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# NASA TECHNICAL MEMORANDUM

(NASA-TM-78279) USER'S GUIDE FOR SKYLAB  
DYNAMICS PROGRAM, SKYDYN (NASA) 73 p  
HC AG/EF A01

CSCL 09B

N80-26056

Unclas  
G3/61 23533

## USERS GUIDE FOR SKYLAB DYNAMICS PROGRAM, SKYDYN

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May, 1980



**NASA**

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Marshall Space Flight Center, Alabama*

TECHNICAL REPORT STANDARD TITLE PAGE

1. REPORT NO. <b>NASA TM-78279</b>		2. GOVERNMENT ACCESSION NO.		3. RECIPIENT'S CATALOG NO.	
4. TITLE AND SUBTITLE <b>Users Guide for Skylab Dynamics Program, SKYDYN</b>				5. REPORT DATE <b>May, 1980</b>	
				6. PERFORMING ORGANIZATION CODE	
7. AUTHOR(S) <b>M. S. Hopkins</b>				8. PERFORMING ORGANIZATION REPORT #	
9. PERFORMING ORGANIZATION NAME AND ADDRESS <b>George C. Marshall Space Flight Center Marshall Space Flight Center, Alabama 35812</b>				10. WORK UNIT NO.	
				11. CONTRACT OR GRANT NO.	
12. SPONSORING AGENCY NAME AND ADDRESS <b>National Aeronautics and Space Administration Washington, D. C. 20546</b>				13. TYPE OF REPORT & PERIOD COVERED  <b>Technical Memorandum</b>	
				14. SPONSORING AGENCY CODE	
15. SUPPLEMENTARY NOTES  <b>Prepared by Systems Dynamics Laboratory, Science and Engineering</b>					
16. ABSTRACT  <p>The Skylab Dynamics Program (SKYDYN) is an extensively modified version of the 6-degree-of-freedom digital program REENTR, developed by Northrop Services, Inc., Huntsville, AL. The program REENTR was modified for the Honeywell CP-V System and was tailored to the specific requirements for Skylab.</p> <p>This user's manual provides a description of the capabilities of SKYDYN, the required input data and the resulting program output.</p>					
17. KEY WORDS			18. DISTRIBUTION STATEMENT  <b>Unclassified-Unlimited</b>		
19. SECURITY CLASSIF. (of this report) <b>Unclassified</b>		20. SECURITY CLASSIF. (of this page) <b>Unclassified</b>		21. NO. OF PAGES <b>73</b>	22. PRICE <b>NTIS</b>

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## TECHNICAL MEMORANDUM

# USERS GUIDE FOR SKYLAB DYNAMICS PROGRAM, SKYDYN

### I. INTRODUCTION

The program SKYDYN was developed to simulate the orbital dynamics of an uncontrolled asymmetric vehicle subjected to perturbing torques due to gravity gradient and aerodynamic forces. The program utilizes an oblate rotating Earth model and a variable step size, five-pass Runge-Kutta integration scheme. Quaternions are used to represent the attitude of the vehicle; thus, there are no restrictions on attitude or small angle motion.

The versatility of the program output allows the user to specify the output parameters without reprogramming. Tape output can be used for plotting or as input to other programs for open-loop calculations that would otherwise increase the run time for the dynamics program.

The input data requirements and a sample data input listing are given in Section II. Program output specifications and a sample program printout are given in Section III.

Appendix A presents definitions of the program variables. The reference frames and corresponding transformation are given in Appendix B. The equations of motion used in the simulation are presented in Appendix C. A listing of the main routine, SKYDYN, and all subroutines used are given in Appendix D.

## II. INPUT DATA REQUIREMENTS

### A. Data Input

Table 1 defines the variables required as input to the program SKYDYN. A change in code number indicates the beginning of a new line of input. Each variable specified to be printed and/or saved on tape (see Code 2) begins a new line of input with a maximum of 90 lines per run.

All angular data are input in degrees and converted to radians at the start of each simulation. A more detailed description of the table input for density and aerodynamic coefficients is presented following the list of input data requirements. The transformation matrix from principal to body axes (Code 25) is used for open-loop calculations only, and if data are unavailable, dummy variables may be used as input.

All data listed in Table 1 are required for initialization of the program. If it is desired to restart the simulation with initial conditions saved from a previous run (IOPT1=1), card input data for Codes 23 and 24, the initial start time and integration step size are ignored. For multiple cases (NCASE > 1, Code 1), data cards Codes 17 through 25 are repeated. Card input data are assigned to Unit 5. Tape input (see IOPT1, Code 19) is assigned to Unit 14.

A typical data input listing is given in Section II. D.

TABLE 1. SKYDYN INPUT

<u>Code</u>	<u>Program Symbol</u>	<u>Variable Definition</u>	<u>Units</u>	<u>Format</u>
1	NCASE	Case number	Unitless	I5 (Col 1-5)
	NX	Number of integration variables	Unitless	I5 (Col 6-10)
2	IVAR	Location of variable in common to be printed and/or saved on tape	Unitless	I3 (Col 1-3)
	ISCAL	Scale factor designation ISCAL=0, Scale factor=1.; ISCAL=1, Scale factor= 57.29578; ISCAL≠0 or ≠1, Scale factor supplied by user.	Unitless	I1 (Col 5)

TABLE 1. (Continued)

<u>Code</u>	<u>Program Symbol</u>	<u>Variable Definition</u>	<u>Units</u>	<u>Format</u>
	SCAL	Scale factor	User Specified	E12.5 (Col 7-18)
	PNAME	Name to be assigned to printed variables	Unitless	A4 (Col 19-22)
	IPW	Print and/or save designation: =0, print and save; =1, print only; =2 save only	Unitless	I1 (Col 23)
3		Blank card to signify end of output variables		
4	ATNM(I) I=1,18	Atmosphere Title Card	Unitless	18A4
5	TLAT(I) I=1,11	Latitude table for density lookup	deg	7F8.3
6	TLNG(I) I=1,37	Longitude table for density lookup	deg	7F8.3
7	FRHO(I,J) I=1,11 J=1,37	Atmospheric density	kg/m <sup>3</sup>	6E9.3
8	NALP	Number of total angle-of-attack values	Unitless	I5 (Col 1-5)
	NPHIA	Number of aerodynamic roll angle values	Unitless	I5 (Col 6-10)
9	TALP(I) I=1,NALP	Total angle-of-attack table for aerodynamic data lookup	deg	7F8.3
10	TPHIA(I) I=1,NPHIA	Aerodynamic roll angle table for aerodynamic data lookup	deg	7F8.3
11	FCA(I,J) I=1,NPHIA J=1,NALP	Axial force coefficient	Unitless	7F8.3
12	FCN(I,J) I=1,NPHIA J=1,NALP	Normal force coefficient	Unitless	7F8.3
13	FCY(I,J) I=1,NPHIA J=1,NALP	Side force coefficient	Unitless	7F8.3



TABLE 1. (Continued)

<u>Code</u>	<u>Program Symbol</u>	<u>Variable Definition</u>	<u>Units</u>	<u>Format</u>
14	FCM(I,J) I=1,NPHIA J=1,NALP	Pitching moment coefficient	Unitless	7F8.3
15	FCEN(I,J) I=1,NPHIA J=1,NALP	Yawing moment coefficient	Unitless	7F8.3
16	FCL(I,J) I=1,NPHIA J=1,NALP	Rolling moment coefficient	Unitless	7F8.3
17	CASE(I) I=1,18	Case title card	Unitless	18A4
18	PROPT	Multiplier for print interval (Print interval=PROPT *DTP)	Unitless	F10.1
19	DT	Initial integration time step	sec	F10.4
	DTP	Output frequency for save tape	sec	F10.4
	DTSAM	Specified time to save variables for restart	sec	F10.4
	TRUN	Total run time	sec	F10.4
	TIME	Initial start time	sec	F10.4
	IOPT1	Initialization option =0, use initial conditions from data pack =1, read in initial conditions from tape	Unitless	I5
20	WT	Vehicle weight	lb	F10.4
	XCG	Vehicle cg in x-direction	ft	F10.4
	YCG	Vehicle cg in y-direction	ft	F10.4
	ZCG	Vehicle cg in z-direction	ft	F10.4
	XMRP	Aerodynamic moment reference point in x-direction	ft	F10.4
	YMRP	Aerodynamic moment reference point in Y-direction	ft	F10.4
	ZMRP	Aerodynamic moment reference point in z-direction	ft	F10.4

TABLE 1. (Continued)

<u>Code</u>	<u>Program Symbol</u>	<u>Variable Definition</u>	<u>Units</u>	<u>Format</u>
21	DREF	Aerodynamic reference diameter	ft	F10.4
	SREF	Aerodynamic reference area	ft <sup>2</sup>	F10.4
22	IXYZ(1,1)	Moment of inertia about x-axis	slugs-ft <sup>2</sup>	F10.1
	IXYZ(2,2)	Moment of inertia about y-axis	slugs-ft <sup>2</sup>	F10.1
	IXYZ(3,3)	Moment of inertia about z-axis	slugs-ft <sup>2</sup>	F10.1
	IXYZ(1,2)	xy product of inertia	slugs-ft <sup>2</sup>	F10.1
	IXYZ(1,3)	xz product of inertia	slugs-ft <sup>2</sup>	F10.1
	IXYZ(2,3)	yz product of inertia	slugs-ft <sup>2</sup>	F10.1
23	PSI	Geocentric latitude (positive north and negative south of equator)	deg	F10.6
	LAMDE	Earth fixed longitude (positive east and negative west of Greenwich)	deg	F10.5
	RMAG	Radius vector magnitude	ft	F10.2
	VIMAG	Inertial velocity	ft/sec	F10.3
	SIGI	Inertial heading (positive clockwise from north)	deg	F10.6
	GAMI	Inertial flight path angle (positive up from local geocentric horizontal)	deg	F10.8
24	PHIBI	Initial bank angle	deg	F10.5
	ALPHAI	Initial total angle-of-attack	deg	F10.5
	PHIAI	Initial aerodynamic roll angle	deg	F10.5

TABLE 1. (Continued)

<u>Code</u>	<u>Program Symbol</u>	<u>Variable Definition</u>	<u>Units</u>	<u>Format</u>
	PQR(I) I=1,3	Initial rates about x, y, and z body axes, respectively	deg/sec	3F10.5
25	ABP(I,J) J=1,3 I=1,3	Transformation matrix from principal axes to body axes	Unitless	610.5
26		Blank card to signify termination of input data		

B. Density Table Input

The density table input is a bivariate function of latitude ( $\psi$ ) and longitude ( $\lambda$ ). The density values were determined for a specified altitude using the Jacchia 1970-3 atmosphere model and predicted solar and geomagnetic data provided by Space Sciences Laboratory, Marshall Space Flight Center.

The dependent density values are input in the following manner:

$$\rho(\psi_1, \lambda_1) \rho(\psi_2, \lambda_1) \dots \rho(\psi_6, \lambda_1)$$

$$\rho(\psi_7, \lambda_1) \dots \rho(\psi_{11}, \lambda_1)$$

$$\vdots \quad \quad \quad \vdots$$

$$\vdots \quad \quad \quad \vdots$$

$$\vdots \quad \quad \quad \vdots$$

$$\rho(\psi_1, \lambda_{37}) \rho(\psi_2, \lambda_{37}) \dots \rho(\psi_6, \lambda_{37})$$

$$\rho(\psi_7, \lambda_{37}) \dots \rho(\psi_{11}, \lambda_{37})$$

### C. Aerodynamic Coefficients Table Input

The aerodynamic coefficients are bivariate functions of aerodynamic roll angle ( $\phi_w$ ) and total angle-of-attack ( $\alpha_T$ ). The dimension of these tables is chosen by the user with the restriction that all six coefficients must have the same dimension.

For the sample case presented, the coefficients are dimensioned 21 x 11 and are input in the following manner:

$C(\phi_{\alpha 1}, \alpha_{T1})$	.....	$C(\phi_{\alpha 7}, \alpha_{T1})$
$C(\phi_{\alpha 8}, \alpha_{T1})$	.....	$C(\phi_{\alpha 14}, \alpha_{T1})$
$C(\phi_{\alpha 15}, \alpha_{T1})$	.....	$C(\phi_{\alpha 21}, \alpha_{T1})$
:		:
:		:
$C(\phi_{\alpha 1}, \alpha_{T11})$	.....	$C(\phi_{\alpha 7}, \alpha_{T11})$
:		:
:		:
$C(\phi_{\alpha 15}, \alpha_{T11})$	.....	$C(\phi_{\alpha 21}, \alpha_{T11})$

D. Sample Data Input Listing

607	1	13	THORO
008			OSQRI
151	1		PHI80
152	1		ALPYO
153	1		PHIAO
503			VRELI
002			DELT1
329	1		GAMR1
328	1		SIGRI
517			VELXI
518			VELVI
519			VELZI
061	1		P 0
021	1		P00T1
526			GG810
431			TOAXO
532			YABXO
410			CAR10
062	1		Q 0
022	1		Q00T1
527			GG820
432			TOAYO
533			YABYO
411			CAR21
063	1		R 0
023	1		R00T1
528			GG830
433			TOAZO
534			YABZO
412			CAR31
154			BR110
155			BR210
156			BR310
157			BR120
158			BR220
159			BR320
160			BR130
161			BR230
162			BR330
181			I8111
182			I8211
183			I8311
184			I8121
185			I8221
186			I8321
187			I8131
188			I8231
189			I8331
501			RHO 1

502  
323 I  
326 I  
331 I  
330 I

QBARI  
LAT I  
LONG I  
GARI I  
SIG I

SSL	SENSITIVES, P (LAT, LONG), 230NM, MEASURED
-50.	-40. -30. -20. -10. 0. 10.
20.	40. 50. 60.
70.	70. 80. 90. 100. 110. 120. 130.
140.	150. 160. 170. 180. 190. 200.
210.	220. 230. 240. 250. 260. 270.
280.	290. 300. 310. 320. 330. 340.
350.	360.
.270E-11	.296E-11 .321E-11 .345E-11 .365E-11 .381E-11 .392E-11
.392E-11	.397E-11 .396E-11 .388E-11 .376E-11
.268E-11	.293E-11 .318E-11 .341E-11 .361E-11 .377E-11
.389E-11	.393E-11 .392E-11 .385E-11 .373E-11
.263E-11	.287E-11 .311E-11 .333E-11 .352E-11 .367E-11
.378E-11	.383E-11 .383E-11 .377E-11 .366E-11
.295E-11	.277E-11 .299E-11 .319E-11 .337E-11 .352E-11
.362E-11	.367E-11 .368E-11 .364E-11 .355E-11
.245E-11	.265E-11 .284E-11 .302E-11 .319E-11 .332E-11
.342E-11	.348E-11 .349E-11 .347E-11 .341E-11
.294E-11	.250E-11 .267E-11 .283E-11 .298E-11 .310E-11
.319E-11	.325E-11 .328E-11 .328E-11 .325E-11
.218E-11	.235E-11 .249E-11 .263E-11 .275E-11 .286E-11
.295E-11	.301E-11 .306E-11 .308E-11 .307E-11
.209E-11	.220E-11 .232E-11 .243E-11 .253E-11 .262E-11
.271E-11	.278E-11 .283E-11 .287E-11 .290E-11
.197E-11	.205E-11 .214E-11 .223E-11 .232E-11 .240E-11
.240E-11	.255E-11 .262E-11 .268E-11 .273E-11
.188E-11	.192E-11 .198E-11 .205E-11 .212E-11 .219E-11
.226E-11	.234E-11 .241E-11 .249E-11 .257E-11
.176E-11	.179E-11 .184E-11 .189E-11 .195E-11 .201E-11
.207E-11	.215E-11 .223E-11 .233E-11 .243E-11
.167E-11	.168E-11 .172E-11 .175E-11 .179E-11 .184E-11
.191E-11	.198E-11 .208E-11 .218E-11 .230E-11
.159E-11	.159E-11 .161E-11 .164E-11 .167E-11 .171E-11
.177E-11	.185E-11 .194E-11 .206E-11 .220E-11
.153E-11	.152E-11 .153E-11 .154E-11 .157E-11 .160E-11
.166E-11	.174E-11 .184E-11 .196E-11 .211E-11
.148E-11	.146E-11 .146E-11 .147E-11 .149E-11 .152E-11
.157E-11	.165E-11 .175E-11 .188E-11 .204E-11
.145E-11	.142E-11 .141E-11 .142E-11 .143E-11 .146E-11
.152E-11	.159E-11 .169E-11 .183E-11 .199E-11
.142E-11	.139E-11 .138E-11 .136E-11 .139E-11 .142E-11
.147E-11	.155E-11 .165E-11 .179E-11 .196E-11
.141E-11	.138E-11 .136E-11 .136E-11 .137E-11 .140E-11
.145E-11	.153E-11 .163E-11 .177E-11 .194E-11
.141E-11	.137E-11 .136E-11 .136E-11 .136E-11 .139E-11

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OF POOR QUALITY

.144E-11	.152E-11	.162E-11	.176E-11	.193E-11	.193E-11	
.140E-11	.137E-11	.136E-11	.135E-11	.136E-11	.139E-11	
.144E-11	.151E-11	.162E-11	.176E-11	.193E-11	.193E-11	
.140E-11	.137E-11	.136E-11	.136E-11	.136E-11	.139E-11	
.144E-11	.152E-11	.162E-11	.176E-11	.193E-11	.193E-11	
.141E-11	.138E-11	.136E-11	.136E-11	.137E-11	.140E-11	
.145E-11	.152E-11	.163E-11	.177E-11	.194E-11	.194E-11	
.142E-11	.139E-11	.138E-11	.138E-11	.139E-11	.142E-11	
.147E-11	.154E-11	.165E-11	.179E-11	.195E-11	.195E-11	
.145E-11	.142E-11	.141E-11	.142E-11	.143E-11	.146E-11	
.151E-11	.159E-11	.169E-11	.183E-11	.199E-11	.199E-11	
.149E-11	.147E-11	.147E-11	.148E-11	.150E-11	.153E-11	
.158E-11	.166E-11	.176E-11	.189E-11	.205E-11	.205E-11	
.155E-11	.154E-11	.155E-11	.157E-11	.159E-11	.163E-11	
.169E-11	.177E-11	.187E-11	.199E-11	.213E-11	.213E-11	
.163E-11	.164E-11	.166E-11	.169E-11	.173E-11	.178E-11	
.184E-11	.191E-11	.201E-11	.212E-11	.225E-11	.225E-11	
.173E-11	.176E-11	.181E-11	.185E-11	.190E-11	.196E-11	
.203E-11	.210E-11	.219E-11	.229E-11	.240E-11	.240E-11	
.165E-11	.191E-11	.198E-11	.205E-11	.212E-11	.218E-11	
.226E-11	.233E-11	.241E-11	.249E-11	.257E-11	.257E-11	
.199E-11	.208E-11	.218E-11	.227E-11	.236E-11	.244E-11	
.252E-11	.259E-11	.266E-11	.271E-11	.276E-11	.276E-11	
.214E-11	.226E-11	.239E-11	.251E-11	.262E-11	.272E-11	
.280E-11	.287E-11	.292E-11	.296E-11	.297E-11	.297E-11	
.229E-11	.244E-11	.260E-11	.275E-11	.288E-11	.300E-11	
.309E-11	.315E-11	.319E-11	.320E-11	.313E-11	.313E-11	
.242E-11	.261E-11	.280E-11	.298E-11	.313E-11	.326E-11	
.336E-11	.342E-11	.344E-11	.342E-11	.337E-11	.337E-11	
.254E-11	.276E-11	.297E-11	.317E-11	.335E-11	.349E-11	
.359E-11	.365E-11	.366E-11	.362E-11	.353E-11	.353E-11	
.263E-11	.267E-11	.310E-11	.332E-11	.351E-11	.367E-11	
.377E-11	.383E-11	.382E-11	.376E-11	.365E-11	.365E-11	
.268E-11	.294E-11	.318E-11	.341E-11	.362E-11	.377E-11	
.388E-11	.393E-11	.392E-11	.385E-11	.373E-11	.373E-11	
.270E-11	.296E-11	.321E-11	.345E-11	.365E-11	.381E-11	
.392E-11	.397E-11	.396E-11	.388E-11	.376E-11	.376E-11	
11	21					
0.0	20.0	40.0	60.0	80.0	90.0	100.0
120.0	140.0	160.0	180.0			
0.0	20.0	40.0	50.0	80.0	90.0	100.0
120.0	140.0	160.0	180.0	200.0	220.0	240.0
260.0	270.0	280.0	300.0	320.0	340.0	360.0
2.401	2.401	2.401	2.401	2.401	2.401	2.401
2.401	2.401	2.401	2.401	2.401	2.401	2.401
2.401	2.401	2.401	2.401	2.401	2.401	2.401
3.166	3.129	2.964	2.787	2.600	2.707	2.517
2.952	3.340	3.630	3.860	3.554	3.212	2.798
2.370	2.625	2.576	2.842	2.945	3.099	3.166
4.124	3.919	3.330	3.036	2.669	2.687	2.710
3.522	4.202	4.713	4.873	4.672	3.909	3.063
2.486	2.628	2.706	3.286	3.699	4.145	4.124

3.366	3.251	2.989	2.560	2.110	1.980	2.154
2.854	3.423	3.857	4.017	3.840	3.187	2.473
1.980	1.988	2.164	2.828	3.187	3.407	3.366
1.433	1.347	1.220	.997	.812	.741	.832
1.122	1.315	1.471	1.518	1.436	1.224	.976
.786	.763	.847	1.125	1.290	1.371	1.433
.001	-.004	-.001	.003	.004	.004	.004
.004	.004	.005	.005	.005	.004	.005
.005	.005	.005	.004	-.001	-.003	.001
-1.529	-1.445	-1.226	-.993	-.801	-.730	-.827
-1.128	-1.317	-1.399	-1.446	-1.359	-1.225	-.974
-.779	-.754	-.839	-1.130	-1.323	-1.492	-1.529
-4.142	-3.905	-3.332	-2.725	-2.111	-1.988	-2.186
-2.943	-3.298	-3.566	-3.515	-3.321	-2.767	-2.419
-1.999	-2.049	-2.204	-2.987	-3.535	-3.971	-4.142
-5.136	-4.899	-4.366	-3.591	-2.760	-2.742	-2.810
-3.513	-3.581	-4.308	-4.308	-3.882	-3.255	-2.962
-2.595	-2.829	-2.868	-3.769	-4.593	-4.956	-5.196
-4.106	-3.966	-3.491	-3.201	-2.700	-2.813	-2.630
-3.044	-3.209	-3.313	-3.344	-3.246	-3.029	-2.901
-2.556	-2.858	-2.760	-3.299	-3.646	-4.007	-4.106
-2.590	-2.590	-2.590	-2.590	-2.590	-2.590	-2.590
-2.590	-2.590	-2.590	-2.590	-2.590	-2.590	-2.590
-2.590	-2.590	-2.590	-2.590	-2.590	-2.590	-2.590
.002	.002	.002	.002	.002	.002	.002
.002	.002	.002	.002	.002	.002	.002
.002	.002	.002	.002	.002	.002	.002
1.314	1.225	.960	.609	.227	-.001	-.224
-.663	-1.096	-1.434	-1.618	-1.404	-1.058	-.632
-.212	-.006	-.235	-.624	-.951	-1.208	-1.314
3.770	3.372	2.366	1.419	.468	-.001	-.472
-1.655	-2.953	-4.022	-4.416	-3.989	-2.759	-1.456
-.440	.010	.493	1.548	2.625	3.566	3.770
6.235	5.657	4.279	2.415	.733	-.001	-.751
-2.691	-4.853	-6.658	-7.368	-6.629	-4.532	-2.357
-.702	-.009	-.780	-2.678	-4.558	-5.923	-6.235
8.578	7.626	5.647	3.026	.903	.000	-.933
-3.422	-6.029	-8.215	-8.985	-8.015	-5.615	-2.993
-.893	.004	.976	3.436	5.971	7.762	8.578
9.330	8.237	5.874	3.115	.922	.000	-.961
-3.578	-6.320	-8.339	-9.236	-8.203	-5.902	-3.149
-.935	.001	-1.009	-3.584	-6.291	-8.460	-9.330
9.153	8.132	5.659	3.040	.900	.000	-.938
-3.465	-6.069	-7.853	-8.640	-7.625	-5.655	-3.020
-.900	.003	.981	3.479	6.114	8.393	9.153
7.605	6.757	4.746	2.578	.734	.000	-.768
-2.778	-4.661	-6.146	-6.438	-5.715	-3.928	-2.312
-.717	-.007	-.800	-2.838	-5.037	-6.867	-7.605
4.644	4.181	3.073	1.695	.491	.000	-.500
-1.643	-2.777	-3.668	-3.886	-3.295	-2.281	-1.406
-.468	.006	.526	1.785	3.189	4.224	4.644
1.703	1.552	1.143	.716	.248	-.001	-.246



-678	-1.041	-1.298	-1.390	-1.271	-982	-649
-239	-002	.257	.739	1.189	1.566	1.703
.000	.000	.000	.000	.000	.000	.000
.000	.000	.000	.000	.000	.000	.000
.000	.000	.000	.000	.000	.000	.000
.002	.002	.002	.002	.002	.002	.002
.002	.002	.002	.002	.002	.002	.002
.000	.408	.724	.929	.994	1.048	.966
.985	.021	.473	.001	.460	.779	.528
.090	1.005	.977	.943	.720	.405	.000
.000	-1.143	-1.040	-2.280	-2.295	-2.346	-2.330
-2.037	-2.322	-1.304	.001	1.368	2.137	2.264
2.109	2.269	2.307	2.457	2.033	1.209	.000
.000	-1.947	-3.375	-3.931	-3.711	-3.551	-3.778
-4.367	-3.876	-2.320	.001	2.307	3.585	3.748
3.445	3.516	3.775	4.321	3.589	2.037	.000
.000	-2.640	-4.490	-4.959	-4.615	-4.280	-4.721
-5.576	-4.840	-3.876	.001	2.007	4.482	4.809
4.423	4.360	4.776	5.568	4.740	2.686	.000
.000	-2.857	-4.670	-5.103	-4.715	-4.348	-4.857
-5.626	-5.072	-2.923	.001	2.875	4.714	5.065
4.626	4.515	4.945	5.806	4.990	2.933	.000
.000	-2.821	-4.495	-4.973	-4.609	-4.269	-4.734
-5.637	-4.871	-2.754	.001	2.674	4.510	4.832
4.431	4.359	4.760	5.628	4.846	2.911	.000
.000	-2.335	-3.752	-4.169	-3.703	-3.545	-3.825
-4.494	-3.731	-2.148	.001	1.999	3.114	3.659
3.464	3.615	3.834	4.548	3.973	2.374	.000
.000	-1.426	-2.388	-2.663	-2.348	-2.372	-2.392
-2.613	-2.194	-1.264	.001	1.136	1.778	2.179
2.186	2.424	2.421	2.784	2.476	1.442	.000
.000	-5.055	-8.840	-1.043	-1.011	-1.066	-988
.998	.783	.429	.002	.418	.733	.940
.951	1.074	1.027	1.070	.874	.510	.000
.001	.001	.001	.001	.001	.001	.001
.001	.001	.001	.001	.001	.001	.001
.001	.001	.001	.001	.001	.001	.001
.332	.332	.332	.332	.332	.332	.332
.332	.332	.332	.332	.332	.332	.332
.332	.332	.332	.332	.332	.332	.332
-1.578	-1.492	-1.249	-937	-497	-317	-150
.030	.075	.169	.335	.116	.009	.086
.175	.339	.516	.951	1.235	1.468	1.578
-3.628	-3.294	-2.490	-1.632	-.695	-.269	.080
.606	1.117	1.598	1.784	1.568	.832	.346
.037	-.292	-.779	-1.774	-2.778	-3.533	-3.628
-6.041	-4.677	-3.778	-2.263	-.074	-.192	.355
1.525	2.804	3.719	4.023	3.678	2.383	1.082
.277	-.203	-.935	-2.577	-4.119	-5.011	-5.041
-6.132	-5.639	-4.170	-2.280	-.928	-.068	.652
2.423	4.102	5.471	5.782	5.210	3.532	1.820

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.594	-.069	-.925	-2.845	-4.627	-5.930	-6.132
-6.423	-5.807	-4.045	-2.124	-.730	.000	.785
2.755	4.593	5.990	6.378	5.757	4.025	2.166
.747	-.001	-.846	-2.772	-4.629	-6.051	-6.423
-5.767	-5.251	-3.564	-1.858	-.593	.068	.872
2.875	-4.740	-5.988	-6.346	-5.740	-4.192	-2.317
-.833	.061	-.708	-2.469	-4.171	-5.535	-5.767
-4.302	-3.842	-2.578	-1.353	-.329	.193	.904
2.722	4.323	5.358	5.334	4.938	3.662	2.292
.884	.177	-.426	-1.721	-2.977	-4.008	-4.302
-2.161	-1.895	-1.326	-.693	-.155	.265	.735
1.923	3.011	3.712	3.821	3.383	2.585	1.727
-.732	-.246	-.201	-.824	-1.462	-1.933	-2.161
-.487	-.419	-.199	-.089	.091	.305	.518
1.035	1.376	1.648	1.731	1.630	1.318	1.013
.518	.297	.076	-.122	-.260	-.439	-.487
.304	.304	.304	.304	.304	.304	.304
.304	.304	.304	.304	.304	.304	.304
.304	.304	.304	.304	.304	.304	.304
-.298	-.298	-.298	-.298	-.298	-.298	-.298
-.298	-.298	-.298	-.298	-.298	-.298	-.298
-.298	-.298	-.298	-.298	-.298	-.298	-.298
-.421	-.143	.121	.527	.728	.706	.788
.663	-.413	-.038	-.536	-.665	-.824	-.908
-.836	-1.134	-1.050	-1.006	-.827	-.651	-.421
-.719	.115	.910	1.583	2.049	2.062	2.061
1.976	1.379	.449	-.686	-1.590	-1.830	-1.769
-1.836	-2.149	-2.227	-2.271	-1.954	-1.522	-.719
-.522	.879	1.971	2.744	3.243	3.221	3.280
3.279	2.552	1.121	-.674	-2.284	-3.015	-2.788
-2.874	-3.251	-3.410	-3.671	-3.120	-1.972	-.522
-.244	1.625	2.925	3.434	3.899	3.865	4.032
4.279	3.427	1.839	-.264	-2.234	-3.302	-3.403
-3.664	-4.011	-4.168	-4.481	-3.656	-2.132	-.244
-.001	2.041	3.273	3.606	3.984	3.948	4.181
4.572	3.735	2.121	.000	-2.043	-3.252	-3.531
-3.858	-4.164	-4.286	-4.579	-3.723	-2.125	-.001
.291	2.253	3.345	3.599	3.862	3.844	4.104
4.550	3.798	2.216	.248	-1.687	-2.918	-3.321
-3.698	-3.969	-4.078	-4.287	-3.398	-1.814	.291
.776	2.418	3.301	3.459	3.255	3.257	3.503
3.977	-3.388	-2.146	-.556	-.970	-1.969	-2.657
-3.070	-3.281	-3.291	-3.314	-2.472	-1.034	.776
.943	1.944	2.537	2.638	2.373	2.378	2.422
2.634	2.316	1.662	.767	-.230	-.983	-1.575
-2.037	-2.117	-2.080	-1.846	-1.191	-.192	.943
.731	1.112	1.261	1.356	1.225	1.350	1.125
1.218	1.096	.846	-.519	-.136	-.138	-.501
-.745	-.659	-.690	-.519	-.137	.270	.731
.436	.436	.436	.436	.436	.436	.436
.436	.436	.436	.436	.436	.436	.436
.436	.436	.436	.436	.436	.436	.436



### III. PROGRAM OUTPUT

#### A. Output Specifications

The program allows the user to specify up to 90 variables, contained in the first 999 locations of the common block, for printing or to be saved on tape. Printed output data are assigned to Unit 6. Each block of printed data are preceded by the simulation time and case title. The block of printed data (6 variables per line of print) uses an E15.8 format with a four character identification name.

All tape output data are written in binary form. Variables saved for restart are assigned to Unit 13. Data to be plotted or used as input to other programs are assigned to Unit 12. The first variable of the data block saved is the simulation time in seconds. The remaining variables, and their order of output, are specified by the input data (See Section III, Code 2).



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TIME .00000000E 00 SAMPLE CASE

THOR .00000000E 00 QSOR .10000000E 01 PHIB-.92000001E 02 ALPT .86777401E 02 PHIA -.27000000E 03 VREL .24106224E 05  
 DELT .14000000E 02 CAMR .50330791E 24 SICR .37034776E 03 VELX .51434911E 03 VELY-.24100726E 05 VELZ .61097015E 06  
 P .17362300E 01 PDOT .29179373E 03 GGB1-.67537424E 01 TOAX-.19997458E 03 TABY .67337449E 01 CAR1-.44971102E 01  
 Q -.57520600E 01 QDOT .42798320E 02 GGB2 .12011496E 01 TOAY .22367242E 04 TABZ .12011719E 01 CAR2 .37668910E 03  
 R .13772000E 00 RDOT .22653979E 02 GGB3 .14629498E 02 TOAZ .25827463E 01 TABZ-.23889513E 01 CAR3 .13059337E 02  
 BR11 .21336776E 01 BR21-.99916331E 00 BR31-.34891552E 01 BR11-.34891552E 01 BR11-.34891552E 01 BR21-.21323778E 01 BR21-.21323778E 01  
 BR13 .25345245E 09 BR23-.34899497E 01 BR33-.99939083E 00 BR11-.34891552E 01 BR11-.34891552E 01 BR11-.34891552E 01  
 BR12-.78475105E 00 BR22-.27859224E 01 BR13 .61882822E 00 BR23-.78524506E 00 BR23-.78524506E 00 BR23-.78524506E 00  
 RHO .73723390E 14 QBAR .21420701E 05 LAT .00000000E 00 LONI .00000000E 00 CAMI .49239970E 24 SICI .40000000E 02

TIME .50460000E 04 SAMPLE CASE

THOR .14000000E 01 QSOR .10000039E 01 PHIB-.14847984E 03 ALPT .10656796E 03 PHIA .31927640E 03 VREL .24091804E 05  
 DELT .14000000E 02 CAMR .03026439E 01 SICR .43189544E 02 VELX-.68698884E 04 VELY-.15065303E 05 VELZ .17500441E 05  
 P .16769681E 01 PDOT .73576451E 03 GGB1 .59038450E 04 TOAX-.79386784E 02 TABY .59892318E 00 CAR1-.25422781E 01  
 Q .29990150E 00 QDOT .31259377E 02 GGB2 .19439304E 01 TOAY .39763889E 01 TABY .98836943E 01 CAR2 .25659871E 00  
 R .43336474E 00 RDOT .42785581E 02 GGB3 .37751404E 01 TOAZ .31983303E 01 TABZ .37431571E 01 CAR3 .10902362E 01  
 BR11-.28515458E 00 BR21-.50109348E 00 BR31-.81706463E 00 BR12-.62532898E 00 BR22-.54878170E 01 BR22-.54878170E 01  
 BR13 .72640643E 00 BR23-.66914806E 00 BR33-.15685382E 00 BR11-.84633506E 00 BR11-.84633506E 00 BR11-.84633506E 00  
 BR12-.23265300E 00 BR22-.94539474E 00 BR32-.22825910E 00 BR13 .47915756E 00 BR23-.31565889E 00 BR33 .01902140E 00  
 RHO .69555831E 14 QBAR .17573757E 05 LAT .25984655E 02 LONI .35551530E 03 CAMI .19934758E 01 SICI .45625149E 02

TIME .10080000E 05 SAMPLE CASE

THOR .28000000E 01 QSOR .10000079E 01 PHIB-.55653710E 02 ALPT .93010592E 02 PHIA .31534739E 02 VREL .24067797E 05  
 DELT .14000000E 02 CAMR .53289897E 01 SICR .66409990E 02 VELX-.15995385E 04 VELY-.12560254E 05 VELZ .20468605E 05  
 P .17174721E 01 PDOT .83596535E 03 GGB1-.54336834E 00 TOAX .62465101E 01 TABY .48090324E 00 CAR1-.78386474E 01  
 Q .16766133E 00 QDOT .10221147E 02 GGB2 .21335679E 01 TOAY .34285919E 01 TABY .21678538E 01 CAR2 .16832387E 00  
 R .25983901E 00 RDOT .50209526E 02 GGB3 .30950126E 01 TOAZ .13556632E 01 TABZ .30814558E 01 CAR3-.21595551E 00  
 BR11-.66459686E 01 BR21-.82383186E 00 BR31-.56299585E 00 BR12 .52186970E 00 BR22 .45218628E 00 BR22 .45218628E 00  
 BR13 .85045610E 00 BR23-.34187357E 00 BR33 .39987746E 00 BR11 .11030652E 00 BR21 .74867493E 00 BR21 .74867493E 00  
 BR12-.98880791E 00 BR22 .16072869E 01 BR32 .14843419E 00 BR13 .10063051E 00 BR23-.66276666E 00 BR33 .74202022E 00  
 RHO .42199782E 14 QBAR .12222299E 05 LAT .45850138E 02 LONI .23945043E 03 CAMI .18323906E 01 SICI .67444995E 02

TIME .15120000E 05 SAMPLE CASE

THOR .42000000E 01 QSOR .10000119E 01 PHIB-.64085556E 02 ALPT .12164011E 03 PHIA .94233077E 02 VREL .24067260E 05  
 DELT .14000000E 02 CAMR .53421578E 01 SICR .10721627E 03 VELX-.12625363E 05 VELY .20434181E 05 VELZ .15124531E 04  
 P .17108091E 01 PDOT .86864621E 03 GGB1-.24130842E 01 TOAX .15920150E 02 TABY .22539641E 01 CAR1-.41579238E 01  
 Q .22888160E 00 QDOT .11841670E 02 GGB2 .17522241E 01 TOAY .14561135E 02 TABY .17536805E 01 CAR2 .32635276E 01  
 R .25570274E 00 RDOT .46911601E 02 GGB3 .30446860E 00 TOAZ .77407638E 02 TABZ .31220931E 00 BR22 .50280950E 00 BR22 .50280950E 00  
 BR11-.52458663E 00 BR21-.76576108E 00 BR31-.37207220E 00 BR12 .84909478E 00 BR12 .84909478E 00 BR12 .84909478E 00  
 BR13 .62842761E 01 BR23 .40104102E 00 BR33 .91395269E 00 BR11-.60225642E 00 BR21 .77832291E 00 BR21 .77832291E 00  
 BR12-.73231543E 00 BR22 .62706959E 00 BR32 .26554769E 00 BR13 .31650678E 00 BR33 .31857627E 01 BR33 .94810399E 00  
 RHO .29633506E 14 QBAR .85822802E 06 LAT .47867339E 02 LONI .24737058E 03 CAMI .10900868E 03 SICI .10647919E 03

TIME .20160000E 05 SAMPLE CASE

THOR .56000000E 01 QSQR .10000159E 01 PHIB-.92602805E 02 ALPT .3425274E 02 PHIA .15911975E 03 VREL .24093032E 05  
 DELT .14000000E 02 GAMR .98312027E 01 SIGR .13428372E 03 VELX .19874588E 05 VELY .48548482E 04 VELZ .12726749E 06  
 P .1634588E 01 PDDT .72622674E 03 GCBI-.24478415E 00 TOAX-.29721171E 02 TABX-.24775627E 00 CAR1-.55804310E 01  
 Q .13251078E 00 QDDT .34428498E 02 GCBI-.36302376E 00 TOAY-.25061130E 01 TABY-.38809489E 00 CAR2-.37029733E 00  
 R .44714938E 00 RDDT .34141259E 02 GCBI-.37371921E 00 TOAZ-.11886536E 01 TABZ .86185068E 00 CAR3 .92113528E 01  
 BR11 .82491620E 00 BR21-.56476793E 01 BR12-.20150425E 00 BR22 .33614470E 00 BR23 .92005448E 00  
 BR13-.52832358E 00 BR23-.75376000E 00 BR11 .55511788E 00 BR21 .83111308E 00 BR22 .33614470E 00 BR23 .92005448E 00  
 BR12-.82860342E 00 BR22-.54035081E 00 BR13-.13620922E 00 BR23-.13179490E 00 BR31-.34553815E 01  
 BR32-.26316836E-14 QBAR .76381219E-06 LAT -.30025320E 02 LONI .20786087E 03 GANI-.10829239E-01 SIGI .13203993E 03

TIME .25200000E 05 SAMPLE CASE

THOR .76000000E 01 QSQR .10000199E 01 PHIB-.89926058E 02 ALPT .91196217E 02 PHIA .22676562E 03 VREL .24113241E 06  
 DELT .14000000E 02 GAMR .20195882E 01 SIGR .14279189E 03 VELX .50343715E 03 VELY-.17565441E 05 VELZ-.16514895E 05  
 P .17391894E 01 PDDT .29290790E 03 GCBI-.23098630E 00 TOAX-.33388075E 01 TABX .19769823E 00 CAR1-.68018946E 01  
 Q .83603655E 01 QDDT .47033452E 02 GCBI-.71178876E 00 TOAY-.14941619E 01 TABY-.72673058E 00 CAR2 .11788410E 01  
 R .11138874E 00 RDDT .11908389E 02 GCBI-.66969949E 00 TOAZ .14447640E 01 TABZ .65525185E 00 CAR3-.31058738E 00  
 BR11-.20878037E 01 BR21-.99982021E 00 BR12-.72845624E 00 BR22 .14334069E 01 BR32 .68502812E 00  
 BR13-.68488906E 00 BR23-.15248600E 01 BR11-.18770412E 01 BR21 .6175713E 00 BR31-.78619451E 00  
 BR12-.78512956E 00 BR22 .47780779E 00 BR32 .39419383E 00 BR13 .61911005E 00 BR23 .62465457E 00 BR33 .47605332E 00  
 BR34-.26629954E-14 QBAR .71419721E-06 LAT -.45909697E 01 LONI .18237691E 03 GANI-.27284854E-02 SIGI .13984665E 03

TIME .30240000E 05 SAMPLE CASE

THOR .84000000E 01 QSQR .10000238E 01 PHIB-.15057682E 03 ALPT .10550746E 03 PHIA .28242493E 03 VREL .24102779E 05  
 DELT .14000000E 02 GAMR .83478081E 01 SIGR .13883130E 03 VELY .64435305E 04 VELY-.22682484E 05 VELZ .49974140E 04  
 P .16685238E 01 PDDT .27485078E 03 GCBI-.29431738E 00 TOAX-.36509205E 02 TABX .29066646E 00 CAR1-.49371637E 01  
 Q .11994295E 00 QDDT .48753305E 02 GCBI-.36294657E 01 TOAY .19398469E 02 TABY .36314056E 01 CAR2 .19840531E 00  
 R .50414431E 00 RDDT .20554326E 02 GCBI-.22428856E 01 TOAZ-.18816029E 02 TABZ .22447672E 01 CAR3 .48341630E 01  
 BR11-.26738262E 00 BR21-.4734446E 00 BR31-.83938097E 00 BR12-.94109294E 00 BR22 .59140360E 01 BR32 .33315752E 00  
 BR13 .20734197E 00 BR23 .87893180E 00 BR33-.42969288E 00 BR11 .83849382E 00 BR21 .17726502E 00 BR31 .51544192E 00  
 BR12-.51920151E 00 BR22 .54766614E 00 BR32 .65623092E 00 BR13 .16593085E 00 BR23 .81779353E 00 BR33 .55120629E 00  
 BR34-.39410736E-14 QBAR .88331002E-06 LAT .21651254E 02 LONI .15272397E 03 GANI .96768489E-02 SIGI .13623309E 03

TIME .35280000E 05 SAMPLE CASE

THOR .98000000E 01 QSQR .10000278E 01 PHIB-.57168979E 02 ALPT .94970126E 02 PHIA .15246627E 03 VREL .24073928E 05  
 DELT .14000000E 02 GAMR .81904632E 01 SIGR .11920856E 03 VELX .20857588E 04 VELY .63072732E 04 VELZ .23140179E 05  
 P .17314916E 01 PDDT .67096724E 03 GCBI-.65834859E 00 TOAX .60909402E 01 TABX .59743919E 00 CAR1-.87391084E 01  
 Q .13844598E 00 QDDT .27343138E 02 GCBI-.12049614E 01 TOAY .40612918E 01 TABY .12455743E 01 CAR2 .9377492E 01  
 R .19042582E 00 RDDT .43338830E 02 GCBI-.36304254E 01 TOAZ-.40890499E 02 TABZ .36263363E 01 CAR3 .94304181E 01  
 BR11 .86639555E 01 BR21 .83715151E 00 BR31 .54014900E 00 BR12 .26199547E 00 BR22 .50403256E 00 BR32 .82311071E 00  
 BR13 .96121126E 00 BR23-.2128291E 00 BR33-.17565346E 00 BR11 .1902277E 00 BR21 .56121353E 00 BR31-.80553104E 00  
 BR12-.30754901E 00 BR22 .81338905E 00 BR32 .49397728E 00 BR13 .93237276E 00 BR23 .15375084E 00 BR33-.32728662E 00  
 BR34-.39717499E-14 QBAR .11509266E-05 LAT .43301751E 02 LONI .12554690E 03 GANI .60318506E-02 SIGI .11789020E 03

## Appendix A

### PROGRAM VARIABLE DEFINITIONS

The following program variables, located in the COMMON BLOCK, are alphabetized according to their Fortran Mnemonics.

<u>Program Symbol</u>	<u>Variable Definition</u>	<u>Units</u>
ABI(3,3)	Transformation matrix from I to B-frame	Unitless
ACCOM(582)	Dummy common	Unitless
ADG(3,3)	Transformation matrix from G to D-frame	Unitless
ADI(3,3)	Transformation matrix from I to D-frame	Unitless
ADR(3,3)	Transformation matrix from R to D-frame	Unitless
AGR(3,3)	Transformation matrix from R to G-frame	Unitless
AIB(3,3)	Transformation matrix from B to I-frame	Unitless
AID(3,3)	Transformation matrix from D to I-frame	Unitless
AIG(3,3)	Transformation matrix from G to I-frame	Unitless
ALPHT	Total angle-of-attack	rad
ARB(3,3)	Transformation matrix from B to R-frame	Unitless
ARD(3,3)	Transformation matrix from D to R-frame	Unitless
ARI(3,3)	Transformation matrix from I to R-frame	Unitless
ARP(3,3)	Transformation matrix from P to R-frame	Unitless
ATCOM(45)	Dummy common	Unitless
CA	Axial force coefficient	Unitless
CCCOM(13)	Dummy common	Unitless



<u>Program Symbol</u>	<u>Variable Definition</u>	<u>Units</u>
CH(3)	Coefficients for geodetic latitude computations	Unitless
CEN	Yawing moment coefficient	Unitless
CL	Rolling moment coefficient	Unitless
CLMNT(3)	Aerodynamic moment coefficients about vehicle center of mass	Unitless
CM	Pitching moment coefficient	Unitless
CN	Normal force coefficient	Unitless
CNV	57.29577951	deg/rad
CR	Oblate earth radial coefficient	Unitless
CW	Oblate earth spin axis coefficient	Unitless
CPLMN(3)	Aerodynamic moment coefficient vector about moment reference point	Unitless
CXYZ(3)	Aerodynamic force coefficient vector	Unitless
CY	Side force coefficient	Unitless
DIW(3)	Dummy variable used in gravity gradient torque calculation	slugs-ft <sup>2</sup>
DPSI	Difference between geodetic and geocentric latitudes	rad
DREF	Aerodynamic reference diameter	ft
DT	Integration time step	sec
DTP	Output frequency for tape save	sec
DTSAM	Specified time to save variables for restart	sec
EPCOM(66)	Dummy common	Unitless
FAB(3)	B-frame aerodynamic forces	lb
FAI(3)	I-frame aerodynamic forces	lb
FAR(3)	R-frame aerodynamic forces	lb
FARC(3)	R-frame aerodynamic force coefficients	Unitless
FCA(21,11)	Table of axial force coefficients	Unitless
FCEN(21,11)	Table of yawing moment coefficients about moment reference point	Unitless

<u>Program Symbol</u>	<u>Variable Definition</u>	<u>Units</u>
FCL(21,11)	Table of rolling moment coefficients about moment reference point	Unitless
FCM(21,11)	Table of pitching moment coefficients about moment reference point	Unitless
FCN(21,11)	Table of normal force coefficients	Unitless
FCY(21,11)	Table of side force coefficients	Unitless
FOMI(3)	Aerodynamic term in translational acceleration calculation	ft/sec <sup>2</sup>
FRHO(11,37)	Table of atmospheric densities	kg/m <sup>3</sup>
G(3)	Gravitational acceleration	ft/sec <sup>2</sup>
GAMI	Inertial flight path angle (positive up from local geocentric horizontal)	rad
GAMR	Relative flight path angle (positive up from local geodetic horizontal)	rad
GCR	Temporary variable in acceleration of gravity calculation	ft/sec <sup>2</sup>
GGB(3)	Gravity gradient torques in B-frame	ft-lb
GMAG	Temporary variable in acceleration of gravity calculation	ft/sec <sup>2</sup>
GMASI	Reciprocal of vehicle mass	1/slugs
GMASS	Vehicle mass	slugs
H	Geodetic altitude	ft
HB(3)	Angular momentum in B-frame	ft-lb-sec
IXYZ(3,3)	Moment of inertia tensor	slugs-ft <sup>2</sup>
IXYZI(3,3)	Inverse of moment of inertia tensor	1/slugs-ft <sup>2</sup>
LAMDA	Inertial longitude measured in I-frame	rad
LAMDE	Earth fixed longitude	rad
LMRP(3)	Temporary variable in aerodynamic moment calculation	Unitless
OMGE	Earth's rotation rate	rad/sec
PCDUM(12)	Dummy common	Unitless
PHIA	Aerodynamic roll angle	rad

<u>Program Symbol</u>	<u>Variable Definition</u>	<u>Units</u>
PHIBK	Bank angle	rad
PI	$\pi$	rad
PQR(3)	Angular rates in B-frame	rad/sec
PQRD(3)	Angular accelerations in B-frame	rad/sec <sup>2</sup>
PSI	Geocentric latitude (positive north, negative south of equator)	rad
PSID	Geodetic latitude (positive north, negative south of equator)	rad
Q(4)	Quaternion parameters	Unitless
QBAR	Dynamic pressure	lb/ft <sup>2</sup>
QD(4)	Time derivatives of quaternions	1/sec
QSQR	$\sqrt{Q(1)^2 + Q(2)^2 + Q(3)^2 + Q(4)^2}$	Unitless
R(3)	Vehicle I-frame position	ft
R1(3)	Unit vector along vehicle I-frame position	Unitless
RB1(3)	Unit vector along vehicle B-frame position	Unitless
RDOT(3)	Vehicle I-frame translational velocity	ft/sec
RHO	Atmospheric density	slugs/ft <sup>3</sup>
RMAG	Magnitude of vehicle position vector	ft
RPSI	Radius of the earth	ft
RR,RR2	Temporary variables used in gravitational acceleration calculations	Unitless
SD,SJ,SH	Earth's gravitational constants	Unitless
SIGI	Inertial heading (positive clockwise from north)	rad
SIGR	Relative heading (positive clockwise from north)	rad
SPSI,SPSI2	Temporary variables used in gravitational acceleration calculation	Unitless
SREF	Aerodynamic reference area	ft <sup>2</sup>
SWD,SWH	Temporary variables used in gravitational acceleration calculation	Unitless

<u>Program Symbol</u>	<u>Variable Definition</u>	<u>Units</u>
TAB(3)	Total external torques in B-frame	ft-lb
TALP(11)	Table of angle-of-attack values	rad
TEND	Simulation stop time	sec
THOR	Simulation time	hr
TIME	Simulation time	sec
TLAT(11)	Table of geocentric latitude values	rad
TLNG(37)	Table of longitude values	rad
TOA(3)	Aerodynamic torques in B-frame	ft-lb
TPHIA(21)	Table of aerodynamic roll angle values	rad
TRUN	Total run time	sec
TSUM(3)	Time rate of change of vehicle angular momentum	ft lb
TWOPI	2 $\pi$	rad
V(3)	Inertial velocity in I-frame	ft/sec
VACOM(67)	Dummy common	Unitless
VATM(3)	Atmospheric velocity in I-frame	ft/sec
VCCOM(18)	Dummy common	Unitless
VDCOM(107)	Dummy common	Unitless
VDOT(3)	Inertial translation acceleration in I-frame	ft/sec <sup>2</sup>
VID(3)	Inertial velocity in D-frame	ft/sec
VIG(3)	Inertial velocity in G-frame	ft/sec
VIMAG	Magnitude of inertial velocity	ft/sec
VPCOM(39)	Dummy common	Unitless
VRELB(3)	Relative velocity in B-frame	ft/sec
VRELD(3)	Relative velocity in D-frame	ft/sec
VRELG(3)	Relative velocity in G-frame	ft/sec
VRELI(3)	Relative velocity in I-frame	ft/sec
VRMAG	Magnitude of relative velocity	ft/sec
WT	Vehicle weight	lb
WXH(3)	Angular momentum direction change	ft-lb
XCG,YCG,ZCG	Cg location in N-frame along x,y, and z-axes, respectively	ft

<u>Program Symbol</u>	<u>Variable Definition</u>	<u>Units</u>
<b>XDUM(27)</b>	Dummy common	Unitless
<b>XDDUM(27)</b>	Dummy common	Unitless
<b>XMRP, YMRP, ZMRP</b>	Moment reference point in N-frame along x, y, and z-axes, respectively	ft

## Appendix B

### REFERENCE FRAMES AND TRANSFORMATIONS

#### A. Reference Frames

All reference frames are right handed systems (Figs. B-1, B-2, and B-3).

1. I - Inertial Frame. The I-frame has its origin at the center of the earth with the  $X_I$  axis through the Greenwich meridian at time zero. The  $Z_I$  axis points through the North Pole and the  $Y_I$  axis completes the right handed system. It is in this frame the accelerations are integrated.

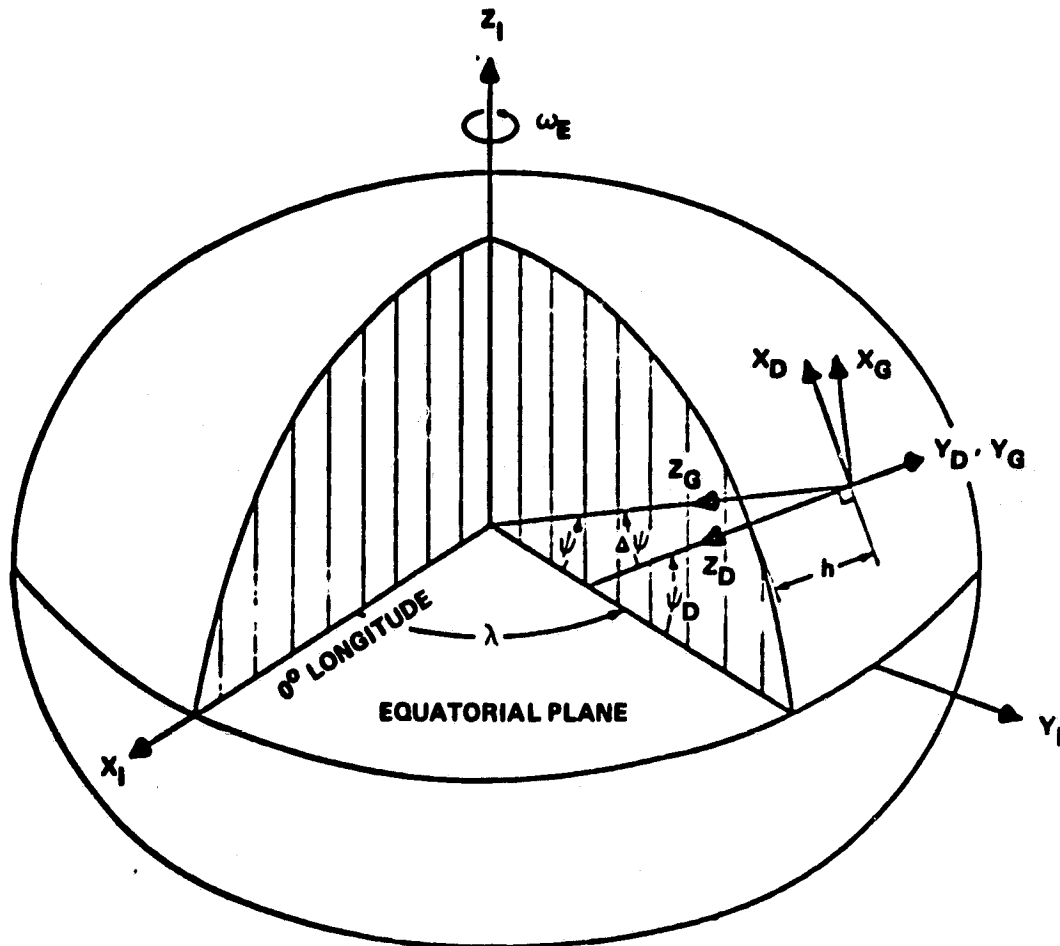
2. G - Geocentric Frame. The G-frame has its origin at the vehicle's center of mass. The  $X_G$  axis points north, the  $Y_G$  axis points east, and the  $Z_G$  axis is directed downward along the radius vector to the earth's center.

3. D - Geodetic Frame. The D-frame has its origin at the vehicle's center of mass (Fig. B-2). The  $X_D$  axis points north, the  $Y_D$  axis points east, and the  $Z_D$  axis is directed downward along the local geodetic.

4. R - Relative Velocity Frame. The R-frame has its origin at the vehicle's center of mass (Fig. B-2). The  $X_R$  axis is directed along the relative velocity vector. The  $Z_R$  axis is directed downward in a plane containing the velocity vector and the local geodetic. The  $Y_R$  axis completes the right handed system.

5. B - Body Frame. The body fixed B-frame has its origin at the vehicle's center of mass (Fig. B-3). The direction of the axes are chosen so as to be consistent with the definition of aerodynamic parameters. It is in this frame that the external forces and moments are computed.

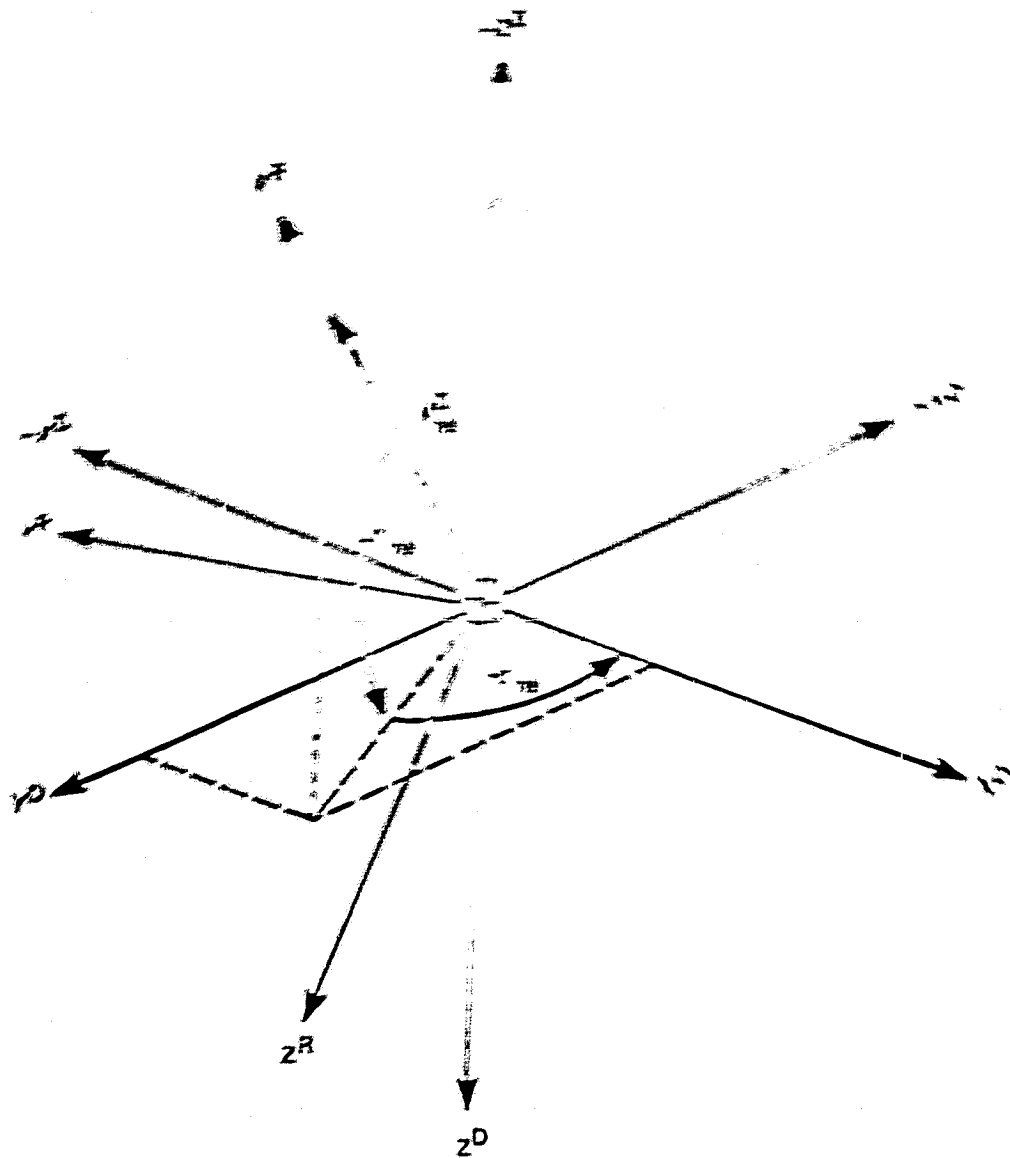
6. N - Input Data Reference Frame. This body fixed reference frame is parallel to the B-frame coordinate system with its origin chosen by the user. It is in this frame that the aerodynamic data and mass properties data are read into the program. Usually, it is convenient to choose the aerodynamic moment reference point as the origin of this frame.



$$A^{GI} = [-(90 + \psi)]_2 [\lambda]_3$$

$$A^{DI} = [-(90 + \psi_D)]_2 [\lambda]_3$$

Figure B-1. Inertial (I), geocentric (G) and geodetic (D) reference frames.

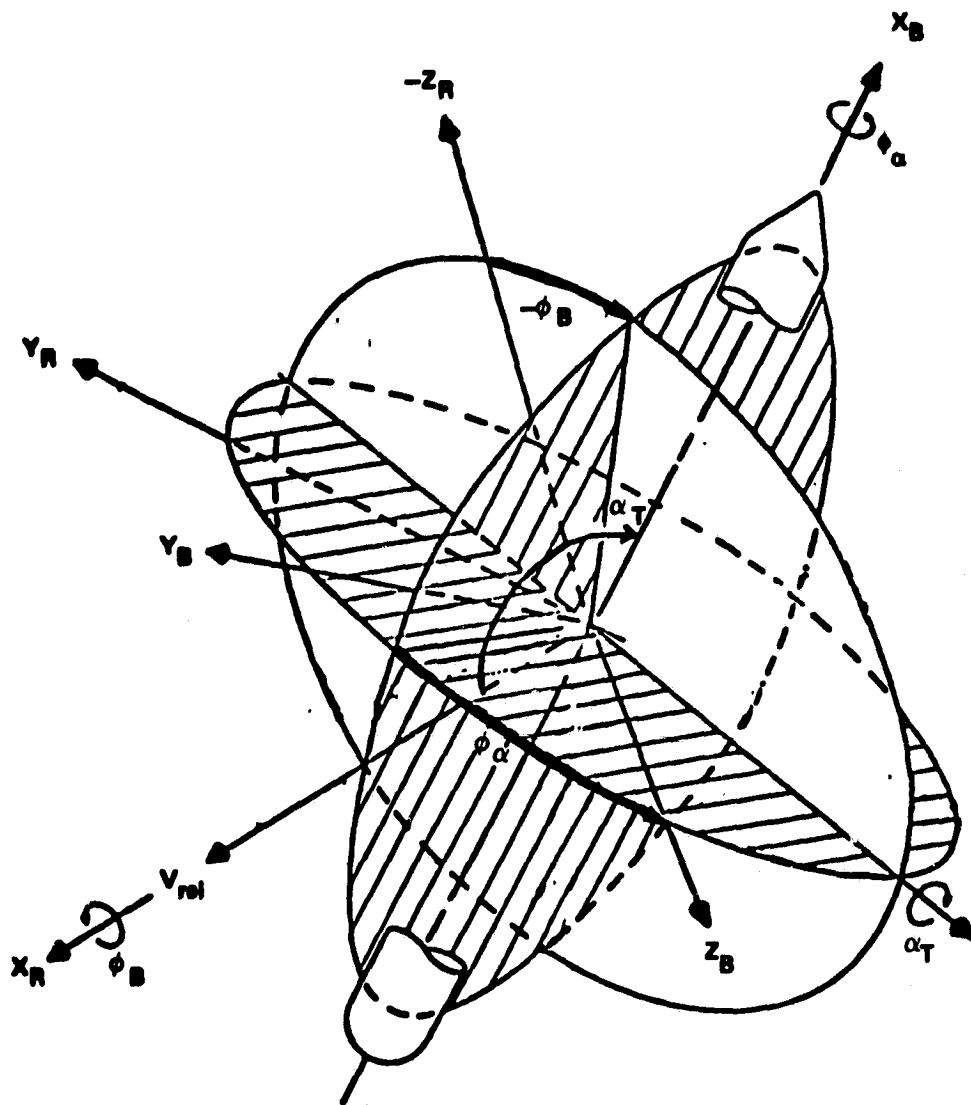


$$A^{RD} = [\delta_R]_2 \quad [\sigma_R]_3$$

Figure B-2. Geodetic (D) and relative velocity (R) reference frames.

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$$A^{BR} = [\varphi_\alpha]_1 [\alpha_T]_2 [\varphi_B]_1$$

Figure B-3. Relative velocity (R) and Body (B) reference frames.

## B. Transformations

The transformation matrix  $A^{ML}$  transforms vectors from the L-frame to the M-frame. The matrices are formed by successive rotations through the indicated Euler angles. The rotation  $[\theta]_i$  is used to indicate the direction cosine matrix for a positive rotation about the  $i^{\text{th}}$  axis through the angle  $\theta$ . The sequence of rotations is read from right to left. Since all transformations shown are orthogonal, the inverse transformation matrices are merely the transpose of those given.

1. Transformation from I to G-frame  $A^{GI}$

$$A^{GI} = [-(90 + \psi)]_2 [\lambda]_3$$

where  $\lambda$  = inertial longitude

$\psi$  = geocentric latitude

2. Transformation from I to D-frame  $A^{DI}$

$$A^{DI} = [-(90 + \psi_D)]_2 [\lambda]_3$$

where  $\lambda$  = inertial longitude

$\psi_D$  = geodetic latitude

3. Transformation from D to R-frame  $A^{RD}$

$$A^{RD} = [\gamma_R]_2 [\sigma_R]_3$$

where  $\sigma_R$  = relative heading

$\gamma_R$  = relative flight path angle

4. Transformation from R to B-frame

$$A^{BR} = [\phi_\alpha]_1 [\alpha_T]_2 [\phi_\beta]_1$$

where  $\phi_\beta$  = bank angle

$\alpha_T$  = total angle-of-attack

$\phi_\alpha$  = aerodynamic roll angle

### 5. Transformation from I to B-frame

Initially, the transformation from the I to B-frame is computed by  $A^{BI} = A^{BR} A^{RD} A^{DI}$

From the inverse of this transformation, the initial quaternion parameters are computed. The four quaternion parameters are defined as follows:

$$Q_1 = \alpha \sin (\phi / 2)$$

$$Q_2 = \beta \sin (\phi / 2)$$

$$Q_3 = \gamma \sin (\phi / 2)$$

$$Q_4 = \cos (\phi / 2)$$

where  $\alpha$ ,  $\beta$ , and  $\gamma$  are eigenaxis direction cosines, and  $\phi$  is the eigenaxis rotation angle. The quaternions are initialized as follows:

$$A^{IB} = \begin{bmatrix} a_{11} & a_{12} & a_{13} \\ a_{21} & a_{22} & a_{23} \\ a_{31} & a_{32} & a_{33} \end{bmatrix}$$

$$Q_4 = \frac{1}{2} \sqrt{1 + a_{11} + a_{22} + a_{33}}$$

If  $Q_4 \neq 0$ ,

$$Q_1 = \frac{1}{4 Q_4} (a_{32} - a_{23})$$

$$Q_2 = \frac{1}{4 Q_4} (a_{13} - a_{31})$$

$$Q_3 = \frac{1}{4 Q_4} (a_{21} - a_{12})$$

If  $Q_4 = 0$ ,

$$Q_1 = \sqrt{-\frac{1}{2} (a_{22} + a_{33})}$$

If  $Q_1 \neq 0$ ,

$$Q_2 = \frac{1}{4 Q_1} (a_{12} + a_{21})$$

$$Q_3 = \frac{1}{4 Q_1} (a_{13} + a_{31})$$

If  $Q_1 = 0$ ,

$$Q_2 = \sqrt{\frac{1}{2} (a_{22} + 1)}$$

If  $Q_2 \neq 0$ ,

$$Q_3 = \frac{1}{4 Q_2} (a_{23} + a_{32})$$

If  $Q_2 = 0$ ,

$$Q_3 = 1$$

From the integrated values of the quaternion parameter time derivatives, the  $A^{IB}$  transformation matrix is updated as shown in Appendix C.

## Appendix C

### EQUATIONS OF MOTION

This appendix presents briefly the equations of motion used to describe the dynamics of a vehicle in 6-degrees-of-freedom. The equations were derived for a vehicle of constant mass distribution and the external forces and torques considered were those resulting only from gravity and aerodynamics. The mathematical models for the Earth and gravity can be found in Reference 1. The atmospheric density is an input to the program as a function of position in orbit.

The aerodynamic force and moment coefficients and the atmospheric density are determined by table lookup at each integration step. The aerodynamic coefficients ( $C_A$ ,  $C_Y$ ,  $C_N$ ,  $C_\ell$ ,  $C_m$ ,  $C_n$ ) are a function of total angle-of-attack,  $\alpha_T$ , and aerodynamic roll angle,  $\phi_\alpha$ . The density ( $\rho$ ) is a function of geocentric latitude,  $\psi$ , and inertial longitude,  $\lambda$ . These angles are defined as

$$\alpha_T = \tan^{-1} \frac{\sqrt{V_{\text{RELB}}(2)^2 + V_{\text{RELB}}(3)^2}}{V_{\text{RELB}}(1)} \quad 0 \leq \alpha_T \leq 180^\circ$$

$$\phi_\alpha = \tan^{-1} \frac{V_{\text{RELB}}(2)}{V_{\text{RELB}}(3)} \quad 0 \leq \phi_\alpha \leq 360^\circ$$

$$\psi = \tan^{-1} \frac{R(3)}{\sqrt{R(1)^2 + R(2)^2}} \quad -90^\circ \leq \psi \leq 90^\circ$$

$$\lambda = \tan^{-1} \frac{R(2)}{R(1)} \quad 0 \leq \lambda \leq 360^\circ$$

where

$\bar{V}_{\text{RELB}}$  = relative velocity vector in B-frame

$\bar{R}$  = inertial I-frame position vector.

### A. Translational Motion

The translational equation of motion for a body in the inertial I-frame is

$$\ddot{\bar{R}} = \bar{g} + \frac{1}{m} \bar{F}_{AI}$$

where

$$\ddot{\bar{R}} = \dot{\bar{V}} = \text{inertial acceleration vector}$$

$$\bar{g} = \text{gravitational acceleration vector}$$

$$m = \text{mass of the body}$$

$$\bar{F}_{AI} = \text{I-frame aerodynamic forces}$$

The I-frame velocity equation is

$$\dot{\bar{R}} = \bar{V} = \dot{\bar{R}}_0 + \int \bar{R} dt$$

where

$$\dot{\bar{R}}_0 = \bar{V}_0 = \text{initial I-frame velocity vector.}$$

Integrating the velocity vector and adding the initial position, the I-frame position vector is

$$\bar{R} = \bar{R}_0 + \int \dot{\bar{R}} dt$$

where

$$\bar{R}_0 = \text{initial I-frame position vector.}$$

The aerodynamic forces are computed in the body B-frame and transformed into the I-frame for the translational acceleration computation. The B-frame aerodynamic forces are

$$\bar{F}_{AB} = q_{BAR} S_{Ref} \bar{C}_{XYZ}$$

where

$$\bar{C}_{XYZ} = \begin{bmatrix} -C_A \\ C_Y \\ -C_N \end{bmatrix} = \text{B-frame aerodynamic force coefficient vector}$$

$$q_{BAR} = \frac{1}{2} \rho |V_{RELB}|^2 = \text{dynamic pressure}$$

$$S_{Ref} = \text{aerodynamic reference area.}$$

Then the I-frame aerodynamic forces are

$$F_{AI} = A^{IB} \bar{F}_{AB} .$$

### B. Rotational Motion

The equation describing the rotational motion about the center of mass of a rigid body in the rotating B-frame is given by

$$[I] \dot{\bar{\omega}} = \bar{T}_{AB} - \bar{\omega} \times ([I] \cdot \bar{\omega})$$

where

$$[I] = \begin{bmatrix} I_{XX} & -I_{XY} & -I_{XZ} \\ -I_{XY} & I_{YY} & -I_{YZ} \\ -I_{XZ} & -I_{YZ} & I_{ZZ} \end{bmatrix} = \text{inertia tensor}$$

$\dot{\bar{\omega}} = \overline{PQRD} = \text{B-frame angular acceleration vector}$

$\bar{\omega} = \overline{PQR} = \text{B-frame angular velocity vector}$

$\bar{T}_{AB} = \text{B-frame external torques.}$

Then

$$\bar{\omega} = \bar{\omega}_0 + \int [I]^{-1} [\bar{T}_{AB} - \bar{\omega} \times ([I] \cdot \bar{\omega})] dt$$

where

$\bar{\omega}_0 = \text{initial B-frame angular velocity vector.}$

The aerodynamic torques about the vehicles center of mass are

$$\bar{T}_{OA} = q_{BAR} S_{Ref} D_{Ref} \left[ \bar{C}_{PLMN} + \frac{(\bar{X}_{MRP} - \bar{X}_{CG})}{D_{Ref}} \times \bar{C}_{XYZ} \right]$$

where

$D_{Ref} = \text{aerodynamic reference diameter}$

$$\bar{C}_{PLMN} = \begin{bmatrix} C_l \\ C_m \\ C_n \end{bmatrix} = \text{moment coefficients about the moment reference point}$$

$\bar{X}_{MRP} = \text{aerodynamic moment reference point}$

$\bar{X}_{CG} = \text{center of mass location.}$



The gravitational torques are given by

$$\overline{GGB} = \frac{3 GM}{|R|^3} [\overline{RB1} \times [I] \overline{RB1}]$$

where

GM = product of universal gravitational constant and the mass of the earth

$\overline{RB1}$  = unit vector along body B-frame position.

The B-frame external torques are

$$\overline{T}_{AB} = \overline{T}_{OA} + \overline{GGB} \quad ,$$

The quaternion parameters are updated in a similar manner:

$$\overline{Q} = \overline{Q}_0 + \int \dot{\overline{Q}} dt$$

where

$\overline{Q}_0$  = initial quaternion parameters defined in Appendix B.

The time derivivity  $\dot{\overline{Q}}$  is defined as

$$\dot{\overline{Q}} = \begin{bmatrix} \dot{Q}_1 \\ \dot{Q}_2 \\ \dot{Q}_3 \\ \dot{Q}_4 \end{bmatrix} = \begin{bmatrix} Q_4 & -Q_3 & Q_2 \\ Q_3 & Q_4 & -Q_1 \\ -Q_2 & Q_1 & -Q_4 \\ -Q_1 & -Q_2 & -Q_3 \end{bmatrix} \overline{\omega} \quad .$$

From these integrated values of  $\bar{Q}$ , the  $A^{IB}$  transformation matrix is calculated as follows:

$$A^{IB} = \begin{bmatrix} (2 Q_1^2 + 2 Q_4^2 - 1) & 2(Q_1 Q_2 - Q_3 Q_4) & 2(Q_1 Q_3 + Q_2 Q_4) \\ 2(Q_1 Q_2 + Q_3 Q_4) & (2 Q_2^2 + 2 Q_4^2 - 1) & 2(Q_2 Q_3 - Q_1 Q_4) \\ 2(Q_1 Q_3 - Q_2 Q_4) & 2(Q_2 Q_3 + Q_1 Q_4) & (2 Q_3^2 + 2 Q_4^2 - 1) \end{bmatrix}$$

Appendix D

PROGRAM LISTING

```

1. C.....
2. C SKYLAB DYNAMICS PROGRAM(SKVDYN)
3. C
4. C
5. C
6. C.....
7. C THIS PROGRAM IS AN ALTERED VERSION OF HORTROP SERVICES PROGRAM
8. C REENTR - SPACE SHUTTLE EXTERNAL TANK REENTRY SIMULATION. THE
9. C THEORY USED IN THIS PROGRAM IS DOCUMENTED IN -
10. C M-250-1303
11. C MANY OF THE OPTIONS IN PROGRAM REENTR ARE DELETED IN
12. C -- ORDER TO GIVE MAXIMUM SPEED TO THIS VERSION.
13. C
14. C ASSUMPTIONS
15. C
16. C 1. FISCHER ELLIPSOID EARTH MODEL
17. C 2. DENSITY INPUT AS FUNCTION OF ORBITAL POSITION ONLY
18. C 3. AERO COEFFICIENTS DEPENDENT ONLY OF ATTITUDE
19. C 4. CONSTANT MASS DISTRIBUTION
20. C 5. ASRU AND GRAVITY TOLERANCE
21. C
22. C
23. C
24. C.....
25. C REAL IXYZ(3,3),IXYZI(3,3),LMRP(3),LANDA,LAMDE
26. C REAL IXYZX(3,3),LMRPX(3),LKC(3)
27. C DIMENSION IVAR(90),SCALE(90),PVALU(90),PNAME(90),CASE(18),
28. C $AI(3,3),A,(3,3),A(3),AS(3,3),IPH(90),PLT(90)
29. C DIMENSION ATNH(13),LI(3),ME(3),ADP(3,3)
30. C
31. C..... C O M M O N B L O C K.....
32. C PROGRAM CONTROL AND INTEGRATION (100)
33. C
34. C
35. C COMMON TIME,DT,DTP,DTSAM,TRUM,TEND,THOR,QSCR,PCDUM(12)
36. C COMMON PQR(3),QD(4),VDDI(3),ADDI(3),XDDUR(27)
37. C COMMON PQR(3),G(4),V(3),R(3),XDDUR(27)
38. C
39. C VEHICLE CHARACTERISTICS COMMON (50)
40. C
41. C COMMON WT,XCG,YCG,ZCG,IXYZ,IXYZI,DREF,SREF,LMRP,CMASS,CMASI,
42. C $ XMRP,YMRP,ZMRP,VCCOM(18)
43. C
44. C VEHICLE POSITION COMMON (150)
45. C
46. C COMMON PHIBK,ALPHI,PHI,ARB(3,3),AIB(3,3),ARP(3,3),ABI(3,3),
47. C $ AID(3,3),AIG(3,3),AGR(3,3),ADR(3,3),ADI(3,3),ADE(3,3),
48. C $ AAD(3,3),ARI(3,3),VPCOM(39)
49. C
50. C EARTH POSITION COMMON (100)
51. C
52. C COMMON RMAG,RPST,RI(3),C(3),CR,CV,CMAG,RR,RR2,SPSI,SPSIZ,SJ,

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53. $ SD,SH,SMH,SWD,GCR,H,PSI,DPSI,PSID,LANDA,LANDE,SIGR,CAMR,
54. $ SIGI,CAMI,RBL(3),EPCOM(66)
55. C
56. C VEHICLE AERODYNAMICS COMMON (100)
57. C
58. COMMON CA,CH,CL,CM,CT,CEM,FAR(3),FARC(3),CPLMH(3),CRYZ(3),
59. $ CLMNT(3),FAR(3),FAI(3),FOMI(3),TOA(3),VACOM(67)
60. C
61. C VEHICLE DYNAMICS COMMON (150)
62. C
63. C
64. COMMON RHO,QBAR,VRMAG,VRELD(3),VINAG,VID(3),VRELC(3),
65. $ VRELI(3),VRELB(3),VATH(3),DIM(3),GEB(3),VIG(3),TAB(3),
66. $ HB(3),WXH(3),TSUM(3),VDCOM(107)
67. C
68. C THE FOLLOWING VARIABLES ARE NOT CHANGED FROM CASE TO CASE AND
69. C ARE CONSIDERED AS CONSTANTS
70. C
71. C ATMOSPHERE TABLES COMMON (500)
72. C
73. C
74. COMMON JLAT(11),JLNG(37),ERR0(11,37),ATCOM(45)
75. C
76. C TABLES OF AERODYNAMIC COEFFICIENTS COMMON (2000)
77. C
78. COMMON TALP(11),TPHIA(21),FCM(21,11),FCA(21,11),
79. $ FCY(21,11),FCL(21,11),FCM(21,11),FCEN(21,11),ACCOM(582)
80. C
81. C
82. C CHANGELESS CONSTANTS COMMON(20)
83. C
84. C
85. COMMON CH(3),TWOPI,OMGE,CNV,PI,CCCOM(13)
86. C
87. C
88. C TOTAL POINTS IN COMMON BLOCK = 3170
89. C TOTAL POINTS IN VARYING COMMON = 650
90. C
91. C DATA BLANK/4H /
92. C
93. C
94. C NCASE = NO. OF CASES TO BE RUN PER CASE DECK
95. C
96. C NX = NO. OF INTEGRATION VARIABLES
97. C
98. C
99. C CALL EBOMB(94S)
100. READ(5,1)NCASE,NX
101. 1 FORMAT(3I5)
102. NR = 5
103. NW = 6
104. NP = 12

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105. NCOM = 656  
106. NCOM1 = 3170  
107. C\*\*\*\*\*ZERO COMPLETE COMMON BLOCK  
108. CALL ZCOM(NCOM1)  
109. C\*\*\*\*\*READ MAIN PRINT SPECIFICATIONS  
110. CALL PSPEC(5,6,12,NPV,IVAR,PHANG,SCALE,IPM)  
111. C\*\*\*\*\*READ IN ATMOSPHERIC DATA  
112. A FORMAT(2F10.5,15)  
113. READ(5,5)(ATNM(I),I=1,18)  
114. 5 FORMAT(18A4)  
115. READ(5,300)(TLAT(I),I=1,11)  
116. READ(5,300)(TLNG(I),I=1,37)  
117. DO 337 J=1,37  
118. 337 READ(5,6)(FRHO(I,J),I=1,11)  
119. 6 FORMAT(6E9.3)  
120. CNV = 57.29577951  
121. C\*\*\*\*\*READ IN VEHICLE AERODYNAMIC DATA  
122. READ(NR,301)NALP,NPHIA  
123. 301 FORMAT(5I5)  
124. C  
125. C\*\*\*READ IN ALPHAT AND PHIA INDEPENDENT VARIABLE TABLES  
126. C  
127. 302 FORMAT(9F8.3)  
128. READ(NR,300)(TALP(I),I=1,NALP)  
129. READ(NR,300)(TPHIA(I),I=1,NPHIA)  
130. 303 FORMAT(6E12.1)  
131. C  
132. C\*\*\*AXIAL FORCE COEFFICIENT TABLE  
133. C  
134. 300 FORMAT(2E8.3)  
135. READ(NR,300)((FCA(I,J),I=1,NPHIA),J=1,NALP)  
136. C  
137. C\*\*\*NORMAL FORCE COEFFICIENT TABLE  
138. C  
139. READ(NR,300)((FCN(I,J),I=1,NPHIA),J=1,NALP)  
140. C  
141. C\*\*\*SIDE FORCE COEFFICIENT TABLE  
142. C  
143. READ(NR,300)((FCY(I,J),I=1,NPHIA),J=1,NALP)  
144. C  
145. C\*\*\*PITCHING MOMENT COEFFICIENT TABLE  
146. C  
147. READ(NR,300)((FCM(I,J),I=1,NPHIA),J=1,NALP)  
148. C  
149. C\*\*\*YAWING MOMENT COEFFICIENT TABLE  
150. C  
151. READ(NR,300)((FCEN(I,J),I=1,NPHIA),J=1,NALP)  
152. C  
153. C\*\*\*ROLLING MOMENT COEFFICIENT TABLE  
154. C  
155. READ(NR,300)((FCL(I,J),I=1,NPHIA),J=1,NALP)  
156. C

```

157. C
158. 00 334-I=1,NALP
159. 334 TALP(I)=TALP(I)/CNV
160. 00 335-I=1,NPHIA
161. 335 TPHA(I)=TPHIA(I)/CNV
162. 00 338-I=1,I1
163. 338 TLAT(I)=TLAT(I)/CNV
164. 00 339-I=1,I37
165. 339 TLNG(I)=TLNG(I)/CNV
166. PI=180-7CNV
167. TWOPI=2.*PI
168. CM=1.40765391616
169. RE=20925721.785
170. RS=20909734.843
171. GF=0.6738525415E-02
172. GJ=-.162405E-02
173. GH=-.640E-05
174. GD=-.69125E-05
175. OMGE=7.29221158E-05
176. CHO=3.3718120539E-03
177. CH(1)=-1.57258544E-10
178. CH(2)=5.907450825E-18
179. CH(3)=-1.08416187E-25
180. 7 FORMAT(BE10.1)
181. ICASE=0
182. C****BEGIN CASE LOOP
183. 8 CALL ZCOM(NCOM)
184. ICASE=ICASE+1
185. IF(ICASE.GT.1)GO TO 11
186. C
187. C****READ CASE DEFINITION DATA
188. C
189. C
190. C
191. READ(5,5)(CASE(I),I=1,18)
192. IF(CASE(1).EQ.BLANK)GO TO 94
193. READ(5,2)PROPT
194. READ(5, 2)DT,DTP,DTSAM,TRUN,TIME,IOP1
195. 2 FORMAT(5F10.4,I5)
196. DTX=DT
197. DTPX=DTP
198. DTSX=DTSAM
199. TRUNX=TRUN
200. TIMEX=TIME
201. GO TO 12
202. 11 IF(ICASE.GT.NCASE)GO TO 90
203. DT=DTX
204. DTP=DTPX
205. DTSAM=DTSX
206. TRUN=TRUNX
207. TIME=TIMEX
208. C

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209. C****INITIALIZE VARIABLES
210. C
211. C      12 TEND=TRUM+TIME
212. TP=TIME
213. TPD=TIME
214. IF (LCASE.CT.1) GO TO 17
215. C****READ VEHICLE DATA
216. READ(5,13)WT,XCG,YCG,ZCG,XMRP,YMRP,ZMRP
217. 13 FORMAT(8F10.4)
218. READ(5,13)DREF,SREF
219. READ(5,7)IXYZ(1,1),IXYZ(2,2),IXYZ(3,3),IXYZ(1,2),IXYZ(1,3),
220. $IXYZ(2,3)
221. IXYZ(1,2)=-IXYZ(1,2)
222. IXYZ(1,3)=-IXYZ(1,3)
223. IXYZ(2,3)=-IXYZ(2,3)
224. IXYZ(2,1)=IXYZ(1,2)
225. IXYZ(3,1)=IXYZ(1,3)
226. IXYZ(3,2)=IXYZ(2,3)
227. LMRP(1)=(XMRP-XCG)/DREF
228. LMRP(2)=(YMRP-YCG)/DREF
229. LMRP(3)=(ZMRP-ZCG)/DREF
230. WTX=WT
231. DREFX=DREF
232. SREFX=SREF
233. DO 14 I=1,3
234. DO 14 J=1,3
235. IXYZX(I,J)=IXYZ(I,J)
236. LMRPX(I)=LMRP(I)
237. 14 CONTINUE
238. C
239. C****POSITION INITIALIZATION
240. C
241. READ(5,15)PSI,LANDE,RMAG,VIMAG,SIGI,GAMI
242. LANDA=LANDE*OMGE*TIME*CNV
243. 15 FORMAT(F10.6,F10.5,F10.2,F10.3,F10.6,F10.8)
244. READ(5,16)PHIB1,ALPHA1,PHIA1,(PQR(I),I=1,3)
245. READ(5,210)((ABP(I,J),J=1,3),I=1,3)
246. 16 FORMAT(6E10.5)
247. PSIX=PSI
248. XLAND=LANDE
249. RMAGX=RMAG
250. VRELX=VIMAG
251. SIGIX=SIGI
252. GAMIX=GAMI
253. PHIAIX=PHIA1
254. ALPHAIX=ALPHA1
255. PHIBIX=PHIB1
256. PP=PQR(1)
257. PQ=PQR(2)
258. PR=PQR(3)
259. GO TO 19
260. 17 CONTINUE

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261. WT=WTX
262. DREF=DREFX
263. SREF=SREFX
264. DO 18 I=1,3
265. DO 18 J=1,3
266. IXYZ(I,J)=IXYZ(I,J)
267. LMRP(I)=LMRPX(I)
268. 18 CONTINUE
269. PSI=PSIX
270. LAMDA=XLAMDA+ONCE*TIME*CNV
271. RMAG=RMAGX
272. VMAG=VR6LX
273. SIGI=SIGIX
274. GAMI=GAMIX
275. PHIAI=PHIAX
276. ALPHAI=ALPAIX
277. PHIBI=PHIBIX
278. PQR(1)=PP
279. PQR(2)=PQ
280. PQR(3)=PR
281. 19 CONTINUE
282. LAMDA=LAMDA/CNV
283. LAMDE=LAMDE/CNV
284. PSI=PSI/CNV
285. SIGI=SIGI/CNV
286. GAMI=GAMI/CNV
287. PHIAI=PHIAI/CNV
288. ALPHAI=ALPHAI/CNV
289. PHIBI=PHIBI/CNV
290. DO 20 I=1,3
291. PQR(I)=PQR(I)/CNV
292. GHASS=WT*RS*RS/GH
293. GHASS=1./GHASS
294. DO 21 I=1,3
295. DO 21 J=1,3
296. 21 IXYZ(I,J)=IXYZ(I,J)
297. CALL MINV(IXYZI,3,DI,LI,MI)
298. C
299. C
300. C
301. INERTIAL POSITION VECTOR COMPUTATION
302. RPSI=RE/SQRT(1.+GF*(SIN(PSI)**2))
303. H=RMAG-RPSI
304. R(1)=RMAG*COS(PSI)*COS(LAMDA)
305. R(2)=RMAG*COS(PSI)*SIN(LAMDA)
306. R(3)=RMAG*SIN(PSI)
307. DPSI=CHO
308. HW=1.
309. DO 22 I=1,3
310. HW=HW*H
311. DPSI=DPSI+CH(I)*HW
312. PSID=DPSI+DPSI

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313. C *****GEOCENTRIC COMPUTATIONS
314. C
315. C
316. CALL TWIST(LANDA,A1,3)
317. PS190=PSID+90./CNV
318. CALL TWIST(-PS190,A2,2)
319. DO 23 I=1,3
320. DO 23 J=1,3
321. 23 AID(I,J)=A1(I,1)*A2(I,J)+A1(I,2)*A2(2,J)+A1(I,3)*A2(3,J)
322. C *****GEOCENTRIC COMPUTATIONS
323. C
324. C
325. PS90=PSI+90./CNV
326. CALL TWIST(-PS90,A2,2)
327. DO 24 I=1,3
328. DO 24 J=1,3
329. 24 AIG(I,J)=A1(I,1)*A2(I,J)+A1(I,2)*A2(2,J)+A1(I,3)*A2(3,J)
330. DO 350 I=1,3
331. DO 350 J=1,3
332. 350 ADI(I,J)=AID(J,I)
333. C
334. C D-FRAME INERTIAL VELOCITY COMPONENTS
335. C
336. VIG(1)=VINAG* $\cos(GAMI)$ * $\cos(SIGI)$ 
337. VIG(2)=VINAG* $\cos(GAMI)$ * $\sin(SIGI)$ 
338. VIG(3)=-VINAG* $\sin(GAMI)$ 
339. CALL TWIST(DPSI,ADG,2)
340. DO 25 I=1,3
341. 25 VID(I)=ADG(I,1)*VIG(1)+ADG(I,2)*VIG(2)+ADG(I,3)*VIG(3)
342. C
343. C COMPUTE INITIAL ATMOSPHERIC VELOCITY COMPONENTS(INERTIAL FRAME)
344. C
345. VATM(1)=-OMGE*R(2)
346. VATM(2)=-OMGE*R(1)
347. VATM(3)=0.0
349. C
350. C RESOLVE VECTORS INTO I-FRAME
351. C
352. DO 29 I=1,3
353. 29 A(I)=V(I)-VATM(I)
354. C D-FRAME RELATIVE VELOCITY COMPONENTS
355. C
356. DO 351 I=1,3
357. 351 VRELD(I)=ADI(I,1)*A(I,1)+ADI(I,2)*A(I,2)+ADI(I,3)*A(I,3)
359. C
360. C DETERMINE EULER MATRIX FROM RELATIVE VELOCITY FRAM TO BODY FRAME
361. C
362. CALL TWIST(-ALPHA,A1,2)
363. DO 30 I=1,3
364. DO 30 J=1,3
365. 30 A3(I,J)=A1(I,1)*A2(I,J)+A1(I,2)*A2(2,J)+A1(I,3)*A2(3,J)

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417. $,11HLONGITUDE =,F10.5/1X,19INERTIAL VELOCITY =,F10.3/1X,10MINERTI
418. $AL HEADING =,F10.5/1X,28INERTIAL FLIGHT PATH ANGLE =,F10.6/1X,23
419. $HVEHICLE ATTITUDE DATA =,1X,11PHPHDI +1 =,F10.5/
420. $ 25X,11H LPHAI +2 =,F10.5/25X,11PHPHAI +1 =,F10.5/1X,
421. $18INITIAL BODY RATES,
422. $6X,11ROLL-RATE =,F10.5/25X,12PITCH-RATE =,F10.5/25X,10RYAW-RATE
423. $ =,F10.5/7/
424. WRITE(6,41)
425. WRITE(6,46)
426. --- 46 FORMAT(1X,32H*****OTHER INFORMATION*****/)
427. WRITE(6,47)(ATNM(I),I=1,18)
428. --- 47 FORMAT(1X,20HTHIS PROGRAM USES ---,10A4/)
429. WRITE(6,98)DT,DTP,DTSAM,TRUN,TIME,IOPT1
430. --- 98 FORMAT(1X,4HDELTA,F10.6,5X,4HDTPR,F10.5,5X,4HDTSM,F10.2,5X,
431. 14HTRUN,F10.2,5X,4HTIME,F10.2,4X,5HIOPT1,13)
432. --- 210 FORMAT(6E12.6/3E12.6)
433. --- 211 FORMAT(1X,4HARP ,5X,3E18.7/10X,3E18.7/10X,3E18.7/)
434. C
435. IF(IOPT1.EQ.0) GO TO 600
436. READ(14)(TIME,DT,(PORD(I),PDR(I)),VDOT(I),V(I),
437. SROD(I),R(I),I=1,3),SQD(J),Q(J),J=1,4)
438. --- 600 CONTINUE
439. C*****BEGIN INTEGRATION LOOP
440. --- 51 CONTINUE
441. DO 86 KUTTA=1,5
442. C
443. C*****EVALUATE DERIVATIVES
444. C
445. RMAG=SQRT(R(1)*R(1)+R(2)*R(2)+R(3)*R(3))
446. RI(1)=R(1)/RMAG
447. RI(2)=R(2)/RMAG
448. RI(3)=R(3)/RMAG
449. GMAG=GM/(RMAG*RMAG)
450. RR=RE/RMAG
451. RR2=RR*RR
452. SPSI=RI(3)
453. SPSI2=SPSI*SPSI
454. RPSI=RE/SQRT(1.+GF*SPSI2)
455. SJ=1.-5.*SPSI2
456. SD=1./7.-2.*SPSI2+3.*SPSI2*SPSI2
457. SH=3.-7.*SPSI2
458. SMH=SJ/5
459. SMD=SH/7.
460. CR=RR2*(GH*RR*SPSI*SH+3.*GD*RR2*SD+GJ*SJ)+1.
461. CW=RR2*(3.*GH*RR*SMH+4.*GD*RR2*SPSI*SMD+2.*GJ*SPSI)
462. GCR=-GMAG*CR
463. G(1)=GCR*RI(1)
464. G(2)=GCR*RI(2)
465. G(3)=-GMAG*CW+GCR*RI(3)
466. H=RMAG-RPSI
467. PSI=ATN2(R(3),SQRT(R(1)*R(1)+R(2)*R(2)))
468. N=3

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469.      DPSI=CHQ
470.      HW=1.
471.      DO 53 I=1,N
472.      HW=HW*H
473.      53  DPSI=DPSI+CH(I)*HW
474.      DPSI=DPSI*SIN(2.0*PSI)
475.      PSIO=PSI+DPSI
476.      PSI90=PSIO+90./CNV
477.      LAMDA=ATN2(R(2),R(1))
478.      CALL TWIST(LAMDA,A3,3)
479.      CALL TWIST(-PSI90,A2,2)
480.      DO 54 J=1,3
481.      DO 54 J=1,3
482.      54  AID(I,J)=A3(I,1)*A2(I,1)*A3(I,2)*A2(2,J)+A3(I,3)*A2(3,J)
483.      PSC90=PSI+90./CNV
484.      CALL TWIST(-PSC90,A2,2)
485.      DO 58 I=1,3
486.      DO 58 J=1,3
487.      58  AIG(I,J)=A3(I,1)*A2(I,1)*A3(I,2)*A2(2,J)+A3(I,3)*A2(3,J)
488.      VATM(1)=-OMGE*R(2)
489.      VATM(2)=OMGE*R(1)
490.      VATM(3)=0.0
491.      DO 55 I=1,3
492.      55  VRELI(I)=W(I)-VATM(I)
493.      VRMAG=SQRT(VRELI(1)*VRELI(1)+VRELI(2)*VRELI(2)+VRELI(3)*VRELI(3))
494.      CALL SULR5(Q,AIB)
495.      DO 56 I=1,3
496.      DO 56 J=1,3
497.      56  ABI(I,J)=AIB(J,I)
498.      DO 57 I=1,3
499.      57  RBI(I)=-ABI(I,1)*RI(1)-ABI(I,2)*RI(2)-ABI(I,3)*RI(3)
500.      VRELB(I)=ABI(I,1)*VRELI(1)+ABI(I,2)*VRELI(2)+ABI(I,3)*VRELI(3)
501.      C*****
502.      C
503.      C  AERODYNAMIC FORCES AND MOMENTS
504.      C
505.      C*****
506.      C
507.      IF(LAMDA.LT.0.) LAMDA=LAMDA+TWOP
508.      CALL LOOK2(RHO,FRHD,11,PSI,TLAT,11,LAMDA,TLNG,37,IPSI,ILNG,
509.      $ I)
510.      RHO=RHO*1.9349971E-03
511.      QBAR=0.5*RHO*VRMAG*VRMAG
512.      ALPHT=ATN2(SQRT(VRELB(2)*VRELB(2)+VRELB(3)*VRELB(3)),VRELB(1))
513.      PHIA=ATN2(VRELB(2),VRELB(3))
514.      IF(PHIA.LT.0.6)PHIA=PHIA+TWOP
515.      501 CONTINUE
516.      C
517.      C*****MAIN BODY COEFFICIENTS
518.      C
519.      C
520.      CALL LOOK2(CN,FCN,21,PHIA,TPHIA,NPHIA,ALPHT,TALP,NALP,IPHIA,IALP,

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521. S 1)
522. CALL LOOK2 CA,FCA,21,PHIA,TPHIA,NPHIA,ALPHA,TALP,WALP,IPHIA,IALP,
523. S 0)
524. CALL LOOK2(CM,FCM,21,PHIA,TPHIA,NPHIA,ALPHA,TALP,WALP,IPHIA,IALP,
525. S 0)
526. CALL LOOK2(CY,FCY,21,PHIA,TPHIA,NPHIA,ALPHA,TALP,WALP,IPHIA,IALP,
527. S 0)
528. CALL LOOK2(CL,FCL,21,PHIA,TPHIA,NPHIA,ALPHA,TALP,WALP,IPHIA,IALP,
529. S 0)
530. CALL LOOK2(CEN,FCEN,21,PHIA,TPHIA,NPHIA,ALPHA,TALP,WALP,IPHIA,IALP,
531. S 0)
532. CPLMN(1)=CL
533. CPLMN(2)=CM
534. CPLMN(3)=CEN
535. XYZ(1)=-CA
536. XYZ(2)=CY
537. XYZ(3)=-CN
538. LXC(1)=LMRP(2)*XYZ(3)-LMRP(3)*XYZ(2)
539. LXC(2)=LMRP(3)*XYZ(1)-LMRP(1)*XYZ(3)
540. LXC(3)=LMRP(1)*XYZ(2)-LMRP(2)*XYZ(1)
541. DO 63 I=1,3
542. DIM(I)=XYZ(I,1)*RBI(1)+XYZ(I,2)*RBI(2)+XYZ(I,3)*RBI(3)
543. 63 CLMNT(1)=CPLMN(1)*LXC(I)
544. GGB(1)=RBI(2)*DIM(3)-RBI(3)*DIM(2)
545. GGB(2)=RBI(3)*DIM(1)-RBI(1)*DIM(3)
546. GGB(3)=RBI(1)*DIM(2)-RBI(2)*DIM(1)
547. GGB(1)=GGB(1)*(GM*3.0/RMAG**2)/RMAG
548. GGB(2)=GGB(2)*(GM*3.0/RMAG**2)/RMAG
549. GGB(3)=GGB(3)*(GM*3.0/RMAG**2)/RMAG
550. QS=QBAR*SREF
551. QSD=QS*DREF
552. DO 64 I=1,3
553. FAB(I)=XYZ(I)*QS
554. TOA(I)=CLMNT(I)*QSD
555. 64 TAB(I)=TOA(I)+GGB(I)
556. C*****
557. C
558. C RIGID-BODY DYNAMICS
559. C
560. C*****
561. DO 65 I=1,3
562. HB(I)=XYZ(I,1)*PQR(1)+XYZ(I,2)*PQR(2)+XYZ(I,3)*PQR(3)
563. WXH(1)=PQR(2)*HB(3)-PQR(3)*HB(2)
564. WXH(2)=PQR(3)*HB(1)-PQR(1)*HB(3)
565. WXH(3)=PQR(1)*HB(2)-PQR(2)*HB(1)
566. DO 66 I=1,3
567. 66 TSUM(I)=TAB(I)-WXH(I)
568. DO 67 I=1,3
569. 67 PQR(I)=XYZ(I,1)*TSUM(1)+XYZ(I,2)*TSUM(2)+XYZ(I,3)*TSUM(3)
570. QD(1)=-.5*(Q(4)*PQR(1)-Q(3)*PQR(2)+Q(2)*PQR(3))
571. QD(2)=-.5*(Q(3)*PQR(1)+Q(4)*PQR(2)-Q(1)*PQR(3))
572. QD(3)=-.5*(-Q(2)*PQR(1)+Q(1)*PQR(2)+Q(4)*PQR(3))

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573. QD(4)=-.5*(Q(1)*PQR(1)+Q(2)*PQR(2)+Q(3)*PQR(3))
574. QSQR=SQRT(Q(1)**2+Q(2)**2+Q(3)**2)
575. DO 68 I=1,3
576. FAI(I)=AIB(L,I,1)*FAB(1)+AIB(L,2)*FAB(2)+AIB(L,3)*FAB(3)
577. FOMI(I)=FAI(I)*GHASI
578. YDOT(I)=FOMI(I)+C(I)
579. 68 ROOT(I)=V(I)
580. IF(KUTTA-I) 86,69,86
581.
582. C*****PERFORM END-OF-DISTEP COMPUTATIONS
583. 69 CONTINUE
584.
585. LANGE=ATN2(R(2),R(1))-ONCE*TIME
586. 497 IF(LAMDE)498,499,499
587. 498 LANGE=LANGE+TWOPI
588. GO TO 497
589. 499 CONTINUE
590. DO 101 I=1,3
591. DO 101 J=1,3
592. 101 ADI(I,J)=AID(J,I)
593. DO 103 I=1,3
594. VIG(I)=AIG(L,I)*V(1)+AIG(L,2)*V(2)+AIG(L,3)*V(3)
595. VID(I)=ADI(L,1)*V(1)+ADI(L,2)*V(2)+ADI(L,3)*V(3)
596. VINAG=SQRT(V(1)*V(1)+V(2)*V(2)+V(3)*V(3))
597. DO 102 I=1,3
598. VRELD(I)=ADI(L,1)*VRELI(1)+ADI(L,2)*VRELI(2)+ADI(L,3)*VRELI(3)
599. GARR=ATN2(-VRELD(3),SQRT(VRELD(1)**2+VRELD(2)**2))
600. SIGR=ATN2(VRELD(2),VRELD(1))
601. GANI=ATN2(-VIG(3),SQRT(VIG(1)**2+VIG(2)**2))
602. SIGI=ATN2(VIG(2),VIG(1))
603. CALL TWIST(SIGR,AL,3)
604. CALL TWIST(SIGI,A2,2)
605. DO 104 I=1,3
606. DO 104 J=1,3
607. 104 ADR(I,J)=A1(I,1)*A2(1,J)+A1(I,2)*A2(2,J)+A1(I,3)*A2(3,J)
608. DO 105 I=1,3
609. DO 105 J=1,3
610. 105 ARD(I,J)=ADR(J,I)
611. DO 106 I=1,3
612. DO 106 J=1,3
613. 106 ARI(I,J)=ARD(1,1)*ARI(L,1)+ARD(1,2)*ARI(L,2)+ARD(1,3)*ARI(L,3)
614. DO 107 I=1,3
615. DO 107 J=1,3
616. 107 ARB(I,J)=ARI(L,1)*ARB(L,1)+ARI(L,2)*ARB(L,2)+ARI(L,3)*ARB(L,3)
617. DO 212 I=1,3
618. DO 212 J=1,3
619. 212 ARP(I,J)=ARB(L,1)*ARP(L,1)+ARB(L,2)*ARP(L,2)+ARB(L,3)*ARP(L,3)
620. PHIBK=ATN2(ARB(2,1),-ARB(3,1))
621. DO 110 I=1,3
622. FAR(I)=ARD(1,1)*FAB(1)+ARB(1,2)*FAB(2)+ARB(1,3)*FAB(3)
623. 110 FARC(I)=FAR(I)/45
624.

```

```

625. C*****PRINT IF APPROPRIATE
626. C
627. IF(TIME-TP)74,73,73
628. C
629. C
630. 73 CONTINUE
631. THOR=TIME/3600.0
632. NXPR=1
633. IF(TIME-TPR)120,121,121
634. 120 NXPR=-1
635. 121 CONTINUE
636. IF(TIME.LT.DTSAM) GO TO 601
637. WRITE(13)(TIME,DT,(PORD(I),PQR(I),VDDI(I),V(I),
638. $RDT(I),P(I),I=1,3),(QD(J),Q(J),J=1,4)
639. DTSAM=DTSAM+TEND
640. NXPR=1
641. 601 CONTINUE
642. IF(NXPR.GT.0)TPR=TIME+PROPT*DTP
643. IF(TIME.GE.TEND)NXPR=1
644. CALL BLOCK( 6,NP,CASE,MPV,IVAE,PHAME,PVALD,SCALE,IPU,NXPR)
645. TP=TIME+DTP
646. C
647. C*****CHECK WHETHER THIS CASE SHOULD BE TERMINATED
648. C
649. 74 CONTINUE
650. IF(TIME-TEND)86,87,87
651. C
652. C***** INTEGRATE DYNAMIC VARIABLES
653. C
654. 86 CALL RUNK2(KUTTA,MX)
655. GO TO 51
656. C
657. C*****TERMINATE THIS CASE
658. C
659. 87 CONTINUE
660. 90 IF(CASE-20)91,91,94
661. 91 ICASE=0
662. GO TO 8
663. 94 STOP
664. END

```





```

1. SUBROUTINE PCOM(NM,NCOM)
2. *****
3. C PCOM-PRINTS ALL LOCATIONS-IN THE COMMON-BLOCK PCO 002
4. C PCO 003
5. C PCO 004
6. C PCO 005
7. C PCO 006
8. C PCO 007
9. C PCO 008
10. C PCO 009
11. C PCO 010
12. C PCO 011
13. C PCO 012
14. C PCO 013
15. C PCO 014
16. C PCO 015
17. C PCO 016
18. C PCO 018
19. C PCO 019

```

\*\*\*\*\*  
PCOM-PRINTS ALL LOCATIONS-IN THE COMMON-BLOCK  
NM - LINE PRINTER LOGICAL UNIT NUMBER  
NCOM = NUMBER OF LOCATIONS IN COMMON BLOCK  
\*\*\*\*\*  
COMMON VALU(1)  
WRITE(NM,2)  
2 FORMAT(/)  
1 WRITE(NM,1) (VALU(I),I=1,100)  
1 FORMAT( 2(10E11.3//),4(10E11.3//),4(10E11.3//))  
3 WRITE(NM,3) (VALU(I),I=101,NCOM)  
3 FORMAT( 5(10E11.3//))  
RETURN  
END

```

1. SUBROUTINE EULR6(A,Q)
2. COMPUTES EULER PARAMETERS FROM ROTATION MATRIX
3. SENSE IS A=TA
4. DIMENSION A(9),Q(4)
5. X=A(1)+A(5)+A(9)+1.
6. IF(X.LT.1E-8.AND.X.GT.-1E-8) X=0.0
7. Z4=SQRT(X)
8. IF(X)10,10,60
9. 10 D=0.
10. X=1.+A(4)-X
11. IF(X.LT.1E-8.AND.X.GT.-1E-8) X=0.0
12. IF(X)20,20,50
13. 20 Z1=0.
14. X=A(5)+1.
15. IF(X.LT.1E-8.AND.X.GT.-1E-8) X=0.0
16. IF(X)30,30,40
17. 30 Z2=0.
18. Z3=2.
19. GO TO 70
20. 40 Z2=SQRT(2.*X)
21. Z3=(A(6)+A(8))/Z2
22. GO TO 70
23. 50 Z1=SQRT(2.*X)
24. Z2=(A(2)+A(4))/Z1
25. Z3=(A(3)+A(7))/Z1
26. GO TO 70
27. 60 Z4=SQRT(X)
28. Z1=(A(6)-A(8))/Z4
29. Z2=(A(7)-A(3))/Z4
30. Z3=(A(2)-A(4))/Z4
31. Q(1)=-.5*Z1
32. Q(2)=-.5*Z2
33. Q(3)=-.5*Z3
34. Q(4)=-.5*Z4
35. RETURN
36. END

```

```

ER6 0010
ER6 0020
ER6 0030
ER6 0040
ER6 0050
ER6 0060
ER6 0070
ER6 0080
ER6 0090
ER6 0100
ER6 0110
ER6 0120
ER6 0130
ER6 0140
ER6 0150
ER6 0160
ER6 0170
ER6 0180
ER6 0190
ER6 0200
ER6 0210
ER6 0220
ER6 0230
ER6 0240
ER6 0250
ER6 0260
ER6 0270
ER6 0280
ER6 0290
ER6 0300
ER6 0310
ER6 0320.

```

```

1. SUBROUTINE EULR5(Q,A)
2. COMPUTES ROTATION MATRIX FROM EULER PARAMETERS
3. SENSE IS R=AR*
4. DIMENSION Q(4),A(3,3)
5. P=Q(4)*Q(4)-0.5
6. DO 50 I=1,3
7. DO 50 J=1,3
8. X=Q(I)*Q(J)
9. KGN=2*(J-I)
10. IF(KGN)10,40,-0
11. 10 SGN=KGN+3
12. GO TO 30
13. 20 SGN=KGN-3
14. 30 KGN=6-I-J
15. X=X+SGN*Q(KGN)*Q(4)
16. GO TO 50
17. 40 X=X+P
18. 50 A(I,J)=2.0*X
19. RETURN
20. END
ERS 0010
ERS 0020
ERS 0030
ERS 0040
ERS 0050
ERS 0060
ERS 0070
ERS 0080
ERS 0090
ERS 0100
ERS 0110
ERS 0120
ERS 0130
ERS 0140
ERS 0150
ERS 0160
ERS 0170
ERS 0180
ERS 0190
ERS 0200

```

```

1. SUBROUTINE LOOK1(F,FT,X,XT,NX,IX,MULT) LK1 0010
2. C***** LK1 0020
3. C ONE-DIMENSIONAL TABLE LOOKUP ROUTINE (* = RETURNED VALUES) LK1 0030
4. C *F ( =FT(X) ) LK1 0040
5. C FT FUNCTION TABLE FT(NR) LK1 0050
6. C NR NO. OF ROWS IN FT-TABLE LK1 0060
7. C NC NO. OF COLUMNS IN FT-TABLE LK1 0070
8. C X WORKING VALUE OF INDEPENDENT VARIABLE LK1 0080
9. C XT INDEPENDENT VARIABLE TABLE LK1 0090
10. C NX DIMENSION OF XT-TABLE LK1 0100
11. C *IX X INDEX ON PREVIOUS LOOKUP (UPDATED ON EACH CALL) LK1 0110
12. C MULT =0, USE PREVIOUS X LK1 0120
13. C ***** LK1 0130
14. C ***** LK1 0140
15. C ***** LK1 0150
16. C ***** LK1 0160
17. C ***** LK1 0170
18. C ***** LK1 0180
19. C ***** LK1 0190
20. C ***** LK1 0200
21. C ***** LK1 0210
22. C ***** LK1 0220

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1. SUBROUTINE LOOK2(F, FT, NR, X, XT, NX, Y, YT, NY, IX, IY, MULT) LK2 0010
2. ***** LK2 0020
3. C TWO-DIMENSIONAL TABLE LOOKUP ROUTINE (* = RETURNED VALUES) LK2 0030
4. C F = FT(X, Y) ( ) LK2 0040
5. C FT FUNCTION TABLE FT(NR, NC) LK2 0050
6. C NR NO. OF ROWS IN FT-TABLE LK2 0060
7. C NC NO. OF COLUMNS IN FT-TABLE LK2 0070
8. C X, Y WORKING VALUES OF INDEPENDENT VARIABLES LK2 0080
9. C XT, YT INDEPENDENT VARIABLE TABLES LK2 0090
10. C NX, NY DIMENSION OF XT, YT TABLES LK2 0100
11. C *IX, IY X, Y INDEXES ON PREVIOUS LOOKUP (UPDATED ON EACH CALL) LK2 0110
12. C MULT = 0, USE PREVIOUS X, Y LK2 0120
13. C MULT = 1, LOOK UP NEW X, Y, LK2 0130
14. C ***** LK2 0140
15. DIMENSION FT(1), XT(1), YT(1) LK2 0150
16. IF(MULT-1) 2, 1, 2 LK2 0160
17. 1 CALL INDEX(Y, YT, NY, IY, KEEP, RY) LK2 0170
18. I=1+(IX-1)*NR LK2 0180
19. II=I+NR LK2 0190
20. 2 CALL LOOK1(F, FT(I), X, XT, NX, IX, MULTI) LK2 0200
21. IF(KEEP-1) 3, 4, 3 LK2 0210
22. 3 CALL LOOK1(F2, FT(II), X, XT, NX, IX, 1) LK2 0220
23. F=(F2-F)*RY+F LK2 0230
24. 4 RETURN LK2 0240
25. END LK2 0250

```

```

1. SUBROUTINE INDEX(X,XT,NX,IX,KEEP,RATIO)          IND 0010
2. C*****                                     IND 0020
3. C TABLE LOOKUP ROUTINE (* = RETURNED VALUES)  IND 0030
4. C X WORKING VALUE OF INDEPENDENT VARIABLES     IND 0040
5. C XT INDEPENDENT VARIABLE TABLE XT(NX)       IND 0050
6. C NX DIMENSION OF X-TABLE                     IND 0060
7. C IX INDEX OF PREVIOUS LOOKUP (UPDATED ON EACH CALL)  IND 0070
8. C *KEEP = 0 - X.NE.ANY XT. INTERPOLATION WAS REQUIRED.  IND 0080
9. C *RATIO = 1 - X.EQ.XT(IX). INTERPOLATION NOT REQUIRED.  IND 0090
10. C ***** INTERPOLATION RATIO                IND 0100
11. C *****                                     IND 0110
12. C DIMENSION XT(1)                             IND 0120
13. C IX=0
14. C RATIO=0.
15. C KEEP=0
16. C IF(NX-IX)1,1,2
17. C 1 IX=NX-1
18. C 2 IF(IX-1)3,3,4
19. C 3 IX=1
20. C 4 IF(NX-1)10,10,5
21. C 5 IF(XT(IX)-X)6,10,7
22. C 6 IF(XT(IX+1)-X)8,9,11
23. C 7 IX=IX-1
24. C 8 IF(IX-1)9,5,5
25. C IX=IX+1
26. C IF(IX-NX)5,10,10
27. C 9 IX=IX+1
28. C 10 KEEP=1
29. C RETURN
30. C 11 RATIO=(X-XT(IX))/XT(IX+1)-XT(IX)
31. C RETURN
32. C END

```

```

1. C FUNCTION ATN2(S,C)
2. C *****
3. C ATN2 IS A SINGLE PRECISION ROUTINE
4. C ARCTAN IS IN RADIANS -PI TO +PI
5. C S=NUMERATOR
6. C C=DENOMINATOR
7. C C=SYSTEM ROUTINES USED ARE ATAN,SIGN
8. C C=ROUTINE IS VALID FOR ALL VALUES OF S AND C
9. C IF S AND C ARE BOTH 0.0, THE VALUE RETURNED IS ZERO.
10. C *****
11. C ATN2=0.
12. C IF(C)4,2,5
13. C 2 IF(S)3,7,3
14. C 3 ATN2=SIGN(1.5707963268,S)
15. C RETURN
16. C 4 ATN2=SIGN(3.1415926536,S)
17. C 5 ATN2=ATAN(S/C)
18. C 7 RETURN
19. C *****
20. C ATN 0010
21. C ATN 0020
22. C ATN 0030
23. C ATN 0040
24. C ATN 0050
25. C ATN 0060
26. C ATN 0070
27. C ATN 0080
28. C ATN 0090
29. C ATN 0100
30. C ATN 0110
31. C ATN 0120
32. C ATN 0130
33. C ATN 0140
34. C ATN 0150
35. C ATN 0160
36. C ATN 0170
37. C ATN 0180
38. C ATN 0190
39. C ATN 0200
40. C ATN 0210

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1. SUBROUTINE ZCOM (NCOM) ZCO 001  
2. C\*\*\*\*\* ZCO 002  
3. C SUBROUTINE TO ZERO ALL LOCATIONS IN COMMON BLOCK ZCO 003  
4. C ZCO 004  
5. C ZCO 005  
6. C NCOM = NUMBER OF LOCATIONS OF COMMON BLOCK ZCO 006  
7. C ZCO 007  
8. C\*\*\*\*\* ZCO 008  
9. COMMON VALU(1) ZCO 009  
10. DO 10 I=1,NCOM ZCO 010  
11. 10 VALU(I)=0. ZCO 011  
12. RETURN ZCO 012  
13. END ZCO 013



```

1. SUBROUTINE TWIST(THETA,T,N) TWI 001
2. C***** TWI 002
3. C TWI 003
4. C TWIST COMPUTES THE TRANSFORMATION MATRIX T FOR A ROTATION ABOUT TWI 004
5. C ONE OF THE 3 AXES IN THE SENSE TWI 005
6. C TWI 006
7. C R = T R' TWI 007
8. C TWI 008
9. C THETA = ANGLE OF ROTATION, IN RADIAN TWI 009
10. C T = 3X3 ROTATION MATRIX OUTPUT TWI 010
11. C N = AXIS NO. FOR WHICH ROTATION IS CALLED (1,2 OR 3) TWI 011
12. C TWI 012
13. C***** TWI 013
14. DIMENSION T(3,3) TWI 014
15. ZERO=0. TWI 015
16. ONE=1. TWI 016
17. CTHET= COS(THETA) TWI 017
18. DO 90 I=1,3 TWI 018
19. DO 90 J=1,3 TWI 019
20. IF(I=J)10,60,10 TWI 020
21. 10 IF((I=N)*(J=N))30,20,30 TWI 021
22. 20 X=ZERO TWI 022
23. GO TO 50 TWI 023
24. 30 X= SIN(THETA) TWI 024
25. IF(N=2)50,40,50 TWI 025
26. 40 X=-X TWI 026
27. 50 T(I,J)=-X TWI 027
28. GO TO 90 TWI 028
29. 60 IF(I=N)70,80,70 TWI 029
30. 70 X=CTHET TWI 030
31. GO TO 90 TWI 031
32. 80 X=ONE TWI 032
33. 90 T(J,I)=X TWI 033
34. RETURN TWI 034
35. END TWI 035

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```

1. SUBROUTINE AUTO(X,E,KONTROL)
2. DIMENSION X(40),E(40)
3. ERW=SQRT(E(1)*E(1)+E(2)*E(2)+E(3)*E(3))
4. ERQ=SQRT(E(4)*E(4)+E(5)*E(5)+E(6)*E(6)+E(7)*E(7))
5. ERV=SQRT(E(8)*E(8)+E(9)*E(9)+E(10)*E(10))
6. ERR=SQRT(E(11)*E(11)+E(12)*E(12)+E(13)*E(13))
7. ER=SQRT(ERW*ERW+ERQ*ERQ)
8. KONTROL=1
9. IF(ER.GT.32.E-5)KONTROL=2
10. IF(ER.LE..5E-5)KONTROL=3
11. RETURN
12. END

```

```

1. SUBROUTINE BLOCK(NM, NP, CASE, NPV, IVAR, PNAME, PVALU, SCALE, IPW, NIPR) BLO 001
2. C***** BLO 002
3. C BLO 003
4. C STANDARD BLOCK-PRINTOUT ROUTINE BLO 004
5. C BLO 005
6. C NM = LINE PRINTER-LOGICAL UNIT NUMBER, = 6 FOR IBM-7044 BLO 006
7. C NP = PLOT FILE LOGICAL UNIT NUMBER, = 12
8. C CASE = ALPHAMERIC CASE TITLE BLO 007
9. C NPV = NUMBER OF PRINT OR PLOT VARIABLES BLO 008
10. C IVAR = LOCATION ARRAY OF PRINT VARIABLES IN COMMON BLOCK BLO 009
11. C PNAME = ALPHAMERIC NAMES OF PRINT OR PLOT VARIABLES BLO 010
12. C JM INPUT DATA
13. C PRNM = ALPHAMERIC NAMES OF PRINT VARIABLES
14. C PVALU = SCALED PRINT OR PLOT VALUES BLO 011
15. C SCALE = SCALE FACTORS TO BE APPLIED TO PRINT VARIABLES BLO 012
16. C IPW = PRINT-PLOT FLAG
17. C IF IPW = 0, PRINT AND PLOT
18. C IF IPW = 1, PRINT ONLY
19. C IF IPW = 2, PLOT ONLY
20. C
21. C***** BLO 013
22. C DIMENSION CASE(18), IVAR(90), PVALU(90), SCALE(90), PNAME(90) BLO 014
23. C I, IPW(90), PLT(90), PRNM(90) BLO 015
24. C COMMON VALU(400)
25. C
26. C*****SET UP. PRINT. ARRAY BLO 016
27. C I=0 BLO 017
28. C K=1 BLO 018
29. C L=1 BLO 019
30. C
31. C 10 J=I+1 BLO 020
32. C J=IVAR(I) BLO 021
33. C IF(IPW(I)-1) 5,6,7
34. C 5 PVALU(L)=SCALE(I)*VALU(J) BLO 022
35. C PRNM(L)=PNAME(I)
36. C PLT(K)=PVALU(L)
37. C K=K+1
38. C L=L+1
39. C IF(I=NPV) 10,20,20 BLO 023
40. C 6 PVALU(L)=SCALE(I)*VALU(J) BLO 022
41. C PRNM(L)=PNAME(I)
42. C L=L+1
43. C IF(I=NPV) 10,20,20 BLO 023
44. C 7 PLT(K) = SCALE(I)*VALU(J)
45. C K=K+1
46. C IF(I=NPV) 10,20,20
47. C*****PRINT OUTPUT BLOCK
48. C 20 IF(NIPR.LT.0) GO TO 30
49. C WRITE(NM,120) VALU(1), ( CASE(J), J=1,18)
50. C WRITE(NM,110) ((PRNM(I)), PVALU(I), I=1, L-1)
51. C 30 CONTINUE
52. C WRITE(MP) VALU(1), (PLT(I), I=1, K-1)
53. C 120 FORMAT(/IX,6HTIME ,1 E15.6,2X,18A4,/)

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53. 110 FURNAT(6(2X,A4,E14.8))  
54. RETURN  
55. END

BLO 026  
BLO 029  
BLO 030

```

1. SUBROUTINE MINV(A,N,D,L,M)
2.
3.
4. MATRIX INVERSE, OF AN NXR MATRIX-A INTO THE SAME MATRIX-A
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\*\*\*\*\*  
 DIMENSION A(1),L(1),M(1)  
 SEARCH FOR LARGEST ELEMENT  
 D=1.0  
 NK=M  
 DO 80 K=1,N  
 NK=NK+M  
 L(K)=K  
 M(K)=K  
 KK=NK+K  
 BIGA=A(KK)  
 DO 20 J=K,N  
 IZ=M\*(J-1)  
 DO 20 I=K,N  
 IJ=IZ+I  
 IF( ABS(BIGA)- ABS(A(IJ))) 15,20,20  
 15 BIGA=A(IJ)  
 L(K)=I  
 M(K)=J  
 20 CONTINUE  
 INTERCHANGE ROWS  
 J=L(K)  
 IF(J=K) 35,35,25  
 25 KI=K-N  
 DO 30 I=1,M  
 KI=KI+N  
 HOLD=-A(KI)  
 JI=KI-K+J  
 A(KI)=A(JI)  
 30 A(JI)=HOLD  
 INTERCHANGE COLUMNS  
 35 I=M(K)  
 IF(I=K) 45,45,38  
 38 JP=N\*(I-1)  
 DO 40 J=1,M  
 JK=NK+J  
 JI=JP+J  
 HOLD=-A(JK)  
 A(JK)=A(JI)

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53.	40 A(JI) = HOLD	MIN 0053
54.	C DIVIDE COLUMN BY MINUS PIVOT (VALUE OF PIVOT-ELEMENT IS CONTAINED IN BIGA)	MIN 0054
55.	C	MIN 0055
56.	45 IF(ABS(BIGA)-1.5-20)46,46,48	MIN 0056
57.	46 D=0.3	MIN 0057
58.	RETURN	MIN 0058
59.	48 DO 55 I=1,N	MIN 0059
60.	IF(I-K) 50,55,50	MIN 0060
61.	50 IK=IK+I	MIN 0061
62.	A(IK)=A(IK)/(-BIGA)	MIN 0062
63.	55 CONTINUE	MIN 0063
64.	C REDUCE MATRIX	MIN 0064
65.	DO 65 I=1,N	MIN 0065
66.	IK=IK+I	MIN 0066
67.	HOLD=A(IK)	MIN 0067
68.	IJ=I-N	MIN 0068
69.	DO 65 J=1,N	MIN 0069
70.	IJ=IJ+N	MIN 0070
71.	IF(I-K) 60,65,60	MIN 0071
72.	60 IF(J-K) 62,65,62	MIN 0072
73.	62 KJ=IJ-I+K	MIN 0073
74.	A(IJ)=HOLD*A(KJ)+A(IJ)	MIN 0074
75.	65 CONTINUE	MIN 0075
76.	C DIVIDE ROW BY PIVOT	MIN 0076
77.	KJ=K-N	MIN 0077
78.	DO 75 J=1,N	MIN 0078
79.	KJ=KJ+N	MIN 0079
80.	IF(J-K) 70,75,70	MIN 0080
81.	70 A(KJ)=A(KJ)/BIGA	MIN 0081
82.	75 CONTINUE	MIN 0082
83.	C PRODUCT OF PIVOTS	MIN 0083
84.	D=D*BIGA	MIN 0084
85.	C REPLACE PIVOT BY RECIPROCAL	MIN 0085
86.	A(KK)=1.0/BIGA	MIN 0086
87.	80 CONTINUE	MIN 0087
88.	C FINAL ROW AND COLUMN INTERCHANGE	MIN 0088
89.	K=N	MIN 0089
90.	100 K=(K-I)	MIN 0090
91.	IF(K) 150,150,105	MIN 0091
92.	105 I=L(K)	MIN 0092
93.	IF(I-K) 120,120,108	MIN 0093
94.	108 JQ=N*(K-I)	MIN 0094
95.	JR=N*(I-I)	MIN 0095
96.	DO 110 J=1,N	MIN 0096
97.	JK=JQ+J	MIN 0097
98.	HOLD=A(JK)	MIN 0098
99.	JI=JR+J	MIN 0099
100.	A(JK)=-A(JI)	MIN 0100
101.	110 A(JI) =HOLD	MIN 0101
102.	120 J=N(K)	MIN 0102
103.	IF(J-K) 100,100,125	MIN 0103
104.	125 KI=K-N	MIN 0104

105.	DO 130 I=1,N	MIN 0105
106.	KI=KI+N	MIN 0106
107.	HOLD=A(KI)	MIN 0107
108.	JI=KI-K+J	MIN 0108
109.	A(KI)=A(JI)	MIN 0109
110.	130 A(JI)=HOLD	MIN 0110
111.	GO TO 100	MIN 0111
112.	150 RETURN	MIN 0112
113.	END	MIN 0113

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1. SUBROUTINE RUMK2(KUTTA,N)
2. REAL NINE
3. DIMENSION C1(40),C2(40),C3(40),C4(40),C5(40),S1(40),E(40)
4. COMMON TIME,DT,DTP,DTSAN,TRUB,TERD,PCOUM(14)
5. COMMON XC(40)
6. COMMON X(40)
7. DATA HALF,THIRD,SIXTH,EIGHTH,.5,.3333333,.16666667,.125/
8. DATA TWO,THREE,FOUR,EIGHT,NINE,THIRTY/2.,3.,4.,8.,9.,30./
9. GO TO (1,2,3,4,5),KUTTA
10. 1 00 11 I=1,N
11. SX(I)=X(I)
12. C1(I)=DT*XD(I)
13. 11 X(I)=SX(I)+THIRD*C1(I)
14. RETURN
15. 2 00 12 I=1,N
16. C2(I)=DT*XD(I)
17. 12 X(I)=SX(I)+SIXTH*(C1(I)+C2(I))
18. RETURN
19. 3 00 13 I=1,N
20. C3(I)=DT*XD(I)
21. 13 X(I)=SX(I)+EIGHT*(C1(I)+THREE*C3(I))
22. RETURN
23. 4 00 14 I=1,N
24. C4(I)=DT*XD(I)
25. 14 X(I)=SX(I)+HALF*(C1(I)-THREE*C3(I)+FOUR*C4(I))
26. RETURN
27. 5 00 15 I=1,N
28. C5(I)=DT*XD(I)
29. X(I)=SX(I)+SIXTH*(C1(I)+FOUR*C4(I)+C5(I))
30. E(I)=(TWO*C1(I)-NINE*C3(I)+EIGHT*C4(I)-C5(I))/THIRTY*(DT/.25)
31. CALL AUTO(X,E,KONTRL)
32. IF(KONTRL-2)10,20,30
33. 20 DT=DT*HALF
34. 00 21 I=1,N
35. 21 X(I)=SX(I)
36. KUTTA=0
37. RETURN
38. 10 TIME=TIME+DT
39. RETURN
40. 30 TIME=TIME+DT
41. DT=DT*TWO
42. RETURN
43. END
```



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APPROVAL

USERS GUIDE FOR SKYLAB DYNAMICS PROGRAM, SKYDYN

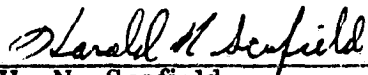
by M. S. Hopkins

The information in this report has been reviewed for technical content. Review of any information concerning Department of Defense or nuclear energy activities or programs has been made by the MSFC Security Classification Officer. This report, in its entirety, has been determined to be unclassified.



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