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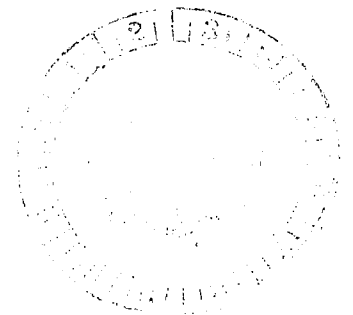
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Pilot Evaluation of Sailplane Handling Qualities

A. G. Bennett, Jr.

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Pilot Evaluation of Sailplane Handling Qualities

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1. INTRODUCTION

The performance of competition sailplanes as measured by maximum lift to drag ratio (L/D_{\max}) or average cross-country speed has shown a steady improvement with time as shown in Figure 1 (Reference 1). This performance improvement has been due to the continual evolution of airfoils and of fiberglass and metal structures to achieve low drag and high aspect ratio wings. The quest for high performance has had a profound effect upon the handling qualities of sailplanes. The increased L/D_{\max} has increased the range of flight speeds. To minimize the trim drag, the static stability margin has been decreased which has increased control sensitivity and decreased pitch control force gradients. The very slender wing and fuselage structures have also introduced aeroelastic effects upon the sailplane control response characteristics.

There has been some concern voiced about the trends in high performance sailplane handling qualities. Poor handling qualities generally result in increased pilot workload which may compromise flight safety. Thus there is a strong interest in determining whether the current trends in sailplane performance improvement can continue while at the same time a high level of flight safety can be maintained.

The primary objective of this study was to make a qualitative evaluation of all aspects of high performance sailplane handling qualities and to define areas which require further study. To accomplish this objective at a modest cost, a round-robin flight evaluation of several sailplanes by several test pilots was conducted. The Cooper-Harper Rating Scale and pilots' comments

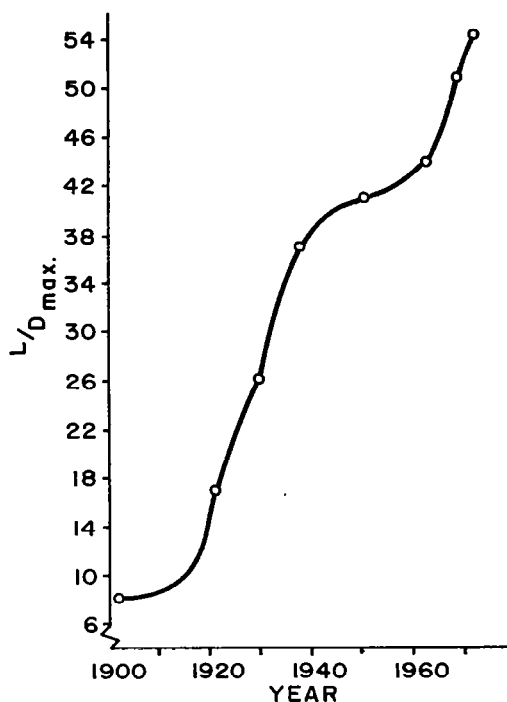


Figure 1. L/D_{\max} Versus Time

were to be used to evaluate the sailplane handling qualities. The specific objectives of this study were:

1. Using the Cooper-Harper Rating Scale and pilot comments investigate the handling qualities of high performance sailplanes.
2. Obtain pilot opinion of handling quality characteristics to assist the formulation of airworthiness standards.
3. Develop a data base of pilot opinion which would be of value in the design of future sailplanes.
4. Delineate areas which warrant more quantitative study.

The development of high performance sailplanes has evolved in discrete stages with several sailplanes vieing for the market at each stage. Thus it was determined that if the sailplanes developed since the early 60's were arranged into groups, then one sailplane from each group should be chosen for the evaluation session. The sailplane grouping logic is given as follows:

- Group 1: Borderline between utility and racing class, L/D_{max} mid 30's.
- Group 2: First sailplanes to use fiberglass structures. Represents technology in the late 60's. Most have camber changing flaps and/or drag chute.
- Group 3: Sailplanes developed in early 70's. Most numerous class in USA today, hence important.
- Group 4: Sailplanes developed during mid 70's. Just becoming available in substantial numbers. Most have landing flaps.
- Group 5: Very high performance, $L/D_{max} \approx 50$. Effect of large span on handling can be established by this class.
- Group 6: High performance two place. Used in transition to high performance single place sailplanes.

Test pilots for the flight session were chosen from NASA, FAA and the soaring community to ensure that a wide range of pilot backgrounds would be brought to bear upon the sailplane handling quality evaluations.

The text which follows describes the evaluation session and presents the analysis of the pilot opinion data. Chapter 2 describes the sailplanes, pilots and the flight session. Chapter 3 presents the analysis of the pilot

ratings and comments. The evaluation questionnaire, pilot ratings, and pilot comments are presented in the Appendices.

The sailplane owners are due a special thanks for lending their sailplanes for the flight test session. They were Mr. John Thompson, McCrory, Arkansas; Mr. Lanier Franz, Roanoke, Virginia; Mr. Dave Lawrence, Starkville, Mississippi; Mr. Marion Griffith, Dallas, Texas; Schweizer Aircraft Corporation, Elmira, New York; and the Air Force Flight Dynamics Laboratory, Dayton, Ohio. Many members of the Soaring Society of America gave this project unstinting support. Mr. Howard Ebersole, Associate Director of the RASPET Flight Research Laboratory, provided excellent organizational support in the sailplane preparation and in the flight session. The departmental staff support for this project was as usual, superb.

2. SAILPLANE FLIGHT TEST SESSION DESCRIPTION

2.1 Introduction

The flight test session had to satisfy several requirements and constraints. The round-robin evaluation format required that six sailplanes and seven test pilots must be on site simultaneously. To accommodate the pilots busy flight schedules, the flight session was organized to conduct the flight activities necessary to acquire the required data in a maximum of 7 days. The session was scheduled for the early May period to avoid conflicts with the soaring season, and yet to have the possibility of encountering soaring conditions. In all respects, the flight session was a complete success. There were no problems acquiring the sailplanes, the weather during the flight session was perfect, the test pilots were very enthusiastic, and cooperative, and all operations were conducted safely.

2.2 Evaluation Sailplanes

Within the previously mentioned groups of sailplanes, a ranking was made to determine which one had characteristics of most interest to this investigation. At the same time, only sailplanes with standard approved type certificates were considered. The soaring community was most cooperative in supporting the acquisition of the evaluation sailplanes.

Sailplane 1. This sailplane was chosen since it represents the transition to higher performance ships. It has a fixed horizontal stabilizer with a fairly large chord elevator. The fixed gear is ahead of the center of gravity. The sailplane is equipped with schemmp-Hirth type divebrakes.

Sailplane 2. This sailplane is equipped with camber changing flaps which are inter-connected with the ailerons. The landing gear is retractable and is ahead of the center of gravity. The sailplane has schemmp-Hirth type divebrakes, and a very short, straight control stick. The sailplane is placarded against intentional spins.

Sailplane 3. This sailplane was selected from Group 3. It has an all-moveable horizontal tail and a control stick which curves slightly toward the pilot. The ship is equipped with retractable landing gear ahead of the center

Table 1
Sailplane Dimensional Parameters

Parameters	Units	Sailplane					
		1	2	3	4	5	6
Wing Span	m	15.0	15.0	15.0	15.0	20.3	17.4
Wing Area	m ²	12.40	9.48	10.00	9.64	14.40	16.72
Aspect Ratio		18.1	23.6	22.5	23.3	28.6	18.0
MAC	m	0.885	0.687	0.704	0.681	0.756	1.069
Max Weight	kg	299	300	300/390	299/422	445/580	649
Wing Loading	n/m ²	234.6	311.2	325.6/383	306.4/430.9	301.6/392.6	378.3
Root Chord	m	1.232	0.940	0.955	0.914	0.980	1.483
Tip Chord	m	0.394	0.343	0.368	0.373	0.350	0.483
Fuselage Length	m	6.680	6.198	6.350	5.842	7.290	8.153
Fuselage Width	m	0.584	0.610	0.635	0.584	0.610	0.813
Hor. Tail Area	m ²	1.65	1.04	0.99	1.00	0.99	2.03
Hor. Tail Span	m	2.819	2.395	2.408	2.032	2.408	3.200
Elevator c_f/c		0.42	0.28	1.00	0.56	1.00	1.00
Vert. Tail Area	m ²	1.13	1.06	0.84	0.78	---	1.43
L/D max (Handbook)		32	39	35.2	37	49	34
Fwd C.G.	% \bar{c}	20	25	26	27.8	29	25
Aft C.G.	% \bar{c}	40	52	47	38.2	45	38
I _{yy} (Approx.)	kg m ²	186	186	204	186	407	1178

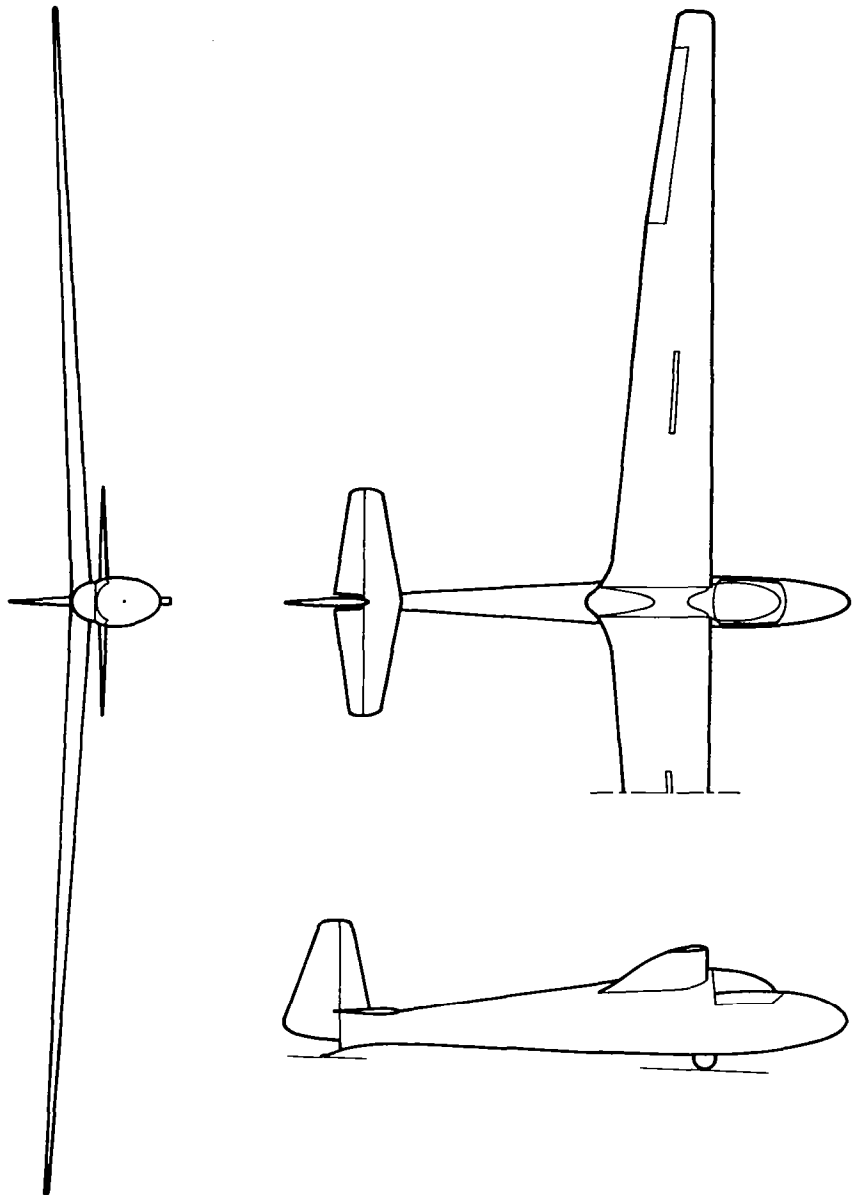


Figure 2. Three View of Sailplane 1.

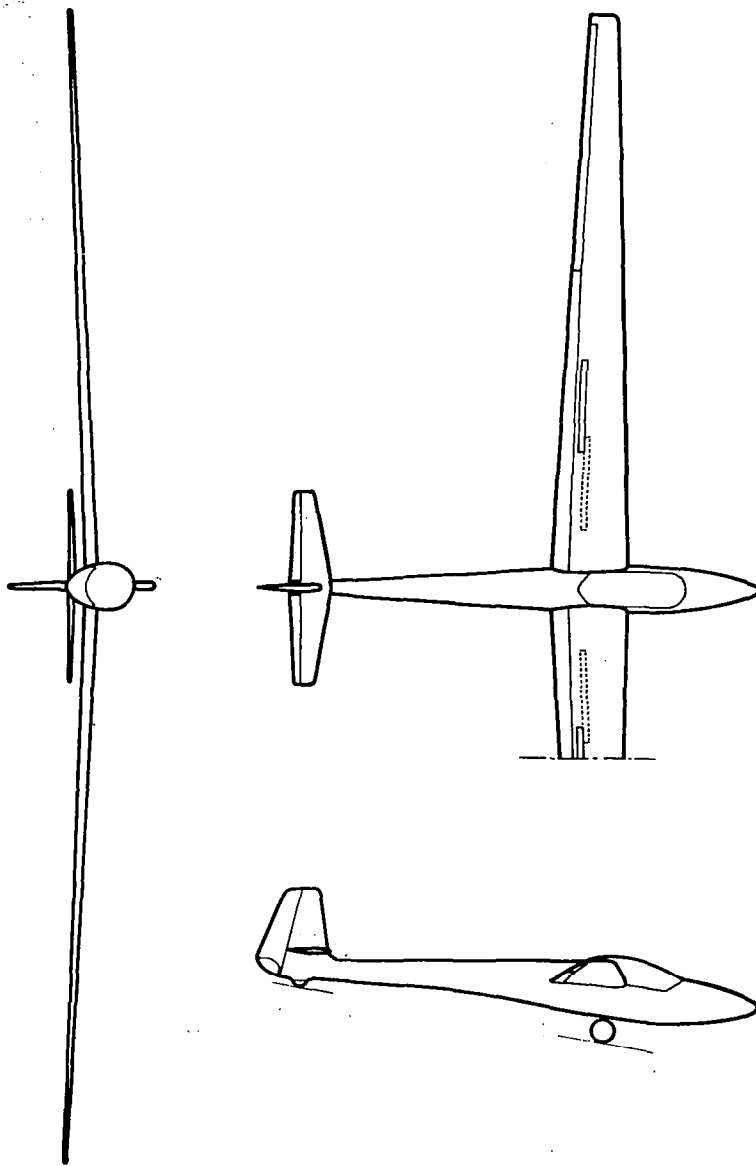


Figure 3. Three View of Sailplane 2.

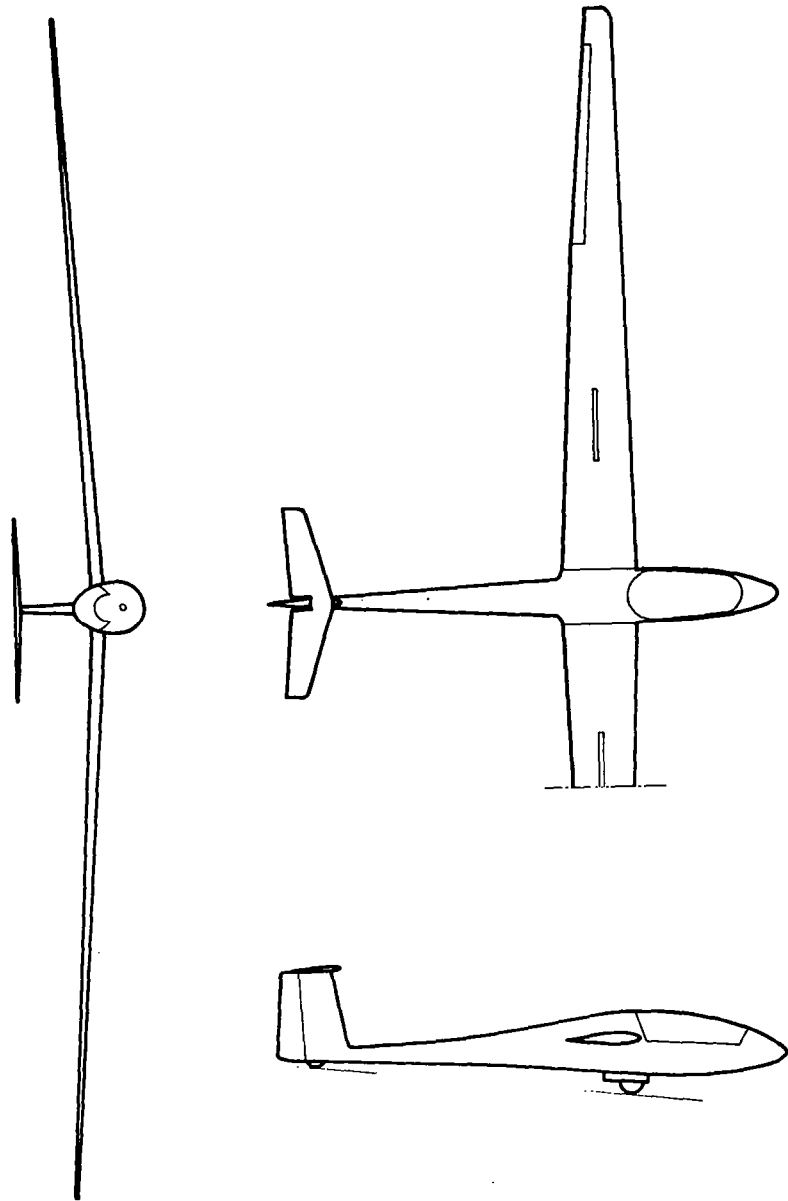


Figure 4. Three View of Sailplane 3.

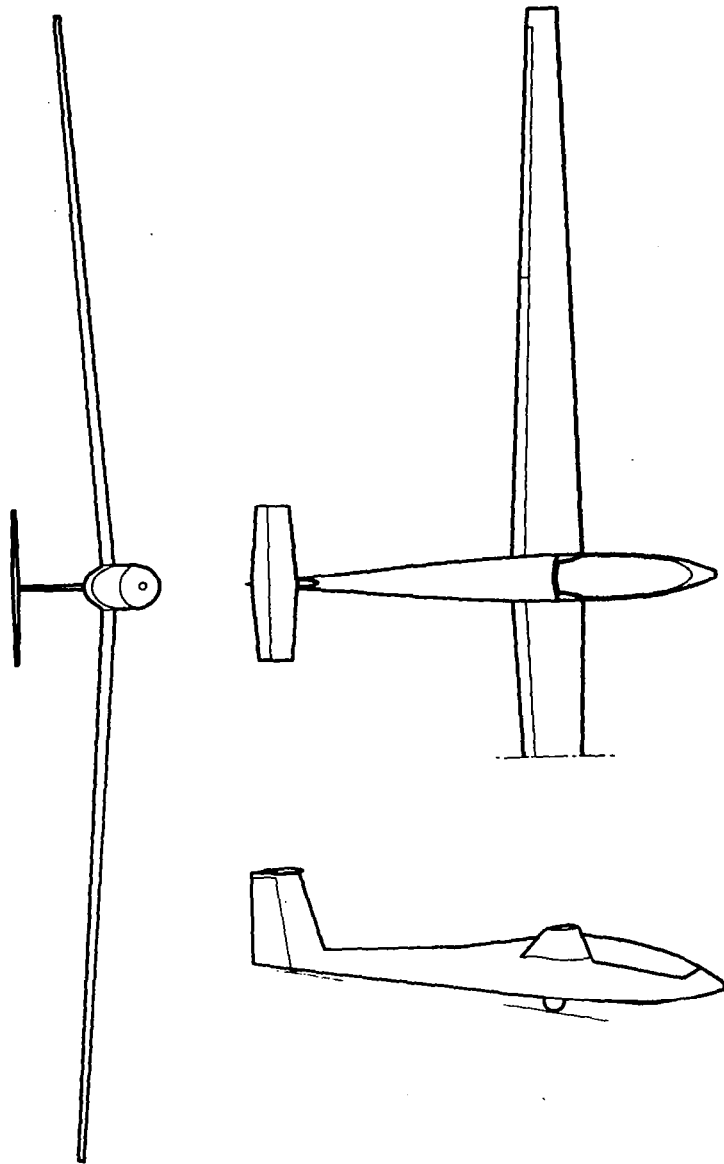


Figure 5. Three View of Sailplane 4.

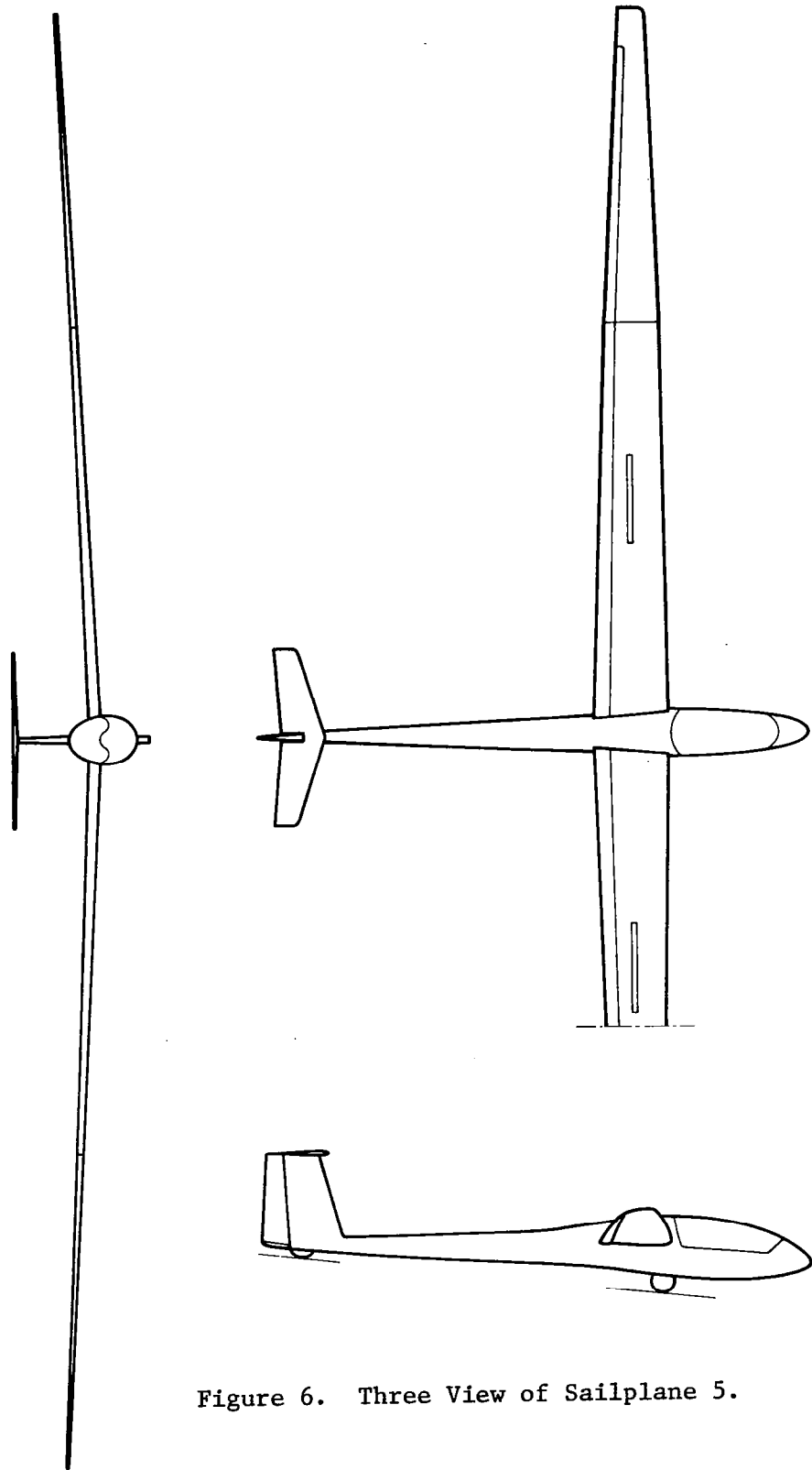


Figure 6. Three View of Sailplane 5.

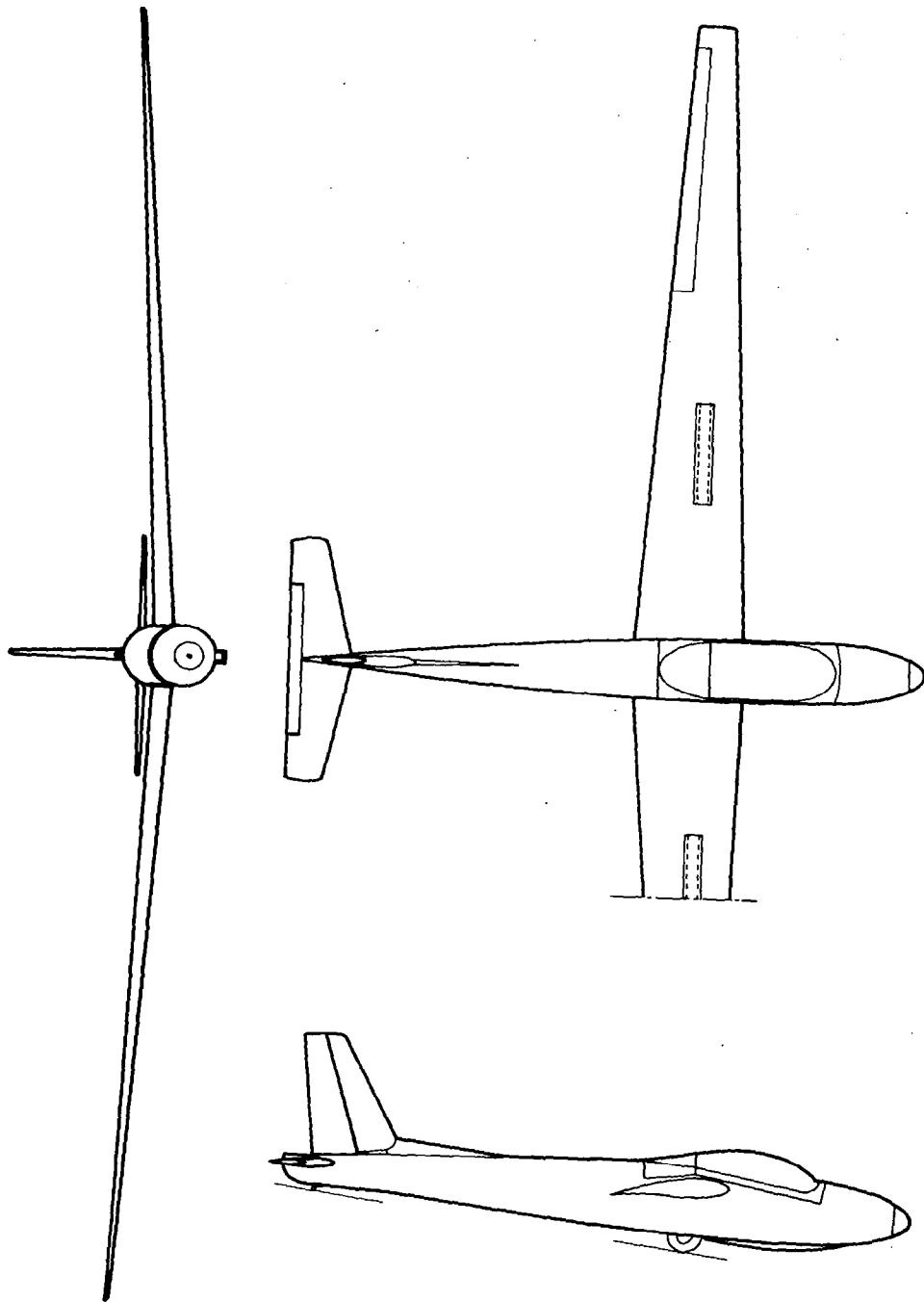


Figure 7. Three View of Sailplane 6.

of gravity, and has upper surface divebrakes. Intentional spins are prohibited with this sailplane.

Sailplane 4. This sailplane has a conventional fixed stabilizer and moveable elevator. The retractable landing gear is located slightly behind the center of gravity. The camber changing flaps, interconnected with the ailerons, can be positioned up to 90 degrees for landing.

Sailplane 5. This ship had the largest wing span among the evaluation sailplanes. The horizontal tail, control stick and landing gear arrangement was identical to that of sailplane 3. This ship is equipped with camber changing flaps interconnected with the ailerons, and with upper surface divebrakes.

Sailplane 6. This sailplane represented a typical, fairly high performance two seater. It features a fixed landing gear, an all moveable horizontal tail equipped with anti-servo tab and large counterbalanced divebrakes.

A three-view drawing of each sailplane is shown in Figures 2 through 7, and the principal geometric characteristics are presented in Table 1.

In general, each sailplane was in excellent mechanical condition. Since in some of the ships intentional spins were prohibited and/or some of the ships were not equipped with water ballast or drag chutes, the effect of these three-factors on the overall sailplane handling qualities was not evaluated.

2.3 Evaluation Pilots

Each evaluation pilot is affiliated with one of the following organizations: Soaring Society of America, Inc., the Federal Aviation Administration and the National Aeronautics and Space Administration. Table 2 indicates the number of flight hours as pilot in command of each pilot. Two of the pilots were professional experimental test pilots and had considerable experience with the Cooper-Harper rating scale. Four of the seven pilots had considerable sailplane cross-country and competition flying experience. Preceding the flight test sessions, these four pilots were asked to describe to the rest of the group in detail what they conceive to be the flight role or mission of

a high-performance sailplane. Thus, all of the pilots had a clear understanding of the broad mission for which this class of aircraft is designed.

Table 2
Evaluation Pilot Flight Experience

Aircraft Type	Pilot						
	<u>1</u>	<u>2</u>	<u>3</u>	<u>4</u>	<u>5</u>	<u>6</u>	<u>7</u>
Sailplane	6500	1500	700	30	20	1500	20
SEL	500	500	200	600	200	1000	2450
MEL		1800		2600	3800	5000	1250
Jet Fighter		2500			1000		1500
Jet Transport		450		7000	3500	4000	550
Helicopter		50					250

2.4 Flight Session Preparation

To achieve the objectives of the evaluation session, several tasks were conducted prior to the session. An overriding consideration was the round-robin format for the session which required six sailplanes and seven pilots to be brought together for a one week period. Since the pilots were available for a limited time, it was most important that the sailplanes be properly prepared in advance of the session. A constraint upon the session date was that it must occur early in the year so that the borrowed sailplanes would not be away from the owners during contest activities.

The session data was scheduled for May 1 thru May 6, 1976, so that University students could assist in the flight operations. With the grant awarded February 16, 1976, this session date would allow time for sailplane acquisition, pilot selection, sailplane checkout, instrumentation development and flight session planning. The schedule was tight but all objectives were accomplished.

The acquisition of the sailplanes was found to be much easier than anticipated. A few phone calls to members of the soaring community quickly revealed that the sailplanes of interest were available in the southeastern region of the U.S. The owners were most interested in assisting in this investigation.

Prior to the flight session, all sailplanes except 4 and 5 were acquired with sufficient time for a thorough inspection, airspeed calibration check, and weight and balance check. Sailplanes 4 and 5 were delivered by evaluation pilots and had prior checkout.

Sailplane 6 was acquired early and was used as a testbed for formulating the evaluation tasks and for the development of a simple sailplane data acquisition system. A battery powered signal conditioning unit was developed to give a digital display of either stick position or stick force to the pilot. It was found that small low friction potentiometers could be quickly attached to the sailplane control linkages, but the press of other flight activities and difficulties with pilot data recording limited the utility of quantitative data recording during the flight session. The stick forces were too low for the stick force balance borrowed from Dryden Flight Research Center and also the balance was too bulky for high performance sailplane control sticks.

2.5 Flight Session

The flight session was conducted May 1 through May 6, 1976. The weather was ideal throughout the session with a wide range of convection conditions present. The pilots were allowed to fly each of the ships as required to complete the evaluation questionnaires. Cassette recorders were used to record inflight comments to be used later during the evaluations. A maneuver list was supplied to further support the evaluation.

A total of ninety-eight flights were made for a total of 80 flying hours. The sailplane evaluation forms were completed during the session to maximize evaluation effectiveness. The pilots were most cooperative and willing to participate. The session was very flight intensive, yet all objectives were accomplished without any mechanical or safety problems.

2.6 Pilot Opinion Sampling Instruments and Data Presentation

The primary objectives of this study were to (1) obtain pilot opinion of the handling qualities of current high performance sailplanes, (2) to aid in the formulation of certification criteria, (3) to provide some guidance in future designs, and (4) to delineate areas which require further study. The most cost effective method to accomplish this task was to stage a round-robin

flight session in which seven test pilots evaluated six sailplanes representing distinct groups. The detailed sailplane handling quality pilot opinion data was obtained with a questionnaire which used the Cooper-Harper Rating Scale and pilot comments.

Questionnaire I (Appendix A) was designed to record the pilot's rating and comments of the sailplanes' handling qualities, design and cockpit layout. Each test pilot completed a questionnaire for each sailplane that he flew. The questionnaire was configured to evaluate the pilots' opinion of the sailplane handling qualities over the entire operating envelope from takeoff to landing. Specifically, each flight consisted of a tow to an altitude of 2700 or 3300 meters (AGL) depending on the pilot's preference. Evaluation tasks in smooth air were carried out before the flight reached lower altitudes (1000-1200 meters AGL) where convective conditions were usually encountered. On the average, the duration of each flight was 45 minutes, although some thermalling flight evaluations lasted as long as two hours. Evaluations were made in both smooth air and in thermalling flight to determine if there were any significant pilot opinion differences between the smooth air test conditions and the usual operational environment, that is under convective conditions. A set of maneuvers listed in Table 3 was flown by each pilot to provide a basis for the evaluations. The pilots made comments on cassette recorders during each flight and these comments were transcribed by the pilots to the questionnaires. The questionnaire included evaluations of the design and cockpit layout.

The Cooper-Harper Rating Scale (Reference 2), widely used in the evaluation of handling qualities of powered aircraft, was adopted for this questionnaire. The attractive feature of the Cooper-Harper Rating Scale, Figure 8, is the decision tree structure which guides the pilot to a number for his rating value. For this initial study, the interpretation of the rating scale was broadened to be used in the evaluation of such sailplane characteristics as ease of assembly, inspection, and cockpit layout. The key to this interpretation was the assumption that the pilots would compensate for deficiencies in the design as they would for deficiencies in flight stability and control. It should also be noted that only two of the seven pilots had extensive previous experience with the Cooper-Harper rating scale.

Table 3
Evaluation Flight Tasks

A. Smooth Air Maneuver List

1. Evaluate take-off roll.
2. Evaluate tow characteristics; box tow plane.
3. Release, slow flight, stall entry, general characteristics.
4. Attain and maintain constant IAS:50-70-90 kts. Evaluate trim capability over speed range. Note friction, noise, and vibration level.
5. Evaluate return to trim at 60 and 90 kts IAS.
6. Evaluate stick free stability. Trim at 60 and 90 kts. Introduce 5 kts airspeed perturbation and release stick. Note rate of convergence or divergence, time period of oscillation.
7. Evaluate stick position and force gradients over speed range. Trim at 75 kts, decelerate slowly to near stall then accelerate to 100 kts.
8. Evaluate pitch altitude response to small stick pulses over speed range especially at high speed (may be combined with Item 7).
9. Evaluate stick forces during pull up from high speeds.
10. Time roll rate during turn reversal (from 45° to 45° bank) at min. sink speed and at 65 kts. Evaluate ease of maintaining constant airspeed and coordination (zero sideslip).
11. Evaluate steady sideslip. Note force levels during rudder over-balance.
12. Evaluate constant g turn, 45° bank, 60 kts, L and R.
13. Evaluate constant g turn, 60° bank, 70 kts, L and R.
14. Evaluate flight path control system, pattern, flare characteristics, ease of touchdown control, landing roll.

B. Convective Flight Maneuver List

1. Evaluate takeoff, possibly crosswind effects, and tow characteristics in turbulence.
2. Evaluate stall/spin (incipient spin only) characteristics. Note onset of pre-stall buffet.
3. Thermalling characteristics
 - a. Low speed turns
 - b. Stall-spin susceptibility, recovery
 - c. Control characteristics near other aircraft
4. Interthermal flight evaluation. Fly at max L/D speed plus 10 kts and at rough air airspeed or 100 kts IAS (whichever is lower).
5. Evaluate handling during secondary task.
6. Evaluate glide path control, touchdown and rollout characteristics in turbulence.

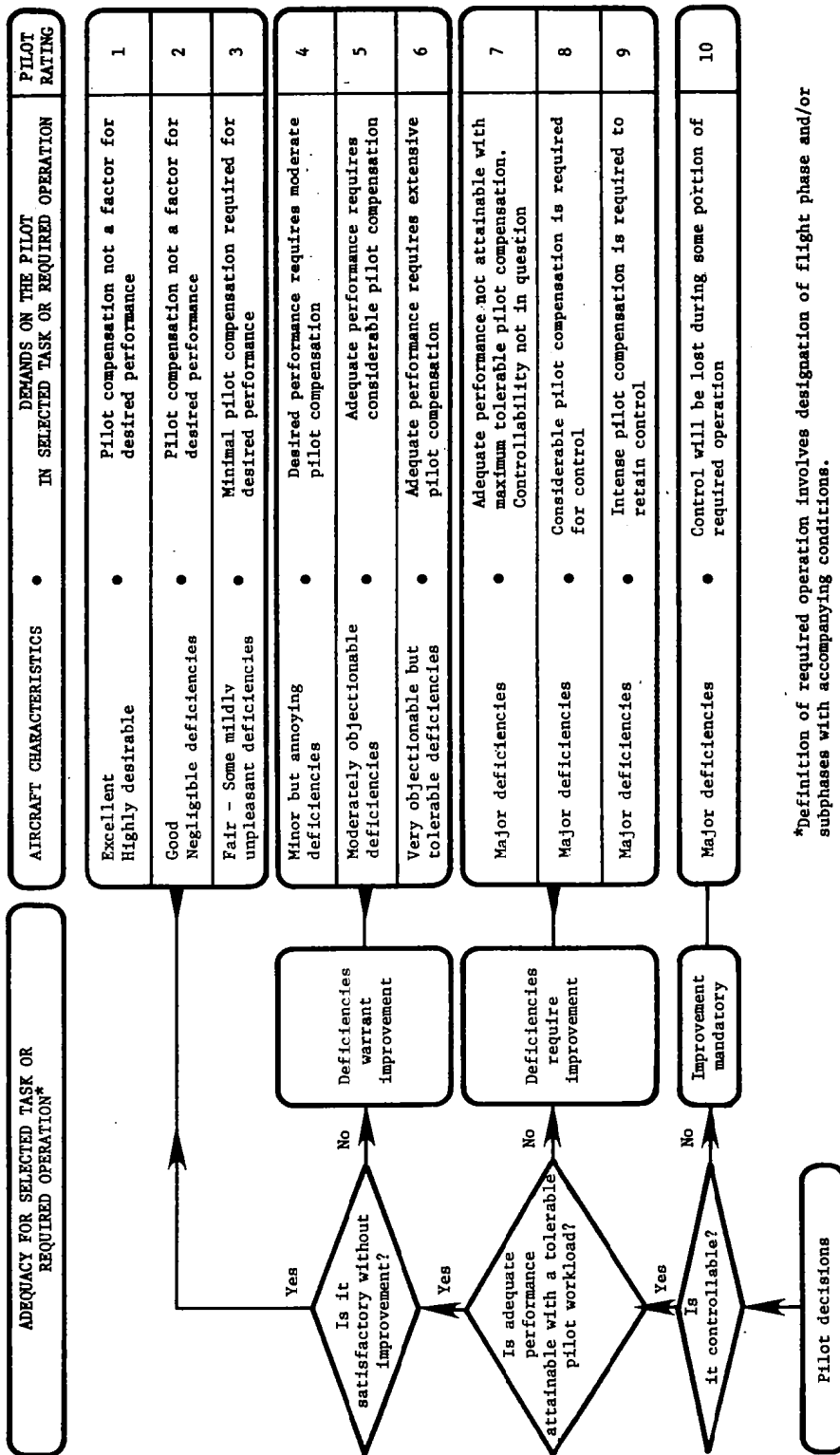


Figure 8. Cooper-Harper Rating Scale

Consequently, the other pilots had a tendency to use the Cooper-Harper Scale as a linear interval scale.

After the flight session was completed, the Cooper-Harper ratings and pilots' comments for each task of Questionnaire I were transcribed into a data file on the university mainframe computer to facilitate the analysis and presentation of the data. The Cooper-Harper Rating Scale, is not a linear scale, thus statistical techniques do not strictly apply. However, averages and standard deviations were computed to gain some measure of the consensus of pilot opinions. An average and standard deviation of all sub tasks for each pilot were computed to allow correlation of the average of sub tasks ratings with the major task rating. The pilots' responses to Questionnaire I are given in Appendix B. The format adopted was to group the responses of all pilots for all sailplanes covering a major area of interest such as longitudinal handling, etc. Extreme caution should be exercised in drawing conclusions from the numerically averaged ratings. As can be seen from the individual pilot ratings, different pilots used different standards of acceptance.

3. RESULTS AND DISCUSSION

3.1 Pilot Rating Summaries

The Cooper-Harper Rating Scale is a valuable tool in the evaluation of aircraft handling qualities. To provide a measure of the variability of the pilot's assignment of ratings, averages and standard deviations for each task were computed for each sailplane. Again, it must be emphasized that the Cooper-Harper Rating Scale is non-linear and thus statistical methods do not strictly apply. Table 4 presents a summary of the average and standard deviation of all pilot ratings of a task for each sailplane. These average readings should not be directly compared with the levels of acceptability shown on the Cooper-Harper scale, but are rather a gross indication. Average Cooper-Harper ratings greater than 3.5 (with no specific meaning attached) have been underlined to delineate areas where problems were noted by most of the pilots. The standard deviations are a measure of the variation in the pilot's rating of a particular task.

Pilot rating numbers without their accompanying pilot comments are of very little value. The individual pilot ratings and comments furnished in Appendix A are rather formidable in their volume and scope. The numerical summaries of Table 4, rather than being accepted by the reader at their Cooper-Harper rating scale face value, should be used as a guide to point out sections of particular interest in the appendix pilot rating information.

Sailplanes 4 and 6 received poor ratings in construction and rigging. Sailplanes 4 and 5 rated down in cockpit layout, sailplanes 3 and 5 in longitudinal handling qualities, and sailplane 6 in stall/spin characteristics. Sailplanes 3, 4, and 5 were given poor ratings in landing characteristics, and sailplane 6 in circling flight. Sailplane 1 received consistently higher ratings than all other aircraft, in every rating category, and was often cited as a benchmark of excellence for sailplane handling qualities. To gain more than this superficial information, the reader must refer to the individual pilot comments in the above areas, which provide an understanding of the reasons for the ratings.

Table 4. Rating Summary for Sailplanes

TASK	SAILPLANE											
	1		2		3		4		5		6	
	AVG	STDV	AVG	STDV	AVG	STDV	AVG	STDV	AVG	STDV	AVG	STDV
1 I. Design	2.50	.50	2.00	.71	2.00	.71	5.00	1.00	2.00	.00	4.50	2.50
2 A. Pilot Opin. of Const. Rigging	2.00	1.00	1.37	.41	2.25	.43	4.50	.50	1.88	.22	5.50	1.50
3 1. Ease of Inspection	3.00	.82	1.50	.50	2.75	1.30	2.50	.50	1.75	.43	3.00	.00
4 2. Safety of Control System	2.00	.00	2.50	1.12	1.75	.43	3.50	1.50	2.75	.43	2.00	.00
5 3. Ease of Assembly	2.33	.47	1.25	.43	1.75	.43	5.00	1.00	2.00	.00	6.00	1.00
6 B. Pilot Opinion of Cockpit Layout	3.60	.49	2.60	.80	1.80	.75	4.25	1.48	1.70	.60	2.00	1.00
7 1. Pilot Comfort	3.29	.88	2.14	.99	1.14	.35	2.33	.75	1.40	.49	1.67	.75
8 2. Control System Arrangement	3.29	1.39	2.71	.70	3.00	1.41	4.80	1.60	2.75	1.48	2.67	.94
9 3. Instrument Display	2.57	.49	2.33	1.11	1.50	.50	2.00	.63	1.60	.49	2.80	.75
10 4. Pilot Visibility	3.29	.88	1.43	.73	1.86	.83	1.83	1.07	2.00	.89	1.67	.47
11 5. Pilot Safety	2.75	.83	3.50	.50	3.50	1.12	1.60	.49	3.75	1.30	1.00	.00
12 II. Smooth Air Maneuvering	1.12	.22	2.40	.49	2.33	.47	2.00	.00	3.00	1.26	1.25	.43
13 A. Pilot Opin. of Initial Takeoff Roll	1.67	.94	2.75	.99	2.57	.73	2.67	1.60	3.20	1.17	1.80	.75
14 1. Towline Hookup	1.60	.49	2.17	.69	2.33	.94	1.17	.37	2.40	1.02	2.00	1.00
15 2. Control of Plane in Init. Roll	1.79	1.19	3.14	.99	2.57	.73	2.00	.58	3.20	1.17	1.83	1.07
16 B. Pilot Opinion of Tow	1.37	.41	2.20	.75	2.50	.50	2.20	.40	3.50	1.26	1.50	.50
17 1. Ease of Maintaining Position	1.43	.73	2.29	.70	2.29	.70	2.00	.00	2.80	1.33	1.67	.75
18 2. Aircraft Trim	3.50	1.34	2.57	.73	2.43	.49	2.50	1.26	2.20	.40	2.40	1.02
19 3. Control in Propwash	1.43	.73	2.14	.64	1.86	.64	2.17	.37	2.50	1.12	2.00	1.00
20 4. Release Characteristics	1.50	.50	1.67	.47	2.17	.69	1.80	.75	1.75	.43	1.83	.69

Table 4 (Continued)

		SAILPLANE											
		1	2	3	4	5	6						
TASK		<u>AVG</u>	<u>STDV</u>	<u>AVG</u>	<u>STDV</u>	<u>AVG</u>	<u>STDV</u>	<u>AVG</u>	<u>STDV</u>	<u>AVG</u>	<u>STDV</u>	<u>AVG</u>	<u>STDV</u>
51	F. Pilot Opin. of Plane Landing Char.	1.70	.40	2.75	1.30	3.20	.40	3.50	.50	2.90	.66	2.33	.47
52	1. Pilot Visibility	2.57	.90	1.43	.73	1.43	.49	1.50	.50	1.40	.49	1.00	.00
53	2. Glide Slope Control	1.57	.73	3.00	.93	2.57	.49	2.67	.47	2.40	.49	1.33	.75
54	3. Airs. Control, Airb. Ease of Mod.	2.14	.99	3.14	.99	3.14	.35	4.08	.61	2.60	.49	1.60	.80
55	4. Ease of Land. at Intended Spot	1.57	.49	2.57	.73	2.57	.73	<u>3.87</u>	.40	2.40	.49	1.50	.50
56	5. Ease of Control, Sink at Touch	1.50	.50	2.29	.88	2.43	.49	2.54	.85	2.40	.49	1.80	.40
57	6. Control During Rollout	1.43	.73	2.57	.73	<u>4.00</u>	2.38	1.67	.47	<u>4.00</u>	1.26	1.33	.47
58	III. Flight Characteristics in Convection	1.00	.00	2.50	.71	2.60	.49	2.62	.41	3.20	1.17	3.00	1.22
59	A. Pilot Opinion of Tow	1.50	.76	2.42	.84	2.42	.61	2.00	.00	<u>3.87</u>	1.43	2.25	.43
60	1. Ease of Maintaining Position	1.33	.75	2.50	.96	2.50	.50	2.00	.00	3.00	1.22	2.00	.00
61	2. Response to Vertical Currents	1.83	.69	2.50	.50	2.83	.69	2.00	.00	2.50	.50	2.00	.00
62	3. Release	1.80	.40	1.75	.43	2.00	.63	2.33	.47	2.00	.82	2.00	.00
63	B. Pilot Opinion of Circling Flight	1.00	.00	2.40	.97	2.00	.00	2.87	.74	2.30	.75	<u>4.33</u>	2.62
64	1. Low Speed Handling	1.17	.37	2.83	.90	2.00	.58	2.75	.83	2.40	.49	<u>5.00</u>	2.16
65	2. Stall-Spin Susceptibility	1.75	.38	2.33	1.37	2.00	.58	2.37	.41	1.60	.49	<u>5.33</u>	2.87
66	3. Ease of Centering Thermal	1.83	.69	2.33	.75	2.00	.58	2.75	.43	2.75	1.09	3.33	.47
67	4. Speed Control	1.50	.50	2.17	1.21	2.33	.47	3.25	1.09	2.20	.98	<u>4.33</u>	1.25
68	C. Pilot Opinion of Cruising Flight	1.60	1.20	2.20	.98	2.60	.97	2.37	.65	2.20	.98	1.67	.47
69	1. Ease of Controlling Airspeed	1.67	1.11	2.17	.69	2.33	.94	2.37	.65	2.60	1.36	1.50	.50
70	2. Pull up into Thermal	1.67	.47	2.00	1.15	2.00	.82	2.87	.89	2.00	.63	2.50	1.50
71	3. Ease of Pref. Secondary Tasks	1.50	.50	2.50	1.12	3.00	.82	2.50	.50	3.20	1.94	1.50	.50
72	4. Ride Quality	2.17	.80	2.17	.37	2.25	.56	2.75	.43	1.80	.75	2.50	.50
73	5. Ease of Main. Straight Flight	1.40	.49	2.33	1.11	1.50	.50	1.75	.43	1.60	.80	1.75	.43

3.2 Pilot Evaluation of Ease of Assembly, Inspection and Cockpit Layout

Although these factors are generally not regarded as an essential part of handling qualities, as, say, longitudinal stability, all three characteristics do influence the ease and precision with which the pilot is able to perform tasks for the overall mission of the sailplane. In rating these characteristics, the pilots tended to disregard the dichotomous structure of the Cooper-Harper scale; instead, they were asked to rate these factors on a linear scale from one to ten. Also, three of the pilots did not rate the ease of assembly and inspection since the flight test session did not provide enough time for them to become familiar with these characteristics.

The pilots who rated the ease of assembly and ease of control system inspection generally gave better ratings to the newer machines. These pilot ratings also confirmed the fact that frequent assembly/disassembly is part of the high-performance sailplane role and the ease of assembly should be a very important design objective.

Pilot comments on the cockpit layout show that there were wide variations among the six evaluation sailplanes. The pilots found visibility was adequate in all ships. They singled out poor ventilation, the use of curved control sticks, confusing or unhandy secondary control handles (such as trim and flap handles), need for good pilot protection as areas of concern. The variety of adverse comments indicates the need of some sort of standardization for the location, shape and color of the secondary control handles.

3.3 Pilot Opinion of Longitudinal Characteristics

Takeoff. Average pilot ratings ranged from 1.8 for sailplanes 1 and 6 to 3.2 for sailplanes 2 and 5. Sailplanes 1 and 6 were generally the most stable, had the highest stick forces, and had strong damping of the short period pitching oscillation. Pilots commented that sailplane 2 was more sensitive in pitch than they liked, and that they tended to overcontrol in pitch during takeoff. On sailplane 5, pilots reported disliking the stick bobbing force and aft when rolling over bumps. One pilot felt it necessary to maintain greater ground clearance while he was airborne and waiting for the towplane to accelerate to takeoff speed than with other gliders and that wing flexing resulted in undesirable excursions in fuselage-to-ground

clearance. Although he gave a pilot rating of 2, one pilot noted that on sailplane 4, the longitudinal stick feel-and-trim spring system had high and unsymmetric breakout forces which caused him to overcontrol.

Tow. Again, pilot ratings were best for sailplanes 1 and 6, averaging 1.4 for 1 and 1.5 for 6. The worst average rating was 3.5 for sailplane 5. Pilots strongly objected to inertially induced stick forces, and reported overcontrolling, and a feeling that a serious PIO could occur. When the tow speed was increased from the standard 70 knots to 80 knots, the overcontrol/PIO tendency was reported more severe. One pilot reported he was unwilling to fly left-handed while raising the landing gear on tow. Sailplane 2 was reported easily upset in rough air, requiring frequent small control corrections. It received several pilot ratings of 3. Sailplane 4 was reported sensitive and easy to overcontrol, receiving pilot ratings of 2 and 3.

Establishing and Maintaining Airspeed. Establishing and holding speed was rated satisfactory for all sailplanes. It was reported by one pilot to be difficult to make fine speed corrections in sailplane 4 due to high breakout forces (his pilot rating was 2 however). For sailplane 5, one pilot reported that a pitch correction tended to continue past the intended point and had to be arrested by a checking control input, (his pilot rating was 4).

Longitudinal Trimming. The trim system on sailplane 1 was rated unsatisfactory. Comments were that it was ineffective and inconvenient. The trim system of every sailplane was reported as inconvenient to use, but only sailplane 1 was rated unsatisfactory. Comments indicated that pilots were content to fly without trimming rather than use inconvenient trim devices, except in the case of sailplane 6 in which stick forces became excessive.

Pitch Sensitivity. Sailplanes 3 and 5 received some pilot ratings of 4 and 5 for oversensitivity. Sailplanes 2, 3, 4, and 5 were described as sensitive, but 2 and 4 did not receive poor pilot ratings for sensitivity.

Stick Force Gradient, Stick Fixed Stability, and Stick Free Stability.

These were not tasks, but requests for opinions on the suitability of the listed characteristics. In the absence of quantitative data and since the pilot comments were rather general, the responses to these three requests for pilot opinion are broadly summarized: sailplane 1 was well liked; numbers 2, 3, and 5 were characterized as having light stick forces, bordering on too

light, while sailplanes 4, and, even more so, 6, were judged to have too-heavy stick forces.

Return to Trim. The pilots were satisfied with the return-to-trim characteristics of all sailplanes, giving pilot ratings of 2 to 3. An exception to this was pilot 1 who apparently excited the phugoid mode on this test and rated phugoid damping. Two pilots felt the task had no relevance to their opinion of a sailplane's handling qualities. Early NACA flying qualities tests by Gilruth (Reference 3) also showed that the tendency to return to trim speed was relatively unimportant for visual flight.

Maneuver Response. Opinions diverged on the maneuvering responses of the six sailplanes. Sailplane 1, 4, and 6 were well liked by all pilots, receiving mostly 1 and 2 pilot ratings. Sailplane 2 received mostly 3 ratings and comments giving the impression it was more responsive than the pilots liked. Sailplanes 3 and 5 got mixed opinions. Sailplane 3 was rated 4 and sailplane 5 rated 5 due to low or nil stick-force-per-g by some pilots. Delayed g response due to the flexible wing was reported to cause difficulty in stabilizing rapidly applied g by one pilot.

Phugoid Characteristics. This was not a flying task susceptible to pilot rating. Nonetheless pilots expressed their opinions of the suitability of the characteristic. Pilots were satisfied with the lightly damped or neutral stick-free phugoids of sailplanes 1, 2, 4, and 6, while some pilots objected to the strongly divergent stick-free phugoids of sailplanes 3 and 5. The divergent motions appeared to be caused by a dynamical interaction between the sailplane phugoid mode and the pitch control system.

Dive Recovery. Sailplanes 1, 4, and 6 were regarded as satisfactory. Sailplane 2 was given satisfactory pilot ratings, but several comments suggested that it was more sensitive than desired. Sailplanes 3 and 5 were rated unsatisfactory by some pilots who commented that the stick forces were too light, and sometimes reversed during pull-outs.

Ease of Centering Thermal, and Speed Control in Circling Flight. All sailplanes were rated satisfactory for these tasks. Comments indicated that the high stick forces and heavy stability of sailplane 6 caused an undesirably high workload in circling at varying bank angles as is typically done in thermalling flight. On sailplane 3, comments noted that the very low or negative stick-force-per-g was very pleasant to fly and felt immediately

natural and comfortable during the thermalling task. On sailplane 5 the same comments were made, and additionally that in an established thermalling turn the stick could be moved as much as 7 cm aft without appreciably affecting the turn. This later characteristic was not felt objectionable.

Table 5
Sailplane Longitudinal Stability and Control Characteristics

<u>Sailplane</u>	<u>Control Forces</u>	<u>Trim</u>	<u>Static Longi- tudinal Stab.</u>	<u>Stick-Free Short Per. Damping</u>	<u>Stick Force Per G</u>	<u>Perceived Sensitivity</u>
1	Aerodynamic + Spring	Spring	Moderate	High	Mod- erate	Moderate
2	"	"	Lo	"	Lo	High
3	Spring + Bobweight	"	"	"	Nil	"
4	Aerodynamic + Spring	"	"	"	Lo	"
5	Spring + Bobweight	"	"	"	Nil	"
6	Aerodynamic	Tab	High	"	Mod- erate	Moderate

Table 6
Summary of Opinions on Longitudinal Handling Qualities

<u>Sailplane</u>	<u>Takeoff and Tow</u>	<u>Straight Flight</u>	<u>Maneuvering & Dive Pull-Out</u>	<u>Thermalling</u>
1	Well Liked	Well Liked	Well Liked	Well Liked
2	Satisfactory	Satisfactory	Satisfactory	Satisfactory
3	Satisfactory	Well Liked	Satisfactory	Well Liked
4	Satisfactory	Satisfactory	Satisfactory	Satisfactory
5	Satisfactory	Well Liked	Unsatisfactory	Well Liked
6	Well Liked	Well Liked	Well Liked	Satisfactory

Table 5 summarizes the longitudinal stability and control characteristics of the sailplanes evaluated and Table 6 summarizes the pilot opinion of longitudinal handling qualities for primary flight tasks. Table 6 shows that longitudinal characteristics best liked for thermalling are less well liked for takeoff, tow, maneuvering, and dive pull-out. From Table 5 it appears that increased stability and reduced sensitivity are beneficial to the first three tasks while lower stability and greater sensitivity are desirable for the last task. Table 6 shows that all the sailplanes had satisfactory or better longitudinal handling qualities for normal flying and thermalling, and that all but one were also satisfactory for maneuvering and dive pull-out. This was not surprising since all of the evaluation sailplanes were commercially successful in series production.

3.4 Sailplane Lateral-Directional Handling Qualities

Sailplane performance growth has not influenced lateral-directional handling qualities as much as the longitudinal handling qualities, although both have been degraded. The only serious lateral-directional problem apparent in current high performance sailplanes is in takeoff and landing, where low roll control and rudder power can lead to loss of directional control, especially in crosswinds. One cause is the placement of the landing wheel ahead of the C.G., which increases weather cock tendencies. Another is a raised C.G. coupled with a further aft and lower placement of the tow line attach point, which introduces a significant rolling moment with sailplane heading/tow line misalignment. This problem warrants further study to better define controllability during takeoff and landing.

Although pilot comments did not reflect any serious inflight problems, improvement in lateral-directional handling qualities, such as roll response quickening, increased roll control power, and reduction in rudder coordination requirements, would enhance performance in soaring flight, due to the importance of quickly acquiring and centering the thermals and of reducing pilot workload. Informal discussions with the evaluation pilots, as well as reported pilot comments, support this conclusion. Pilot opinions were mostly in the "excellent" to "minor but annoying deficiencies" region (pilot ratings 1 to 4).

Sailplane 1 was "excellent" to "good" (pilot rating 1 to 2) in almost every area. Pilot comments emphasized the good control harmony between rudder and aileron and ease of rudder-aileron coordination. Spiral stability was neutral, which was noted as beneficial for thermalling flight.

Sailplane 2 pilot ratings ranged from 2 to 4, with many comments about high rudder coordination workload in maintaining ball-in-the-center flight, both in turns and turn entries as well as level flight. Inadequate rudder control power was cited, as evidenced by insufficient rudder to maintain balanced flight in moderate rate turn entries. Spiral stability was slightly negative in thermalling configuration, which increased rudder-aileron coordination problems. Lateral-directional characteristics for this sailplane could be summarized as distracting and irritating. One pilot commented negatively on pitchup with sideslip, which is peculiar to this sailplane.

Pilot ratings for sailplanes 3, 4, and 5 fell in the 1 to 4 range. In average overall pilot ratings, sailplane 3 was slightly better than sailplanes 4 and 5, but ratings for each sailplane showed different areas of emphasis, as indicated in the following paragraphs.

Sailplane 3 lateral-directional control harmony and coordination was good. Comments ranged from "no problem" to "pleasant". Comments showed, however, that sailplane 1 was better. A comment for sailplane 3 on aileron effectiveness was that ailerons remained very effective even below stall speed.

The only complaints for sailplane 4 were due to the requirement for considerable top aileron in turning flight and mild objection to coordination workload in lateral maneuvering.

Sailplane 5 received good to excellent ratings for its ease of control in maintaining desired bank angles in turning flight. Several pilots objected to its low maximum roll rate of about 15 deg/sec, about 5 deg/sec less than that of all the other sailplanes, though 2 pilots commented that roll rate was surprisingly good for a sailplane of this large a wing span. Other comments indicated that the rudder force gradient was too high and noted too wide a deadband around neutral for airplane response to rudder inputs.

Sailplane 6 was judged as a training sailplane, suitable for transitioning into high performance ships. In this context, it received very good ratings, except for ease of maintaining desired bank angles and for control near the stall. Concerning turning flight, pilots commented that rudder forces were

too high relative to longitudinal stick forces and that unintentional overcontrolling in pitch produced frequent pre-stall airframe buffeting. Lateral control near stall was poor due to decaying roll control power with airspeed decrease.

Rudder overbalance, or "rudder lock" was a characteristic common to sailplanes 2, 3, and 5. The pilots did not find this unsafe or even annoying, except on sailplane 5; one pilot gave sideslips a rating of 4 due to this feature, noting that about 180 N pedal force was required to "unlock" the rudder and that large sideslip angles were possible. Control, however, remained good and very little buffeting occurred at the high sideslip angles. This is classified as a minor but annoying deficiency. Rudder overbalance on the other sailplanes required much less pedal force to unlock. It is concluded that although proportionally increasing rudder pedal force with rudder deflection is a desirable characteristic, rudder overbalance is not unsafe unless very high pedal forces or other overruling characteristics are involved. For instance, sailplane 2 encountered overbalance at about 1/2 rudder deflection and sailplanes 3 and 5 at about 3/4 deflection. These conditions were acceptable, but it might be that overbalance of significantly less rudder deflection would be unacceptable.

3.5 Sailplane Stall/Spin Characteristics

Cross-country soaring flight sometimes involves steep turns at low altitudes to take advantage of whatever lift may be available, avoiding landing unless absolutely necessary. Since optimum airspeed for thermalling flight is near the stall speed, stall and incipient spin characteristics are of prime importance in safety of flight.

Stall warning characteristics of the evaluation sailplanes were described as mild for sailplanes 1 through 5 and too much for sailplane 6. The airspeed stall warning band varied from 1 to 3 kts for the first 4 sailplanes, and were often in a form that could be masked by atmospheric turbulence. However, once the stall was recognized, recovery in most cases was easily and quickly effected by merely relaxing aft stick pressure and flying out of the stalled condition with little altitude loss. Sailplane 6, on the other hand, had a wide stall warning airspeed band of 10-12 kts, which caused stall buffet to

occur frequently at thermalling flight airspeeds. The pilots noted that this is an undesirable characteristic because familiarity with the stall warning buffet degrades its effectiveness and tends to cause the pilot to ignore the warning.

As to stall, incipient spin, and recovery characteristics, sailplanes 1, 2, 3, and 5 generally received good to excellent ratings with sailplane 1 being foremost. Good aileron control was noted, even below stall speed, and abused, cross-controlled stalls did not reveal undesirable qualities. Sailplane 4 recovered immediately with relaxation of aft stick force, but two pilots noted a definite autorotative (spin) tendency if recovery was not executed promptly with wing drop. Sailplane 6 showed a tendency to yaw and roll to the left and to pitch down from a cross-control stall and received lower ratings due to this characteristic toward spinning.

3.6 Sailplane Approach and Landing Characteristics

Once committed to landing, sailplanes cannot go up; it follows that one of the primary considerations in evaluating approach and landing characteristics is ease of glidepath control. Precision in touchdown control is paramount for landing in unprepared and restricted areas, a situation often encountered in cross-country soaring flight. It is therefore not surprising that most of the evaluation sailplanes were criticized for lack of spoiler, flap, or air-brake effectiveness and precision.

Sailplane 6 received the best ratings, in the fair to good category, largely because of the effectiveness of spoilers in controlling glidepath. For instance, one pilot noted that due to dive brake effectiveness, it was easy to make "difficult" landings. "Difficult" here means landings over obstructions into a limited landing area.

Sailplane 1 again received the best rating of all except sailplane 6, although it was noted that the divebrakes were somewhat ineffective. The same comment was made about sailplanes 2, 3, and 5. Sailplane 4 relied only on flaps for glidepath control. This concept was criticized on two points: large changes in pitch attitude with varying degrees of flap extension made precise glidepath control more difficult, and awkward placement, high force requirements, and complex flap control positioning requirements degraded precision of

glidepath control. Some pilots criticized the "suck-open" tendency of spoiler controls on the other sailplanes for the same reasons; the necessity to hold force to restrain spoiler control lever aft movement degraded precise control in pitch with light stick forces, especially if spoiler control forces were high.

It is concluded that more quantitative information should be gathered on primary glide path control capability and also interaction of glide path controls with primary flight controls.

3.7 Pilot Opinion and Certification Criteria

Pilot opinion specifies the characteristics pilots like in sailplanes. Certification criteria specify the characteristics thought by the certifying authority to be essential to their safe operation. There is no reason to expect that pilots will invariably prefer a safer characteristic to one less safe. The contribution to safety of a given characteristic sometimes being recognizable only by a complex analysis or demonstrated in accident patterns. However, in the absence of such analysis or evidence, it would seem sensible that criteria should conform in general to favorable pilot opinion.

General and specific examples of conflicting criteria and pilot opinion follow:

In general, pilots were willing to accept sailplanes that were somewhat more sensitive and less stable in pitch than they liked for take-off, tow, and dive recovery in order to get easy longitudinal maneuvering and low stick forces for soaring flight--the mission of a sailplane. In particular, the criteria specifying a return-to-trim within, say, 10 percent of trim speed was felt to be of no benefit, and when achieved through increased stick centering forces considered to be a harassment. In what way such a criterion is essential to safety is not clear.

The only undesirable characteristic exhibited by some of the high performance sailplanes was marginal control during takeoff and landing. Current certification requirements are vague in this area. A requirement of controllability during takeoff and landing in crosswinds up to a prescribed level would be appropriate.

The requirement that no rudder overbalance occur was considered by some pilots to be overly restrictive. They argued that the natural instinct to straighten out would be sufficient to cue the pilot to overcome the mild overbalance that commonly occurs on gliders at large sideslip angles.

The sailplanes flown illustrated the ways in which stalling behavior desirable for sailplanes differs from that desirable for power planes. First, pre-stall warning was found to be of little or no value because of the normal course of thermalling, the stall boundary is commonly exceeded--an alarm quickly loses its value when often sounded. In any case, regardless of the presence or absence of any pre-stall warning, the considerable loss of climb that would result from reacting to every momentary gust-induced stall warning is unacceptable to most sailplane pilots. They will maneuver as the thermal demands and accept brief occasional stalls. Because occasional stalls must be accepted, it is important that only the least reduction in angle-of-attack be sufficient to achieve an immediate unstall, and that very little loss in altitude and very minor upset accompany the stall. Fortunately, this was just the behavior observed for all the sailplanes except sailplane 6 which had considerable altitude loss and some roll and yaw upset. For deeper or more prolonged or abused stalls, traditional criteria appeared acceptable. Thus, a modification to the traditional criteria such that the initial stall replaced buffet as a warning, and the deeper or aggravated stall be treated as the stall for purposes of certification.

The drag modulation observed on the test sailplanes was felt to be generally insufficient and the operating forces for the drag devices were felt to be generally undesirable for both flaps and airbrakes. Additionally, the variation of divebrake or flap effectiveness during the flare, float and touchdown phase was felt to degrade the pilots' ability to control his landing accuracy. In view of the importance of accurate landings for sailplanes, it was felt that a rational basis should be established for future criteria.

4. CONCLUDING REMARKS

The handling qualities of six sailplanes were evaluated by seven pilots in a flight test session consisting of 98 flights. The term "handling qualities" was defined to be those broad characteristics or attributes which influence the ease and precision with which the pilot is able to perform tasks for the overall mission of the sailplane. In this context the evaluation pilots were instructed to regard cross-country flight under visual flight rules as the principal mission of the sailplane.

Sailplane characteristics were evaluated using the Cooper-Harper rating scale with additional comments. The pilot opinion data indicates the following:

1. The evaluation sailplanes were found generally deficient in the area of cockpit layout. Poor cockpit ventilation, the use of curved control stick, confusing secondary control handles and the need for better cockpit crashworthiness were cited as reasons for deficiency.
2. The pilots indicated general dissatisfaction with pitch sensitivity which in some cases was coupled with inertially induced stick forces. While all sailplanes were judged satisfactory for centering thermals and in the ease of speed control in circling flight, pilot opinions diverged on the maneuvering response, pull-out characteristics from a dive, and on phugoid damping. The pilots found that the tendency to return to trim airspeed is relatively unimportant for visual flight.
3. Lateral-directional control problems were noted mainly during takeoff and landing. Pilot comments indicate the desirability of overall improvements in roll response quickening, increasing roll control power and reduction in the rudder coordination requirement. Existing levels of rudder overbalance or "rudder lock" was not found unsafe or even annoying.
4. Five of the evaluation sailplanes had very narrow airspeed band in which perceptible stall warning buffet occurred. This was not objectionable, however, since stall recovery was easy. The pilots objected to the characteristics of wide airspeed band of stall warning followed

by a stall with yawing and rolling tendency and substantial loss of altitude during the stall.

5. Landing characteristics of the evaluation sailplanes were found generally objectionable. Ineffective divebrakes, and the necessity of exerting a force to restrain divebrake control lever were quoted by some of the pilots. Flap type glide path control was also rated deficient due to the large attitude changes accompanying flap deflections and to the excessive flap actuation forces.

The present study shows the need for a more quantitative investigation of the factors influencing pitch control sensitivity such as precise measurements of stick forces due to both the aerodynamic hinge moments and the bobweight effects arising from the different horizontal tail configurations. Further study is required of lateral-directional control during takeoff and landing. More quantitative information should be gathered also on the various glide path control systems and the interaction of glide path controls with primary flight controls.

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Appendix A
Pilots' Questionnaire



Appendix A.
Questionnaire

SAILEPLANE EVALUATION

Pilot _____ Sailplane _____

Date _____ Flight No. _____

I. Design.

A. Pilot Opinion of Construction & Rigging.

1. Ease of Inspection.

2. Safety of Control System.

3. Ease of Assembly.

4. Comments _____

B. Pilot Opinion of Cockpit Layout.

1. Pilot Comfort.

2. Control System Arrangement.

3. Instrument Display.

4. Pilot Visibility.

5. Pilot Safety.

6. Comments _____

II. Smooth Air Maneuvering.

A. Pilot Opinion of Initial Takeoff Roll.

1. Towline Hookup.

2. Control of Sailplane During Initial Roll. . .

3. Comments _____

B. Pilot Opinion of Tow.

1. Ease of Maintaining Position.

2. Aircraft Trim.

3. Control in Propwash.

4. Release Characteristics.

5. Comments _____

C. Pilot Opinion of Longitudinal Handling.

1. Ease of Establishing and Maintaining a
Constant Airspeed.

2. Sailplane Trim System Over Speed Range. . .

3. Pitch Sensitivity.

4. Stick Force Gradient.

5. Stick Fixed Stability.

- 6. Stick Free Stability.
- 7. Return to Trim.
- 8. Maneuvering Response.
- 9. Phugoid Characteristics.
- 10. Dive Recovery.
- 11. Comments _____

- D. Pilot Opinion of Lateral Handling.
- 1. Aileron Force Gradient.
- 2. Rudder Force Gradient.
- 3. Roll Rate Over Speed Range.
- 4. Sideslip Characteristics.
- 5. Ease of Turn Entry.
- 6. Yaw Due to Aileron.
- 7. Yaw Due to Roll.
- 8. Ease of Maintaining 45° Bank Turn.
- 9. Ease of Maintaining 60° Bank Turn.
- 10. Comments _____

E. Pilot Opinion of Sailplane Stall-Spin Characteristics

- 1. Rudder and Aileron Effectiveness During Stall
- 2. Stall Warning.
- 3. Aggravated Stall-Tendency to Spin.
- 4. Stick Force Gradient.
- 5. Stall Recovery, Altitude Loss.
- 6. Spin Entry.
- 7. Spin Recovery.
- 8. Stall From Turn at Low Speed.

9. Comments _____

F. Pilot Opinion of Sailplane Landing Characteristics.

- 1. Pilot Visibility.
- 2. Glide Slope Control.
- 3. Airspeed Control, Airbrake Ease of Modulation
- 4. Ease of Landing at Intended Spot.
- 5. Ease of Controlling Sink at Touchdown.
- 6. Control During Rollout.

7. Comments _____

III. Flight Characteristics in Convection.

A. Pilot Opinion of Tow.

1. Ease of Maintaining Position.

2. Response to Vertical Currents.

3. Release.

4. Comments _____

B. Pilot Opinion of Circling Flight.

1. Low Speed Handling.

2. Stall-Spin Susceptibility.

3. Ease of Centering Thermal.

4. Speed Control.

5. Comments _____

C. Pilot Opinion of Cruising Flight.

1. Ease of Controlling Airspeed.

2. Pull up into Thermal.

3. Ease of Performing Secondary Tasks.

4. Ride Quality

5. Ease of Maintaining Straight Flight

6. Comments _____

Appendix B
Cooper Harper Ratings and Pilots' Comments



***** ZEROS INDICATE NO RATING BY PILOT *****

SAILPLANE 1 DATA

TASK	DESCRIPTION OF TASKS	1	2	3	PILOT	5	6	7	AVER.	STD DEV
1	1. DESIGN	.00	.00	3.00	.00	.00	2.00	.00	2.500	.500
2	A. PILOT OPIN. OF CONST. & RIGGING	.00	.00	3.00	.00	.00	1.00	.00	1.000	1.000
3	1. EASE OF INSPECTION	.00	4.00	3.00	.00	.00	2.00	.00	3.000	.816
4	2. EASE OF CONTROL SYSTEM	.00	2.00	2.00	.00	.00	2.00	.00	2.000	.000
5	3. EASE OF ASSEMBLY	.00	2.00	3.00	.00	.00	2.00	.00	2.333	.471
74	AVER. AND STD. DEV. OF SUBTASKS(EX 1,2,..)	.0	.0	2.7	.5	.0	2.0	.0	2.4	.68

COMMENTS

TASK PILOT
 2 3
 3 3
 4 3
 5 3
 74 6
 74 6
 74 6

NOT AS GOOD AS GLASS SHIPS
 HAVE TO REMOVE OVERWING FAIRING
 GOOD
 MODERATELY EASY
 AFTER ASSEMBLY, INSPECTION IS DIFFICULT AT ELEVATOR AND WING PINS
 /AILERON CONNECTION

SAILPLANE 2 DATA

TASK	DESCRIPTION OF TASKS	1	2	3	PILOT	5	6	7	AVER.	STD DEV
1	1. DESIGN	2.00	1.00	3.00	.00	.00	2.00	.00	2.000	.707
2	A. PILOT OPIN. OF CONST. & RIGGING	1.50	1.00	1.00	.00	.00	2.00	.00	1.375	.415
3	1. EASE OF INSPECTION	2.00	1.00	1.00	.00	.00	2.00	.00	1.500	.500
4	2. EASE OF CONTROL SYSTEM	1.00	2.00	3.00	.00	.00	4.00	.00	1.118	1.118
5	3. EASE OF ASSEMBLY	1.00	1.00	1.00	.00	.00	2.00	.00	1.250	.433
74	AVER. AND STD. DEV. OF SUBTASKS(EX 1,2,..)	1.3	.5	1.7	.9	.0	2.7	.9	1.7	.92

COMMENTS

TASK PILOT
 74 3
 3 3
 4 3
 5 3
 74 3
 74 3
 74 6

EXCELLENT
 APPEARS MECHANICALLY OF MARGINAL DURABILITY
 POSSIBLE TO GET AILERON MOVEMENT WITH DISCONNECTED PUSH RODS
 OUTSTANDING
 HAS POOR HISTORY FOR RUDDER ACTIVATION SYSTEM. ELEVATOR, AILERON
 AND FLAP SYSTEM IS EXCELLENT
 AILERONS CONTROL RODS ENDS, CAN BE INSTALLED BUT NOT PINNED.
 OTHERWISE IT IS BY FAR THE BEST ASSEMBLY OF ANY SAILPLANE.

SAILPLANE 3 DATA

TASK	DESCRIPTION OF TASKS	1	2	3	PILOT	5	6	7	AVER.	STD DEV
1	1. DESIGN	2.00	1.00	2.00	.00	.00	3.00	.00	2.000	.707
2	A. PILOT OPIN. OF CONST. & RIGGING	2.00	2.00	2.00	.00	.00	3.00	.00	2.250	.433
3	1. EASE OF INSPECTION	2.00	2.00	2.00	.00	.00	5.00	.00	2.750	1.299
4	2. EASE OF CONTROL SYSTEM	1.00	2.00	2.00	.00	.00	2.00	.00	1.750	.433
5	3. EASE OF ASSEMBLY	2.00	2.00	1.00	.00	.00	2.00	.00	1.750	.433
74	AVER. AND STD. DEV. OF SUBTASKS(EX 1,2,..)	1.7	.5	2.0	.0	.0	3.0	1.4	2.1	.95

COMMENTS

TASK PILOT
 74 3
 3 3
 4 3
 5 3
 74 3
 74 3

EXCELLENT
 NOT AS EASY AS SAILPLANE 2 OR 5
 UNABLE TO VISUALLY INSPECT AILERON CONNECTORS BEHIND SPAR
 EXCELLENT
 EXCELLENT
 QUALITY OF CONSTRUCTION IS EXCELLENT--AILERON AND AIR BRAKE LINKAGES

***** ZEROS INDICATE NO RATING BY PILOT *****

SAILPLANE 3 DATA

TASK	DESCRIPTION OF TASKS	1	2	PILOT 3	4	5	6	7	AVER.	STD DEV							
9	B. PILOT OPINION OF COCKPIT LAYOUT	2.00	1.00	2.00	1.00	1.00	1.00	3.00	1.809	.748							
9	1. CONTROL SYSTEM ARRANGEMENT	2.00	1.00	2.00	1.00	1.00	1.00	3.00	1.800	1.414							
10	2. INSTRUMENT DISPLAY	3.00	2.00	2.00	1.00	1.00	1.00	1.00	1.857	.899							
11	3. PILOT VISIBILITY	3.00	2.00	1.00	1.00	1.00	1.00	1.00	1.857	.899							
11	4. PILOT SAFETY	3.00	3.00	3.00	3.00	3.00	3.00	3.00	3.500	1.118							
75	AVER. AND STD. DEV. OF SUBTASKS(EX 1,2,...	2.0	.9	1.7	.8	2.0	.6	1.8	1.0	2.0	.9	3.4	1.9	2.2	1.6	2.2	1.29

COMMENTS

VERY GOOD, BETTER THAN SAILPLANE 2. COULD USE MORE VENTILATION
 CONTROL STICK, RELEASE LEVER TOO FAR FWD.
 FOR RELEASE HARD TO REACH, BRAKE A LITTLE AWKWARD TO REACH.
 HEAD AT SPEED, SO THAT POSITIVE FEEL GIVES UP ELEVATOR INPUT, VERY
 VIBRATED AND DOWN SLIGHTLY OBSCURED
 VERY GOOD CONSTRUCTION MINIMAL IN STRENGTH
 CROSS FUSELAGE BOOR ENERGY ABSORBER
 NOT A BELT IN STAY PLANE AS SUCH THAT SEAT BELT ADJUSTMENT WAS
 DIFFICULT TO RUN AND OVER A DITCH IN FLIGHT
 SEAT BELT A LITTLE LOOSE, SO BOUNCED HEAD ON CANOPY. SEAT BELT
 ADJUSTMENT DIFFICULT TO USE
 ADDITIONAL NOSE STRENGTH SHOULD BE ADDED TO PROTECT PILOT'S FEET/LEGS
 IN CASE OF BAD LANDING.
 INSTRUMENT PANEL TOO FAR FWD. ACTUALLY WITH CUSHIONS, THE PANEL
 IS NOT DIRECTLY VISIBLE.
 WOULD BE ACCEPTABLE FOR PEOPLE WITH SHORT REACH ON CONTROL STICK
 WOULD BE ACCEPTABLE FOR PEOPLE WITH SHORT REACH ON CONTROL STICK
 AWKWARD TO APPLY FULLY WITHOUT MOVING HAND ON CONTROL COLUMN
 ARM LOCK (KNOB) MEANS DIFFICULT TO UNLOCK. RUDDER ADJUSTMENT
 AND EASE OF ADJUSTMENT EXCELLENT.
 CANNOT REACH TOW RELEASE--NEED ROPE! CANNOT REACH SWITCHES ON FWD
 PANEL! TRIM CONTROL TIRING AND IRRITATING TO USE.

SAILPLANE 4 DATA

TASK	DESCRIPTION OF TASKS	1	2	PILOT 3	4	5	6	7	AVER.	STD DEV							
9	B. PILOT OPINION OF COCKPIT LAYOUT	.00	.00	4.00	.00	2.00	6.00	5.00	4.250	1.478							
9	1. PILOT COMFORT	.00	2.00	2.00	2.00	2.00	4.00	2.00	2.333	1.600							
10	2. INSTRUMENT DISPLAY	.00	.00	3.00	1.00	2.00	2.00	2.00	2.000	1.600							
11	3. PILOT VISIBILITY	.00	4.00	1.00	1.00	2.00	2.00	1.00	1.833	1.047							
11	4. PILOT SAFETY	.00	2.00	2.00	1.00	1.00	2.00	1.00	1.600	.490							
75	AVER. AND STD. DEV. OF SUBTASKS(EX 1,2,...	.0	.0	2.7	.9	2.8	1.7	1.6	.8	2.0	.6	3.0	1.3	3.0	2.3	2.5	1.50

COMMENTS

COCKPIT IS SMALL. MY HEAD ALMOST TOUCHES THE CANOPY WHICH CAN LEAD
 TO SOME BUMPS IN TURBULENCE. FOR 1.33RAD FLAP
 COMPLEX CONTROL AWKWARD. RELEASE LEVER TOO FAR FWD.
 FLAP UNHANDY, COMPLICATED TO USE. SUSCEPTIBLE TO MIS-USE
 (FLAP HANDLE, TRIM HANDLE AND BRAKE SHOULD BE IMPROVED)
 FLAP HANDLE, TRIM HANDLE AND BRAKE SHOULD BE IMPROVED
 AND TRIM CONTROL IS TOO HIGH AT MAX FLAP SPEEDS
 THE TRIM CONTROL IS A LITTLE AWKWARD TO REACH AND TO MOVE PRECISELY.
 OPERATE RELEASE NOT NEARLY AS GOOD AS SAILPLANE 3.
 THE RELEASE IS A LITTLE AWKWARD TO REACH AND TO MOVE PRECISELY.
 WHILE SEAT IS A LITTLE AWKWARD TO REACH AND TO MOVE PRECISELY.
 TRIM CONTROL TOO FAR FWD. ON TOW, BREAKOUT FORCE IN FWD. DIRECTION

***** ZEROS INDICATE NO RATING BY PILOT *****

SAILPLANE 5 DATA

TASK	DESCRIPTION OF TASKS	1	2	PILOT 3	4	5	6	7	AVER.	STD DEV	
8	B. PILOT OPINION OF COCKPIT LAYOUT	2.50	2.00	2.00	.00	.00	1.00	1.00	1.700	.600	
9	1. PILOT COMFORT	1.00	2.00	2.00	.00	.00	1.00	1.00	1.400	.490	
10	2. CONTROL SYSTEM ARRANGEMENT	3.00	2.00	2.00	.00	.00	5.00	1.00	2.750	1.479	
11	3. INSTRUMENT DISPLAY	1.00	2.00	2.00	.00	.00	2.00	1.00	1.600	.894	
	4. PILOT VISIBILITY	3.00	2.00	1.00	.00	.00	3.00	1.00	2.000	.894	
	5. PILOT SAFETY	3.00	3.00	3.00	.00	.00	6.00	1.00	3.750	1.299	
75	AVER. AND STD. DEV. OF SUBTASKS(EX 1,2,..)	2.2	1.0	2.2	.4	2.0	.6	.0	.0	.0	2.2

TASK PILOT

COMMENTS

1 DRAG CHUTE DEPLOYMENT LEVER IN ANKWARD POSITION
 2 CONTROL STICK AND RELEASE LEVER TOO FAR FWD
 3 VERY LARGE COMFORTABLE COCKPIT GENERALLY WELL LAID OUT. TRIMMER IS HARD TO OPERATE AND HIGHLY ANNOYING. DRAG CHUTE KNOW SUSCEPTIBLE TO INADVERTENT OPERATION.
 4 EXCELLENT COCKPIT LAYOUT
 5 EXCELLENT COCKPIT LAYOUT
 6 ELEVATOR OFFSET SO AS TO GIVE MOMENTUM TO UP ELEVATOR WHEN YOU HIT A POSITIVE IGL. TOW RELEASE TOO FAR FWD.
 7 END VISIBILITY MARGINAL DURING TOW
 8 EXCELLENT
 9 VIEW OF TOWPLANE OK, BUT COULD BE IMPROVED.
 10 COCKPIT CONSTRUCTION MINIMAL IN STRENGTH
 11 NO AS SAFE AS SOME
 12 EXCESSIVE BALLAST IN NOSE COULD BE CONVERTED INTO GLASS TO IMPROVE PILOT COMFORT VS. EXCELLEN
 13 PILOT COMFORT IS EXCELLEN
 14 VENTILATION SHOULD RE BETTER. VENT AIR BECAUSE SHOULD HAVE BEEN PROVIDED.
 15 EXCELLENT CONTROL PLACEMENT, SEAT DESIGN AND VISIBILITY. FLAP AND SPEED BRAKE CONTROLS ARE WELL LOCATED AND CONVENIENT TO USE.

SAILPLANE 6 DATA

TASK	DESCRIPTION OF TASKS	1	2	PILOT 3	4	5	6	7	AVER.	STD DEV	
8	B. PILOT OPINION OF COCKPIT LAYOUT	.00	.00	3.00	.00	.00	1.00	.00	2.000	1.000	
9	1. PILOT COMFORT	.00	2.00	3.00	1.00	1.00	4.00	3.00	1.667	.745	
10	2. CONTROL SYSTEM ARRANGEMENT	.00	2.00	3.00	3.00	2.00	3.00	4.00	2.800	.943	
11	3. INSTRUMENT DISPLAY	.00	2.00	3.00	2.00	2.00	2.00	2.00	2.667	.748	
	4. PILOT VISIBILITY	.00	2.00	1.00	2.00	1.00	1.00	1.00	1.667	.471	
	5. PILOT SAFETY	.00	1.00	1.00	1.00	1.00	1.00	1.00	1.000	.000	
75	AVER. AND STD. DEV. OF SUBTASKS(EX 1,2,..)	.0	.0	1.7	.4	2.0	.9	1.8	.7	1.6	1.9

TASK PILOT

COMMENTS

3 EXCELLENT
 4 TRIM WHEEL SHOULD BE ON LEFT
 5 TRIM WHEEL LOCATED ON WRONG SIDE OF COCKPIT
 6 TRIM TOO FAR FWD, TRIM WHEEL ON WRONG SIDE.
 7 TOW RELEASE SHOULD BE OFF TO LEFT SIDE; TRIM WHEEL ON LEFT SIDE
 8 TRIM CONTROL SHOULD BE ON LEFT SIDE OF COCKPIT. STICK TOO FAR FWD AT MOST FWD POSITION
 9 AT FAIRLY POOR ON THIS GLIDER, SHOULD HAVE COMPENSATED VARIOMETERS NON STANDARD
 10 EXCELLENT
 11 VERY SUBSTANTIAL COCKPIT STRUCTURE
 12 TRIM WHEEL ON WRONG SIDE AND HARD TO USE
 13 GOOD, SAFE DESIGN FEATURES IN COCKPIT. I WOULD QUESTION SOME OF THE AERODYNAMIC COMPROMISES MADE FOR THE SAKE OF ROOMINESS
 14 CONTROL TRAVELS IS MUCH TOO EXTENSIVE FOR RUDDER, AILERON, ELEVATOR, AND DIVE BRAKES

***** ZEROS INDICATE NO RATING BY PILOT *****

SAILPLANE 1 DATA

TASK	DESCRIPTION OF TASKS	1	2	PILOT 3	4	5	6	7	AVER.	STD DEV			
12	II. SMOOTH AIR MANEUVERING	1.50	1.00	1.00	.00	.00	1.00	.00	1.125	.217			
13	A. PILOT OPIN OF INITIAL TAKEOFF RLL	1.00	1.00	1.00	.00	3.00	1.00	3.00	1.667	.943			
14	1. TOWLINE HOOKUP	1.00	1.00	2.00	.00	2.00	1.00	2.00	1.600	.490			
15	2. CONTROL OF PLANE IN INIT. ROLL	1.00	1.00	1.00	2.00	4.50	1.00	2.00	1.786	1.191			
76	AVER. AND STD. DEV. OF SUBTASKS(EX 1,2,..)	1.0	.0	1.0	.0	3.2	1.3	1.0	.0	2.0	.0	1.7	.97

COMMENTS

3 EXCELLENT CHARACTERISTICS IN THIS PHASE OF THE FLIGHT
 4 ON ONE TOW I HAD FULL FORWARD STICK AND WAS STILL GOING UP WHILE
 5 TOW PLANE WAS STILL ON GROUND. PROBABLY SHOULD HAVE RELEASED.
 7 NO PROBLEMS IN TAKE OFF, INCLUDING LIGHT CROSSWIND 9KTS, 45DEG TO RWY

SAILPLANE 2 DATA

TASK	DESCRIPTION OF TASKS	1	2	PILOT 3	4	5	6	7	AVER.	STD DEV					
12	II. SMOOTH AIR MANEUVERING	2.00	2.00	3.00	.00	.00	2.00	3.00	2.400	.490					
13	A. PILOT OPIN OF INITIAL TAKEOFF RLL	1.50	2.00	3.00	.00	.00	4.00	2.00	2.750	.990					
14	1. TOWLINE HOOKUP	1.00	2.00	2.00	.00	3.00	3.00	2.00	2.167	.687					
15	2. CONTROL OF PLANE IN INIT. ROLL	2.00	2.00	4.00	4.00	4.00	4.00	2.00	3.143	.990					
76	AVER. AND STD. DEV. OF SUBTASKS(EX 1,2,..)	1.5	.5	2.0	.0	3.0	1.0	4.0	.0	3.5	.5	2.0	.0	2.7	.99

COMMENTS

2 SOME TENDENCY TO DROP WING AT START, DON'T LIKE TO HAVE TO MOVE
 3 FLAPS DURING 1.0. ROLLTOP AT START, TO NEUTRALY FLAP OPERATING
 4 THERE IS EXCELLENT TENDENCY TO DROP A WING ON ROLLOUT. STICK LOCATION IS
 5 INSUFFICIENT. RUDDER LOCATION OF CONTROL STICK, CONTROL STICK SHORT
 6 RESULTED IN POOR 1.0. CONTROL
 7 ALL FLAPS ALWAYS DRAGGED BACK TOO FAR FORWARD. FELT LIKE NOT ENOUGH
 8 RUDDERON IN TAKEOFF AT FIRST EVEN WITH FLAPS IN THE NEGATIVE
 9 NO PROBLEMS IN TAKEOFF, INCLUDING LIGHT CROSSWIND 19KTS, 785RAD TO RW

***** ZEROS INDICATE NO RATING BY PILOT *****

SAILPLANE 3 DATA

TASK	DESCRIPTION OF TASKS	1	2	PILOT 3	4	5	6	7	AVER.	STD DEV							
12	II. SMOOTH AIR MANEUVERING	3.00	.00	2.00	.00	.00	2.00	.00	2.333	.471							
13	A. PILOT OPIN. OF INITIAL TAKEOFF RLL	2.00	3.00	2.00	2.00	2.00	4.00	3.00	2.671	.728							
14	1. CONTROL OF PLANE IN INIT. ROLL	3.00	3.00	1.00	.00	.00	4.00	2.00	2.333	.923							
15	2. CONTROL OF PLANE IN INIT. ROLL	2.00	4.00	2.00	2.00	2.00	3.00	3.00	2.571	.928							
76	AVER. AND STD. DEV. OF SUBTASKS(EX 1,2,..)	2.5	.5	3.0	1.0	1.5	.5	2.0	.0	2.0	.5	2.5	.5	2.5	.5	2.5	.64

COMMENTS

13 PILOT USUALLY PUMPS ELEVATOR
 14 PULLED ON ROPE EXTENSION BECAUSE HANDLE TOO FAR FWD.
 15 VISIBILITY AND DIRECTIONAL CONTROL LIMITED
 16 CROSS WIND CAPABILITY MARGINAL
 17 6,7,9 DIVERGES, TOO DANGEROUS, EXTREME
 18 RUDER WEAK DURING ROLL. EASY TO DROP
 19 NO PROBLEM WITH INITIAL TAKEOFF ROLL
 20 ON TAKEOFF ROLL WITH AIR VENT OPEN, SAND AND ROCKS WERE FLOWN
 21 THROUGH THE VENT INTO THE COCKPIT BY THE TOWPLANE.

SAILPLANE 4 DATA

TASK	DESCRIPTION OF TASKS	1	2	PILOT 3	4	5	6	7	AVER.	STD DEV							
12	II. SMOOTH AIR MANEUVERING	.00	.00	2.00	.00	2.00	2.00	2.00	2.000	.000							
13	A. PILOT OPIN. OF INITIAL TAKEOFF RLL	.00	3.00	6.00	1.00	2.00	2.00	2.00	2.667	1.599							
14	1. CONTROL OF PLANE IN INIT. ROLL	.00	1.00	2.00	1.00	1.00	1.00	1.00	1.167	.373							
15	2. CONTROL OF PLANE IN INIT. ROLL	.00	3.00	2.00	1.00	2.00	2.00	2.00	2.000	.577							
76	AVER. AND STD. DEV. OF SUBTASKS(EX 1,2,..)	.0	.0	2.0	1.0	2.0	.0	1.0	.0	1.5	.5	1.5	.5	1.5	.5	1.6	.64

COMMENTS

13 EXCELLENT AERODYNAMICALLY, CONFUSING FOR PILOT SINCE HE ALWAYS PULLS
 14 RELEASE FOR HOOKUP.
 15 GOOD
 16 REQUIREMENT TO START T.O. WITH FLAP UP, THEN PUT NEUTRAL IS
 17 UNDERSTANDABLE. SOME TENDENCY TO DROP WING AT START OF ROLL
 18 WHEN SERIOUS DEFICIENCY I NOTE IS THE SUDDEN BLOW TO THE TAILWHEEL
 19 WHEN THE TAILWHEEL BECOMES TAUT
 20 THERE IS ADEQUATE CONTROL DURING T.O. TO MAINTAIN WINGS LEVEL EVEN
 21 IN CROSSWINDS OF AT LEAST 10KTS.
 22 IS ABOUT TWICE THE AFT BREAKOUT FORCE, WHEN THE STICK IS MOVED AFT
 23 TO FWD, THE FWD BREAKOUT FORCE IS RELATIVELY SO HEAVY THAT IT FEELS
 24 AS IF A STOP HAS BEEN ENCOUNTERED. THIS UNBALANCED BREAKOUT FORCE
 25 CAUSED ME TO OVERCONTROL IN PITCHDOWN ON ONE TAKEOFF. IT HAS BEEN
 26 SUGGESTED (PILOT 4) THAT WITH LONG, TRIM CONTROL ALMOST FULL FWD.
 27 (AS REQD ON T.O.), BREAKOUT FORCES ARE UNEVEN FORE AND AFT AS AN
 28 INHERENT CHARACTERISTIC OF THE FEEL SPRING MECHANISM.

***** ZEROS INDICATE NO RATING BY PILOT *****

SAILPLANE 5 DATA

TASK	DESCRIPTION OF TASKS	1	2	PILOT 3			4	5	6	7	AVER.	STD DEV				
12	II. SMOOTH AIR MANEUVERING	2.00	5.00	2.00	.00	.00	.00	2.00	4.00	3.000	1.265					
13	A. PILOT OPIN OF INITIAL TAKEOFF RLL	2.00	4.00	2.00	.00	.00	.00	5.00	3.00	3.200	1.166					
14	1. TOWLINE HOOKUP	3.00	2.00	1.00	.00	.00	.00	4.00	2.00	2.400	1.020					
15	2. CONTROL OF PLANE IN INIT. ROLL	2.00	4.00	3.00	.00	.00	.00	5.00	2.00	3.200	1.166					
76	AVER. AND STD. DEV. OF SUBTASKS(EX 1,2,*)	2.5	.5	3.0	1.0	2.0	1.0	.0	.0	.0	4.5	.5	2.0	.0	2.8	1.17

COMMENTS

RUDDER INEFFECTIVE, FLAP/AILERON MOVEMENT NECESSARY TO CONTROL WING LEVELATION
 POOR LOCATION TOO FAR FROM PILOT'S SHOULDER. TOW HOOK TOO FAR AFT
 TOW RELEASE TOO FAR FROM PILOT'S SHOULDER. TOW HOOK TOO FAR AFT
 CAUSING DIRECTORIAL CONTROL LIMITED
 VISIBILITY DIRECTORIAL CONTROL LIMITED
 AILERON WEAR. RUDDER IMPROVE WHEEL LOCKING CAPABILITY
 THE USE OF DUAL FLIGHT CONTROLS UNDER CROSSWIND CONDITIONS AN UNDESIRABLE
 PRACTICE. THE USE OF DUAL FLIGHT CONTROLS UNDER LONG TERM CONTROL
 PROBABLY CAUSES THE STICK TO BOUNCE FORE AND AFT WHILE ROLLING OVER
 BUT NOT NEARLY ENOUGH TO BOUNCE FORE AND AFT WHILE ROLLING OVER
 NO PROBLEMS ON TAKEOFF (STEARMAN TOW)
 SLIGHT BOUNCE ON TAKEOFF WHICH COULD BE
 ATTRIBUTED TO WING FLAPPING. PROBABLY IT WAS NOT OFF ERROR IN ANY
 AILERON OR FLAP POSITION. THE PLANE SHOULD BE FOLLOWED HIGHER THAN WITH
 OTHER SAILPLANES
 CROSSWINDS A MAJOR PROBLEM. MAX VECTOR PROBABLY ABOUT 15KNOTS.
 NO PROBLEMS ON TAKEOFF (STEARMAN TOW)

SAILPLANE 6 DATA

TASK	DESCRIPTION OF TASKS	1	2	PILOT 3			4	5	6	7	AVER.	STD DEV					
12	II. SMOOTH AIR MANEUVERING	.00	1.00	1.00	.00	.00	.00	2.00	1.00	1.250	.433						
13	A. PILOT OPIN OF INITIAL TAKEOFF RLL	.00	4.00	2.00	.00	.00	.00	3.00	2.00	1.800	.788						
14	1. TOWLINE HOOKUP	.00	4.00	2.00	1.00	1.00	1.00	2.00	1.00	2.000	1.000						
15	2. CONTROL OF PLANE IN INIT. ROLL	.00	1.00	1.00	.00	.00	.00	2.00	2.00	1.833	1.067						
76	AVER. AND STD. DEV. OF SUBTASKS(EX 1,2,*)	.0	.0	2.5	1.5	1.5	.5	1.0	.0	2.0	.0	3.0	1.0	1.5	.5	1.9	1.04

COMMENTS

FWD STICK ARM OUTSTRETCHED WHEN PILOT OVERCONTROLS PITCH EVER
 FWD STICK THEN NOSE STRIKES HITS WHEN PILOT OVERCONTROLS PITCH EVER
 EXCELLENT
 EXCELLENT
 EXCELLENT CONTROL DURING INITIAL ROLL AND LIFTOFF
 VERY GOOD CONTROL IN ALL AXES FOR TAKEOFF-ADEQUATE AUTHORITY AND
 RESPONSE.

SAILPLANE 1 DATA

TASK	DESCRIPTION OF TASKS	1	2	PILOT 3	4	5	6	7	AVER.	STD DEV							
16	B. PILOT OPTION OF TOW	1.50	1.00	2.00	.00	.00	1.00	.00	1.375	.415							
17	EASE OF MAINTAINING POSITION	1.00	1.00	1.00	2.00	3.00	1.00	1.00	1.429	.728							
18	AIRCRAFT TRIM	2.00	5.00	1.00	4.00	3.00	4.00	4.00	1.500	1.336							
19	CONTROL IN PROPWASH	1.00	1.00	1.00	2.00	3.00	1.00	1.00	1.429	.728							
20	RELEASE CHARACTERISTICS	1.00	1.00	2.00	1.00	2.00	1.00	2.00	1.500	.500							
77	AVER. AND STD. DEV. OF SUBTASKS(EX 1,2,...)	1.3	.4	2.3	1.3	1.3	.4	2.2	1.3	3.1	.9	1.7	1.3	2.0	1.2	2.0	1.27

COMMENTS

INSUFFICIENT ELEVATOR TRIM. REQUIRES ABOUT 13N CONSTANT PUSH FORCE
 HEAD DOES NOT HUNT. EXCELLENT FOLLOWING OF TOMPLANE.
 TOO MUCH FORWARD STICK TO MAINTAIN POSITION.
 INEFFECTIVE--UNSATISFACTORY
 POOR. NONEXISTENT
 MAX TRIM SPEED 45-50KTS, HOWEVER FORCES ARE LIGHT THROUGH SPEED RANGE
 EXCELLENT RESPONSIVE--WELL DAMPED--LIGHT CONTROL FORCES
 EXTREMELY RESPONSIVE--WELL DAMPED--LIGHT CONTROL FORCES
 GOOD HARMONY--OUTSTANDING
 GLIDER CANNOT BE TRIMMED ON TOW. WOULD BE TIRESOME AS A CROSS-COUNTRY
 TOW
 CONSTANT FORWARD FORCE ON STICK
 TRIM-REQUIRED 13-18N FWD FORCE IN TOW. CONTROL VERY GOOD IN TOW.
 BOXING SAILPLANE IS SIMPLE TASK, WINGS LEVEL(ADEQUATE RUDDER CONTROL)

SAILPLANE 2 DATA

TASK	DESCRIPTION OF TASKS	1	2	PILOT 3	4	5	6	7	AVER.	STD DEV							
16	B. PILOT OPTION OF TOW	1.00	2.00	3.00	.00	.00	2.00	3.00	2.200	.748							
17	EASE OF MAINTAINING POSITION	1.00	2.00	3.00	3.00	3.00	2.00	3.00	2.286	.700							
18	AIRCRAFT TRIM	1.00	3.00	3.00	3.00	3.00	3.00	2.00	2.571	.639							
19	CONTROL IN PROPWASH	1.00	2.00	3.00	2.00	3.00	2.00	2.00	2.143	.639							
20	RELEASE CHARACTERISTICS	1.00	.00	2.00	1.00	2.00	2.00	2.00	1.667	.471							
77	AVER. AND STD. DEV. OF SUBTASKS(EX 1,2,...)	1.0	.0	2.3	.5	2.5	.5	2.2	.4	2.7	.4	2.2	.4	2.2	.4	2.2	.72

COMMENTS

INSUFFICIENT RUDDER TO BOX TOMPLANE
 EFFICIENT BUT HARD TO OPERATE
 FRICTION FORCE IS SUFFICIENT
 SUFFICIENT TRIM AVAILABLE HOWEVER EACH DETENT RESULTED IN AT LEAST
 4KT INCREMENTS
 DIRECTIONAL-COULD NOT BOX TOW VERY WELL
 FAIRLY LARGE ALLERON DEPLECTIONS ARE REQUIRED.
 ALWAYS NEED PUSH FORCES ON STICK
 ALWAYS QUIET
 TOUCHY IN DIRECTIONAL
 SOME CONTROL REQUIRED FOR DIRECTIONAL-LATERAL CONTROL
 HANDLES EXCELLENTLY. EASILY UPSET BY DRAUGHTS BUT EASILY RESTORED
 BY CONTROLLING LIGHT RUDDER FORCES. GEAR RETRACTION FORCES ARE HEAVY,
 PLEASEASPORTABLE. SLACK OVER FOOT WHEN COYING BACK TO CENTER
 LINE ON STICK. CURVED COYING BACK TO CENTER LINE IN THE
 RUDER CONTROL. UNPLEASANT STICK FORCE EXCESSIVE FRICTION. POOR
 VISIBILITY
 WOULD BE TO FLY IN ROUGH AIR. HAD TO WORK TO RETURN TO CORRECT
 POSITION
 NON-STANDARD STICK TOO FAR FORWARD RESULTING IN TROUBLE HOLDING
 NOSE DOWN AT HIGH TOW SPEEDS.
 ADEQUATE RUDDER CONTROL TO BOX TOMPLANE WITH WINGS LEVEL. SMALL BUT
 FREQUENT STICK AND RUDDER INPUTS REQUIRED IN NORMAL TOW.

***** ZEROS INDICATE NO RATING BY PILOT *****

SAILPLANE 1 DATA

TASK	DESCRIPTION OF TASKS	1	2	PILOT 3	4	5	6	7	AVER.	STD DEV			
21	C. PILOT OPINION OF LONG HANGLING	2.00	1.00	1.00	3.00	3.00	1.00	.00	1.250	.433			
22	EASE OF INLET & MAIN CONTROL AIRSPEED	3.00	1.00	1.00	3.00	3.00	1.00	.00	1.571	.904			
23	PLANCH RELATIVE SPEED RANGE	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.571	.633			
24	STICK FORCE GRADIENT	1.00	1.00	2.00	1.00	2.00	2.00	2.00	1.571	.495			
25	STICK FORCE STABILITY	1.00	1.00	1.00	1.00	1.00	1.00	.00	1.250	.473			
26	STICK FORCE TRIM	1.00	1.00	1.00	1.00	1.00	1.00	.00	1.250	.682			
27	RECOVERY CHARACTERISTICS	1.00	1.00	1.00	1.00	1.00	1.00	2.00	1.250	.492			
28	MANEUVERING RESPONSE	1.00	1.00	1.00	1.00	1.00	1.00	2.00	1.604	.452			
29	RECOVERY	1.00	2.00	2.00	1.00	2.00	2.00	2.00	1.604	.452			
30	DIVE RECOVERY	1.00	2.00	2.00	1.00	2.00	2.00	2.00	1.604	.452			
78	AVER. AND STD. DEV. OF SUBTASKS (EX 1,2,..)	1.5	.8	1.6	1.3	1.6	.7	1.6	1.0	2.1	.8	1.7	.96

COMMENTS

78 AVER. AND STD. DEV. OF SUBTASKS (EX 1,2,..) 1.5 .8 1.6 1.3 1.6 .7 1.6 1.0 2.1 .8 1.7 .96

4: EASY TO OBTAIN, BUT HAD TO HOLD A FORCE AT SPEEDS ABOVE 48KTS.
 5: VERY EASY TASK
 6: TRIMMER UNSATISFACTORY
 7: NOT NEEDED
 8: MAX TRIM SPEED 48KTS.
 9: COULD ONLY TRIM TO 61 IAS
 10: INSUFFICIENT NOSE DOWN TRIM FOR MAX AIRSPEED
 11: STICK FORCE STABLE WITH FULL FWD TRIM AT 55KTS-NEEDS FULL TRIM CAP.
 12: EXCELLENT
 13: NO PROBLEMS AT ALL IN OVER EGL OR UNDESIRABLE RESPONSE
 14: EXCELLENT BUT GOOD-RARELY BOTHER TRIMMING WHILE SOARING
 15: VERY GOOD
 16: TRIMMER INOPERATIVE
 17: VERY GOOD
 18: THINGS TO ME IS EVIDENCED BY STICK FORCE GRADIENT
 19: TRIMMER INOPERATIVE BUT PROBABLY WOULD RETURN TO TRIM
 20: MAXIMUM OF TRIM
 21: EXCELLENT
 22: NEUTRALLY STABLE AT 52KTS
 23: NEUTRAL
 24: A LITTLE TOO LIGHT STABILITY CAUSES G TO BUILDUP DURING DIVE ACCEL.
 25: STICK FORCE REQUIRED
 26: MODERATE IN TURNING FLIGHT AT 52KTS POSITIVE AND OK
 27: STABILITY IN TURNING FLIGHT DIVE RECOVERY LEADS TO EASE OF OVER G
 28: EXCELLENT LONGITUDINAL STABILITY, VERY PERCEPTIBLE STICK TRAVEL AND
 29: FORCE REQUIRED FOR SPEED CHANGE. NON LINEAR RESPONSE DURING PRECISE
 30: ATTITUDE CHANGE (SLOWER RESPONSE TO PUSH THAN TO PULL).
 31: STICK FORCE PERWARD EXCELLENT
 32: STICK VERY FORWARD
 33: SWITCH-ROLL CONTROL AND RESPONSE HARMONY IS VERY GOOD

***** ZEROS INDICATE NO RATING BY PILOT *****

SAILPLANE 4 DATA

TASK	DESCRIPTION OF TASKS	1	2	PILOT 3	4	5	6	7	AVER.	STD DEV
21	C. PILOT OPTN OF LONG. HANDLING	.00	2.00	4.00	3.00	3.00	4.00	3.00	3.200	.748
22	BASE OF EST & MAX. CONTROL SPEED	.00	2.00	2.00	3.00	3.00	3.00	3.00	2.937	.471
23	PITCH STIFFNESS	.00	2.00	2.00	3.00	3.00	3.00	3.00	2.937	.471
24	PITCH SENSITIVITY	.00	2.00	2.00	3.00	3.00	3.00	3.00	2.937	.471
25	PITCH FORCE GRADIENT	.00	2.00	2.00	3.00	3.00	3.00	3.00	2.937	.471
26	STICK FORCE STABILITY	.00	2.00	2.00	3.00	3.00	3.00	3.00	2.937	.471
27	STICK FREE TRIM	.00	2.00	2.00	3.00	3.00	3.00	3.00	2.937	.471
28	RETURN TO TRIM	.00	2.00	2.00	3.00	3.00	3.00	3.00	2.937	.471
29	MANEUVERING RESPNSE	.00	2.00	2.00	3.00	3.00	3.00	3.00	2.937	.471
30	MANEUVERING CHARACTERISTICS	.00	2.00	2.00	3.00	3.00	3.00	3.00	2.937	.471
31	DIVE RECOVERY	.00	2.00	2.00	3.00	3.00	3.00	3.00	2.937	.471
78	AVER. AND STD. DEV. OF SUBTASKS(EX 1,2,..)	.0	2.1	3.2	3.6	3.2	3.9	2.2	2.6	.87

COMMENTS

PILOT

3 OCCASIONAL OVERSHOOT IS EXPERIENCED WHEN CHANGES ARE ATTEMPTED
 4 AS EASY TO OBTAIN, HOWEVER, IT IS DIFFICULT TO ACTUATE TRIM LEVER
 4 FOR MAINTAINING IAS
 4 HARD TO ADJUST PRECISELY
 4 ABLE TO TRIM THROUGHOUT REGD TRIM RANGE
 4 VERY GOOD
 4 VERY SENSITIVE
 4 FOUND CENTERING SPRING ANNOYING AGAINST SPRINGS, THIS
 4 FORCE GRADIENT IS THE RESULT OF WORKING AGAINST SPRINGS, EXCEPT
 4 RESULTS IN FORCES AS HIGH AS 18-22N, DURING ALL MANEUVERS, EXCEPT
 4 T.O., LANDING, AND STICK FORCE/LGL. VERY LIGHT FORCES WOULD BE
 4 MORE DESIRABLE.
 4 LIGHT BUT OK
 4 NONLINEARITY OBSERVED GOING BACK FROM 57 TO 52 OK. STARTING FROM
 3 48 OSCILLATION BEGAN, SAME AS STICK FIXED
 3 POSITIVE STICK FORCE/V GRADIENT
 3 DID NOT DO
 3 GOOD
 3 VERY PLEASANT IF SAME TRIM SPEED IS DESIRED AT END OF MANEUVER
 3 POSITIVE FORCE GRADIENT WITH LGL.
 3 OK
 3 NEUTRAL--APPROX. 16SEC PERIOD
 3 NEAR 48IAS 20 SEC PERIOD MODERATELY DAMPED
 3 LIGHT BUT NO SURPRISES
 3 GOOD NO PROBLEM
 3 POSITIVE FORCE GRADIENT WITH LGL
 3 GIVES IMPRESSION OF LIGHT STABILITY WITH STIFF, INSENSITIVE STICK.
 3 QUICK, LIGHT BUT CONSISTENT. PLEASANT TO FLY
 3 WHEN RETURNING FROM OFF TRIM CONDITION, PHUGOID OSCILLATION WAS
 3 EXCITED IN 2 OF 3 CASES.
 3 STICK FORCE PER LGL TOO LIGHT. STICK FORCE PER DISPLACEMENT MAY BE
 3 OK. STICK FORCE GRADIENT IN BOTH LGL AND MANEUVERING FLIGHT, CONSISTS
 3 HIGH STICK FORCE GRADIENT IN BOTH LGL AND CONTROL ACTIVITY. CONSISTS
 3 OF SMALL FLIGHT, MUCH OF THE REQUIRED PITCH CENTERING SPRING DETENT. RESPONSE
 3 IN FREE FLIGHT, AROUND THE STRONG CENTERING SPRING DETENT. RESPONSE
 3 THE PILOT IS DEPRIVED OF TRUE ANTI-CAPTIVITY FEEL FOR AIRPLANE. THIS IS A
 3 SERIOUS DEFICIENCY. BUT THERE ARE SOME REASONS FOR THIS. IT DOES NOT
 3 DEPEND ONLY ON THE AIRPLANE CONTROL. THE POSSIBLE EXPLANATION OF THIS
 3 SERIOUSLY AFFECTS PILOT WORKLOAD IN ITERATING SMALL
 3 PITCH INPUTS AND IS IRRITATING.

***** ZEROS INDICATE NO RATING BY PILOT *****

SAILPLANE 6 DATA

TASK	DESCRIPTION OF TASKS	1	2	PILOT 3	4	5	6	7	AVER.	STD DEV					
21	C. PILOT OPTN OF LONG. HANDLING	.00	.00	2.00	.00	.00	4.00	2.00	2.667	.943					
22	1. USE OF TRIM TO MAINTAIN COPIES SPEED	.00	1.00	2.00	.00	.00	3.00	2.00	2.000	.577					
23	2. STICK RELIABILITY	.00	1.00	3.00	.00	.00	4.00	2.00	2.667	1.020					
24	3. STICK SMOOTH GRADIENT	.00	1.00	4.00	.00	.00	4.00	2.00	2.333	1.247					
25	4. STICK LEVEL STABILITY	.00	1.00	3.00	.00	.00	2.00	2.00	2.000	.400					
26	5. RETURN TO TRIM	.00	2.00	3.00	.00	.00	3.00	2.00	1.800	.748					
27	6. MANEUVERING CHARACTERISTICS	.00	2.00	2.00	.00	.00	2.00	2.00	2.000	.577					
28	7. PHUGO RECOVERY	.00	2.00	2.00	.00	.00	2.00	2.00	2.000	.000					
30	10. DIVE RECOVERY	.00	2.00	2.00	.00	.00	2.00	2.00	2.000	.000					
70	AVER. AND STD. DEV. OF SUBTASKS (EX 1,2,..)	.0	.0	1.4	.5	2.4	.8	2.0	.5	2.7	.8	1.7	.5	2.1	.73

COMMENTS

VERY EASY WITHIN TRIM RANGE. STICK FORCES ARE ON HEAVY SIDE.

POWERFUL AND POSITIVE
 MAX TRIM AROUND 74IAS
 NO TRIM BEYOND 70

GOOD, BUT GOOD FOR TRAINER
 HXCESSIVE

FOR AIRSPEED TOO POWERFUL
 HIGH, BUT GOOD FOR TRAINER

QUITE STABLE
 APPEARS TO BE POSITIVE

EXCESSIVE, HEAVY FORCES ARE REQUIRED TO CHANGE AIRSPEED

POSITIVE
 QUALITATIVELY GOOD

GOOD FREE RETURN
 +2-3 KTS

TOO STRONG A TENDENCY
 VTRIM 52IAS LOW 50 HIGH 54, VTRIM 65IAS LOW 58 HIGH 79

SOMEWHAT SLOW
 POSITIVE STICK FORCE/EGC

LIGHTLY DAMPED
 UNSTABLE PHUGOID AT 60KTS

NEUTRAL
 VTRIM 52IAS 22SEC PERIOD, VTRIM 65IAS 26 SEC PERIOD

GOOD ON ELEVATOR
 BUT ONLY GRADIENTS ARE LITTLE TOO HEAVY. SOME BUZZING WELL INTO

STICKING AT LOW RANGE. SMOOTHNESS IN
 EXCELLENT CONTROL CHARACTERISTICS FOR TRAINING MISSION

***** ZEROS INDICATE NO RATING BY PILOT *****

SAILPLANE 1 DATA

TASK	DESCRIPTION OF TASKS	1	2	3	4	5	6	7	AVER.	STD DEV							
32	D. PILOT OPINION OF LATERAL HANDLING	1.00	1.00	1.00	.00	.00	.00	.00	1.000	.000							
33	1. AILERON FORCE GRADIENT	1.00	1.00	1.00	2.00	2.00	2.00	1.00	1.429	.495							
34	2. ROLL RATE OVER SPEED RANGE	1.00	1.00	2.00	3.00	3.00	3.00	1.00	2.000	.495							
35	3. ROLL RATE OVER SPEED RANGE	1.00	1.00	2.00	2.00	2.00	3.00	2.00	2.000	.756							
36	4. SIDESLIP CHARACTERISTICS	1.00	1.00	2.00	2.00	2.00	2.00	2.00	2.286	.452							
37	5. EASE OF TURN ENTRY	1.00	1.00	2.00	2.00	2.00	2.00	2.00	2.000	.577							
38	6. YAW DUE TO ROLL	2.00	3.00	3.00	1.00	2.00	2.00	2.00	2.000	.632							
39	7. YAW DUE TO ROLL	2.00	3.00	3.00	1.00	2.00	2.00	2.00	2.000	.728							
40	8. EASE OF MAIN. 0.785RAD BANK TURN	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.429	.728							
41	9. EASE OF MAIN. 1.047RAD BANK TURN	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.571	.728							
79	AVER. AND STD. DEV. OF SUBTASKS(EX 1:2...)	1.3	.5	1.2	.6	1.4	.5	1.7	.7	2.2	.4	1.9	.8	2.0	.8	1.7	.72

COMMENTS

TASK	PILOT	COMMENTS
32	3	VERY PLEASANT CONTROL HARMONY VERY GOOD OCCASIONALLY TOO LIGHT
33	3	EXCELLENT
34	3	ABOVE 209 TO .262 RAD./SEC AT SPEEDS CHECKED
35	3	.384RAD/SEC AT 39 IAS, .463RAD/SEC AT 57IAS
36	3	RUDDER FORCE REVERSED, BUT GOOD OTHERWISE APPROX .262RAD BANK REQD FOR MAX RUDDER DEFLECTION FOR CONSTANT HEADI
37	3	POSITIVE STABILITY HOWEVER A/S BLANKS OUT WITH YAW RUDDER LOCKS
38	3	STEADY HEADING SIDESLIP--RUDDER FORCE GRADIENT LIGHTENS AFTERR ABOUT 1/2 TURN--LIGHTLY POSITIVE DIHEDRAL EFFECT
39	3	PITCH UP--EASY RUDDER REQUIRED FOR INITIAL ROLL, SLIGHTLY MORE FOR LATER VERY EASY TO NOTICEABLE, BUT STILL IT IS POSSIBLE TO MAKE A GOOD TURN WITH AILERONS ONLY
40	3	VERY EASY TO MAINTAIN COORDINATED CONTROL
41	3	ABOUT .262RAD RUDDER FIXED
42	3	CAN PICK UP LOW WING WITH RUDDER-- .262RAD ROLL IN 5 SEC WITH FULL RUDDER AT 39IAS
43	3	ONE OF THE BEST
44	3	GOOD--SLIGHT AMOUNT OF TOP STICK REQUIRED
45	3	EXCELLENT
46	3	SAME AS D.8
47	3	VERY LIGHT AND RESPONSIVE
48	3	SUPERIOR COORDINATION IN MANEUVERING FLIGHT
49	3	EXCELLENT FOR THERMALING
79	3	SPIRAL STABILITY NEUTRAL--VERY GOOD--PITCH ROLL CONTROL AND RESPONSE HARMONY IS VERY GOOD

***** ZEROS INDICATE NO RATING BY PILOT *****

SAILPLANE 2 DATA

TASK	DESCRIPTION OF TASKS	1	2	PILOT 3	4	5	6	7	AVER.	STD DEV									
32	D. PILOT OPINION OF LATERAL HANDLING	2.00	2.00	3.00	4.00	4.00	4.00	4.00	2.800	.748									
33	1. AILERON FORCE GRADIENT	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.143	.639									
34	2. AILERON FORCE GRADIENT RANGE	2.00	2.00	2.00	2.00	2.00	2.00	2.00	1.857	.639									
35	3. ROLL RATE CHARACTERISTICS	3.00	3.00	3.00	3.00	3.00	3.00	3.00	2.143	.748									
36	4. ROLL RATE TO TURN AILERON	2.00	2.00	2.00	2.00	2.00	2.00	2.00	2.857	.748									
37	5. YAW DUE TO ROLL	2.00	2.00	2.00	2.00	2.00	2.00	2.00	2.714	.490									
38	6. YAW DUE TO ROLL	1.00	1.00	1.00	1.00	1.00	1.00	1.00	2.429	.639									
39	7. YAW DUE TO ROLL	2.00	2.00	2.00	2.00	2.00	2.00	2.00	2.143	.748									
40	8. EASE OF MAIN. 1.0475RAD BANK TURN	2.00	2.00	2.00	2.00	2.00	2.00	2.00	2.143	.748									
41	9. EASE OF MAIN. 1.0475RAD BANK TURN	2.00	2.00	2.00	2.00	2.00	2.00	2.00	2.143	.748									
79	AVER. AND STD. DEV. OF SUBTASKS(EX 1,2,..)	1.9	.7	2.1	.3	2.1	.6	2.5	.9	2.8	.6	2.1	.8	3.0	.8	2.4	.8	2.4	.8

TASK PILOT

COMMENTS

32 CONTROL HARMONY NOT GOOD--FOR LONG PERIODS OF TURNING FLT. IT
 33 BECAME OBVIOUS THAT AILERON FORCES ARE TOO HEAVY. IT
 34 JUST PLEASES AN
 35 RUDDER NOT EFFECTIVE ENOUGH AT LOW SPEEDS WHEN EXECUTING RAPIDLY
 36 APPROX 3.5 SEC AT THERMALLING SPEEDS
 37 ABOUT 349RAD/SEC AVERAGE
 38 ABOUT 78IAS .489RAD/SEC, VTRIM 52IAS .384RAD/SEC
 39 NOT CHECKED
 40 VERY LITTLE BANK REQUIRED FOR MAXIMUM RUDDER DEFLECTION FOR CONSTANT
 41 HEADING FLT.
 42 RUDDER OVERBALANCES BUT NO PROBLEM.
 43 VTRIM 48 DEFLETS, SPIRAL STABILITY SLIGHTLY NEGATIVE. MODERATE
 44 PITCHUP--UNUSUAL; RUDDER OVER BALANCE ABOUT 1/2 DEFLECTION
 45 RUDDER INSUFFICIENT BUT EVEN SO, THE TURN ENTRY WAS GOOD
 46 NOT TOO EASY
 47 HAVE TO WORK AT RUDDER TO COORDINATE
 48 VERY DIFFICULT TO KEEP YAW STRING CENTERED
 49 RUDDER KEEP WORKING TO CENTER OF YAW STRING
 50 CAN BE DOWN HANDS OFF
 51 FAIRLY DIFFICULT AT LOWER SPEEDS
 52 NO LEAS TO COORDINATE
 53 WORKS OK WITH WALK
 54 FAIRLY OK WITH WALK
 55 NO LEAS TO COORDINATE
 56 NO LEAS TO COORDINATE
 57 2.54 WOULD BE BETTER WITH MORE EFFECTIVE RUDDER
 58 TURN COORDINATION. AT LOWER SPEEDS THERE MUST BE SOME SEPARATION
 59 ON THE STICKATOR ROLLING OCCILLATION IS ALSO EMBARRASSED DURING LOW
 60 SPEED STRAHLING PLANE 2. RUDDER DEFLECTION IS ACCOMPANIED BY CHANGED
 61 CHARACTERISTICS
 62 STRAHLING PLANE POSITIVE, HOWEVER, EXPERIENCED RUDDER LOCK BOTH
 63 DIRECTION. ALSO LOSE A75 WITH ABOUT 172 RUDER DEFLECTION.
 64 GIVES GOOD CONTROL FOR SMALL TURNS.
 65 NOT ENOUGH RUDDER TO COORDINATE INITIAL MODERATE RATE TURN ENTRY.
 66 STRONG PITCHUP WITH SIDESLIP VERY UNDESIRABLE

***** ZEROS INDICATE NO RATING BY PILOT *****

SAILPLANE 3 DATA

TASK	DESCRIPTION OF TASKS	1	2	3	4	5	6	7	AVER.	STD DEV
D.	PILOT OPTION OF LATERAL HANDLING	1.50	2.00	2.50	3.00	3.00	3.00	3.00	2.200	.510
33	1. AILERON FORCE GRADIENT	1.00	2.00	2.50	3.00	3.00	3.00	3.00	1.857	.639
34	2. RUDDER FORCE GRADIENT	1.00	2.00	2.00	2.00	2.00	2.00	2.00	1.857	.639
35	3. ROLLER OVER RANGE	1.00	2.00	2.00	2.00	2.00	2.00	2.00	1.857	.639
36	4. STICK SLIP CHARACTERISTICS	1.00	2.00	2.00	2.00	2.00	2.00	2.00	1.857	.639
37	5. STICK ENTRY	1.00	2.00	2.00	2.00	2.00	2.00	2.00	1.857	.639
38	6. YAW DUE TO ROLL	1.00	2.00	2.00	2.00	2.00	2.00	2.00	1.857	.639
39	7. YAW DUE TO ROLL	1.00	2.00	2.00	2.00	2.00	2.00	2.00	1.857	.639
40	8. EASE OF MAIN. 0.785RAD BANK TURN	1.00	2.00	1.50	2.00	2.00	2.00	2.00	1.643	.693
41	9. EASE OF MAIN. 1.047RAD BANK TURN	2.00	2.00	1.50	2.00	2.00	1.00	2.00	1.643	.693
79	AVER. AND STD. DEV. OF SUBTASKS(EX 1,2,..)	1.3	.5 2.1	.6 2.0	.4 1.4	.7 2.8	.6 2.0	.7 2.8	.6 2.1	.81

COMMENTS

TASK PILOT

33 FLEXIBLE WING ON SAILPLANE 5 MAKES IT WORSE
 34 FLIGHT, MAYBE TOO MUCH SO.
 35 AILERON ELEVATOR FORCE HARMONY-EXCELLENT
 36 TOOK ATTENTION EFFORT TO COORDINATE
 37 NO VARIATION OBSERVED, ADEQUATE THROUGHOUT.
 38 ABOUT 34.6RAD/SEC AT SPEEDS CHECKED.
 39 AT 48KTS. 38.4RAD/SEC, 80KTS. 52.4RAD/SEC
 40 PLEASANT, WEAK. PITCHES NOSE DOWN MODERATELY
 41 RUDDER WINGS ARE LEVELLED. RUDDER RETURNS TO NEUTRAL
 42 POSITIVE AT 60 KTS, FULL RUDDER DEFLECTION WILL RESULT IN RUDDER
 43 LOCK, ALSO A LOSS OF AIRSPEED.
 44 RUDDER FORCE LIGHTENED BUT NEVER ZERO OR REVERSED.
 45 BUZZY OVERBALANCE IN RUDDER IN BOTH DIRECTIONS, PITCH DOWN WITH SLIP
 46 LESS RUDER REQUIRED YAW
 47 AVERAGE ADVERSE YAW
 48 TAKES ATTENTION TO RUDDER
 49 SEEMS PRONOUNCED. HAVE TO MODULATE RUDDER TO COORDINATE.
 50 NO DIDER PROBLEM
 51 NO DIDER PROBLEM
 52 NO DIDER PROBLEM
 53 NO DIDER PROBLEM
 54 NO DIDER PROBLEM
 55 NO DIDER PROBLEM
 56 NO DIDER PROBLEM
 57 NO DIDER PROBLEM
 58 NO DIDER PROBLEM
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 70 NO DIDER PROBLEM
 71 NO DIDER PROBLEM
 72 NO DIDER PROBLEM
 73 NO DIDER PROBLEM
 74 NO DIDER PROBLEM
 75 NO DIDER PROBLEM
 76 NO DIDER PROBLEM
 77 NO DIDER PROBLEM
 78 NO DIDER PROBLEM
 79 NO DIDER PROBLEM

ABOVE 26 TURNS WILL SELF
 OPEN SIDELIPS ARE NOT
 OBJECTIONABLE.
 BUT FALLS SHORT OF SAILPLANE 1 OR 5. SPD 130
 VERY EFFECTIVE BELOW STALL

***** ZEROS INDICATE NO RATING BY PILOT *****

SAILPLANE 4 DATA

TASK	DESCRIPTION OF TASKS	1	2	PILOT 3	4	5	6	7	AVER.	STD DEV					
32	D. PILOT OPINION OF LATERAL HANDLING	.00	2.00	2.00	.00	2.00	2.00	3.00	2.200	.400					
33	1. AILERON FORCE GRADIENT	.00	2.00	2.00	2.00	2.00	2.00	3.00	2.167	.373					
34	2. RUDDER FORCE GRADIENT	.00	2.00	2.00	2.00	2.00	2.00	3.00	2.167	.373					
35	3. ROLL RATE OVER SPEED RANGE	.00	2.00	2.00	2.00	2.00	2.00	3.00	2.167	.419					
36	4. SLIP CHARACTERISTICS	.00	2.00	2.00	2.00	2.00	2.00	3.00	2.167	.498					
37	5. EASE OF TURN ENTRY	.00	2.00	2.00	1.00	2.00	2.00	3.00	2.167	.577					
38	6. YAW DUE TO ROLL	.00	1.00	2.00	2.00	2.00	2.00	3.00	2.000	.500					
39	7. EASE OF MAIN. 0.785RAD BANK TURN	.00	2.00	2.00	1.00	2.00	2.00	3.00	2.250	.829					
40	8. EASE OF MAIN. 1.047RAD BANK TURN	.00	2.00	2.00	1.00	2.00	2.00	3.00	2.250	1.000					
41	9. EASE OF MAIN. 1.047RAD BANK TURN	.00	2.00	2.00	1.00	2.00	2.00	4.00	2.000	1.000					
79	AVER. AND STD. DEV. OF SUBTASKS(EX 1,2,...)	.0	.0	1.9	.3	2.1	.2	1.5	.7	2.2	.4	3.1	.6	2.2	.76

COMMENTS

PLEASANT
 ABOUT 3.5 SEC
 SLOWER WITH FLAPS DOWN
 ROLL RATE IS ADEQUATE BUT NOT AS GOOD AS THE OTHER HIGH PERFORMANCE
 SAILPLANES
 ABOUT 2.49RAD/SEC
 AT 0 FLAP 52IAS, 55SEC AT .209RAD FLAP AT 39IAS.
 4 VTIME 48IAS .105RAD FLAP .384RAD/SEC.
 SEEMED TO TUCK IN PITCH IN RIGHT FWD SLIP
 RUFFICIENT DOWN RUDDER TO BALANCE AILERON CONTROL
 WING ROCKS AT BUFFER ONSET. GOOD
 BECAUSE OF STICK BACK PRESSURE WORKING AGAINST CENTERING SPRING
 IN LATERAL MANEUVERS. SOME LATERAL MANEUVERS ARE MILDLY OBJECTIONABLE
 IN STRONGLY POSITIVE DIHEDRAL EFFECT. CONSIDERABLE TOP AILERON
 REQD IN TURNS.

***** ZEROS INDICATE NO RATING BY PILOT *****

SAILPLANE 6 DATA

TASK	DESCRIPTION OF TASKS	1	2	3	4	5	6	7	AVER.	STD DEV
32	D. PILOT OPINION OF LATERAL HANDLING	.00	.00	2.00	.00	.00	2.00	2.00	2.000	.000
33	1. RUDDER FORCE GRADIENT	.00	2.00	2.00	2.00	2.00	2.00	2.00	2.000	.000
34	2. RUDDER RATE GRADIENT	.00	2.00	2.00	2.00	2.00	2.00	2.00	2.000	.000
35	3. ROLL RATE OVER SPEED RANGE	.00	2.00	2.00	2.00	2.00	2.00	2.00	2.000	.000
36	4. SIDESLIP CHARACTERISTICS	.00	2.00	2.00	2.00	2.00	2.00	2.00	2.000	.000
37	5. EASE TO TURN	.00	2.00	2.00	2.00	2.00	2.00	2.00	2.000	.000
38	6. YAW DUE TO ROLL	.00	2.00	2.00	2.00	2.00	2.00	2.00	2.000	.000
39	7. YAW DUE TO ROLL	.00	2.00	2.00	2.00	2.00	2.00	2.00	2.000	.000
40	8. EASE OF TURN	.00	2.00	2.00	2.00	2.00	2.00	2.00	2.000	.000
41	9. EASE OF TURN	.00	2.00	2.00	2.00	2.00	2.00	2.00	2.000	.000
79	AVER. AND STD. DEV. OF SUBTASKS (EX 1,2,3,4)	.0	.0	2.4	.5	1.9	.6	2.4	.5	2.6
					.4	3.2	1.2	2.1	.6	2.4
										.81

COMMENTS

PILOT

FEELS BETTER THAN PITCH STICK GRADIENT
 GOOD
 TOO HEAVY
 HIGH RUDDER FORCE TO COORDINATE
 VTRIM 52IAS .314RAD/SEC, VTRIM 78IAS .454RAD/SEC
 SLIGHT PITCH/ROLL COUPLING-ALSO RUDDER A LITTLE WEAK
 LOWER SINK RATE THAN OTHERS
 LOCK. BANK WITH FULL RUDDER FOR CONSTANT HEADING SLIP--NO RUDDER
 LOCK. LOSE AIRSPEED AFTER APPROX. .49RAD YAW
 SLIGHT PITCH DOWN WITH SIDESLIP. .17RAD BANK FOR FULL RUDDER, SLIGHT
 SKEWAL EFFECT AT 52IAS, NEUTRAL AT 78IAS
 A LITTLE SLOW NEAR STALL.
 VERY GOOD
 ABOUT AVERAGE
 VERY GOOD
 BECAUSE OF HEAVY RUDDER FORCES, APPROX 89N IN MAINTAINING TURN
 NEUTRAL OF LOW AMPLITUDE, LONG PERIOD
 STICK FORCE/LGL APPROX 9N
 VERY GOOD
 BUFFETING
 SAME AS .785RAD BANK
 SINK FORCE/LGL APPROX 22N
 EXCELLENT LATERAL- DIRECTIONAL CHARACTERISTICS MIXED SOMEWHAT BY
 BUFFETING
 EXCELLENT COORDINATE RUDDER RESPONSE, UNHARMONIOUS FORCE (ONLY ABOUT 89N
 BUT SEEMS HIGH RELATIVE TO STICKY TO CONTROL, BUT STICK FORCE/LGL
 49 AND 80DEG- BANK LESS THAN EASY TO CONTROL, BUT STICK FORCE/LGL
 VERY LIGHT RESULTING IN OVERCONTROLLING ELEVATOR AND GETTING STALL
 BUFFETING FREQUENTLY
 VERY GOOD RUDDER COORDINATION WOULD NOT BE ACCEPTABLE IN A
 POWERED AIRPLANE, BUT AS SAILPLANES 60....

***** ZEROS INDICATE NO RATING BY PILOT *****

SAILPLANE 1 DATA

TASK	DESCRIPTION OF TASKS	1	2	PILOT 3	4	5	6	7	AVER.	STD DEV
42	E. PILOT OPTN OF PLANE STALLSPIN CHAR	1.50	3.00	1.00	.00	.00	2.00	.00	1.875	.740
43	1. RUDDER AIMING	2.00	3.00	2.00	1.00	2.00	3.00	3.00	2.429	.493
44	2. SLOW WINGING	1.00	2.00	2.00	2.00	2.00	2.00	1.00	2.070	1.000
45	3. AGGRAVATED STALL-TEND TO SPIN	1.00	4.00	2.00	1.00	2.00	2.00	2.00	1.933	.451
46	4. SLOW RECOVERY	1.00	1.00	1.00	1.00	1.00	2.00	1.00	1.750	.829
47	5. STALL RECOVERY, ALTITUDE LOSS	.00	3.00	1.00	.00	.00	2.00	1.00	1.900	.900
48	6. SLOW RECOVERY	1.00	3.00	1.00	.00	.00	2.00	.00	1.500	.500
49	7. STALL FROM TURN AT LOW SPEED	1.00	2.00	1.00	1.00	2.00	2.00	.00	1.500	.500
80	AVER. AND STD. DEV. OF SUBTASKS(EX 1,2,..)	1.3	.5 2.1 1.1 1.4	.5 1.5	.7 1.8	.5 1.8	.7 1.8	.7 1.8	.76	

COMMENTS

TASK PILOT

33 RUDDER EFFECTIVE, AILERONS INEFFECTIVE. RUDDER WILL NOT PICK UP
 34 BUT WILL ARREST FURTHER DROP
 35 ADEQUATE
 36 ADJUST OCCURRED APPROX 1/2 KT ABOVE STALL
 37 THERE IS A DEFINITE TENDENCY TO FALL OFF TO ONE SIDE
 38 VERY SLOW WING DROP OFF, BUT EASILY RECOVERABLE BY RELEASING STICK
 39 EXCELLENT
 40 VERY LITTLE
 41 VERY SURE THAN 15M.
 42 MODERATE ENTRY RATE
 43 SLOW BUT PLENTY OF TIME TO CATCH IT
 44 SLOW RATE RECOVERY
 45 SLIGHTLY NEUTRAL ELEVATOR, SLIGHTLY OPPOSITE RUDDER
 46 NO AGGRAVATED STALL-SPIN ENTRY
 47 DIFFICULT TO DO
 48 STALL-SPIN CHARACTERISTICS ARE GOOD TO EXCELLENT. LACK OF SLIPPER-
 49 NET (ASSOCIATED WITH CHARACTERISTICS
 50 ALL THE ABOVE SAFELY
 51 LOW ALTITUDE SAFETY
 52 LIGHT BUFFET AT 35IAS
 53 CONTROLS, AIRPLANE PRACTICALLY RECOVERS BY ITSELF; NOSE FALLS THRU
 54 AND AIRPLANE STARTS FLYING AGAIN. EXCELLENT CHARACTERISTICS-VERY SAFE

***** ZEROS INDICATE NO RATING BY PILOT ***** SAILPLANE 2 DATA

TASK	DESCRIPTION OF TASKS	1	2	3	4	5	6	7	AVER.	STD DEV							
42	E. PILOT OPIN OF PLANE STALLSPIN CHAR	1.00	1.00	3.00	.00	.00	5.00	1.00	2.200	1.600							
43	1. RUDDER WARNING EFFECT DUR. STALL	1.00	1.00	3.00	.00	2.00	4.00	1.00	1.857	1.385							
44	2. STALL WARNING EFFECT DUR. STALL	1.00	1.00	3.00	.00	5.00	5.00	1.00	2.114	1.326							
45	3. AGGRAVATED STALL TEND TO SPIN	1.00	1.00	3.00	.00	3.00	2.00	1.00	2.143	1.256							
46	4. STICK FORCE GRADIENT	1.00	1.00	3.00	.00	2.00	3.00	1.00	2.000	.745							
47	5. STALL RECOVERY, ALTITUDE LOSS	1.00	.00	2.00	.00	2.00	3.00	1.00	1.667	1.414							
48	6. SPIN ENTRY	1.00	.00	2.00	.00	.00	5.00	2.00	1.500	1.400							
49	7. SPIN RECOVERY	1.00	1.00	2.00	.00	3.00	4.00	1.00	1.857	1.325							
50	8. STALL FROM TURN AT LOW SPEED	1.00	1.00	2.00	.00	.00	4.00	1.00	1.857	1.325							
80	AVER. AND STD. DEV. OF SUBTASKS(EX 1,2,..)	1.0	.0	1.0	.0	2.2	.4	1.5	.8	2.5	.5	4.3	1.0	1.6	1.0	2.1	1.27

COMMENTS

42 DURING STALLS RUDDER POOR, AILERON FAIRLY GOOD
 43 ADEQUATE, SOME OF IT IS IN THE FORM OF CHANGING NOISE CHARACTER.
 44 NO BUFFET WARNING-DIRECTIONAL STABILITY APPARENTLY DETERIATES!
 45 WANDERS IN YAW
 46 NONE FOUND
 47 ABOUT AVERAGE
 48 15M. PILOT SPIN FAIRLY MILD
 49 EASY RECOVERY AFT STICK FORCE
 50 JUST RELAX AFT STICK FORCE
 51 NO PROBLEM
 52 PILOT STALL THERE IS A TENDENCY OF ROLL OSCILLATIONS.
 53 EASY STALL RECOVERY FROM EITHER TURN DIRECTION.
 54 VERY SENSITIVE TO Sudden BREAK AND SUDDEN BREAK MAKE SHIP UNDESIRABLE
 55 VERY EXTENSIVE THERMAL SOARING FOR A LOW TIME PILOT
 56 VERY SENSITIVE TO STALLS TURNING AND 1 LGT STICK CAN RE HELD FULL AFT
 57 VERY SENSITIVE TO STALLS TURNING AND 1 LGT STICK CAN RE HELD FULL AFT
 58 VERY SENSITIVE TO STALLS TURNING AND 1 LGT STICK CAN RE HELD FULL AFT
 59 VERY SENSITIVE TO STALLS TURNING AND 1 LGT STICK CAN RE HELD FULL AFT
 60 VERY SENSITIVE TO STALLS TURNING AND 1 LGT STICK CAN RE HELD FULL AFT
 61 VERY SENSITIVE TO STALLS TURNING AND 1 LGT STICK CAN RE HELD FULL AFT

***** ZEROS INDICATE NO RATING BY PILOT *****

SAILPLANE 3 DATA

TASK	DESCRIPTION OF TASKS	1	2	PILOT 3	4	5	6	7	AVER.	STD DEV							
42	E. PILOT OPIN OF PLANE STALLSPIN CHAR	2.00	2.00	3.00	.00	.00	4.00	1.00	2.400	1.020							
43	1. RUDDER-AILERON EFFECT DUR. STALL	1.00	2.00	2.00	2.00	2.00	3.00	1.00	1.857	.639							
44	2. STALL WARNINGS	1.00	2.00	3.00	3.00	3.00	3.00	4.00	2.459	.904							
45	3. AGGRAVATED STALL-TEND TO SPIN	2.00	2.00	3.00	2.00	3.00	4.00	1.00	2.571	.728							
46	4. STICK FORCE GRADIENT	2.00	2.00	3.00	2.00	2.00	3.00	1.00	2.143	.639							
47	5. STALL RECOVERY, ALTITUDE LOSS	2.00	2.00	3.00	3.00	3.00	3.00	1.00	2.353	.943							
48	6. STALL RECOVERY	2.00	1.00	3.00	.00	.00	2.00	1.00	1.000	1.000							
49	7. SPIN RECOVERY	2.00	1.00	2.00	.00	.00	2.00	1.00	1.667	.471							
50	8. STALL FROM TURN AT LOW SPEED	2.00	1.00	2.00	.00	.00	2.00	1.00	1.667	.471							
80	AVER. AND STD. DEV. OF SUBTASKS(EX 1,2,*)	1.8	.7	1.8	.4	2.6	.5	2.4	.5	2.2	.4	3.1	.6	1.5	1.0	2.2	.83

COMMENTS

PILOT

3 KTS
 4 VERY LIGHT AIRFRAME BUFFET APPROX. 2KTS ABOVE STALL.
 4 LIGHT BUFFETING CLOSE (3KTS) TO STALL
 4 NO WARNINGS
 4 WITH FULLY DEVELOPED STALL, A/C ROLLS OFF ON LEFT WING AND NOSE
 4 FALLS OFF ON WING AND ROTATES, EASY TO CONTROL
 4 COULD BE IMPROVED--NOT ENOUGH FORCE
 1 GOOD REALLY GOOD CUE FOR IMMINENT STALL
 2 VERY LIGHT
 3 15 METERS
 4 LITTLE LOSS IN ALTITUDE
 4 ALTITUDE LESS THAN 30M
 4 15M/19M STALL AT 42KTS
 4 NONE QUITE RESISTANT
 4 FAIRLY ABRUPT FALL-OFF TO ONE SIDE
 3 NONE
 3 SLOWER THAN OTHERS
 3 UNABLE TO STALL DUE TO LACK OF UP CONTROL TRAVEL
 3 AILERON REMAINS EFFECTIVE THROUGHOUT STALL
 3 FAIRLY QUICKLY. DOES NOT RESPOND TO CORRECTIVE ACTION AS READILY
 3 AS SAILPLANE 2
 3 STALL CHARACTERISTICS EXCELLENT-AILERONS EFFECTIVE THROUGHOUT STALL-
 3 CAN HOLD STICK FULL AFT AND USE RUDDER AND AILERONS FOR CONTROL
 3 FOR SOME TIME.

***** ZEROS INDICATE NO RATING BY PILOT *****

SAILPLANE 4 DATA

TASK	DESCRIPTION OF TASKS	1	2	PILOT 3	4	5	6	7	AVER.	STD DEV							
42	E. PILOT OPIN OF PLANE STALL SPIN CHAR	.00	2.00	2.00	2.00	3.00	4.00	4.00	3.000	.872							
43	1. RUDDER/AILERON EFFECT DUR. STALL	.00	2.00	2.00	2.00	3.00	4.00	4.00	3.333	.743							
44	2. STALL WARNING	.00	2.00	2.00	2.00	3.00	4.00	4.00	3.500	.297							
45	3. AGGRAVATED STALL-TEND TO SPIN	.00	2.00	3.00	2.00	3.00	4.00	4.00	3.000	1.000							
46	4. STICK FORCE GRADIENT	.00	1.00	2.00	1.00	2.00	3.00	3.00	2.000	.471							
47	5. STALL RECOVERY, ALTITUDE LOSS	.00	1.00	2.00	1.00	2.00	3.00	3.00	2.000	.471							
48	6. SPIN ENTRY	.00	3.00	.00	.00	.00	2.00	2.00	2.500	.560							
49	7. SPIN RECOVERY	.00	1.00	2.00	2.00	3.00	4.00	4.00	3.250	1.000							
50	8. STALL FROM TURN AT LOW SPEED	.00	1.00	2.00	2.00	3.00	4.00	4.00	2.250	1.000							
80	AVER. AND STD. DEV. OF SUBTASKS(EX 1,2,*)	.0	.0	1.7	.8	2.2	.4	1.7	.5	2.2	.4	2.7	.7	3.2	.8	2.3	.89

COMMENTS

GOOD WARNING OCCURS APPROX. 2 KTS ABOVE STALL.
 NONE - LIGHT BUFFET AT STALL V. STALL 39KTS. FLAP 0
 ALL WING DROPS UNCONTROLLABLE WITH AGGRAVATED, BUT NOT ABRUPT WING DROP
 SUEMED TO HAVE TENDENCY TO SPIN
 DEFINITE FEELING OF BEGINNING AUTOROTATION
 POSITIVE GRADIENT
 NEGATIVE GRADIENT
 NEGATIVE ALT LOSS
 LOSS OF STICK FORCE
 LOSS OF STICK FORCE
 UNABLE TO DO DUE TO LIMITED STICK TRAVEL.
 GOOD OBJECTIONABLE CHARACTERISTICS
 WING DROP FOLLOWING ABUSED STALL IS UNCONTROLLABLE AND IS FOLLOWED
 BY AUTOROTATIVE TENDENCY.

***** ZEROS INDICATE NO RATING BY PILOT *****

SAILPLANE 1 DATA

TASK	DESCRIPTION OF TASKS	1	2	PILOT 3	4	5	6	7	AVER.	STD DEV
51	F. PILOT OPIN. OF PLANE LANDING CHAR.	1.50	2.00	1.00	.00	.00	2.00	2.00	1.700	.400
52	1. PILOT VISIBILITY CONTROL	2.00	1.00	3.00	3.00	2.00	4.00	3.00	2.571	.904
53	2. GLIDE SLOPE CONTROL	1.00	1.00	1.00	1.00	2.00	2.00	2.00	1.571	.990
54	3. AIRBRAKE CONTROL AT EASE OF MOD.	2.00	4.00	1.00	1.00	2.00	2.00	2.00	2.143	.495
55	4. EASE OF LANDING AT ANTENDED SPOT.	1.00	2.00	1.00	1.00	2.00	2.00	2.00	1.571	.500
56	5. EASE OF CONTROL AT SINK AT TOUCH.	1.00	1.00	1.00	1.00	2.00	2.00	2.00	1.500	.500
57	6. CONTROL DURING ROLLOUT	1.00	1.00	1.00	1.00	2.00	2.00	1.00	1.429	.728
81	AVER. AND STD. DEV. OF SUBTASKS(EX 1,2,...)	1.3	.5	1.1	1.3	.7	1.3	.7	2.0	.6
	PILOT								1.8	.86

COMMENTS

VISIBILITY DOWN AND AFT RESTRICTED BY FUSELAGE AND WING
 48KTS V-TRIM--SLIGHT NOSE UP TRIM CHANGE WITH SPOTLER DEPLOYMENT.
 MOMENTARY 4KT STICK-FREE, THEN INCREASE TO ABOUT 45KTS-VERY GD
 AIRBRAKES SUCK OPEN
 OUTSTANDING GROUND MANEUVERABILITY
 VERY EASY TO LAND IT WELL
 OVER THE NOSE VISIBLY WEAK. SPOILERS COULD BE MORE POWERFUL.
 TAIL SKID RESTRICTS GROUND STEERING.

SAILPLANE 2 DATA

TASK	DESCRIPTION OF TASKS	1	2	PILOT 3	4	5	6	7	AVER.	STD DEV
51	F. PILOT OPIN. OF PLANE LANDING CHAR.	2.00	.00	2.00	.00	1.00	5.00	2.00	2.750	1.289
52	1. PILOT VISIBILITY CONTROL	3.00	1.00	2.00	1.00	1.00	2.00	1.00	1.429	.928
53	2. GLIDE SLOPE CONTROL	3.00	3.00	3.00	2.00	2.00	3.00	3.00	3.000	.000
54	3. AIRBRAKE CONTROL AT EASE OF MOD.	3.00	3.00	3.00	3.00	3.00	4.00	3.00	3.143	.750
55	4. EASE OF LANDING AT ANTENDED SPOT.	1.00	2.00	2.00	3.00	3.00	4.00	2.00	2.571	.990
56	5. EASE OF CONTROL AT SINK AT TOUCH.	2.00	2.00	2.00	3.00	3.00	4.00	2.00	2.571	.990
57	6. CONTROL DURING ROLLOUT	2.00	2.00	2.00	3.00	3.00	4.00	2.00	2.571	.928
81	AVER. AND STD. DEV. OF SUBTASKS(EX 1,2,...)	2.2	.9	2.0	.6	2.3	.5	2.7	.9	2.0
	PILOT								2.5	1.01

COMMENTS

GOOD BRAKES A LITTLE WEAK
 6000 USE MORE EFFECTIVE DIVE BRAKES
 VERY LOW FORCE GRADIENT RESULTS IN OVERCONTROL.
 CONTROL NOT AT ALL TIGHT
 CONTROL LOCK VERY POOR. UNLOCKING OF AIRBRAKES RESULTS IN FORCE IS
 REQUIRED TO CLOSE THE AIRBRAKES. I FEEL THAT YOU SHOULD BE ABLE
 TO SELECT AIRBRAKE RAPIDLY AND IT WILL REMAIN AT SELECTED POSITION
 WHEN THE CONTROL IS RELEASED.
 HAVE TO HOLD AGAINST FURTHER EXTENSION WHICH I PREFER TO HOLDING WITH
 GOOD BRAKES COULD BE MORE EFFECTIVE
 A LONG TUDINAL OK - DIRECT WIND EFFECT
 VERY GOOD LOW FORCE GRADIENT AND SHORT CONTROL STICK RESULTED IN OVERCENTRI.
 BETTER THAN SAILPLANE 5 ADEQUATE MANEUVERING.
 INSUFFICIENT RUDDER FOR A LITTLE EFFORT
 DIRECT INADEQUATE DIVE BRAKE EFFECTIVENESS. 6. SOME CONCENTRATION
 2,3,4 REQUIRED CHARACTERISTICS ARE BETTER THAN AVERAGE. NO TENDENCY TO GO
 LANDING CHARACTERISTICS ARE BETTER THAN AVERAGE. NO TENDENCY TO GO
 TO EITHER SIDE.
 DIVE BRAKES WEAK. USE OF DRAG CHUTE NOT INCLUDED IN TEST EVALUATION.
 TOUCHDOWN CAN BE ACHIEVED BUT ONLY THRU USE OF EXCESSIVE SPEED.

***** ZEROS INDICATE NO RATING BY PILOT *****

SAILPLANE 3 DATA

TASK	DESCRIPTION OF TASKS	1	2	3	4	5	6	7	AVER.	STD DEV					
51	F. PILOT OPIN. OF PLANE LANDING CHAR.	3.00	3.00	3.00	3.00	.00	4.00	3.00	3.200	.400					
52	1. PILOT VISIBILITY	2.00	1.00	1.00	1.00	2.00	3.00	1.00	1.429	.498					
53	2. GLIDE SLOPE CONTROL	3.00	3.00	3.00	3.00	3.00	3.00	3.00	3.071	.498					
54	3. AIRS. CONTROL, AIRB. EASE OF MOD.	3.00	3.00	3.00	4.00	2.00	3.00	3.00	3.143	.750					
55	4. AIRS. OF LAND. AT INTENDED SPOT	3.00	3.00	4.00	3.00	2.00	3.00	2.00	3.143	.429					
56	5. EASE OF CONTROL. SINK AT TOUCH.	3.00	3.00	2.00	3.00	3.00	4.00	2.00	2.429	.429					
57	6. CONTROL DURING ROLLOUT	2.00	3.50	2.00	3.00	3.50	4.00	4.00	4.000	2.375					
61	AVER. AND STD. DEV. OF SUBTASKS(EX 1,2,...)	2.7	5.2	6.8	2.5	1.0	2.5	1.0	3.4	2.7	2.8	2.3	.9	2.7	1.33

COMMENTS

TASK PILOT

52 EXCELLENT
 53 AIR BRAKES A LITTLE WEAK
 54 VERY LOW FORCE GRADIENT RESULTS IN SOME PORPOSING PRIOR TO FLARE.
 55 LIGHT SUCK CONTROL, BUT FAST
 56 AIR BRAKE HAS A TENDENCY, AFTER BEING UNLOCKED TO FLOAT TO APPROX.
 57 3/4 EXTENDED POSITION. I FELT THE AIR BRAKE SHOULD REMAIN IN
 THE SELECTED POSITION. SPOILER EXTENSION AT 55 KTS.
 58 SIGHT LINE DOWN WITH SPOILER EXTENSION AT 55 KTS.
 59 AIR BRAKES AS THEY COULD BE MORE EFFECTIVE
 60 EASY TO CONTROL IN PITCH IN TURBULENCE
 61 GOOD LOW FORCE GRADIENT RESULTS IN SOME VERTICAL OSCILLATION DURING
 YARE FLARE
 62 RUDDER FAIR--AILERONS FAIR
 63 GOOD
 64 BRAKE CONTROL ANKWARD TO APPLY WITHOUT TAKING HAND FROM CONTROL STICK
 65 FULL BRAKE APPLICATION RESULTED IN ONLY MINOR BRAKING ACTION
 66 LOST CONTROL DURING ONE OF LANDINGS.
 67 MINIMUM RUDDER AND TAILSKID FOR DIRECTIONAL CONTROL. A STEERABLE
 68 YAW WHEEL WOULD BE IMPROVED WITH MORE POWERFUL DIVE BRAKE
 69 2,3,4,5 CROSSWIND CAPABILITY
 70 FAIR CROSSWIND CAPABILITY
 71 MAIN ONE WOULD MAKE TO.
 72 LIMITED YAW CONTROL ON ROLLOUT.

***** ZEROS INDICATE NO RATING BY PILOT *****

SAILPLANE 1 DATA

TASK	DESCRIPTION OF TASKS	1	2	PILOT	4	5	6	7	AVER.	STD DEV					
58	III. FLIGHT CHARACTERISTICS IN CONVECTION	1.00	1.00	1.00	.00	.00	1.00	.00	1.000	.000					
59	A. PILOT OPINION OF TOW	1.00	1.00	1.00	.00	.00	2.00	1.00	1.500	.764					
60	1. EASE OF MAINTAINING POSITION	1.00	1.00	1.00	.00	.00	1.00	1.00	1.333	.745					
61	2. RESPONSE TO VERTICAL CURRENTS	1.00	.00	1.00	.00	.00	2.00	2.00	1.833	.687					
62	3. RELEASE	1.00	.00	2.00	.00	.00	2.00	2.00	1.800	.400					
82	AVER. AND STD. DEV. OF SUBTASKS(EX 1,2,..)	1.0	.0	1.5	.5	1.3	.5	.0	.0	2.7	.5	1.7	.5	1.6	.68

COMMENTS

59 PITCH PRIMARILY--LAT/DIR-2
 60 NO DIFFICULTY WAS EXPERIENCED DUE TO PRESENCE OF VERTICAL CURRENTS
 61 HAD TO USE SLIGHT FORWARD STICK FORCE DURING TOW--TRIM NOT ADEQUATE
 62 FORCE WAS VERY LOW HOWEVER

SAILPLANE 2 DATA

TASK	DESCRIPTION OF TASKS	1	2	PILOT	4	5	6	7	AVER.	STD DEV							
58	III. FLIGHT CHARACTERISTICS IN CONVECTION	1.50	2.00	3.00	.00	.00	2.00	3.00	2.500	.707							
59	A. PILOT OPINION OF TOW	1.00	2.00	3.00	.00	.00	2.00	4.00	2.417	.837							
60	1. EASE OF MAINTAINING POSITION	2.00	3.00	3.00	.00	.00	2.00	4.00	2.500	.957							
61	2. RESPONSE TO VERTICAL CURRENTS	1.00	3.00	3.00	.00	.00	2.00	3.00	2.500	.500							
62	3. RELEASE	1.00	.00	2.00	.00	.00	2.00	2.00	1.750	.433							
82	AVER. AND STD. DEV. OF SUBTASKS(EX 1,2,..)	1.3	.5	2.5	.5	2.7	.5	.0	.0	2.5	.5	2.0	.0	3.0	.8	2.3	.77

COMMENTS

59 GOT TO STAY WITH IT, DIRECTIONAL MOST OBVIOUS
 60 GOT SOME TOW ROPE REBOUNDING
 61 I BELIEVE THAT THE BOUNCY ROPE IN TURBULENCE IS CAUSED BY WING FLX
 62 I WOULD RATE THE SAILPLANE ABOUT THE SAME HERE AS IN SMOOTH AIR.

SAILPLANE 3 DATA

TASK	DESCRIPTION OF TASKS	1	2	PILOT	4	5	6	7	AVER.	STD DEV							
58	III. FLIGHT CHARACTERISTICS IN CONVECTION	2.00	3.00	2.00	.00	.00	3.00	3.00	2.600	.490							
59	A. PILOT OPINION OF TOW	1.50	3.00	2.00	.00	.00	2.00	3.00	2.417	.607							
60	1. EASE OF MAINTAINING POSITION	2.00	3.00	2.00	.00	.00	2.00	3.00	2.500	.500							
61	2. RESPONSE TO VERTICAL CURRENTS	3.00	4.00	2.00	.00	.00	2.00	3.00	2.833	.687							
62	3. RELEASE	1.00	4.00	3.00	.00	.00	2.00	2.00	2.000	.632							
82	AVER. AND STD. DEV. OF SUBTASKS(EX 1,2,..)	2.0	.8	3.5	.5	2.3	.5	.0	.0	2.7	.5	2.0	.0	2.7	.5	2.5	.70

COMMENTS

59 MODERATE CONTROL ACTIVITY REQD.
 60 NO PROBLEMS
 61 SOME TENDENCY OF NOSE TO PORPOISE.
 62 TENDENCY TO PITCH WHEN ENCOUNTERING TURBULENCE
 63 NO PROBLEMS
 64 NOISY
 65 SOME STICK INSTABILITY IN TURBULENCE
 66 HIGH WORKLOAD IN RUDDERS ANDAILERONS

***** ZEROS INDICATE NO RATING BY PILOT *****

SAILPLANE 4 DATA

TASK	DESCRIPTION OF TASKS	1	2	PILOT 3	4	5	6	7	AVER.	STD DEV							
58	III. FLIGHT CHARACTERISTICS IN CONVECTION																
59	A. PILOT OPINION OF TOW	.00	2.00	2.50	.00	.00	3.00	3.00	2.625	.415							
60	1. EASE OF MAINTAINING POSITION	.00	2.00	2.00	.00	.00	2.00	2.00	2.000	.000							
61	2. RESPONSE TO VERTICAL CURRENTS	.00	2.00	2.00	.00	.00	2.00	2.00	2.000	.000							
62	3. RELEASE	.00	2.00	3.00	.00	.00	2.00	2.00	2.333	.471							
82	AVER. AND STD. DEV. OF SUBTASKS(EX 1,2,..)	.0	.0	2.0	.0	2.3	.5	.0	.0	2.0	.0	2.0	.0	2.0	.0	2.1	.29

COMMENTS

TASK	PILOT	COMMENTS
60	3	NO PROBLEM AT ALL
62	3	NOISY
82	3	GOOD
82	3	NO SIGNIFICANT DIFFERENCE FROM STILL AIR

SAILPLANE 5 DATA

TASK	DESCRIPTION OF TASKS	1	2	PILOT 3	4	5	6	7	AVER.	STD DEV		
58	III. FLIGHT CHARACTERISTICS IN CONVECTION											
59	A. PILOT OPINION OF TOW	2.00	5.00	2.00	.00	.00	4.00	3.00	3.875	1.156		
60	1. EASE OF MAINTAINING POSITION	1.50	2.00	.00	.00	.00	3.00	5.00	3.000	1.431		
61	2. RESPONSE TO VERTICAL CURRENTS	2.00	2.00	.00	.00	.00	3.00	3.00	2.500	.800		
62	3. RELEASE	1.00	.00	.00	.00	.00	3.00	2.00	2.000	.816		
82	AVER. AND STD. DEV. OF SUBTASKS(EX 1,2,..)	1.7	5.2	0	0	0	3.0	0	3.3	1.2	2.5	.99

COMMENTS

TASK	PILOT	COMMENTS
59	2	OK AT 70KTS, AT 80KTS WORSE THAN IN SMOOTH AIR. MUST FLY WITH STICK RIGID. FLY PITCH BY PRESSURE, MUST FLY BY POSITION.
60	2	CANNOT FLY PITCH BY PRESSURE, MUST FLY BY POSITION.
62	3	NO ROUGH AIR TOW MADE.
82	3	TAW AND ROLL RATES MAKE STAYING BEHIND TOMPLANE DIFFICULT IN ROUGH THE RAILS
82	9	LATERAL POSITIONING IS AN EASY TASK; PITCH IS DIFFICULT DUE TO OVERCONTROL TENDENCY
82	7	

SAILPLANE 6 DATA

TASK	DESCRIPTION OF TASKS	1	2	PILOT 3	4	5	6	7	AVER.	STD DEV							
58	III. FLIGHT CHARACTERISTICS IN CONVECTION																
59	A. PILOT OPINION OF TOW	.00	3.00	2.00	.00	.00	5.00	2.00	3.000	1.233							
60	1. EASE OF MAINTAINING POSITION	.00	2.00	2.00	.00	.00	2.00	2.00	2.000	.000							
61	2. RESPONSE TO VERTICAL CURRENTS	.00	2.00	2.00	.00	.00	2.00	2.00	2.000	.000							
62	3. RELEASE	.00	.00	2.00	.00	.00	2.00	2.00	2.000	.000							
82	AVER. AND STD. DEV. OF SUBTASKS(EX 1,2,..)	.0	.0	2.0	.0	2.0	.0	.0	.0	2.0	.0	2.0	.0	2.0	.0	2.0	.00

COMMENTS

TASK	PILOT	COMMENTS
61	3	NOT EXCESSIVE
82	3	SAME AS SMOOTH AIR
82	3	AIR SPEED BLEEDS OFF QUICKLY DURING PULLUP, REQUIRING PILOT ATTENTION
82	7	HIGHER WORKLOAD THAN IN SMOOTH AIR, OF COURSE, BUT NO UNUSUAL CHARACTERISTICS DUE TO TURBULENCE

***** ZEROS INDICATE NO RATING BY PILOT *****

SAILPLANE 1 DATA

TASK	DESCRIPTION OF TASKS	1	2	PILOT 3	4	5	6	7	AVER.	STD DEV
63	B. PILOT OPINION OF CIRCLING FLIGHT	1.00	1.00	1.00	.00	.00	1.00	1.00	1.000	.000
64	1. LOW SPEED HANDLING	1.00	1.00	1.00	.00	2.00	1.00	1.00	1.167	.173
65	2. STALL SUSCEPTIBILITY	2.00	1.00	1.00	.00	2.00	1.00	2.00	1.167	.173
66	3. STALL RECOVERING THERMAL	1.00	1.00	2.00	.00	2.00	1.00	2.00	1.633	.362
67	4. SPEED CONTROL	1.00	1.00	2.00	.00	2.00	1.00	2.00	1.500	.500
63	AVER. AND STD. DEV. OF SUBTASKS(EX 1+2+...)	1.3	.4	1.3	.4	1.6	.4	1.3	.4	1.6
TASK	PILOT									
63	2									
64	3									
65	3									
66	7									
67	7									

COMMENTS

BEST THERMAL MANEUVERING OF ANY SAILPLANE--PERHAPS DUE TO POWERFUL RUDDER
 GOOD AILERON -- ROLL RESPONSE IN THERMALS, EASY TO MUSCLE GLIDER
 AROUND IN THERMALS EXCELLENT--VERY LOW WORKLOAD--LITTLE RUDDER ROD
 FOR TIGHT COORDINATION--EXCELLENT CONTROL HARMONY, BOTH IN FORCES
 AND RESPONSES

SAILPLANE 2 DATA

TASK	DESCRIPTION OF TASKS	1	2	PILOT 3	4	5	6	7	AVER.	STD DEV
63	B. PILOT OPINION OF CIRCLING FLIGHT	1.50	1.50	3.00	.00	.00	2.00	4.00	2.400	.970
64	1. LOW SPEED HANDLING	2.00	2.00	2.00	.00	4.00	2.00	4.00	2.833	.898
65	2. STALL SUSCEPTIBILITY	1.00	1.00	2.00	.00	3.00	2.00	2.00	2.167	.574
66	3. STALL RECOVERING THERMAL	2.00	1.00	2.00	.00	3.00	2.00	2.00	2.167	.574
67	4. SPEED CONTROL	1.00	1.00	4.00	.00	3.00	1.00	3.00	2.167	.574
63	AVER. AND STD. DEV. OF SUBTASKS(EX 1+2+...)	1.5	.5	1.3	.4	2.7	.8	2.7	1.5	3.0
TASK	PILOT									
63	3									
64	3									
65	3									
66	7									
67	7									

COMMENTS

HAS SOME UNDESIRABLE CHARACTERISTICS, RUFFETING
 HELD IN PRECARIOUS DUE TO STICK POSITION AFT WITH LOW FORCE AND YAW
 STRONG OSCILLATION
 VERY DIFFICULT THAN OTHERS
 AILERS VERY DIFFICULT
 1. RUDDER EFFECTIVENESS COULD BE IMPROVED. 4, WILL SPIRAL HANDS
 LACK FOR LONG PERIODS STABILITY AND DIFFICULT TURN COORDINATION
 LOW RUDDER EFFECTIVENESS
 HIGH WORKLOAD DUE TO RUDDER AND AILERON ACTIVITY TO KEEP SIDESLIP
 NEAR ZERO--GIVES IMPRESSION OF LOW DIRECTIONAL STABILITY.

***** ZEROS INDICATE NO RATING BY PILOT *****

SAILPLANE 3 DATA

TASK	DESCRIPTION OF TASKS	1	2	PILOT 3	4	5	6	7	AVER.	STD DEV							
63	B. PILOT OPINION OF CIRCLING FLIGHT	2.00	2.00	2.00	.00	.00	2.00	2.00	2.000	.000							
64	1: LOW SPEED HANDLING	1.00	2.00	3.00	.00	2.00	2.00	2.00	2.000	.577							
65	2: STALL-SPIN SUSCEPTIBILITY	2.00	2.00	2.00	.00	2.00	3.00	1.00	2.000	.577							
66	3: EASE OF CENTERING THERMAL	1.00	2.00	2.00	.00	2.00	2.00	3.00	2.000	.577							
67	4: SPEED CONTROL	2.00	2.00	3.00	.00	2.00	2.00	3.00	2.333	.471							
83	AVER. AND STD. DEV. OF SUBTASKS(EX 1,2,*)	1.5	.5	2.0	.0	2.5	.5	.0	.0	2.0	.0	2.2	.4	2.2	.3	2.1	.57

COMMENTS

64 PLEASANT, ALTHOUGH STICK FORCES ON THE LIGHT SIDE
 65 NO STALL-SPIN TENDENCY OBSERVED WHILE THERMALING
 66 COMFORTABLE
 67 TENDENCY TO PITCH IN TURBULENT THERMALS
 83 BETTER THAN SAILPLANE 2
 83 WHILE OCCASIONALLY SELF-TIGHTEN DURING STRONG UP-GUSTS. CAN TIGHTEN
 83 ITSELF INTO STALL IN STRONG GUST
 83 ONE SELF FEELS IMMEDIATELY AT HOME IN THE SHIP
 83 GOOD CONTROL HARMONY AT SOKTS BUT POOR AT HIGHER SPEEDS, RUDDER
 83 COORDINATION AND AIRSPEED CONTROL CREATE FAIRLY HIGH WORKLOAD.

SAILPLANE 4 DATA

TASK	DESCRIPTION OF TASKS	1	2	PILOT 3	4	5	6	7	AVER.	STD DEV							
63	B. PILOT OPINION OF CIRCLING FLIGHT	.00	2.00	2.50	.00	.00	3.00	4.00	2.875	.740							
64	1: LOW SPEED HANDLING	.00	2.00	2.50	.00	.00	3.00	4.00	2.750	.829							
65	2: STALL-SPIN SUSCEPTIBILITY	.00	2.00	2.50	.00	.00	3.00	3.00	2.375	.415							
66	3: EASE OF CENTERING THERMAL	.00	2.00	3.00	.00	.00	3.00	3.00	2.750	.433							
67	4: SPEED CONTROL	.00	2.00	3.00	.00	.00	5.00	3.00	3.250	1.090							
83	AVER. AND STD. DEV. OF SUBTASKS(EX 1,2,*)	.0	.0	2.0	.0	2.6	.4	.0	.0	2.0	.0	3.2	1.1	3.2	.4	2.8	.81

COMMENTS

64 GOOD
 65 UNDESIRABLE CHARACTERISTICS NOTED
 66 TENDED TO OVERCONTROL WITH RUDDER
 67 NOT AS GOOD AS SAILPLANE 1
 83 I DON'T FIND TRIMMER OBJECTIONABLE. WING-ROCK IS BOTHERSOME
 83 WHENEVER BUFFER ENCOUNTERED IN GUSTY THERMALS
 83 QUITE GOOD IN CIRCLING FLIGHT, THOUGH NOT AS GOOD AS SAILPLANE 1
 83 GUSTS CAUSE NOSE TO CHANGE ALTITUDE UP AND DOWN. THIS TENDENCY
 83 MUST BE BROUGHT BY PILOT TO MAINTAIN THERMAL LOCATION.
 83 EXCESSIVE TOP ALLEKON REQUIRED.

***** ZEROS INDICATE NO RATING BY PILOT *****

SAILPLANE 5 DATA

TASK	DESCRIPTION OF TASKS	1	2	3	4	5	6	7	AVER.	STD DEV
63	B. PILOT OPINION OF CIRCLING FLIGHT	2.50	3.00	1.00	.00	.00	3.00	2.00	2.300	.748
64	1. LOWSPEED HANDLING	2.00	3.00	2.00	.00	.00	3.00	2.00	2.400	.490
65	2. STALL-SP IN SUSCEPTIBILITY	1.00	2.00	2.00	.00	.00	2.00	1.00	1.600	.490
66	3. EASE OF CENTERING THERMAL	3.00	3.00	3.00	.00	.00	4.00	4.00	2.750	1.090
67	4. SPEED CONTROL	2.00	2.00	1.00	.00	.00	2.00	4.00	2.200	.980
83	AVER. AND STD. DEV. OF SUBTASKS(EX 1,2,..)	2.0	.7 2.5	.5 1.7	.5 .0	.0 .0	.0 2.7	.8 2.0 1.2 2.2		.89
TASK	PILOT									
64	3									
65	3									
66	3									
67	3									
83	3									
83	3									
83	3									
83	3									
83	3									
83	7									

COMMENTS

EXCELLENT
MILDLY SUSCEPTIBLE
NOT TRIED
LOW STICK FORCE/LGL RATHER NICE FOR THERMALLING.
BETTER TRICK THAN SMALLER SPAN GLIDERS
STICK CANNOT BE RELEASED FOR MORE THAN A FEW SECONDS
IN STEEPLY BANKED CIRCLING FLIGHT, FAIRLY LARGE LONG. STICK INPUTS
COULD BE MADE WITHOUT ANY CHANGE IN SPEED OR LGL FORCES.
(ELASTIC EFFECT?)
ROLL RATE AND YAW DUE TO AILERON MAKE THERMAL CENTERING DIFFICULT
IN SMALL ROUGH THERMALS.
VERY STABLE IN BANK ANGLE BUT ATTENTION REQUIRED TO CONTROL AIRSPEED.

SAILPLANE 6 DATA

TASK	DESCRIPTION OF TASKS	1	2	3	4	5	6	7	AVER.	STD DEV
63	B. PILOT OPINION OF CIRCLING FLIGHT	.00	.00	2.00	.00	.00	8.00	3.00	4.333	2.625
64	1. LOWSPEED HANDLING	.00	4.00	.00	.00	.00	8.00	3.00	5.000	2.160
65	2. STALL-SP IN SUSCEPTIBILITY	.00	5.00	.00	.00	.00	8.00	2.00	5.333	2.867
66	3. EASE OF CENTERING THERMAL	.00	3.00	.00	.00	.00	4.00	3.00	3.333	.471
67	4. SPEED CONTROL	.00	4.00	.00	.00	.00	6.00	3.00	4.333	1.247
83	AVER. AND STD. DEV. OF SUBTASKS(EX 1,2,..)	.0	.0 4.0	.7 .0	.0 .0	.0 .0	.0 6.7 1.9 2.7	.4 4.5		2.06
TASK	PILOT									
64	2									
65	3									
66	3									
67	3									
83	3									
83	7									

COMMENTS

GOOD EXCEPT NEAR STALL
GOOD, BUFFETING IS ANNOYING
MODERATE
BREAKS OFF INTO INCIPIENT SPIN EASILY
YES
GOOD
EXCESSIVE PITCH FORCE CHANGE WITH BANK CHANGE
EXCELLENT, BUT ON HEAVY SIDE
HIGH WORKLOAD! TURBULENCE CAUSES UPSETS IN ALL THREE AXES,
REQUIRING LOTS OF STICK AND RUDDER MOVEMENT

***** ZEROS INDICATE NO RATING BY PILOT *****

SAILPLANE 1 DATA

TASK	DESCRIPTION OF TASKS	1	2	PILOT 3	4	5	6	7	AVER.	STD DEV								
68	C. PILOT OPINION OF CRUISING FLIGHT	1.00	1.00	1.00	.00	.00	4.00	1.00	1.600	1.200								
69	1. EASE OF CONTROLLING AIRSPEED	1.00	1.00	1.00	.00	2.00	4.00	1.00	1.667	1.479								
70	2. PULL UP INTO THERMAL	1.00	1.00	2.00	.00	2.00	2.00	2.00	1.867	1.571								
71	3. EASE OF PERF. SECONDARY TASKS	1.00	1.00	1.00	.00	2.00	2.00	2.00	1.500	.900								
72	4. RIDE QUALITY	1.00	1.00	4.00	.00	2.00	2.00	1.00	2.167	.800								
73	5. EASE OF MAIN. STRAIGHT FLIGHT	1.00	2.00	1.00	.00	.00	2.00	1.00	1.400	.490								
84	AVER. AND STD. DEV. OF SUBTASKS(EX 1,2,..)	1.0	.0	1.4	.5	1.8	1.2	.0	2.0	.0	2.0	.0	2.4	.8	1.6	.5	1.7	.79

COMMENTS

TASK PILOT
 69 5
 70 3
 71 3
 72 3
 73 3
 84 7
 85 7

BELOW 61AS+73 ABOVE 61AS DUE TO TRIM UNABLE TO TRIM TO HIGH SPEEDS, I.C. ABOVE 61KTS. SPEED BLEEDS OFF QUICKLY. HAVE TO WATCH IT. EXCELLENT GOOD, BUT SMALL, UNCOMFORTABLE COCKPIT DEGRADES IT EXCELLENT LARGE ATTITUDE CHANGES WITH AIRSPEED VERY LOW WORKLOAD. OVERALL, THE BEST FLYING OF ALL SAILPLANES THEY SHOULD ALL FLY THIS WAYC

SAILPLANE 2 DATA

TASK	DESCRIPTION OF TASKS	1	2	PILOT 3	4	5	6	7	AVER.	STD DEV								
68	C. PILOT OPINION OF CRUISING FLIGHT	1.00	2.00	2.00	.00	.00	2.00	4.00	2.200	.980								
69	1. EASE OF CONTROLLING AIRSPEED	1.00	2.00	2.00	.00	3.00	2.00	3.00	2.167	.667								
70	2. PULL UP INTO THERMAL	1.00	1.00	1.00	.00	3.00	3.00	4.00	2.000	1.175								
71	3. EASE OF PERF. SECONDARY TASKS	1.00	1.00	3.00	.00	3.00	3.00	4.00	2.500	1.175								
72	4. RIDE QUALITY	2.00	2.00	2.00	.00	3.00	2.00	3.00	2.167	.373								
73	5. EASE OF MAIN. STRAIGHT FLIGHT	1.00	1.00	2.00	.00	3.00	4.00	3.00	2.333	1.106								
84	AVER. AND STD. DEV. OF SUBTASKS(EX 1,2,..)	1.2	.4	1.4	.5	2.0	.6	.0	2.8	.4	2.8	.4	2.6	.8	3.4	.5	2.2	.96

COMMENTS

TASK PILOT
 70 3
 71 3
 72 3
 73 3
 84 3
 85 3

VERY PLEASANT DIFFICULT NO PROBLEM NO. OPERATIONALLY LOOSE NOSE WANDERS, BUT NOT SO AS TO DETRACT FROM MISSION BODY HAS TO CHANGE SPEEDS. NEGATIVE FLAPS RESULT IN QUICK AIRSPEED CHANGES (QUICKER THAN SAILPLANE 5) WITH NO ATTITUDE OR SOUND CHANGES. THIS FEATURE MAY MAKE SHIP DIFFICULT FOR TRANSITIONING.

***** ZEROS INDICATE NC RATING BY PILOT *****

SAILPLANE 3 DATA

TASK	DESCRIPTION OF TASKS	1	2	PILOT 3	4	5	6	7	AVER.	STD DEV	
68	C. PILOT OPINION OF CRUISING FLIGHT	1.50	3.00	1.50	.00	.00	4.00	3.00	2.6500	.9770	
69	1. EASE UP CONTROLLING AIRSPEED	2.00	3.00	1.00	.00	3.00	4.00	3.00	2.6500	.9770	
70	2. EASE DOWN CONTROLLING AIRSPEED	1.00	3.00	1.00	.00	3.00	4.00	3.00	2.6500	.9770	
71	3. EASE OF PITCH. THERMAL	2.00	4.00	2.00	.00	4.00	3.00	3.00	2.6500	.9770	
72	4. EASE OF PITCH. STRAIGHT FLIGHT	1.00	3.00	1.50	.00	2.00	3.00	2.00	2.6500	.9770	
73	5. EASE OF MAIN. STRAIGHT FLIGHT	1.00	1.00	1.00	.00	2.00	2.00	2.00	1.5000	.5000	
64	AVER. AND STD. DEV. OF SUBTASKS(EX 1,2,..)	1.6	5.2	1.0	1.3	.4	.0	.0	2.8	.7	
	PILOT								2.4	.5	
	COMMENTS	EASY TASK TO TRIM TO INTERTHERMAL SPEEDS, I.E. ABOVE 80 KTS.									
69	UNABLE TO TRIM TO INTERTHERMAL SPEEDS, I.E. ABOVE 80 KTS.										
70	FEELS PLEASANT										
71	OK										
72	NO HANDS OFF; OVERCONTROLS										
73	MUST HOLD STICK AT ALL TIMES										
74	PLEASANT TO FLY										
75	ANY DISTURBANCE IN PITCH REQUIRES IMMEDIATE ATTENTION										
76	1,3,4 TENDENCY TO PITCH IN TURBULENT AIR-CAN'T RELEASE STICK										
77	WITHOUT DIVERGENCE WHETHER CIRCLING OR STRI AND LEVEL FLIGHT										
78	FASTER IN THIS PHASE OF FLIGHT										
79	GENERALLY GOOD; POOR CONTROL HARMONY AT HIGHER SPEEDS(SENSITIVE										
80	PITCH, SLUGGISH AILERONS).										

SAILPLANE 4 DATA

TASK	DESCRIPTION OF TASKS	1	2	PILOT 3	4	5	6	7	AVER.	STD DEV	
68	C. PILOT OPINION OF CRUISING FLIGHT	.00	2.00	3.50	.00	.00	2.00	2.00	2.3750	.6500	
69	1. EASE UP CONTROLLING AIRSPEED	.00	2.00	3.50	.00	.00	2.00	2.00	2.3750	.6500	
70	2. EASE DOWN CONTROLLING AIRSPEED	.00	2.00	3.50	.00	.00	2.00	2.00	2.3750	.6500	
71	3. EASE OF PITCH. THERMAL	.00	2.00	3.00	.00	.00	3.00	2.00	2.5000	.5000	
72	4. EASE OF PITCH. STRAIGHT FLIGHT	.00	2.00	2.00	.00	.00	3.00	2.00	2.7500	.4330	
73	5. EASE OF MAIN. STRAIGHT FLIGHT	.00	1.00	2.00	.00	.00	2.00	2.00	1.7500	.4330	
64	AVER. AND STD. DEV. OF SUBTASKS(EX 1,2,..)	.0	0.1	1.8	.4	3.0	.5	.0	2.8	.7	
	PILOT								2.4	.5	
	COMMENTS	WORKING AGAINST SPRING IS ANNOYING									
69	WORKING AGAINST SPRING IS ANNOYING										
70	FEELS PLEASANT										
71	OCCASIONAL LACK OF COORDINATION NOTED WHILE WATCHING OTHER GLIDERS										
72	NOT AS GOOD AS OTHER THAN MOST										
73	GOOD										
74	MAINLY CONCERNED WITH WORKING AGAINST THE FEEL SPRING										
75	PULL UP TENDS TO PITCH UP TOO HIGH; ROLL AT TOP OK BUT IF YOU										
76	OVERSHOOT, UNBANKING MAY BE DIFFICULT DUE TO LACK OF TOP AILERON										
77	AT SPEEDS BELOW 40 KTS WITH FLAPS AT 3/4 RAD										
78	HOLDS HEADING AND SPEED WELL; SECONDARY TASKS CAN BE ATTENDED TO.										

***** ZEROS INDICATE NO RATING BY PILOT *****

SAILPLANE 5 DATA

TASK	DESCRIPTION OF TASKS	1	2	PILOT 3	4	5	6	7	AVER.	STD DEV
68	C. PILOT OPINION OF CRUISING FLIGHT	1.00	3.00	1.00	.00	.00	3.00	3.00	2.200	.980
69	1. EASE OF CONTROLLING AIRSPEED	1.00	2.00	2.00	.00	.00	3.00	3.00	2.600	1.366
70	2. PULL UP INTO THERMAL	2.00	3.00	1.00	.00	.00	2.00	2.00	2.000	.632
71	3. EASE OF PERF. SECONDARY TASKS	1.00	6.00	1.00	.00	.00	4.00	4.00	3.200	1.939
72	4. RIDE QUALITY	1.00	2.00	1.00	.00	.00	2.00	3.00	1.800	1.748
73	5. EASE OF MAIN. STRAIGHT FLIGHT	1.00	1.00	1.00	.00	.00	3.00	2.00	1.600	.800
84	AVER. AND STD. DEV. OF SUBTASKS(EX 1,2,..)	1.2	4.2	1.7	1.2	.4	.0	.0	.0	1.34

COMMENTS

69 AT HIGH CRUISING SPEEDS, UNABLE TO TRIM. POSITIVE LAG GIVES NOSE UP INPUT TO STICK
 70 SPECTACULAR DUE TO LARGER KINETIC ENERGY OF GLIDER
 71 MUST HOLD STICK RIGID, NOT UNPLEASANT IF CONTROL TASK IS VERY
 72 OK OPEN LOOP.
 73 EXCELLENT
 74 CAN'T LET GO OF STICK
 75 IN TURBULENCE, IN THE APPROACH CONFIGURATION, FULL PILOT ATTENTION
 76 IS REQUIRED. SLOWER ROLL RATE IS NOTICEABLE, LOT OF RUDDER ACTIVITY
 77 WAS NEEDED IN THIS PHASE OF FLIGHT
 78 AT 85-90 KTS PENETRATION SPEED, QUIET EXCEPT FOR LIGHT RATTLE IN
 79 WINGS; ATTENTION TO AIRSPEED(PITCH) CONTROL LEAVES LITTLE TIME FOR
 80 SECONDARY TASKS; TURBULENCE CAUSES CONTINUAL SMALL PITCH UPSETS.
 81
 82
 83
 84
 85

SAILPLANE 6 DATA

TASK	DESCRIPTION OF TASKS	1	2	PILOT 3	4	5	6	7	AVER.	STD DEV
68	C. PILOT OPINION OF CRUISING FLIGHT	.00	.00	1.00	.00	.00	2.00	2.00	1.667	.471
69	1. EASE OF CONTROLLING AIRSPEED	.00	1.00	2.00	.00	.00	5.00	5.00	2.200	.500
70	2. PULL UP INTO THERMAL	.00	1.00	1.00	.00	.00	2.00	2.00	1.200	1.200
71	3. EASE OF PERF. SECONDARY TASKS	.00	1.00	1.00	.00	.00	2.00	2.00	1.200	.500
72	4. RIDE QUALITY	.00	2.00	1.00	.00	.00	3.00	2.00	2.200	.500
73	5. EASE OF MAIN. STRAIGHT FLIGHT	.00	1.00	2.00	.00	.00	2.00	2.00	1.750	.433
84	AVER. AND STD. DEV. OF SUBTASKS(EX 1,2,..)	.0	0.1	1.2	.4	1.8	.7	.0	.0	1.9

COMMENTS

69 EXCELLENT BE VERY MODERATE IN THIS GLIDER
 70 AIRSPEED DECREASES VERY RAPIDLY
 71 QUICK, EASY BECAUSE OF LARGE STABILITY
 72 NOT AS SOFT AS GLAS SHIP, NOISY
 73 GOOD
 74 LARGE ATTITUDE CHANGES WITH AIRSPEED; NOISY AT TIMES
 75 SAME GENERAL COMMENTS AS FOR CIRCLING FLIGHT
 76
 77

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16. Abstract Seven test pilots flew six sailplanes in a round-robin evaluation of sailplane handling qualities. An evaluation was made of the handling qualities over the sailplane operational envelope using the Cooper-Harper Rating Scale and pilot comments as the evaluation instrument. The sailplanes were chosen to represent the range of handling and performance characteristics of high performance sailplanes in current use. The evaluation sailplanes were found generally deficient in the area of cockpit layout. The pilots indicated general dissatisfaction with high pitch sensitivity especially when coupled with inertially induced stick forces. While all sailplanes were judged satisfactory for centering thermals and in the ease of speed control in circling flight, pilot opinions diverged on the maneuvering response, pull-out characteristics from a dive, and on phugoid damping. Lateral-directional control problems were noted mainly during takeoff and landing for most sailplanes with the landing wheel ahead of center of gravity. Pilot opinion of in-flight lateral-directional stability and control was generally satisfactory. Five of the evaluation sailplanes exhibited a very narrow airspeed band in which perceptible stall warning buffet occurred. However, this characteristic was considered not objectionable when stall recovery was easy. The pilots objected to the characteristics of a wide airspeed band of stall warning followed by a stall with yawing and rolling tendency and substantial loss of altitude during the stall. Glide path control for the evaluation sailplanes was found to be generally objectionable.					
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