

(NASA-CR-135239-Vol-1-Sect-3)	ACOUSTIC	N78-28096
TESTS OF DUCT-BURNING TURBOFAN JET NOISE		
SIMULATION: COMPREHENSIVE DATA REPORT.		
VOLUME 1, SECTION 3: DATA PLOTS Final		Unclas
Report (General Electric Co.) 520 p	G3/07	27186

ACOUSTIC TESTS of DUCT-BURNING TURBOFAN JET NOISE SIMULATION

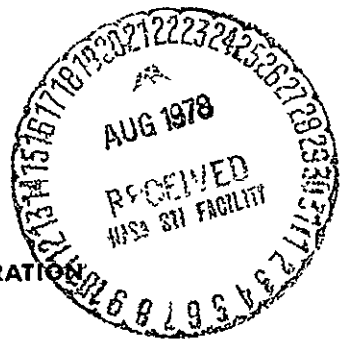
COMPREHENSIVE DATA REPORT

VOLUME I

SECTION III
DATA PLOTS

- P.H. HECK
- D. LATHAM
- J.F. BRAUSCH
- E.J. STRINGAS
- P.S. STAID
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General Electric



NATIONAL AERONAUTICS AND SPACE ADMINISTRATION
 LEWIS RESEARCH CENTER
 21000 BROOKPARK ROAD
 CLEVELAND, OHIO 44135

NASA CONTRACT: NAS3-18008



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TABLE OF CONTENTS

Volume I

<u>Section I</u>		<u>Page</u>
1.0	INTRODUCTION	1
2.0	TEST SPECIFICATIONS	3
3.0	ACOUSTIC DATA	23
	A. Test Conditions	26
	B. 12.2 m (40 ft) Arc Data	39
<u>Section II</u>		
	C. 96.9 m (320 ft) Radial - Scaled	443
	D. 731.5 m (2400 ft) Sideline - Scaled	443
<u>Section III</u>		
4.0	ACOUSTIC PLOTS	1245
	4.1 Acoustic Comparison of Various Nozzle Models at Selected Test Conditions for a Full Size Engine	1247
	4.2 Acoustic Data Plots for a Full Size Engine Utilizing a Scale Factor of 8	1309
5.0	ON-LINE NARROWBANDS	1611
6.0	AERODYNAMIC DATA FORMAT - ACOUSTIC TESTS	1667
7.0	LASER DATA RECORDING	1675
8.0	STATIC PRESSURES - ACOUSTIC MODELS	1691

Volume II

Part 1.	"Concept Screening and Model Design for Acoustic Tests of Duct-Burning Turbofan Jet Noise Simulation," J.F. Brausch and P.S. Staid, General Electric AEG TM-74-270, June 1974.
Part 2.	"Hot/Cold Flow Model Tests to Determine Static Performance of Duct Noise Suppression Nozzles," R.A. Kirschbaum and R.G. Brasket, Fluidyne Engineering Corporation Report 1008, July 1974.

4.0 ACOUSTIC PLOTS

4.1 Acoustic Comparison of Various Nozzle Models at Selected Test Conditions for a Full Size Engine

The data from the full size engine utilizing a scale factor of 8 was plotted for $V_f/V_c \geq 1.5$ at 3 test conditions corresponding to acoustic test matrix points of X 13, X 15, X 25 (where X is the model designation in Section 3.0 (a) of CDR Volume I. These were included in the Final Report, NASA CR 2966, in reduced form. The following plots are in original size for easier detailed analysis. The plots include:

- OASPL directivity
- PNL directivity
- PWL spectra
- SPL spectra at 50°, 90°, 130° and angle corresponding to max.PNL

The solid lines in the OASPL and PNL directivity curves represent a synthesized conical nozzle.

4.2 Acoustic Data Plots for a Full Size Engine Utilizing a Scale Factor of 8

The following plots are presented for a full size engine utilizing a scale factor of 8. GE high frequency atmospheric attenuation factors have been used.

Ground reflection corrections have been applied to the model data prior to scaling.

The spectral data is presented on the basis of 1/3 octave band analysis.

The angular distribution of overall sound pressure levels and perceived noise levels are presented at a microphone location consistent with a FAR36 regulation monitoring location - 2128 ft (648.6 m) sideline and 1110 ft (338.3 m) altitude.

Four types of figures have been used per configuration to present the acoustic data.

The first set of figures shows the effect of velocity and temperature on sound power generation as indicated by sound power level spectra.

The second set shows the effect of velocity and temperature upon sound generation as indicated by overall sound pressure level sideline directivities

The third set shows the effect of velocity and temperature upon noise generation as indicated by changes in perceived noise level along the sideline.

The fourth set shows the effect of velocity and temperature upon sound propagation as indicated by sound pressure level spectra at 50°, 90°, and 130°.

The plots demonstrate the effect of four basic parameters; fan velocity, core velocity, fan stream temperature and core stream temperature. Some general observations relating to these parameters can be made in terms of the power level spectra. The unsuppressed configurations, (Models 7 and 8), have little variation in their spectra when $V_f/V_c \lesssim 1.0$. The sound power is basically core stream controlled and peaks at low frequencies. When $V_f/V_c > 1.0$, then a second frequency peak occurs at mid frequencies. This is attributed to the high fan radius ratio effects. When the fan stream temperature is increased, sound power levels were reduced, but conversely increases in the core stream temperature leads to small increases in sound power level. The suppressed configurations follow similar trends except that increasing the fan velocity increases the sound power more predominantly in the mid to high frequency regime.

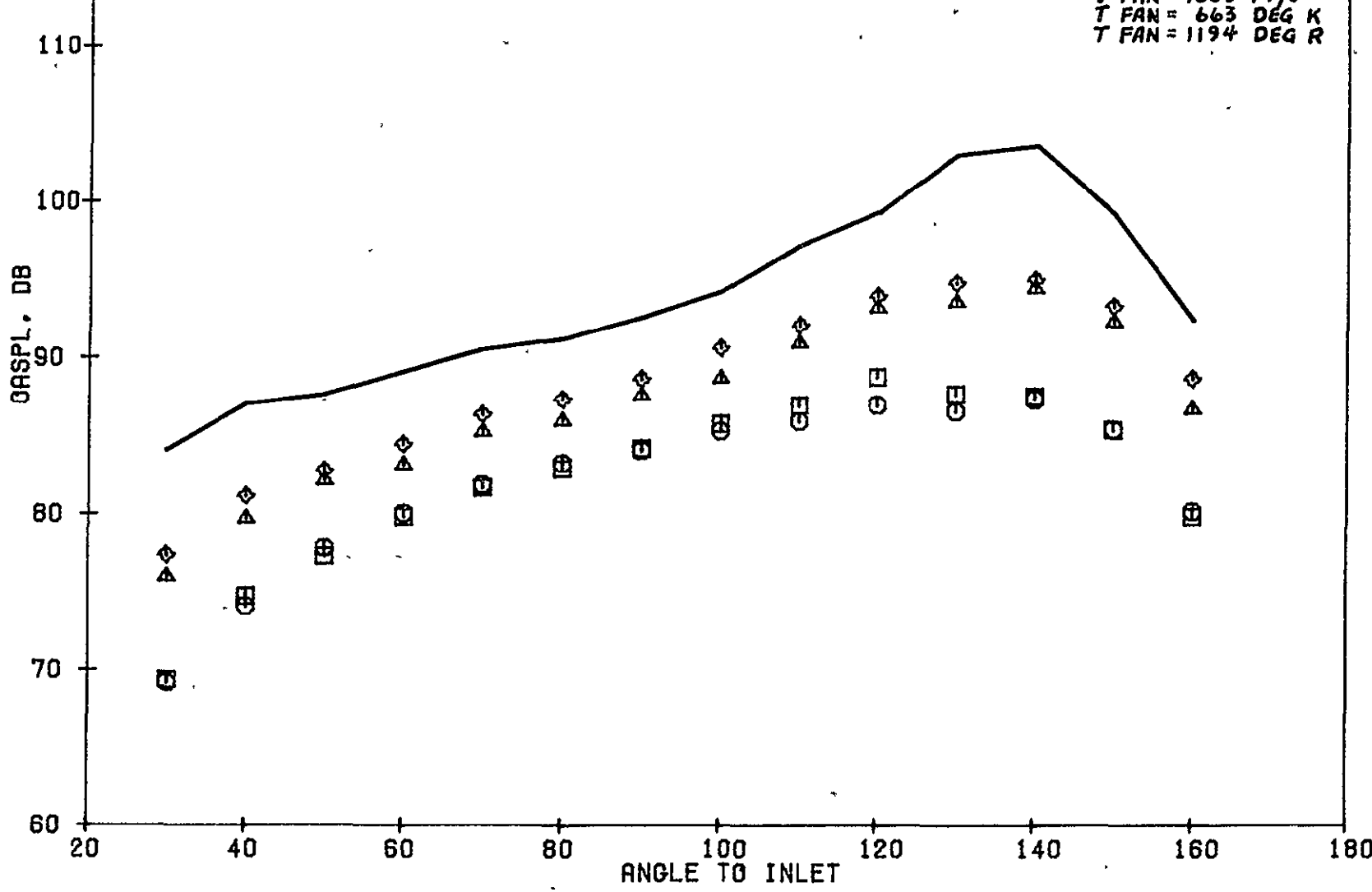
4.1 ACOUSTIC COMPARISON OF VARIOUS NOZZLE MODELS AT
SELECTED TEST CONDITIONS FOR A FULL SIZE ENGINE

V CORE = 368 M/S
 Y CORE = 1208 FT/S
 T CORE = 556 DEG K
 T CORE = 1000 DEG R

DBTF CONFIGURATION EFFECT
 GASPL VS ANGLE
 649 M. S.L. 338 M. ALT.
 2128 FT. S.L. 1110 FT. ALT.

◇ CONFIO. 8 - PT 13
 ▲ CONFIO. 7 - PT 13
 □ CONFIO. 1 - PT 13
 ○ CONFIO. 2 - PT 13

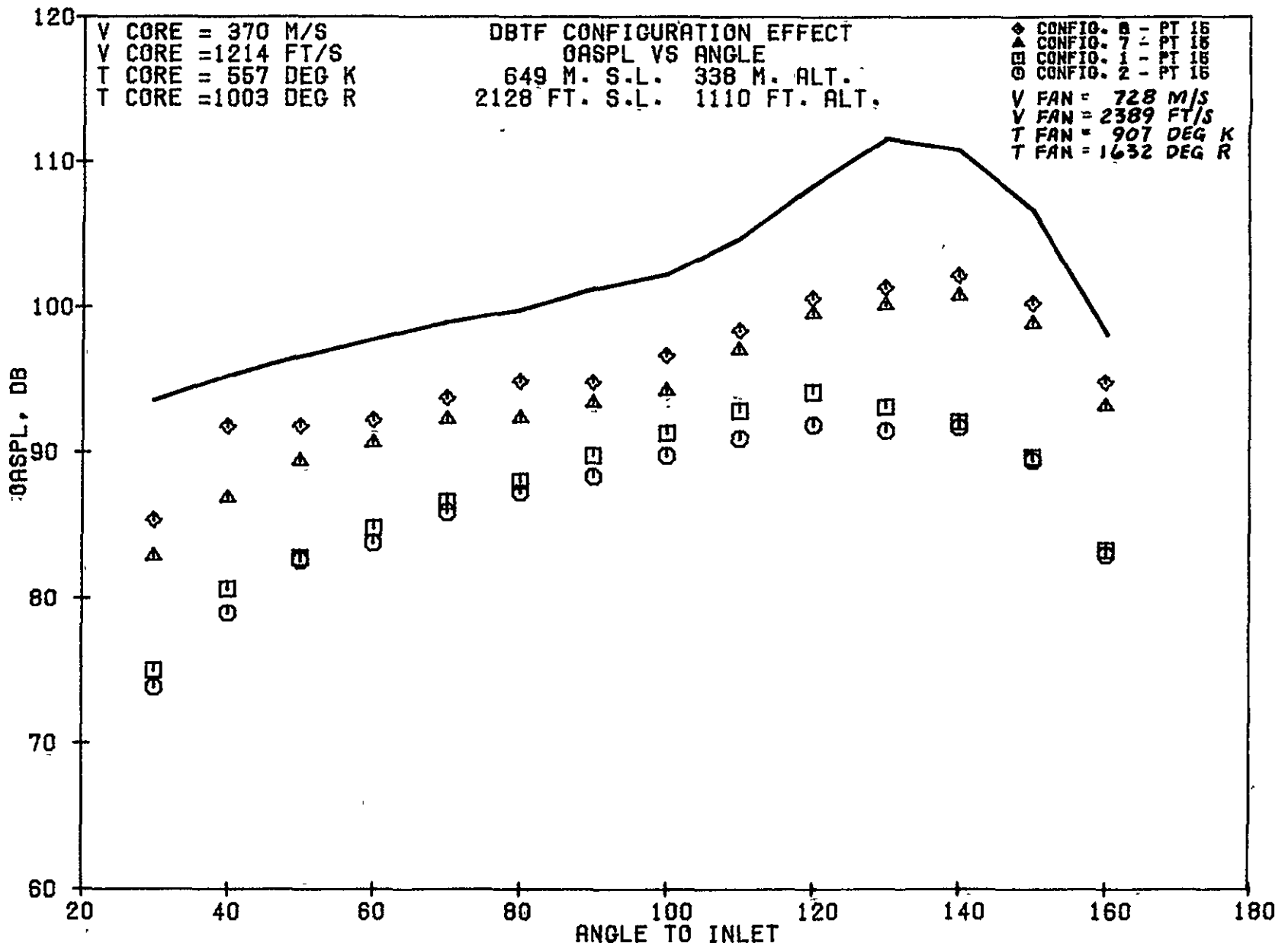
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 V FAN = 1803 FT/S
 T FAN = 663 DEG K
 T FAN = 1194 DEG R



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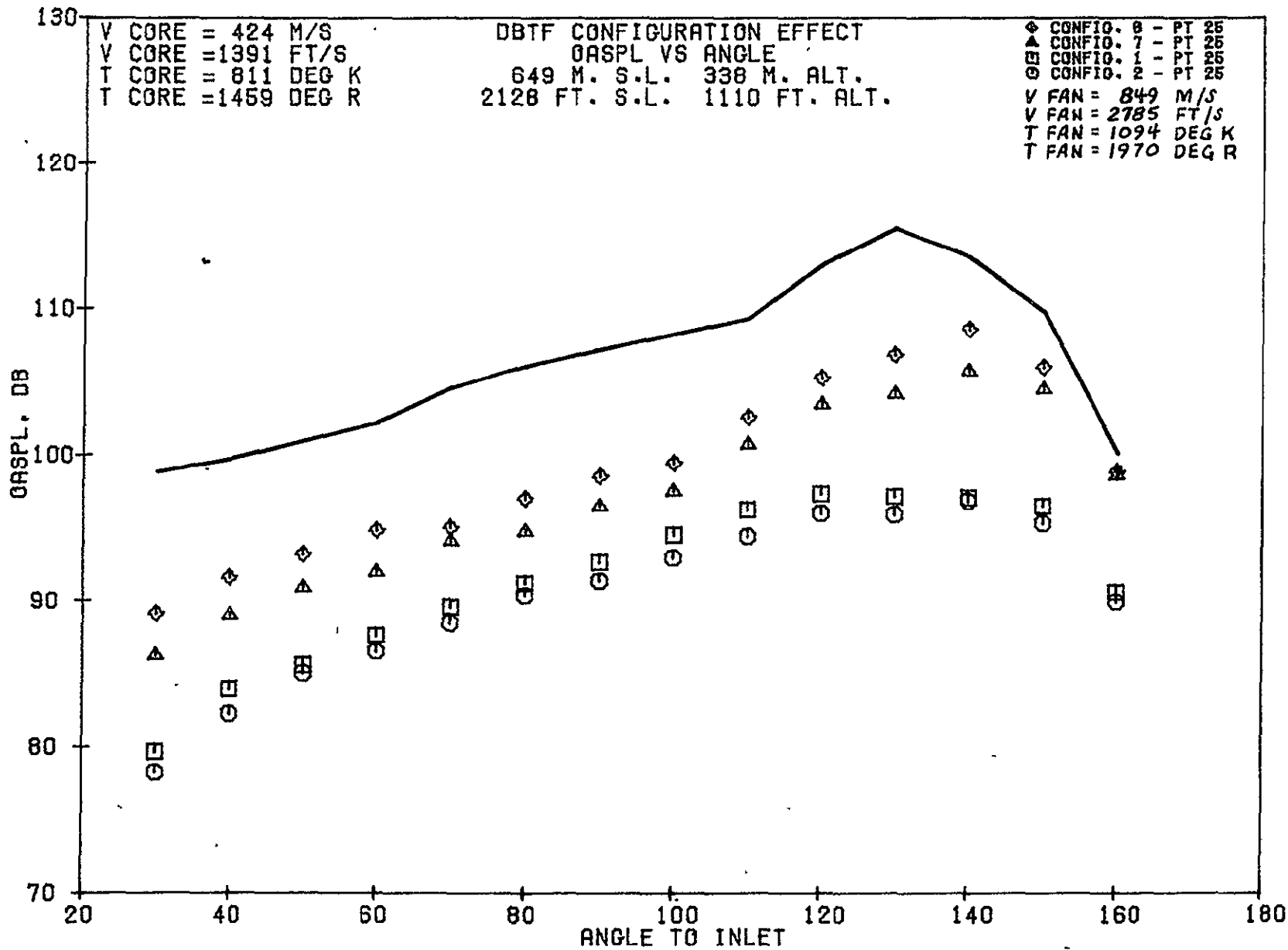


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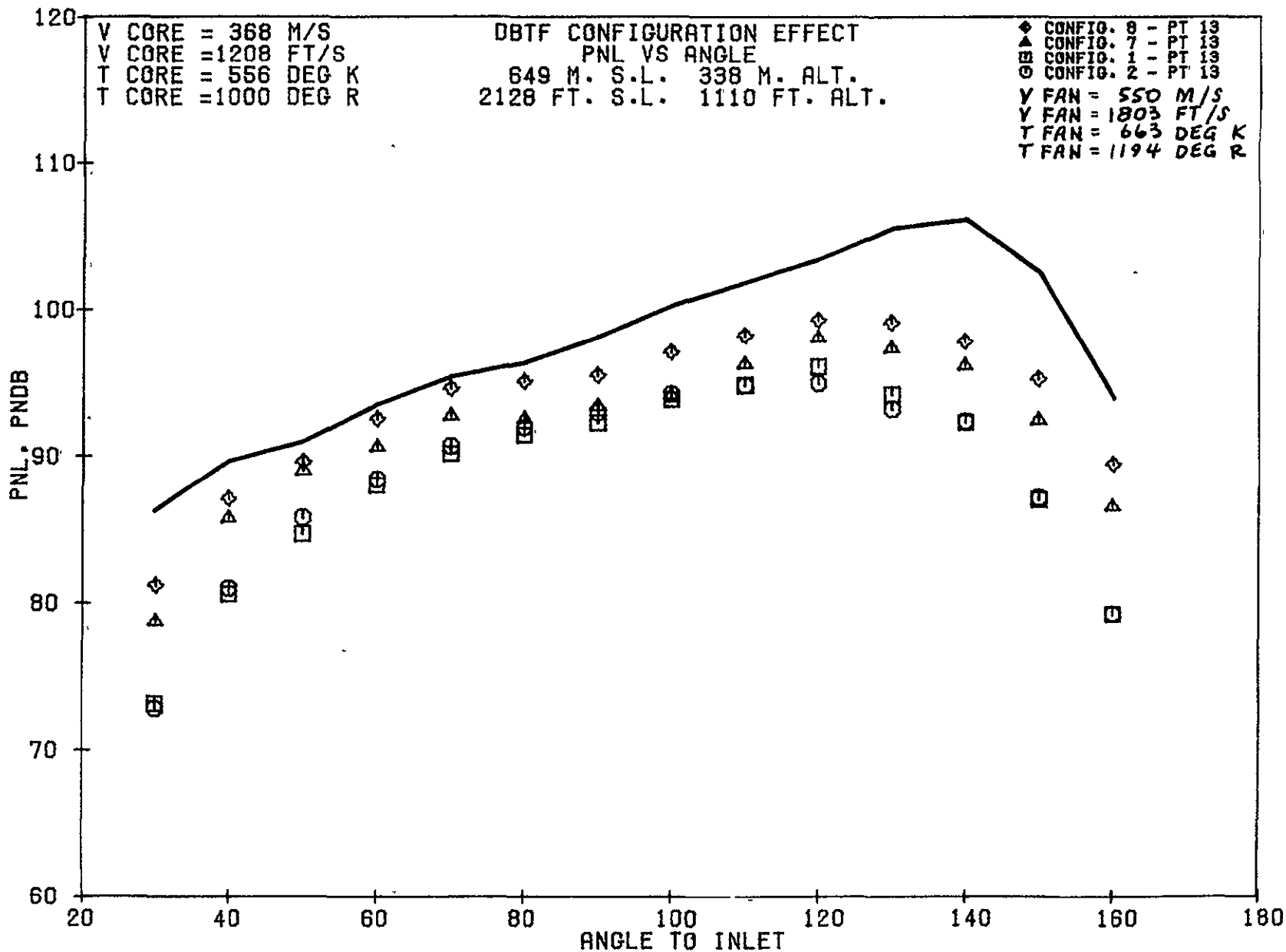
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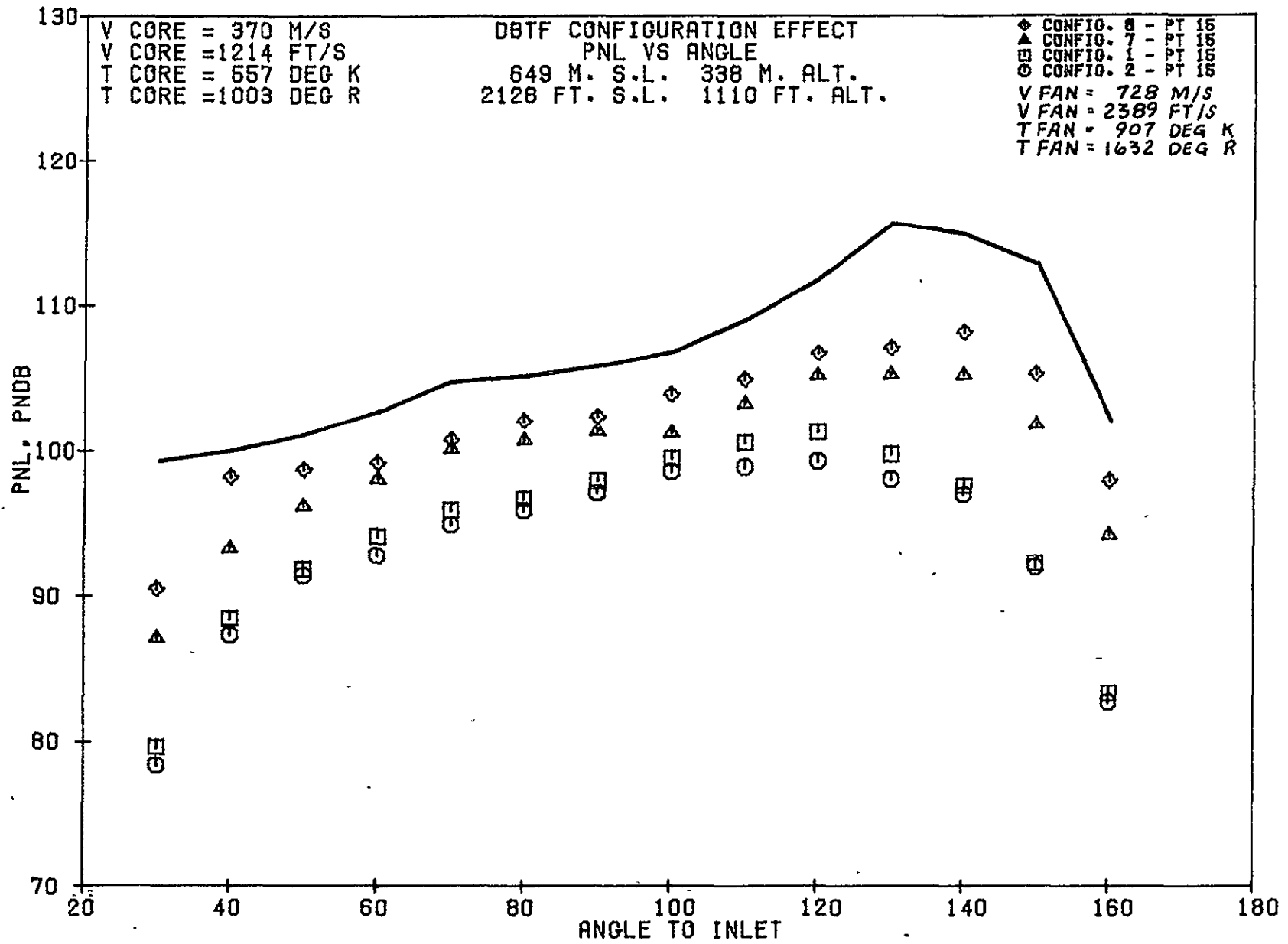
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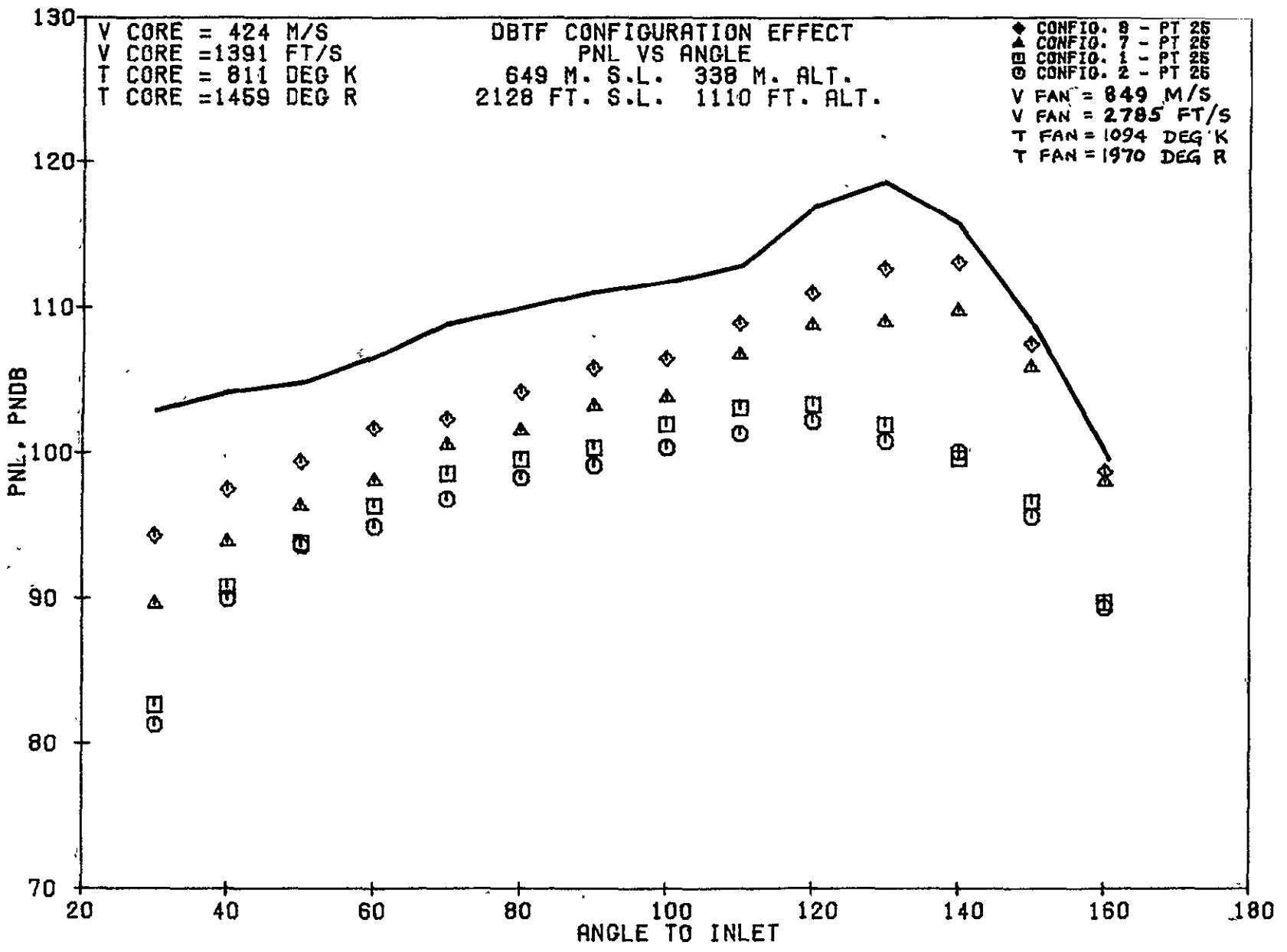
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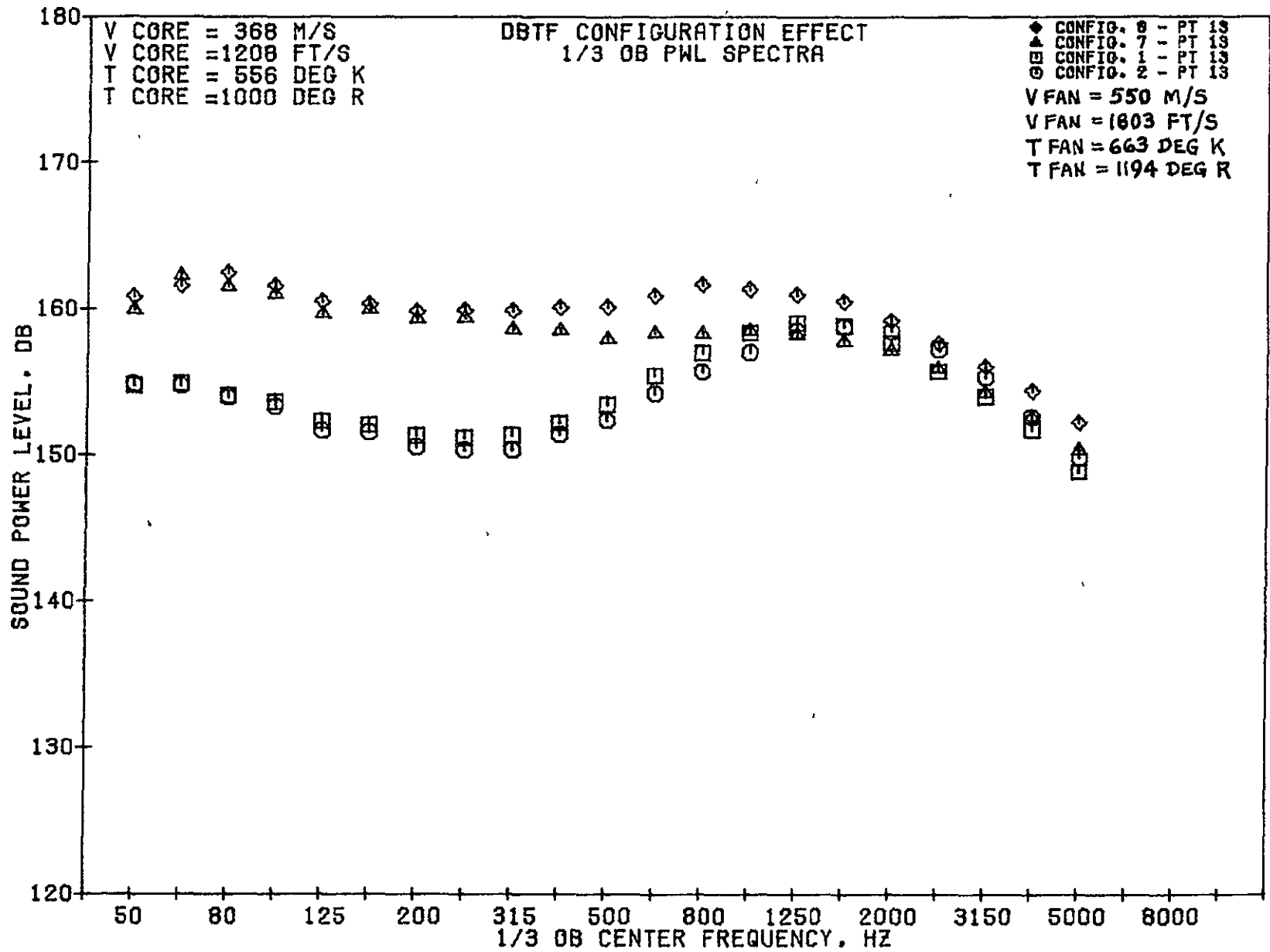
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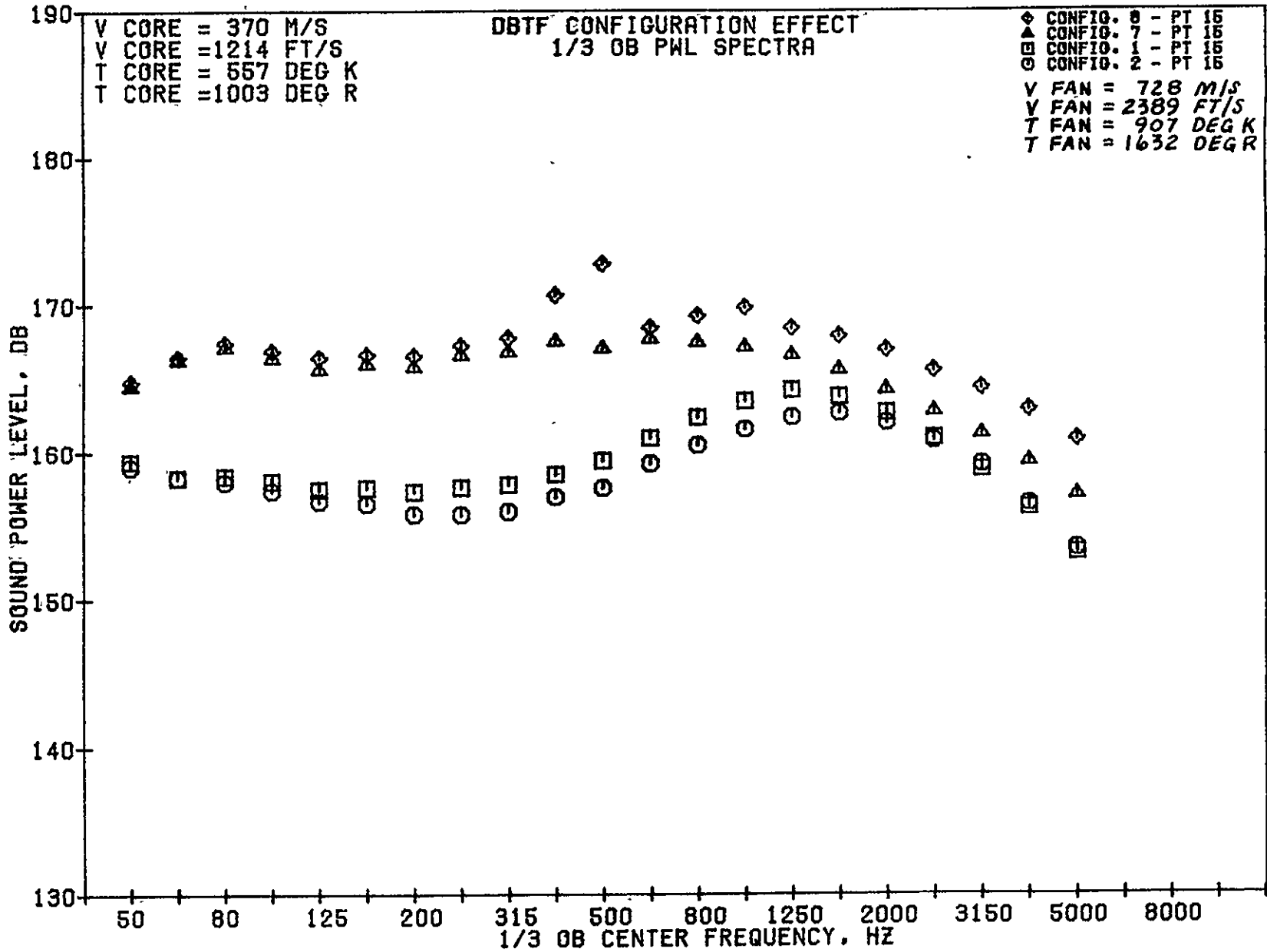
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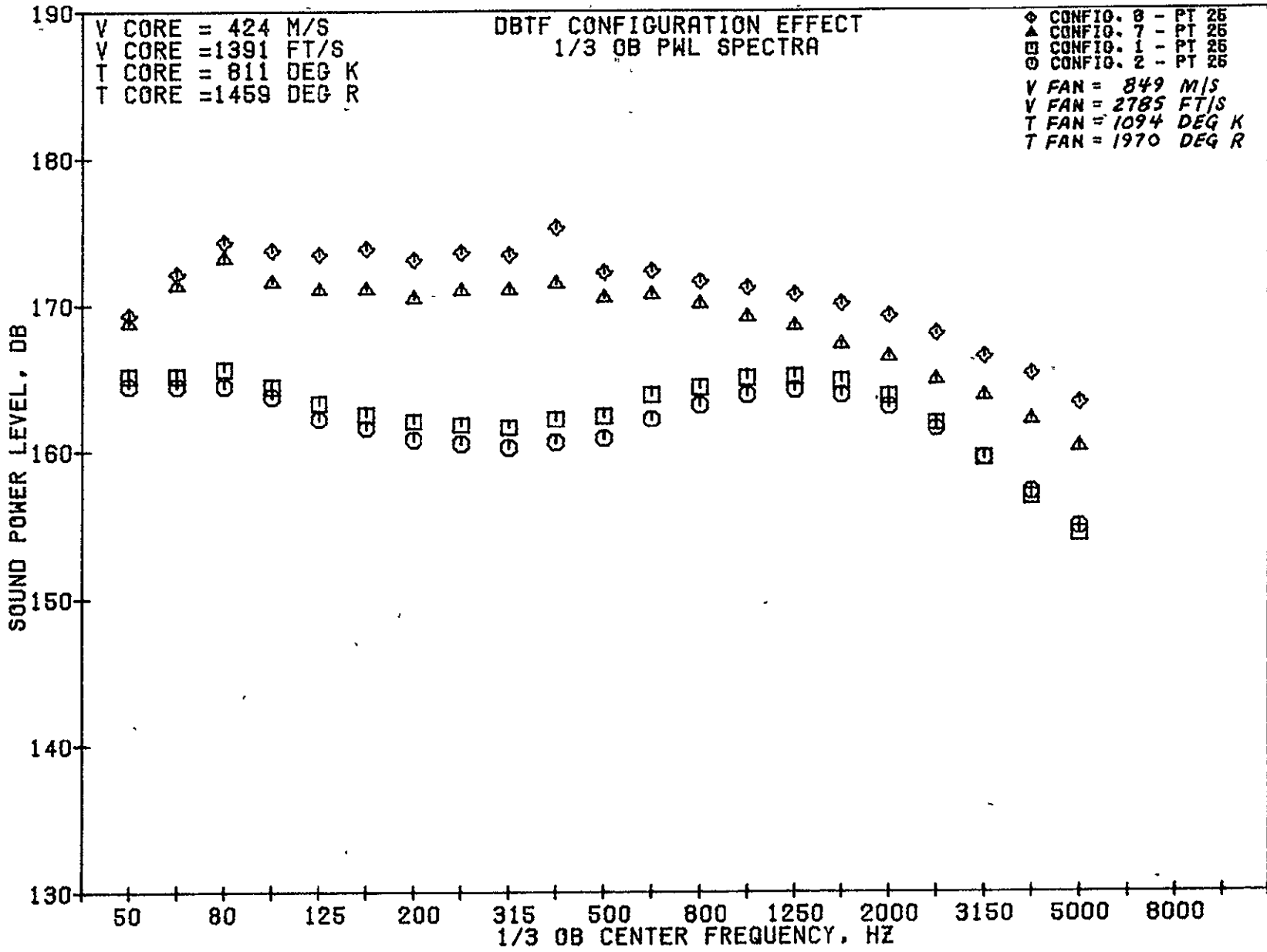


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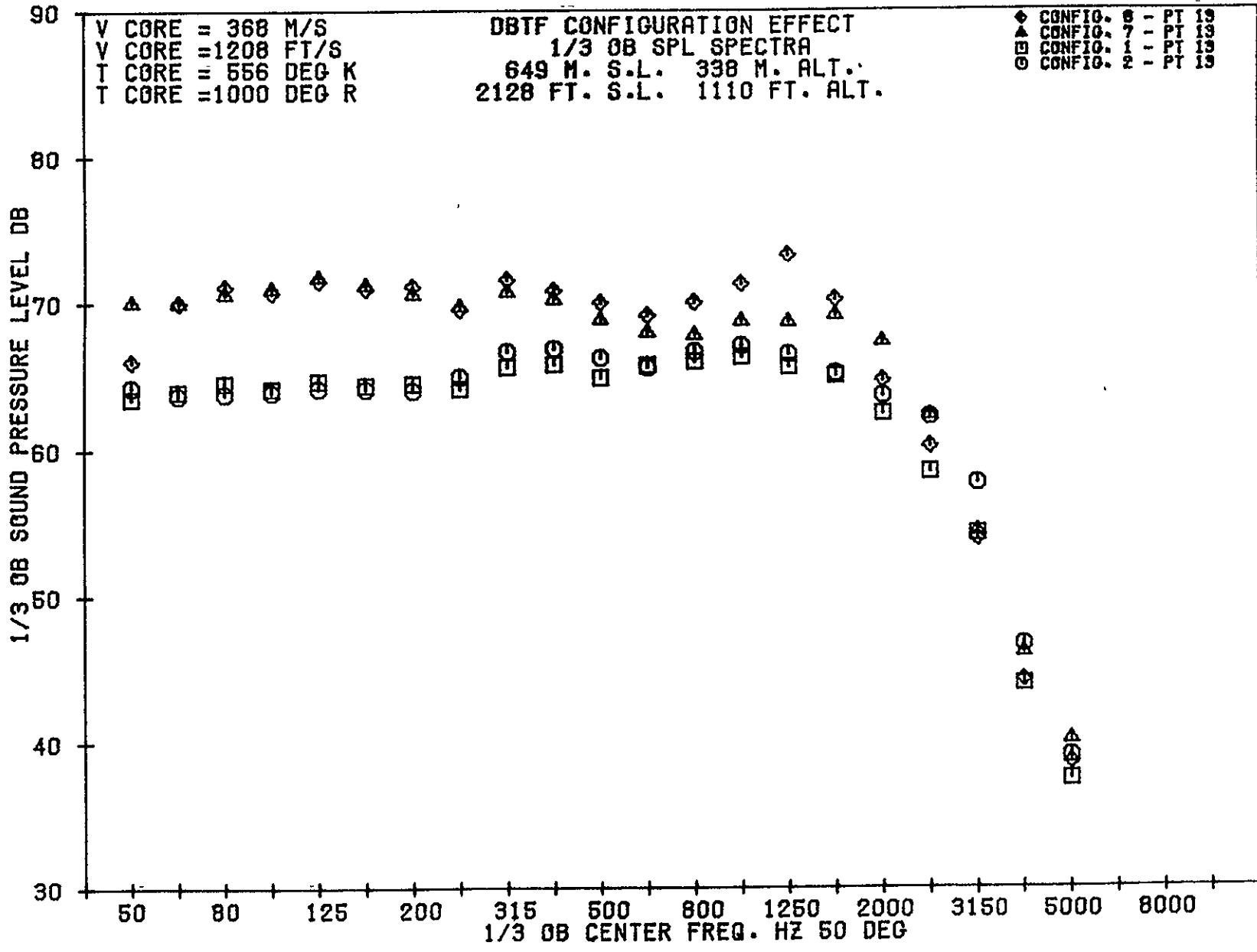
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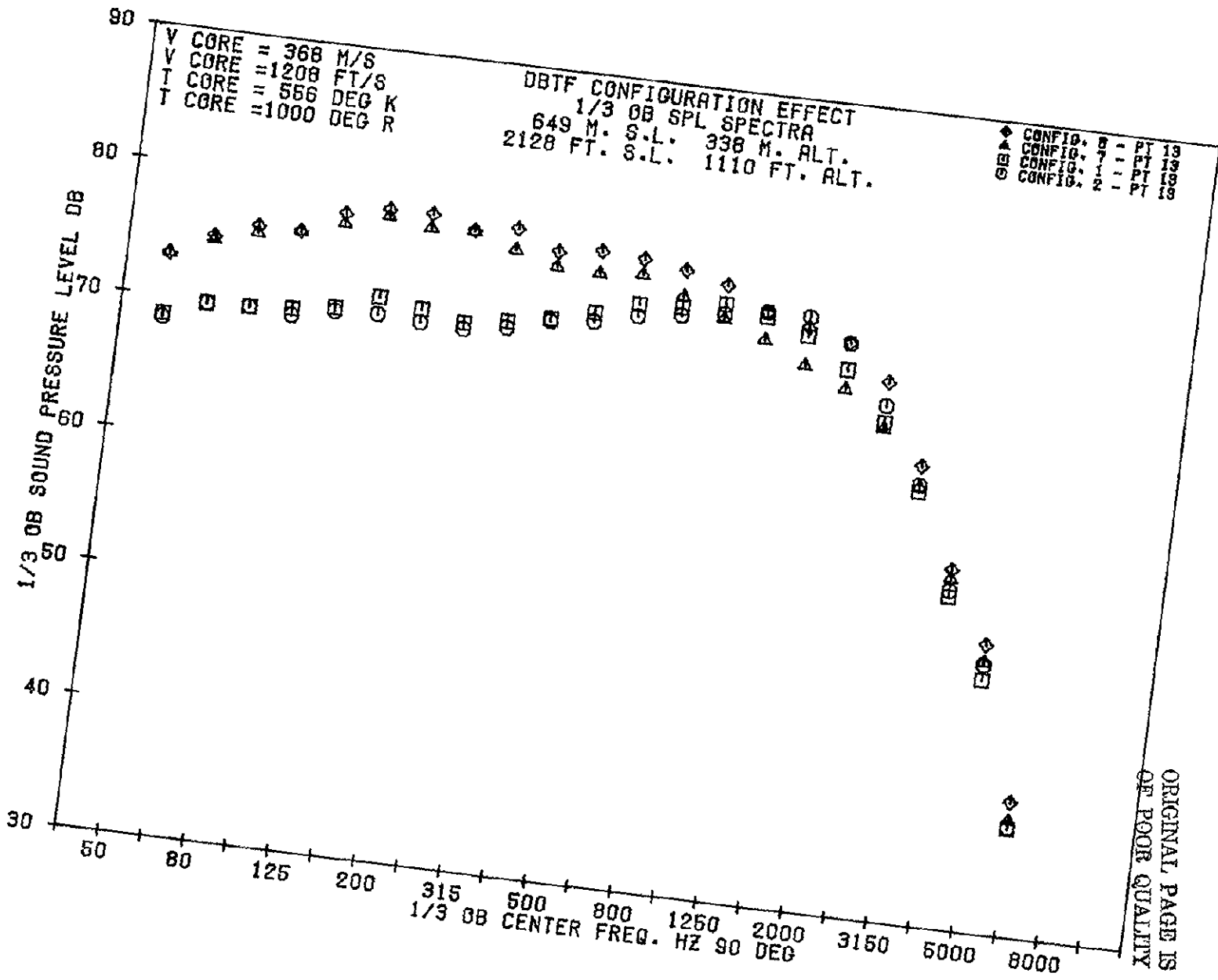


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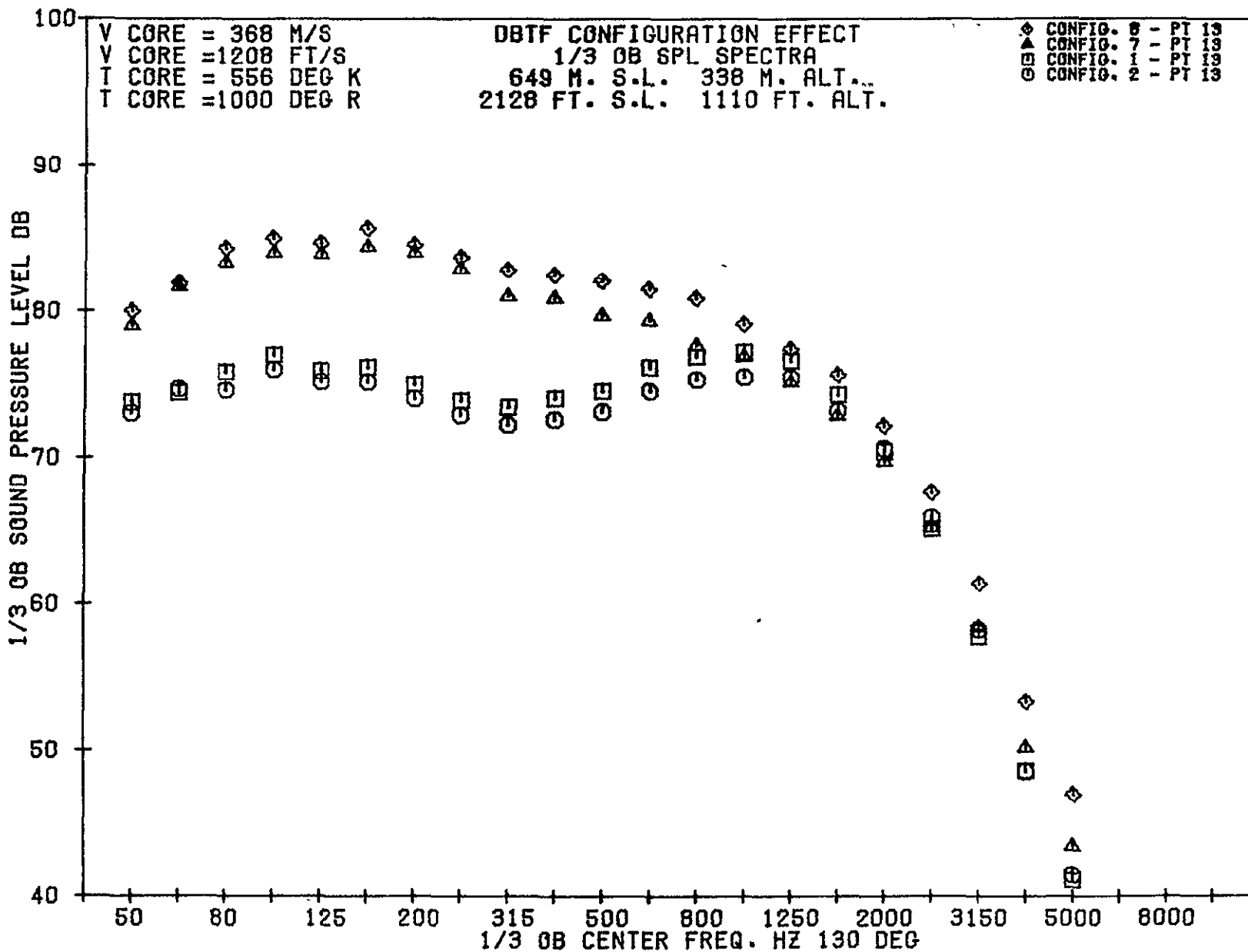
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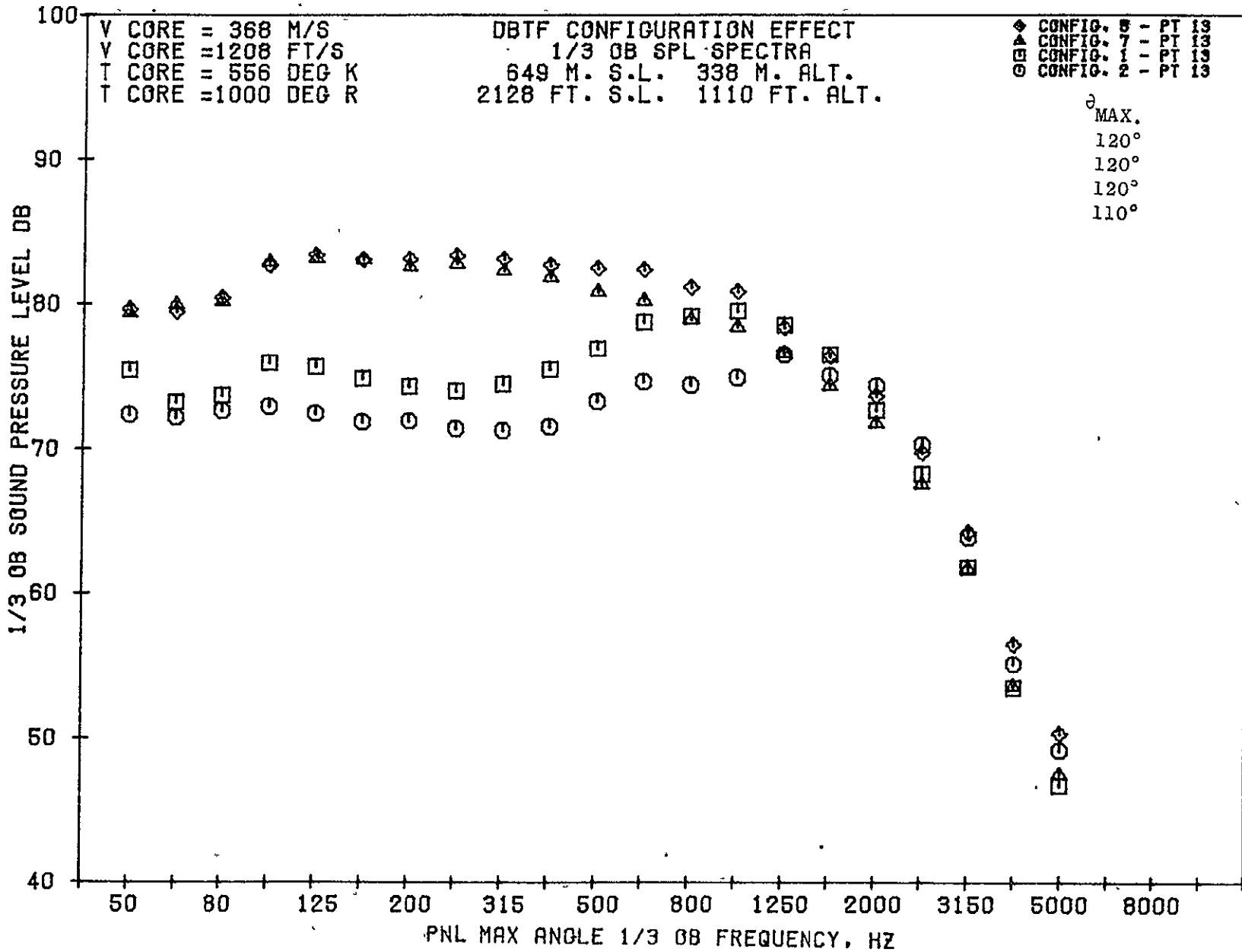
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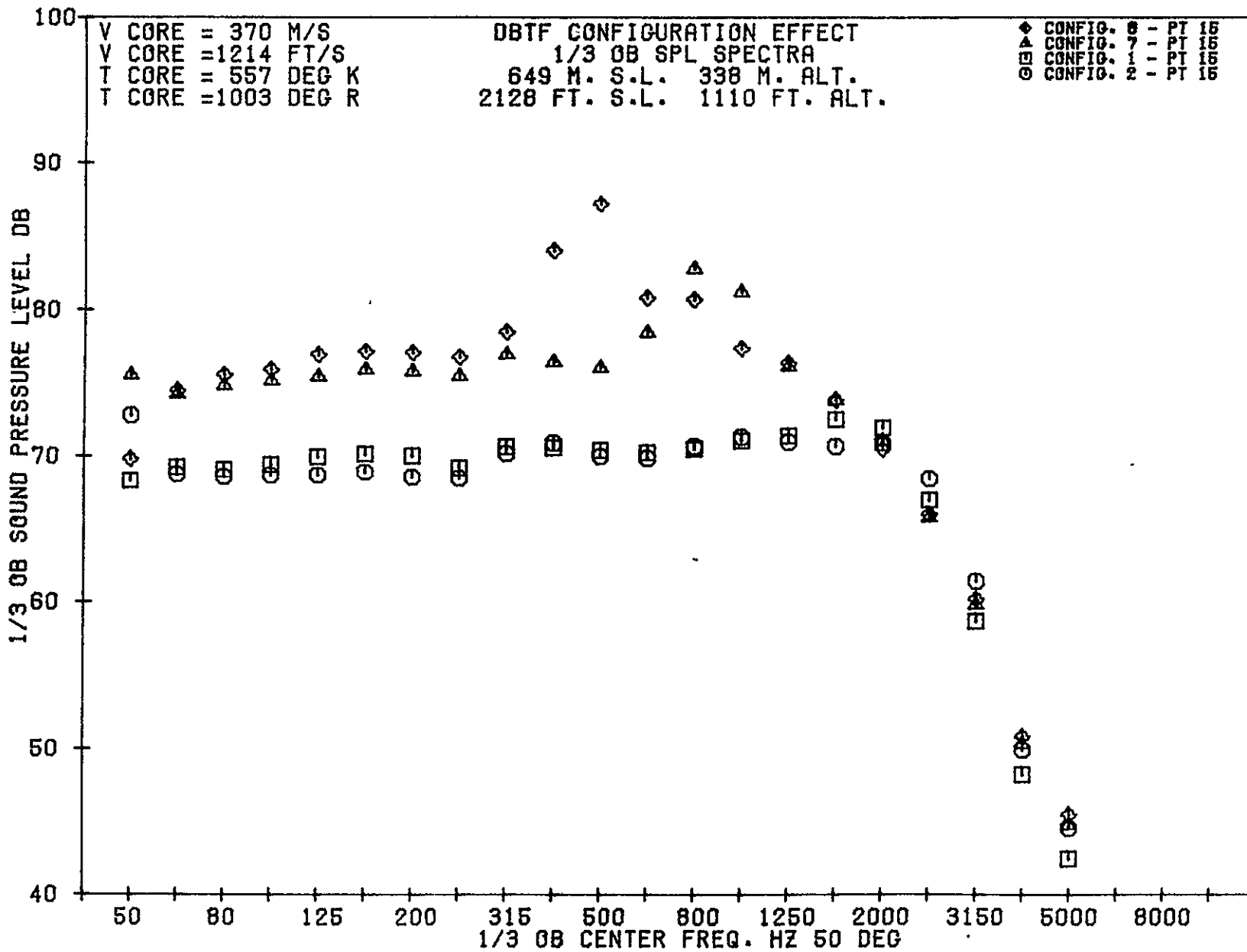


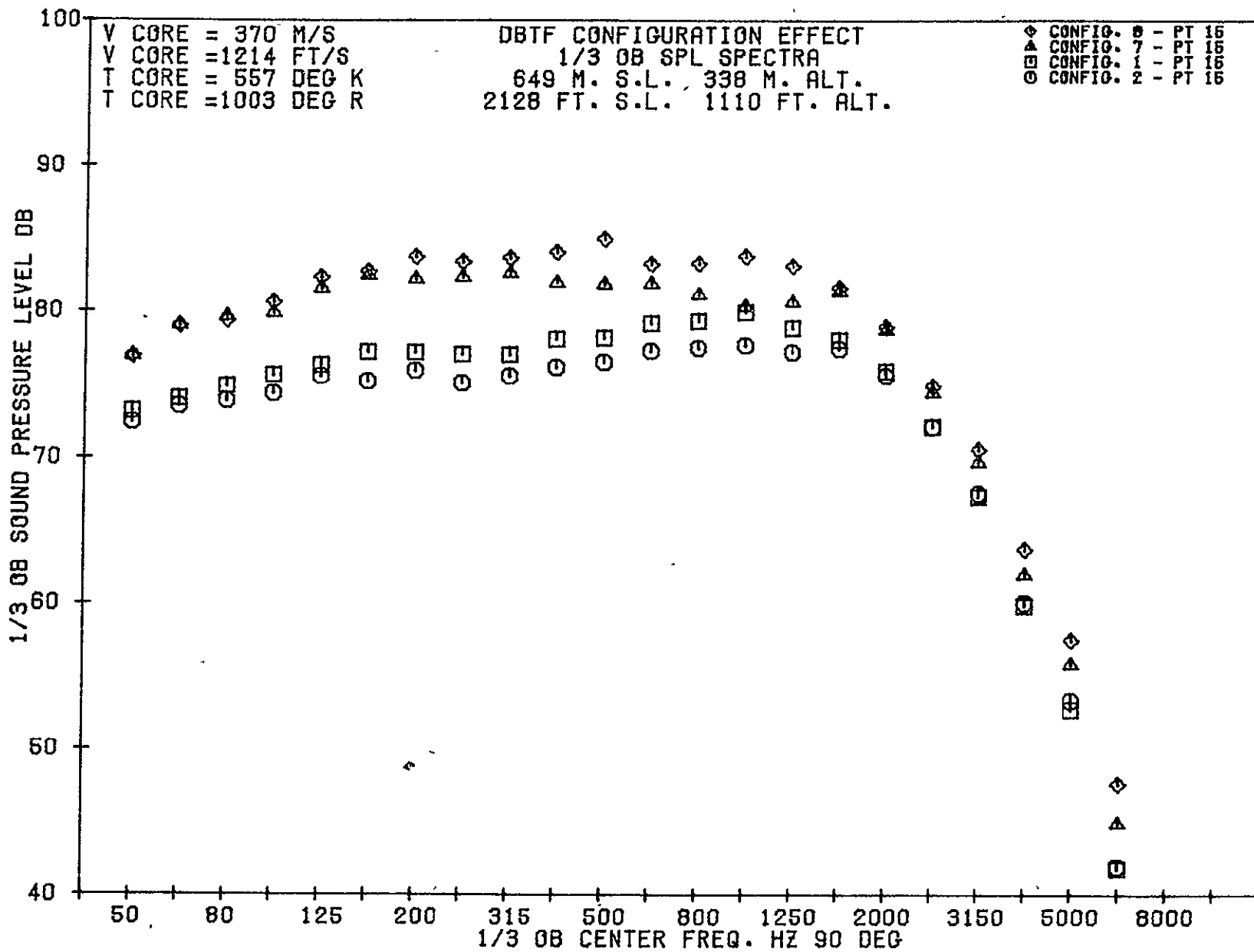
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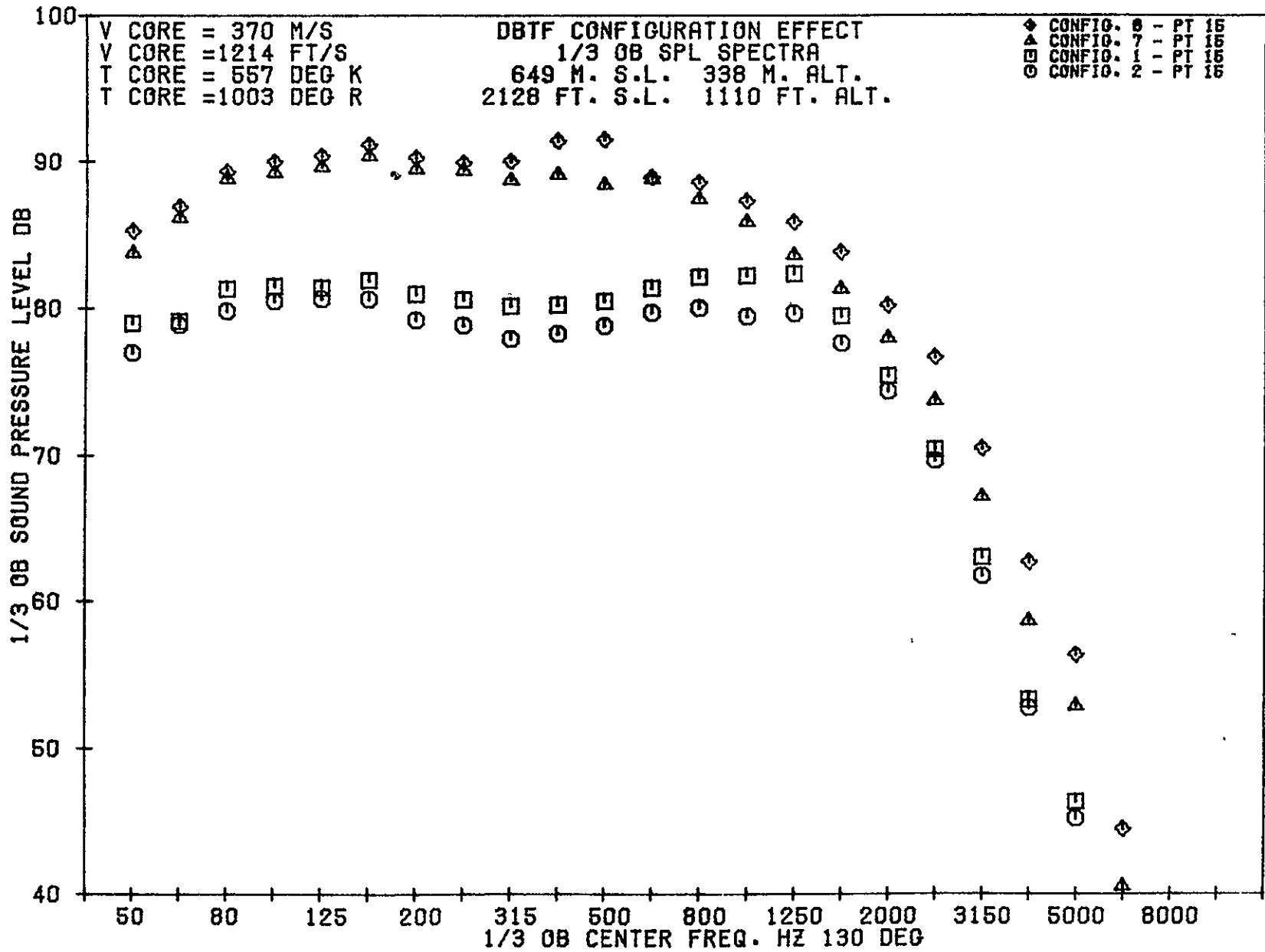




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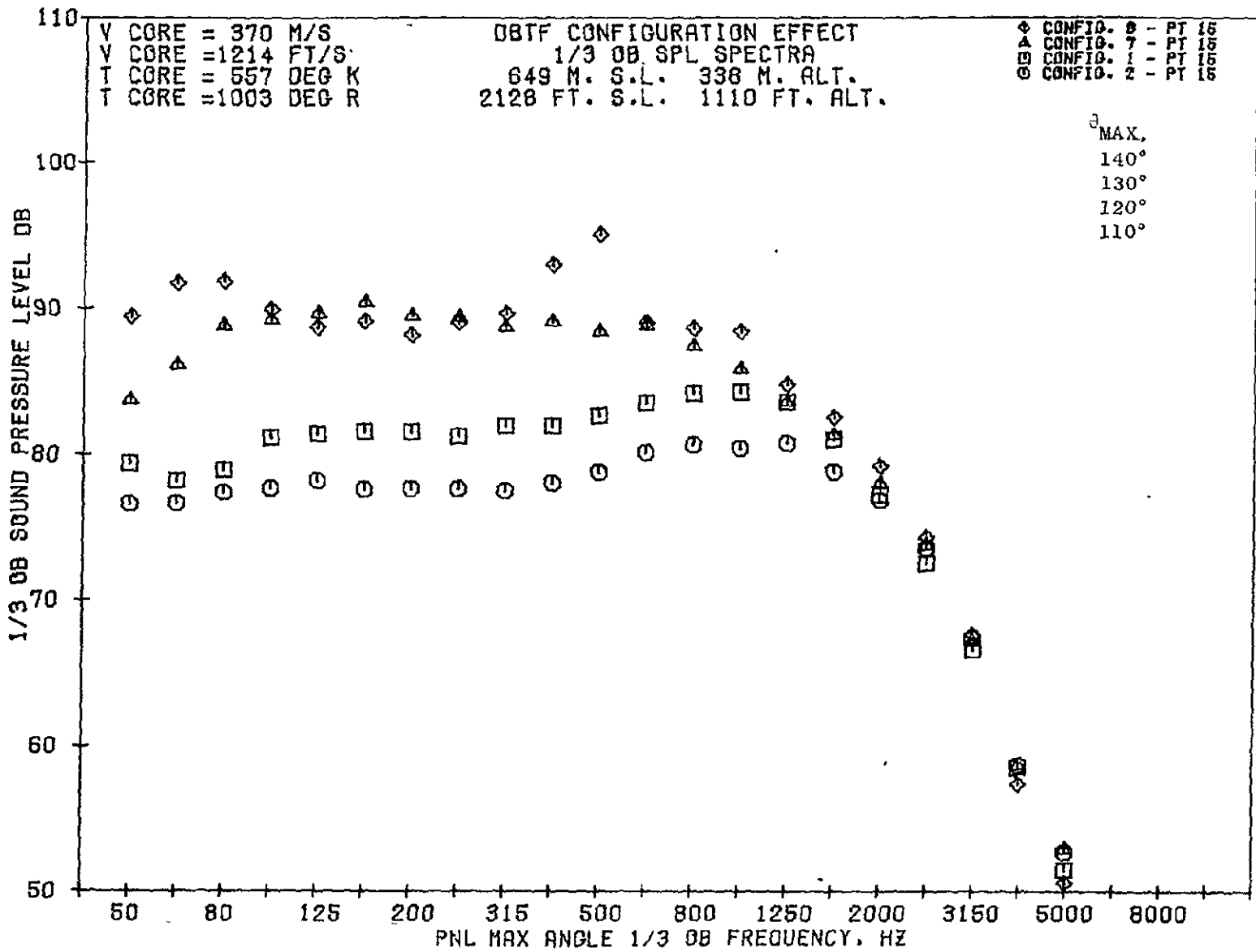
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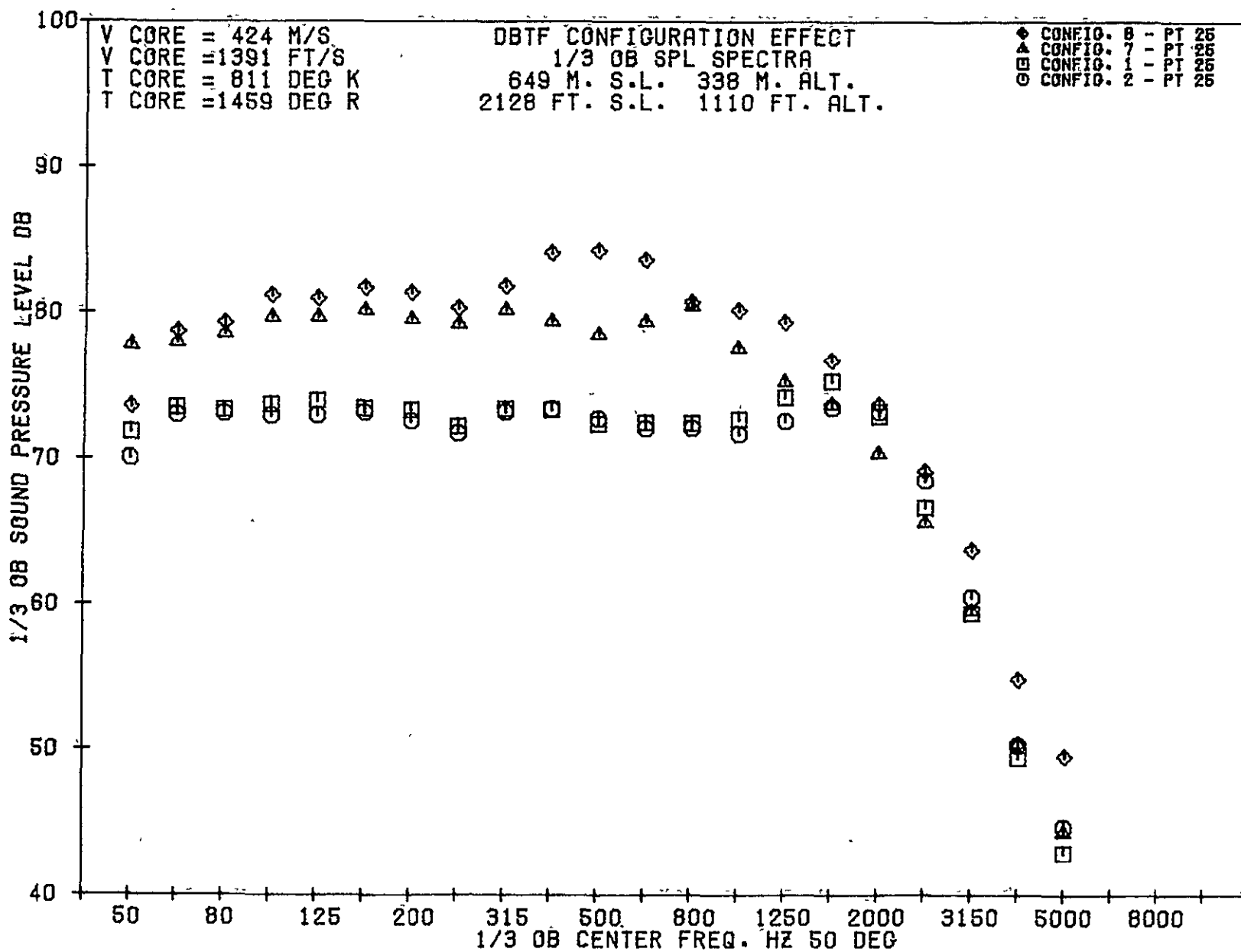
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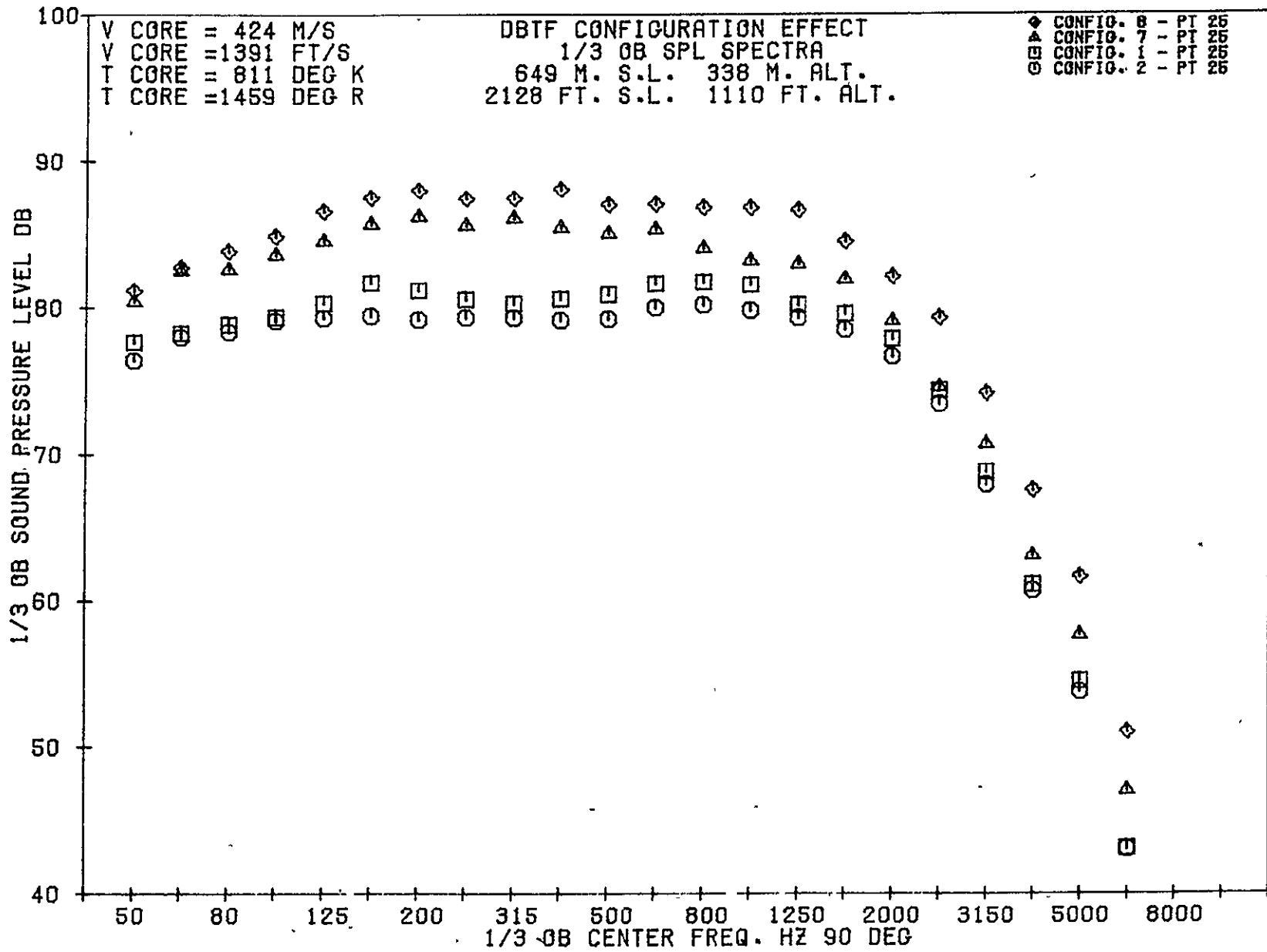
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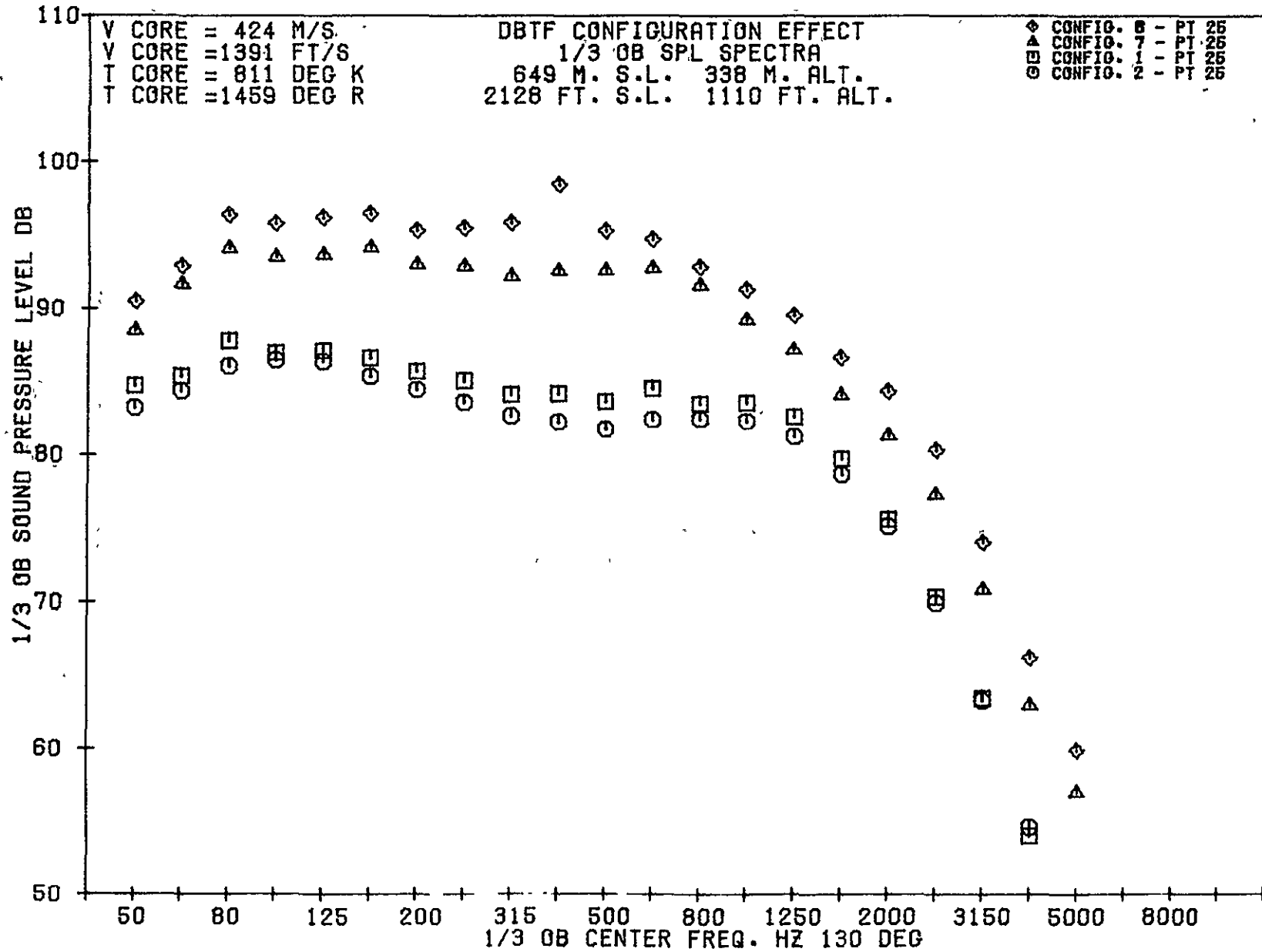
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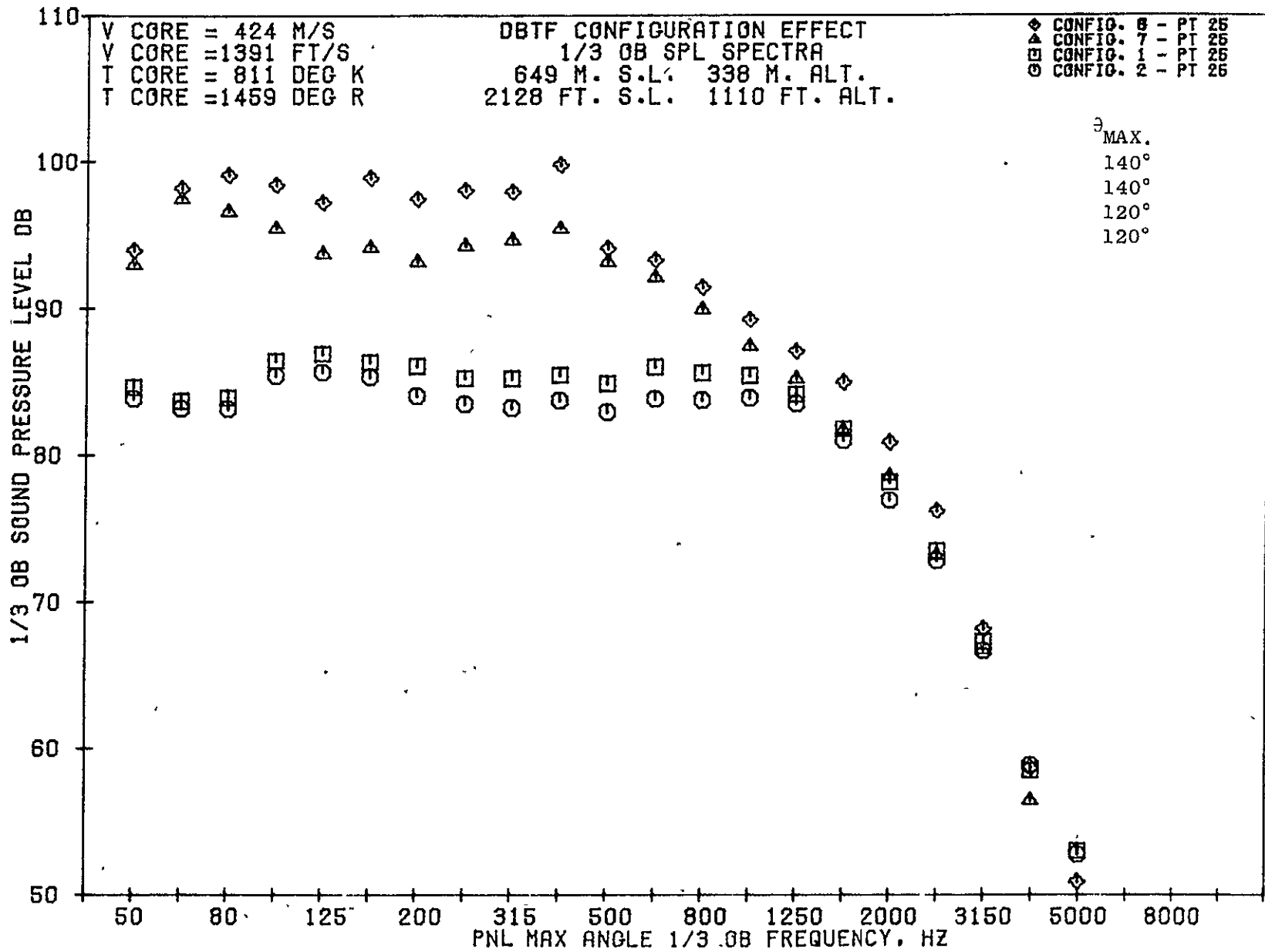


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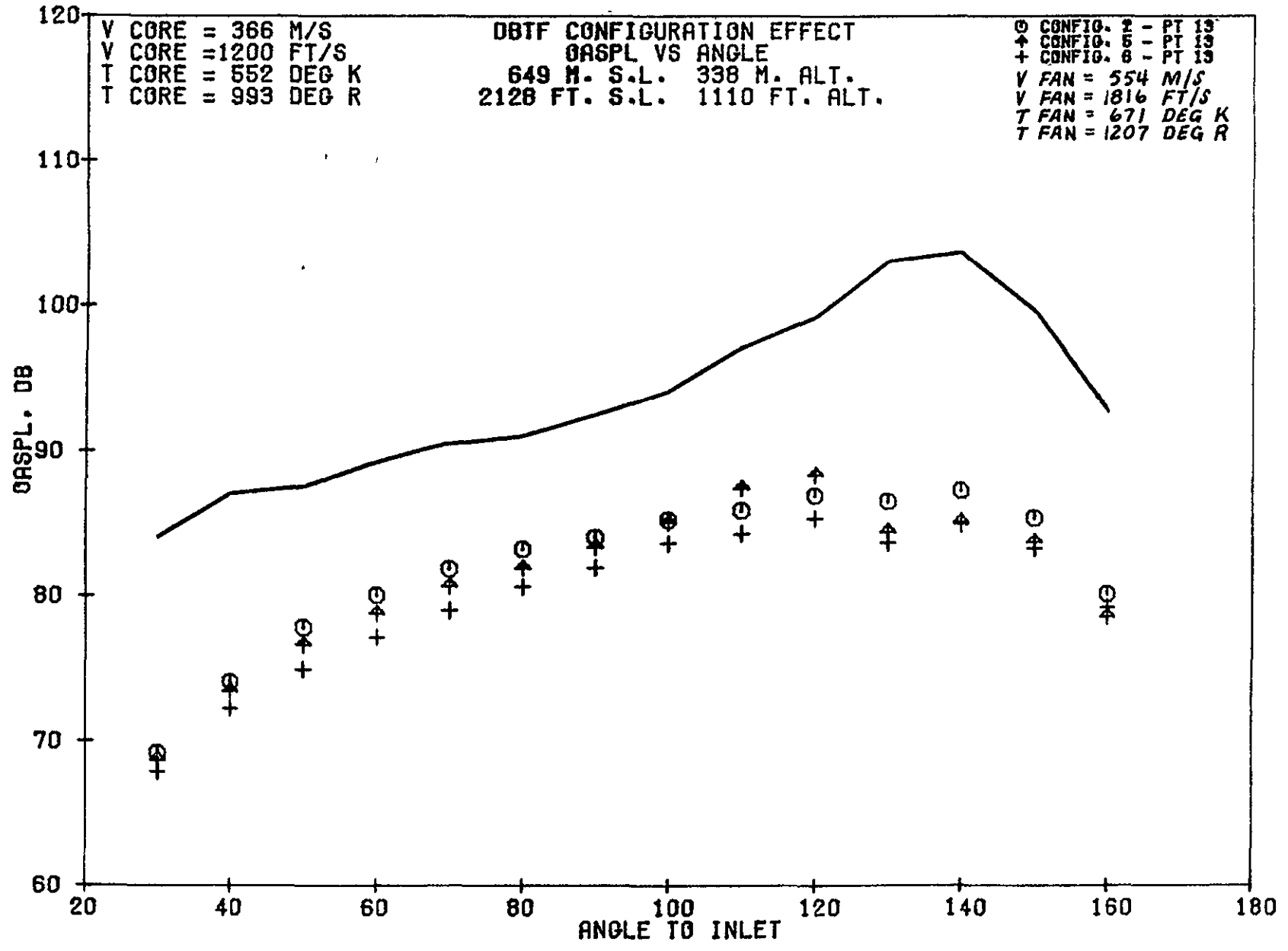
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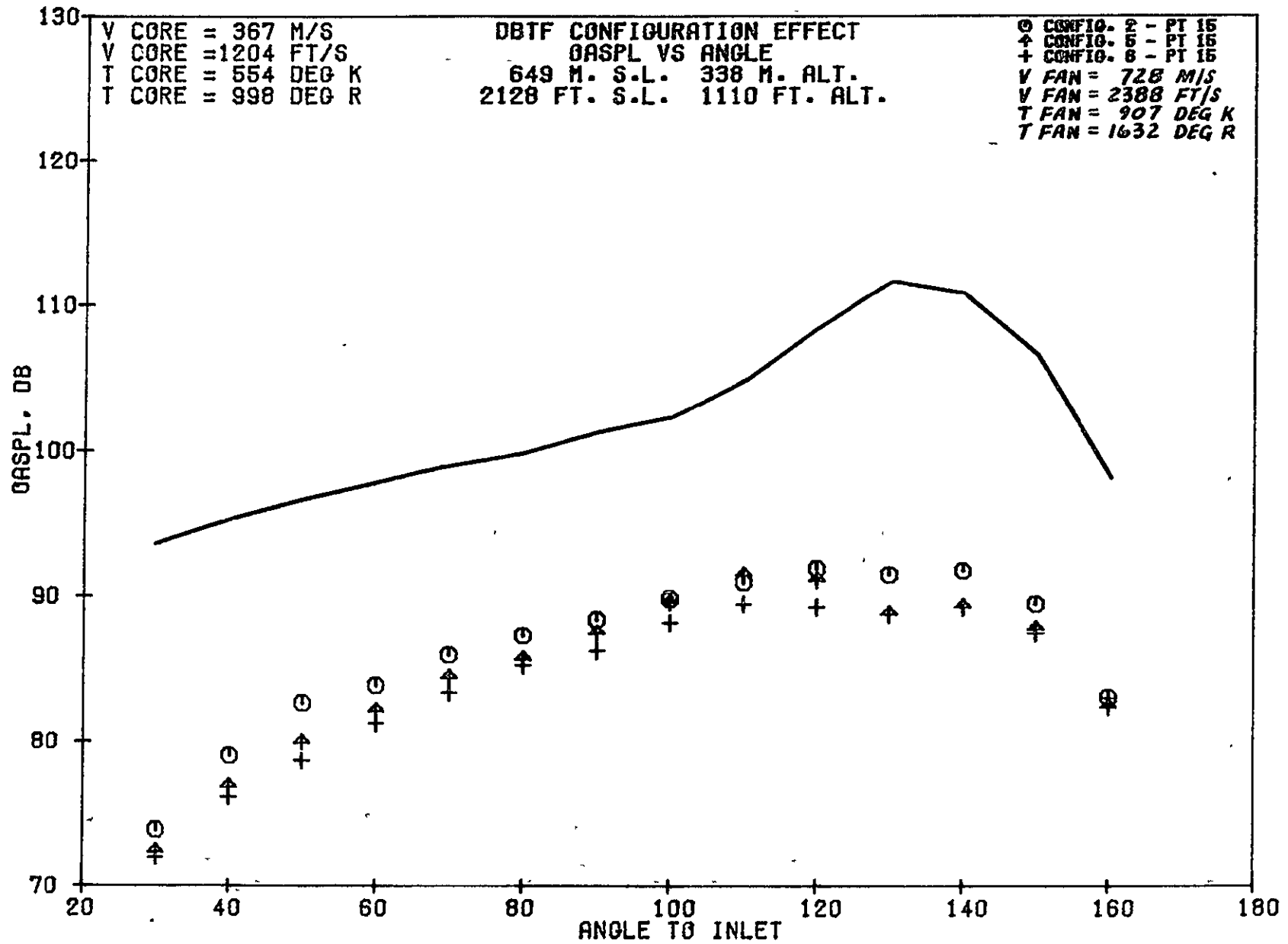
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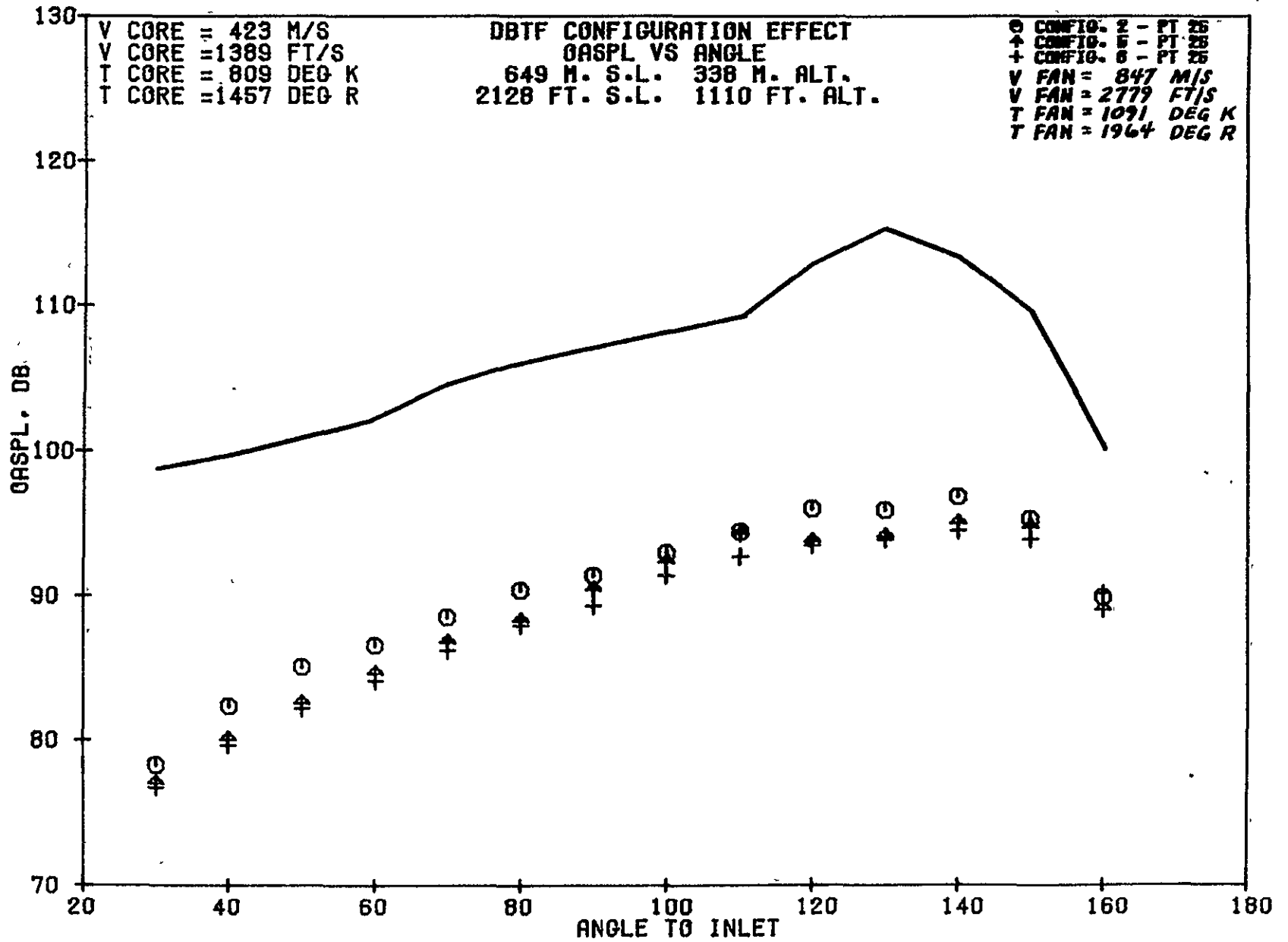


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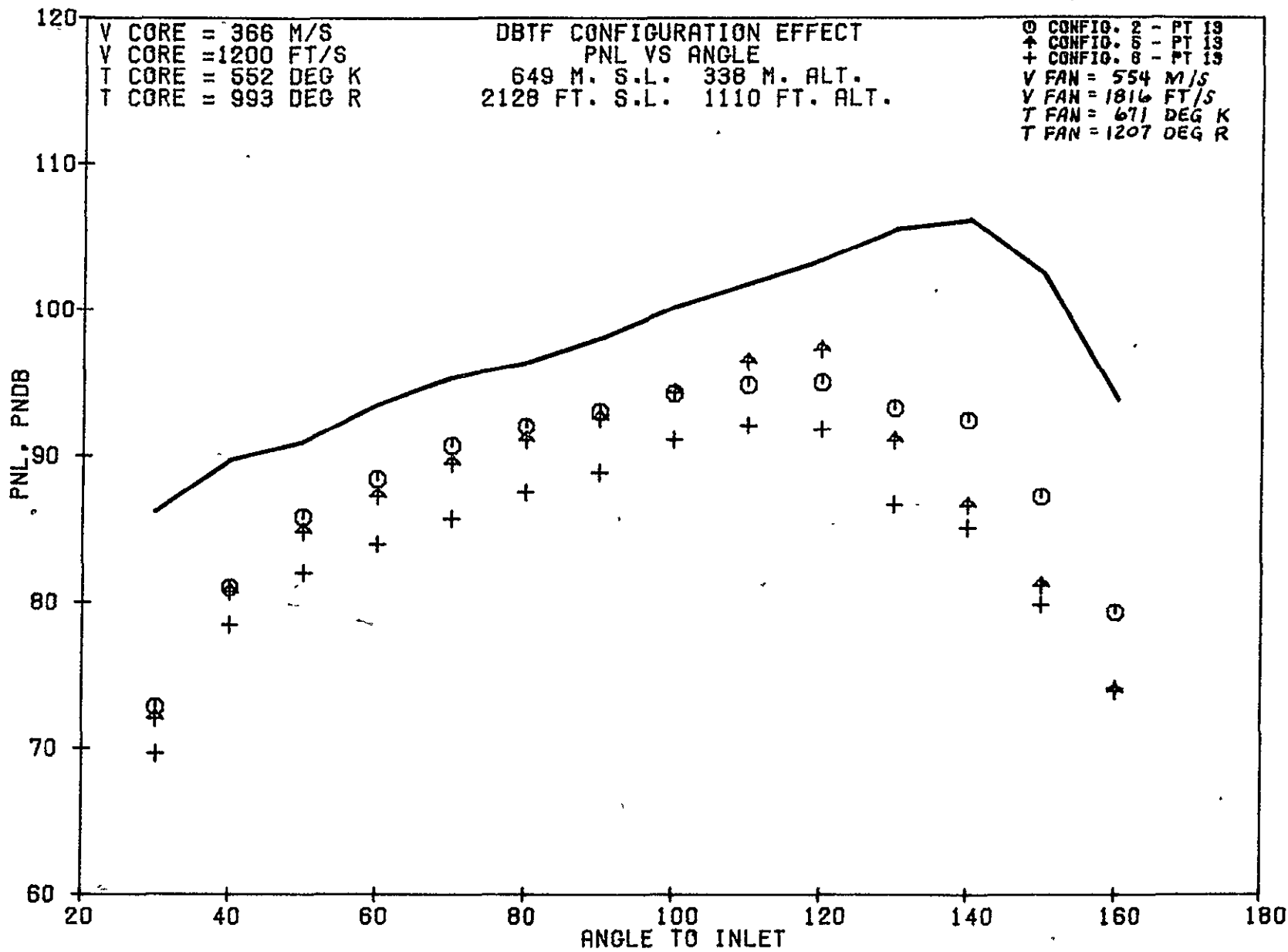


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11.2.7

130

V CORE = 367 M/S
V CORE = 1204 FT/S
T CORE = 554 DEG K
T CORE = 998 DEG R

DBTF CONFIGURATION EFFECT
PNL VS ANGLE
649 M. S.L. 338 M. ALT.
2128 FT. S.L. 1110 FT. ALT.

⊙ CONFIO. 2 - PT 16
↑ CONFIO. 5 - PT 16
+ CONFIO. 6 - PT 16
V FAN = 728 M/S
V FAN = 2388 FT/S
T FAN = 907 DEG K
T FAN = 1632 DEG R

120

110

100

90

80

70

PNL: PND8

20

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60

80

100

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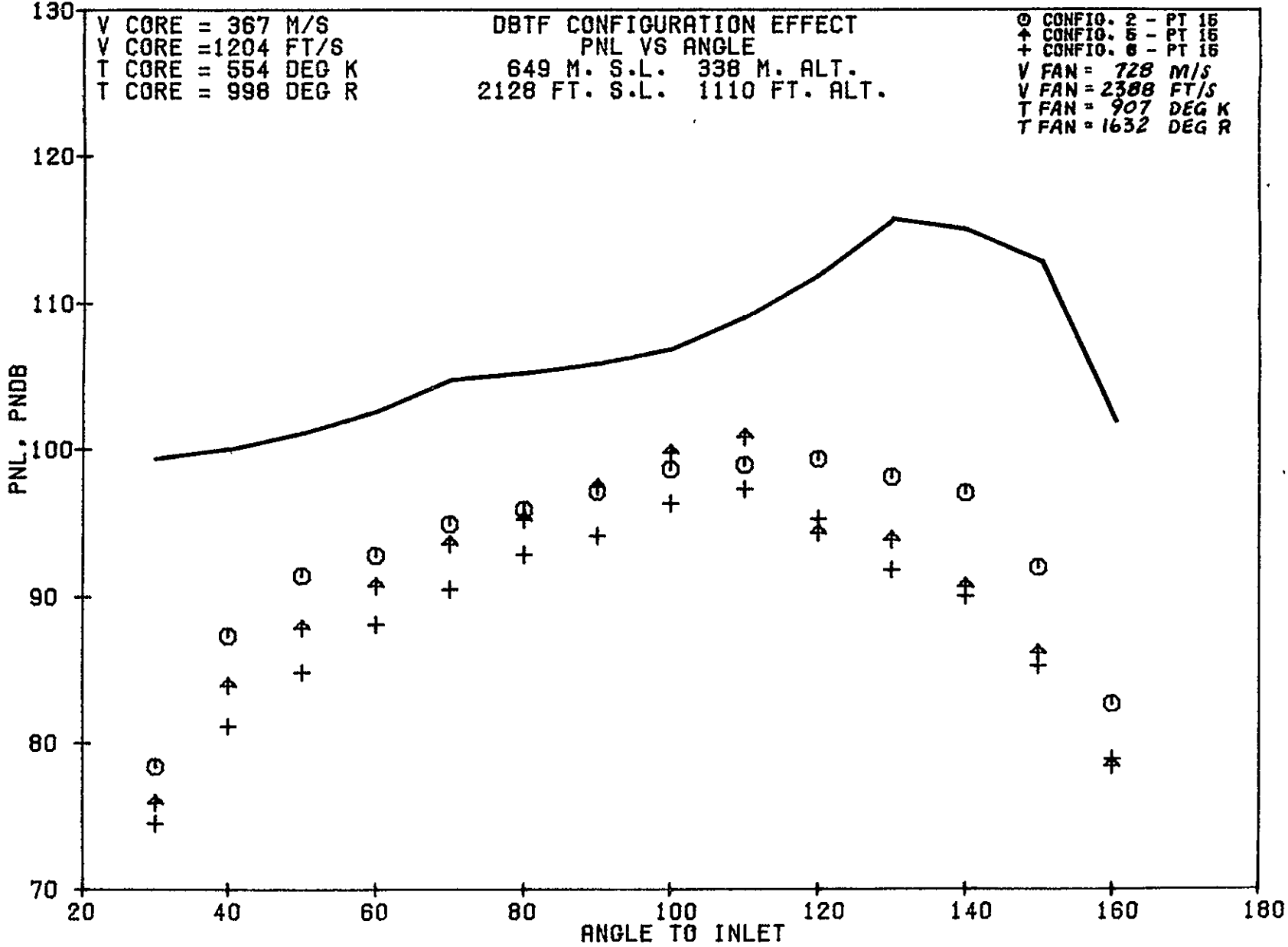
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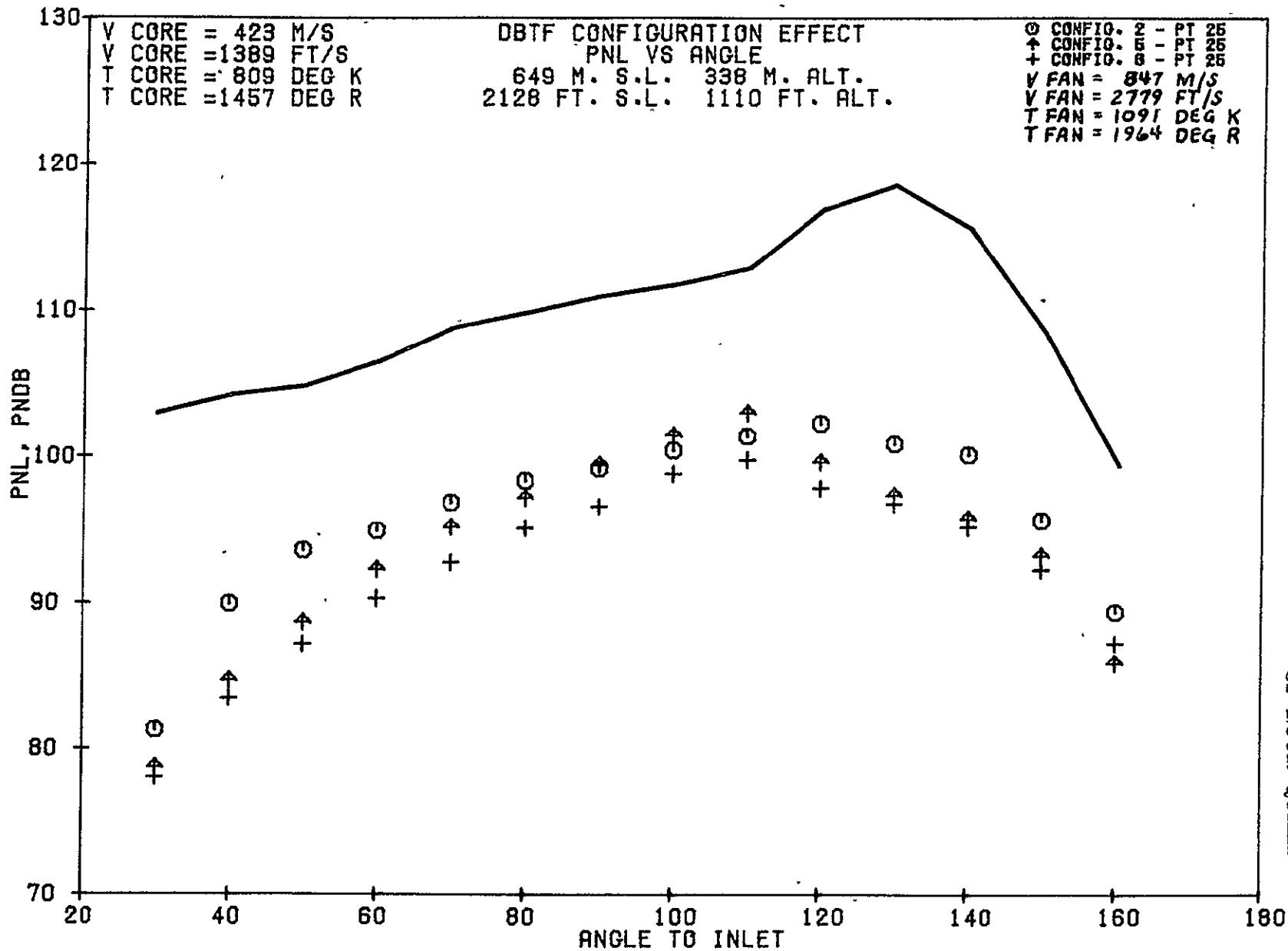
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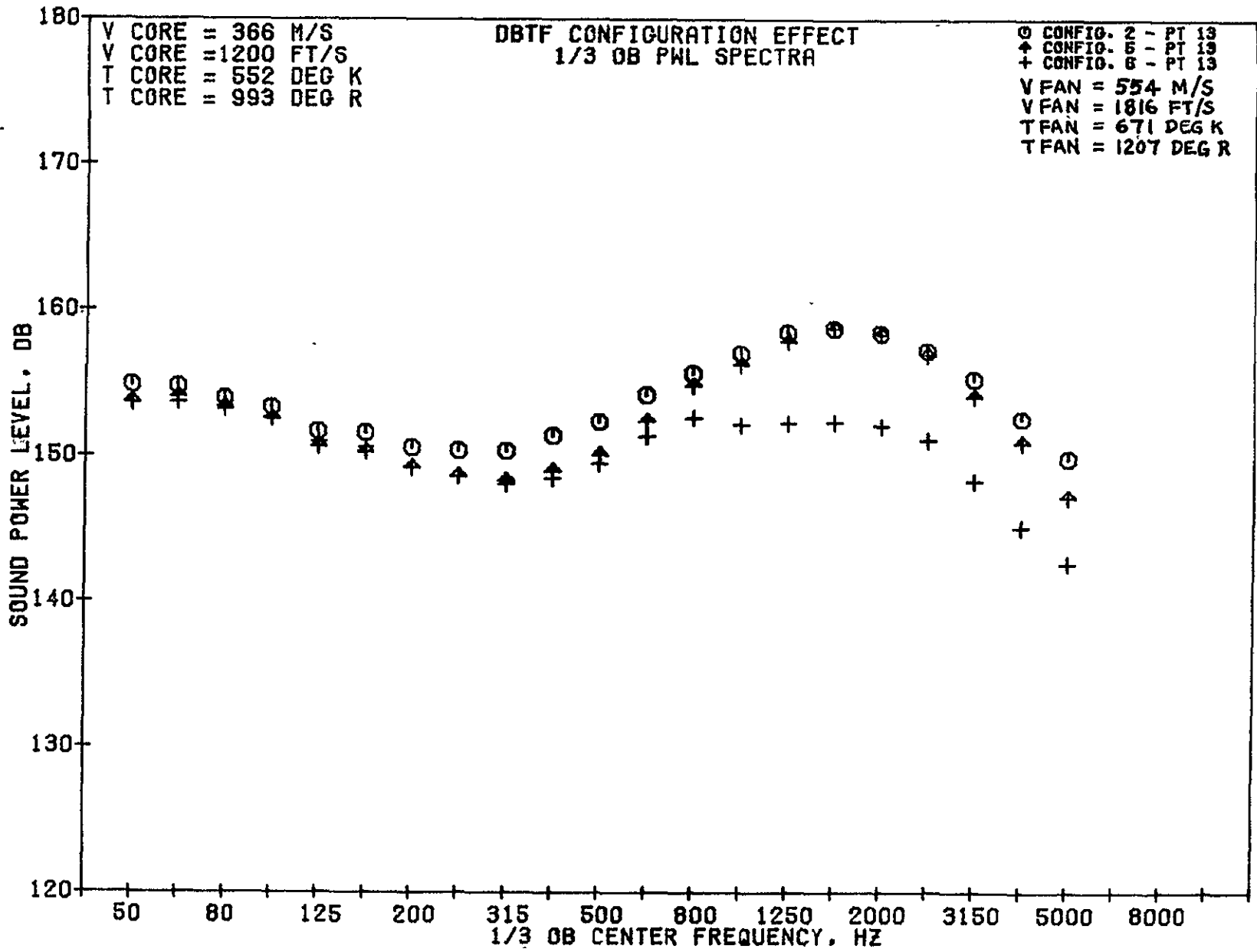
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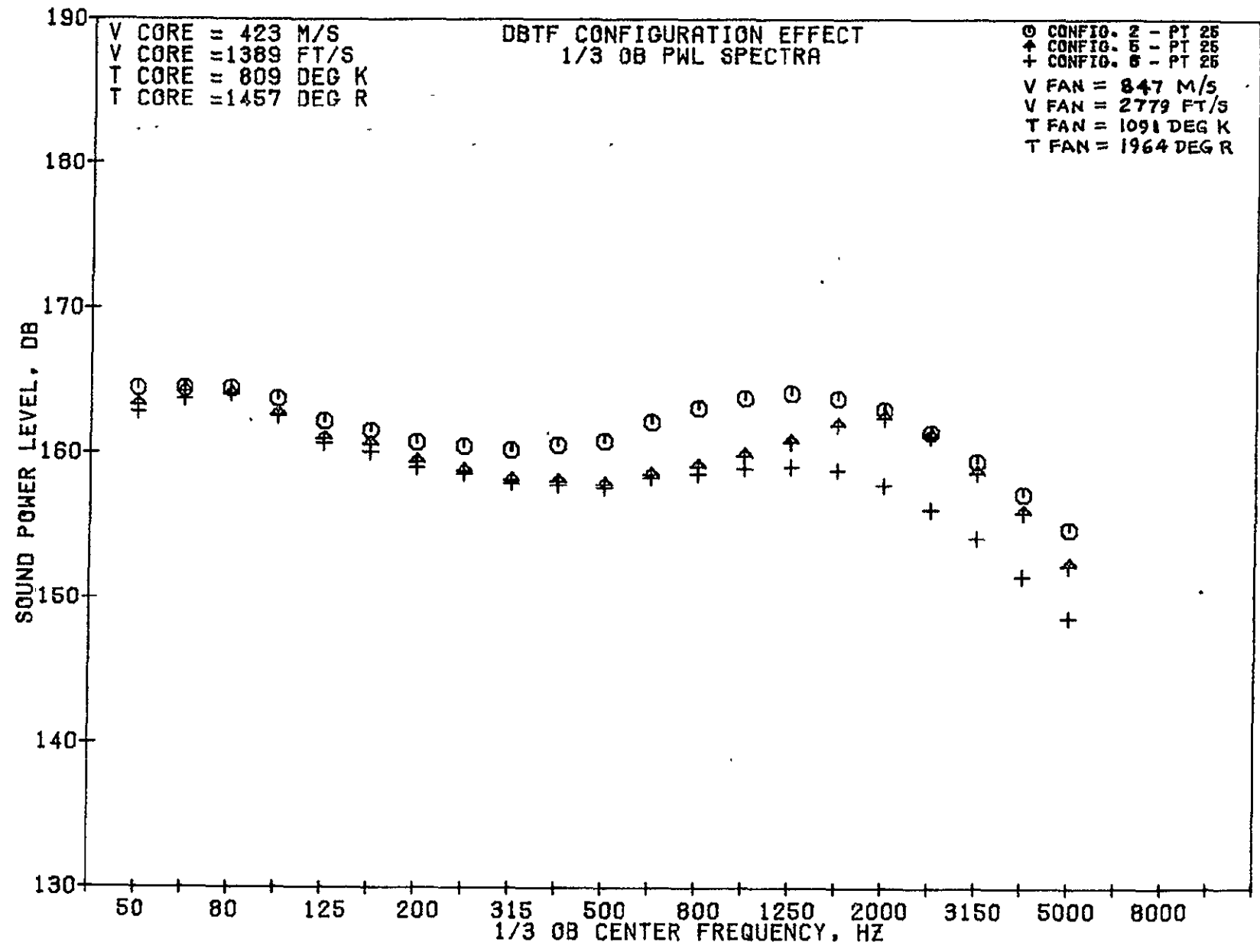
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79 BUREAU

DBTF CONFIGURATION EFFECT
1/3 OB PWL SPECTRA

V CORE = 423 M/S
V CORE = 1389 FT/S
T CORE = 809 DEG K
T CORE = 1457 DEG R

⊙ CONFIG. 2 - PT 25
↑ CONFIG. 5 - PT 25
+ CONFIG. 6 - PT 25
V FAN = 847 M/S
V FAN = 2779 FT/S
T FAN = 1091 DEG K
T FAN = 1964 DEG R



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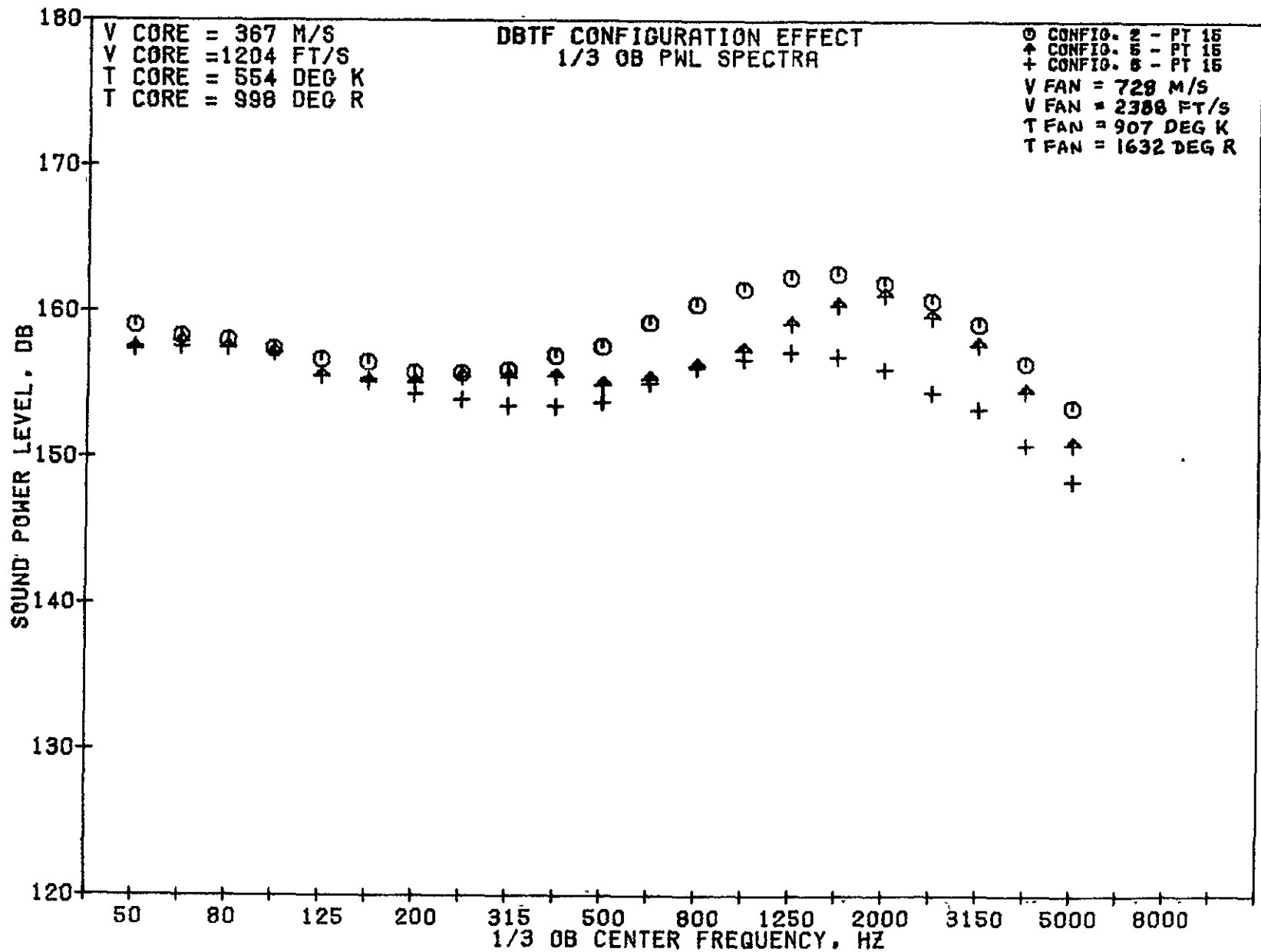
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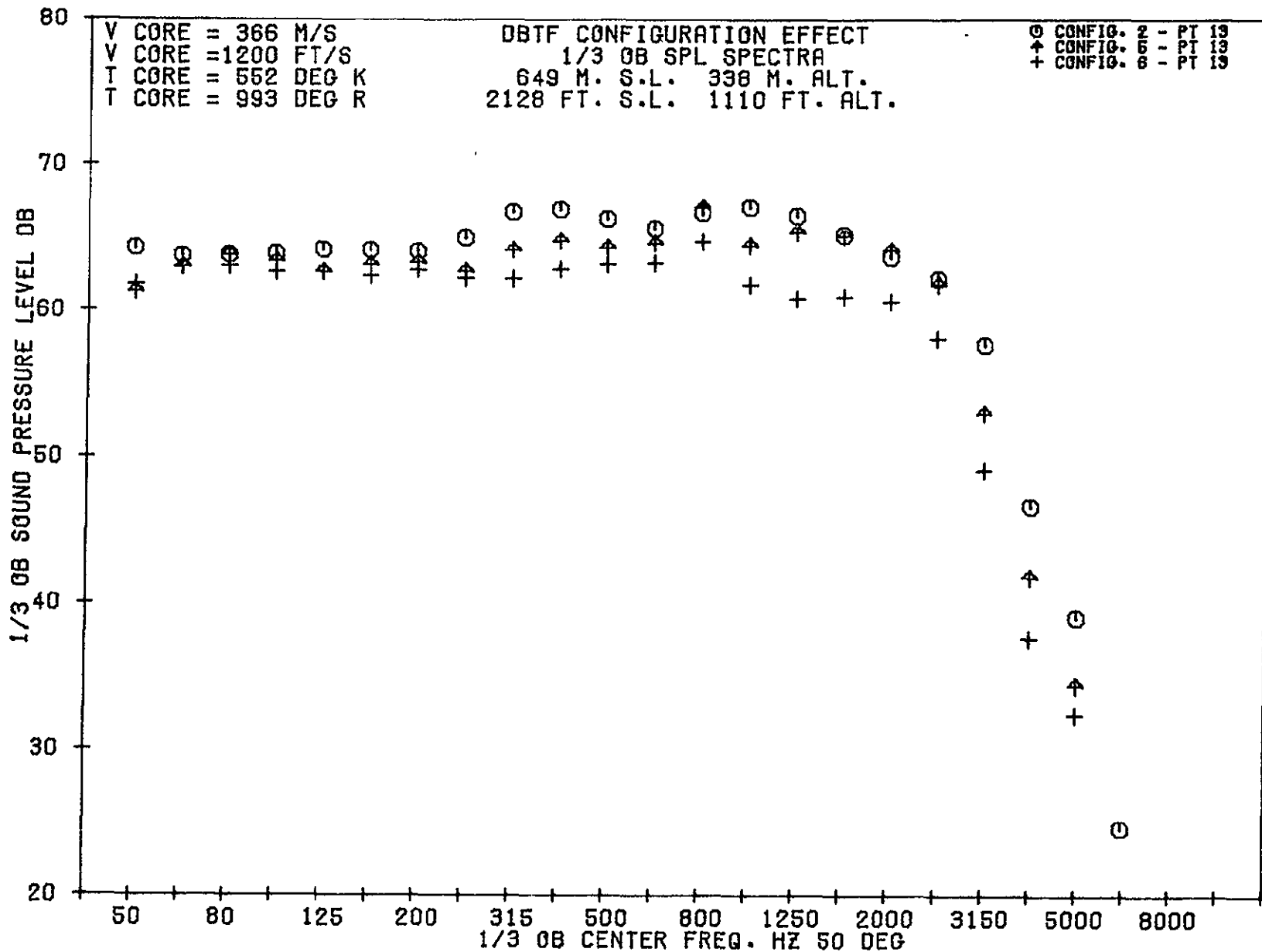
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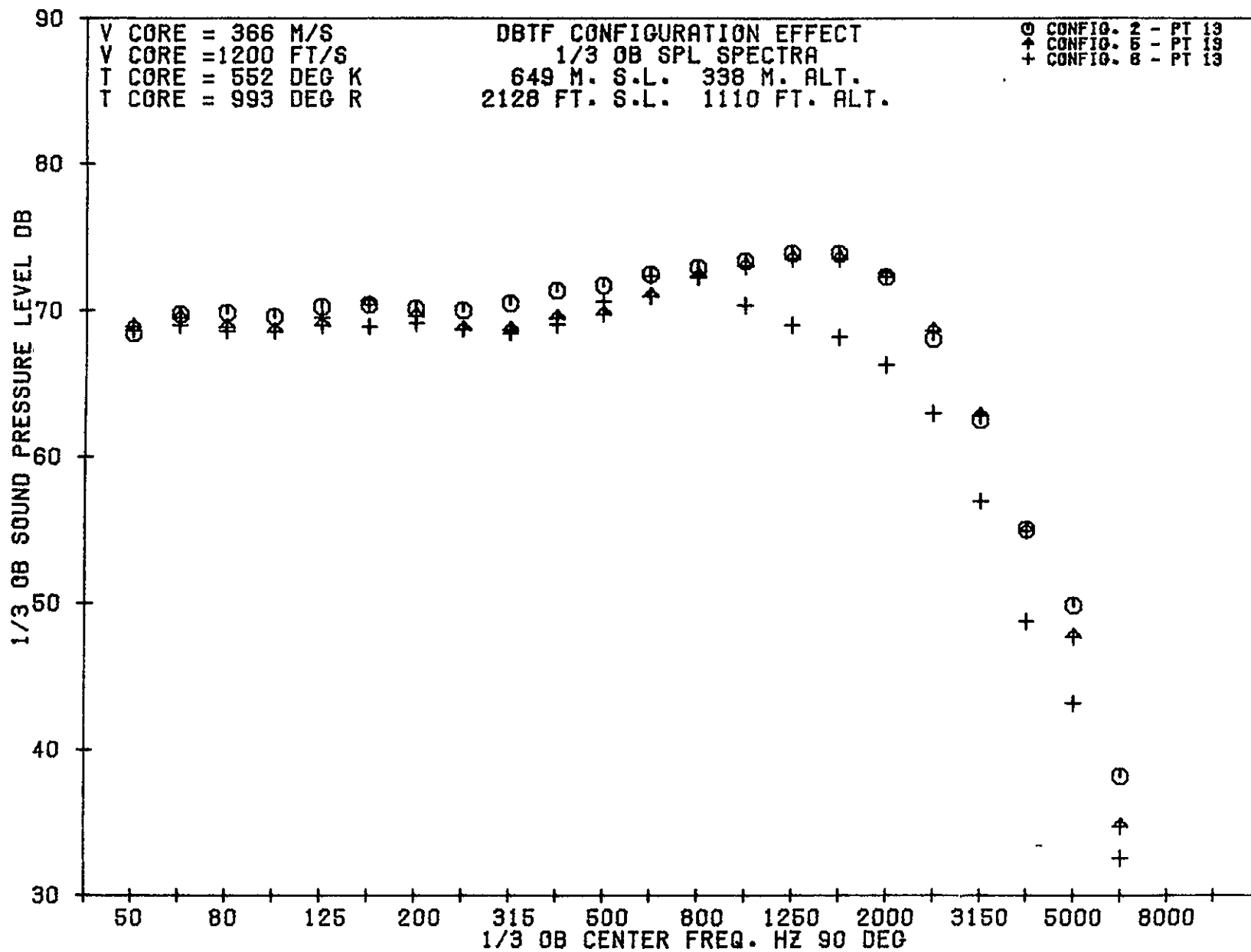
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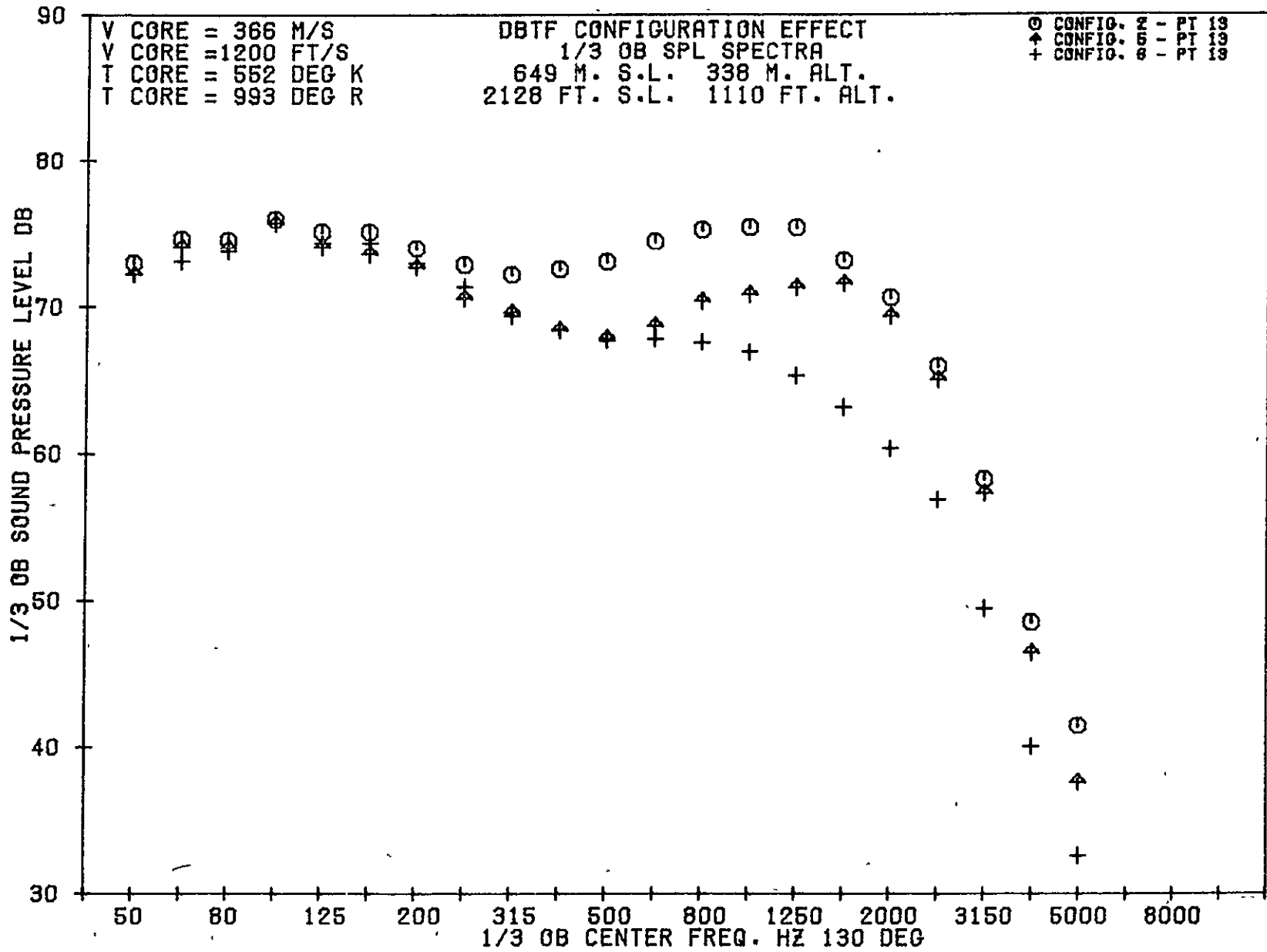


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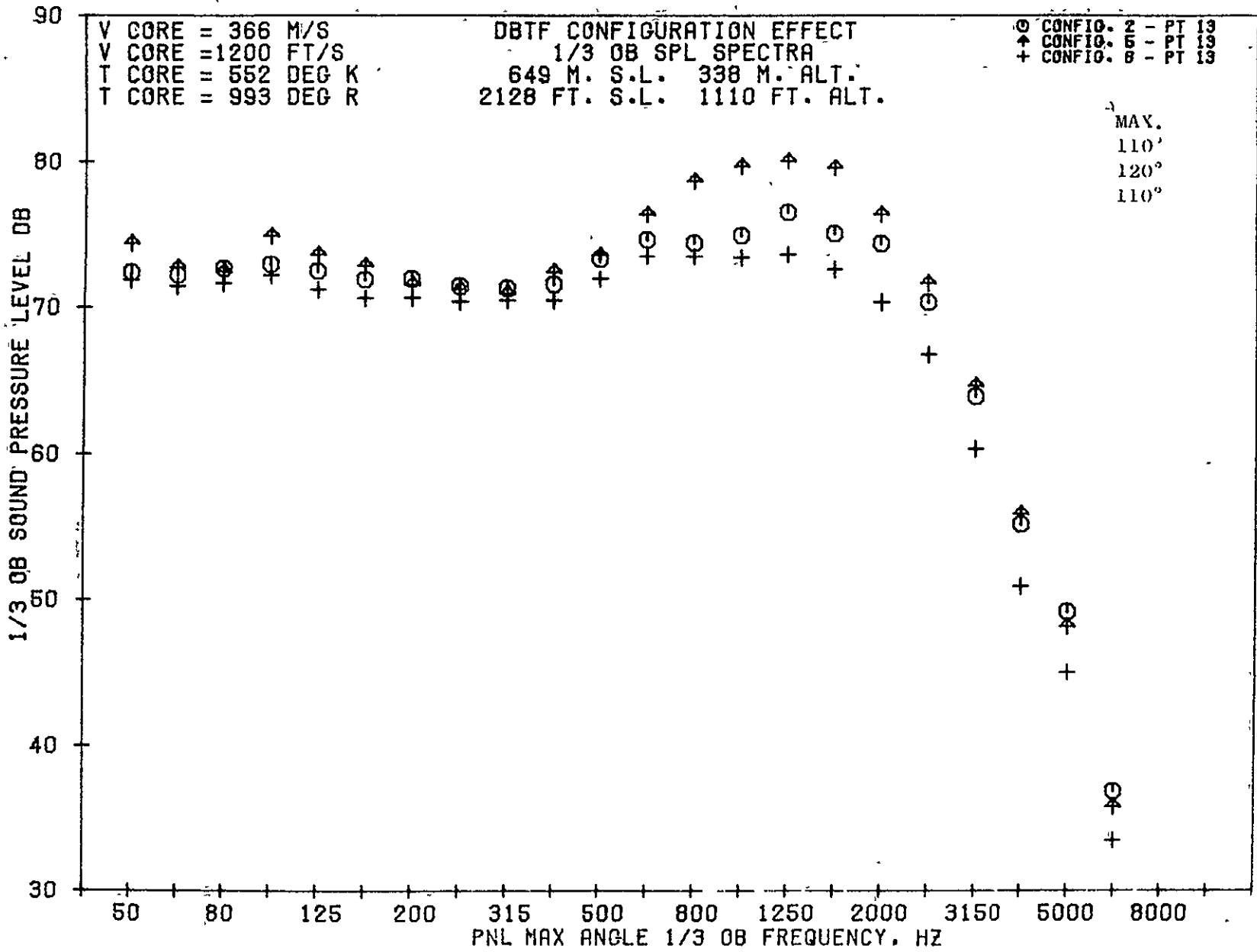


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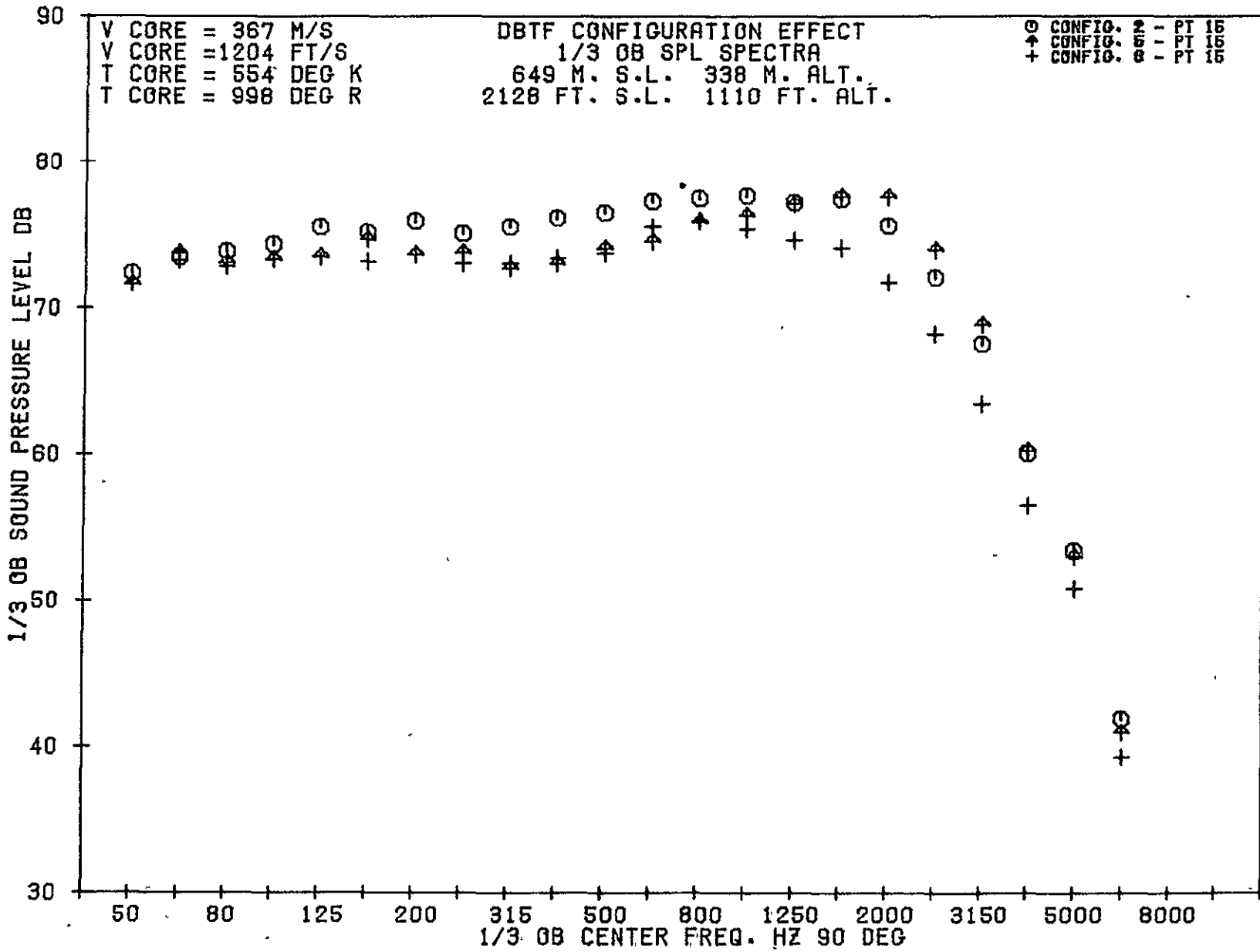
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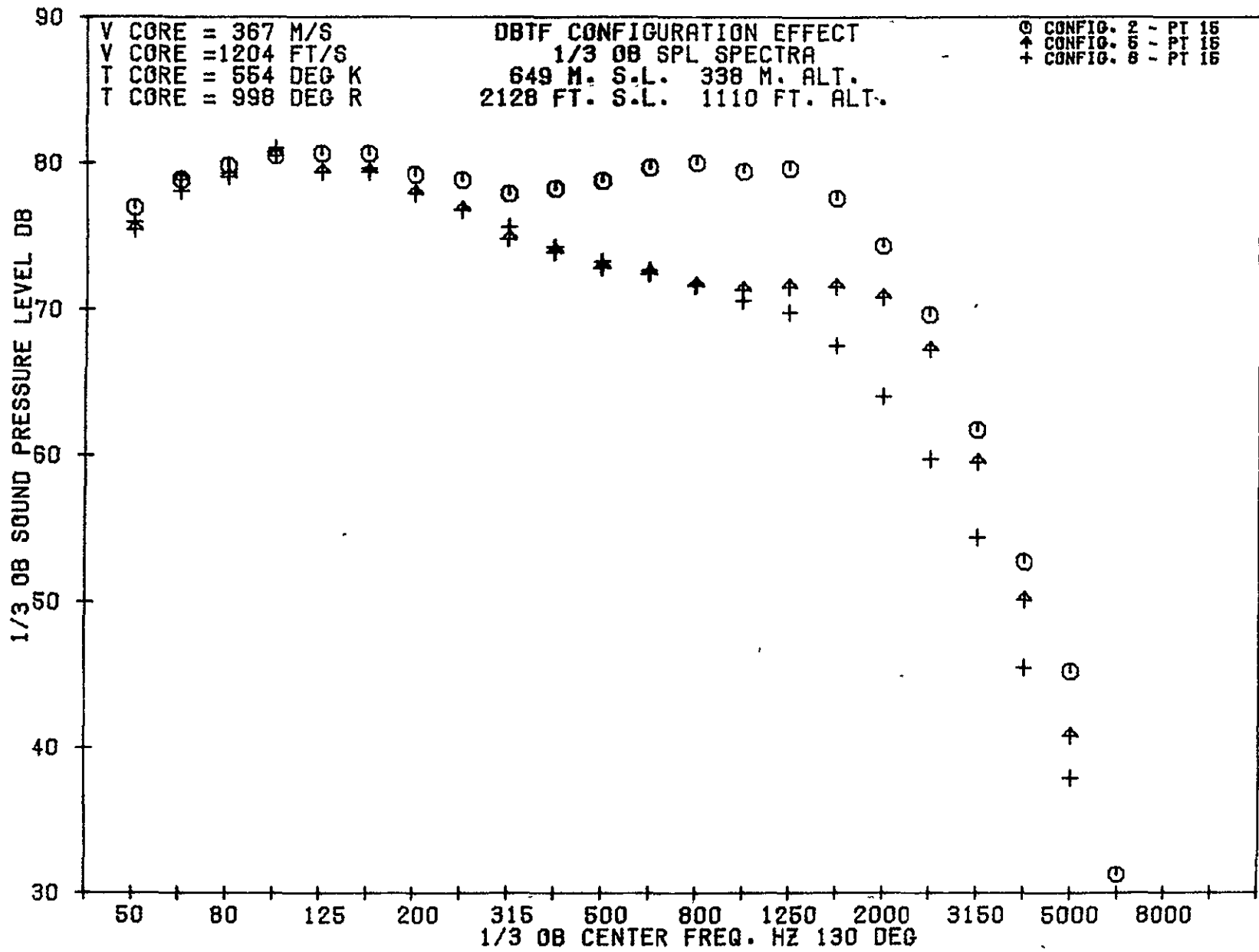
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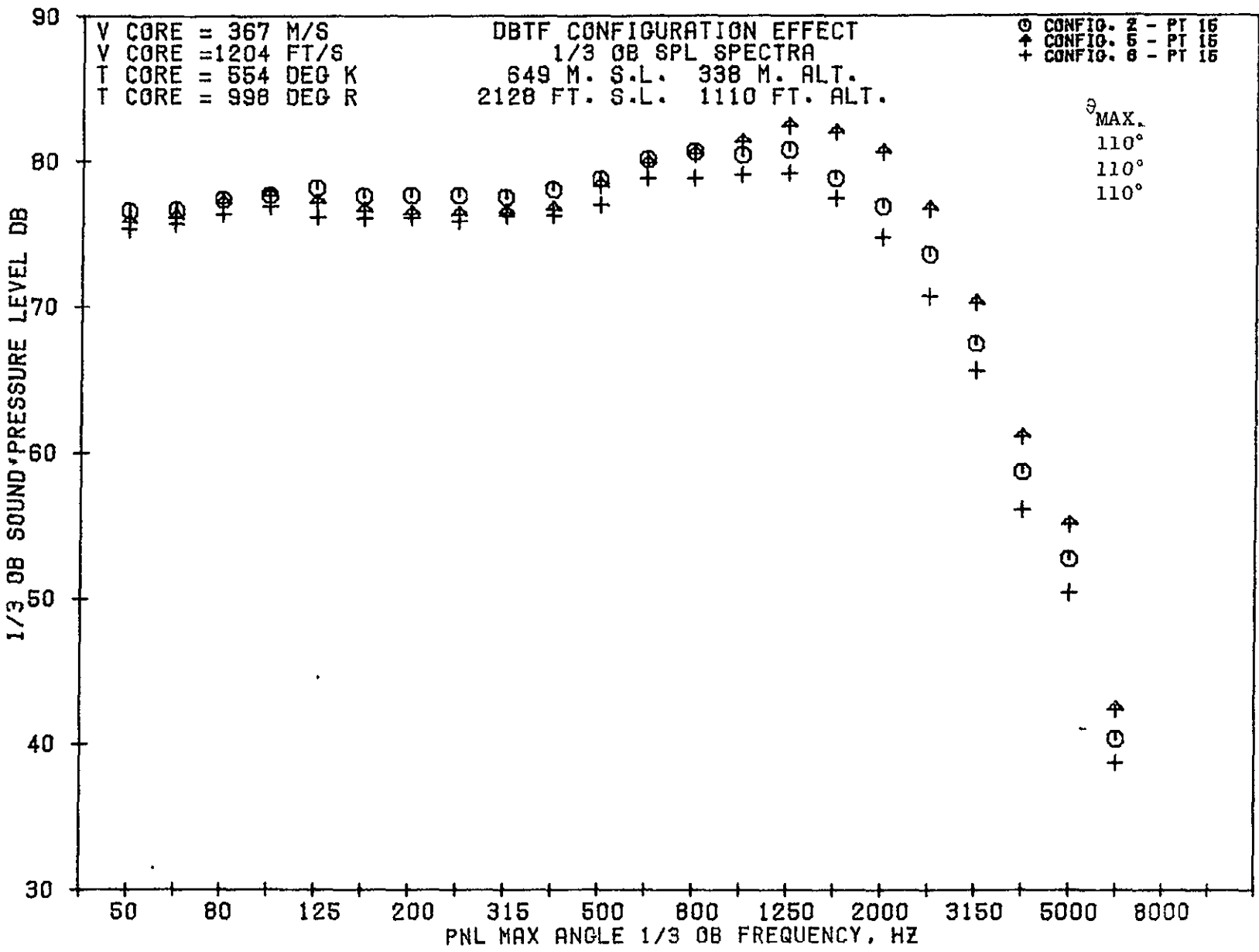
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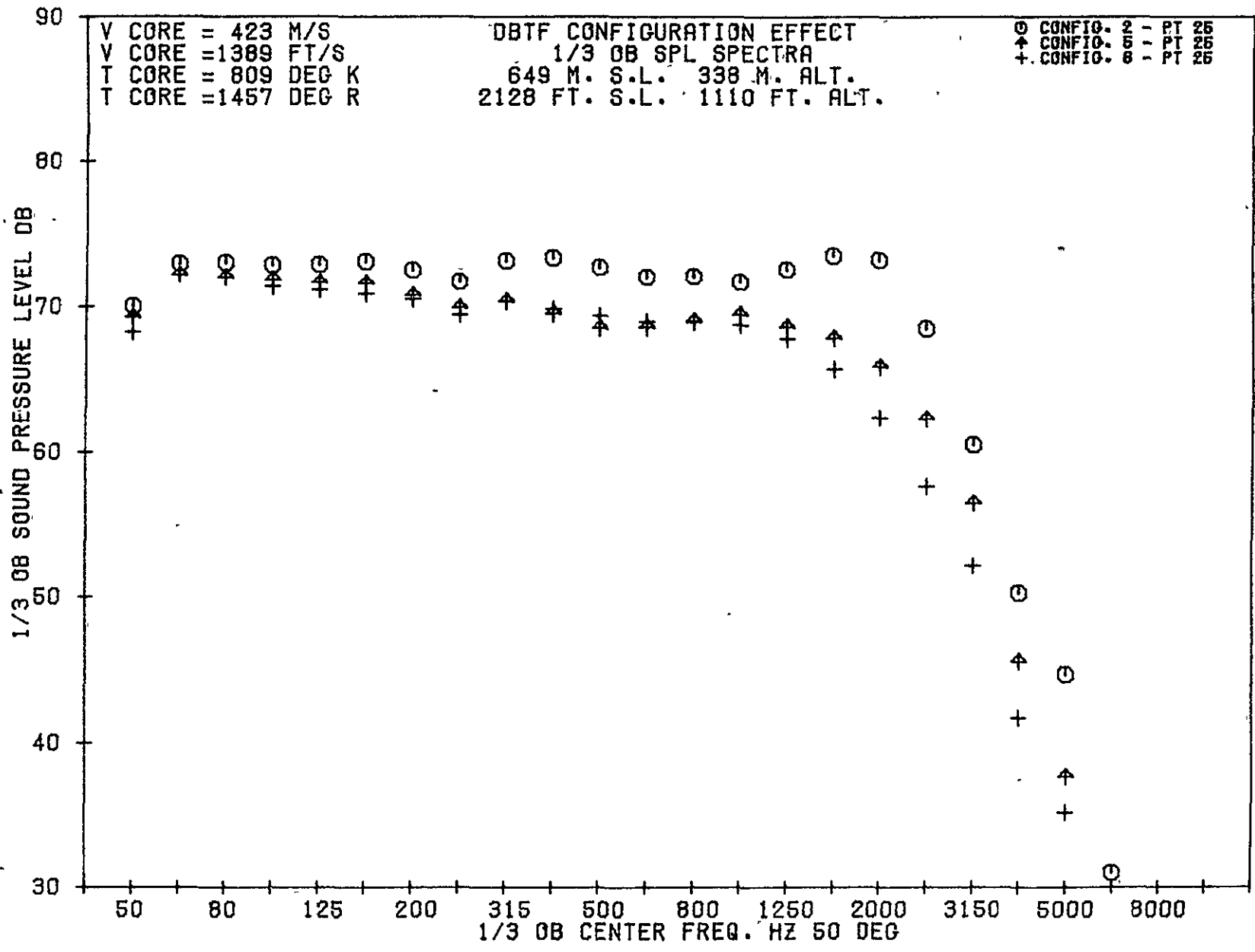
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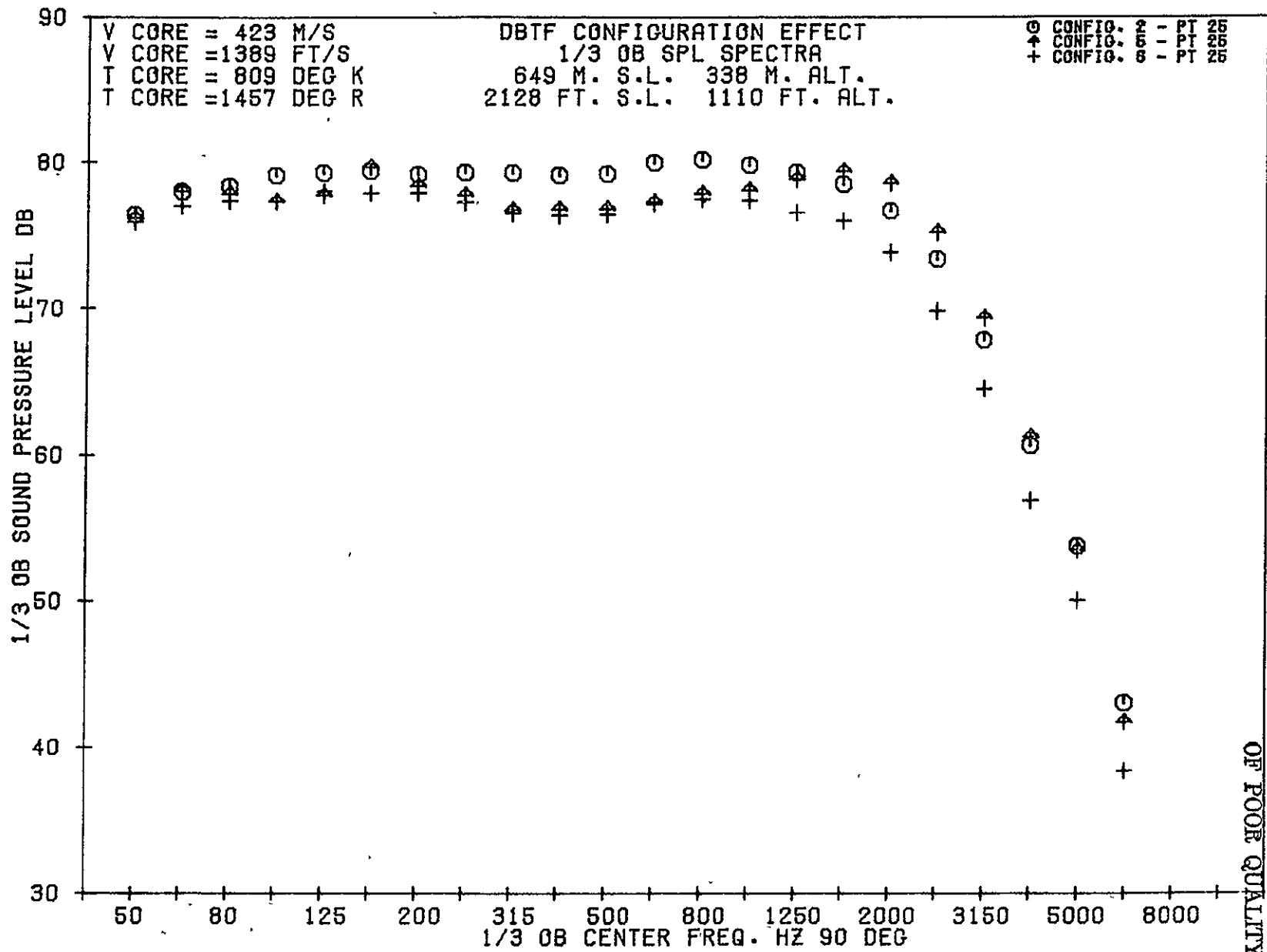


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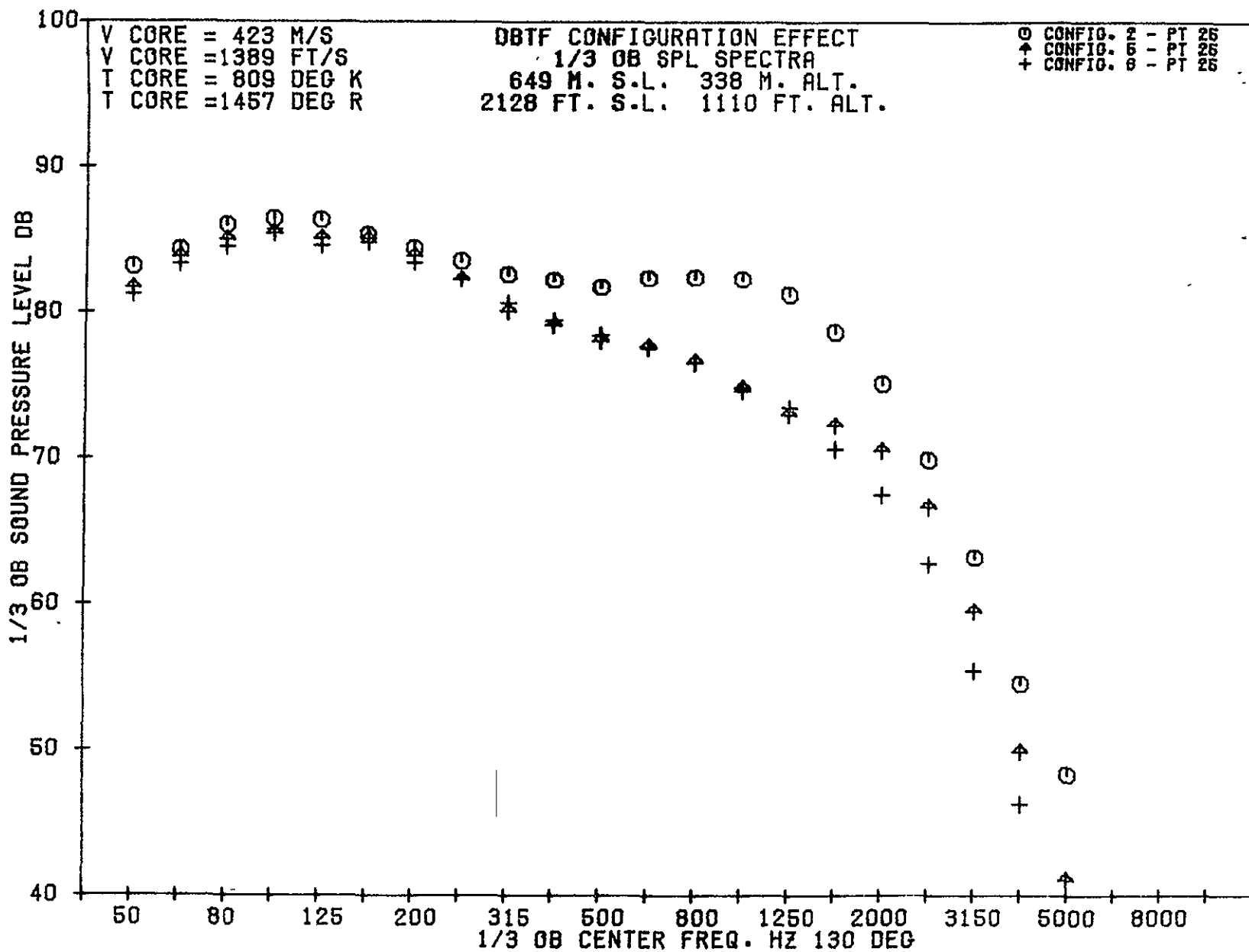
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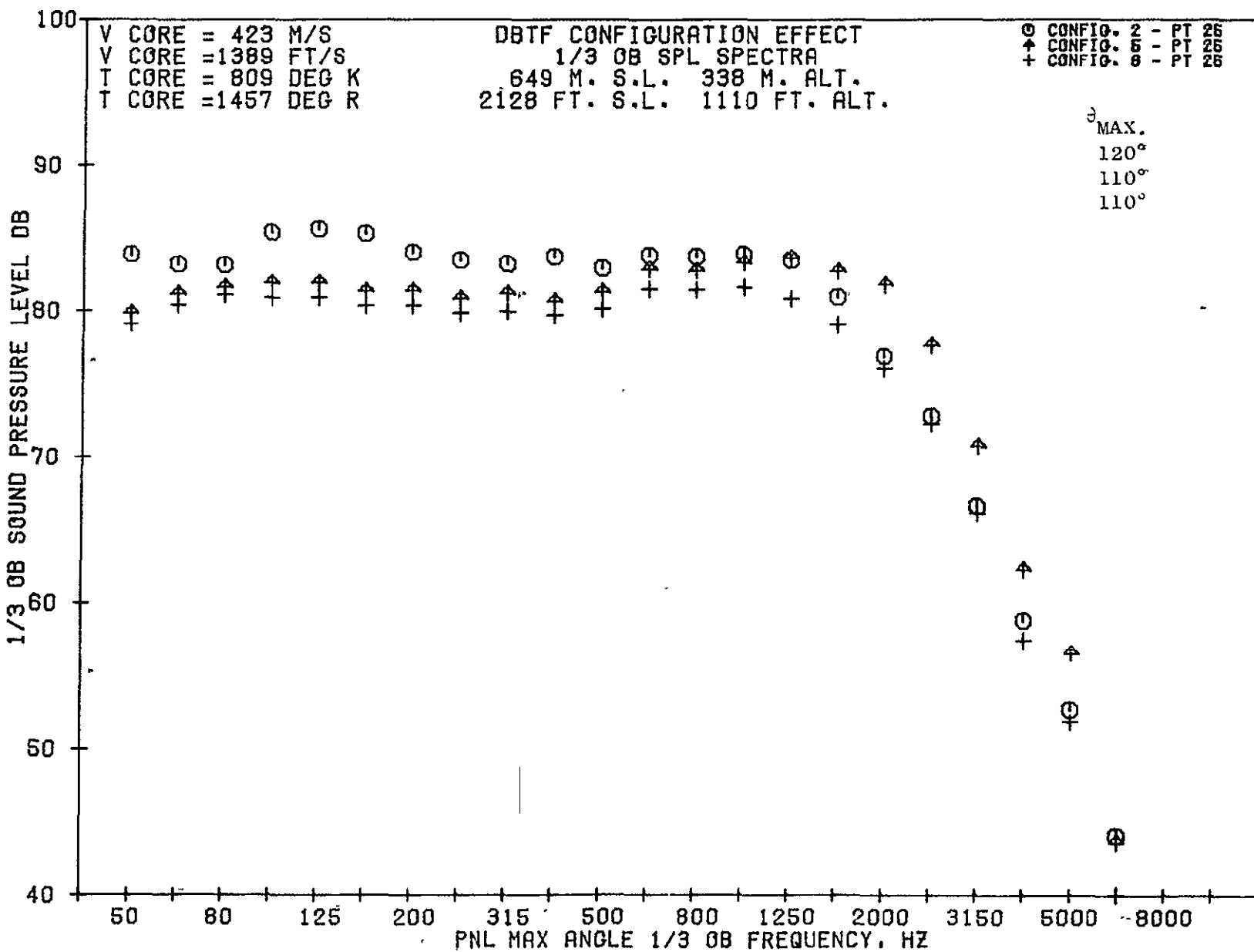
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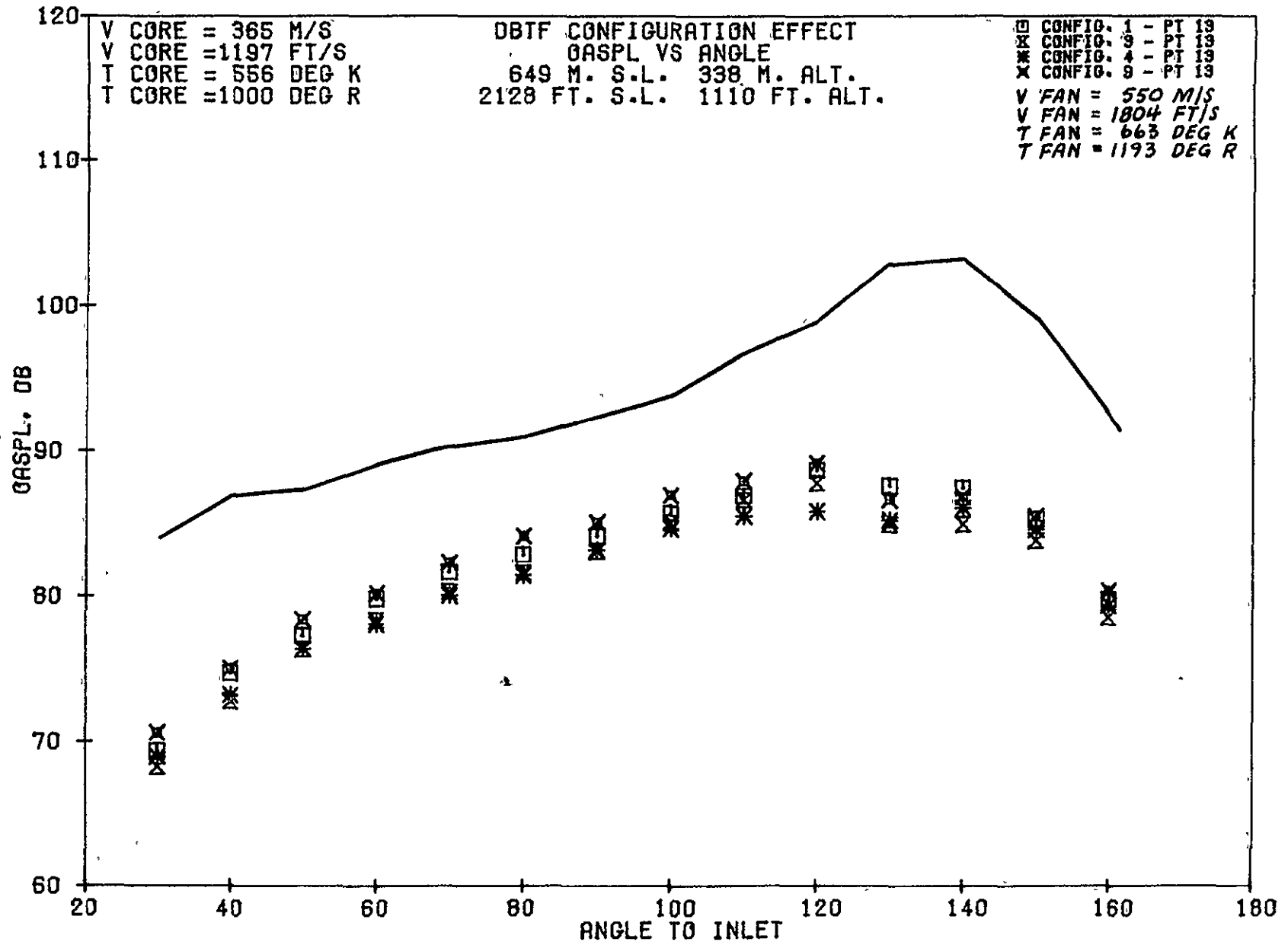
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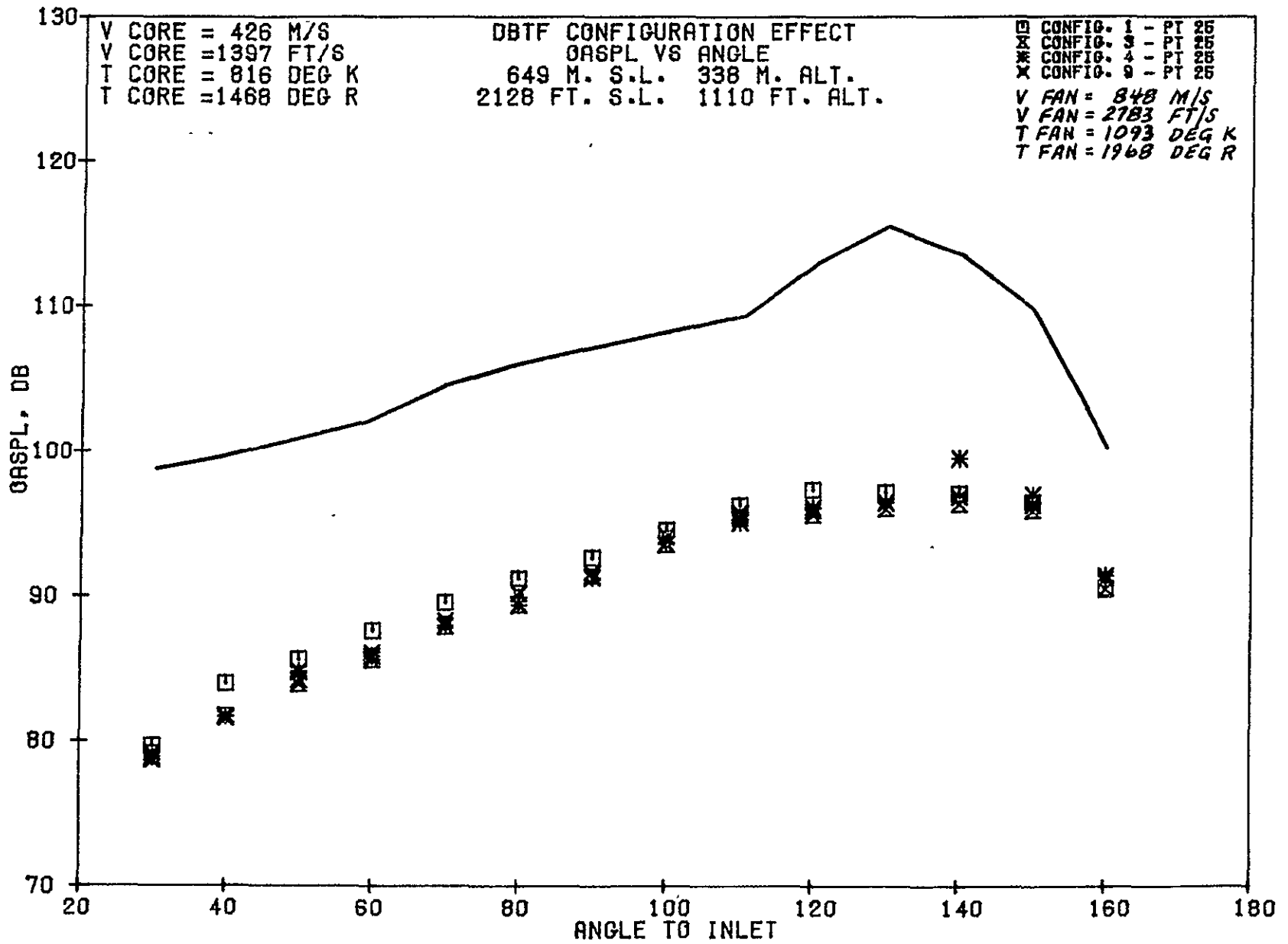
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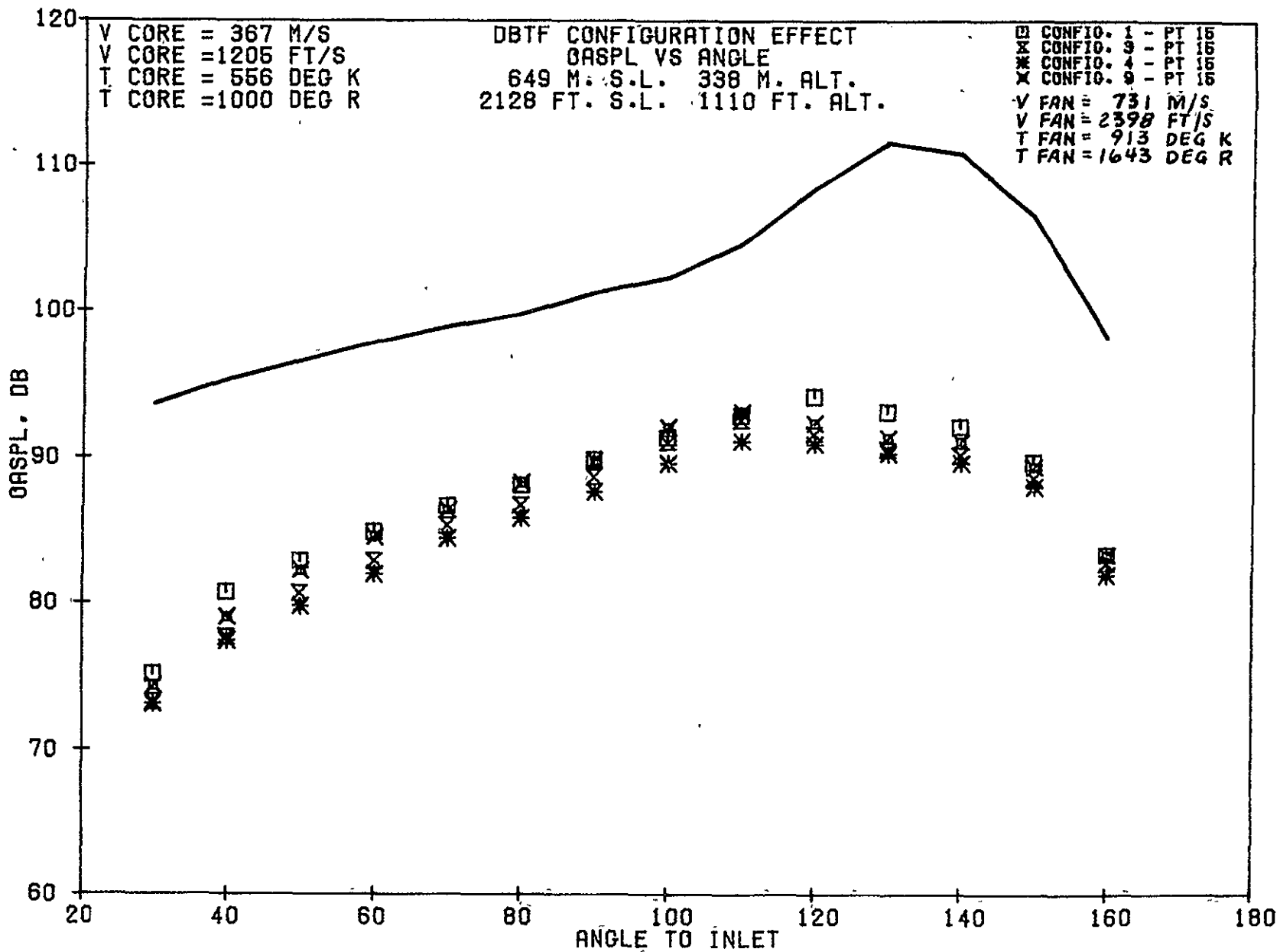
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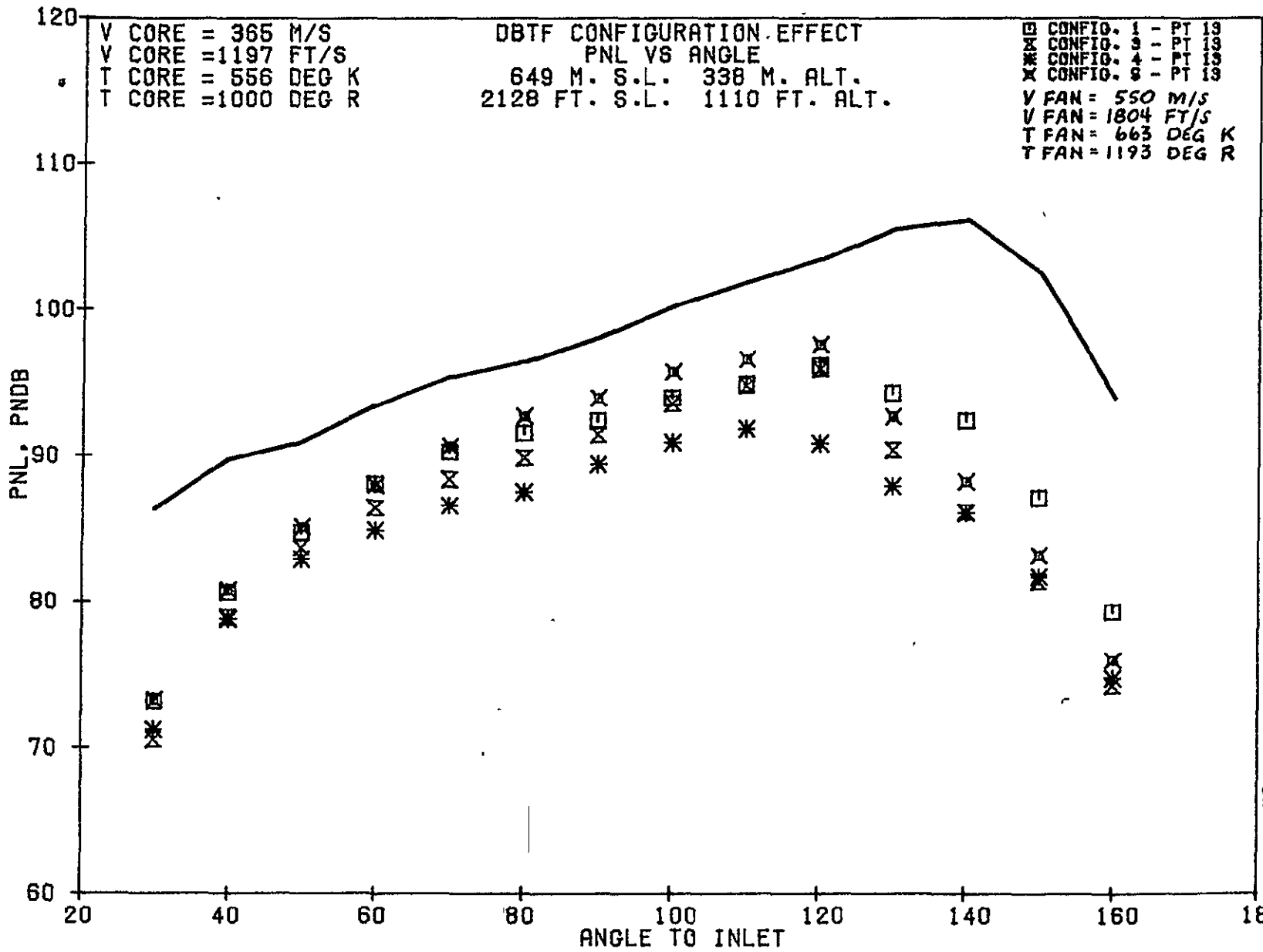
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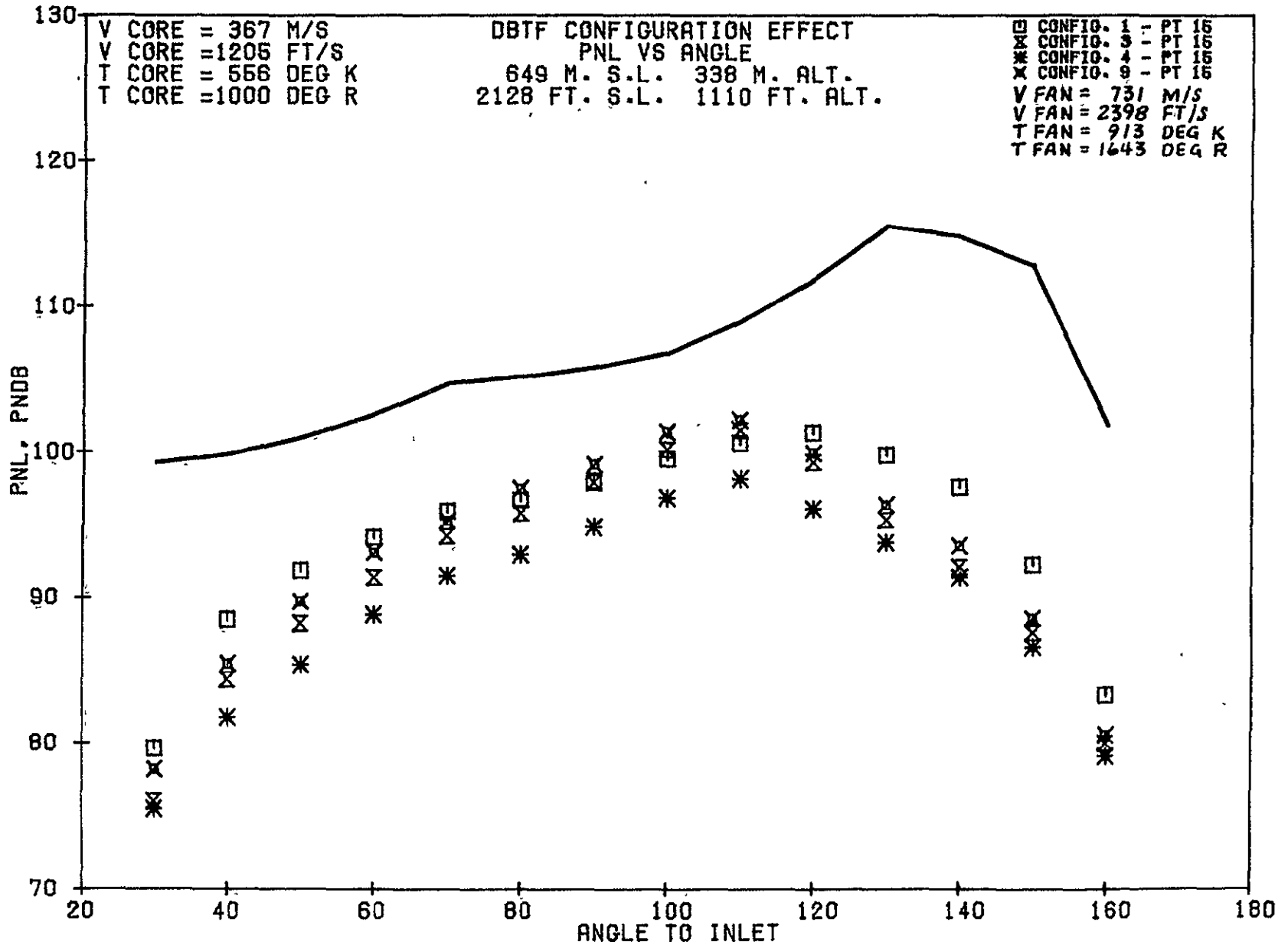


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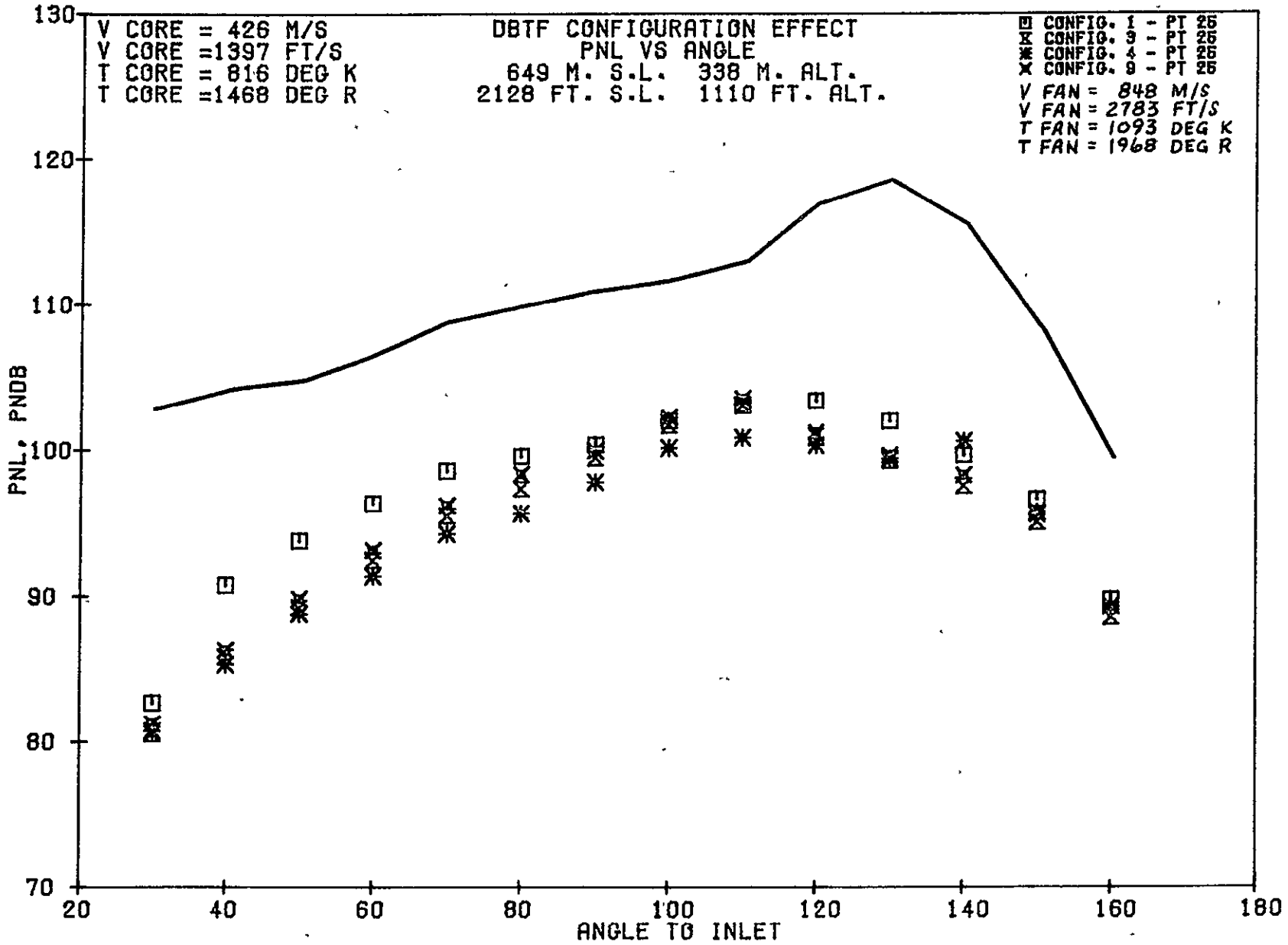
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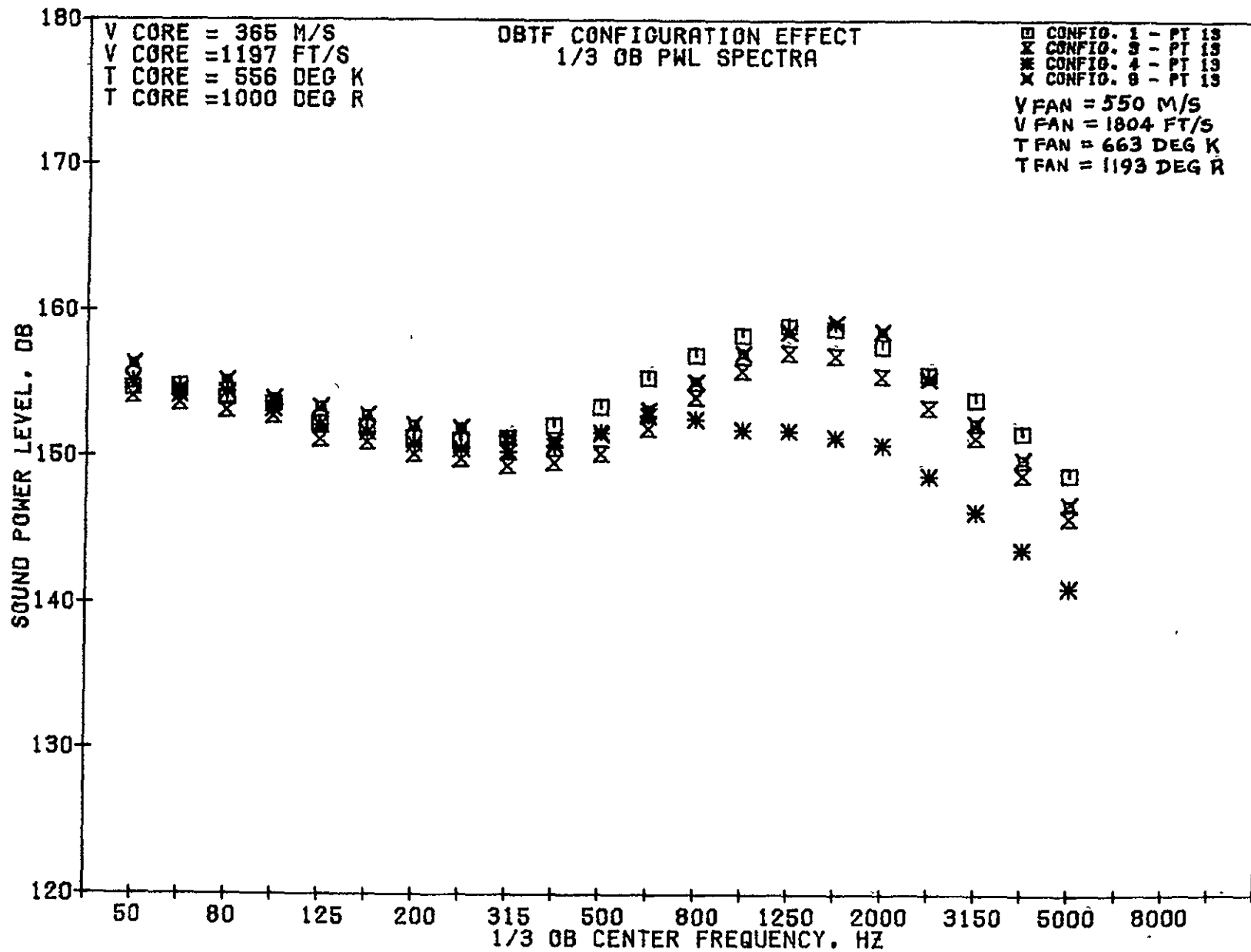
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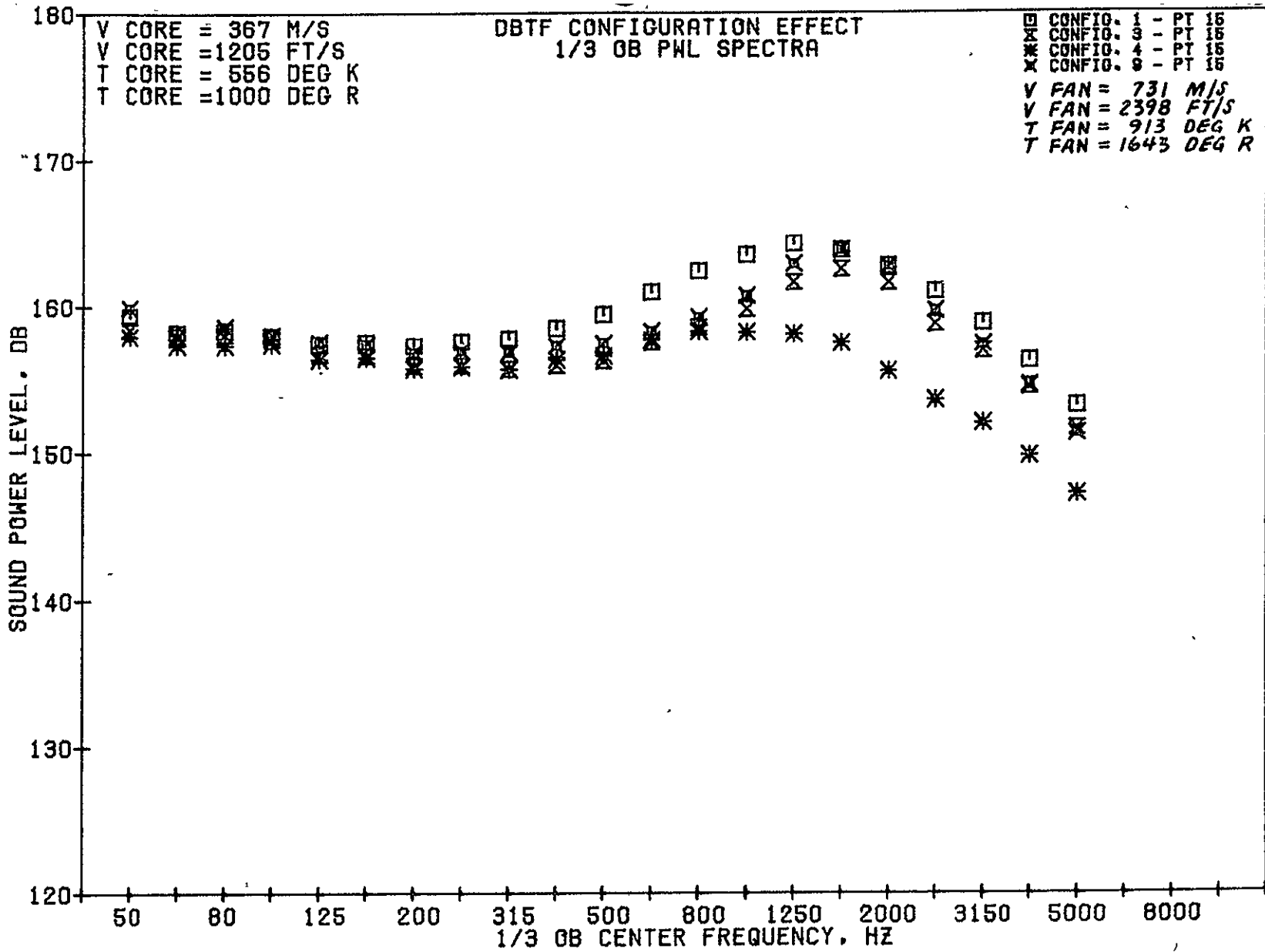


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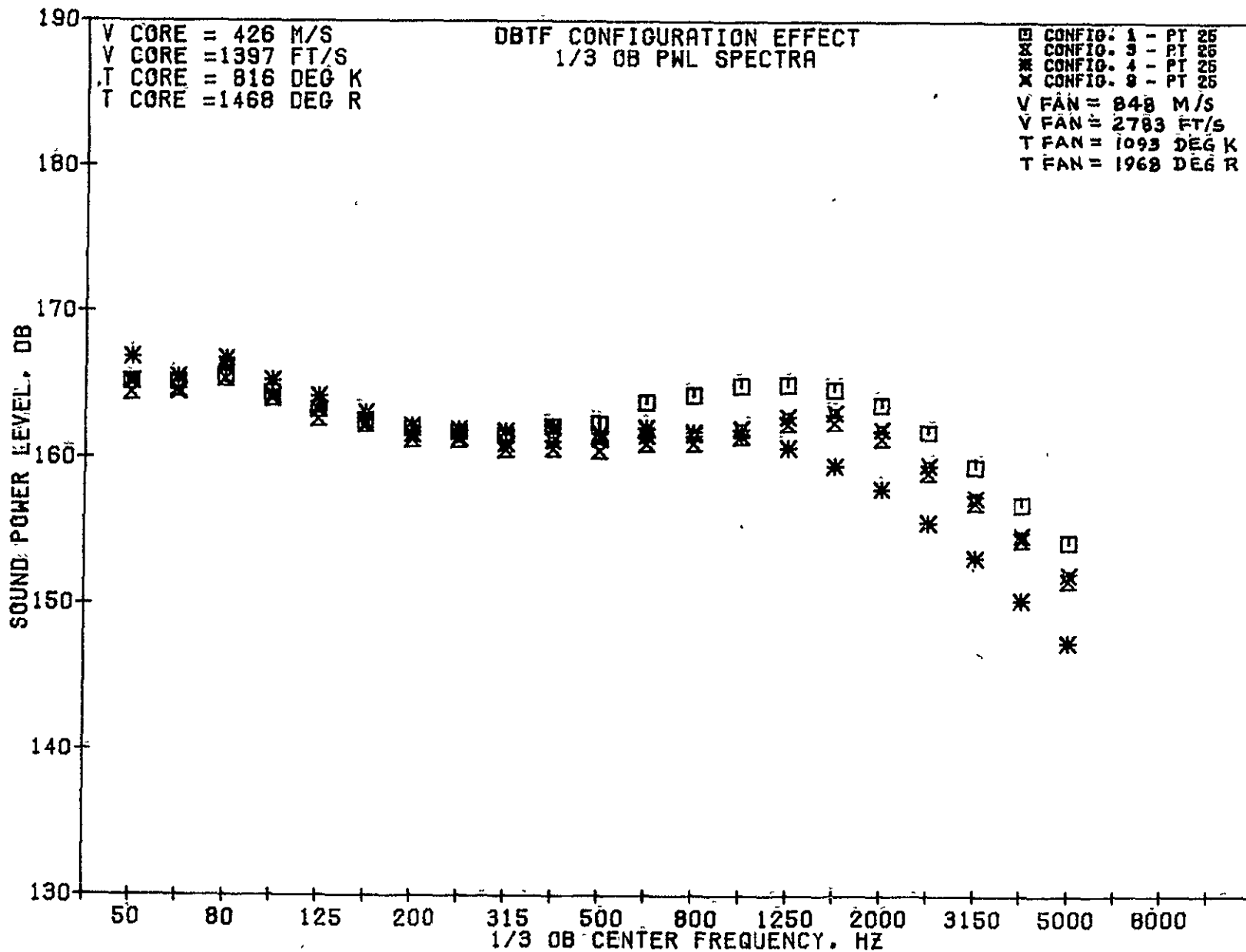
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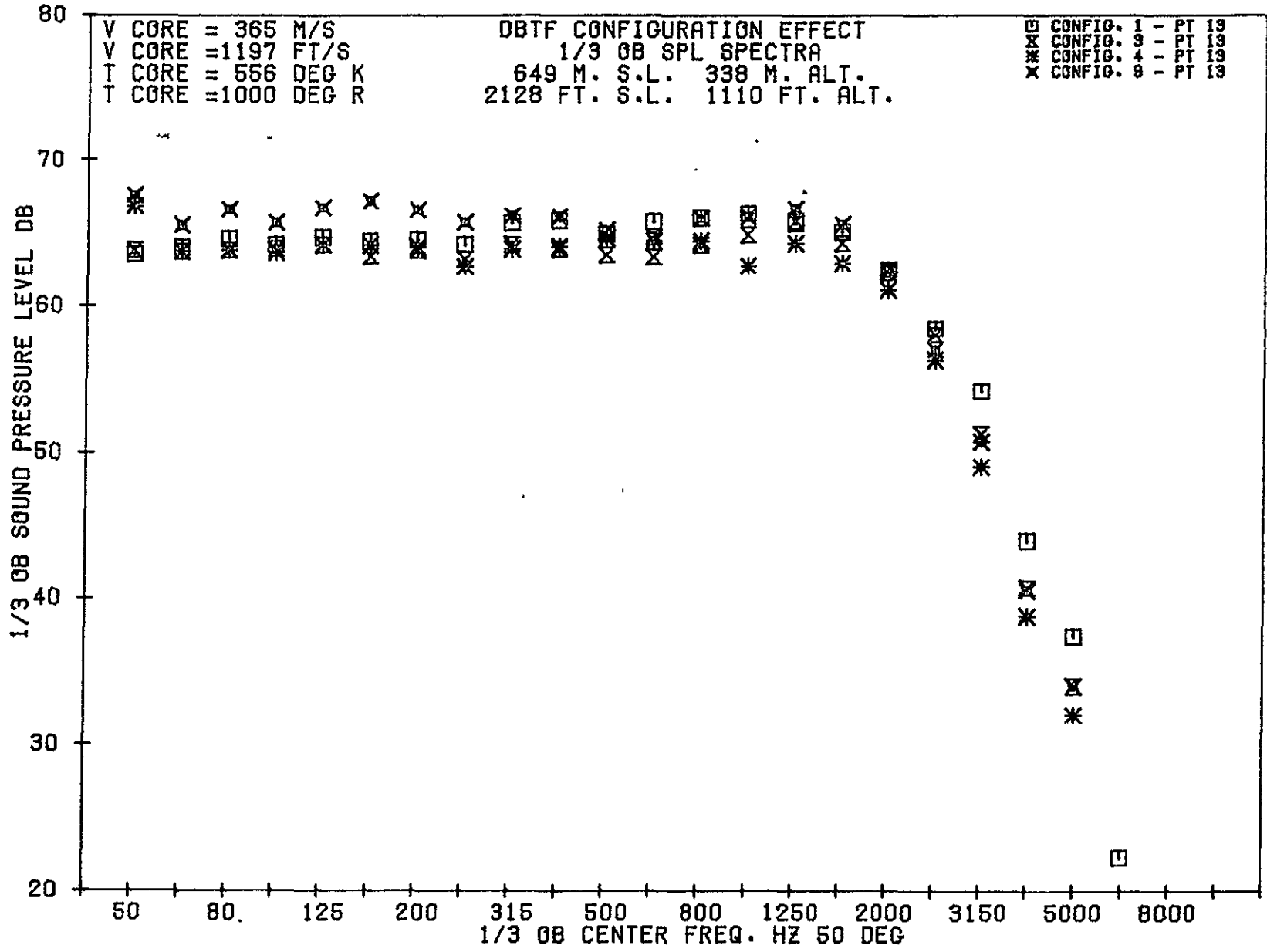


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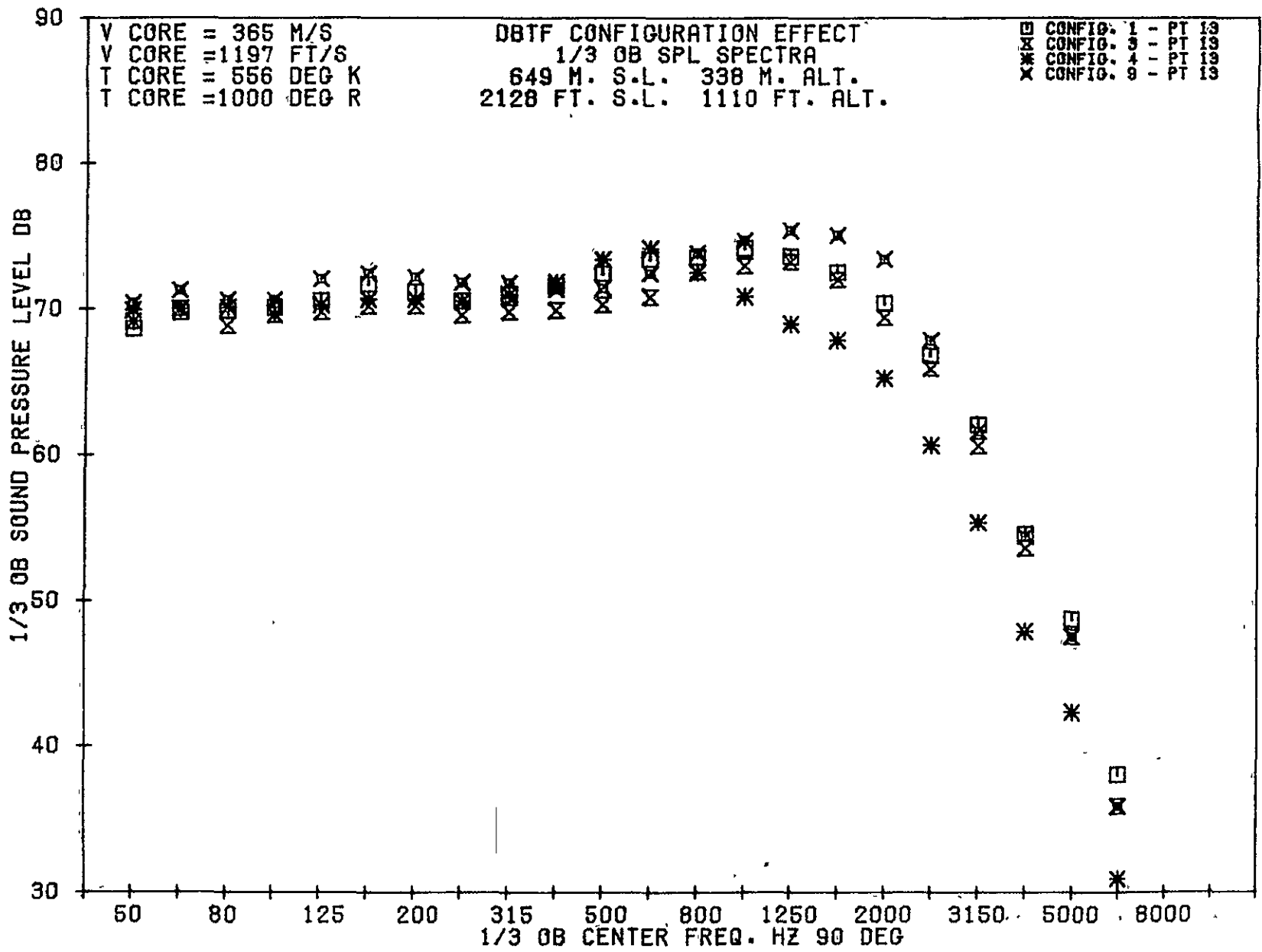
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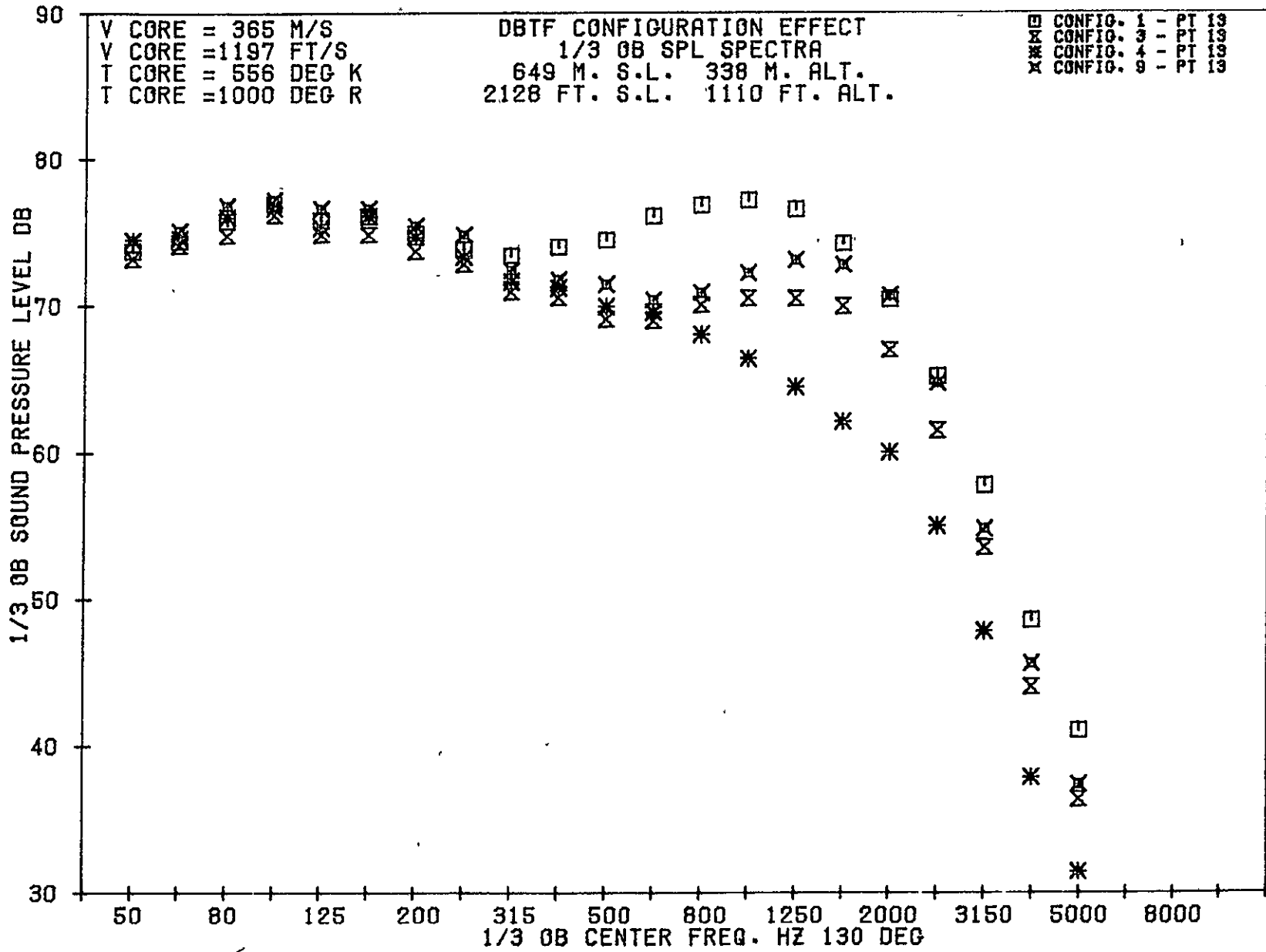
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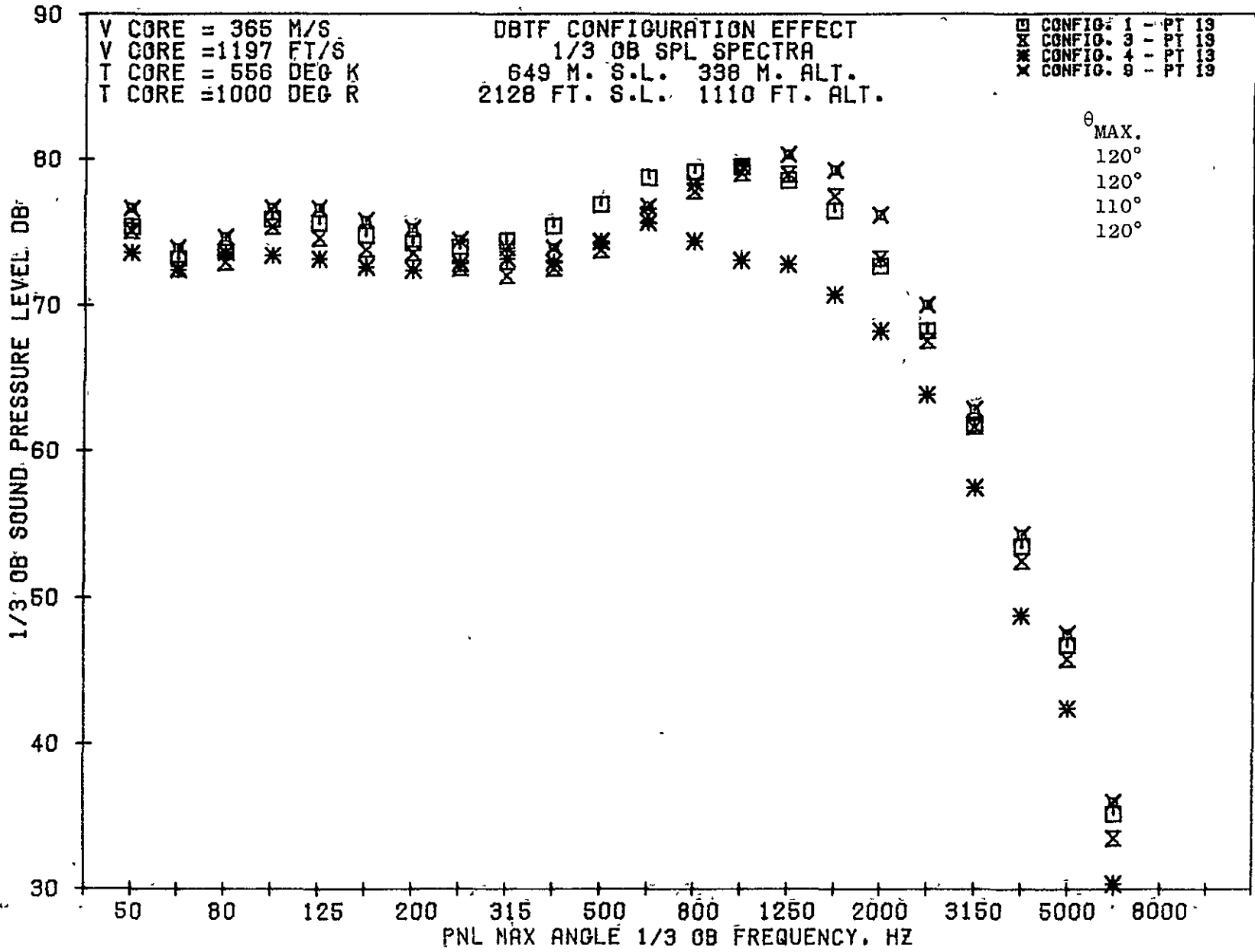
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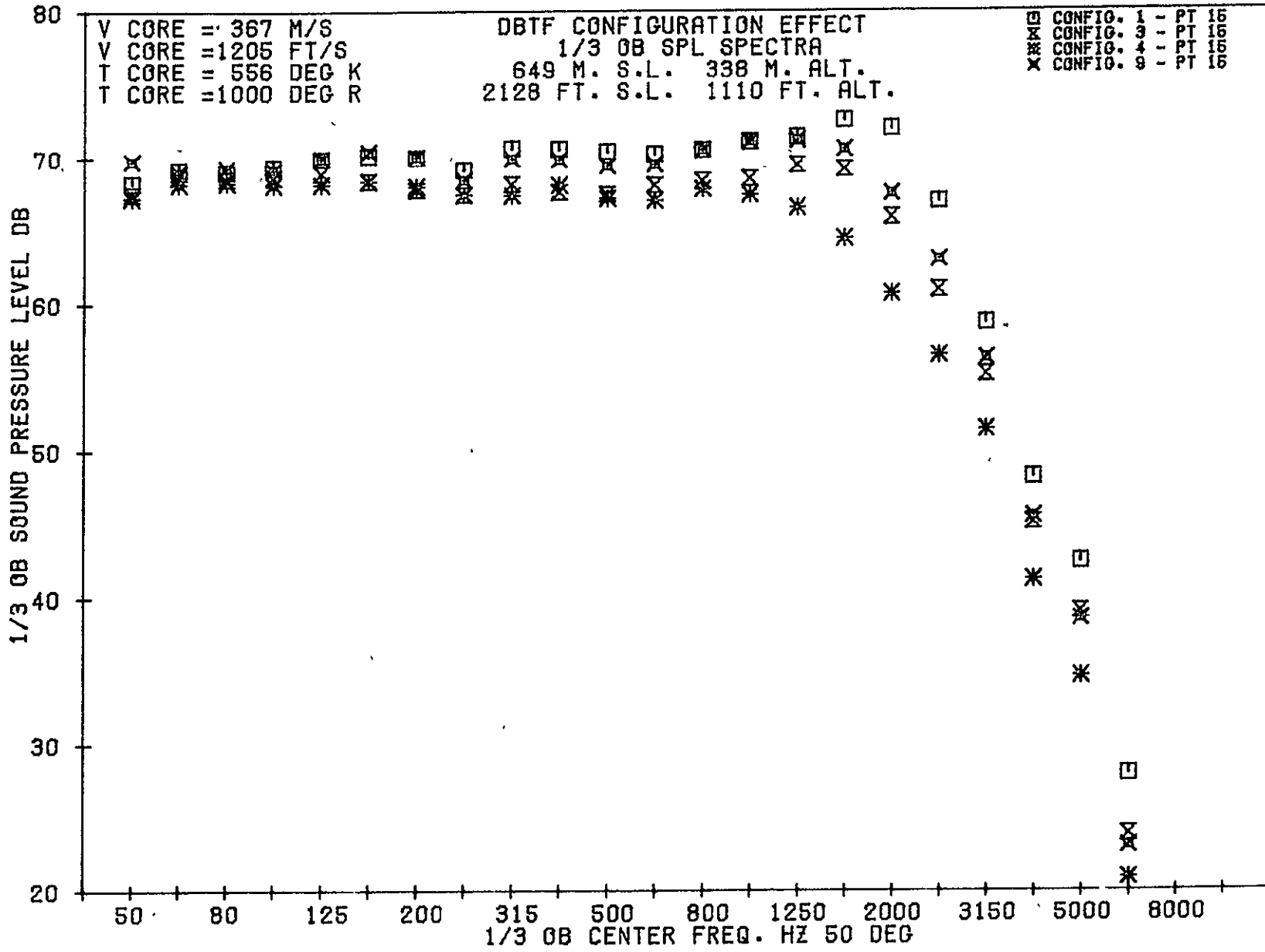
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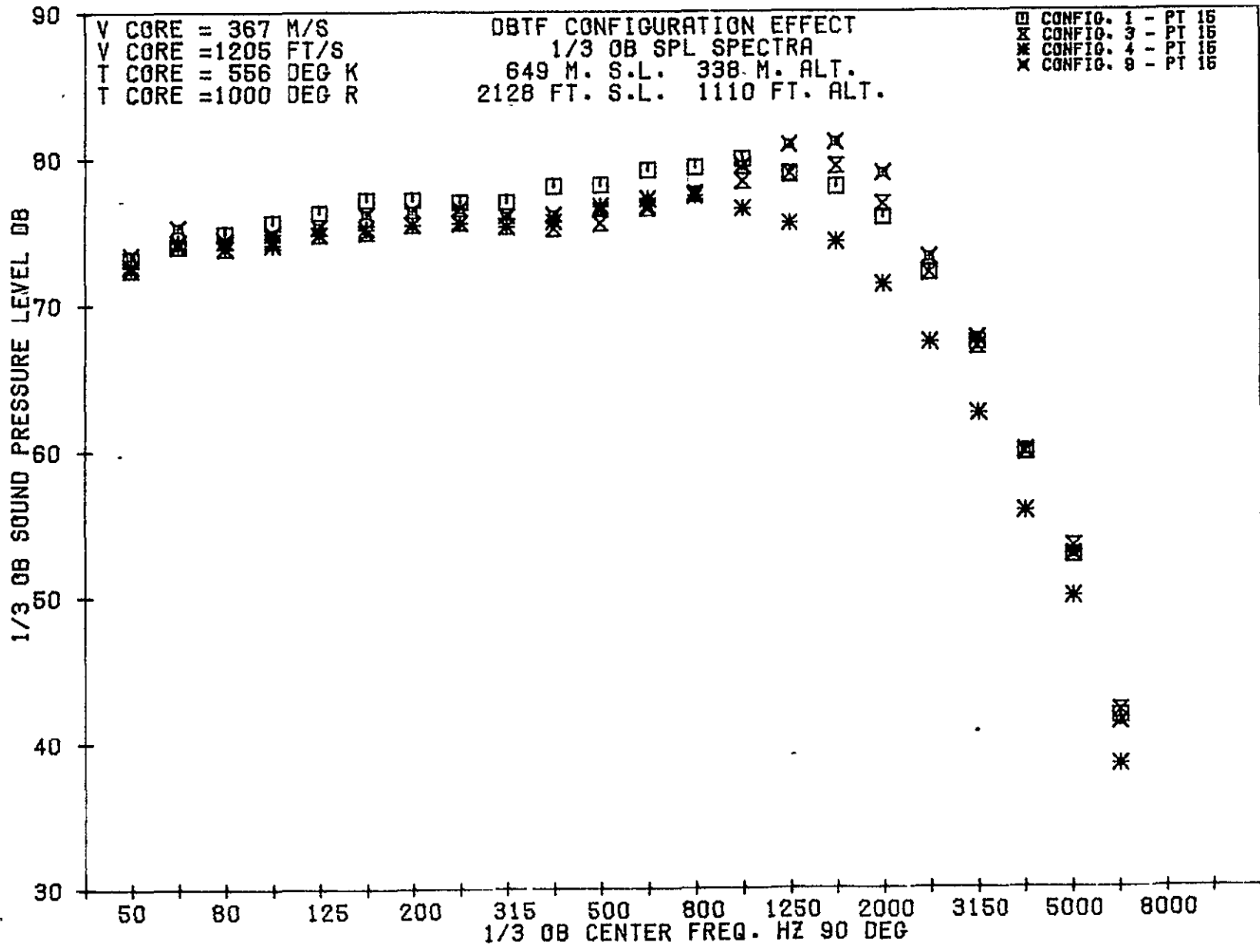
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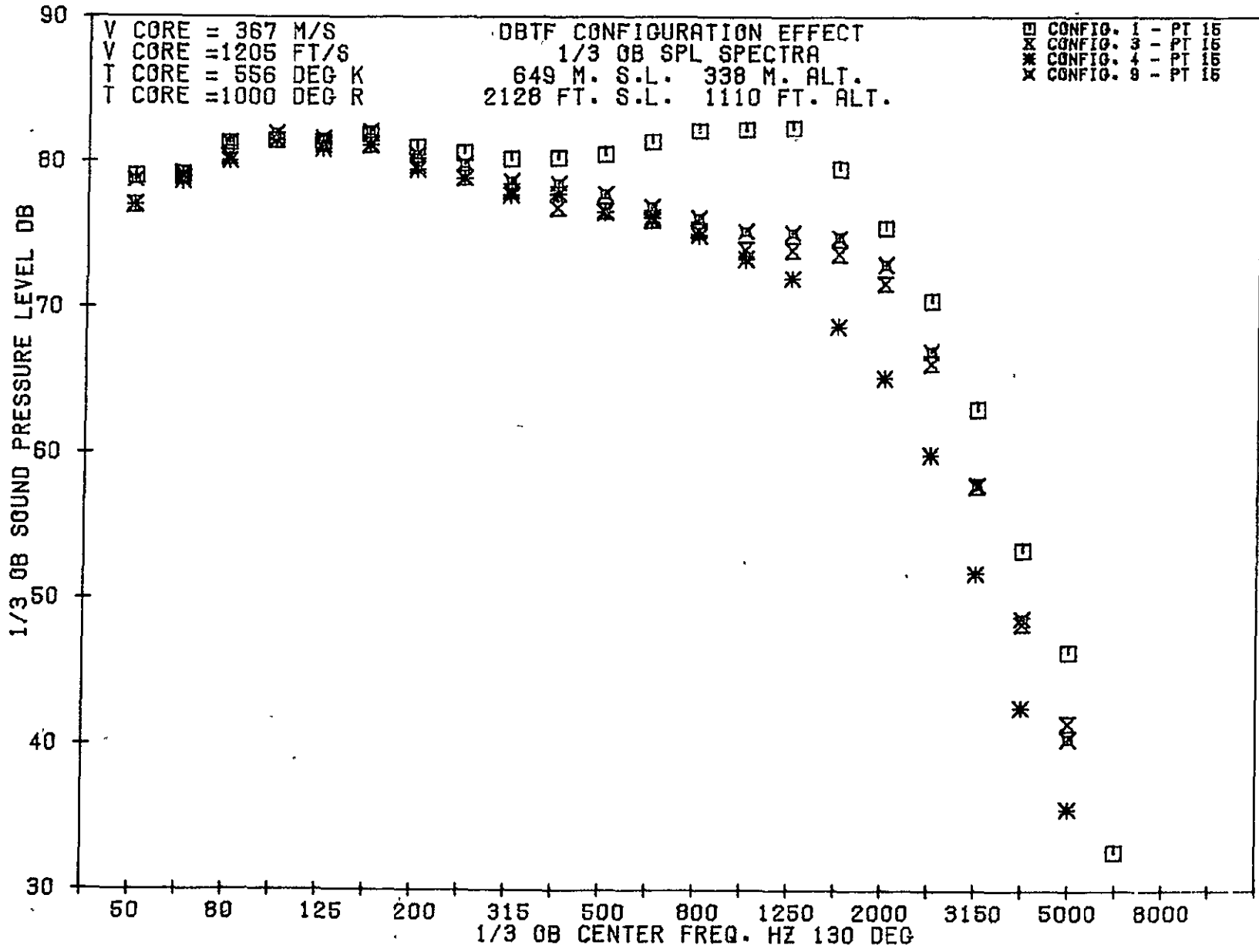
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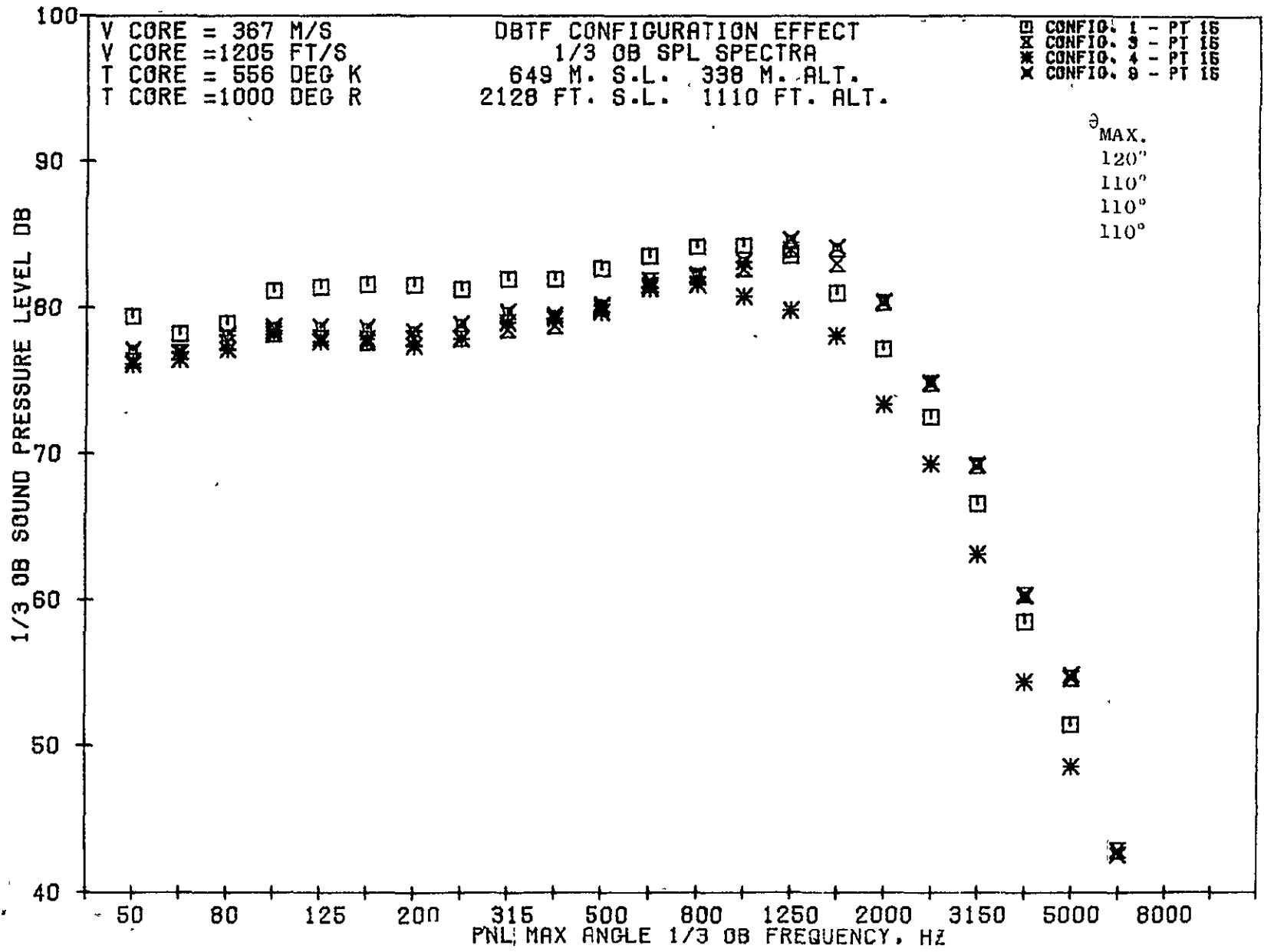
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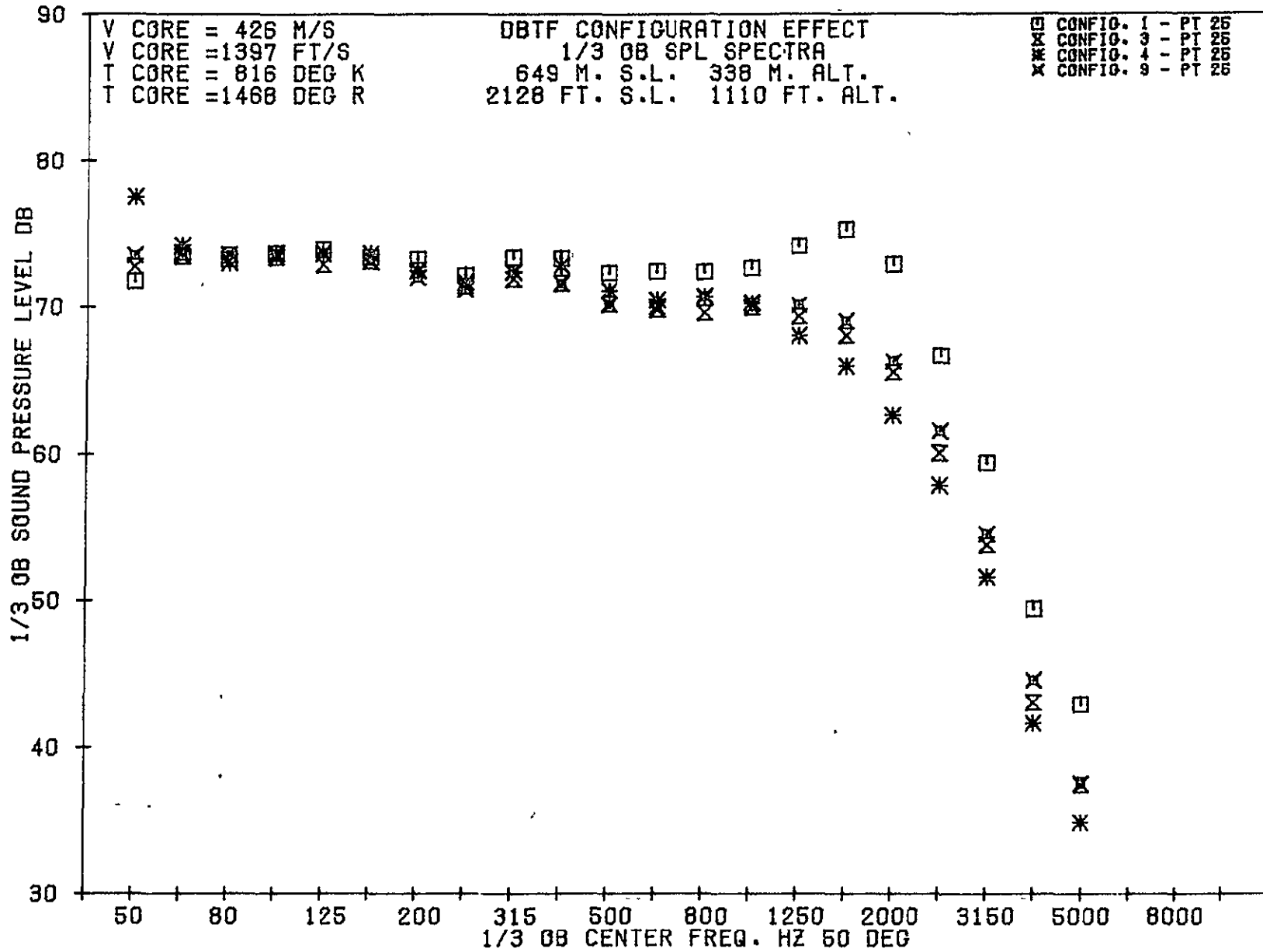
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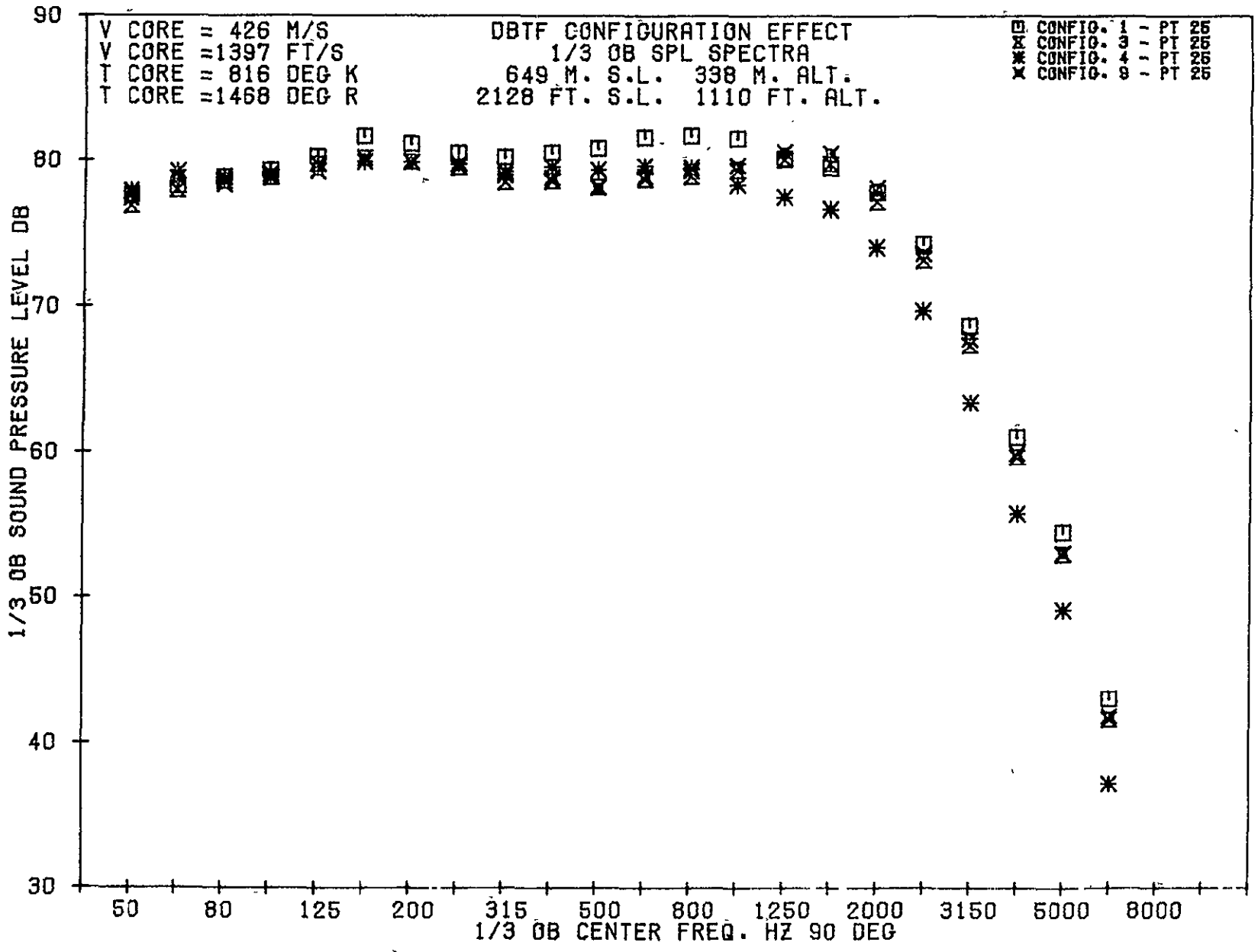


197

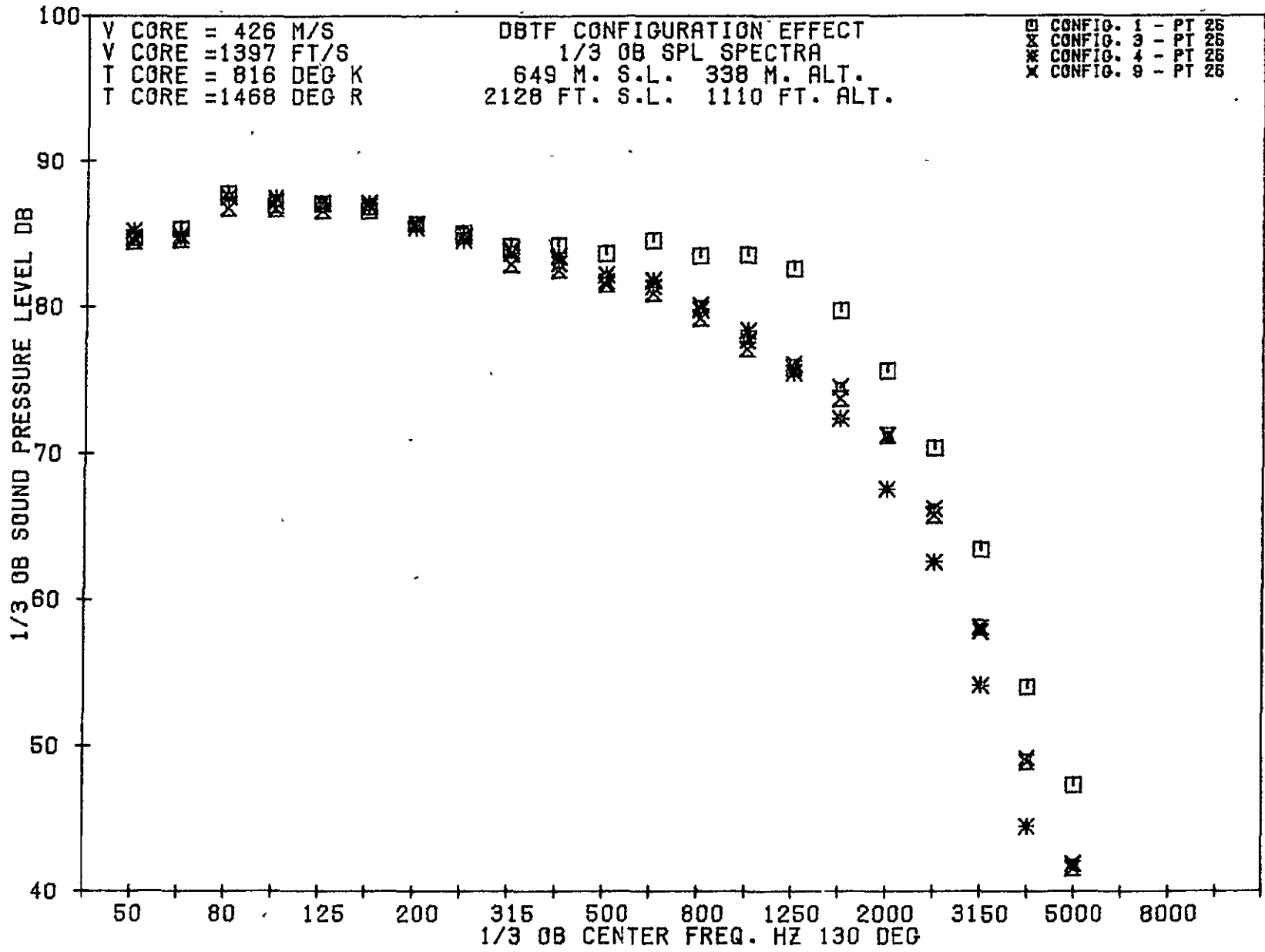
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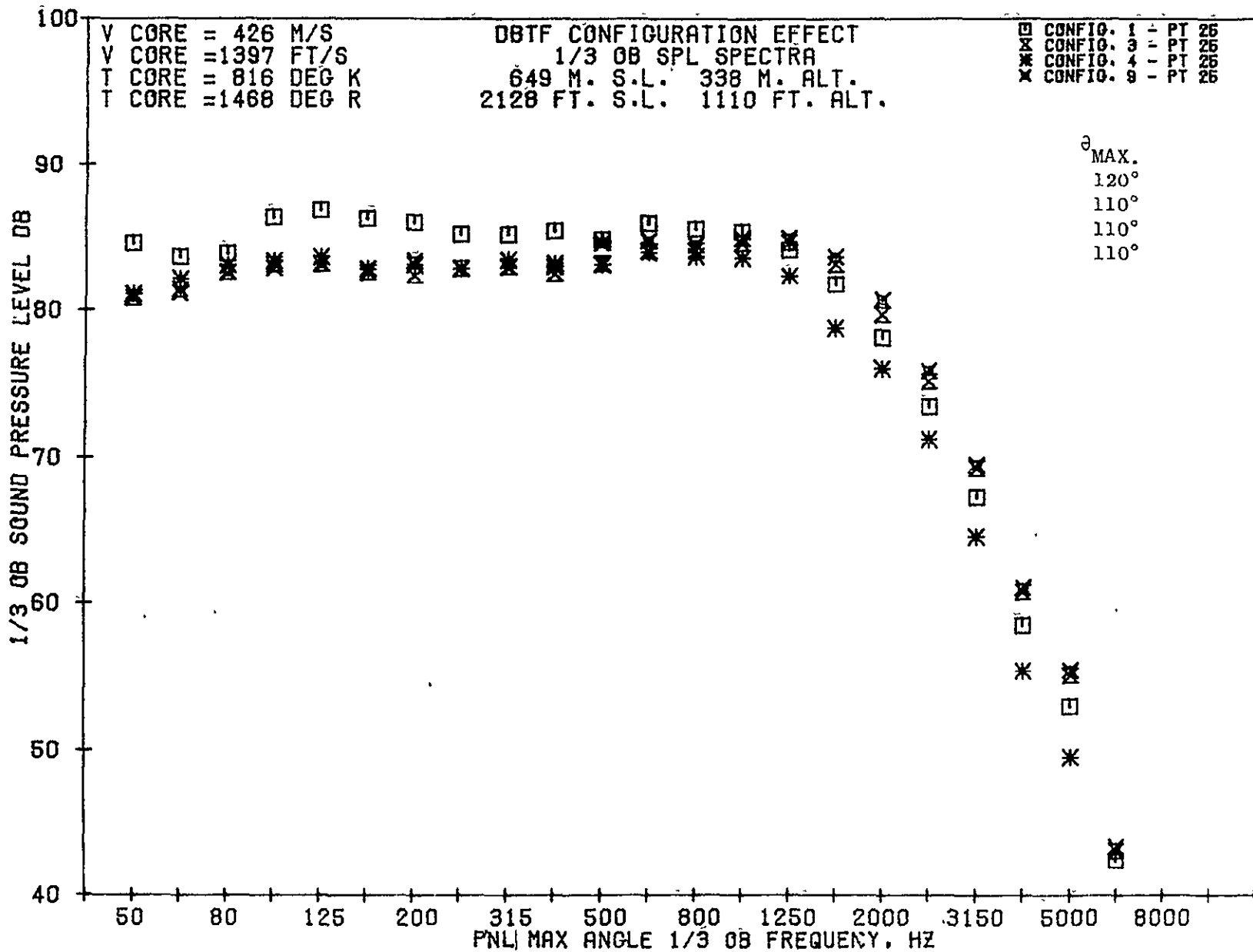
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4-6-7

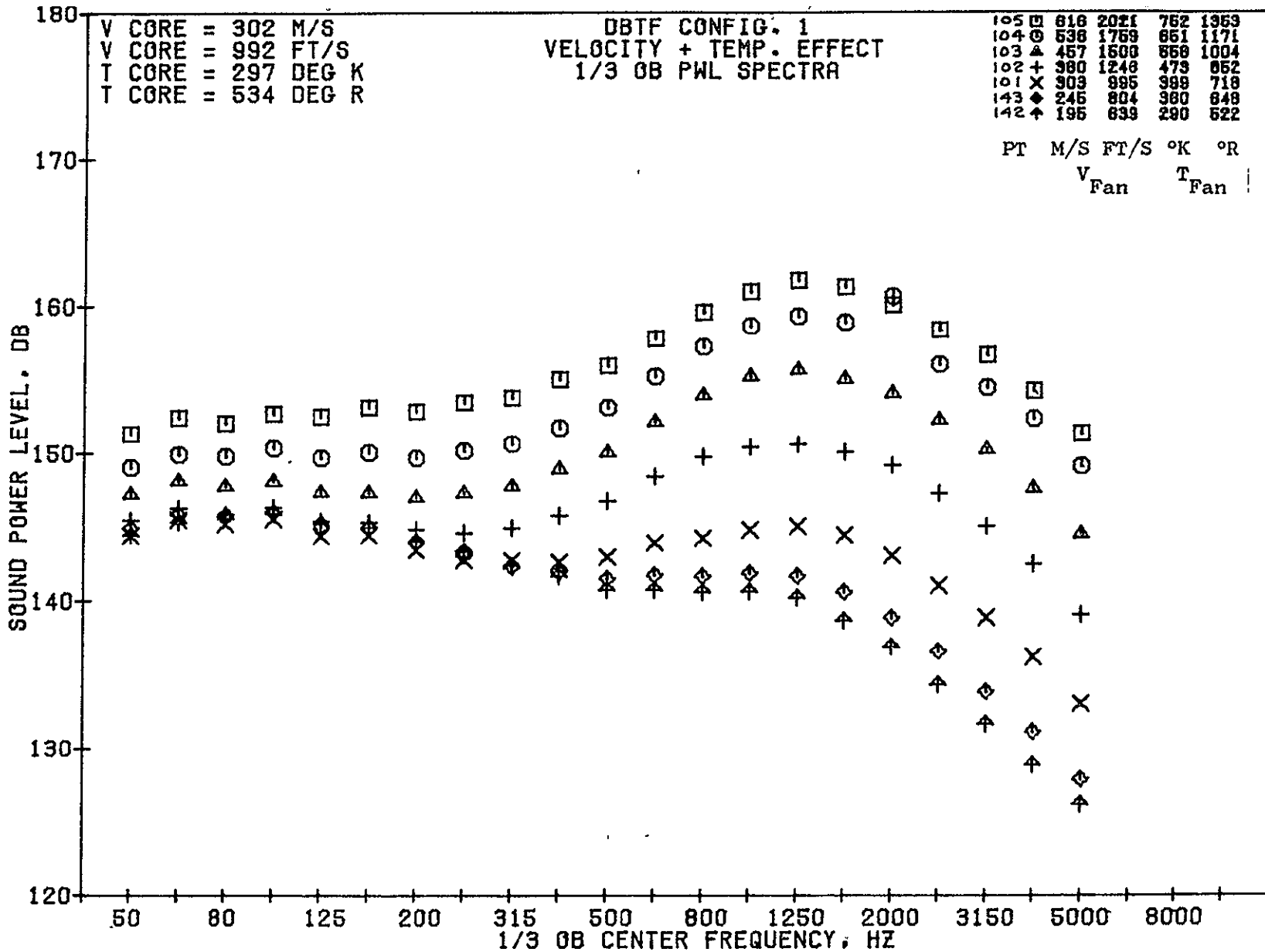
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463

**4.2 ACOUSTIC DATA PLOTS FOR A FULL SIZE ENGINE
UTILIZING A SCALE FACTOR OF 8**

1309



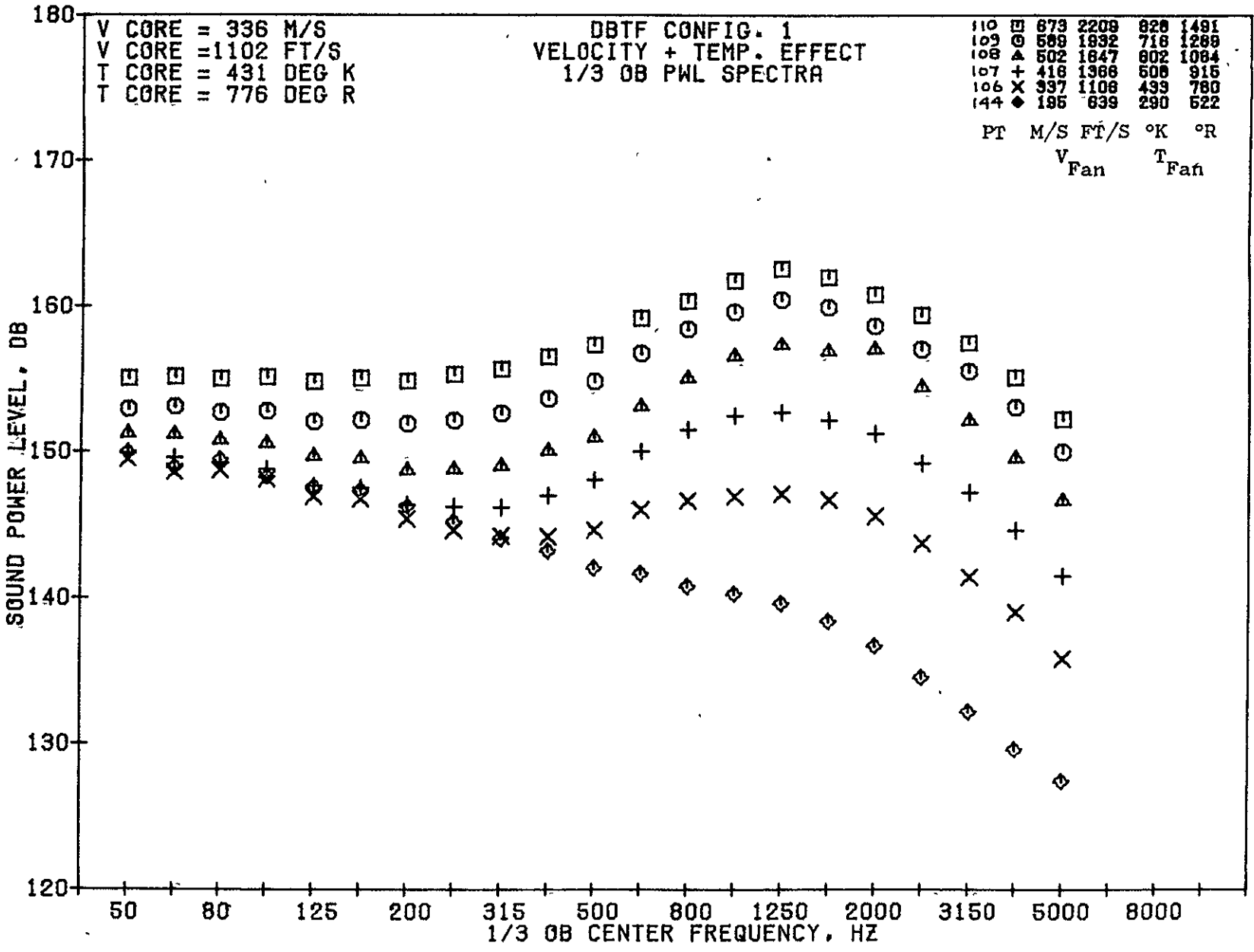
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79 BURCH A.

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108

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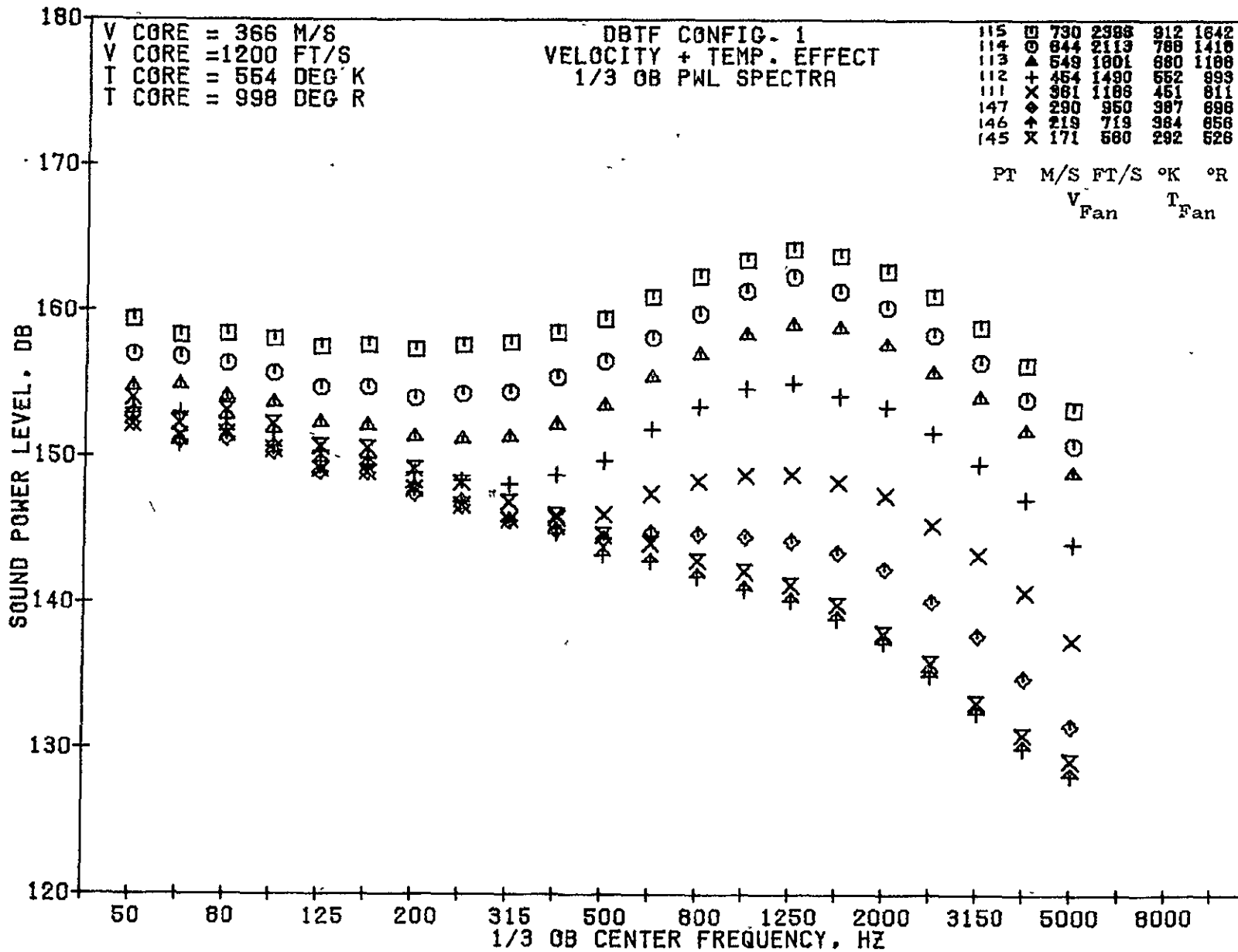


128

08/13/75
5R031-001

79 BURCORP.

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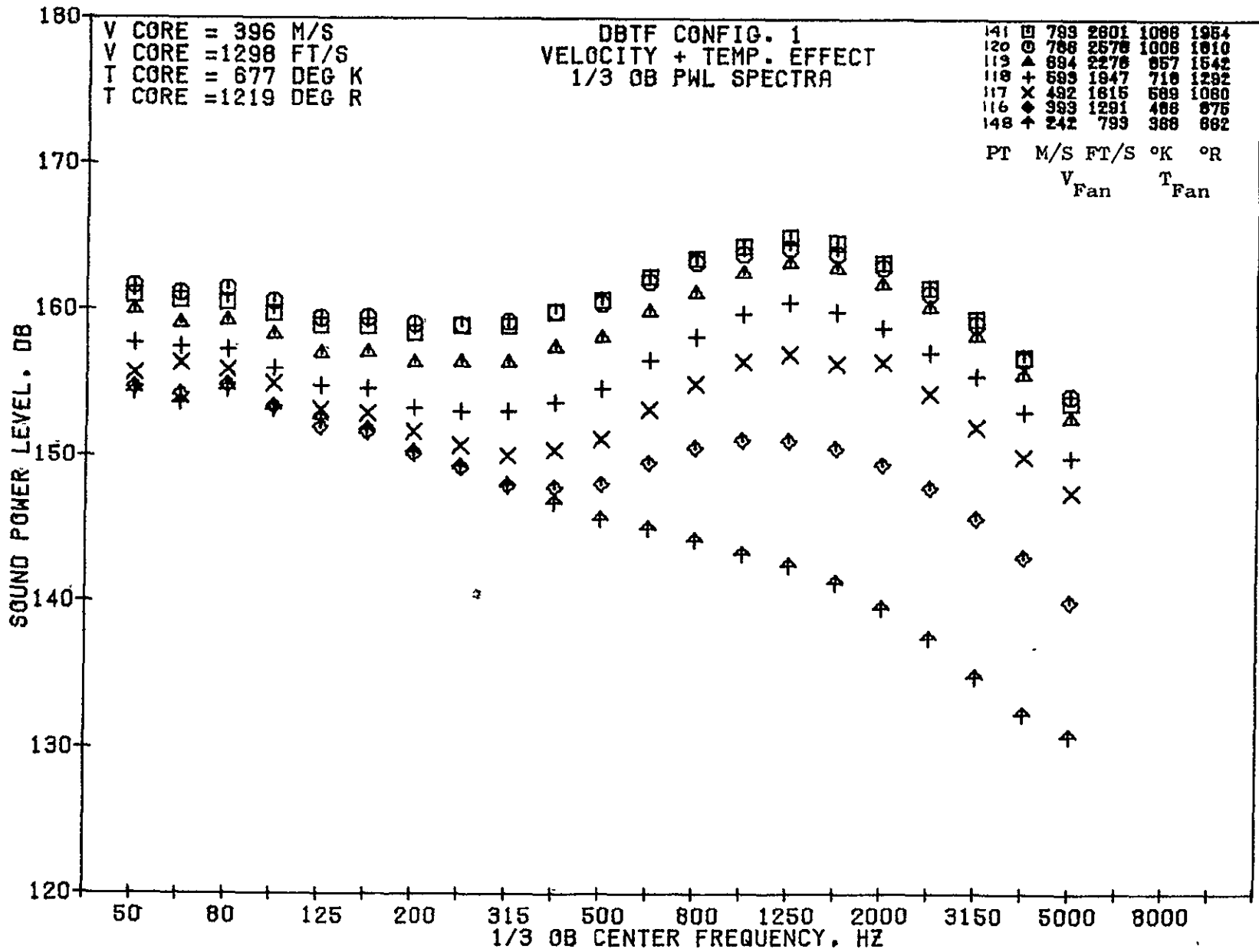


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79 BURCH A.

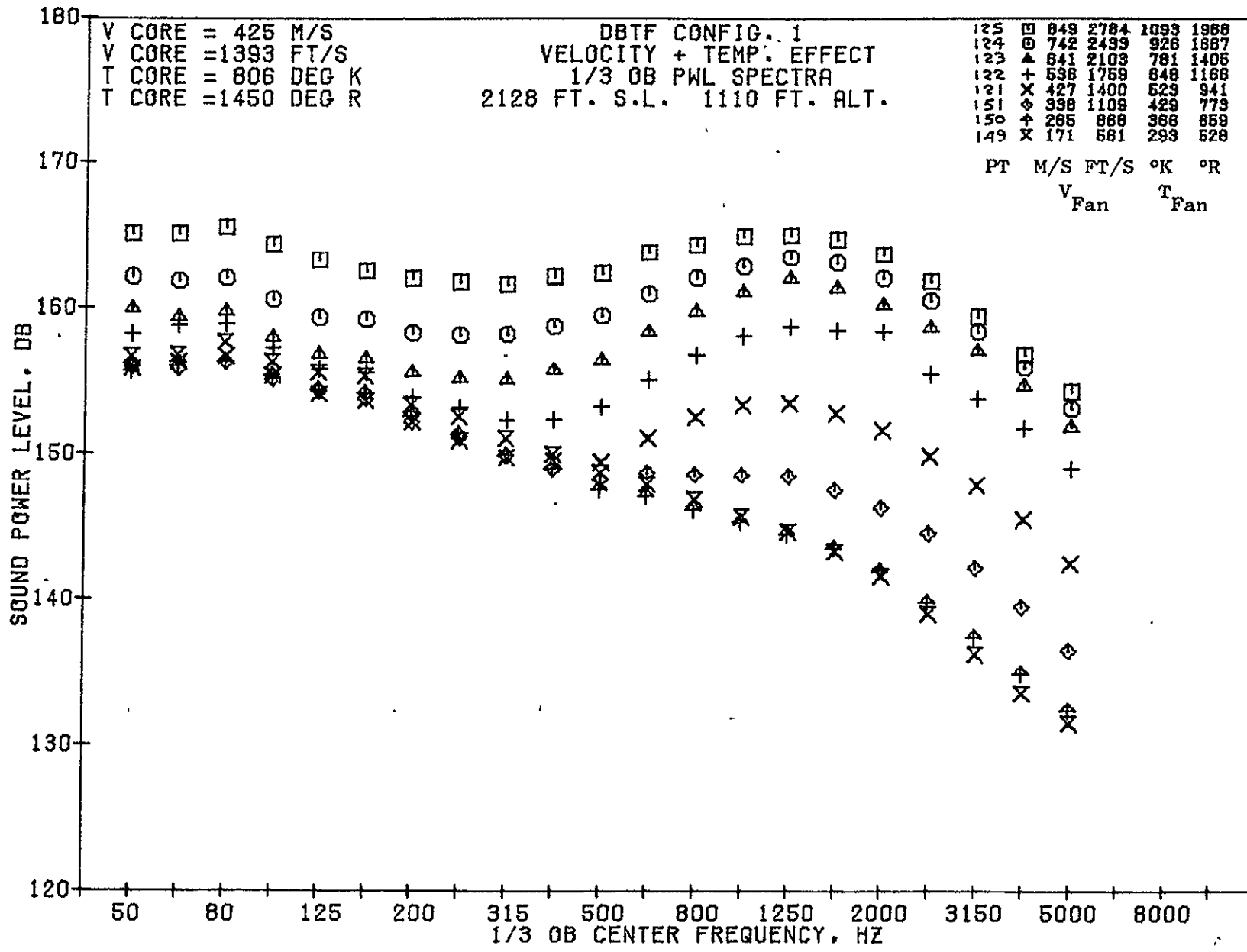
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5R031-001

79 BUROR A.

1313



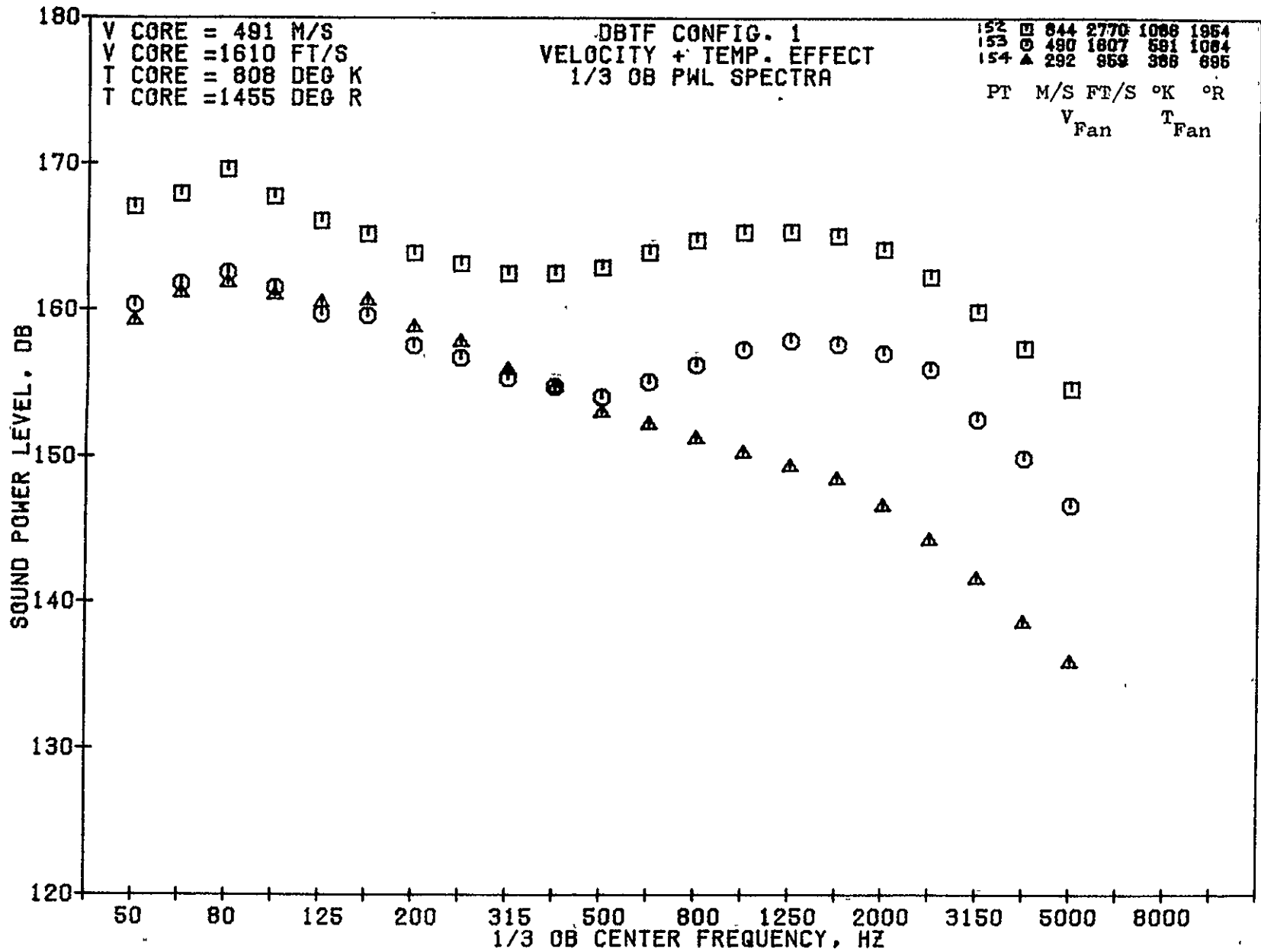
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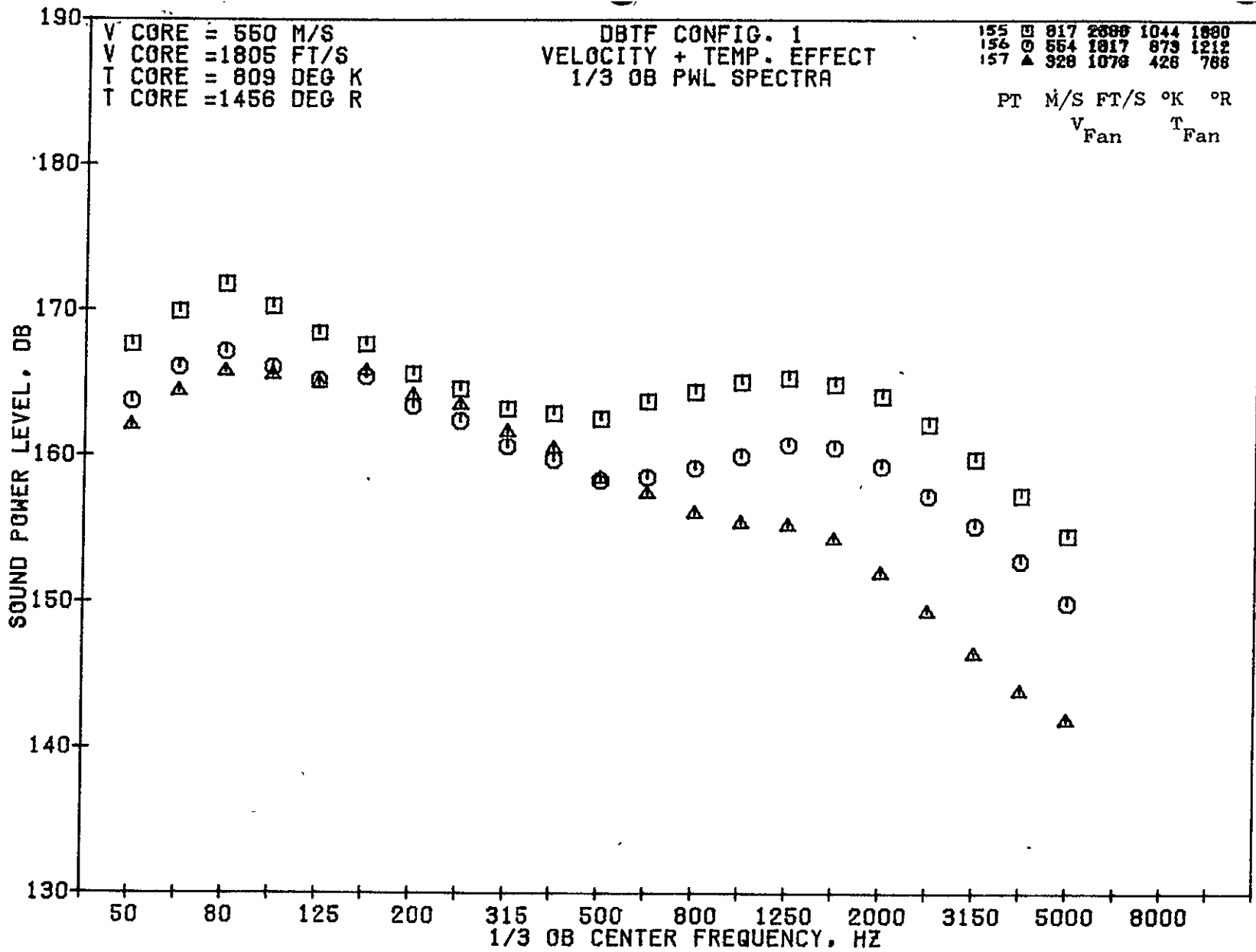
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187

08/13/75
5R031-001

79 BURC



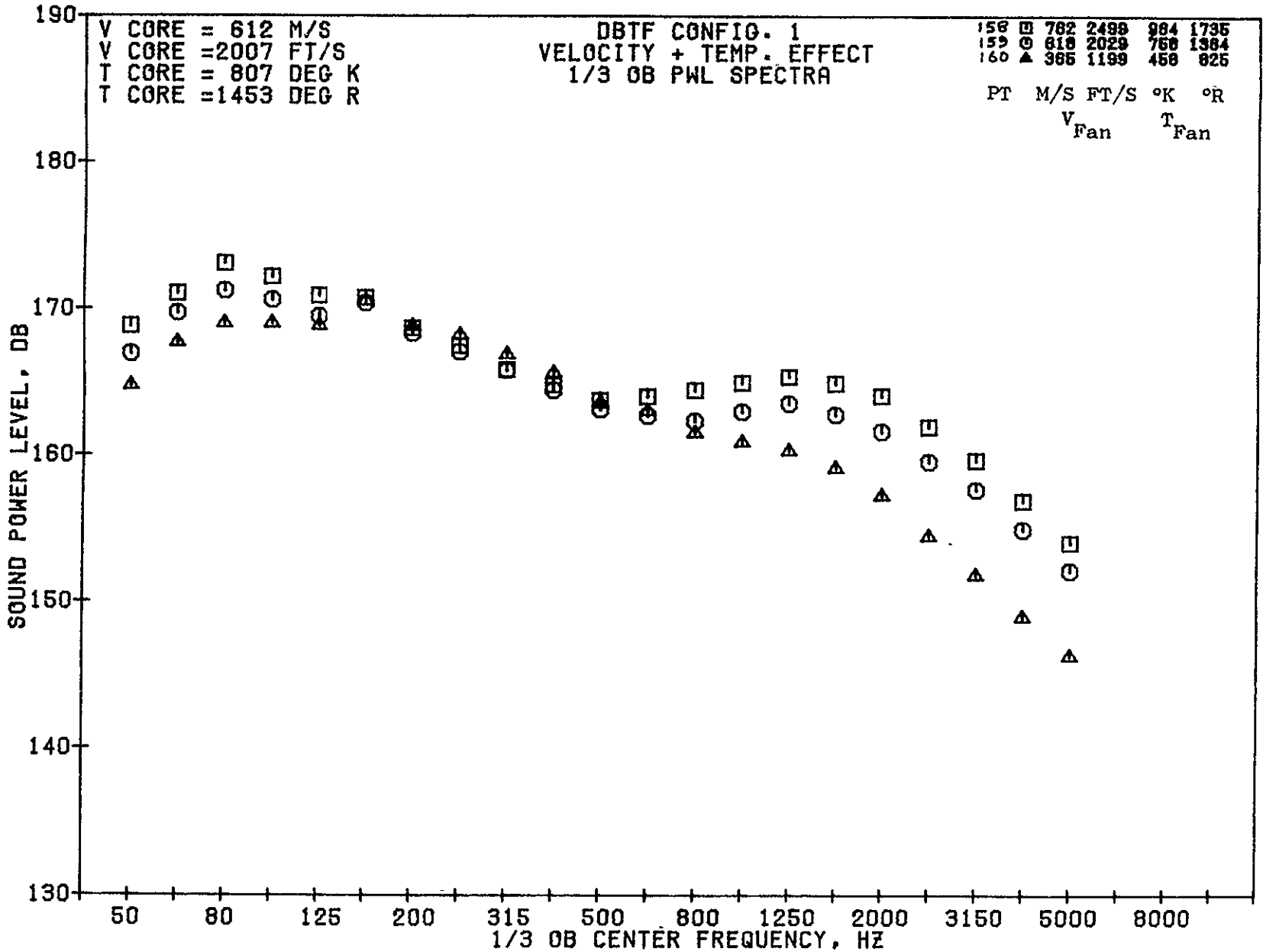
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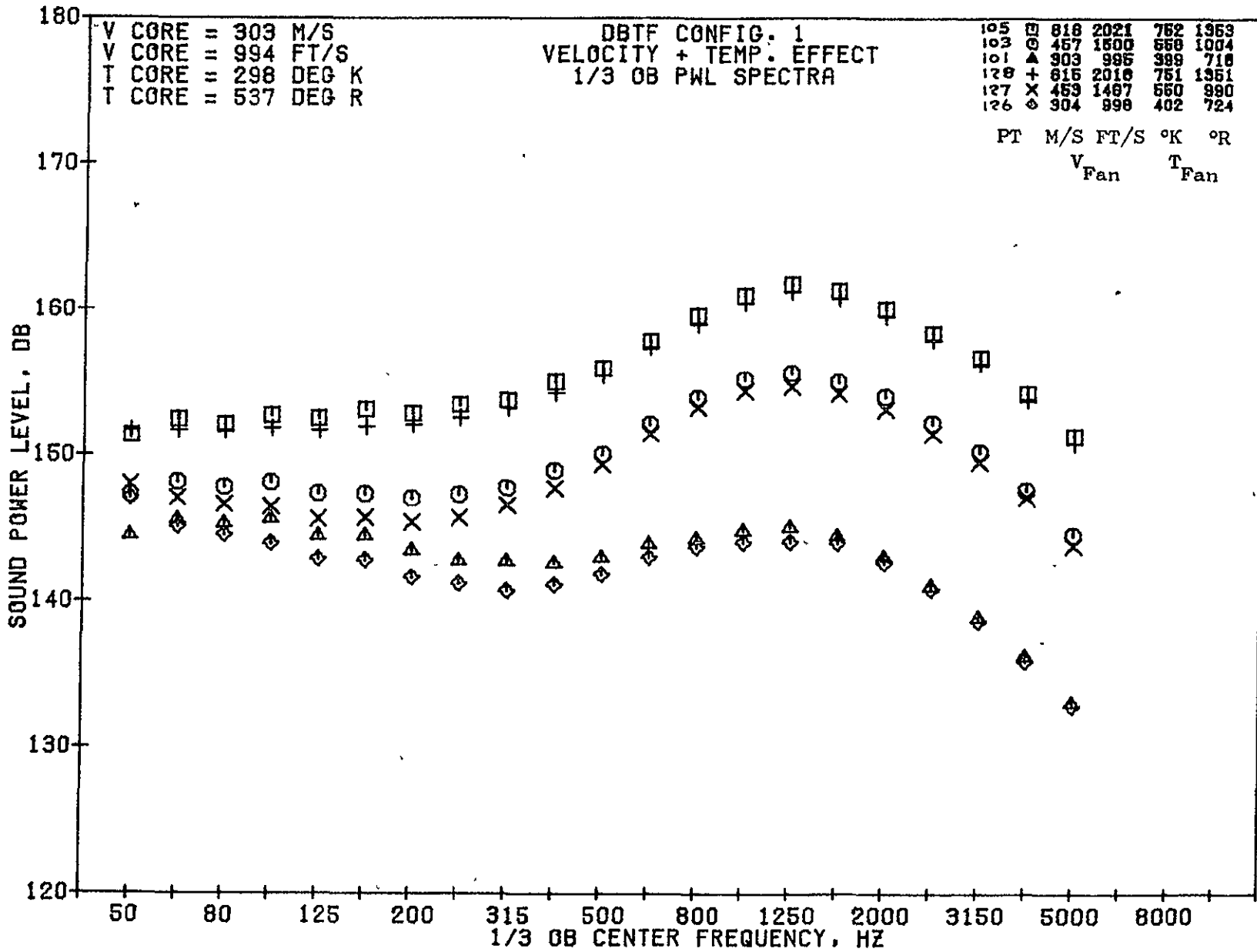


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79 BURCOR

1317



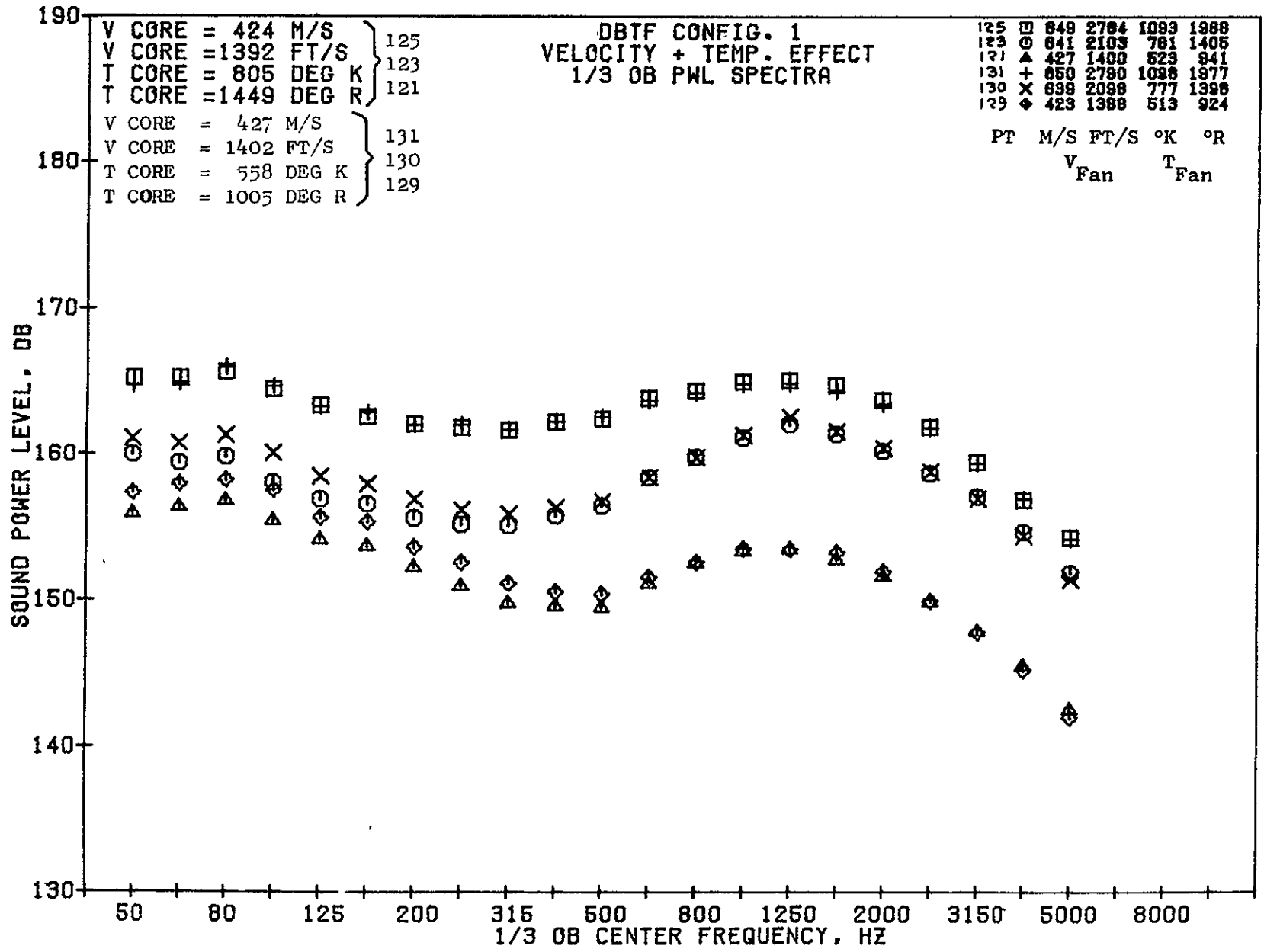
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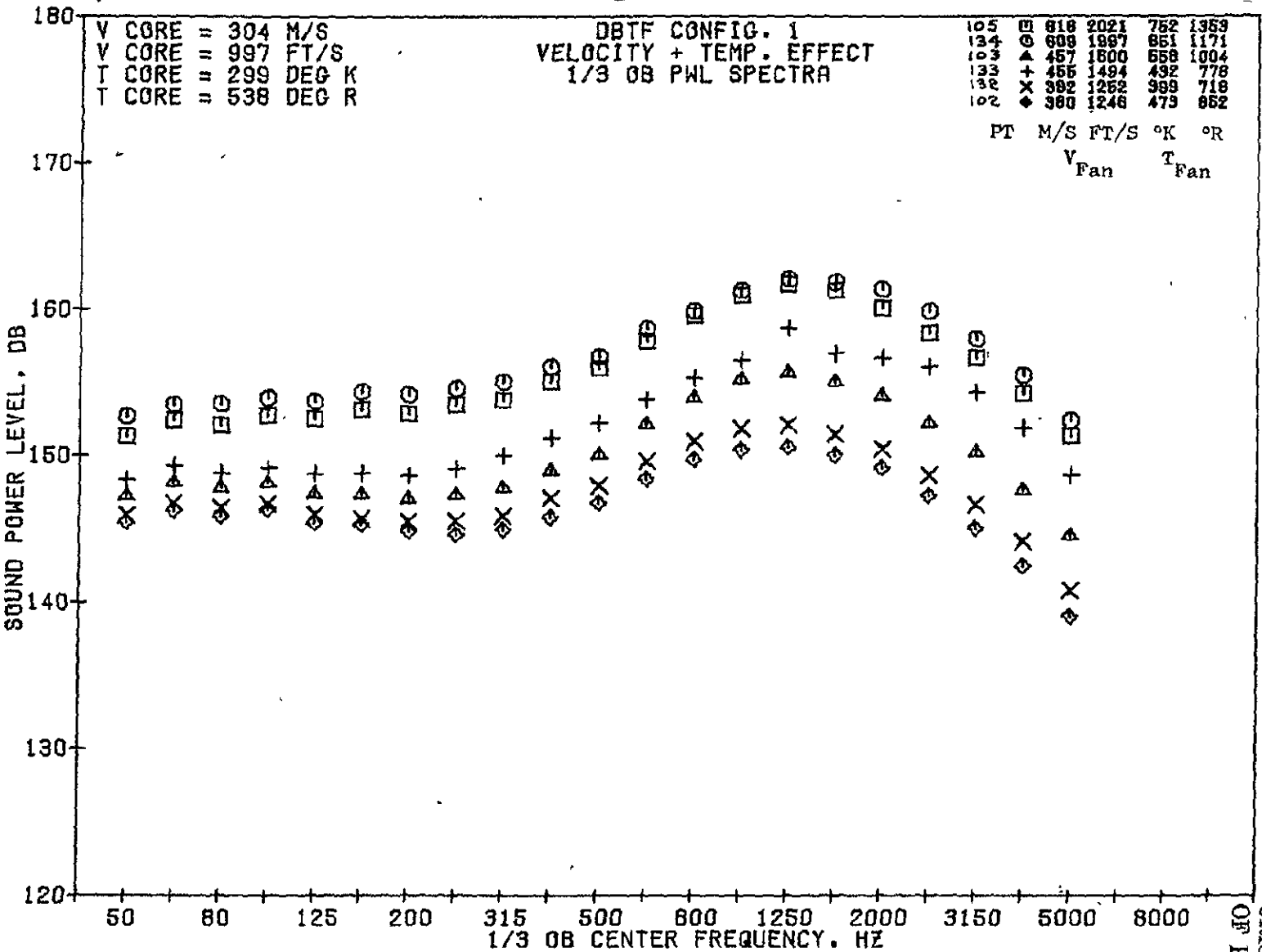
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 5R031-001

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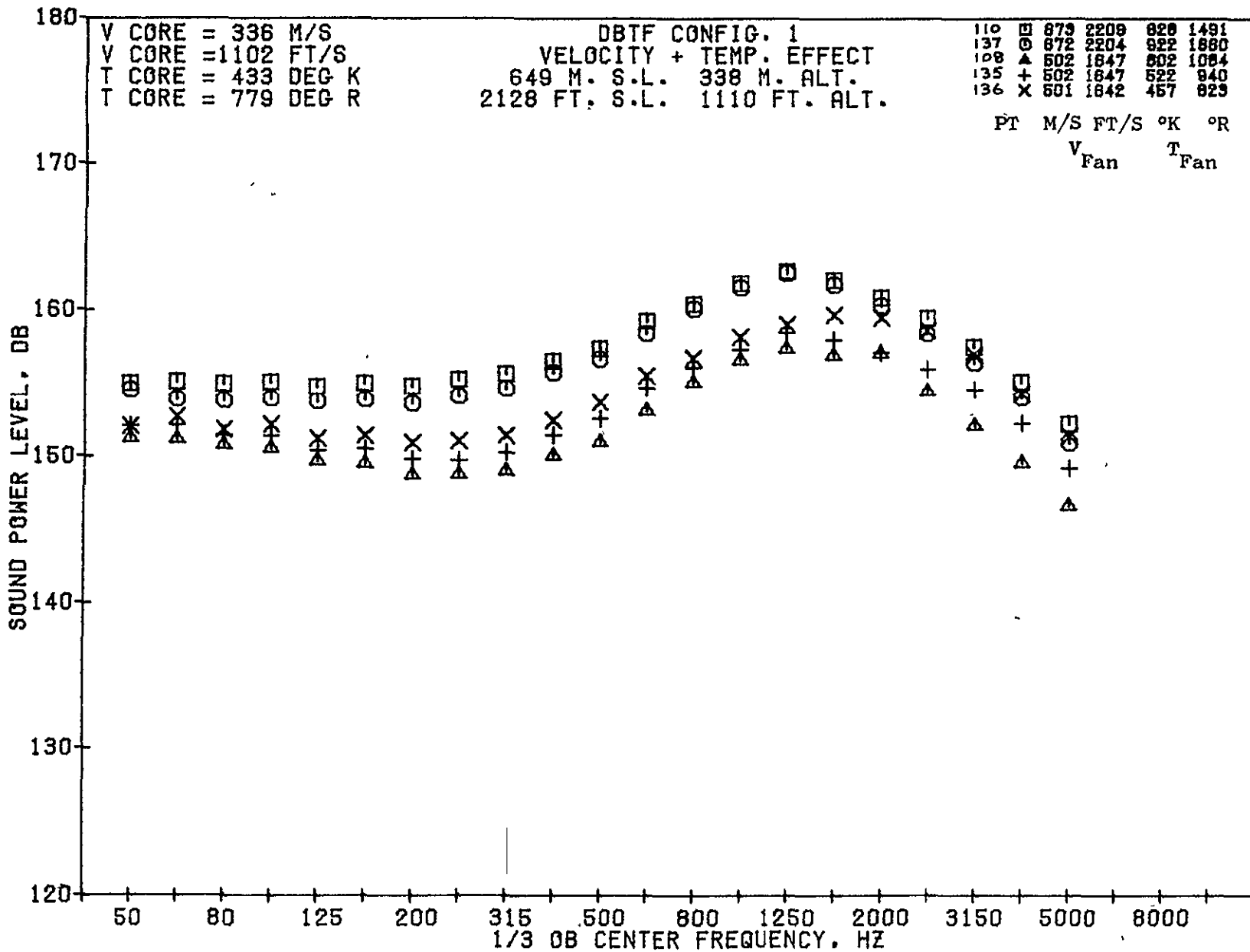


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79 BURCH

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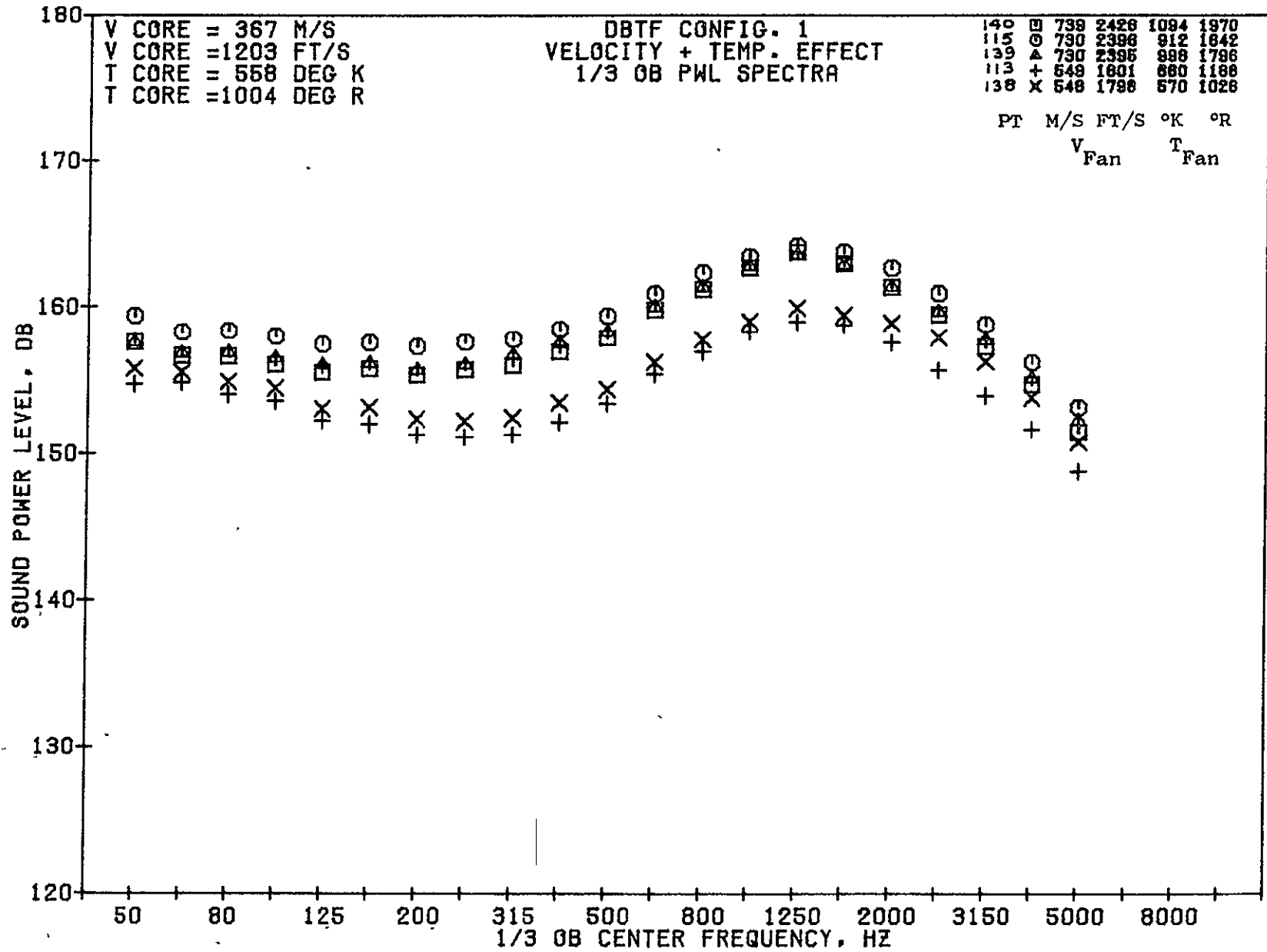


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1983

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 5R266-001

79 BURCI



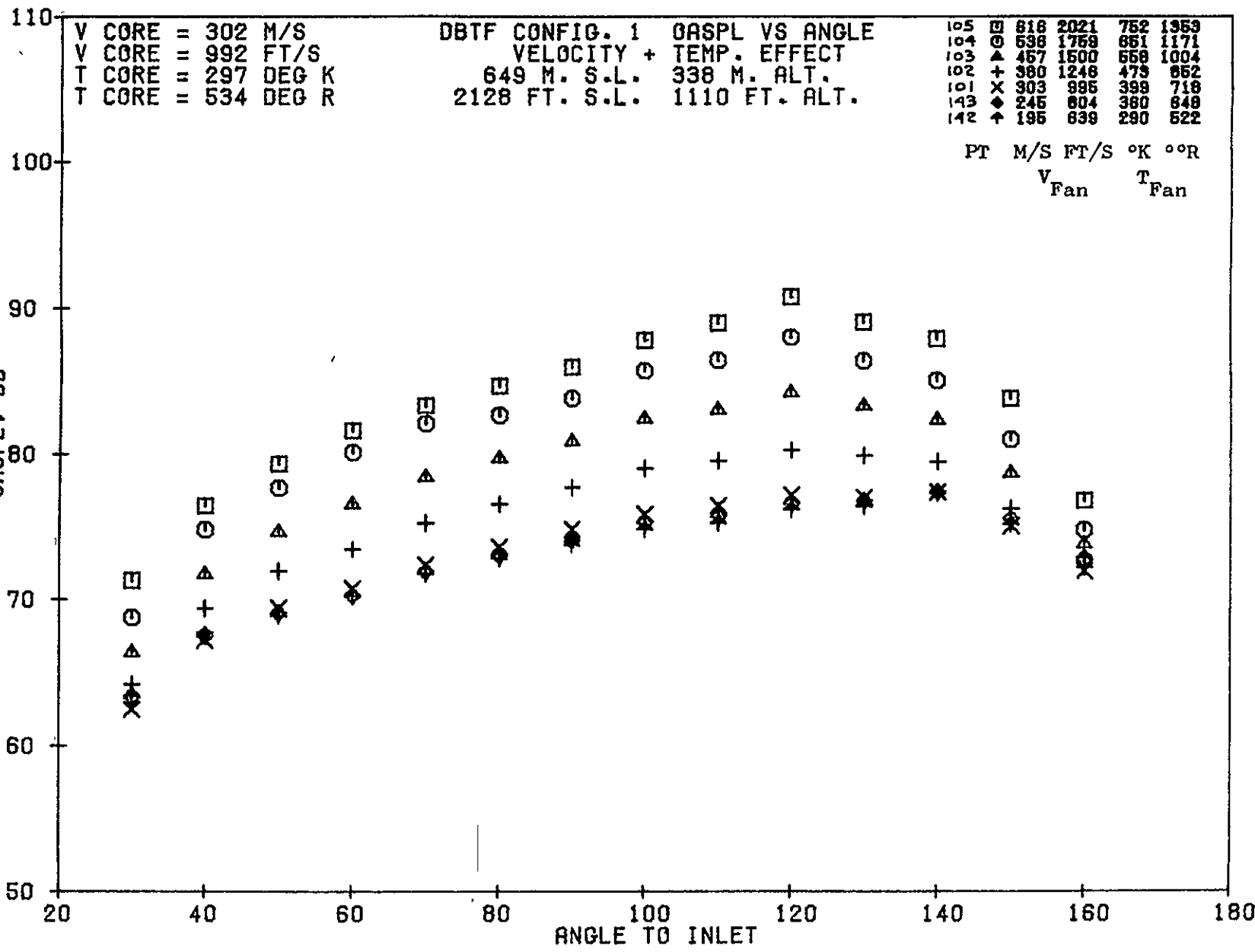
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79 BURCH A.

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4-94



56-7

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5R031-001

79 BURC

110
100
90
80
70
60
50

V CORE = 336 M/S
V CORE = 1102 FT/S
T CORE = 431 DEG K
T CORE = 776 DEG R

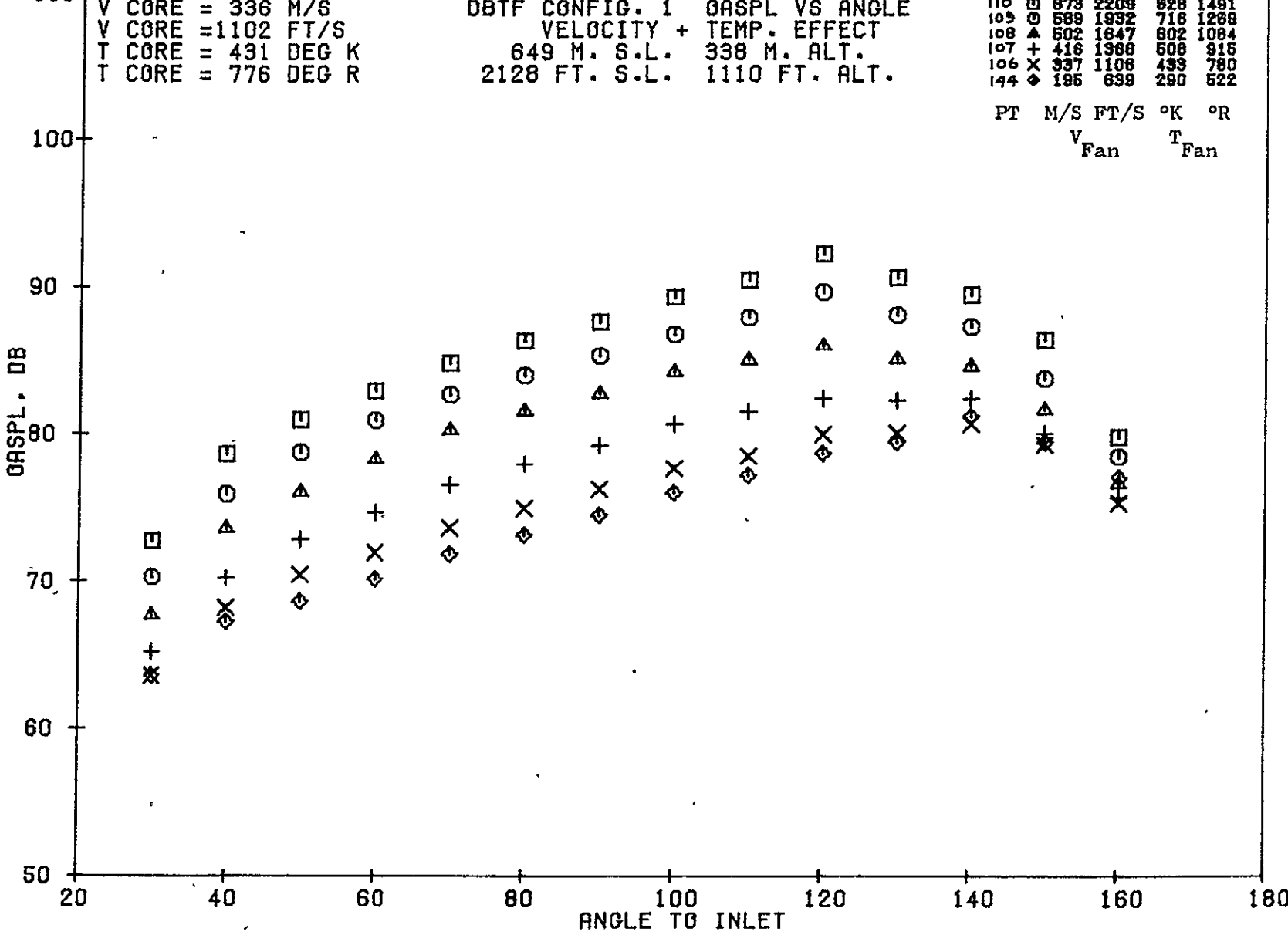
DBTF CONFIG. 1 GASPL VS ANGLE
VELOCITY + TEMP. EFFECT
649 M. S.L. 338 M. ALT.
2128 FT. S.L. 1110 FT. ALT.

110	□	873	2209	828	1491
109	○	589	1932	716	1288
108	▲	502	1847	602	1084
107	+	418	1988	508	915
106	X	337	1108	433	780
144	◇	186	638	290	522

PT M/S FT/S °K °R
V_{Fan} T_{Fan}

GASPL, DB

ANGLE TO INLET



1323

A 9/6

110

V CORE = 366 M/S
V CORE = 1200 FT/S
T CORE = 554 DEG K
T CORE = 998 DEG R

DBTF CONFIG. 1 OASPL VS ANGLE
VELOCITY + TEMP. EFFECT
649 M. S.L. 338 M. ALT.
2128 FT. S.L. 1110 FT. ALT.

115	□	730	2398	912	1842
114	○	644	2113	788	1418
113	△	549	1801	660	1189
112	+	464	1480	552	993
111	X	361	1188	451	811
147	◇	290	950	367	698
146	↑	219	719	364	656
145	X	171	580	292	528

PT M/S FT/S °K °R
V Fan T Fan

OASPL. DB

100

90

80

70

60

50

20 40 60 80 100 120 140 160 180

ANGLE TO INLET

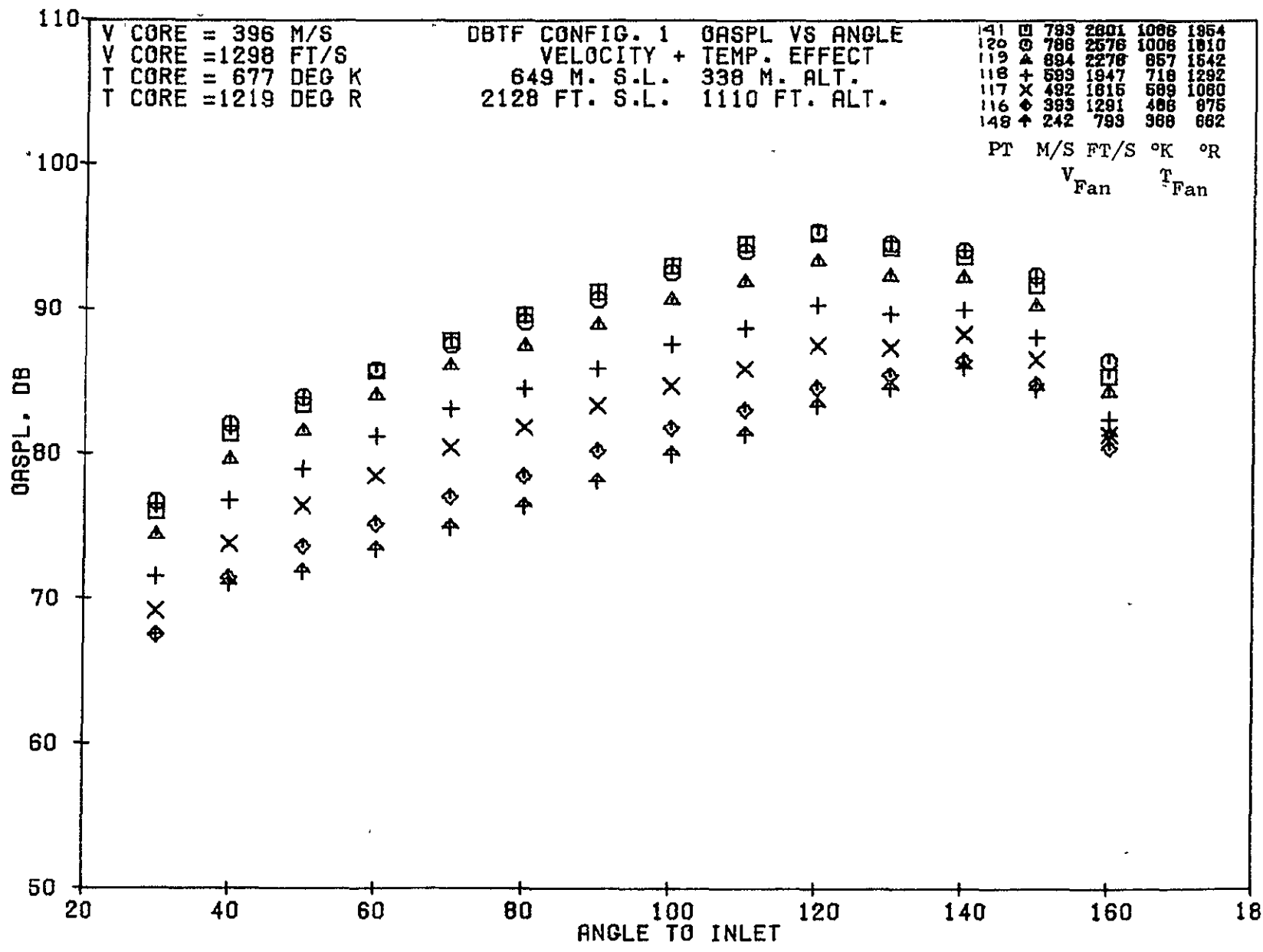
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4
1/2

08/13/75
SR031-001

79 BURC

1325



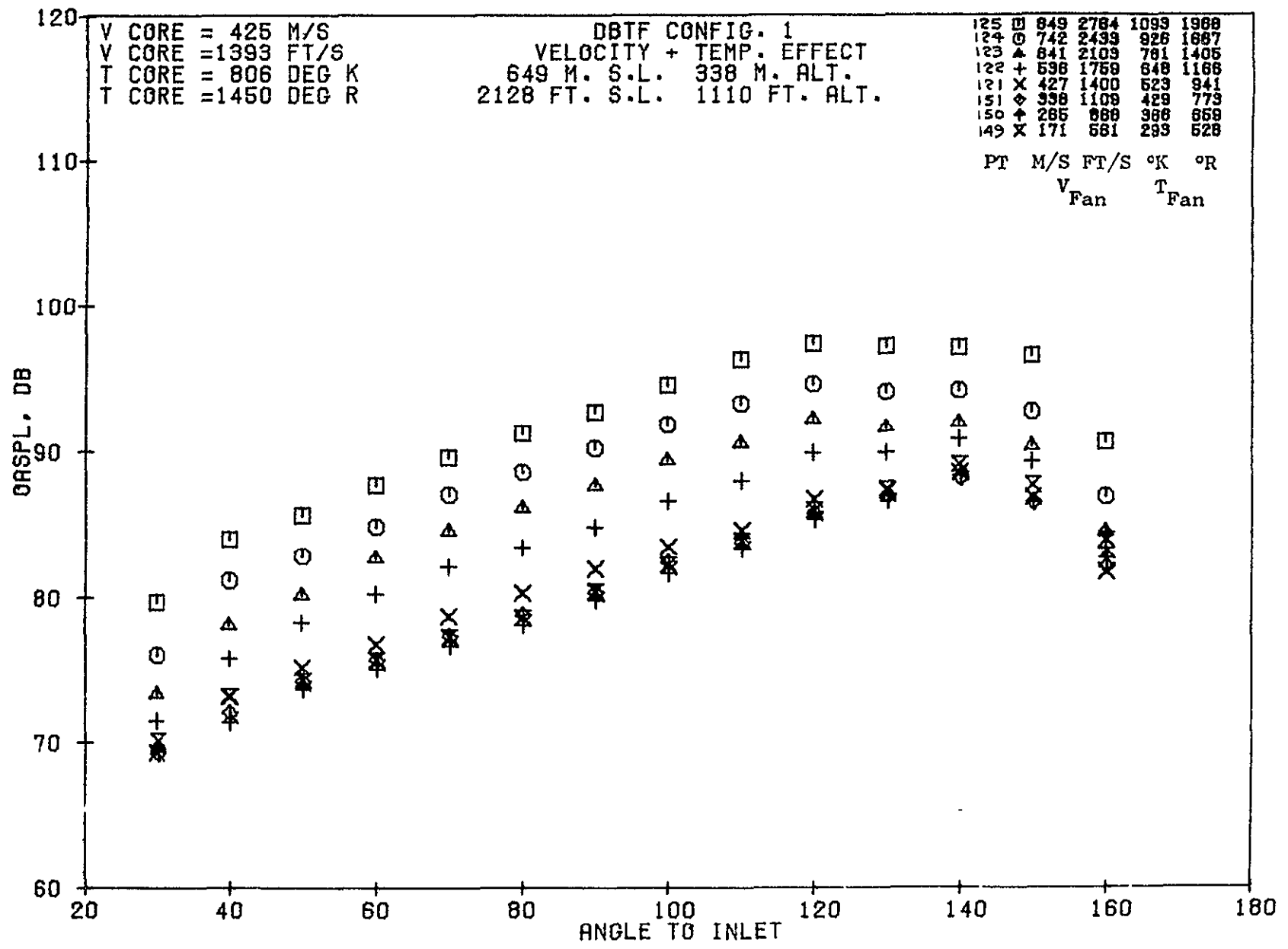
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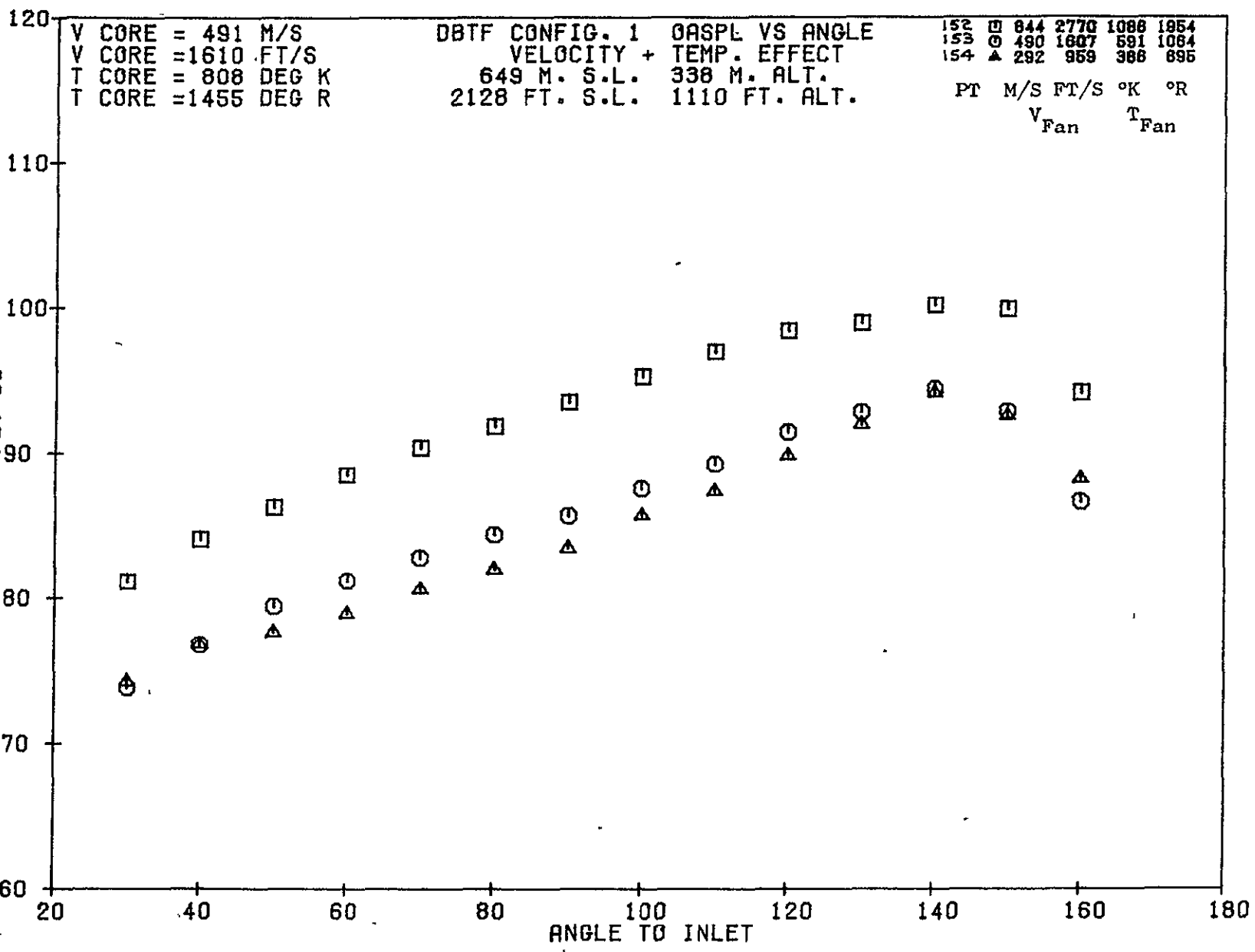
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79 BURCH



1327

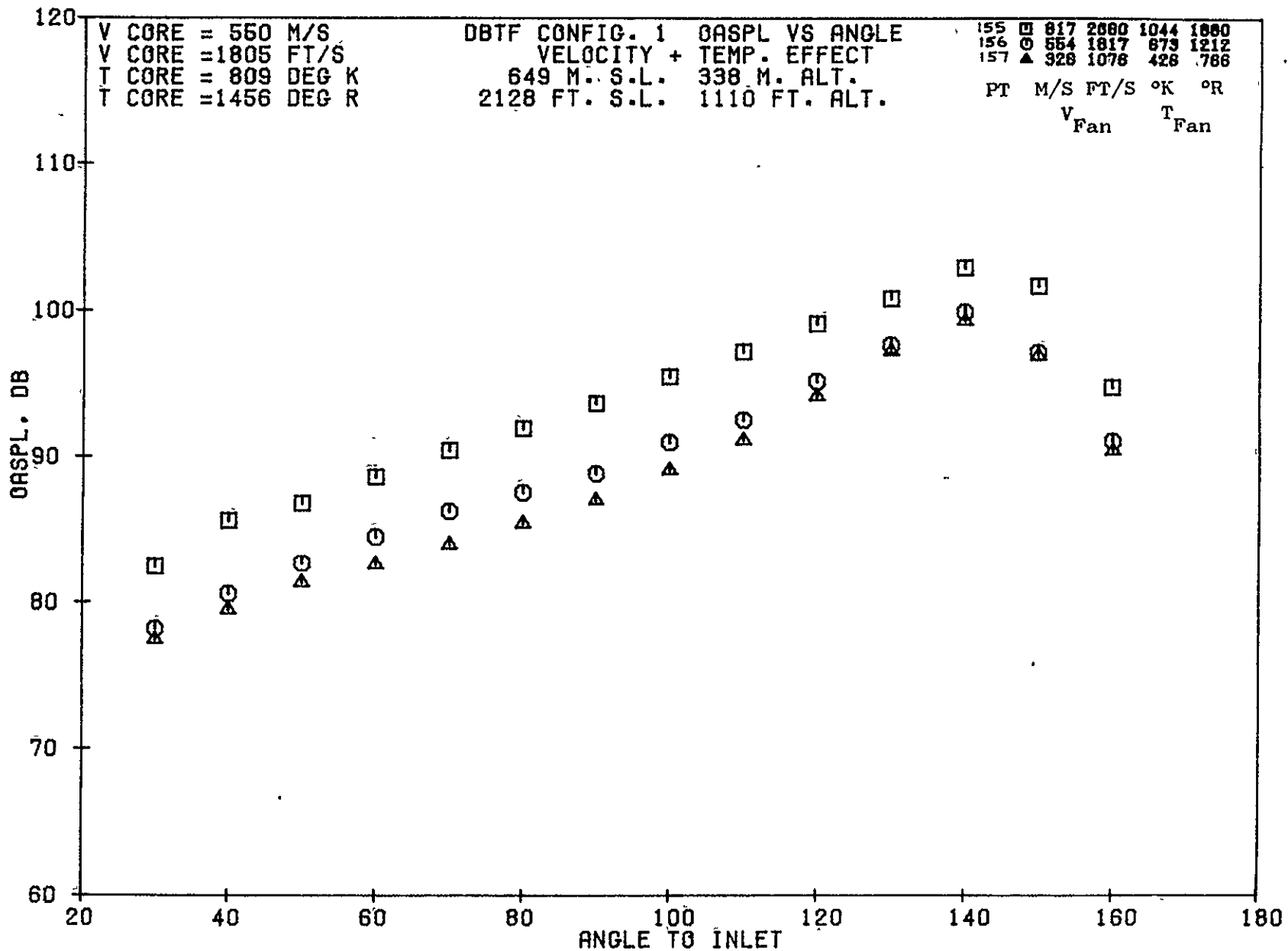
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4-100

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79 BURCH A.

1328



08/13/75
5R031-001.

79 BURQA.

120
110
100
90
80
70
60

V CORE = 612 M/S
V CORE = 2007 FT/S
T CORE = 807 DEG K
T CORE = 1453 DEG R

DBTF CONFIG. 1 GASPL VS ANGLE
VELOCITY + TEMP. EFFECT
649 M. S.L. 338 M. ALT.
2128 FT. S.L. 1110 FT. ALT.

158	782	2488	984	1738
159	818	2029	768	1384
160	385	1199	458	825
PT	M/S	FT/S	°K	°R
	V _{Fan}		T _{Fan}	

GASPL, DB

ANGLE TO INLET

1329

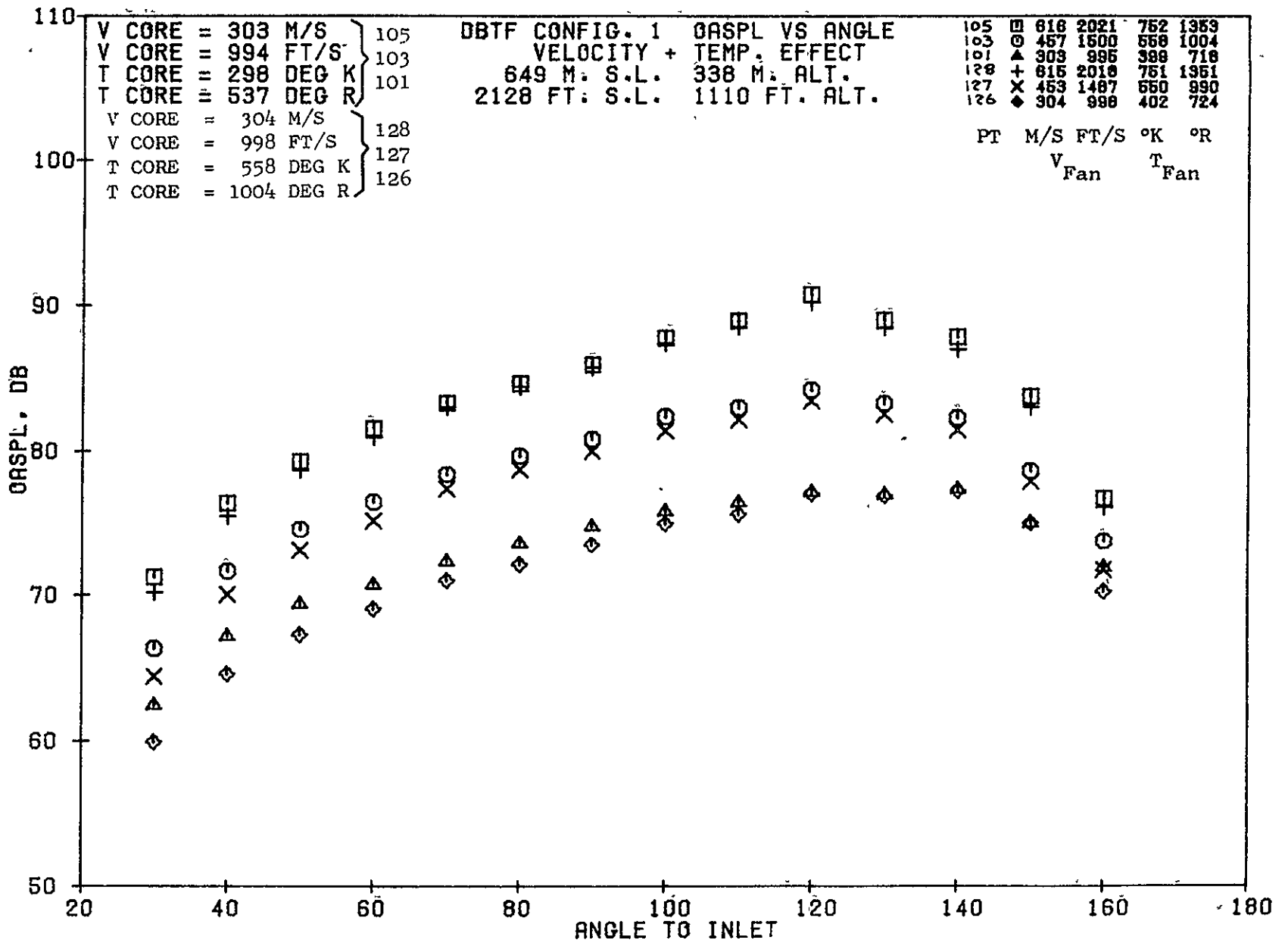
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79 BURCH A.

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1330

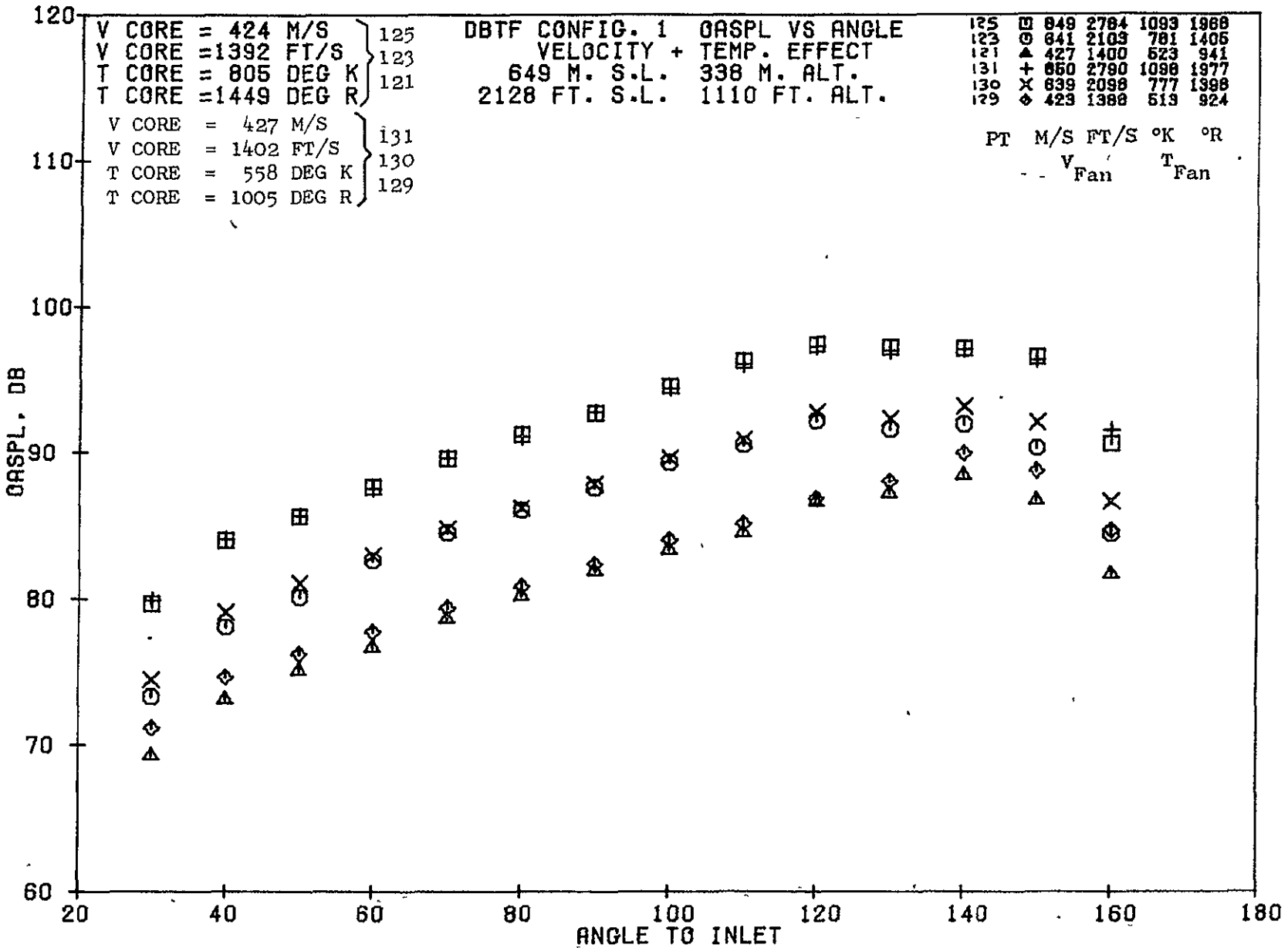


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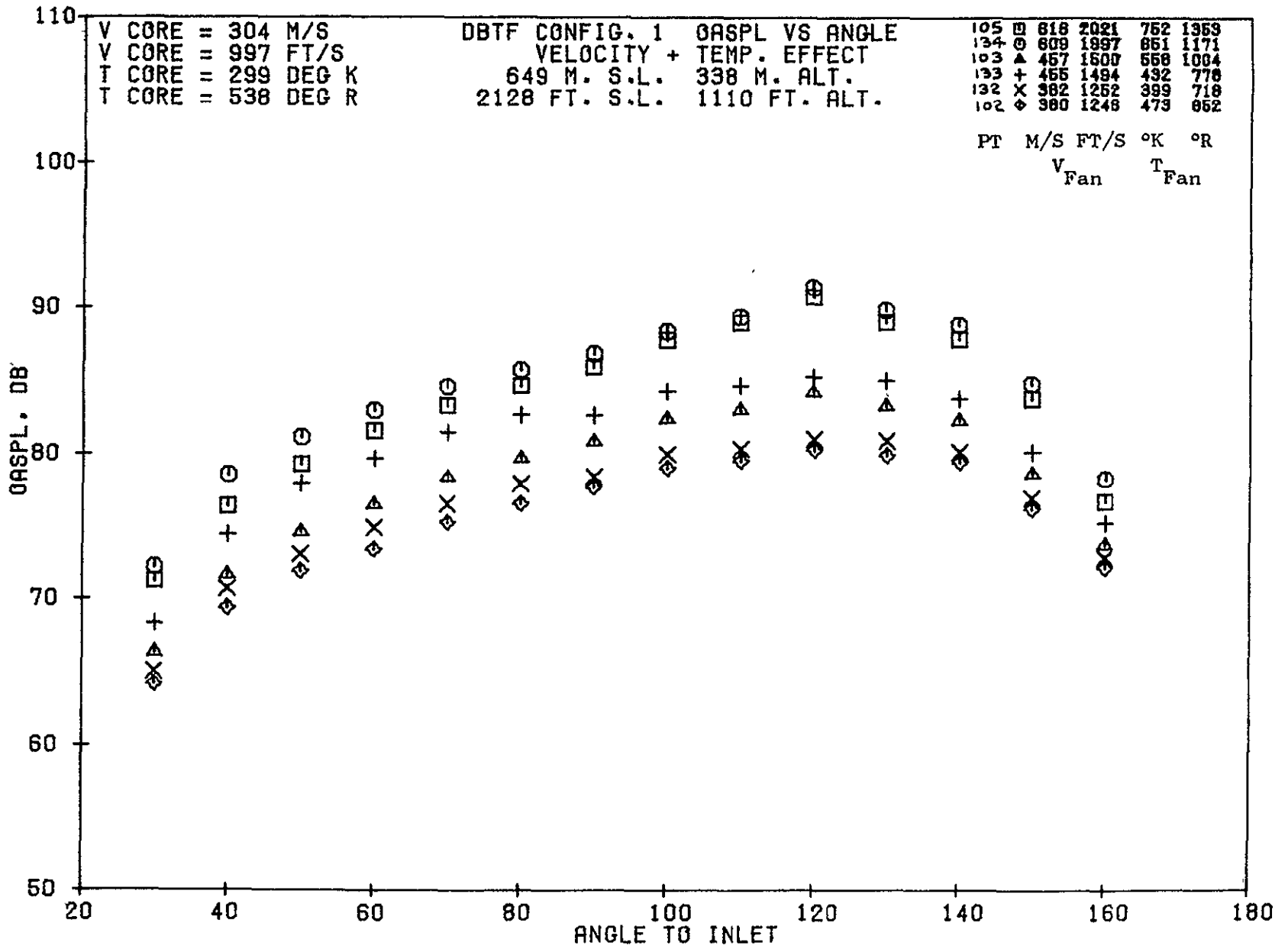
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10-17

1332

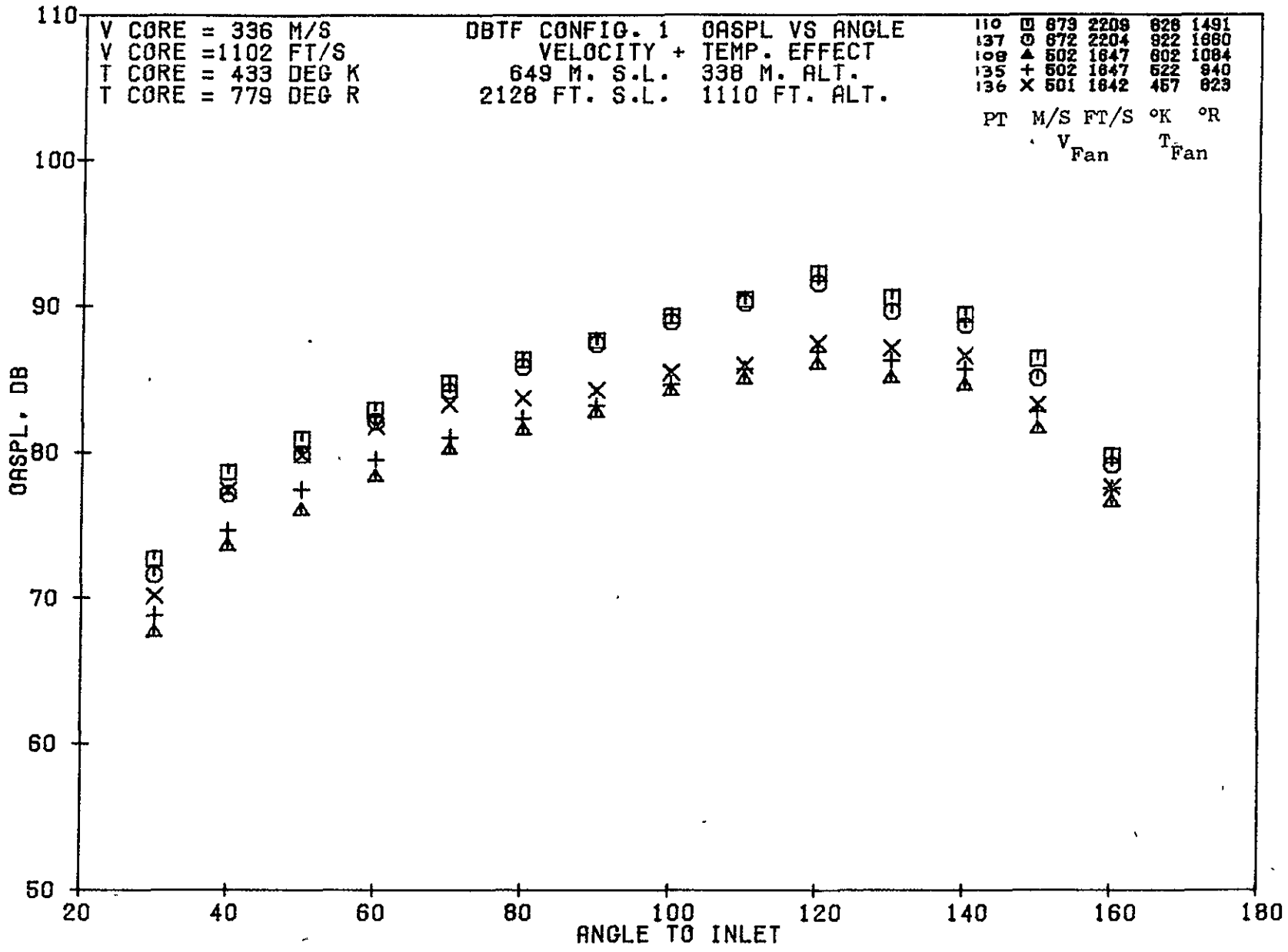


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5R031-001

79 BURD A.

1333



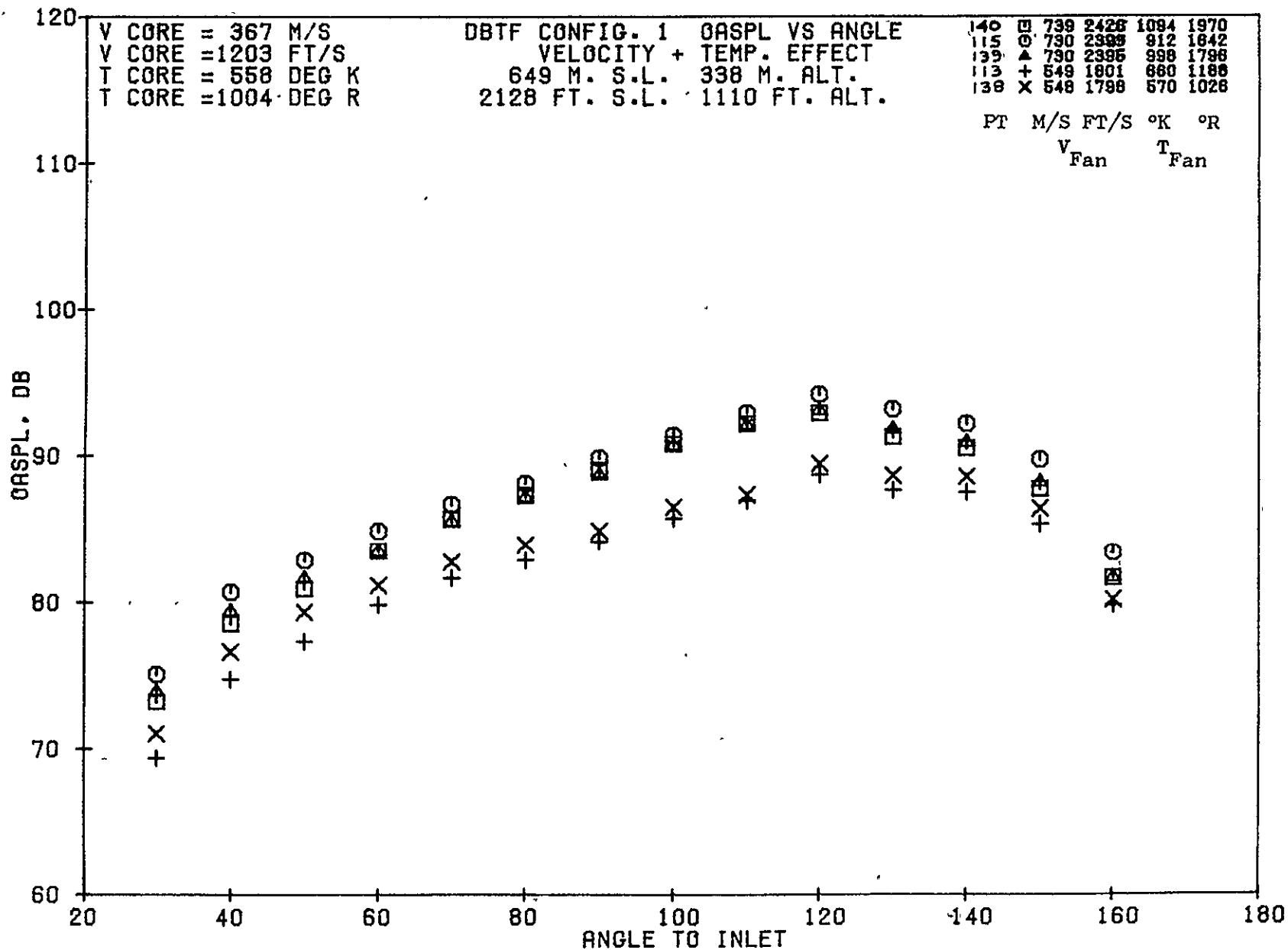
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70 BURCH 0.

1334

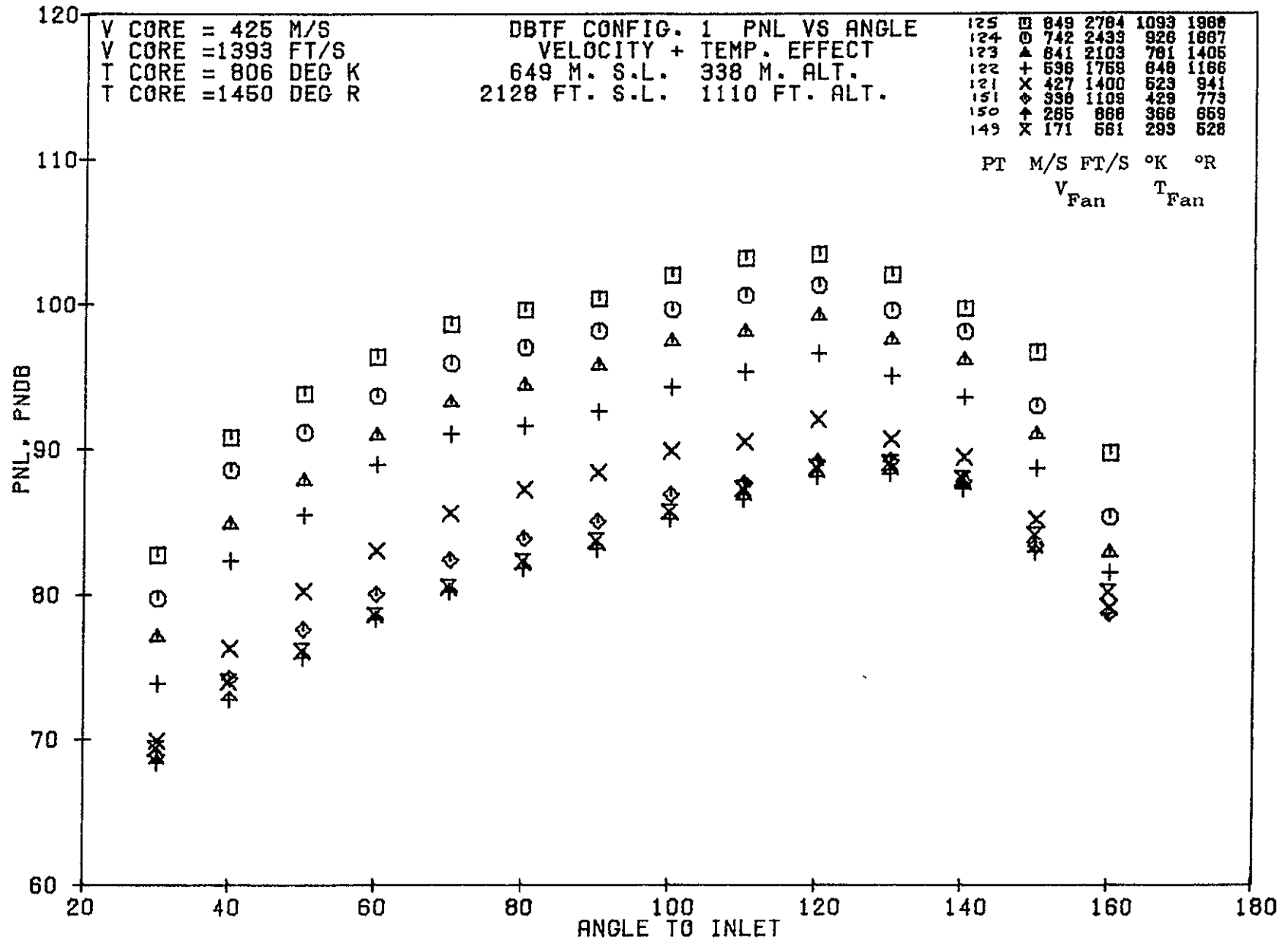


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08/13/75
5R031-001

79 BURCOR

1335

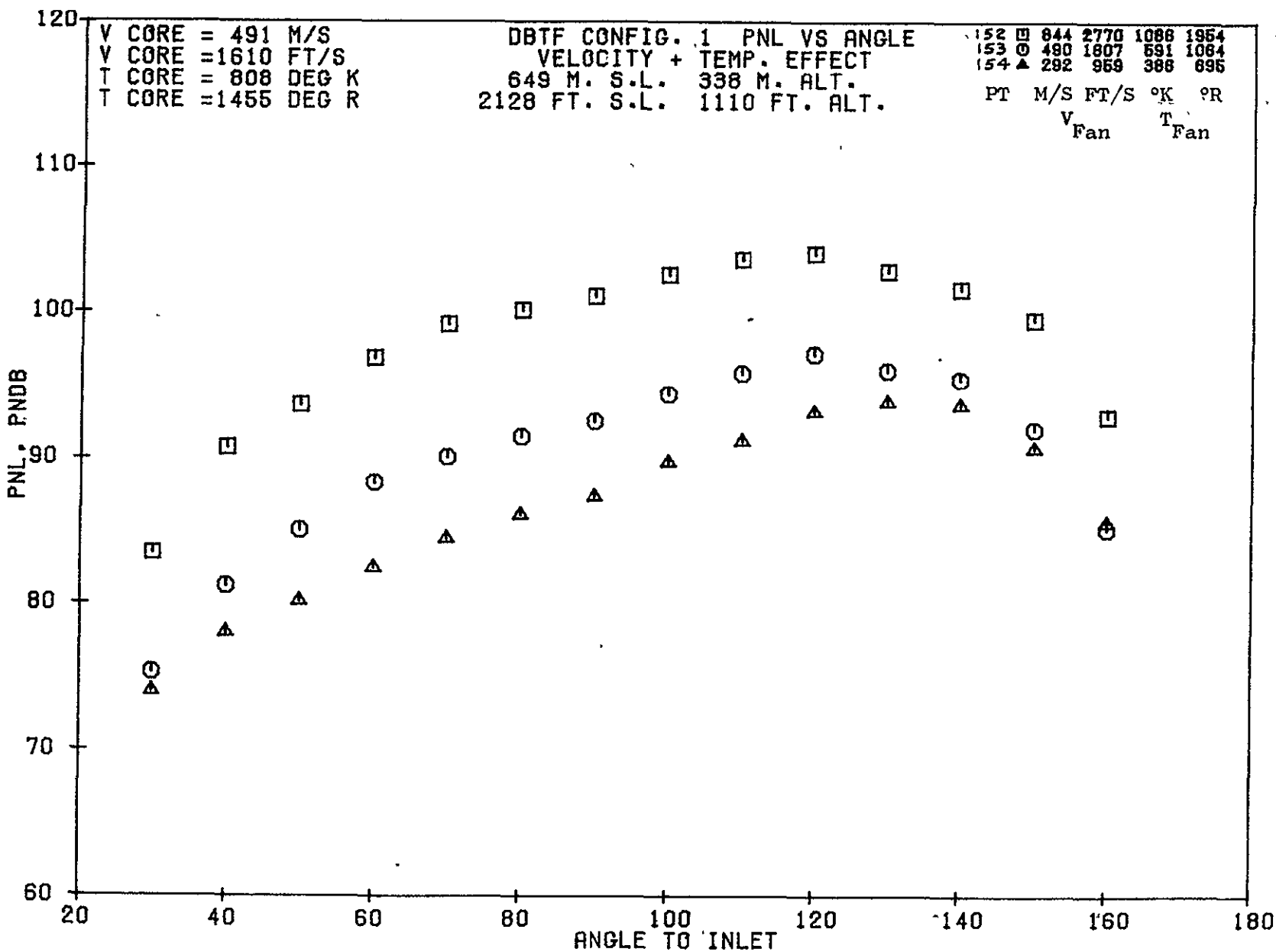


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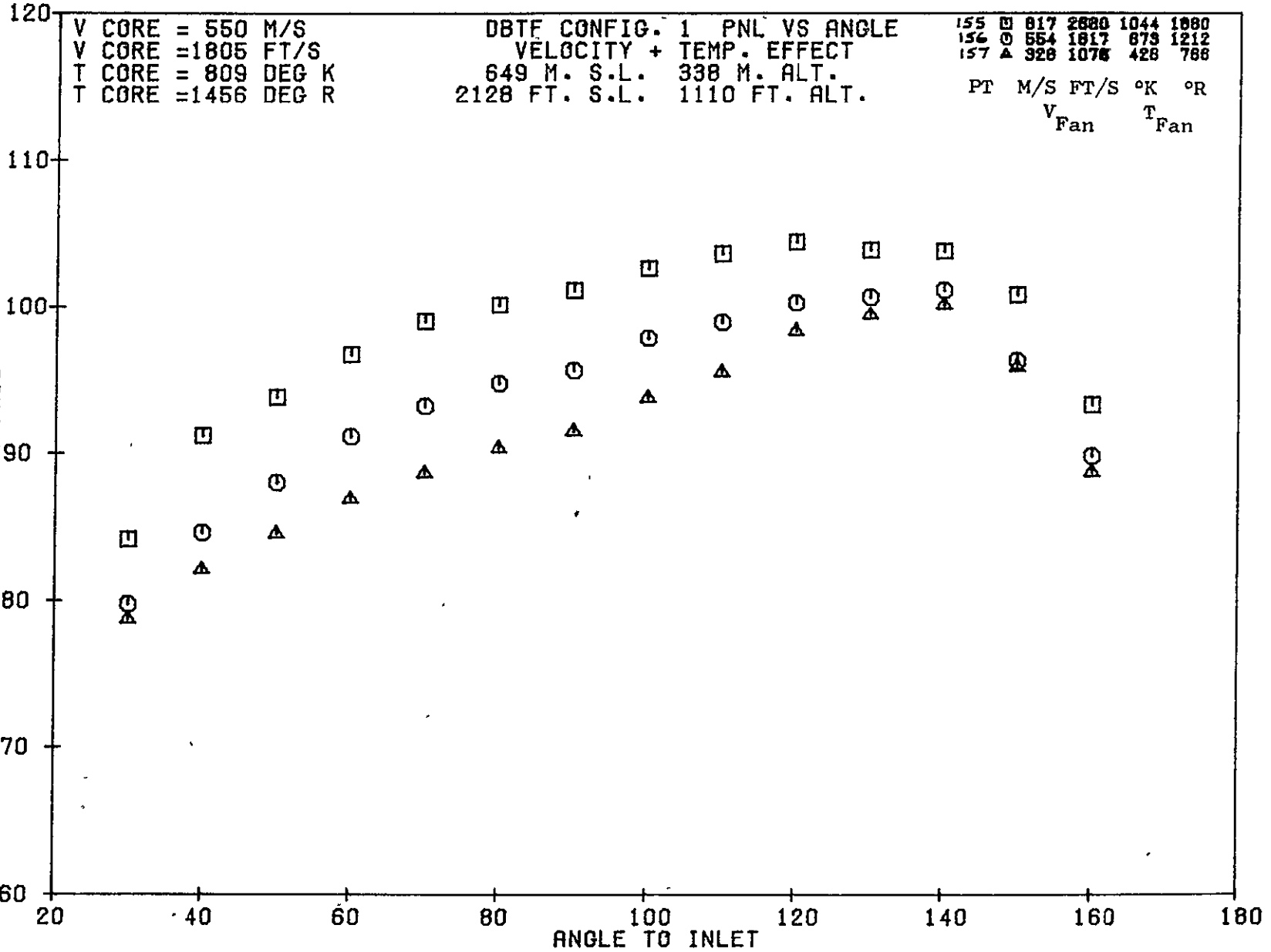
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0-2

4-108

08/13/75
5R031-001

79 BURC



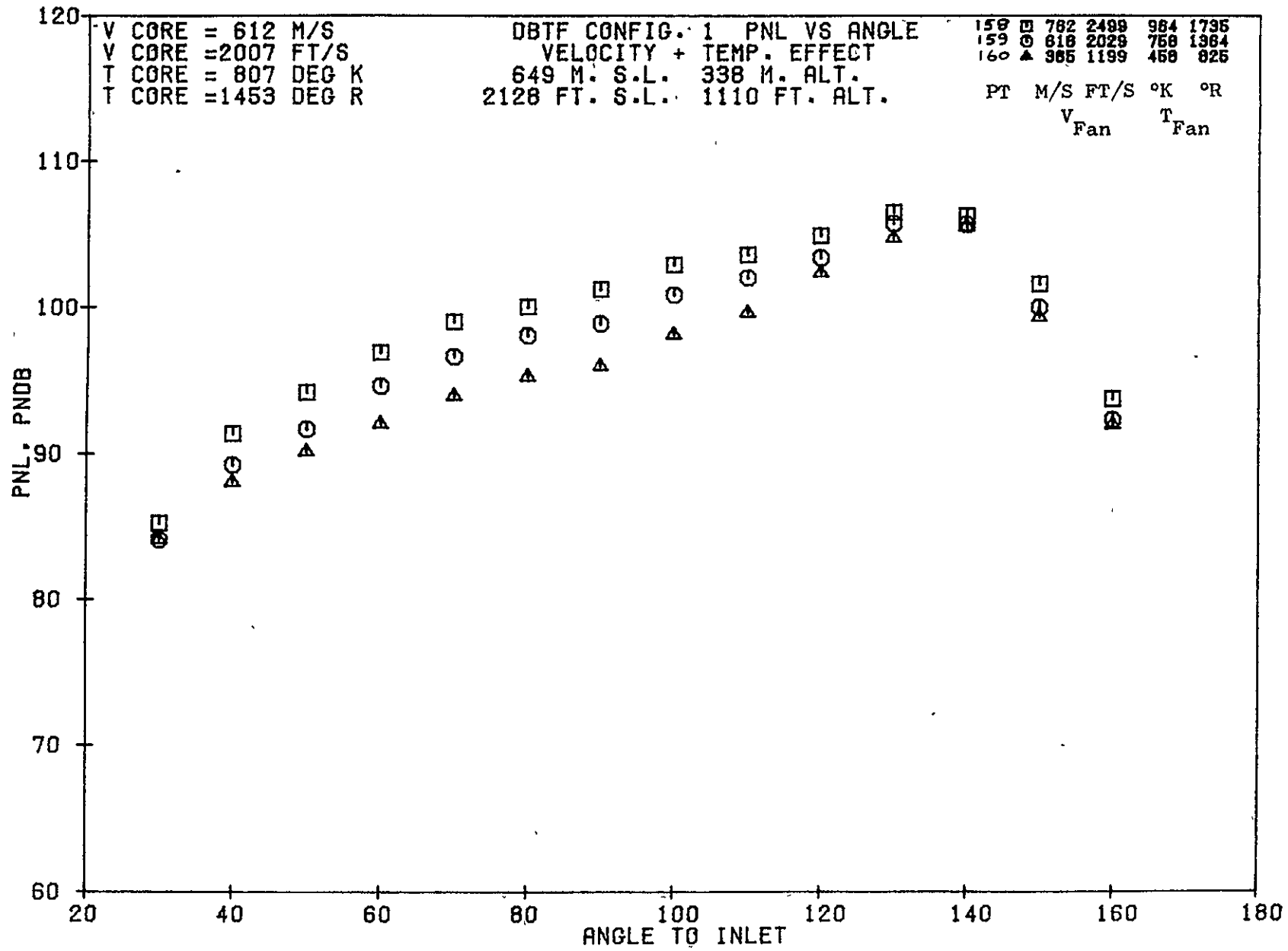
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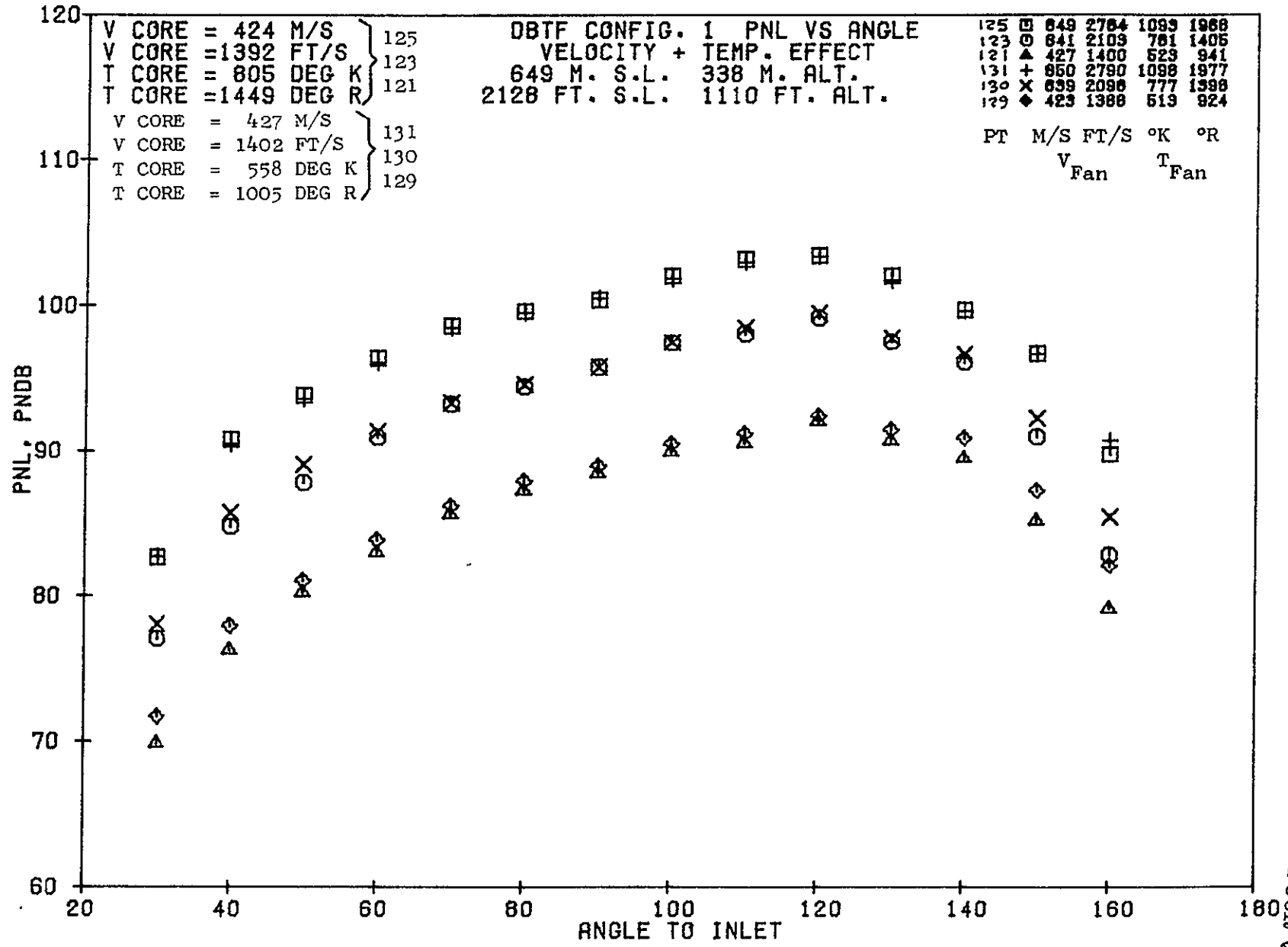
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79 BURCH A.

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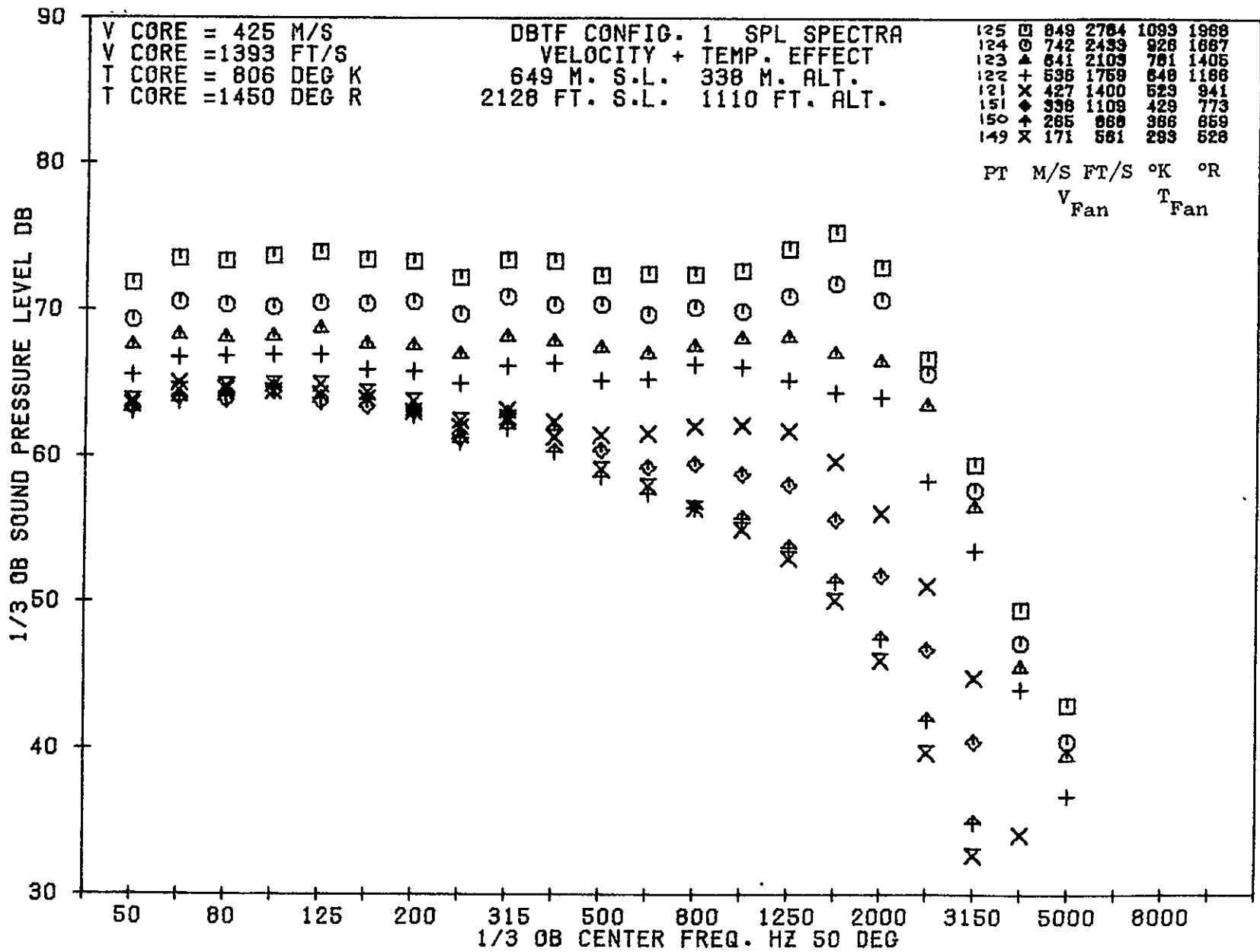


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79 BURCH A.

11-112

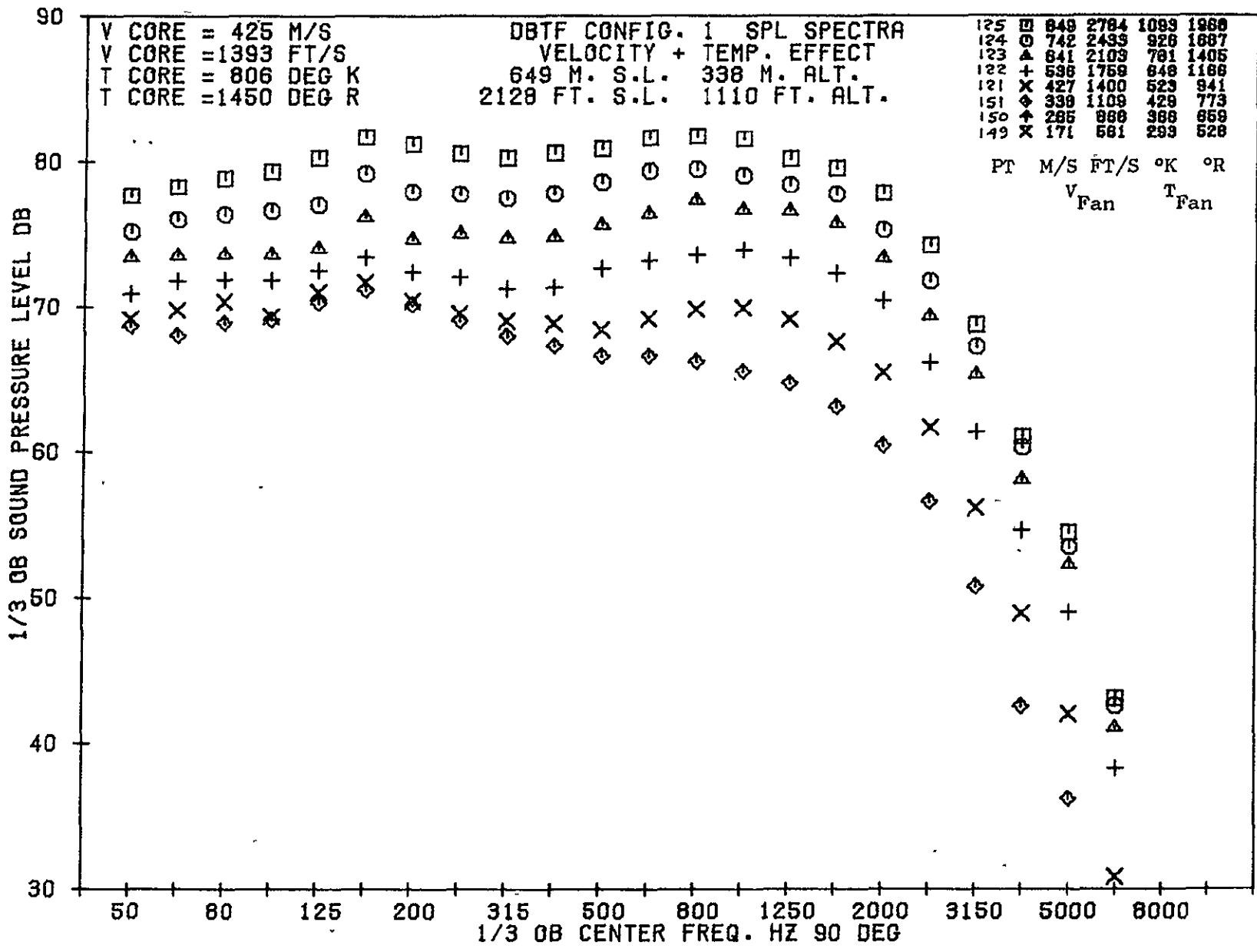


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1341



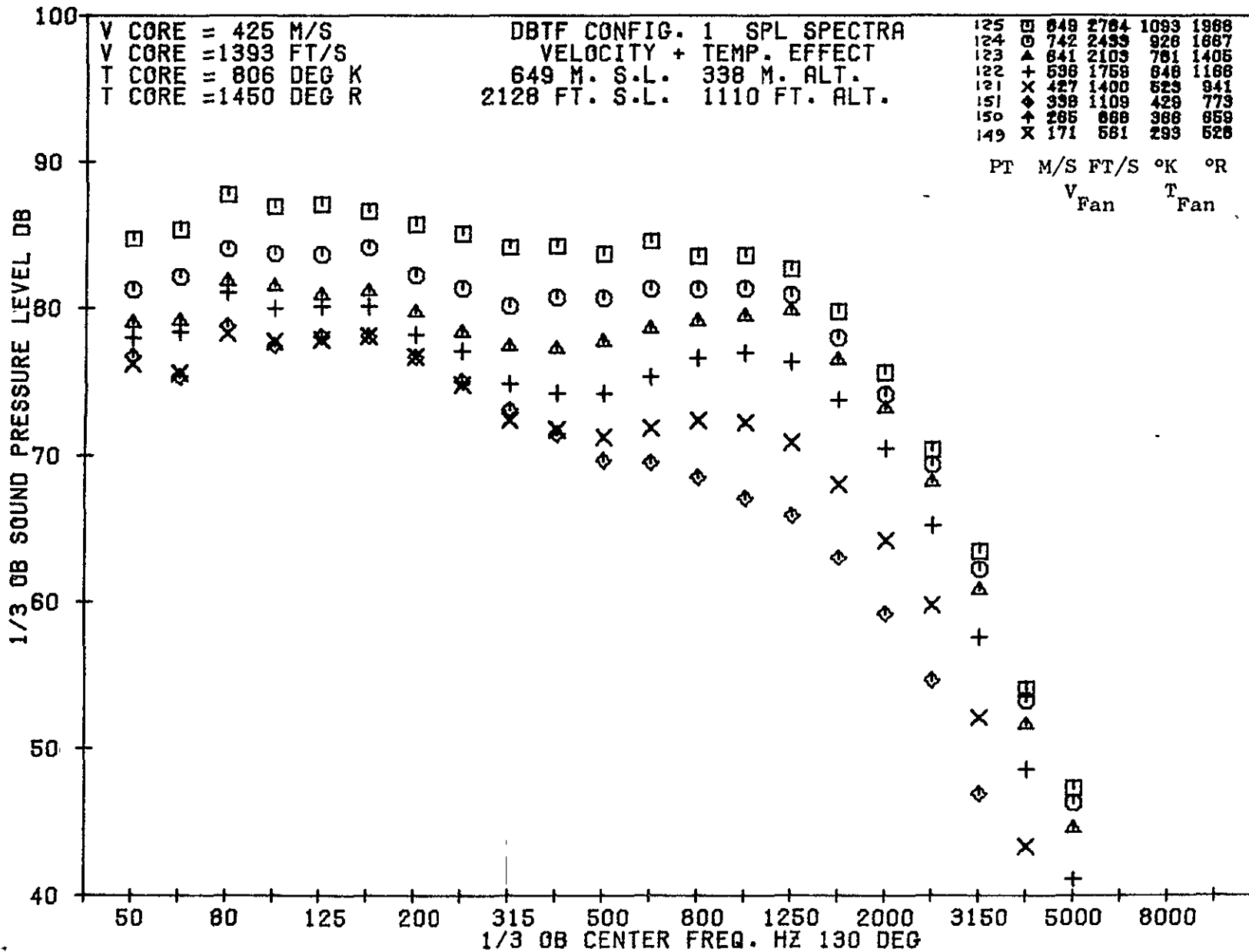
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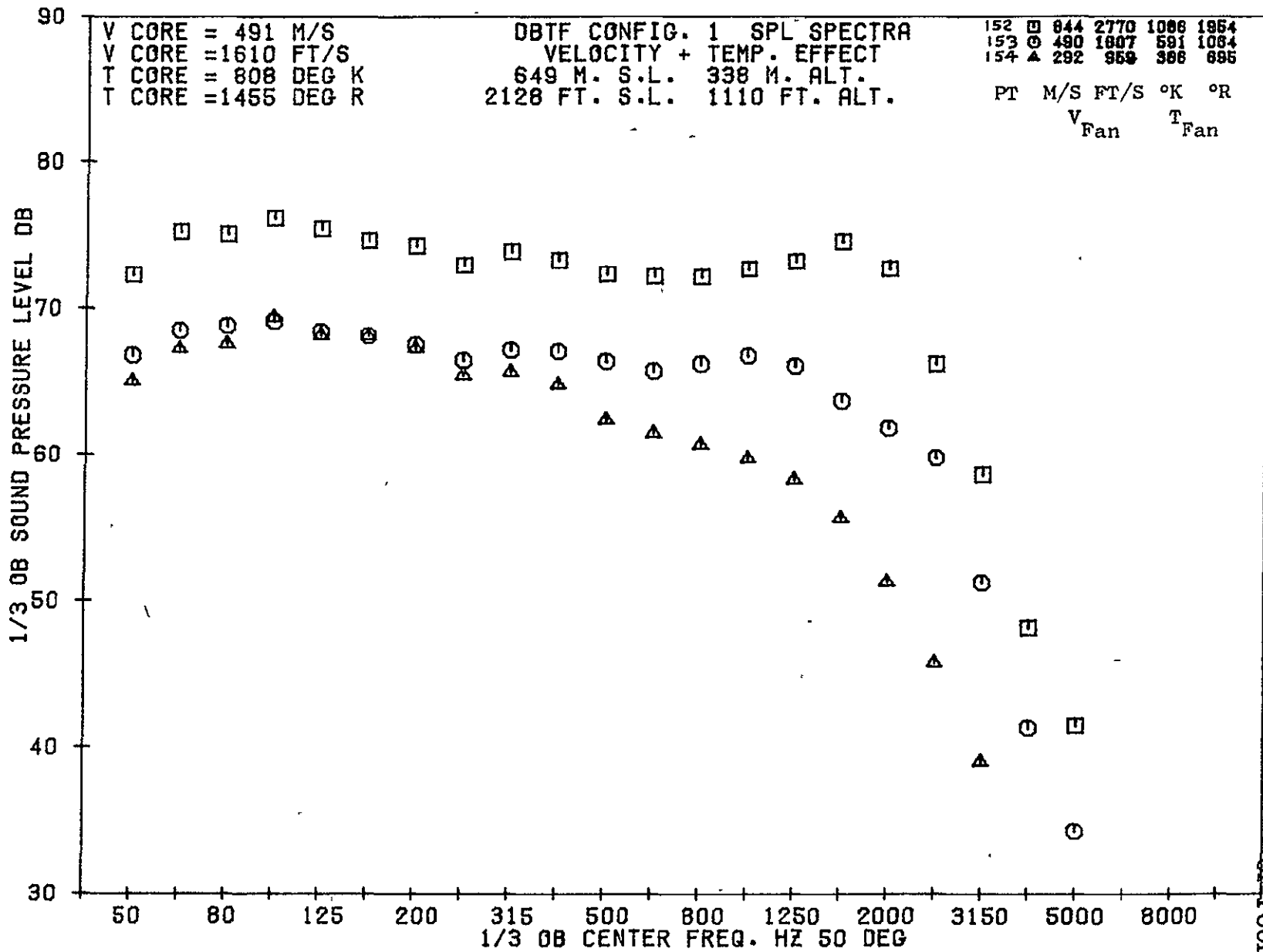
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4-1/5

08/13/75
 5R031-001

79 BURCH



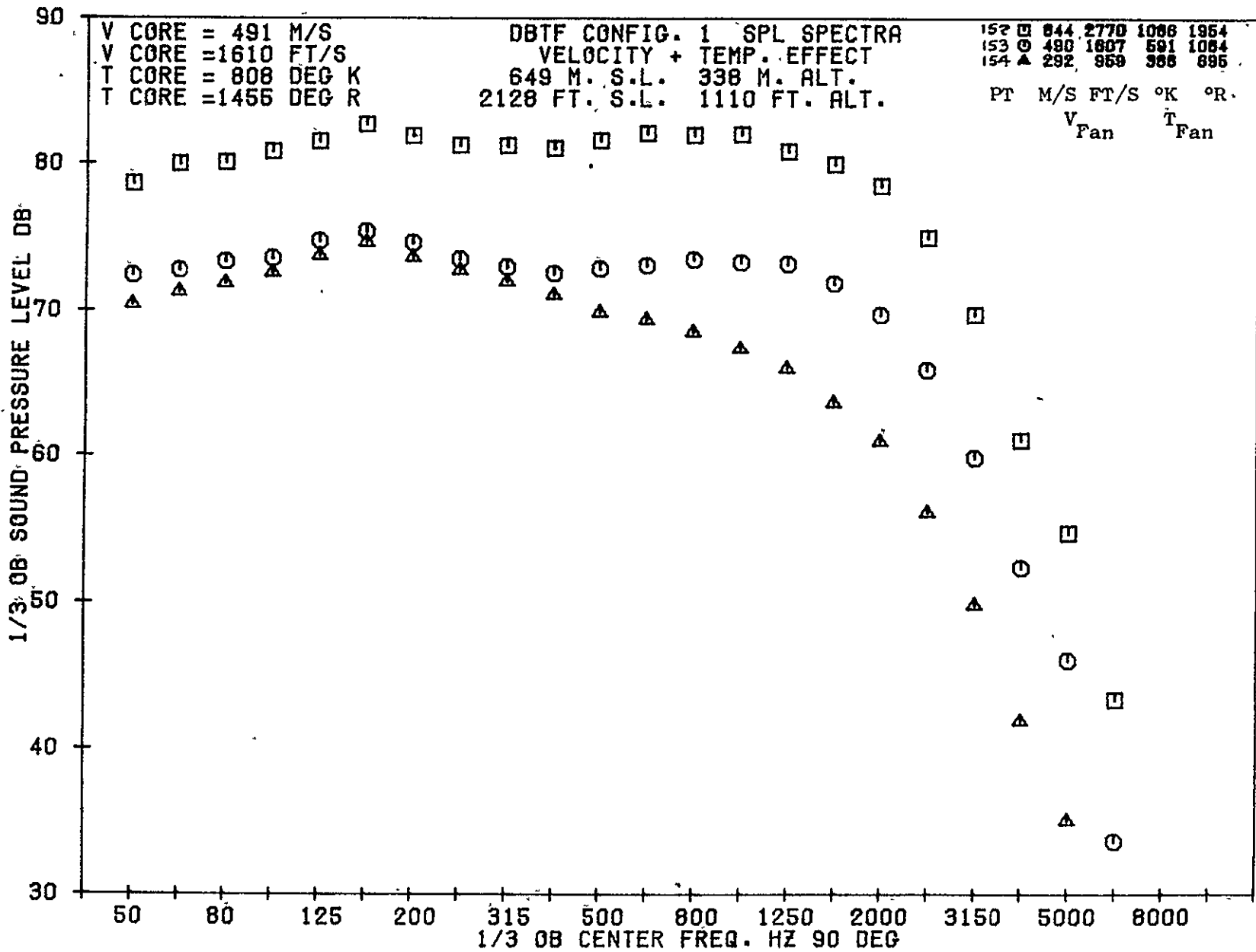
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79 BURCH A.

4 1/2



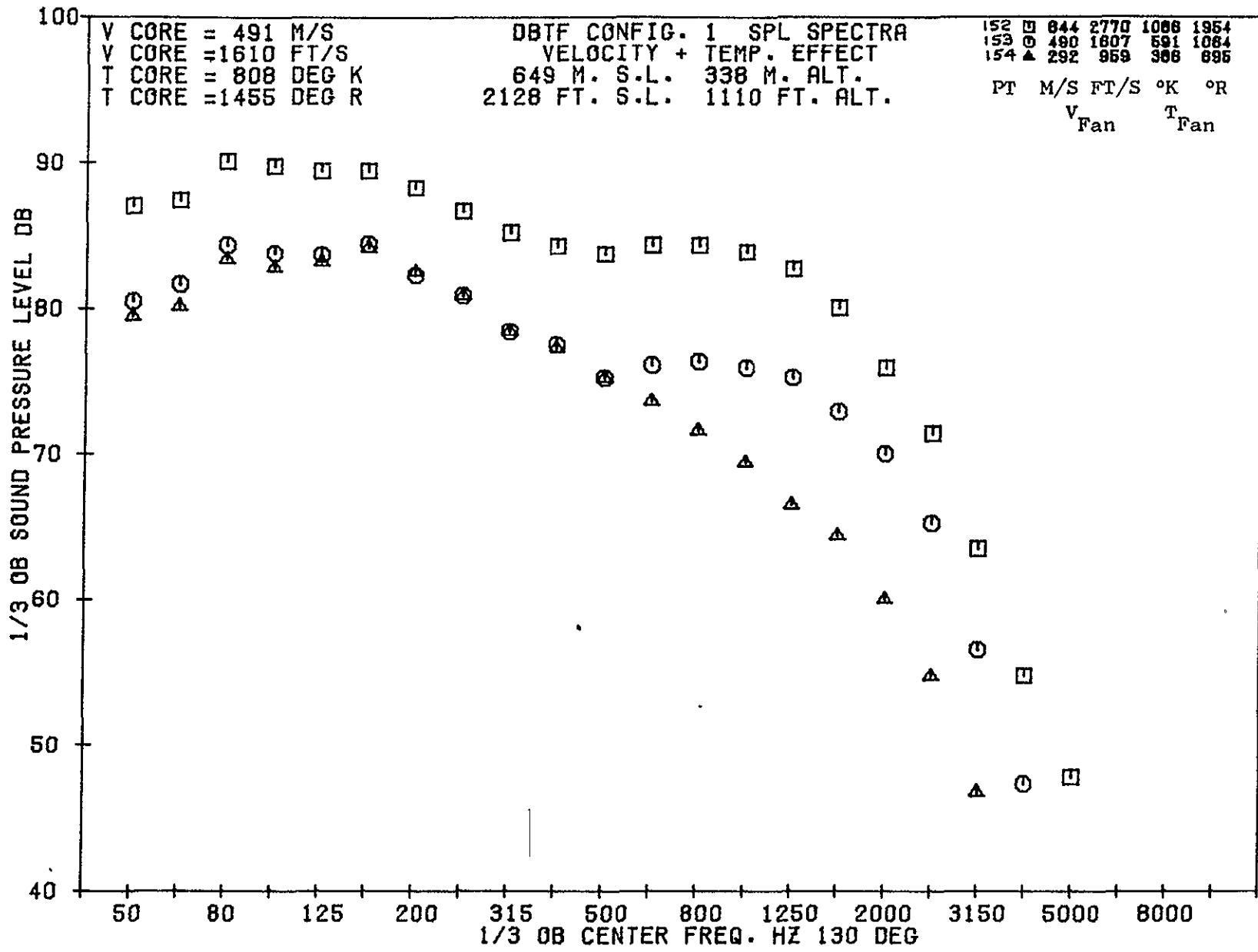
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79 BURQA.

1345



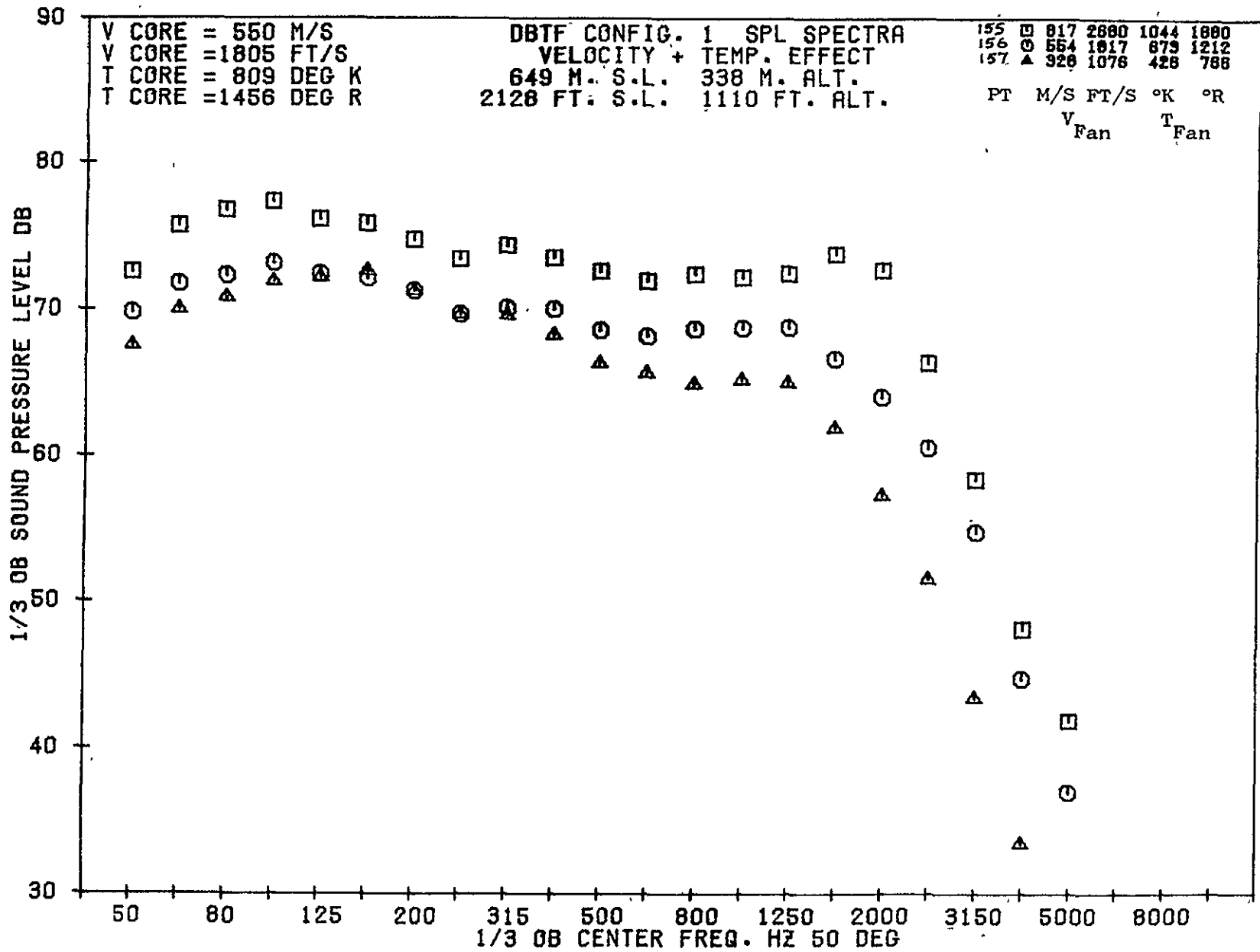
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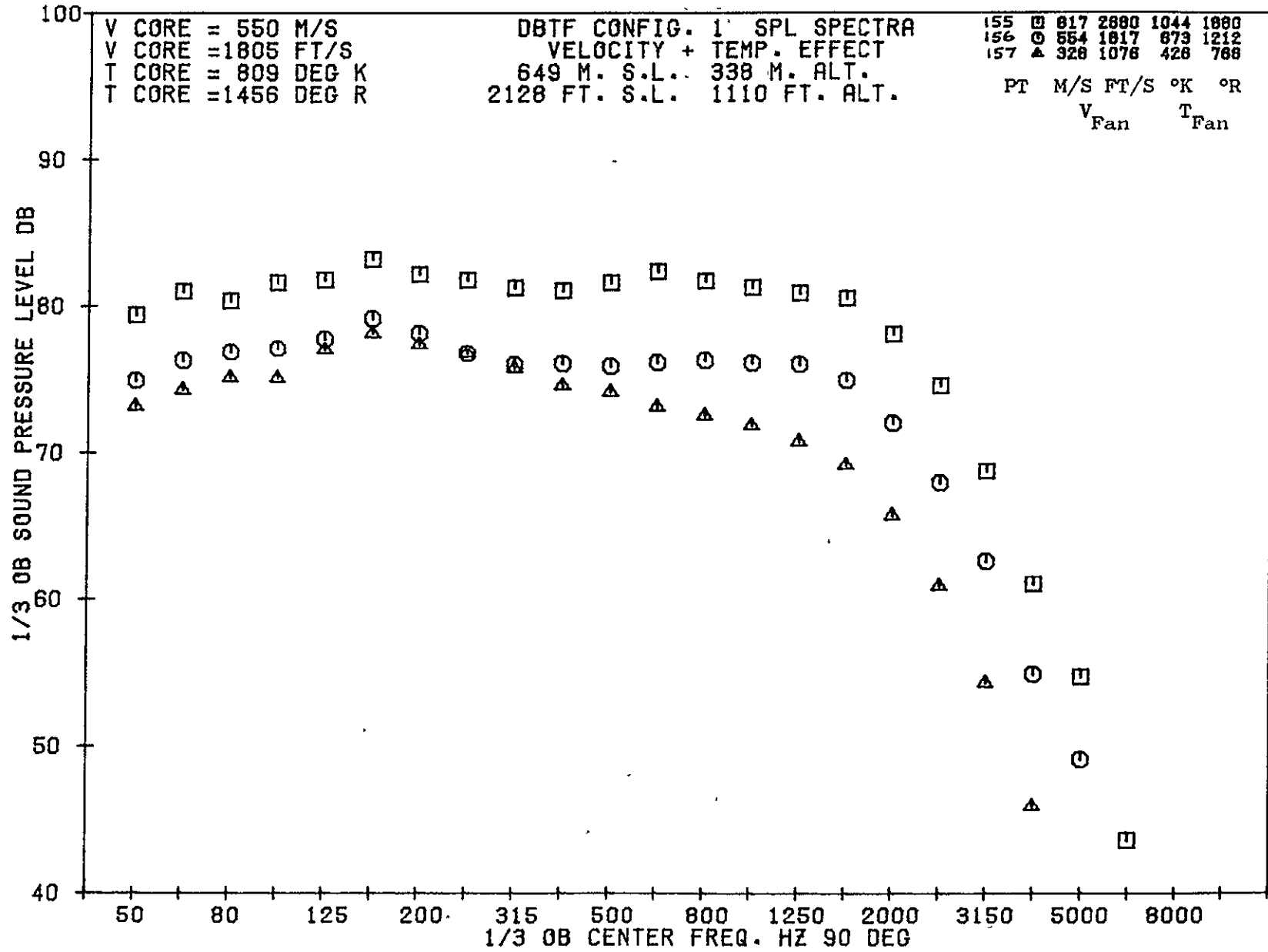
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61-119

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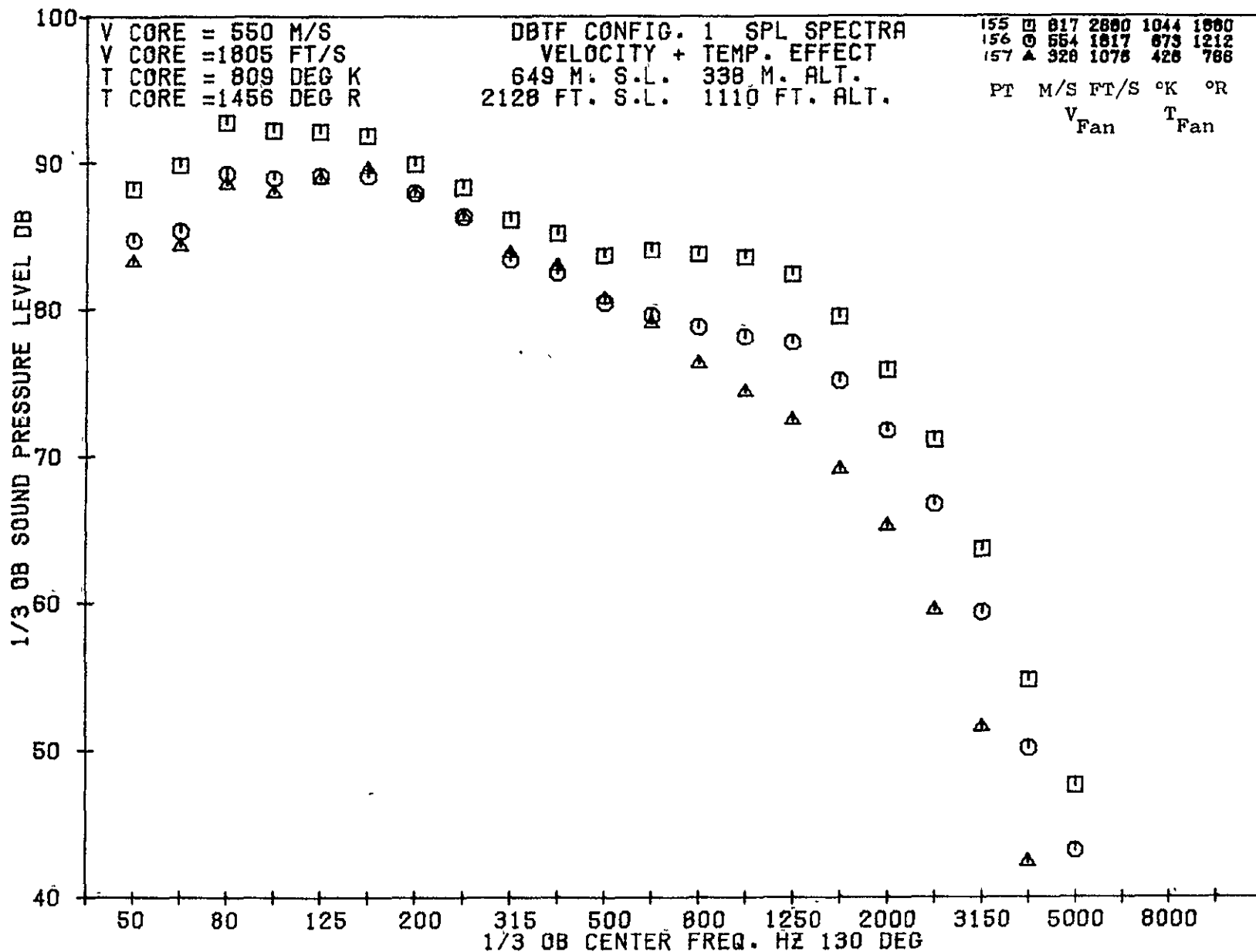


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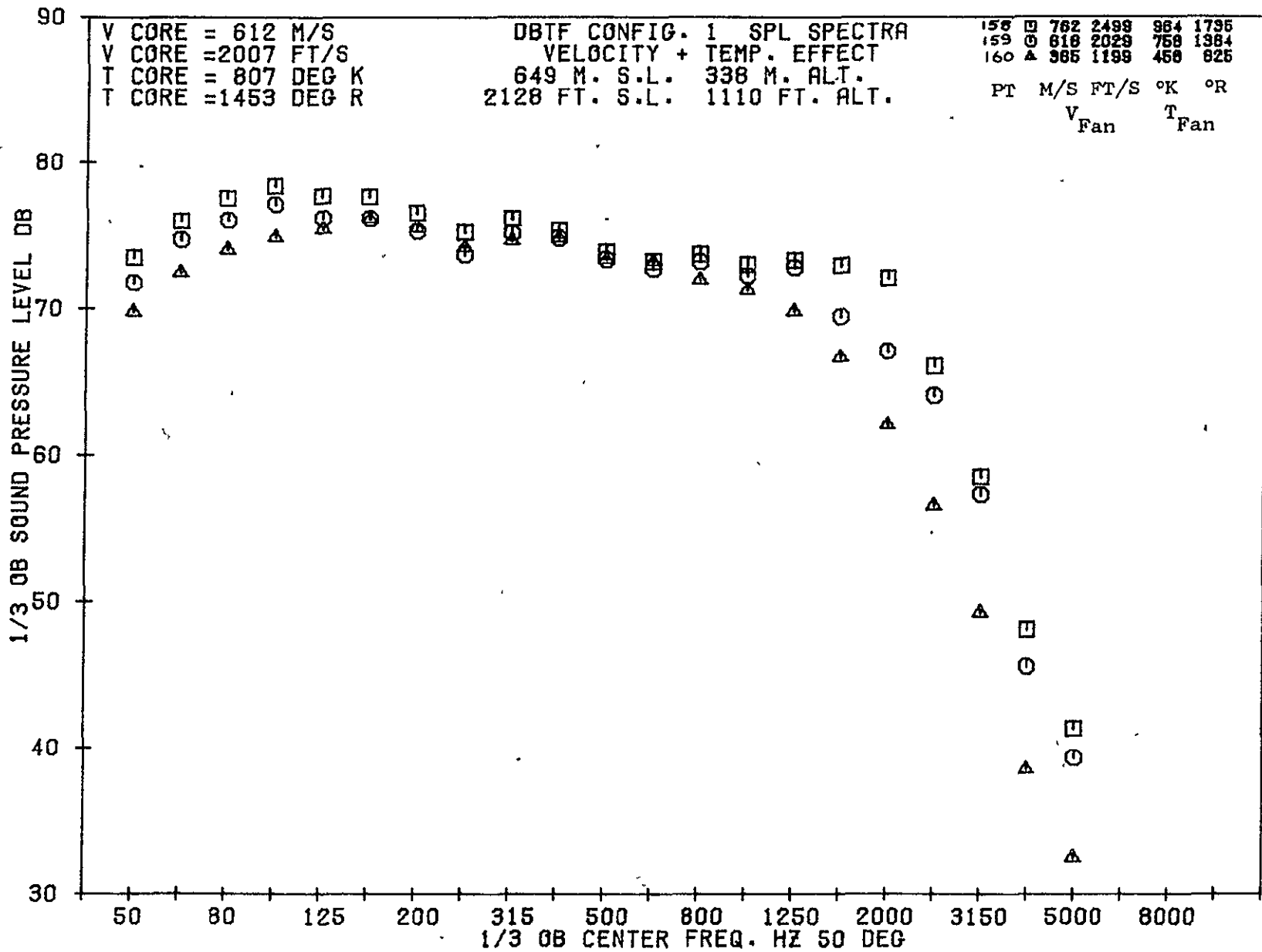
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5R031-001

79 BURCH

1349



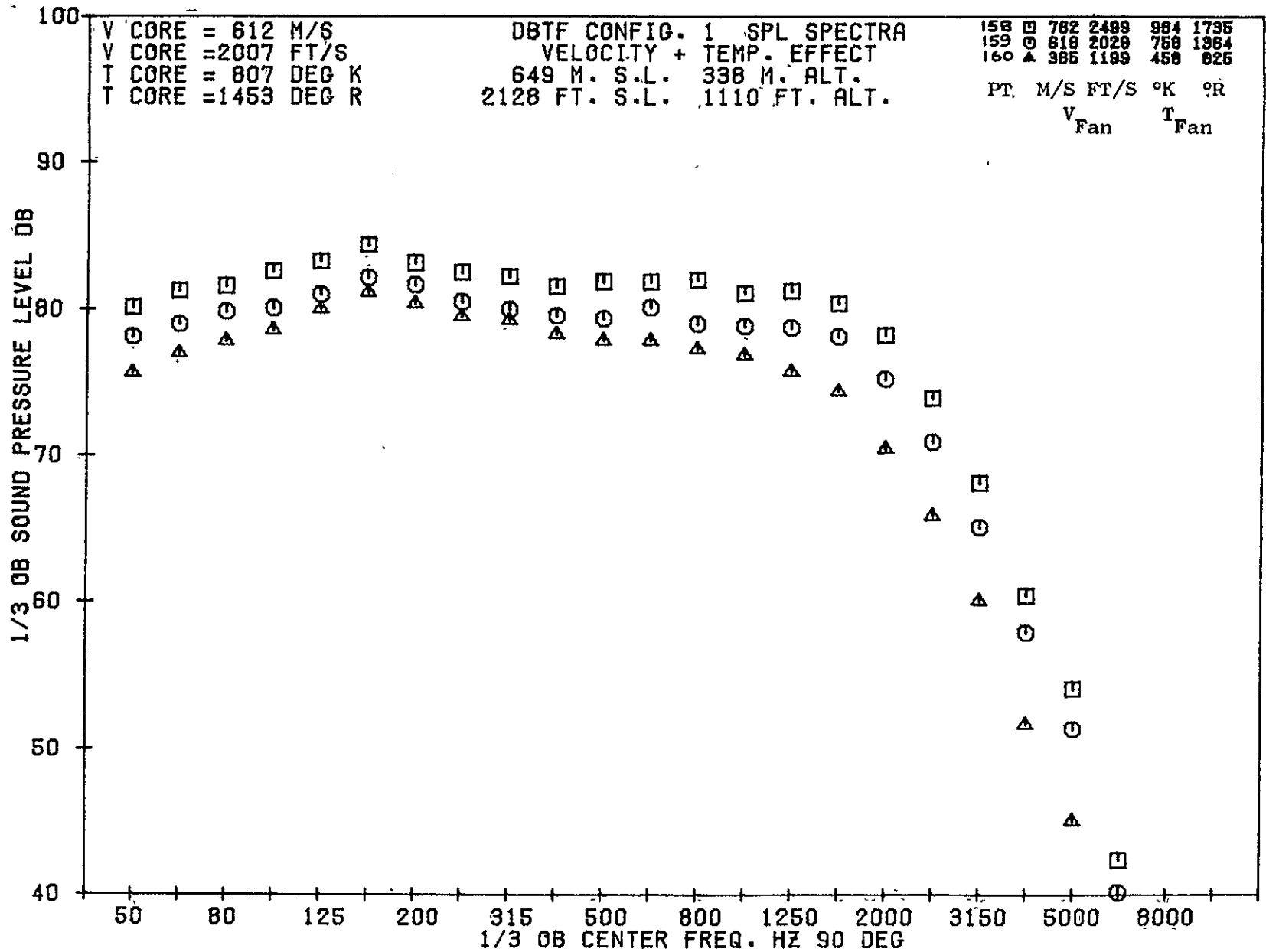
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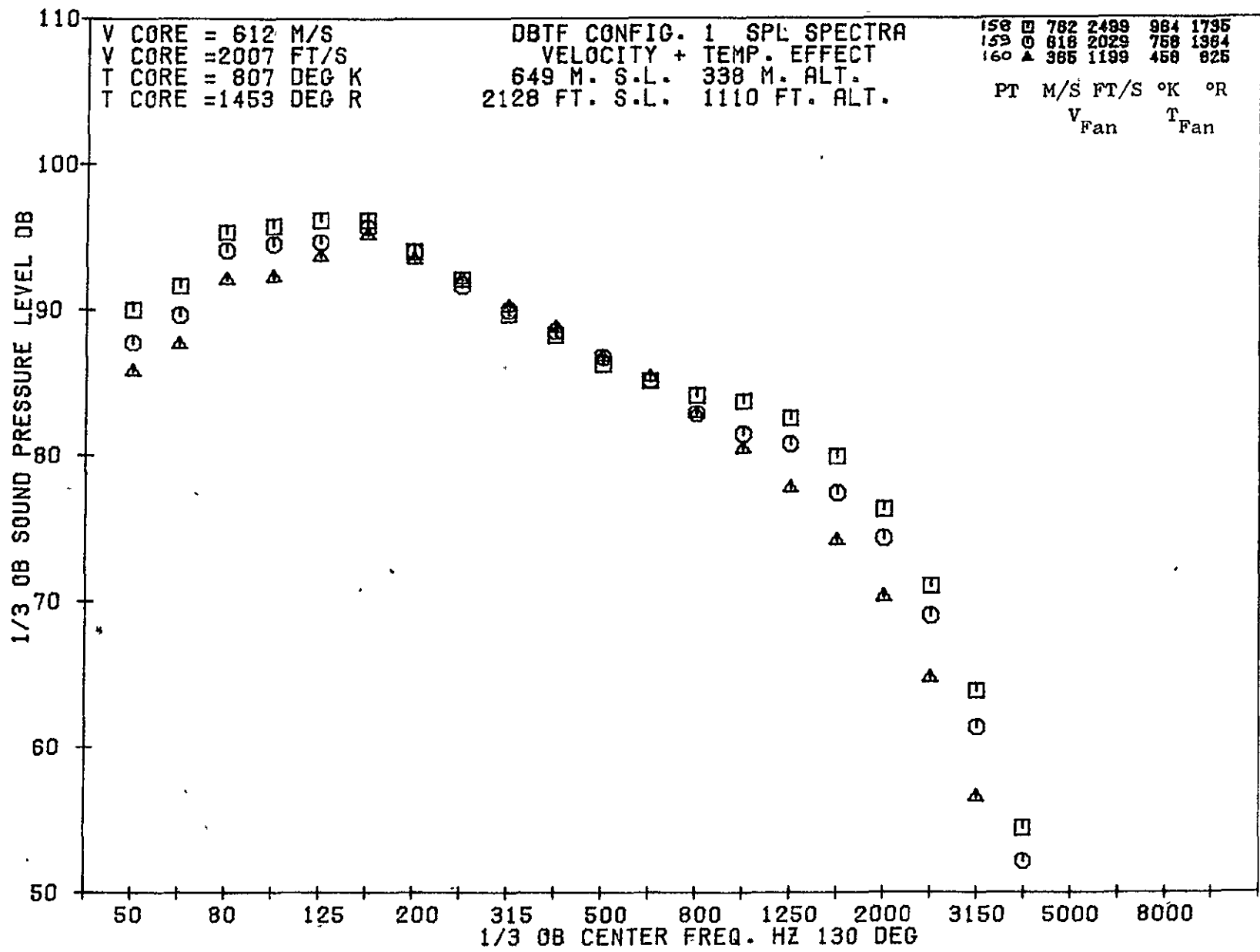


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1351



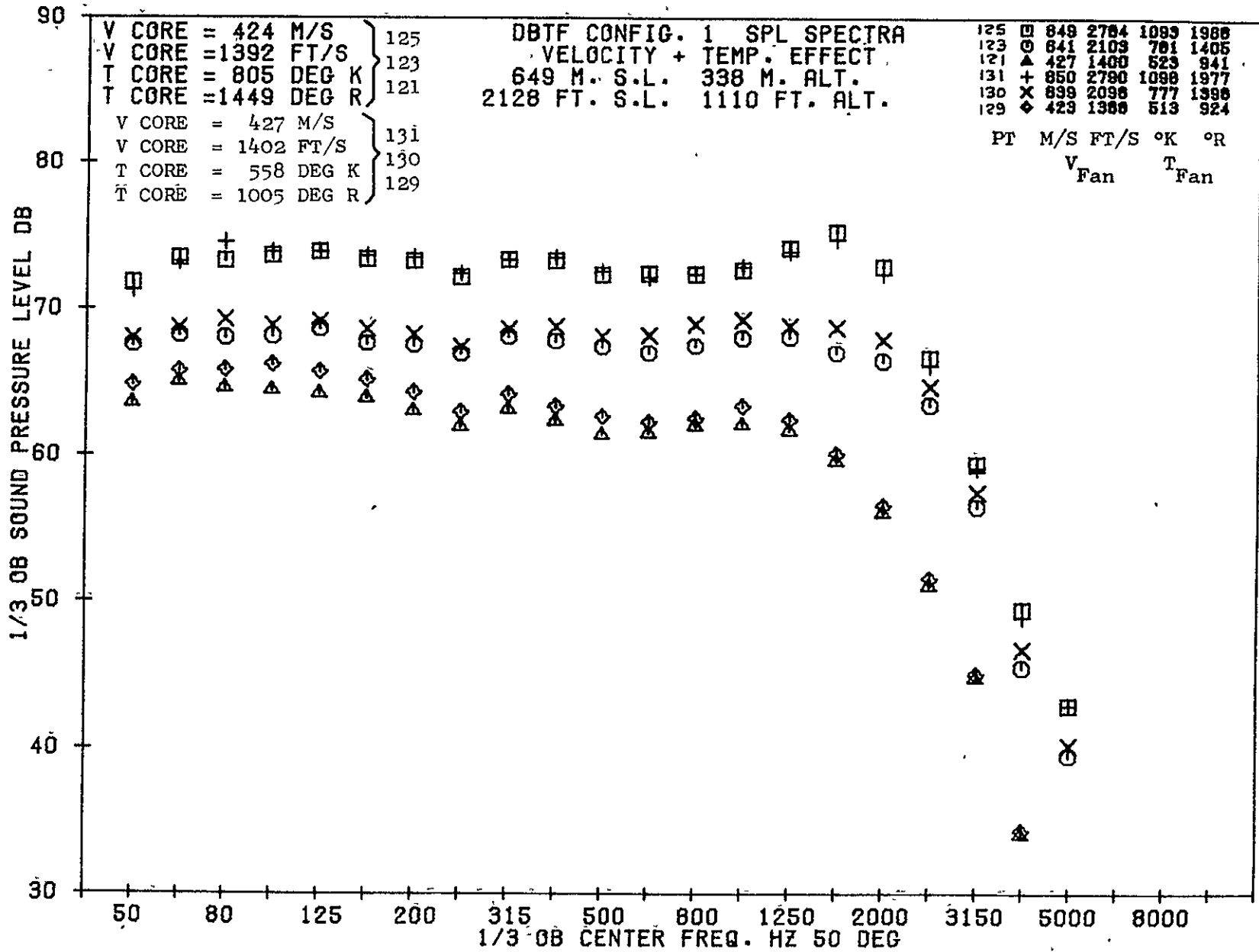
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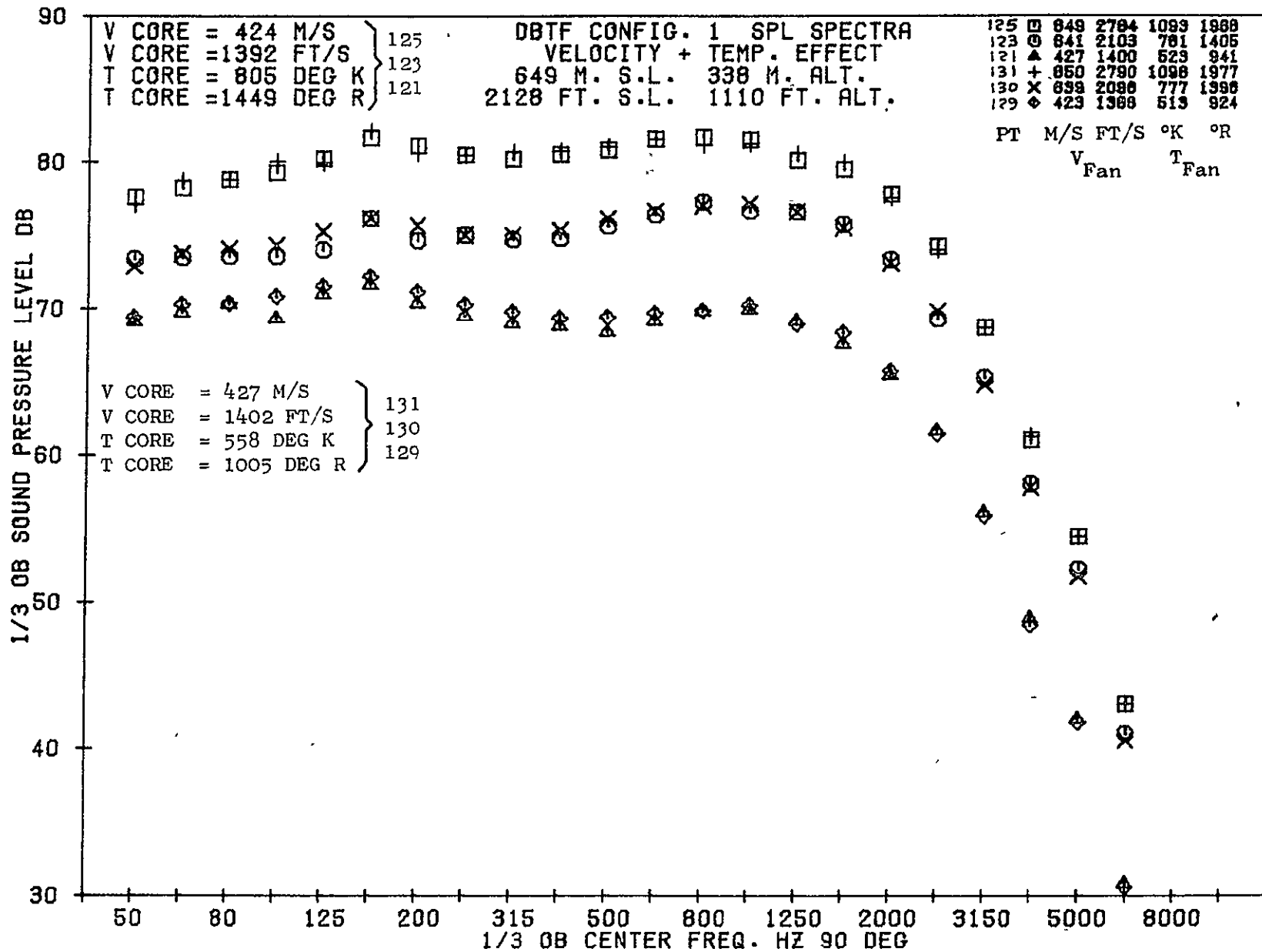
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79 BURCH

1353



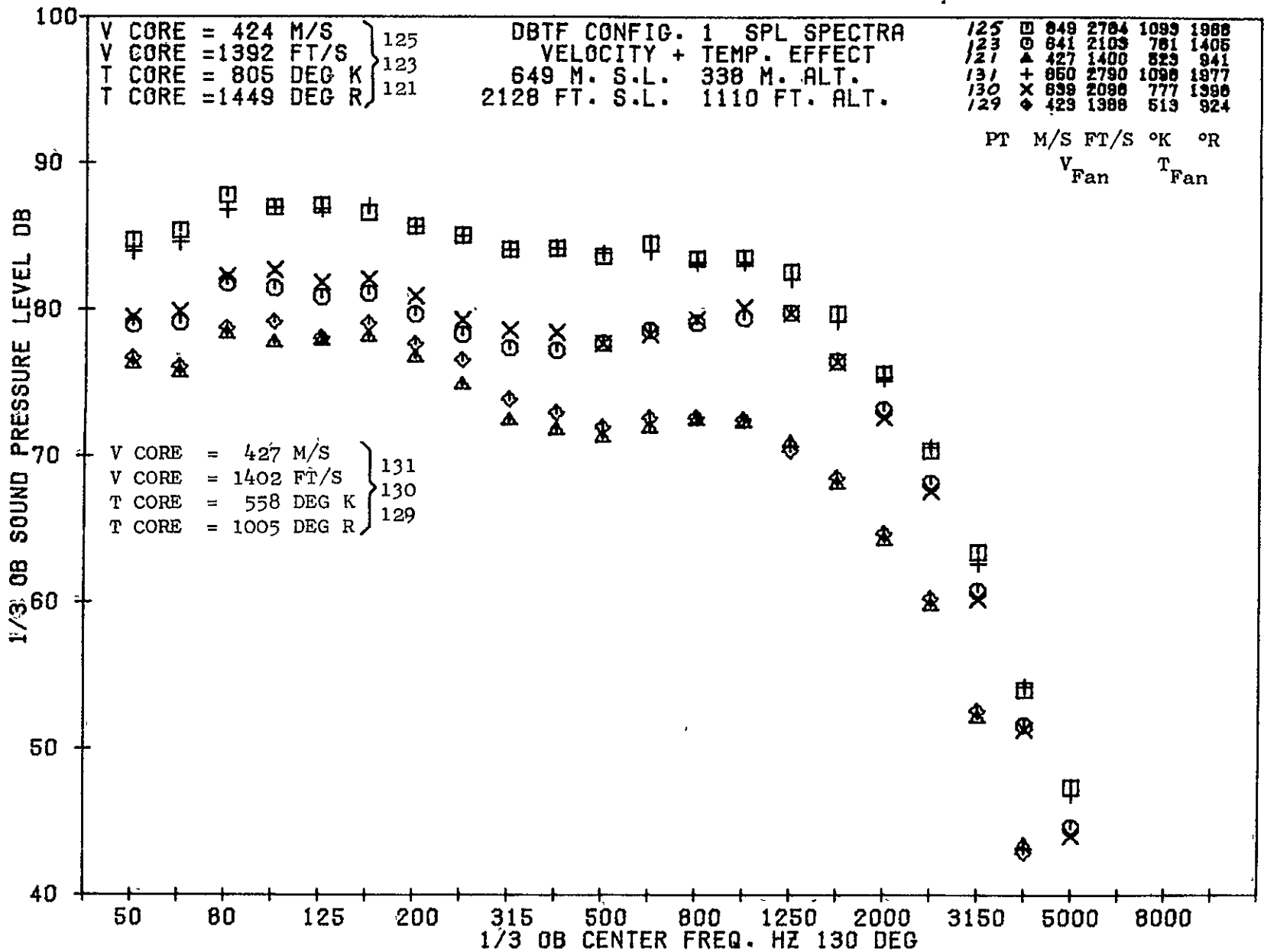
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1354

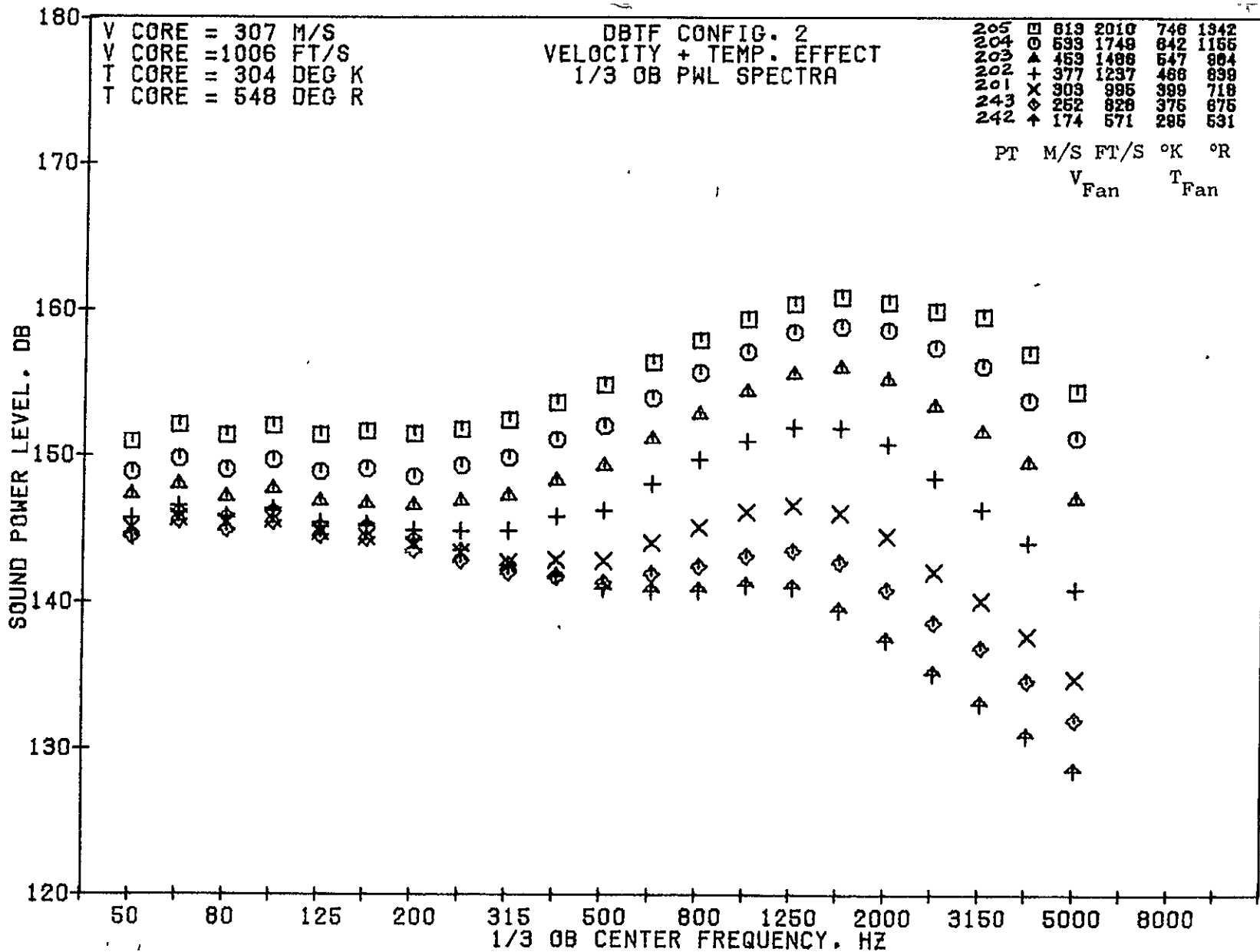


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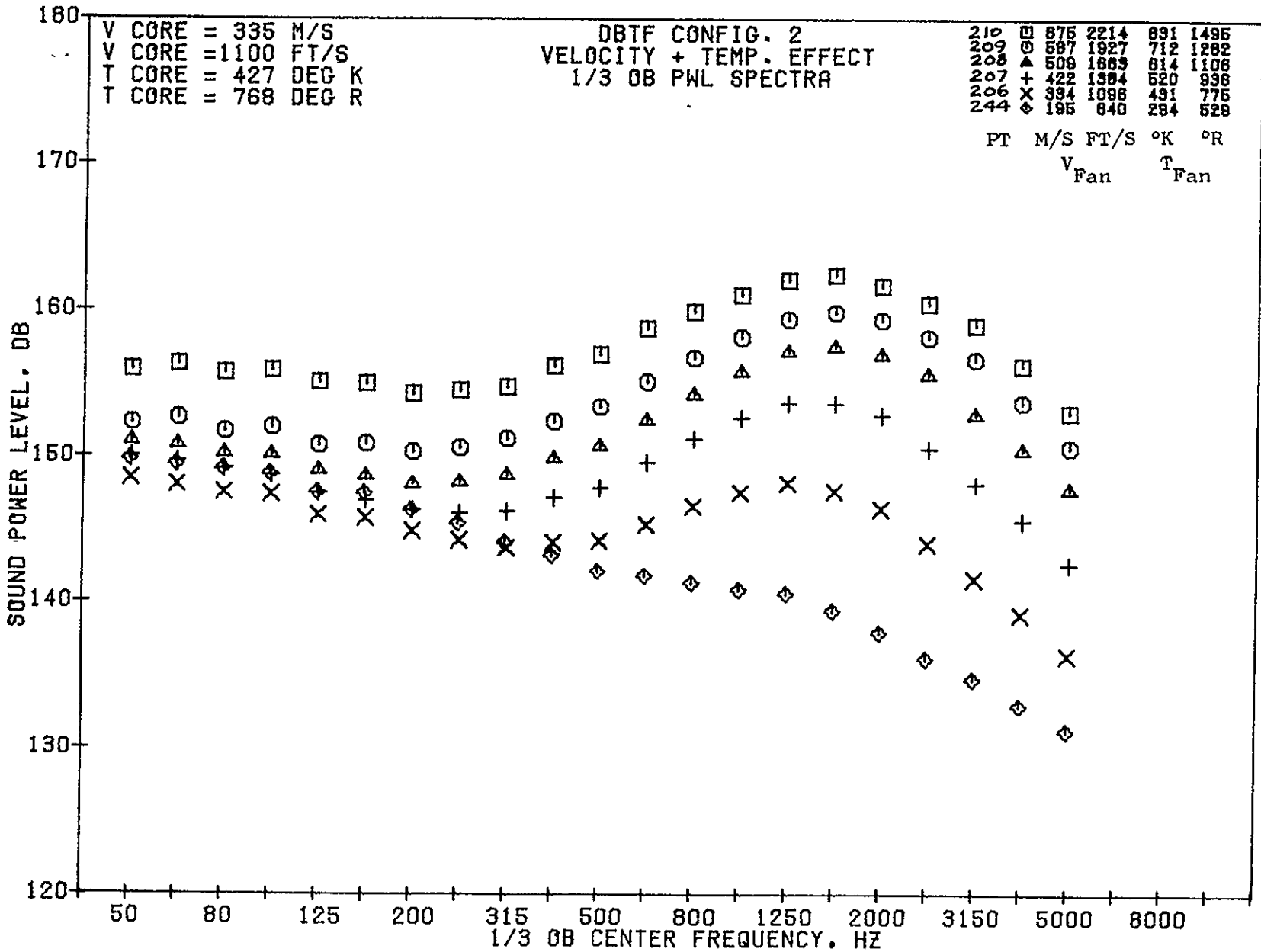
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4-128

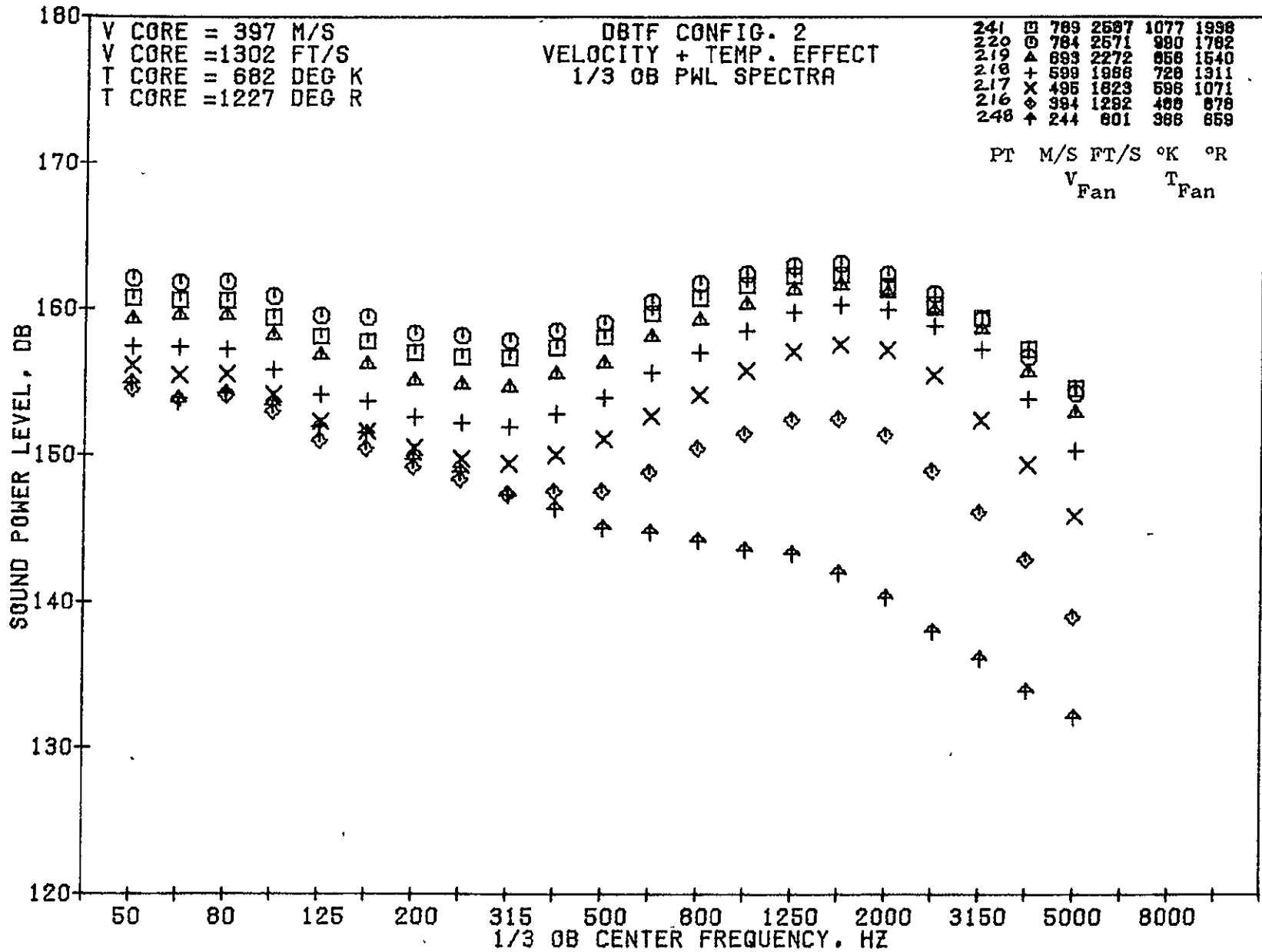
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5R266-001

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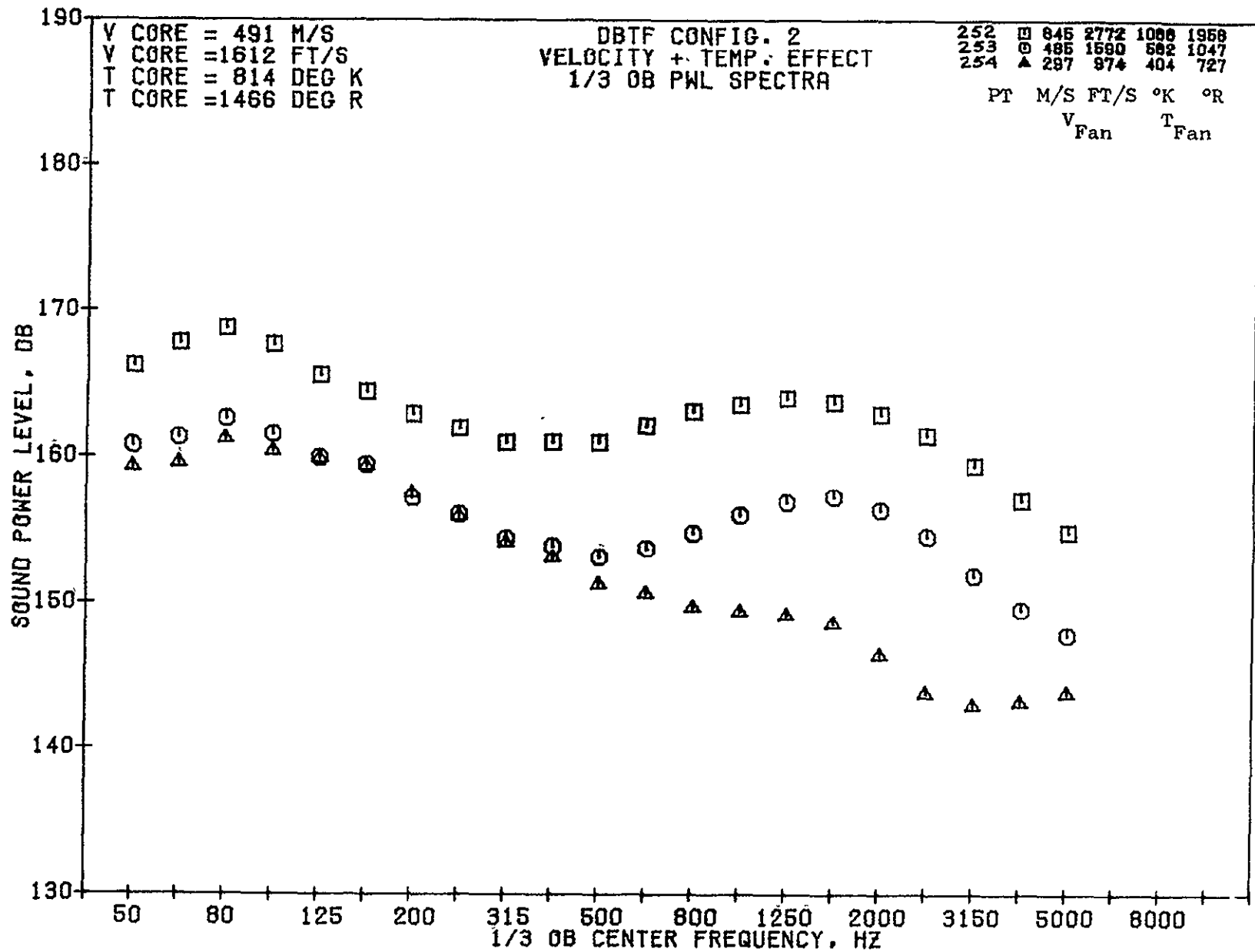


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79 BURCH A.

4-130



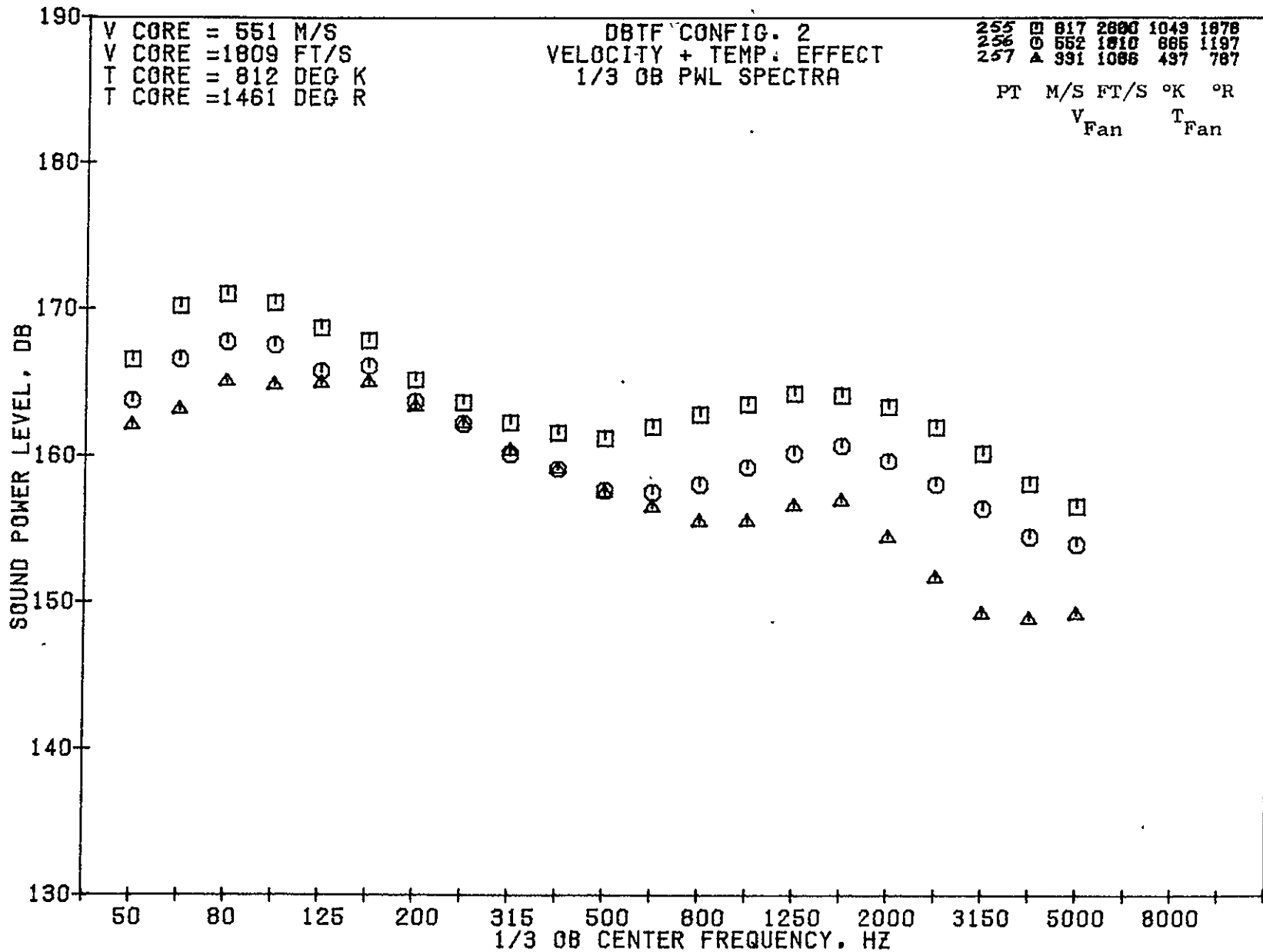
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1359

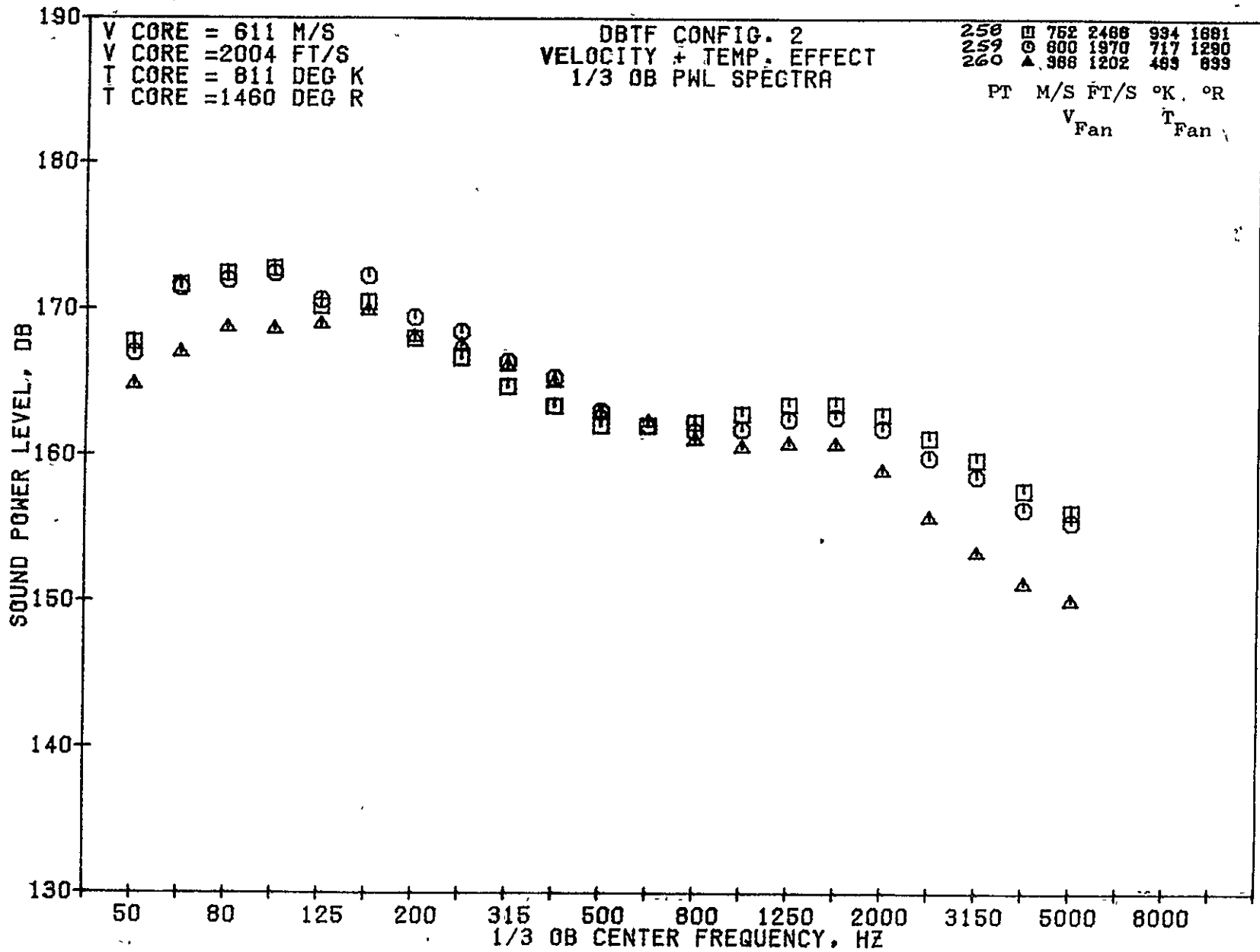


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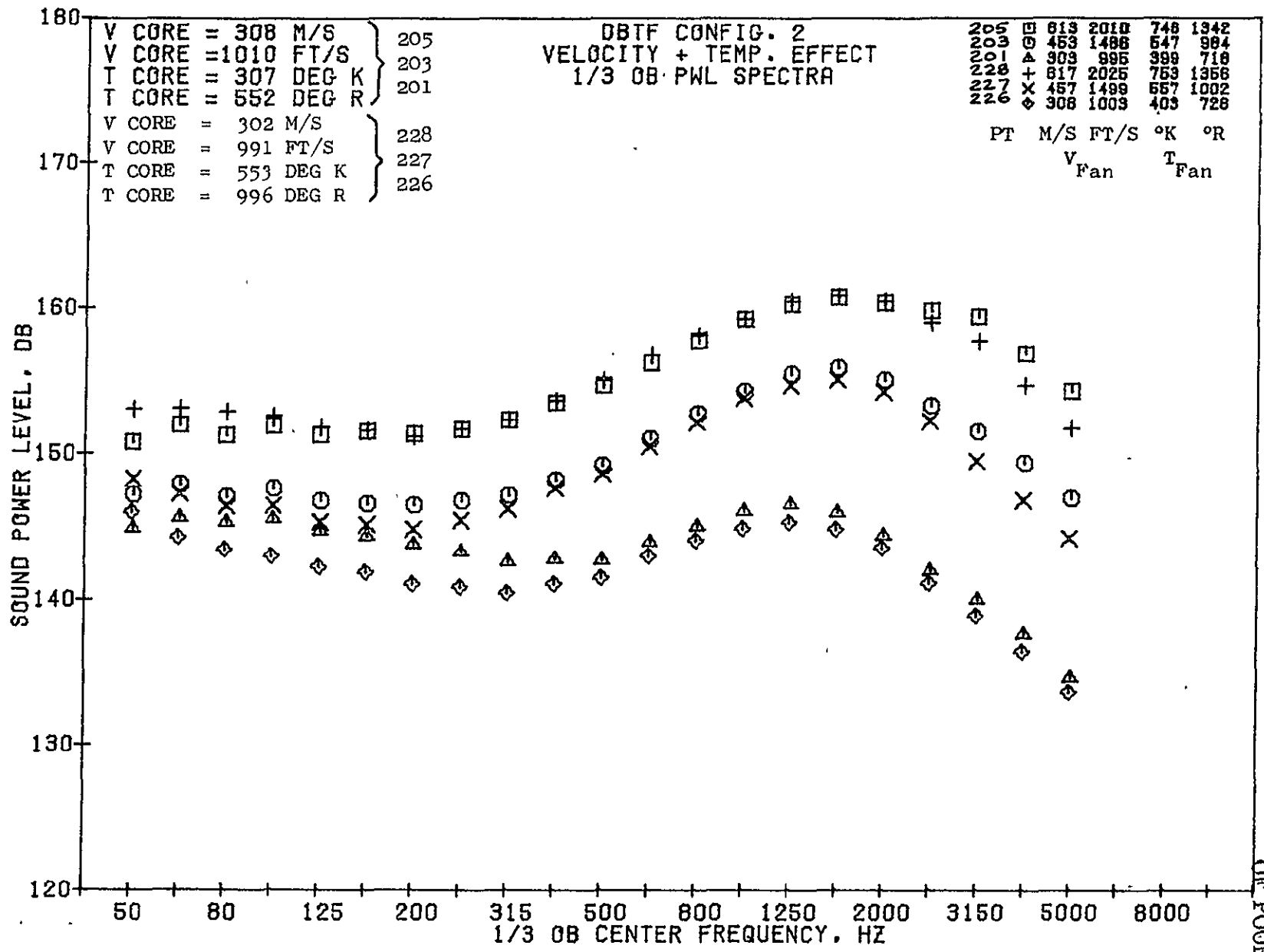


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79 BURC 9.

1361



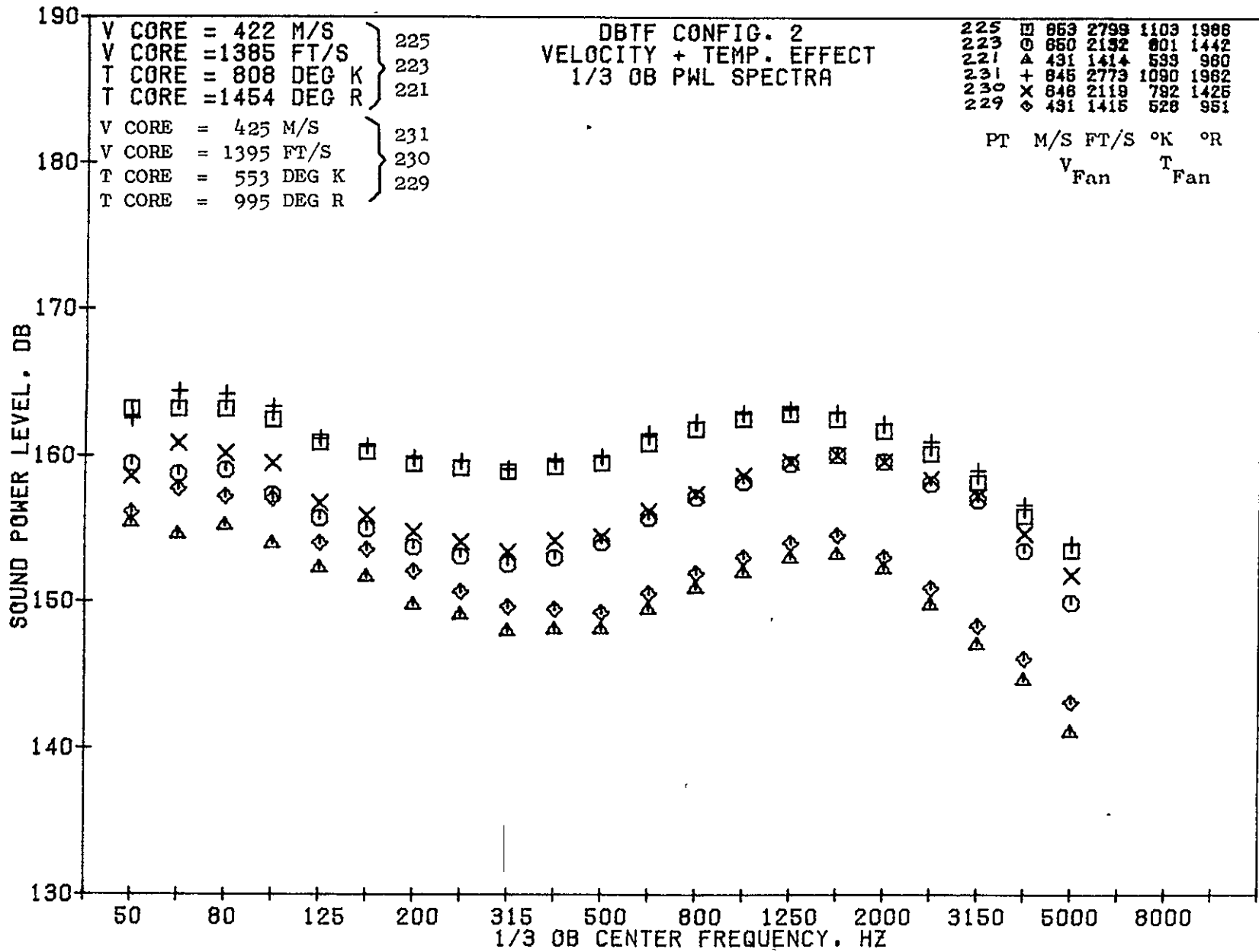
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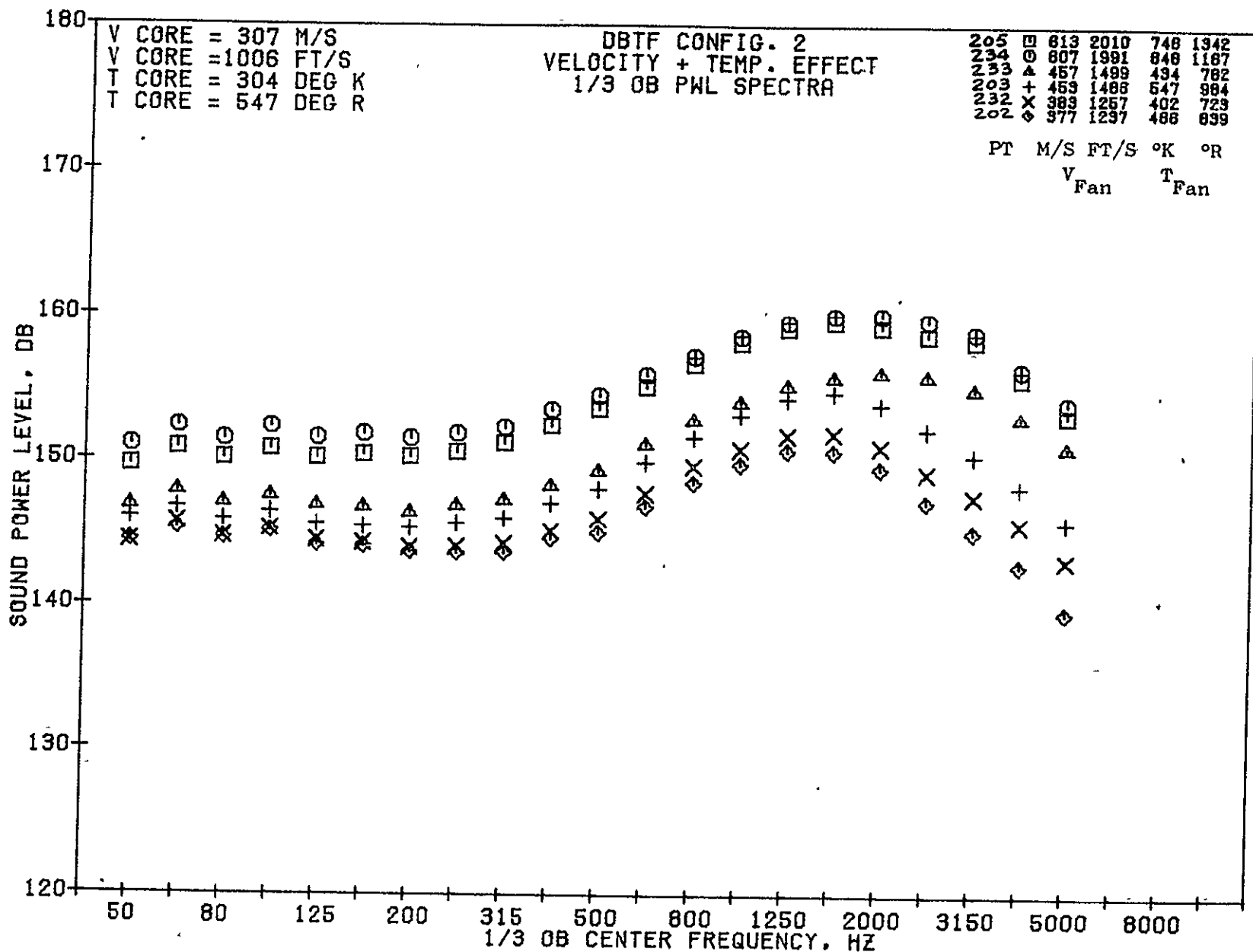


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79 BURC

1363



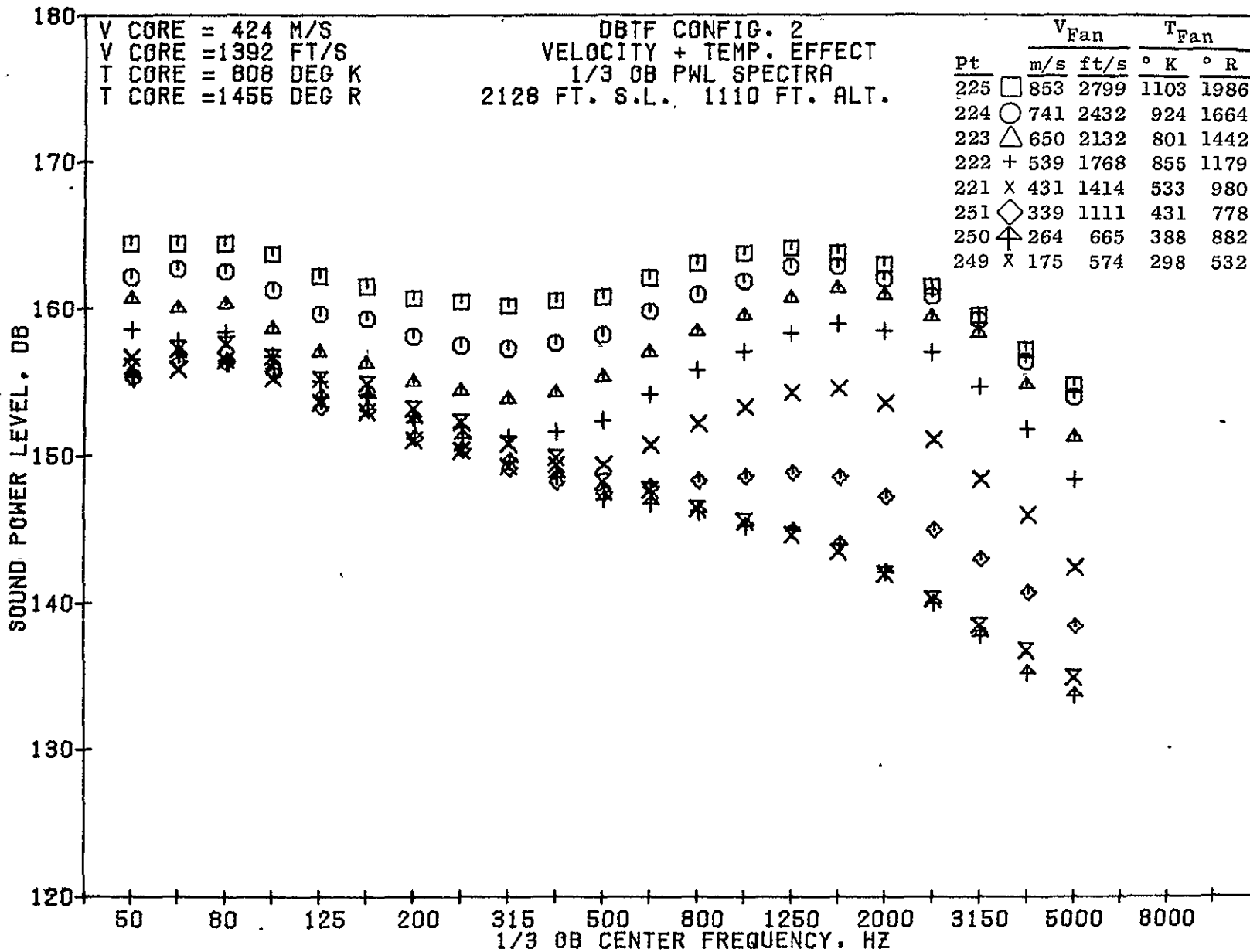
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1364

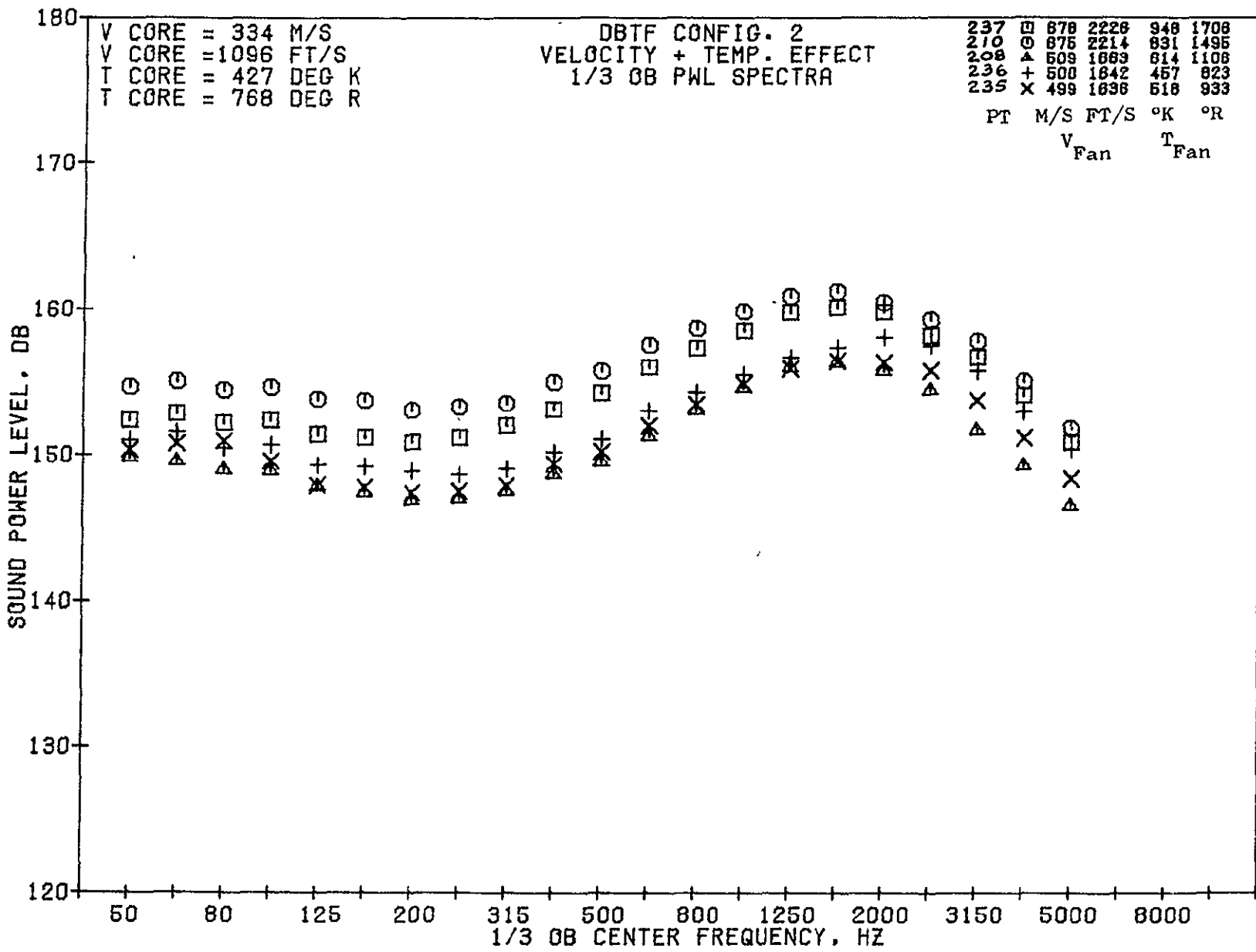


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79 BURC



1365

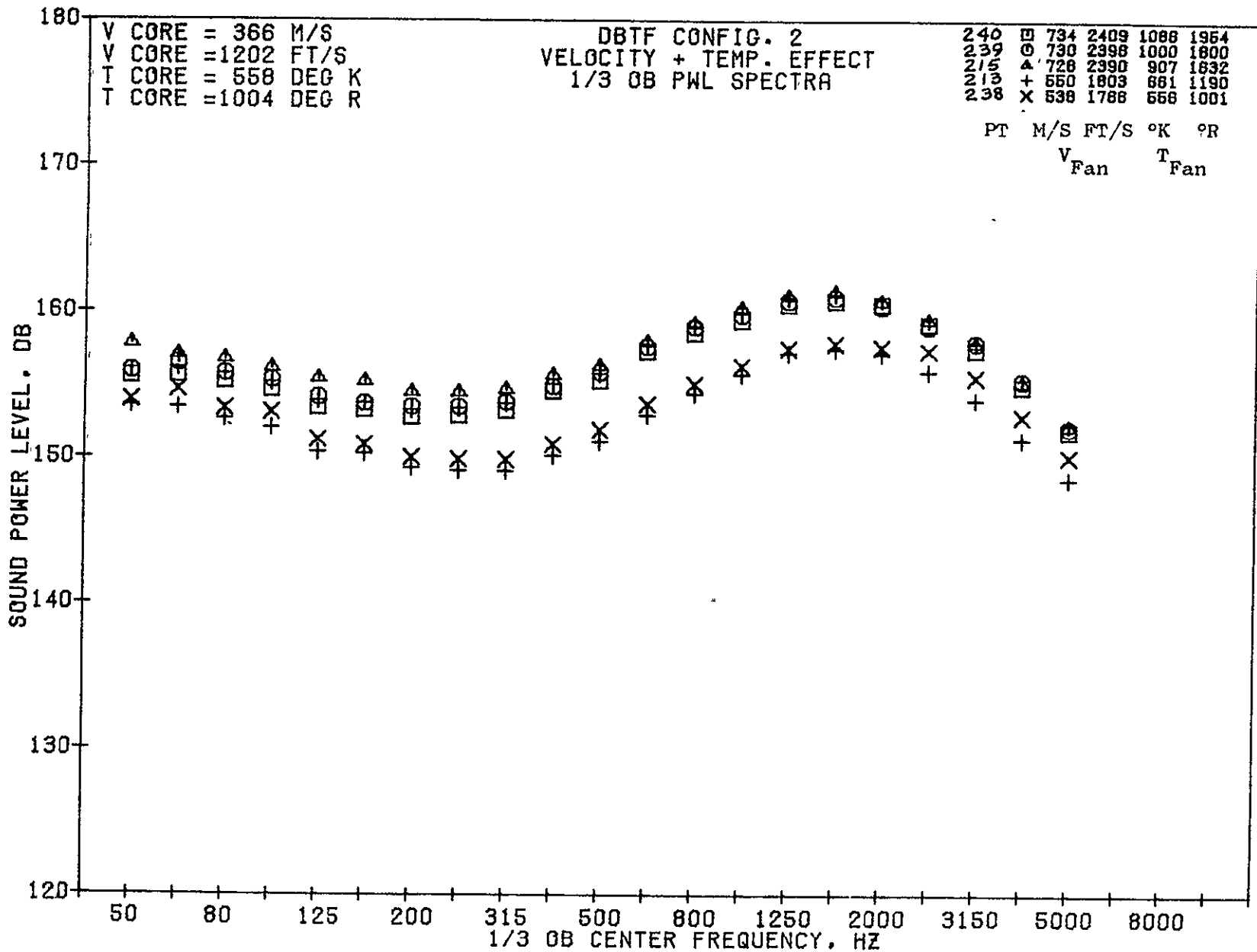
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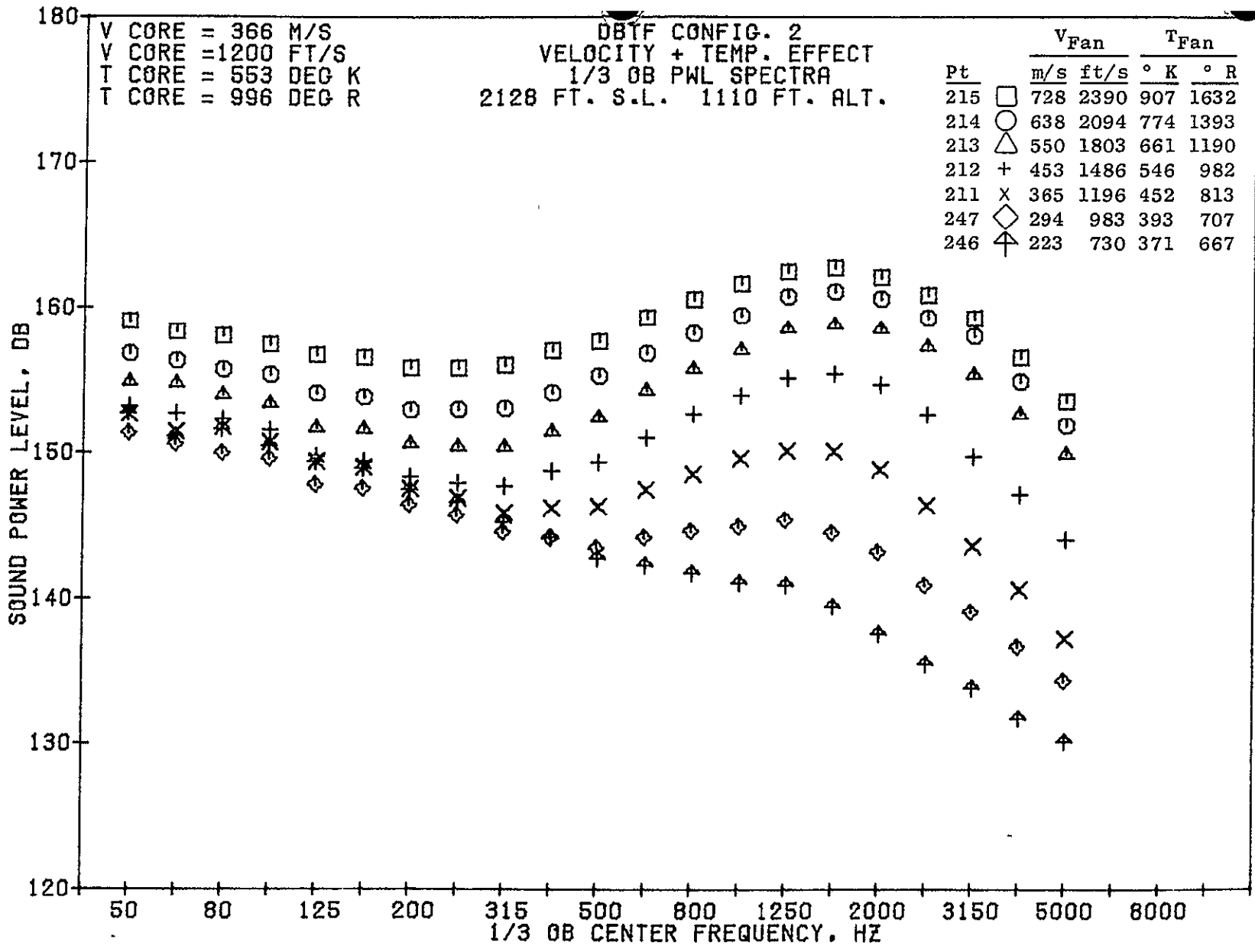
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79 BURCH



1367

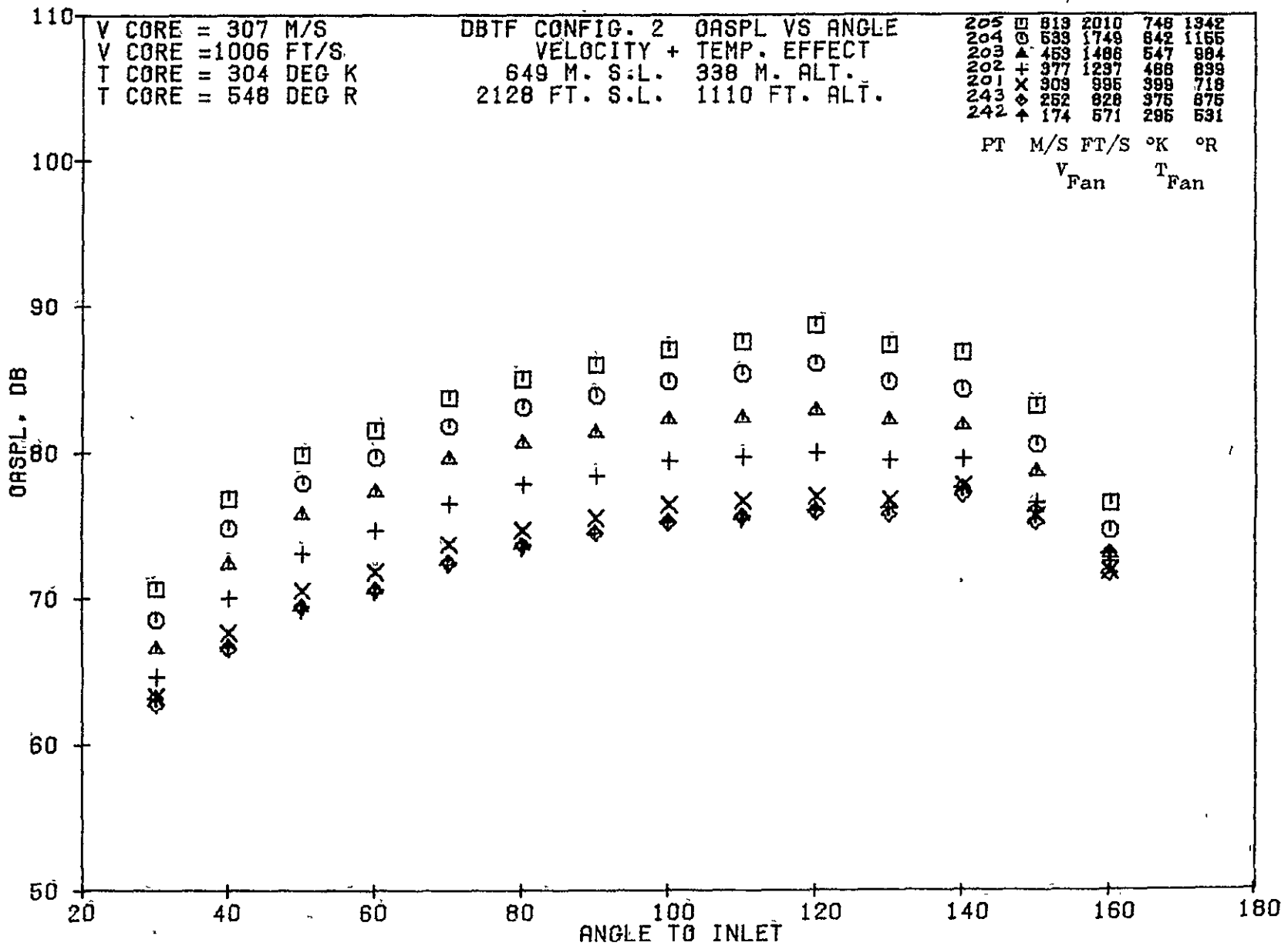
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99-7

08/18/75
5R266-001

79 AIRCRAFT

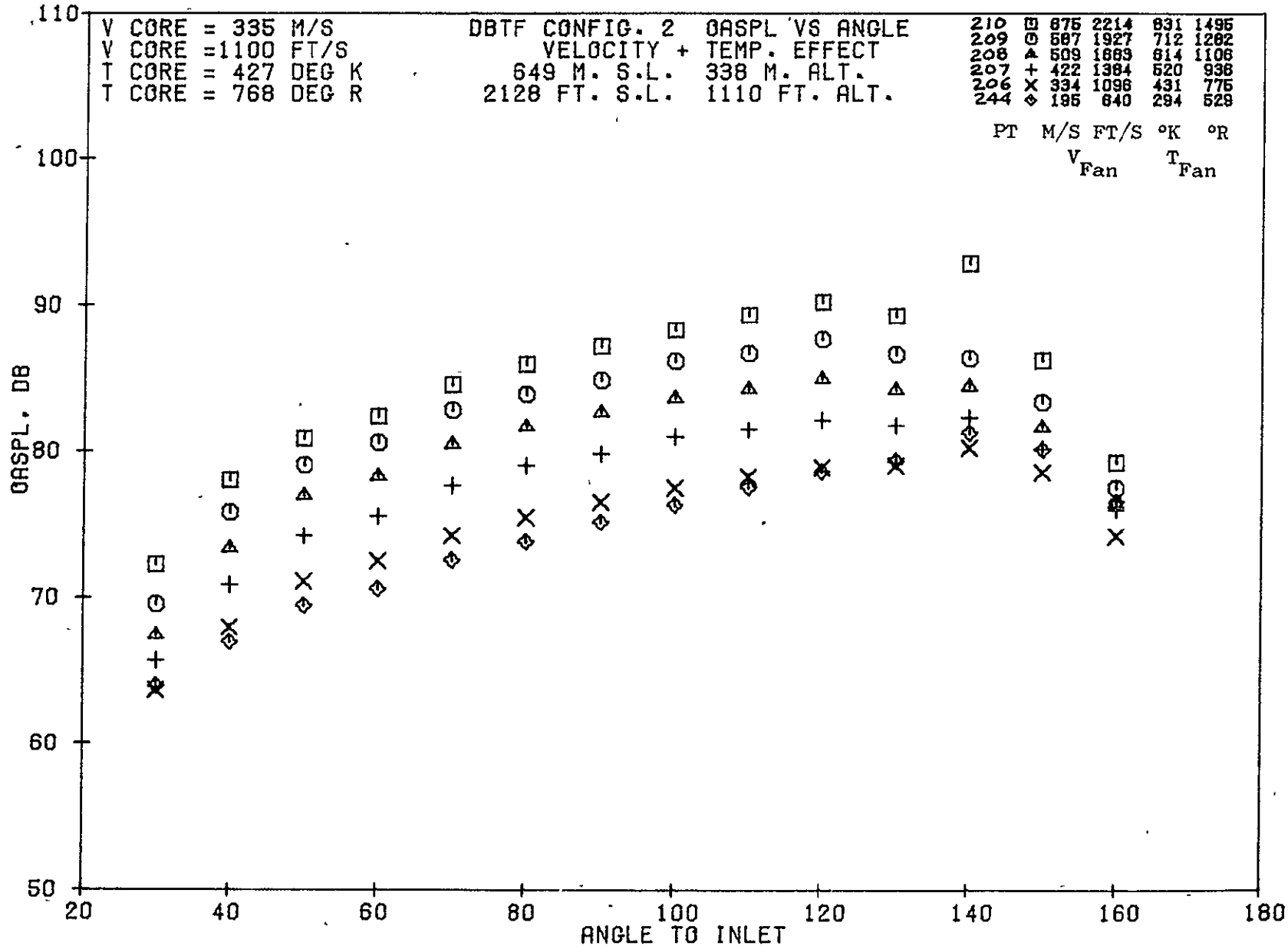
1368



1179

08/18/75
 5R266-001

79 BURCH



1369

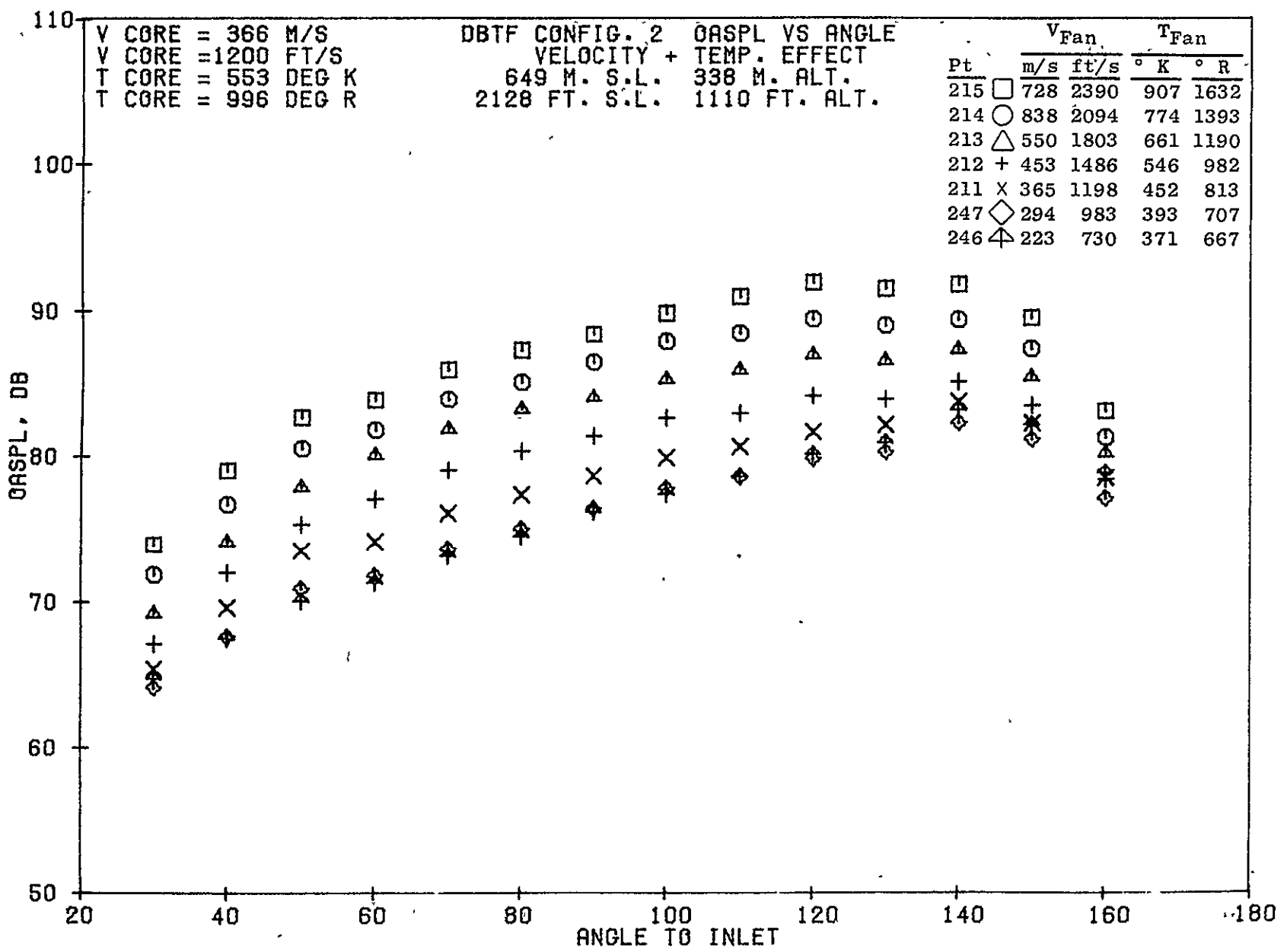
4-140

08/13/75
5R032-001

79 BURCH A.

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1370

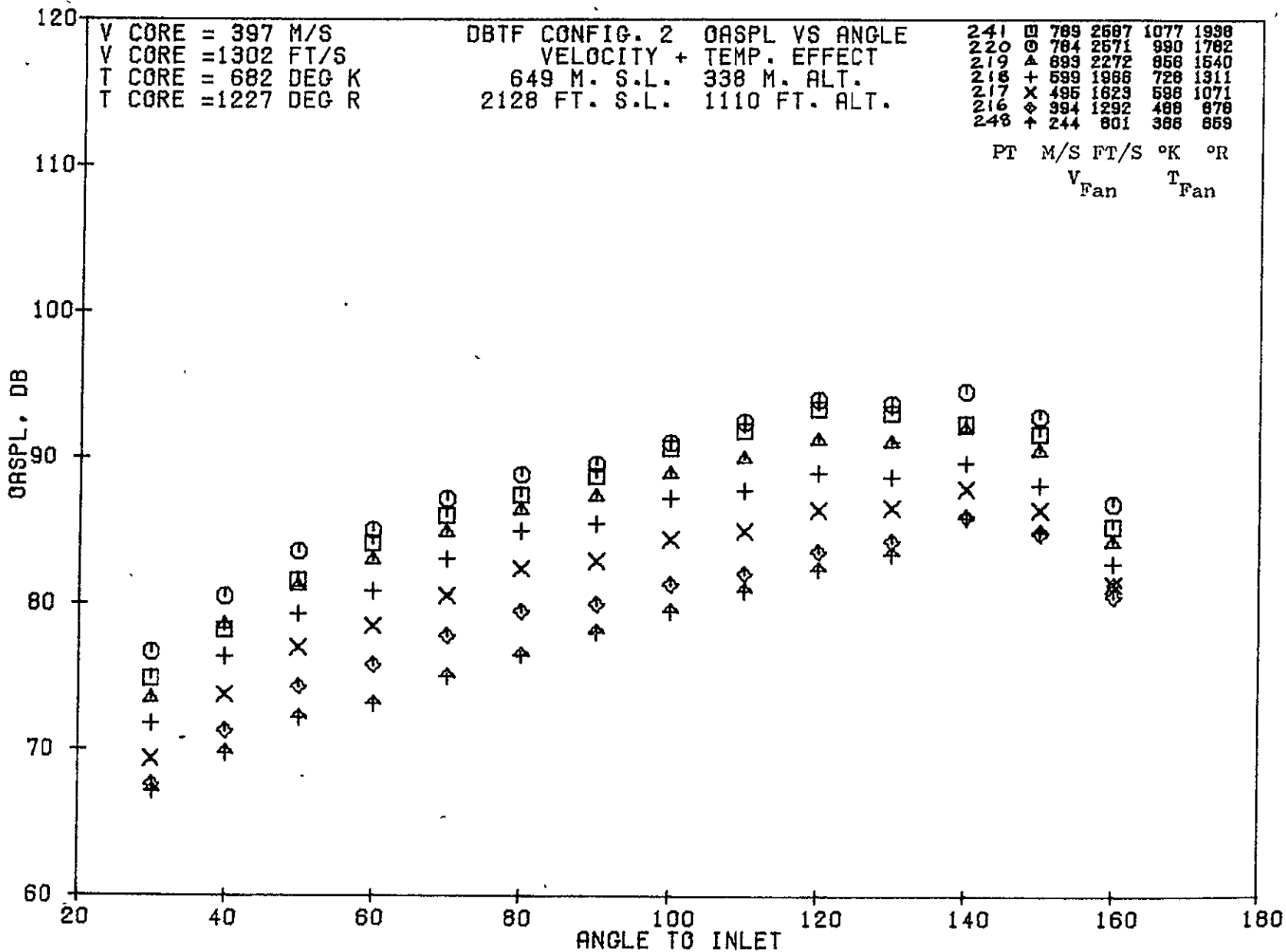


96-7

08/18/75
5R266-001

79 BURCI

1371

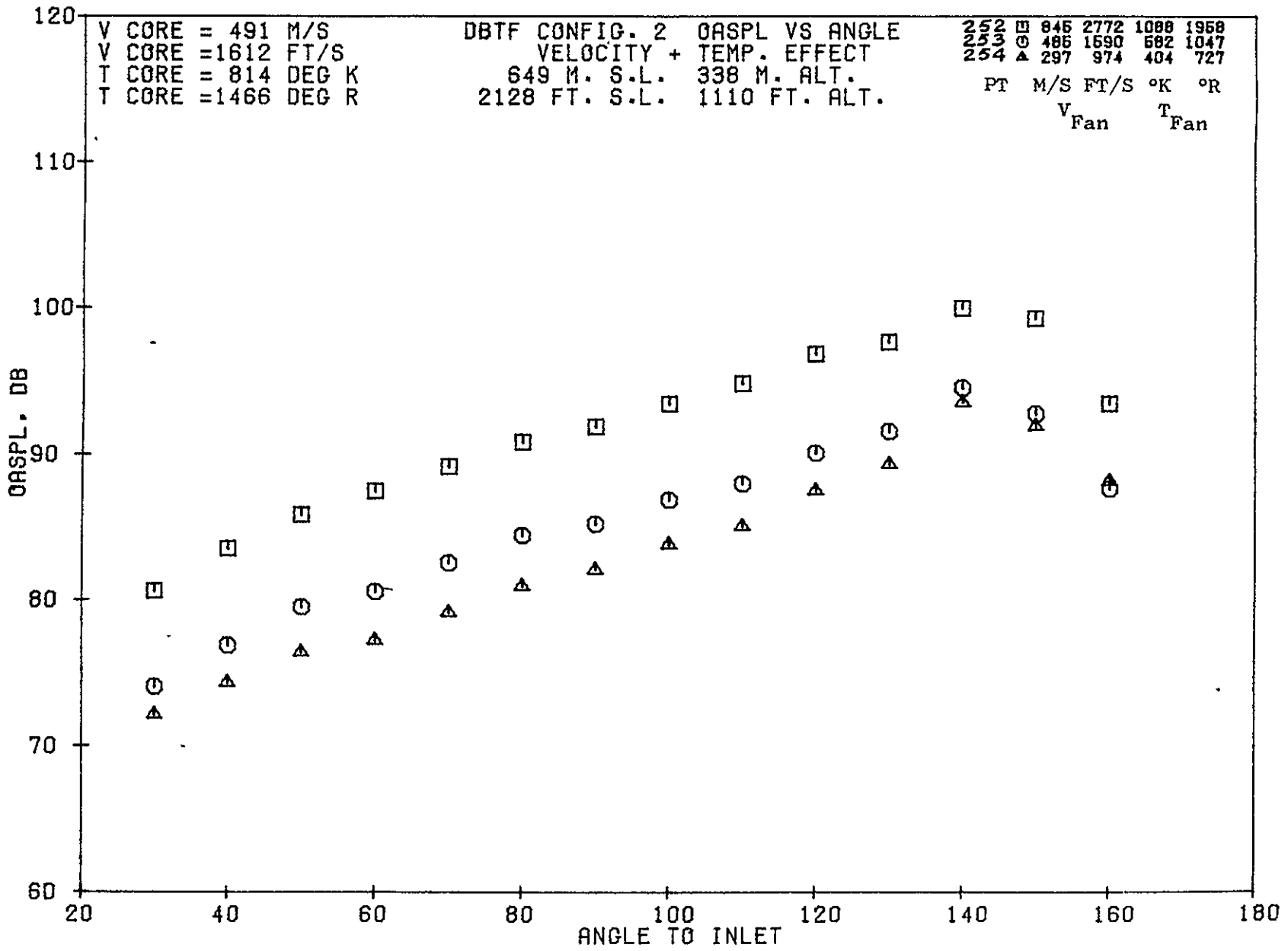


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5R266-001

79 BIRCH A.

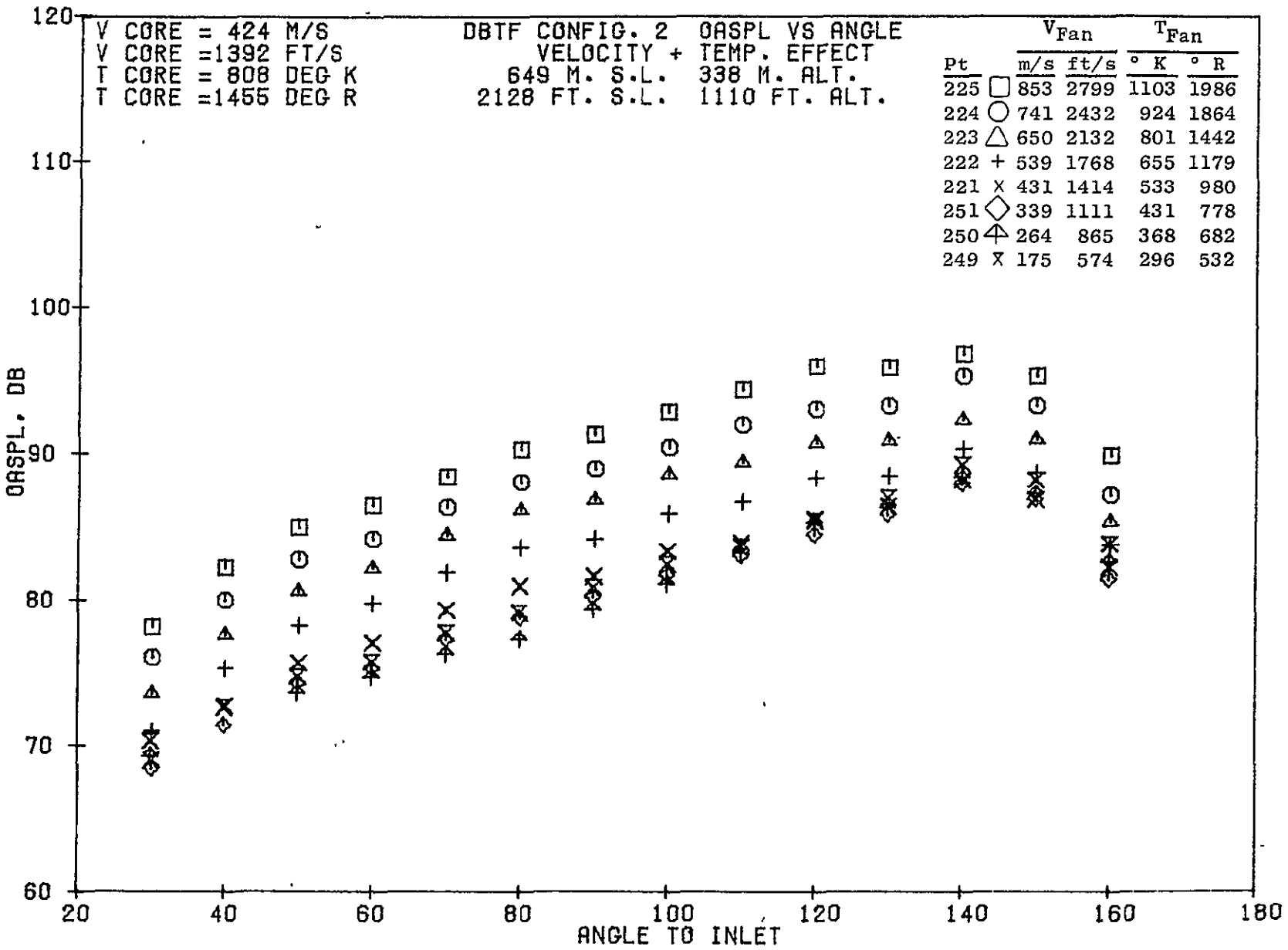
141



08/13/75
5R032-001

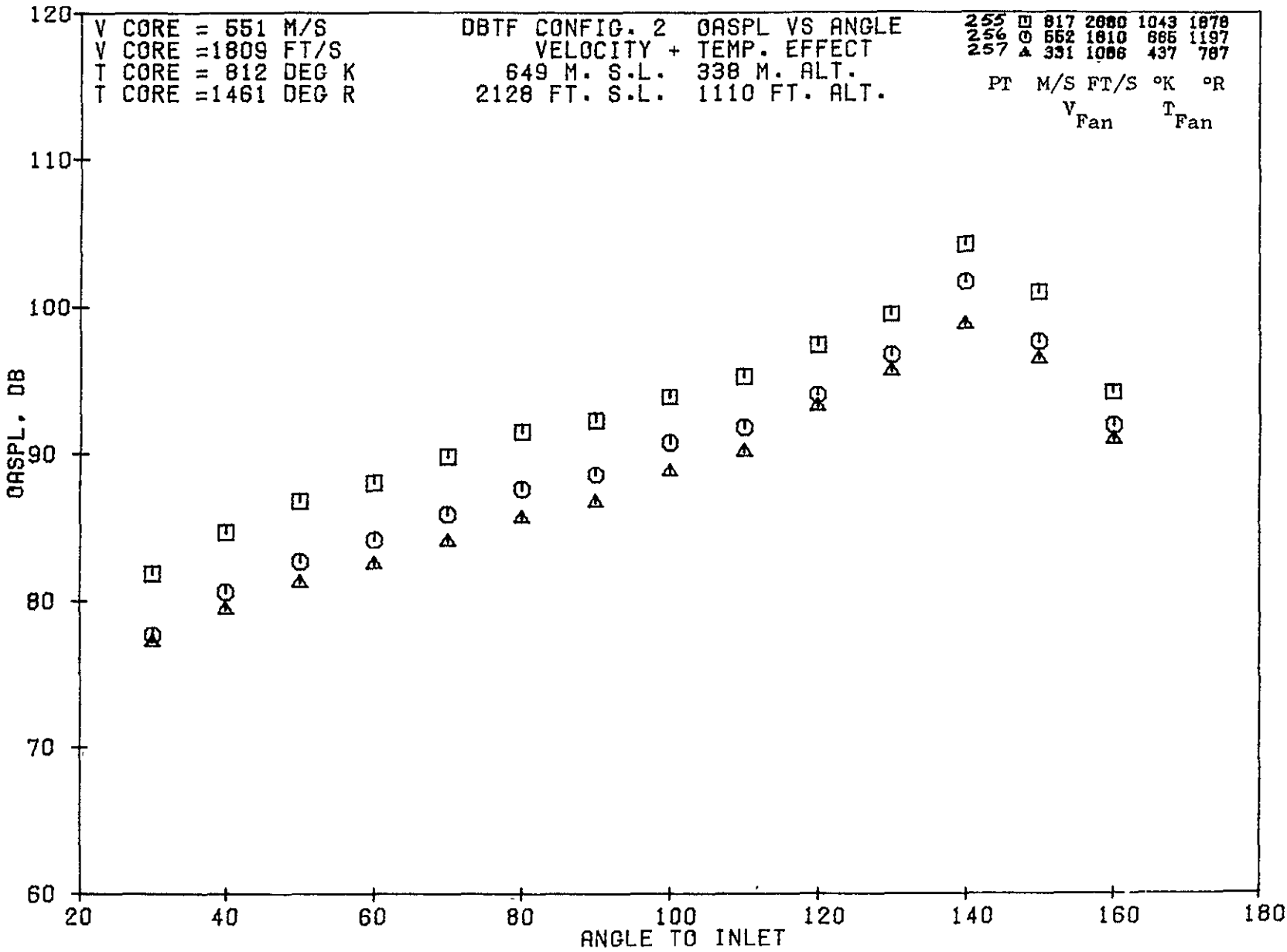
79 BURCH A.

1373



477

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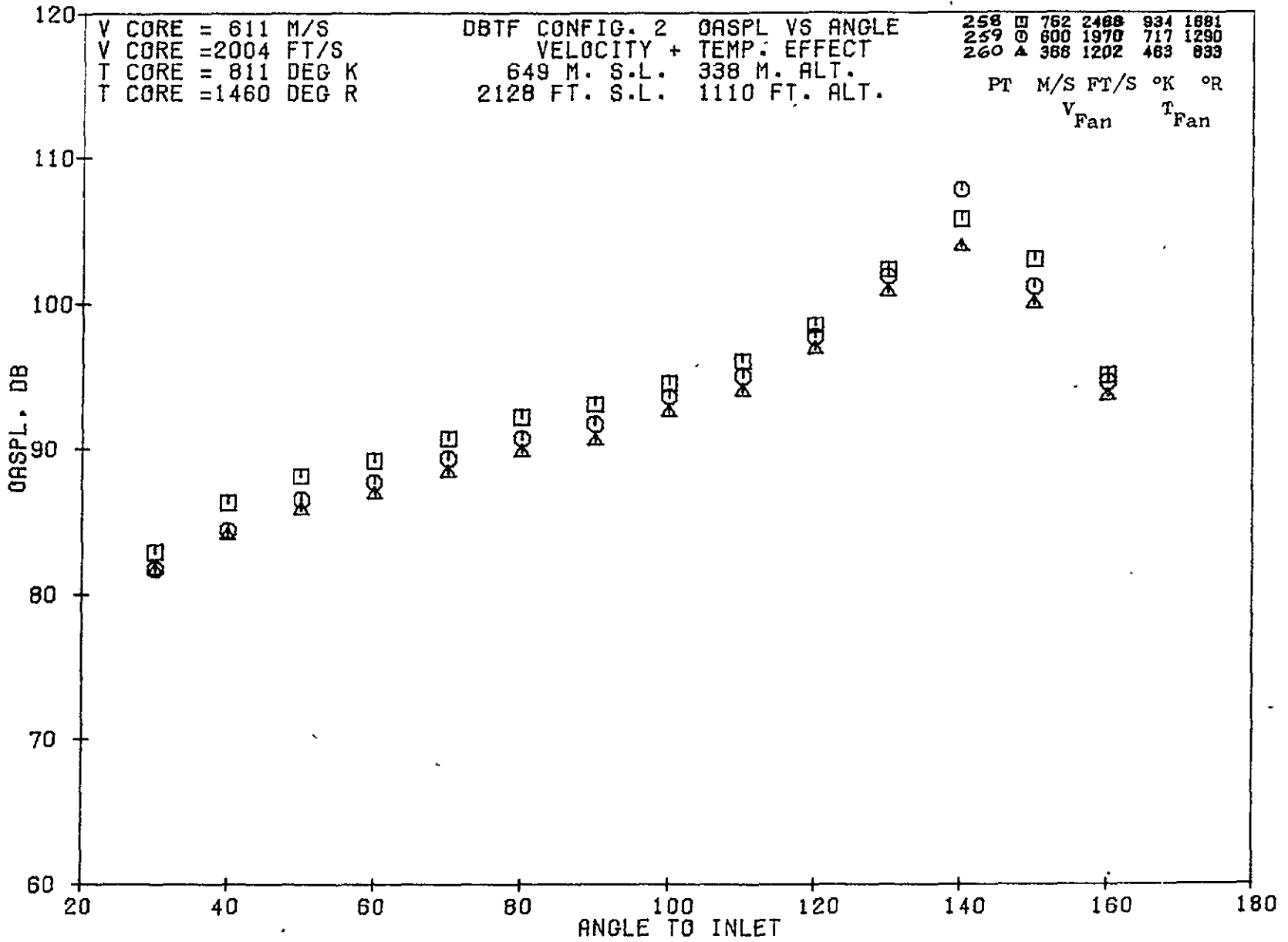
1374

1.113

08/13/75
5R032-001

79 BURC

1375



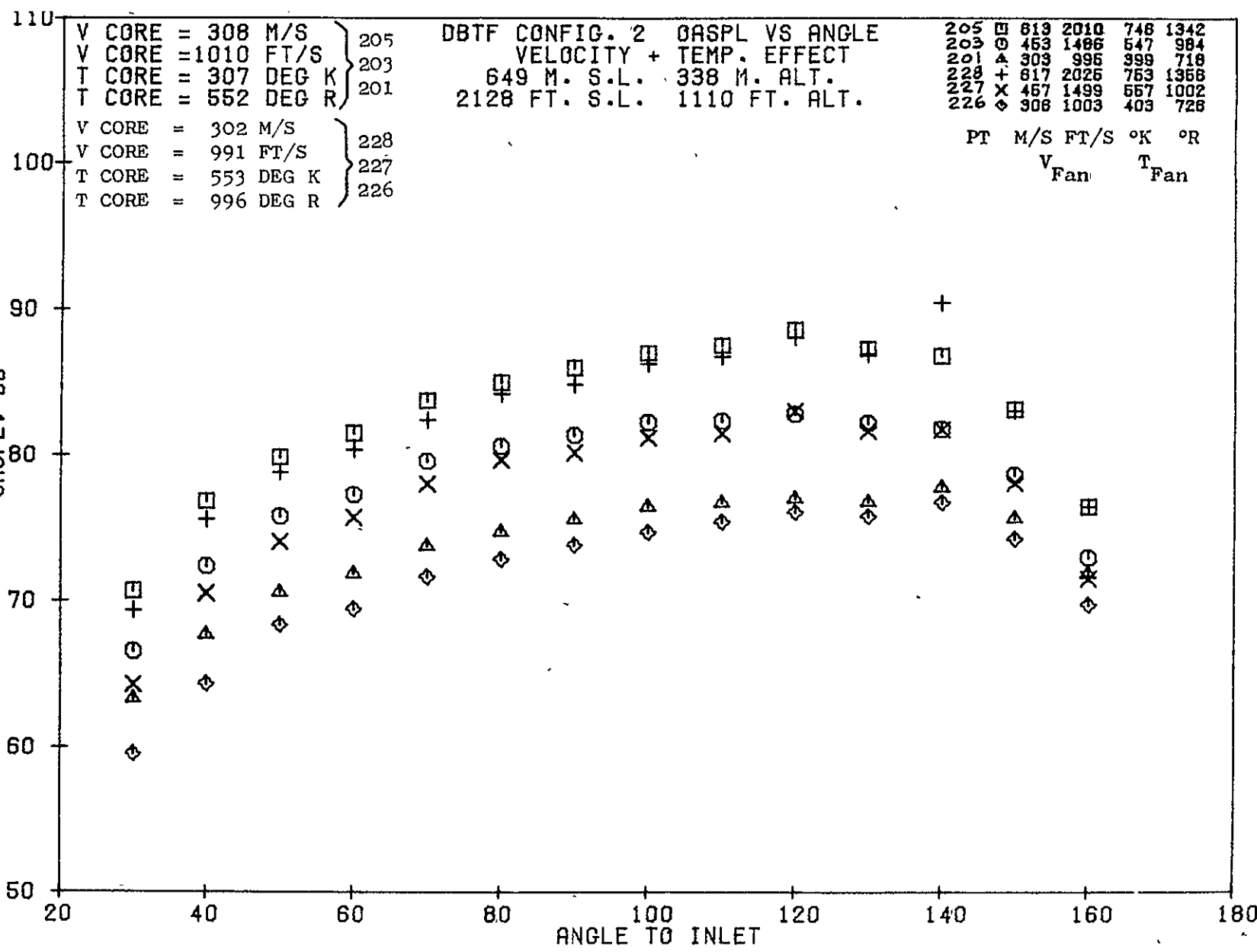
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08/13/75
5R032-001

79 BURCH A.

4-14-75

1376

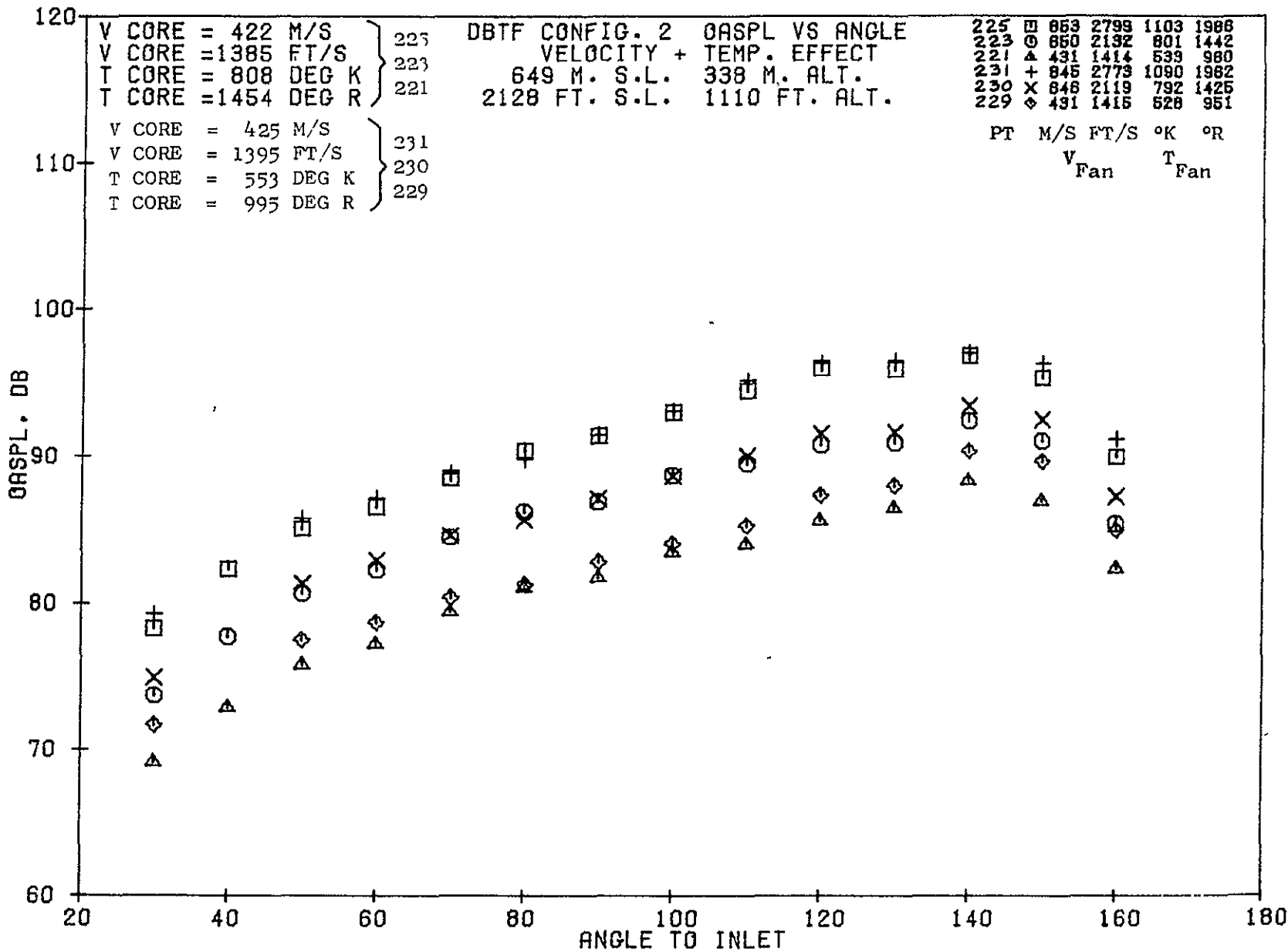


4-145

08/13/75
5R032-001-

79 BURC

1377



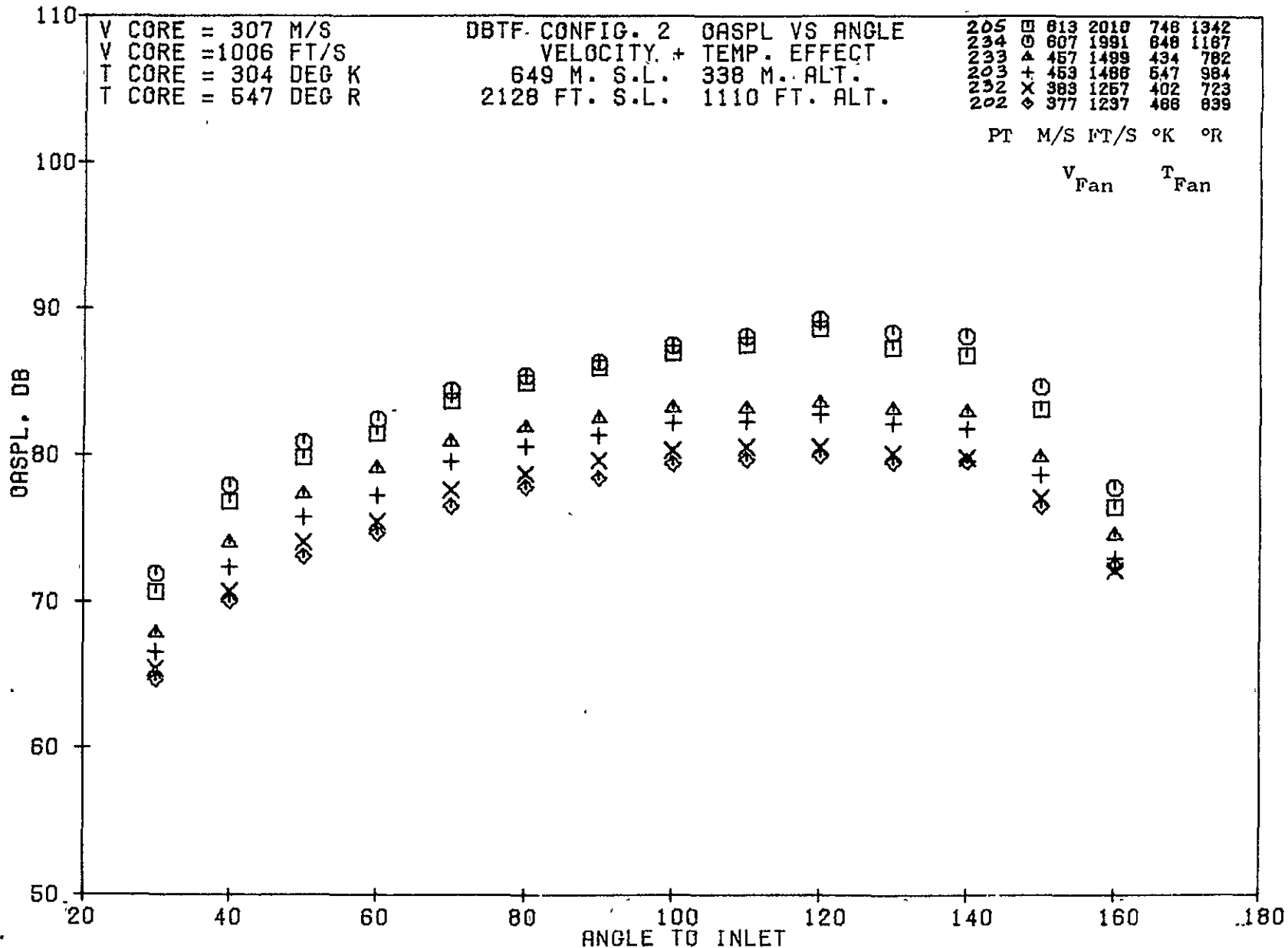
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08/13/75
5R032-001

79 BURCH-A.

1-11-75

1378

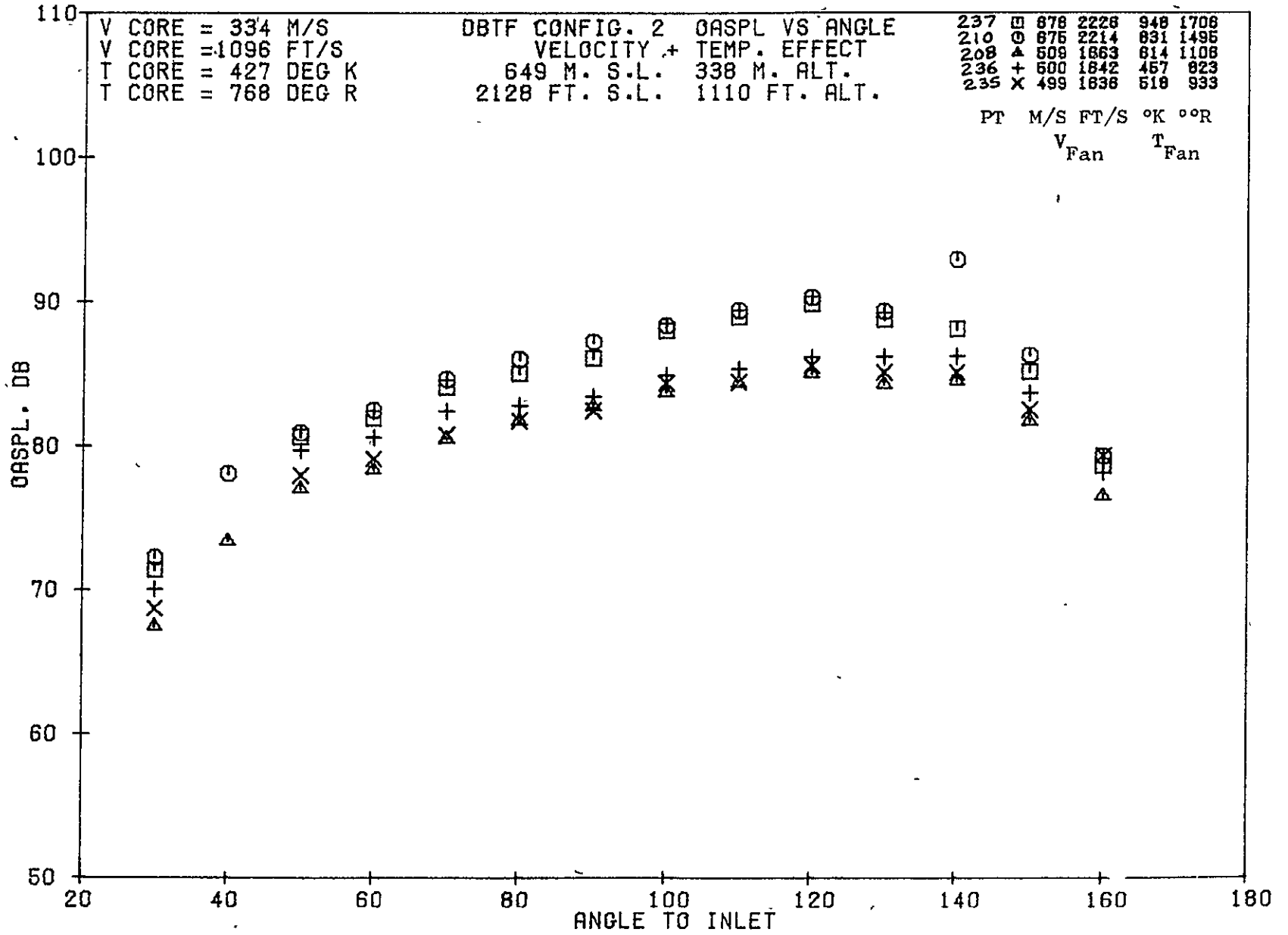


147

08/13/75
5R032-001

79 BURCH A.

1379

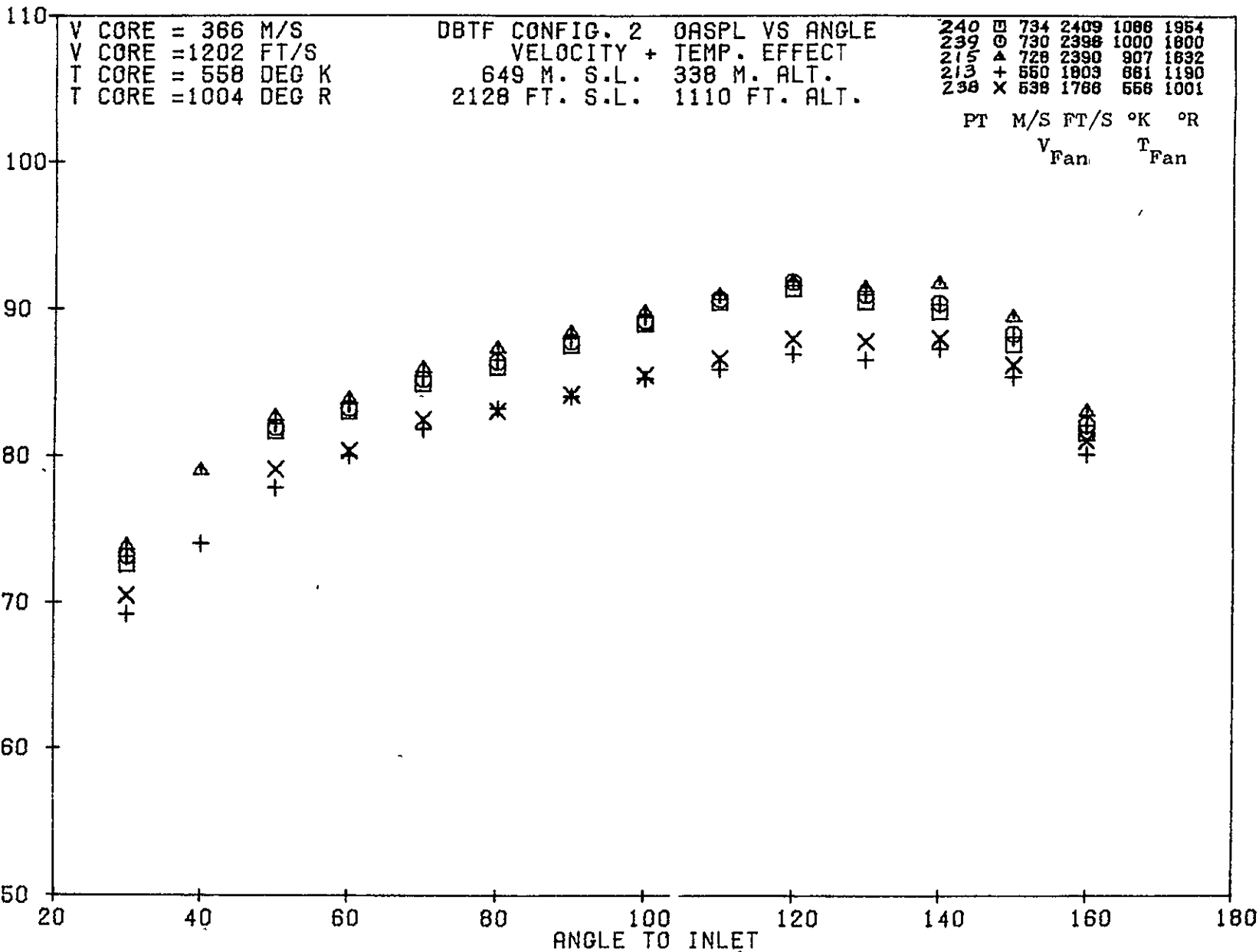


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1-11-75

08/13/75
5R032-001

79 BURCH A.

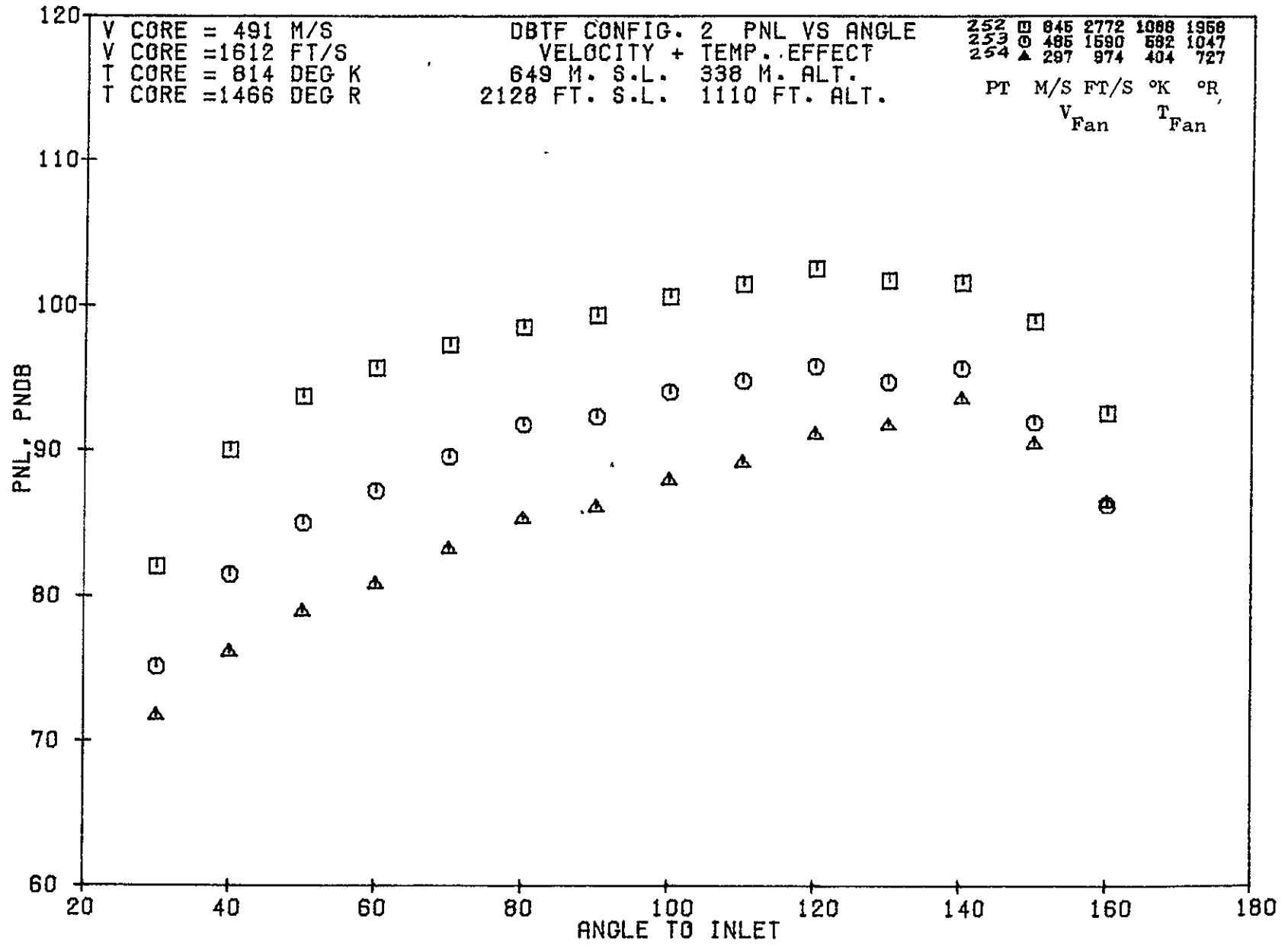


1380

U
149

08/13/75
 5R032-001

79 BURCK



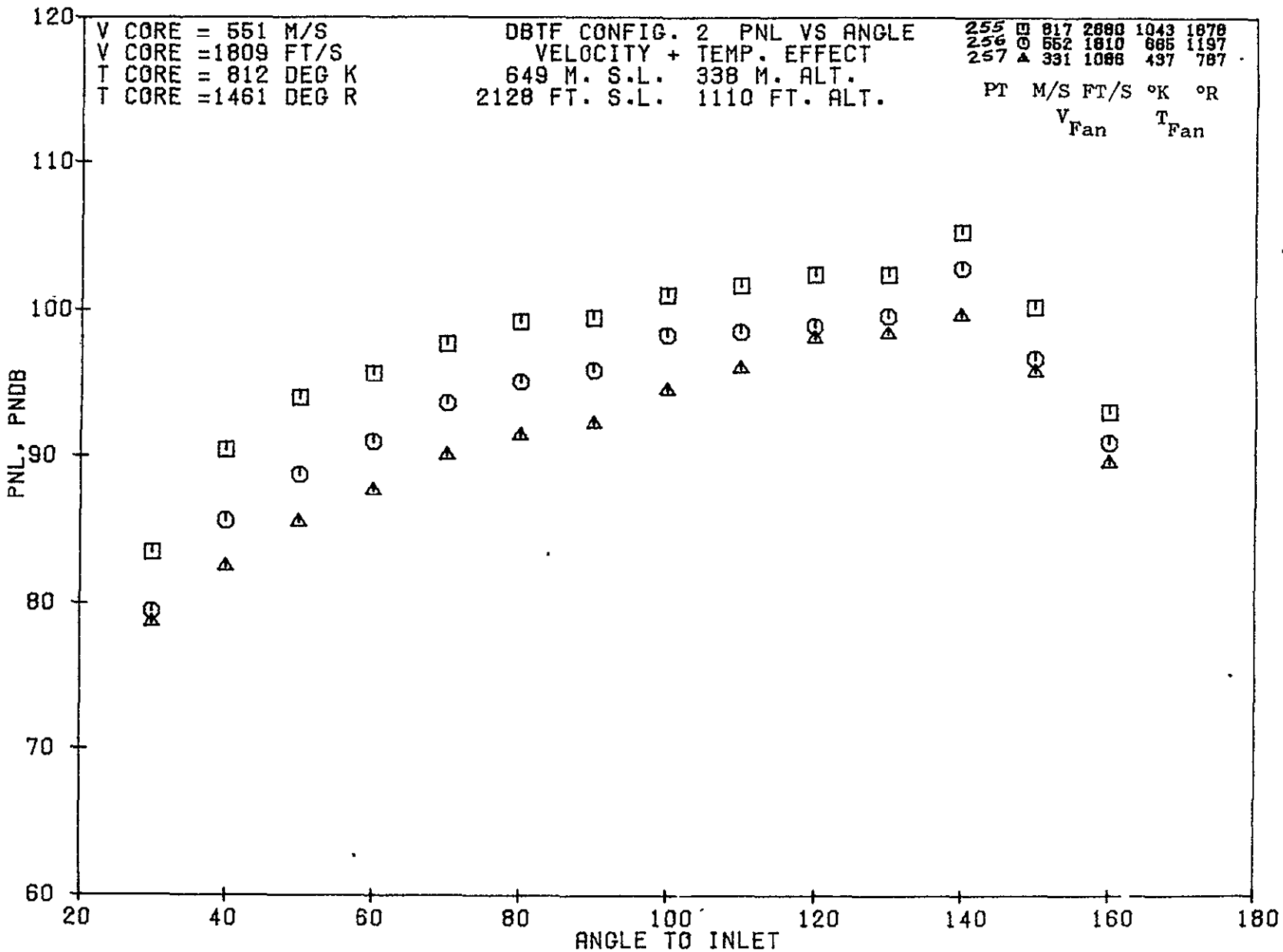
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5R266-001

79 BIRCH A.

U-150

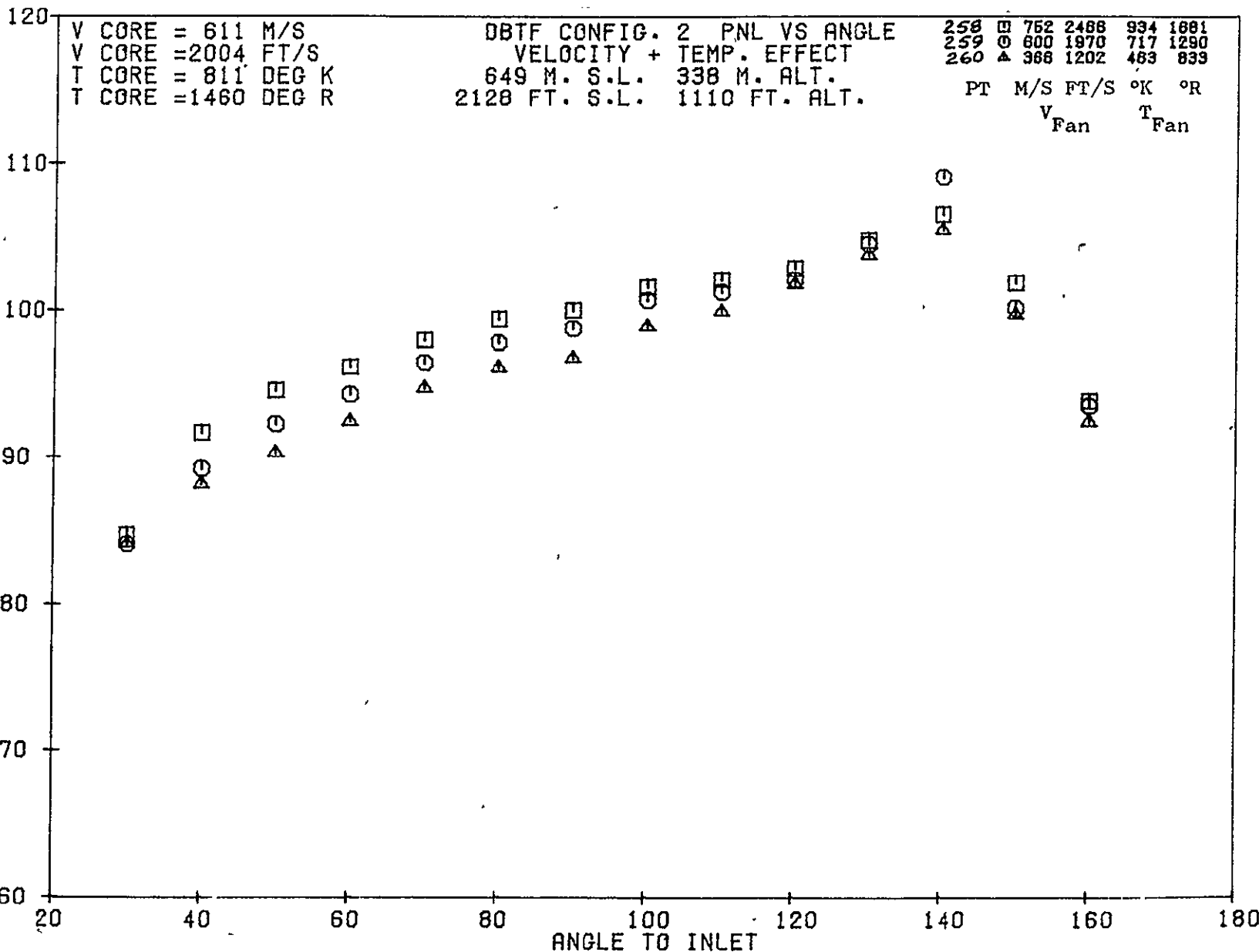


1382

1.51

08/13/75
 5R032-001

79 BURCA



1383

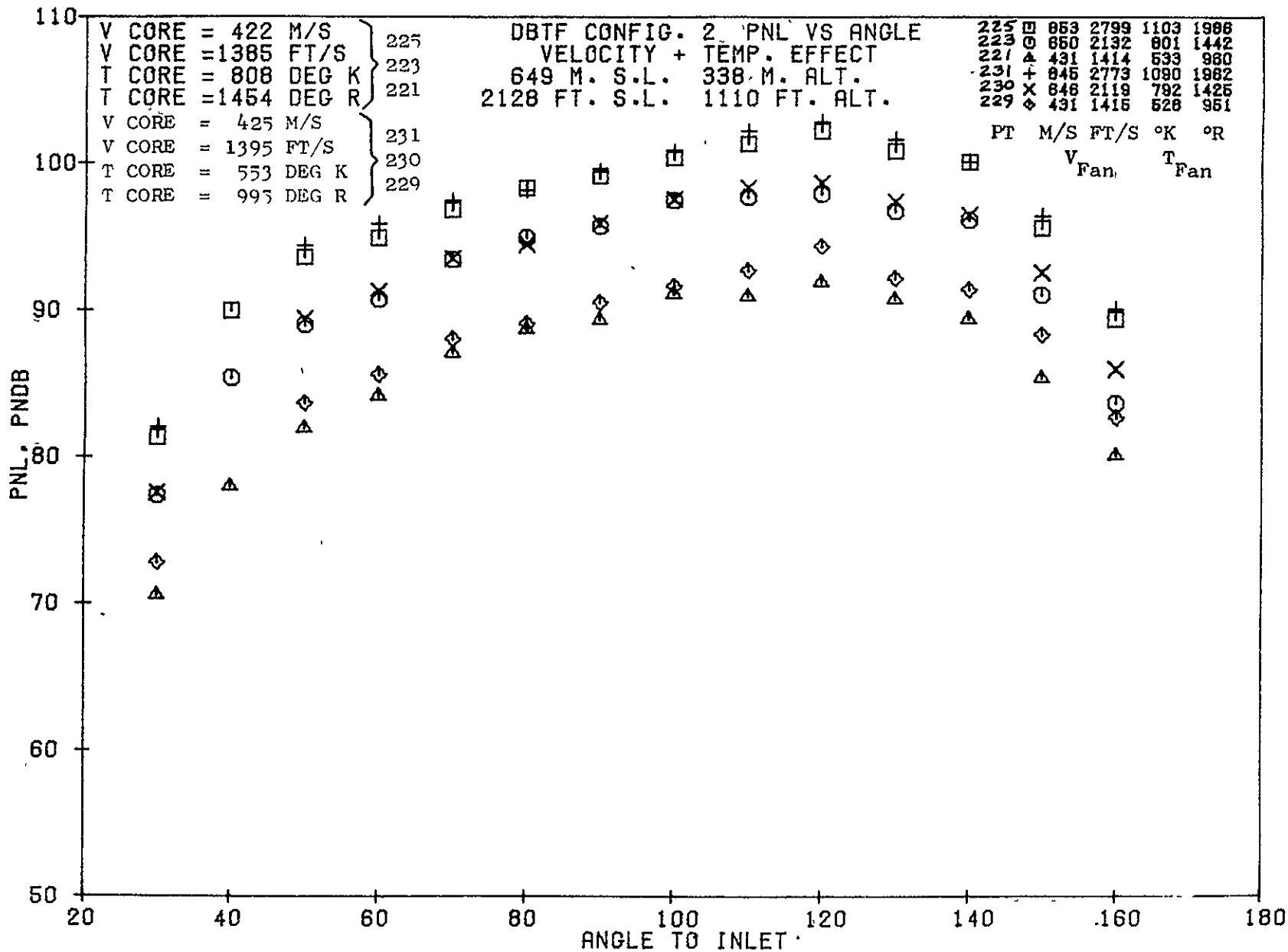
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08/13/75
5R032-001

79 BURCH A.

4152

1384

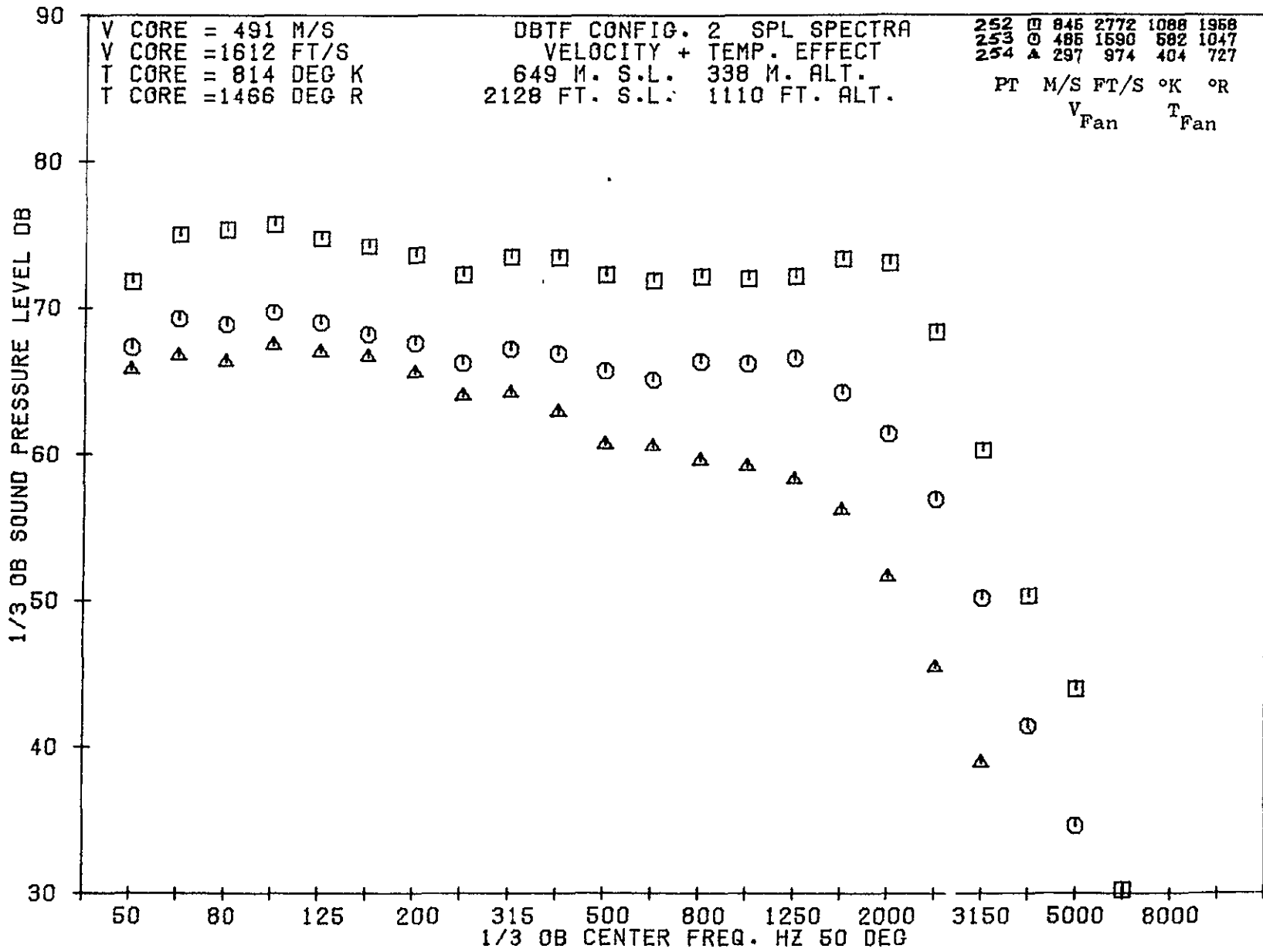


1-153

08/13/75
5R032-001

79 BURC

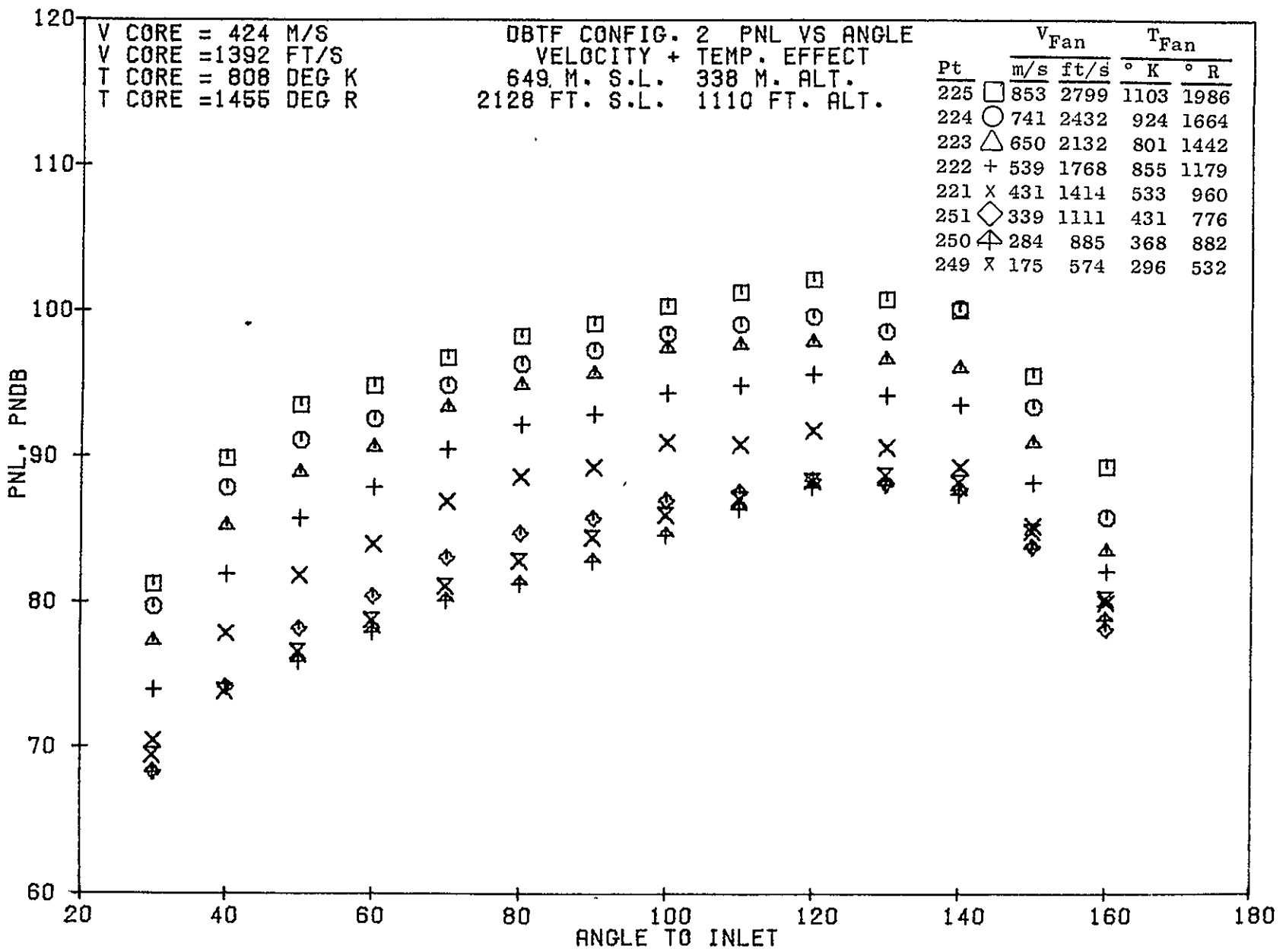
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1-151

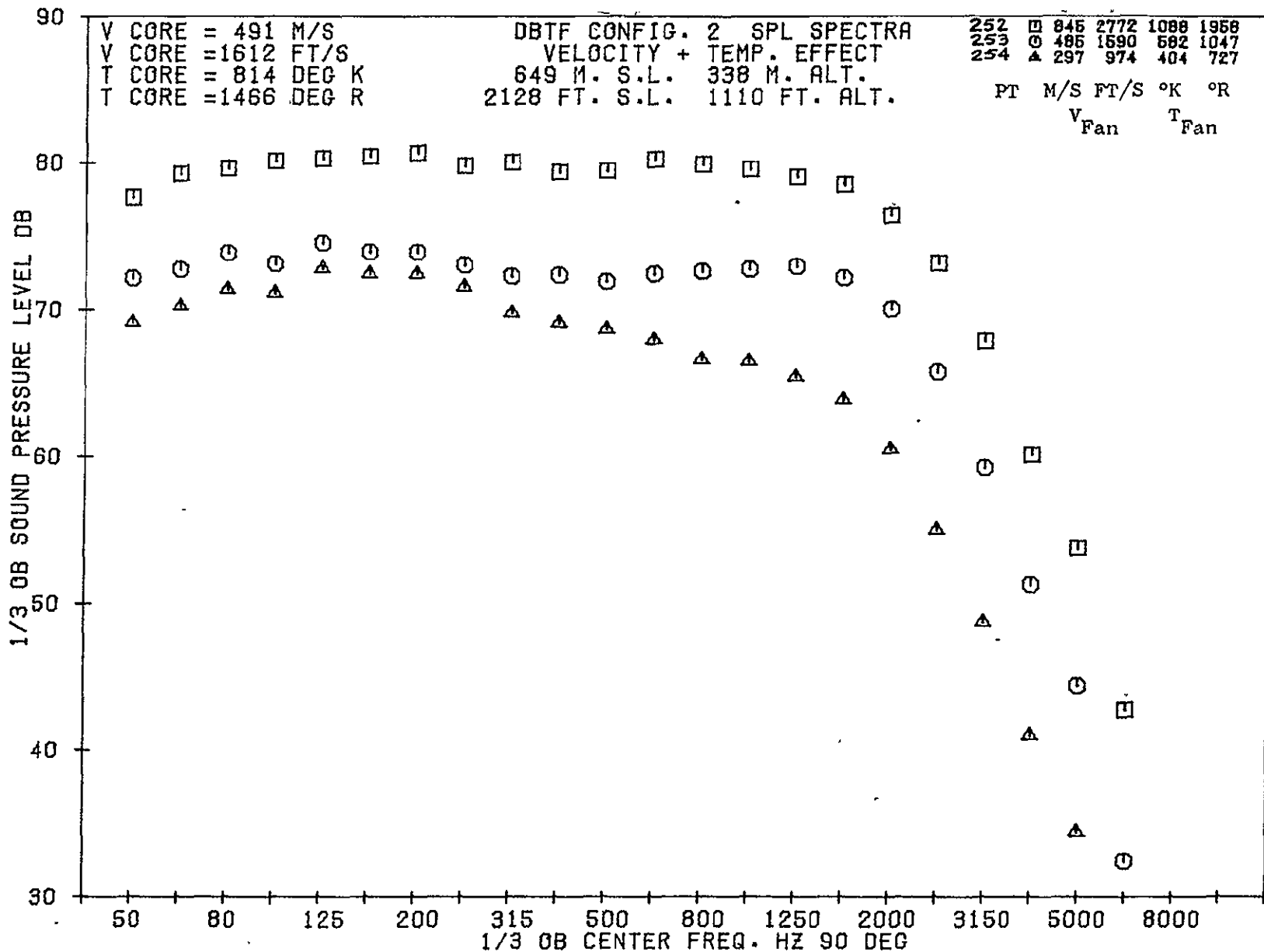
1386



0254

08/18/75
5R266-001

79 BURC



1387

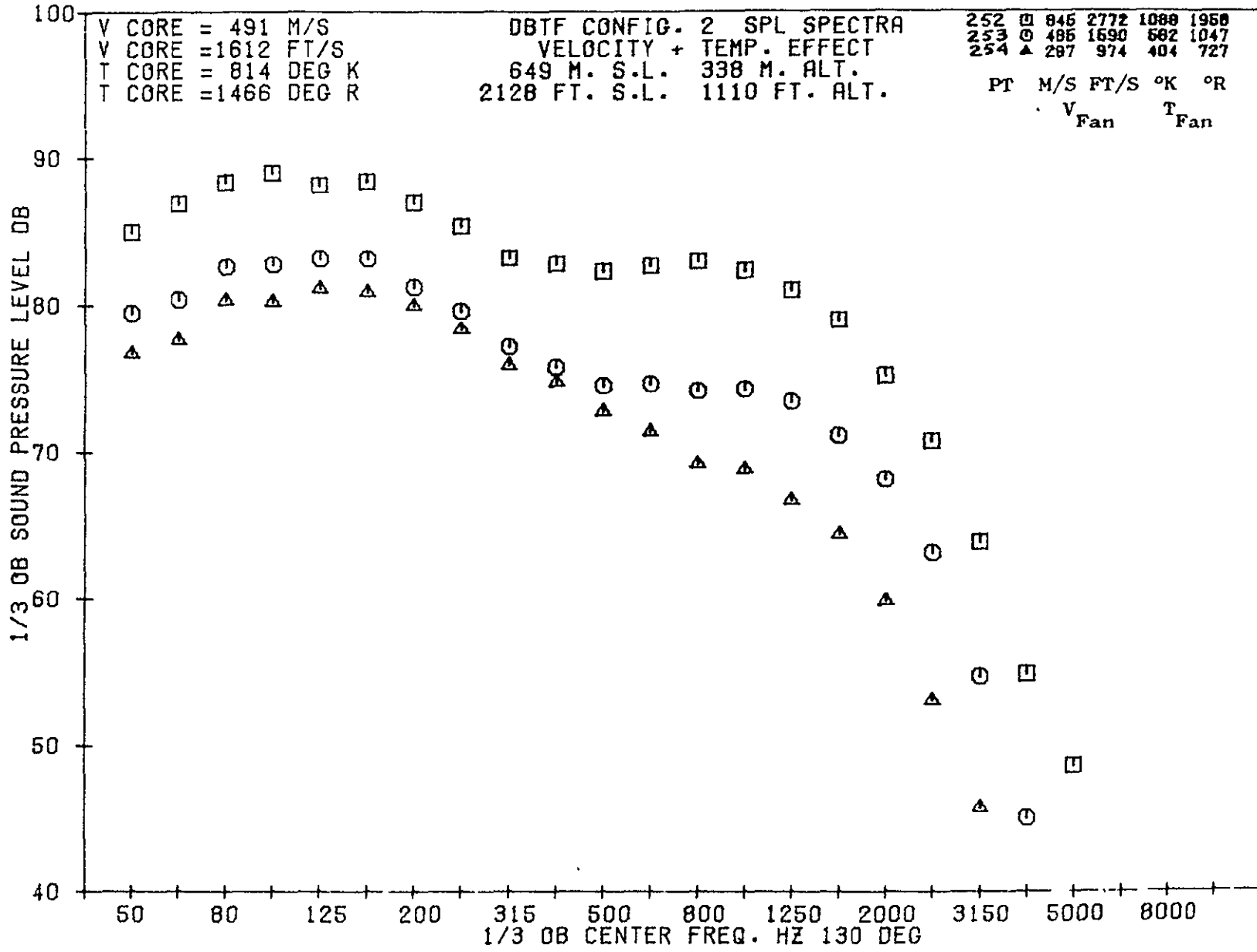
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08/13/75
 5R032-001

79 BURCH A.

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1388



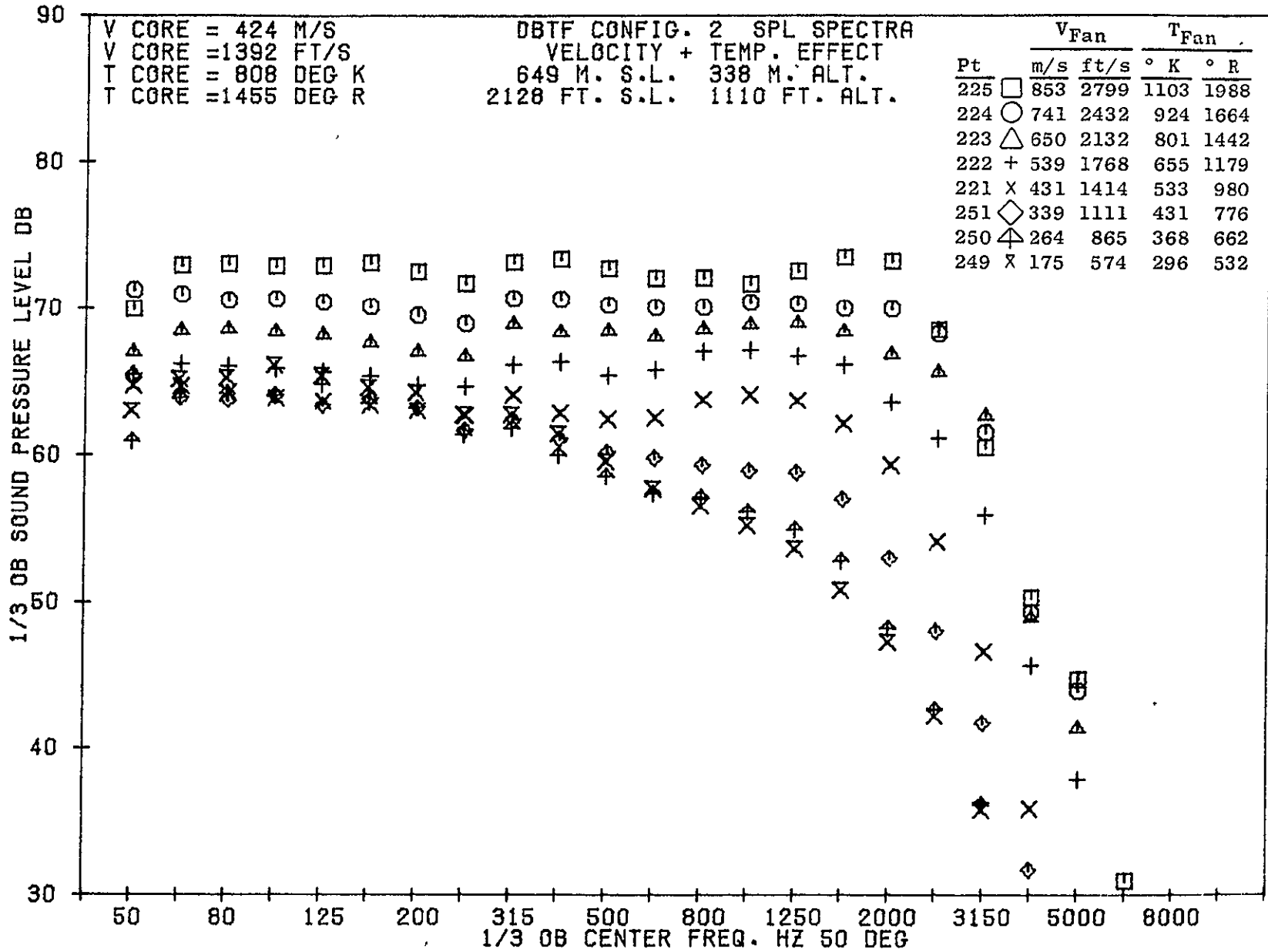
4156

08/13/75
5R032-001

79 BURCH A.

1170

1389

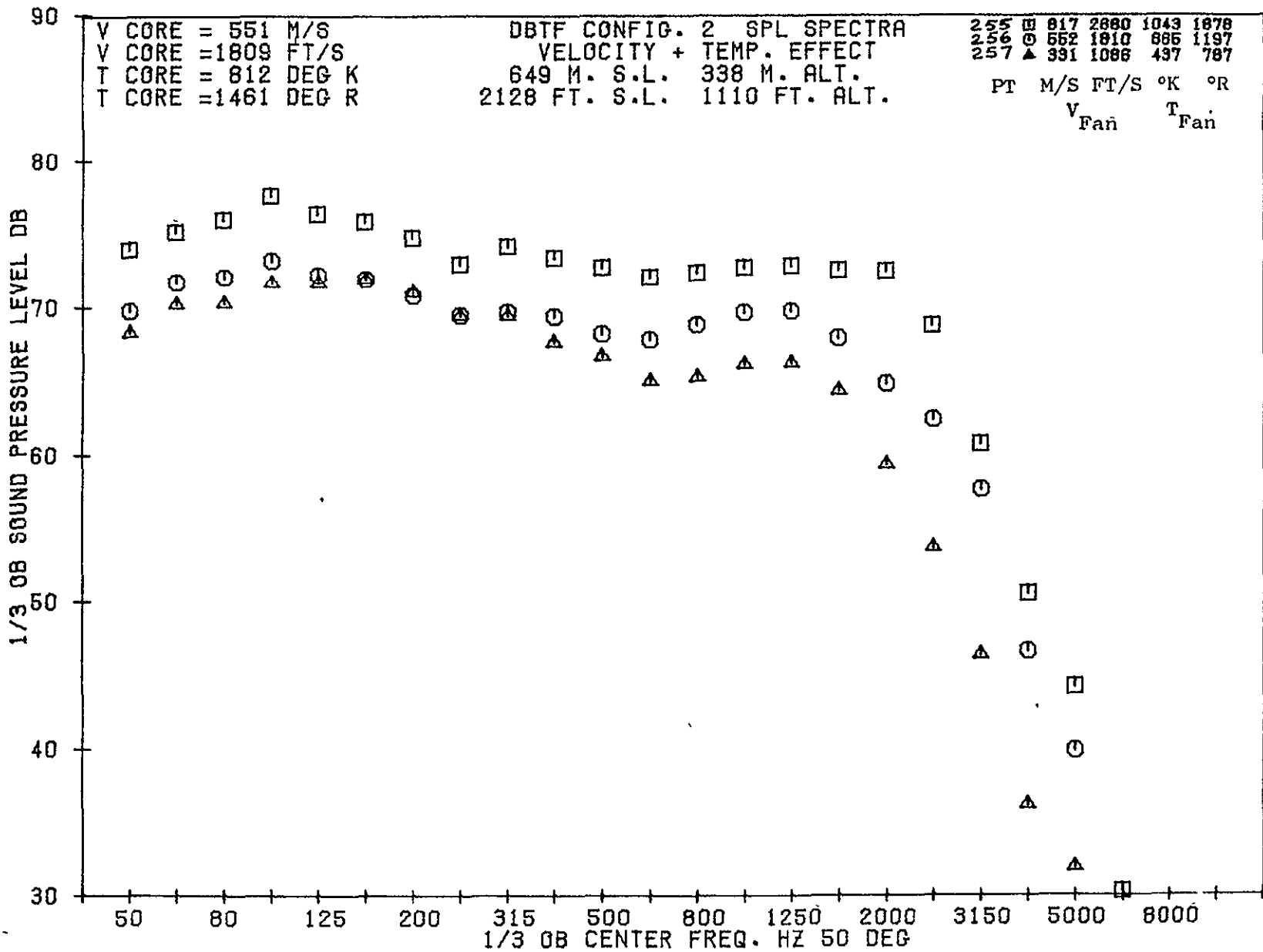


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5R266-001

79 BURCH A.

1390

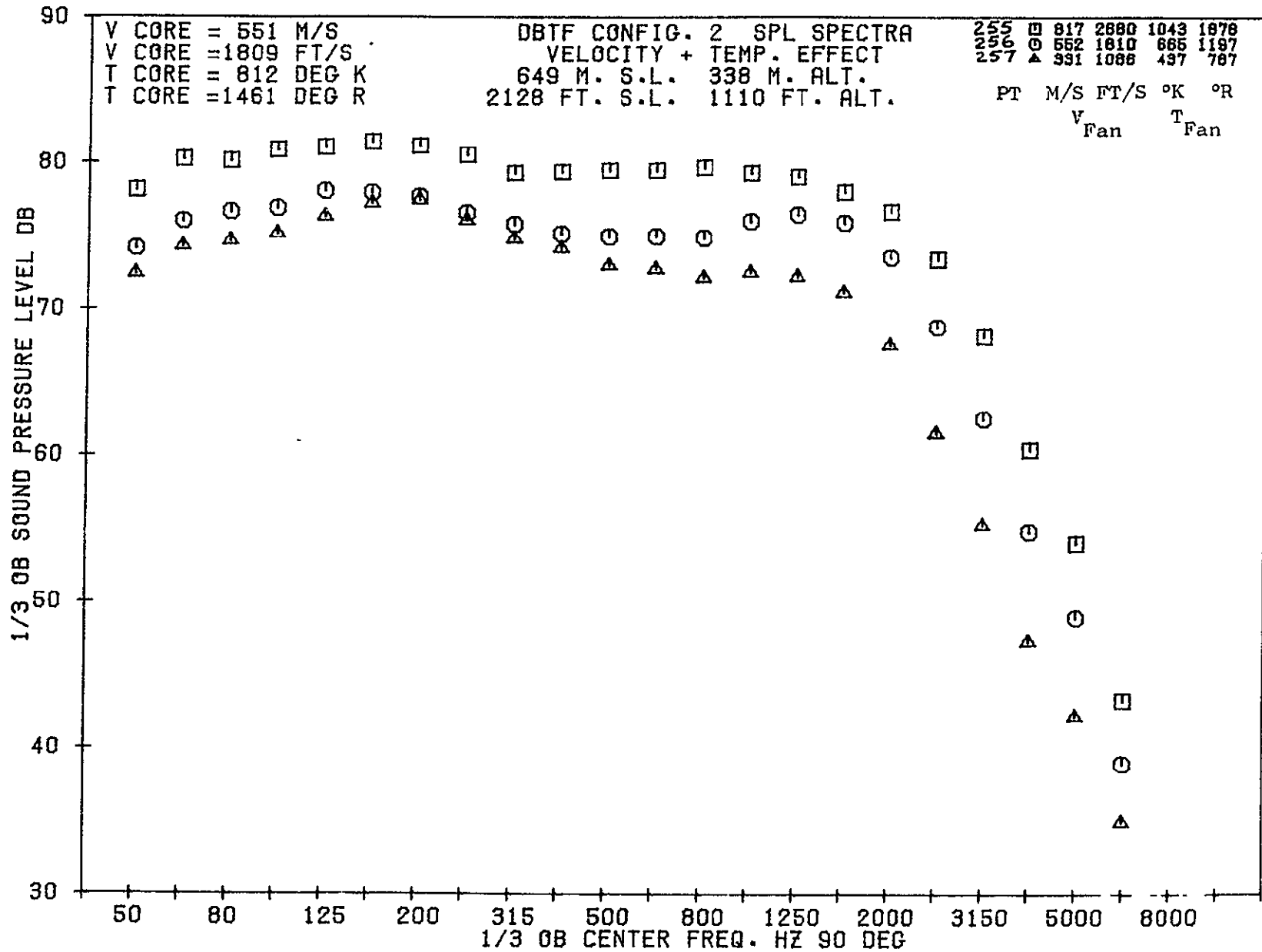


1-157

08/18/75
5R266-001

79 AIRC

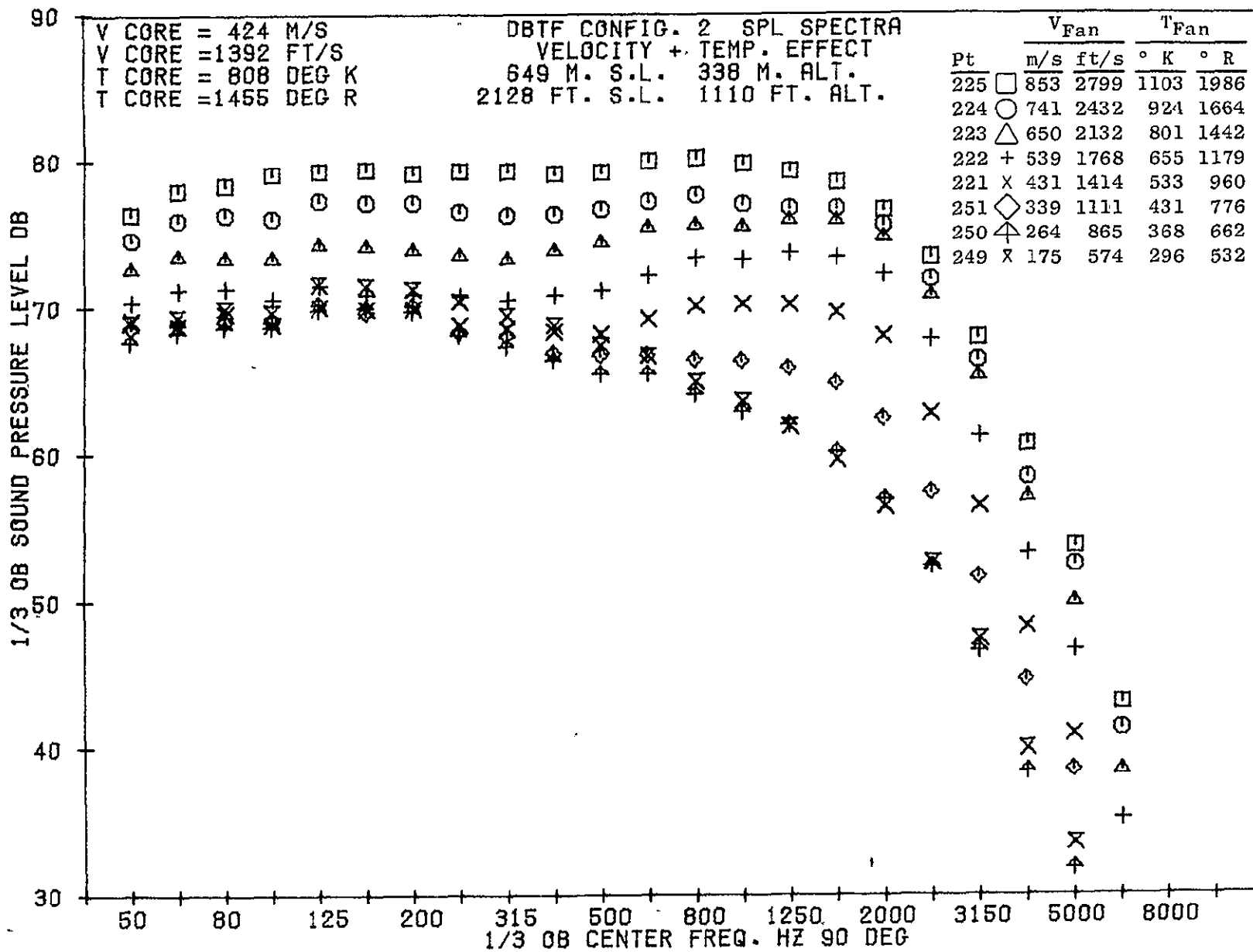
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1158

1392

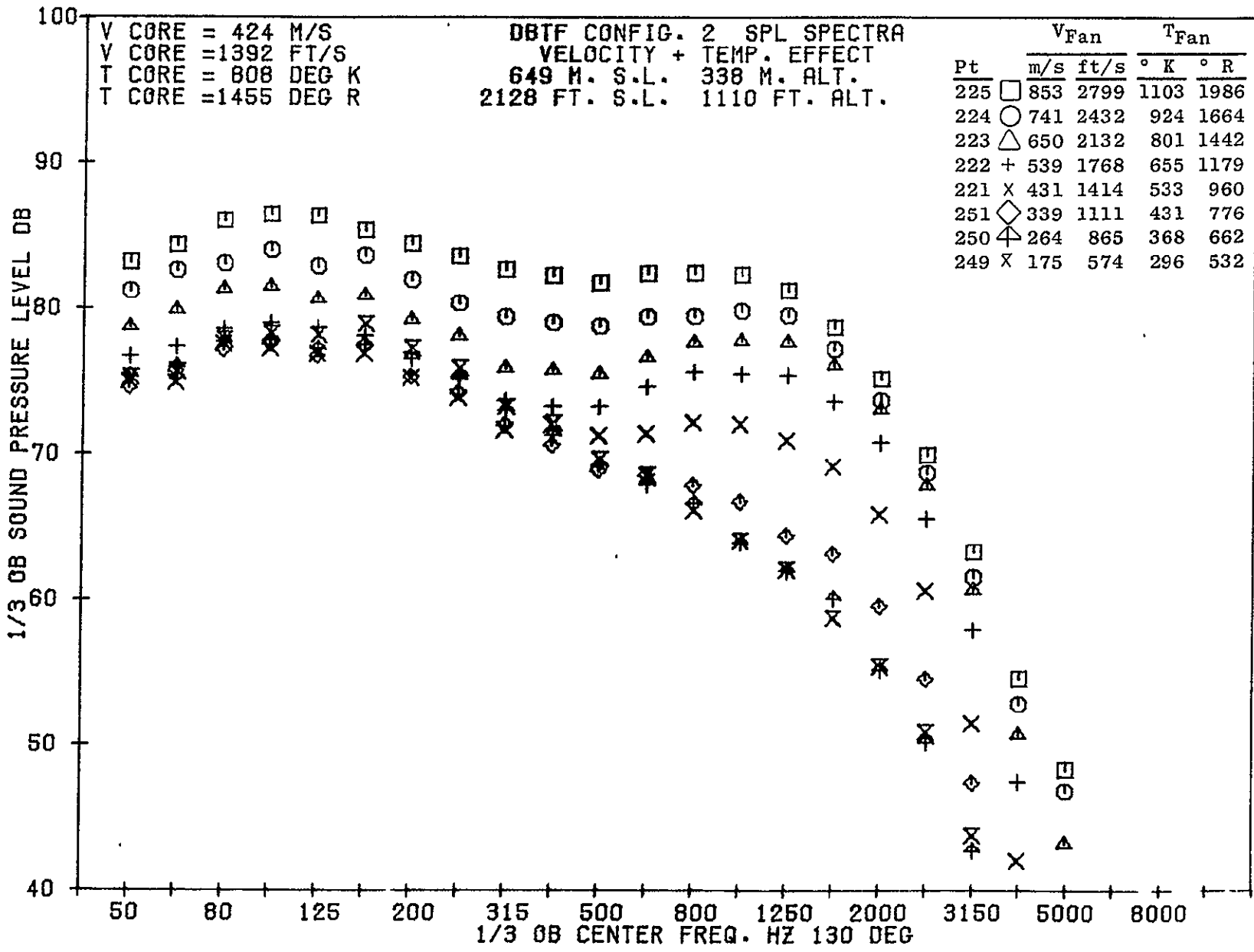


117

08/18/75
5R266-001

79. BURCH

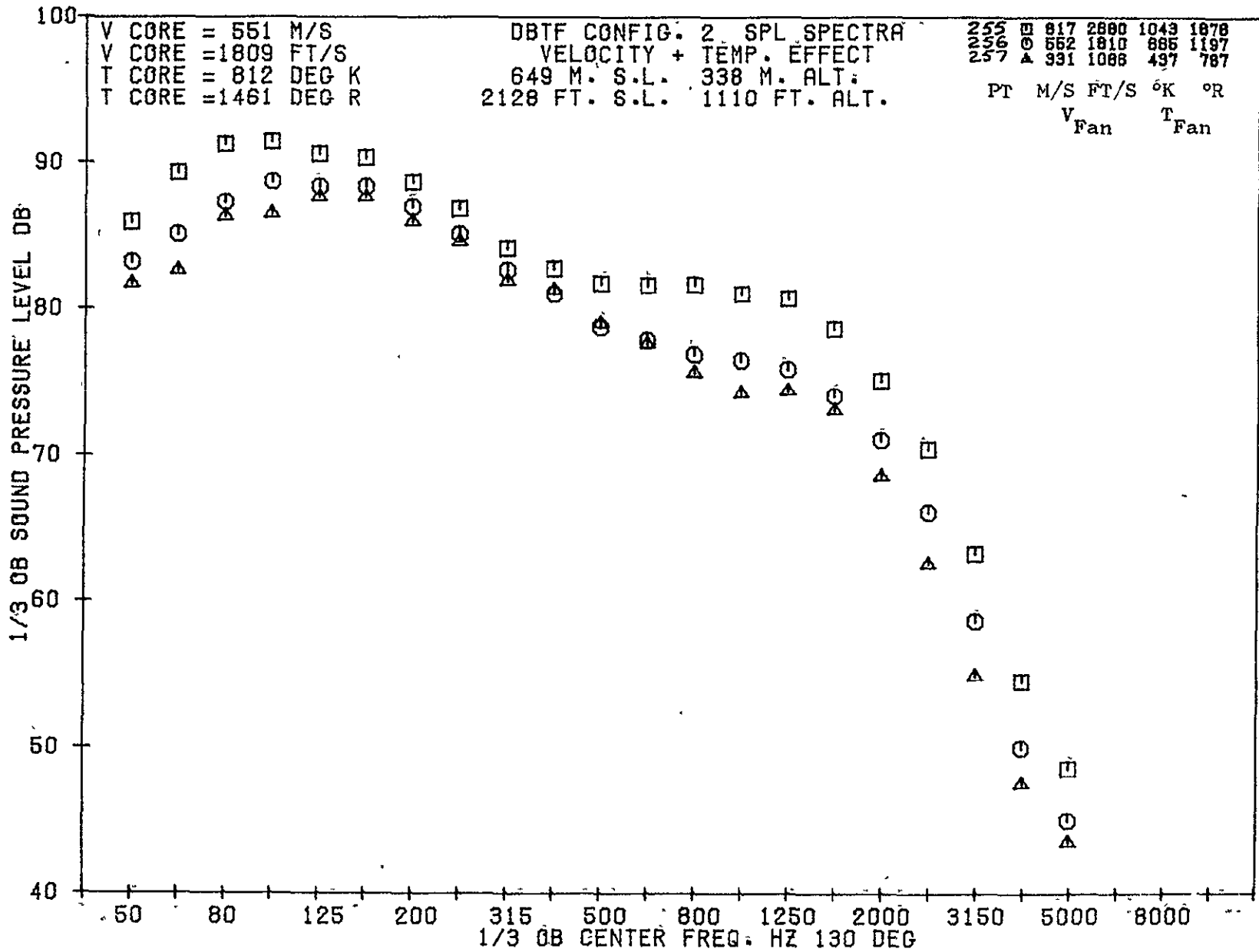
1393



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ALT

1394

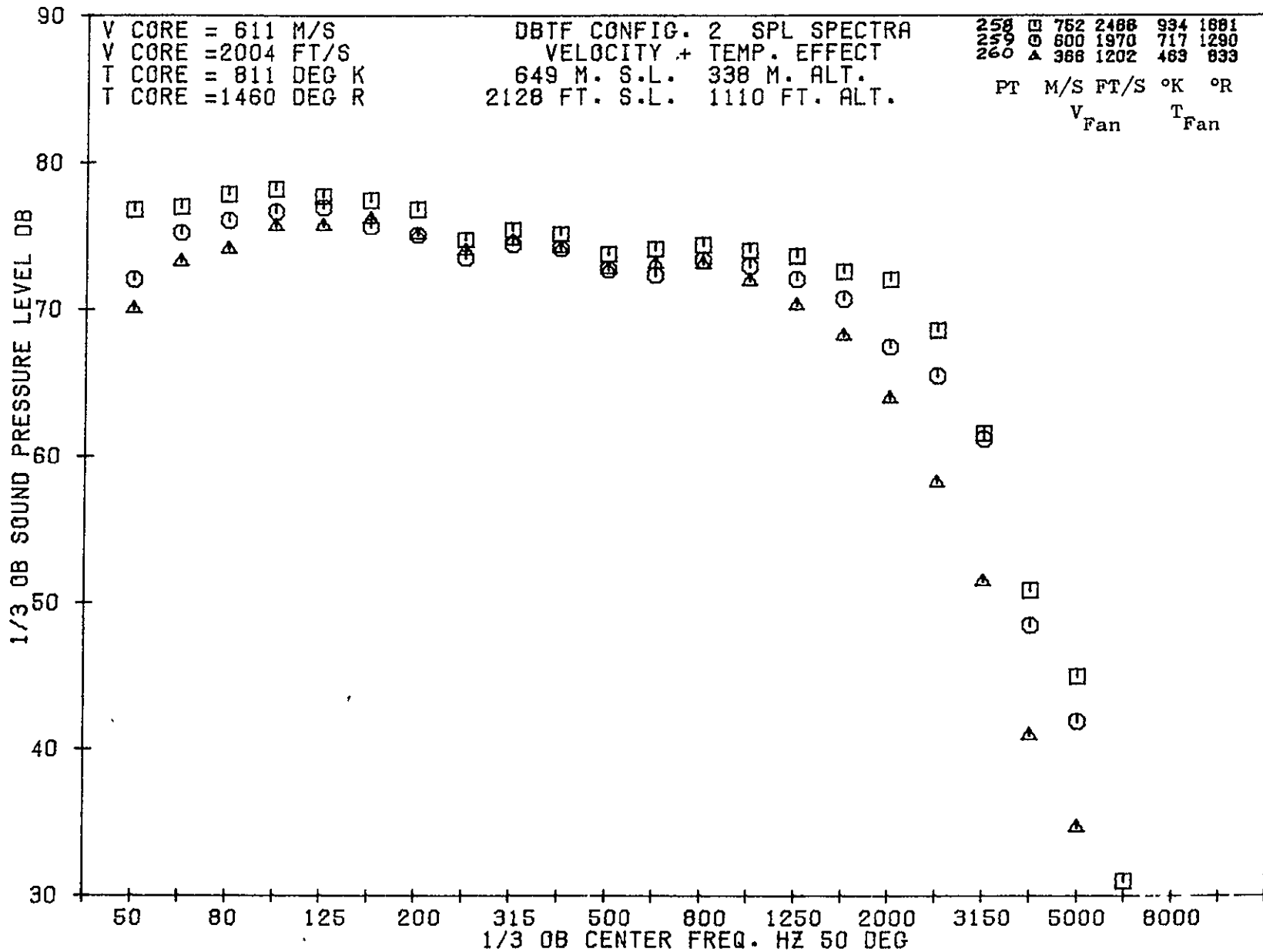


1.1394

08/18/75
5R266-001

79 BURD A.

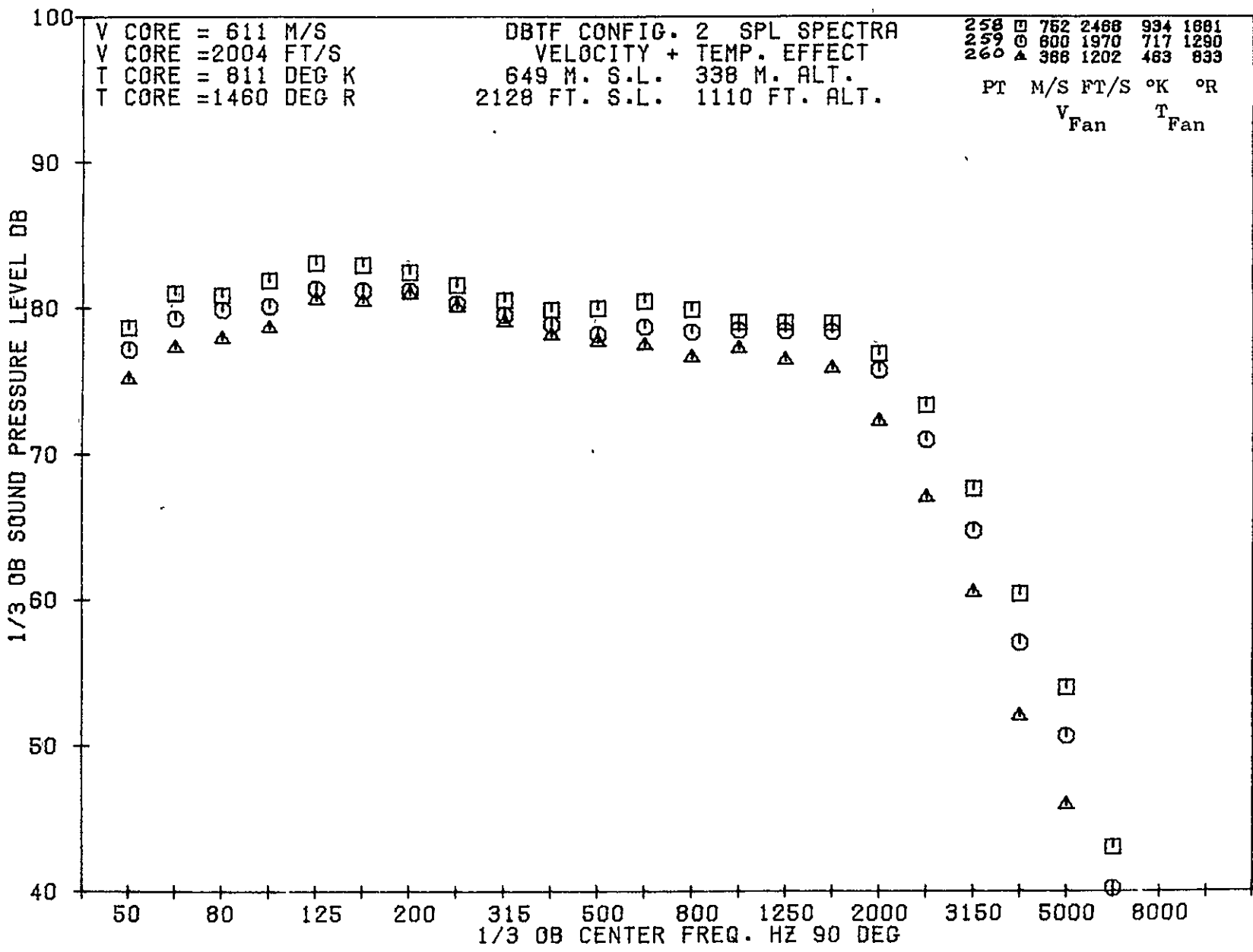
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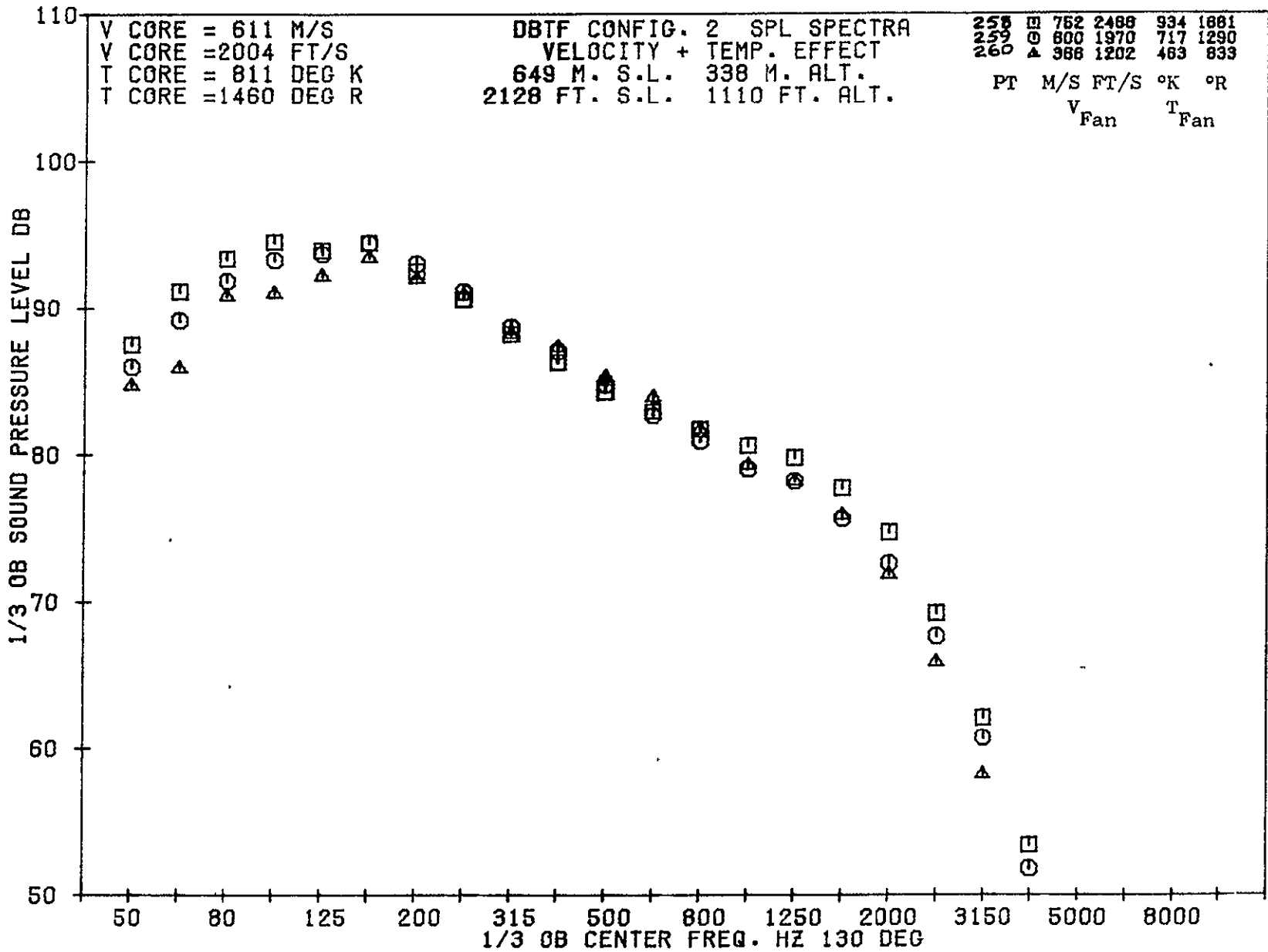
1396



08/13/75
5R032-001

79 BURC

1397



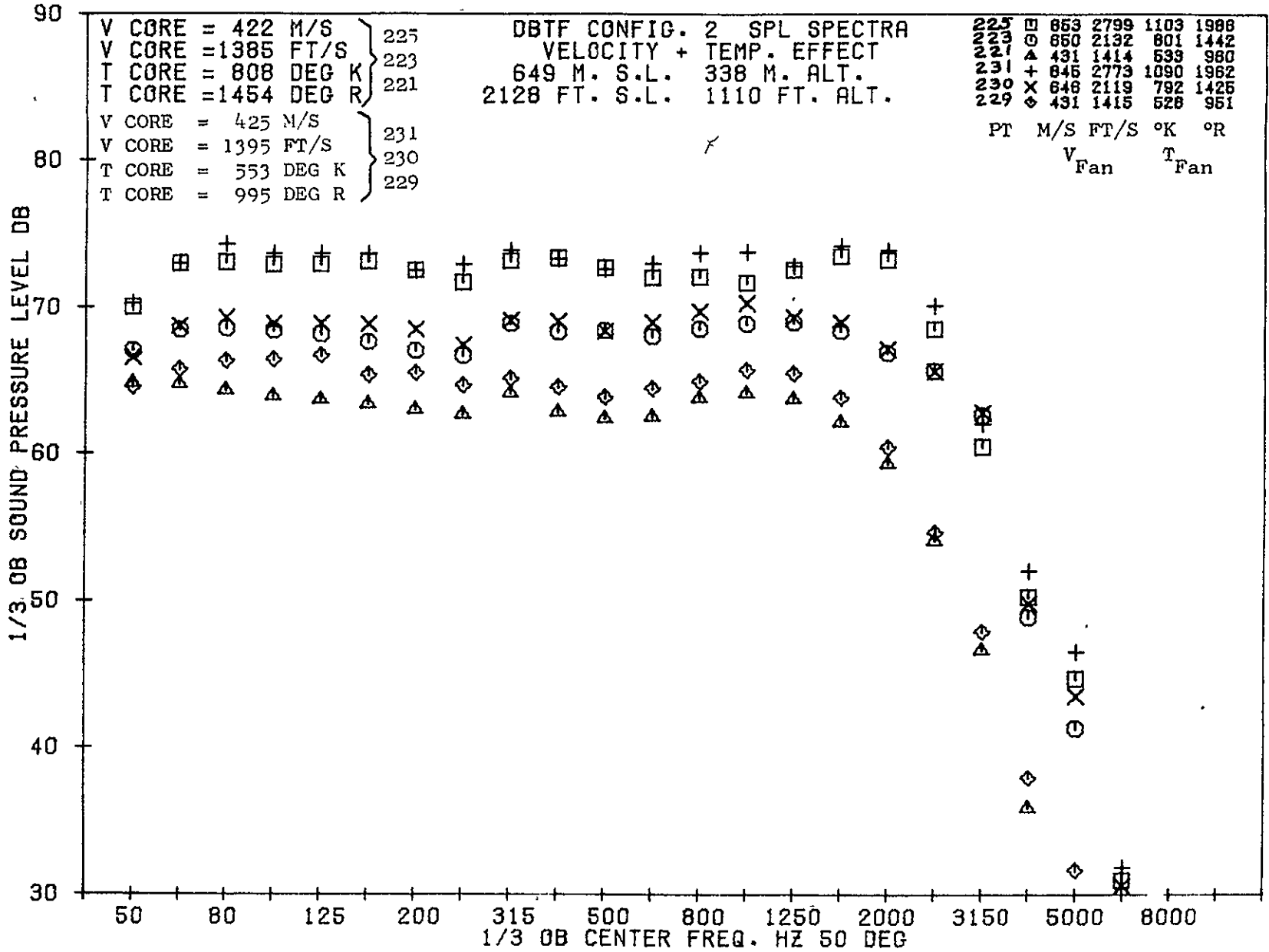
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08/13/75
5R032-001

79 BURCH A.

Handwritten mark

1398

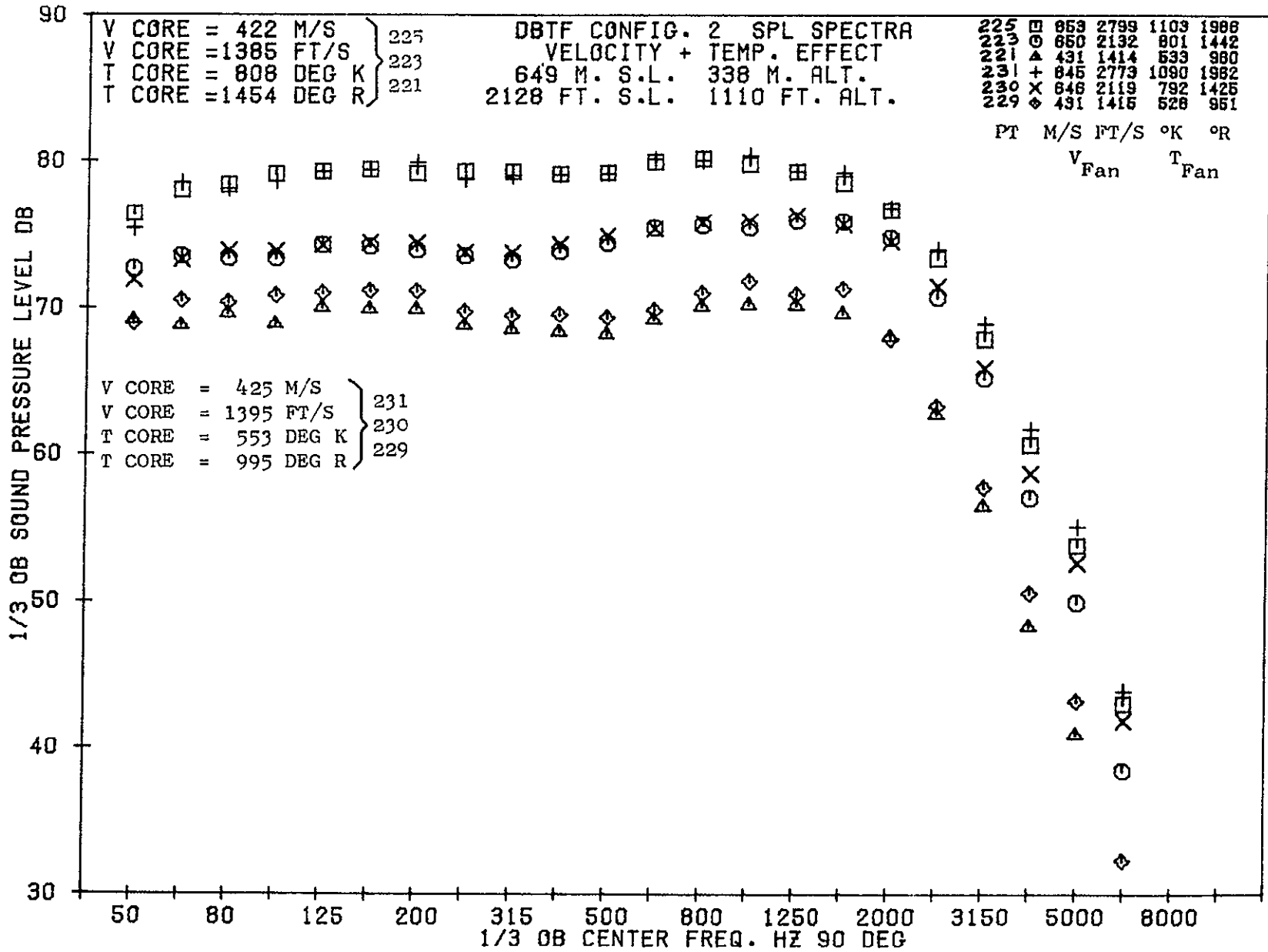


08/13/75
5R032-001

79 BURCOR

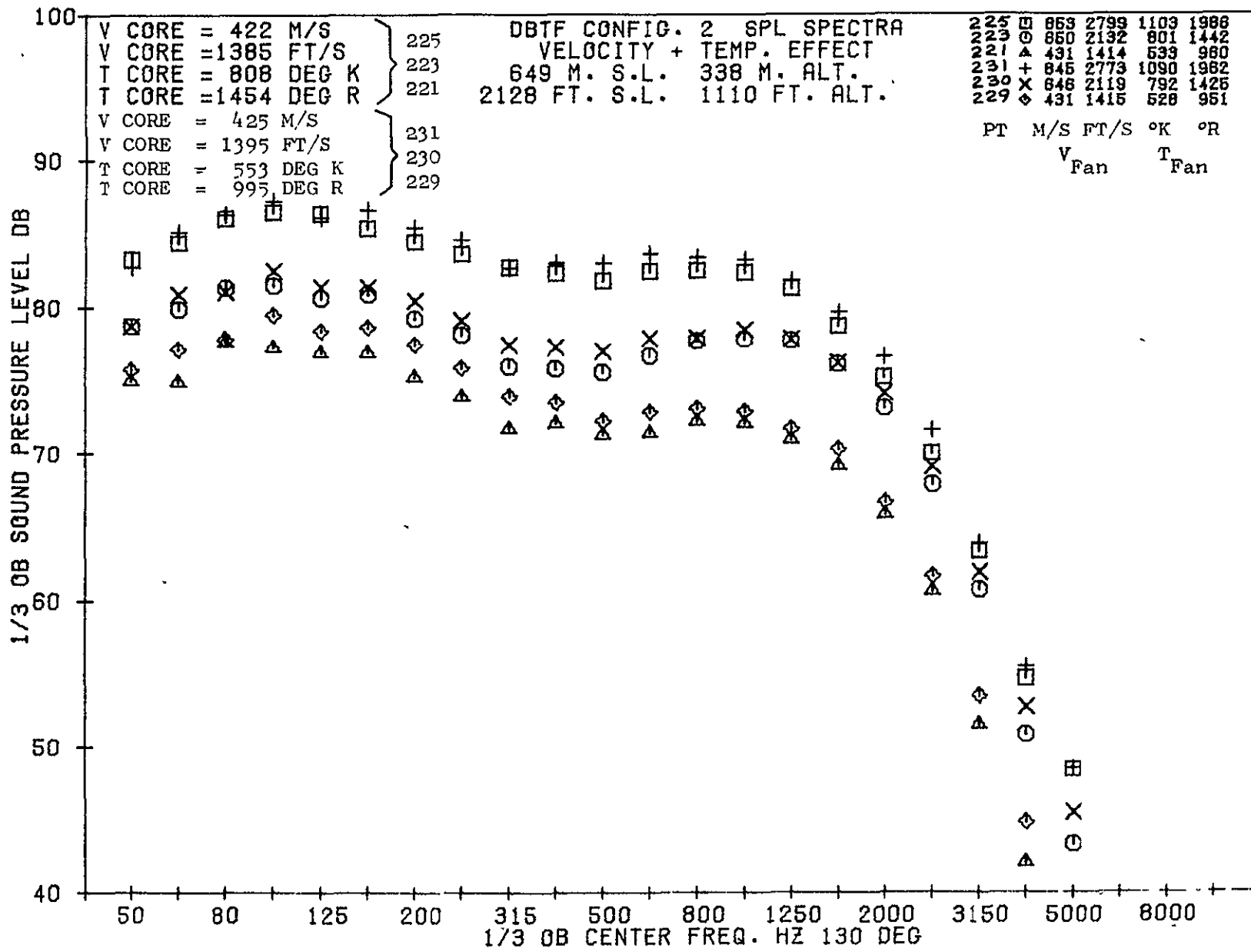
1163

1399



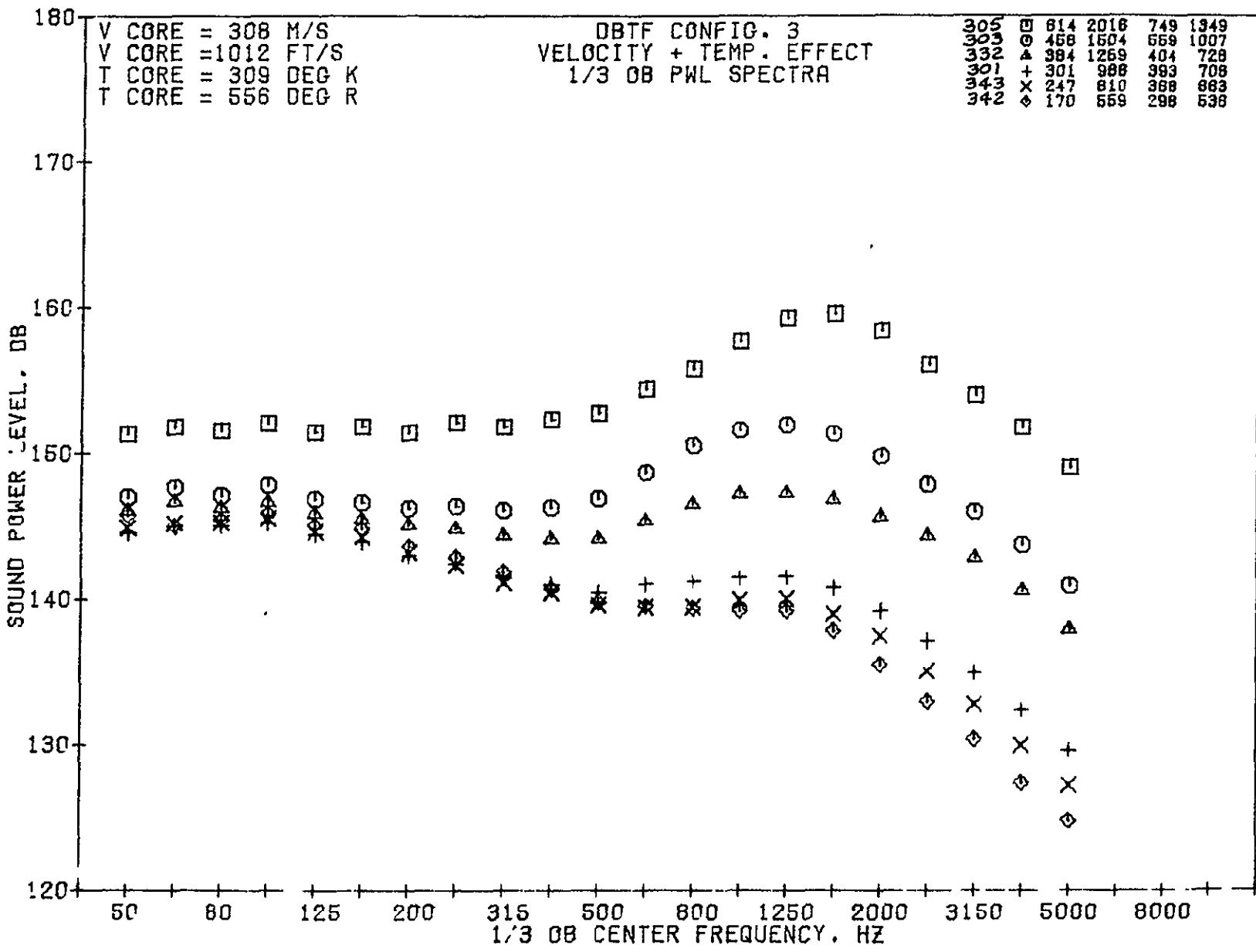
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1400



08/13/75
5R032-001

79 BURCH



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4-11-75

08/13/75
 5R960-001

79 BURCH A.

180
170
160
150
140
130
120

V CORE = 335 M/S
V CORE = 1099 FT/S
T CORE = 429 DEG K
T CORE = 773 DEG R

DBTF CONFIG. 3
VELOCITY + TEMP. EFFECT
1/3 OB PWL SPECTRA

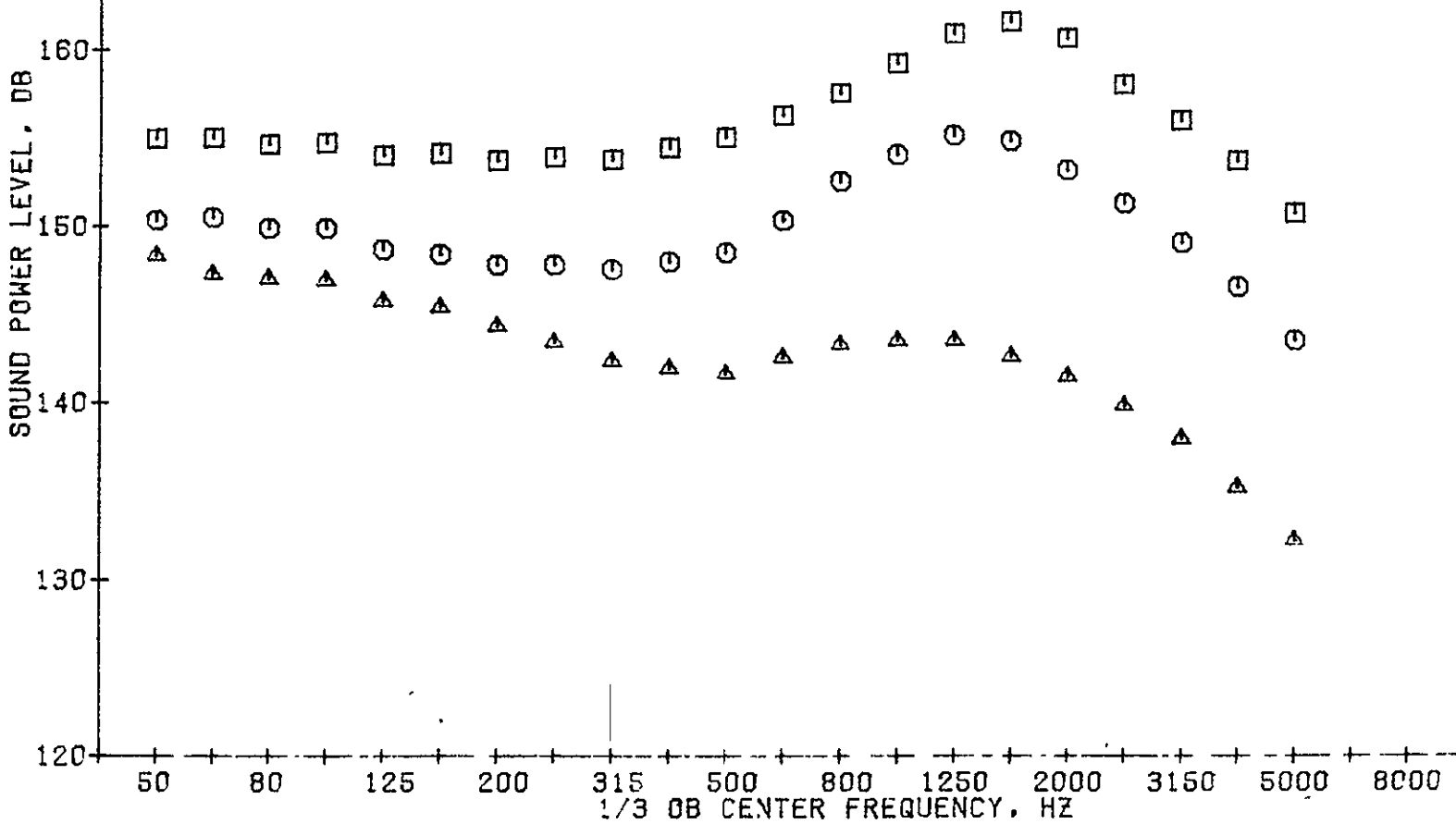
310	□	689	2194	819	1474
306	○	500	1841	598	1077
306	△	331	1067	424	789

PT	M/S	FT/S	°K	°R
	V _{Fan}			T _{Fan}

SOUND POWER LEVEL, DB

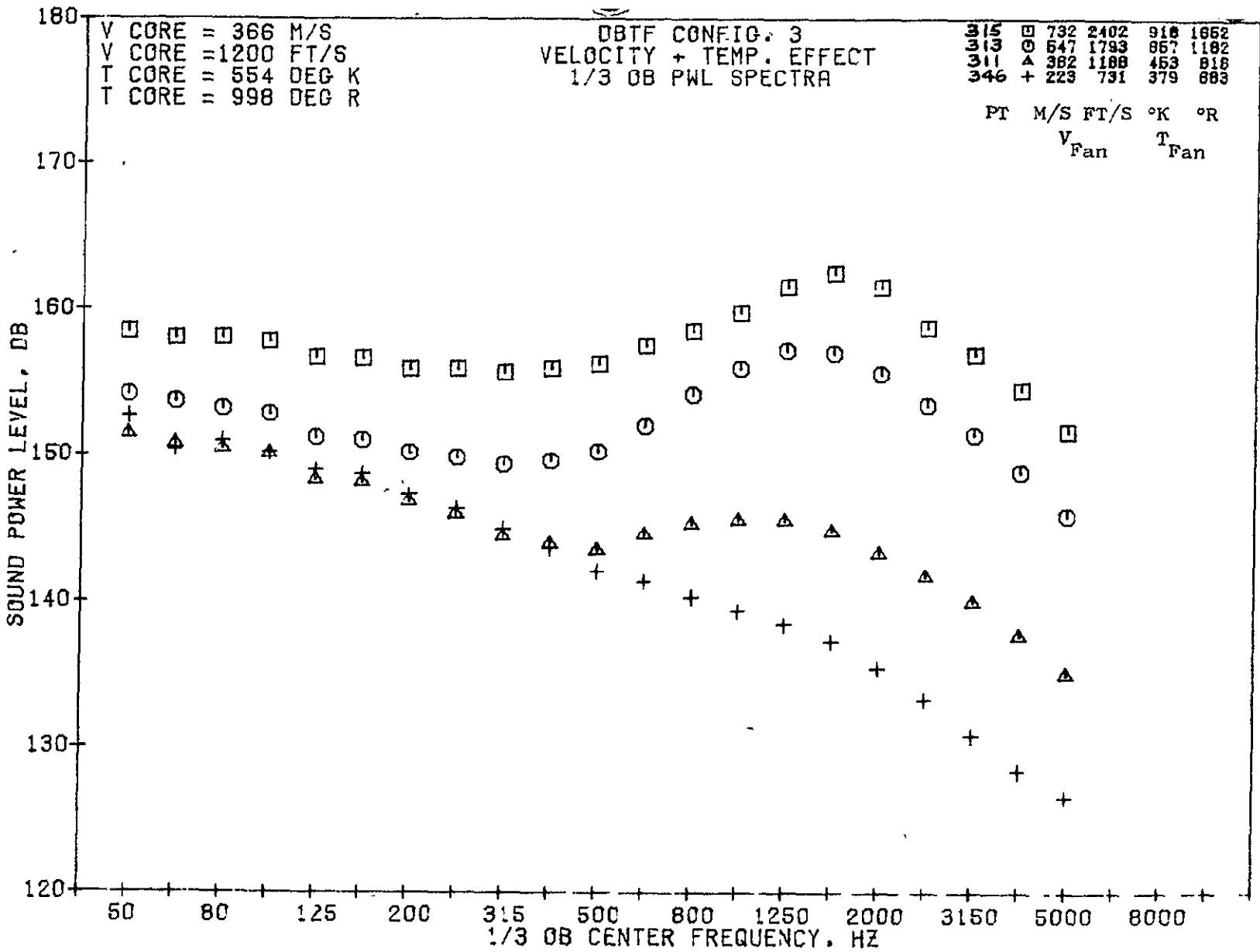
50 80 125 200 315 500 800 1250 2000 3150 5000 8000
1/3 OB CENTER FREQUENCY, HZ

1402



08/13/75
5R960-001

79 BURCH 9.

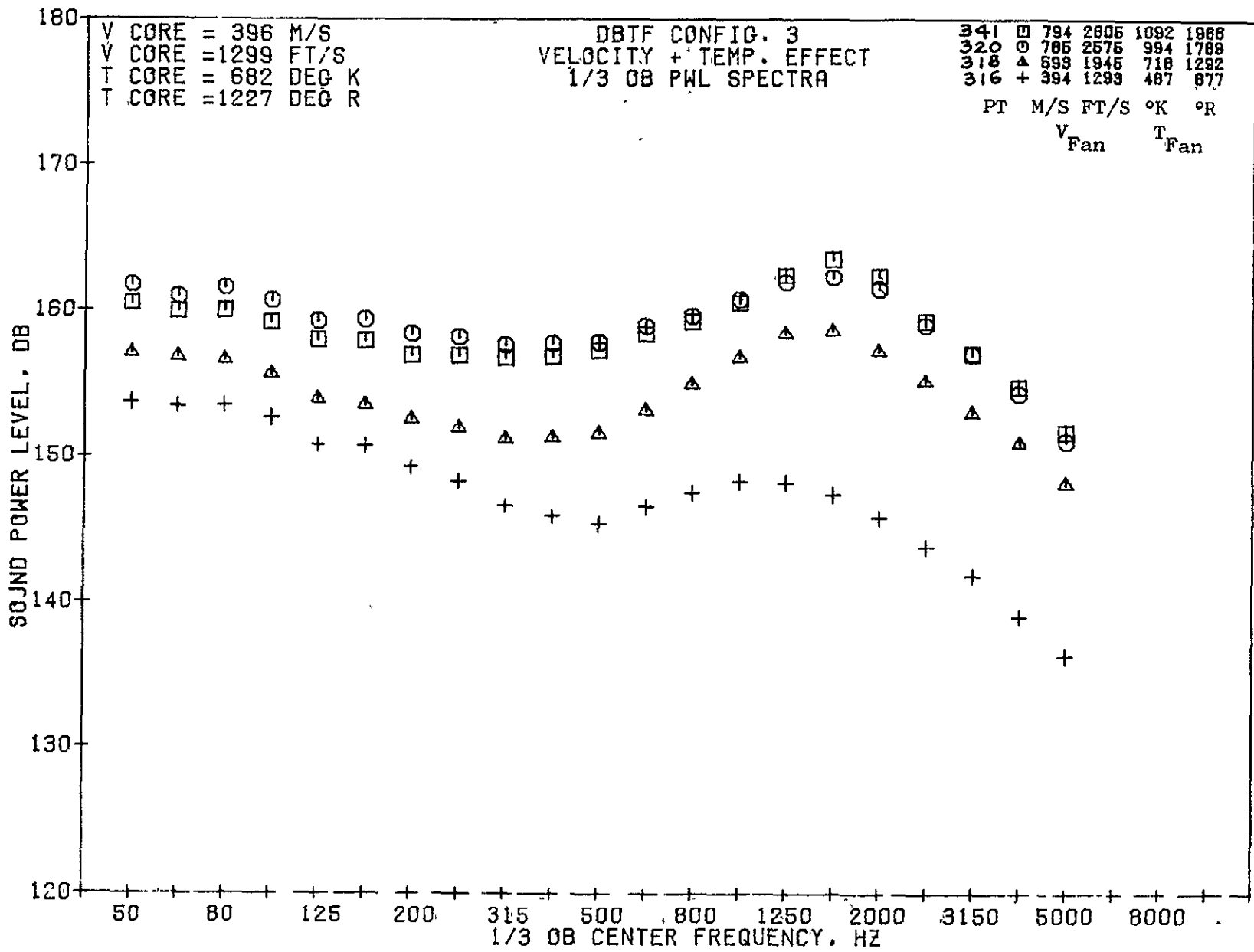


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891-1

08/13/75
 5R960-001

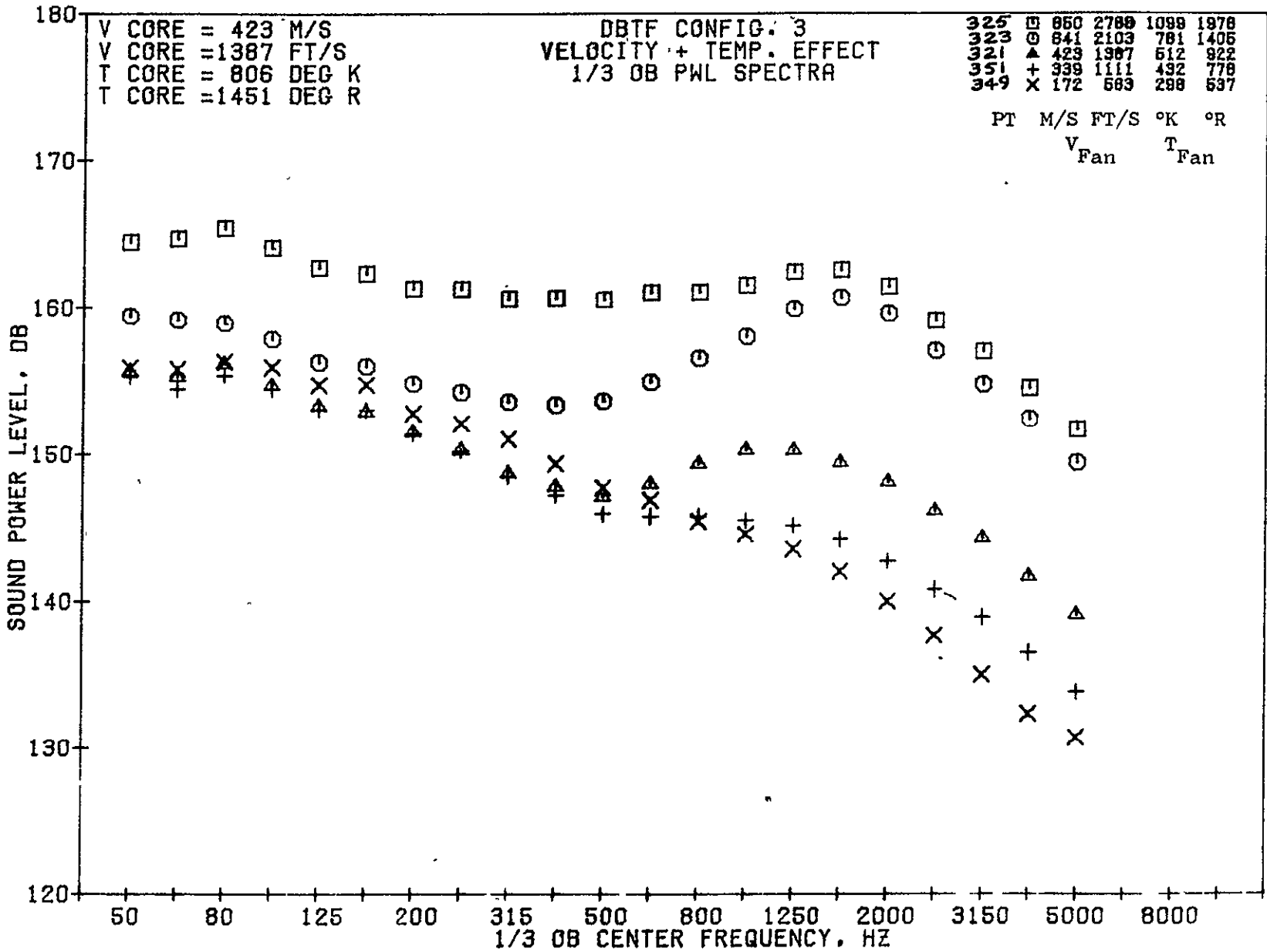
79 BURCH A.



4-1-75

08/13/75
5R960-001

79 BUR A.



1405

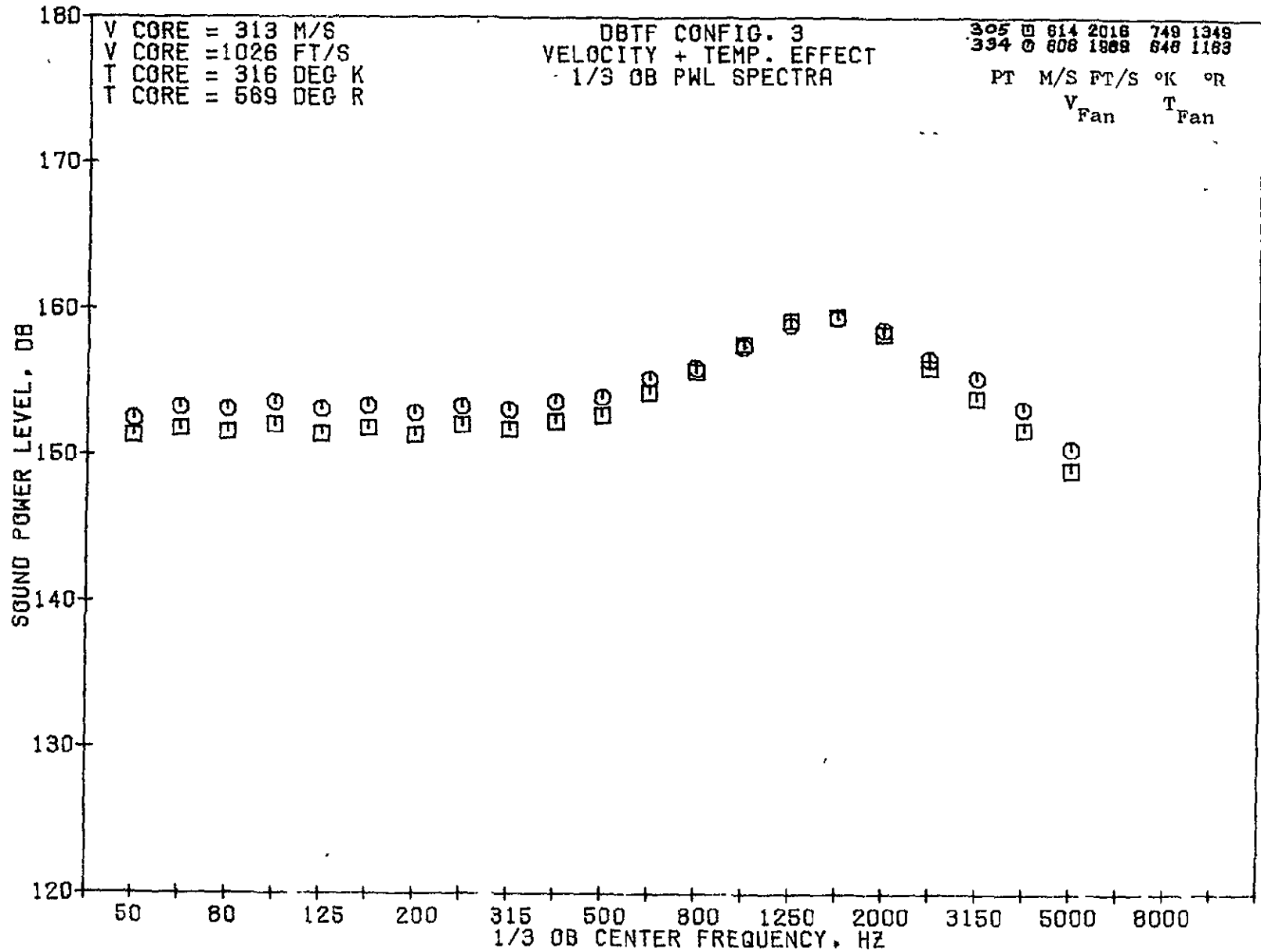
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0677

08/13/75
5R960-001

79 BURCH A.

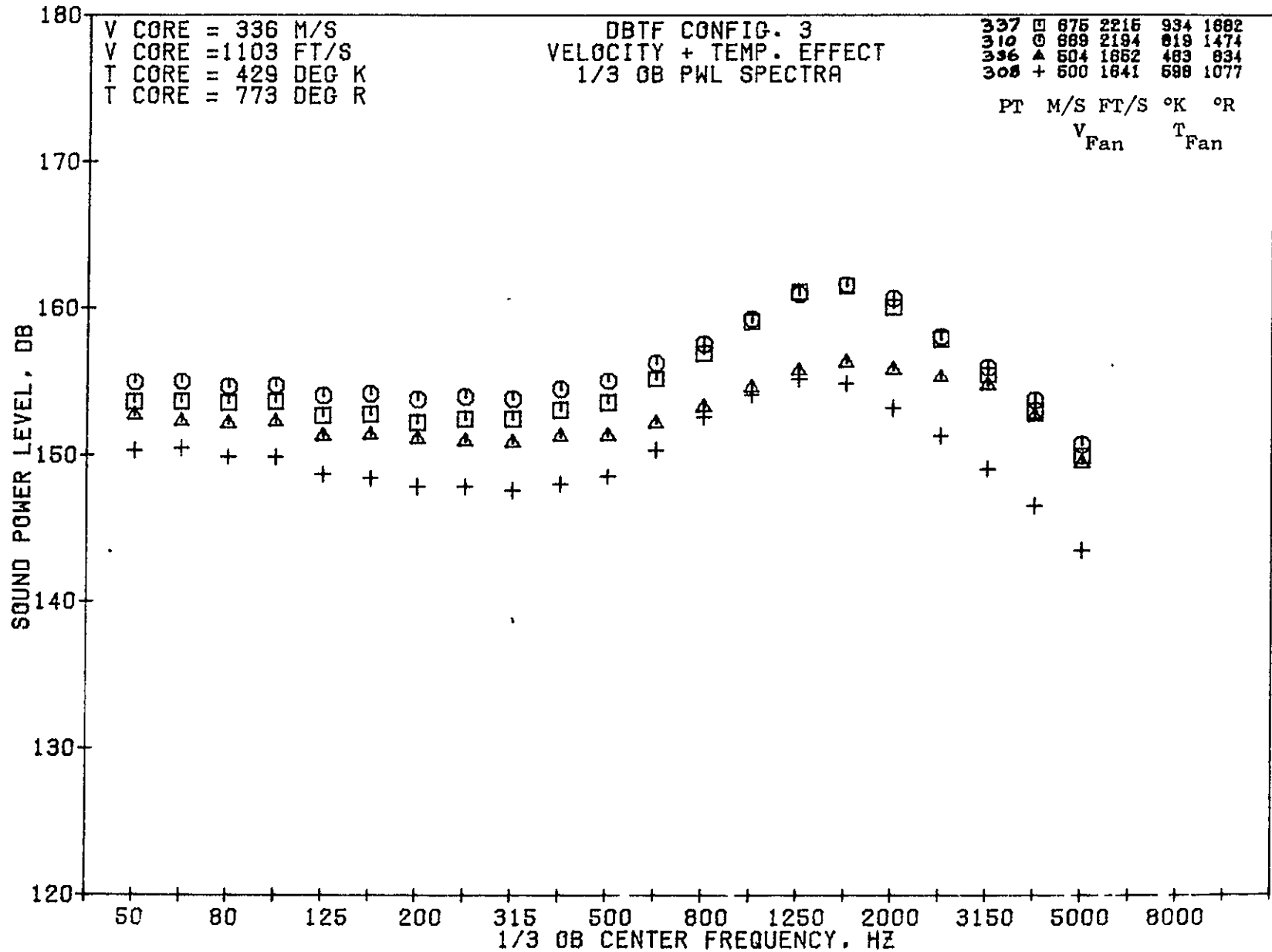
1406



161

08/13/75
5R960-001

79 BURCH A.

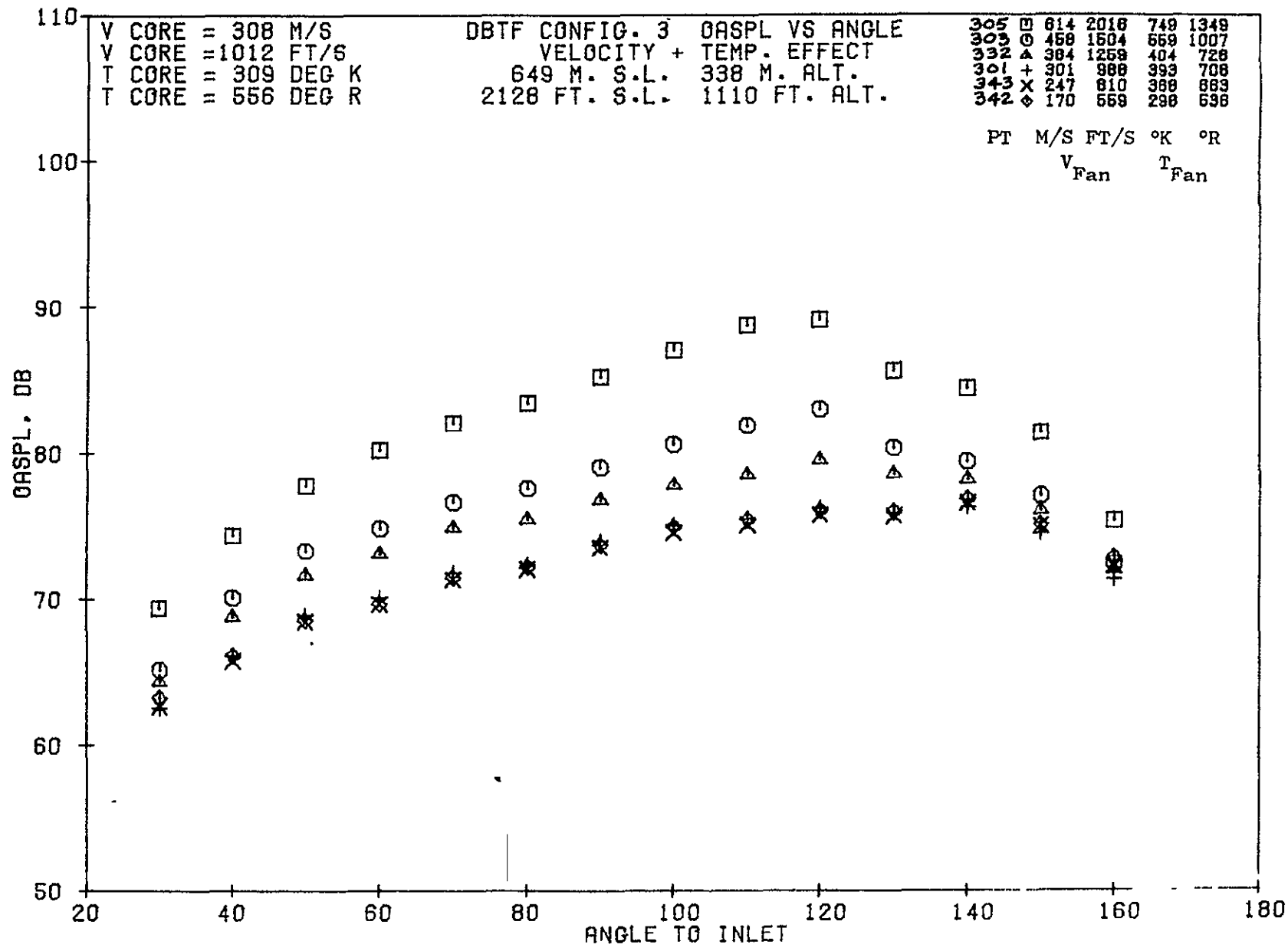


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1407

08/13/75
5R960-001

79 BURCH A.



1408

1173

08/13/75
 5R960-001

79 BURCH

110

V CORE = 335 M/S
V CORE = 1099 FT/S
T CORE = 429 DEG K
T CORE = 773 DEG R

DBTF CONFIG. 3 OASPL VS ANGLE
VELOCITY + TEMP. EFFECT
649 M. S.L. 338 M. ALT.
2128 FT. S.L. 1110 FT. ALT.

310	□	889	2184	819	1474
308	○	600	1841	598	1077
306	△	331	1087	424	789
PT		M/S	FT/S	°K	°R
		V _{Fan}	T _{Fan}		

100

90

80

70

60

50

OASPL, DB

20

40

60

80

100

120

140

160

180

ANGLE TO INLET

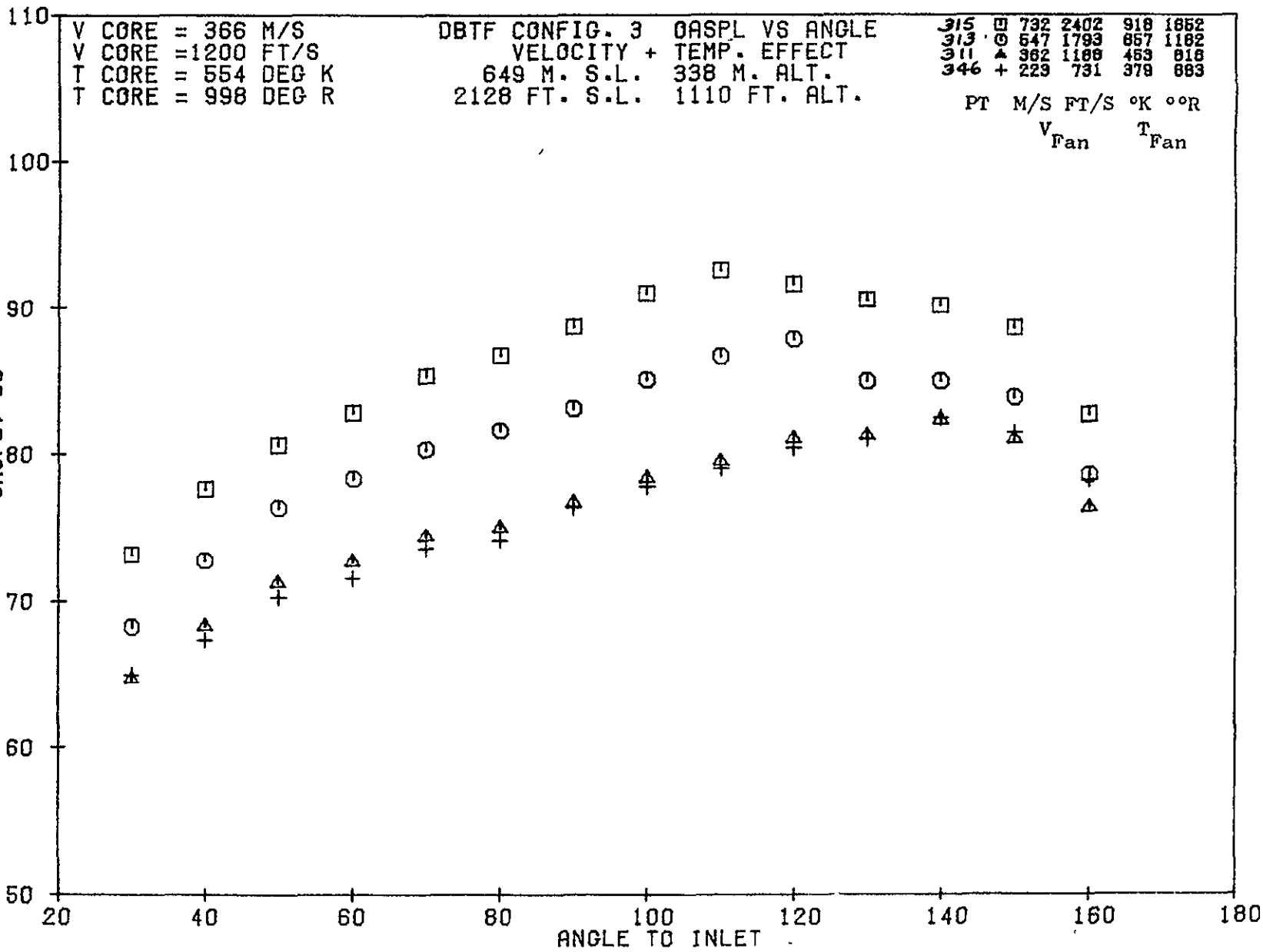
1409

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08/13/75
5R960-001

79 BURCH A.

Handwritten marks



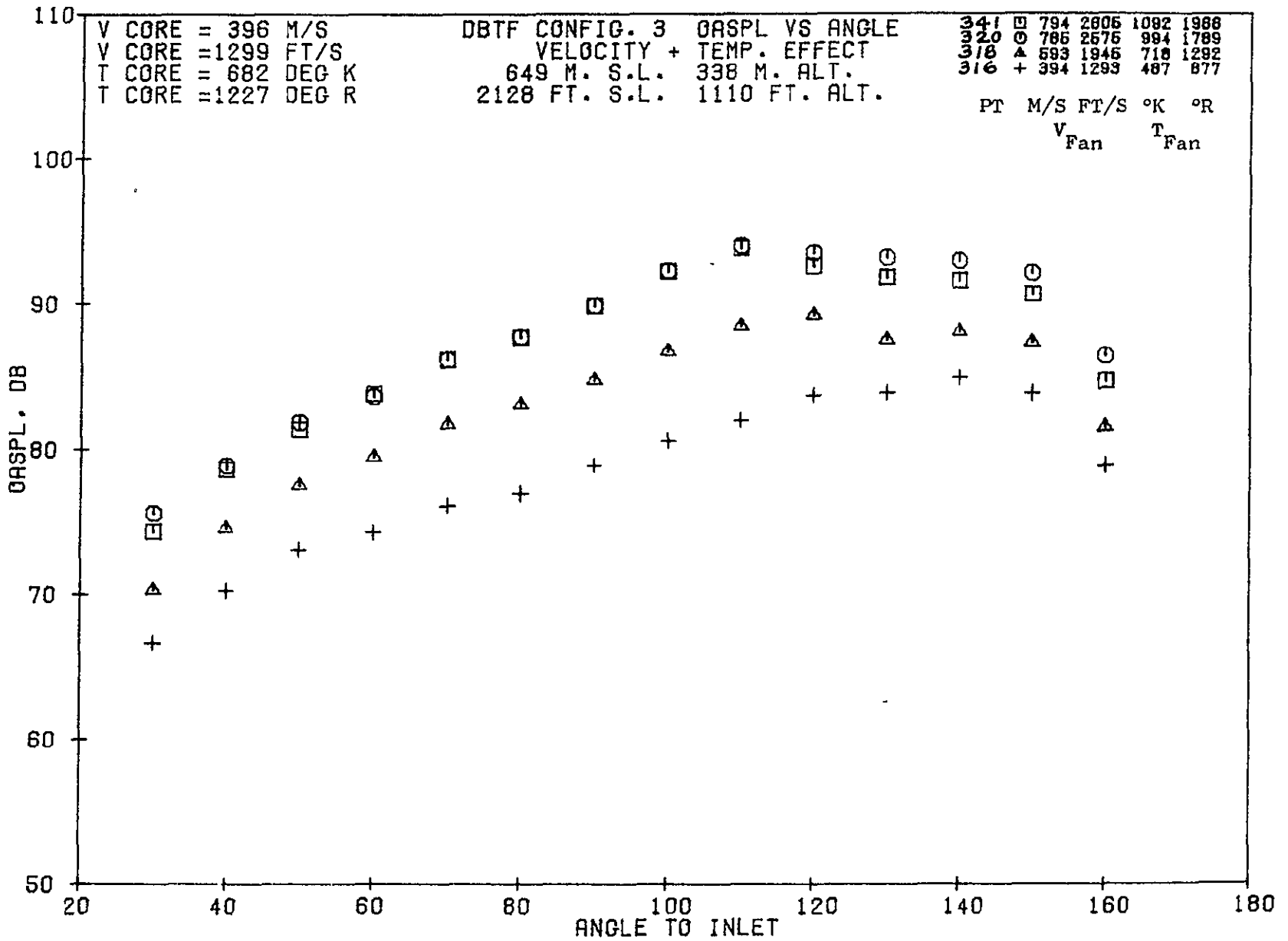
1410

4-175

08/13/75
 5R960-001

79 BURCH

1411



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9/1/75

08/13/75
5R960-001

79 BURCH A.

110
100
90
80
70
60
50

V CORE = 423 M/S
V CORE = 1387 FT/S
T CORE = 806 DEG K
T CORE = 1451 DEG R

DBTF CONFIG. 3 OASPL VS ANGLE
VELOCITY + TEMP. EFFECT
649 M. S.L. 338 M. ALT.
2128 FT. S.L. 1110 FT. ALT.

325	□	860	2788	1099	1978
323	○	841	2103	781	1406
321	△	423	1987	612	922
351	+	399	1111	432	778
349	X	172	563	298	537

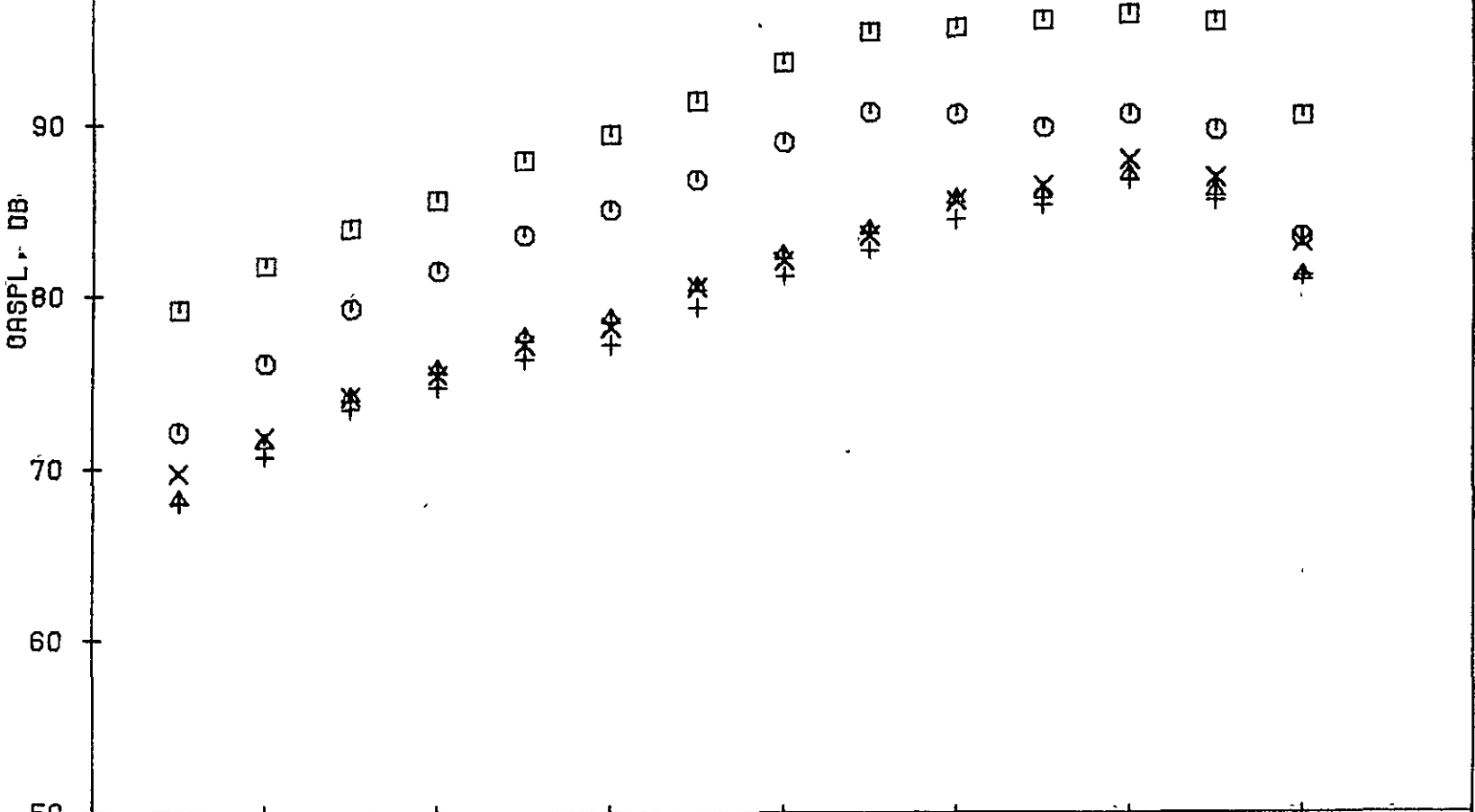
PT M/S FT/S °K °R
V Fan T Fan

OASPL - DB

ANGLE TO INLET

1412

20 40 60 80 100 120 140 160 180

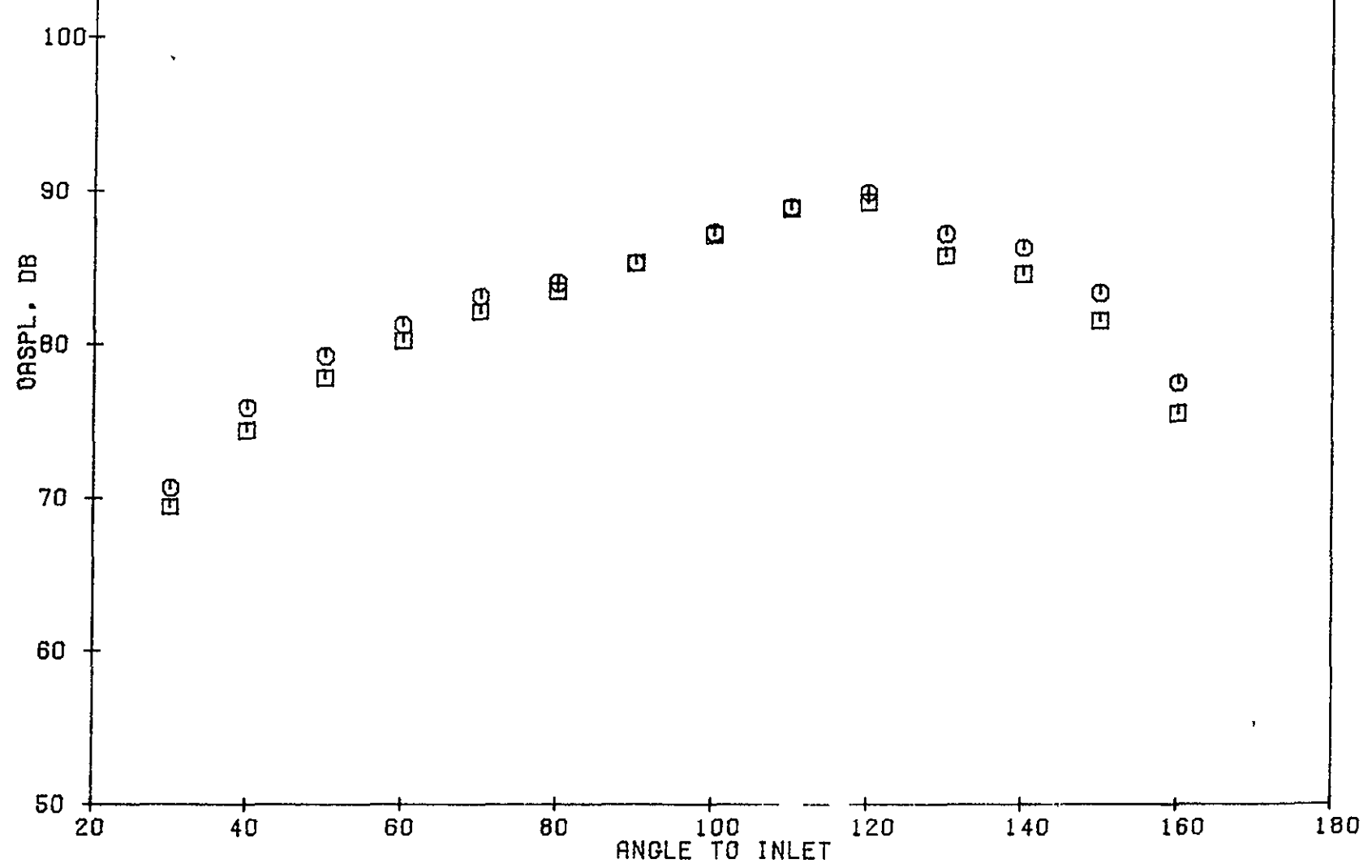


141

08/13/75
5R960-001

79 BURD

V CORE = 313 M/S DBTF CONFIG. 3 GASPL VS ANGLE 305 □ 814 2018 748 1349
 V CORE = 1026 FT/S VELOCITY + TEMP. EFFECT 334 ○ 808 1989 648 1163
 T CORE = 316 DEG K 649 M. S.L. 338 M. ALT. PT M/S FT/S °K °R
 T CORE = 569 DEG R 2128 FT. S.L. 1110 FT. ALT. V_{Fan} T_{Fan}



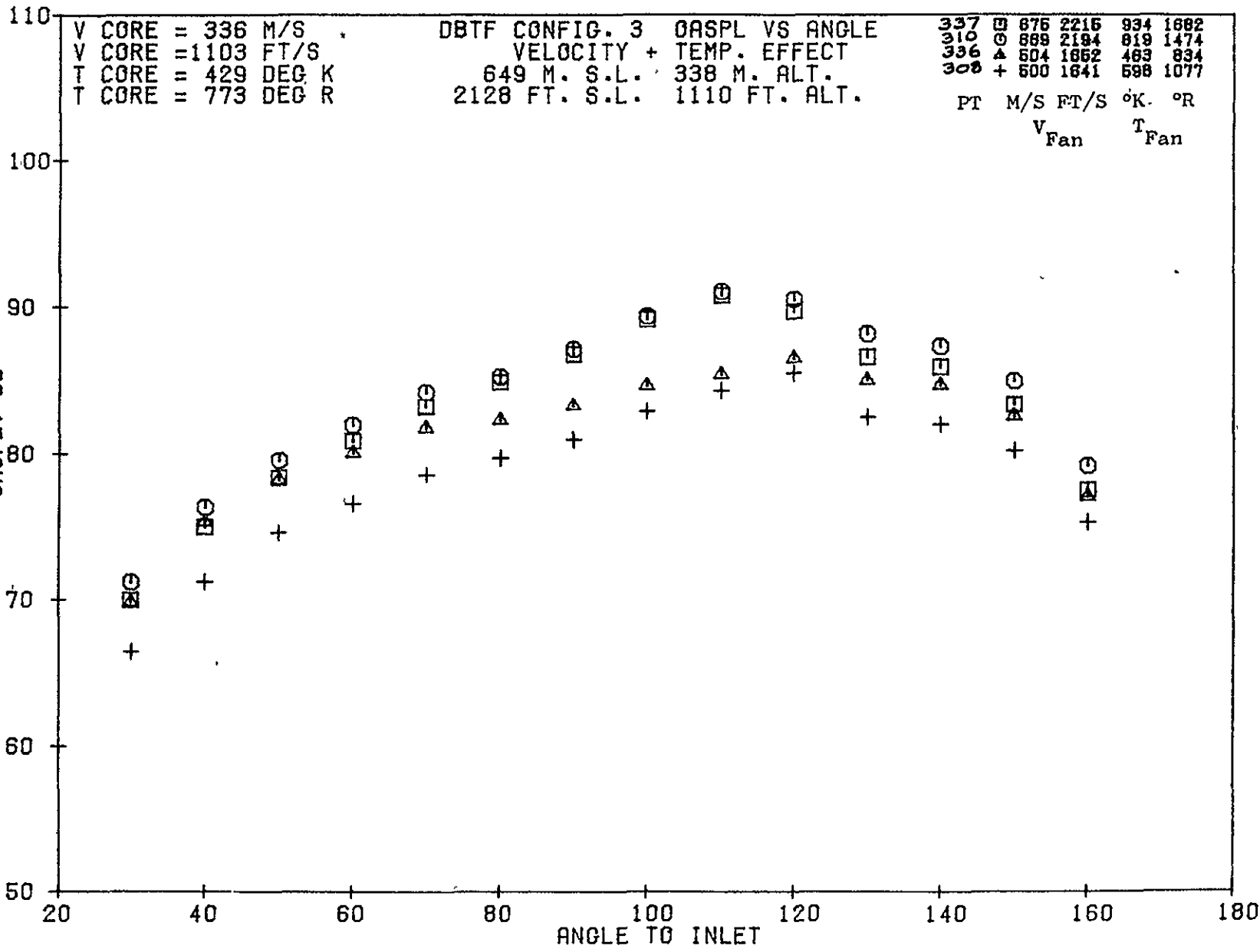
1413

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41-16

08/13/75
5R960-001

79 BURCH A.

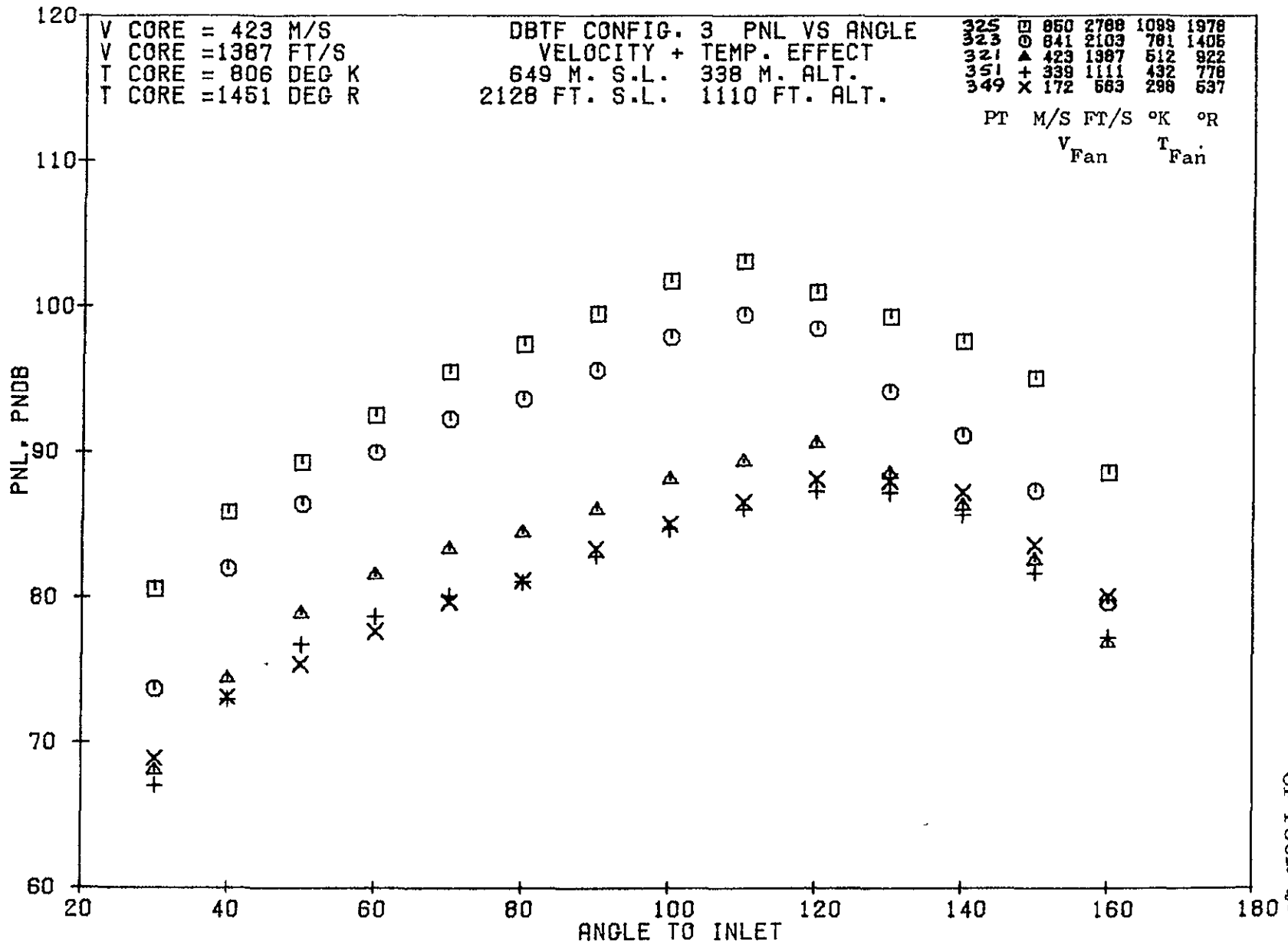


1414

1414

08/13/75
6R960-001

79 BURCH



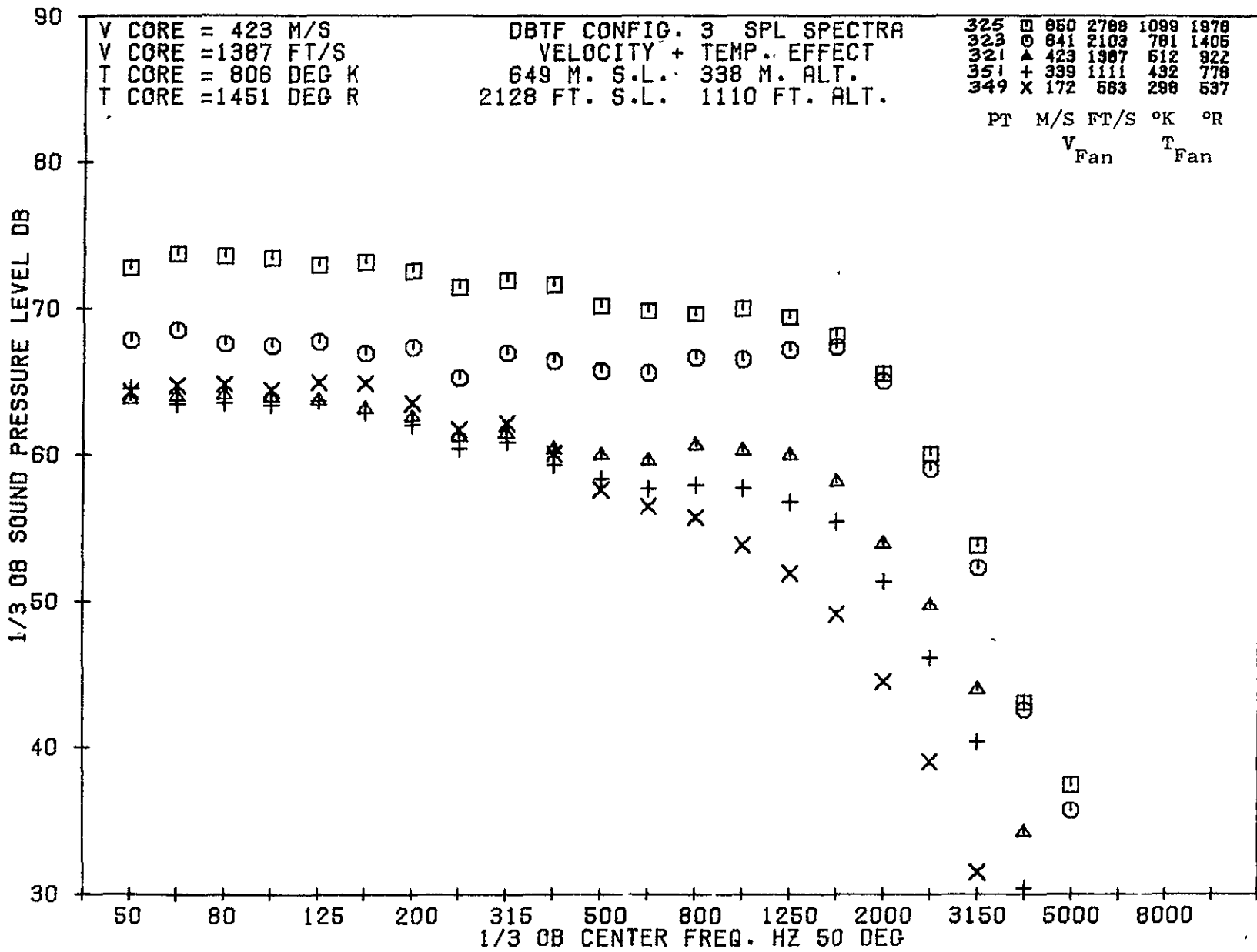
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08/13/75
5R960-001

79 BURCH A.

4180

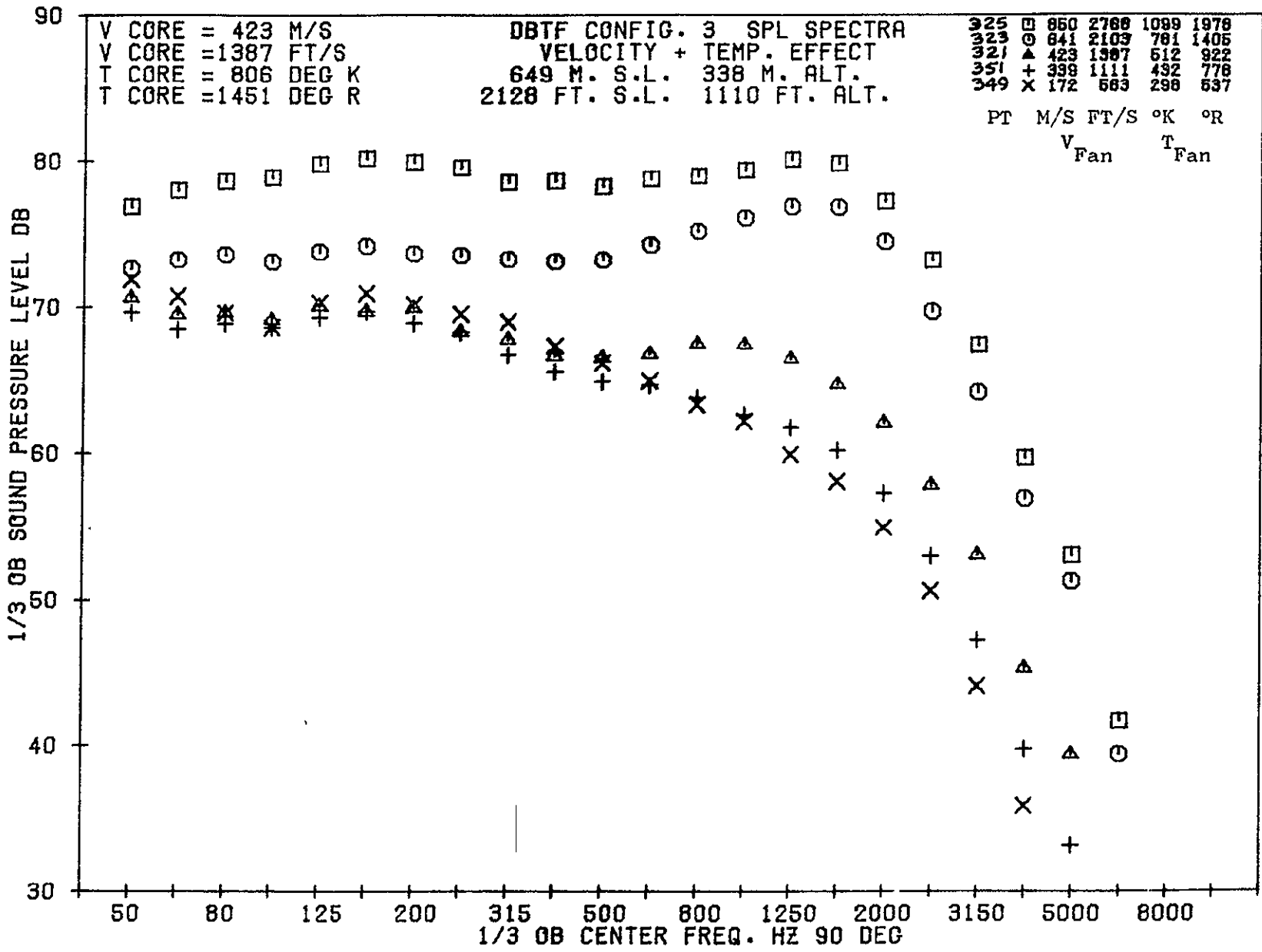
1416



PT

08/13/75
5R960-001

79 BURCH A.



1417

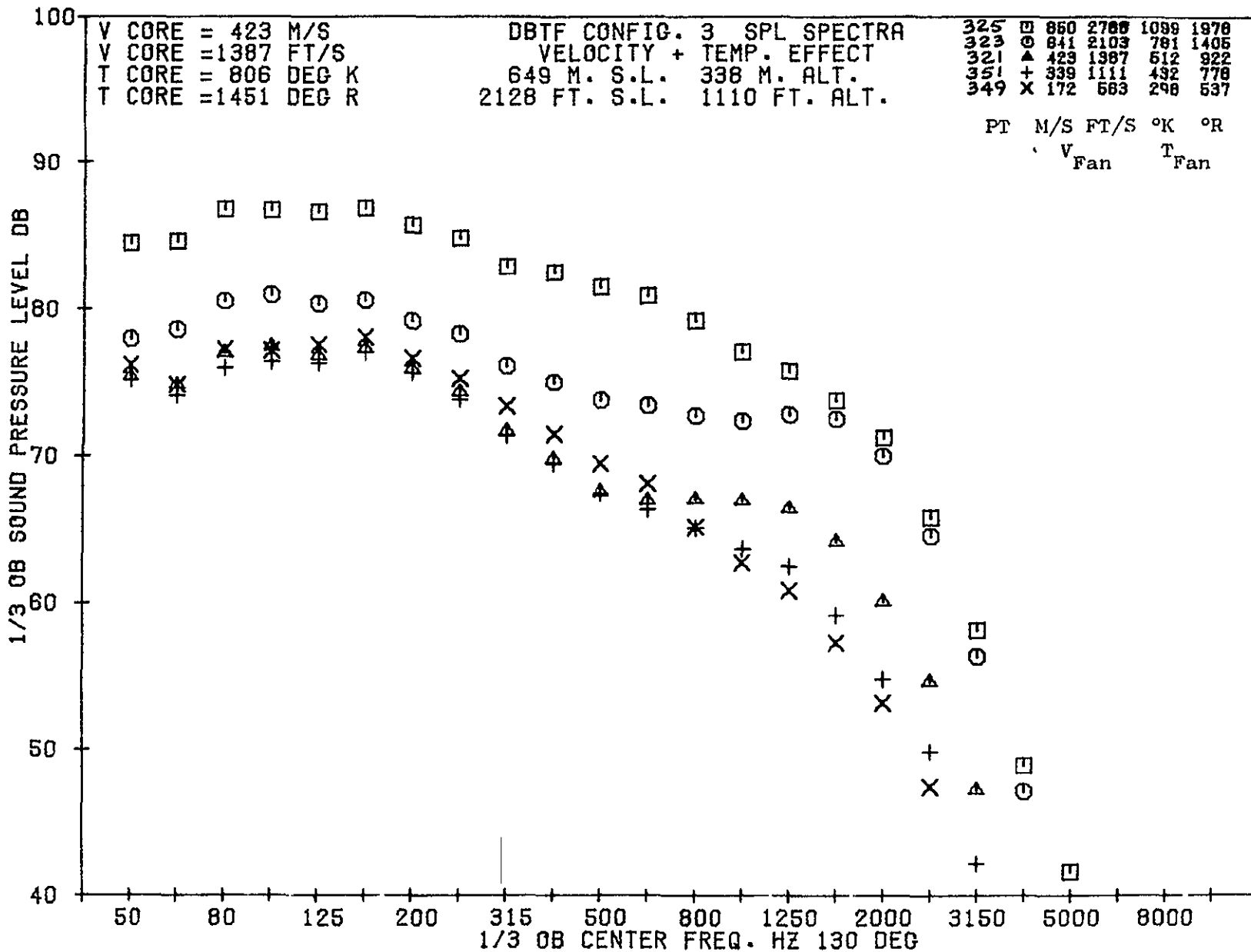
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4-181

08/13/75
5R960-001

79 BURCH A.

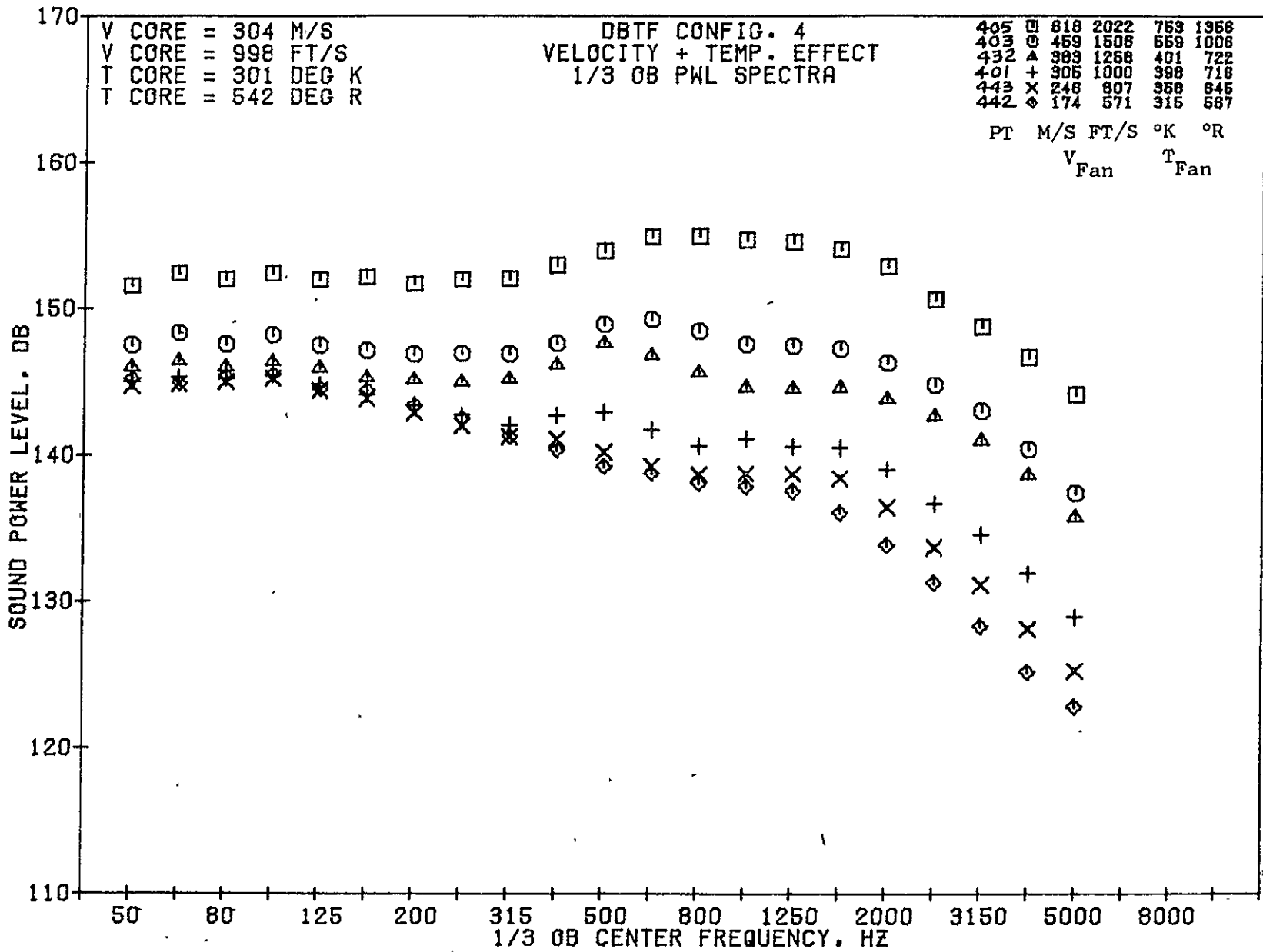
1418



11/63

08/13/75
5R960-001

79 BURCH A.



1419

08/13/75
5R959-001

79 BURCH A.

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170

V CORE = 336 M/S
V CORE = 1101 FT/S
T CORE = 431 DEG K
T CORE = 775 DEG R

DBTF CONFIG. 4
VELOCITY + TEMP. EFFECT
1/3 OB PWL SPECTRA

410	□	888	2191	817	1471
408	○	504	1653	804	1088
406	▲	336	1102	430	774
PT		M/S	FT/S	°K	°R
		V _{Fan}	T _{Fan}		

160

150

140

130

120

110

SOUND POWER LEVEL, DB

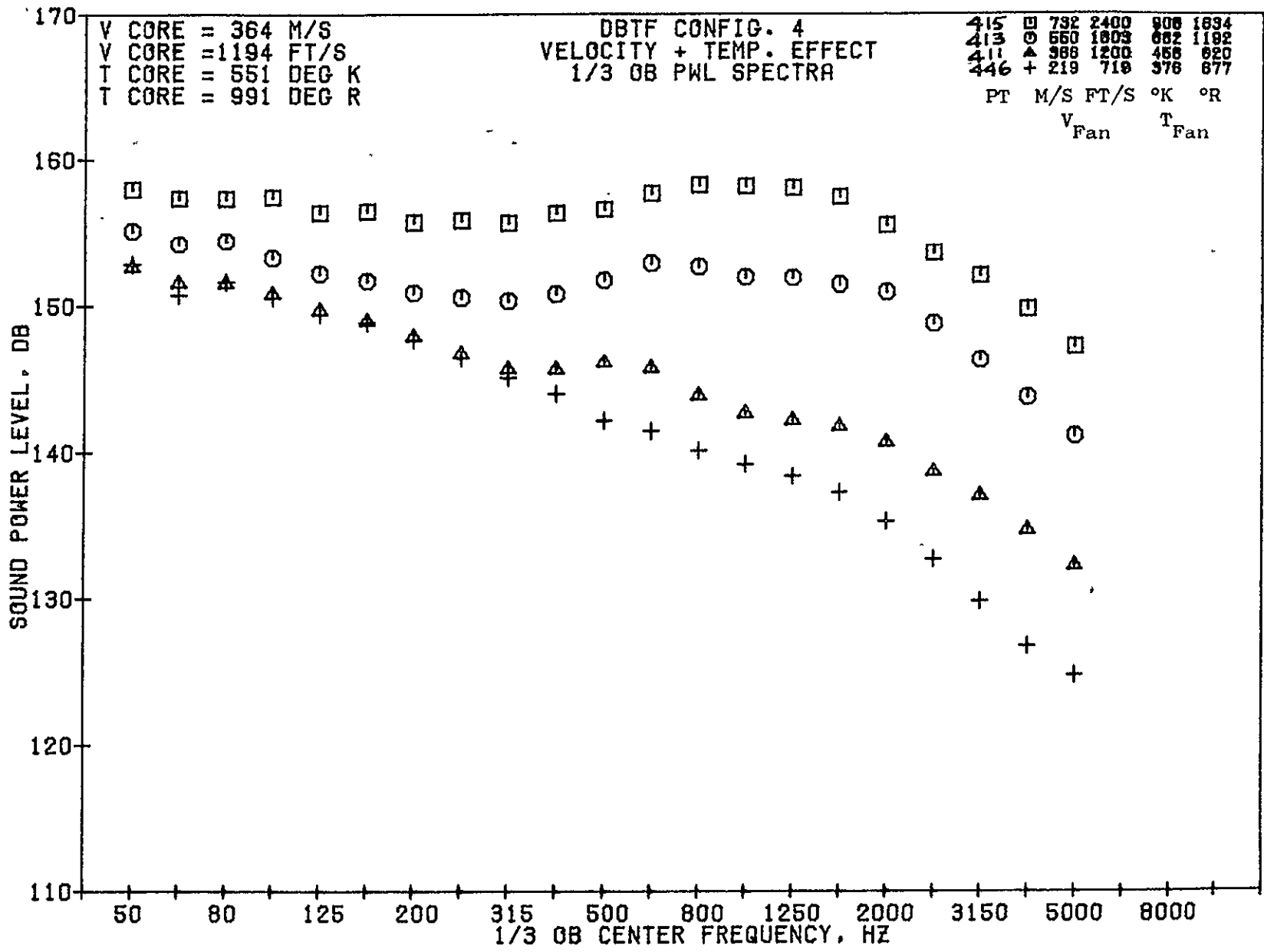
50 80 125 200 315 500 800 1250 2000 3150 5000 8000
1/3 OB CENTER FREQUENCY, HZ

1420

08/20/75
5R552-001

79 BURCH 8.

1125



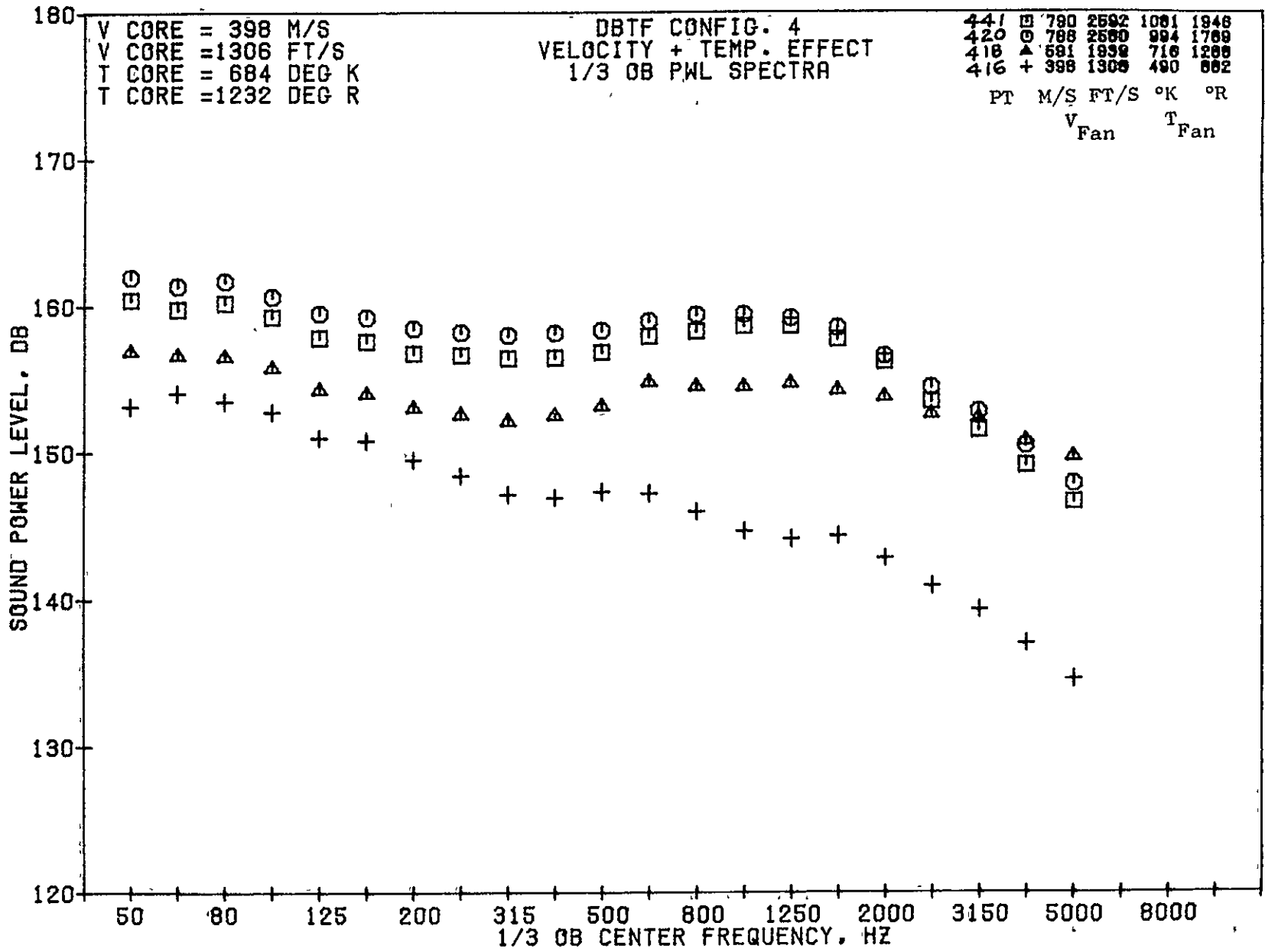
1421

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4-1986

08/20/75
5R552-001

79 BURCH A.

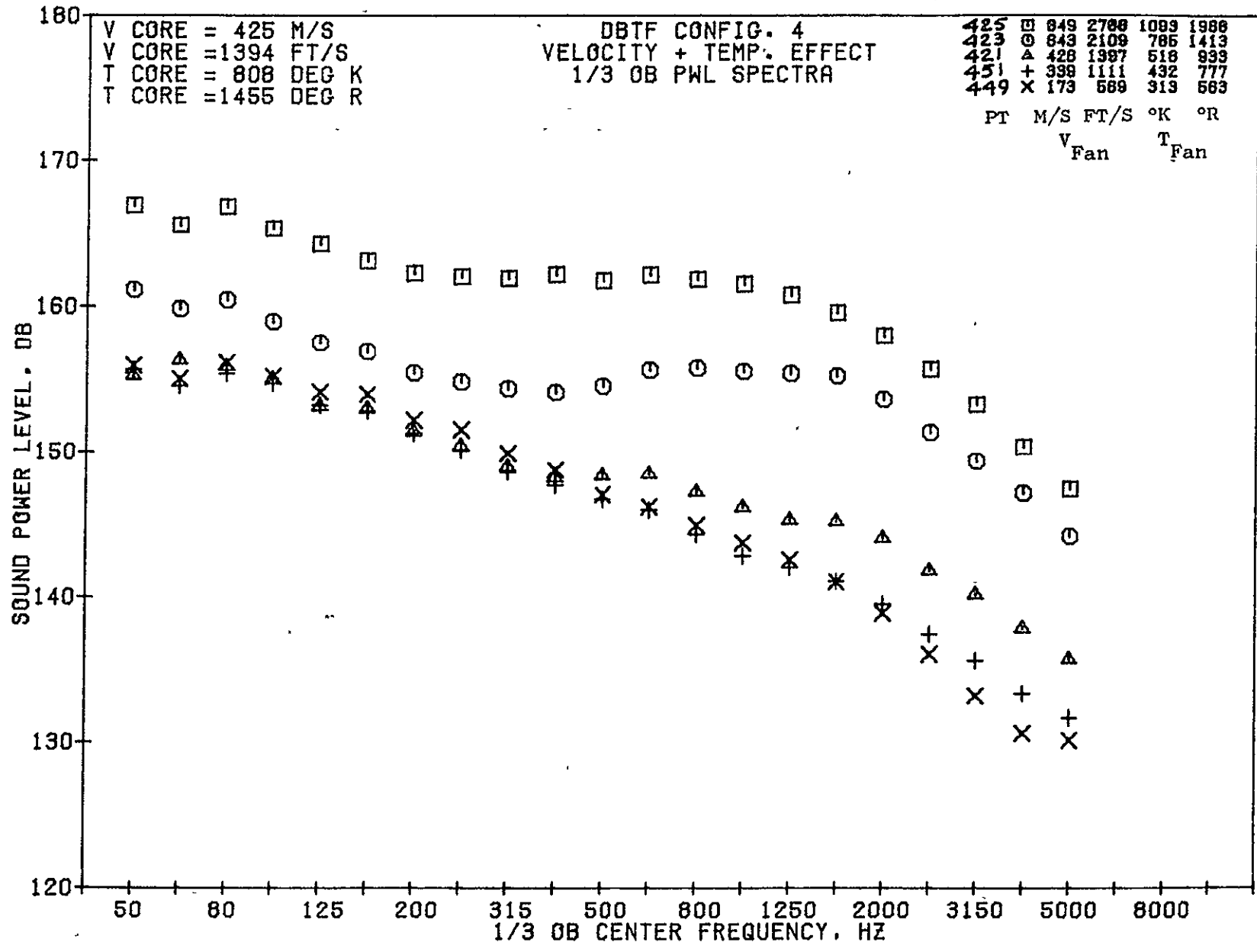


1422

4-187

08/20/75
5R552-001

79 BURCH A.



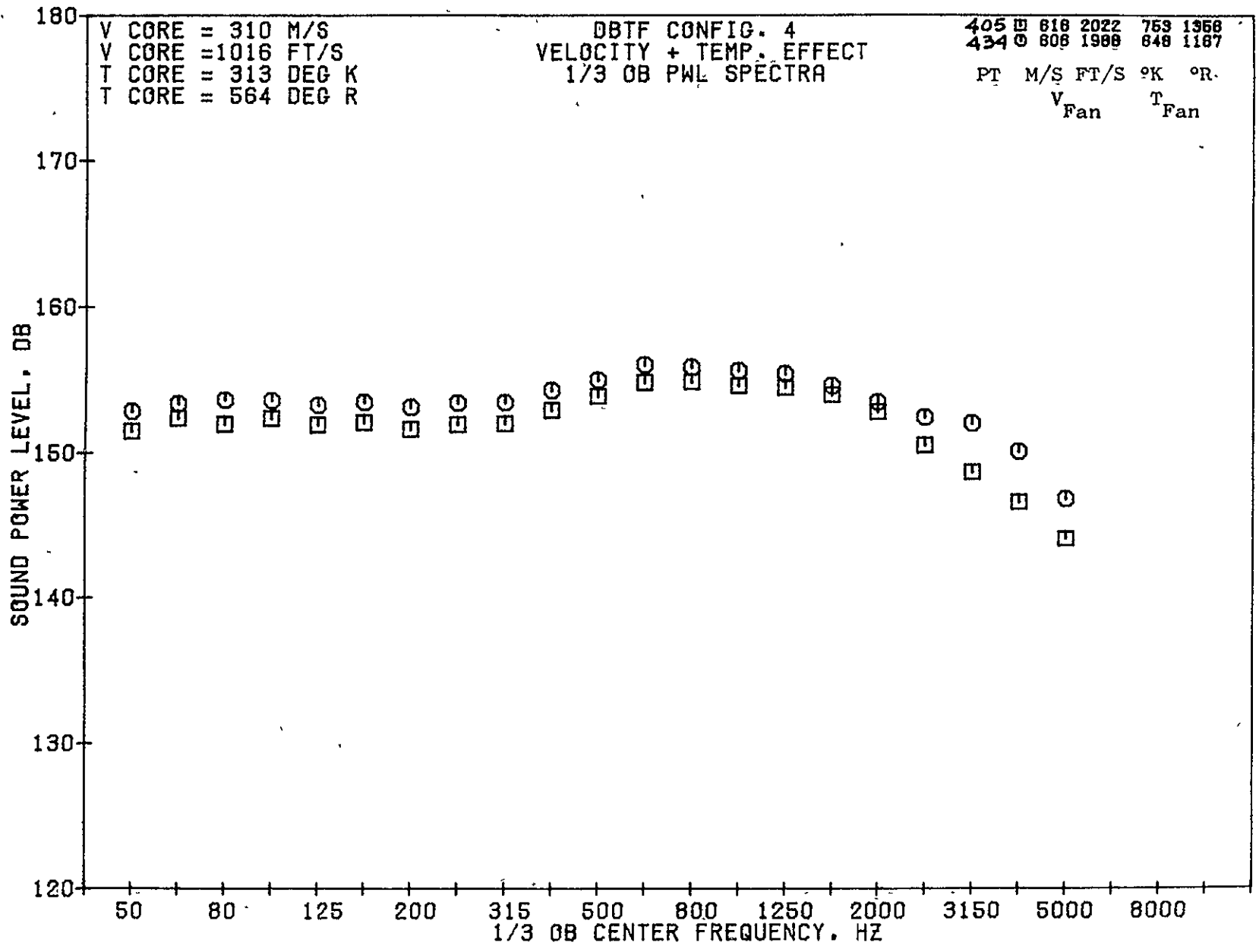
1423

41860

08/13/75
5R959-001

79 BURCH A.

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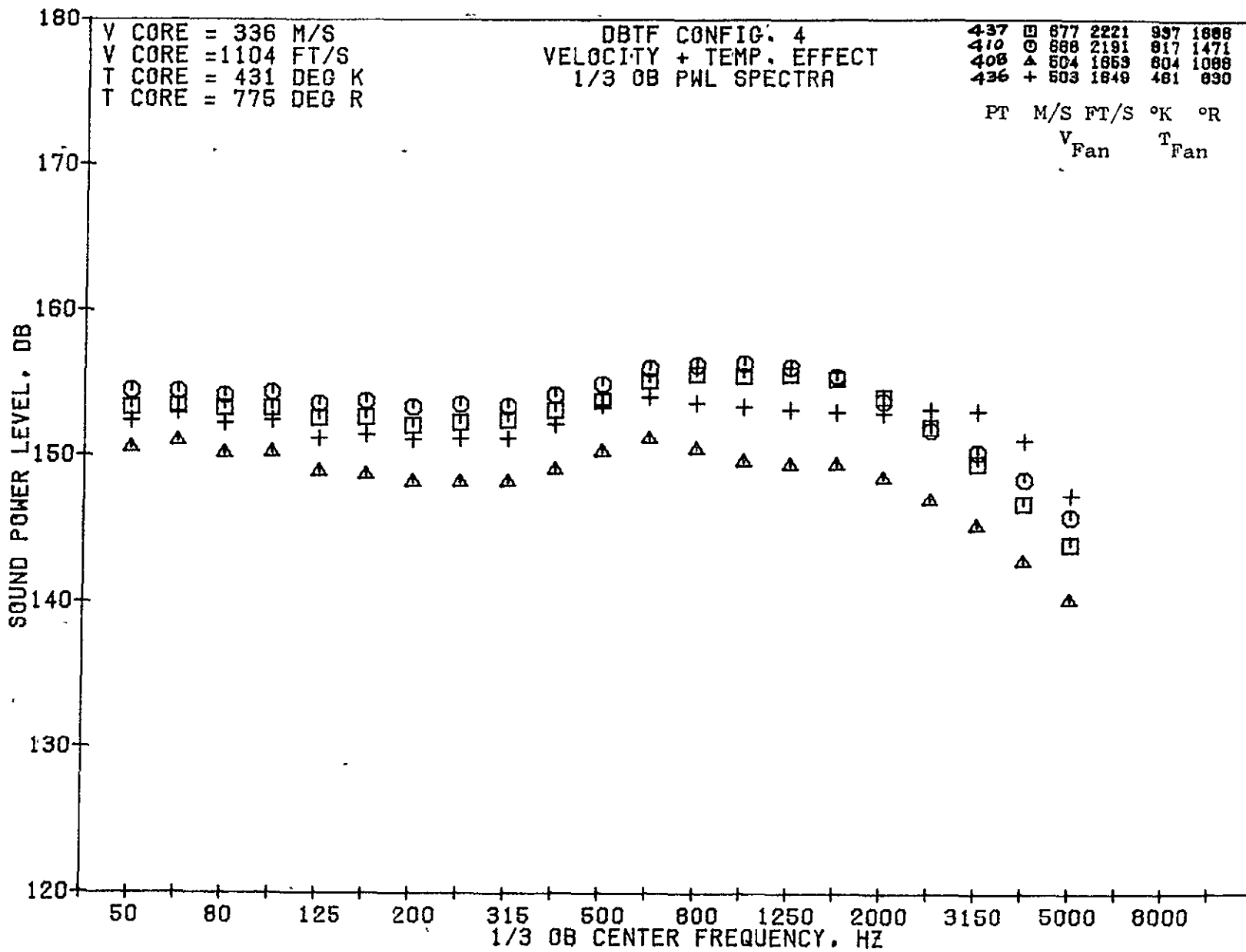
1424

11/89

08/13/75
 5R959-001

79 BURC A.

1425

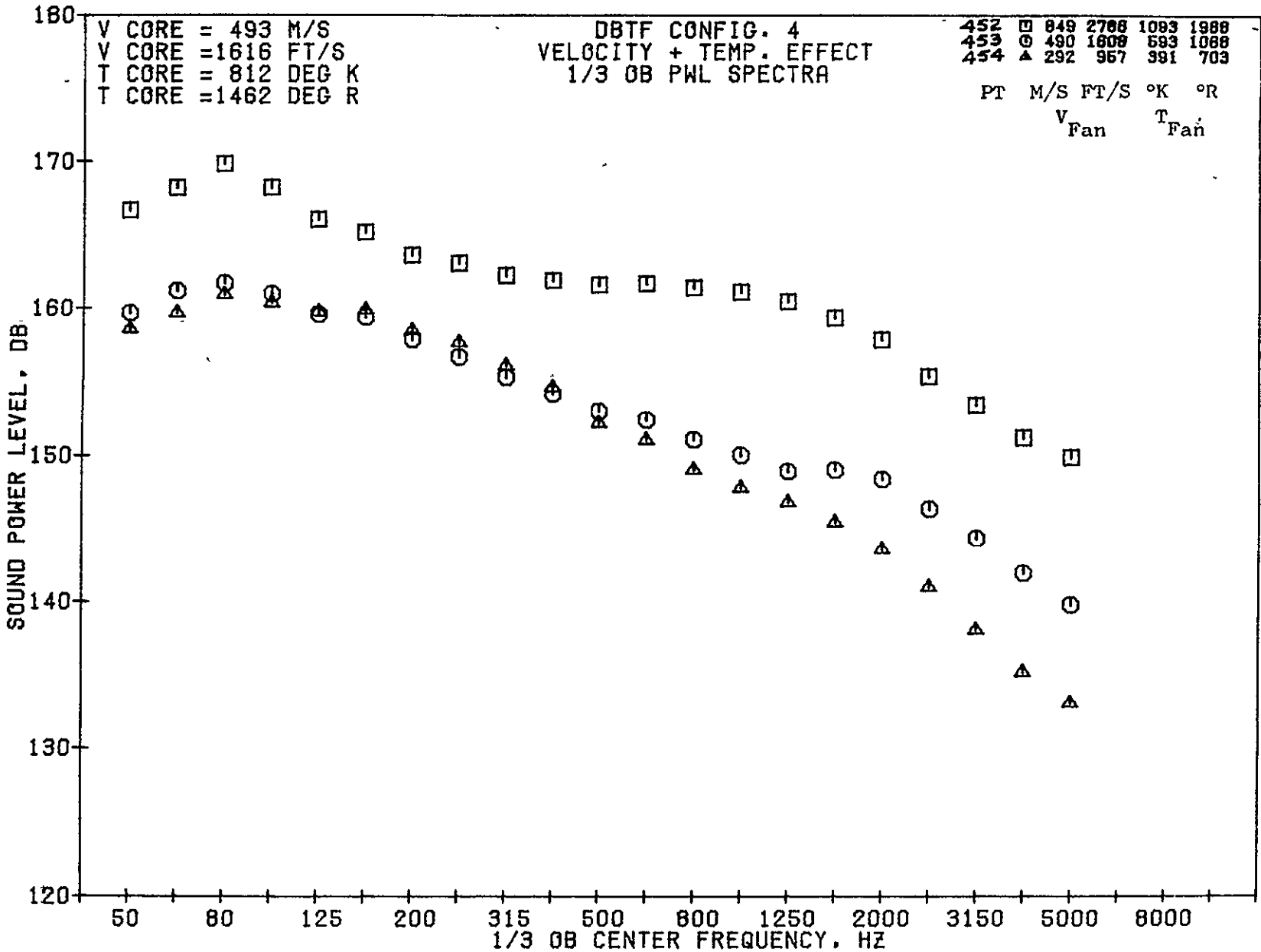


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1-1-75

08/13/75
5R959-001

79 BURCH A.

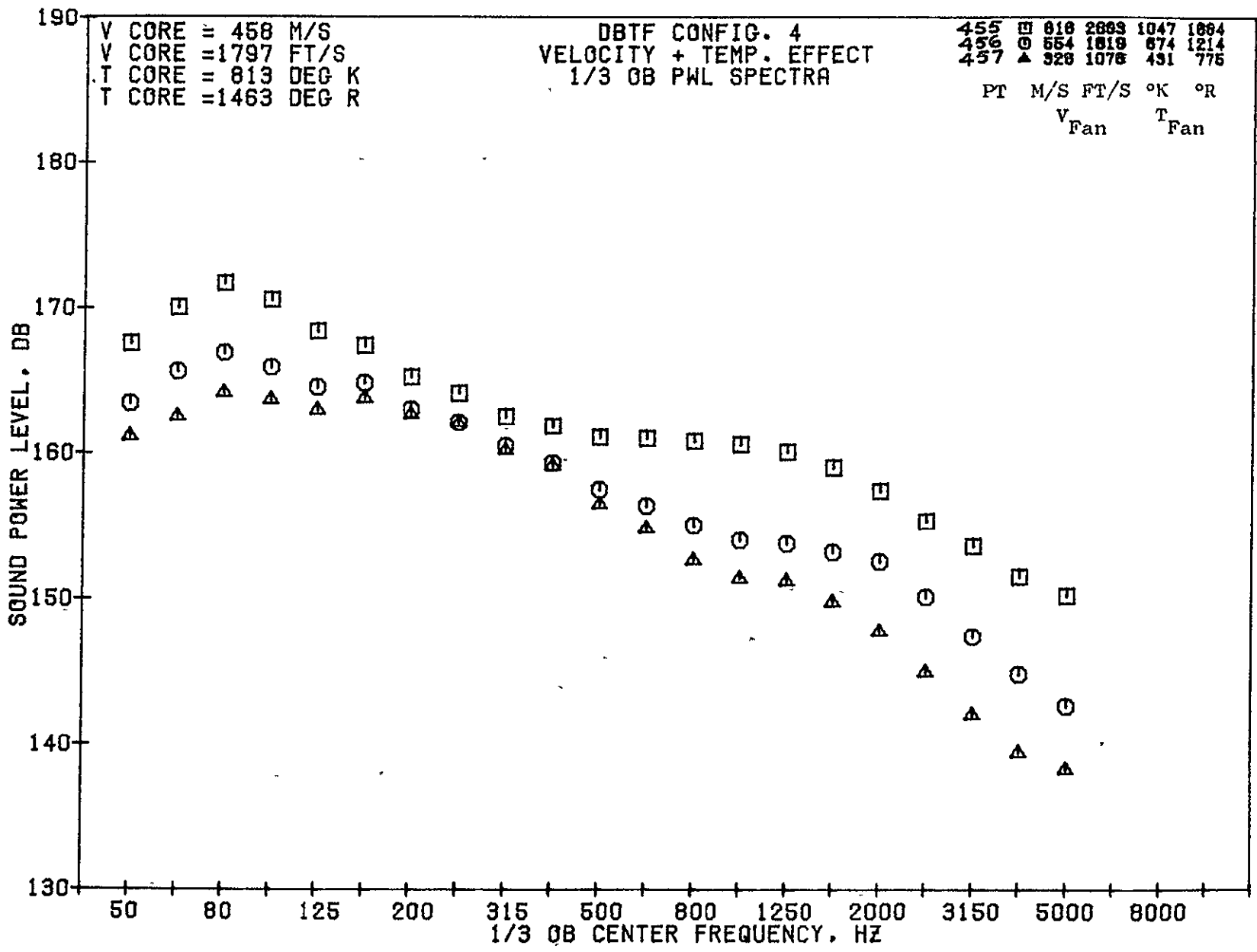


1426

1.191

08/13/75
5R959-001

79 BURC A.



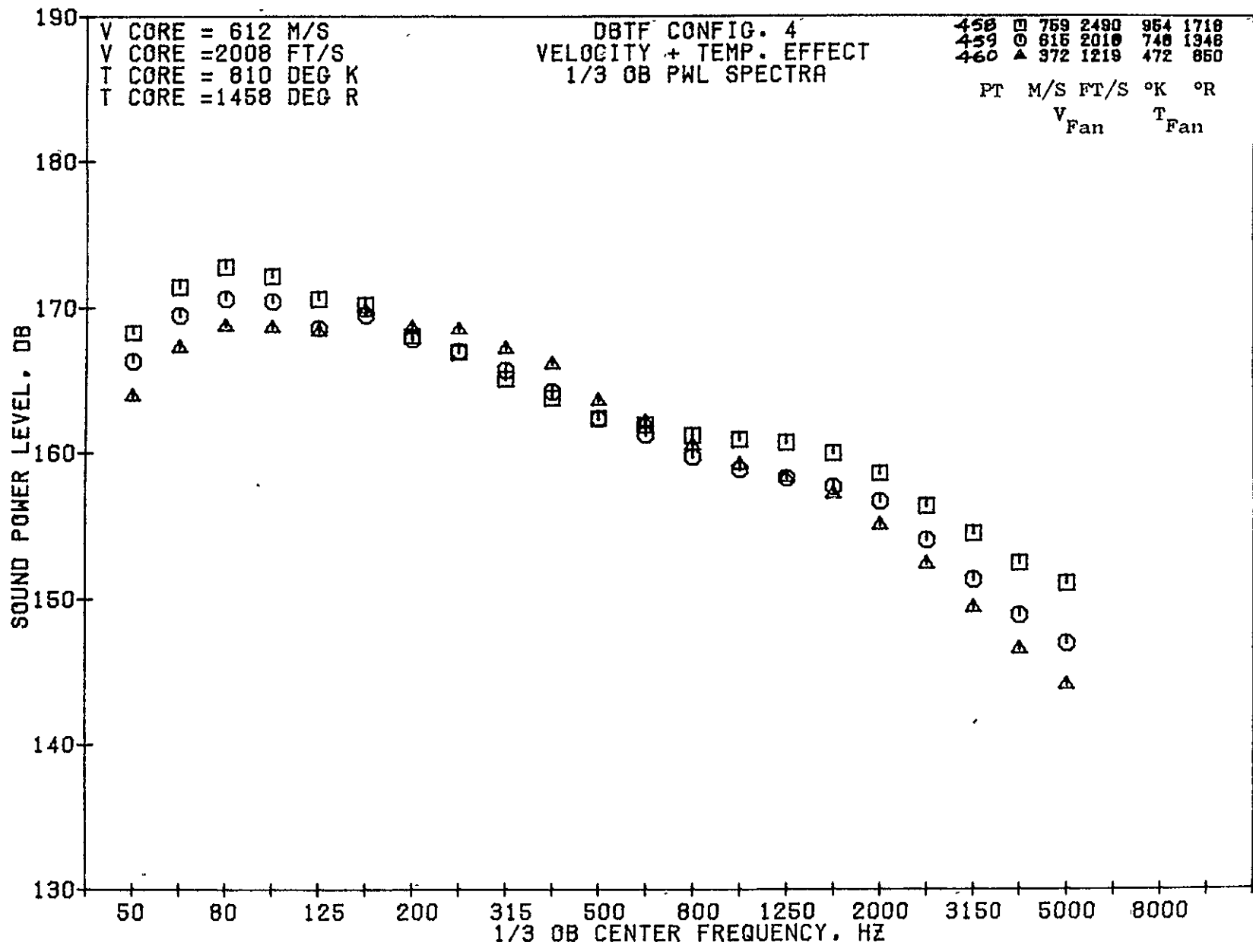
1427

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08/20/75
 5R552-001

79 BURCH A.

Ab-1-7



1428

1143

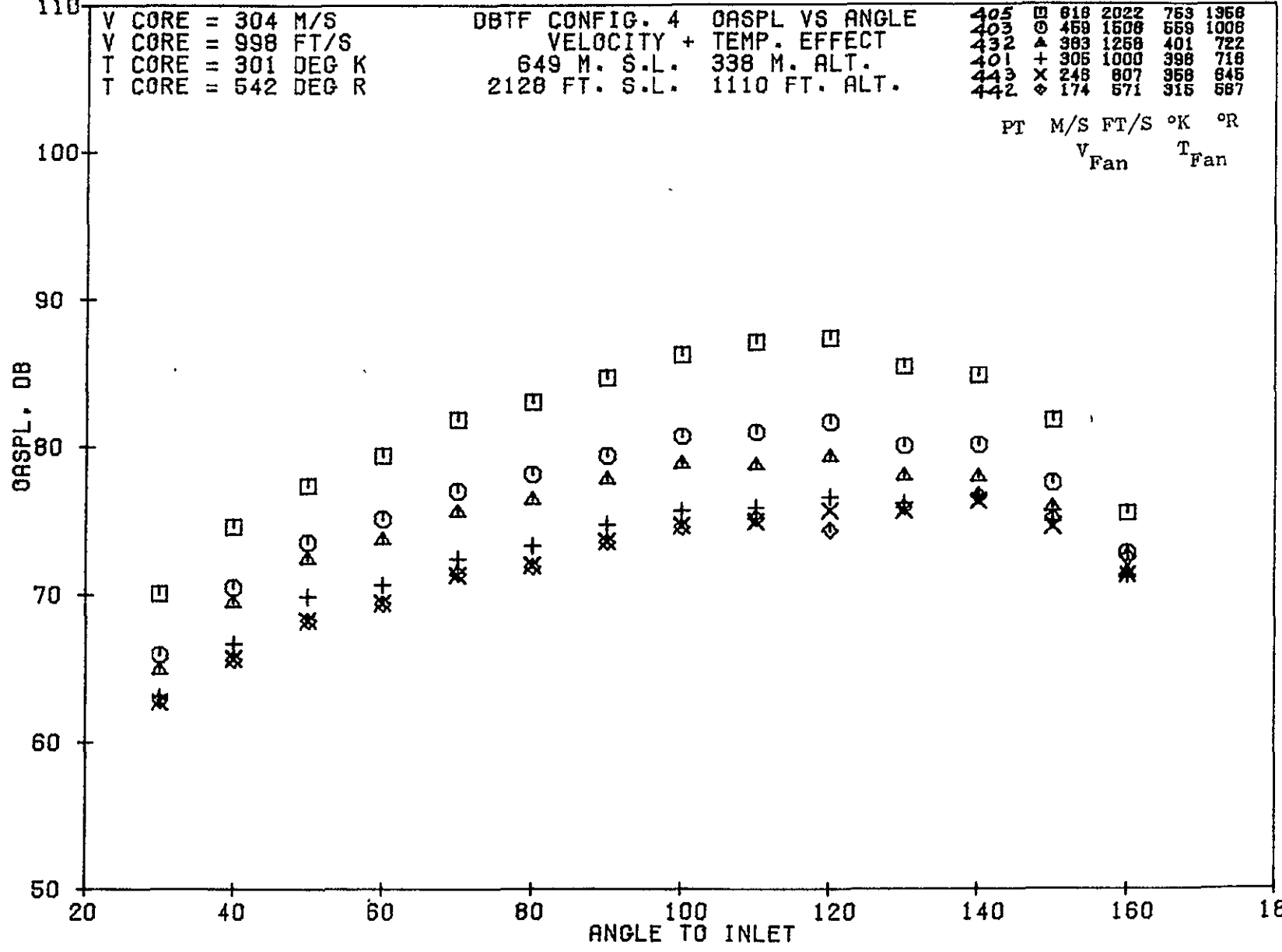
110

V CORE = 304 M/S
 V CORE = 998 FT/S
 T CORE = 301 DEG K
 T CORE = 542 DEG R

DBTF CONFIG. 4 OASPL VS ANGLE
 VELOCITY + TEMP. EFFECT
 649 M. S.L. 338 M. ALT.
 2128 FT. S.L. 1110 FT. ALT.

405	□	818	2022	753	1968
403	○	459	1508	559	1008
432	△	383	1258	401	722
401	+	305	1000	398	718
443	x	248	807	358	645
442	◇	174	571	316	587

PT M/S FT/S °K °R
 V_{Fan} T_{Fan}



1429

4-1944

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110

V CORE = 336 M/S
V CORE = 1101 FT/S
T CORE = 431 DEG K
T CORE = 775 DEG R

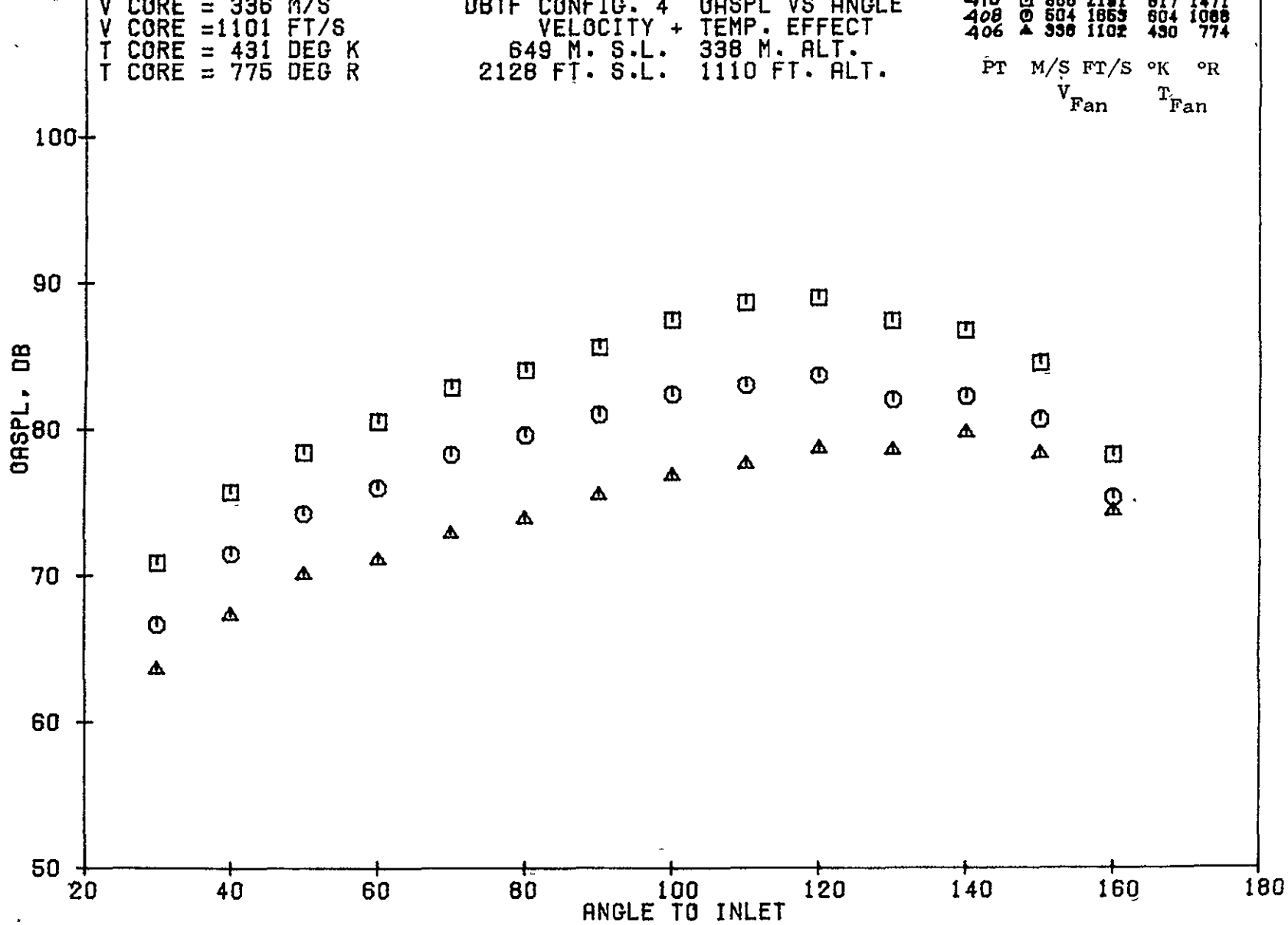
DBTF CONFIG. 4 OASPL VS ANGLE
VELOCITY + TEMP. EFFECT
649 M. S.L. 338 M. ALT.
2128 FT. S.L. 1110 FT. ALT.

410	□	880	2191	817	1471
408	○	504	1859	804	1088
406	▲	336	1102	430	774
PT		M/S	FT/S	°K	°R
		V _{Fan}		T _{Fan}	

OASPL, DB
100
90
80
70
60
50

1430

20 40 60 80 100 120 140 160 180
ANGLE TO INLET



08/20/75
5R552-001

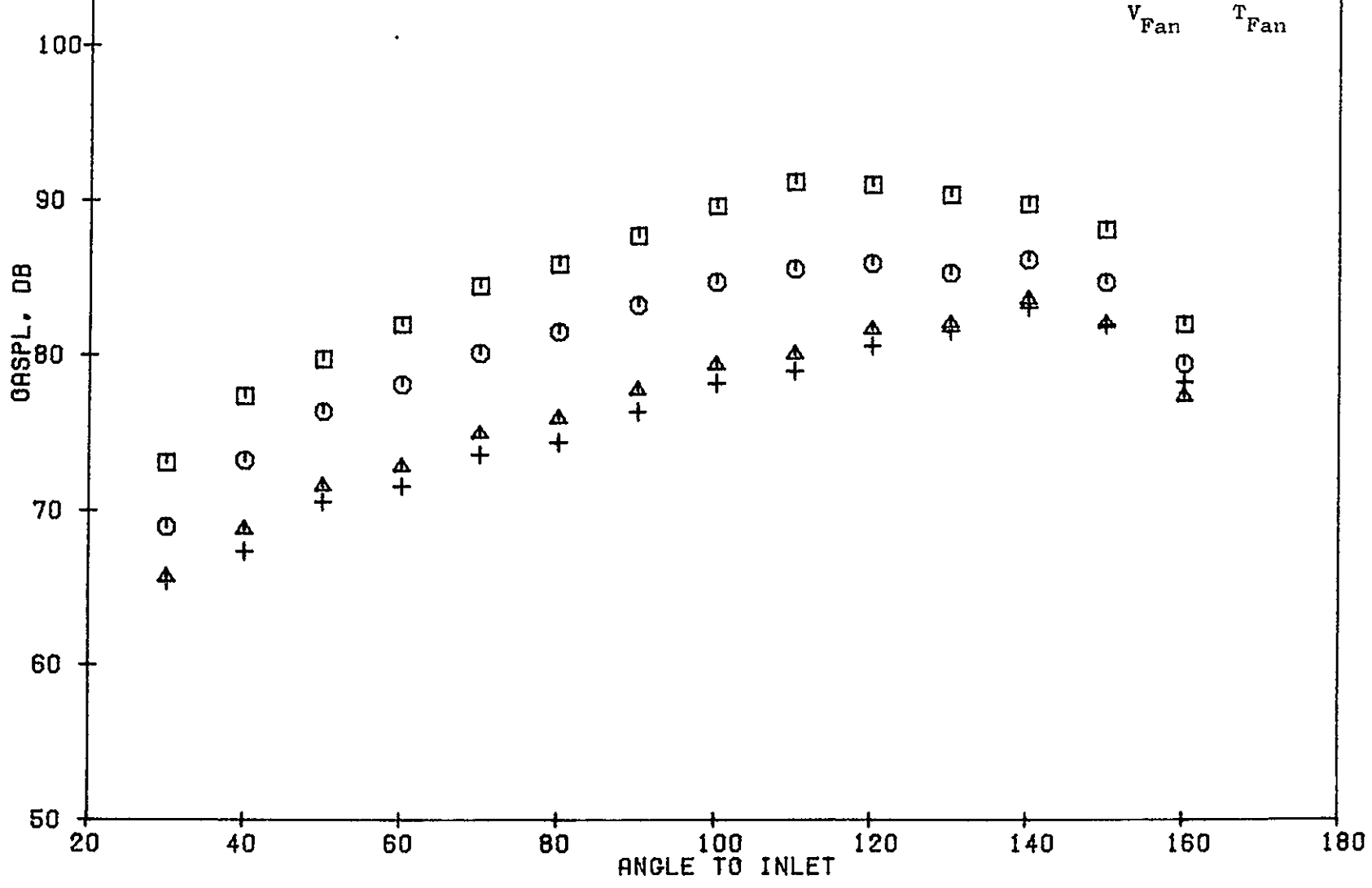
79 BURCH 3.

V CORE = 364 M/S
 V CORE = 1194 FT/S
 T CORE = 551 DEG K
 T CORE = 991 DEG R

DBTF CONFIG. 4 GASPL VS ANGLE
 VELOCITY + TEMP. EFFECT
 649 M. S.L. 338 M. ALT.
 2128 FT. S.L. 1110 FT. ALT.

415	□	732	2400	908	1634
413	○	560	1809	862	1192
411	▲	388	1200	458	820
446	+	219	719	376	677

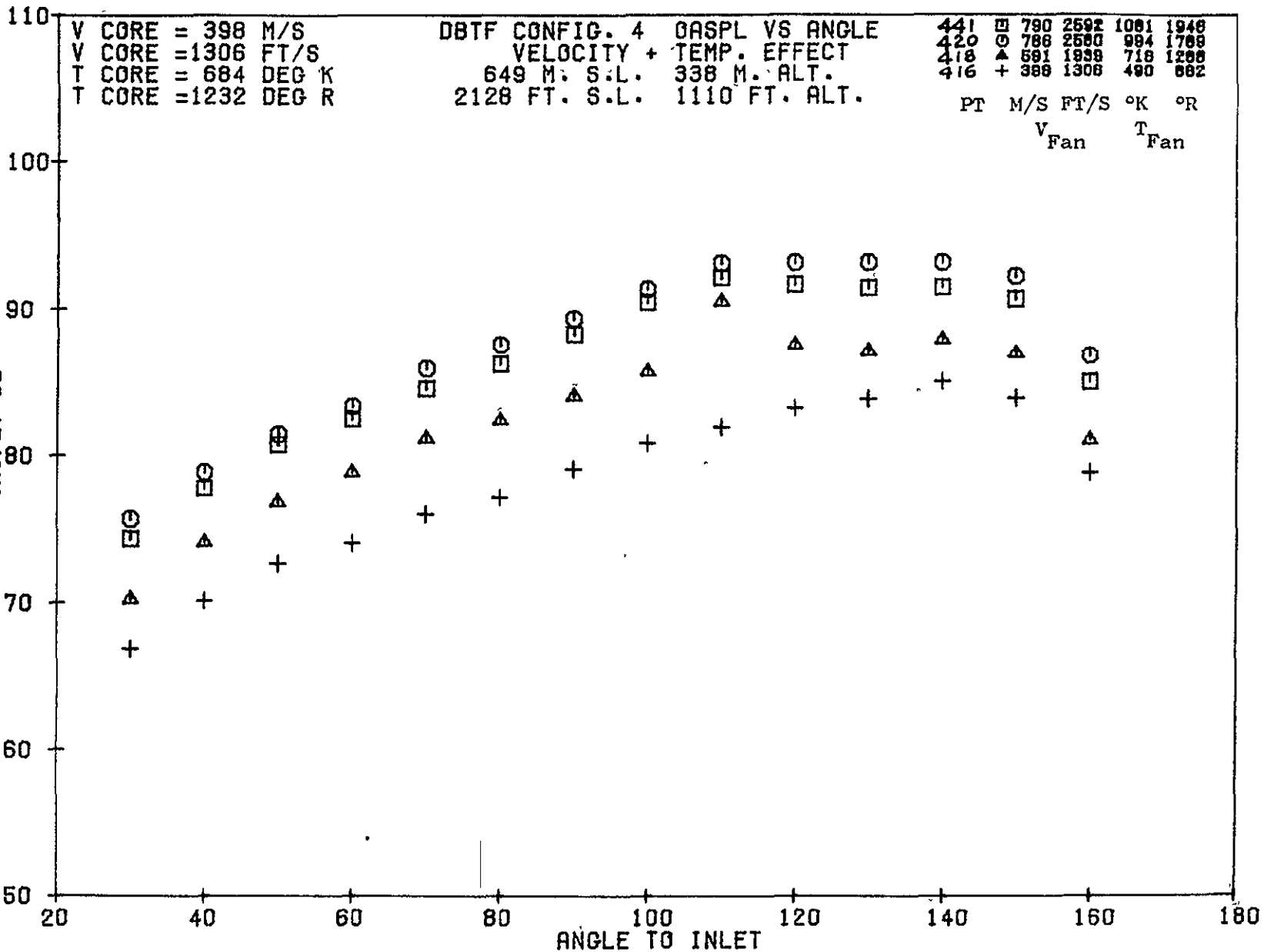
PT M/S FT/S °K °R
 V_{Fan} T_{Fan}



1431

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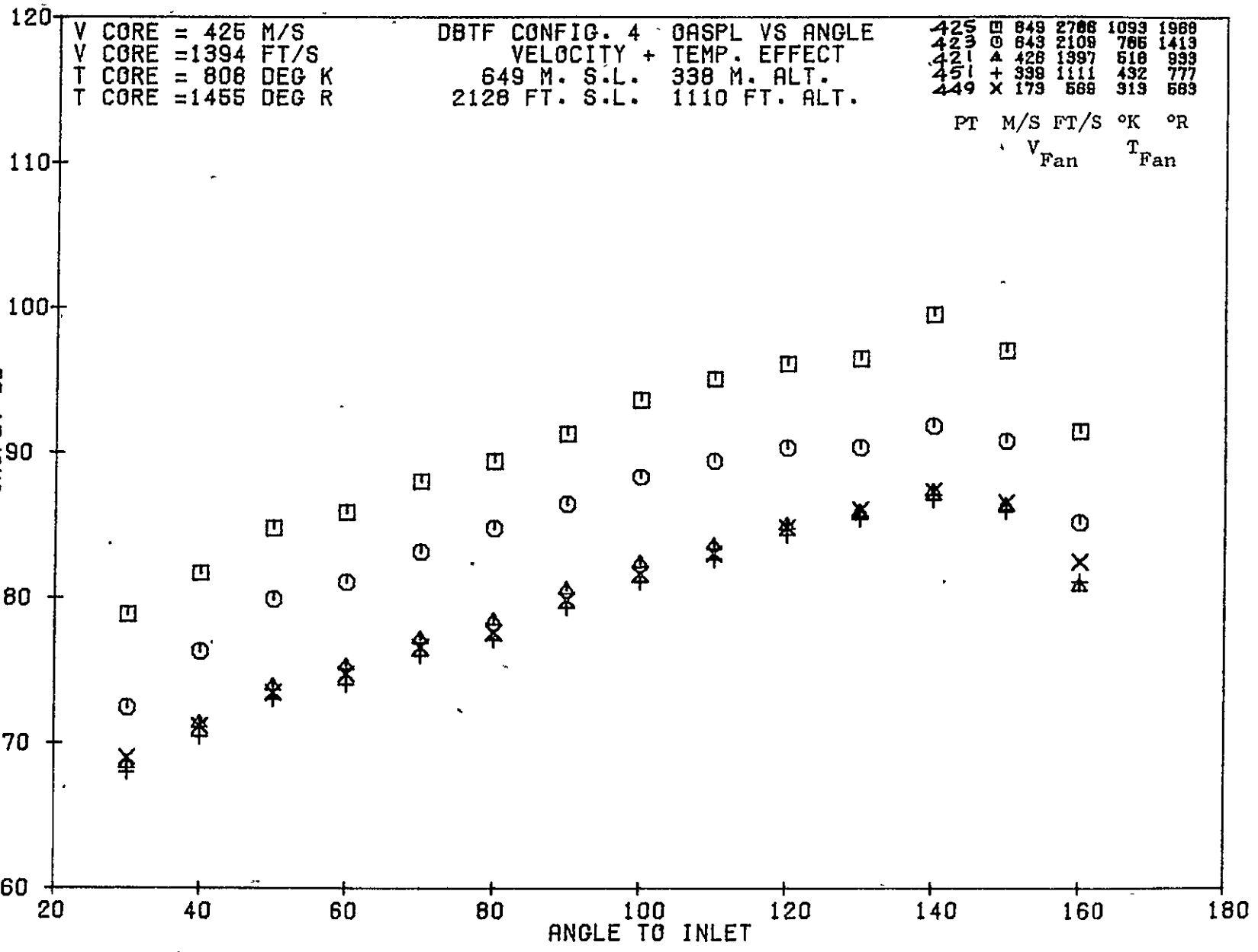
110



1432

08/20/75
5R552-001

79 BURCH



1433

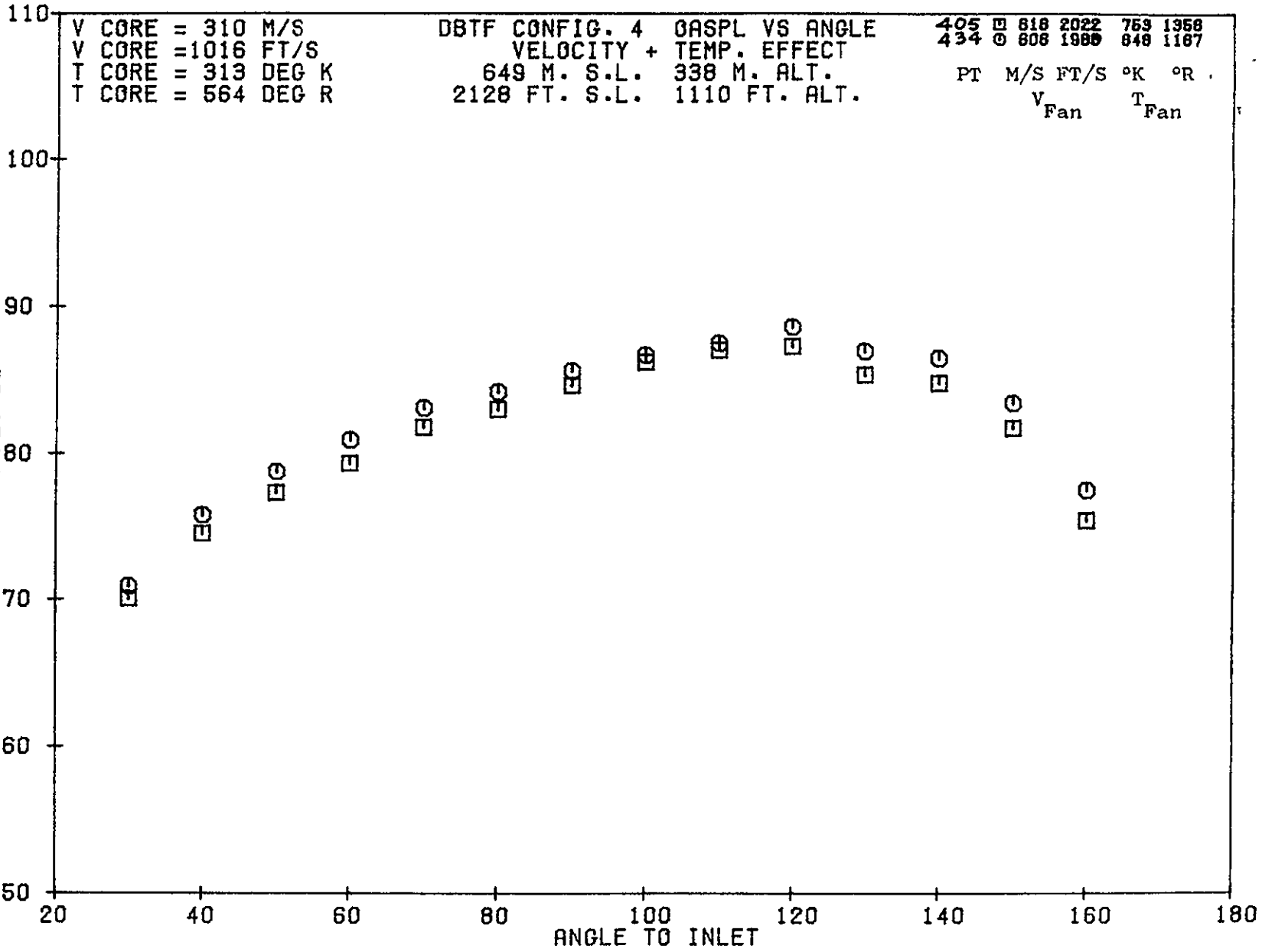
C-3

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4-198

08/13/75
 5R959-001

79 BURCH A.

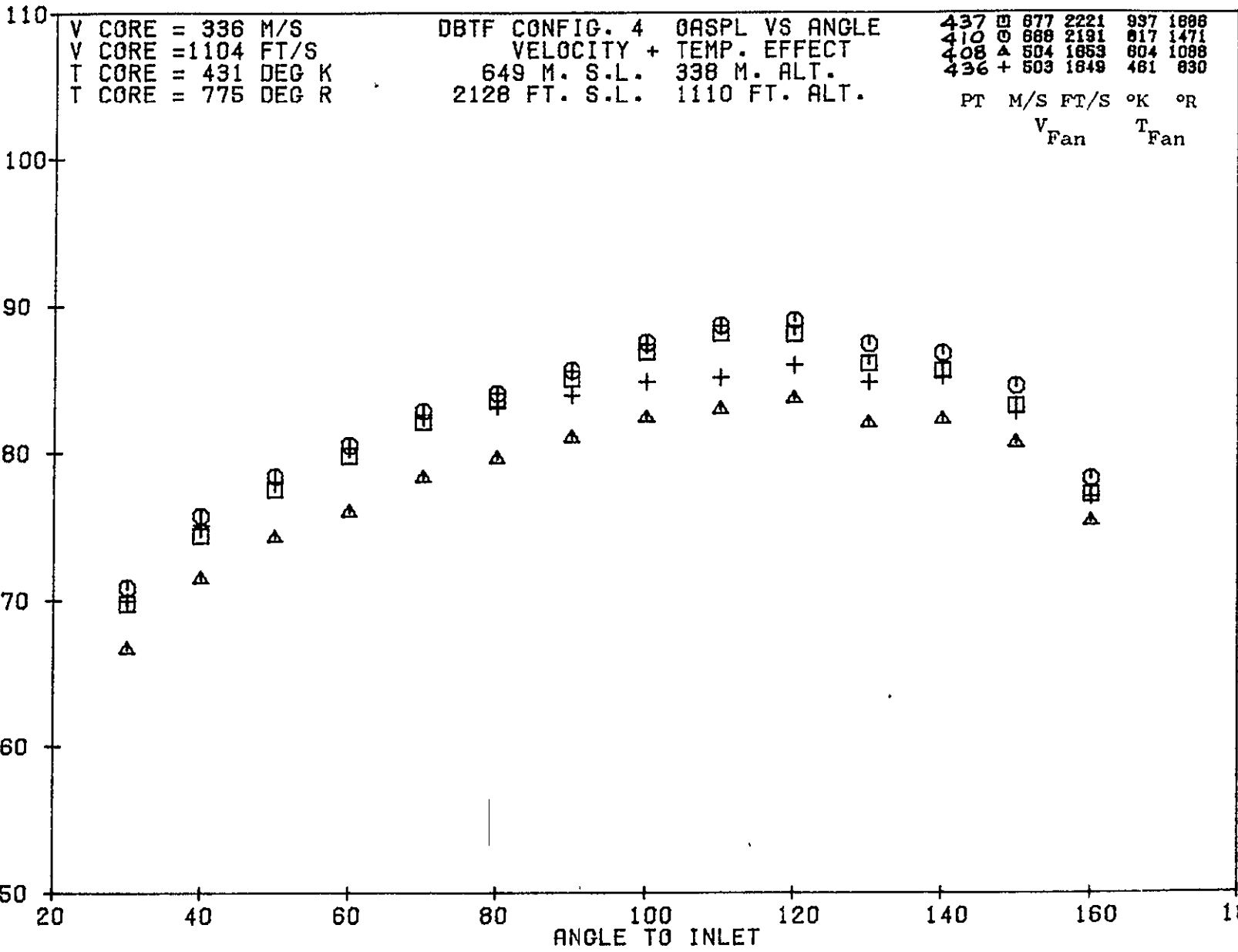


1434

11-199

08/13/75
5R959-001

79 BURC



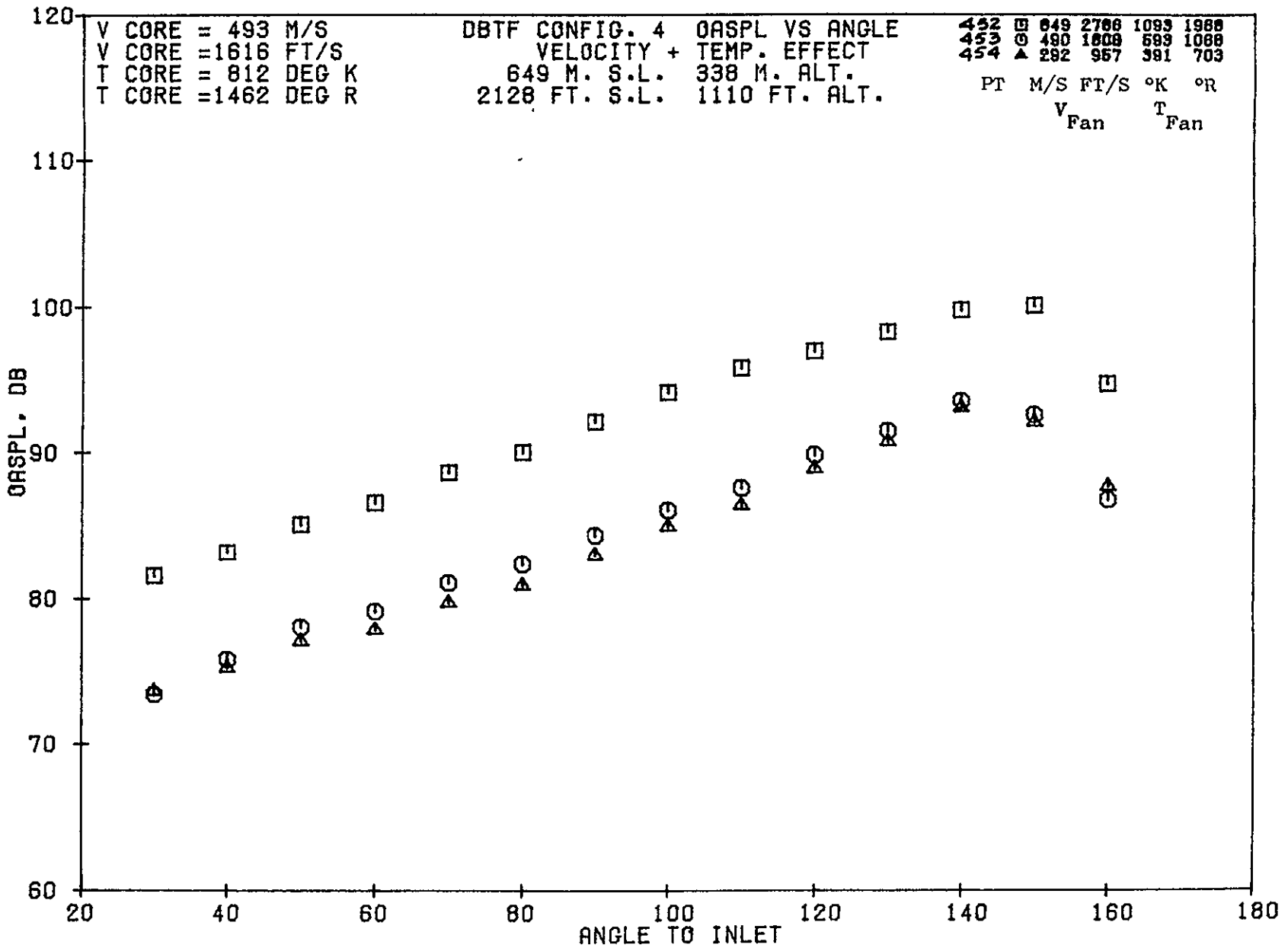
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4-200

08/13/75
5R959-001

79 BURCH A.



1436

08/13/75
5R959-001

79 BURC A.

120
110
100
90
80
70
60

V CORE = 458 M/S
V CORE = 1797 FT/S
T CORE = 813 DEG K
T CORE = 1463 DEG R

DBTF CONFIG. 4 OASPL VS ANGLE
VELOCITY + TEMP. EFFECT
649 M. S.L. 338 M. ALT.
2128 FT. S.L. 1110 FT. ALT.

455	□	818	2883	1047	1884
456	○	554	1819	674	1214
457	▲	326	1078	431	775
PT		M/S	FT/S	°K	°R
		V _{Fan}	T _{Fan}		

OASPL, DB

ANGLE TO INLET

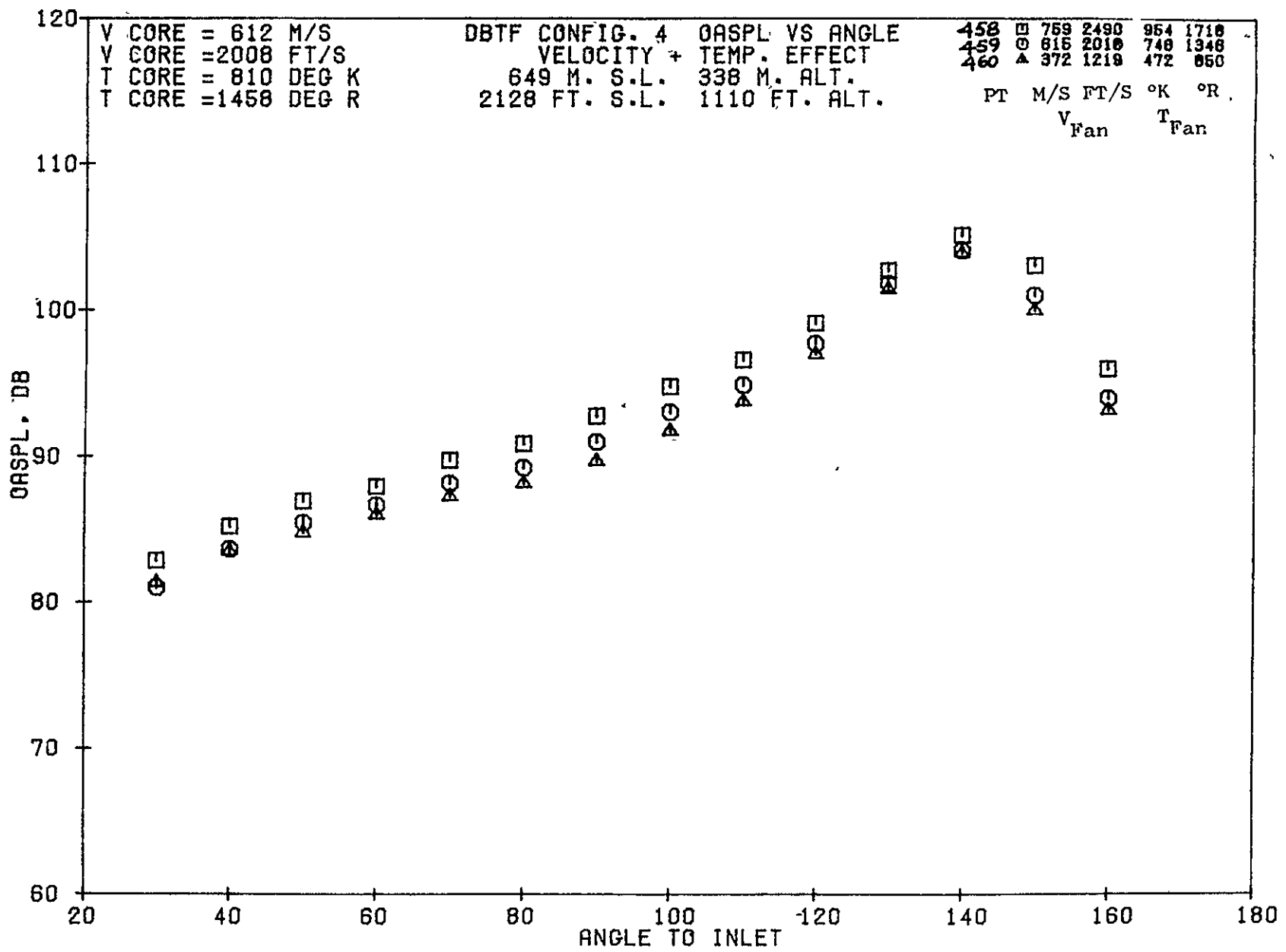
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M-201

08/20/75
5R552-001

79 BURCH A.

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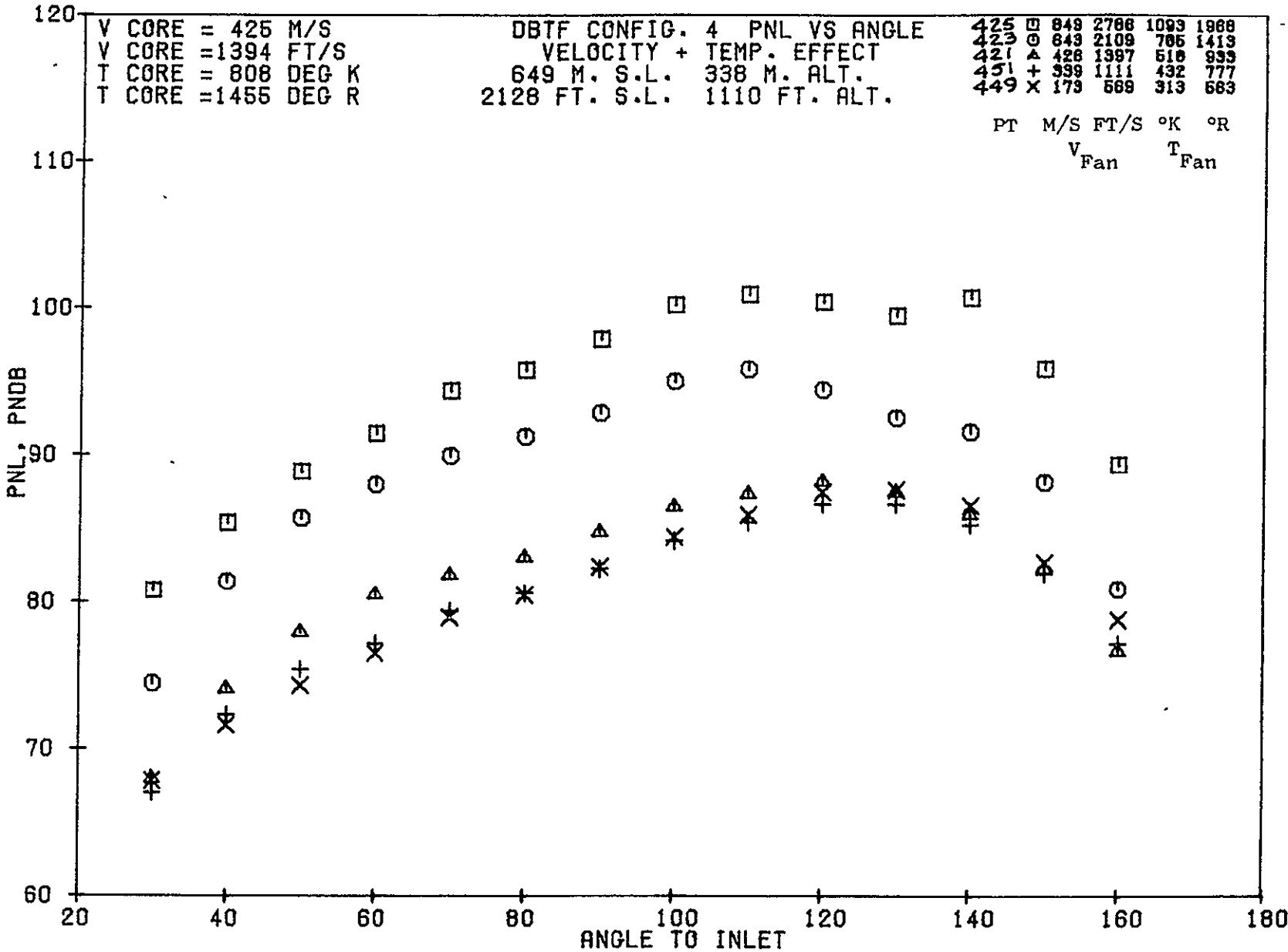
1438

11 103

08/13/75
5R959-001

79 BURC A.

1439



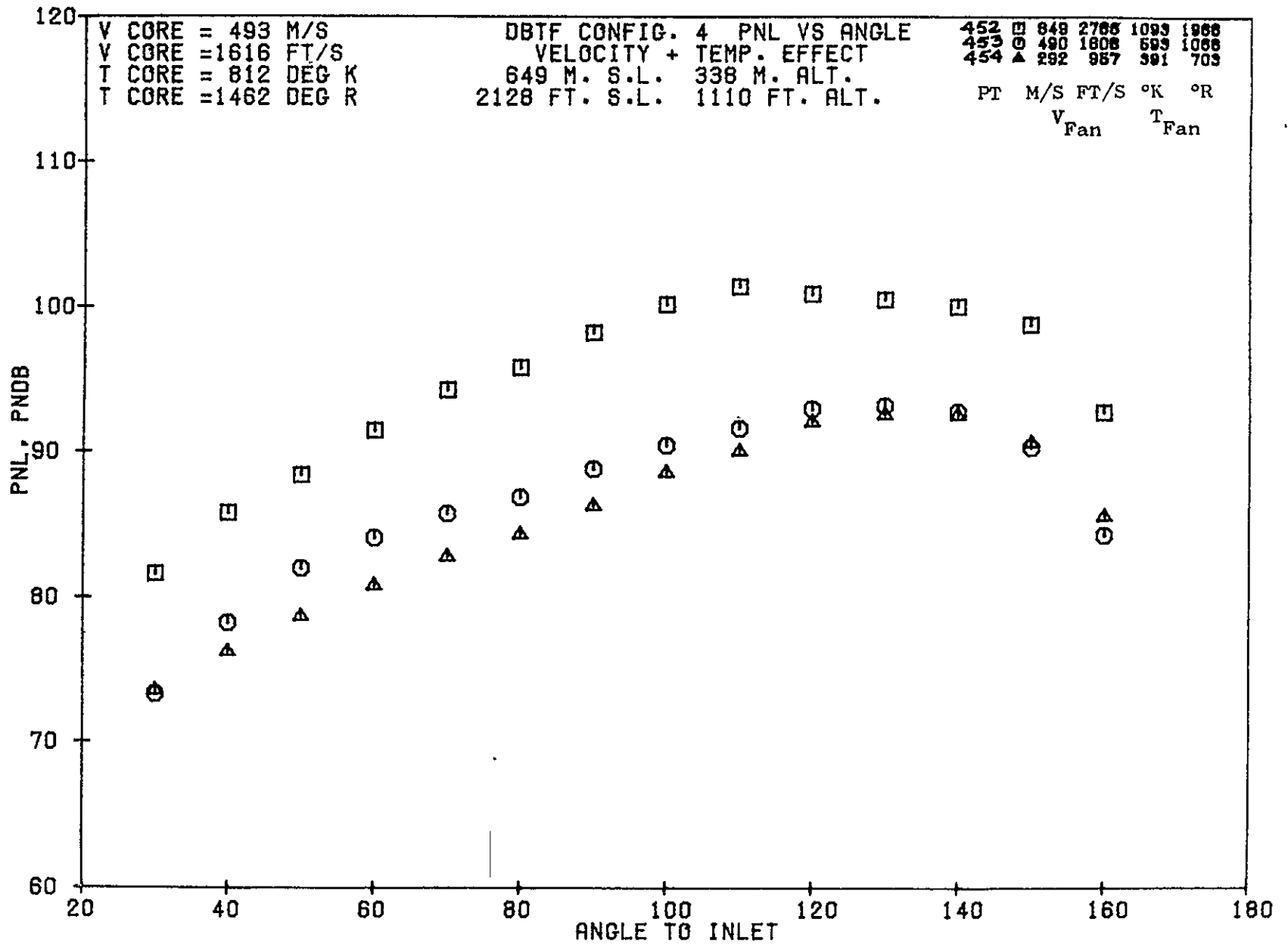
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5R552-001

79 BURCH A.

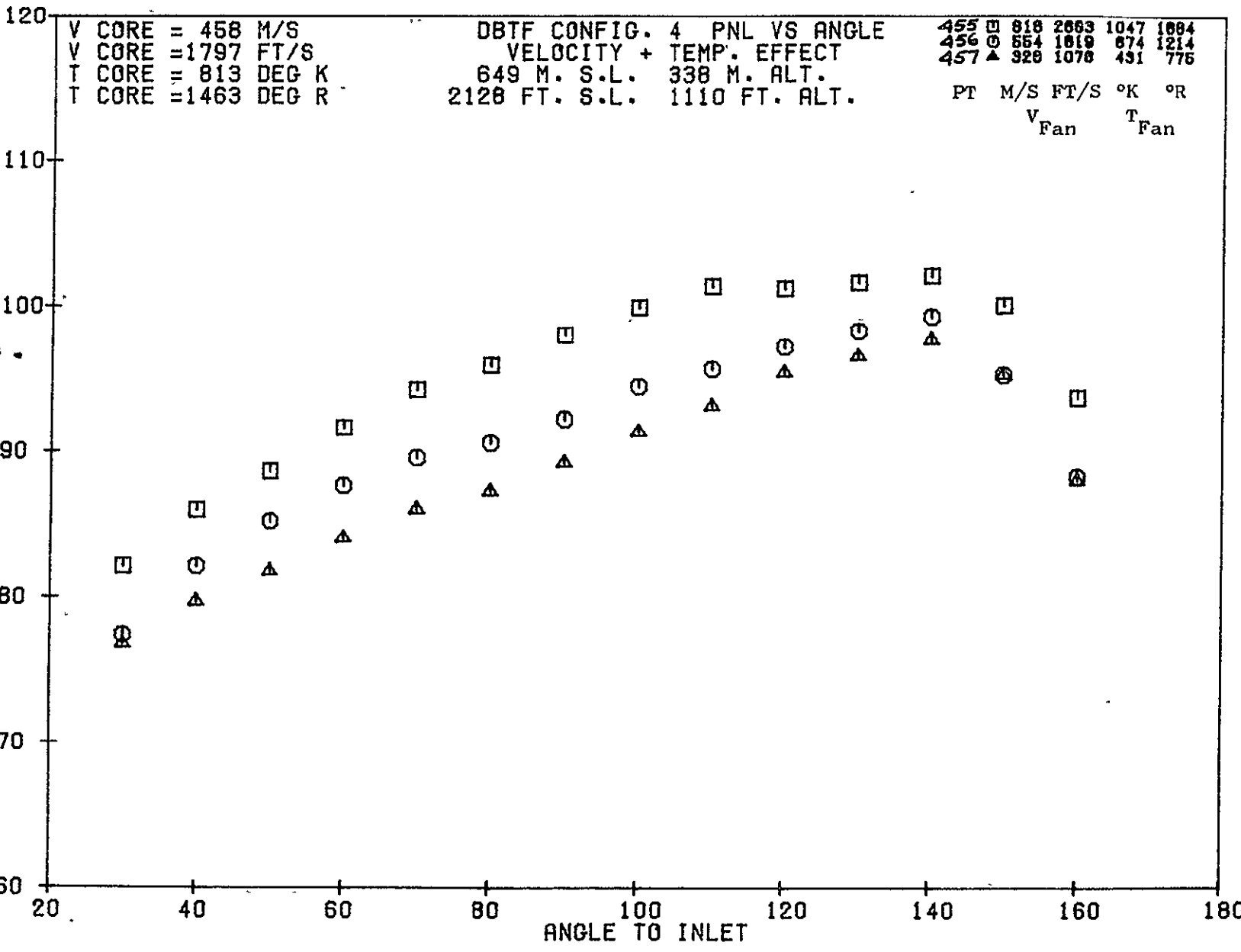
107 H

1440



08/20/75
5R552-001

79 BURCH A.



1441

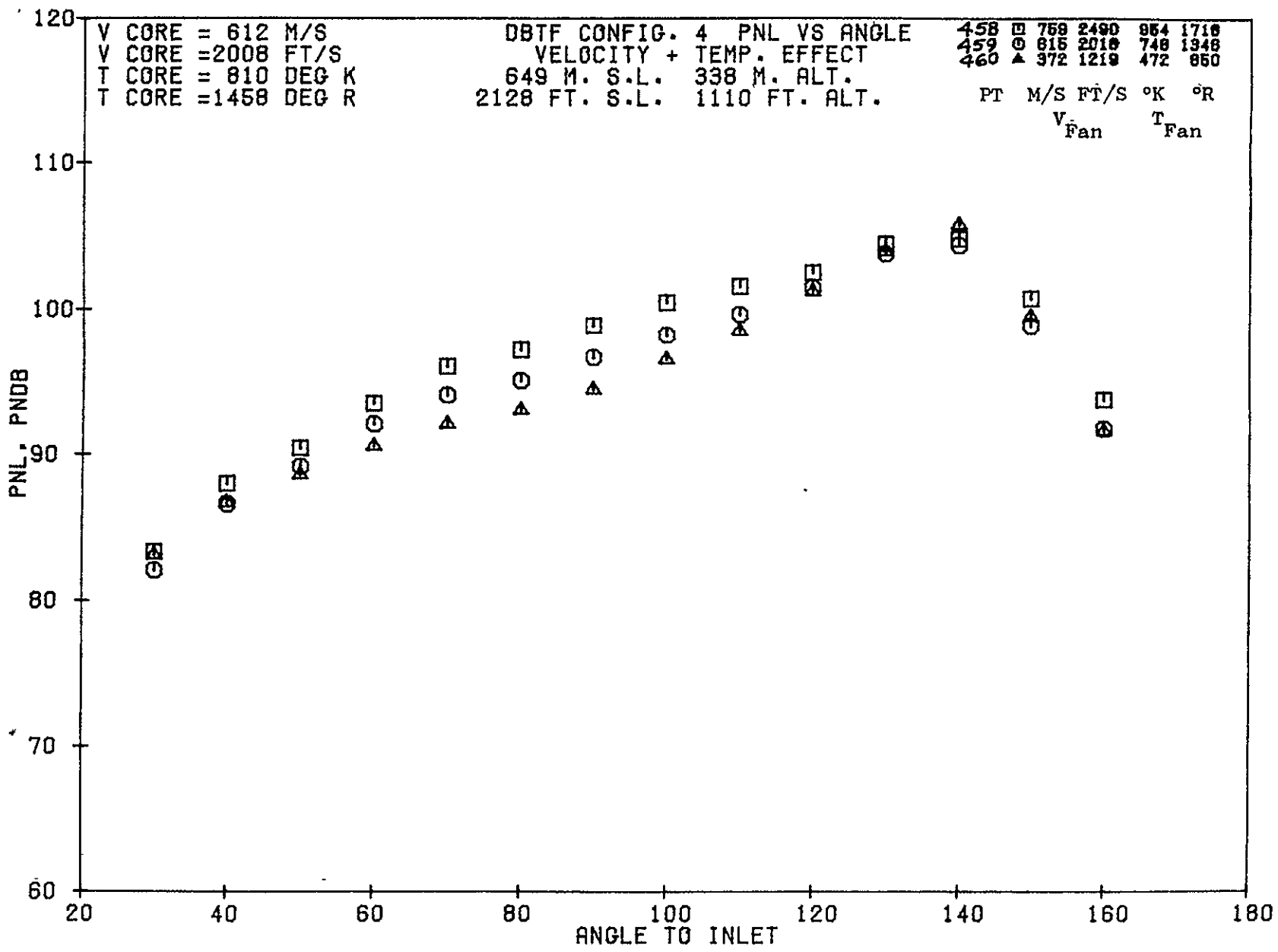
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4 206

08/20/75
5R552-001

79 BURCH A.

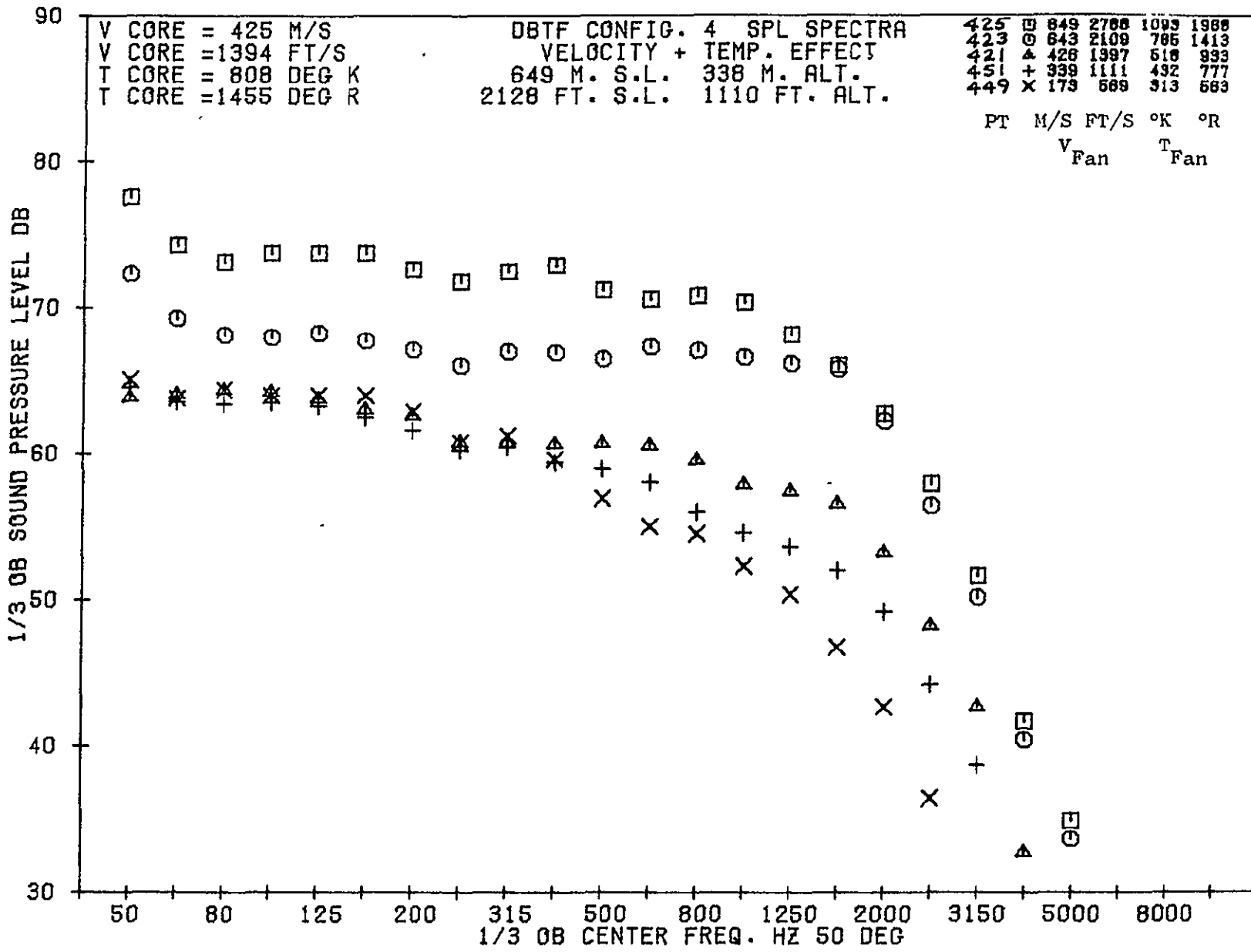
1442



Lot 1

08/13/75
5R959-001

79 BURCOR



1443

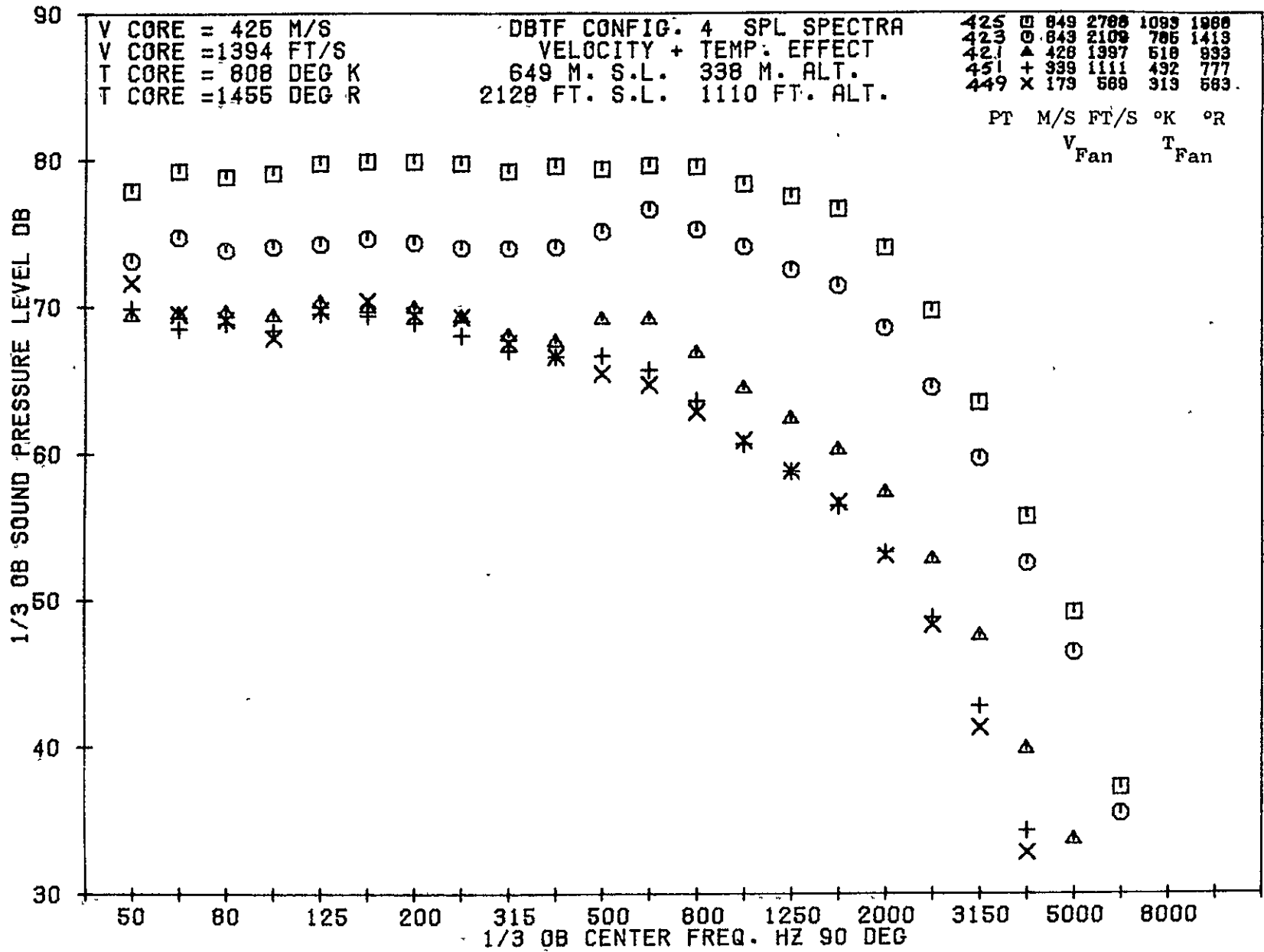
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4-205

08/13/75
5R959-001

79 BURCH A.

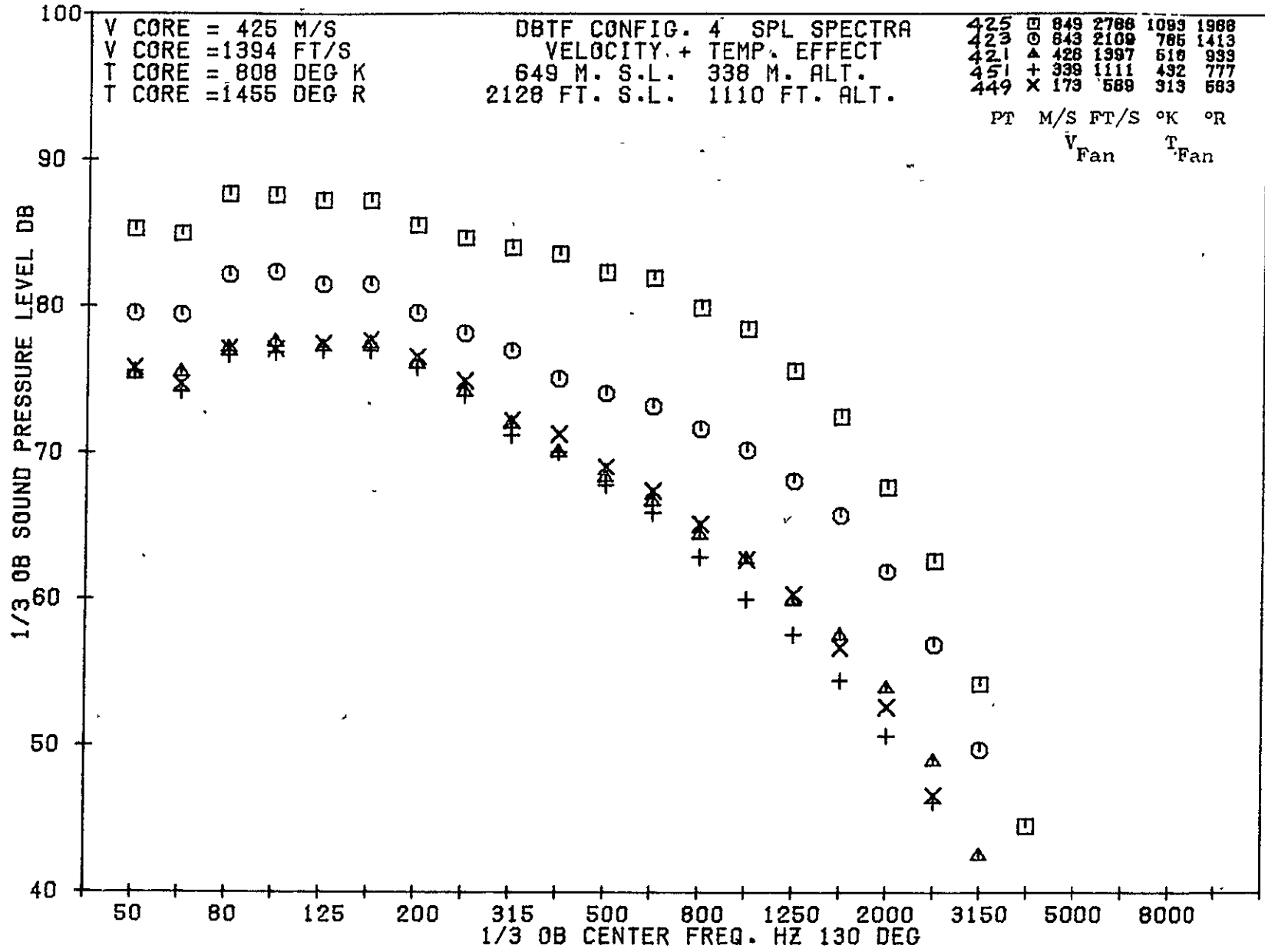
1444



1-209

08/13/75
5R959-001

79 BURC A.



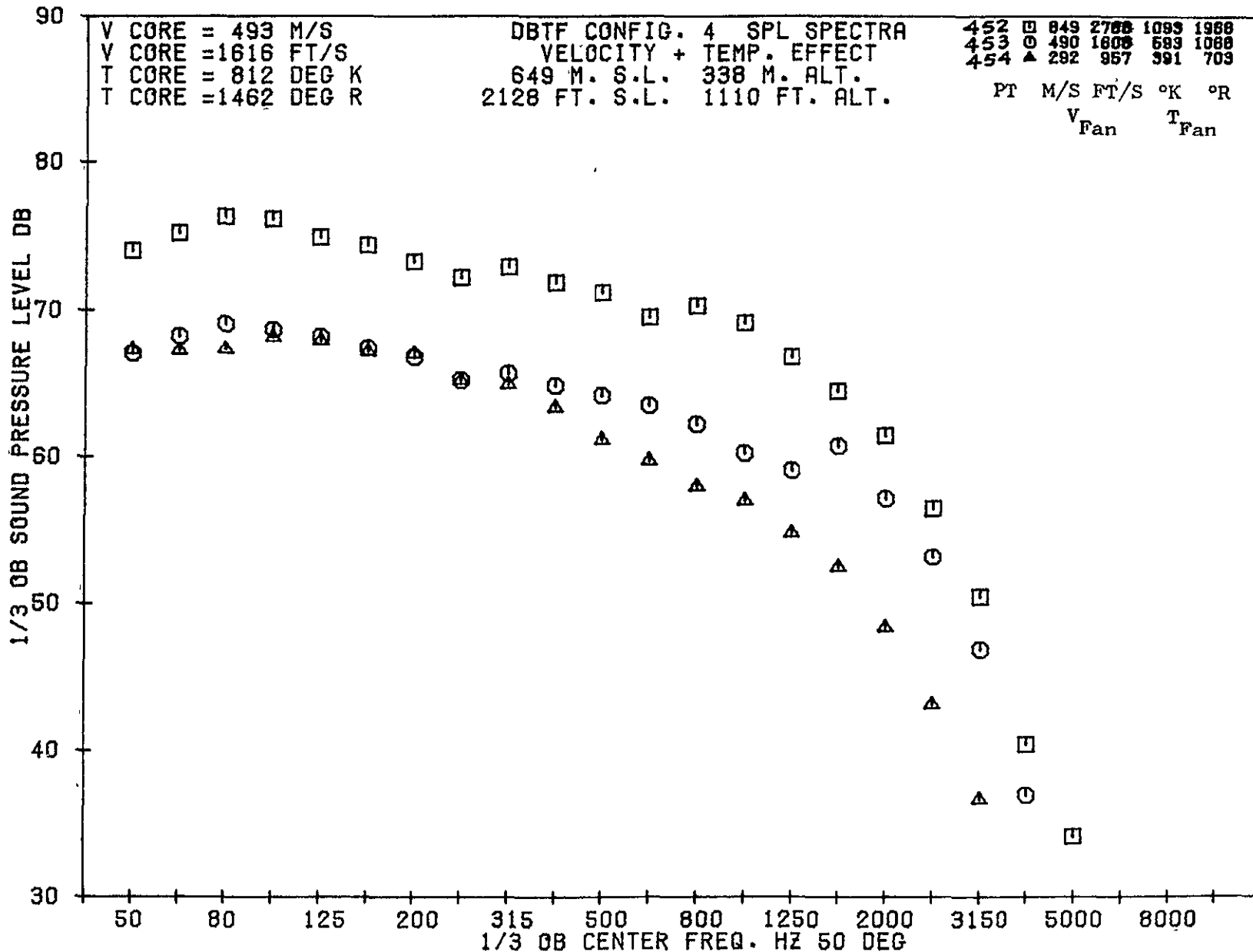
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4210

08/13/75
5R959-001

79 BURCH A.

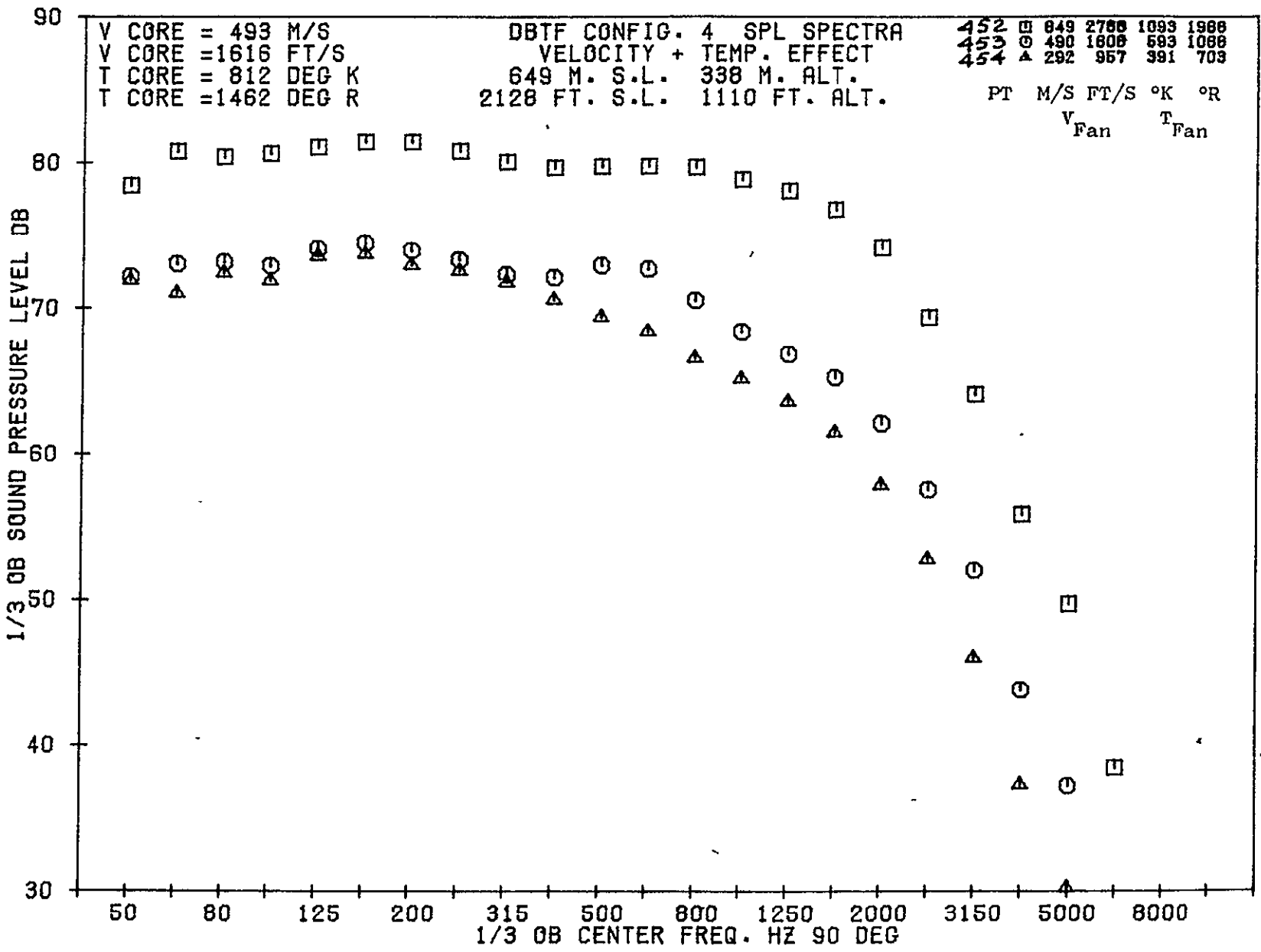
1446



4-2-77

08/13/75
5R959-001

79 BURCH A.



1447

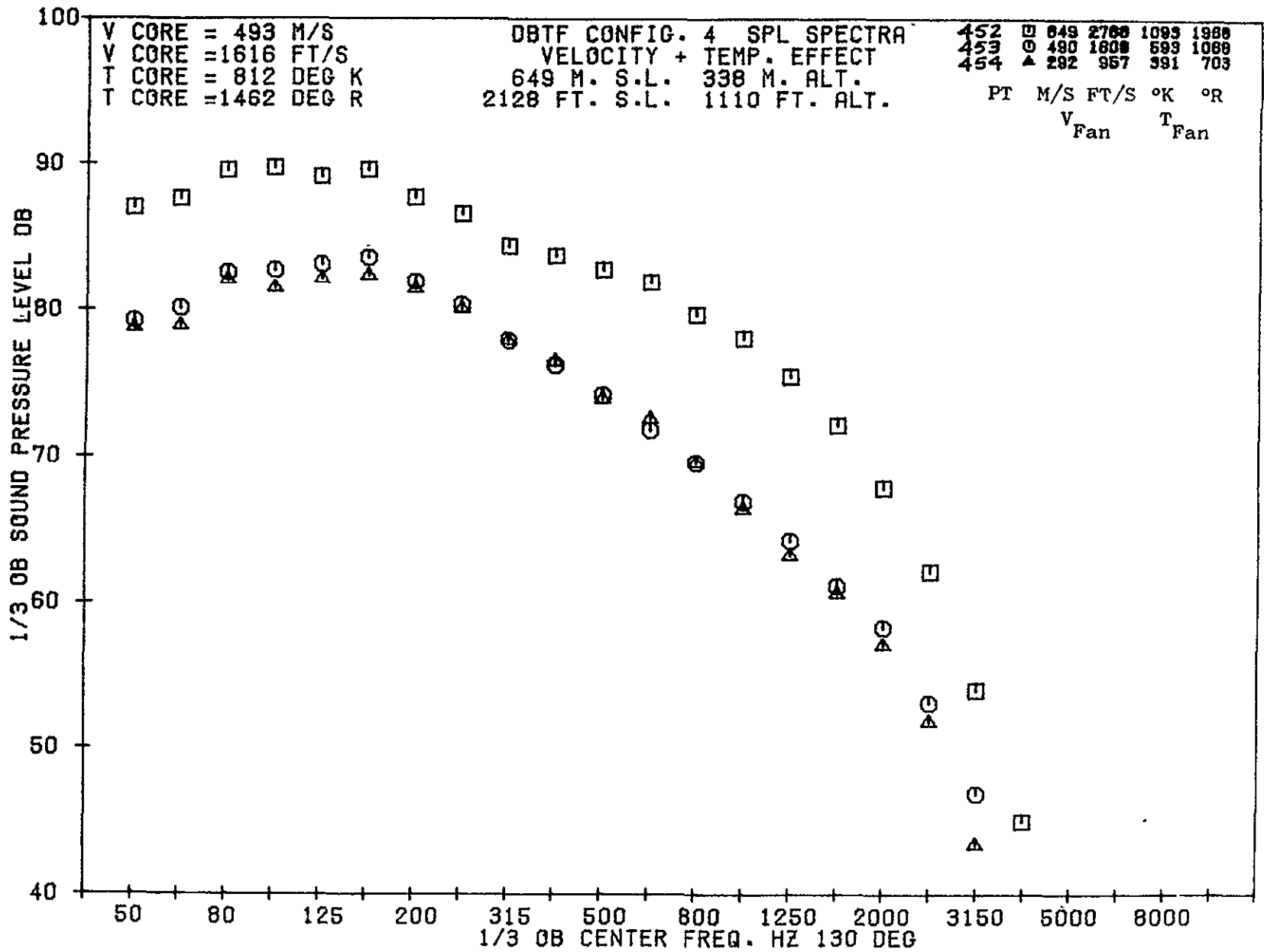
11-217

08/13/75
5R959-001

79 BURCH A.

ORIGINAL PAGE
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1448

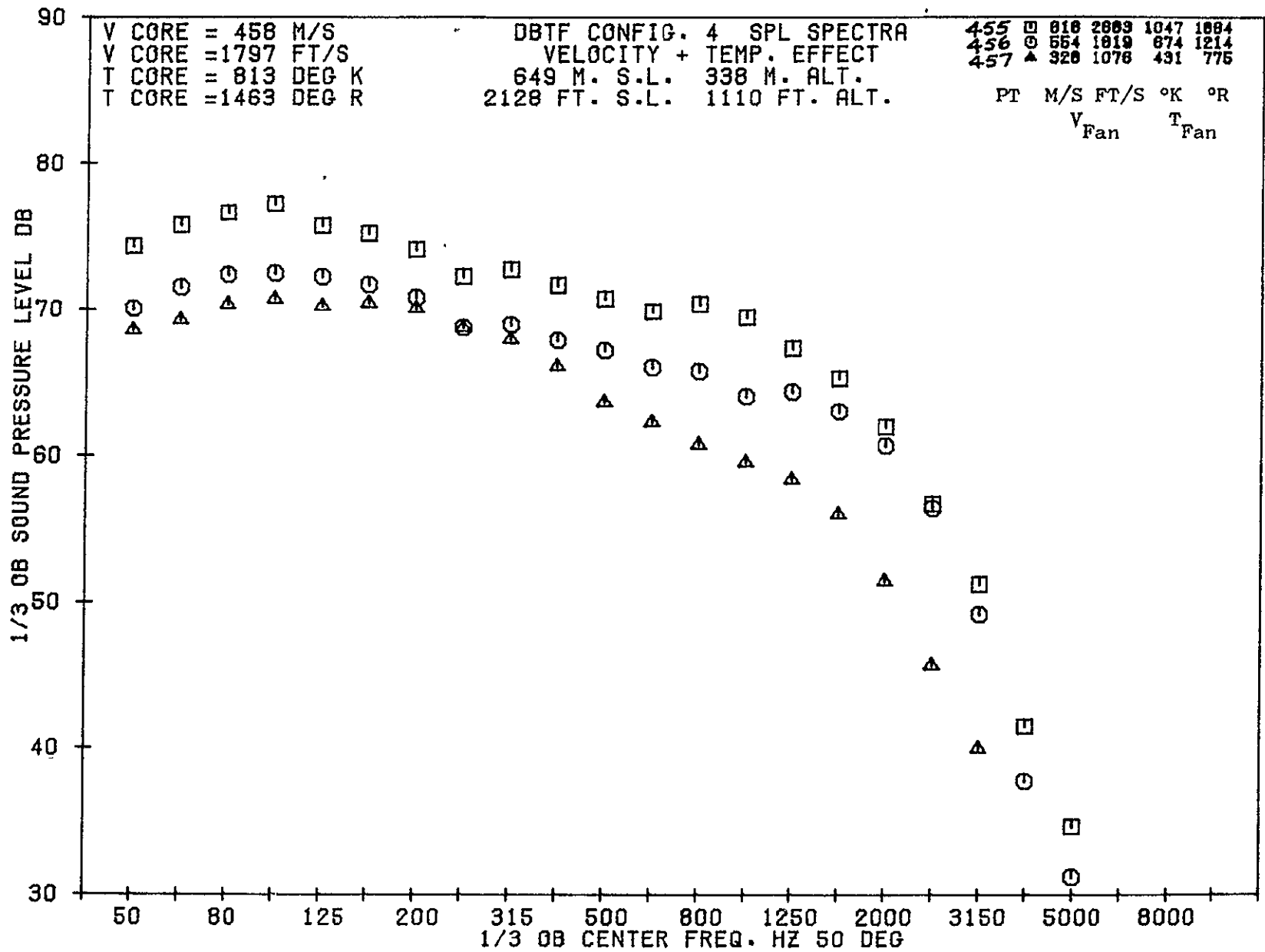


1-213

08/13/75
5R959-001

79 BURCOR.

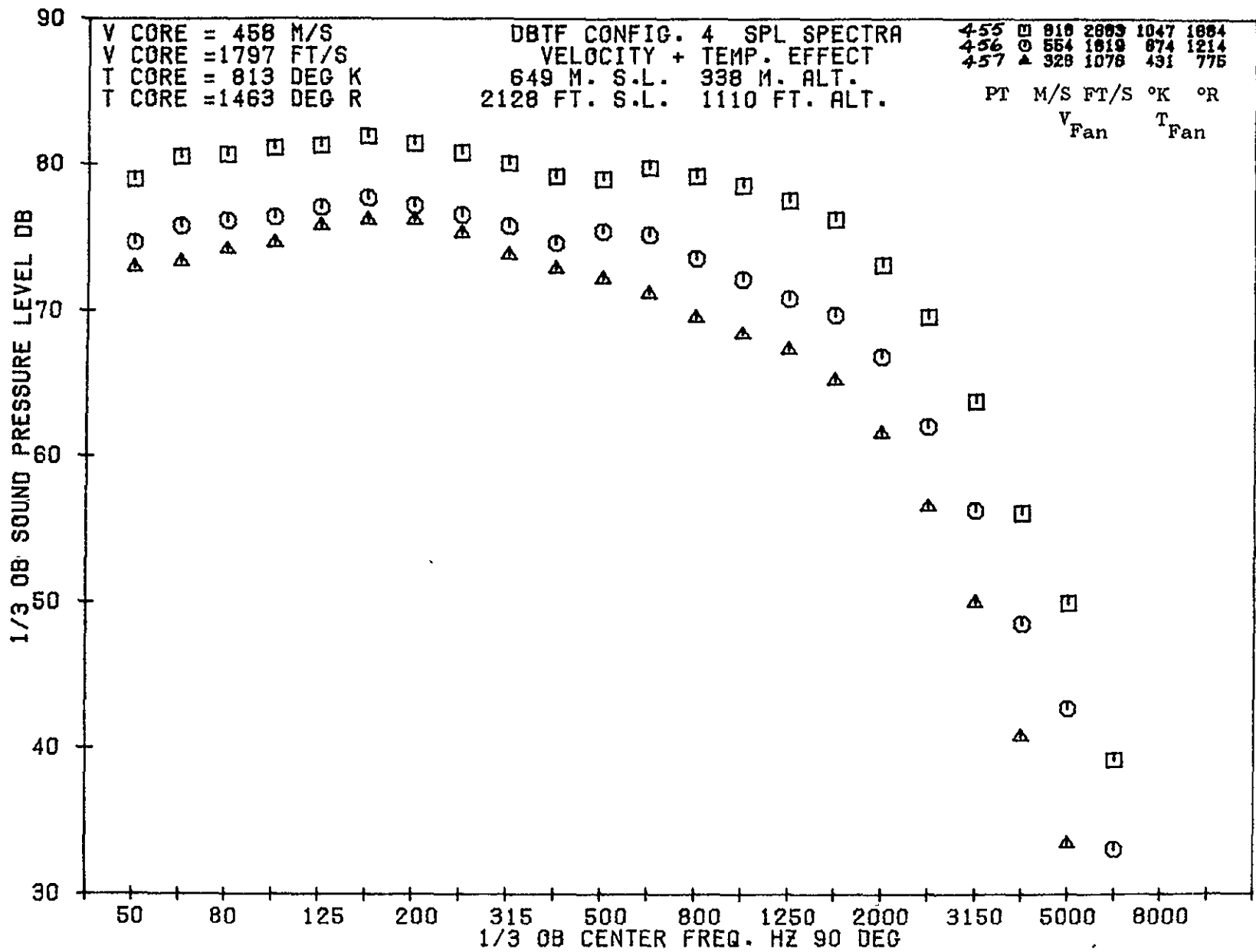
1449



08/13/75
5R959-001

79 BURCH A.

4-214

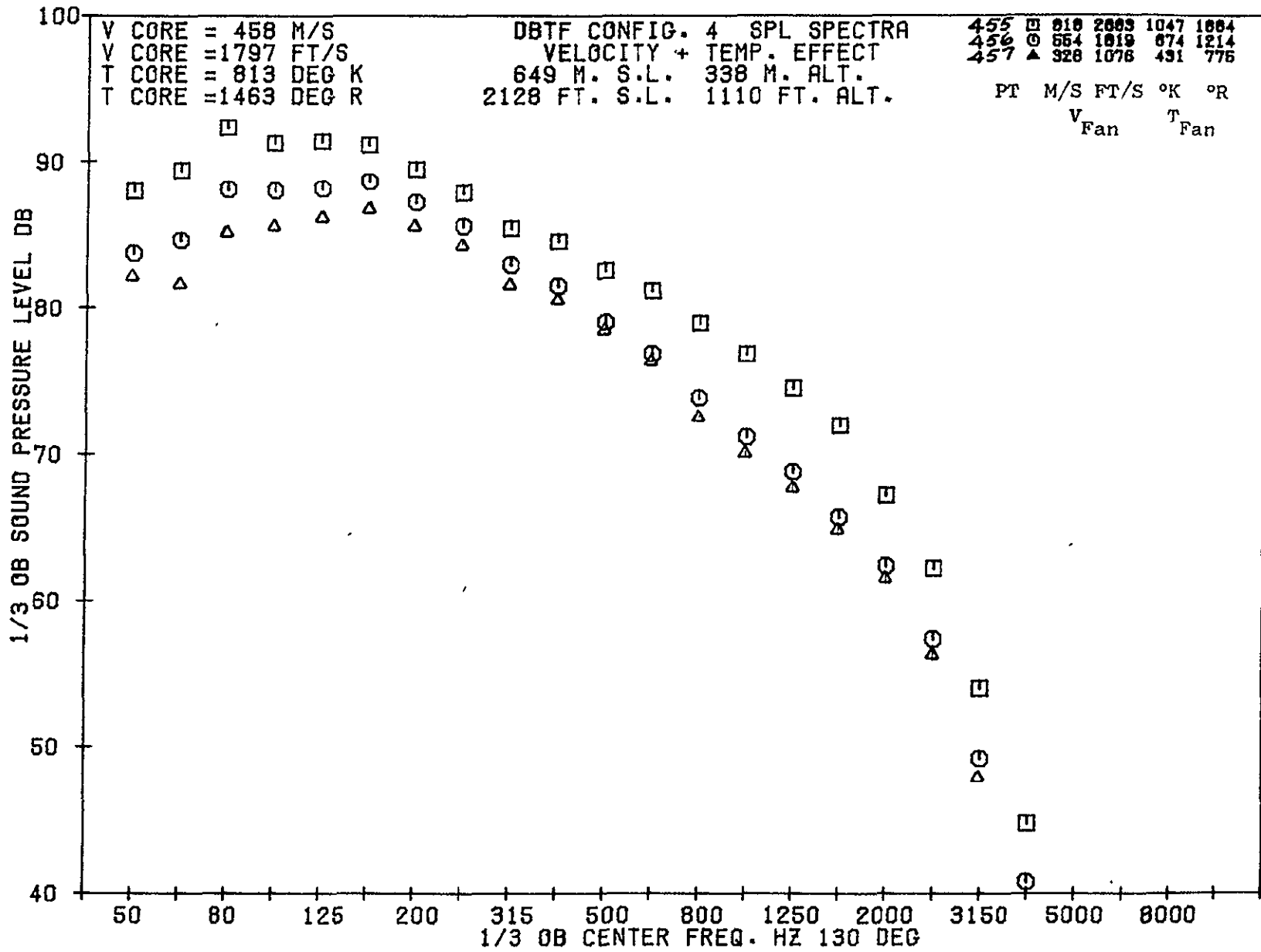


J 215

08/13/75
5R959-001

79 BURCOR.

1451



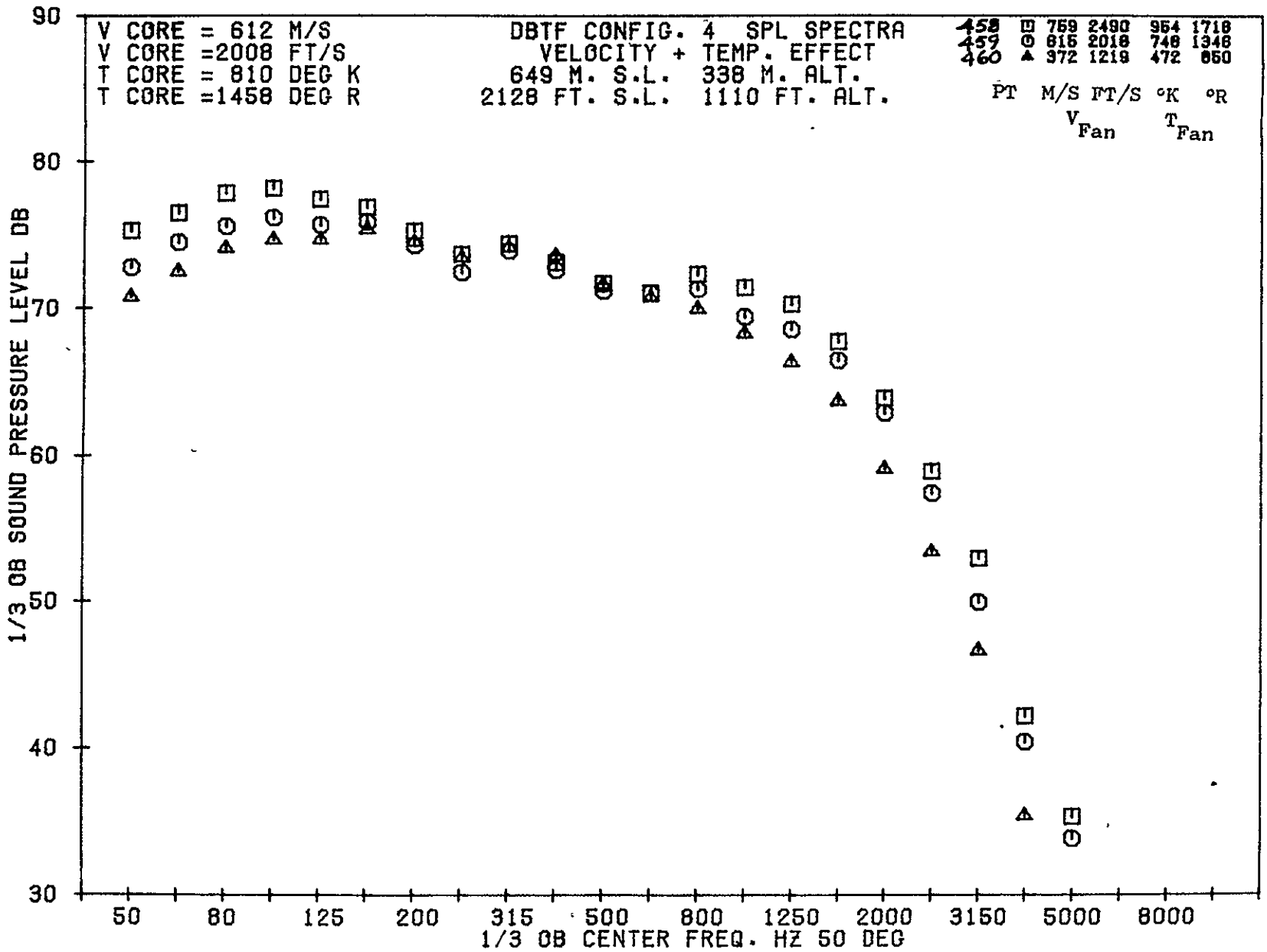
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1-216

08/13/75
5R959-001

79 BURCH A.

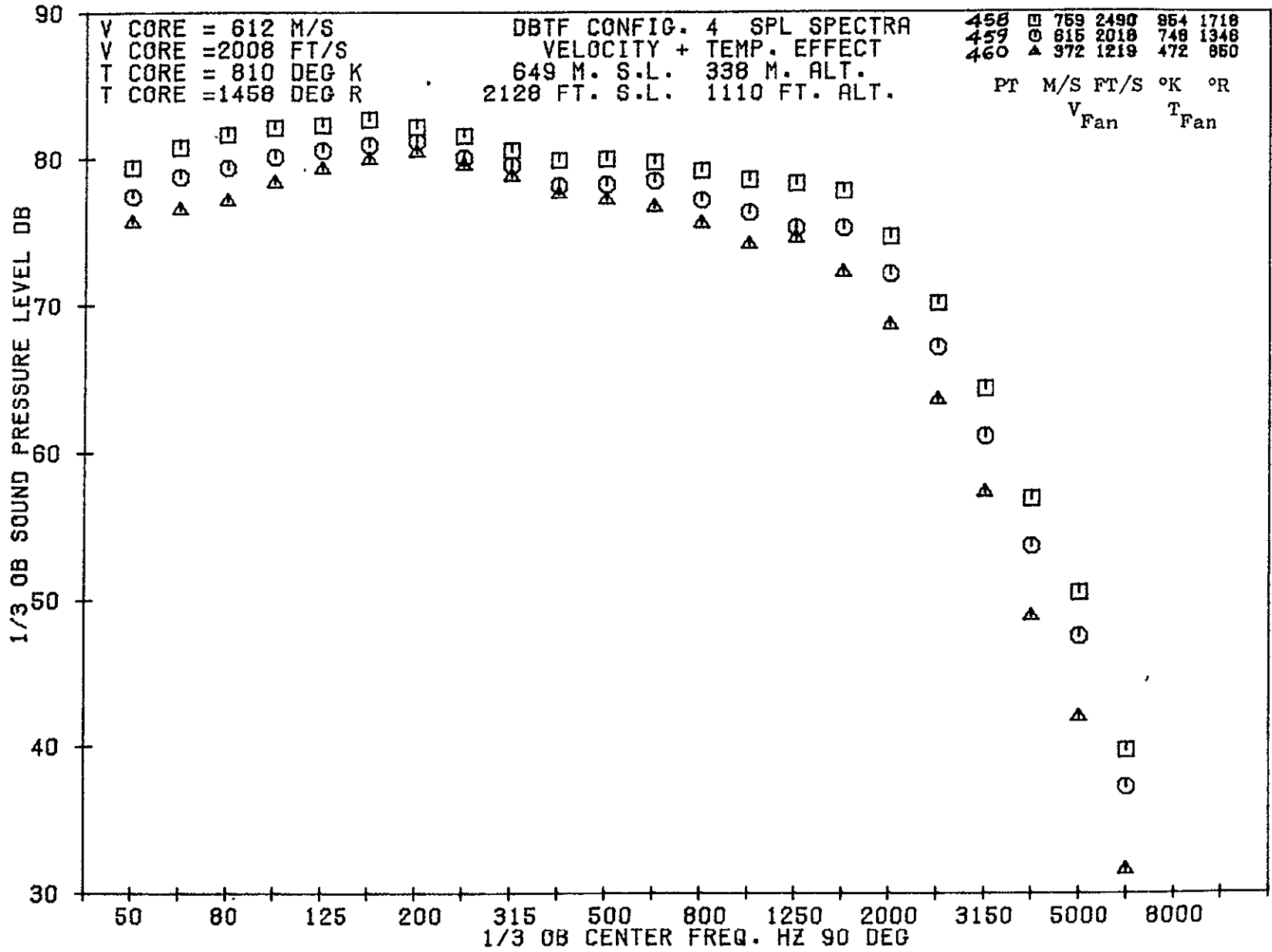
1452



1-21

08/13/75
5R959-001

79 BURC ● A.



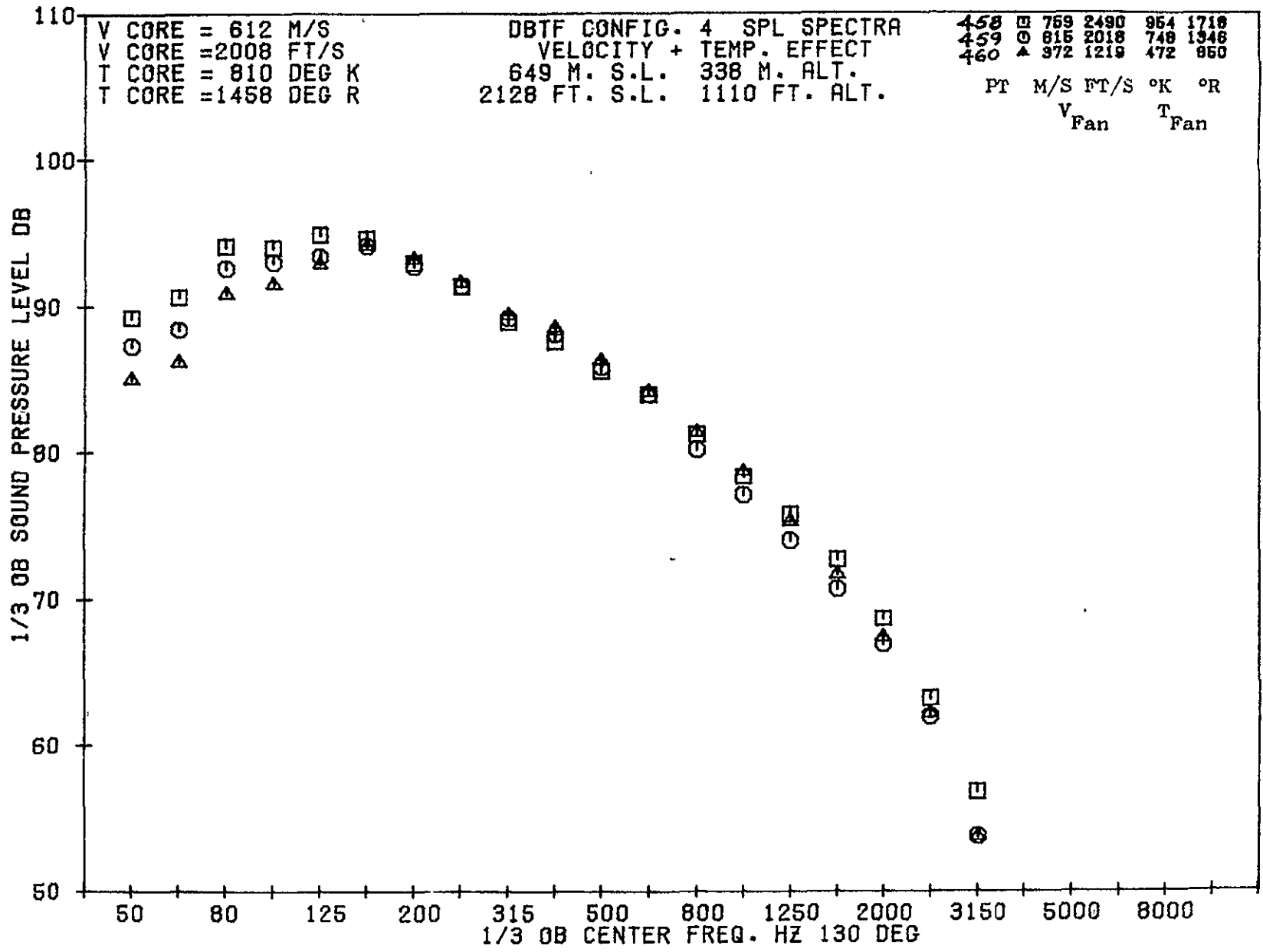
1453

4-218

08/13/75
 5R959-001

79 BURCH A.

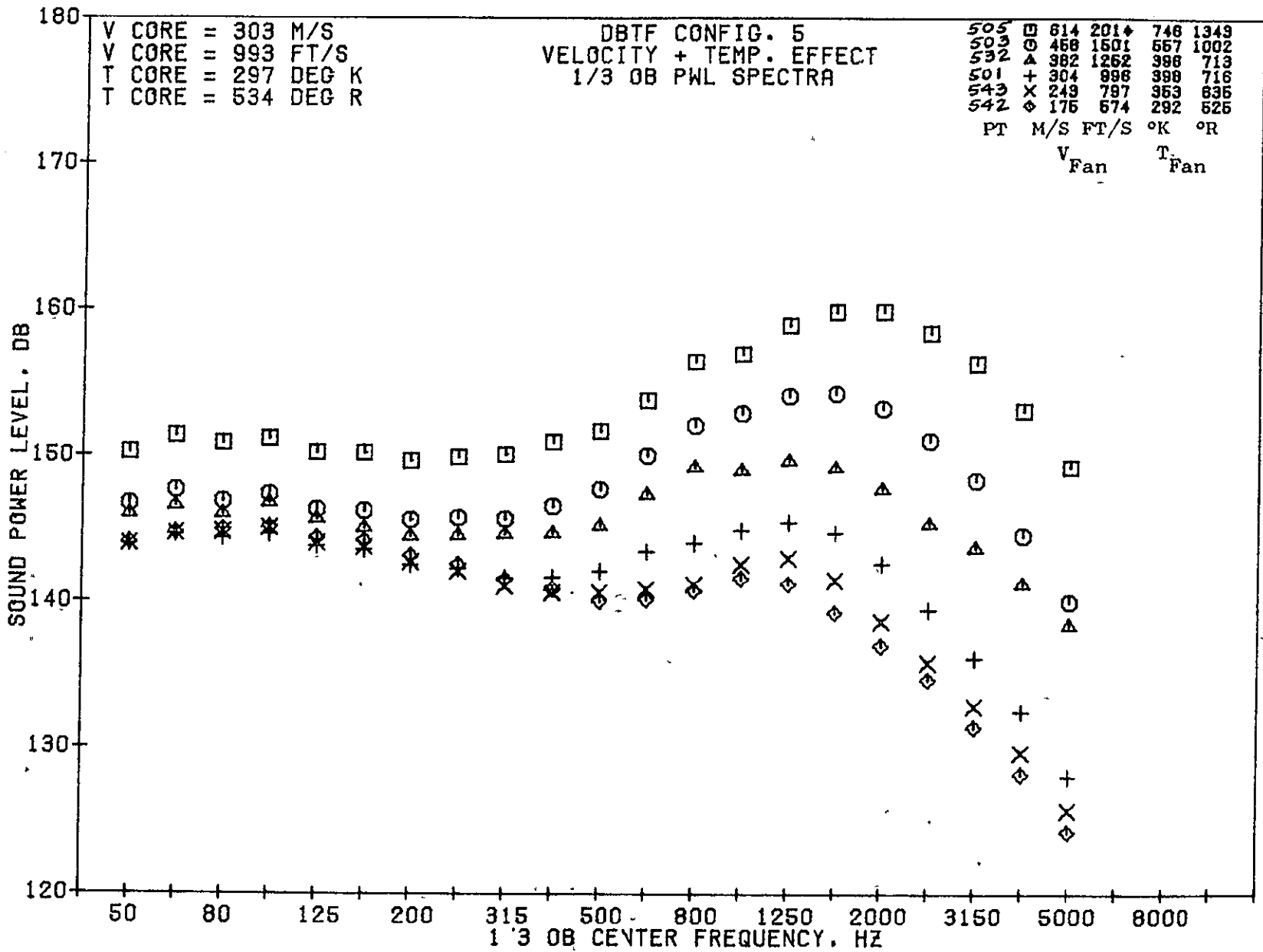
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1-2-79

08/13/75
 5R959-001

79 BURC

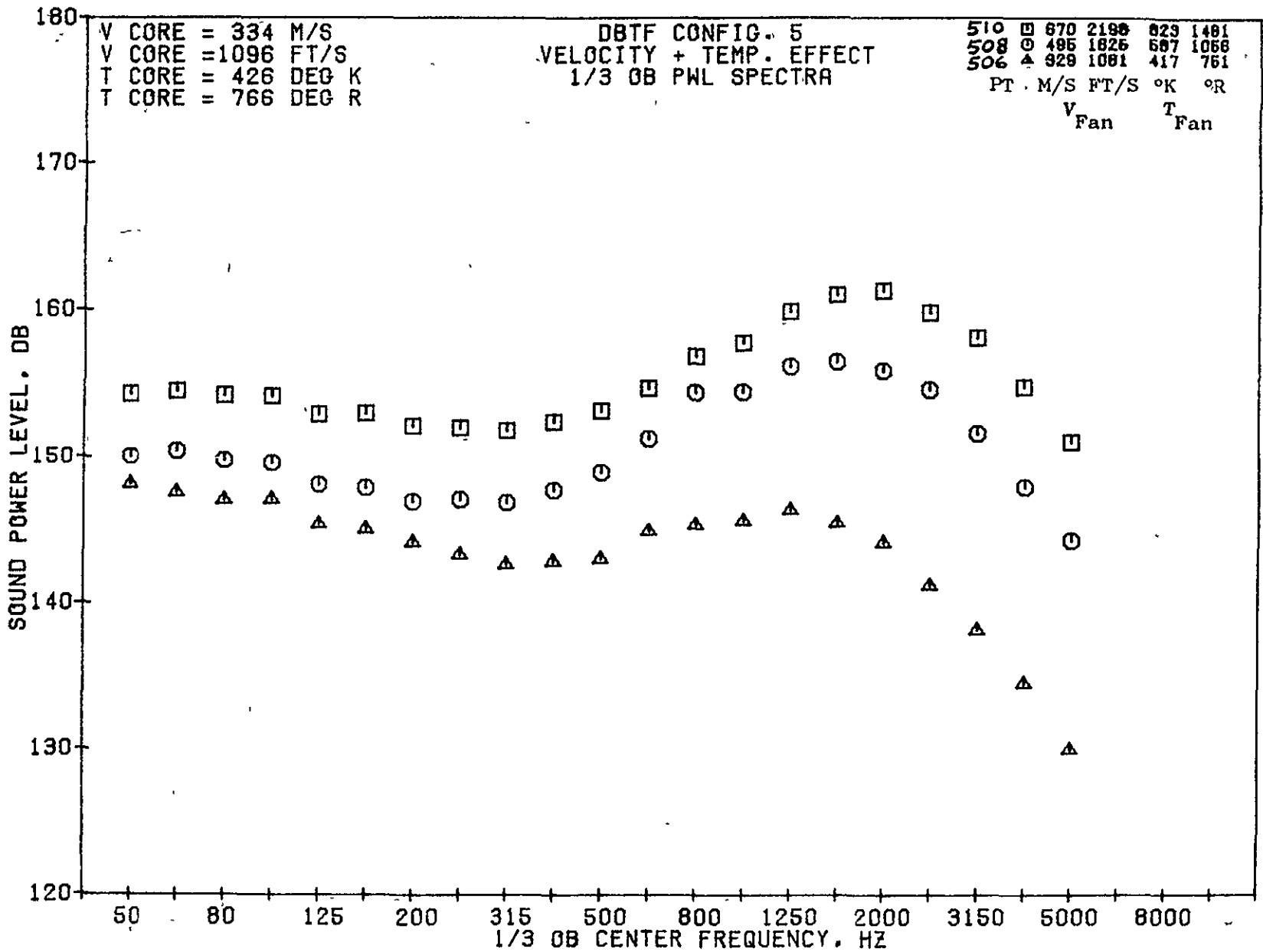


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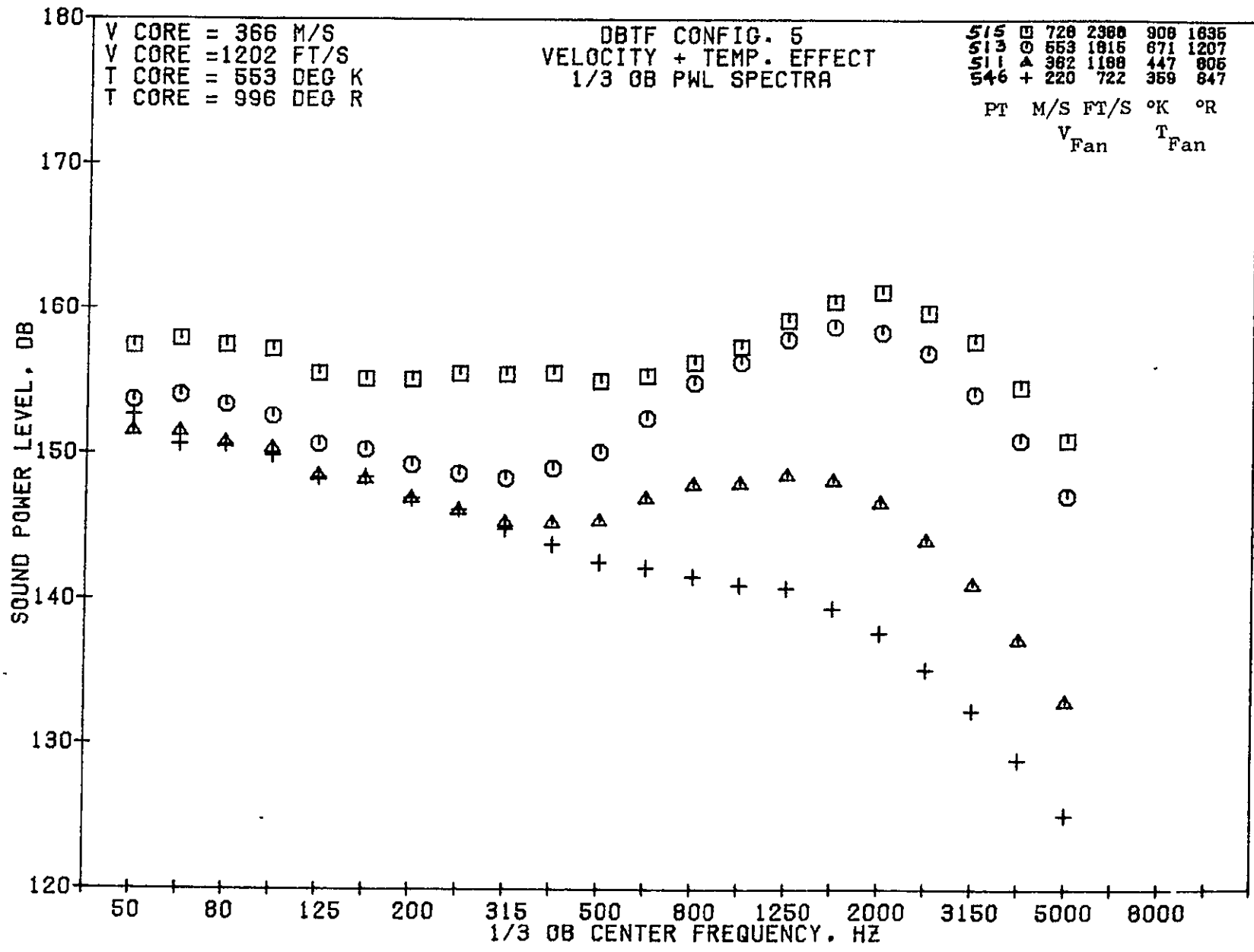
79 BURCH A.

1220



08/13/75
 5R947-001

79 BUR A.



1457

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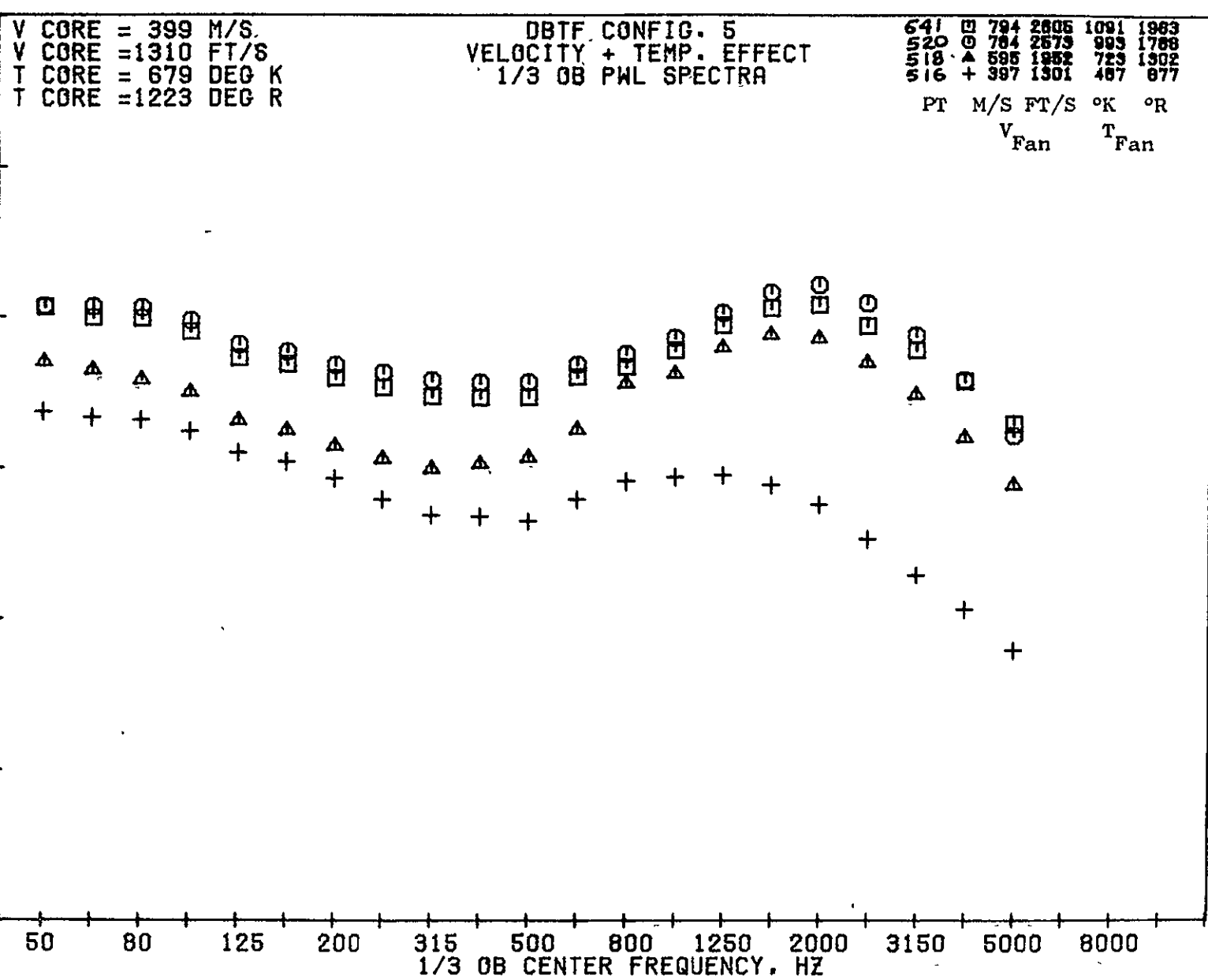
11-2222

08/13/75
5R947-001

79 BURCH A.

1458

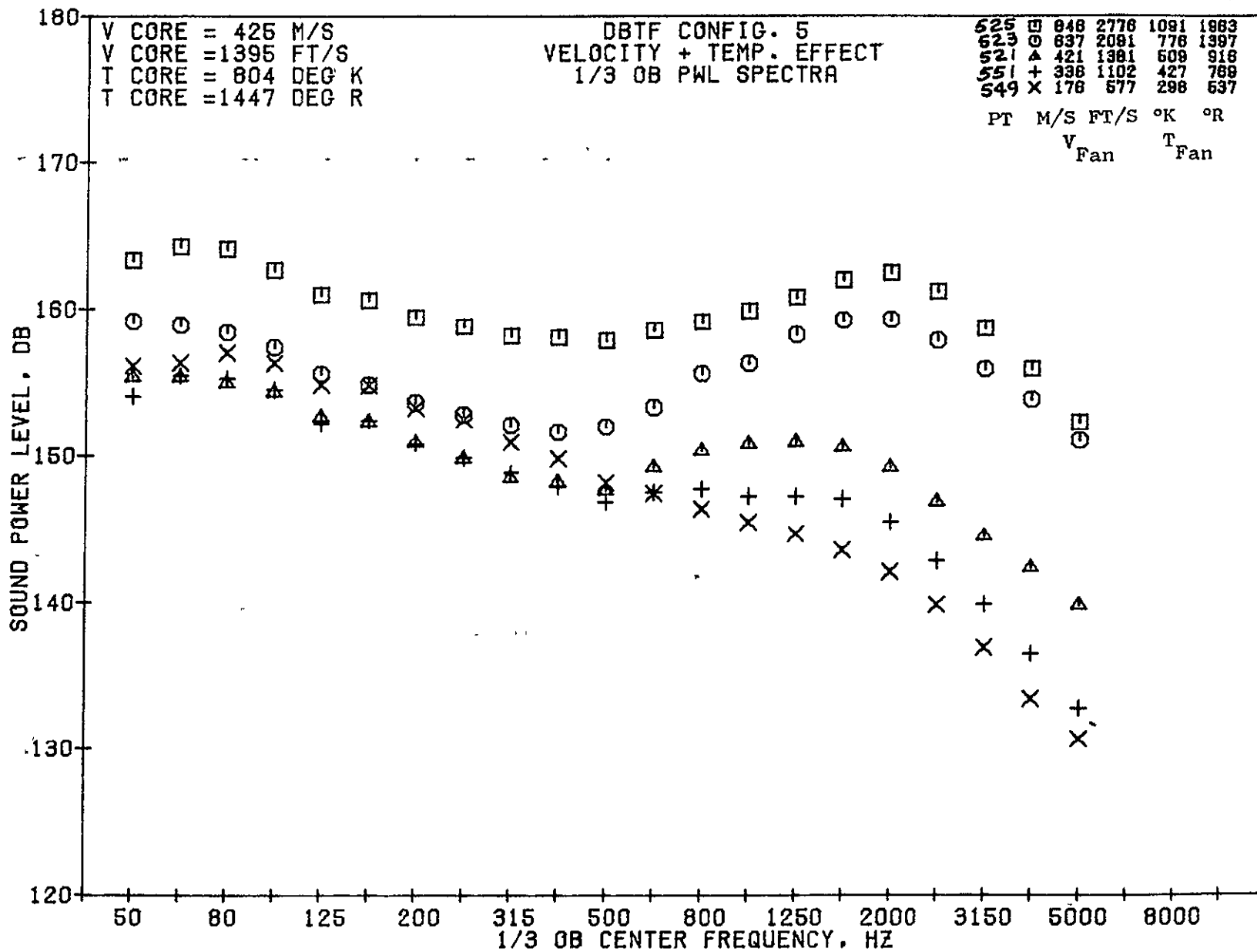
SOUND POWER LEVEL, DB



L.223

08/20/75
5R552-001

79 BURCH A.



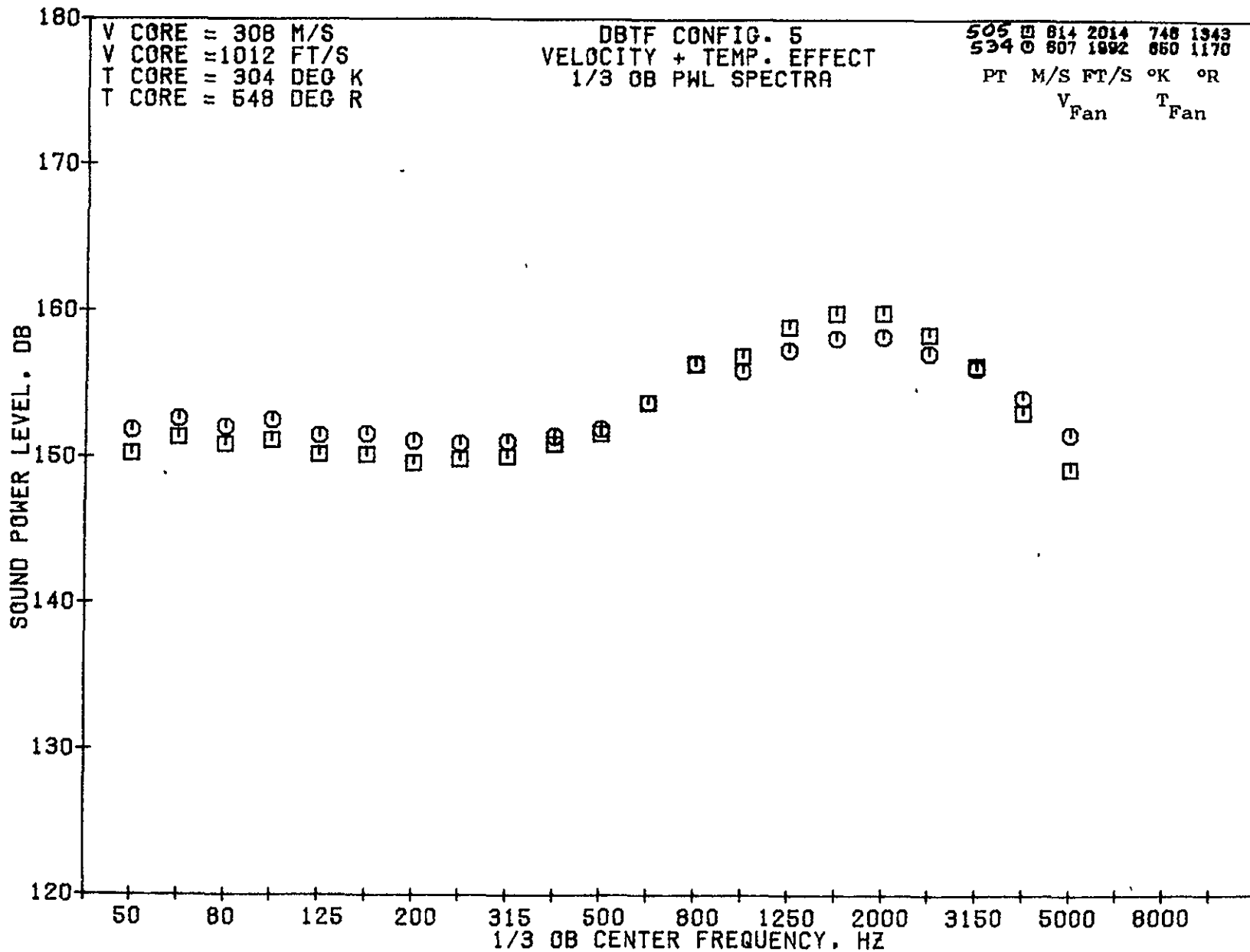
1459

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5R947-001

79 BURCH A.

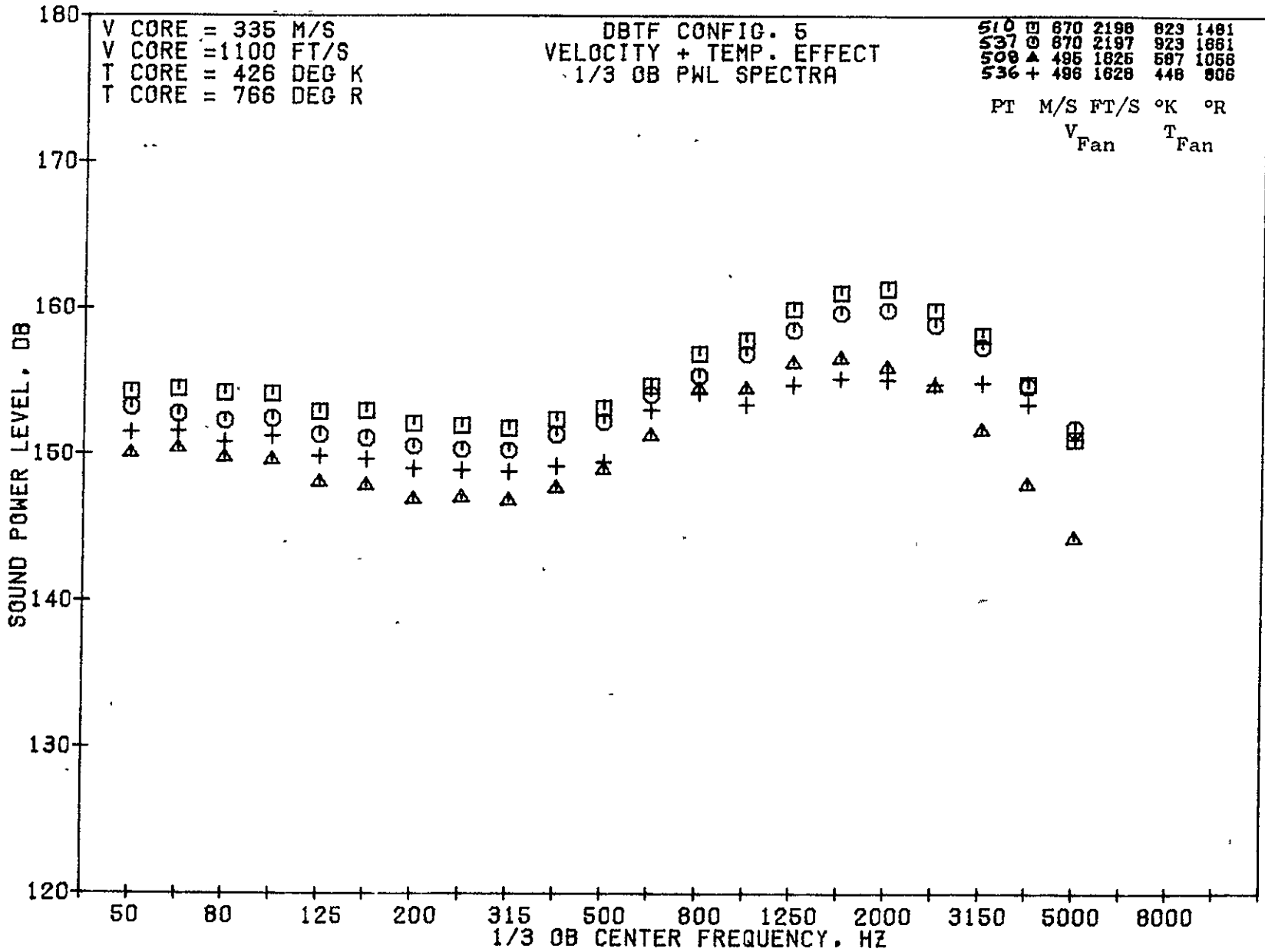
4-224



11-225

08/13/75
 5R947-001

79 BUR A.



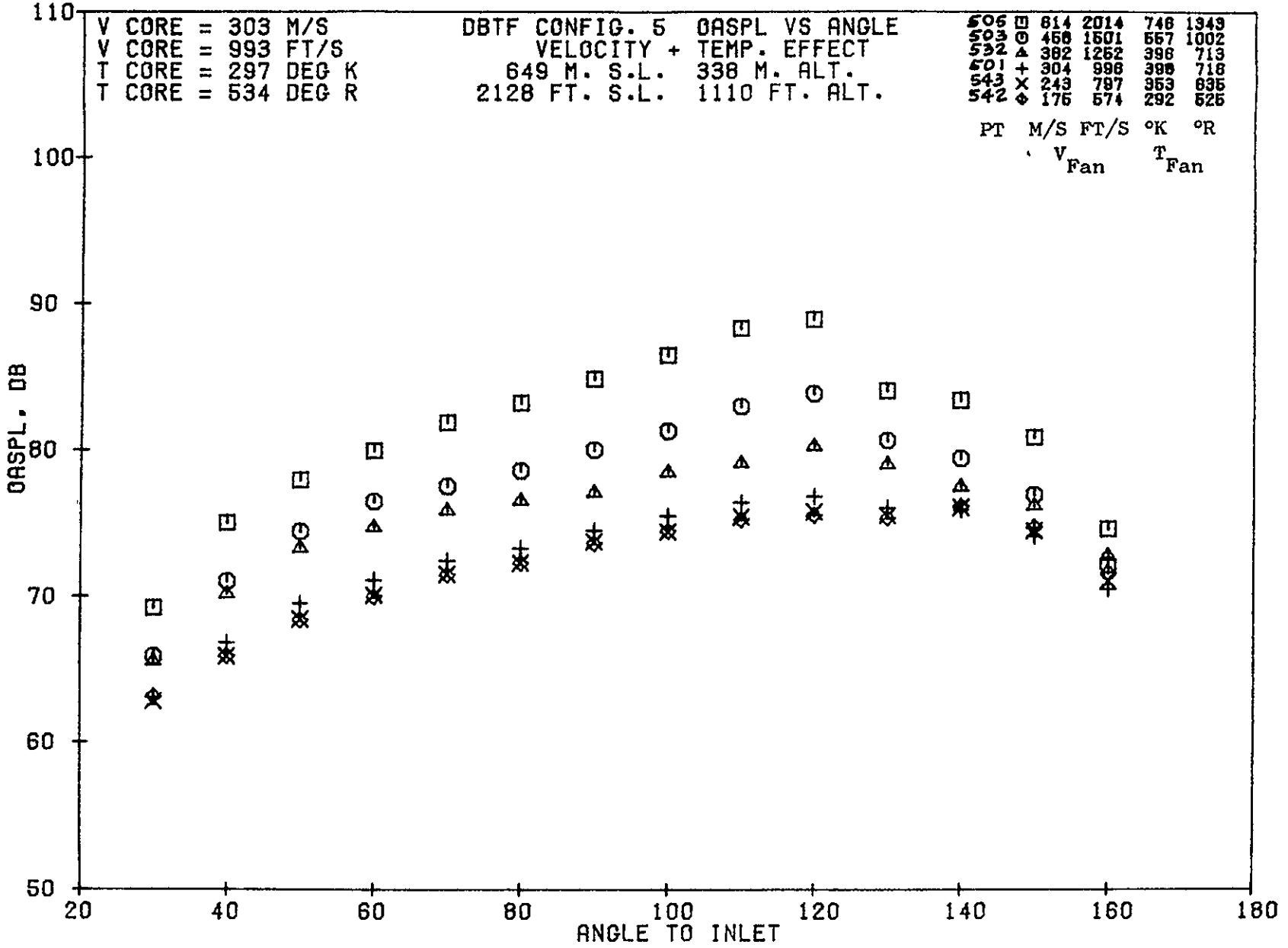
1461

4-226

08/13/75
5R947-001

79 BURCH A.

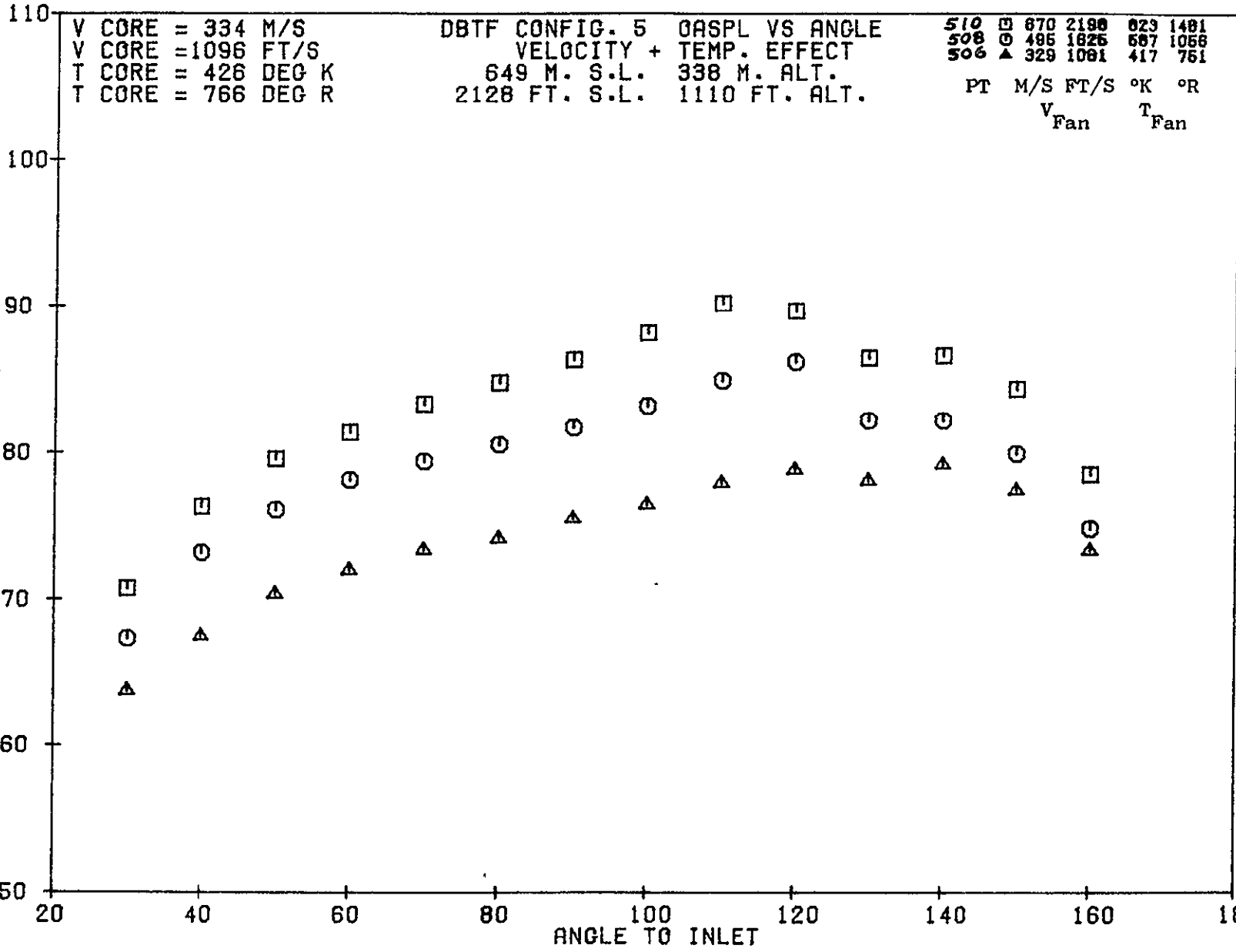
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1.229

08/13/75
5R947-001

79 BURQA



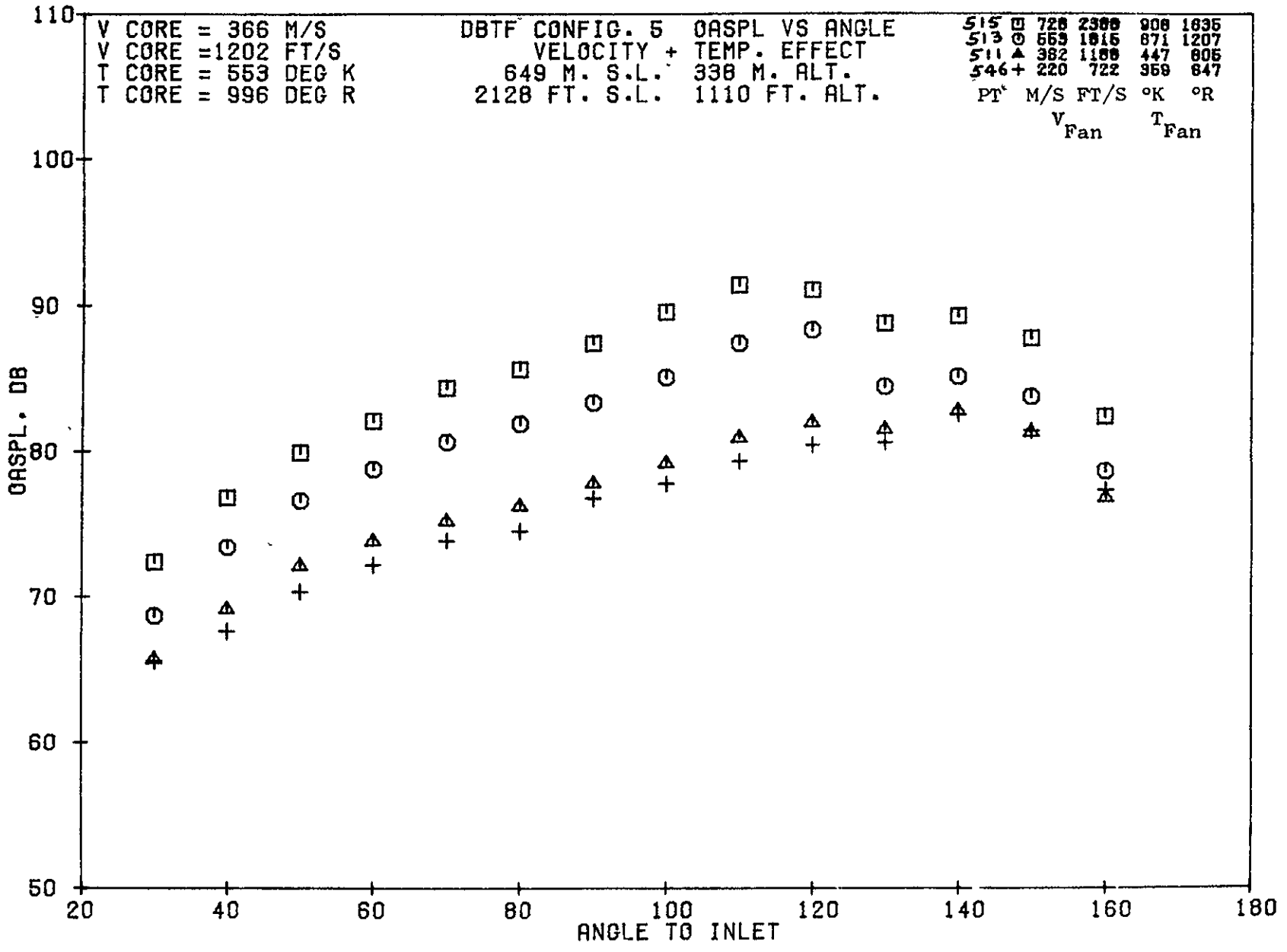
1463

4-228

08/13/75
 5R947-001

79 BURCH A.

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1464

W-229

08/13/75
5R947-001

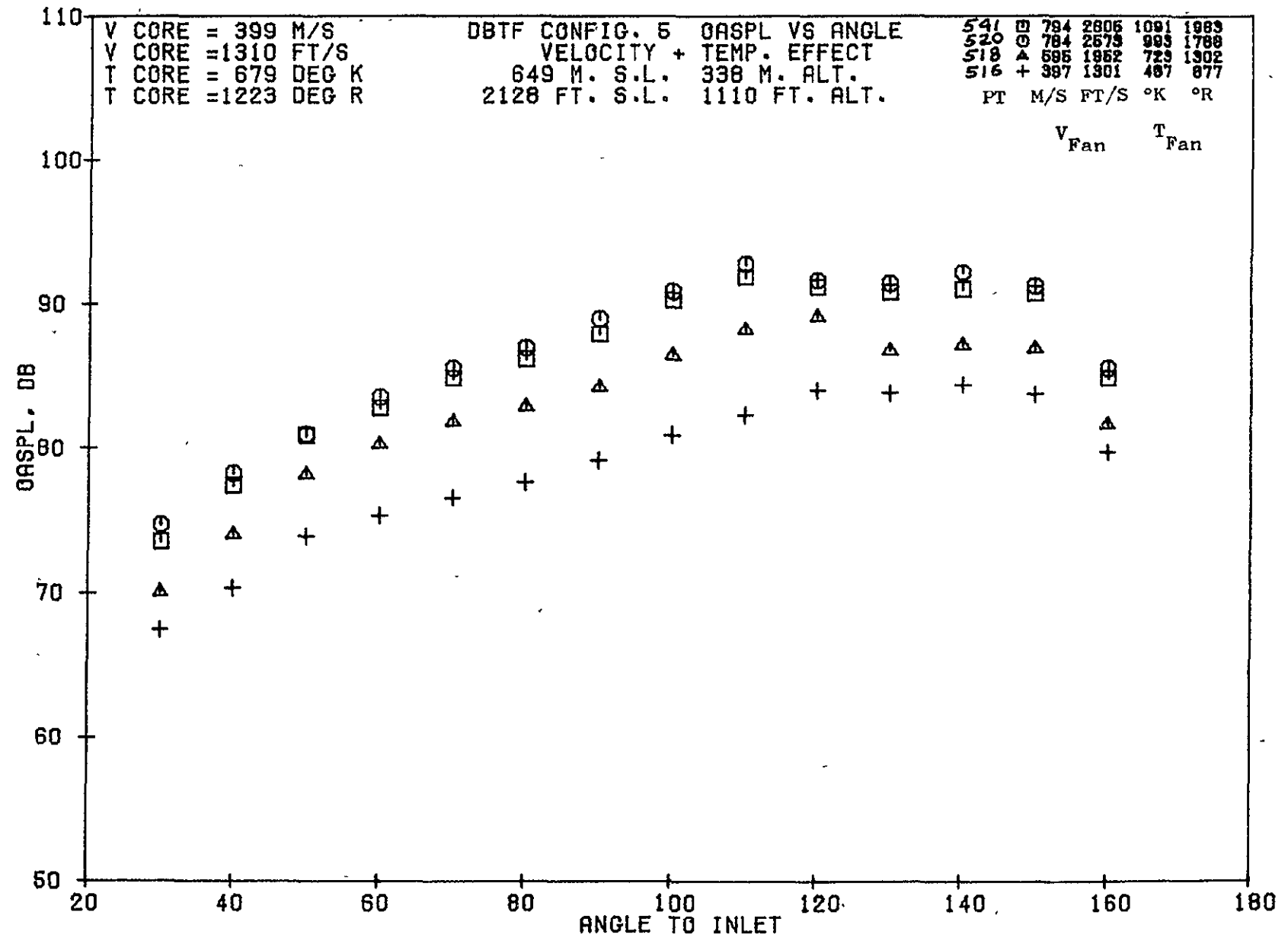
79 BURQA.

V CORE = 399 M/S
 V CORE = 1310 FT/S
 T CORE = 679 DEG K
 T CORE = 1223 DEG R

DBTF CONFIG. 5 OASPL VS ANGLE
 VELOCITY + TEMP. EFFECT
 649 M. S.L. 338 M. ALT.
 2128 FT. S.L. 1110 FT. ALT.

PT	M/S	FT/S	°K	°R
541	794	2606	1091	1983
520	784	2573	993	1788
518	695	1962	729	1302
516	397	1301	487	877

V_{Fan} T_{Fan}



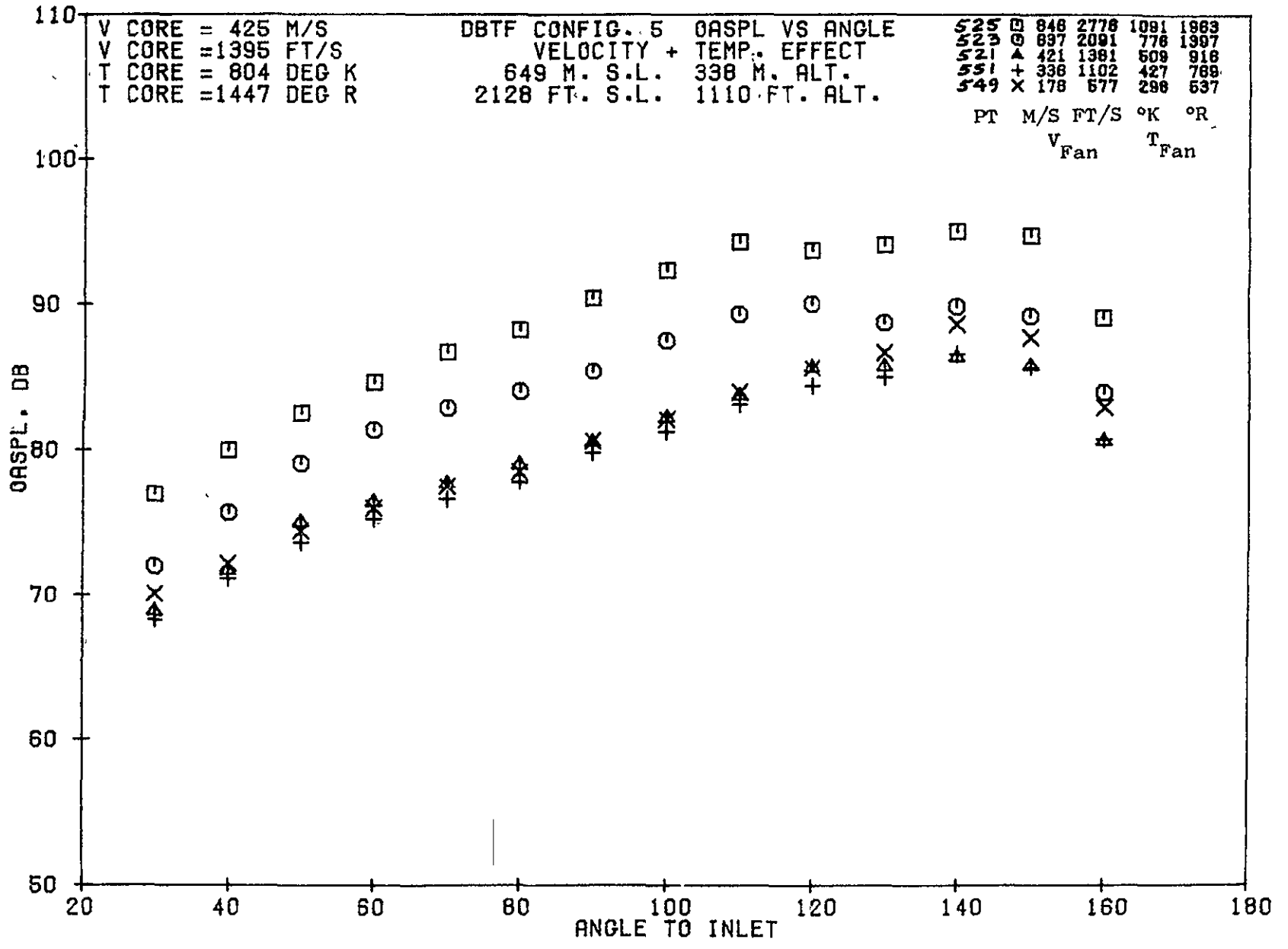
1465

4.230

08/20/75
5R552-001

79 BURCH A.

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1466

15231

08/13/75
 5R947-001

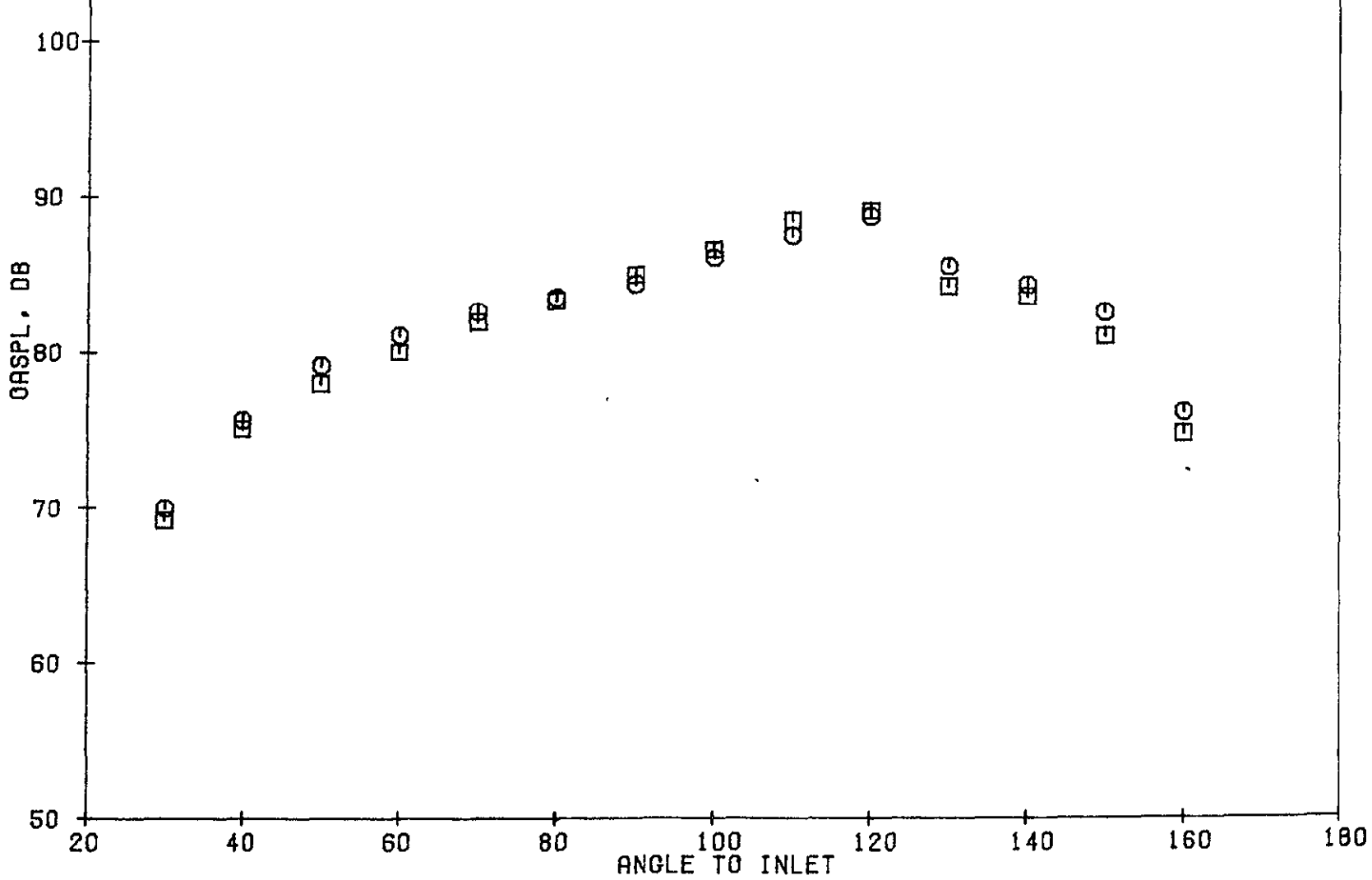
79 BURGLA.

V CORE = 308 M/S
 V CORE = 1012 FT/S
 T CORE = 304 DEG K
 T CORE = 548 DEG R

DBTF CONFIG. 5 GASPL VS ANGLE
 VELOCITY + TEMP. EFFECT
 649 M. S.L. 338 M. ALT.
 2128 FT. S.L. 1110 FT. ALT.

505 @ 814 2014 748 1343
 534 @ 807 1992 860 1170

PT M/S FT/S °K °R
 V_{Fan} T_{Fan}



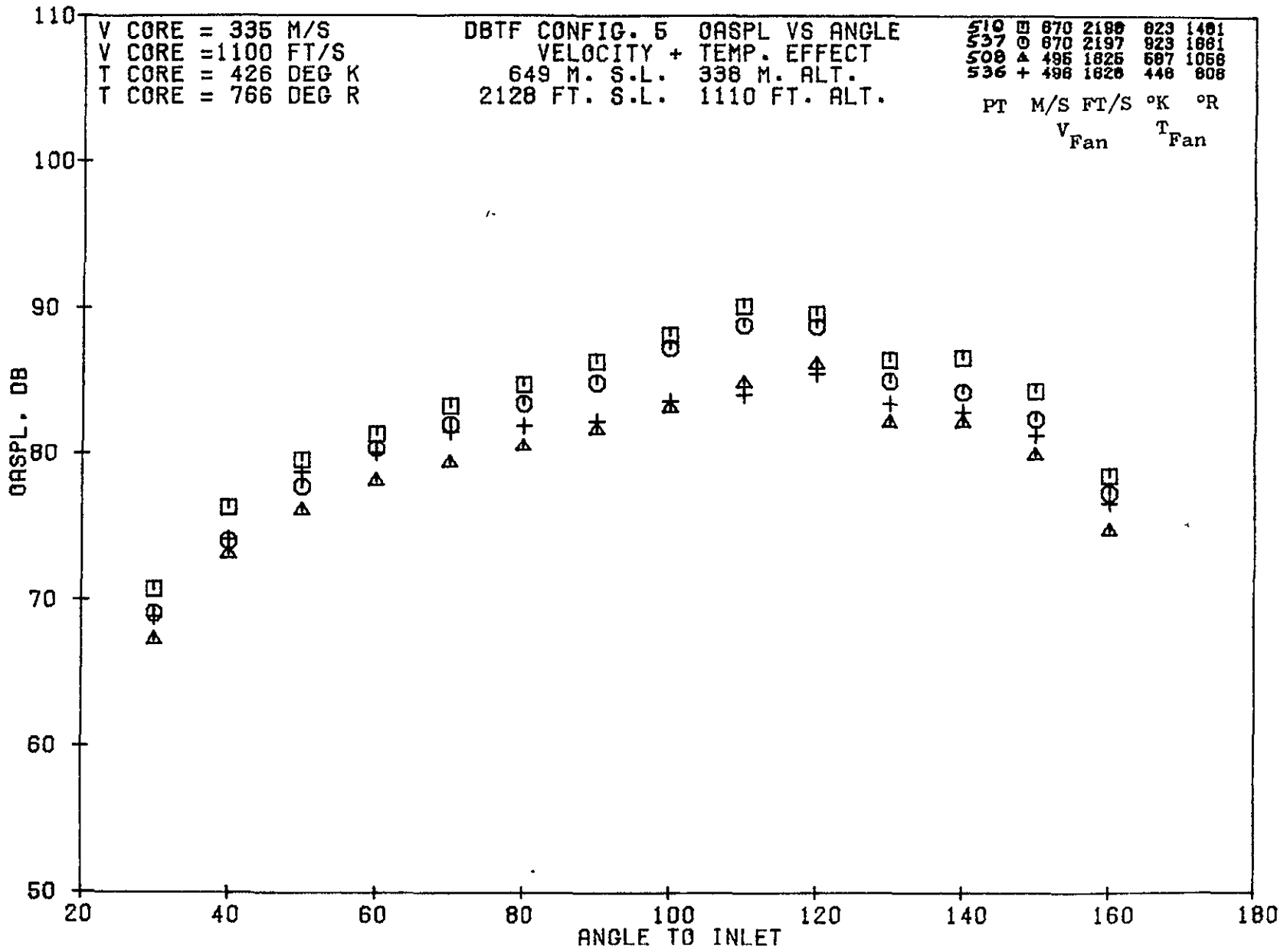
1467

11.23V

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5R947-001

79 BURCH A.

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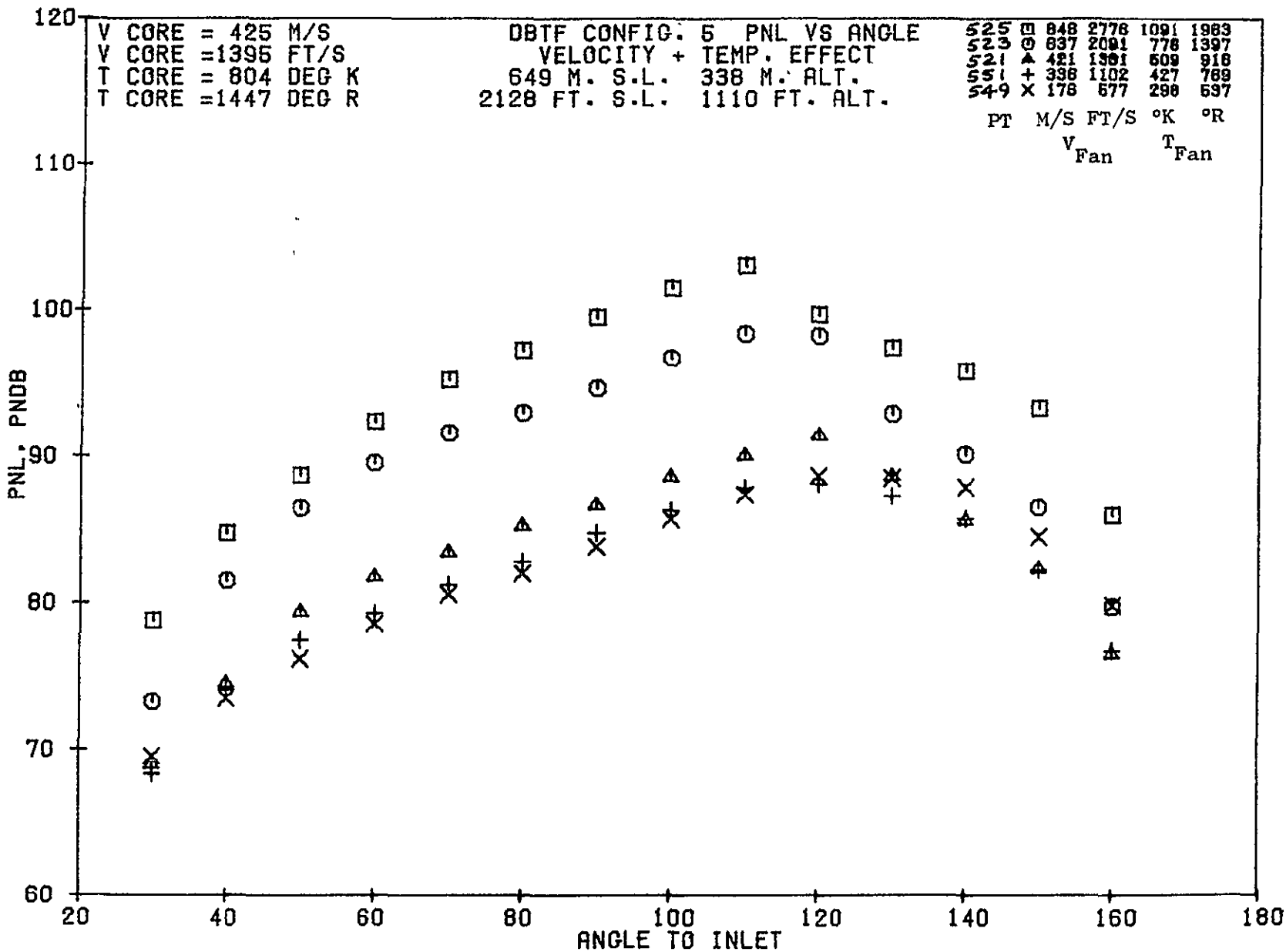
1468

J-233

08/13/75
 5R947-001

79 BURCH A.

1469

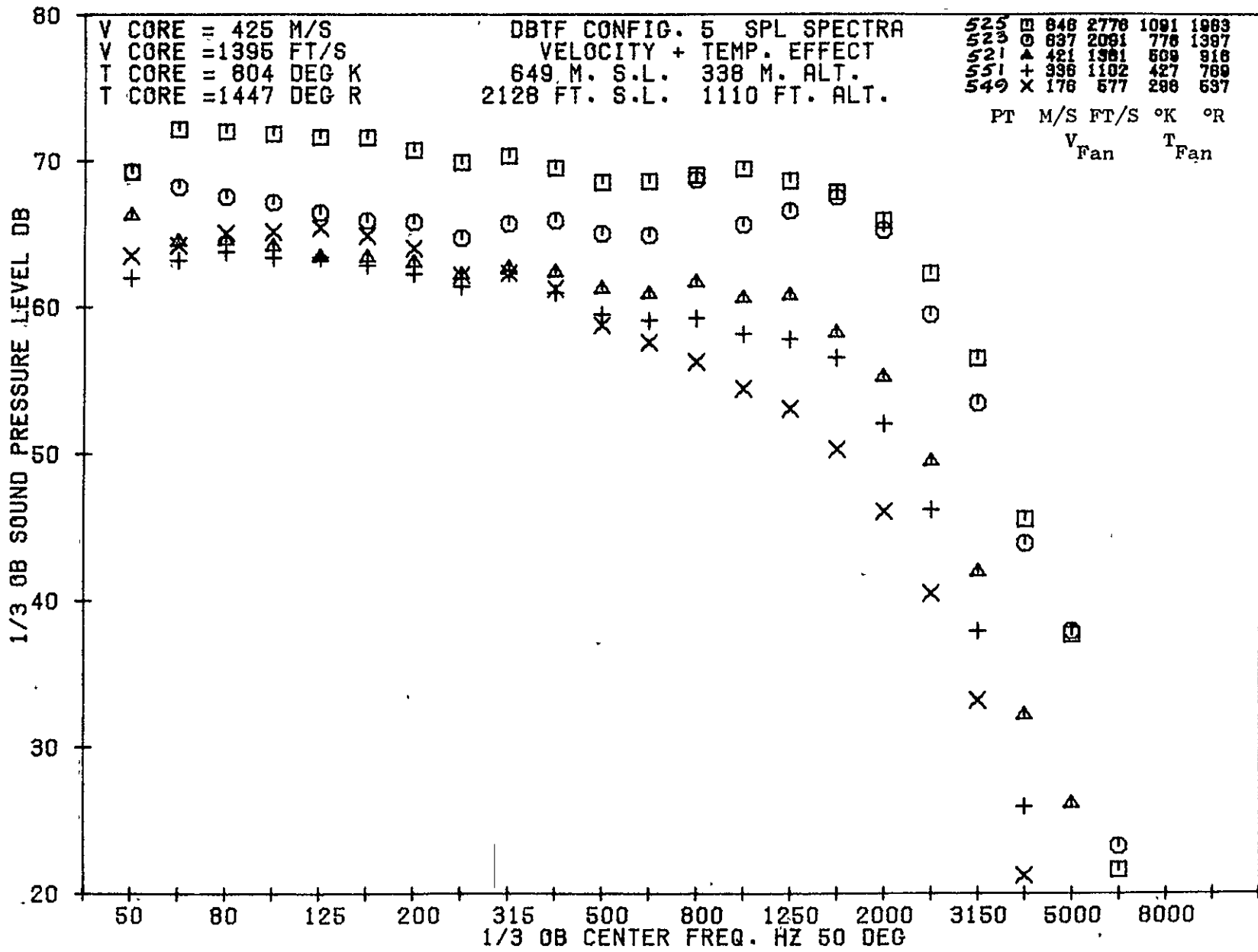


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79 BURCH A.

U-134

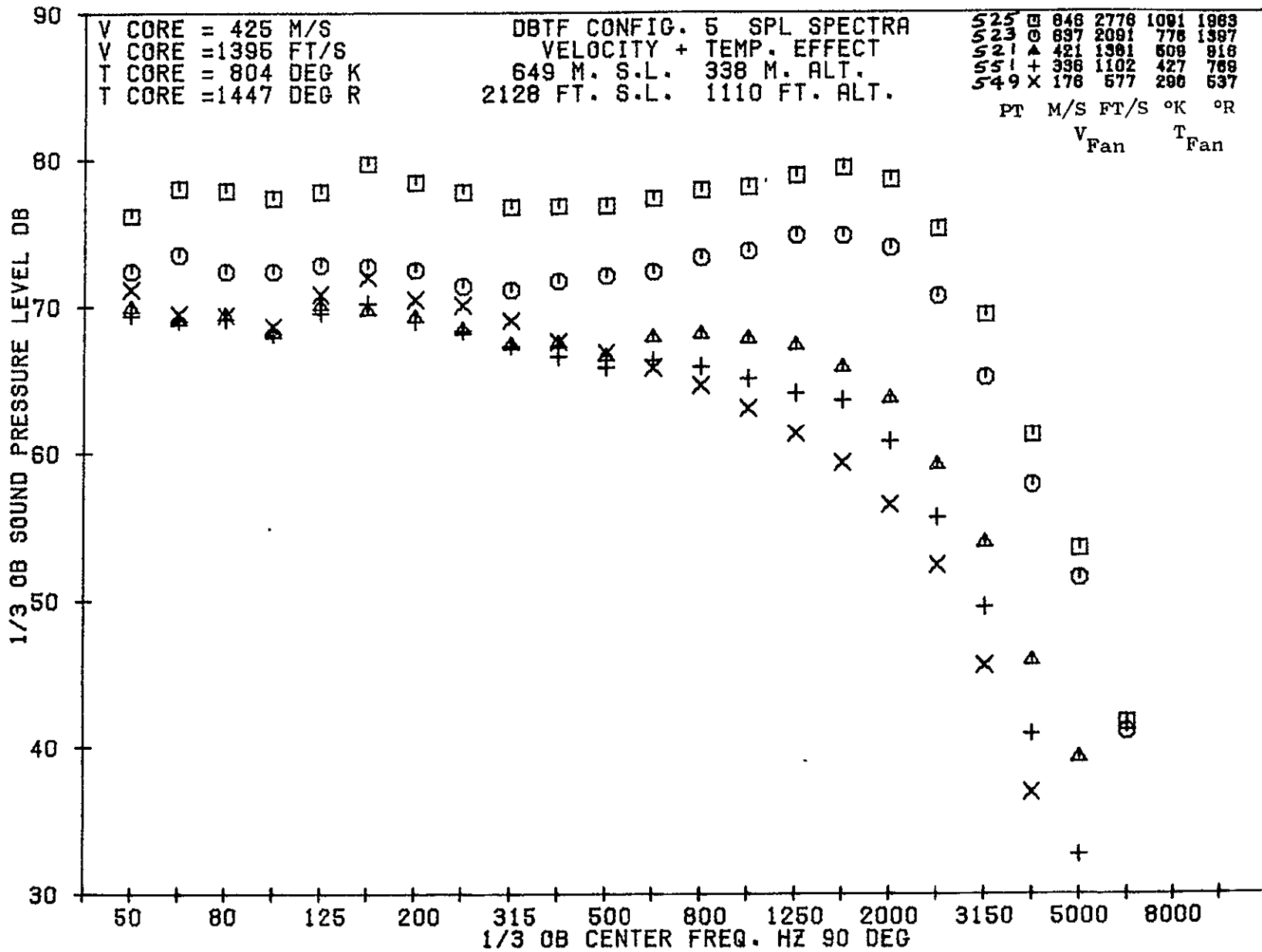


4-235

08/20/75
5R552-001

79 BURCH A.

1471

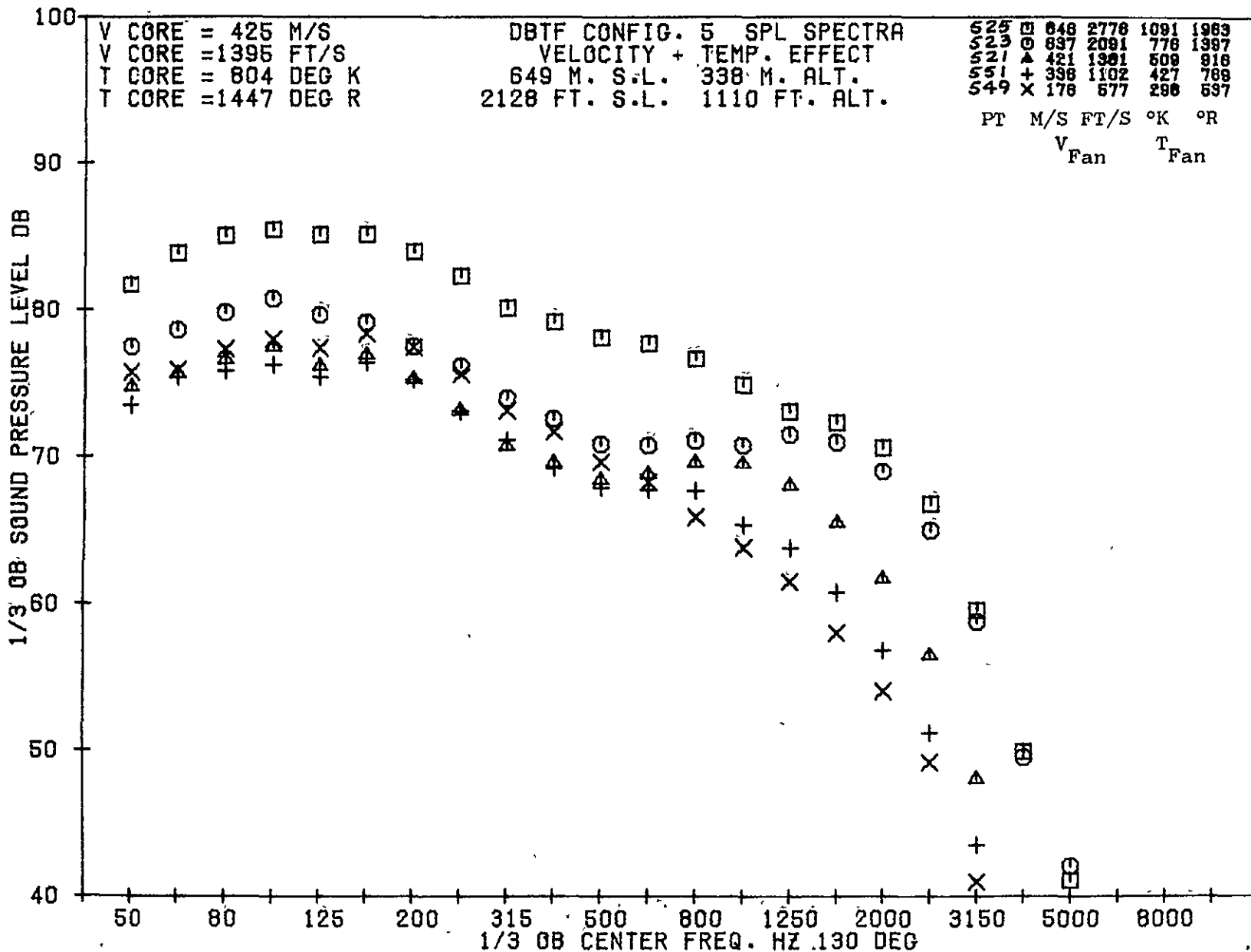


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5R552-001

79 BURCH A.

4-236

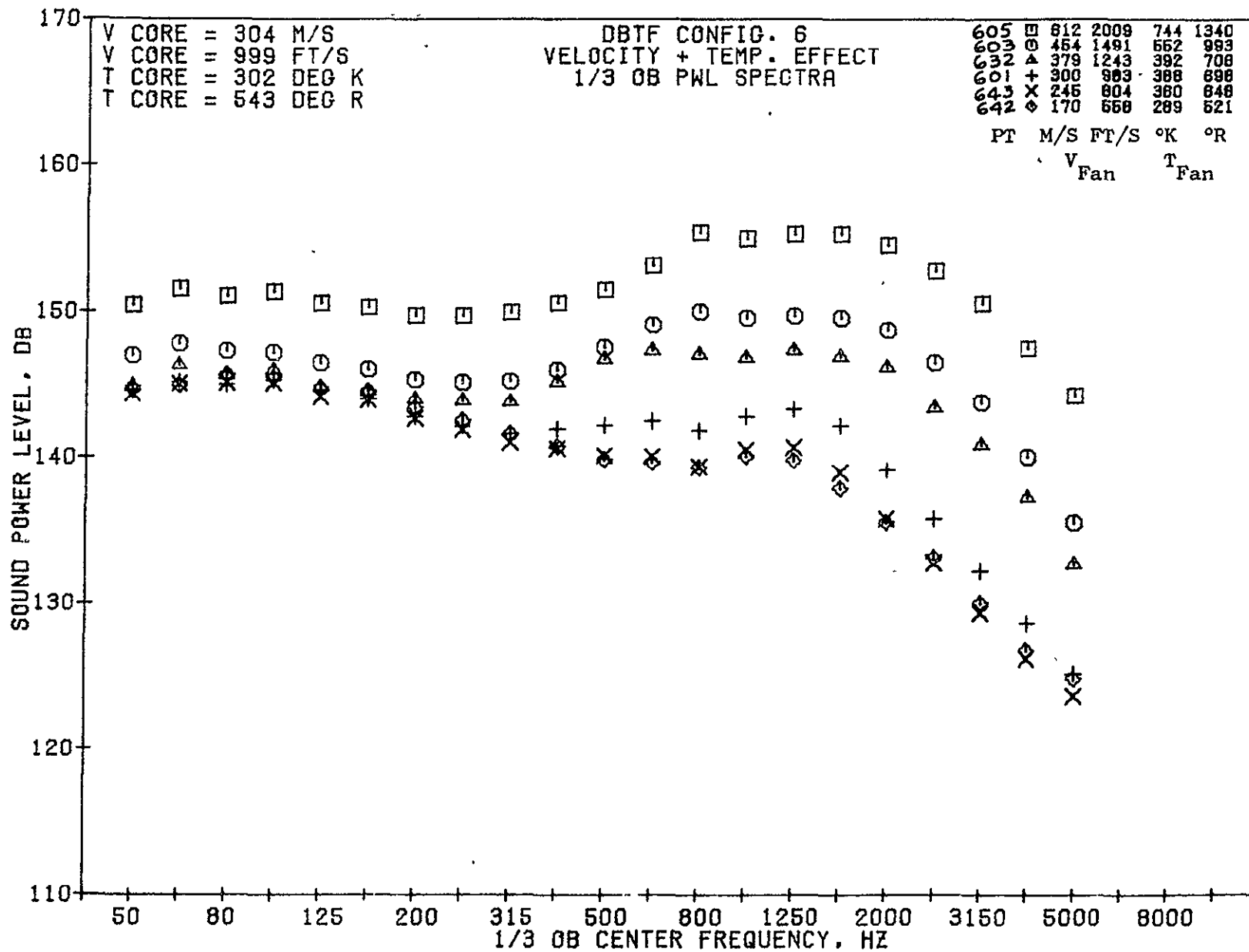


1472

4-2991

08/20/75
 5R552-001

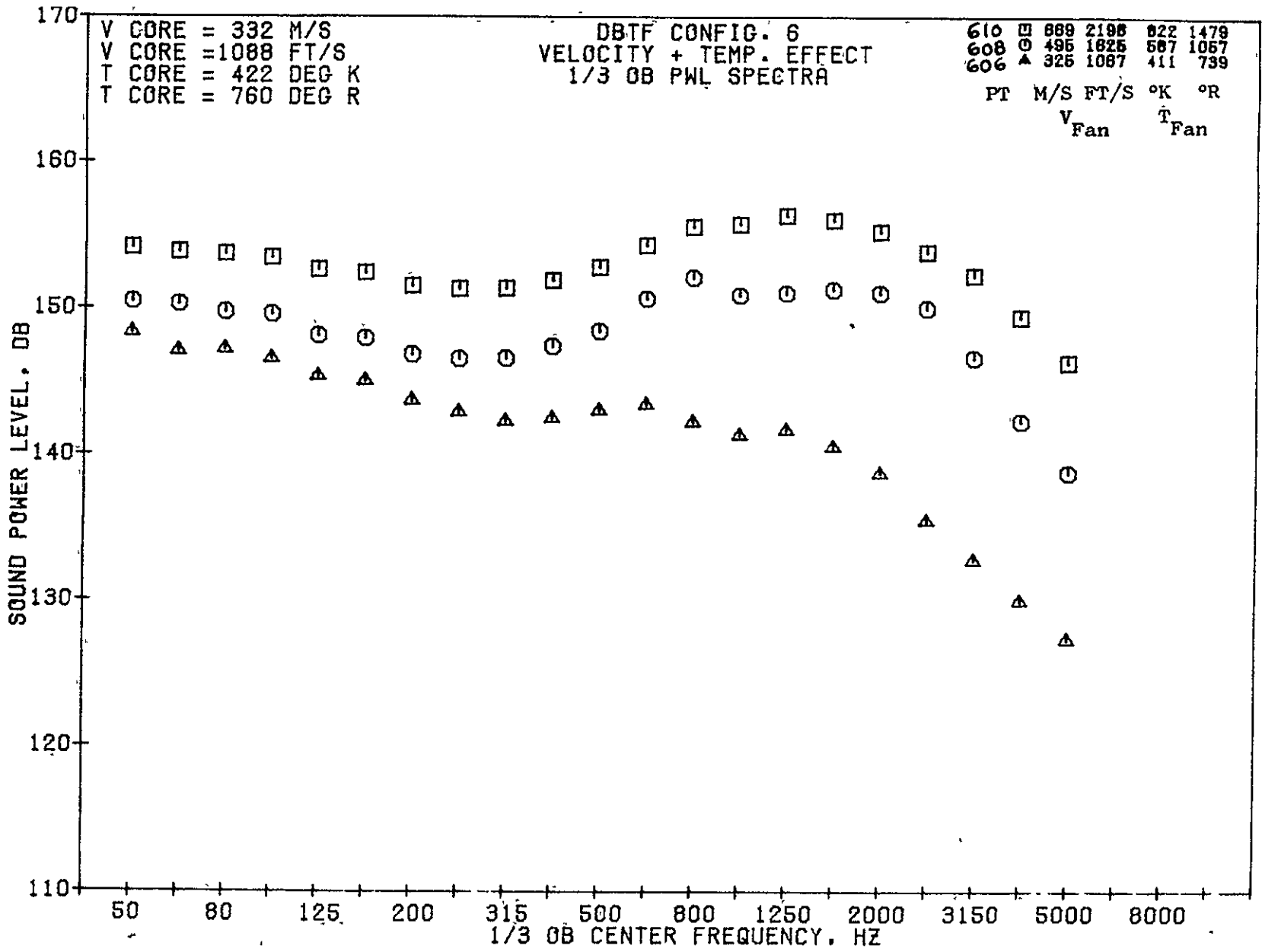
79 BURCH A.



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08/12/75
5R921-001

79 BURCH A.

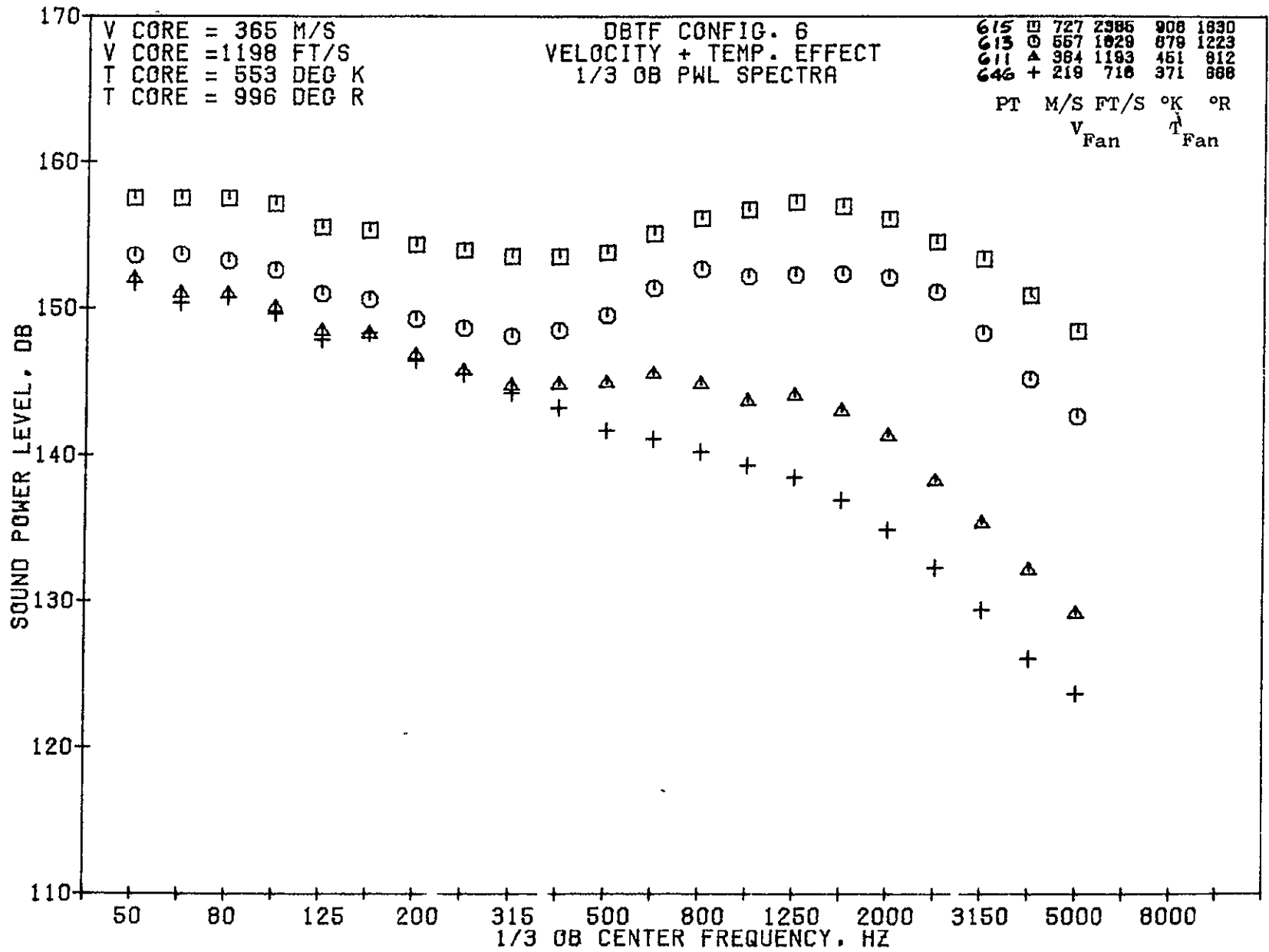


1474

10239

08/12/75
5R921-001

79 BURC



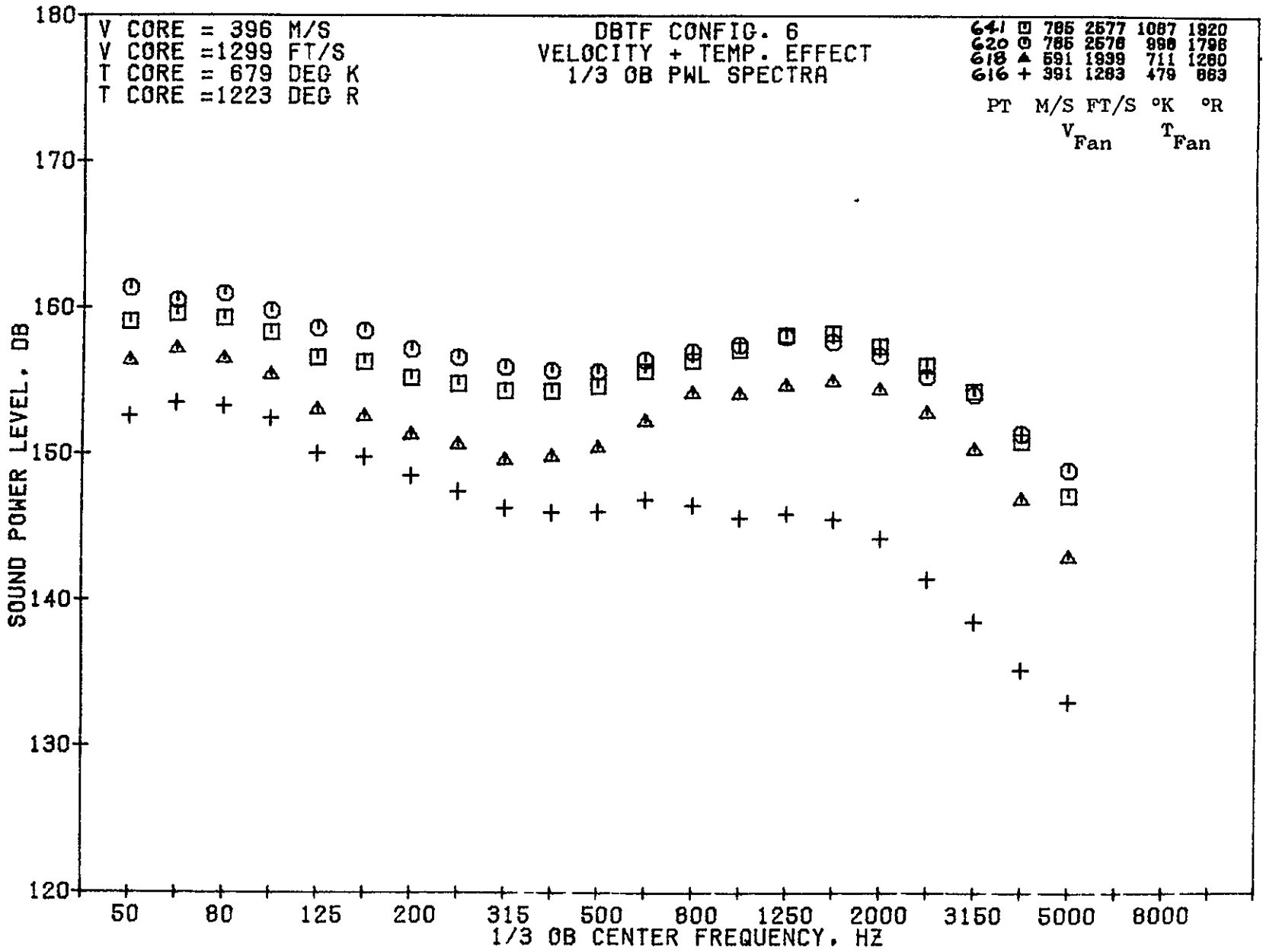
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4-2-75

08/12/75
5R921-001

79 BURCH A.

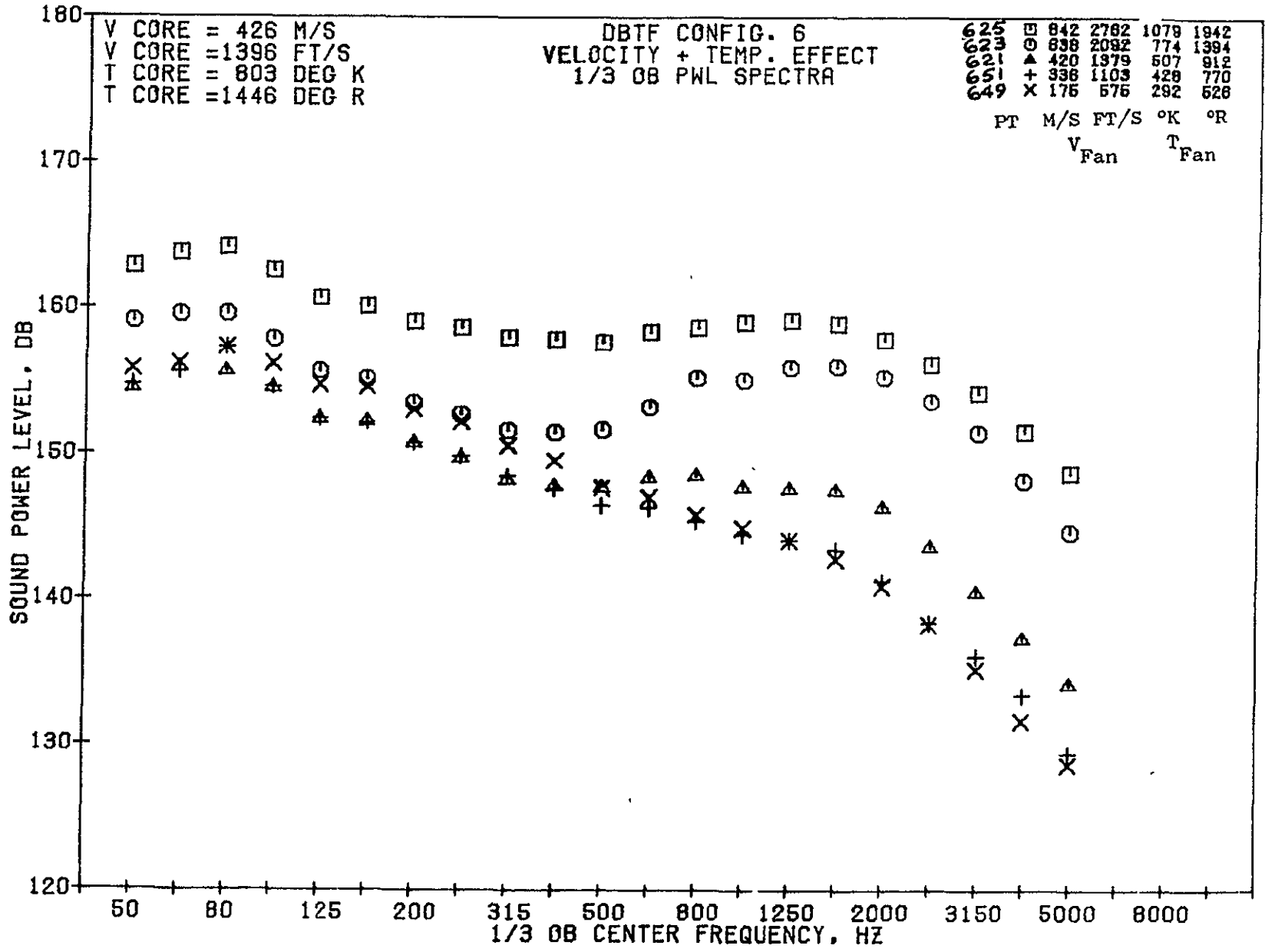
1476



11-241

08/12/75
5R921-001

79 BURCH A.



1477

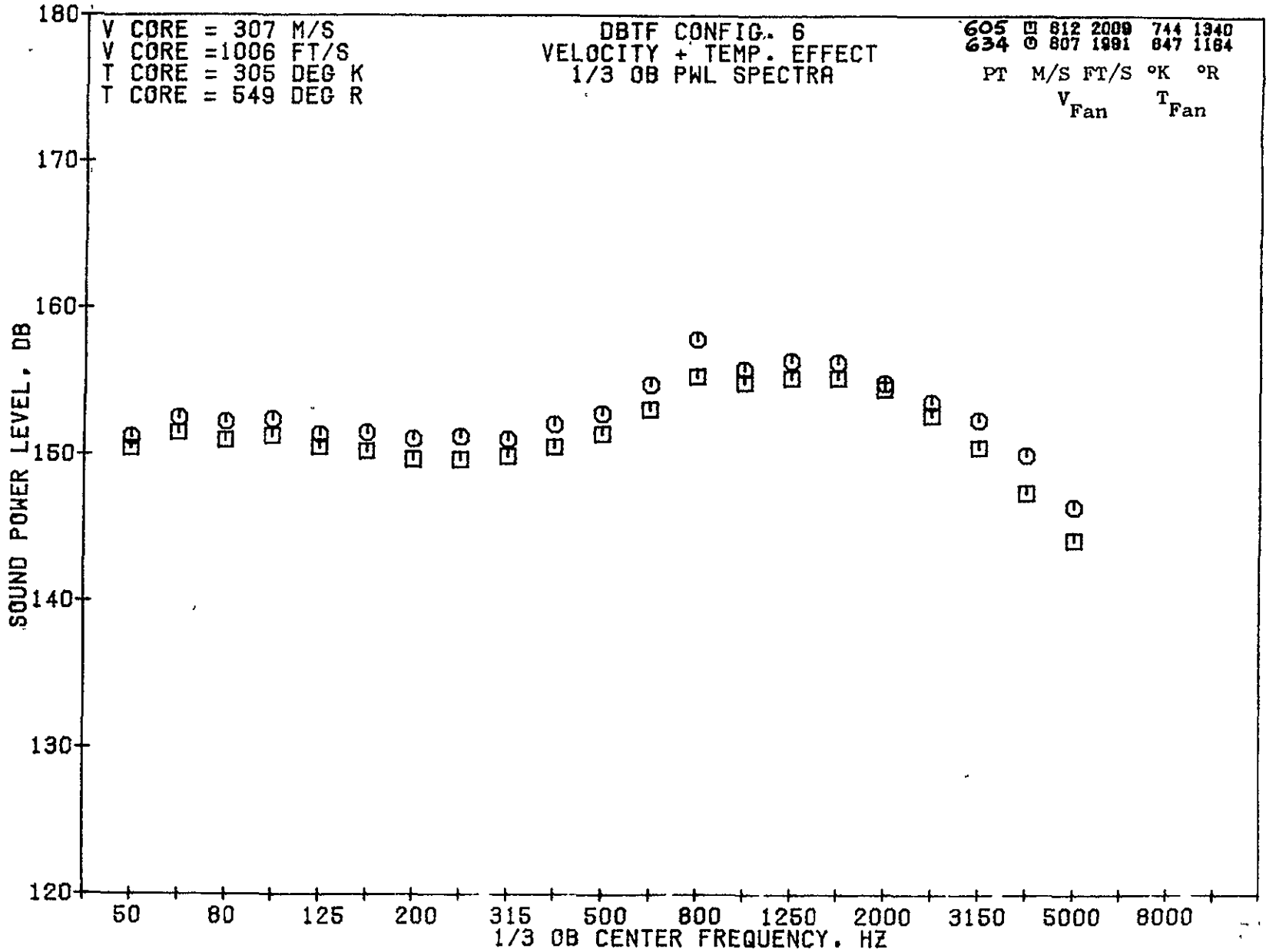
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OF FOUR OF

08/12/75
5R921-001

79 BURCH A.

1-24-75

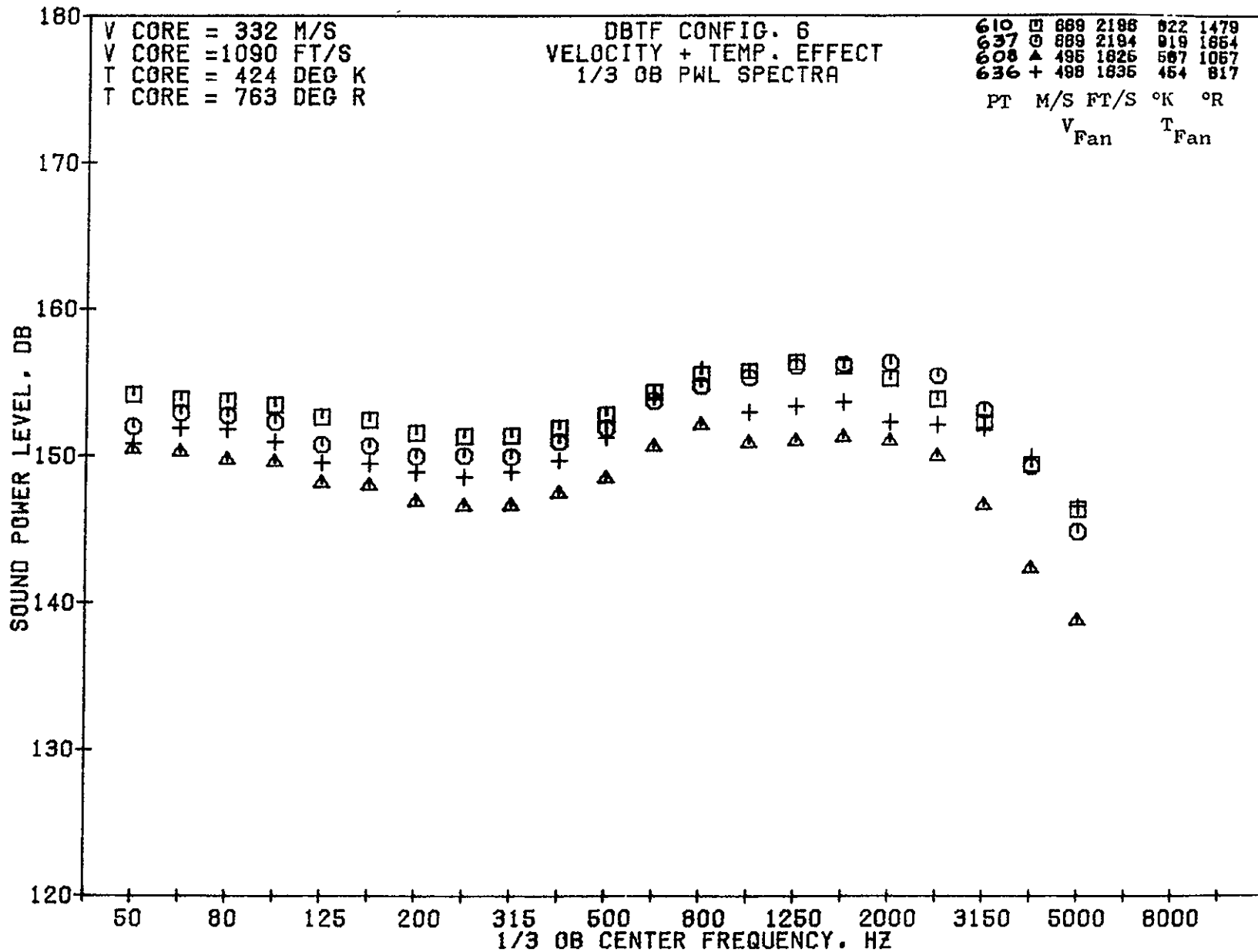
1478



11-243

08/12/75
5R921-001

79 BURCOR A.



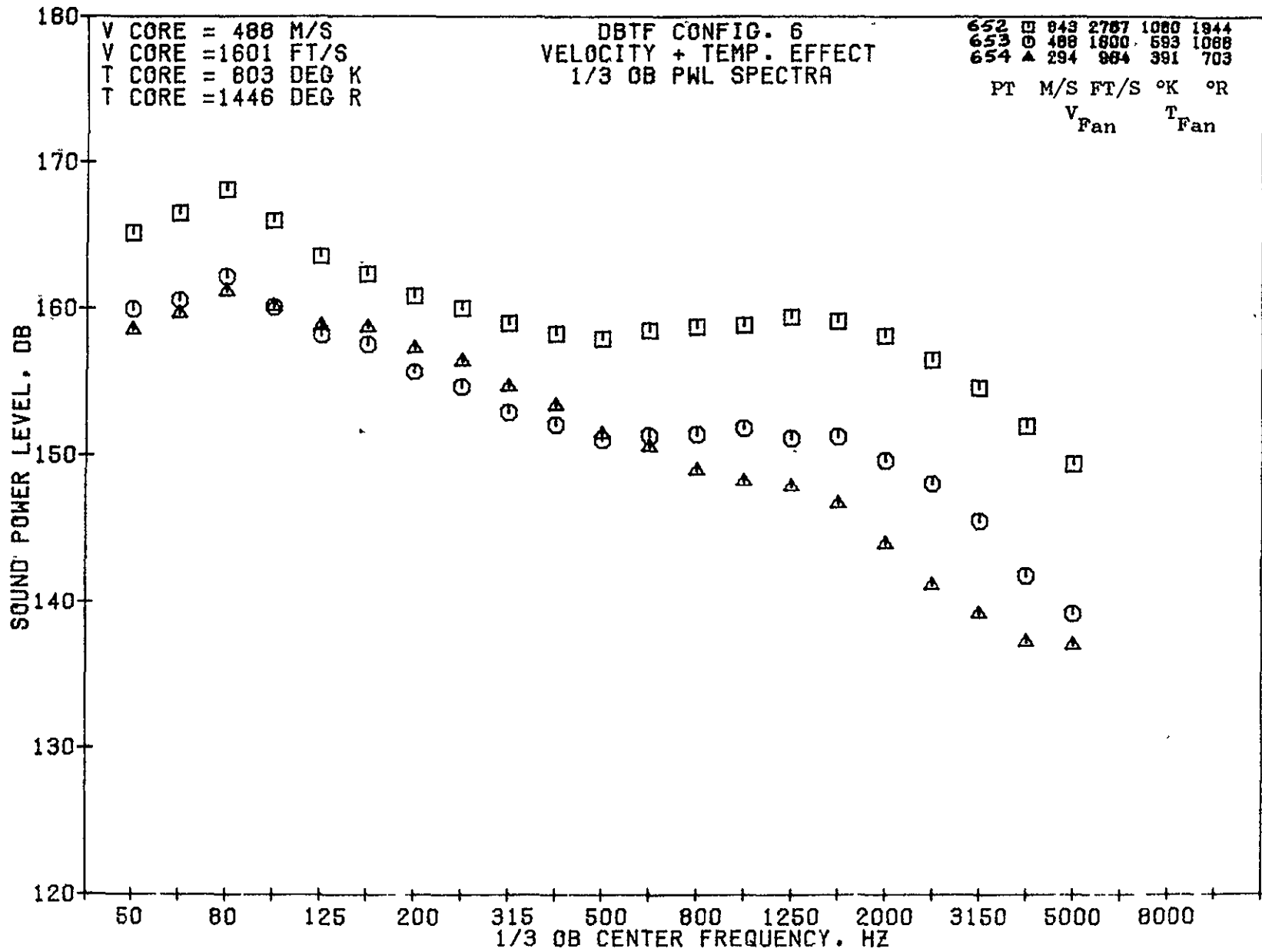
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5R921-001

79 BURCH A.

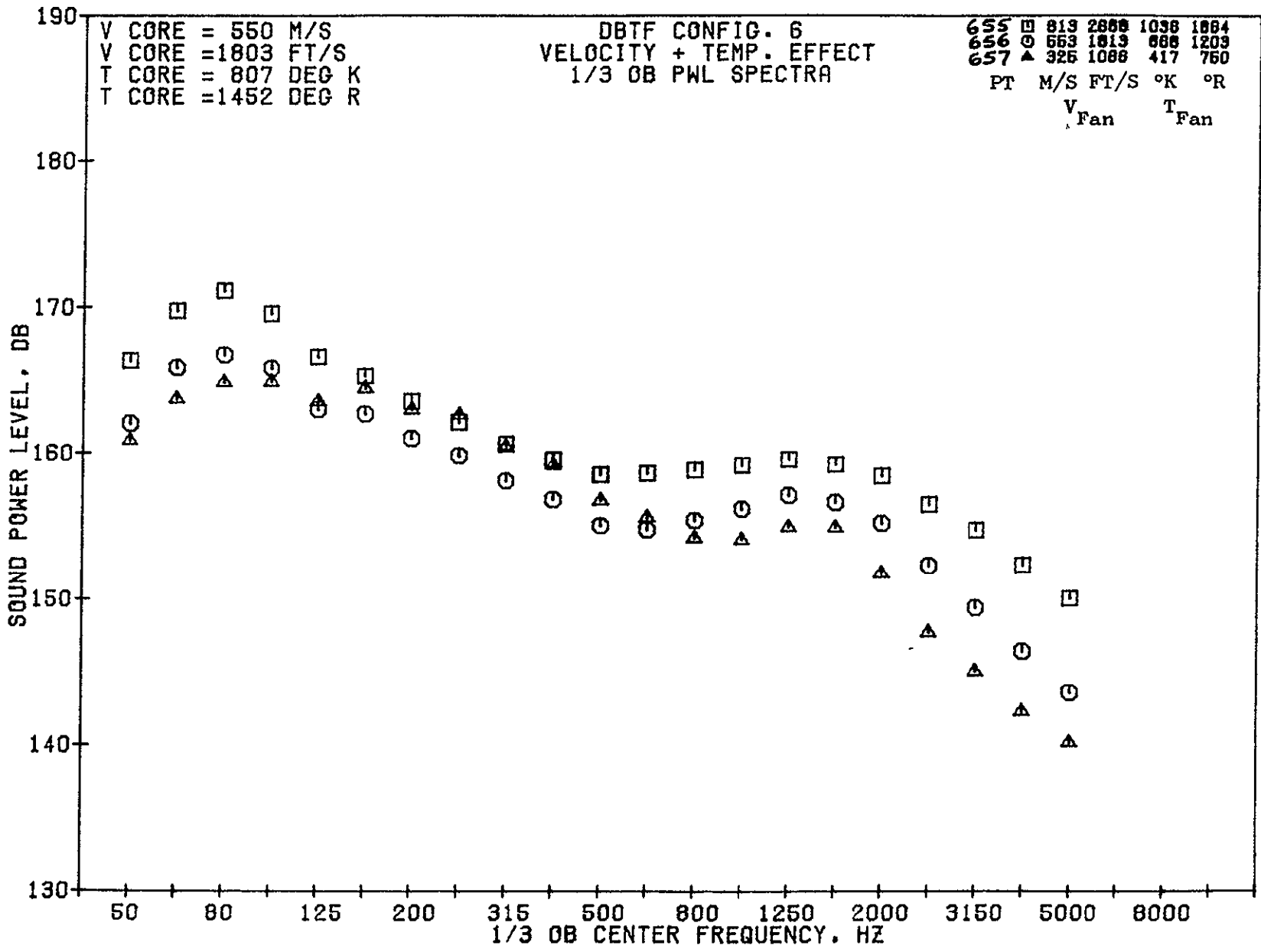
4-244



4-245

08/12/75
5R921-001

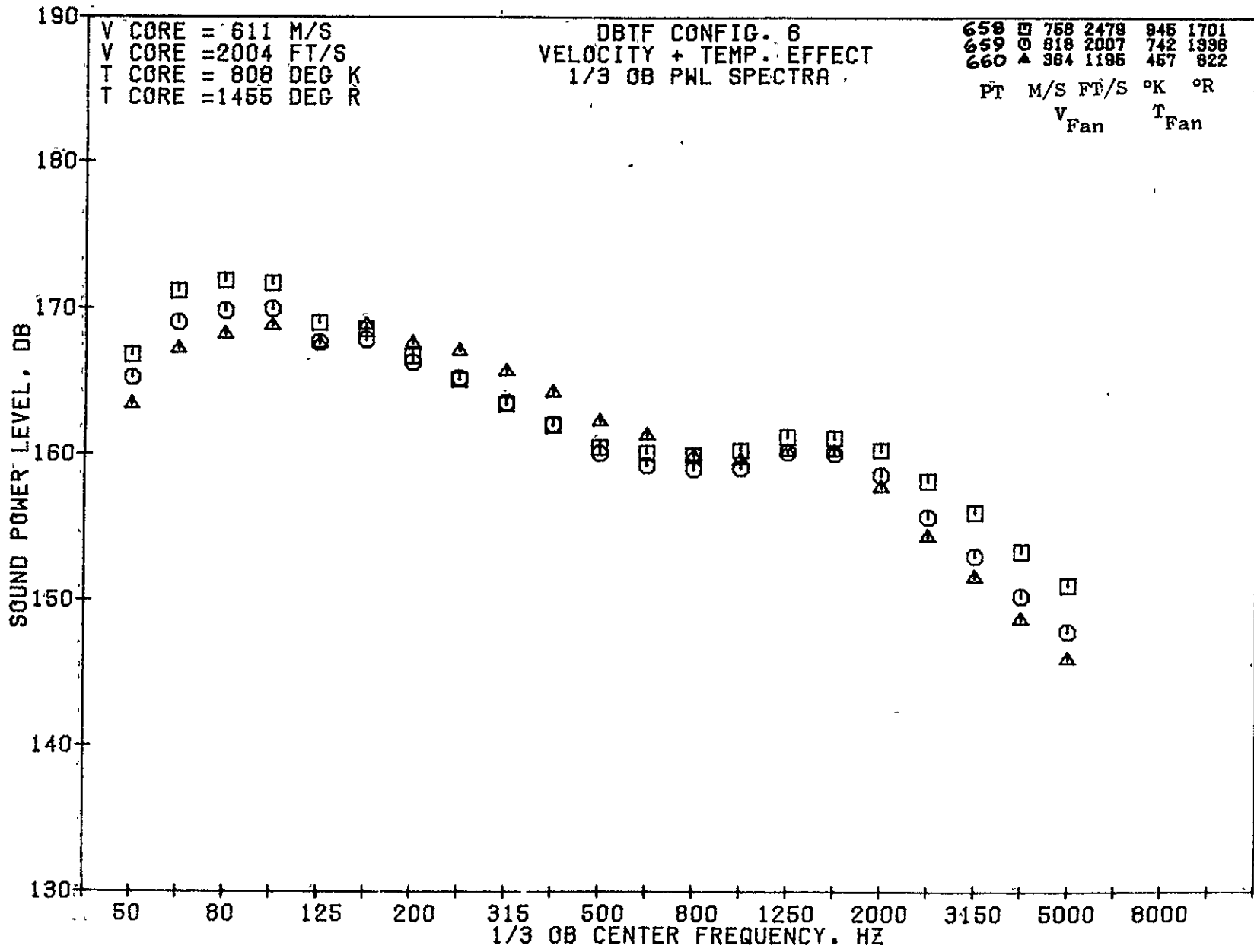
79 BUR A.



1481

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4-246

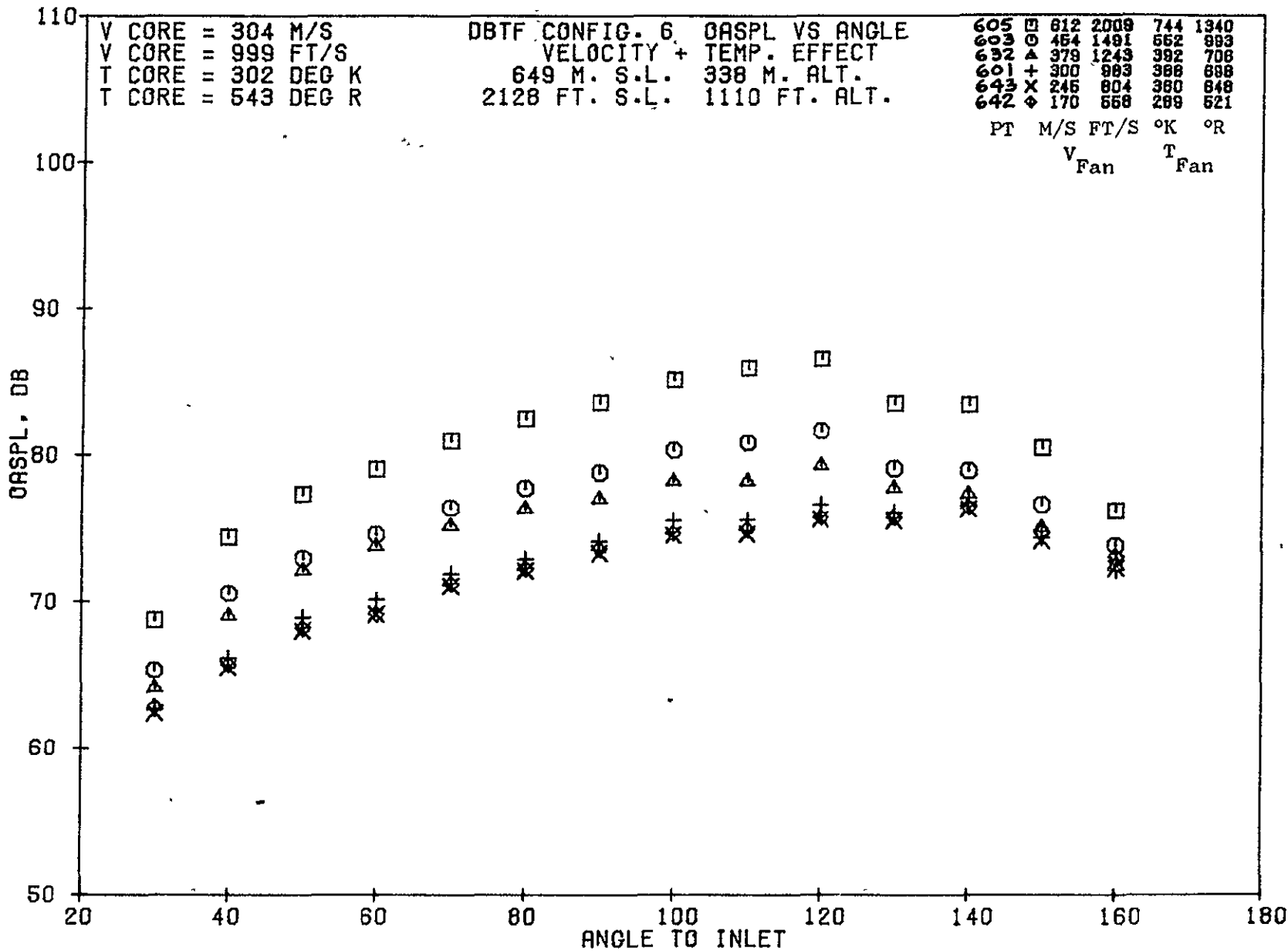


4-247

08/12/75
5R921-001.

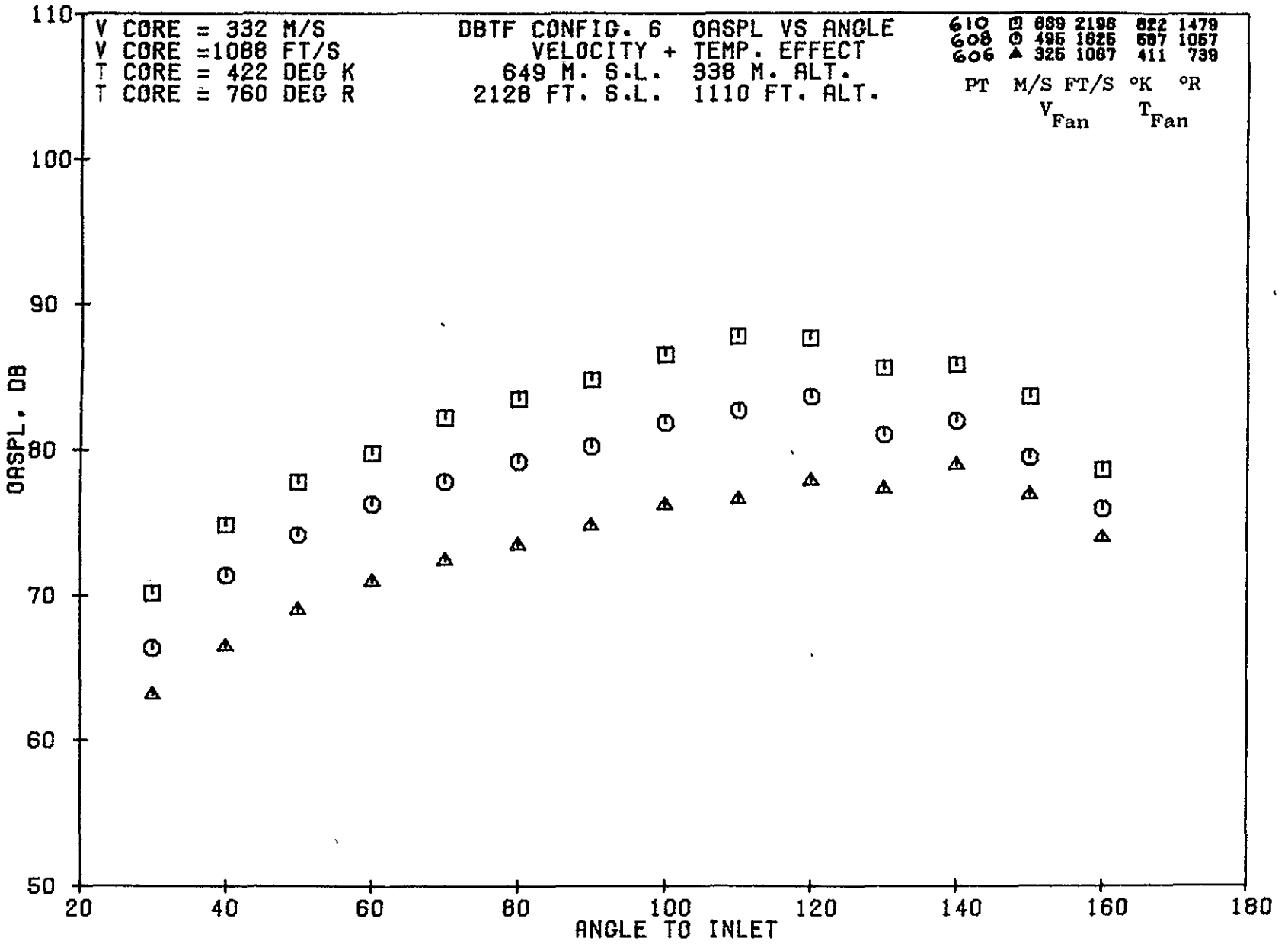
79 BURD A.

1483



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11-248

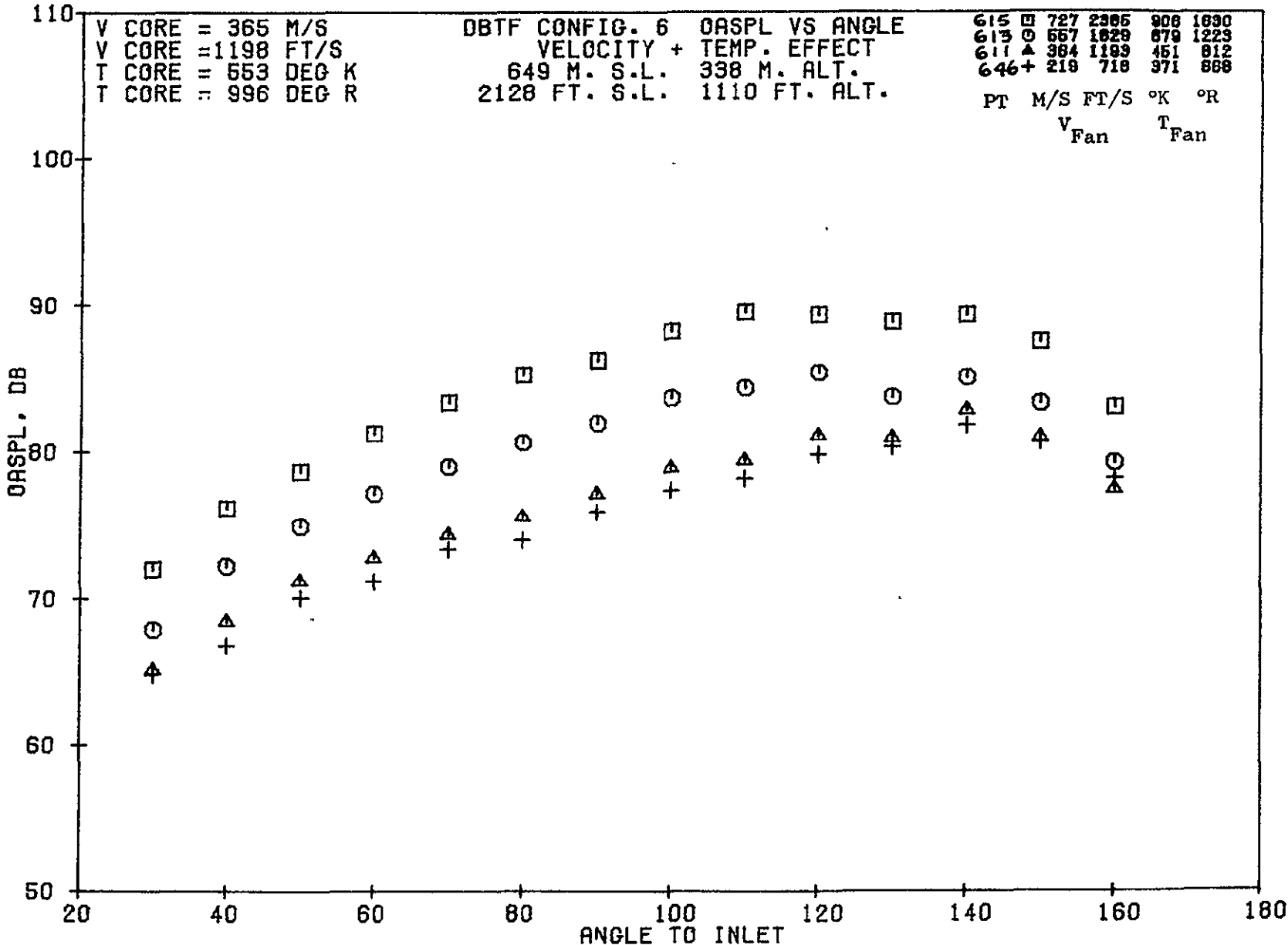


1484

1-219

08/12/75
 5R921-001

79 BURC A.



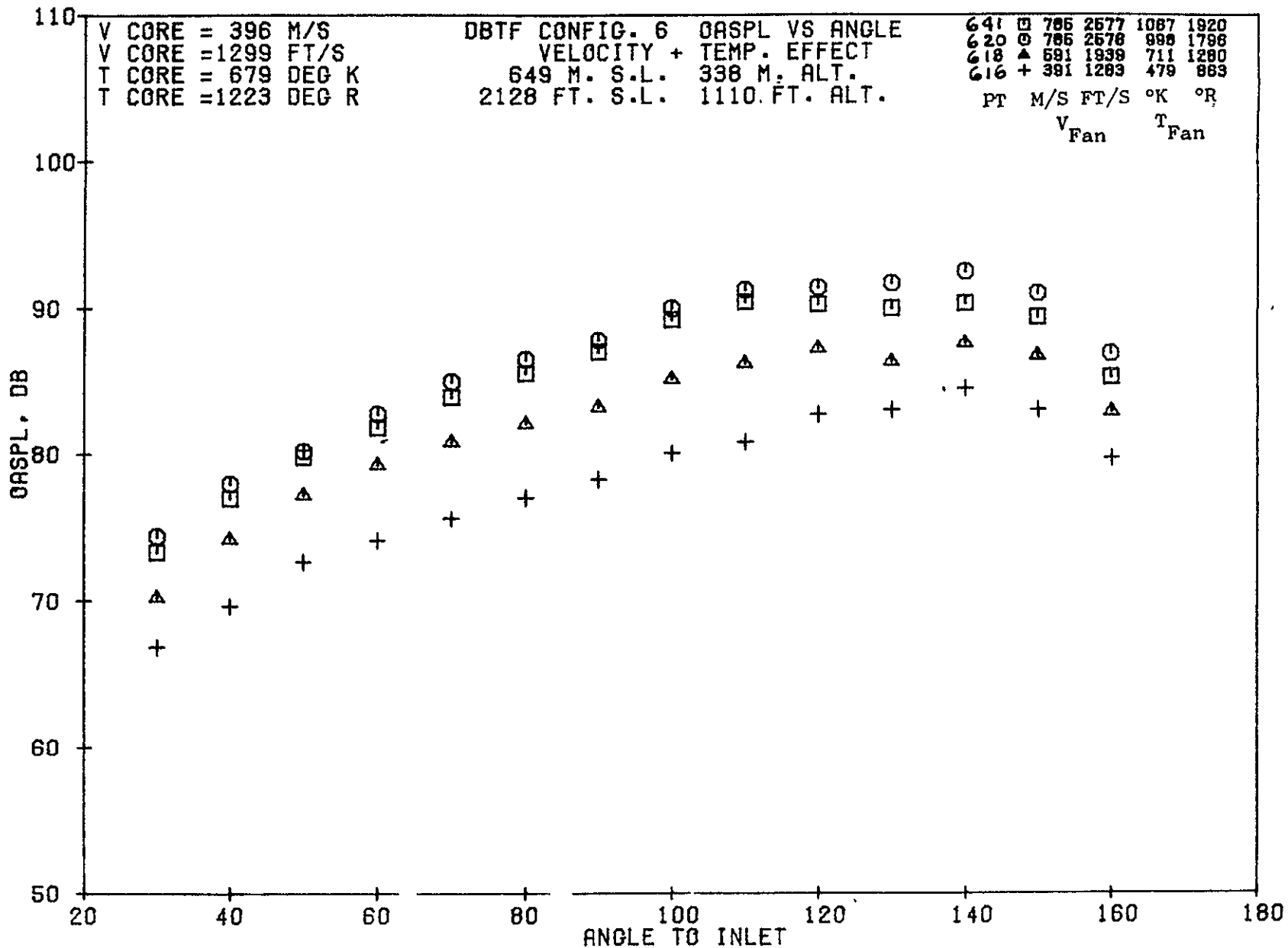
1485

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POOR QUALITY

11-250

08/12/75
5R921-001

79 BURCH A.

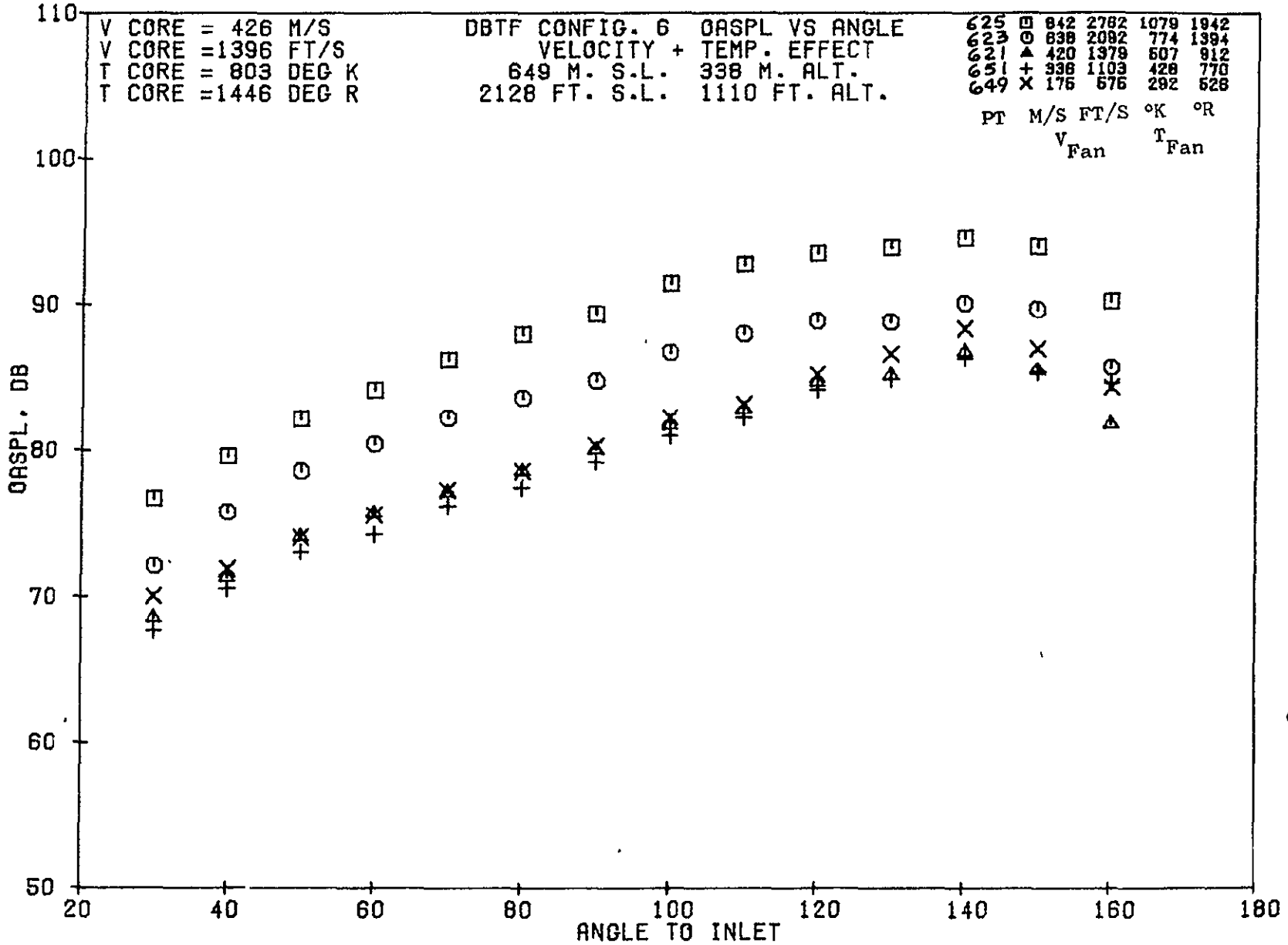


1486

4-251

08/12/75
 5R921-001

79 BURQA.



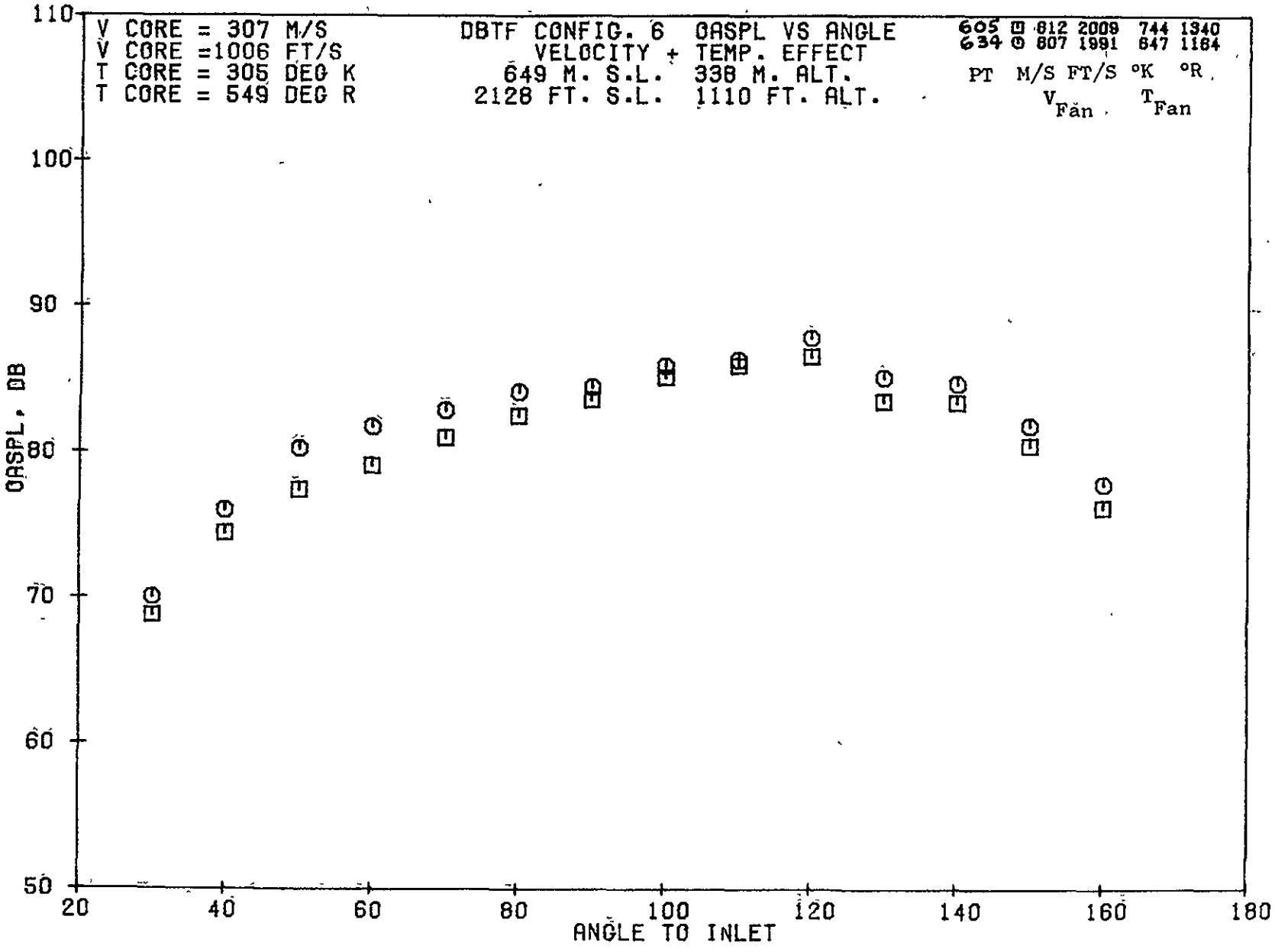
1487

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4-252

08/12/75
 5R921-001

79 BURCH A.

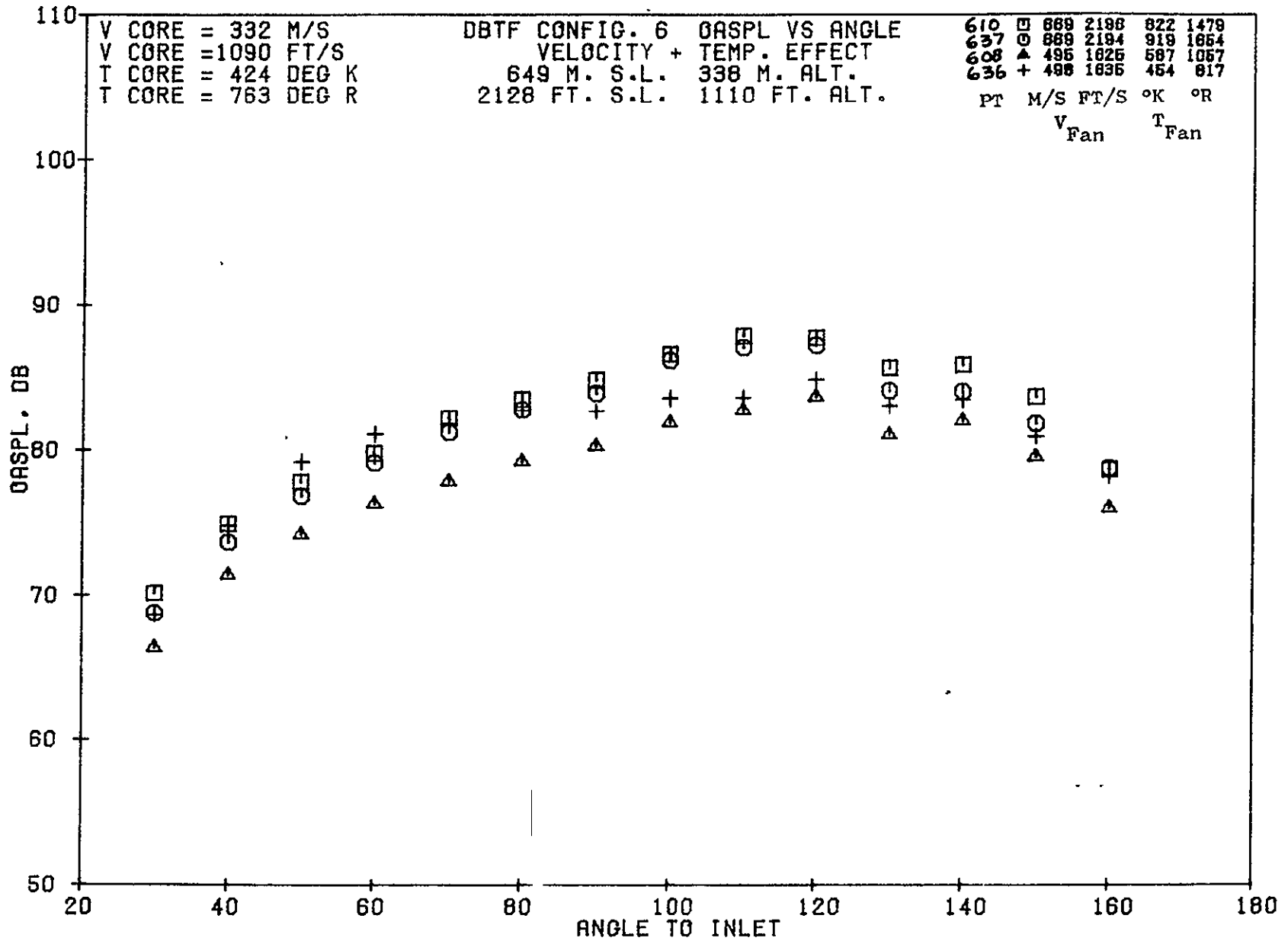


1488

4-123

08/12/75
5R921-001

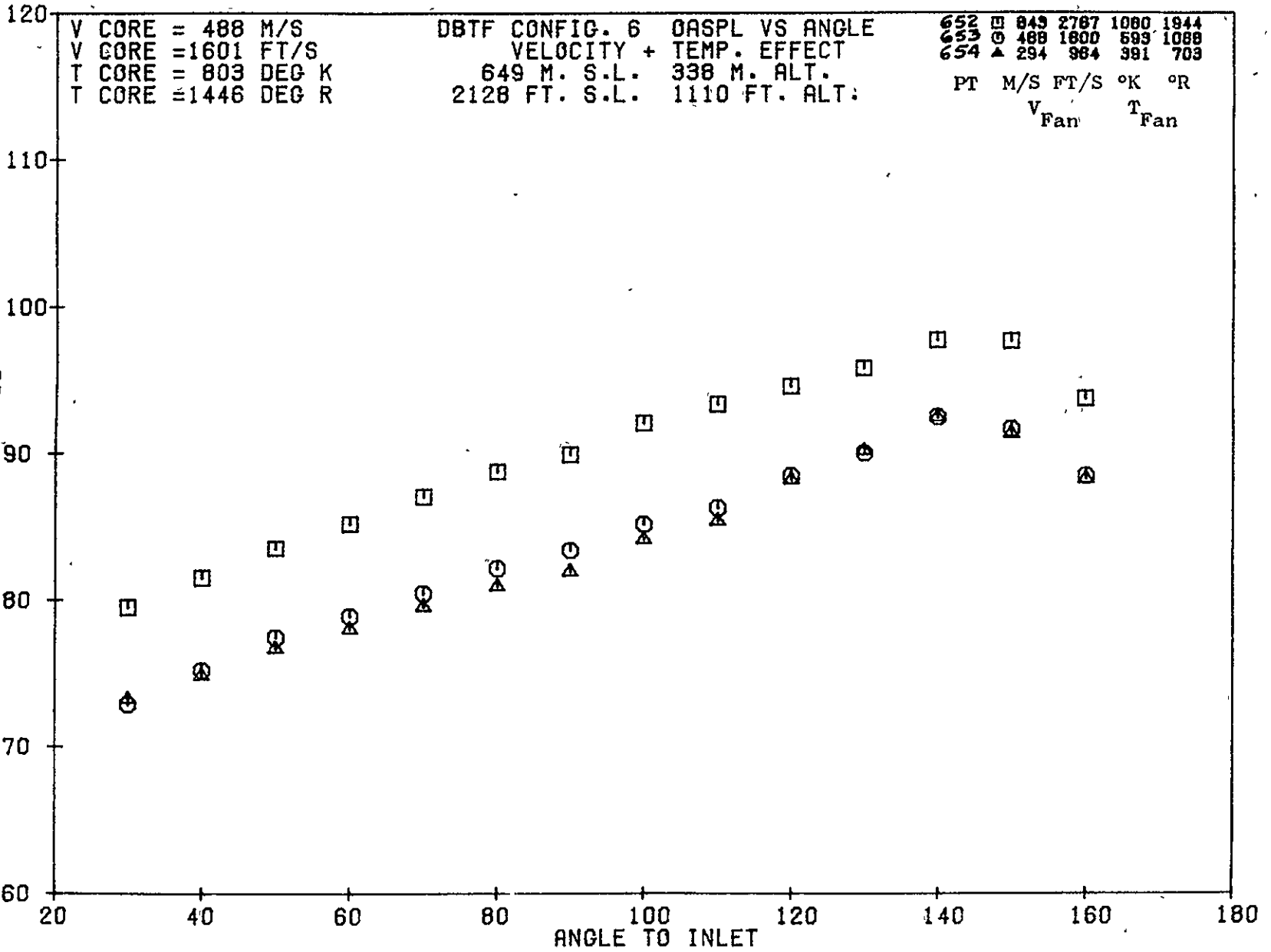
79 BURC



1489

4-154

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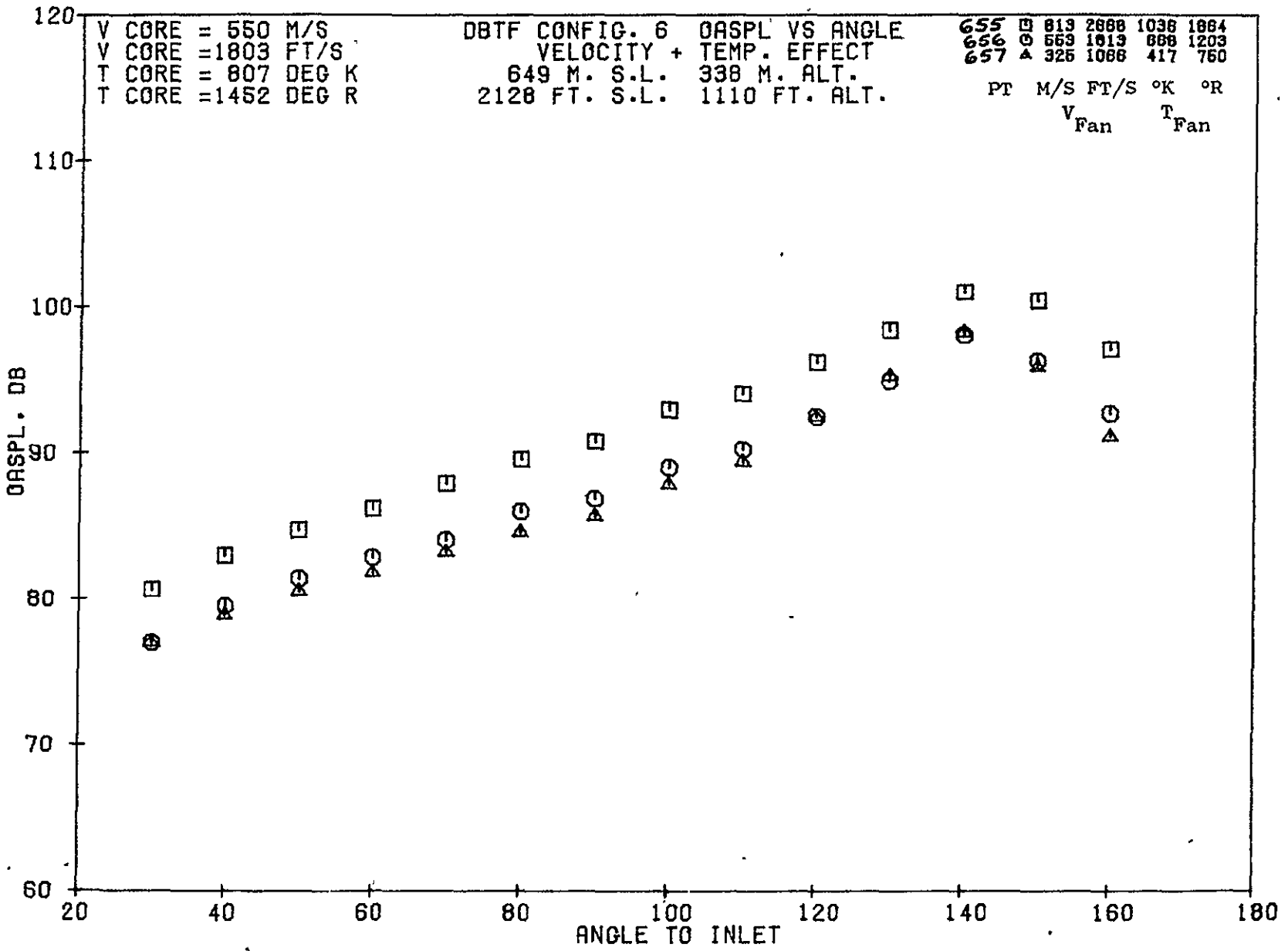


1490

4-255

08/12/75
5R921-001

79 BURC A.



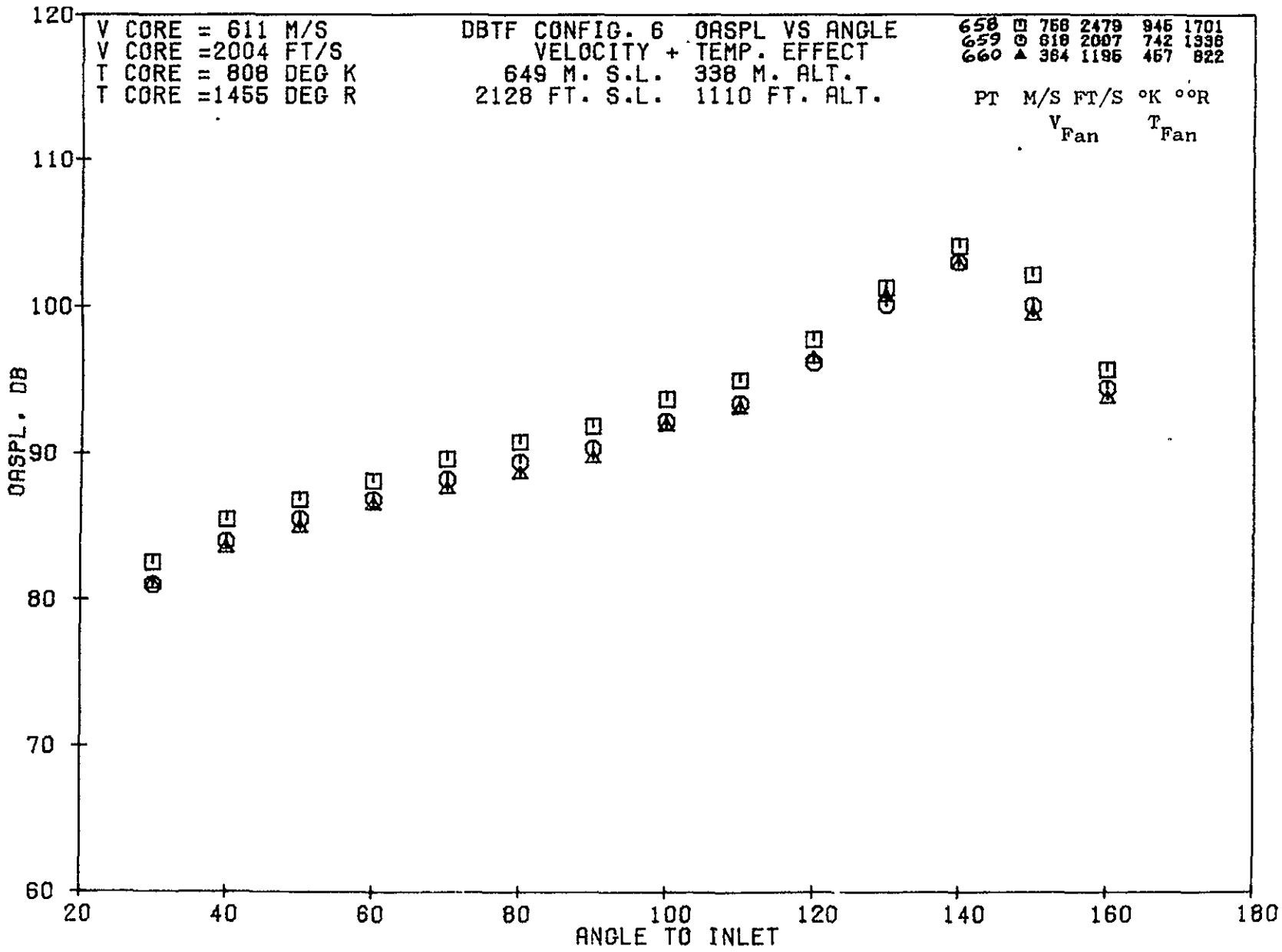
1491

4-256

08/12/75
5R921-001

79 BURCH A.

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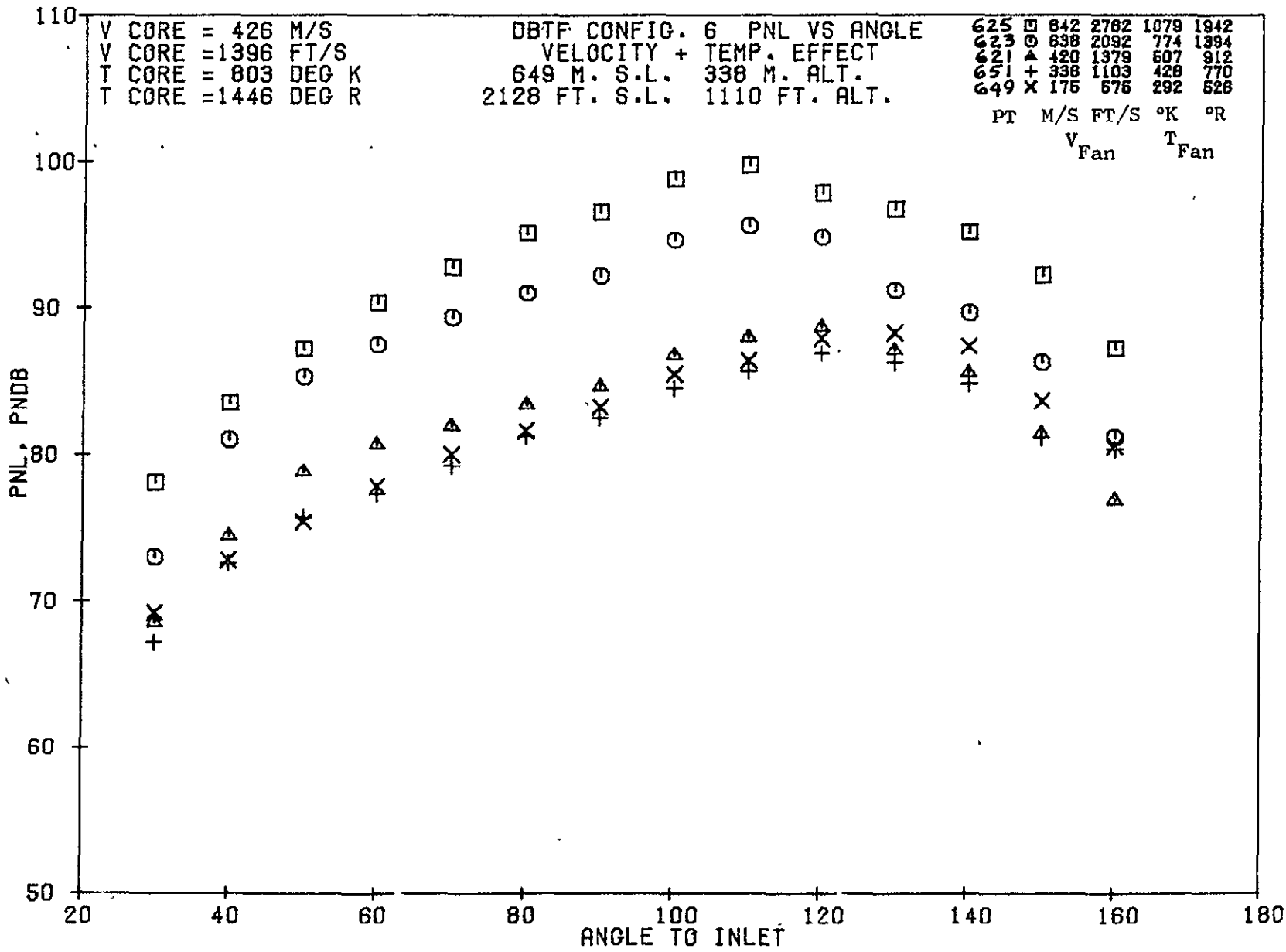


1492

4-157

08/12/75
5R921-001

79 BURCH A.



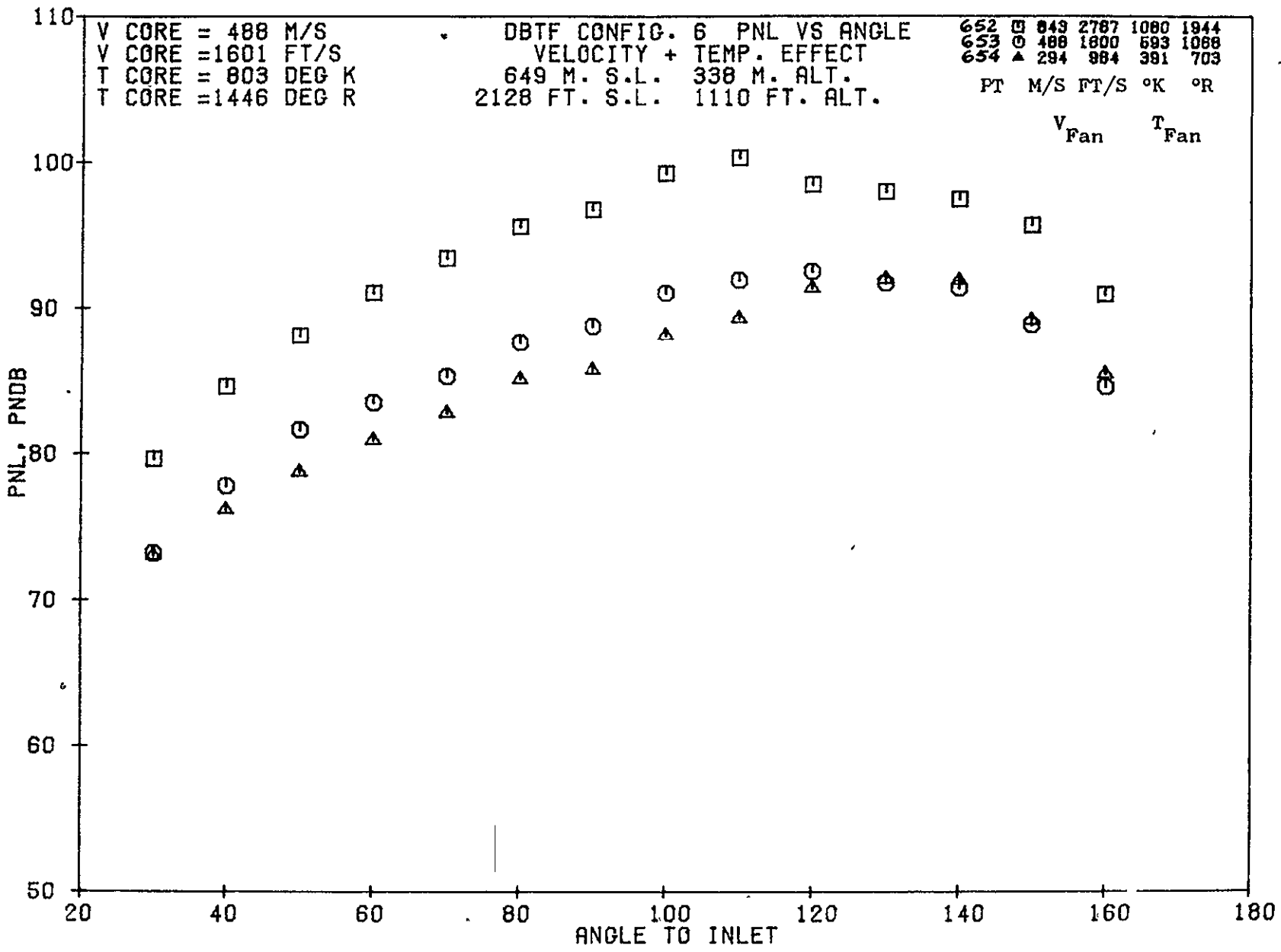
1493

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08/12/75
5R921-001

79 BURCH A.

1-25-8

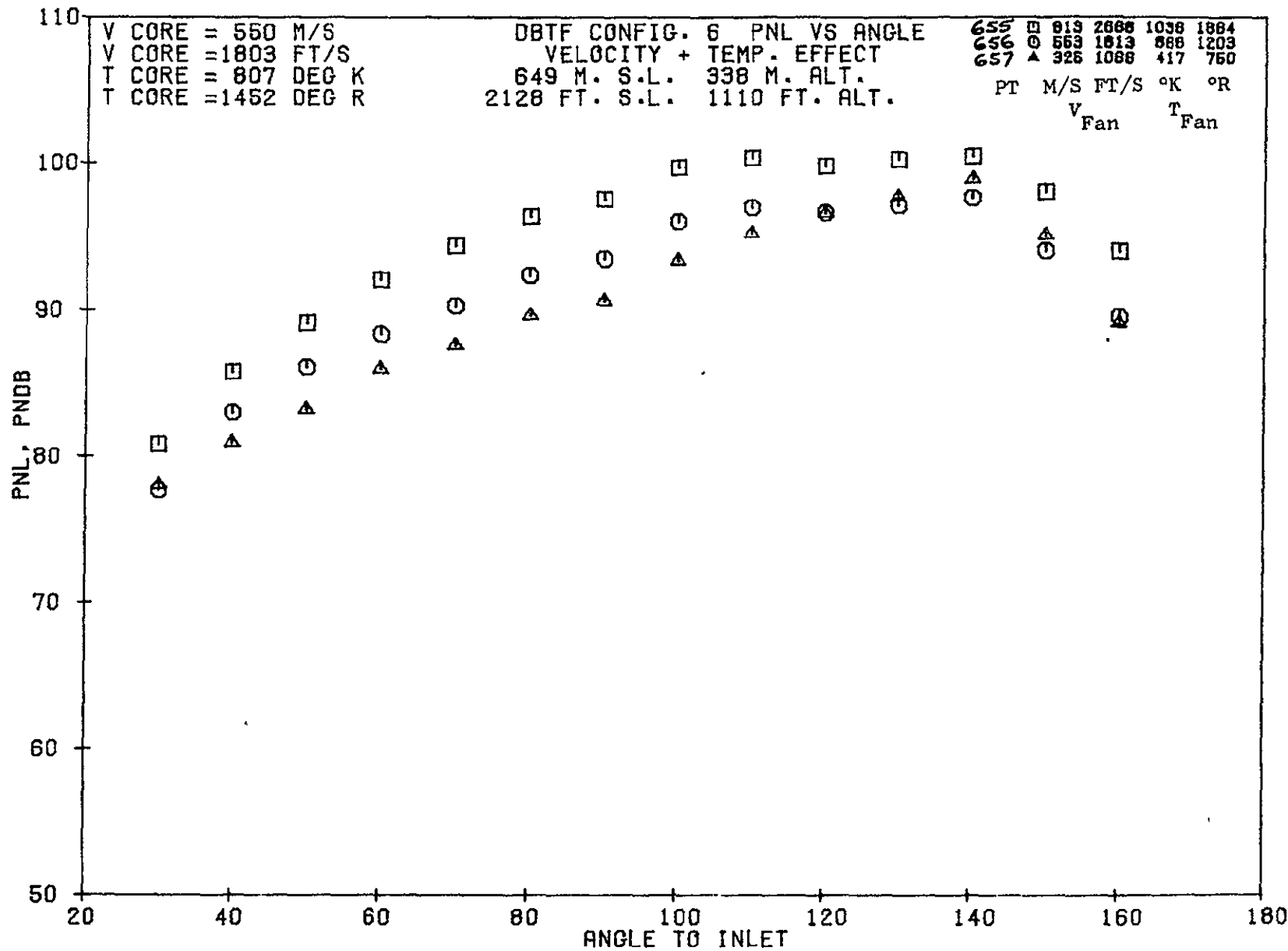


1494

11-25-79

08/12/75
5R921-001

79 BURCOR



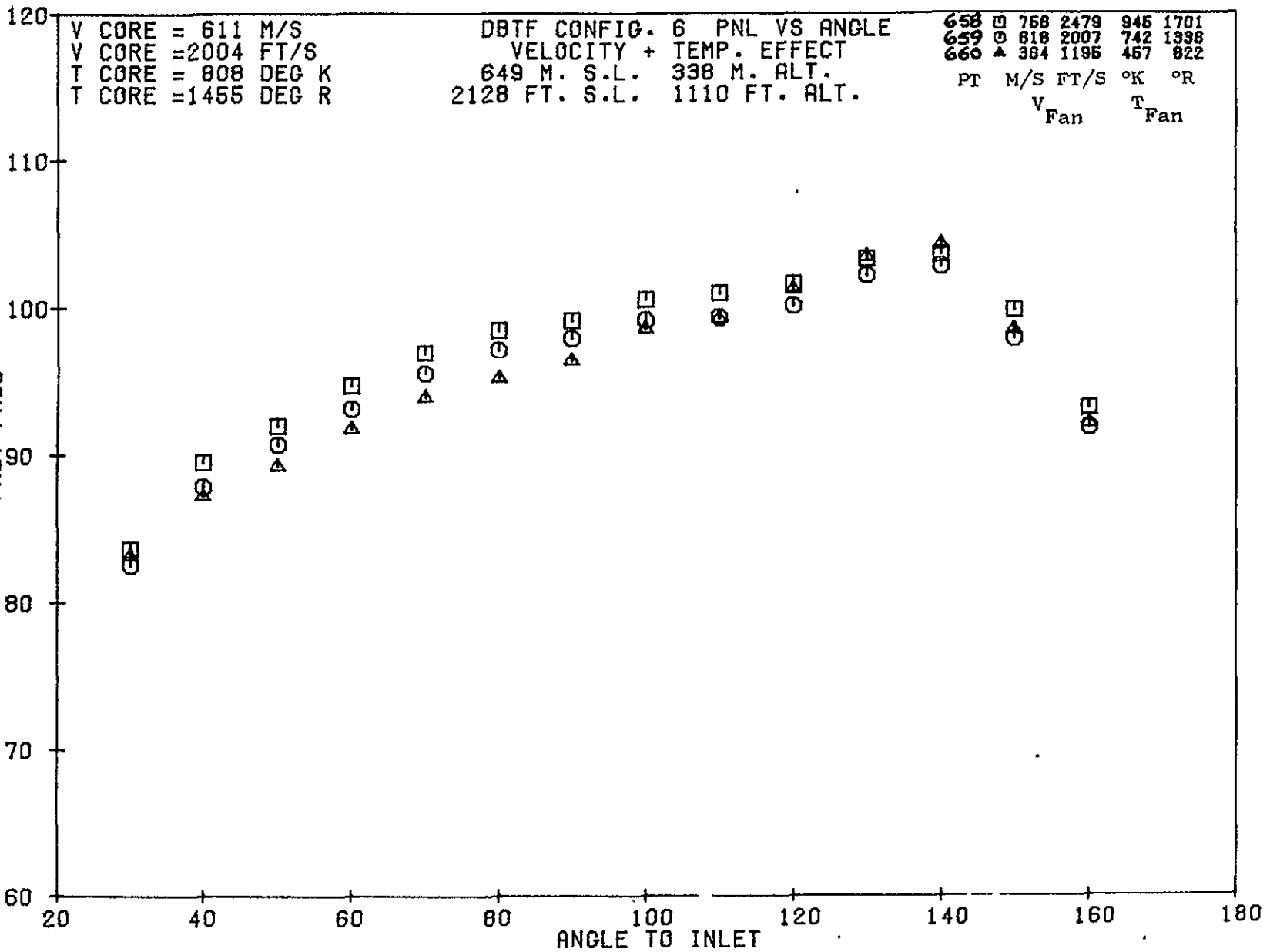
1495

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08/12/75
 5R921-001

79 BURCH A.

14-260

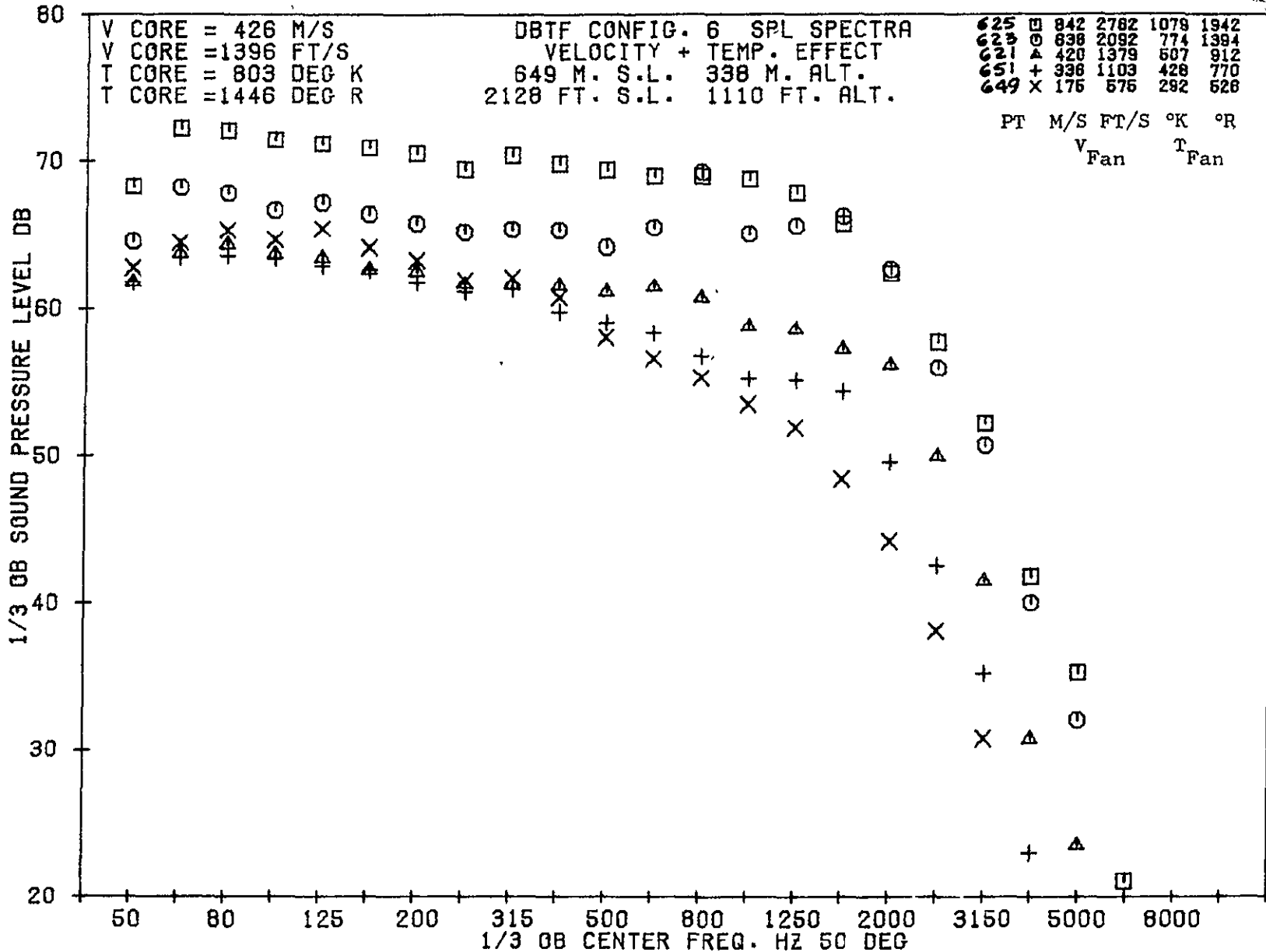


1496

4-261

08/12/75
5R921-001

79 BURCH A.



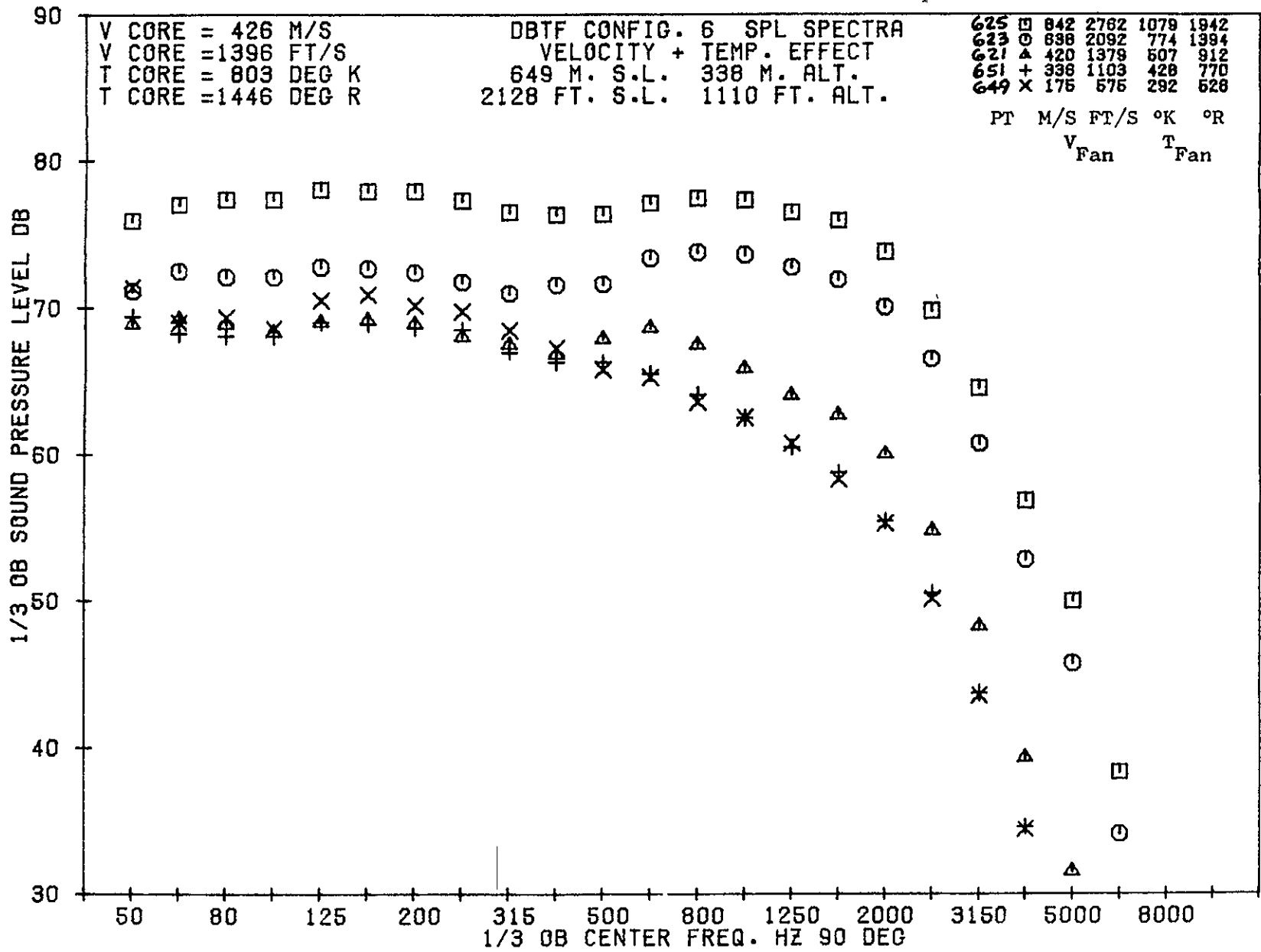
4.262

08/13/75
 5R947-001

79 BURCH A.

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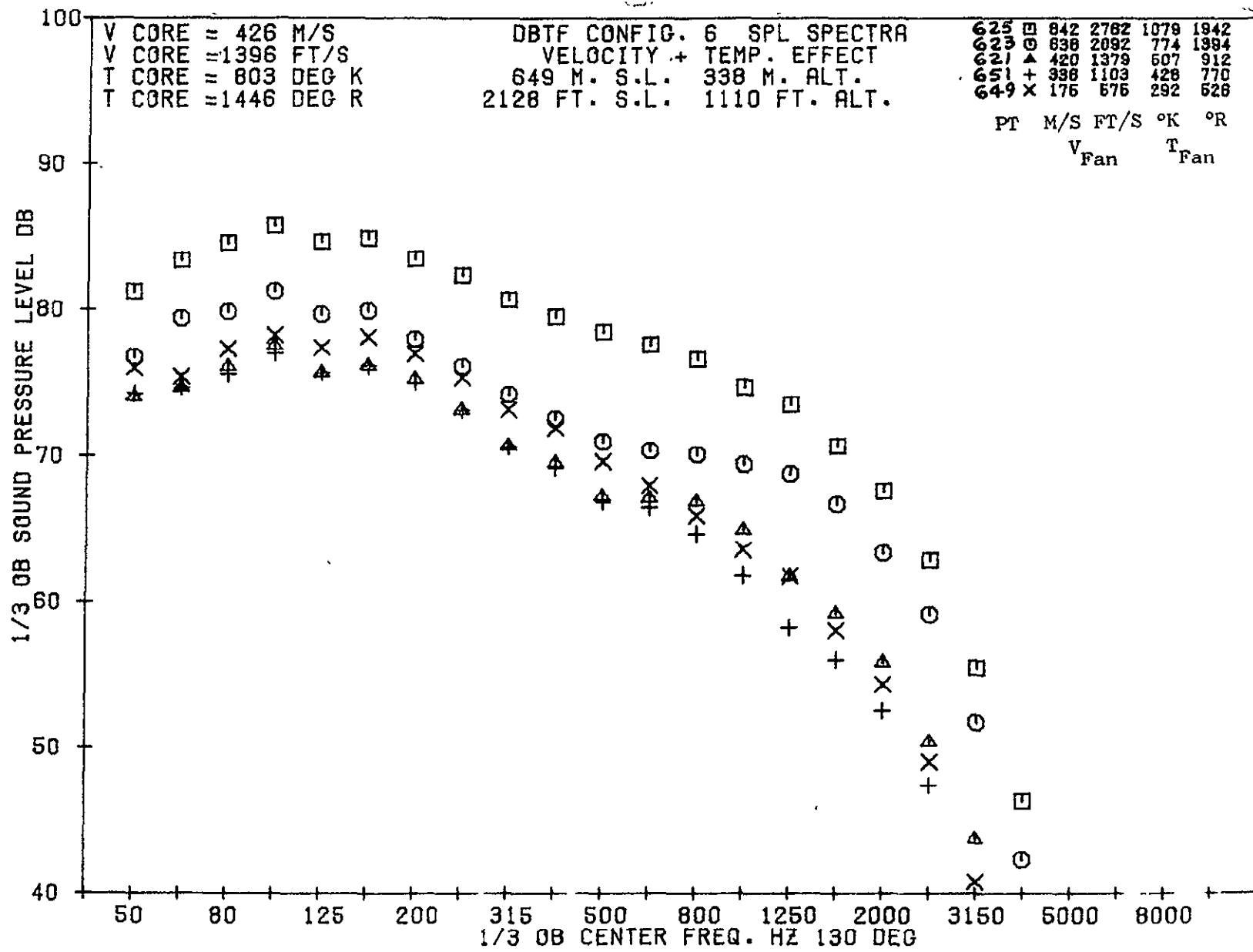
1498



4-263

08/13/75
 5R947-001

79 BURCH A.



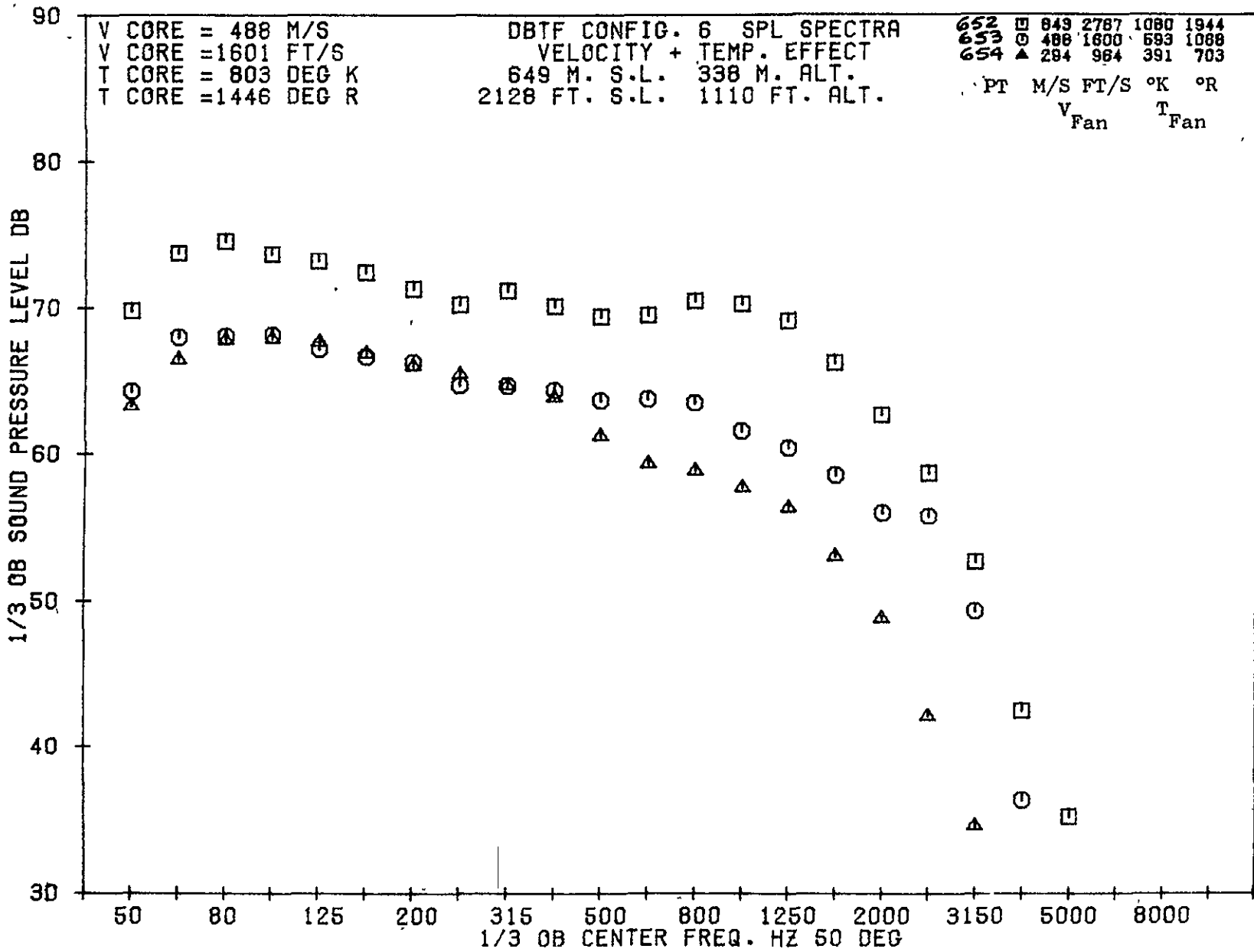
1499

4-264

08/13/75
5R947-001

79 BURCH A.

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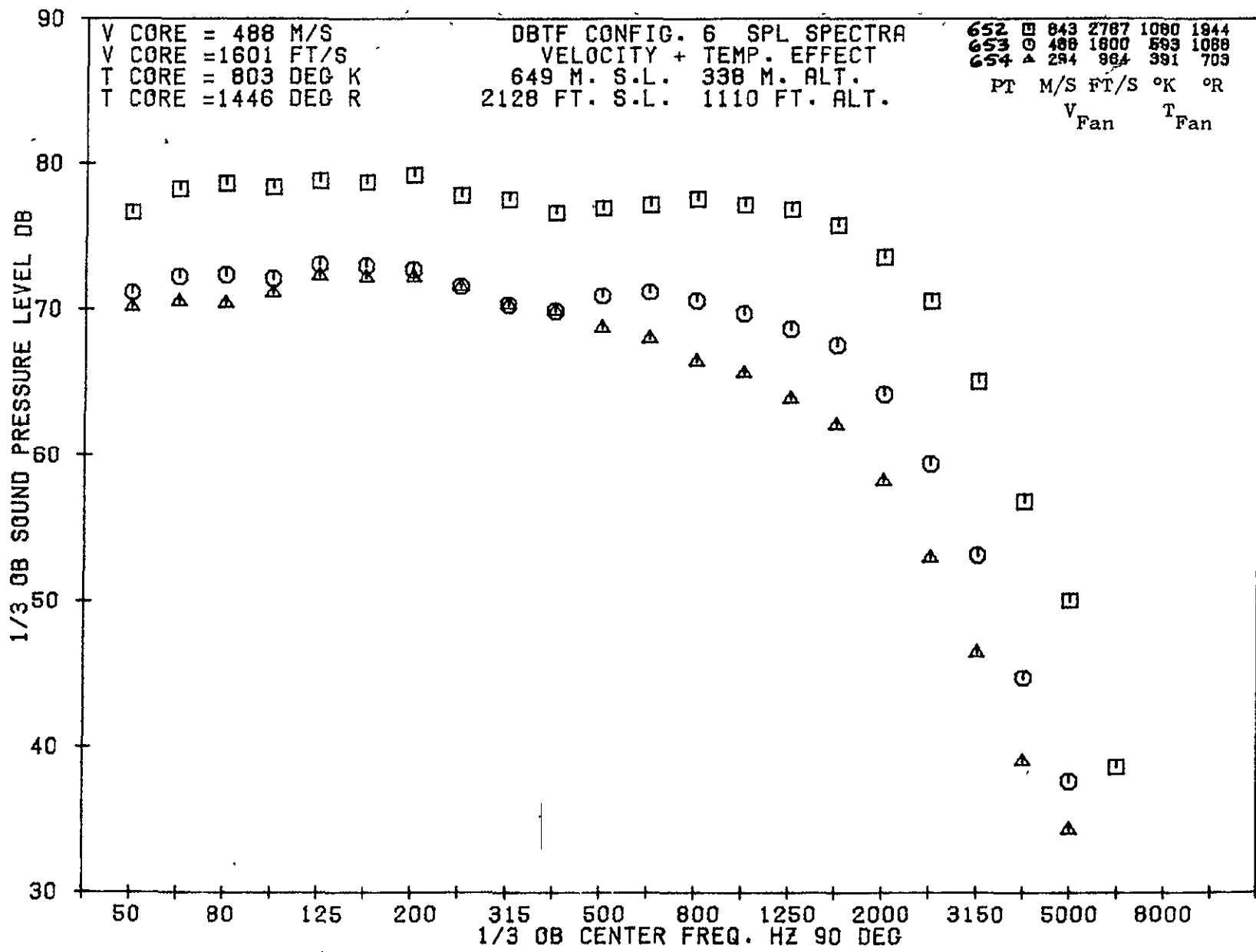


4-265

08/13/75
5R947-001

79 BURCH A.

1501



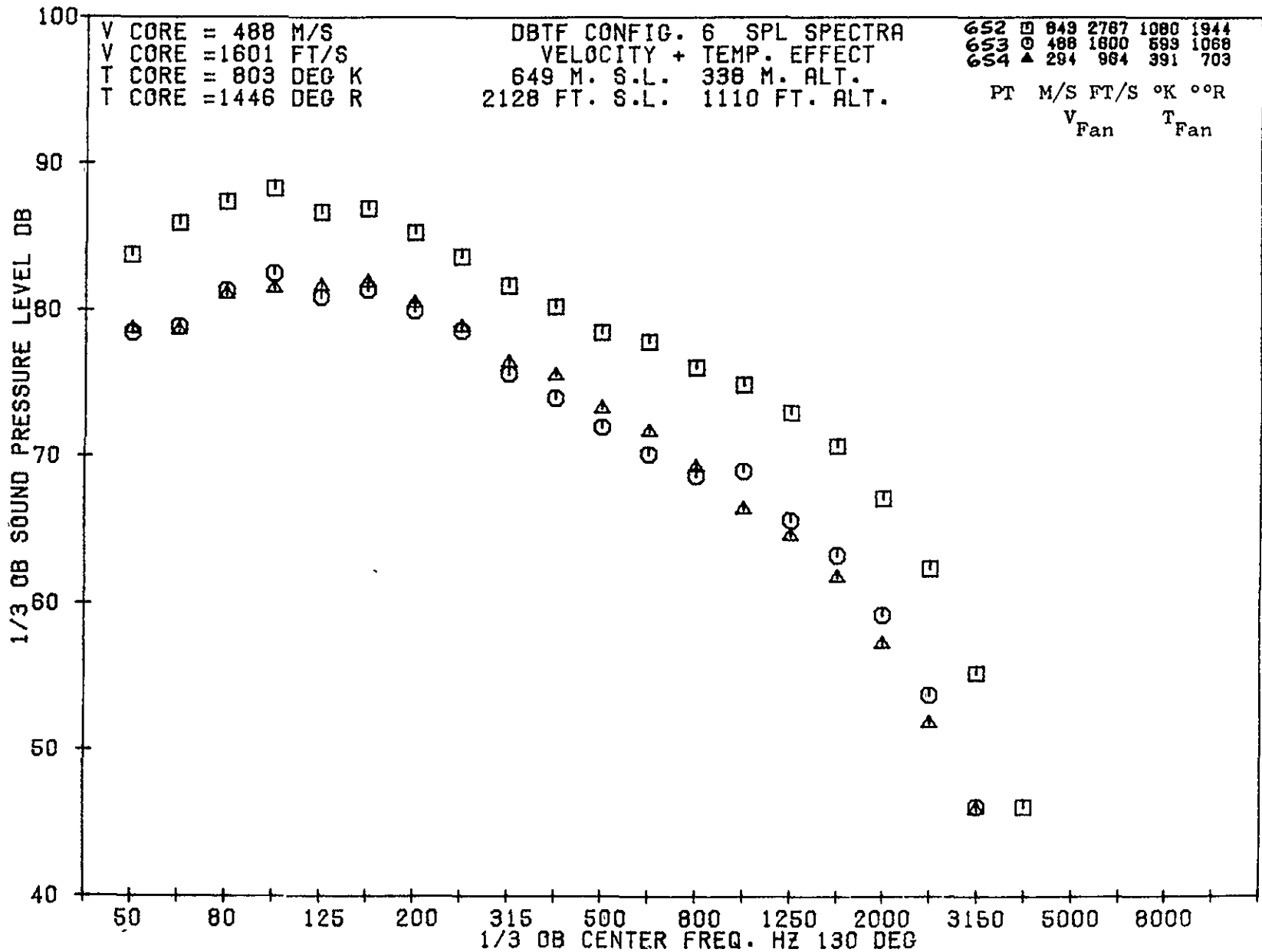
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5R947-001

79 BURCH A.

4. 266

1502

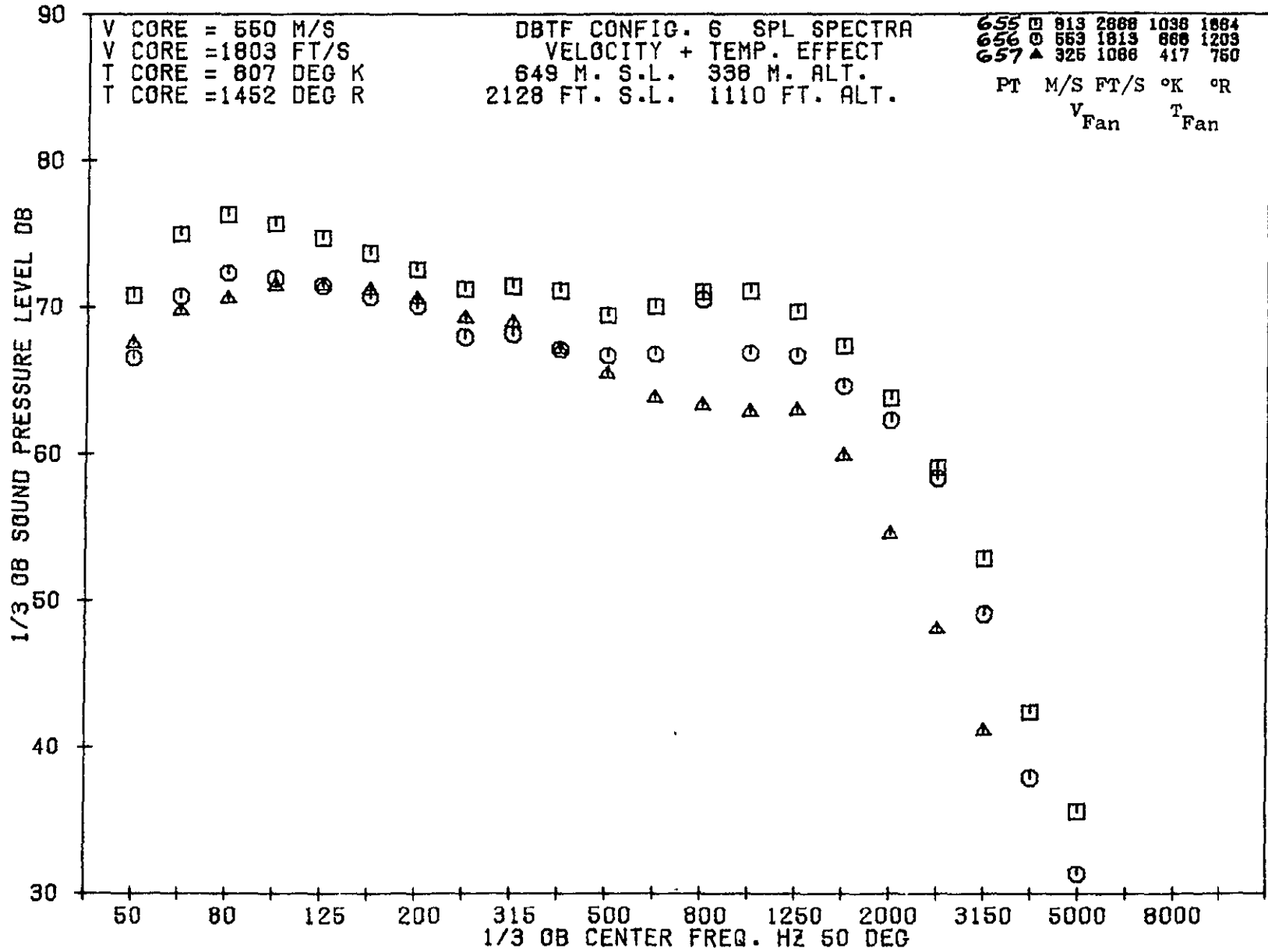


4-267

08/13/75
5R947-001

79 BURQA

1503



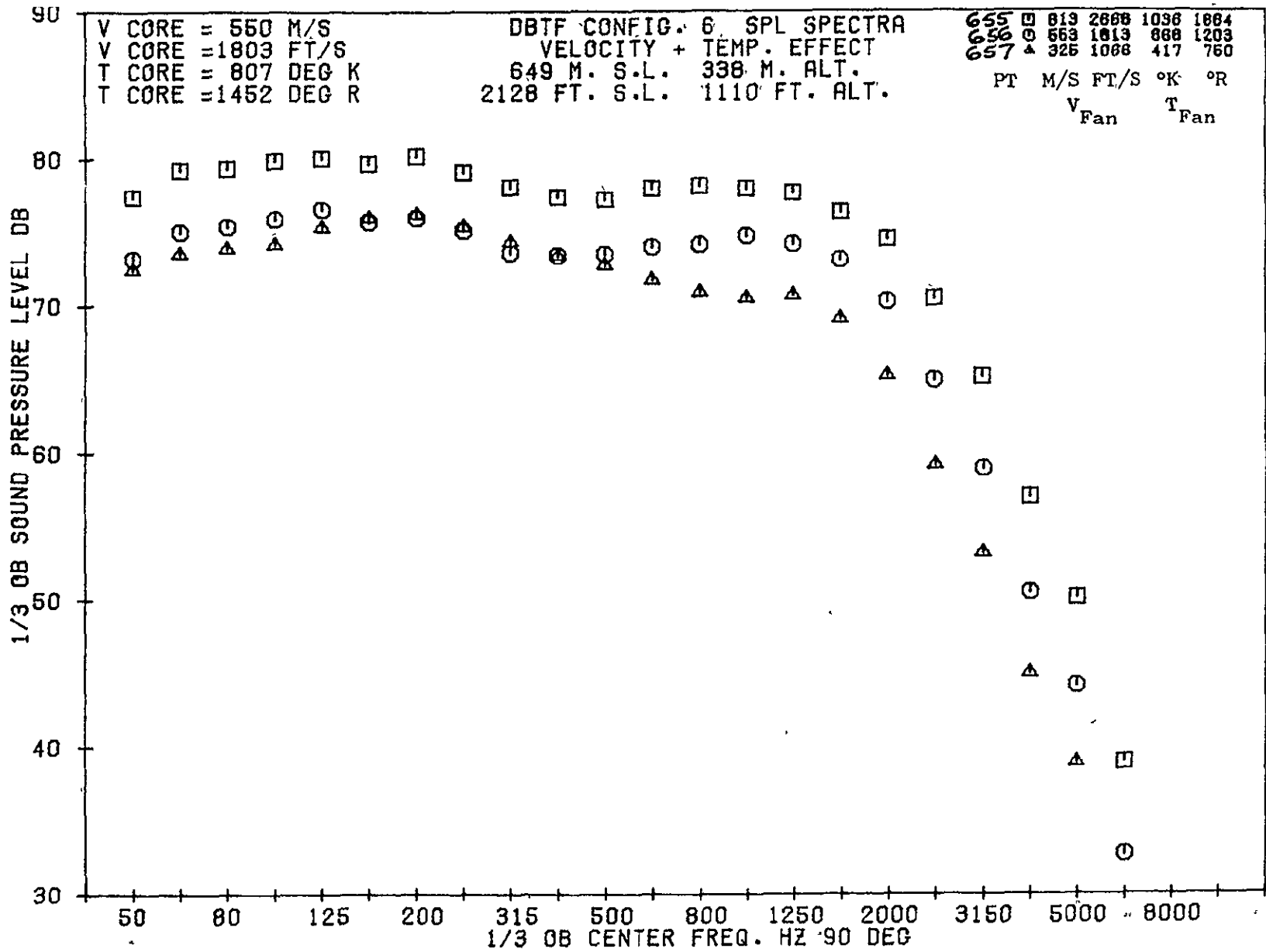
M. 268

08/13/75
5R947-001

79 BURCH A.

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1504

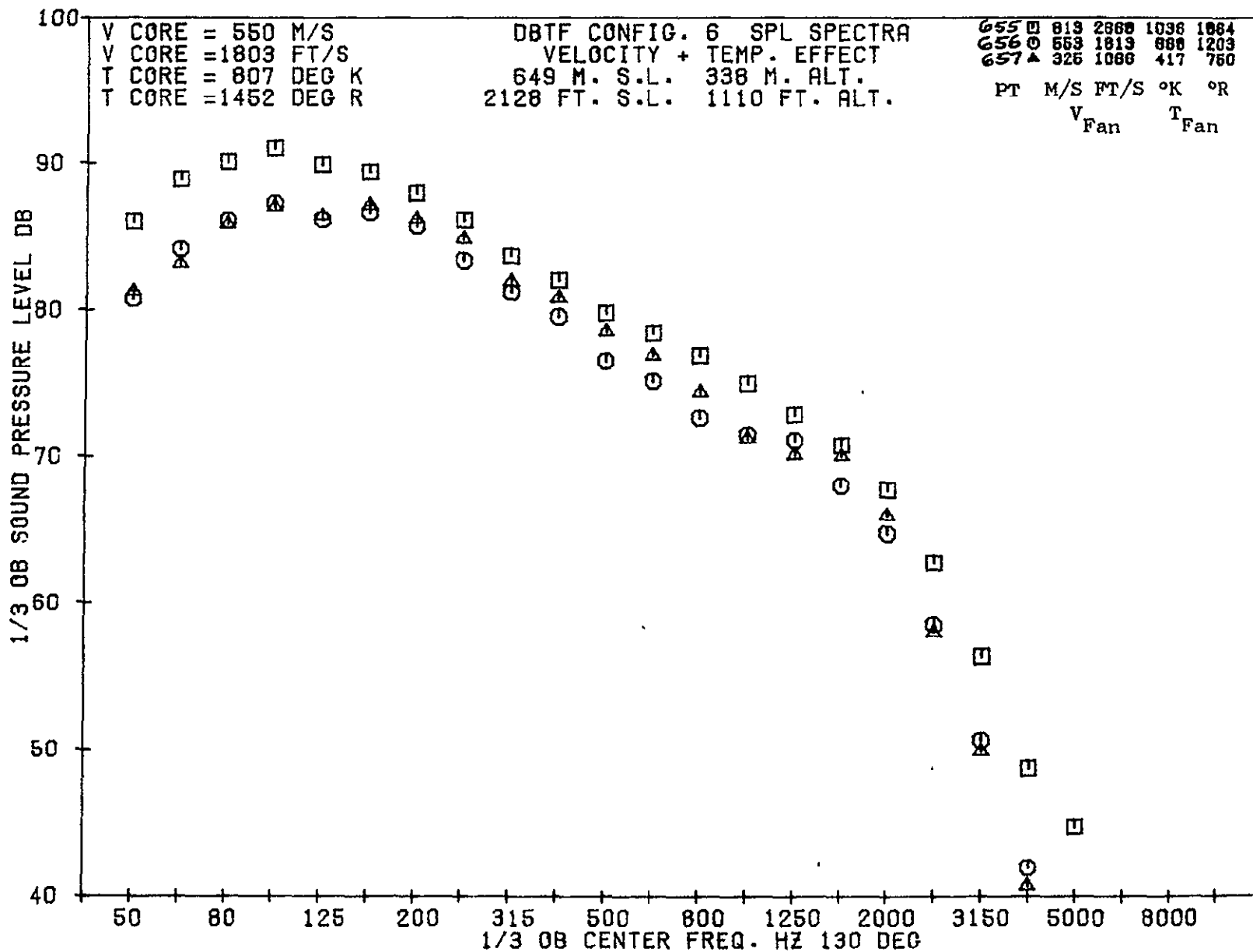


11.269

08/13/75
5R947-001

79 BURCH

1505



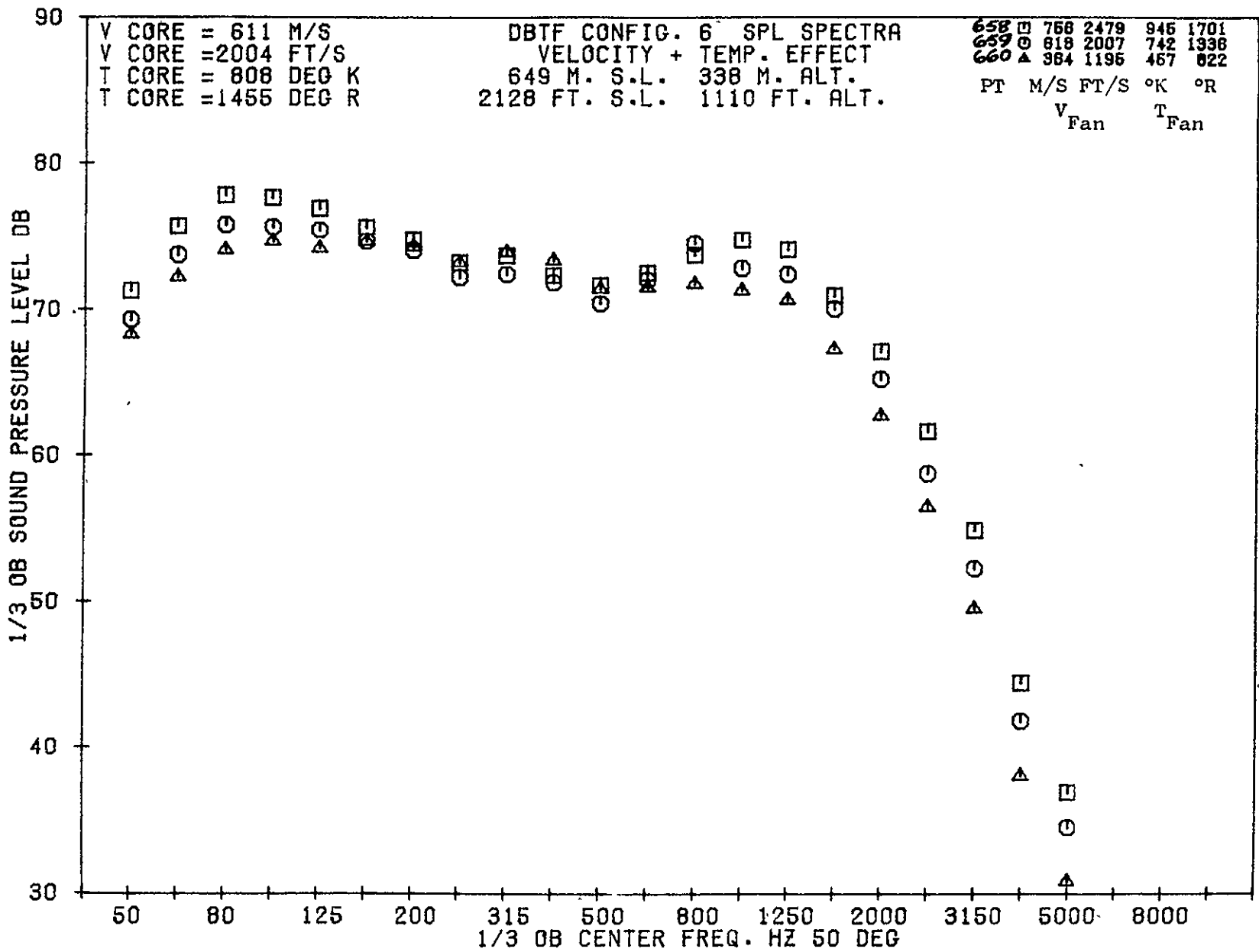
4-270

08/13/75

79 BURCH A.

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1506

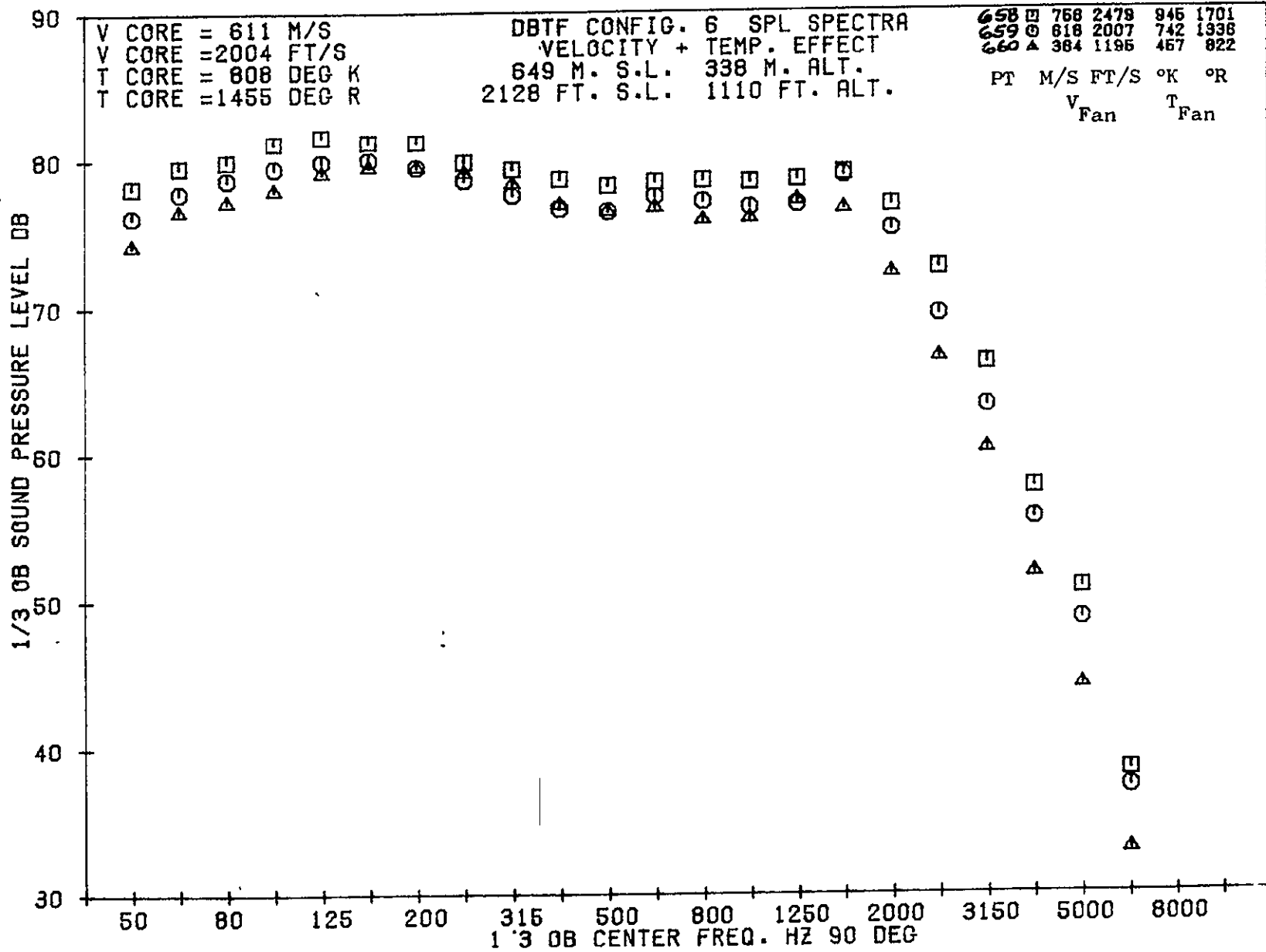


11.7.71

08/13/75
5R947-001

79 BURCOR.

1507



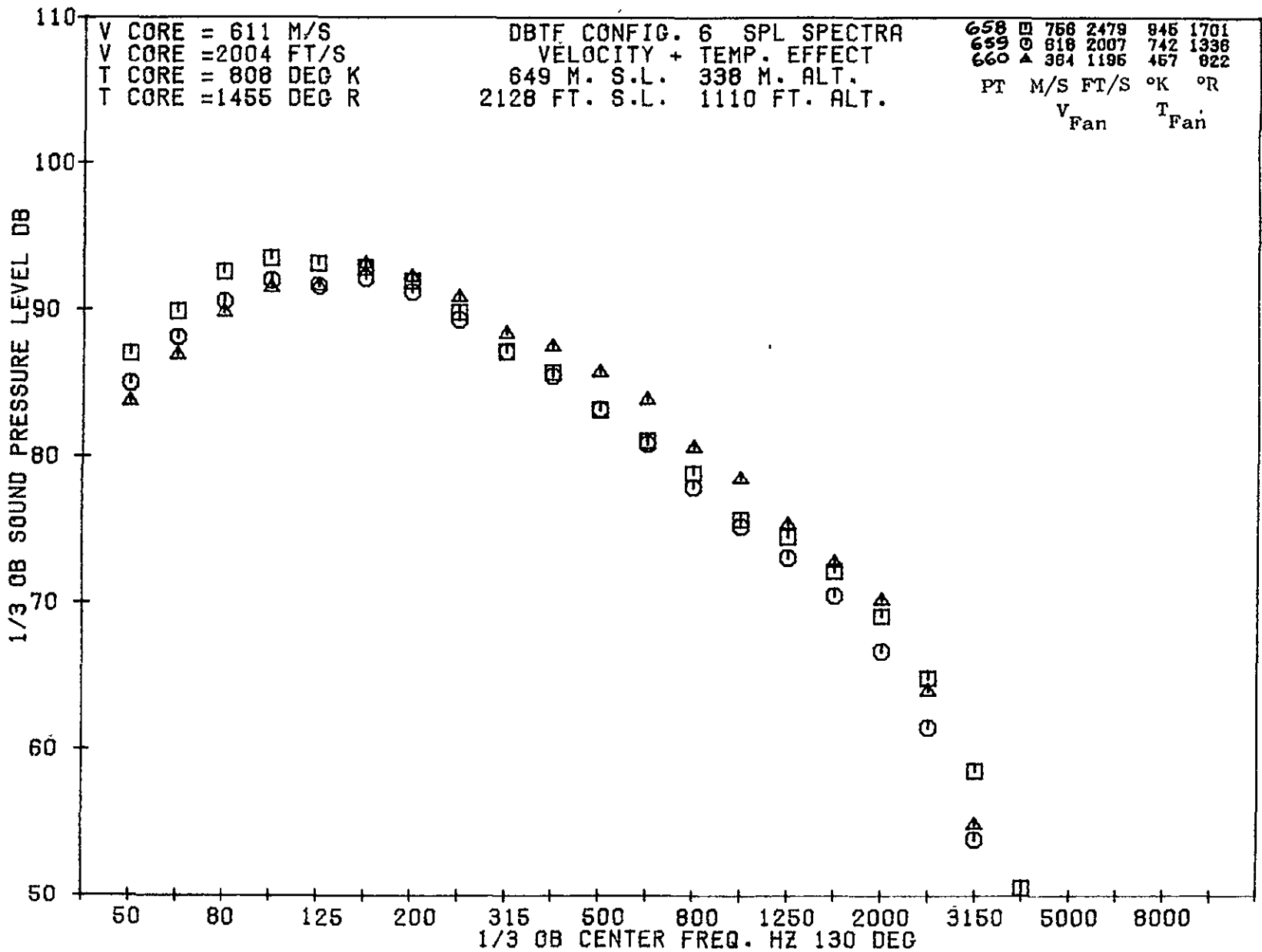
08/13/75
FR947-001

79 BURCH A.

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4-2-75

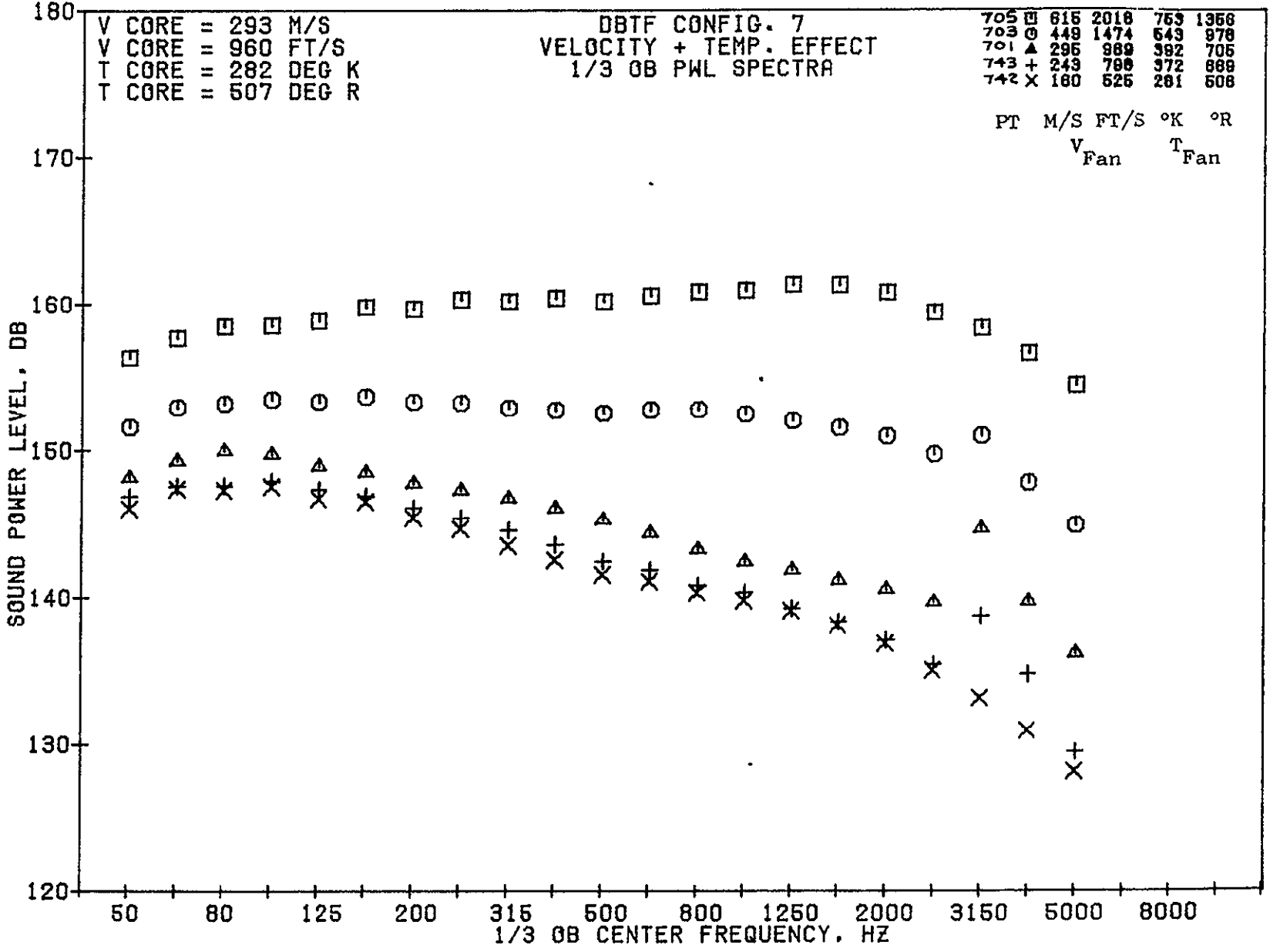
1508



4-273

08/13/75
5R947-001

79 BUR



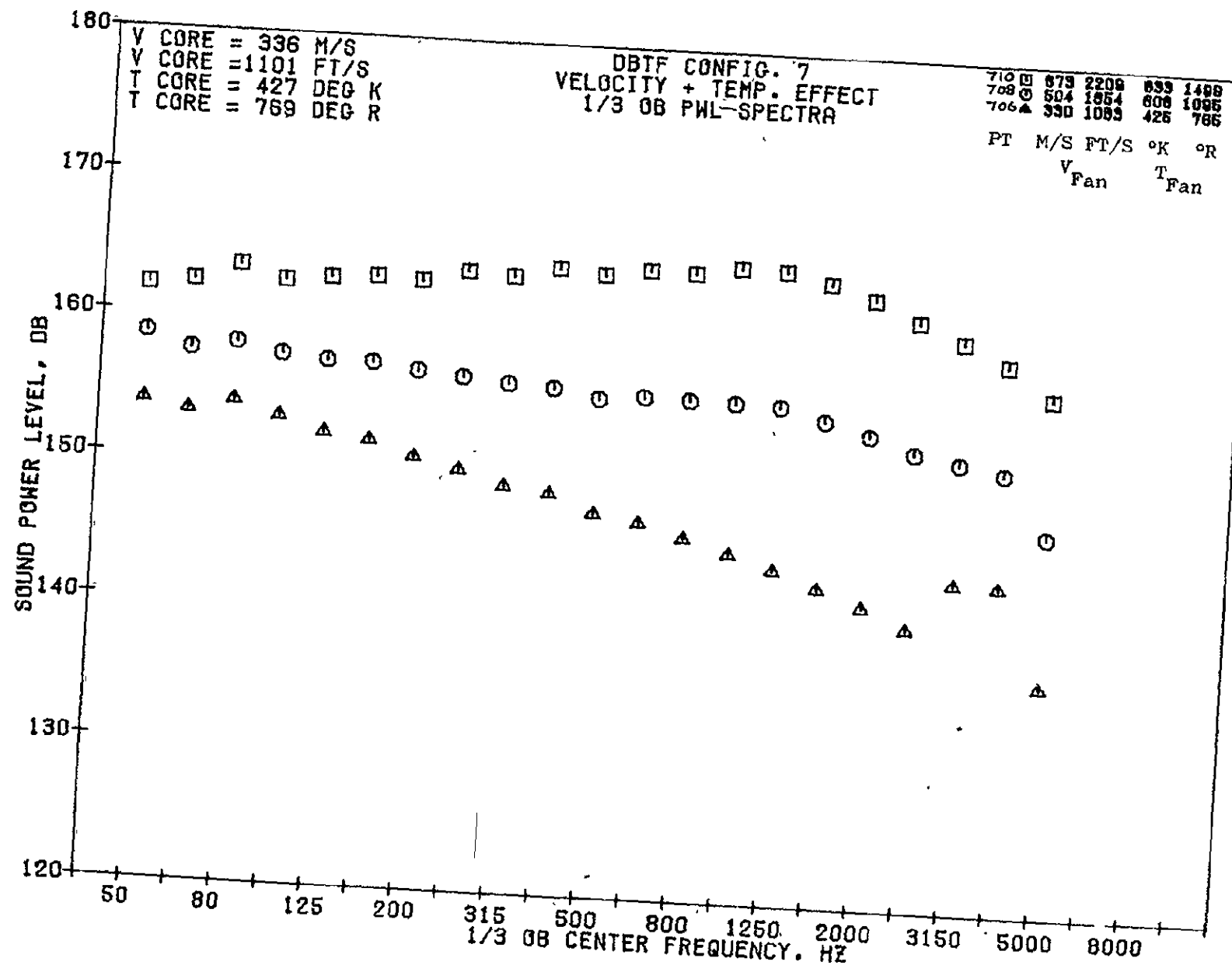
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5R412-001

79 BURCH A.

1-1

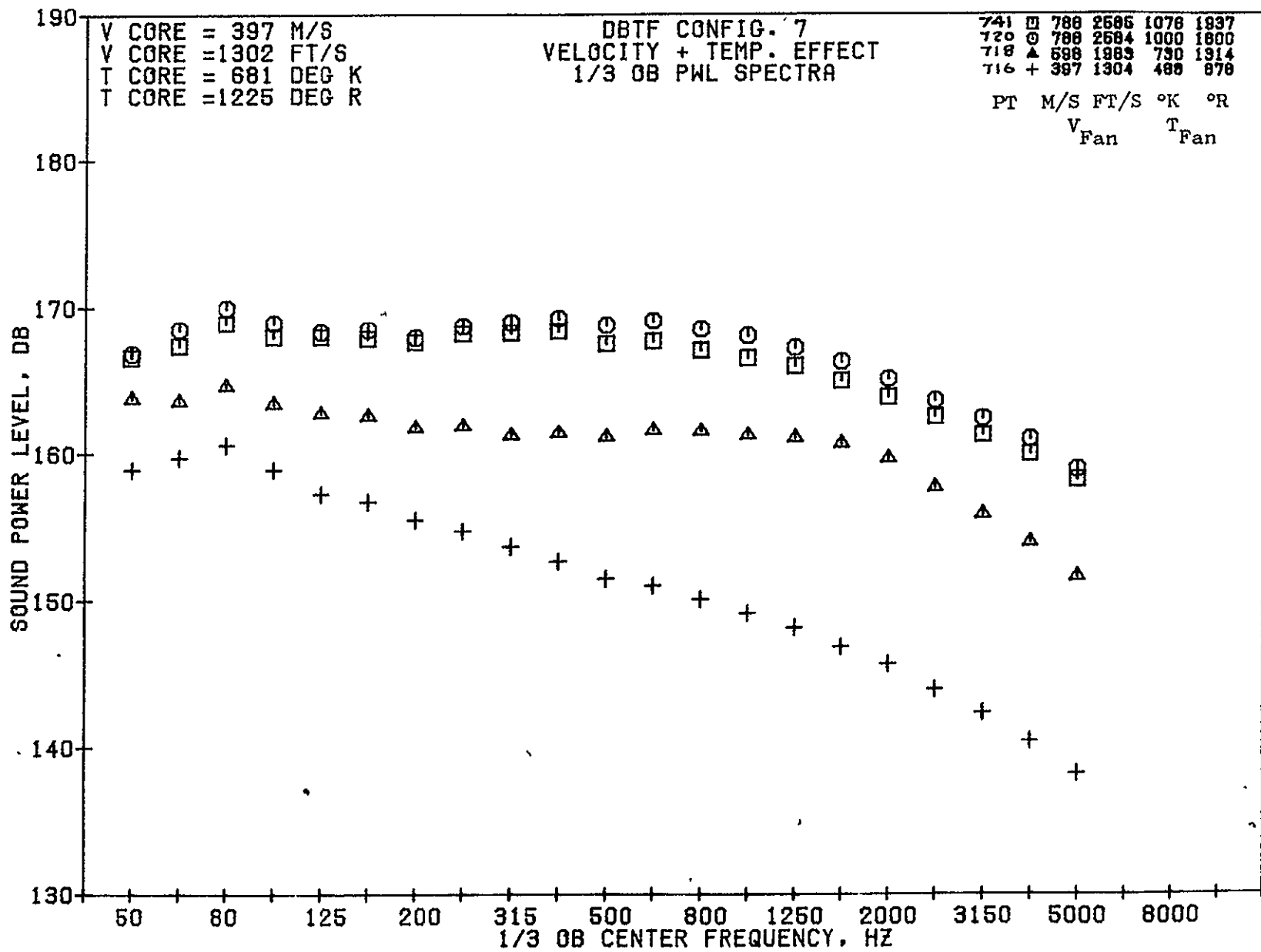
1510



6/26/75

08/22/75
5R682-001

1511

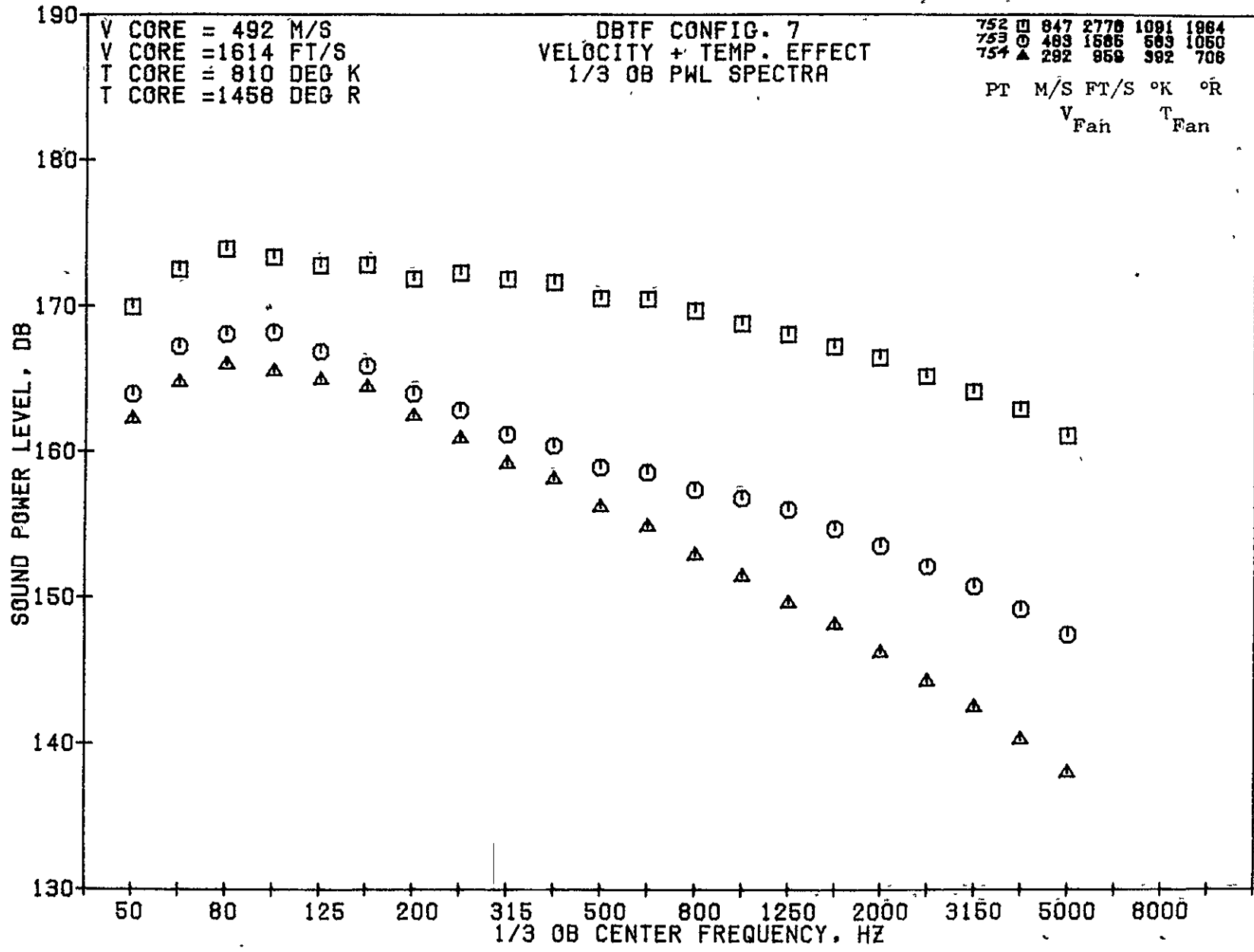


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5R412-001

79 BURCH A.

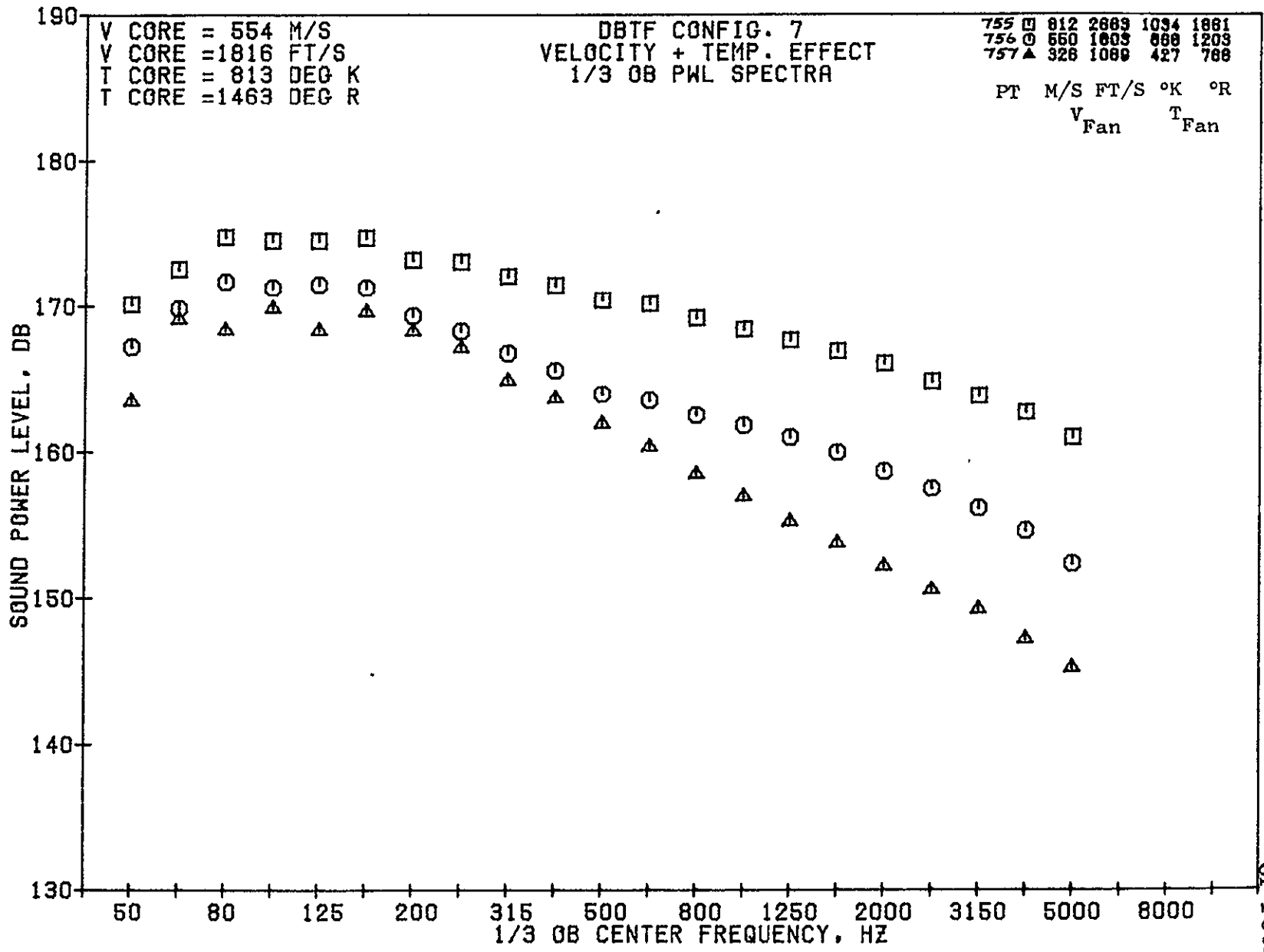
11/19



1.12-1

08/19/75
 5R412-001

79 BURCH A.



1513

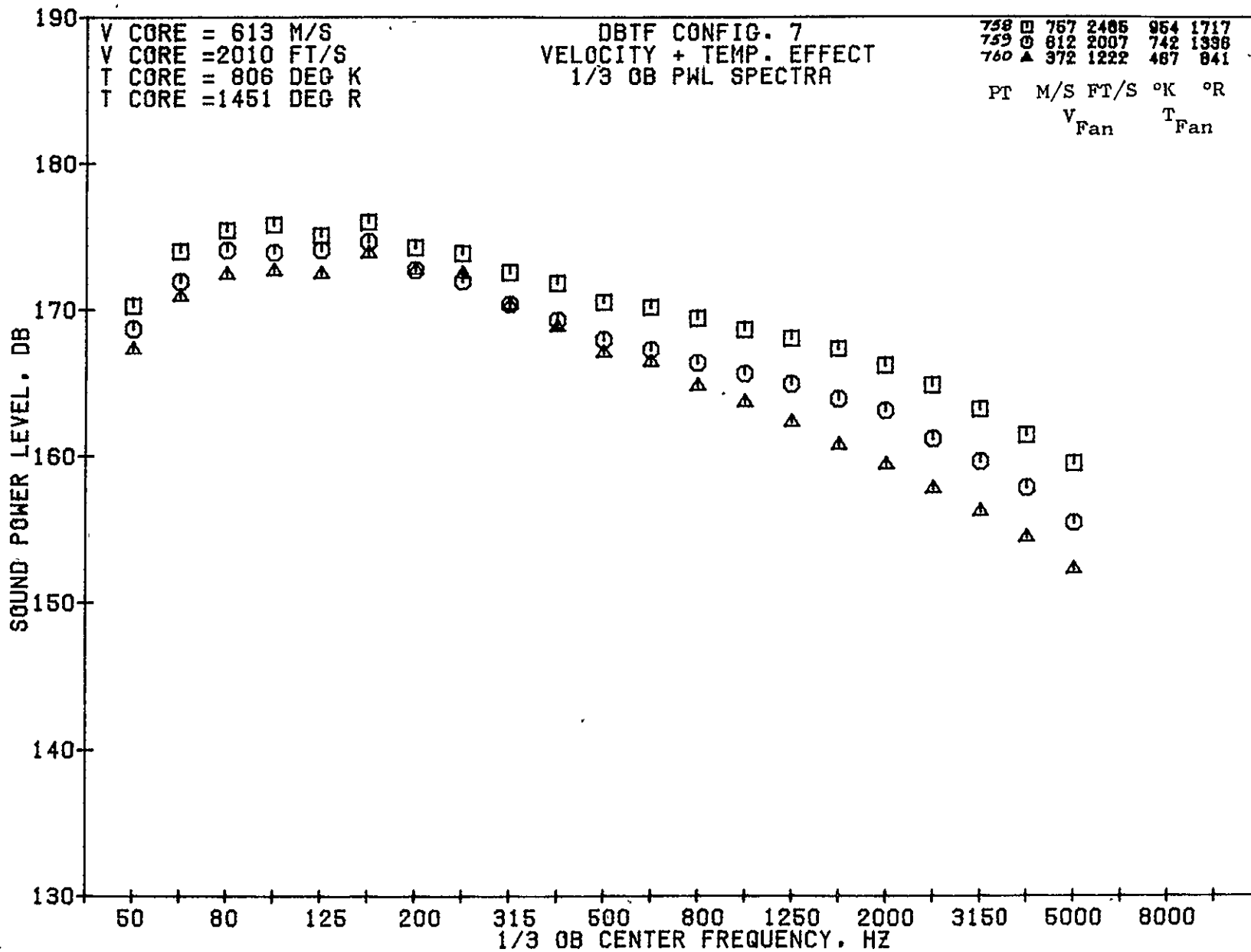
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91.7-1

08/19/75
 5R412-001

79 BURCH A.

1514

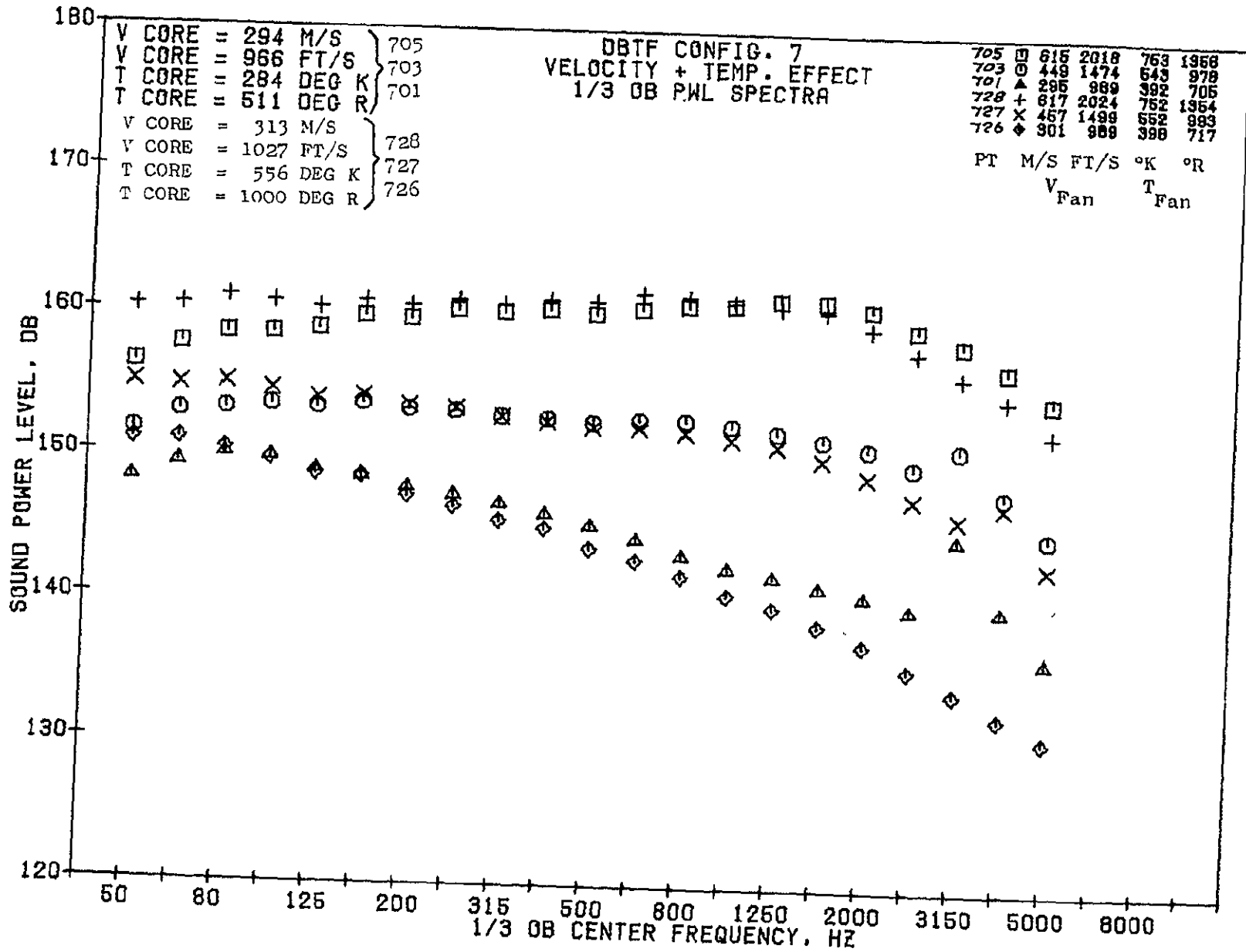


4 219

08/19/75
5R412-001 . . .

79 BURCH A.

1515



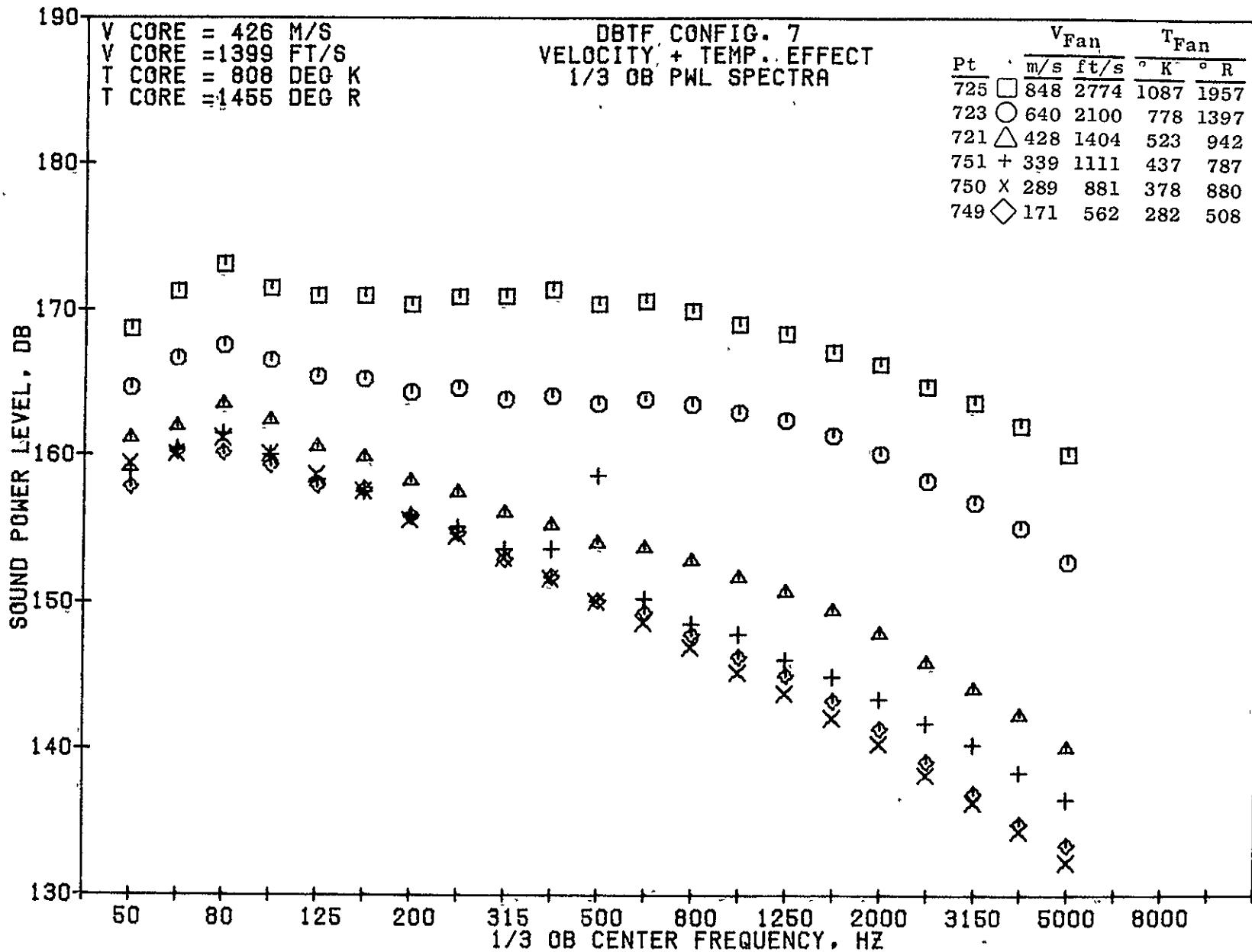
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08/19/75
5R412-001

79 BURCH A.

4.130

1516

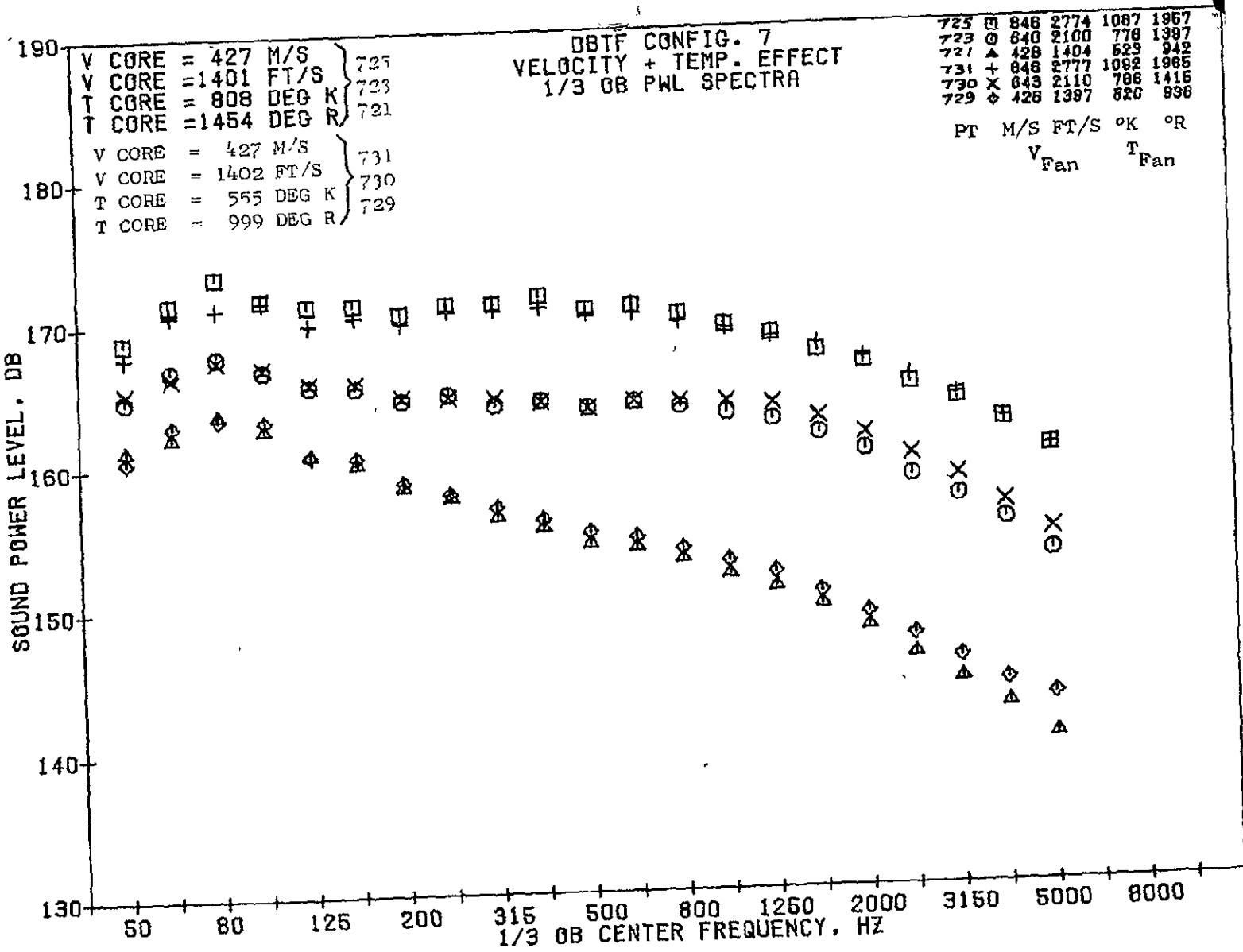


697

08/19/75
 5R412-001

79 BURCH A.

1517



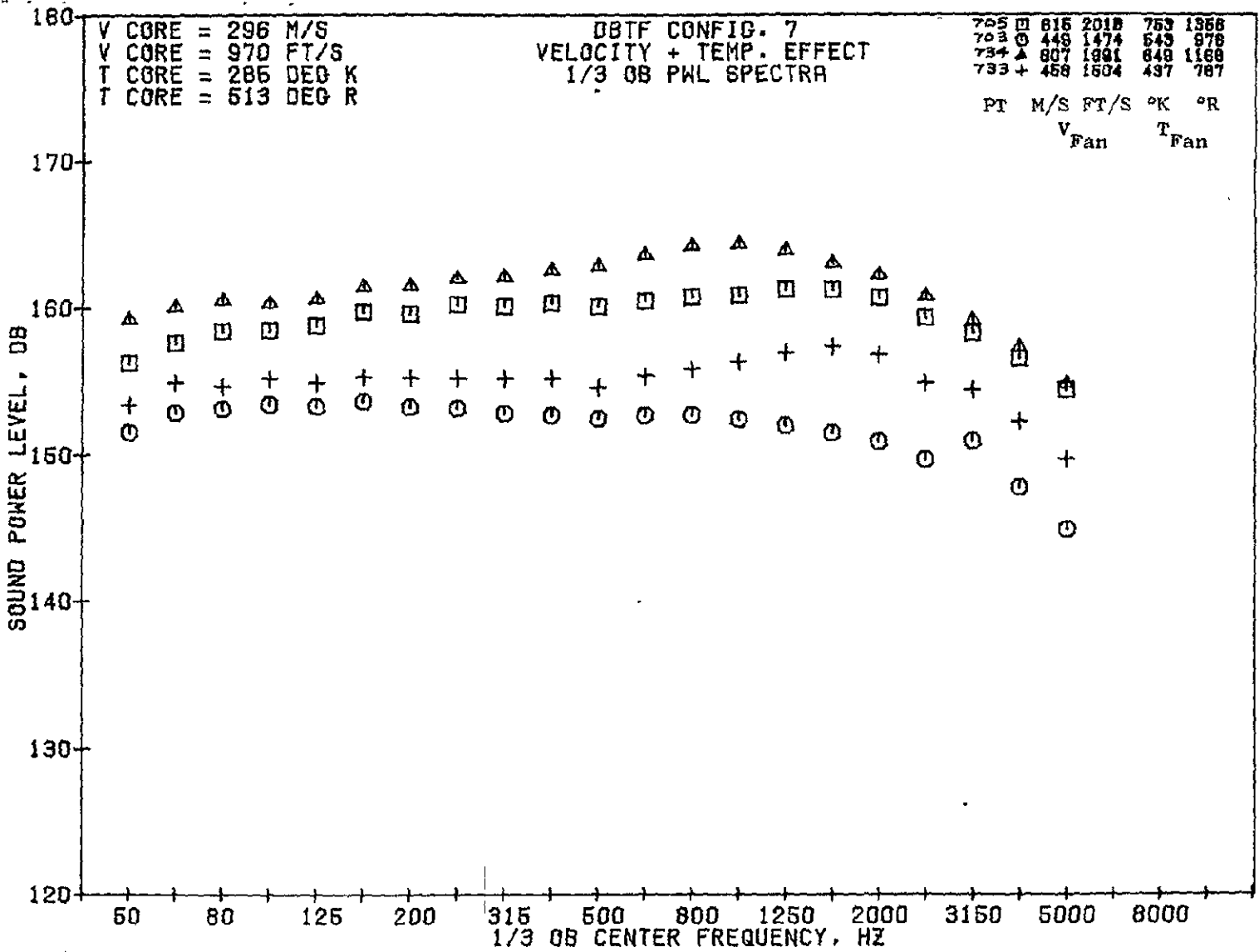
4-281

08/19/75
5R412-001

79 BURCH A.

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8151

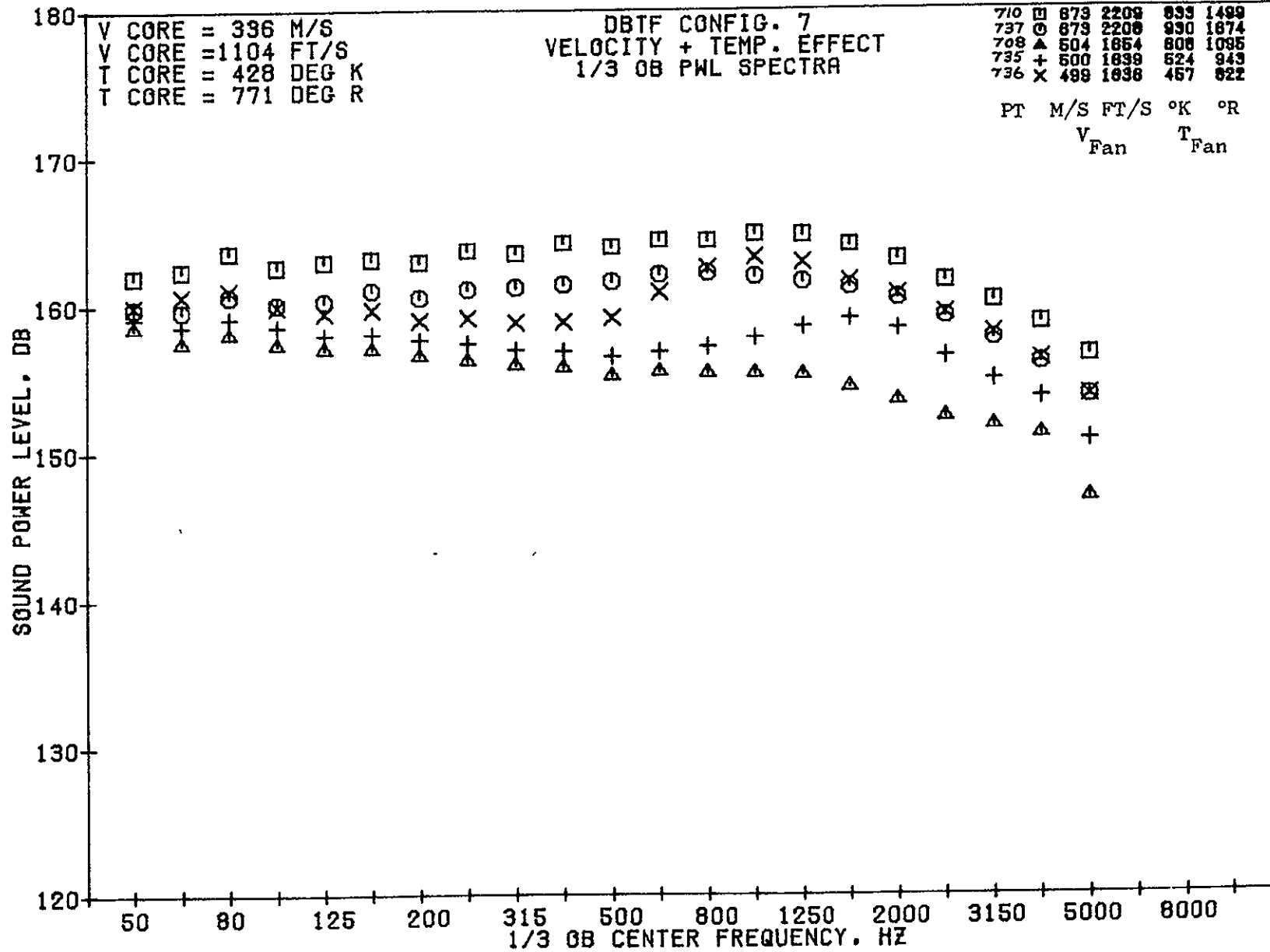


4-28

08/19/75
5R412-001

79 BURCH A.

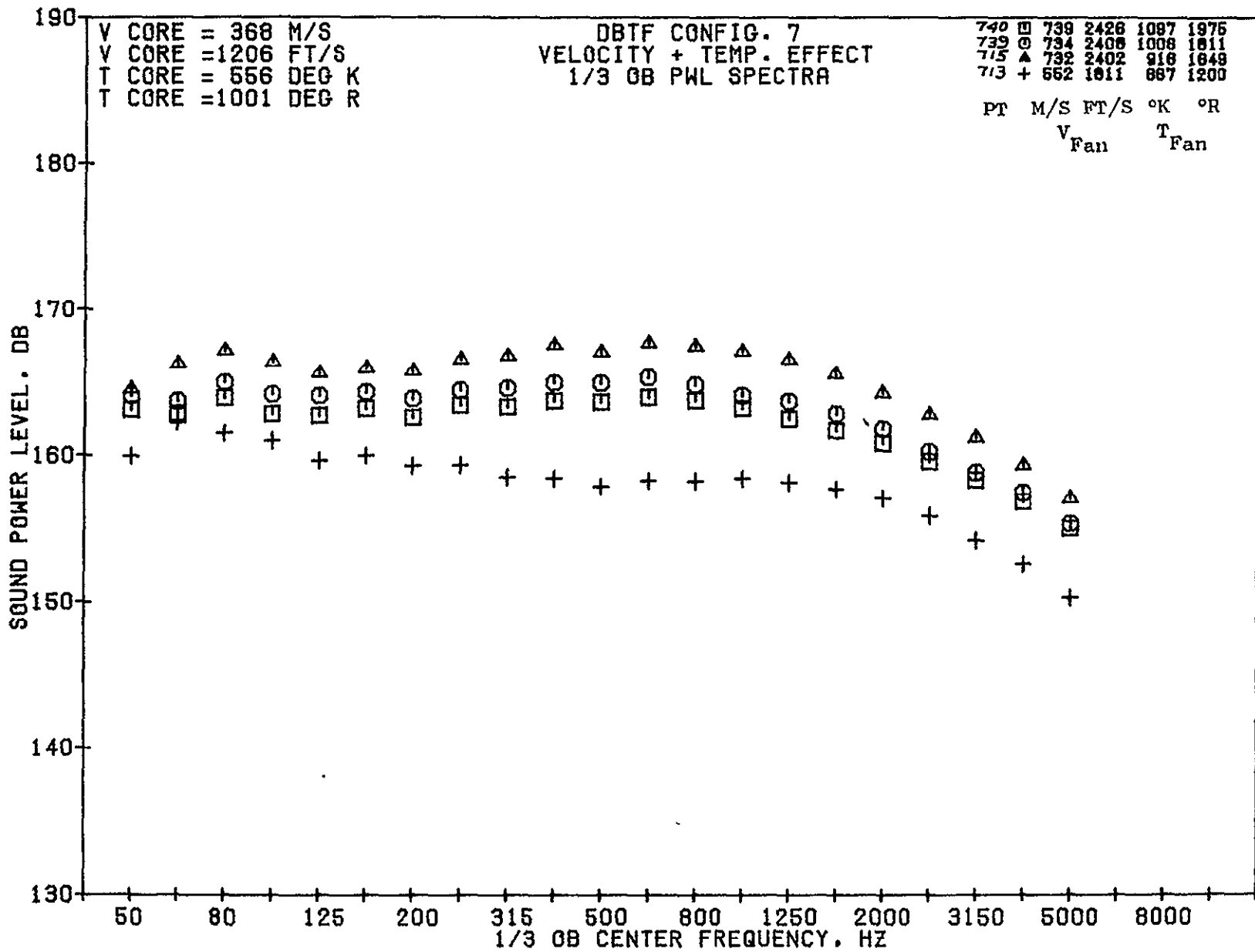
1519



08/22/75
5R682-001

79 BURCH A.

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OF FOUR QUARTS

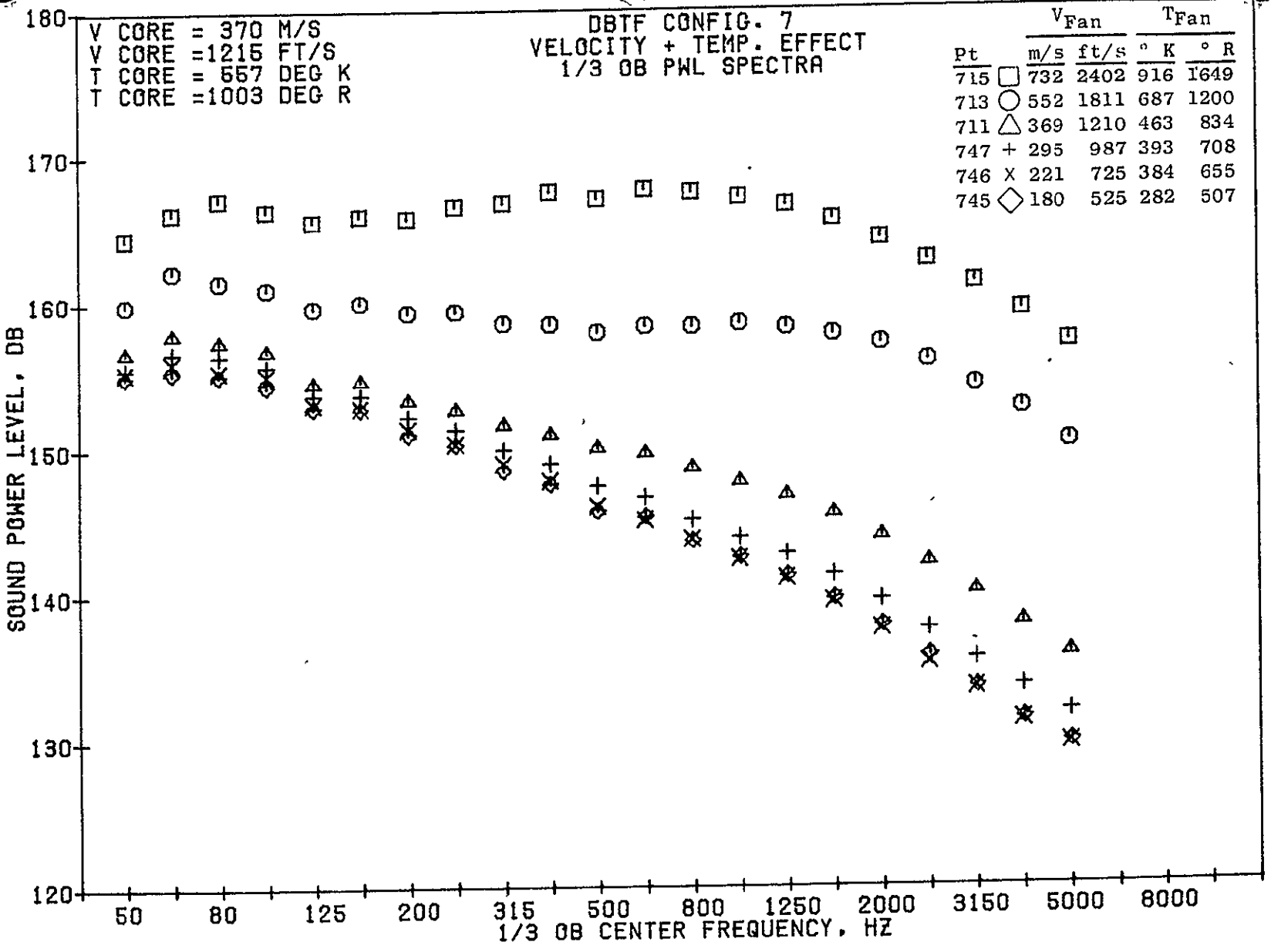


1520

4-284

08/19/75
5R412-001

79 BURGH A.



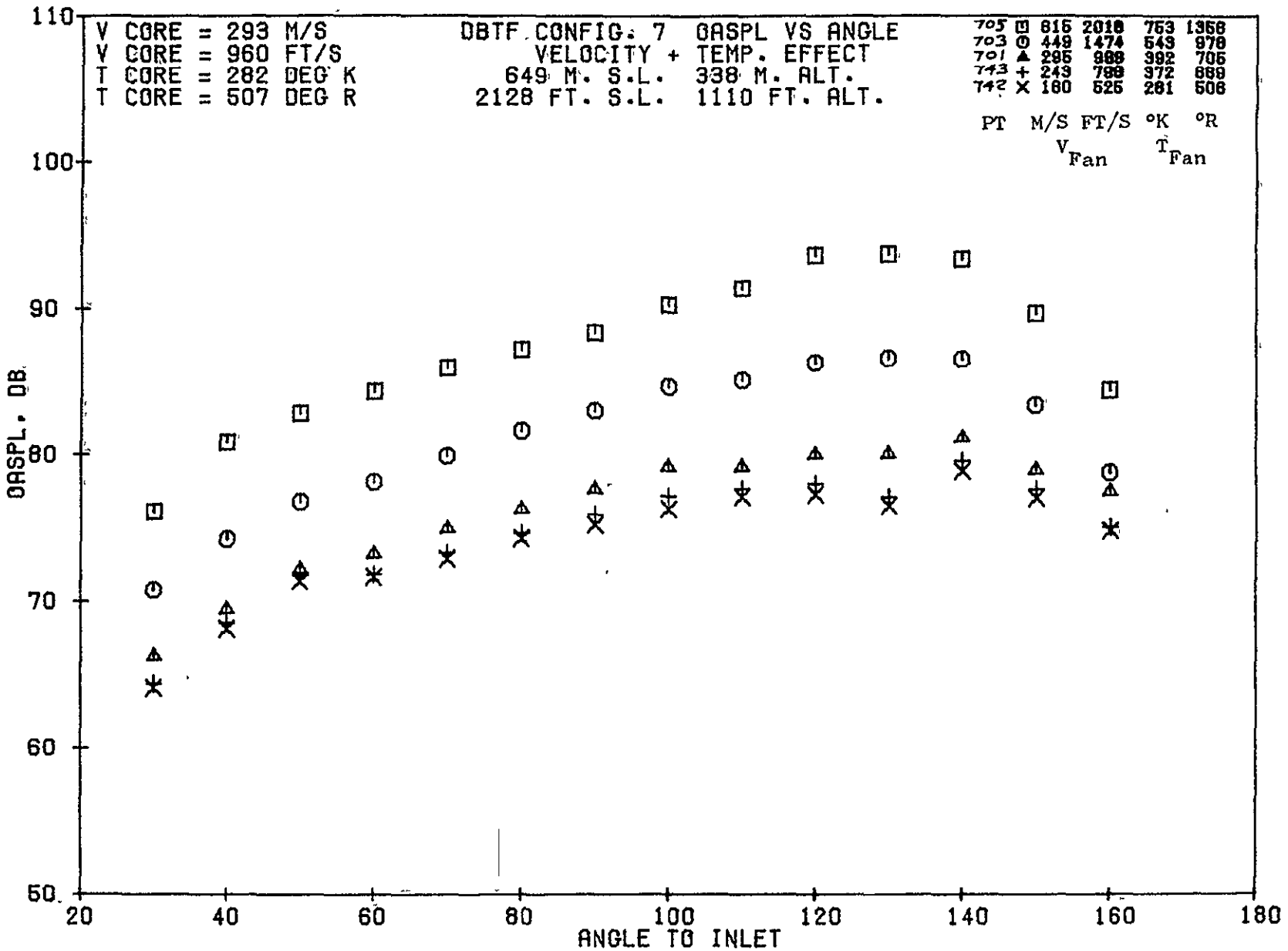
1521

4.68

08/19/75
5R412-001

79 BURCH A.

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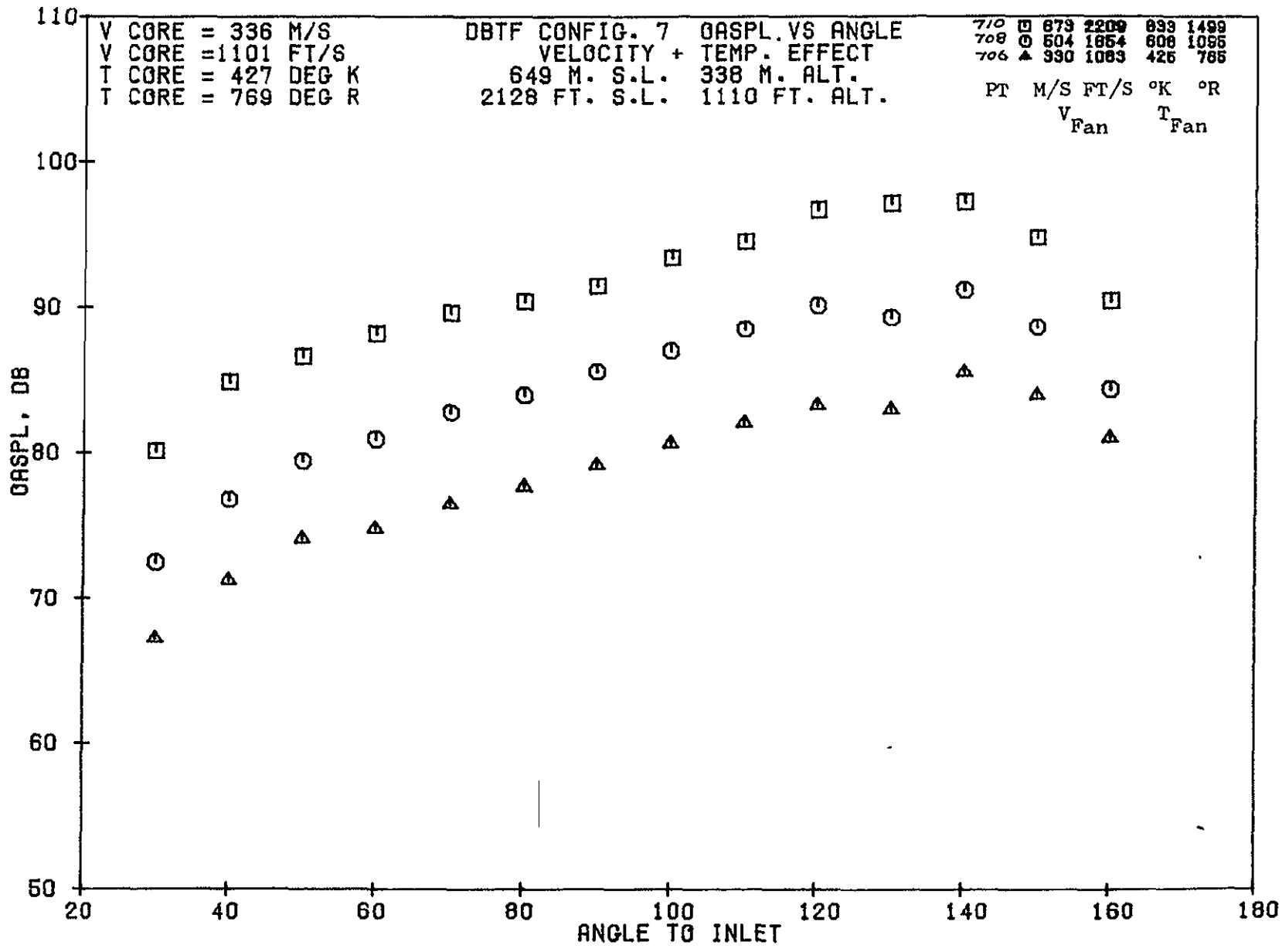


15222

11285

08/19/75
 5R412-001

79 BURCH A.



V CORE = 336 M/S
 V CORE = 1101 FT/S
 T CORE = 427 DEG K
 T CORE = 769 DEG R

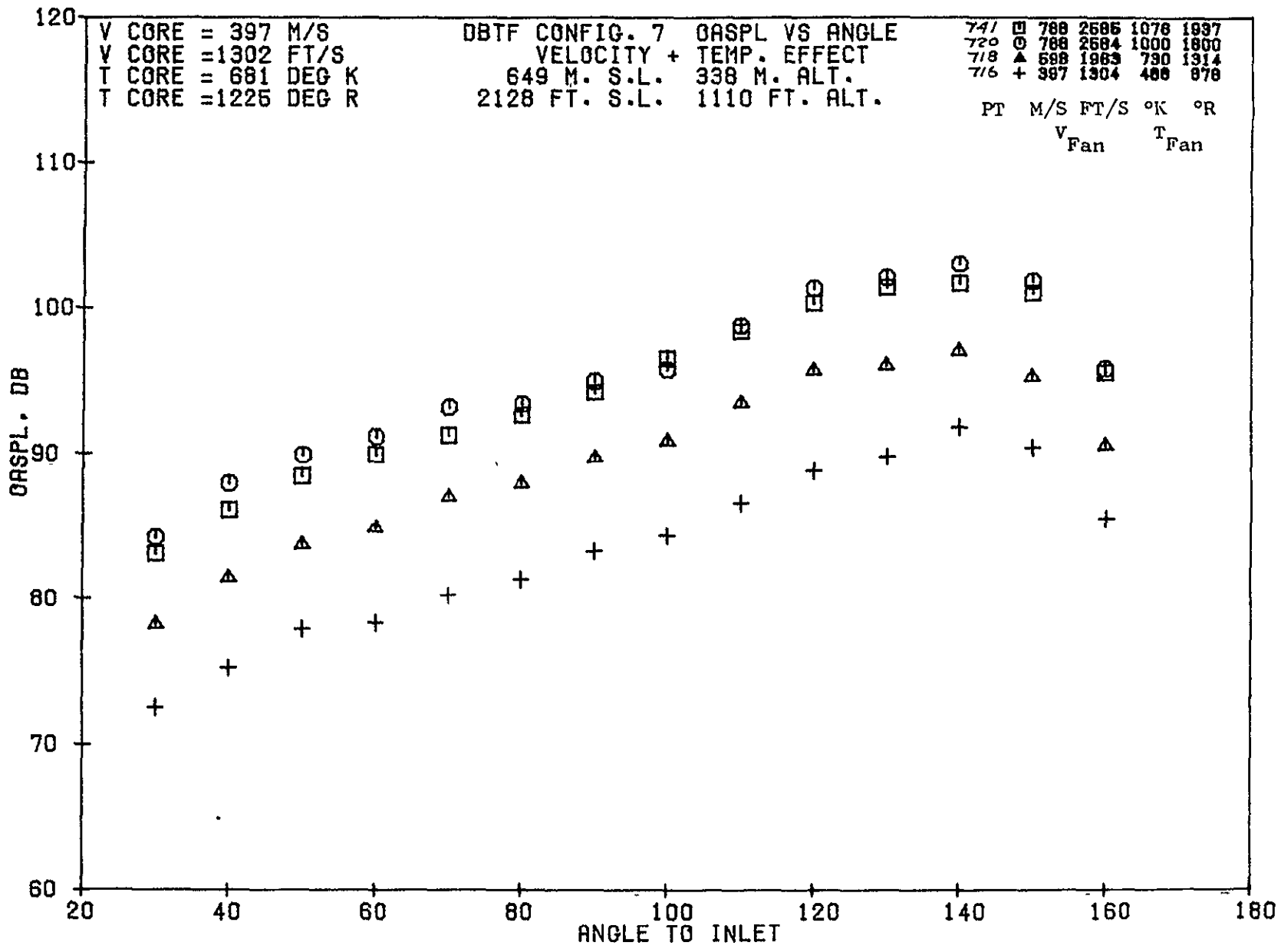
DBTF CONFIG. 7 GASPL. VS ANGLE
 VELOCITY + TEMP. EFFECT
 649 M. S.L. 338 M. ALT.
 2128 FT. S.L. 1110 FT. ALT.

708	706	706	706	706
679	2200	833	1499	
504	1854	808	1095	
390	1083	426	785	
PT	M/S	FT/S	°K	°R
	V _{Fan}		T _{Fan}	

1523

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4-286

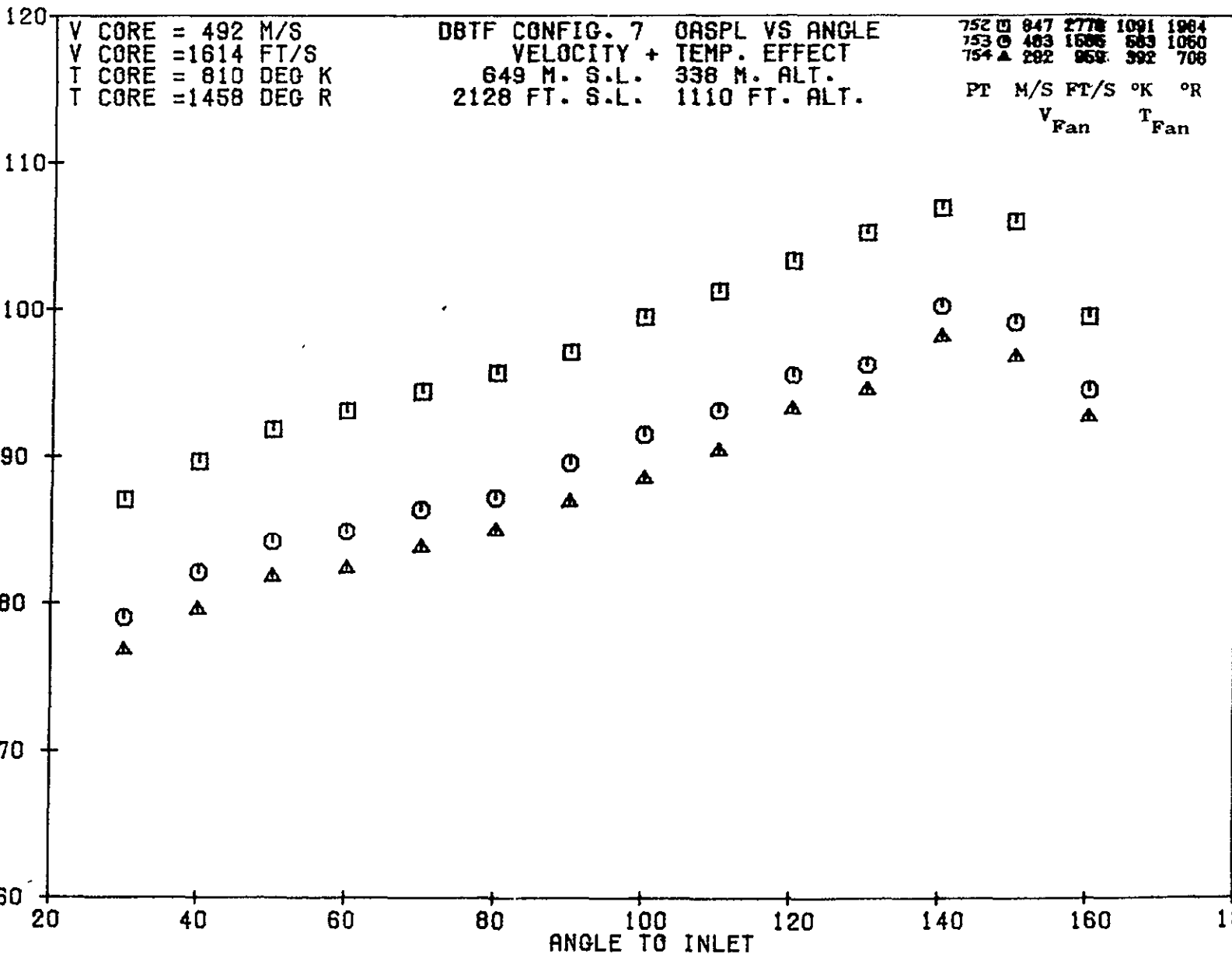


1524

4289

08/19/76
5R412-001

79 BURCH A.



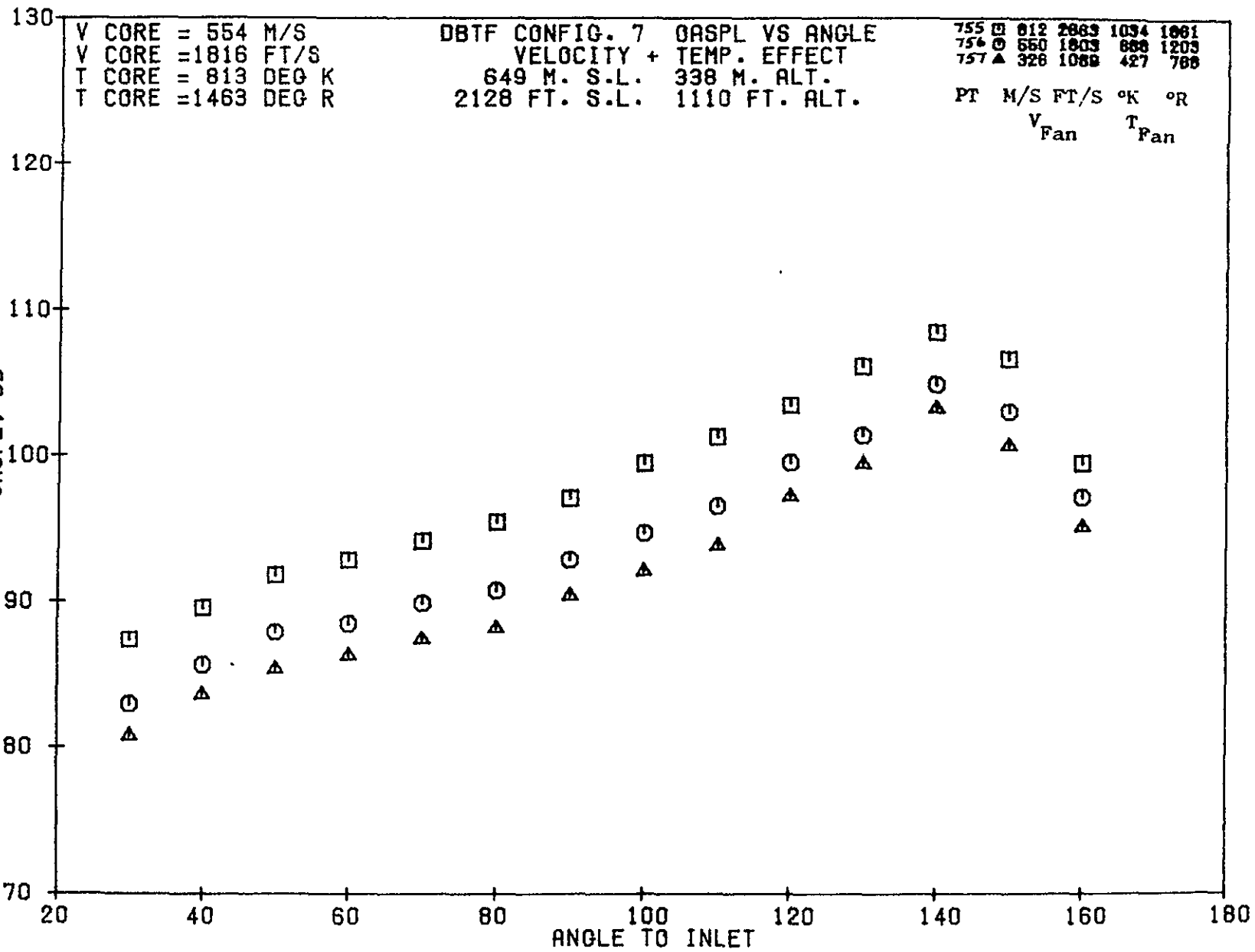
1525

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08/19/75
 5R412-001

79 BURCH A.

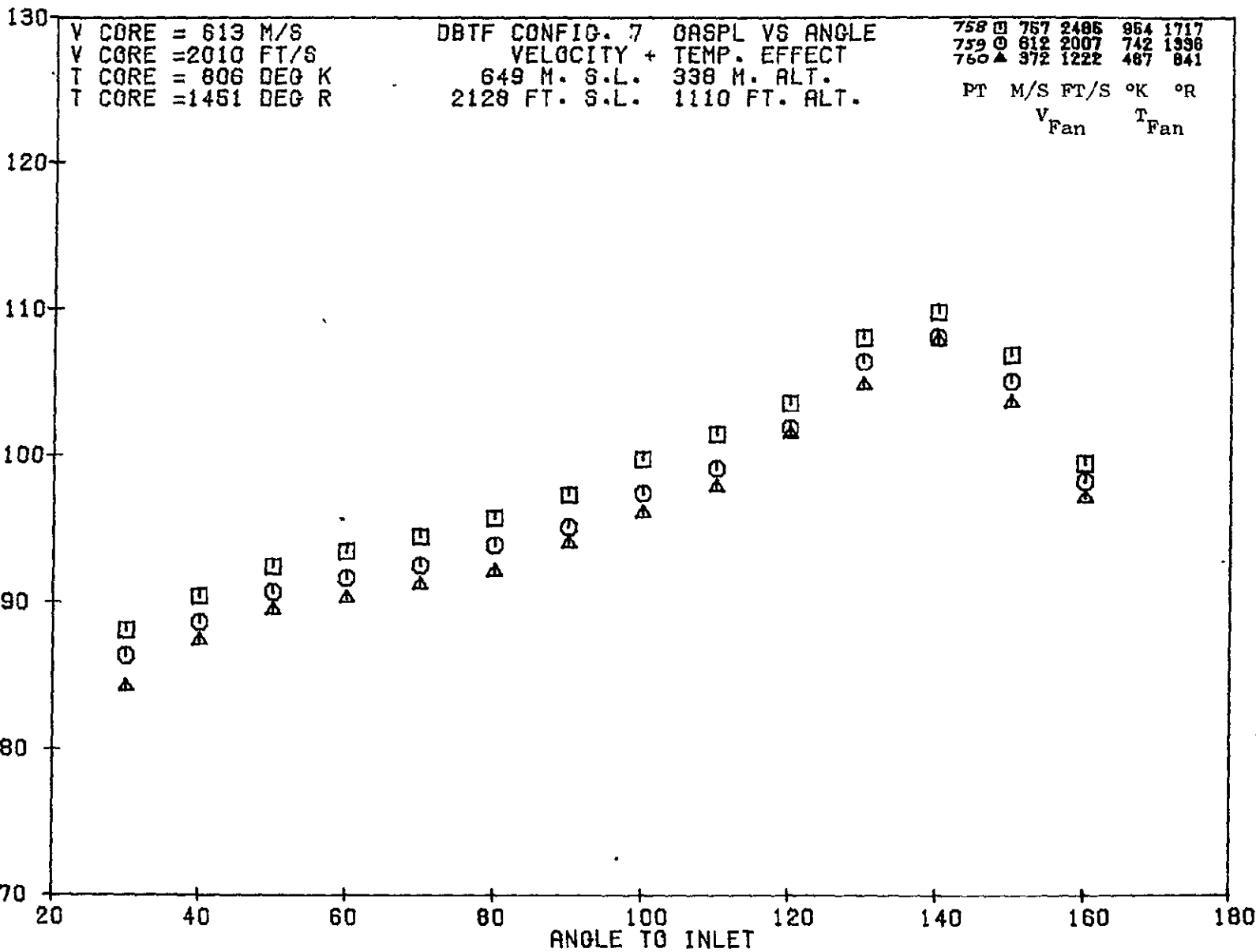
4 258



289

08/19/75
 5R412-001

79 BURGH A.



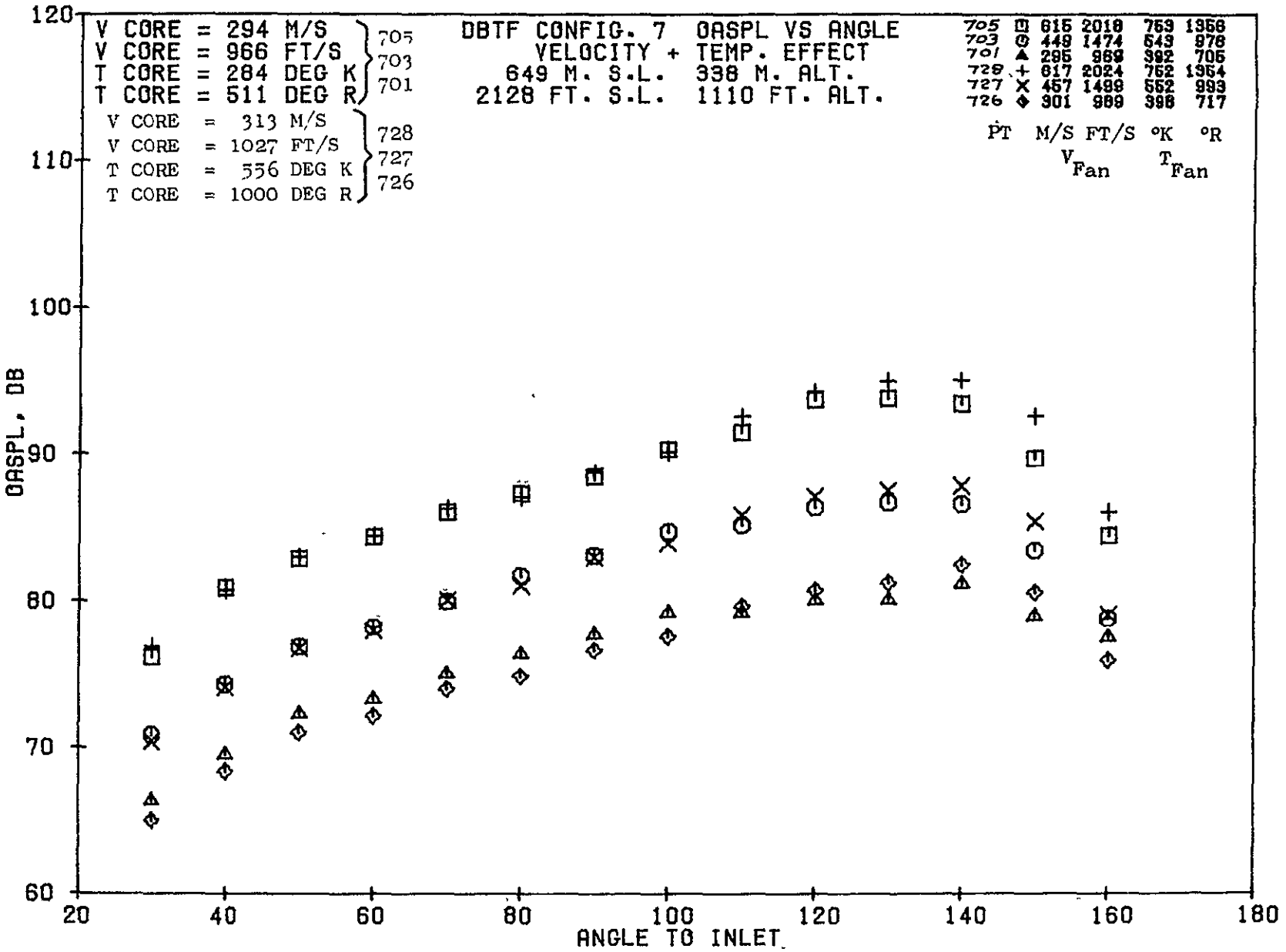
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08/19/75
 RR419-001

79 BURCH A.

4-29

1528



4-291

08/19/75
5R412-001

79 BUR A.

120
110
100
90
80
70
60

V CORE = 427 M/S } 725
 V CORE = 1401 FT/S } 723
 T CORE = 808 DEG K } 721
 T CORE = 1454 DEG R }
 V CORE = 427 M/S } 731
 V CORE = 1402 FT/S } 730
 T CORE = 555 DEG K } 729
 T CORE = 999 DEG R }

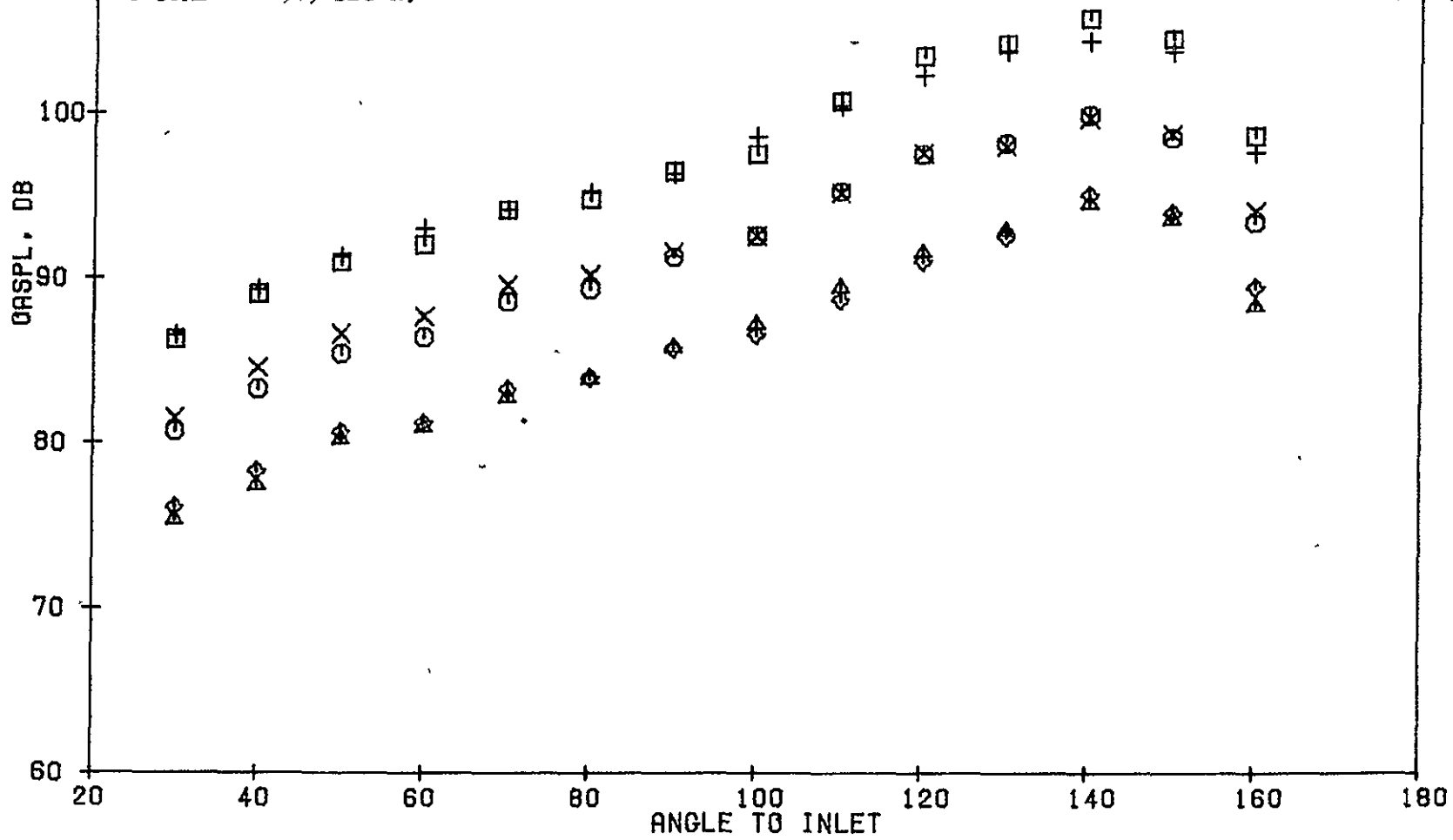
DBTF CONFIG 7 GASPL VS ANGLE
 VELOCITY + TEMP. EFFECT
 649 M. S.L. 338 M. ALT.
 2128 FT. S.L. 1110 FT. ALT.

725	□	848	2774	1087	1957
723	○	840	2100	778	1397
721	▲	428	1404	523	842
731	+	848	2777	1082	1865
730	X	843	2110	786	1416
729	◆	428	1397	520	838

PT M/S FT/S °K °R
 V Fan T Fan

GASPL, DB

ANGLE TO INLET



1529

08/19/75
 5R412-001

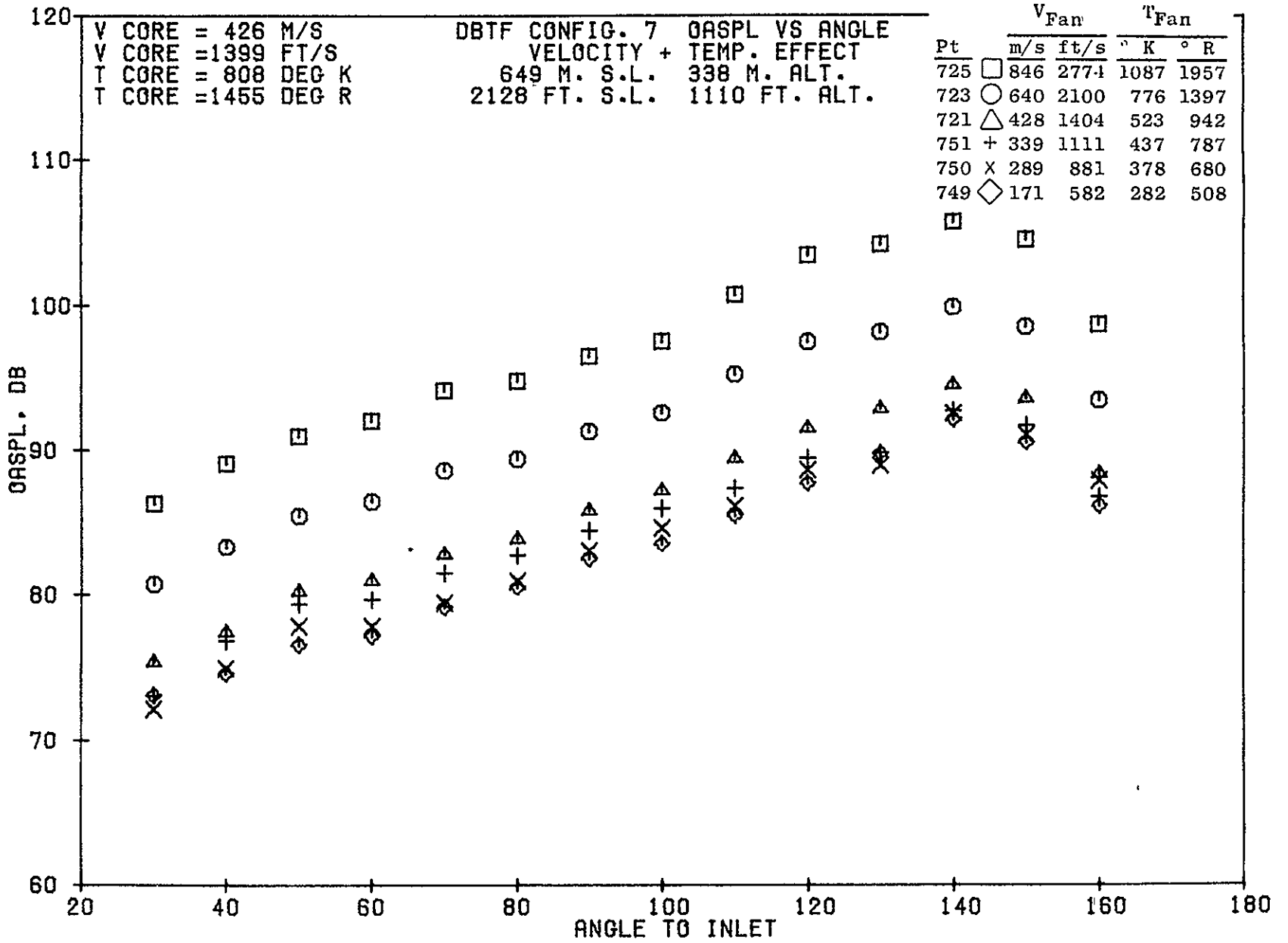
79 BURCH A.

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11.297

0-4

1530



8.7

08/19/75
5R412-001

79 BURMAN A.

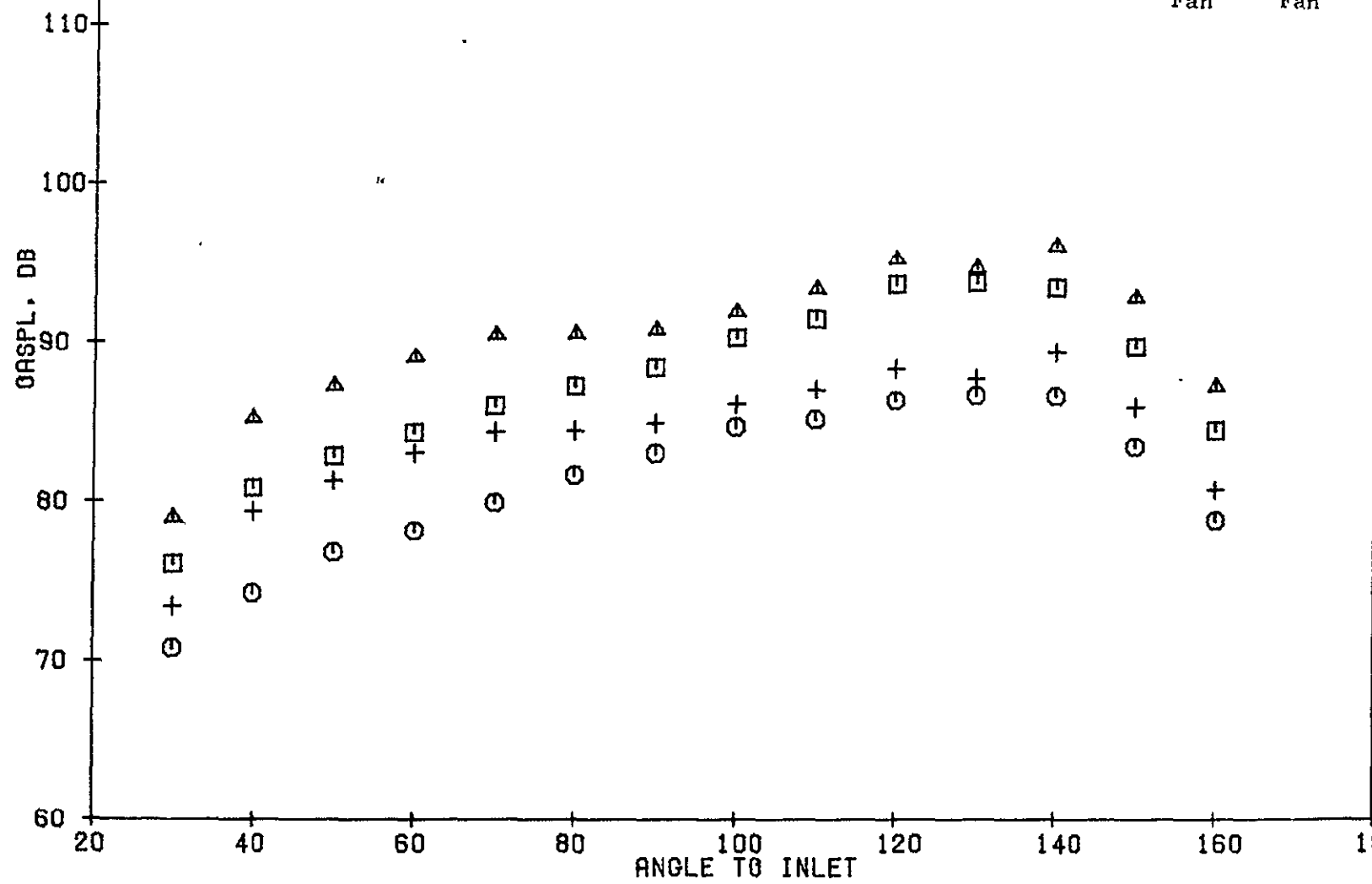
V CORE = 296 M/S
 V CORE = 970 FT/S
 T CORE = 285 DEG K
 T CORE = 513 DEG R

DBTF CONFIG. 7 GASPL VS ANGLE
 VELOCITY + TEMP. EFFECT
 649 M. S.L. 338 M. ALT.
 2128 FT. S.L. 1110 FT. ALT.

705	□	615	2018	759	1358
703	○	448	1474	543	978
734	△	807	1991	849	1188
733	+	458	1504	437	787

PT M/S FT/S °K °R
 V_{Fan} T_{Fan}

1531



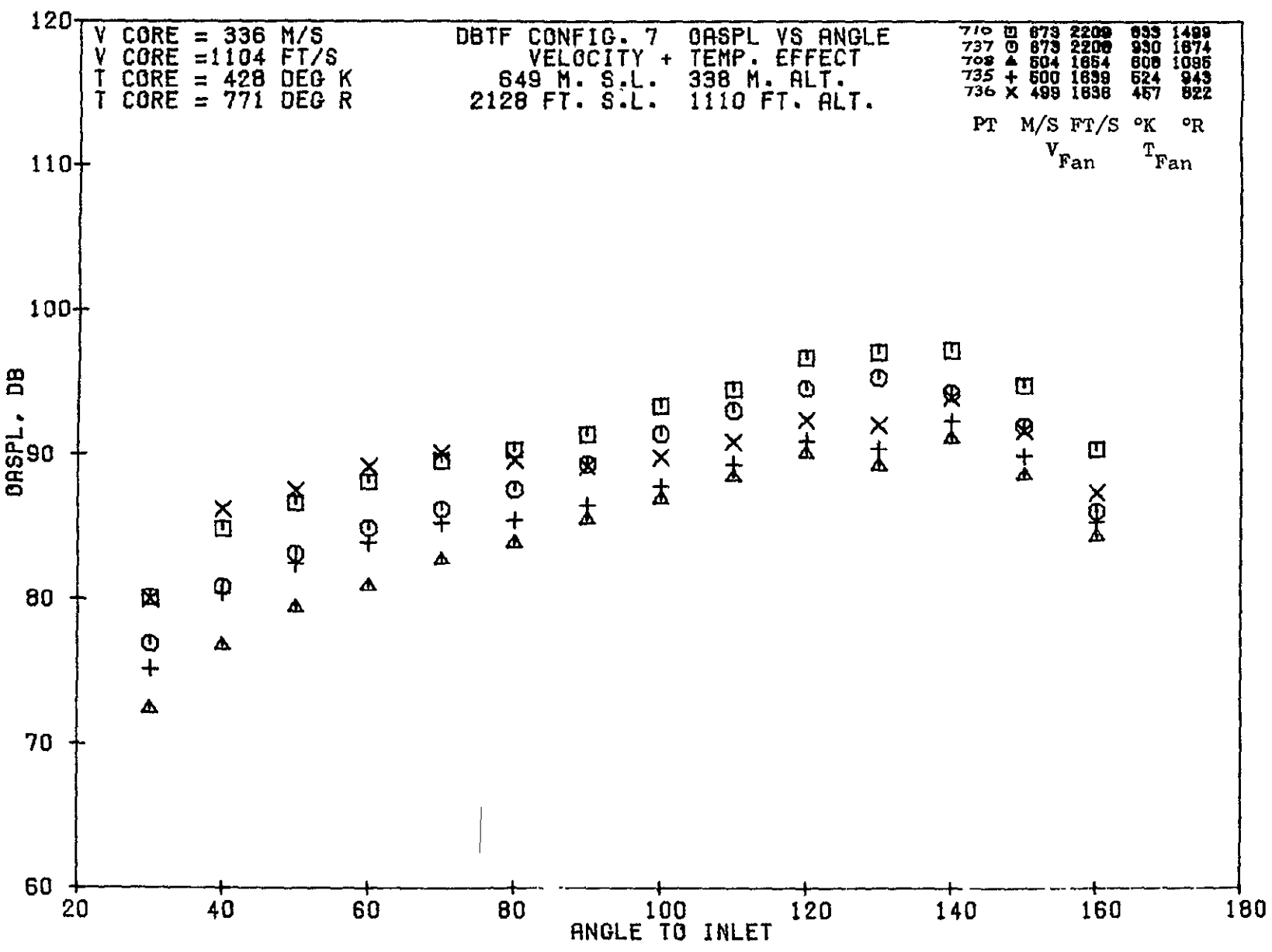
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4293

08/19/75
5R412-001

79 BURCH A.

1532

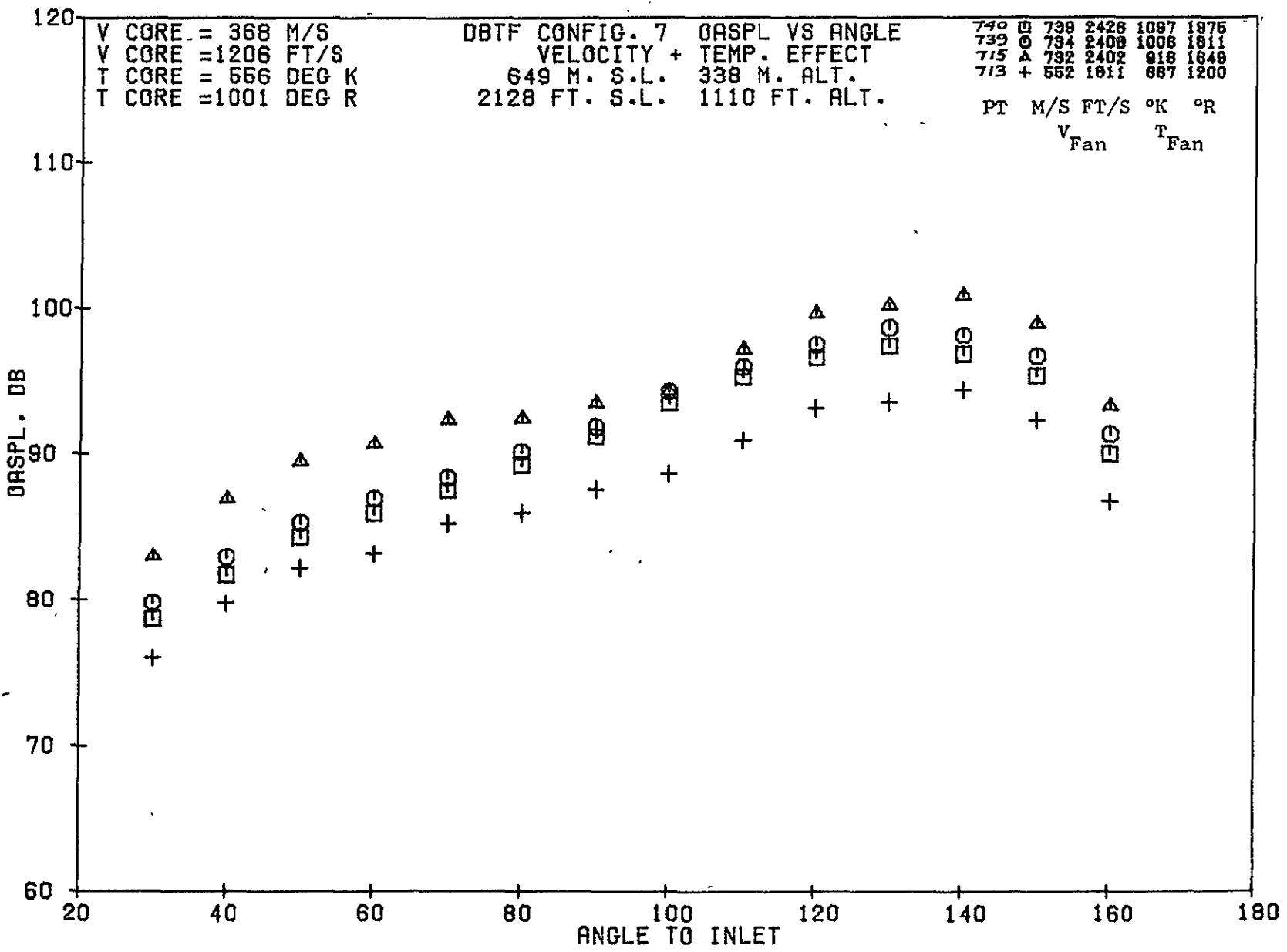


4-294

08/22/75
5R682-001

79 BUR A.

1533

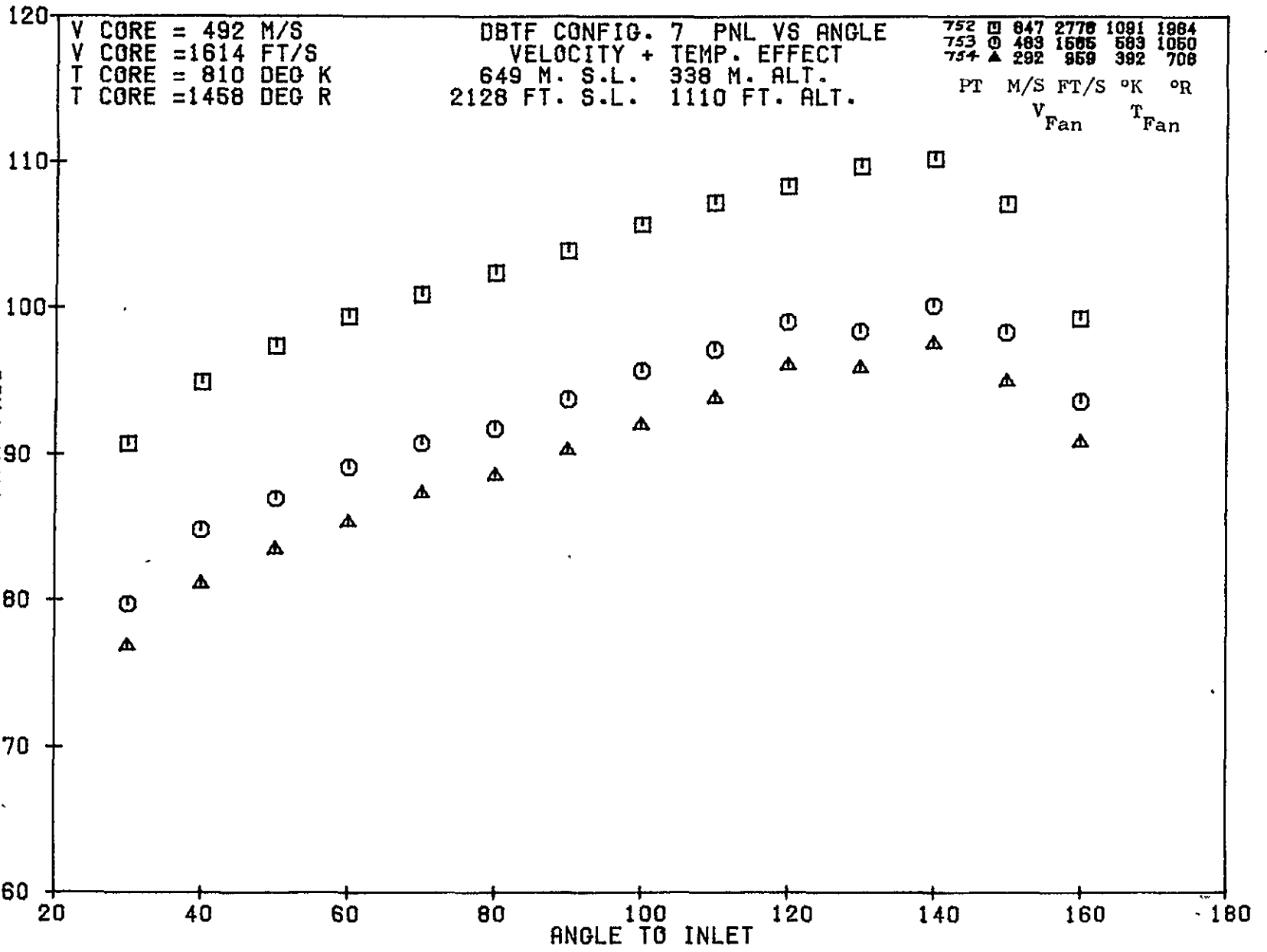


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5R412-001

79 BURCH A.

1-295



1534

U-296

08/19/75
5R412-001

79 BURCH A.

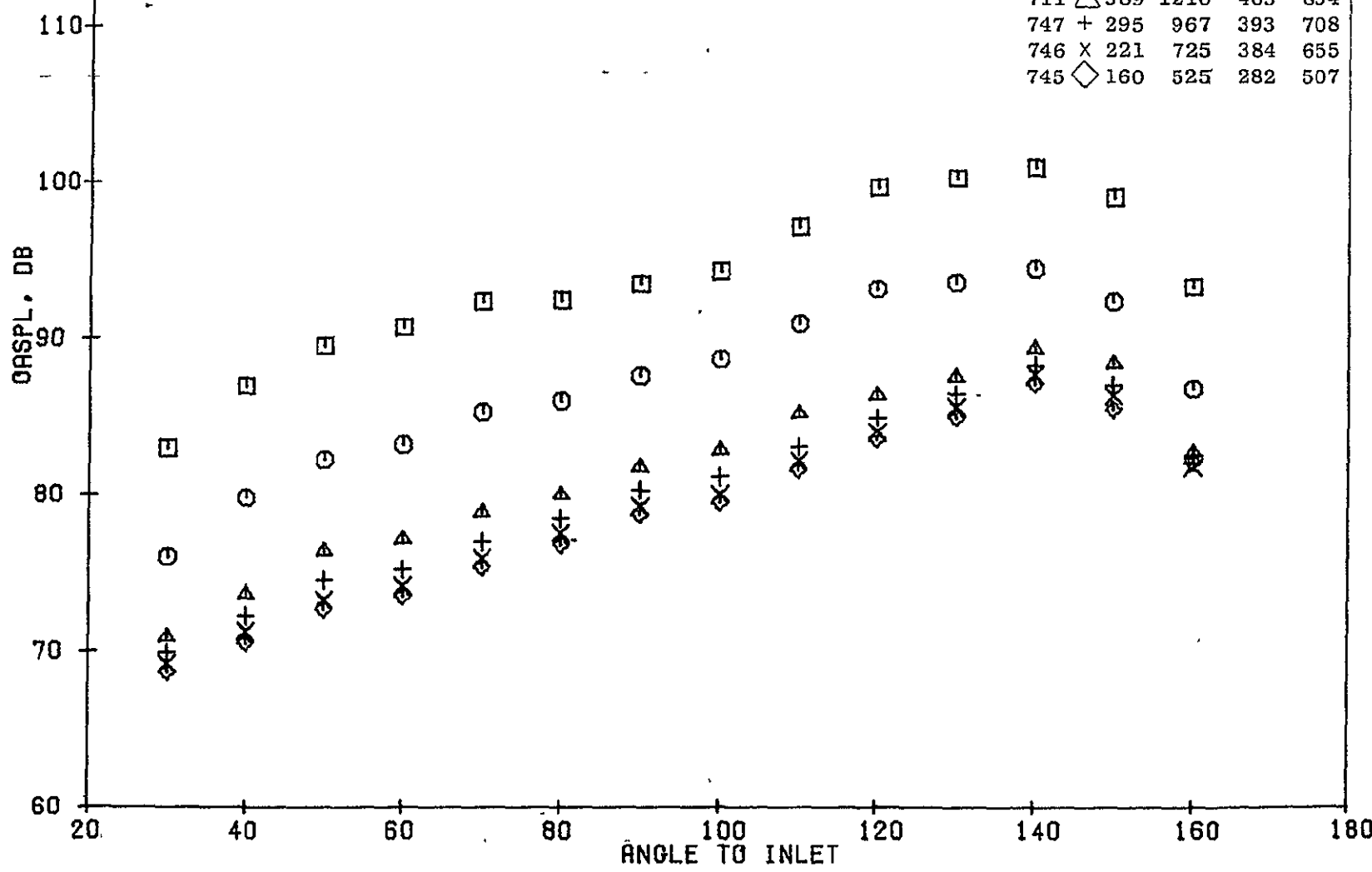
1535

OASPL, DB

V CORE = 370 M/S
 V CORE = 1215 FT/S
 T CORE = 557 DEG K
 T CORE = 1003 DEG R

DBTF CONFIG. 7 OASPL VS ANGLE
 VELOCITY + TEMP. EFFECT
 649 M. S.L. 338 M. ALT.
 2128 FT. S.L. 1110 FT. ALT.

Pt	V _{Fan}		T _{Fan}	
	m/s	ft/s	° K	° R
715	732	2402	916	1849
713	552	1811	867	1200
711	389	1210	463	834
747	295	967	393	708
746	221	725	384	655
745	160	525	282	507



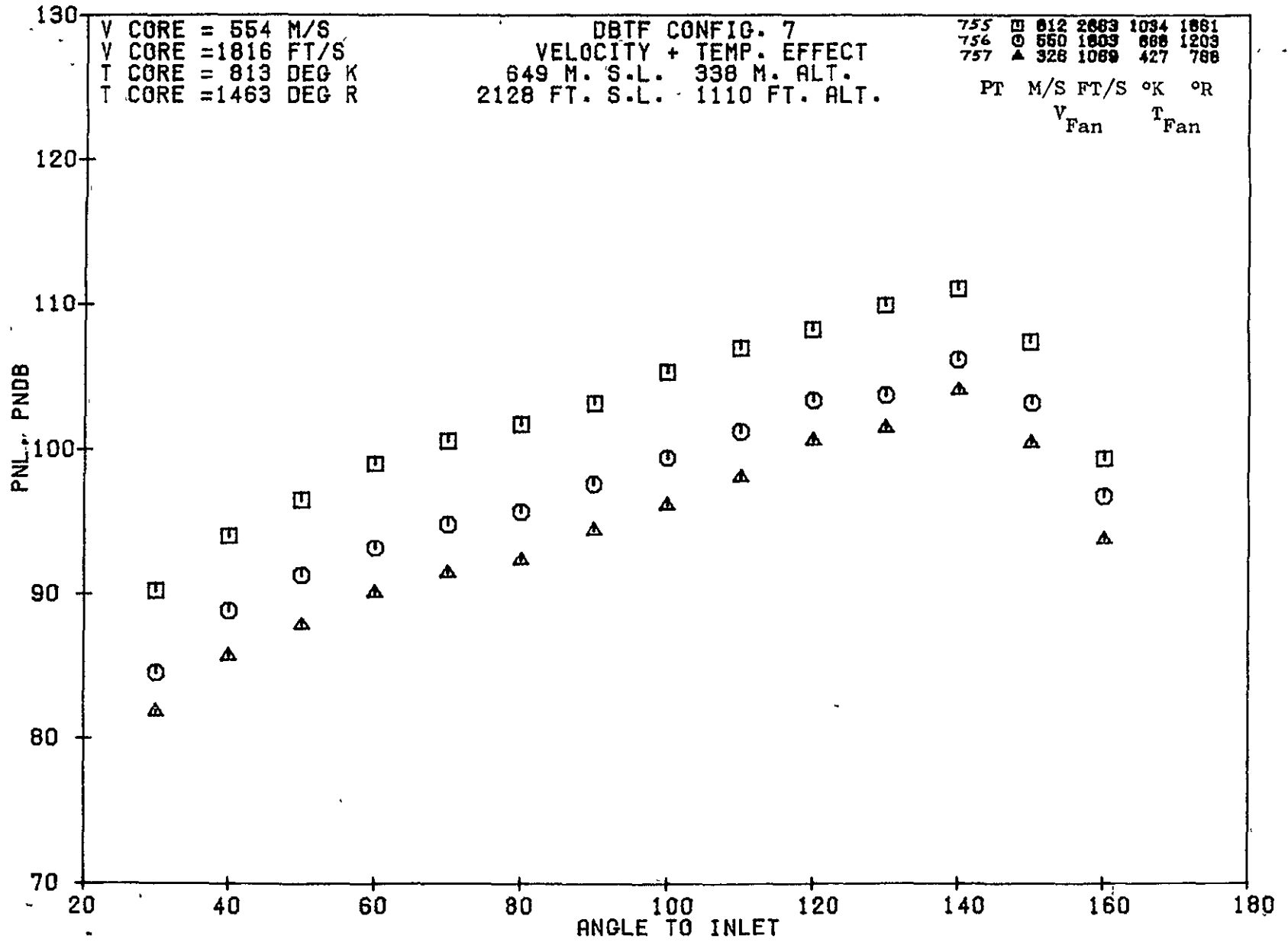
08/19/75
 5R412-001

79 BURCH A.

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W.P.

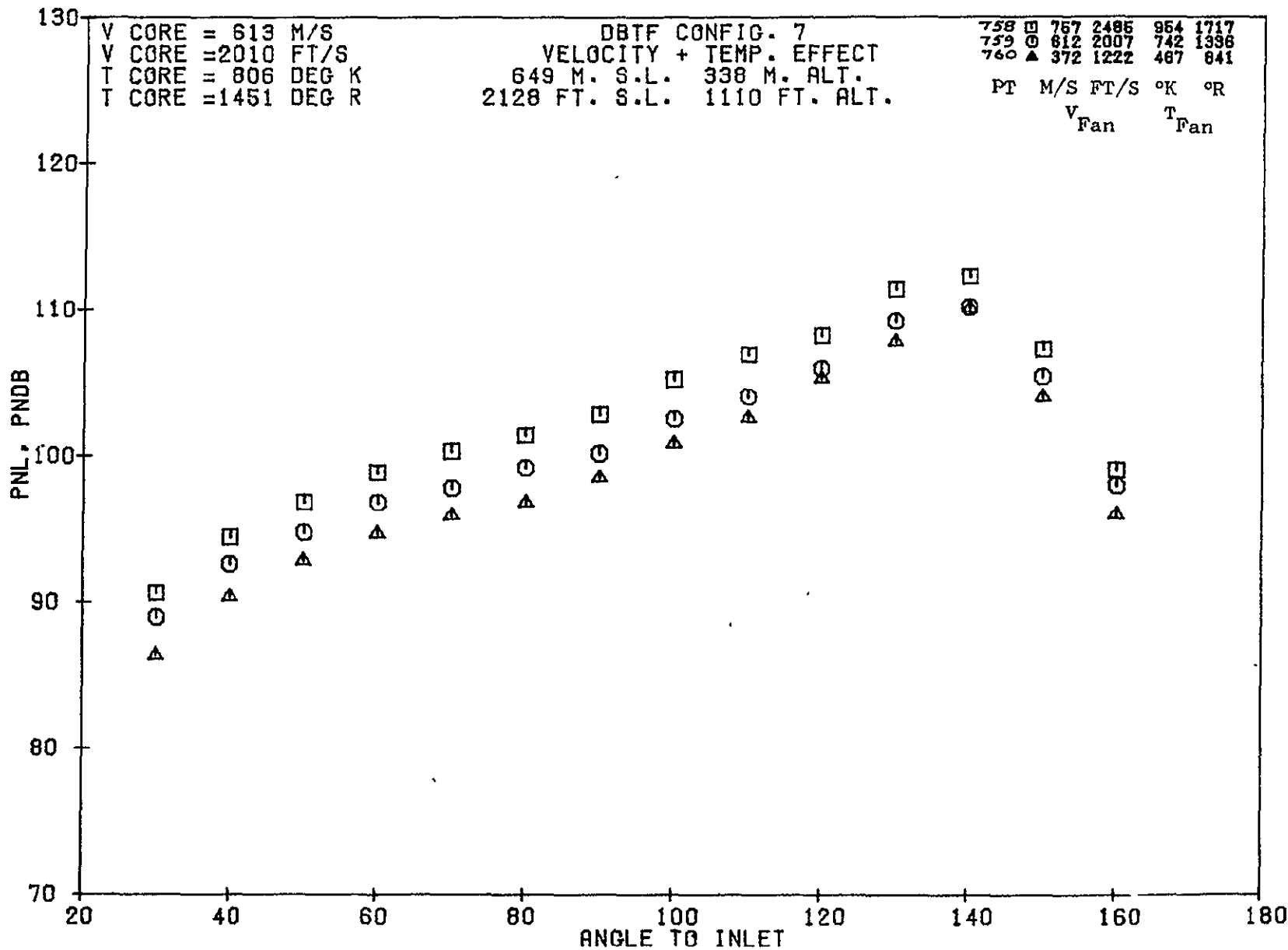
1536



08/22/75
5R682-001.

79 BURDIA.

1537



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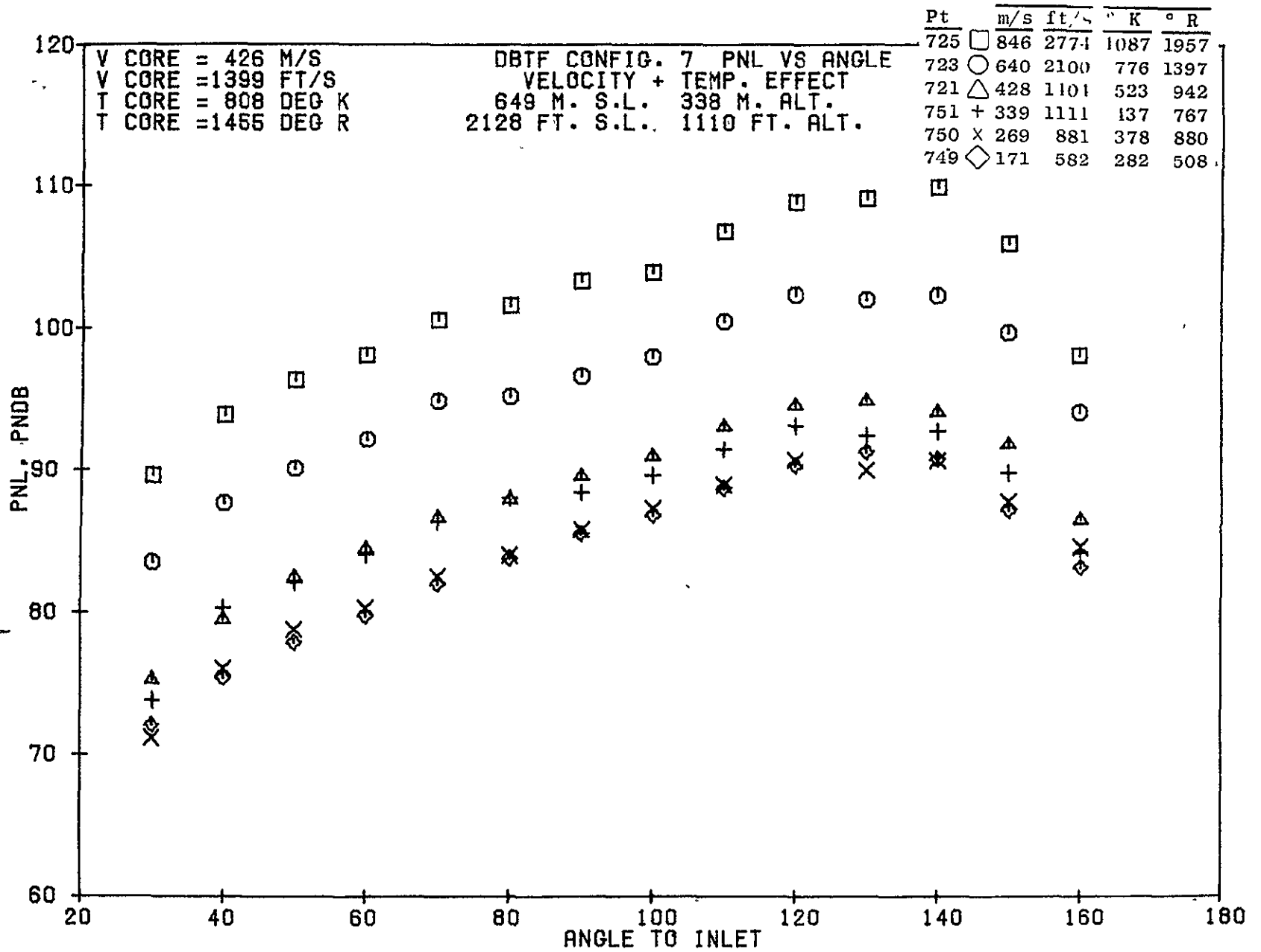
2

08/22/75
5R682-001

79 BURCH A.

11298

1538

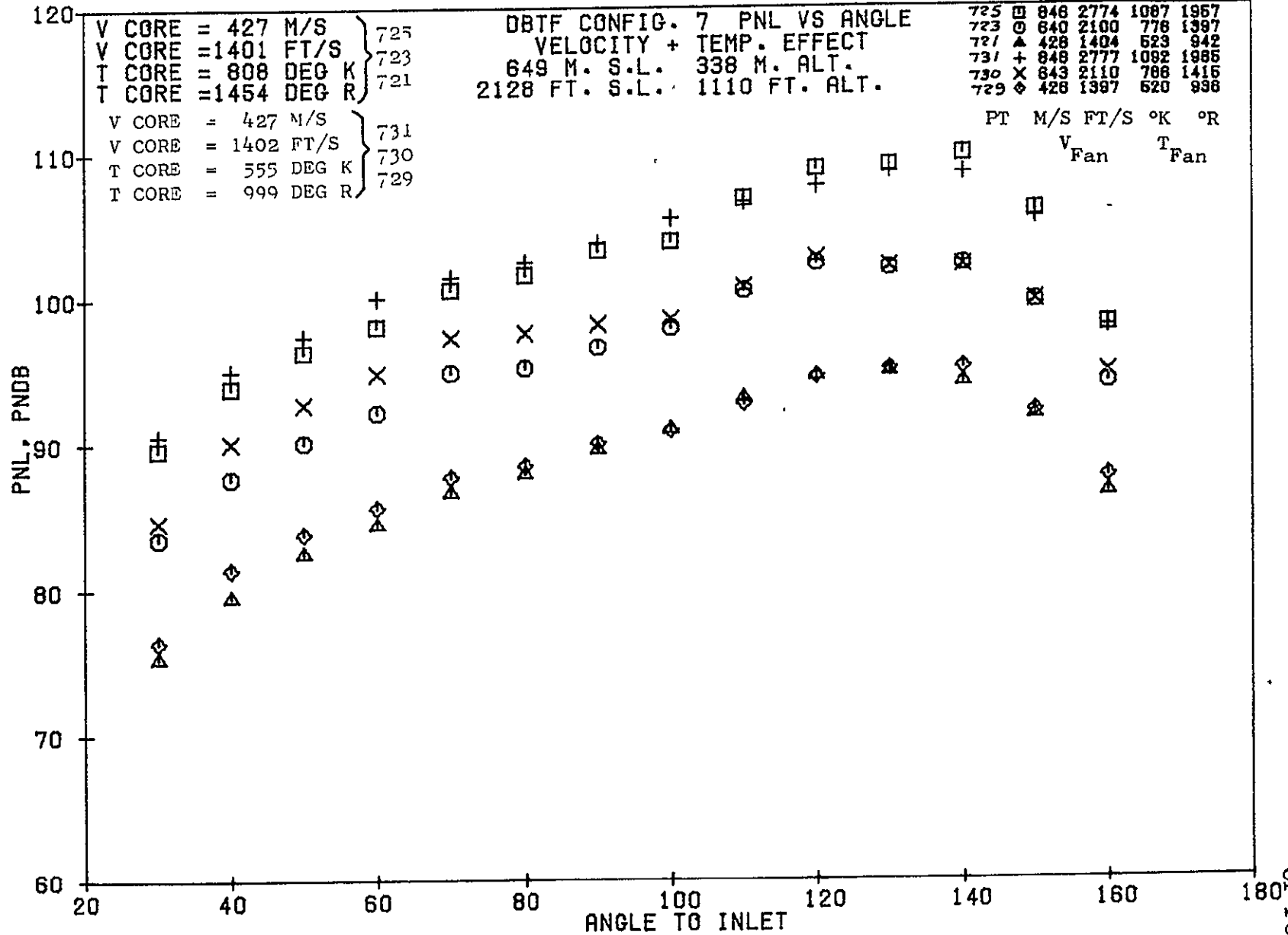


15-4

08/19/75
 5R412-001

79 BURCH A.

1539

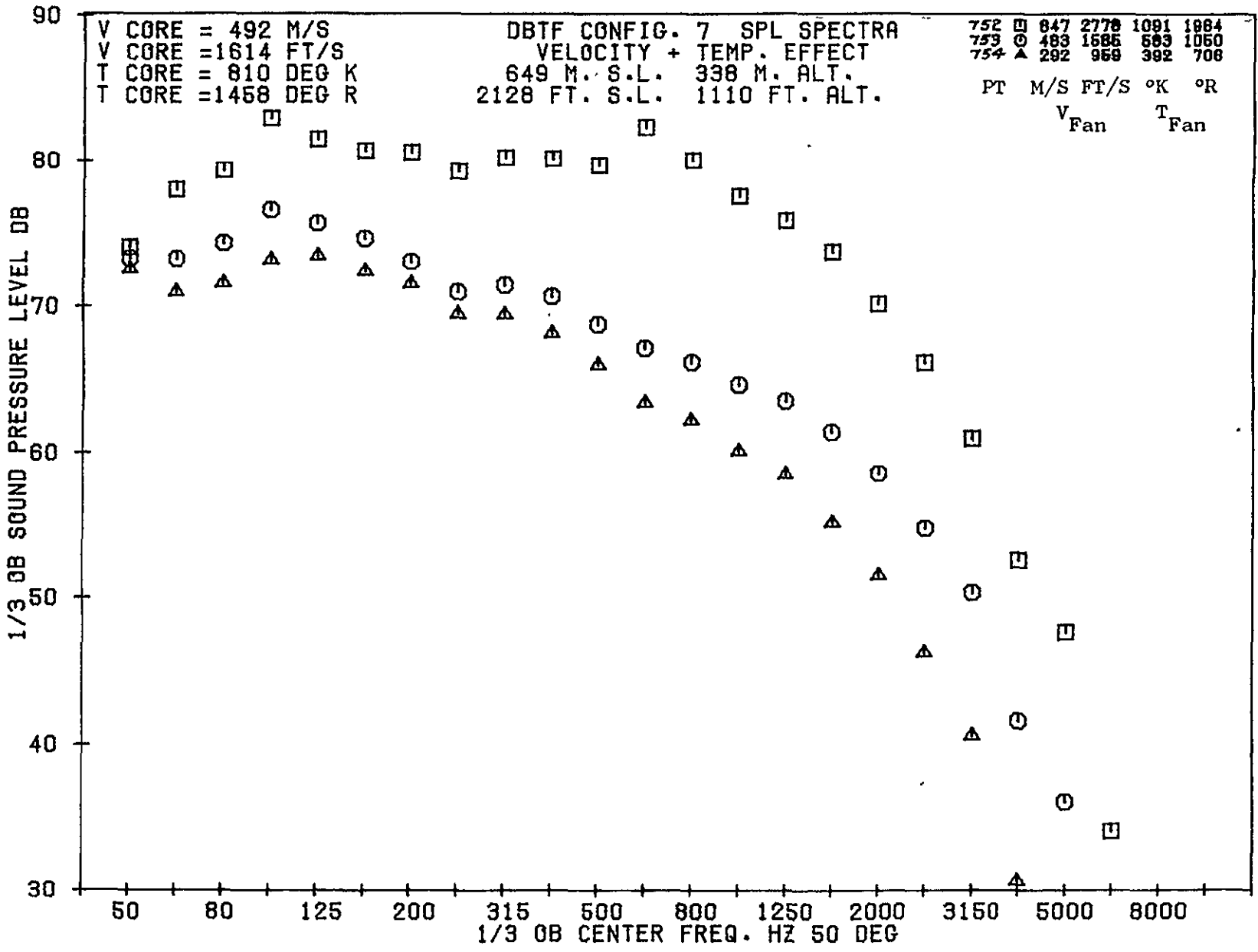


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5R412-001

79 BURCH A.

4-299

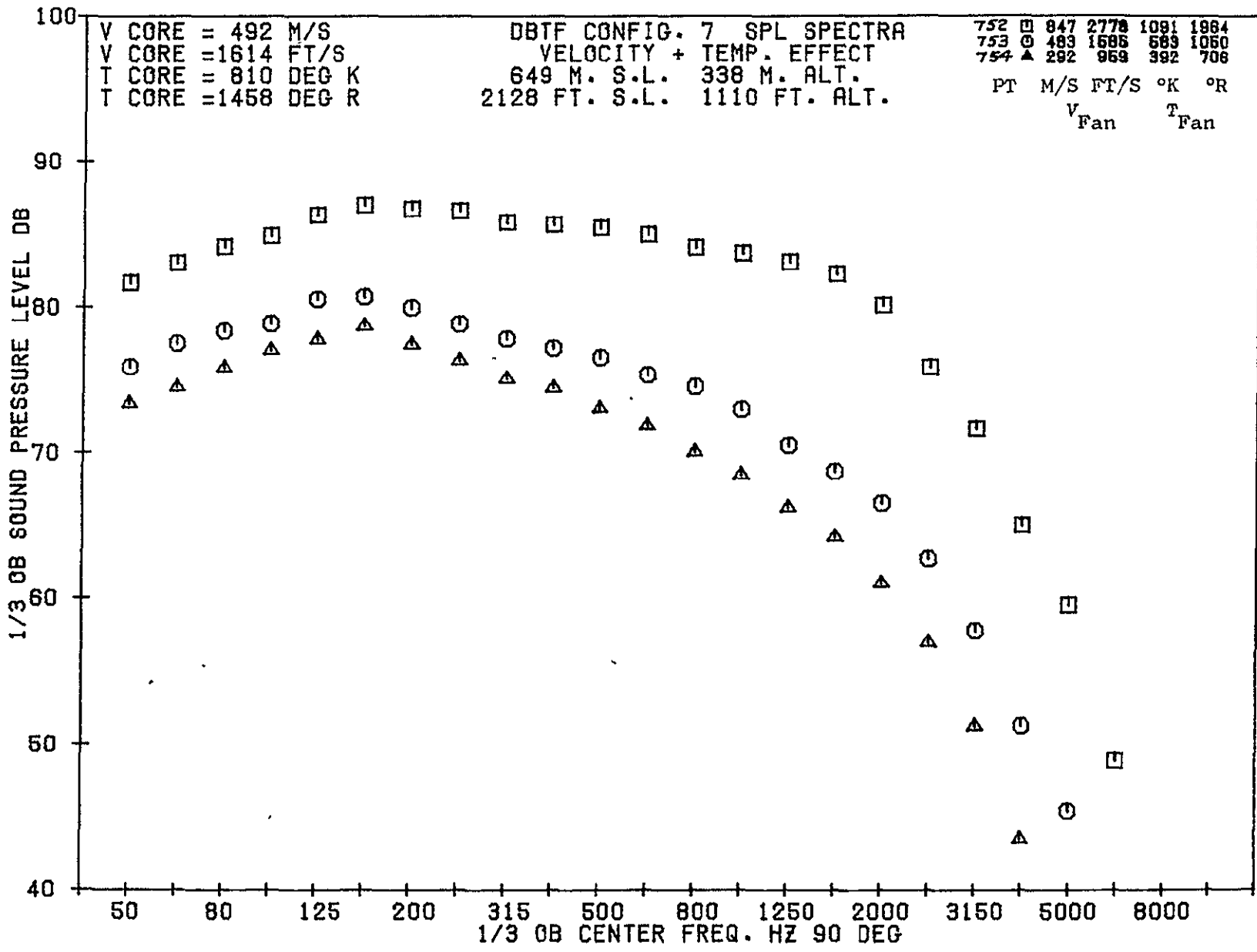


1540

U-300

08/19/75
5R412-001

79 BURCH A.

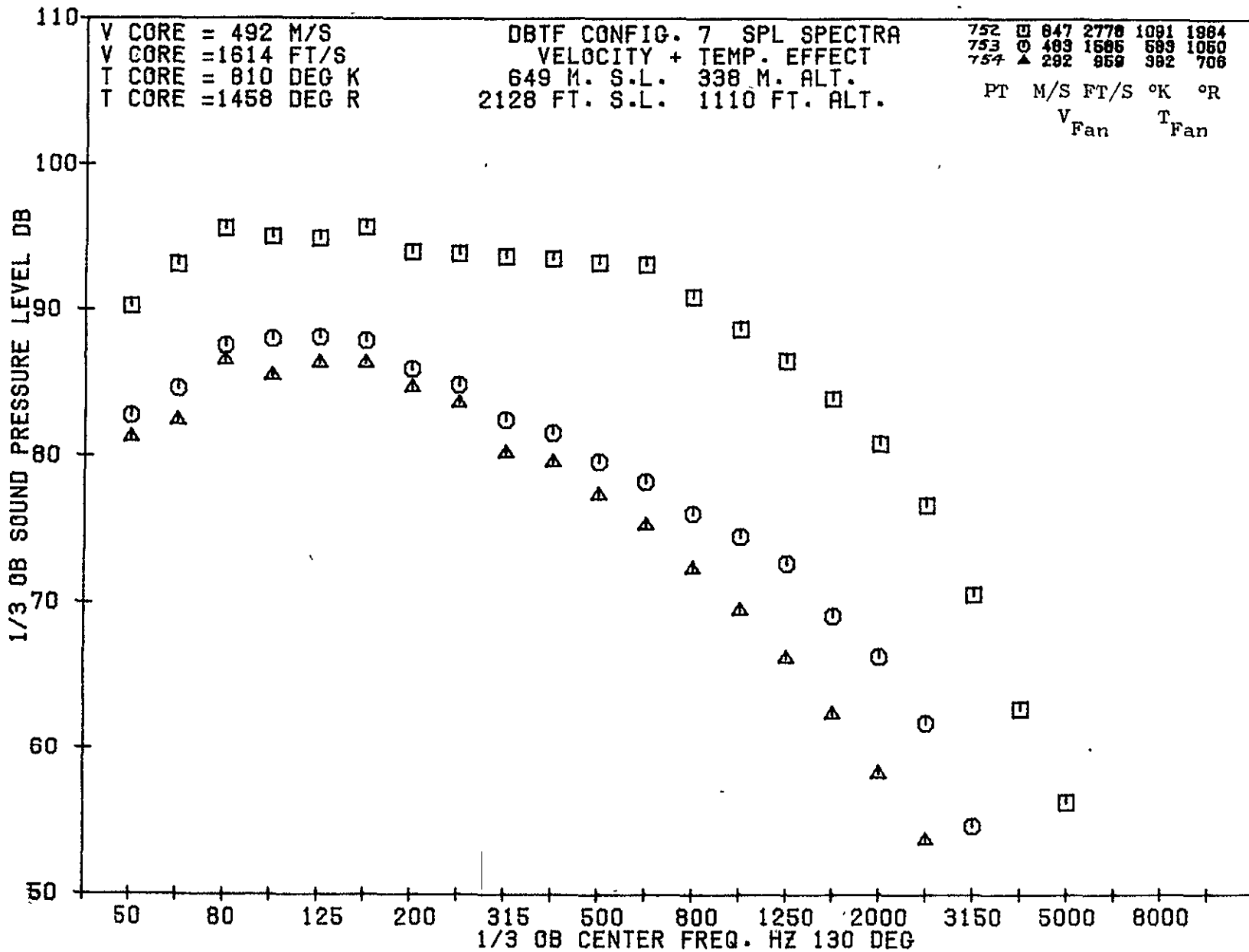


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 5R412-001

79 BURCH A.

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1301



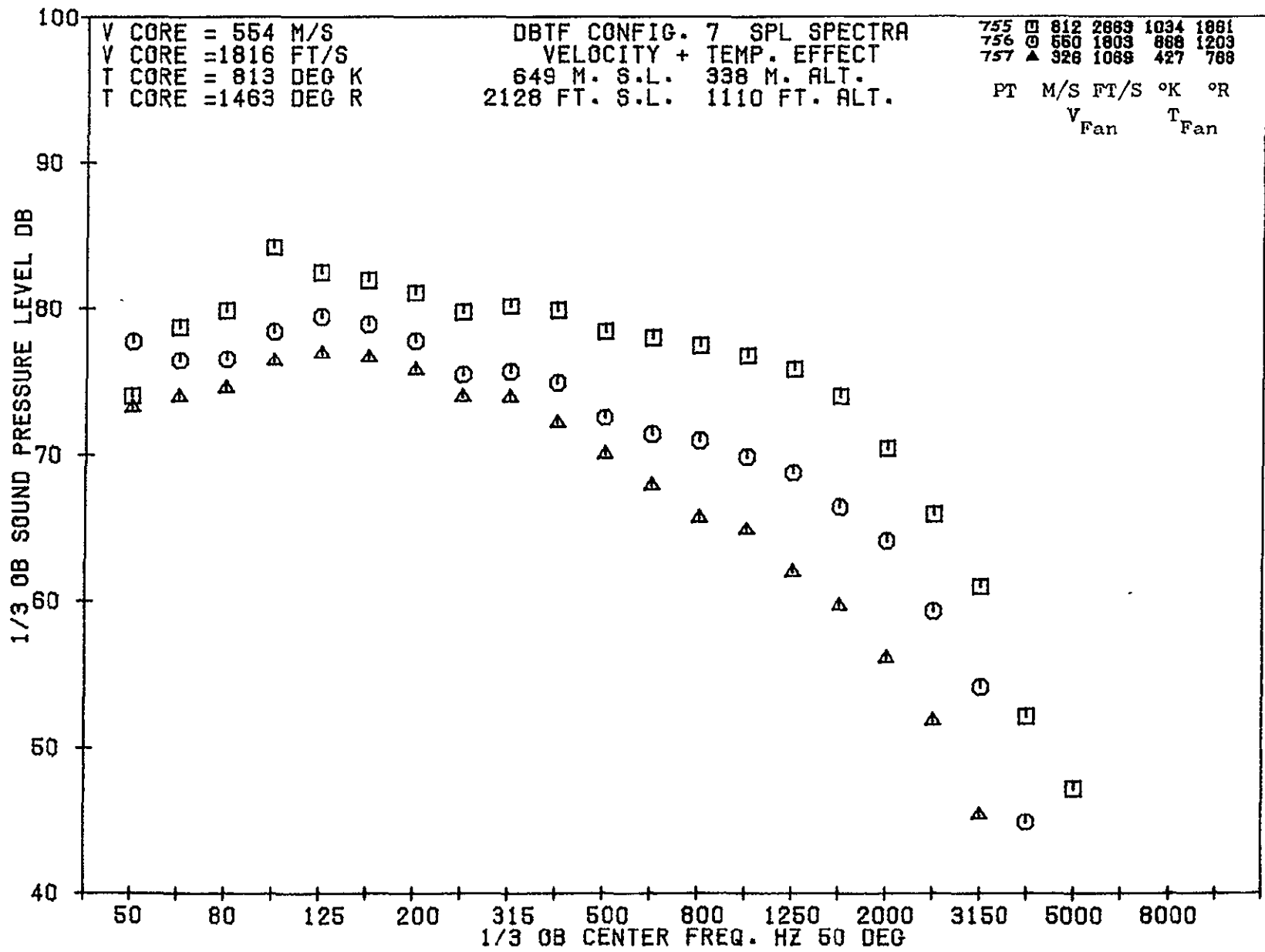
4-306

08/19/75
5R412-001

79 BURCH A.

4-303

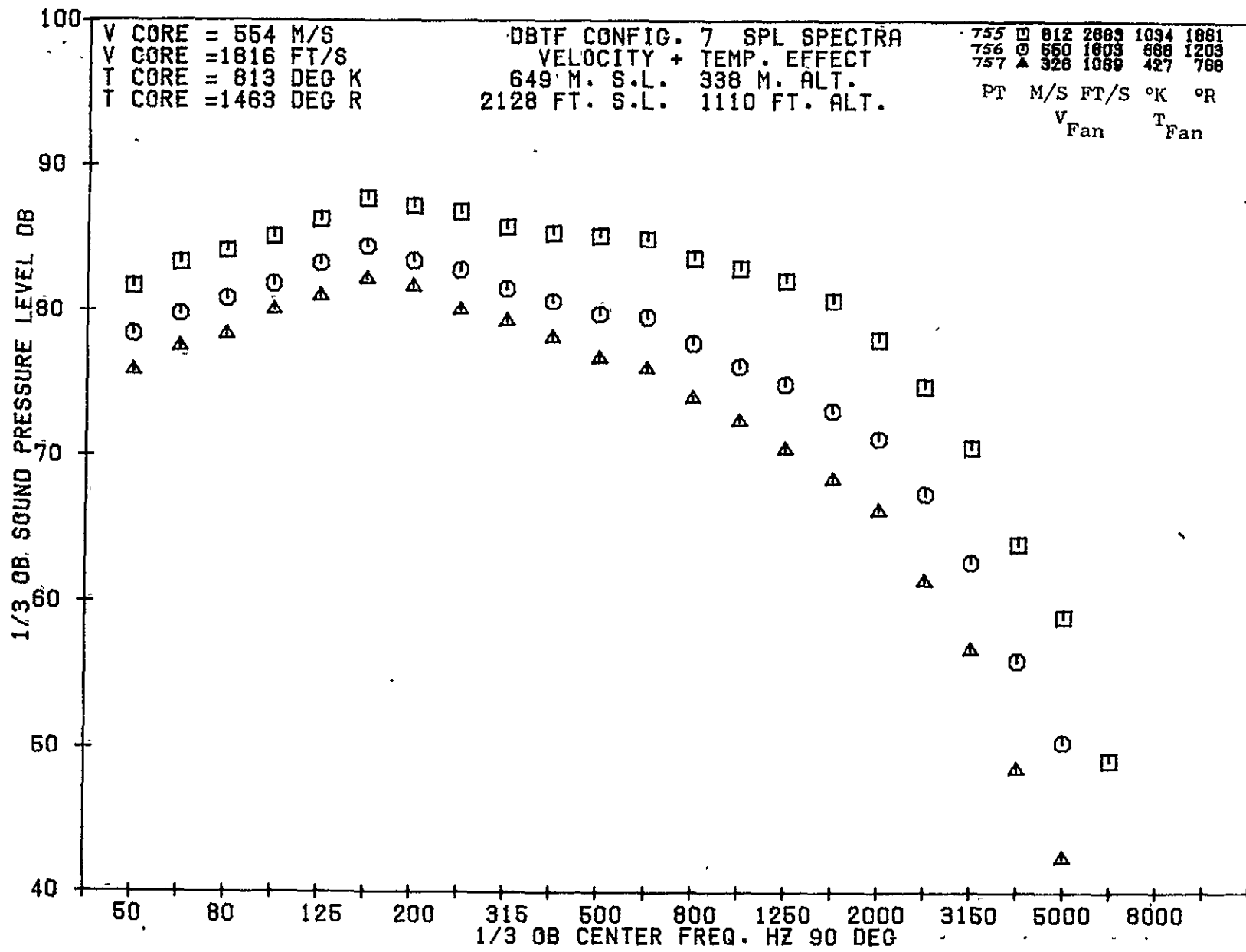
1543



08/19/75
5R412-001

79 BURCH A.

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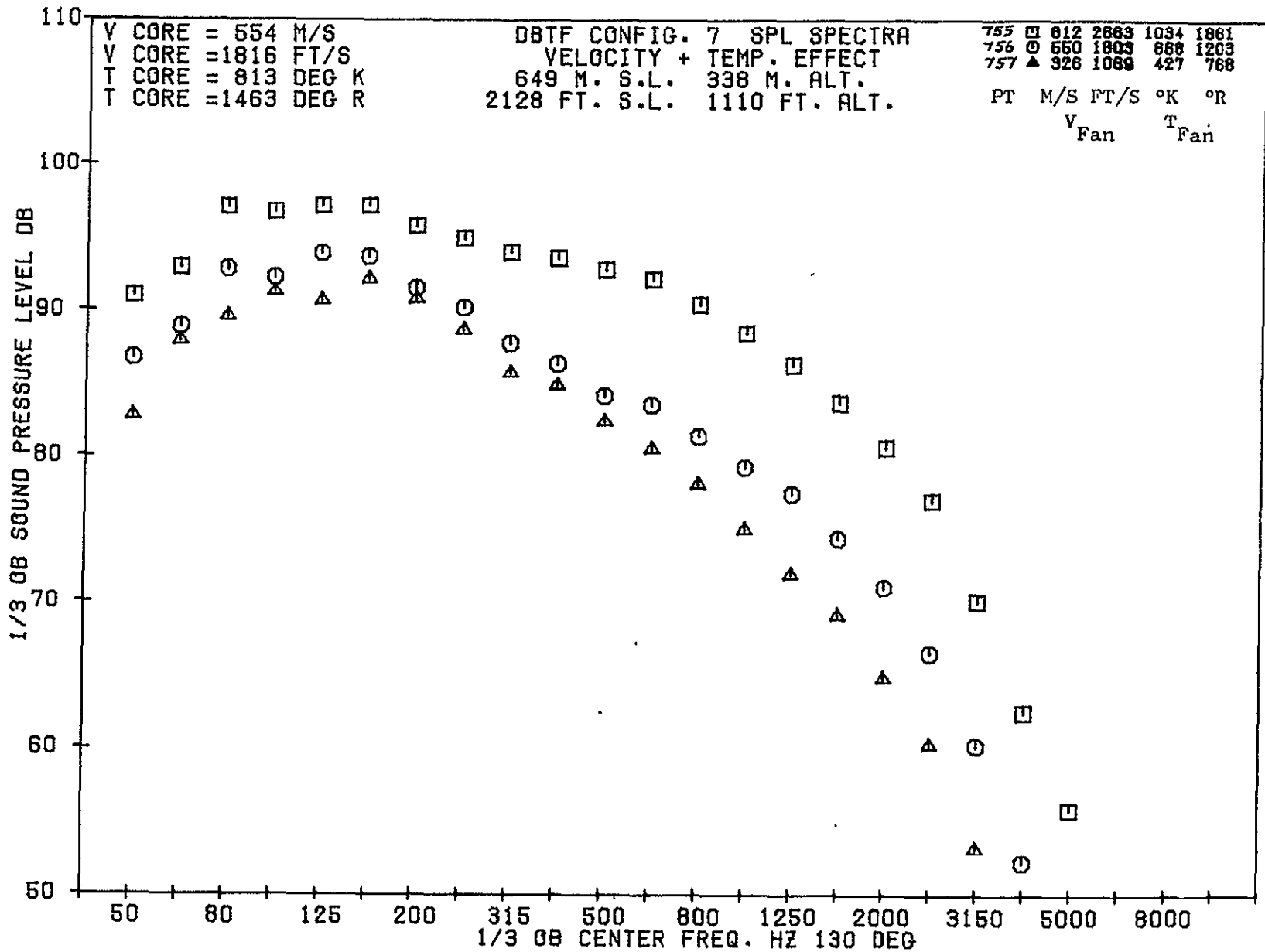


4 304

08/19/75
5R412-001

79 BURCH A.

1545

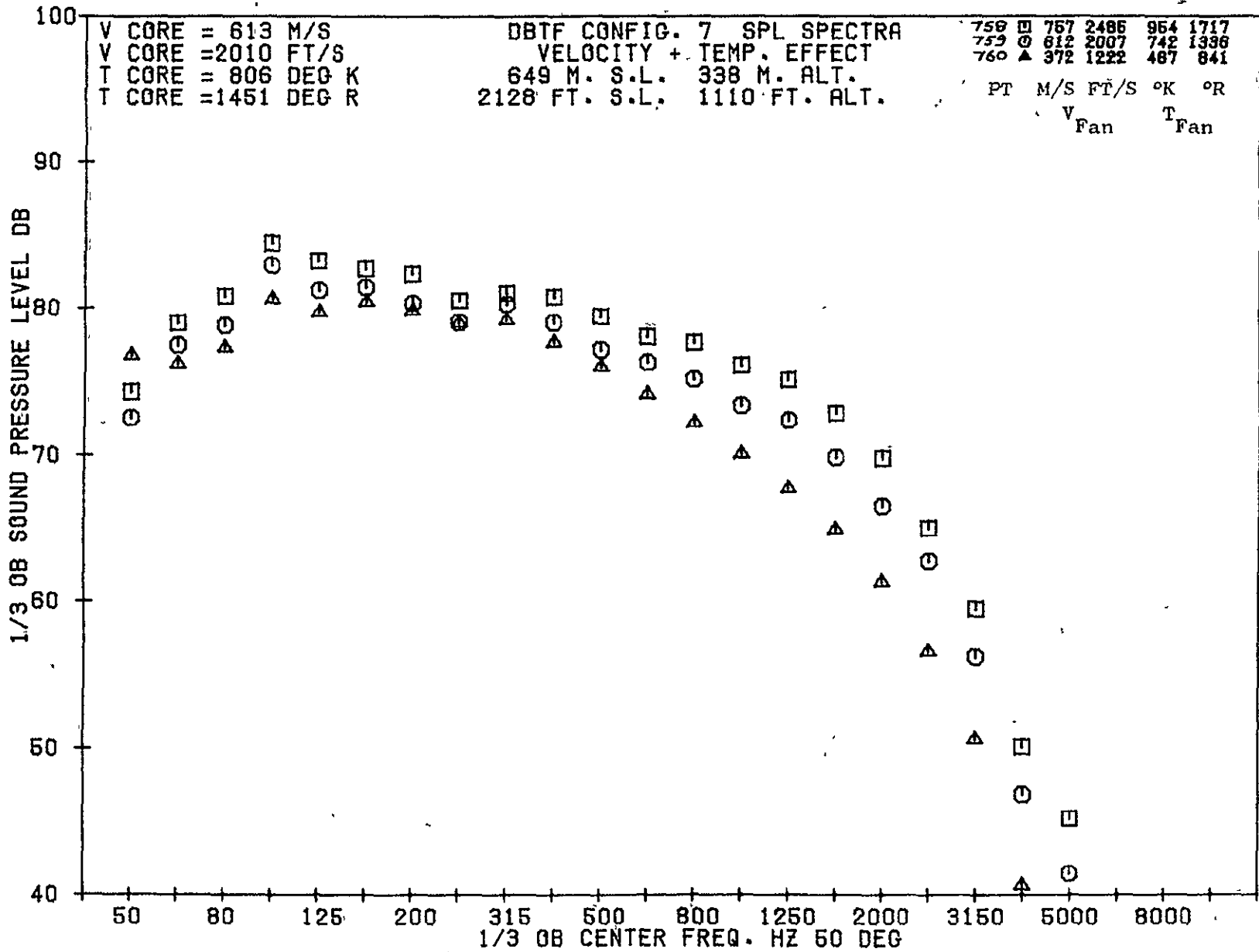


4-305

08/19/75
5R412-001

79 BURCH A.

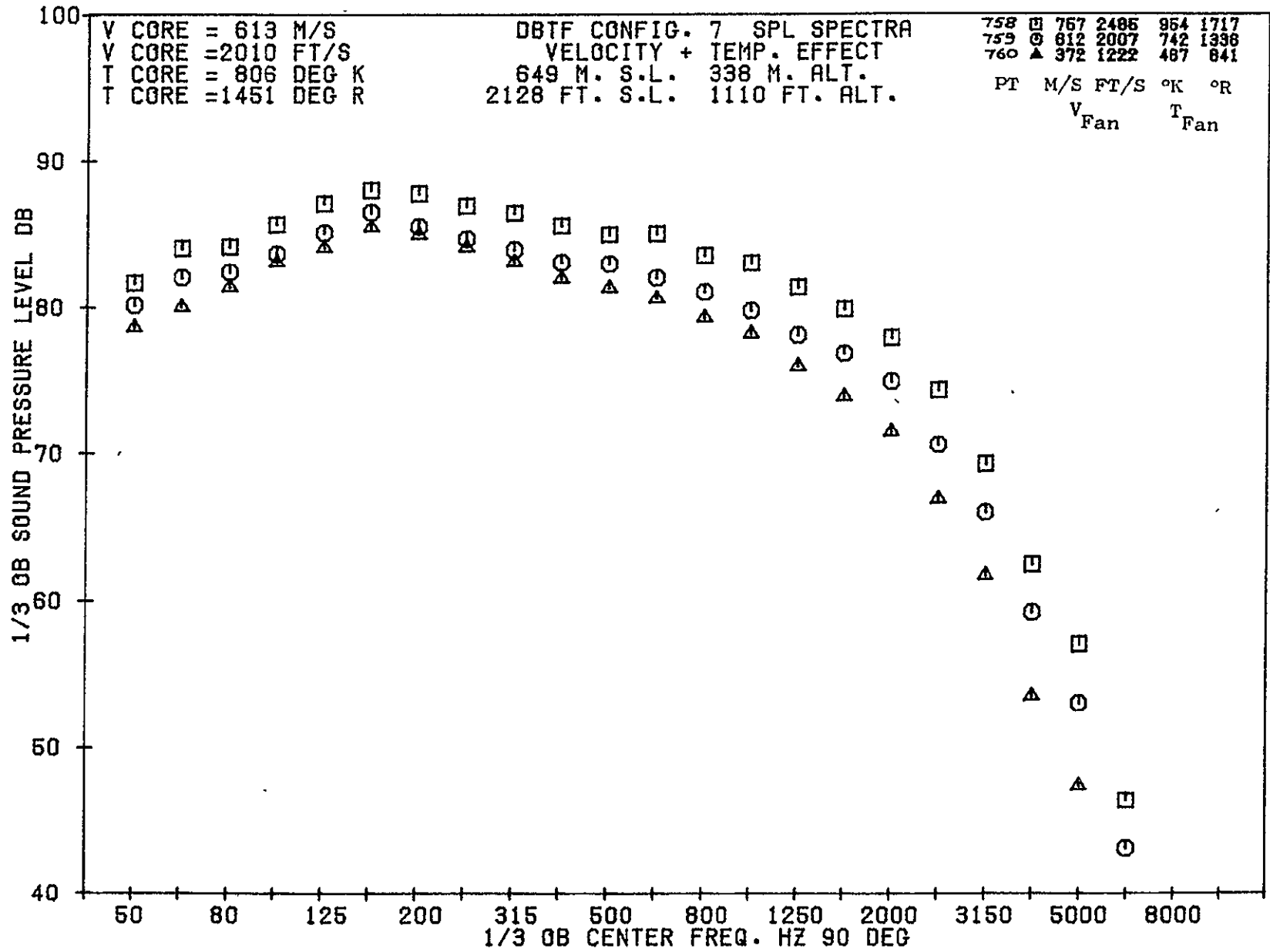
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4-306

08/19/75
5R412-001

79 BURCH A.



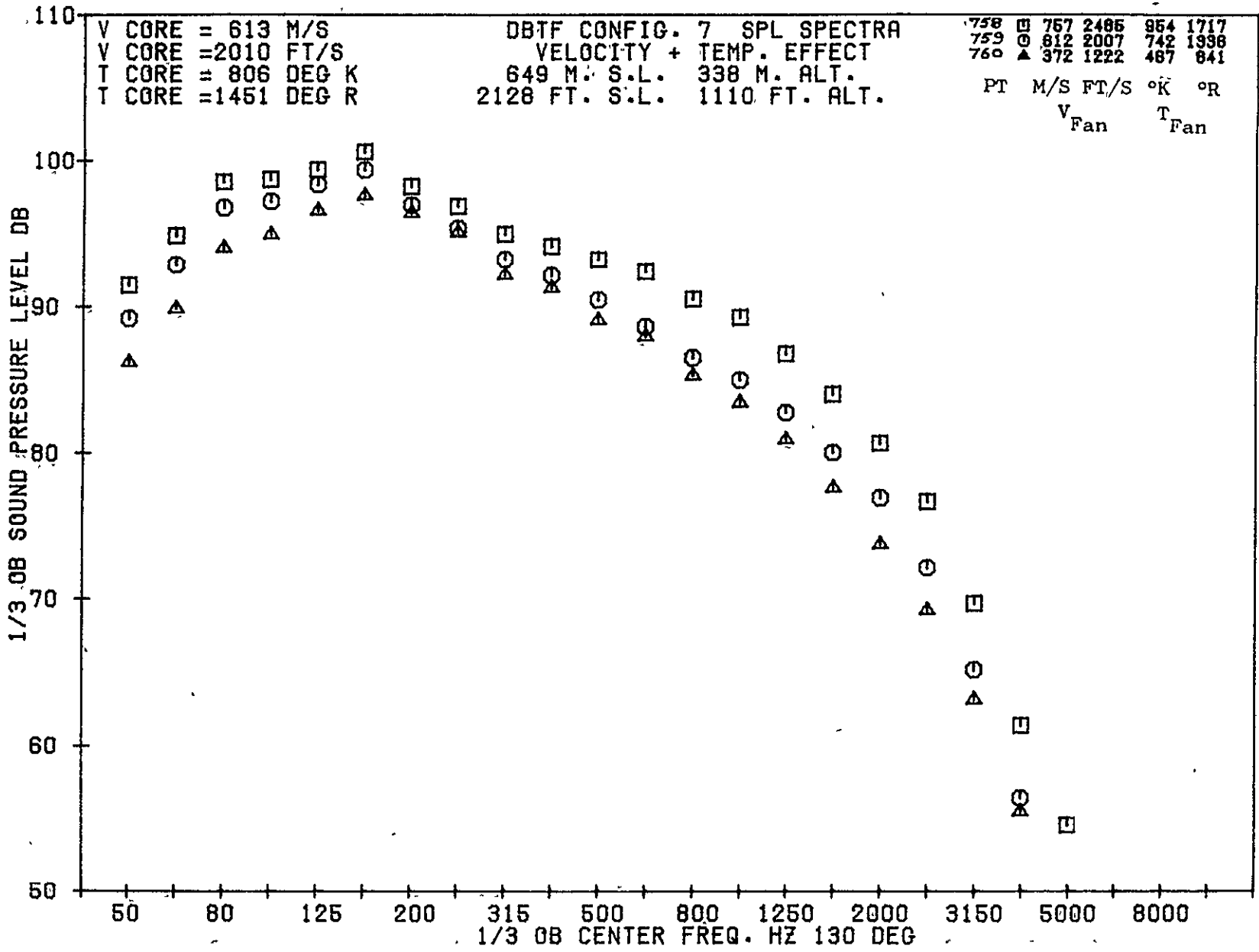
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4-307

08/19/75
5R412-001

79 BURCH A.

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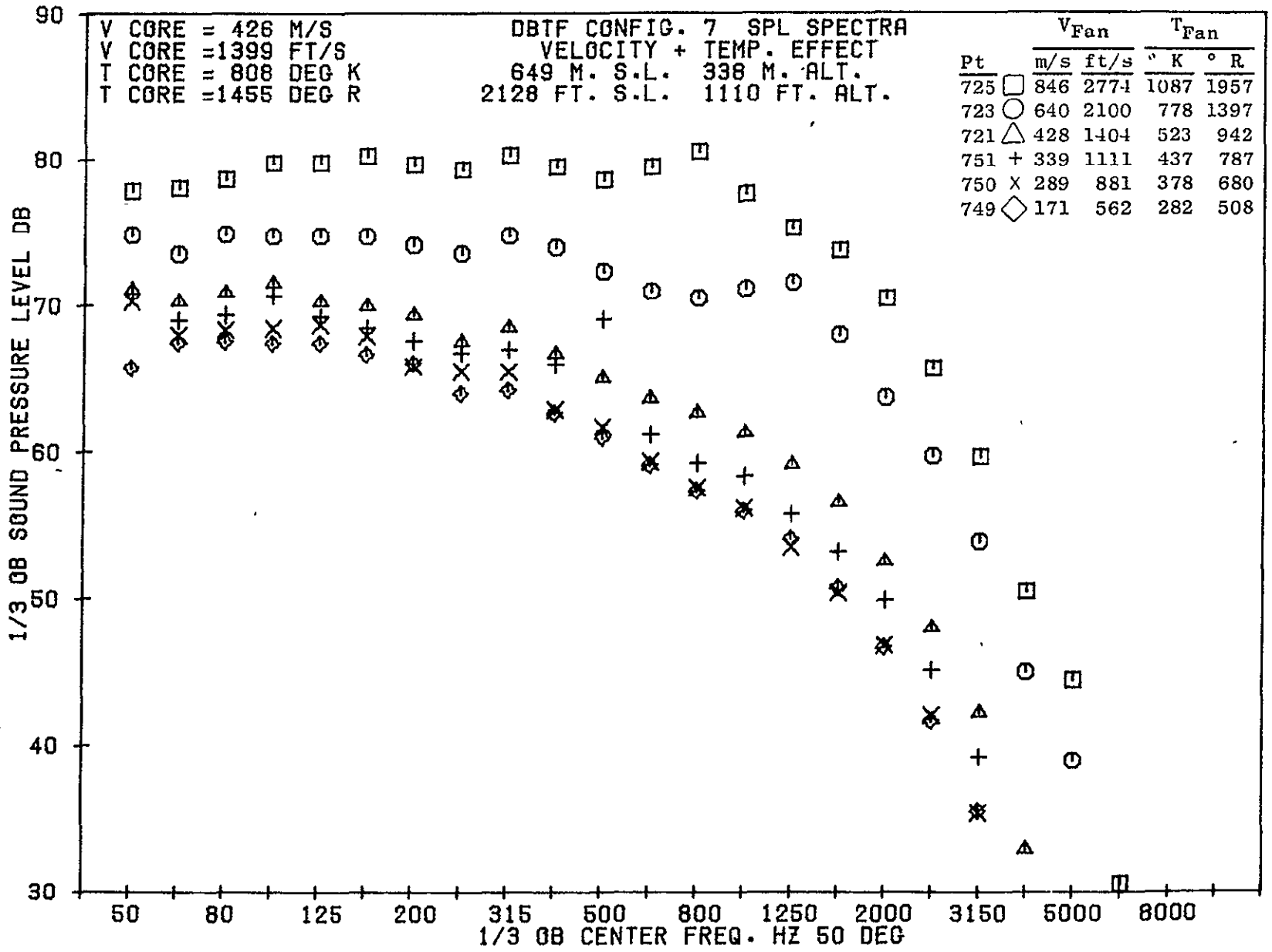


1548

4-562

08/19/75
 5R412-001

79 BURCH A.



1549

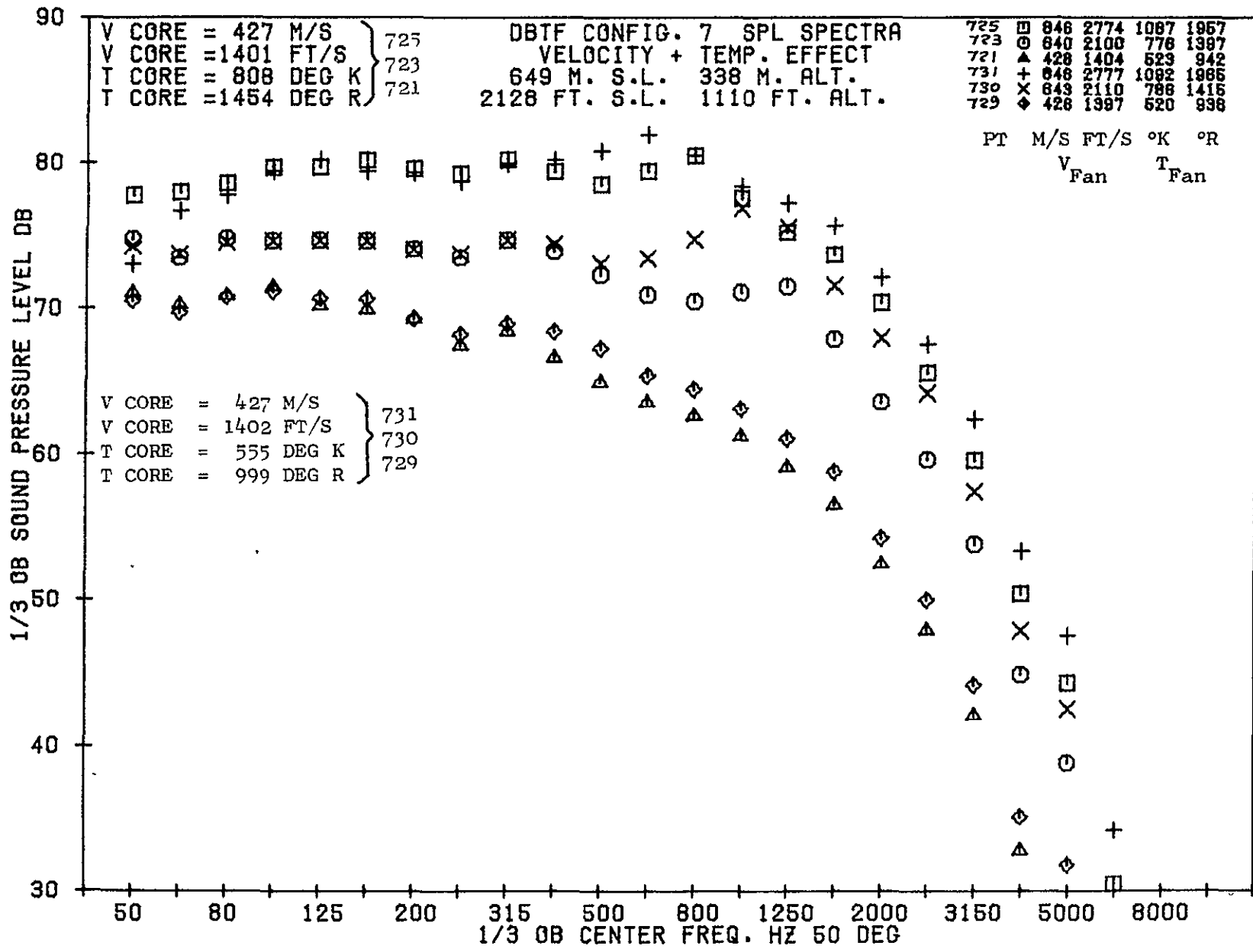
173

08/19/75
5R412-001

79 BURCH A.

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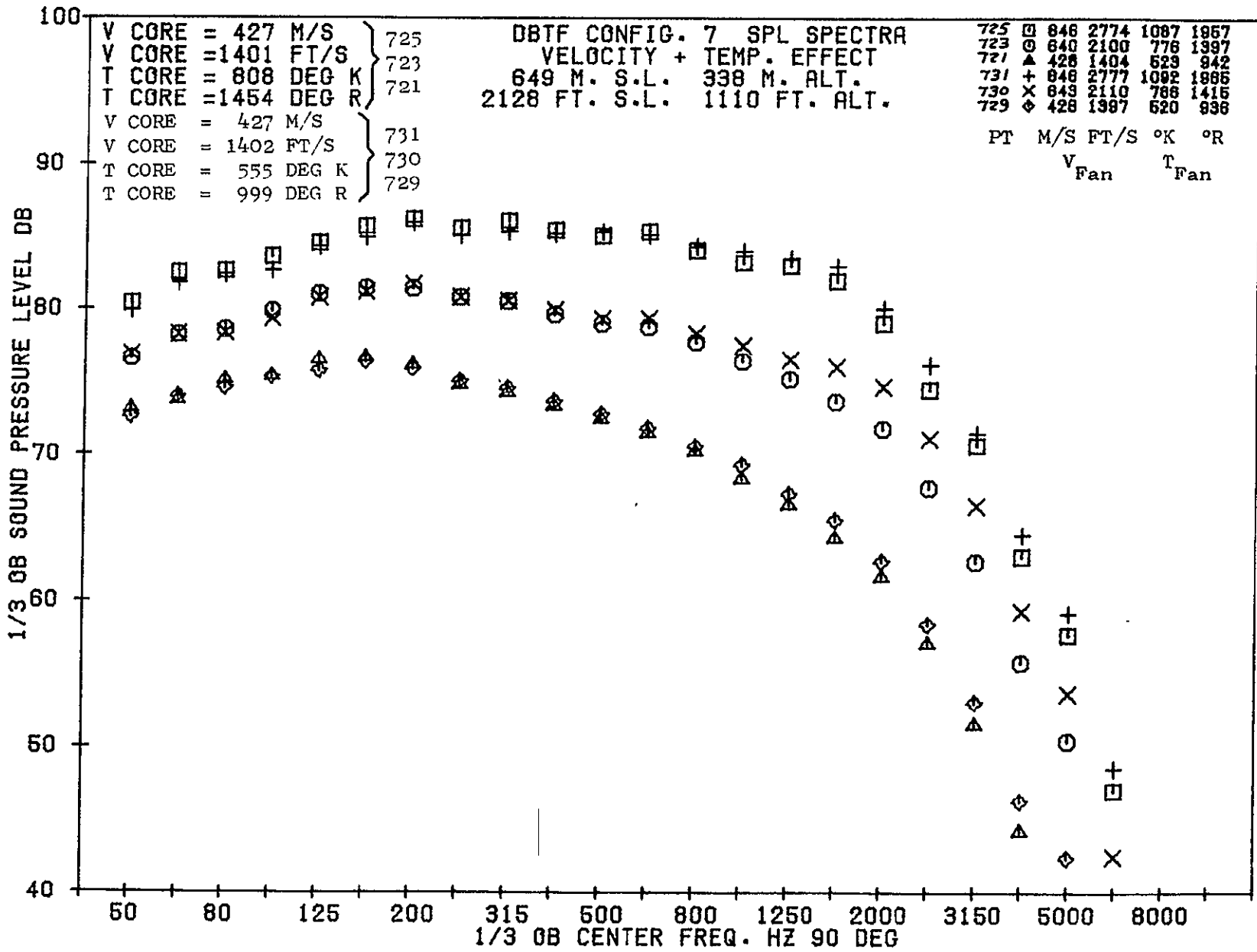
1550



4-309

08/19/75
 5R412-001

79 BURCH A.



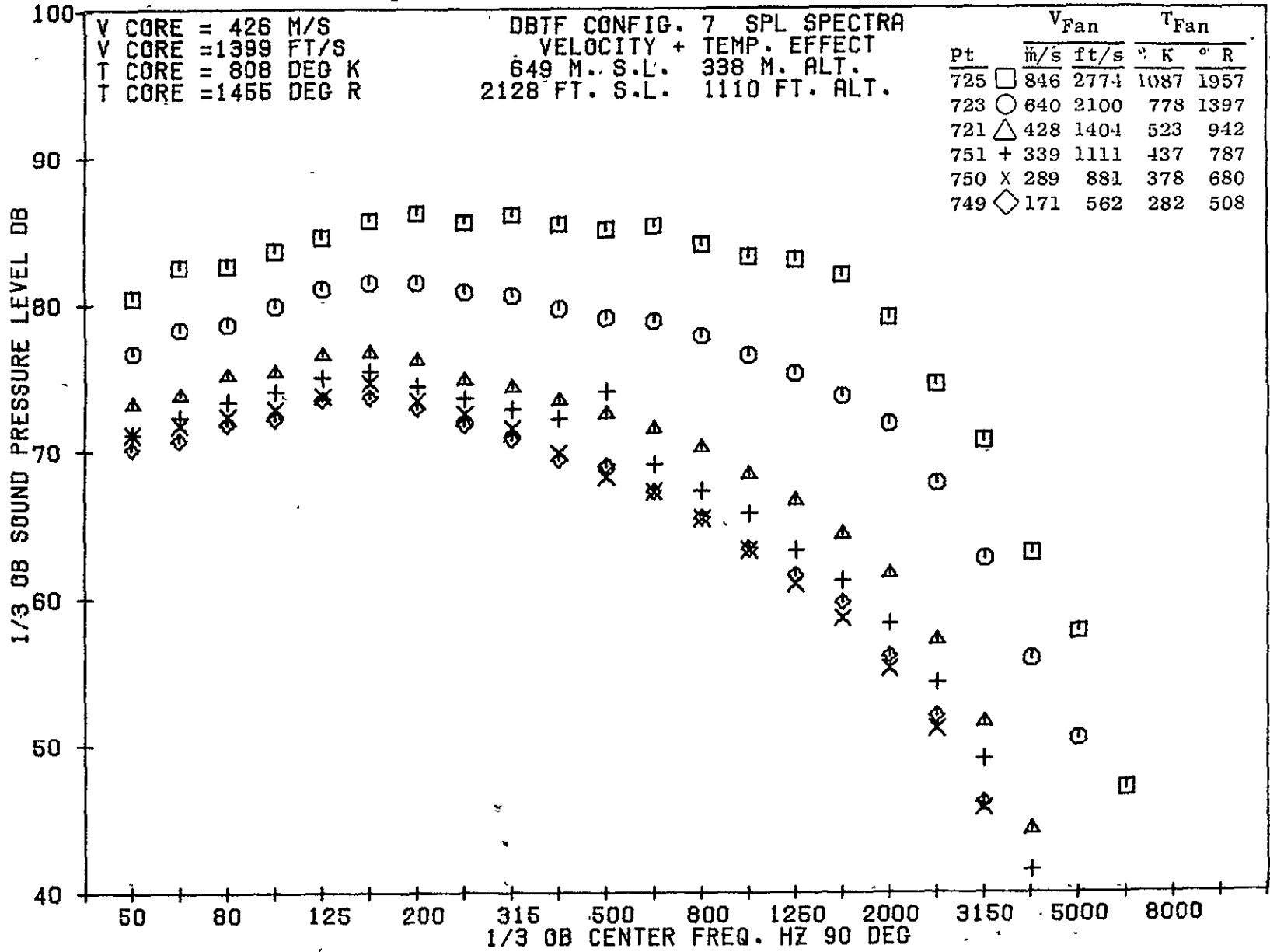
08/19/75
 5R412-001

79 BURCH A.

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4-2/10

1552

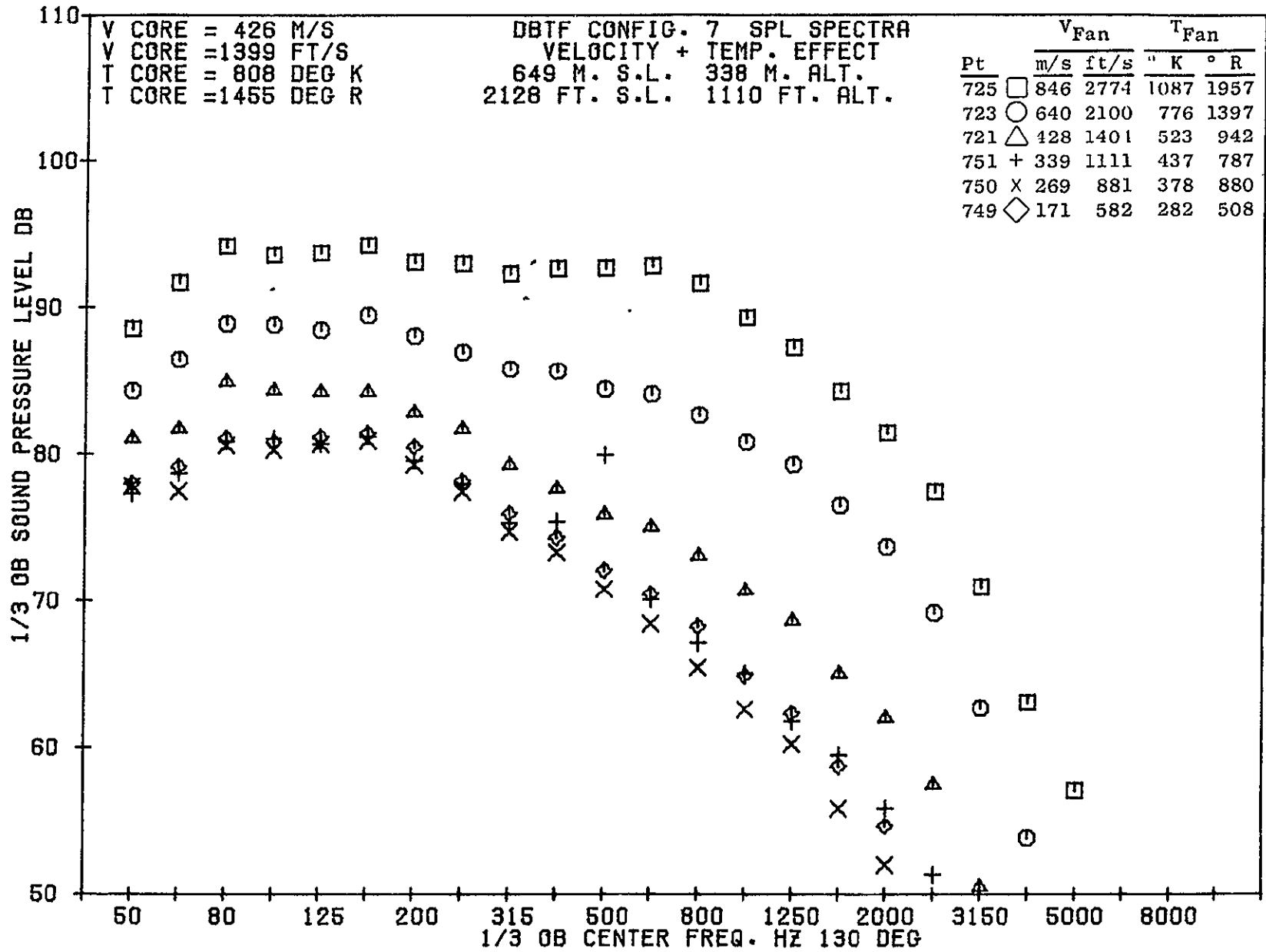


1552

08/19/75
5R412-001

79 BURCH A.

1553

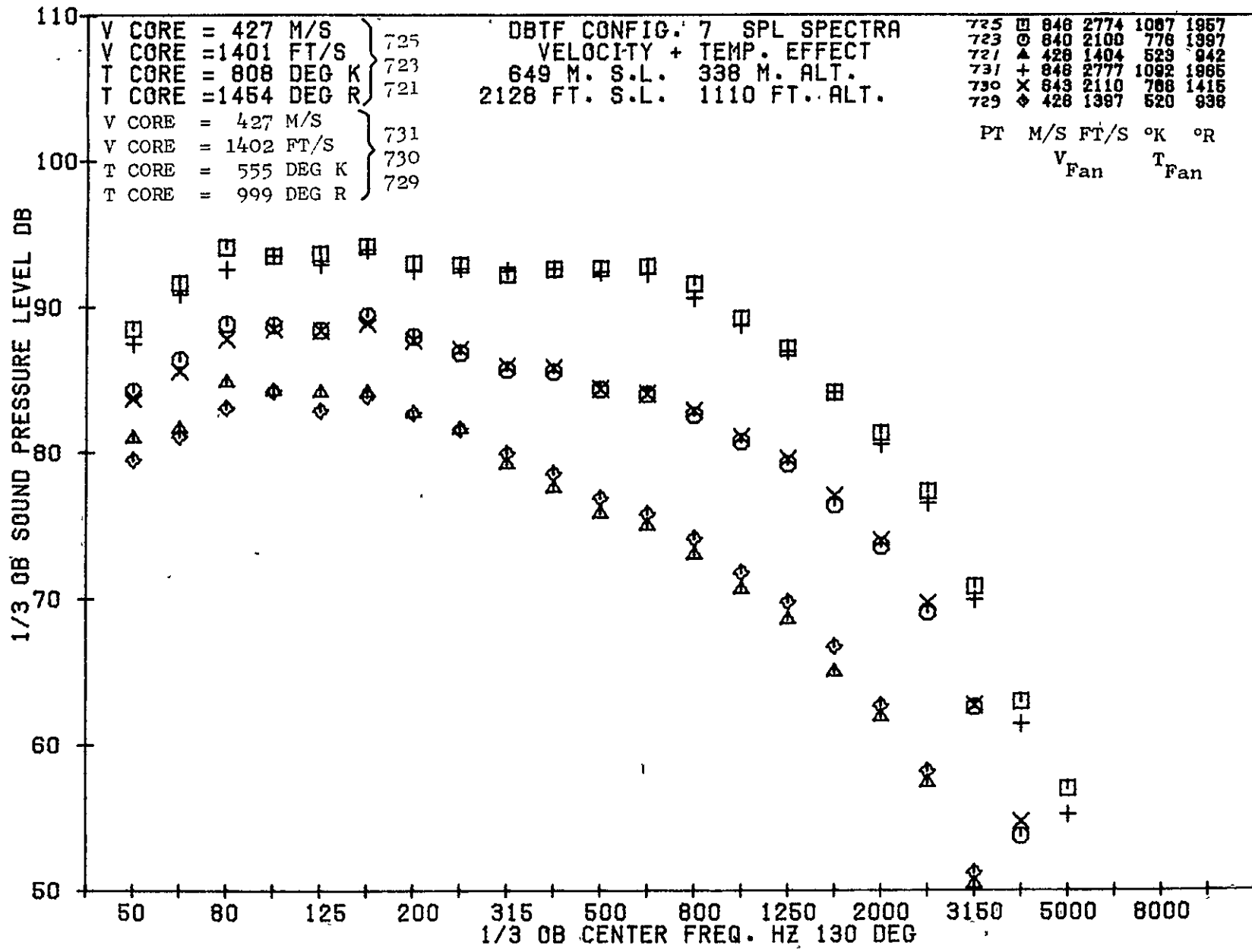


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08/19/75
5R412-001

79 BURCH A.

4-75

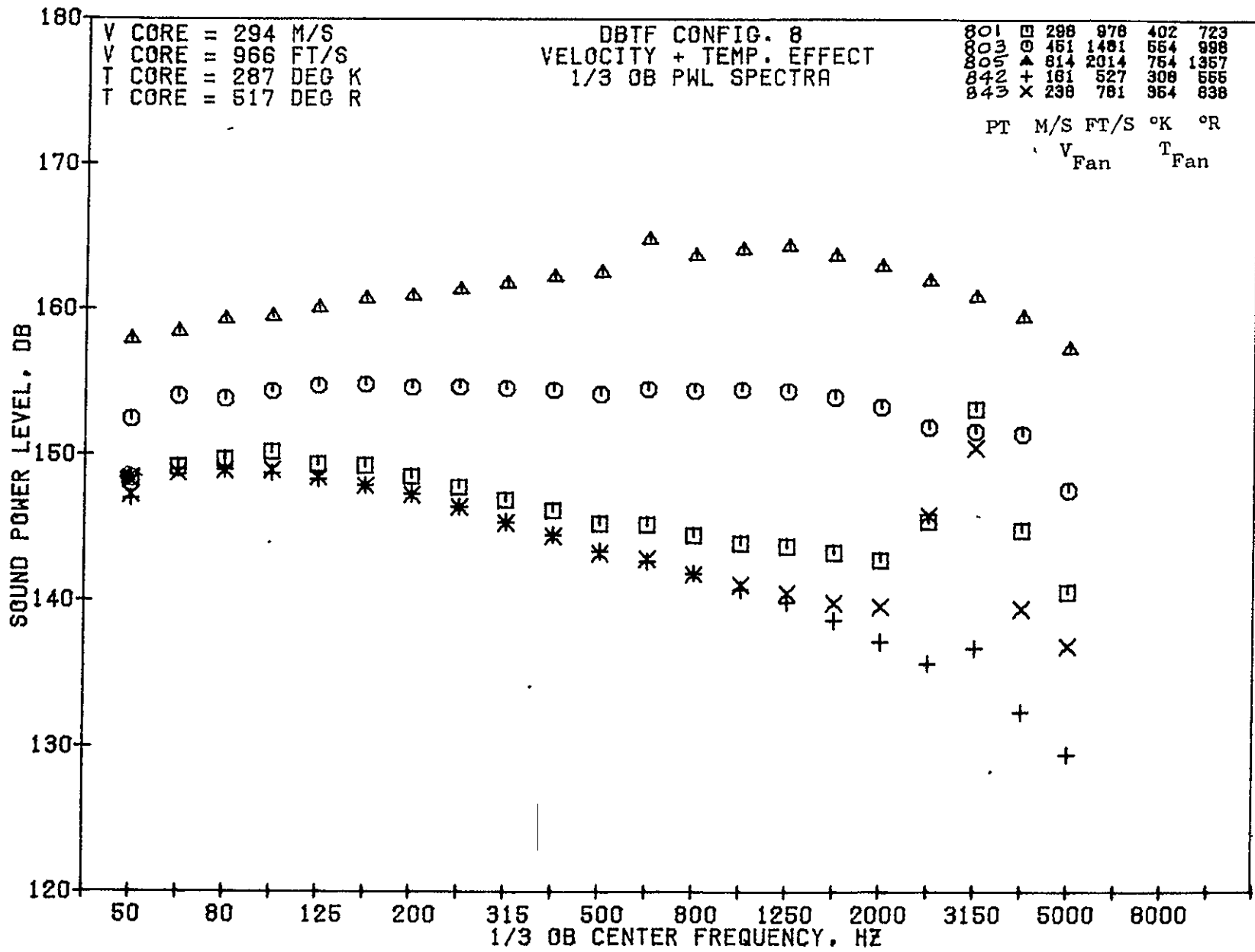


4-311

08/19/75
5R412-001

79 BURCH A.

1555



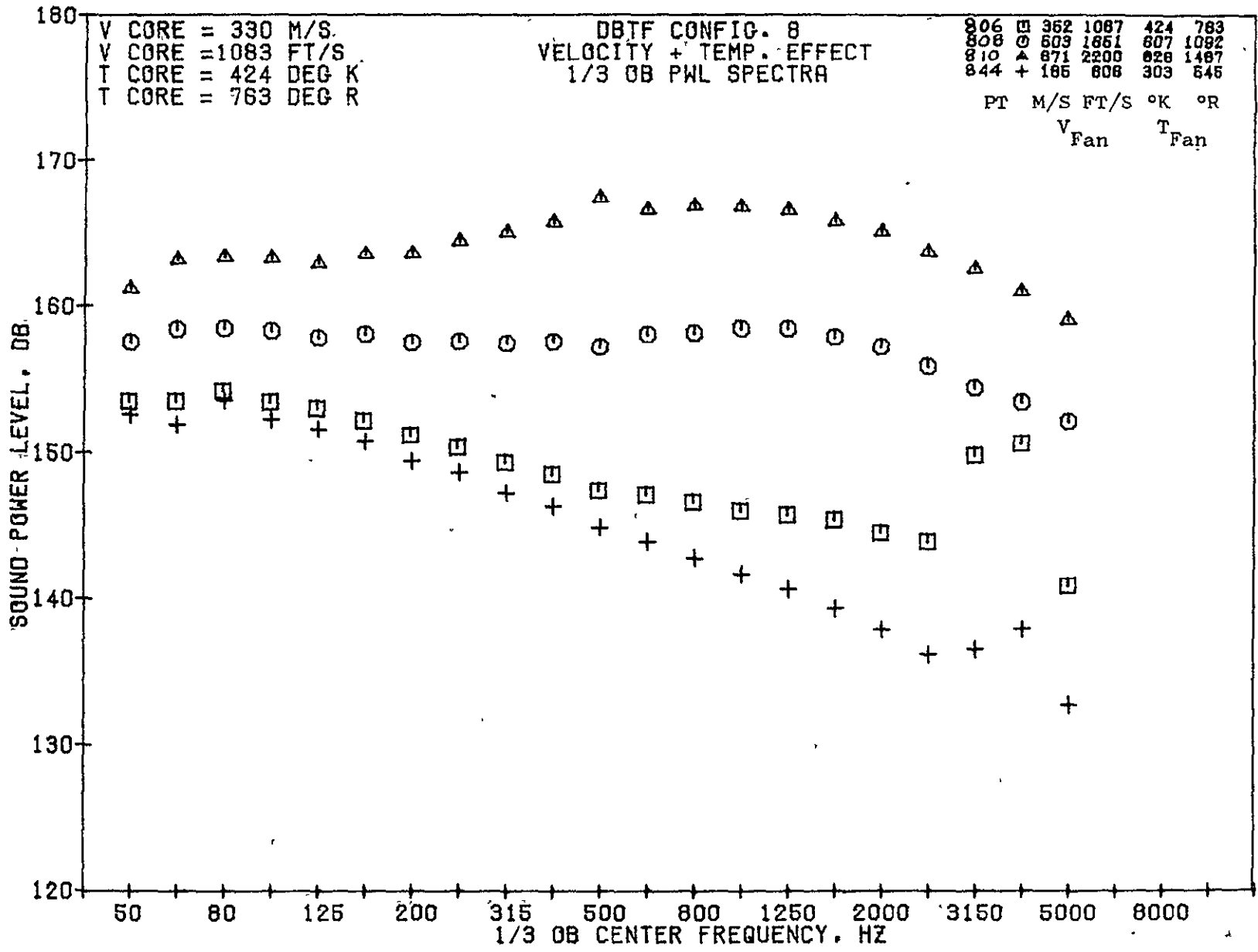
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08/20/75
 5R524-001

79 BURCH A.

13/12

1556

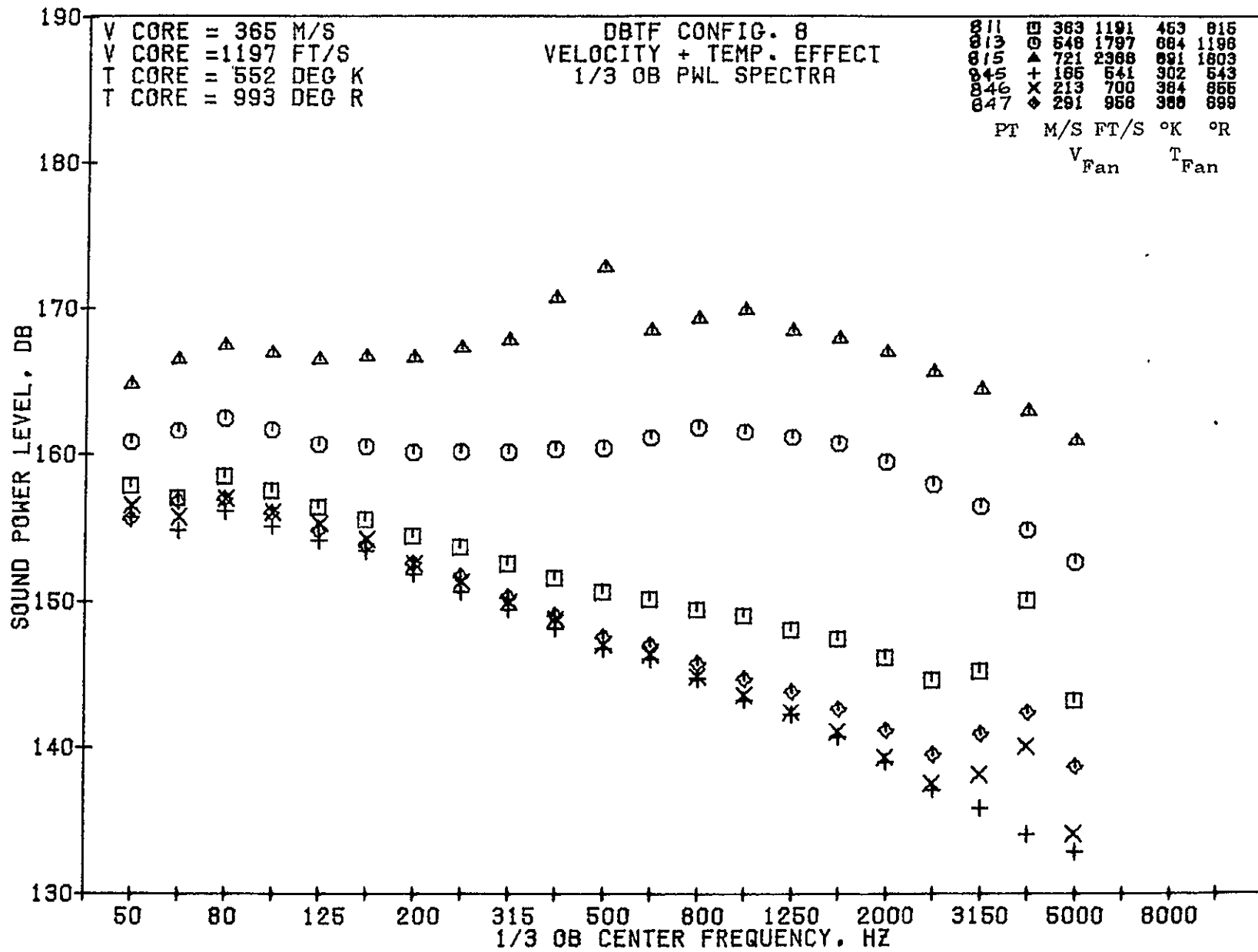


12/13

08/20/75
5R524-001

79 BURCH, A.

1557

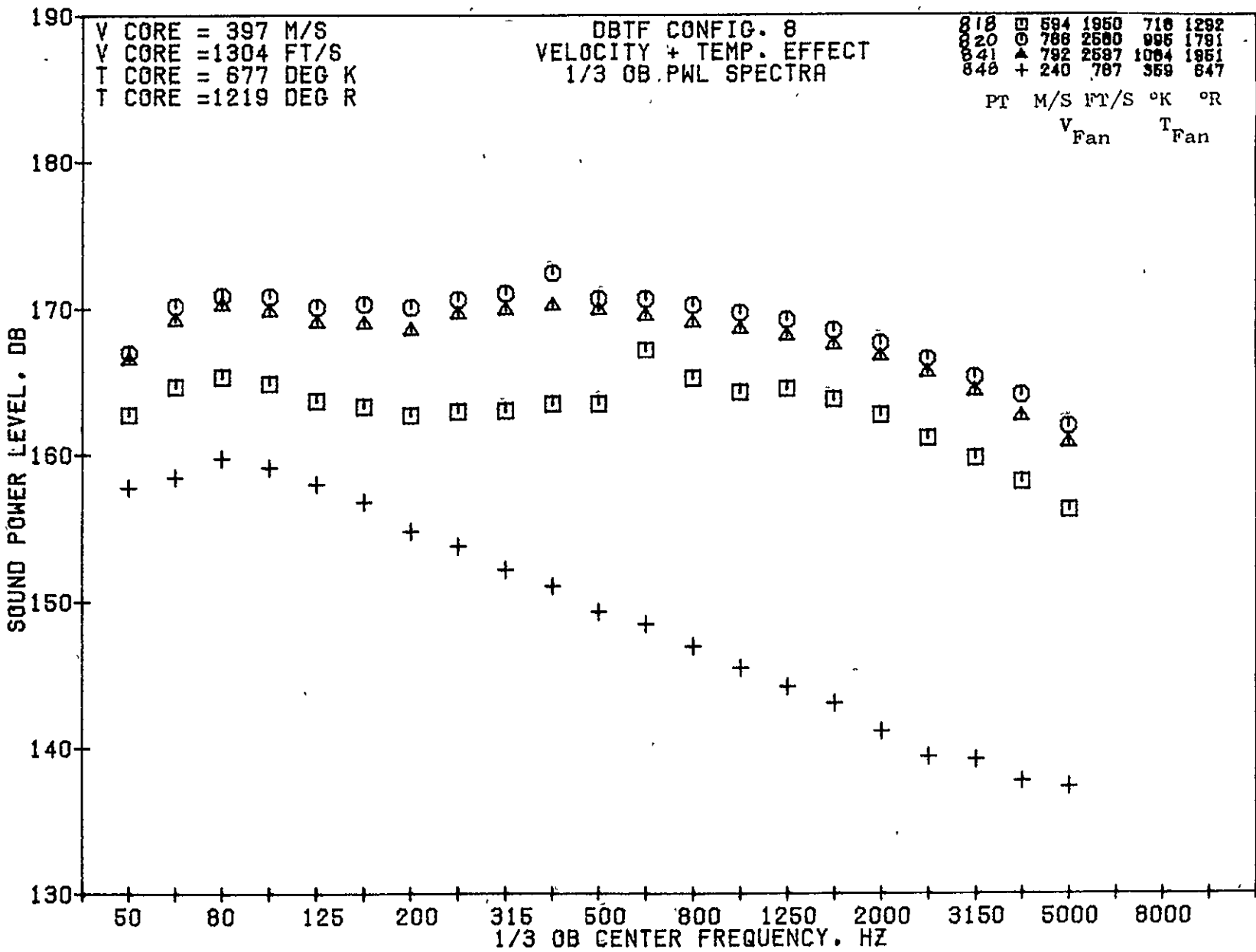


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08/20/75
 5R524-001

79 BURCH A.

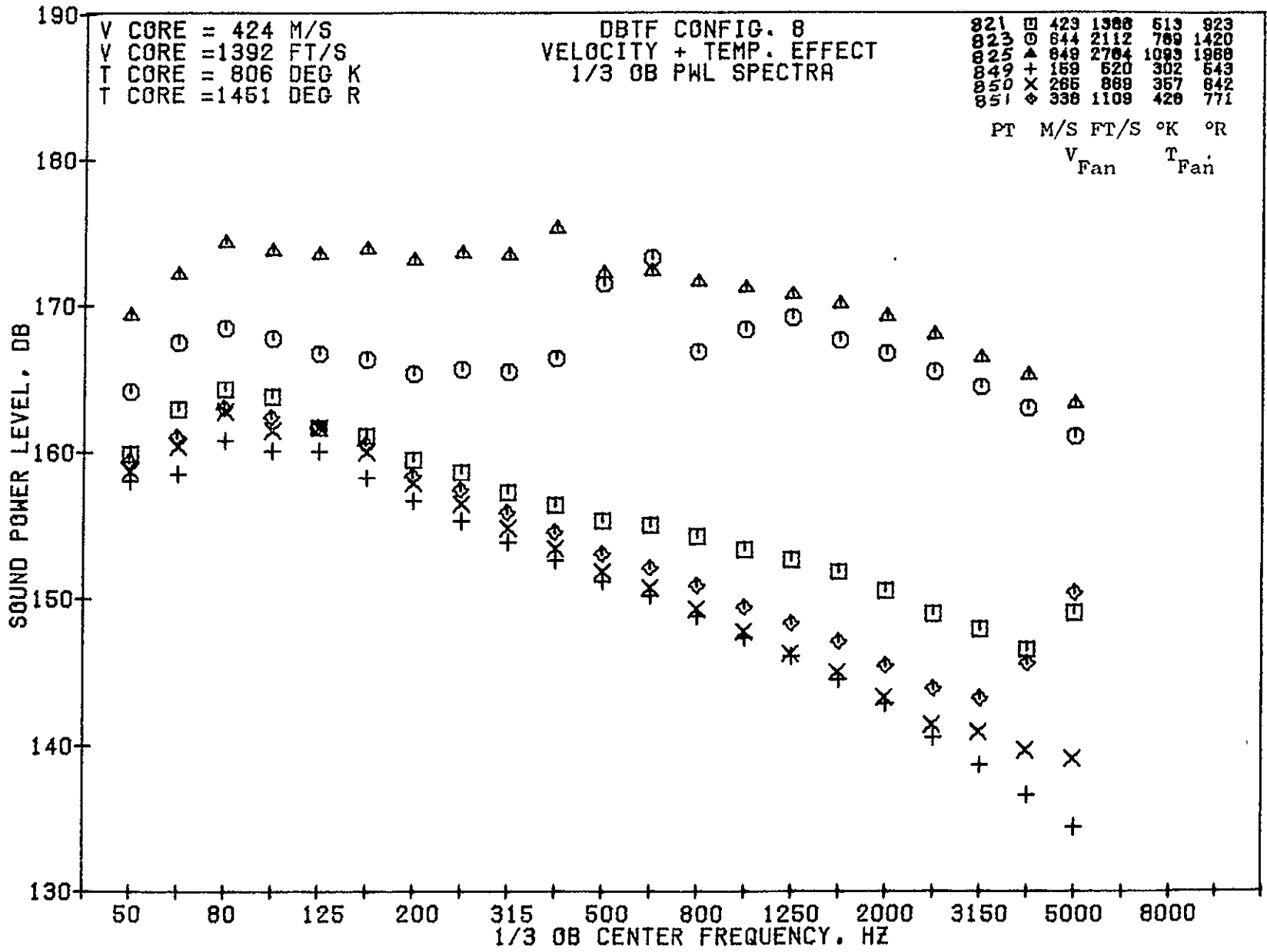
11-5/75



1-315

08/20/75
 5R524-001

79 BURCH. A.



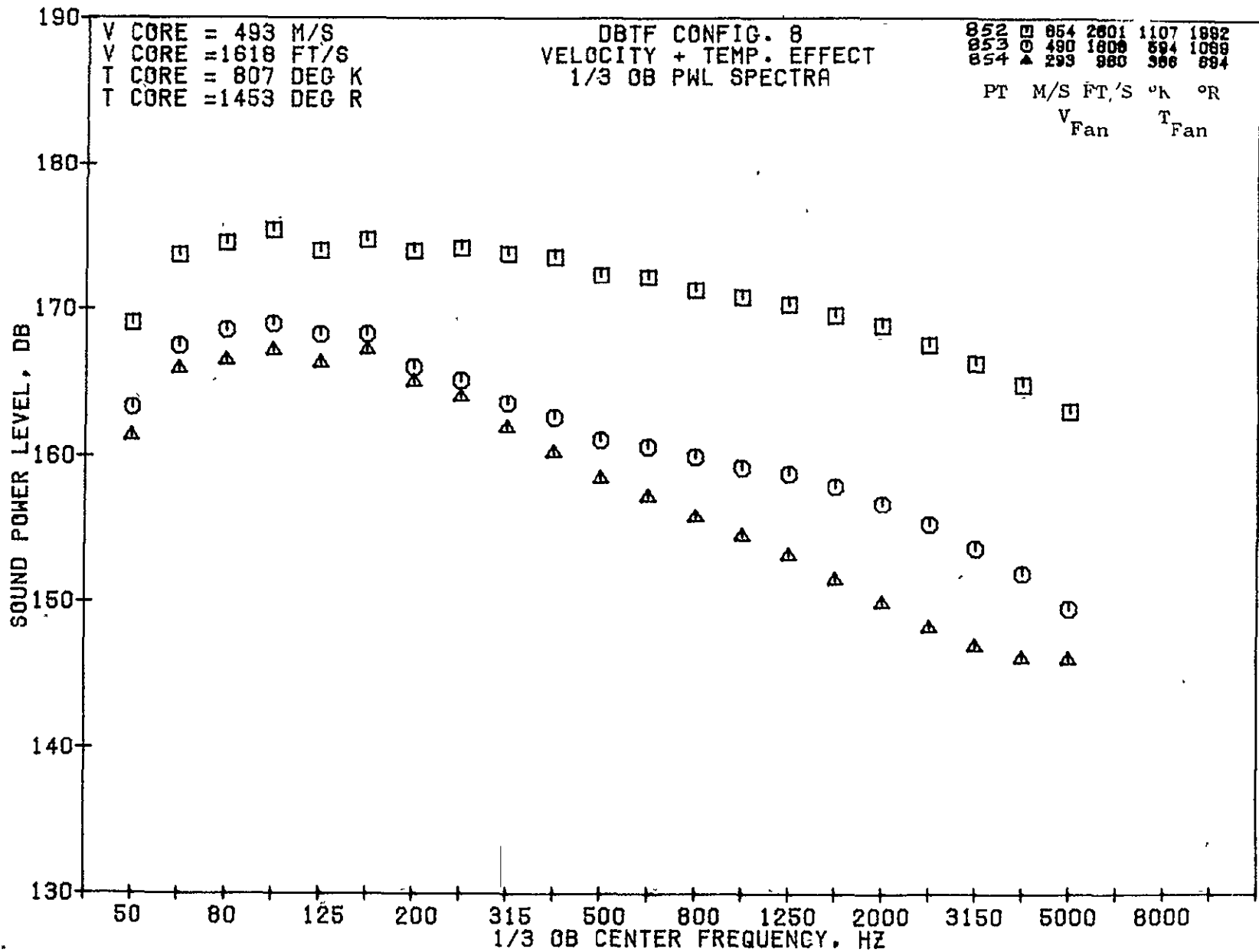
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4-3/b

08/20/75
5R524-001

79 BURCH A.

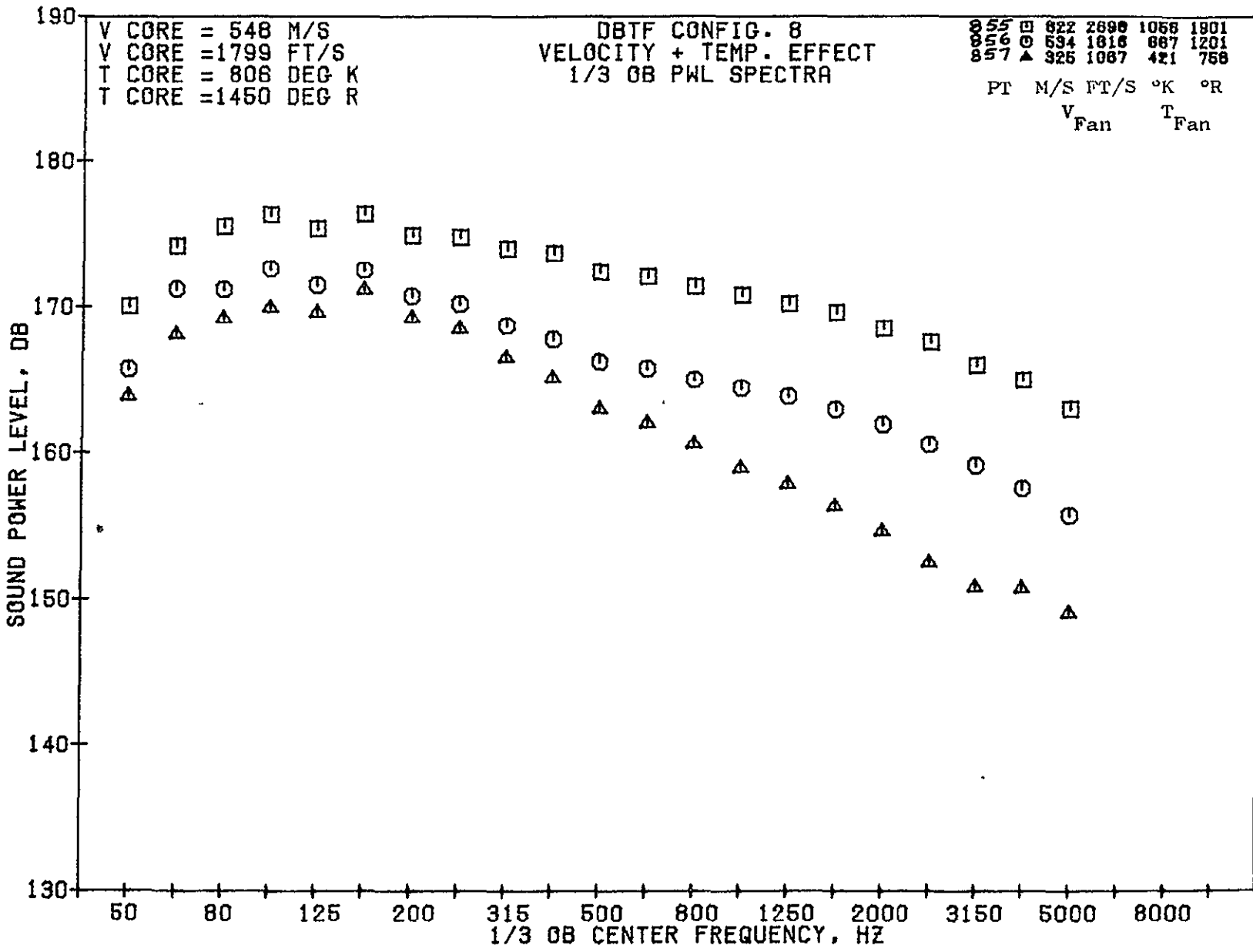
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4-317

08/20/75
 5R524-001

79 BURCH A.



1561

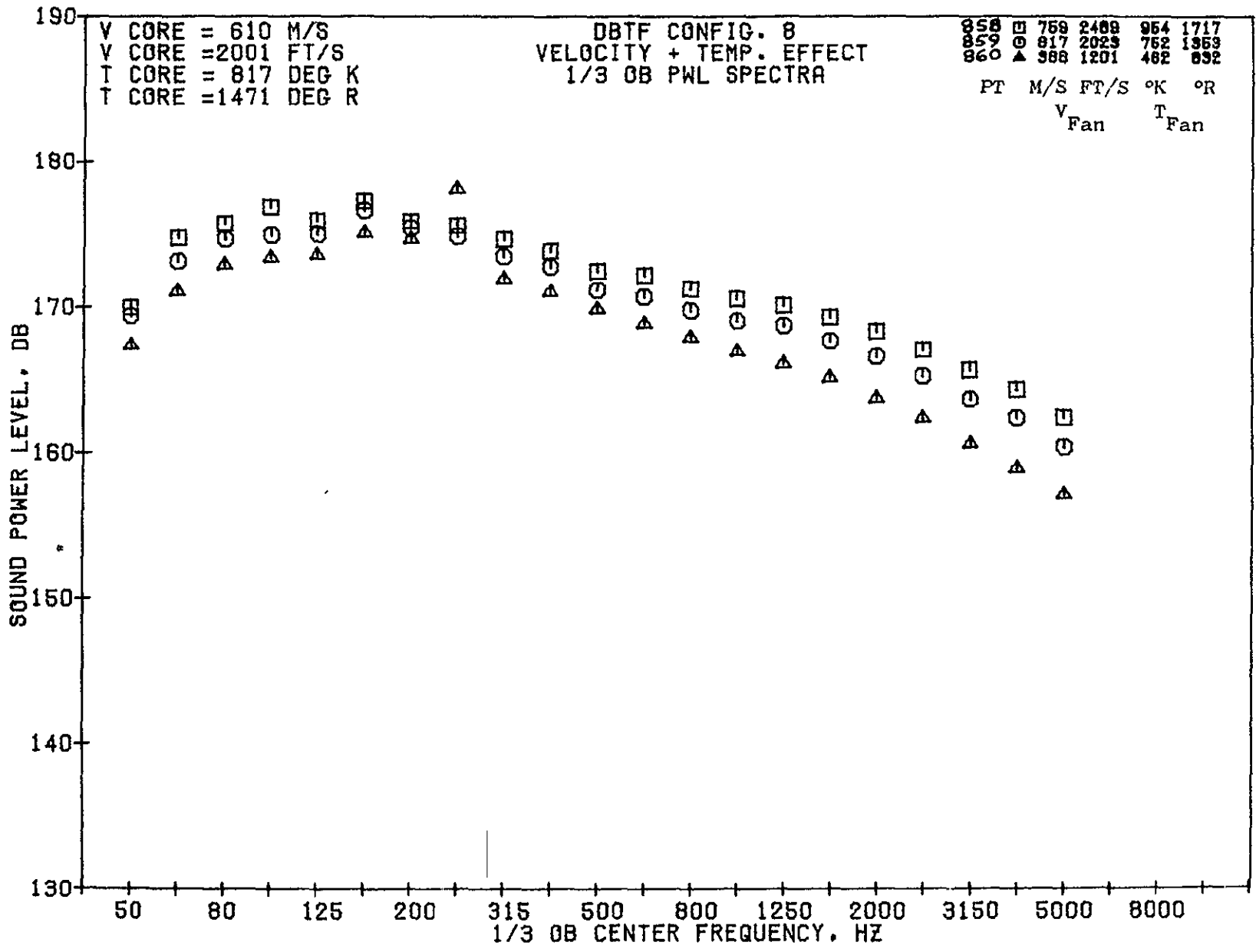
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08/20/75
5R524-001

79 BURCH A.

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1562

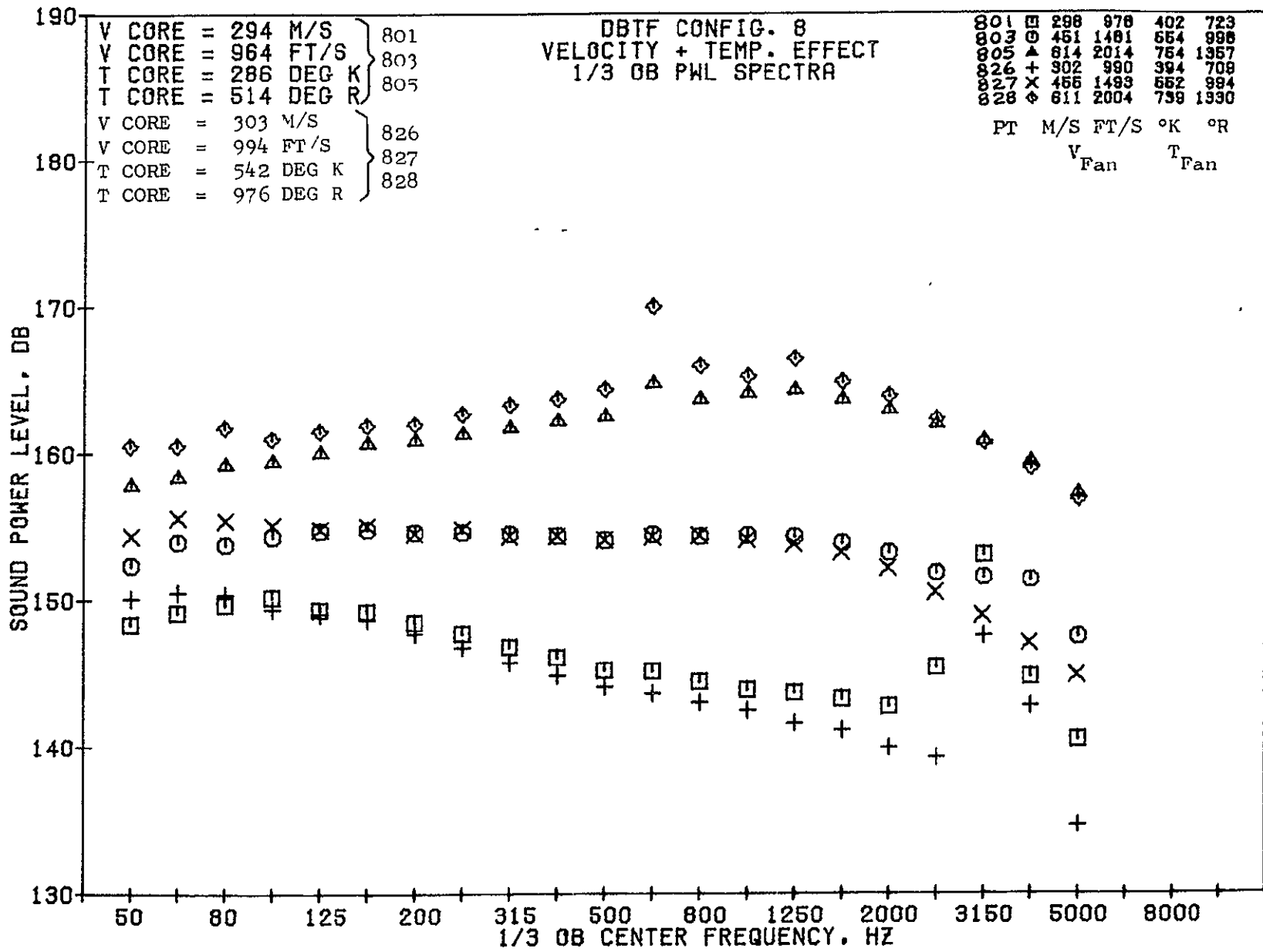


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08/20/75
5R524-001

79 BURCH A.

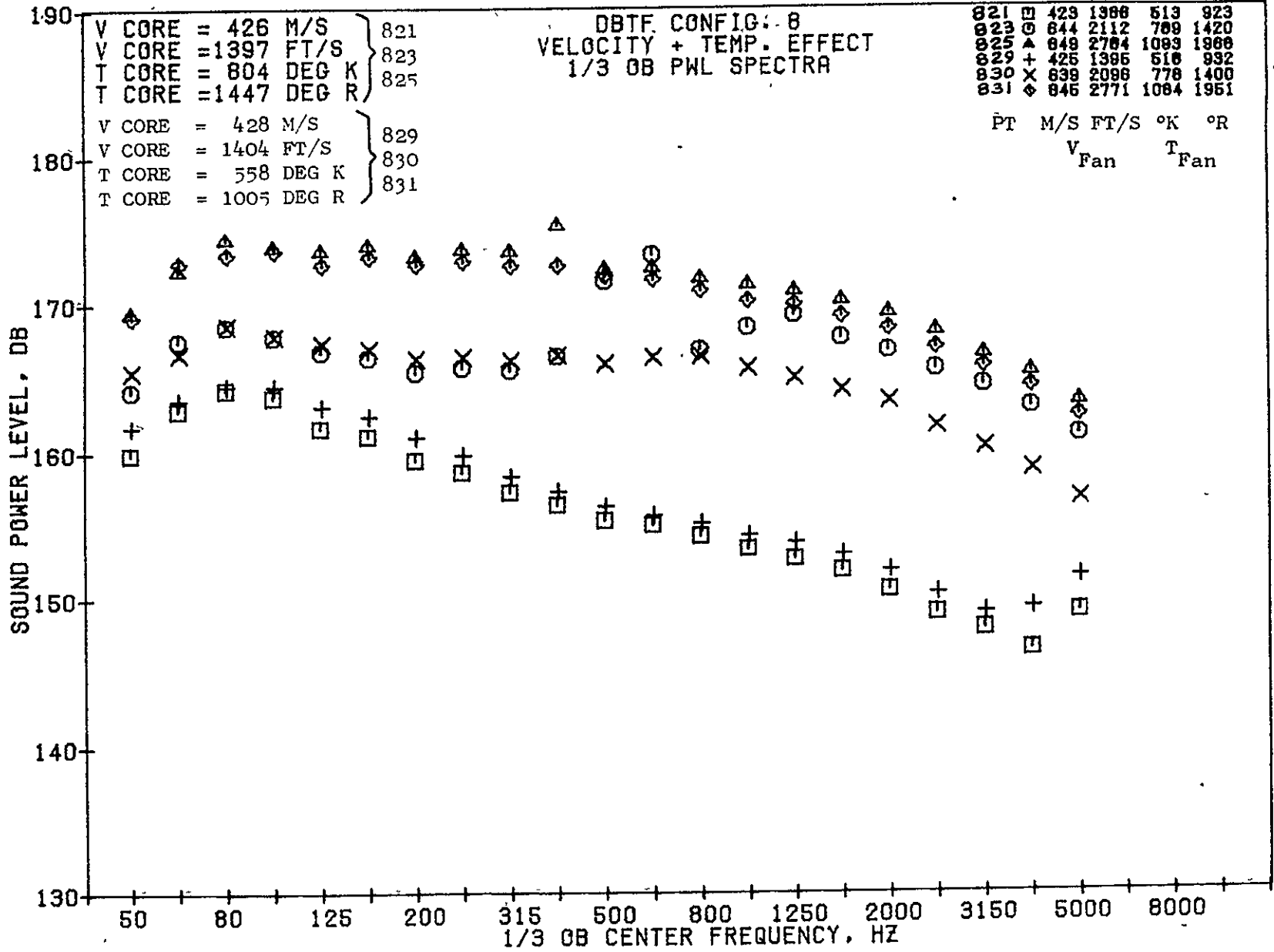
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4320

08/20/75
5R524-001

79 BURCH A.



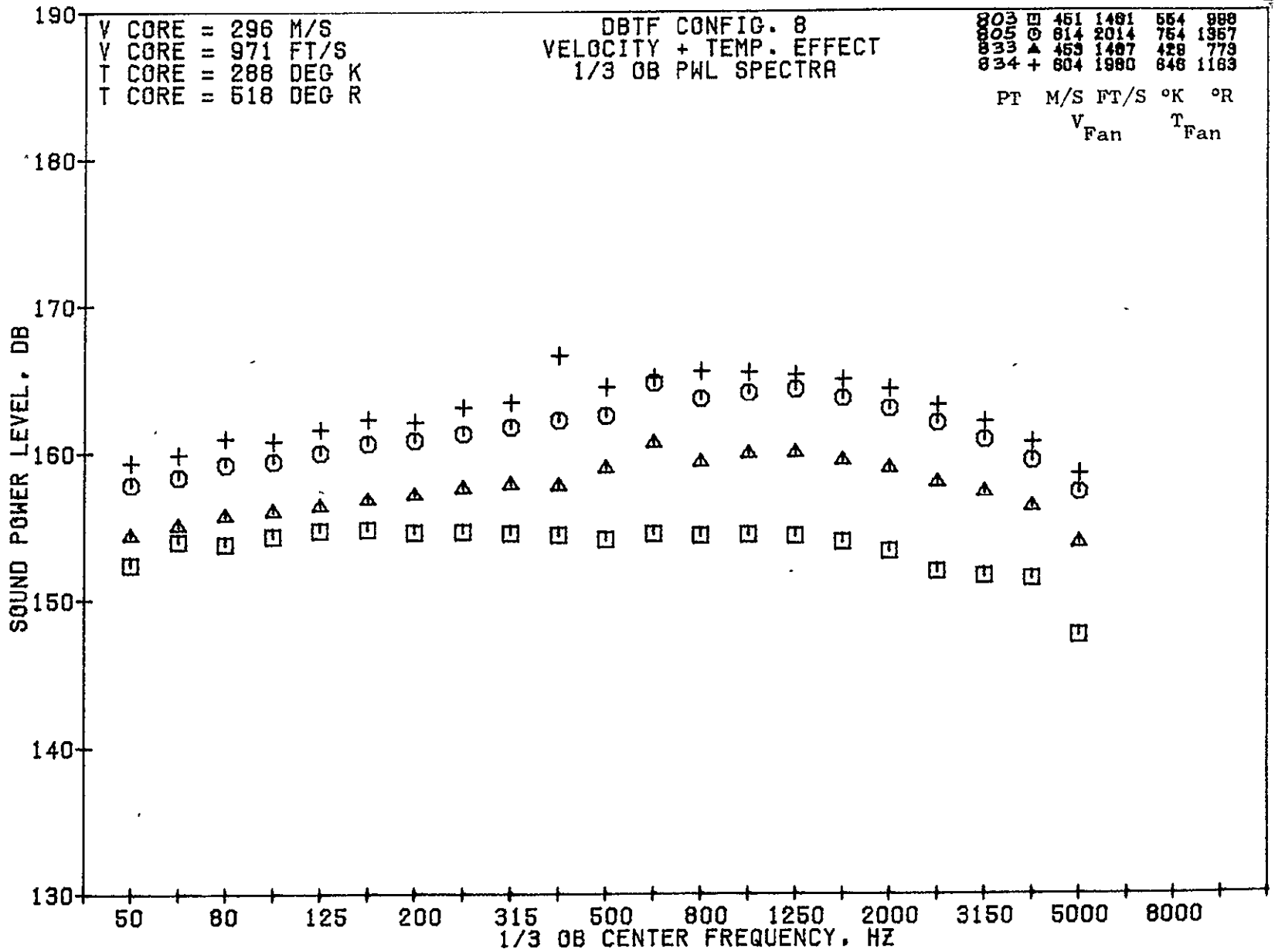
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17-321

08/20/75
5R524-001

79 BURGH A.

1565



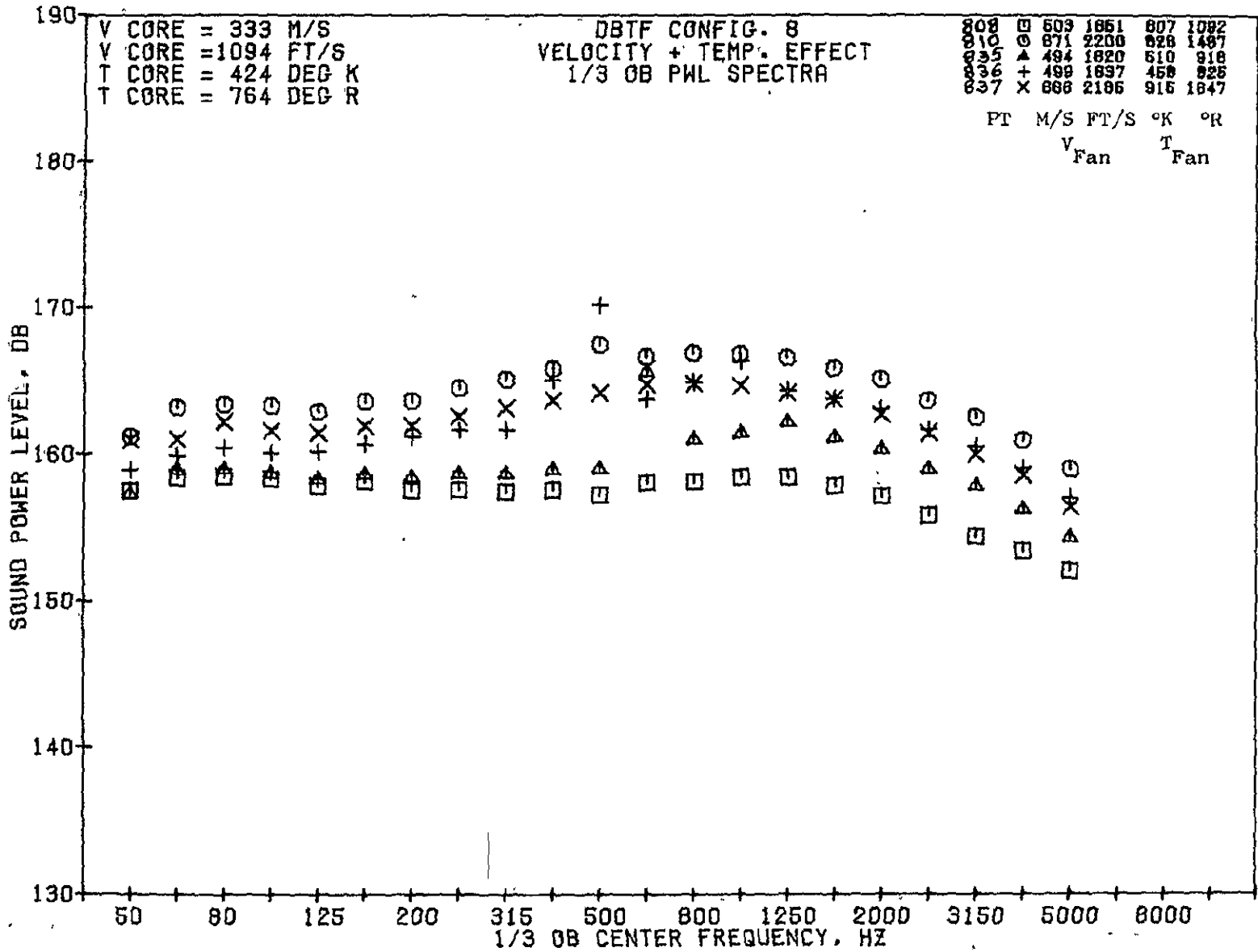
08/20/75
5R524-001

79 BURCH A.

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4 322

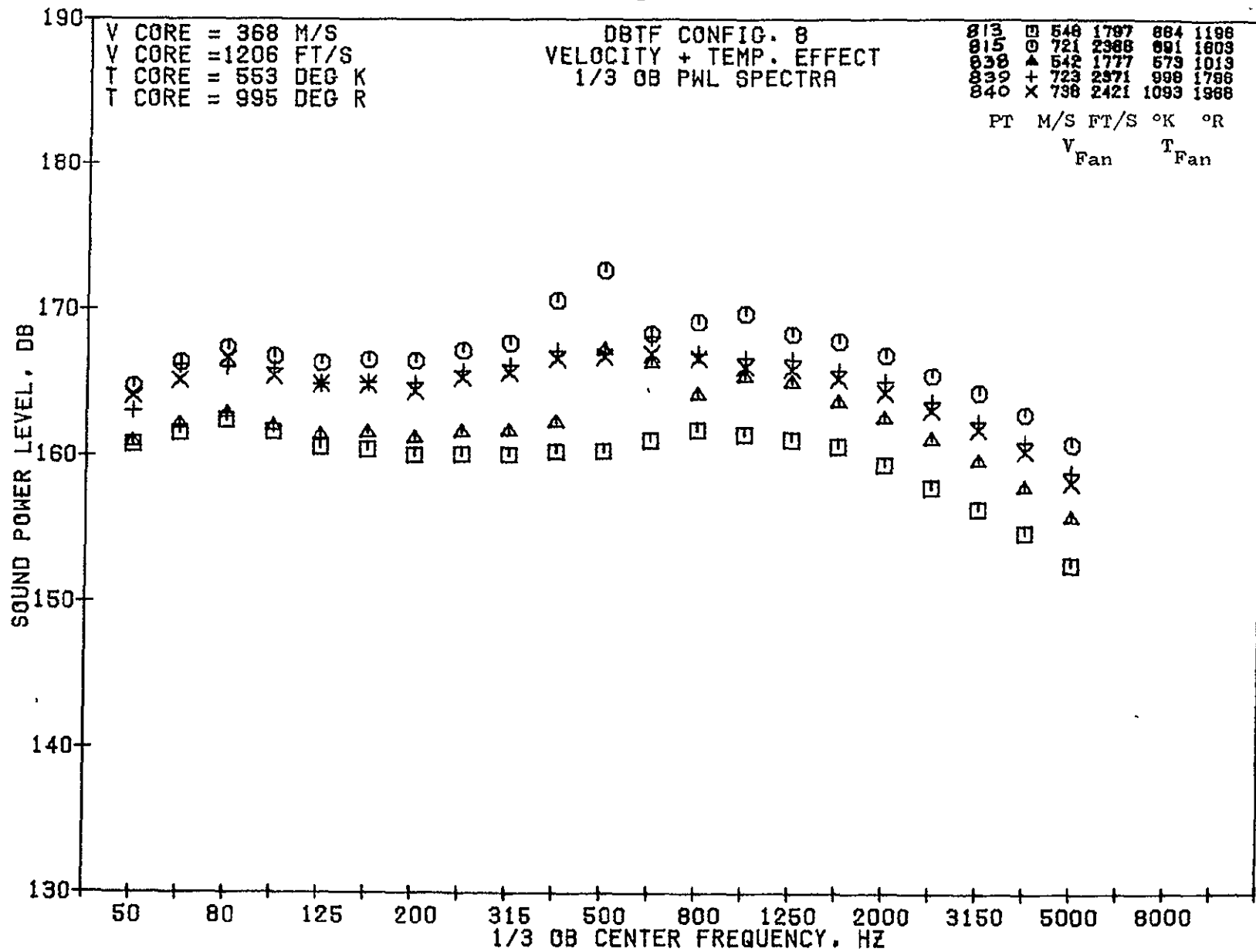
1566



1-52-5

08/20/75
 SR524-001

79 BURGLA.



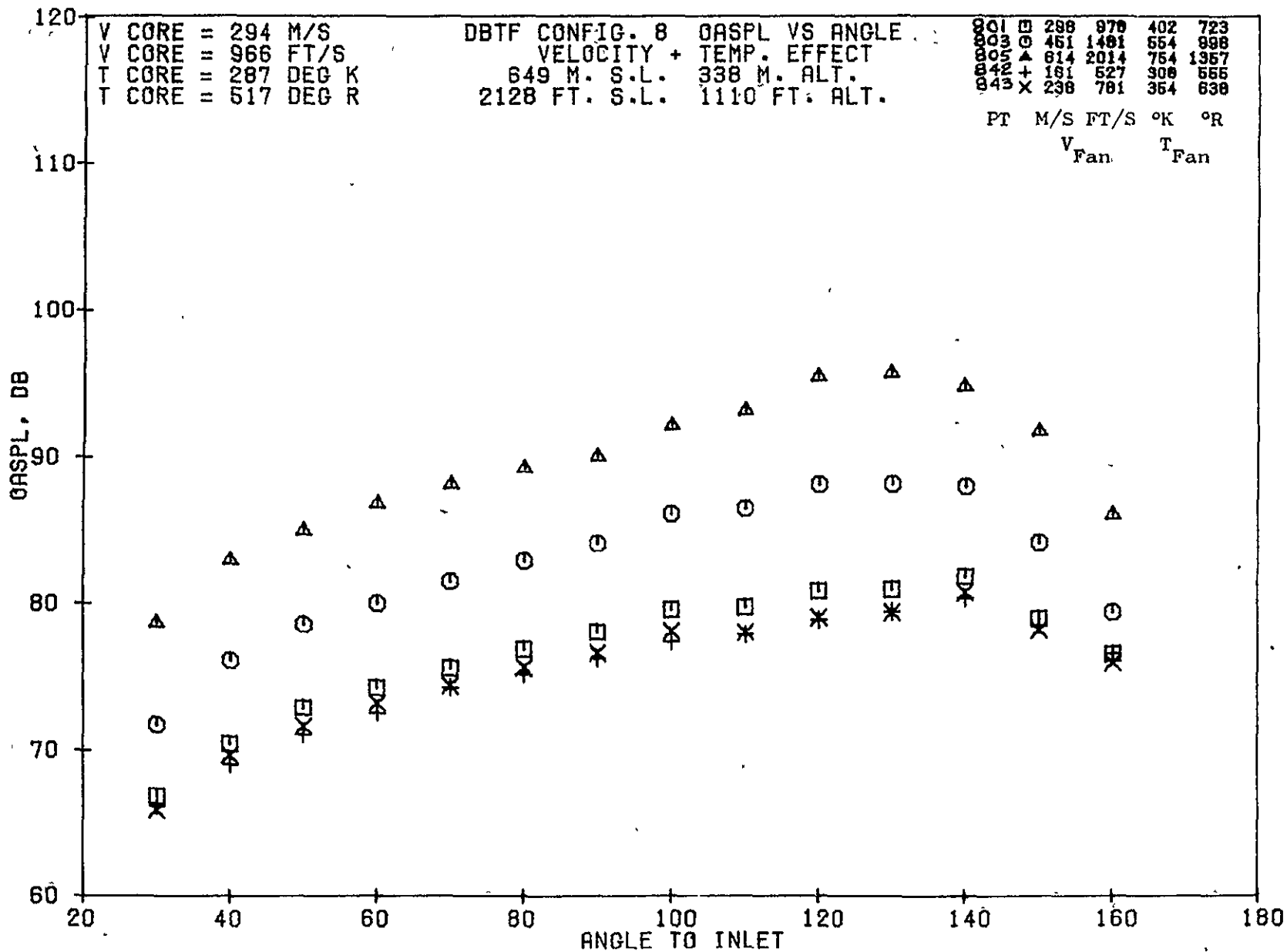
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4-304

08/20/75
5R524-001

79 BURCH A.

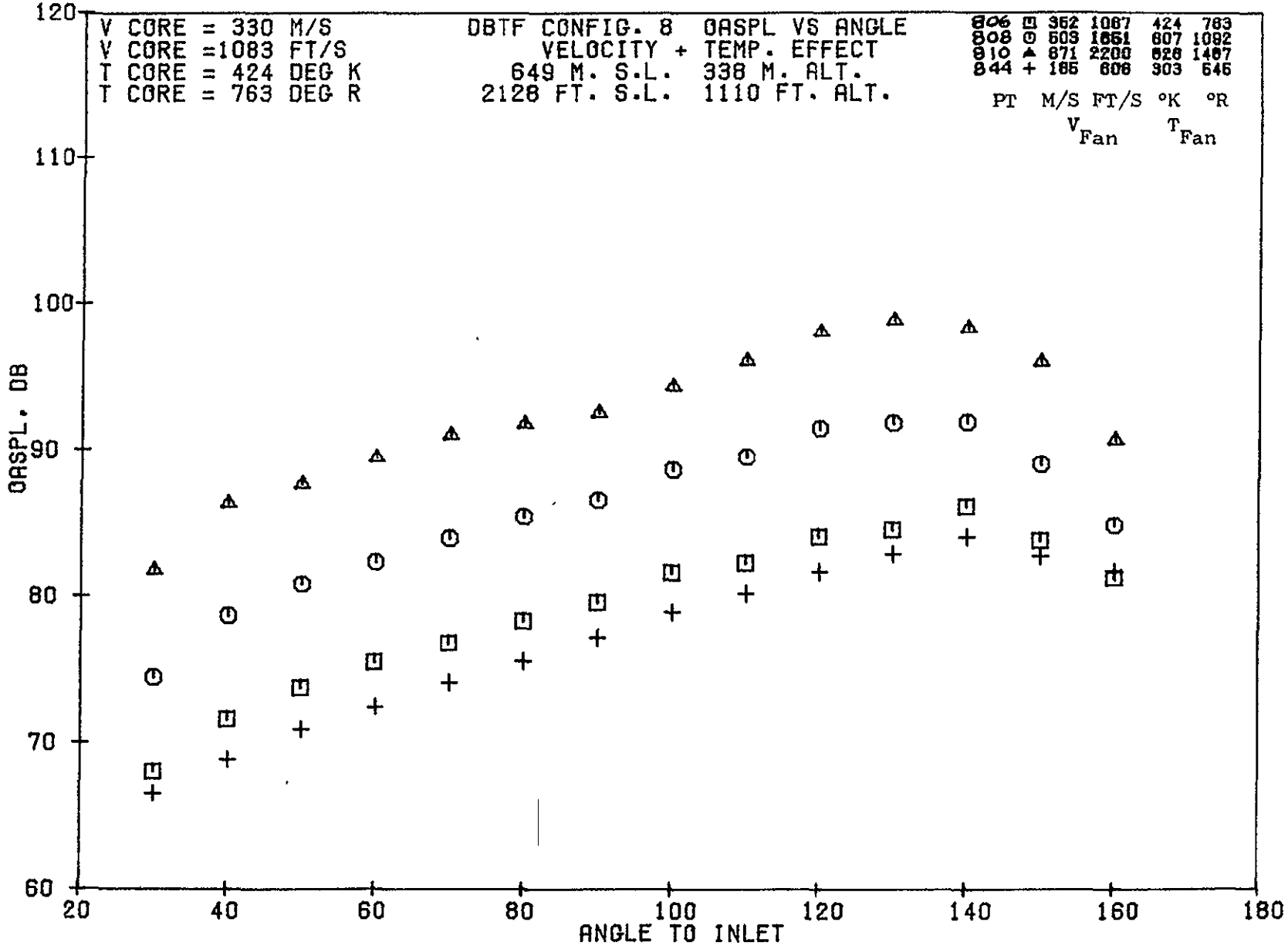
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4
325

08/20/75
 5R524-001

79 BURCH A.



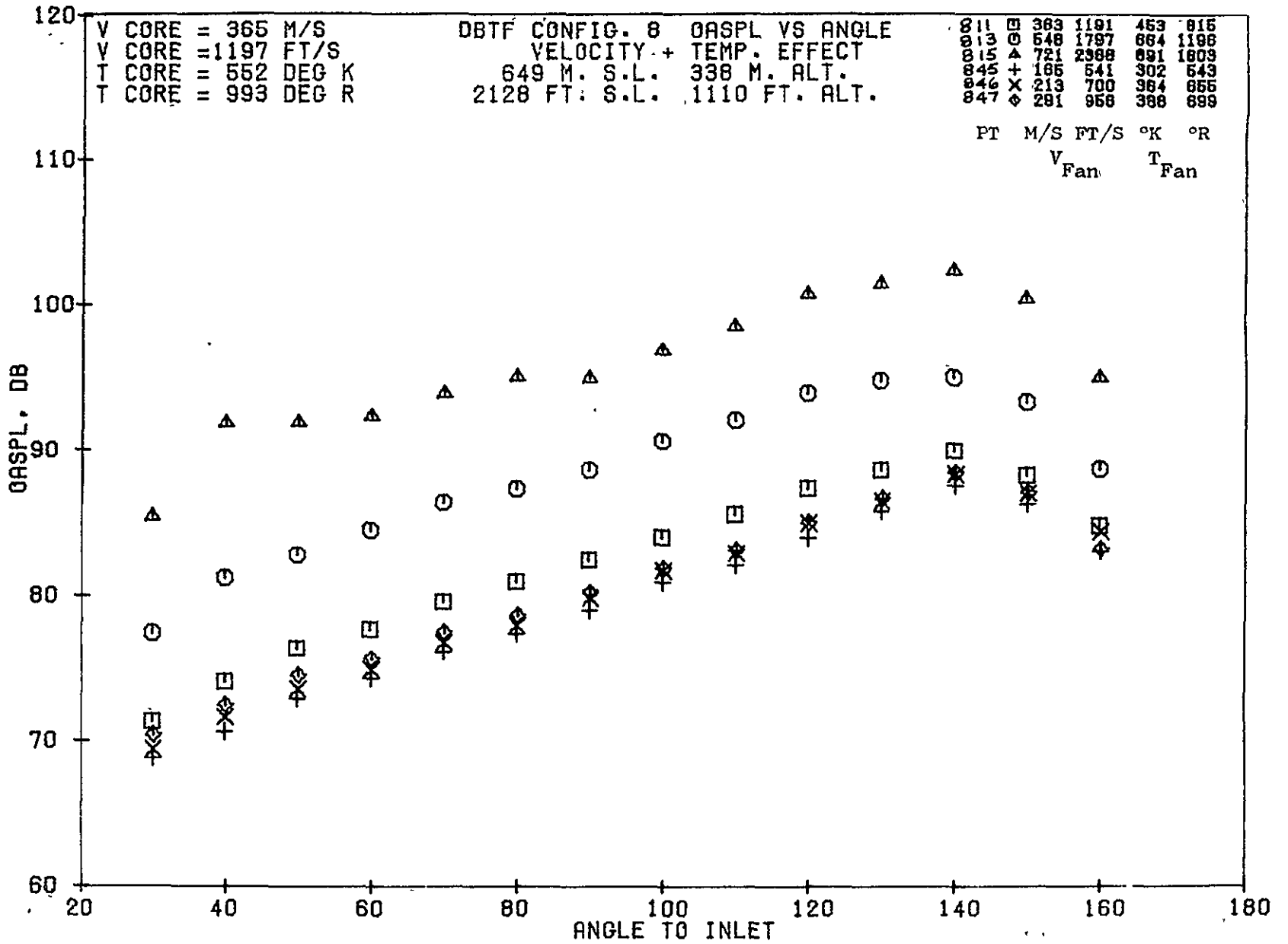
1569

4-326

08/20/75
5R524-001

79 BURCH A.

ORIGINAL PART
OF POOR QT



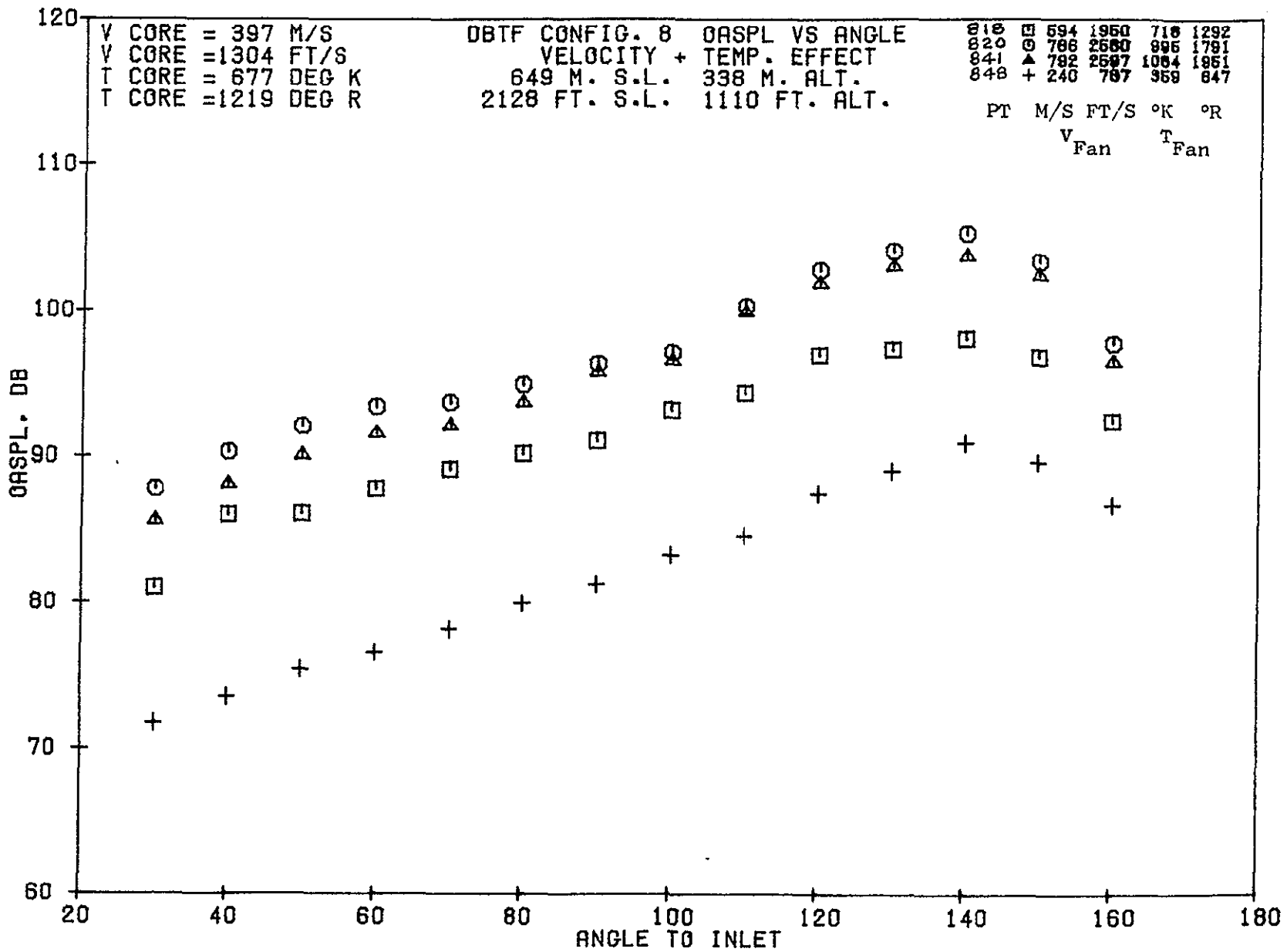
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4-329

08/20/75
5R524-001

79 BURCH A.

1571

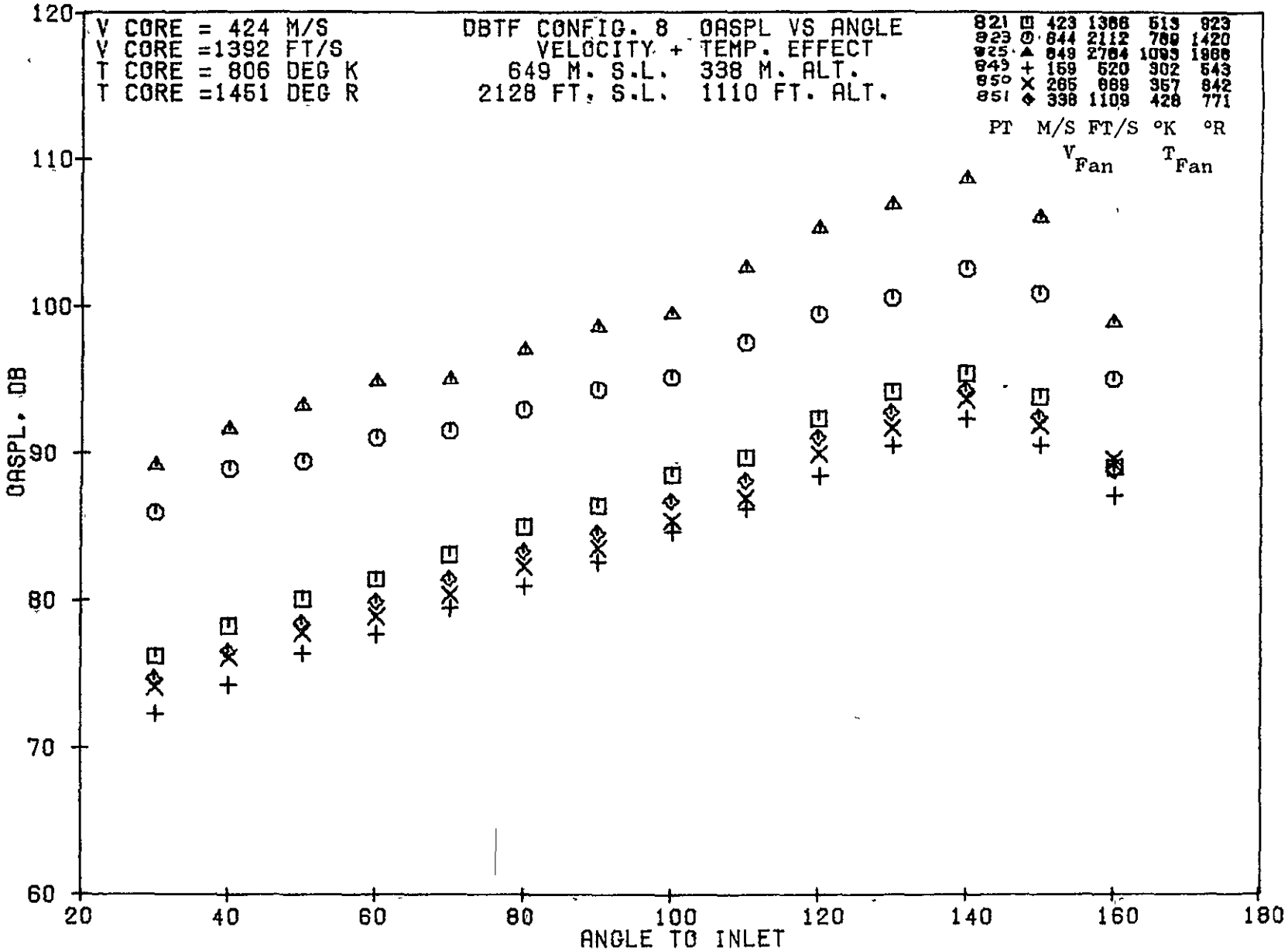


08/20/75
5R524-001

79 BURCH A.

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4-328

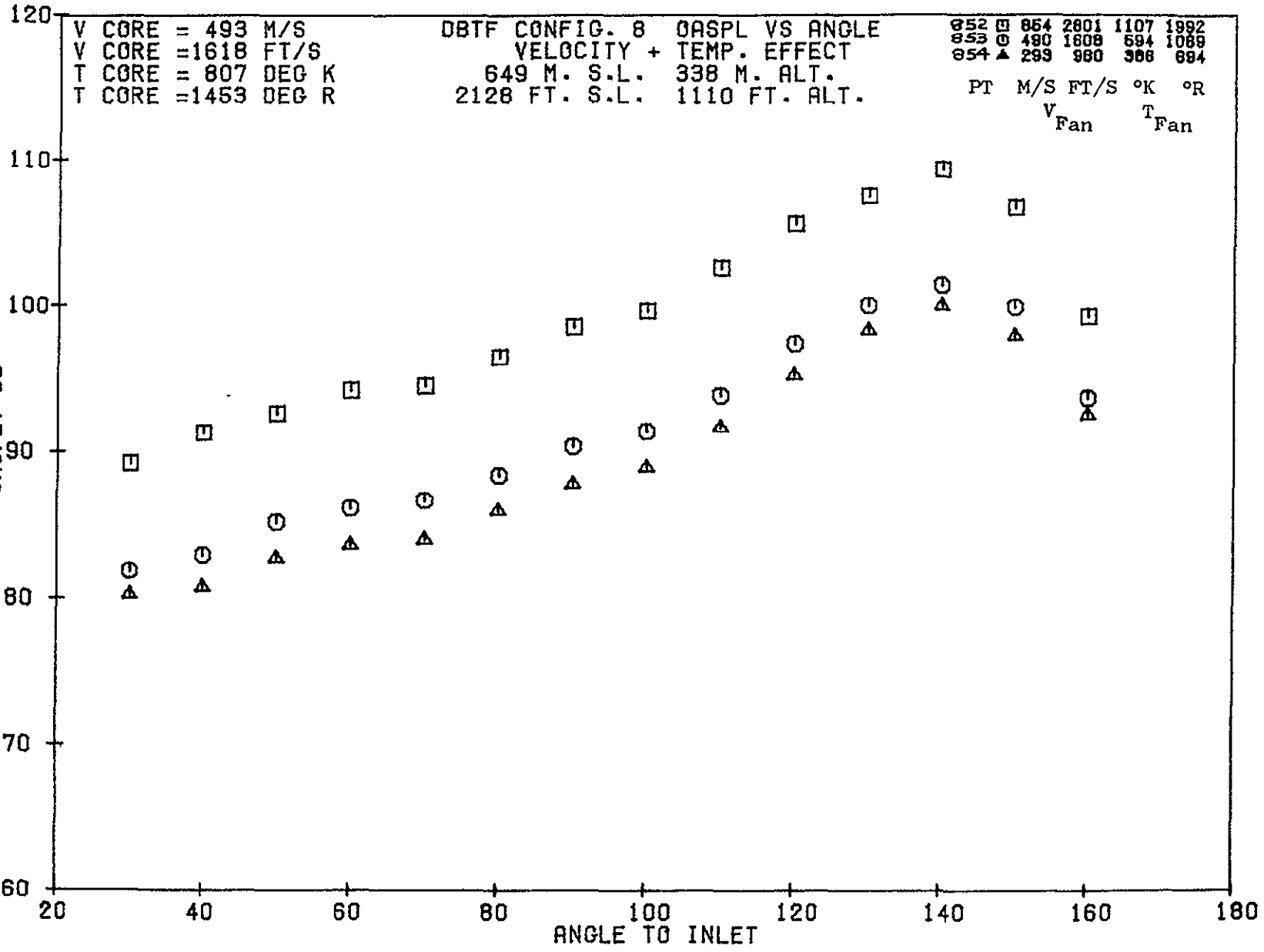


1572

4-329

08/20/75
 5R524-001

79 BURCH A.



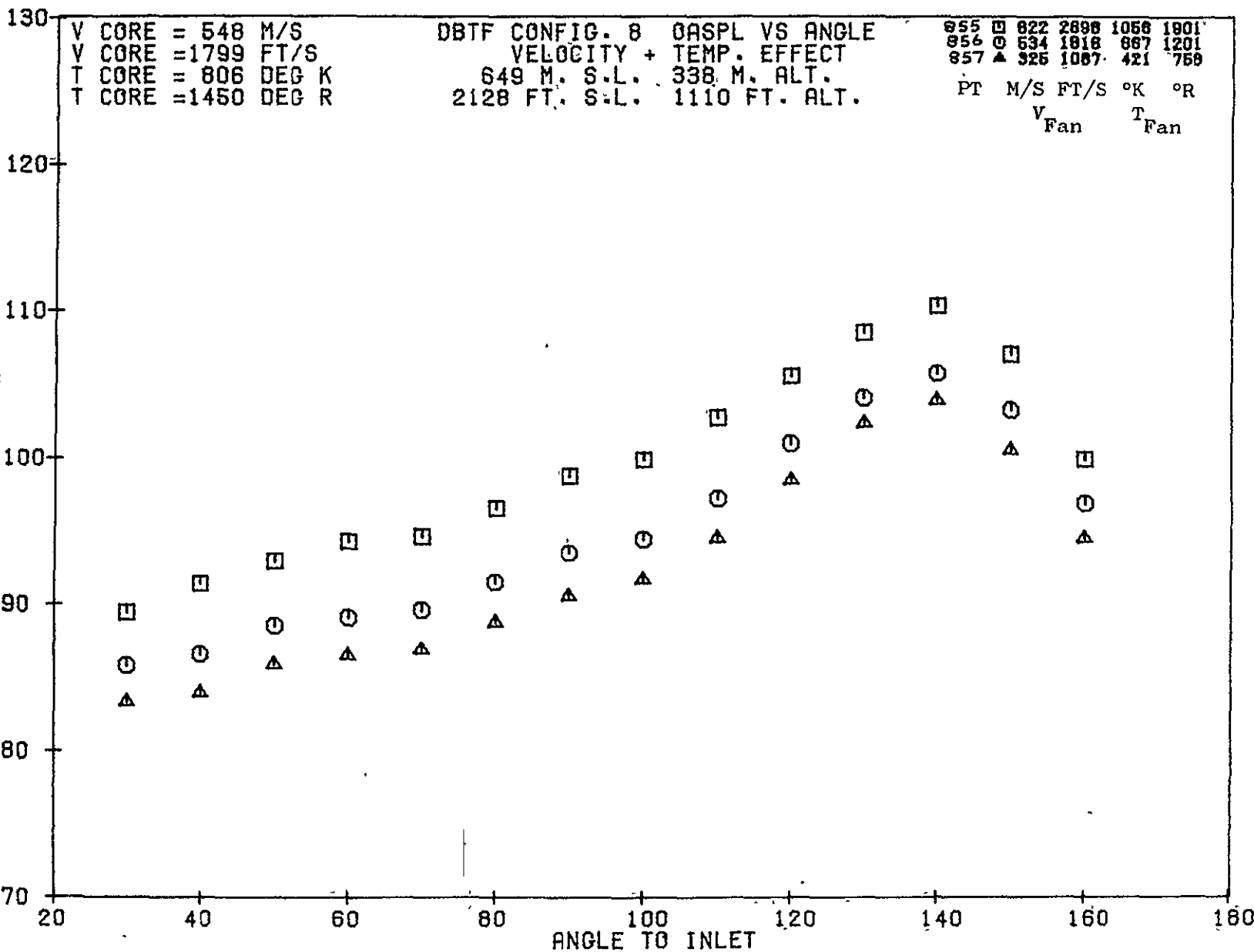
1573

08/20/75
 5R524-001

79 BURCH A.

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1-55c



1574

4-331

08/20/76
 5R524-001

79 BURD A.

130
120
110
100
90
80
70

V CORE = 610 M/S
V CORE = 2001 FT/S
T CORE = 817 DEG K
T CORE = 1471 DEG R

DBTF CONFIG. 8 OASPL VS ANGLE
VELOCITY + TEMP. EFFECT
649 M. S.L. 338 M. ALT.
2128 FT. S.L. 1110 FT. ALT.

858	759	2469	964	1717
859	817	2023	752	1353
860	388	1201	462	832
PT	M/S	FT/S	°K	°R
	V _{Fan}		T _{Fan}	

OASPL, DB

ANGLE TO INLET

20 40 60 80 100 120 140 160 180

1575

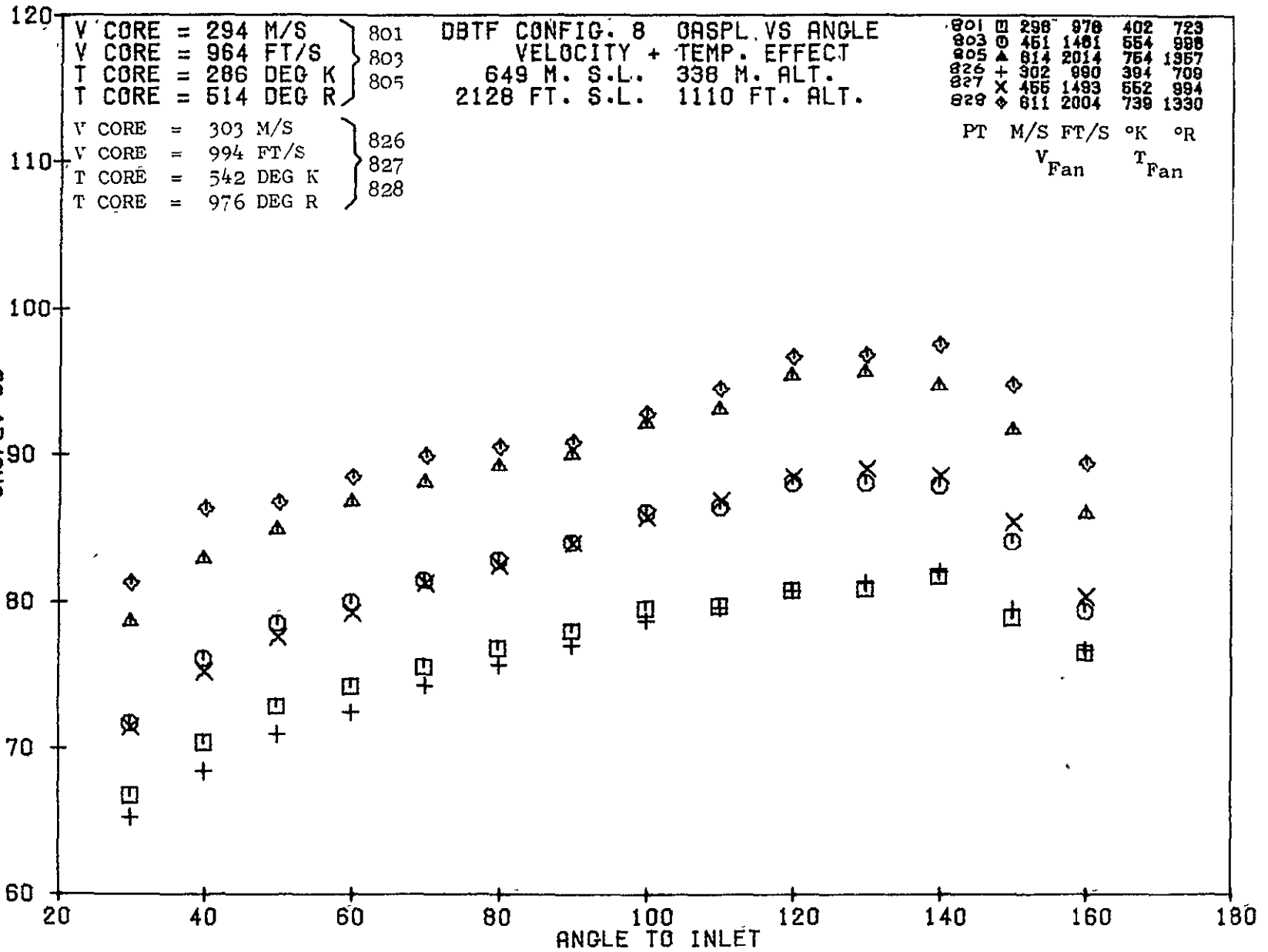
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5R524-001

79 BURCH A.

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4-532

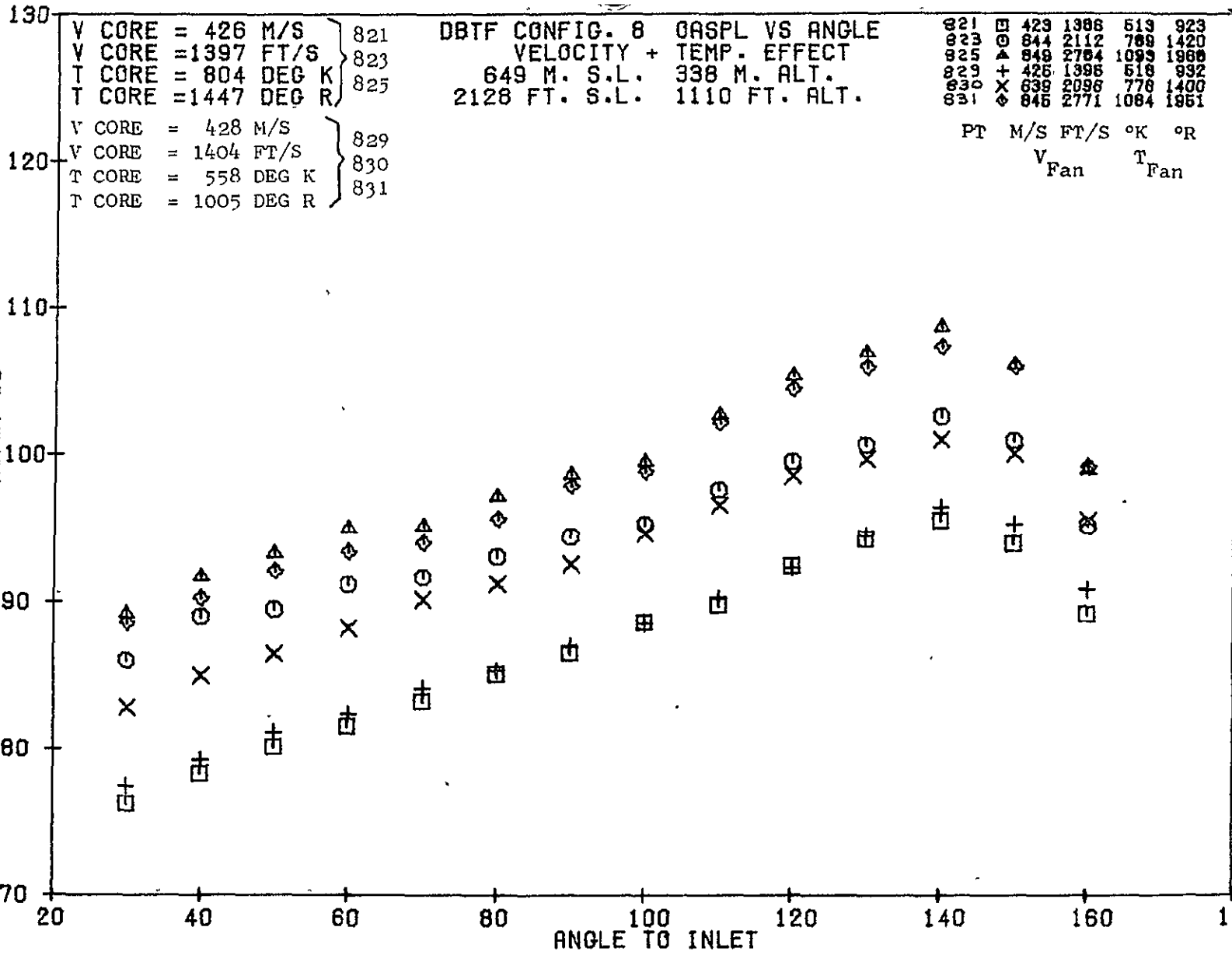
1576



14
1533

08/20/75
5R524-001

79 BURCH A.



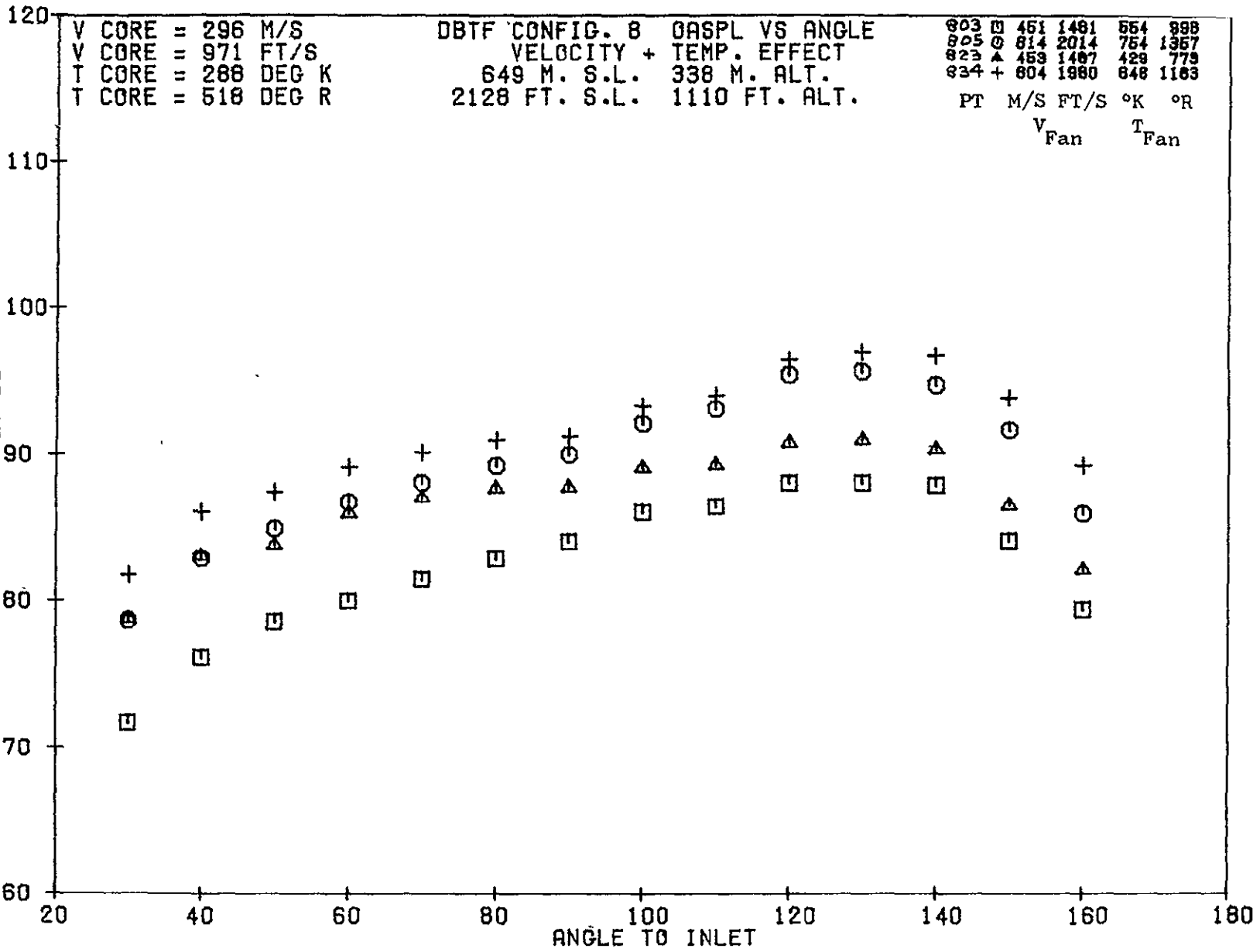
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4-364

08/20/75
5R524-001

79 BURCH A.

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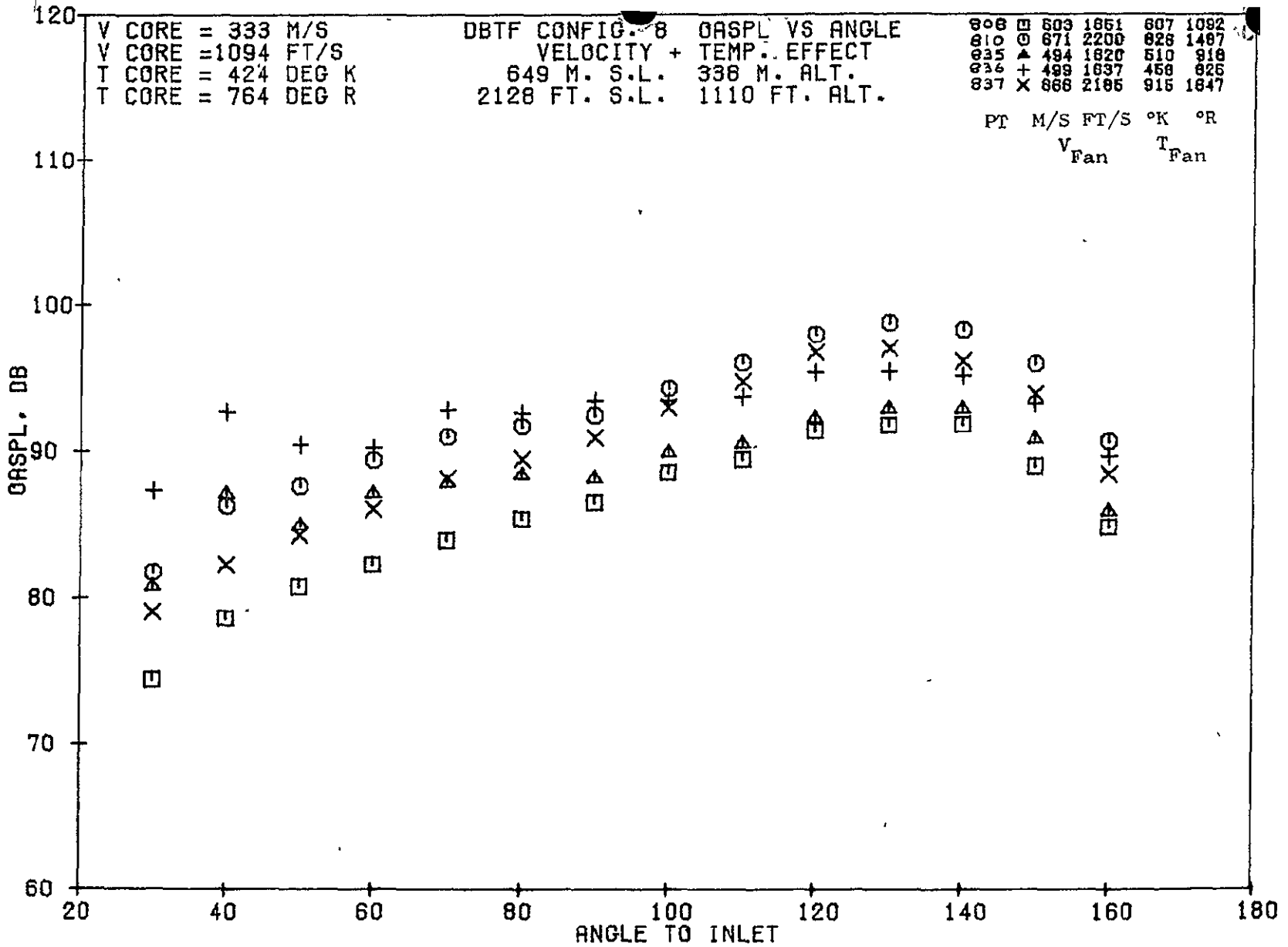


4-335

08/20/76
 5R524-001

79 BURCH A.

1579

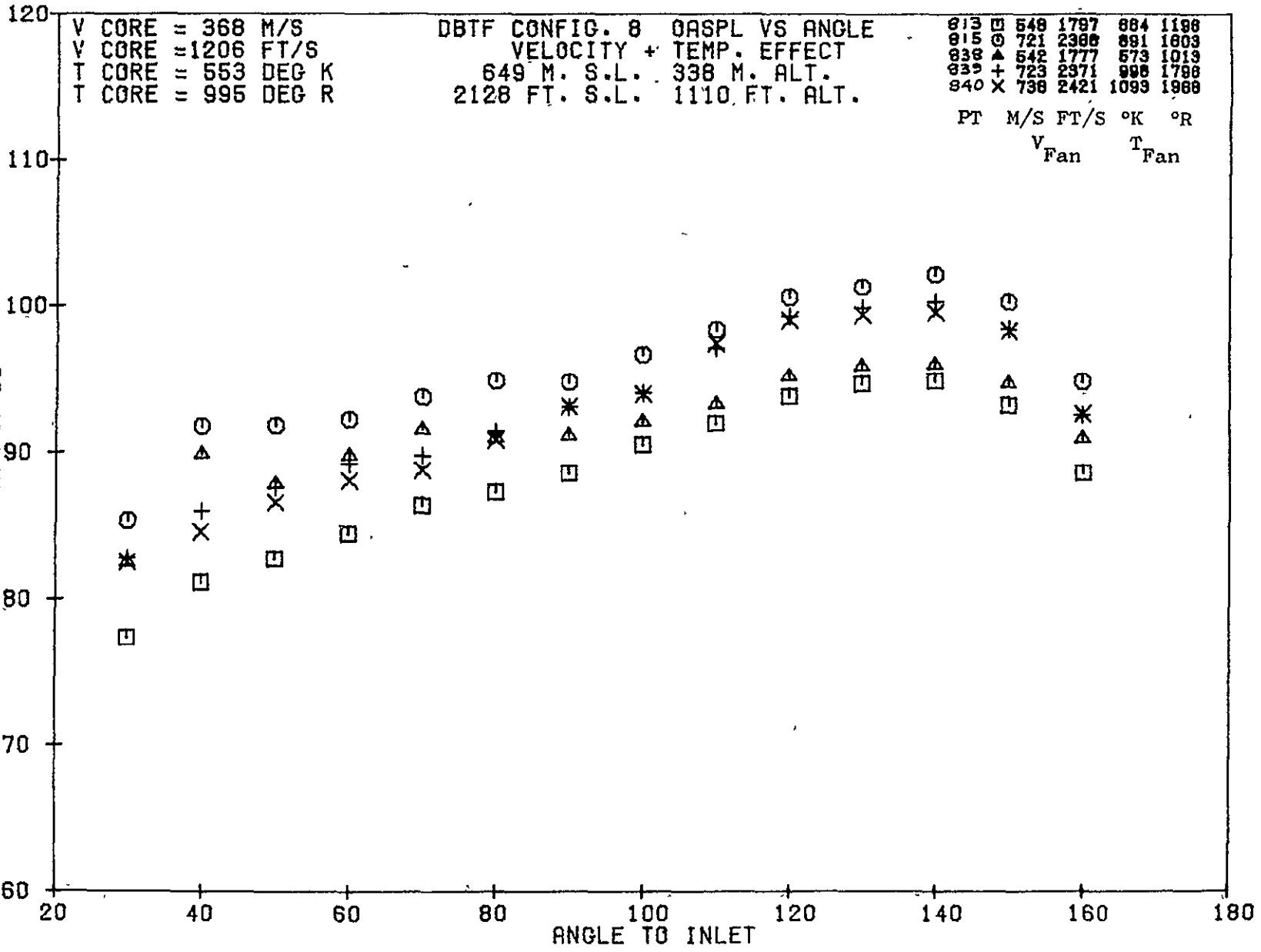


08/20/75
5R524-001

79 BURCH A.

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4-3-76



4-257

08/20/75
5R524-001

79 BURCH A.

1581

PNL: PNOB

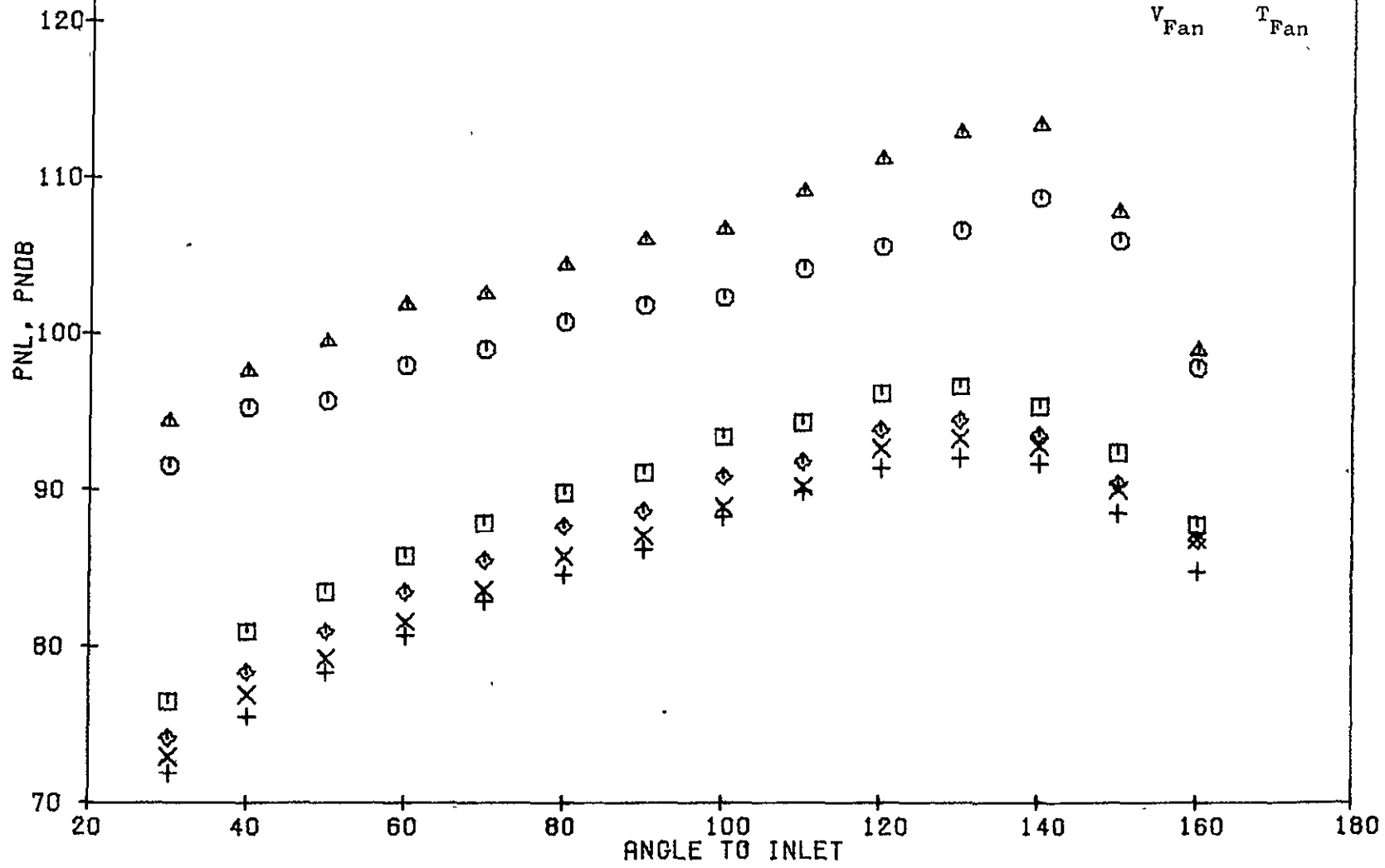
PNL: PNOB

V CORE = 424 M/S
 V CORE = 1392 FT/S
 T CORE = 806 DEG K
 T CORE = 1461 DEG R

DBTF CONFIG. 8 PNL VS ANGLE
 VELOCITY + TEMP. EFFECT
 649 M. S.L. 338 M. ALT.
 2128 FT. S.L. 1110 FT. ALT.

021	0	423	1386	613	929
023	0	844	2112	789	1420
025	▲	948	2764	1093	1888
049	+	169	520	302	543
050	X	265	889	367	642
051	◇	338	1109	426	771

PT M/S FT/S °K °R
 V Fan T Fan

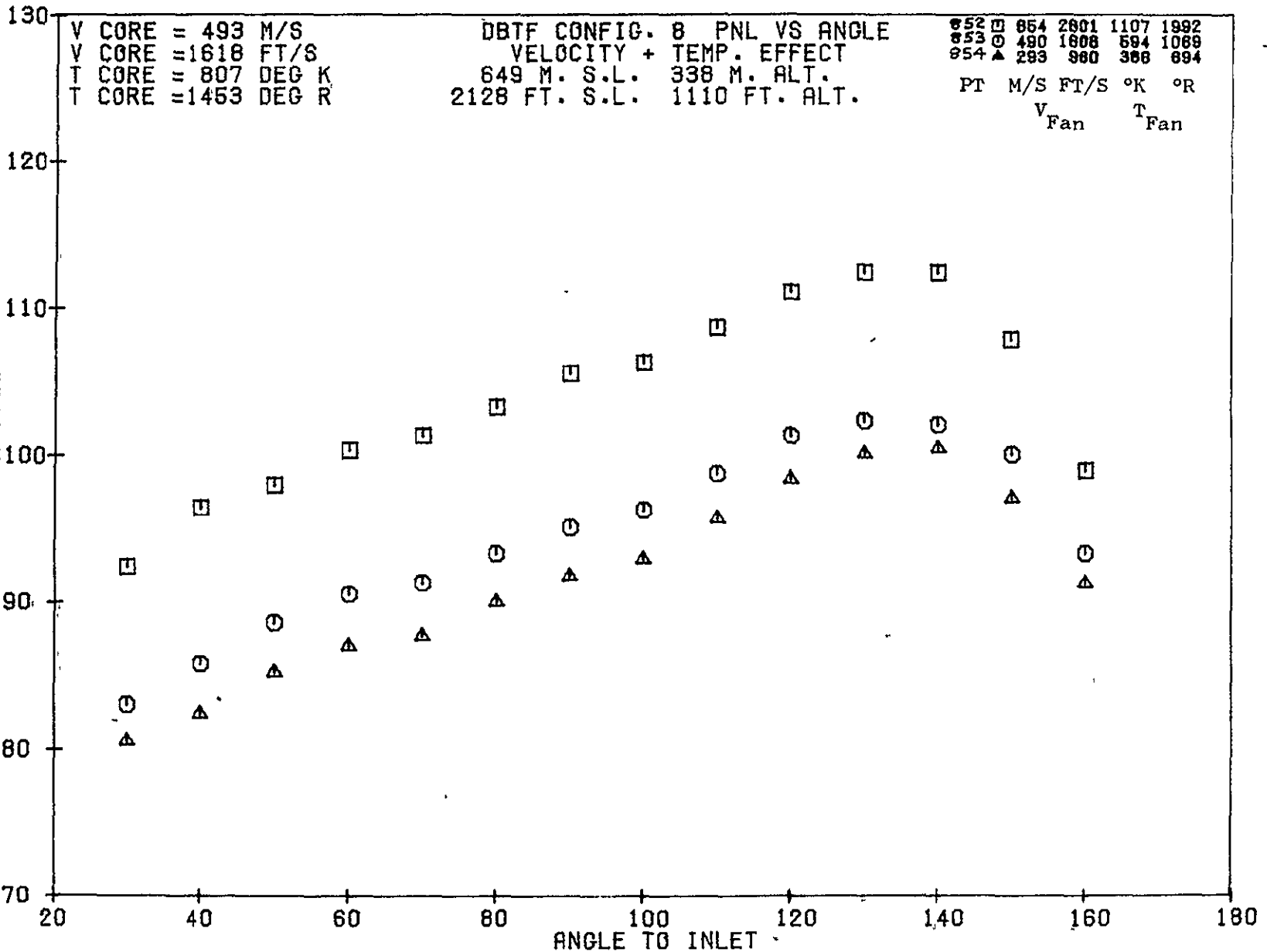


08/20/75
 5R524-001

79 BURCH A.

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11-338



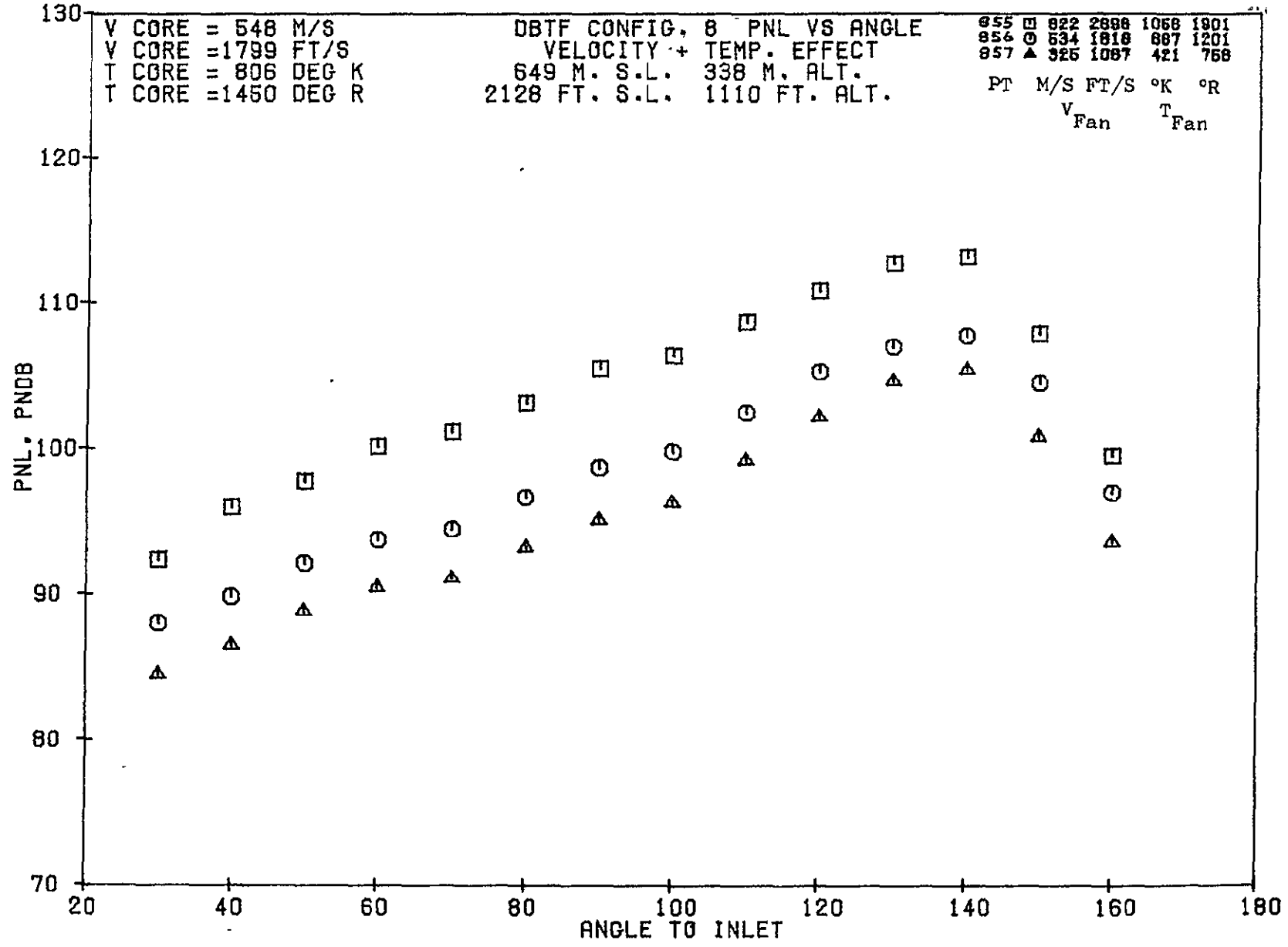
1582

11-539

08/20/75
5R524-001

79 BURCH A.

1583

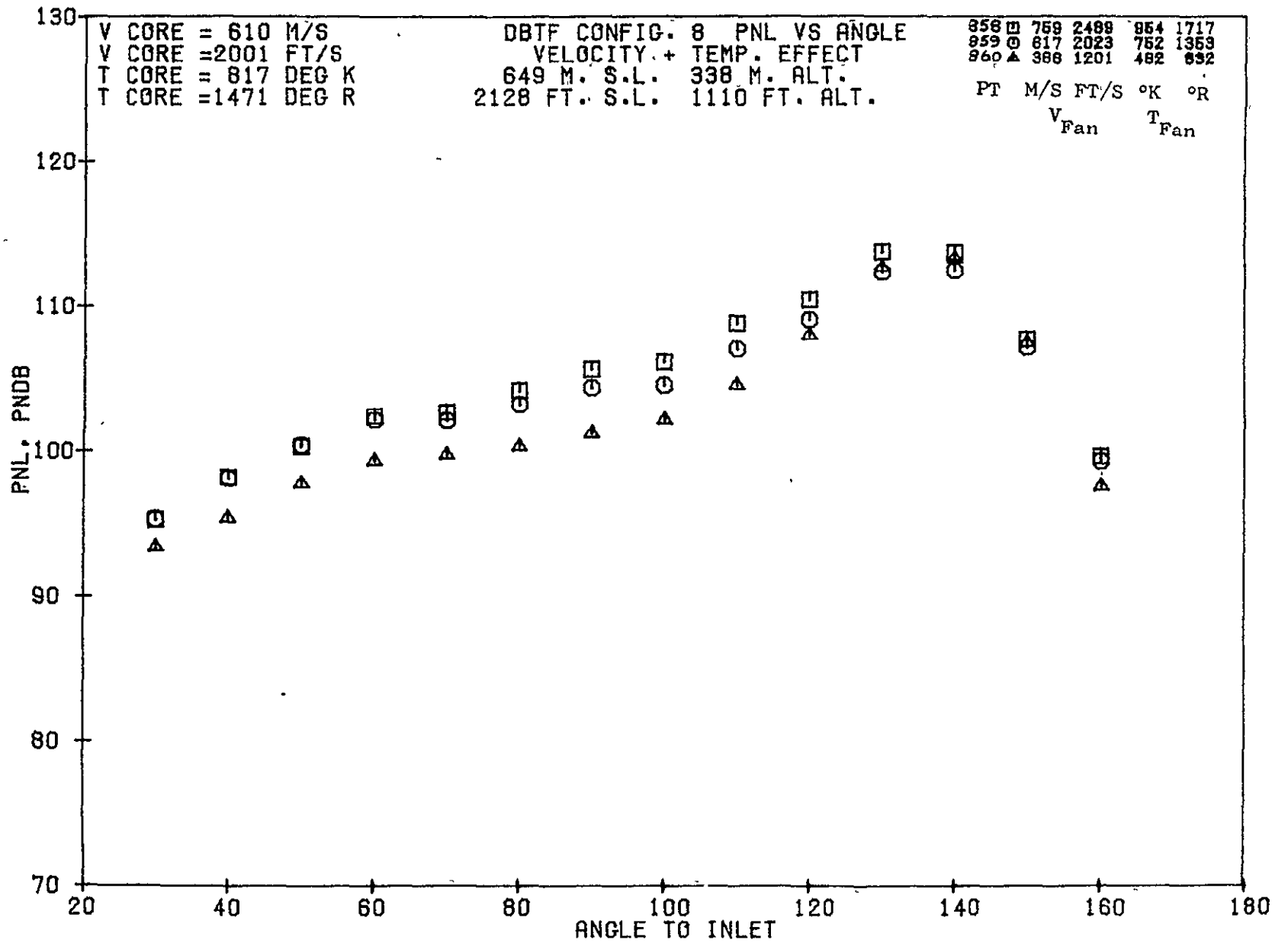


4-27-75

08/20/75
5R524-001

79 BURCH A.

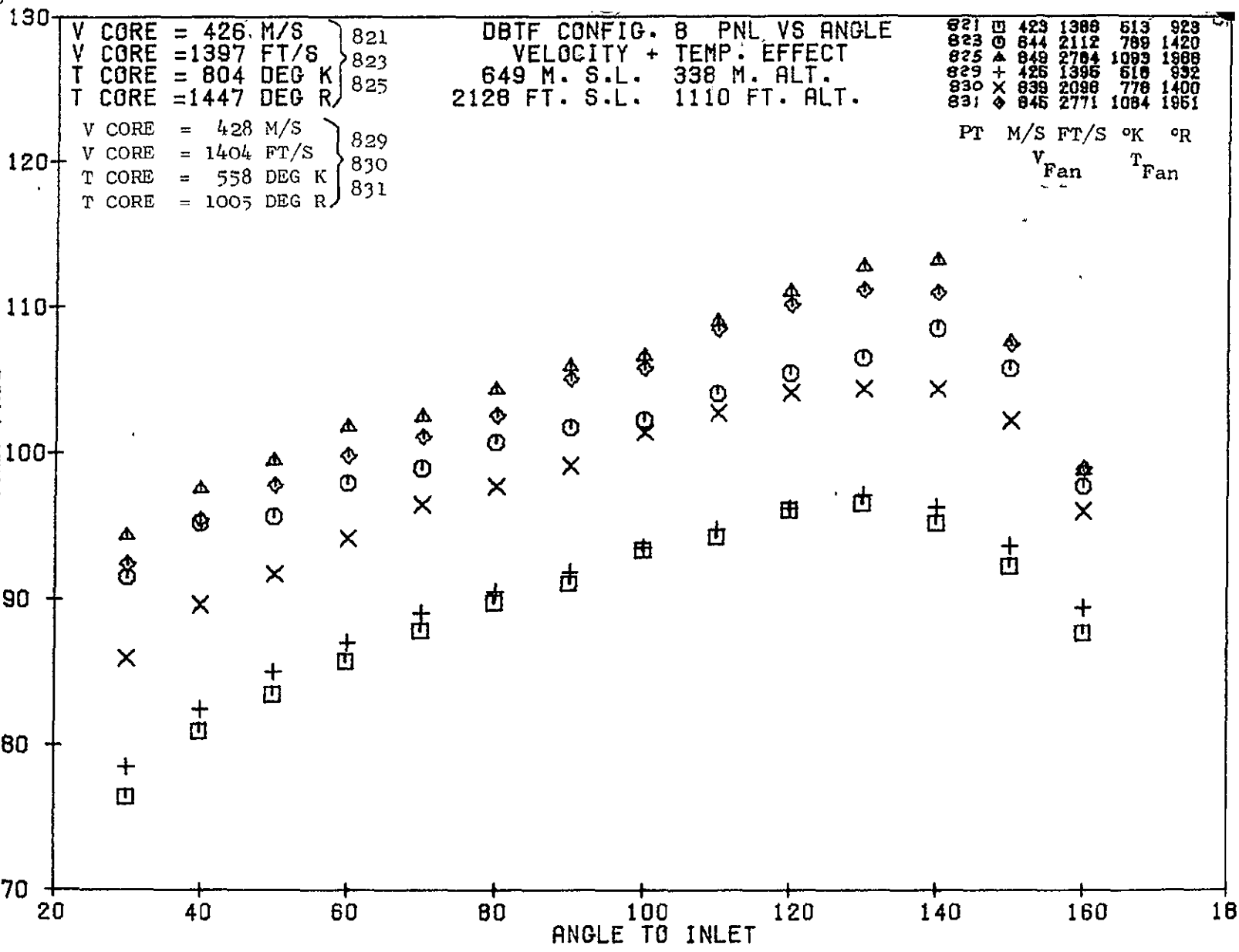
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08/20/75
 5R524-001

79 BURCH A.

1585



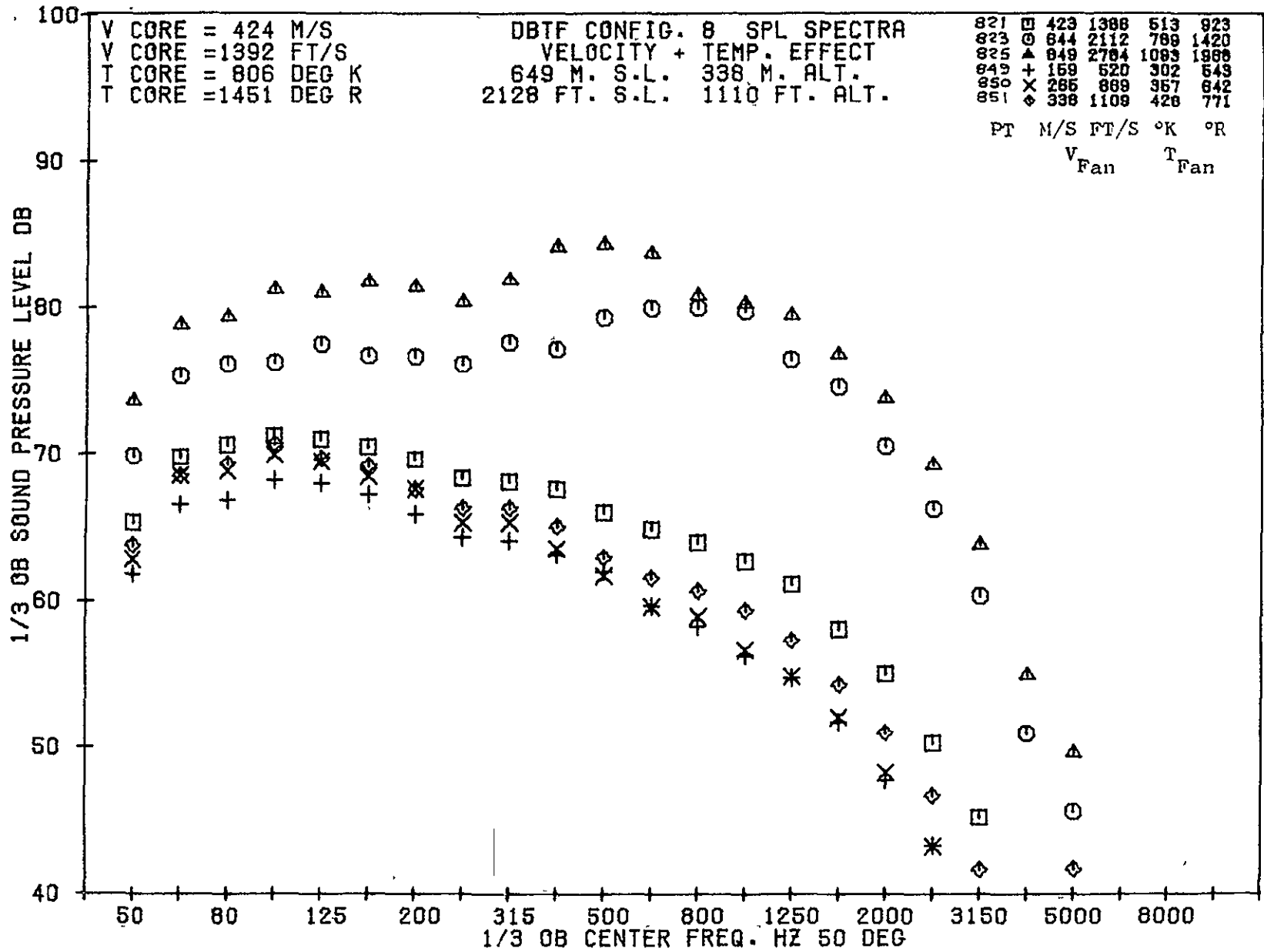
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08/20/75
5R524-001

79 BURCH A.

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1586

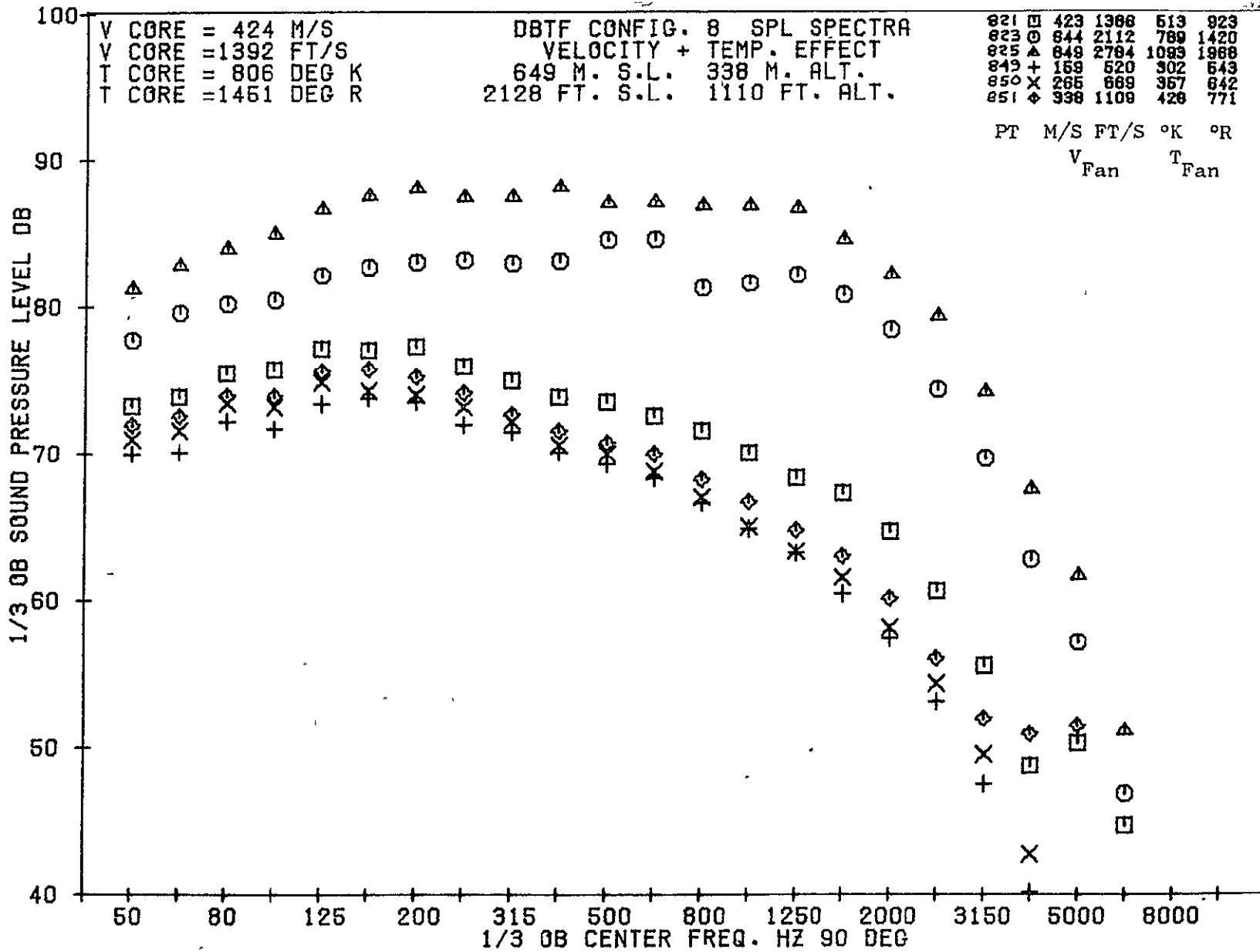


11-343

08/20/75
 5R524-001

79 BURD A.

1587



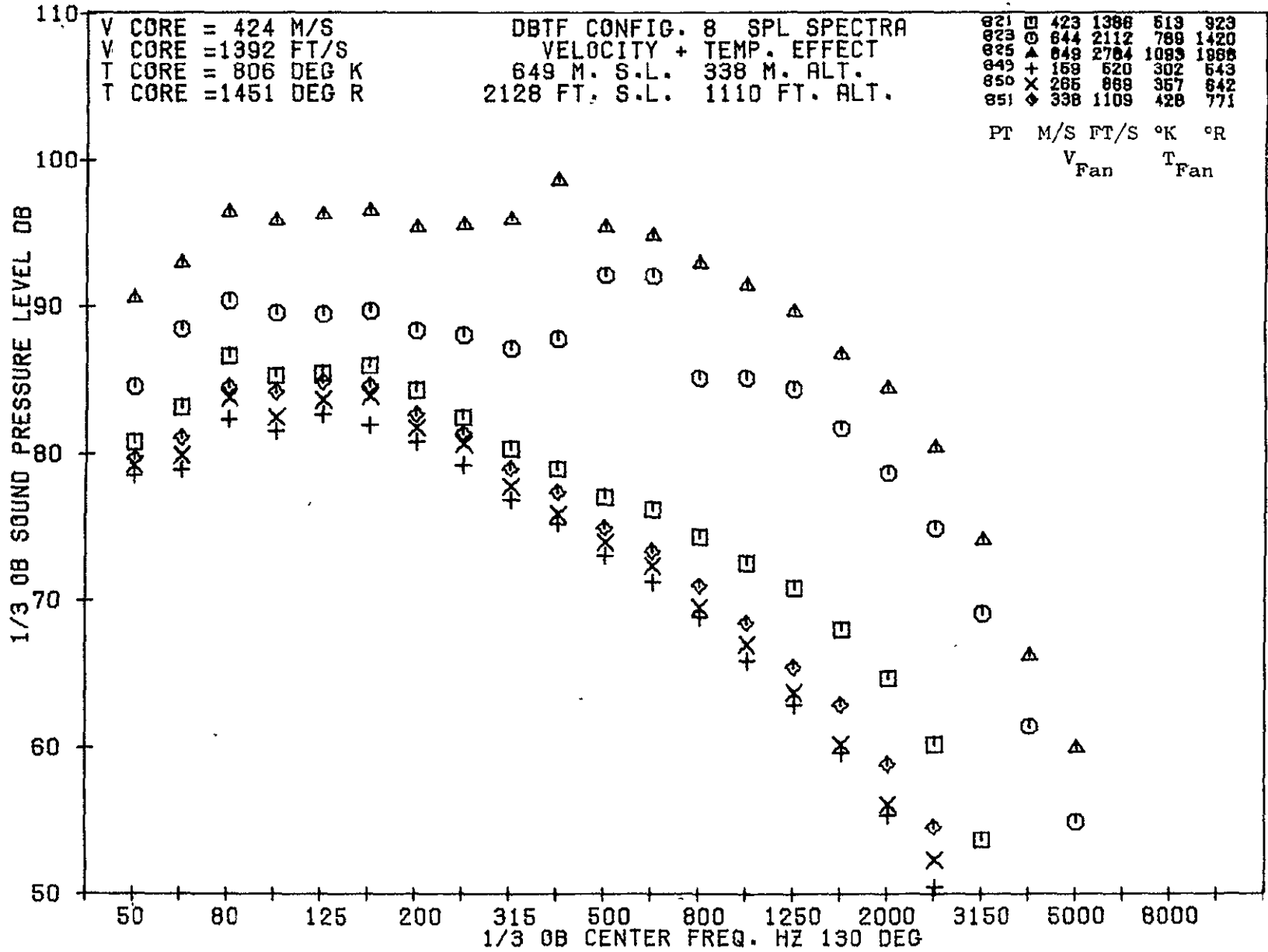
08/20/75
5R524-001

79 BURCH A.

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4-344

1588

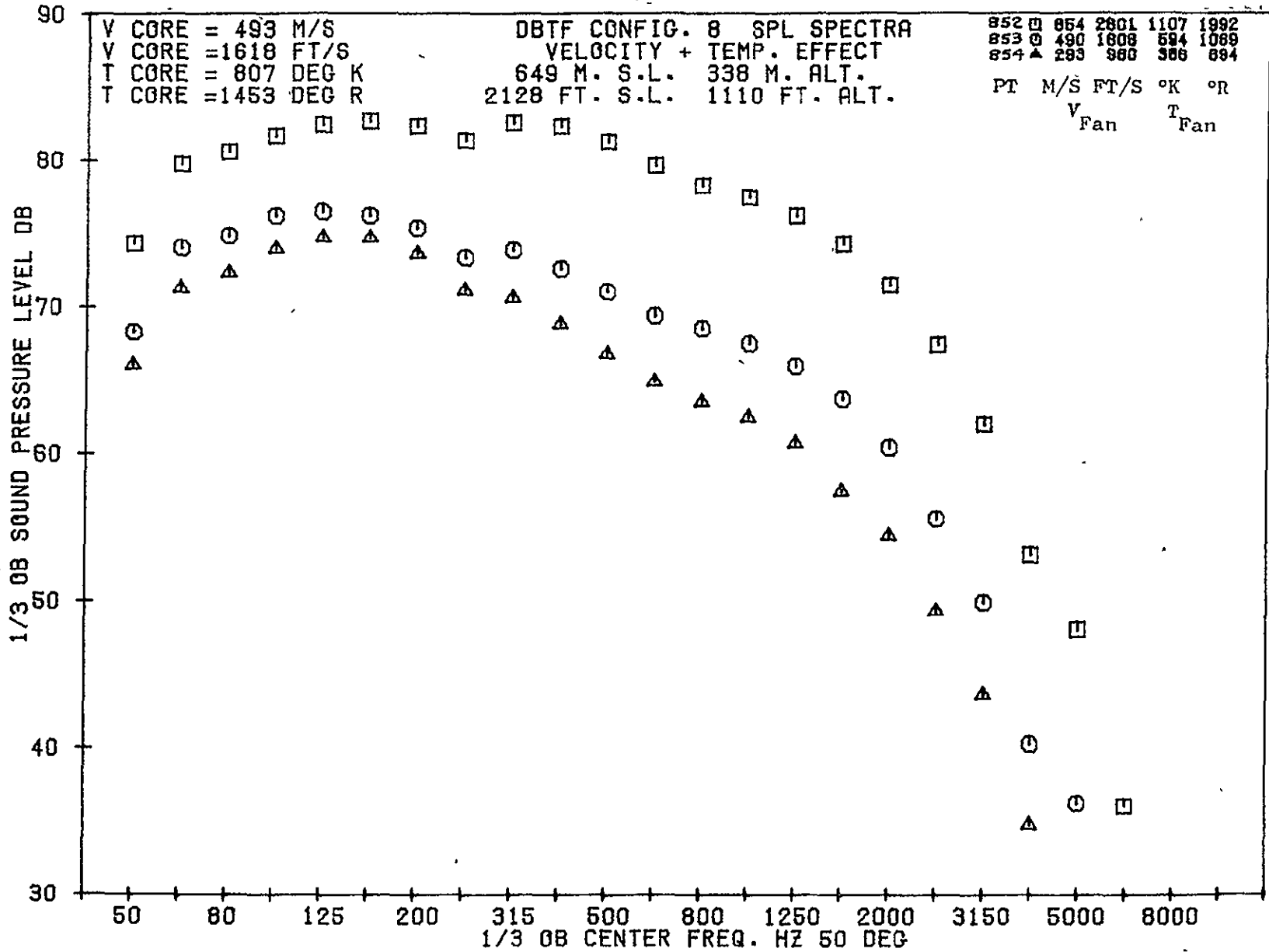


549-71

08/20/75
5R524-001

79 BURCH A.

1589



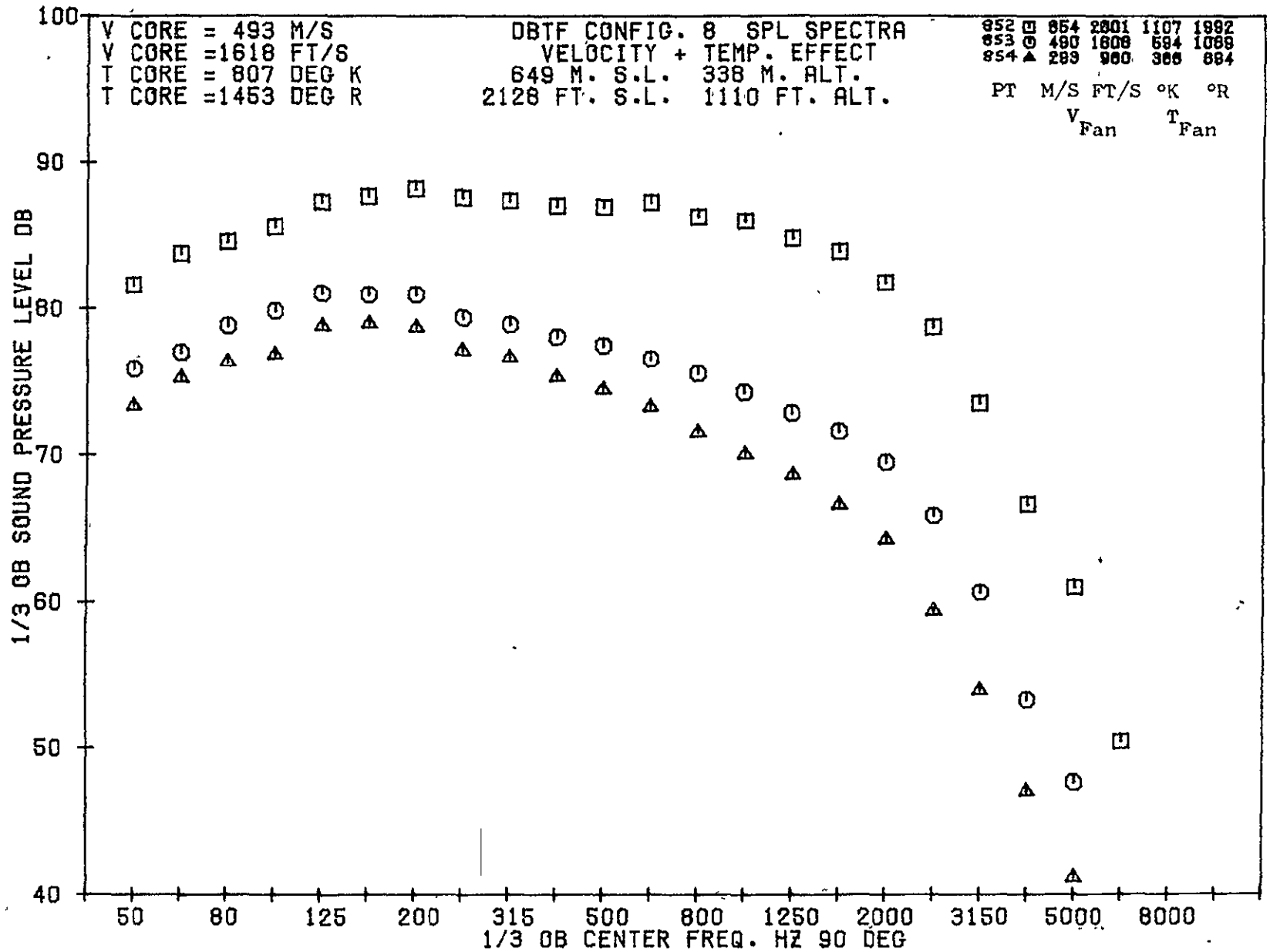
08/20/75
5R524-001

79 BURCH A.

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1.27/6

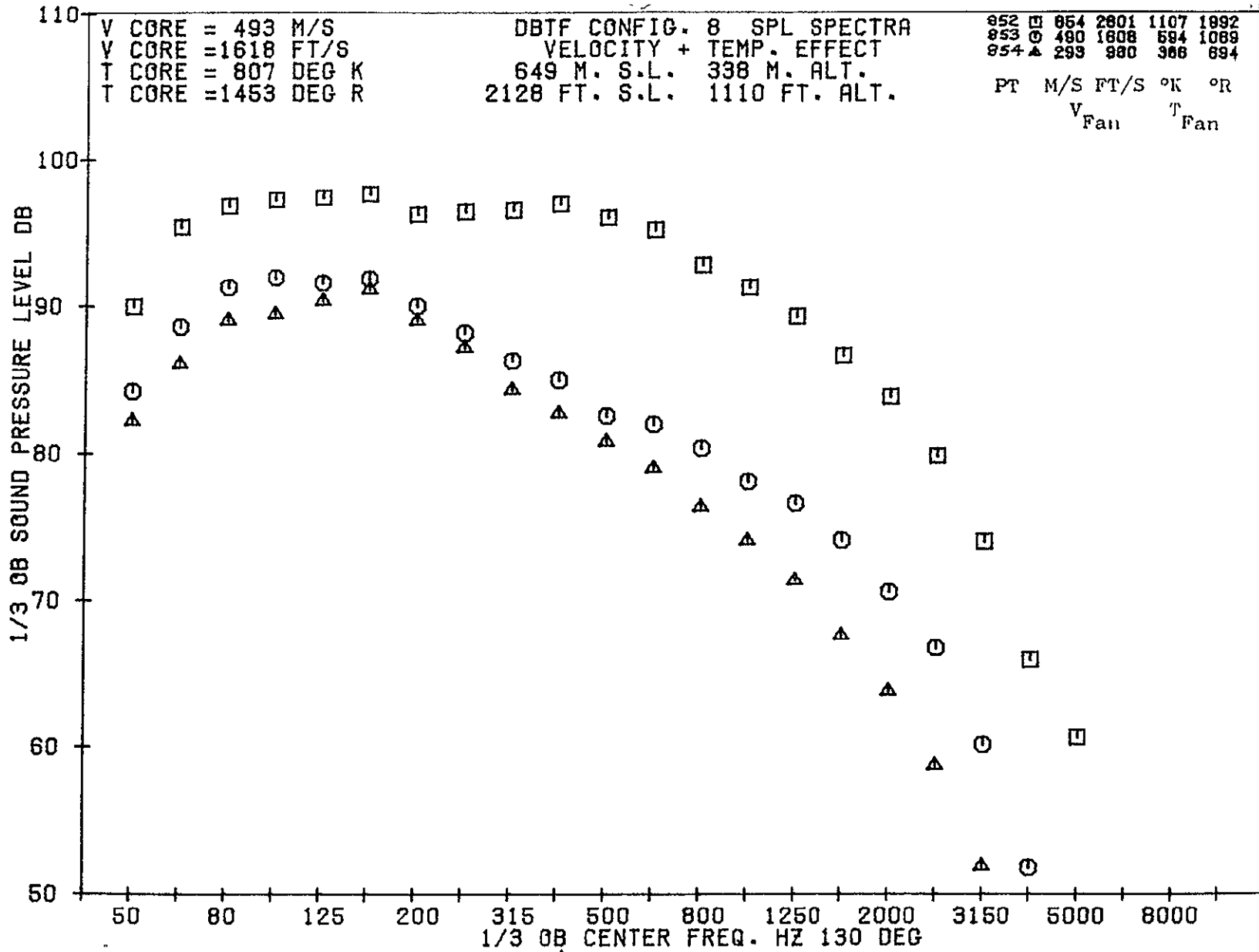
1590



1 pc. 7

08/20/75
5R524-001

79 BUEN R.



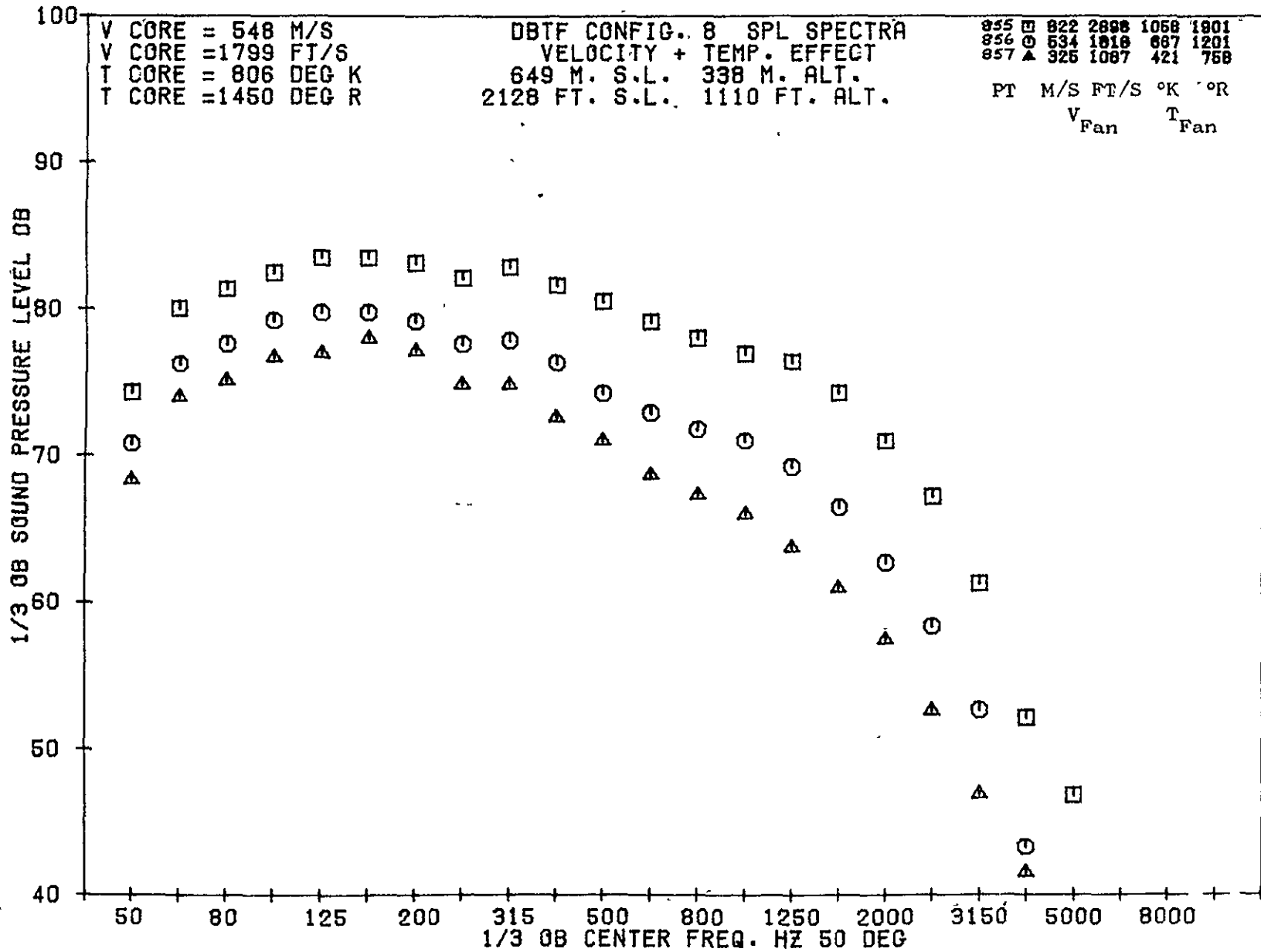
08/20/75
 5R524-001

79 BURCH A.

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U-248

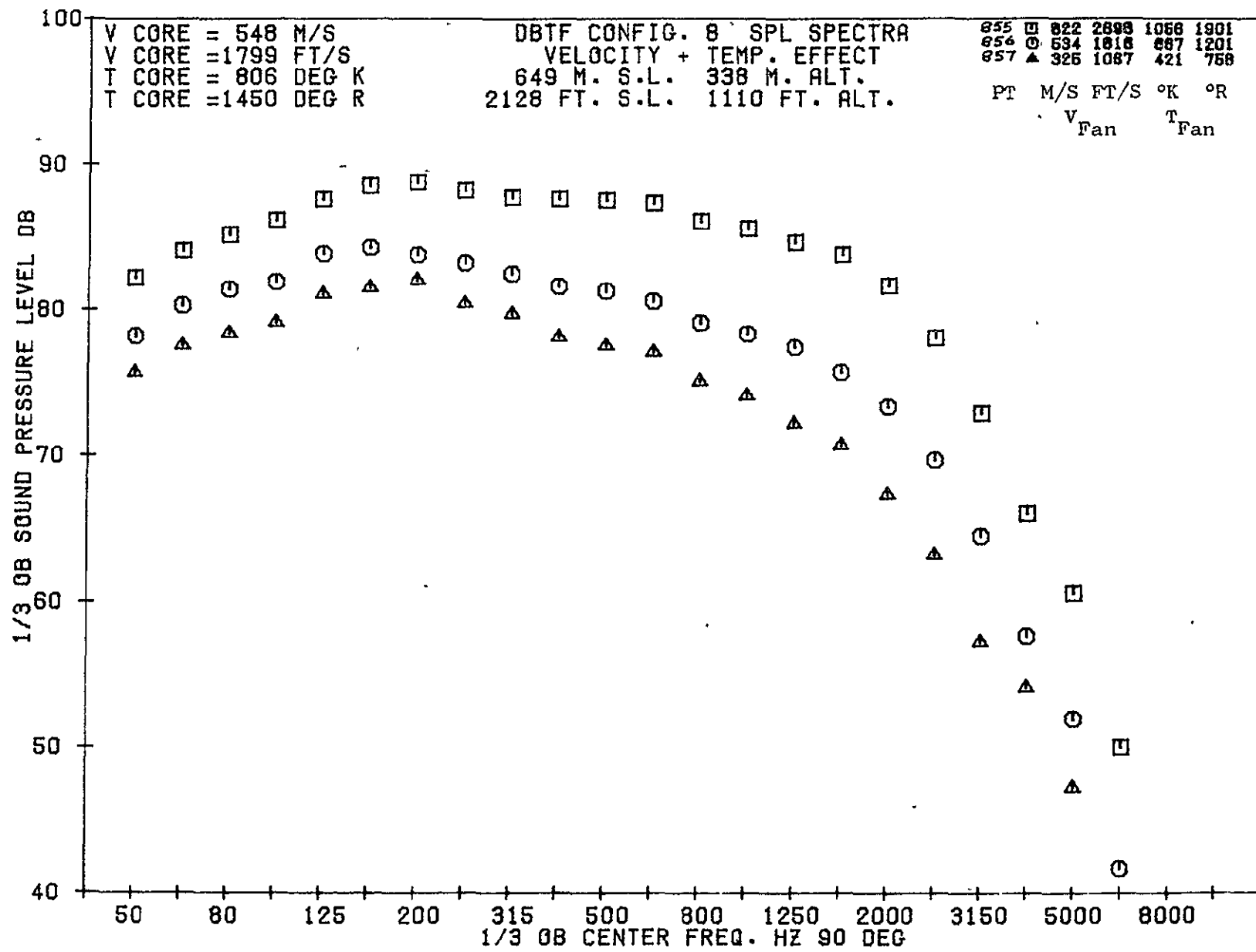
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4-344

08/22/75
FR682-001

79 BURBANK, CA.



1593

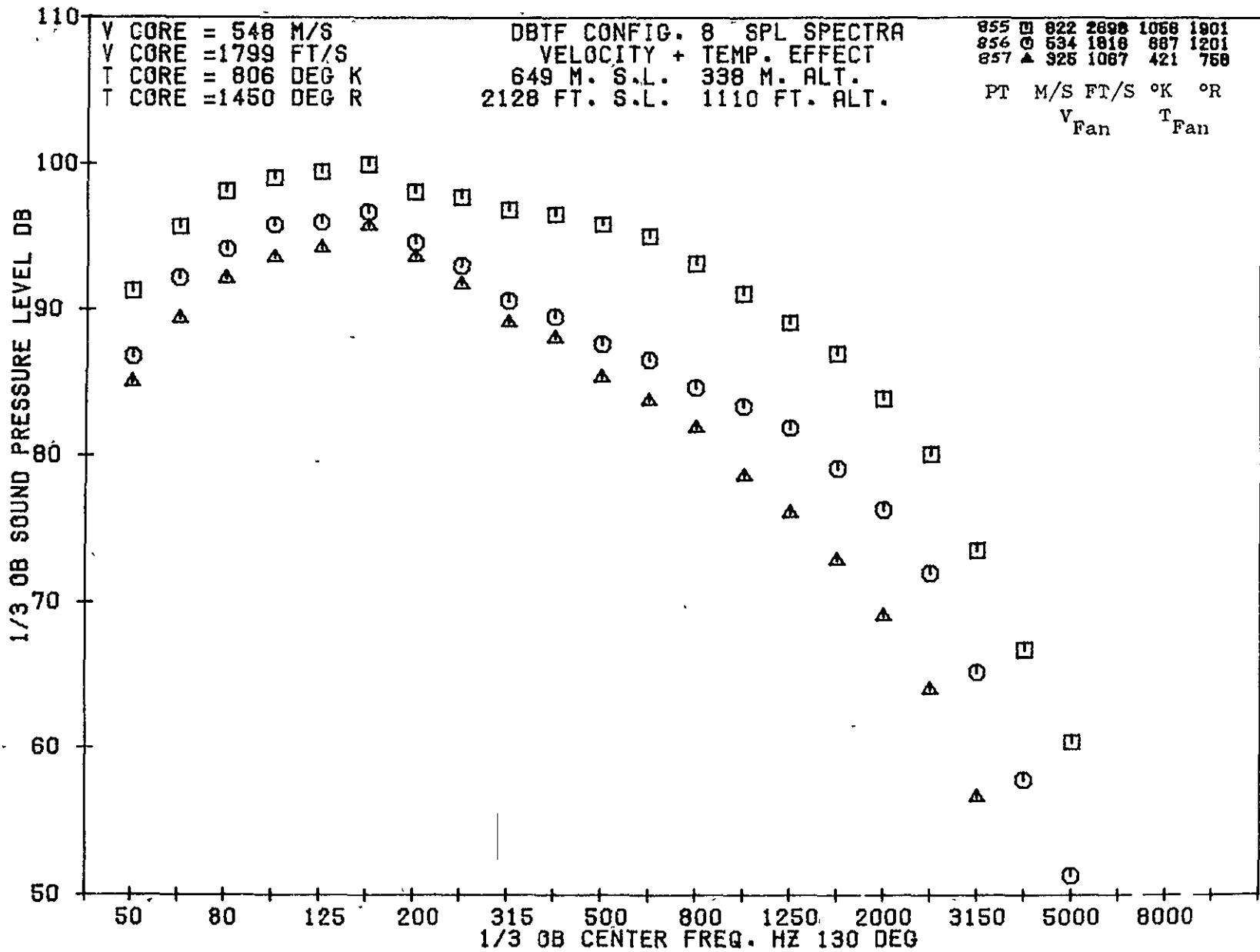
1
250

08/22/75
 5R682-001

79 BURCH A.

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1594

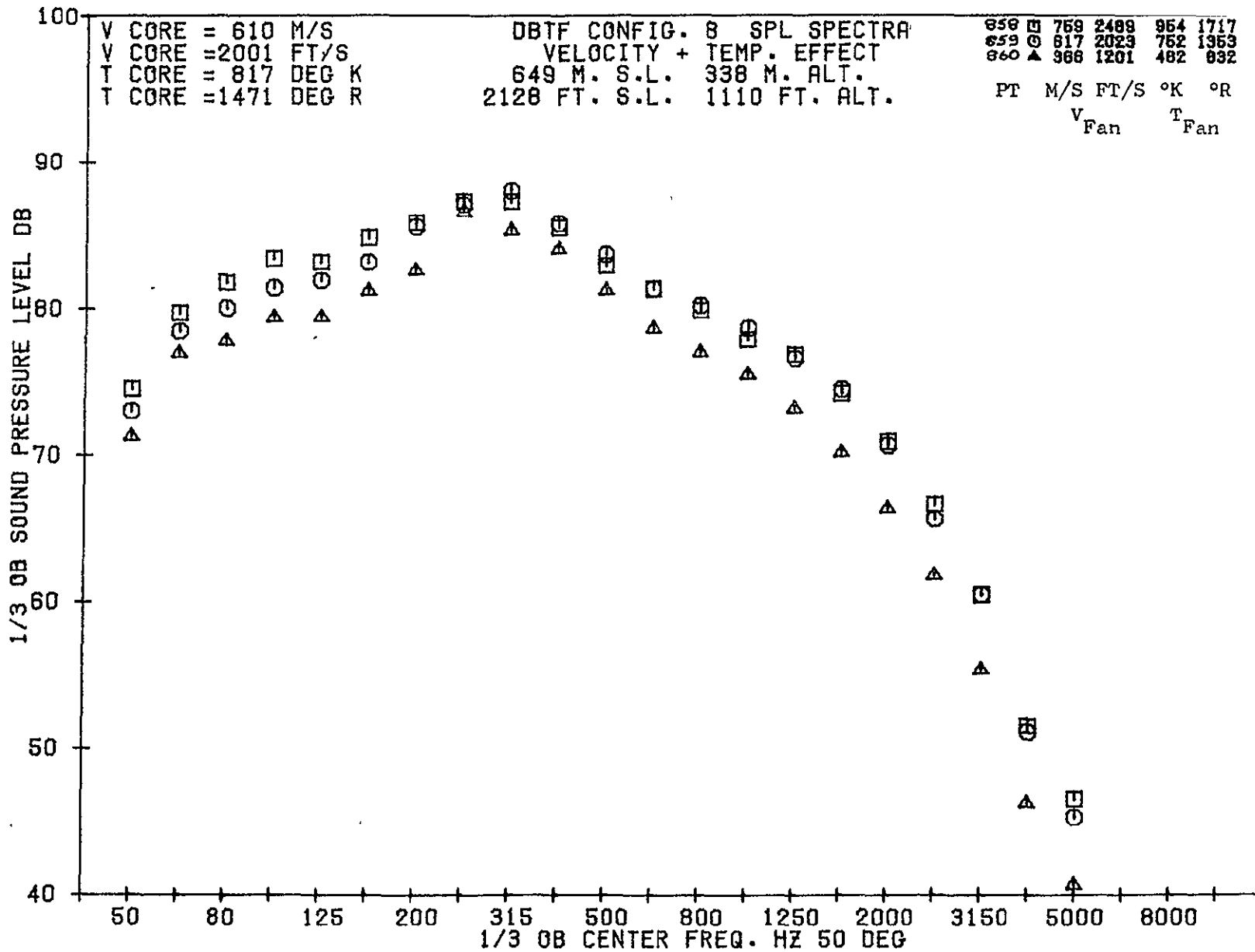


4-351

08/22/75
5R682-001

79 BURCOR

1595



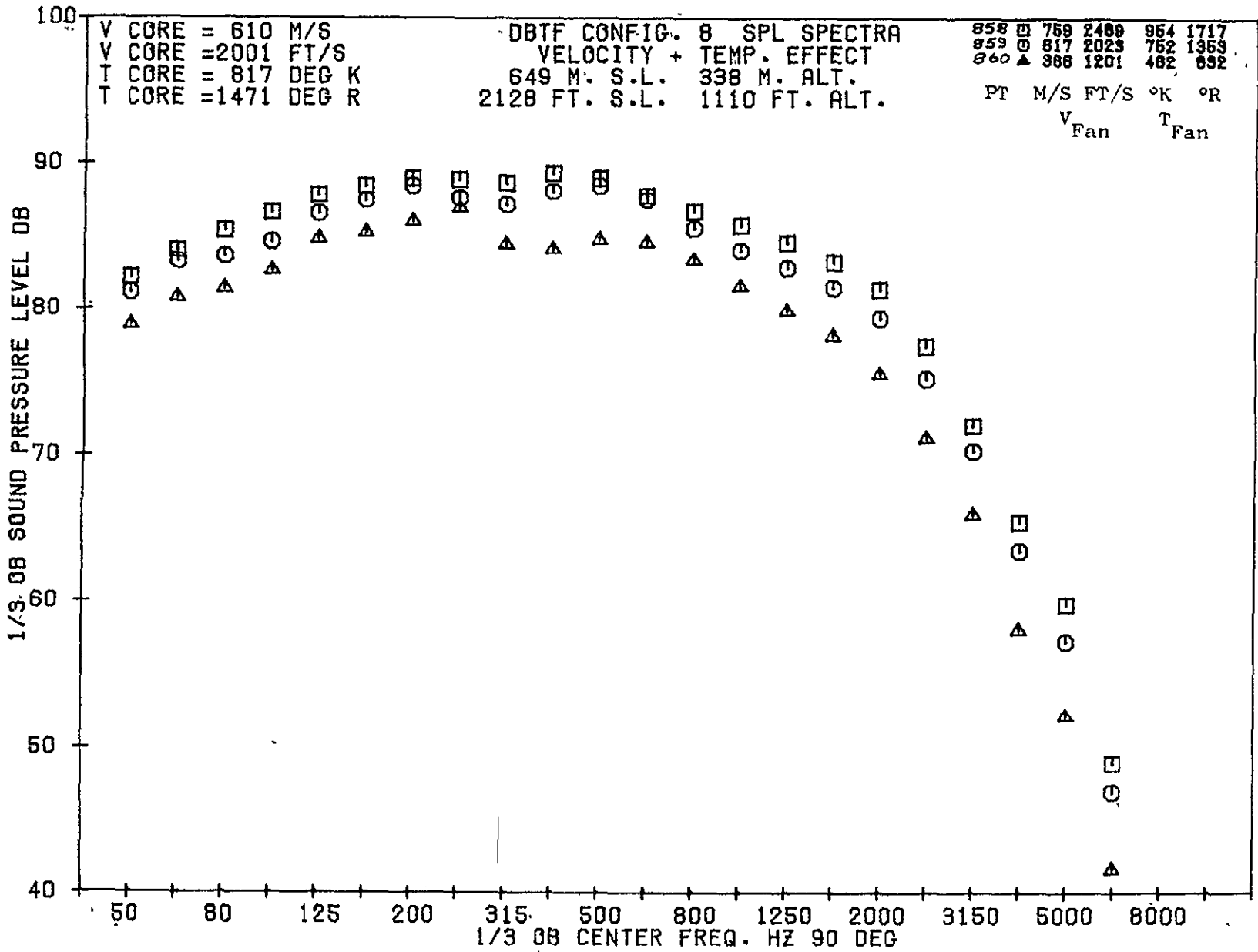
08/20/75
5R524-001

79 BURCH A.

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11-352

1596

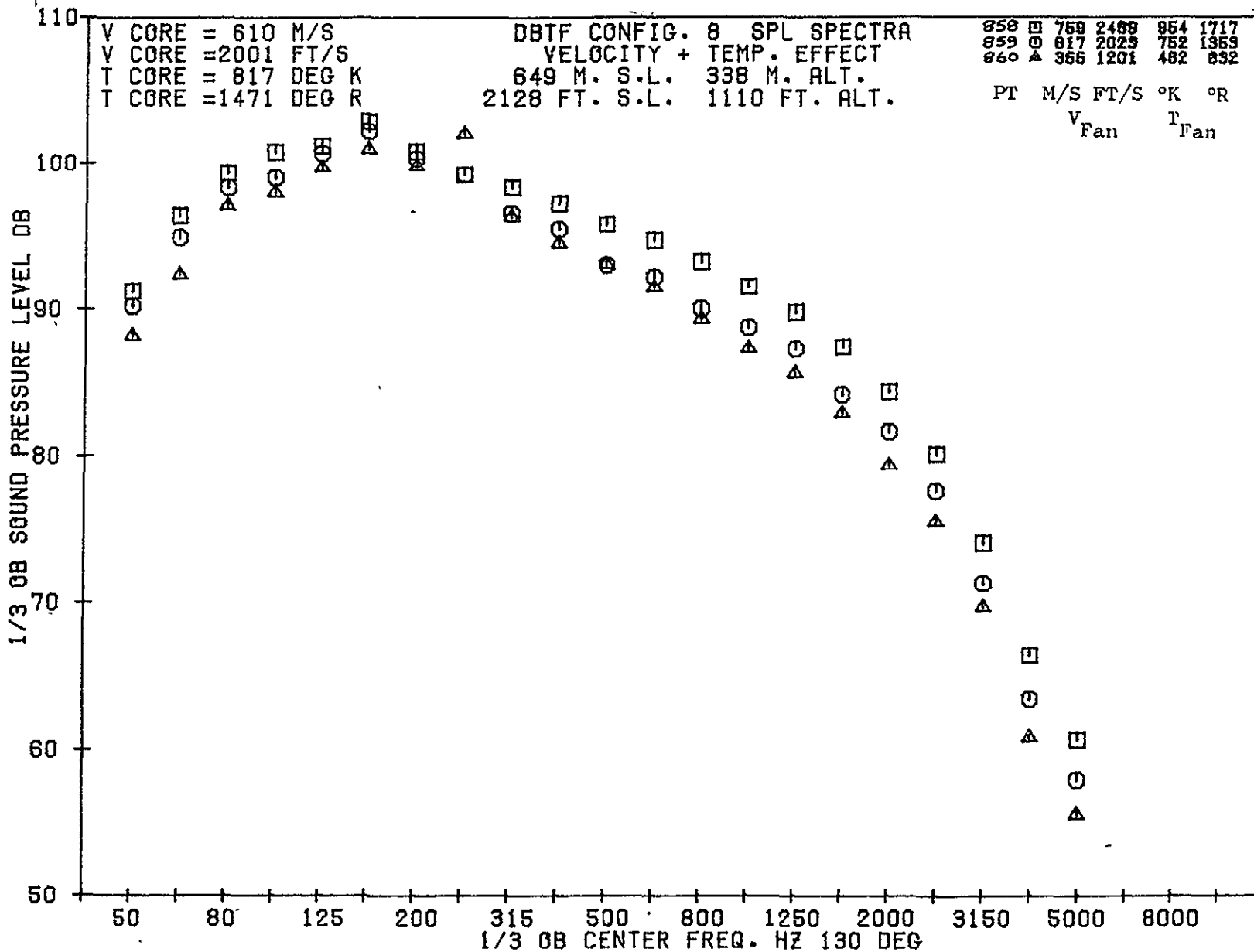


4-253

08/20/75
5R524-001

79 BURCOR

1597

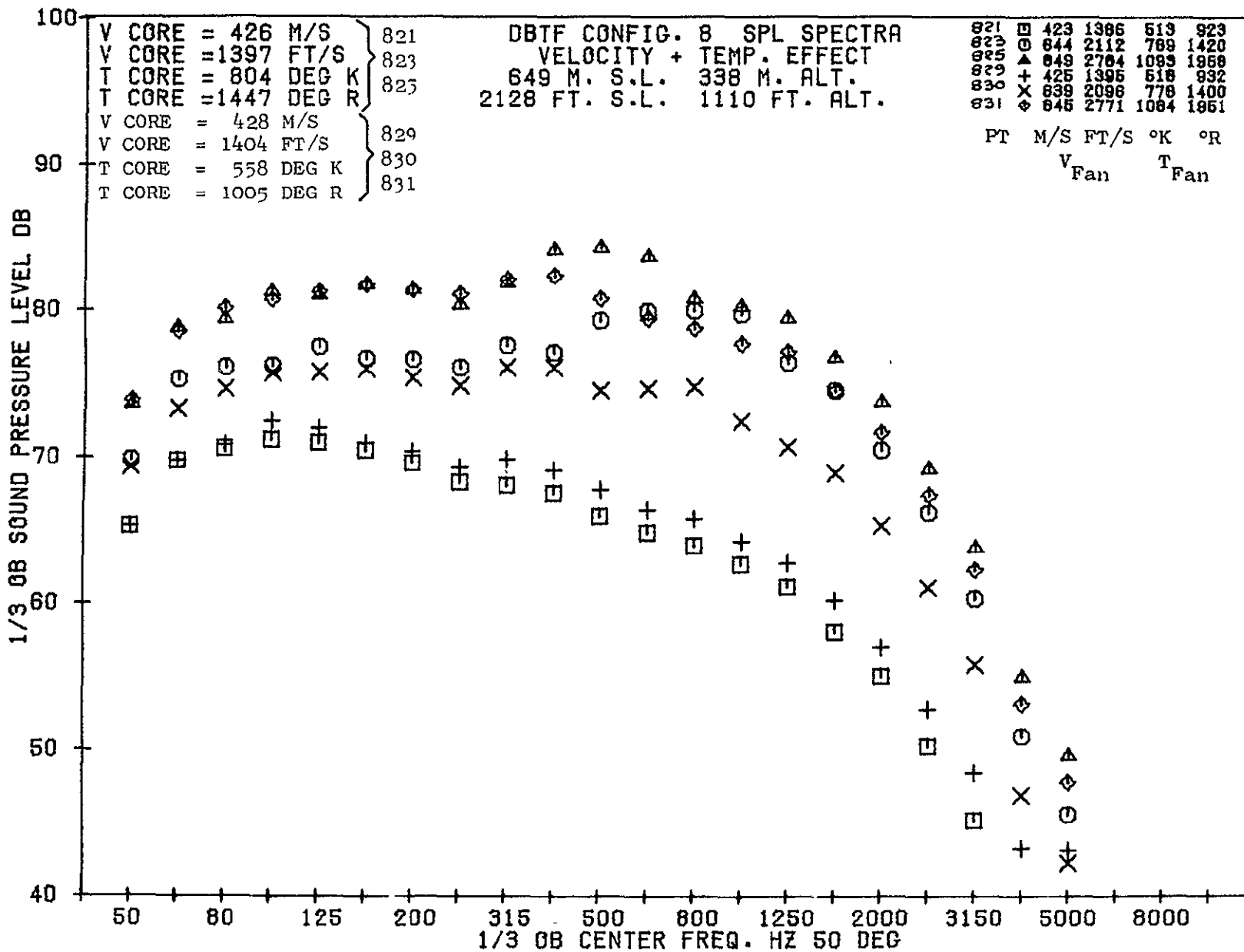


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5R524-001

79 BURCH A.

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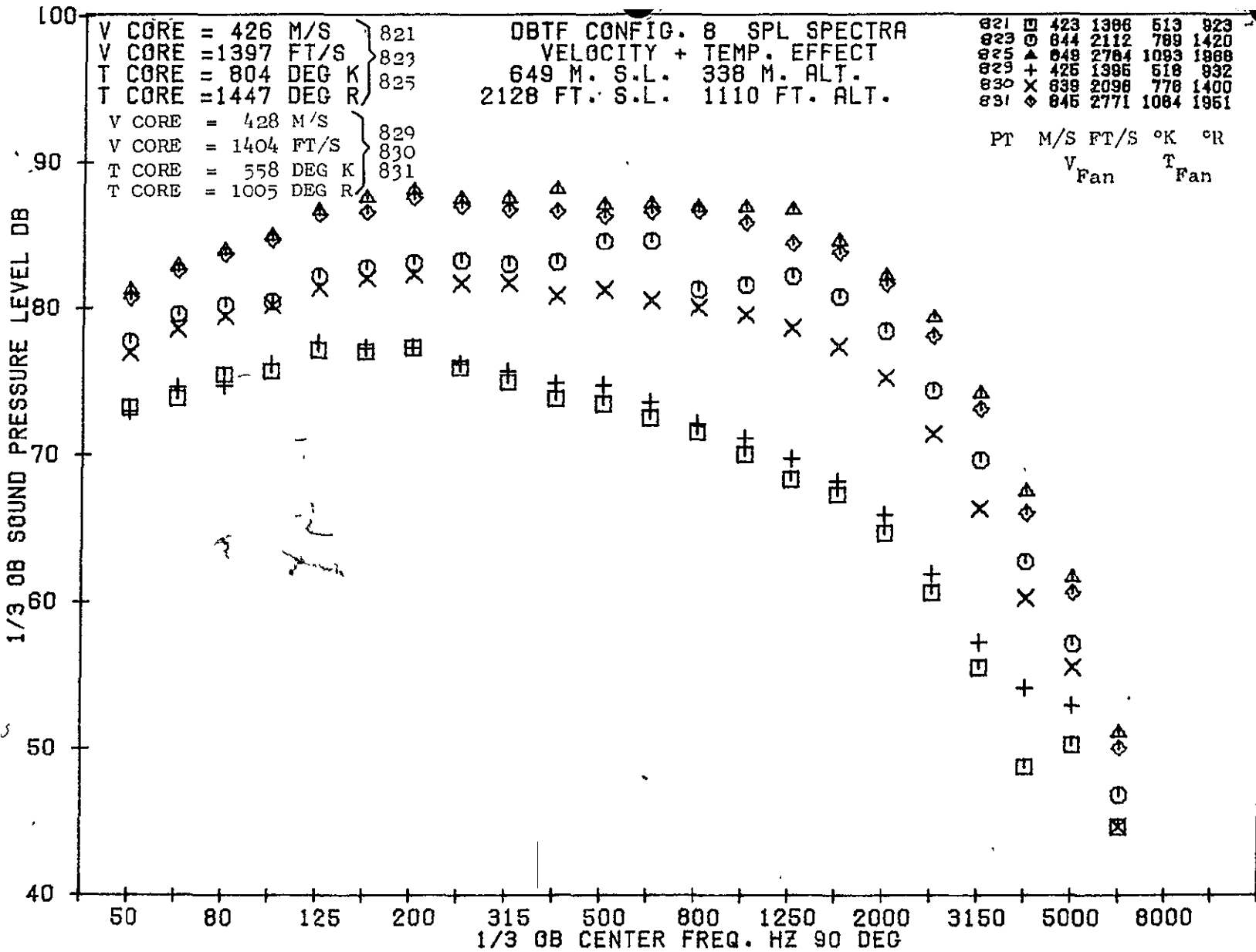
1598



17

08/20/75
 5R524-001

79 BURGLA.



1599

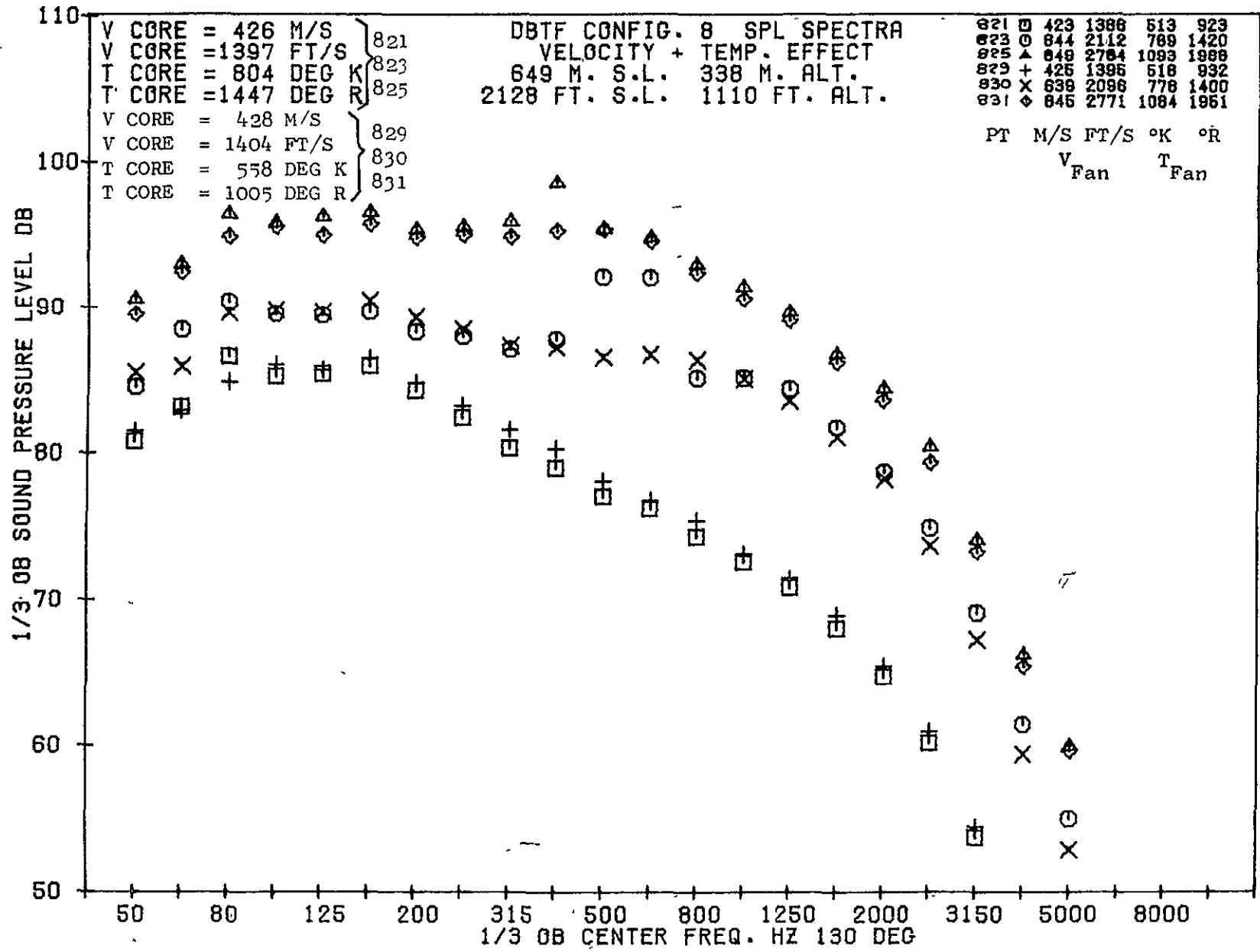
08/20/75
 5R524-001

79 BURCH A.

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956-11

1600

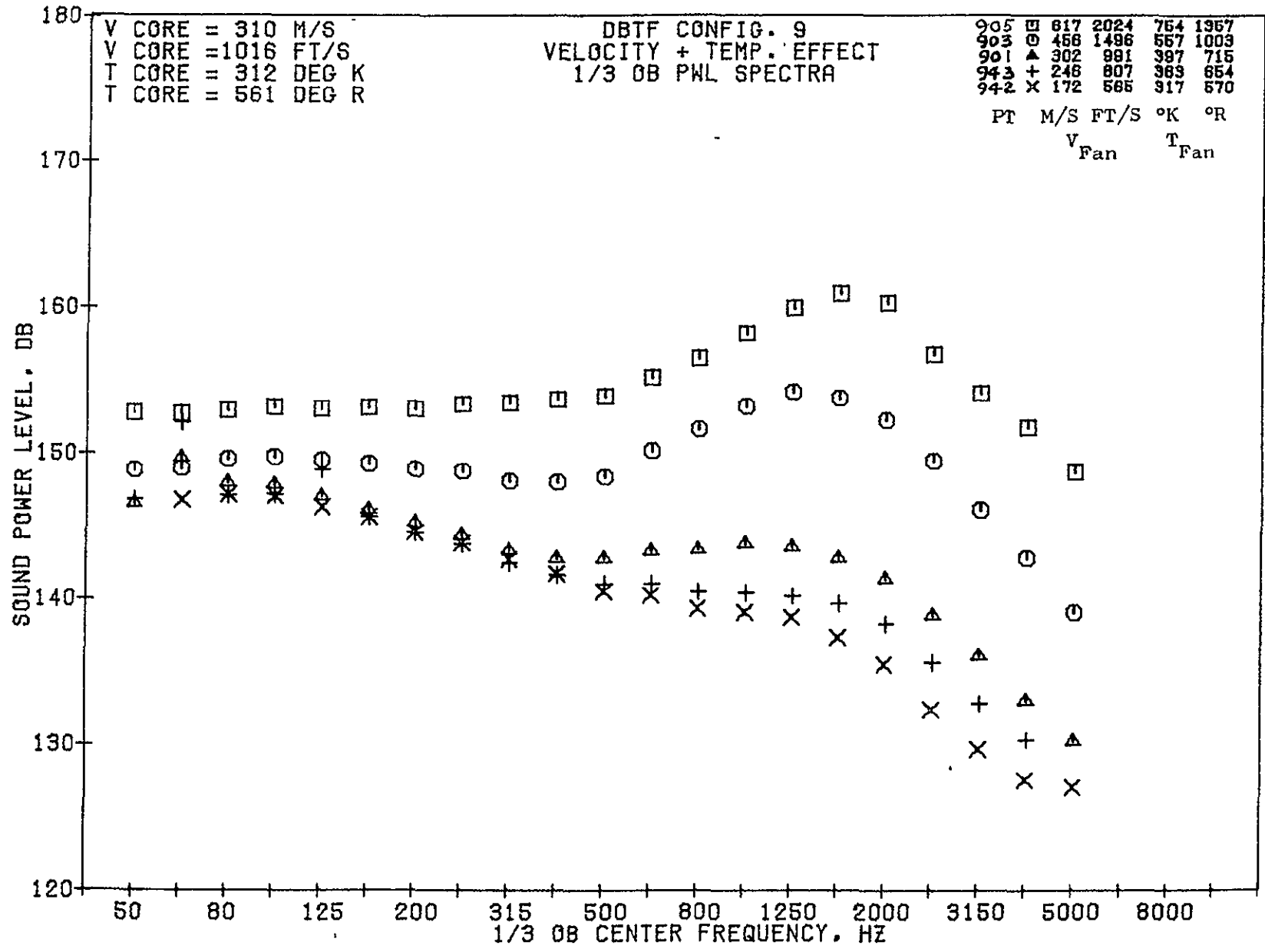


4-156-1

08/20/75
5R524-001

79 BURCH A.

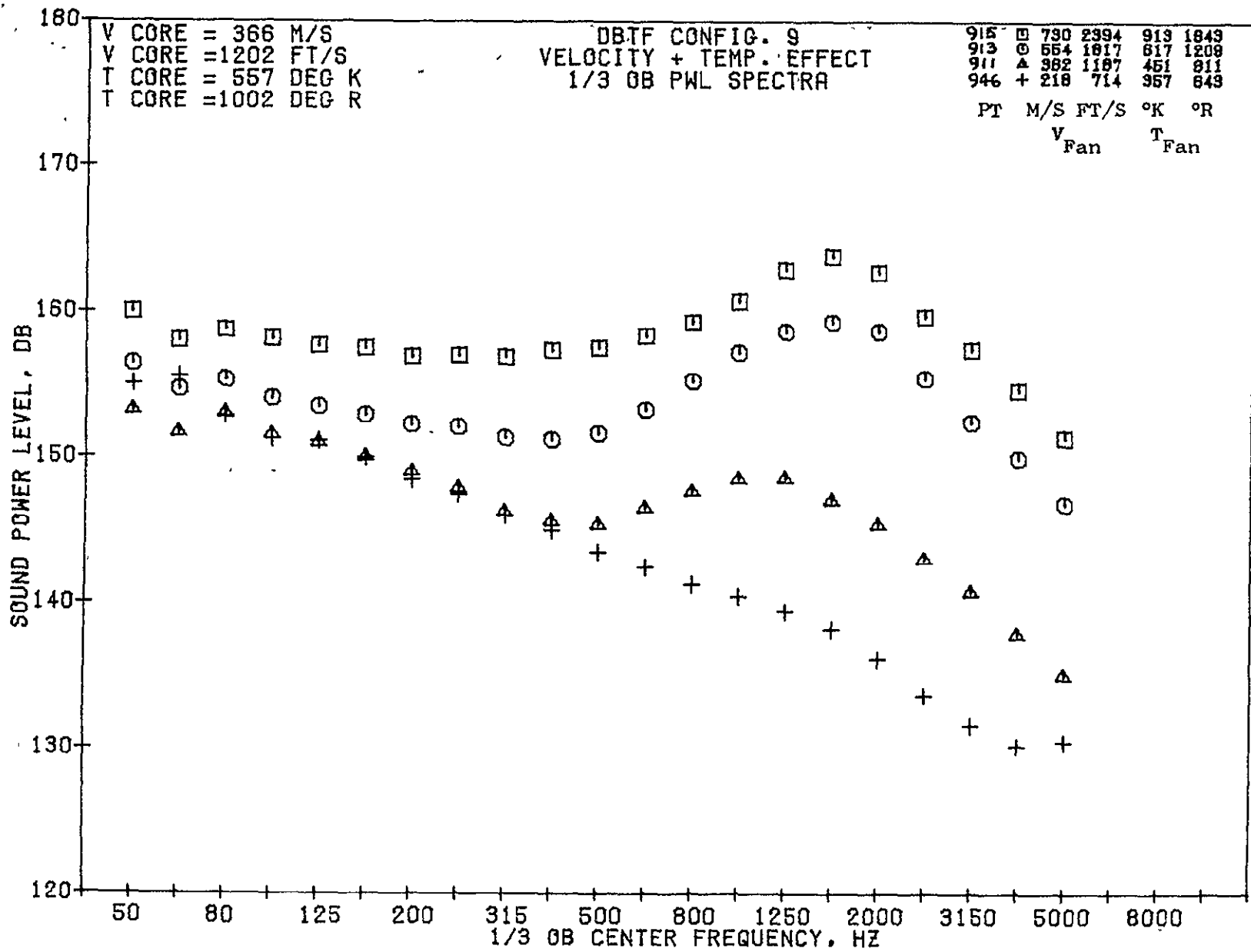
1258



08/18/75
5R266-001

79 BURCH A.

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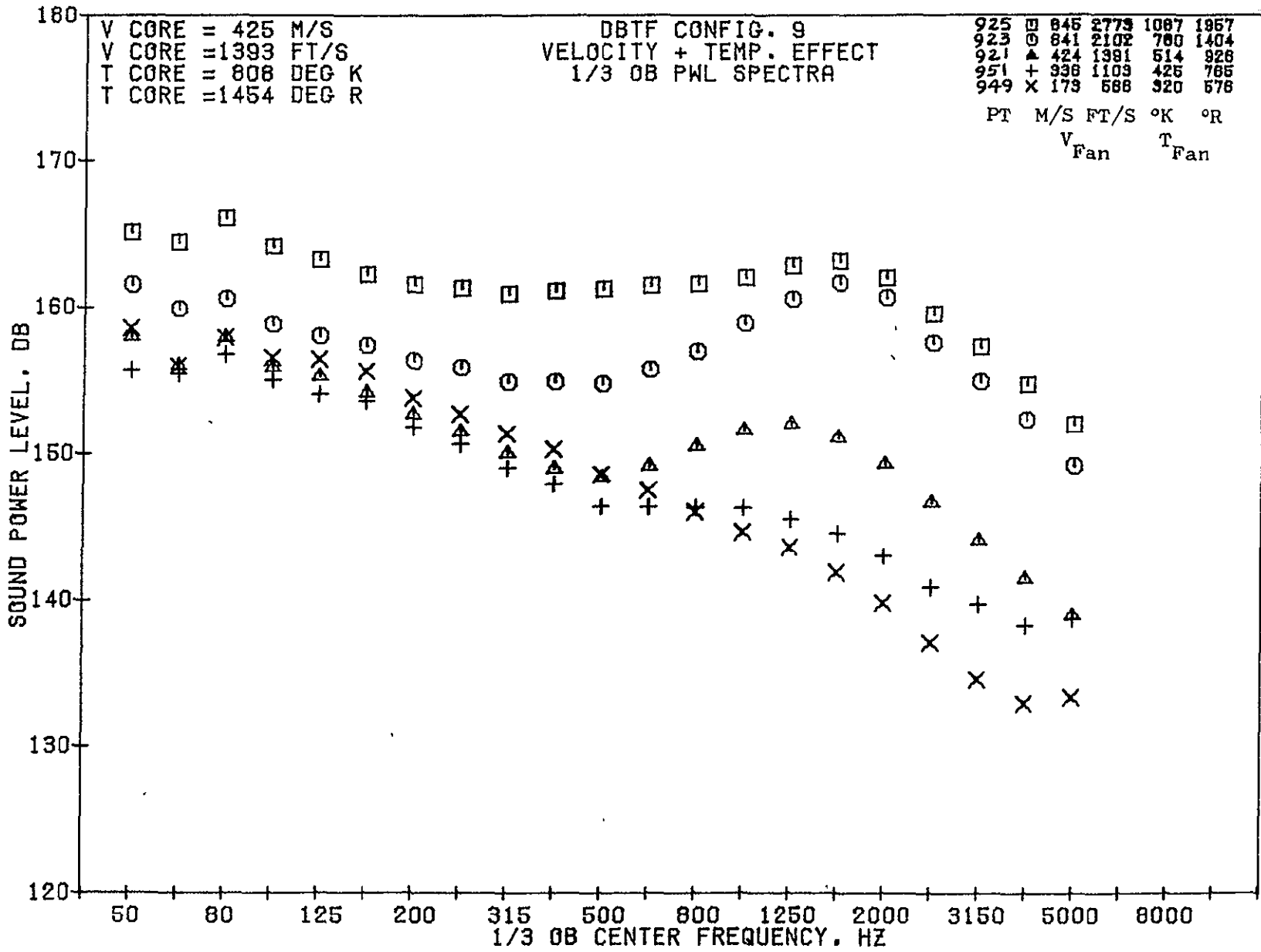
1602

4-35A

08/18/75
5R266-001

79 AIR A.

1603



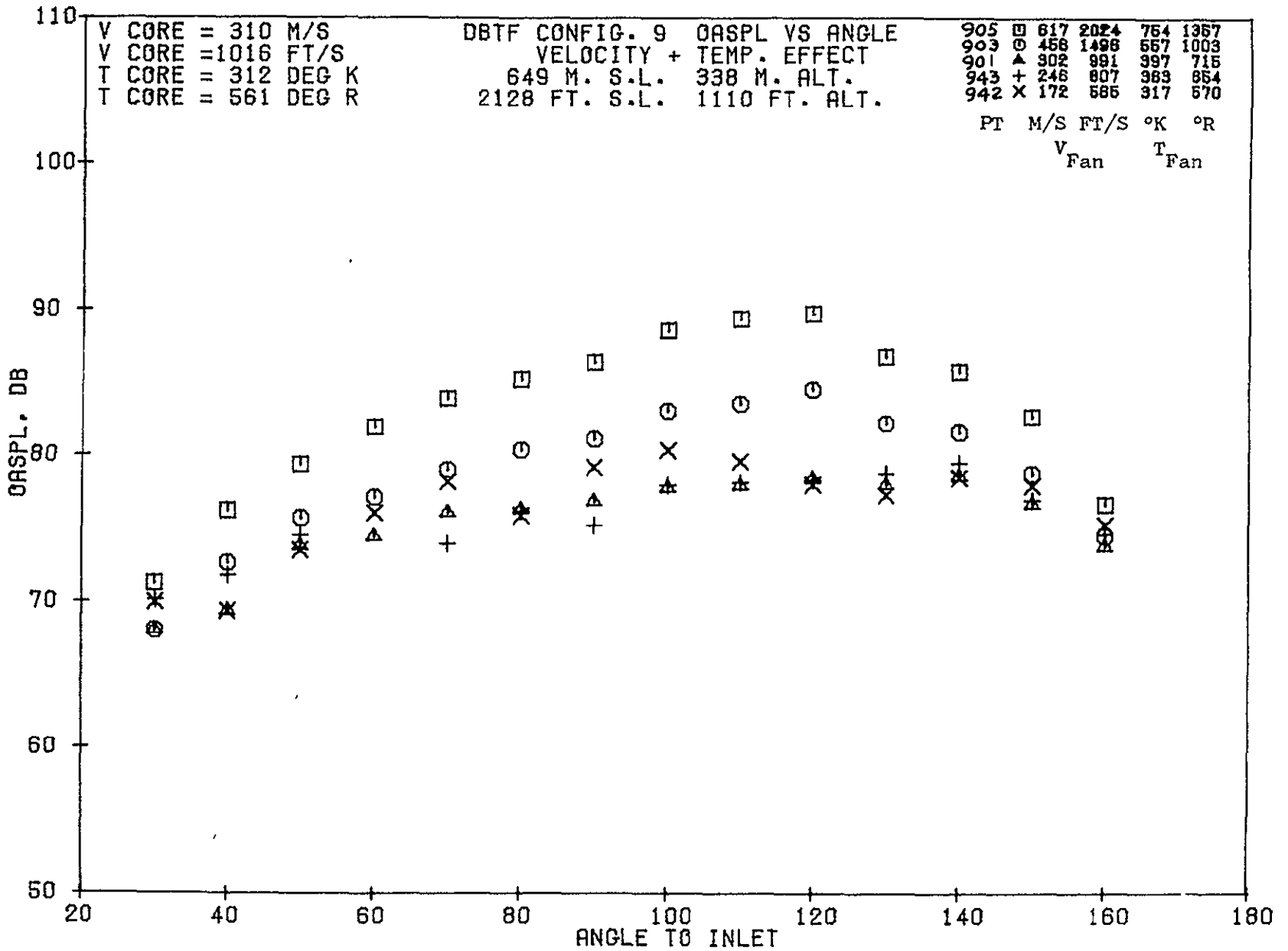
08/18/75
5R266-001

79 BURCH A.

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1 360

1604

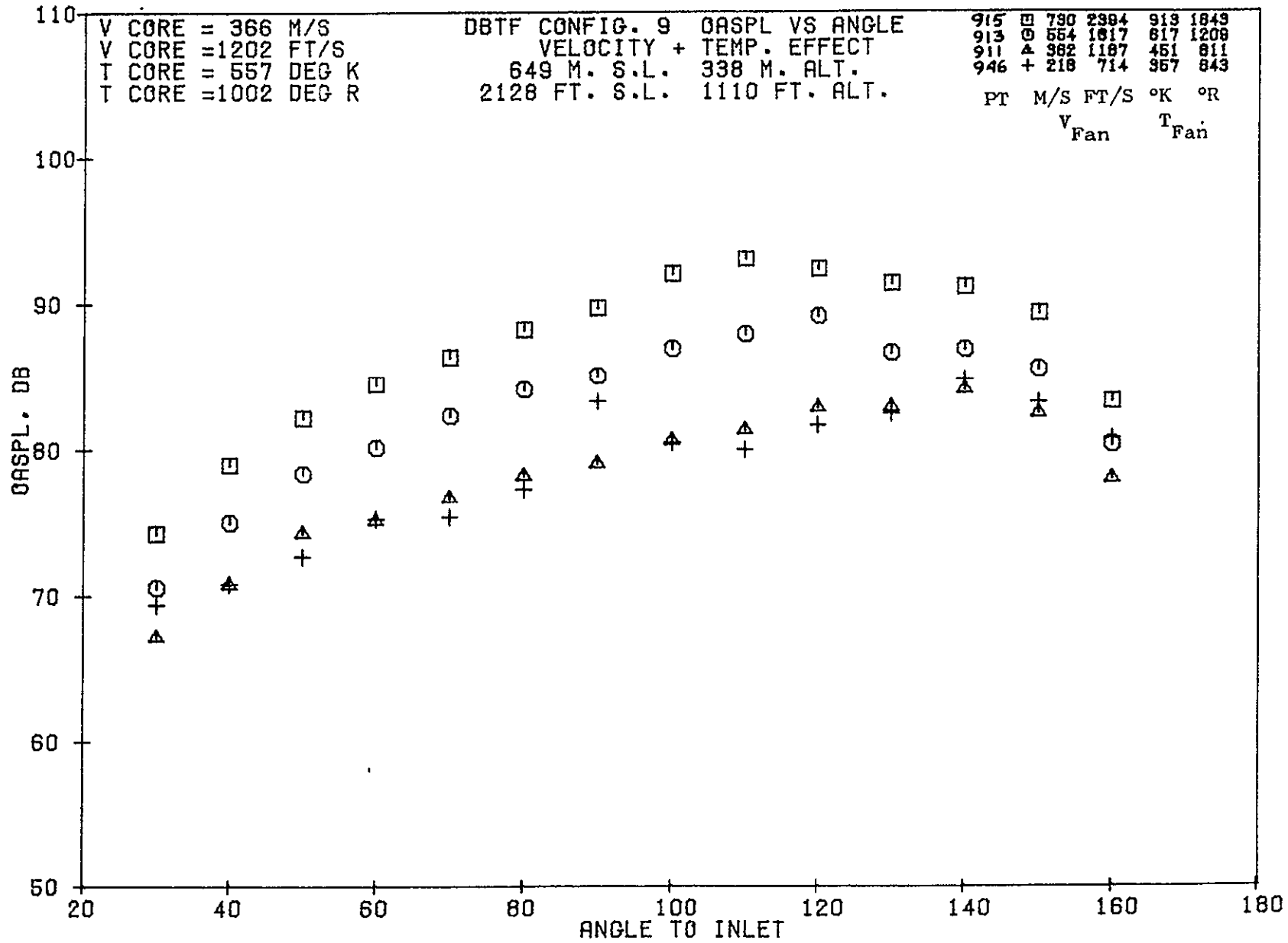


196-1

08/18/75
5R266-001

79 AIRR A.

1605



08/18/75
5R266-001

79 BURCH A.

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110

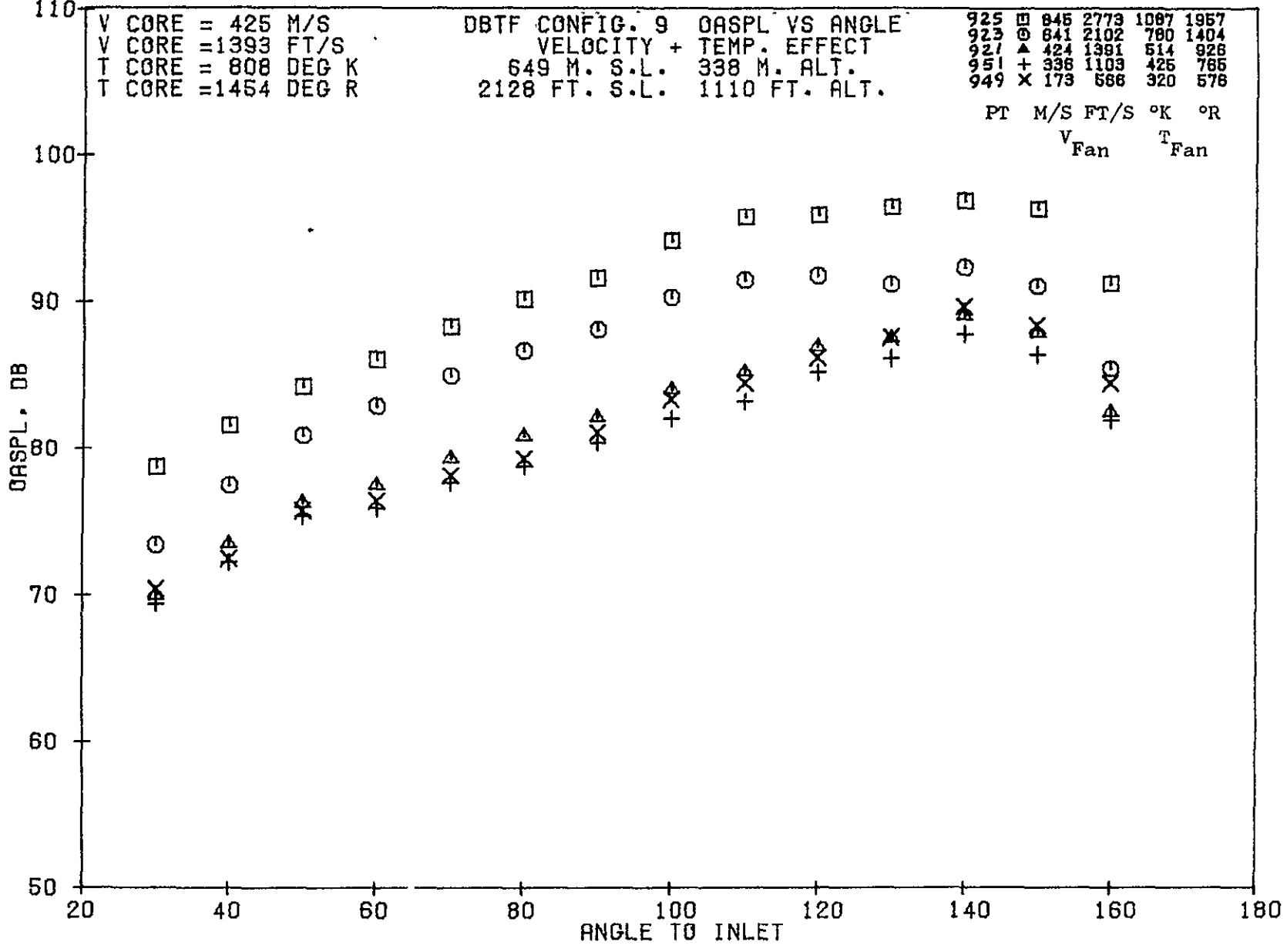
V CORE = 425 M/S
V CORE = 1393 FT/S
T CORE = 808 DEG K
T CORE = 1454 DEG R

DBTF CONFIG. 9 OASPL VS ANGLE
VELOCITY + TEMP. EFFECT
649 M. S.L. 338 M. ALT.
2128 FT. S.L. 1110 FT. ALT.

925	□	845	2773	1087	1957
923	○	841	2102	780	1404
927	△	424	1381	514	928
951	+	338	1103	425	785
949	x	173	588	320	576

PT M/S FT/S °K °R
V Fan T Fan

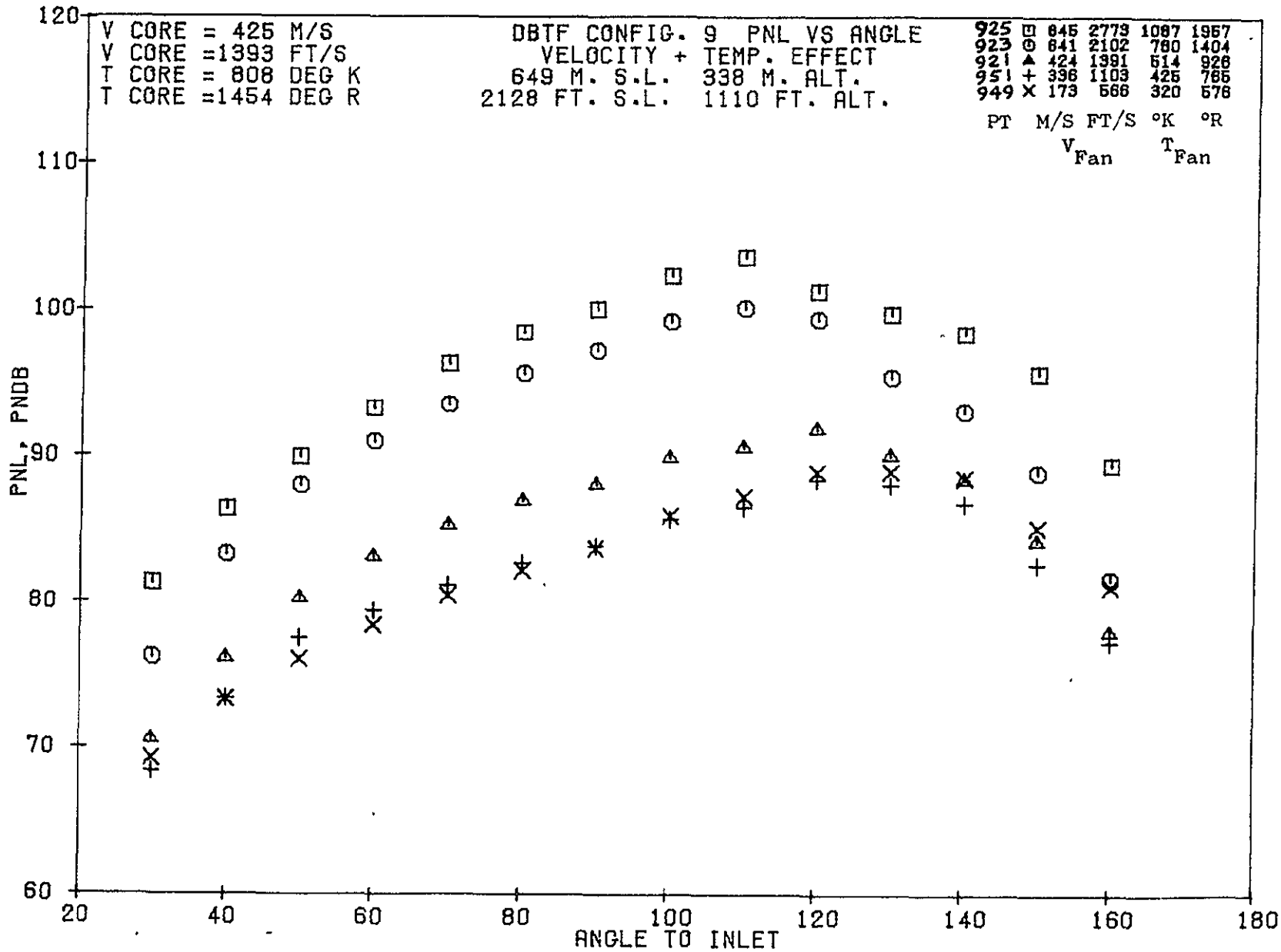
9091
OASPL. DB
1606



1606

08/18/75
5R266-001

79 BUR



1607

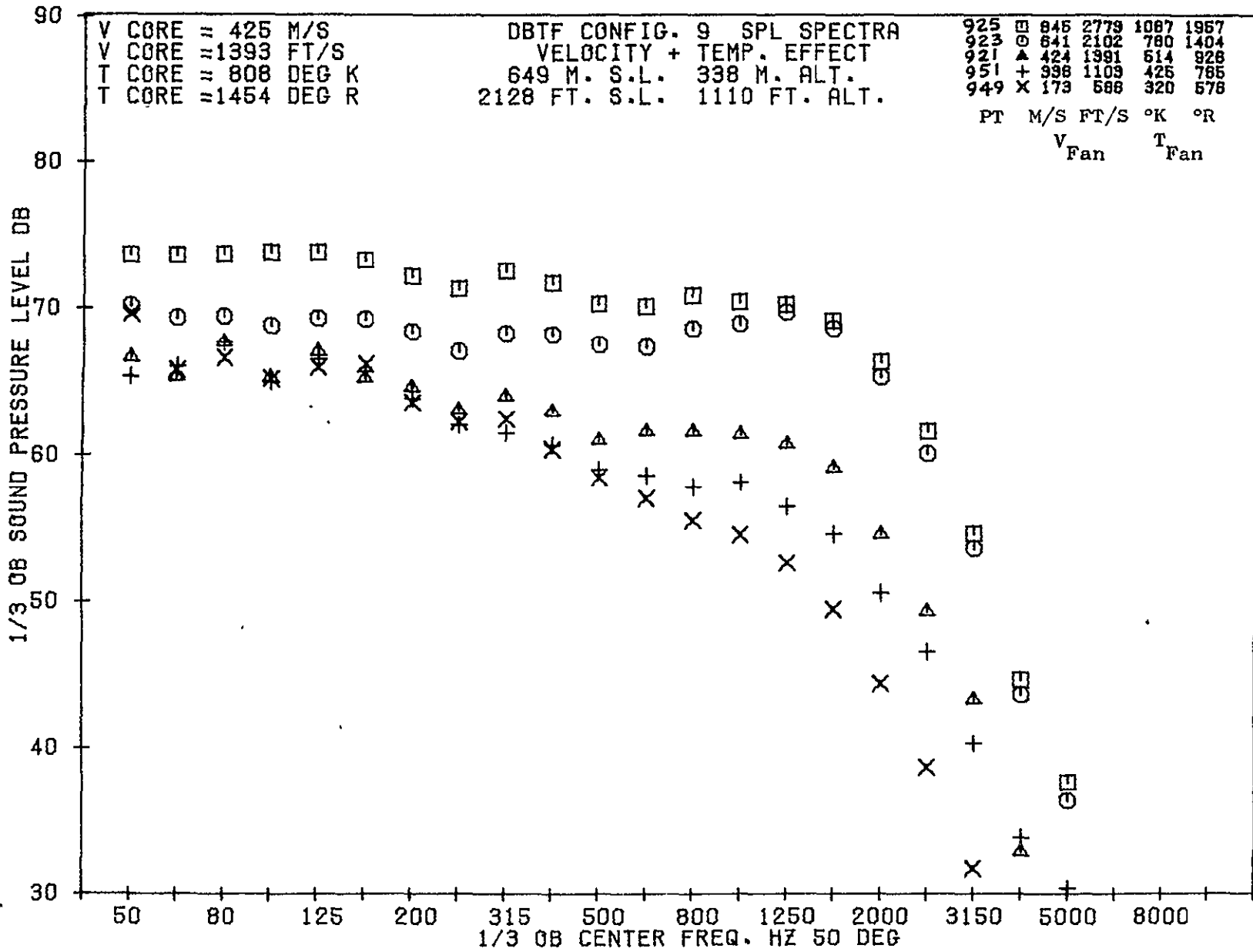
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08/18/75
 ER266-001

70 BURCH 0

4-364

1608

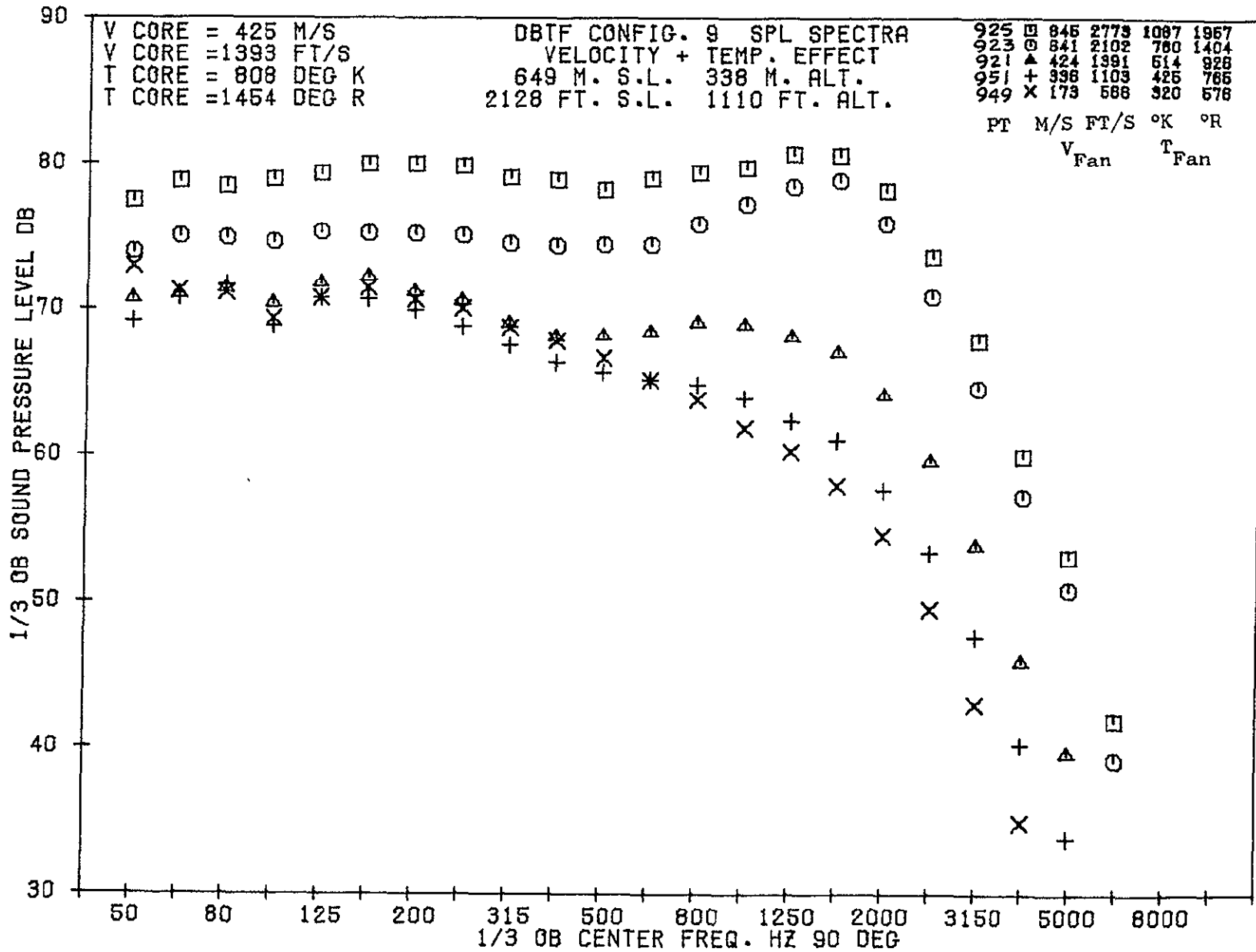


U-3615

08/18/75
 BR266-001

79 BURCOR.

1609

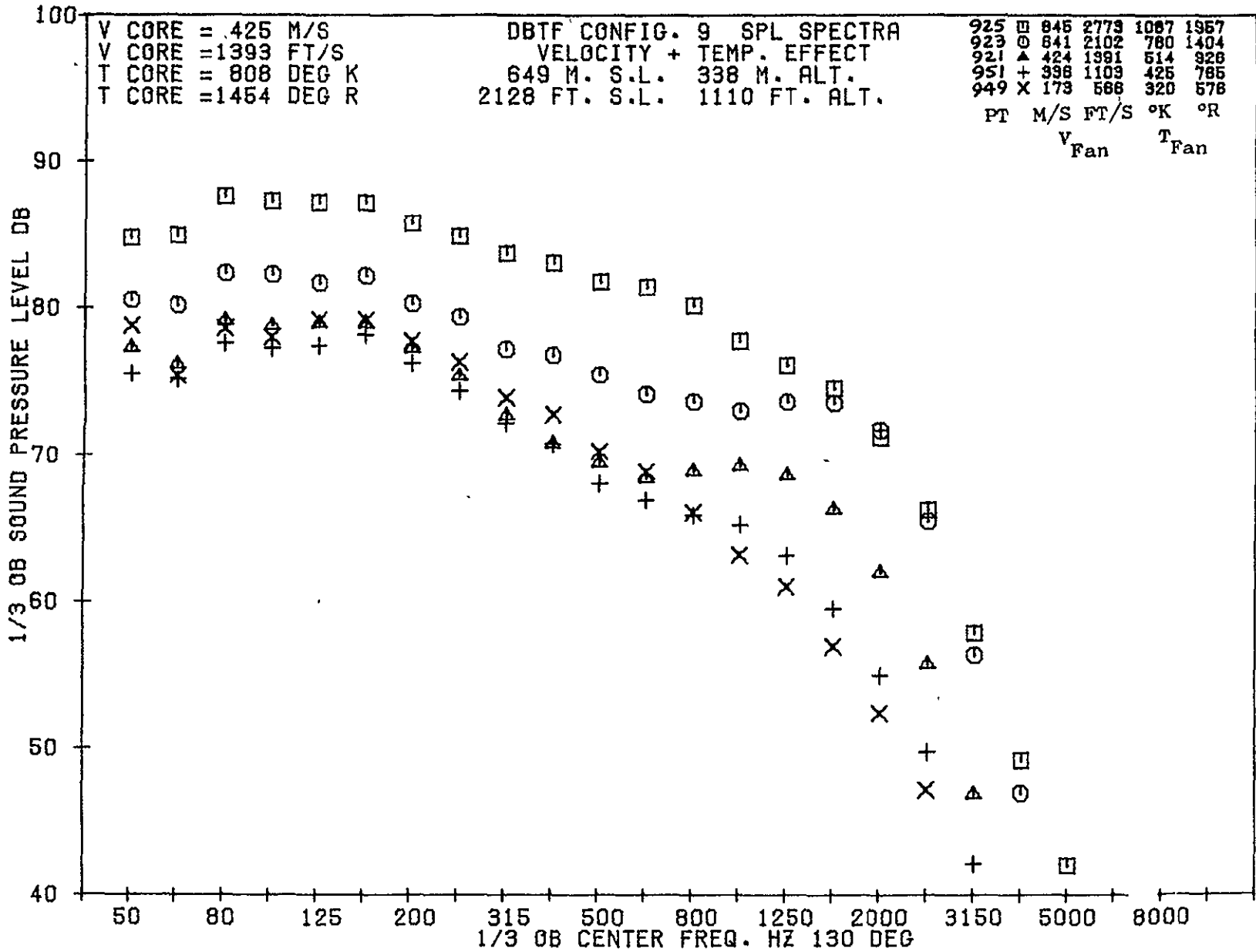


08/18/75
5R266-001

79 BURCH A.

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1610



4-26-75

08/18/75
5R266-001

74 BURC A.

5.0 ON-LINE NARROWBANDS

5.0 ON-LINE NARROWBANDS

The acoustic data was monitored during test with an on-line spectrum analyzer. Any unusual tones were investigated. The narrowbands were documented in graph form using an X-Y plotter.

The following graphs are for Model #8, the coannular, coplanar acoustic configuration. This test model exhibited lip tones when the core and fan velocities were matched and shock tones at pressure ratios above critical. The tones are evident in the 1/3 Octave band spectral plots and the narrowbands verify the actual frequencies at which the tones occurred.

The other test configurations did not have significant tones evident and the 1/3 octave band plots have similar characteristics to the narrowbands. The narrowbands were recorded, but are not included in this document.

4 APR 1975

RDC I P E C L

34°

AMPL 90° +10
 130° +10
 ANAL +10

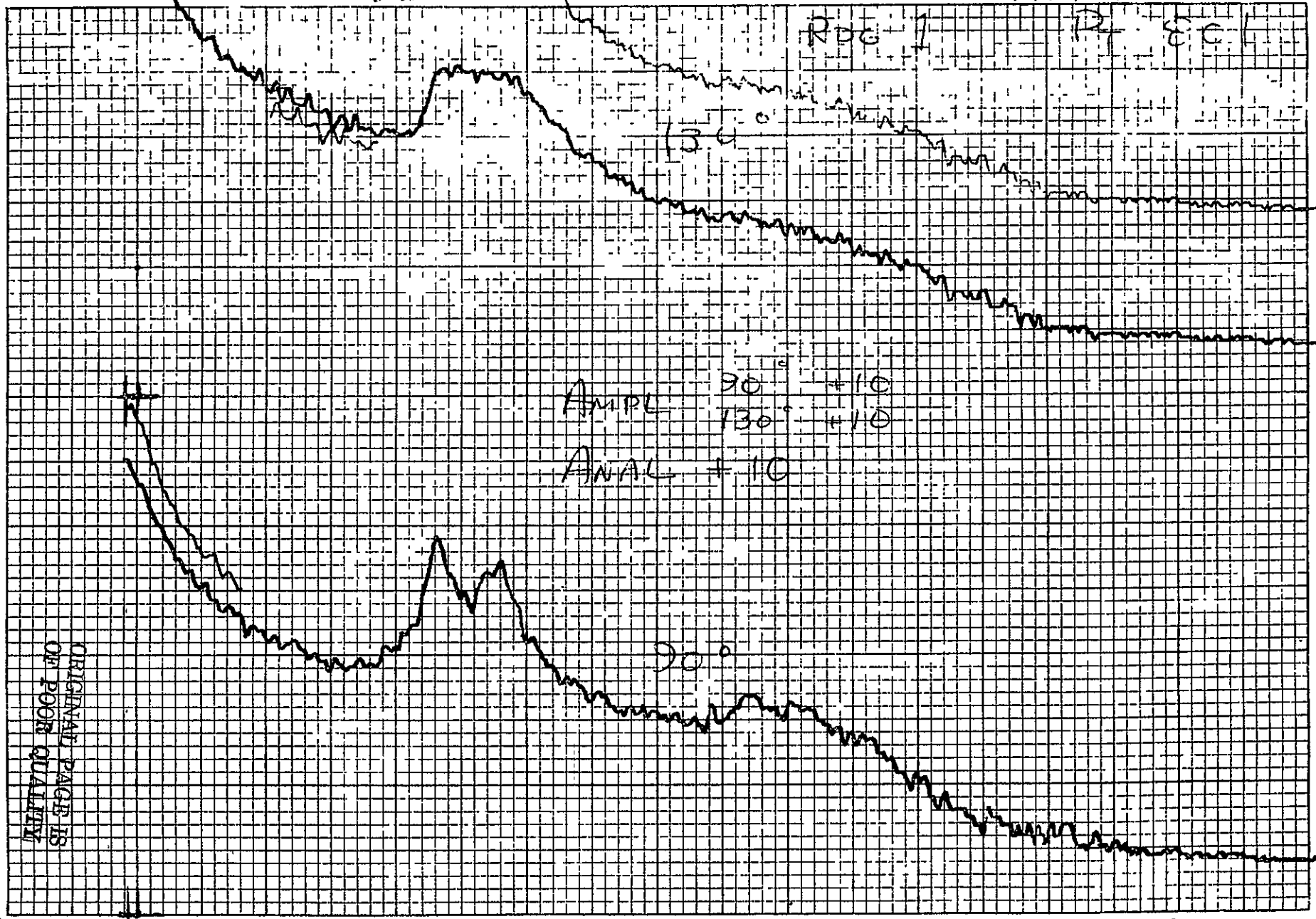
90°

1612

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5-2

0 10 20 30 40 50 60 70 80
 KHz



4-7-75

30.9 KHz

PT 803

PT 803

90

Axis A

90

430

133

723

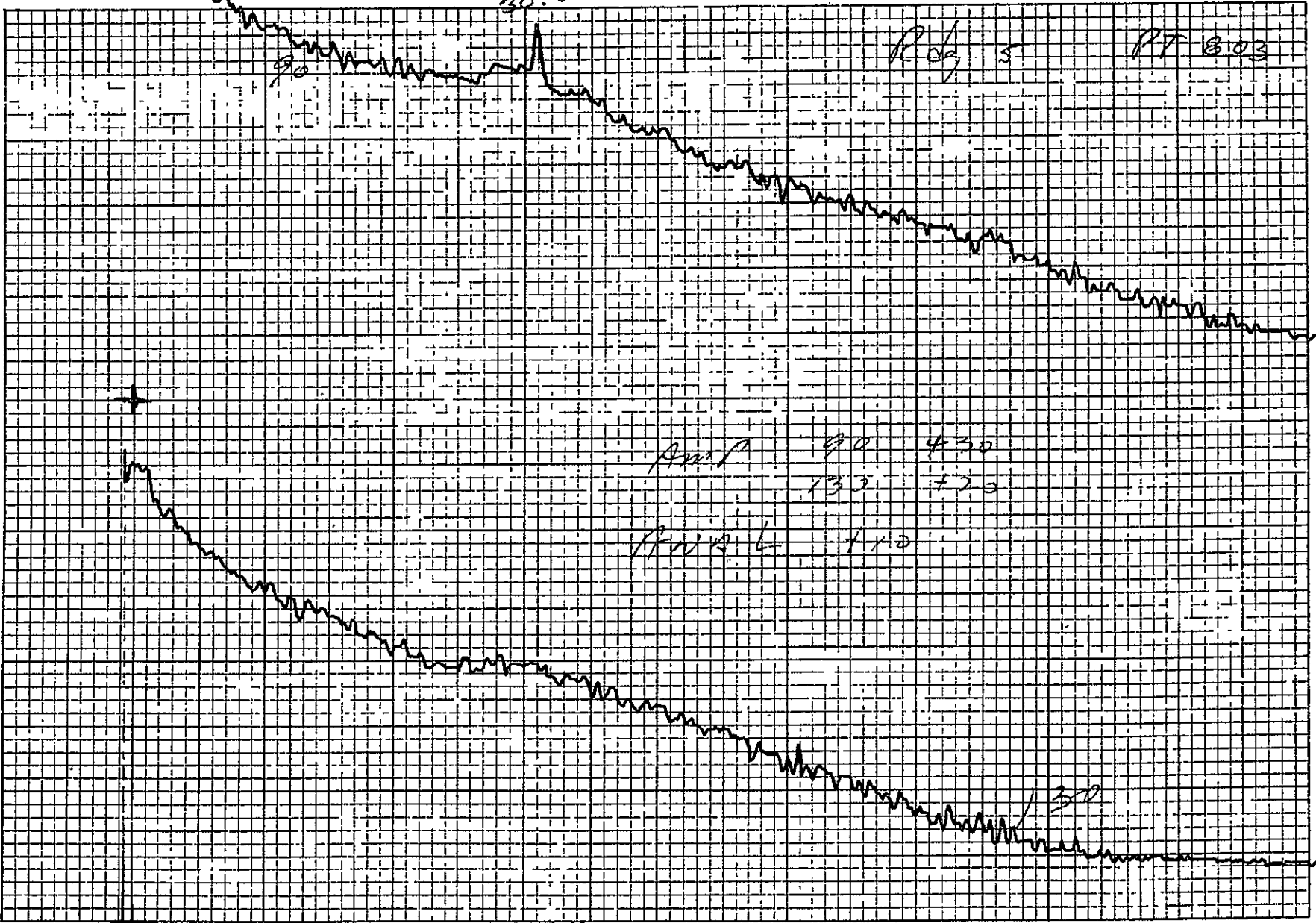
Axis B

410

300

1613

5-4



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4-7-75

Adj 3

PT 805

PLOTTED
PROBLEMS

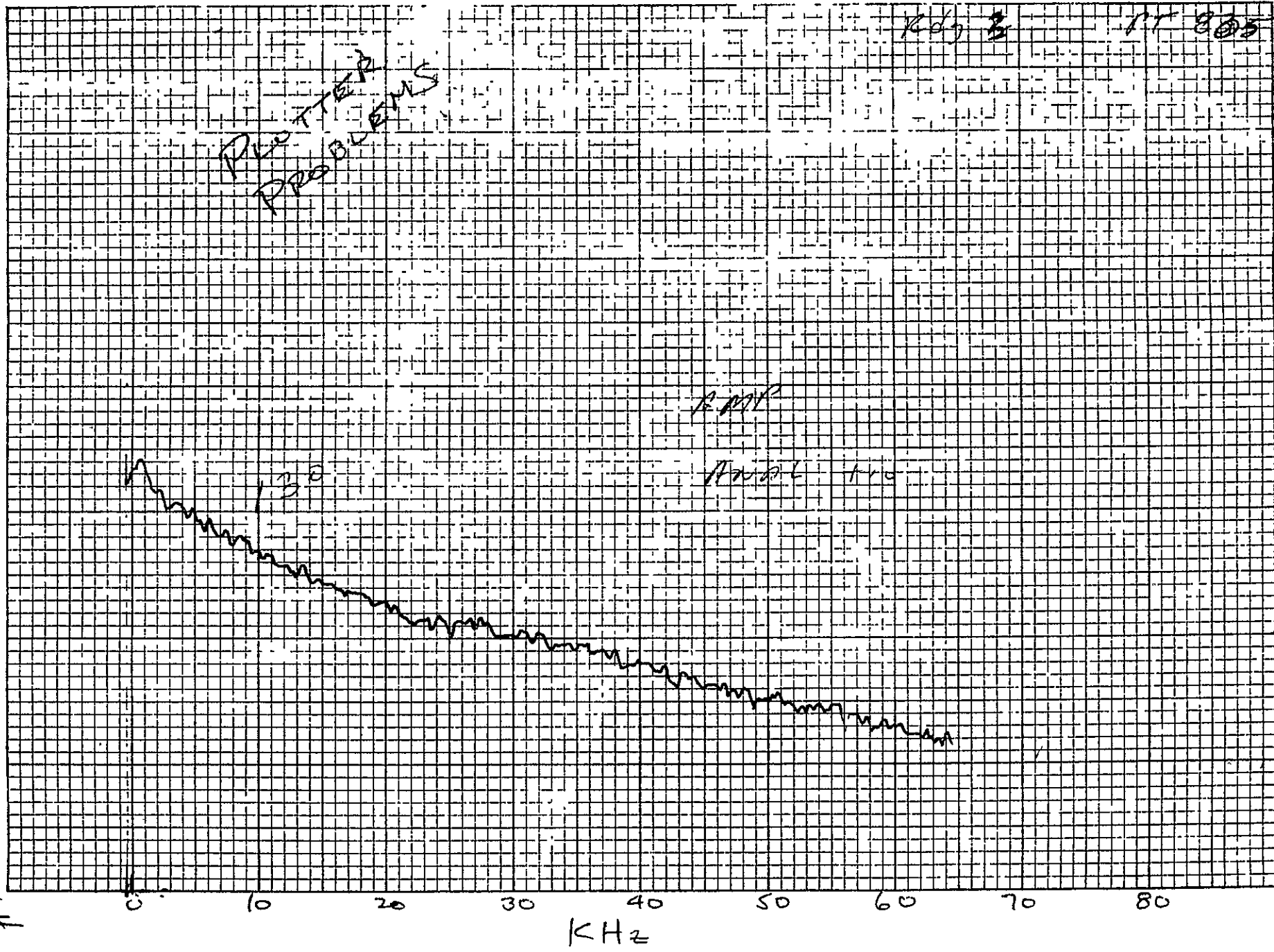
R.M.P.

ANAL. TRC

30

1614

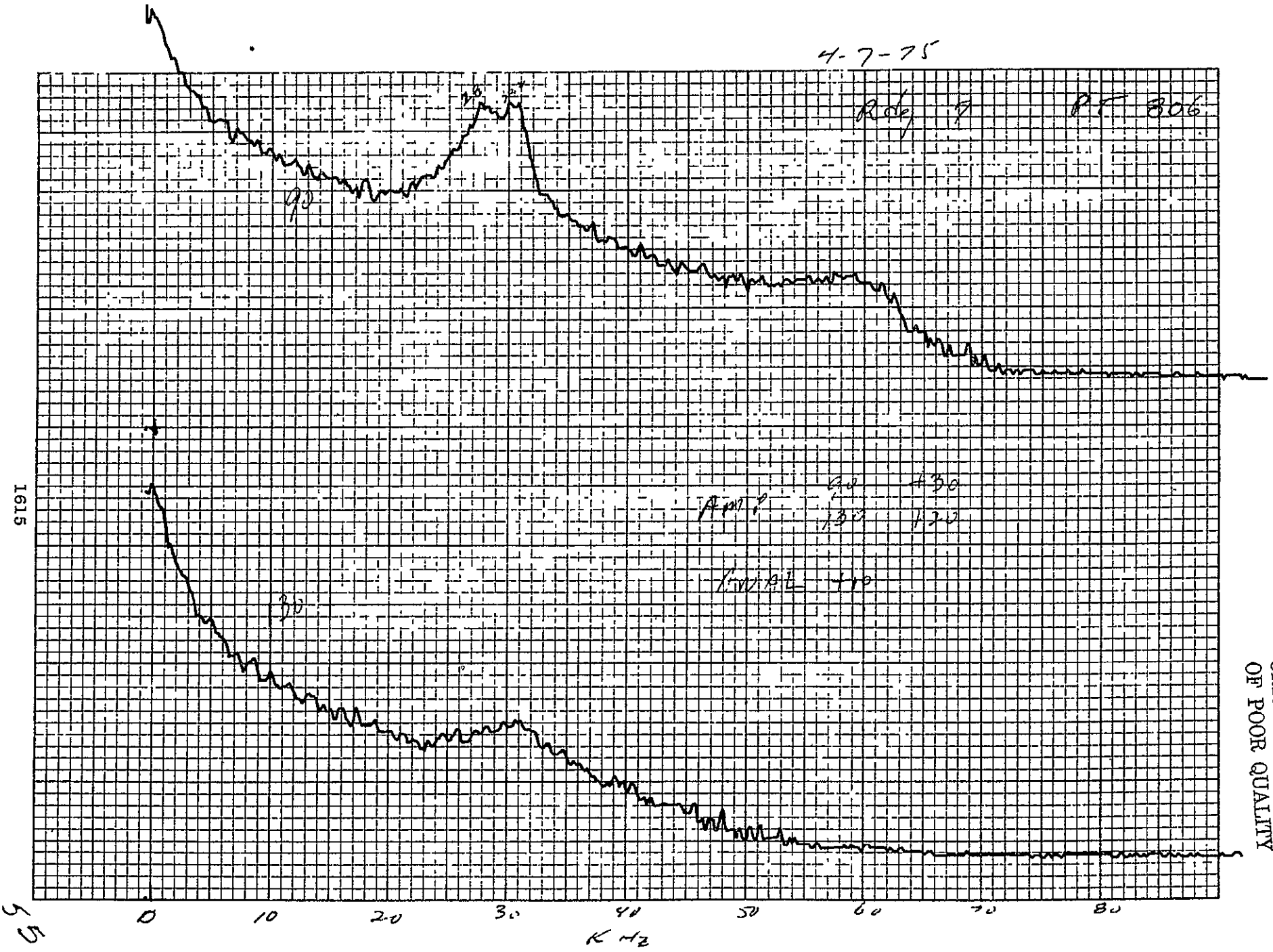
5-4



4-7-75

Rd 7

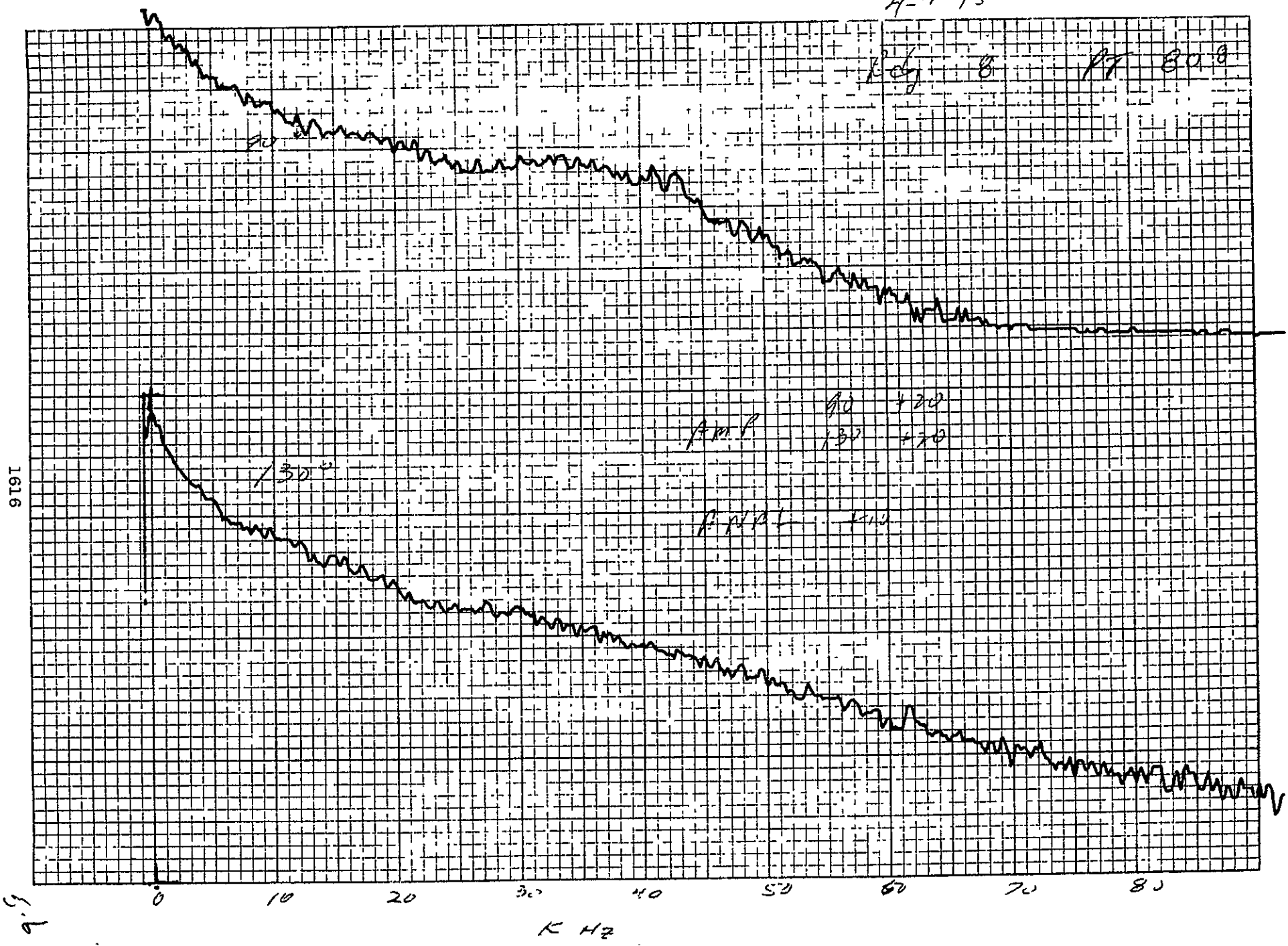
PT 806

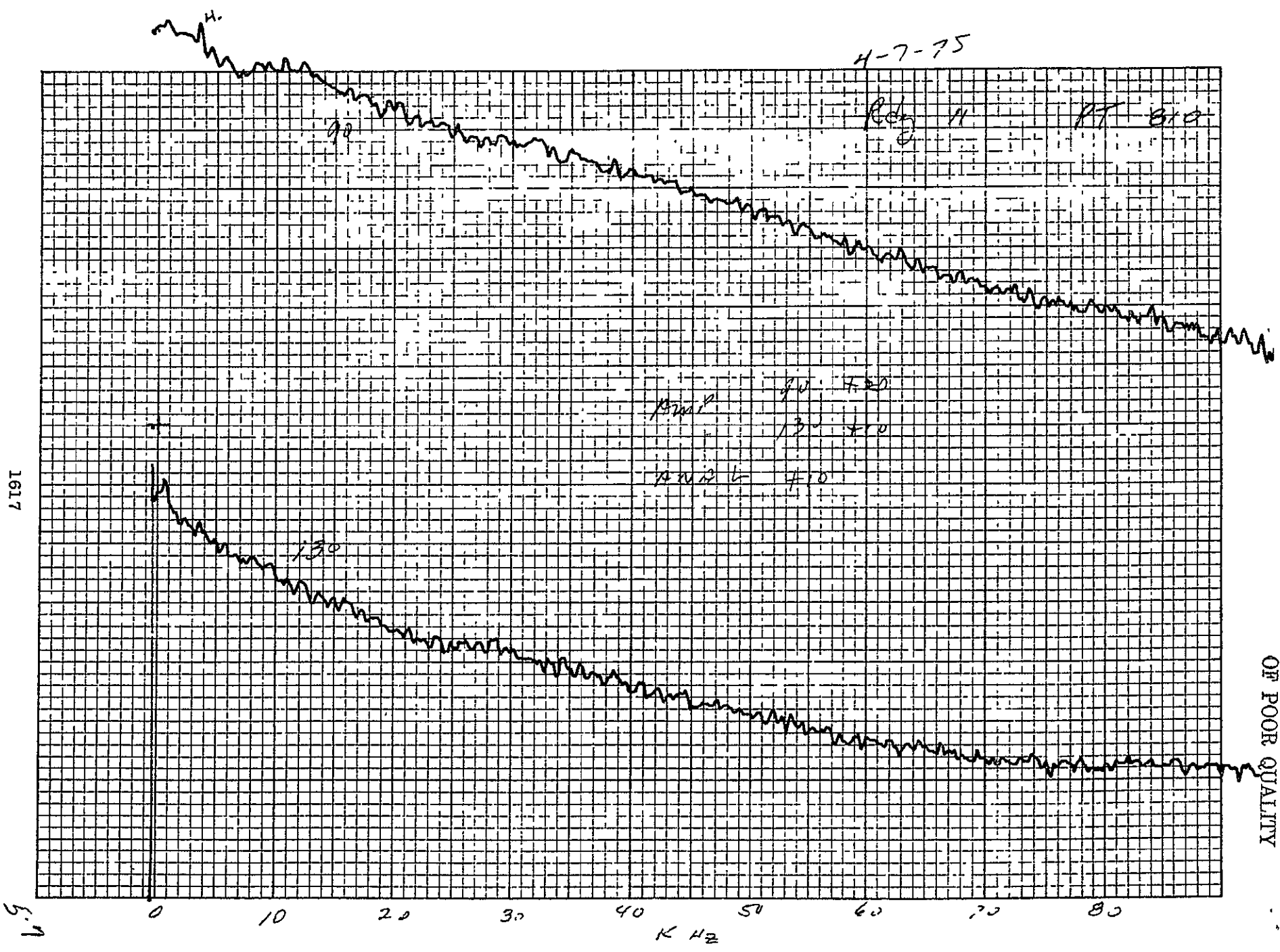


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4-7-75

Ref 8 AF 80.0





1617

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4-7-72

Rdg 20 Pt 811

90°

5.8

10

1618

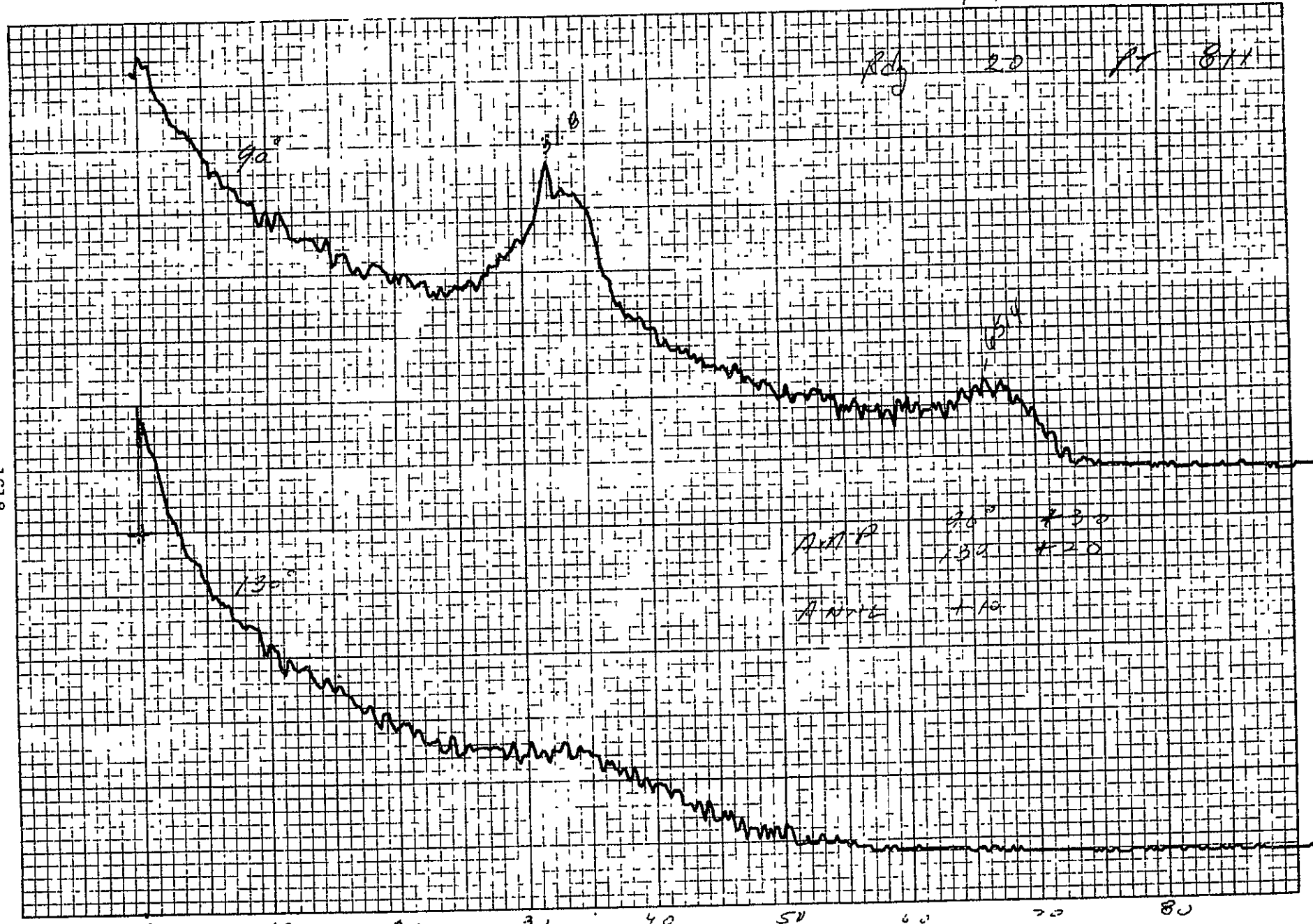
130°

DATA 20° F 30
130° F 20

ANNE 1/10

5.8

K HZ



4-7-75

Fig 29 PT 813

90°

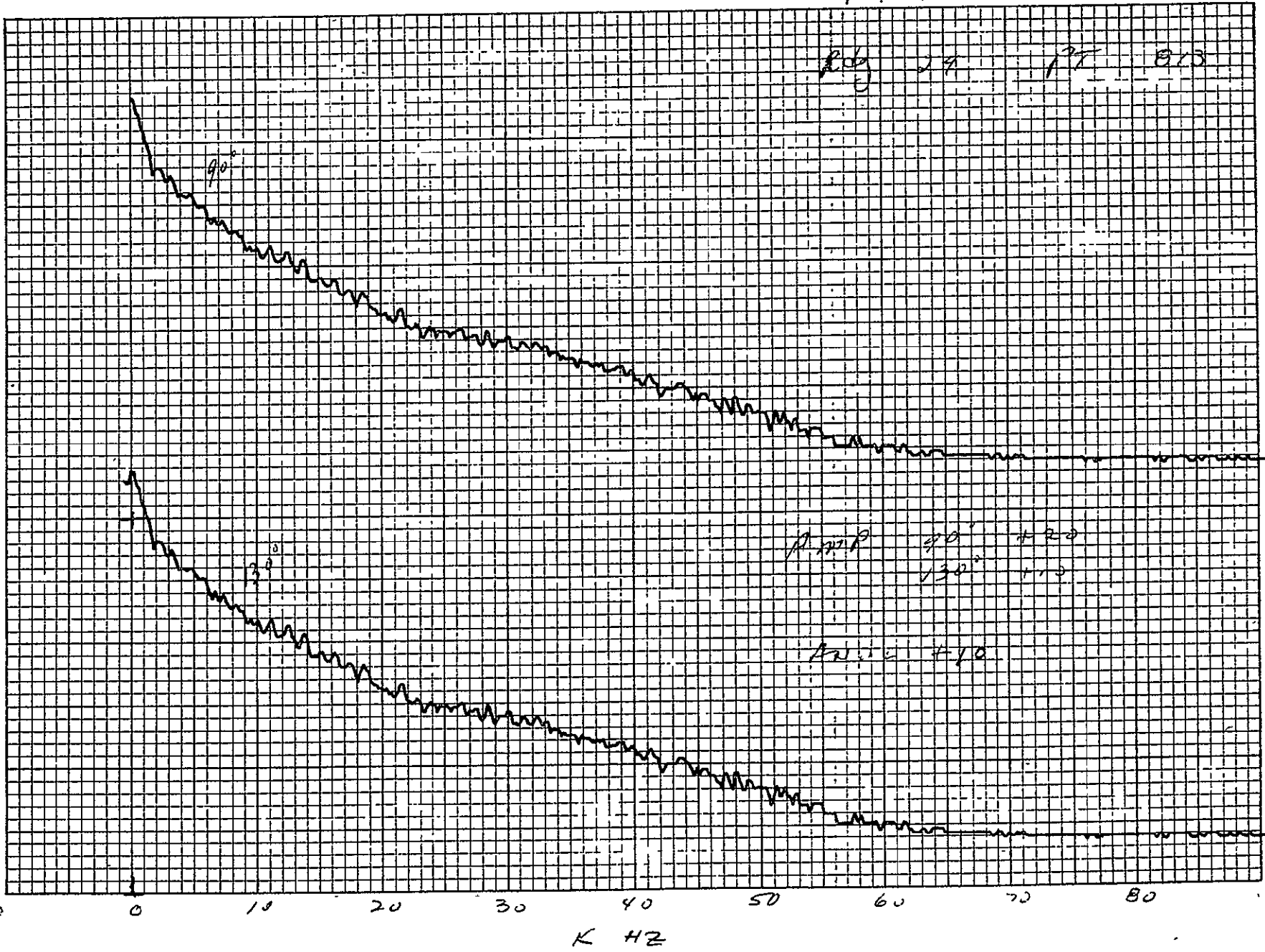
30°

AMP 90° +20
130° +10

Phase +10

1619

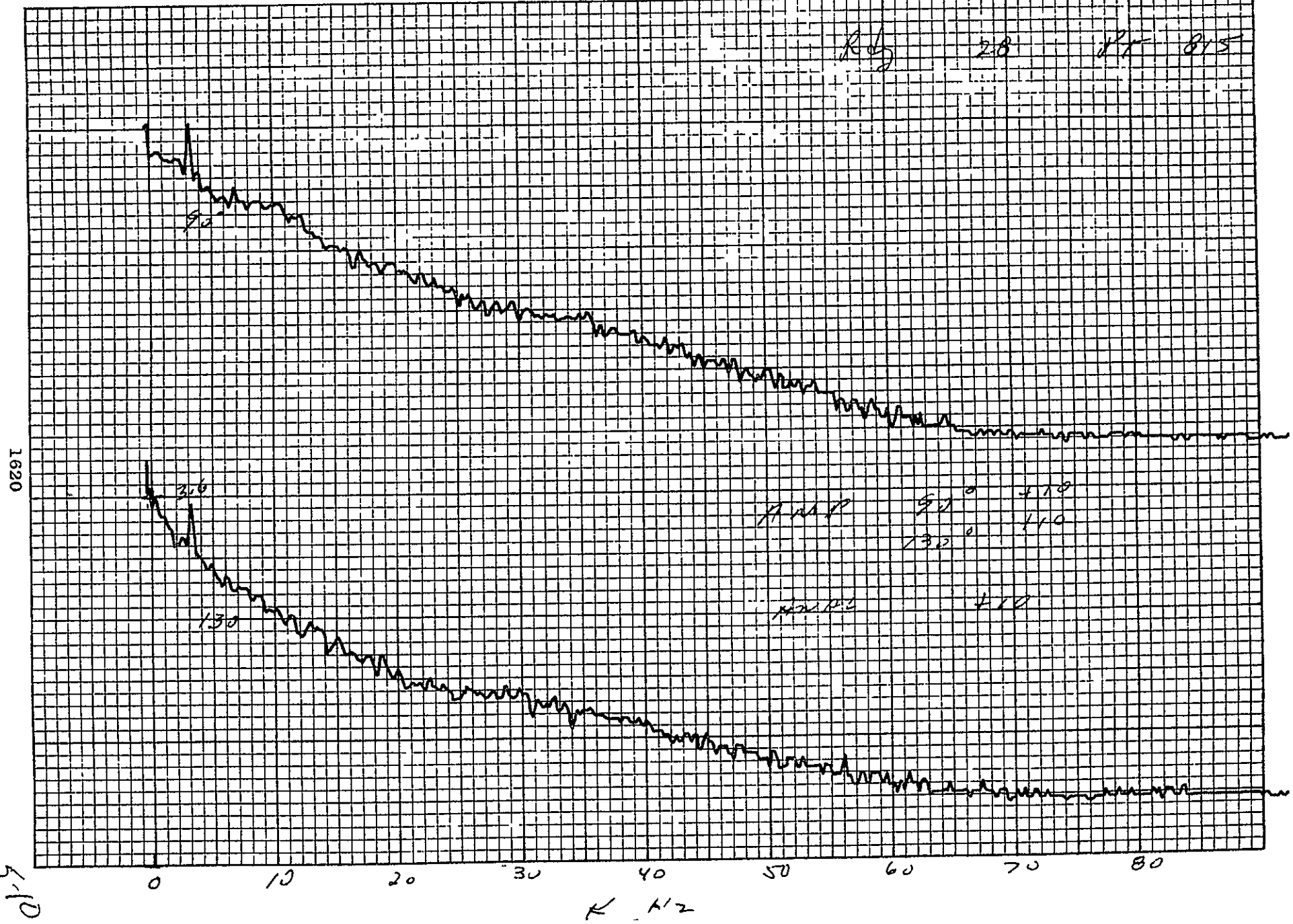
5.9



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4-7-75

R_g 2.8 PF 815



4-7-75

APR 28 11 31 AM

1621

APR 13 7 10

APR 7 10

120°

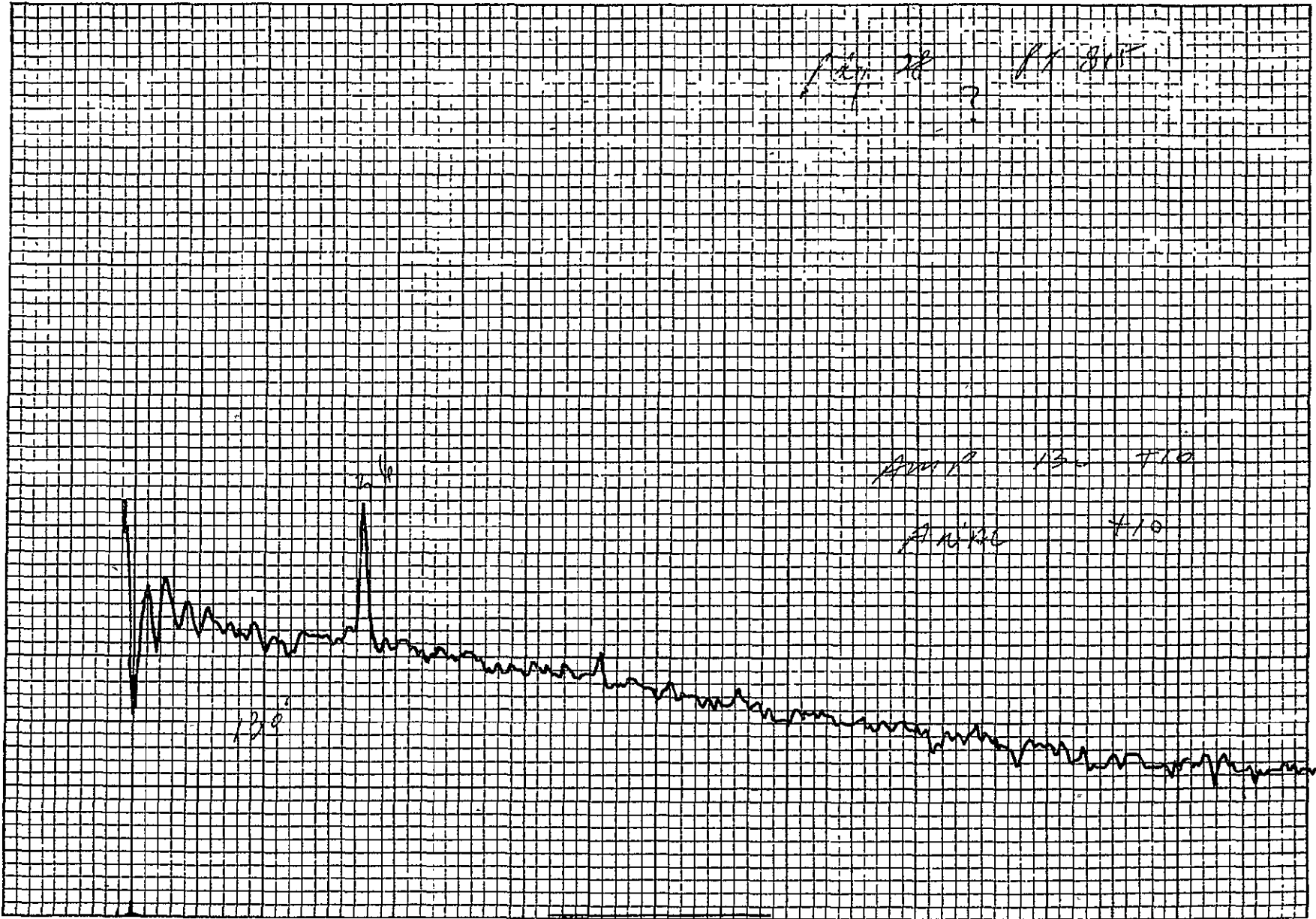
200

5-11

0 2 4 6 8 10 12 14 16 18

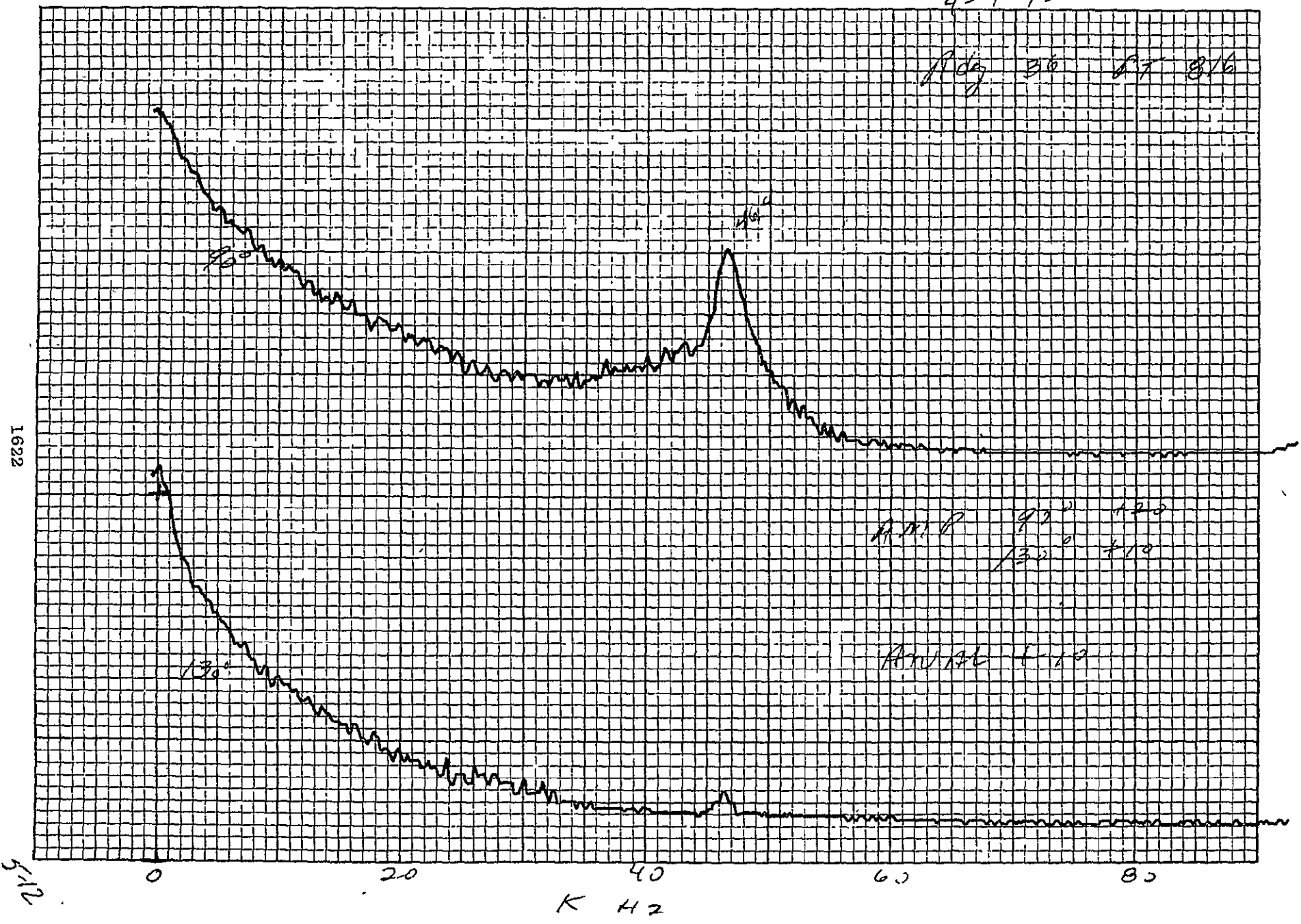
K H z

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4-7-75

Adj 36 27 3/6



4-7-75

REG 31

PT 818

90

1823

60

AWA P

90

470

100

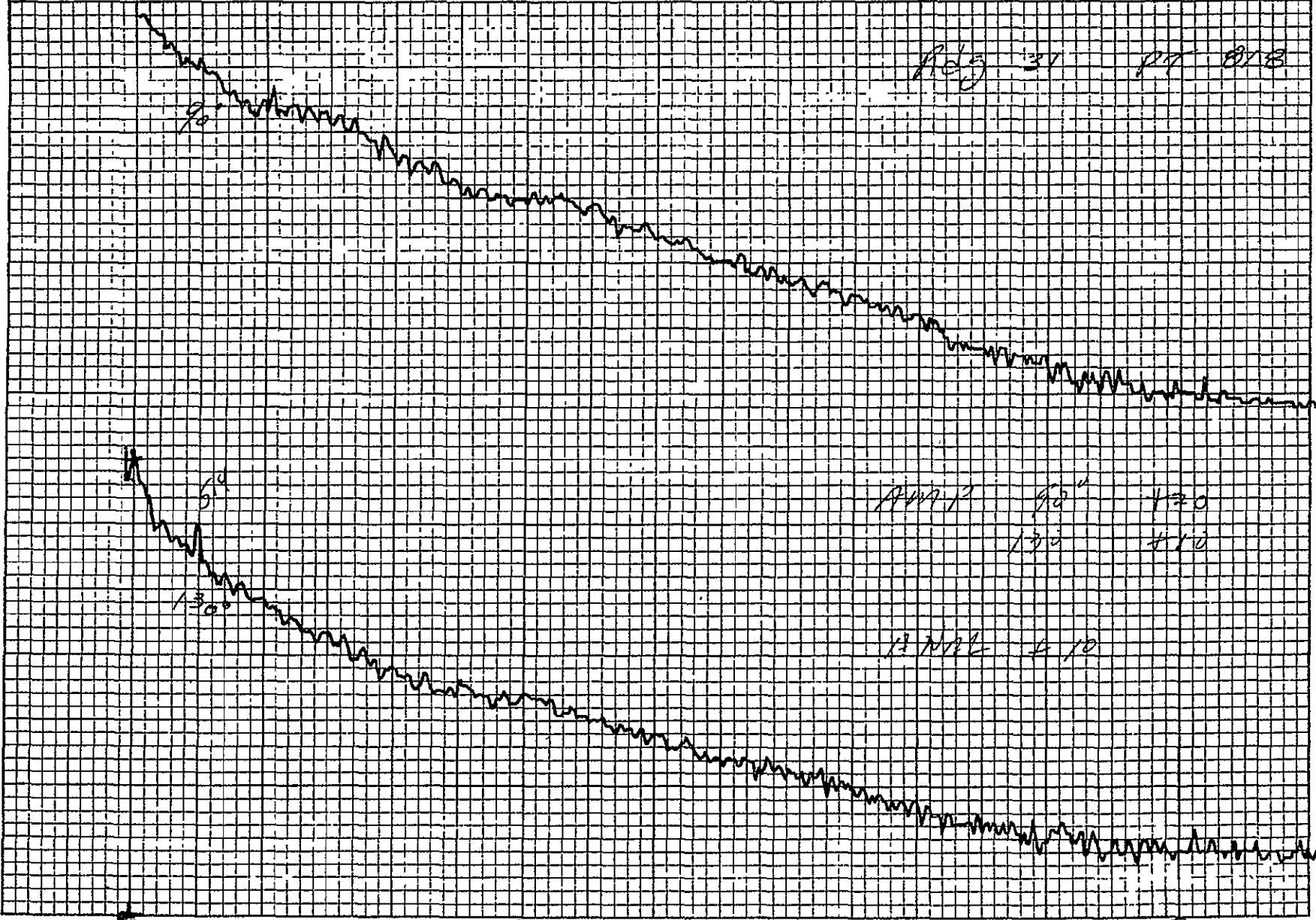
410

100

13 N/A

410

5/3

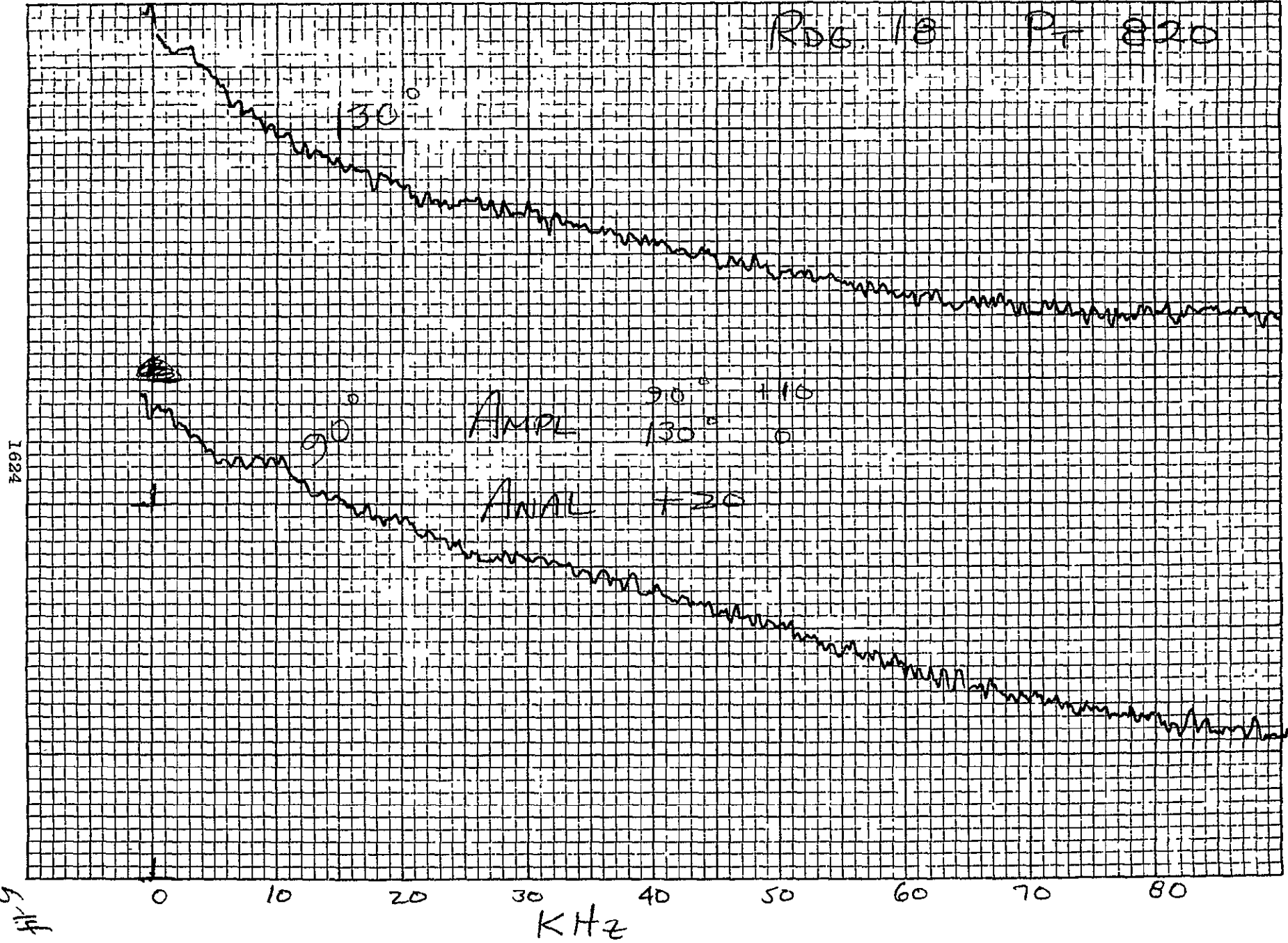


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K Hz

4 APR 1975

RDG. 18 P_F 820



4-7-75

Adj 92 RT ER

90

46.5

1625

AMP

30° + 20
120° + 10

120 Hz

+ 10

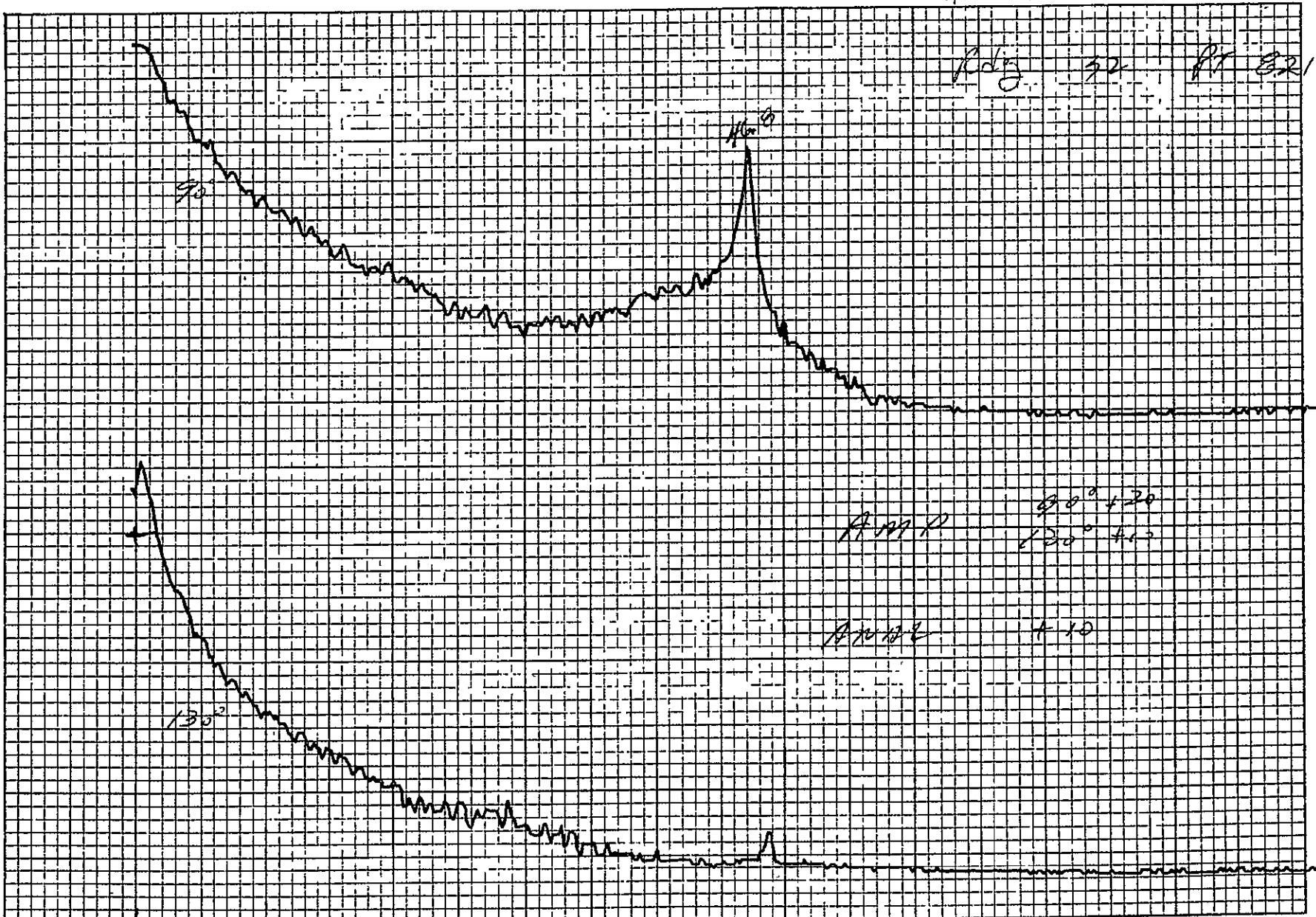
130°

5-15

0 10 20 30 40 50 60 70 80

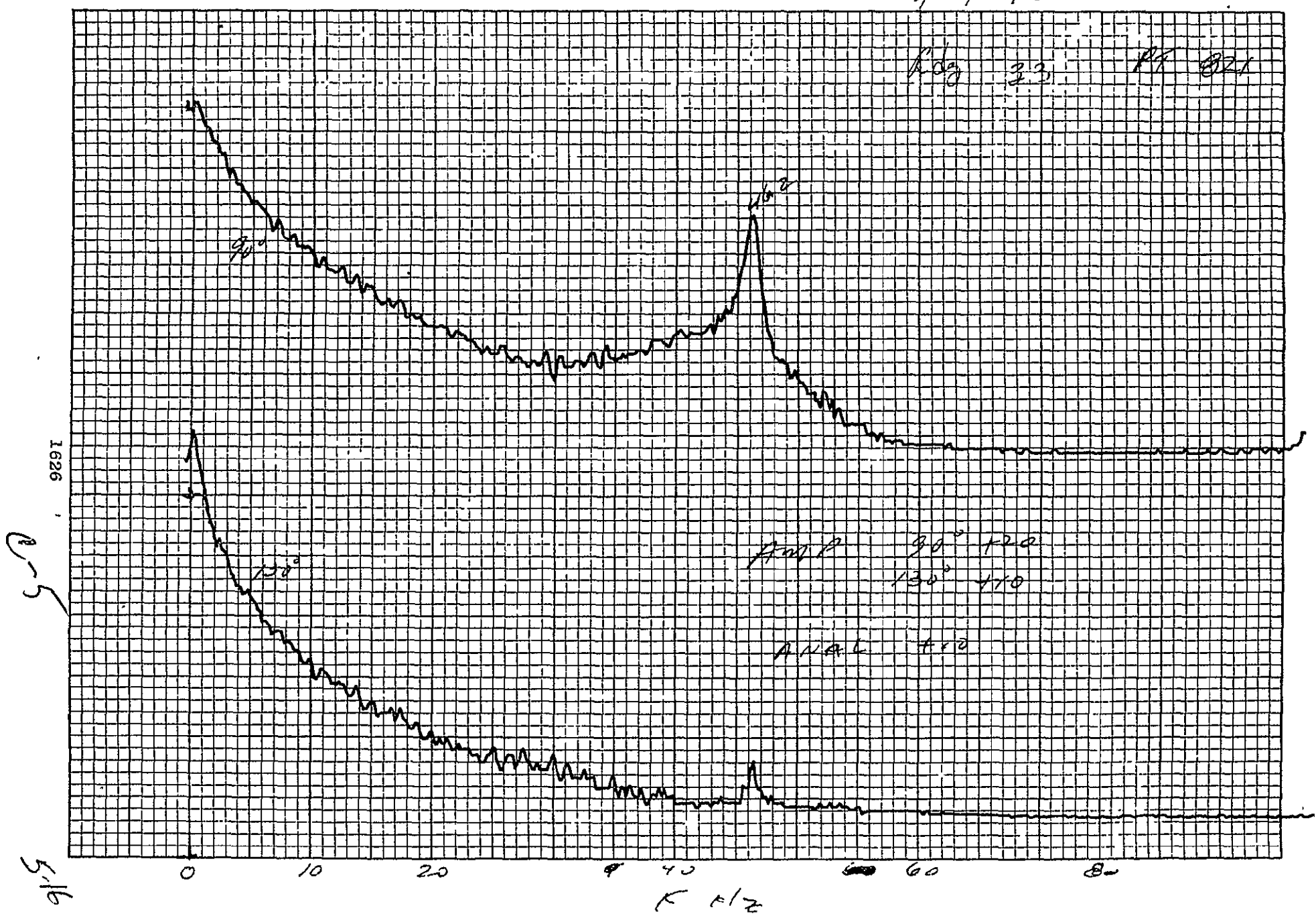
KHz

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4-7-75

Adg 33 PF 821



AMP 90° 120
130° 470

ANAL 470

P-5

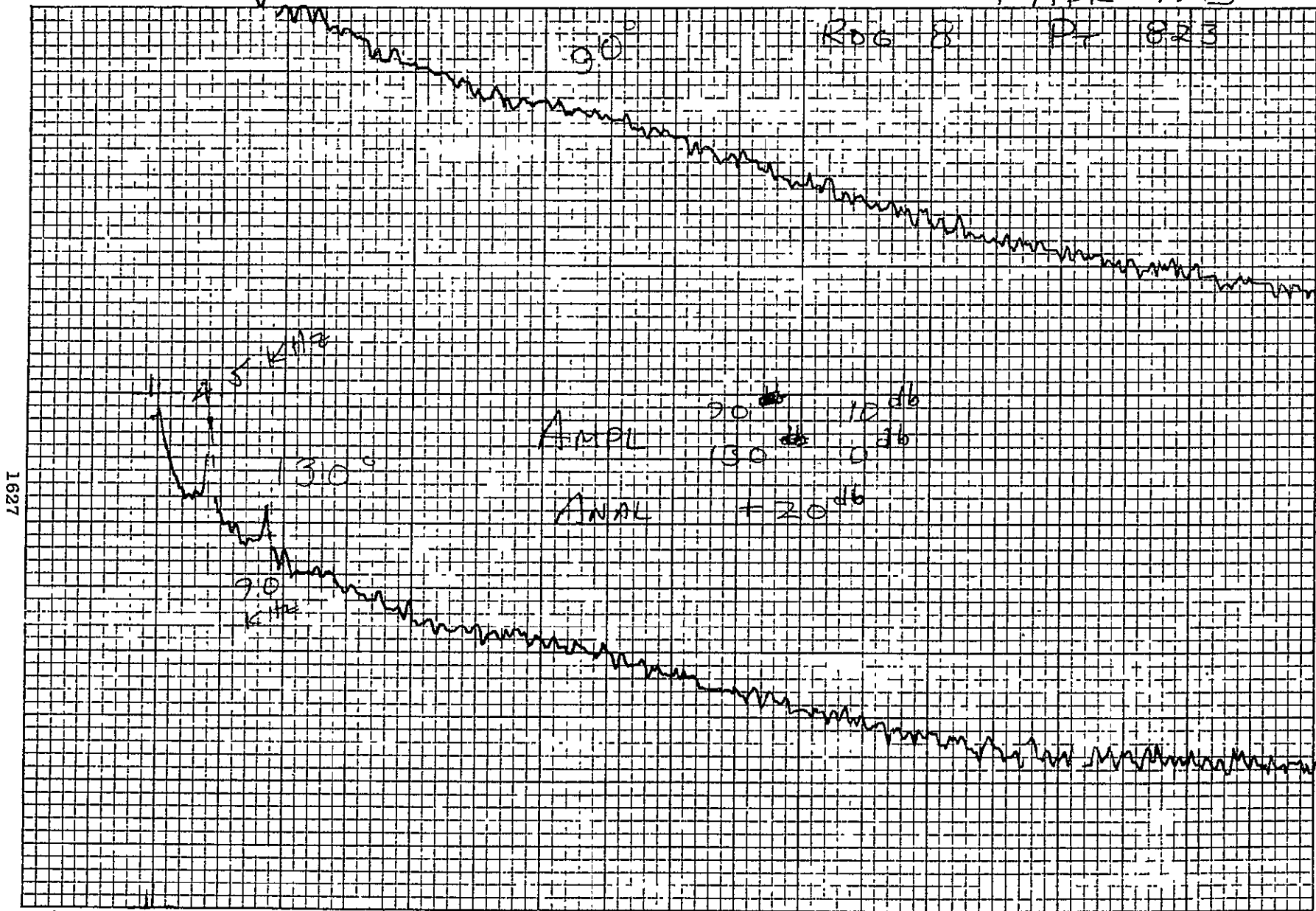
5.16

4 APR 1975

LOG 8 PL 823

30°

2000



1627

KHz

5.11

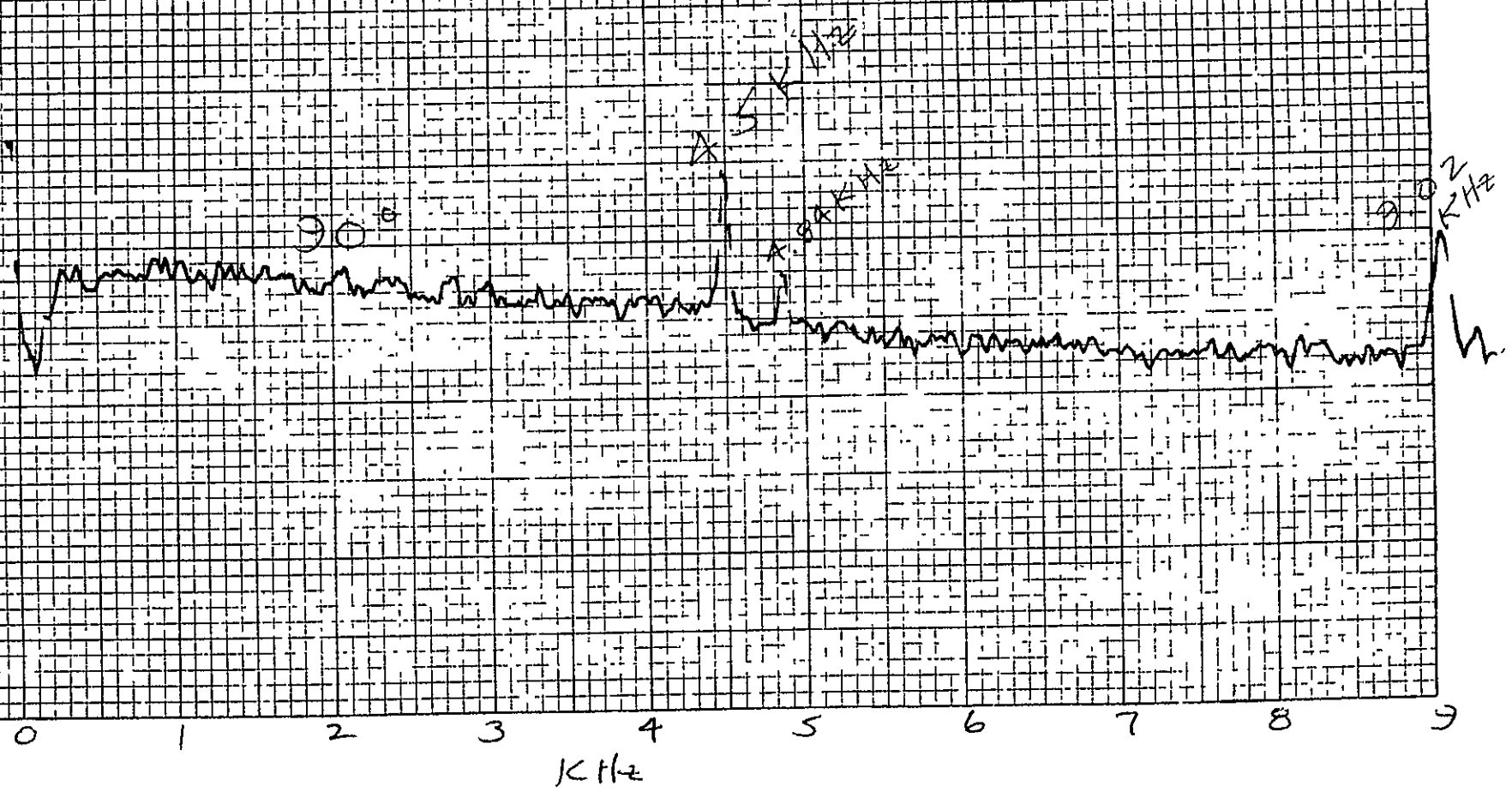
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4 Apr 1975

R068 Pt 23

1628

5-18



2.34 KHz

4 Apr 1975

ROG 12 Pt 825

130°

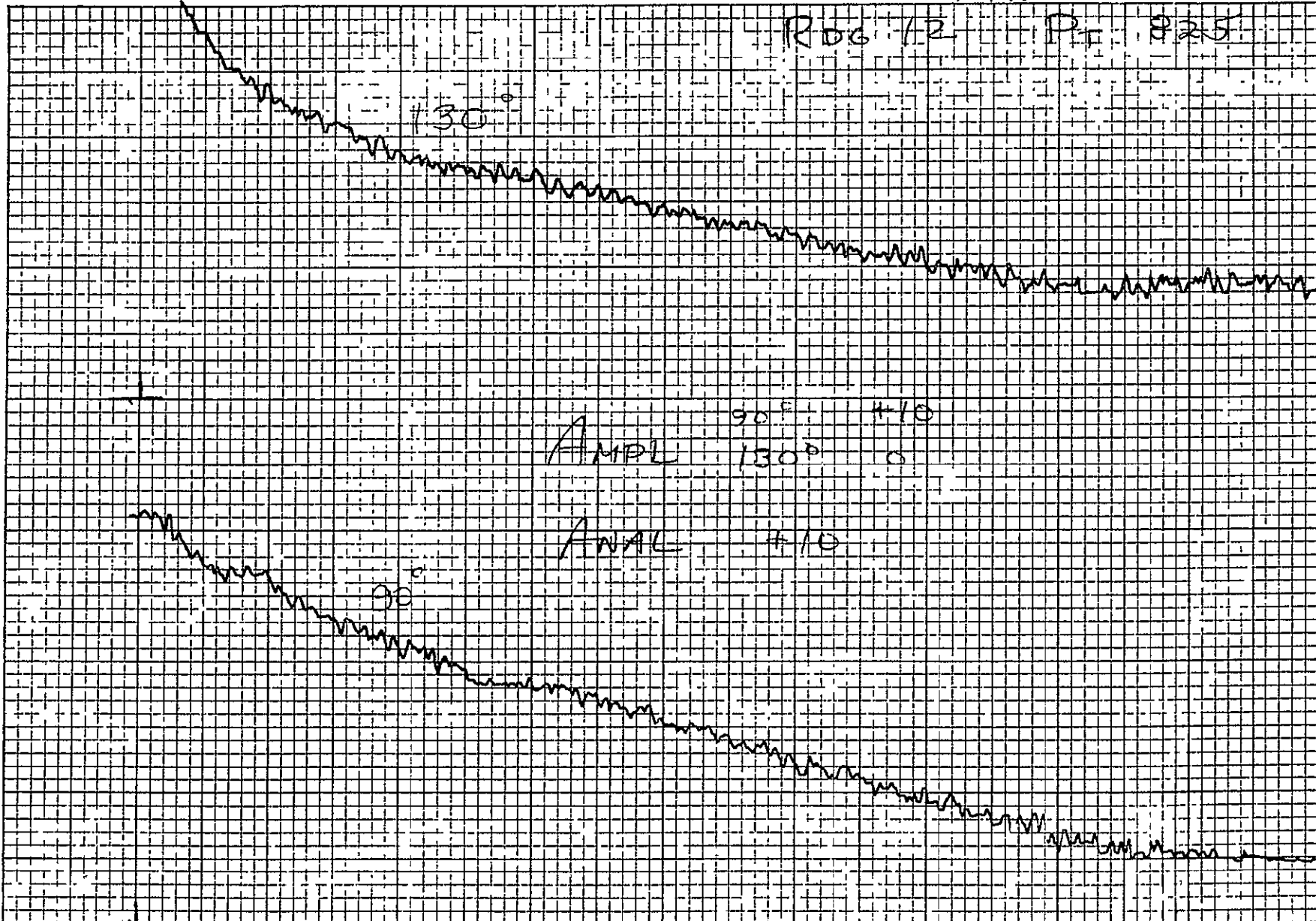
AMPL 90° #10
130° 0

ANAL #10

90°

1629

5.9

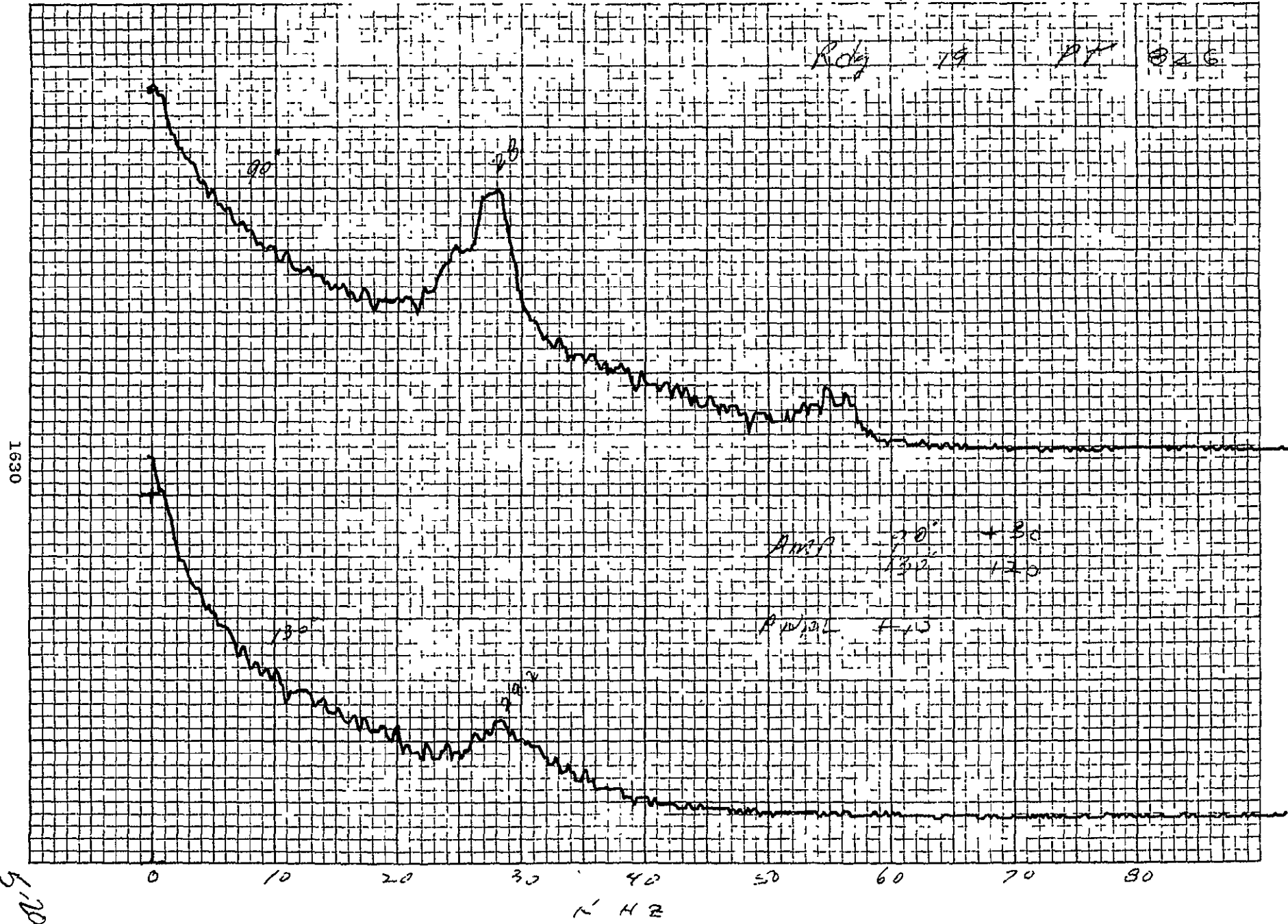


0 10 20 30 40 50 60 70 80
KHz

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4-7-75

Rdg 19 PT 826



5.20

4-7-75

104 2.2 AT 82.7

190°

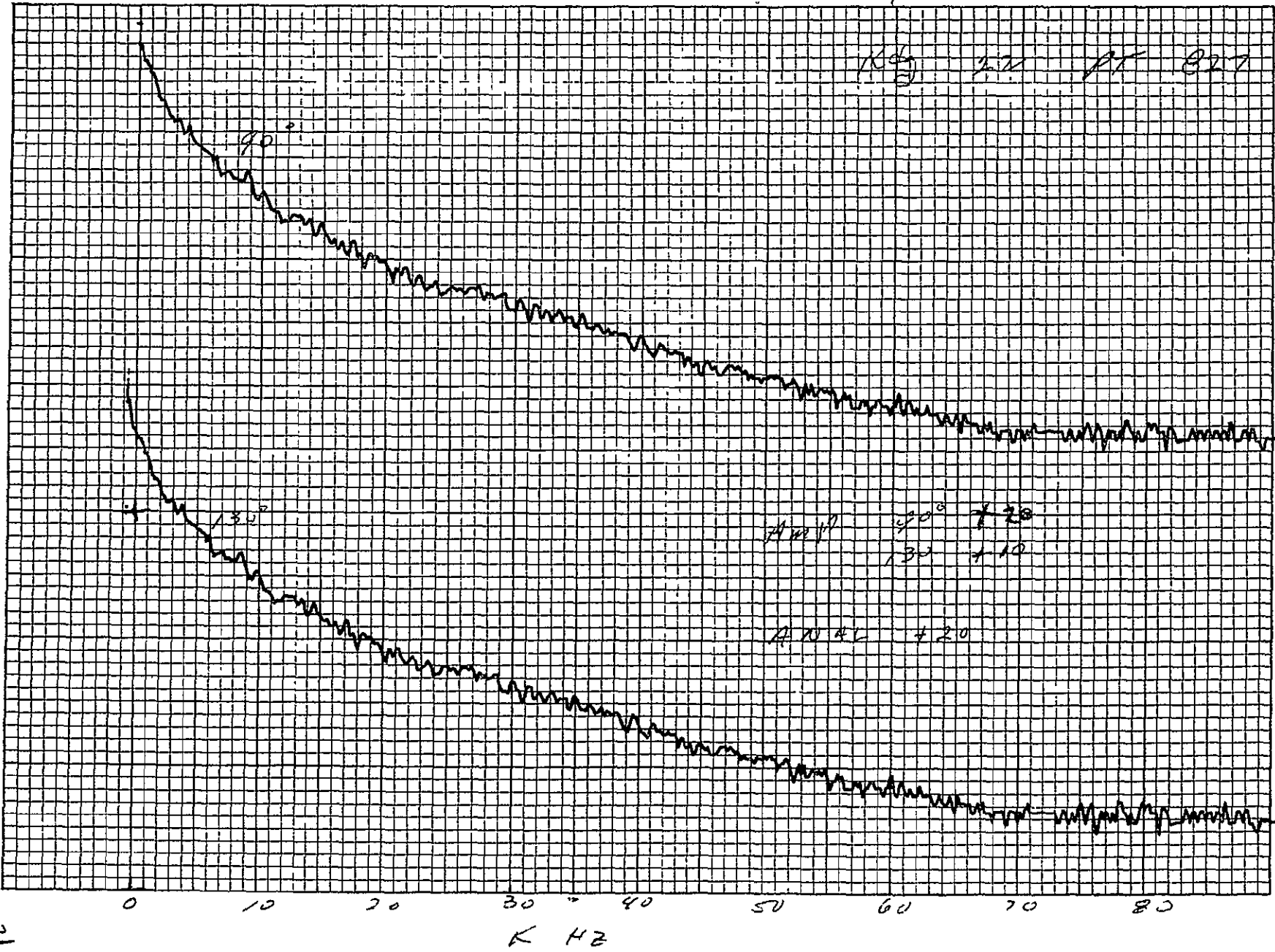
130°

APR 19 190° + 20
130° + 10

APR 19 + 20

1631

5.21



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H-7-75

Red
6

16

PT 82.8



Red 10

9.0

12.0

13.0

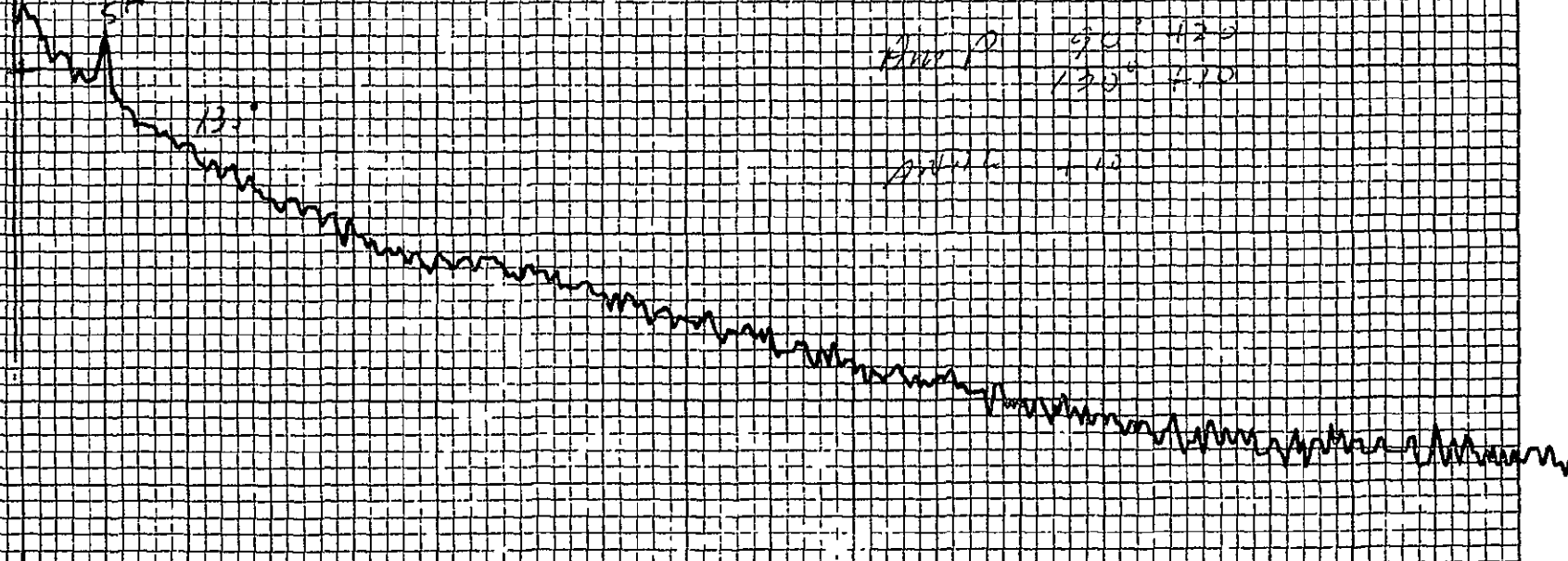
4.0

Red 10

1.0

1632

5.22



K H2

4-7-75

Rdg

25

PT

~~8.5~~

90°

130°

A.M.P

90°

7.20

130°

7.10

P.M.P.L

7.10

1633

5.23



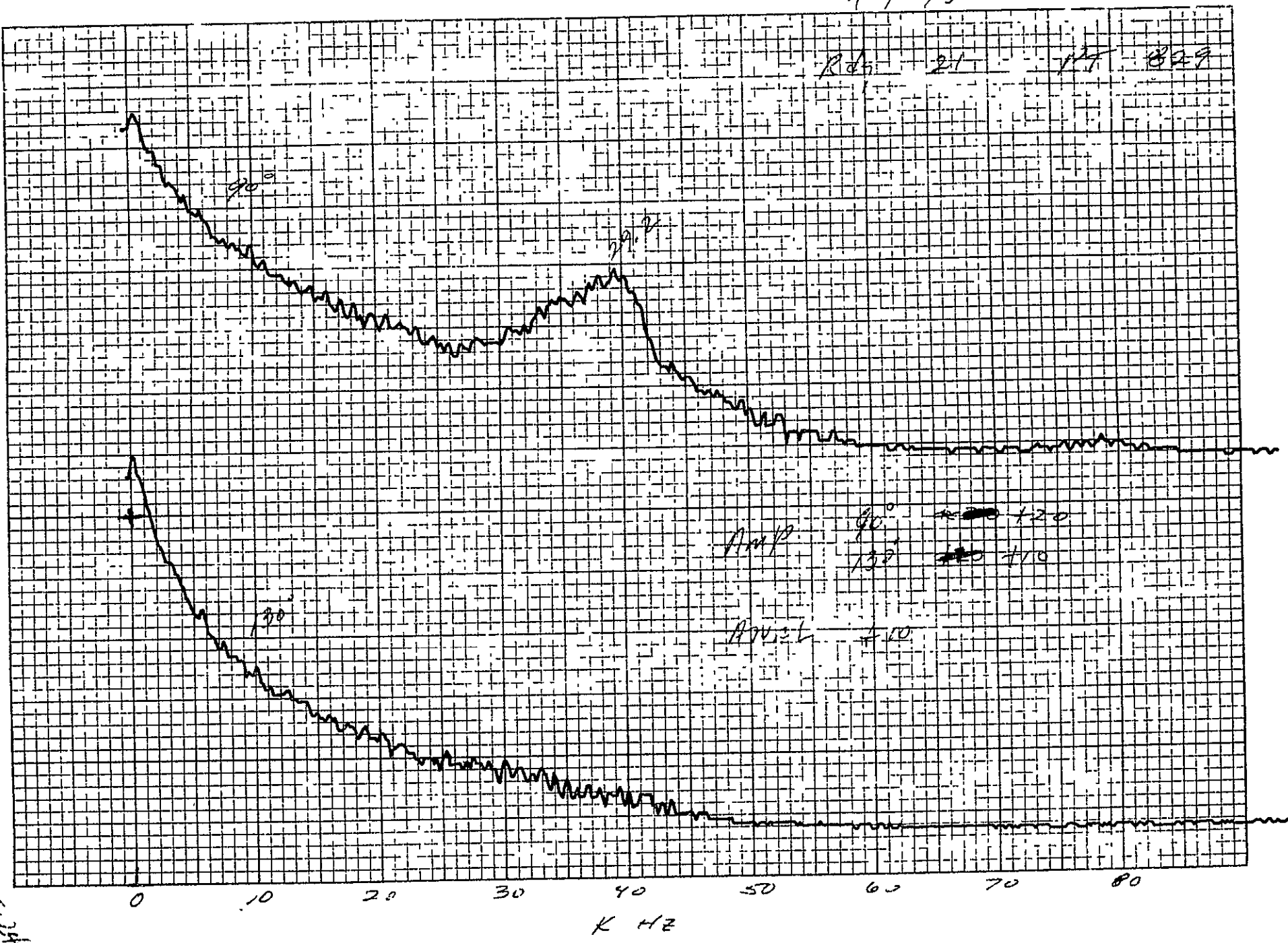
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4-7-75

RD 21 117 829

1634

5.24



AMP
 90° → +20
 130° → +10
 AVG. L ±10

1-7-75

-Rdg- 2.7 PF 83.0

90°

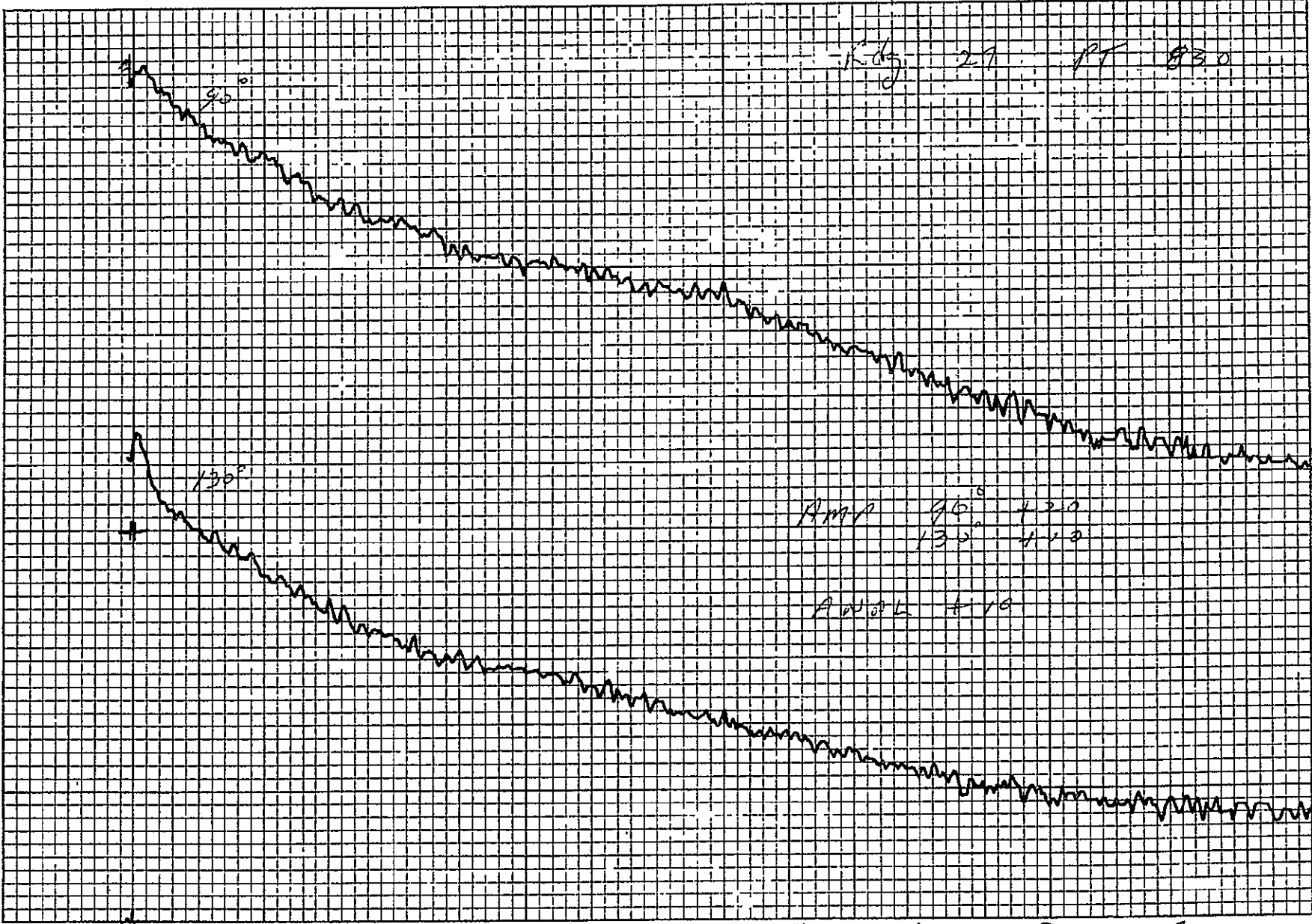
130°

AMP	46 ⁸	430
	130°	410

A.W.O.L. 4.19

1635

5.25



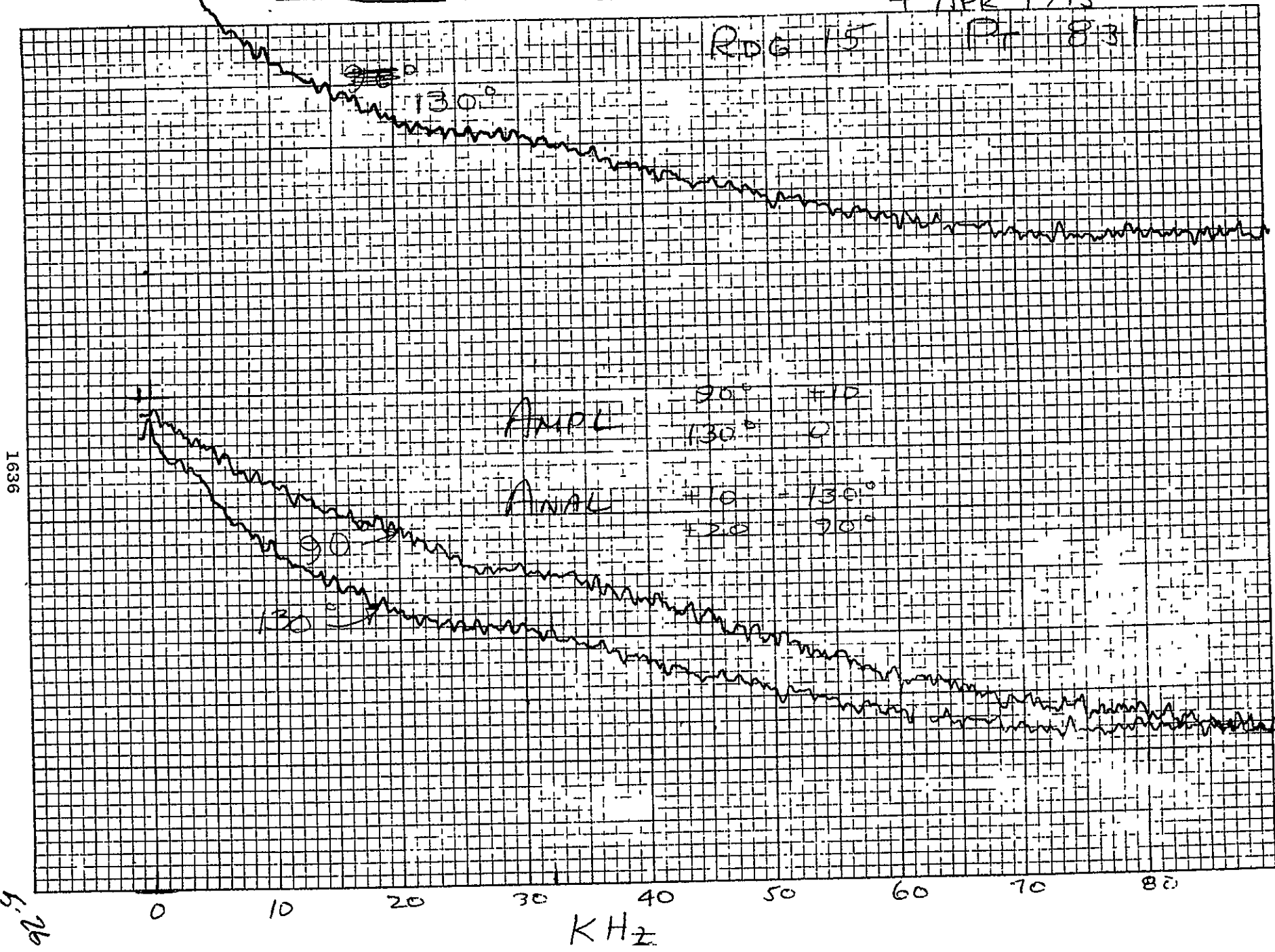
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~~RESEARCH~~
~~PROBLEMS~~

4 APR 1975

ROG 15

Pt 83



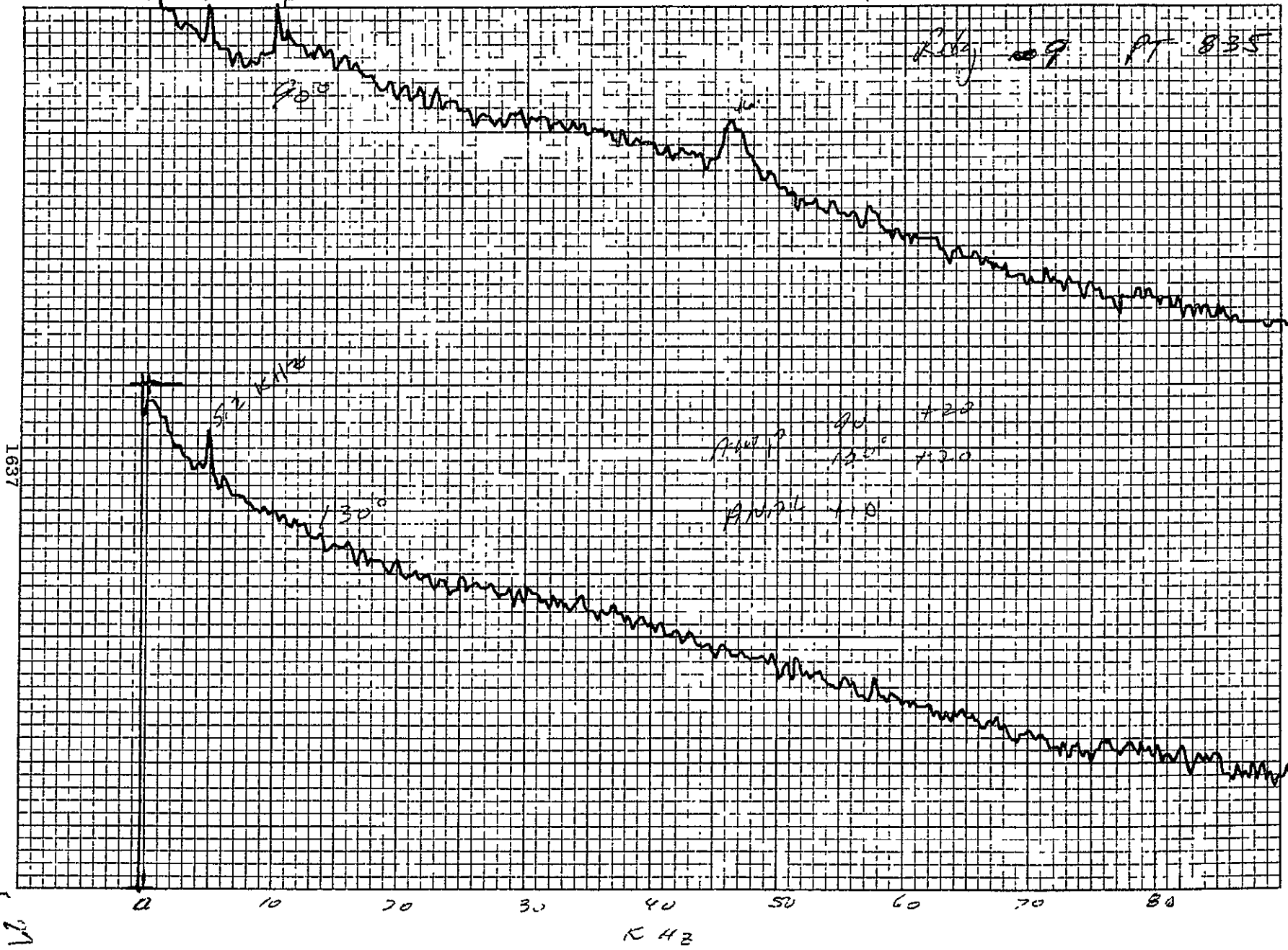
6-9

4-7-75

King of Pt 835

5.2 KHz
10.6 KHz

F₀



Amplitude	80	+20
Amplitude	120°	+20
Amplitude	110	

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4-7-75

Rdg 10 PT 836

90

APR 90 420
130 410

APR 90

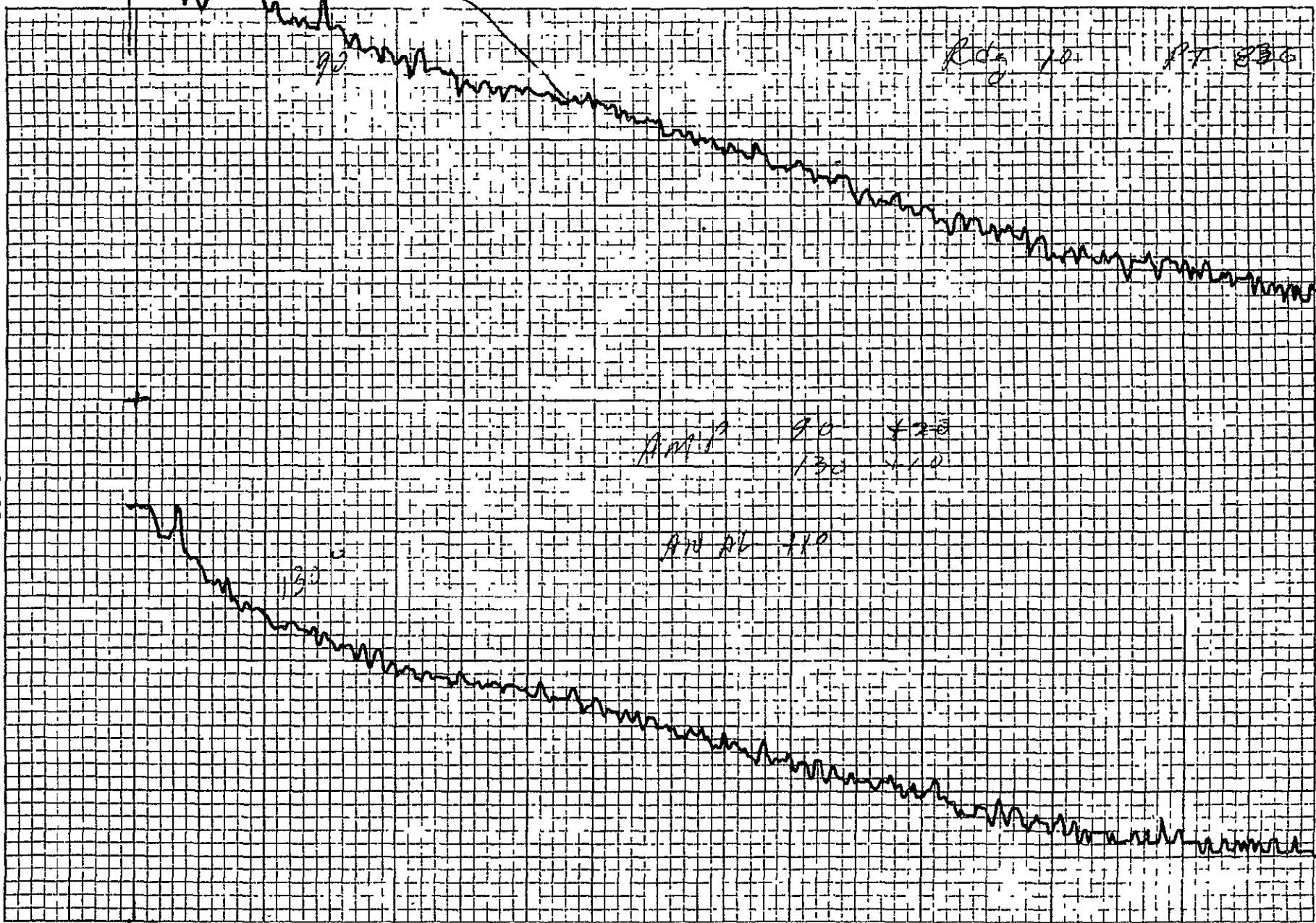
130

1638

528

0 10 20 30 40 50 60 70 80

K 4/2



4-7-75

PLG 30

AT 837

90°

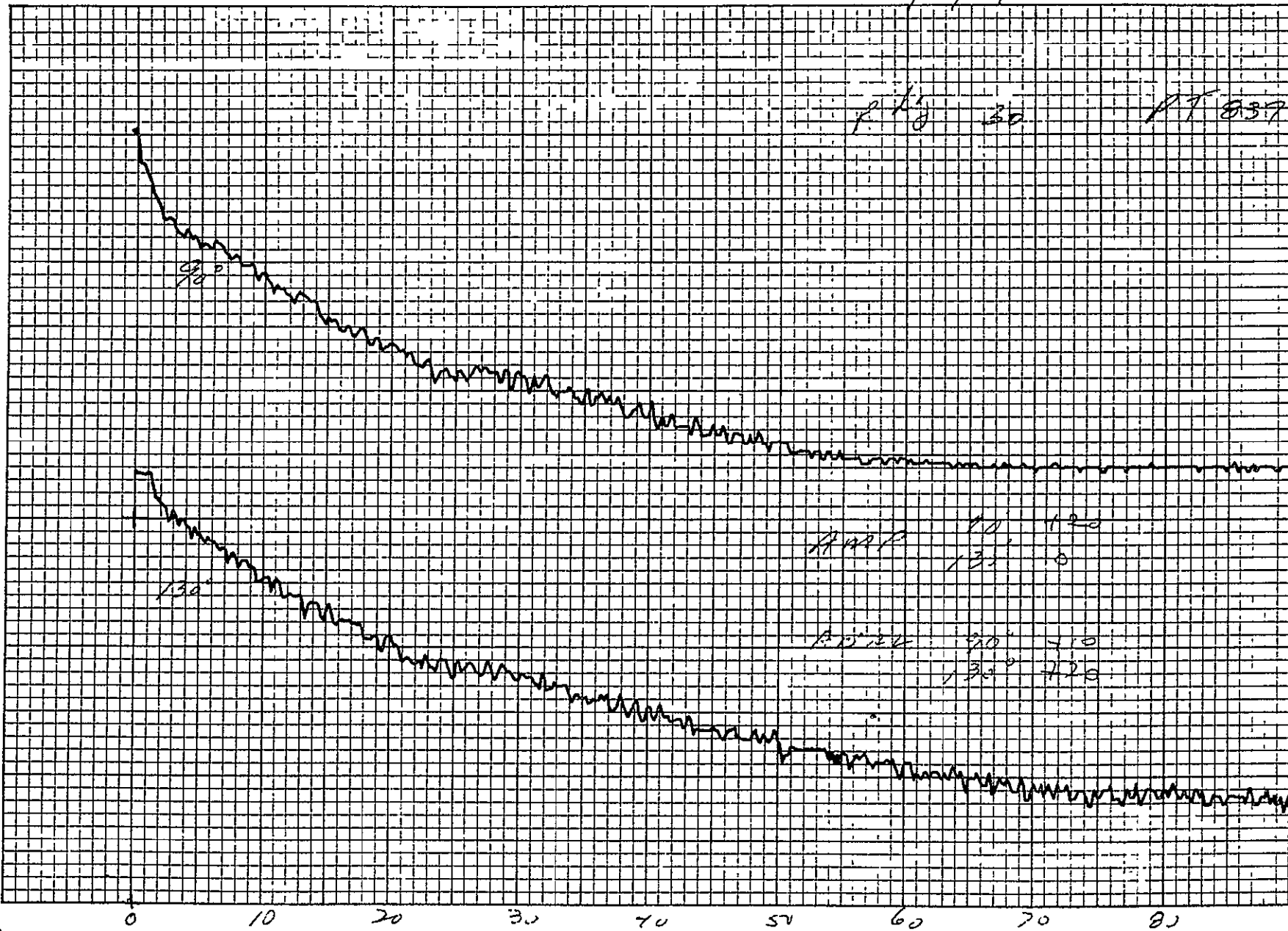
130°

PLG	10	120
	130	0

PLG	20	410
	30	720

1639

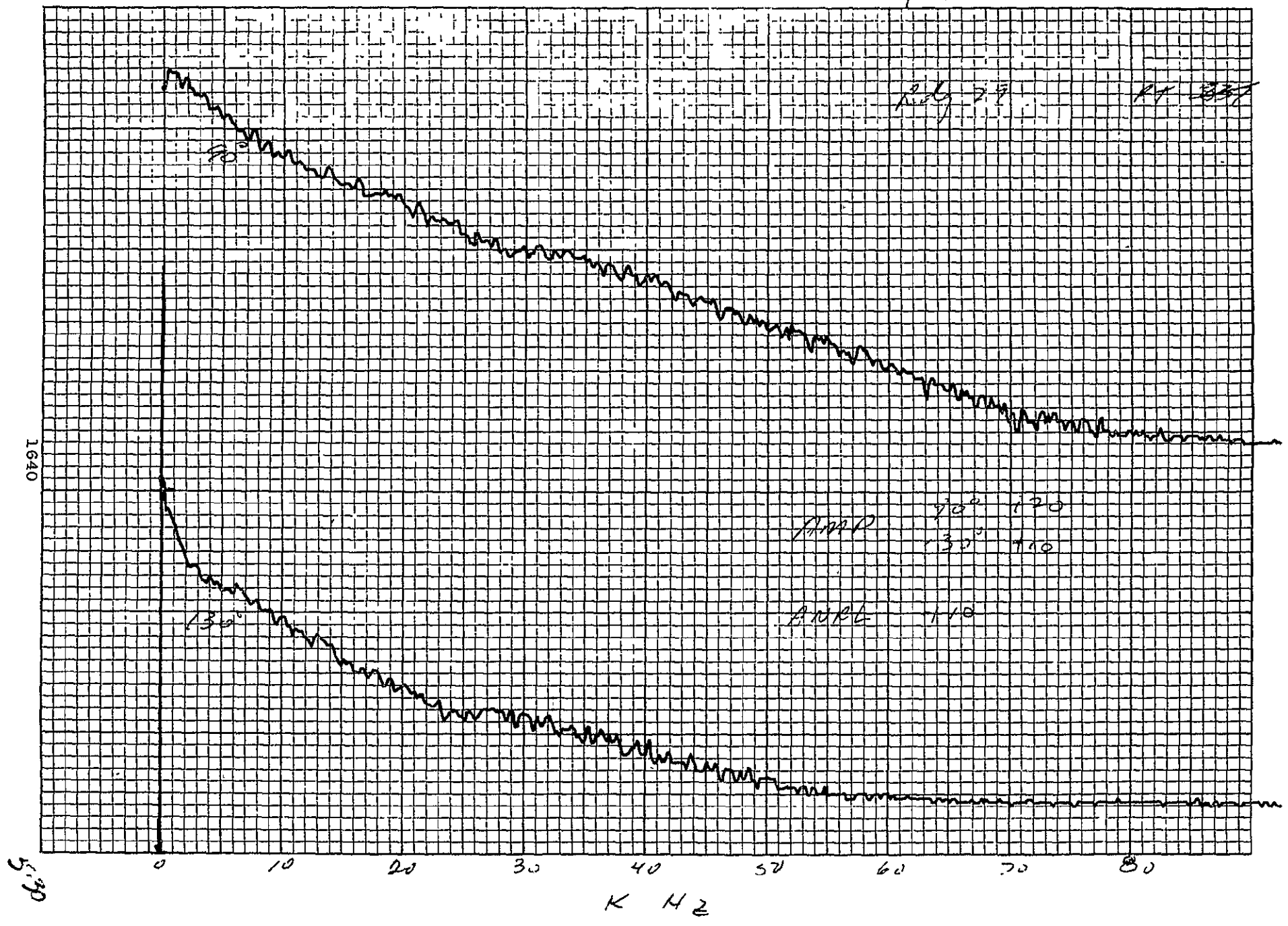
529



K 112

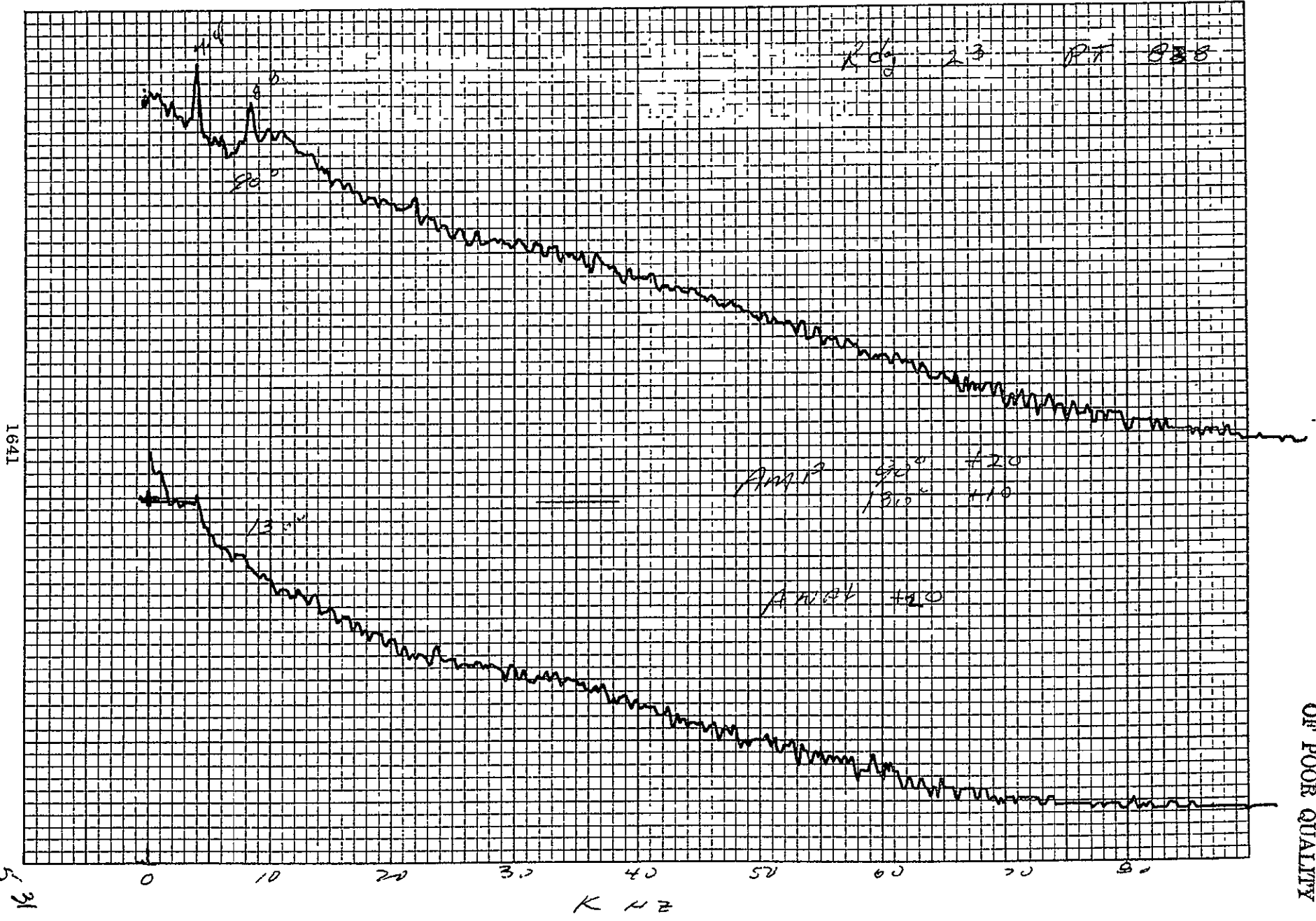
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4-7-75



4-7-75

K_{dg} 23 RT 888



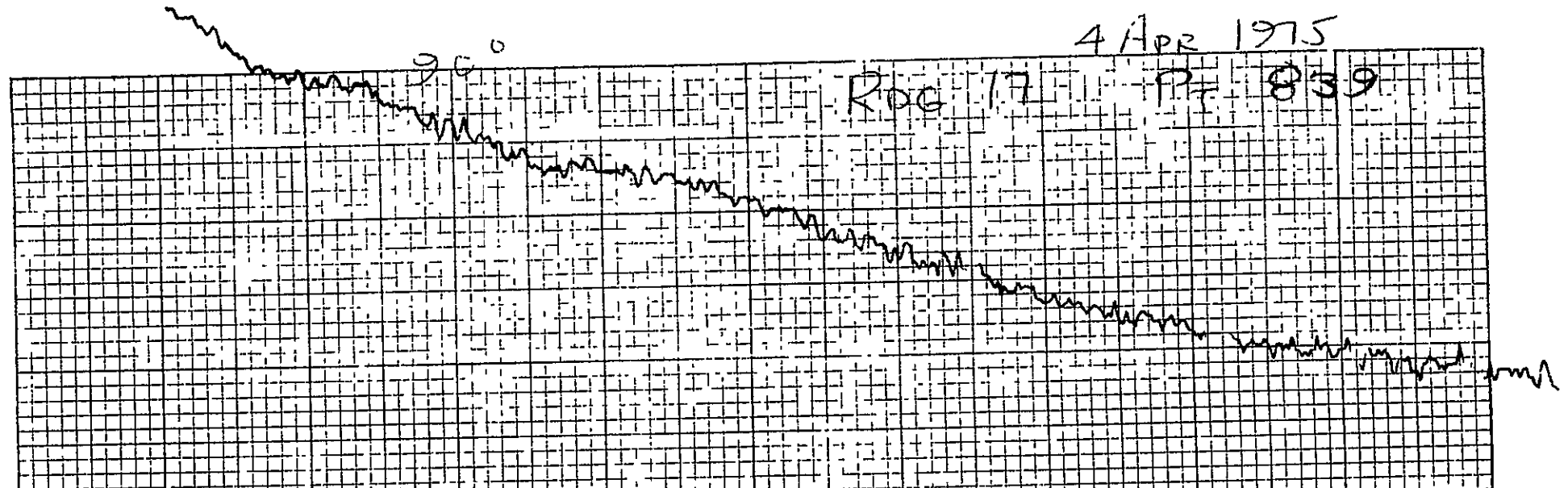
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4 Apr 1975

ROC 17

P# 839

90°



AMPL 90° +10
130° 0

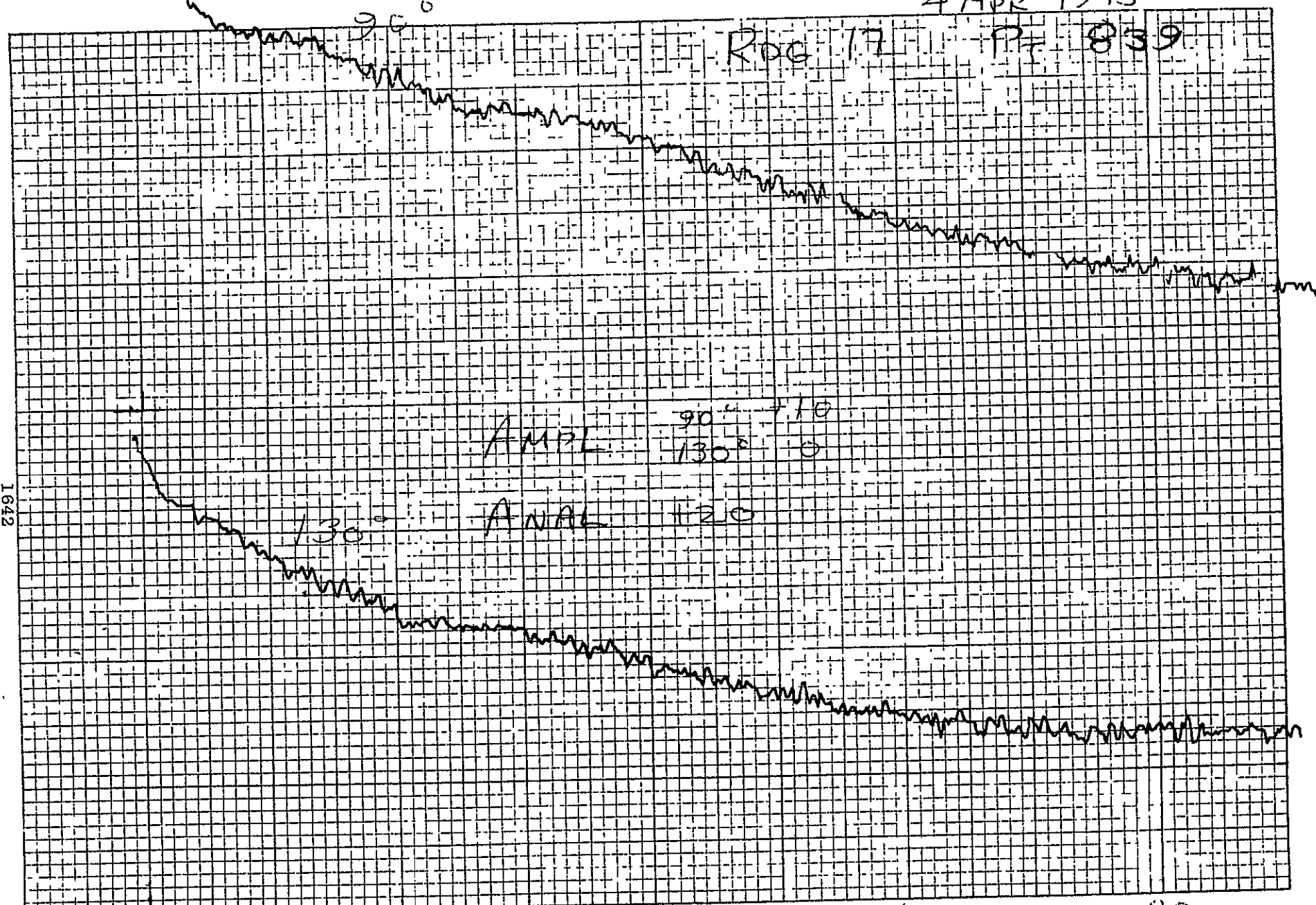
ANAL H₂O

130°

1642

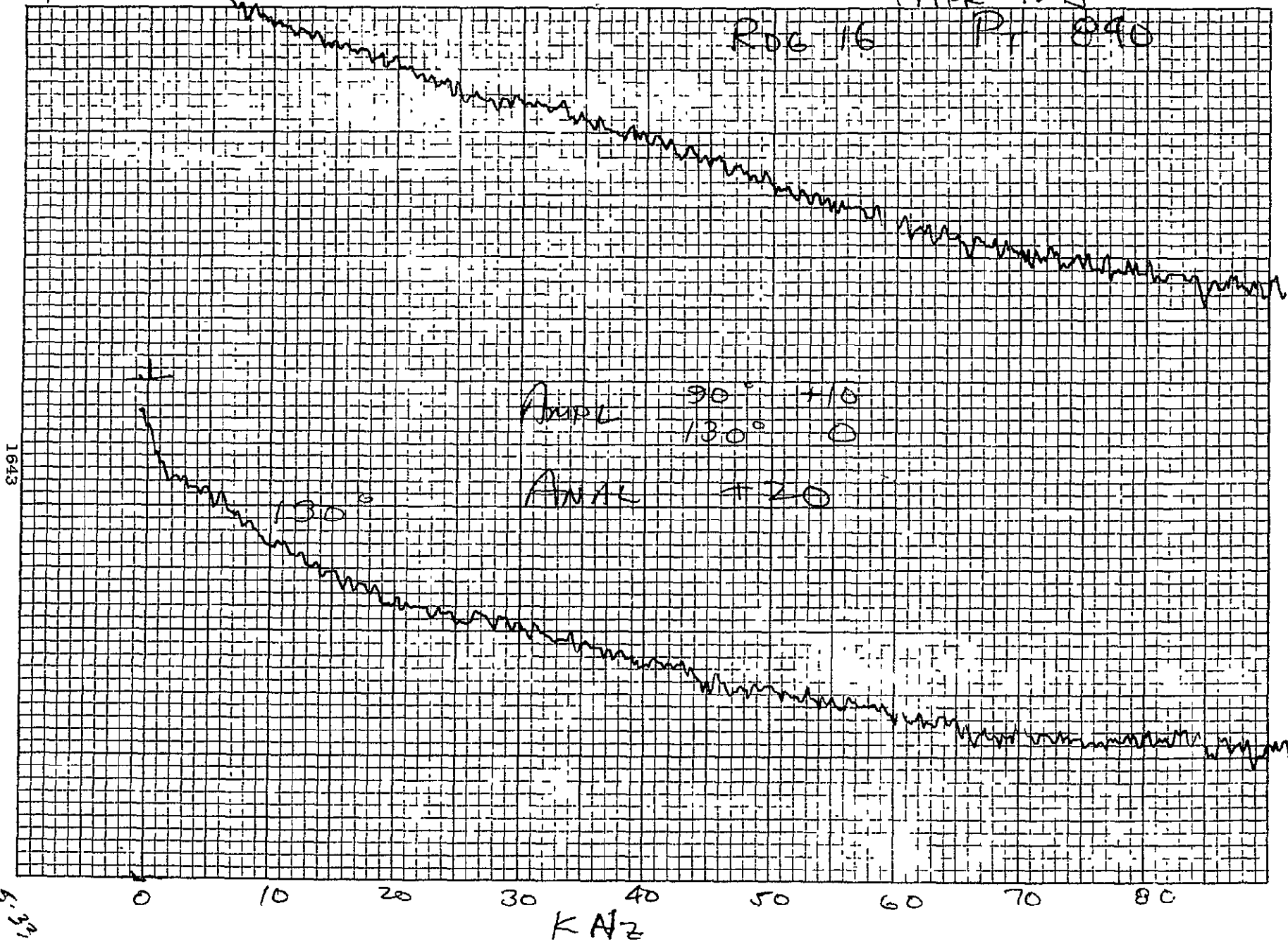
131

0 10 20 30 40 50 60 70 80
KHz



4 APR 1975

ROC 16 P. 890



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4 Apr 1975

RDG 14 PF 80

90°

AMPL 90° +10
 130° +0
 AMPL #10

90°

130°

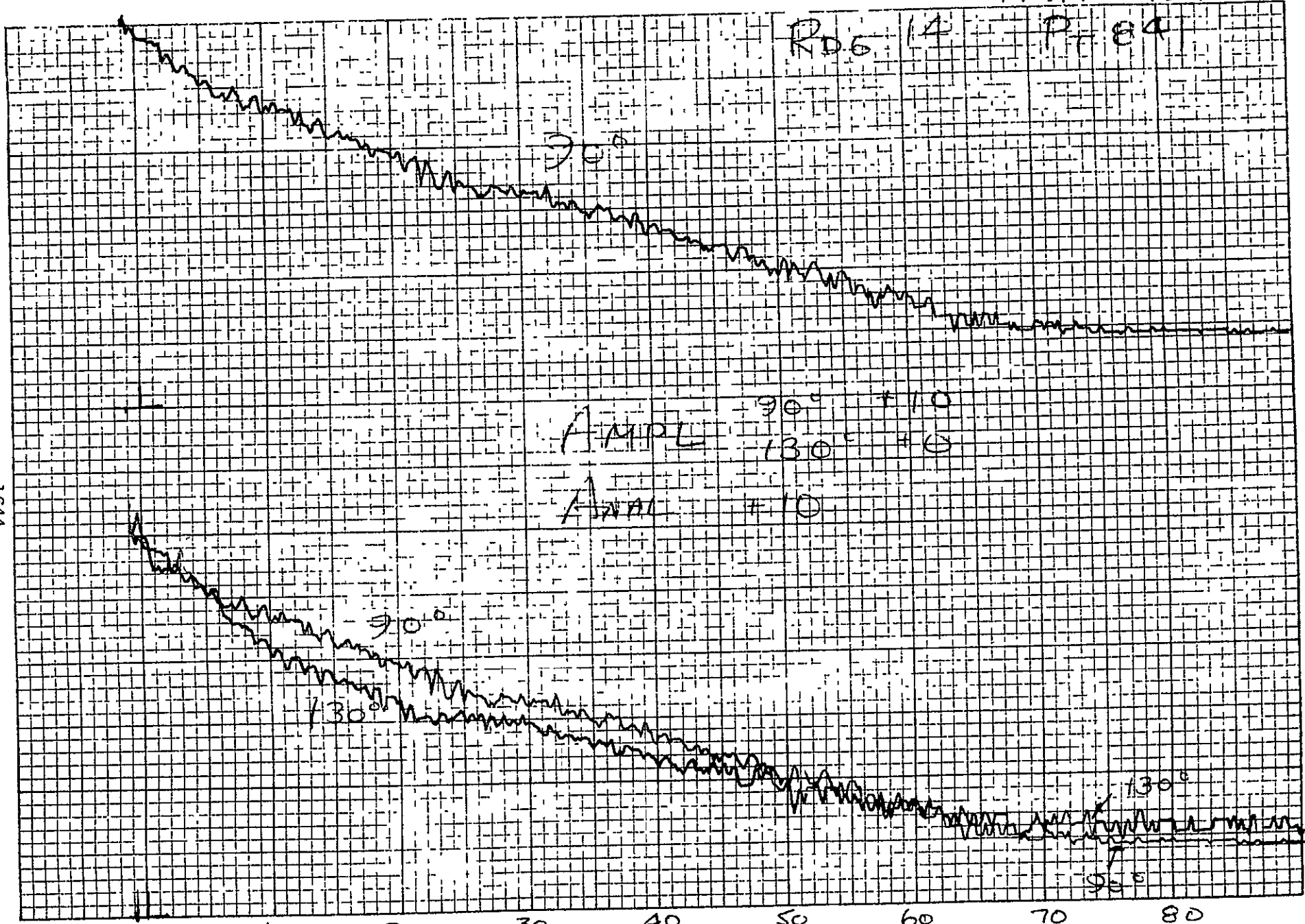
130°

90°

1644

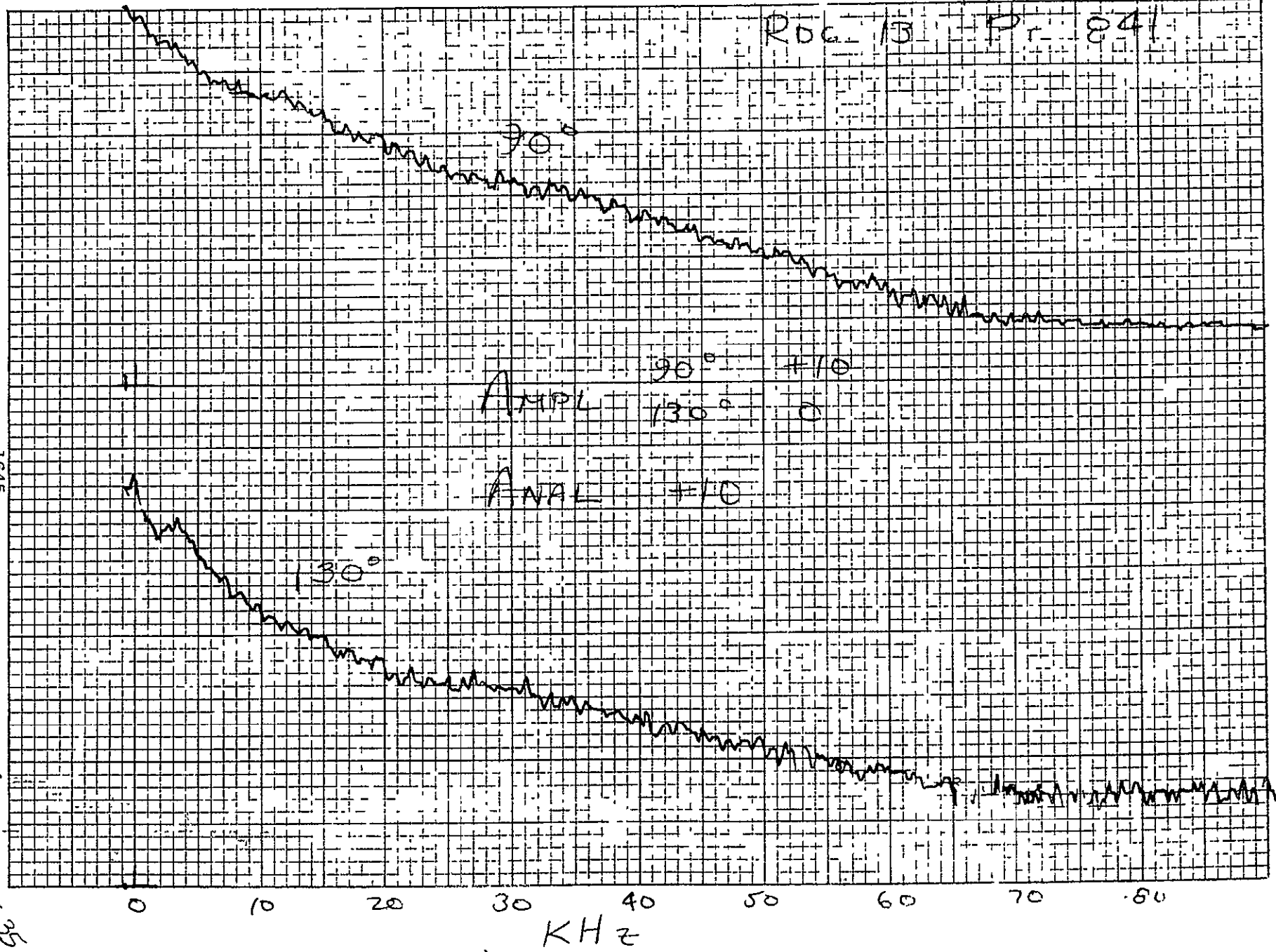
Fig 9

70 10 20 30 40 50 60 70 80
KHz



4 APR 1975

ROG-13 Pr 841

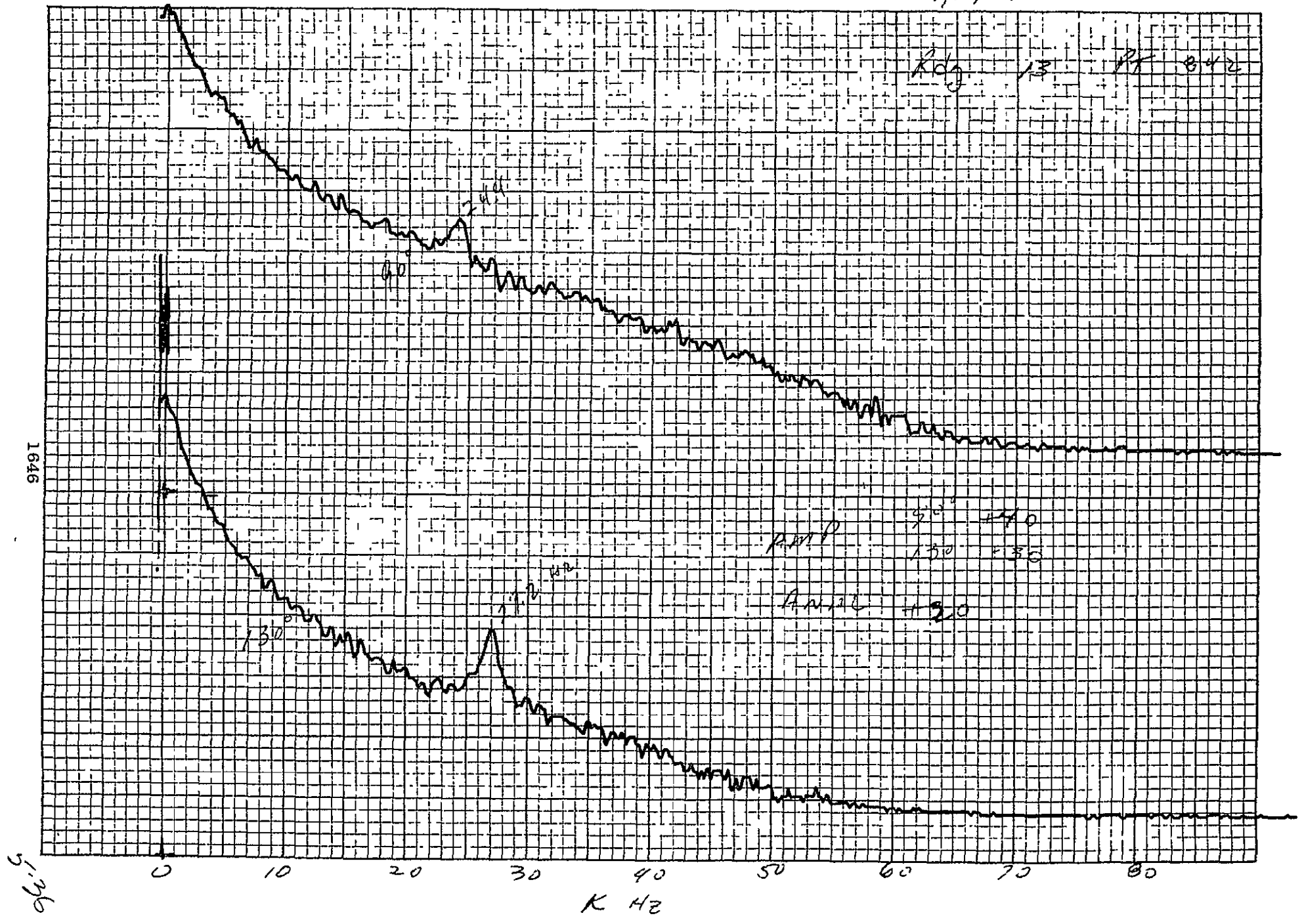


5-35

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4-7-75

K₀₃ 13 P₁ 842



K.M.P. 4.0
1.30
A.M.P. 1.35
1.20

4-7-75

Rdg 6

PT 843

90

29.12

1647

130

AMPL

90

+30

130

+30

AMPL

90

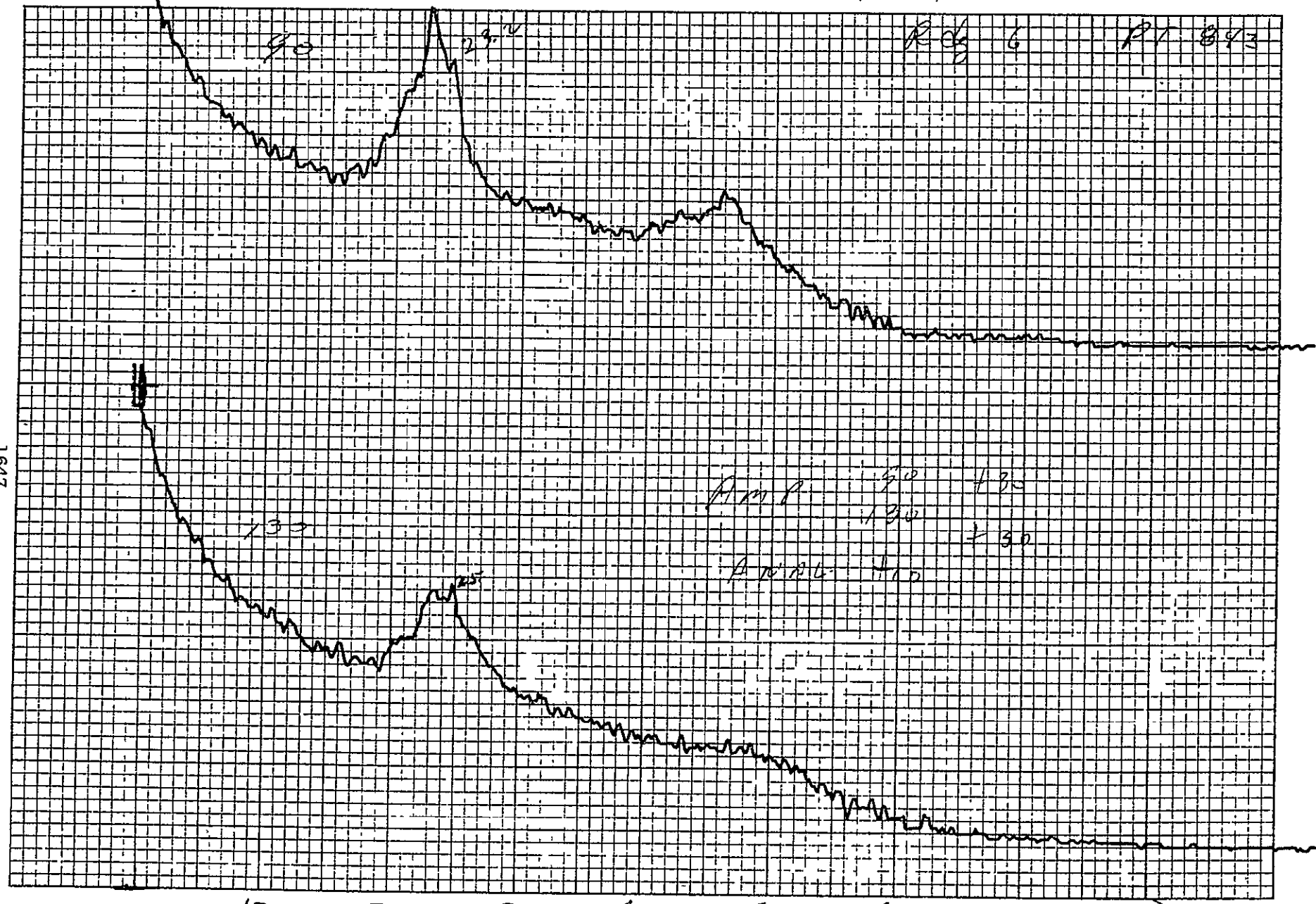
+30

5.97

0 10 20 30 40 50 60 70 80

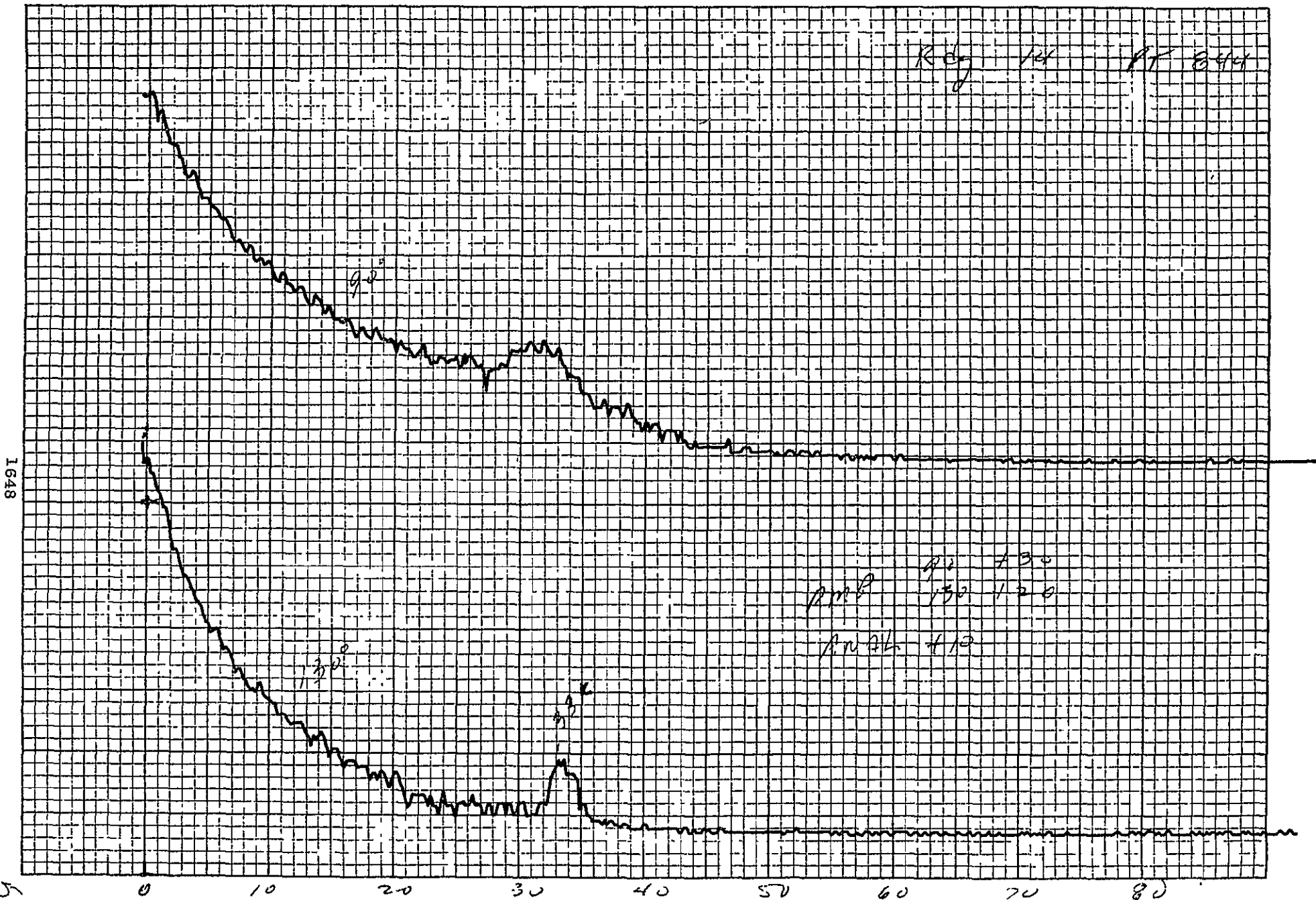
KHz

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4-7-75

Reg 14 RT 844



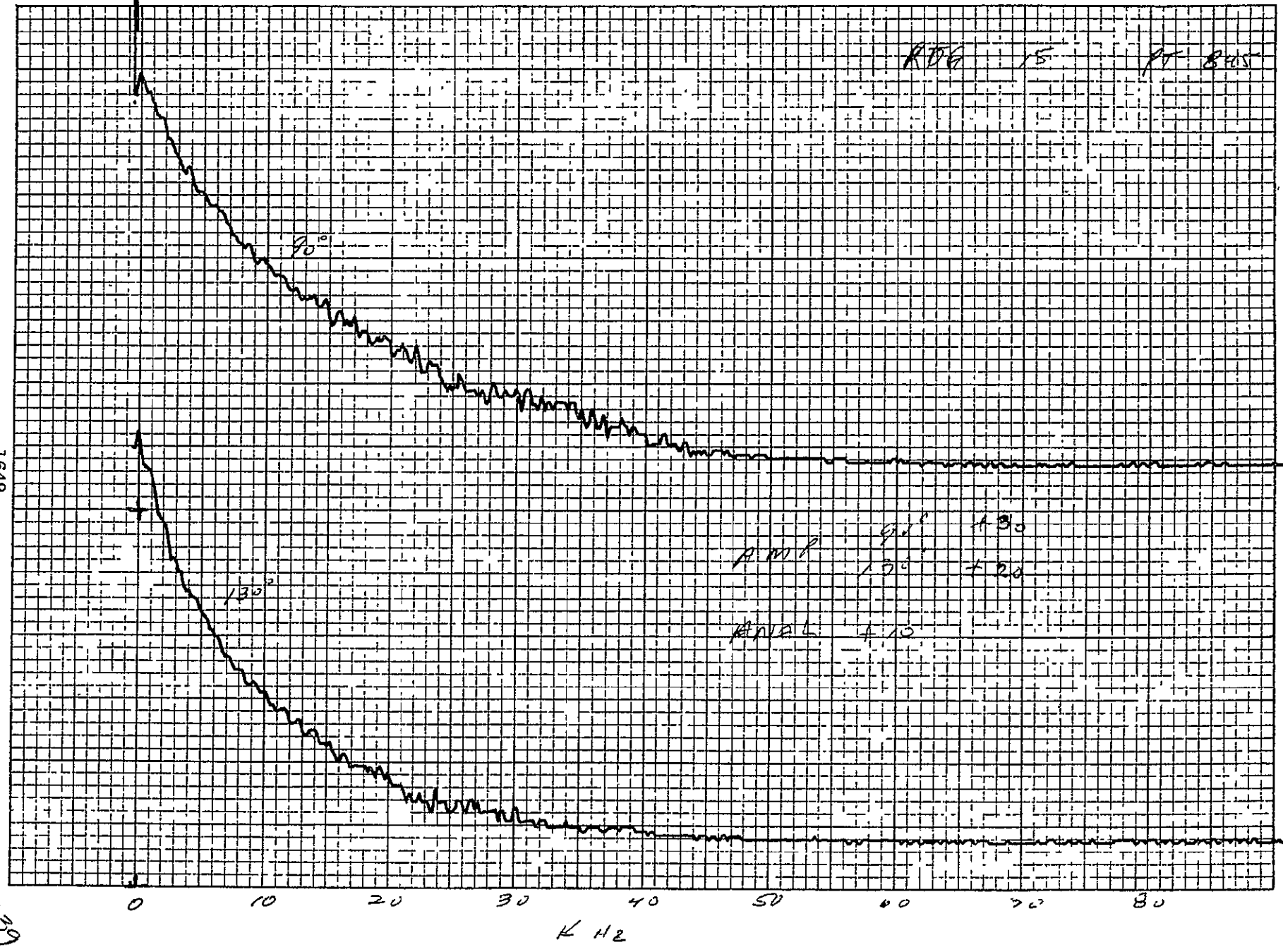
5-28

4-7-75

RDG 15 FT 8405

1649

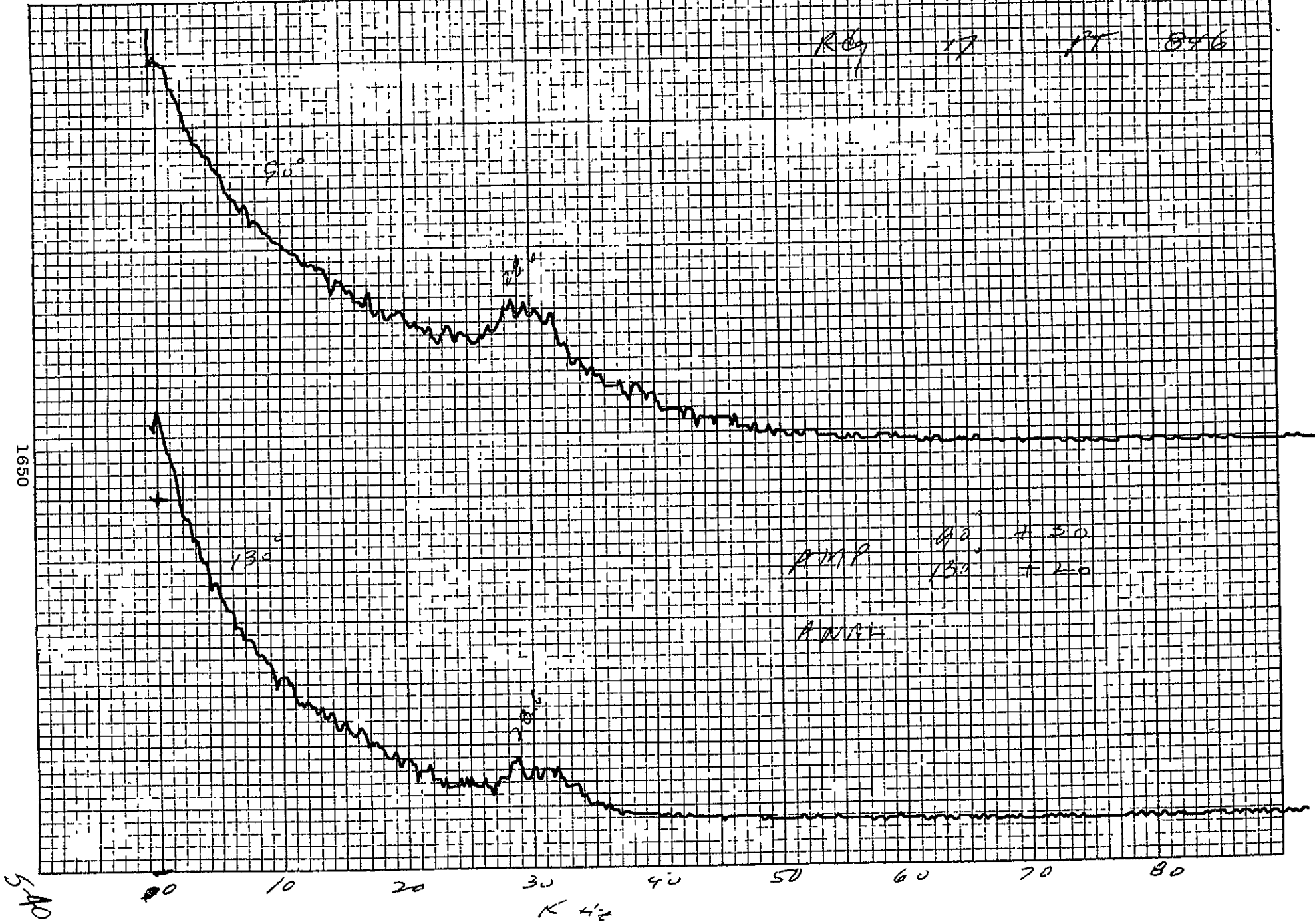
60-9



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4-7-75

Reg 17 PT 896



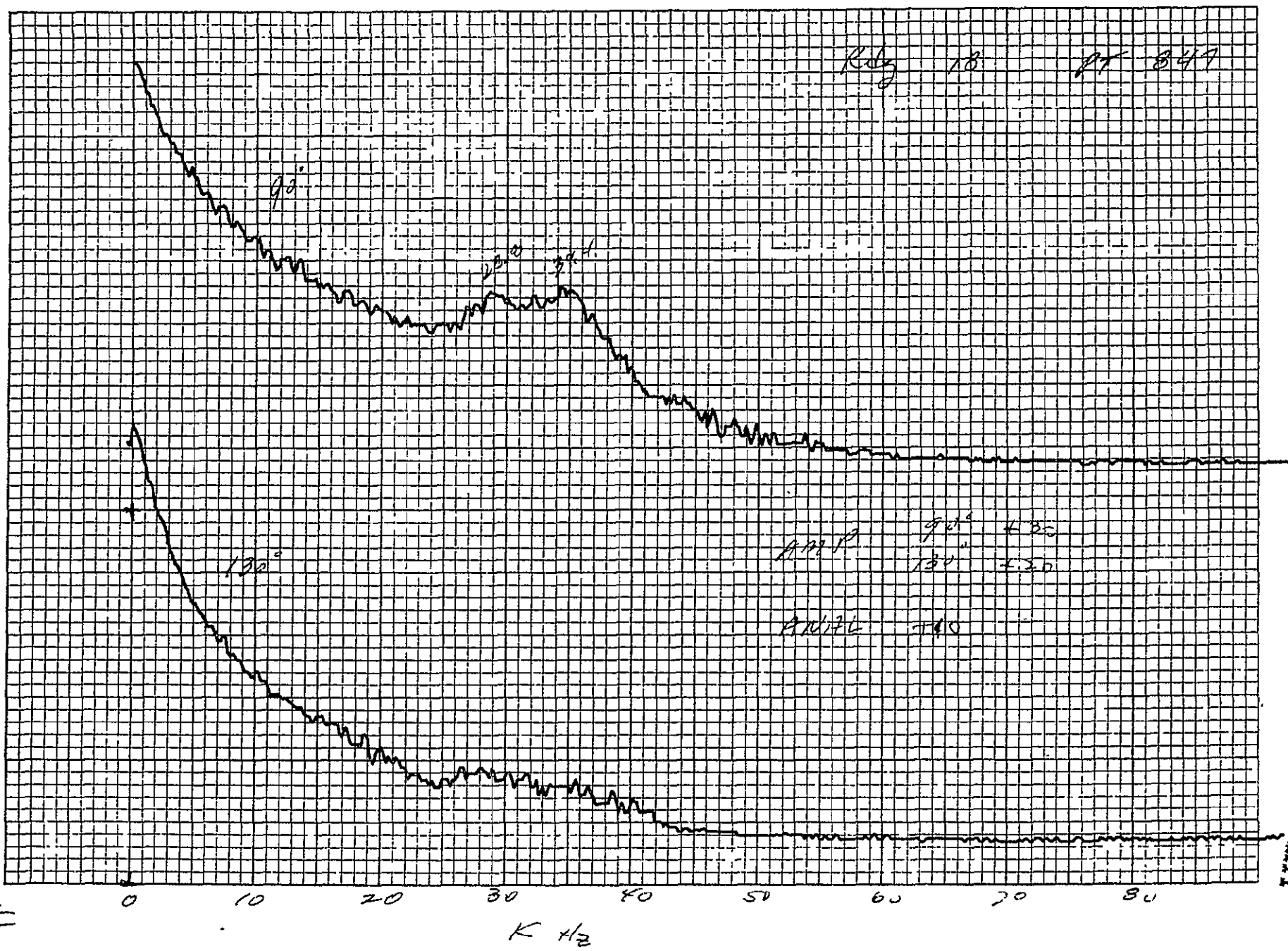
5 AD

4-7-75

Rdy 18 RT 847

1651

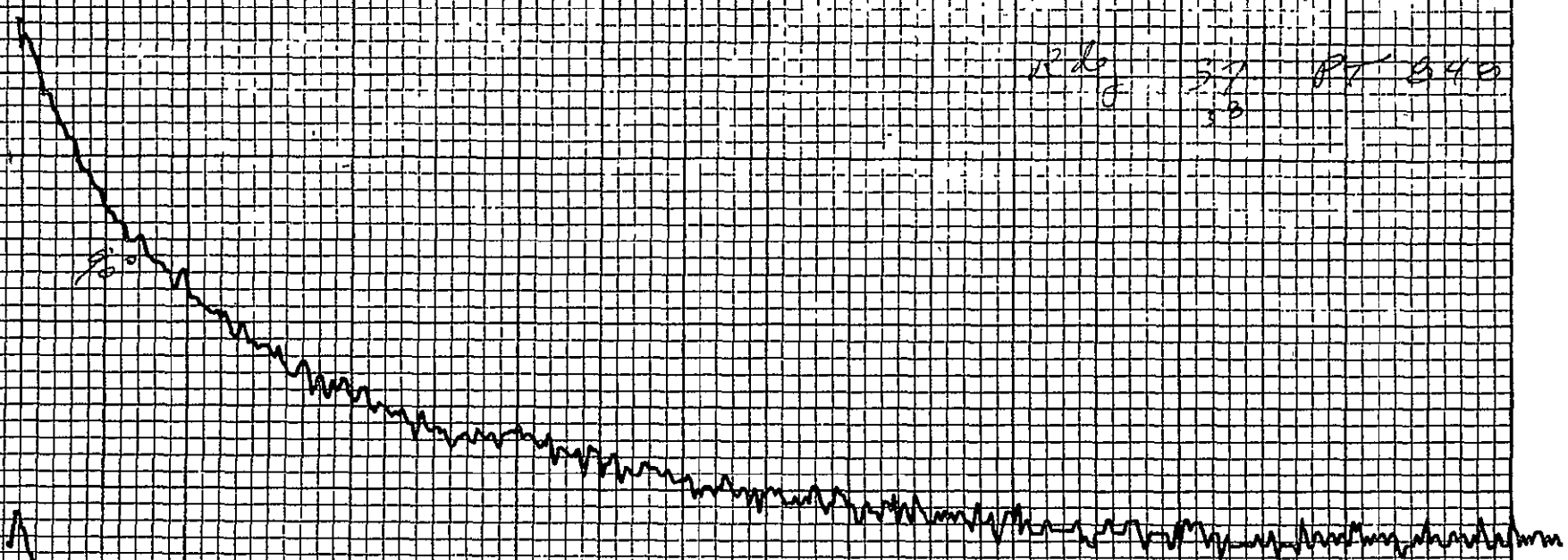
5.411



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4-7-75

side 57 840
58



1652

AWP 90° 420
130° 710



AWAL 90° 100
130° 710

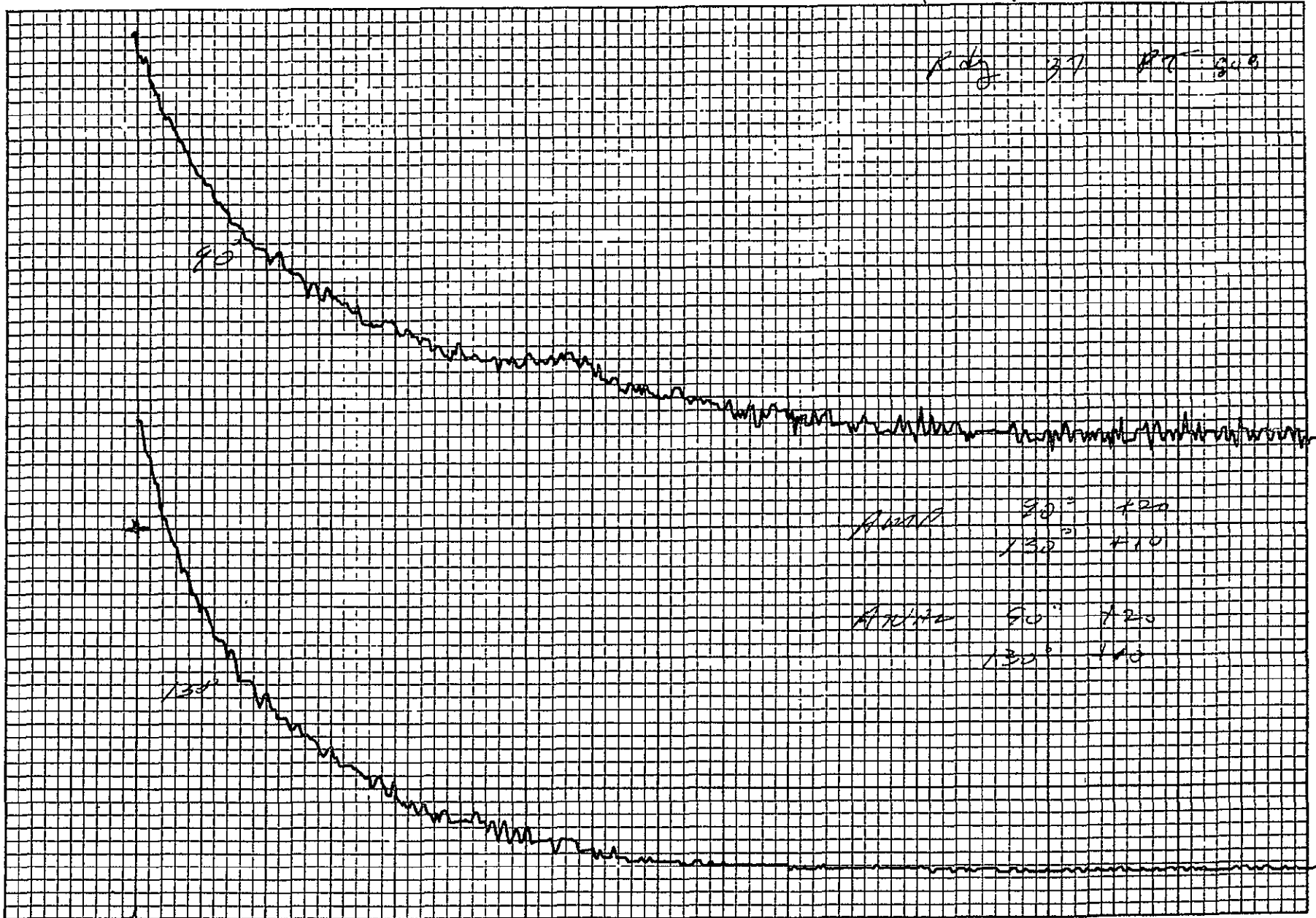
542

0 20 40 60 80

4-7-75

Adj. 37 80-90

1653



AMP 90° 120
 130° 110
 AMP 90° 120
 130° 110

5-11-75

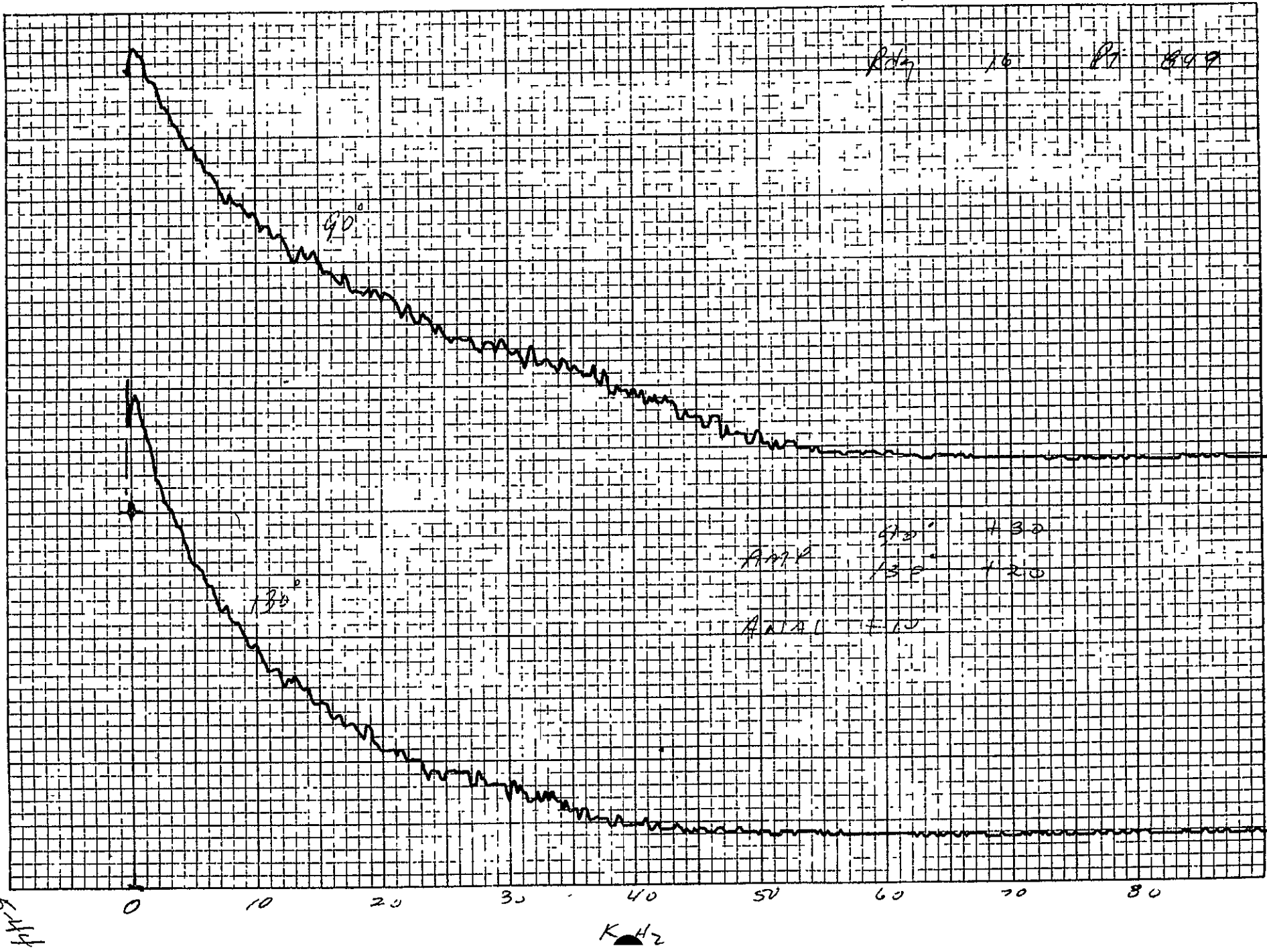
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4-7-75

Adg 16 Pt 1999

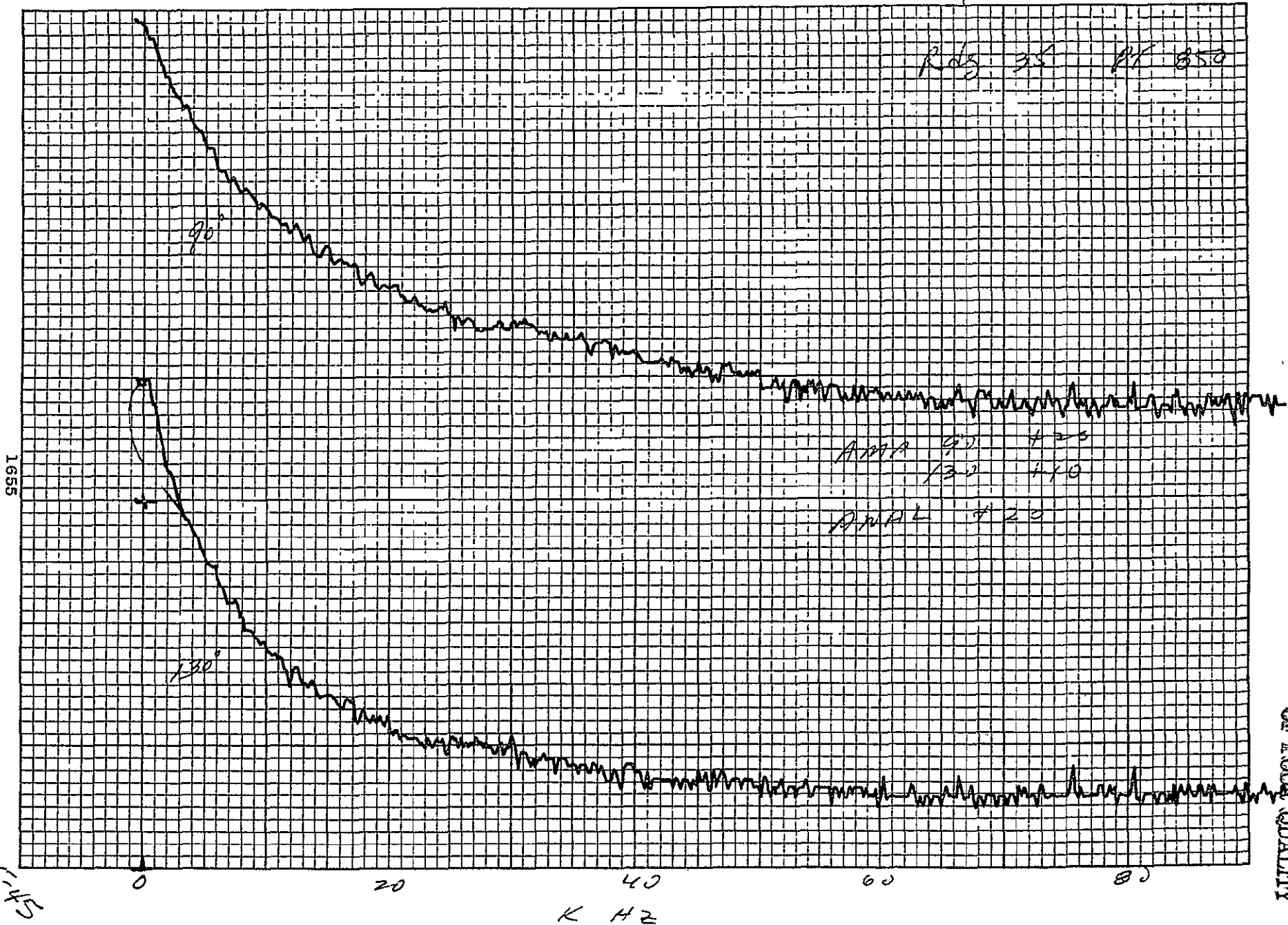
1654

5 kHz



4-7-75

Rds 35 RT 850



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4-7-75

Adj 34 PR 851

90°

20.2

1656

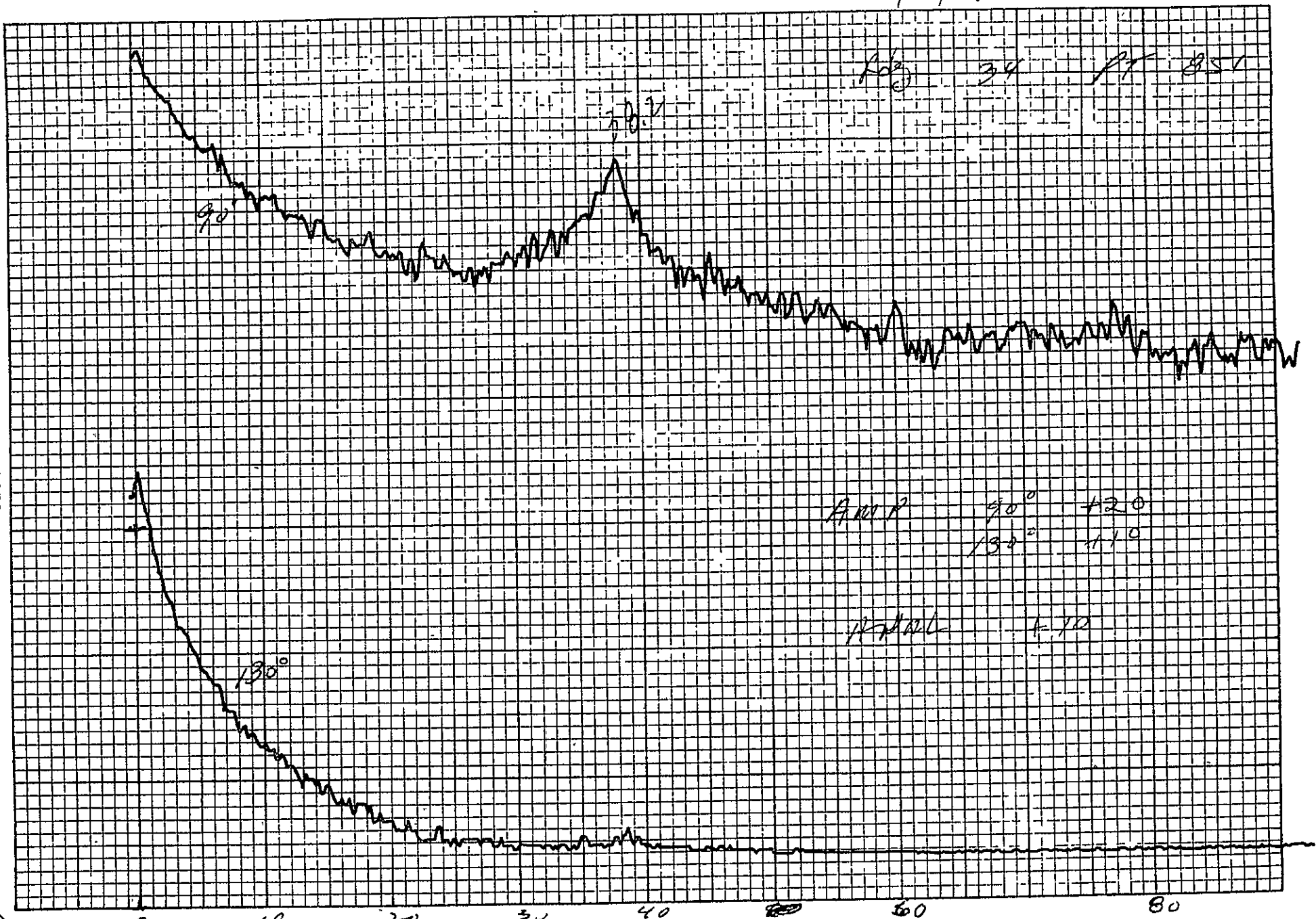
ARRR 90° +20
130° +10

ARRR +10

130°

5-46

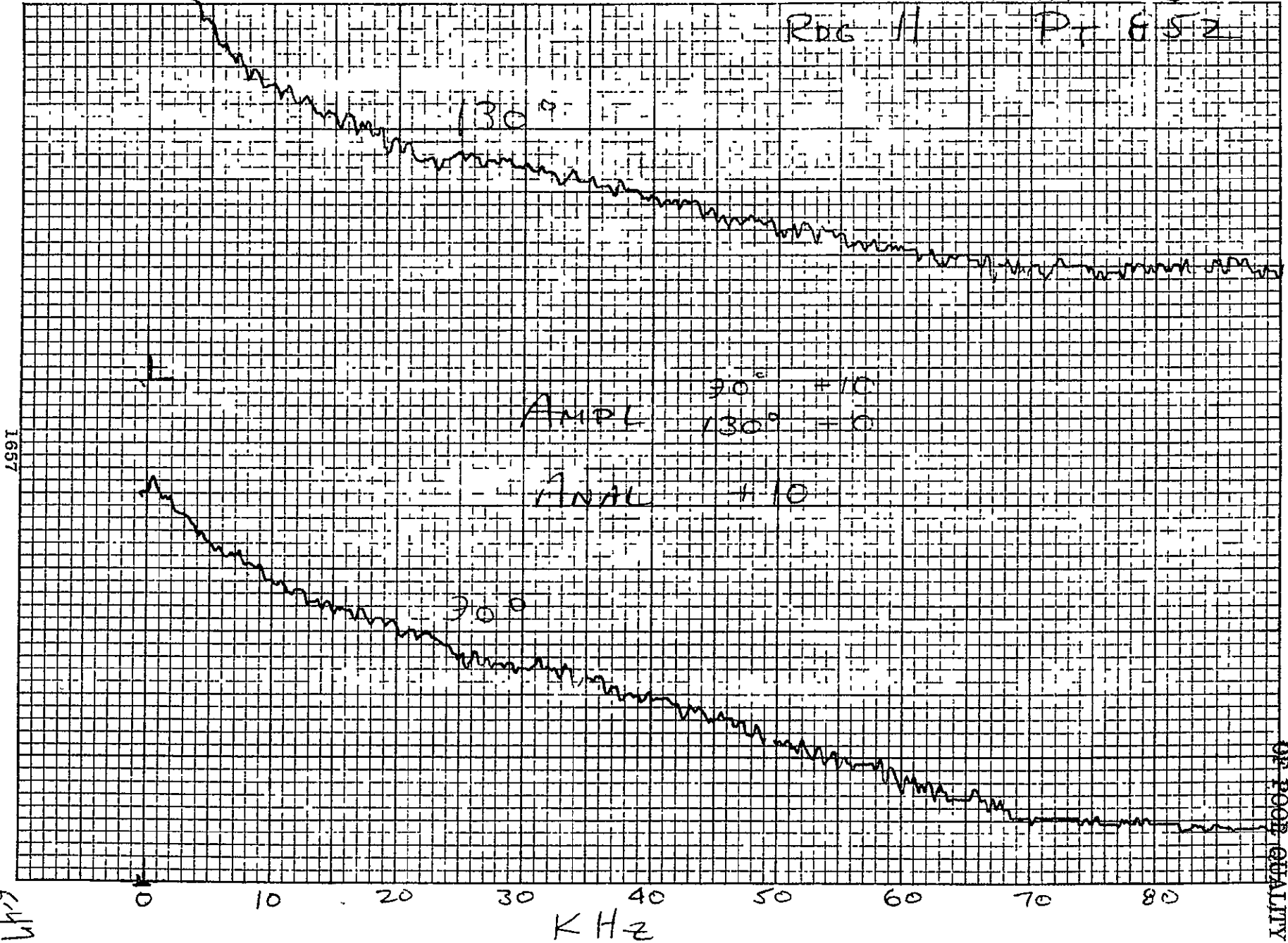
KHz



4 Apr 1975

Rdg II

Pt 852

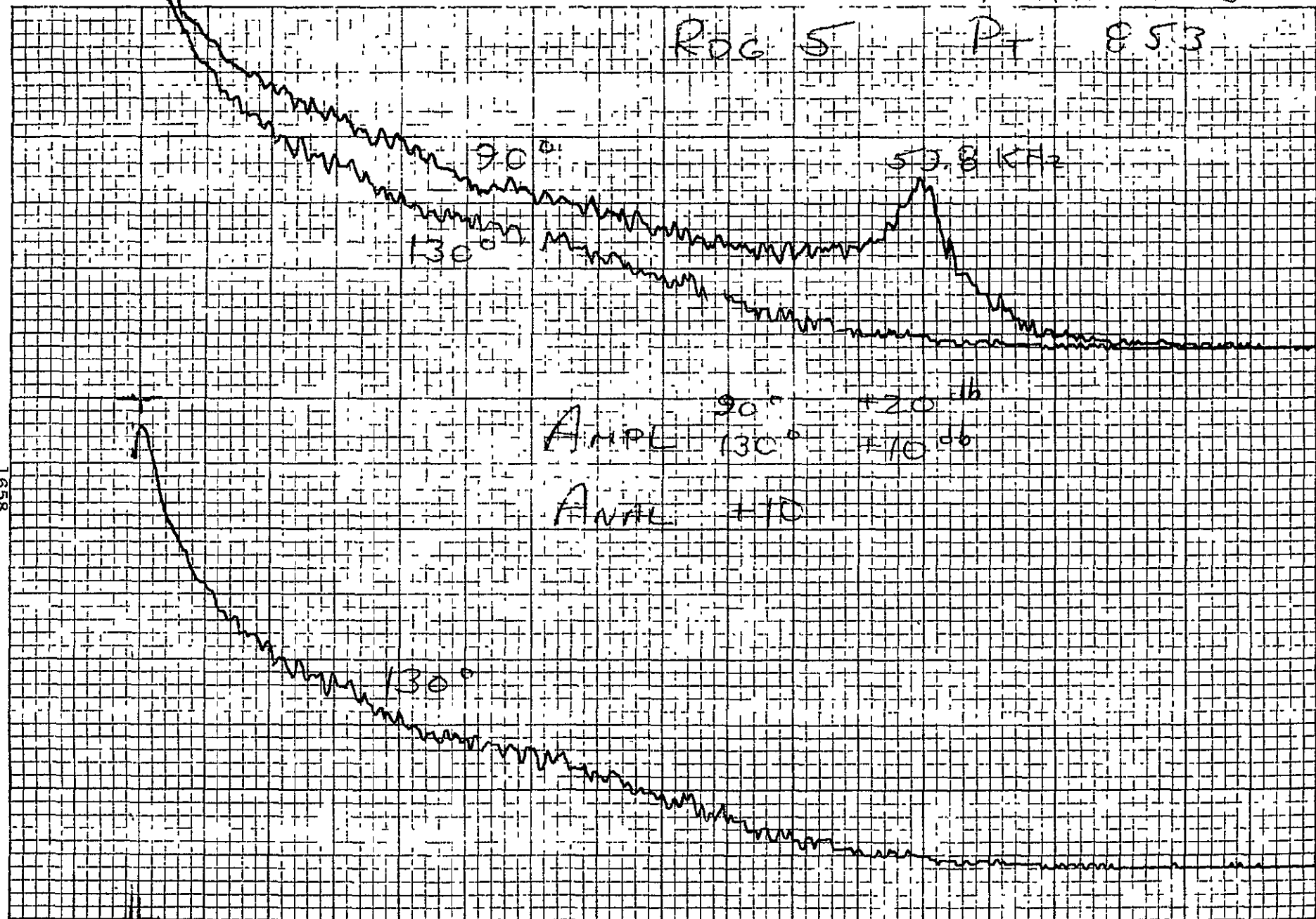


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4 APR 1975

ROC 5

Pt 853



1658

5-V

KHz

4 APR 1975

RDG 2 P 854

90°

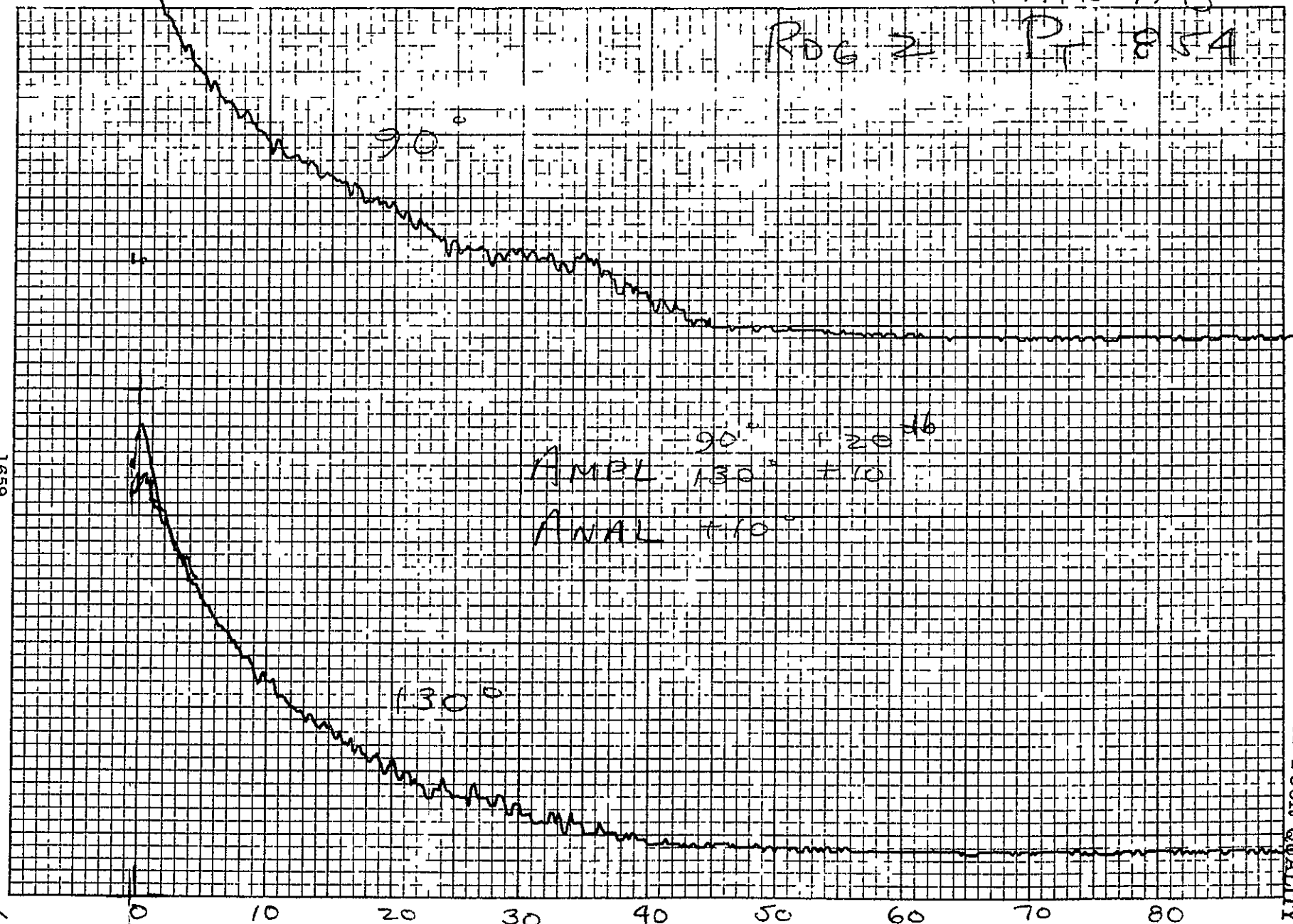
90° ± 20 dB
ANAL 130° ± 10
ANAL ± 10°

130°

1659

5-19

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4 APR 1975

ROG 10 PR 8.55

130°

AMPL 90° 10 db
130° 0 db
ANAL +10

1660

550

0

10

20

30

K Hz

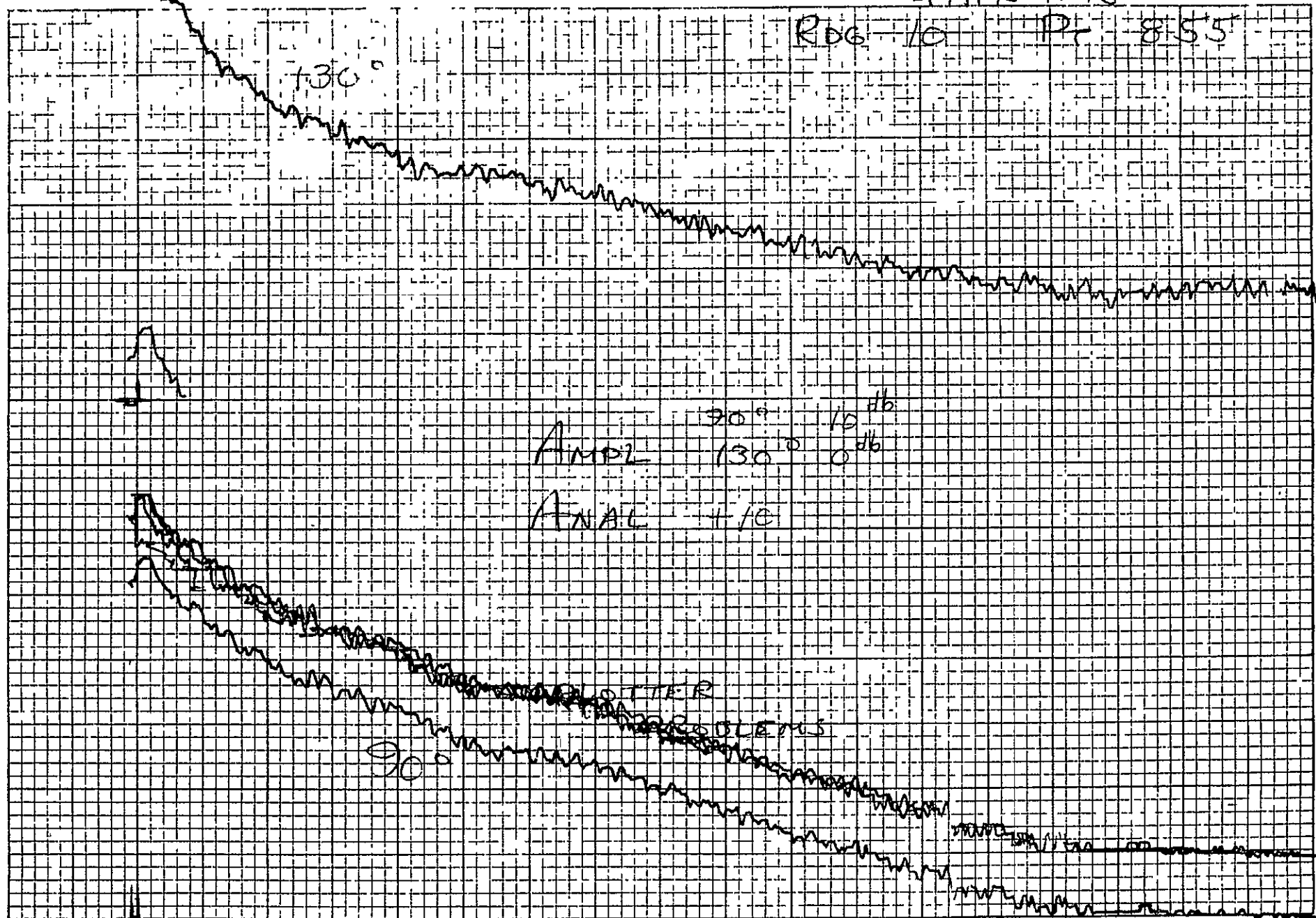
50

60

70

80

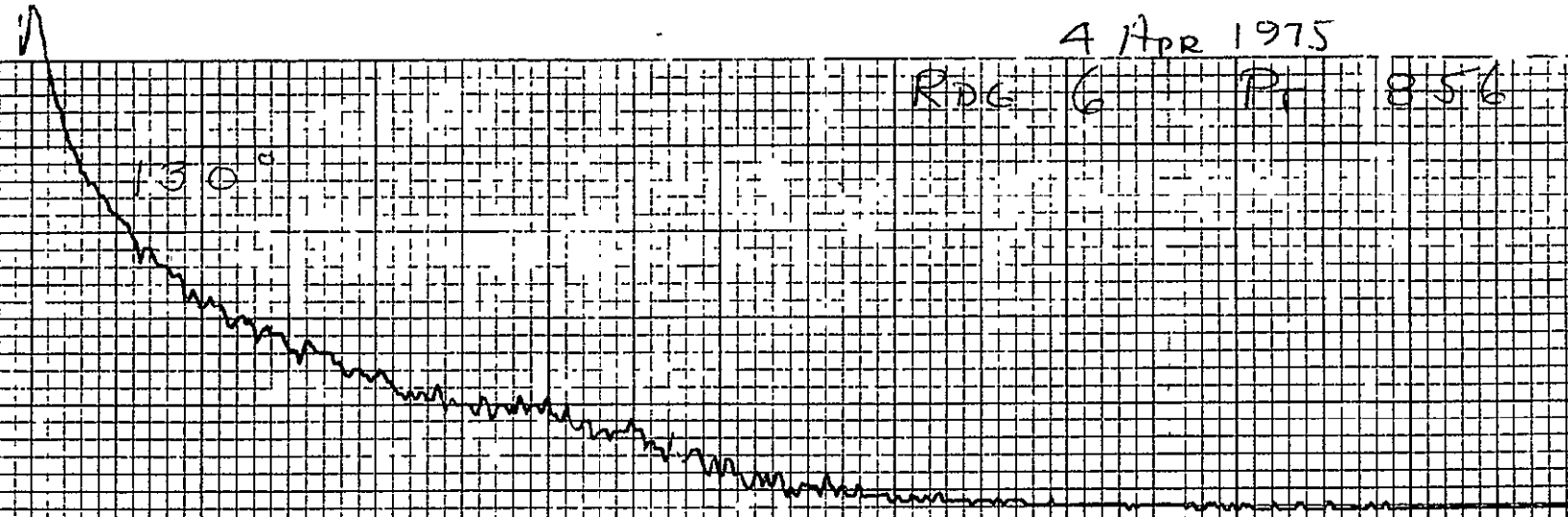
NOTTER
SOLEMS



4 Apr 1975

Rdg 6 P. 856

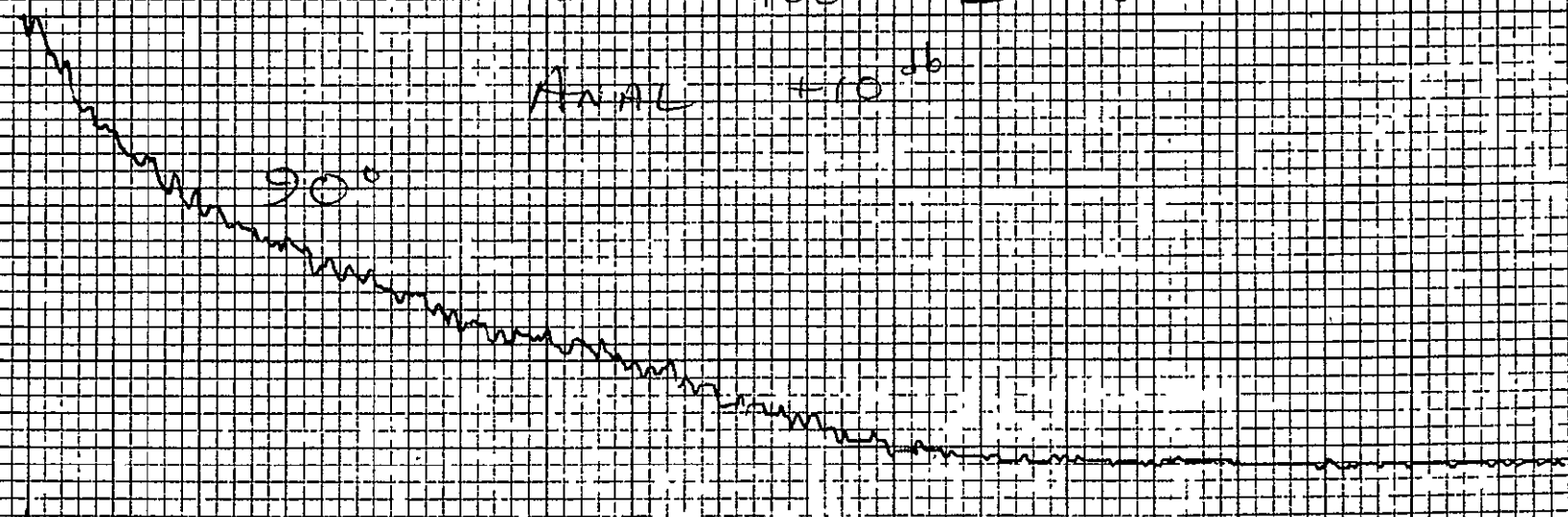
130°



1661

AMPL 30° = ~~30~~° = +10 db
130° = ~~30~~° = 0 db
ANAL +10 db

90°



551

0 10 20 30 40 50 60 70 80
K Hz

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4 Apr 1975

Rdg B

Pt 257

34.6 KHz

90°

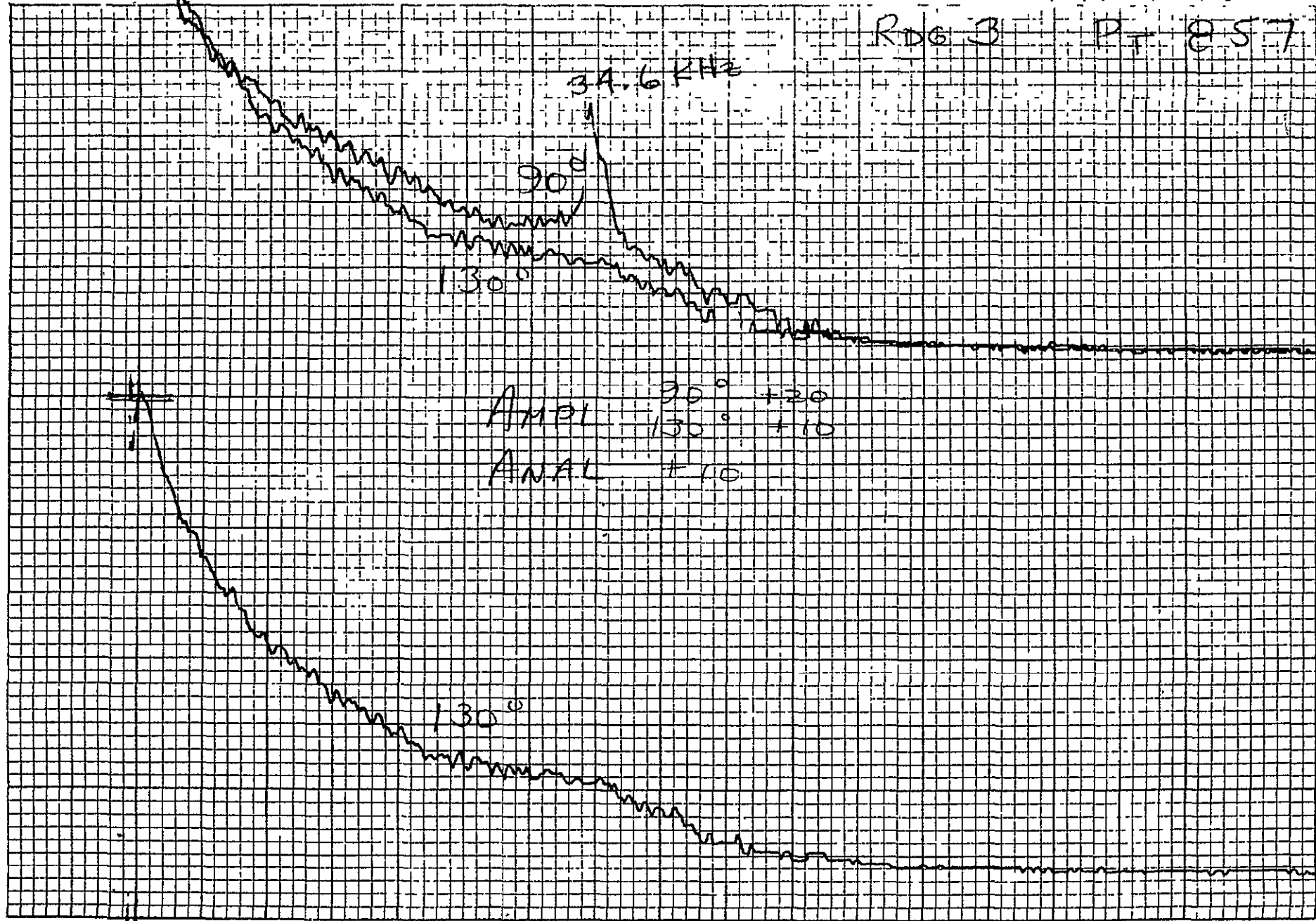
130°

AMPL 90° +20
130° +10
ANAL +10

130°

1662

552



4 APR 1975

ROC: 9 Pf: 858

90°

90°

+20

+10

1663

AMPL 90° 10 db
130° 0 db

ANAL 90° (+20 db) +10 db
130° +10 db

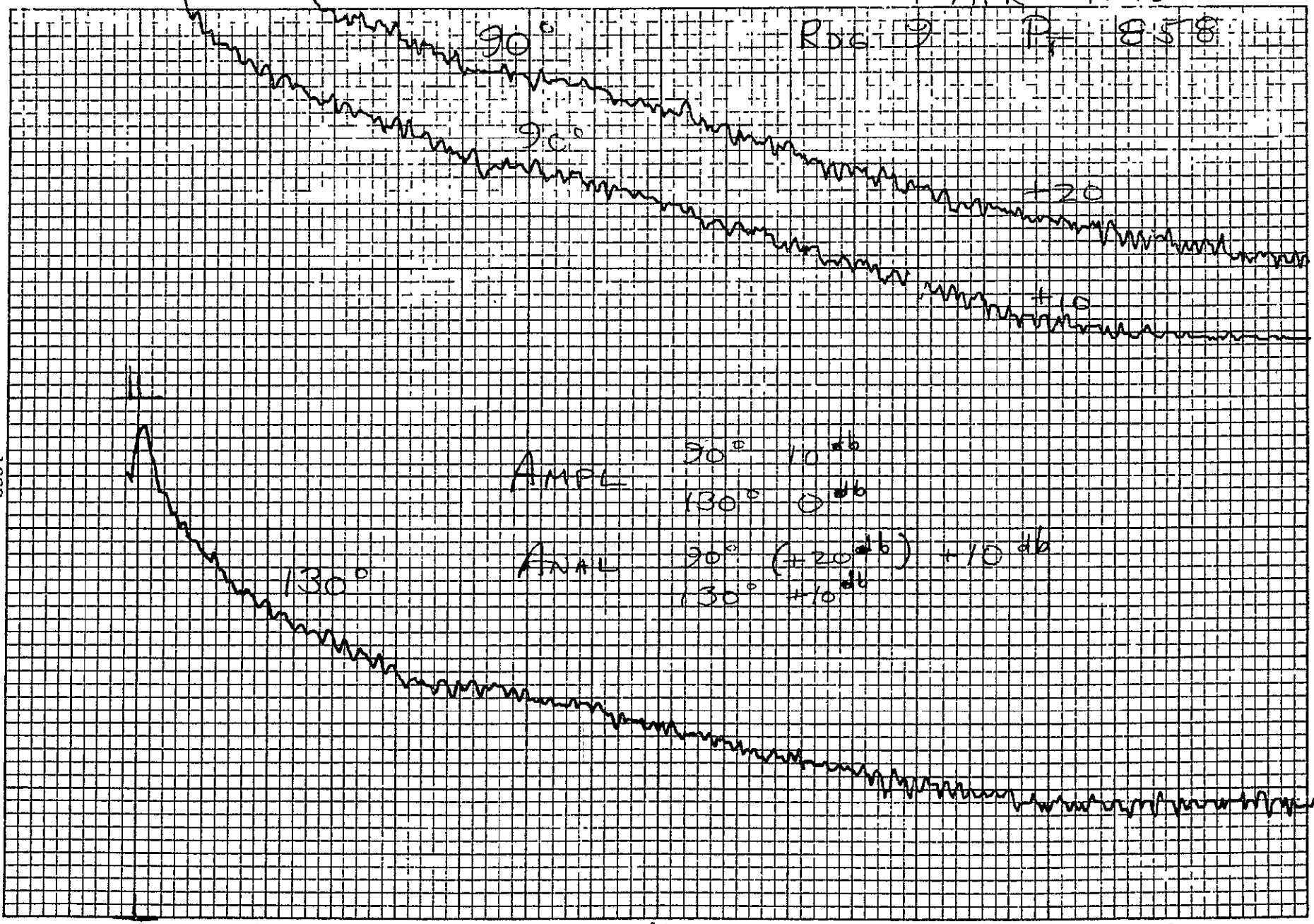
130°

5-53

0 10 20 30 40 50 60 70 80

KHz

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4 APR 1975

RDG 7 P. 859

130°

90°

AMPL

90° + 10 db

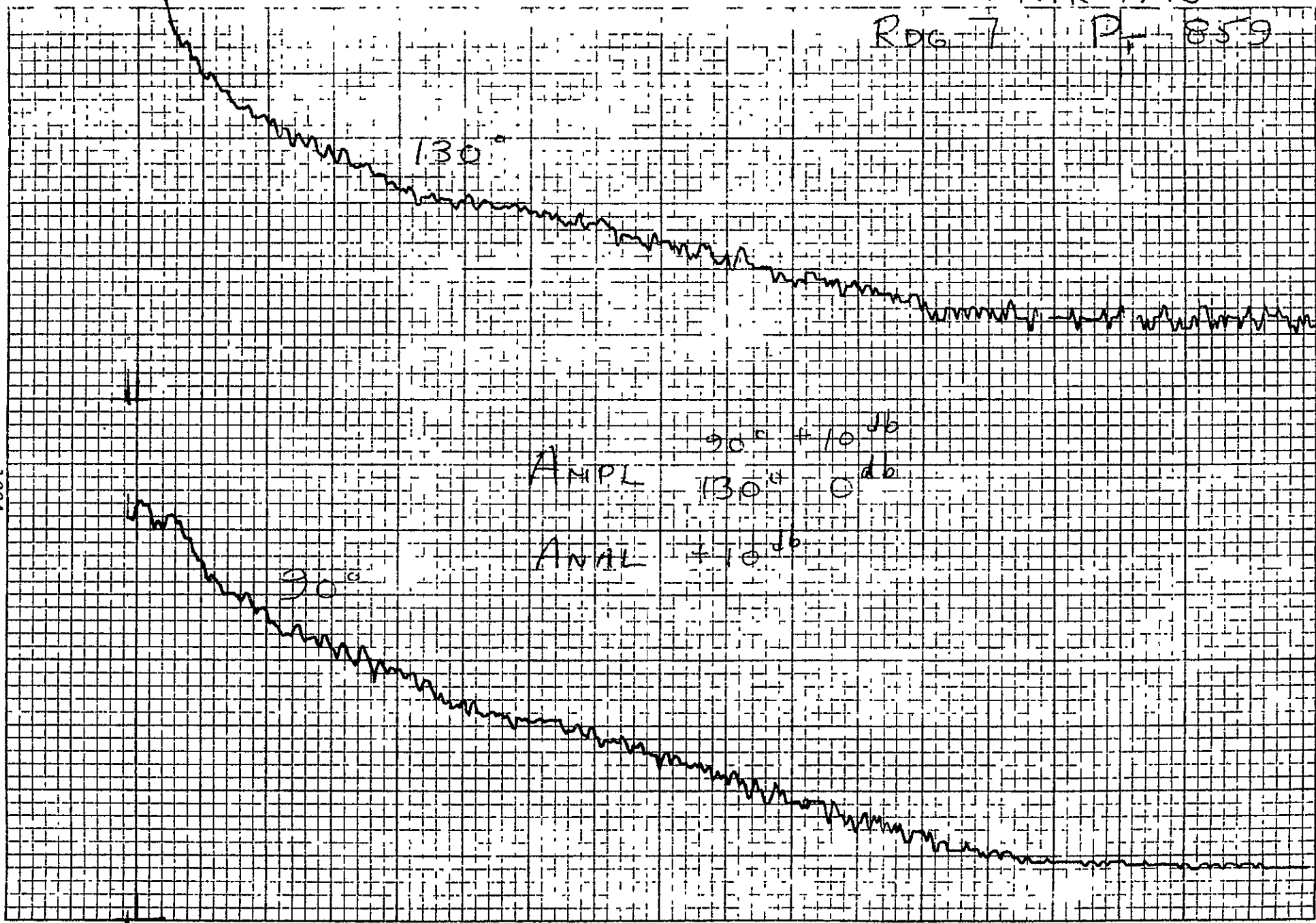
130° 0 db

ANAL

+ 10 db

1664

554



4-7-75

RDG 12 PF 859

90

Amplitude 90 ± 10
130 0

Amplitude 10

130

1.5

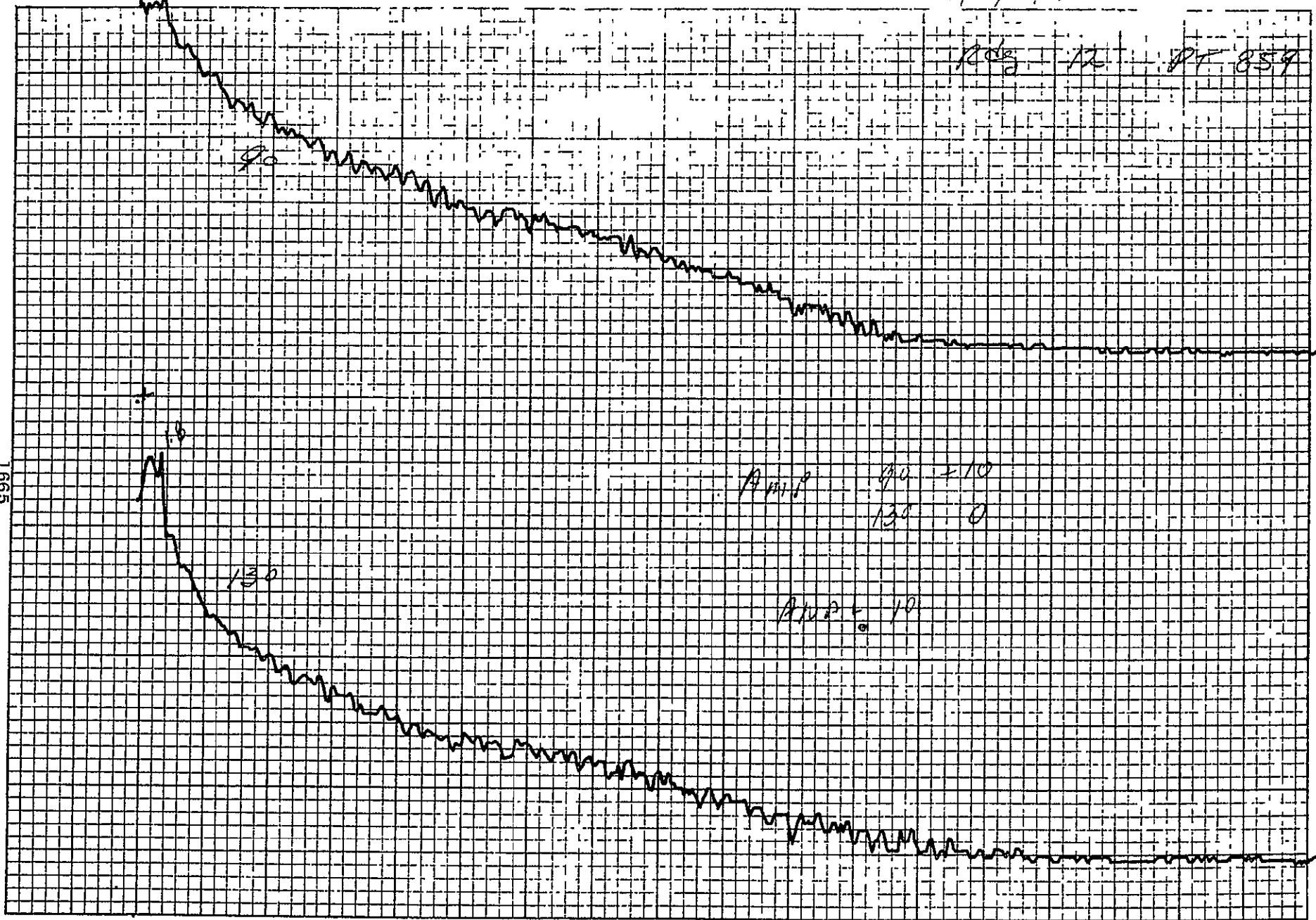
1665

5-55

0 10 20 30 40 50 60 70 80

KHz

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4 APR 1975

R DG. 4

Pt

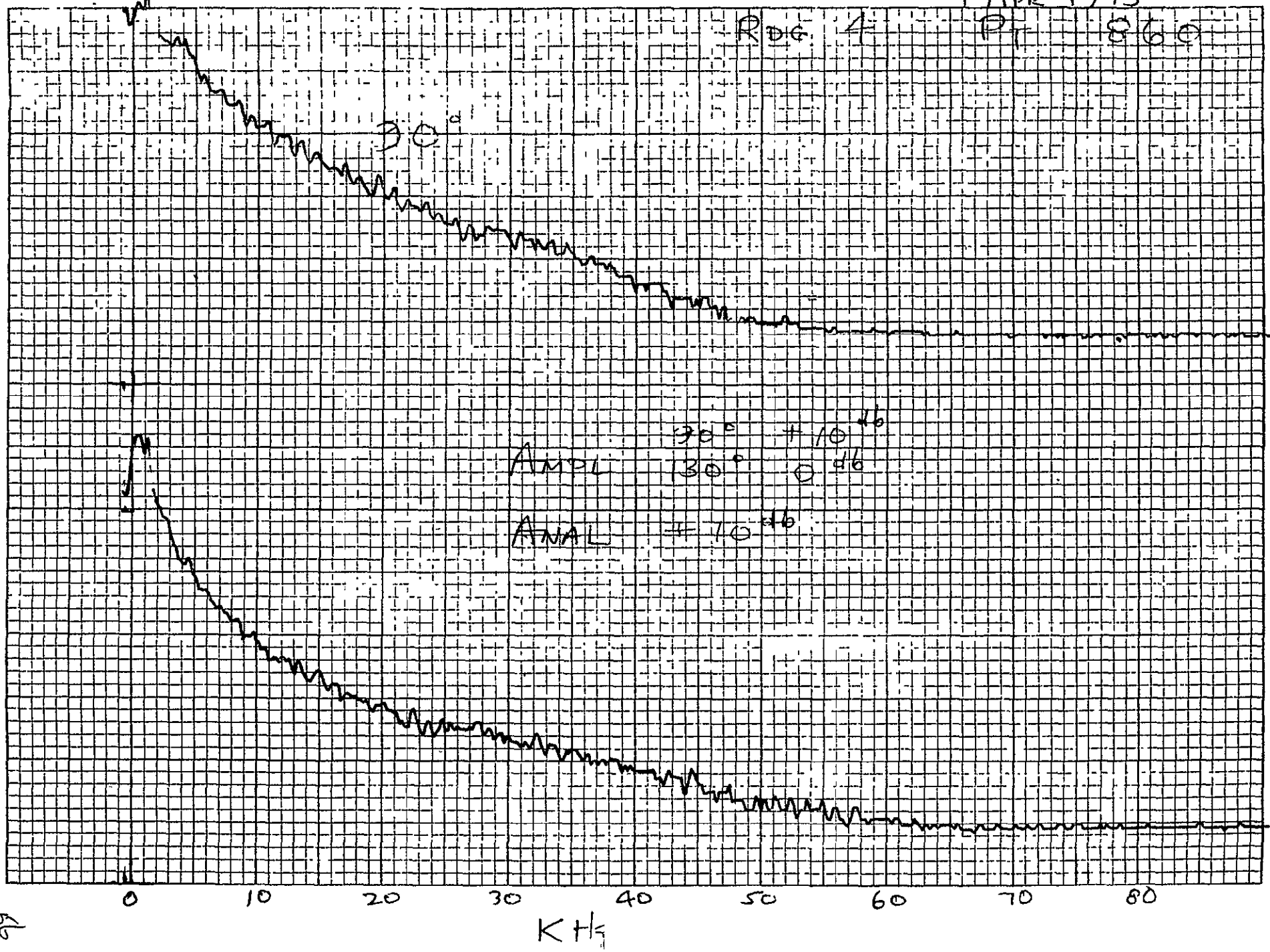
860

① ②

AMPL 30° # 10 db
30° ① db
ANAL # 10 db

1666

5-57



6.0 AERODYNAMIC DATA FORMAT - ACOUSTIC TESTS

6.0 AERODYNAMIC DATA FORMAT - ACOUSTIC TESTS

The test conditions for the acoustic tests at JENOTS were set using the instrumentation rakes, measuring total pressure and total temperature. The fuel flow to the fan and core burners, the fan air flow, the core (primary airflow) and facility temperatures were monitored and recorded. All this basic data and the resultant calculations were processed through a Time-Sharing computer program. These results were available during the test to validate that the test conditions were as specified.

The following sample output sheet includes the physical geometry constants and reference constants, the summary results of the calculations showing pressure ratio, weight flows, temperatures, and velocities, the averages of the multiple rake input or orifice statics, and a complete listing of each individual measurement in engineering units (psia, °R). A configuration sheet defining each of the measurements is also included.

DUAL FLOW CHECKOUT

4/ 7/75 RUN: 12 RDG: 28 PNT: 815 BAROM: 14.489
 PF28 ALPHA OUT OF TABLE
 PF3 ALPHA OUT OF TABLE

LIST #13/ FOL. OUTPUT

*LIST A#13"

DUAL FLOW CHECKOUT

4/ 7/75 RUN: 12 RDG: 28 PNT: 315 BAROM: 14.489

CONSTANTS

DI	=	12.0000	D8	=	4.6270	MAO-DIA=	5.0000
MAO-BEF=		0.4990	SAO-DIA=		9.1500	SAO-BET=	0.6000
SGSAMP =		0.7530	TSAMP =		512.0000	SECAREA=	10.8420

CALCULATIONS

PT3/P0	=	1.590	PT28/P0	=	3.269		
TI8	=	994.087	DEG. R	TI28	=	1603.352	DEG. R
WA8	=	6.066	PPS	WA28	=	6.691	PPS
WI8	=	6.104	PPS	WT28	=	6.691	PPS
WF8	=	0.038	PPS	WF28	=	0.	PPS
WF1	=	0.148	PPS	WFTV	=	0.038	PPS
F/A8	=	0.006		F/A28	=	0.	
GAM 8	=	1.390		GAM28	=	1.362	
V8	=	1218.833	FT/SEC				
V28	=	2366.023	FT/SEC				
TS8	=	872.757	DEG. R	TS28	=	1170.578	DEG. R

6-2

```

M3      =      0.844      M28      =      1.430
F8      =      231.050  -F      F28      =      491.623  -F
AE8     =      16.092  SQ. IN  AE28     =      12.187  SQ. IN
10 LOG(R8*A8)      =      -23.003
10 LOG(R28*A28)    =      -25.485
10 LOG(R8**2*A8)   =      -36.489
10 LOG(R28**2*A28) =      -40.246

```

AVERAGES

```

TT-TMV( 0)= 0.      T-OUT( 1)= 508.495  MAO-P1( 6)= 29.631
MAO-P2( 6)= 26.563  MAO-T1( 2)= 414.871  WFTCPS( 1)= 0.148
COREPT( 6)= 23.042  CORTT5( 2)= 948.634  FTEMPT( 1)= 512.129
SAO-P1( 4)= 48.465  SAO-P2( 2)= 48.242  SAO-TT( 2)= 526.921
WF1( 1)= 0.038     WF2( 1)= 0.      WF3( 1)= 0.
FTEMPT( 1)= 512.129  COR-IN( 5)= 994.087  FAN-TT( 6)= 1603.352
FAN-P1( 6)= 47.368  CORE-T( 0)= 0.

```

ENGINEERING UNITS

CHAN	DATA	CHAN	DATA	CHAN	DATA	CHAN	DATA	CHAN	DATA
3	1254.839	4	964.791	5	1443.913	7	1446.023	8	1548.147
9	10458.670	10	1012.068	18	1282.883	19	1295.630	20	1220.776
21	1396.642	23	1428.720	24	1238.253	25	1203.724	26	1209.692
27	1016.857	28	1008.585	37	994.616	38	990.668	39	991.107
40	1001.619	41	992.423	43	1622.496	44	1450.106	45	1635.601
46	1622.070	47	1639.948	48	1640.799	52	735.239	53	783.807
54	795.952	55	1176.016	57	624.300	59	984.528	61	508.495
62	524.680	63	305.062	64	526.921	65	526.921	66	512.129
68	511.631	69	512.129	70	0.	71	99.722	72	888.248
73	735.685	75	1009.020	76	581.359	77	1661.688	78	1756.255
79	990.440	102	-42.434	103	-79.285	104	-163.037	105	-37.968
106	-5756.561	107	-35.734	108	29.567	109	29.540	110	22.983
111	23.001	112	14.489	113	14.489	114	26.630	115	26.626
116	23.039	117	23.073	118	14.484	119	14.490	120	48.348
121	48.555	122	23.039	123	23.117	124	14.489	125	14.490
126	48.259	127	48.287	128	47.155	129	47.390	130	14.489
131	14.490	132	29.622	133	29.685	134	47.441	135	47.401
136	14.484	137	14.490	138	26.553	139	26.491	140	47.441
141	47.379	142	14.484	143	14.490	144	48.481	145	48.477
146	22.676	147	22.685	148	14.467	149	14.490	150	48.226
151	48.219	152	22.609	153	22.624	154	14.489	155	14.490
156	14.467	157	14.489	158	47.413	159	47.301	160	14.467
161	14.489	162	29.667	163	29.708	164	47.368	165	47.278
166	14.478	167	14.490	168	26.553	169	26.525	170	47.463
171	23.028	172	14.484	173	14.490	178	0.	179	300.154
181	145.900	182	-0.800	183	-7.600	184	289.800	202	9941.000
203	9939.000	204	9935.000	205	9942.000	206	9936.000	207	9938.000

ready

```

*DONE
SYSTEM ?REMO CLEARFILES
SYSTEM ?

```

63

COMPUTER CHANNEL	PARAMETER DESCRIPTION	LOCATION
3	T/C - T2	Support Cone - P06
4	T/C - T6	" "
5	T/C - T1	" " - P06
7	T/C - T12	Support Cone - P07
8	T/C - T16	" "
9	T/C - T18	" "
18	T/C - T4	Support Cone - P06
19	T/C - T5	" "
20	T/C - T7	" "
21	T/C - T8	" "
23	T/C - T13	Support Cone - P07
24	T/C - T14	" "
25	T/C - T15	" "
26	T/C - T17	" "
27	T/C - T20	" "
28	T/C - T21	Inner Frame - P08
37	T/C	Core T/C Rake - 0°
38	T/C	" "
39	T/C	Core T/C Rake - 180°
40	T/C	" "
41	T/C	" "
43	T/C	Fan T/C Rake - 30°
44	T/C	" "
45	T/C	" "
46	T/C	Fan T/C Rake - 210°
47	T/C	" "
48	T/C	" "
52	T/C	Fan - Outside Burner
53	T/C	Fan Elbow - Top
54	T/C	Fan Elbow - V.C.L.
55	T/C	Elbow & Plenum
57	T/C	Plenum - Inside
59	T/C	Plenum - Mid Sec. Pipe

COMPUTER CHANNEL	PARAMETER DESCRIPTION	LOCATION
61	T/C	Outside (Amb) Temp.
62	T/C	Main Air Orifice - A
63	T/C	" " " - B
64	T/C	Sec. Air Orifice - A
65	T/C	" " " - B
66	T/C	Fan P/B Fuel
68	T/C	Core P/B Fuel
69	T/C	Total Fuel
70	-	Digital Zero
71	-	Cal. 32.42
72	T/C	Core P/B Dish - T _{T5}
73		
75	T/C	Core P/B Discharge
76	T/C	Fan P/B Discharge
77	T/C	" " "
78	T/C	" " "
79	T/C	" " "
102	Press-Vent A	
103	" -Vent B	
104	" -Vent C	
105	" -Vent D	
106	" -Vent E	
107	" -Vent F	
108	PS	Main Air Orifice - Upstream
109	PS	" " " "
110	PT - 1A	Core 0° Rake
111	PT - 2A	Core 180° Rake
112	Open	
113	Open	
114	PS	Main Air Orifice - Downstream
115	PS	Main Air Orifice - Downstream
116	PT - 1B	Core 0° Rake
117	PT - 2B	Core 180° Rake
118	Open	
119	Open	
120	PS	Sec. Air Orifice - Upstream
121	PS	" " " "
122	PT - 1C	Core 0° Rake
123	PT - 2C	Core 180° Rake

COMPUTER CHANNEL	PARAMETER DESCRIPTION	LOCATION
124	Open	
125	Open	
126	PS	Sec. Air Orifice - Downstream
127	PS	" " " - "
128	PT - 1A	Fan 30° Rake
129	PT - 2A	Fan 210° Rake
130	Open	
131	Open	
132	PS - 1A	Main Air Orifice - Upstream
133	PS - 1B	Main Air Orifice - Upstream
134	PT - 1B	Fan 30° Rake
135	PT - 2B	Fan 210° Rake
136	Open	
137	Open	
138	PS - 2A	Main Air Orifice - Downstream
139	PS - 2B	Main Air Orifice - Downstream
140	PT - 1C	Fan 30° Rake
141	PT - 2C	Fan 210° Rake
142	Open	
143	Open	
144	PS - 1A	Sec. Air Orifice - Upstream
145	PS - 1B	Sec. Air Orifice - Upstream
146	PS	Core Outer - 16°
147	PS	Core Outer - 196°
148	Open	
149	Open	
150	PS - 2A	Sec. Air Orifice - Downstream
151	PS - 2B	Sec. Air Orifice - Downstream
152	PS	Core Inner - 164°
153	PS	Core Inner - 344°
154	Open	
155	Open	
156	Open	
157	Open	
158	PS	Fan Outer - 37.5°
159	PS	Fan Outer - 217.5°
160	Open	
161	Open	
162	PS - 1A	Main Air Orifice - Upstream
163	PS - 1B	Main Air Orifice - Upstream
164	PS	Fan Inner - 37.5°
165	PS	Fan Inner - 217.5°

COMPUTER CHANNEL	PARAMETER DESCRIPTION	LOCATION
166	Open	
167	Open	
168	PS - 2A	Main Air Orifice - Downstream
169	PS - 2B	" " " " " "
170	PT - 2B	Fan 210° Rake
171	PT - 1B	Core 0° Rake
172	Open	
173	Open	
178	Zero	AMP - Scanner
179	Cal	Scanner
180	Jump	
181	Fuel Flow	Core Pre-Burner
182	Fuel Flow	Fan Pre-Burner
183	Open	
184	Fuel Flow	Total Flow
202	Volts	Sense
203	"	"
204	"	"
205	"	"
206	"	"
207	"	"

6-1

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7.0 LASER DATA RECORDING

7.0 LASER VELOCIMETER DATA RECORDING

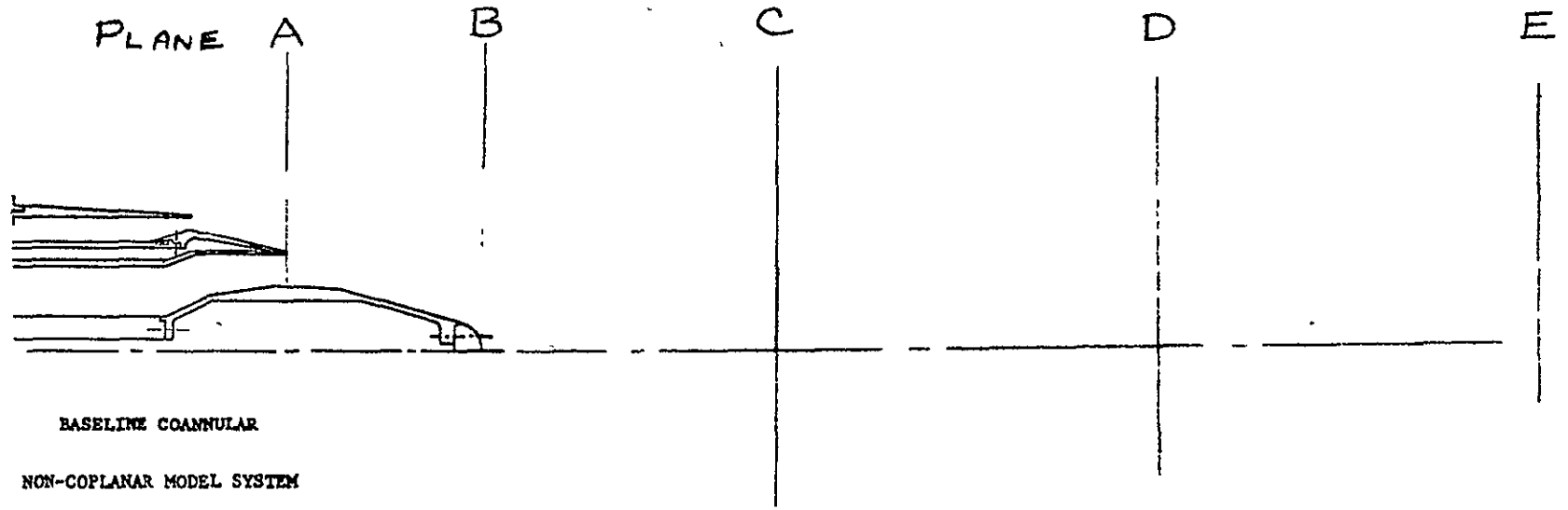
The actual process of surveying the plume of a scale model jet exhaust nozzle starts with the definition of the traverse planes of interest and the approximate number of histograms to be taken in each plane. When the test point has been set and the test conditions have stabilized, the location of the first traverse position relative to a fixed position on the nozzle at the test conditions is established. Vertical and horizontal traverses are used to verify the location of the nozzle flow centerline. A typical traverse is shown in the following pages with the histogram locations noted.

At each of the noted histogram locations, a histogram is taken, recorded with an X-Y plotter, and processed through an on-line computer. The mean velocity and turbulence level are calculated and printed out as shown.

In order to construct the velocity profile from the histograms, the recorded location of each histogram is calculated, and the mean velocity and turbulence level tabulated. These tabulations are plotted as shown in the Final Report.

A sample of the laser velocimeter data records is included.

1676



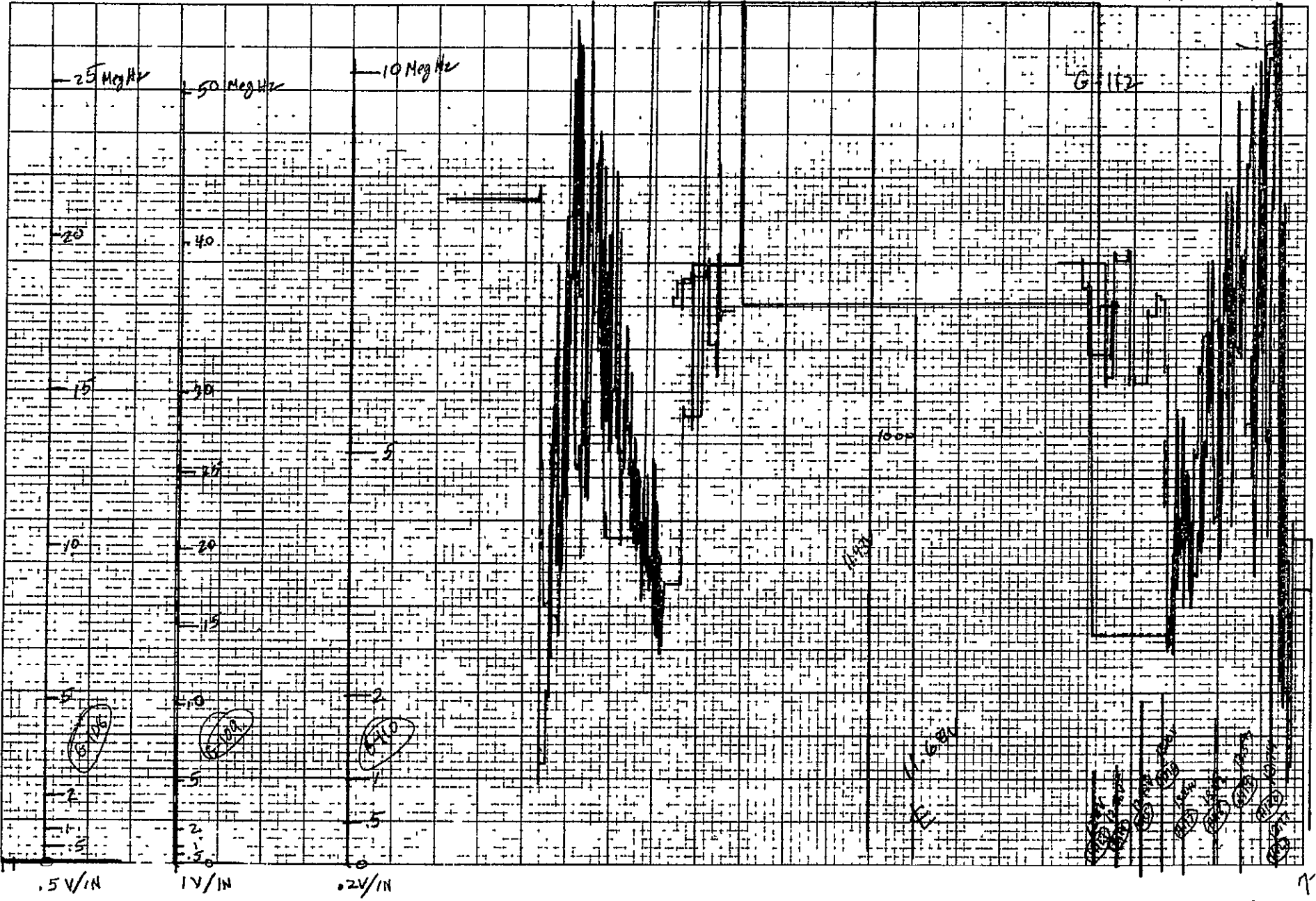
BASELINE COANNULAR
NON-COPLANAR MODEL SYSTEM

$$x/D_{EQ} \quad 0$$

22

75415-0572

1677

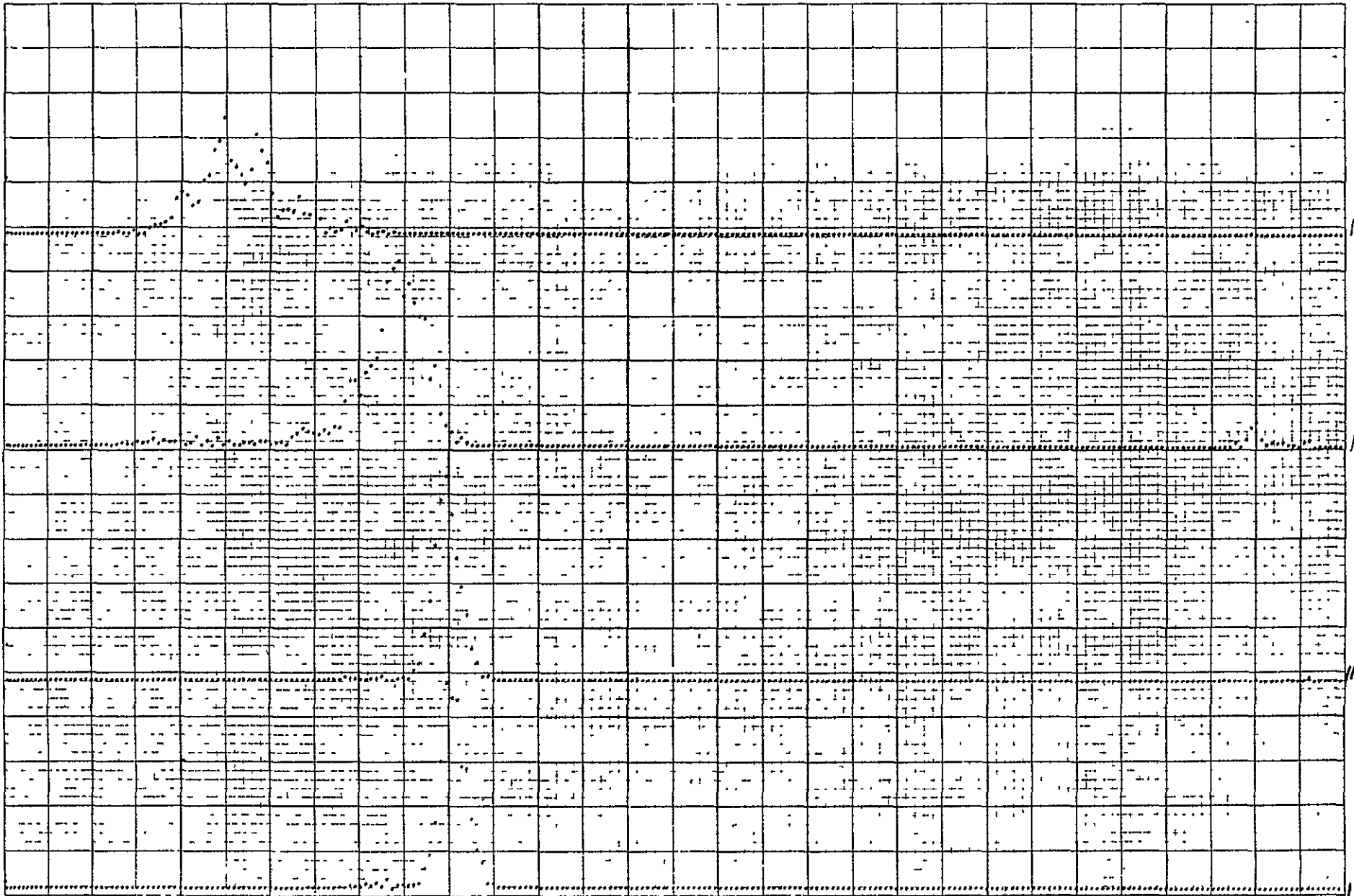


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73

75415-0512

1678



117

116

115

114

7-4

75415-0512

The image shows a large grid of graph paper. The grid is composed of small squares. There are some faint, scattered markings and lines across the grid, but they are mostly illegible. The grid is bounded by a solid line on the top, bottom, and left sides, and a dashed line on the right side.

121

SEE NEXT PAGE

MOVED

120

119

118

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75

1679

①

DATE MODEL #1 LV ~~11~~ MAY 1975
12

~~FILE CHECK~~

X=O

PT 123 ✓

F HISTGM #113

INPUT NUMBER OF DATA POINTS 1000
DELTA V 4 51
FINAL POINT NUMBER=500

PLANE A X.
FAN LIP
CORE EXIT

113

NUMBER OF DATA POINTS = 1000

PARAMETER	VALUE	95% CONFIDENCE INTERVAL	% ERROR
MEAN	1298 479 ✓	(1294 855, 1302 102)	0 2791
TURBULENCE (SD)	57 295	(54 815, 59 947)	4 5228
TURE RATIO	0 044		

1=NOPE DATA, 2=PPINT HISTOGRAM, 3=END >3

H NUMBER #114

P HISTGM
"FIL NOT FND"

P HISTGM

INPUT NUMBER OF DATA POINTS 600

DELTA V 50°C
°C

R HISTGM

INPUT NUMBER OF DATA POINTS 600

DELTA V 4 52

FINAL POINT NUMBER=600

7-6

NUMBER OF DATA POINTS = 588.

114

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OF POOR QUALITY

PARAMETER	VALUE	95% CONFIDENCE INTERVAL	% ERROR
MEAN	1301 114	(1296 259, 1305 970)	0 3732
TURBULENCE (SD)	58 870	(55 579, 62 462)	5 9208
TURB RATIO	0 045		

1=MORE DATA, 2=PRINT HISTOGRAM, 3=END ?3

H NUMBER 115

R HISTGM

INPUT NUMBER OF DATA POINTS 600

DELTA V 4 5J

FINAL POINT NUMBER=500

NUMBER OF DATA POINTS = 600

PARAMETER	VALUE	95% CONFIDENCE INTERVAL	% ERROR
MEAN	1259 297	(1254.668, 1263 927)	0 3676
TURBULENCE (SD)	56 702	(53.563, 60 125)	5 8604
TURB RATIO	0 045		

1=MORE DATA, 2=PRINT HISTOGRAM, 3=END ?3

R HIS

H NUMBER 116

R HISTGM

INPUT NUMBER OF DATA POINTS 600

DELTA V 4.5

^C

R HISTGM

^C

^C

^CM

INPUT NUMBER OF DATA POINTS R

^C

R HISTGM

1681

7-1

INPUT NUMBER OF DATA POINTS 500

DELTA V 4 45

3

FINAL POINT NUMBER=500

NUMBER OF DATA POINTS = 477 #116

PARAMETER	VALUE	95% CONFIDENCE INTERVAL	% ERROR
MEAN	1077.576	(1067.887, 1091.266)	1.2704
TURBULENCE (SD)	149.489	(140.253, 159.668)	6.5850
TURB RATIO	0.139		

1=MORE DATA, 2=PRINT HISTOGRAM, 3=END 03

H NUMBER 117
R HISTOGRAM

INPUT NUMBER OF DATA POINTS 500

DELTA V 4 4

FINAL POINT NUMBER=500

NUMBER OF DATA POINTS = 497.

PARAMETER	VALUE	95% CONFIDENCE INTERVAL	% ERROR
MEAN	681.712	(671.482, 691.943)	1.5007
TURBULENCE (SD)	114.014	(107.126, 121.633)	6.4489
TURB RATIO	0.167		

1=MORE DATA, 2=PRINT HISTOGRAM, 3=END 03

H NUMBER 118

R HISTOGRAM

INPUT NUMBER OF DATA POINTS 500

DELTA V 4 5

FINAL POINT NUMBER=500

NUMBER OF DATA POINTS = 596

7-8

PARAMETER	VALUE	95% CONFIDENCE INTERVAL	% ERROR
-----------	-------	-------------------------	---------

MEAN 1137.775 ✓ (1119.302, 1156.248) .1.6236
 TURBULENCE (SD) 225.487 (212.965, 239.148) 5.8803
 TURB RATIO 0.198 118

④

1=MORE DATA, 2=PRINT HISTOGRAM, 3=END ?3

H NUMBER 119
 R HISTGM

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INPUT NUMBER OF DATA POINTS 600

DELTA V 4 53

FINAL POINT NUMBER=500

NUMBER OF DATA POINTS = 599

PARAMETER	VALUE	95% CONFIDENCE INTERVAL	% ERROR
MEAN	1370.219 ✓	(1347.478, 1392.961)	1.6597
TURBULENCE (SD)	278.295	(262.877, 295.111)	5.8653
TURB RATIO	0.203		

1=MORE DATA, 2=PRINT HISTOGRAM, 3=END ?3

H NUMBER 120
 R HISTGM

INPUT NUMBER OF DATA POINTS 600

DELTA V 4 53

FINAL POINT NUMBER=500

NUMBER OF DATA POINTS = 599

PARAMETER	VALUE	95% CONFIDENCE INTERVAL	% ERROR
MEAN	1720.443 ✓	(1692.176, 1748.711)	1.6431
TURBULENCE (SD)	345.920	(326.755, 366.822)	5.8653
TURB RATIO	0.201		

1=MORE DATA, 2=PRINT HISTOGRAM, 3=END ?3

H NUMBER 121

1683

79

R HISTGM

MODEL *1

TEST 12 MAY 1975

Pt 123

PLANE A

FAN LIP - CORE EXIT

X = 0 inches
VERTICAL $\phi = 11.68^\circ$ V = 106

	V	ΔV	R-INCHES	V_{MEAN}	u'	u'/U
H113	12.71	1.03	2.28	1298	57	.044
H114	12.86	1.18	2.61	1301	59	.045
H115	12.99	1.31	2.90	1259	57	.045
H116	13.10	1.42	3.14	1078	149	.133
H117	13.24	1.56	3.45	682	114	.167
H118	13.42	1.74	3.85	1138	225	.198
H119	13.57	1.89	4.18	1370	278	.253
H120	13.74	2.06	4.56	1720	346	.261
H121	13.77	2.09	4.62	1572	424	.270

PLANE B

PLUG TIP X = 6.15"

Vertical $\phi = 11.68^\circ$ V = 384 v

	V	ΔV	R-INCHES	V_{MEAN}	u'	u'/U
H128	12.57	.89	1.97	1251	10	.081
H129	12.71	1.03	2.28	1093	122.5	.112
H130	12.86	1.18	2.61	884	88	.100
H131	12.99	1.31	2.90	882	9	.103
H132	13.10	1.42	3.14	990	117	.118
H133	13.24	1.56	3.45	1132	121	.107
H134	13.42	1.74	3.85	1208	136	.113
H135	13.57	1.89	4.18	1072	208	.194
H136	13.74	2.06	4.56	803	225	.280
H137	13.89	2.21	4.89	547	194	.355

P_T 123

12 MAY 1975

PLANE C

V = 8.23 v.

X = 15.86"

VERTICAL

z = 11.68 v.

BASE

	V.	ΔV	R-INCHES	V _{MEAN}	u'	u'/U
H140	12.17	.49	1.08	1337	67	.050
H141	12.50	.82	1.81	1208	102	.084
H142	12.71	1.03	2.28	1076	93	.086
H143	12.99	1.31	2.90	1033	92	.089
H144	13.24	1.56	3.45	1019	113	.111
H145	13.57	1.89	4.18	866	161	.186
H146	13.89	2.21	4.89	593	167	.282
H147	14.30	2.62	5.80	340	134	.396
H148	14.10	2.42	5.35	440	150	.341

PLANE D

V = 13.56

X = 27.65"

VERTICAL

z = 11.68 v.

	V.	ΔV	R-INCHES	V _{MEAN}	u'	u'/U
H150	8.50	-3.18	-7.04	224	107	.478
H151	9.00	-2.68	-5.93	372	123	.330
H152	9.47	-2.21	-4.89	541	155	.287
H153	11.68	0	0	130	72	.055
H154	11.93	-.25	.55	1303	63	.047
H155	12.7	.49	1.08	1302	90	.063
H156	12.71	1.03	2.28	1102	121	.110
H157	12.99	1.31	2.90	992	125	.126
H158	13.24	1.56	3.45	897	140	.156
H159	13.57	1.89	4.18	776	153	.198
H160	13.89	2.21	4.89	612	156	.251

MODEL #1

TEST

12 MAY 1975

P_T 151

P_T/P_0

$T_T - ^\circ R$

V_j

FAN
CORE

1.64

775

1.5

1460

1400

PLANE A

FAN LIP - CORE EXT

$X = .13$

$\Delta X = .06$

$V = 1.06$

VERTICAL $z = 11.68$

$H = 4.85$

$l = 4.15^*$

	V	ΔV	R-INCHES	\bar{u}	u'	u'/\bar{u}
H162	CAL					
H163	12.71	1.03	2.28	1351	41	.030
H164	12.86	1.18	2.61	1328	40	.030
H165	12.99	1.31	2.90	1312	41	.031
H166	13.10	1.42	3.14	1240	69	.056
H167	13.24	1.56	3.45	381	60	.158
H168	13.42	1.74	3.85	588	81	.137
H169	13.57	1.89	4.18	714	89	.125
H170	13.74	2.06	4.56	786	167	.213
H171	13.81	2.13	4.71	635	195	.307
H173	13.57	1.89	4.18 ⁺	954	138	.144

PLANE B

$X = 6.28$

$\Delta X = 2.84$

	V	ΔV	R-INCHES	\bar{u}	u'	u'/\bar{u}
H175	TRAV					
H176	12.15	0.47	1.04	1284	32	.025
H177	12.57	0.89	1.97	1332	64	.048
H178	12.71	1.03	2.28	1210	137	.113
H179	12.85	1.17	2.59	735	152	.207
H180	12.99	1.31	2.90	556	64	.116
H182	13.42	1.74	3.85	627	65	.104
H183	13.57	1.89	4.18	541	95	.176
H184	13.74	2.06	4.56	394	113	.286
H185	13.89	2.21	4.89	257	101	.393
H186	12.78	1.10	2.43	989	187	.189
H186	13.24	1.56	3.45	630	59	.093

MODEL * 1

TEST

12 MAY 1975

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PLANE C

 $X = 16.0''$ $\Delta X = 7.23$ VERT. $\phi = 11.68$

	V	ΔV	R-INCHES	\bar{U}	u'	u'/\bar{u}
H190	11.68	0	0	1285	77	.060
H191	12.17	0.49	1.08	1382	39	.028
H192	12.50	0.82	1.81	1266	118	.093
H193	12.71	1.03	2.28	963	174	.180
H194	12.99	1.31	2.90	654	73	.111
H195	13.23	1.55	3.43	563	63	.112
H196	13.58	1.90	4.20	462	84	.181
H197	13.89	2.21	4.89	338	88	.260

PLANE D

 $X = 27.7''$ $\Delta X = 12.56$

	V	ΔV	R-INCHES	\bar{U}	u'	u'/\bar{u}
H199	13.89	2.21	4.89	334	94	.280
H200	9.47	2.21	4.89	315	89	.284
H201	11.68	0	0	1315	61	.047
H202	11.97	0.29	.64	1353	62	.046
H203	12.17	0.49	1.08	1329	86	.065
H204	12.50	0.82	1.81	1131	164	.145
H205	12.71	1.03	2.28	907	172	.190
H206	12.99	1.31	2.90	689	131	.190
H207	13.24	1.56	3.45	550	106	.193
H208	13.57	1.89	4.18	431	99	.229

MODEL #1

TEST 12 MAY 1975

P_T 125

P_T/P_0

T_T

V_J

FAN

3.9

1960

2800

CORE

1.5

1460

1400

PLANE A

$X = 0.13''$

$\Delta X = 0.6$

VERT

$E = 11.68$

\dot{V}

ΔV

R-INCHES

\bar{u}

u'

u'/\bar{u}

H210

12.99

1.31

2.90

1272

47

.037

H211

12.71

1.03

2.28

1318

48

.036

H236

?

?

?

2448

247

.101

PLANE B

$X = 6.46''$

$\Delta X = 2.92$

R-INCHES

\bar{u}

u'

u'/\bar{u}

H213

10.79

0.89

1.97

1301

26

.028

H214

10.65

1.03

2.28

1296

60

.046

H215

10.50

1.18

2.61

1253

88

.070

H216

10.37

1.31

2.90

1329

132

.099

H217

10.12

1.56

3.45

1698

160

.094

H218

9.94

1.74

3.85

1605

241

.150

TOP

TTOM

MODEL #1

TEST

12 MAY 1975

Pt ~~125~~ 125

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PLANE C X = 16.0"
VERT Z = 11.68

$\Delta X = 7.23$

	V	ΔV	R-INCHES	\bar{u}	u'	u'/\bar{u}
H221	11.68	0	0	1296	86	.066
H222	11.19	0.49	1.08	1295	97	.075
H223	10.50	1.18	2.61	1427	117	.082
H224	9.47	2.21	4.89	1294	232	.179
H225	9.78	1.90	4.20	1082	270	.249
H226	9.59	2.09	4.62	819	218	.266
→ H224	9.95	1.73	3.83	1294	232	.179

PLANE D X = 27.7"

$\Delta X = 12.56$

	V	ΔV	R-INCHES	\bar{u}	u'	u'/\bar{u}
H228	11.68	0	0	1326	82	.062
H229	10.50	1.18	2.61	1381	110	.080
H230	10.12	1.56	3.45	1270	206	.162
H231	9.79	1.89	4.18	954	245	.257
H232	9.59	2.09	4.62	864	235	.272
H233	10.79	0.89	1.97	1346	100	.074
H234	11.19	0.49	1.08	1303	95	.073

7-15

8.0 STATIC PRESSURES - ACOUSTIC MODELS

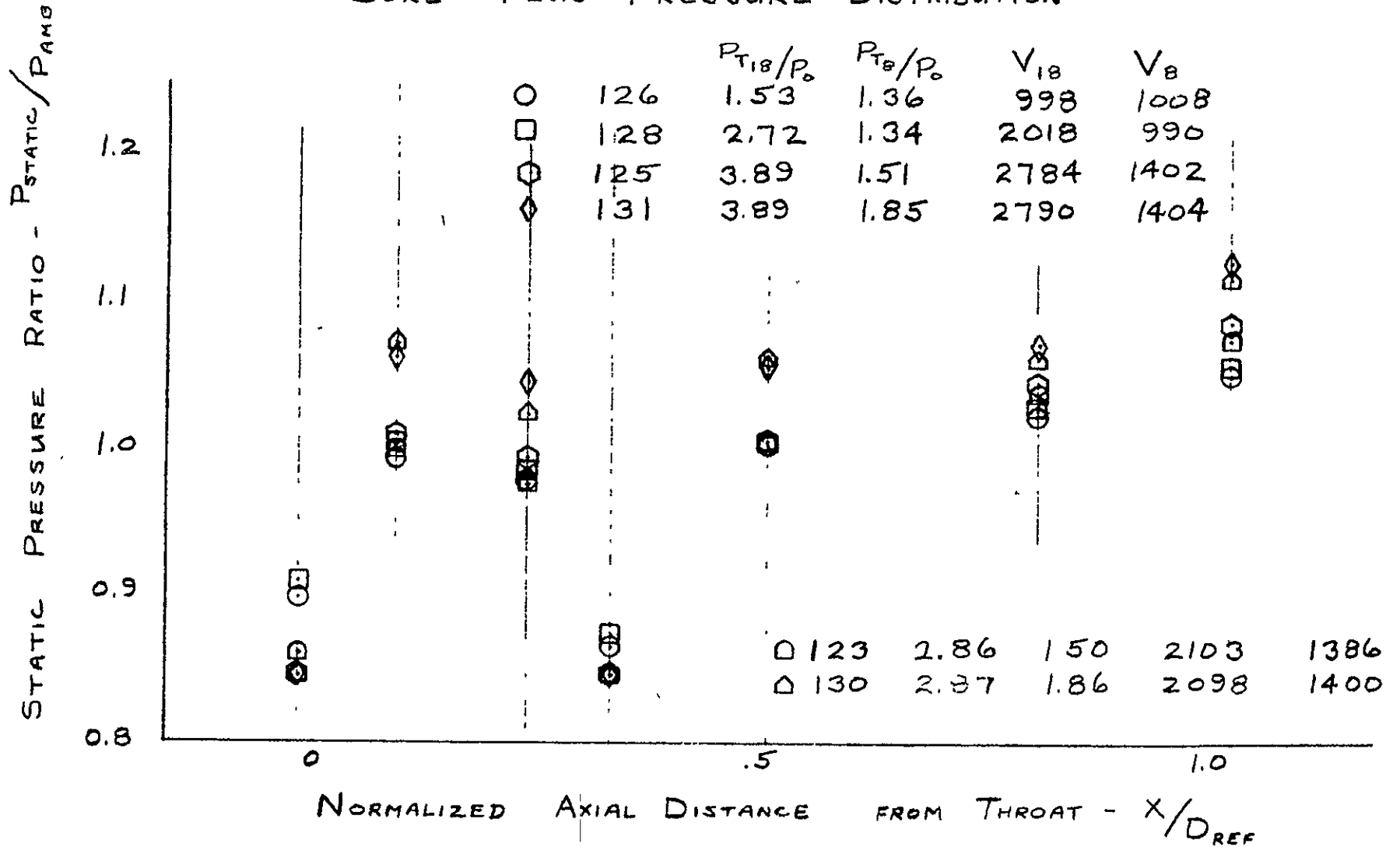
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8.0 STATIC PRESSURES - ACOUSTIC MODELS

The static pressure data from the acoustic test runs are tabulated for selected conditions.

1692

CORE PLUG PRESSURE DISTRIBUTION

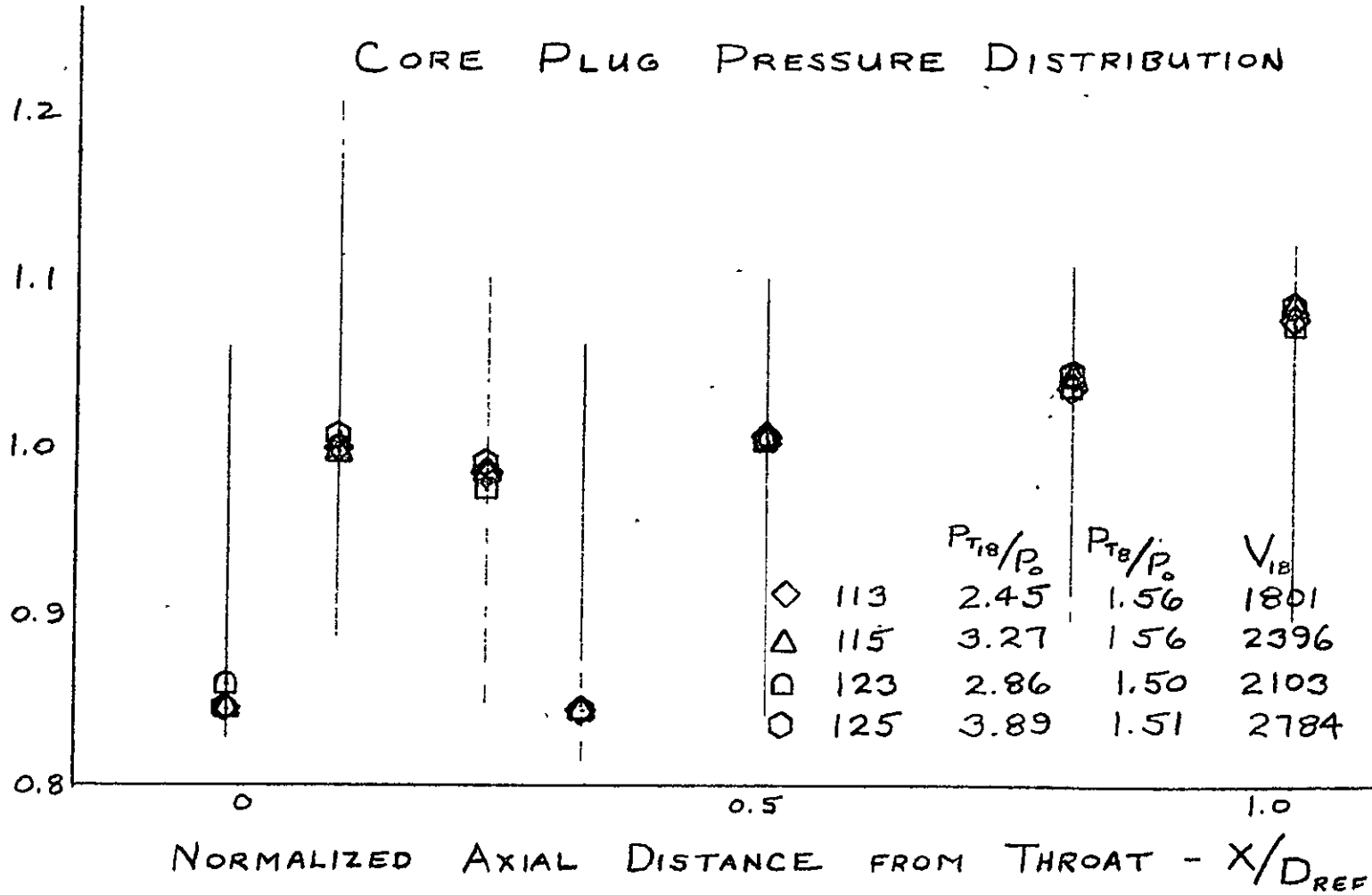


CHUTE SUPPRESSOR WITHOUT EJECTOR
CONFIGURATION 1

1693

STATIC PRESSURE RATIO - P_{STATIC}/P_{AMB}

CORE PLUG PRESSURE DISTRIBUTION



		P_{T18}/P_0	P_{T8}/P_0	V_{18}	V_8
◇	113	2.45	1.56	1801	1197
△	115	3.27	1.56	2396	1209
□	123	2.86	1.50	2103	1386
○	125	3.89	1.51	2784	1402

CHUTE SUPPRESSOR WITHOUT EJECTOR
CONFIGURATION 1

ORIGINAL PAGE IS
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4-3

- MODEL # 1 -

MULTI-CHUTE

FAN PLUG

FEC N-AXIAL & CW.

GE LINE

✓	51	2.38	355°	Flow ↓ Corner	155
	50	2.000	345°		149
✓	49	1.625	335°		143
✓	48	1.272	355°		137
✓	47	1.005	345°		131
✓	46	.832	335°		125
	45	.680	355°		119
✓	44	.315	345°		
✓	43	-.145	335°		
	42	-.220	355°		
✓	41	1.005	90°	Chute ↓	113
	40	.832	80°		172
✓	39	.680	70°		166
✓	38	.315	90°		160
✓	37	-.145	80°		154
✓	36	-.220	70°		

Chute Base
T-RADIUS

52	3.83	0°	161
53	3.98	10°	
54	4.13	20°	167
55	4.28	30°	
56	4.43	40°	173
57	4.58	50°	
58	4.72	60°	

PT

MODEL # 1

MULTI-CHUTE FAN SUPPRESSOR

CORE PLUG
STATICS

X

FAN PLUG
STATICS

LINE			LINE	
112	51	-0.1	154	36
118	53	.57	160	37
124	55	1.44	166	38
130	57	1.98	172	39
136	60	2.4 3.03	113	41
142	62	4.84	119	43
148	64	6.15	125	44
			131	46
			137	47
			143	48
			149	49
			155	51

CHUTE BASE

161	52
167	54
173	56

85

PT 113

MODEL # 1

MULTI-CHUTE FAN SUPPRESSOR

CORE PLUG STATICS

FAN PLUG STATICS

LINE			LINE		
112	12.172	cavity 845	154	14.329	.995 36
118	14.430	1.002	160	14.321	.994 37
124	14.186	.985	166	14.246	.989 38
130	12.172	cavity 845	172	13.413	.931 39
136	14.509	1.007	113	13.570	.942 41
142	14.931	1.037	119	15.247	1.058 43
148	15.524	1.078	125	13.784	.957 44
			131	12.995	.902 46
			137	13.464	.935 47
			143	13.852	.962 48
			149	13.948	.968 49
			155	14.446	1.003 51

CHUTE BASE

161	14.079	.978	$P_{A\text{ amb}} = 14.403$
167	14.125	.981	

	P_T / P_0	T_T	V_T
PT 113			
CORE	1.56	1002	1197
FAN	2.45	1188	1801

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PT 115 ORIGINAL PAGE IS
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MODEL # 1

MULTI-CHUTE FAN SUPPRESSOR

CORE PLUG STATICS

FAN PLUG STATICS

LINE			LINE		
112	12.172 Cavity	.845	154	14.035	.996
118	14.373	.998	160	14.207	.986
124	14.204	.986	166	14.152	.982
130	12.172 Cavity	.845	172	12.760	.886
136	14.519	1.008	113	13.088	.908
142	15.013	1.042	119	16.090	1.117
148	15.632	1.085	125	14.474	1.005
			131	12.379	.859
			137	13.005	.903
			143	13.562	.941
			149	13.746	.954
			155	14.461	1.004

CHUTE BASE

161	13.999	.972	$P_{AMB} = 14.406$
167	14.034	.974	

	PT 115	P_T/P_0	T_T	V_T
CORE		1.57	1004	1209
FAN		3.27	1642	2396

MODEL # 1

PT 123

MULTI-CHUTE FAN SUPPRESSOR

CORE PLUG
STATICS

FAN PLUG
STATICS

LINE			LINE		
112	12.404	.860	154	14.135	.980
118	14.411	.9996	160	14.439	1.002
124	14.108	.976	166	14.300	.992
130	12.180	.845	172	13.342	.925
136	14.478	1.004	113	13.440	.932
142	14.929	1.036	119	17.318	1.201
148	15.466	1.073	125	15.307	1.062
			131	12.884	.894
			137	13.446	.933
			143	13.576	.942
			149	13.669	.948
			155	14.271	.990

CHUTE BASE

161	14.298	.992	$P_{AMB} = 14.416$
167	14.289	.991	

	PT 123	P_T / P_0	T_T	V_T
CORE		1.50	1457	1386
FAN		2.86	1405	2103

MODEL * 1

P_T 125

MULTI-CHUTE FAN SUPPRESSOR

CORE PLUG
STATICS

FAN PLUG
STATICS

LINE			LINE		
51	112	12.181 cavity .845	154	14.141	.981
53	118	14.549 1.009	160	13.321	.924
55	124	14.305 .992	166	15.338	1.064
57	130	12.181 cavity .845	172	12.181 cavity	.845
60	136	14.483 1.005	113	12.992	.901
62	142	15.031 1.043	119	19.565	1.357
64	148	15.633 1.084	125	15.655	1.086
			131	11.995	.832
			137	12.825	.890
			143	13.232	.918
			149	13.232	.918
			155	14.468	1.004

CHUTE BASE

161	14.308	.9925
167	14.271	.990

$P_{AMB} = 14.416$

P _T 125	P _r /P ₀	T _T	V _T
CORE	1.51	1471	1402
FAN	3.89	1968	2784

MODEL # 1

PT 126

MULTI-CHUTE FAN SUPPRESSOR

CORE PLUG
STATICS

FAN PLUG
STATICS

LINE			LINE		
112	12.943	.898	154	{ 14.320	.993
118	14.320	.993	160	{ 14.379	.997
124	14.107	.978	166	{ 14.276	.990
130	12.456	.864	172	{ 14.007	.971
136	14.433	1.001	113	{ 14.062	.975
142	14.725	1.021	119	14.887	1.032
148	15.113	1.048	125	14.088	.977
			131	13.903	.964
			137	14.039	.974
			143	14.162	.982
			149	14.214	.986
			155	14.422	1.0001

CHUTE BASE

161	14.341	.9945
167	14.374	.997

$P_{AMB} = 14.420$

PT 126

P_T / P_0

T_T

V_T

CORE

1.36

1004

1008

FAN

1.53

724

998

P_T 128

MODEL # 1

MULTI-CHUTE FAN SUPPRESSOR

CORE PLUG
STATICS

FAN PLUG
STATICS

LINE			LINE		
112	13.097	.909	154	14.274	.991
118	14.467	1.004	160	14.130	.981
124	14.175	.984	166	14.317	.994
130	12.565	.872	172	13.281	.922
136	14.445	1.003	113	13.477	.936
142	14.810	1.028	119	15.107	1.049
148	15.196	1.055	125	13.510	.938
			131	12.744	.885
			137	13.220	.918
			143	13.766	.956
			149	13.888	.964
			155	14.473	1.005

CHUTE BASE

161	14.115	.980
167	14.296	.992

$P_{AMB} = 14.406$

P _T 128	P _T /P ₀	T _T	V _J
CORE	1.34	1004	990
FAN	2.725	1351	2018

MODEL # 1 P_T 130

MULTI-CHUTE FAN SUPPRESSOR

CORE PLUG STATICS

LINE		
112	12.173	.845
118	15.422	1.070
124	14.731	1.022
130	12.173	.845
136	15.269	1.060
142	15.236	1.058
148	16.043	1.114

FAN PLUG STATICS

LINE		
154	14.113	.980
160	14.264	.990
166	14.311	.993
172	13.121	.911
113	13.334	.926
119	15.914	1.105
125	14.186	.985
131	12.791	.888
137	13.301	.923
143	13.595	.944
149	13.780	.956
155	14.311	.993

CHUTE BASE

161	14.076	.977
167	14.197	.985

$$P_{AMB} = 14.407$$

P _T 130	P _T /P ₀	T _T	V _T
CORE	1.86	1002	1400
FAN	2.87	1398	2098

Pt 131

MODEL # 1

MULTI-CHUTE FAN SUPPRESSOR

CORE PLUG
STATICS

FAN PLUG
STATICS

LINE			LINE		
112	12.180	.845	154	13.216	.917
118	15.307	1.062	160	13.026	.904
124	15.044	1.044	166	15.499	1.075
130	12.179	.845	172	12.180	.845
136	15.201	1.054	113	12.948	.898
142	15.407	1.069	119	17.571	1.219
148	16.214	1.125	125	15.118	1.048
			131	11.997	.832
			137	12.843	.891
			143	13.243	.918
			149	13.218	.917
			155	14.443	1.002

CHUTE BASE

161	14.321	.993
167	14.273	.990

$P_{AMB} = 14.418$

Pt 131

P_t/P_0

T/T

V_J

CORE

1.85

1015

1404

FAN

3.89

1977

2790

MODEL # Z

MULTI-TUBE

FAN PLUG STATICS

FEC	M-AXIAL	ϕ CW	Behind Inner Row Tube	Behind Middle Tube
49	2.38	0	✓	
48	2.038	15.62°	✓	
47	1.655	31.30	✓	
46	1.292	0	✓	
45	1.000	15.62°	✓	
44	.835	31.30°	✓	
43	.560	0	✓	
42	.080	15.62°	✓	
41	-.300	31.30°	✓	
40	1.292	54.78°		✓
39	1.000	39.16°		✓
38	.835	23.53°		✓
37	.560	54.78°		✓
36	.080	39.16°		✓

$$\Delta\theta = 15.652^\circ$$

23 Tube Row

MODEL # 7

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MULTI TUBE

FAN PLUG STATICS

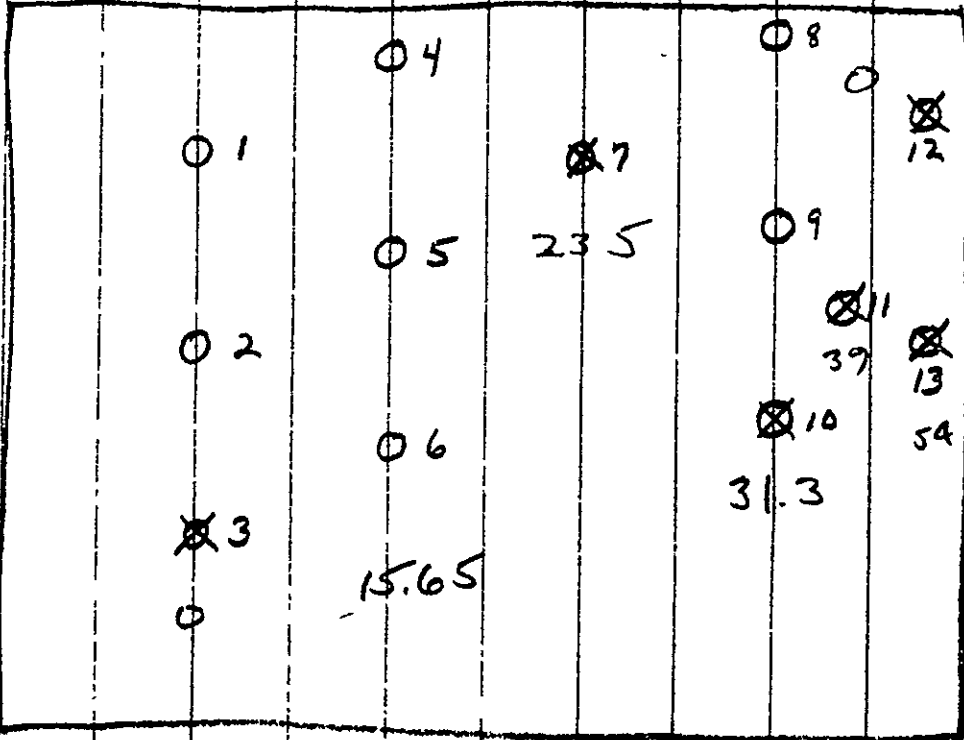
GE	FEC	M	AXIAL	ϕ C.W.	Behind Inner Tube	Behind Middle Tube
3-NG	49		2.38	0	✓	
6	48	161	2.38	15.62°	✓	
10-NG	47		1.655	31.30°	✓	
- 2	46	143	1.292	0	✓	
5	45	155	1.000	15.62°	✓	
9	44	173	.835	31.30°	✓	
- 1	43	137	.560	0	✓	
4	42	149	.080	15.62°	✓	
8	41	167	.300	31.30°	✓	
13	40		1.292	54.78°		✓
11	39		1.000	33.16°		✓
7-NG	38		.835	23.53°		✓
12	37		.560	54.78°		✓
-	36		.080	33.16°		✓

$\Delta \theta = 15.652^\circ$ 23 Tube Row

TDC
↓

↓
FLOW

FAN NO 2,
OUTER STATICS
4-21-75



Ps #	SCANNER	COMP. Pds
#1	F-6	137
2	F-7	143
4	F-8	149
5	F-9	155
6	F-10	161
8	F-11	167
9	F-12	173

MODEL #2

1,4

ORIGINAL PAGE
OF POOR QUALITY

Pt 210

MODEL #2

CORE PLUG STATICS psia

FAN PLUG STATICS psia

112	12.312	.847	137	13.770	.947
118	13.697	.942	143	13.618	.936
124	14.517	.998			
130	14.700	1.011	149	13.810	.950
136	14.725	1.0125	155	13.485	.927
142	13.664	.9395	161	13.960	.960
148	12.313	.847			
154	12.853	.884	167	13.650	.938
160	14.505	.997	173	13.563	.933
166	14.915	1.026			
172	15.125	1.040			
113	15.189	1.044			
119	15.086	1.037			
125	15.865	1.091			
131	16.047	1.103			

$P_{amb} \approx 14.543$ psia

P_T/P_0 T_T V_J

FAN

3.01

1495

2214

CORE

1.63

776

1097

12, *6
1, *4

P_T 215

MODEL # 2

CORE PLUG
STATICS
psia

FAN PLUG
STATICS
psia

112	12.310	.8465	137
118	13.856	.953	143
124	14.414	.991	
130	14.639	1.007	149
136	14.604	1.004	155
142	13.610	.936	161
148	12.311	.8465	
154	13.455	.925	167
160	14.481	.996	173
166	14.861	1.022	
172	15.090	1.038	
113	15.186	1.044	
119	15.106	1.039	
125	15.786	1.086	
131	15.963	1.098	

137	13.660	.939
143	13.522	.930
149	13.738	.945
155	13.410	.922
161	13.889	.955
167	13.636	.938
173	13.368	.919

P_{amb} ~ 14.542 psia

	P _T /P ₀	T _T	V _J
FAN	3.28	1632	2390
CORE	1.57	1010	1211

1, 4

PT 220

MODEL # 2

CORE PLUG
STATICS
psia

FAN PLUG
STATICS
psia

112	12.302	.847	137	13.694	.943
118	13.960	.961	143	13.580	.935
124	14.422	.993			
130	14.618	1.006	149	13.719	.944
136	14.573	1.003	155	13.445	.925
142	13.593	.936	161	13.832	.952
148	12.302	.847			
154	13.599	.936	167	13.166	.906
160	14.477	.996	173	13.167	.906
166	14.832	1.021			
172	15.062	1.037			
113	15.174	1.044			
119	15.117	1.040			
125	15.772	1.086			
131	15.922	1.096			

$P_{amb} = 14.528$ psia

P_T/P_0

T_r

V_J

FAN

3.56

1782

2571

CORE

1.54

1233

1315

2, *6
1, *4

PT 223

MODEL # 2

CORE PLUG
STATICS
psia

FAN PLUG
STATICS
psia

112	14.479	.998	137
118	14.034	.968	143
124	14.536	1.002	
130	14.592	1.006	149
136	14.476	.998	155
142	13.268	.915	161
148	10.616	.870	
154	13.543	.934	167
160	14.430	.995	173
166	14.709	1.014	
172	14.935	1.030	
113	15.020	1.036	
119	14.969	1.032	
125	14.530	1.002	
131	15.709	1.083	

13.897	.958
13.764	.949
13.804	.952
13.686	.944
14.000	.965
13.359	.921
13.511	.932

$P_{amb} \approx 14.504$ psia

	P_T/P_0	T_r	V_j
FAN	2.87	1442 1442	2132
CORE	1.50	1465	1395

1, 4

Pt 205

MODEL # 2

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CORE Plug
STATICS
psia

FAN Plug
STATICS
psia

X					
-0.1	112	21	12.343	.846	137
18	118	22	12.342	.846	143
-57	124	23	15.160	1.041 1.040	
1.03	130	24	15.020	1.043 1.03	149
1.44	136	25	15.173	1.041	155
1.80	142	26	14.147	.971	161
1.98	148	27	12.342	.846	
2.16	154	28	12.342	.846	167
2.49	160	29	14.397	.988	173
3.03	166	30	15.331	1.052	
3.84	172	31	15.284	1.049	
4.84	113	32	15.293	1.050	
5.53	119	33	15.112	1.038	
6.15	125	34	16.048	1.101	
6.59	131	35	16.286	1.118	

13.984	.960
13.845	.950
14.063	.965
13.685	.939
14.067	.965
13.875	.952
13.583	.932

Pamb = 14.573 psia

P _T /P ₀	T _r	V ₅
FAN - 28	2.72	1342
CORE - 8	1.80	552
		1010

CORE - 8

1.80 552 1010

2, °6
1, °4

P_T 225

MODEL # 2

CORE PLUG
STATICS
psia

FAN PLUG
STATICS
psia

112	12.284	.847	137	13.455	.927
118	13.757	.948	143	13.430	.926
124	14.347	.989			
130	14.578	1.005	149	13.579	.936
136	14.536	1.002	155	13.437	.926
142	13.675	.942	161	13.793	.951
148	10.284	.847			
154	13.749	.948	167	12.929	.891
160	14.476	.998	173	13.139	.906
166	14.803	1.020			
172	15.038	1.036			
113	15.161	1.045			
119	15.140	1.043			
125	15.696	1.082			
131	15.808	1.090			

P_{amb} = 14.509 psia

	P _T /P ₀	T _r	V _J
FAN	3.90	1986	2799
CORE	1.50	1452	1380

Pt 237

MODEL # 2

CORE PLUG
STATICS
psia

FAN PLUG
STATICS
psia

112	14.448	1.000 ^F	137	13.992	.969
118	12.216	.846	143	13.848	.953
124	14.355	.994			
130	14.491	1.003	149	13.805	.956
136	14.542	1.007	155	13.804	.956
142	13.306	.921	161	13.995	.969
148	12.444	.861			
154	12.787	.885	167	13.605	.942
160	14.398	.997	173	13.521	.936
166	14.820	1.026			
172	15.027	1.040			
113	15.087	1.044			
119	14.977	1.037			
125	14.535	1.006			
131	15.865	1.098			

$P_{amb} = 14.445$ psia

P_T/P_0

T_T

V_T

FAN

2.60

1706

2226

CORE

1.63

778

1102

0.163

2, *6
1, *4

PT 254

MODEL # 2

CORE PLUG
STATICS
psia

FAN PLUG
STATICS
psia

112	14.497	.9995	137	14.254	.983
118	12.282	.847	143	14.247	.982
124	14.917	1.028			
130	14.649	1.010	149	14.267	.984
136	14.642	1.0095	155	14.199	.979
142	13.457	.928	161		
148	12.282	.847			
154	12.282	.847	167	14.378	.991
160	14.198	.979	173	14.185	.978
166	14.885	1.026			
172	14.923	1.032			
113	14.977	1.033			
119	14.803	1.021			
125	14.548	1.003			
131	15.977	1.101			

$P_{amb} \approx 14.504$ psia

	P_T/P_0	T_r	V_J
FAN	1.50	727.	974
CORE	1.74	1460.	1608

L+1, 4

PT 257

MODEL # 2

ORIGINAL PAGE IS
OF POOR QUALITY

CORE PLUG
STATICS
psia

FAN PLUG
STATICS
psia

112	14.514	1.0006	137	14.233	.981
118	12.841	.885	143	14.210	.980
124	14.062	.969			
130	15.164	1.045	149	14.236	.981
136	15.086	1.040	155	14.141	.975
142	14.355	.990	161	14.313	.987
148	12.284	.847			
154	12.283	.847	167	14.322	.987
160	12.282	.847	173	14.105	.972
166	15.074	1.039			
172	15.777	1.088			
113	15.266	1.052			
119	15.040	1.037			
125	14.569	1.004			
131	16.320	1.125			

$P_{amb} \approx 14.506$ psia

	P_T/P_0	T_T	V_T
FAN	1.59	787	1086
CORE	2.05	1459	1807

Q-25

2, *6
1, *4

P_T 260

MODEL # 2

CORE PLUG
STATICS
psia

FAN PLUG
STATICS
psia

112	14.481	.998	137	14.188	.978
118	15.324	1.056	143	14.158	.976
124	15.140	1.044			
130	12.491	.861	149	14.146	.975
136	15.437	1.068	155	14.062	.969
142	14.889	1.026	161	14.249	.982
148	12.285	.847			
154	12.283	.847	167	14.112	.973
160	12.283	.847	173	14.046	.966
166	12.335	.854			
172	16.831	1.160			
113	15.699	1.082			
119	15.994	1.102			
125	14.567	1.004			
131	16.410	1.131			

P_{amb} = 14.506 psia

	P _T /P ₀	T _T	V _T
FAN	1.725	833	1202
CORE	2.46	1455	2002

PLUG STATICS

ORIGINAL PAGE IS
OF POOR QUALITY

P_T 270

14.446 psia = P_{amb} Bar

THROAT

CORE PLUG

- 14.448
- 14.083
- 14.101
- 14.149
- 14.134
- 14.153
- 14.138
- 14.125
- 14.279
- 14.068
- 14.068
- 14.299
- 14.563
- 14.457
- 15.107

P_T 270

$P_{T10}/P_0 = 3.85$

$T_{T10} = 1967$

$V_{10} = 2775$

$P_{T8}/P_0 = .983$

$V_8 = 0$

TIP

FAN PLUG

	<u>P_T 271</u>	<u>270</u>	<u>272</u>
1	13.86	13.653	13.915
2	13.728	13.568	13.845
4	13.838	13.441	13.971
5	13.746	13.581	13.817
6	13.986	13.844	14.048
8	13.522	12.825	13.831
9	13.542	13.316	13.675

4/7/71

PLUG STATICS

PT 271

$$14.445 \text{ psia} = P_{\text{amb}} \quad \text{BAR}$$

THREAT

14.454

14.232

14.244

14.272

14.265

14.272

14.298

14.265

14.338

14.228

14.255

14.487

14.709

14.463

15.010

CORE PLUG

TIP

$$P_{T18}/P_0 = 2.83$$

$$T_{T18} = 1394$$

$$V_{18} = 2083$$

$$P_{T0}/P_0 = .99$$

$$V_0 = 0$$

FAN PLUG

- 1 13.86
- 2 13.728
- 4 13.838
- 5 13.746
- 6 13.986
- 8 13.522
- 9 13.542

PLUG STATICS

Pt 272

ORIGINAL PAGE IS
OF POOR QUALITY

$$14.492 \text{ psia} = P_{amb} \quad \text{BAR}$$

14.373
14.395
14.417
14.450
14.440
14.442
14.450
14.454
14.454
14.450
14.431
14.436
14.498
14.617
Tip 14.716

Pt 272

$$P_{T_{10}}/P_0 = 2.44$$

$$T_{T_{10}} = 1214 \text{ }^\circ\text{R}$$

$$V_{10} = 1817$$

$$P_{T_0}/P_0 = 1.003$$

$$V_0 = 83.8$$

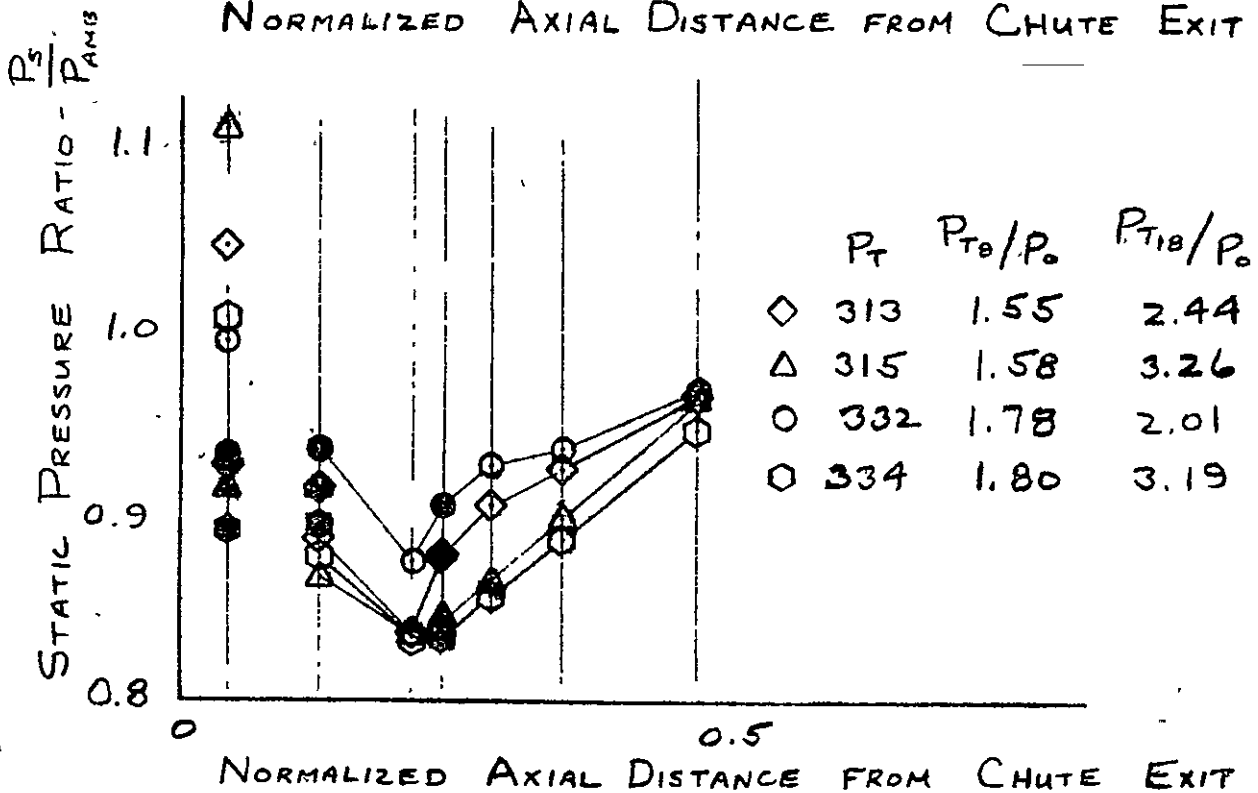
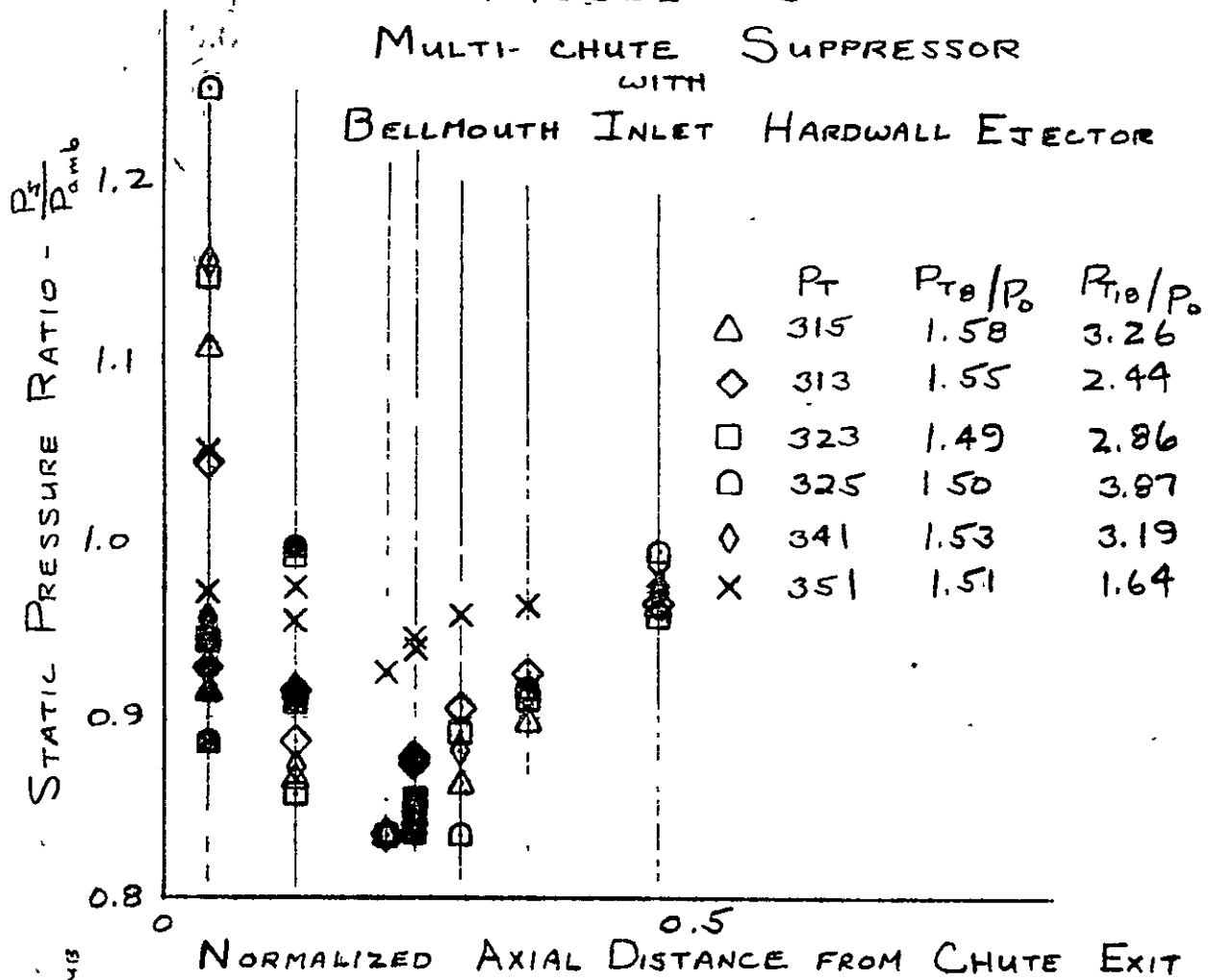
FAN PLUG

137	1	13.880
143	2	13.955
149	4	13.967
155	5	14.414
161	6	14.079
	8	13.803
	9	13.769

11/11

MODEL #3

MULTI-CHUTE SUPPRESSOR WITH BELLMOUTH INLET HARDWALL EJECTOR

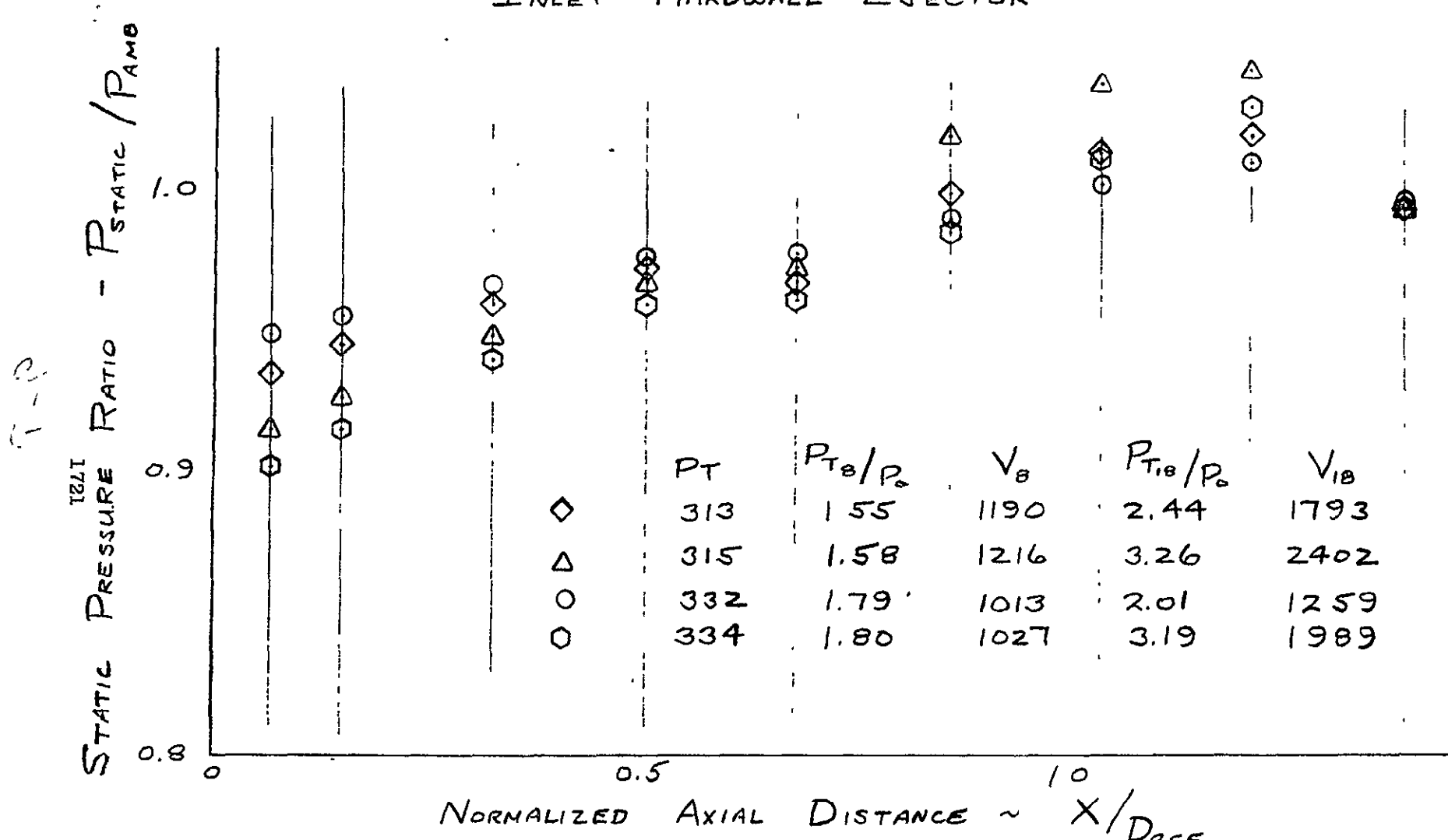


FAN PLUG PRESSURE DISTRIBUTIONS

1720

8-30 PH#
26 Sept 75

MULTI-CHUTE SUPPRESSOR WITH BELLMOUTH
INLET HARDWALL EJECTOR

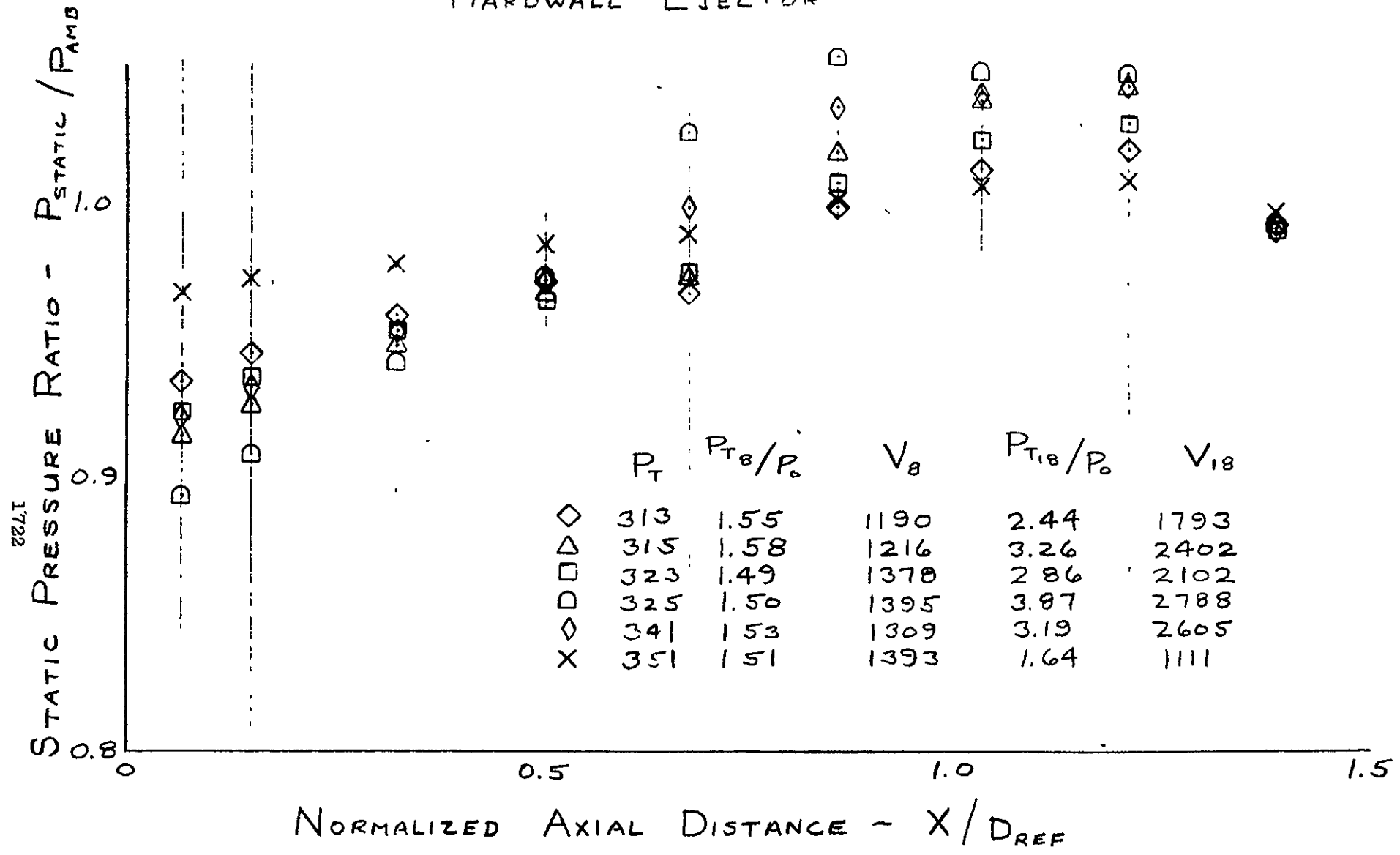


EJECTOR SHROUD PRESSURE DISTRIBUTIONS
MODEL * 3

168

ORIGINAL PAGE IS
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MULTI CHUTE SUPPRESSOR WITH BELLMOUTH INLET
HARDWALL EJECTOR



	P_T	P_{T18}/P_0	V_0	P_{T18}/P_0	V_{18}
◇	313	1.55	1190	2.44	1793
△	315	1.58	1216	3.26	2402
□	323	1.49	1370	2.86	2102
○	325	1.50	1395	3.87	2788
◇	341	1.53	1309	3.19	2605
X	351	1.51	1393	1.64	1111

EJECTOR SHROUD PRESSURE DISTRIBUTIONS
MODEL * 3

9-20

158

1722

P_T

MODEL # 3

HARDWALL EJECTOR - CHUTES

EJECTOR STATICS

Fan Plug Statics

EC	LINE	GE
63	112	
64	118	
65	124	
66	130	
67	136	
68	142	
69	148	
70	154	
71	172	

P_s	psia	P_s/P_0
X	.40	
	.90	
	1.96	
	3.02	
	4.08	
	5.14	
	6.20	
	7.26	
	8.32	

LINE	FEC	P_s	psia	P_s/P_0
GE		X		$\times 10/P_0$
160	37	.265		.014
166	38	.725		.121
113	41	1.415		.236
119	43	.265		.044
125	44	.125		.121
131	46	1.242		.207
137	47	1.415		.236
143	48	1.682		.285
149	49	2.035		.333
155	51	2.79		.465

CHUTE BASE

	P_s	psia	P_s/P_0
161	52		
167	54		
173	56		

$P_{amb.}$

$P_0 =$ psia

P_T/P_0

T_T

V_T

FAN

CORE

4.33

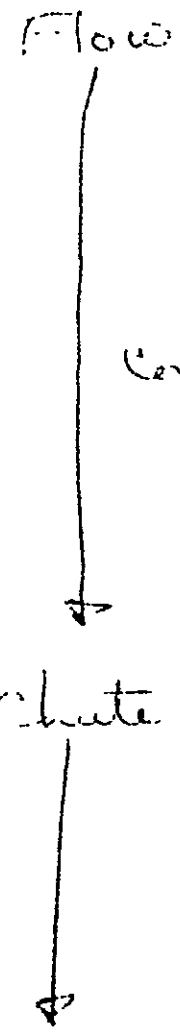
Model # 1

Multi-CHANCE

TAN PLUG

FEC	chute	Exit	N-ARC	of	CH	G.E
						LINE
51	2.79	2	38		355°	155
50	2.41	2	000		345°	
49	2.035	1.625			335°	149
48	1.682	1	272		355°	143
47	1.415	1	005		345°	137
46	1.242		.832		335°	131
45	1.09		680		355	
44	.725		315		345°	125
43	.265	-	145		335°	119
42	.19	-	220		355°	
41	1.415	1	005		90°	113
40	1.242		.832		80°	
39	1.090		680		70°	172
38	.725		315		90°	166
37	.265	-	145		80°	160
36	.190	-	220		70°	154

$\Delta = 0.41^\circ$
 Chute EXIT



Chute Base T-RADIUS

52	3.83	0°	161
53	3.98	10°	
54	4.13	20°	167
55	4.28	30°	
56	4.43	40°	173
57	4.58	50°	
58	4.72	60°	

g. 34

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PT 313

MODEL # 3

HARDWALL EJECTOR - CHUTES
BELLMOUTH

EJECTOR STATICS

LINE	P_s psia	P_s/P_0
112	13.511	.935
118	13.648	.945
124	13.848	.959
130	14.042	.972
136	13.973	.967
142	14.412	.998
148	14.621	1.012
154	14.710	1.018
172	14.327	.992

Fan Plug Statics

LINE	P_s psia	P_s/P_0
160	13.400	.928
166	13.227	.916
113	12.696	.879
119	15.066	1.043
125	12.831	.888
131	12.071	.836
137	12.690	.878
143	13.094	.906
149	13.347	.924
155	13.928	.964

$P_{amb.}$

$P_0 = 14.445$ psia

CHUTE BASE

	P_s psia	P_s/P_0
161	13.379	.926
167	13.434	.930
173	13.245	.917

	P_T/P_0	T_T	V_T
FAN	2.44	1182	1793
CORE	1.55	995	1190

9.75

P_T 315

MODEL # 3

HARDWALL EJECTOR - CHUTES
BELLMOUTH

EJECTOR STATICS

LINE	psia	
	P_s	P_s/P_0
112	13.206	.915
118	13.368	.926
124	13.685	.948
130	13.962	.967
136	14.036	.972
142	14.703	1.018
148	14.954	1.036
154	15.028	1.041
172	14.305	.991

Fan Plug Statics

LINE	psia	
	P_s	P_s/P_0
160	13.174	.914
166	13.205	.915
113	12.166	.843
119	16.005	1.109
125	12.508	.866
131	12.019	.833
137	12.127	.840
143	12.452	.863
149	12.970	.898
155	13.874	.961

P_{amb.}

P₀ = 14.435 psia

CHUTE BASE

	psia	
	P_s	P_s/P_0
161	12.878	.892
167	13.370	.926
173	13.163	.912

	P_T/P_0	T _T	V _T
FAN	3.265	1652	2402

CORE	1.58	1008	1216
------	------	------	------

gjk

P_T 323

MODEL # 3

HARDWALL EJECTOR CHUTES

EJECTOR STATICS

LINE	<u>P_s</u> psia	<u>P_s/P₀</u>
112	13.334	.924
118	13.496	.936
124	13.751	.953
130	13.976	.969
136	14.056	.974
142	14.519	1.0065
148	14.746	1.022
154	14.834	1.028
172	14.285	.990

Fan Plug Statics

LINE	<u>P_s</u> psia	<u>P_s/P₀</u>
160	13.585	.942
166	13.134	.910
113	12.314	.854
119	16.558	1.148
125	12.376	.858
131	12.013	.833
137	12.262	.850
143	12.865	.892
149	13.129	.910
155	13.823	.958

P_{amb.}

P₀ = 14.425 psia

CHUTE BASE

	<u>P_s</u> psia	<u>P_s/P₀</u>
161	13.315	.923
167	13.377	.927
173	13.153	.912

P_T/P₀

T_T

V_T

FAN 2.86 1405 2102

CORE 1.49 1450 1378

(1.2) 1

P_T 325

MODEL # 3

HARDWALL EJECTOR - CHUTES BELL MOUTH

EJECTOR STATICS

LINE	<u>P_s</u> psia	<u>P_s/P₀</u>
112	12.887	.894
118	13.099	.909
124	13.580	.942
130	14.031	.973
136	14.781	1.025
142	15.161	1.052
148	15.100	1.047
154	15.076	1.046
172	14.301	.992

Fan Plug Statics

LINE	<u>P_s</u> psia	<u>P_s/P₀</u>
160	12.777	.886
166	14.374	.997
113	12.005	.833
119	18.032	1.251
125	14.273	.990
131	12.005	.833
137	12.004	.833
143	12.004	.833
149	13.193	.915
155	14.302	.992

P_{amb.}

P₀ = 14.416 psia

CHUTE BASE

	<u>P_s</u> psia	<u>P_s/P₀</u>
161	12.643	.877
167	13.439	.932
173	13.360	.927

P_T/P₀

T_T

V_T

FAN 3.87 1978 2788

CORE 1.50 1470 139.5

g(2)1

P_T 341

MODEL # 3

HARDWALL EJECTOR CHUTES

EJECTOR STATICS

LINE	<u>P_s</u> psia	<u>P_s</u> / <u>P₀</u>
112	13.300	.922
118	13.455	.933
124	13.744	.953
130	14.020	.972
136	14.373	.998
142	14.903	1.034
148	14.982	1.039
154	15.011	1.041
172	14.258	.989

Fan Plug Static

LINE	<u>P_s</u> psia	<u>P_s</u> / <u>P₀</u>
160	13.765	.955
166	13.218	.917
113	12.244	.849
119	16.680	1.157
125	12.576	.872
131	12.008	.833
137	12.237	.849
143	12.697	.881
149	13.144	.912
155	13.979	.970

CHUTE BASE

	<u>P_s</u> psia	<u>P_s</u> / <u>P₀</u>
161	13.168	.913
167	13.463	.934
173	13.325	.924

P_{amb.}

P₀ = 14.418 psia

P_T/
P₀

T_T

V_T

FAN	3.19	1966	2605
CORE	1.53	1243	1309

8.29

P_T 351

MODEL # 3

HARDWALL EJECTOR - CHUTES

EJECTOR STATICS

LINE	<u>P_s</u> psia	<u>P_s/P₀</u>
112	13.968	.967
118	14.034	.972
124	14.127	.978
130	14.225	.985
136	14.266	.988
142	14.443	1.000 ⁺
148	14.510	1.005
154	14.544	1.007
172	14.376	.996

Fan Plug Statics

LINE	<u>P_s</u> psia	<u>P_s/P₀</u>
160	14.001	.970
166	13.780	.954
113	13.554	.939
119	15.138	1.048
125	14.021	.971
131	13.331	.923
137	13.613	.943
143	13.772	.954
149	13.875	.961
155	14.141	.979

CHUTE BASE

	<u>P_s</u> psia	<u>P_s/P₀</u>
161	13.787	.955
167	13.756	.953
173	13.700	.949

P_{amb.}

P₀ = 14.440 psia

	<u>P_T/P₀</u>	<u>T_T</u>	<u>V_T</u>
FAN	1.64	778	1111
CORE	1.51	1450	1393

4-4

P_T 332

MODEL # 3

HARDWALL EJECTOR - CHUTES

EJECTOR STATICS

Fan Plug Statics

LINE	<u>P_s</u> psia	<u>P_s/P₀</u>	LINE	<u>P_s</u> psia	<u>P_s/P₀</u>
112	13.697	.9485	160	13.466	.932
118	13.797	.955	166	13.518	.936
124	13.950	.966	113	13.063	.905
130	14.100	.976	119	14.333	.993
136	14.165	.977	125	13.519	.936
142	14.282	.989	131	12.637	.875
148	14.471	1.002	137	13.084	.906
154	14.572	1.009	143	13.405	.928
172	14.370	.995	149	13.531	.937
			155	13.979	.968

P_{amb.}

P₀ = 14.440 psia

CHUTE BASE

	<u>P_s</u> psia	<u>P_s/P₀</u>
161	13.563	.939
167	13.487	.934
173	13.447	.931

	<u>P_T/P₀</u>	<u>T_T</u>	<u>V_J</u>
FAN	2.01	728	1259
CORE	1.79	556	1013

P_T 334

MODEL # 3

HARDWALL EJECTOR - CHUTES

EJECTOR STATICS

LINE	psia	
	P_s	P_s/P_0
112	13.028	.902
118	13.218	.915
124	13.566	.939
130	13.851	.959
136	13.864	.960
142	14.214	.984
148	14.576	1.010
154	14.846	1.028
172	14.328	.992

Fan Plug Statitics

LINE	psia	
	P_s	P_s/P_0
160	12.889	.892
166	12.915	.894
113	12.058	.835
119	14.546	1.007
125	12.665	.877
131	12.026	.832
137	12.089	.837
143	12.386	.857
149	12.818	.887
155	13.679	.947

P_{amb.}

P₀ = 14.447 psia

CHUTE BASE

	psia	
	P_s	P_s/P_0
161	12.712	.894
167	13.135	.909
173	12.768	.898

P_T/P₀

T_T

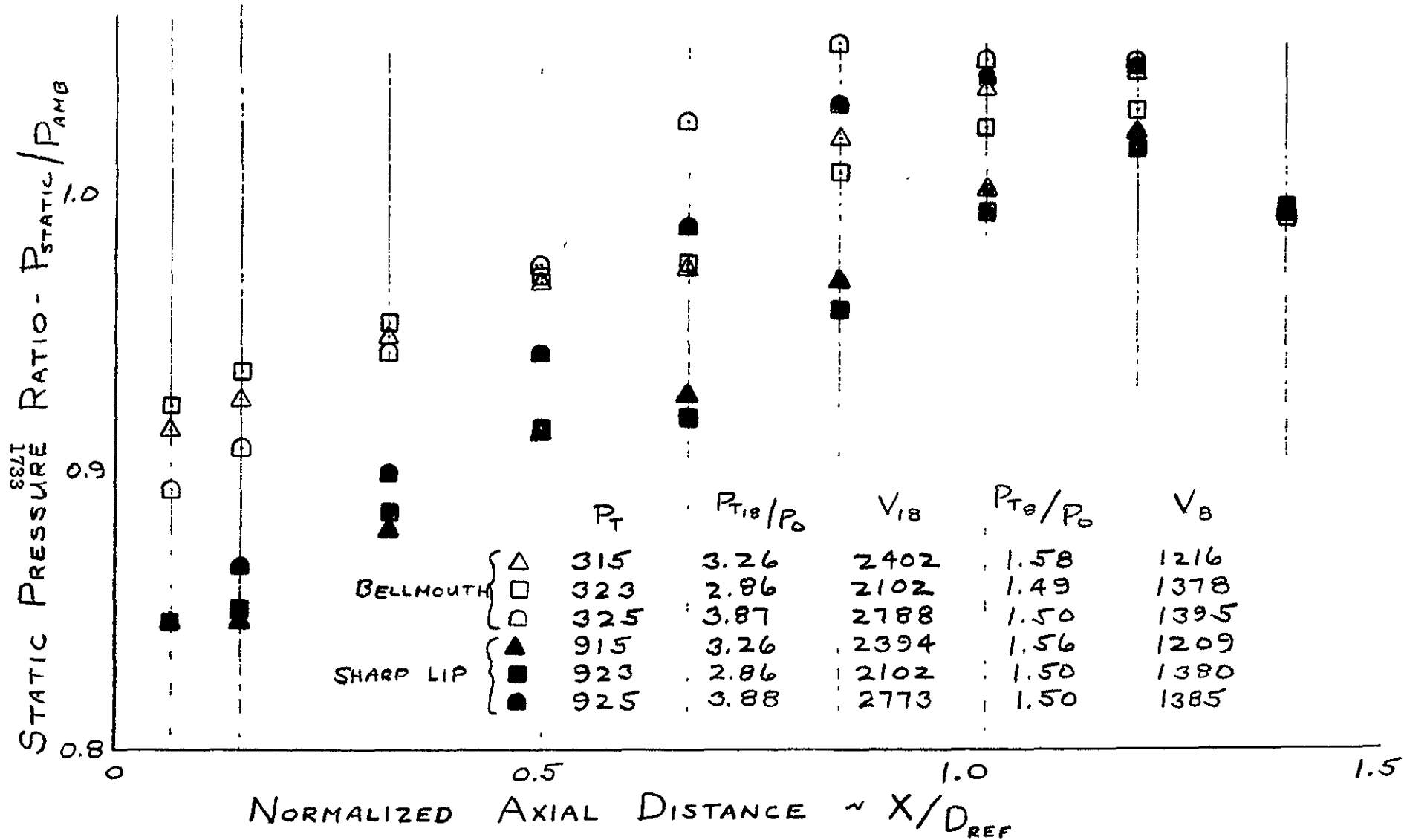
V_T

FAN 3.19 1163 1989

CORE 1.80 570 1027

G-42

MULTI-CHUTE SUPPRESSOR WITH HARDWALL EJECTOR



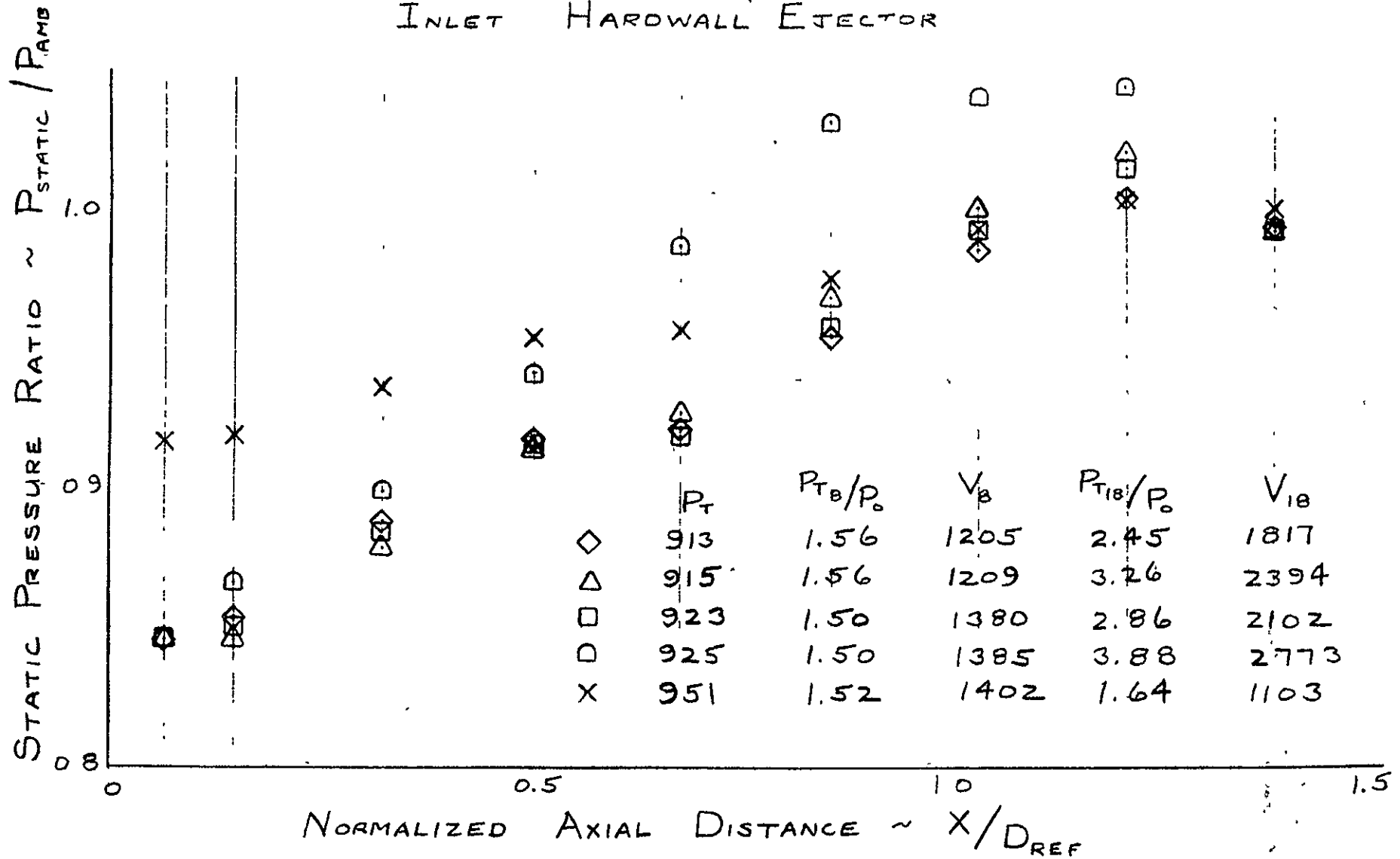
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GH-8

29 JUL 1975

MULTI-CHUTE SUPPRESSOR WITH SHARP LIP
INLET HARDWALL EJECTOR

1734



EJECTOR SHROUD PRESSURE DISTRIBUTIONS
MODEL * 9

8-11-8

P_T 913

MODEL # 9

HARDWALL EJECTOR CHUTES
SHARP LIP

EJECTOR STATICS

LINE	<u>P_s</u> psia	<u>P_s/P₀</u>
112	12.221	.846
118	12.338	.854
124	12.828	.888
130	13.269	.918
136	13.308	.921
142	13.783	.954
148	14.234	.985
154	14.503	1.004
154	14.368	.994

Fan Plug Statics

LINE	<u>P_s</u> psia	<u>P_s/P₀</u>
112	12.219	.846
166	13.454	.931
113	12.043	.833
119	15.464	1.070
125	13.054	.903
131	12.043	.833
137	12.043	.833
143	12.175	.842
149	12.370	.856
155	13.194	.913

CHUTE BASE

	<u>P_s</u> psia	<u>P_s/P₀</u>
161	14.054	.972
167	14.176	.981
173	14.179	.981

P_{amb.}
P₀ = 14.451 psia

	<u>P_T/P₀</u>	<u>T_T</u>	<u>V_T</u>
FAN	2.45	1209	1817
CORE	1.56	1005	1205

2.45

PT 915

MODEL # 9

HARDWALL EJECTOR - CHUTES SHARP LIP

EJECTOR STATICS

LINE	P_s psia	P_s/P_0
112	12.221	.846
118	12.219	.846
124	12.702	.879
130	13.203	.914
136	13.389	.927
142	13.985	.968
148	14.450	1.000
154	14.740	1.020
0 154	14.330	.992

Fan Plug Statics

LINE	P_s psia	P_s/P_0
172 172	12.220	.846
166	13.609	.942
113	12.043	.833
119	16.137	1.117
125	13.097	.906
131	12.041	.833
137	12.040	.833
143	12.041	.833
149	12.041	.833
155	13.183	.912

$P_{amb.}$

$P_0 = 14.450$ psia

CHUTE BASE

	P_s psia	P_s/P_0
161	14.113	.977
167	14.134	.978
173	14.160	.980

	P_T/P_0	T_T	V_T
FAN	3.26	1643	2394
CORE	1.56	1013	1209

4-46

P_T 923

MODEL # 9

HARDWALL EJECTOR CHUTES
SHARP LIP

EJECTOR STATICS

Fan Plug Static

LINE	<u>P_s</u> psia	<u>P_s/P₀</u>	LINE	<u>P_s</u> psia	<u>P_s/P₀</u>
112	12.219	.8465	172	12.217	.8465
118	12.261	.85	166	13.535	.9375
124	12.776	.885	113	12.039	.8335
130	13.203	.915	119	16.664	1.154
136	13.265	.919	125	12.832	.889
142	13.806	.957	131	12.040	.8335
148	14.308	.992	137	12.039	.8335
154	14.635	1.014	143	12.039	.8335
150 150	14.343	.993	149	12.115	.84
			155	13.125	.909

P_{amb.}

P₀ = 14.447 psia

CHUTE BASE

	<u>P_s</u> psia	<u>P_s/P₀</u>
161	14.013	.97
167	14.162	.9815
173	14.165	.9815

	<u>P_T/P₀</u>	<u>T_T</u>	<u>V_T</u>
FAN	2.86	1404	2102
CORE	1.50	1451	1380

2.117

MODEL # 8 * 9

PT 925

HARDWALL EJECTOR - CHUTES
SHARP LIP

EJECTOR STATICS

LINE	P_s psia	P_s/P_0	LINE
112	12.219	.846	172 165
118	12.514	.866	166
124	12.991	.899	113
130	13.591	.941	119
136	14.261	.987	125
142	14.808	1.0305	131
148	15.022	1.040	137
154	15.077	1.044	143
154	14.325	.992	149
			155

Fan Plug Statics

P_s psia	P_s/P_0
12.217	.846
14.474	1.002
12.040	.833
17.838	1.235
15.102	1.045
12.040	.833
12.041	.833
12.040	.833
12.543	.862
13.966	.967

$P_{amb.}$

$P_0 = 14.447$ psia

CHUTE BASE

	P_s psia	P_s/P_0
161	13.293	.920
167	14.054	.973
173	14.178	.981

	P_T/P_0	T_T	V_T
FAN	3.88	1957	2773
CORE	1.50	1463	1385

e-48

PT 951

MODEL # 9

HARDWALL EJECTOR - CHUTES
SHARP LIP

EJECTOR STATICS

Fan Plug Statics

LINE	P_s psia	P_s/P_0
112	13.249	.917
118	13.278	.919
124	13.518	.936
130	13.787	.954
136	13.805	.956
142	14.068	.974
148	14.329	.992
154	14.484	1.003
154	14.449	1.0003

LINE	P_s psia	P_s/P_0
172 166	13.031	.902
166	13.813	.956
113	13.117	.908
119	15.289	1.058
125	13.833	.958
131	12.965	.898
137	13.267	.914
143	13.351	.924
149	13.395	.927
155	13.739	.951

$P_{amb.}$

$P_0 = 14.445$ psia

CHUTE BASE

	P_s psia	P_s/P_0
161	14.221	.984
167	14.309	.991
173	14.300	.990

	P_T/P_0	T_T	V_T
FAN	1.64	765	110.3
CORE	1.52	1454	1402

Pt 508

MODEL *5

HARDWALL EJECTOR

CORE PLUG STATICS

psia

112 12.149

130 13.948

148 12.149

166 14.608

119 14.952

131 15.904

EJECTOR STATICS

psia

118 13.109

124 13.262

136 13.524

142 13.716

154 13.915

160 14.375

172 14.532

113 14.617

125 14.259

FAN PLUG STATICS

psia

137 12.669

143 12.852

149 12.564

155 14.256

161 13.006

167 12.433

173 12.512

$P_{amb} = 14.376$ psia

P_T/P_0

T_T

V_J

FAN 2.26 1056 1625

CORE 1.630 766 1075

Pt 510

MODEL #5

HARDWALL EJECTOR

CORE PLUG
STATICS

psia

112 12.142

130 13.730

148 12.141

166 14.643

119 15.166

131 16.102

EJECTOR
STATICS

psia

118 12.715

124 12.872

136 13.165

142 13.425

154 13.697

160 14.342

172 14.641

113 14.848

125 14.131

FAN PLUG
STATICS

psia

137 11.958

143 12.147

149 11.954

155 ~~14.262~~

161 12.396

167 11.955

173 11.954

1741

$P_{amb} = 14.376$ psia

P_T/P_0

T_T

V_T

FAN 2.99 1481 2198

CORE 1.64 768 1104

0.51

PT 5.20

MODEL #5

HARDWALL EJECTOR

CORE PLUG STATICS

psia

112 12.150

130 13.607

148 12.150

166 14.516

119 15.213

131 15.911

EJECTOR STATICS

psia

118 12.554

124 12.682

136 13.001

142 13.304

154 13.642

160 14.336

172 14.686

113 14.995

125 14.073

FAN PLUG STATICS

psia

137 11.966

143 11.964

149 11.964

155 ~~14.206~~

161 12.253

167 11.963

173 11.963

$P_{amb} = 14.381$ psia

P_T/P_0

T_T

V_J

FAN 3.54 1788 2573

CORE 1.54 1219 1310

1742

52

P 551

MODEL #5

HARD WALL EJECTOR

CORE PLUG
STATICS
psia

EJECTOR
STATICS
psia

112	12.143	.845			
118				13.686	.9525
124				13.781	
130	13.998				
136				13.931	
142				14.029	
148	12.142	.845			
154				14.109	
160				14.319	
166	14.420				
172				14.441	
113				14.476	
119	14.733				
125				14.327	
131	15.501				

$P_{amb} = 14.378$ psia

FAN PLUG
psia

P_T / P_0 T_T V

137	13.405	.933			
143	13.536	.942			
149	13.421	.934	FAN	1.52	1439 1395
155	14.142				
161	13.665	.952			
167	13.501	.940	CORE	1.64	769 1102
173	13.398	.932			

Pt 525

MODEL *5

HARDWALL EJECTOR

CORE PLUG
STATICS

psia

EJECTOR
STATICS

psia

112 12.150

118 12.574

124 12.679

130 13.632

136 12.992

142 13.309

148 12.150

154 13.682

160 14.409

166 14.549

172 14.740

113 15.111

119 15.1282

125 13.982

131 15.834

FAN PLUG
STATICS

psia

$P_{amb} = 14.381$ psia

P_T/P_0 T_T V_T

137 11.968

143 11.964

FAN 3.87 1763 2776

149 11.965

155 ~~14.205~~

161 11.965

CORE 1.50 1460 13901

167 11.964

1744

173 11.963

Pt 5 13

MODEL #5

HARDWALL EJECTOR

CORE PLUG
STATICS

psia

EJECTOR
STATICS

psia

112	12.150	118	12.954
		124	13.129
130	13.828	136	13.430
		142	13.651
148	12.150	154	13.872
		160	14.404
166	14.545	172	14.580
		113	14.673
119	14.978	125	14.252
131	15.785		

FAN PLUG
STATICS

psia

$P_{amb} = 14.381$ psia

P_T/P_0 T_T V_T

137	12.385			
143	12.612			
149	12.514	FAN	2.45	1207 1815
155	14.226			
161	12.873	CORE	1.57	988 1198
167	11.971			
173	12.260			

Pt 515

MODEL *5

HARDWALL EJECTOR

CORE PLUG
STATICS
psia

EJECTOR
STATICS
psia

112 12.151

118 12.591

124 12.748

130 13.648

136 13.058

142 13.355

148 12.151

154 13.652

160 14.331

166 14.525

172 14.670

113 14.925

119 15.168

125 14.130

131 15.950

FAN PLUG
STATICS
psia

$P_{amb} = 14.382$ psia

P_T/P_0 T_T V_T

137 11.966

143 12.000

FAN 3.26 1635 237.8

149 11.964

155 ~~14.217~~

161 12.387

CORE 1.57 988 1199

167 11.964

173 11.964

Pt 503

MODEL #5

HARDWALL EJECTOR

CORE PLUG
STATICS

psia

EJECTOR
STATICS

psia

112	12.142	63 118	13.236
		64 124	13.700
130	14.124	65 136	13.602
		66 142	13.778
148	12.142	67 154	13.925
		68 160	14.277
166	14.954	69 172	14.506
		70 113	14.573
119	14.954	71 125	14.304
131	16.119		

FAN PLUG
STATICS

psia

$$P_{amb} = 14.38 \text{ psia}$$

		P_T/P_0	T_T	V_T
137	12.867			
143	13.017			
		FAN	2.06	1002
149	12.875			1501
155	14.206			
161	13.241	CORE	1.80	536
				1000
167	13.047			
173	12.897			

Pt 505

MODEL *5

HARDWALL EJECTOR

CORE PLUG
STATICS
psia

EJECTOR
STATICS
psia

112 12.142

118 12.809

124 12.968

130 13.840

136 13.247

142 13.482

148 12.140

154 13.774

160 14.718

166 14.802

172 14.614

113 14.772

~~15.190~~
119 15.190

125 14.190

131 16.362

FAN PLUG
STATICS
psia

$P_{amb} = 14.377$ psia

137 12.126

P_T/P_0 T_T V_J

143 12.376

FAN 2.73 1343 2014

149 12.136

155 ~~14.233~~

161 12.593

CORE 1.80 545 100.6

167 11.953

173 11.974

PT 534

MODEL *5

HARDWALL EJECTOR

CORE PLUG
STATICS

psia

EJECTOR
STATICS

psia

112	12.276	.846	?
130	13.976	.964	
148	12.276	.846	?
166	14.285	.984	
119	15.340	1.057	
131	16.558	1.141	

118	12.410	.856
124	12.611	.87
136	12.783	.895
142	13.300	.917
154	13.544	.933
160	14.021	.966
172	14.576	1.005
113	14.943	1.030
125	14.367	.988

FAN PLUG
STATICS

psia

$P_{amb} = 14.514$ psia

P_T/P_0

T_T

V_T

137	12.094	} Cavity P_s .834
143	12.094	
149	12.094	
155	14.683	1.011
161	12.224	.843
167	12.094	} Cavity P_s
173	12.094	

FAN	3.17	1170	1992
CORE	1.81	551	1018

P_T 536

MODEL *5

HARDWALL EJECTOR

CORE PLUG
STATICS
psia

EJECTOR
STATICS
psia

112 12.256 .846

118 12.393 .856

124 12.625 .872

130 13.798 .953

136 13.023 .90

142 13.315 .92

148 12.256 .846

154 13.547 .936

160 13.917 .962

166 14.480 .999⁺

172 14.464 .999

113 14.812 1.024

119 15.124 1.045

125 14.321 .989

131 16.106 1.112

FAN PLUG
STATICS
psia

P_{amb} = 14.494 psia

137 12.076 }
143 12.075 } .834

P_T/P₀ T_T V_J

149 12.075 }
155 14.604 } 1.009

FAN 3.05 806 1628

161 12.354 .854

CORE 1.63 761 1092

167 12.075 }
173 12.075 } .834

*2, *6
*4

PT 726

MODEL # 7

CORE PLUG
STATICS
psia

FAN PLUG
STATICS
psia

112 13.963

118 14.847

124 14.891

130 14.563

136 14.251

142 14.067

148 12.269

154 13.715

160 14.339

166 14.490

172 14.703

113 14.804

119 14.765

125 15.263

131 15.382

137 14.502

143 14.502

149 14.502

155 14.500

161 14.500

167 14.502

173 14.500

$P_{amb} \sim 14.504$ psia

P_T/P_0

T_T

V_T

FAN

1.524

717

989

CORE

1.369

1004

1018

*2, *6
*1, *4

15/2

PT 728

MODEL # 7

CORE PLUG
STATICS
psia

FAN PLUG
STATICS
psia

112	14.785	1.021	137	Amb
118	15.659	1.081	143	✓
124	15.740	1.086		
130	15.212	1.050	149	✓
136	14.681	1.013	155	✓
142	14.131	.975	161	✓
148	12.270	.847		
154	13.765		167	✓
160	14.368		173	✓
166	14.579			
172	14.862			
113	15.009			
119	15.002			
125	15.495			
131	15.619			

$P_{amb} \approx 14.498$ psia

P_T/P_0

T_r

V_5

FAN

2.734

1354

2024

CORE

1.389

992

1035

*2, *6
*1, *4

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15/21

MODEL #7

PT 730
(FEC 20)

CORE PLUG
STATICS
psia

FAN PLUG
STATICS
psia

112	13.775	.952	137	Amb
118	16.769	1.173	143	✓
124	17.404	1.202		
130	16.132	1.115	149	✓
136	15.705	1.086	155	✓
142	14.388	.994	161	Amb
ITY 148	12.252	.865		
154	12.250	.864	167	✓
160	12.249	.863	173	✓
166	14.222	.983		
172	15.781	1.105		
113	15.657	1.081		
119	15.275	1.055		
125	16.294	1.125		
131	16.679	1.153		

$P_{amb} \approx 14.475$ psia

FAN

P_T/P_0
2.861

T_r
1415

V_j
2110

CORE

1.869

1003

1406

*2, *6
*1, *4

17/2

MODEL # 7

PT 731
(FEC 21)

CORE PLUG
STATICS
psia

FAN PLUG
STATICS
psia

CAVITY 112	12.411	.848	137	Amb
" 118	12.410	.848	143	✓
124	16.271	1.111		
130	16.679	1.140	149	✓
136	16.822	1.149	155	✓
142	14.697	1.004	161	✓
CAVITY 148	12.412	.848		
" 154	12.410	.848	167	✓
160	12.420	.8485	173	✓
166	13.739	.938		
172	15.631	1.068		
113	15.933	1.089		
119	15.788	1.078		
125	16.758	1.132		
131	17.187	1.174		

$P_{amb} = 14.645$ psia

	P_T/P_0	T_T	V_T
FAN	3.864	1965	2777
CORE	1.86	1002	1409