114E+02	9.114E+02	9.114E+02	9.114E+02	9.114E+02	9.114E+02	9.114E+02
ROW / COL	1.404E+03	1.512E+03	1.111E+03	1.012E+03	1.012E+03	1.012E+03	1.012E+03	1.012E+03	1.012E+03	1.012E+03	1.012E+03	1.012E+03	1.012E+03	1.012E+03
ROW / COL	1.404E+03	1.512E+03	1.111E+03	1.111E+03	1.111E+03	1.111E+03	1.111E+03	1.111E+03	1.111E+03	1.111E+03	1.111E+03	1.111E+03	1.111E+03	1.111E+03
ROW / COL	1.404E+03	1.512E+03	1.111E+03	9.408E+02	1.111E+03	1.111E+03	1.111E+03	1.111E+03	1.111E+03	1.111E+03	1.111E+03	1.111E+03	1.111E+03	1.111E+03
ROW / COL	1.404E+03	1.512E+03	1.111E+03	1.111E+03	8.408E+02	8.408E+02	8.408E+02	8.408E+02	8.408E+02	8.408E+02	8.408E+02	8.408E+02	8.408E+02	8.408E+02
ROW / COL	1.404E+03	1.512E+03	1.111E+03	1.111E+03	8.408E+02	8.408E+02	8.408E+02	8.408E+02	8.408E+02	8.408E+02	8.408E+02	8.408E+02	8.408E+02	8.408E+02
ROW / COL	1.404E+03	1.512E+03	1.111E+03	8.613E+02	8.613E+02	8.613E+02	8.613E+02	8.613E+02	8.613E+02	8.613E+02	8.613E+02	8.613E+02	8.613E+02	8.613E+02
ROW / COL	1.404E+03	1.512E+03	1.111E+03	8.613E+02	8.613E+02	8.613E+02	8.613E+02	8.613E+02	8.613E+02	8.613E+02	8.613E+02	8.613E+02	8.613E+02	8.613E+02

Figure 5-8. Model 2A Output (Sheet 7 of 49)





REPRODUCIBILITY OF THE ORIGINAL PAGE IS POOR

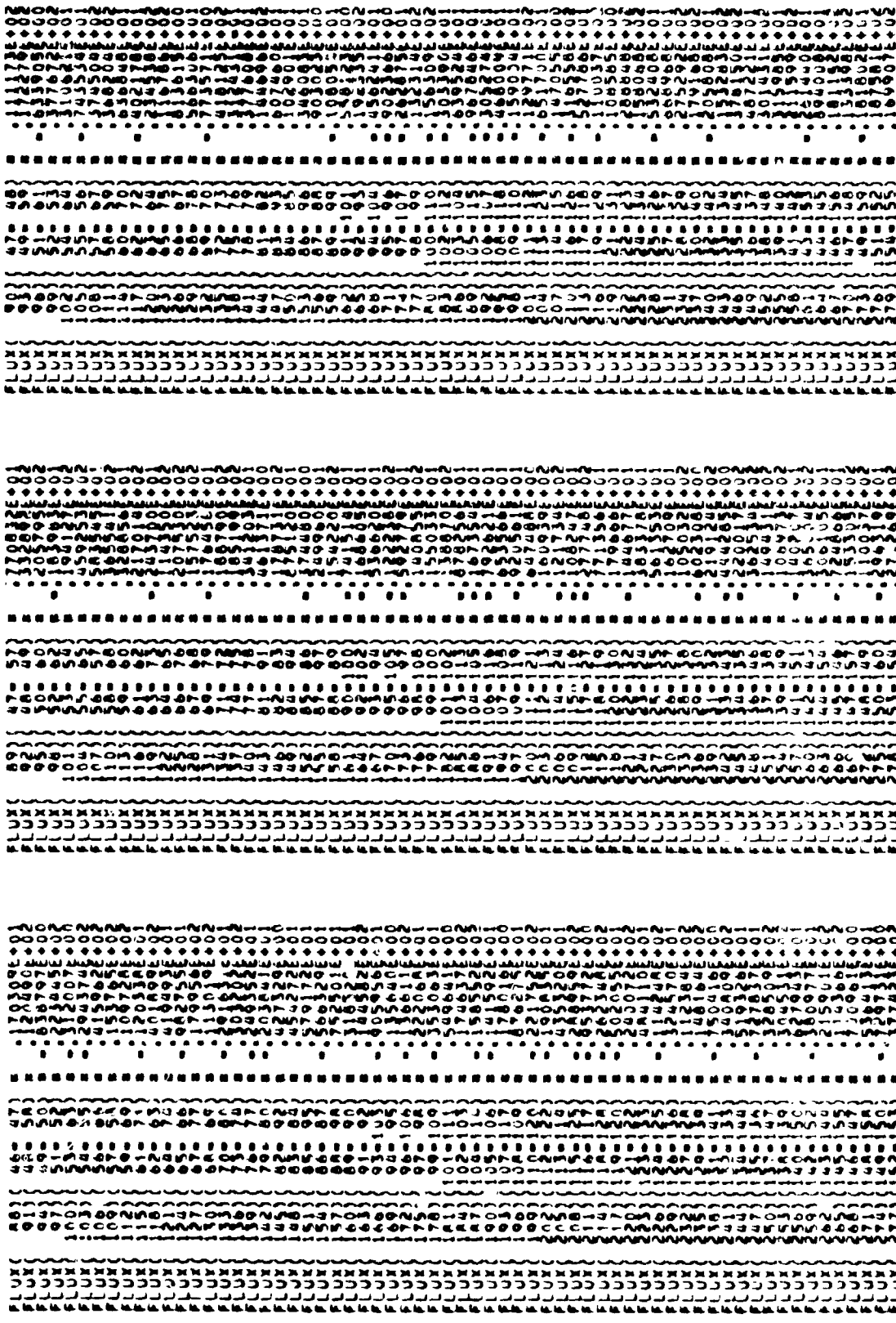


Figure 5-2. Model 2:A Output (Sheet 9 of 19)





REPRODUCIBILITY OF THE ORIGINAL PAGE IS POOR

MUM / COL	1.99E+03	41	42E+03	1.50E+03	40E+03	1.61E+03	47E+03	1.49E+03	49E+03	1.15E+03	50E+03
ROM / COL	2.00E+03	1.54E+03	1.54E+03	1.54E+03	1.54E+03	1.54E+03	1.54E+03	1.54E+03	1.54E+03	1.01E+03	9.11E+02
ROM / COL	2.00E+03	1.54E+03	1.54E+03	1.54E+03	1.54E+03	1.54E+03	1.54E+03	1.54E+03	1.54E+03	0.71E+02	8.21E+02
ROM / COL	2.00E+03	1.54E+03	1.54E+03	1.54E+03	1.54E+03	1.54E+03	1.54E+03	1.54E+03	1.54E+03	0.08E+02	7.89E+02
RUM / COL	1.99E+03	1.54E+03	1.54E+03	1.54E+03	1.54E+03	1.54E+03	1.54E+03	1.54E+03	1.54E+03	0.87E+02	8.11E+02
ROM / COL	1.99E+03	1.54E+03	1.54E+03	1.54E+03	1.54E+03	1.54E+03	1.54E+03	1.54E+03	1.54E+03	0.92E+02	9.11E+02
ROM / COL	1.99E+03	1.54E+03	1.54E+03	1.54E+03	1.54E+03	1.54E+03	1.54E+03	1.54E+03	1.54E+03	1.00E+03	9.11E+02
ROM / COL	1.99E+03	1.54E+03	1.54E+03	1.54E+03	1.54E+03	1.54E+03	1.54E+03	1.54E+03	1.54E+03	1.05E+03	1.00E+03
ROM / COL	1.99E+03	1.54E+03	1.54E+03	1.54E+03	1.54E+03	1.54E+03	1.54E+03	1.54E+03	1.54E+03	1.12E+03	1.00E+03
ROM / COL	1.99E+03	1.54E+03	1.54E+03	1.54E+03	1.54E+03	1.54E+03	1.54E+03	1.54E+03	1.54E+03	0.94E+02	9.11E+02
ROM / COL	1.99E+03	1.54E+03	1.54E+03	1.54E+03	1.54E+03	1.54E+03	1.54E+03	1.54E+03	1.54E+03	0.54E+02	8.11E+02
ROM / COL	1.99E+03	1.54E+03	1.54E+03	1.54E+03	1.54E+03	1.54E+03	1.54E+03	1.54E+03	1.54E+03	0.71E+02	7.11E+02

Figure 5-8. Model 2A Output (Sheet 12 of 49)

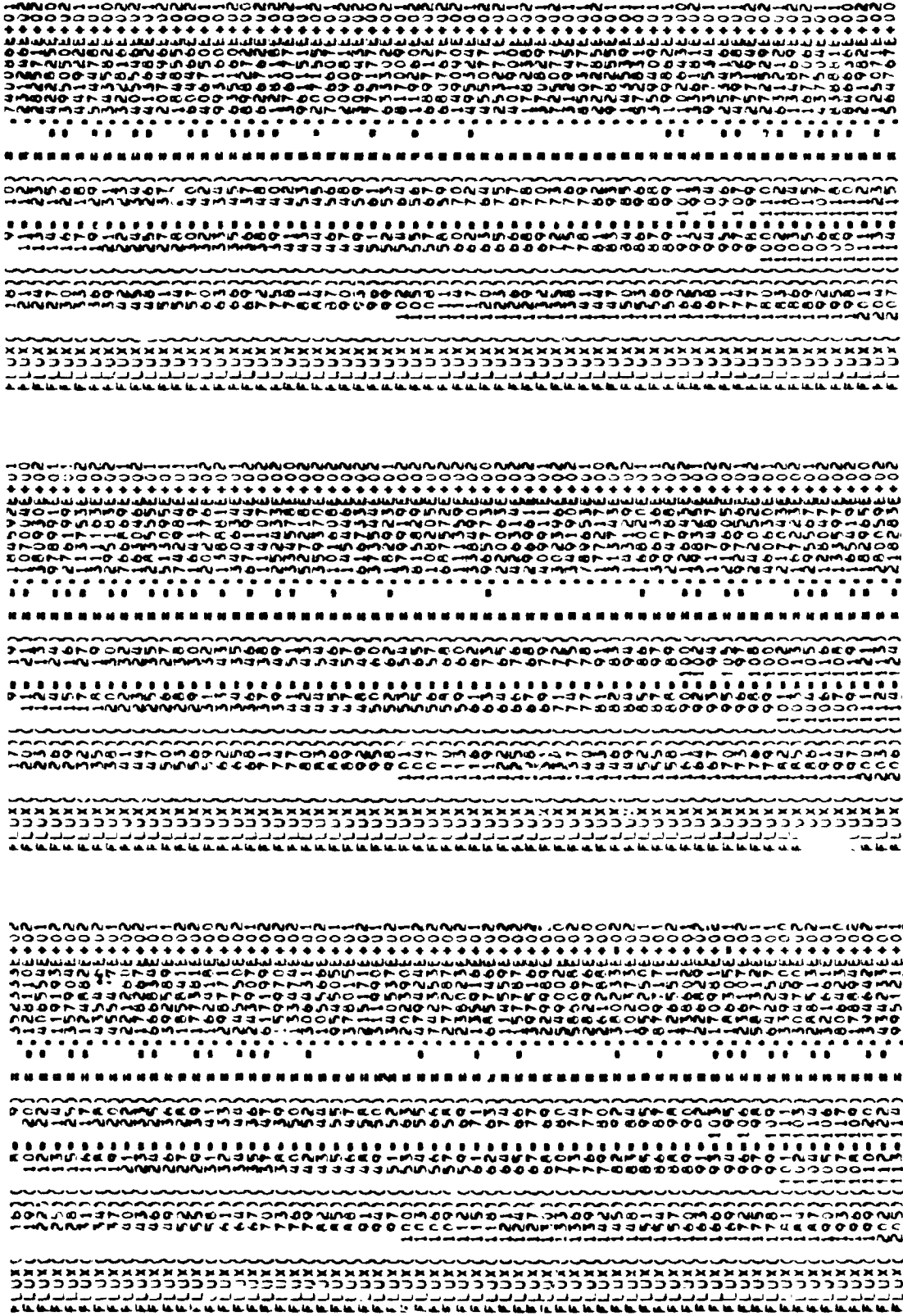


Figure 5-8. Model 2A Output (Sheet 13 of 49)









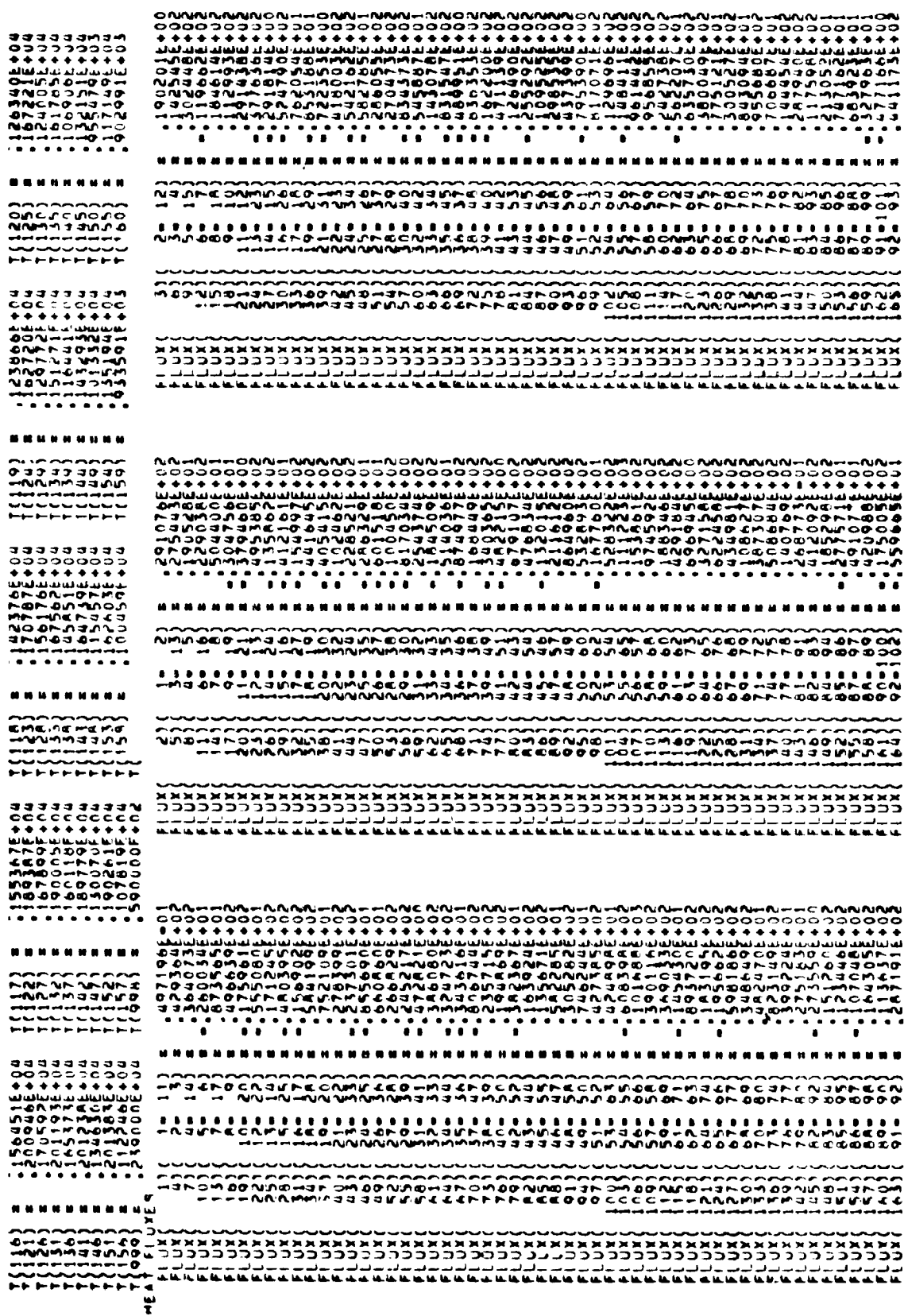


Figure 5-8. Model 2A Output (Sheet 17 of 49)



























### REPRODUCIBILITY OF THE ORIGINAL PAGE IS POOR

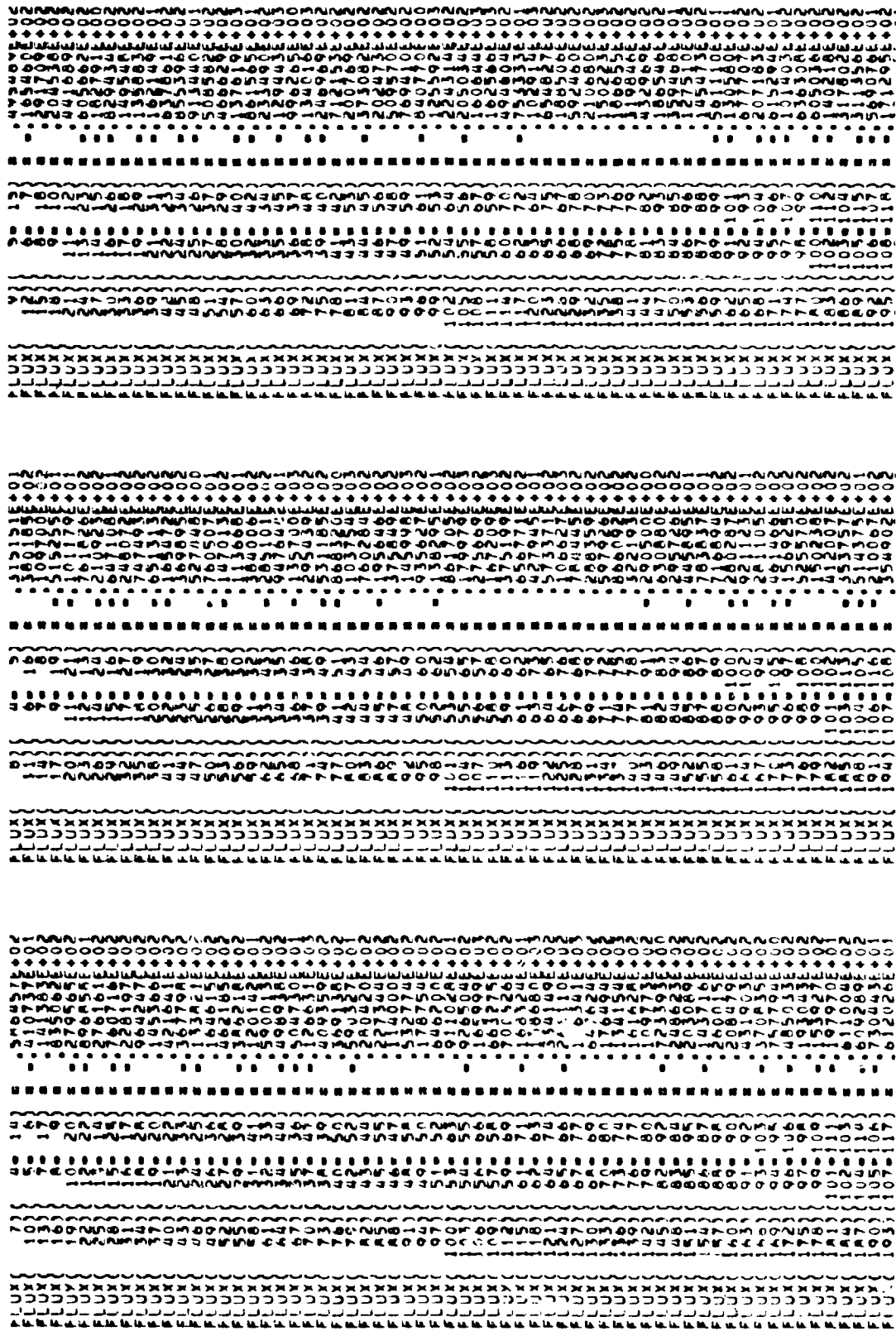


Figure 5-8. Model 2A Output (Sheet 30 of 49)

















REPRODUCIBILITY OF THE ORIGINAL PAGE IS POOR

[Illegible text block 1]  
[Illegible text block 2]  
[Illegible text block 3]  
[Illegible text block 4]  
[Illegible text block 5]  
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[Illegible text block 7]  
[Illegible text block 8]  
[Illegible text block 9]  
[Illegible text block 10]

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[Illegible text block 12]  
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[Illegible text block 21]  
[Illegible text block 22]  
[Illegible text block 23]  
[Illegible text block 24]  
[Illegible text block 25]

Figure 5-8. Model 2A Output (Sheet 38 of 49)

0-2



REPRODUCIBILITY OF THE ORIGINAL PAGE IS POOR

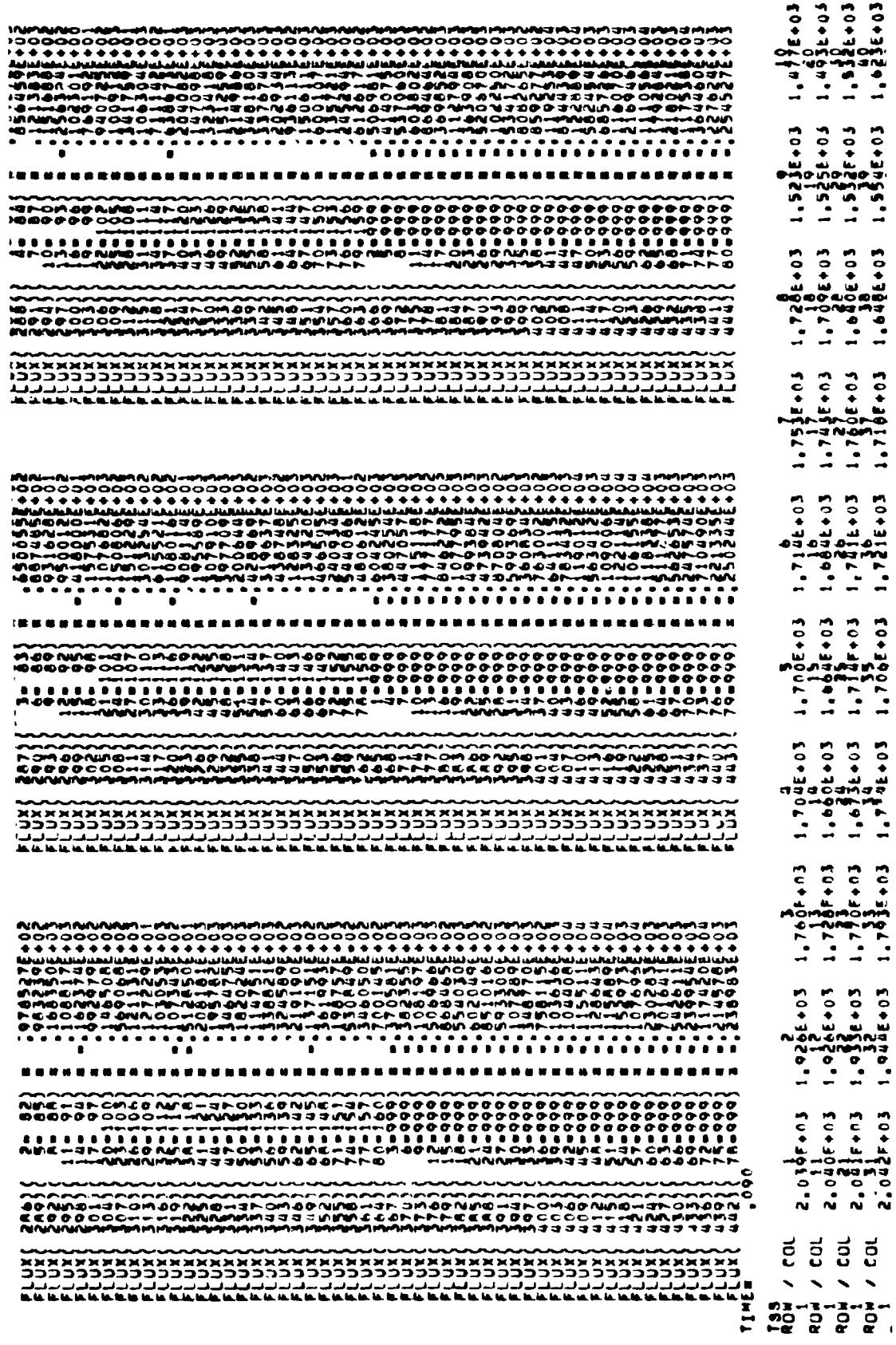


Figure 5-8. Model 2A Output (Sheet 40 of 49)



ROW / COL	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60
1	2.044F+03	1.052E+03	1.825E+03	1.796E+03	1.831E+03	1.859E+03	1.875E+03	1.894E+03	1.914E+03	1.935E+03	1.957E+03	1.979E+03	1.999E+03	2.019E+03	2.039E+03	2.059E+03	2.079E+03	2.099E+03	2.119E+03	2.139E+03
2	2.046F+03	1.062E+03	1.799E+03	1.681E+03	1.809E+03	1.809E+03	1.835E+03	1.861E+03	1.887E+03	1.913E+03	1.939E+03	1.965E+03	1.991E+03	2.017E+03	2.043E+03	2.069E+03	2.095E+03	2.121E+03	2.147E+03	2.173E+03
3	2.047F+03	1.062E+03	1.799E+03	1.681E+03	1.809E+03	1.809E+03	1.835E+03	1.861E+03	1.887E+03	1.913E+03	1.939E+03	1.965E+03	1.991E+03	2.017E+03	2.043E+03	2.069E+03	2.095E+03	2.121E+03	2.147E+03	2.173E+03
4	2.047E+03	1.071E+03	1.777E+03	1.614E+03	1.516E+03	1.646E+03	1.711E+03	1.777E+03	1.843E+03	1.909E+03	1.975E+03	2.041E+03	2.107E+03	2.173E+03	2.239E+03	2.305E+03	2.371E+03	2.437E+03	2.503E+03	2.569E+03
5	2.049F+03	1.072E+03	1.797E+03	1.701E+03	1.699E+03	1.699E+03	1.701E+03	1.701E+03	1.701E+03	1.701E+03	1.701E+03	1.701E+03	1.701E+03	1.701E+03	1.701E+03	1.701E+03	1.701E+03	1.701E+03	1.701E+03	1.701E+03
6	2.031F+03	1.072E+03	1.797E+03	1.701E+03	1.699E+03	1.699E+03	1.701E+03	1.701E+03	1.701E+03	1.701E+03	1.701E+03	1.701E+03	1.701E+03	1.701E+03	1.701E+03	1.701E+03	1.701E+03	1.701E+03	1.701E+03	1.701E+03
7	2.032F+03	1.072E+03	1.797E+03	1.701E+03	1.699E+03	1.699E+03	1.701E+03	1.701E+03	1.701E+03	1.701E+03	1.701E+03	1.701E+03	1.701E+03	1.701E+03	1.701E+03	1.701E+03	1.701E+03	1.701E+03	1.701E+03	1.701E+03
8	2.033F+03	1.072E+03	1.797E+03	1.701E+03	1.699E+03	1.699E+03	1.701E+03	1.701E+03	1.701E+03	1.701E+03	1.701E+03	1.701E+03	1.701E+03	1.701E+03	1.701E+03	1.701E+03	1.701E+03	1.701E+03	1.701E+03	1.701E+03
9	2.033E+03	1.072E+03	1.797E+03	1.701E+03	1.699E+03	1.699E+03	1.701E+03	1.701E+03	1.701E+03	1.701E+03	1.701E+03	1.701E+03	1.701E+03	1.701E+03	1.701E+03	1.701E+03	1.701E+03	1.701E+03	1.701E+03	1.701E+03
10	2.033F+03	1.072E+03	1.797E+03	1.701E+03	1.699E+03	1.699E+03	1.701E+03	1.701E+03	1.701E+03	1.701E+03	1.701E+03	1.701E+03	1.701E+03	1.701E+03	1.701E+03	1.701E+03	1.701E+03	1.701E+03	1.701E+03	1.701E+03
11	2.033F+03	1.072E+03	1.797E+03	1.701E+03	1.699E+03	1.699E+03	1.701E+03	1.701E+03	1.701E+03	1.701E+03	1.701E+03	1.701E+03	1.701E+03	1.701E+03	1.701E+03	1.701E+03	1.701E+03	1.701E+03	1.701E+03	1.701E+03
12	2.033E+03	1.072E+03	1.797E+03	1.701E+03	1.699E+03	1.699E+03	1.701E+03	1.701E+03	1.701E+03	1.701E+03	1.701E+03	1.701E+03	1.701E+03	1.701E+03	1.701E+03	1.701E+03	1.701E+03	1.701E+03	1.701E+03	1.701E+03
13	2.033E+03	1.072E+03	1.797E+03	1.701E+03	1.699E+03	1.699E+03	1.701E+03	1.701E+03	1.701E+03	1.701E+03	1.701E+03	1.701E+03	1.701E+03	1.701E+03	1.701E+03	1.701E+03	1.701E+03	1.701E+03	1.701E+03	1.701E+03
14	2.033E+03	1.072E+03	1.797E+03	1.701E+03	1.699E+03	1.699E+03	1.701E+03	1.701E+03	1.701E+03	1.701E+03	1.701E+03	1.701E+03	1.701E+03	1.701E+03	1.701E+03	1.701E+03	1.701E+03	1.701E+03	1.701E+03	1.701E+03
15	2.033E+03	1.072E+03	1.797E+03	1.701E+03	1.699E+03	1.699E+03	1.701E+03	1.701E+03	1.701E+03	1.701E+03	1.701E+03	1.701E+03	1.701E+03	1.701E+03	1.701E+03	1.701E+03	1.701E+03	1.701E+03	1.701E+03	1.701E+03

ITERATION NUMBER 2 MAXIMUM ABSOLUTE ERROR = .001

EST ABS ERR

ROW / COL	1	2	3	4	5	6	7	8	9	10
1	1.620E+04	3.520E+04	7.562E+04	1.181E+03	2.036E+03	4.007E+03	5.684E+03	1.287E+02	2.114E+02	1.878E+02
2	1.348F+01	1.015E+01	1.990F+01	2.011E+01						

RAYLEIGH QUOTIENTS

ROW / COL	1	2	3	4	5	6	7	8	9	10
1	-2.624E+01	-4.039E+01	-4.584E+01	-5.910E+01	-7.133E+01	-8.348E+01	-9.540E+01	-1.111E+02	-1.133E+02	-1.133E+02
2	-1.274E+02	-1.348E+02	-1.402E+02	-1.421E+02						

DOMINANT EIGENVALUES

ROW / COL	1	2	3	4	5	6	7	8	9	10
1	-2.624F+01	-4.039E+01	-4.584E+01	-5.910E+01	-7.133E+01	-8.348E+01	-9.540E+01	-1.111E+02	-1.133E+02	-1.133E+02
2	-1.274E+02	-1.348E+02	-1.402E+02	-1.421E+02						

TIME = .000E+01 NUMBER OF DOMINANT EIGENVALUES = 14

TEMP	ROW / COL	1	2	3	4	5	6	7	8	9	10
1	1	2.016F+03	1.926E+03	1.758E+03	1.708E+03	1.658E+03	1.608E+03	1.558E+03	1.508E+03	1.458E+03	1.408E+03
2	2	2.021E+03	1.931E+03	1.763E+03	1.713E+03	1.663E+03	1.613E+03	1.563E+03	1.513E+03	1.463E+03	1.413E+03
3	3	2.026E+03	1.936E+03	1.768E+03	1.718E+03	1.668E+03	1.618E+03	1.568E+03	1.518E+03	1.468E+03	1.418E+03
4	4	2.031E+03	1.941E+03	1.773E+03	1.723E+03	1.673E+03	1.623E+03	1.573E+03	1.523E+03	1.473E+03	1.423E+03
5	5	2.036E+03	1.946E+03	1.778E+03	1.728E+03	1.678E+03	1.628E+03	1.578E+03	1.528E+03	1.478E+03	1.428E+03
6	6	2.041E+03	1.951E+03	1.783E+03	1.733E+03	1.683E+03	1.633E+03	1.583E+03	1.533E+03	1.483E+03	1.433E+03
7	7	2.046E+03	1.956E+03	1.788E+03	1.738E+03	1.688E+03	1.638E+03	1.588E+03	1.538E+03	1.488E+03	1.438E+03
8	8	2.051E+03	1.961E+03	1.793E+03	1.743E+03	1.693E+03	1.643E+03	1.593E+03	1.543E+03	1.493E+03	1.443E+03
9	9	2.056E+03	1.966E+03	1.798E+03	1.748E+03	1.698E+03	1.648E+03	1.598E+03	1.548E+03	1.498E+03	1.448E+03
10	10	2.061E+03	1.971E+03	1.803E+03	1.753E+03	1.703E+03	1.653E+03	1.603E+03	1.553E+03	1.503E+03	1.453E+03

Figure 5-8. Model 2A Output (Sheet 41 of 49).



REPRODUCIBILITY OF THE  
ORBITALS IS POOR

ITERATION NUMBER	2	MAXIMUM ABSOLUTE ERROR	=	.178
EST ABS ERR				
ROW / COL	1.147E+04	2.102E+04	4.253E+04	6.403E+04
ROW / COL	1.149E+01	1.052E+01	1.776E+01	1.776E+01
RAYLEIGH QUOTIENTS				
ROW / COL	-2.642E+01	-4.597E+01	-7.142E+01	-9.953E+01
ROW / COL	-1.275E+02	-1.347E+02	-1.402E+02	-1.422E+02
DOMINANT EIGENVALUES				
ROW / COL	-2.642E+01	-4.597E+01	-7.142E+01	-9.953E+01
ROW / COL	-1.275E+02	-1.347E+02	-1.402E+02	-1.422E+02
TIME =	100E+00	NUMBER OF DOMINANT EIGENVALUES =	14	
TEMP				
ROW / COL	2.090E+03	1.753E+03	1.701E+03	1.696E+03
ROW / COL	2.090E+03	1.723E+03	1.657E+03	1.640E+03
ROW / COL	2.090E+03	1.703E+03	1.630E+03	1.610E+03
ROW / COL	2.090E+03	1.683E+03	1.613E+03	1.593E+03
ROW / COL	2.090E+03	1.663E+03	1.593E+03	1.573E+03
ROW / COL	2.090E+03	1.643E+03	1.573E+03	1.553E+03
ROW / COL	2.090E+03	1.623E+03	1.553E+03	1.533E+03
ROW / COL	2.090E+03	1.603E+03	1.533E+03	1.513E+03
ROW / COL	2.090E+03	1.583E+03	1.513E+03	1.493E+03
ROW / COL	2.090E+03	1.563E+03	1.493E+03	1.473E+03
ROW / COL	2.090E+03	1.543E+03	1.473E+03	1.453E+03
ROW / COL	2.090E+03	1.523E+03	1.453E+03	1.433E+03
ROW / COL	2.090E+03	1.503E+03	1.433E+03	1.413E+03
ROW / COL	2.090E+03	1.483E+03	1.413E+03	1.393E+03
ROW / COL	2.090E+03	1.463E+03	1.393E+03	1.373E+03
ROW / COL	2.090E+03	1.443E+03	1.373E+03	1.353E+03
ROW / COL	2.090E+03	1.423E+03	1.353E+03	1.333E+03
ROW / COL	2.090E+03	1.403E+03	1.333E+03	1.313E+03
ROW / COL	2.090E+03	1.383E+03	1.313E+03	1.293E+03
ROW / COL	2.090E+03	1.363E+03	1.293E+03	1.273E+03
ROW / COL	2.090E+03	1.343E+03	1.273E+03	1.253E+03
ROW / COL	2.090E+03	1.323E+03	1.253E+03	1.233E+03
ROW / COL	2.090E+03	1.303E+03	1.233E+03	1.213E+03
ROW / COL	2.090E+03	1.283E+03	1.213E+03	1.193E+03
ROW / COL	2.090E+03	1.263E+03	1.193E+03	1.173E+03
ROW / COL	2.090E+03	1.243E+03	1.173E+03	1.153E+03
ROW / COL	2.090E+03	1.223E+03	1.153E+03	1.133E+03
ROW / COL	2.090E+03	1.203E+03	1.133E+03	1.113E+03
ROW / COL	2.090E+03	1.183E+03	1.113E+03	1.093E+03
ROW / COL	2.090E+03	1.163E+03	1.093E+03	1.073E+03
ROW / COL	2.090E+03	1.143E+03	1.073E+03	1.053E+03
ROW / COL	2.090E+03	1.123E+03	1.053E+03	1.033E+03
ROW / COL	2.090E+03	1.103E+03	1.033E+03	1.013E+03
ROW / COL	2.090E+03	1.083E+03	1.013E+03	0.993E+03
ROW / COL	2.090E+03	1.063E+03	0.993E+03	0.973E+03
ROW / COL	2.090E+03	1.043E+03	0.973E+03	0.953E+03
ROW / COL	2.090E+03	1.023E+03	0.953E+03	0.933E+03
ROW / COL	2.090E+03	1.003E+03	0.933E+03	0.913E+03
ROW / COL	2.090E+03	0.983E+03	0.913E+03	0.893E+03
ROW / COL	2.090E+03	0.963E+03	0.893E+03	0.873E+03
ROW / COL	2.090E+03	0.943E+03	0.873E+03	0.853E+03
ROW / COL	2.090E+03	0.923E+03	0.853E+03	0.833E+03
ROW / COL	2.090E+03	0.903E+03	0.833E+03	0.813E+03
ROW / COL	2.090E+03	0.883E+03	0.813E+03	0.793E+03
ROW / COL	2.090E+03	0.863E+03	0.793E+03	0.773E+03
ROW / COL	2.090E+03	0.843E+03	0.773E+03	0.753E+03
ROW / COL	2.090E+03	0.823E+03	0.753E+03	0.733E+03
ROW / COL	2.090E+03	0.803E+03	0.733E+03	0.713E+03
ROW / COL	2.090E+03	0.783E+03	0.713E+03	0.693E+03
ROW / COL	2.090E+03	0.763E+03	0.693E+03	0.673E+03
ROW / COL	2.090E+03	0.743E+03	0.673E+03	0.653E+03
ROW / COL	2.090E+03	0.723E+03	0.653E+03	0.633E+03
ROW / COL	2.090E+03	0.703E+03	0.633E+03	0.613E+03
ROW / COL	2.090E+03	0.683E+03	0.613E+03	0.593E+03
ROW / COL	2.090E+03	0.663E+03	0.593E+03	0.573E+03
ROW / COL	2.090E+03	0.643E+03	0.573E+03	0.553E+03
ROW / COL	2.090E+03	0.623E+03	0.553E+03	0.533E+03
ROW / COL	2.090E+03	0.603E+03	0.533E+03	0.513E+03
ROW / COL	2.090E+03	0.583E+03	0.513E+03	0.493E+03
ROW / COL	2.090E+03	0.563E+03	0.493E+03	0.473E+03
ROW / COL	2.090E+03	0.543E+03	0.473E+03	0.453E+03
ROW / COL	2.090E+03	0.523E+03	0.453E+03	0.433E+03
ROW / COL	2.090E+03	0.503E+03	0.433E+03	0.413E+03
ROW / COL	2.090E+03	0.483E+03	0.413E+03	0.393E+03
ROW / COL	2.090E+03	0.463E+03	0.393E+03	0.373E+03
ROW / COL	2.090E+03	0.443E+03	0.373E+03	0.353E+03
ROW / COL	2.090E+03	0.423E+03	0.353E+03	0.333E+03
ROW / COL	2.090E+03	0.403E+03	0.333E+03	0.313E+03
ROW / COL	2.090E+03	0.383E+03	0.313E+03	0.293E+03
ROW / COL	2.090E+03	0.363E+03	0.293E+03	0.273E+03
ROW / COL	2.090E+03	0.343E+03	0.273E+03	0.253E+03
ROW / COL	2.090E+03	0.323E+03	0.253E+03	0.233E+03
ROW / COL	2.090E+03	0.303E+03	0.233E+03	0.213E+03
ROW / COL	2.090E+03	0.283E+03	0.213E+03	0.193E+03
ROW / COL	2.090E+03	0.263E+03	0.193E+03	0.173E+03
ROW / COL	2.090E+03	0.243E+03	0.173E+03	0.153E+03
ROW / COL	2.090E+03	0.223E+03	0.153E+03	0.133E+03
ROW / COL	2.090E+03	0.203E+03	0.133E+03	0.113E+03
ROW / COL	2.090E+03	0.183E+03	0.113E+03	0.093E+03
ROW / COL	2.090E+03	0.163E+03	0.093E+03	0.073E+03
ROW / COL	2.090E+03	0.143E+03	0.073E+03	0.053E+03
ROW / COL	2.090E+03	0.123E+03	0.053E+03	0.033E+03
ROW / COL	2.090E+03	0.103E+03	0.033E+03	0.013E+03
ROW / COL	2.090E+03	0.083E+03	0.013E+03	0.003E+03
ROW / COL	2.090E+03	0.063E+03	0.003E+03	0.000E+03
ROW / COL	2.090E+03	0.043E+03	0.000E+03	0.000E+03
ROW / COL	2.090E+03	0.023E+03	0.000E+03	0.000E+03
ROW / COL	2.090E+03	0.003E+03	0.000E+03	0.000E+03
ROW / COL	2.090E+03	0.000E+03	0.000E+03	0.000E+03

Figure 5-8. Model 2A Output (Sheet 43 of 49)



REPRODUCIBILITY OF THE  
ORIG. PAGE IS POOR

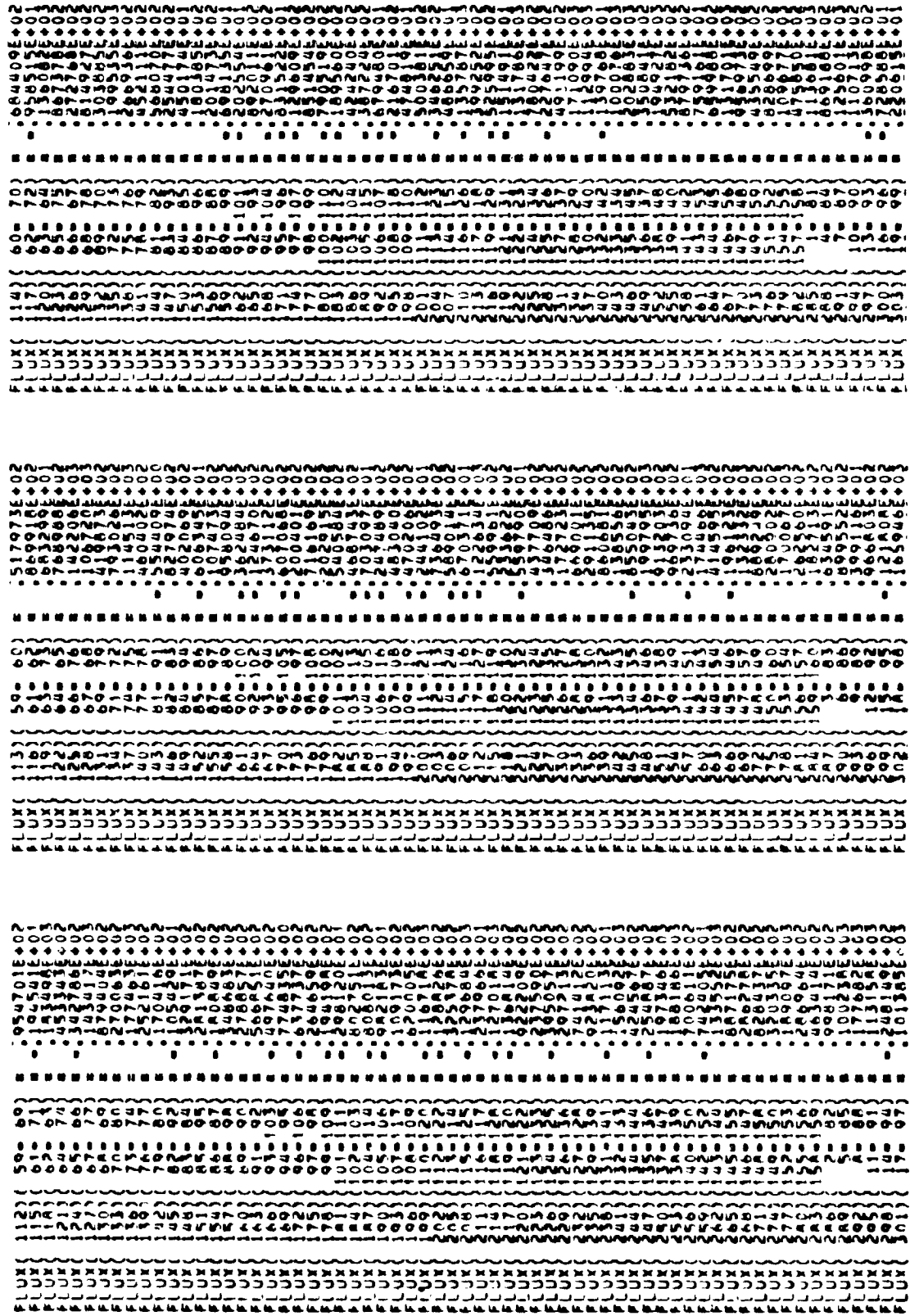


Figure 5-5. Model 2A Output (Sheet 45 of 49)



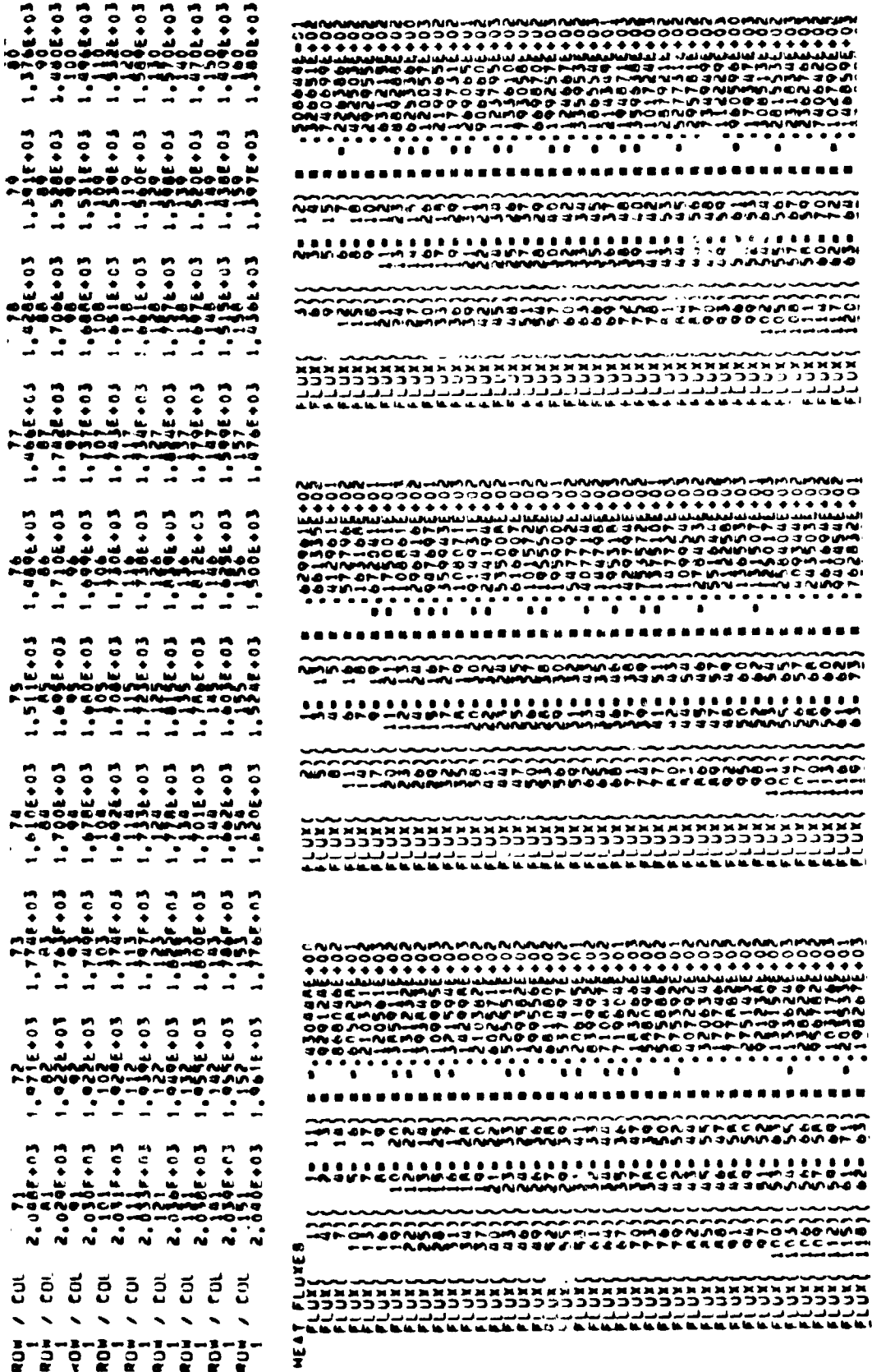


Figure 5-5. Model 2A Output (Sheet 47 of 49)







REPRODUCIBILITY OF THE ORIGINAL PAGE IS POOR

```

SSSTORE
NUMRND = 2,
NUMIYR = 260,
NUMCCN = 700,
NUMTCN = 1560
NUMMND = 1000,
NUMFLX = 0,
NSTW = 15000,
NEVALU = 14,
NUMTNT = 262,
NUMSCH = 2106,
NUMMJD = 80,
SEND
T'S RUN REQUIRES A DATA AREA OF
262 500 262 14 262 160 262 3640 262 1000 0
262 700 262 14 262 3640 262 1000 15000
262 8451 262 14 262 3640 262 1000 15000
262 8451 262 14 262 3640 262 1000 15000
NUMRND = 2,
NUMIYR = 260,
NUMCCN = 700,
NUMTCN = 1560
NUMMND = 1000,
NUMFLX = 0,
NSTW = 15000,
NEVALU = 14,
NUMTNT = 262,
NUMSCH = 2106,
NUMMJD = 80,
SEND

```

Figure 5-9. Model 2B Output (Sheet 1 of 16)

REPRODUCIBILITY OF THE  
OUTPUT OF MODEL 2B

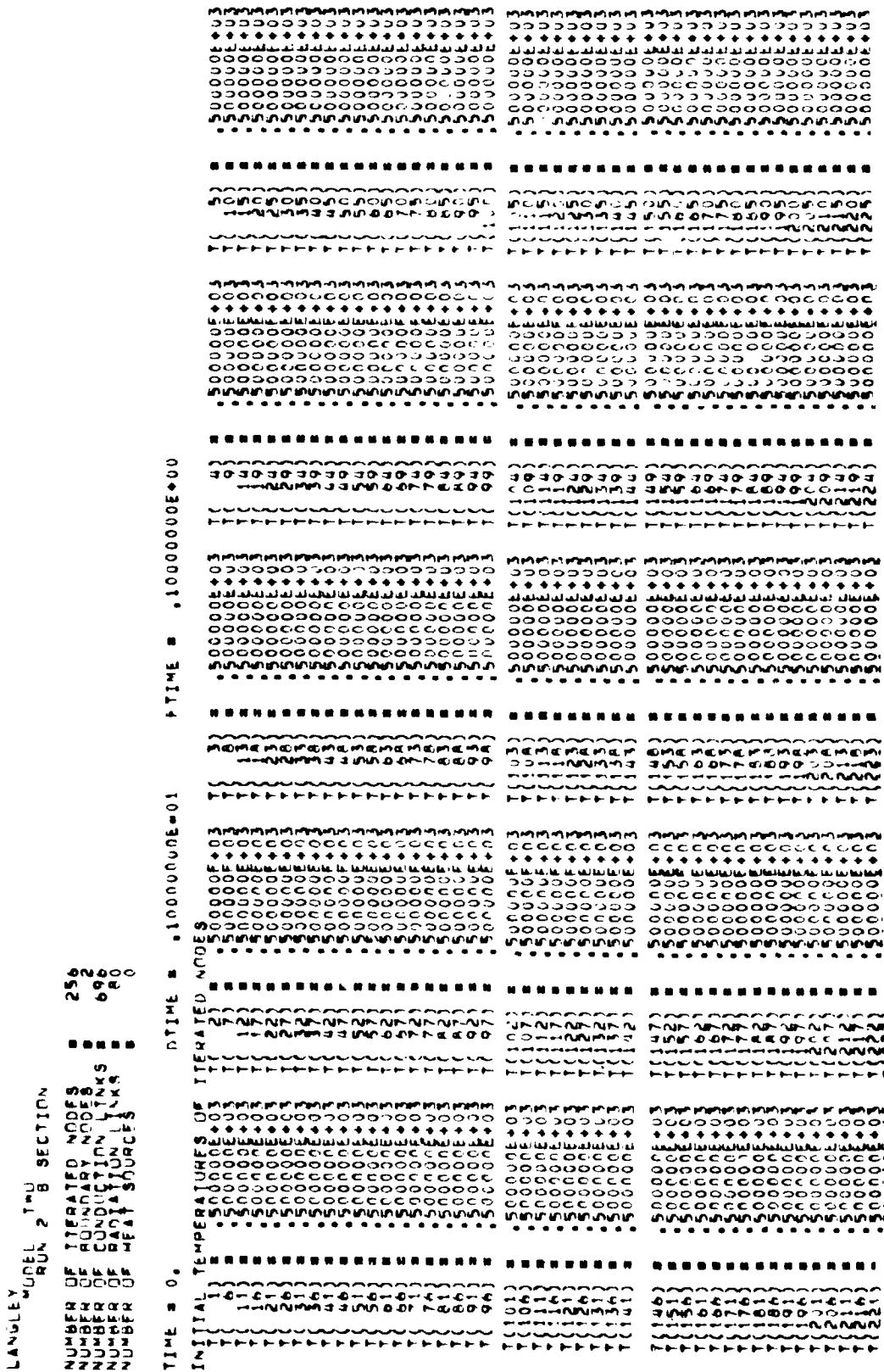


Figure 5-9. Model 2B Output (Sheet 2 of 16)

REPRODUCIBILITY OF THE ORIGINAL PAGE IS POOR

..... ++++++ ..... ..... ..... ..... ..... ..... ..... .....	..... ..... ..... ..... ..... ..... ..... ..... ..... .....	..... ..... ..... ..... ..... ..... ..... ..... ..... .....	..... ..... ..... ..... ..... ..... ..... ..... ..... .....	..... ..... ..... ..... ..... ..... ..... ..... ..... .....	..... ..... ..... ..... ..... ..... ..... ..... ..... .....	..... ..... ..... ..... ..... ..... ..... ..... ..... .....	..... ..... ..... ..... ..... ..... ..... ..... ..... .....	..... ..... ..... ..... ..... ..... ..... ..... ..... .....	..... ..... ..... ..... ..... ..... ..... ..... ..... .....	..... ..... ..... ..... ..... ..... ..... ..... ..... .....	..... ..... ..... ..... ..... ..... ..... ..... ..... .....	..... ..... ..... ..... ..... ..... ..... ..... ..... .....	..... ..... ..... ..... ..... ..... ..... ..... ..... .....
---	--	--	--	--	--	--	--	--	--	--	--	--	--

Figure 5-9. Model 2B Output (Sheet 3 of 16)

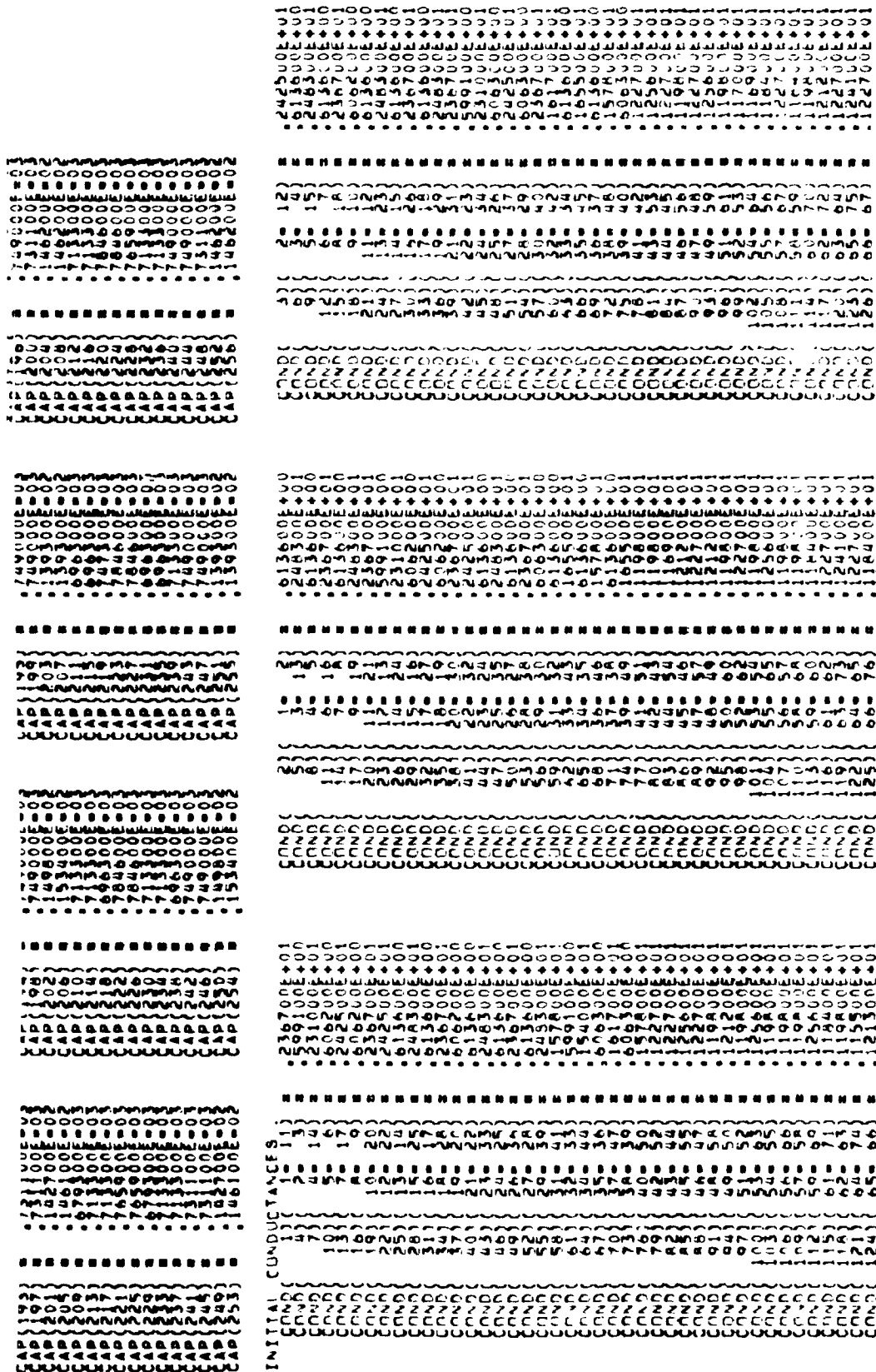


Figure 5-9. Model 2B Output (Sheet 4 of 16)



REPRODUCIBILITY OF THE  
PAGE IS POOR

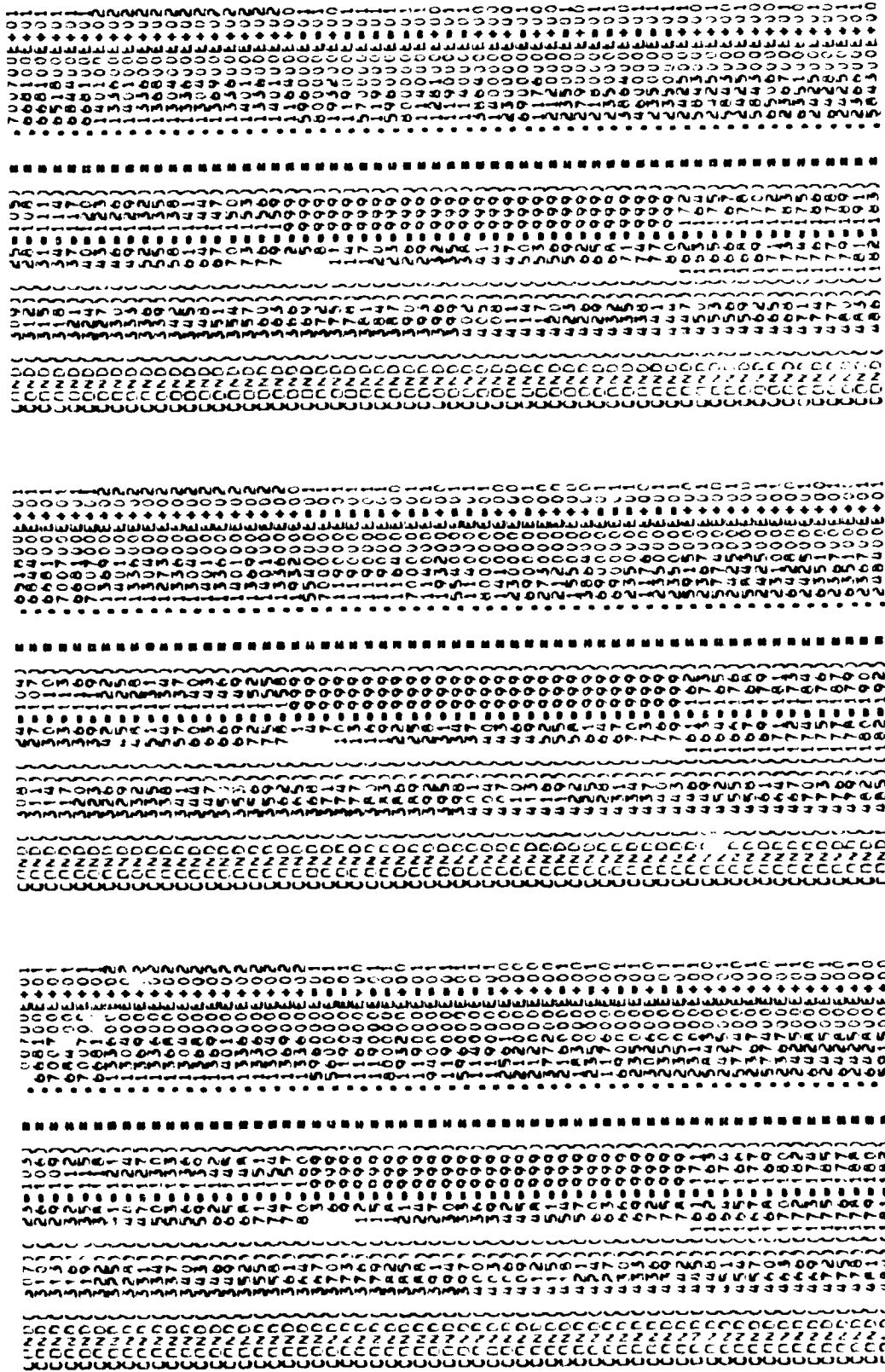


Figure 5-9. Model 2B Output (Sheet 6 of 16)





```

INITIAL HEAT FLUXES
I 6 2 TEMPERATURES AT 1000000E+00 1000000E+00 1000000E+00
RESERVE STORAGE IS 15000. REPEAT IS 12 REACHED
TIME 1) 100000E-01 124104E+04 09295E+03 04295E+03 04295E+03 04295E+03
T( 4) 4643E+04 124104E+04 09295E+03 04295E+03 04295E+03 04295E+03
T( 11) 17944E+04 124104E+04 09295E+03 04295E+03 04295E+03 04295E+03
T( 14) 11554E+04 124104E+04 09295E+03 04295E+03 04295E+03 04295E+03
T( 26) 11987E+04 124104E+04 09295E+03 04295E+03 04295E+03 04295E+03
T( 31) 15052E+04 124104E+04 09295E+03 04295E+03 04295E+03 04295E+03

INITIAL TEMPERATURES
I 6 2 TEMPERATURES AT 1000000E+00 1000000E+00 1000000E+00
RESERVE STORAGE IS 15000. REPEAT IS 12 REACHED
TIME 1) 100000E-01 124104E+04 09295E+03 04295E+03 04295E+03 04295E+03
T( 4) 4643E+04 124104E+04 09295E+03 04295E+03 04295E+03 04295E+03
T( 11) 17944E+04 124104E+04 09295E+03 04295E+03 04295E+03 04295E+03
T( 14) 11554E+04 124104E+04 09295E+03 04295E+03 04295E+03 04295E+03
T( 26) 11987E+04 124104E+04 09295E+03 04295E+03 04295E+03 04295E+03
T( 31) 15052E+04 124104E+04 09295E+03 04295E+03 04295E+03 04295E+03

INITIAL PRESSURES
I 6 2 TEMPERATURES AT 1000000E+00 1000000E+00 1000000E+00
RESERVE STORAGE IS 15000. REPEAT IS 12 REACHED
TIME 1) 100000E-01 124104E+04 09295E+03 04295E+03 04295E+03 04295E+03
T( 4) 4643E+04 124104E+04 09295E+03 04295E+03 04295E+03 04295E+03
T( 11) 17944E+04 124104E+04 09295E+03 04295E+03 04295E+03 04295E+03
T( 14) 11554E+04 124104E+04 09295E+03 04295E+03 04295E+03 04295E+03
T( 26) 11987E+04 124104E+04 09295E+03 04295E+03 04295E+03 04295E+03
T( 31) 15052E+04 124104E+04 09295E+03 04295E+03 04295E+03 04295E+03

INITIAL DENSITIES
I 6 2 TEMPERATURES AT 1000000E+00 1000000E+00 1000000E+00
RESERVE STORAGE IS 15000. REPEAT IS 12 REACHED
TIME 1) 100000E-01 124104E+04 09295E+03 04295E+03 04295E+03 04295E+03
T( 4) 4643E+04 124104E+04 09295E+03 04295E+03 04295E+03 04295E+03
T( 11) 17944E+04 124104E+04 09295E+03 04295E+03 04295E+03 04295E+03
T( 14) 11554E+04 124104E+04 09295E+03 04295E+03 04295E+03 04295E+03
T( 26) 11987E+04 124104E+04 09295E+03 04295E+03 04295E+03 04295E+03
T( 31) 15052E+04 124104E+04 09295E+03 04295E+03 04295E+03 04295E+03

```

Figure 5-9. Model 2B Output (Sheet 8 of 16)

REPRODUCIBILITY OF THE ORIGINAL PAGE IS POOR

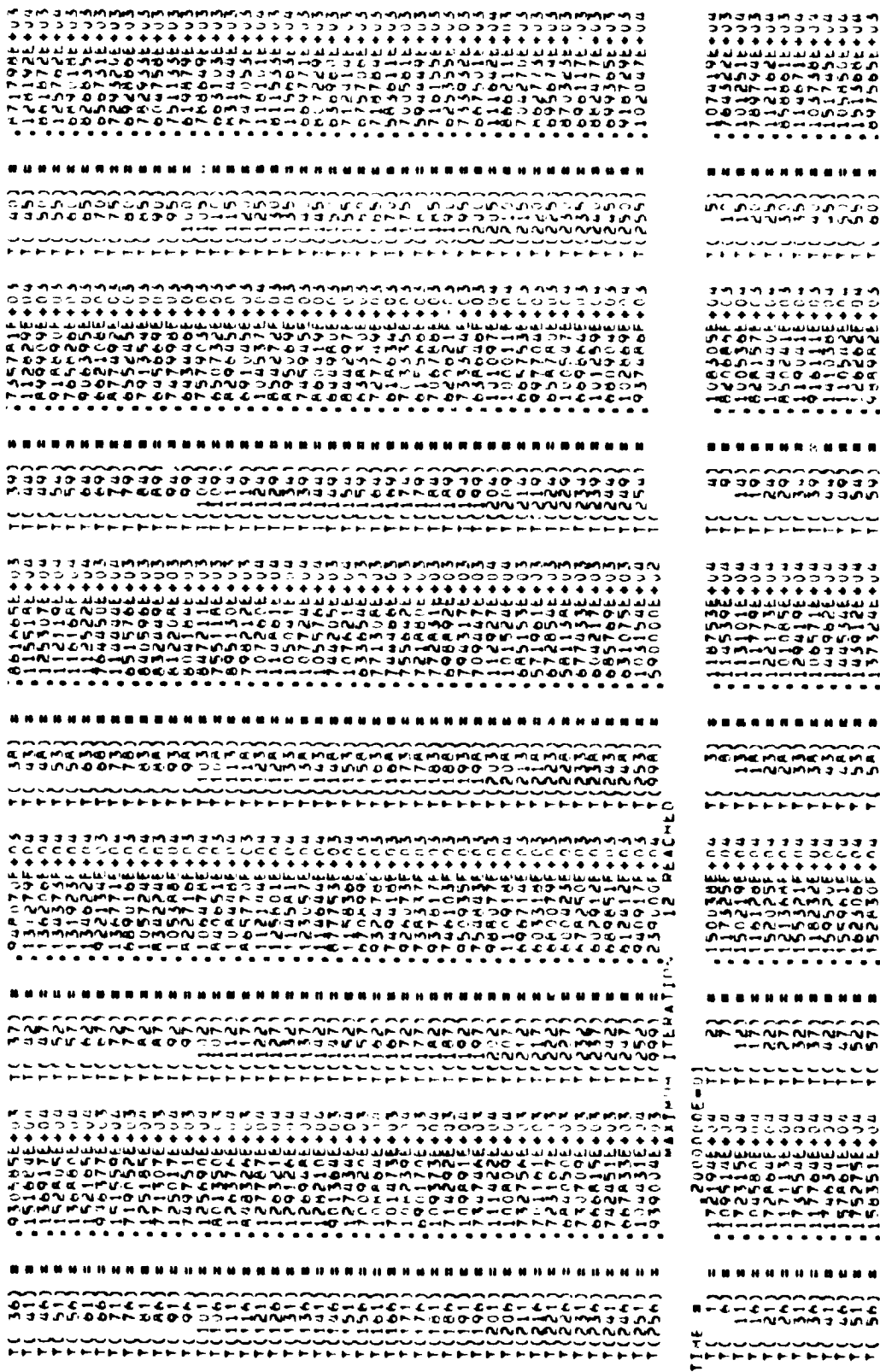


Figure 5-9. Model 2B Output (Sheet 9 of 16)

REPRODUCIBILITY OF THE ORIGINAL PAGE IS POOR

The figure displays a 2x10 grid of low-resolution, high-contrast images, likely a degraded scan of a document page. The images are arranged in two columns and ten rows. Each image contains faint, illegible characters and symbols, possibly representing a table or a list of data points. The overall quality is very poor, with significant noise and loss of detail.

Figure 5-9. Model 2B Output (Sheet 10 of 16)

REPRODUCIBILITY OF THE ORIGINAL PAGE IS POOR

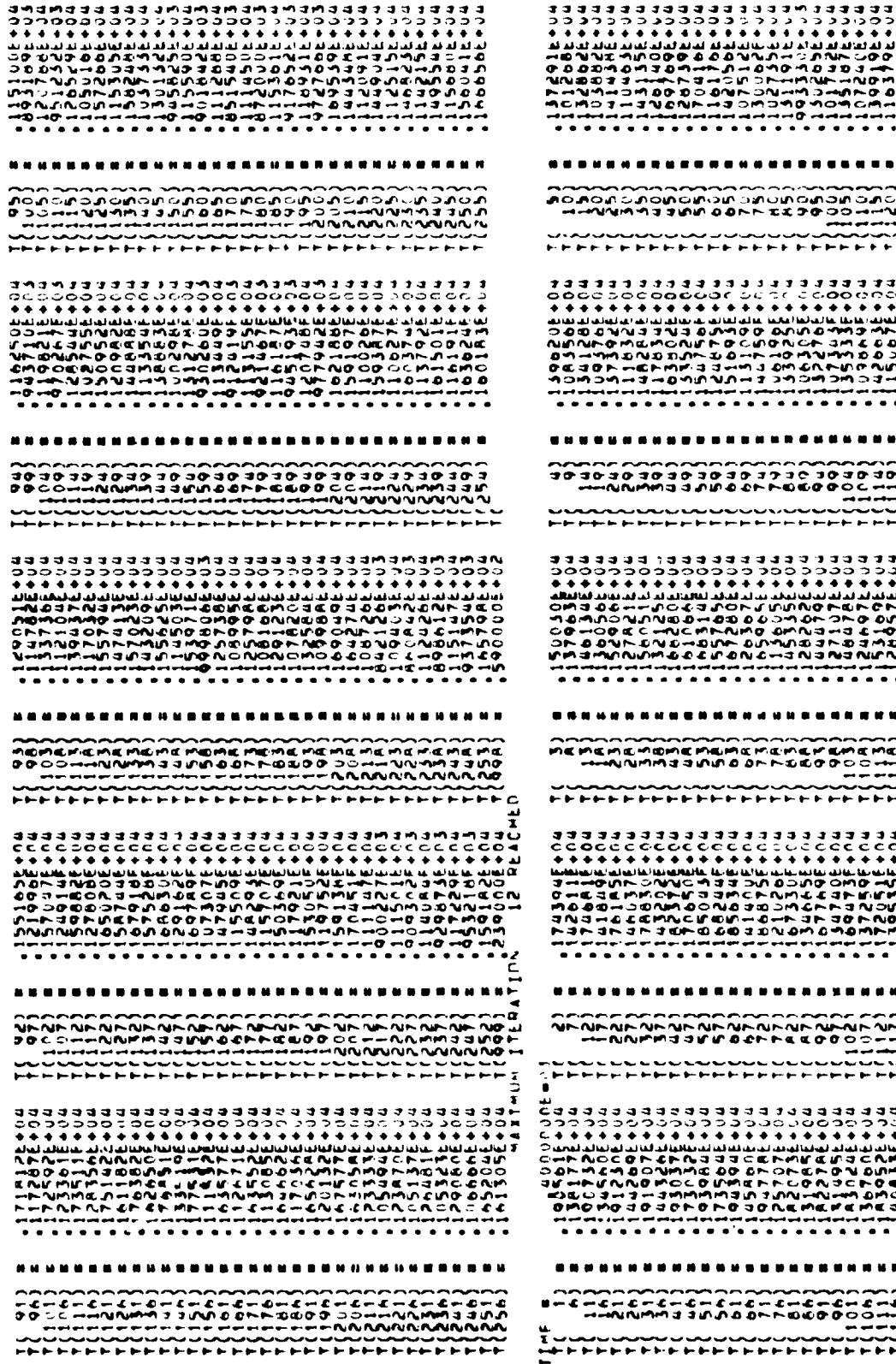


Figure 5-9. Model 2B Output (Sheet 11 of 16)

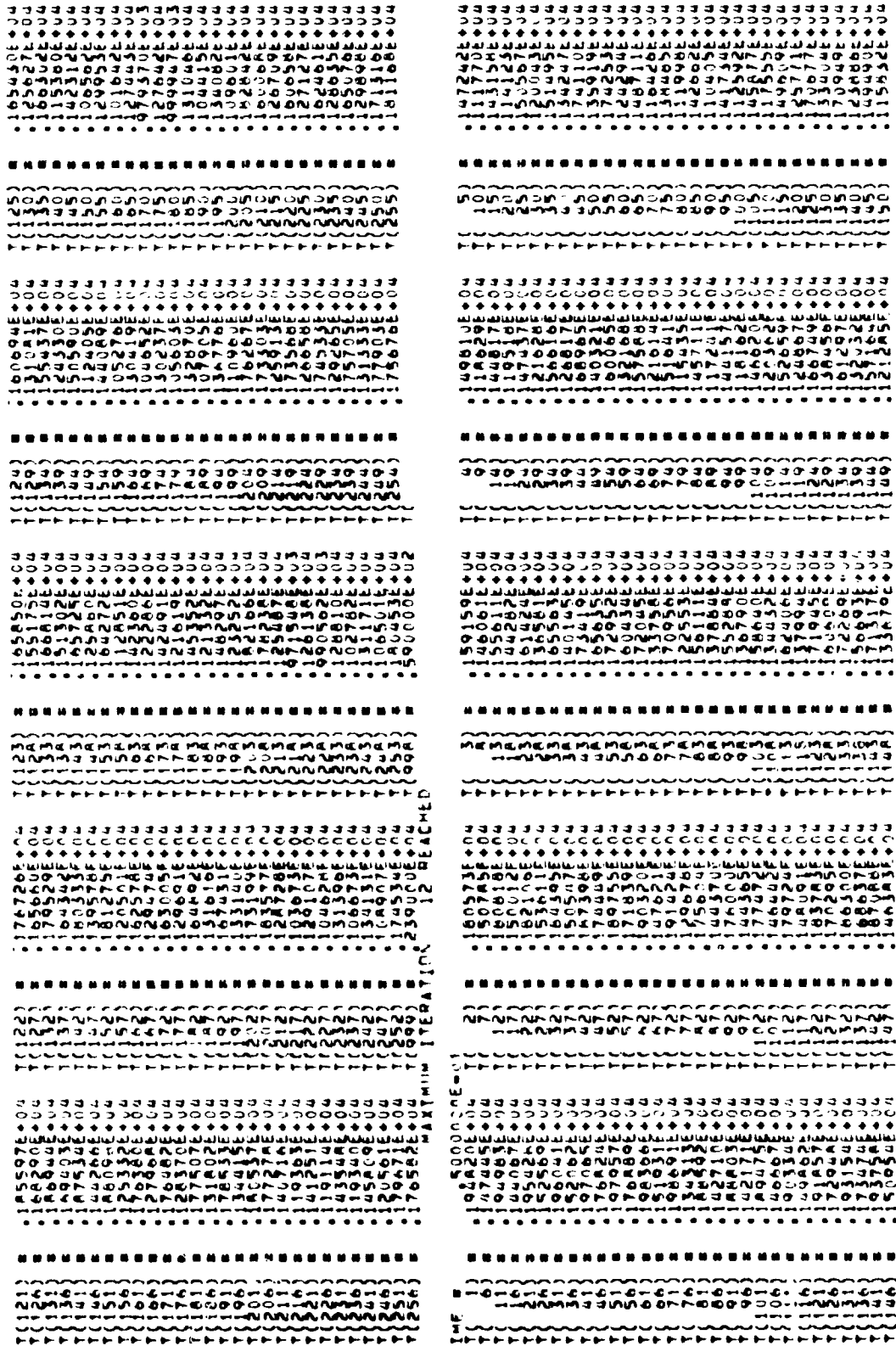


Figure 5-9. Model 2B Output (Sheet 12 of 16)

REPRODUCIBILITY OF THE ORIGINAL PAGE IS POOR

Figure 5-9 displays two columns of highly distorted and illegible text, likely representing a degraded scan of a document page. The text is severely blurred and contains many artifacts, making it impossible to read.

Figure 5-9. Model 2B Output (Sheet 13 of 16)

PROBABILITY OF THE  
LAW IS 100%

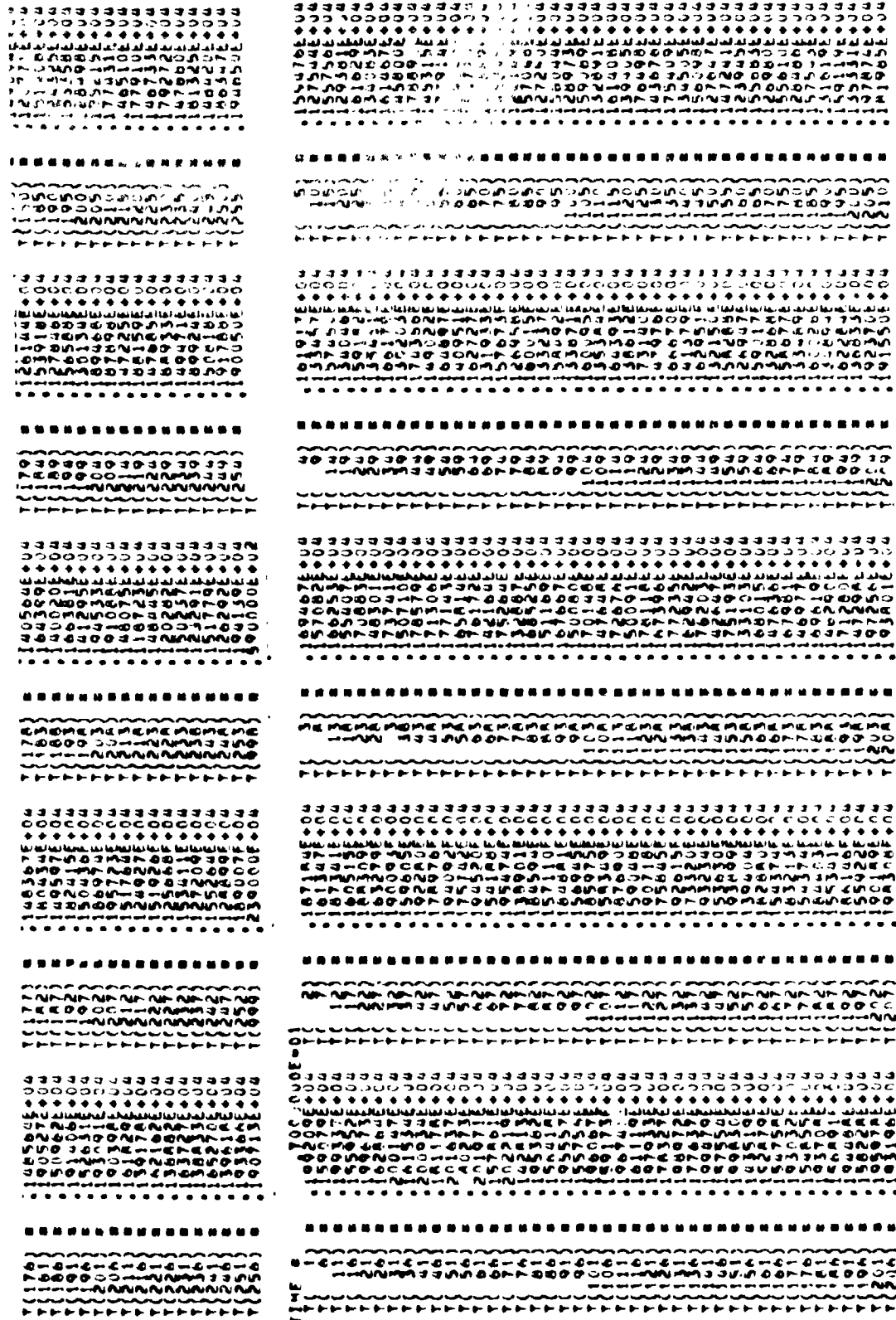


Figure 5-9. Model 2 B Output (Sheet 14 of 16)

REPRODUCIBILITY OF THE ORIGINAL PAGE IS POOR

The image displays a grid of 20 blocks of text arranged in 10 rows and 2 columns. Each block contains several lines of text that are extremely noisy and difficult to read. The text appears to be a mix of characters, including letters, numbers, and symbols, but is largely illegible due to the quality of the reproduction. The noise is most prominent in the first few rows of each block, where the characters are distorted and overlapping. The overall appearance is that of a very poor quality scan of a document page.

Figure 5-9. Model 2 B Output (Sheet 15 of 16)



```

T(241)
T(244)
T(251)
T(250)
=====
1740139E+04
1504170E+04
1198199E+04
1198434E+04
T(247)
T(257)
T(259)
=====
1540024E+04
1414144E+04
194100E+04
23000E+04
T(243)
T(247)
T(253)
T(254)
=====
162328E+04
18100E+04
59000E+04
T(249)
T(254)
T(255)
=====
161193E+04
146771
149206E+04
T(245)
T(250)
T(255)
=====
19706E+04
192039E+04
199195E+04

```

REPRODUCIBILITY OF THE ORIGINAL PAGE IS POOR

Figure 5-9. Model 2B Output (Sheet 16 of 16)

REPRODUCIBILITY OF THE ORIGINAL PAGE IS POOR

```

3STURE
NUMBD = 2,
NUMTR = 272,
NUMCCH = 734,
NUMTCN = 1628,
NUMNDD = 1000,
NUMFLX = 0,
NSTW = 17000,
NEVALJ = 14,
NUMTOT = 274,
NUMSCH = 2291,
NUMHAD = 80,
SEND

THIS FILE REQUIRES A DATA AREA OF
274 0 500 274 274 274 274 274 274 274 274 274 274 274 274
4720 35272 500 3500 3500 3500 3500 3500 3500 3500 3500 3500 3500 3500 3500
HIGHEST MEMORY IN HEXADECIMAL IS 3500 3500 3500 3500 3500 3500 3500 3500 3500 3500 3500 3500 3500 3500
274 272 14 730 100 80 100 0002330 0 2291 17000

1468 274 160 1000 0
572 14 3808 2291
3734 14 4720 14958
6665 3899 3729 12707
17000 4720 31998

```

Figure 5-10. Model 2C Output (Sheet 1 of 16)

LANGLEY MODEL THERMAL SECTION  
NUMBER OF ITERATED NODES = 272  
NUMBER OF BOUNDARY NODES = 734  
NUMBER OF CONDUCTION LINKS = 80  
NUMBER OF RADIATION LINKS = 0  
NUMBER OF HEAT SOURCES = 0

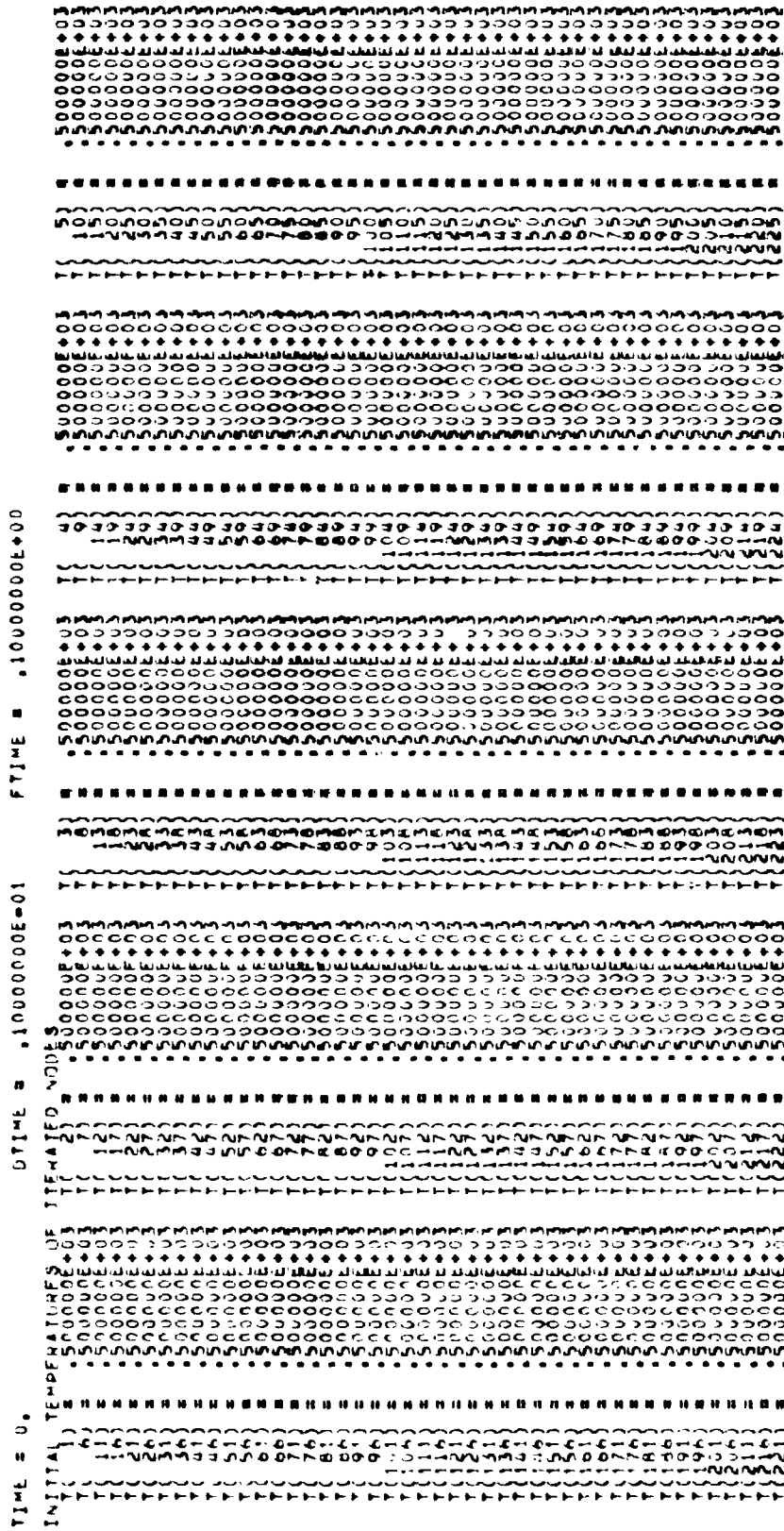


Figure 5-10. Model 2C Output (Sheet 2 of 16)



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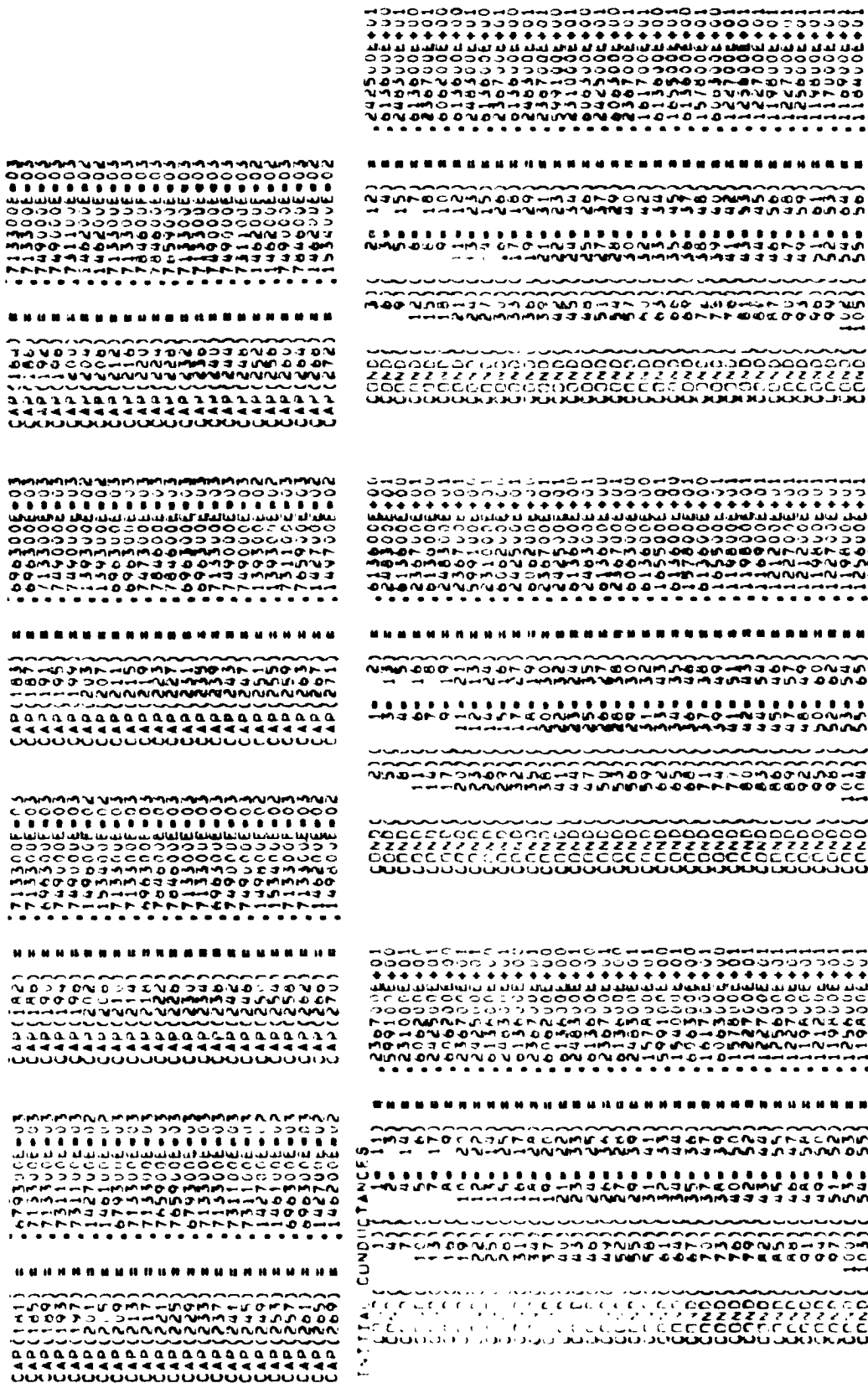


Figure 5-10. Model 2C Output (Sheet 4 of 16)

REPRODUCIBILITY OF THE ORIGINAL PAGE IS POOR

[The text in this block is extremely faint and illegible, appearing as a series of horizontal lines of varying lengths and densities. It likely represents a large table or a list of data that has been severely degraded in quality during the scanning process.]

Figure 5-10. Model 2C Output (Sheet 5 of 16)



REPRODUCIBILITY OF THE ORIGINAL PAGE IS POOR

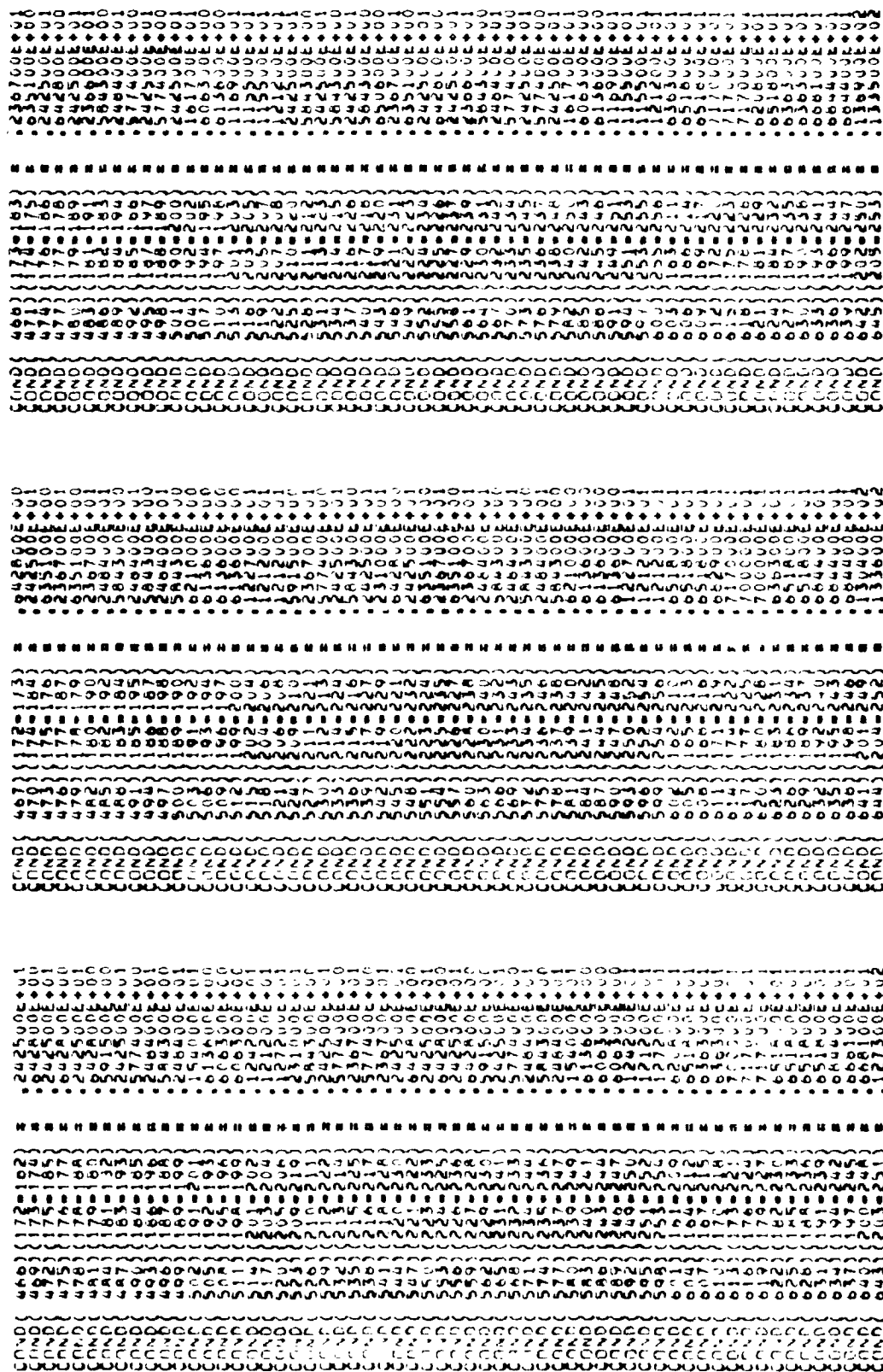


Figure 5-10. Model 2C Output (Sheet 7 of 16)



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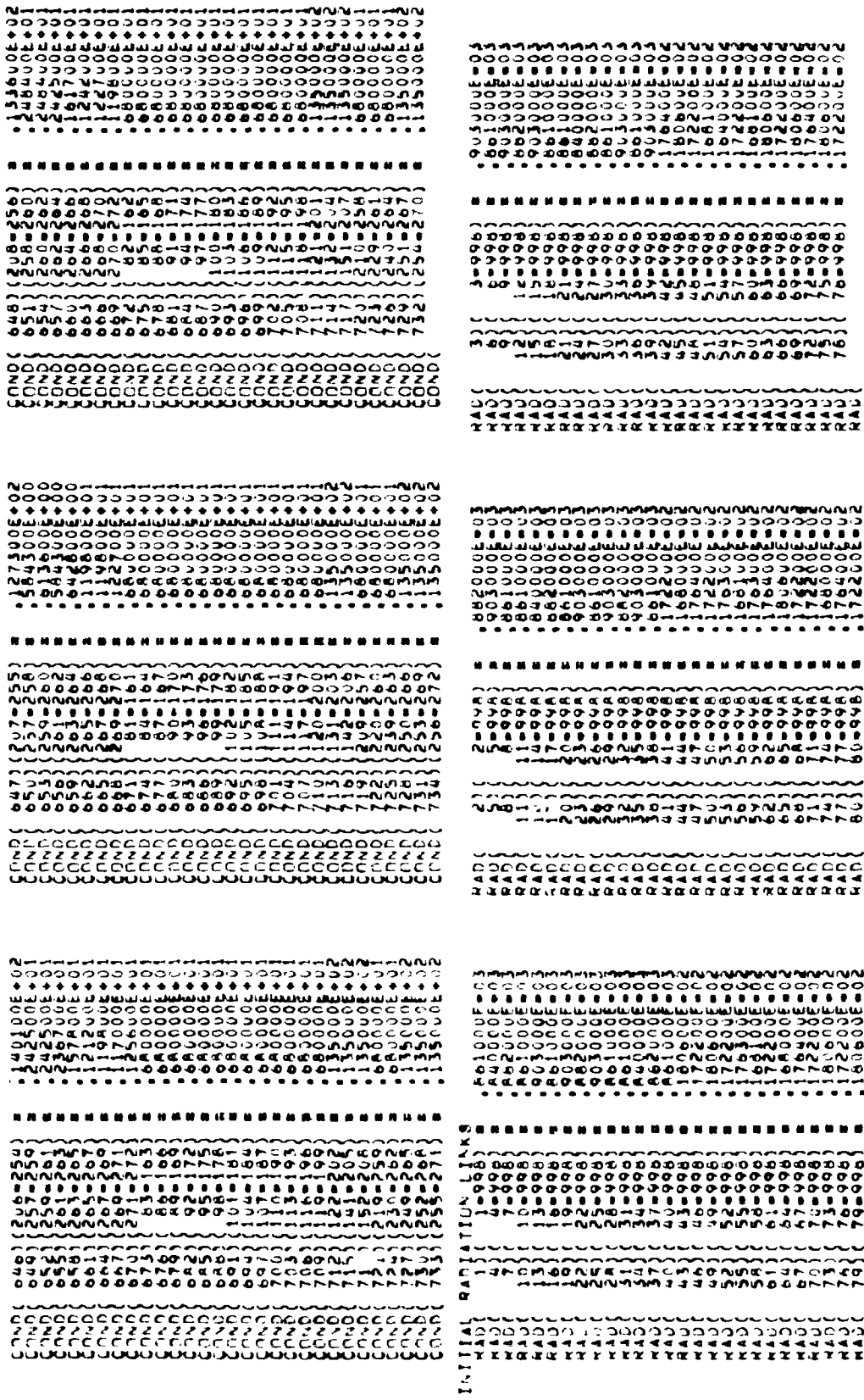


Figure 5-10. Model 2C Output (Sheet 8 of 16)

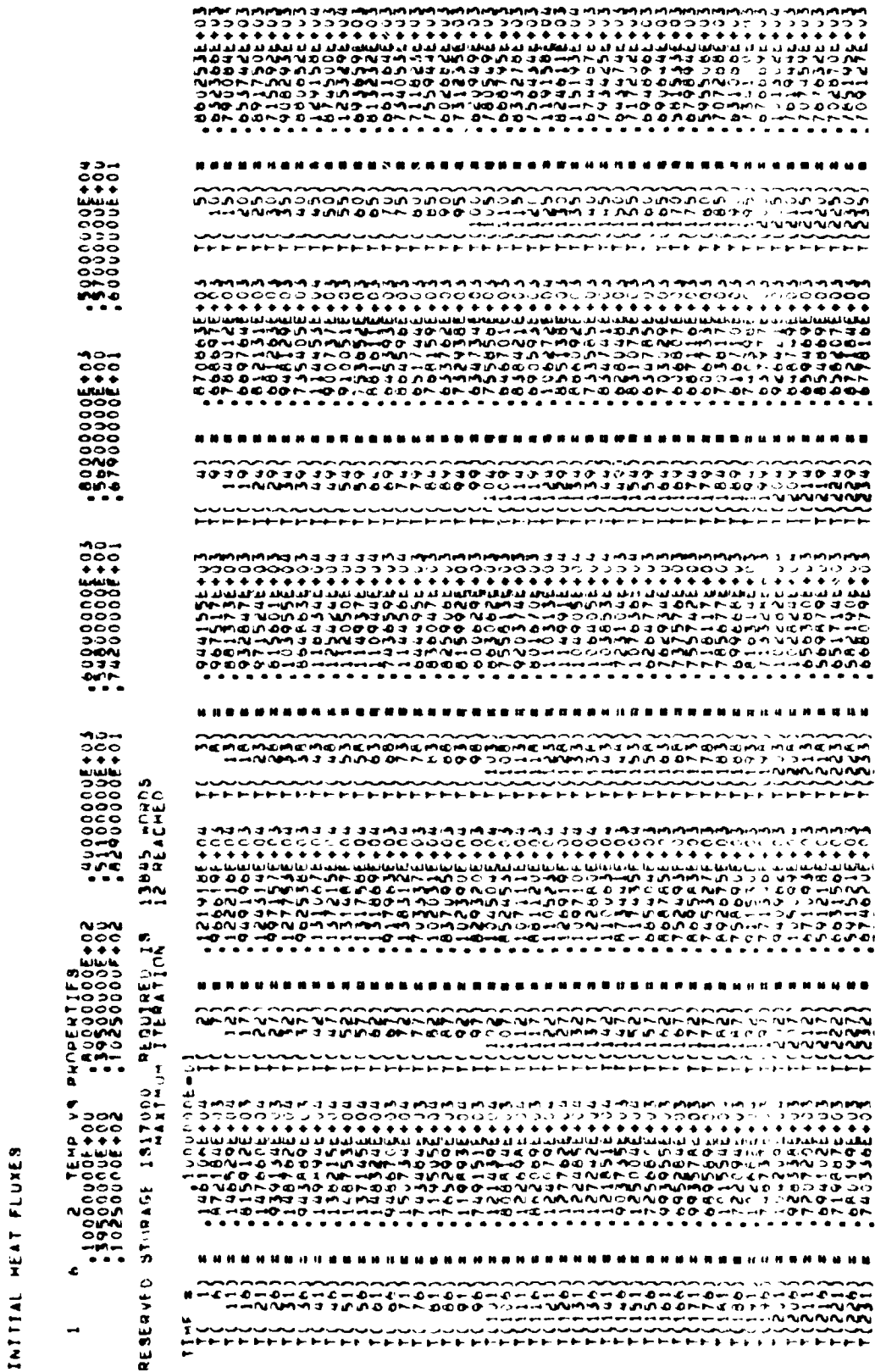


Figure 5-10. Model 2C Output (Sheet 9 of 16)



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Figure 5-10. Model 2C Output (Sheet 11 of 16)

REPRODUCIBILITY OF  
ORIGINAL PAGE INFORMATION

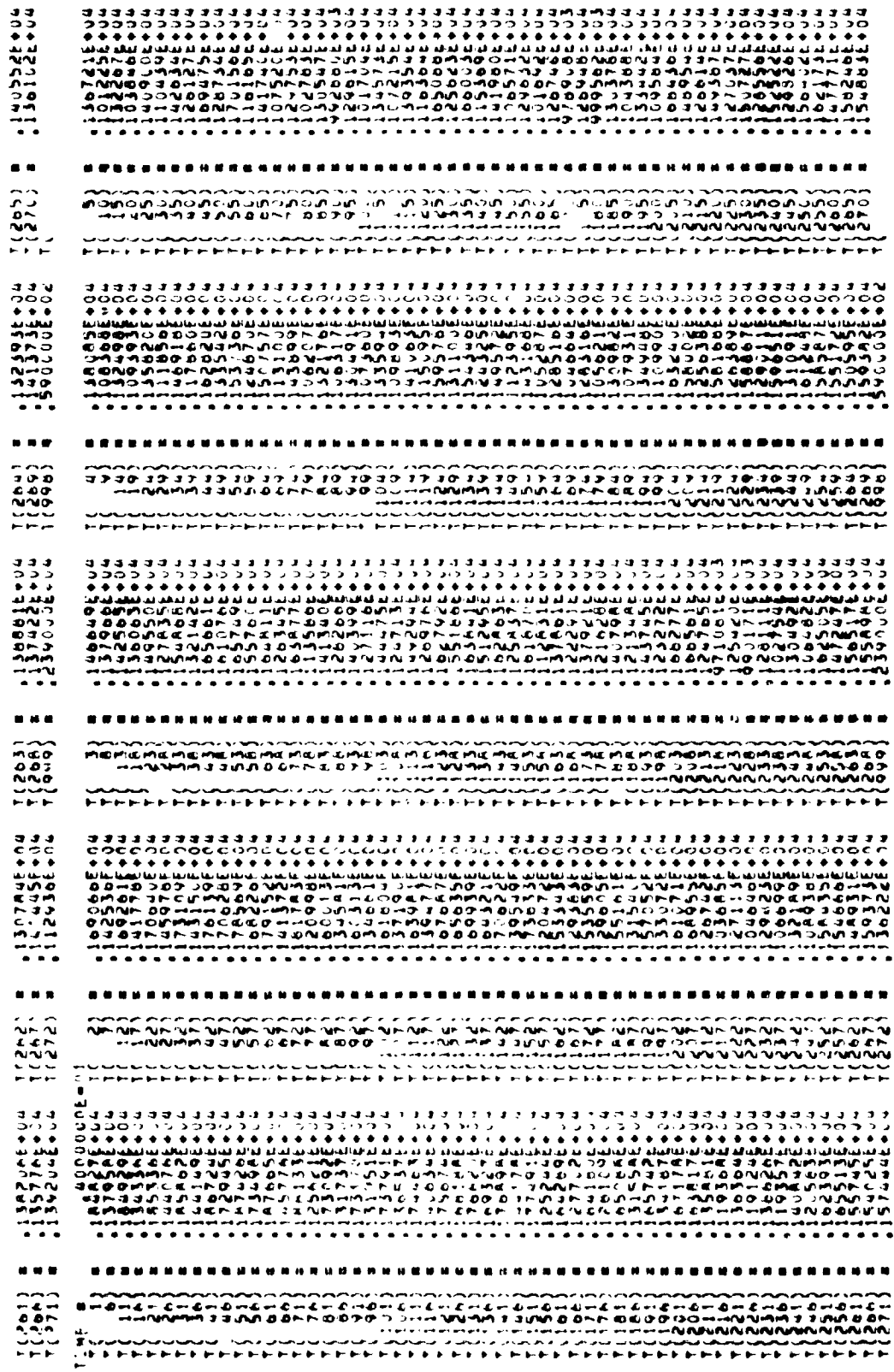


Figure 5-10. Model 2C Output (Sheet 12 of 16)

REPRODUCIBILITY OF THE ORIGINAL PAGE IS POOR



Figure 5-10. Model 2C Output (Sheet 13 of 16)



Figure 5-10. Model 2C Output (Sheet 14 of 16)

REPRODUCIBILITY OF THE ORIGINAL PAGE IS POOR

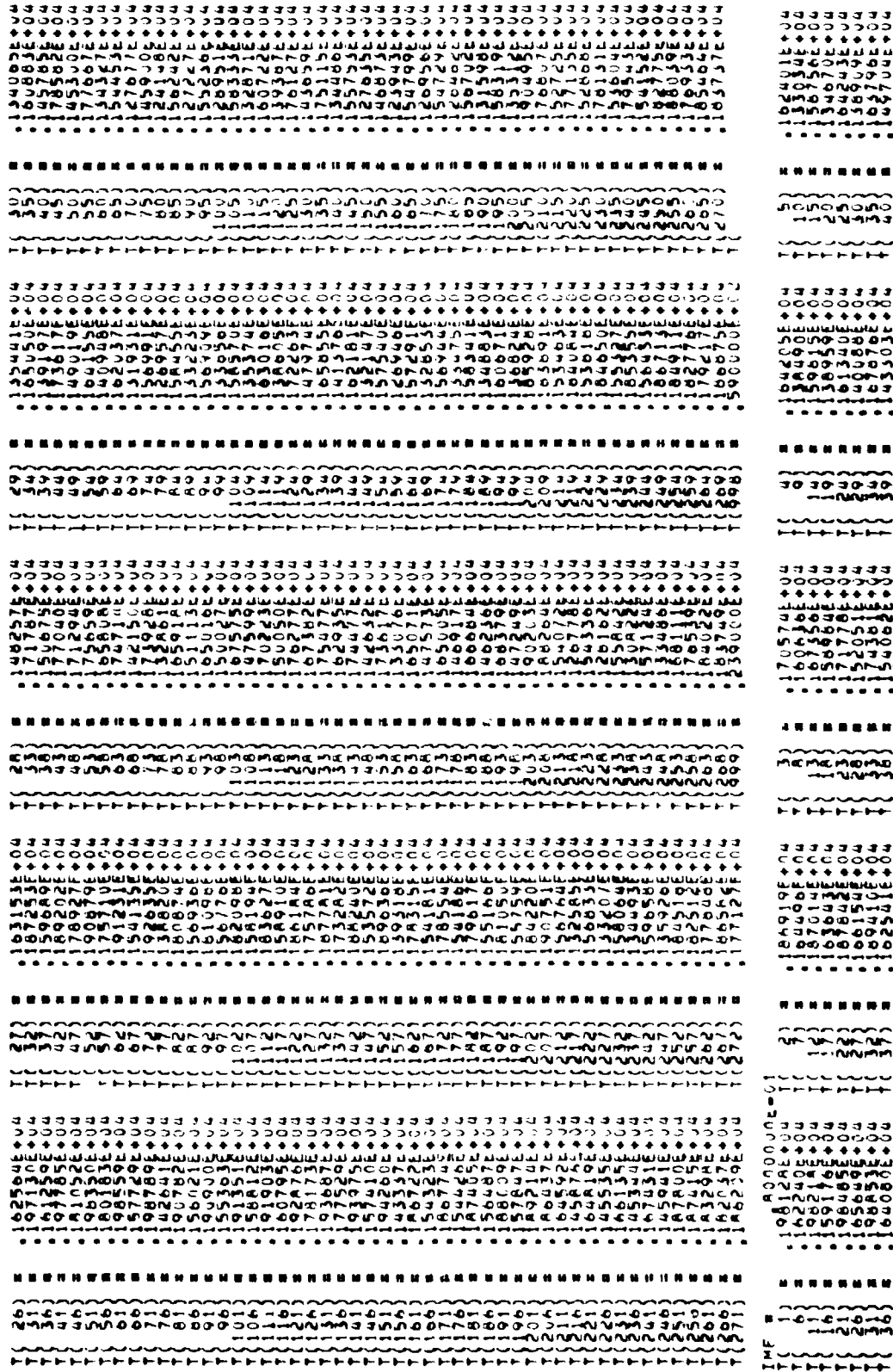


Figure 5-10. Model 2C Output (Sheet 15 of 16)



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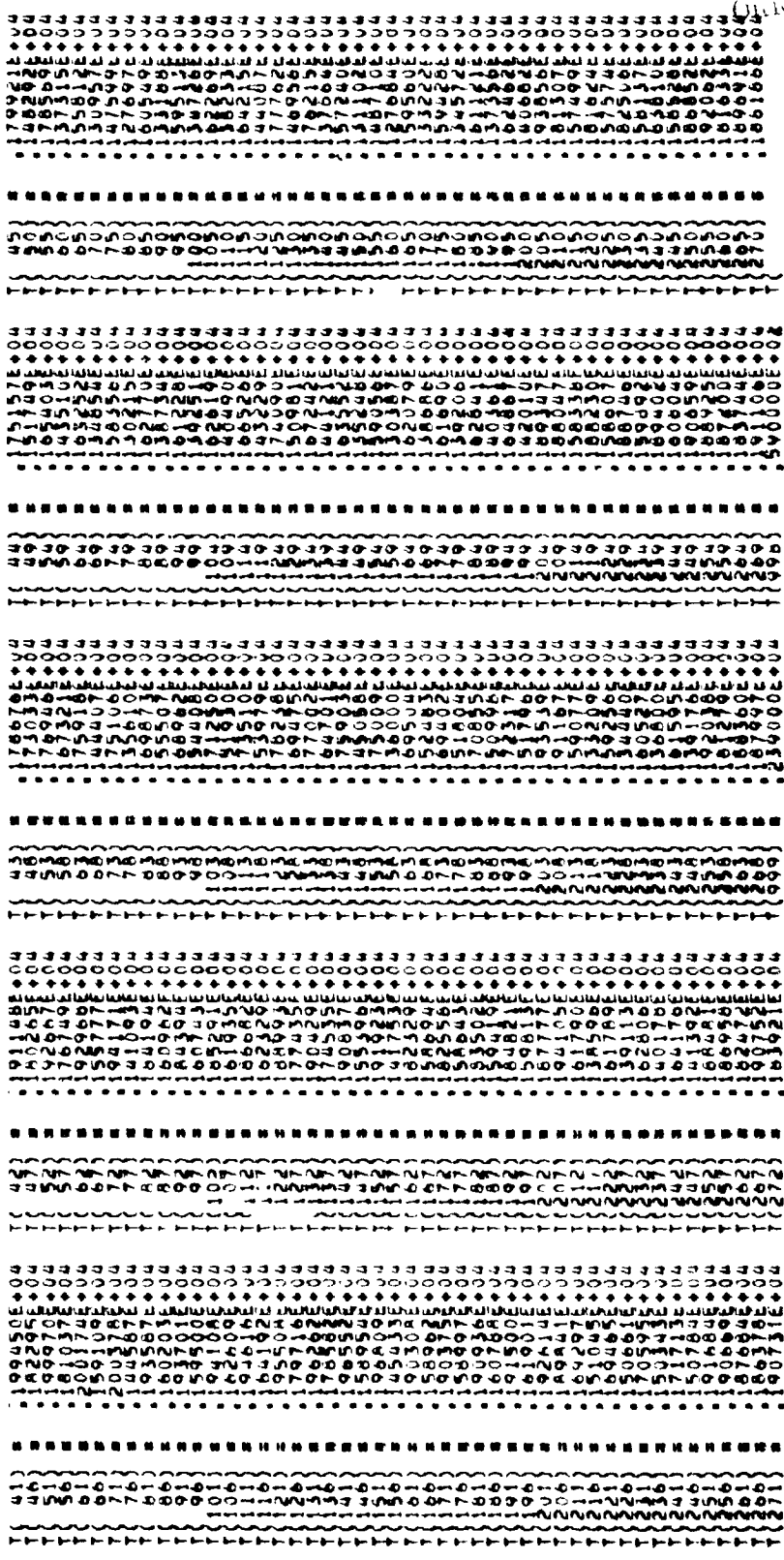


Figure 5-10. Model 2C Output (Sheet 16 of 16)

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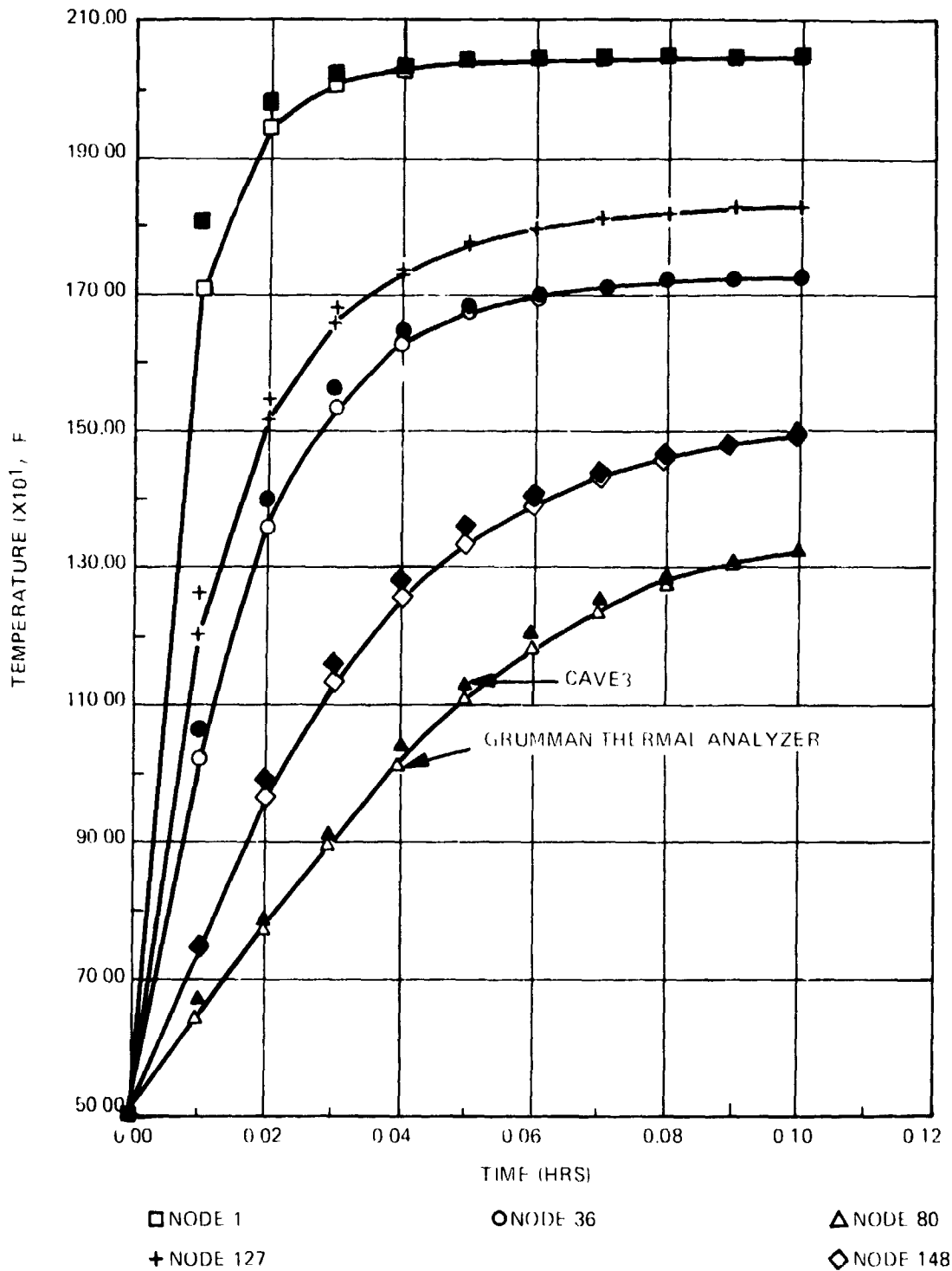


Figure 5-11. Sample Problem No. 2, Model 2A, Verification Plot

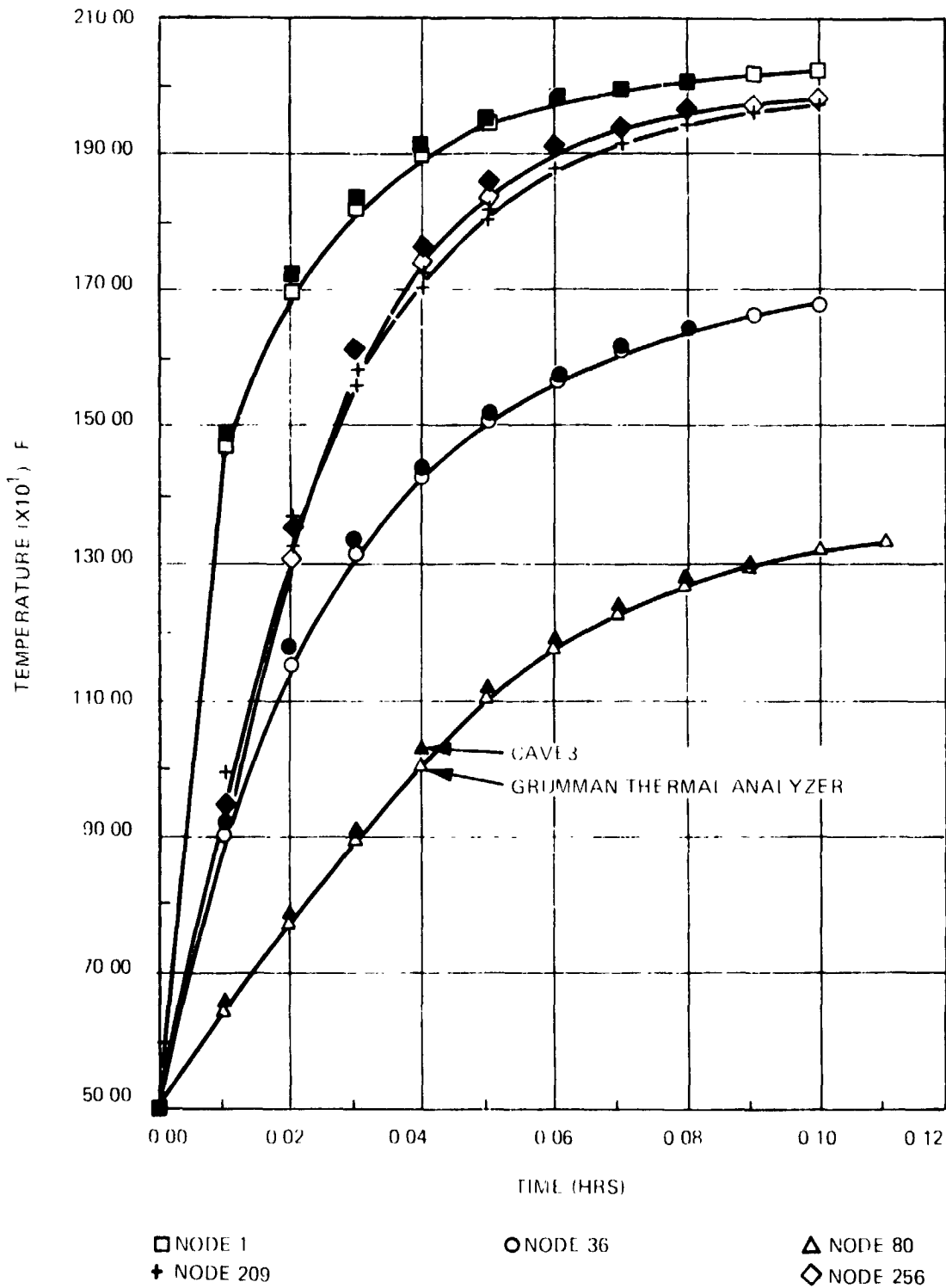


Figure 5-12. Sample Problem No. 2, Model 2B, Verification Plot

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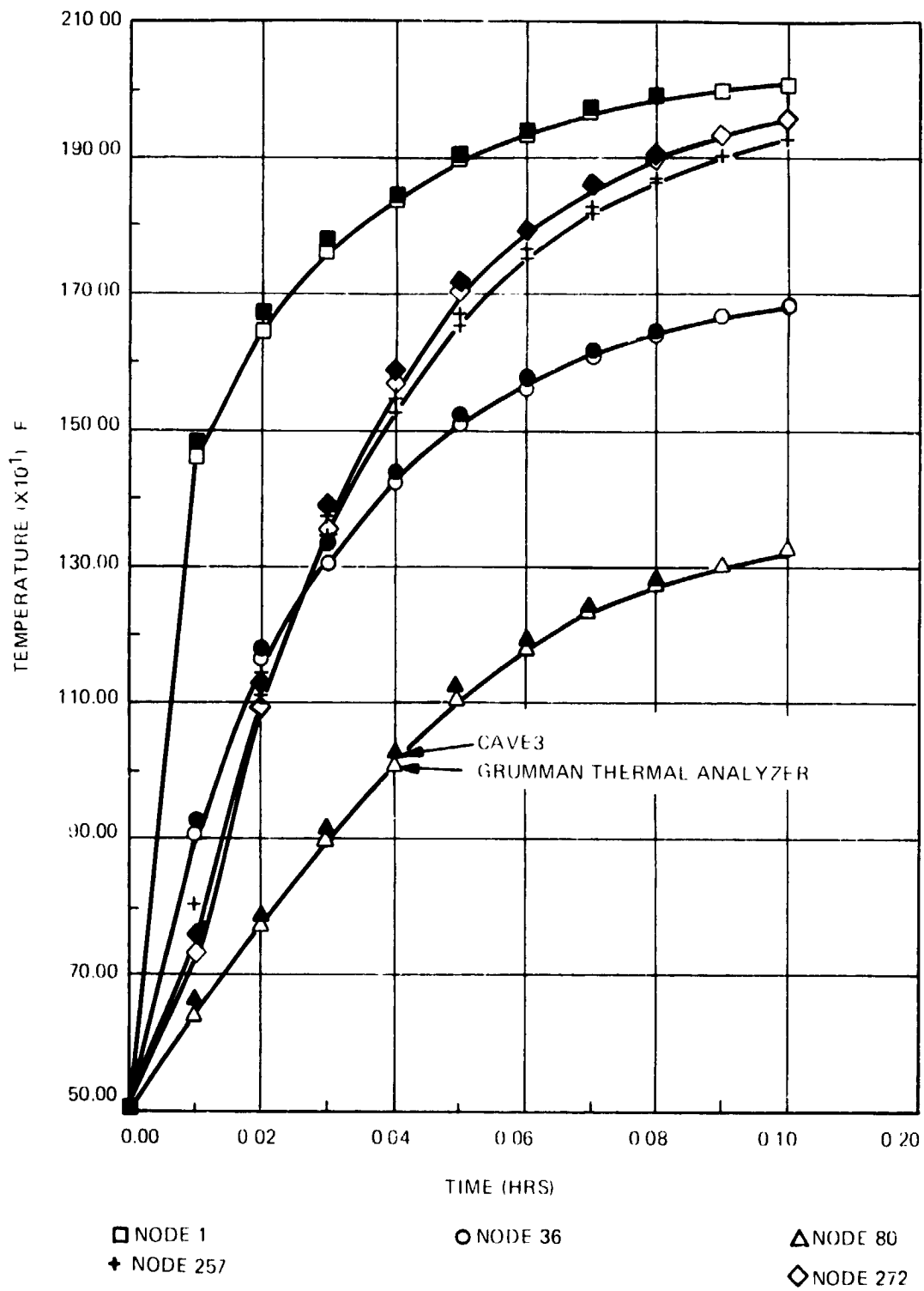


Figure 5-13. Sample Problem No. 2, Model 2C, Verification Plot

Section 6

PROGRAMMER ORIENTED DOCUMENTATION

This section presents the details of the CAVE3 organization and structure. A simplified flow diagram of CAVE3 is presented in Figure 6-1.

CAVE3 is organized in a main program with 18 subroutines. The list of subroutines is given in Table 6-1 together with the function of each subroutine. Many subroutines are identical to subroutines used in the CAVE (Ref (1)) and CAPE codes (NASA CR-2435). Figure 6-2 presents the organization of CAVE3 in terms of the more important subroutine calls. Table 6-2 gives the variable list for CAVE3.

Flow charts or descriptions for each subroutine are given in Figures 6-3 through 6-19. They are arranged in alphabetical order. For convenience and completeness, they are given for subroutines that are identical to the CAVE and CAPE routines as well as the new subroutines.

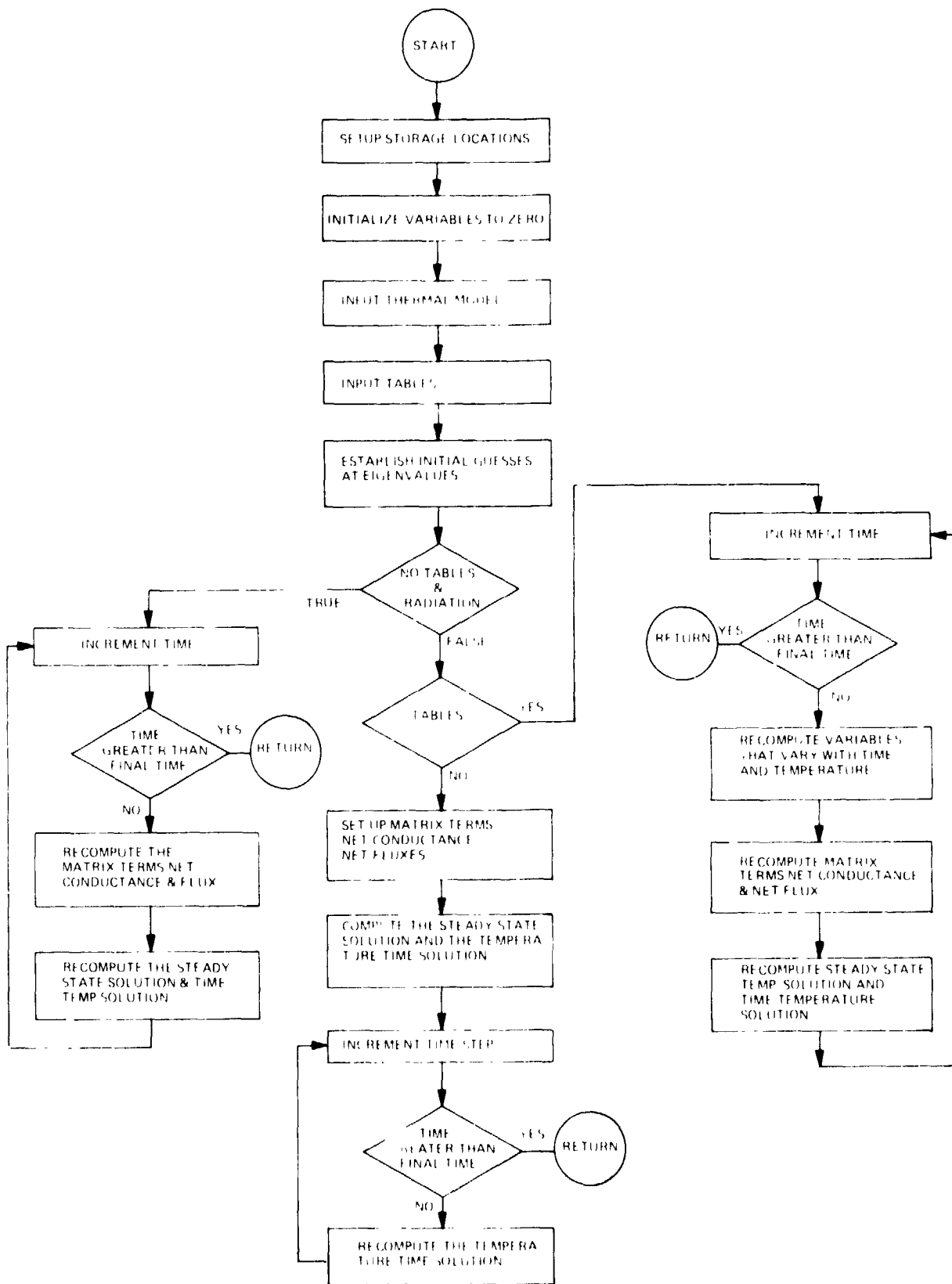


Figure 6-1. Simplified Flow of Logic in CAVE3

Table 6-1. Subroutine Descriptions

Routine	Description
CAVE	Main routine - Sets up storage array and dynamically allocate core storage to match the input requirements.
AORDER	Orders a set of real numbers.
BJEN	Obtains dominant eigenvectors and eigenvalues of a given matrix (using Jennings Method of simultaneous vector iteration).
SWITCH	Utility routine to convert columns of a matrix to rows or vice versa.
SCAPR2	Computes scalar product of two vectors.
CAVE3	Establishes the main flow of the program.
CINIT	Initializes variables to zero.
DSCT	Computes the steady state and time dependent solutions.
DISPLA	Prints scalars, vectors, rectangular matrices, packed symmetric matrices and Hessenburg matrices.
EVECGS	Prepares approximate guesses for the eigenvectors.
LLTRAN	Cholesky decomposition of a positive definite symmetric matrix.
ORNML	Carries out the standard Gram-Schmidt orthonormalization of a group of vectors.
RVORDR	Reorders estimated eigenvalues according to magnitude.
SETUP	Establishes the CONNET and BFLUX arrays which are the matrix diagonal terms: the net conductance and net flux terms respectively.
XTABS	Table read-in routine.
XINTP	Finds values of several dependent variables from a table by linear interpolation on a single independent variable.
TABLE	Determines which variables are changing and calls the appropriate tables to compute the result. Changes the COND, CAP, Q and T arrays as required.
TRISLV	Solution of a system of N linear equations using the Cholesky factor.
XREDE	Input routine.

Table 6-2. Variable List

The following is an alphabetical listing of the principle program variables and their definitions. Most are stored in COMMON. Other variables are used as indices, counters, or intermediate storage locations; but their functions may easily be determined from an inspection of the program listing. Input variables are indicated by the letter "I". Array names show their dimensions.

BFLUX (NUMTOT)		Net Flux of each node including heat sources and boundary conductance times boundary temperature.
BUFF (20)	I	Buffer region for listing of title cards.
CAP (NUMTOT)	I	Thermal capacitance. Subscript is node numbers. Inputted as mass x specific heat, stored as $1/\sqrt{(\text{mass} \times \text{specific heat})}$
COND (NUMCON)	I	Thermal conductance. Subscript is conductance number (UA)
CONNET (NUMTOT)		Net conductance of each node.
CP1 (NUMITR)		Storage location for previously computed value of CAP (N) used for readjusting CAP (N) when properties change.
DTIME	I	Time step
DUM		Input buffer and intermediate storage in several areas
EVAL (NEVALV)		eigenvalues
EVEC (NUMITR, NEVALV)		eigenvector
FCT (50)		Table look-up return
FTIME	I	End computing time
IDIAG	I	Diagnostic Flag
IFLUX	I	Flux output flag
II	I	"Limit" for multiple parameter input (see input data discussion Section)



Table 6-2. Variable List (Cont'd)

IJ2 (NUMTOT)	I	Table of subscripted node representing variable physical property
JJ	I	"Spacing" for multiple parameter input (see input data discussion Section)
KNBN		Number of boundary nodes
KNIN		Number of iterated nodes and boundary nodes
KNQ		Number of heat sources
KODE	I	Program control parameter
LFLAG (50)	I	Table flag indicating type of table
L1 (50)	I	Number of values of independent variable in a table. Subscript is table number
L2 (50)	I	Number of dependent variables in a table. Subscript is table number.
MAXB		Total number of nodes iterated and boundary
MAXT		Total number of iterated nodes
N3		$N4 + N5$
N4		Number of conductances
N5		Number of radiation couplings
NCOND (2, NUMCON)	I	List of nodes connected by conductors. First subscript reserves room for two nodes. Second subscript is conductor number
NEVALU	I	Number of eigenvalues to be used.
NIN (NUMITR)		List of node numbers of iterated nodes
NLAST (50)		Position of independent variable in STG array from previous table look-up. Subscript is table number
NMAXB		High node number of boundary nodes

Table 6-2. Variable List (Cont'd)

NMTRIC	I	Flag indicating units of input
NODE (NUMNOD)		Array containing node position in NEN array as function of node label
NPOS (50)		Position of variable list for table in STG array. Subscript is table number
NQ (NUMFLX)	I	List of nodes to which heat sources are applied. Subscript is source number
NRAD (2, NUMRAD)	I	List of nodes connected by radiation couplings. First subscript reserves space for two nodes. Second subscript is radiation coupling number
NSTR	I	Reserve Storage words
NTABS (50)		Number of tables
Q (NUMFLX)	I	Heat source. Subscript is source number
NUMBND	I	Number of boundary nodes
NUMCON	I	Number of conductances
NUMNOD	I	Number of highest nodes
NUMFLX	I	Number of fluxes
NUMTR	I	Number of iterated nodes
NUMRAD	I	Number of radiations
NUMSCR	I	Storage variables
NUMTOT		Number of iterated and boundary nodes
Q1 (NUMCON)		Heat flux from node to each adjacent nodes, accumulated over each time
SIG	I	Stephen-Boltzmann constant
STG (5000)	I	Independent and dependent table variables
T (NUMTOT)	I	Temperature of iterated and boundary nodes. Subscript is node number

Table 6-2. Variable List (Cont'd)

TIME	I	Time
TSS (NUMITR)		Steady State Temperature array
XK1 (NUMITR)		Initial value of conductivity
XNOD (NUMCON)		Conductance Constant $A/\Delta X$ in x direction
YNOD (NUMCON)		Conductance Constant $A/\Delta X$ in y direction

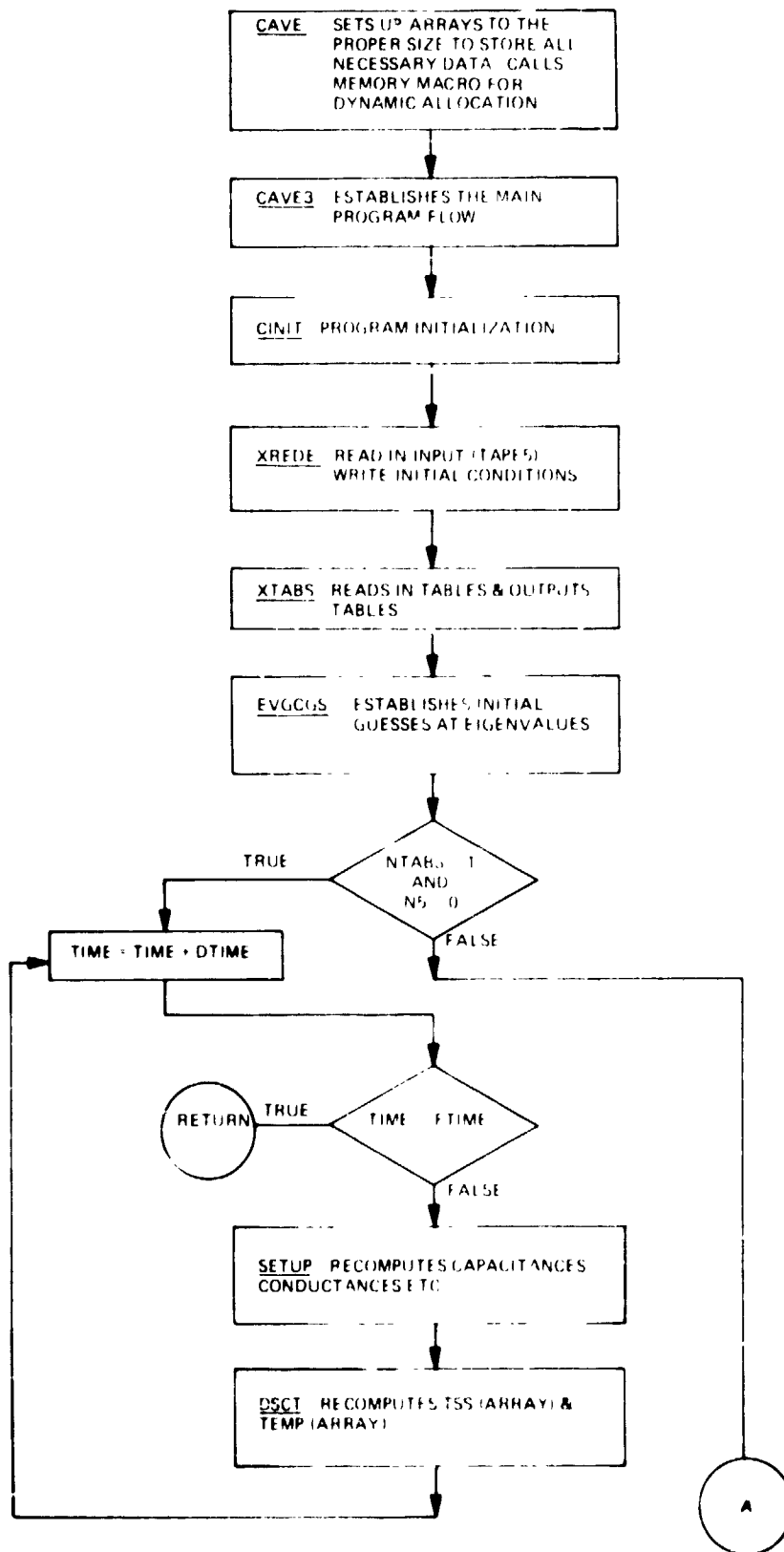


Figure 6-2. Organization of CAVE3 in Terms of the More Important Subroutine Calls (Sheet 1 of 2)

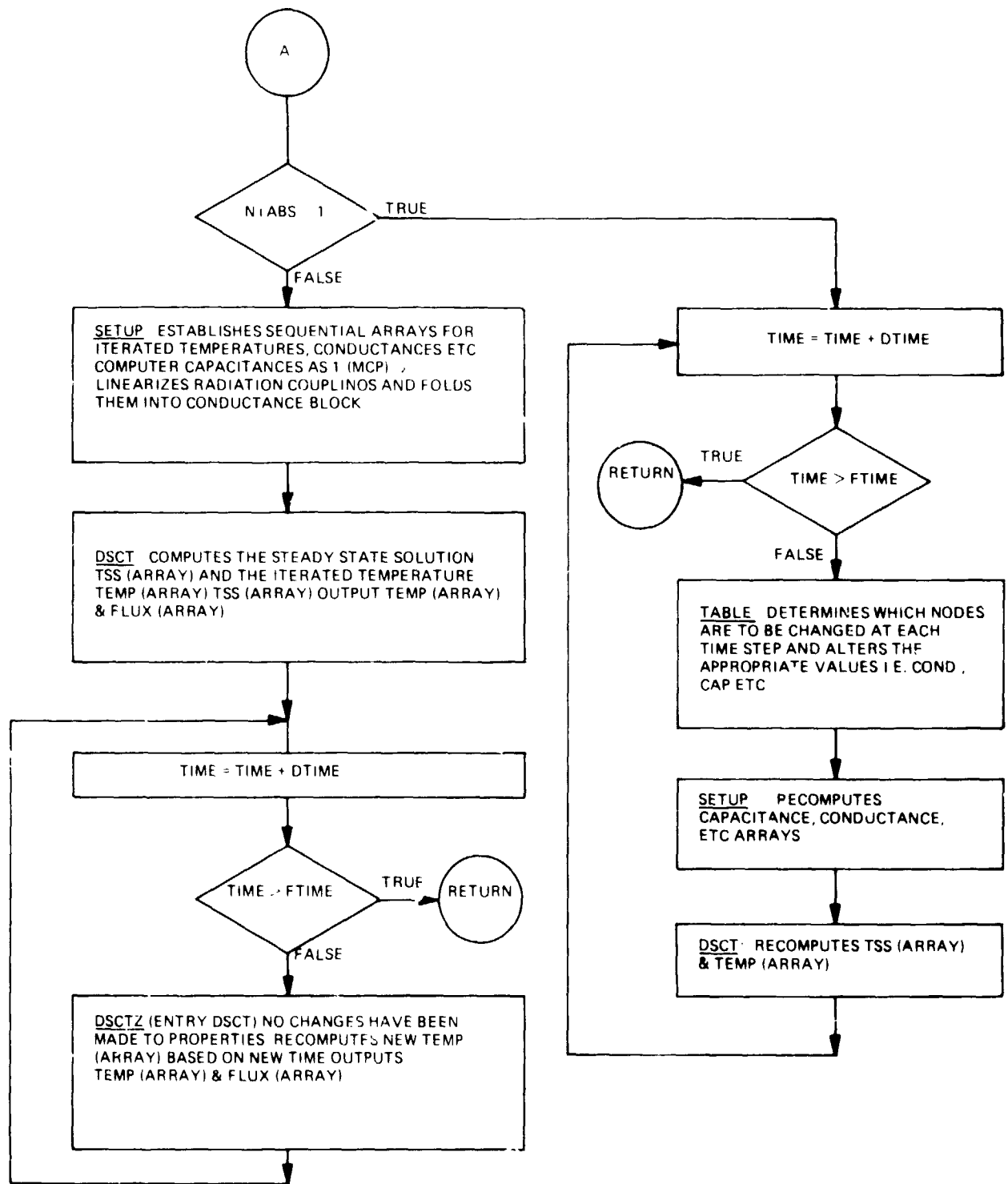


Figure 6-2. Organization of CAVE3 in Terms of the More Important Subroutine Calls  
(Sheet 2 of 2)

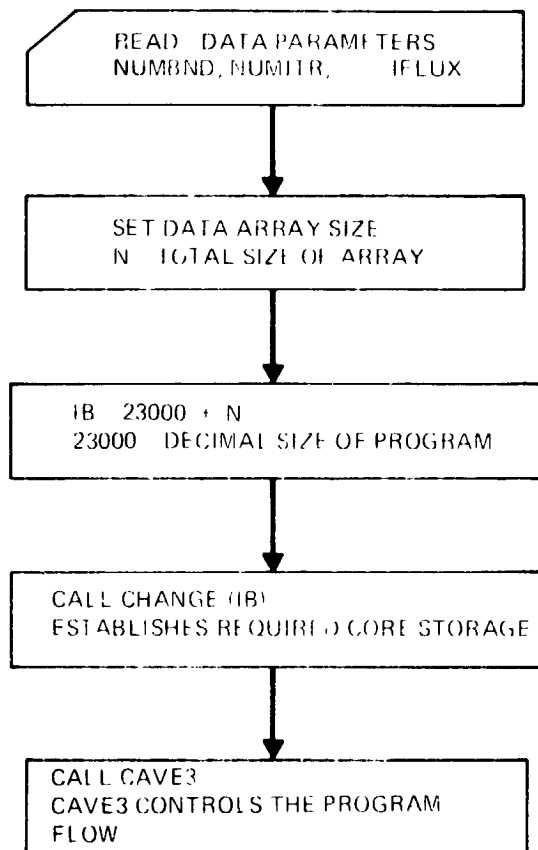


Figure 6-3. Main Routine Flow Chart

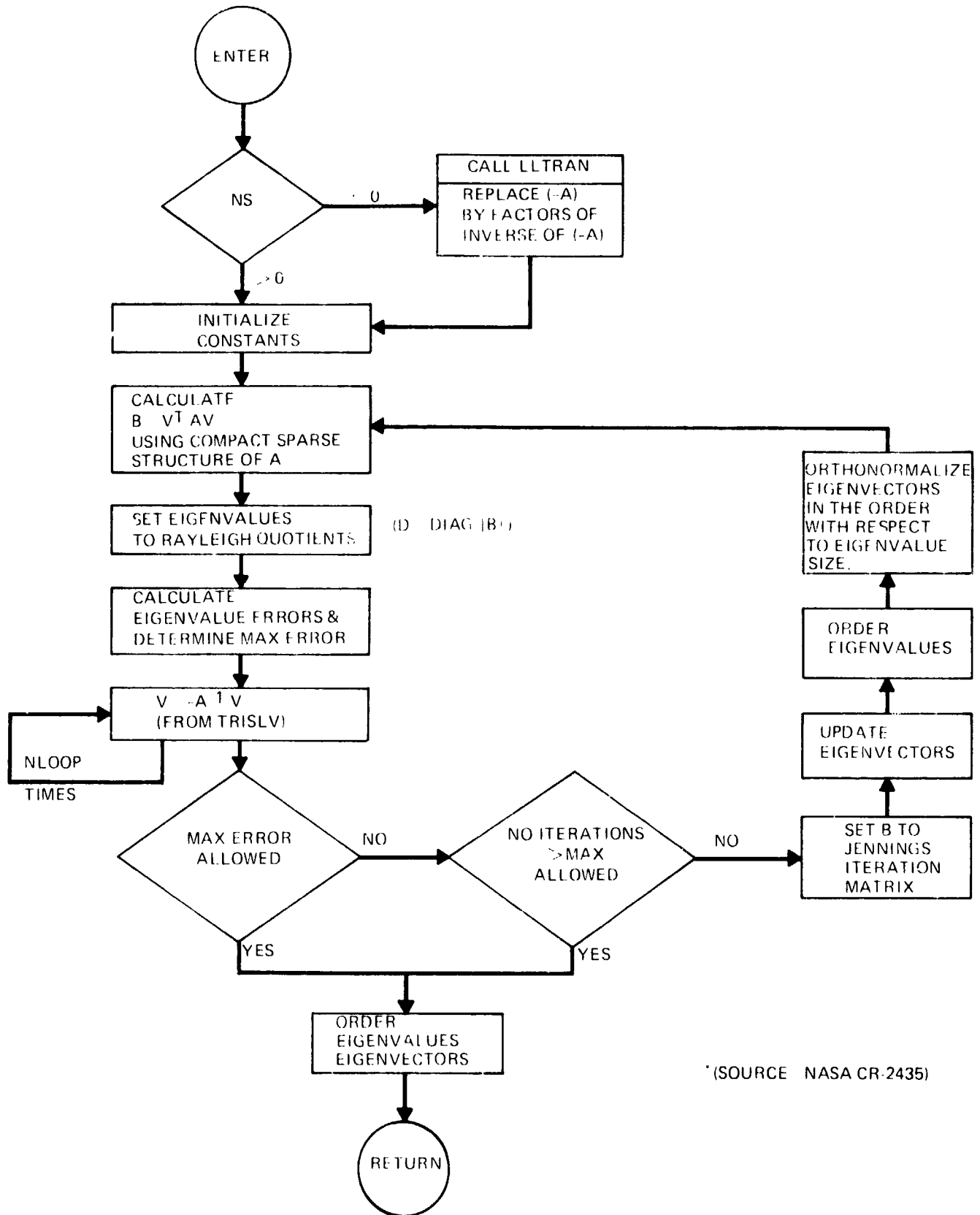
PURPOSE: ORDER A SET OF REAL NUMBERS

CALLING SEQUENCE: CALL AORDER (A, N, IPERM)

	<u>NAME</u>	<u>DIMENSION</u>	<u>DESCRIPTION</u>
INPUT	A N	A(N)	ELEMENTS TO BE ORDERED NUMBER OF ELEMENTS =  N  N > 0 INCREASING ORDER N < 0 DECREASING ORDER
OUTPUT	IPERM	IPERM(N)	ORDER VECTOR - SPECIFIES THE SEQUENCE OF ELEMENT INDEX NUMBERS WHICH WILL PRESENT A AS AN ORDERED SET, i.e. DO 100 I = 1, N 100 WRITE (6, 1) A (IPERM(I)) 1 FORMAT (F 10.5)  WILL LIST A AS AN ORDERED ARRAY

AORDER CALLS NO OTHER SUBROUTINES

Figure 6-4. Subroutine AORDER Description  
(From NASA CR-2435)



(SOURCE NASA CR-2435)

Figure 6-5. Subroutine BIJEN Flow Chart\*



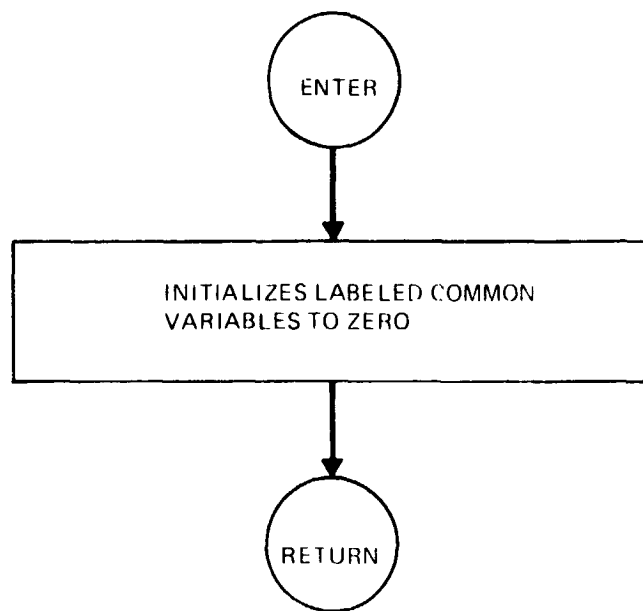


Figure 6-6. Subroutine CINIT Flow Chart

TITLE: DISPLA -- Prints scalars, vectors, rectangular matrices, packed symmetric matrices, and Hessenberg matrices.

AUTHOR: M.J. Rossi

DATE: September 1973

APPLICABLE COMPUTERS: IBM 360/370, CDC 6000 SERIES

SOURCE LANGUAGE: FORTRAN IV

PURPOSE: To simplify printing of mathematical types of data structures in an easily read format which allows titles and index labels

METHOD: FORTRAN looping and write statements which indexes and addresses arrays according to their type.

USAGE: Call DISPLA (X, NFILE, TITLE, KAR, KIND, NROWS, NCOLS, MID).

X -- Input -- Array of one or more values to be printed  
 NFILE -- Input -- FORTRAN unit for printing  
 TITLE -- Input -- Vector of KAR characters used as title.  
 KAR -- Input -- Number of characters in above string  
 KIND -- Input -- Type of mathematical data structure.  
   = 0 scalar (or vector printed on one line with no index)  
   1 vector of |NROWS| elements, indexed  
   = 2 Rectangular |NROWS| by NCOLS matrix -- Dimension (MID, \*)  
   = 3 Packed Symmetric matrix of order |NROWS|

  -  $\begin{bmatrix} 1 & 2 & 4 \\ 2 & 3 & 5 \\ 4 & 5 & 6 \end{bmatrix}$  -- lower triangular partial rows if NROWS positive

  -  $\begin{bmatrix} 1 & 2 & 3 \\ 2 & 4 & 5 \\ 3 & 5 & 6 \end{bmatrix}$  -- lower triangular partial columns if NROWS negative

  - 4 - Transposed Hessenberg matrix of order NROWS -- Dimension (MID, MID)

NROWS -- Input -- Number of elements if KIND = 0 or 1  
           -- Number of rows if KIND = 2  
           -- Matrix order if KIND = 3 or 4

NCOLS -- Input -- Number of columns if KIND = 2  
           -- Ignored otherwise

MID -- Input -- Matrix Dimension if KIND = 2 or 4  
           -- Ignored otherwise

SUBROUTINE REQUIRED: SWITCH

Figure 6-7. Subroutine DISPLA Description  
 (From NASA CR-2435)

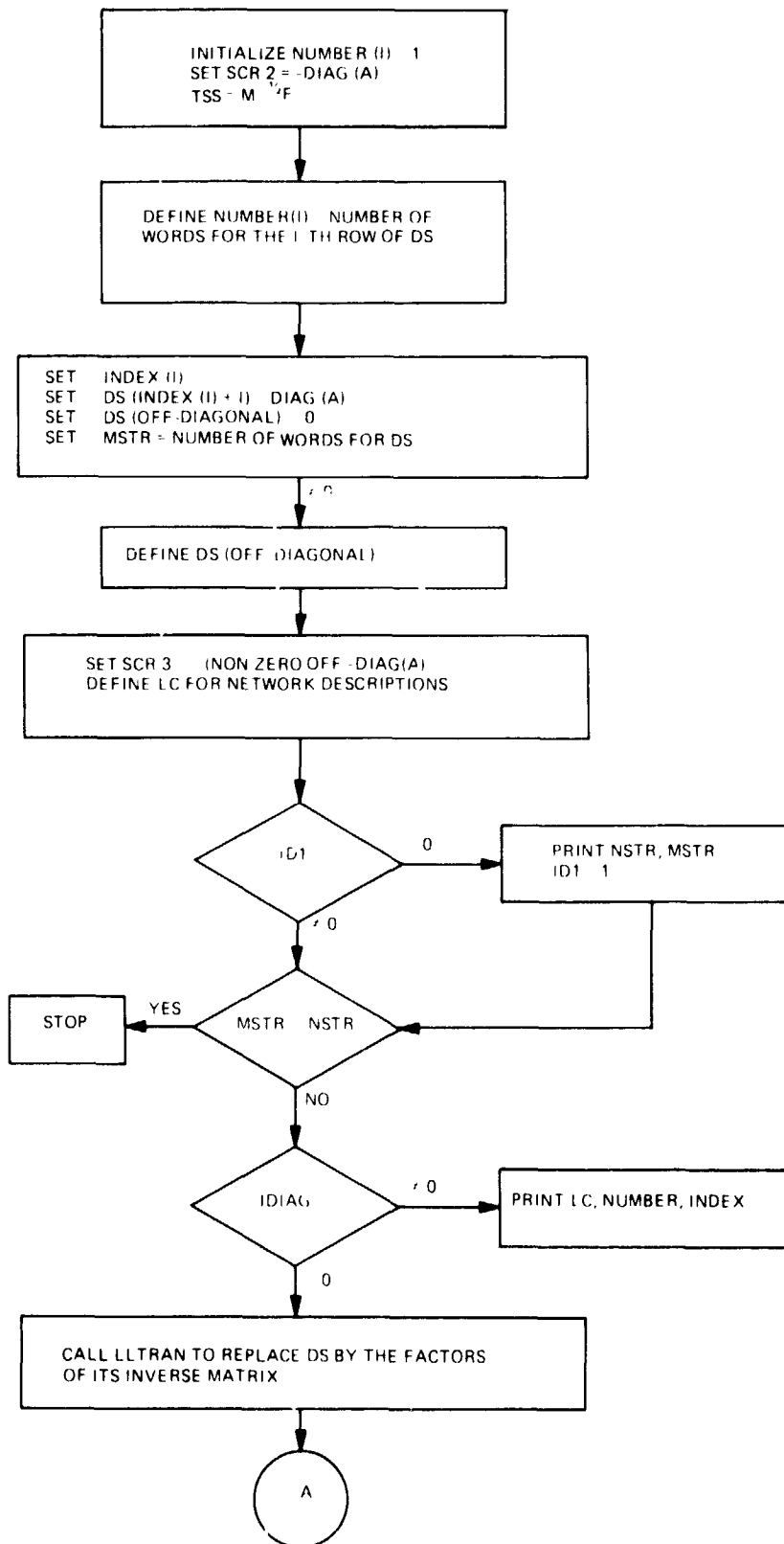


Figure 6-8. Subroutine DSCT Flow Chart (Sheet 1 of 2)

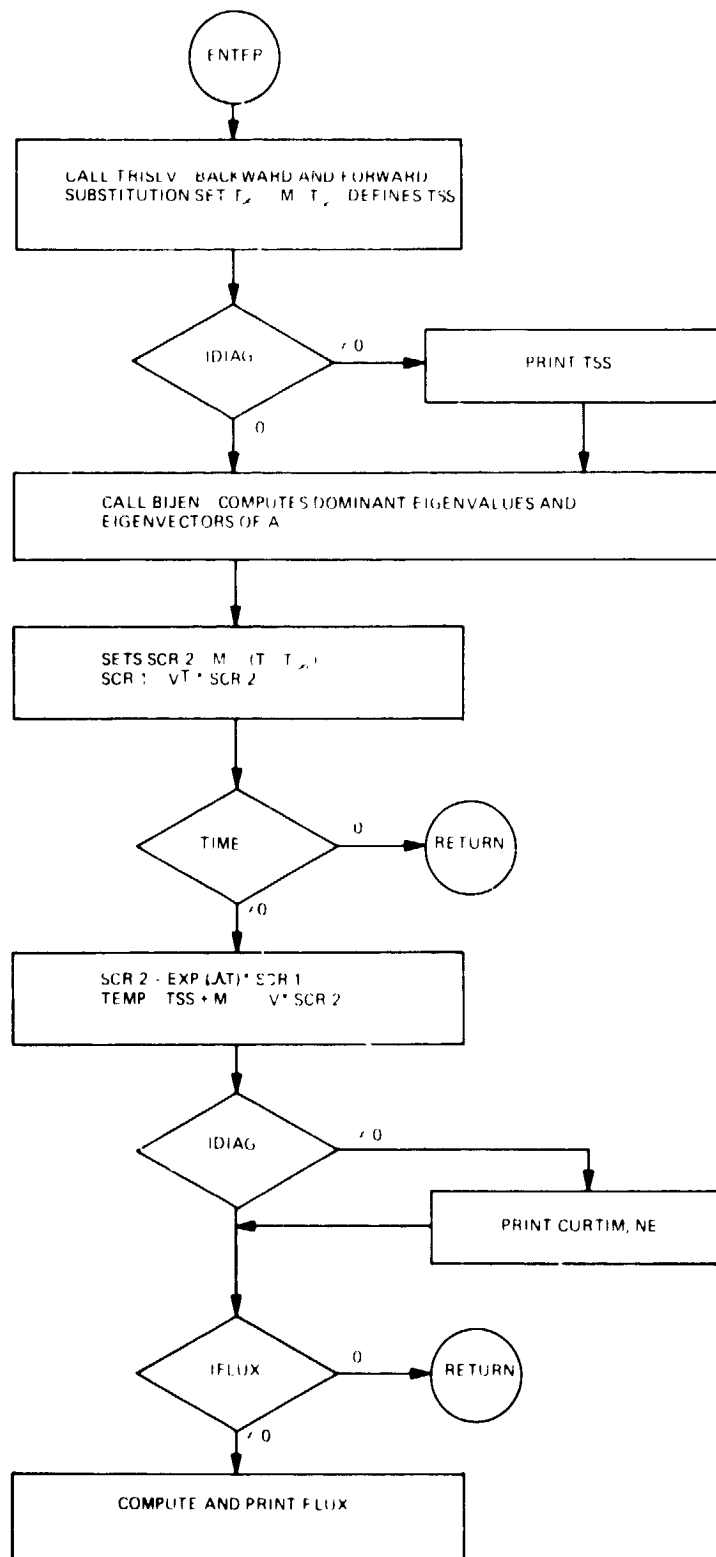


Figure 6-8. Subroutine DSCT Flow Chart (Sheet 2 of 2)

EVECGS computes guesses of the eigenvalues, eigenvectors and associated permutation index that are necessary to start the iteration in the Jennings method to calculate eigenvalues and eigenvectors. The formulae used for these guesses are:

$$i\text{th eigenvalue } R \sim -i$$

$$i\text{th eigenvector } A \approx e^{+y/(h/2)} \sin \left\{ \frac{\pi}{2} + \pi \frac{x}{b} (i - 1) \right\}$$

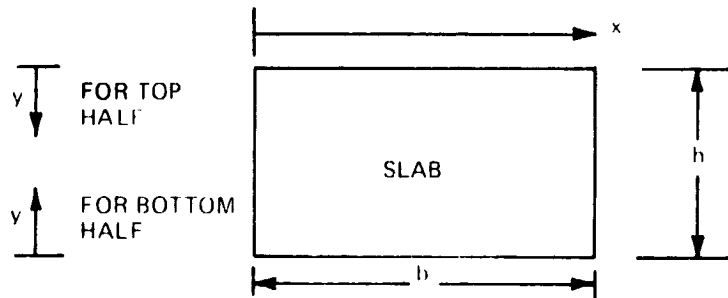


Figure 6-9. Subroutine EVECGS Description  
(From NASA CR-2435)

CHOLESKY DECOMPOSITION OF A POSITIVE DEFINITE SYMMETRIC MATRIX,  
 A USEFUL PRELIMINARY FOR LINEAR SYSTEM SOLUTION VIA SUBROUTINE TRISLV.

THE MATRIX IS STORED IN A ONE DIMENSIONAL ARRAY, A, IN A COMPACT  
 WAY WHICH IS MOTIVATED BY THE PATTERN OF NONZERO ELEMENTS IN THE  
 FACTOR.

THE MATRIX IS GIVEN ROW-WISE STARTING WITH THE FIRST NONZERO  
 ELEMENT AND CONCLUDING WITH THE DIAGONAL ELEMENT INCLUDING INTERIOR  
 ZEROS.

THE ARRAY NUMBER GIVES THE NUMBER OF ELEMENTS STORED FOR EACH  
 ROW.

THE ARRAY KDIAG IS DEFINED BY THE ROUTINE TO BE THE INDEX OF  
 DIAGONAL ELEMENTS OF THE MATRIX.

NSTR IS THE NUMBER OF WORDS IN THE ARRAY FOR STORING THE MATRIX.

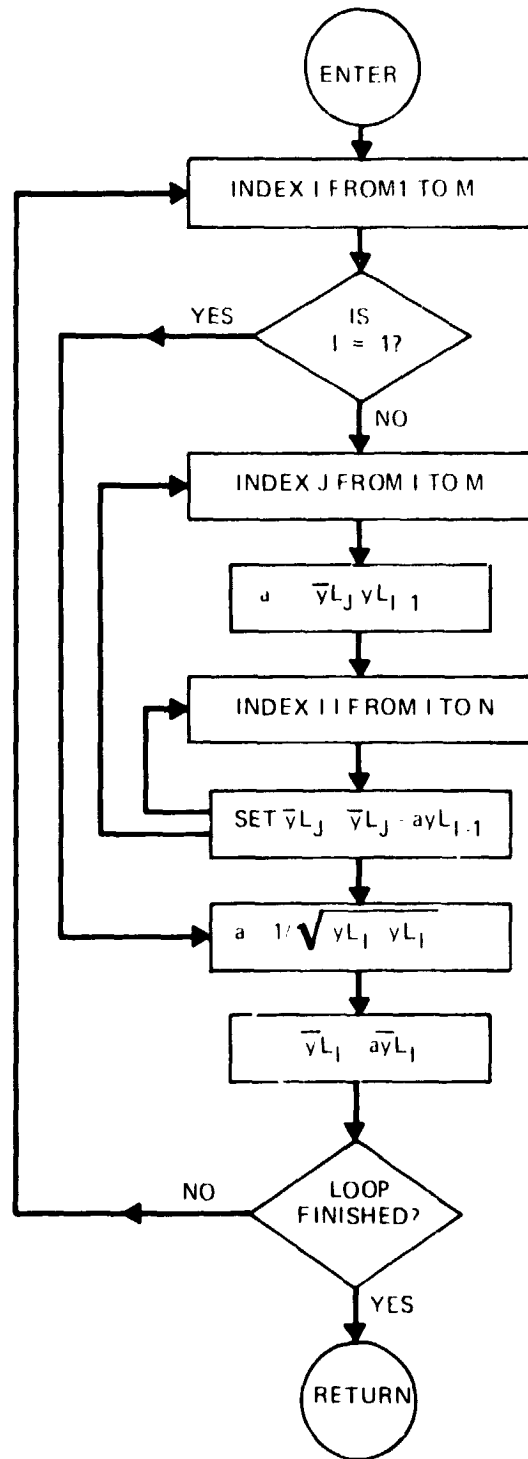
N IS THE ORDER OF THE MATRIX.

NIX IS SET BY THE ROUTINE AS ZERO NORMALLY, AND AS  $H$  IF THE  
 $H$ -TH LEADING PRINCIPLE MINOR FAILS TO BE NUMERICALLY POSITIVE  
 DEFINITE.

THE ARRAY A IS REDEFINED TO REPRESENT THE LOWER DIAGONAL  
 CHOLESKY FACTOR. GENERALLY ALL KDIAG(N) ELEMENTS OF A WILL BE NON-  
 ZERO ON OUTPUT, EVEN IF THERE ARE MANY INTERIOR ZEROS ON INPUT.  
 THE PATTERN OF STORAGE IS ILLUSTRATED BY THE 6X6 CASE BELOW.

MATRIX	A(I,J)	NUMBER(I)
X X 0 0 0 0	1	1
X X X X 0 X	2 3	2
0 X X 0 0 0	* 4 5	2
0 X 0 X X X	* 6 7 8	3
0 0 0 X X 0	* * * 9 A	2
0 X 0 X 0 X	* B C D E F	5

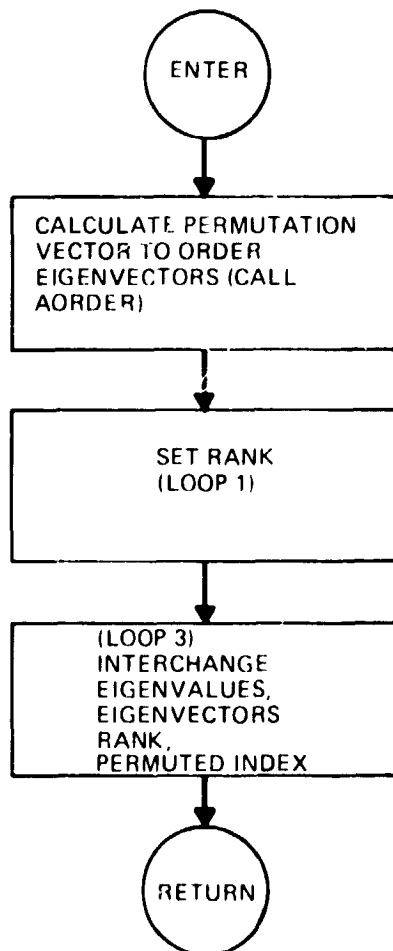
Figure 6-10. Subroutine LLTRAN Description



\*(SOURCE: NASA CR-2435)

Figure 6-11. Subroutine ORNML Flow Chart\*

<u>QUANTITY</u>	<u>SYMBOL</u>	<u>INPUT/OUTPUT</u>	<u>DIMENSION</u>
EIGENVALUES	R	IN + OUT	R(MM)
EIGENVECTORS	V	IN + OUT	V(MID, MM)
RANK VECTOR	K	OUT	K(MM)
PERMUTATION VECTOR	L	OUT	L(MM)
EIGENVECTOR DIMENSION	N	IN	-
NUMBER OF EIGENVECTORS	MM	IN	-
DIMENSION OF ARRAY USED TO STORE EIGENVECTORS	MID	IN	-

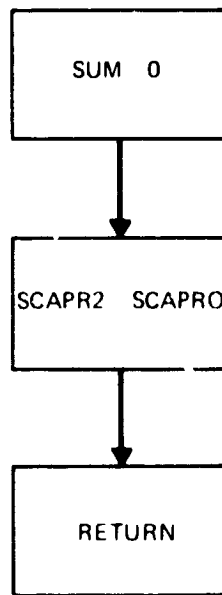


\*(SOURCE: NASA CR-2435)

Figure 6-12. Subroutine RVORDR Flow Chart\*



SCAPR2 CALCULATES THE INNER  
PRODUCT OF TWO VECTORS STORED  
AS EQUALLY SPACED WORDS IN FORTRAN ARRAYS



\*(SOURCE NASA CR 2435)

Figure 6-13. Subroutine SCAPR2 Flow Chart\*

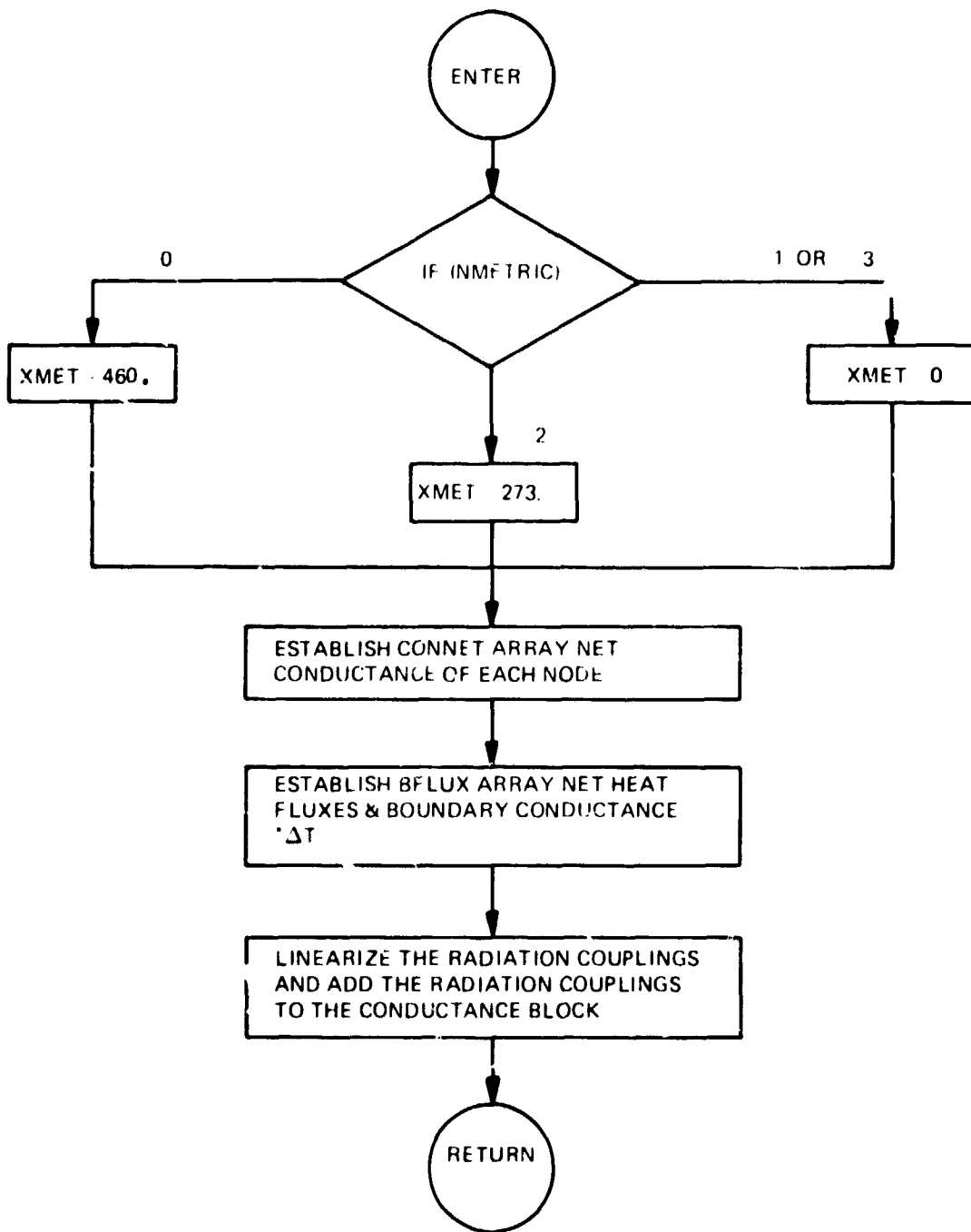


Figure 6-14. Subroutine SETUP Flow Chart

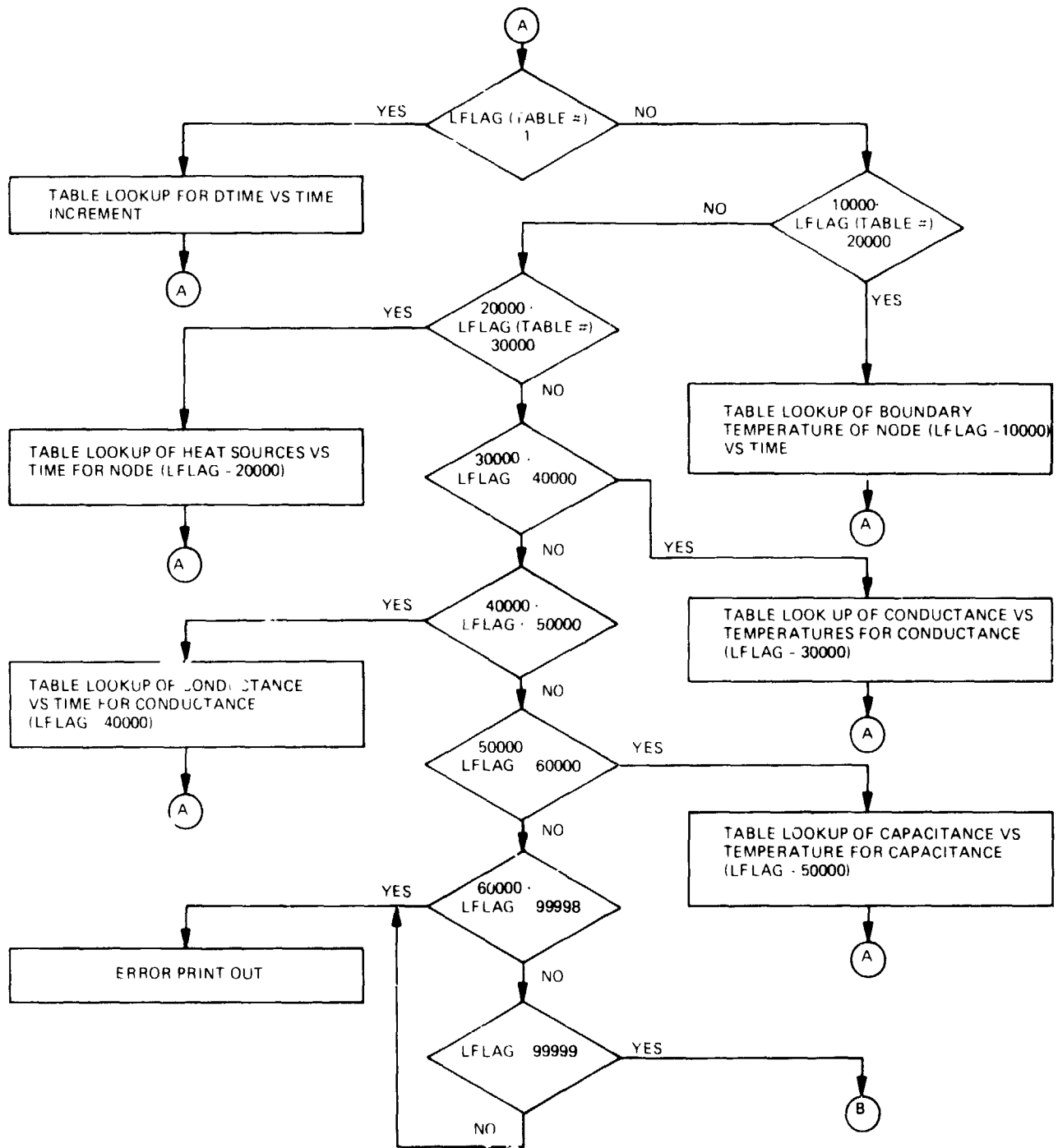


Figure 6-15. Subroutine TABLE Flow Chart (Sheet 1 of 2)

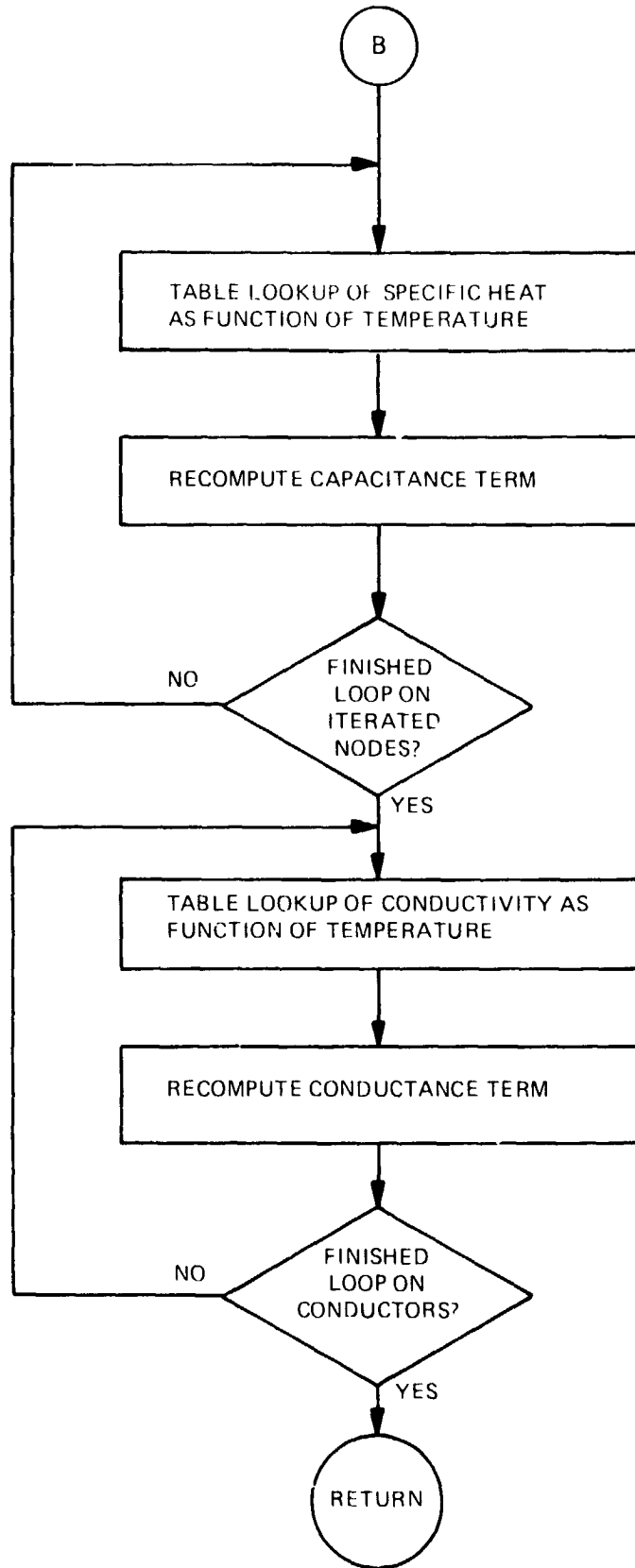


Figure 6-15. Subroutine TABLE Flow Chart (Sheet 2 of 2)

SOLUTION OF A SYSTEM OF N LINEAR EQUATIONS USING THE CHOLESKY FACTOR OFTEN COMPUTED BY SUBROUTINE ULTRAN. IN OTHER WORDS, THE COEFFICIENT MATRIX IS REPRESENTED AS THE PRODUCT OF A LOWER TRIANGULAR MATRIX TIMES ITS TRANSPOSE. THIS LOWER TRIANGULAR MATRIX IS SPECIFIED BY THE FORTRAN ARRAYS, A AND NUMBER. THE MATRIX IS STORED WITHOUT LEADING OR TRAILING ZEROS -- IN EACH ROW, DIAGONALS MUST BE NONZERO. THE PATTERN OF STORAGE IS ILLUSTRATED BY THE 6X6 CASE BELOW.

MATRIX	A(IJ)	NUMBER(I)
X 0 0 0 0 0	1	1
X X 0 0 0 0	2 3	2
0 X X 0 0 0	* 4 5	2
0 X 0 X 0 0	* 6 7 8	3
0 0 0 X X 0	* * * 9 A	2
0 X 0 X 0 X	* B C D E F	5

STORED IN THE ORDER

WHERE A THROUGH F DENOTE 10 THROUGH 15.

THE ROUTINE NEEDS TO BE TOLD THE NUMBER OF ELEMENTS STORED IN EACH ROW GIVEN BY THE ARRAY NUMBER. NSTR IS .GE. SUM NUMBER (I), I = 1, N) THE ROUTINE SOLVES THE M RIGHT HAND - SIDES AT ONCE, IT REPLACES THE RIGHT HAND SIDES BY THE CORRESPONDING SOLUTIONS. THE RIGHT HAND SIDES ARE STORED AS COLUMNS OF THE 2 DIMENSIONAL ARRAY, Y, DIMENSION TO MID BY M, WHERE MID, GE, N, THE ROUTINE ALSO CAN RECURSE N/LOG TIMES WHICH IS USEFUL IN SOME EIGENVECTOR CALCULATIONS.

Figure 6-16. Subroutine TRISLV Description

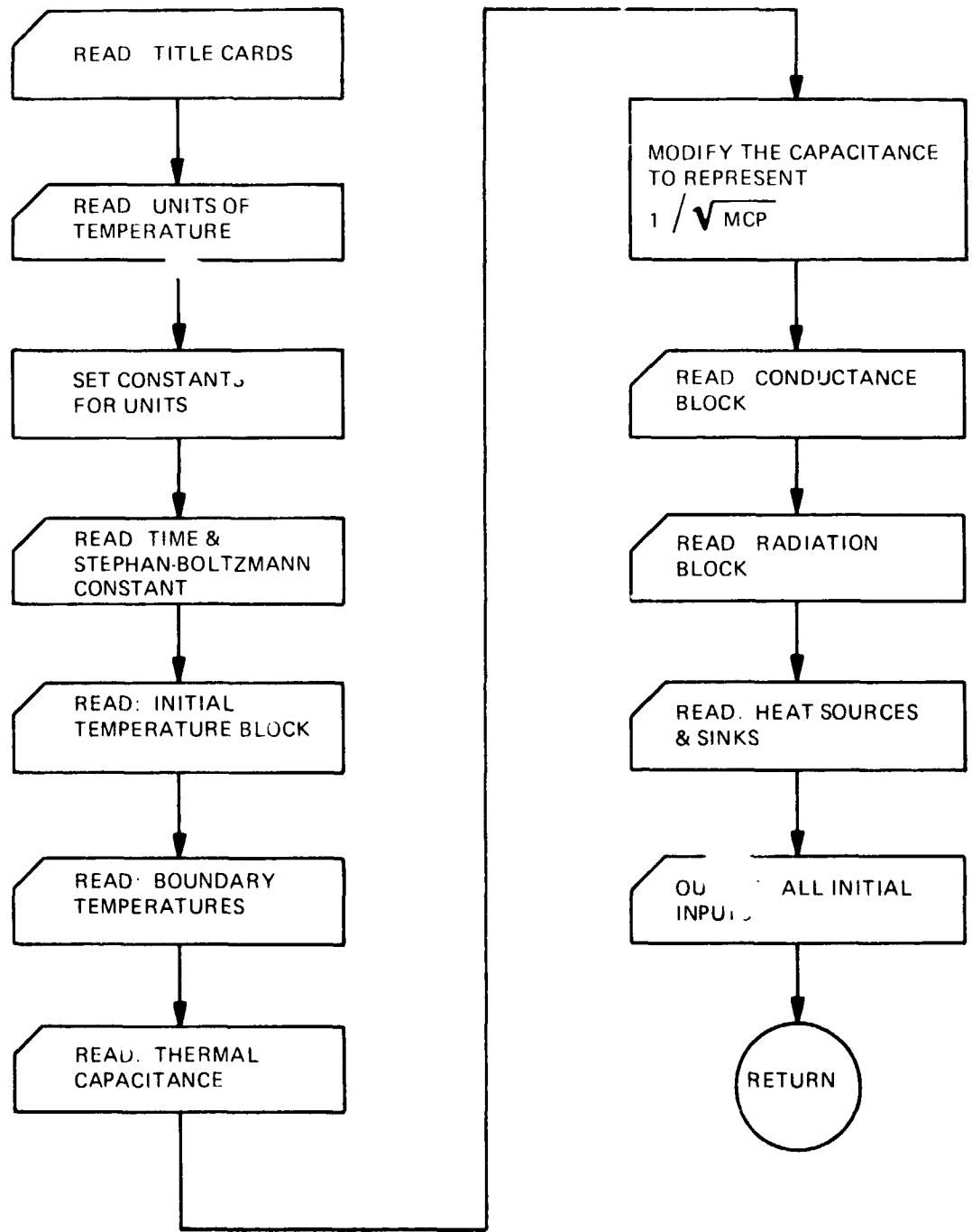


Figure 6-17. Subroutine XREDE Flow Chart

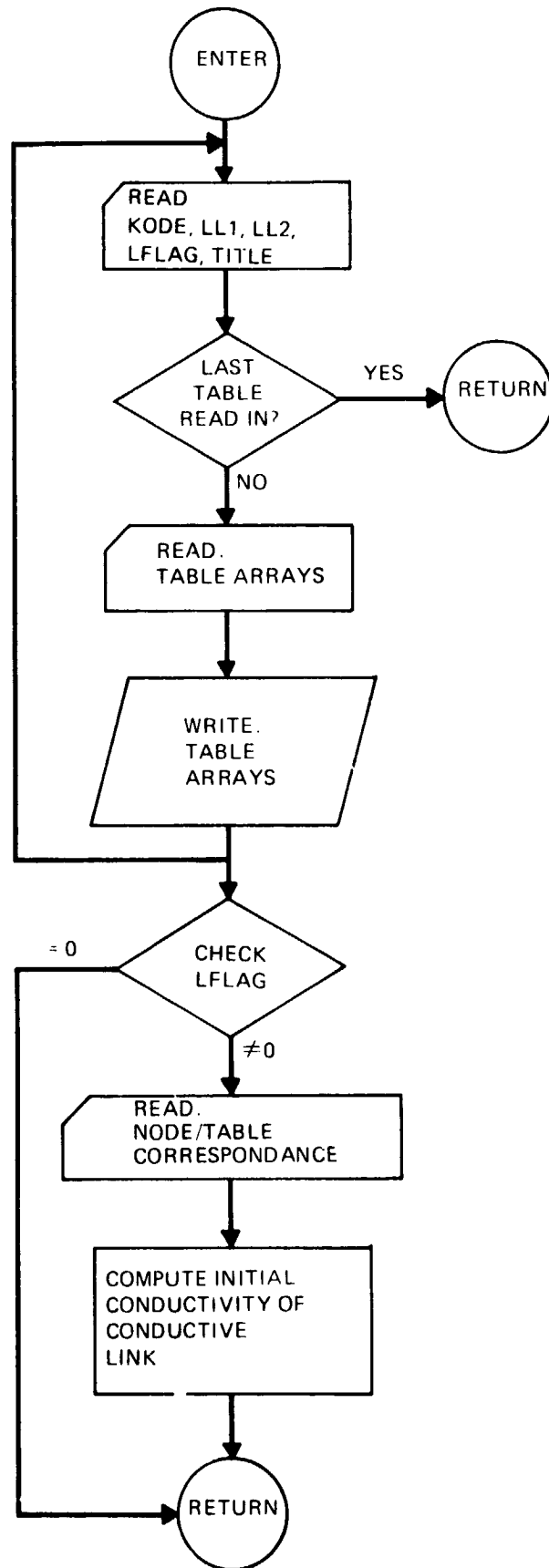


Figure 6-18. Subroutine XTABS Flow Chart

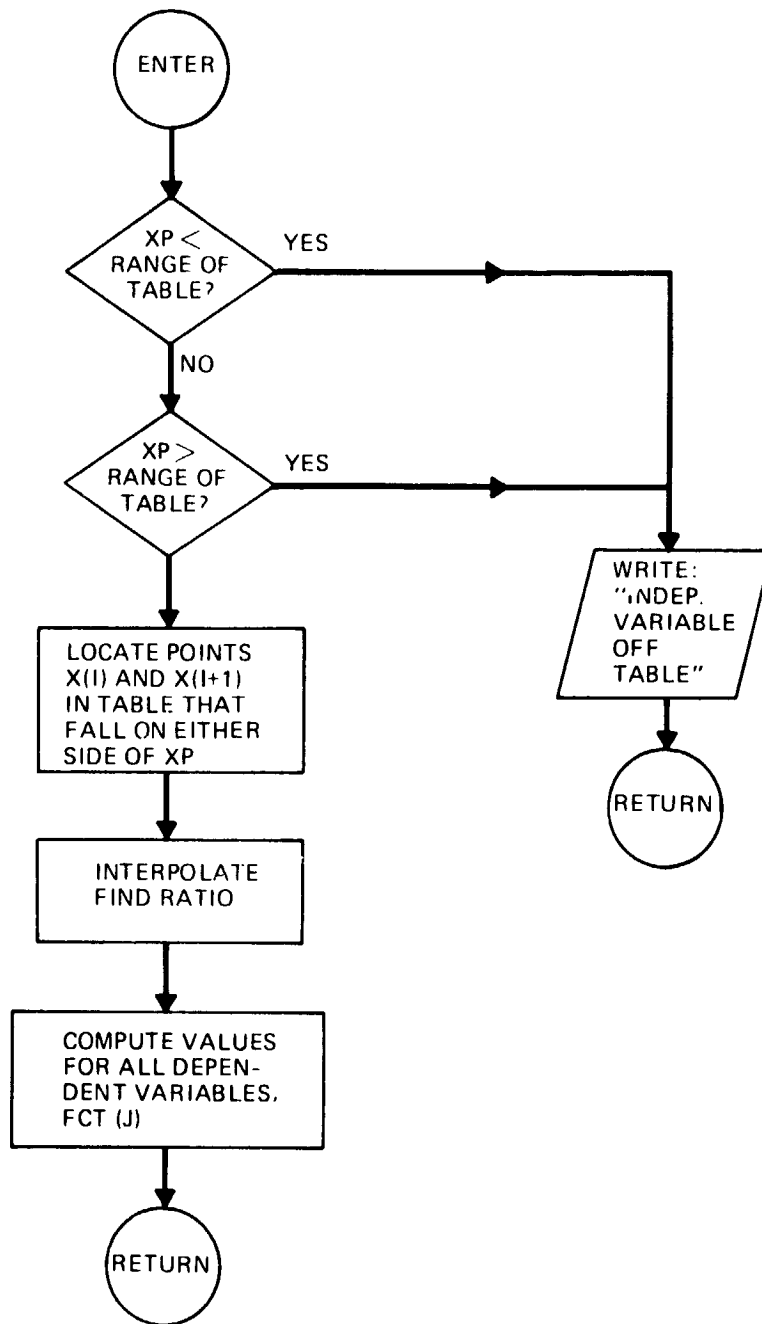


Figure 6-19. Subroutine XINTP Flow Chart



Section 7

REFERENCES

1. Rathjen, K. "CAVE, A Computer Code for Two-Dimensional Transient Heating Analysis of Conceptual Thermal Protection Systems for Hypersonic Vehicles" NASA CR-2897, 1977
2. Jennings, A., "A Direct Iteration Method of Obtaining Latent Roots and Vectors of a Symmetric Matrix", Proc. Cambridge Phil. Soc., 63, 1967, pp. 755-765