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Numerical Procedure To Determine  
Geometric View Factors for  
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National Aeronautics  
and Space Administration

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## SUMMARY

A numerical procedure has been developed to determine geometric view factors between connected infinite strips occluded by any number of infinite circular cylinders. The procedure requires a two-dimensional cross-sectional model of the configuration of interest. The two-dimensional model consists of a convex polygon enclosing any number of circles. Each side of the polygon represents one strip, and each circle represents a circular cylinder. A description and listing of a computer program based on this procedure are included in this report. The program calculates geometric view factors between individual strips and between individual strips and the collection of occluding cylinders.

## INTRODUCTION

Most comprehensive thermal analyzers which deal with radiation (such as MITAS (ref. 1)) require, as part of their input, geometric view factors which define the fraction of radiant energy emanating from one surface and intercepted by another. Reliable computer programs (such as CONFAC II (ref. 2)) are available for calculating geometric view factors for many complex configurations, and geometric view factors for simple configurations can be obtained from tables or calculated by hand. However, a simple method is not currently available for calculating geometric view factors for surfaces occluded by multiple arbitrarily located circular cylinders. This configuration is frequently encountered in heater arrays with tubular elements and can be analyzed with sufficient accuracy for many applications by using a two-dimensional model.

This report describes a numerical procedure to determine geometric view factors between connected infinite strips that enclose any number of arbitrarily located circular cylinders. The computer program which performs the computation and its input requirements are described, and a demonstration problem and a listing of the program are included.

## SYMBOLS

Values are given in both SI and U.S. Customary Units. The measurements and calculations were made in U.S. Customary Units.

C	center of tube
$C_{V-J}$	configuration factor from view point V to region J
$D_1, D_2$	two endpoints of destination region
$\overline{D_1 D_2}$	destination region
$F_{I-J}$	geometric view factor from region I to region J

$M$	distance in x-direction from view point to center of occluding tube
$N$	distance in y-direction from view point to center of occluding tube
$N_{reg}$	number of regions
$N_{vp}$	number of view points in region
$\vec{n}$	vector normal to source region at view point
$P_1, P_2$	two endpoints of unshadowed portion of destination region
$\overline{P_1P_2}$	unshadowed portion of destination region
$r$	radius of tube
$S_1, S_2$	two endpoints of source region
$\overline{S_1S_2}$	source region
$T_1, T_2$	two points of tangency
$V$	view point
$X, Y$	global axis system
$X'$	line passing through view point parallel to X-axis
$Y'$	line passing through view point parallel to Y-axis
$x, y$	global coordinates
$\alpha_1$	angle formed by normal to source region at view point and $\overline{VP_1}$ , measured clockwise
$\alpha_2$	angle formed by normal to source region at view point and $\overline{VP_2}$ , measured counterclockwise
$\theta_C$	angle from $X'$ to $\overline{VC}$
$\theta_n$	angle from $X'$ to $\vec{n}$
$\theta_{P_1}$	angle from $X'$ to $\overline{VP_1}$
$\theta_{P_2}$	angle from $X'$ to $\overline{VP_2}$
$\theta_{T_1}$	angle from $X'$ to $\overline{VT_1}$
$\theta_{T_2}$	angle from $X'$ to $\overline{VT_2}$
$\Delta\theta$	$= \theta_C - \theta_{T_1}$

## Subscripts:

D	destination region
S	source region
T	tubes
V	view point

## GENERAL DESCRIPTION OF NUMERICAL PROCEDURE

A numerical procedure was developed to compute geometric view factors between connected infinite strips that enclose any number of arbitrarily located circular cylinders. The procedure requires a two-dimensional cross-sectional model of the configuration of interest. The two-dimensional model consists of a convex polygon enclosing any number of circles, hereafter called tubes. Each side of the polygon represents one strip, and the tubes represent the circular cylinders. Any number of strips and cylinders may be defined in the model with no change to the computer program itself, because computer memory is dynamically allocated according to problem size. There is, of course, a maximum number of strips and tubes that may be analyzed within the user's computer memory allotment.

## ANALYSIS

The geometric view factors required as input in most comprehensive thermal analyzers may be approximated for many applications by geometric view factors based on a two-dimensional cross-sectional model of the configuration of interest. A typical cross-sectional model of a pentagonal enclosure with three arbitrarily located circular cylinders is illustrated in figure 1. In the two-dimensional analysis, geometric view factors are required from each side of the pentagon to each remaining side and also from each side to the collection of circles. Since a geometric view factor represents the fraction of radiant energy emanating from one region which is intercepted by another, one side of the model must be considered a "source" region while all others are in turn considered "destination" regions. In figure 1, region  $S_1S_2$  is the source region, region  $D_1D_2$  is the destination region, and the geometric view factor computed is from  $S_1S_2$  to  $D_1D_2$ .

The equation for this geometric view factor involves an integration over the source region, which is performed using a closed-form approach when occlusion is not present. In complicated configurations, however, the integration is performed by dividing the source region into a finite number of subregions and averaging the geometric view factors from all subregions. The energy emanating from each of the subregions is considered constant over that subregion, so a representative point, called a view point, at the center of the subregion may be used as the energy source in the computation. The fraction of total energy emanating from this view point which is intercepted by the destination region is called the configuration factor from the point to the

region. Hence, the geometric view factor from a source region to a destination region is the average of configuration factors from a finite number of view points spaced evenly along the source region. The number of view points used in computation may be increased to improve the accuracy of the resulting geometric view factor.

When there is no occlusion between source and destination regions, this computation is relatively simple to perform. If no tubes are present in the triangle formed by the view point and the endpoints of the destination region, then the destination region receives all radiant energy cast in its direction from the view point. If tubes are present in the triangle, however, the tubes intercept a fraction of this energy, and the configuration factor to that destination region is proportionately reduced. The triangle formed by the view point and the ends of the destination region is called the look wedge. When occlusions are present, the configuration factor from a view point to the destination region is equal to the sum of the configuration factors from that view point to each unshadowed portion of the destination region. In figure 1, the occluding tubes obscure only the ends of the destination region; therefore, only one unshadowed portion must be considered. An unshadowed portion within a look wedge is always defined by the edges of the look wedge or by lines tangent to occluding tubes from the view point.

To determine which tubes lie inside the look wedge, angles from  $X'$  to the lines from the view point to the two points of tangency must be computed. Figure 2 shows the geometry used to compute the angles  $\theta_{T_1}$  and  $\theta_{T_2}$  to the tangent lines. In the figure,  $M$  represents the distance in the  $x$ -direction from  $V$  to the center  $C$  of the tube,  $N$  represents the distance in the  $y$ -direction, and  $r$  is the radius of the tube. By trigonometric manipulation,

$$\cos \theta_{T_1} = \frac{M\sqrt{M^2 + N^2 - r^2} + rN}{M^2 + N^2}$$

and

$$\cos \theta_{T_2} = \frac{M\sqrt{M^2 + N^2 - r^2} - rN}{M^2 + N^2}$$

These cosines and the corresponding sines are used to compute the two angles. A comparison of the angles defining the look wedge and the angles to the tangent lines of each tube identifies occluding tubes for the look wedge. These angles are then used to define the unshadowed portions of the destination region to which the configuration factors must be computed.

A configuration factor  $C_{V-\overline{P_1P_2}}$  from a view point  $V$  on a source region to an unshadowed region  $\overline{P_1P_2}$  may be computed according to the following formula (ref. 3, p. 141):

$$C_{V-P_1P_2} = \frac{1}{2}(\sin \alpha_1 + \sin \alpha_2)$$

where  $\alpha_1$  and  $\alpha_2$  are angles formed by the normal to the source region at  $V$  and lines connecting  $V$  and the two ends of region  $P_1P_2$ . Angle  $\alpha_1$  is measured clockwise from the normal and  $\alpha_2$  is measured counterclockwise. Figure 3 illustrates the angles necessary for the computation of this configuration factor.

For each view point, configuration factors from the view point to all unshadowed portions of the destination region are summed to obtain the configuration factor  $C_{V-D}$  from the view point to the destination region. The mean of configuration factors from all view points in the source region is the geometric view factor  $F_{S-D}$  from the source region to the destination region; that is,

$$F_{S-D} = \frac{1}{N_{vp}} \sum_{V=1}^{N_{vp}} C_{V-D}$$

where  $N_{vp}$  is the number of view points in the source region. A geometric view factor is computed in a similar manner for every source and destination region within the enclosure. The energy conservation principle dictates that

$$\sum_{D=1}^{N_{reg}} F_{S-D} + F_{S-T} = 1$$

where  $N_{reg}$  is the number of regions defined in the polygonal model. Therefore, the view factor  $F_{S-T}$  from the source region to the collection of occluding tubes may also be calculated.

This analysis may be generalized for nonconvex arrangements of regions. In this case, the possibility of occluding regions as well as occluding tubes must be taken into consideration, but the concept of summation of configuration factors to unshadowed regions remains the same.

## IMPLEMENTATION OF NUMERICAL PROCEDURE

### Computer Program

Program VIEWFAC computes geometric view factors according to the analysis just described. It was written in FORTRAN Extended 4.6 language for a Control Data CYBER computer under network operating system (NOS) 1.2. The program

occupies 22076 octal locations in memory, and additional memory is required for the storage of arrays of problem-related data. The dynamic allocation of blank common allows the user to specify memory requirements as a function of the problem size according to the following formula:

$$\begin{aligned}(\text{Memory required})_8 &= 22076_8 + \left( (\text{No. of regions})^2 \right. \\ &\quad \left. + 5(\text{No. of regions} + \text{No. of tubes}) \right)_8\end{aligned}$$

A simplified flow chart of program VIEWFAC is shown in figure 4. Input data required by the program are (1) the number of regions and tubes in the model, (2) coordinates of the endpoints of each region, (3) the number of subregions into which each region is to be divided, (4) coordinates of each tube center, and (5) the radius of each tube. Details of data input are given in appendix A, and a listing of the program is presented in appendix B. The program prints out the input data, computed geometric view factors, and also an area-weighted geometric view factor (AF), which may be used to check reciprocity within the model.

Many check cases were used to verify the computer program; two of them are shown in figure 5. The reciprocity between regions was demonstrated with the check case shown in figure 5(a) in which there were no occluding tubes present. The check case in figure 5(b) verified the detection of an occluding tube and the subsequent computation of configuration factors to unoccluded subregions. These cases are simple enough to be analyzed with a hand calculator in order to check the values generated by the program.

#### Demonstration Problem

The problem chosen to demonstrate the use of program VIEWFAC is one configuration of a quartz-lamp radiant heater currently in use in thermal structures research at the Langley Research Center. (See fig. 6.) The heater consists of an array of quartz lamps. The arrangement of the lamps - number of lamps, distance between lamps, and number of rows of lamps - may be varied according to the particular application. In the demonstration problem, 41 pairs of lamps were arranged in a single row, and a cross section of half of the symmetric array (41 lamps) was modeled for the analysis.

The area surrounding the array was divided into regions. The purpose of the heater analysis was to determine the heat flux uniformity near the ends of the array; therefore, the area near the end was modeled in more detail. Figure 6(a) shows the region definitions, and figure 6(b) shows the position of the row of lamps between the upper and lower regions. Region 22, located along the line of symmetry, actually represented the half of the heater which was not modeled for analysis. In the demonstration problem, all regions were divided into 10 subregions, except regions 10 and 20 which were divided into 120 subregions because of their longer length. A listing of program input and output for this problem is included in appendix C.



Figure 7 shows the effect of occlusion by the tubes on the geometric view factors from a typical lower region, region 4, to upper regions. The difference in the values with and without occlusion is a measure of the amount of energy intercepted by the tubes between region 4 and the upper regions.

For each region I,

$$(\text{Area}_I)(\text{View Factor}_{I-\text{Lamps}}) = (\text{Area}_{\text{Lamps}})(\text{View Factor}_{\text{Lamps}-I})$$

Therefore, the geometric view factors from each region to the lamps are also an indication of the amount of radiant energy that each region receives from the lamps. A comparison of these values indicated that the amount of radiant energy received from the lamps near the end of the heater was significantly less than that received nearer the center line. These results are shown graphically in figure 8.

#### CONCLUDING REMARKS

A numerical procedure has been developed to determine geometric view factors between connected infinite strips occluded by any number of infinite, arbitrarily located, circular cylinders. A description of the procedure, a listing of the computer program based on this procedure, and a discussion of a demonstration problem are given. Taking into account possible occlusion by the cylinders, the computer program calculates the geometric view factors between the individual strips. The program also calculates the geometric view factors between the individual strips and the collection of occluding cylinders.

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July 19, 1978

## APPENDIX A

### INPUT REQUIRED FOR PROGRAM VIEWFAC

The input data for program VIEWFAC are defined in this appendix. The list-directed read capability of FORTRAN is used for all input; therefore, data values on each card must be separated by commas or blanks and may be positioned anywhere within the 80 columns. Real-type data values must contain a decimal point. A data value must be input for every variable read; a blank card or field does not cause variables to be set to zero.

Input cards are of the following five types and must appear in the order discussed:

The configuration card contains one value (NCONFIG, an integer-type variable) which specifies the number of configurations to be analyzed. For each configuration, a set of the following four types of cards must be input.

The title card contains up to 80 characters describing the configuration to be analyzed. This card may be blank but must be present.

The problem-size card contains two values (NREG and NTUBE, integer-type variables) specifying the number of regions and tubes to be defined in this configuration. If no tubes are present in the configuration, a zero may be input for NTUBE.

A region-definition card must be input for each region defined in the configuration. Each card contains five values:

- (1) The x-coordinate of the first endpoint of the region (REGX1, a real-type variable).
- (2) The y-coordinate of the first endpoint of the region (REGY1, a real-type variable).
- (3) The x-coordinate of the second endpoint of the region (REGX2, a real-type variable).
- (4) The y-coordinate of the second endpoint of the region (REGY2, a real-type variable).
- (5) The number of subregions into which the region is to be divided (IDELREG, an integer-type variable). A view point is automatically located at the midpoint of each subregion during the computation of the configuration factor for the region.

Either end of the region may be designated the first end. The x- and y-coordinates of the endpoints are relative to a global origin defined by the user for the entire configuration.

## APPENDIX A

A tube-definition card must be input for each tube defined in the configuration. Each card contains three values:

- (1) The x-coordinate of the center of the tube (TUBX, a real-type variable).
- (2) The y-coordinate of the center of the tube (TUBY, a real-type variable).
- (3) The radius of the tube (TUBRAD, a real-type variable).

The x- and y-coordinates at the center of the tube are also relative to the global origin defined by the user. If NTUBE is input as zero on the problem-size card, no tube-definition cards should be input.

A listing of input for a demonstration problem is contained in appendix C.

APPENDIX B

LISTING OF PROGRAM VIEWFAC

```

PROGRAM VIEWFAC(INPUT,OUTPUT)
C
C THIS PROGRAM CALCULATES VIEW FACTORS FROM ONE REGION
C TO ANOTHER WHEN THE SECOND SURFACE MAY BE OCCLUDED
C BY ONE OR MORE ROUND OBJECTS
C
COMMON /CON/ PI
COMMON /POINTER/ KREGX1,KREGY1,KREGX2,KREGY2,KDELREG,KTUBX,KTUBY,
. KTUBRAD,KTUBIN,KVFRE
COMMON /LIMITS/ NCONFIG,NREG,NTUBE,TITLE(8)
COMMON ICORE(1)
DIMENSION CORE(1)
EQUIVALENCE (CORE,ICORE)
C
C CALCULATE CONSTANTS
PI=ACOS(-1.)
C
C CONFIGURATION CASE LOOP
READ *,NCONFIG
DO 100 I=1,NCONFIG
CALL PROBSIZ
CALL INPUT (CORE(KREGX1),CORE(KREGY1),CORE(KREGX2),CORE(KREGY2),
. ICORE(KDELREG),CORE(KTUBX),CORE(KTUBY),CORE(KTUBRAD))
CALL FACTOR (CORE(KREGX1),CORE(KREGY1),CORE(KREGX2),CORE(KREGY2),
. ICORE(KDELREG),CORE(KTUBX),CORE(KTUBY),CORE(KTUBRAD),
. CORE(KTUBIN),CORE(KVFRE),NREG,NTUBE)
CALL PRINT (CORE(KVFRE),NREG,CORE(KREGX1),CORE(KREGY1),
. CORE(KREGX2),CORE(KREGY2))
100 CONTINUE
C
STOP
END

```

APPENDIX B

SUBROUTINE FACTOR (REGX1,REGY1,REGX2,REGY2,IDELREG,TUBX,TUBY,  
 . TUBRAD,TUBIN,VFRE,NREG,NTUBE)

```

C
C THIS SUBROUTINE CALCULATES VIEW FACTORS FROM EACH REGION TO
C ALL OTHER REGIONS
C
  DIMENSION VFRE(NREG,1)
  DIMENSION REGX1(1),REGX2(1),REGY1(1),REGY2(1),TUBX(1),TUBY(1)
  DIMENSION IDELREG(1)
  DIMENSION TUBRAD(1)
  DIMENSION TUBIN(3,1)
C
C LOOP ON SOURCE REGION
  DO 300 ISREG=1,NREG
    NVP=IDELREG(ISREG)
C
C LOOP ON DESTINATION REGION
  DO 200 IDREG=1,NREG
C
C DO NOT COMPUTE VF FROM ELEMENT TO ITSELF
    VFRE(ISREG,IDREG)=0.
    IF (IDREG.EQ.ISREG) GOTO 200
    VFVPSUM=0.
C
C LOOP ON VIEW POINT
  DO 100 IVP=1,NVP
C
C FIND COORDINATES OF CURRENT VIEW POINT IN SOURCE REGION
C AND ANGLE TO NORMAL OF SOURCE REGION
    CALL VPINFO (REGX1(ISREG),REGY1(ISREG),REGX2(ISREG),REGY2(ISREG),
    . NVP,IVP,XP,YP,SNORM)
C
C FIND ANGLES FROM VIEW POINT TO ENDS OF DESTINATION REGION
    CALL LOOKWDG (XP,YP,REGX1(IDREG),REGY1(IDREG),REGX2(IDREG),
    . REGY2(IDREG),ANG1,ANG2)
C
C CHECK IF VIEW POINT AND DESTINATION REGION ARE COLINEAR
    IF (ANG2-ANG1.LE.1.E-10) GOTO 200
C
C IDENTIFY TUBES IN LOOK WEDGE, COMPUTE ANGLES TO THEM, AND ORDER THEM
    CALL TUBID (XP,YP,ANG1,ANG2,TUBX,TUBY,TUBRAD,TUBIN,NTUBIN)
C
C TEST FOR TOTAL OCCLUSION FROM THIS VIEW POINT
    IF (NTUBIN.LE.NTUBE) GOTO 50
    VFVPVAL=0.
    GOTO 60
C
C COMPUTE VIEW FACTOR CONTRIBUTION FROM CURRENT VIEW POINT
  50 CALL VFVP (TUBIN,VFVPVAL,NTUBIN,ANG1,ANG2,SNORM)
  60 VFVPSUM=VFVPSUM+VFVPVAL
  100 CONTINUE
    VFRE(ISREG,IDREG)=VFVPSUM/FLOAT(NVP)
  200 CONTINUE
  300 CONTINUE
C
  RETURN
  END

```

APPENDIX B

```

SUBROUTINE INPUT (REGX1,REGY1,REGX2,REGY2,IDELREG,TUBX,TUBY,
. TUBRAD)
C
C THIS SUBROUTINE DEFINES AND PRINTS CONFIGURATIONS OF
C REGIONS AND TUBES
C
COMMON /LIMITS/ NCONFIG,NREG,NTUBE,TITLE(8)
DIMENSION REGX1(1),REGX2(1),REGY1(1),REGY2(1),TUBX(1),TUBY(1)
DIMENSION IDELREG(1)
DIMENSION TUBRAD(1)
C
C REGION DEFINITION
DO 10 I=1,NREG
READ *, REGX1(I),REGY1(I),REGX2(I),REGY2(I),IDELREG(I)
10 CONTINUE
C
C TUBE DEFINITION
IF (NTUBE.EQ.0) GOTO 25
DO 20 I=1,NTUBE
READ *, TUBX(I),TUBY(I),TUBRAD(I)
20 CONTINUE
C
C PRINT
25 PRINT 1000
1000 FORMAT (1X,27HCONFIGURATION DEFINITION: ,
. //28X,4HEND1,36X,4HEND2,19X,10HNO. REGION /
. 2X,8HREG. NO.,7X,8HX-COORD.,12X,8HY-COORD.,
. 12X,8HX-COORD., 12X,8HY-COORD.,
. 6X,10HINCREMENTS /)
DO 30 I=1,NREG
PRINT 1001,I,REGX1(I),REGY1(I),REGX2(I),REGY2(I),IDELREG(I)
1001 FORMAT (3X,I5,5X,F15.5,5X,F15.5,5X,F15.5,5X,F15.5,5X,I5)
30 CONTINUE
IF (NTUBE.EQ.0) GOTO 50
PRINT 1002
1002 FORMAT (/28X, 6HCENTER /2X, 8HTUBE NO.,7X,8HX-COORD.,12X,
. 8HY-COORD.,13X,6HRADIUS/)
DO 40 I=1,NTUBE
PRINT 1003,I,TUBX(I),TUBY(I),TUBRAD(I)
1003 FORMAT (3X,I5,5X,F15.5,5X,F15.5,5X,F15.5)
40 CONTINUE
C
50 RETURN
END

```

APPENDIX B

SUBROUTINE LOCATE (XP,YP,TX,TY,TRAD,ANGT1,ANGT2)

```

C
C THIS SUBROUTINE COMPUTES THE ANGLES FROM THE CURRENT VIEW POINT TO
C THE CURRENT TUBE RADIUS
C
COMMON /CON/ PI
C
C COMPUTE COSINES
DISTX=TX-XP
DISTY=TY-YP
DISTX2=DISTX*DISTX
DISTY2=DISTY*DISTY
TRAD2=TRAD*TRAD
RAD=SQRT(DISTX2+DISTY2-TRAD2)
C TEST FOR TUBE TOUCHING VIEW POINT
IF (RAD.LT.(1.E-10)) GOTO 10
TERM1=(DISTX*RAD)/(DISTX2+DISTY2)
TERM2=(TRAD*DISTY)/(DISTX2+DISTY2)
COST1=TERM1+TERM2
COST2=TERM1-TERM2
SINT1=(DISTY-TRAD*COST1)/RAD
SINT2=(DISTY+TRAD*COST2)/RAD
C
C COMPUTE ANGLES
ANGT1=ACOS(COST1)
ANGT2=ACOS(COST2)
IF (SINT1.LT.0.) ANGT1=PI+PI-ANGT1
IF (SINT2.LT.0.) ANGT2=PI+PI-ANGT2
GOTO 20
C
C IF TUBE IS TOUCHING VIEW POINT, SET BOTH ANGLES=0.
10 ANGT1=0.
ANGT2=0.
GOTO 30
C
C ORDER ANGLES
20 IF (ANGT1.LT.ANGT2) RETURN
DUM=ANGT1
ANGT1=ANGT2
ANGT2=DUM
C
C CHECK FOR ANGLE ASTRIDE X AXIS
IF ((ANGT2-ANGT1).LT.PI) GOTO 30
DUM=ANGT2
ANGT2=PI+PI+ANGT1
ANGT1=DUM
C
30 RETURN
END

```

APPENDIX B

```

SUBROUTINE LOOKWDG(XP,YP,X1,Y1,X2,Y2,ANG1,ANG2)
C
C THIS SUBROUTINE CALCULATES THE ANGLES FORMING THE
C LOOK WEDGE FROM THE CURRENT VIEW POINT TO THE DESTINATION ELEMENT
C
COMMON /CON/ PI
C
C ANGLE TO FIRST EDGE
DELX=X1-XP
DELY=Y1-YP
DENOM=SQRT(DELX*DELX+DELY*DELY)
COS1=DELX/DENOM
SIN1=DELY/DENOM
ANG1=ACOS(COS1)
IF (SIN1.LT.0.) ANG1=PI+PI-ANG1
C
C ANGLE TO SECOND EDGE
DELX=X2-XP
DELY=Y2-YP
DENOM=SQRT(DELX*DELX+DELY*DELY)
COS2=DELX/DENOM
SIN2=DELY/DENOM
ANG2=ACOS(COS2)
IF (SIN2.LT.0.) ANG2=PI+PI-ANG2
C
C ORDER ANGLES
IF (ANG1.LT.ANG2) GOTO 10
DUM=ANG1
ANG1=ANG2
ANG2=DUM
C
C CHECK FOR ANGLE ASTRIDE X AXIS
10 IF ((ANG2-ANG1).LT.PI) RETURN
DUM=ANG2
ANG2=PI+PI+ANG1
ANG1=DUM
C
RETURN
END

```



APPENDIX B

SUBROUTINE PRINT (VFRE,NREG,REGX1,REGY1,REGX2,REGY2)

```

C
C THIS SUBROUTINE PRINTS VIEW FACTORS FROM EACH REGION TO ALL OF THE
C OTHERS, AND TO THE TUBES
C
  DIMENSION REGX1(1),REGX2(1),REGY1(1),REGY2(1)
  DIMENSION VFRE(NREG,1)
C
  PRINT 1000
1000 FORMAT (1H1)
  DO 200 ISREG=1,NREG
  PRINT 1001,ISREG
1001 FORMAT (/1X,25HVIEW FACTORS FROM REGION ,I3)
  SAREA=SQRT(((REGX1(ISREG)-REGX2(ISREG))**2)+((REGY1(ISREG)-
  . REGY2(ISREG))**2))
  SUM=0.
  DO 100 IDREG=1,NREG
  AF=SAREA*VFRE(ISREG, IDREG)
  PRINT 1002, IDREG, VFRE(ISREG, IDREG), AF
1002 FORMAT (5X,10HTO REGION ,I3,2H= ,F8.5,6H, AF= ,F15.5)
  SUM=SUM+VFRE(ISREG, IDREG)
  100 CONTINUE
  AFS=SAREA*SUM
  VFTUB=1.-SUM
  AFT=VFTUB*SAREA
  PRINT 1003, SUM, AFS, VFTUB, AFT
1003 FORMAT (5X,18HTO ALL ELEMENTS = ,F9.5,6H AF= ,F15.5/
  . 5X,11HTO TUBES = ,F8.5,7H, AF= ,F15.5)
  200 CONTINUE
C
  RETURN
  END

```

APPENDIX B

SUBROUTINE PROBSIZ

```

C
C THIS SUBROUTINE DEFINES THE SIZE OF THE PROBLEM
C AND FIXES POINTERS TO BEGINNING LOCATIONS OF THE
C ARRAYS NEEDED FOR COMPUTATIONS
C
COMMON /POINTER/ KREGX1,KREGY1,KREGX2,KREGY2,KDELREG,KTUBX,KTUBY,
. KTUBRAD,KTUBIN,KVFRE
COMMON /LIMITS/ NCONFIG,NREG,NTUBE,TITLE(8)
C
C CASE TITLE
READ 1000, TITLE
1000 FORMAT (8A10)
PRINT 1001, (TITLE(I),I=1,8)
1001 FORMAT (1H1,7HCASE: ,8A10/1X,5H-----,/)
C
C LIMITS
READ *,NREG,NTUBE
PRINT 1002,NREG,NTUBE
1002 FORMAT (1X,16HNO. OF REGIONS= ,I5,/1X,14HNO. OF TUBES= ,I5//)
C
C ARRAY POINTERS FOR DYNAMIC CORE ALLOCATION
KREGX1=1
KREGY1=KREGX1+NREG
KREGX2=KREGY1+NREG
KREGY2=KREGX2+NREG
KDELREG=KREGY2+NREG
KTUBX=KDELREG +NREG
KTUBY=KTUBX+NTUBE
KTUBRAD=KTUBY+NTUBE
KTUBIN=KTUBRAD+NTUBE
KVFRE=KTUBIN+(NTUBE*3)
C
RETURN
END

```

APPENDIX B

```

SUBROUTINE RSORT (NROW,NCOL,ISC,B)
C
C THIS SUBROUTINE PERFORMS A KEY BUBBLE SORT,
C ORDERING THE COLUMNS IN INCREASING ORDER
C ACCORDING TO THE VALUES IN A KEY ROW
C
    DIMENSION B(NROW,NCOL)
C
C TEST FOR TRIVIAL CASE OF ONE COLUMN
    IF (NCOL.EQ.1) RETURN
C
C SORT
    NSRT=NCOL-1
    DO 100 I=1,NSRT
    IEND=NCOL+1-I
    DO 50 J=2,IEND
    ITEST=J-1
    IF (B(ISC,J).GE.B(ISC,ITEST)) GOTO 50
    DO 20 K=1,NROW
    SAVE=B(K,J)
    B(K,J)=B(K,ITEST)
    B(K,ITEST)=SAVE
    20 CONTINUE
    50 CONTINUE
    100 CONTINUE
C
    RETURN
    END

SUBROUTINE SUMMER (VFVPVAL,ANG1,ANG2,SNORM)
C
C THIS SUBROUTINE SUMS SINES OF ANGLES FORMED BY THE
C NORMAL TO THE SOURCE REGION AND THE EDGES OF THE
C DESTINATION REGION
C
    COMMON /CON/ PI
C
    IF ((ANG1.LE.SNORM).AND.(ANG2.GE.SNORM)) GOTO 10
C
C NORMAL LIES OUTSIDE TWO ANGLES
    PHI1=ABS(ANG1-SNORM)
    PHI2=2.*PI-ABS(ANG2-SNORM)
    GOTO 20
C
C NORMAL LIES BETWEEN TWO ANGLES
    10 PHI1=ABS(ANG1-SNORM)
    PHI2=ABS(ANG2-SNORM)
C
    20 SINTERM=SIN(PHI1)+SIN(PHI2)
    VFVPVAL=VFVPVAL+.5*ABS(SINTERM)
C
    RETURN
    END

```

APPENDIX B

```

SUBROUTINE TUBID (XP,YP,ANG1,ANG2,TUBX,TUBY,TUBRAD,TUBIN,NTUBIN)
C
C THIS SUBROUTINE IDENTIFIES TUBES IN THE CURRENT LOOK WEDGE AND SORTS
C THEM ACCORDING TO THEIR POSITION IN THE WEDGE
C
COMMON /LIMITS/ NCONFIG,NREG,NTUBE,TITLE(8)
COMMON /CON/ PI
DIMENSION TUBIN(3,1)
DIMENSION TUBRAD(1)
DIMENSION TUBX(1),TUBY(1)
C
C IDENTIFY TUBES IN THE LOOK WEDGE
NTUBIN=0
IF (NTUBE.EQ.0) GOTO 20
DO 10 ITUBE=1,NTUBE
CALL LOCATE (XP,YP,TUBX(ITUBE),TUBY(ITUBE),TUBRAD(ITUBE),ANGT1,
. ANGT2)
C
C TEST FOR TOTAL OCCLUSION
IF ((ANGT1.EQ.ANGT2).AND.(ANGT1.EQ.0.)) GOTO 15
C
C ADJUST FOR ONE OR MORE ANGLES ASTRIDE X AXIS
IF ((ANG2.GE.(PI+PI)).AND.(ANGT1.LT.(ANG2-(PI+PI))))GOTO 2
IF ((ANG2.LT.(PI+PI)).AND.(ANGT2.GT.(PI+PI))) GOTO 3
GOTO 5
C
C LOOK WEDGE ASTRIDE X AXIS, TUBE IS IN WEDGE BUT NOT ASTRIDE
2 ANGT1=PI+PI+ANGT1
ANGT2=PI+PI+ANGT2
GOTO 5
C
C TUBE ASTRIDE X AXIS, LOOK WEDGE NOT ASTRIDE
3 ANGT1=0.
ANGT2=ANGT2-(PI+PI)
C
C COMPARE ANGLES AND LOAD TABLE OF OCCLUDING TUBES
5 IF (ANGT1.GT.ANG2) GOTO 10
IF (ANGT2.LT.ANG1) GOTO 10
NTUBIN=NTUBIN+1
TUBIN(1,NTUBIN)=ITUBE
TUBIN(2,NTUBIN)=ANGT1
TUBIN(3,NTUBIN)=ANGT2
10 CONTINUE
C
C SORT TABLE OF TUBES AND ANGLES
IF (NTUBIN.LE.1) GOTO 20
CALL RSORT (3,NTUBIN,2,TUBIN)
GOTO 20
C
C TOTAL OCCLUSION DUE TO TUBE TOUCHING VIEW POINT.
C SET NTUBIN.LT.NTUBE TO FLAG THIS.
15 NTUBIN=NTUBE+1
C
20 RETURN
END

```

## APPENDIX B

```

SUBROUTINE VFVP (TUBIN,VFVPVAL,NTUBIN,ANG1,ANG2,SNORM)
C
C THIS SUBROUTINE COMPUTES THE CONTRIBUTION OF THE CURRENT VIEW POINT
C TO THE VIEW FACTOR FROM THE CURRENT SOURCE REGION TO THE CURRENT
C DESTINATION REGION
C
C     DIMENSION TUBIN(3,1)
C
C     INITIALIZE SUM
C     VFVPVAL=0.
C
C EXAMINE EACH TUBE IN LOOK WEDGE
C     IF (NTUBIN.NE.0) GOTO 10
C     CALL SUMMER (VFVPVAL,ANG1,ANG2,SNORM)
C     GOTO 200
10 DO 100 IT=1,NTUBIN
C     ANGT1=TUBIN(2,IT)
C     ANGT2=TUBIN(3,IT)
C     IF ((ANGT1.LE.ANG1).AND.(ANGT2.LE.ANG1)) GOTO 100
C     IF ((ANGT1.LE.ANG1).AND.(ANGT2.GE.ANG2)) GOTO 200
C     IF ((ANGT1.GT.ANG1).AND.(ANGT2.LT.ANG2)) GOTO 50
C     IF ((ANGT1.LE.ANG1).AND.(ANGT2.LT.ANG2)) GOTO 60
C     IF ((ANGT1.GT.ANG1).AND.(ANGT2.GE.ANG2)) GOTO 70
C
C TUBE IS TOTALLY WITHIN LOOK WEDGE
C     50 CALL SUMMER (VFVPVAL,ANG1,ANGT1,SNORM)
C     ANGT1=ANGT2
C     GOTO 100
C
C TUBE OCCLUDES FIRST PART OF LOOK WEDGE
C     60 ANGT1=ANGT2
C     GOTO 100
C
C TUBE OCCLUDES LAST PART OF LOOK WEDGE
C     70 CALL SUMMER (VFVPVAL,ANG1,ANGT1,SNORM)
C     GOTO 200
100 CONTINUE
C     ADD IN CONTRIBUTION FROM LAST PART OF LOOK WEDGE
C     CALL SUMMER (VFVPVAL,ANG1,ANG2,SNORM)
C
C     200 RETURN
C     END

```

APPENDIX B

```

SUBROUTINE VPINFO (X1,Y1,X2,Y2,NVP,IVP,XP,YP,SNORM)
C
C THIS SUBROUTINE COMPUTES THE X-Y COORDINATES OF THE CURRENT VIEW POINT
C
COMMON /CON/ PI
C
IF (IVP.NE.1) GOTO 100
C
C COMPUTE ANGLE TO NORMAL OF SOURCE REGION
DELX=X2-X1
DELY=Y2-Y1
IF (DELY.EQ.0.) GOTO 10
TANORM=-DELX/DELY
SNORM=ATAN(TANORM)
IF (SNORM.LE.0.) SNORM=PI+SNORM
GOTO 20
10 SNORM=PI*.5
C
C COMPUTE X-Y INCREMENT FOR NEW VIEW POINT ON FIRST PASS THROUGH
C SUBROUTINE
20 XINC=(X2-X1)/FLOAT(NVP)
YINC=(Y2-Y1)/FLOAT(NVP)
XP=X1+XINC*.5
YP=Y1+YINC*.5
RETURN
C
100 XP=XP+XINC
YP=YP+YINC
C
RETURN
END

```

## APPENDIX C

### DEMONSTRATION PROBLEM

In this appendix, the input required and the printout generated by program VIEWFAC is given for a demonstration problem. The problem is a quartz-lamp radiant heater consisting of an array of 41 pairs of lamps. A two-dimensional model of the heater is shown in figure 6.

A closed area around the lamps was divided into 22 regions. Geometric view factors were computed from each region to each other region, from each region to all other regions, and from each region to the lamps. The view factors were required as input to the MITAS thermal analyzer (ref. 1) used to determine the heat flux near the edges of the heater.

This problem required 23535 octal memory locations and 93.315 seconds of execution time on a Control Data CYBER 173 computer system.

#### Program Input

Configuration card: 1

Title card: QUARTZ LAMP RADIANT HEATER, 2-TUBE CONFIGURATION

Problem-size card: 22 41

Region-definition cards:

0.	0.	.75	0.	10
0.75	0.	1.95	0.	10
1.95	0.	3.15	0.	10
3.15	0.	4.35	0.	10
4.35	0.	5.55	0.	10
5.55	0.	6.75	0.	10
6.75	0.	7.95	0.	10
7.95	0.	9.15	0.	10
9.15	0.	10.35	0.	10
10.35	0.	24.75	0.	120
0.	2.38	.75	2.38	10
0.75	2.38	1.95	2.38	10
1.95	2.38	3.15	2.38	10
3.15	2.38	4.35	2.38	10
4.35	2.38	5.55	2.38	10
5.55	2.38	6.75	2.38	10
6.75	2.38	7.95	2.38	10
7.95	2.38	9.15	2.38	10
9.15	2.38	10.35	2.38	10
10.35	2.38	24.75	2.38	120
0.	0.	0.	2.38	10
24.75	0.	24.75	2.38	10

## APPENDIX C

## Tube-definition cards:

.53700000	1.62700000	.12300000
.96300000	1.62700000	.12300000
1.73700000	1.62700000	.12300000
2.16300000	1.62700000	.12300000
2.93700000	1.62700000	.12300000
3.36300000	1.62700000	.12300000
4.13700000	1.62700000	.12300000
4.56300000	1.62700000	.12300000
5.33700000	1.62700000	.12300000
5.76300000	1.62700000	.12300000
6.53700000	1.62700000	.12300000
6.96300000	1.62700000	.12300000
7.73700000	1.62700000	.12300000
8.16300000	1.62700000	.12300000
8.93700000	1.62700000	.12300000
9.36300000	1.62700000	.12300000
10.13700000	1.62700000	.12300000
10.56300000	1.62700000	.12300000
11.33700000	1.62700000	.12300000
11.76300000	1.62700000	.12300000
12.53700000	1.62700000	.12300000
12.96300000	1.62700000	.12300000
13.73700000	1.62700000	.12300000
14.16300000	1.62700000	.12300000
14.93700000	1.62700000	.12300000
15.36300000	1.62700000	.12300000
16.13700000	1.62700000	.12300000
16.56300000	1.62700000	.12300000
17.33700000	1.62700000	.12300000
17.76300000	1.62700000	.12300000
18.53700000	1.62700000	.12300000
18.96300000	1.62700000	.12300000
19.73700000	1.62700000	.12300000
20.16300000	1.62700000	.12300000
20.93700000	1.62700000	.12300000
21.36300000	1.62700000	.12300000
22.13700000	1.62700000	.12300000
22.56300000	1.62700000	.12300000
23.33700000	1.62700000	.12300000
23.76300000	1.62700000	.12300000
24.53700000	1.62700000	.12300000



APPENDIX C

Program Output

CASE: QUARTZ LAMP RADIANT HEATER, 2-TUBE CONFIGURATION

-----  
 NO. OF REGIONS= 22  
 NO. OF TUBES= 41

CONFIGURATION DEFINITION:

REG. NO.	X-COORD.	END1	Y-COORD.
1	0.00000		0.00000
2	.75000		0.00000
3	1.95000		0.00000
4	3.15000		0.00000
5	4.35000		0.00000
6	5.55000		0.00000
7	6.75000		0.00000
8	7.95000		0.00000
9	9.15000		0.00000
10	10.35000		0.00000
11	0.00000		2.38000
12	.75000		2.38000
13	1.95000		2.38000
14	3.15000		2.38000
15	4.35000		2.38000
16	5.55000		2.38000
17	6.75000		2.38000
18	7.95000		2.38000
19	9.15000		2.38000
20	10.35000		2.38000
21	0.00000		0.00000
22	24.75000		0.00000

APPENDIX C

X-COORD.	END2	Y-COORD.	NO. REGION INCREMENTS
.75000		0.00000	10
1.95000		0.00000	10
3.15000		0.00000	10
4.35000		0.00000	10
5.55000		0.00000	10
6.75000		0.00000	10
7.95000		0.00000	10
9.15000		0.00000	10
10.35000		0.00000	10
24.75000		0.00000	120
.75000		2.38000	10
1.95000		2.38000	10
3.15000		2.38000	10
4.35000		2.38000	10
5.55000		2.38000	10
6.75000		2.38000	10
7.95000		2.38000	10
9.15000		2.38000	10
10.35000		2.38000	10
24.75000		2.38000	120
0.00000		2.38000	10
24.75000		2.38000	10

## APPENDIX C

TUBE NO.	X-COORD.	CENTER	Y-COORD.	RADIUS
1	.53700		1.62700	.12300
2	.96300		1.62700	.12300
3	1.73700		1.62700	.12300
4	2.16300		1.62700	.12300
5	2.93700		1.62700	.12300
6	3.36300		1.62700	.12300
7	4.13700		1.62700	.12300
8	4.56300		1.62700	.12300
9	5.33700		1.62700	.12300
10	5.76300		1.62700	.12300
11	6.53700		1.62700	.12300
12	6.96300		1.62700	.12300
13	7.73700		1.62700	.12300
14	8.16300		1.62700	.12300
15	8.93700		1.62700	.12300
16	9.36300		1.62700	.12300
17	10.13700		1.62700	.12300
18	10.56300		1.62700	.12300
19	11.33700		1.62700	.12300
20	11.76300		1.62700	.12300
21	12.53700		1.62700	.12300
22	12.96300		1.62700	.12300
23	13.73700		1.62700	.12300
24	14.16300		1.62700	.12300
25	14.93700		1.62700	.12300
26	15.36300		1.62700	.12300
27	16.13700		1.62700	.12300
28	16.56300		1.62700	.12300
29	17.33700		1.62700	.12300
30	17.76300		1.62700	.12300
31	18.53700		1.62700	.12300
32	18.96300		1.62700	.12300
33	19.73700		1.62700	.12300
34	20.16300		1.62700	.12300
35	20.93700		1.62700	.12300
36	21.36300		1.62700	.12300
37	22.13700		1.62700	.12300
38	22.56300		1.62700	.12300
39	23.33700		1.62700	.12300
40	23.76300		1.62700	.12300
41	24.53700		1.62700	.12300

APPENDIX C

VIEW FACTORS FROM REGION 1

TO REGION 1=	0.00000,	AF=	0.00000
TO REGION 2=	0.00000,	AF=	0.00000
TO REGION 3=	0.00000,	AF=	0.00000
TO REGION 4=	0.00000,	AF=	0.00000
TO REGION 5=	0.00000,	AF=	0.00000
TO REGION 6=	0.00000,	AF=	0.00000
TO REGION 7=	0.00000,	AF=	0.00000
TO REGION 8=	0.00000,	AF=	0.00000
TO REGION 9=	0.00000,	AF=	0.00000
TO REGION 10=	0.00000,	AF=	0.00000
TO REGION 11=	.09347,	AF=	.07010
TO REGION 12=	.11781,	AF=	.08836
TO REGION 13=	.03160,	AF=	.02370
TO REGION 14=	.02465,	AF=	.01848
TO REGION 15=	.00544,	AF=	.00408
TO REGION 16=	.00004,	AF=	.00003
TO REGION 17=	.00052,	AF=	.00039
TO REGION 18=	0.00000,	AF=	0.00000
TO REGION 19=	0.00000,	AF=	0.00000
TO REGION 20=	0.00000,	AF=	0.00000
TO REGION 21=	.42307,	AF=	.31731
TO REGION 22=	.00097,	AF=	.00072
TO ALL ELEMENTS =	.69756	AF=	.52317
TO TUBES =	.30244,	AF=	.22683

VIEW FACTORS FROM REGION 2

TO REGION 1=	0.00000,	AF=	0.00000
TO REGION 2=	0.00000,	AF=	0.00000
TO REGION 3=	0.00000,	AF=	0.00000
TO REGION 4=	0.00000,	AF=	0.00000
TO REGION 5=	0.00000,	AF=	0.00000
TO REGION 6=	0.00000,	AF=	0.00000
TO REGION 7=	0.00000,	AF=	0.00000
TO REGION 8=	0.00000,	AF=	0.00000
TO REGION 9=	0.00000,	AF=	0.00000
TO REGION 10=	0.00000,	AF=	0.00000
TO REGION 11=	.04681,	AF=	.05617
TO REGION 12=	.15461,	AF=	.18553
TO REGION 13=	.09126,	AF=	.10951
TO REGION 14=	.03202,	AF=	.03842
TO REGION 15=	.01981,	AF=	.02377
TO REGION 16=	.00371,	AF=	.00446
TO REGION 17=	.00050,	AF=	.00060
TO REGION 18=	.00032,	AF=	.00039
TO REGION 19=	0.00000,	AF=	0.00000
TO REGION 20=	0.00000,	AF=	0.00000
TO REGION 21=	.24667,	AF=	.29600
TO REGION 22=	.00105,	AF=	.00126
TO ALL ELEMENTS =	.59676	AF=	.71611
TO TUBES =	.40324,	AF=	.48389

## APPENDIX C

## VIEW FACTORS FROM REGION 3

TO REGION 1=	0.00000,	AF=	0.00000
TO REGION 2=	0.00000,	AF=	0.00000
TO REGION 3=	0.00000,	AF=	0.00000
TO REGION 4=	0.00000,	AF=	0.00000
TO REGION 5=	0.00000,	AF=	0.00000
TO REGION 6=	0.00000,	AF=	0.00000
TO REGION 7=	0.00000,	AF=	0.00000
TO REGION 8=	0.00000,	AF=	0.00000
TO REGION 9=	0.00000,	AF=	0.00000
TO REGION 10=	0.00000,	AF=	0.00000
TO REGION 11=	.02955,	AF=	.03546
TO REGION 12=	.09126,	AF=	.10951
TO REGION 13=	.15461,	AF=	.18553
TO REGION 14=	.09126,	AF=	.10951
TO REGION 15=	.03202,	AF=	.03842
TO REGION 16=	.01981,	AF=	.02377
TO REGION 17=	.00371,	AF=	.00446
TO REGION 18=	.00050,	AF=	.00060
TO REGION 19=	.00032,	AF=	.00039
TO REGION 20=	0.00000,	AF=	0.00000
TO REGION 21=	.10253,	AF=	.12303
TO REGION 22=	.00117,	AF=	.00140
TO ALL ELEMENTS =	.52674	AF=	.63209
TO TUBES =	.47326,	AF=	.56791

## VIEW FACTORS FROM REGION 4

TO REGION 1=	0.00000,	AF=	0.00000
TO REGION 2=	0.00000,	AF=	0.00000
TO REGION 3=	0.00000,	AF=	0.00000
TO REGION 4=	0.00000,	AF=	0.00000
TO REGION 5=	0.00000,	AF=	0.00000
TO REGION 6=	0.00000,	AF=	0.00000
TO REGION 7=	0.00000,	AF=	0.00000
TO REGION 8=	0.00000,	AF=	0.00000
TO REGION 9=	0.00000,	AF=	0.00000
TO REGION 10=	0.00000,	AF=	0.00000
TO REGION 11=	.01852,	AF=	.02222
TO REGION 12=	.03202,	AF=	.03842
TO REGION 13=	.09126,	AF=	.10951
TO REGION 14=	.15461,	AF=	.18553
TO REGION 15=	.09126,	AF=	.10951
TO REGION 16=	.03202,	AF=	.03842
TO REGION 17=	.01981,	AF=	.02377
TO REGION 18=	.00371,	AF=	.00446
TO REGION 19=	.00050,	AF=	.00060
TO REGION 20=	.00032,	AF=	.00039
TO REGION 21=	.04889,	AF=	.05867
TO REGION 22=	.00130,	AF=	.00156
TO ALL ELEMENTS =	.49423	AF=	.59307
TO TUBES =	.50577,	AF=	.60693

## APPENDIX C

## VIEW FACTORS FROM REGION 5

TO REGION 1=	0.00000,	AF=	0.00000
TO REGION 2=	0.00000,	AF=	0.00000
TO REGION 3=	0.00000,	AF=	0.00000
TO REGION 4=	0.00000,	AF=	0.00000
TO REGION 5=	0.00000,	AF=	0.00000
TO REGION 6=	0.00000,	AF=	0.00000
TO REGION 7=	0.00000,	AF=	0.00000
TO REGION 8=	0.00000,	AF=	0.00000
TO REGION 9=	0.00000,	AF=	0.00000
TO REGION 10=	0.00000,	AF=	0.00000
TO REGION 11=	.00043,	AF=	.00052
TO REGION 12=	.01981,	AF=	.02377
TO REGION 13=	.03202,	AF=	.03842
TO REGION 14=	.09126,	AF=	.10951
TO REGION 15=	.15461,	AF=	.18553
TO REGION 16=	.09126,	AF=	.10951
TO REGION 17=	.03202,	AF=	.03842
TO REGION 18=	.01981,	AF=	.02377
TO REGION 19=	.00371,	AF=	.00446
TO REGION 20=	.00083,	AF=	.00099
TO REGION 21=	.03069,	AF=	.03682
TO REGION 22=	.00147,	AF=	.00176
TO ALL ELEMENTS =	.47791	AF=	.57350
TO TUBES =	.52209,	AF=	.62650

## VIEW FACTORS FROM REGION 6

TO REGION 1=	0.00000,	AF=	0.00000
TO REGION 2=	0.00000,	AF=	0.00000
TO REGION 3=	0.00000,	AF=	0.00000
TO REGION 4=	0.00000,	AF=	0.00000
TO REGION 5=	0.00000,	AF=	0.00000
TO REGION 6=	0.00000,	AF=	0.00000
TO REGION 7=	0.00000,	AF=	0.00000
TO REGION 8=	0.00000,	AF=	0.00000
TO REGION 9=	0.00000,	AF=	0.00000
TO REGION 10=	0.00000,	AF=	0.00000
TO REGION 11=	.00050,	AF=	.00060
TO REGION 12=	.00371,	AF=	.00446
TO REGION 13=	.01981,	AF=	.02377
TO REGION 14=	.03202,	AF=	.03842
TO REGION 15=	.09126,	AF=	.10951
TO REGION 16=	.15461,	AF=	.18553
TO REGION 17=	.09126,	AF=	.10951
TO REGION 18=	.03202,	AF=	.03842
TO REGION 19=	.01981,	AF=	.02377
TO REGION 20=	.00454,	AF=	.00545
TO REGION 21=	.01744,	AF=	.02092
TO REGION 22=	.00167,	AF=	.00200
TO ALL ELEMENTS =	.46865	AF=	.56237
TO TUBES =	.53135,	AF=	.63763

APPENDIX C

VIEW FACTORS FROM REGION 7

TO REGION 1=	0.00000,	AF=	0.00000
TO REGION 2=	0.00000,	AF=	0.00000
TO REGION 3=	0.00000,	AF=	0.00000
TO REGION 4=	0.00000,	AF=	0.00000
TO REGION 5=	0.00000,	AF=	0.00000
TO REGION 6=	0.00000,	AF=	0.00000
TO REGION 7=	0.00000,	AF=	0.00000
TO REGION 8=	0.00000,	AF=	0.00000
TO REGION 9=	0.00000,	AF=	0.00000
TO REGION 10=	0.00000,	AF=	0.00000
TO REGION 11=	.00032,	AF=	.00039
TO REGION 12=	.00050,	AF=	.00060
TO REGION 13=	.00371,	AF=	.00446
TO REGION 14=	.01981,	AF=	.02377
TO REGION 15=	.03202,	AF=	.03842
TO REGION 16=	.09126,	AF=	.10951
TO REGION 17=	.15461,	AF=	.18553
TO REGION 18=	.09126,	AF=	.10951
TO REGION 19=	.03202,	AF=	.03842
TO REGION 20=	.02435,	AF=	.02922
TO REGION 21=	.01179,	AF=	.01415
TO REGION 22=	.00190,	AF=	.00229
TO ALL ELEMENTS =	.46356	AF=	.55628
TO TUBES =	.53644,	AF=	.64372

VIEW FACTORS FROM REGION 8

TO REGION 1=	0.00000,	AF=	0.00000
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TO REGION 3=	0.00000,	AF=	0.00000
TO REGION 4=	0.00000,	AF=	0.00000
TO REGION 5=	0.00000,	AF=	0.00000
TO REGION 6=	0.00000,	AF=	0.00000
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TO REGION 8=	0.00000,	AF=	0.00000
TO REGION 9=	0.00000,	AF=	0.00000
TO REGION 10=	0.00000,	AF=	0.00000
TO REGION 11=	0.00000,	AF=	0.00000
TO REGION 12=	.00032,	AF=	.00039
TO REGION 13=	.00050,	AF=	.00060
TO REGION 14=	.00371,	AF=	.00446
TO REGION 15=	.01981,	AF=	.02377
TO REGION 16=	.03202,	AF=	.03842
TO REGION 17=	.09126,	AF=	.10951
TO REGION 18=	.15461,	AF=	.18553
TO REGION 19=	.09126,	AF=	.10951
TO REGION 20=	.05637,	AF=	.06764
TO REGION 21=	.00860,	AF=	.01032
TO REGION 22=	.00220,	AF=	.00264
TO ALL ELEMENTS =	.46067	AF=	.55280
TO TUBES =	.53933,	AF=	.64720

## APPENDIX C

## VIEW FACTORS FROM REGION 9

TO REGION 1=	0.00000,	AF=	0.00000
TO REGION 2=	0.00000,	AF=	0.00000
TO REGION 3=	0.00000,	AF=	0.00000
TO REGION 4=	0.00000,	AF=	0.00000
TO REGION 5=	0.00000,	AF=	0.00000
TO REGION 6=	0.00000,	AF=	0.00000
TO REGION 7=	0.00000,	AF=	0.00000
TO REGION 8=	0.00000,	AF=	0.00000
TO REGION 9=	0.00000,	AF=	0.00000
TO REGION 10=	0.00000,	AF=	0.00000
TO REGION 11=	0.00000,	AF=	0.00000
TO REGION 12=	0.00000,	AF=	0.00000
TO REGION 13=	.00032,	AF=	.00039
TO REGION 14=	.00050,	AF=	.00060
TO REGION 15=	.00371,	AF=	.00446
TO REGION 16=	.01981,	AF=	.02377
TO REGION 17=	.03202,	AF=	.03842
TO REGION 18=	.09126,	AF=	.10951
TO REGION 19=	.15461,	AF=	.18553
TO REGION 20=	.14763,	AF=	.17716
TO REGION 21=	.00654,	AF=	.00785
TO REGION 22=	.00257,	AF=	.00308
TO ALL ELEMENTS =	.45898	AF=	.55078
TO TUBES =	.54102,	AF=	.64922

## VIEW FACTORS FROM REGION 10

TO REGION 1=	0.00000,	AF=	0.00000
TO REGION 2=	0.00000,	AF=	0.00000
TO REGION 3=	0.00000,	AF=	0.00000
TO REGION 4=	0.00000,	AF=	0.00000
TO REGION 5=	0.00000,	AF=	0.00000
TO REGION 6=	0.00000,	AF=	0.00000
TO REGION 7=	0.00000,	AF=	0.00000
TO REGION 8=	0.00000,	AF=	0.00000
TO REGION 9=	0.00000,	AF=	0.00000
TO REGION 10=	0.00000,	AF=	0.00000
TO REGION 11=	0.00000,	AF=	0.00000
TO REGION 12=	0.00000,	AF=	0.00000
TO REGION 13=	0.00000,	AF=	0.00000
TO REGION 14=	.00003,	AF=	.00039
TO REGION 15=	.00007,	AF=	.00099
TO REGION 16=	.00038,	AF=	.00545
TO REGION 17=	.00203,	AF=	.02922
TO REGION 18=	.00470,	AF=	.06764
TO REGION 19=	.01230,	AF=	.17716
TO REGION 20=	.41086,	AF=	5.91638
TO REGION 21=	.00236,	AF=	.03393
TO REGION 22=	.05842,	AF=	.84124
TO ALL ELEMENTS =	.49114	AF=	7.07239
TO TUBES =	.50886,	AF=	7.32761



APPENDIX C

VIEW FACTORS FROM REGION 11

TO REGION 1=	.09364,	AF=	.07023
TO REGION 2=	.07427,	AF=	.05570
TO REGION 3=	.04768,	AF=	.03576
TO REGION 4=	.02965,	AF=	.02224
TO REGION 5=	.00071,	AF=	.00054
TO REGION 6=	.00080,	AF=	.00060
TO REGION 7=	.00053,	AF=	.00039
TO REGION 8=	0.00000,	AF=	0.00000
TO REGION 9=	0.00000,	AF=	0.00000
TO REGION 10=	0.00000,	AF=	0.00000
TO REGION 11=	0.00000,	AF=	0.00000
TO REGION 12=	0.00000,	AF=	0.00000
TO REGION 13=	0.00000,	AF=	0.00000
TO REGION 14=	0.00000,	AF=	0.00000
TO REGION 15=	0.00000,	AF=	0.00000
TO REGION 16=	0.00000,	AF=	0.00000
TO REGION 17=	0.00000,	AF=	0.00000
TO REGION 18=	0.00000,	AF=	0.00000
TO REGION 19=	0.00000,	AF=	0.00000
TO REGION 20=	0.00000,	AF=	0.00000
TO REGION 21=	.41685,	AF=	.31264
TO REGION 22=	.00017,	AF=	.00013
TO ALL ELEMENTS =	.66430	AF=	.49822
TO TUBES =	.33570,	AF=	.25178

VIEW FACTORS FROM REGION 12

TO REGION 1=	.07378,	AF=	.08853
TO REGION 2=	.15467,	AF=	.18561
TO REGION 3=	.09109,	AF=	.10931
TO REGION 4=	.03210,	AF=	.03852
TO REGION 5=	.01987,	AF=	.02385
TO REGION 6=	.00372,	AF=	.00446
TO REGION 7=	.00051,	AF=	.00061
TO REGION 8=	.00032,	AF=	.00038
TO REGION 9=	0.00000,	AF=	0.00000
TO REGION 10=	0.00000,	AF=	0.00000
TO REGION 11=	0.00000,	AF=	0.00000
TO REGION 12=	0.00000,	AF=	0.00000
TO REGION 13=	0.00000,	AF=	0.00000
TO REGION 14=	0.00000,	AF=	0.00000
TO REGION 15=	0.00000,	AF=	0.00000
TO REGION 16=	0.00000,	AF=	0.00000
TO REGION 17=	0.00000,	AF=	0.00000
TO REGION 18=	0.00000,	AF=	0.00000
TO REGION 19=	0.00000,	AF=	0.00000
TO REGION 20=	0.00000,	AF=	0.00000
TO REGION 21=	.14403,	AF=	.17284
TO REGION 22=	.00018,	AF=	.00022
TO ALL ELEMENTS =	.52028	AF=	.62433
TO TUBES =	.47972,	AF=	.57567

## APPENDIX C

## VIEW FACTORS FROM REGION 13

TO REGION 1=	.01989,	AF=	.02387
TO REGION 2=	.09109,	AF=	.10931
TO REGION 3=	.15467,	AF=	.18561
TO REGION 4=	.09109,	AF=	.10931
TO REGION 5=	.03210,	AF=	.03852
TO REGION 6=	.01987,	AF=	.02385
TO REGION 7=	.00372,	AF=	.00446
TO REGION 8=	.00051,	AF=	.00061
TO REGION 9=	.00032,	AF=	.00038
TO REGION 10=	0.00000,	AF=	0.00000
TO REGION 11=	0.00000,	AF=	0.00000
TO REGION 12=	0.00000,	AF=	0.00000
TO REGION 13=	0.00000,	AF=	0.00000
TO REGION 14=	0.00000,	AF=	0.00000
TO REGION 15=	0.00000,	AF=	0.00000
TO REGION 16=	0.00000,	AF=	0.00000
TO REGION 17=	0.00000,	AF=	0.00000
TO REGION 18=	0.00000,	AF=	0.00000
TO REGION 19=	0.00000,	AF=	0.00000
TO REGION 20=	0.00000,	AF=	0.00000
TO REGION 21=	.05995,	AF=	.07194
TO REGION 22=	.00021,	AF=	.00025
TO ALL ELEMENTS =	.47343	AF=	.56811
TO TUBES =	.52657,	AF=	.63189

## VIEW FACTORS FROM REGION 14

TO REGION 1=	.01543,	AF=	.01851
TO REGION 2=	.03210,	AF=	.03852
TO REGION 3=	.09109,	AF=	.10931
TO REGION 4=	.15467,	AF=	.18561
TO REGION 5=	.09109,	AF=	.10931
TO REGION 6=	.03210,	AF=	.03852
TO REGION 7=	.01987,	AF=	.02385
TO REGION 8=	.00372,	AF=	.00446
TO REGION 9=	.00051,	AF=	.00061
TO REGION 10=	.00032,	AF=	.00038
TO REGION 11=	0.00000,	AF=	0.00000
TO REGION 12=	0.00000,	AF=	0.00000
TO REGION 13=	0.00000,	AF=	0.00000
TO REGION 14=	0.00000,	AF=	0.00000
TO REGION 15=	0.00000,	AF=	0.00000
TO REGION 16=	0.00000,	AF=	0.00000
TO REGION 17=	0.00000,	AF=	0.00000
TO REGION 18=	0.00000,	AF=	0.00000
TO REGION 19=	0.00000,	AF=	0.00000
TO REGION 20=	0.00000,	AF=	0.00000
TO REGION 21=	.01857,	AF=	.02228
TO REGION 22=	.00023,	AF=	.00028
TO ALL ELEMENTS =	.45970	AF=	.55164
TO TUBES =	.54030,	AF=	.64836

APPENDIX C

VIEW FACTORS FROM REGION 15

TO REGION 1=	.00342,	AF=	.00411
TO REGION 2=	.01987,	AF=	.02385
TO REGION 3=	.03210,	AF=	.03852
TO REGION 4=	.09109,	AF=	.10931
TO REGION 5=	.15467,	AF=	.18561
TO REGION 6=	.09109,	AF=	.10931
TO REGION 7=	.03210,	AF=	.03852
TO REGION 8=	.01987,	AF=	.02385
TO REGION 9=	.00372,	AF=	.00446
TO REGION 10=	.00082,	AF=	.00099
TO REGION 11=	0.00000,	AF=	0.00000
TO REGION 12=	0.00000,	AF=	0.00000
TO REGION 13=	0.00000,	AF=	0.00000
TO REGION 14=	0.00000,	AF=	0.00000
TO REGION 15=	0.00000,	AF=	0.00000
TO REGION 16=	0.00000,	AF=	0.00000
TO REGION 17=	0.00000,	AF=	0.00000
TO REGION 18=	0.00000,	AF=	0.00000
TO REGION 19=	0.00000,	AF=	0.00000
TO REGION 20=	0.00000,	AF=	0.00000
TO REGION 21=	.00621,	AF=	.00745
TO REGION 22=	.00026,	AF=	.00031
TO ALL ELEMENTS =	.45524	AF=	.54628
TO TUBES =	.54476,	AF=	.65372

VIEW FACTORS FROM REGION 16

TO REGION 1=	0.00000,	AF=	0.00000
TO REGION 2=	.00372,	AF=	.00446
TO REGION 3=	.01987,	AF=	.02385
TO REGION 4=	.03210,	AF=	.03852
TO REGION 5=	.09109,	AF=	.10931
TO REGION 6=	.15467,	AF=	.18561
TO REGION 7=	.09109,	AF=	.10931
TO REGION 8=	.03210,	AF=	.03852
TO REGION 9=	.01987,	AF=	.02385
TO REGION 10=	.00454,	AF=	.00545
TO REGION 11=	0.00000,	AF=	0.00000
TO REGION 12=	0.00000,	AF=	0.00000
TO REGION 13=	0.00000,	AF=	0.00000
TO REGION 14=	0.00000,	AF=	0.00000
TO REGION 15=	0.00000,	AF=	0.00000
TO REGION 16=	0.00000,	AF=	0.00000
TO REGION 17=	0.00000,	AF=	0.00000
TO REGION 18=	0.00000,	AF=	0.00000
TO REGION 19=	0.00000,	AF=	0.00000
TO REGION 20=	0.00000,	AF=	0.00000
TO REGION 21=	.00397,	AF=	.00476
TO REGION 22=	.00029,	AF=	.00035
TO ALL ELEMENTS =	.45333	AF=	.54400
TO TUBES =	.54667,	AF=	.65600

APPENDIX C

VIEW FACTORS FROM REGION 17

TO REGION 1=	.00032,	AF=	.00038
TO REGION 2=	.00051,	AF=	.00061
TO REGION 3=	.00372,	AF=	.00446
TO REGION 4=	.01987,	AF=	.02385
TO REGION 5=	.03210,	AF=	.03852
TO REGION 6=	.09109,	AF=	.10931
TO REGION 7=	.15467,	AF=	.18561
TO REGION 8=	.09109,	AF=	.10931
TO REGION 9=	.03210,	AF=	.03852
TO REGION 10=	.02441,	AF=	.02930
TO REGION 11=	0.00000,	AF=	0.00000
TO REGION 12=	0.00000,	AF=	0.00000
TO REGION 13=	0.00000,	AF=	0.00000
TO REGION 14=	0.00000,	AF=	0.00000
TO REGION 15=	0.00000,	AF=	0.00000
TO REGION 16=	0.00000,	AF=	0.00000
TO REGION 17=	0.00000,	AF=	0.00000
TO REGION 18=	0.00000,	AF=	0.00000
TO REGION 19=	0.00000,	AF=	0.00000
TO REGION 20=	0.00000,	AF=	0.00000
TO REGION 21=	.00214,	AF=	.00256
TO REGION 22=	.00034,	AF=	.00040
TO ALL ELEMENTS =	.45236	AF=	.54283
TO TUBES =	.54764,	AF=	.65717

VIEW FACTORS FROM REGION 18

TO REGION 1=	0.00000,	AF=	0.00000
TO REGION 2=	.00032,	AF=	.00038
TO REGION 3=	.00051,	AF=	.00061
TO REGION 4=	.00372,	AF=	.00446
TO REGION 5=	.01987,	AF=	.02385
TO REGION 6=	.03210,	AF=	.03852
TO REGION 7=	.09109,	AF=	.10931
TO REGION 8=	.15467,	AF=	.18561
TO REGION 9=	.09109,	AF=	.10931
TO REGION 10=	.05651,	AF=	.06782
TO REGION 11=	0.00000,	AF=	0.00000
TO REGION 12=	0.00000,	AF=	0.00000
TO REGION 13=	0.00000,	AF=	0.00000
TO REGION 14=	0.00000,	AF=	0.00000
TO REGION 15=	0.00000,	AF=	0.00000
TO REGION 16=	0.00000,	AF=	0.00000
TO REGION 17=	0.00000,	AF=	0.00000
TO REGION 18=	0.00000,	AF=	0.00000
TO REGION 19=	0.00000,	AF=	0.00000
TO REGION 20=	0.00000,	AF=	0.00000
TO REGION 21=	.00154,	AF=	.00185
TO REGION 22=	.00039,	AF=	.00047
TO ALL ELEMENTS =	.45182	AF=	.54219
TO TUBES =	.54818,	AF=	.65781

APPENDIX C

VIEW FACTORS FROM REGION 19

TO REGION	1=	0.00000,	AF=	0.00000
TO REGION	2=	0.00000,	AF=	0.00000
TO REGION	3=	.00032,	AF=	.00038
TO REGION	4=	.00051,	AF=	.00061
TO REGION	5=	.00372,	AF=	.00446
TO REGION	6=	.01987,	AF=	.02385
TO REGION	7=	.03210,	AF=	.03852
TO REGION	8=	.09109,	AF=	.10931
TO REGION	9=	.15467,	AF=	.18561
TO REGION	10=	.14761,	AF=	.17713
TO REGION	11=	0.00000,	AF=	0.00000
TO REGION	12=	0.00000,	AF=	0.00000
TO REGION	13=	0.00000,	AF=	0.00000
TO REGION	14=	0.00000,	AF=	0.00000
TO REGION	15=	0.00000,	AF=	0.00000
TO REGION	16=	0.00000,	AF=	0.00000
TO REGION	17=	0.00000,	AF=	0.00000
TO REGION	18=	0.00000,	AF=	0.00000
TO REGION	19=	0.00000,	AF=	0.00000
TO REGION	20=	0.00000,	AF=	0.00000
TO REGION	21=	.00117,	AF=	.00140
TO REGION	22=	.00045,	AF=	.00054
TO ALL ELEMENTS	=	.45151	AF=	.54181
TO TUBES	=	.54849,	AF=	.65819

VIEW FACTORS FROM REGION 20

TO REGION	1=	0.00000,	AF=	0.00000
TO REGION	2=	0.00000,	AF=	0.00000
TO REGION	3=	0.00000,	AF=	0.00000
TO REGION	4=	.00003,	AF=	.00038
TO REGION	5=	.00007,	AF=	.00099
TO REGION	6=	.00038,	AF=	.00545
TO REGION	7=	.00203,	AF=	.02930
TO REGION	8=	.00471,	AF=	.06782
TO REGION	9=	.01230,	AF=	.17713
TO REGION	10=	.41085,	AF=	5.91630
TO REGION	11=	0.00000,	AF=	0.00000
TO REGION	12=	0.00000,	AF=	0.00000
TO REGION	13=	0.00000,	AF=	0.00000
TO REGION	14=	0.00000,	AF=	0.00000
TO REGION	15=	0.00000,	AF=	0.00000
TO REGION	16=	0.00000,	AF=	0.00000
TO REGION	17=	0.00000,	AF=	0.00000
TO REGION	18=	0.00000,	AF=	0.00000
TO REGION	19=	0.00000,	AF=	0.00000
TO REGION	20=	0.00000,	AF=	0.00000
TO REGION	21=	.00042,	AF=	.00600
TO REGION	22=	.03793,	AF=	.54620
TO ALL ELEMENTS	=	.46872	AF=	6.74956
TO TUBES	=	.53128,	AF=	7.65044

## APPENDIX C

## VIEW FACTORS FROM REGION 21

TO REGION 1=	.13268,	AF=	.31577
TO REGION 2=	.12517,	AF=	.29789
TO REGION 3=	.05266,	AF=	.12533
TO REGION 4=	.02250,	AF=	.05354
TO REGION 5=	.01599,	AF=	.03807
TO REGION 6=	.00885,	AF=	.02106
TO REGION 7=	.00628,	AF=	.01494
TO REGION 8=	.00468,	AF=	.01113
TO REGION 9=	.00362,	AF=	.00860
TO REGION 10=	.01622,	AF=	.03861
TO REGION 11=	.13071,	AF=	.31108
TO REGION 12=	.07367,	AF=	.17534
TO REGION 13=	.02907,	AF=	.06918
TO REGION 14=	.00929,	AF=	.02210
TO REGION 15=	.00324,	AF=	.00770
TO REGION 16=	.00216,	AF=	.00514
TO REGION 17=	.00119,	AF=	.00283
TO REGION 18=	.00088,	AF=	.00209
TO REGION 19=	.00068,	AF=	.00161
TO REGION 20=	.00300,	AF=	.00715
TO REGION 21=	0.00000,	AF=	0.00000
TO REGION 22=	.02213,	AF=	.05267
TO ALL ELEMENTS =	.66464	AF=	1.58184
TO TUBES =	.33536,	AF=	.79816

## VIEW FACTORS FROM REGION 22

TO REGION 1=	.00027,	AF=	.00064
TO REGION 2=	.00047,	AF=	.00111
TO REGION 3=	.00052,	AF=	.00124
TO REGION 4=	.00058,	AF=	.00138
TO REGION 5=	.00065,	AF=	.00156
TO REGION 6=	.00074,	AF=	.00176
TO REGION 7=	.00065,	AF=	.00201
TO REGION 8=	.00098,	AF=	.00232
TO REGION 9=	.00114,	AF=	.00271
TO REGION 10=	.35596,	AF=	.84718
TO REGION 11=	.00007,	AF=	.00016
TO REGION 12=	.00012,	AF=	.00028
TO REGION 13=	.00013,	AF=	.00031
TO REGION 14=	.00015,	AF=	.00035
TO REGION 15=	.00016,	AF=	.00039
TO REGION 16=	.00019,	AF=	.00044
TO REGION 17=	.00021,	AF=	.00051
TO REGION 18=	.00024,	AF=	.00058
TO REGION 19=	.00029,	AF=	.00068
TO REGION 20=	.23101,	AF=	.54980
TO REGION 21=	.02228,	AF=	.05302
TO REGION 22=	0.00000,	AF=	0.00000
TO ALL ELEMENTS =	.61699	AF=	1.46844
TO TUBES =	.38301,	AF=	.91156

## REFERENCES

1. Martin Interactive Thermal Analyzer System - Version 1.0. User's Manual. MDS-SPLPD-71-FD238 (REV 3), Martin Marietta Corp., Mar. 1972.
2. Touns, K. A.: A General Computer Program for the Determination of Radiant-Interchange Configuration and Form Factors - CONFAC II. SID-65-1043-2, North American Aviat., Inc., Oct. 1965. (Available as NASA CR-65257.)
3. Sparrow, E. M.; and Cess, R. D.: Radiation Heat Transfer. Augmented Ed. Hemisphere Pub. Corp., c.1978.

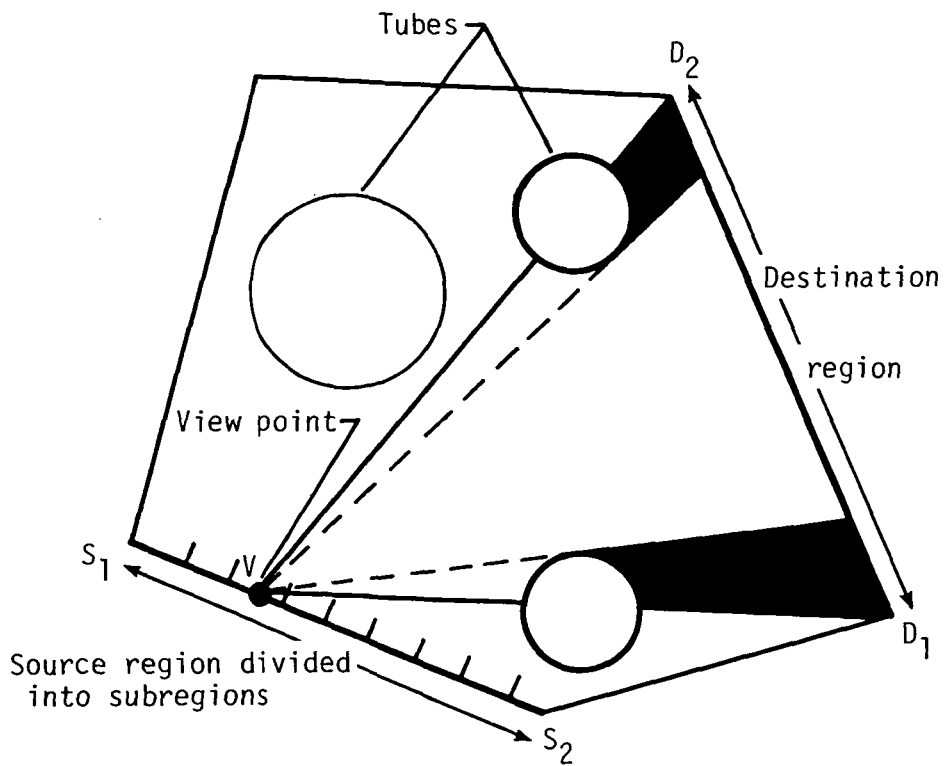


Figure 1.- Typical arrangement of source and destination regions and occluding tubes.



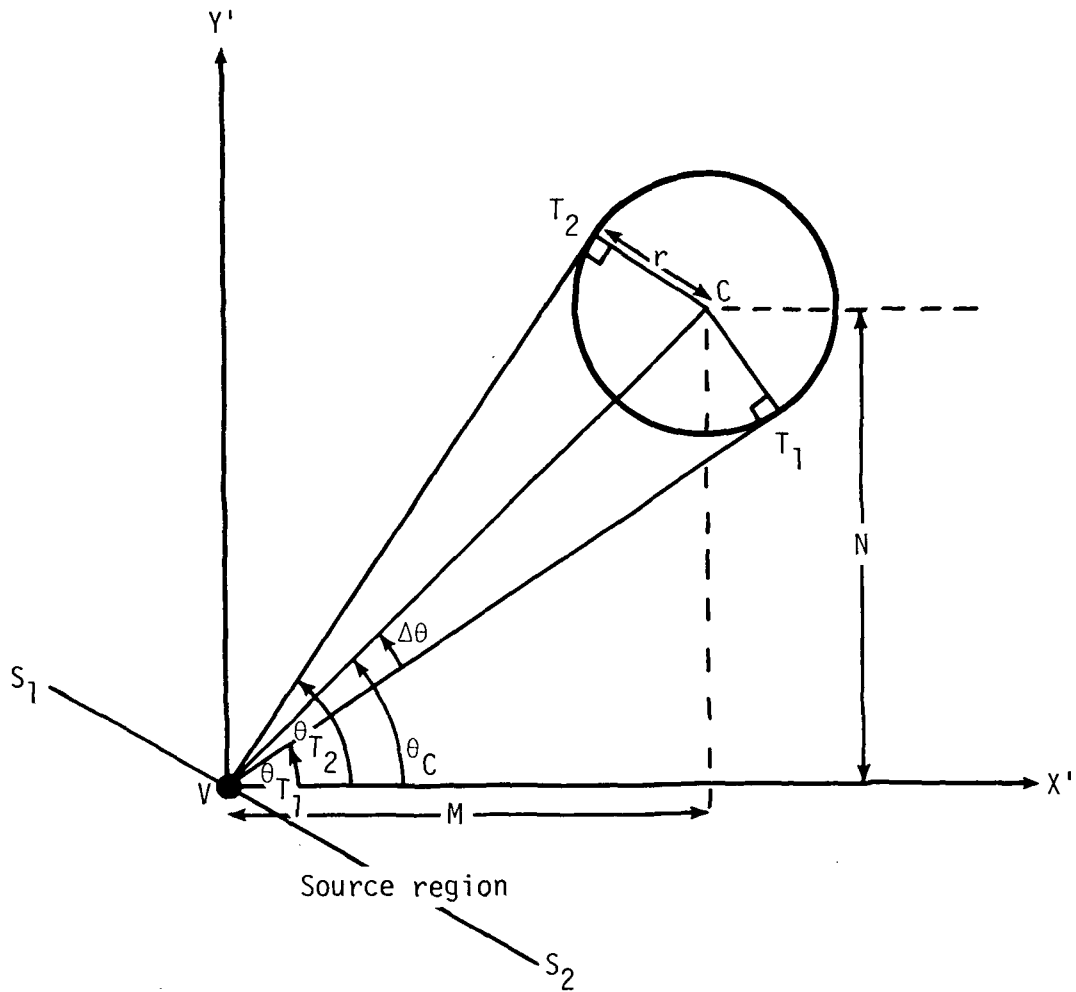


Figure 2.- Geometry used in computation of angles from  $X'$  to lines from view point  $V$  to points of tangency  $T_1$  and  $T_2$  of tube.

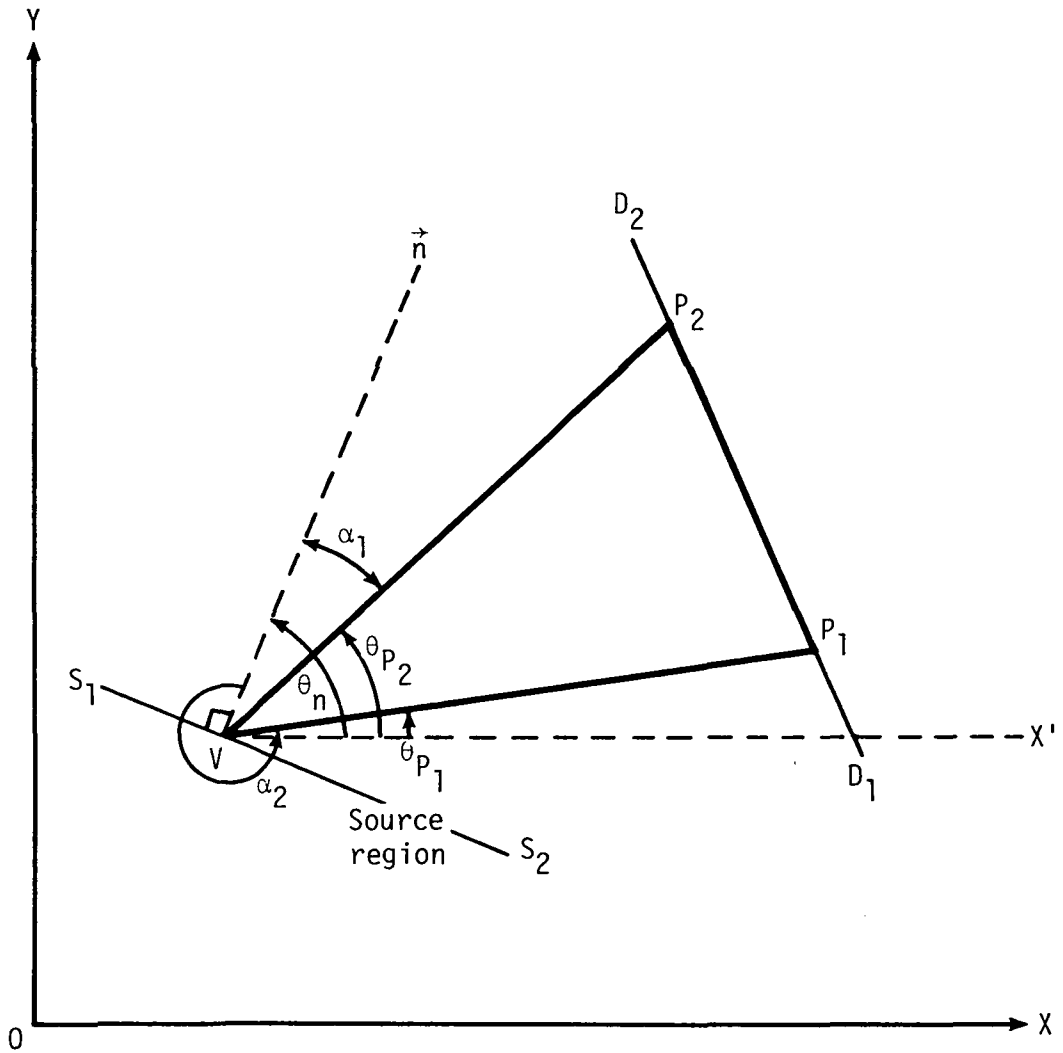


Figure 3.- Angles necessary for computation of configuration factor from view point V to unshadowed portion P<sub>1</sub>P<sub>2</sub> of destination region D<sub>1</sub>D<sub>2</sub>.

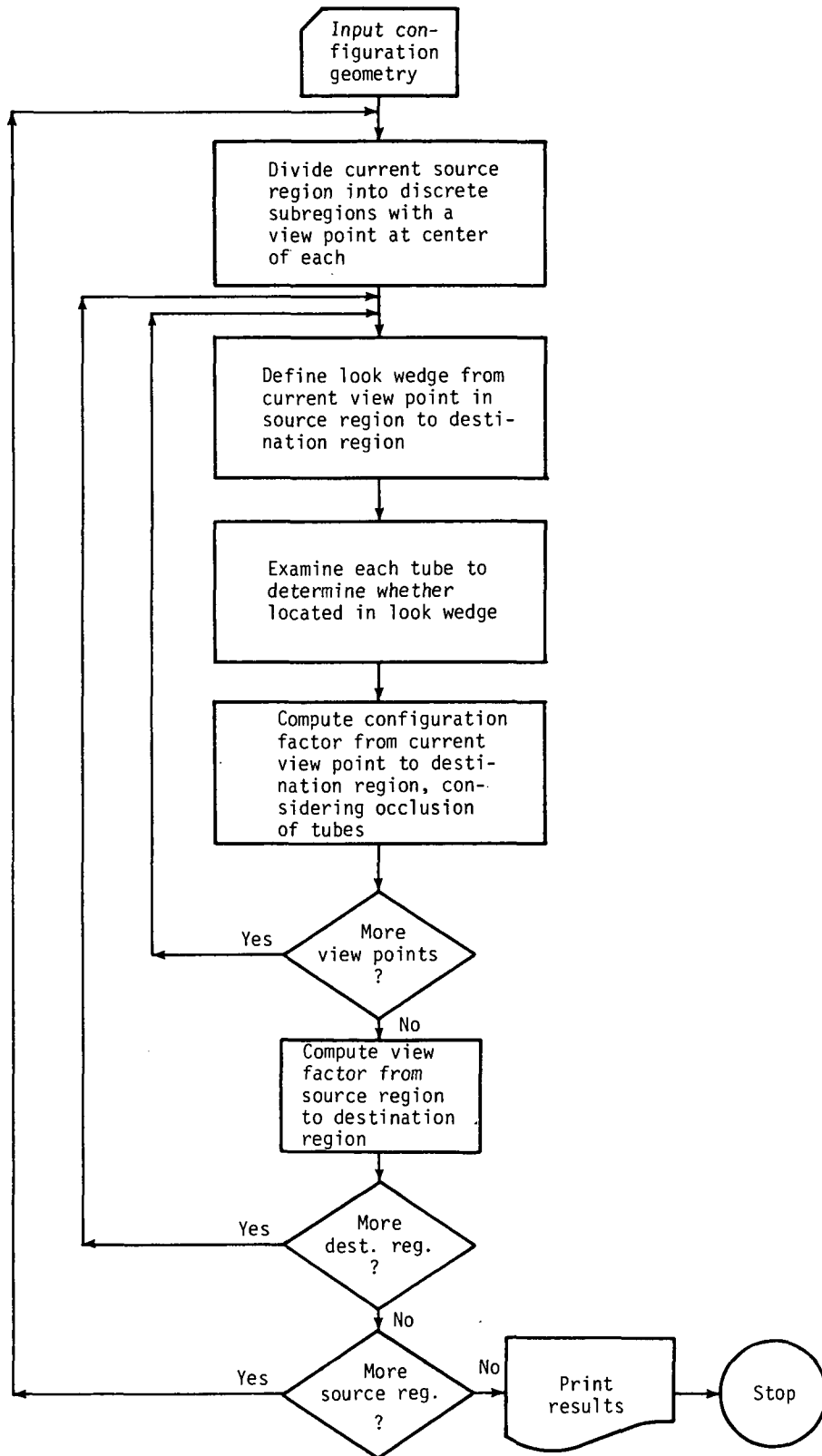
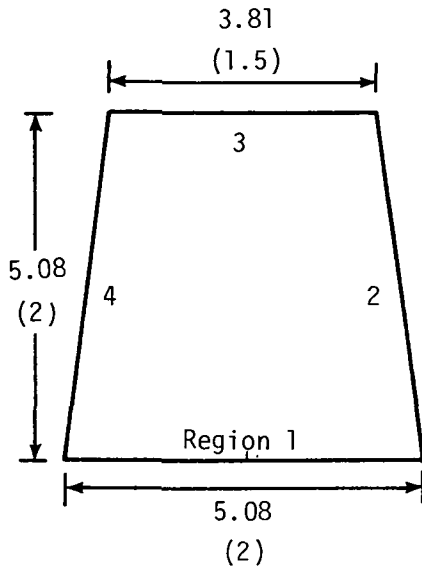


Figure 4.- Simplified flow chart of program VIEWFAC.



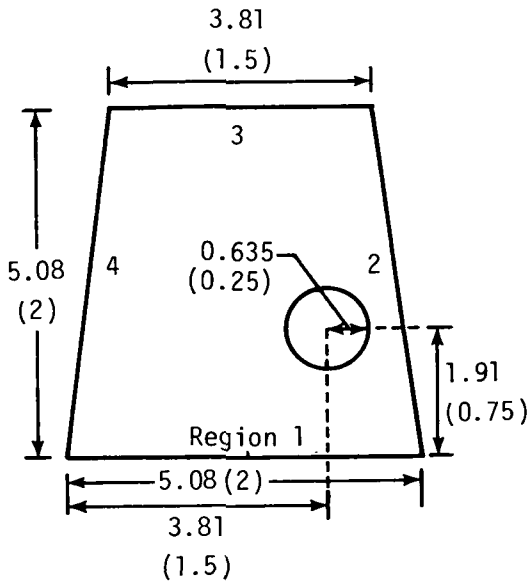
VIEW FACTORS FROM REGION 1  
 TO REGION 1 = 0.0000, AF = 0.00000  
 TO REGION 2 = .33951, AF = .67901  
 TO REGION 3 = .32099, AF = .64198  
 TO REGION 4 = .33951, AF = .67901  
 TO ALL ELEMENTS = 1.00000 AF = 2.00000  
 TO TUBES = .00000, AF = .00000

VIEW FACTORS FROM REGION 2  
 TO REGION 1 = .33688, AF = .67901  
 TO REGION 2 = 0.00000, AF = 0.00000  
 TO REGION 3 = .21285, AF = .42901  
 TO REGION 4 = .45027, AF = .90754  
 TO ALL ELEMENTS = 1.00000 AF = 2.01556  
 TO TUBES = .00000, AF = .00000

VIEW FACTORS FROM REGION 3  
 TO REGION 1 = .42798, AF = .64197  
 TO REGION 2 = .28601, AF = .42901  
 TO REGION 3 = 0.00000, AF = 0.00000  
 TO REGION 4 = .28601, AF = .42901  
 TO ALL ELEMENTS = 1.00000 AF = 1.50000  
 TO TUBES = .00000, AF = .00000

VIEW FACTORS FROM REGION 4  
 TO REGION 1 = .33688, AF = .67901  
 TO REGION 2 = .45027, AF = .90754  
 TO REGION 3 = .21285, AF = .42901  
 TO REGION 4 = 0.00000, AF = 0.00000  
 TO ALL ELEMENTS = 1.00000 AF = 2.01556  
 TO TUBES = .00000, AF = .00000

(a) No occlusion.



VIEW FACTORS FROM REGION 1  
 TO REGION 1 = 0.00000, AF = 0.00000  
 TO REGION 2 = .22579, AF = .45159  
 TO REGION 3 = .22651, AF = .45303  
 TO REGION 4 = .33579, AF = .67159  
 TO ALL ELEMENTS = .78810 AF = 1.57621  
 TO TUBES = .21190, AF = .42379

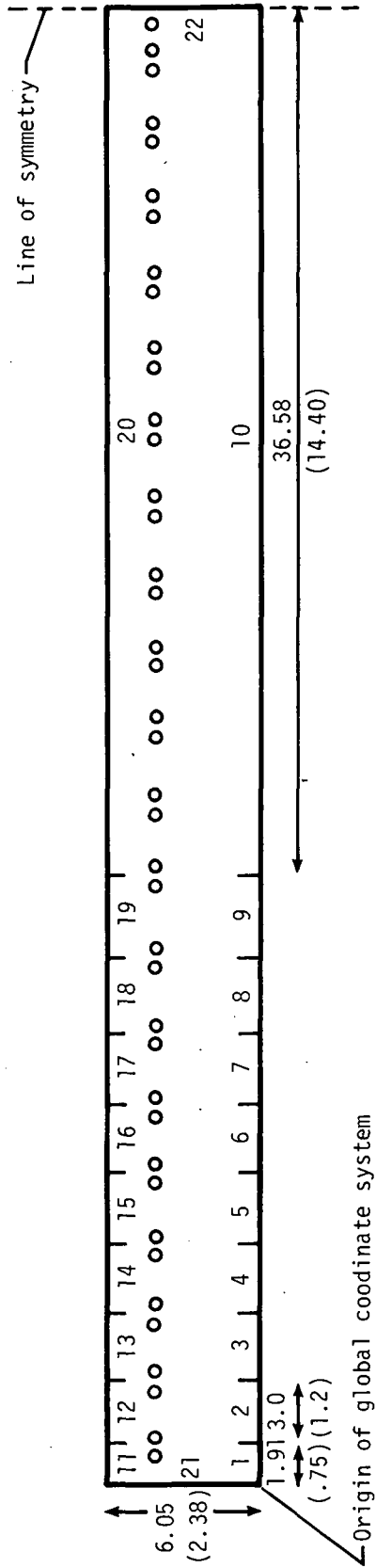
VIEW FACTORS FROM REGION 2  
 TO REGION 1 = .22404, AF = .45156  
 TO REGION 2 = 0.00000, AF = 0.00000  
 TO REGION 3 = .18467, AF = .37221  
 TO REGION 4 = .29904, AF = .60274  
 TO ALL ELEMENTS = .70775 AF = 1.42651  
 TO TUBES = .29225, AF = .58905

VIEW FACTORS FROM REGION 3  
 TO REGION 1 = .30204, AF = .45306  
 TO REGION 2 = .24815, AF = .37223  
 TO REGION 3 = 0.00000, AF = 0.00000  
 TO REGION 4 = .28601, AF = .42901  
 TO ALL ELEMENTS = .83620 AF = 1.25430  
 TO TUBES = .16380, AF = .24570

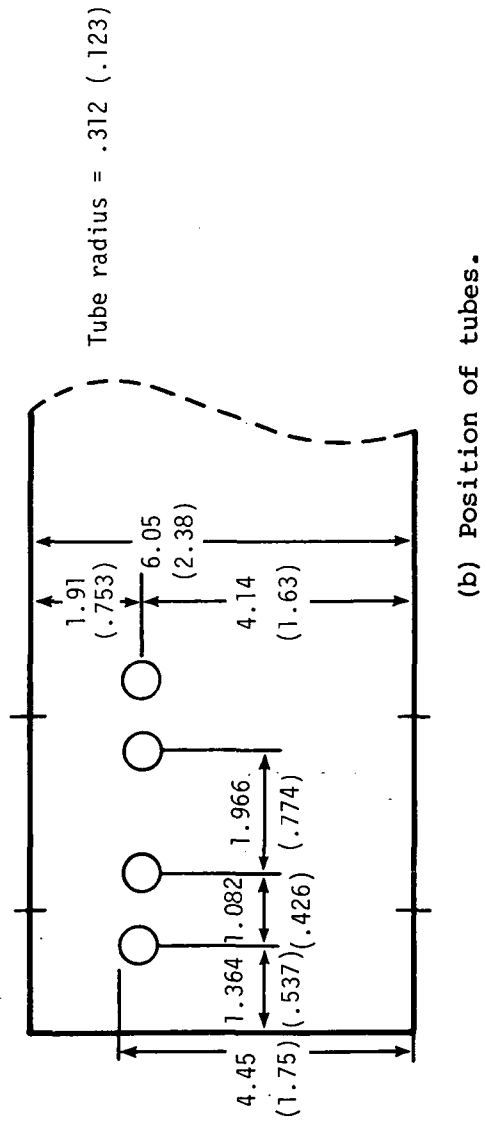
VIEW FACTORS FROM REGION 4  
 TO REGION 1 = .33320, AF = .67158  
 TO REGION 2 = .29903, AF = .60271  
 TO REGION 3 = .21285, AF = .42901  
 TO REGION 4 = 0.00000, AF = 0.00000  
 TO ALL ELEMENTS = .84507 AF = 1.70330  
 TO TUBES = .15493, AF = .31226

(b) Partial occlusion.

Figure 5.- Check cases used to verify program VIEWFAC.



(a) Region definition.



(b) Position of tubes.

Figure 6.- Demonstration problem: Two-dimensional model of quartz-lamp radiant heater. Dimensions shown are centimeters (inches).

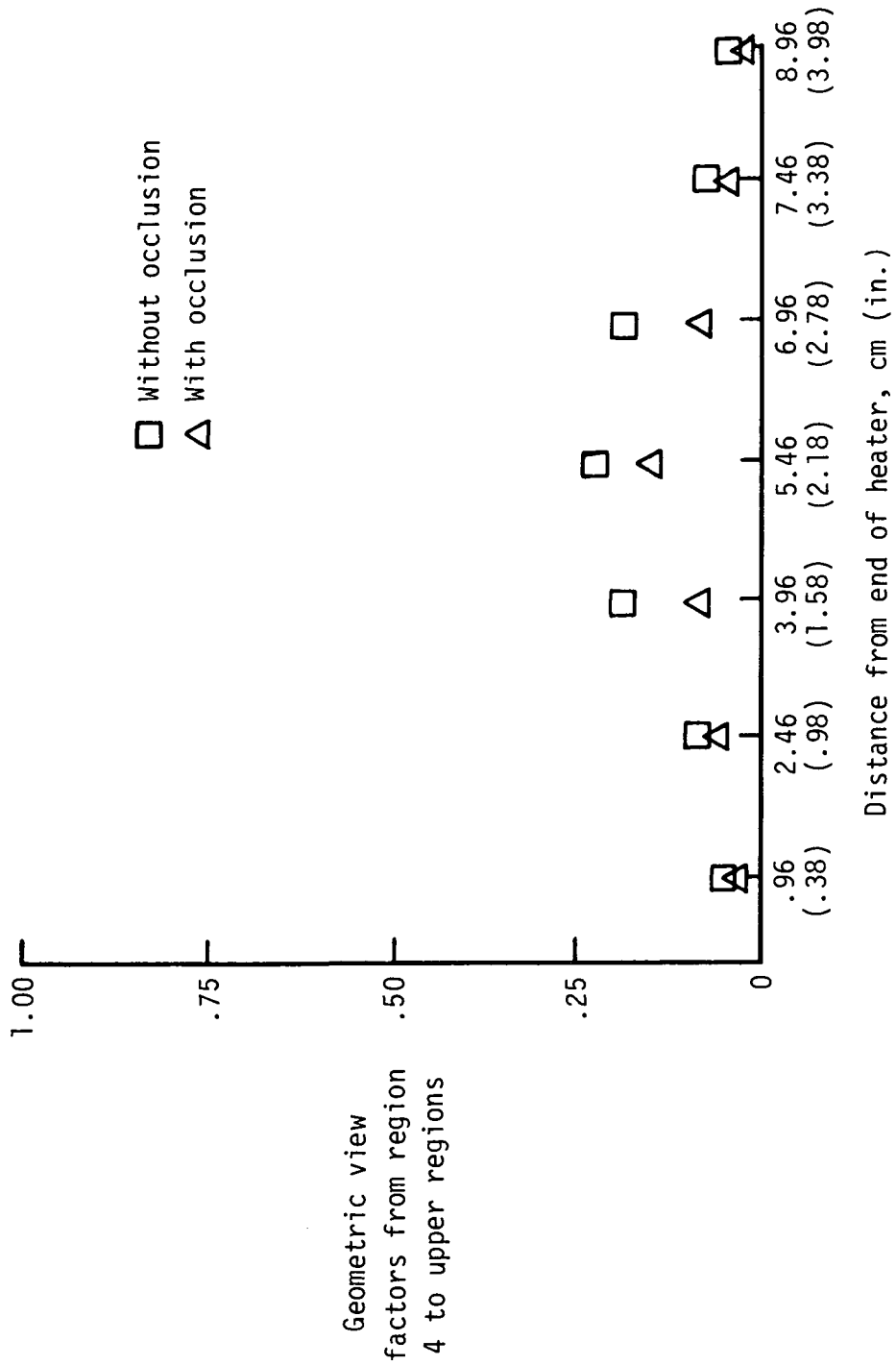


Figure 7.- Demonstration problem: Difference in geometric view factors with and without occlusion by lamps in heater.

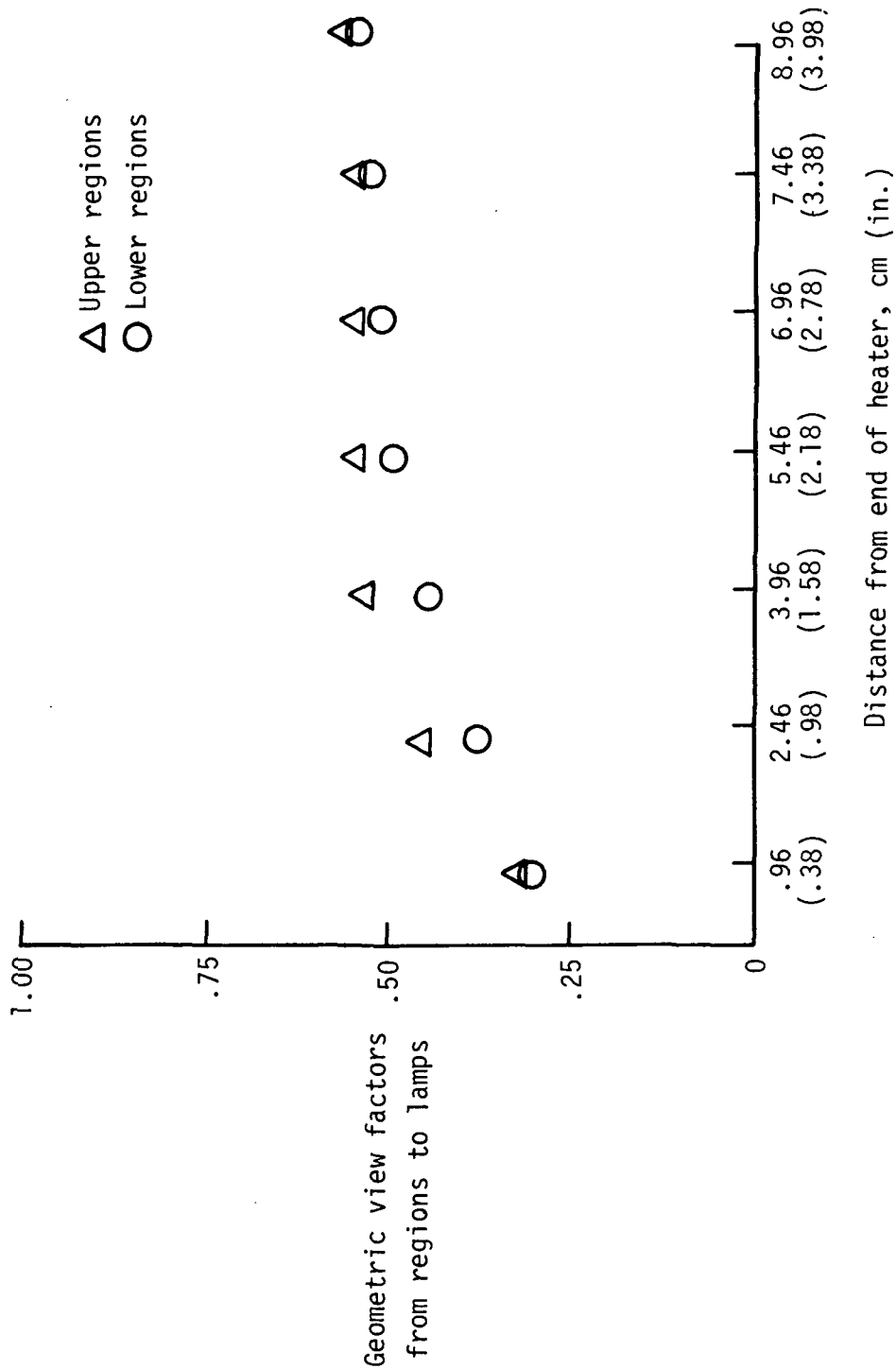


Figure 8.- Demonstration problem: Variation of geometric view factors from regions to lamps near end of heater.

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