

(NASA-TM-80195) TRANSONIC PRESSURE AND LOAD
DISTRIBUTIONS FOR A GROUP OF SIMULATED
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SUMMARY

Results in the form of pressure and load distributions for a related group of simulated launch vehicle configurations are presented. The configurations were selected so that the nose-cone and interstage transition-flare components were relatively close to one another and subject to mutual interference effects. Tests extended over a Mach number range from 0.40 to 1.20 at angles of attack from 0° to about 10° . The test Reynolds numbers, based on main stage diameter, were of the order of 0.98×10^6 .

INTRODUCTION

In the past, considerable experimental effort has been directed to the determination of aerodynamic force, moment, and loading characteristics for launch vehicle configurations. (See refs. 1 to 10.) This experimental effort was required, in part, because of the lack of suitable theoretical methods which could be used to predict vehicle aerodynamic characteristics with the required accuracy, particularly in the transonic speed range. Also, the available experimental results were applied in the development of empirical methods which could be used to make relatively rapid estimates of aerodynamic load distributions for some launch vehicle configurations. (See ref. 3, for example.) The empirical methods were limited in their application, however, to cone-cylinders or to configurations having no local flow separation. More recently, analytical methods have become available. (See ref. 11, for example.) The analytical approaches, however, are generally restricted to cases for attached flows.

As part of the experimental effort noted earlier, investigations have been conducted in the Langley 8-Foot Transonic Pressure Tunnel and the Langley Unitary Plan Wind Tunnel in order to determine the effects on force, moment, and loading characteristics of systematic variations in the geometry for simulated launch vehicles. Results for a number of configurations for which the nose-cone and stage transition-flare components were separated by a cylinder of relatively high fineness ratio are available in references 5 to 9.

The investigation was conducted in the Langley 8-Foot Transonic Pressure Tunnel in order to determine the effects of systematic variations in geometry on the load distributions of a number of configurations for which the nose-cone and stage transition-flare components were located relatively close to one another and were, therefore, subject to mutual interference effects which, in many cases, caused flow separation to occur. The tests extended over a Mach number range from 0.40 to 1.20 and angles of attack from 0° to about 10° . Test Reynolds numbers, based on the main stage diameter, were of the order of 0.98×10^6 . Transonic force and moment results for a number of identical configurations are given in reference 10.

SYMBOLS

Values are given in both SI and U.S. Customary Units. Measurements for this investigation were taken in U.S. Customary Units. Details concerning the use of SI Units, together with physical constants and conversion factors, are given in reference 12.

C_n	body section normal-force coefficient, $\int_0^1 (C_{p,l} - C_{p,u}) d\left(\frac{y}{r}\right)$
C_p	pressure coefficient, $\frac{p_l - p}{q}$
D	local diameter, cm (in.)
D_{ref}	main-stage diameter, 7.87 cm (3.10 in.)
l	model reference length, 127 cm (50 in.)
M	Mach number
p	free-stream static pressure, Pa (lb/ft ²)
p_l	local static pressure, Pa (lb/ft ²)
q	free-stream dynamic pressure, Pa (lb/ft ²)
$q_{M=1.20}$	free-stream dynamic pressure at $M = 1.20$, Pa (lb/ft ²)
R	Reynolds number based on main-stage diameter
r	local body radius, cm (in.)
x	longitudinal distance, measured from reference station 0 ahead of body, cm (in.)
y	lateral distance, measured from body center line, cm (in.)
α	true angle of attack, deg
α_{nom}	nominal angle of attack of model center line (does not include corrections for deflection of model and support system due to load), deg
δ_F	transition-flare half-angle, deg
δ_N	nose-cone half-angle, deg

ϕ orifice row meridian angle, measured clockwise from the vertical
as viewed from front, deg

Subscripts:

l lower

u upper

APPARATUS AND TESTS

Tunnel

The investigation was conducted in the Langley 8-Foot Transonic Pressure Tunnel. This facility is a single-return, rectangular, slotted-throat tunnel with controls that allow for the independent variation of Mach number, density, temperature, and humidity. The tunnel is designed to obtain aerodynamic data for speeds up to and through the speed of sound while minimizing the usual effects of blockage.

Model

The model used for the investigation was the variable-geometry model described in reference 5. For this investigation, the upper-stage cylinder fineness ratio was held constant at 1.42 for most configurations, and nose cones having half-angles from 15.3° to 30.0° were each tested in combination with interstage transition flares having half-angles from 5.0° to 30.0° . In addition, for one set of nose-cone and transition-flare components, the upper-stage fineness ratio was varied from 1.42 to 0. To aid the reader, model configurations are designated by a three-digit number according to the following arrangement:

First digit - nose-cone half-angle:

1	15.3°
2	22.5°
3	30.0°

Second digit - upper-stage fineness ratio:

2	1.42
3	.96
4	.50
5	0

Third digit - stage transition-flare half-angles:

1	5.0°
2	10.1°
3	15.0°
4	30.0°

For example, configuration 321 has a nose-cone half-angle of 30.0°, an upper-stage fineness ratio of 1.42, and a stage transition-flare half-angle of 5.0°. Model configurations are also listed in table 1.

Model pressure orifices were installed along four longitudinal rows which were located at meridian angles (measured clockwise from the vertical as viewed from the front) of 0°, 30°, 60°, and 90°. All orifice locations, which are indicated nondimensionally in the tables of results, are referenced to model station 0 which was located 127 cm (50 in.) forward of the model base. (See fig. 1(b).)

Tests and Procedure

The investigation was conducted at a stagnation pressure maintained at approximately 101.5 kPa (2120 lb/ft²). All configurations were tested at an angle of attack of 0° through a Mach number range from 0.40 to 1.20. Results were also obtained over an angle-of-attack range from -10° to 10° at Mach numbers of 0.60, 0.80, 1.00, and 1.20. Average test Reynolds numbers and dynamic pressures are given in figure 2.

The investigation was conducted with a transition strip located at the juncture of the nose cone and upper stage. The transition strip was 0.254 cm (0.1 in.) wide and was composed of No. 80 carborundum grains set in a plastic adhesive.

Model pressures were measured by the use of six scanning valve units. Differential pressure transducers were utilized, with ranges selected to provide nearly maximum gage outputs for the expected maximum pressure levels. No force or moment measurements were made during this investigation.

Boundary Interference Effects

At the time of the wind-tunnel investigation, the effects of subsonic boundary interference in the slotted test section were considered negligible. More recently, however, boundary-wall interference effects have been identified at Mach numbers close to 1.00. (See ref. 13.) These effects approach a maximum at a Mach number of 1.00; however, on the basis of the results of reference 13, they are confined to the rearward 50 percent of the bodies tested. For this investigation, therefore, the variations in loads over the regions of primary interest are judged to be valid at a Mach number of 1.00. At supersonic speeds,

the experimental results are generally affected by boundary-reflected disturbances which occur at Mach numbers from slightly over 1.00 to those at which disturbances are reflected downstream of the model base. For this investigation, the model lengths were such that no reflected disturbances affected the results at a Mach number of 1.20. Schlieren photographs, however, and an examination of the results indicate that a disturbance originating at the tunnel wall has a slight but noticeable effect on the pressure distributions at a Mach number of 1.20 at model stations between about $x/l = 0.82$ and $x/l = 0.86$. Because this effect is slight and occurs well to the rear of the model components which were varied, it is judged to be negligible in configuration comparisons.

CORRECTIONS AND ACCURACY

Angles of attack presented in this paper should be considered as nominal angles for this reason: although corrections have been made for tunnel airflow angularity, none have been applied for deflections of the model and support system under load. Estimates of the true angles of attack can be made, however, based upon the static loadings of reference 7 and the force and moment characteristics for the present configurations given in reference 10. The true angle of attack may be determined (to within $\pm 0.1^\circ$) from the empirical expression

$$\alpha = \alpha_{nom} \left(1 + 0.015 \frac{q}{q_{M=1.20}} \right)$$

where the values of dynamic pressure are obtained from figure 2.

A consideration of factors affecting the results of this investigation has indicated that pressure coefficients are generally accurate within ± 0.01 . However, in model regions of extremely varying pressures (for example, in the region of the juncture of the nose cone and upper stage or for conditions in which pressures are noticeably sensitive to small Mach number changes, such accuracies may not be expected. (See fig. 3.) Local deviations from the quoted free-stream Mach numbers did not exceed ± 0.015 .

DISCUSSION OF RESULTS.

Results of this investigation are presented as pressure coefficients (tables 2 to 15) and section normal-force coefficients (tables 16 to 26). Since the orifice rows extended only 90° radially about the model, section normal-force coefficients were obtained by combining pressure distribution results at identical positive and negative angles of attack. Representative data from the tables have been selected for graphical presentation (figs. 4 to 10) and are plotted to show the general effects of configuration variables on the pressure coefficients and on the section normal-force coefficients (multiplied by a diameter ratio to give load distributions).

Pressure Distributions

Effect of nose angle, $\alpha = 0^\circ$.— The effects of a variation in nose-cone angle on the longitudinal pressure distributions are presented in figure 4 for configurations having stage transition-flare angles ranging from 5.0° to 30.0° . For the lowest stage transition-flare angle ($\delta_F = 5^\circ$, fig. 4(a)), the effects of varying nose-cone angle are relatively slight; the most noticeable result is a broadening of the negative pressure-coefficient peaks just downstream of the juncture of the nose cone and upper stage at Mach numbers of 0.80 and 0.90 as nose-cone angle is increased. As noted in reference 5, the broadening of these peaks is associated with increases in separation as the nose-cone angle and associated adverse pressure gradient are increased.

As the stage transition-flare angle is increased to 30.0° (figs. 4(b) to 4(d)), the effects are greatly amplified because of the increased adverse pressure gradients resulting from the flare-angle increase. In the extreme case, a significant region of separated flow is evident for configuration 324 ($\delta_N = 30^\circ$, $\delta_F = 30^\circ$) at a Mach number of 0.90 just downstream of the nose-cone juncture. (See fig. 4(d).) Separation is also evident just downstream of the juncture of the transition flare and main stage at a Mach number of 0.90. This separation is indicated by the broadening of the associated peaks for all transition-flare angles and for nose-cone half-angles of 15.0° and 22.5° . (See figs. 4(b) to 4(d).) The configurations which exhibit the greatest degree of separation downstream of the juncture of the nose cone and upper stage appear to have the least amount of separation downstream of the juncture of the stage transition flare and the main stage. (See fig. 4(d) where $M = 0.90$, for example.) This characteristic results from the fact that for low nose-cone angles, the flow apparently remains attached over the upper-stage surface. Therefore, the full effect of the transition-flare compression and overexpansion is felt, and an adverse pressure gradient severe enough to separate the flow downstream of the juncture of the transition flare and the main stage results. For the higher nose-cone angles, separation over the upper stage tends to mask the effect of the transition flare, so that from an aerodynamic standpoint, the flow acts as if it were approaching a transition flare of a significantly lower angle and probably reattaches at the corner between the transition flare and the main stage.

Effects of angle of attack.— The effects of a variation in angle of attack from -6° to 6° on the pressure coefficients in the top row ($\phi = 0^\circ$) are presented in figures 5 to 8. For a transition-flare angle of 5° , pressure distributions at angles of attack from -6° to 6° are very similar to those at 0° and show little variation in characteristics as Mach number is varied (figs. 5(a) to 8(a)). As the transition-flare angle is increased to 10.1° , however, a noticeable broadening of the pressure-coefficient peak for the nose cone and upper stage occurs. This broadening, indicative of separation, appears as the angle of attack is increased to 3° and 6° (figs. 7(b) and 8(b)).

Generally, increases in stage transition-flare angle to 15.0° and 30.0° result in an earlier onset of the noted separation effects with regard to both angle of attack and Mach number. For the higher flare angles, separation on the main stage becomes apparent at the higher Mach numbers. (See figs. 7(c) and 8(c), for example, at Mach numbers of 1.00 and 1.20.)

Loading Distributions

The effects of variations in nose-cone angle on the load distributions for angles of attack of 3° and 6° are presented in figures 9 and 10, respectively. As expected, the nose-cone and transition-flare components carry the greater portion of the loading. For configurations which experience a significant degree of separation (see, for example, configuration 324 at a Mach number of 0.80, fig. 10(d)), a notable portion of the load is carried by the upper stage.

SUMMARY OF RESULTS

Results of this investigation are presented as pressure coefficients and section normal-force coefficients. At low stage transition-flare angles, effects of varying nose-cone angle are slight. As stage transition-flare angle is increased, significant regions of flow separation occur. These regions are associated with increased adverse pressure gradients. Generally, increases in stage transition-flare angle to 30.0° result in an earlier onset of the noted separation effects with regard to both angle of attack and Mach number.

Langley Research Center
National Aeronautics and Space Administration
Hampton, VA 23665
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TABLE 1.- MODEL CONFIGURATIONS

Configuration	Nose-cone half-angle, deg	Upper-stage fineness ratio	Transition-flare half-angle, deg
121	15.3	1.42	5.0
221	22.5	↓	↓
321	30.0		↓
122	15.3		10.1
222	22.5		↓
322	30.0		↓
123	15.3		15.0
223	22.5		↓
323	30.0		↓
124	15.3		30.0
324	30.0		↓
133	15.3	.96	15.0
143	↓	.50	↓
153	↓	0	↓

TABLE 2.- PRESSURE COEFFICIENTS FOR CONFIGURATION 121

(a) $M = 0.40$ to 0.95 ; $\alpha = 0^\circ$

		C_p for -					
		$\beta = 0^\circ$					
x/l		$M = 0.40$	$M = 0.70$	$M = 0.85$	$M = 0.90$	$M = 0.95$	
Nose	328	.251	.282	.289	.312	.329	.356
	330	.229	.251	.257	.281	.300	.328
	348	.196	.220	.225	.250	.271	.301
	358	.163	.176	.180	.208	.231	.267
	378	.065	.075	.080	.115	.147	.192
Upper stage	368	-.045	-.037	-.026	.031	.078	.131
	393	-.169	-.179	-.156	-.057	.006	.072
	399	-.857	-1.273	-1.287	-.968	-.830	-.697
	404	-.224	-.301	-.408	-.992	-.916	-.798
	409	-.123	-.155	-.192	-.396	-.809	-.709
Transition	419	-.045	-.055	-.059	-.103	-.198	-.553
	429	.000	-.010	-.014	.018	.007	-.416
	439	.022	.027	.024	.043	.088	-.012
	449	.067	.072	.070	.083	.121	.135
	459	.179	.191	.150	.200	.225	.243
Main stage	482	.055	.058	.056	.060	.076	.133
	492	.033	.035	.032	.036	.043	.092
	512	.033	.026	.015	.018	.023	.034
	532	.011	-.005	-.009	-.017	-.010	.020
	552	-.045	-.026	-.064	-.079	-.078	-.037
Transition	562	-.079	-.106	-.118	-.144	-.156	-.111
	577	-.068	-.220	-.234	-.304	-.448	-.417
	587	-.045	-.056	-.064	-.078	-.077	-.283
	597	-.034	-.037	-.047	-.057	-.057	-.117
	607	-.023	-.028	-.034	-.046	-.044	-.021
Main stage	617	-.023	-.024	-.030	-.046	-.037	-.012
	627	-.023	-.019	-.026	-.032	-.034	-.009
	637	.000	-.010	-.018	-.028	-.023	-.009
	657	.000	.004	.008	-.022	-.016	-.010
	677	.000	.005	.008	-.011	-.013	-.013
Transition	697	.004	.009	.005	.011	-.011	-.012
	737	.008	.010	.004	-.009	-.010	-.013
	777	.008	.013	.000	-.005	-.005	-.010
	785	.011	.016	.005	-.002	-.002	-.005
	817	.009	.008	.004	-.003	-.003	-.005
Main stage	857	.006	.005	.000	-.003	-.006	-.009
	877	.006	.005	.001	-.006	-.006	-.008
	897	.004	.002	-.003	-.009	-.009	-.012

		C_p for -				
		$\beta = -30^\circ$				
x/l		$M = 0.40$	$M = 0.70$	$M = 0.85$	$M = 0.90$	$M = 0.95$
Nose	338	.229	.242	.249	.267	.290
	348	.185	.203	.213	.236	.257
	358	.152	.172	.180	.205	.228
	378	.065	.070	.05	.108	.140
	388	-.045	-.042	-.030	.028	.075
Upper stage	393	.180	.179	-.151	-.057	.006
	399	-.823	-1.204	-1.433	-1.115	-.969
	404	-.224	-.315	-.412	-1.013	-.916
	409	-.112	-.146	-.188	-.389	-.832
	419	-.045	-.055	-.059	-.096	-.191
Transition	429	.000	-.010	-.009	.018	-.017
	439	.022	.027	.024	.043	-.088
	449	.078	.081	.078	.090	-.128
	459	.191	.200	.194	.208	-.232
	482	.055	.062	.060	.060	.076
Main stage	492	.033	.035	.032	.036	.043
	512	.033	.013	.015	.007	.013
	532	.000	-.010	-.014	-.021	-.017
	552	-.045	-.056	-.064	-.079	-.078
	562	-.091	-.134	-.144	-.176	-.193
Transition	577	.158	.197	.218	.279	.421
	587	.068	.092	.101	.125	.131
	597	.045	.056	.064	.082	.084
	607	.034	.028	.034	.046	.044
	617	-.023	-.024	-.030	-.046	-.044
Main stage	627	-.023	-.024	-.030	-.046	-.044
	637	.000	-.010	-.018	-.028	-.037
	657	.004	.002	.011	-.021	-.027
	677	.004	.012	.007	-.009	-.020
	697	.000	.009	.007	-.011	-.012
Transition	737	.004	.012	.007	-.008	-.009
	777	.011	.016	.005	-.002	-.011
	785	.011	.016	.005	-.002	-.005
	817	.009	.008	.003	-.003	-.005
	857	.006	.004	.003	-.003	-.005
Main stage	877	.006	.003	.003	-.003	-.005
	897	.003	.001	.003	-.003	-.010
	917	.003	.001	.003	-.003	-.009
	957	-.006	-.010	-.014	-.021	-.013
	997	-.058	-.064	-.070	-.077	-.080

TABLE 2.- PRESSURE COEFFICIENTS FOR CONFIGURATION 121 - Continued

(a) $M = 0.40$ to 0.95 ; $\alpha = 0^\circ$ - Concluded

		C_p for -												
		$\beta = -50^\circ$												
		$M = 0.40$	$M = 0.70$	$M = 0.85$	$M = 0.90$	$M = 0.95$	$M = 0.40$	$M = 0.70$	$M = 0.85$	$M = 0.90$	$M = 0.95$			
Main stage	x/z	.338	.242	.265	.267	.287	.293	.287	.261	.287	.293	.316	.336	.362
		.348	.203	.209	.232	.287	.287	.225	.207	.225	.22	.255	.277	.307
Transition flare	x/z	.358	.163	.168	.198	.218	.254	.163	.152	.163	.168	.194	.218	.251
		.378	.067	.067	.101	.134	.180	.057	.054	.057	.063	.101	.134	.180
Upper stage	x/z	.388	-.051	-.039	.021	.075	.21	.021	-.051	.057	.063	.101	.134	.180
		.393	-.069	-.072	-.075	-.077	-.089	.021	-.203	-.207	-.185	-.082	-.023	.047
Nose	x/z	.399	-1.127	-1.237	-.965	-.837	-.710	-.077	-.755	-1.062	-1.007	-.904	-.776	-.655
		.404	-.224	-.425	-1.020	-.947	-.824	-.077	-.045	-.051	-.051	-.039	-.158	-.559
Main stage	x/z	.409	-.101	-.133	-.406	-.816	-.718	-.078	-.045	-.051	-.024	.036	.088	.014
		.419	-.045	-.059	-.078	-.185	-.566	.034	.022	.027	.024	.211	.235	.256
Transition flare	x/z	.429	.000	.031	.043	.091	.004	.091	.022	.027	.024	.036	.088	.014
		.449	.078	.070	.083	.121	.144	.070	.022	.027	.024	.036	.088	.014
Upper stage	x/z	.459	.179	.186	.197	.225	.246	.186	.191	.200	.194	.211	.235	.256
		.482	.055	.052	.057	.073	.130	.052	.055	.058	.052	.057	.073	.130
Main stage	x/z	.492	.033	.032	.036	.043	.097	.043	.022	.013	.011	.007	.013	.048
		.512	.033	.015	.007	.013	.048	.013	.022	.013	.011	.007	.013	.048
Transition flare	x/z	.532	.000	-.010	-.021	-.017	.013	-.017	-.045	-.060	-.068	-.082	-.081	-.041
		.552	-.045	-.065	-.072	-.085	-.044	-.044	-.045	-.060	-.068	-.085	-.084	-.299
Upper stage	x/z	.562	-.102	-.134	-.176	-.090	-.085	-.085	-.180	-.247	-.264	-.340	-.522	-.475
		.568	.158	.192	.214	.268	.397	.360	-.180	-.247	-.264	-.340	-.522	-.475
Main stage	x/z	.577	-.068	-.092	-.125	-.128	-.296	-.360	-.045	-.060	-.068	-.085	-.084	-.299
		.587	-.045	-.060	-.082	-.084	-.296	-.360	-.045	-.060	-.068	-.085	-.084	-.299
Transition flare	x/z	.597	-.034	-.037	-.043	-.057	-.057	-.117	-.023	-.028	-.034	-.046	-.044	-.021
		.607	-.023	-.028	-.034	-.044	-.021	-.117	-.023	-.028	-.034	-.046	-.044	-.021
Main stage	x/z	.617	-.023	-.024	-.030	-.046	-.037	-.012	.000	.019	.022	.032	.034	.012
		.627	.000	-.019	-.022	-.032	-.034	-.012	.000	.019	.022	.032	.034	.012
Upper stage	x/z	.637	.000	-.014	-.018	-.028	-.027	-.012	-.004	.002	.011	.021	.018	.012
		.657	-.004	-.009	-.009	-.014	-.014	-.011	-.004	.002	.011	.021	.018	.012
Main stage	x/z	.677	.000	-.005	-.007	-.014	-.014	-.011	-.004	.002	.011	.021	.018	.012
		.697	.004	.010	.009	.010	.010	.010	.000	.007	.005	.013	.012	.013
Transition flare	x/z	.737	.004	.012	.007	.008	.011	.011	.004	.012	.001	.007	.008	.011
		.777	.008	.015	.003	.002	.004	.004	.008	.013	.002	.004	.004	.006
Main stage	x/z	.785	.008	.016	.005	.004	.007	.007	.008	.015	.007	.002	.002	.005
		.817	.009	.009	.004	.002	.004	.004	.010	.010	.005	.002	.002	.005
Upper stage	x/z	.877	.004	.004	.004	.007	.010	.010	.006	.005	.005	.007	.006	.010
		.897	.004	.004	.004	.007	.010	.010	.006	.005	.005	.007	.006	.010
Main stage	x/z	.917	.001	.003	.003	.008	.011	.011	.003	.002	.003	.009	.009	.012
		.957	-.009	-.014	-.020	-.013	-.016	-.016	.003	.002	.003	.009	.009	.012
Transition flare	x/z	.997	-.059	-.066	-.079	-.083	-.095	-.095	-.059	.002	.003	.009	.009	.012

TABLE 2.- PRESSURE COEFFICIENTS FOR CONFIGURATION 121 - Continued

(b) $M = 0.60$; $\alpha = -10^\circ$ to 10°

		C_p for $\beta = 0^\circ$						C_p for $\beta = -30^\circ$							
		$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$	$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$
Main stage	x/z	.328	.367	.305	.27	.205	.177	.119	.377	.317	.272	.224	.178	.138	.089
		.438	.367	.305	.27	.205	.177	.119	.377	.317	.272	.224	.178	.138	.089
		.405	.334	.278	.233	.178	.144	.085	.348	.284	.239	.191	.139	.085	.030
		.372	.301	.250	.205	.150	.110	.052	.318	.245	.206	.158	.106	.066	.003
		.333	.262	.212	.158	.106	.066	.019	.284	.206	.166	.118	.078	.038	-.003
		.288	.228	.162	.106	.053	.029	-.083	.245	.166	.126	.078	.038	-.003	-.040
		.248	.182	.116	.054	.006	-.029	-.083	.206	.126	.086	.038	-.003	-.040	-.100
		.208	.142	.076	-.004	-.108	-.138	-.181	.166	.086	.046	-.010	-.050	-.090	-.130
		.168	.102	.036	-.054	-.138	-.181	-.224	.126	.046	.006	-.040	-.080	-.120	-.160
		.128	.062	-.014	-.083	-.168	-.212	-.256	.086	.006	-.040	-.080	-.120	-.160	-.200
Transition Plate	x/z	.399	.220	.124	.059	.024	.012	.015	.399	.220	.124	.059	.024	.012	.015
		.404	.220	.124	.059	.024	.012	.015	.399	.220	.124	.059	.024	.012	.015
		.409	.220	.124	.059	.024	.012	.015	.404	.220	.124	.059	.024	.012	.015
		.419	.220	.124	.059	.024	.012	.015	.409	.220	.124	.059	.024	.012	.015
		.429	.220	.124	.059	.024	.012	.015	.419	.220	.124	.059	.024	.012	.015
		.439	.220	.124	.059	.024	.012	.015	.429	.220	.124	.059	.024	.012	.015
		.449	.220	.124	.059	.024	.012	.015	.439	.220	.124	.059	.024	.012	.015
		.459	.220	.124	.059	.024	.012	.015	.449	.220	.124	.059	.024	.012	.015
		.462	.220	.124	.059	.024	.012	.015	.459	.220	.124	.059	.024	.012	.015
		.468	.220	.124	.059	.024	.012	.015	.462	.220	.124	.059	.024	.012	.015
Rise	x/z	.512	.301	.182	.082	.042	.024	.012	.512	.301	.182	.082	.042	.024	.012
		.532	.301	.182	.082	.042	.024	.012	.512	.301	.182	.082	.042	.024	.012
		.552	.301	.182	.082	.042	.024	.012	.532	.301	.182	.082	.042	.024	.012
		.562	.301	.182	.082	.042	.024	.012	.552	.301	.182	.082	.042	.024	.012
		.568	.301	.182	.082	.042	.024	.012	.562	.301	.182	.082	.042	.024	.012
		.577	.301	.182	.082	.042	.024	.012	.568	.301	.182	.082	.042	.024	.012
		.587	.301	.182	.082	.042	.024	.012	.577	.301	.182	.082	.042	.024	.012
		.597	.301	.182	.082	.042	.024	.012	.587	.301	.182	.082	.042	.024	.012
		.607	.301	.182	.082	.042	.024	.012	.597	.301	.182	.082	.042	.024	.012
		.617	.301	.182	.082	.042	.024	.012	.607	.301	.182	.082	.042	.024	.012

TABLE 2.-- PRESSURE COEFFICIENTS FOR CONFIGURATION 121 - Continued

(b) $M = 0.60$; $\alpha = -10^\circ$ to 10° - Concluded

		C_p for $\beta = -60^\circ$						C_p for $\beta = -90^\circ$						
		$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$	$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$
Rose	x/t	.338	.250	.219	.189	.149	.069	.328	.240	.267	.268	.261	.238	.168
		.348	.222	.180	.150	.110	.036	.358	.124	.145	.141	.134	.116	.047
		.378	.184	.141	.112	.072	-.003	.378	.030	.046	.042	.029	.011	-.049
		.388	.084	.042	.012	-.029	-.100							
		.393	-.021	-.044	-.071	-.138	-.198	.393	-.244	-.228	-.226	-.239	-.252	-.301
		.399	-.124	-.079	-.095	-.103	-.135	.399	-.834	-.881	-.902	-.909	-.939	-.977
		.404	-.817	-.834	-.881	-.947	-1.045							
		.404	-.283	-.271	-.266	-.272	-.302							
		.404	-.158	-.129	-.124	-.124	-.143							
		.419	-.101	-.072	-.056	-.034	-.185	.419	-.083	-.061	-.059	-.056	-.080	-.146
Upper stage	x/t	.429	-.061	-.020	.010	.034	-.033	.439	-.015	.013	.015	.018	-.012	-.077
		.439	.027	.008	.024	.006	-.043							
		.449	.019	.053	.064	.046	.094	.459	.098	.178	.174	.183	.154	.088
		.459	.150	.179	.184	.148	.094	.482	-.050	.035	.037	.029	.006	-.043
		.482	.013	.041	.052	.012	-.038							
		.492	-.004	.025	.020	-.012	-.055	.512	-.085	.001	.003	-.010	-.023	-.078
		.512	.016	.019	.024	-.023	-.072							
		.532	-.039	-.015	-.010	-.039	-.058	.552	-.142	-.068	-.071	-.079	-.098	-.141
		.552	-.096	-.067	-.068	-.071	-.104							
		.562	-.159	-.136	-.140	-.148	-.161	.568	-.330	-.233	-.231	-.256	-.274	-.335
Transition Flare	x/t	.568	-.192	-.187	-.193	-.200	-.237	.587	-.089	-.061	-.065	-.079	-.097	-.146
		.577	-.136	-.084	-.089	-.114	-.135							
		.587	-.107	-.072	-.065	-.073	-.080	.607	-.118	-.033	-.037	-.045	-.069	-.112
		.597	-.090	-.055	-.042	-.056	-.069	.627	-.101	-.044	-.025	-.039	-.052	-.106
		.607	-.084	-.049	-.037	-.045	-.052	.657	-.094	-.036	-.006	-.020	-.038	-.091
		.617	-.078	-.044	-.031	-.039	-.052							
		.627	-.073	-.032	-.025	-.033	-.046	.697	-.088	-.012	-.004	-.004	-.020	-.036
		.637	-.067	-.027	-.016	-.027	-.040	.737	-.082	-.006	-.002	-.002	-.014	-.031
		.657	-.054	-.021	-.012	-.020	-.025	.777	-.079	-.004	-.001	-.001	-.014	-.027
		.677	-.047	-.017	-.008	-.005	-.024	.785	-.082	-.004	-.004	-.014	-.025	-.076
Main stage	x/t	.677	-.047	-.008	-.005	-.024	-.044	.817	-.071	-.016	-.003	-.005	-.020	-.069
		.697	-.040	-.004	-.004	-.023	-.045	.857	-.074	-.023	-.002	-.010	-.027	-.073
		.737	-.052	-.019	-.006	-.002	-.034							
		.777	-.052	-.013	-.000	-.010	-.032	.897	-.075	-.027	-.004	-.012	-.030	-.076
		.785	-.054	-.017	-.004	-.013	-.030							
		.817	-.047	-.009	-.002	-.004	-.027	.917	-.062	-.010	-.003	-.005	-.020	-.069
		.857	-.033	-.016	-.003	-.009	-.029	.957	-.066	-.031	-.017	-.016	-.023	-.073
		.877	-.052	-.004	-.003	-.009	-.013							
		.917	-.053	-.019	-.005	-.004	-.020	.997	-.086	-.030	-.023	-.030	-.044	-.124
		.957	-.062	-.023	-.015	-.023	-.030							

Table 1 - FREQUENCIES FOR CONFIDENCES 22 - Continues

$$N = 1000, \alpha = .10, \beta = .10$$

z	$\frac{r}{N} = .50$										
	$\beta = .10$					$\beta = .50$					
	$\alpha = .10$	$\alpha = .50$	$\alpha = .90$	$\alpha = .95$	$\alpha = .99$	$\alpha = .10$	$\alpha = .50$	$\alpha = .90$	$\alpha = .95$	$\alpha = .99$	
.00	.480	.342	.253	.200	.152	.410	.345	.304	.259	.215	.165
.01	.481	.342	.253	.200	.152	.410	.345	.304	.259	.215	.165
.02	.482	.343	.254	.201	.153	.411	.346	.305	.260	.216	.166
.03	.483	.344	.255	.202	.154	.412	.347	.306	.261	.217	.167
.04	.484	.345	.256	.203	.155	.413	.348	.307	.262	.218	.168
.05	.485	.346	.257	.204	.156	.414	.349	.308	.263	.219	.169
.06	.486	.347	.258	.205	.157	.415	.350	.309	.264	.220	.170
.07	.487	.348	.259	.206	.158	.416	.351	.310	.265	.221	.171
.08	.488	.349	.260	.207	.159	.417	.352	.311	.266	.222	.172
.09	.489	.350	.261	.208	.160	.418	.353	.312	.267	.223	.173
.10	.490	.351	.262	.209	.161	.419	.354	.313	.268	.224	.174
.11	.491	.352	.263	.210	.162	.420	.355	.314	.269	.225	.175
.12	.492	.353	.264	.211	.163	.421	.356	.315	.270	.226	.176
.13	.493	.354	.265	.212	.164	.422	.357	.316	.271	.227	.177
.14	.494	.355	.266	.213	.165	.423	.358	.317	.272	.228	.178
.15	.495	.356	.267	.214	.166	.424	.359	.318	.273	.229	.179
.16	.496	.357	.268	.215	.167	.425	.360	.319	.274	.230	.180
.17	.497	.358	.269	.216	.168	.426	.361	.320	.275	.231	.181
.18	.498	.359	.270	.217	.169	.427	.362	.321	.276	.232	.182
.19	.499	.360	.271	.218	.170	.428	.363	.322	.277	.233	.183
.20	.500	.361	.272	.219	.171	.429	.364	.323	.278	.234	.184
.21	.501	.362	.273	.220	.172	.430	.365	.324	.279	.235	.185
.22	.502	.363	.274	.221	.173	.431	.366	.325	.280	.236	.186
.23	.503	.364	.275	.222	.174	.432	.367	.326	.281	.237	.187
.24	.504	.365	.276	.223	.175	.433	.368	.327	.282	.238	.188
.25	.505	.366	.277	.224	.176	.434	.369	.328	.283	.239	.189
.26	.506	.367	.278	.225	.177	.435	.370	.329	.284	.240	.190
.27	.507	.368	.279	.226	.178	.436	.371	.330	.285	.241	.191
.28	.508	.369	.280	.227	.179	.437	.372	.331	.286	.242	.192
.29	.509	.370	.281	.228	.180	.438	.373	.332	.287	.243	.193
.30	.510	.371	.282	.229	.181	.439	.374	.333	.288	.244	.194
.31	.511	.372	.283	.230	.182	.440	.375	.334	.289	.245	.195
.32	.512	.373	.284	.231	.183	.441	.376	.335	.290	.246	.196
.33	.513	.374	.285	.232	.184	.442	.377	.336	.291	.247	.197
.34	.514	.375	.286	.233	.185	.443	.378	.337	.292	.248	.198
.35	.515	.376	.287	.234	.186	.444	.379	.338	.293	.249	.199
.36	.516	.377	.288	.235	.187	.445	.380	.339	.294	.250	.200
.37	.517	.378	.289	.236	.188	.446	.381	.340	.295	.251	.201
.38	.518	.379	.290	.237	.189	.447	.382	.341	.296	.252	.202
.39	.519	.380	.291	.238	.190	.448	.383	.342	.297	.253	.203
.40	.520	.381	.292	.239	.191	.449	.384	.343	.298	.254	.204
.41	.521	.382	.293	.240	.192	.450	.385	.344	.299	.255	.205
.42	.522	.383	.294	.241	.193	.451	.386	.345	.300	.256	.206
.43	.523	.384	.295	.242	.194	.452	.387	.346	.301	.257	.207
.44	.524	.385	.296	.243	.195	.453	.388	.347	.302	.258	.208
.45	.525	.386	.297	.244	.196	.454	.389	.348	.303	.259	.209
.46	.526	.387	.298	.245	.197	.455	.390	.349	.304	.260	.210
.47	.527	.388	.299	.246	.198	.456	.391	.350	.305	.261	.211
.48	.528	.389	.300	.247	.199	.457	.392	.351	.306	.262	.212
.49	.529	.390	.301	.248	.200	.458	.393	.352	.307	.263	.213
.50	.530	.391	.302	.249	.201	.459	.394	.353	.308	.264	.214

TABLE 2.- PRESSURE COEFFICIENTS FOR CONFIGURATION 221 - Continued

(c) $M = 0.86$, $\alpha = -10^\circ$ to 10° - Continued

x, z	C_p for $\beta = -30^\circ$						
	$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$
Main stage	.328	.271	.293	.357	.297	.273	.212
	.358	.152	.171	.181	.170	.143	.093
	.373	.063	.078	.084	.074	.053	-.008
Upper stage	.353	-.162	-.143	-.136	-.143	-.168	-.216
	.399	-1.055	-1.044	-1.037	-1.056	-1.073	-1.109
	.419	-.145	-.062	-.044	-.054	-.094	-.157
Transition	.439	-.072	.019	.029	.019	-.006	-.077
	.459	.124	.187	.158	.195	.166	.107
	.482	-.034	.045	.052	.049	.013	-.035
Main stage	.512	-.080	-.004	.006	.003	-.029	-.081
	.552	-.146	-.085	-.079	-.082	-.114	-.167
	.568	-.418	-.300	-.286	-.308	-.352	-.419
Main stage	.587	-.157	-.085	-.074	-.085	-.110	-.162
	.607	-.122	-.046	-.036	-.047	-.071	-.127
	.627	-.107	-.062	-.024	-.035	-.060	-.108
Main stage	.657	-.095	-.048	-.020	-.022	-.046	-.098
	.697	-.088	-.044	-.018	-.016	-.041	-.090
	.737	-.081	-.040	-.013	-.012	-.034	-.081
Main stage	.777	-.077	-.035	-.009	-.008	-.030	-.075
	.785	-.081	-.037	-.004	-.006	-.029	-.075
	.817	-.070	-.025	-.004	-.004	-.025	-.068
Main stage	.857	-.072	-.033	-.011	-.006	-.032	-.073
	.897	-.075	-.037	-.013	-.009	-.035	-.074
	.937	-.075	-.037	-.013	-.009	-.035	-.074
Main stage	.997	-.134	-.106	-.073	-.080	-.104	-.129
	.997	-.106	-.084	-.073	-.080	-.104	-.129
	.997	-.106	-.084	-.073	-.080	-.104	-.129
Main stage	.338	.293	.278	.254	.226	.180	.104
	.348	.256	.241	.222	.185	.143	.067
	.358	.224	.219	.181	.152	.126	.083
Main stage	.378	.127	.107	.084	.055	.009	-.034
	.388	.027	.014	-.013	-.039	-.083	-.147
	.393	-.122	-.096	-.071	-.078	-.102	-.131
Main stage	.399	-1.081	-1.099	-1.118	-1.152	-1.192	-1.167
	.404	-.470	-.521	-.557	-.552	-.550	-.571
	.409	-.221	-.280	-.285	-.272	-.277	-.218
Main stage	.419	-.114	-.058	-.047	-.054	-.094	-.131
	.429	-.044	-.031	-.005	-.068	-.021	-.065
	.439	-.022	.007	.033	.026	.009	-.027
Main stage	.449	.028	.053	.079	.068	.048	.015
	.459	.173	.199	.176	.147	.111	.033
	.462	.035	.049	.052	.049	.043	-.034
Main stage	.497	-.003	.034	.033	.022	-.006	-.081
	.512	-.050	.023	.016	-.031	-.056	-.103
	.532	-.092	-.089	-.083	-.090	-.122	-.167
Main stage	.552	-.173	-.163	-.160	-.163	-.196	-.232
	.562	-.265	-.242	-.228	-.231	-.248	-.277
	.568	-.153	-.127	-.112	-.105	-.129	-.154
Main stage	.577	-.122	-.100	-.074	-.081	-.094	-.123
	.597	-.103	-.058	-.059	-.058	-.071	-.100
	.607	-.091	-.062	-.036	-.043	-.060	-.085
Main stage	.617	-.084	-.039	-.037	-.035	-.056	-.077
	.627	-.080	-.031	-.024	-.031	-.044	-.069
	.637	-.076	-.027	-.021	-.027	-.041	-.062
Main stage	.647	-.064	-.020	-.012	-.019	-.033	-.053
	.657	-.052	-.016	-.008	-.015	-.029	-.048
	.677	-.040	-.013	-.004	-.012	-.025	-.043
Main stage	.697	-.053	-.013	-.001	-.010	-.021	-.036
	.717	-.048	-.005	.001	-.006	-.018	-.031
	.727	-.055	-.004	.003	-.004	-.015	-.025
Main stage	.737	-.045	-.003	.003	-.001	-.018	-.027
	.747	-.052	-.009	-.002	-.004	-.015	-.030
	.757	-.051	-.026	-.009	-.005	-.018	-.030
Main stage	.767	-.052	-.009	-.003	-.006	-.020	-.032
	.777	-.052	-.009	-.003	-.006	-.020	-.032
	.787	-.052	-.009	-.003	-.006	-.020	-.032
Main stage	.797	-.052	-.009	-.003	-.006	-.020	-.032
	.807	-.052	-.009	-.003	-.006	-.020	-.032
	.817	-.052	-.009	-.003	-.006	-.020	-.032
Main stage	.827	-.052	-.009	-.003	-.006	-.020	-.032
	.837	-.052	-.009	-.003	-.006	-.020	-.032
	.847	-.052	-.009	-.003	-.006	-.020	-.032
Main stage	.857	-.052	-.009	-.003	-.006	-.020	-.032
	.867	-.052	-.009	-.003	-.006	-.020	-.032
	.877	-.052	-.009	-.003	-.006	-.020	-.032
Main stage	.887	-.052	-.009	-.003	-.006	-.020	-.032
	.897	-.052	-.009	-.003	-.006	-.020	-.032
	.907	-.052	-.009	-.003	-.006	-.020	-.032
Main stage	.917	-.052	-.009	-.003	-.006	-.020	-.032
	.927	-.052	-.009	-.003	-.006	-.020	-.032
	.937	-.052	-.009	-.003	-.006	-.020	-.032
Main stage	.947	-.052	-.009	-.003	-.006	-.020	-.032
	.957	-.052	-.009	-.003	-.006	-.020	-.032
	.967	-.052	-.009	-.003	-.006	-.020	-.032
Main stage	.977	-.052	-.009	-.003	-.006	-.020	-.032
	.987	-.052	-.009	-.003	-.006	-.020	-.032
	.997	-.052	-.009	-.003	-.006	-.020	-.032

TABLE 2.- PRESSURE COEFFICIENTS FOR CONFIGURATION 121 - Continued

(a) $M = 1.00$; $\alpha = -10^\circ$ to 10°

		C_p for $\beta = 0^\circ$						x/l	C_p for $\beta = -30^\circ$					
		$\alpha = -10^\circ$	$\alpha = -5^\circ$	$\alpha = 0^\circ$	$\alpha = 5^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$		$\alpha = -10^\circ$	$\alpha = -5^\circ$	$\alpha = 0^\circ$	$\alpha = 5^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$
Main stage	Nozzle	.583	.498	.406	.355	.321	.264	.338	.456	.365	.322	.280	.219	
		.553	.474	.377	.328	.289	.234	.348	.427	.378	.292	.248	.187	
		.488	.451	.347	.301	.256	.205	.358	.456	.375	.263	.218	.154	
		.412	.361	.315	.266	.221	.169	.378	.427	.378	.263	.218	.154	
		.341	.276	.247	.201	.159	.104	.388	.376	.241	.201	.154	.095	
		.270	.214	.174	.134	.093	.063	.393	.311	.222	.190	.142	.087	
		.534	.558	.586	.596	.616	.638	.399	.240	.202	.165	.109	.057	
		.419	.422	.460	.479	.478	.450	.409	.669	.687	.704	.711	.667	
		.348	.348	.366	.367	.373	.350	.419	.583	.628	.660	.712	.758	
		.285	.266	.244	.217	.193	.168	.429	.467	.540	.600	.712	.758	
Transition Laird	Upper stage	.139	.208	.364	.401	.563	.601	.439	.267	.364	.502	.694	.723	
		.242	.181	.096	.027	.001	.020	.449	.185	.233	.392	.417	.407	
		.169	.137	.114	.087	.084	.091	.459	.223	.212	.166	.109	.028	
		.148	.110	.084	.060	.057	.061	.492	.139	.125	.101	.090	.078	
		.133	.092	.074	.039	.033	.022	.512	.110	.084	.074	.060	.055	
		.127	.083	.064	.024	.012	.002	.532	.106	.066	.053	.040	.031	
		.100	.056	.044	.007	.002	.002	.552	.097	.074	.051	.039	.024	
		.016	.017	.040	.083	.099	.048	.562	.067	.044	.021	.021	.006	
		.203	.258	.319	.339	.370	.381	.568	.001	.026	.078	.104	.079	
		.188	.142	.197	.279	.284	.292	.577	.219	.252	.293	.330	.329	
Main stage	Main stage	.115	.160	.200	.244	.245	.249	.597	.173	.220	.290	.300	.316	
		.106	.154	.166	.165	.196	.191	.607	.142	.139	.153	.156	.155	
		.109	.139	.142	.134	.120	.109	.617	.115	.114	.121	.126	.127	
		.106	.128	.121	.113	.095	.082	.627	.087	.087	.099	.104	.106	
		.081	.096	.069	.064	.042	.060	.637	.055	.055	.070	.083	.088	
		.091	.074	.069	.050	.003	.032	.647	.021	.021	.021	.010	.011	
		.039	.074	.045	.015	.019	.009	.657	.001	.001	.001	.001	.016	
		.014	.031	.012	.015	.019	.010	.677	.040	.042	.042	.054	.058	
		.046	.039	.025	.025	.022	.014	.697	.074	.074	.074	.074	.074	
		.056	.044	.029	.027	.023	.017	.737	.074	.074	.074	.074	.074	

TABLE 1.- PRESSURE COEFFICIENTS FOR CONFIGURATION 121 - Continued

(±) M = 1.00; α = -10° to 10° - Calculated

x/l	C _p for - β = -1°						
	α = -10°	α = -6°	α = -3°	α = 0°	α = 3°	α = 6°	α = 10°
None	.328	.383	.405	.406	.402	.384	.329
Upper stage	.358	.279	.296	.303	.292	.268	.216
	.378	.223	.228	.232	.227	.212	.151
Main stage	.393	.090	.104	.114	.109	.082	.027
	.399	-.580	-.578	-.559	-.569	-.600	-.638
Upper stage	.419	-.464	-.466	-.476	-.481	-.484	-.495
	.439	-.364	-.306	-.276	-.283	-.317	-.376
Transition	.459	.092	.142	.175	.161	.133	.080
	.482	-.011	.059	.095	.084	.063	-.005
Transition	.512	-.042	.020	.053	.045	.024	-.033
	.552	-.082	-.020	.004	.000	-.028	-.091
Main stage	.568	-.432	-.379	-.377	-.388	-.413	-.469
	.587	-.326	-.259	-.249	-.259	-.281	-.338
Main stage	.607	-.268	-.177	-.166	-.174	-.199	-.262
	.627	-.228	-.131	-.121	-.128	-.153	-.216
Main stage	.657	-.157	-.084	-.070	-.080	-.095	-.147
	.697	-.110	-.007	.014	-.042	-.042	-.064
Main stage	.737	-.056	-.003	.025	.021	-.006	-.055
	.777	-.047	-.001	.025	.022	-.005	-.049
Main stage	.785	-.057	-.003	.014	.025	.004	-.038
	.817	-.041	-.003	.018	.024	-.000	-.040
Main stage	.857	-.055	-.014	.003	.007	-.017	-.056
	.897	-.062	-.022	-.007	.001	-.024	-.061

x/l	C _p for - β = 0°						
	α = -10°	α = -6°	α = -3°	α = 0°	α = 3°	α = 6°	α = 10°
None	.466	.403	.384	.365	.334	.295	.222
Upper stage	.376	.371	.355	.332	.301	.262	.190
	.367	.347	.322	.303	.272	.230	.157
Upper stage	.276	.276	.257	.232	.207	.165	.094
	.214	.214	.201	.182	.157	.118	.051
Main stage	.192	-.151	-.128	-.121	-.131	-.150	-.189
	.589	-.586	-.600	-.607	-.621	-.648	-.699
Main stage	.604	-.653	-.668	-.671	-.721	-.740	-.765
	.609	-.516	-.549	-.587	-.651	-.685	-.729
Main stage	.419	-.373	-.418	-.474	-.496	-.518	-.547
	.429	-.306	-.347	-.364	-.380	-.408	-.446
Upper stage	.439	-.273	-.274	-.276	-.283	-.305	-.291
	.449	-.245	-.208	-.152	-.093	-.064	-.063
Upper stage	.459	.123	.166	.168	.155	.109	.044
	.482	.052	.089	.093	.084	.063	.013
Transition	.492	.062	.072	.074	.060	.042	-.002
	.512	.028	.053	.057	.039	.018	-.027
Transition	.532	.016	.032	.037	.021	.003	-.048
	.552	-.001	-.001	-.002	-.015	-.044	-.094
Transition	.562	-.091	-.078	-.078	-.098	-.127	-.174
	.568	-.322	-.293	-.283	-.296	-.321	-.371
Main stage	.577	-.294	-.284	-.284	-.296	-.330	-.381
	.587	-.252	-.246	-.241	-.243	-.275	-.301
Main stage	.597	-.237	-.215	-.208	-.214	-.226	-.249
	.607	-.222	-.191	-.177	-.174	-.184	-.204
Main stage	.617	-.222	-.172	-.142	-.149	-.153	-.173
	.627	-.206	-.160	-.121	-.122	-.126	-.146
Main stage	.637	-.185	-.136	-.102	-.104	-.107	-.124
	.657	-.144	-.099	-.069	-.075	-.072	-.081
Main stage	.677	-.109	-.074	-.046	-.049	-.036	-.056
	.697	-.073	-.048	-.014	-.022	.001	-.020
Main stage	.717	-.029	-.009	.025	.022	.007	-.012
	.777	-.020	.011	.026	.023	.010	-.006
Main stage	.785	-.032	.003	.027	.020	.013	.000
	.817	-.016	.012	.020	.024	.008	-.008
Main stage	.857	-.033	-.005	.011	.009	-.004	-.016
	.877	-.033	-.007	.005	.006	-.006	-.019
Main stage	.897	-.039	-.013	.005	.003	-.008	-.022
	.917	-.048	-.020	.000	-.002	-.012	-.023
Main stage	.957	-.069	-.021	-.003	-.009	-.014	-.029
	.997	-.107	-.091	-.093	-.115	-.132	-.157

TABLE 2.- PRESSURE COEFFICIENTS FOR CONFIGURATION 121 - Concluded

(e) $M = 1.20$; $\alpha = -10^\circ$ to 10° - Concluded

		C_p for - $\beta = -5^\circ$							
		$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$	
Nose	x/l	.328	.256	.299	.311	.316	.317	.296	-.259
		.358	.258	.294	.303	.313	.301	.288	-.254
		.378	.253	.304	.311	.310	.304	.296	-.243
		.393	.198	.249	.285	.279	.285	.254	-.196
		.399	-.329	-.295	-.296	-.264	-.306	-.325	-.363
		.419	-.281	-.253	-.251	-.257	-.261	-.271	-.304
		.439	-.221	-.166	-.153	-.146	-.153	-.171	-.226
		.459	.006	.091	.115	.133	.115	.089	-.001
		.482	-.016	.058	.089	.097	.090	.064	-.009
		.512	-.038	.034	.065	.064	.060	.039	-.023
		.552	-.032	.018	.041	.048	.042	.007	-.039
		.568	-.211	-.191	-.178	-.179	-.183	-.199	-.248
Transition	x/l	.587	-.181	-.150	-.127	-.114	-.126	-.150	-.213
		.607	-.176	-.118	-.094	-.079	-.094	-.118	-.191
		.627	-.162	-.085	-.070	-.062	-.069	-.093	-.159
		.657	-.124	-.053	-.026	-.021	-.028	-.059	-.118
		.697	-.125	-.068	-.037	-.029	-.041	-.060	-.124
		.737	-.106	-.056	-.030	-.028	-.029	-.056	-.110
		.777	-.073	-.043	-.021	-.015	-.020	-.045	-.093
		.785	-.083	-.047	-.023	-.011	-.019	-.042	-.095
		.817	-.071	-.024	-.008	-.009	-.015	-.037	-.083
		.857	-.075	-.027	-.014	-.009	-.028	-.046	-.083
		.897	-.083	-.037	-.015	-.004	-.005	-.023	-.072
		.937	-.087	-.037	-.015	-.004	-.005	-.023	-.072
Main stage	x/l	.338	.374	.357	.313	.283	.244	.186	
		.348	.382	.357	.316	.283	.249	.193	
		.358	.370	.362	.316	.277	.252	.193	
		.378	.363	.357	.310	.285	.257	.188	
		.388	.344	.338	.310	.296	.252	.183	
		.393	.171	.148	.122	.129	.161	.192	
		.399	-.293	-.287	-.289	-.320	-.346	-.368	
		.404	-.367	-.364	-.375	-.399	-.418	-.450	
		.409	-.292	-.304	-.341	-.364	-.391	-.434	
		.419	-.223	-.223	-.254	-.269	-.285	-.323	
		.429	-.167	-.169	-.180	-.204	-.225	-.272	
		.439	-.146	-.133	-.142	-.158	-.174	-.226	
	.449	-.127	-.104	-.107	-.105	-.131	-.168		
	.459	-.095	.118	.120	.125	.086	.042		
	.482	-.033	.077	.082	.097	.066	.018		
	.492	-.033	.087	.087	.081	.076	.004		
	.512	-.030	.066	.076	.064	.052	.012		
	.532	-.030	.064	.063	.059	.044	-.026		
	.552	-.022	.045	.047	.043	-.028	-.001		
	.562	-.006	.018	.020	.011	-.004	-.028		
	.568	-.143	-.137	-.129	-.138	-.148	-.158		
	.577	-.124	-.137	-.129	-.133	-.151	-.169		
	.587	-.118	-.118	-.110	-.111	-.129	-.147		
	.597	-.113	-.107	-.097	-.092	-.107	-.128		
	.607	-.113	-.093	-.089	-.079	-.088	-.107		
	.617	-.116	-.090	-.075	-.068	-.077	-.090		
	.627	-.108	-.088	-.067	-.062	-.069	-.085		
	.637	-.108	-.088	-.066	-.051	-.053	-.069		
	.657	-.091	-.034	-.031	-.020	-.022	-.045		
	.677	-.084	-.040	-.028	-.022	-.027	-.042		
	.697	-.077	-.045	-.024	-.025	-.031	-.039		
	.737	-.082	-.044	-.026	-.025	-.028	-.035		
	.777	-.057	-.034	-.023	-.013	-.021	-.030		
	.785	-.048	-.035	-.017	-.006	-.017	-.024		
	.817	-.052	-.019	-.008	-.014	-.016	-.028		
	.857	-.060	-.014	-.008	-.013	-.021	-.028		
	.877	-.049	-.027	-.006	-.002	-.006	-.019		
	.897	-.061	-.025	-.007	-.001	-.001	-.014		
	.917	-.066	-.028	-.007	-.004	-.007	-.018		
	.957	-.065	-.033	-.012	-.005	-.017	-.032		
	.997	-.056	-.043	-.039	-.032	-.066	-.087		

TABLE 3.- PRESSURE COEFFICIENTS FOR CONFIGURATION 221 - Continued

(a) $M = 0.10$ to 0.95 ; $\alpha = 0^\circ$ - Concluded

		C_p for -					
		$\theta = -60^\circ$					
		$M = 0.10$	$M = 0.70$	$M = 0.75$	$M = 0.85$	$M = 0.95$	
Main stage	x/l	.367	.350	.358	.399	.430	.469
		.377	.752	.264	.308	.345	.394
		.387	.118	.130	.197	.246	.301
		.399	-1.330	-1.342	-1.123	-.969	-.834
		.409	-.331	-.732	-.911	-1.117	-.984
		.419	-.173	-.503	-.632	-1.013	-.901
		.429	-.094	-.100	-.296	-.353	-.684
		.439	-.038	-.008	-.045	-.138	-.528
		.445	.004	.029	.044	.050	-.167
		.459	.142	.070	.063	.134	.081
Flare	x/l	.492	.056	.158	.158	.224	.202
		.492	.007	.029	.055	.083	.148
		.532	-.007	.004	.030	.050	.110
		.552	-.038	-.016	.001	.017	.059
		.562	-.084	-.076	-.093	-.089	-.043
		.568	-.141	-.128	-.176	-.191	-.371
		.577	-.163	-.192	-.205	-.248	-.359
		.587	-.084	-.091	-.121	-.129	-.285
		.597	-.061	-.063	-.085	-.085	-.285
		.607	-.050	-.040	-.060	-.058	-.082
Transition	x/l	.617	-.038	-.026	-.042	-.049	-.044
		.627	-.027	-.022	-.029	-.042	-.037
		.637	-.015	-.017	-.025	-.035	-.031
		.657	-.019	-.002	-.021	-.031	-.024
		.677	-.017	-.014	-.014	-.018	-.015
		.697	-.015	-.002	-.010	-.017	-.015
		.737	-.012	-.006	-.007	-.011	-.014
		.777	-.008	-.011	-.001	-.002	-.009
		.817	-.007	-.011	-.000	-.003	-.013
		.857	-.011	-.006	-.001	-.006	-.011
Nozzle	x/l	.897	-.011	-.004	-.010	-.007	-.007
		.917	-.011	-.006	-.010	-.007	-.007
		.957	-.005	-.004	-.010	-.009	-.013
		.997	-.023	-.009	-.012	-.009	-.013
			-.007	-.016	-.012	-.009	-.014
			-.017	-.023	-.022	-.014	-.018
			-.073	-.083	-.084	-.022	-.025
							-.084
							-.097

		C_p for -					
		$\theta = -90^\circ$					
		$M = 0.10$	$M = 0.70$	$M = 0.75$	$M = 0.85$	$M = 0.95$	
Main stage	x/l	.357	.369	.435	.447	.487	.515
		.377	.182	.261	.268	.315	.358
		.387	.040	.140	.155	.218	.266
		.399	-1.575	-1.506	-1.514	-1.228	-1.054
		.419	-.083	-.062	-.100	-.328	-.404
		.439	-.004	.024	.021	.041	.017
		.459	.142	.175	.166	.158	.198
		.482	.018	.056	.050	.055	.083
		.512	-.015	.015	.004	.001	.017
		.552	-.084	-.063	-.076	-.089	-.085
Transition	x/l	.568	-.197	-.234	-.252	-.365	-.411
		.587	-.061	-.063	-.071	-.089	-.085
		.607	-.038	-.026	-.042	-.049	-.044
		.627	-.015	-.017	-.025	-.035	-.024
		.657	-.019	-.003	-.015	-.021	-.017
		.697	-.015	.000	-.012	-.015	-.016
		.737	-.012	.008	-.004	-.015	-.014
		.785	-.008	.009	-.002	-.013	-.013
		.817	-.008	.009	-.002	-.008	-.013
		.857	-.005	.012	-.003	-.008	-.011
Nozzle	x/l	.897	-.011	.005	-.005	-.009	-.005
							-.012
							-.010
							-.012
							-.007
							-.007
							-.007
							-.007
							-.007
							-.012

TABLE 1.- PRESSURE COEFFICIENTS FOR CONFIGURATION 221 - Continued

(b) $M = 0.60$; $\alpha = -10^\circ$ to 10°

		C_p for $\beta = 0^\circ$						C_p for $\beta = -30^\circ$							
		$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$	$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$
Nozzle	x/l	.635	.551	.485	.420	.357	.290	.206	.367	.429	.379	.320	.262	.201	.128
		.540	.457	.390	.325	.262	.201	.128	.377	.406	.279	.225	.173	.111	.044
Upper stage	x/l	.417	.328	.265	.203	.139	.083	.018	.387	.178	.122	.074	.017	-.035	-.099
		.295	.200	.139	.080	.017	-.035	-.093	.399	-.170	-1.339	-1.326	-1.270	-1.206	-1.253
Transition flare	x/l	-1.351	-1.495	-1.553	-1.528	-1.431	-1.235	-.941	.399	-1.310	-1.365	-1.426	-1.480	-1.537	-1.583
		.404	-.314	-.377	-.432	-.514	-.588	-.663	.404	-.320	-.365	-.426	-.480	-.537	-.583
Main stage	x/l	-.098	-.149	-.171	-.198	-.234	-.285	-.377	.404	-.320	-.365	-.426	-.480	-.537	-.583
		-.012	-.046	-.063	-.072	-.080	-.080	-.080	.419	-.109	-.166	-.251	-.309	-.380	-.451
Nozzle	x/l	.026	.000	-.017	-.021	-.023	-.023	-.012	.429	.005	-.012	-.023	-.023	-.023	-.029
		.067	.034	.023	.013	.011	.011	.017	.439	.039	-.017	.013	-.011	-.011	-.005
Upper stage	x/l	.107	.079	.062	.059	.051	.051	.051	.449	.096	-.017	.065	.057	.051	.045
		.255	.216	.193	.167	.148	.1.1	.108	.459	.244	.193	.176	.153	.142	.119
Transition flare	x/l	.482	.435	.402	.442	.423	.411	.401	.482	.107	.062	.042	.028	.011	.005
		.592	.532	.462	.425	.400	.400	.412	.492	.090	.040	.025	.006	.000	.000
Main stage	x/l	.067	.022	.000	-.015	-.029	-.046	-.058	.512	.034	.017	.008	.012	-.029	-.041
		.552	.423	-.046	-.062	-.075	-.081	-.087	.532	.050	-.006	-.021	-.035	-.052	-.064
Transition flare	x/l	.562	-.105	-.122	-.137	-.139	-.139	-.140	.552	-.023	-.046	-.062	-.075	-.087	-.105
		.568	-.104	-.122	-.137	-.139	-.139	-.140	.562	-.110	-.128	-.137	-.145	-.151	-.151
Main stage	x/l	.577	-.030	-.069	-.090	-.092	-.092	-.081	.577	-.173	-.184	-.182	-.184	-.173	-.156
		.587	-.001	-.052	-.056	-.063	-.058	-.052	.587	-.081	-.086	-.090	-.092	-.092	-.093
Transition flare	x/l	.597	.005	-.040	-.044	-.046	-.040	-.035	.597	-.030	-.058	-.061	-.063	-.063	-.064
		.607	.016	-.029	-.033	-.040	-.035	-.023	.607	-.035	-.040	-.040	-.040	-.040	-.035
Main stage	x/l	.617	.016	-.023	-.027	-.029	-.029	-.018	.617	-.029	-.029	-.027	-.029	-.029	-.035
		.627	.021	-.023	-.027	-.023	-.023	-.018	.627	-.023	-.029	-.027	-.029	-.029	-.029
Transition flare	x/l	.637	.027	-.021	-.021	-.023	-.023	-.006	.637	-.023	-.023	-.023	-.023	-.023	-.029
		.657	.036	-.004	-.002	-.004	-.008	-.000	.657	-.012	-.012	-.002	-.023	-.023	-.023
Main stage	x/l	.677	.036	-.004	-.000	-.006	-.006	-.002	.677	-.006	-.010	-.002	-.008	-.015	-.022
		.697	.040	-.000	-.004	-.000	-.002	-.002	.697	-.004	-.004	-.002	-.004	-.010	-.020
Transition flare	x/l	.737	.040	-.000	-.002	-.004	-.002	-.000	.737	-.002	-.000	-.004	-.002	-.008	-.018
		.777	.042	-.006	-.006	-.000	-.000	-.005	.777	-.008	-.004	-.004	-.000	-.006	-.018
Main stage	x/l	.785	.047	-.008	-.008	-.002	-.004	-.005	.785	-.008	-.004	-.004	-.000	-.006	-.018
		.817	.045	-.009	-.006	-.003	-.003	-.009	.817	-.004	-.004	-.002	-.002	-.006	-.014
Transition flare	x/l	.857	.038	-.004	-.003	-.000	-.002	-.009	.857	-.007	-.006	-.005	-.002	-.004	-.017
		.877	.039	-.004	-.003	-.000	-.002	-.002	.877	-.000	-.000	-.002	-.003	-.008	-.020
Main stage	x/l	.897	.034	-.001	-.000	-.004	-.005	-.003	.897	-.002	-.001	-.001	-.003	-.010	-.020
		.917	.008	-.002	-.002	-.004	-.005	-.003	.917	-.002	-.001	-.001	-.004	-.013	-.022
Transition flare	x/l	.957	-.008	-.014	-.014	-.013	-.014	-.014	.957	-.008	-.004	-.001	-.004	-.016	-.025
		.997	-.087	-.077	-.077	-.064	-.065	-.063	.997	-.077	-.064	-.064	-.074	-.090	-.112

TABLE 5.- PRESSURE COEFFICIENTS FOR CONFIGURATION 221 - Continued

(b) $M = 0.60$; $\alpha = -10^\circ$ to 10° - Concluded

		C_p for $\beta = -60^\circ$						C_p for $\beta = -50^\circ$							
		$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$	$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$
Main stage	x/l	.367	.367	.345	.320	.279	.234	.145	.357	.328	.390	.412	.401	.362	.284
		.377	.284	.251	.225	.184	.134	.061	.377	.155	.195	.217	.225	.178	.128
		.387	.133	.111	.080	.045	.022	-.075	.387	.022	.067	.078	.097	.045	.005
		.399	-1.397	-1.484	-1.541	-1.633	-1.662	-1.559	.399	-1.645	-1.651	-1.553	-1.599	-1.662	-1.709
		.404	-.320	-.337	-.364	-.417	-.451	-.480							
		.419	-.172	-.166	-.169	-.188	-.211	-.232							
		.429	-.104	-.080	-.078	-.080	-.097	-.137							
		.439	-.058	-.029	-.021	-.029	-.046	-.080							
		.449	-.022	-.045	-.057	-.051	-.034	-.006							
		.459	.153	.170	.167	.153	.136	.091							
Transition Flare	x/l	.482	.028	.039	.042	.023	.006	-.041	.459	.096	.148	.165	.165	.142	.085
		.492	.011	.022	.019	.006	-.012	-.053	.482	-.036	.011	.034	.042	.006	-.041
		.512	-.030	-.017	-.021	-.012	-.029	-.070							
		.532	-.082	-.076	-.068	-.081	-.104	-.145							
		.552	-.146	-.139	-.137	-.145	-.162	-.192							
		.568	-.220	-.202	-.184	-.184	-.196	-.231							
		.577	-.093	-.086	-.084	-.092	-.109	-.127							
		.587	-.081	-.063	-.061	-.069	-.081	-.104							
		.597	-.070	-.046	-.046	-.038	-.046	-.081							
		.607	-.070	-.035	-.033	-.040	-.052	-.075							
Noose	x/l	.617	-.064	-.029	-.027	-.035	-.046	-.064	.552	-.134	-.093	-.070	-.068	-.099	-.145
		.627	-.058	-.041	-.029	-.029	-.040	-.058	.568	-.317	-.259	-.230	-.217	-.242	-.323
		.637	-.053	-.023	-.021	-.023	-.035	-.052	.587	-.127	-.092	-.069	-.061	-.069	-.139
		.657	-.051	-.023	-.015	-.004	-.029	-.047	.607	-.104	-.064	-.040	-.033	-.040	-.110
		.677	-.041	-.010	-.001	-.010	-.024	-.040	.627	-.093	-.046	-.029	-.021	-.029	-.098
		.697	-.032	-.004	.002	.006	-.019	-.033	.657	-.082	-.037	-.017	-.002	-.013	-.083
		.737	-.041	-.006	.006	.006	-.019	-.033	.697	-.076	-.035	-.014	.000	-.013	-.079
		.777	-.037	-.016	.002	.008	-.015	-.023	.737	-.068	-.029	-.008	-.004	-.031	-.07
		.785	-.041	-.004	.008	.008	-.013	-.023	.777	-.066	-.029	-.006	-.008	-.027	-.070
		.817	-.038	.000	.006	.006	-.010	-.019	.785	-.070	-.029	-.006	-.006	-.027	-.066
	.857	-.042	-.017	-.004	.002	-.013	-.022	.817	-.061	-.020	-.001	.008	-.020	-.059	
	.877	-.042	-.019	-.004	.002	-.013	-.022	.857	-.067	-.026	-.006	.002	-.025	-.065	
	.897	-.045	-.019	-.006	.004	-.015	-.023	.897	-.065	-.028	-.009	-.001	-.029	-.068	
	.917	-.053	-.026	-.010	.004	-.019	-.027								
	.957	-.057	-.034	-.018	-.012	-.019	-.037								
	.997	-.123	-.097	-.078	-.066	-.077	-.116								

TABLE 5.- PRESSURE COEFFICIENTS FOR CONFIGURATION 221 - Continued

(a) $M = 1.00$; $\alpha = -10^\circ$ to 10°

x/l	C_p for $\gamma = 0^\circ$						x/l	C_p for $\gamma = -30^\circ$						
	$\alpha = -10^\circ$	$\alpha = -5^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$		$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$
	Nose	.814	.730	.610	.547	.488		.412	.367	.686	.626	.580	.523	.470
Upper stage	.731	.650	.529	.470	.407	.331	.377	.612	.551	.502	.455	.396	.339	.278
	.637	.560	.445	.388	.328	.255	.387	.499	.447	.401	.354	.306	.255	.185
	.544	.471	.340	.306	.249	.179	.399	.775	.788	.793	.805	.814	.832	.852
Transition	.719	.753	.777	.786	.792	.803	.399	.404	.404	.404	.404	.404	.404	.404
	.721	.791	.869	.896	.918	.944	.409	.854	.854	.854	.854	.854	.854	.854
	.544	.726	.778	.829	.869	.904	.419	.859	.859	.859	.859	.859	.859	.859
Main stage	.303	.435	.592	.665	.720	.770	.429	.318	.435	.510	.577	.634	.686	.739
	.208	.313	.443	.497	.546	.607	.439	.236	.388	.446	.494	.537	.586	.634
	.166	.243	.327	.345	.265	.230	.449	.205	.305	.336	.354	.371	.388	.404
Flare	.157	.229	.174	.079	.046	.015	.449	.178	.212	.217	.165	.089	.053	.018
	.193	.159	.148	.097	.045	.009	.459	.172	.159	.151	.130	.106	.079	.048
	.129	.096	.091	.082	.075	.065	.482	1.4	.093	.093	.082	.072	.064	.057
Nose	.123	.089	.051	.039	.027	.022	.512	.096	.096	.060	.048	.036	.028	.021
	.096	.059	.039	.021	.006	.008	.532	.090	.071	.045	.036	.018	.000	.000
	.052	.027	.006	.019	.040	.061	.552	.063	.046	.018	.006	.019	.043	.079
Transition	.005	.024	.081	.108	.130	.147	.566	.004	.024	.056	.081	.108	.139	.175
	.207	.251	.311	.332	.345	.343	.577	.253	.270	.290	.302	.320	.335	.343
	.189	.239	.283	.283	.289	.288	.587	.219	.248	.277	.283	.289	.305	.312
Main stage	.146	.193	.234	.240	.252	.251	.597	.173	.205	.228	.237	.249	.262	.265
	.115	.159	.200	.203	.209	.199	.607	.115	.134	.151	.157	.157	.166	.168
	.106	.147	.169	.163	.166	.152	.617	.146	.162	.173	.173	.169	.172	.168
Transition	.109	.137	.145	.135	.136	.125	.637	.142	.150	.154	.123	.111	.120	.122
	.109	.119	.120	.111	.108	.103	.647	.118	.111	.111	.102	.095	.102	.109
	.084	.097	.099	.089	.092	.088	.657	.099	.089	.085	.075	.071	.081	.090
Main stage	.069	.077	.074	.068	.071	.064	.677	.062	.061	.065	.065	.052	.059	.071
	.047	.061	.068	.055	.064	.049	.697	.052	.057	.061	.058	.051	.057	.053
	.029	.058	.058	.047	.047	.024	.737	.029	.027	.028	.028	.034	.034	.034
Transition	.051	.037	.026	.034	.017	.017	.777	.048	.046	.043	.042	.046	.046	.046
	.066	.049	.039	.039	.030	.025	.785	.042	.045	.042	.040	.039	.039	.039
	.072	.054	.047	.047	.039	.029	.817	.042	.037	.034	.031	.023	.015	.009
Main stage	.068	.036	.031	.024	.028	.013	.857	.023	.017	.016	.016	.016	.016	.016
	.050	.028	.016	.013	.010	.008	.877	.020	.015	.012	.010	.006	.003	.002
	.050	.018	.013	.009	.010	.003	.897	.015	.007	.005	.003	.003	.003	.003
Transition	.040	.010	.006	.004	.003	.006	.917	.012	.007	.003	.003	.000	.000	.000
	.029	.020	.010	.004	.003	.003	.957	.002	.003	.003	.003	.003	.003	.003
	.040	.010	.006	.004	.003	.006	.997	.004	.005	.005	.005	.005	.005	.005

TABLE 3.- PRESSURE COEFFICIENTS FOR CONFIGURATION 221 - Continued

(a) $M = 1.0$; $\alpha = -10^\circ$ to 10° - Concluded

		C_p for $\beta = -90^\circ$						
		$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$
Main stage	x/l	.529	.587	.606	.601	.589	.559	.495
	Rose	.357	.377	.383	.455	.431	.407	.349
Transition Lare	x/l	.387	.294	.359	.381	.345	.321	.272
	Rose	.399	.799	.777	.796	.786	.795	.812
Upper stage	x/l	.419	.538	.583	.595	.594	.589	.575
	Rose	.439	.407	.342	.336	.348	.372	.416
Transition Lare	x/l	.459	.035	.127	.133	.127	.100	.028
	Rose	.482	.035	.072	.087	.076	.048	.042
Main stage	x/l	.512	.054	.036	.046	.039	.015	.042
	Rose	.552	.088	.007	.003	.006	.031	.092
Transition Lare	x/l	.568	.432	.379	.373	.391	.415	.475
	Rose	.587	.327	.276	.249	.258	.292	.346
Main stage	x/l	.607	.269	.182	.169	.175	.209	.272
	Rose	.627	.235	.136	.120	.126	.163	.229
Transition Lare	x/l	.657	.168	.088	.076	.082	.117	.173
	Rose	.697	.117	.066	.057	.040	.094	.127
Main stage	x/l	.737	.046	.019	.028	.030	.003	.045
	Rose	.777	.039	.010	.040	.029	.006	.038
Transition Lare	x/l	.785	.050	.005	.040	.032	.010	.029
	Rose	.817	.036	.007	.027	.023	.007	.033
Main stage	x/l	.857	.054	.011	.016	.006	.012	.052
	Rose	.897	.065	.001	.006	.001	.024	.061
Transition Lare	x/l	.917	.050	.000	.000	.004	.015	.024
	Rose	.957	.052	.020	.006	.010	.024	.033
Main stage	x/l	.997	.110	.092	.104	.114	.141	.159
	Rose	.570	.569	.550	.520	.482	.440	.355
Transition Lare	x/l	.502	.495	.475	.446	.411	.377	.293
	Rose	.610	.603	.589	.557	.527	.500	.406
Upper stage	x/l	.704	.702	.709	.722	.755	.768	.791
	Rose	.806	.825	.845	.863	.881	.896	.919
Transition Lare	x/l	.841	.841	.844	.841	.820	.851	.883
	Rose	.939	.937	.945	.946	.949	.956	.960
Main stage	x/l	.939	.937	.945	.946	.949	.956	.960
	Rose	.939	.937	.945	.946	.949	.956	.960
Transition Lare	x/l	.949	.949	.949	.949	.949	.949	.949
	Rose	.949	.949	.949	.949	.949	.949	.949
Main stage	x/l	.949	.949	.949	.949	.949	.949	.949
	Rose	.949	.949	.949	.949	.949	.949	.949

TABLE 3.- PRESSURE COEFFICIENTS FOR CONFIGURATION 221 - Concretes

(e) $M = 1.20$; $\alpha = -10^\circ$ to 10° - Concluded

		C_p for -								
		$\beta = -5^\circ$	$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$	
Main stage	x/l	.657	.607	.654	.673	.670	.635	.638	.573	
	Transition	.657	.607	.654	.673	.670	.635	.638	.573	
		.697	.637	.684	.703	.699	.664	.667	.603	.538
	Upper stage	.737	.677	.724	.743	.739	.704	.707	.643	.578
		.777	.717	.764	.783	.779	.744	.747	.683	.618
	Rooftop	.817	.757	.804	.823	.819	.784	.787	.723	.658
		.857	.797	.844	.863	.859	.824	.827	.763	.698
	Rooftop	.897	.837	.884	.903	.899	.864	.867	.803	.738
		.937	.877	.924	.943	.939	.904	.907	.843	.778
	Transition	.977	.917	.964	.983	.979	.944	.947	.883	.818
1.017		.957	1.004	1.023	1.019	.984	.987	.923	.858	
Main stage	.454	.404	.451	.470	.466	.431	.434	.370	.305	
	.494	.444	.491	.510	.506	.471	.474	.410	.345	
Transition	.534	.484	.531	.550	.546	.511	.514	.450	.385	
	.574	.524	.571	.590	.586	.551	.554	.490	.425	
Upper stage	.614	.564	.611	.630	.626	.591	.594	.530	.465	
	.654	.604	.651	.670	.666	.631	.634	.570	.505	
Rooftop	.694	.644	.691	.710	.706	.671	.674	.610	.545	
	.734	.684	.731	.750	.746	.711	.714	.650	.585	
Rooftop	.774	.724	.771	.790	.786	.751	.754	.690	.625	
	.814	.764	.811	.830	.826	.791	.794	.730	.665	
Transition	.854	.804	.851	.870	.866	.831	.834	.770	.705	
	.894	.844	.891	.910	.906	.871	.874	.810	.745	
Main stage	.934	.884	.931	.950	.946	.911	.914	.850	.785	
	.974	.924	.971	.990	.986	.951	.954	.890	.825	
Rooftop	1.014	.964	1.011	1.030	1.026	.991	.994	.930	.865	
	1.054	1.004	1.051	1.070	1.066	1.031	1.034	.970	.905	
Transition	1.094	1.044	1.091	1.110	1.106	1.071	1.074	1.010	.945	
	1.134	1.084	1.131	1.150	1.146	1.111	1.114	1.050	.985	
Upper stage	1.174	1.124	1.171	1.190	1.186	1.151	1.154	1.090	1.025	
	1.214	1.164	1.211	1.230	1.226	1.191	1.194	1.130	1.065	
Rooftop	1.254	1.204	1.251	1.270	1.266	1.231	1.234	1.170	1.105	
	1.294	1.244	1.291	1.310	1.306	1.271	1.274	1.210	1.145	
Transition	1.334	1.284	1.331	1.350	1.346	1.311	1.314	1.250	1.185	
	1.374	1.324	1.371	1.390	1.386	1.351	1.354	1.290	1.225	
Main stage	1.414	1.364	1.411	1.430	1.426	1.391	1.394	1.330	1.265	
	1.454	1.404	1.451	1.470	1.466	1.431	1.434	1.370	1.305	
Rooftop	1.494	1.444	1.491	1.510	1.506	1.471	1.474	1.410	1.345	
	1.534	1.484	1.531	1.550	1.546	1.511	1.514	1.450	1.385	
Transition	1.574	1.524	1.571	1.590	1.586	1.551	1.554	1.490	1.425	
	1.614	1.564	1.611	1.630	1.626	1.591	1.594	1.530	1.465	
Upper stage	1.654	1.604	1.651	1.670	1.666	1.631	1.634	1.570	1.505	
	1.694	1.644	1.691	1.710	1.706	1.671	1.674	1.610	1.545	
Rooftop	1.734	1.684	1.731	1.750	1.746	1.711	1.714	1.650	1.585	
	1.774	1.724	1.771	1.790	1.786	1.751	1.754	1.690	1.625	
Transition	1.814	1.764	1.811	1.830	1.826	1.791	1.794	1.730	1.665	
	1.854	1.804	1.851	1.870	1.866	1.831	1.834	1.770	1.705	
Main stage	1.894	1.844	1.891	1.910	1.906	1.871	1.874	1.810	1.745	
	1.934	1.884	1.931	1.950	1.946	1.911	1.914	1.850	1.785	
Rooftop	1.974	1.924	1.971	1.990	1.986	1.951	1.954	1.890	1.825	
	2.014	1.964	2.011	2.030	2.026	1.991	1.994	1.930	1.865	
Transition	2.054	2.004	2.051	2.070	2.066	2.031	2.034	1.970	1.905	
	2.094	2.044	2.091	2.110	2.106	2.071	2.074	2.010	1.945	
Upper stage	2.134	2.084	2.131	2.150	2.146	2.111	2.114	2.050	1.985	
	2.174	2.124	2.171	2.190	2.186	2.151	2.154	2.090	2.025	
Rooftop	2.214	2.164	2.211	2.230	2.226	2.191	2.194	2.130	2.065	
	2.254	2.204	2.251	2.270	2.266	2.231	2.234	2.170	2.105	
Transition	2.294	2.244	2.291	2.310	2.306	2.271	2.274	2.210	2.145	
	2.334	2.284	2.331	2.350	2.346	2.311	2.314	2.250	2.185	
Main stage	2.374	2.324	2.371	2.390	2.386	2.351	2.354	2.290	2.225	
	2.414	2.364	2.411	2.430	2.426	2.391	2.394	2.330	2.265	
Rooftop	2.454	2.404	2.451	2.470	2.466	2.431	2.434	2.370	2.305	
	2.494	2.444	2.491	2.510	2.506	2.471	2.474	2.410	2.345	
Transition	2.534	2.484	2.531	2.550	2.546	2.511	2.514	2.450	2.385	
	2.574	2.524	2.571	2.590	2.586	2.551	2.554	2.490	2.425	
Upper stage	2.614	2.564	2.611	2.630	2.626	2.591	2.594	2.530	2.465	
	2.654	2.604	2.651	2.670	2.666	2.631	2.634	2.570	2.505	
Rooftop	2.694	2.644	2.691	2.710	2.706	2.671	2.674	2.610	2.545	
	2.734	2.684	2.731	2.750	2.746	2.711	2.714	2.650	2.585	
Transition	2.774	2.724	2.771	2.790	2.786	2.751	2.754	2.690	2.625	
	2.814	2.764	2.811	2.830	2.826	2.791	2.794	2.730	2.665	
Main stage	2.854	2.804	2.851	2.870	2.866	2.831	2.834	2.770	2.705	
	2.894	2.844	2.891	2.910	2.906	2.871	2.874	2.810	2.745	
Rooftop	2.934	2.884	2.931	2.950	2.946	2.911	2.914	2.850	2.785	
	2.974	2.924	2.971	2.990	2.986	2.951	2.954	2.890	2.825	
Transition	3.014	2.964	3.011	3.030	3.026	2.991	2.994	2.930	2.865	
	3.054	2.904	3.051	3.070	3.066	3.031	3.034	2.970	2.905	
Upper stage	3.094	2.944	3.091	3.110	3.106	3.071	3.074	3.010	2.945	
	3.134	2.984	3.131	3.150	3.146	3.111	3.114	3.050	2.985	
Rooftop	3.174	2.924	3.171	3.190	3.186	3.151	3.154	3.090	2.925	
	3.214	2.964	3.211	3.230	3.226	3.191	3.194	3.130	2.965	
Transition	3.254	2.904	3.251	3.270	3.266	3.231	3.234	3.170	2.905	
	3.294	2.944	3.291	3.310	3.306	3.271	3.274	3.210	2.945	
Main stage	3.334	2.984	3.331	3.350	3.346	3.311	3.314	3.250	2.985	
	3.374	3.024	3.371	3.390	3.386	3.351	3.354	3.290	2.925	
Rooftop	3.414	3.064	3.411	3.430	3.426	3.391	3.394	3.330	2.965	
	3.454	3.104	3.451	3.470	3.466	3.431	3.434	3.370	2.905	
Transition	3.494	3.144	3.491	3.510	3.506	3.471	3.474	3.410	2.945	
	3.534	3.184	3.531	3.550	3.546	3.511	3.514	3.450	2.985	
Upper stage	3.574	3.224	3.571	3.590	3.586	3.551	3.554	3.490	2.925	
	3.614	3.264	3.611	3.630	3.626	3.591	3.594	3.530	2.965	
Rooftop	3.654	3.304	3.651	3.670	3.666	3.631	3.634	3.570	2.905	
	3.694	3.344	3.691	3.710	3.706	3.671	3.674	3.610	2.945	
Transition	3.734	3.384	3.731	3.750	3.746	3.711	3.714	3.650	2.985	
	3.774	3.424	3.771	3.790	3.786	3.751	3.754	3.690	2.925	
Main stage	3.814	3.464	3.811	3.830	3.826	3.791	3.794	3.730	2.965	
	3.854	3.504	3.851	3.870	3.866	3.831	3.834	3.770	2.905	
Rooftop	3.894	3.544	3.891	3.910	3.906	3.871	3.874	3.810	2.945	
	3.934	3.584	3.931	3.950	3.946	3.911	3.914	3.850	2.985	
Transition	3.974	3.624	3.971	3.990	3.986	3.951	3.954	3.890	2.925	
	4.014	3.664	4.011	4.030	4.026	3.991	3.994	3.930	2.965	
Upper stage	4.054	3.704	4.051	4.070	4.066	4.031	4.034	3.970	2.905	
	4.094	3.744	4.091	4.110	4.106	4.071	4.074	4.010	2.945	
Rooftop	4.134	3.784	4.131	4.150	4.146	4.111	4.114	4.050	2.985	
	4.174	3.824	4.171	4.190	4.186	4.151	4.154	4.090	2.925	
Transition	4.214	3.864	4.211	4.230	4.226	4.191	4.194	4.130	2.965	
	4.254	3.904	4.251	4.270	4.266	4.231	4.234	4.170	2.905	
Main stage	4.294	3.944	4.291	4.310	4.306	4.271	4.274	4.210	2.945	
	4.334	3.984	4.331	4.350	4.346	4.311	4.314	4.250	2.985	
Rooftop	4.374	4.024	4.371	4.390	4.386	4.351	4.354	4.290	2.925	
	4.414	4.064	4.411	4.430	4.426	4.391	4.394	4.330	2.965	
Transition	4.454	4.104	4.451	4.470	4.466	4.431	4.434			

TABLE 4.- PRESSURE COEFFICIENTS FOR CONFIGURATION 321

(a) $M = 0.40$ to 0.95 ; $\alpha = 0^\circ$

		C_p for -																																			
		$\beta = 0^\circ$																																			
		$M = 0.40$	$M = 0.70$	$M = 0.85$	$M = 0.90$	$M = 0.95$																															
Nose	x/l	.371	.381	.391	.399	.404	.409	.419	.429	.439	.449	.459	.482	.492	.512	.532	.552	.562	.568	.577	.587	.597	.607	.617	.627	.637	.657	.677	.737	.777	.785	.817	.877	.897	.957	.997	
		.492	.338	.173	-1.404	-1.409	-1.172	-0.60	-0.04	.030	.075	.176	.053	.053	.041	.019	-0.038	-0.095	-0.129	-0.129	-0.049	-0.015	-0.004	-0.004	.008	.008	.019	.019	.023	.027	.028	.028	.028	.025	.024		
Upper stage	x/l	.371	.381	.391	.399	.404	.409	.419	.429	.439	.449	.459	.482	.492	.512	.532	.552	.562	.568	.577	.587	.597	.607	.617	.627	.637	.657	.677	.737	.777	.785	.817	.877	.897	.957	.997	
		.575	.421	.209	-1.042	-0.844	-0.669	-0.319	-0.094	.010	.068	.151	.064	.043	.018	-0.007	-0.057	-0.129	-0.208	-0.208	-0.095	-0.061	-0.044	-0.032	-0.028	-0.019	-0.007	-0.005	-0.002	.003	.008	.007	.004	.004	.001		
Transition flare	x/l	.371	.381	.391	.399	.404	.409	.419	.429	.439	.449	.459	.482	.492	.512	.532	.552	.562	.568	.577	.587	.597	.607	.617	.627	.637	.657	.677	.737	.777	.785	.817	.877	.897	.957	.997	
		.627	.480	.291	-0.835	-0.686	-0.443	-0.221	-0.042	.022	.080	.145	.054	.036	.013	-0.010	-0.061	-0.126	-0.203	-0.203	-0.093	-0.060	-0.047	-0.033	-0.028	-0.023	-0.014	-0.007	-0.002	.003	.008	.007	.005	.004	.002	.002	
Main stage	x/l	.371	.381	.391	.399	.404	.409	.419	.429	.439	.449	.459	.482	.492	.512	.532	.552	.562	.568	.577	.587	.597	.607	.617	.627	.637	.657	.677	.737	.777	.785	.817	.877	.897	.957	.997	
		.575	.421	.209	-1.042	-0.844	-0.669	-0.319	-0.094	.010	.068	.151	.064	.043	.018	-0.007	-0.057	-0.129	-0.208	-0.208	-0.095	-0.061	-0.044	-0.032	-0.028	-0.019	-0.007	-0.005	-0.002	.003	.008	.007	.004	.004	.001		
		C_p for -																																			
		$\beta = -30^\circ$																																			
		$M = 0.40$	$M = 0.70$	$M = 0.85$	$M = 0.90$	$M = 0.95$																															
Nose	x/l	.371	.381	.391	.399	.404	.409	.419	.429	.439	.449	.459	.482	.492	.512	.532	.552	.562	.568	.577	.587	.597	.607	.617	.627	.637	.657	.677	.737	.777	.785	.817	.877	.897	.957	.997	
		.492	.288	.085	-1.483	-1.409	-1.172	-0.60	-0.04	.030	.075	.176	.053	.053	.030	.008	-0.038	-0.095	-0.129	-0.129	-0.049	-0.026	-0.004	-0.004	.008	.008	.019	.015	.023	.027	.027	.027	.025	.022	.013		
Upper stage	x/l	.371	.381	.391	.399	.404	.409	.419	.429	.439	.449	.459	.482	.492	.512	.532	.552	.562	.568	.577	.587	.597	.607	.617	.627	.637	.657	.677	.737	.777	.785	.817	.877	.897	.957	.997	
		.548	.358	.169	-0.961	-0.813	-0.644	-0.229	-0.032	.027	.072	.154	.054	.036	.013	-0.014	-0.061	-0.126	-0.185	-0.185	-0.093	-0.060	-0.037	-0.033	-0.028	-0.023	-0.019	-0.008	-0.002	.006	.007	.005	.001	.003	.003		
Transition flare	x/l	.371	.381	.391	.399	.404	.409	.419	.429	.439	.449	.459	.482	.492	.512	.532	.552	.562	.568	.577	.587	.597	.607	.617	.627	.637	.657	.677	.737	.777	.785	.817	.877	.897	.957	.997	
		.623	.456	.288	-0.861	-0.781	-0.626	-0.504	-0.335	-0.167	-0.045	.069	.090	.069	.026	-0.010	-0.068	-0.129	-0.148	-0.148	-0.071	-0.043	-0.032	-0.038	-0.031	-0.028	-0.020	-0.017	-0.008	-0.002	.006	.006	.006	.006	.006	.006	
Main stage	x/l	.371	.381	.391	.399	.404	.409	.419	.429	.439	.449	.459	.482	.492	.512	.532	.552	.562	.568	.577	.587	.597	.607	.617	.627	.637	.657	.677	.737	.777	.785	.817	.877	.897	.957	.997	
		.575	.421	.209	-1.042	-0.844	-0.669	-0.319	-0.094	.010	.068	.151	.064	.043	.018	-0.007	-0.057	-0.129	-0.208	-0.208	-0.095	-0.061	-0.044	-0.032	-0.028	-0.019	-0.007	-0.005	-0.002	.003	.008	.007	.004	.004	.001		

TABLE 4.- PRESSURE COEFFICIENTS FOR CONFIGURATION 321 - Continued

(a) $M = 0.40$ to 0.95 ; $\alpha = 0^\circ$ - Concluded

		C_p for -					
		$\gamma = -60^\circ$					
		$M = 0.40$	$M = 0.70$	$M = 0.85$	$M = 0.90$	$M = 0.95$	
Nose	x/l	.481	.548	.571	.616	.652	.690
		.316	.387	.413	.466	.504	.553
Upper stage	x/l	.085	.173	.209	.284	.333	.388
		-1.119	-1.012	-0.903	-0.821	-0.809	-0.719
Transition	x/l	.375	.436	.498	.643	.676	-1.085
		.184	.640	.656	.618	.656	-1.002
Main stage	x/l	.060	.297	.415	.515	.555	.779
		.004	.042	.131	.353	.410	.590
Transition	x/l	.030	.036	.014	.185	.252	.216
		.075	.068	.072	.053	.100	.007
Main stage	x/l	.165	.145	.143	.058	.028	.138
		.053	.054	.064	.090	.098	.153
Transition	x/l	.041	.036	.043	.069	.081	.118
		.030	.013	.018	.026	.038	.064
Main stage	x/l	.008	.014	.011	.013	.006	.023
		.038	.065	.066	.075	.074	.047
Transition	x/l	.129	.126	.129	.148	.160	.145
		.095	.093	.091	.107	.115	.347
Main stage	x/l	.026	.042	.041	.075	.081	.208
		.004	.042	.040	.049	.053	.044
Transition	x/l	.008	.033	.032	.038	.043	.021
		.028	.028	.028	.035	.036	.018
Main stage	x/l	.008	.023	.019	.028	.030	.018
		.019	.019	.015	.020	.023	.018
Transition	x/l	.015	.008	.008	.017	.017	.016
		.019	.004	.005	.013	.014	.015
Main stage	x/l	.023	.000	.002	.010	.010	.014
		.023	.003	.001	.008	.008	.014
Transition	x/l	.027	.004	.005	.004	.005	.010
		.028	.006	.006	.005	.005	.011
Main stage	x/l	.028	.005	.008	.001	.001	.008
		.025	.001	.003	.006	.007	.013
Transition	x/l	.024	.000	.002	.006	.007	.014
		.024	.000	.001	.008	.008	.015
Main stage	x/l	.021	.005	.003	.012	.013	.020
		.013	.014	.011	.020	.021	.077
Transition	x/l	.039	.067	.067	.081	.086	.098
		.039	.067	.067	.081	.086	.098

		C_p for -					
		$\gamma = -90^\circ$					
		$M = 0.40$	$M = 0.70$	$M = 0.85$	$M = 0.90$	$M = 0.95$	
Nose	x/l	.481	.543	.567	.616	.649	.690
		.391	.485	.567	.616	.649	.690
Upper stage	x/l	.399	.702	.655	.622	.622	.800
		.404	.736	.698	.643	.676	-1.085
Transition	x/l	.409	.184	.640	.656	.618	.656
		.419	.060	.297	.415	.515	.555
Main stage	x/l	.429	.004	.042	.131	.353	.410
		.439	.030	.036	.014	.185	.252
Transition	x/l	.449	.075	.068	.072	.053	.100
		.459	.165	.145	.143	.058	.028
Main stage	x/l	.482	.053	.054	.064	.090	.098
		.492	.041	.036	.043	.069	.081
Transition	x/l	.512	.030	.013	.018	.026	.038
		.532	.008	.014	.011	.013	.006
Main stage	x/l	.552	.038	.065	.075	.074	.047
		.562	.095	.126	.129	.148	.160
Transition	x/l	.568	.129	.185	.212	.244	.366
		.577	.049	.093	.107	.115	.347
Main stage	x/l	.587	.026	.065	.075	.081	.208
		.597	.004	.042	.049	.053	.044
Transition	x/l	.607	.008	.033	.032	.038	.021
		.617	.008	.028	.028	.035	.018
Main stage	x/l	.627	.008	.023	.019	.028	.018
		.637	.019	.019	.015	.020	.018
Transition	x/l	.657	.015	.008	.008	.017	.016
		.677	.019	.004	.005	.013	.015
Main stage	x/l	.697	.023	.000	.002	.010	.014
		.737	.023	.003	.001	.008	.014
Transition	x/l	.777	.027	.004	.005	.004	.005
		.785	.028	.006	.006	.005	.011
Main stage	x/l	.817	.028	.005	.008	.001	.008
		.857	.025	.001	.003	.006	.013
Transition	x/l	.877	.024	.000	.002	.006	.014
		.897	.024	.000	.001	.008	.015
Main stage	x/l	.917	.021	.005	.003	.012	.020
		.957	.013	.014	.011	.020	.077
Transition	x/l	.997	.039	.067	.067	.081	.098
		.997	.039	.067	.067	.081	.098

TABLE 2. -- PRESSURE COEFFICIENTS FOR CONFIGURATION 321 - Continued

(b) $M = 0.60$; $\alpha = -10^\circ$ to 10°

		C_p for $\beta = 0^\circ$						
		$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$
None	x/l	.735	.655	.584	.523	.445	.381	.279
		.584	.493	.428	.366	.289	.230	.139
None		.344	.248	.177	.126	.060	.018	-.046
		-1.273	-1.344	-1.325	-1.204	-1.163	-.993	-.722
Upper stage		.409	.649	.785	.819	.830	.753	.629
		.419	.192	.287	.408	.510	.570	.623
Upper stage		.429	.655	.700	.682	.614	.419	.314
		.439	.209	.024	.019	-.041	-.056	-.097
Upper stage		.449	.016	.061	.015	-.001	.001	-.006
		.459	.279	.061	.157	.039	.036	.034
Transition		.482	.129	.082	.049	.016	.093	.068
		.492	.106	.055	.049	.017	.013	.008
Transition		.512	.095	.033	.026	.004	.001	-.017
		.532	.061	.021	.018	-.007	-.010	-.046
Transition		.552	.021	.007	.008	-.042	-.045	-.058
		.562	-.065	-.054	-.054	-.082	-.074	-.087
Transition		.568	-.111	-.129	-.118	-.135	-.126	-.133
		.577	-.036	-.166	-.181	-.180	-.154	-.144
Transition		.587	-.072	-.082	-.083	-.093	-.085	-.087
		.597	-.044	-.053	-.054	-.063	-.056	-.058
Transition		.607	-.009	-.030	-.031	-.042	-.035	-.046
		.617	.015	-.025	-.025	-.036	-.027	-.029
Transition		.627	.026	-.019	-.019	-.030	-.022	-.023
		.637	.026	-.013	-.014	-.024	-.016	-.017
Transition		.657	.028	-.001	-.002	-.019	-.004	-.010
		.677	.031	.003	.000	.015	.004	.010
Transition		.697	.031	.009	.004	.013	.002	.008
		.717	.031	.007	.000	.011	.002	.010
Transition		.737	.035	.007	.004	.009	.002	.008
		.757	.039	.001	.006	.005	.005	.006
Transition		.785	.039	.003	.008	.004	.003	.004
		.817	.039	.003	.005	.007	.001	.011
Transition		.857	.035	-.002	.005	.007	.001	.010
		.877	.031	-.005	.002	.010	.004	.014
Transition		.897	.031	-.005	.002	.010	.004	.014

		C_p for $\beta = -30^\circ$						
		$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$
None	x/l	.371	.702	.633	.573	.517	.451	.386
		.381	.504	.432	.372	.319	.255	.116
None		.391	.305	.231	.171	.121	.060	-.052
		.399	-1.429	-1.361	-1.331	-1.354	-1.093	-.809
None		.404	-.379	-.655	-.750	-.739	-.836	-.720
		.409	-.127	-.226	-.339	-.379	-.561	-.593
None		.419	-.053	-.066	-.076	-.088	-.139	-.274
		.429	-.007	-.020	-.024	-.019	-.036	-.086
None		.439	.027	.014	.010	.015	.001	-.011
		.449	.095	.077	.067	.066	.044	.036
None		.459	.232	.207	.181	.157	.118	.104
		.482	.101	.082	.055	.049	.021	.000
None		.492	.067	.054	.033	.038	.004	-.023
		.512	.047	.037	.021	.019	-.022	-.046
None		.532	.044	.008	-.007	.015	-.019	-.046
		.552	-.002	-.026	-.054	-.008	-.042	-.070
None		.562	-.083	-.119	-.135	-.118	-.082	-.104
		.568	-.140	-.170	-.180	-.174	-.160	-.161
None		.577	-.059	-.084	-.088	-.083	-.085	-.098
		.587	-.036	-.055	-.059	-.054	-.062	-.069
None		.597	.019	.032	.036	.037	.047	.046
		.607	.013	.032	.030	.031	.042	.040
None		.617	.013	.026	.025	.025	.036	.040
		.627	.007	.020	.025	.030	.022	.029
None		.637	.002	.015	.019	.014	.024	.029
		.657	.001	.011	.019	.016	.016	.029
None		.677	.012	.001	.009	.002	.019	.025
		.697	.004	.007	.009	.002	.017	.021
None		.717	.008	.003	.013	.002	.015	.023
		.737	.014	.003	.009	.002	.015	.023
None		.757	.014	.003	.005	.006	.004	.023
		.785	.014	.001	.005	.006	.007	.021
None		.817	.013	.006	.002	.006	.007	.020
		.837	.007	.001	.006	.004	.004	.020
None		.857	.007	.001	.006	.004	.008	.025
		.877	.004	.003	.008	.001	.009	.025
None		.897	.004	.004	.009	.001	.013	.029
		.917	.004	.004	.009	.001	.013	.029
None		.937	-.012	-.016	-.019	-.010	-.023	.041
		.957	-.091	-.077	-.071	-.063	-.080	-.115

TABLE 2. -- PRESSURE COEFFICIENTS FOR CONFIGURATION 321 - Continued

(b) $M = 0.60$; $\alpha = -10^\circ$ to 10° - Concluded

		C_p for $\beta = -60^\circ$						C_p for $\beta = -70^\circ$									
		$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$	$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$		
Nose	x/l	.371	.428	.488	.512	.517	.501	.476	.402	.371	.428	.488	.512	.517	.501	.476	.402
		.381	.404	.378	.350	.305	.264	.173	.050	.391	.471	.508	.512	.426	.310	.102	.050
		.399	.333	.292	.198	.121	.046	-.029	-.144	.399	.399	-1.071	-1.055	-.932	-.718	-.756	-.930
Upper stage	x/l	.409	.242	.289	.448	.304	.713	.732	.554	.419	.173	.112	.122	-.082	.150	.130	.154
		.419	.139	.104	.105	.139	.113	.143	.109	.439	.087	.020	.010	.032	.010	.016	.086
		.429	.076	.030	.019	.036	.050	.109	.109	.459	.084	.128	.146	.157	.130	.127	.058
Transition	x/l	.449	.010	.037	.050	.041	.039	.024	.017	.512	.083	.032	.007	.015	.013	.028	.081
		.459	.156	.152	.152	.118	.107	.080	.080	.552	.135	.090	.077	.060	.082	.097	.151
		.482	.021	.037	.038	.049	.021	.007	.046	.568	.324	.257	.226	.204	.232	.270	.334
Main stage	x/l	.512	.002	.002	.032	.004	.028	.075	.099	.587	.134	.090	.071	.060	.076	.085	.144
		.532	.030	.021	.015	.019	.028	.057	.099	.607	.105	.061	.042	.031	.047	.056	.115
		.552	.088	.073	.071	.082	.097	.145	.192	.627	.099	.055	.030	.019	.036	.045	.104
		.562	.152	.141	.141	.118	.140	.149	.192	.657	.090	.044	.026	.002	.022	.037	.092
		.568	.221	.199	.186	.189	.189	.231	.233	.697	.084	.040	.021	.002	.020	.031	.085
		.577	.123	.101	.088	.083	.093	.102	.133	.737	.078	.036	.017	.002	.015	.027	.079
		.587	.099	.078	.065	.054	.070	.074	.110	.777	.075	.032	.015	.006	.017	.024	.073
		.597	.082	.061	.048	.037	.053	.056	.087	.785	.077	.034	.013	.006	.013	.024	.071
		.607	.071	.049	.036	.031	.042	.045	.075	.817	.068	.023	.007	.006	.006	.019	.066
		.617	.071	.049	.030	.025	.030	.027	.058	.857	.072	.027	.011	.005	.012	.023	.069
		.627	.065	.044	.030	.019	.030	.027	.058	.897	.072	.027	.011	.001	.015	.026	.072
		.637	.059	.038	.025	.014	.030	.027	.058								
		.657	.059	.032	.025	.002	.022	.024	.050								
		.677	.048	.025	.019	.000	.019	.021	.044								
		.697	.036	.019	.013	.002	.015	.018	.035								
	.737	.050	.022	.015	.002	.015	.016	.033									
	.777	.046	.020	.011	.006	.011	.010	.029									
	.785	.050	.022	.013	.006	.011	.010	.027									
	.817	.044	.014	.005	.009	.006	.007	.025									
	.857	.051	.020	.011	.004	.010	.010	.026									
	.877	.049	.020	.011	.003	.010	.010	.027									
	.897	.050	.020	.012	.002	.012	.013	.028									
	.917	.059	.028	.017	.003	.017	.016	.032									
	.957	.064	.034	.025	.010	.025	.026	.042									
	.997	.128	.096	.085	.064	.082	.092	.120									

TABLE 4.- PRESSURE COEFFICIENTS FOR CONFIGURATION 3E1 - Continued

(c) $M = 0.80$; $\alpha = -10^\circ$ to 10°

		C_p for -						
		$\beta = -30^\circ$						
		$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$
Main stage	x/z	.775	.709	.655	.592	.539	.461	.367
	Noise	.371	.381	.399	.404	.419	.429	.439
Transition	x/z	.595	.527	.477	.420	.366	.300	.215
	Noise	.381	.399	.419	.429	.439	.449	.459
Upper stage	x/z	.415	.347	.299	.247	.194	.138	.083
	Noise	.399	.404	.419	.429	.439	.449	.459
Flare	x/z	-1.427	-1.173	-.849	-.665	-.524	-.434	-.354
	Noise	.409	.419	.429	.439	.449	.459	.469
Main stage	x/z	.775	.709	.655	.592	.539	.461	.367
	Noise	.371	.381	.399	.404	.419	.429	.439
Transition	x/z	.595	.527	.477	.420	.366	.300	.215
	Noise	.381	.399	.419	.429	.439	.449	.459
Upper stage	x/z	.415	.347	.299	.247	.194	.138	.083
	Noise	.399	.404	.419	.429	.439	.449	.459
Flare	x/z	-1.427	-1.173	-.849	-.665	-.524	-.434	-.354
	Noise	.409	.419	.429	.439	.449	.459	.469
Main stage	x/z	.775	.709	.655	.592	.539	.461	.367
	Noise	.371	.381	.399	.404	.419	.429	.439
Transition	x/z	.595	.527	.477	.420	.366	.300	.215
	Noise	.381	.399	.419	.429	.439	.449	.459
Upper stage	x/z	.415	.347	.299	.247	.194	.138	.083
	Noise	.399	.404	.419	.429	.439	.449	.459
Flare	x/z	-1.427	-1.173	-.849	-.665	-.524	-.434	-.354
	Noise	.409	.419	.429	.439	.449	.459	.469
Main stage	x/z	.775	.709	.655	.592	.539	.461	.367
	Noise	.371	.381	.399	.404	.419	.429	.439
Transition	x/z	.595	.527	.477	.420	.366	.300	.215
	Noise	.381	.399	.419	.429	.439	.449	.459
Upper stage	x/z	.415	.347	.299	.247	.194	.138	.083
	Noise	.399	.404	.419	.429	.439	.449	.459
Flare	x/z	-1.427	-1.173	-.849	-.665	-.524	-.434	-.354
	Noise	.409	.419	.429	.439	.449	.459	.469

TABLE 21.- PRESSURE COEFFICIENTS FOR CONFIGURATION 321 - Continued

(c) $M = 0.80$; $\alpha = -10^\circ$ to 10° - Concluded

		C_p for -							
		$\beta = -50^\circ$							
		$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$	
Rose	x/l	.371	.505	.567	.592	.592	.584	.555	.487
		.391	.194	.229	.250	.247	.235	.217	.168
Upper stage	x/l	.399	-.801	-.753	-.720	-.641	-.689	-.746	-.782
		.404	-.854	-.780	-.743	-.669	-.746	-.766	-.804
Upper stage	x/l	.409	-.612	-.718	-.677	-.665	-.609	-.596	-.604
		.419	-.797	-.372	-.424	-.474	-.454	-.439	-.485
Upper stage	x/l	.429	-.109	-.142	-.193	-.262	-.281	-.300	-.339
		.439	-.063	-.023	-.028	-.062	-.094	-.135	-.177
Upper stage	x/l	.449	-.009	-.039	-.053	-.038	-.006	-.035	-.078
		.459	.140	.157	.141	.122	.083	.049	.026
Upper stage	x/l	.459	.022	.058	.068	.065	.060	.019	-.040
		.492	.006	.035	.045	.047	.037	.003	-.055
Transition	x/l	.512	-.009	.012	.018	.007	.002	.031	-.075
		.532	-.032	-.015	-.013	-.020	-.029	-.043	-.106
Transition	x/l	.552	-.099	-.077	-.075	-.078	-.079	-.117	-.157
		.562	-.181	-.159	-.153	-.152	-.142	-.180	-.223
Transition	x/l	.568	-.288	-.255	-.222	-.206	-.195	-.225	-.268
		.577	-.148	-.124	-.102	-.101	-.098	-.120	-.148
Transition	x/l	.587	-.117	-.093	-.075	-.074	-.071	-.093	-.121
		.597	-.098	-.069	-.051	-.051	-.052	-.066	-.094
Transition	x/l	.607	-.086	-.058	-.040	-.043	-.040	-.058	-.082
		.617	-.083	-.054	-.032	-.035	-.036	-.055	-.074
Main stage	x/l	.627	-.079	-.050	-.028	-.031	-.029	-.047	-.074
		.637	-.071	-.042	-.020	-.023	-.021	-.039	-.063
Main stage	x/l	.657	-.066	-.034	-.018	-.018	-.017	-.034	-.055
		.677	-.054	-.027	-.013	-.014	-.014	-.031	-.051
Main stage	x/l	.697	-.041	-.019	-.009	-.011	-.011	-.028	-.046
		.737	-.054	-.025	-.009	-.009	-.008	-.022	-.039
Main stage	x/l	.777	-.050	-.019	-.005	-.005	-.005	-.018	-.034
		.785	-.054	-.025	-.007	-.005	-.003	-.017	-.033
Main stage	x/l	.817	-.047	-.017	-.002	-.002	-.000	-.016	-.030
		.857	-.053	-.024	-.008	-.007	-.005	-.020	-.033
Main stage	x/l	.877	-.052	-.024	-.008	-.008	-.005	-.021	-.034
		.897	-.055	-.024	-.007	-.009	-.006	-.021	-.035
Main stage	x/l	.917	-.060	-.032	-.015	-.013	-.011	-.025	-.040
		.957	-.066	-.036	-.021	-.021	-.020	-.035	-.050
Main stage	x/l	.997	-.134	-.103	-.085	-.081	-.082	-.105	-.129

TABLE 4.- PRESSURE COEFFICIENTS FOR CONFIGURATION 321 - Continued

x/t		C _p for -						
		β = 0°						
		α = -10°	α = -6°	α = -3°	α = 0°	α = 3°	α = 6°	
Nose	.371	.942	.867	.807	.747	.677	.610	.518
	.381	.811	.733	.670	.616	.551	.482	.399
	.391	.641	.563	.506	.455	.399	.341	.268
	.404	.667	.686	.702	.715	.730	.745	.766
	.409	.821	.904	.948	.985	1.018	1.042	1.035
	.419	.607	.733	.811	.875	.930	.972	.907
	.429	.330	.489	.582	.667	.743	.810	.802
	.439	.326	.443	.526	.599	.667	.729	.716
	.449	.274	.363	.422	.471	.510	.549	.534
	.459	.174	.230	.252	.272	.291	.310	.328
Upper stage	.459	.165	.133	.123	.108	.066	.014	.126
	.459	.195	.133	.096	.087	.078	.075	.039
	.482	.128	.106	.075	.066	.060	.056	.048
	.492	.110	.087	.075	.066	.060	.056	.024
	.512	.113	.081	.065	.054	.042	.032	.007
	.532	.119	.054	.029	.008	.024	.008	.007
	.552	.097	.078	.051	.038	.024	.008	.062
	.562	.009	.009	.028	.008	.019	.042	.152
	.568	.188	.238	.253	.278	.297	.334	.330
	.577	.141	.161	.186	.217	.229	.235	.225
Transition	.587	.117	.108	.125	.143	.155	.176	.176
	.597	.108	.148	.165	.186	.195	.192	.114
	.607	.108	.139	.155	.174	.184	.192	.139
	.617	.108	.124	.143	.161	.174	.184	.114
	.627	.108	.124	.143	.161	.174	.184	.114
	.637	.108	.124	.143	.161	.174	.184	.114
	.647	.108	.124	.143	.161	.174	.184	.114
	.657	.108	.124	.143	.161	.174	.184	.114
	.667	.108	.124	.143	.161	.174	.184	.114
	.677	.108	.124	.143	.161	.174	.184	.114
Main stage	.687	.108	.124	.143	.161	.174	.184	.114
	.697	.108	.124	.143	.161	.174	.184	.114
	.707	.108	.124	.143	.161	.174	.184	.114
	.717	.108	.124	.143	.161	.174	.184	.114
	.727	.108	.124	.143	.161	.174	.184	.114
	.737	.108	.124	.143	.161	.174	.184	.114
	.747	.108	.124	.143	.161	.174	.184	.114
	.757	.108	.124	.143	.161	.174	.184	.114
	.767	.108	.124	.143	.161	.174	.184	.114
	.777	.108	.124	.143	.161	.174	.184	.114

x/t		C _p for -					
		β = -30°					
		α = -10°	α = -6°	α = -3°	α = 0°	α = 3°	α = 6°
Nose	.371	.910	.852	.795	.744	.680	.616
	.381	.758	.700	.647	.598	.544	.487
	.391	.606	.548	.500	.452	.408	.347
	.404	.877	.893	.906	.915	.918	.927
	.409	.863	.908	.948	.985	1.018	1.071
	.419	.354	.404	.423	.432	.433	.433
	.429	.253	.361	.432	.505	.557	.608
	.439	.213	.288	.334	.377	.401	.428
	.449	.187	.230	.263	.294	.312	.333
	.459	.133	.136	.129	.111	.069	.001
Upper stage	.459	.094	.096	.096	.087	.078	.053
	.459	.082	.078	.075	.066	.059	.026
	.482	.088	.072	.059	.050	.039	.005
	.492	.052	.066	.050	.038	.021	.042
	.512	.067	.066	.054	.038	.019	.042
	.532	.000	.042	.028	.023	.008	.019
	.552	.285	.269	.285	.303	.324	.351
	.562	.252	.252	.269	.282	.284	.285
	.568	.218	.218	.223	.235	.241	.244
	.577	.172	.207	.223	.223	.223	.223
Transition	.587	.117	.136	.149	.164	.171	.158
	.597	.144	.144	.164	.164	.164	.158
	.607	.144	.144	.164	.164	.164	.158
	.617	.144	.144	.164	.164	.164	.158
	.627	.144	.144	.164	.164	.164	.158
	.637	.144	.144	.164	.164	.164	.158
	.647	.144	.144	.164	.164	.164	.158
	.657	.144	.144	.164	.164	.164	.158
	.667	.144	.144	.164	.164	.164	.158
	.677	.144	.144	.164	.164	.164	.158
Main stage	.687	.144	.144	.164	.164	.164	.158
	.697	.144	.144	.164	.164	.164	.158
	.707	.144	.144	.164	.164	.164	.158
	.717	.144	.144	.164	.164	.164	.158
	.727	.144	.144	.164	.164	.164	.158
	.737	.144	.144	.164	.164	.164	.158
	.747	.144	.144	.164	.164	.164	.158
	.757	.144	.144	.164	.164	.164	.158
	.767	.144	.144	.164	.164	.164	.158
	.777	.144	.144	.164	.164	.164	.158

TABLE 4.- PRESSURE COEFFICIENTS FOR CONFIGURATION 321 - Continued

(d) $M = 1.00$; $\alpha = -10^\circ$ to 10° - Concluded

x/l	C_p for $\beta = -60^\circ$						C_p for $\beta = -90^\circ$					
	$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$	$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$
	371	.790	.792	.768	.735	.698	.551	.653	.715	.735	.727	.702
381	.665	.658	.637	.601	.566	.520	.371	.375	.375	.377	.370	.378
391	.507	.500	.476	.452	.420	.377	.391	.438	.452	.444	.425	.378
399	-.555	-.566	-.588	-.603	-.622	-.643	.399	-.680	-.684	-.680	-.665	-.667
404	-.885	-.917	-.936	-.957	-.979	-1.032						
409	-.742	-.801	-.841	-.899	-.927	-.962						
419	-.497	-.584	-.631	-.670	-.704	-.719	.419	-.639	-.649	-.661	-.655	-.632
429	-.363	-.419	-.460	-.499	-.538	-.569						
439	-.314	-.333	-.350	-.374	-.398	-.404	.439	-.395	-.380	-.386	-.404	-.428
449	-.281	-.275	-.249	-.181	-.135	-.133						
459	.064	.085	.105	.102	.057	.017						
482	-.003	.060	.081	.087	.078	.047	.459	.069	.084	.085	.063	-.007
492	-.009	.048	.065	.066	.040	.035	.482	.033	.075	.078	.044	-.069
512	.006	.042	.050	.050	.038	.014						
532	.006	.030	.038	.038	.021	.004	.512	.009	.041	.042	.017	-.050
552	-.031	-.004	-.002	-.001	-.019	-.045						
562	.076	.069	.066	.079	.103	.128	.552	-.025	-.001	-.004	-.029	-.097
568	.323	.296	.288	.288	.300	.325						
577	.299	.284	.282	.282	.290	.308	.568	-.392	-.377	-.386	-.411	-.468
587	.255	.244	.239	.242	.247	.272						
597	.237	.216	.202	.201	.204	.220	.587	-.278	-.251	-.253	-.285	-.342
607	.228	.192	.174	.164	.164	.180						
617	.228	.173	.152	.134	.133	.152	.607	-.201	-.174	-.167	-.198	-.274
627	.209	.158	.134	.112	.112	.131						
637	.178	.133	.109	.094	.093	.112	.627	-.158	-.126	-.118	-.152	-.213
657	.148	.101	.083	.068	.062	.088						
677	.114	.082	.070	.049	.045	.054	.657	-.109	-.084	-.073	-.107	-.165
697	.080	.063	.057	.030	.027	.021						
737	.010	.022	.030	.044	.040	.023	.697	-.068	-.061	-.068	-.063	-.086
777	-.008	.025	.040	.046	.044	.002	.737	.011	.028	.038	.013	-.033
785	-.022	.019	.039	.048	.046	.026	.777	.013	.037	.046	.013	-.034
817	-.012	.019	.032	.029	.020	.015	.785	.008	.035	.044	.017	-.028
857	-.034	.001	.014	.013	.007	.001	.817	.008	.030	.020	.007	-.039
877	-.037	.006	.009	.010	.007	.002	.857	.011	.011	.006	-.011	-.057
897	-.040	.011	.004	.010	.006	.005						
917	-.051	.019	.004	.006	.003	.010	.897	-.022	.001	.003	-.020	-.062
957	-.050	.019	.006	.002	.004	.018						
997	-.110	.031	-.090	-.096	-.109	-.133						

TABLE 4.- PRESSURE COEFFICIENTS FOR CONFIGURATION 321 - Concluded

(e) $M = 1.20$; $\alpha = -10^\circ$ to 10° - Concluded

		C_p for $\beta = -60^\circ$						C_p for $\beta = -50^\circ$								
		$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$	$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$	
		x/l							x/l							
None	None	.371	.922	.918	.897	.868	.832	.777	.691	.371	.784	.843	.865	.858	.832	.774
		.381	.811	.798	.778	.748	.717	.668	.588	.391	.564	.610	.624	.617	.599	.551
		.399	.673	.658	.650	.624	.593	.554	.484	.399	-.336	-.330	-.324	-.304	-.300	-.312
		.404	.240	.253	.280	.288	.301	.314	.347							
		.409	-.563	-.585	-.600	-.616	-.626	-.645	-.670							
		.419	-.438	-.492	-.526	-.559	-.583	-.601	-.621							
		.429	-.286	-.338	-.374	-.404	-.428	-.444	-.452							
		.439	-.183	-.226	-.260	-.293	-.325	-.346	-.376							
		.449	-.153	-.172	-.195	-.217	-.241	-.264	-.308							
		.459	-.131	-.134	-.143	-.154	-.154	-.202	-.276							
Upper stage	Upper stage	.482	.078	.078	.084	.079	.055	.032	.026							
		.492	.007	.051	.076	.087	.082	.056	.010							
		.512	-.007	.051	.076	.076	.074	.048	.010							
		.532	.010	.056	.071	.065	.053	.032	.012							
		.552	.021	.056	.060	.060	.044	.021	.023							
		.562	.021	.043	.044	.041	.026	.002	.032							
		.568	.007	.016	.019	.006	.007	.028	.062							
		.577	-.141	-.135	-.128	-.128	-.134	-.157	-.199							
		.587	-.144	-.135	-.126	-.126	-.128	-.144	-.223							
		.597	-.124	-.121	-.106	-.106	-.106	-.125	-.188							
Transition flare	Transition flare	.597	-.113	-.102	-.093	-.087	-.103	-.121	-.160							
		.607	-.116	-.094	-.084	-.076	-.084	-.102	-.136							
		.617	-.116	-.091	-.071	-.065	-.073	-.086	-.114							
		.627	-.122	-.085	-.063	-.060	-.065	-.080	-.100							
		.637	-.111	-.064	-.052	-.049	-.051	-.064	-.078							
		.657	-.089	-.034	-.031	-.019	-.026	-.044	-.069							
		.677	-.081	-.039	-.028	-.021	-.030	-.047	-.066							
		.697	-.073	-.044	-.025	-.024	-.034	-.039	-.064							
		.717	-.041	-.044	-.025	-.025	-.024	-.043	-.050							
		.737	-.051	-.035	-.023	-.014	-.022	-.029	-.044							
Main stage	Main stage	.785	-.047	-.034	-.017	-.009	-.017	-.024	-.043							
		.817	-.051	-.023	-.009	-.014	-.016	-.029	-.044							
		.857	-.059	-.015	-.013	-.013	-.020	-.029	-.044							
		.877	-.048	-.027	-.005	-.003	-.006	-.020	-.038							
		.897	-.061	-.028	-.008	-.001	-.002	-.014	-.029							
		.917	-.065	-.031	-.015	-.005	-.008	-.018	-.026							
		.957	-.065	-.035	-.013	-.014	-.018	-.017	-.030							
		.997	-.056	-.046	-.040	-.054	-.069	-.089	-.100							

TABLE 5.- PRESSURE COEFFICIENTS FOR CONFIGURATION 122

(a) $M = 0.40$ to 0.95 ; $\alpha = 0^\circ$

x/l		C_p for -					
		$\phi = 0^\circ$					
		M = 0.40	M = 0.70	M = 0.85	M = 0.90	M = 0.95	
Nose	.392	.420	.535	.607	.785	.837	.892
	.402	.227	.251	.261	.275	.294	.320
	.412	.182	.219	.224	.243	.264	.292
	.432	.149	.179	.179	.204	.228	.254
	.442	.060	.075	.084	.116	.144	.178
	.447	-.041	-.034	-.023	-.031	.071	.118
	.453	.168	.165	.142	.142	.056	.058
	.458	.357	.986	.887	.840	.660	.554
	.463	.222	.316	.507	.729	.728	.814
	.473	.109	.140	.158	.370	.186	.545
Upper stage	.483	.027	.017	.015	.053	.025	-.037
	.493	.061	.063	.065	.093	.134	.114
	.503	.129	.132	.132	.162	.198	.233
	.513	.265	.283	.288	.302	.324	.343
	.525	.118	.150	.157	.179	.211	.287
	.535	.061	.072	.069	.089	.120	.185
	.545	.016	.012	.011	.035	.063	.127
	.555	.065	.077	.079	.048	.005	.056
	.565	.307	.509	.434	.361	.287	.192
	.568	.419	.584	.664	.930	.810	.684
Transition Flare	.577	.121	.160	.172	.183	.652	.566
	.587	.076	.095	.100	.088	.181	.478
	.597	.053	.062	.070	.066	.036	.390
	.607	.030	.044	.053	.052	.022	.269
	.617	.018	.034	.040	.041	.026	.060
	.627	-.018	.025	.032	.037	.022	.016
	.637	.007	.016	.019	.026	.019	.019
	.657	.003	.009	.015	.018	.015	.007
	.677	.003	.008	.013	.015	.016	.001
	.697	.005	.005	.007	.012	.016	.001
Main stage	.737	.005	.002	.006	.010	.014	.010
	.777	.009	.000	.002	.006	.010	.005
	.785	.012	.008	.003	.001	.004	.005
	.817	.014	.007	.002	.001	.006	.007
	.857	.011	.004	.001	.004	.009	.011
	.877	.011	.005	.000	.004	.008	.011
	.897	.009	.001	.003	.007	.011	.014

x/l		C_p for -				
		$\phi = -30^\circ$				
		M = 0.40	M = 0.70	M = 0.85	M = 0.90	M = 0.95
Nose	.392	.215	.246	.245	.268	.314
	.402	.182	.206	.212	.233	.279
	.412	.149	.174	.179	.201	.251
	.432	.060	.071	.076	.112	.138
	.442	.053	.034	.027	.031	.071
	.447	.168	.165	.147	.056	.001
	.453	.903	1.075	1.219	1.280	.989
	.458	.211	.320	.457	.827	.912
	.463	.098	.131	.170	.378	.720
	.473	.018	.034	.036	.051	.162
Upper stage	.483	.027	.017	.019	.057	.056
	.493	.061	.063	.065	.097	.137
	.503	.129	.136	.141	.169	.240
	.513	.276	.293	.292	.317	.352
	.525	.129	.150	.153	.176	.284
	.535	.061	.067	.069	.089	.120
	.545	.005	.003	.002	.021	.111
	.555	.065	.095	.096	.067	.040
	.565	.341	.428	.455	.372	.205
	.568	.373	.509	.614	.926	.684
Transition Flare	.577	.121	.160	.172	.180	.579
	.587	.076	.095	.104	.092	.478
	.597	.041	.048	.053	.048	.305
	.607	.030	.044	.044	.052	.253
	.617	.018	.034	.040	.041	.054
	.627	.018	.025	.032	.037	.001
	.637	.007	.016	.023	.026	.016
	.657	.005	.002	.017	.020	.017
	.677	.005	.002	.006	.010	.011
	.697	.005	.005	.009	.013	.002
Main stage	.737	.005	.000	.005	.008	.009
	.777	.012	.006	.001	.002	.006
	.785	.014	.008	.003	.001	.005
	.817	.014	.008	.002	.001	.007
	.857	.011	.002	.002	.005	.017
	.877	.008	.001	.004	.006	.013
	.897	.008	.000	.004	.007	.015
	.957	.001	.011	.015	.019	.027
	.997	.053	.064	.071	.074	.095

TABLE 5.- PRESSURE COEFFICIENTS FOR CONFIGURATION 122 - Continued

(a) M = 0.40 to 0.95; $\alpha = 0^\circ$ - Concluded

		C_p for -				
		$\beta = -50^\circ$				
x/l	None	M = 0.40	M = 0.70	M = 0.85	M = 0.90	M = 0.95
		.392	.215	.246	.245	.268
.402	.182	.206	.208	.229	.248	.276
.412	.149	.165	.171	.194	.214	.244
.432	.049	.066	.072	.102	.134	.177
.442	-.053	-.044	-.036	.024	.068	.115
.447	-.076	-.067	-.078	-.078	-.088	-.100
.453	-.811	-1.187	-1.207	-.957	-.818	-.708
.458	-.200	-.269	-.402	-1.027	-.939	-.817
.463	-.096	-.122	-.128	-.331	-.793	-.697
.473	-.018	-.039	-.036	-.012	-.101	-.558
.483	.027	.017	.015	.046	.076	-.015
.493	.073	.067	.065	.093	.134	.137
.503	.129	.136	.137	.165	.198	.240
.513	.287	.302	.300	.335	.358	.356
.525	.118	.141	.140	.165	.198	.268
.535	.050	.067	.069	.089	.120	.185
.545	.005	.003	.002	.021	.052	.111
.555	-.088	-.105	-.109	-.074	-.026	.040
.565	-.341	-.424	-.451	-.347	-.265	-.186
.568	-.362	-.491	-.584	-.415	-.296	-.671
.577	-.121	-.151	-.163	.165	-.676	-.579
.587	-.076	-.095	-.104	.092	-.174	-.478
.597	-.041	-.057	-.066	.063	-.029	-.384
.607	-.030	-.044	-.049	.052	-.022	-.256
.617	-.018	-.034	-.040	.041	-.026	-.051
.627	-.018	-.025	-.032	.037	-.026	.001
.637	-.007	-.016	-.023	.026	-.026	.016
.657	-.007	-.012	-.016	.020	-.020	.017
.677	-.001	-.007	-.011	.015	-.017	.008
.697	.005	-.002	-.006	.010	-.014	-.001
.737	.005	.000	-.005	.008	-.012	-.009
.777	.009	.005	.000	.003	-.007	-.007
.785	.009	.005	.001	-.003	-.007	-.008
.817	.014	.007	.002	.000	-.005	-.006
.857	.011	.003	-.002	-.005	-.009	-.012
.877	.011	.003	-.002	-.005	-.010	-.013
.897	.009	.002	-.004	-.007	-.012	-.015
.917	.005	-.003	-.008	-.011	-.016	-.019
.957	-.004	-.010	-.015	-.019	-.024	-.026
.997	-.054	-.066	-.072	-.077	-.087	-.098

		C_p for -				
		$\beta = -50^\circ$				
x/l	None	M = 0.40	M = 0.70	M = 0.85	M = 0.90	M = 0.95
		.382	.249	.291	.294	.314
.392	-.891	.246	.331	.505	.574	.633
.412	.149	.165	.171	.194	.214	.244
.432	.049	.066	.068	.102	.134	.172
.447	-.202	-.198	-.181	-.081	-.022	.033
.453	-.811	-1.299	-1.339	-1.034	-.887	-.774
.473	-.018	-.034	-.036	.007	-.094	-.555
.493	.061	.063	.061	.090	.131	.137
.513	.287	.306	.304	.339	.365	.362
.535	.050	.067	.069	.089	.120	.185
.565	-.341	-.438	-.459	-.358	-.275	-.195
.568	-.396	-.565	-.673	-.933	-.813	-.690
.587	-.076	-.099	-.104	-.092	-.177	-.488
.607	-.030	-.044	-.049	-.052	-.022	-.253
.627	-.018	-.025	-.032	-.034	-.026	.004
.657	-.007	-.012	-.017	-.020	-.020	.016
.697	.001	-.005	-.010	-.013	-.017	-.004
.737	.005	.000	-.005	-.008	-.012	-.008
.777	.009	.005	-.002	-.004	-.009	-.008
.785	.009	.003	-.000	-.004	-.009	-.008
.817	.014	.009	-.004	-.004	-.009	-.004
.857	.011	.003	-.001	-.004	-.009	-.012
.897	.008	.001	-.004	-.007	-.012	-.015

TABLE 5.- PRESSURE COEFFICIENTS FOR CONFIGURATION 122 - Continued

(b) $M = 0.60$; $\alpha = -10^\circ$ to 10°

x/l	C_p for $\beta = 0^\circ$					
	$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$
	$\alpha = 10^\circ$	$\alpha = 6^\circ$	$\alpha = 3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$
None	.392	.374	.313	.277	.224	.144
	.402	.334	.279	.237	.190	.105
	.412	.295	.245	.203	.156	.071
	.432	.199	.138	.102	.054	-.026
	.442	.092	.031	-.005	-.054	-.131
	.447	-.045	-.108	-.146	-.194	-.260
	.453	-.066	-.128	-.166	-.214	-.288
	.458	-.079	-.141	-.179	-.224	-.299
	.463	-.092	-.154	-.190	-.233	-.306
	.483	-.101	-.166	-.201	-.241	-.313
Upper stage	.483	.036	.026	.012	.015	.009
	.493	.076	.066	.058	.055	.049
	.503	.157	.127	.127	.125	.113
	.513	.250	.200	.200	.199	.181
	.525	.202	.169	.155	.130	.089
	.535	.151	.106	.086	.056	.015
	.545	.093	.043	.018	-.026	-.076
	.555	.007	-.038	-.064	-.084	-.143
	.565	-.310	-.361	-.381	-.395	-.407
	.568	-.372	-.422	-.425	-.425	-.428
Transition	.577	-.109	-.137	-.139	-.153	-.160
	.587	-.063	-.084	-.087	-.096	-.102
	.597	-.028	-.049	-.052	-.054	-.049
	.607	-.022	-.044	-.040	-.048	-.049
	.617	-.016	-.032	-.029	-.032	-.032
	.627	-.010	-.020	-.023	-.026	-.026
	.637	-.004	-.010	-.011	-.014	-.014
	.657	-.002	-.013	-.011	-.014	-.014
	.677	.009	.007	.002	.004	.008
	.697	.004	.007	.003	.004	.008
Main stage	.737	.007	.003	.001	.001	.008
	.777	.015	.005	.006	.006	.003
	.785	.013	.001	.006	.011	.001
	.817	.013	.003	.005	.005	.001
	.857	.008	.002	.001	.002	.002
	.877	.006	.003	.001	.001	.006
	.897	.004	.002	.001	.001	.006
	.917	.003	.001	.001	.001	.006
	.957	.001	.001	.001	.001	.006
	.997	.001	.001	.001	.001	.006
None	.368	.346	.344	.336	.330	.330
	.408	.330	.277	.229	.189	.144
	.412	.254	.215	.195	.155	.110
	.432	.233	.215	.162	.116	.076
	.442	.155	.113	.060	.026	-.067
	.447	.042	.000	-.049	-.090	-.125
	.453	-.004	-.090	-.140	-.189	-.224
	.458	-.028	-.140	-.189	-.224	-.260
	.463	-.051	-.160	-.211	-.248	-.280
	.473	-.079	-.181	-.224	-.260	-.291
Upper stage	.483	-.095	-.115	-.135	-.141	-.136
	.483	-.059	-.029	-.010	.009	.020
	.493	.078	.064	.055	.055	.061
	.503	.174	.147	.119	.118	.113
	.513	.267	.236	.209	.209	.200
	.525	.192	.161	.112	.095	.078
	.535	.118	.086	.032	.015	.009
	.545	.040	.046	.020	.038	-.061
	.555	-.009	-.046	-.102	.126	-.138
	.565	-.251	-.319	-.346	-.372	-.372
Transition	.568	-.442	-.498	-.514	-.503	-.486
	.577	-.086	-.131	-.139	-.154	-.154
	.587	-.039	-.079	-.081	-.090	-.084
	.607	-.016	-.049	-.052	-.061	-.049
	.617	.007	-.040	-.040	-.038	-.032
	.627	.007	-.026	-.035	-.032	-.020
	.637	.018	-.020	-.023	-.020	-.014
	.657	.021	-.015	-.017	-.014	-.009
	.677	.025	-.001	-.007	-.006	-.005
	.697	.031	.005	-.002	-.004	-.003
Main stage	.737	.029	.005	.004	.002	.005
	.777	.035	.011	.006	.005	.003
	.785	.041	.006	.009	.011	.019
	.817	.040	.014	.008	.007	.013
	.857	.033	.008	.005	.003	.004
	.877	.036	.009	.005	.004	.005
	.897	.029	.005	.002	.001	.001
	.917	.029	.005	.002	.001	.001
	.957	.029	.005	.002	.001	.001
	.997	.029	.005	.002	.001	.001

TABLE 5.- PRESSURE COEFFICIENTS FOR CONFIGURATION 122 - Continued

(b) $M = 0.60$; $\alpha = -10^\circ$ to 10° - Concluded

		C_p for -							
		$\beta = -30^\circ$							
		$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$	
Nozzle	x/l	.382	.176	.239	.265	.274	.268	.240	.178
		.412	.080	.121	.147	.150	.144	.122	.059
		.432	-.004	.031	.045	.049	.043	.026	-.038
		.447	-.279	-.236	-.221	-.212	-.218	-.242	-.289
		.453	-.928	-.931	-.974	-1.000	-1.001	-1.019	-1.036
		.473	-.108	-.061	-.046	-.037	-.043	-.066	-.118
		.493	-.027	.026	.046	.056	.049	.026	-.037
		.513	.214	.26	.288	.297	.291	.262	.204
		.535	-.016	.026	.052	.050	.049	.026	-.032
		.565	-.462	-.425	-.404	-.406	-.401	-.425	-.472
Transition	x/l	.568	-.535	-.498	-.483	-.479	-.486	-.504	-.544
		.587	-.162	-.131	-.099	-.095	-.096	-.119	-.172
		.607	-.121	-.079	-.052	-.048	-.043	-.067	-.125
		.627	-.103	-.061	-.035	-.031	-.032	-.049	-.108
		.657	-.092	-.046	-.019	-.014	-.016	-.043	-.096
		.697	-.082	-.040	-.011	-.008	-.010	-.036	-.084
		.737	-.078	-.034	-.007	-.002	-.002	-.030	-.081
		.777	-.073	-.030	-.003	-.002	-.002	-.026	-.075
		.785	-.078	-.030	-.007	-.002	-.002	-.024	-.073
		.817	-.068	-.024	-.001	-.003	-.003	-.019	-.067
Main stage	x/l	.857	-.070	-.030	-.005	-.002	-.003	-.024	-.070
		.897	-.072	-.033	-.008	-.005	-.006	-.028	-.072
		.915	-.074	-.039	-.011	-.009	-.010	-.034	-.081
		.939	-.077	-.042	-.013	-.011	-.012	-.036	-.084
		.957	-.077	-.042	-.013	-.011	-.012	-.036	-.084
		.977	-.077	-.042	-.013	-.011	-.012	-.036	-.084
		.997	-.077	-.042	-.013	-.011	-.012	-.036	-.084
		.997	-.077	-.042	-.013	-.011	-.012	-.036	-.084
		.997	-.077	-.042	-.013	-.011	-.012	-.036	-.084
		.997	-.077	-.042	-.013	-.011	-.012	-.036	-.084
Flare	x/l	.255	.256	.248	.224	.195	.155	.071	.071
		.227	.222	.215	.190	.161	.116	.042	.042
		.193	.189	.175	.150	.122	.082	.009	.009
		.092	.087	.079	.049	.026	-.020	-.084	-.084
		-.016	-.026	-.035	-.066	-.084	-.125	-.190	-.190
		-.115	-.096	-.078	-.078	-.073	-.084	-.125	-.125
		-.852	-.890	-.939	-1.006	-1.041	-1.059	-1.106	-1.106
		-.247	-.245	-.242	-.239	-.251	-.257	-.303	-.303
		-.137	-.124	-.121	-.112	-.112	-.141	-.170	-.170
		-.074	-.049	-.046	-.037	-.043	-.060	-.095	-.095
Upper stage	x/l	.027	.006	.006	.010	.009	-.014	-.055	-.055
		.019	.043	.052	.061	.055	.032	-.003	-.003
		.088	.121	.118	.125	.118	.095	.049	.049
		.278	.296	.288	.291	.274	.239	.187	.187
		.088	.118	.127	.124	.107	.072	.015	.015
		.065	.066	.069	.050	.038	.009	-.050	-.050
		.013	.014	.012	.008	-.026	-.050	-.108	-.108
		-.089	-.083	-.081	-.113	-.109	-.133	-.187	-.187
		-.380	-.384	-.381	-.395	-.401	-.419	-.460	-.460
		-.430	-.434	-.425	-.427	-.433	-.445	-.475	-.475
Transition	x/l	-.577	-.449	-.435	-.427	-.448	-.460	-.495	-.495
		-.156	-.149	-.139	-.142	-.148	-.160	-.195	-.195
		-.127	-.114	-.093	-.095	-.096	-.107	-.143	-.143
		-.098	-.064	-.060	-.060	-.061	-.078	-.108	-.108
		-.080	-.048	-.048	-.048	-.043	-.061	-.096	-.096
		-.074	-.035	-.035	-.037	-.037	-.049	-.078	-.078
		-.061	-.023	-.023	-.023	-.026	-.043	-.073	-.073
		-.017	-.010	-.010	-.014	-.012	-.032	-.059	-.059
		-.068	-.044	-.044	-.044	-.044	-.059	-.092	-.092
		-.061	-.026	-.026	-.026	-.026	-.043	-.073	-.073
Main stage	x/l	.677	.649	.626	.610	.609	.604	.592	.592
		.697	.637	.615	.602	.602	.601	.586	.586
		.737	.649	.620	.602	.603	.603	.586	.586
		.777	.643	.620	.602	.603	.603	.586	.586
		.785	.649	.620	.602	.603	.603	.586	.586
		.817	.642	.617	.602	.603	.603	.586	.586
		.857	.646	.622	.605	.604	.604	.586	.586
		.877	.646	.622	.605	.604	.604	.586	.586
		.897	.649	.623	.607	.607	.607	.586	.586
		.917	.649	.623	.607	.607	.607	.586	.586

TABLE 5.- PRESSURE COEFFICIENTS FOR CONFIGURATION 122 - Continued

(c) $M = 0.80$; $\alpha = -10^\circ$ to 10°

x/l	C_p for $\beta = 0^\circ$							x/l	C_p for $\beta = -30^\circ$																				
	$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$		$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$														
	Nose	.382	.727	.718	.713	.704	.696		.683	.678	.392	.408	.346	.303	.267	.218	.171	.105	.392	.402	.367	.332	.299	.269	.231	.195	.142	.095	.033
Upper stage	.463	.709	.692	.685	.677	.669	.661	.653	.412	.432	.175	.133	.100	.051	.004	-.056	.442	.442	.176	.133	.098	.067	.037	.006	-.086	-.143	-.229		
Upper stage	.463	.709	.692	.685	.677	.669	.661	.653	.453	-1.401	-1.430	-1.443	-1.445	-1.433	-1.417	-1.411	.458	.458	-.340	-.443	-.482	-.500	-.546	-.551	-.565	-.565	-.565		
Upper stage	.463	.709	.692	.685	.677	.669	.661	.653	.473	.017	-.027	-.027	-.026	-.026	-.026	-.026	.463	.463	-.111	-.159	-.210	-.240	-.255	-.279	-.339	-.339	-.339		
Upper stage	.463	.709	.692	.685	.677	.669	.661	.653	.483	.084	.074	.073	.072	.072	.072	.072	.483	.483	.033	.028	.027	.026	.026	.026	.026	.026	.026	.026	
Upper stage	.463	.709	.692	.685	.677	.669	.661	.653	.503	.173	.159	.155	.155	.155	.155	.155	.503	.503	.075	.074	.073	.072	.072	.072	.072	.072	.072	.072	
Upper stage	.463	.709	.692	.685	.677	.669	.661	.653	.513	.393	.361	.329	.307	.281	.252	.212	.513	.513	.329	.329	.329	.329	.329	.329	.329	.329	.329	.329	.329
Transition	.525	.288	.236	.197	.171	.137	.109	.092	.525	.238	.20	.185	.168	.137	.105	.072	.525	.525	.20	.136	.108	.083	.052	.020	-.009	-.009	-.009	-.009	
Transition	.525	.288	.236	.197	.171	.137	.109	.092	.535	.176	.136	.108	.083	.052	.020	-.009	.535	.535	.176	.136	.108	.083	.052	.020	-.009	-.009	-.009	-.009	-.009
Transition	.525	.288	.236	.197	.171	.137	.109	.092	.545	.114	.070	.039	.017	-.022	-.055	-.088	.545	.545	.114	.070	.039	.017	-.022	-.055	-.088	-.119	-.191	-.433	
Transition	.525	.288	.236	.197	.171	.137	.109	.092	.555	.072	-.032	-.062	-.062	-.062	-.062	-.062	.555	.555	.072	-.032	-.062	-.062	-.062	-.062	-.062	-.062	-.062	-.062	
Transition	.525	.288	.236	.197	.171	.137	.109	.092	.565	-.276	-.343	-.417	-.456	-.469	-.443	-.443	.565	.565	-.276	-.343	-.417	-.456	-.469	-.443	-.443	-.443	-.443	-.443	
Main stage	.577	-.829	-.909	-.930	-.858	-.751	-.658	-.581	.577	-.123	-.156	-.169	-.179	-.191	-.181	-.181	.577	.577	-.123	-.156	-.169	-.179	-.191	-.181	-.181	-.181	-.181	-.181	
Main stage	.577	-.829	-.909	-.930	-.858	-.751	-.658	-.581	.587	-.060	-.086	-.098	-.101	-.112	-.109	-.099	.587	.587	-.060	-.086	-.098	-.101	-.112	-.109	-.099	-.099	-.099	-.099	-.099
Main stage	.577	-.829	-.909	-.930	-.858	-.751	-.658	-.581	.597	-.033	-.058	-.067	-.069	-.077	-.074	-.064	.597	.597	-.033	-.058	-.067	-.069	-.077	-.074	-.064	-.064	-.064	-.064	-.064
Main stage	.577	-.829	-.909	-.930	-.858	-.751	-.658	-.581	.607	-.017	-.039	-.051	-.050	-.057	-.054	-.040	.607	.607	-.017	-.039	-.051	-.050	-.057	-.054	-.040	-.040	-.040	-.040	-.040
Main stage	.577	-.829	-.909	-.930	-.858	-.751	-.658	-.581	.617	-.006	-.031	-.039	-.038	-.045	-.042	-.032	.617	.617	-.006	-.031	-.039	-.038	-.045	-.042	-.032	-.032	-.032	-.032	-.032
Main stage	.577	-.829	-.909	-.930	-.858	-.751	-.658	-.581	.627	-.002	-.019	-.020	-.020	-.023	-.023	-.013	.627	.627	-.002	-.019	-.020	-.020	-.023	-.023	-.013	-.013	-.013	-.013	-.013
Main stage	.577	-.829	-.909	-.930	-.858	-.751	-.658	-.581	.637	-.013	-.011	-.020	-.018	-.026	-.023	-.013	.637	.637	-.013	-.011	-.020	-.018	-.026	-.023	-.013	-.013	-.013	-.013	-.013
Main stage	.577	-.829	-.909	-.930	-.858	-.751	-.658	-.581	.647	-.019	-.002	-.014	-.013	-.015	-.012	-.009	.647	.647	-.019	-.002	-.014	-.013	-.015	-.012	-.009	-.009	-.009	-.009	-.009
Main stage	.577	-.829	-.909	-.930	-.858	-.751	-.658	-.581	.657	-.022	-.001	-.012	-.010	-.013	-.012	-.006	.657	.657	-.022	-.001	-.012	-.010	-.013	-.012	-.006	-.006	-.006	-.006	-.006
Main stage	.577	-.829	-.909	-.930	-.858	-.751	-.658	-.581	.667	-.026	-.003	-.008	-.006	-.009	-.007	-.006	.667	.667	-.026	-.003	-.008	-.006	-.009	-.007	-.006	-.006	-.006	-.006	-.006
Main stage	.577	-.829	-.909	-.930	-.858	-.751	-.658	-.581	.677	-.031	-.003	-.007	-.004	-.005	-.005	-.005	.677	.677	-.031	-.003	-.007	-.004	-.005	-.005	-.005	-.005	-.005	-.005	-.005
Main stage	.577	-.829	-.909	-.930	-.858	-.751	-.658	-.581	.687	-.038	-.004	-.004	-.001	-.002	-.002	-.005	.687	.687	-.038	-.004	-.004	-.001	-.002	-.002	-.005	-.005	-.005	-.005	-.005
Main stage	.577	-.829	-.909	-.930	-.858	-.751	-.658	-.581	.697	-.041	-.004	-.004	-.005	-.003	-.005	-.006	.697	.697	-.041	-.004	-.004	-.005	-.003	-.005	-.006	-.006	-.006	-.006	-.006
Main stage	.577	-.829	-.909	-.930	-.858	-.751	-.658	-.581	.707	-.049	-.004	-.004	-.005	-.003	-.005	-.006	.707	.707	-.049	-.004	-.004	-.005	-.003	-.005	-.006	-.006	-.006	-.006	-.006
Main stage	.577	-.829	-.909	-.930	-.858	-.751	-.658	-.581	.717	-.059	-.004	-.004	-.005	-.003	-.005	-.006	.717	.717	-.059	-.004	-.004	-.005	-.003	-.005	-.006	-.006	-.006	-.006	-.006
Main stage	.577	-.829	-.909	-.930	-.858	-.751	-.658	-.581	.727	-.069	-.004	-.004	-.005	-.003	-.005	-.006	.727	.727	-.069	-.004	-.004	-.005	-.003	-.005	-.006	-.006	-.006	-.006	-.006
Main stage	.577	-.829	-.909	-.930	-.858	-.751	-.658	-.581	.737	-.079	-.004	-.004	-.005	-.003	-.005	-.006	.737	.737	-.079	-.004	-.004	-.005	-.003	-.005	-.006	-.006	-.006	-.006	-.006
Main stage	.577	-.829	-.909	-.930	-.858	-.751	-.658	-.581	.747	-.089	-.004	-.004	-.005	-.003	-.005	-.006	.747	.747	-.089	-.004	-.004	-.005	-.003	-.005	-.006	-.006	-.006	-.006	-.006
Main stage	.577	-.829	-.909	-.930	-.858	-.751	-.658	-.581	.757	-.099	-.004	-.004	-.005	-.003	-.005	-.006	.757	.757	-.099	-.004	-.004	-.005	-.003	-.005	-.006	-.006	-.006	-.006	-.006
Main stage	.577	-.829	-.909	-.930	-.858	-.751	-.658	-.581	.767	-.109	-.004	-.004	-.005	-.003	-.005	-.006	.767	.767	-.109	-.004	-.004	-.005	-.003	-.005	-.006	-.006	-.006	-.006	-.006
Main stage	.577	-.829	-.909	-.930	-.858	-.751	-.658	-.581	.777	-.119	-.004	-.004	-.005	-.003	-.005	-.006	.777	.777	-.119	-.004	-.004	-.005	-.003	-.005	-.006	-.006	-.006	-.006	-.006
Main stage	.577	-.829	-.909	-.930	-.858	-.751	-.658	-.581	.787	-.129	-.004	-.004	-.005	-.003	-.005	-.006	.787	.787	-.129	-.004	-.004	-.005	-.003	-.005	-.006	-.006	-.006	-.006	-.006
Main stage	.577	-.829	-.909	-.930	-.858	-.751	-.658	-.581	.797	-.139	-.004	-.004	-.005	-.003	-.005	-.006	.797	.797	-.139	-.004	-.004	-.005	-.003	-.005	-.006	-.006	-.006	-.006	-.006
Main stage	.577	-.829	-.909	-.930	-.858	-.751	-.658	-.581	.807	-.149	-.004	-.004	-.005	-.003	-.005	-.006	.807	.807	-.149	-.004	-.004	-.005	-.003	-.005	-.006	-.006	-.006	-.006	-.006
Main stage	.577	-.829	-.909	-.930	-.858	-.751	-.658	-.581	.817	-.159	-.004	-.004	-.005	-.003	-.005	-.006	.817	.817	-.159	-.004	-.004	-.005	-.003	-.005	-.006	-.006	-.006	-.006	-.006
Main stage	.577	-.829	-.909	-.930	-.858	-.751	-.658	-.581	.827	-.169	-.004	-.004	-.005	-.003	-.005	-.006	.827	.827	-.169	-.004	-.004	-.005	-.003	-.005	-.006	-.006	-.006	-.006	-.006
Main stage	.577	-.829	-.909	-.930	-.858	-.751	-.658	-.581	.837	-.179	-.004	-.004	-.005	-.003	-.005	-.006	.837	.837	-.179	-.004	-.004	-.005	-.003	-.005	-.006	-.006	-.006	-.006	-.006
Main stage	.577	-.829	-.909	-.930	-.858	-.751	-.658	-.581	.847	-.189	-.004	-.004	-.005	-.003	-.005	-.006	.847	.847	-.189	-.004	-.004	-.005	-.003	-.005	-.006	-.006	-.006	-.006	-.006
Main stage	.577	-.829	-.909	-.930	-.858	-.751	-.658	-.581	.857	-.199	-.004	-.004	-.005	-.003	-.005	-.006	.857	.857	-.199	-.004	-.004	-.005	-.003	-.005	-.006	-.006	-.006	-.006	-.006
Main stage	.577	-.829	-.909	-.930	-.858	-.751	-.658	-.581	.867	-.209	-.004	-.004	-.005	-.003	-.005	-.006	.867	.867	-.209	-.004	-.004	-.005	-.003	-.005	-.006	-.006	-.006	-.006	-.006
Main stage	.577	-.829	-.909	-.930	-.858	-.751	-.658	-.581	.877	-.219	-.004	-.004	-.005	-.003	-.005	-.006	.877	.877	-.219	-.004	-.004	-.005	-.003	-.005	-.006	-.006	-.006	-.006	-.006
Main stage	.577	-.829	-.909	-.930	-.858	-.751	-.658	-.581	.887	-.229	-.004	-.004	-.005	-.003	-.005	-.006	.887	.887	-.229	-.004	-.004	-.005	-.003	-.005	-.006	-.006	-.006	-.006	-.006
Main stage	.577	-.829	-.909	-.930	-.858	-.751	-.658	-.581	.897	-.239	-.004	-.004	-.005	-.003	-.005	-.006	.897	.89											

TABLE 5.- PRESSURE COEFFICIENTS FOR CONFIGURATION 122 - Continued

(c) $M = 0.80$; $\alpha = -10^\circ$ to 10° - Concluded

		C_p for $\beta = -50^\circ$						C_p for $\beta = -90^\circ$								
		$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$	$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$	
Main stage	x/l	.392	.291	.277	.259	.226	.183	.105	.382	.211	.278	.296	.302	.277	.211	
	Roar	.402	.260	.255	.243	.225	.188	.145	.071	.412	.226	.224	.205	.187	.148	.090
Transition flare	x/l	.432	.127	.130	.110	.092	.083	.016	-.056	.432	.021	.073	.083	.078	.054	-.005
	Roar	.442	.029	.027	.019	.003	-.074	-.139	-.119	.447	-.202	-.157	-.138	-.128	-.160	-.209
Upper stage	x/l	.453	-.1039	-.094	-.073	-.081	-.094	-.115	-.160	.453	-.193	-.186	-.195	-.213	-.1225	-.1251
	Roar	.458	-.460	-.645	-.677	-.687	-.710	-.693	-.693	.473	-.122	-.062	-.031	-.029	-.062	-.122
Main stage	x/l	.473	-.083	-.027	-.006	-.018	-.046	-.094	-.208	.493	-.021	.039	.062	.064	.035	-.032
	Roar	.483	-.033	.004	.019	.021	.001	-.044	-.044	.513	.242	.299	.317	.312	.287	.223
Transition flare	x/l	.493	.026	.059	.070	.083	.051	.011	.072	.535	.002	.055	.077	.083	.039	-.017
	Roar	.503	.103	.147	.156	.137	.113	.072	.072	.565	-.471	.442	-.430	-.428	-.449	-.479
Main stage	x/l	.513	.304	.322	.319	.292	.260	.208	.208	.568	-.1033	-.984	-.953	-.955	-.987	-.1024
	Roar	.525	.114	.162	.160	.129	.093	.034	.034	.587	-.182	-.133	-.114	-.105	-.144	-.193
Transition flare	x/l	.535	.083	.089	.083	.056	.020	-.033	-.033	.607	-.131	-.078	-.059	-.061	-.090	-.138
	Roar	.545	.025	.027	.017	-.014	-.051	-.100	-.100	.627	-.115	-.058	-.039	-.041	-.066	-.115
Main stage	x/l	.555	-.076	-.066	-.093	-.106	-.143	-.192	-.192	.657	-.097	-.048	-.026	-.027	-.050	-.103
	Roar	.565	-.317	.382	-.403	-.440	-.465	-.506	-.506	.697	-.091	-.039	-.020	-.018	-.043	-.097
Transition flare	x/l	.577	-.959	-.968	-.924	-.904	-.960	-.989	-.989	.777	-.092	-.033	-.014	-.003	-.035	-.086
	Roar	.587	-.168	-.165	-.159	-.179	-.191	-.213	-.213	.785	-.078	-.030	-.011	-.009	-.031	-.084
Main stage	x/l	.597	-.151	-.110	-.105	-.116	-.133	-.154	-.154	.817	-.069	-.033	-.011	-.001	-.029	-.076
	Roar	.607	-.096	-.075	-.065	-.077	-.093	-.123	-.123	.857	-.074	-.023	-.010	-.003	-.026	-.070
Transition flare	x/l	.617	-.092	-.055	-.050	-.057	-.074	-.103	-.103	.897	-.075	-.031	-.012	-.002	-.033	-.077
	Roar	.627	-.084	-.047	-.038	-.049	-.062	-.091	-.091							
Main stage	x/l	.637	-.076	-.031	-.030	-.041	-.054	-.083	-.083							
	Roar	.657	-.068	-.036	-.022	-.033	-.050	-.076	-.076							
Transition flare	x/l	.677	-.055	-.028	-.014	-.023	-.037	-.065	-.065							
	Roar	.697	-.041	-.018	-.014	-.018	-.033	-.058	-.058							
Main stage	x/l	.737	-.053	-.022	-.001	-.010	-.023	-.051	-.051							
	Roar	.777	-.047	-.018	.003	-.006	-.018	-.042	-.042							
Transition flare	x/l	.785	-.054	-.022	.003	-.003	-.016	-.035	-.035							
	Roar	.817	-.045	.015	.003	-.003	-.014	-.028	-.028							
Main stage	x/l	.857	-.050	.021	.001	-.006	-.018	-.031	-.031							
	Roar	.877	-.050	.020	.008	-.004	-.018	-.030	-.030							
Transition flare	x/l	.897	-.052	.021	.000	-.008	-.019	-.032	-.032							
	Roar	.917	-.058	.028	.015	-.005	-.024	-.035	-.035							
Main stage	x/l	.957	-.064	.036	-.022	-.021	-.033	-.046	-.046							
	Roar	.997	-.133	-.100	-.070	-.083	-.104	-.128	-.128							

TABLE 5.- PRESSURE COEFFICIENTS FOR CONFIGURATION 122 - Continued

(a) $M = 1.00$; $\alpha = -10^\circ$ to 10°

		C_p for $\beta = 0^\circ$						C_p for $\beta = -50^\circ$							
		$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -5^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$	$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -5^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$
Main stage	x/l	.947	.958	.970	.980	.992	1.006	1.013	.509	.448	.406	.367	.322	.279	.216
	Nose	.542	.469	.415	.370	.325	.282	.228	.420	.375	.348	.321	.292	.245	.183
		.521	.442	.396	.346	.298	.255	.201	.446	.387	.354	.327	.289	.218	.153
		.482	.405	.354	.310	.265	.221	.165	.432	.367	.335	.308	.266	.198	.136
		.432	.353	.291	.247	.198	.155	.101	.442	.374	.342	.315	.271	.207	.147
		.404	.323	.261	.217	.168	.125	.059	.422	.354	.322	.295	.251	.187	.127
		.334	.268	.206	.162	.113	.064	.020	.447	.379	.347	.320	.276	.212	.152
		.268	.206	.144	.100	.051	.004	.000	.453	.385	.353	.326	.282	.218	.158
		.236	.173	.111	.067	.018	.000	.000	.458	.390	.358	.331	.287	.223	.163
		.206	.143	.081	.037	.000	.000	.000	.453	.385	.353	.326	.282	.218	.158
Transition flare	x/l	.411	.376	.351	.319	.254	.222	.186	.355	.348	.342	.322	.285	.250	.183
		.334	.293	.268	.251	.233	.213	.186	.306	.284	.262	.251	.236	.207	.162
		.300	.250	.219	.193	.174	.158	.134	.257	.228	.204	.183	.171	.139	.100
		.251	.204	.170	.134	.097	.075	.054	.196	.170	.146	.122	.094	.056	.017
		.027	.018	.049	.098	.164	.218	.218	.017	.046	.074	.108	.133	.168	.202
		.510	.532	.551	.572	.566	.579	.585	.519	.532	.548	.572	.591	.607	.635
		.329	.398	.438	.463	.438	.423	.432	.372	.423	.454	.472	.494	.529	.569
		.229	.311	.354	.385	.391	.398	.407	.251	.317	.357	.385	.391	.401	.419
		.163	.236	.279	.313	.335	.345	.338	.166	.211	.236	.241	.251	.258	.251
		.138	.199	.236	.257	.263	.258	.223	.166	.211	.236	.241	.251	.258	.251
Nose	x/l	.129	.177	.198	.204	.197	.183	.154	.157	.174	.170	.170	.197	.189	.163
		.123	.158	.164	.160	.144	.127	.107	.145	.149	.136	.126	.148	.136	.101
		.107	.130	.127	.123	.107	.096	.079	.123	.105	.092	.082	.110	.102	.073
		.092	.088	.088	.079	.070	.061	.052	.105	.088	.068	.058	.074	.073	.054
		.049	.068	.065	.063	.057	.042	.046	.064	.068	.054	.046	.045	.056	.072
		.022	.044	.046	.046	.041	.030	.038	.049	.054	.030	.030	.031	.036	.076
		.009	.026	.029	.031	.031	.031	.029	.034	.035	.026	.025	.028	.036	.070
		.000	.023	.026	.030	.031	.031	.029	.018	.026	.021	.021	.023	.032	.054
		.014	.019	.019	.022	.022	.020	.003	.014	.022	.021	.016	.013	.023	.032
		.049	.012	.011	.015	.010	.011	.018	.022	.022	.023	.016	.013	.016	.013
	.062	.034	.029	.026	.024	.022	.018	.034	.031	.026	.026	.024	.016	.014	
	.066	.045	.035	.030	.029	.027	.018	.033	.031	.028	.027	.024	.014	.014	
	.060	.038	.030	.027	.025	.023	.011	.020	.011	.013	.011	.005	.006	.025	
	.060	.038	.030	.027	.025	.023	.011	.020	.011	.013	.011	.005	.006	.025	

TABLE 5.- PRESSURE COEFFICIENTS FOR CONFIGURATION 122 - Continued

(d) $M = 1.00$; $\alpha = -10^\circ$ to 10° - Concluded

		C_p for $\beta = -60^\circ$						C_p for $\beta = -90^\circ$										
		$\alpha = -10^\circ$		$\alpha = -5^\circ$		$\alpha = 0^\circ$		$\alpha = -10^\circ$		$\alpha = -5^\circ$		$\alpha = 0^\circ$						
		x/l						x/l										
Main stage	Noose	.392	.401	.396	.381	.361	.331	.291	.216	.382	.325	.378	.400	.406	.401	.381	.325	
		.412	.370	.366	.351	.331	.301	.261	.183	.412	.228	.276	.294	.307	.292	.267	.210	
		.432	.340	.339	.321	.304	.271	.230	.153	.432	.165	.215	.230	.237	.222	.200	.138	
		.442	.268	.269	.255	.237	.201	.164	.086	.447	.032	.082	.107	.111	.105	.082	.023	
		.447	.207	.209	.203	.186	.153	.119	.044	.453	-.658	-.646	-.646	-.645	-.661	-.671	-.711	
		.453	.192	.192	.185	.168	.132	.095	-.086	.473	-.468	-.460	-.469	-.471	-.477	-.478	-.490	
		.458	.136	.136	.129	.112	.076	.039	-.035	.493	-.078	-.039	-.014	.011	-.007	-.036	-.066	
		.463	.081	.081	.074	.057	.021	-.016	-.084	.513	.270	.318	.321	.301	.332	.321	.270	
		.483	.037	.037	.030	.013	-.023	-.058	-.112	.535	.122	.207	.235	.251	.233	.192	.109	
		.503	-.193	-.148	-.058	.008	.033	.004	.134	.565	-.161	-.115	-.102	-.105	-.098	-.112	-.158	
.513	.375	.377	.349	.304	.292	.247	.174	.568	-.622	-.586	-.569	-.575	-.572	-.585	-.619			
Transition	Flare	.223	.223	.293	.318	.319	.297	.241	.134	.587	-.432	-.405	-.392	-.388	-.400	-.420	-.451	
		.214	.214	.247	.251	.251	.226	.185	.100	.607	-.341	-.286	-.258	-.254	-.260	-.292	-.354	
		.171	.171	.194	.192	.183	.171	.127	.054	.627	-.276	-.196	-.167	-.160	-.160	-.195	-.273	
		.112	.112	.138	.140	.119	.107	.068	-.002	.657	-.176	-.120	-.090	-.081	-.092	-.123	-.185	
		.070	.070	.059	.074	.092	.108	.131	.180	.697	-.131	-.078	-.055	-.046	-.055	-.081	-.138	
		.560	.542	.542	.545	.556	.569	.585	.619	.737	-.122	-.066	-.036	-.030	-.038	-.064	-.125	
		.577	.461	.461	.467	.472	.494	.526	.575	.777	-.107	-.059	-.034	-.026	-.037	-.061	-.117	
		.587	.347	.347	.373	.388	.416	.448	.500	.817	-.043	-.043	-.033	-.026	-.033	-.056	-.104	
		.597	.285	.292	.298	.298	.282	.257	.228	.857	-.044	.001	.020	.026	.019	-.002	-.044	
		.607	.257	.252	.248	.248	.230	.204	.174	.897	-.049	-.003	.019	.027	.019	-.001	-.048	
Main stage	Noose	.617	.248	.224	.204	.204	.201	.214	.298									
		.627	.248	.224	.204	.204	.201	.214	.298									
		.637	.229	.199	.170	.163	.157	.170	.170	.198								
		.657	.167	.119	.092	.080	.080	.119	.139	.163								
		.677	-.127	-.090	.071	.062	.066	.081	.107	.125								
		.697	-.088	.041	.049	.045	.050	.065	.089									
		.737	-.092	.054	.049	.045	.050	.065	.089									
		.777	-.081	.049	.031	.030	.035	.050	.077									
		.795	-.082	.049	.030	.026	.033	.047	.066									
		.817	-.020	.039	.025	.025	.030	.043	.059									

TABLE 5.- PRESSURE COEFFICIENTS FOR CONFIGURATION 122 - Continued

(a) $M = 1.20$; $\alpha = -10^\circ$ to 10°

x/l	C_p for $\beta = 0^\circ$						x/l	C_p for $\beta = -30^\circ$							
	$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$		$\alpha = 10^\circ$	$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$
	None	1.308	1.290	1.275	1.259	1.227		1.198	1.185	.382	.403	.361	.307	.276	.227
None	.512	.422	.372	.315	.268	.227	.194	.392	.477	.406	.361	.276	.227	.186	
	.523	.430	.377	.321	.281	.235	.202	.402	.474	.406	.313	.278	.235	.183	
	.509	.425	.366	.315	.278	.235	.194	.412	.474	.358	.313	.278	.235	.183	
None	.499	.419	.361	.315	.270	.235	.189	.432	.458	.350	.318	.270	.233	.175	
	.472	.403	.353	.318	.270	.230	.178	.442	.440	.348	.318	.276	.233	.175	
	.472	.434	.337	.305	.262	.222	.173	.447	.405	.331	.305	.262	.222	.162	
None	.447	.376	.337	.302	.262	.222	.173	.453	.469	.363	.341	.285	.235	.175	
	.453	.398	.348	.322	.284	.244	.194	.458	.458	.341	.307	.263	.211	.151	
	.458	.409	.363	.341	.309	.269	.229	.463	.463	.354	.327	.285	.235	.175	
None	.463	.429	.387	.359	.327	.299	.266	.463	.458	.354	.327	.285	.235	.175	
	.473	.443	.409	.382	.343	.309	.276	.473	.473	.354	.327	.285	.235	.175	
	.483	.455	.429	.409	.374	.343	.310	.483	.483	.354	.327	.285	.235	.175	
None	.483	.455	.429	.409	.374	.343	.310	.483	.483	.354	.327	.285	.235	.175	
	.503	.477	.455	.439	.409	.374	.343	.503	.503	.385	.354	.327	.285	.235	
	.503	.477	.455	.439	.409	.374	.343	.503	.503	.385	.354	.327	.285	.235	
None	.513	.489	.466	.443	.415	.387	.362	.513	.513	.389	.354	.327	.285	.235	
	.525	.504	.481	.458	.435	.412	.389	.525	.525	.403	.368	.333	.298	.263	
	.535	.514	.491	.468	.445	.422	.399	.535	.535	.422	.387	.352	.317	.282	
None	.545	.524	.501	.478	.455	.432	.409	.545	.545	.441	.406	.371	.336	.301	
	.555	.534	.511	.488	.465	.442	.419	.555	.555	.460	.425	.390	.355	.320	
	.565	.544	.521	.498	.475	.452	.429	.565	.565	.479	.444	.409	.374	.339	
None	.568	.547	.524	.501	.478	.455	.432	.568	.568	.498	.463	.428	.393	.358	
	.577	.556	.533	.510	.487	.464	.441	.577	.577	.507	.472	.437	.402	.367	
	.587	.566	.543	.520	.497	.474	.451	.587	.587	.517	.482	.447	.412	.377	
None	.587	.566	.543	.520	.497	.474	.451	.587	.587	.517	.482	.447	.412	.377	
	.597	.576	.553	.530	.507	.484	.461	.597	.597	.527	.492	.457	.422	.387	
	.607	.586	.563	.540	.517	.494	.471	.607	.607	.537	.502	.467	.432	.397	
None	.617	.596	.573	.550	.527	.504	.481	.617	.617	.547	.512	.477	.442	.407	
	.627	.606	.583	.560	.537	.514	.491	.627	.627	.557	.522	.487	.452	.417	
	.637	.616	.593	.570	.547	.524	.501	.637	.637	.567	.532	.497	.462	.427	
None	.657	.636	.613	.590	.567	.544	.521	.657	.657	.587	.552	.517	.482	.447	
	.677	.656	.633	.610	.587	.564	.541	.677	.677	.607	.572	.537	.502	.467	
	.697	.676	.653	.630	.607	.584	.561	.697	.697	.627	.592	.557	.522	.487	
None	.717	.696	.673	.650	.627	.604	.581	.717	.717	.647	.612	.577	.542	.507	
	.737	.716	.693	.670	.647	.624	.601	.737	.737	.667	.632	.597	.562	.527	
	.757	.736	.713	.690	.667	.644	.621	.757	.757	.687	.652	.617	.582	.547	
None	.777	.756	.733	.710	.687	.664	.641	.777	.777	.707	.672	.637	.602	.567	
	.797	.776	.753	.730	.707	.684	.661	.797	.797	.727	.692	.657	.622	.587	
	.817	.796	.773	.750	.727	.704	.681	.817	.817	.747	.712	.677	.642	.607	
None	.837	.816	.793	.770	.747	.724	.701	.837	.837	.767	.732	.697	.662	.627	
	.857	.836	.813	.790	.767	.744	.721	.857	.857	.787	.752	.717	.682	.647	
	.877	.856	.833	.810	.787	.764	.741	.877	.877	.807	.772	.737	.702	.667	
None	.897	.876	.853	.830	.807	.784	.761	.897	.897	.827	.792	.757	.722	.687	
	.917	.896	.873	.850	.827	.804	.781	.917	.917	.847	.812	.777	.742	.707	
	.937	.916	.893	.870	.847	.824	.801	.937	.937	.867	.832	.797	.762	.727	
None	.957	.936	.913	.890	.867	.844	.821	.957	.957	.887	.852	.817	.782	.747	
	.977	.956	.933	.910	.887	.864	.841	.977	.977	.907	.872	.837	.802	.767	
	.997	.976	.953	.930	.907	.884	.861	.997	.997	.927	.892	.857	.822	.787	
None	.185	.198	1.227	1.259	1.227	1.198	1.185	.392	.403	.361	.307	.276	.227	.183	
	.194	.227	.268	.315	.372	.422	.477	.402	.474	.406	.361	.276	.227	.186	
	.202	.235	.281	.321	.377	.430	.482	.412	.474	.358	.313	.278	.235	.183	
None	.194	.235	.278	.315	.366	.425	.489	.432	.458	.350	.318	.270	.233	.175	
	.189	.235	.270	.315	.361	.419	.489	.442	.440	.348	.318	.276	.233	.175	
	.173	.222	.262	.305	.353	.419	.499	.447	.440	.348	.318	.276	.233	.175	
None	.178	.222	.262	.305	.353	.419	.499	.447	.440	.348	.318	.276	.233	.175	
	.189	.235	.270	.315	.361	.419	.489	.442	.440	.348	.318	.276	.233	.175	
	.173	.222	.262	.305	.353	.419	.499	.447	.440	.348	.318	.276	.233	.175	
None	.173	.222	.262	.305	.353	.419	.499	.447	.440	.348	.318	.276	.233	.175	
	.189	.235	.270	.315	.361	.419	.489	.442	.440	.348	.318	.276	.233	.175	
	.173	.222	.262	.305	.353	.419	.499	.447	.440	.348	.318	.276	.233	.175	
None	.189	.235	.270	.315	.361	.419	.489	.442	.440	.348	.318	.276	.233	.175	
	.173	.222	.262	.305	.353	.419	.499	.447	.440	.348	.318	.276	.233	.175	
	.189	.235	.270	.315	.361	.419	.489	.442	.440	.348	.318	.276	.233	.175	
None	.173	.222	.262	.305	.353	.419	.499	.447	.440	.348	.318	.276	.233	.175	
	.189	.235	.270	.315	.361	.419	.489	.442	.440	.348	.318	.276	.233	.175	
	.173	.222	.262	.305	.353	.419	.499	.447	.440	.348	.318	.276	.233	.175	
None	.173	.222	.262	.305	.353	.419	.499	.447	.440	.348	.318	.276	.233	.175	
	.189	.235	.270	.315	.361	.419	.489	.442	.440	.348	.318	.276	.233	.175	
	.173	.222	.262	.305	.353	.419	.499	.447	.440	.348	.318	.276	.233	.175	
None	.173	.222	.262	.305	.353	.419	.499	.447	.440	.348	.318	.276	.233	.175	
	.189	.235	.270	.315	.361	.419	.489	.442	.440	.348	.318	.276	.233	.175	
	.173	.222	.262	.305	.353	.419	.499	.447	.440	.348	.318	.276	.233	.175	

TABLE 5.- PRESSURE COEFFICIENTS FOR CONFIGURATION 122 - Concluded

(e) $M = 1.20$; $\alpha = -10^\circ$ to 10° - Concluded

		C_p for $\beta = -90^\circ$							
		$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$	
Nose	x/l	.382	.254	.290	.307	.318	.308	.297	.267
		.412	.257	.288	.310	.307	.303	.284	.245
Upper stage	x/l	.432	.254	.304	.305	.315	.303	.292	.232
		.447	.192	.250	.275	.280	.276	.252	.191
Transition	x/l	.453	.344	.312	.303	.308	.319	.344	.381
		.473	.282	.261	.247	.247	.260	.271	.302
Main stage	x/l	.493	.216	.173	.151	.145	.150	.175	.231
		.513	.188	.244	.269	.264	.270	.243	.168
Nose	x/l	.392	.364	.347	.334	.307	.276	.241	.186
		.402	.372	.350	.334	.313	.281	.243	.191
Upper stage	x/l	.412	.370	.358	.334	.310	.284	.243	.186
		.432	.359	.338	.331	.313	.286	.262	.186
Transition	x/l	.442	.340	.342	.331	.315	.286	.249	.175
		.447	.340	.342	.331	.313	.286	.249	.175
Main stage	x/l	.453	.221	.156	.138	.133	.140	.157	.186
		.458	.362	.349	.321	.261	.282	.310	.356
Nose	x/l	.463	.288	.303	.305	.307	.332	.367	.420
		.463	.288	.303	.305	.307	.332	.367	.420
Upper stage	x/l	.483	.199	.223	.236	.244	.260	.277	.272
		.483	.199	.223	.236	.244	.260	.277	.272
Transition	x/l	.493	.142	.140	.34	.186	.205	.227	.228
		.493	.142	.140	.34	.186	.205	.227	.228
Main stage	x/l	.503	.120	.107	.098	.098	.100	.100	.052
		.503	.120	.107	.098	.098	.100	.100	.052
Nose	x/l	.513	.226	.266	.275	.264	.251	.215	.146
		.513	.226	.266	.275	.264	.251	.215	.146
Upper stage	x/l	.525	.248	.293	.304	.299	.275	.237	.156
		.525	.248	.293	.304	.299	.275	.237	.156
Transition	x/l	.535	.209	.227	.231	.220	.242	.204	.135
		.535	.209	.227	.231	.220	.242	.204	.135
Main stage	x/l	.545	.207	.223	.231	.214	.197	.168	.121
		.545	.207	.223	.231	.214	.197	.168	.121
Nose	x/l	.555	.130	.134	.127	.097	.078	.056	.012
		.555	.130	.134	.127	.097	.078	.056	.012
Upper stage	x/l	.565	.268	.258	.266	.266	.279	.298	.335
		.565	.268	.258	.266	.266	.279	.298	.335
Transition	x/l	.577	.237	.233	.230	.232	.246	.273	.323
		.577	.237	.233	.230	.232	.246	.273	.323
Main stage	x/l	.587	.187	.186	.188	.191	.207	.237	.291
		.587	.187	.186	.188	.191	.207	.237	.291
Nose	x/l	.597	.148	.150	.155	.152	.168	.193	.238
		.597	.148	.150	.155	.152	.168	.193	.238
Upper stage	x/l	.607	.137	.130	.130	.132	.143	.160	.202
		.607	.137	.130	.130	.132	.143	.160	.202
Transition	x/l	.617	.135	.119	.108	.110	.118	.135	.174
		.617	.135	.119	.108	.110	.118	.135	.174
Main stage	x/l	.627	.108	.108	.096	.096	.101	.121	.149
		.627	.108	.108	.096	.096	.101	.121	.149
Nose	x/l	.637	.121	.086	.080	.077	.079	.098	.127
		.637	.121	.086	.080	.077	.079	.098	.127
Upper stage	x/l	.647	.110	.057	.050	.037	.042	.067	.102
		.647	.110	.057	.050	.037	.042	.067	.102
Transition	x/l	.657	.102	.058	.043	.036	.041	.059	.091
		.657	.102	.058	.043	.036	.041	.059	.091
Main stage	x/l	.677	.093	.058	.036	.031	.033	.051	.063
		.677	.093	.058	.036	.031	.033	.051	.063
Nose	x/l	.737	.091	.053	.032	.031	.025	.037	.051
		.737	.091	.053	.032	.031	.025	.037	.051
Upper stage	x/l	.777	.066	.041	.028	.014	.018	.030	.049
		.777	.066	.041	.028	.014	.018	.030	.049
Transition	x/l	.785	.052	.039	.020	.016	.018	.031	.048
		.785	.052	.039	.020	.016	.018	.031	.048
Main stage	x/l	.817	.054	.026	.012	.015	.023	.022	.042
		.817	.054	.026	.012	.015	.023	.022	.042
Nose	x/l	.857	.062	.016	.007	.003	.008	.016	.032
		.857	.062	.016	.007	.003	.008	.016	.032
Upper stage	x/l	.877	.053	.027	.009	.001	.002	.016	.032
		.877	.053	.027	.009	.001	.002	.016	.032
Transition	x/l	.897	.062	.028	.005	.005	.008	.020	.033
		.897	.062	.028	.005	.005	.008	.020	.033
Main stage	x/l	.917	.068	.031	.014	.014	.018	.018	.033
		.917	.068	.031	.014	.014	.018	.018	.033
Nose	x/l	.957	.068	.035	.014	.014	.018	.018	.033
		.957	.068	.035	.014	.014	.018	.018	.033
Upper stage	x/l	.977	.060	.046	.041	.053	.068	.088	.101
		.977	.060	.046	.041	.053	.068	.088	.101

TABLE 6.- PRESSURE COEFFICIENTS FOR CONFIGURATION 222

(a) $M = 0.40$ to 0.95 ; $\alpha = 0^\circ$

		C_p for -				
		$\beta = 0^\circ$				
x/l		$M = 0.40$	$M = 0.70$	$M = 0.75$	$M = 0.85$	$M = 0.95$
		Nose				
	.421		.345	.358	.406	.471
Main stage						
		.431	.255	.268	.321	.395
		.441	.110	.131	.197	.241
		.453	-1.239	-1.137	-1.140	-1.056
		.458	.642	.685	.634	.907
		.463	.383	.512	.554	.600
		.473	.063	.144	.347	.364
		.483	.020	.012	.012	.532
		.493	.062	.067	.027	.163
		.503	.131	.130	.118	.130
Transition						
		.513	.265	.248	.215	.229
		.525	.144	.147	.172	.208
		.535	.061	.067	.103	.130
		.545	.002	.001	.031	.062
		.555	.092	.099	.068	.027
		.565	.403	.425	.389	.051
		.577	.498	.567	.852	.211
		.587	.162	.175	.181	.693
		.597	.101	.107	.112	.540
Flare						
		.607	.054	.060	.060	.438
		.617	.050	.056	.057	.278
		.627	.040	.043	.046	.154
		.637	.031	.039	.038	.033
		.647	.017	.026	.031	.026
		.657	.014	.022	.016	.021
		.677	.005	.012	.008	.012
		.697	.005	.013	.009	.005
		.717	.001	.009	.005	.004
Main stage						
		.737	.003	.002	.001	.010
		.757	.006	.000	.001	.006
		.777	.005	.000	.002	.006
		.785	.001	.000	.001	.006
		.817	.005	.000	.002	.006
		.837	.001	.004	.007	.006
		.857	.001	.006	.007	.012
		.877	.001	.007	.007	.012
		.897	.001	.008	.008	.014
Nose						
		.917	.001	.008	.008	.014
		.937	.013	.018	.018	.010
		.957	.013	.018	.018	.010
		.977	.066	.076	.081	.026

TABLE 6.- PRESSURE COEFFICIENTS FOR CONFIGURATION 222 - Continued

(a) $M = 0.40$ to 0.95 ; $\alpha = 0^\circ$ - Concluded

		C_p for -				
		$\beta = -60^\circ$				
		$M = 0.40$	$M = 0.70$	$M = 0.85$	$M = 0.90$	$M = 0.95$
Main stage	x/l	.345	.358	.406	.431	.468
		.255	.268	.314	.351	.389
		.119	.144	.207	.248	.294
		-1.155	-1.052	-1.041	-1.007	-0.941
		-.651	-.694	-.634	-.935	-.995
		-.378	-.512	-.554	-.580	-.898
		-.049	-.140	-.354	-.375	-.503
		.020	.016	-.125	-.163	-.130
		.066	.071	.038	.028	-.020
		.126	.126	.121	.140	.090
Transition Flare	x/l	.265	.252	.212	.232	.193
		.135	.134	.164	.201	.296
		.061	.067	.099	.130	.209
		.002	-.001	.031	.062	.138
		-.107	-.112	-.083	-.040	.042
		-.398	-.417	-.374	-.304	-.211
		-.456	-.512	-.422	-.795	-.667
		-.157	-.171	-.181	-.433	-.523
		-.101	-.107	-.112	-.106	-.445
		-.059	-.069	-.075	-.051	-.350
Upper stage	x/l	-.050	-.056	-.057	-.040	-.151
		-.040	-.043	-.046	-.037	-.036
		-.031	-.039	-.038	-.033	-.004
		-.022	-.026	-.031	-.026	.009
		-.012	-.020	-.015	-.021	.010
		-.008	-.015	-.011	-.016	.003
		-.003	-.010	-.008	-.012	.003
		-.001	-.009	-.005	-.008	.010
		.003	.003	.000	.005	.006
		.006	.001	.002	.003	.008
Lower stage	x/l	.001	.004	.006	.007	.011
		.817	.857	.877	.897	.917
		.777	.785	.777	.737	.697
		.677	.657	.677	.627	.607
		.617	.607	.607	.587	.568
		.577	.577	.567	.565	.565
		.517	.517	.517	.517	.517
		.456	.456	.456	.456	.456
		.398	.398	.398	.398	.398
		.345	.345	.345	.345	.345
Nose	x/l	.411	.436	.449	.488	.553
		.431	.241	.268	.314	.389
		.441	.119	.136	.204	.294
		.453	-1.253	-1.163	-1.092	-.997
		.473	-.049	-.131	-.347	-.496
		.493	.062	.067	.035	-.004
		.513	.274	.269	.223	.266
		.535	.061	.067	.103	.130
		.565	-.408	-.430	-.382	-.301
		.568	-.517	-.589	-.866	-.822
Main stage	x/l	.607	-.050	-.056	-.057	-.040
		.627	-.031	-.039	-.039	-.033
		.657	-.014	-.022	-.016	-.021
		.697	-.008	-.016	-.010	-.015
		.737	-.001	-.009	-.004	-.008
		.785	.002	.005	.002	.005
		.817	.008	.001	.001	.008
		.857	.002	-.004	-.005	-.007
		.897	-.001	-.007	-.008	-.010
		.917	-.012	-.018	-.020	-.026
	.957	-.012	-.018	-.020	-.026	
	.997	-.068	-.077	-.082	-.085	

TABLE 6.- PRESSURE COEFFICIENTS FOR CONFIGURATION 222 - Continued

(b) $M = 0.60$; $\alpha = -10^\circ$ to 10°

		C_p for -						
		$\beta = 0^\circ$						
		$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$
Main stage	$x/1$.631	.547	.484	.419	.353	.285	.213
	Nose	.411	.451	.388	.328	.257	.200	.123
Transition	$x/1$.421	.326	.263	.209	.138	.086	.016
	Late	.441	.297	.139	.090	.019	-.027	-.090
Upper stage	$x/1$.453	-1.246	-1.421	-1.419	-1.382	-1.224	-.923
	Upper stage	.458	-.235	-.414	-.470	-.549	-.601	-.617
Lower stage	$x/1$.473	-.079	-.136	-.192	-.242	-.317	-.425
	Lower stage	.483	.054	-.031	-.055	-.062	-.068	-.106
Nose	$x/1$.493	.101	.061	.044	.047	.042	.039
	Nose	.503	.170	.136	.113	.100	.094	.079
Main stage	$x/1$.513	.372	.286	.265	.221	.192	.148
	Main stage	.525	.244	.159	.132	.100	.077	.056
Transition	$x/1$.535	.170	.078	.052	.025	.002	-.020
	Late	.545	.118	.061	.005	-.021	-.051	-.067
Upper stage	$x/1$.555	-.049	-.055	-.077	-.110	-.134	-.143
	Upper stage	.565	-.251	-.308	-.344	-.363	-.352	-.338
Lower stage	$x/1$.568	-.436	-.517	-.503	-.490	-.455	-.429
	Lower stage	.577	-.085	-.125	-.149	-.162	-.167	-.160
Main stage	$x/1$.587	-.038	-.072	-.094	-.103	-.103	-.096
	Main stage	.597	.015	-.049	-.065	-.068	-.074	-.066
Transition	$x/1$.607	-.003	-.032	-.047	-.051	-.051	-.049
	Late	.617	.008	-.043	-.041	-.045	-.039	-.037
Upper stage	$x/1$.627	.008	-.032	-.030	-.033	-.033	-.025
	Upper stage	.637	.019	-.008	-.024	-.021	-.022	-.020
Lower stage	$x/1$.657	.026	-.016	-.012	-.016	-.016	-.010
	Lower stage	.677	.026	-.014	-.012	-.016	-.010	-.010
Main stage	$x/1$.697	.032	-.004	-.006	-.010	-.008	-.008
	Main stage	.737	.032	-.004	-.006	-.010	-.006	-.008
Transition	$x/1$.777	.036	-.010	-.006	-.004	-.004	-.004
	Late	.785	.042	-.000	-.002	-.001	-.000	-.004
Upper stage	$x/1$.815	.041	-.015	-.001	-.002	-.001	-.002
	Upper stage	.857	.034	-.010	-.004	-.004	-.005	-.005
Lower stage	$x/1$.877	.037	-.011	-.004	-.004	-.004	-.005
	Lower stage	.897	.034	-.006	-.003	-.007	-.008	-.011

		C_p for -						
		$\beta = -30^\circ$						
		$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$
Main stage	$x/1$.421	.428	.371	.322	.262	.200	.117
	Main stage	.431	.332	.269	.226	.166	.109	.038
Transition	$x/1$.441	.179	.122	.073	.024	-.027	-.096
	Late	.453	-1.345	-1.404	-1.419	-1.341	-1.283	-1.064
Upper stage	$x/1$.458	-.344	-.408	-.447	-.526	-.572	-.629
	Upper stage	.473	-.141	-.177	-.182	-.236	-.282	-.385
Lower stage	$x/1$.483	-.043	-.061	-.058	-.068	-.074	-.101
	Lower stage	.493	.009	-.003	-.006	-.004	-.010	-.014
Main stage	$x/1$.503	.055	.044	.052	.042	.036	.027
	Main stage	.513	.315	.286	.265	.233	.210	.171
Transition	$x/1$.525	.171	.147	.126	.100	.077	.044
	Late	.535	.107	.078	.052	.025	.002	-.031
Upper stage	$x/1$.545	.043	.009	-.006	-.033	-.063	-.090
	Upper stage	.555	-.043	-.073	-.083	-.127	-.151	-.179
Lower stage	$x/1$.565	.309	.385	.383	.393	.405	.433
	Lower stage	.568	-.389	-.435	-.445	-.443	-.449	-.435
Main stage	$x/1$.577	-.109	-.159	-.152	-.162	-.168	-.166
	Main stage	.587	-.068	-.078	-.094	-.103	-.103	-.107
Transition	$x/1$.597	-.033	-.049	-.063	-.062	-.063	-.080
	Late	.607	-.027	-.037	-.047	-.051	-.057	-.053
Upper stage	$x/1$.617	-.015	-.032	-.043	-.045	-.045	-.043
	Upper stage	.627	-.015	-.026	-.037	-.030	-.033	-.037
Lower stage	$x/1$.637	-.009	-.020	-.024	-.021	-.027	-.025
	Lower stage	.657	.000	-.014	-.016	-.019	-.022	-.047
Main stage	$x/1$.677	.010	-.002	-.006	-.012	-.016	-.023
	Main stage	.697	.007	-.008	-.014	-.012	-.016	-.027
Transition	$x/1$.737	.007	-.002	-.002	-.008	-.010	-.027
	Late	.777	.016	.004	.002	.002	.008	.029
Upper stage	$x/1$.815	.014	.004	.002	.002	.006	.025
	Upper stage	.857	.016	.005	.002	.002	.007	.028
Lower stage	$x/1$.877	.009	.000	-.002	-.002	-.007	-.028
	Lower stage	.897	.006	-.001	-.003	-.003	-.007	-.029
Main stage	$x/1$.917	.006	-.004	-.004	-.010	-.018	-.033
	Main stage	.957	-.009	-.017	-.022	-.015	-.020	-.044
Transition	$x/1$.997	-.089	-.081	-.068	-.068	-.091	-.117
	Late							

TABLE 6.- PRESSURE COEFFICIENTS FOR CONFIGURATION 222 - Continued

(b) $M = 0.60$; $\alpha = -1.5^\circ$ to 10° - Concluded

		C_p for -						
		$\beta = -50^\circ$						
x/l		$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$
		.421	Nose	.365	.360	.343	.317	.279
.285	.269			.241	.220	.183	.143	.055
.431	Nose	.155	.134	.105	.085	.047	.002	-.066
.441		-1.299	-1.419	-1.429	-1.453	-1.445	-1.445	-1.591
.458	Upper stage	.345	.368	.397	.412	.462	.485	.536
.463		.166	.182	.174	.201	.219	.275	.275
.473	Upper stage	.090	.072	.066	.058	.068	.085	.135
.483		.038	.014	.014	.000	.010	.027	.077
.493	Upper stage	.014	.032	.038	.052	.037	.025	-.025
.503		.078	.102	.107	.115	.106	.088	.033
.513	Upper stage	.268	.281	.269	.265	.245	.221	.160
.525		.083	.113	.118	.121	.094	.065	.004
.535	Flare	.054	.067	.061	.052	.025	.004	-.055
.545		.008	.009	.003	.006	.033	.063	.114
.555	Transition	.100	.089	.090	.106	.117	.146	.192
.565		.380	.379	.385	.383	.393	.422	.461
.568	Transition	.430	.429	.435	.421	.431	.449	.482
.577		.167	.154	.155	.152	.162	.174	.207
.587	Main stage	.126	.108	.102	.094	.103	.115	.148
.597		.097	.072	.073	.059	.068	.080	.119
.607	Main stage	.085	.061	.055	.047	.056	.068	.101
.617		.079	.055	.043	.035	.045	.057	.090
.627	Main stage	.074	.049	.038	.030	.039	.051	.082
.637		.068	.037	.032	.024	.027	.045	.072
.657	Main stage	.060	.034	.028	.014	.023	.039	.060
.677		.048	.026	.022	.010	.019	.034	.060
.697	Main stage	.037	.018	.016	.004	.010	.029	.053
.737		.046	.024	.018	.004	.010	.025	.045
.777	Main stage	.048	.022	.014	.000	.008	.020	.035
.785		.046	.020	.014	.002	.006	.015	.030
.817	Main stage	.041	.015	.009	.003	.005	.015	.030
.857		.046	.020	.013	.002	.008	.018	.032
.877	Main stage	.044	.020	.013	.002	.009	.018	.030
.897		.046	.023	.014	.002	.009	.019	.036
.917	Main stage	.034	.029	.021	.007	.014	.024	.046
.957		.063	.033	.026	.015	.023	.031	.063
.997	Main stage	.124	.097	.086	.069	.082	.098	.123
		.086	.069	.059	.046	.051	.063	.086

TABLE 6.- PRESSURE COEFFICIENTS FOR CONFIGURATION 222 - Continued

(c) $M = 0.80$; $\alpha = -10^\circ$ to 10°

		C_p for $\beta = 0^\circ$							
		$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$	
x/l	None	.411	.692	.601	.539	.474	.411	.345	.271
		.421	.597	.514	.447	.387	.319	.254	.183
None	None	.431	.480	.400	.337	.278	.215	.152	.090
		.441	.364	.285	.227	.170	.110	.056	-.003
Upper stage	None	.453	-1.357	-1.412	-1.350	-1.196	-0.907	-0.702	-.508
		.458	.734	.757	.742	.703	.608	.531	.444
Upper stage	None	.473	.003	.047	-.532	-.551	-.530	-.500	-.456
		.483	.042	.035	-.146	-.259	-.328	-.367	-.366
Upper stage	None	.493	.096	.081	-.029	-.109	-.188	-.198	-.198
		.503	.182	.159	.084	.068	.023	-.036	-.054
Transition	None	.513	.395	.349	.305	.239	.171	.112	.098
		.525	.246	.232	.196	.157	.116	.084	.074
Transition	None	.535	.200	.147	.114	.076	.050	.022	.001
		.545	.146	.093	.060	.022	-.016	-.040	-.039
Transition	None	.555	.069	.015	-.029	-.073	-.107	-.130	-.130
		.565	-.286	-.245	-.382	-.413	-.388	-.361	-.328
Main stage	None	.568	.823	.878	.843	.698	.558	.480	.428
		.577	.127	.158	.167	.182	.189	.185	.165
Main stage	None	.587	-.064	-.087	-.096	-.112	-.118	-.123	-.098
		.597	.036	-.059	-.049	-.076	-.083	-.087	-.066
Main stage	None	.607	.021	-.039	-.049	-.057	-.063	-.067	-.047
		.617	.013	-.032	-.037	-.045	.051	-.056	.035
Main stage	None	.627	.001	-.020	-.029	-.037	-.043	-.044	.027
		.637	.006	-.012	-.017	-.029	-.031	-.036	.015
Main stage	None	.657	.016	-.005	-.011	-.020	-.024	-.026	.009
		.677	.018	-.003	-.010	-.019	-.021	-.023	.007
Main stage	None	.697	.022	.001	-.008	-.015	-.017	-.019	.005
		.717	.028	.008	.001	-.003	-.012	-.014	-.006
Main stage	None	.737	.036	.013	.006	-.007	-.010	-.014	.003
		.755	.035	.015	.006	-.003	-.008	-.008	.005
Main stage	None	.817	.036	.015	.007	-.002	-.005	-.011	.001
		.857	.029	.010	.004	-.005	-.009	-.016	.010
Main stage	None	.877	.032	.011	.004	-.004	-.009	-.016	.010
		.897	.027	.007	.001	-.001	-.007	-.019	.015
Main stage	None	.917	.001	-.001	-.001	-.004	-.004	-.004	.014
		.957	.014	-.016	-.016	-.016	-.016	-.016	-.026
Main stage	None	.997	-.095	-.082	-.082	-.082	-.082	-.082	-.108
		.551	.487	.440	.379	.319	.258	.179	
		.463	.400	.345	.291	.236	.182	.115	
		.372	.259	.211	.162	.114	.056	.003	
		-1.321	-1.329	-1.314	-1.121	-.922	-.710	-.611	
		-.667	-.714	-.688	-.676	-.620	-.535	-.479	
		-.285	-.472	-.544	-.555	-.538	-.504	-.471	
		.873	.873	.873	.873	.873	.873	.873	
		.019	.027	.022	-.029	-.098	-.184	-.195	
		.069	.070	.068	.068	.031	-.036	-.054	
		.158	.155	.154	.134	.105	-.054	-.043	
		.368	.342	.305	.235	.178	.127	.121	
		.228	.209	.184	.157	.116	.084	.059	
		.173	.139	.111	.076	.050	.022	.001	
		.111	.070	.041	.006	-.020	-.048	-.071	
		.555	.555	.555	.555	.555	.555	.555	
		.329	.376	.409	.429	.416	.432	.459	
		.874	.913	.951	.986	.974	.967	.950	
		.150	.161	.167	.182	.185	.165	.165	
		.095	.098	.104	.112	.122	.126	.110	
		.048	.055	.053	.060	.067	.071	.055	
		.044	.051	.049	.045	.063	.067	.055	
		.036	.039	.037	.045	.051	.056	.043	
		.028	.032	.033	.037	.043	.048	.043	
		.021	.024	.025	.029	.031	.040	.035	
		.013	.017	.017	.024	.026	.033	.024	
		.001	.005	.006	.013	.017	.024	.024	
		.003	.008	.010	.015	.018	.024	.021	
		.001	.005	.010	.015	.018	.024	.021	
		.777	.777	.777	.777	.777	.777	.777	
		.010	.004	.002	.003	.008	.016	.019	
		.007	.007	.007	.007	.007	.007	.007	
		.009	.003	.004	.004	.006	.016	.021	
		.857	.857	.857	.857	.857	.857	.857	
		.001	.002	.002	.002	.002	.002	.002	
		.897	.897	.897	.897	.897	.897	.897	
		.001	.004	.004	.004	.004	.004	.004	
		.957	.957	.957	.957	.957	.957	.957	
		.014	.016	.014	.014	.014	.014	.014	
		.076	.076	.076	.076	.076	.076	.076	

TABLE 6.- PRESSURE COEFFICIENTS FOR CONFIGURATION 222 - Continued

(c) $M = 0.80$; $\alpha = -10^\circ$ to 10° - Concluded

		C_p for -						
		$\beta = -60^\circ$						
		$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$
x/l	Nose	.421	.422	.405	.379	.338	.288	.202
		.342	.335	.318	.288	.247	.201	.126
		.224	.213	.196	.170	.137	.094	.027
		-1.301	-1.234	-1.129	-1.007	-.926	-.805	-.753
		-.706	-.722	-.707	-.672	-.667	-.582	-.565
		.531	.554	-.559	-.559	-.73	-.543	-.530
		.079	-.129	-.193	-.259	-.289	-.363	-.358
		-.048	.008	.010	-.025	-.062	-.149	-.159
		.007	.058	.080	.072	.050	-.075	.493
		.088	.142	.130	.130	.113	.077	.032
		.286	.314	.282	.239	.210	.193	.167
		.108	.147	.157	.146	.116	.077	.012
		.080	.097	.095	.076	.050	.022	-.039
		.026	.039	.029	.006	-.016	-.048	-.099
		-.079	-.066	-.072	-.089	-.111	-.140	-.188
		.381	.384	-.406	-.417	-.431	-.460	-.495
		.945	.944	-.843	-.643	-.649	-.846	-.908
		.209	.177	-.175	-.178	-.185	-.193	-.208
		.158	.122	.108	.116	.122	.134	.149
		-.123	-.091	-.073	-.076	-.083	-.103	-.118
		.103	.071	.053	.057	.063	.083	.094
		-.095	-.059	-.045	-.045	-.051	-.067	-.086
		-.091	-.055	-.037	-.037	-.043	-.064	-.078
		-.040	-.047	-.039	-.029	-.035	-.056	-.074
		-.073	-.038	-.021	-.022	-.029	-.047	-.061
		-.061	-.030	-.016	-.017	-.024	-.043	-.053
		-.048	-.021	-.010	-.012	-.020	-.039	-.046
		-.059	-.025	-.010	-.011	-.017	-.032	-.038
		-.055	-.020	-.006	-.005	-.012	-.027	-.028
		-.059	-.025	-.007	-.004	-.008	-.024	-.028
		-.049	-.016	-.001	-.001	-.008	-.024	-.026
		-.054	-.020	-.005	-.005	-.011	-.027	-.027
		-.053	-.022	-.006	-.006	-.012	-.027	-.027
		-.055	-.023	-.007	-.007	-.013	-.028	-.028
		-.061	-.029	-.013	-.012	-.019	-.033	-.031
		-.067	-.036	-.019	-.020	-.027	-.043	-.043
		-.135	-.104	-.083	-.080	-.090	-.113	-.123

		C_p for -						
		$\beta = -90^\circ$						
		$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$
x/l	Nose	.411	.445	.470	.467	.456	.429	.358
		.212	.266	.284	.284	.270	.250	.198
		.106	.148	.170	.170	.156	.140	.096
		-1.258	-1.203	-1.180	-1.125	-1.115	-1.116	-1.072
		-.235	-.222	-.228	-.255	-.265	-.278	-.249
		-.048	.035	.064	.072	.058	.007	-.054
		.224	.260	.254	.247	.256	.244	.202
		-.005	.058	.076	.076	.066	.038	-.023
		-.476	-.436	-.437	-.425	-.439	-.452	-.479
		-1.019	-.972	-.800	-.729	-.834	-.968	-.995
		-.190	-.134	-.116	-.116	-.122	-.150	-.188
		-.138	-.083	-.057	-.057	-.063	-.095	-.133
		-.119	-.059	-.037	-.037	-.043	-.071	-.114
		-.103	-.050	-.027	-.022	-.033	-.060	-.099
		-.097	-.043	-.019	-.016	-.026	-.053	-.092
		-.088	-.036	-.011	-.009	-.018	-.045	-.080
		-.082	-.033	-.008	-.007	-.014	-.040	-.073
		-.085	-.033	-.008	-.005	-.013	-.039	-.072
		-.073	-.023	-.002	-.001	-.008	-.033	-.067
		-.077	-.030	-.006	-.005	-.013	-.039	-.070
		-.079	-.033	-.010	-.007	-.016	-.043	-.072
	Main stage	.627	.657	.627	.607	.587	.565	.568
	Transition	.565	.568	.587	.607	.627	.657	.697
	Plate	.431	.437	.437	.437	.437	.437	.437

TABLE 1.- PRESSURE COEFFICIENTS FOR CONFIGURATION 222 - Continued

(a) $M = 1.00$; $\alpha = -10^\circ$ to 10°

		C_p for $\beta = 0^\circ$					
		$\alpha = -10^\circ$	$\alpha = -5^\circ$	$\alpha = 0^\circ$	$\alpha = 5^\circ$	$\alpha = 10^\circ$	$\alpha = 10^\circ$
x, z	Nose	.411	.729	.609	.548	.492	.409
		.421	.646	.530	.470	.407	.331
	Main stage	.431	.552	.445	.387	.329	.257
		.441	.459	.361	.303	.250	.183
	Upper stage	.453	.483	.452	.412	.380	.349
		.458	.479	.475	.466	.458	.458
	Transition	.463	.454	.470	.420	.377	.325
		.473	.441	.459	.441	.426	.426
	Flare	.483	.317	.381	.200	.273	.355
		.493	.242	.304	.104	.208	.271
	Main stage	.503	.163	.160	.032	.112	.152
		.513	.406	.254	.118	.009	.051
x, z	Nose	.525	.399	.306	.195	.104	.066
		.535	.319	.261	.204	.144	.112
	Main stage	.545	.291	.244	.184	.125	.100
		.555	.216	.166	.104	.055	.035
	Transition	.565	.027	.050	-.178	-.211	-.222
		.568	.513	.570	.568	.510	.545
	Flare	.577	.75	.407	.411	.357	.367
		.587	.39	.356	.374	.347	.345
	Main stage	.597	.173	.244	.324	.310	.283
		.607	.148	.210	.258	.238	.205
	Transition	.617	.135	.200	.193	.179	.158
		.627	.119	.166	.140	.136	.120
	Flare	.637	.108	.128	.108	.107	.098
		.647	.087	.088	.075	.076	.069
	Main stage	.657	.069	.076	.065	.067	.060
		.667	.059	.063	.052	.057	.041
	Transition	.677	.041	.055	.023	.034	.018
		.687	.030	.041	.014	.004	.005
	Flare	.697	.016	.024	.023	.016	.012
		.707	.000	.009	.025	.018	.017
	Main stage	.717	.000	.009	.025	.019	.012
		.727	.000	.009	.025	.019	.011
	Transition	.737	.000	.009	.025	.019	.003
		.747	.000	.009	.025	.019	.003
	Flare	.757	.000	.009	.025	.019	.003
		.767	.000	.009	.025	.019	.003
	Main stage	.777	.000	.009	.025	.019	.003
		.787	.000	.009	.025	.019	.003
	Transition	.797	.000	.009	.025	.019	.003
		.807	.000	.009	.025	.019	.003
	Flare	.817	.000	.009	.025	.019	.003
		.827	.000	.009	.025	.019	.003
	Main stage	.837	.000	.009	.025	.019	.003
		.847	.000	.009	.025	.019	.003
	Transition	.857	.000	.009	.025	.019	.003
		.867	.000	.009	.025	.019	.003
	Flare	.877	.000	.009	.025	.019	.003
		.887	.000	.009	.025	.019	.003
	Main stage	.897	.000	.009	.025	.019	.003
		.907	.000	.009	.025	.019	.003
	Transition	.917	.000	.009	.025	.019	.003
		.927	.000	.009	.025	.019	.003
	Flare	.937	.000	.009	.025	.019	.003
		.947	.000	.009	.025	.019	.003
	Main stage	.957	.000	.009	.025	.019	.003
		.967	.000	.009	.025	.019	.003
	Transition	.977	.000	.009	.025	.019	.003
		.987	.000	.009	.025	.019	.003
	Flare	.997	.000	.009	.025	.019	.003

TABLE 1.- PRESSURE COEFFICIENTS FOR CONFIGURATION 222 - Continued

(a) $M = 1.00$; $\alpha = -10^\circ$ to 10° - Concluded

		C_p for $\beta = -5^\circ$							C_p for $\beta = -10^\circ$						
		$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$	$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$
None	x/l	.421	.570	.550	.524	.488	.437	.352	.411	.528	.604	.603	.588	.564	.497
		.431	.561	.477	.448	.412	.371	.285	.431	.380	.422	.444	.436	.413	.355
		.441	.467	.394	.361	.328	.288	.204	.441	.298	.338	.360	.349	.332	.273
		.453	.411	.805	.806	.810	.817	.828	.453	.755	.746	.703	.700	.714	.762
		.459	.806	.849	.866	.891	.911	.918							
		.463	.842	.779	.779	.820	.836	.689							
		.473	.437	.512	.587	.618	.576	.423	.473	.499	.567	.590	.594	.589	.506
		.483	.329	.385	.415	.426	.448	.327	.493	.274	.140	.069	.095	.149	.221
		.493	.230	.198	.085	.052	.171	.228	.513	.212	.256	.251	.251	.243	.199
		.503	.095	.135	.148	.060	.041	.101							
Upper stage	x/l	.332	.332	.302	.247	.171	.113	.051							
		.211	.282	.311	.306	.281	.196	.072							
		.235	.187	.224	.241	.223	.159	.048	.535	.082	.181	.231	.229	.171	.066
		.345	.147	.178	.188	.164	.110	.020							
		.555	.101	.126	.134	.103	.056	.029							
		.565	.076	.067	.109	.112	.139	.193	.565	.174	.120	.112	.103	.123	.168
		.568	.563	.547	.547	.571	.591	.633	.568	.629	.594	.573	.574	.591	.626
		.577	.472	.472	.469	.496	.535	.589	.587	.447	.397	.389	.405	.432	.470
		.587	.363	.373	.378	.405	.463	.517	.607	.363	.285	.255	.252	.297	.373
		.597	.297	.304	.314	.311	.325	.383							
Transition Lift	x/l	.607	.276	.263	.255	.249	.247	.281							
		.617	.266	.232	.203	.196	.201	.214							
		.627	.263	.191	.169	.155	.163	.183	.627	.254	.182	.158	.155	.179	.248
		.637	.232	.157	.134	.127	.141	.167	.657	.190	.120	.093	.092	.179	.189
		.657	.172	.118	.094	.084	.108	.134							
		.677	.141	.092	.076	.072	.095	.113							
		.697	.109	.066	.059	.059	.082	.091	.697	.150	.081	.065	.066	.099	.167
		.737	.107	.020	.047	.030	.059	.053	.737	.125	.029	.042	.035	.078	.105
		.777	.071	.000	.009	.013	.019	.036	.777	.089	.010	.006	.005	.025	.080
		.785	.066	.001	.005	.016	.006	.031	.785	.087	.010	.006	.004	.015	.069
Main stage	x/l	.817	.039	.011	.022	.022	.001	.011							
		.857	.027	.003	.019	.020	.007	.007	.817	.054	.003	.022	.018	.022	.044
		.877	.020	.002	.018	.022	.019	.008	.857	.044	.006	.021	.018	.005	.042
		.897	.020	.003	.016	.019	.005	.009	.897	.039	.013	.012	.013	.008	.047
		.917	.025	.012	.009	.015	.001	.011							
		.957	.024	.015	.003	.006	.013	.022							
		.997	.098	.089	.103	.112	.137	.154							

TABLE 6.- PRESSURE COEFFICIENTS FOR CONFIGURATION 222 - Continued

(e) $M = 1.20$; $\alpha = -10^\circ$ to 10°

x/t	C_p for $\beta = 0^\circ$					x/t	C_p for $\beta = -30^\circ$				
	$\alpha = -10^\circ$	$\alpha = -5^\circ$	$\alpha = 0^\circ$	$\alpha = 5^\circ$	$\alpha = 10^\circ$		$\alpha = -10^\circ$	$\alpha = -5^\circ$	$\alpha = 0^\circ$	$\alpha = 5^\circ$	$\alpha = 10^\circ$
	Main stage	.896	.802	.672	.614		.558	.484	.421	.300	.263
Transition Flare	.833	.745	.568	.511	.457	.427	.431	.254	.236	.210	.169
	.783	.682	.511	.460	.410	.382	.441	.218	.198	.179	.153
Upper stage	.694	.619	.516	.452	.410	.336	.453	.202	.173	.152	.115
	.594	.517	.410	.350	.322	.299	.424	.182	.163	.146	.115
Main stage	.410	.470	.532	.550	.566	.587	.458	.290	.269	.244	.202
	.379	.470	.532	.550	.566	.587	.458	.290	.269	.244	.202
Upper stage	.279	.371	.463	.495	.527	.551	.463	.316	.290	.263	.220
	.126	.231	.345	.393	.431	.471	.473	.316	.290	.263	.220
Transition Flare	.053	.148	.248	.294	.329	.369	.483	.334	.313	.289	.244
	.023	.104	.214	.260	.293	.333	.493	.341	.321	.297	.252
Main stage	.021	.085	.138	.183	.224	.264	.503	.353	.333	.308	.263
	.359	.294	.241	.206	.161	.096	.513	.353	.333	.308	.263
Transition Flare	.383	.348	.298	.260	.220	.167	.525	.363	.343	.318	.273
	.327	.290	.254	.215	.186	.137	.535	.375	.355	.330	.285
Main stage	.332	.277	.232	.208	.193	.169	.545	.384	.364	.339	.294
	.343	.282	.237	.213	.198	.173	.555	.394	.374	.349	.304
Transition Flare	.214	.173	.101	.042	.001	.031	.565	.403	.383	.358	.313
	.230	.252	.287	.305	.321	.336	.575	.413	.393	.368	.323
Main stage	.143	.188	.231	.241	.229	.217	.587	.423	.403	.378	.333
	.086	.138	.190	.202	.201	.209	.597	.433	.413	.388	.343
Transition Flare	.062	.108	.153	.169	.179	.189	.607	.443	.423	.398	.353
	.037	.086	.131	.144	.149	.159	.617	.453	.433	.408	.363
Main stage	.034	.077	.115	.119	.118	.114	.627	.463	.443	.418	.373
	.024	.069	.109	.109	.108	.106	.637	.473	.453	.428	.383
Transition Flare	.013	.055	.095	.094	.090	.086	.647	.483	.463	.438	.393
	.016	.048	.087	.087	.086	.084	.657	.493	.473	.448	.403
Main stage	.016	.048	.087	.087	.086	.084	.667	.503	.483	.458	.413
	.015	.026	.060	.067	.063	.053	.677	.513	.493	.468	.423
Transition Flare	.004	.031	.030	.019	.023	.020	.687	.523	.503	.478	.433
	.014	.022	.033	.025	.024	.010	.697	.533	.513	.488	.443
Main stage	.019	.011	.021	.025	.025	.009	.707	.543	.523	.498	.453
	.011	.004	.013	.016	.012	.003	.717	.553	.533	.508	.463
Transition Flare	.028	.004	.021	.024	.024	.003	.727	.563	.543	.518	.473
	.025	.000	.021	.024	.024	.004	.737	.573	.553	.528	.483
Main stage	.025	.011	.021	.024	.024	.004	.747	.583	.563	.538	.493
	.025	.011	.021	.024	.024	.004	.757	.593	.573	.548	.503
Transition Flare	.033	.011	.021	.024	.024	.007	.767	.603	.583	.558	.513
	.033	.011	.021	.024	.024	.007	.777	.613	.593	.568	.523
Main stage	.015	.001	.004	.009	.014	.017	.787	.623	.603	.578	.533
	.015	.001	.004	.009	.014	.017	.797	.633	.613	.588	.543
Transition Flare	.015	.001	.004	.009	.014	.017	.807	.643	.623	.598	.553
	.015	.001	.004	.009	.014	.017	.817	.653	.633	.608	.563
Main stage	.015	.001	.004	.009	.014	.017	.827	.663	.643	.618	.573
	.015	.001	.004	.009	.014	.017	.837	.673	.653	.628	.583
Transition Flare	.015	.001	.004	.009	.014	.017	.847	.683	.663	.638	.593
	.015	.001	.004	.009	.014	.017	.857	.693	.673	.648	.603
Main stage	.015	.001	.004	.009	.014	.017	.867	.703	.683	.658	.613
	.015	.001	.004	.009	.014	.017	.877	.713	.693	.668	.623
Transition Flare	.015	.001	.004	.009	.014	.017	.887	.723	.703	.678	.633
	.015	.001	.004	.009	.014	.017	.897	.733	.713	.688	.643
Main stage	.015	.001	.004	.009	.014	.017	.907	.743	.723	.698	.653
	.015	.001	.004	.009	.014	.017	.917	.753	.733	.708	.663
Transition Flare	.015	.001	.004	.009	.014	.017	.927	.763	.743	.718	.673
	.015	.001	.004	.009	.014	.017	.937	.773	.753	.728	.683
Main stage	.015	.001	.004	.009	.014	.017	.947	.783	.763	.738	.693
	.015	.001	.004	.009	.014	.017	.957	.793	.773	.748	.703
Transition Flare	.015	.001	.004	.009	.014	.017	.967	.803	.783	.758	.713
	.015	.001	.004	.009	.014	.017	.977	.813	.793	.768	.723
Main stage	.015	.001	.004	.009	.014	.017	.987	.823	.803	.778	.733
	.015	.001	.004	.009	.014	.017	.997	.833	.813	.788	.743

TABLE 5.- PRESSURE COEFFICIENTS FOR CONFIGURATION 222 - Concluded

(e) $M = 1.20$; $\alpha = -10^\circ$ to 10° - Concluded

		C_p for -						
		$\beta = -5^\circ$						
		$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -5^\circ$	$\alpha = 0^\circ$	$\alpha = 5^\circ$	$\alpha = 10^\circ$	
Nozzle	x/l	.411	.602	.651	.664	.657	.634	.578
		.431	.494	.546	.567	.557	.537	.479
		.441	.439	.492	.510	.501	.483	.425
		.453	.415	.364	.351	.356	.374	.426
Upper stage	x/l	.473	.324	.333	.345	.346	.346	.345
		.493	.233	.206	.191	.195	.208	.248
		.513	.145	.209	.241	.234	.211	.129
Transition	x/l	.535	.132	.211	.257	.241	.201	.117
		.565	.036	.077	.092	.085	.078	.027
		.568	.333	.302	.276	.283	.296	.331
Main stage	x/l	.587	.254	.219	.190	.200	.224	.273
		.607	.219	.161	.131	.141	.165	.225
		.627	.200	.116	.095	.099	.121	.200
		.657	.149	.075	.041	.048	.080	.143
		.697	.140	.078	.039	.051	.072	.141
		.737	.112	.063	.033	.033	.062	.119
		.777	.079	.046	.017	.024	.049	.099
		.785	.086	.049	.014	.021	.046	.101
		.817	.078	.028	.010	.018	.039	.087
		.857	.078	.029	.011	.029	.048	.086
	.897	.084	.039	.006	.007	.025	.073	
Nozzle	x/l	.421	.665	.662	.615	.591	.542	.452
		.431	.617	.611	.569	.543	.491	.406
		.441	.552	.552	.510	.479	.443	.358
		.453	.491	.459	.441	.462	.455	.365
		.458	.488	.495	.458	.489	.469	.390
		.463	.378	.418	.474	.501	.514	.537
		.473	.236	.283	.339	.360	.376	.405
		.483	.174	.209	.257	.301	.318	.331
		.493	.144	.162	.191	.219	.235	.281
		.503	.126	.126	.133	.147	.147	.110
Upper stage	x/l	.513	.207	.239	.235	.212	.183	.115
		.525	.217	.274	.292	.266	.223	.134
		.535	.214	.249	.254	.236	.196	.115
		.545	.196	.217	.218	.198	.171	.104
		.555	.196	.214	.213	.193	.167	.118
		.565	.118	.129	.098	.072	.054	.008
		.568	.273	.258	.270	.277	.301	.336
		.577	.241	.236	.231	.247	.274	.328
		.587	.192	.191	.190	.205	.235	.295
		.597	.156	.149	.153	.163	.190	.248
Transition	x/l	.607	.140	.133	.128	.141	.157	.198
		.617	.140	.122	.109	.116	.132	.167
		.627	.140	.108	.095	.102	.118	.145
		.637	.119	.086	.078	.080	.096	.125
		.657	.115	.057	.039	.042	.065	.101
		.677	.105	.057	.038	.041	.056	.090
		.697	.094	.057	.037	.040	.047	.079
		.737	.052	.051	.029	.031	.049	.060
		.777	.059	.059	.015	.023	.036	.050
		.817	.052	.037	.009	.018	.027	.049
Main stage	x/l	.857	.051	.024	.016	.016	.031	.048
		.877	.051	.024	.004	.004	.021	.041
		.897	.051	.027	.000	.003	.016	.032
		.917	.066	.030	.007	.008	.020	.028
		.957	.067	.035	.016	.019	.031	.031
		.997	.056	.047	.055	.069	.089	.103

TABLE 7.- PRESSURE COEFFICIENTS FOR CONFIGURATION 322

(a) $M = 0.40$ to 0.95 ; $\alpha = 0^\circ$

		C_p for -				
		$\beta = -30^\circ$				
x/l	Stage	$M = 0.40$	$M = 0.70$	$M = 0.85$	$M = 0.90$	$M = 0.95$
			Nose	.426	.475	.554
	Upper stage	.436	.475	.575	.629	.694
		.446	.475	.575	.629	.694
		.453	.475	.575	.629	.694
	Transition	.458	.475	.575	.629	.694
		.463	.475	.575	.629	.694
		.473	.475	.575	.629	.694
	Main stage	.483	.475	.575	.629	.694
		.493	.475	.575	.629	.694
		.503	.475	.575	.629	.694
		.513	.475	.575	.629	.694
		.525	.475	.575	.629	.694
		.535	.475	.575	.629	.694
		.545	.475	.575	.629	.694
		.555	.475	.575	.629	.694
		.565	.475	.575	.629	.694
		.577	.475	.575	.629	.694
	.587	.475	.575	.629	.694	
	.597	.475	.575	.629	.694	
	.607	.475	.575	.629	.694	
	.617	.475	.575	.629	.694	
	.627	.475	.575	.629	.694	
	.637	.475	.575	.629	.694	
	.647	.475	.575	.629	.694	
	.657	.475	.575	.629	.694	
	.667	.475	.575	.629	.694	
	.677	.475	.575	.629	.694	
	.687	.475	.575	.629	.694	
	.697	.475	.575	.629	.694	
	.707	.475	.575	.629	.694	
	.717	.475	.575	.629	.694	
	.727	.475	.575	.629	.694	
	.737	.475	.575	.629	.694	
	.747	.475	.575	.629	.694	
	.757	.475	.575	.629	.694	
	.767	.475	.575	.629	.694	
	.777	.475	.575	.629	.694	
	.785	.475	.575	.629	.694	
	.817	.475	.575	.629	.694	
	.857	.475	.575	.629	.694	
	.877	.475	.575	.629	.694	
	.897	.475	.575	.629	.694	
	.917	.475	.575	.629	.694	
	.937	.475	.575	.629	.694	
	.957	.475	.575	.629	.694	
	.977	.475	.575	.629	.694	
	.997	.475	.575	.629	.694	

TABLE 7.- PRESSURE COEFFICIENTS FOR CONFIGURATION 222 - Continued

(a) $M = 0.40$ to 0.95 ; $\alpha = 0^\circ$ - Concluded

		C_p for -				
		$\beta = -60^\circ$				
		$M = 0.40$	$M = 0.70$	$M = 0.85$	$M = 0.90$	$M = 0.95$
Nose	x/l	.475	.554	.575	.625	.654
		.308	.393	.416	.478	.512
Upper stage	x/l	-1.495	-1.277	-1.277	-1.277	-1.016
		.458	.742	.700	.738	.688
Upper stage	x/l	.473	.623	.642	.558	.515
		.483	.289	.375	.454	.464
Transition	x/l	.493	.042	.137	.181	.185
		.503	.043	.022	.101	.167
Transition	x/l	.513	.114	.101	.056	.067
		.236	.214	.196	.070	.074
Transition	x/l	.100	.131	.138	.148	.129
		.032	.068	.080	.112	.112
Transition	x/l	.013	.004	.013	.055	.079
		.106	.103	.096	.060	.015
Transition	x/l	.337	.354	.355	.322	.283
		.380	.412	.433	.523	.519
Transition	x/l	.140	.153	.159	.161	.165
		.094	.098	.104	.110	.111
Transition	x/l	.071	.065	.066	.074	.073
		.048	.042	.054	.045	.046
Transition	x/l	.036	.042	.041	.045	.046
		.036	.033	.037	.038	.036
Transition	x/l	.025	.024	.028	.031	.029
		.021	.014	.014	.021	.010
Transition	x/l	.017	.010	.010	.016	.008
		.013	.005	.005	.011	.009
Transition	x/l	.010	.004	.003	.009	.012
		.010	.001	.002	.004	.011
Transition	x/l	.006	.001	.000	.004	.008
		.004	.004	.002	.001	.002
Transition	x/l	.009	.001	.004	.007	.007
		.009	.002	.004	.007	.008
Transition	x/l	.010	.002	.005	.008	.008
		.013	.007	.010	.013	.014
Transition	x/l	.022	.015	.018	.021	.023
		.074	.072	.075	.085	.089
Main stage	x/l	.426	.475	.549	.622	.654
		.446	.075	.187	.225	.344
Main stage	x/l	.453	-1.277	-0.802	-0.733	-0.619
		.473	-0.048	-0.344	-0.450	-0.471
Main stage	x/l	.493	.043	.063	.018	-0.299
		.513	.236	.218	.196	-0.059
Main stage	x/l	.535	.032	.072	.084	.099
		.565	.348	.363	.363	.279
Main stage	x/l	.568	.392	.453	.483	.502
		.587	.094	.102	.104	.111
Main stage	x/l	.607	.048	.051	.054	.056
		.627	.036	.033	.037	.036
Main stage	x/l	.657	.025	.016	.014	.021
		.697	.013	.008	.007	.014
Main stage	x/l	.737	.010	.004	.003	.009
		.777	.010	.001	.002	.005
Main stage	x/l	.785	.006	.001	.002	.005
		.817	.004	.005	.003	.000
Main stage	x/l	.857	.009	.009	.002	.007
		.897	.010	.003	.006	.009
Main stage	x/l	.917	.013	.007	.010	.017
		.997	.022	.015	.018	.021
Main stage	x/l	.997	.074	.072	.075	.089
		.694	.394	-1.074	.694	.694

TABLE 7.- PRESSURE COEFFICIENTS FOR CONFIGURATION 322 - Continued

(b) M = 0.60; $\alpha = -10^\circ$ to 10°

x/l	C_p for $\beta = 0^\circ$						x/l	C_p for $\beta = -30^\circ$							
	$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -5^\circ$	$\alpha = 0^\circ$	$\alpha = 5^\circ$	$\alpha = 10^\circ$		$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -5^\circ$	$\alpha = 0^\circ$	$\alpha = 5^\circ$	$\alpha = 10^\circ$		
	Rose														
Upper stage	.728	.648	.590	.522	.457	.384	.281	.426	.688	.620	.573	.527	.462	.390	.287
Upper stage	.576	.479	.427	.369	.293	.238	.140	.436	.497	.419	.376	.333	.274	.221	.132
Upper stage	.333	.236	.184	.127	.068	.029	-.035	.446	.305	.219	.178	.138	.085	.052	-.024
Upper stage	-1.558	-1.489	-1.344	-1.258	-1.115	-0.910	-.677	.453	-1.388	-1.290	-1.169	-1.007	-.747	-.583	-.525
Upper stage	.458	.555	.810	.846	.768	.727	.578	.458	.519	.722	.787	.834	.710	.594	.549
Upper stage	.463	.419	.262	.419	.485	.623	.624	.463	.149	.324	.458	.551	.670	.611	.595
Upper stage	.473	.041	.048	-.072	-.144	-.247	-.381	.473	-.034	-.041	-.054	-.084	-.179	-.322	-.404
Upper stage	.483	.041	.004	-.003	-.011	-.051	-.127	.483	.018	.011	.016	.049	-.068	-.145	.145
Upper stage	.493	.093	.056	.043	.052	.024	-.012	.493	.064	.051	.056	.049	.064	.024	-.018
Upper stage	.503	.162	.119	.107	.098	.070	.040	.503	.145	.132	.125	.112	.110	.076	.040
Upper stage	.513	.369	.286	.245	.196	.145	.092	.513	.346	.304	.280	.233	.202	.139	.109
Transition	.230	.178	.147	.118	.086	.058	.028	.525	.179	.155	.142	.118	.086	.058	.017
Transition	.156	.097	.073	.049	.017	.001	-.024	.535	.133	.051	.073	.049	.017	.001	-.035
Transition	.110	.046	.033	.003	-.029	-.052	-.071	.545	.075	.028	.004	.014	-.035	-.057	-.094
Transition	.035	-.023	-.060	-.085	-.111	-.122	-.141	.555	-.016	-.059	-.078	-.091	-.117	-.145	-.182
Transition	.269	.328	.342	.343	.328	.316	.299	.565	.321	.370	.377	.360	.351	.333	.307
Main stage	.568	.501	.520	.492	.454	.407	.379	.568	.471	.507	.514	.480	.454	.413	.466
Main stage	.577	.098	.159	.160	.169	.162	.158	.577	.127	.146	.159	.160	.169	.156	.169
Main stage	.587	.051	.088	.101	.116	.110	.111	.587	.075	.099	.106	.102	.116	.110	.117
Main stage	.597	.028	.047	.073	.087	.080	.082	.597	.046	.064	.071	.067	.075	.075	.076
Main stage	.607	.016	.060	.055	.070	.063	.064	.607	.034	.053	.066	.055	.070	.063	.070
Main stage	.617	.005	.054	.049	.058	.051	.053	.617	.028	.041	.054	.049	.058	.051	.064
Main stage	.627	.005	.042	.038	.046	.040	.047	.627	.022	.041	.048	.038	.052	.045	.053
Main stage	.637	.006	.037	.032	.040	.034	.035	.637	.016	.035	.037	.032	.040	.034	.047
Main stage	.657	.013	.015	.016	.021	.020	.027	.657	.016	.027	.019	.018	.025	.022	.041
Main stage	.677	.013	.014	.014	.019	.018	.026	.677	.005	.016	.009	.008	.015	.018	.029
Main stage	.697	.017	.011	.008	.013	.012	.022	.697	.009	.020	.011	.010	.017	.018	.037
Main stage	.737	.017	.008	.007	.011	.012	.024	.737	.007	.016	.015	.007	.013	.014	.037
Main stage	.777	.021	.004	.005	.009	.009	.022	.777	.003	.010	.005	.012	.013	.011	.035
Main stage	.805	.026	.003	.003	.009	.005	.014	.805	.001	.012	.013	.005	.005	.009	.033
Main stage	.817	.029	.000	.000	.004	.004	.015	.817	.002	.004	.003	.000	.004	.008	.034
Main stage	.857	.022	.001	.003	.007	.007	.023	.857	.004	.009	.008	.004	.008	.012	.036
Main stage	.877	.025	.002	.002	.007	.008	.023	.877	.006	.011	.009	.005	.008	.013	.036
Main stage	.897	.021	.007	.005	.010	.011	.027	.897	.007	.012	.010	.005	.008	.013	.039
Main stage	.917	.027	.007	.007	.007	.008	.027	.917	.007	.014	.012	.007	.012	.017	.041
Main stage	.957	.022	.007	.007	.007	.008	.027	.957	.022	.025	.021	.018	.024	.030	.051
Main stage	.997	.106	.089	.089	.089	.095	.128	.997	.106	.089	.077	.070	.080	.095	.128

TABLE 7.- PRESSURE COEFFICIENTS FOR CONFIGURATION 322 - Continued

(b) $M = 0.60$; $\alpha = -10^\circ$ to 10° - Concluded

		C_p for $\beta = -60^\circ$						C_p for $\beta = -90^\circ$								
		$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$	$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$	
Nozzle	x/l	.559	.558	.545	.522	.479	.424	.320	.426	.418	.479	.511	.516	.508	.486	.416
		.436	.405	.387	.358	.321	.283	.206								
Upper stage	x/l	.446	.169	.156	.133	.113	.090	-.001	.446	.074	.107	.122	.138	.141	.125	.067
		.453	-1.470	-1.274	-1.223	-.858	-.828	-.782	.453	-1.149	-1.133	-1.105	-1.001	-.765	-.770	-.934
Transition	x/l	.463	.699	-.747	-.748	-.670	-.657	-.687								
		.473	-.335	-.441	-.465	-.583	-.571	-.612	.473	-.172	-.127	-.135	-.118	-.219	-.230	-.185
Main stage	x/l	.483	-.057	-.071	-.112	-.219	-.305	-.347	.493	-.063	.005	.050	.061	.069	.030	-.070
		.493	.034	.050	.055	.064	-.068	-.127	.513	.185	.224	.246	.239	.236	.243	.166
Flare	x/l	.503	.070	.115	.112	.104	.076	-.041								
		.513	.264	.257	.233	.202	.185	.155	.535	-.040	.017	.038	.049	.035	.013	-.059
Transition	x/l	.525	.064	.097	.104	.081	.047	-.018								
		.535	.047	.056	.043	.023	.001	-.071	.565	-.480	-.416	-.389	-.366	-.375	-.415	-.487
Main stage	x/l	.545	-.005	-.006	-.014	-.041	-.057	-.123	.568	-.547	-.490	-.468	-.440	-.454	-.494	-.559
		.555	-.112	-.104	-.114	-.119	-.146	-.206	.587	-.180	-.140	-.118	-.108	-.122	-.133	-.192
Upper stage	x/l	.565	-.398	-.377	-.360	-.351	-.398	-.457	.607	-.133	-.088	-.071	-.055	-.070	-.080	-.146
		.568	-.453	-.449	-.399	-.390	-.430	-.478	.627	-.116	-.070	-.054	-.038	-.052	-.063	-.128
Transition	x/l	.577	-.180	-.159	-.154	-.169	-.174	-.216	.657	-.108	-.058	-.023	-.018	-.031	-.049	-.109
		.587	-.139	-.122	-.102	-.116	-.121	-.158	.697	-.100	-.053	-.021	-.012	-.023	-.044	-.105
Main stage	x/l	.597	-.110	-.083	-.073	-.081	-.086	-.128	.737	-.094	-.047	-.013	-.008	-.017	-.038	-.098
		.607	-.098	-.070	-.055	-.070	-.075	-.111	.777	-.088	-.043	-.011	-.008	-.013	-.034	-.094
Transition	x/l	.617	-.086	-.060	-.049	-.058	-.063	-.099	.857	-.079	-.032	-.009	-.002	-.015	-.032	-.088
		.627	-.086	-.048	-.038	-.052	-.057	-.093	.897	-.085	-.039	-.016	-.005	-.014	-.034	-.086
Main stage	x/l	.637	-.075	-.053	-.042	-.040	-.051	-.088								
		.657	-.077	-.051	-.032	-.027	-.038	-.076								
Transition	x/l	.677	-.063	-.025	-.018	-.023	-.034	-.070								
		.697	-.063	-.042	-.013	-.025	-.034	-.076								
Main stage	x/l	.737	-.050	-.011	-.008	-.019	-.030	-.064								
		.777	-.059	-.037	-.012	-.013	-.026	-.055								
Transition	x/l	.785	-.059	-.009	-.008	-.011	-.026	-.055								
		.817	-.053	-.013	-.014	-.009	-.020	-.045								
Main stage	x/l	.857	-.057	-.009	-.001	-.006	-.015	-.038								
		.877	-.058	-.029	-.003	-.010	-.019	-.040								
Transition	x/l	.897	-.058	-.030	-.004	-.010	-.019	-.041								
		.917	-.066	-.031	-.005	-.010	-.020	-.041								
Main stage	x/l	.957	-.074	-.019	-.010	-.017	-.024	-.045								
		.997	-.137	-.106	-.073	-.085	-.100	-.135								

TABLE 7.- PRESSURE COEFFICIENTS FOR CONFIGURATION 322 - Continued

(c) $M = 0.80$; $\alpha = -10^\circ$ to 10° - Concluded

		C_p for $\beta = -60^\circ$						C_p for $\beta = -50^\circ$											
		$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$	$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$				
Main stage	x/z	.649	.629	.598	.555	.401	.273	.507	.592	.594	.589	.498	.426	.507	.592	.594	.589	.498	
		.507	.475	.444	.408	.273	.104	.195	.253	.256	.250	.190	.446	.453	.453	.453	.453	.453	
		.311	.283	.252	.228	.104	.046	.253	.253	.256	.250	.190	.446	.453	.453	.453	.453	.453	.453
		-1.063	-1.007	-0.820	-0.597	-0.586	-0.586	-0.931	-0.804	-0.708	-0.675	-0.753	.453	.453	.453	.453	.453	.453	.453
		.463	.458	.447	.426	.556	.541	.401	.503	.496	.444	.464	.473	.473	.473	.473	.473	.473	.473
		.605	.619	.619	.619	.541	.541	.401	.503	.496	.444	.464	.473	.473	.473	.473	.473	.473	.473
		.274	.391	.407	.475	.475	.475	.401	.503	.496	.444	.464	.473	.473	.473	.473	.473	.473	.473
		.085	.176	.223	.290	.321	.321	.401	.503	.496	.444	.464	.473	.473	.473	.473	.473	.473	.473
		.016	.002	.053	.113	.183	.183	.401	.503	.496	.444	.464	.473	.473	.473	.473	.473	.473	.473
		.065	.093	.058	.006	.075	.075	.401	.503	.496	.444	.464	.473	.473	.473	.473	.473	.473	.473
	.264	.212	.154	.106	.060	.060	.168	.182	.169	.140	.163	.513	.513	.513	.513	.513	.513	.513	
Transition flap	x/z	.095	.158	.157	.121	.013	.013	.012	.097	.108	.094	.021	.535	.535	.535	.535	.535	.535	
		.076	.109	.100	.075	.037	.037	.012	.097	.108	.094	.021	.535	.535	.535	.535	.535	.535	.535
		.019	.044	.031	.014	.092	.092	.012	.097	.108	.094	.021	.535	.535	.535	.535	.535	.535	.535
		.082	.060	.081	.080	.176	.176	.012	.097	.108	.094	.021	.535	.535	.535	.535	.535	.535	.535
		.384	.382	.347	.334	.475	.475	.012	.097	.108	.094	.021	.535	.535	.535	.535	.535	.535	.535
		.932	.620	.469	.425	.860	.860	.012	.097	.108	.094	.021	.535	.535	.535	.535	.535	.535	.535
		.206	.166	.162	.157	.204	.204	.012	.097	.108	.094	.021	.535	.535	.535	.535	.535	.535	.535
		.152	.107	.104	.110	.145	.145	.012	.097	.108	.094	.021	.535	.535	.535	.535	.535	.535	.535
		.117	.072	.069	.075	.114	.114	.012	.097	.108	.094	.021	.535	.535	.535	.535	.535	.535	.535
		.098	.053	.054	.056	.099	.099	.012	.097	.108	.094	.021	.535	.535	.535	.535	.535	.535	.535
Rose	x/z	.090	.037	.042	.044	.087	.087	.136	.057	.054	.056	.134	.607	.607	.607	.607	.607	.607	
		.090	.037	.042	.044	.087	.087	.136	.057	.054	.056	.134	.607	.607	.607	.607	.607	.607	
		.078	.026	.027	.033	.072	.072	.136	.057	.054	.056	.134	.607	.607	.607	.607	.607	.607	.607
		.069	.022	.016	.022	.063	.063	.136	.057	.054	.056	.134	.607	.607	.607	.607	.607	.607	.607
		.056	.016	.012	.018	.057	.057	.136	.057	.054	.056	.134	.607	.607	.607	.607	.607	.607	.607
		.043	.010	.007	.015	.051	.051	.136	.057	.054	.056	.134	.607	.607	.607	.607	.607	.607	.607
		.055	.010	.003	.007	.042	.042	.136	.057	.054	.056	.134	.607	.607	.607	.607	.607	.607	.607
		.051	.005	.001	.007	.034	.034	.136	.057	.054	.056	.134	.607	.607	.607	.607	.607	.607	.607
		.055	.006	.001	.004	.032	.032	.136	.057	.054	.056	.134	.607	.607	.607	.607	.607	.607	.607
		.047	.001	.004	.002	.029	.029	.136	.057	.054	.056	.134	.607	.607	.607	.607	.607	.607	.607
	.052	.006	.001	.006	.031	.031	.136	.057	.054	.056	.134	.607	.607	.607	.607	.607	.607	.607	
	.052	.007	.001	.007	.031	.031	.136	.057	.054	.056	.134	.607	.607	.607	.607	.607	.607	.607	
	.053	.008	.001	.008	.034	.034	.136	.057	.054	.056	.134	.607	.607	.607	.607	.607	.607	.607	
	.059	.013	.007	.014	.036	.036	.136	.057	.054	.056	.134	.607	.607	.607	.607	.607	.607	.607	
	.068	.020	.015	.021	.047	.047	.136	.057	.054	.056	.134	.607	.607	.607	.607	.607	.607	.607	
	.137	.086	.077	.084	.127	.127	.136	.057	.054	.056	.134	.607	.607	.607	.607	.607	.607	.607	

TABLE 7.- PRESSURE COEFFICIENTS FOR CONFIGURATION 322 - Continued

(a) $M = 1.00$; $\alpha = -10^\circ$ to 10°

x/l	C_p for $\beta = 0^\circ$						
	$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$
.426	.944	.866	.801	.736	.674	.605	.516
.436	.813	.735	.670	.607	.546	.480	.396
.446	.689	.608	.545	.484	.423	.357	.271
.453	.568	.484	.421	.360	.299	.232	.148
.458	.444	.368	.305	.244	.182	.115	.031
.463	.319	.244	.181	.120	.058	-.004	-.068
.473	.194	.119	.056	.000	-.056	-.115	-.182
.483	.068	-.006	-.068	-.127	-.186	-.244	-.301
.493	-.068	-.142	-.209	-.266	-.324	-.382	-.439
.503	-.194	-.268	-.335	-.392	-.450	-.507	-.565
.513	-.319	-.393	-.460	-.517	-.574	-.631	-.688
.525	-.444	-.518	-.585	-.642	-.700	-.757	-.814
.535	-.568	-.642	-.709	-.766	-.824	-.881	-.938
.545	-.693	-.767	-.834	-.891	-.948	-.1005	-.1062
.555	-.817	-.891	-.958	-.1015	-.1072	-.1129	-.1186
.565	-.941	-.1012	-.1069	-.1126	-.1183	-.1240	-.1297
.575	-.1064	-.1111	-.1168	-.1225	-.1282	-.1339	-.1396
.585	-.1188	-.1235	-.1292	-.1349	-.1406	-.1463	-.1520
.595	-.1312	-.1359	-.1416	-.1473	-.1530	-.1587	-.1644
.605	-.1436	-.1483	-.1540	-.1597	-.1654	-.1711	-.1768
.615	-.1560	-.1607	-.1664	-.1721	-.1778	-.1835	-.1892
.625	-.1684	-.1731	-.1788	-.1845	-.1902	-.1959	-.2016
.635	-.1808	-.1855	-.1912	-.1969	-.2026	-.2083	-.2140
.645	-.1932	-.1979	-.2036	-.2093	-.2150	-.2207	-.2264
.655	-.2056	-.2103	-.2160	-.2217	-.2274	-.2331	-.2388
.665	-.2180	-.2227	-.2284	-.2341	-.2398	-.2455	-.2512
.675	-.2304	-.2351	-.2408	-.2465	-.2522	-.2579	-.2636
.685	-.2428	-.2475	-.2532	-.2589	-.2646	-.2703	-.2760
.695	-.2552	-.2599	-.2656	-.2713	-.2770	-.2827	-.2884
.705	-.2676	-.2723	-.2780	-.2837	-.2894	-.2951	-.3008
.715	-.2800	-.2847	-.2904	-.2961	-.3018	-.3075	-.3132
.725	-.2924	-.2971	-.3028	-.3085	-.3142	-.3199	-.3256
.735	-.3048	-.3095	-.3152	-.3209	-.3266	-.3323	-.3380
.745	-.3172	-.3219	-.3276	-.3333	-.3390	-.3447	-.3504
.755	-.3296	-.3343	-.3400	-.3457	-.3514	-.3571	-.3628
.765	-.3420	-.3467	-.3524	-.3581	-.3638	-.3695	-.3752
.775	-.3544	-.3591	-.3648	-.3705	-.3762	-.3819	-.3876
.785	-.3668	-.3715	-.3772	-.3829	-.3886	-.3943	-.4000
.795	-.3792	-.3839	-.3896	-.3953	-.4010	-.4067	-.4124
.805	-.3916	-.3963	-.4020	-.4077	-.4134	-.4191	-.4248
.815	-.4040	-.4087	-.4144	-.4201	-.4258	-.4315	-.4372
.825	-.4164	-.4211	-.4268	-.4325	-.4382	-.4439	-.4496
.835	-.4288	-.4335	-.4392	-.4449	-.4506	-.4563	-.4620
.845	-.4412	-.4459	-.4516	-.4573	-.4630	-.4687	-.4744
.855	-.4536	-.4583	-.4640	-.4697	-.4754	-.4811	-.4868
.865	-.4660	-.4707	-.4764	-.4821	-.4878	-.4935	-.4992
.875	-.4784	-.4831	-.4888	-.4945	-.5002	-.5059	-.5116
.885	-.4908	-.4955	-.5012	-.5069	-.5126	-.5183	-.5240
.895	-.5032	-.5079	-.5136	-.5193	-.5250	-.5307	-.5364
.905	-.5156	-.5203	-.5260	-.5317	-.5374	-.5431	-.5488
.915	-.5280	-.5327	-.5384	-.5441	-.5498	-.5555	-.5612
.925	-.5404	-.5451	-.5508	-.5565	-.5622	-.5679	-.5736
.935	-.5528	-.5575	-.5632	-.5689	-.5746	-.5803	-.5860
.945	-.5652	-.5699	-.5756	-.5813	-.5870	-.5927	-.5984
.955	-.5776	-.5823	-.5880	-.5937	-.5994	-.6051	-.6108
.965	-.5900	-.5947	-.6004	-.6061	-.6118	-.6175	-.6232
.975	-.6024	-.6071	-.6128	-.6185	-.6242	-.6299	-.6356
.985	-.6148	-.6195	-.6252	-.6309	-.6366	-.6423	-.6480
.995	-.6272	-.6319	-.6376	-.6433	-.6490	-.6547	-.6604

x/l	C_p for $\beta = -30^\circ$						
	$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$
.426	.905	.851	.792	.739	.677	.617	.522
.436	.754	.727	.646	.595	.541	.487	.396
.446	.603	.547	.500	.452	.405	.357	.271
.453	.466	.406	.374	.329	.289	.249	.162
.458	.331	.266	.232	.188	.151	.104	.017
.463	.200	.135	.101	.057	.013	-.034	-.101
.473	.068	.003	-.032	-.088	-.144	-.200	-.267
.483	-.064	-.129	-.195	-.251	-.307	-.363	-.429
.493	-.190	-.255	-.321	-.377	-.433	-.489	-.555
.503	-.316	-.381	-.447	-.503	-.559	-.615	-.681
.513	-.441	-.506	-.572	-.628	-.684	-.740	-.806
.525	-.565	-.630	-.696	-.752	-.808	-.864	-.930
.535	-.689	-.754	-.820	-.876	-.932	-.988	-.1054
.545	-.813	-.878	-.944	-.1000	-.1056	-.1112	-.1178
.555	-.937	-.1002	-.1068	-.1124	-.1180	-.1236	-.1302
.565	-.1060	-.1116	-.1172	-.1228	-.1284	-.1340	-.1406
.575	-.1184	-.1240	-.1296	-.1352	-.1408	-.1464	-.1530
.585	-.1308	-.1364	-.1420	-.1476	-.1532	-.1588	-.1654
.595	-.1432	-.1488	-.1544	-.1600	-.1656	-.1712	-.1778
.605	-.1556	-.1612	-.1668	-.1724	-.1780	-.1836	-.1902
.615	-.1680	-.1736	-.1792	-.1848	-.1904	-.1960	-.2026
.625	-.1804	-.1860	-.1916	-.1972	-.2028	-.2084	-.2150
.635	-.1928	-.1984	-.2040	-.2096	-.2152	-.2208	-.2274
.645	-.2052	-.2108	-.2164	-.2220	-.2276	-.2332	-.2398
.655	-.2176	-.2232	-.2288	-.2344	-.2400	-.2456	-.2522
.665	-.2300	-.2356	-.2412	-.2468	-.2524	-.2580	-.2646
.675	-.2424	-.2480	-.2536	-.2592	-.2648	-.2704	-.2770
.685	-.2548	-.2604	-.2660	-.2716	-.2772	-.2828	-.2894
.695	-.2672	-.2728	-.2784	-.2840	-.2896	-.2952	-.3018
.705	-.2796	-.2852	-.2908	-.2964	-.3020	-.3076	-.3142
.715	-.2920	-.2976	-.3032	-.3088	-.3144	-.3200	-.3266
.725	-.3044	-.3100	-.3156	-.3212	-.3268	-.3324	-.3390
.735	-.3168	-.3224	-.3280	-.3336	-.3392	-.3448	-.3514
.745	-.3292	-.3348	-.3404	-.3460	-.3516	-.3572	-.3638
.755	-.3416	-.3472	-.3528	-.3584	-.3640	-.3696	-.3762
.765	-.3540	-.3596	-.3652	-.3708	-.3764	-.3820	-.3886
.775	-.3664	-.3720	-.3776	-.3832	-.3888	-.3944	-.4010
.785	-.3788	-.3844	-.3900	-.3956	-.4012	-.4068	-.4134
.795	-.3912	-.3968	-.4024	-.4080	-.4136	-.4192	-.4258
.805	-.4036	-.4092	-.4148	-.4204	-.4260	-.4316	-.4382
.815	-.4160	-.4216	-.4272	-.4328	-.4384	-.4440	-.4506
.825	-.4284	-.4340	-.4396	-.4452	-.4508	-.4564	-.4630
.835	-.4408	-.4464	-.4520	-.4576	-.4632	-.4688	-.4754
.845	-.4532	-.4588	-.4644	-.4700	-.4756	-.4812	-.4878
.855	-.4656	-.4712	-.4768	-.4824	-.4880	-.4936	-.5002
.865	-.4780	-.4836	-.4892	-.4948	-.5004	-.5060	-.5126
.875	-.4904	-.4960	-.5016	-.5072	-.5128	-.5184	-.5250
.885	-.5028	-.5084	-.5140	-.5196	-.5252	-.5308	-.5374
.895	-.5152	-.5208	-.5264	-.5320	-.5376	-.5432	-.5498
.905	-.5276	-.5332	-.5388	-.5444	-.5500	-.5556	-.5622
.915	-.5400	-.5456	-.5512	-.5568	-.5624	-.5680	-.5746
.925	-.5524	-.5580	-.5636	-.5692	-.5748	-.5804	-.5870
.935	-.5648	-.5704	-.5760	-.5816	-.5872	-.5928	-.5994
.945	-.5772	-.5828	-.5884	-.5940	-.5996	-.6052	-.6118
.955	-.5896	-.5952	-.6008	-.6064	-.6120	-.6176	-.6242
.965	-.6020	-.6076	-.6132	-.6188	-.6244	-.6300	-.6366
.975	-.6144	-.6200	-.6256	-.6312	-.6368	-.6424	-.6490
.985	-.6268	-.6324	-.6380	-.6436	-.6492	-.6548	-.6614
.995	-.6392	-.6448	-.6504	-.6560	-.6616	-.6672	-.6738

TABLE 7.- PRESSURE COEFFICIENTS FOR CONFIGURATION 322 - Continued

(d) $M = 1.00$; $\alpha = -10^\circ$ to 10° - Concluded

		C_p for $\beta = -60^\circ$						C_p for $\beta = -90^\circ$							
		$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$	$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$
Main stage	x/l	.789	.786	.769	.736	.698	.647	.552	.709	.706	.700	.674	.625	.570	.499
		.663	.657	.631	.604	.564	.519	.435	.651	.649	.649	.633	.619	.606	.598
		.508	.502	.476	.449	.414	.378	.304	.446	.439	.449	.438	.426	.412	.404
		.854	.860	.878	.890	.899	.884	.828	.984	.978	.983	.984	.985	.985	.981
		.945	.979	-1.000	-1.018	-1.032	-1.008	-628	.714	.714	.714	.714	.714	.714	.714
		.719	.823	.871	.908	.937	.964	.984	.733	.733	.733	.733	.733	.733	.733
		.352	.566	.623	.669	.692	.728	.761	.439	.439	.439	.439	.439	.439	.439
		.269	.407	.464	.507	.531	.561	.584	.394	.394	.394	.394	.394	.394	.394
		.239	.272	.253	.209	.169	.125	.084	.051	.051	.051	.051	.051	.051	.051
		.006	.097	.108	.092	.062	.031	.020	.107	.107	.107	.107	.107	.107	.107
	.513	.311	.266	.184	.091	.020	.120	.244	.244	.244	.244	.244	.244	.244	
Transition flare	x/l	.152	.249	.293	.296	.265	.145	-.063	.021	.167	.223	.215	.148	.011	
		.137	.210	.232	.244	.266	.120	-.026	.021	.167	.223	.215	.148	.011	
		.119	.173	.183	.183	.194	.087	-.029	.021	.167	.223	.215	.148	.011	
		.078	.123	.130	.110	.093	.036	-.062	.021	.167	.223	.215	.148	.011	
		.093	.165	.177	.108	.125	.154	.218	.199	.118	.105	.110	.129	.187	
		.574	.553	.552	.564	.578	.603	.652	.642	.593	.579	.576	.591	.637	
		.487	.475	.474	.465	.489	.538	.606	.472	.426	.405	.385	.440	.488	
		.386	.377	.382	.385	.371	.353	.326	.379	.281	.249	.249	.270	.390	
		.321	.306	.311	.311	.291	.220	.228	.379	.281	.249	.249	.270	.390	
		.296	.269	.258	.249	.232	.220	.223	.379	.281	.249	.249	.270	.390	
Nose	x/l	.275	.185	.163	.157	.152	.153	.174	.222	.170	.150	.152	.165	.226	
		.200	.148	.129	.119	.121	.134	.164	.222	.170	.150	.152	.165	.226	
		.161	.114	.093	.085	.090	.107	.138	.184	.121	.095	.096	.127	.186	
		.134	.094	.078	.077	.077	.080	.097	.184	.121	.095	.096	.127	.186	
		.107	.074	.063	.060	.065	.056	.044	.150	.093	.070	.069	.096	.149	
		.104	.071	.060	.054	.050	.044	.044	.150	.093	.070	.069	.096	.149	
		.027	.012	.010	.012	.017	.006	.014	.121	.077	.059	.053	.078	.107	
		.033	.002	.022	.025	.023	.013	.010	.121	.077	.059	.053	.078	.107	
		.013	.020	.033	.034	.036	.017	.007	.051	.015	.009	.011	.012	.004	
		.022	.009	.023	.026	.022	.011	.010	.051	.015	.009	.011	.012	.004	
	.023	.009	.021	.025	.020	.009	.011	.035	.012	.030	.029	.030	.042		
	.024	.006	.017	.022	.017	.005	.014	.044	.001	.021	.021	.021	.049		
	.034	.001	.009	.014	.010	.001	.018	.049	.003	.014	.021	.013	.008		
	.035	.006	.009	.004	.001	.001	.013	.049	.003	.014	.021	.013	.008		
	.103	.086	.093	.102	.115	.134	.155	.049	.003	.014	.021	.013	.008		

TABLE 7.- PRESSURE COEFFICIENTS FOR CONFIGURATION 322 - Concluded

(e) $M = 1.20$; $\alpha = -10^\circ$ to 10° - Concluded

		C_p for $\beta = -60^\circ$						C_p for $\beta = -90^\circ$							
		$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$	$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$
None	$x/1$.914	.511	.095	.864	.834	.782	.685	.426	.776	.837	.858	.864	.837	.773
		.800	.795	.779	.748	.715	.670	.584	.446	.564	.604	.619	.623	.617	.547
Upper stage	$x/1$.737	.668	.646	.623	.596	.556	.481	.453	.619	.614	.611	.611	.602	.608
		.556	.566	.575	.581	.582	.591	.608	.669	.612	.614	.611	.611	.599	.608
Transition	$x/1$.463	.630	.642	.653	.660	.669	.691	.473	.376	.394	.406	.412	.403	.395
		.447	.505	.542	.575	.595	.618	.642	.493	.262	.226	.218	.219	.220	.264
Main stage	$x/1$.483	.326	.365	.404	.427	.454	.479	.513	.189	.189	.218	.222	.213	.116
		.186	.226	.265	.301	.329	.354	.381	.535	.112	.202	.244	.257	.245	.103
None	$x/1$.493	.174	.197	.217	.237	.269	.299	.565	.073	.088	.090	.089	.079	.019
		.159	.140	.140	.146	.154	.160	.166	.568	.299	.281	.279	.282	.294	.335
Transition	$x/1$.503	.221	.234	.225	.197	.160	.087	.587	.256	.193	.183	.183	.222	.277
		.180	.221	.234	.225	.197	.160	.087	.607	.220	.159	.138	.128	.170	.231
Main stage	$x/1$.204	.261	.282	.289	.264	.211	.111	.627	.212	.100	.093	.093	.123	.209
		.202	.246	.253	.254	.240	.190	.084	.657	.148	.077	.048	.040	.080	.142
None	$x/1$.180	.210	.223	.222	.204	.165	.081	.697	.142	.078	.046	.034	.071	.137
		.173	.208	.225	.219	.198	.167	.081	.737	.115	.043	.038	.031	.032	.116
Transition	$x/1$.565	.112	.120	.098	.072	.054	.005	.777	.082	.027	.018	.018	.024	.098
		.278	.263	.259	.268	.277	.299	.338	.785	.093	.051	.028	.010	.022	.102
Main stage	$x/1$.577	.241	.229	.229	.241	.272	.327	.817	.081	.029	.013	.011	.016	.091
		.198	.189	.182	.186	.198	.236	.294	.857	.087	.030	.017	.009	.027	.089
None	$x/1$.597	.151	.152	.147	.159	.189	.258	.897	.087	.041	.017	.006	.026	.078
		.163	.132	.127	.125	.137	.156	.209	.607	.220	.138	.128	.128	.170	.231
Transition	$x/1$.617	.146	.105	.106	.115	.132	.168	.627	.212	.118	.093	.093	.123	.209
		.146	.107	.094	.093	.099	.118	.146	.657	.148	.077	.048	.040	.080	.142
Main stage	$x/1$.637	.086	.078	.076	.077	.086	.121	.697	.142	.078	.046	.034	.071	.137
		.130	.086	.078	.076	.077	.086	.121	.737	.115	.043	.038	.031	.032	.116
None	$x/1$.657	.121	.095	.093	.093	.099	.149	.777	.082	.027	.018	.018	.024	.098
		.107	.099	.093	.093	.093	.099	.149	.785	.093	.051	.028	.010	.022	.102
Transition	$x/1$.677	.057	.043	.043	.041	.048	.079	.817	.081	.029	.013	.011	.016	.091
		.093	.057	.036	.034	.030	.036	.062	.857	.087	.030	.017	.009	.027	.089
Main stage	$x/1$.737	.052	.032	.030	.025	.036	.050	.897	.087	.041	.017	.006	.026	.078
		.096	.052	.032	.030	.025	.036	.050	.697	.142	.078	.046	.034	.071	.137
None	$x/1$.777	.039	.019	.017	.016	.029	.049	.737	.115	.043	.038	.031	.032	.116
		.068	.039	.019	.017	.016	.029	.049	.777	.082	.027	.018	.018	.024	.098
Transition	$x/1$.817	.023	.012	.011	.010	.020	.049	.785	.093	.051	.028	.010	.022	.102
		.058	.023	.012	.011	.010	.020	.049	.817	.081	.029	.013	.011	.016	.091
Main stage	$x/1$.877	.008	.008	.000	.006	.013	.045	.857	.087	.041	.017	.009	.027	.089
		.056	.029	.010	.000	.002	.017	.035	.897	.087	.041	.017	.006	.026	.078
None	$x/1$.917	.032	.018	.007	.008	.021	.031	.937	.070	.036	.014	.014	.034	.106
		.070	.032	.018	.007	.008	.021	.031	.957	.070	.036	.014	.014	.034	.106
Transition	$x/1$.957	.042	.042	.054	.067	.067	.067	.997	.066	.066	.066	.066	.066	.106
		.042	.042	.042	.054	.067	.067	.067	.997	.066	.066	.066	.066	.066	.106

TABLE 1. - PRESSURE COEFFICIENTS FOR CONFIGURATION 123

(a) $M = 0.45$ to 0.95 ; $\alpha = 0^\circ$

		C_p for -					
		$\beta = -30^\circ$					
z/t		M = 0.40	M = 0.70	M = 0.75	M = 0.85	M = 0.90	M = 0.95
		None	.410	.224	.247	.263	.283
.420	.190		.211	.227	.248	.271	.302
Upper stage	.430	.147	.171	.186	.209	.231	.262
	.450	.056	.088	.098	.121	.146	.183
Transition	.460	-.042	-.036	-.015	.037	.076	.127
	.465	-.166	-.175	-.137	-.049	.007	.067
Main stage	.471	-.806	-.854	-.873	-.897	-.924	-.967
	.476	-.223	-.254	-.295	-.348	-.402	-.482
Plate	.481	-.099	-.137	-.166	-.238	-.313	-.412
	.491	-.019	-.022	-.019	-.041	-.122	-.179
Rose	.501	.037	.035	.044	.078	.069	-.001
	.511	.083	.099	.107	.140	.174	.211
Transition	.521	.162	.190	.204	.234	.266	.289
	.531	.344	.374	.385	.407	.419	.412
Plate	.539	.205	.236	.251	.291	.333	.391
	.546	.071	.078	.143	.191	.239	.314
Main stage	.552	.026	.028	.044	.106	.155	.225
	.562	-.214	-.231	-.197	-.089	-.023	.053
Transition	.568	-.565	-.666	-.643	-.574	-.505	-.436
	.577	-.167	-.216	-.230	-.274	-.322	-.371
Plate	.587	-.088	-.113	-.124	-.092	-.086	-.071
	.597	.054	.077	.082	.052	.041	.054
Main stage	.607	-.042	-.054	-.057	-.045	.003	.031
	.617	-.031	-.045	-.048	-.038	.010	.034
Transition	.627	-.019	-.031	-.036	-.034	.003	.009
	.637	-.008	-.027	-.027	-.027	.002	.005
Plate	.647	-.008	-.016	-.012	-.016	-.012	.001
	.657	-.008	-.004	-.009	-.010	-.011	.009
Main stage	.667	.003	.004	.006	.009	.012	.017
	.677	.003	.005	.005	.009	.012	.017
Transition	.687	.007	.007	.008	.012	.012	.017
	.697	.011	.011	.011	.012	.012	.012
Plate	.707	.011	.011	.011	.011	.011	.011
	.717	.011	.011	.011	.011	.011	.011
Main stage	.727	.011	.011	.011	.011	.011	.011
	.737	.011	.011	.011	.011	.011	.011
Transition	.747	.011	.011	.011	.011	.011	.011
	.757	.011	.011	.011	.011	.011	.011
Plate	.767	.011	.011	.011	.011	.011	.011
	.777	.011	.011	.011	.011	.011	.011
Main stage	.787	.011	.011	.011	.011	.011	.011
	.797	.011	.011	.011	.011	.011	.011
Transition	.807	.011	.011	.011	.011	.011	.011
	.817	.011	.011	.011	.011	.011	.011
Plate	.827	.011	.011	.011	.011	.011	.011
	.837	.011	.011	.011	.011	.011	.011
Main stage	.847	.011	.011	.011	.011	.011	.011
	.857	.011	.011	.011	.011	.011	.011
Transition	.867	.011	.011	.011	.011	.011	.011
	.877	.011	.011	.011	.011	.011	.011
Plate	.887	.011	.011	.011	.011	.011	.011
	.897	.011	.011	.011	.011	.011	.011
Main stage	.907	.011	.011	.011	.011	.011	.011
	.917	.011	.011	.011	.011	.011	.011
Transition	.927	.011	.011	.011	.011	.011	.011
	.937	.011	.011	.011	.011	.011	.011
Plate	.947	.011	.011	.011	.011	.011	.011
	.957	.011	.011	.011	.011	.011	.011
Main stage	.967	.011	.011	.011	.011	.011	.011
	.977	.011	.011	.011	.011	.011	.011
Transition	.987	.011	.011	.011	.011	.011	.011
	.997	.011	.011	.011	.011	.011	.011

Table 1. - Statistical Characteristics of the Distribution of C_p for $\alpha = 0^\circ$ - Continued

$\beta = 0.5$, $M = 0.40$ to 0.95 , $\alpha = 0^\circ$ - Continued

		C_p for -					
		$M = 0.40$	$M = 0.70$	$M = 0.75$	$M = 0.85$	$M = 0.90$	$M = 0.95$
None	x/λ	.400	.283	.256	.318	.337	.362
		.410	.131	.227	.378	.446	.559
Upper stage		.430	.162	.178	.199	.225	.255
		.450	.047	.040	.111	.142	.183
Transition stage		.465	-.198	-.167	-.078	-.023	-.039
		.471	-1.239	-1.228	-.928	-.786	-.660
Main stage		.491	-.019	-.015	-.001	-.176	-.156
		.511	.083	.107	.140	.171	.070
Transition stage		.531	.355	.393	.425	.402	.312
		.552	.026	.024	.102	.148	.219
None		.568	-.702	-1.103	-1.251	-.982	-.843
		.587	-.088	-.119	-.124	-.078	-.513
Upper stage		.607	-.031	-.054	-.057	-.045	-.354
		.627	-.019	-.031	-.036	-.003	-.089
Transition stage		.657	-.008	-.016	-.015	-.018	.025
		.697	.003	-.007	-.006	-.011	.015
Main stage		.737	.007	-.002	-.001	-.010	.003
		.777	.011	.001	.002	-.005	.000
None		.785	.011	-.004	.002	-.005	.001
		.817	.014	.006	.007	-.001	-.001
Upper stage		.857	.009	.001	.002	-.002	-.008
		.897	.008	-.002	.000	-.005	-.010
Transition stage		.917	.005	-.000	-.000	-.000	.000
		.957	-.004	-.013	-.017	-.022	-.073
Main stage		.977	-.056	-.074	-.074	-.086	-.094
		.997	-.075	-.074	-.074	-.086	-.094

TABLE 8.- PRESSURE COEFFICIENTS FOR CONFIGURATION 125 - Continued

(b) $M = 0.60$; $\alpha = -10^\circ$ to 10°

x/l		C_p for $\beta = 0^\circ$						C_p for $\beta = -30^\circ$									
		$\alpha = -10^\circ$		$\alpha = -5^\circ$		$\alpha = 0^\circ$		$\alpha = -10^\circ$		$\alpha = -5^\circ$		$\alpha = 0^\circ$		$\alpha = 5^\circ$		$\alpha = 10^\circ$	
		$\alpha = -10^\circ$	$\alpha = -5^\circ$	$\alpha = 0^\circ$	$\alpha = 5^\circ$	$\alpha = 10^\circ$	$\alpha = -10^\circ$	$\alpha = -5^\circ$	$\alpha = 0^\circ$	$\alpha = 5^\circ$	$\alpha = 10^\circ$	$\alpha = -10^\circ$	$\alpha = -5^\circ$	$\alpha = 0^\circ$	$\alpha = 5^\circ$	$\alpha = 10^\circ$	
Nozzle	.410	.392	.334	.275	.226	.188	.131	.087	.410	.364	.317	.270	.221	.183	.131	.070	
	.420	.364	.306	.242	.193	.149	.098	.053	.430	.320	.276	.225	.187	.143	.098	.036	
Upper stage	.430	.320	.261	.208	.154	.115	.064	.020	.450	.292	.250	.197	.154	.110	.058	.003	
	.460	.219	.161	.107	.058	.020	-.032	-.072	.450	.185	.144	.090	.053	.015	-.032	-.188	
Transition flare	.460	.219	.161	.107	.058	.020	-.032	-.072	.460	.073	.037	-.010	-.055	-.089	-.142	-.315	
	.471	.172	.123	.069	.019	-.036	-.082	-.126	.471	-.057	-.100	-.155	-.194	-.228	-.275	-.458	
Main stage	.471	.172	.123	.069	.019	-.036	-.082	-.126	.476	-.201	-.221	-.258	-.288	-.267	-.274	-.273	
	.481	.068	.008	-.028	-.078	-.135	-.197	-.259	.481	.080	.088	.114	.118	.117	.130	.129	
Transition flare	.491	.013	-.042	-.092	-.147	-.202	-.258	-.312	.491	-.011	-.008	-.034	-.032	-.031	-.043	-.037	
	.501	.064	.050	.030	.026	.020	.020	.020	.501	.041	.044	.024	.026	.027	.020	.020	
Nozzle	.511	.116	.088	.068	.054	.044	.038	.034	.511	.093	.102	.082	.084	.084	.072	.072	
	.521	.214	.200	.180	.176	.171	.158	.144	.521	.191	.200	.180	.176	.171	.158	.141	
Transition flare	.531	.485	.442	.399	.354	.321	.291	.268	.531	.456	.436	.393	.360	.338	.308	.262	
	.539	.337	.289	.246	.213	.186	.156	.134	.539	.177	.220	.229	.213	.192	.151	.094	
Main stage	.546	.246	.192	.149	.111	.083	.048	.026	.546	.052	.078	.069	.065	.038	-.003	-.061	
	.552	.155	.101	.047	.008	-.019	-.055	-.073	.552	.126	.089	.047	.008	-.019	-.055	-.078	
Transition flare	.562	-.092	-.153	-.208	-.247	-.275	-.312	-.311	.562	-.127	-.171	-.214	-.247	-.275	-.312	-.334	
	.568	-.699	-.765	-.826	-.830	-.805	-.801	-.812	.568	-.623	-.666	-.710	-.720	-.713	-.709	-.673	
Main stage	.577	-.132	-.158	-.190	-.205	-.199	-.211	-.199	.577	-.149	-.169	-.196	-.205	-.199	-.211	-.211	
	.587	-.063	-.088	-.115	-.119	-.112	-.125	-.107	.587	-.091	-.100	-.120	-.119	-.118	-.125	-.124	
Transition flare	.597	-.034	-.054	-.080	-.084	-.071	-.078	-.066	.597	-.051	-.054	-.068	-.072	-.068	-.072	-.066	
	.607	-.022	-.036	-.057	-.061	-.048	-.055	-.037	.607	-.045	-.042	-.051	-.049	-.048	-.055	-.055	
Main stage	.617	-.016	-.025	-.045	-.049	-.037	-.044	-.026	.617	-.034	-.036	-.042	-.039	-.037	-.044	-.043	
	.627	-.005	-.019	-.034	-.038	-.025	-.026	-.014	.627	-.028	-.025	-.039	-.036	-.025	-.038	-.043	
Transition flare	.637	-.006	-.008	-.028	-.032	-.019	-.020	-.009	.637	-.022	-.019	-.028	-.032	-.019	-.026	-.020	
	.657	-.011	.004	-.016	-.016	-.010	-.013	-.001	.657	-.016	-.008	-.020	-.020	-.014	-.022	-.020	
Main stage	.677	-.013	.006	-.010	-.013	-.006	-.009	.005	.677	-.003	.000	-.010	-.009	-.002	-.015	-.016	
	.697	.017	.000	-.009	-.009	-.002	-.005	.005	.697	.014	.000	-.010	-.009	-.002	-.013	-.018	
Transition flare	.717	.015	.003	-.007	-.003	-.000	-.005	.003	.717	.009	.002	-.009	-.005	-.000	-.009	-.020	
	.737	.022	.016	-.007	-.003	.004	-.001	.007	.737	.007	.004	-.024	-.001	.004	.007	-.020	
Main stage	.757	.026	.021	.003	-.007	.008	.005	.019	.757	.001	.010	-.014	.001	.006	.003	-.018	
	.817	.028	.020	.003	-.006	.006	.004	.011	.817	.003	.011	-.001	.000	.006	.007	-.022	
Transition flare	.857	.022	.017	-.001	-.003	.003	-.004	.004	.857	.005	.005	-.005	.003	.002	.011	-.025	
	.877	.023	.017	-.001	-.003	.003	-.004	.005	.877	.005	.004	-.007	.005	.001	.013	-.026	
Main stage	.897	.018	.013	-.004	-.006	.001	-.007	.000	.897	.006	.002	-.008	.006	.000	.014	-.026	
	.917	.028	.021	.004	-.003	.003	-.004	.007	.917	.006	.002	-.008	.006	.003	.018	-.026	
Transition flare	.937	.023	.017	-.001	-.003	.003	-.004	.005	.937	.023	.011	-.019	.017	.013	.038	-.038	
	.957	.018	.013	-.004	-.006	.001	-.007	.000	.957	.023	.011	-.019	.017	.013	.038	-.038	
Main stage	.977	.018	.013	-.004	-.006	.001	-.007	.000	.977	.015	-.074	-.071	-.073	-.074	-.096	-.115	
	.997	.018	.013	-.004	-.006	.001	-.007	.000	.997	.015	-.074	-.071	-.073	-.074	-.096	-.115	

TABLE 5.- PRESSURE COEFFICIENTS FOR CONFIGURATION 123 - Continued

(b) $M = 0.60$; $\alpha = -10^\circ$ to 10° - Concluded

		C_p for -						C_p for -							
		$\beta = -60^\circ$						$\beta = -90^\circ$							
x/l		$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$	$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$
Rear	.410	.247	.261	.242	.221	.194	.142	.064	.400	.239	.253	.260	.261	.226	.159
	.420	.213	.228	.208	.182	.155	.109	.031	.430	.133	.146	.148	.138	.109	.048
	.430	.180	.194	.169	.148	.121	.070	.003	.450	.043	.040	.042	.043	.014	.043
	.450	.085	.093	.074	.042	.026	-.026	-.090	.465	-.277	-.219	-.212	-.216	-.246	-.286
	.460	-.016	-.013	-.039	-.067	-.089	-.136	-.188	.471	-.972	-1.031	-1.011	-.998	-1.046	-1.045
Upper stage	.471	.961	.569	-1.054	-1.109	-1.131	-1.162	-1.161	.471	-.972	-1.031	-1.011	-.998	-1.046	-1.045
	.476	.264	.244	-1.258	-1.245	-1.250	-1.260	-1.308	.491	-.120	-.039	-.026	-.031	-.067	-.112
	.481	.137	.105	-.114	-.101	-.106	-.136	-.164	.511	-.022	.070	.084	.079	.043	-.009
	.491	-.080	-.036	-.039	-.032	-.031	-.003	-.089	.531	.350	.364	.372	.367	.337	.279
	.501	-.028	-.021	.018	.026	.027	.060	.026							
Transition	.511	.030	.079	.076	.084	.084	.060	.026							
	.521	.122	.165	.168	.176	.165	.135	.095							
	.531	.353	.379	.364	.360	.344	.302	.251							
	.539	.274	.266	.235	.213	.192	.151	.105							
	.546	.215	.203	.168	.105	.118	.077	.035							
Main stage	.552	.024	.038	.018	.008	-.014	-.055	-.107	.552	-.002	.007	.008	.004	-.026	-.078
	.562	-.220	-.217	-.238	-.253	-.275	-.312	-.352	.568	-.909	-.907	-.911	-.909	-.946	-.956
	.568	-.808	-.805	-.820	-.824	-.817	-.836	-.846	.587	-.201	-.132	-.124	-.118	-.148	-.188
	.577	-.219	-.192	-.201	-.205	-.199	-.223	-.245	.607	-.138	-.068	-.061	-.054	-.084	-.130
	.587	-.155	-.123	-.126	-.119	-.116	-.142	-.165	.627	-.120	-.045	-.038	-.031	-.067	-.107
Main stage	.597	-.120	-.083	-.086	-.078	-.071	-.101	-.124	.657	-.109	-.028	-.020	-.021	-.051	-.097
	.607	-.109	-.065	-.063	-.061	-.048	-.072	-.101	.697	-.101	-.022	-.011	-.012	-.044	-.088
	.617	-.091	-.054	-.051	-.049	-.042	-.061	-.089	.737	-.092	-.014	-.005	-.006	-.036	-.080
	.627	-.086	-.048	-.045	-.038	-.031	-.055	-.078	.777	-.086	-.010	-.003	-.002	-.030	-.072
	.637	-.080	-.042	-.034	-.032	-.019	-.044	-.072	.785	-.092	-.010	-.002	-.002	-.030	-.072
	.647	-.074	-.031	-.024	-.018	-.016	-.038	-.059	.817	-.082	-.016	-.007	-.002	-.026	-.068
	.657	-.074	-.031	-.024	-.018	-.016	-.038	-.059	.857	-.082	-.011	-.003	-.003	-.030	-.072
	.677	-.063	-.022	-.019	-.014	-.012	-.034	-.053	.897	-.084	-.014	-.006	-.006	-.034	-.073
	.697	-.051	-.013	-.012	-.009	-.008	-.030	-.047							
	.737	-.063	-.015	-.010	-.005	-.002	-.022	-.037							
	.777	-.059	-.011	-.009	-.009	.000	-.019	-.030							
	.785	-.063	-.013	-.009	-.001	.004	-.017	-.030							
	.817	-.053	-.010	-.005	.000	.003	-.016	-.026							
	.857	-.059	-.013	-.010	-.004	-.001	-.019	-.026							
	.877	-.060	-.015	-.011	-.004	-.001	-.018	-.026							
.897	-.060	-.015	-.011	-.005	-.002	-.020	-.027								
.917	-.071	-.022	-.017	-.010	-.007	-.024	-.031								
.937	-.073	-.023	-.018	-.012	-.007	-.023	-.031								
.957	-.139	-.091	-.084	-.072	-.075	-.101	-.122								

TABLE 2.- PRESSURE COEFFICIENTS FOR CONFIGURATION 123 - Continued

(c) $M = 0.80$; $\alpha = -10^\circ$ to 10°

		C_p for $\beta = 0^\circ$						C_p for $\beta = -30^\circ$							
		$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -5^\circ$	$\alpha = 0^\circ$	$\alpha = 5^\circ$	$\alpha = 10^\circ$	$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -5^\circ$	$\alpha = 0^\circ$	$\alpha = 5^\circ$	$\alpha = 10^\circ$		
Main stage	x/l	.456	.370	.312	.262	.212	.169	.126	.410	.348	.301	.254	.208	.165	.111
		.422	.332	.282	.228	.178	.135	.092	.420	.361	.314	.267	.217	.171	.126
		.381	.295	.240	.190	.137	.094	.055	.430	.347	.280	.233	.186	.133	.094
		.450	.379	.313	.245	.183	.133	.093	.450	.345	.285	.237	.189	.146	.100
		.460	.395	.325	.255	.185	.135	.095	.460	.345	.285	.237	.189	.146	.100
		.465	.395	.325	.255	.185	.135	.095	.465	.345	.285	.237	.189	.146	.100
		.471	.404	.334	.264	.194	.144	.104	.471	.354	.294	.244	.194	.144	.104
		.476	.404	.334	.264	.194	.144	.104	.476	.354	.294	.244	.194	.144	.104
		.481	.404	.334	.264	.194	.144	.104	.481	.354	.294	.244	.194	.144	.104
		.491	.404	.334	.264	.194	.144	.104	.491	.354	.294	.244	.194	.144	.104
Transition Plate	x/l	.501	.416	.346	.276	.206	.136	.066	.501	.416	.346	.276	.206	.136	.066
		.511	.426	.356	.286	.216	.146	.076	.511	.426	.356	.286	.216	.146	.076
		.521	.436	.366	.296	.226	.156	.086	.521	.436	.366	.296	.226	.156	.086
		.531	.446	.376	.306	.236	.166	.096	.531	.446	.376	.306	.236	.166	.096
		.547	.462	.392	.322	.252	.182	.112	.547	.462	.392	.322	.252	.182	.112
		.539	.454	.384	.314	.244	.174	.104	.539	.454	.384	.314	.244	.174	.104
		.546	.461	.391	.321	.251	.181	.111	.546	.461	.391	.321	.251	.181	.111
		.552	.468	.398	.328	.258	.188	.118	.552	.468	.398	.328	.258	.188	.118
		.562	.478	.408	.338	.268	.198	.128	.562	.478	.408	.338	.268	.198	.128
		.568	.484	.414	.344	.274	.204	.134	.568	.484	.414	.344	.274	.204	.134
Main stage	x/l	-1.193	-1.228	-1.253	-1.285	-1.293	-1.272	-1.071	-1.049	-1.069	-1.078	-1.102	-1.103	-1.097	-0.970
		-1.132	-1.178	-1.210	-1.239	-1.267	-1.272	-1.266	-1.198	-1.222	-1.239	-1.248	-1.249	-1.249	-1.136
		-0.66	-0.696	-0.709	-0.726	-0.738	-0.736	-0.734	-0.733	-0.733	-0.733	-0.733	-0.733	-0.733	-0.688
		-0.35	-0.361	-0.370	-0.383	-0.388	-0.382	-0.376	-0.38	-0.38	-0.38	-0.38	-0.38	-0.38	-0.38
		-0.15	-0.145	-0.145	-0.144	-0.145	-0.145	-0.145	-0.145	-0.145	-0.145	-0.145	-0.145	-0.145	-0.145
		-0.04	-0.034	-0.033	-0.033	-0.033	-0.033	-0.033	-0.033	-0.033	-0.033	-0.033	-0.033	-0.033	-0.033
		-0.16	-0.16	-0.16	-0.16	-0.16	-0.16	-0.16	-0.16	-0.16	-0.16	-0.16	-0.16	-0.16	-0.16
		-0.057	-0.057	-0.057	-0.057	-0.057	-0.057	-0.057	-0.057	-0.057	-0.057	-0.057	-0.057	-0.057	-0.057
		-0.033	-0.033	-0.033	-0.033	-0.033	-0.033	-0.033	-0.033	-0.033	-0.033	-0.033	-0.033	-0.033	-0.033
		-0.03	-0.03	-0.03	-0.03	-0.03	-0.03	-0.03	-0.03	-0.03	-0.03	-0.03	-0.03	-0.03	-0.03

TABLE 8.- PRESSURE COEFFICIENTS FOR CONFIGURATION 123 - Continued

(c) $M = 0.80$; $\alpha = -10^\circ$ to 10° - Concluded

		C_p for $\beta = -60^\circ$						C_p for $\beta = -90^\circ$									
		$\alpha = -10^\circ$		$\alpha = -5^\circ$		$\alpha = 0^\circ$		$\alpha = -10^\circ$		$\alpha = -5^\circ$		$\alpha = 0^\circ$		$\alpha = 5^\circ$		$\alpha = 10^\circ$	
		x/l						x/l									
Nose		.410	.305	.278	.250	.220	.180	.111	.400	.226	.276	.297	.299	.287	.267	.213	
		.420	.272	.261	.240	.182	.139	.073	.430	.121	.163	.180	.179	.167	.143	.092	
		.430	.238	.203	.179	.144	.105	.040	.450	.035	.073	.086	.085	.073	.049	.002	
		.460	.144	.129	.085	.050	.011	-.053	.465	-.191	-.151	-.137	-.138	-.147	-.168	-.209	
		.465	-.120	-.090	-.083	-.092	-.102	-.127	.471	-1.137	-1.102	-1.103	-1.085	-1.082	-1.080	-1.105	
Upper stage		.471	-1.250	-1.262	-1.268	-1.304	-1.275	-1.253	.491	-.100	-.049	-.027	-.017	-.026	-.047	-.103	
		.476	-.437	-.491	-.528	-.553	-.558	-.537	.491	-.100	-.049	-.027	-.017	-.026	-.047	-.103	
		.481	-.174	-.239	-.277	-.270	-.283	-.312	.511	.024	.083	.104	.111	.099	.073	.021	
		.491	-.054	-.020	-.017	-.022	-.035	-.076	.531	.345	.389	.391	.358	.393	.372	.316	
		.501	.004	.032	.046	.046	.027	-.006									
Transition flange		.511	.074	.102	.112	.106	.089	.056									
		.521	.179	.203	.204	.195	.174	.141									
		.531	.415	.424	.407	.366	.337	.289									
		.539	.361	.323	.295	.224	.184	.144									
		.546	.301	.254	.231	.157	.117	.077									
Main stage		.562	-.109	-.124	-.141	-.198	-.227	-.272	.552	.012	.047	.065	.056	.051	.027	-.018	
		.568	-1.252	-1.251	-1.264	-1.290	-1.311	-1.308	.568	-1.306	-1.294	-1.284	-1.293	-1.301	-1.303	-1.312	
		.577	-.221	-.213	-.210	-.236	-.261	-.321	.587	-.182	-.131	-.125	-.122	-.131	-.140	-.193	
		.587	-.151	-.127	-.117	-.126	-.140	-.169	.607	-.132	-.084	-.063	-.064	-.072	-.090	-.134	
		.597	-.116	-.088	-.078	-.083	-.101	-.123	.627	-.108	-.061	-.043	-.044	-.053	-.066	-.115	
Main stage		.607	-.097	-.069	-.059	-.064	-.068	-.088	.627	-.108	-.061	-.043	-.044	-.053	-.066	-.115	
		.617	-.089	-.061	-.051	-.052	-.055	-.080	.657	-.090	-.048	-.029	-.024	-.032	-.055	-.103	
		.627	-.081	-.057	-.043	-.044	-.049	-.076	.657	-.090	-.048	-.029	-.024	-.032	-.055	-.103	
		.637	-.070	-.049	-.035	-.037	-.041	-.076	.697	-.083	-.040	-.020	-.015	-.023	-.043	-.094	
		.657	-.063	-.039	-.025	-.022	-.027	-.064	.737	-.074	-.032	-.015	-.009	-.017	-.037	-.081	
		.677	-.048	-.029	-.019	-.023	-.036	-.039	.777	-.068	-.029	-.009	-.004	-.013	-.033	-.076	
		.697	-.033	-.020	-.013	-.018	-.024	-.041	.785	-.072	-.031	-.012	-.005	-.011	-.031	-.073	
		.737	-.044	.022	-.012	-.009	-.018	-.032	.817	-.060	-.021	-.004	-.001	-.009	-.027	-.066	
		.777	-.040	-.018	-.007	-.004	-.010	-.031	.857	-.065	-.029	-.011	-.006	-.013	-.032	-.070	
		.817	-.045	-.023	-.002	-.002	-.008	-.024	.897	-.066	-.031	-.013	-.008	-.016	-.035	-.072	
		.857	-.039	-.016	-.008	-.006	-.011	-.019									
		.877	-.041	-.020	-.009	-.007	-.012	-.027									
		.897	-.041	-.022	-.009	-.007	-.013	-.020									
		.917	-.050	-.027	-.015	-.012	-.017	-.025									
		.957	-.055	-.034	-.021	-.012	-.027	-.042									
	.997	-.124	-.102	-.083	-.077	-.090	-.123										

TABLE 8.- PRESSURE COEFFICIENTS FOR CONFIGURATION 123 - Continued

(a) $M = 1.00$; $\alpha = -10^\circ$ to 10°

		C_p for $\beta = 0^\circ$						
		$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$
Main stage	x/t	.565	.473	.416	.370	.322	.284	.232
		.519	.443	.392	.346	.298	.251	.202
Transition flare	x/t	.483	.407	.356	.307	.262	.219	.166
		.405	.336	.288	.241	.196	.153	.101
Nose	x/t	.460	.396	.347	.300	.255	.212	.165
		.465	.400	.351	.304	.259	.216	.171
Main stage	x/t	.471	.414	.366	.319	.274	.231	.184
		.428	.362	.314	.267	.222	.178	.130
Transition flare	x/t	.491	.428	.379	.332	.287	.244	.198
		.425	.358	.310	.263	.218	.173	.127
Nose	x/t	.420	.357	.308	.261	.216	.171	.125
		.430	.367	.318	.271	.226	.181	.135
Main stage	x/t	.447	.384	.335	.288	.243	.198	.152
		.369	.302	.253	.206	.161	.116	.070
Transition flare	x/t	.452	.389	.340	.293	.248	.203	.157
		.375	.308	.259	.212	.167	.122	.076
Nose	x/t	.477	.414	.365	.318	.273	.228	.182
		.420	.353	.304	.257	.212	.167	.121
Main stage	x/t	.510	.447	.398	.351	.306	.261	.215
		.455	.388	.339	.292	.247	.202	.156
Transition flare	x/t	.475	.412	.363	.316	.271	.226	.181
		.420	.353	.304	.257	.212	.167	.121
Nose	x/t	.568	.505	.456	.409	.364	.319	.273
		.511	.444	.395	.348	.303	.258	.212
Main stage	x/t	.617	.554	.505	.458	.413	.368	.322
		.560	.493	.444	.397	.352	.307	.261
Transition flare	x/t	.627	.564	.515	.468	.423	.378	.332
		.570	.503	.454	.407	.362	.317	.271
Nose	x/t	.646	.583	.534	.487	.442	.397	.351
		.589	.522	.473	.426	.381	.336	.290
Main stage	x/t	.677	.614	.565	.518	.473	.428	.382
		.620	.553	.504	.457	.412	.367	.321
Transition flare	x/t	.697	.634	.585	.538	.493	.448	.402
		.640	.573	.524	.477	.432	.387	.341
Nose	x/t	.737	.674	.625	.578	.533	.488	.442
		.680	.613	.564	.517	.472	.427	.381
Main stage	x/t	.777	.714	.665	.618	.573	.528	.482
		.720	.653	.604	.557	.512	.467	.421
Transition flare	x/t	.817	.754	.705	.658	.613	.568	.522
		.760	.693	.644	.597	.552	.507	.461
Nose	x/t	.877	.814	.765	.718	.673	.628	.582
		.820	.753	.704	.657	.612	.567	.521
Main stage	x/t	.917	.854	.805	.758	.713	.668	.622
		.860	.793	.744	.697	.652	.607	.561
Transition flare	x/t	.957	.894	.845	.798	.753	.708	.662
		.900	.833	.784	.737	.692	.647	.601
Nose	x/t	.997	.934	.885	.838	.793	.748	.702
		.940	.873	.824	.777	.732	.687	.641

TABLE 2.- PRESSURE COEFFICIENTS FOR CONFIGURATION 123 - Continued

(d) $M = 1.00$; $\alpha = -10^\circ$ to 10° - Concluded

		C_p for $\beta = -50^\circ$							C_p for $\beta = -30^\circ$							
		$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -5^\circ$	$\alpha = 0^\circ$	$\alpha = 5^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$	$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -5^\circ$	$\alpha = 0^\circ$	$\alpha = 5^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$	
Nozzle	x/l	.410	.402	.383	.364	.331	.290	.220	.400	.327	.383	.404	.406	.397	.374	.322
		.420	.368	.353	.334	.298	.257	.187								
Main stage	x/l	.430	.345	.323	.304	.268	.224	.154	.430	.234	.282	.293	.304	.292	.263	.208
		.450	.276	.257	.235	.202	.162	.089	.450	.171	.219	.231	.235	.223	.198	.136
Transition	x/l	.460	.216	.204	.184	.151	.111	.044	.465	.037	.087	.102	.106	.100	.075	.014
		.465	.191	.183	.126	.129	.152	.181	.471	.625	.576	.561	.554	.544	.546	.596
Flare	x/l	.471	.715	.709	.715	.702	.710	.739	.491	.277	.456	.463	.480	.480	.484	.245
		.476	.665	.681	.708	.729	.740	.692	.511	.016	.112	.139	.079	.131	.111	.020
Upper stage	x/l	.481	.517	.598	.628	.665	.658	.656	.531	.380	.432	.410	.264	.412	.417	.356
		.501	.135	.422	.313	.208	.250	.217								
Transition	x/l	.511	.130	.197	.088	.045	.086	.158								
		.521	.272	.176	.174	.187	.164	.070								
Flare	x/l	.531	.503	.497	.447	.310	.318	.221								
		.539	.500	.484	.453	.370	.290	.258								
Main stage	x/l	.546	.445	.433	.395	.366	.282	.238								
		.552	.275	.308	.291	.282	.223	.130								
Transition	x/l	.562	.138	.156	.143	.114	.073	.005								
		.568	.710	.705	.701	.719	.736	.771								
Flare	x/l	.577	.565	.575	.521	.623	.662	.713								
		.587	.417	.458	.410	.478	.551	.604								
Main stage	x/l	.597	.324	.336	.336	.339	.411	.443								
		.607	.290	.287	.280	.271	.288	.307								
Transition	x/l	.617	.271	.250	.227	.218	.229	.261								
		.627	.271	.216	.181	.175	.192	.224								
Flare	x/l	.637	.253	.167	.144	.141	.158	.196								
		.657	.183	.129	.098	.101	.119	.147								
Main stage	x/l	.677	.150	.104	.085	.086	.104	.127								
		.697	.117	.079	.067	.071	.090	.107								
Transition	x/l	.737	.117	.060	.058	.061	.078	.087								
		.777	.101	.045	.046	.038	.067	.058								
Flare	x/l	.785	.100	.059	.041	.043	.063	.040								
		.817	.090	.033	.040	.040	.061	.015								
Main stage	x/l	.857	.062	.058	.016	.009	.065	.002								
		.877	.021	.032	.009	.022	.052	.003								
Transition	x/l	.897	.019	.028	.028	.027	.026	.001								
		.917	.022	.012	.026	.023	.005	.003								
Flare	x/l	.937	.023	.008	.014	.011	.004	.016								
		.957	.022	.004	.017	.011	.004	.016								
Main stage	x/l	.997	.098	.084	.096	.107	.127	.149								

TABLE 8.- PRESSURE COEFFICIENTS FOR CONFIGURATION 125 - Continued

(e) $M = 1.20$; $\alpha = -10^\circ$ to 10°

		C_p for $\beta = 0^\circ$						C_p for $\beta = -30^\circ$							
		$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -5^\circ$	$\alpha = 0^\circ$	$\alpha = 5^\circ$	$\alpha = 10^\circ$	$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -5^\circ$	$\alpha = 0^\circ$	$\alpha = 5^\circ$	$\alpha = 10^\circ$		
Main stage	Moist	.509	.417	.363	.956	.272	.230	.194	.477	.399	.355	.303	.277	.228	.183
	Moist	.519	.431	.371	.308	.282	.241	.199	.420	.409	.355	.305	.277	.233	.178
	Moist	.503	.423	.363	.319	.272	.241	.188	.430	.412	.355	.311	.274	.244	.180
	Moist	.450	.415	.358	.319	.269	.233	.183	.460	.399	.350	.316	.269	.236	.172
	Moist	.460	.469	.399	.352	.277	.230	.178	.439	.368	.347	.313	.277	.233	.162
	Moist	.465	.431	.334	.297	.264	.222	.172	.405	.361	.328	.297	.277	.225	.162
	Moist	.471	.200	.215	.233	.251	.272	.307	.291	.311	.325	.341	.362	.385	.415
	Moist	.476	.334	.354	.372	.390	.402	.421	.293	.336	.354	.369	.382	.408	.435
	Moist	.481	.273	.304	.331	.349	.369	.396	.303	.336	.354	.369	.382	.408	.435
	Moist	.491	.183	.219	.254	.280	.304	.330	.245	.301	.326	.350	.368	.394	.421
Transition	Moist	.501	.045	.122	.191	.217	.232	.130	.108	.180	.214	.245	.272	.301	.326
	Moist	.511	.028	.115	.141	.162	.173	.073	.075	.133	.159	.191	.214	.232	.259
	Moist	.521	.023	.102	.120	.135	.140	.073	.061	.108	.126	.147	.164	.182	.201
	Moist	.531	.524	.390	.320	.232	.213	.186	.496	.430	.377	.317	.244	.188	.142
	Moist	.539	.642	.510	.414	.298	.234	.216	.539	.506	.478	.419	.396	.354	.265
	Moist	.546	.574	.500	.441	.333	.264	.243	.546	.444	.423	.438	.409	.365	.273
	Moist	.552	.526	.451	.414	.333	.267	.243	.552	.468	.448	.414	.355	.300	.243
	Moist	.562	.428	.348	.305	.230	.172	.140	.562	.362	.337	.297	.252	.207	.159
	Moist	.568	.334	.371	.387	.306	.234	.216	.568	.343	.355	.356	.372	.394	.420
	Moist	.577	.241	.272	.288	.259	.236	.227	.577	.280	.300	.304	.295	.307	.315
Main stage	Moist	.587	.197	.239	.255	.247	.254	.254	.587	.197	.228	.244	.237	.247	.265
	Moist	.597	.081	.184	.208	.221	.230	.246	.597	.114	.140	.150	.160	.164	.172
	Moist	.607	.050	.146	.166	.188	.200	.205	.607	.078	.122	.151	.166	.164	.172
	Moist	.617	.039	.121	.139	.154	.161	.155	.617	.064	.103	.123	.139	.152	.159
	Moist	.627	.025	.109	.114	.124	.123	.108	.627	.059	.089	.104	.124	.128	.125
	Moist	.637	.014	.079	.087	.091	.090	.073	.637	.048	.076	.092	.097	.098	.092
	Moist	.657	.020	.056	.066	.055	.045	.035	.657	.041	.055	.064	.067	.068	.059
	Moist	.677	.019	.031	.043	.038	.025	.021	.677	.038	.044	.051	.051	.051	.047
	Moist	.697	.010	.026	.033	.026	.012	.008	.697	.032	.040	.036	.036	.032	.047
	Moist	.737	.018	.026	.036	.026	.023	.008	.737	.042	.037	.028	.026	.025	.047
Main stage	Moist	.777	.016	.030	.024	.026	.014	.005	.777	.010	.021	.019	.024	.027	.046
	Moist	.817	.024	.004	.016	.016	.012	.006	.817	.002	.015	.017	.024	.027	.057
	Moist	.857	.022	.004	.022	.020	.011	.006	.857	.000	.015	.019	.018	.022	.053
	Moist	.877	.033	.008	.004	.001	.006	.010	.877	.006	.004	.010	.010	.021	.069
	Moist	.877	.033	.008	.004	.001	.006	.010	.877	.003	.010	.010	.010	.021	.071
	Moist	.897	.014	.001	.005	.010	.015	.018	.897	.010	.005	.005	.006	.020	.068
	Moist	.917	.009	.004	.004	.001	.006	.010	.917	.009	.004	.006	.006	.020	.068
	Moist	.957	.012	.015	.015	.015	.015	.015	.957	.012	.015	.015	.016	.019	.046
	Moist	.997	.001	.021	.036	.036	.036	.036	.997	.001	.021	.036	.036	.036	.036
	Moist	.997	.001	.021	.036	.036	.036	.036	.997	.001	.021	.036	.036	.036	.036

TABLE 6.- PRESSURE COEFFICIENTS FOR CONFIGURATION 123 - Concluded

(e) $M = 1.20$; $\alpha = -10^\circ$ to 10° - Concluded

x/l	C_p for $\beta = -9^\circ$						
	$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$
	Moore	.293	.289	.312	.311	.306	.294
	.400	.253	.312	.311	.306	.294	.258
	.430	.295	.302	.308	.304	.286	.236
	.450	.300	.302	.316	.298	.289	.234
	.465	.249	.275	.276	.269	.246	.188
	.471	-.269	-.245	-.244	-.227	-.245	-.288
	.491	-.259	-.252	-.259	-.269	-.282	-.306
	.511	-.174	-.153	-.147	-.157	-.177	-.232
	.531	.277	.330	.306	.324	.300	.238
	.552	.379	.407	.408	.401	.362	.278
Transition layer	.568	-.401	-.391	-.378	-.391	-.406	-.439
	.587	-.306	-.261	-.241	-.265	-.288	-.329
	.607	-.235	-.176	-.164	-.174	-.203	-.246
	.627	-.216	-.136	-.117	-.116	-.137	-.227
	.657	-.153	-.080	-.049	-.055	-.088	-.154
	.697	-.147	-.082	-.043	-.052	-.075	-.150
	.737	-.118	-.066	-.034	-.034	-.063	-.125
	.777	-.083	-.049	-.028	-.024	-.049	-.103
	.785	-.093	-.053	-.023	-.023	-.049	-.106
	.817	-.083	-.030	-.015	-.019	-.041	-.093
	.857	-.086	-.030	-.019	-.032	-.051	-.090
	.897	-.089	-.042	-.006	-.007	-.027	-.078
	.186	.238	.280	.303	.280	.238	.186
	.188	.249	.285	.311	.285	.249	.188
	.180	.252	.282	.311	.282	.252	.180
	.183	.254	.285	.313	.285	.254	.183
	.175	.246	.288	.313	.288	.246	.175
	.202	.164	.141	.139	.141	.164	.202
	.412	-.391	-.381	-.371	-.381	-.391	.412
	.448	-.419	-.406	-.388	-.406	-.419	.448
	.443	-.394	-.365	-.344	-.365	-.394	.443
	.330	-.293	-.267	-.251	-.267	-.293	.330
	.273	-.235	-.212	-.193	-.212	-.235	.273
	.084	-.068	-.148	-.147	-.148	-.068	.084
	.145	.160	.203	.216	.203	.160	.145
	.229	.229	.280	.309	.280	.229	.229
	.202	.286	.344	.417	.344	.286	.202
	.239	.318	.376	.446	.376	.318	.239
	.251	.337	.379	.408	.379	.337	.251
	.173	.245	.276	.297	.276	.245	.173
	.444	.406	.386	.378	.386	.406	.444
	.422	.373	.336	.310	.336	.373	.422
	.370	.313	.276	.241	.276	.313	.370
	.312	.247	.212	.194	.212	.247	.312
	.224	.183	.168	.164	.168	.183	.224
	.183	.153	.143	.139	.143	.153	.183
	.169	.137	.124	.120	.124	.137	.169
	.144	.097	.091	.095	.097	.112	.144
	.119	.076	.051	.043	.051	.076	.119
	.104	.063	.046	.038	.046	.063	.104
	.088	.050	.042	.033	.042	.050	.088
	.066	.051	.033	.032	.033	.051	.066
	.038	.027	.027	.020	.027	.038	.038
	.053	.029	.020	.011	.020	.029	.053
	.051	.029	.016	.016	.029	.051	.051
	.049	.032	.018	.018	.032	.049	.049
	.044	.022	.010	.005	.022	.044	.044
	.035	.018	.004	.001	.018	.035	.035
	.031	.009	.004	.001	.009	.031	.031
	.034	.007	.004	.001	.007	.034	.034
	.019	.016	.017	.017	.016	.019	.019
	.089	.047	.045	.055	.047	.089	.089
	.106	.089	.087	.089	.089	.106	.106
	.365	.345	.328	.303	.328	.345	.365
	.375	.356	.331	.311	.331	.356	.375
	.373	.359	.328	.311	.328	.359	.373
	.362	.351	.331	.313	.331	.351	.362
	.341	.343	.328	.313	.328	.343	.341
	.188	.161	.143	.139	.143	.161	.188
	.382	.371	.367	.371	.367	.382	.382
	.371	.380	.381	.388	.381	.371	.371
	.283	.314	.326	.344	.326	.283	.283
	.201	.226	.241	.251	.241	.201	.201
	.163	.174	.181	.193	.181	.163	.163
	.141	.139	.137	.147	.137	.141	.141
	.105	.032	.154	.216	.154	.105	.105
	.384	.372	.357	.309	.357	.384	.384
	.591	.555	.502	.417	.502	.555	.591
	.546	.530	.497	.446	.497	.546	.546
	.390	.419	.424	.408	.424	.390	.390
	.306	.322	.315	.297	.315	.306	.306
	.386	.373	.374	.378	.374	.386	.386
	.315	.315	.314	.310	.314	.315	.315
	.229	.244	.250	.241	.250	.229	.229
	.174	.183	.195	.194	.183	.174	.174
	.155	.153	.157	.164	.153	.155	.155
	.144	.139	.135	.139	.135	.144	.144
	.141	.122	.118	.120	.122	.141	.141
	.125	.103	.118	.120	.103	.125	.125
	.064	.064	.064	.064	.064	.064	.064
	.111	.062	.047	.043	.047	.111	.111
	.098	.061	.039	.038	.061	.098	.098
	.069	.055	.034	.032	.055	.069	.069
	.069	.042	.029	.020	.042	.069	.069
	.058	.041	.023	.011	.041	.058	.058
	.057	.028	.014	.016	.028	.057	.057
	.064	.017	.017	.018	.017	.064	.064
	.054	.029	.010	.005	.029	.054	.054
	.071	.054	.029	.001	.054	.071	.071
	.071	.033	.018	.007	.033	.071	.071
	.069	.036	.017	.016	.036	.069	.069
	.061	.047	.045	.055	.047	.061	.061

TABLE 9.- PRESSURE COEFFICIENTS FOR CONFIGURATION 223

(a) $M = 0.40$ to 0.95 ; $\alpha = 0^\circ$

		C_p for -													
		$\beta = 0^\circ$													
		$M = 0.40$	$M = 0.70$	$M = 0.75$	$M = 0.85$	$M = 0.90$	$M = 0.95$	$M = 0.40$	$M = 0.70$	$M = 0.75$	$M = 0.85$	$M = 0.90$	$M = 0.95$		
Nose	x/l	.428	.395	.436	.453	.499	.524	.561	.438	.307	.362	.360	.405	.430	.474
		.438	.307	.346	.360	.408	.440	.474	.448	.198	.248	.247	.267	.278	.291
Upper stage		.458	.068	.231	.247	.306	.343	.384	.458	.057	.101	.134	.192	.244	.291
		.471	-1.159	-1.173	-1.118	-1.062	-.943	-.813	.471	-1.283	-1.275	-1.248	-1.137	-1.054	-.919
Upper stage		.481	-.278	-.676	-.720	-.834	-.867	-.978	.476	-.300	-.653	-.681	-.644	-.662	-.933
		.491	-.042	-.345	-.449	-.568	-.535	-.653	.449	-.143	-.336	-.481	-.449	-.579	-.694
Upper stage		.501	.014	.027	.034	-.038	-.111	-.163	.501	.042	.027	.096	.038	.357	-.288
		.511	.070	.086	.096	.084	.060	-.032	.511	.070	.086	.096	.091	.142	-.042
Transition Plate		.521	.149	.174	.180	.181	.174	.108	.521	.160	.178	.180	.181	.168	-.083
		.531	.339	.343	.338	.302	.312	.265	.531	.339	.348	.342	.306	.268	-.023
Transition Plate		.539	.191	.212	.223	.246	.275	.331	.539	.191	.217	.231	.253	.278	.350
		.546	.102	.121	.136	.182	.219	.306	.546	.047	.076	.091	.139	.182	.274
Transition Plate		.552	.014	.026	.038	.093	.145	.230	.552	.014	.026	.042	.093	.145	.217
		.562	-.235	-.233	-.206	-.114	-.045	.047	.562	-.235	-.237	-.210	-.129	-.075	.009
Main stage		.568	-.628	-1.005	-1.115	-1.110	-.971	-.830	.568	-.583	-.862	-.982	-1.059	-.921	-.776
		.577	-.189	-.222	-.225	-.290	-.722	-.619	.577	-.177	-.213	-.217	-.268	-.268	-.558
Main stage		.587	-.076	-.130	-.129	-.106	-.220	-.520	.587	-.110	-.130	-.129	-.106	-.106	-.481
		.607	-.054	-.088	-.087	-.074	-.048	-.401	.607	-.076	-.070	-.070	-.060	-.044	-.318
Main stage		.617	-.042	-.065	-.062	-.060	-.024	-.289	.617	-.054	-.065	-.062	-.060	-.044	-.298
		.627	-.042	-.052	-.050	-.049	-.024	-.148	.627	-.042	-.052	-.050	-.049	-.027	-.164
Main stage		.637	-.020	-.033	-.029	-.031	-.021	-.052	.637	-.031	-.042	-.041	-.042	-.027	-.055
		.647	-.016	-.022	-.019	-.021	-.017	.017	.647	-.020	-.024	-.020	-.023	-.024	-.010
Main stage		.677	-.012	-.019	-.015	-.018	-.016	.010	.677	-.009	-.013	-.009	-.012	-.020	.012
		.697	-.009	-.016	-.011	-.014	-.014	.005	.697	-.009	-.016	-.009	-.014	-.011	.015
Main stage		.737	-.009	-.013	-.008	-.012	-.013	-.009	.737	-.005	-.012	-.006	-.009	-.014	.003
		.777	-.001	-.009	-.004	-.006	-.007	-.009	.777	-.001	-.006	-.004	-.009	-.011	.008
Main stage		.785	.003	-.002	.002	.000	.007	-.007	.785	.003	-.002	-.004	-.001	-.005	.006
		.817	.001	-.002	.000	.003	.005	-.008	.817	.001	-.002	-.002	-.001	-.002	.006
Main stage		.857	.001	-.005	-.003	-.006	-.008	-.013	.857	.003	-.007	-.004	-.003	-.004	.008
		.877	-.003	-.005	-.002	-.006	-.008	-.013	.877	-.004	-.007	-.004	-.007	-.009	.015
Main stage		.897	-.006	-.008	-.005	-.009	-.011	-.016	.897	-.006	-.008	-.006	-.008	-.010	.015
									.917	-.006	-.008	-.006	-.009	-.011	.017
									.957	-.016	-.020	-.018	-.021	-.018	.018
									.997	-.069	-.076	-.076	-.080	-.088	-.104

TABLE 9.-- PRESSURE COEFFICIENTS FOR CONFIGURATION 223 - Continued

(a) M = 0.40 to 0.95; $\alpha = 0^\circ$ - Concluded

		C_p for -					
		$\beta = -60^\circ$					
		M = 0.40	M = 0.70	M = 0.85	M = 0.90	M = 0.95	
Nozzle	x/l	.307	.338	.360	.401	.430	.474
		.198	.248	.267	.314	.348	.393
		.068	.115	.138	.206	.247	.297
		.471	-1.227	-1.080	-1.054	-0.987	-0.855
		.476	-.289	-.662	-.691	-.682	-.565
		.481	-.143	-.474	-.547	-.538	-.474
		.491	-.042	-.083	-.314	-.343	-.285
		.501	.014	.042	-.060	-.135	-.167
		.511	.070	.101	.087	.040	-.045
		.521	.149	.180	.173	.157	.083
Upper stage	x/l	.531	.334	.330	.277	.255	.217
		.539	.191	.223	.249	.282	.375
		.546	.091	.132	.182	.225	.321
		.552	.014	.038	.086	.132	.205
		.562	-.235	-.242	-.136	-.075	.009
		.568	-.639	-.991	-1.113	-.971	-.871
		.577	-.177	-.213	-.217	-.254	-.564
		.587	-.110	-.130	-.133	-.114	-.452
		.597	-.076	-.084	-.083	-.074	-.372
		.607	-.054	-.065	-.062	-.060	-.298
Transition Flare	x/l	.617	-.042	-.050	-.049	-.031	-.167
		.627	-.031	-.042	-.041	-.031	-.058
		.637	-.020	-.033	-.033	-.027	-.016
		.657	-.020	-.024	-.020	-.020	.010
		.677	-.014	-.019	-.015	-.016	.012
		.697	-.009	-.013	-.009	-.012	.004
		.737	-.005	-.012	-.006	-.009	.007
		.777	-.001	-.009	-.002	-.005	.008
		.785	-.001	-.006	-.002	-.005	.007
		.817	.000	-.001	.001	-.002	.008
Main stage	x/l	.857	-.003	-.006	-.004	-.007	.014
		.877	-.004	-.007	-.004	-.007	.015
		.897	-.006	-.007	-.005	-.008	.016
		.917	-.009	-.013	-.010	-.014	.021
		.957	-.016	-.019	-.018	-.021	.030
		.997	-.069	-.076	-.075	-.081	.104

		C_p for -							
		$\beta = -90^\circ$							
		M = 0.40	M = 0.70	M = 0.85	M = 0.90	M = 0.95			
Nozzle	x/l	.384	.431	.449	.492	.518	.554		
		.198	.240	.263	.311	.348	.387		
		.068	.106	.134	.199	.244	.294		
		.471	-1.243	-1.151	-1.159	-1.031	-.893		
	Upper stage	x/l	-.042	-.047	-.083	-.285	-.330	-.297	
			.070	.086	.101	.080	.033	-.045	
			.339	.343	.334	.288	.268	.198	
		Transition Flare	x/l	.003	.022	.038	.086	.136	.205
				.568	-1.037	-1.107	-1.128	-.978	-.834
				.587	-.110	-.133	-.110	-.186	-.449
			.607	-.054	-.062	-.060	-.034	-.295	
			.627	-.031	-.042	-.042	-.031	-.058	
			.657	-.020	-.024	-.024	-.021	.008	
			.697	-.009	-.016	-.012	-.015	.001	
	.737		-.005	-.012	-.006	-.011	.007		
	.777		-.001	-.009	-.005	-.006	.008		
	.785		-.001	-.009	-.008	-.005	.008		
Main stage	x/l	.817	.000	.000	-.003	-.003	.006		
		.857	-.003	-.005	-.007	-.007	.014		
		.897	-.006	-.008	-.006	-.007	.015		
		.917	-.009	-.013	-.010	-.014	.021		
		.957	-.016	-.019	-.018	-.021	.030		
		.997	-.069	-.076	-.075	-.081	.104		

TABLE 9.- PRESSURE COEFFICIENTS FOR CONFIGURATION 225 - Continued

(b) $k = 0.60$; $\alpha = -10^\circ$ to 10°

		C_p for $\beta = 0^\circ$						C_p for $\beta = -30^\circ$							
		$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$	$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$
Nose	x/l	.428	.479	.425	.425	.355	.294	.205	.551	.479	.425	.355	.294	.205	.121
		.438	.390	.326	.326	.261	.205	.127	.457	.390	.326	.261	.205	.127	.038
Upper stage	x/l	.448	.263	.204	.204	.142	.089	.015	.458	.263	.204	.142	.089	.015	.109
		.458	.208	.082	.082	.023	-.028	-.097	.471	.208	.082	.023	-.028	-.097	.038
Transition flaps	x/l	.471	-1.219	-1.348	-1.348	-1.283	-1.163	-1.049	.471	-1.219	-1.348	-1.283	-1.163	-1.049	.112
		.481	-.265	-.327	-.383	-.472	-.547	-.656	.476	-.265	-.327	-.383	-.472	-.547	.087
Main stage	x/l	.481	-.123	-.172	-.172	-.193	-.227	-.331	.481	-.123	-.172	-.193	-.227	-.331	.274
		.491	-.020	-.042	-.046	-.050	-.045	-.051	.491	-.020	-.042	-.046	-.050	-.051	.088
Transition flaps	x/l	.501	.037	.020	.011	.018	.015	.023	.501	.037	.020	.011	.015	.023	.006
		.511	.100	.073	.073	.075	.075	.048	.511	.100	.073	.075	.075	.048	.051
Main stage	x/l	.521	.191	.159	.159	.149	.149	.125	.521	.191	.159	.149	.149	.125	.120
		.531	.436	.347	.347	.309	.280	.228	.531	.436	.347	.309	.280	.228	.239
Transition flaps	x/l	.539	.285	.245	.208	.170	.141	.096	.539	.285	.245	.208	.181	.153	.079
		.546	.189	.144	.106	.074	.046	.006	.546	.189	.144	.106	.074	.046	.069
Main stage	x/l	.552	.099	.048	.010	-.028	-.051	-.092	.552	.099	.048	.010	-.028	-.051	.051
		.562	-.153	-.210	-.242	-.270	-.287	-.305	.562	-.153	-.210	-.242	-.270	-.287	.334
Transition flaps	x/l	.568	.770	.814	.801	.771	.709	.664	.568	.770	.814	.801	.771	.709	.684
		.577	.169	.191	.127	.125	.119	.126	.577	.169	.191	.127	.125	.119	.283
Main stage	x/l	.587	.060	.083	.086	.085	.074	.086	.587	.060	.083	.086	.085	.074	.030
		.607	.043	.060	.064	.062	.051	.063	.607	.043	.060	.064	.062	.051	.030
Transition flaps	x/l	.617	.031	.048	.052	.045	.039	.046	.617	.031	.048	.052	.045	.039	.057
		.627	.020	.037	.041	.039	.028	.034	.627	.020	.037	.041	.039	.028	.057
Main stage	x/l	.637	.003	.018	.020	.018	.009	.011	.637	.003	.018	.020	.018	.009	.048
		.647	-.010	.014	.018	.014	.005	.010	.647	-.010	.014	.018	.014	.005	.034
Transition flaps	x/l	.657	.003	.010	.012	.011	.003	.006	.657	.003	.010	.012	.011	.003	.029
		.667	.005	.012	.012	.009	.001	.008	.667	.005	.012	.012	.009	.001	.029
Main stage	x/l	.677	.009	.014	.006	.005	.003	.006	.677	.009	.014	.006	.005	.003	.029
		.687	.009	.014	.006	.005	.003	.006	.687	.009	.014	.006	.005	.003	.029
Transition flaps	x/l	.697	.014	.006	.003	.001	.003	.002	.697	.014	.006	.003	.001	.003	.029
		.707	.010	.006	.003	.001	.003	.002	.707	.010	.006	.003	.001	.003	.029
Main stage	x/l	.717	.006	.006	.003	.001	.003	.002	.717	.006	.006	.003	.001	.003	.029
		.727	.006	.006	.003	.001	.003	.002	.727	.006	.006	.003	.001	.003	.029
Transition flaps	x/l	.737	.010	.006	.003	.001	.003	.002	.737	.010	.006	.003	.001	.003	.029
		.747	.006	.006	.003	.001	.003	.002	.747	.006	.006	.003	.001	.003	.029
Main stage	x/l	.757	.006	.006	.003	.001	.003	.002	.757	.006	.006	.003	.001	.003	.029
		.767	.006	.006	.003	.001	.003	.002	.767	.006	.006	.003	.001	.003	.029
Transition flaps	x/l	.777	.006	.006	.003	.001	.003	.002	.777	.006	.006	.003	.001	.003	.029
		.787	.006	.006	.003	.001	.003	.002	.787	.006	.006	.003	.001	.003	.029
Main stage	x/l	.797	.006	.006	.003	.001	.003	.002	.797	.006	.006	.003	.001	.003	.029
		.807	.006	.006	.003	.001	.003	.002	.807	.006	.006	.003	.001	.003	.029
Transition flaps	x/l	.817	.006	.006	.003	.001	.003	.002	.817	.006	.006	.003	.001	.003	.029
		.827	.006	.006	.003	.001	.003	.002	.827	.006	.006	.003	.001	.003	.029
Main stage	x/l	.837	.006	.006	.003	.001	.003	.002	.837	.006	.006	.003	.001	.003	.029
		.847	.006	.006	.003	.001	.003	.002	.847	.006	.006	.003	.001	.003	.029
Transition flaps	x/l	.857	.006	.006	.003	.001	.003	.002	.857	.006	.006	.003	.001	.003	.029
		.867	.006	.006	.003	.001	.003	.002	.867	.006	.006	.003	.001	.003	.029
Main stage	x/l	.877	.006	.006	.003	.001	.003	.002	.877	.006	.006	.003	.001	.003	.029
		.887	.006	.006	.003	.001	.003	.002	.887	.006	.006	.003	.001	.003	.029

TABLE 1.- PRESSURE COEFFICIENTS FOR CONFIGURATION 223 - Continued

(b) $M = 0.60$; $\alpha = -10^\circ$ to 10° - Concluded

		C_p for $\beta = -90^\circ$						
		$\beta = -90^\circ$						
		$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -5^\circ$	$\alpha = 0^\circ$	$\alpha = 5^\circ$	$\alpha = 10^\circ$	
None	x/z							
		.426	.396	.407	.409	.399	.377	.288
Upper stage	x/z							
		.448	.208	.219	.215	.205	.189	.121
Transition Flare	x/z							
		.458	.069	.080	.077	.072	.072	.000
Main stage	x/z							
		.471	-1.568	-1.567	-1.543	-1.570	-1.541	-1.576
None	x/z							
		.476	.367	.367	.377	.368	.348	.285
Upper stage	x/z							
		.481	.163	.168	.166	.168	.168	.137
Transition Flare	x/z							
		.501	.060	.052	.056	.068	.114	.064
Main stage	x/z							
		.511	.066	.072	.073	.069	.068	.029
None	x/z							
		.521	.157	.155	.155	.157	.137	.080
Upper stage	x/z							
		.531	.368	.351	.336	.328	.291	.262
Transition Flare	x/z							
		.539	.234	.234	.208	.175	.141	.084
Main stage	x/z							
		.546	.198	.198	.198	.198	.198	.198
None	x/z							
		.552	.037	.026	.010	-.045	-.121	-.092
Transition Flare	x/z							
		.562	-.222	-.238	-.248	-.270	-.299	-.363
Main stage	x/z							
		.568	.798	.809	.790	.763	.800	.864
None	x/z							
		.577	.197	.197	.201	.205	.217	.263
Upper stage	x/z							
		.587	.129	.126	.127	.125	.137	.177
Transition Flare	x/z							
		.597	.089	.083	.081	.085	.097	.143
Main stage	x/z							
		.607	.060	.060	.064	.062	.065	.109
None	x/z							
		.617	.071	.074	.072	.073	.071	.092
Upper stage	x/z							
		.627	.054	.054	.051	.051	.051	.086
Transition Flare	x/z							
		.637	.043	.037	.029	.033	.039	.073
Main stage	x/z							
		.657	.035	.029	.022	.024	.036	.073
None	x/z							
		.677	.028	.022	.017	.020	.031	.084
Upper stage	x/z							
		.697	.020	.014	.012	.016	.026	.055
Transition Flare	x/z							
		.737	.024	.014	.008	.011	.018	.048
Main stage	x/z							
		.777	.020	.010	.006	.009	.015	.040
None	x/z							
		.785	.022	.012	.003	.005	.013	.036
Upper stage	x/z							
		.812	.015	.009	.003	.006	.012	.036
Transition Flare	x/z							
		.837	.021	.013	.008	.010	.013	.037
Main stage	x/z							
		.877	.023	.011	.008	.010	.014	.036
None	x/z							
		.897	.024	.011	.008	.011	.014	.038
Upper stage	x/z							
		.917	.036	.020	.013	.016	.019	.042
Transition Flare	x/z							
		.936	.026	.020	.020	.024	.029	.051
Main stage	x/z							
		.957	.100	.085	.075	.085	.095	.129

(c) $M = 0.86$; $\alpha = -10^\circ$ to 10°

		C_p for $\beta = 0^\circ$						C_p for $\beta = -10^\circ$							
		$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$	$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$
Main stage	x 1	.428	.687	.539	.477	.413	.349	.271	.568	1.098	1.105	1.083	.963	-.933	-1.029
	None	.438	.557	.489	.438	.382	.324	.267	.577	1.098	1.105	1.083	.963	-.933	-1.029
Transition	x 1	.438	.557	.489	.438	.382	.324	.267	.577	1.098	1.105	1.083	.963	-.933	-1.029
	None	.438	.557	.489	.438	.382	.324	.267	.577	1.098	1.105	1.083	.963	-.933	-1.029
Upper stage	x 1	.438	.557	.489	.438	.382	.324	.267	.577	1.098	1.105	1.083	.963	-.933	-1.029
	None	.438	.557	.489	.438	.382	.324	.267	.577	1.098	1.105	1.083	.963	-.933	-1.029
Lower stage	x 1	.438	.557	.489	.438	.382	.324	.267	.577	1.098	1.105	1.083	.963	-.933	-1.029
	None	.438	.557	.489	.438	.382	.324	.267	.577	1.098	1.105	1.083	.963	-.933	-1.029
Main stage	x 1	.428	.687	.539	.477	.413	.349	.271	.568	1.098	1.105	1.083	.963	-.933	-1.029
	None	.438	.557	.489	.438	.382	.324	.267	.577	1.098	1.105	1.083	.963	-.933	-1.029
Transition	x 1	.438	.557	.489	.438	.382	.324	.267	.577	1.098	1.105	1.083	.963	-.933	-1.029
	None	.438	.557	.489	.438	.382	.324	.267	.577	1.098	1.105	1.083	.963	-.933	-1.029
Upper stage	x 1	.438	.557	.489	.438	.382	.324	.267	.577	1.098	1.105	1.083	.963	-.933	-1.029
	None	.438	.557	.489	.438	.382	.324	.267	.577	1.098	1.105	1.083	.963	-.933	-1.029
Lower stage	x 1	.438	.557	.489	.438	.382	.324	.267	.577	1.098	1.105	1.083	.963	-.933	-1.029
	None	.438	.557	.489	.438	.382	.324	.267	.577	1.098	1.105	1.083	.963	-.933	-1.029

M - 283 a - 101 to 105 - Continues

Date	1954					1955				
	2 = 101	3 = 102	4 = 103	5 = 104	6 = 105	7 = 101	8 = 102	9 = 103	10 = 104	11 = 105
Mean	.428	.357	.444	.472	.433	.454	.423	.423	.353	.353
Upper range	.461	.379	.465	.491	.465	.486	.455	.455	.386	.386
Lower range	.415	.335	.423	.453	.401	.440	.411	.411	.320	.320
Time	.546	.285	.285	.285	.285	.285	.285	.285	.285	.285
Terminal	.557	.285	.285	.285	.285	.285	.285	.285	.285	.285
Mean	.428	.357	.444	.472	.433	.454	.423	.423	.353	.353
Upper range	.461	.379	.465	.491	.465	.486	.455	.455	.386	.386
Lower range	.415	.335	.423	.453	.401	.440	.411	.411	.320	.320
Time	.546	.285	.285	.285	.285	.285	.285	.285	.285	.285
Terminal	.557	.285	.285	.285	.285	.285	.285	.285	.285	.285
Mean	.428	.357	.444	.472	.433	.454	.423	.423	.353	.353
Upper range	.461	.379	.465	.491	.465	.486	.455	.455	.386	.386
Lower range	.415	.335	.423	.453	.401	.440	.411	.411	.320	.320
Time	.546	.285	.285	.285	.285	.285	.285	.285	.285	.285
Terminal	.557	.285	.285	.285	.285	.285	.285	.285	.285	.285

... - PRESSURE COEFFICIENTS FOR CONFIGURATION 223 - Continued

(1) $M = 1.06$; $\alpha = -10^\circ$ to 10°

x, z	C_p for $\beta = 0^\circ$						
	$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -5^\circ$	$\alpha = 0^\circ$	$\alpha = 5^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$
Main stage	.424	.413	.689	.609	.544	.490	.410
	.436	.731	.652	.584	.465	.407	.330
	.448	.634	.500	.529	.465	.407	.330
	.451	.606	.500	.442	.384	.329	.255
	.471	.634	.411	.355	.302	.250	.179
	.476	.677	.674	.692	.694	.638	.712
	.481	.656	.614	.656	.611	.645	.625
	.491	.639	.645	.622	.603	.605	.507
	.501	.648	.622	.622	.603	.605	.406
	.511	.648	.622	.622	.603	.605	.293
Upper stage	.521	.351	.293	.079	.108	.202	.181
	.531	.614	.543	.451	.359	.276	.065
	.539	.554	.519	.484	.376	.315	.045
	.546	.673	.613	.534	.413	.374	.104
	.552	.654	.599	.531	.413	.374	.128
	.562	.253	.215	.178	.130	.143	.104
	.568	.661	.601	.531	.413	.374	.104
	.577	.614	.557	.487	.376	.315	.045
	.587	.622	.568	.499	.376	.315	.045
	.597	.622	.568	.499	.376	.315	.045
Transition	.617	.176	.234	.272	.283	.343	.330
	.627	.161	.224	.272	.283	.343	.330
	.637	.152	.183	.204	.221	.261	.239
	.657	.133	.177	.182	.170	.166	.126
	.677	.117	.145	.125	.136	.145	.126
	.697	.096	.122	.104	.111	.099	.081
	.717	.077	.104	.094	.078	.066	.056
	.737	.058	.087	.079	.068	.056	.046
	.757	.039	.068	.068	.056	.046	.036
	.777	.020	.049	.049	.036	.026	.016
Main stage	.438	.686	.628	.560	.498	.434	.382
	.448	.612	.551	.503	.434	.370	.317
	.458	.497	.447	.403	.317	.250	.190
	.471	.709	.759	.781	.759	.680	.604
	.481	.738	.800	.831	.800	.712	.636
	.491	.683	.738	.779	.738	.650	.574
	.501	.612	.672	.731	.672	.584	.508
	.511	.509	.572	.631	.572	.484	.408
	.521	.320	.324	.381	.324	.236	.160
	.531	.588	.528	.433	.382	.287	.190
Transition	.539	.382	.434	.470	.470	.382	.306
	.546	.277	.317	.363	.363	.277	.201
	.552	.370	.350	.331	.322	.237	.161
	.562	.217	.190	.166	.124	.159	.089
	.568	.652	.659	.669	.672	.586	.510
	.577	.490	.537	.571	.525	.437	.361
	.587	.370	.387	.431	.437	.347	.271
	.597	.197	.244	.278	.278	.197	.121
	.607	.216	.250	.281	.275	.197	.121
	.617	.194	.213	.226	.215	.131	.055
Main stage	.627	.188	.198	.186	.171	.094	.018
	.637	.173	.164	.151	.139	.067	.001
	.657	.128	.094	.091	.098	.018	.001
	.677	.076	.068	.068	.070	.001	.001
	.697	.069	.061	.062	.061	.001	.001
	.717	.045	.043	.043	.040	.001	.001
	.737	.025	.022	.024	.022	.001	.001
	.757	.019	.013	.018	.018	.001	.001
	.777	.018	.014	.018	.018	.001	.001
	.797	.018	.014	.018	.018	.001	.001

TABLE 1.- PRESSURE COEFFICIENTS FOR CONFIGURATION 223 - Continued

(3) $M = .60$; $\alpha = -10^\circ$ to 10° - Concluded

x	C_p for $\beta = -3^\circ$							Main range	Transition range	Flat	Transition	Main range						
	$\beta = -3^\circ$																	
	$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$											
.439	.571	.569	.550	.520	.483	.440	.351	.428	.532	.586	.610	.666	.586	.666	.610	.586	.564	.493
.446	.575	.574	.555	.525	.488	.445	.358	.435	.539	.600	.624	.680	.599	.677	.651	.625	.503	.431
.454	.579	.578	.559	.529	.492	.449	.362	.439	.543	.604	.628	.684	.603	.681	.655	.629	.507	.435
.471	.581	.580	.561	.531	.494	.451	.364	.441	.545	.606	.630	.686	.605	.683	.657	.631	.509	.437
.476	.584	.583	.564	.534	.497	.454	.367	.444	.548	.609	.633	.689	.608	.686	.660	.634	.512	.440
.491	.587	.586	.567	.537	.500	.457	.370	.447	.551	.612	.636	.692	.611	.689	.663	.637	.515	.443
.496	.590	.589	.570	.540	.503	.460	.373	.449	.553	.614	.638	.694	.613	.691	.665	.639	.517	.445
.511	.593	.592	.573	.543	.506	.463	.376	.452	.556	.617	.641	.697	.616	.695	.669	.643	.521	.449
.516	.596	.595	.576	.546	.509	.466	.379	.455	.559	.620	.644	.700	.619	.698	.672	.646	.524	.452
.521	.599	.598	.579	.549	.512	.469	.382	.458	.562	.623	.647	.703	.622	.701	.675	.649	.527	.455
.531	.604	.603	.584	.554	.517	.474	.387	.461	.565	.626	.650	.706	.625	.704	.678	.652	.530	.458
.539	.608	.607	.588	.558	.521	.478	.391	.464	.568	.629	.653	.709	.628	.707	.681	.655	.533	.461
.546	.611	.610	.591	.561	.524	.481	.394	.467	.571	.632	.656	.712	.631	.710	.684	.658	.536	.463
.552	.615	.614	.595	.565	.528	.485	.398	.469	.573	.634	.658	.714	.633	.712	.686	.660	.538	.465
.566	.619	.618	.599	.569	.532	.489	.402	.472	.576	.637	.661	.717	.635	.714	.688	.662	.540	.467
.577	.623	.622	.603	.573	.536	.493	.406	.475	.579	.640	.664	.716	.637	.715	.689	.663	.542	.469
.587	.626	.625	.606	.576	.539	.496	.409	.478	.582	.643	.667	.719	.639	.718	.691	.665	.544	.471
.597	.629	.628	.609	.579	.542	.499	.413	.481	.585	.646	.670	.722	.641	.721	.694	.668	.546	.473
.607	.632	.631	.612	.582	.545	.502	.416	.484	.588	.649	.673	.724	.643	.723	.696	.670	.548	.475
.617	.635	.634	.615	.585	.548	.505	.420	.487	.591	.652	.676	.726	.645	.725	.698	.672	.550	.477
.627	.638	.637	.618	.588	.551	.508	.423	.490	.594	.655	.679	.727	.647	.726	.700	.674	.552	.479
.637	.641	.640	.621	.591	.554	.511	.427	.493	.597	.658	.682	.729	.649	.728	.702	.676	.554	.481
.647	.644	.643	.624	.594	.557	.514	.430	.496	.600	.661	.685	.730	.651	.729	.703	.678	.556	.483
.657	.647	.646	.627	.597	.560	.517	.434	.500	.603	.664	.688	.731	.653	.730	.704	.679	.558	.485
.667	.650	.649	.630	.600	.563	.520	.437	.503	.606	.667	.691	.732	.655	.731	.705	.680	.560	.487
.677	.653	.652	.633	.603	.566	.523	.440	.506	.609	.670	.694	.733	.657	.732	.706	.681	.562	.489
.687	.656	.655	.636	.606	.569	.526	.443	.509	.612	.673	.697	.734	.659	.733	.707	.682	.564	.491
.697	.659	.658	.639	.609	.572	.529	.446	.512	.615	.676	.700	.735	.661	.734	.708	.683	.566	.493
.707	.662	.661	.642	.612	.575	.532	.449	.515	.618	.679	.703	.736	.663	.735	.709	.684	.568	.495
.717	.665	.664	.645	.615	.578	.535	.452	.518	.621	.682	.706	.737	.665	.736	.710	.685	.570	.497
.727	.668	.667	.648	.618	.581	.538	.455	.521	.624	.685	.709	.738	.667	.737	.711	.686	.572	.499
.737	.671	.670	.651	.621	.584	.541	.458	.524	.627	.688	.712	.739	.669	.738	.712	.687	.574	.501
.747	.674	.673	.654	.624	.587	.544	.461	.527	.630	.691	.715	.740	.671	.739	.713	.688	.576	.503
.757	.677	.676	.657	.627	.590	.547	.464	.530	.633	.694	.718	.741	.673	.740	.714	.689	.578	.505
.767	.680	.679	.660	.630	.593	.550	.467	.533	.636	.697	.720	.742	.675	.741	.715	.690	.580	.507
.777	.683	.682	.663	.633	.596	.553	.470	.536	.639	.699	.723	.743	.677	.742	.716	.691	.582	.509
.787	.686	.685	.666	.636	.599	.556	.473	.539	.642	.702	.724	.744	.679	.743	.717	.692	.584	.511
.797	.689	.688	.669	.639	.602	.559	.476	.542	.645	.705	.727	.745	.681	.744	.718	.693	.586	.513
.807	.692	.691	.672	.642	.605	.562	.479	.545	.648	.708	.729	.746	.683	.745	.719	.694	.588	.515
.817	.695	.694	.675	.645	.608	.565	.482	.548	.651	.711	.732	.747	.685	.746	.720	.695	.590	.517
.827	.698	.697	.678	.648	.611	.568	.485	.551	.654	.714	.735	.748	.687	.747	.721	.696	.592	.519
.837	.701	.700	.681	.651	.614	.571	.488	.554	.657	.717	.738	.749	.689	.748	.722	.697	.594	.521
.847	.704	.703	.684	.654	.617	.574	.491	.557	.660	.720	.741	.750	.691	.749	.723	.698	.596	.523
.857	.707	.706	.687	.657	.620	.577	.494	.560	.663	.723	.744	.751	.693	.750	.724	.699	.598	.525
.867	.710	.709	.690	.660	.623	.580	.497	.563	.666	.726	.747	.752	.695	.751	.725	.700	.599	.527
.877	.713	.712	.693	.663	.626	.583	.500	.566	.669	.729	.750	.753	.697	.752	.726	.701	.600	.529
.887	.716	.715	.696	.666	.629	.586	.503	.569	.672	.732	.753	.754	.699	.753	.727	.702	.601	.531
.897	.719	.718	.699	.669	.632	.589	.506	.572	.675	.735	.754	.755	.701	.754	.728	.703	.602	.533
.907	.722	.721	.702	.672	.635	.592	.509	.575	.678	.738	.755	.756	.703	.755	.729	.704	.603	.535
.917	.725	.724	.705	.675	.638	.595	.512	.578	.681	.741	.756	.757	.705	.756	.730	.705	.604	.537
.927	.728	.727	.708	.678	.641	.598	.515	.581	.684	.744	.757	.758	.707	.757	.731	.706	.605	.539
.937	.731	.730	.711	.681	.644	.601	.518	.584	.687	.747	.758	.759	.709	.758	.732	.707	.606	.541

TABLE 9.- PRESSURE COEFFICIENTS FOR CONFIGURATION 223 - Concluded

(e) $M = 1.20$; $\alpha = -10^\circ$ to 10° - Concluded

x/l		C_p for $\beta = -50^\circ$						
		α						
		-10°	-6°	-3°	0°	3°	6°	10°
Nose		.438	.643	.614	.560	.543	.448	
		.448	.613	.569	.535	.490	.404	
		.458	.550	.514	.480	.438	.354	
		.471	.419	.390	.360	.428	.452	
		.476	.487	.513	.524	.555	.588	
		.481	.407	.464	.437	.512	.547	
		.491	.282	.342	.366	.393	.425	
		.501	.204	.258	.285	.303	.260	
		.511	.167	.231	.258	.285	.260	
		.521	.137	.160	.203	.059	.085	
Upper stage		.521	.117	.195	.176	.101	.030	
		.531	.355	.304	.255	.196	.131	
		.539	.546	.418	.332	.279	.218	
		.546	.496	.453	.367	.317	.252	
		.552	.415	.426	.381	.330	.234	
		.562	.316	.297	.274	.239	.159	
		.568	.379	.361	.369	.413	.449	
		.577	.319	.305	.332	.372	.420	
		.587	.239	.248	.272	.321	.372	
		.597	.184	.193	.207	.244	.299	
Transition		.607	.155	.161	.169	.179	.244	
		.617	.154	.139	.144	.152	.182	
		.627	.154	.128	.125	.138	.160	
		.637	.132	.117	.117	.125	.138	
		.647	.131	.106	.098	.111	.138	
		.657	.115	.093	.098	.111	.138	
		.667	.063	.044	.049	.076	.113	
		.677	.100	.040	.045	.063	.100	
		.687	.097	.037	.041	.050	.086	
		.697	.097	.032	.032	.052	.064	
Main stage		.707	.053	.031	.032	.052	.064	
		.717	.065	.026	.025	.037	.052	
		.727	.054	.020	.016	.030	.050	
		.737	.056	.015	.016	.033	.050	
		.747	.043	.017	.015	.032	.047	
		.757	.053	.007	.003	.022	.041	
		.767	.062	.009	.001	.016	.031	
		.777	.069	.017	.007	.021	.028	
		.787	.068	.032	.010	.020	.032	
		.797	.059	.047	.053	.066	.089	
None		.426	.607	.655	.667	.669	.633	.572
		.448	.496	.553	.569	.569	.533	.475
		.458	.435	.489	.509	.508	.480	.419
		.471	.416	.461	.439	.461	.411	.339
		.491	.322	.334	.342	.350	.349	.352
		.511	.232	.204	.190	.187	.211	.252
		.531	.272	.295	.304	.304	.277	.231
		.552	.293	.372	.408	.413	.360	.269
		.568	.440	.406	.392	.384	.408	.443
		.587	.320	.281	.259	.242	.291	.334
	.607	.247	.194	.174	.161	.212	.253	
	.627	.230	.142	.117	.114	.136	.234	
	.657	.153	.078	.054	.045	.088	.152	
	.697	.145	.079	.047	.038	.075	.146	
	.717	.115	.063	.036	.033	.065	.124	
	.737	.080	.046	.027	.017	.050	.102	
	.757	.090	.051	.027	.013	.049	.090	
	.777	.079	.030	.012	.010	.041	.090	
	.787	.082	.030	.017	.010	.050	.087	
	.797	.085	.041	.017	.007	.026	.073	

TABLE 1. - PRESSURE COEFFICIENTS FOR CONFIGURATION 323

(a) $M = 0.40$ to 0.95 ; $\alpha = 0^\circ$

		C_p for -				
		$\beta = 0^\circ$				
x/l		$M = 0.40$	$M = 0.70$	$M = 0.85$	$M = 0.90$	$M = 0.95$
		Nose		.443	.553	.577
	.453		.407	.436	.488	.516
Upper stage		.463	.203	.734	.308	.346
		.471	-1.366	-0.661	-0.545	-0.583
Upper stage		.476	-0.625	-0.471	-0.403	-0.409
		.481	-0.536	-0.489	-0.396	-0.477
Upper stage		.491	-0.400	-0.413	-0.389	-0.395
		.501	-0.161	-0.259	-0.353	-0.379
Upper stage		.511	-0.072	-0.088	-0.281	-0.328
		.521	.132	-0.066	-0.177	-0.257
Upper stage		.531	.319	.179	-0.048	-0.153
		.539	-1.334	-0.188	-0.192	-0.112
Transition		.546	.093	.164	.125	.034
		.552	-0.015	.090	.129	.096
Transition		.562	-0.220	-0.138	-0.041	-0.014
		.568	-0.592	-0.705	-0.615	-0.554
Main stage		.577	-0.187	-0.188	-0.163	-0.169
		.587	-0.108	-0.113	-0.098	-0.105
Main stage		.597	-0.074	-0.076	-0.066	-0.072
		.607	-0.063	-0.055	-0.052	-0.055
Main stage		.617	-0.041	-0.044	-0.041	-0.045
		.627	-0.029	-0.034	-0.030	-0.034
Main stage		.637	-0.029	-0.024	-0.023	-0.028
		.657	-0.019	-0.017	-0.015	-0.020
Main stage		.677	-0.014	-0.017	-0.013	-0.018
		.697	-0.007	-0.009	-0.008	-0.015
Main stage		.737	-0.007	-0.008	-0.008	-0.013
		.777	-0.003	-0.002	-0.001	-0.008
Main stage		.785	.001	.006	.004	.005
		.817	.001	.002	.002	.004
Main stage		.857	.001	.001	.002	.008
		.877	.001	.001	.002	.017
Main stage		.897	.002	.004	.004	.017

		C_p for -				
		$\beta = -5^\circ$				
x/l		$M = 0.40$	$M = 0.70$	$M = 0.85$	$M = 0.90$	$M = 0.95$
		Nose		.473	.553	.581
	.282		.360	.410	.498	.542
Upper stage		.091	.207	.238	.308	.390
		-0.965	-0.644	-0.567	-0.474	-0.375
Upper stage		-0.693	-0.499	-0.430	-0.367	-0.282
		-0.412	-0.517	-0.451	-0.371	-0.285
Upper stage		-0.041	-0.421	-0.426	-0.378	-0.289
		.027	-0.193	-0.292	-0.353	-0.404
Upper stage		.072	.008	.113	.288	.343
		.151	.127	.041	-0.199	-0.273
Upper stage		.308	.237	.162	-0.163	-0.183
		-1.907	-0.376	-0.242	-0.091	-0.128
Transition		-1.030	-0.02	-0.01	-0.027	-0.191
		.015	.057	.090	.094	.037
Transition		-0.220	-0.175	-0.138	-0.045	-0.046
		-0.535	-0.595	-0.576	-0.439	-0.468
Main stage		-0.176	-0.184	-0.176	-0.156	-0.163
		-0.108	-0.115	-0.113	-0.102	-0.109
Main stage		-0.063	-0.060	-0.059	-0.048	-0.055
		-0.052	-0.056	-0.055	-0.052	-0.055
Main stage		-0.041	-0.047	-0.042	-0.041	-0.042
		-0.029	-0.038	-0.034	-0.030	-0.036
Main stage		-0.029	-0.028	-0.026	-0.023	-0.026
		-0.019	-0.020	-0.018	-0.018	-0.021
Main stage		-0.007	-0.007	-0.006	-0.008	-0.013
		-0.011	-0.009	-0.009	-0.009	-0.014
Main stage		-0.007	-0.004	-0.005	-0.006	-0.014
		-0.003	-0.002	-0.001	-0.001	-0.009
Main stage		.001	.004	.006	.004	.006
		.001	.003	.003	.002	.004
Main stage		.002	.001	.001	.003	.013
		-0.002	-0.003	-0.002	-0.003	-0.014
Main stage		-0.004	-0.004	-0.004	-0.005	-0.016
		-0.004	-0.005	-0.005	-0.006	-0.016
Main stage		-0.014	-0.016	-0.016	-0.017	-0.029
		-0.066	-0.074	-0.077	-0.081	-0.104

TABLE 11.- PRESSURE COEFFICIENTS FOR CONCENTRATION 50% - Continued

(e) $M = 0.40$ to 0.90 ; $\alpha = 0^\circ$ - Concluded

		C_p for -					
		$\beta = -5^\circ$					
x/t		$M = 0.40$	$M = 0.70$	$M = 0.85$	$M = 0.90$	$M = 0.95$	
		Main stage		.473	.553	.581	.628
	.309		.398	.428	.482	.509	.551
	.463		.212	.242	.308	.346	.390
	.471		.522	.459	.385	.422	.511
	.476		.704	.401	.342	.368	.436
	.481		.423	.413	.349	.368	.442
	.491		.417	.405	.367	.379	.439
	.501		.027	.220	.346	.368	.398
	.511		.072	.138	.285	.328	.337
	.521		.139	.104	.202	.267	.270
Transition flare		.531	.200	.120	.095	.176	.186
		.181	.201	.205	.069	.018	.055
		.546	.138	.155	.073	.036	.040
		.552	.048	.073	.073	.036	.015
		.562	.175	.134	.055	.041	.058
		.568	.595	.576	.396	.379	.417
		.577	.179	.176	.152	.156	.250
		.587	.115	.113	.102	.109	.173
		.597	.074	.071	.070	.075	.116
		.607	.052	.056	.052	.055	.068
Rise		.617	.041	.047	.041	.045	.046
		.627	.029	.038	.034	.038	.036
		.637	.023	.028	.027	.031	.030
		.657	.019	.018	.018	.023	.021
		.677	.013	.013	.013	.019	.017
		.697	.007	.008	.008	.014	.014
		.737	.005	.005	.005	.011	.010
		.777	.003	.003	.000	.007	.010
		.785	.001	.000	.000	.006	.009
		.817	.001	.003	.002	.004	.007
None		.857	.001	.001	.003	.009	.015
		.877	.002	.002	.003	.010	.014
		.897	.002	.004	.004	.011	.015
		.917	.007	.008	.009	.016	.020
		.957	.014	.015	.018	.024	.029
		.997	.068	.075	.081	.092	.104

		C_p for -					
		$\beta = -5^\circ$					
x/t		$M = 0.40$	$M = 0.70$	$M = 0.85$	$M = 0.90$	$M = 0.95$	
		Main stage		.443	.557	.577	.628
	.462		.207	.242	.304	.343	.390
	.471		.531	.447	.417	.432	.562
	.491		.412	.405	.367	.385	.439
	.511		.015	.142	.288	.328	.340
	.531		.214	.133	.095	.183	.186
	.552		.053	.073	.080	.052	.031
	.568		.718	.651	.464	.409	.500
	.587		.115	.113	.102	.109	.196
	.607		.052	.055	.052	.055	.065
Transition flare		.627	.038	.034	.034	.038	.036
		.657	.023	.020	.019	.024	.022
		.697	.011	.011	.010	.017	.017
		.737	.007	.004	.005	.011	.013
		.777	.003	.001	.000	.005	.010
		.785	.003	.001	.000	.007	.010
		.817	.004	.005	.004	.002	.006
		.857	.001	.001	.001	.009	.012
		.897	.004	.003	.004	.005	.016
		.917	.014	.015	.018	.024	.029

TABLE 10.- PRESSURE COEFFICIENTS FOR CONFIGURATION 225 - Continued

(b) $M = 0.60$; $\alpha = -10^\circ$ to 10°

		C_p for $\beta = 0^\circ$						C_p for $\beta = -30^\circ$							
		$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$	$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$
Main stage	$x/1$.737	.655	.601	.527	.456	.385	.292	.699	.638	.584	.527	.467	.396	.292
		.582	.494	.435	.372	.306	.247	.159	.510	.445	.393	.341	.289	.233	.148
		.463	.382	.320	.251	.186	.112	.049	.322	.251	.186	.112	.049	.004	.004
		.471	.390	.328	.266	.204	.142	.080	-1.246	-1.171	-1.099	-1.027	-0.955	-0.883	-0.811
		.476	.395	.333	.271	.209	.147	.085	-1.600	-1.524	-1.448	-1.372	-1.296	-1.220	-1.144
		.481	.400	.338	.276	.214	.152	.090	-2.17	-2.10	-2.02	-1.94	-1.86	-1.78	-1.70
		.491	.410	.348	.286	.224	.162	.100	-0.000	-0.07	-0.14	-0.21	-0.28	-0.35	-0.42
		.501	.420	.358	.296	.234	.172	.110	-0.046	-0.11	-0.18	-0.25	-0.32	-0.39	-0.46
		.511	.430	.368	.306	.244	.182	.120	0.103	0.07	0.04	0.01	-0.02	-0.09	-0.16
		.521	.440	.378	.316	.254	.192	.130	0.200	0.18	0.16	0.14	0.12	0.10	0.08
	.531	.450	.388	.326	.264	.202	.140	0.446	0.407	0.363	0.292	0.202	0.166	0.110	
Transition flange	$x/1$.539	.457	.395	.333	.271	.209	.147	.748	.707	.666	.623	.581	.540	.495
		.546	.464	.402	.340	.278	.216	.154	-0.320	-0.244	-0.191	-0.148	-0.119	-0.094	-0.065
		.552	.470	.408	.346	.284	.222	.160	0.135	0.086	0.053	0.023	-0.010	-0.026	-0.059
		.562	.480	.418	.356	.294	.232	.170	-0.170	-0.170	-0.203	-0.211	-0.216	-0.226	-0.239
		.568	.486	.424	.362	.300	.238	.176	-0.583	-0.633	-0.631	-0.565	-0.490	-0.505	-0.551
		.577	.494	.432	.370	.308	.246	.184	-0.143	-0.170	-0.186	-0.188	-0.187	-0.180	-0.185
		.587	.503	.441	.379	.317	.255	.193	-0.080	-0.101	-0.111	-0.114	-0.124	-0.117	-0.116
		.597	.512	.450	.388	.326	.264	.202	0.040	0.056	0.060	0.057	0.067	0.060	0.059
		.607	.521	.459	.397	.335	.273	.211	0.034	0.050	0.054	0.045	0.050	0.043	0.042
		.617	.530	.468	.406	.344	.282	.220	0.028	0.038	0.043	0.044	0.044	0.037	0.036
Nozzle	$x/1$.627	.545	.483	.421	.359	.297	.235	0.617	0.638	0.637	0.628	0.621	0.626	0.630
		.637	.555	.493	.431	.369	.307	.245	0.637	0.658	0.657	0.648	0.641	0.646	0.650
		.647	.564	.502	.440	.378	.316	.254	0.657	0.678	0.677	0.668	0.661	0.666	0.670
		.657	.574	.512	.450	.388	.326	.264	0.677	0.698	0.697	0.688	0.681	0.686	0.690
		.667	.584	.522	.460	.398	.336	.274	0.697	0.718	0.717	0.708	0.701	0.706	0.710
		.677	.593	.531	.469	.407	.345	.283	0.717	0.738	0.737	0.728	0.721	0.726	0.730
		.687	.600	.538	.476	.414	.352	.290	0.737	0.758	0.757	0.748	0.741	0.746	0.750
		.697	.607	.545	.483	.421	.359	.297	0.757	0.778	0.777	0.768	0.761	0.766	0.770
		.707	.614	.552	.490	.428	.366	.304	0.777	0.798	0.797	0.788	0.781	0.786	0.790
		.717	.621	.559	.497	.435	.373	.311	0.797	0.818	0.817	0.808	0.801	0.806	0.810
	.727	.628	.566	.504	.442	.380	.318	0.817	0.838	0.837	0.828	0.821	0.826	0.830	
	.737	.639	.577	.515	.453	.391	.329	0.837	0.858	0.857	0.848	0.841	0.846	0.850	
	.747	.640	.578	.516	.454	.392	.330	0.857	0.878	0.877	0.868	0.861	0.866	0.870	
	.757	.641	.579	.517	.455	.393	.331	0.877	0.898	0.897	0.888	0.881	0.886	0.890	
	.767	.642	.580	.518	.456	.394	.332	0.897	0.918	0.917	0.908	0.901	0.906	0.910	
	.777	.643	.581	.519	.457	.395	.333	0.917	0.938	0.937	0.928	0.921	0.926	0.930	
	.787	.644	.582	.520	.458	.396	.334	0.937	0.958	0.957	0.948	0.941	0.946	0.950	
	.797	.645	.583	.521	.459	.397	.335	0.957	0.978	0.977	0.968	0.961	0.966	0.970	
	.807	.646	.584	.522	.460	.398	.336	0.977	0.998	0.997	0.988	0.981	0.986	0.990	
	.817	.647	.585	.523	.461	.399	.337	0.997	1.018	1.017	1.008	1.001	1.006	1.010	
	.827	.648	.586	.524	.462	.400	.338	1.017	1.038	1.037	1.028	1.021	1.026	1.030	
	.837	.649	.587	.525	.463	.401	.339	1.037	1.058	1.057	1.048	1.041	1.046	1.050	
	.847	.650	.588	.526	.464	.402	.340	1.057	1.078	1.077	1.068	1.061	1.066	1.070	
	.857	.651	.589	.527	.465	.403	.341	1.077	1.098	1.097	1.088	1.081	1.086	1.090	
	.867	.652	.590	.528	.466	.404	.342	1.097	1.118	1.117	1.108	1.101	1.106	1.110	
	.877	.653	.591	.529	.467	.405	.343	1.117	1.138	1.137	1.128	1.121	1.126	1.130	
	.887	.654	.592	.530	.468	.406	.344	1.137	1.158	1.157	1.148	1.141	1.146	1.150	
	.897	.655	.593	.531	.469	.407	.345	1.157	1.178	1.177	1.168	1.161	1.166	1.170	
	.907	.656	.594	.532	.470	.408	.346	1.177	1.198	1.197	1.188	1.181	1.186	1.190	
	.917	.657	.595	.533	.471	.409	.347	1.197	1.218	1.217	1.208	1.201	1.206	1.210	
	.927	.658	.596	.534	.472	.410	.348	1.217	1.238	1.237	1.228	1.221	1.226	1.230	
	.937	.659	.597	.535	.473	.411	.349	1.237	1.258	1.257	1.248	1.241	1.246	1.250	
	.947	.660	.598	.536	.474	.412	.350	1.257	1.278	1.277	1.268	1.261	1.266	1.270	
	.957	.661	.599	.537	.475	.413	.351	1.277	1.298	1.297	1.288	1.281	1.286	1.290	
	.967	.662	.600	.538	.476	.414	.352	1.297	1.318	1.317	1.308	1.301	1.306	1.310	
	.977	.663	.601	.539	.477	.415	.353	1.317	1.338	1.337	1.328	1.321	1.326	1.330	
	.987	.664	.602	.540	.478	.416	.354	1.337	1.358	1.357	1.348	1.341	1.346	1.350	
	.997	.665	.603	.541	.479	.417	.355	1.357	1.378	1.377	1.368	1.361	1.366	1.370	

TABLE 1.1.1 - PRESSURE COEFFICIENTS FOR CONFIGURATION 303 - Continued

(b) $M = 0.60$; $\alpha = -10^\circ$ to 10° - Concluded

		C_p for $\beta = -60^\circ$						C_p for $\beta = -30^\circ$							
		$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$	$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$
Main stage	x/l	.582	.583	.562	.527	.478	.424	.326	.443	.506	.518	.521	.506	.490	.420
	Moore	.432	.422	.402	.366	.323	.285	.198	.463	.506	.518	.521	.506	.490	.420
Transition	x/l	.222	.206	.185	.161	.123	.092	.021	.463	.463	.471	.471	.463	.455	.376
	Moore	.008	.008	.007	.007	.007	.007	.007	.471	.471	.471	.471	.471	.471	.471
Upper stage	x/l	.703	.701	.694	.688	.659	.626	.585	.471	.471	.471	.471	.471	.471	.471
	Moore	.008	.008	.007	.007	.007	.007	.007	.471	.471	.471	.471	.471	.471	.471
Transition	x/l	.023	.025	.037	.012	.067	.071	.127	.511	.511	.511	.511	.511	.511	.511
	Moore	.023	.025	.037	.012	.067	.071	.127	.511	.511	.511	.511	.511	.511	.511
Main stage	x/l	.126	.150	.157	.155	.127	.089	.030	.531	.531	.531	.531	.531	.531	.531
	Moore	.338	.336	.323	.263	.247	.249	.210	.531	.531	.531	.531	.531	.531	.531
Transition	x/l	.276	.255	.228	.192	.142	.110	.077	.552	.552	.552	.552	.552	.552	.552
	Moore	.034	.035	.037	.017	.001	.026	.093	.552	.552	.552	.552	.552	.552	.552
Main stage	x/l	.737	.741	.694	.588	.439	.311	.178	.568	.568	.568	.568	.568	.568	.568
	Moore	.211	.193	.186	.182	.193	.203	.236	.568	.568	.568	.568	.568	.568	.568
Transition	x/l	.148	.130	.117	.114	.124	.128	.162	.587	.587	.587	.587	.587	.587	.587
	Moore	.008	.008	.007	.007	.007	.007	.007	.587	.587	.587	.587	.587	.587	.587
Main stage	x/l	.091	.067	.060	.057	.061	.066	.099	.607	.607	.607	.607	.607	.607	.607
	Moore	.085	.061	.049	.045	.050	.060	.087	.607	.607	.607	.607	.607	.607	.607
Transition	x/l	.085	.068	.043	.034	.044	.048	.076	.627	.627	.627	.627	.627	.627	.627
	Moore	.068	.056	.043	.034	.044	.048	.076	.627	.627	.627	.627	.627	.627	.627
Main stage	x/l	.071	.047	.025	.018	.022	.039	.067	.657	.657	.657	.657	.657	.657	.657
	Moore	.046	.034	.019	.011	.022	.032	.060	.657	.657	.657	.657	.657	.657	.657
Transition	x/l	.054	.026	.013	.005	.018	.025	.053	.697	.697	.697	.697	.697	.697	.697
	Moore	.054	.026	.013	.005	.018	.025	.053	.697	.697	.697	.697	.697	.697	.697
Main stage	x/l	.052	.020	.007	.001	.010	.013	.043	.777	.777	.777	.777	.777	.777	.777
	Moore	.052	.020	.007	.001	.010	.013	.043	.777	.777	.777	.777	.777	.777	.777
Transition	x/l	.043	.017	.003	.004	.004	.010	.030	.817	.817	.817	.817	.817	.817	.817
	Moore	.043	.017	.003	.004	.004	.010	.030	.817	.817	.817	.817	.817	.817	.817
Main stage	x/l	.047	.021	.007	.000	.008	.012	.026	.857	.857	.857	.857	.857	.857	.857
	Moore	.047	.021	.007	.000	.008	.012	.026	.857	.857	.857	.857	.857	.857	.857
Transition	x/l	.048	.023	.009	.002	.010	.013	.027	.897	.897	.897	.897	.897	.897	.897
	Moore	.048	.023	.009	.002	.010	.013	.027	.897	.897	.897	.897	.897	.897	.897
Main stage	x/l	.054	.030	.015	.007	.014	.019	.031	.917	.917	.917	.917	.917	.917	.917
	Moore	.054	.030	.015	.007	.014	.019	.031	.917	.917	.917	.917	.917	.917	.917
Transition	x/l	.063	.036	.021	.014	.024	.027	.040	.957	.957	.957	.957	.957	.957	.957
	Moore	.063	.036	.021	.014	.024	.027	.040	.957	.957	.957	.957	.957	.957	.957
Main stage	x/l	.130	.100	.081	.070	.084	.094	.120	.997	.997	.997	.997	.997	.997	.997
	Moore	.130	.100	.081	.070	.084	.094	.120	.997	.997	.997	.997	.997	.997	.997

TABLE 10.- PRESSURE COEFFICIENTS FOR CONFIGURATION 323 - Continued

(c) $M = 0.80$; $\alpha = -10^\circ$ to 10°

		C_p for - $\beta = 0^\circ$						C_p for - $\beta = -30^\circ$								
		$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$	$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$	
Main stage	$x/2$.814	.732	.673	.604	.539	.465	.366	.443	.773	.713	.666	.600	.539	.473	.373
		.661	.579	.524	.462	.393	.324	.235	.453	.599	.536	.492	.438	.384	.320	.231
		.552	.374	.330	.276	.222	.163	.082	.463	.426	.359	.319	.276	.229	.167	.090
		-1.180	-0.979	-0.733	-0.575	-0.490	-0.421	-0.396	.471	-1.043	-0.862	-0.808	-0.791	-0.799	-0.771	-0.733
		.779	.707	.559	.423	.344	.328	.315	.476	.772	.692	.653	.638	.625	.622	.593
		.514	.611	.544	.427	.364	.358	.350	.481	.568	.548	.544	.548	.548	.548	.548
		.037	.311	.440	.411	.390	.397	.400	.491	.114	.338	.444	.396	.375	.393	.423
		.067	.026	.240	.334	.348	.355	.369	.501	.047	.049	.232	.330	.337	.355	.388
		.132	.120	.029	.211	.244	.239	.269	.511	.105	.093	.236	.244	.244	.251	.296
		.243	.228	.148	.077	.121	.109	.138	.521	.220	.212	.117	.107	.125	.128	.181
	.509	.431	.306	.062	.010	.001	.007	.531	.478	.412	.267	.039	.014	.016	.023	
Transition flare	$x/2$.199	.172	.148	.134	.114	.097	.088	.539	.149	.144	.146	.137	.132	.127	
		.308	.262	.248	.163	.051	.037	.042	.546	.058	.084	.110	.100	.094	.084	
		.221	.175	.161	.118	.017	.003	.004	.552	.190	.161	.106	.017	.001	.034	
		.001	-0.049	-0.083	-0.092	-0.121	-0.139	-0.146	.562	-0.037	-0.076	-0.102	-0.092	-0.121	-0.211	
Main stage	$x/2$	-1.214	-1.218	-1.171	-0.669	-0.417	-0.355	-0.353	.568	-1.064	-1.084	-1.017	-0.864	-0.364	-0.489	
		.145	.169	.182	.177	.167	.155	.154	.577	.183	.184	.182	.169	.164	.170	
		.076	.092	.102	.107	.114	.105	.096	.587	.087	.092	.106	.111	.114	.116	
		.041	.061	.067	.073	.083	.074	.065	.597	.045	.045	.048	.057	.064	.059	
		.026	.042	.048	.054	.064	.055	.046	.607	.045	.045	.048	.054	.064	.062	
		.014	.030	.036	.046	.048	.039	.034	.617	.033	.034	.036	.046	.048	.047	
		.003	.019	.029	.034	.041	.032	.027	.627	.030	.030	.029	.034	.041	.039	
		.008	.011	.017	.027	.033	.024	.019	.637	.018	.022	.021	.027	.033	.028	
		.020	.002	.009	.016	.021	.015	.009	.657	.011	.014	.016	.021	.024	.024	
		.027	.007	.000	.018	.028	.020	.008	.677	.003	.000	.000	.010	.013	.012	
	.028	.007	.000	.012	.013	.006	.006	.697	.002	.005	.005	.012	.014	.013		
	.035	.015	.004	.003	.010	.005	.009	.737	.002	.002	.002	.002	.009	.009		
	.028	.015	.004	.003	.010	.005	.008	.777	.014	.008	.005	.004	.005	.004		
	.042	.020	.012	.002	.001	.001	.001	.785	.010	.008	.008	.001	.000	.001		
	.039	.019	.010	.000	.002	.002	.007	.817	.011	.008	.007	.000	.002	.003		
	.030	.014	.006	.003	.005	.003	.015	.857	.006	.002	.002	.004	.007	.006		
	.033	.015	.007	.003	.004	.003	.015	.877	.003	.001	.001	.000	.000	.000		
	.029	.016	.003	.006	.008	.006	.020	.897	.001	.000	.000	.000	.000	.000		
								.917	.003	.001	.001	.000	.001	.001		
								.957	.013	.012	.011	.010	.011	.011		
								.997	.094	.078	.069	.081	.088	.095		

TABLE 1.- PRESSURE COEFFICIENTS FOR CONFIGURATION 323 - Continued

(c) $M = 0.86$; $\alpha = -10^\circ$ to 10° - Concluded

		C_p for $\beta = -50^\circ$							
		$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$	
Nozzle	x/l	.443	.516	.579	.602	.600	.587	.562	.493
		.453	.210	.254	.270	.276	.259	.234	.187
Upper stage	x/l	.471	-.654	-.625	-.554	-.460	-.524	-.618	-.655
		.476	-.599	-.502	-.377	-.439	-.429	-.470	-.488
Upper stage	x/l	.481	-.614	-.504	-.387	-.443	-.429	-.470	-.488
		.491	-.345	-.448	-.380	-.443	-.429	-.470	-.488
Upper stage	x/l	.501	-.049	-.176	-.286	-.370	-.202	-.116	-.130
		.511	.032	-.094	-.234	-.400	-.238	-.116	-.130
Upper stage	x/l	.521	.132	.170	.071	-.119	-.087	-.163	-.130
		.531	.347	.210	.004	-.082	.141	-.222	.216
Transition flange	x/l	.539	.319	.297	.148	.023	.060	.060	.030
		.544	.280	.263	.171	.093	.062	.060	.030
Transition flange	x/l	.552	.084	.114	.084	.037	.076	.104	.060
		.562	-.111	-.113	-.092	-.182	.112	.060	.030
Main stage	x/l	.568	-1.252	-1.094	-.473	-1.095	-1.249	-1.247	-1.315
		.577	-.222	-.184	-.165	-.189	-.130	-.963	-.546
Main stage	x/l	.587	-.156	-.122	-.111	-.124	-.117	-.121	-.196
		.597	-.126	-.084	-.075	-.079	-.085	-.064	-.142
Main stage	x/l	.607	-.107	-.056	-.054	-.064	-.056	-.056	-.078
		.617	-.099	-.044	-.046	-.048	-.059	-.041	-.123
Main stage	x/l	.627	-.091	-.036	-.038	-.041	-.057	-.036	-.059
		.637	-.080	-.029	-.031	-.033	-.043	-.024	-.050
Main stage	x/l	.657	-.074	-.020	-.023	-.024	-.049	-.024	-.028
		.677	-.061	-.013	-.016	-.020	-.030	-.014	-.039
Main stage	x/l	.697	-.048	-.006	-.010	-.016	-.024	-.007	-.031
		.737	-.060	-.006	-.007	-.010	-.019	-.007	-.027
Main stage	x/l	.777	-.052	-.002	-.003	-.006	-.013	-.003	-.026
		.785	-.059	-.002	-.003	-.005	-.010	-.002	-.026
Main stage	x/l	.817	-.045	-.003	-.004	-.003	-.009	-.001	-.019
		.857	-.050	-.001	-.004	-.007	-.011	-.003	-.008
Main stage	x/l	.877	-.050	-.002	-.005	-.008	-.012	-.006	-.024
		.897	-.054	-.003	-.006	-.009	-.014	-.008	-.027
Main stage	x/l	.917	-.059	-.010	-.011	-.014	-.018	-.014	-.027
		.957	-.064	-.016	-.020	-.023	-.028	-.024	-.027
Main stage	x/l	.997	-.136	-.080	-.081	-.088	-.100	-.076	-.076

TABLE 10.- PRESSURE COEFFICIENTS FOR CONFIGURATION 323 - Continued

(d) $M = 1.00$; $\alpha = -10^\circ$ to 10°

x/l	C_p for $\beta = 0^\circ$						x/l	C_p for $\beta = -30^\circ$							
	$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$		$\alpha = 10^\circ$	$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$
	Main stage	.941	.865	.813	.743	.676		.608	.517	.643	.904	.844	.795	.737	.679
Transition	.811	.732	.671	.612	.546	.483	.399	.653	.784	.696	.647	.595	.541	.485	.400
	.636	.563	.508	.455	.400	.350	.271	.463	.603	.548	.499	.452	.403	.350	.277
Upper stage	.833	.852	.866	.868	.845	.822	.893	.471	.932	.893	.863	.831	.806	.776	.693
	.604	.731	.804	.848	.875	.893	.933	.476	.855	.821	.796	.766	.737	.707	.630
Main stage	.326	.487	.584	.694	.771	.834	.839	.481	.677	.641	.616	.591	.566	.541	.464
	.136	.270	.388	.491	.594	.676	.739	.501	.693	.657	.632	.607	.582	.557	.480
Transition	.044	.099	.144	.191	.239	.289	.349	.511	.688	.652	.627	.602	.577	.552	.475
	.295	.259	.236	.204	.189	.164	.157	.521	.698	.662	.637	.612	.587	.562	.485
Main stage	.582	.476	.392	.336	.281	.234	.197	.531	.646	.562	.517	.472	.427	.382	.305
	.040	.045	.052	.056	.072	.084	.092	.539	.646	.562	.517	.472	.427	.382	.305
Transition	.456	.415	.379	.300	.215	.158	.111	.546	.653	.569	.524	.479	.434	.389	.312
	.393	.346	.329	.261	.181	.119	.063	.552	.659	.575	.530	.485	.440	.395	.318
Main stage	.245	.204	.172	.086	.104	.119	.063	.562	.669	.585	.540	.495	.450	.405	.328
	.662	.682	.700	.695	.625	.529	.307	.568	.675	.591	.546	.501	.456	.411	.334
Transition	.424	.499	.538	.500	.460	.426	.228	.577	.684	.600	.555	.510	.465	.420	.343
	.320	.413	.458	.399	.248	.242	.240	.587	.694	.610	.565	.520	.475	.430	.353
Main stage	.234	.316	.357	.283	.229	.213	.213	.597	.704	.620	.575	.530	.485	.440	.363
	.188	.254	.278	.243	.211	.199	.170	.607	.714	.630	.585	.540	.495	.450	.373
Transition	.170	.221	.226	.194	.186	.171	.139	.617	.724	.640	.595	.550	.505	.460	.383
	.161	.199	.162	.154	.162	.147	.112	.627	.734	.650	.605	.560	.515	.470	.393
Main stage	.142	.144	.107	.124	.137	.122	.093	.637	.744	.660	.615	.570	.525	.480	.403
	.131	.086	.085	.099	.111	.097	.064	.647	.754	.670	.625	.580	.535	.490	.413
Transition	.057	.075	.077	.085	.090	.080	.064	.657	.764	.680	.635	.590	.545	.500	.423
	.045	.064	.063	.070	.074	.065	.047	.667	.774	.690	.645	.600	.555	.510	.433
Main stage	.030	.058	.046	.062	.052	.046	.025	.677	.784	.700	.655	.610	.565	.520	.443
	.014	.022	.018	.042	.031	.024	.005	.687	.794	.710	.665	.620	.575	.530	.453
Transition	.031	.009	.026	.027	.013	.004	.005	.697	.804	.720	.675	.630	.585	.540	.463
	.027	.009	.035	.026	.024	.019	.015	.707	.814	.730	.685	.640	.595	.550	.473
Main stage	.055	.027	.035	.026	.024	.020	.015	.717	.824	.740	.695	.650	.605	.560	.483
	.061	.039	.032	.028	.023	.021	.014	.727	.834	.750	.705	.660	.615	.570	.493
Transition	.055	.025	.025	.025	.018	.017	.007	.737	.844	.760	.715	.670	.625	.580	.503
	.061	.035	.032	.028	.023	.021	.014	.747	.854	.770	.725	.680	.635	.590	.513
Main stage	.055	.025	.025	.025	.018	.017	.007	.757	.864	.780	.735	.690	.645	.600	.523
	.061	.035	.032	.028	.023	.021	.014	.767	.874	.790	.745	.700	.655	.610	.533
Transition	.055	.025	.025	.025	.018	.017	.007	.777	.884	.800	.755	.710	.665	.620	.543
	.061	.035	.032	.028	.023	.021	.014	.787	.894	.810	.765	.720	.675	.630	.553
Main stage	.055	.025	.025	.025	.018	.017	.007	.797	.904	.820	.775	.730	.685	.640	.563
	.061	.035	.032	.028	.023	.021	.014	.807	.914	.830	.785	.740	.695	.650	.573

TABLE 10. -- PRESSURE COEFFICIENTS FOR CONFIGURATION 323 - Continued

(d) $M = 1.0$, $\alpha = -1.0^\circ$ to 10° - (continued)

x/l	C_p for $\beta = -60^\circ$						C_p for $\beta = -90^\circ$									
	$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -5^\circ$	$\alpha = 0^\circ$	$\alpha = 5^\circ$	$\alpha = 10^\circ$	$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -5^\circ$	$\alpha = 0^\circ$	$\alpha = 5^\circ$	$\alpha = 10^\circ$				
	Rose	.453	.793	.791	.768	.737	.697	.643	.553	.443	.660	.717	.736	.737	.729	.706
Melt stage	.455	.658	.658	.638	.607	.563	.516	.437	.463	.399	.441	.451	.452	.442	.424	.375
	.463	.511	.497	.481	.455	.418	.374	.307	.471	.847	.867	.866	.862	.715	.728	.759
Transition flange	.471	.783	.783	.782	.789	.789	.789	.789	.471	.471	.471	.471	.471	.471	.471	.471
	.476	.964	.964	.964	.964	.964	.964	.964	.471	.471	.471	.471	.471	.471	.471	.471
Upper stage	.481	.856	.856	.856	.856	.856	.856	.856	.491	.497	.478	.464	.484	.483	.499	.506
	.491	.438	.438	.438	.438	.438	.438	.438	.511	.265	.212	.113	.059	.318	.343	.310
Melt stage	.501	.271	.291	.263	.179	.400	.440	.472	.531	.173	.140	.163	.135	.027	.003	.106
	.511	.106	.042	.038	.315	.370	.370	.399	.552	.122	.225	.268	.258	.193	.208	.080
Transition flange	.521	.136	.128	.129	.054	.226	.272	.271	.568	.775	.744	.727	.711	.760	.743	.784
	.531	.384	.336	.279	.143	.119	.159	.161	.587	.546	.514	.461	.396	.364	.514	.567
Melt stage	.539	.471	.466	.467	.188	.015	.101	.157	.607	.424	.267	.229	.243	.220	.254	.430
	.546	.422	.417	.426	.164	.014	.055	.104	.627	.237	.172	.156	.157	.156	.162	.228
Transition flange	.552	.236	.276	.302	.164	.057	.081	.026	.657	.208	.138	.104	.101	.110	.138	.206
	.562	.107	.132	.133	.092	.046	.003	.063	.697	.167	.109	.074	.072	.080	.108	.166
Melt stage	.568	.720	.713	.706	.671	.630	.734	.787	.657	.775	.744	.727	.711	.760	.743	.784
	.577	.586	.591	.590	.530	.318	.581	.720	.657	.775	.744	.727	.711	.760	.743	.784
Transition flange	.587	.448	.465	.474	.405	.284	.379	.462	.587	.546	.514	.461	.396	.364	.514	.567
	.597	.359	.364	.360	.304	.248	.275	.372	.607	.424	.267	.229	.243	.220	.254	.430
Melt stage	.607	.326	.316	.289	.231	.211	.211	.231	.627	.424	.267	.229	.243	.220	.254	.430
	.617	.307	.187	.192	.188	.186	.177	.191	.657	.237	.172	.156	.157	.156	.162	.228
Transition flange	.627	.301	.245	.192	.157	.162	.159	.176	.657	.208	.138	.104	.101	.110	.138	.206
	.637	.243	.150	.125	.133	.141	.147	.167	.697	.167	.109	.074	.072	.080	.108	.166
Melt stage	.657	.180	.123	.098	.101	.110	.126	.156	.717	.129	.091	.049	.058	.061	.089	.128
	.677	.150	.105	.082	.086	.070	.092	.133	.777	.097	.033	.004	.042	.013	.047	.100
Transition flange	.697	.120	.087	.067	.070	.076	.071	.109	.817	.097	.033	.004	.042	.013	.047	.100
	.737	.109	.083	.049	.059	.055	.071	.068	.857	.059	.029	.009	.031	.010	.024	.084
Melt stage	.777	.069	.034	.007	.040	.005	.021	.045	.877	.059	.029	.009	.031	.010	.024	.084
	.785	.072	.021	.014	.030	.014	.011	.036	.897	.046	.004	.022	.027	.021	.002	.044
Transition flange	.817	.049	.002	.028	.026	.022	.010	.008	.917	.046	.004	.022	.027	.021	.002	.044
	.857	.024	.004	.023	.026	.022	.010	.003	.957	.036	.007	.008	.012	.009	.020	.153
Melt stage	.877	.021	.004	.022	.027	.020	.010	.004	.997	.036	.007	.008	.012	.009	.020	.153
	.897	.024	.004	.019	.027	.016	.009	.005	.997	.036	.007	.008	.012	.009	.020	.153
Transition flange	.917	.033	.002	.014	.021	.011	.004	.009	.997	.036	.007	.008	.012	.009	.020	.153
	.957	.036	.007	.008	.012	.002	.009	.020	.997	.036	.007	.008	.012	.009	.020	.153
Melt stage	.997	.107	.089	.085	.100	.118	.132	.153	.997	.036	.007	.008	.012	.009	.020	.153

TABLE 10.- PRESSURE COEFFICIENTS FOR CONFIGURATION 203 - Continued

(e) $M = 1.20; \alpha = -10^\circ$ to 10°

x/l		C_p for $\beta = 0^\circ$							C_p for $\beta = -30^\circ$						
		$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -5^\circ$	$\alpha = 0^\circ$	$\alpha = 5^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$	$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -5^\circ$	$\alpha = 0^\circ$	$\alpha = 5^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$
		Nose		1.070	.589	.927	.869	.808	.739	.647	1.030	.973	.921	.866	.811
Upper stage		.948	.870	.813	.758	.698	.634	.547	.900	.842	.796	.746	.695	.639	.552
		.803	.727	.679	.626	.579	.528	.452	.769	.712	.671	.626	.579	.528	.452
Transition		.473	.457	.503	.517	.527	.536	.544	.589	.618	.625	.630	.635	.644	.652
		.502	.567	.600	.631	.654	.672	.644	.476	.575	.606	.628	.630	.644	.652
Main stage		.333	.436	.497	.549	.592	.628	.632	.393	.485	.535	.576	.611	.636	.693
		.070	.169	.231	.293	.350	.410	.467	.491	.539	.576	.611	.636	.649	.695
Nose		.070	.115	.145	.165	.178	.188	.195	.075	.130	.176	.221	.263	.306	.345
		.031	.050	.074	.092	.115	.138	.155	.162	.270	.339	.399	.450	.495	.545
Upper stage		.031	.050	.074	.092	.115	.138	.155	.048	.099	.147	.191	.233	.273	.316
		.505	.410	.349	.275	.178	.101	.044	.475	.399	.344	.275	.170	.077	.014
Transition		.826	.720	.630	.555	.481	.418	.368	1.140	1.079	1.021	.962	.890	.826	.767
		.561	.519	.491	.424	.266	.191	.178	.992	.921	.860	.801	.722	.641	.582
Main stage		.419	.369	.341	.301	.194	.134	.140	.562	.455	.437	.402	.306	.260	.194
		.342	.354	.367	.383	.393	.234	.296	.344	.352	.353	.364	.374	.402	.446
Nose		.192	.243	.269	.285	.219	.168	.168	.252	.266	.296	.296	.244	.342	.446
		.140	.205	.236	.253	.222	.204	.195	.151	.202	.225	.233	.217	.223	.288
Upper stage		.091	.148	.182	.204	.206	.201	.198	.078	.112	.130	.141	.140	.138	.146
		.061	.115	.143	.163	.178	.176	.171	.091	.131	.152	.165	.176	.171	.171
Main stage		.050	.099	.119	.136	.149	.144	.133	.080	.110	.122	.136	.146	.144	.135
		.037	.085	.100	.111	.119	.111	.095	.072	.099	.105	.114	.121	.117	.108
Transition		.023	.066	.078	.081	.086	.084	.062	.061	.085	.086	.087	.089	.089	.081
		.030	.064	.071	.063	.054	.046	.033	.056	.062	.064	.054	.048	.051	.051
Main stage		.031	.038	.044	.041	.040	.025	.022	.037	.048	.039	.034	.035	.032	.058
		.023	.037	.038	.031	.019	.014	.020	.044	.037	.029	.032	.027	.027	.058
Nose		.016	.026	.025	.034	.029	.027	.010	.044	.044	.029	.032	.027	.035	.059
		.019	.014	.028	.021	.028	.028	.017	.005	.020	.024	.015	.024	.030	.071
Upper stage		.029	.005	.017	.013	.018	.011	.005	.001	.015	.015	.008	.012	.020	.063
		.023	.002	.002	.021	.018	.008	.007	.002	.014	.014	.019	.017	.023	.072
Main stage		.032	.004	.008	.003	.000	.008	.017	.008	.000	.007	.011	.008	.022	.069
		.013	.003	.000	.000	.004	.007	.015	.003	.011	.004	.002	.005	.019	.063
Nose		.897	.803	.000	.005	.009	.017	.023	.897	.805	.004	.002	.005	.021	.056
		.817	.023	.002	.021	.018	.008	.017	.817	.015	.005	.006	.007	.019	.045
Upper stage		.877	.007	.008	.003	.000	.008	.017	.877	.008	.004	.002	.005	.019	.045
		.032	.004	.003	.000	.004	.007	.015	.032	.011	.004	.002	.005	.019	.045
Main stage		.013	.003	.000	.000	.009	.017	.023	.013	.011	.004	.002	.005	.019	.045
		.013	.003	.000	.000	.009	.017	.023	.013	.011	.004	.002	.005	.019	.045

TABLE 10.- PRESSURE COEFFICIENTS FOR CONFIGURATION 323 - Concluded.

(e) $M = 1.20$; $\alpha = -10^\circ$ to 10° - Concluded

		C_p for -						
		$\beta = -60^\circ$						
		$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$
Rose	x/t	.443	.443	.443	.443	.443	.443	.443
		.919	.801	.779	.750	.719	.671	.684
Upper stage		.809	.669	.655	.626	.595	.555	.581
	x/t	.471	.476	.482	.493	.500	.512	.533
Upper stage		.578	.607	.625	.642	.662	.682	.682
		.481	.504	.535	.568	.595	.614	.636
Upper stage		.491	.433	.405	.434	.462	.451	.451
	x/t	.501	.232	.266	.299	.328	.326	.228
Transition		.511	.175	.192	.206	.207	.152	.152
		.521	.118	.110	.177	.126	.041	.029
Transition		.531	.348	.319	.259	.202	.156	.110
	x/t	.539	.572	.486	.392	.288	.193	.132
Transition		.546	.535	.491	.434	.331	.242	.170
		.552	.404	.419	.397	.365	.319	.210
Transition		.562	.293	.309	.287	.266	.226	.137
	x/t	.568	.393	.372	.372	.385	.413	.459
Main stage		.577	.325	.312	.293	.336	.375	.446
		.587	.241	.247	.236	.274	.326	.389
Main stage		.597	.192	.192	.190	.195	.266	.345
		.607	.173	.164	.160	.159	.176	.288
Main stage		.617	.165	.135	.136	.135	.144	.190
		.627	.165	.116	.114	.119	.125	.154
Main stage		.637	.143	.112	.089	.089	.100	.133
	x/t	.657	.155	.067	.042	.050	.076	.116
Main stage		.677	.130	.049	.042	.048	.065	.106
		.697	.105	.067	.038	.045	.054	.096
Main stage		.737	.106	.033	.032	.034	.042	.075
		.777	.073	.029	.016	.028	.042	.065
Main stage		.785	.060	.043	.008	.020	.033	.060
		.817	.057	.024	.017	.018	.034	.054
Main stage		.857	.065	.019	.014	.022	.033	.053
		.877	.054	.007	.004	.007	.023	.048
Main stage		.897	.065	.029	.001	.003	.019	.038
		.917	.070	.033	.017	.010	.022	.035
Main stage		.957	.069	.038	.015	.019	.022	.038
		.997	.061	.042	.053	.065	.090	.109

		C_p for -						
		$\beta = -90^\circ$						
		$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$
Rose	x/t	.443	.443	.443	.443	.443	.443	.443
		.785	.844	.866	.866	.858	.837	.771
Upper stage		.566	.609	.623	.623	.618	.597	.544
	x/t	.471	.533	.525	.525	.530	.525	.533
Upper stage		.682	.662	.642	.636	.636	.636	.636
		.481	.504	.535	.568	.595	.614	.636
Upper stage		.491	.433	.405	.434	.462	.451	.451
	x/t	.501	.232	.266	.299	.328	.326	.228
Transition		.511	.175	.192	.206	.207	.152	.152
		.521	.118	.110	.177	.126	.041	.029
Transition		.531	.348	.319	.259	.202	.156	.110
	x/t	.539	.572	.486	.392	.288	.193	.132
Transition		.546	.535	.491	.434	.331	.242	.170
		.552	.404	.419	.397	.365	.319	.210
Transition		.562	.293	.309	.287	.266	.226	.137
	x/t	.568	.393	.372	.372	.385	.413	.459
Main stage		.577	.325	.312	.293	.336	.375	.446
		.587	.241	.247	.236	.274	.326	.389
Main stage		.597	.192	.192	.190	.195	.266	.345
		.607	.173	.164	.160	.159	.176	.288
Main stage		.617	.165	.135	.136	.135	.144	.190
		.627	.165	.116	.114	.119	.125	.154
Main stage		.637	.143	.112	.089	.089	.100	.133
	x/t	.657	.155	.067	.042	.050	.076	.116
Main stage		.677	.130	.049	.042	.048	.065	.106
		.697	.105	.067	.038	.045	.054	.096
Main stage		.737	.106	.033	.032	.034	.042	.075
		.777	.073	.029	.016	.028	.042	.065
Main stage		.785	.060	.043	.008	.020	.033	.060
		.817	.057	.024	.017	.018	.034	.054
Main stage		.857	.065	.019	.014	.022	.033	.053
		.877	.054	.007	.004	.007	.023	.048
Main stage		.897	.065	.029	.001	.003	.019	.038
		.917	.070	.033	.017	.010	.022	.035
Main stage		.957	.069	.038	.015	.019	.022	.038
		.997	.061	.042	.053	.065	.090	.109

TABLE 11.- PRESSURE COEFFICIENTS FOR CONFIGURATION 124

(a) $M = 0.40$ to 0.95 ; $\alpha = 0^\circ$

x/l	C_p for -					x/l	C_p for -						
	$\beta = 0^\circ$						$\beta = -50^\circ$						
	$M = 0.40$	$M = 0.70$	$M = 0.75$	$M = 0.85$	$M = 0.90$		$M = 0.95$	$M = 0.40$	$M = 0.70$	$M = 0.75$	$M = 0.85$	$M = 0.90$	$M = 0.95$
Nose	.428	.223	.256	.263	.274	.301	.329	.223	.251	.255	.275	.301	.329
	.438	.190	.220	.230	.247	.271	.301	.190	.215	.222	.240	.265	.295
	.448	.157	.179	.185	.205	.232	.266	.157	.175	.181	.205	.232	.263
	.468	.057	.080	.087	.113	.152	.194	.057	.076	.083	.110	.145	.188
	.478	-.032	-.028	-.016	.029	.079	.134	-.043	-.028	-.020	.029	.076	.134
	.483	-.167	-.166	-.142	-.057	.003	.071	-.167	-.170	-.146	-.064	-.004	.065
	.489	-.788	-1.144	-1.243	-.989	-.843	-.711	-.683	-.170	-1.046	-.906	-.772	-.641
	.494	-.203	-.250	-.320	-.449	-.413	-.348	-.494	-.283	-.354	-.478	-.413	-.319
	.499	-.089	-.112	-.134	-.308	-.308	-.234	-.699	-.116	-.151	-.333	-.338	-.270
	.509	.003	.004	.014	-.032	-.109	-.131	.509	.004	.018	-.046	-.120	-.140
	.519	.060	.083	.102	.132	.103	.022	.519	.088	.107	.136	.096	.016
	.529	.139	.180	.200	.237	.246	.165	.529	.180	.200	.237	.239	.155
	.539	.276	.333	.343	.364	.355	.282	.539	.333	.343	.361	.345	.272
	.549	.447	.482	.491	.513	.475	.385	.549	.482	.487	.502	.468	.382
Transition Flare	.554	.014	.027	.026	.022	.034	.031	.554	.479	.483	.466	.447	.389
	.558	.204	.314	.334	.391	.420	.421	.558	.360	.371	.412	.431	.408
Main stage	.568	-1.182	-.913	-.912	-1.477	-1.295	-1.117	.568	-.932	-.966	-1.495	-1.305	-1.123
	.577	-.271	-.691	-.743	-1.143	-.977	-.773	.577	-.667	-.696	-1.114	-.974	-.734
	.587	-.146	-.250	-.324	-.300	-.255	-.175	.587	-.292	-.345	-.304	-.241	-.165
	.597	-.100	-.112	-.138	-.057	-.229	-.448	.597	-.098	-.117	-.042	-.071	-.364
	.607	-.077	-.070	-.075	-.035	-.024	-.390	.607	-.065	-.075	-.035	-.021	-.400
	.617	-.054	-.051	-.054	-.039	.016	-.341	.617	-.047	-.050	-.039	.016	-.345
	.627	-.043	-.042	-.041	-.039	.016	-.286	.627	-.043	-.041	-.039	.016	-.289
	.637	-.043	-.028	-.033	-.035	.012	-.202	.637	-.042	.33	-.035	.009	-.195
	.647	-.021	-.020	-.022	-.031	-.003	.005	.647	-.023	-.024	-.034	-.005	.003
	.657	-.021	-.016	-.019	-.028	-.010	.031	.657	-.010	-.015	-.023	-.003	.035
	.697	-.013	-.013	-.013	-.026	-.012	.079	.697	-.013	-.015	-.026	-.012	.029
	.737	-.009	-.010	-.013	-.025	-.016	.011	.737	-.010	-.012	-.022	-.012	.014
	.777	-.005	-.006	-.007	-.017	-.010	.004	.777	-.005	-.004	-.015	-.006	.007
	.785	-.001	-.000	-.001	-.012	-.004	.010	.785	-.000	-.003	-.012	-.004	.010
	.817	.000	-.001	-.004	-.014	-.006	.003	.817	-.002	-.004	-.014	-.006	.004
	.857	.001	-.005	-.008	-.017	-.011	.011	.857	-.006	-.008	-.018	-.006	.012
	.877	-.001	-.004	-.006	-.017	-.011	.011	.877	-.007	-.009	-.018	-.013	.014
	.897	-.004	-.007	-.010	-.020	-.014	.015	.897	-.009	-.011	-.021	-.015	.016
								.917	-.010	-.012	-.021	-.015	.017
								.957	-.021	-.023	-.034	-.026	.029
								.997	-.080	-.083	-.093	-.092	.110

TABLE 11.- PRESSURE COEFFICIENTS FOR CONFIGURATION 12+ - Continued

(a) $M = 0.40$ to 0.95 ; $\alpha = 0^\circ$ - Concluded

		C_p for -					
		$\beta = -60^\circ$					
		$M = 0.40$	$M = 0.70$	$M = 0.85$	$M = 0.90$	$M = 0.95$	
Nose	x/l	.223	.247	.255	.275	.298	.379
		.190	.211	.218	.240	.265	.295
Upper stage		.448	.175	.177	.201	.232	.263
		.468	.071	.079	.110	.145	.188
Upper stage		.478	-.033	-.020	.029	.073	.131
		.483	-.088	-.091	-.096	-.092	-.110
Upper stage		.489	-1.047	-1.184	-1.003	-.860	-.774
		.494	-.283	-.354	-.456	-.362	-.285
Upper stage		.499	-.112	-.151	-.377	-.335	-.265
		.509	.004	.018	-.046	-.154	-.160
Upper stage		.519	.088	.102	.143	.096	.006
		.529	.190	.204	.245	.250	.158
Transition Flare		.539	.333	.343	.361	.352	.272
		.549	.477	.487	.492	.451	.363
Transition Flare		.554	.488	.492	.491	.491	.440
		.558	-.093	.030	.180	.249	.315
Main stage		.562	.155	.188	.273	.309	.347
		.568	-.848	-.886	-1.499	-1.309	-1.126
Main stage		.577	-.339	-.686	-1.103	-.909	-.672
		.587	-.134	-.343	-.268	-.752	-.581
Main stage		.597	-.077	-.135	-.164	-.243	-.500
		.607	-.066	-.065	-.079	-.039	-.416
Main stage		.617	-.054	-.042	-.050	-.024	-.345
		.627	-.043	-.037	-.041	-.016	-.283
Main stage		.637	-.043	-.028	-.033	-.012	-.189
		.657	-.025	-.020	-.032	-.009	-.189
Main stage		.677	-.17	-.020	-.022	-.004	.007
		.697	-.009	-.015	-.018	-.028	.020
Main stage		.737	-.009	-.008	-.013	-.011	.032
		.777	-.005	-.008	-.010	-.021	.017
Main stage		.785	-.005	-.005	-.007	-.015	.007
		.817	.000	-.001	-.003	-.014	.006
Main stage		.857	-.003	-.006	-.008	-.018	.006
		.877	-.004	-.007	-.009	-.019	.015
Main stage		.897	-.004	-.007	-.009	-.020	.015
		.917	-.009	-.012	-.015	-.025	.020
Main stage		.957	-.016	-.023	-.034	-.026	.029
		.997	-.072	-.084	-.094	-.092	.111

		C_p for -					
		$\beta = -90^\circ$					
		$M = 0.40$	$M = 0.70$	$M = 0.85$	$M = 0.90$	$M = 0.95$	
Nose	x/l	.418	.267	.287	.300	.314	.338
		.448	.157	.170	.173	.194	.222
Upper stage		.468	.057	.076	.083	.113	.145
		.483	-.178	-.189	-.171	-.085	-.027
Upper stage		.489	-.653	-.956	-1.012	-.802	-.677
		.509	.003	.004	.018	.001	-.092
Upper stage		.529	.139	.190	.200	.237	.260
		.549	.447	.495	.504	.528	.499
Transition Flare		.558	.238	.346	.359	.401	.437
		.568	-1.011	-.830	-.869	-1.517	-1.329
Main stage		.587	-.134	-.371	-.392	-.322	-.786
		.607	-.066	-.065	-.079	-.042	-.014
Main stage		.627	-.043	-.033	-.037	-.042	.019
		.657	-.025	-.021	-.022	-.032	-.004
Main stage		.697	-.013	-.015	-.016	-.027	.013
		.737	-.009	-.010	-.010	-.021	-.014
Main stage		.777	-.005	-.005	-.007	-.017	-.012
		.785	-.005	-.006	-.007	-.017	-.009
Main stage		.817	.000	-.000	-.000	-.010	.006
		.857	-.003	-.006	-.006	-.018	.005
Main stage		.877	-.004	-.007	-.009	-.017	.005
		.897	-.004	-.007	-.009	-.017	.005
Main stage		.917	-.009	-.012	-.015	-.021	.005
		.957	-.016	-.023	-.034	-.026	.005
Main stage		.997	-.072	-.084	-.094	-.092	.001
							-.011

TABLE 11.- PRESSURE COEFFICIENTS FOR CONFIGURATION 12A - Continued

(d) $M = 0.60$; $\alpha = -10^\circ$ to 10°

		C_p for -						
		$\beta = -30^\circ$						
		$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$
x/l								
Rose		.428	.380	.269	.242	.188	.145	.092
		.438	.335	.236	.208	.154	.117	.064
		.448	.307	.196	.169	.121	.078	.025
		.468	.206	.101	.073	.020	-.018	-.067
		.478	.105	-.006	-.034	-.083	-.116	-.158
		.483	-.036	-.149	-.172	-.242	-.285	-.328
		.489	-.091	-.298	-.324	-.398	-.441	-.484
		.494	-.149	-.441	-.467	-.541	-.584	-.627
		.499	-.208	-.598	-.624	-.698	-.741	-.784
		.509	-.264	-.748	-.774	-.848	-.891	-.934
Upper stage		.519	-.324	-.803	-.829	-.898	-.941	-.984
		.529	-.381	-.858	-.884	-.953	-.996	-.1039
		.539	-.434	-.903	-.929	-.998	-.1041	-.1114
		.549	-.487	-.948	-.974	-.1044	-.1117	-.1190
		.554	-.541	-.993	-.1046	-.1119	-.1192	-.1265
		.558	-.594	-.1048	-.1121	-.1194	-.1267	-.1340
		.568	-.647	-.1050	-.1123	-.1196	-.1269	-.1342
		.577	-.699	-.1052	-.1125	-.1198	-.1271	-.1344
		.587	-.752	-.1054	-.1127	-.1200	-.1273	-.1346
		.597	-.805	-.1056	-.1129	-.1202	-.1275	-.1348
Flare		.607	-.858	-.1058	-.1131	-.1204	-.1277	-.1350
		.617	-.911	-.1060	-.1133	-.1206	-.1279	-.1352
		.627	-.964	-.1062	-.1135	-.1208	-.1281	-.1354
		.637	-.1011	-.1064	-.1137	-.1210	-.1283	-.1356
		.647	-.1013	-.1066	-.1139	-.1212	-.1285	-.1358
		.657	-.1015	-.1068	-.1141	-.1214	-.1287	-.1360
		.667	-.1017	-.1070	-.1143	-.1216	-.1289	-.1362
		.677	-.1019	-.1072	-.1145	-.1218	-.1291	-.1364
		.687	-.1021	-.1074	-.1147	-.1220	-.1293	-.1366
		.697	-.1023	-.1076	-.1149	-.1222	-.1295	-.1368
Transition		.707	-.1025	-.1078	-.1151	-.1224	-.1297	-.1370
		.717	-.1027	-.1080	-.1153	-.1226	-.1299	-.1372
		.727	-.1029	-.1082	-.1155	-.1228	-.1301	-.1374
		.737	-.1031	-.1084	-.1157	-.1230	-.1303	-.1376
		.747	-.1033	-.1086	-.1159	-.1232	-.1305	-.1378
		.757	-.1035	-.1088	-.1161	-.1234	-.1307	-.1380
		.767	-.1037	-.1090	-.1163	-.1236	-.1309	-.1382
		.777	-.1039	-.1092	-.1165	-.1238	-.1311	-.1384
		.787	-.1041	-.1094	-.1167	-.1240	-.1313	-.1386
		.797	-.1043	-.1096	-.1169	-.1242	-.1315	-.1388
Main stage		.807	-.1045	-.1098	-.1171	-.1244	-.1317	-.1390
		.817	-.1047	-.1100	-.1173	-.1246	-.1319	-.1392
		.827	-.1049	-.1102	-.1175	-.1248	-.1321	-.1394
		.837	-.1051	-.1104	-.1177	-.1250	-.1323	-.1396
		.847	-.1053	-.1106	-.1179	-.1252	-.1325	-.1398
		.857	-.1055	-.1108	-.1181	-.1254	-.1327	-.1400
		.867	-.1057	-.1110	-.1183	-.1256	-.1329	-.1402
		.877	-.1059	-.1112	-.1185	-.1258	-.1331	-.1404
		.887	-.1061	-.1114	-.1187	-.1260	-.1333	-.1406
		.897	-.1063	-.1116	-.1189	-.1262	-.1335	-.1408

TABLE 11.- PRESSURE COEFFICIENTS FOR CONFIGURATION 124 - Continued

(b) $M = 0.60$; $\alpha = -10^\circ$ to 10° - Concluded

		C_p for -						C_p for -									
		$\beta = -60^\circ$						$\beta = -30^\circ$									
x/l		$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$	$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$		
Main stage	Nose	.428	.262	.270	.247	.236	.199	.156	.075	.418	.178	.248	.264	.275	.267	.241	
		.438	.229	.242	.208	.202	.166	.128	.041	.448	.071	.136	.151	.157	.143	.128	
		.448	.195	.197	.179	.163	.132	.089	.013	.468	-.002	.051	.061	.068	.048	.027	
		.468	.100	.172	.073	.068	.031	-.012	-.078	.064	.483	-.254	-.212	-.212	-.195	-.225	-.273
		.478	-.002	-.005	-.029	-.040	-.072	-.089	-.176	-.032	.489	-.788	-.763	-.792	-.769	-.847	-.904
		.483	.128	-.097	-.103	-.086	-.086	-.098	-.135	-.073	.509	-.065	-.017	-.006	.012	-.024	-.079
		.489	.800	-.809	-.850	-.843	-.843	-.910	-.999	-.014	.529	.074	.140	.157	.174	.160	.066
		.494	.222	-.225	-.243	-.231	-.252	-.255	-.299	.234	.549	.421	.464	.464	.475	.478	.408
		.499	-.106	-.092	-.104	-.092	-.101	-.101	-.148	.361	.559	.238	.286	.297	.308	.284	.230
		.509	-.025	-.005	-.006	-.006	-.003	-.003	-.018	.316	.568	-.830	-.833	-.863	-.834	-.785	-.808
.519	-.039	-.070	-.070	.081	.073	.057	.014	.587	-.297	-.260	-.249	-.243	-.298	-.325			
.529	.120	.157	.162	.144	.144	.107	.107	.607	-.140	-.074	-.069	-.052	-.055	-.076			
.539	.271	.302	.307	.314	.304	.283	.234	.627	-.123	-.063	-.052	-.034	-.038	-.064			
.549	.508	.511	.493	.469	.461	.422	.361	.657	-.111	-.048	-.038	-.018	-.027	-.056			
.554	.449	.469	.462	.462	.425	.381	.316	.697	-.102	-.040	-.030	-.010	-.021	-.049			
Transition flare	Nose	.568	-.998	-.932	-.909	-.857	-.745	-.701	-.652	.777	-.088	-.032	-.019	-.003	-.013	-.064	
		.577	-.546	-.602	-.620	-.602	-.640	-.640	-.634	.785	-.092	-.030	-.023	-.003	-.037	-.094	
		.587	.132	.132	.185	.208	.322	.383	.461	.817	-.088	-.030	-.019	-.001	-.009	-.088	
		.597	-.123	-.080	-.087	-.081	-.119	-.163	-.223	.857	-.092	-.032	-.019	-.001	-.009	-.035	
		.607	-.106	-.069	-.069	-.052	-.061	-.076	-.108	.877	-.071	-.019	-.012	-.005	-.005	-.029	
		.617	-.100	-.063	-.058	-.058	-.046	-.043	-.084	.897	-.074	-.026	-.019	-.000	-.009	-.034	
		.627	-.094	-.057	-.052	-.040	-.040	-.047	-.079	.917	-.058	-.023	-.021	-.003	-.012	-.078	
		.637	-.083	-.046	-.040	-.029	-.029	-.032	-.073	.957	-.068	-.032	-.023	-.007	-.047		
		.657	-.078	-.036	-.034	-.018	-.018	-.025	-.045	.997	-.135	-.101	-.097	-.087			
		.677	-.063	-.027	-.029	-.012	-.021	-.021	-.071								
.697	-.049	-.017	-.023	-.006	-.017	-.017	-.066										
.737	-.059	-.022	-.021	-.003	-.003	-.011	-.051										
.777	-.057	-.019	-.015	-.003	-.003	-.007	-.040										
.785	-.063	-.019	-.017	-.001	-.001	-.007	-.020										
.817	-.046	-.011	-.012	.005	.004	.004	-.040										
.857	-.050	-.018	-.017	.000	.000	.004	-.033										
.877	-.049	-.018	-.017	.000	.000	.009	-.021										
.897	-.051	-.018	-.019	-.001	-.001	-.009	-.034										
.917	-.058	-.023	-.023	-.007	-.007	-.015	-.038										
.957	-.068	-.032	-.032	-.015	-.023	-.037	-.047										
.997	-.135	-.101	-.097	-.073	-.087	-.106	-.128										

TABLE 11.- PRESSURE COEFFICIENTS FOR CONFIGURATION 12A - Continued

(c) $M = 0.80$; $\alpha = -10^\circ$ to 10°

		C_p for $\beta = 0^\circ$						C_p for $\beta = -30^\circ$											
		$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$	$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$				
Main stage	x/l	.428	.448	.381	.324	.275	.226	.183	.123	.428	.438	.414	.359	.313	.272	.226	.176	.108	
	Nose	.436	.425	.351	.294	.241	.196	.149	.092	.438	.436	.376	.325	.279	.234	.192	.138	.074	
Transition	x/l	.568	.577	.554	.558	.568	.577	.554	.558	.568	.577	.554	.558	.568	.577	.554	.558	.568	.577
	Flare	.577	.577	.554	.558	.568	.577	.554	.558	.568	.577	.554	.558	.568	.577	.554	.558	.568	.577
Main stage	x/l	.428	.448	.381	.324	.275	.226	.183	.123	.428	.438	.414	.359	.313	.272	.226	.176	.108	
	Nose	.436	.425	.351	.294	.241	.196	.149	.092	.438	.436	.376	.325	.279	.234	.192	.138	.074	
Transition	x/l	.568	.577	.554	.558	.568	.577	.554	.558	.568	.577	.554	.558	.568	.577	.554	.558	.568	.577
	Flare	.577	.577	.554	.558	.568	.577	.554	.558	.568	.577	.554	.558	.568	.577	.554	.558	.568	.577
Main stage	x/l	.428	.448	.381	.324	.275	.226	.183	.123	.428	.438	.414	.359	.313	.272	.226	.176	.108	
	Nose	.436	.425	.351	.294	.241	.196	.149	.092	.438	.436	.376	.325	.279	.234	.192	.138	.074	
Transition	x/l	.568	.577	.554	.558	.568	.577	.554	.558	.568	.577	.554	.558	.568	.577	.554	.558	.568	.577
	Flare	.577	.577	.554	.558	.568	.577	.554	.558	.568	.577	.554	.558	.568	.577	.554	.558	.568	.577
Main stage	x/l	.428	.448	.381	.324	.275	.226	.183	.123	.428	.438	.414	.359	.313	.272	.226	.176	.108	
	Nose	.436	.425	.351	.294	.241	.196	.149	.092	.438	.436	.376	.325	.279	.234	.192	.138	.074	
Transition	x/l	.568	.577	.554	.558	.568	.577	.554	.558	.568	.577	.554	.558	.568	.577	.554	.558	.568	.577
	Flare	.577	.577	.554	.558	.568	.577	.554	.558	.568	.577	.554	.558	.568	.577	.554	.558	.568	.577
Main stage	x/l	.428	.448	.381	.324	.275	.226	.183	.123	.428	.438	.414	.359	.313	.272	.226	.176	.108	
	Nose	.436	.425	.351	.294	.241	.196	.149	.092	.438	.436	.376	.325	.279	.234	.192	.138	.074	
Transition	x/l	.568	.577	.554	.558	.568	.577	.554	.558	.568	.577	.554	.558	.568	.577	.554	.558	.568	.577
	Flare	.577	.577	.554	.558	.568	.577	.554	.558	.568	.577	.554	.558	.568	.577	.554	.558	.568	.577
Main stage	x/l	.428	.448	.381	.324	.275	.226	.183	.123	.428	.438	.414	.359	.313	.272	.226	.176	.108	
	Nose	.436	.425	.351	.294	.241	.196	.149	.092	.438	.436	.376	.325	.279	.234	.192	.138	.074	
Transition	x/l	.568	.577	.554	.558	.568	.577	.554	.558	.568	.577	.554	.558	.568	.577	.554	.558	.568	.577
	Flare	.577	.577	.554	.558	.568	.577	.554	.558	.568	.577	.554	.558	.568	.577	.554	.558	.568	.577

TABLE 11.- PRESSURE COEFFICIENTS FOR CONFIGURATION 124 - Continued

(c) $M = 0.80$; $\alpha = -10^\circ$ to 10° - Concluded

		C_p for $\beta = -60^\circ$						C_p for $\beta = -90^\circ$							
		$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$	$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$
x/l	Nose	.428	.301	.286	.272	.233	.191	.108	.418	.287	.309	.309	.309	.278	.217
		.438	.267	.275	.248	.196	.161	.074	.448	.173	.189	.189	.180	.157	.092
x/l	Nose	.448	.233	.218	.196	.165	.119	.040	.468	.087	.102	.102	.086	.062	.005
		.478	.134	.139	.120	.098	.071	.028	.483	.195	.128	.128	.136	.156	.211
x/l	Upper stage	.483	.044	.025	.007	.020	.098	.133	.489	.143	.132	.128	.136	.156	.211
		.489	.133	.101	.085	.090	.098	.133	.489	.947	.928	.915	.928	.940	.963
x/l	Upper stage	.494	.140	.155	.137	.129	.129	.153	.509	.004	.023	.031	.023	.002	.064
		.494	.417	.441	.432	.445	.457	.454	.509	.056	.023	.031	.023	.002	.064
x/l	Upper stage	.499	.185	.211	.246	.270	.247	.282	.529	.191	.217	.222	.214	.185	.115
		.509	.017	.023	.027	.019	.010	.037	.549	.514	.514	.518	.525	.505	.446
x/l	Upper stage	.519	.061	.105	.120	.120	.104	.057	.554	.458	.514	.518	.525	.505	.446
		.529	.162	.210	.226	.217	.201	.154	.558	.372	.398	.379	.387	.370	.324
x/l	Upper stage	.539	.334	.373	.362	.350	.329	.275	.568	.869	.925	.947	.878	.831	.820
		.549	.556	.537	.506	.494	.466	.403	.587	.476	.430	.413	.457	.489	.532
x/l	Upper stage	.554	.548	.513	.498	.471	.432	.389	.607	.177	.095	.098	.126	.130	.189
		.568	.955	.971	.950	.823	.761	.664	.627	.122	.036	.039	.040	.056	.130
x/l	Transition	.577	.820	.791	.732	.714	.695	.676	.657	.114	.027	.019	.027	.046	.115
		.587	.278	.417	.410	.465	.485	.559	.697	.039	.021	.012	.020	.039	.103
x/l	Transition	.597	.153	.152	.172	.242	.286	.372	.737	.094	.032	.007	.014	.033	.095
		.607	.130	.079	.094	.118	.150	.212	.777	.087	.028	.004	.010	.029	.088
x/l	Transition	.617	.115	.048	.055	.063	.084	.123	.817	.074	.029	.004	.009	.028	.086
		.627	.103	.036	.039	.044	.056	.084	.857	.025	.005	.004	.006	.020	.074
x/l	Transition	.637	.091	.028	.031	.032	.041	.072	.897	.028	.014	.007	.014	.030	.082
		.657	.082	.024	.018	.023	.032	.064	.957	.070	.023	.004	.004	.026	.078
x/l	Transition	.677	.066	.027	.014	.020	.030	.060	.997	.146	.092	.052	.052	.082	.134
		.697	.051	.018	.011	.017	.028	.056							
x/l	Transition	.737	.062	.021	.008	.013	.024	.049							
		.7	.058	.018	.004	.009	.018	.042							
x/l	Transition	.5	.042	.018	.002	.007	.015	.038							
		.817	.049	.012	.001	.006	.012	.033							
x/l	Transition	.857	.055	.019	.005	.010	.016	.035							
		.877	.054	.018	.006	.012	.016	.035							
x/l	Transition	.897	.057	.010	.007	.012	.017	.037							
		.917	.064	.017	.012	.017	.023	.042							
x/l	Transition	.957	.070	.023	.020	.026	.033	.052							
		.997	.146	.092	.083	.095	.106	.134							

TABLE 11.- PRESSURE COEFFICIENTS FOR CONFIGURATION 124 - Continued

(a) $M = 1.00$; $\alpha = -10^\circ$ to 10°

		C_p for $\beta = 0^\circ$						C_p for $\beta = -30^\circ$							
		$\beta = 0^\circ$						$\beta = -30^\circ$							
		$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$	$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$
Rose	x/l	.551	.477	.426	.374	.332	.292	.238	.515	.458	.423	.374	.332	.286	.226
		.524	.452	.402	.350	.305	.262	.211	.438	.428	.393	.344	.302	.253	.190
		.485	.413	.366	.314	.269	.225	.178	.448	.428	.395	.357	.311	.269	.222
Upper stage	x/l	.410	.338	.297	.245	.200	.159	.109	.370	.320	.285	.242	.200	.159	.100
		.337	.275	.237	.188	.149	.108	.064	.478	.460	.431	.388	.348	.305	.262
		.483	.429	.377	.324	.270	.219	.167	.489	.468	.448	.428	.409	.388	.368
Transition	x/l	.558	.485	.434	.382	.330	.278	.226	.549	.486	.434	.382	.330	.278	.226
		.524	.452	.402	.350	.305	.262	.211	.558	.486	.434	.382	.330	.278	.226
		.485	.413	.366	.314	.269	.225	.178	.549	.486	.434	.382	.330	.278	.226
Main stage	x/l	.998	.918	.838	.758	.678	.598	.518	.997	.917	.837	.757	.677	.597	.517
		.951	.871	.791	.711	.631	.551	.471	.950	.870	.790	.710	.630	.550	.470
		.904	.824	.744	.664	.584	.504	.424	.903	.823	.743	.663	.583	.503	.423

TABLE 11.- PRESSURE COEFFICIENTS FOR CONFIGURATION 124 - Continued

(d) $M = 1.00$; $\alpha = -10^\circ$ to 10° - Concluded

		C_p for $\beta = -60^\circ$							C_p for $\beta = -30^\circ$							AC 100							
		$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$	$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$	$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$	
Main stage	x/l	.428	.407	.393	.371	.338	.298	.226	.428	.404	.393	.371	.338	.298	.226	.328	.386	.408	.407	.408	.407	.380	.331
	Nose	.438	.373	.363	.341	.308	.271	.193	.226	.448	.404	.371	.338	.298	.226	.328	.386	.408	.407	.408	.407	.380	.331
		.448	.343	.336	.311	.281	.234	.163	.193	.468	.344	.311	.281	.234	.163	.226	.281	.309	.305	.309	.305	.271	.220
		.478	.271	.272	.257	.239	.165	.097	.097	.483	.272	.257	.239	.165	.097	.169	.221	.249	.242	.249	.242	.201	.148
		.483	.208	.215	.188	.161	.114	.052	.052	.489	.215	.188	.161	.114	.052	.228	.283	.309	.305	.309	.283	.201	.148
		.489	.187	.149	.123	.115	.088	.041	.041	.494	.149	.123	.115	.088	.041	.028	.083	.111	.107	.107	.083	.072	.022
		.494	.165	.135	.108	.092	.065	.018	.018	.499	.135	.108	.092	.065	.018	.028	.083	.111	.107	.107	.083	.072	.022
		.499	.144	.114	.087	.071	.044	.007	.007	.509	.114	.087	.071	.044	.007	.028	.083	.111	.107	.107	.083	.072	.022
		.509	.135	.105	.078	.062	.035	.008	.008	.519	.105	.078	.062	.035	.008	.028	.083	.111	.107	.107	.083	.072	.022
		.519	.122	.092	.065	.049	.022	.005	.005	.529	.092	.065	.049	.022	.005	.028	.083	.111	.107	.107	.083	.072	.022
		.529	.105	.075	.048	.032	.005	.008	.008	.539	.075	.048	.032	.005	.008	.028	.083	.111	.107	.107	.083	.072	.022
		.539	.088	.058	.031	.015	.008	.005	.005	.549	.058	.031	.015	.008	.005	.028	.083	.111	.107	.107	.083	.072	.022
		.549	.068	.038	.011	.005	.008	.005	.005	.554	.038	.011	.005	.008	.005	.028	.083	.111	.107	.107	.083	.072	.022
	Transition	x/l	.568	.577	.587	.597	.607	.617	.627	.568	.577	.587	.597	.607	.617	.627	.568	.577	.587	.597	.607	.617	.627
Flare		.577	.587	.597	.607	.617	.627	.637	.577	.587	.597	.607	.617	.627	.637	.577	.587	.597	.607	.617	.627	.637	
Main stage		.587	.597	.607	.617	.627	.637	.647	.587	.597	.607	.617	.627	.637	.647	.587	.597	.607	.617	.627	.637	.647	
		.597	.607	.617	.627	.637	.647	.657	.597	.607	.617	.627	.637	.647	.657	.597	.607	.617	.627	.637	.647	.657	
		.607	.617	.627	.637	.647	.657	.667	.607	.617	.627	.637	.647	.657	.667	.607	.617	.627	.637	.647	.657	.667	
		.617	.627	.637	.647	.657	.667	.677	.617	.627	.637	.647	.657	.667	.677	.617	.627	.637	.647	.657	.667	.677	
		.627	.637	.647	.657	.667	.677	.687	.627	.637	.647	.657	.667	.677	.687	.627	.637	.647	.657	.667	.677	.687	
		.637	.647	.657	.667	.677	.687	.697	.637	.647	.657	.667	.677	.687	.697	.637	.647	.657	.667	.677	.687	.697	
		.647	.657	.667	.677	.687	.697	.707	.647	.657	.667	.677	.687	.697	.707	.647	.657	.667	.677	.687	.697	.707	
		.657	.667	.677	.687	.697	.707	.717	.657	.667	.677	.687	.697	.707	.717	.657	.667	.677	.687	.697	.707	.717	
		.667	.677	.687	.697	.707	.717	.727	.667	.677	.687	.697	.707	.717	.727	.667	.677	.687	.697	.707	.717	.727	
		.677	.687	.697	.707	.717	.727	.737	.677	.687	.697	.707	.717	.727	.737	.677	.687	.697	.707	.717	.727	.737	
		.687	.697	.707	.717	.727	.737	.747	.687	.697	.707	.717	.727	.737	.747	.687	.697	.707	.717	.727	.737	.747	
		.697	.707	.717	.727	.737	.747	.757	.697	.707	.717	.727	.737	.747	.757	.697	.707	.717	.727	.737	.747	.757	
		.707	.717	.727	.737	.747	.757	.767	.707	.717	.727	.737	.747	.757	.767	.707	.717	.727	.737	.747	.757	.767	
		.717	.727	.737	.747	.757	.767	.777	.717	.727	.737	.747	.757	.767	.777	.717	.727	.737	.747	.757	.767	.777	
		.727	.737	.747	.757	.767	.777	.787	.727	.737	.747	.757	.767	.777	.787	.727	.737	.747	.757	.767	.777	.787	
		.737	.747	.757	.767	.777	.787	.797	.737	.747	.757	.767	.777	.787	.797	.737	.747	.757	.767	.777	.787	.797	
		.747	.757	.767	.777	.787	.797	.807	.747	.757	.767	.777	.787	.797	.807	.747	.757	.767	.777	.787	.797	.807	
		.757	.767	.777	.787	.797	.807	.817	.757	.767	.777	.787	.797	.807	.817	.757	.767	.777	.787	.797	.807	.817	
		.767	.777	.787	.797	.807	.817	.827	.767	.777	.787	.797	.807	.817	.827	.767	.777	.787	.797	.807	.817	.827	
		.777	.787	.797	.807	.817	.827	.837	.777	.787	.797	.807	.817	.827	.837	.777	.787	.797	.807	.817	.827	.837	
		.787	.797	.807	.817	.827	.837	.847	.787	.797	.807	.817	.827	.837	.847	.787	.797	.807	.817	.827	.837	.847	
		.797	.807	.817	.827	.837	.847	.857	.797	.807	.817	.827	.837	.847	.857	.797	.807	.817	.827	.837	.847	.857	
		.807	.817	.827	.837	.847	.857	.867	.807	.817	.827	.837	.847	.857	.867	.807	.817	.827	.837	.847	.857	.867	
		.817	.827	.837	.847	.857	.867	.877	.817	.827	.837	.847	.857	.867	.877	.817	.827	.837	.847	.857	.867	.877	
		.827	.837	.847	.857	.867	.877	.887	.827	.837	.847	.857	.867	.877	.887	.827	.837	.847	.857	.867	.877	.887	
		.837	.847	.857	.867	.877	.887	.897	.837	.847	.857	.867	.877	.887	.897	.837	.847	.857	.867	.877	.887	.897	
		.847	.857	.867	.877	.887	.897	.907	.847	.857	.867	.877	.887	.897	.907	.847	.857	.867	.877	.887	.897	.907	
		.857	.867	.877	.887	.897	.907	.917	.857	.867	.877	.887	.897	.907	.917	.857	.867	.877	.887	.897	.907	.917	
		.867	.877	.887	.897	.907	.917	.927	.867	.877	.887	.897	.907	.917	.927	.867	.877	.887	.897	.907	.917	.927	
		.877	.887	.897	.907	.917	.927	.937	.877	.887	.897	.907	.917	.927	.937	.877	.887	.897	.907	.917	.927	.937	
		.887	.897	.907	.917	.927	.937	.947	.887	.897	.907	.917	.927	.937	.947	.887	.897	.907	.917	.927	.937	.947	
		.897	.907	.917	.927	.937	.947	.957	.897	.907	.917	.927	.937	.947	.957	.897	.907	.917	.927	.937	.947	.957	
		.907	.917	.927	.937	.947	.957	.967	.907	.917	.927	.937	.947	.957	.967	.907	.917	.927	.937	.947	.957	.967	
		.917	.927	.937	.947	.957	.967	.977	.917	.927	.937	.947	.957	.967	.977	.917	.927	.937	.947	.957	.967	.977	
		.927	.937	.947	.957	.967	.977	.987	.927	.937	.947	.957	.967	.977	.987	.927	.937	.947	.957	.967	.977	.987	
		.937	.947	.957	.967	.977	.987	.997	.937	.947	.957	.967	.977	.987	.997	.937	.947	.957	.967	.977	.987	.997	
		.947	.957	.967	.977	.987	.997	1.007	.947	.957	.967	.977	.987	.997	1.007	.947	.957	.967	.977	.987	.997	1.007	

TABLE 11.- PRESSURE COEFFICIENTS FOR CONFIGURATION 124 - Continued.

(a) $M = 1.20$; $\alpha = -10^\circ$ to 10°

x/l	C_p for $\beta = 0^\circ$						C_p for $\beta = -30^\circ$							
	$\alpha = 0^\circ$		$\alpha = 3^\circ$		$\alpha = 6^\circ$		$\alpha = 0^\circ$		$\alpha = 3^\circ$		$\alpha = 6^\circ$			
	$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$	$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$
	Nozzle													
.428	.506	.430	.364	.314	.277	.239	.192	.428	.411	.359	.314	.282	.233	.181
.438	.517	.435	.375	.322	.277	.247	.192	.438	.413	.359	.317	.274	.239	.173
.448	.506	.427	.359	.320	.269	.236	.181	.448	.408	.354	.317	.274	.236	.173
.468	.493	.416	.362	.317	.274	.231	.181	.468	.397	.354	.312	.274	.236	.173
.478	.466	.403	.359	.312	.274	.231	.176	.478	.394	.351	.312	.277	.236	.173
.483	.426	.376	.338	.298	.258	.220	.165	.483	.389	.351	.312	.277	.236	.173
.489	.283	.258	.273	.289	.310	.328	.359	.489	.355	.327	.250	.258	.217	.157
.494	.289	.332	.350	.371	.385	.391	.379	.494	.217	.226	.239	.266	.287	.315
.499	.203	.266	.292	.324	.343	.352	.343	.499	.308	.355	.374	.390	.442	.442
.509	.112	.183	.220	.253	.271	.281	.270	.509	.297	.317	.341	.360	.372	.296
.519	.066	.123	.178	.225	.262	.280	.288	.519	.181	.215	.219	.251	.280	.250
.529	.299	.346	.293	.225	.162	.092	.032	.529	.128	.037	.175	.098	.042	.008
.539	.344	.421	.334	.247	.195	.139	.110	.539	.339	.288	.219	.140	.083	.057
.549	.635	.487	.387	.275	.211	.152	.154	.549	.482	.381	.269	.167	.108	.057
.554	.060	.050	.049	.050	.048	.052	.054	.554	.637	.462	.300	.220	.115	.103
.558	.995	.893	.712	.414	.197	.128	.135	.558	.887	.688	.341	.303	.373	.342
	Transition													
	Flare													
.568	.568	.594	.565	.528	.453	.365	.266	.568	.606	.565	.443	.347	.262	.182
.577	.344	.360	.350	.327	.285	.215	.157	.577	.577	.369	.275	.238	.199	.150
.587	.159	.225	.259	.230	.219	.223	.246	.587	.247	.261	.228	.244	.341	.442
.597	.090	.161	.198	.181	.214	.220	.255	.597	.126	.148	.145	.150	.176	.219
.607	.052	.120	.151	.162	.191	.204	.227	.607	.082	.131	.154	.164	.195	.219
.617	.041	.098	.124	.145	.167	.170	.175	.617	.063	.106	.124	.15	.195	.219
.627	.027	.081	.104	.128	.136	.135	.119	.627	.060	.092	.107	.150	.162	.169
.637	.016	.065	.082	.098	.111	.104	.078	.637	.049	.079	.131	.131	.132	.130
.657	.027	.070	.080	.077	.073	.058	.041	.657	.053	.069	.075	.106	.104	.092
.677	.034	.044	.049	.051	.052	.032	.024	.677	.057	.042	.043	.062	.063	.073
.697	.027	.040	.042	.039	.030	.018	.018	.697	.069	.047	.043	.045	.043	.050
.717	.020	.025	.027	.024	.027	.024	.016	.717	.049	.039	.040	.041	.035	.058
.737	.015	.012	.021	.038	.033	.027	.012	.737	.014	.019	.033	.033	.039	.058
.755	.026	.004	.018	.024	.028	.026	.016	.755	.007	.017	.028	.025	.029	.059
.817	.021	.002	.005	.021	.018	.009	.004	.817	.005	.016	.017	.013	.016	.056
.857	.020	.010	.009	.002	.001	.010	.010	.857	.005	.014	.009	.016	.020	.058
.877	.030	.003	.007	.001	.004	.005	.010	.877	.001	.002	.010	.016	.018	.058
.897	.013	.003	.001	.005	.009	.013	.017	.897	.001	.011	.007	.006	.015	.058
								.897	.013	.003	.002	.006	.015	.057
								.917	.016	.003	.006	.006	.016	.050
								.957	.016	.015	.006	.006	.016	.050
								.997	.006	.021	.006	.006	.016	.044
								.997	.006	.021	.003	.006	.016	.095

TABLE 11.- PRESSURE COEFFICIENTS FOR CONFIGURATION 124 - Concluded

(e) $M = 1.20$; $\alpha = -10^\circ$ to 10° - Concluded

		C_p for $\beta = -60^\circ$							C_p for $\beta = -30^\circ$						
		$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$	$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$
Main stage	x/l	.428	.362	.330	.312	.282	.247	.184	.418	.241	.288	.308	.314	.297	.259
	Nose	.438	.367	.327	.314	.282	.263	.181	.448	.244	.293	.303	.298	.289	.235
		.448	.364	.332	.312	.285	.249	.176	.468	.239	.296	.316	.317	.287	.232
		.468	.348	.332	.312	.290	.252	.173	.483	.182	.250	.268	.274	.249	.189
		.477	.330	.322	.312	.290	.252	.173	.489	-.262	-.204	-.180	-.171	-.194	-.244
		.483	.204	-.153	-.144	-.146	-.169	-.211	.509	-.292	-.261	-.256	-.260	-.273	-.304
		.489	.368	.327	.302	.299	.299	-.317	.529	.188	.233	.238	.253	.245	.192
		.494	.377	.319	.305	.296	.296	-.413	.549	.332	.322	.299	.294	.334	.322
		.499	.294	.310	.330	.351	.380	-.437	.558	.723	.648	.514	.479	.631	.706
		.509	-.220	-.225	-.230	-.211	-.157	-.092	.568	-.670	-.611	-.551	-.556	-.612	-.666
Transition Flare	x/l	.519	.128	.106	.170	.084	.056	.001	.587	-.374	-.330	-.278	-.327	-.339	-.390
	Nose	.529	.268	.265	.211	.156	.144	.063	.607	-.259	-.219	-.201	-.170	-.228	-.268
		.539	.390	.344	.236	.206	.202	.137	.627	-.239	-.153	-.121	-.120	-.158	-.249
		.549	.334	.334	.261	.264	.260	.168	.657	-.180	-.084	-.059	-.052	-.093	-.183
		.554	.699	.550	.371	.344	.324	.339	.697	-.168	-.093	-.055	-.044	-.061	-.170
									.737	-.145	-.074	-.046	-.037	-.073	-.150
									.777	-.100	-.056	-.031	-.020	-.057	-.123
									.785	-.112	-.060	-.032	-.014	-.026	-.124
									.817	-.093	-.032	-.013	-.008	-.019	-.105
									.857	-.096	-.032	-.018	-.031	-.052	-.103
Main stage	x/l	.897	.071	-.031	-.004	.009	.024	.03	.897	-.100	-.043	-.017	-.006	-.027	-.091
	Nose	.917	.079	-.010	-.001	.004	.018	.04							
		.937	-.077	-.037	-.015	-.021	-.023	.0							
		.937	-.077	-.037	-.015	-.021	-.023	.0							
		.937	-.077	-.037	-.015	-.021	-.023	.0							
		.937	-.077	-.037	-.015	-.021	-.023	.0							
		.937	-.077	-.037	-.015	-.021	-.023	.0							
		.937	-.077	-.037	-.015	-.021	-.023	.0							
		.937	-.077	-.037	-.015	-.021	-.023	.0							
		.937	-.077	-.037	-.015	-.021	-.023	.0							
	.937	-.077	-.037	-.015	-.021	-.023	.0								

TABLE 12.- PRESSURE COEFFICIENTS FOR CONFIGURATION 324

(a) $M = 0.40$ to 0.95 ; $\alpha = 0^\circ$

		C_p for -					C_p for -				
		$\phi = 0^\circ$					$\phi = -30^\circ$				
		$M = 0.40$	$M = 0.70$	$M = 0.85$	$M = 0.90$	$M = 0.95$	$M = 0.40$	$M = 0.70$	$M = 0.85$	$M = 0.90$	$M = 0.95$
Nose	x/l	.487	.558	.636	.658	.696	.461	.553	.582	.636	.652
		.334	.399	.490	.518	.563	.471	.374	.407	.471	.497
Upper stage	x/l	.095	.195	.310	.342	.393	.481	.195	.232	.306	.342
		-1.148	-0.739	-0.378	-0.367	-0.467	.489	-.622	-.513	-.381	-.370
Upper stage	x/l	.485	.668	.538	.367	.433	.494	-.550	-.467	-.352	-.350
		-1.160	-0.541	-0.384	-0.374	-0.414	.499	-.532	-.467	-.359	-.357
Upper stage	x/l	.025	.240	.359	.377	.414	.509	-.014	-.360	-.363	.414
		-0.25	-0.17	-0.31	-0.357	-0.356	.519	-.053	-.205	-.327	-.347
Transition Flare	x/l	.132	.120	.023	.306	.280	.529	.132	.102	.263	.306
		.255	.225	.152	-0.232	-0.219	.539	.244	-.023	.119	.249
Transition Flare	x/l	.446	.347	.268	.020	-.092	.549	.423	.247	-.023	-.118
		.030	.042	.043	.046	.045	.554	.373	.317	.089	.000
Main stage	x/l	.196	.239	.174	.089	.038	.558	.207	.264	.114	.036
		-1.237	-1.051	-1.036	-.710	-.653	.568	-1.203	-.991	-.656	-.532
Main stage	x/l	.327	.327	.297	.216	.269	.577	-.238	-.272	-.195	-.205
		-1.138	-1.154	-1.139	-.118	-.289	.587	-.138	-.139	-.120	-.125
Main stage	x/l	.093	.104	.093	.078	.197	.597	.070	.064	-.056	.057
		-0.059	-0.076	-0.064	-0.057	-0.089	.607	-.059	-.064	-.059	-.061
Main stage	x/l	.048	.058	.048	.047	.038	.617	-.048	.052	-.048	-.044
		-0.037	-0.049	-0.039	-0.037	-0.072	.627	-.037	-.039	-.038	-.037
Main stage	x/l	.025	.040	.031	.027	.012	.637	-.025	-.031	-.031	.031
		-0.019	-0.023	-0.021	-0.021	-0.011	.657	-.019	-.022	-.023	-.025
Main stage	x/l	.015	.018	.016	.019	.012	.677	-.015	-.011	-.013	-.012
		-0.007	-0.011	-0.009	-0.015	-0.012	.697	-.011	-.012	-.013	-.007
Main stage	x/l	.003	.005	.003	.014	.014	.737	-.003	-.012	-.014	-.012
		-0.001	-0.005	-0.003	-0.009	-0.009	.777	-.003	-.006	-.009	-.015
Main stage	x/l	.005	.004	.004	.009	.009	.777	.001	.000	-.003	-.006
		-0.005	-0.004	-0.004	-0.004	-0.006	.785	.005	.004	-.002	-.003
Main stage	x/l	.003	.000	.002	.004	.006	.817	.003	.004	-.002	-.004
		-0.003	-0.004	-0.002	-0.007	-0.010	.857	.002	.001	-.002	-.004
Main stage	x/l	.000	.006	.005	.007	.010	.877	.002	.004	-.007	-.009
		-0.000	-0.006	-0.004	-0.008	-0.013	.897	-.001	-.006	-.010	-.012
Main stage	x/l						.917	-.001	-.006	-.011	-.014
							.957	-.012	-.018	-.022	-.024
Main stage	x/l						.997	-.065	-.078	-.087	-.093

TABLE 2.- PRESSURE COEFFICIENTS FOR TRANSDUCER TUBES - Continued

(a) $M = 0.40$ to 0.95 ; $\alpha = 0^\circ$ - Continued

NC 324

		C_p for -						
		$\beta = 90^\circ$						
		$M = 0.40$	$M = 0.70$	$M = 0.85$	$M = 0.90$	$M = 0.95$		
Nose	x/l	.461	.487	.553	.582	.629	.652	.690
		.471	.399	.429	.483	.511	.551	.590
Upper stage		.481	.095	.209	.248	.310	.342	.390
		.489	-1.170	-0.500	-0.410	-0.399	-0.434	-0.527
Upper stage		.494	.482	.413	.331	.340	.395	.461
		.499	-0.486	-0.472	-0.334	-0.347	-0.401	-0.385
Upper stage		.509	-0.255	-0.354	-0.372	-0.353	-0.353	-0.302
		.519	.053	-0.126	-0.230	-0.337	-0.296	-0.299
Transition Flare		.529	.132	.068	.069	.069	.069	.069
		.539	.244	.179	.069	.188	.249	.251
Transition Flare		.545	.412	.302	.202	.077	-0.155	-0.159
		.554	.373	.355	.313	.114	.019	-0.006
Main stage		.558	-0.073	.239	.227	.065	-0.027	-0.031
		.562	.036	.127	.174	.216	.208	.186
Main stage		.568	-1.147	-1.037	-.953	-.592	-.491	-.564
		.577	-.238	-.281	-.247	-.191	-.199	-.334
Main stage		.587	-0.138	-0.149	-0.135	-.124	-.128	-.267
		.597	-.081	-.094	-.085	-.081	-.088	-.191
Main stage		.607	-.059	-.072	-.064	-.059	-.061	-.097
		.617	-.048	-.058	-.052	-.048	-.047	-.047
Main stage		.627	-.037	-.049	-.039	-.038	-.041	-.031
		.637	-.025	-.040	-.031	-.031	-.031	-.018
Main stage		.657	-.019	-.023	-.022	-.024	-.025	-.015
		.677	-.013	-.017	-.016	-.019	-.019	-.013
Main stage		.697	-.007	-.011	-.011	-.013	-.014	-.011
		.737	-.003	-.006	-.006	-.009	-.012	-.011
Main stage		.777	.001	-.001	-.002	-.007	-.007	-.007
		.785	.001	.000	.000	-.004	-.006	-.007
Main stage		.817	.005	.001	.001	-.002	-.004	-.005
		.857	.002	.004	.003	-.007	-.009	-.011
Main stage		.877	.000	.005	.004	-.007	-.009	-.012
		.917	-.004	.005	.010	-.013	-.015	-.017
Main stage		.957	-.017	-.019	-.018	-.022	-.024	-.027
		.997	-.066	-.079	-.079	-.089	-.094	-.104

TABLE 12.- PRESSURE COEFFICIENTS FOR CONFIGURATION 264 - Continued

324
NO 264

(b) $M = 0.60$; $\alpha = -10^\circ$ to 10°

		C_p for $\beta = 0^\circ$						C_p for $\beta = -30^\circ$								
		$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$	$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$	
x/l	Nose	.461	.752	.659	.598	.531	.460	.390	.296	.461	.708	.643	.587	.531	.466	.401
		.471	.592	.505	.432	.371	.311	.252	.163	.471	.515	.447	.391	.341	.292	.238
		.481	.360	.261	.194	.150	.101	.059	-.008	.481	.321	.250	.194	.150	.118	.075
x/l	Upper stage	.489	-1.125	-1.094	-.988	-.846	-.761	-.663	-.488	.489	-1.085	-.964	-1.044	-.894	-.535	-.464
		.494	-.382	-.630	-.763	-.608	-.555	-.418	-.281	.494	-.564	-.773	-.728	-.694	-.517	-.461
		.499	-.068	-.163	-.301	-.466	-.481	-.464	-.379	.499	-.137	-.283	-.432	-.546	-.540	-.481
x/l	Upper stage	.509	.040	.020	.016	.064	.007	-.048	-.134	.509	.018	.062	-.030	-.085	-.278	-.316
		.519	.109	.076	.070	.050	.086	.019	.075	.519	.086	.070	.070	.075	-.010	-.053
		.529	.194	.167	.155	.143	.110	.078	.015	.529	.166	.156	.150	.143	.104	.078
x/l	Upper stage	.539	.354	.315	.292	.257	.190	.140	.094	.539	.325	.310	.286	.252	.184	.152
		.549	.622	.555	.497	.428	.310	.220	.163	.549	.599	.543	.491	.417	.292	.249
		.554	.040	.036	.035	.035	.030	.043	.042	.554	.534	.490	.445	.377	.277	.211
x/l	Transition	.558	.399	.333	.276	.214	.136	.082	.059	.558	.410	.361	.310	.242	.148	.105
		.568	-1.009	-1.052	-1.082	-1.059	-1.041	-.937	-.880	.568	-1.386	-1.280	-1.179	-1.076	-1.019	-.994
		.577	-.199	-.289	-.307	-.295	-.266	-.247	-.236	.577	-.211	-.283	-.301	-.284	-.255	-.270
x/l	Main stage	.587	-.062	-.106	-.136	-.142	-.150	-.139	-.139	.587	-.097	-.123	-.136	-.142	-.152	-.156
		.597	.034	-.066	-.090	-.096	-.107	-.105	-.088	.597	.040	-.081	-.067	-.067	-.078	-.076
		.607	-.017	-.049	-.067	-.067	-.078	-.076	-.060	.607	-.043	-.055	-.067	-.067	-.078	-.071
x/l	Main stage	.617	-.005	-.038	-.050	-.050	-.061	-.053	-.043	.617	-.028	-.044	-.050	-.050	-.061	-.053
		.627	.006	-.027	-.039	-.039	-.050	-.042	-.031	.627	-.023	-.032	-.039	-.039	-.050	-.048
		.637	.011	-.015	-.027	-.033	-.038	-.036	-.025	.637	-.011	-.027	-.027	-.033	-.038	-.037
x/l	Main stage	.657	.019	-.009	-.020	-.021	-.026	-.016	-.014	.657	-.009	-.020	-.024	-.023	-.030	-.025
		.677	.023	-.003	-.016	-.015	-.022	-.010	-.010	.677	.005	-.007	-.010	-.009	-.018	-.012
		.697	.027	-.003	-.010	-.009	-.006	-.006	-.008	.697	.001	-.009	-.014	-.011	-.016	-.012
x/l	Main stage	.737	.023	-.007	-.008	-.007	-.014	-.002	-.008	.737	.015	-.005	-.010	-.005	-.010	-.006
		.777	.035	.009	-.004	-.001	-.008	.000	-.008	.777	.001	-.003	-.004	-.001	-.004	.000
		.785	.042	.015	.004	.001	-.002	.004	-.002	.785	.011	.003	.012	.001	.004	.002
x/l	Main stage	.813	.038	.003	.003	.004	.004	.003	-.008	.813	.007	.003	.000	.004	-.004	.000
		.857	.032	.009	.001	-.001	-.007	-.001	-.015	.857	.007	-.003	-.005	.001	-.007	-.004
		.877	.035	.009	.000	.001	-.007	-.001	-.017	.877	.004	-.004	-.005	-.001	-.008	-.005
x/l	Main stage	.897	.029	.006	-.003	-.001	-.009	-.004	-.021	.897	.003	-.006	-.007	-.003	-.010	-.007
											.003	-.006	-.008	-.003	-.012	-.010
											.003	-.018	-.018	-.015	-.023	-.023
x/l	Main stage										-.096	-.087	-.076	-.072	-.086	-.091

TABLE 12.- PRESSURE COEFFICIENTS FOR CONFIGURATION 364 - Continued

(b) $M = 0.60$; $\alpha = -10^\circ$ to 10° - Concluded

		C_p for $\beta = -90^\circ$						x/z	C_p for $\beta = -60^\circ$							
		$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$		$\alpha = 10^\circ$	$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$
None		.461	.443	.521	.526	.510	.490	.417								
	Main stage	.481	.105	.145	.161	.145	.131	.086	.489	-.961	-.699	-.705	-.795	-.793	-.906	
		Transition	.509	-.137	-.238	-.187	-.186	-.150	-.162	.529	.099	.132	.143	.133	.176	.020
None		.549	.388	.429	.360	.401	.437	.368	.549	.388	.429	.360	.401	.437	.368	
	Transition	.558	.214	.249	.214	.221	.250	.188	.558	.214	.249	.214	.221	.250	.188	
None		.568	-.907	-.961	-1.070	-1.041	-.946	-.880	.568	-.907	-.961	-1.070	-1.041	-.946	-.880	
	Main stage	.587	-.216	-.158	-.136	-.147	-.167	-.236	.607	-.131	-.067	-.067	-.072	-.082	-.134	
		Transition	.627	-.108	-.061	-.039	-.050	-.065	-.117	.627	-.108	-.061	-.039	-.050	-.065	-.117
None		.657	-.105	-.056	-.021	-.034	-.049	-.114	.657	-.105	-.056	-.021	-.034	-.049	-.114	
	Transition	.697	-.099	-.044	-.024	-.024	-.039	-.104	.697	-.099	-.044	-.024	-.024	-.039	-.104	
None		.737	.091	-.036	-.016	-.016	-.031	-.096	.737	.091	-.036	-.016	-.016	-.031	-.096	
	Main stage	.775	-.085	-.034	-.010	-.010	-.027	-.098	.775	-.085	-.034	-.010	-.010	-.027	-.098	
		Transition	.817	-.089	-.040	-.014	-.014	-.029	-.098	.817	-.089	-.040	-.014	-.014	-.029	-.098
None		.857	-.073	-.028	-.010	-.010	-.024	-.081	.857	-.073	-.028	-.010	-.010	-.024	-.081	
	Transition	.897	-.075	-.032	-.003	-.014	-.027	-.082	.897	-.075	-.032	-.003	-.014	-.027	-.082	
None		.937	-.105	-.028	-.015	-.028	-.050	-.128	.937	-.105	-.028	-.015	-.028	-.050	-.128	
	Main stage	.977	-.105	-.089	-.072	-.087	-.097	-.128	.977	-.105	-.089	-.072	-.087	-.097	-.128	
		Transition	.997	-.072	-.087	-.072	-.087	-.097	-.128	.997	-.072	-.087	-.072	-.087	-.097	-.128

TABLE 12.- PRESSURE COEFFICIENTS FOR CONFIGURATION 204 - Continued

(c) $M = 0.80$; $\alpha = -10^\circ$ to 10°

		C_p for $\beta = 0^\circ$						C_p for $\beta = -30^\circ$																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																	
		$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$							$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																				
Nozzle	x/l	.461	.471	.481	.489	.494	.499	.509	.519	.529	.539	.549	.554	.558	.568	.577	.587	.597	.607	.617	.627	.637	.647	.657	.667	.677	.687	.697	.707	.717	.727	.737	.747	.757	.767	.777	.787	.797	.807	.817	.827	.837	.847	.857	.867	.877	.887	.897	.907	.917	.927	.937	.947	.957	.967	.977	.987	.997																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																															
	Upper stage	.775	.597	.418	-1.081	.723	.052	-.006	-.012	-.018	-.024	-.030	-.036	-.042	-.048	-.054	-.060	-.066	-.072	-.078	-.084	-.090	-.096	-.102	-.108	-.114	-.120	-.126	-.132	-.138	-.144	-.150	-.156	-.162	-.168	-.174	-.180	-.186	-.192	-.198	-.204	-.210	-.216	-.222	-.228	-.234	-.240	-.246	-.252	-.258	-.264	-.270	-.276	-.282	-.288	-.294	-.300	-.306	-.312	-.318	-.324	-.330	-.336	-.342	-.348	-.354	-.360	-.366	-.372	-.378	-.384	-.390	-.396	-.402	-.408	-.414	-.420	-.426	-.432	-.438	-.444	-.450	-.456	-.462	-.468	-.474	-.480	-.486	-.492	-.498	-.504	-.510	-.516	-.522	-.528	-.534	-.540	-.546	-.552	-.558	-.564	-.570	-.576	-.582	-.588	-.594	-.600	-.606	-.612	-.618	-.624	-.630	-.636	-.642	-.648	-.654	-.660	-.666	-.672	-.678	-.684	-.690	-.696	-.702	-.708	-.714	-.720	-.726	-.732	-.738	-.744	-.750	-.756	-.762	-.768	-.774	-.780	-.786	-.792	-.798	-.804	-.810	-.816	-.822	-.828	-.834	-.840	-.846	-.852	-.858	-.864	-.870	-.876	-.882	-.888	-.894	-.900	-.906	-.912	-.918	-.924	-.930	-.936	-.942	-.948	-.954	-.960	-.966	-.972	-.978	-.984	-.990	-.996	-.002	-.008	-.014	-.020	-.026	-.032	-.038	-.044	-.050	-.056	-.062	-.068	-.074	-.080	-.086	-.092	-.098	-.104	-.110	-.116	-.122	-.128	-.134	-.140	-.146	-.152	-.158	-.164	-.170	-.176	-.182	-.188	-.194	-.200	-.206	-.212	-.218	-.224	-.230	-.236	-.242	-.248	-.254	-.260	-.266	-.272	-.278	-.284	-.290	-.296	-.302	-.308	-.314	-.320	-.326	-.332	-.338	-.344	-.350	-.356	-.362	-.368	-.374	-.380	-.386	-.392	-.398	-.404	-.410	-.416	-.422	-.428	-.434	-.440	-.446	-.452	-.458	-.464	-.470	-.476	-.482	-.488	-.494	-.500	-.506	-.512	-.518	-.524	-.530	-.536	-.542	-.548	-.554	-.560	-.566	-.572	-.578	-.584	-.590	-.596	-.602	-.608	-.614	-.620	-.626	-.632	-.638	-.644	-.650	-.656	-.662	-.668	-.674	-.680	-.686	-.692	-.698	-.704	-.710	-.716	-.722	-.728	-.734	-.740	-.746	-.752	-.758	-.764	-.770	-.776	-.782	-.788	-.794	-.800	-.806	-.812	-.818	-.824	-.830	-.836	-.842	-.848	-.854	-.860	-.866	-.872	-.878	-.884	-.890	-.896	-.902	-.908	-.914	-.920	-.926	-.932	-.938	-.944	-.950	-.956	-.962	-.968	-.974	-.980	-.986	-.992	-.998	-.004	-.010	-.016	-.022	-.028	-.034	-.040	-.046	-.052	-.058	-.064	-.070	-.076	-.082	-.088	-.094	-.100	-.106	-.112	-.118	-.124	-.130	-.136	-.142	-.148	-.154	-.160	-.166	-.172	-.178	-.184	-.190	-.196	-.202	-.208	-.214	-.220	-.226	-.232	-.238	-.244	-.250	-.256	-.262	-.268	-.274	-.280	-.286	-.292	-.298	-.304	-.310	-.316	-.322	-.328	-.334	-.340	-.346	-.352	-.358	-.364	-.370	-.376	-.382	-.388	-.394	-.400	-.406	-.412	-.418	-.424	-.430	-.436	-.442	-.448	-.454	-.460	-.466	-.472	-.478	-.484	-.490	-.496	-.502	-.508	-.514	-.520	-.526	-.532	-.538	-.544	-.550	-.556	-.562	-.568	-.574	-.580	-.586	-.592	-.598	-.604	-.610	-.616	-.622	-.628	-.634	-.640	-.646	-.652	-.658	-.664	-.670	-.676	-.682	-.688	-.694	-.700	-.706	-.712	-.718	-.724	-.730	-.736	-.742	-.748	-.754	-.760	-.766	-.772	-.778	-.784	-.790	-.796	-.802	-.808	-.814	-.820	-.826	-.832	-.838	-.844	-.850	-.856	-.862	-.868	-.874	-.880	-.886	-.892	-.898	-.904	-.910	-.916	-.922	-.928	-.934	-.940	-.946	-.952	-.958	-.964	-.970	-.976	-.982	-.988	-.994	-.000	-.006	-.012	-.018	-.024	-.030	-.036	-.042	-.048	-.054	-.060	-.066	-.072	-.078	-.084	-.090	-.096	-.102	-.108	-.114	-.120	-.126	-.132	-.138	-.144	-.150	-.156	-.162	-.168	-.174	-.180	-.186	-.192	-.198	-.204	-.210	-.216	-.222	-.228	-.234	-.240	-.246	-.252	-.258	-.264	-.270	-.276	-.282	-.288	-.294	-.300	-.306	-.312	-.318	-.324	-.330	-.336	-.342	-.348	-.354	-.360	-.366	-.372	-.378	-.384	-.390	-.396	-.402	-.408	-.414	-.420	-.426	-.432	-.438	-.444	-.450	-.456	-.462	-.468	-.474	-.480	-.486	-.492	-.498	-.504	-.510	-.516	-.522	-.528	-.534	-.540	-.546	-.552	-.558	-.564	-.570	-.576	-.582	-.588	-.594	-.600	-.606	-.612	-.618	-.624	-.630	-.636	-.642	-.648	-.654	-.660	-.666	-.672	-.678	-.684	-.690	-.696	-.702	-.708	-.714	-.720	-.726	-.732	-.738	-.744	-.750	-.756	-.762	-.768	-.774	-.780	-.786	-.792	-.798	-.804	-.810	-.816	-.822	-.828	-.834	-.840	-.846	-.852	-.858	-.864	-.870	-.876	-.882	-.888	-.894	-.900	-.906	-.912	-.918	-.924	-.930	-.936	-.942	-.948	-.954	-.960	-.966	-.972	-.978	-.984	-.990	-.996	-.002	-.008	-.014	-.020	-.026	-.032	-.038	-.044	-.050	-.056	-.062	-.068	-.074	-.080	-.086	-.092	-.098	-.104	-.110	-.116	-.122	-.128	-.134	-.140	-.146	-.152	-.158	-.164	-.170	-.176	-.182	-.188	-.194	-.200	-.206	-.212	-.218	-.224	-.230	-.236	-.242	-.248	-.254	-.260	-.266	-.272	-.278	-.284	-.290	-.296	-.302	-.308	-.314	-.320	-.326	-.332	-.338	-.344	-.350	-.356	-.362	-.368	-.374	-.380	-.386	-.392	-.398	-.404	-.410	-.416	-.422	-.428	-.434	-.440	-.446	-.452	-.458	-.464	-.470	-.476	-.482	-.488	-.494	-.500	-.506	-.512	-.518	-.524	-.530	-.536	-.542	-.548	-.554	-.560	-.566	-.572	-.578	-.584	-.590	-.596	-.602	-.608	-.614	-.620	-.626	-.632	-.638	-.644	-.650	-.656	-.662	-.668	-.674	-.680	-.686	-.692	-.698	-.704	-.710	-.716	-.722	-.728	-.734	-.740	-.746	-.752	-.758	-.764	-.770	-.776	-.782	-.788	-.794	-.800	-.806	-.812	-.818	-.824	-.830	-.836	-.842	-.848	-.854	-.860	-.866	-.872	-.878	-.884	-.890	-.896	-.902	-.908	-.914	-.920	-.926	-.932	-.938	-.944	-.950	-.956	-.962	-.968	-.974	-.980	-.986	-.992	-.998	-.004	-.010	-.016	-.022	-.028	-.034	-.040	-.046	-.052	-.058	-.064	-.070	-.076	-.082	-.088	-.094	-.100	-.106	-.112	-.118	-.124	-.130	-.136	-.142	-.148	-.154	-.160	-.166	-.172	-.178	-.184	-.190	-.196	-.202	-.208	-.214	-.220	-.226	-.232	-.238	-.244	-.250	-.256	-.262	-.268	-.274	-.280	-.286	-.292	-.298	-.304	-.310	-.316	-.322	-.328	-.334	-.340	-.346	-.352	-.358	-.364	-.370	-.376	-.382	-.388	-.394	-.400	-.406	-.412	-.418	-.424	-.430	-.436	-.442	-.448	-.454	-.460	-.466	-.472	-.478	-.484	-.490	-.496	-.502	-.508	-.514	-.520	-.526	-.532	-.538	-.544	-.550	-.556	-.562	-.568	-.574	-.580	-.586	-.592	-.598	-.604	-.610	-.616	-.622	-.628	-.634	-.640	-.646	-.652	-.658	-.664	-.670	-.676	-.682	-.688	-.694	-.700	-.706	-.712	-.718	-.724	-.730	-.736	-.742	-.748	-.754	-.760	-.766	-.772	-.778	-.784	-.790	-.796	-.802	-.808	-.814	-.820	-.826	-.832	-.838	-.844	-.850	-.856	-.862	-.868	-.874	-.880	-.886	-.892	-.898	-.904	-.910	-.916	-.922	-.928	-.934	-.940	-.946	-.952	-.958	-.964	-.970	-.976	-.982	-.988	-.994	-.000	-.006	-.012	-.018	-.024	-.030	-.036	-.042	-.048	-.054	-.060	-.066	-.072	-.078	-.084	-.090	-.096	-.102	-.108	-.114	-.120	-.126	-.132	-.138	-.144	-.150	-.156	-.162	-.168	-.174	-.180	-.186	-.192	-.198	-.204	-.210	-.216	-.222	-.228	-.234	-.240	-.246	-.252	-.258	-.264	-.270	-.276	-.282	-.288	-.294	-.300	-.306	-.312	-.318	-.324	-.330	-.336	-.342	-.348	-.354	-.360	-.366	-.372	-.378	-.384	-.390	-.396	-.402	-.408	-.414	-.420	-.426	-.432	-.438	-.444	-.450	-.456	-.462	-.468	-.474	-.480	-.486	-.492	-.498	-.504	-.510	-.516	-.522	-.528	-.534	-.540	-.546	-.552	-.558	-.564	-.570	-.576	-.582	-.588	-.594	-.600	-.606	-.612	-.618	-.624	-.630	-.636	-.642	-.648	-.654	-.660	-.666	-.672	-.678	-.684	-.690	-.696	-.702	-.708	-.714	-.720	-.726	-.732

TABLE 12.- PRESSURE COEFFICIENTS FOR CONFIGURATION 3A - Continued

(c) $M = 0.80$; $\alpha = -10^\circ$ to 10° - Concluded

NC 80

		C_p for $\gamma = -60^\circ$							C_p for $\gamma = 60^\circ$						
		$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$	$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$
Main stage	x/l	.653	.655	.628	.608	.561	.501	.403	.657	.650	.623	.608	.587	.561	.496
	Noise	.471	.503	.479	.452	.416	.364	.273	.461	.489	.468	.408	.377	.357	.268
Upper stage	x/l	.322	.309	.293	.273	.238	.193	.113	.481	.489	.489	.477	.468	.448	.387
	Noise	.811	.834	.813	.786	.732	.640	.572	.489	.489	.489	.477	.468	.448	.387
Transition flare	x/l	.109	.105	.102	.101	.099	.098	.097	.509	.529	.529	.529	.529	.529	.428
	Noise	.109	.105	.102	.101	.099	.098	.097	.509	.529	.529	.529	.529	.529	.428
Main stage	x/l	.090	.085	.082	.081	.080	.079	.078	.549	.549	.549	.549	.549	.549	.496
	Noise	.090	.085	.082	.081	.080	.079	.078	.549	.549	.549	.549	.549	.549	.496
Transition flare	x/l	.073	.071	.070	.069	.068	.067	.066	.554	.554	.554	.554	.554	.554	.501
	Noise	.073	.071	.070	.069	.068	.067	.066	.554	.554	.554	.554	.554	.554	.501
Main stage	x/l	.054	.052	.051	.050	.049	.048	.047	.568	.568	.568	.568	.568	.568	.517
	Noise	.054	.052	.051	.050	.049	.048	.047	.568	.568	.568	.568	.568	.568	.517
Transition flare	x/l	.043	.042	.041	.040	.039	.038	.037	.587	.587	.587	.587	.587	.587	.536
	Noise	.043	.042	.041	.040	.039	.038	.037	.587	.587	.587	.587	.587	.587	.536
Main stage	x/l	.033	.032	.031	.030	.029	.028	.027	.607	.607	.607	.607	.607	.607	.556
	Noise	.033	.032	.031	.030	.029	.028	.027	.607	.607	.607	.607	.607	.607	.556
Transition flare	x/l	.023	.022	.021	.020	.019	.018	.017	.627	.627	.627	.627	.627	.627	.576
	Noise	.023	.022	.021	.020	.019	.018	.017	.627	.627	.627	.627	.627	.627	.576
Main stage	x/l	.013	.012	.011	.010	.009	.008	.007	.647	.647	.647	.647	.647	.647	.596
	Noise	.013	.012	.011	.010	.009	.008	.007	.647	.647	.647	.647	.647	.647	.596
Transition flare	x/l	.003	.002	.001	.000	.000	.000	.000	.667	.667	.667	.667	.667	.667	.616
	Noise	.003	.002	.001	.000	.000	.000	.000	.667	.667	.667	.667	.667	.667	.616

TABLE 12.- PRESSURE COEFFICIENTS FOR CONFIGURATION 324 - Continued

(a) $M = 1.00$; $\alpha = -10^\circ$ to 10°

		C_p for $\beta = 0^\circ$							C_p for $\beta = -30^\circ$						
		$\alpha = 0^\circ$							$\alpha = 0^\circ$						
		$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$	$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$
Main stage	x/l	.945	.869	.805	.742	.677	.610	.515	.904	.845	.794	.739	.677	.616	.524
		.812	.730	.669	.609	.544	.486	.397	.753	.694	.646	.594	.537	.483	.398
Transition	x/l	.812	.730	.669	.609	.544	.486	.397	.753	.694	.646	.594	.537	.483	.398
		.796	.718	.660	.602	.537	.479	.390	.602	.544	.498	.449	.396	.350	.273
Flare	x/l	.796	.718	.660	.602	.537	.479	.390	.602	.544	.498	.449	.396	.350	.273
		.611	.538	.483	.428	.372	.317	.262	.484	.428	.372	.317	.262	.207	.152
Nose	x/l	.611	.538	.483	.428	.372	.317	.262	.484	.428	.372	.317	.262	.207	.152
		.509	.436	.381	.326	.271	.216	.161	.509	.436	.381	.326	.271	.216	.161
Main stage	x/l	.509	.436	.381	.326	.271	.216	.161	.509	.436	.381	.326	.271	.216	.161
		.529	.456	.401	.346	.291	.236	.181	.529	.456	.401	.346	.291	.236	.181
Transition	x/l	.529	.456	.401	.346	.291	.236	.181	.529	.456	.401	.346	.291	.236	.181
		.549	.476	.421	.366	.311	.256	.201	.549	.476	.421	.366	.311	.256	.201
Flare	x/l	.549	.476	.421	.366	.311	.256	.201	.549	.476	.421	.366	.311	.256	.201
		.554	.481	.426	.371	.316	.261	.206	.554	.481	.426	.371	.316	.261	.206
Nose	x/l	.554	.481	.426	.371	.316	.261	.206	.554	.481	.426	.371	.316	.261	.206
		.568	.495	.440	.385	.330	.275	.220	.568	.495	.440	.385	.330	.275	.220
Main stage	x/l	.568	.495	.440	.385	.330	.275	.220	.568	.495	.440	.385	.330	.275	.220
		.577	.504	.449	.394	.339	.284	.229	.577	.504	.449	.394	.339	.284	.229
Transition	x/l	.577	.504	.449	.394	.339	.284	.229	.577	.504	.449	.394	.339	.284	.229
		.587	.514	.459	.404	.349	.294	.239	.587	.514	.459	.404	.349	.294	.239
Flare	x/l	.587	.514	.459	.404	.349	.294	.239	.587	.514	.459	.404	.349	.294	.239
		.607	.534	.479	.424	.369	.314	.259	.607	.534	.479	.424	.369	.314	.259
Nose	x/l	.607	.534	.479	.424	.369	.314	.259	.607	.534	.479	.424	.369	.314	.259
		.617	.544	.489	.434	.379	.324	.269	.617	.544	.489	.434	.379	.324	.269
Main stage	x/l	.617	.544	.489	.434	.379	.324	.269	.617	.544	.489	.434	.379	.324	.269
		.627	.554	.500	.445	.390	.335	.280	.627	.554	.500	.445	.390	.335	.280
Transition	x/l	.627	.554	.500	.445	.390	.335	.280	.627	.554	.500	.445	.390	.335	.280
		.637	.567	.513	.458	.403	.348	.293	.637	.567	.513	.458	.403	.348	.293
Flare	x/l	.637	.567	.513	.458	.403	.348	.293	.637	.567	.513	.458	.403	.348	.293
		.657	.587	.533	.478	.423	.368	.313	.657	.587	.533	.478	.423	.368	.313
Nose	x/l	.657	.587	.533	.478	.423	.368	.313	.657	.587	.533	.478	.423	.368	.313
		.677	.607	.553	.498	.443	.388	.333	.677	.607	.553	.498	.443	.388	.333
Main stage	x/l	.677	.607	.553	.498	.443	.388	.333	.677	.607	.553	.498	.443	.388	.333
		.697	.627	.573	.518	.463	.408	.353	.697	.627	.573	.518	.463	.408	.353
Transition	x/l	.697	.627	.573	.518	.463	.408	.353	.697	.627	.573	.518	.463	.408	.353
		.717	.647	.593	.538	.483	.428	.373	.717	.647	.593	.538	.483	.428	.373
Flare	x/l	.717	.647	.593	.538	.483	.428	.373	.717	.647	.593	.538	.483	.428	.373
		.737	.667	.613	.558	.503	.448	.393	.737	.667	.613	.558	.503	.448	.393
Nose	x/l	.737	.667	.613	.558	.503	.448	.393	.737	.667	.613	.558	.503	.448	.393
		.757	.687	.633	.578	.523	.468	.413	.757	.687	.633	.578	.523	.468	.413
Main stage	x/l	.757	.687	.633	.578	.523	.468	.413	.757	.687	.633	.578	.523	.468	.413
		.777	.707	.653	.598	.543	.488	.433	.777	.707	.653	.598	.543	.488	.433
Transition	x/l	.777	.707	.653	.598	.543	.488	.433	.777	.707	.653	.598	.543	.488	.433
		.797	.727	.673	.618	.563	.508	.453	.797	.727	.673	.618	.563	.508	.453
Flare	x/l	.797	.727	.673	.618	.563	.508	.453	.797	.727	.673	.618	.563	.508	.453
		.817	.747	.693	.638	.583	.528	.473	.817	.747	.693	.638	.583	.528	.473
Nose	x/l	.817	.747	.693	.638	.583	.528	.473	.817	.747	.693	.638	.583	.528	.473
		.837	.767	.713	.658	.603	.548	.493	.837	.767	.713	.658	.603	.548	.493
Main stage	x/l	.837	.767	.713	.658	.603	.548	.493	.837	.767	.713	.658	.603	.548	.493
		.857	.787	.733	.678	.623	.568	.513	.857	.787	.733	.678	.623	.568	.513
Transition	x/l	.857	.787	.733	.678	.623	.568	.513	.857	.787	.733	.678	.623	.568	.513
		.877	.807	.753	.698	.643	.588	.533	.877	.807	.753	.698	.643	.588	.533
Flare	x/l	.877	.807	.753	.698	.643	.588	.533	.877	.807	.753	.698	.643	.588	.533
		.897	.827	.773	.718	.663	.608	.553	.897	.827	.773	.718	.663	.608	.553
Nose	x/l	.897	.827	.773	.718	.663	.608	.553	.897	.827	.773	.718	.663	.608	.553

MC | 60

TABLE 12.- PRESSURE COEFFICIENTS FOR CONFIGURATION 324 - Continued

(a) $M = 1.00$; $\alpha = -10^\circ$ to 10° - Concluded

NO 100

		C_p for $\beta = -30^\circ$							
		$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$	
Nozzle	x/l	.461	.658	.715	.737	.739	.727	.705	.639
		.481	.398	.437	.451	.452	.441	.427	.379
Upper stage	x/l	.489	-.629	-.693	-.621	-.523	-.825	-.899	-.918
		.494	-.540	-.496	-.418	-.420	-.370	-.350	-.365
Upper stage	x/l	.499	-.504	-.474	-.409	-.381	-.398	-.350	-.365
		.509	-.403	-.412	-.389	-.381	-.425	-.414	-.368
Upper stage	x/l	.519	-.153	-.269	-.282	-.314	-.305	-.328	-.368
		.529	.091	-.034	-.163	-.229	-.176	-.175	-.231
Upper stage	x/l	.539	.377	.195	-.044	-.146	-.109	-.117	-.139
		.549	.375	.414	.111	-.040	-.045	-.093	-.106
Transition Flare	x/l	.554	.665	.609	.353	.105	.012	.043	.238
		.568	-.745	-.702	-.505	-.348	-.390	-.889	-1.051
Main stage	x/l	.567	-.519	-.516	-.401	-.311	-.326	-.544	-.853
		.597	-.382	-.388	-.328	-.285	-.283	-.416	-.713
Main stage	x/l	.607	-.333	-.299	-.258	-.220	-.241	-.258	-.493
		.617	-.315	-.235	-.209	-.186	-.207	-.215	-.277
Main stage	x/l	.627	-.315	-.192	-.175	-.159	-.183	-.188	-.200
		.637	-.275	-.156	-.145	-.134	-.158	-.166	-.191
Main stage	x/l	.657	-.195	-.134	-.113	-.111	-.124	-.146	-.190
		.677	-.167	-.113	-.096	-.093	-.106	-.126	-.165
Main stage	x/l	.697	-.139	-.093	-.078	-.075	-.087	-.107	-.140
		.737	-.133	-.084	-.068	-.061	-.067	-.083	-.113
Main stage	x/l	.777	-.113	-.064	-.046	-.042	-.037	-.064	-.094
		.785	-.112	-.061	-.035	-.036	-.024	-.061	-.088
Main stage	x/l	.817	-.087	-.043	-.013	-.027	-.006	-.050	-.069
		.857	-.071	.006	.017	.029	.015	-.024	-.036
Main stage	x/l	.877	-.024	.014	.024	.029	.019	.003	-.010
		.897	-.016	.013	.025	.027	.017	.013	-.003
Main stage	x/l	.917	-.019	.006	.019	.021	.010	.013	-.003
		.937	-.019	.002	.012	.009	-.003	.001	-.002
Main stage	x/l	.997	-.095	-.087	-.088	-.106	-.122	-.127	-.148

TABLE 12.- PRESSURE COEFFICIENTS FOR CONFIGURATION 304 - Continued

(e) $M = 1.20$; $\alpha = -10^\circ$ to 10°

		C_p for -						C_p for -							
		$\beta = 0^\circ$						$\beta = -30^\circ$							
x/t		$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$	$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$
		.461	Nose	1.068	.992	.929	.872	.803	.740	.646	1.029	.971	.921	.869	.811
-.950	-.869			-.813	-.756	-.696	-.632	-.543	-.471	-.896	-.841	-.795	-.746	-.693	-.638
-.481	Upper stage	-.481	-.489	-.499	-.510	-.521	-.516	-.477	-.573	-.594	-.610	-.625	-.631	-.580	-.448
-.348		-.442	-.498	-.547	-.571	-.571	-.549	-.494	-.524	-.575	-.610	-.639	-.652	-.632	-.516
-.509	Upper stage	-.142	-.268	-.344	-.403	-.430	-.393	-.349	-.386	-.472	-.528	-.571	-.589	-.522	-.227
-.519		-.052	-.143	-.192	-.245	-.272	-.270	-.240	-.219	-.255	-.311	-.343	-.362	-.322	-.248
-.529	Upper stage	-.236	-.315	-.345	-.332	-.329	-.240	-.164	-.052	-.124	-.029	-.012	-.067	-.148	-.235
-.539		-.583	-.448	-.332	-.110	-.034	-.053	-.164	-.233	-.299	-.201	-.061	-.036	-.148	-.175
-.549	Upper stage	-.654	-.516	-.418	-.292	-.145	-.102	-.020	-.629	-.483	-.372	-.273	-.140	-.034	-.056
-.554		-.093	-.075	-.070	-.073	-.063	-.068	-.073	-.554	-.778	-.642	-.365	-.183	-.084	-.129
-.558	Transition	-.959	-.838	-.877	-.717	-.175	-.089	-.036	-.956	-.882	-.743	-.546	-.137	-.063	-.041
-.568		-.614	-.607	-.604	-.609	-.588	-.455	-.539	-.568	-.615	-.577	-.555	-.509	-.558	-.653
-.577	Transition	-.361	-.398	-.425	-.438	-.235	-.181	-.210	-.378	-.396	-.385	-.384	-.221	-.275	-.284
-.597		-.177	-.255	-.295	-.316	-.194	-.189	-.213	-.587	-.212	-.268	-.295	-.202	-.224	-.240
-.607	Main stage	-.066	-.138	-.168	-.235	-.183	-.189	-.216	-.097	-.135	-.162	-.151	-.132	-.140	-.154
-.617		-.052	-.113	-.132	-.151	-.167	-.172	-.189	-.607	-.098	-.176	-.159	-.170	-.181	-.191
-.627	Main stage	-.038	-.094	-.111	-.113	-.148	-.148	-.143	-.082	-.124	-.135	-.118	-.148	-.151	-.151
-.637		-.028	-.075	-.084	-.091	-.124	-.118	-.099	-.627	-.074	-.111	-.094	-.129	-.129	-.116
-.657	Main stage	-.038	-.076	-.070	-.069	-.069	-.091	-.064	-.063	-.092	-.084	-.075	-.102	-.096	-.088
-.677		-.044	-.036	-.042	-.046	-.069	-.057	-.037	-.657	-.059	-.056	-.051	-.068	-.067	-.067
-.697	Main stage	-.031	-.034	-.037	-.031	-.033	-.024	-.024	-.070	-.059	-.038	-.037	-.049	-.042	-.053
-.737		-.015	-.024	-.026	-.035	-.035	-.029	-.022	-.697	-.061	-.046	-.040	-.037	-.040	-.038
-.777	Main stage	-.018	-.015	-.030	-.022	-.029	-.029	-.013	-.044	-.037	-.030	-.033	-.034	-.040	-.034
-.785		-.028	-.006	-.017	-.012	-.026	-.026	-.023	-.777	-.007	-.025	-.014	-.026	-.029	-.048
-.817	Main stage	-.021	-.003	-.004	-.020	-.009	-.010	-.008	-.002	-.016	-.016	-.016	-.014	-.029	-.056
-.857		-.021	-.007	-.009	-.004	-.012	-.008	-.018	-.817	-.004	-.007	-.008	-.014	-.015	-.050
-.877	Main stage	-.032	-.004	-.004	-.003	-.004	-.008	-.019	-.857	-.008	-.008	-.010	-.009	-.022	-.054
-.897		-.013	-.002	-.001	-.002	-.007	-.009	-.018	-.897	-.012	-.012	-.008	-.008	-.019	-.054
-.917	Main stage	-.004	-.004	-.004	-.002	-.007	-.009	-.018	-.917	-.008	-.004	-.004	-.004	-.019	-.043
-.957		-.012	-.004	-.004	-.005	-.009	-.017	-.022	-.957	-.012	-.016	-.016	-.016	-.017	-.036
-.997	Main stage	-.000	-.022	-.034	-.047	-.068	-.082	-.090	-.000	-.022	-.034	-.047	-.068	-.090	-.080
-.997		-.000	-.022	-.034	-.047	-.068	-.082	-.090	-.997	-.022	-.034	-.047	-.068	-.090	-.080

TABLE 12.- PRESSURE COEFFICIENTS FOR CONFIGURATION 304 - Concluded

(e) $M = 1.20$; $\alpha = -10^\circ$ to 10° - Concluded

		C_p for -						C_p for -							
		$\beta = -60^\circ$						$\beta = -90^\circ$							
x/l	Stage	$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$	$\alpha = -10^\circ$	$\alpha = -6^\circ$	$\alpha = -3^\circ$	$\alpha = 0^\circ$	$\alpha = 3^\circ$	$\alpha = 6^\circ$	$\alpha = 10^\circ$
		.461	Main stage	.910	.516	.695	.869	.830	.777	.682	.779	.840	.867	.859	.835
.471	.802	.795		.777	.751	.714	.669	.580	.560	.606	.622	.617	.596	.546	
.481	.671	.663		.645	.622	.590	.554	.477	.481	.606	.621	.622	.617	.596	
.489	.530	.532		.537	.550	.561	.555	.448	.489	.606	.602	.598	.598	.596	
.494	.473	.477		.499	.533	.609	.695	.219							
.499	.410	.477		.501	.552	.652	.822	.224							
.509	.182	.236		.211	.126	.052	.022	.238	.509	.261	.246	.132	.189	.210	
.519	.112	.113		.062	.026	.064	.151	.213	.529	.033	.017	.056	.061	.031	
.529	.157	.190		.087	.053	.026	.067	.140	.549	.236	.193	.164	.218	.243	
.539	.382	.285		.172	.107	.066	.010	.015							
.549	.442	.337	.264	.170	.112	.069	.078								
.554	.750	.639	.465	.234	.319	.327	.399								
.568	Transition Flare	.652	.615	.555	.517	.569	.604	.691	.668	.621	.547	.569	.617	.682	
.577		.454	.423	.366	.254	.324	.452	.593							
.587		.302	.306	.287	.216	.243	.360	.517	.587	.410	.263	.180	.308	.441	
.597		.226	.241	.230	.189	.189	.265	.389							
.607		.185	.195	.178	.161	.162	.183	.229	.607	.296	.227	.161	.173	.316	
.617		.174	.168	.138	.140	.135	.145	.170							
.627		.171	.143	.111	.121	.118	.126	.140	.627	.261	.124	.132	.107	.276	
.637		.152	.105	.084	.091	.094	.096	.126							
.657		.174	.067	.056	.053	.058	.079	.119	.657	.161	.080	.063	.057	.154	
.697		.142	.067	.051	.047	.055	.072	.108							
.737	.110	.064	.044	.041	.052	.065	.097								
.777	.110	.058	.034	.034	.036	.063	.071	.697	.162	.091	.044	.062	.088		
.785	.064	.047	.032	.017	.030	.046	.058	.737	.135	.071	.042	.038	.074		
.817	.058	.044	.023	.010	.021	.034	.057	.777	.096	.055	.030	.029	.060		
.857	.066	.025	.012	.017	.018	.035	.048	.785	.106	.058	.030	.028	.057		
.877	.055	.020	.014	.011	.021	.033	.045	.817	.086	.031	.015	.019	.044		
.897	.066	.033	.009	.004	.008	.023	.045	.857	.087	.032	.018	.020	.053		
.917	.070	.029	.011	.001	.004	.019	.030	.897	.091	.040	.008	.008	.028		
.957	.069	.032	.017	.008	.011	.023	.027								
.997	.060	.047	.015	.005	.019	.021	.029								

NO. 120

TABLE 13.- PRESSURE COEFFICIENTS FOR CONFIGURATION 133

(a) $M = 0.40$ to 1.20 ; $\alpha = 0^\circ$; $\phi = 0^\circ$

$x/2$	C_p for -									
	$M = 0.40$	$M = 0.60$	$M = 0.70$	$M = 0.75$	$M = 0.80$	$M = 0.85$	$M = 0.90$	$M = 0.95$	$M = 1.00$	$M = 1.20$
Nose	.089	.580	.709	.763	.820	.844	.785	.863	.912	1.002
Upper stage Transi- tion plate	.209	.234	.251	.259	.272	.273	.304	.328	.377	.307
	.440	.201	.219	.227	.242	.242	.271	.297	.350	.315
	.450	.162	.184	.186	.197	.204	.235	.259	.318	.307
	.470	.061	.086	.093	.100	.113	.152	.184	.246	.304
	.480	-.043	-.022	-.009	.010	.033	.080	.125	.189	.291
	.485	-.180	-.176	-.158	-.138	-.097	-.055	.004	.062	.135
	.491	-.750	-.888	-1.078	-1.205	-1.116	-.965	-.828	-.595	-.284
	.496	-.202	-.229	-.251	-.311	-.399	-.462	-.485	-.671	-.366
	.501	-.089	-.097	-.095	-.110	-.179	-.268	-.261	-.199	-.325
	.511	.024	.029	.043	.050	.053	-.016	-.053	-.027	-.251
.521	.126	.144	.167	.175	.184	.171	.144	.060	.114	
.531	.318	.340	.360	.360	.358	.325	.297	.187	.161	
.540	.001	.012	.024	.024	.025	.016	.031	.028	.040	
.546	.079	.091	.105	.135	.159	.189	.245	.292	.344	
.552	-.010	.000	.019	.036	.063	.097	.155	.216	.292	
.562	.247	-.258	-.238	-.210	+.160	-.103	-.036	.028	.116	
.568	-.767	-.953	-1.078	-1.207	-1.281	-1.128	-.981	-.845	-.717	
.577	-.213	-.224	-.224	-.252	-.256	-.265	-.284	-.312	-.312	
.587	-.134	-.132	-.123	-.131	-.117	-.131	-.150	-.166	-.246	
.597	-.100	-.097	-.086	-.093	-.086	-.059	-.097	-.138	-.207	
.607	-.989	-.074	-.058	-.068	-.067	-.056	-.009	-.371	-.172	
.617	-.066	-.063	-.049	-.055	-.055	-.056	-.003	-.290	-.144	
.627	-.066	-.051	-.040	-.047	-.044	-.052	-.006	-.132	-.122	
.637	-.055	-.040	-.031	-.034	-.032	-.045	-.009	-.166	-.092	
.647	-.029	-.027	-.019	-.023	-.021	-.035	-.012	-.131	-.073	
.657	-.029	-.023	-.016	-.018	-.019	-.032	-.016	-.024	-.048	
.677	-.029	-.023	-.016	-.018	-.019	-.028	-.015	-.015	-.098	
.697	-.017	-.017	-.008	-.012	-.010	-.027	-.015	-.003	-.040	
.717	-.017	-.011	-.003	-.006	-.006	-.021	-.010	-.007	-.025	
.737	-.017	-.009	-.002	-.002	-.001	-.017	-.004	-.001	-.015	
.785	-.013	-.009	-.001	-.001	-.001	-.017	-.006	-.001	-.022	
.817	-.012	-.008	-.001	-.001	-.002	-.017	-.010	-.006	-.042	
.857	-.014	-.010	-.003	-.004	-.005	-.021	-.010	-.012	-.035	
.877	-.014	-.010	-.003	-.004	-.004	-.021	-.009	-.012	-.001	
.897	-.017	-.014	-.006	-.007	-.008	-.024	-.012	-.016	-.005	

TABLE 13.-- PRESSURE COEFFICIENTS FOR CONFIGURATION 133 - Continued

(b) $M = 0.40$ to 1.20 ; $\alpha = 0^\circ$; $\phi = -30^\circ$

x/l	C_p for --									
	$M = 0.40$	$M = 0.60$	$M = 0.70$	$M = 0.75$	$M = 0.80$	$M = 0.85$	$M = 0.90$	$M = 0.95$	$M = 1.00$	$M = 1.20$
Nose	.209	.223	.246	.255	.265	.267	.298	.322	.368	.364
	.166	.189	.210	.223	.231	.235	.268	.290	.344	.310
	.133	.156	.179	.186	.193	.200	.235	.256	.312	.310
	.045	.056	.077	.085	.100	.109	.149	.181	.243	.304
	-.043	-.045	-.026	-.013	.006	.033	.080	.122	.189	.304
	-.178	-.170	-.158	-.138	-.101	-.095	.004	.059	.135	.288
	-.750	-.882	-1.023	-1.110	-1.063	-.944	-.828	-.713	-.598	-.290
	-.213	-.241	-.270	-.344	-.426	-.434	-.417	-.397	-.434	-.369
	-.078	-.086	-.095	-.122	-.225	-.326	-.308	-.268	-.209	-.342
	.024	.029	.047	.054	.053	-.041	-.074	-.110	-.073	-.240
	.126	.150	.171	.180	.188	.164	.127	.045	.050	.122
	.318	.334	.350	.351	.351	.301	.273	.171	.143	.240
	.180	.204	.236	.247	.265	.285	.329	.378	.444	.222
	.035	.046	.074	.086	.109	.140	.195	.267	.359	.439
	-.010	.000	.019	.036	.063	.097	.152	.206	.268	.406
	-.259	-.270	-.251	-.219	-.171	-.121	-.053	.016	.092	.298
	-.643	-.769	-1.074	-1.325	-1.277	-1.118	-.964	-.822	-.690	-.386
	-.134	-.224	-.219	-.135	-.121	-.117	-.767	-.622	-.465	-.314
	-.213	-.237	-.227	-.135	-.121	-.117	-.533	-.510	-.381	-.246
	-.100	-.097	-.077	-.084	-.082	-.059	-.070	-.332	-.258	-.152
	-.078	-.074	-.058	-.068	-.067	-.056	-.009	-.368	-.292	-.169
	-.066	-.063	-.049	-.055	-.052	-.052	-.006	-.293	-.252	-.144
	-.066	-.051	-.040	-.047	-.044	-.052	-.009	-.132	-.209	-.125
	-.055	-.040	-.031	-.034	-.036	-.045	-.009	-.029	-.172	-.098
	-.053	-.029	-.023	-.025	-.024	-.037	-.016	-.020	-.134	-.066
	-.021	-.017	-.010	-.014	-.012	-.026	-.009	.030	-.099	-.040
	-.021	-.019	-.011	-.015	-.013	-.028	-.015	.014	-.085	-.042
	-.017	-.015	-.006	-.009	-.008	-.017	-.012	-.001	-.068	-.037
	-.013	-.009	-.003	-.006	-.004	-.016	-.005	-.002	-.051	-.020
	-.012	-.008	-.002	-.002	-.001	-.016	-.004	-.001	-.047	-.009
	-.012	-.008	-.000	-.001	-.002	-.017	-.006	-.006	-.042	-.021
	-.015	-.011	-.004	-.005	-.006	-.021	-.011	-.013	-.039	-.013
	-.018	-.012	-.004	-.006	-.006	-.022	-.012	-.014	-.010	-.004
	-.018	-.014	-.006	-.007	-.008	-.024	-.013	-.017	-.023	-.002
	-.018	-.014	-.006	-.008	-.008	-.025	-.013	-.017	-.034	-.007
	-.030	-.025	-.018	-.019	-.020	-.036	-.013	-.029	-.023	-.017
	-.081	-.080	-.073	-.077	-.077	-.096	-.089	-.104	-.088	-.055

TABLE 13.-- PRESSURE COEFFICIENTS FOR CONFIGURATION 133 - Concluded

(d) $M = 0.40$ to 1.20 ; $\alpha = 0^\circ$; $\phi = -90^\circ$

x/l	C_p for -									
	$M = 0.40$	$M = 0.60$	$M = 0.70$	$M = 0.75$	$M = 0.80$	$M = 0.85$	$M = 0.90$	$M = 0.95$	$M = 1.00$	$M = 1.20$
Nose	.242 .012 .133 .034 .200 -.772	.267 .513 .150 .056 -.193 -.865	.286 .660 .170 .077 -.181 -.992	.296 .719 .178 .089 -.159 -1.089	.310 .782 .190 .104 -.120 -1.017	.315 .877 .193 .113 -.080 -.890	.340 .743 .225 .149 -.016 -.750	.366 .813 .253 .184 .037 -.643	.413 .871 .309 .246 .111 -.525	.405 .251 .172 .120 -.646 -.539 -.021 -.017 -.012 -.013 -.025
Upper stage	.024 .341	.035 .368	.047 .373	.054 .368	.057 .352	-.041 .304	-.101 .249	-.123 .148	-.064 .146	-.254 .243
Transition flare	-.010	.000	.019	.032	.063	.097	.152	.197	.277	.405
Main stage	-.767 -.134 -.078 -.066 -.033 -.025 -.017 -.013 -.011 -.013 -.011 -.015 -.011 -.018 -.015 -.018	-.970 -.137 -.074 -.051 -.029 -.019 -.015 -.005 -.011 -.009 -.001 -.002 -.003 -.014	-1.166 .132 .058 -.040 -.023 -.013 -.005 -.001 -.001 -.002 -.003 -.005	-1.367 -.135 -.068 -.047 -.025 -.015 -.009 -.005 -.006 -.000 -.005 -.007	-1.312 -.121 -.067 -.044 -.024 -.015 -.008 -.005 -.004 -.000 -.005 -.008	-1.150 -.124 -.056 -.052 -.037 -.030 -.023 -.019 -.018 -.015 -.020 -.023	-.998 -.539 -.012 -.012 -.016 -.016 -.011 -.008 -.009 -.003 -.010 -.012	-.851 -.513 -.371 -.126 -.020 -.012 -.000 -.005 -.006 -.004 -.013 -.017	-.726 -.400 -.289 -.203 -.133 -.087 -.060 -.053 -.050 -.038 -.032 -.025	-.350 -.251 -.172 -.120 -.646 -.539 -.021 -.017 -.012 -.013 -.007

TABLE 14.-- PRESSURE COEFFICIENTS FOR CONFIGURATION 143

(a) $M = 0.40$ to 1.20 ; $\alpha = 0^\circ$; $\phi = 0^\circ$

x/l	C_p for --									
	$M = 0.40$	$M = 0.60$	$M = 0.70$	$M = 0.75$	$M = 0.80$	$M = 0.85$	$M = 0.90$	$M = 0.95$	$M = 1.00$	$M = 1.20$
Nose	.440 -.257 .230 .197 .470 .490 .500 .505 .511 .516 .521 .531	.393 .243 .215 .176 .087 .000 -.112 -.638 -.113 .046 .050 .314	.561 .264 .237 .193 .104 .015 -.108 -.852 -.118 .061 .318	.634 .269 .237 .201 .107 .018 -.098 -.943 -.136 .056 .299	.705 .278 .248 .207 .121 .035 -.067 -.894 -.184 .021 .256	.765 .290 .259 .224 .140 .063 -.028 -.823 -.201 -.043 .173	.827 .314 .281 .245 .169 .100 .024 -.792 -.182 -.080 .103	.871 .329 .304 .267 .192 .133 .065 -.716 -.148 -.087 .064	.928 .377 .353 .315 .249 .196 .133 .066 -.090 -.037 .085	1.109 .520 .330 .322 .317 .320 .301 .291 .359 .512 .155
Upper stage	.540 .546 .552 .562 .568 .577 .587 .597 .607 .617 .627 .637 .657 .667 .697	.021 .077 -.014 .266 -.960 .220 -.128 -.094 -.065 -.054 .042 .036 .018 .016 -.010 -.008 -.004 .003 .001 -.003 -.002 -.005 -.007	.029 .096 .006 -.245 -1.116 .228 -.127 -.086 .063 -.049 .035 .026 .018 -.013 -.008 -.005 -.001 .005 .005 .002 -.002 -.003 -.003 -.004	.027 .117 .018 -.215 -1.340 .257 -.136 -.090 -.069 -.052 -.044 -.031 -.020 -.015 -.011 -.008 -.002 -.002 .001 .001 -.002 -.001 -.004	.028 .142 .051 -.164 -1.292 .284 -.118 -.087 -.072 .056 .049 .037 -.024 -.020 -.014 -.013 -.007 -.002 -.003 -.003 -.007 -.007 -.010	.032 .192 .096 -.107 -1.122 -.820 -.122 -.043 -.039 -.039 -.035 -.025 -.018 -.016 -.012 -.009 -.004 -.002 -.001 -.004 -.004 -.006	.032 .242 .155 -.032 -.979 -.803 -.660 -.212 -.012 .017 -.225 .011 -.006 -.010 -.010 -.011 -.007 -.000 -.002 -.002 -.006 -.006 -.009	.028 .284 .211 .031 -.857 -.690 -.571 -.491 -.421 -.353 -.225 -.048 .027 .035 .028 .006 -.003 -.002 -.004 -.011 -.002 -.006 -.011 -.015	.039 .344 .283 .114 -.734 -.575 -.467 -.397 -.338 -.283 -.237 -.191 -.147 -.117 -.093 -.075 -.062 -.052 -.048 -.052 -.050 -.050 -.049	.050 .108 .441 .282 -.405 -.337 -.255 -.219 -.181 -.151 -.127 -.097 -.077 -.051 -.040 -.038 -.022 -.014 -.019 -.001 -.002 -.002 -.002
Transition stage	.540 .546 .552 .562 .568 .577 .587 .597 .607 .617 .627 .637 .657 .667 .697	.021 .077 -.014 .266 -.960 .220 -.128 -.094 -.065 -.054 .042 .036 .018 .016 -.010 -.008 -.004 .003 .001 -.003 -.002 -.005 -.007	.029 .096 .006 -.245 -1.116 .228 -.127 -.086 .063 -.049 .035 .026 .018 -.013 -.008 -.005 -.001 .005 .005 .002 -.002 -.003 -.003 -.004	.027 .117 .018 -.215 -1.340 .257 -.136 -.090 -.069 -.052 -.044 -.031 -.020 -.015 -.011 -.008 -.002 -.002 .001 .001 -.002 -.001 -.004	.028 .142 .051 -.164 -1.292 .284 -.118 -.087 -.072 .056 .049 .037 -.024 -.020 -.014 -.013 -.007 -.002 -.003 -.003 -.007 -.007 -.010	.032 .192 .096 -.107 -1.122 -.820 -.122 -.043 -.039 -.039 -.035 -.025 -.018 -.016 -.012 -.009 -.004 -.002 -.001 -.004 -.004 -.006	.032 .242 .155 -.032 -.979 -.803 -.660 -.212 -.012 .017 -.225 .011 -.006 -.010 -.010 -.011 -.007 -.000 -.002 -.002 -.006 -.006 -.009	.028 .284 .211 .031 -.857 -.690 -.571 -.491 -.421 -.353 -.225 -.048 .027 .035 .028 .006 -.003 -.002 -.004 -.011 -.002 -.006 -.011 -.015	.039 .344 .283 .114 -.734 -.575 -.467 -.397 -.338 -.283 -.237 -.191 -.147 -.117 -.093 -.075 -.062 -.052 -.048 -.052 -.050 -.050 -.049	.050 .108 .441 .282 -.405 -.337 -.255 -.219 -.181 -.151 -.127 -.097 -.077 -.051 -.040 -.038 -.022 -.014 -.019 -.001 -.002 -.002 -.002
Main Stage	.440 .430 .460 .470 .490 .500 .505 .511 .516 .521 .531	.393 .243 .215 .176 .087 .000 -.112 -.638 -.113 .046 .050 .314	.561 .264 .237 .193 .104 .015 -.108 -.852 -.118 .061 .318	.634 .269 .237 .201 .107 .018 -.098 -.943 -.136 .056 .299	.705 .278 .248 .207 .121 .035 -.067 -.894 -.184 .021 .256	.765 .290 .259 .224 .140 .063 -.028 -.823 -.201 -.043 .173	.827 .314 .281 .245 .169 .100 .024 -.792 -.182 -.080 .103	.871 .329 .304 .267 .192 .133 .065 -.716 -.148 -.087 .064	.928 .377 .353 .315 .249 .196 .133 .066 -.090 -.037 .085	1.109 .520 .330 .322 .317 .320 .301 .291 .359 .512 .155

TABLE 14.-- PRESSURE COEFFICIENTS FOR CONFIGURATION 143 - Continued

(c) $\gamma = 0.40$ to 1.20 ; $\alpha = 0^\circ$; $\beta = -60^\circ$

x/l	C_p for -									
	M = 0.40	M = 0.60	M = 0.70	M = 0.75	M = 0.80	M = 0.85	M = 0.90	M = 0.95	M = 1.00	M = 1.20
Nose	.219 .186 .153 .066 -.011 -.078 -.626	.231 .196 .165 .076 -.013 -.082 -.736	.255 .224 .193 .104 .010 -.076 -.748	.261 .229 .195 .107 .018 -.077 -.810	.271 .241 .203 .117 .031 -.079 -.783	.287 .255 .217 .133 .060 -.082 -.706	.304 .275 .242 .166 .094 -.089 -.634	.326 .295 .261 .186 .127 -.105 -.579	.374 .344 .315 .246 .190 -.113 -.497	.383 .345 .320 .314 .317 -.128 -.231
Upper stage	-.101 .057 .328	-.117 .061 .325	-.127 .057 .286	-.148 .031 .257	-.176 -.029 .214	-.194 -.075 .152	-.182 -.100 .087	-.154 -.097 .048	-.093 -.044 .073	-.383 -.143 -.133
Trailing edge	.156 .056 -.022 -.259 -.700 -.214 -.135 -.090 -.079 -.056 -.045 -.023 -.015 -.015 -.007 -.003 -.003 -.002 -.005 -.007 -.008 -.008 -.011 -.020 -.020 -.023 -.027 -.027 -.027	.184 .083 -.014 -.277 -.597 -.220 -.134 -.088 -.065 -.054 -.042 -.036 -.020 -.002 -.010 -.006 -.004 -.002 -.004 -.001 -.001 -.003 -.003 -.004 -.009 -.016 -.013 -.016 -.073	.209 .096 .006 -.255 -1.194 -.223 -.131 -.081 -.058 -.044 -.035 -.026 -.019 -.002 -.008 -.003 -.001 -.002 -.004 -.001 -.001 -.003 -.004 -.004 -.017 -.013 -.017 -.070	.228 .117 .023 -.224 -1.411 -.232 -.136 -.090 -.069 -.052 -.044 -.036 -.021 -.003 -.011 -.005 -.002 -.002 -.001 -.001 -.002 -.003 -.004 -.009 -.009 -.017 -.075	.249 .146 .051 -.176 -1.296 -.246 -.122 -.087 -.068 -.056 -.049 -.041 -.025 -.002 -.014 -.010 -.006 -.005 -.003 -.003 -.008 -.008 -.009 -.013 -.021 -.079	.280 .195 .100 -.115 -1.122 -.798 -.097 -.039 -.039 -.035 -.028 -.021 -.004 -.007 -.007 -.002 -.002 -.001 -.001 -.004 -.005 -.006 -.006 -.009 -.019 -.080	.292 .249 .159 -.040 -.972 -.796 -.660 -.188 -.009 -.017 -.014 -.008 -.007 -.006 -.009 -.005 -.004 -.004 -.004 -.004 -.007 -.007 -.009 -.005 -.004 -.012 -.013 -.015 -.021 -.089	.281 .290 .280 .105 -.841 -.681 -.575 -.491 -.417 -.335 -.228 -.052 -.024 -.028 -.028 -.007 -.009 -.007 -.000 -.003 -.003 -.003 -.012 -.013 -.015 -.020 -.027 -.104	.305 .344 .280 .105 -.716 -.562 -.470 -.397 -.283 -.243 -.197 -.148 -.060 -.092 -.073 -.058 -.055 -.046 -.053 -.053 -.048 -.030 -.083	.338 .416 .376 .281 -.380 -.323 -.260 -.217 -.178 -.148 -.129 -.102 -.057 -.010 -.046 -.035 -.008 -.016 -.011 -.001 -.001 -.005 -.013 -.030 -.050

TABLE 14.-- PRESSURE COEFFICIENTS FOR CONFIGURATION 143 - Concluded

(a) $M = 0.40$ to 1.20 ; $\alpha = 0^\circ$; $\phi = -90^\circ$

x/l	C_p for -										
	$M = 0.40$	$M = 0.60$	$M = 0.70$	$M = 0.75$	$M = 0.80$	$M = 0.85$	$M = 0.90$	$M = 0.95$	$M = 1.00$	$M = 1.20$	
Nose	.263 -.257 .153 .066 -.145 -.626	.276 .382 .165 .081 -.139 -.713	.299 .548 .184 .104 -.130 -.775	.502 .618 .192 .107 -.118 -.848	.308 .690 .200 .121 -.090 -.852	.325 .747 .213 .136 -.053 -.756	.347 .818 .238 .166 .001 -.654	.367 .865 .258 .192 .043 -.586	.413 .925 .312 .249 .112 -.494	.312 1.093 .314 .320 .280 -.231	
Upper stage	.339	.342	.318	.295	.253	.163	.093	.054	.079	.149	
Transition	.552	-.014	.006	.018	.051	.100	.155	.211	.280	.378	
Main stage	-.790 -.135 -.079 -.056 -.023 -.015 -.007 -.003 -.003 -.001 -.003 -.008	-.994 -.134 -.065 -.042 -.022 -.012 -.006 -.006 -.002 -.003 -.003 -.005	-1.208 -.151 -.058 -.035 -.019 -.010 -.003 -.000 -.008 -.007 -.002 -.001	-1.432 -.136 -.069 -.044 -.021 -.012 -.005 -.002 -.002 -.003 -.002 -.005	-1.323 -.122 -.068 -.049 -.027 -.017 -.009 -.006 -.007 -.002 -.002 -.007	-1.151 -.104 -.039 -.035 -.022 -.013 -.005 -.003 -.002 -.001 -.004 -.007	-.999 -.667 -.009 -.014 -.009 -.012 -.009 -.005 -.005 -.000 -.007 -.007 -.009	-.867 -.584 -.417 -.225 -.023 -.026 -.008 -.001 -.004 -.001 -.011 -.015	-.740 -.476 -.335 -.237 -.149 -.094 -.072 -.058 -.056 -.044 -.044 -.048	-.410 -.263 -.178 -.127 -.058 -.044 -.039 -.019 -.013 -.011 -.007 -.005	

TABLE 15.- PRESSURE COEFFICIENTS FOR CONFIGURATION 153

(a) $M = 0.40$ to 1.20 ; $\alpha = 0^\circ$; $\phi = 0^\circ$

$x/2$	C_p for -									
	$M = 0.40$	$M = 0.60$	$M = 0.70$	$M = 0.75$	$M = 0.80$	$M = 0.85$	$M = 0.90$	$M = 0.95$	$M = 1.00$	$M = 1.20$
Nose	.555 .471 .481 .491 .511 .521 .525 .532	.260 .255 .233 .199 .144 .110 .094 .088	.446 .273 .237 .211 .153 .122 .109 .104	.532 .277 .249 .220 .164 .135 .115 .111	.601 .287 .265 .231 .175 .141 .130 .126	.658 .306 .278 .250 .195 .167 .153 .153	.720 .320 .294 .265 .215 .186 .176 .176	.778 .346 .321 .296 .247 .222 .216 .216	.833 .397 .370 .344 .299 .278 .269 .275	1.015 .325 .325 .317 .325 .325 .330 .346
Upper stage	.014 -.009 -.076 -.290 -.763 -.234 -.144 -.110 -.087 -.076 -.065 -.053 -.032 -.028 -.024 -.020 -.016 -.012 -.011 -.012 -.012 -.012	.016 -.006 -.069 -.298 -.950 -.241 -.138 -.096 -.069 -.058 -.046 -.035 -.018 -.014 -.008 -.006 -.002 -.004 -.003 -.001 -.001 -.001 -.001	.025 .011 -.053 -.268 -1.214 -.281 -.144 -.094 -.071 -.053 -.043 -.034 -.022 -.017 -.010 -.008 -.002 -.003 -.002 -.002 -.002 -.002	.031 .022 -.036 -.224 -1.471 -.361 -.148 -.090 -.069 -.052 -.044 -.032 -.021 -.017 -.012 -.011 -.005 -.001 -.001 -.001 -.001 -.001 -.001	.030 .041 -.008 -1.174 -.474 -.178 -.077 -.054 -.050 -.043 -.051 -.022 -.018 -.014 -.011 -.005 -.002 -.002 -.001 -.001 -.001 -.001 -.001	.035 .074 .028 -.104 -1.145 -.886 -.291 -.090 -.018 -.014 -.018 -.018 -.014 -.013 -.009 -.007 -.002 -.004 -.004 -.004 -.004 -.004 -.004	.033 .109 .069 -.038 -.996 -.888 -.740 -.402 -.092 -.009 -.031 -.025 -.009 -.003 -.007 -.007 -.007 -.001 -.001 -.001 -.001 -.001 -.001	.033 .156 .125 .033 -.863 -.776 -.655 -.568 -.488 -.411 -.337 -.328 -.126 -.035 -.057 -.050 -.021 -.008 -.008 -.008 -.008 -.008 -.008	.039 .216 .186 .102 -.738 -.662 -.551 -.475 -.401 -.337 -.279 -.224 -.165 -.125 -.096 -.074 -.057 -.048 -.043 -.040 -.040 -.040	.051 .319 .317 .293 -.400 -.351 -.291 -.245 -.209 -.177 -.150 -.114 -.090 -.058 -.040 -.022 -.014 -.019 -.000 -.003 -.003 -.004
Main stage	.577 .587 .597 .607 .617 .627 .637 .657 .677 .697 .737 .777 .785 .817 .857 .877 .897	.016 -.006 -.069 -.298 -.950 -.241 -.138 -.096 -.069 -.058 -.046 -.035 -.018 -.014 -.008 -.006 -.002 -.004 -.003 -.001 -.001 -.001 -.001	.025 .011 -.053 -.268 -1.214 -.281 -.144 -.094 -.071 -.053 -.043 -.034 -.022 -.017 -.010 -.008 -.002 -.003 -.002 -.002 -.002 -.002	.031 .022 -.036 -.224 -1.471 -.361 -.148 -.090 -.069 -.052 -.044 -.032 -.021 -.017 -.012 -.011 -.005 -.001 -.001 -.001 -.001 -.001 -.001	.030 .041 -.008 -1.174 -.474 -.178 -.077 -.054 -.050 -.043 -.051 -.022 -.018 -.014 -.011 -.005 -.002 -.002 -.001 -.001 -.001 -.001 -.001	.035 .074 .028 -.104 -1.145 -.886 -.291 -.090 -.018 -.014 -.018 -.018 -.014 -.013 -.009 -.007 -.002 -.004 -.004 -.004 -.004 -.004 -.004	.033 .109 .069 -.038 -.996 -.888 -.740 -.402 -.092 -.009 -.031 -.025 -.009 -.003 -.007 -.007 -.007 -.001 -.001 -.001 -.001 -.001 -.001	.033 .156 .125 .033 -.863 -.776 -.655 -.568 -.488 -.411 -.337 -.328 -.126 -.035 -.057 -.050 -.021 -.008 -.008 -.008 -.008 -.008 -.008	.039 .216 .186 .102 -.738 -.662 -.551 -.475 -.401 -.337 -.279 -.224 -.165 -.125 -.096 -.074 -.057 -.048 -.043 -.040 -.040 -.040	.051 .319 .317 .293 -.400 -.351 -.291 -.245 -.209 -.177 -.150 -.114 -.090 -.058 -.040 -.022 -.014 -.019 -.000 -.003 -.003 -.004

TABLE 15.- PRESSURE COEFFICIENTS FOR CONFIGURATION 153 - Continued

(c) $M = 0.40$ to 1.20 ; $\alpha = 0^\circ$; $\phi = -60^\circ$

x/l	Cp for -									
	M = 0.40	M = 0.60	M = 0.70	M = 0.75	M = 0.80	M = 0.85	M = 0.90	M = 0.95	M = 1.00	M = 1.20
Nose	.221	.244	.255	.269	.280	.292	.310	.340	.358	.312
	.188	.210	.228	.236	.246	.264	.278	.309	.358	.309
	.166	.183	.197	.208	.220	.237	.251	.284	.335	.309
	.111	.133	.144	.151	.164	.184	.206	.237	.293	.315
	.079	.099	.113	.119	.134	.157	.176	.216	.269	.320
	-.087	-.080	-.079	-.077	-.081	-.078	-.091	-.100	-.110	-.132
	.035	.044	.055	.066	.078	.104	.130	.166	.228	.285
Upper										
Flare	.025	.039	.052	.063	.079	.106	.139	.181	.240	.322
	-.020	-.001	.016	.027	.045	.078	.109	.159	.219	.328
	.076	.075	-.053	-.036	-.012	.025	.066	.125	.186	.319
	.290	-.298	-.268	-.224	-.170	-.104	-.038	.030	.105	.295
	.864	-1.002	-1.269	-1.492	-1.260	-1.152	-.949	-.821	-.695	-.575
	.222	-.229	-.272	-.353	-.474	-.911	-.905	-.792	-.674	-.565
	-.144	-.138	-.144	-.148	-.166	-.283	-.763	-.671	-.567	-.299
	.099	.092	-.098	.090	-.070	.075	-.385	-.571	-.478	-.248
	.087	.069	-.071	.065	-.054	-.014	-.079	-.479	-.395	-.204
	.076	.058	-.057	.052	-.050	.018	.018	-.402	-.331	-.171
	.065	.046	-.048	.044	-.043	-.022	.031	-.328	-.282	-.147
	.053	.035	-.034	.036	-.035	.022	.022	-.142	-.230	-.117
	.032	.020	-.022	.023	-.023	.015	.006	.039	-.163	-.073
	.016	.002	.050	.001	.002	.005	.010	.044	-.062	.015
	.097	-.024	-.010	.011	-.011	-.007	-.006	.051	-.093	-.050
	.757	-.016	-.005	.006	-.007	.004	.008	.022	-.071	.037
	.777	.012	.000	.002	-.003	.000	-.005	.011	-.053	.014
	.785	.012	.000	.002	-.001	.002	-.003	.010	-.048	.008
	.817	.003	.002	.001	.000	.004	-.003	.005	-.041	.017
	.857	-.014	-.003	-.003	-.005	-.001	-.008	-.005	-.041	.011
	.877	-.014	-.003	-.003	-.006	-.001	-.009	-.006	.034	.000
	.897	-.015	-.004	-.004	-.006	-.002	-.010	-.008	.036	.003
	.917	-.017	-.006	-.007	-.008	-.005	-.012	-.011	.028	.003
	.957	-.027	-.016	-.017	-.019	-.015	-.022	-.021	.028	.013
	.937	-.081	-.076	-.076	-.079	-.077	-.090	-.099	-.080	-.037

TABLE 15.- PRESSURE COEFFICIENTS FOR CONFIGURATION 153 - Concluded

(a) $M = 0.40$ to 1.20 ; $\alpha = 0^\circ$; $\phi = -90^\circ$

x/l	Cp for -										
		M = 0.40	M = 0.60	M = 0.70	M = 0.75	M = 0.80	M = 0.85	M = 0.90	M = 0.95	M = 1.00	M = 1.20
Nose		.253 -.388 .166 .111 .526 .532 .024	.288 .327 .183 .133 .077 .033	.259 .495 .197 .144 .082 .033	.305 .572 .208 .151 .099 .046	.317 .631 .216 .164 .111 .053	.337 .689 .237 .184 .136 .094	.353 .752 .295 .205 .157 .120	.360 .806 .284 .237 .197 .160	.433 .863 .335 .290 .255 .216	.312 1.022 .309 .315 .317 .257
Upper stage											
Transition flare											
Main stage											
		.552	-.075	-.553	-.036	-.008	.028	.069	.125	.185	.322
		.568	-1.013	-1.237	-1.467	-1.306	-1.134	-.979	-.847	-.726	-.381
		.590	-.138	-.139	-.136	-.131	-.327	-.767	-.677	-.570	-.299
		.607	-.069	-.071	-.065	-.058	-.007	-.065	-.479	-.398	-.209
		.627	-.046	-.048	-.044	-.043	-.022	.035	-.322	-.273	-.147
		.657	-.020	-.022	-.024	-.025	-.018	.006	-.041	-.164	-.072
		.697	-.010	-.012	-.014	-.014	-.011	-.008	-.049	-.096	-.045
		.737	-.004	-.005	-.006	-.007	-.004	-.007	-.022	-.070	-.041
		.777	.000	-.002	-.005	-.003	-.002	-.005	.010	-.053	-.018
		.765	.000	.000	-.002	-.003	.000	-.005	.008	-.050	-.012
		.817	.004	.003	.002	.002	.006	-.001	.007	-.039	-.011
		.857	-.001	-.002	-.003	-.004	.000	-.008	-.004	-.041	-.006
		.897	-.003	-.005	-.005	-.007	-.003	-.011	-.009	.034	-.003

TABLE 16.-- SECTION NORMAL-FORCE COEFFICIENTS FOR CONFIGURATION 121

x/l	C _n for											
	α = 3°				α = 6°				α = 10°			
	M = 0.60	M = 0.80	M = 1.00	M = 1.20	M = 0.60	M = 0.80	M = 1.00	M = 1.20	M = 0.60	M = 0.80	M = 1.00	M = 1.20
Nose	.0875	.0808	.0774	.0781	.1647	.1656	.1604	.1694	.2761	.2814	.2719	.2785
	.0920	.0824	.0795	.0874	.1647	.1690	.1630	.1641	.2742	.2825	.2731	.2742
	.0911	.0817	.0793	.0847	.1685	.1694	.1668	.1606	.2728	.2815	.2766	.2747
	.0830	.0771	.0728	.0820	.1680	.1642	.1564	.1531	.2680	.2675	.2606	.2609
	.0835	.0727	.0636	.0637	.1608	.1519	.1411	.1424	.2549	.2533	.2367	.2381
	.0550	.0496	.0407	.0417	.1132	.0997	.0884	.0977	.1830	.1679	.1476	.1656
	.0980	.0452	.0205	.0312	.1485	.0867	.0641	.0606	.2151	.0905	.1071	.1010
	.0142	.0269	.0461	.0303	.0446	.0407	.0990	.0676	.0871	.1293	.1632	.1152
	.0082	.0639	.0729	.0498	.0282	.1580	.1590	.0983	.0516	.2280	.2614	.1714
	.0028	.0088	.0778	.0520	.0146	.0342	.1686	.1062	.0354	.0707	.2868	.1880
	.0007	.0054	.0597	.0430	.0074	.0067	.1308	.0918	.0296	.0166	.1872	.1614
	.0017	.0013	.0149	.0292	.0088	.0026	.0241	.0619	.0271	.0108	.0131	.1109
	.0017	.0052	.0123	.0142	.0156	.0119	.1775	.0315	.0344	.0325	.1540	.0540
	.0261	.0413	.0343	.0270	.0585	.0830	.0910	.0699	.1027	.1248	.1554	.1260
	.0387	.0197	.0176	.0062	.0611	.0578	.0427	.0207	.0836	.1085	.0689	.0486
	.0314	.0216	.0204	.0167	.0578	.0557	.0415	.0335	.0882	.1091	.0723	.0594
	.0348	.0223	.0238	.0309	.0559	.0565	.0526	.0510	.0931	.1180	.0941	.0829
	.0365	.0240	.0276	.0269	.0572	.0577	.0591	.0660	.0914	.1198	.1087	.0982
	.0295	.0232	.0302	.0327	.0572	.0581	.0729	.0734	.0806	.1131	.1236	.1109
	.0185	.0043	.0415	.0419	.0326	.0282	.0887	.0792	.0503	.0734	.1328	.1209
	.0091	.0184	.0244	.0335	.0156	.0252	.0601	.0519	.0282	.0067	.0946	.0895
	.0221	.0027	.0156	.0230	.0211	.0034	.0476	.0393	.0236	.0209	.0987	.0930
	.0174	.0027	.0188	.0212	.0185	.0046	.0432	.0385	.0210	.0184	.0841	.0855
	.0153	.0012	.0079	.0139	.0195	.0001	.0205	.0271	.0127	.0133	.0397	.0619
	.0160	.0012	.0033	.0086	.0132	.0024	.0035	.0244	.0124	.0117	.0086	.0527
	.0159	.0014	.0129	.0059	.0135	.0029	.0350	.0103	.0145	.0107	.0265	.0341
	.0184	.0012	.0176	.0018	.0159	.0034	.0304	.0012	.0123	.0115	.0448	.0191
	.0152	.0027	.0117	.0019	.0166	.0003	.0304	.0032	.0121	.0105	.0417	.0078
	.0087	.0017	.0107	.0129	.0166	.0001	.0311	.0004	.0174	.0145	.0467	.0053
	.0121	.0000	.0057	.0002	.0112	.0047	.0486	.0068	.0210	.0208	.0392	.0100
	.0114	.0002	.0011	.0015	.0111	.0049	.0554	.0066	.0210	.0228	.0371	.0122
	.0091	.0006	.0033	.0042	.0068	.0035	.0107	.0039	.0137	.0161	.0165	.0032
	.0099	.0014	.0043	.0004	.0083	.0038	.0109	.0090	.0149	.0192	.0235	.0256
	.0080	.0005	.0085	.0022	.0054	.0014	.0035	.0026	.0077	.0063	.0043	.0267
	.0090	.0002	.0031	.0114	.0101	.0063	.0139	.0111	.0122	.0164	.0234	.0250
	.0074	.0020	.0021	.0020	.0080	.0038	.0098	.0203	.0104	.0136	.0180	.0208
	.0080	.0015	.0029	.0006	.0086	.0036	.0099	.0004	.0114	.0147	.0201	.0272
	.0075	.0010	.0053	.0009	.0081	.0044	.0072	.0028	.0107	.0143	.0182	.0070

TABLE 17.- SECTION NORMAL-FORCE COEFFICIENTS FOR CONFIGURATION 221

x/l	C _n for -											
	α = 3°				α = 6°				α = 10°			
	M = 0.60	M = 0.80	M = 1.00	M = 1.20	M = 0.60	M = 0.80	M = 1.00	M = 1.20	M = 0.60	M = 0.80	M = 1.00	M = 1.20
Nose	.1056	.1062	.1016	.1027	.2089	.2098	.1988	.1943	.3438	.3443	.3297	.3274
	.1006	.1031	.2972	.0937	.2043	.2011	.1900	.1838	.3341	.3232	.3135	.3073
	.0998	.0936	.0896	.0813	.1879	.1804	.1731	.1629	.3270	.3113	.2985	.2904
	-.0180	-.2534	.0360	.0228	-.0294	-.4089	.0578	.0473	-.0134	-.5860	.0878	.0764
Upper stage	.1049	-.0721	.0502	.0339	.2004	-.1312	.1024	.0700	.3004	-.0763	.1747	.1288
	.0407	.0336	.0931	.0644	.0952	.1033	.1855	.1296	.1807	.2049	.3140	.2268
	.0086	.1882	.1120	.0762	.0195	.2700	.2258	.1601	.0533	.3139	.3742	.2757
	.0035	.0861	.0968	.0755	.0147	.1157	.1949	.1498	.0325	.1443	.1405	.2457
	.0049	.0247	.0481	.0318	.0146	.0418	.0568	.1042	.0352	.0608	.0259	.1766
	.0096	.0268	-.1300	.0245	.0205	.0371	-.1562	.0538	.0457	.0545	-.0328	.0893
	.0339	.0722	.0403	.0233	.0640	.1098	.0861	.0611	.1113	.1376	.1860	.1331
Transition flare	.0302	.0318	.0105	-.0014	.0567	.0573	.0396	.0061	.0994	.0861	.0687	.0408
	.0288	.0293	.0105	.0089	.0539	.0555	.0383	.0168	.0996	.0877	.0572	.0439
	.0262	.0343	.0213	.0278	.0529	.0592	.0541	.0388	.1053	.0975	.0830	.0695
	.0257	.0363	.0233	.0266	.0587	.0596	.0640	.0545	.1025	.1018	.1034	.0881
	.0233	.0338	.0317	.0306	.0511	.0583	.0756	.0659	.0944	.0876	.1231	.1039
	.0133	.0106	.0462	.0421	.0339	.0256	.0982	.0765	.0651	.0495	.1373	.1217
Main stage	-.0001	-.0198	.0268	.0298	-.0014	-.0325	.0637	.0462	.0228	-.0241	.0899	.0819
	.0061	.0060	.0126	.0207	.0148	.0021	.0560	.0347	.0308	.0076	.0976	.0860
	.0075	.0083	.0177	.0259	.0084	-.0001	.0543	.0314	.0308	.0060	.0861	.0821
	.0013	.0059	.0049	.0136	.0073	.0016	.0347	.0239	.0185	.0083	.0485	.0643
	.0097	.0084	-.0058	.0107	.0073	.0032	.0121	.0196	.0208	.0066	.0141	.0505
	.0038	.0074	-.0159	.0066	.0062	.0006	-.0068	.0062	.0192	.0001	-.0134	.0316
	-.0001	.0086	-.0225	.0021	.0026	.0015	.0180	-.0016	.0206	.0031	-.0286	.0176
	.0072	.0058	-.0168	.0015	.0070	.0047	-.0102	.0005	.0189	.0039	-.0189	.0089
	.0017	.0072	-.0135	.0118	.0071	.0108	.0071	.0005	.0189	.0056	-.0219	.0042
	.0019	.0079	-.0182	-.0011	.0082	.0136	.0042	.0080	.0219	.0113	-.0101	.0107
	.0001	.0083	-.0468	-.0004	.0068	.0134	.0022	-.0058	.0234	.0134	-.0113	.0121
	.0021	.0059	-.0109	-.0003	.0063	.0134	.0146	.0039	.0208	.0073	-.0223	-.0002
	.0028	.0096	.0061	-.0040	.0082	.0111	.0142	.0091	.0194	.0106	.0267	.0219
	.0005	.0019	.0019	.0018	.0056	.0066	.0096	.0012	.0130	.0006	.0119	.0261
	.0032	.0088	.0133	.0115	.0068	.0066	.0151	.0085	.0136	.0113	.0254	.0244
	.0019	.0067	.0062	.0014	.0061	.0087	.0081	.0188	.0127	.0083	.0162	.0204
	.0025	.0069	.0056	-.0013	.0054	.0088	.0165	-.0011	.0124	.0093	.0183	.0271
	.0024	.0068	.0035	.0004	.0062	.0092	.0114	.0006	.0121	.0092	.0164	.0083

TABLE 18.- SECTION NORMAL-FORCE COEFFICIENTS FOR CONFIGURATION 321

x/l	C_n for -											
	$\alpha = 30^\circ$				$\alpha = 6^\circ$				$\alpha = 10^\circ$			
	M = 0.60	M = 0.80	M = 1.00	M = 1.20	M = 0.60	M = 0.80	M = 1.00	M = 1.20	M = 0.60	M = 0.80	M = 1.00	M = 1.20
Noise	.1152	.1100	.1068	.1015	.2282	.2278	.2167	.2103	.3835	.3783	.3581	.3469
	.1107	.1053	.0993	.0932	.2132	.2157	.2038	.1952	.3608	.3608	.3409	.3277
	.1030	.0955	.0855	.0846	.1902	.1919	.1850	.1746	.3501	.3298	.3093	.2894
	.1641	.1405	.0259	.0167	.3209	.3872	.0613	.0549	.4266	.5560	.1062	.0929
	.0442	.0814	.0627	.0471	.1029	.2283	.1243	.0963	.2659	.2869	.2040	.1672
	.1974	.0643	.1083	.0775	.3388	.1256	.2012	.1519	.4482	.0167	.3038	.2596
	.0572	.0389	.1244	.0981	.0891	.2027	.2475	.1955	.1613	.3476	.2711	.3242
	.0109	.0950	.1175	.0950	.0236	.2546	.2308	.1850	.0724	.3024	.2034	.3025
	.0084	.0913	.0653	.0466	.0137	.1713	.0303	.1324	.0417	.1856	.1219	.2136
	.0190	.0657	.1418	.0372	.0313	.1126	.1457	.0724	.0541	.1327	.0186	.1093
	.0554	.0947	.0579	.0363	.0910	.1588	.1185	.0787	.1255	.2069	.2368	.1748
	.0301	.0207	.0120	.0041	.0566	.0603	.0240	.0017	.0965	.0936	.0706	.0416
	.0251	.0168	.0114	.0034	.0472	.0531	.0229	.0113	.1008	.0904	.0490	.0350
	.0319	.0238	.0187	.0227	.0469	.0608	.0421	.0356	.1104	.0994	.0716	.0524
	.0291	.0244	.0270	.0240	.0519	.0699	.0558	.0525	.1026	.1114	.1005	.0799
	.0232	.0180	.0373	.0320	.0444	.0616	.0735	.0675	.0908	.0981	.1240	.0968
	.0034	.0119	.0516	.0452	.0149	.0221	.0945	.0814	.0600	.0550	.1411	.1219
	.0064	.0372	.0341	.0287	.0109	.0463	.0564	.0496	.0209	.0156	.0904	.0877
	.0073	.0011	.0124	.0210	.0041	.0011	.0393	.0348	.0320	.0206	.0962	.0898
	.0096	.0038	.0144	.0114	.0039	.0093	.0368	.0316	.0297	.0232	.0750	.0835
	.0096	.0040	.0030	.0123	.0039	.0071	.0157	.0223	.0249	.0200	.0276	.0604
	.0095	.0040	.0116	.0076	.0017	.0102	.0061	.0281	.0234	.0189	.0035	.0471
	.0096	.0046	.0202	.0060	.0022	.0093	.0237	.0077	.0285	.0187	.0285	.0308
	.0049	.0039	.0247	.0039	.0003	.0075	.0322	.0014	.0172	.0187	.0403	.0153
	.0073	.0040	.0181	.0017	.0009	.0070	.0221	.0005	.0206	.0195	.0286	.0053
	.0004	.0002	.0270	.0086	.0014	.0080	.0149	.0011	.0152	.0174	.0294	.0049
	.0032	.0022	.0576	.0018	.0006	.0136	.0212	.0068	.0207	.0228	.0331	.0117
	.0023	.0012	.0923	.0011	.0015	.0132	.0526	.0057	.0214	.0249	.0461	.0155
	.0014	.0011	.0099	.0031	.0006	.0085	.0070	.0039	.0152	.0177	.0241	.0007
	.0020	.0028	.0005	.0008	.0010	.0106	.0108	.0092	.0166	.0200	.0285	.0265
	.0007	.0015	.0050	.0011	.0030	.0046	.0056	.0020	.0110	.0118	.0123	.0268
	.0029	.0008	.0164	.0114	.0030	.0103	.0165	.0093	.0153	.0198	.0304	.0268
	.0019	.0005	.0091	.0019	.0004	.0085	.0092	.0212	.0127	.0169	.0195	.0215
	.0024	.0004	.0054	.0000	.0012	.0087	.0085	.0012	.0142	.0190	.0193	.0281
	.0022	.0005	.0009	.0008	.0021	.0087	.0050	.0013	.0133	.0179	.0169	.0076
Transition Plate												
Main stage												

TABLE 19.- SECTION NORMAL-FORCE COEFFICIENTS FOR CONFIGURATION 12E

x/l	C _n for -											
	α = 30°				α = 6°				α = 10°			
	M = 0.60	M = 0.80	M = 1.00	M = 1.20	M = 0.60	M = 0.80	M = 1.00	M = 1.20	M = 0.60	M = 0.80	M = 1.00	M = 1.20
Nose	.392	.0799	.0759	.0838	.1543	.1637	.1569	.1617	.2720	.2755	.2702	.2688
	.402	.0820	.0782	.0784	.1603	.1665	.1551	.1628	.2712	.2775	.2718	.2685
	.412	.0804	.0783	.0742	.1575	.1688	.1574	.1617	.2661	.2782	.2722	.2693
	.432	.0756	.0757	.0726	.1525	.1658	.1511	.1492	.2590	.2664	.2612	.2572
	.442	.0738	.0691	.0675	.1463	.1488	.1354	.1434	.2515	.2498	.2373	.2457
.447	.0563	.0423	.0462	.0957	.0988	.0866	.0937	.1776	.1603	.1157	.1620	
.453	.0884	.0055	.0232	.0345	.1337	.0295	.0351	.0664	.1999	.0818	.1104	.1113
.458	.0171	.0334	.0427	.0248	.0426	.0803	.0872	.0567	.0960	.1950	.1478	.1147
.463	.0046	.0483	.0627	.0382	.0297	.1133	.1368	.0843	.0591	.2030	.2010	.1724
.473	.0019	.0056	.0798	.0444	.0184	.0155	.0939	.1022	.0367	.0492	.0489	.1957
.483	.0003	.0030	.0505	.0420	.0169	.0016	.1101	.0873	.0340	.0157	.0479	.1667
.493	.0019	.0011	.1266	.0327	.0168	.0082	.1334	.0598	.0330	.0237	.0737	.1104
.503	.0044	.0127	.0736	.0202	.0266	.0291	.1410	.0627	.0536	.0535	.2043	.0904
.513	.0305	.0496	.1253	.0480	.0866	.1022	.2226	.0921	.1422	.1671	.3255	.1621
.525	.0372	.0476	.0551	.0506	.0744	.0968	.0984	.0962	.1323	.1473	.1606	.1434
.535	.0480	.0515	.0280	.0323	.0852	.1094	.0730	.0790	.1624	.1698	.1412	.1323
.545	.0494	.0565	.0326	.0412	.0873	.1176	.0861	.0840	.1661	.1855	.1518	.1338
.555	.0429	.0612	.0521	.0521	.0910	.1227	.1058	.0946	.1584	.1813	.1668	.1521
.565	.0217	.0579	.0657	.0778	.0484	.1152	.1218	.1340	.1022	.1192	.1795	.1905
.564	.0071	.1161	.0306	.0309	.0086	.1289	.0590	.0588	.0547	.1250	.0885	.0912
.577	.0129	.0182	.0268	.0229	.0209	.0323	.0749	.0516	.0555	.0394	.1521	.1089
.587	.0067	.0083	.0404	.0269	.0046	.0184	.0927	.0635	.0331	.0185	.1746	.1280
.597	.0002	.0056	.0346	.0205	.0026	.0102	.0753	.0544	.0209	.0166	.1329	.1046
.607	.0006	.0046	.0209	.0234	.0011	.0101	.0466	.0503	.0242	.0132	.0638	.0944
.617	.0016	.0047	.0023	.0163	.0014	.0060	.0014	.0339	.0169	.0123	.0662	.0688
.627	.0005	.0031	.0193	.0086	.0051	.0069	.0343	.0210	.0130	.0083	.0370	.0430
.637	.0031	.0031	.0219	.0016	.0050	.0076	.0374	.0147	.0120	.0106	.0516	.0299
.647	.0027	.0009	.0162	.0128	.0095	.0052	.0301	.0015	.0119	.0131	.0440	.0092
.677	.0023	.0035	.0068	.0039	.0044	.0094	.0120	.0010	.0175	.0189	.0061	.0067
.697	.0023	.0002	.0025	.0040	.0052	.0096	.0025	.0131	.0190	.0213	.0133	.0048
.717	.0035	.0020	.0036	.0006	.0010	.0057	.0004	.0022	.0122	.0154	.0168	.0073
.727	.0023	.0002	.0043	.0015	.0001	.0076	.0047	.0072	.0146	.0193	.0209	.0180
.735	.0047	.0025	.0017	.0006	.0019	.0034	.0031	.0025	.0086	.0108	.0244	.0244
.817	.0003	.0015	.0088	.0100	.0001	.0091	.0018	.0077	.0066	.0099	.0218	.0218
.857	.0017	.0031	.0020	.0017	.0011	.0065	.0064	.0266	.0127	.0149	.0237	.0228
.877	.0016	.0021	.0033	.0007	.0021	.0073	.0160	.0003	.0108	.0145	.0256	.0269
.897	.0013	.0003	.0036	.0001	.0014	.0076	.0077	.0024	.0094	.0146	.0237	.0084

TABLE 20.- SECTION NORMAL-FORCE COEFFICIENTS FOR CONFIGURATION 222

x/l	C _x for --											
	α = 30°				α = 60°				α = 100°			
	M = 0.60	M = 0.80	M = 1.00	M = 1.20	M = 0.60	M = 0.80	M = 1.00	M = 1.20	M = 0.60	M = 0.80	M = 1.00	M = 1.20
Nose	.1017	.1069	.0979		.2092	.2106	.1944	.9394	.3449	.3415	.3333	.3301
	.0957	.1026	.0981		.1996	.2030	.1869	.8761	.3387	.3238	.3174	.3126
	.0922	.0920	.0885		.1929	.1861	.1710	.7637	.3248	.3012	.3000	.2928
	.0333	.03482	.0106		.0201	.0247	.0247	.4556	.0755	.07197	.0551	.0258
	.1068	.0770	.0578		.2038	.1853	.1124	.6238	.3147	.2053	.0278	.1492
	.0471	.0034	.0894		.1228	.0200	.1639	.2882	.2400	.1168	.0035	.2286
	.0051	.1472	.1102		.0266	.2957	.0285	.1071	.0787	.3369	.0699	.2814
	.0011	.1115	.1066		.0178	.2035	.0851	.0369	.0426	.1898	.0877	.2512
	.493	.0465	.1938		.0153	.0967	.0552	.0326	.0495	.1043	.0373	.1448
	.503	.0087	.1250		.0280	.0874	.2506	.1582	.0724	.1041	.2941	.0507
	.513	.1130	.1994		.0982	.1936	.3400	.3893	.1727	.2202	.4415	.2006
	.0433	.0636	.0839		.0858	.1151	.1780	.4215	.1404	.1587	.2447	.1563
	.0490	.0584	.0379		.0986	.1079	.1072	.3598	.1623	.1646	.1906	.1300
	.0465	.0615	.0373		.0998	.1154	.0941	.3276	.1670	.1696	.1710	.1302
	.555	.0461	.0559		.0975	.1202	.1115	.3416	.1551	.1657	.1840	.1500
	.565	.0108	.0786		.0480	.0576	.1283	.2835	.0923	.1089	.1899	.1939
	.568	.0128	.0315		.0037	.02748	.0442	.2079	.0378	.2239	.0899	.0971
	.577	.0114	.0028		.0316	.0231	.0271	.1782	.0576	.0146	.1049	.0932
	.587	.0088	.0183		.0207	.0250	.0569	.1134	.0390	.0102	.1287	.1167
	.597	.0011	.0196		.0148	.0185	.0363	.0717	.0330	.0079	.0834	.0995
	.607	.0014	.0068		.0155	.0158	.0074	.0694	.0290	.0067	.0179	.0388
	.617	.0014	.0079		.0093	.0158	.0218	.0741	.0264	.0042	.0194	.0359
	.627	.0014	.0212		.0071	.0159	.0356	.0747	.0187	.0035	.0508	.0346
	.637	.0048	.0197		.0095	.0158	.0279	.0605	.0178	.0072	.0493	.0266
	.657	.0030	.0126		.0087	.0149	.0127	.0524	.0300	.0058	.0371	.0041
	.677	.0010	.0053		.0112	.0178	.0031	.0424	.0268	.0108	.0101	.0027
	.737	.0019	.0021		.0107	.0189	.0116	.0631	.0299	.0116	.0061	.0023
	.777	.0055	.0074		.0061	.0139	.0423	.0387	.0224	.0056	.0265	.0083
	.785	.0052	.0020		.0069	.0162	.0193	.0179	.0200	.0039	.0027	.0248
	.817	.0042	.0061		.0070	.0113	.0138	.0188	.0214	.0113	.0066	.0262
	.857	.0014	.0099		.0083	.0177	.0173	.0029	.0188	.0092	.0139	.0242
	.877	.0028	.0012		.0076	.0159	.0057	.0179	.0188	.0092	.0139	.0242
	.877	.0025	.0090		.0069	.0160	.0052	.0159	.0188	.0097	.0221	.0288
	.897	.0029	.0092		.0071	.0155	.0021	.0104	.0194	.0097	.0255	.0104

TABLE 21.- SECTION NORMAL-FORCE COEFFICIENTS FOR CONFIGURATION 322

x/l	C_n for -											
	$\alpha = 30^\circ$				$\alpha = 6^\circ$				$\alpha = 10^\circ$			
	M = 0.60	M = 0.80	M = 1.00	M = 1.20	M = 0.60	M = 0.80	M = 1.00	M = 1.20	M = 0.60	M = 0.80	M = 1.00	M = 1.20
None	.1041	.1115	.1064	.0977	.2114	.1889	.2146	.2029	.3680	.3727	.3557	.3475
	.1008	.1004	.1003	.0935	.1889	.1542	.2154	.1891	.3462	.3507	.3391	.3261
	.0837	.0858	.0892	.0785	.1542	.0435	.1820	.1666	.3009	.3143	.3079	.2916
	.3975	.4016	.0200	.0133	.6542		.0334	.0334	.8456	.6982	.1130	.0669
	.0731	.2394	.0531	.0412	.0242		.0861	.0861	.1127	.3182	.3428	.518
	.1981	.1480	.0955	.3220	.0355		.1612	.1612	.4568	.0574	.1229	.2721
	.1354	.0839	.0442	.1014	.2605		.2094	.2094	.3417	.3561	.2210	.3500
Upper stage	.0072	.1842	.1735	.0957	.0677		.1934	.1934	.1349	.3340	.2502	.2658
	.0077	.1634	.0674	.0222	.0222		.1372	.1372	.0754	.2431	.2390	.0914
	.0152	.1283	.2049	.0463	.0463		.0777	.0777	.0959	.2112	.3770	.0070
	.0764	.1540	.2570	.0575	.1403		.4057	.1214	.2029	.3169	.5674	.2393
	.0505	.0718	.1133	.0390	.0883		.2201	.0974	.1477	.1813	.3487	.1860
	.0491	.0512	.0691	.0189	.0803		.1504	.0663	.1595	.1609	.2496	.1495
	.0469	.0448	.0458	.0271	.0792		.1251	.0616	.1606	.1531	.2106	.1353
	.0382	.0366	.0642	.0415	.0760		.1348	.0792	.1478	.1456	.2061	.1439
	.0240	.0707	.0959	.0738	.0153		.1527	.1317	.0583	.0504	.1960	.1867
	.0530	.2698	.0210	.0291	.0680		.0278	.0507	.0101	.3096	.0490	.0789
	.0103	.0116	.0416	.0195	.0101		.0189	.0385	.0465	.0861	.0412	.0852
	.0093	.0042	.0199	.0225	.0090		.0144	.0550	.0391	.0118	.0664	.1041
	.0031	.0042	.0054	.0165	.0075		.0011	.0474	.0331	.0134	.0087	.0919
	.0056	.0057	.0119	.0198	.0100		.0233	.0444	.0314	.0150	.0348	.0762
	.0016	.0040	.0197	.0160	.0036		.0364	.0277	.0313	.0093	.0538	.0487
	.0064	.0026	.0190	.0085	.0001		.0395	.0162	.0251	.0115	.0659	.0271
	.0017	.0073	.0092	.0027	.0016		.0229	.0119	.0274	.0115	.0391	.0145
	.0046	.0037	.0042	.0122	.0059		.0042	.0022	.0188	.0141	.0164	.0145
	.0062	.0051	.0024	.0050	.0013		.0021	.0009	.0221	.0199	.0060	.0012
	.0061	.0058	.0006	.0051	.0012		.0044	.0147	.0269	.0223	.0053	.0001
	.0007	.0037	.0119	.0001	.0040		.0167	.0001	.0199	.0143	.0344	.0093
	.0034	.0044	.0059	.0029	.0041		.0176	.0079	.0199	.0171	.0120	.0198
	.0027	.0012	.0009	.0013	.0056		.0047	.0013	.0201	.0107	.0121	.0245
	.0002	.0042	.0053	.0083	.0001		.0100	.0100	.0185	.0161	.0290	.0306
	.0003	.0019	.0030	.0012	.0001		.0100	.0209	.0163	.0140	.0238	.0246
	.0005	.0028	.0039	.0031	.0014		.0121	.0005	.0174	.0151	.0255	.0296
	.0004	.0032	.0031	.0015	.0013		.0125	.0032	.0176	.0150	.0259	.0146

TABLE 22.- SECTION NORMAL-FORCE COEFFICIENTS FOR CONFIGURATION 123

x/l	C _n for -											
	α = 30°				α = 60°				α = 100°			
	M = 0.60	M = 0.80	M = 1.00	M = 1.20	M = 0.60	M = 0.80	M = 1.00	M = 1.20	M = 0.60	M = 0.80	M = 1.00	M = 1.20
None	.0756	.0856	.0767	.0737	.1730	.1693	.1627	.1582	.2675	.2837	.2671	.2681
	.0772	.0879	.0803	.0698	.1723	.1730	.1658	.1609	.2646	.2853	.2703	.2728
	.0769	.0894	.0803	.0736	.1762	.1723	.1676	.1565	.2615	.2844	.2741	.2761
	.0710	.0833	.0776	.0729	.1668	.1656	.1601	.1492	.2527	.2749	.2651	.2623
	.0724	.0789	.0725	.0631	.1678	.1599	.1462	.1428	.2432	.2580	.2428	.2461
	.0440	.0497	.0414	.0417	.1159	.1022	.0917	.0920	.1641	.1655	.1437	.1644
	.0689	.0460	.0164	.0294	.1708	-.0292	.0316	.0552	.2030	-.0635	.0895	.0928
	.0060	.0259	.0455	.0306	.0564	.0761	.0843	.0613	.0734	.1365	-.0225	.1180
	.0012	.0538	.0646	.0439	.0437	.1276	.0155	.0941	.0459	.1982	-.1812	.1844
	.0039	.0155	.0290	.0486	.0332	.0319	.1927	.1051	.0225	-.0596	-.1080	.2007
	.0038	.0048	.0409	.0512	.0273	.0057	.1136	.0916	.0164	.0202	.0117	.0841
	.0071	.0229	.1749	.0497	.0271	.0125	.2116	.1547	.0179	.0260	.2570	.1495
	.0498	.0778	.2300	.1187	.0392	.0472	.2504	.1685	.0461	.0706	.2987	.1730
	.0477	.0728	.1234	.1520	.1194	.1477	.3101	.2113	.1726	.2184	.4335	.3230
	.0500	.0741	.0783	.1102	.1089	.1311	.1902	.2593	.1546	.2053	.2374	.3596
	.0554	.0805	.0866	.0840	.1209	.1286	.1452	.1881	.1750	.2129	.2024	.2645
	.0564	.0866	.0788	.0786	.1342	.1482	.1241	.1528	.1914	.2347	.2040	.2271
	.0059	.0305	.0215	.0152	.0384	.0473	.0534	.0379	.0633	.0372	.0977	.0749
	.0021	.0076	.0446	.0045	.0424	.0432	.0620	.0341	.0519	.1205	.1253	.0838
	.0054	.0305	.0057	.0172	.0264	.0357	.0855	.0611	.0277	.0512	.1774	.1381
	.0115	.0170	.0032	.0241	.0213	.0189	.0822	.0678	.0156	.0245	.1458	.1373
	.0137	.0104	.0042	.0285	.0127	.0114	.0412	.0626	.0042	.0172	.0461	.1149
	.0112	.0087	.0068	.0231	.0105	.0082	.0015	.0447	.0052	.0083	.0133	.0817
	.0137	.0088	.0140	.0167	.0098	.0034	.0264	.0328	.0004	.0073	.0255	.0581
	.0115	.0098	.0079	.0068	.0065	.0059	.0238	.0199	.0006	.0120	.0398	.0399
	.0077	.0039	.0032	.0096	.0129	.0059	.0151	.0199	.0027	.0149	.0447	.0088
	.0073	.0054	.0013	.0030	.0153	.0101	.0015	.0010	.0030	.0136	.0090	.0009
	.0068	.0048	.0010	.0078	.0134	.0104	.0052	.0185	.0027	.0136	.0010	.0018
	.0089	.0027	.0010	.0013	.0110	.0054	.0024	.0050	.0026	.0184	.0028	.0138
	.0176	.0049	.0029	.0030	.0085	.0063	.0109	.0037	.0010	.0215	.0090	.0187
	.0141	.0044	.0030	.0035	.0105	.0048	.0118	.0031	.0054	.0178	.0239	.0238
	.0069	.0065	.0065	.0091	.0140	.0093	.0118	.0066	.0021	.0202	.0381	.0314
	.0080	.0046	.0262	.0004	.0136	.0077	.0139	.0206	.0018	.0201	.0345	.0274
	.0083	.0047	.0086	.0030	.0129	.0087	.0197	.0000	.0021	.0213	.0116	.0328
	.0082	.0052	.0031	.0011	.0131	.0086	.0429	.0017	.0016	.0212	.0196	.0141

TABLE 24.- SECTION NORMAL-FORCE COEFFICIENTS FOR CONFIGURATION 323

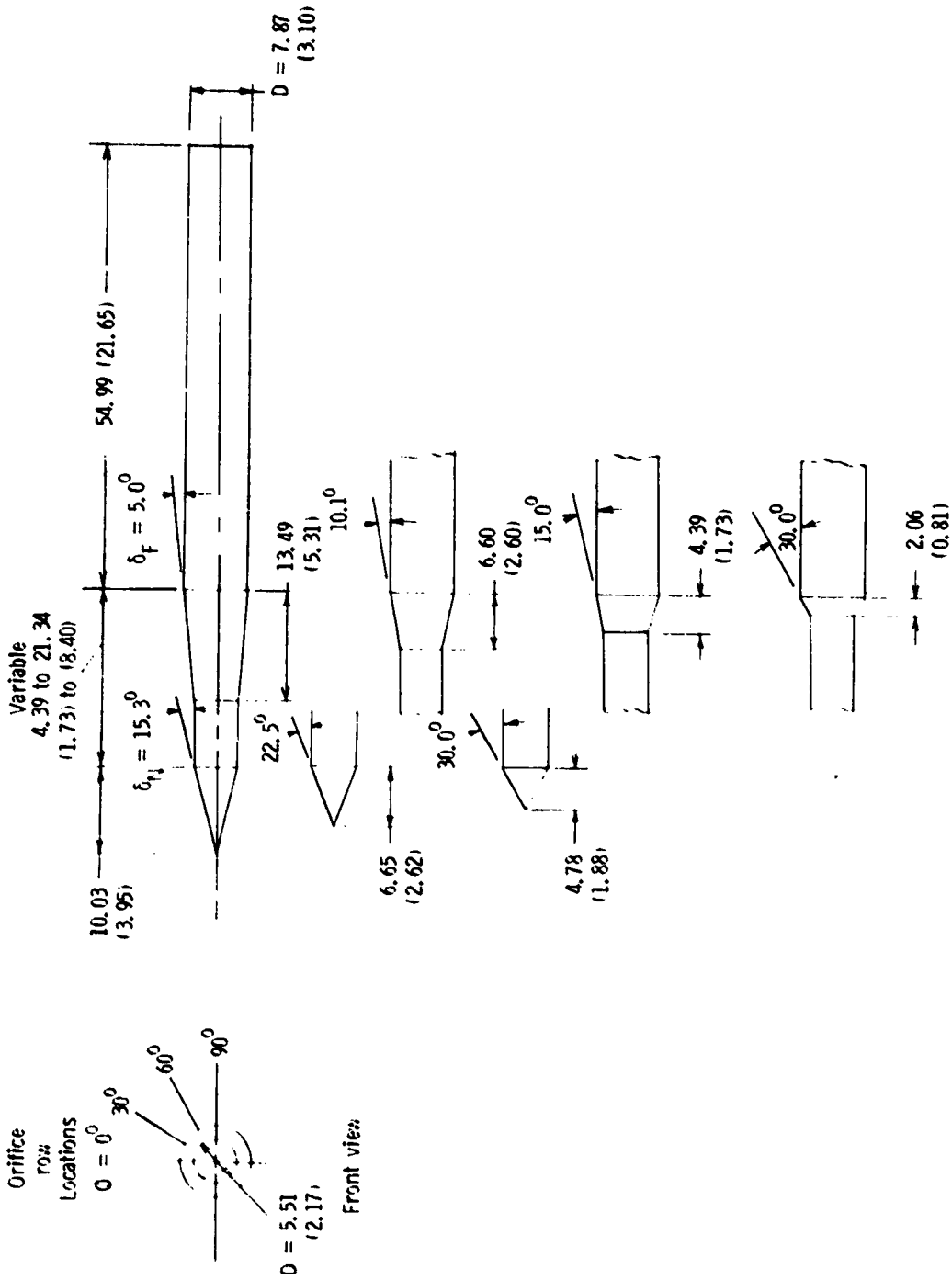
x/l	C _n for -											
	α = 3°				α = 6°				α = 10°			
	M = 0.60	M = 0.80	M = 1.00	M = 1.20	M = 0.60	M = 0.80	M = 1.00	M = 1.20	M = 0.60	M = 0.80	M = 1.00	M = 1.20
Rose												
Upper stage												
Transition												
Main stage												
.443	.1177	.1162	.1095	.1023	.2286	.2248	.2137	.2062	.3771	.3728	.3556	.3513
.453	.1058	.1064	.1037	.0935	.2019	.2079	.2038	.1929	.3451	.3502	.3367	.3311
.463	.0851	.0874	.0903	.0860	.1696	.1778	.1823	.1694	.2945	.3113	.3039	.2945
.471	-.3524	-.2484	-.3065	-.0179	-.4826	-.4202	-.3633	.0353	-.6266	-.5870	-.3654	.0663
.476	-.1818	-.1961	-.5545	.0416	-.1970	-.3050	-.5612	.0874	-.1302	-.3588	-.4849	.1453
.481	.0364	.1710	-.4110	.0783	.0943	.2392	.3631	.1532	.2658	.1706	-.2077	.1891
.491	.2510	-.0584	.1320	.1012	.3394	.0419	-.0057	.1910	.4031	.2640	-.2077	.1968
.501	.1187	.0951	.0839	.0960	.1409	.2823	.1625	.0170	.2094	.4260	.2770	.1351
.511	.0366	.1981	.3248	-.1613	.0532	.3375	.3440	-.0782	.1217	.3680	.3956	.0767
.521	.0513	.2428	.4108	-.0228	.0728	.3339	.4996	-.0414	.1265	.3345	.5484	-.0041
.531	.1375	.2708	.4670	.1594	.1949	.3885	.6154	.2833	.2484	.4419	.7159	.3982
.539	-.0229	.0805	.1581	.1720	-.0562	.0843	.1587	.3205	-.1146	.0961	.1531	.4455
.544	.0237	.1258	.3004	.1776	.0307	.1384	.3328	.3066	.0351	.1658	.3396	.4095
.552	.0565	.1176	.3244	.1132	.0994	.1377	.3331	.1755	.1788	.1978	.3427	.2612
.562	.0164	.0223	.2479	.0970	.0543	.0843	.2571	.1571	.1351	.1549	.2775	.2324
.568	-.1294	-.6298	-.2107	-.0206	.1293	.5102	.1337	.0038	-.0602	-.3378	-.0131	-.0558
.577	.0053	-.0141	-.3076	-.0222	.0120	-.0066	-.1381	.0267	.0373	.0143	.0179	.1200
.587	.0112	.0079	.2085	.0046	.0094	.0134	.1281	.0407	.0302	.0176	.0446	.1293
.597	.0089	.0118	.1192	.0111	.0074	.0090	.0879	.0552	.0235	.0127	.0097	.1182
.607	.0050	.0134	-.0695	.0191	.0057	.0088	-.0833	.0359	.0219	.0131	.0628	.1069
.617	.0051	.0094	-.0228	.0165	.0036	.0079	-.0626	.0228	.0136	.0101	.0796	.0525
.627	.0065	.0102	.0239	.0027	.0011	.0038	-.0441	.0094	.0143	.0095	.0904	.0240
.637	.0037	.0081	.0197	.0135	.0035	.0060	.0131	.0010	.0142	.0134	.0657	.0130
.647	.0049	.0103	.0129	.0035	.0001	.0067	.0072	.0051	.0128	.0122	.0367	.0133
.657	.0063	.0109	.0095	.0052	.0024	.0086	.0050	.0064	.0165	.0161	.0007	.0108
.677	.0026	.0073	.0055	.0002	.0019	.0091	.0015	.0197	.0179	.0184	.0011	.0033
.737	.0038	.0079	.0162	.0008	.0063	.0053	.0130	.0008	.0122	.0122	.0153	.0090
.785	.0060	.0072	.0059	.0022	.0064	.0067	.0145	.0058	.0137	.0122	.0153	.0300
.817	.0042	.0094	.0066	.0110	.0019	.0029	.0043	.0011	.0071	.0096	.0026	.0333
.857	.0029	.0090	.0045	.0018	.0007	.0078	.0001	.0102	.0132	.0172	.0093	.0333
.877	.0026	.0089	.0057	.0007	.0011	.0047	.0035	.0180	.0119	.0149	.0166	.0280
.897	.0031	.0087	.0055	.0005	.0012	.0058	.0081	.0016	.0115	.0151	.0203	.0344
						.0062	.0075	.0030	.0122	.0148	.0190	.0150

TABLE 25.- SECTION NORMAL-FORCE COEFFICIENTS FOR CONFIGURATION 12-4

x/l	C _n for -												
	α = 30°				α = 6°				α = 10°				
	M = 0.60	M = 0.80	M = 1.00	M = 1.20	M = 0.60	M = 0.80	M = 1.00	M = 1.20	M = 0.60	M = 0.80	M = 1.00	M = 1.20	
Nose													
Upper stage	.420	.0760	.0805	.0825	.0715	.1666	.1673	.1584	.1610	.2780	.2818	.2666	.2672
	.433	.0722	.0805	.0832	.0762	.1667	.1713	.1610	.1570	.2722	.2818	.2666	.2754
	.440	.0725	.0791	.0821	.0733	.1628	.1655	.1604	.1570	.2677	.2774	.2639	.2734
	.454	.0762	.0775	.0810	.0715	.1595	.1586	.1521	.1522	.2618	.2652	.2539	.2580
	.475	.0681	.0719	.0750	.0676	.1537	.1529	.1419	.1396	.2529	.2523	.2313	.2397
	.482	.0388	.0429	.0468	.0435	.1008	.0966	.0780	.0924	.1722	.1559	.1368	.1574
	.497	.0534	.0398	.0164	.0196	.1747	.0196	.0151	.0397	.2484	.0578	.0153	.0636
	.494	.0182	.0078	.0422	.0275	.0572	.0410	.0394	.0572	.1023	.0958	.0334	.0815
	.504	.0059	.0500	.0365	.0442	.0384	.0906	.0359	.0176	.0634	.1578	.0286	.0446
	.513	.0015	.0247	.0701	.0191	.0248	.0347	.0778	.1406	.0368	.0533	.1664	.0968
.524	.0031	.0006	.1303	.0474	.0175	.0040	.1926	.1816	.0303	.0165	.2538	.1246	
.530	.0032	.0067	.1827	.1365	.0168	.0183	.2186	.2237	.0289	.0315	.2538	.2428	
.530	.0140	.0465	.2534	.1356	.0399	.0831	.2799	.2430	.0766	.1183	.3297	.3847	
.549	.0785	.1029	.2988	.1567	.1577	.1844	.3579	.2590	.2397	.2651	.4570	.4288	
.554	.0453	.0683	.2700	.1337	.1041	.1389	.2532	.2974	.1577	.1838	.2770	.4529	
.558	.0488	.0825	.2302	.2774	.1010	.1473	.2453	.3896	.1528	.2096	.2847	.4618	
Transition stage	.564	.2202	.1489	.0282	.0257	.3574	.3366	.0111	.0320	.4904	.5936	.0436	.0145
	.577	.0867	.0455	.1758	.0253	.1695	.0744	.0621	.0056	.2469	.0748	.0734	.0632
	.587	.1101	.0271	.0851	.0086	.2359	.0995	.0537	.0728	.3090	.2944	.2082	.1961
	.597	.0250	.0599	.0133	.0194	.0749	.1345	.0813	.0769	.1123	.2295	.2149	.1708
	.607	.0041	.0466	.0151	.0213	.0193	.0900	.0583	.0013	.0321	.1254	.1217	.1652
	.617	.0103	.0248	.0192	.0194	.0046	.0449	.0132	.0507	.0100	.0483	.0417	.1161
	.627	.0078	.0141	.0210	.0156	.0032	.0225	.0097	.0301	.0041	.0153	.0075	.0614
	.637	.0077	.0075	.0265	.0141	.0081	.0143	.0155	.0155	.0051	.0103	.0311	.0350
	.657	.0090	.0330	.0134	.0071	.0127	.0068	.0165	.0022	.0113	.0075	.0366	.0004
	.677	.0068	.0045	.0072	.0040	.0174	.0174	.0118	.0021	.0232	.0075	.0233	.0076
Main stage	.737	.0096	.0024	.0012	.0038	.0148	.0126	.0126	.0121	.0219	.0208	.0124	.0066
	.777	.0124	.0017	.0046	.0036	.0138	.0085	.0156	.0019	.0123	.0148	.0031	.0107
	.765	.0067	.0030	.0052	.0028	.0138	.0083	.0224	.0065	.0167	.0207	.0151	.0187
	.817	.0062	.0052	.0052	.0028	.0152	.0082	.0392	.0032	.0122	.0153	.0122	.0258
	.857	.0067	.0036	.0010	.0015	.0132	.0087	.0481	.0073	.0175	.0192	.0228	.0327
	.877	.0067	.0038	.0010	.0015	.0140	.0087	.0861	.0181	.0164	.0168	.0139	.0256
	.877	.0070	.0036	.0010	.0003	.0142	.0100	.0368	.0016	.0178	.0178	.0139	.0256
	.877	.0070	.0036	.0010	.0003	.0142	.0105	.0004	.0007	.0172	.0179	.0427	.0124

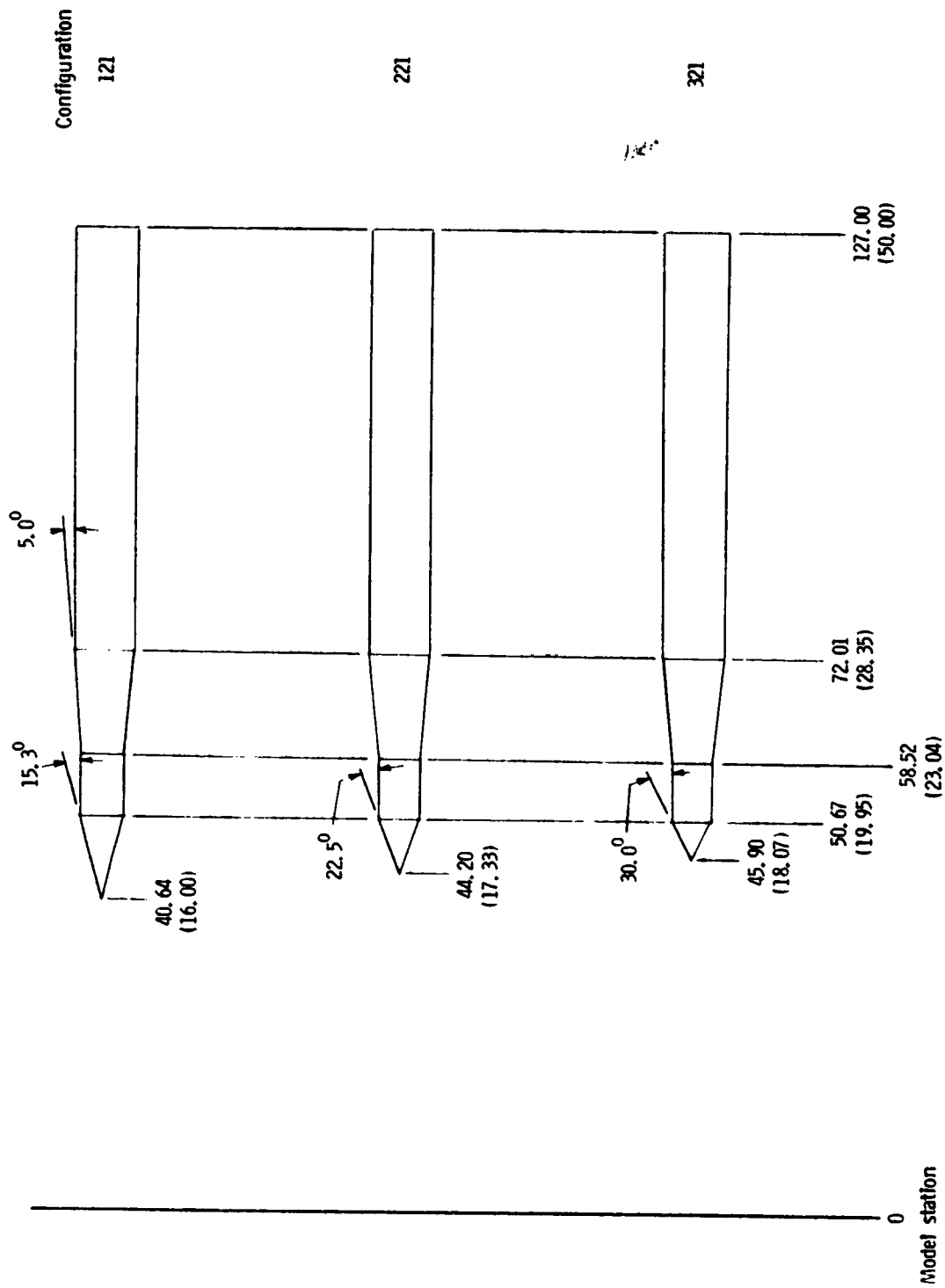
TABLE 26.- SECTION NORMAL-FORCE COEFFICIENTS FOR CONFIGURATION 324

x/l	C_n for -											
	$\alpha = 30^\circ$				$\alpha = 6^\circ$				$\alpha = 10^\circ$			
	M = 0.60	M = 0.80	M = 1.00	M = 1.20	M = 0.60	M = 0.80	M = 1.00	M = 1.20	M = 0.60	M = 0.80	M = 1.00	M = 1.20
Nozzle	.1139	.1058	.1076	.1015	.2254	.2242	.2128	.2070	.3854	.3771	.3550	.3482
	.0942	.0974	.1015	.0954	.2014	.2057	.1957	.1909	.3508	.3546	.3366	.3298
	.0740	.0827	.0917	.0851	.1621	.1776	.1779	.1697	.3007	.3146	.3068	.2908
	.2965	.2005	.3339	.2235	.4345	.3802	.4597	.0139	.5835	.5719	.5039	.1320
	.1615	.2139	.2085	.0405	.1825	.3337	.4230	.1811	.0399	.3047	.4180	.3026
	.0921	.1760	.1061	.1021	.2268	.2010	.2034	.1586	.3469	.0825	.2282	.1497
	.2036	.0386	.0307	.1082	.2781	.1653	.0722	.0128	.3607	.3567	.1060	.0927
Upper stage	.0703	.1306	.0472	.0146	.1093	.2997	.1463	.0316	.1946	.4088	.3661	.1607
	.529	.0431	.0909	.1427	.0689	.3205	.2817	.3319	.1383	.3553	.4949	.3838
	.539	.2850	.2268	.1638	.1404	.3736	.4735	.3645	.1996	.4132	.6621	.5514
	.543	.3530	.3388	.2225	.2524	.4625	.6359	.3889	.3287	.5371	.8256	.5974
Transition	.1088	.2526	.3671	.24.2	.1623	.3067	.5482	.4021	.1959	.3180	.5348	.4569
Flare	.0976	.2213	.3897	.4093	.1617	.2792	.5156	.5284	.2140	.3228	.4771	.5839
Main stage	.0552	.6069	.2145	.0250	.2006	.5319	.2632	.0654	.3640	.5699	.0833	.0044
	.0692	.1904	.2231	.1281	.0058	.2318	.2897	.0984	.1982	.1169	.1049	.0148
	.0177	.0009	.1270	.0796	.0376	.0031	.1360	.0107	.1216	.1314	.0686	.1115
	.0155	.0180	.0560	.0395	.0222	.0229	.0516	.0124	.0411	.0702	.0756	.1219
	.0117	.0180	.0215	.0096	.0167	.0284	.0277	.0150	.0240	.0344	.0086	.0857
	.0093	.0140	.0016	.0076	.0094	.0218	.0159	.0093	.0204	.0229	.0480	.0474
	.0093	.0083	.0149	.0136	.0092	.0178	.0079	.0058	.0203	.0217	.0673	.0179
	.0059	.0058	.0191	.0154	.0108	.0162	.0137	.0019	.0202	.0247	.0594	.0079
	.0059	.0063	.0136	.0082	.0023	.0137	.0155	.0034	.0210	.0263	.0303	.0079
	.0044	.0061	.0094	.0029	.0040	.0150	.0156	.0038	.0248	.0317	.0060	.0251
	.0010	.0037	.0011	.0043	.0049	.0146	.0098	.0065	.0267	.0344	.0071	.0106
	.0014	.0037	.0092	.0012	.0049	.0079	.0012	.0043	.0155	.0271	.0035	.0153
	.0030	.0027	.0096	.0006	.0017	.0069	.0052	.0035	.0224	.0294	.0174	.0213
	.0035	.0044	.0058	.0106	.0007	.0107	.0092	.0035	.0167	.0246	.0154	.0247
	.0025	.0026	.0053	.0018	.0007	.0111	.0088	.0173	.0225	.0288	.0148	.0228
	.0030	.0037	.0095	.0003	.0009	.0088	.0334	.0173	.0202	.0252	.0099	.0191
	.0028	.0028	.0114	.0001	.0006	.0098	.0220	.0027	.0199	.0263	.0201	.0265
							.0114	.0027	.0194	.0269	.0234	.0059



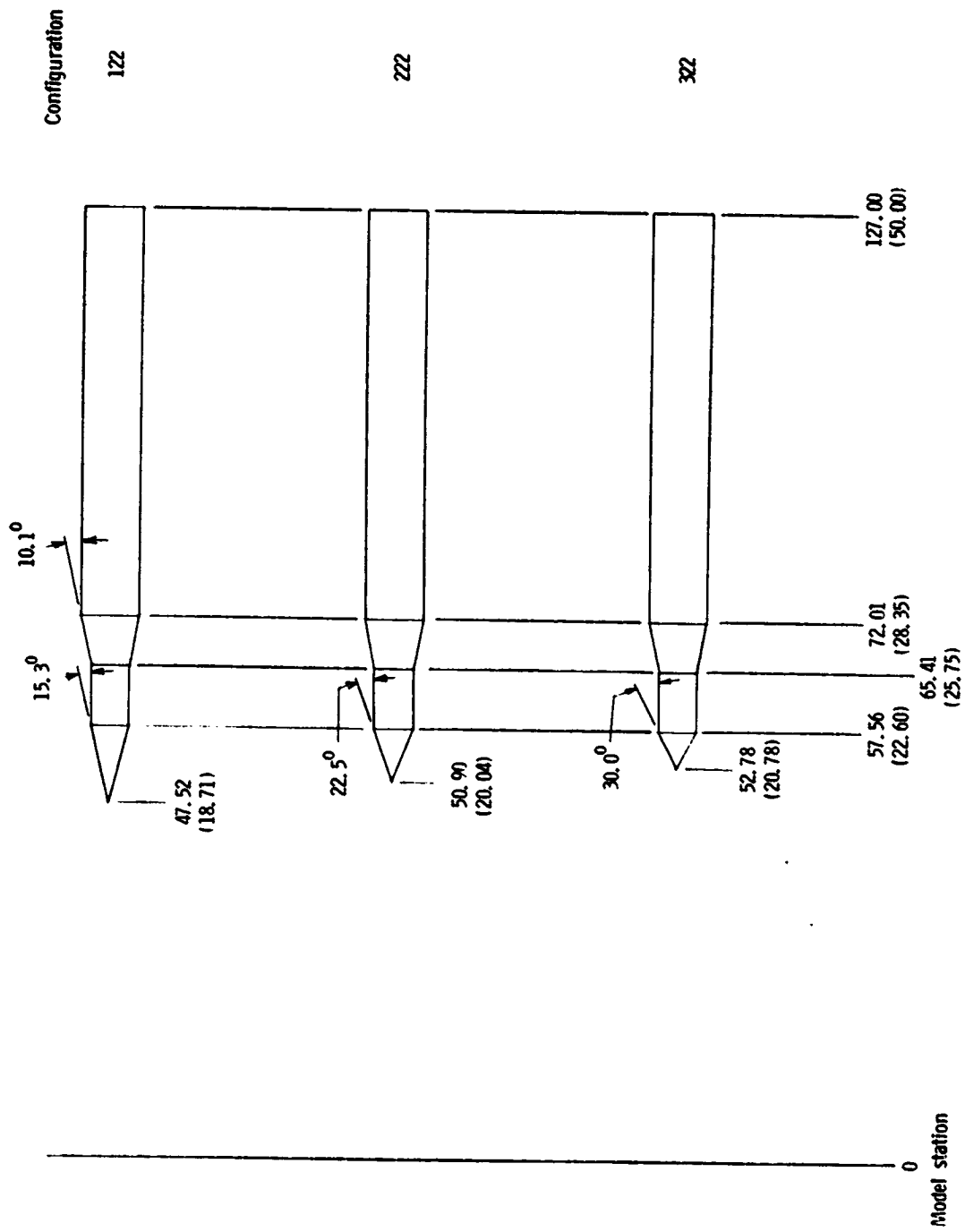
(a) Configuration geometry.

Figure 1.- Details of models. Dimensions are given in centimeters (inches) unless otherwise specified.



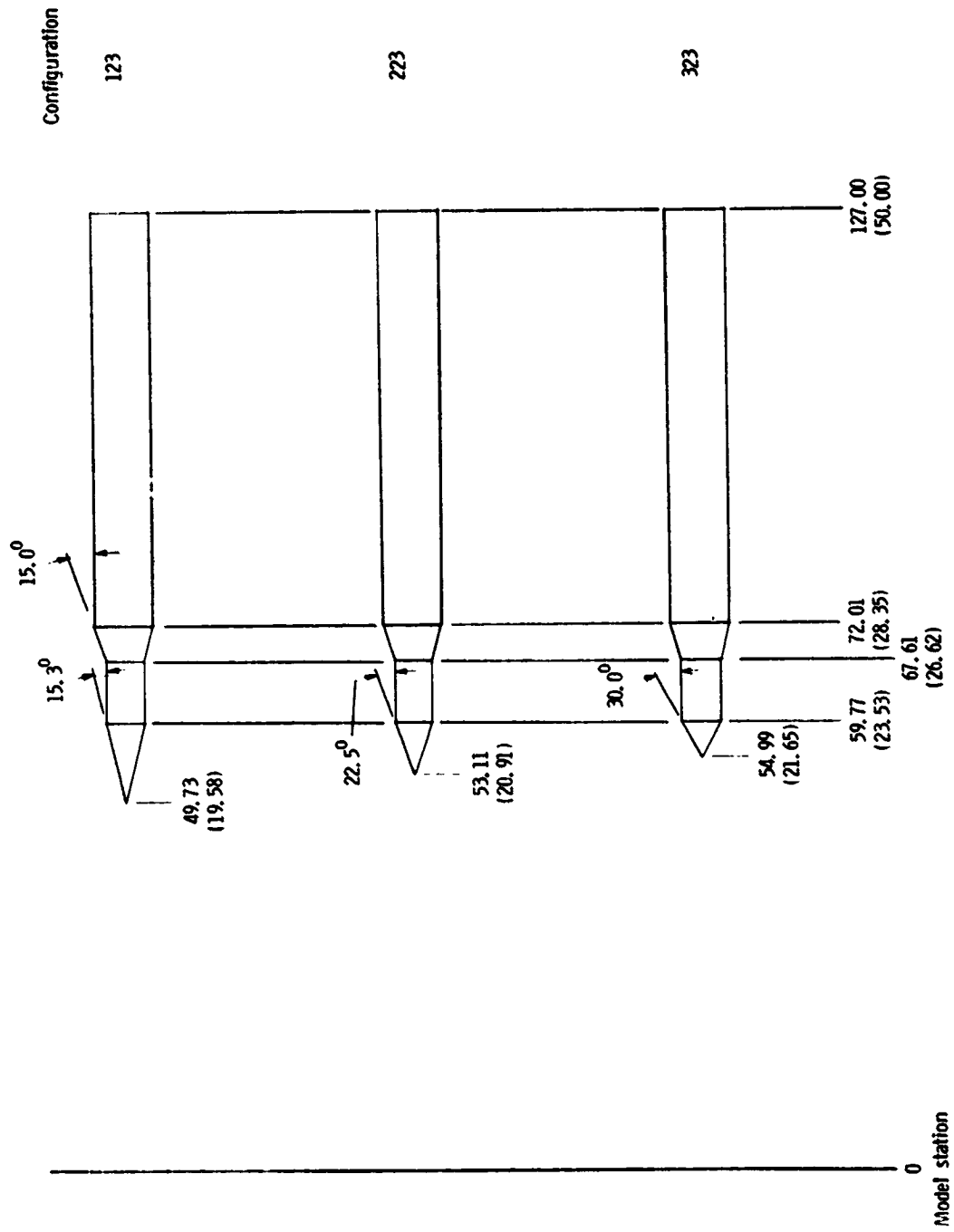
(b) Configurations 121, 221, and 321.

Figure 1.- Continued.



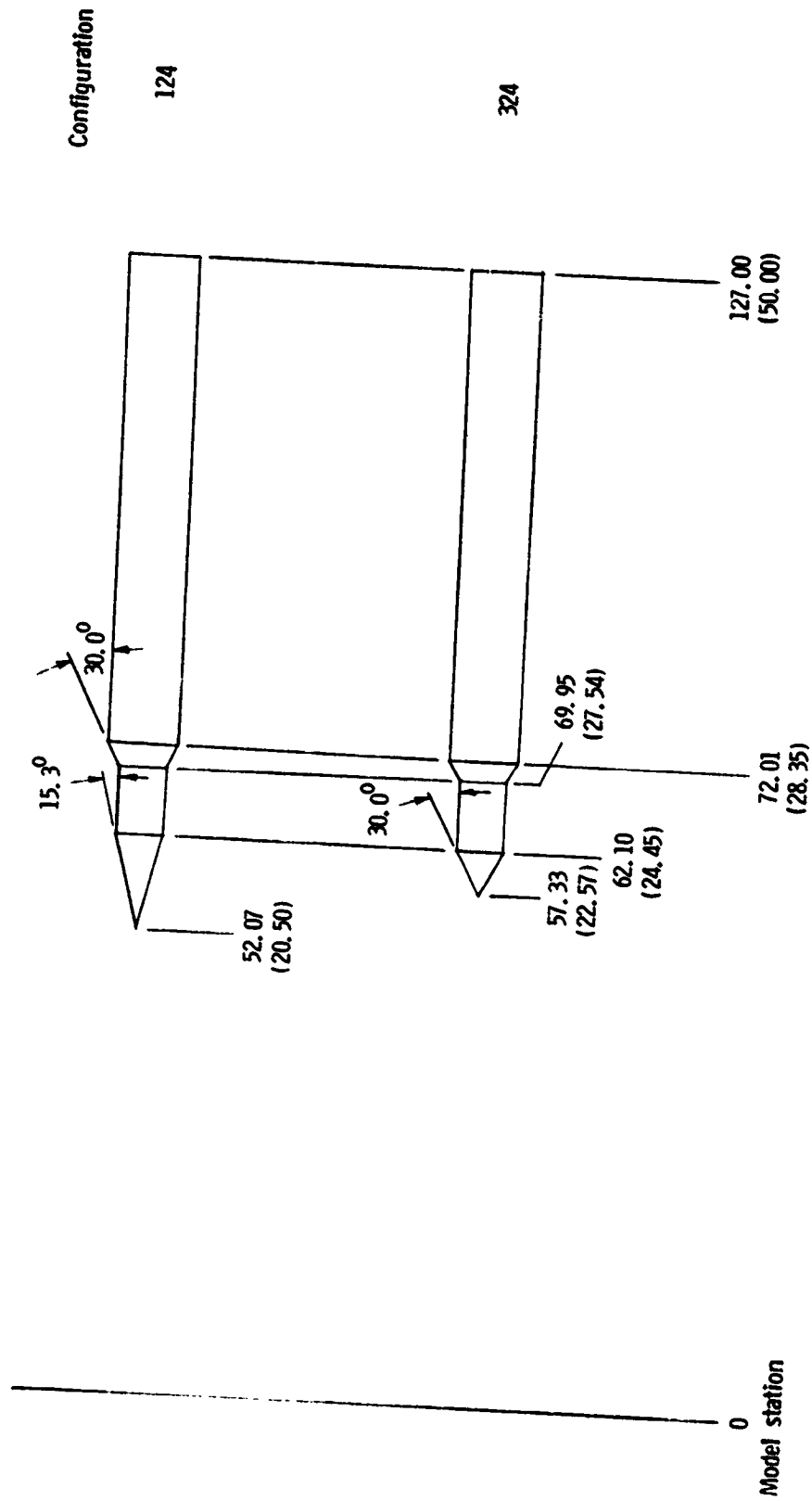
(c) Configurations 122, 222, and 322.

Figure 1.- Continued.



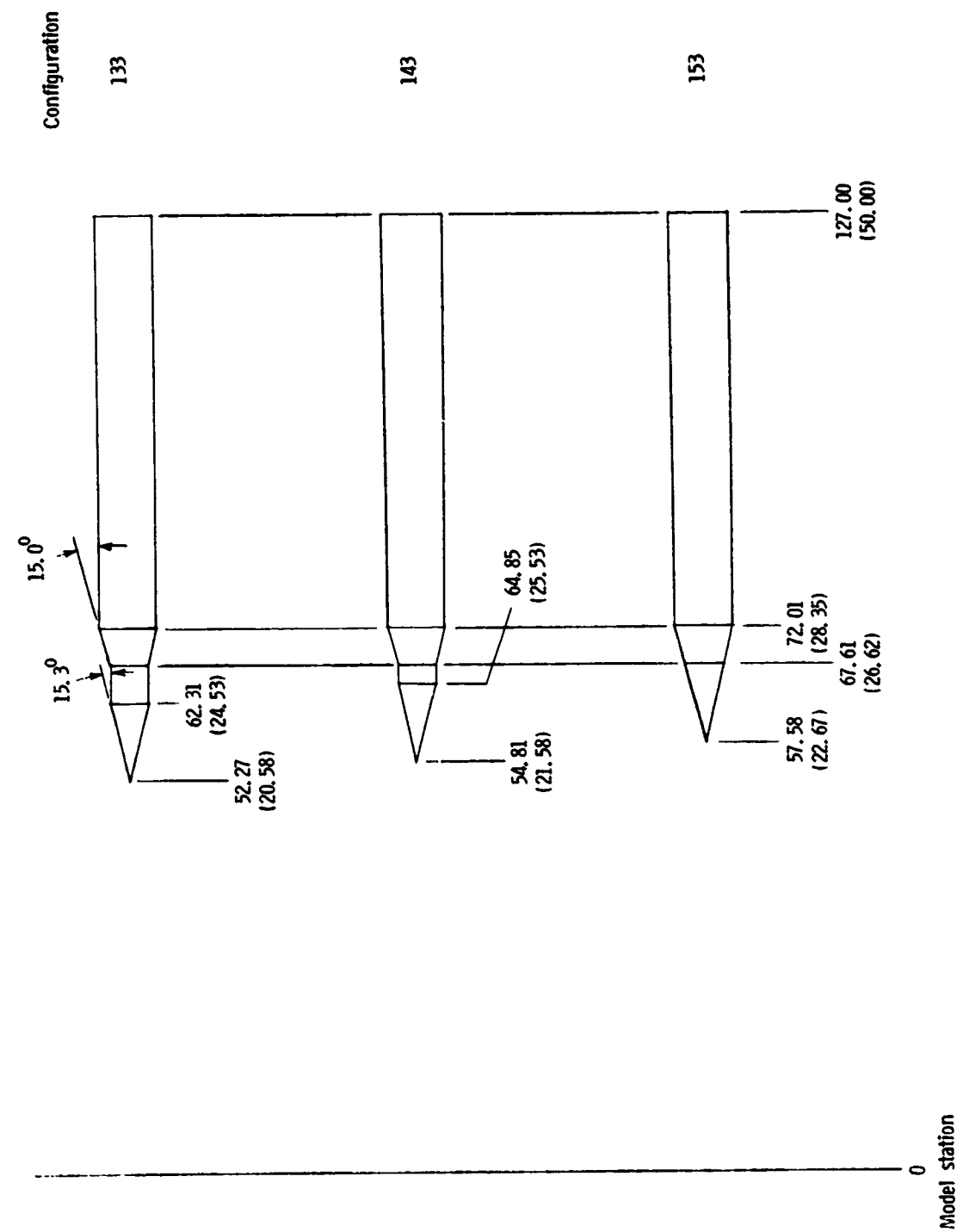
(d) Configurations 123, 223, and 323.

Figure 1.- Continued.



(e) Configurations 124 and 324.

Figure 1.- Continued.



(f) Configurations 133, 143, and 153.

Figure 1.- Concluded.

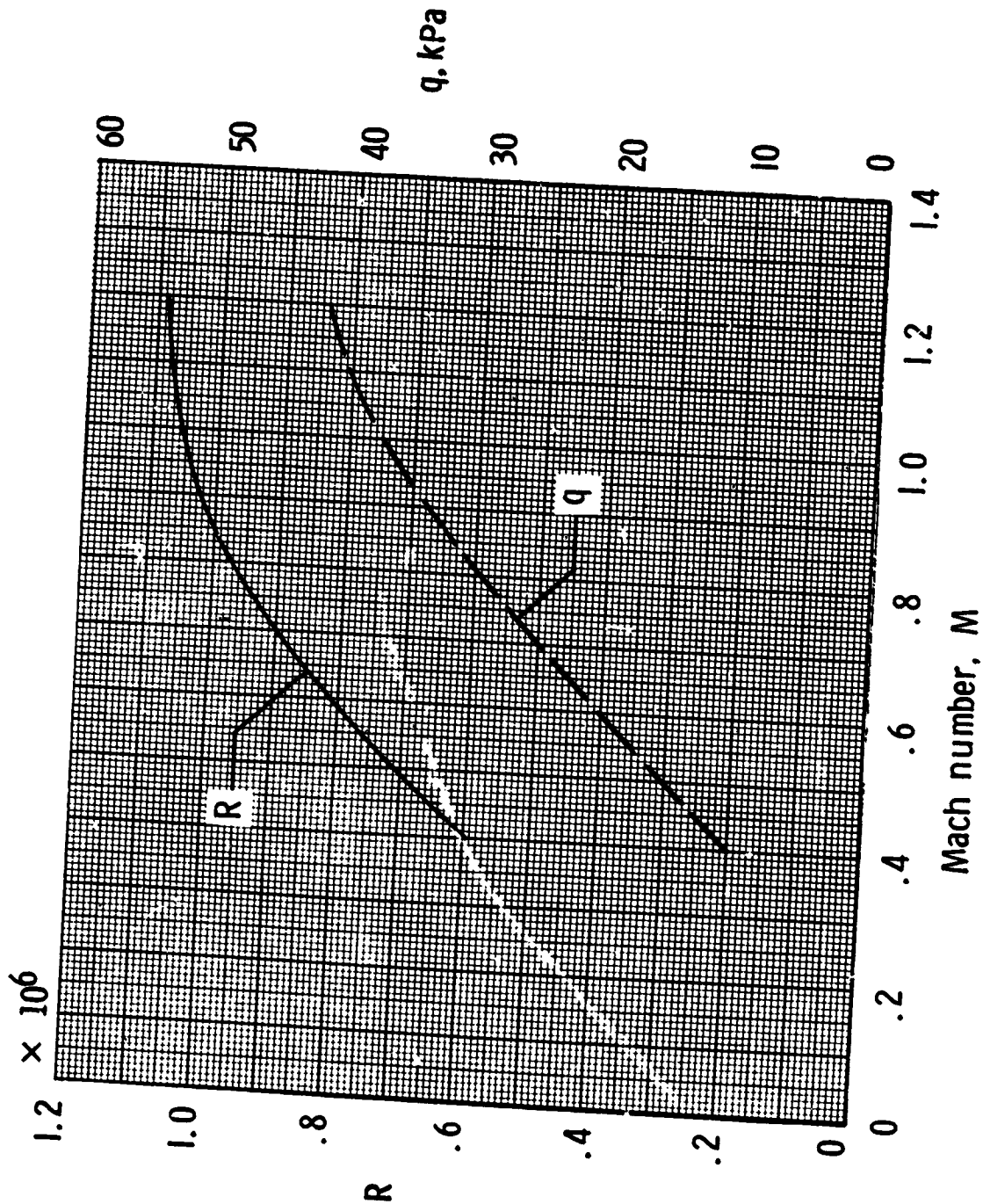
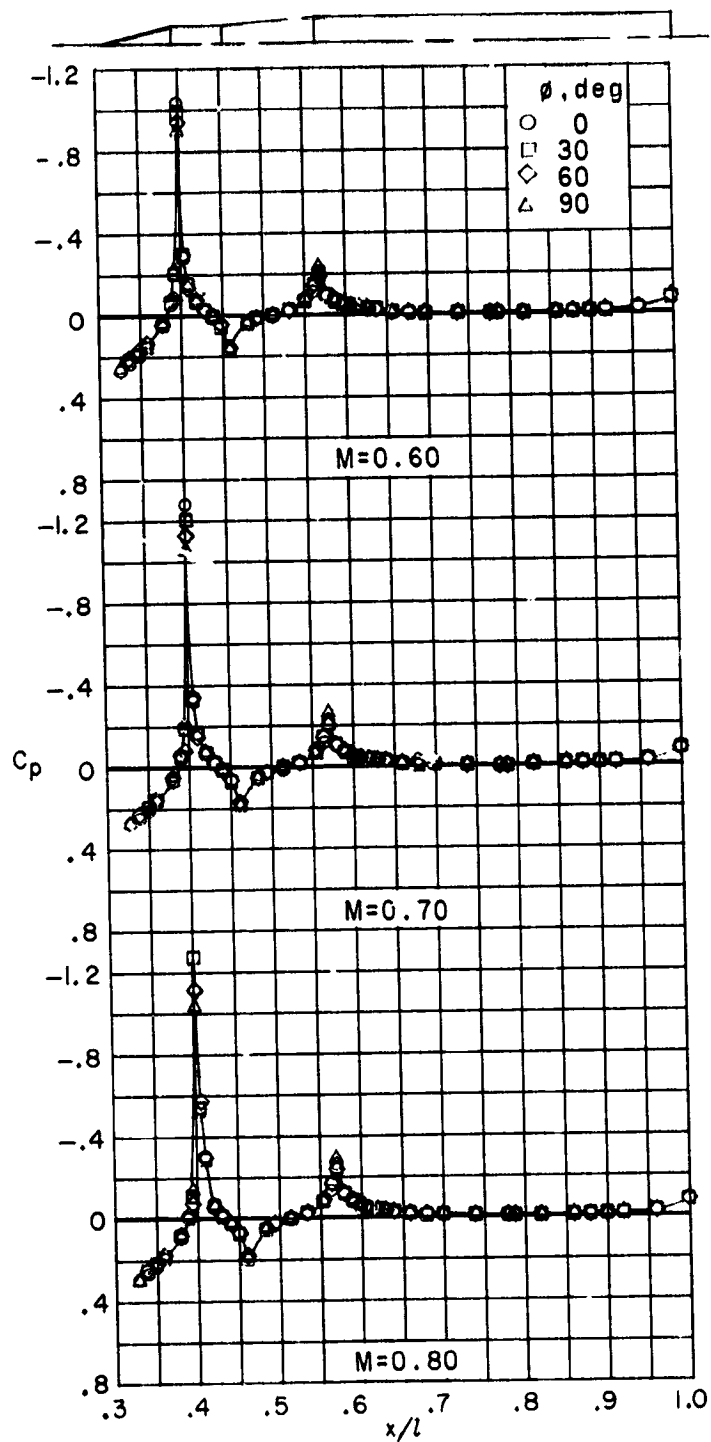


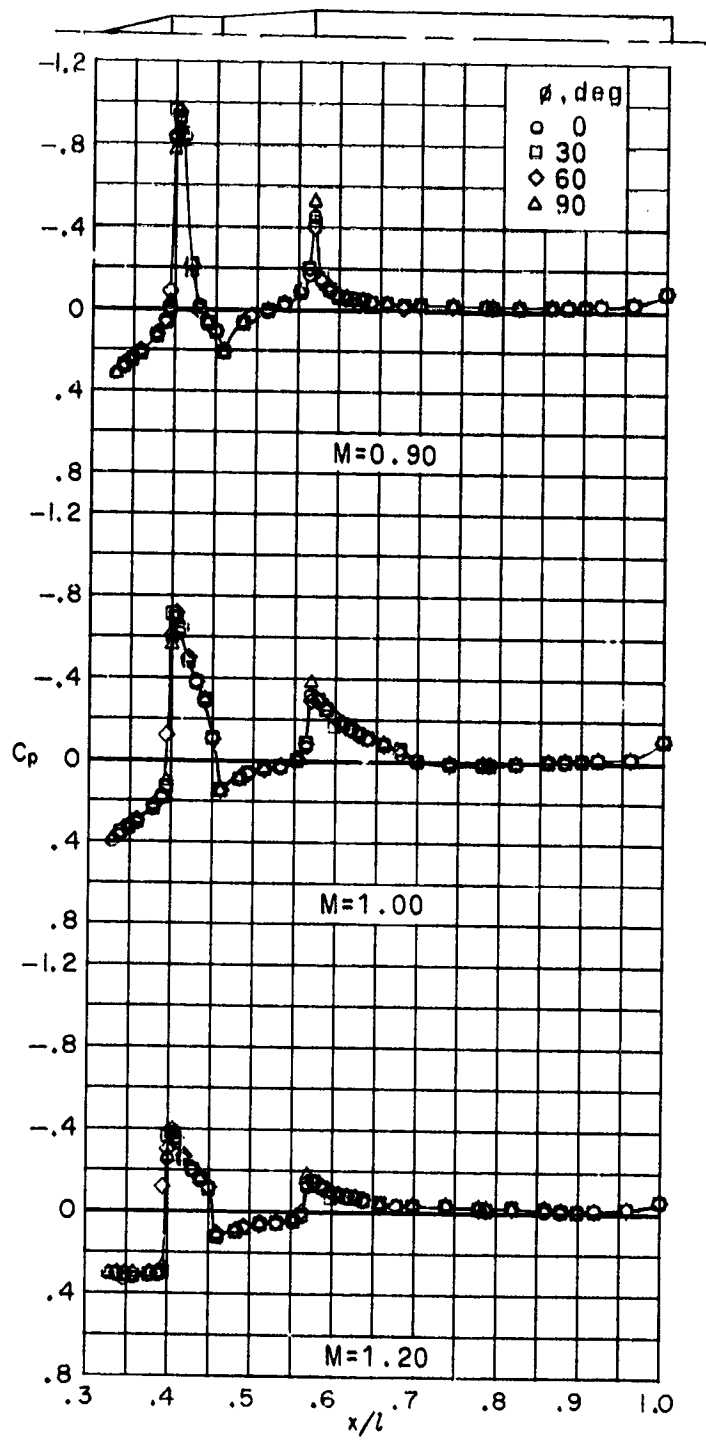
Figure 2.- Variation with Mach number of average test Reynolds number per meter and dynamic pressure.

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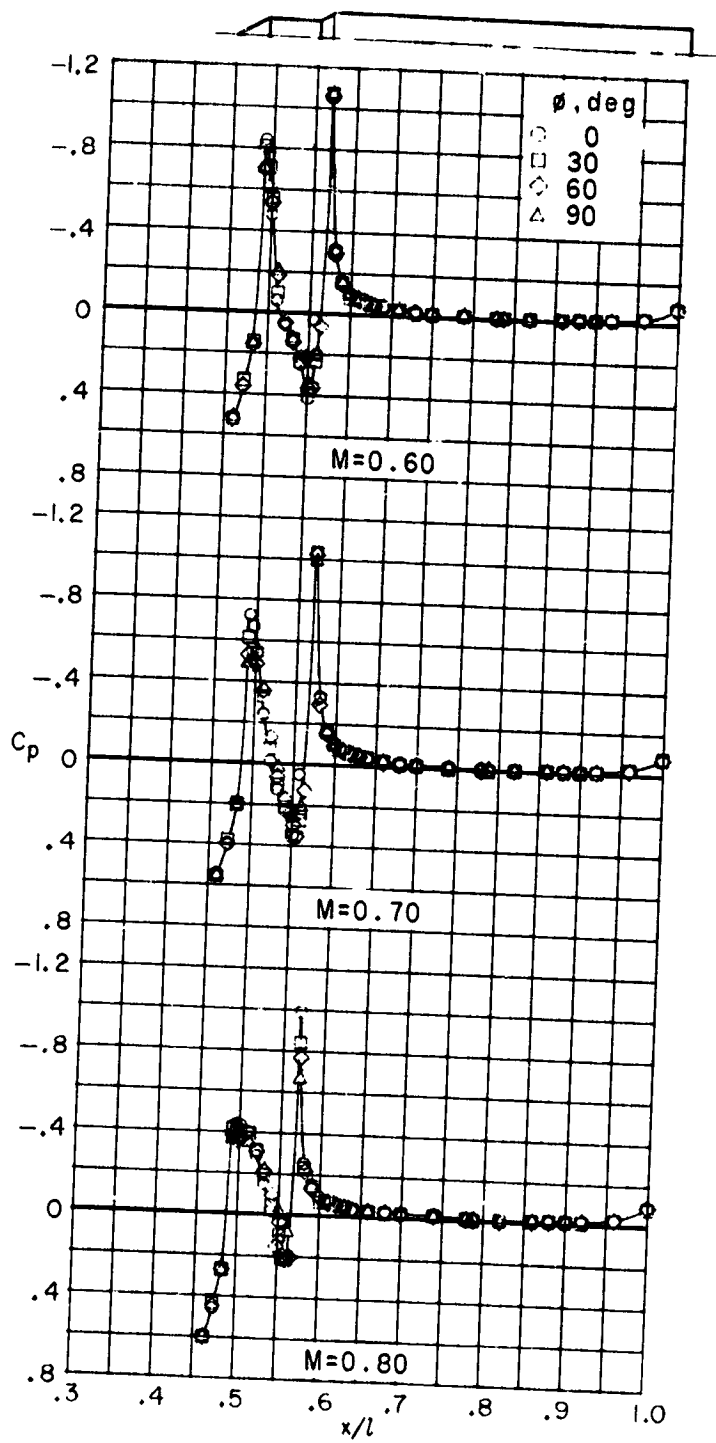
(a) Configuration 121, $\alpha = 0^\circ$.

Figure 3.- Comparison of surface pressure coefficients.



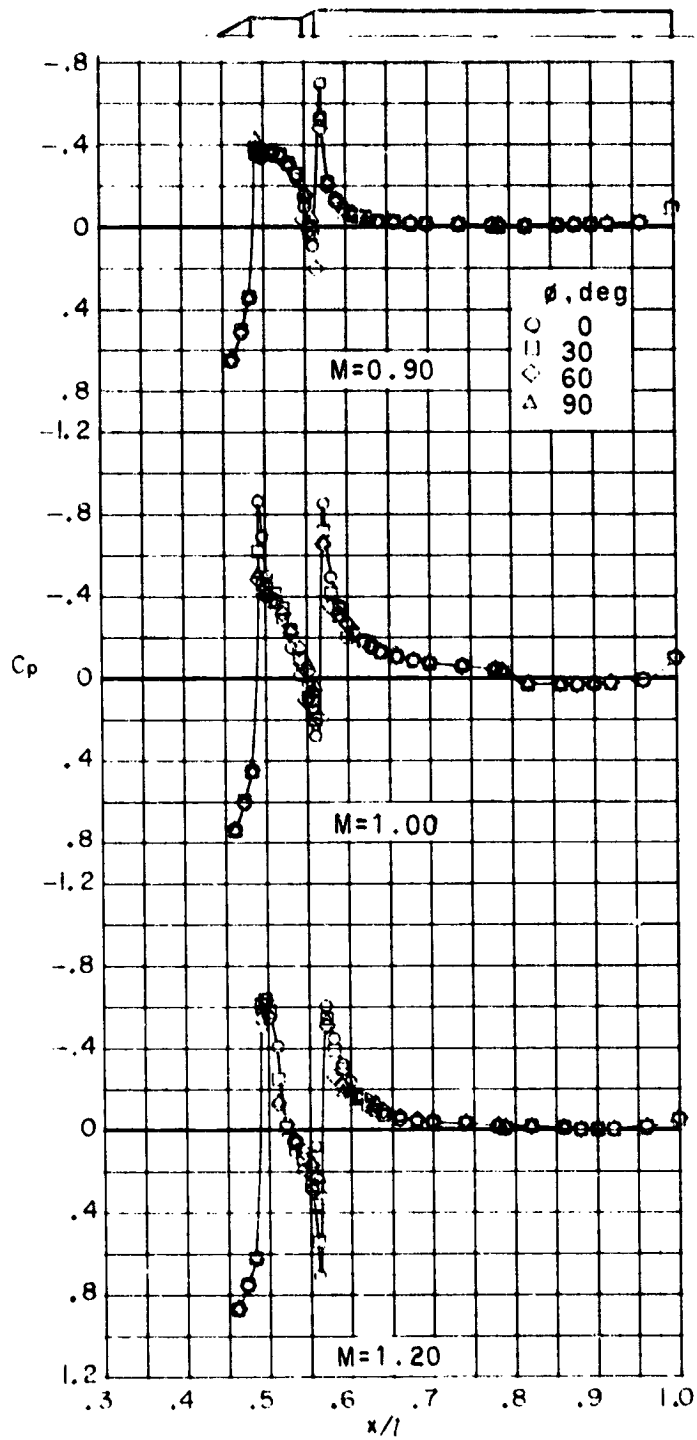
(a) Concluded.

Figure 3.- Continued.



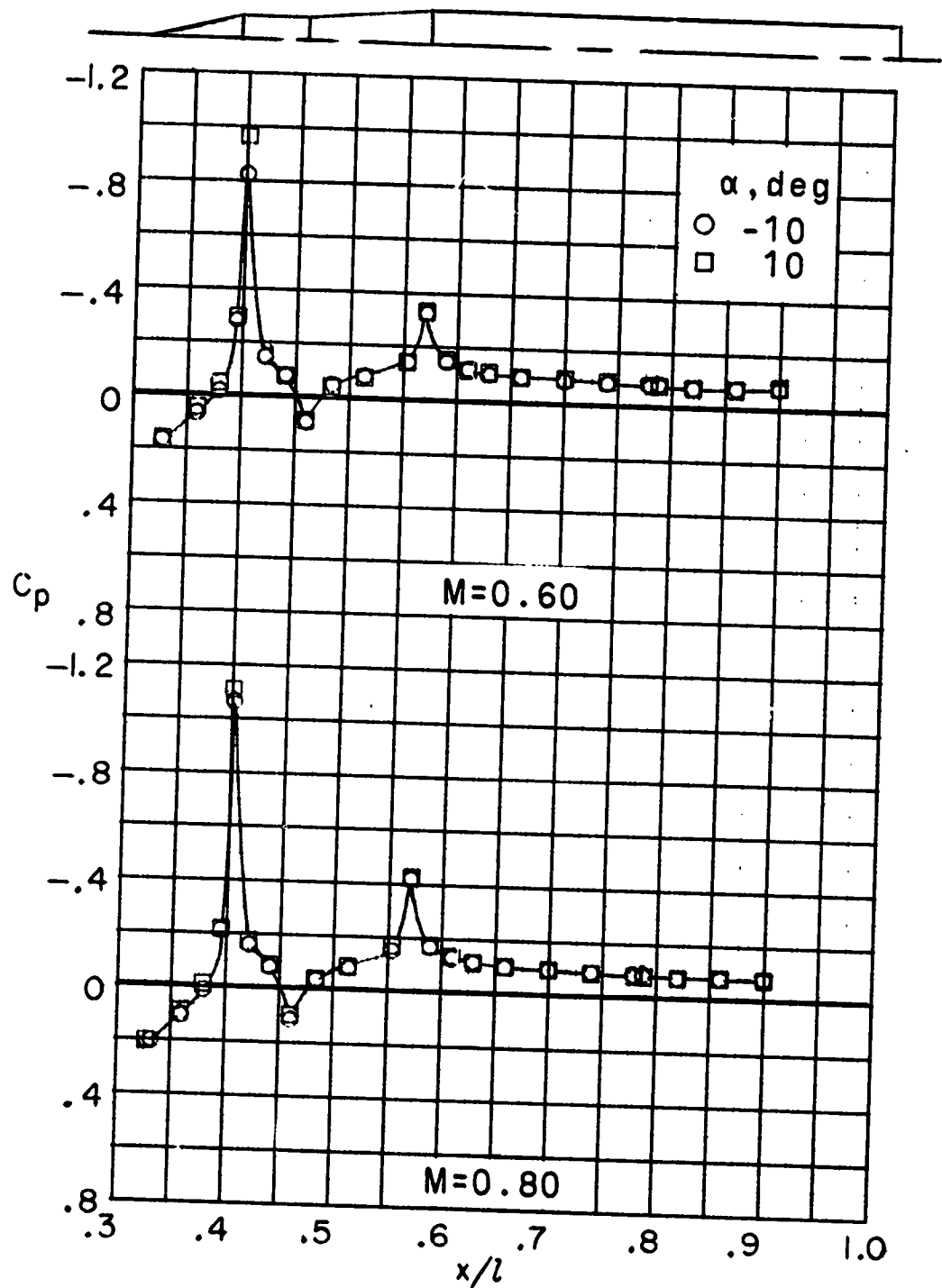
(b) Configuration 324, $\alpha = 0^\circ$.

Figure 3.- Continued.



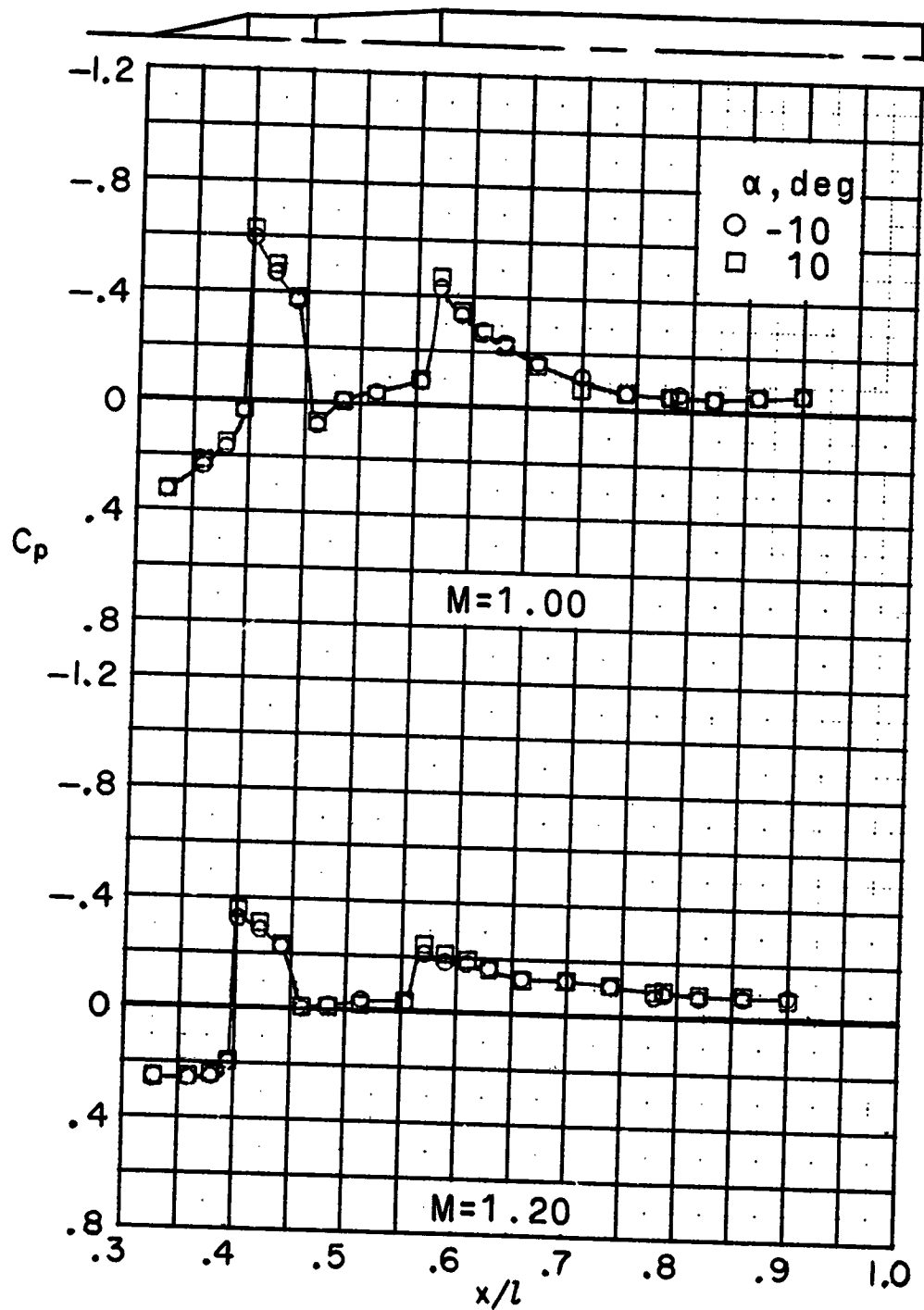
(b) Concluded.

Figure 3.- Continued.



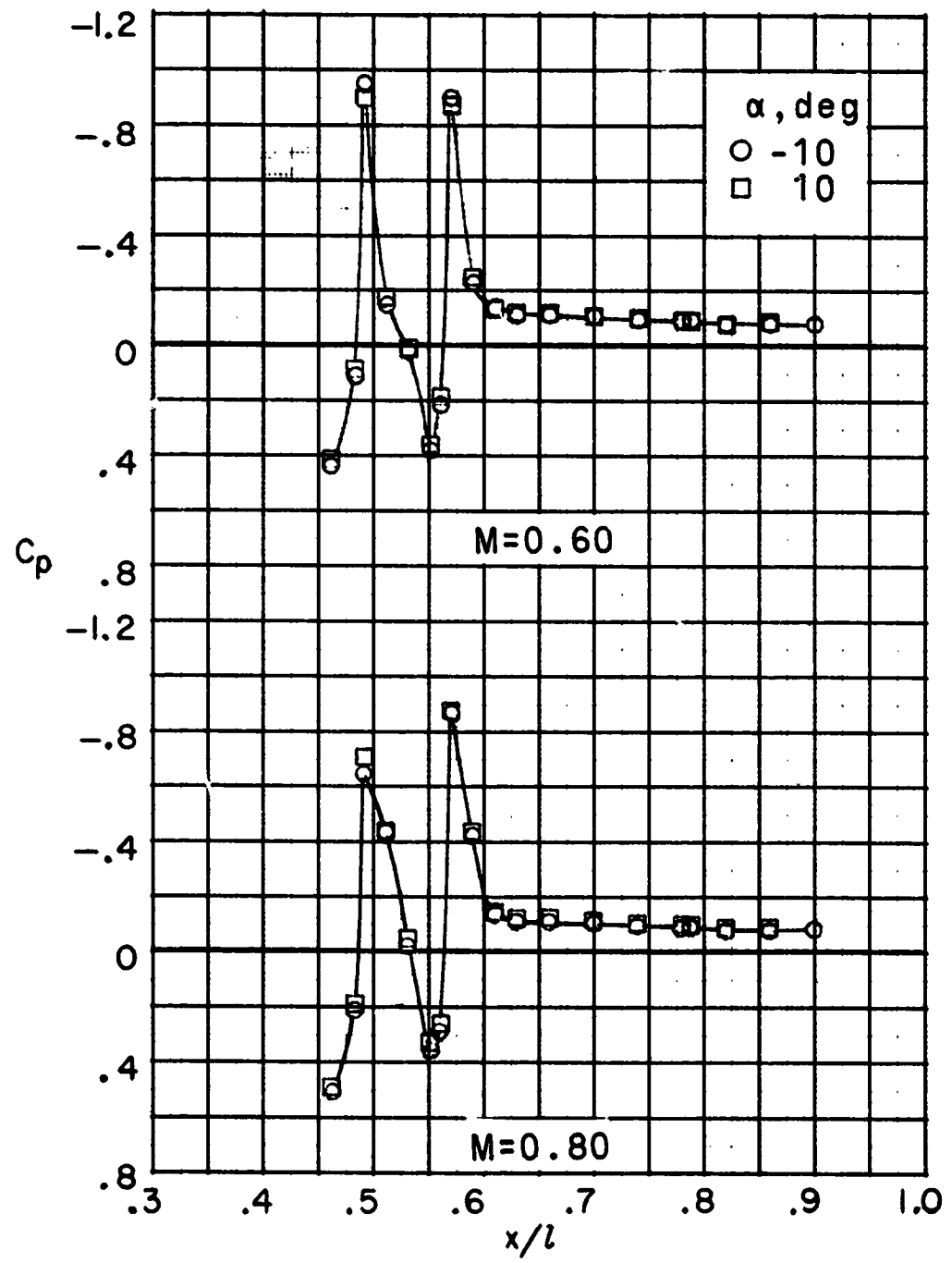
(c) Configuration 121, $\alpha = \pm 10^\circ$.

Figure 3.- Continued.



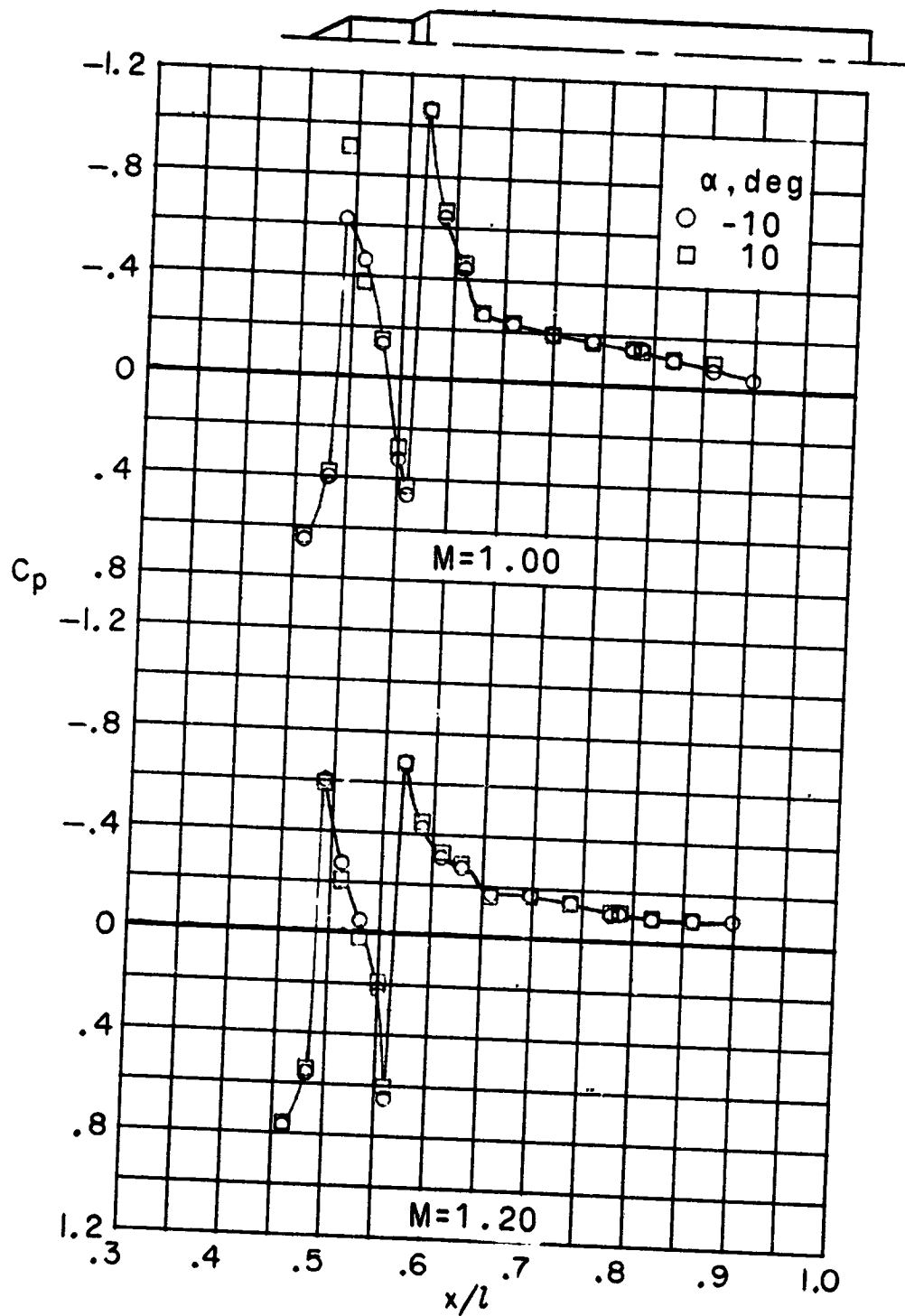
(c) Concluded.

Figure 3.- Continued.



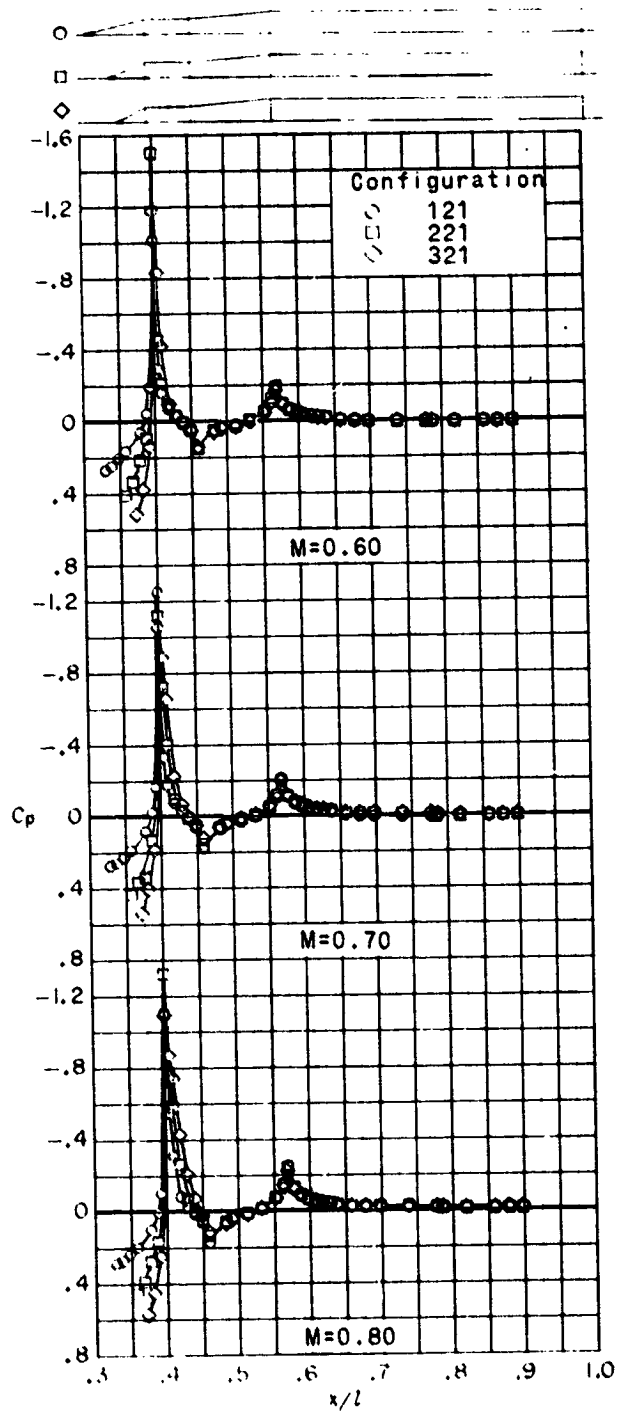
(d) Configuration 324, $\alpha = \pm 10^\circ$.

Figure 3.- Continued.



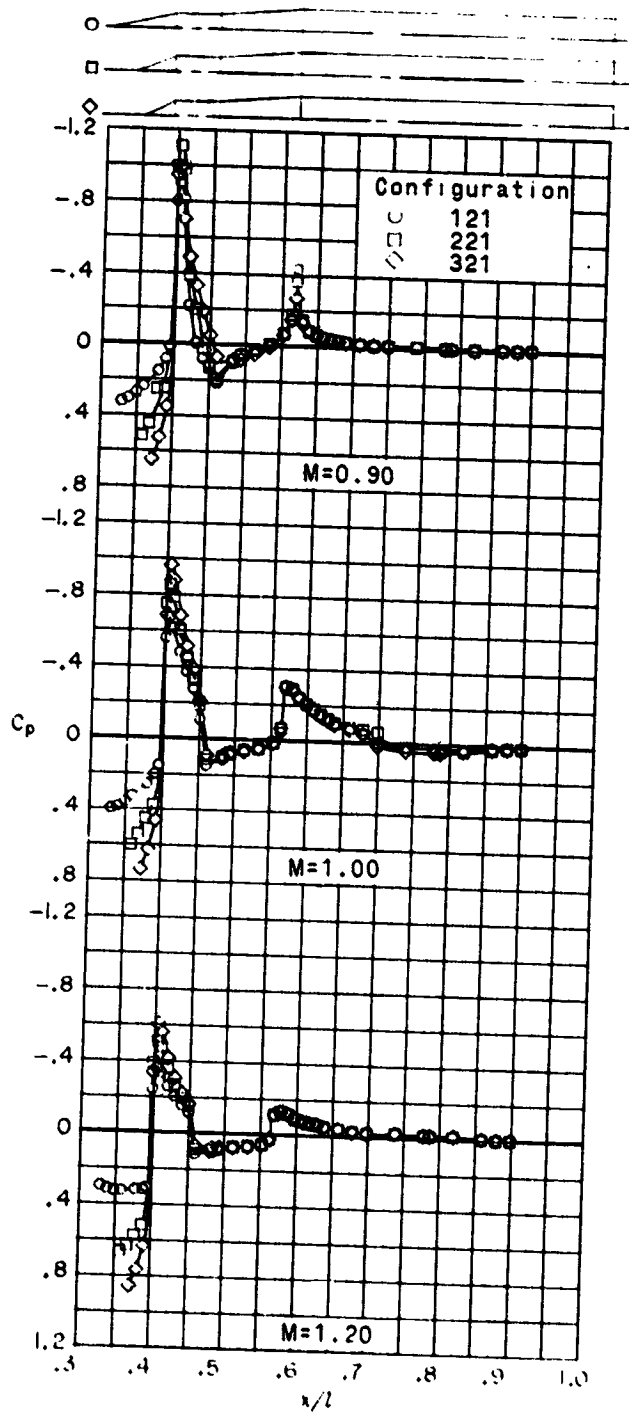
(d) Concluded.

Figure 3.- Concluded.



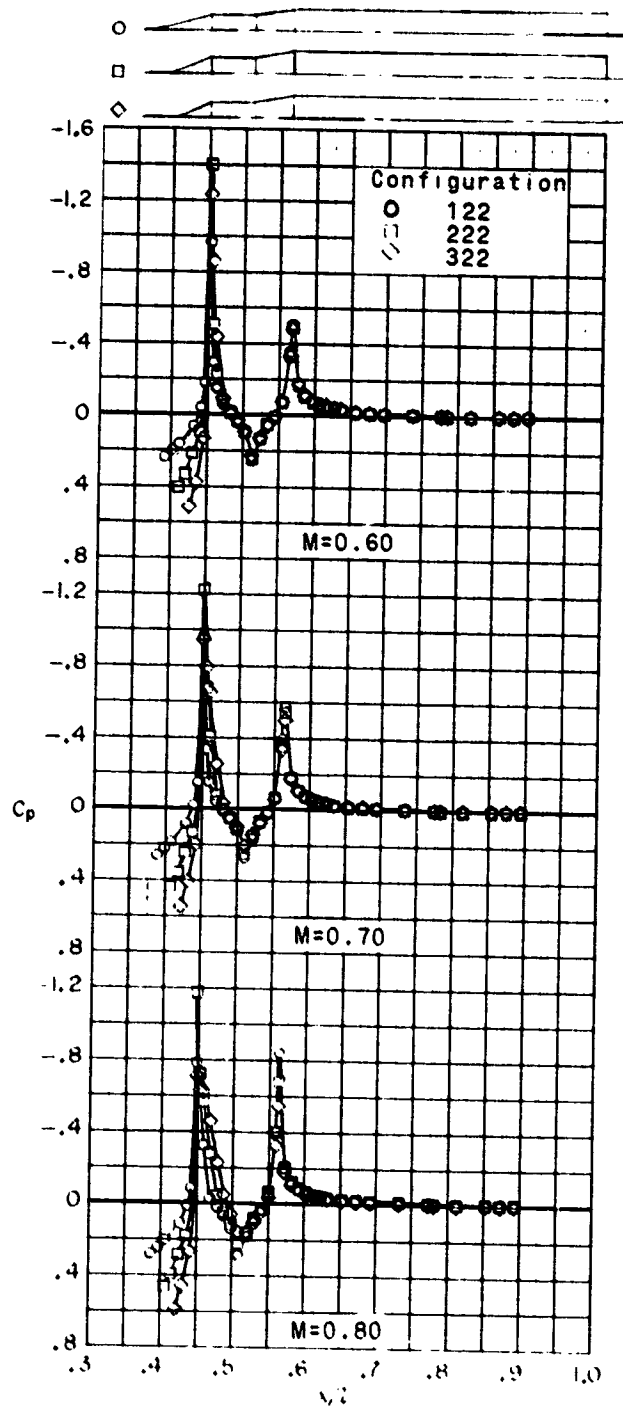
(a) $\delta_F = 5^\circ$.

Figure 4.- Effects of variation in nose-cone angle for $\phi = 0^\circ$ and $\alpha = 0^\circ$.



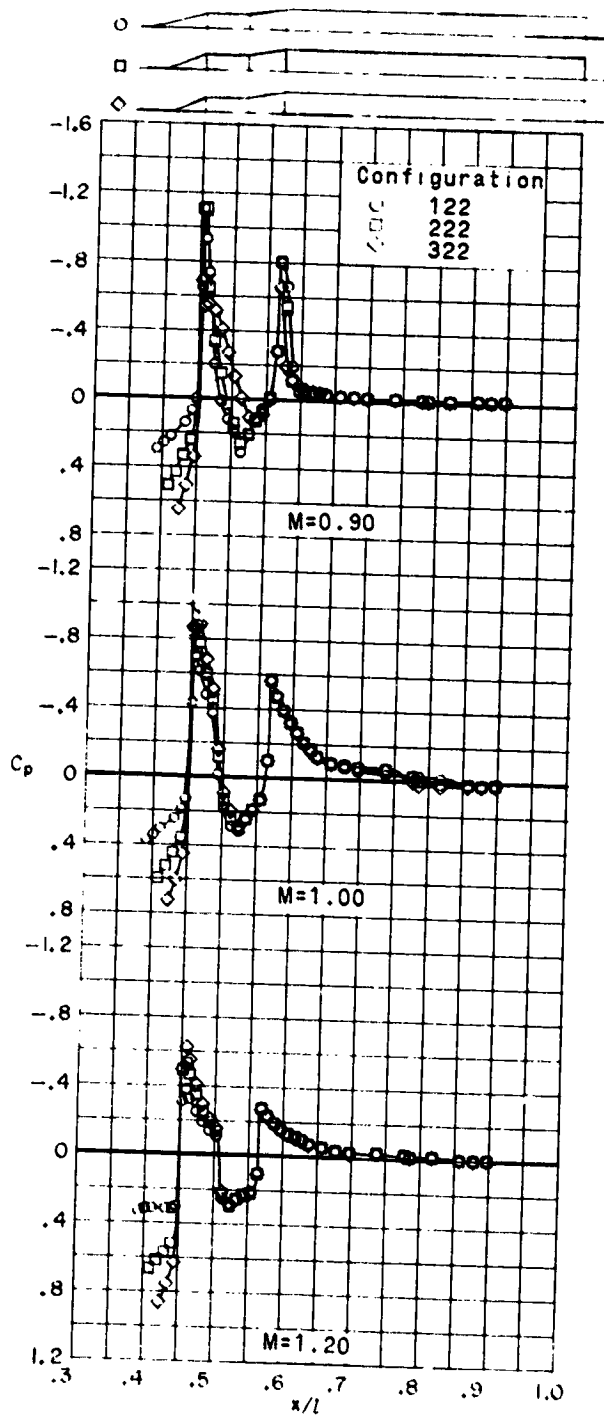
(a) Concluded.

Figure 4.- Continued.



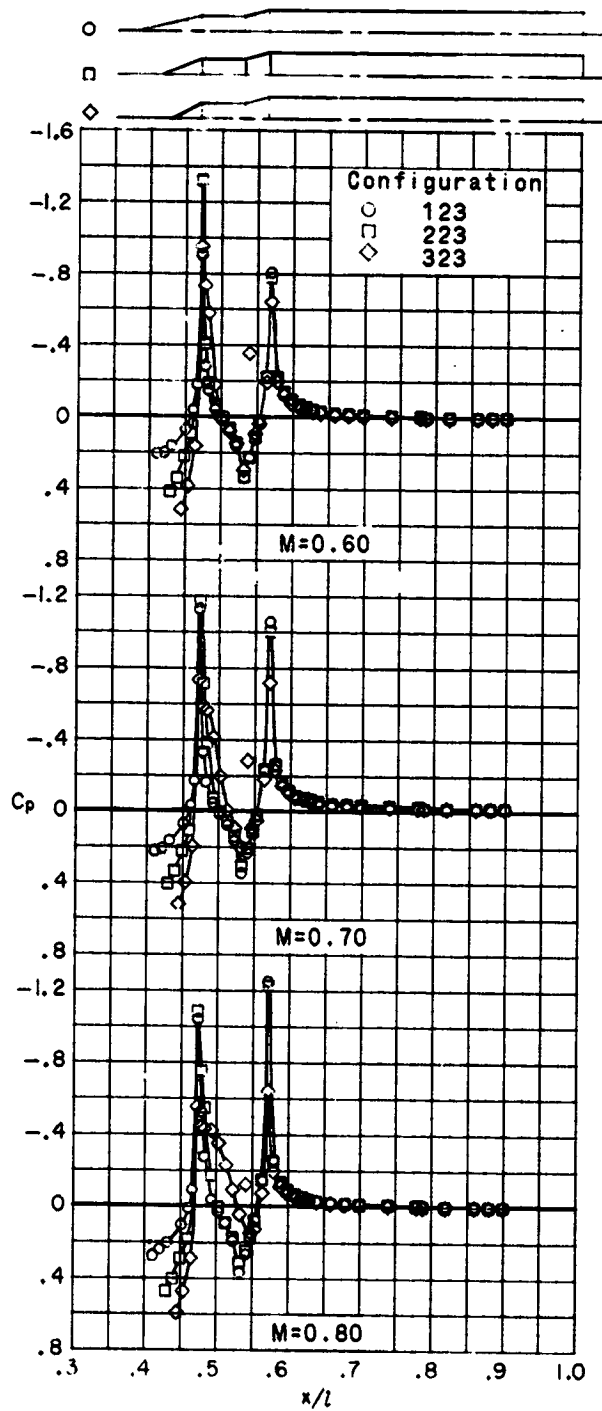
(b) $\delta_F = 10.1^\circ$.

Figure 4.- Continued.



(b) Concluded.

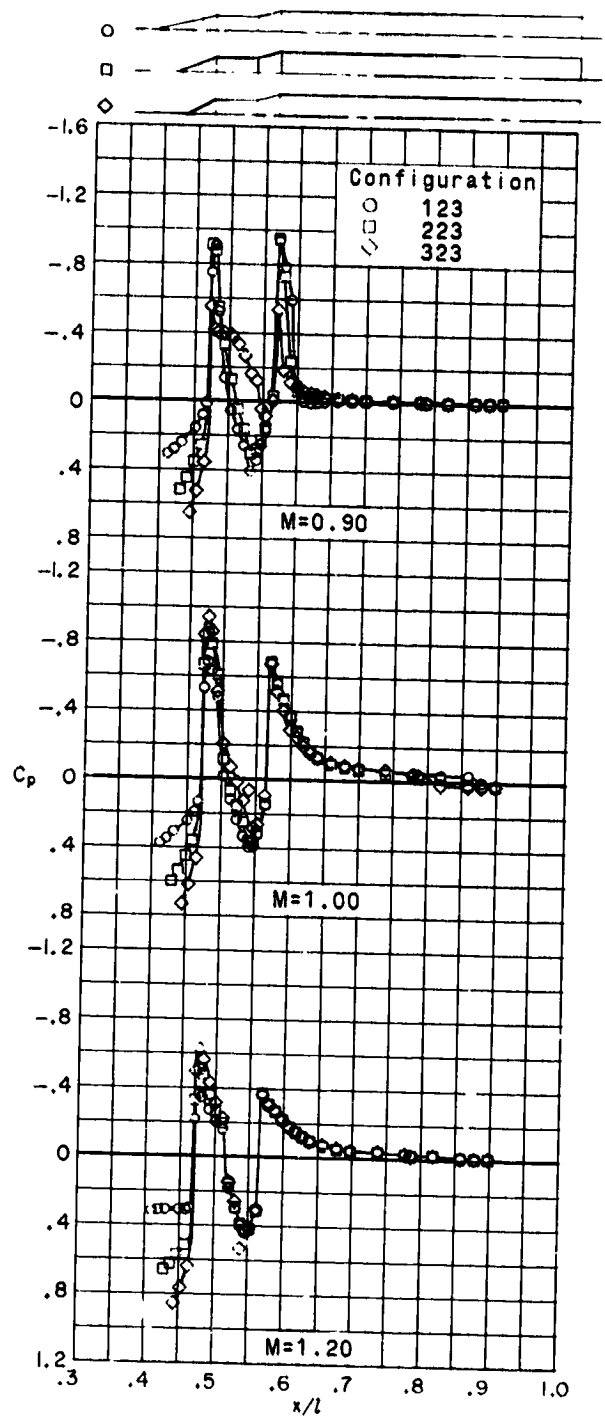
Figure 4.- Continued.



(c) $\delta_F = 15^\circ$.

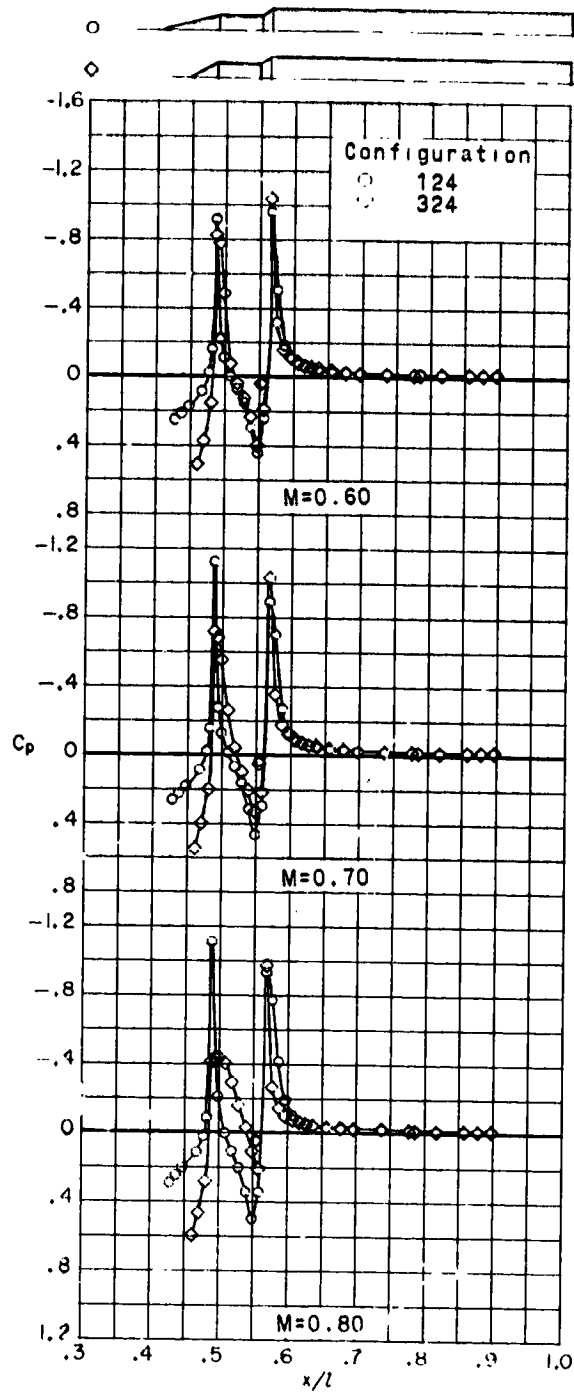
Figure 4.- Continued.

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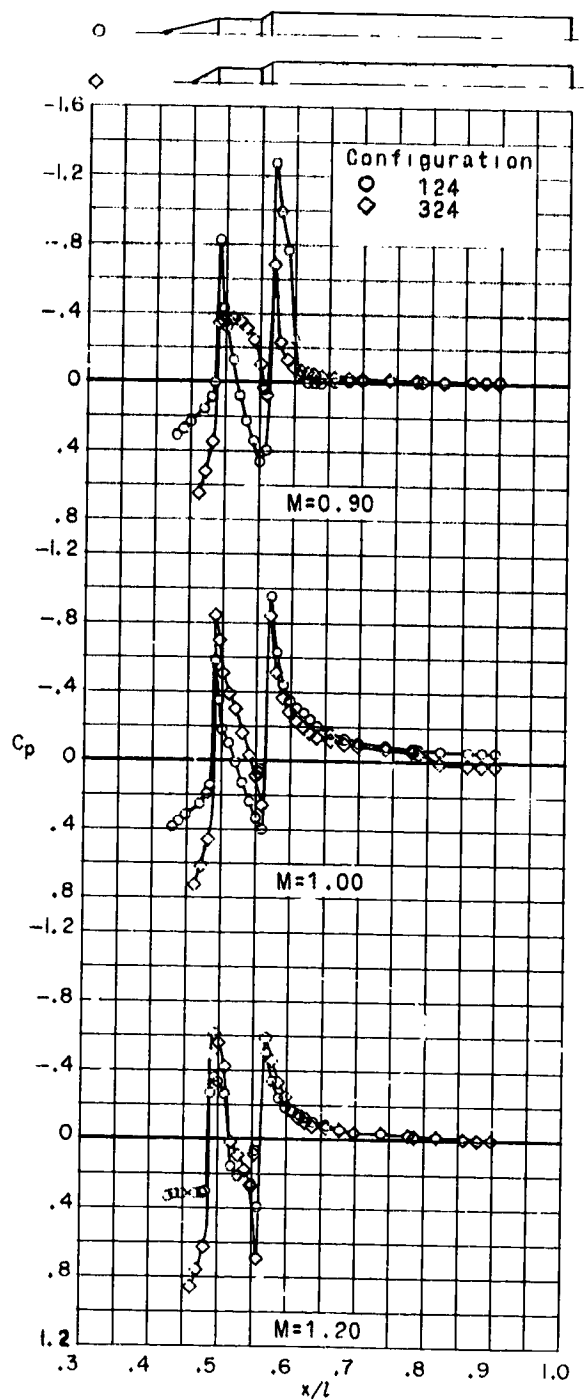
(c) Concluded.

Figure 4.- Continued.



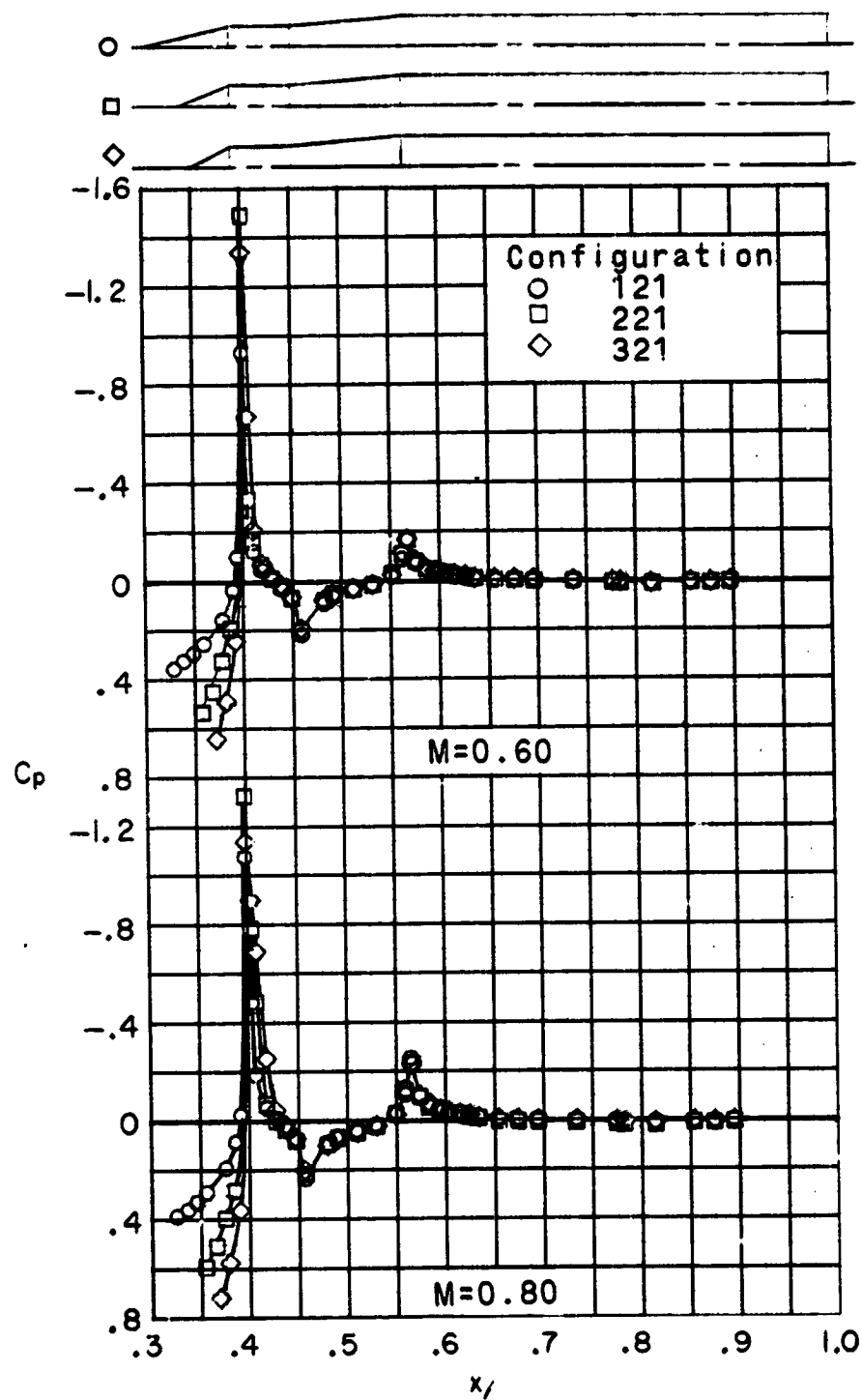
(d) $\delta_p = 30^\circ$.

Figure 4.- Continued.



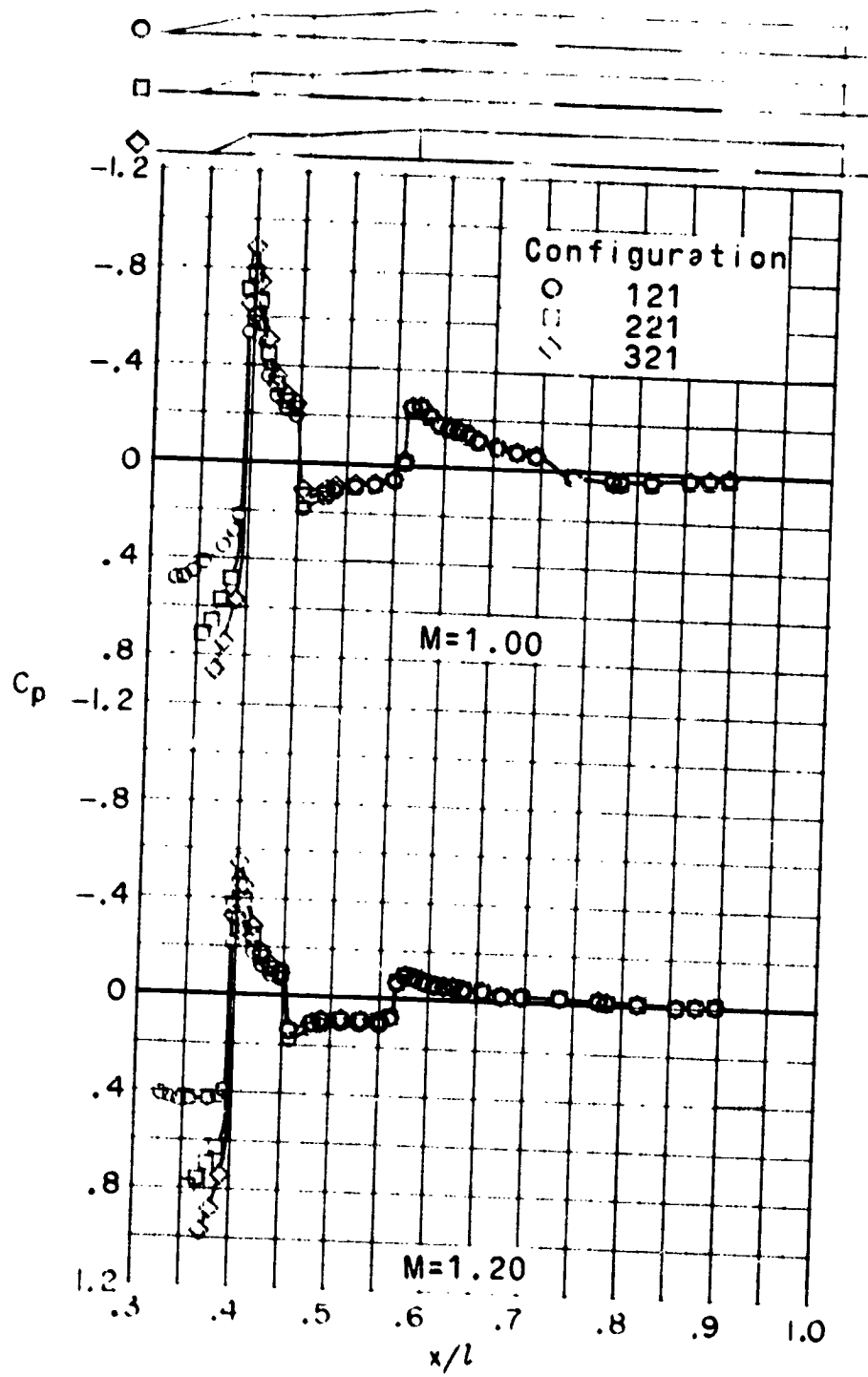
(d) Concluded.

Figure 4.- Concluded.



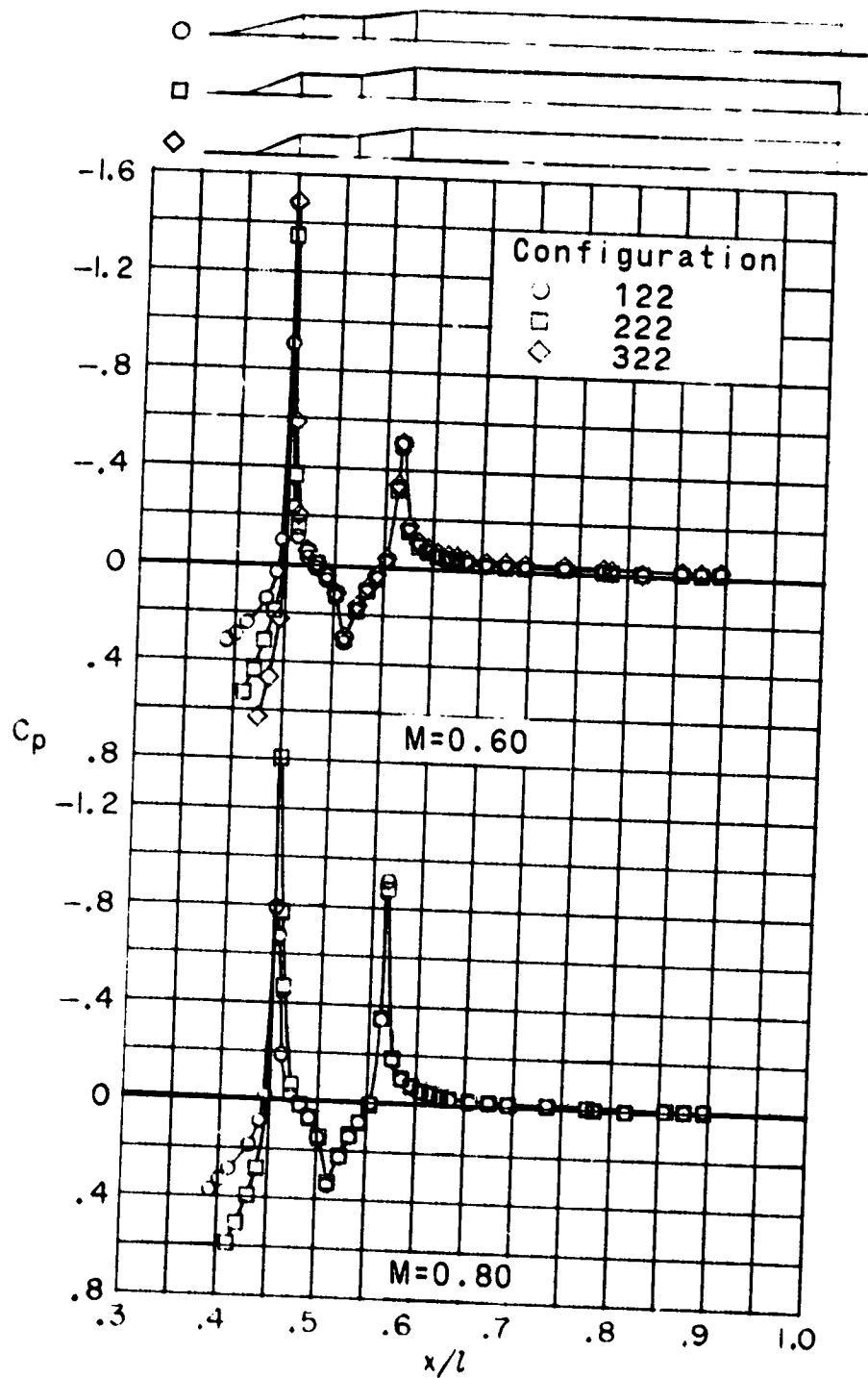
(a) $\delta_F = 5^\circ$.

Figure 5.- Effects of variation in nose-cone angle for $\phi = 0^\circ$ and $\alpha = -6^\circ$.



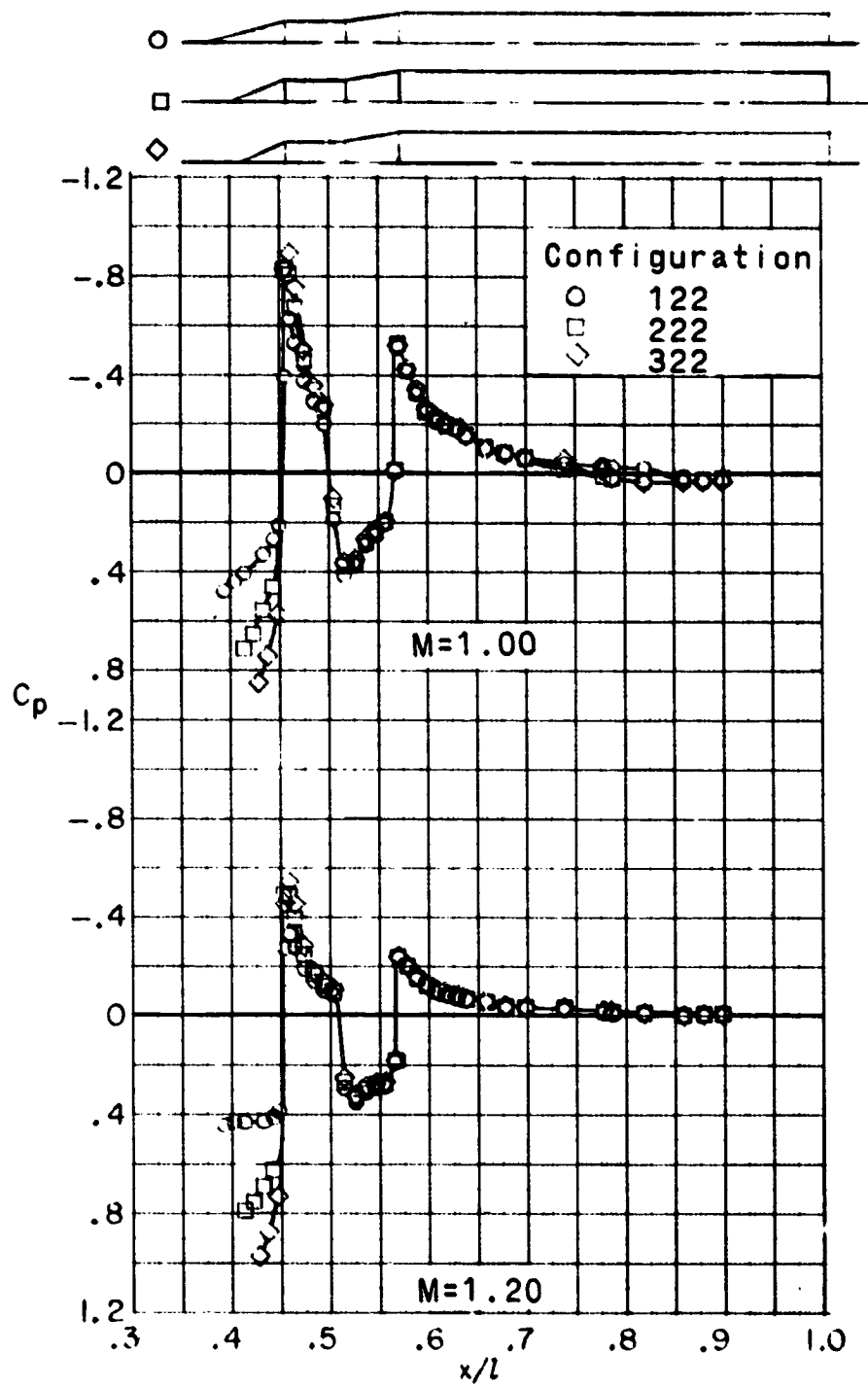
(a) Concluded.

Figure 5.- Continued.



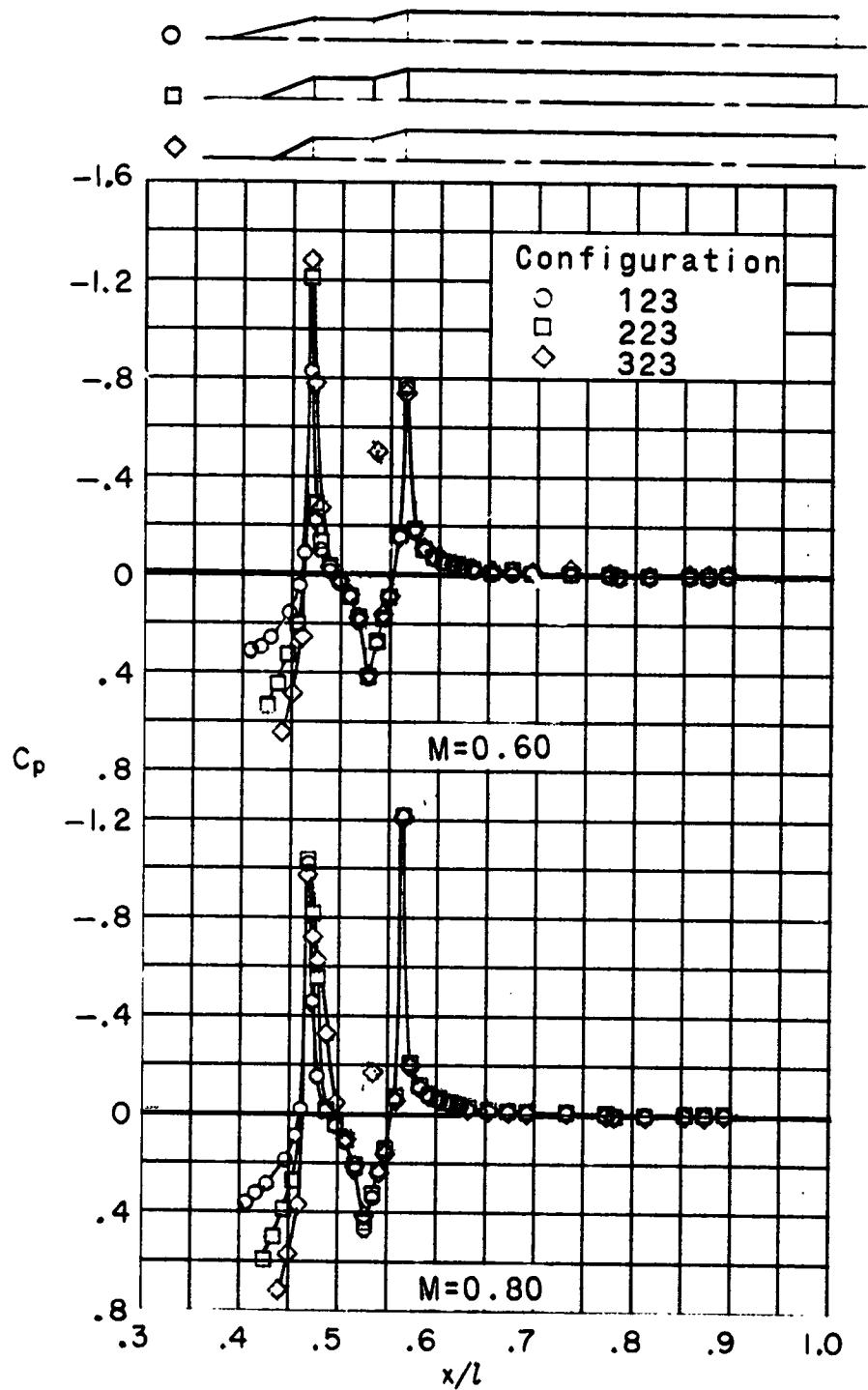
(b) $\delta_F = 10.1^\circ$.

Figure 5.- Continued.



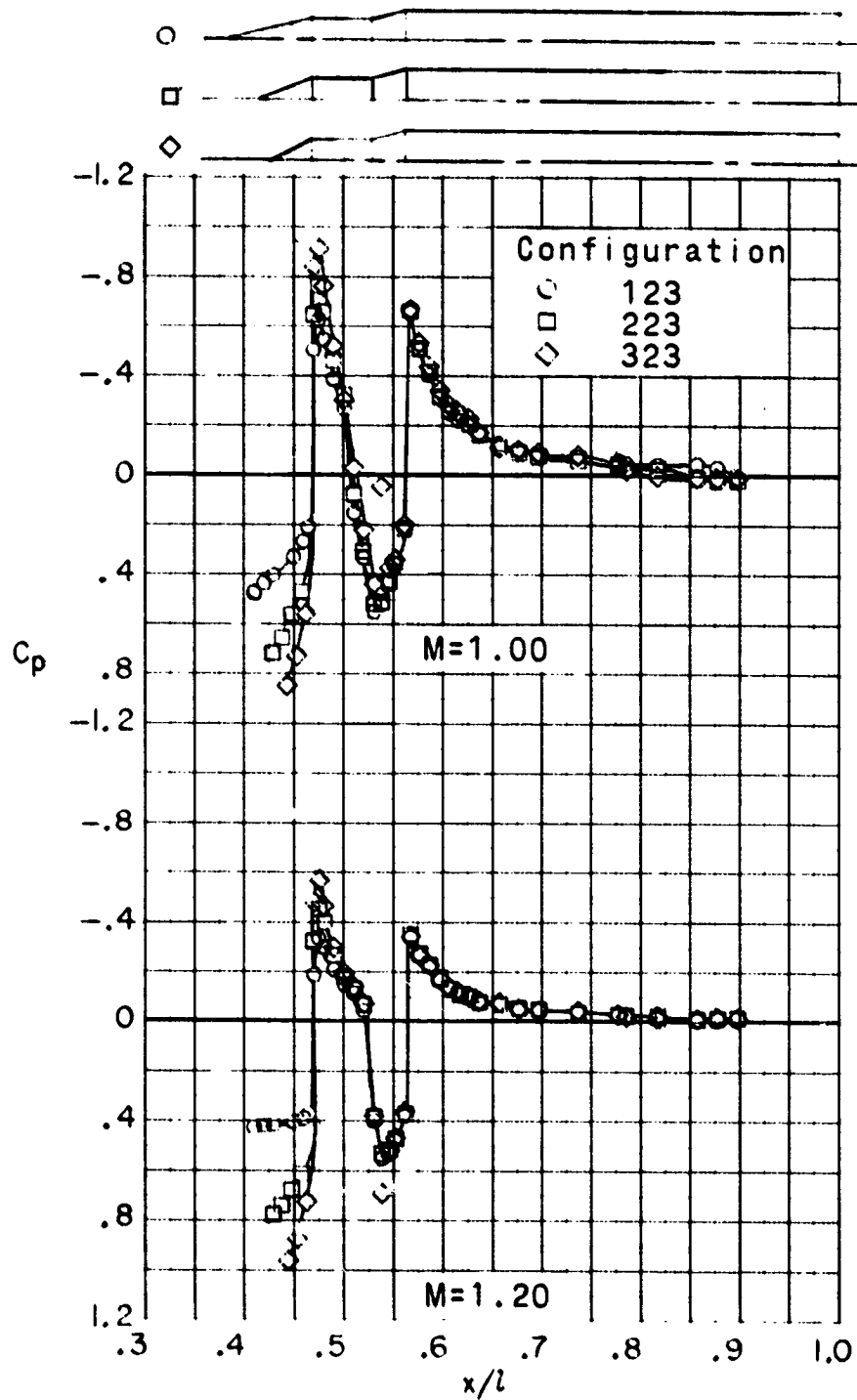
(b) Concluded.

Figure 5.- Continued.



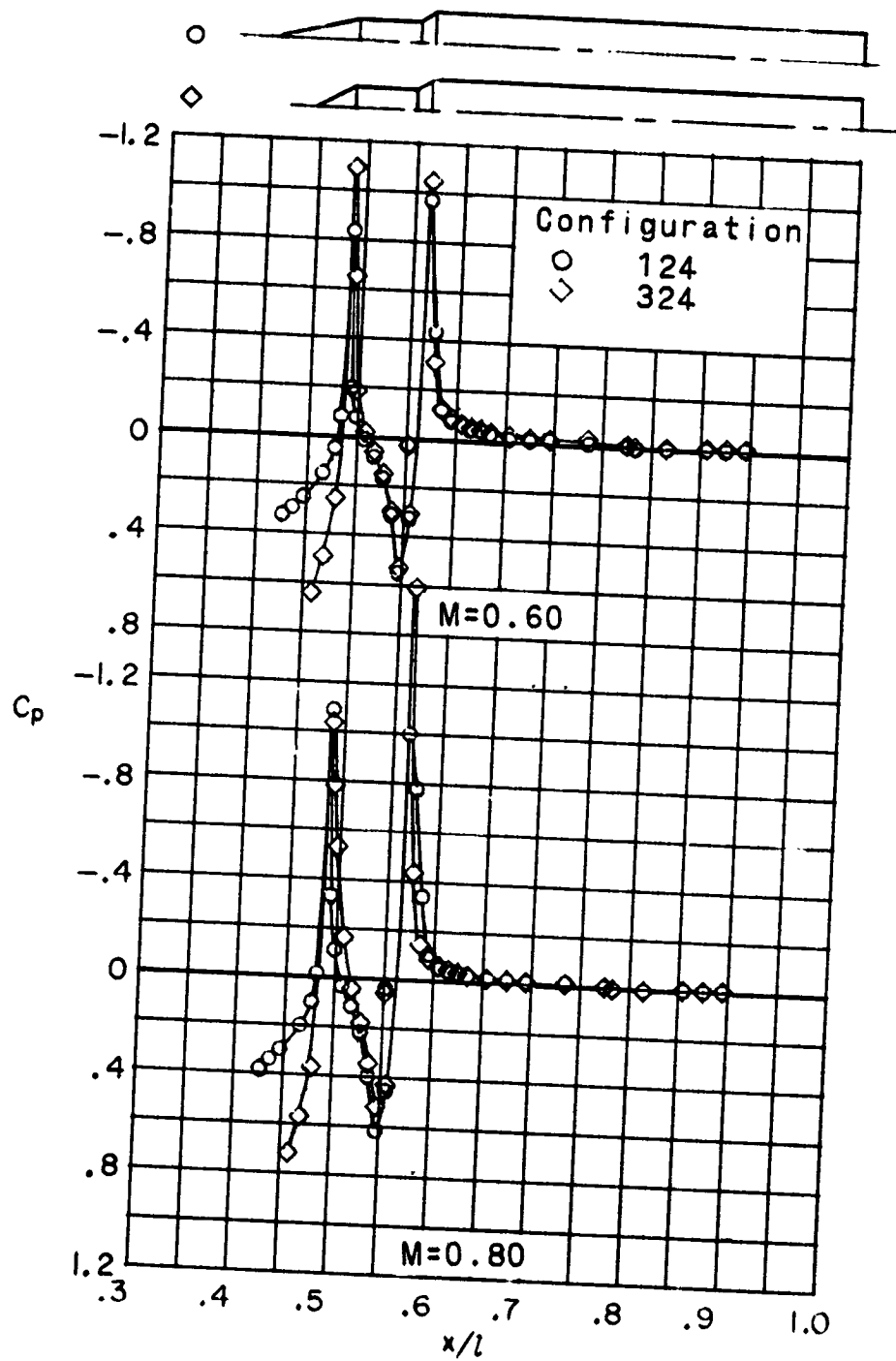
(c) $\delta_F = 15^\circ$.

Figure 5.- Continued.



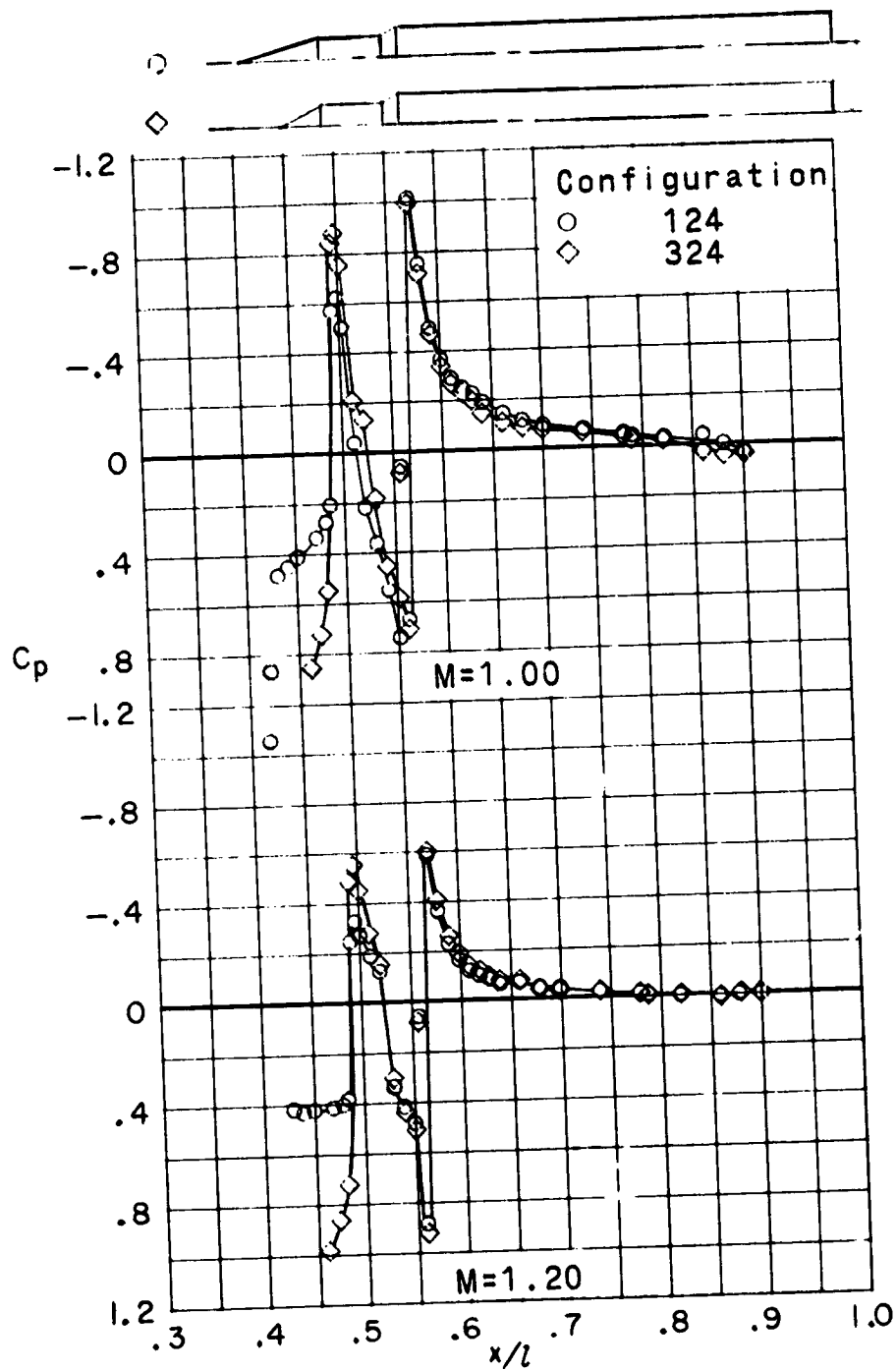
(c) Concluded.

Figure 5.- Continued.



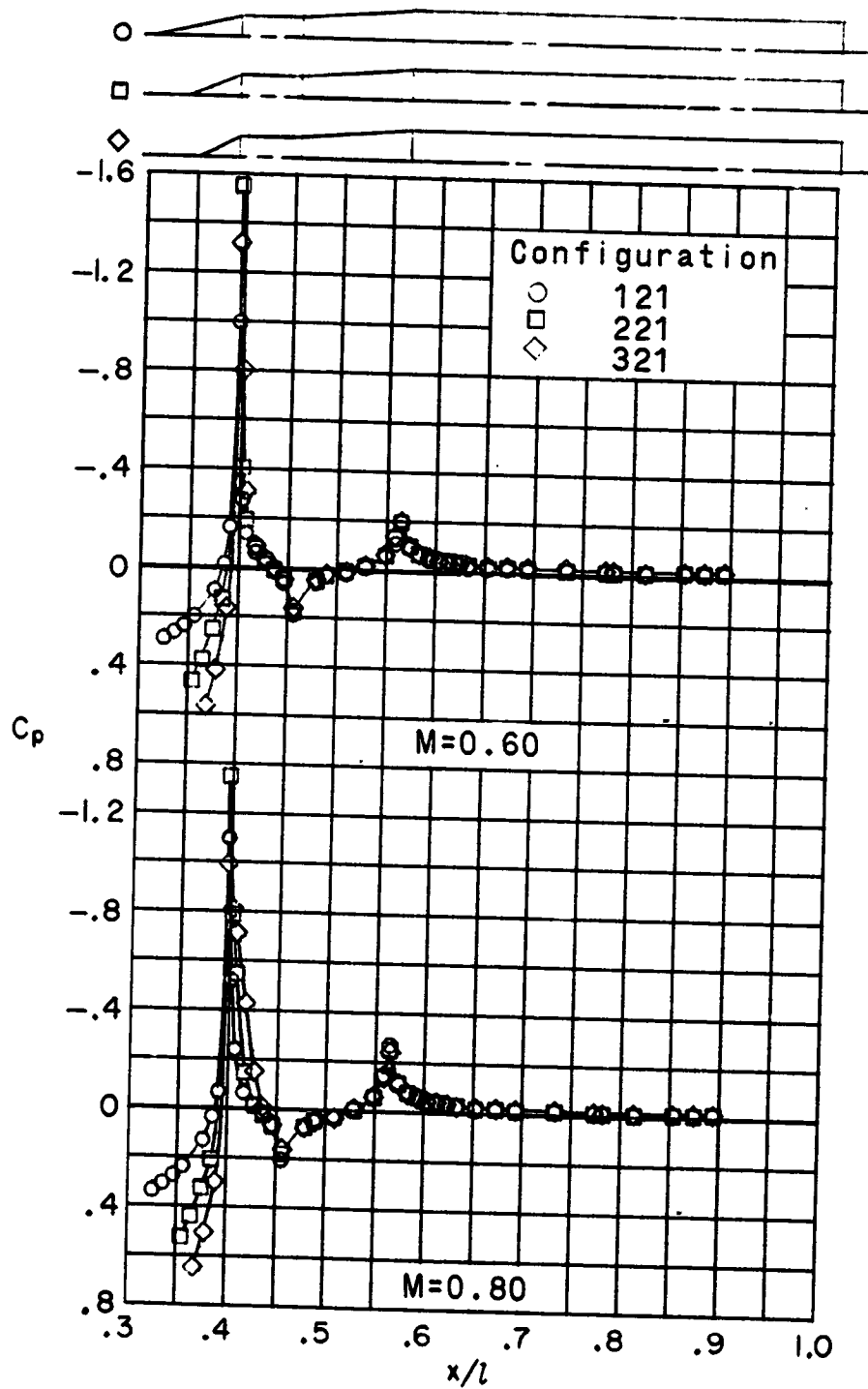
(d) $\delta_F = 30^\circ$.

Figure 5.- Continued.



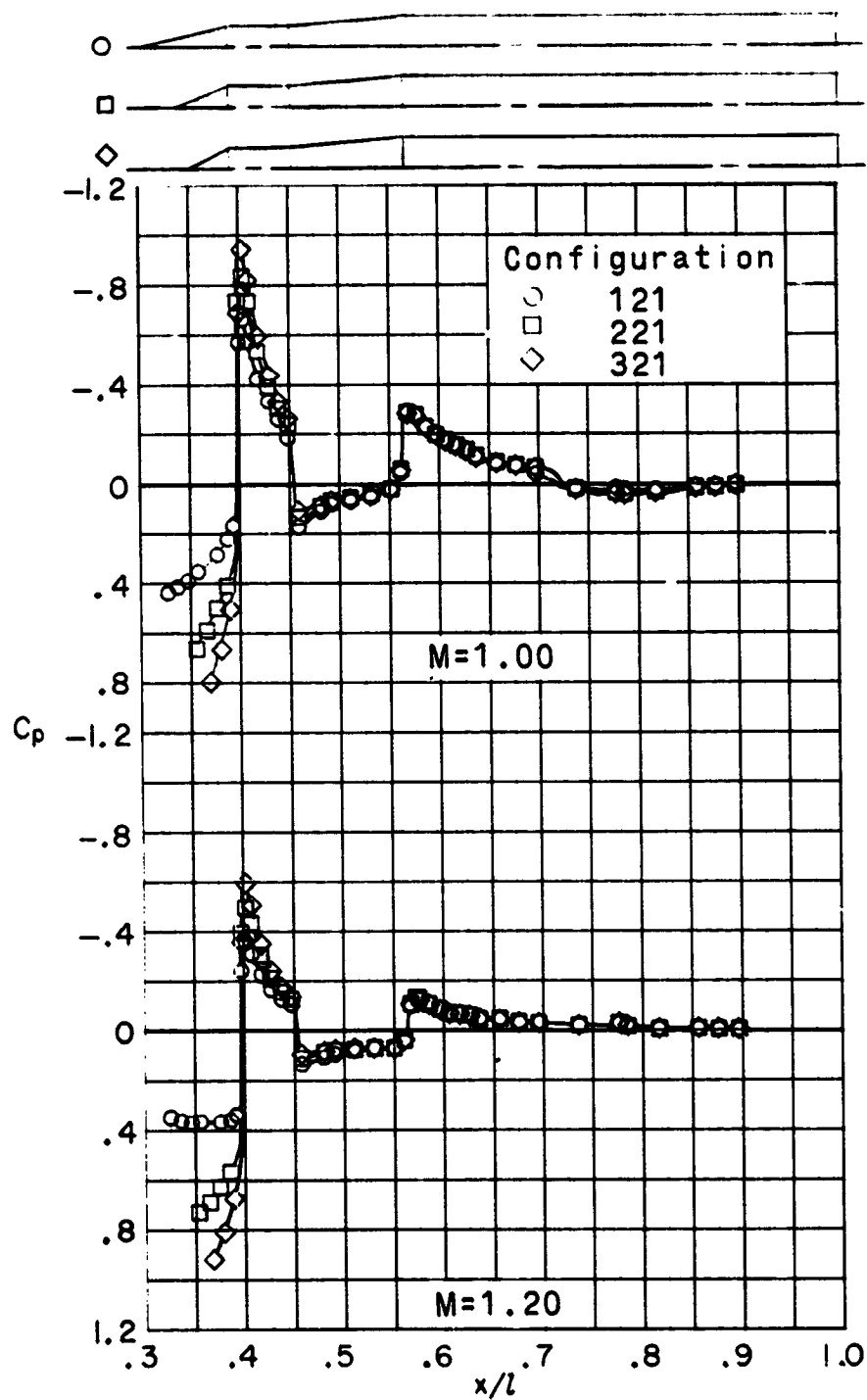
(d) Concluded.

Figure 5.- Concluded.



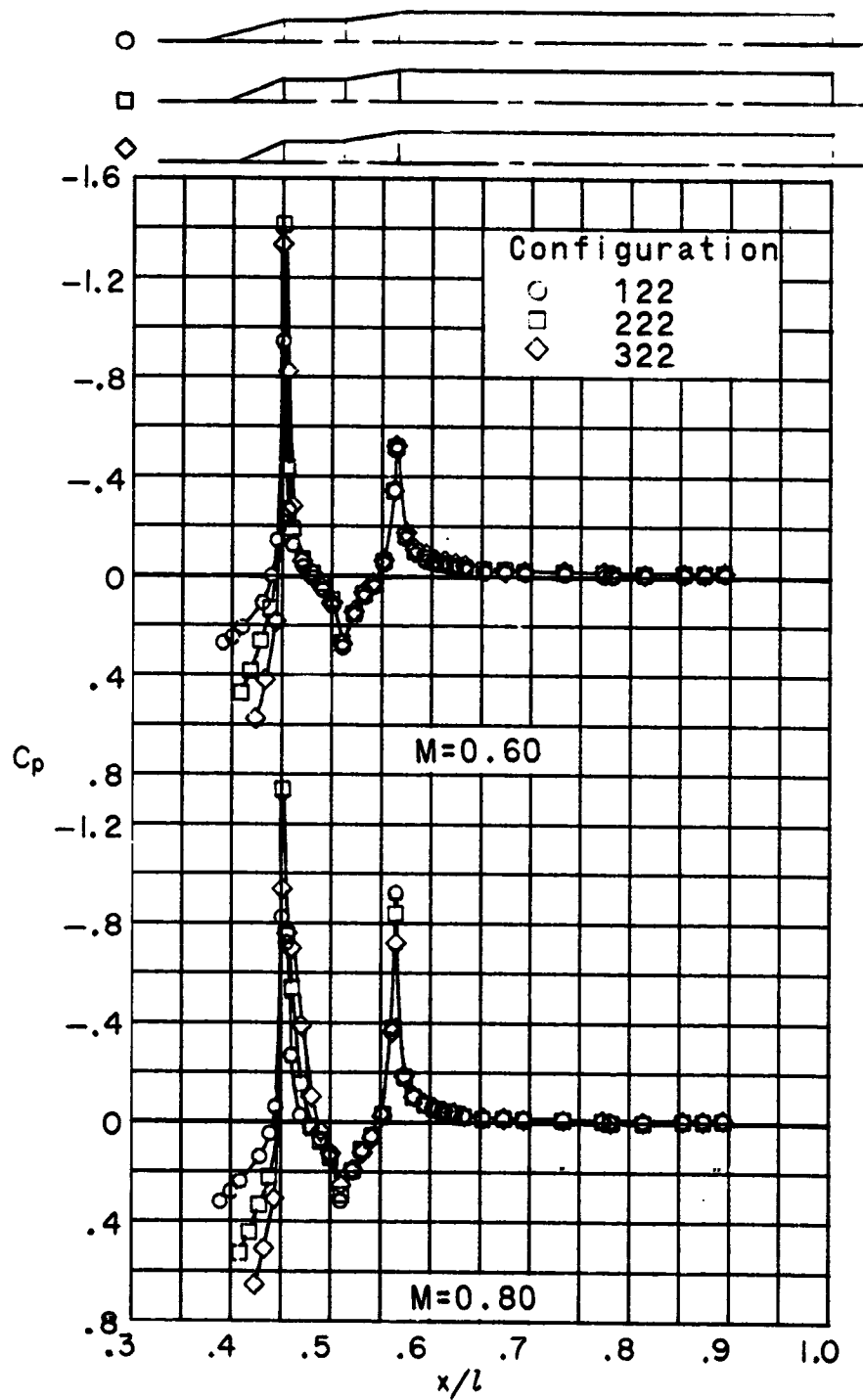
(a) $\delta_F = 5^\circ$.

Figure 6.- Effects of variation in nose-cone angle for $\phi = 0^\circ$ and $\alpha = -3^\circ$.



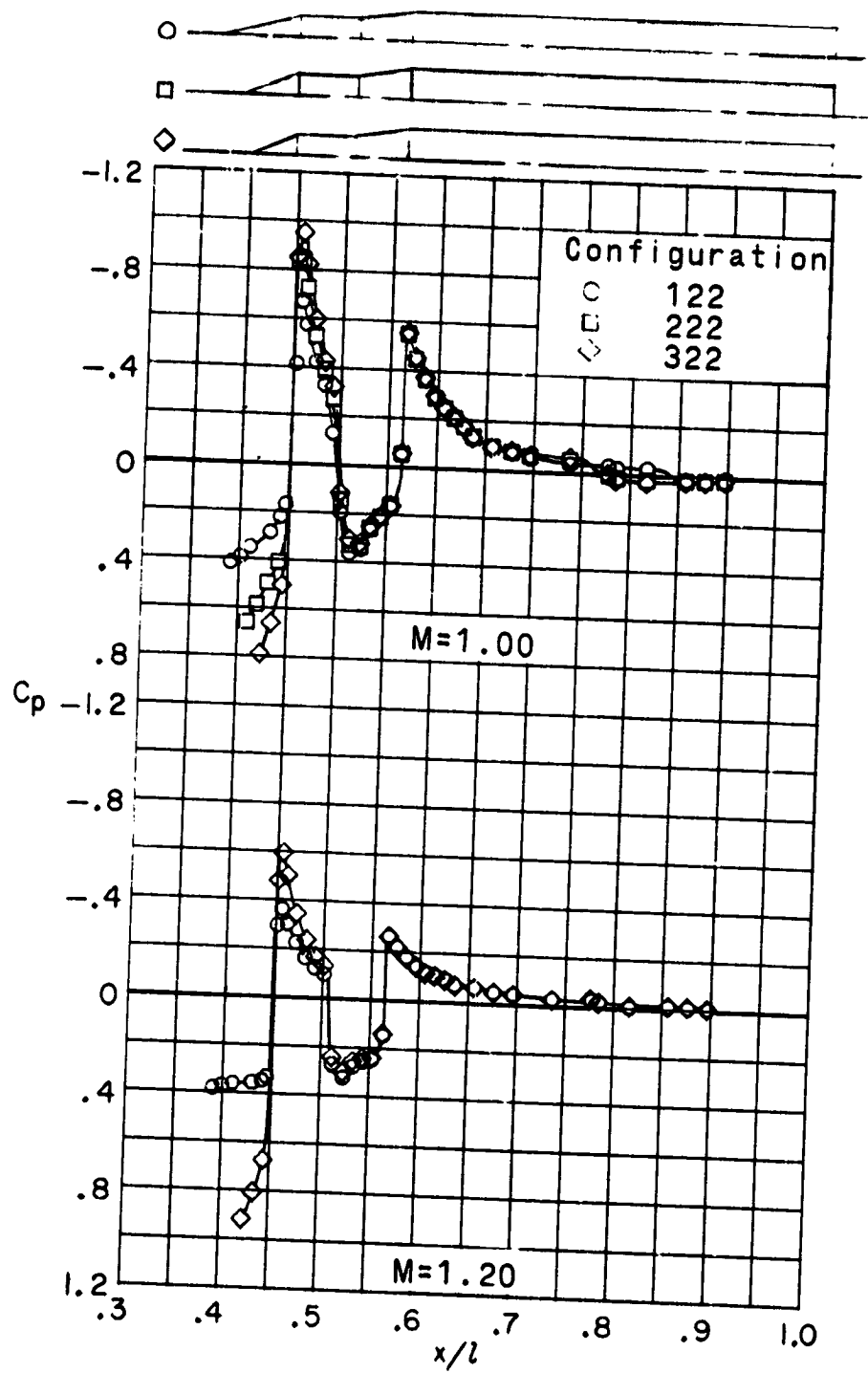
(a) Concluded.

Figure 6.- Continued.



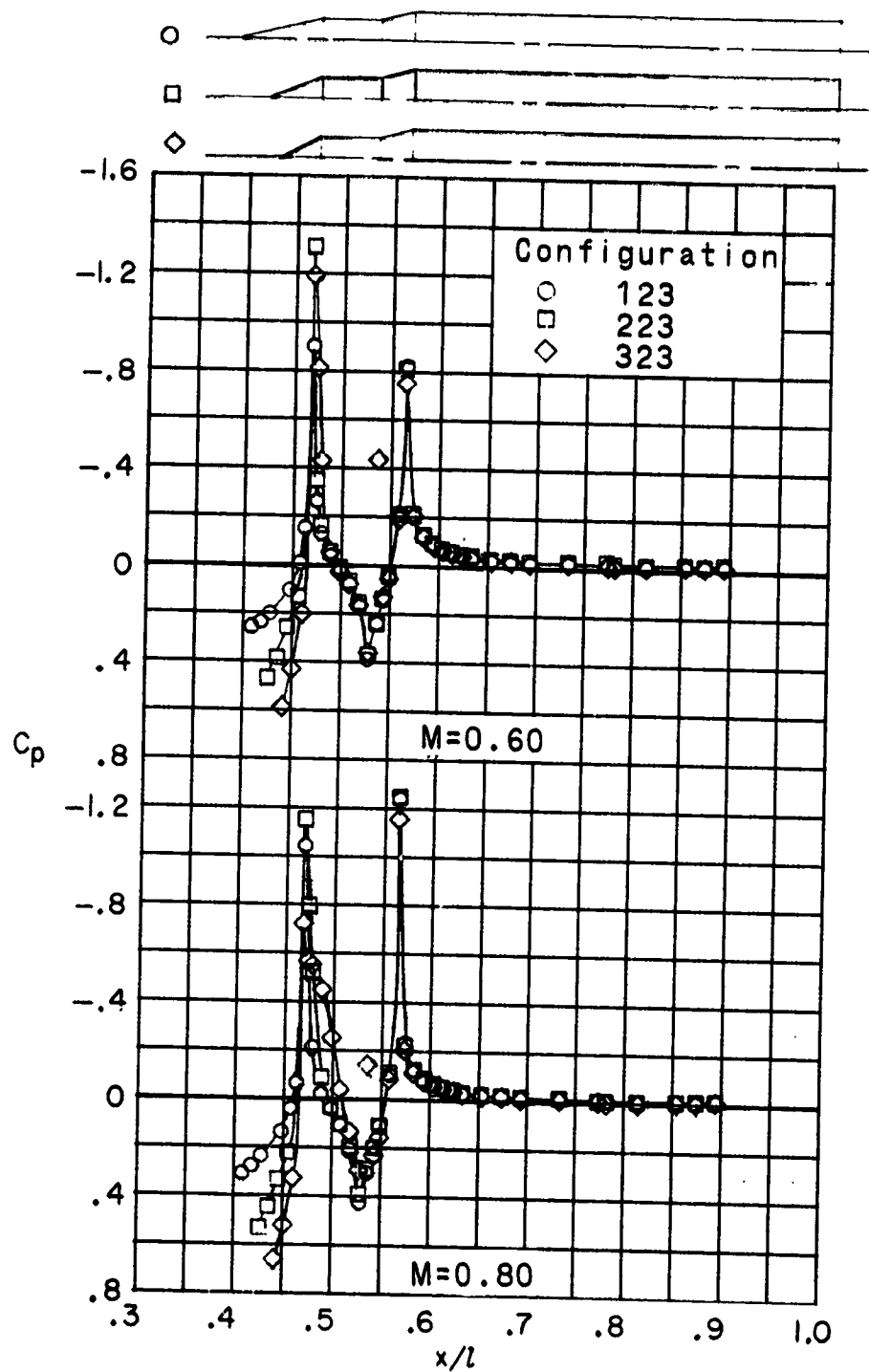
(b) $\delta_F = 10.1^\circ$.

Figure 6.- Continued.



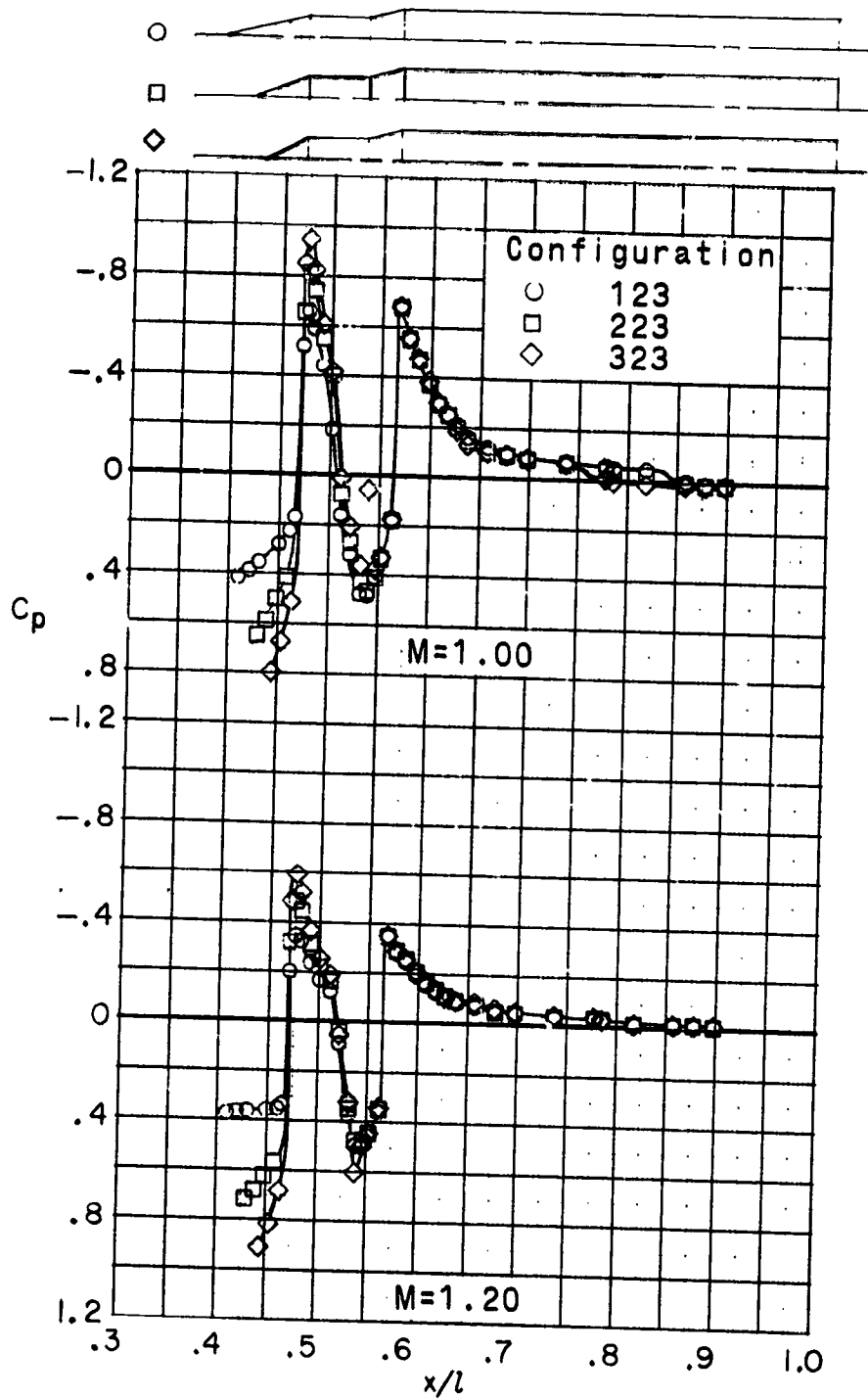
(b) Concluded.

Figure 6.- Continued.



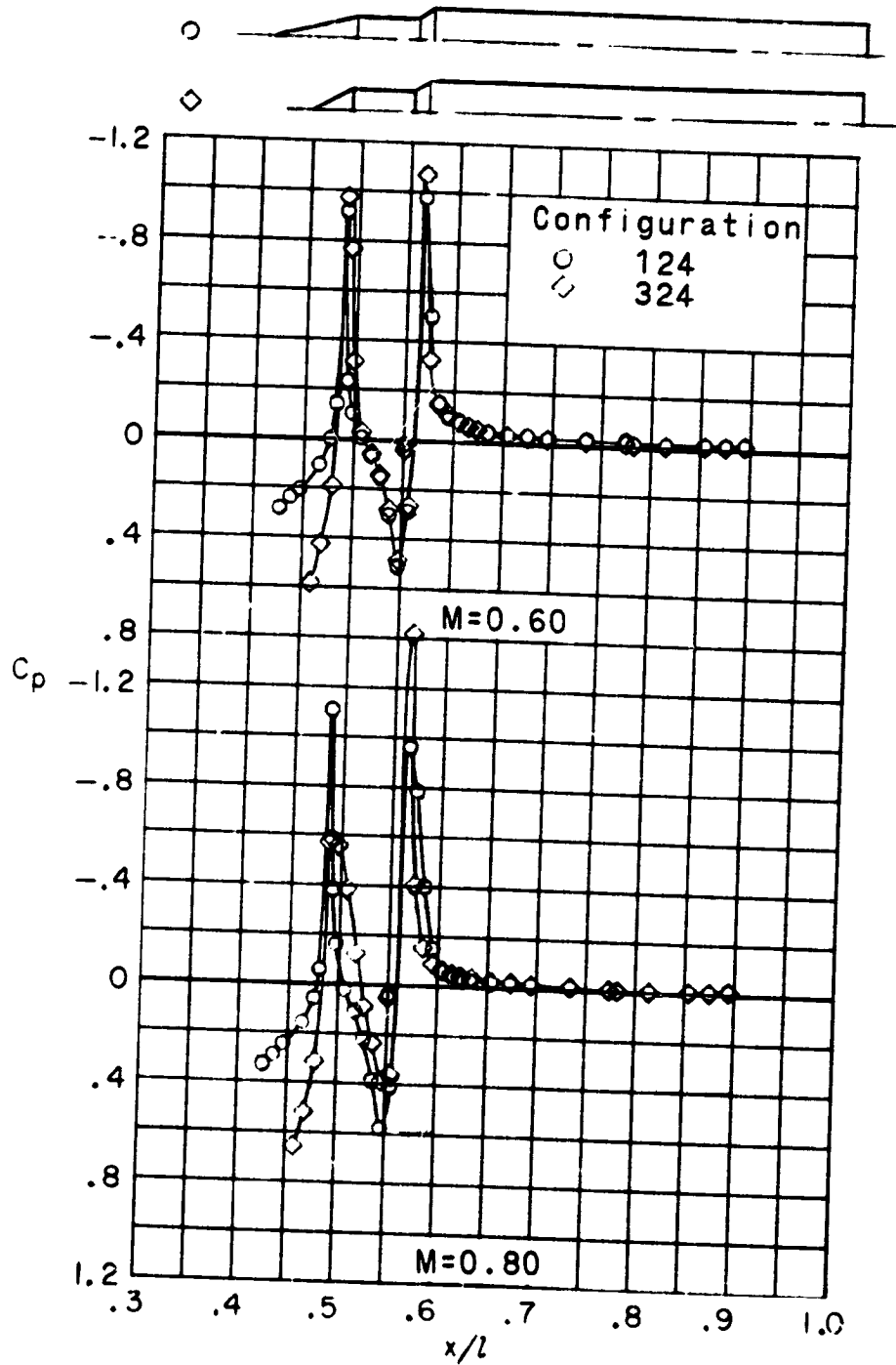
(c) $\delta_F = 15^\circ$.

Figure 6.- Continued.



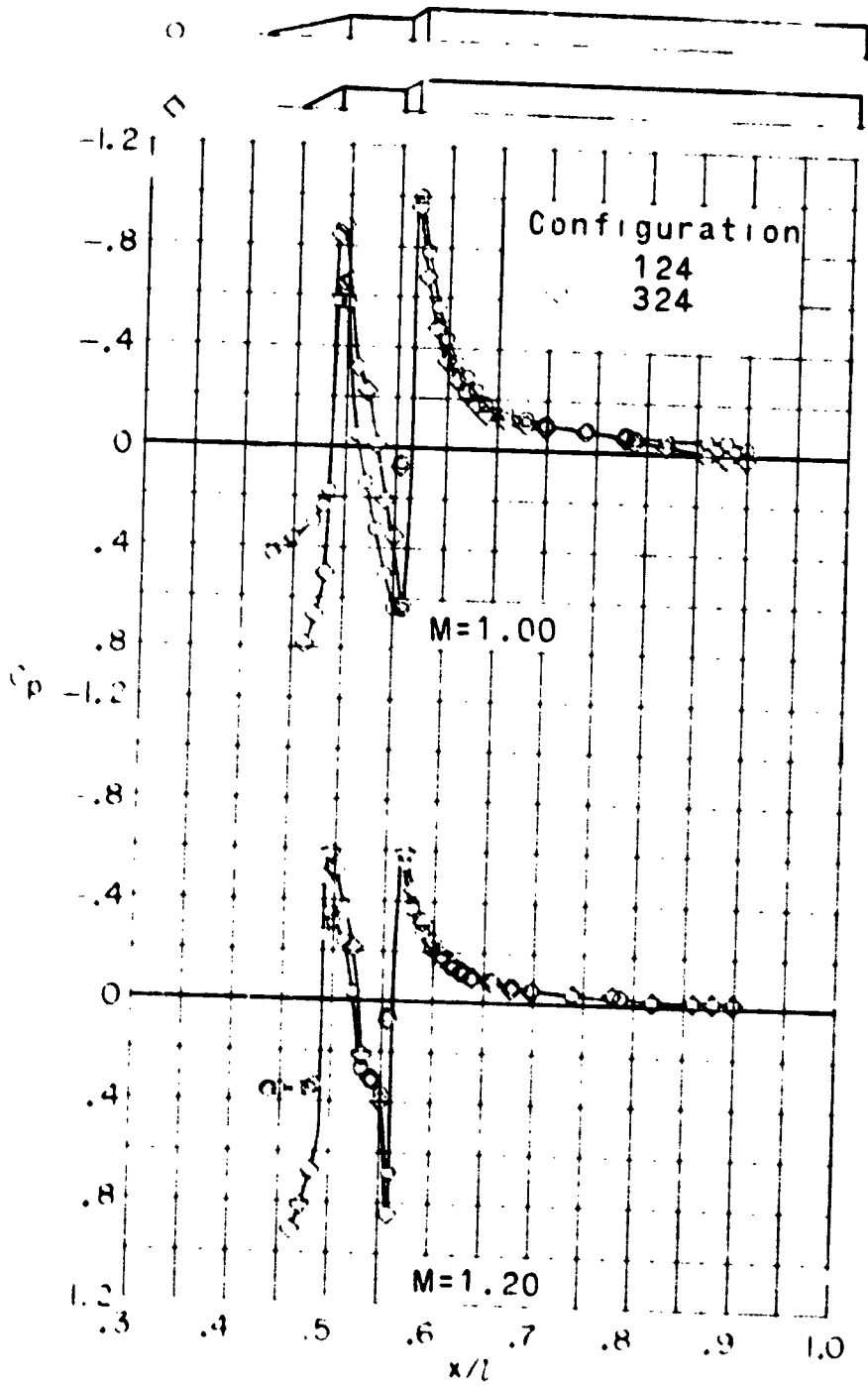
(c) Concluded.

Figure 6.- Continued.



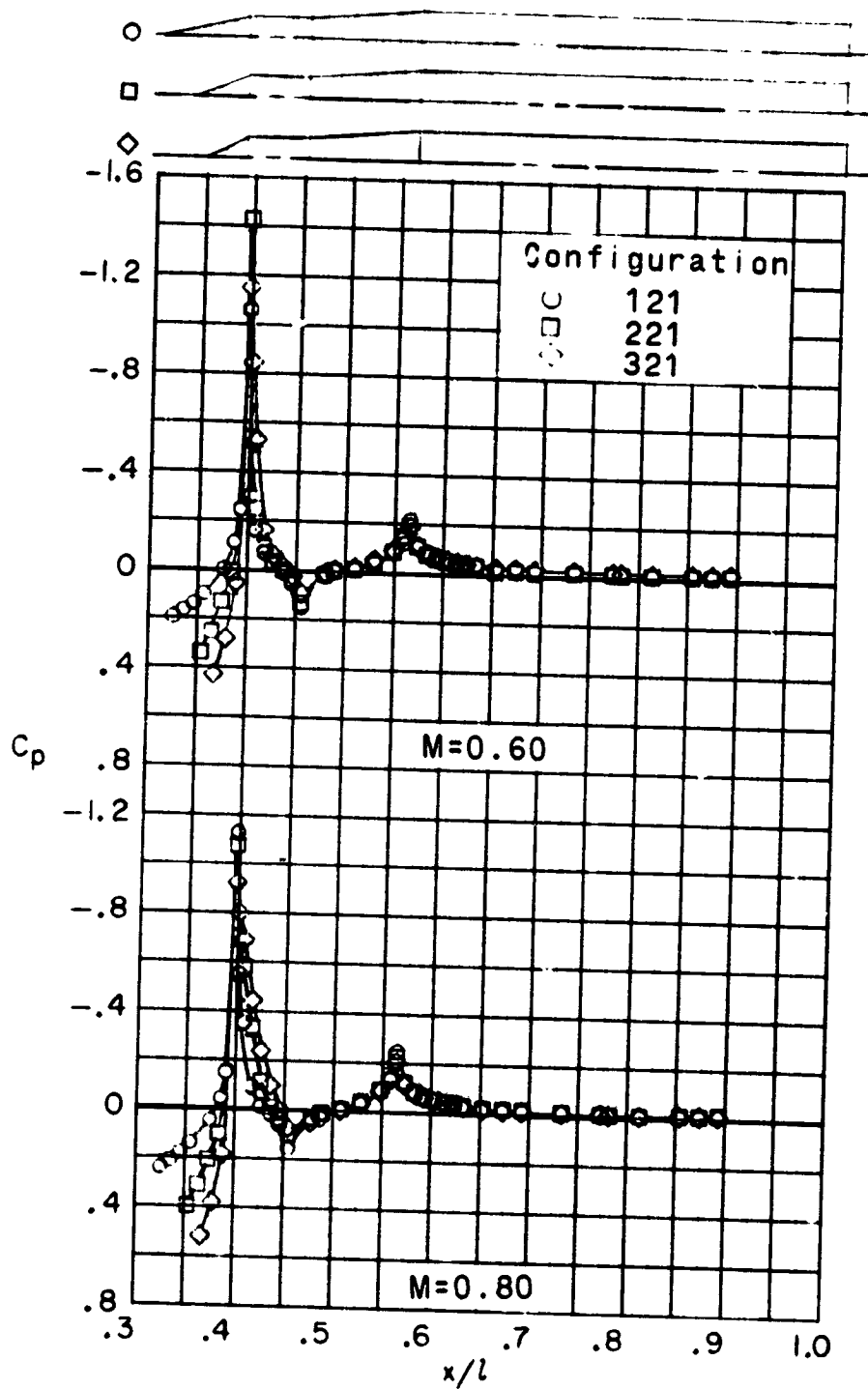
(d) $\delta_F = 30^\circ$.

Figure 6.- Continued.



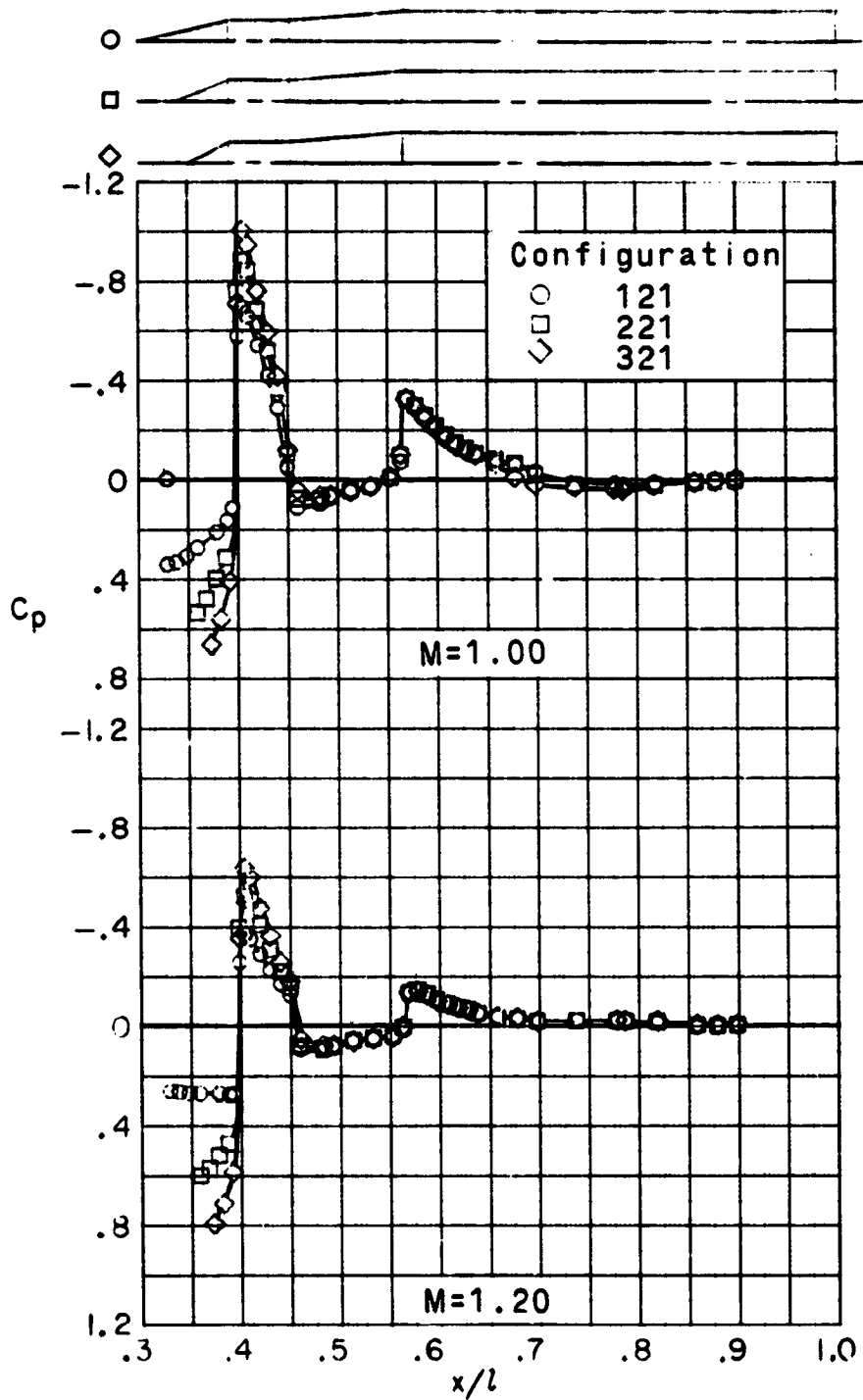
(d) Concluded.

Figure 6.- Concluded.



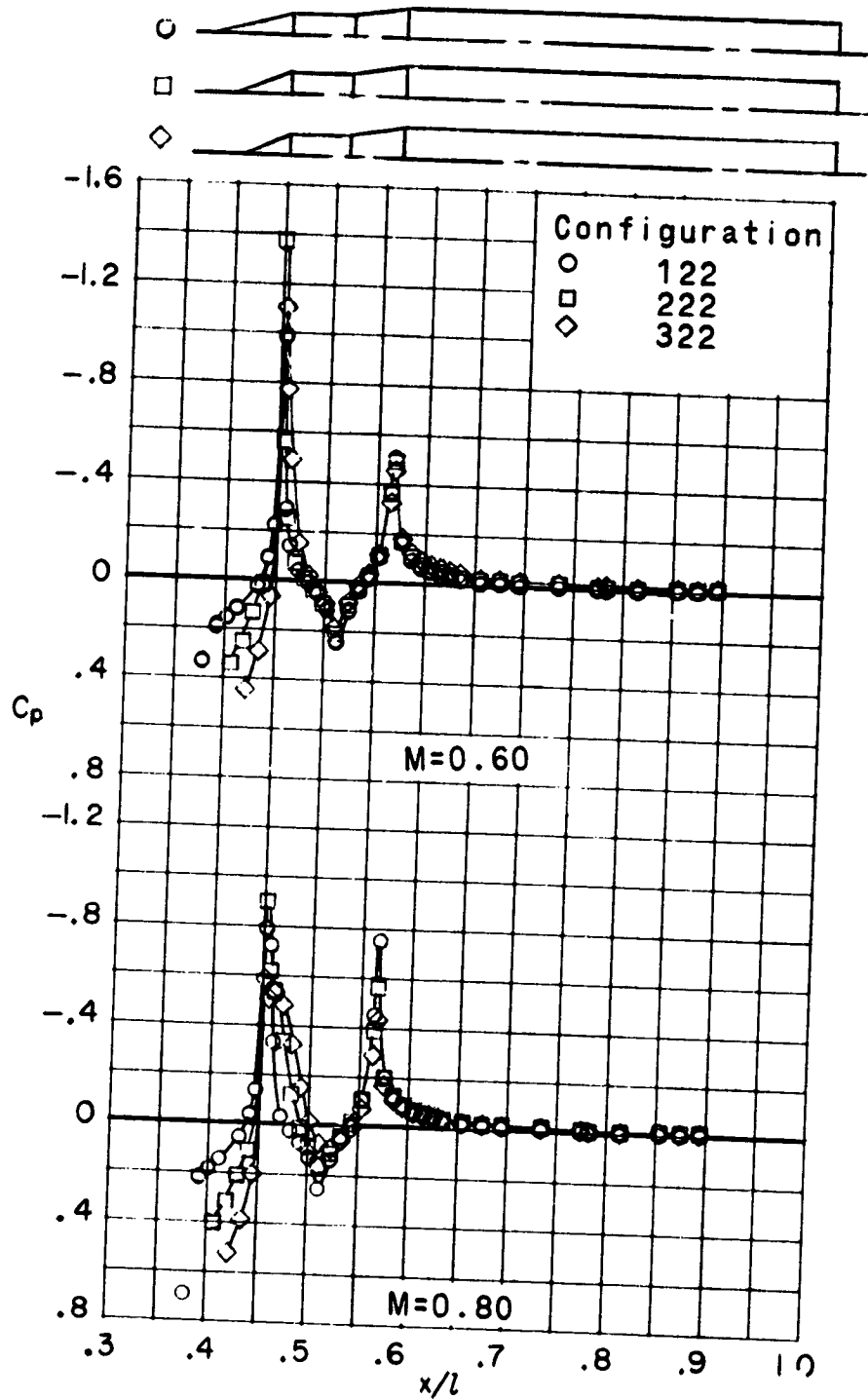
(a) $\delta_F = 5^\circ$.

Figure 7.- Effects of variation in nose-cone angle for $\phi = 0^\circ$ and $\alpha = 3^\circ$.



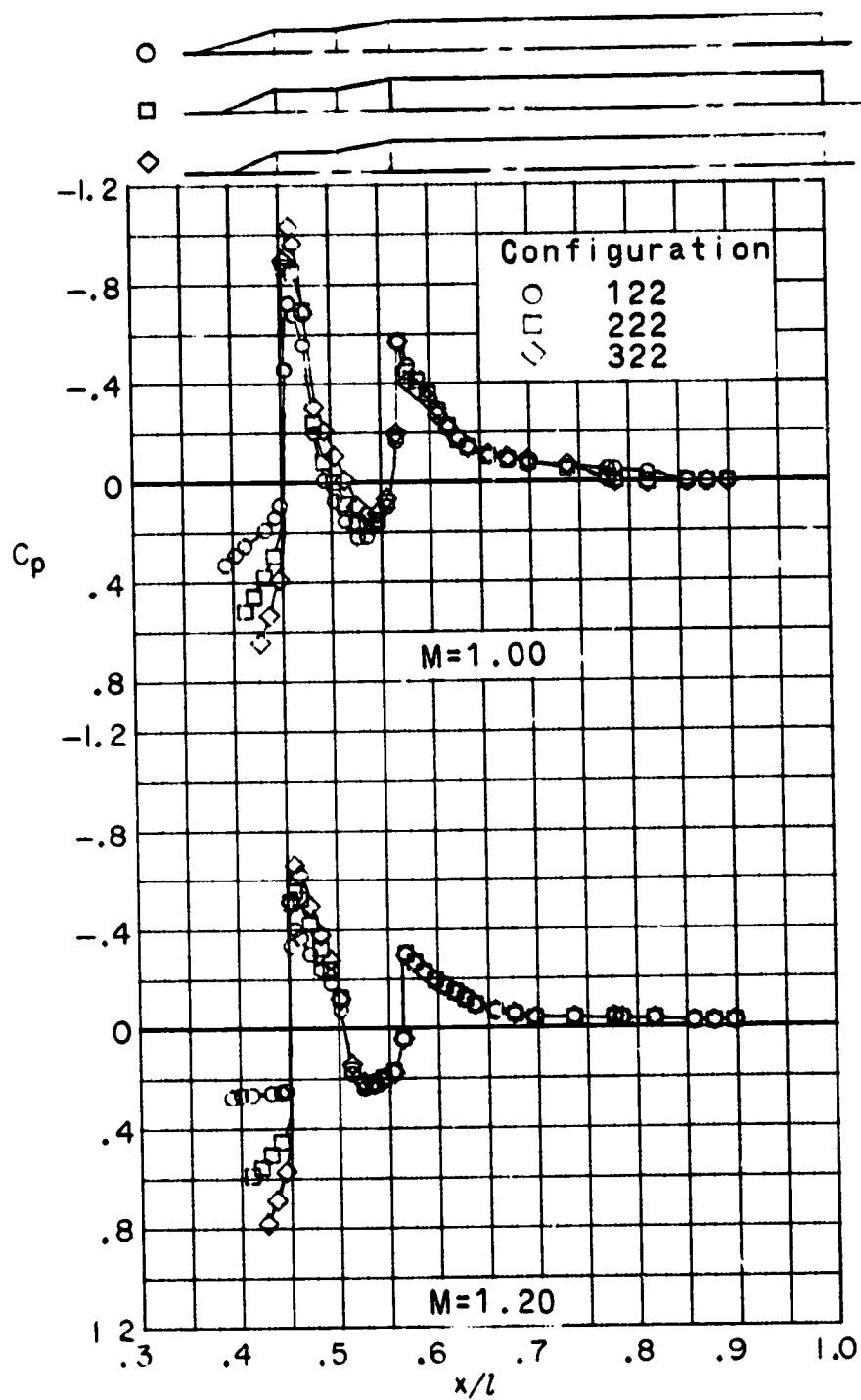
(a) Concluded.

Figure 7.- Continued.



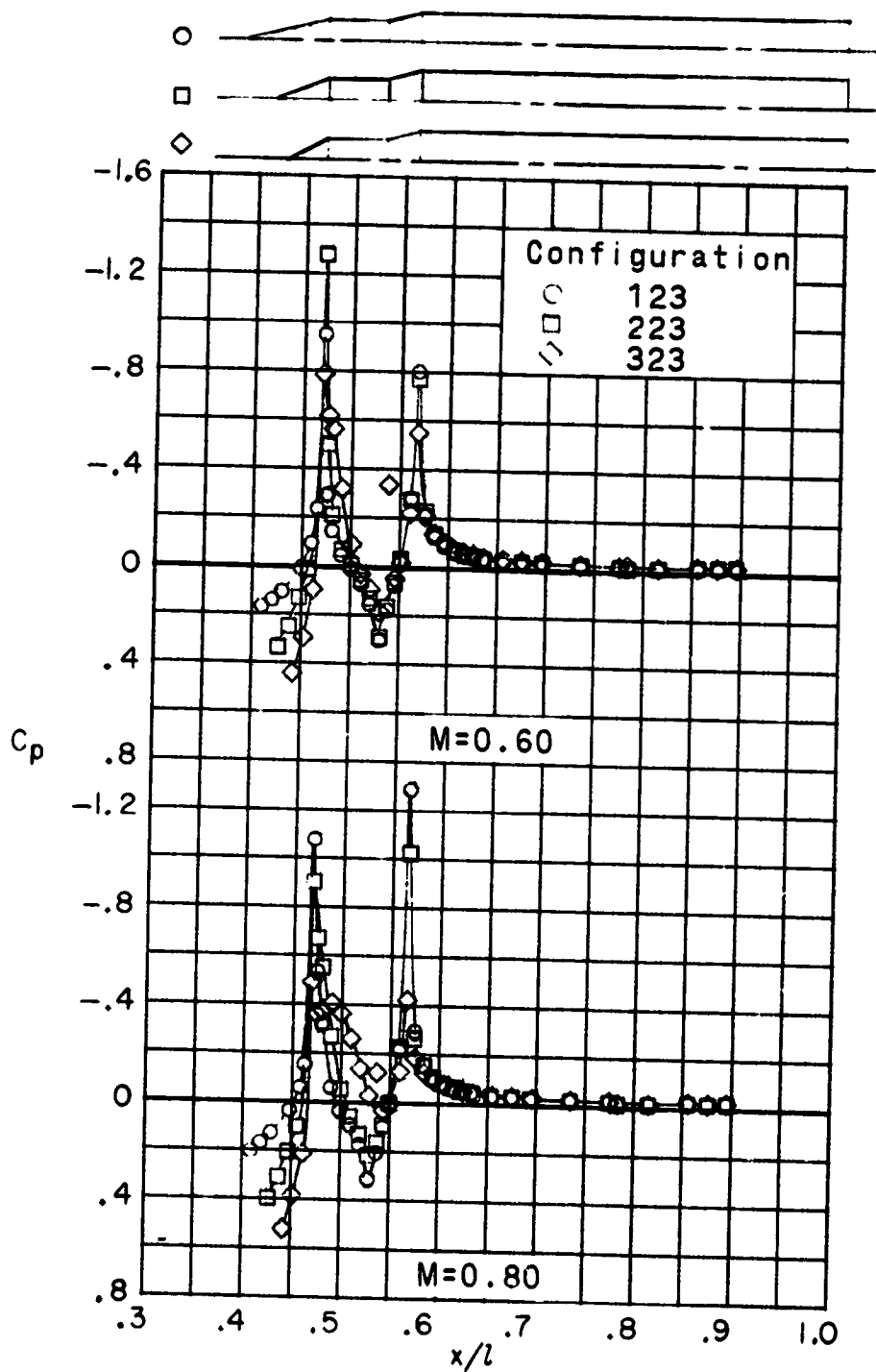
(b) $\delta_F = 10.1^\circ$.

Figure 7.- Continued.



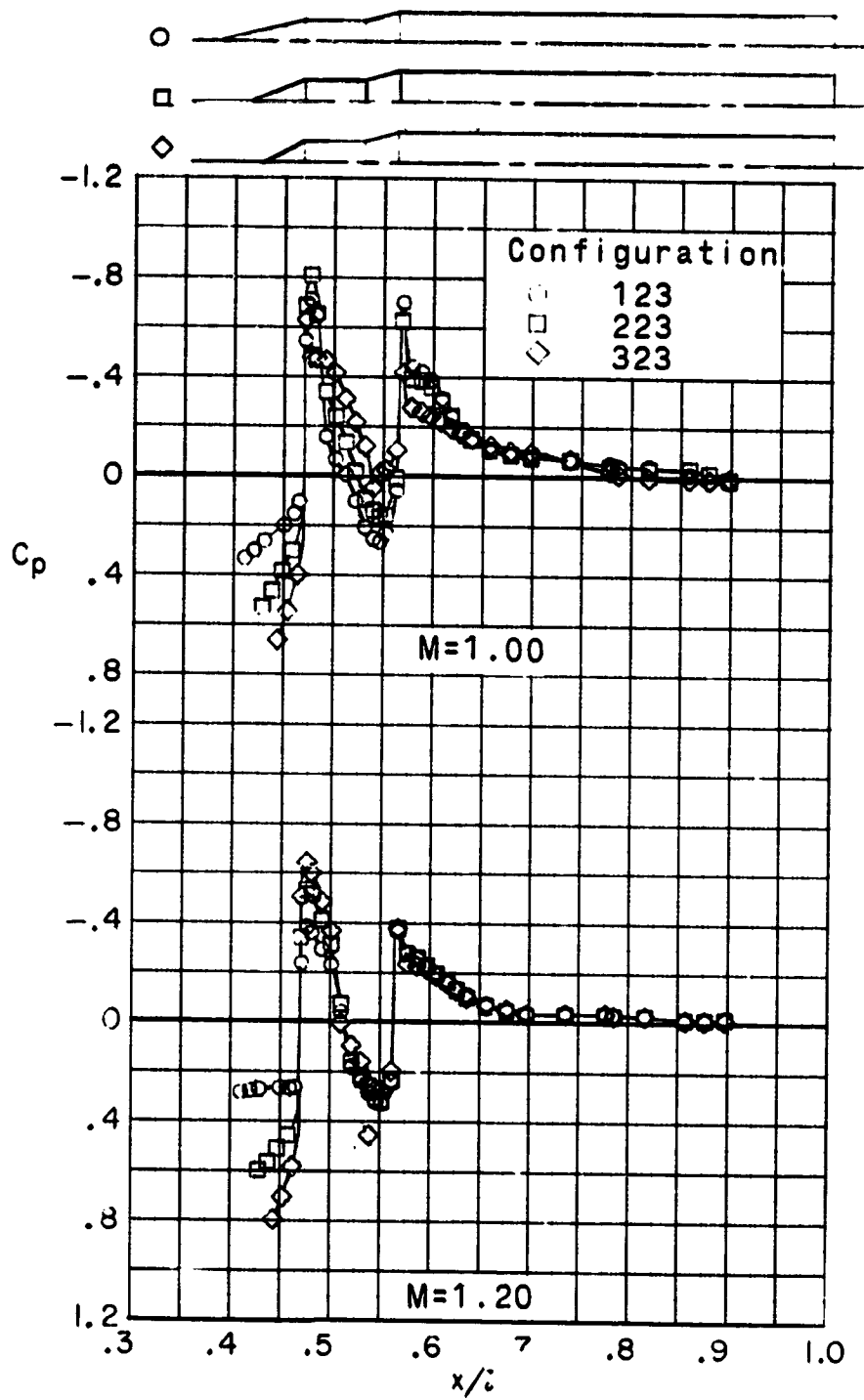
(b) Concluded.

Figure 7.- Continued.



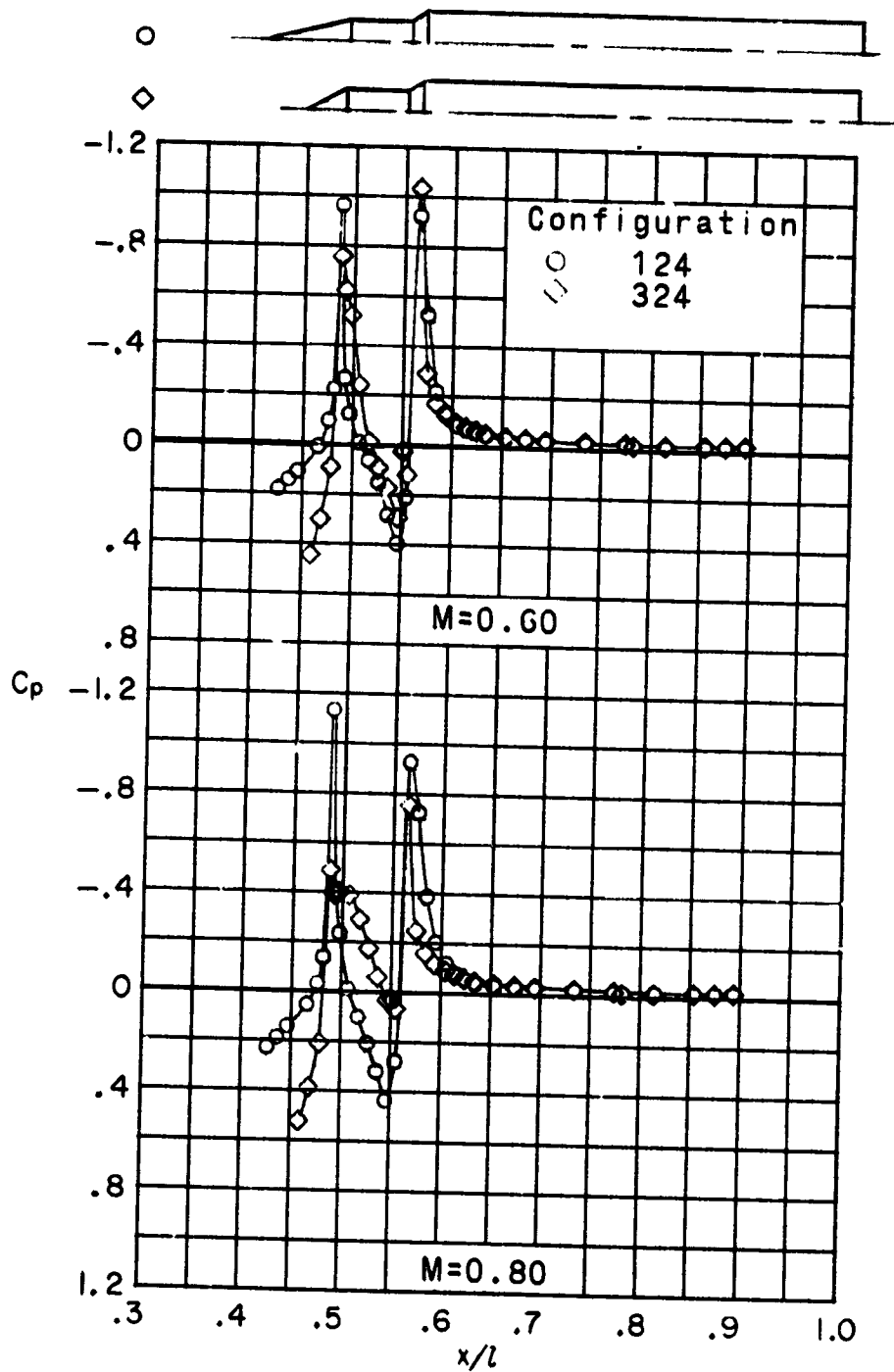
(c) $\delta_P = 15^\circ$.

Figure 7.- Continued.



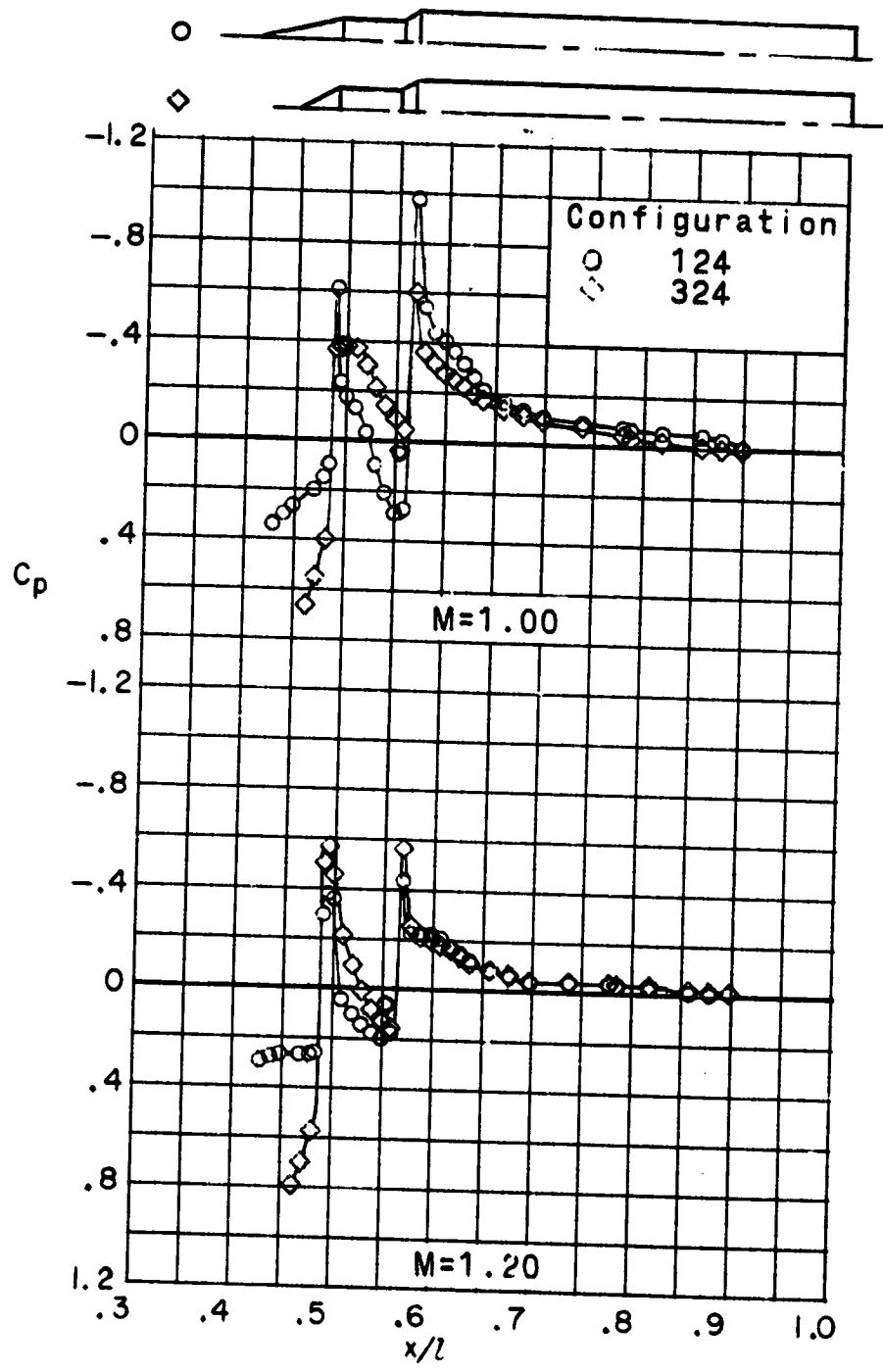
(c) Concluded.

Figure 7.- Continued.



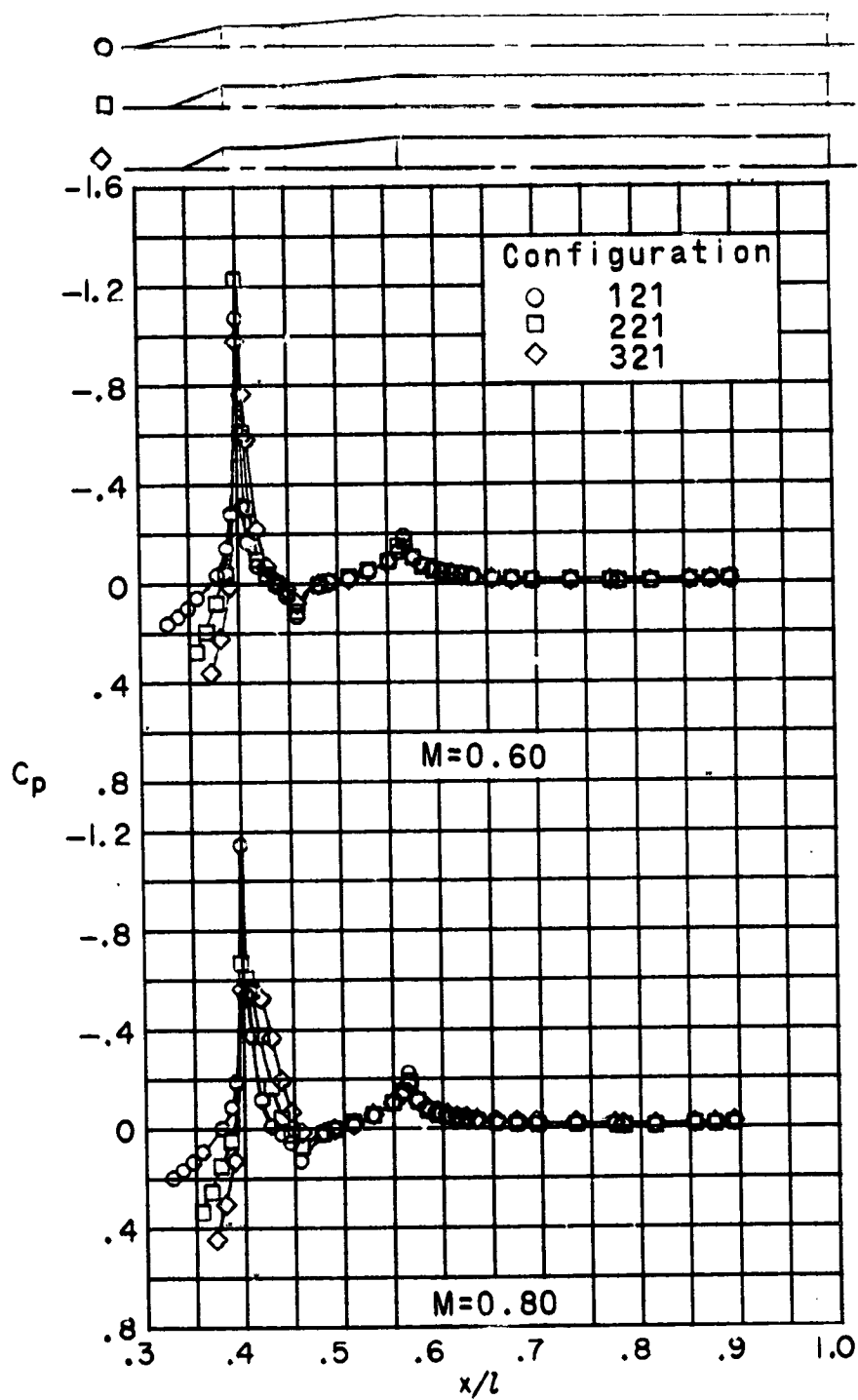
(d) $\delta_F = 30^\circ$.

Figure 7.- Continued.



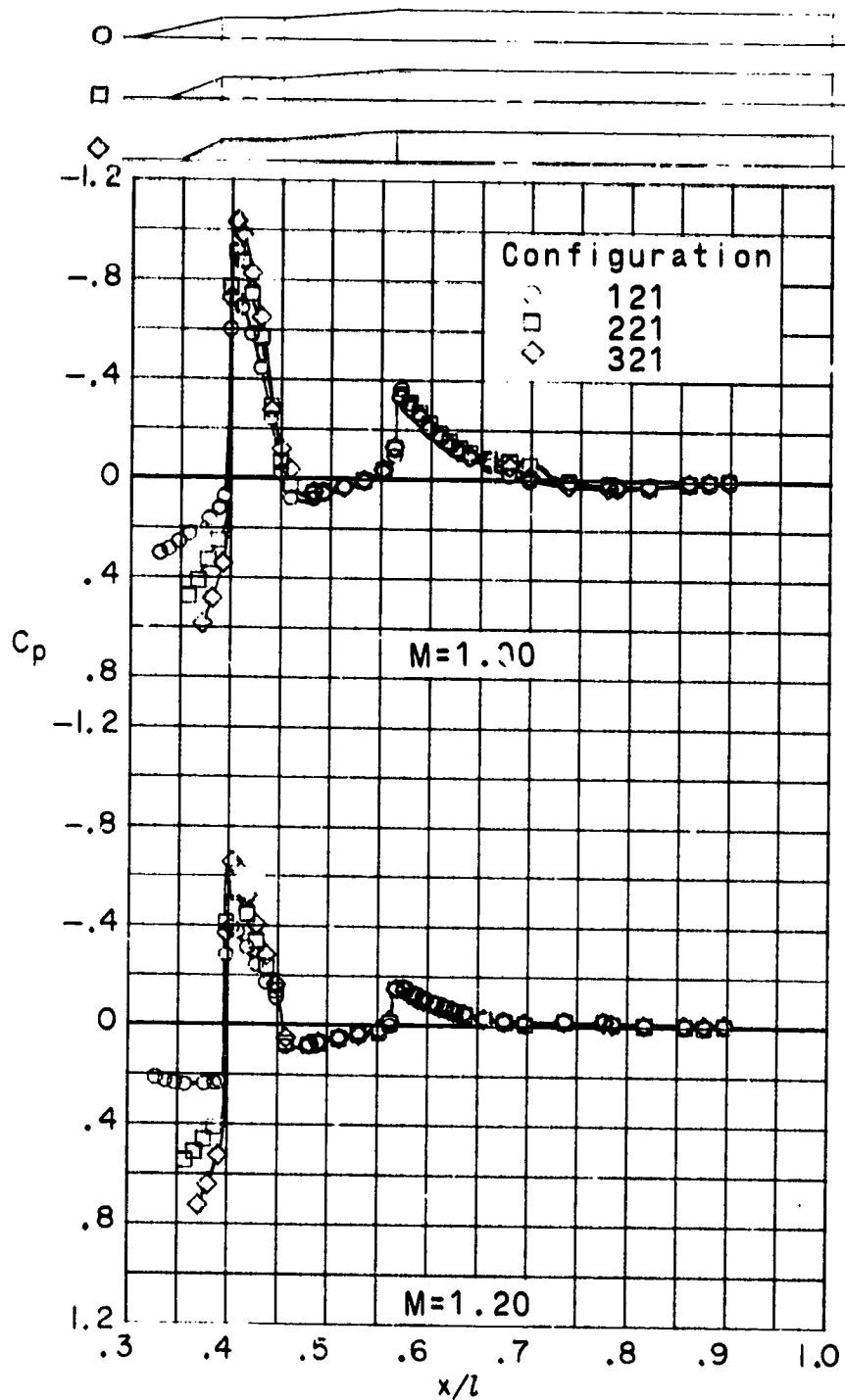
(d) Concluded.

Figure 7.- Concluded.



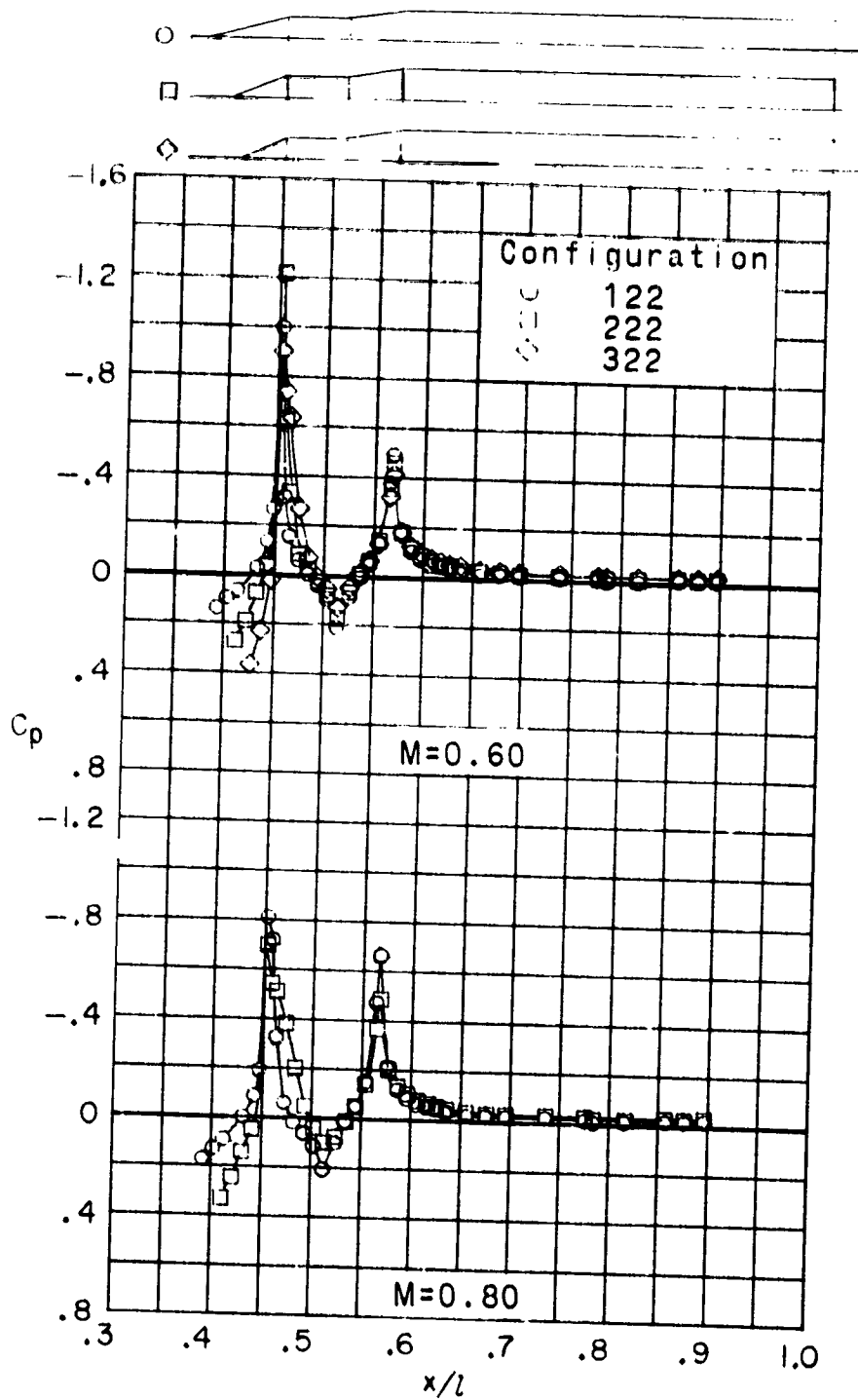
(a) $\delta_F = 5^\circ$.

Figure 8.- Effects of variation in nose-cone angle for $\phi = 0^\circ$ and $\alpha = 6^\circ$.



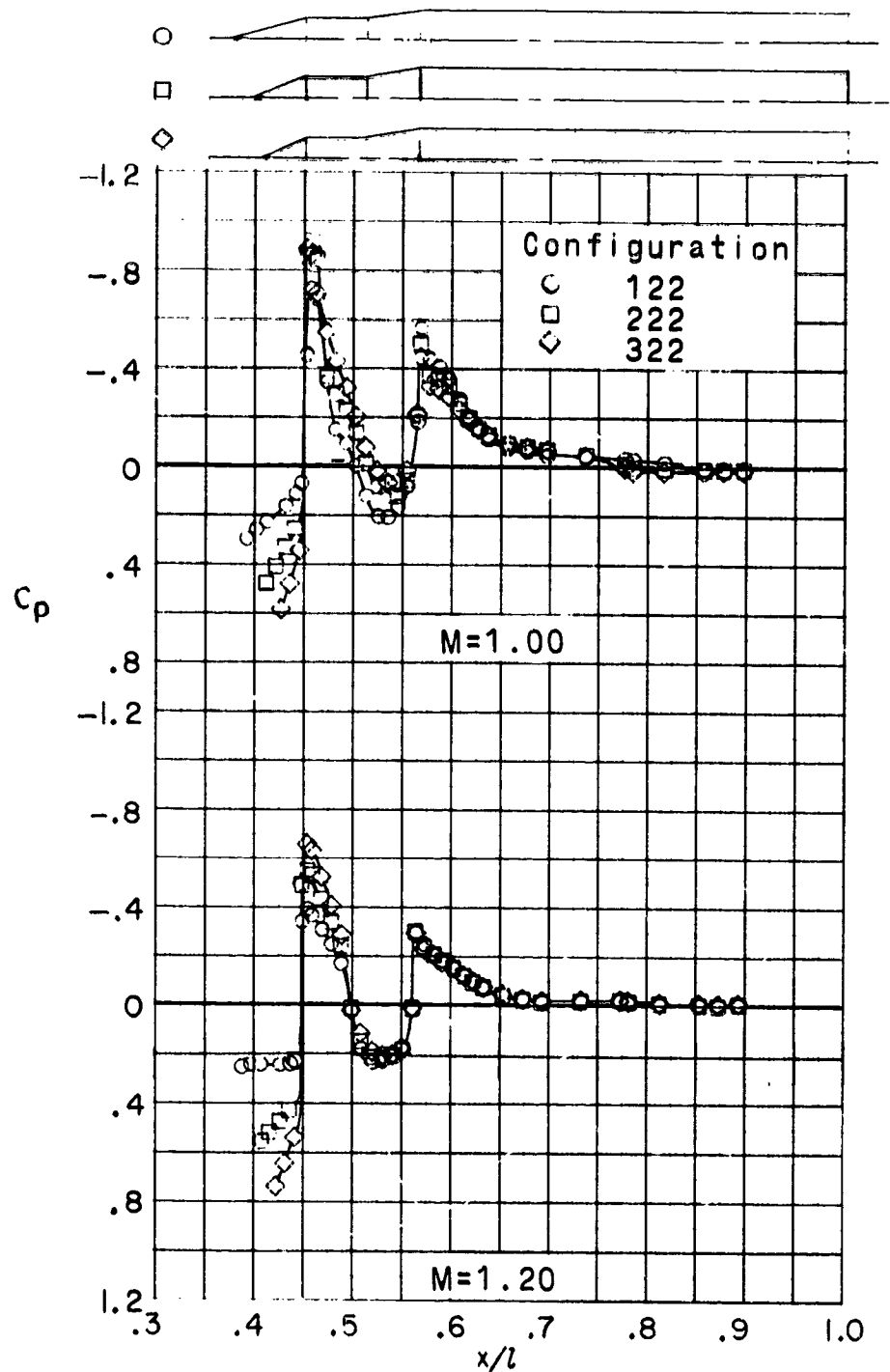
(a) Concluded.

Figure 8.- Continued.



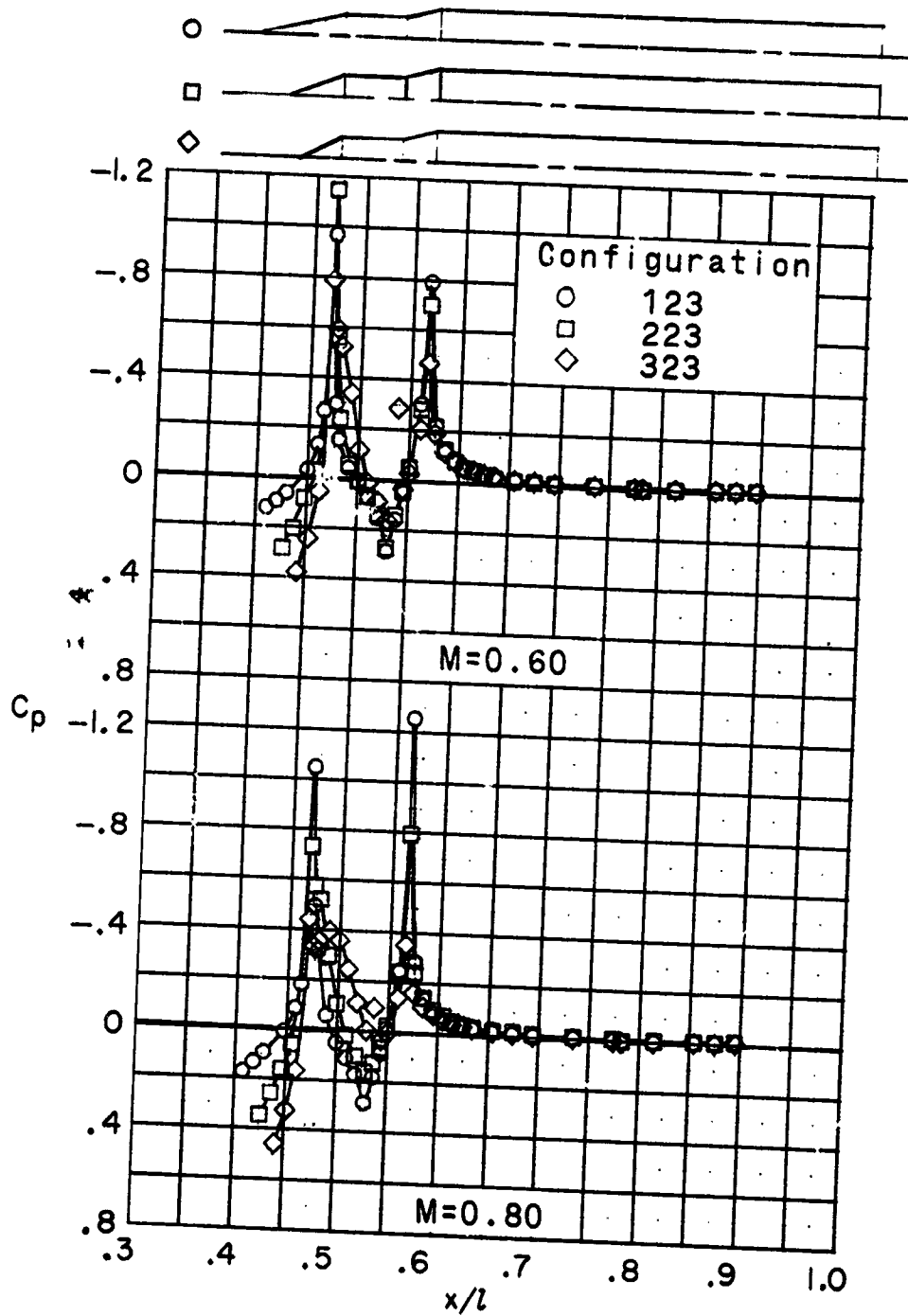
(b) $\delta_F = 10.1^\circ$.

Figure 8.- Continued.



(b) Concluded.

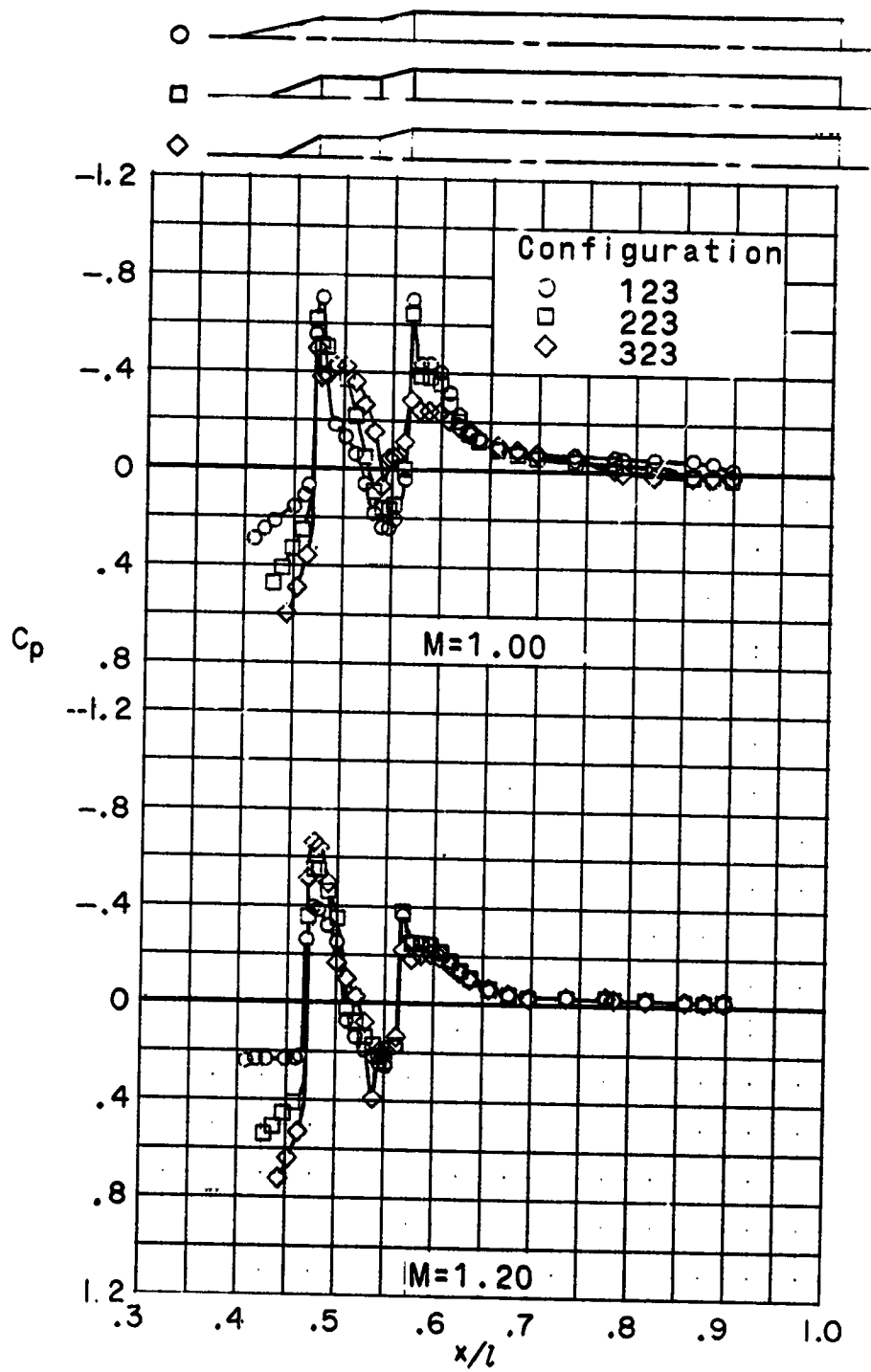
Figure 8.- Continued.



(c) $\delta_F = 15^\circ$.

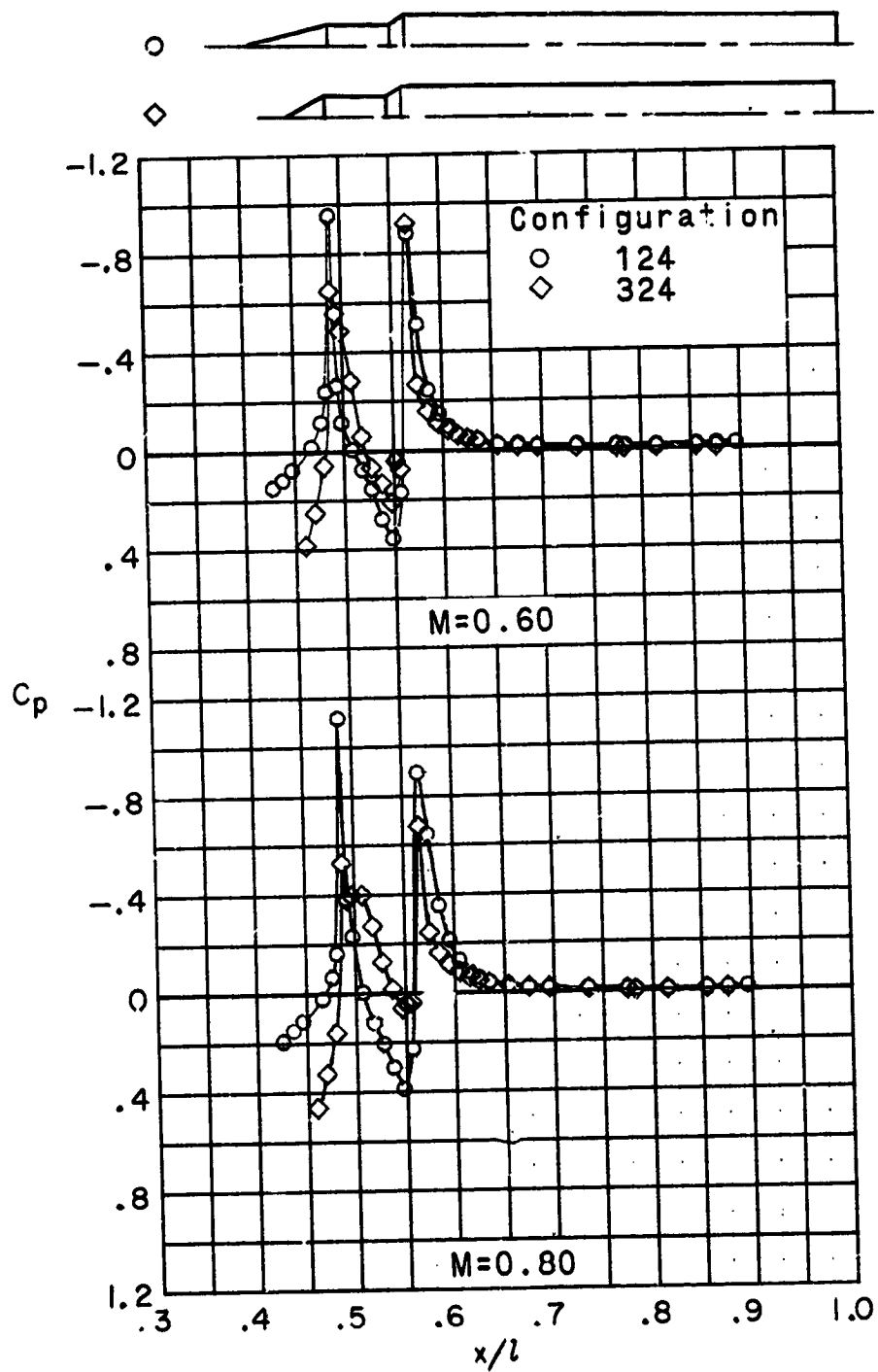
Figure 8.- Continued.

C-3



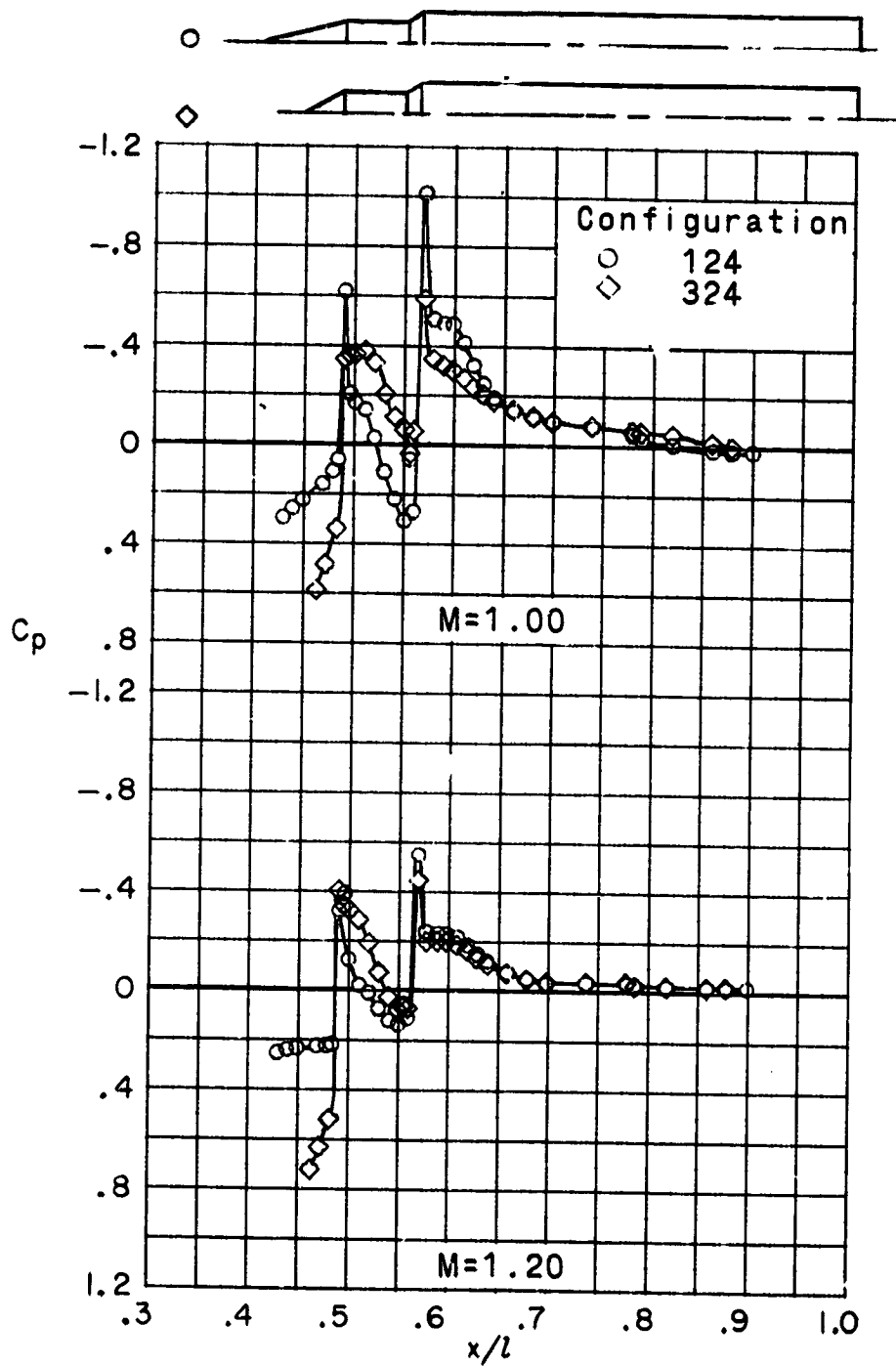
(c) Concluded.

Figure 8.- Continued.



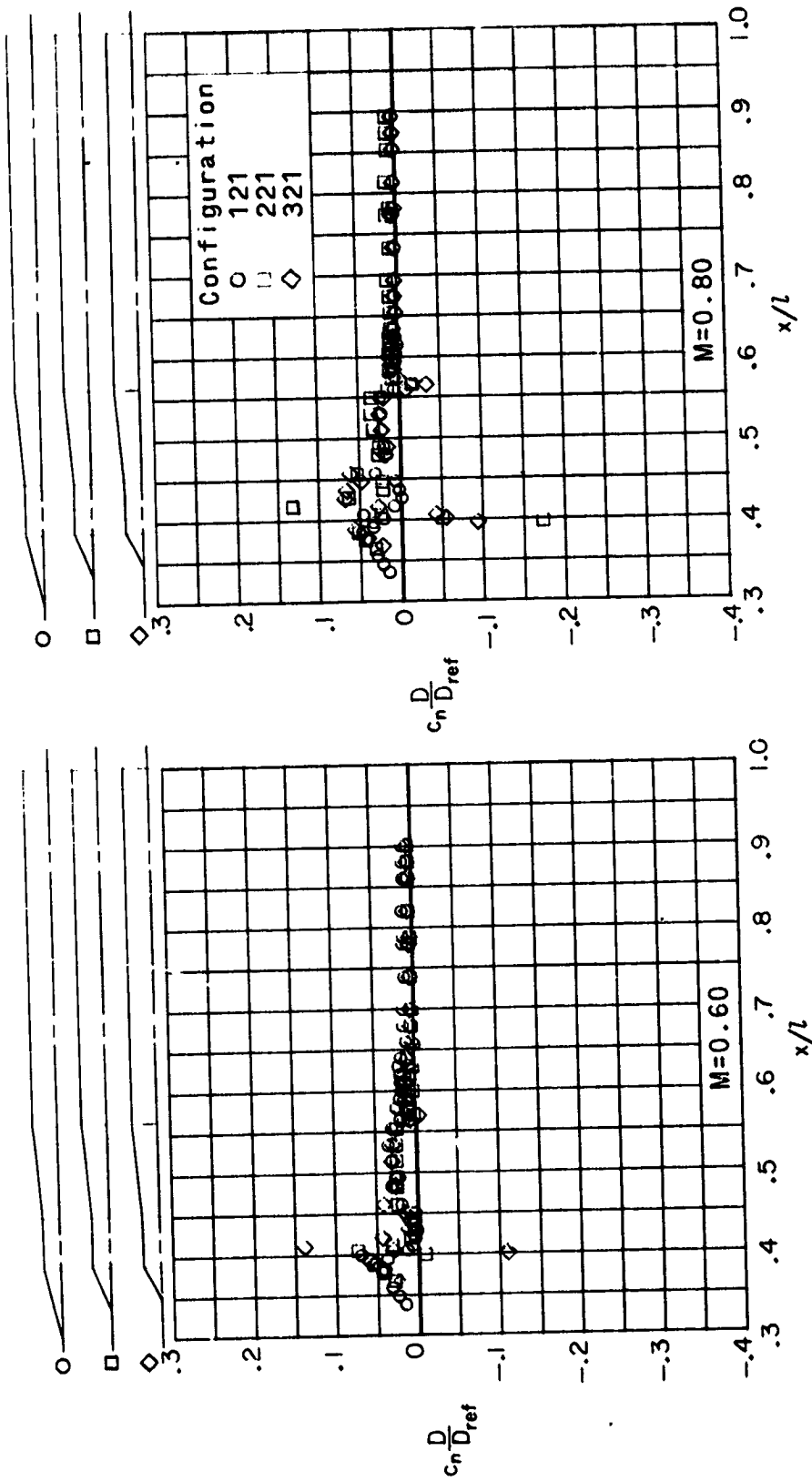
(d) $\delta_F = 30^\circ$.

Figure 8.- Continued.



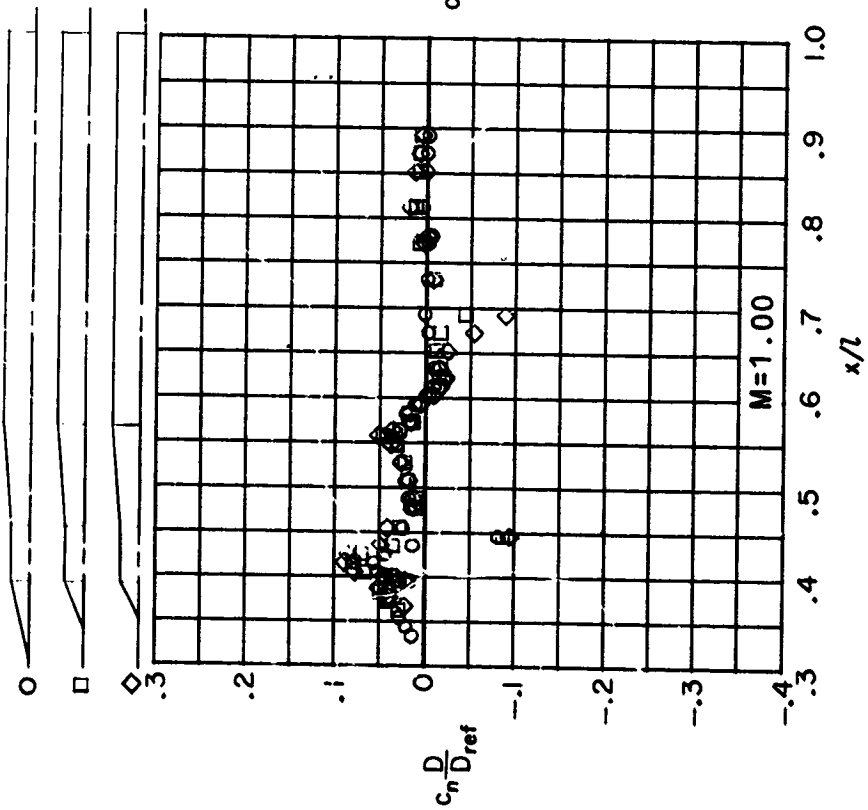
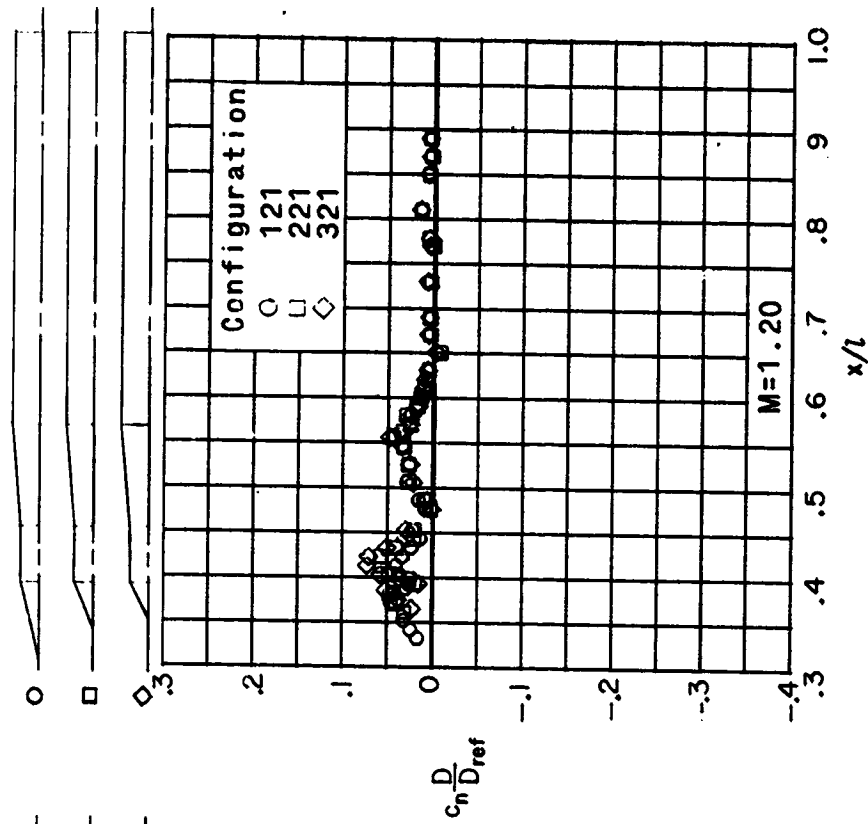
(d) Concluded.

Figure 8.- Concluded.



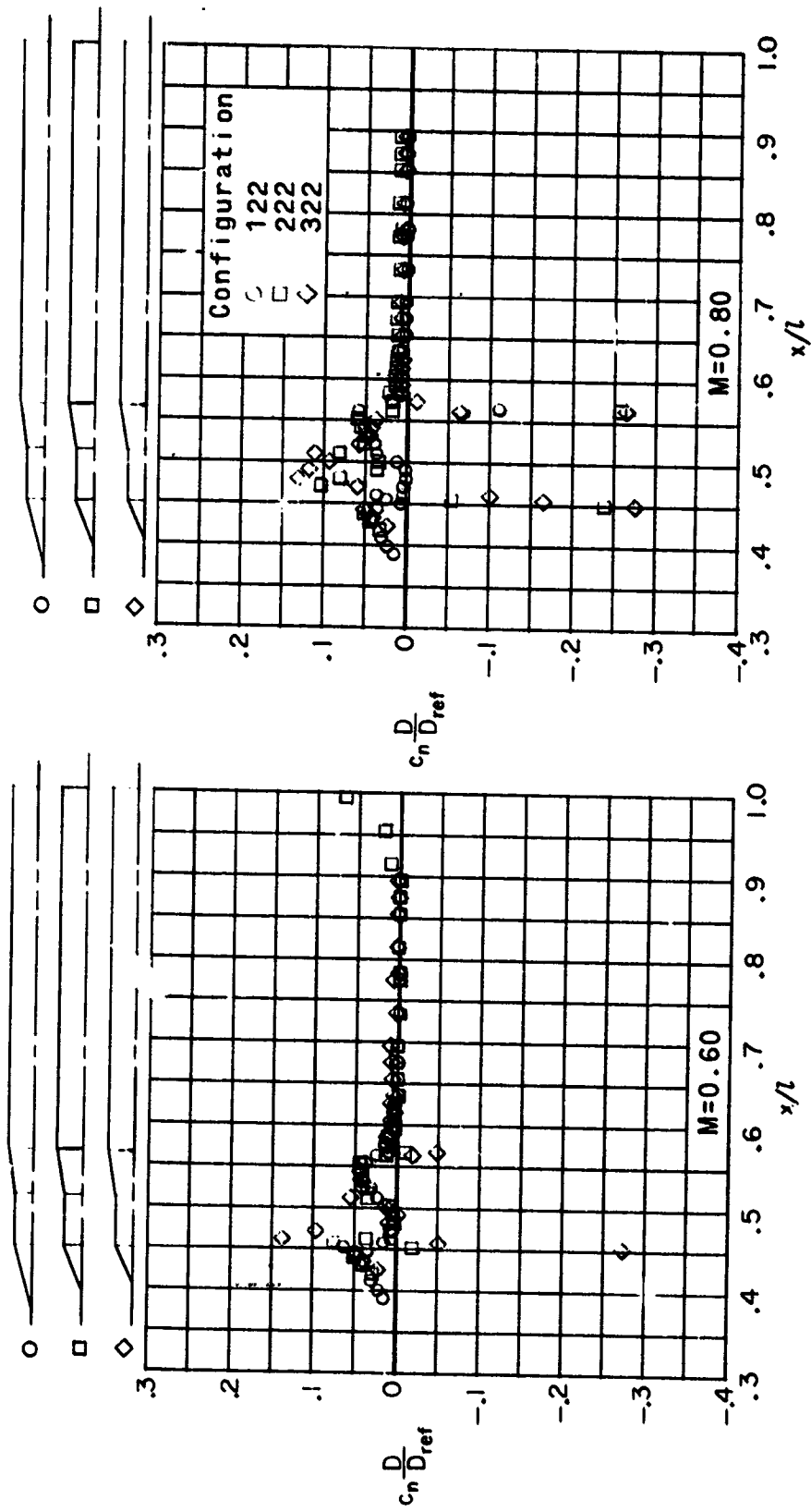
(a) $\delta_f = 5^\circ$.

Figure 9.- Effect of variation in nose-cone angle on load distributions at $\alpha = 30^\circ$.



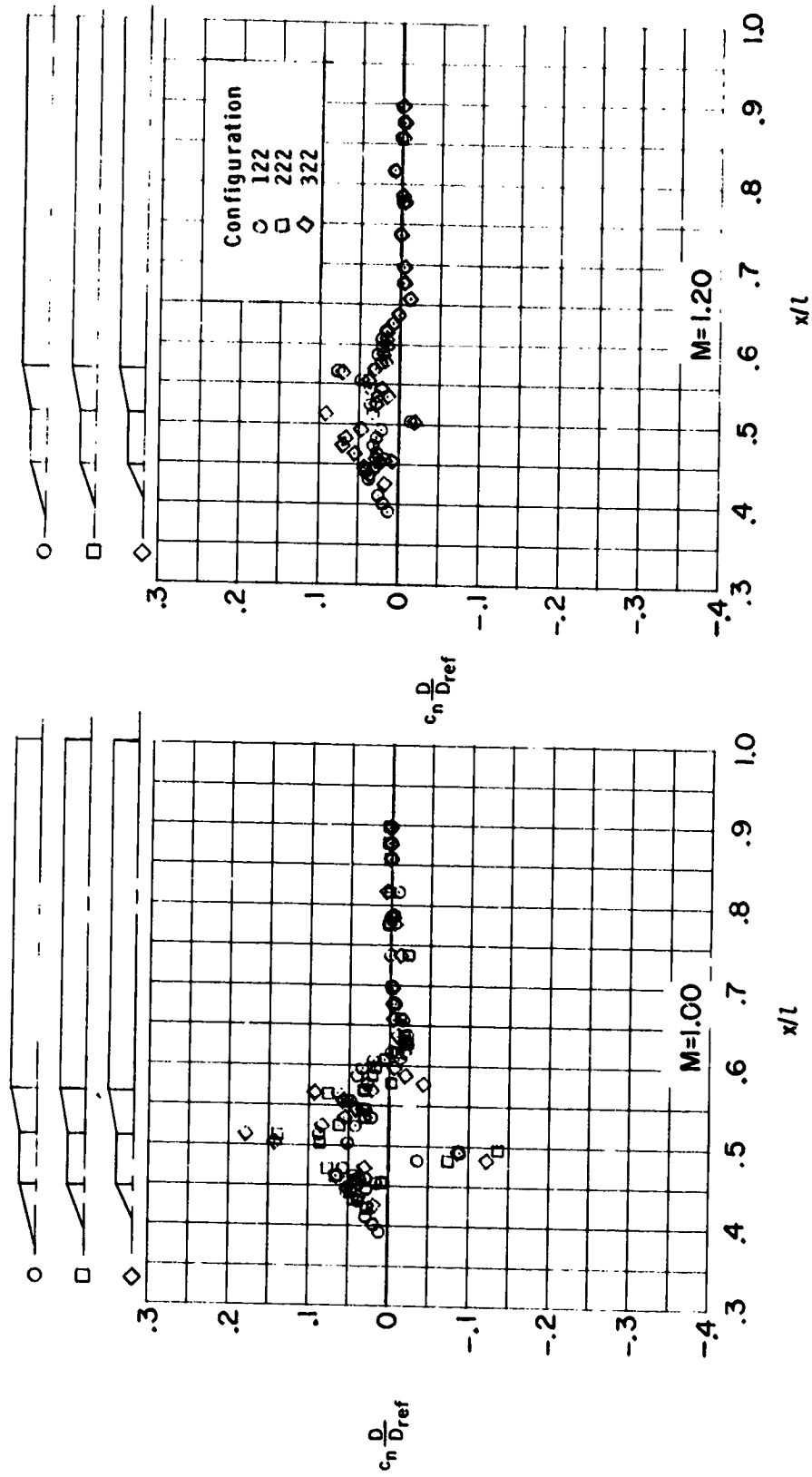
(a) Concluded.

Figure 9.- Continued.



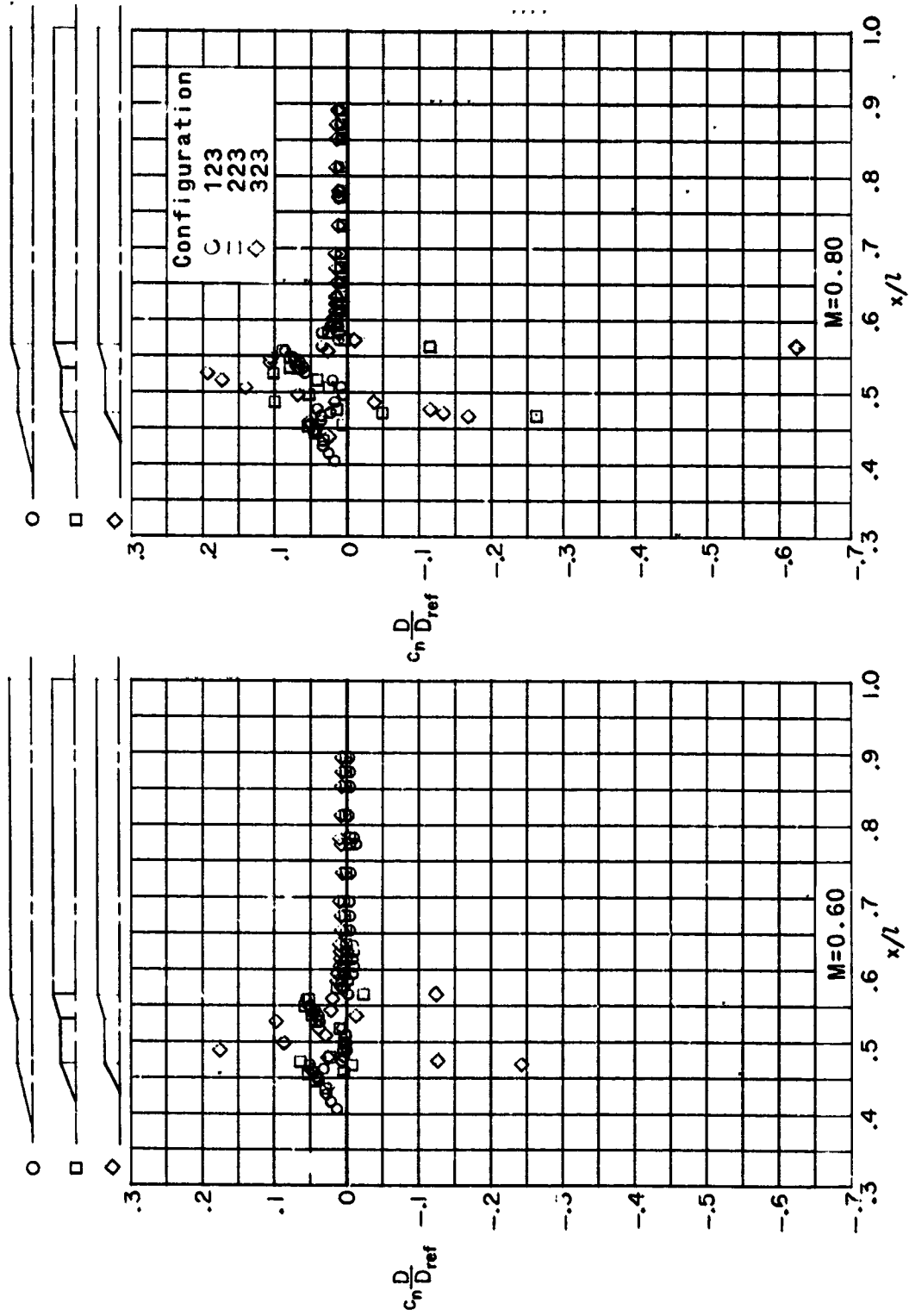
(b) $\delta_P = 10.10^\circ$.

Figure 9.- Continued.



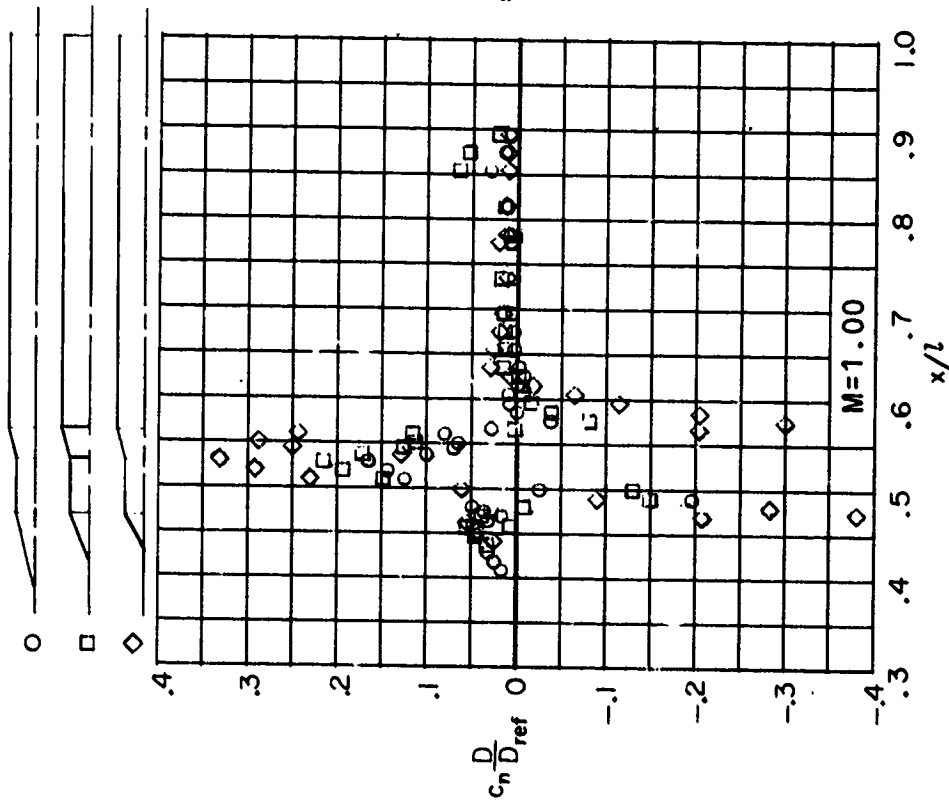
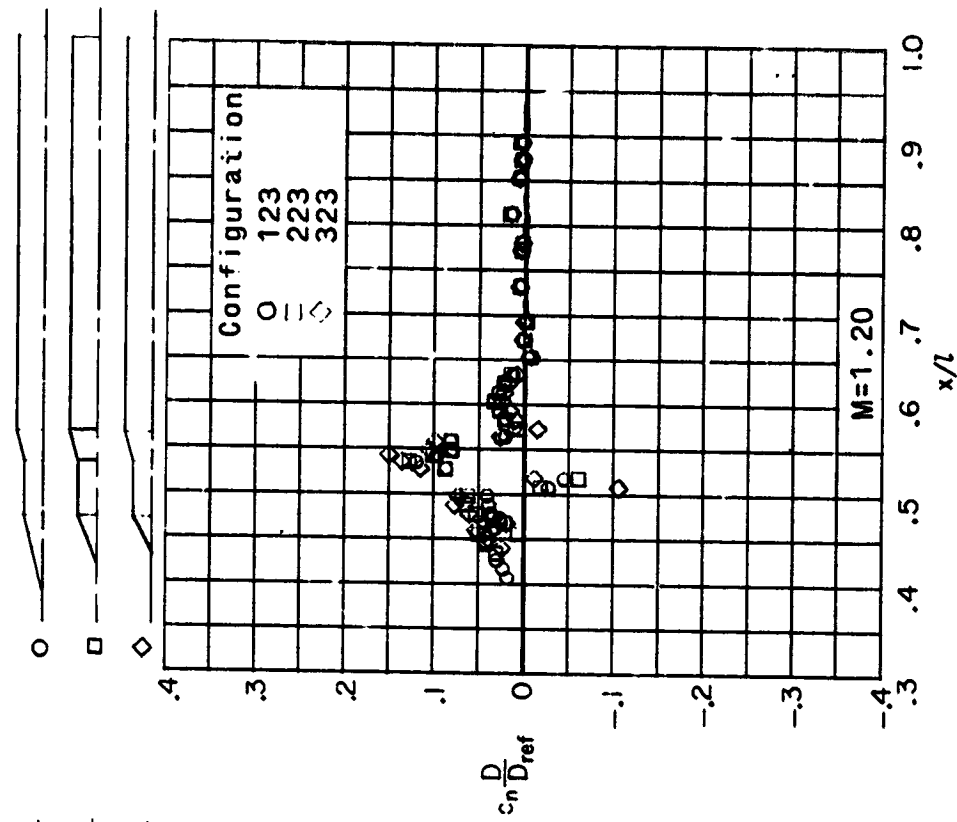
(b) Concluded.

Figure 9.- Continued.



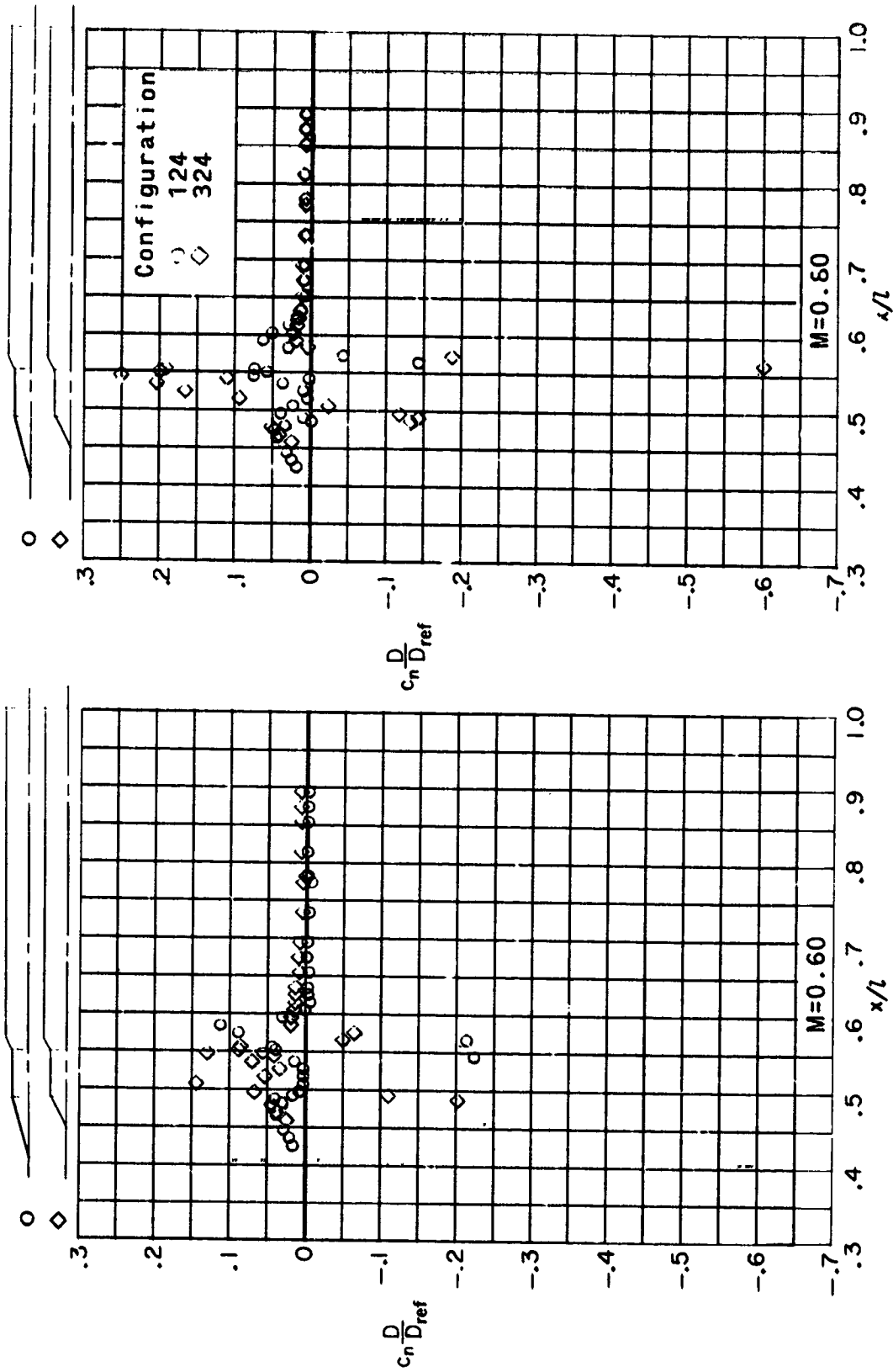
(c) $\delta_P = 15^\circ$.

Figure 9.- Continued.



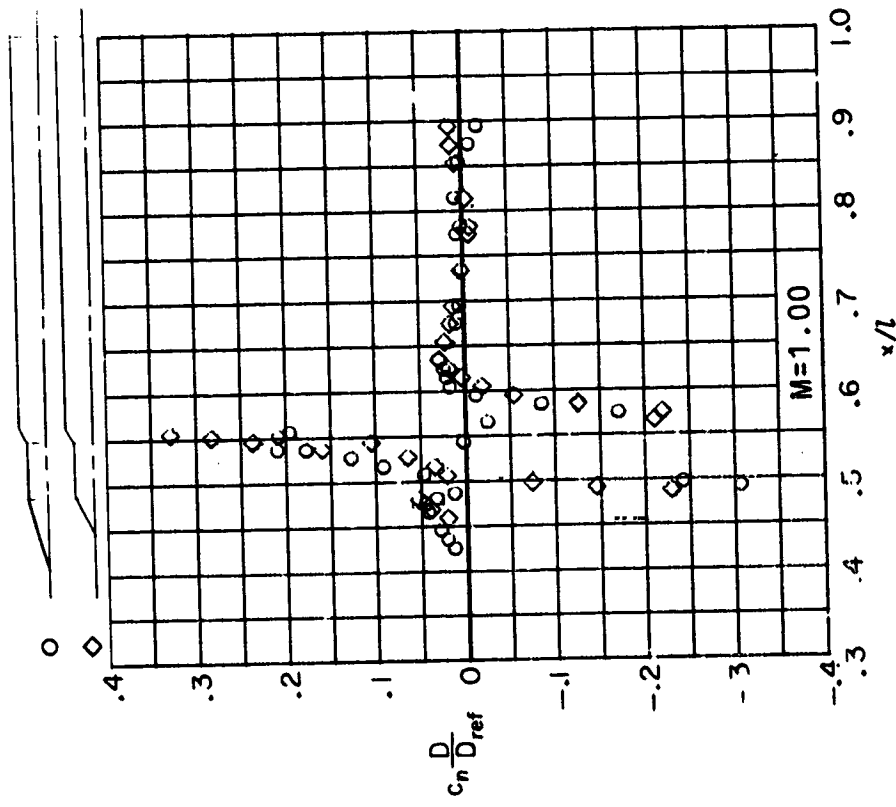
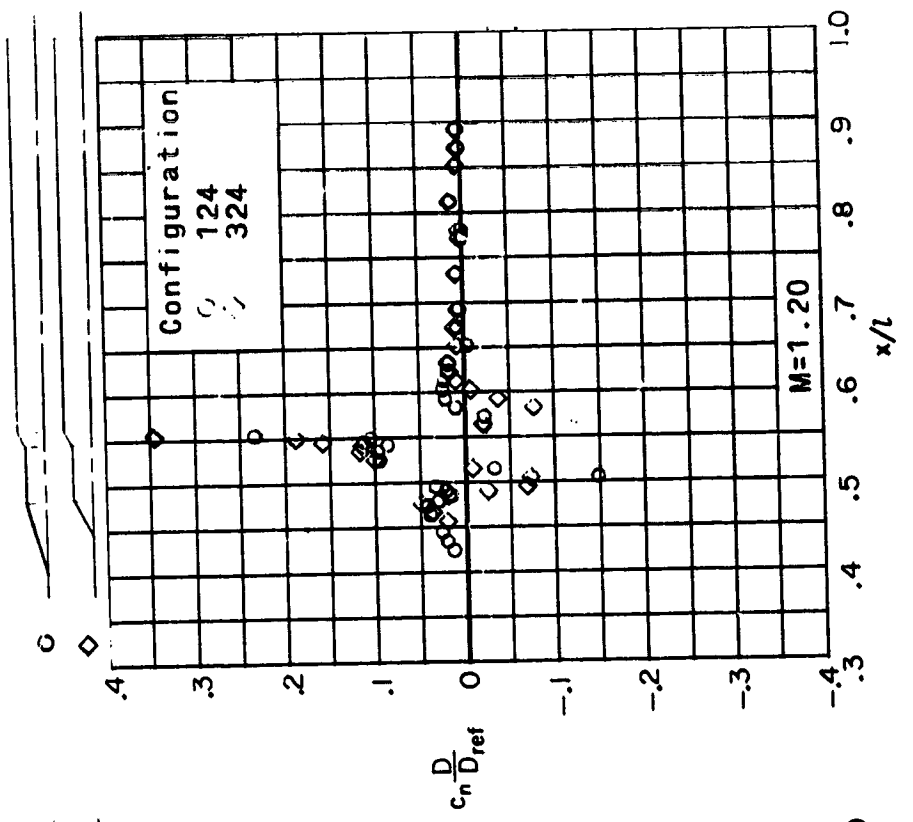
(c) Concluded.

Figure 9.- Continued.



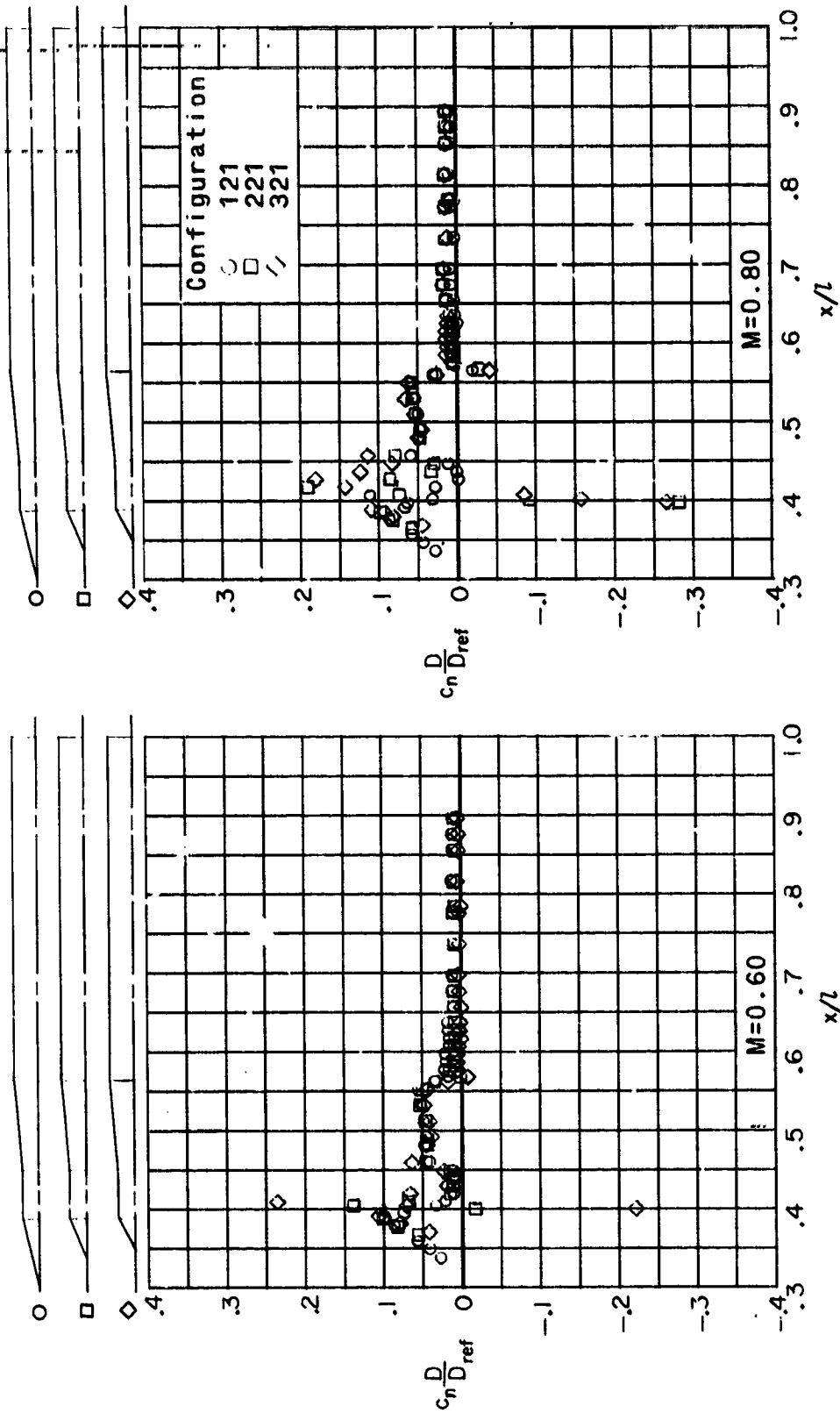
(d) $\delta_F = 30^\circ$.

Figure 9.- Continued.

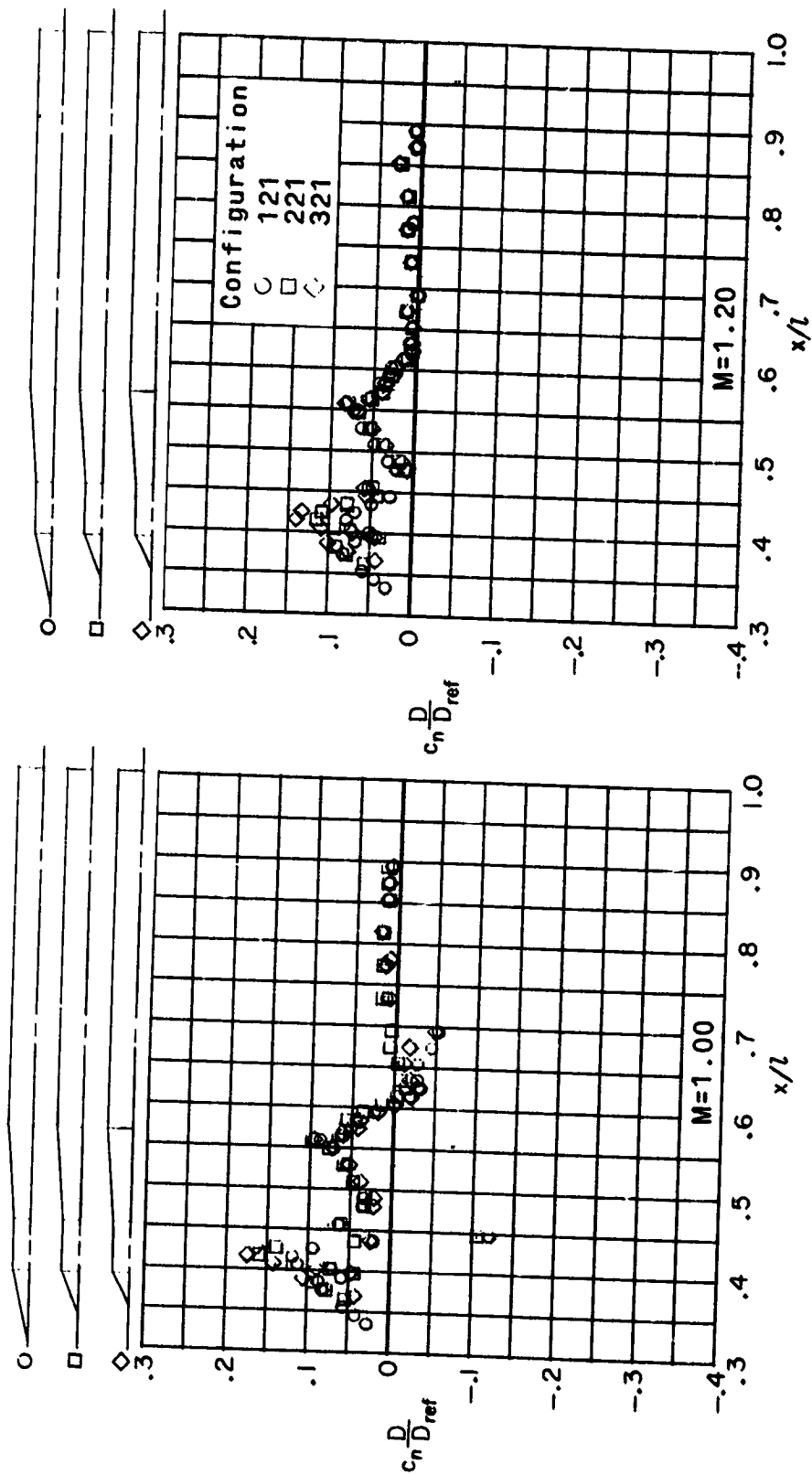


(d) Concluded.

Figure 9.- Concluded.

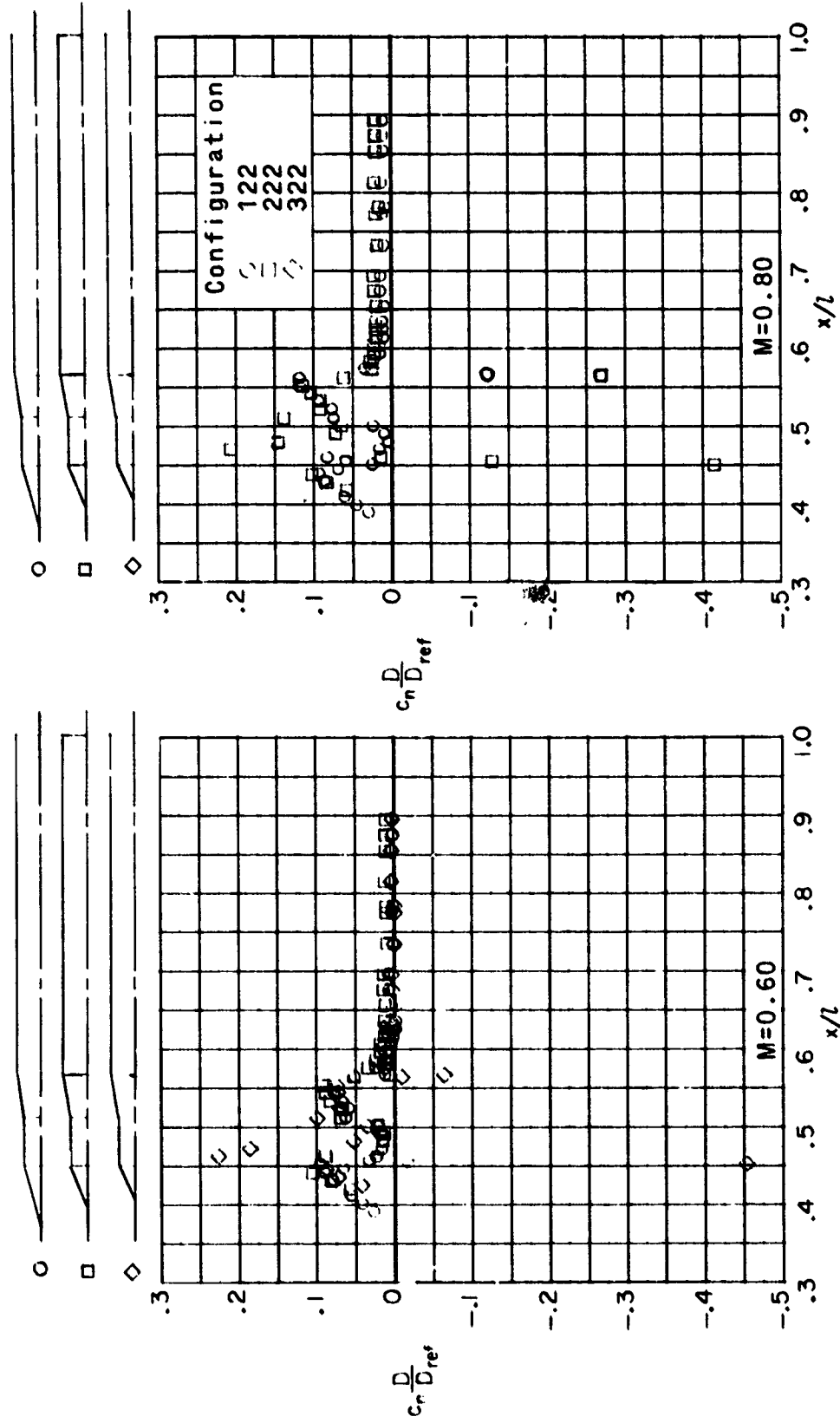


(a) $\delta_P = 50^\circ$
 Figure 10.- Effect of variation in nose-cone angle on load distributions
 at $\alpha = 60^\circ$.



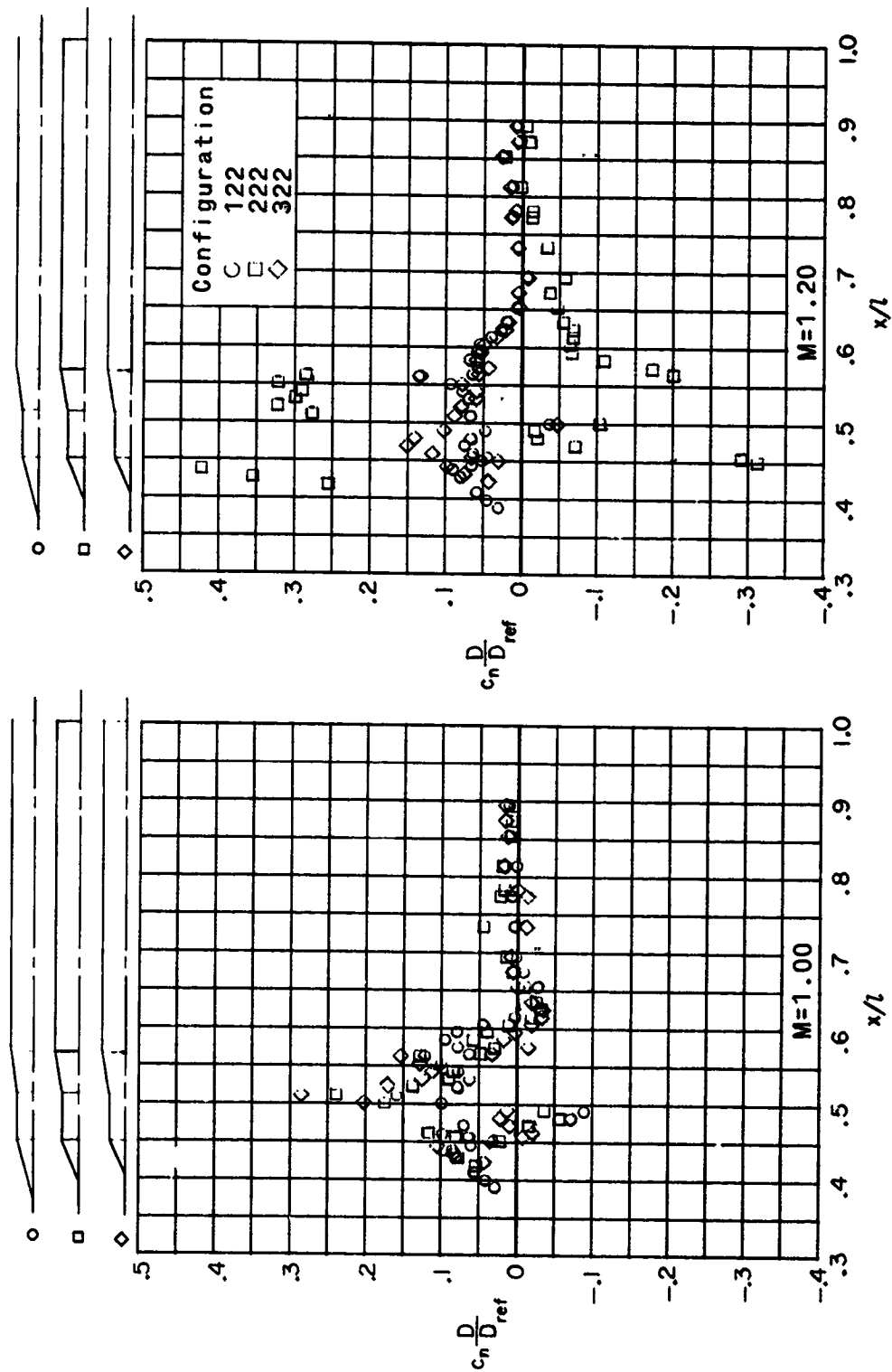
(a) Concluded.

Figure 10.- Continued.



(b) $\delta \bar{p} = 10.1^\circ$

Figure 10.- Continued.



(b) Concluded.

Figure 10.- Continued.

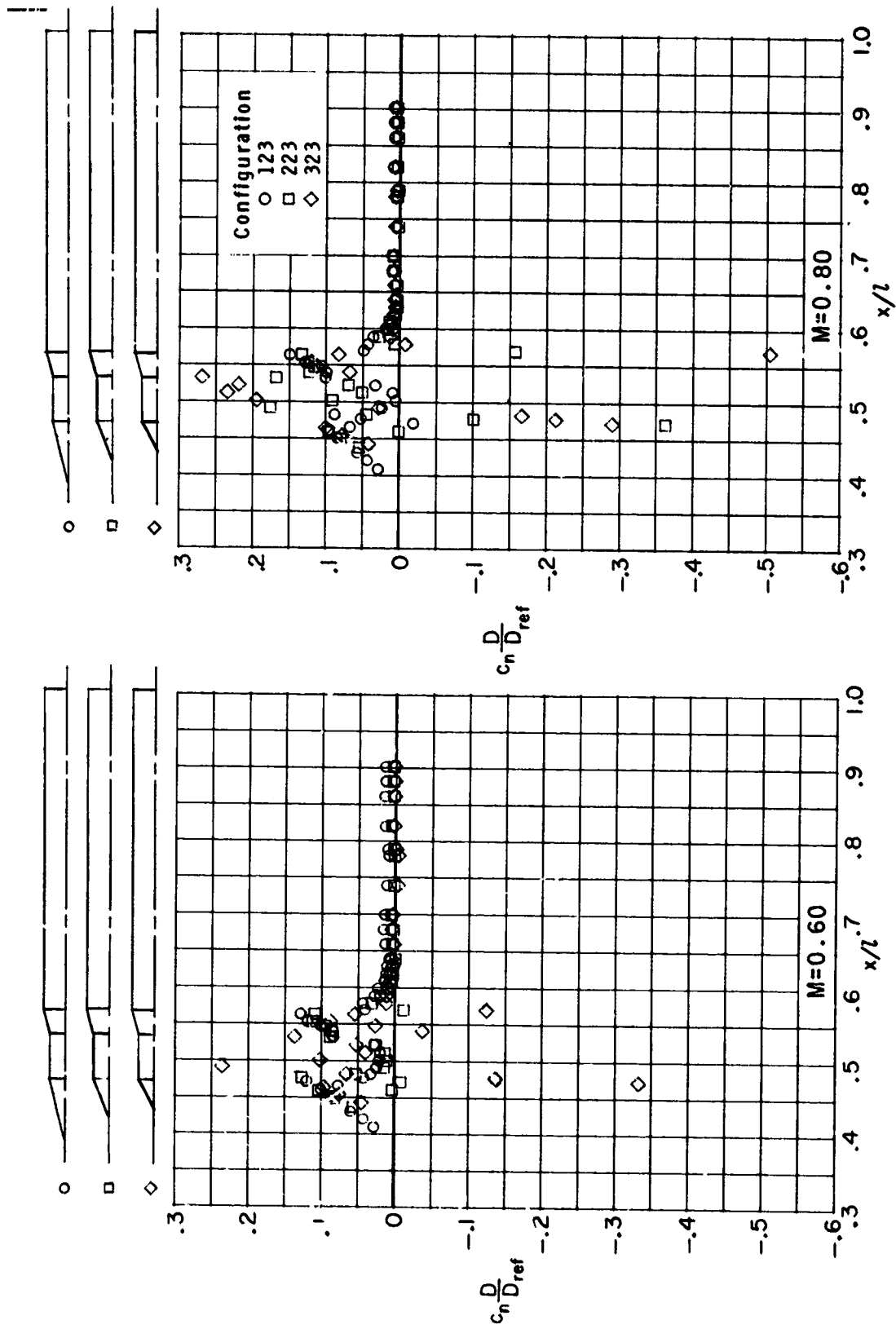
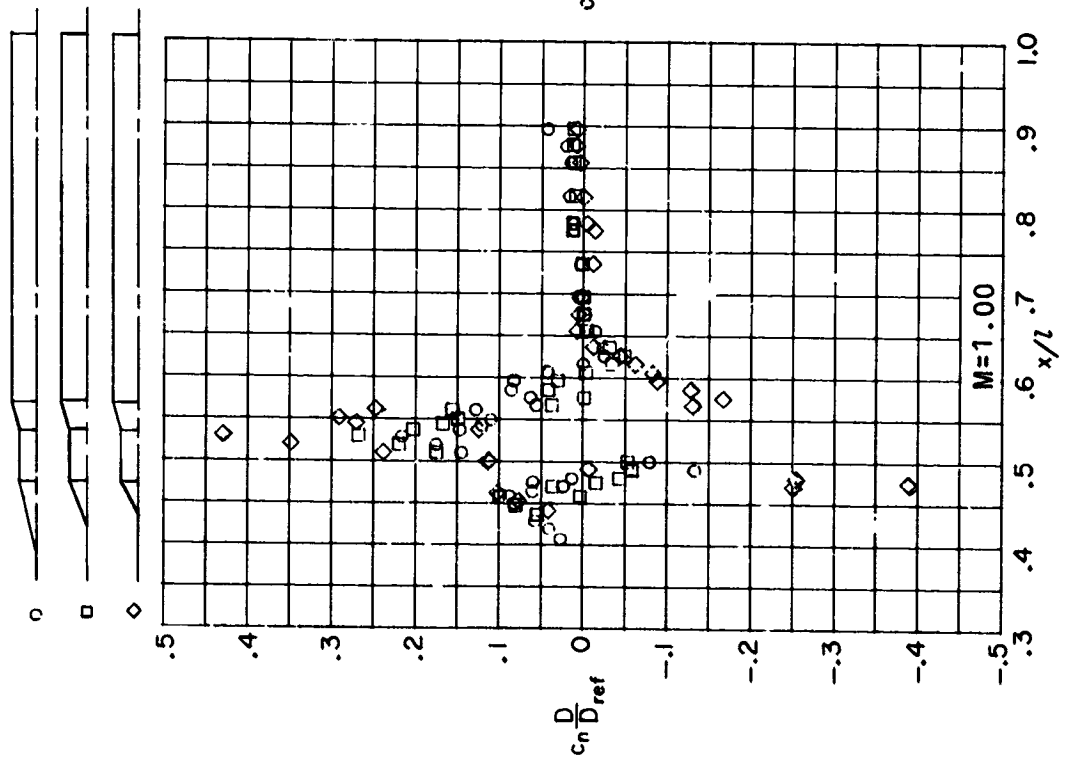
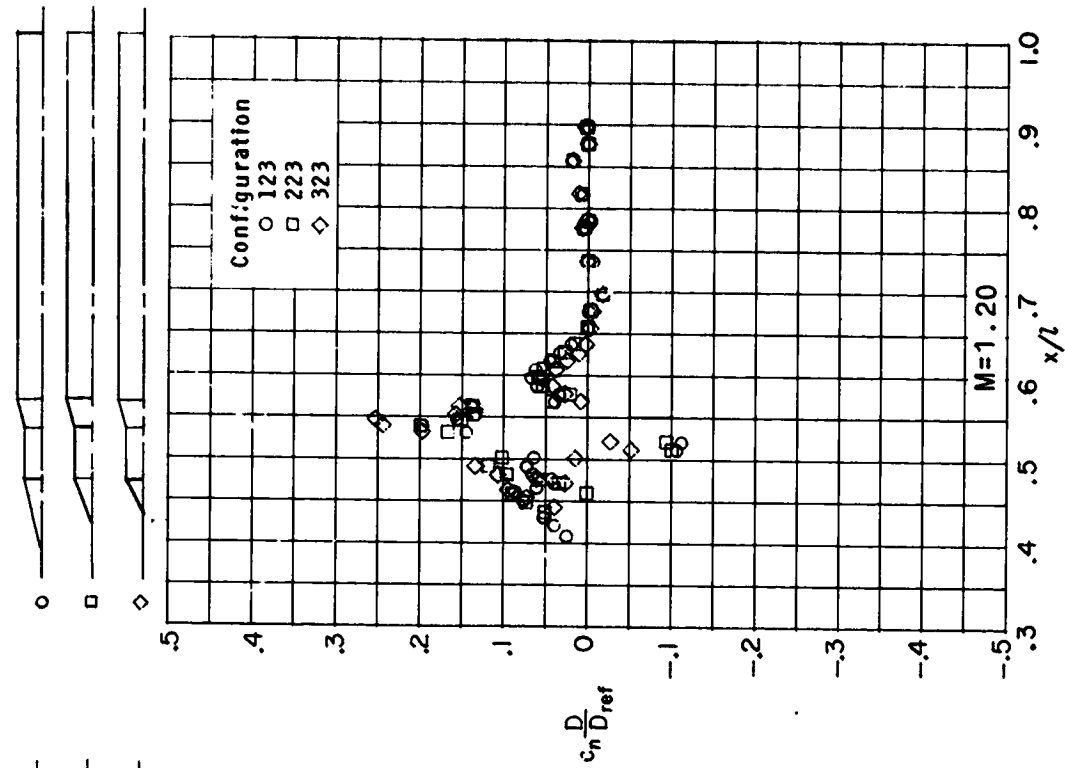
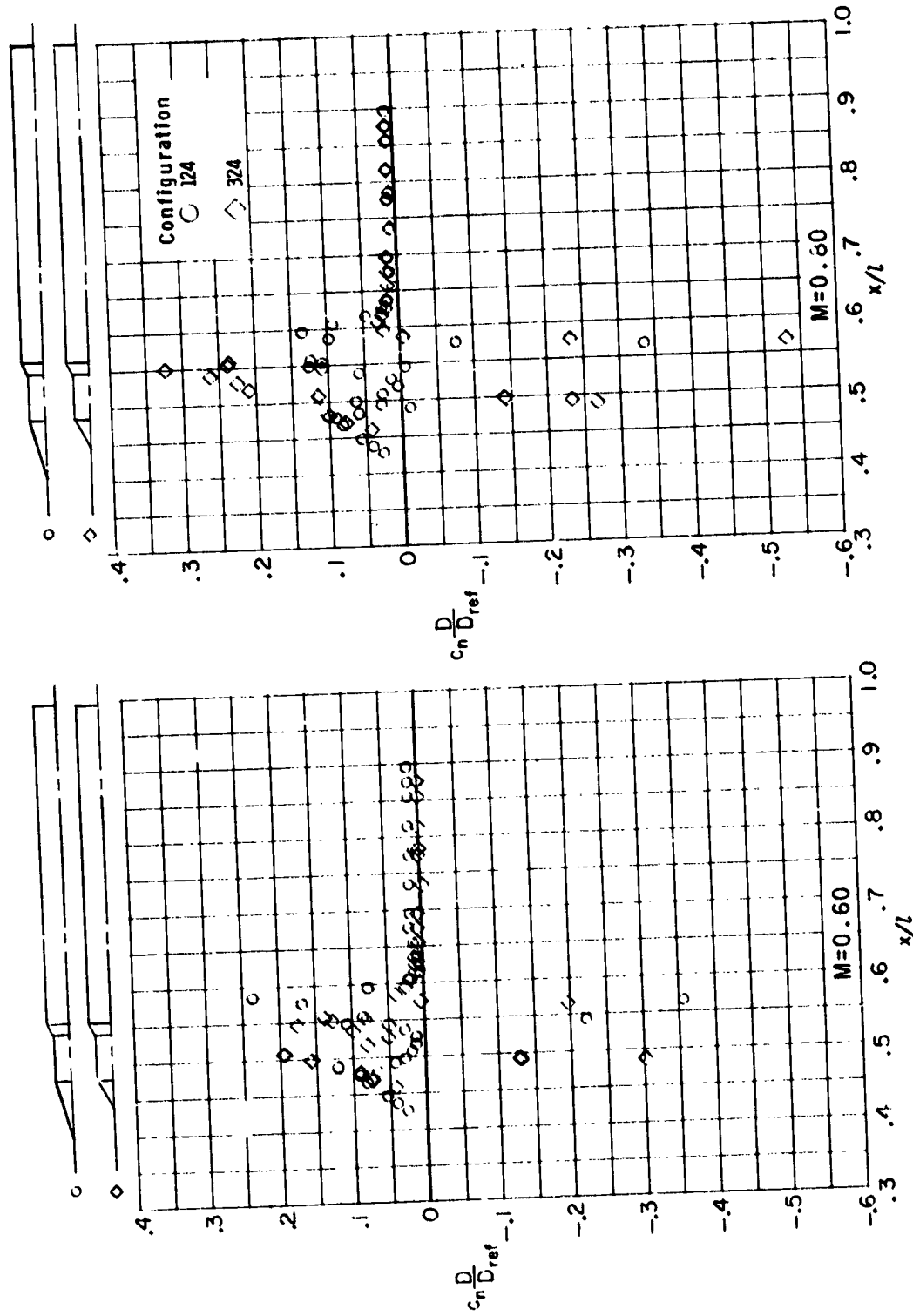
(c) $\delta_F = 150^\circ$.

Figure 10.- Continued.



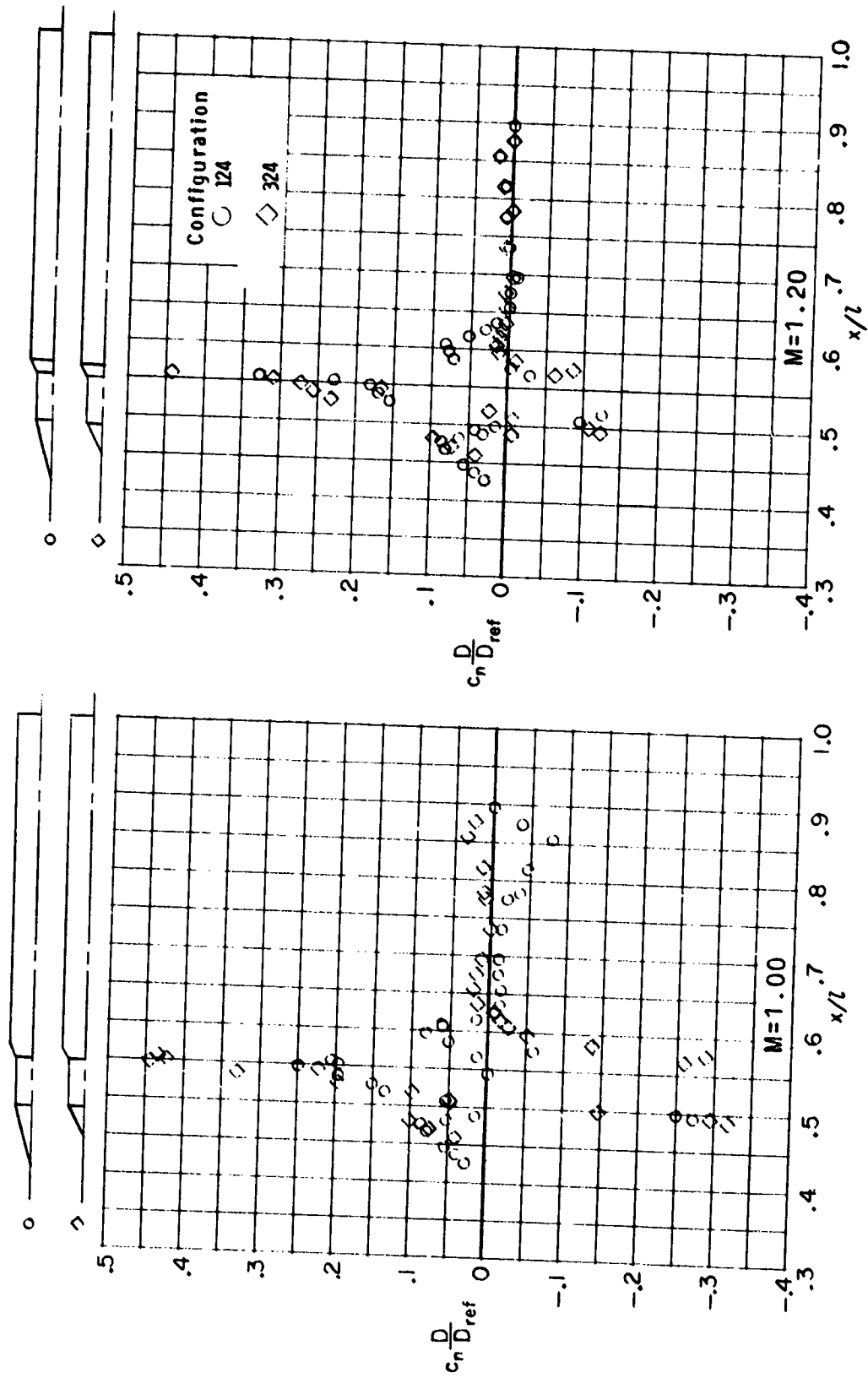
(c) Concluded.

Figure 10.- Continued.



(d) $\delta_F = 30^\circ$.

Figure 10.- Continued.



(d) Concluded.

Figure 10.- Concluded.