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## NASA TECHNICAL MEMORANDUM

NASA TM-82429

### ASSEMBLY AND TESTING OF 1/4 INCH MR54040 TF04 RESISTOFLEX DYNATUBE FITTINGS

By J. H. Enl Materials and Processes Laboratory





NASA

# George C. Marshall Space Flight Center Marshall Space Flight Center, Alabama

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### TECHNICAL MEMORANDUM

### ASSEMBLY AND PERFORMANCE OF 1/4 INCH MR54040 TF04 RESISTOFLEX DYNATUBE FITTINGS

### 1. INTRODUCTION AND BACKGROUND

Dynatube is a trede name for a titanium (6AI-4V) threaded fitting used to join metal tubing (Figs. 1 and 2). These fitting are manufactured by the Resistoflex Corporation of Rcseland, N.J. The outside surface of the metal tube is mechanically swaged into grooves in the inside surface of the fitting. Swaging is performed either by manual or power rotation of an expanding mandrel type tool (Figs. 3 and 4). These fittings have a long history of successful use in commercial and military aircraft and aerospace systems with minimum weight and critical leak rate requirements.

During build-up of hardware for the Space Shuttle Thrust Vector Control (TVC) system, some tube assemblies using Dynatube fittings  $_{5}$ were fabricated that did not pass the prescribed leak test of  $1 \times 10^{-5}$ standard cubic centimeters per second of helium at 400 psig. Leakage was detected between the fitting and the outside diameter of the tube. These tests were conducted using a helium sniffer and also by using "Leak Tek" solution and noting bubbles of escaping helium gas. It was determined that these same tube assemblies had previously passed the leak test requirements. Fittings are tested repeatedly as build-up of the assembly progresses to the next higher level. Sectioning of the leaking joint revealed a very light swage of less than 0.002 in. radial deformation of the tube into the fitting grooves which are 0.007 in. deep. Further investigation revealed that some lightly swaged fittings had passed all hydrostatic leak testing but could be made to leak if they were rotated on the tube during installation (Figs. 5 and 6).

Further investigation determined that Dynatube fitting assemblies had been made using swage tooling that was worn and/or misassembled. The worn tooling swaged light, as little as 0.002 in. deep in the four 0.007 in. deep fitting joints. The misassembled swage tool swaged short, i.e. good swages in the first three grooves but little or no swage in the farthest groove (4th groove) from the point of entry of the mandrel into the tube to be swaged. Refurbishment of the tooling by replacing the worn rollers on the expanding mandrel and by correcting the out of place spacer washers in the misassembled tool corrected the problem of swaging good joints. Correctly assembled and refurbished tooling can consistently swage grooves 0.005 in. deep or more when used by a trained operator. However, x-ray of inplace tubing assemblies revealed that some joints had been manufactured and installed that were lightly swaged and that had successfully passed the helium leak tests. A program was developed to determine the performance of lightly swaged joints and to duplicate and test joints equal to or worse than those known to be installed on the flight TVC hardware. This program was comprised of the following:

1) To be statistically meaningful, 100 each  $\frac{1}{4}$  in. fittings were procured and fabricated into 50 each tube assemblies with one fitting at each end (Fig. 1).

2) All swage tooling was refurbished by the Resistoflex Corporation to the correct company specifications.

3) A tolerance study was made on the tubing, the tooling, and the fitting to determine the worst case swage that could be made (Appendix). Swages were made at minimum possible, medium range, and full depth. Additionally, samples were prepared that were fully swaged, but swaged short. Swage tool settings to accomplish these conditions were 0.219. 0.221, 0.223, 0.225, and 0.228 in. The 0.228 in. setting is the normal setting recommended by Resistoflex Corporation for these fittings. A11 samples were measured (I.D.) x-rayed to determine amount of swage, proof pressure tested at 7000 psi, mass spectrometer leak tested (sniffer method) at 400 psi with helium, rotated  $15^{\circ}$  in the fitting to simulate a careless fit-up, re-leak checked, and pressure tested. After rotation, approximately 25 percent of the samples did not pass the helium leak. These were assembled into a closed loop arrangement and pressurized at 400 psi with water. The pressure was maintained for two weeks. None of the swaged fittings that leaked helium, leaked water during the two weeks under pressure.

After static testing, the tubes were vibration tested to Shuttle flight level in the radial, tangential, and longitudinal axis (Table 1). While being vibrated, all tubes were pressurized at 400 psi with water containing red dye to enhance visibility in case of a leak. Sixty each fittings, including all the shallow swages and all the short swages, were tested. None leaked water at 400 psi during the vibration tests which simulated flight conditions.

### 2. FINDINGS

1) Resistoflex Dynatube swage tooling in the proper state of repair and used properly will consistently yield adequate swages. (0.005 or more in the first three grooves.)

2) The light and short swage conditions found were caused by worn and improperly assembled tooling respectively.

3) The inhouse MSFC test program demonstrated that a MR 54040 TF04 swage joint with at least 0.0015 in. radial tube deformation, while 5 not desirable, will pass the required leak rate of not more than  $1 \times 10^{-5}$  sccb helium at 400 psig. Additionally this joint will not leak water when pressurized to 400 psi and vibrated to 28.2 grms composite in the radial and tangential axis and 27.0 grms composite in the longitudinal axis.

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Figure 1.  $\frac{1}{4}$  inch 304L stainless steel tube with MR54050 TF04 fitting each end.

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### SWAGED TUBE

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### 6AL -4V DYNATUBE FITTING

Figure 2. MR 54040 TF04 dynatube fitting.



Figure 3. Swage tool (fully assembled).



Figure 4. Swage tooi (disassembled).



Figure 5. Enlarged x-ray of fitting and tube showing minimal swage of tube into fitting greeves.



ROTATING THE TUBE IN THE SWAGE FITTING COULD OCCUR DURING INSTALLATION WHEN ONE END OF THE ASSEMBLY HAS BEEN SECURED THEN THE OTHER END IS DRAWN AGAINST ITS MATING FITTING CAUSING A ROTATIONAL TORQUE ON THE OPPOSITE END.

Figure 6. Example of possible rotation.

**APPEN DIX** 

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### **TOLERANCE ANALYSIS**

### FITTING

### TUBE

### Resistoflex MR54040

### MIL-T-6845C

Size Range Outside Diameter (Inch)	Tolerance
‡ thru ½ INCL	+.004000
over ½ thru 1½	+.005000
over 1½ thru 24	+.010000
over 2 <del>]</del> thru 3	+.010010
over 3 thru 5	+.015015

Tuba	OD.	950	+.004
TUDE	<b>UD</b> :	. 230	000

Tube Wall:  $.020 \pm .002 = .040 \pm .004$  cumulative

			. 250	+.004
			040	±.004
Tubo	ID	_	210	+.008
Tupe	IJ	-	. 210	004

Test Gage	
Diameter	.224 ±.002
Tube Wt.	<u>+.040</u> ±.004
Range	.264 ±.006
Fitting ID	$255 \pm .002$
	<u>.009 ±.008</u>

This tolerance guarantees positive interference fit even if (in the unlikely event) the tube is the smallest possible, with the thinnest wall permissible, and the fitting is at the extreme upper limit. Factors such as spring back and wall thinning are handled by adding an additional .004 inch extra expansion to tool settings.



# TABLE 1. VIBRATION INPUT TO SRB TVC TUBE (0.25" Dia.)ASSEMBLIES

Lift-off and Boost Random Vibration Criteria (180 seconds in each axis)

RADIAL AXIS	LONGITUDINAL AXIS						
20 Hz @ 0.1 g <sup>2</sup> /Hz	20- 60 Hz <b>0</b> 0.1 g <sup>2</sup> /Hz						
20- 60 Hz @ +7 dB/oct	60- 200 Hz @ +5.5 dB/oct						
60- 150 Hz @ 1.2 g <sup>2</sup> /Hz	200- 400 Hz @ 0.9 g <sup>2</sup> /Hz						
150-2000 Hz @ -2 dB/oct	400-2000 Hz @ -4 dB/oct						
2000 Hz @ 0.2 g <sup>2</sup> /Hz	2000 Hz @ 0.1 g <sup>2</sup> /Hz						
Composite = 28.2 grms	Composite = 27.0 grms						
TANGENTIAL AXIS							

### IANGENTIAL AAIS

20-	60	Hz	Q	$0.1 \text{ g}^2/\text{Hz}$
60-	100	Hz	0	13.5 dB/oct
100-	300	Hz	0	$1.0 \mathrm{g}^2/\mathrm{Hz}$
300-	2000	Hz	0	-3.5 dB/oct
	2000	Ηz	0	$0.1 \text{ g}^2/\text{Hz}$

Composite = 28.6 grms

### **EXPLANATION OF TABLE 2**

The data contained in Table 2 denote the specimen number, the fitting on each end (No. 1 and No. 2) of the tube, the tube diameter in inches, and the swage tool setting in inches. The depth of swage per groove determination was made by evaluation of x-rays using an optical comparator. The No. 1 groove is the first groove from the sealing surface and the No. 4 groove is the last groove on the tube end of the fitting. The x-ray is a cross sectional view and the reading is left to right top and bottom. The determination was made by positioning the fine line of the optical comparator on the land of the groove and reading the amount of upset of the tube into the fitting groove. The tube internal diameter of swage was made using an internal micrometer with a stop to ensure that all tubes were measured at the same position. The column noting helium leakage determines if the fitting leaked in excess of 1 x 10<sup>-5</sup> scc's of helium at 400 psig. Next, the fitting was rotated 15 degrees on the tube to simulate a careless assembly (Fig. 6). After rotation the fitting was rechecked with the mass spectrometer to determine leakage. The remaining data column denotes those fittings selected for vibration testing.

\*Sealing surface to left.

ILING SURFACE TO LEFT		COMMENTS												1			
· SEA	0	1315	11	×	×	×	×	×	×	×	×	×	×	×	×	×	×
	ED	13	0.1	×	×	×	×	×				×			×	×	×
	-14	104	S3A ON	×		×	× -	- × -	×	×	×	×	x	×	×	×	×
	3	14	SIA		×												
	3	194 194	ANN IN	2168	2168	217	2168	2167	2167	2168	217	2168	2112	217	217	219	219
		H	4	000	000	000	000	000	000	000	000	000	000	000	000	000	000
	#	+ RIG	9	000	000	000	000	000	000	000	000	000	000	000	000	000	.001
	<ul> <li>DEPTH OF SWAGE PER GROOVE</li> </ul>	A LEFT.	2	000	000	000	000	000	000	000	000	000	000	100.	000	.001	.002
ESTIN		BOTTON	-	900	002	002	002	100	100	100	001	100	100	.002	.002	0025	.0025
ASFC T		-	4	000	000	000	000	000	000	000	000	000	000	000	000	000	100
		- RIGH	3	000	000	000	000	000	000	000	000	000	000	000	000	000	.002
		EFT -	2	000	000	000	000	000	100	000	000	001	000	100	000	100	002
		TOPL	-	900	.002	.002	.002	.001	100	100	001	100	.001	.002	100	9200.	0025
	108E 0.D 100L 35WMGE 100L 35THNG		3S 1 1S	219	219	219	219	219	219	219	219	219	219	219	219	122	122.
			.250	.250	250	.250	250	250	250	250	250	250	250	.250	.250	.250	
		380. .0.1	1	205	204	203	204	204	204	204	204	204	203	207	.207	206	206
	9	.0.I	.13	253	253	254	255	254	757	754	253	754	254	754	254	253	253
	# 5	0.011	ш	-	2	-	2	-	2	-	2	-	2	-	2	-	2
	= 3.JO <b>1</b>		т				•		7		•		n		0		

# TABLE 2. RESISTOFLEX DYNATUBE MSFC TESTING

RESISTOFLEX DYNATUBE MSFC TESTING

_	_	_	_	_	_	-	-	-								
COMMENTS									FAILED PRESSURE TEST AT 6500PSI							
NO	ITAR ITAR	VIBI	×	×	×	×	×	×			×	×	×	×	×	×
03)	LEAL	ON		×	×	×	×				×	×	×	×	×	
-14	101	SEA	×					×								×
X	737	ON	×	×	×	×	×	×			×	×	×	×	×	×
	3H	SEA														
	.D.	AS V	2188	2138	2136	2192	2192	2188	2165	2155	2193	2185	2187	2135	2186	2185
	TH	•	8	8	8	8	8	8	8	8	80	8	8	8	8	8
#	1 H		100	100	100	<b>10</b> 0	6	8	8	8	<b>1</b> 8	8	100	<b>10</b>	<b>1</b> 8	1001
GROOVE	M LEFT	2	002	002	.002	.002	.002	002	8	8	8	.002	.002	002	.002	200
GE PER	BOTTO	-	.003	<b>60</b>	600	003	.003	003	<b>100</b>	8	8	8	88	<b>60</b>	8	600
OF SWA	H	+	000	100	80	80	80	8	000	80	<b>10</b> 0	900	900	900	100	900
HT430.	H RIG	3	100'	100	100.	<b>10</b> 0	100	100	900	8	.002	100	<b>19</b>	100	190	190
	LEFT -	2	200	.002	.002	.002	.002	.002	900	80	.003	.002	.002	002	.002	.002
	TOP	1	603	.003	E00.	<b>COO</b> .	.003	600	100	100	000	003	.003	.003	600	500
SWAGE TOOL SNITT32		122	122	122	122	221	122	219	219	122	122	122	122	127	127	
38UT .0.0		250	250	250	250	952	220	250	957	250	220	720	952	982	220	
38UT .0.1		202	202	202	201	204	204	201	502	207	205	201	81.	208	208	
9	FITTING .D.I		283	223	Ŕ	12	121	×.	12	222	223	121	527	121	Ā	527
# DNILLIA		-	~	-	~	-	~	-	~	-	8	-	~	-	~	

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12

\*Sealing surface to left.

(Continued) TABLE 2.

# DNILLIS

# 3801

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TABLE 2. (Continued)

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COMMENTS																
VIBRATION		×	×	×	×	×	×			×	×			×	×	
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-14	LOH	SEA	~	~	×		×	*	-	×	×	×	×	×	×	×
J N N	H	SEA	-	-		-	-	-		~	-	-	-			
1	DAV	A	2166	<b>61</b> 0'	2188	2183	219	219	2193	2192	2196	2196	220	2204	2166	2168
	нт	4	100'	100'	<b>1</b> 8	.002	<b>10</b> 0	<b>10</b>	.003	600	60	00	88	.003	8	8
# 3	+ RIG	3	100	100	100	.002	100	100.	1004	.004	100	100	8	100	8	8
GROOVI	M LEFT	2	.002	.002	200.	<b>600</b> .	.002	.002	1004	900	100	90	8	8	8	8
SE PER	BOTTO	1	.003	.003	003	8	.003	:003	.005	.005	.005	900	500	500;	100	100
DF SWA	Ŧ		100	100	<b>10</b> 0	<b>10</b>	100	100	.003	.003	.003	.003	E001	.003	990	.000
DEPTH	+ RIG	3	196	18	100	<b>10</b>	100	100	100	100	.003	100	100	1001	80	900
•	EFT -	2	003	.002	2007	2007	2003	.002	100	<b>N</b> 00	100	900	100	1004	000	.000
1 TOP L		-	88	800	.003	.003	500	003	.005	300;	.005	.005	3005	005	100	1001
SWAGE SWAGE		35 1 15	127	127	127	127	127	127	222	223	223	223	223	223	219	219
33UT .0.0		9 <b>2</b>	750	250	250	720	250	720	220	957	520	22	720	957	957	
38UT .0.1		Ŕ	201	200	203	202	202	708	700	207	702	205	708	206	206	
PITTING .D.I		2	2	22	597	74	355	55	727	253	223	124	5	154	192	
# DNITTIA		-	2	-	2	-	2	-	2	-	2	-	2	-	2	
# 33UT		2		2		"		2		2		\$	8	5	5	

\*Sealing surface to left.

TABLE 2. (Continued)

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Σ	2
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IG SURFACE TO LEFT		COMMENTS															
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	3.	/11	GN	×	×	×	×	×	×	×	×	×	×	×	×	×	×
		H	SBA					-				-					
	1	.D.	IA 12	2198	2196	2198	2187	2195	2197	2197	2197	2198	2196	220	2197	2196	2195
		IIGHT	4	.003	.003	50	903	002	003	003	003	003	8	.003	8	50	8
	n	+ RIG		8	8	002	80	003	803	.003	500	8	8	8	60	5	100
DNIIC	ROOVE	M LEFT-	2	8	8	68	003	603	803	003	003	8	8	8	80	003	003
	GE PER (	BOTTOM	-	80	.003	8	8	8	8	8	8	8	500;	8	80	80	80
	DF SWAG		4	003	80	100	8	003	003	.003	002	803	003	80	600	100	100
	DEPTH	TOP LEFT RIGH	3	8	8	903	8	80	.003	88	8	900	80	100	.003	<b>100</b>	50
	•		2	8	8	8	8	600	500	58	.00 0	8	8	8	900	002	003
			-	500	8	8	8	8	8	8	8	8	8	8	100	<b>30</b> 0	100
Ì	D/	001 100	3S 1 1	223	223	523	52	223	223	223	223	223	22	223	223	527	523
I	1	0.0		220	720	952	8	952	8	220	250	250	952	952	957	250	952
I		1001		201	<b>50</b>	80	502	207	5	306	<b>50</b>	508	201	201	202	50	205
	91	.a.i		2	322	283	Ŕ	Ā	×.	A	2	52	223	552	Ā	2	254
	# DNIL	nц		-	2	-	2	-	2	-	2	-	2	-	2	-	2
		1 I.A.	L	2	1	2	1	2	5	*	8	*		2	1		1

\*Sealing surface to left.

\*Sealing surface to left.

ALING SURFACE TO LEFT		COMMENTS							FAILED PRESSURE TEST- IMPROPER SWAGE - GAP								
· SE	0	1115	31 131A			×	×			×	×	×	×				
	11	11	, C.i		×	×	×	-		-	×	×	×	×	×	×	×
1	N	m	leñ	×	×	×	×			×	×	×	×	×	×	×	×
	-	114	334		-	-	-	+		-			-			-	
	1	.D.	14	2209	2206	2122	1127	216	Ę,	2206	2213	3206	2206	5022	Ŗ	2208	1027
		H	4	8	8	8	80	8	GAP	8	8	8	8	8	8	8	80
	11	PII +		8	8	8	8	8	GAP	8	8	8	8	8	500	8	8
	GROOV	DM LEFT	2	8	8	8	. 8	80	đ	8	8	8	8	8	500	8	8
ESTIN	GE PER	80110	-	8	8	8	8	8	GAP	8	8	8	8	80	8	8	802
MSFC	OF SWA	LEFT RIGHT	4	8	8	8	8	8	8	8	8	8	8	8	8	8	500
	DEPTH		3	8	8	ğ	8	8	8	8	8	8	8	10	10	8	8
			2	8	8	8	8	8	8	8	8	8	8	8	30	8	24
		10P	-	8	8	ŝ	8	100	80	8	900	8	8	8	80	8	8
[			.35 1 15	222	82	522	8	219	510	82	225	527	322	325	275	27	325
	1	33UT .0.0		220	250	250	250	952	250	8	250	220	952	250	250	82	8
	1.D. 1.D. 33UT 1.D.			306	802	50	500	203	201	302	208	204	201	206	82	208	206
			14	Ā	527	2	52	2	Ā	ž	Ā	14	152	192	52	Ā	12
	# DNITTIA		113	-	2	-	2	-	2	-	2	-	2	-	2	-	2
L	#	390	1	2	1	1	R	;	•	\$	*		8	;	5	,	R

# TABLE 2. (Continued)

RESISTOFLEX DYNATULE MSEC TESTING

# TABLE 2. (Continued)

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\*Sealing surface to left.

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\*Seeling surface to left.

COMMENTS																
NO	TAR 312	81V 3T	×	×	×	×	×	×								
KED D	LEA	ON	×	×	×	×	×	×	×	×	×	×	×	×	×	×
NA.	31	0.4	×	×	×	×	×	×	×	×	×	×	×	×	×	×
3	Ĥ	SBA														
5	.0.1 1311	A	2236	2234	12231	2236	2236	224	227	223	2228	2232	224	2232	222	6222
	IGHT	4	000	000	000	000	000	000	900	500	900	900	900	500	900	8
	1	3	001	001	001	001	001	001	900	905	900	900	900	900	800	88
SOUVE :	ALEFT	2	001	001	001	001	001	001	001	001	001	001	001	001	001	603
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TABLE 2. (Continued)

TABLE 2. (Concluded)

RESISTOFLEX DYNATUBE	MSFC TESTING	

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### APPROVAL

### ASSEMBLY AND TESTING OF 1/4 INCH MR54040 TF04 RESISTOFLEX DYNATUBE FITTINGS

### By J. H. Ehl

The information in this report has been reviewed for technical content. Review of any information concerning Department of Defense or nuclear energy activities or programs has been made by the MSFC Security Classification Officer. This report, in its entirety, has been determined to be unclassified.

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