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Development of Flying Qualities Criteria for Single-Pilot Instrument Flight Operations: Interim Report

Aharon Bar-Gill, W. Barry Nixon
and George E. Miller

FLIGHT RESEARCH LABORATORY
PRINCETON UNIVERSITY
Princeton, N.J. 08544

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June 1982

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National Aeronautics and
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Langley Research Center
Hampton, Virginia 23665
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ABSTRACT

Research is being conducted to develop flying qualities criteria for Single Pilot Instrument Flight Rule (SPIFR) operations. Significant progress has been made with regard to most of the key issues encompassed in the SPIFR research program. The ARA aircraft has been modified and adapted for SPIFR operations. Aircraft configurations to be flight-tested have been chosen and matched on the ARA in-flight simulator, implementing modern control theory algorithms. Mission planning and experimental matrix design have been completed. Microprocessor software for the onboard data acquisition system has been debugged and flight-tested. Flight-path reconstruction procedure and the associated FORTRAN program are at a final stage of development. Work has begun on algorithms associated with the statistical analysis of flight test results and the SPIFR flying qualities criteria deduction.

PREFACE

This investigation is being conducted by the Flight Research Laboratory at Princeton University, Princeton, New Jersey under Contract No. NAS1-15764 for the NASA Langley Research Center. This is the first annual technical report, and it reflects the SPIFR research effort through May 1981.

The principal investigator for the study is Professor Robert F. Stengel. He is assisted by W. Barry Nixon, senior technical staff member, George E. Miller, technical staff member, Aharon Bar-Gill, graduate student, Thomas O. Williams, technical staff member, Barton C. Reavis, technical associate and electronic technicians Louis Pokrocos, Thomas Frobose and Karl Thomas.

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TABLE OF CONTENTS

	<u>Page</u>
PREFACE	i
LIST OF FIGURES	iv
LIST OF TABLES	v
LIST OF SYMBOLS	vi
1. INTRODUCTION	1
1.1 Background and Goals	1
1.2 Organization of the Report	2
2. AIRCRAFT AND DATA ACQUISITION SYSTEM PREPARATION	3
2.1 Aircraft System Modifications	3
2.2 Instrumentation and Data Recording System	8
2.3 Software Development	12
3. THEORETICAL ASPECTS OF EXPERIMENT DESIGN AND FLIGHT PATH RECONSTRUCTION	14
3.1 Aircraft Dynamic Model	14
3.2 Candidate SPIFR Configurations via the Output Command Algorithm	18
3.3 Experimental Matrix Design	20
3.4 Implementation of SPIFR Configurations via the Implicit-Model-Following Algorithm	22
3.5 Effects of Navigational Accuracy and the "Learning Curve" Effect on Mission Planning	24
3.6 Optimal Smoothing of Flight Test Records and Flight Path Reconstruction	28
4. PRELIMINARY FLIGHTS	40
5. CONCLUSION	45

TABLE OF CONTENTS (cont.)

	<u>Page</u>
APPENDIX A: DERIVATION OF THE LINEARIZED VERSIONS OF THE SIMPLIFIED AND THE IMPROVED KINEMATIC MODELS	47
APPENDIX B: PROGRAM LISTINGS	54
APPENDIX C: COMPUTER SYSTEMS FOR PREPROCESSING AND POST-FLIGHT DATA REDUCTION	130
APPENDIX D: INTEGRATION OF DISTANCE MEASURING EQUIPMENT (DME) INTO THE DATA COLLECTION SYSTEM	138
REFERENCES	153

LIST OF FIGURES

<u>No.</u>		<u>Page</u>
2-1	Avionics Research Aircraft, Navion N5113K	4
2-2	Overview of the ARA In-Flight Simulator System	5
2-3	Cockpit Displays of the ARA. Modular SPIFR Evaluation Pilot Panel at Left	7
2-4	SPIFR Digital Data Recording System	9
3-1	Block Diagram for Implementation of a SPIFR Configuration on the ARA In-Flight Simulator	23
3-2	SPIFR Flight Path, Variant I	25
3-3	SPIFR Flight Path, Variant II	25
3-4	SPIFR Flight Path, Variant III	25
3-5	SPIFR Flight Path, Variant IV	25
3-6	Ground Station Engagement in the VOR/VOR or the DME/DME Modes	26
3-7	Examples of Application of the Optimal Flight Path Reconstruction Algorithm to the Climbing Turn Pseudo-Flight-Test Data	36
4-1	Knee-Pad Versions of the Performance and Work- load PORs and of the Evaluation Sheet	41
C-1	Data Reduction Procedure	130
D-1	DME Tuning Via NAV/COM	140
D-2	Serial Data Word Format	140
D-3	Bit Format	142
D-4	DME Tuning Electrical Interface	144
D-5	DME - Microprocessor Electrical Interface	146
D-6	DME Interface Block Diagram	147

LIST OF TABLES

<u>No.</u>		<u>Page</u>
2-1	Input Assignments for SPIFR Digital Data Recording System	10
2-2	Output Assignments for SPIFR Digital Data Recording System	11
3-1	Experimental Matrix for First SPIFR Flight-Test Series	21

LIST OF SYMBOLS

<u>Variables</u>	<u>Description</u>
\underline{a}_B	acceleration vector in body axes, "g"
a_x, a_y, a_z	cartesian components of \underline{a}_B , "g"
C	implicit model following gain matrix
F	system dynamics matrix
\underline{f}	nonlinear functions for vehicle equations of motion
G	control effects matrix
g	gravitational acceleration, ft/sec ²
H	observation matrix
	transformation matrix
h	altitude, ft
\underline{h}	nonlinear measurement functions
I	identity matrix
K	Kalman gain matrix
L	transformation matrix
M ()	pitch moment stability-and-control derivative
n ()	random noise associated with the () variable
P	state covariance matrix
p	roll rate, deg/sec
Q	process noise covariance matrix
q	pitch rate, deg/sec
R	measurement noise covariance matrix
r	yaw rate, deg/sec
S	intermediate command output matrix
s	Laplace transform variable
T	duration of flight segment to be reconstructed, sec

t	time, sec
u	x-axis velocity, ft/sec
\underline{u}	control vector
$\underline{V}_{\text{air}}$	airspeed vector, ft/sec
v	y-axis velocity, ft/sec
\underline{v}	measurement noise
w	z-axis velocity, ft/sec
\underline{w}	process noise vector
\underline{W}_I	wind vector in inertial frame, ft/sec
$X()$	(aerodynamic + thrust)-force along the x-axis derivative
x_I	axial position in inertial frame, ft
\underline{x}	state vector
y_I	lateral position in inertial frame, ft
\underline{y}	command vector
$Z()$	(aerodynamic + thrust)-force along the z-axis derivative
z_I	vertical position in inertial frame, ft
\underline{z}	observation vector

Variables (Greek)

α	angle of attack, deg
β	angle of sideslip, deg
δE	elevator deflection, deg
δF	flap deflection, deg
δT	throttle deflection, percent
θ	pitch attitude angle, deg
Σ	summation
Φ	state transition matrix
ϕ	roll attitude angle, deg
ψ	yaw attitude angle, deg
$\tilde{\omega}$	body angular rate skew matrix
$\underline{\omega}$	angular rate vector

Superscripts

B	transformation <u>to</u> body axes
I	transformation <u>to</u> inertial axes

Subscripts

A	kinematic model A
ARA	Avionics Research Aircraft
B	body-axis frame <u>from</u> body axes (with transformation matrix) kinematic model B feedback backward filter
comm	commanded (desired) value
F	feed forward
I	inertial frame <u>from</u> inertial axes (with transformation matrix)
i	navigation station sequencing index
k	sampling instant index
M	model
o	nominal value
q	sensitivity to pitch rate
u	sensitivity to x-axis velocity
w	sensitivity to z-axis velocity
δE	sensitivity to elevator deflection
δF	sensitivity to flap deflection
δT	sensitivity to throttle deflection

Punctuation

($\dot{\quad}$)	derivative of quantity with respect to time
($\underline{\quad}$)	vector quantity
$\delta(\quad)/\delta(\quad)$	partial derivative of one variable with respect to another

$\Delta()$	perturbation variable
$()^*$	steady-state variable
$()^T$	transpose of a vector or matrix
$()^{-1}$	inverse of a matrix
$(\hat{)}$	estimated value of a variable
$()^\#$	pseudoinverse of a matrix
$s()$	$\sin()$
$c()$	$\cos()$

Acronyms

A/D	analog-to-digital
ADF	automatic direction finder
ARA	Avionics Research Aircraft
CDU	control-display unit
CHR	Cooper-Harper Rating
D/A	digital-to-analog
DME	distance measuring equipment
FBW	fly-by-wire
FRL	Flight Research Laboratory
GA	general aviation
GDOP	geometric dilution of precision
IAS	indicated airspeed
IFR	instrument flight rule
I/O	input/output
POR	pilot opinion rating
PROM	programmable read-only memory
RAM	random access memory
SBC	single-board computer
SPIFR	single-pilot instrument flight rule
TAS	true airspeed
VFR	visual flight rule
VOR	very-high-frequency omni-range



1.

INTRODUCTION

1.1 BACKGROUND AND GOALS

This investigation of Single-Pilot Instrument Flight Rule (SPIFR) flying qualities criteria focuses on General Aviation (GA) operations. General Aviation plays an important role in this nation's transportation network (there are about 200,000 active GA aircraft, with the projected number for 1990 being about 300,000), but the difficulty of piloting and the inherent hazards associated with the SPIFR flight regime pose obstacles to continued growth of this mode of transportation (Ref. 1).

An important effect which contributes to an increased hazard for SPIFR operation is the low-frequency dynamic response of a GA aircraft, which does not have to comply with any federal aviation regulation (Ref. 2). As a result, most contemporary GA aircraft have, at best, a marginally stable phugoid mode which may become divergent under wind shear conditions (Ref. 3). This dynamic response problem generally can be coped with under VFR conditions, although it increases pilot's workload significantly. In typical commercial flight, the IFR workload is shared by two pilots; however, GA IFR flight often is controlled by a single pilot. Airframe dynamic deficiencies, finite capabilities of the human operator, and the often limited capabilities of communications and navigation equipment available in typical GA aircraft compound the flight problem under SPIFR conditions.

Prior research has addressed separately various issues, which coupled together, result in this unique flight mission/regime. For example, Ref. 4 and 5 look into the dynamic response

characteristics of GA aircraft, Ref. 6 presents the effect of advanced cockpit controls and displays, and Ref. 7 addresses the pilot workload issue. The SPIFR research initiated by the Flight Research Laboratory (FRL) at Princeton University is an integrated theoretical and flight test program, whose principal objectives are:

- To pursue the trends revealed in previous research,
- To develop new methodologies for analysis of complete SPIFR missions,
- To obtain statistically significant flying qualities criteria for single-pilot instrument flight operations.

1.2 ORGANIZATION OF THE REPORT

Chapter 2 describes the preparation of the ARA for SPIFR mission flights and the onboard experimental setup -- in particular, the hardware and software aspects associated with the data acquisition process. Chapter 3 presents theoretical aspects of the SPIFR research, including modern estimation and control theory algorithms for in-flight simulation and flight path reconstruction. Chapter 4 refers to preliminary flights and to the post-flight data preprocessing procedure verification. Conclusions are contained in Chapter 5. The four appendices contain additional theoretical derivations, program listings for onboard and post-flight processing, description of computer systems employed in this research, and the hardware scheme of the unique DME integration into the SPIFR experimental setup.

2. AIRCRAFT AND DATA ACQUISITION SYSTEM PREPARATION

This chapter describes the preparation of the in-flight simulator and of the onboard digital data acquisition system for SPIFR flight testing. Extensive engineering and technical effort was required for aircraft modifications and rewiring, for new avionics system installation, and for onboard experimental setup integration. The results of this effort are summarized in the following sections.

2.1 AIRCRAFT SYSTEM MODIFICATIONS

The Avionics Research Aircraft (ARA) is a Ryan Navion (N5113K) that has been modified into a fly-by-wire (FBW), variable-stability aircraft (Fig. 2-1). It is capable of simulating a variety of other aircraft using feedback control and command augmentation. The ARA is equipped to measure attitude, angular rates, and linear accelerations in three axes, aerodynamic angles (α , β), airspeed, altitude, and a number of other flight variables. Details of the ARA FBW system can be found in Ref. 8.

The evaluation pilot is to fly a SPIFR mission with the ARA responding as a desired configuration. In an emergency, the safety pilot can override the FBW system and take direct control of the aircraft, (Fig. 2-2).

To be used with the SPIFR program, the ARA had to undergo extensive modifications:

- Design and installation of a modular instrument panel.
- Acquisition and installation of a modern navigation/communication instrument package.
- Addition of secondary workload devices in the cockpit.



Figure 2-1. Avionics Research Aircraft, Navion N5113K.

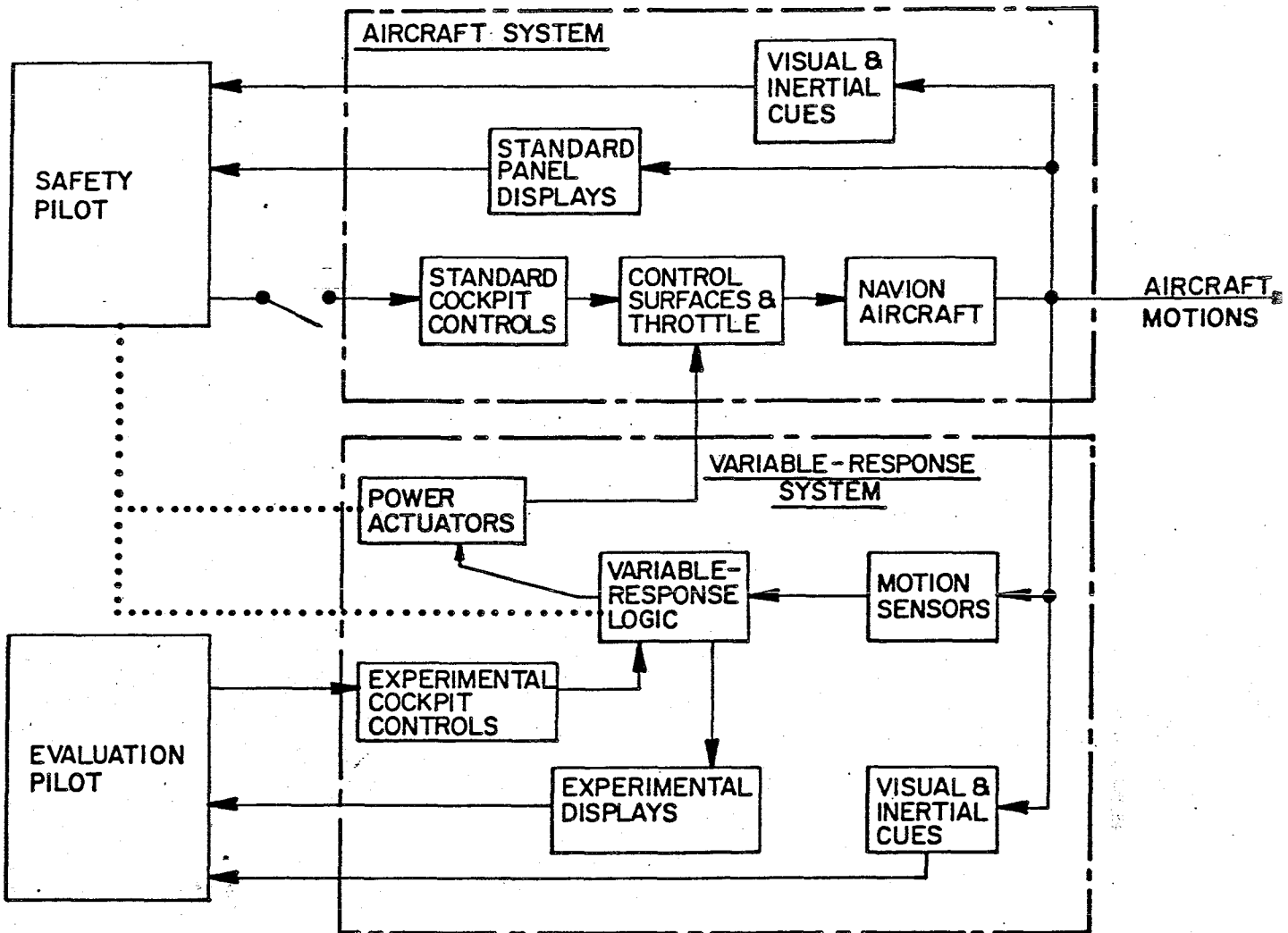


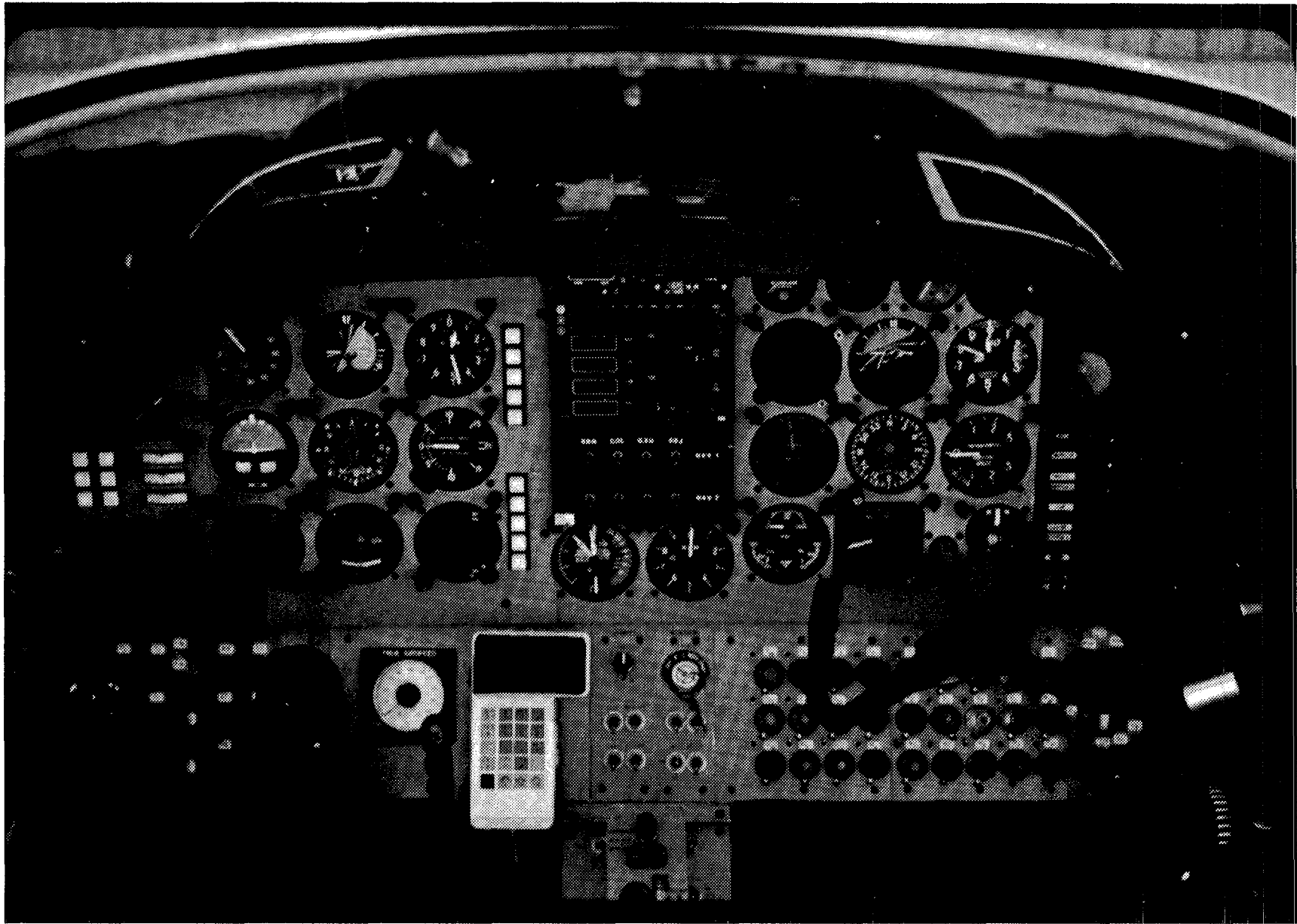
Figure 2-2. Overview of the ARA in-flight Simulator System.

Figure 2-3 illustrates the ARA's modular display panel configuration, with the evaluation pilot's station on the left, the safety pilot's station on the right, and the Bendix BX-2000 navigation/communication stack separating the two. The Distance Measuring Equipment (DME) readout is mounted on a switching panel at the top of the radio stack. The Very-high-frequency Omni-Range (VOR) navigation/communication unit is located under the switching panel. The blank space below this unit is reserved for the Automatic Direction Finder (ADF) and for the transponder.

The DME unit has been integrated into the onboard experimental setup, maintaining the capability to sequence the available navigational stations automatically (through microprocessor control). The importance of this option is discussed in Section 3.5. The technical implementation details are presented in Appendix D.

The safety pilot's panel is a permanent fixture, with conventional instruments and elements for control of the variable-stability system. The latter occupy the right side of the panel and the lower and middle consoles. The evaluation pilot's panel can be removed as a unit to facilitate installation of alternate panels for other investigations. Secondary workload meters, lights, and switches also have been added to the panel.

The secondary workload meters are additional instruments slaved to the onboard microprocessor, which occasionally forces the needles into their "red zones". The evaluation pilot is instructed to keep them "green". Alternately, the pilot can be asked to extinguish lights turned on (pseudorandomly) by the microprocessor program. It is also possible to



7

Figure 2-3. Cockpit Displays of the Avionics Research Aircraft. Modular SPIFR Evaluation Pilot Panel at Left.

simulate typical communications workload by blending audio inputs from a pre-recorded tape with specific instructions radioed from the ground on the flight test frequency.

2.2 INSTRUMENTATION AND DATA RECORDING SYSTEM

The SPIFR digital data acquisition system is illustrated in Fig. 2-4. It is built around the SPIFR microcomputer, which uses the Z-80A central processing unit and the Am9511 mathematics processor in a MultibusTM architecture. As currently configured, the SPIFR microcomputer contains 48K bytes of RAM (random access memory) and 16K bytes of PROM (programmable read-only memory). It accepts 32 analog inputs and produces 6 analog outputs.

The ARA's safety pilot communicates with the SPIFR Microcomputer through a hand-held control/display unit (CDU), the Termiflex HT/4. The pilot is able to start and stop processing or recording through the CDU, change stored numerical values, and so on. Conversely, the CDU can display internally triggered error messages to the safety pilot. The evaluation pilot normally is unaware of the SPIFR Microcomputer's operation, other than through secondary workload stimuli and responses.

Analog and digital inputs and outputs shown in Fig. 2-4 are, for the most part, self-explanatory. Tables 2-1 and 2-2 contain lists of inputs and outputs. The SPIFR Microcomputer obtains its analog inputs from the Digital Avionics Research System (DARE) junction box (J-Box) previously installed in the ARA for another Langley Research Center program. Thus, there is a high degree of "plug compatibility" between the SPIFR and DARE programs.

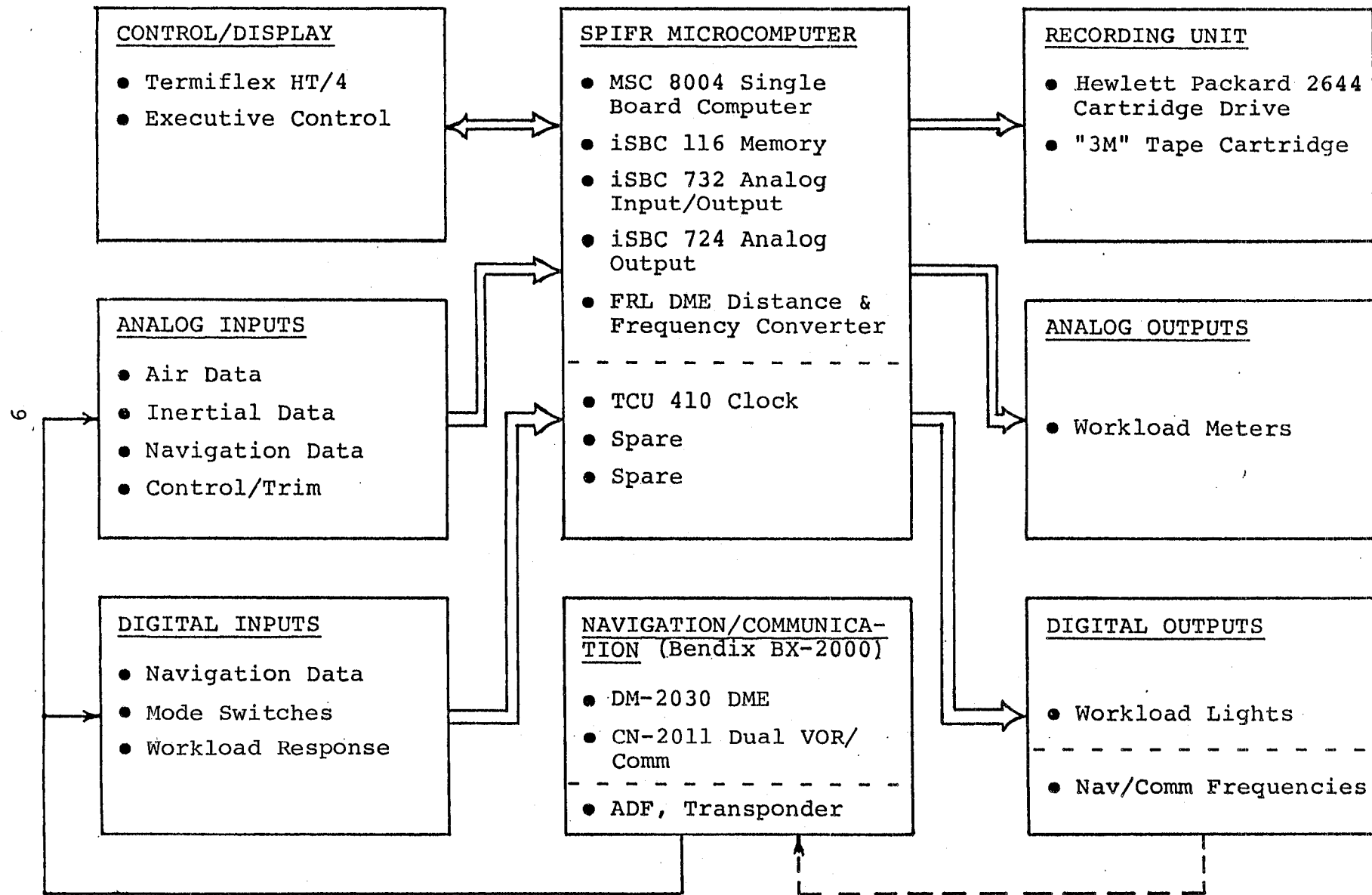


Figure 2-4. SPIFR Digital Data Recording System.

TABLE 2-1
 Input Assignments For
 SPIFR Digital Data Recording System

Analog Inputs

- | | |
|-------------------------|--------------------------------|
| 1. Control Column Angle | 17. Yaw Trim |
| 2. Throttle Setting | 18. Normal Acceleration |
| 3. Flap Command | 19. Axial Acceleration |
| 4. Angle of Attack | 20. Lateral Acceleration |
| 5. Pitch Angle | 21. VOR#1 Azimuth |
| 6. Pitch Rate | 22. VOR#2 Azimuth |
| 7. Airspeed | 23. Glide Slope Elevation |
| 8. Control Wheel Angle | 24. MLS Azimuth |
| 9. Foot Pedals | 25. MLS Elevation |
| 10. Sideslip Angle | 26. Radar Altitude |
| 11. Roll Angle | 27. Barometric Altitude |
| 12. Yaw Angle | 28. Stick Force (3rd Year) |
| 13. Roll Rate | 29. Simulated Turbulence Level |
| 14. Yaw Rate | 30. Landing Gear |
| 15. Pitch Trim | 31. Wind Shear |
| 16. Roll Trim | 32. System Engage |

Digital Inputs

- | | |
|--------------------|-------------------------------------|
| 1. DME Distance | 6. Barometric Altitude |
| 2. VOR#1 Frequency | 7. ADF Bearing |
| 3. VOR#2 Frequency | 8. Variable-Stability System Status |
| 4. DME Frequency | 9. Pilot Mode Switches (8) |
| 5. Time | 10. Avionics System Status (8) |

TABLE 2-2
Output Assignments For
SPIFR Digital Data Recording System

Analog Outputs

- | | |
|--------------------------------|----------|
| 1. Secondary workload meter #1 | 4. Spare |
| 2. Secondary workload meter #2 | 5. Spare |
| 3. Secondary workload meter #3 | 6. Spare |

Digital Outputs

- | | |
|--------------------------|----------------------------------|
| 1. DME tuning | 4. Avionics System status lights |
| 2. DME station indicator | 5. Tape recorder |
| 3. Pilot workload lights | |

A presampling filter (16 Hz break-point frequency) has been introduced for each analog channel to filter out the engine-vibration-induced noise.

Figure 2-4 also illustrates the digital radio tuning feature that will be put to use during the second phase of the project. Error budget analyses conducted during the first phase confirmed the superiority of DME over VOR for position fixing, even at the short ranges to be used in our flight tests. Consequently, it is advantageous to substitute multiple DME measurements for VOR measurements in flight data reduction. The BX-2000 DME unit can acquire and lock on a new station in considerably less than one second; this feature will be used in DME-only "round-robin" position fixing for flight path determination.

The digital tape recording unit is the Hewlett Packard (HP) 2644 terminal, which houses two DC100A magnetic tape cartridge drive units. Its built-in memory enables transition from one cartridge to the other without losing any information. Such a pair of cartridges has a storage capability of about 220K bytes, which is more than enough for a complete SPIFR mission run.

To accommodate the complete experimental setup, a pallet to fit into the ARA-aircraft behind the pilots' seats has been designed and built by the FRL technical staff. It weighs 215 lb. and uses the same mounting brackets as the DARE pallet.

2.3 SOFTWARE DEVELOPMENT

The SPIFR program focuses on the low-frequency dynamic response of the airframe and on navigation-related information,

whose rate of change is low as well. On the other hand, as discussed in Section 3.5, simulated SPIFR flight duration has to be about 30 min, during which all the data channels have to be recorded at least every second. Thus, the main objectives of the onboard software design are to:

- Sample the analog data at a high enough rate to avoid aliasing.
- Compress the high frequency data so that the most significant flight test information can be recorded efficiently with minimal error.
- Trigger preprogrammed sequences of the secondary workload devices (lights, dummy meters).
- Enable the safety pilot to operate the data acquisition system via the hand-held CDU.

The information recorded in flight can be separated into "slow" and "fast" variables. The "slow" variables are principally the positional measurements, which can be sampled once per second with minimal aliasing effect. The "fast" variables -- for example, angular rates and linear accelerations -- are sampled 10 times per second. For the sake of data compaction, they are averaged and recorded once each second. The simple averaging process is analogous to "low-pass" filtering. Thus, low-frequency information is passed with little modification, while high-frequency signals are attenuated.

The HP 2644's recording format uses 16-bit binary words. The SBC 732 A/D board is designed to fill in the 12 left-most bit positions of a 16-bit field, and an appropriate shift is performed to comply with the standard output format. Appendix B contains additional detail with regard to the software aspects of the SPIFR onboard data acquisition system, plus the complete listing of the microprocessor assembly program.

3. THEORETICAL ASPECTS OF EXPERIMENT DESIGN AND FLIGHT PATH RECONSTRUCTION

This chapter starts with the presentation of the 6-DOF dynamic model of aircraft motion, as it is applied in the subsequent sections. Section 3.2 discusses the output command algorithm and its implementation to set up a priority list of aircraft configurations to be simulated in the first SPIFR flight test series. The experimental matrix design, based on statistical reasoning, follows in Section 3.3; the application of the chosen configurations on the ARA-in-flight simulator, via the implicit model following algorithm appears in Section 3.4. SPIFR mission planning (Section 3.5) is based mainly on mathematical-statistical modeling of the en-route navigational errors. Finally, the algorithm for post-flight optimal smoothing and flight path reconstruction is presented in Section 3.6.

3.1 AIRCRAFT DYNAMIC MODEL

The general formulation of a nonlinear dynamic model of a system is:

$$\dot{\underline{x}} = \underline{f}(\underline{x}, \underline{u}) \quad (3-1)$$

where \underline{x} is the state vector and \underline{u} is the control vector. The state vector \underline{x} used here contains three components each of translational rate (u, v, w), translational position (x_I, y_I, z_I), angular rate (p, q, r) and angular attitude (ϕ, θ, ψ). Both body and inertial axis frames are taken right-handed and with z pointing downward. The translational rate equation of the aircraft mathematical model is:

$$\dot{\underline{V}}_{\text{air}} = \underline{a}_B + \tilde{\omega} \underline{V}_{\text{air}} + H_{I-I}^B \underline{g}_I \quad (3-2)$$

The airspeed, expressed in body axes, is:

$$\underline{v}_{\text{air}} = [u \ v \ w]^T \quad (3-3)$$

Acceleration, expressed in body axes, is:

$$\underline{a}_B = [a_x \ a_y \ a_z]^T \quad (3-4)$$

The angular rate cross-product-equivalent matrix $\tilde{\omega}$ is defined as:

$$\tilde{\omega} \triangleq \begin{bmatrix} 0 & r & -q \\ -r & 0 & p \\ q & -p & 0 \end{bmatrix} \quad (3-5)$$

The gravity vector in an assumed local level/local north inertial axis system is:

$$\underline{g}_I \triangleq [0 \ 0 \ g]^T \quad (3-6)$$

The transformation matrix H_I^B from inertial (I) to body (B) axes, with $[\psi \ \theta \ \phi]$ Euler rotations in the specified order, is:

$$H_I^B \triangleq \begin{bmatrix} c\psi c\theta & s\psi c\theta & -s\theta \\ c\psi s\theta s\phi - s\psi c\phi & s\psi s\theta s\phi + c\psi c\phi & c\theta s\phi \\ c\psi s\theta c\phi + s\psi s\phi & s\psi s\theta c\phi - c\psi s\phi & c\theta c\phi \end{bmatrix} \quad (3-7)$$

where

$$\begin{aligned} s(\) &\triangleq \sin(\) \\ c(\) &\triangleq \cos(\) \end{aligned} \quad (3-8)$$

The second equation of the aircraft motion 6-DOF mathematical model describes the transformation of body-axis rates to Euler angle rates, and it is

$$\begin{bmatrix} \dot{\phi} \\ \dot{\theta} \\ \dot{\psi} \end{bmatrix} = L_B^I \begin{bmatrix} p \\ q \\ r \end{bmatrix} \quad (3-9)$$

where

$$L_B^I \triangleq \frac{1}{c\theta} \begin{bmatrix} c\theta & s\theta s\phi & s\theta c\phi \\ 0 & c\theta c\phi & -c\theta s\phi \\ 0 & s\phi & c\phi \end{bmatrix} \quad (3-10)$$

The third aircraft equation combines the effects of airspeed V_{air} and of the wind vector \underline{W}_I (expressed in inertial axes) to compute translational rate:

$$\dot{\underline{x}}_I = H_{B\text{-air}}^I V_{\text{air}} + \underline{W}_I \quad (3-11)$$

where \underline{x}_I is the position vector expressed in inertial axes:

$$\underline{x}_I \triangleq [x_I \ y_I \ z_I]^T \quad (3-12)$$

Based on the orthonormality of H_I^B in eq. (3-7):

$$H_B^I = (H_I^B)^{-1} = (H_I^B)^T \quad (3-13)$$

The following relationships constitute the algebraic part of the model, yielding the output or the measurement models. The airspeed absolute value is:

$$|\underline{V}_{\text{air}}| = (u^2 + v^2 + w^2)^{1/2} \quad (3-14)$$

The angle of attack is given by:

$$\alpha = \tan^{-1} \left(\frac{w}{u} \right) \quad (3-15)$$

The sideslip angle is:

$$\beta = \tan^{-1} \left(\frac{v}{u} \right) \quad (3-16)$$

The definition of the aerodynamic angles with respect to body axes is compatible with the actual measurement mechanization in the ARA.* Assuming that the origin of the inertial frame is at sea level, the altitude h is:

$$h = -z_I \quad (3-17)$$

The acceleration vector \underline{a}_B of eq. (3-2) and (3-4) reflects the effect of aerodynamic and thrust forces, which act on the airframe. For example, the linearized version of eq. (3-1) for the longitudinal case is:

$$\begin{bmatrix} \Delta \dot{u} \\ \Delta \dot{w} \end{bmatrix}_{\underline{a}_B} = \begin{bmatrix} X_u & X_w & X_q \\ Z_u & Z_w & Z_q \end{bmatrix} \begin{bmatrix} \Delta u \\ \Delta w \\ \Delta q \end{bmatrix} + \begin{bmatrix} X_{\delta E} & X_{\delta T} & X_{\delta F} \\ Z_{\delta E} & Z_{\delta T} & Z_{\delta F} \end{bmatrix} \begin{bmatrix} \Delta \delta E \\ \Delta \delta T \\ \Delta \delta F \end{bmatrix} \quad (3-18)$$

The control vector here is:

* The sideslip angle definition differs from the conventional definition, which is:

$$\beta = \sin^{-1} \left(\frac{v}{|\underline{V}_{\text{air}}|} \right)$$

$$\underline{u} = [\Delta\delta E \ \Delta\delta T \ \Delta\delta F]^T \quad (3-19)$$

where δE is the elevator deflection, δT is the throttle travel and δF is the flap deflection.

To complete this illustration of aerodynamic and thrust effects within the context of longitudinal dynamics, the pitch moment (about the center of gravity of the airplane) equation must be introduced:

$$\Delta\dot{q} = M_u \Delta u + M_w \Delta w + M_q \Delta q + M_{\delta E} \Delta\delta E + M_{\delta T} \Delta\delta T + M_{\delta F} \Delta\delta F \quad (3-20)$$

Combining eq. (3-18) with eq. (3-20) and fully accounting for the physical effects reflected in eq. (3-2) to (3-10), we obtain:

$$\begin{bmatrix} \Delta\dot{u} \\ \Delta\dot{w} \\ \Delta\dot{q} \\ \Delta\dot{\theta} \end{bmatrix} = \begin{bmatrix} X_u & X_w & -w+X_q & -gc\theta \\ Z_u & Z_w & u+Z_q & -gs\theta \\ M_u & M_w & M_q & 0 \\ 0 & 0 & 1 & 0 \end{bmatrix} \begin{bmatrix} \Delta u \\ \Delta w \\ \Delta q \\ \Delta \theta \end{bmatrix} + \begin{bmatrix} X_{\delta E} & X_{\delta T} & X_{\delta F} \\ Z_{\delta E} & Z_{\delta T} & Z_{\delta F} \\ M_{\delta E} & M_{\delta T} & M_{\delta F} \\ 0 & 0 & 0 \end{bmatrix} \begin{bmatrix} \Delta\delta E \\ \Delta\delta T \\ \Delta\delta F \end{bmatrix} \quad (3-21)$$

Equation (3-21) is of the form of a state equation:

$$\underline{\Delta\dot{x}} = F \underline{\Delta x} + G \underline{\Delta u} \quad (3-22)$$

where F is the state matrix and G - the control matrix.

3.2 CANDIDATE SPIFR CONFIGURATIONS VIA THE OUTPUT COMMAND ALGORITHM

The basic assumption underlying the following derivation

is that if a configuration requires large state and control variations to retrim from one nominal SPIFR flight equilibrium to another, it may also be problematic for the pilot.* Thus, to pick the candidate configurations for SPIFR in-flight simulation, we first choose initial configuration parameters and flight equilibrium. Then we examine the required variations in state and control variables, which correspond to various retrimming requirements. The retrimming requirement may be formulated in terms of flight path variables, e.g., variation in airspeed ΔV^* or in flight path angle $\Delta \gamma^*$.

The mathematical formulation uses the output command algorithm (Ref. 9). The following output equation is added to the state equation eq. (3-22):

$$\underline{\Delta y} = H_x \underline{\Delta x} + H_u \underline{\Delta u} \quad (3-23)$$

where $\underline{\Delta y}$ represents the required retrimming flight-path variations. An ideal transition to the new flight equilibrium is assumed:

$$\left. \begin{aligned} 0 &= F \underline{\Delta x}^* + G \underline{\Delta u}^* \\ \underline{\Delta y}_{\text{comm}} &= H_x \underline{\Delta x}^* + H_u \underline{\Delta u}^* \end{aligned} \right\} \quad (3-24)$$

where (*) symbolizes the steady-state variations in state and control that correspond to $\underline{\Delta y}_{\text{comm}}$.

As shown in Ref. 9, the solution to eq. (3-24) is:

* As used here, a configuration is a set of aerodynamic coefficients which characterizes the dynamic response of the aircraft.

$$\underline{\Delta x}^* = - F^{-1} G S \underline{\Delta y}_{\text{comm}} \quad (3-25)$$

$$\underline{\Delta u}^* = S \underline{\Delta y}_{\text{comm}} \quad (3-26)$$

where:

$$S \equiv (-H_x F^{-1} G + H_u)^{-1} \quad (3-27)$$

As a result of application of the output command algorithm, variations in the following aerodynamic parameters have received priority in the context of SPIFR flight testing:

- a) X_u , Z_u , Z_α , M_u
- b) $Z_{\delta E}$, $Z_{\delta T}$, $M_{\delta T}$

Stability and control derivatives to be varied in the flight tests fall into two categories: those that affect only trim and those that affect both trim and stability. Control derivatives (list in (b) above) fall into the first category because, as demonstrated by eq. (3-21), they appear in the control matrix G, thus affecting $\underline{\Delta x}^*$ and $\underline{\Delta u}^*$. Stability derivatives (list in (a) above) fall into the second category because they appear in the F matrix, thus affecting both trim and stability.

The ranges of variation of the aerodynamic parameters must reflect the trends in GA aircraft design. These are discussed in the context of the experimental matrix design in the next section.

3.3 EXPERIMENTAL MATRIX DESIGN

The high-priority list of configurations of the previous section has been limited to seven configurations, as we must tradeoff between:

- Number of configurations to be flight-tested.
- Number of replications of SPIFR mission with a given configuration (important for statistical soundness).
- Number of evaluation pilots.

All of this must be done under the constraint of about 25 flight hours.

These tradeoff considerations resulted in the following:

- 15 configurations (nominal ARA and plus/minus variations of each of the 7 coefficients).
- Two test pilots plus one GA pilot.
- Numbers of replications are shown, along with all the other information relevant to the experimental matrix, in Table 3.1. The pluses and the minuses to the right of the numbers of replications describe how many positive and how many negative parameter variations (with respect to nominal) are simulated for each of these numbers.

Parameter to be varied	Test pilot 1	Test pilot 2	GA pilot	Number of mission runs
Nominal	2	2	2	6
X_u	2 ₊	2 ₊	3 ₊₊	7
Z_u	2 ₊	2 ₊	3 ₊₊	7
M_u	2 ₊	2 ₊	3 ₊₊	7
Z_α	2 ₊	2 ₊	3 ₊₊	7
$M_{\delta T}$	2 ₊	2 ₊	3 ₊₊	7
$Z_{\delta E}$	2 ₊	2 ₊	2 ₊	6
$Z_{\delta T}$	2 ₊	2 ₊	2 ₊	6
				Sum = 53

Table 3.1: Experimental Matrix for the First SPIFR Flight Series.

The ranges of the variations in the aerodynamic parameters are intended to reflect possible trends in GA aircraft design. For example, if the design goal is a configuration with a shorter body, an increase in elevator area may be required in order to preserve its moment effectiveness $M_{\delta E}$. Such an area change may affect the vertical force sensitivity of the elevator $\Delta Z_{\delta E} < 0$. On the other hand, introduction of a canard control surface may result in $Z_{\delta E} > 0$. Another example may be of a configuration design that features a high wing for improved cabin visibility and wing-mounted shrouded propellers for increased thrust. As a result M_u and $M_{\delta T}$ may be affected by the variations in the aerodynamic forces and the moment arms.

3.4 IMPLEMENTATION OF SPIFR CONFIGURATIONS VIA IMPLICIT-MODEL-FOLLOWING ALGORITHM

The chosen SPIFR configurations are implemented on the in-flight simulator via the implicit-model-following algorithm (Ref. 10). State equations of the type of eq. (3-21) may be written for the nominal ARA configuration (subscript ARA) and for the configurations to be simulated (subscript M),

$$\frac{\Delta \dot{x}}{\Delta x}_{ARA} = F_{ARA} \frac{\Delta x}{\Delta x}_{ARA} + G_{ARA} \frac{\Delta u}{\Delta u}_{ARA} \quad (3-28)$$

$$\frac{\Delta \dot{x}}{\Delta x}_M = F_M \frac{\Delta x}{\Delta x}_M + G_M \frac{\Delta u}{\Delta u}_M \quad (3-29)$$

Our objective is to obtain the control vector $\frac{\Delta u}{\Delta u}_{ARA}$, which will make the ARA respond as the required configuration. The perfect model following condition is:

$$\dot{\Delta x}_{ARA} = \dot{\Delta x}_M \quad (3-30)$$

Substituting eq. (3-28) and (3-29) into eq. (3-30) and rearranging:

$$\begin{aligned} \Delta u_{ARA} &= G_{ARA}^{\#} [(F_M - F_{ARA}) \Delta x_{ARA} + G_M \Delta u_M] \triangleq \\ &= C_B \Delta x_{ARA} + C_F \Delta u_M \end{aligned} \quad (3-31)$$

where:

$$G_{ARA}^{\#} \triangleq [G_{ARA}^T G_{ARA}]^{-1} G_{ARA}^T \quad (3-32)$$

Eq. (3-30) renders:

$$\Delta x_{ARA} = \Delta x_M \quad (3-33)$$

Thus, Δx_{ARA} is the solution of eq. (3-29). A block diagram of the derived algorithm is presented in Figure 3.1.

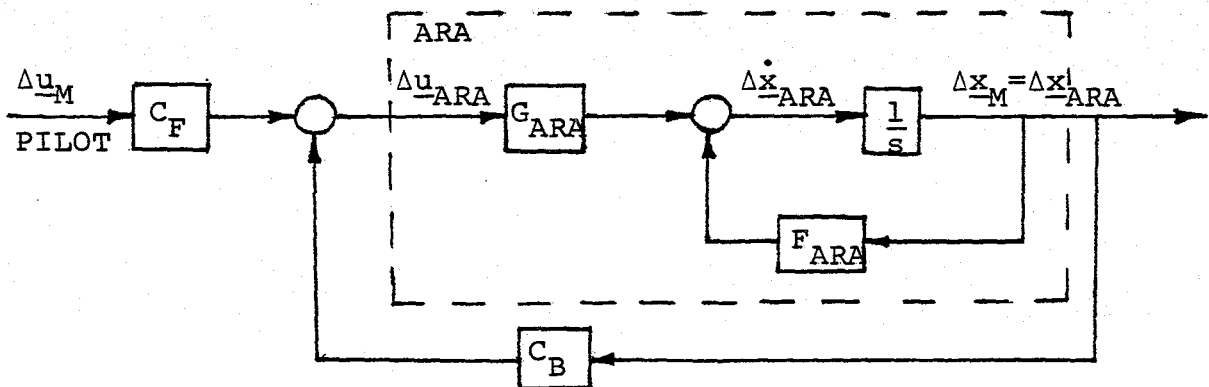


Figure 3.1. Block Diagram for Implementation of a SPIFR Configuration on the ARA In-Flight Simulator.

3.5 EFFECTS OF NAVIGATIONAL ACCURACY AND THE "LEARNING CURVE" EFFECT ON MISSION PLANNING

To simulate realistic SPIFR conditions, the mission has to contain several typical flight-path segments, including

- Climb, acceleration and cruise with airspeed retrimming.
- Holding pattern.
- Deceleration and descent.
- Localizer and glide slope interception.
- Approach and missed-approach go-around.

Also, a realistic VOR-radial navigation should consist of at least once switching navigational stations in the "TO"-mode and of a leg in the "FROM"-mode. The above considerations roughly size the SPIFR mission simulation to a minimum flight duration of about 30 minutes and the geometry shown in Fig. 3-2.

One problem associated with deciding the flight path geometry is the "learning curve" effect. The "learning curve" is the ability of a human being to improve his performance by taking advantage of past experience. Flying all missions along the same trajectory invokes memorization by the pilot, reducing the navigation workload to a level unrealistic for a SPIFR-type mission. To cope with this issue, additional flight path variants have been devised (Fig. 3-3, 3-4, 3-5). All variants are of comparable structure and flight duration.

The other problem associated with the decision of flight path geometry is navigational accuracy. Conclusions of the following discussion with regard to this issue have been implemented with the SPIFR missions of figures 3-2 to 3-5 and, as will be shown, they also contribute to post-flight flight-path reconstruction accuracy improvement.

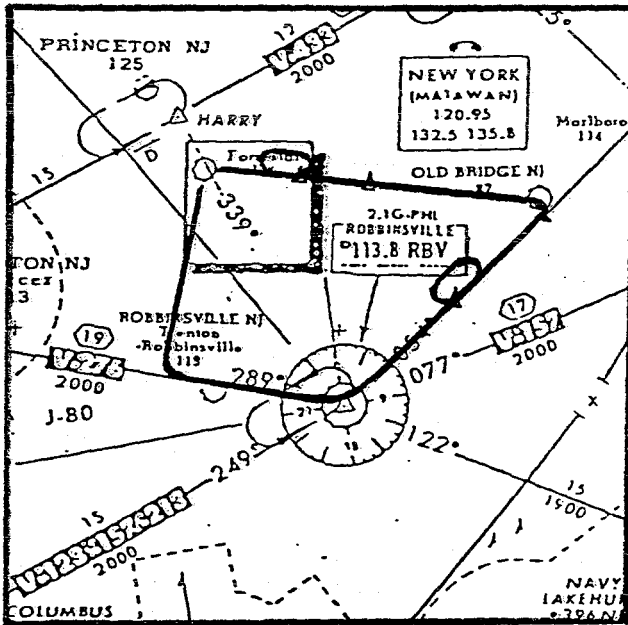


Figure 3-2. Variant I.

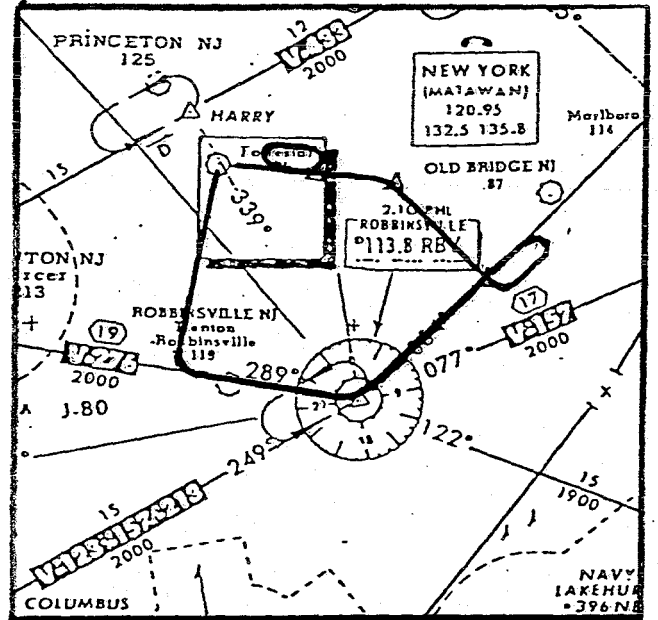


Figure 3-3. Variant II.

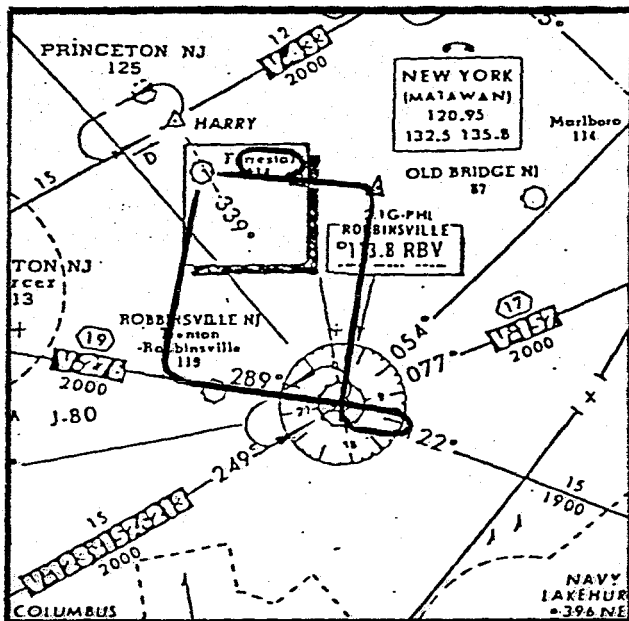


Figure 3-4. Variant III.

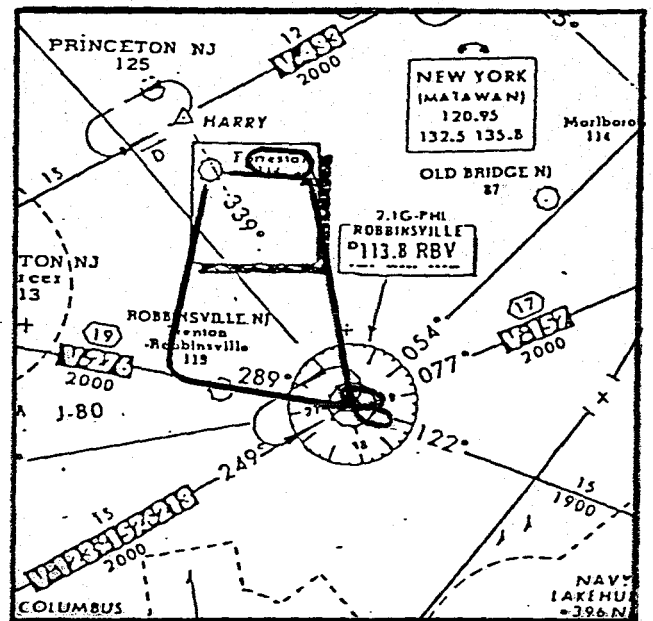


Figure 3-5. Variant IV.

Figures 3-2 to 3-5. SPIFR Flight Path Variants.

The standard navigational modes for GA are VOR/VOR, VOR/DME and DME/DME. At least two navigation stations are required to achieve a horizontal "fix" of the aircraft's position. With proper geometry any of these combinations can provide a fix; however the accuracy of the fix is subject to several factors. The accuracy requirements have been imposed by the Federal Aviation Administration (FAA), and their numerical values appear in Ref. 11.

$$\left. \begin{aligned} \sigma_{\psi} &\equiv \sigma_{\text{VOR}} = 1.9^{\circ} \\ \sigma_{\text{R}} &= \sigma_{\text{DME}} = .15\% \text{ range or } .1 \text{ mile:} \\ &\quad \text{whichever is larger} \end{aligned} \right\} \quad (3-34)$$

These navigational errors are with respect to a single ground station. The position errors associated with a navigational mode have to be computed accounting for the Geometric Dilution of Precision (GDOP) effect. GDOP is an inaccuracy due to the nonperpendicularity of the lines connecting the aircraft with the engaged stations.

Applying analytical geometry to the typical situation depicted in Fig. 3-6 and assuming that the two navigational-

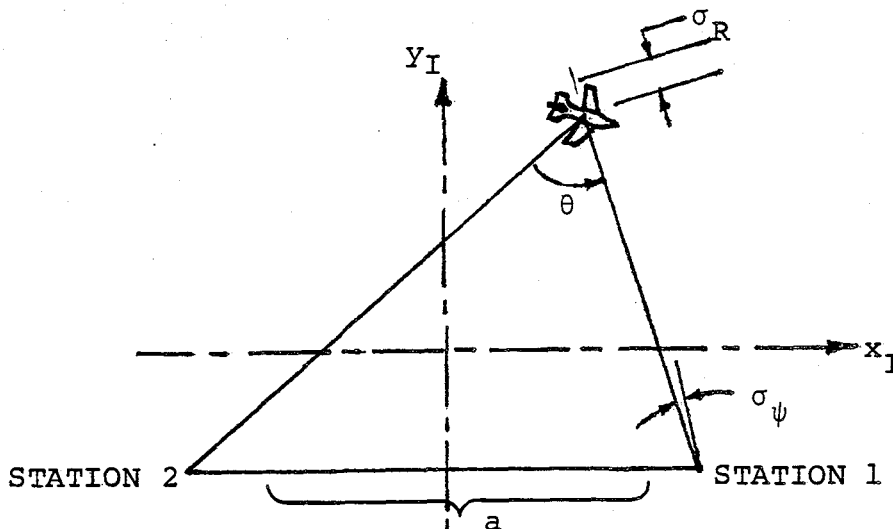


Figure 3-6. Ground Stations Engagement in the VOR/VOR or the DME/DME Modes.

stations' errors are statistically uncorrelated, we obtain:

$$\sigma = (1/s\theta) [\sigma_1^2 + \sigma_2^2]^{1/2} \quad (3-35)$$

The $1/s\theta$ term reflects the GDOP effect. For angles between radials in the vicinity of $\theta = 0^\circ$ or $\theta = 180^\circ$, the position error becomes very large, becoming infinite in the limit. To improve position accuracy using two similar ground stations while flying a given leg, it is desirable that the stations be as nearly perpendicular as possible. For VOR/VOR, eq. (3-35) can be rewritten as,

$$\sigma = \frac{a\sigma_\psi}{\sqrt{2} s^2\theta} (1+s^2\theta)^{1/2} \quad (3-36)$$

For DME/DME, eq. (3-35) becomes

$$\sigma = \sqrt{2} \sigma_R/s\theta \quad (3-37)$$

Numerical values of eq. (3-34) and dependence of $\sigma_{\text{VOR/VOR}}$ on the $\sin^2\theta$ suggest that this navigational mode is much less accurate than the DME/DME mode. For example, at a range of 50 miles from both stations and for $\theta = 30^\circ$ the VOR/VOR error is 2.71 miles, while the DME/DME error is 0.28 miles and the results favour the DME/DME pairing at greater ranges. Based on this observation and on the feasibility of microprocessor-controlled sequential engagements of several DME stations, this technique will be employed to improve the flight path reconstruction accuracy. In particular, this accuracy improvement may be achieved by making use of redundant measurements, while applying the optimal Kalman filtering/smoothing algorithm.

3.6 OPTIMAL SMOOTHING OF FLIGHT-TEST RECORDS AND FLIGHT-PATH RECONSTRUCTION

One way to smooth flight test records is to pass the data through a filter, which chops off the high frequency content of the recorded information. A better way is to account for the particular system's dynamic characteristics. This can be done applying the extended Kalman filter algorithm.

For post-flight analysis, even higher accuracy may be achieved by accounting for the "future" information. This improvement is obtained by using an optimal smoothing algorithm. An additional advantage of this algorithm is that it estimates flight path variables that have not been measured directly. Thus, smoothing and flight path reconstruction are obtained via a single algorithm implementation (as in Ref. 12, 13). For this application we need the system state eq. (3-1), which constitutes a concise representation of eq. (3-2) to (3-13),

$$\dot{\underline{x}} = \underline{f}(\underline{x}, \underline{u}) + \underline{w} \quad (3-38)$$

and the measurement equation,

$$\underline{z} = \underline{h}(\underline{x}, \underline{u}) + \underline{v} \quad (3-39)$$

which stands for relationships of the type of eq. (3-14) to (3-17). Equation (3-38) differs from eq. (3-1) by the additional term \underline{w} , which is referred to in the literature as "process noise". The vector \underline{v} in eq. (3-39) is the "measurement noise".

Equations (3-18) to (3-31) need not be used in the post-flight optimal smoothing and flight-path reconstruction because the accelerations \underline{a}_B are measured directly. Equations (3-2) to (3-17) constitute a kinematic model, as they do not reflect the dynamic mechanism by which \underline{a}_B is actually produced.

The differential equations of the kinematic model (3-2), (3-9) and (3-11) constitute the "state model" and the algebraic relationships (3-14) to (3-17) the "measurement model". Even without accounting for the \underline{a}_B -producing-mechanism, the kinematic model is nonlinear and high-dimensional. Thus, it is more efficient to tackle it in two steps. This is made possible by the fact that the SPIFR experimental setup records both $[p \ q \ r]^T$ and $[\phi \ \theta \ \psi]^T$. The first step is to smooth these six measurements. Treating all six as state variables and using eq. (3-9) we may write:

$$\text{STATE MODEL A} \left\{ \begin{array}{l} \dot{p} = n_p \\ \dot{q} = n_q \\ \dot{r} = n_r \\ \dot{\phi} = p + \tan \theta (s\phi * q + c\phi * r) \\ \dot{\theta} = c\phi * q - s\phi * r \\ \dot{\psi} = \frac{1}{c\theta} (s\phi * q + c\phi * r) \end{array} \right. \quad (3-40)$$

$$\text{MEASUREMENT MODEL A} \left\{ \begin{array}{l} \underline{z}_A = H_A \underline{x}_A + \underline{v}_A \end{array} \right. \quad (3-41)$$

The state vector for model A is:

$$\underline{x}_A = [p \ q \ r \ \phi \ \theta \ \psi]^T \quad (3-42)$$

The process noise vector (with n_p , n_q and n_r random and unknown angular acceleration inputs) is:

$$\underline{w}_A = [n_p \ n_q \ n_r \ 0 \ 0 \ 0]^T \quad (3-43)$$

The measurement noise vector for model A is:

$$\underline{v}_A = [n_p \ n_q \ n_r \ n_\phi \ n_\theta \ n_\psi]^T \quad (3-44)$$

The measurement vector \underline{z}_A in (3-41) contains the measured values of \underline{x}_A . Thus, the observation matrix H_A is an identity matrix.

Before elaborating on the optimal smoother algorithm implementation based on eq. (3-40) and (3-41), the kinematic model for the second step is now derived. We assume that the time histories,

$$\hat{p}(t), \hat{q}(t), \hat{r}(t); \hat{\phi}(t), \hat{\theta}(t), \hat{\psi}(t) \quad (3-45)$$

and the associated matrices,

$$\hat{H}_B^I(t) \ , \ \hat{H}_I^B(t) \ , \ \hat{\omega}(t) \quad (3-46)$$

are given, having completed the first step. The 6-component state vector for the next step is,

$$\underline{x}_B = [x_I \ y_I \ z_I \ u \ v \ w]^T \quad (3-47)$$

and the 6-component input vector is,

$$\underline{u}_B = [w_{x_I} \ w_{y_I} \ w_{z_I} \ (a_x - s\hat{\theta}g) \ (a_y + c\hat{\theta}s\hat{\phi}g) \ (a_x + c\hat{\theta}c\hat{\phi}g)]^T \quad (3-48)$$

The input vector contains components of the true wind and accelerations, \underline{w}_I and \underline{a}_B . In this context, the actual values of these measured variables are interpreted as inputs and their measurement inaccuracies as process noise*:

* Appendix A presents an improved wind model.

$$\underline{w}_B = [0 \ 0 \ 0 \ n_{a_x} \ n_{a_y} \ n_{a_z}]^T \quad (3-49)$$

Unlike the first step, in which the \underline{x}_A components have been smoothed optimally, this step reconstructs the \underline{x}_B components with eq. (3-2) and (3-11) constituting the state model B:

$$\text{STATE MODEL B} \left\{ \begin{array}{l} \begin{bmatrix} \dot{x}_I \\ \dot{y}_I \\ \dot{z}_I \end{bmatrix} = \hat{H}_B^I(t) \begin{bmatrix} u \\ v \\ w \end{bmatrix} + \begin{bmatrix} w_{x_I} \\ w_{y_I} \\ w_{z_I} \end{bmatrix} \\ \begin{bmatrix} \dot{u} \\ \dot{v} \\ \dot{w} \end{bmatrix} = \hat{\omega}(t) \begin{bmatrix} u \\ v \\ w \end{bmatrix} + \begin{bmatrix} a_x - s\hat{\theta}g \\ a_y + c\hat{\theta}s\hat{\phi}g \\ a_z + c\hat{\theta}c\hat{\phi}g \end{bmatrix} + \begin{bmatrix} n_{a_x} \\ n_{a_y} \\ n_{a_z} \end{bmatrix} \end{array} \right. \quad (3-50)$$

Equations (3-14) to (3-17) plus VOR and DME measurement equations constitute the measurement model B:

$$\text{MEASUREMENT MODEL B} \left\{ \begin{array}{l} |\underline{v}_{air}| = (u^2 + v^2 + w^2)^{1/2} + n_v \\ \alpha = \tan^{-1} \left(\frac{w}{u} \right) + n_\alpha \\ \beta = \tan^{-1} \left(\frac{v}{u} \right) + n_\beta \\ h = -z_I + n_h \\ r_{DME_{si}} = [(x_I - x_{si})^2 + (y_I - y_{si})^2 + (z_I - z_{si})^2]^{1/2} + n_{DME} \\ \theta_{VOR_{si}} = \tan^{-1} [(y_I - y_{si}) / (x_I - x_{si})] + n_{VOR} \end{array} \right. \quad (3-51)$$

where s_i symbolizes the distance $r_{DME_{s_i}}$ or angle $\theta_{VOR_{s_i}}$ being measured with respect to navigational station i . The measurement noise vector is:

$$\underline{v}_B = [n_v \ n_\alpha \ n_\beta \ n_h \ n_{DME_1} \ n_{DME_2} \ \dots \ n_{VOR_1} \ n_{VOR_2} \ \dots]^T \quad (3-52)$$

Estimates of measurement biases and scale factor errors may be obtained at the expense of significant increase in state vector dimension. Such an increase in dimension may affect not only the computing cost but also the computational accuracy.

Examination of eq. (3-40) to (3-51) shows that both models A and B are nonlinear. Thus the extended Kalman smoother algorithm has to be applied (Ref. 14). This algorithm is implemented as a combination of forward- and backward-running Kalman filters. The extended Kalman filter algorithm constitutes an adaptation of the linear Kalman filter theory to nonlinear situations. It propagates the nonlinear dynamic model between measurements and utilizes a locally linearized model for the measurement updates.

The following is the discrete formulation of the extended Kalman smoother algorithm, applied to the dynamic model of the system, which constitutes of the state model (eq. (3-38)) and measurement model (eq. (3-39)). The propagation of the estimated states $\hat{\underline{x}}$ and of the state covariance matrix P between measurements, for forward filtering uses

$$\hat{\underline{x}}(t) = \underline{f}[\hat{\underline{x}}(t), \underline{u}(t)] \quad (3-53)$$

$$P_k(-) = \phi_{k-1} P_{k-1}(+) \phi_{k-1}^T + Q_{k-1} \quad (3-54)$$

where Q is the process noise covariance matrix and ϕ is the transition matrix obtained after local linearization of eq. (3-38) into:

$$\dot{\underline{x}} = F\underline{x} + G\underline{u} + L\underline{w} \quad (3-55)$$

In order not to create inaccuracies due to numerical differentiation, analytical derivation of the Jacobian matrices (F , G and L) has been carried out for both models A and B; this is documented in Appendix A. The Kalman gain matrix for forward filtering is,

$$K_k = P_k(-) H_k^T [H_k P_k(-) H_k^T + R_k]^{-1} \quad (3-56)$$

where R is the measurement noise covariance matrix and H is obtained by local linearization of eq. (3-39) as

$$\underline{z}_k = H_k \underline{x} + \underline{v}_k \quad (3-57)$$

State and covariance updates account for measurements as

$$\hat{\underline{x}}_k(+) = \hat{\underline{x}}_k(t) + K_k [\underline{z}_k - \underline{h}_k(\hat{\underline{x}}_k(t))] \quad (3-58)$$

$$P_k(+) = [I - K_k H_k] P_k(-) \quad (3-59)$$

where $\hat{\underline{x}}_k(t)$ is obtained by integration of eq. (3-53) from t_{k-1} to t_k .

The filter processing of the raw data renders the state estimates before the measurement update $\hat{\underline{x}}_k(-) \equiv \hat{\underline{x}}(t)$ and after the measurement update $\hat{\underline{x}}_k(+)$ and the associated covariance matrices $P_k(-)$ and $P_k(+)$. The smoother algorithm uses this information as input and running backwards in time produces the improved estimates of the states $\hat{\underline{x}}_{k/n}$ and of the covariance matrix $P_{k/n}$. The first step is the computation of the state matrix F_k :

$$F_k = f[\hat{\underline{x}}_k(+)] \quad (3-60)$$

The state matrix is used to calculate the state transition matrix Φ_k . The state transition matrix and the input covariance matrices render matrix A_k :

$$A_k = P_k(+)\Phi_k^T P_{k+1}^{-1}(-) \quad (3-61)$$

Using the input state estimates $\hat{\underline{x}}_k(-)$ and $\hat{\underline{x}}_k(+)$ and the associated covariance matrices $P_k(+)$ and $P_k(-)$ along with A_k , the smoothed and reconstructed states $\hat{\underline{x}}_{k/n}$ are obtained:

$$\hat{\underline{x}}_{k/n} = \hat{\underline{x}}_k(+) + A_k [\hat{\underline{x}}_{k+1/n} - \hat{\underline{x}}_{k+1}(-)] \quad (3-62)$$

$$P_{k/n} = P_k(+) + A_k [P_{k+1/n} - P_{k+1}(-)]A_k^T \quad (3-63)$$

This complete optimal estimation algorithm, which performs post-flight data smoothing and flight-path reconstruction has been coded in FORTRAN (Appendix B) and verified by application to a computer-generated SPIFR trajectory.

Examples of the optimal flight path reconstruction algorithm's application to the generic flight-test data records are given in Fig. 3-7 for a coordinated climbing turn flight segment of 60 seconds. Figure 3-7a) to f) present reconstructed measurements demonstrating both state variable reconstruction and improvement with respect to data corrupted by noise. The symbol convention used in these figures is: (+) for nominal, (□) for corrupted, (∇) for filtered and (Δ) for smoothed time histories. Line segments are used to link results but they do not suggest a functional relationship.

Figures 3-7a) and b) represent the optimal smoothing of the angular states. As may have been expected, the "derivative" states (e.g., Fig. 3-7b) are noisier than the "integral" states (e.g., Fig. 3-7a). In a sense, this distinction is applicable to the airspeed versus aerodynamic angle measurements, which reflect the atmospheric turbulence effect. As follows from the translational submodel formulation, to reconstruct these measurements (e.g., Fig. 3-7c) and d)), the states u , v and w are first estimated. The typical lag introduced by filtering is more apparent in some of the figures; it is then reduced by the smoother. The trajectory reconstruction is represented in Fig. 3-7e), f) and g). Note that optimal smoothing improves the filtered state estimates and also shrinks the position uncertainty ellipsoid.

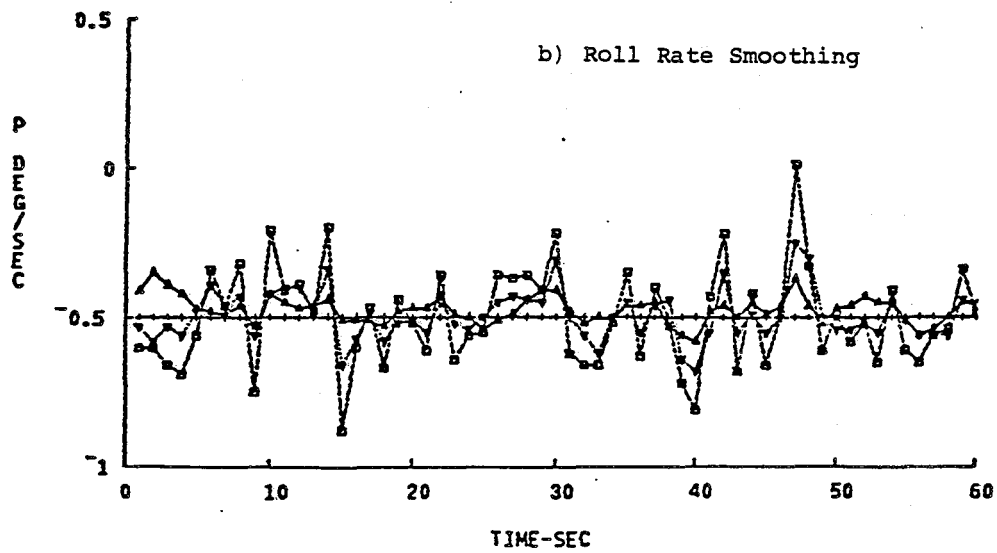
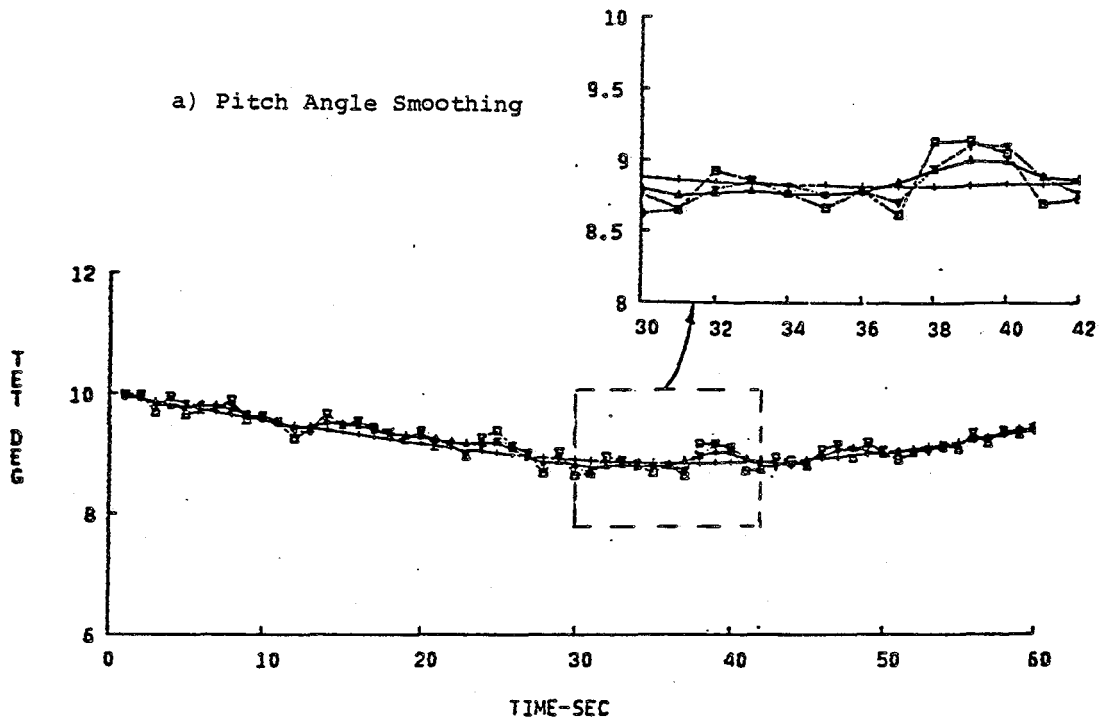


Figure 3-7: Examples of application of the optimal flight path reconstruction algorithm to the climbing turn pseudo-flight-test data.

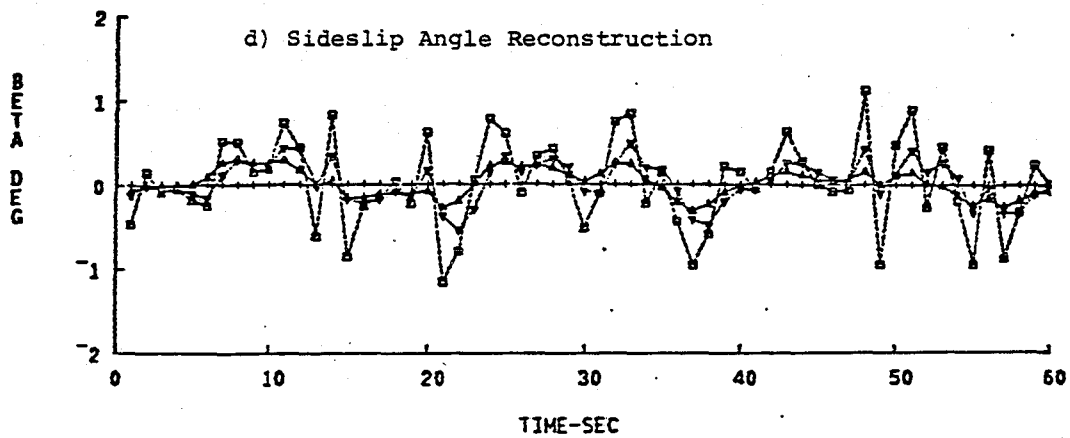
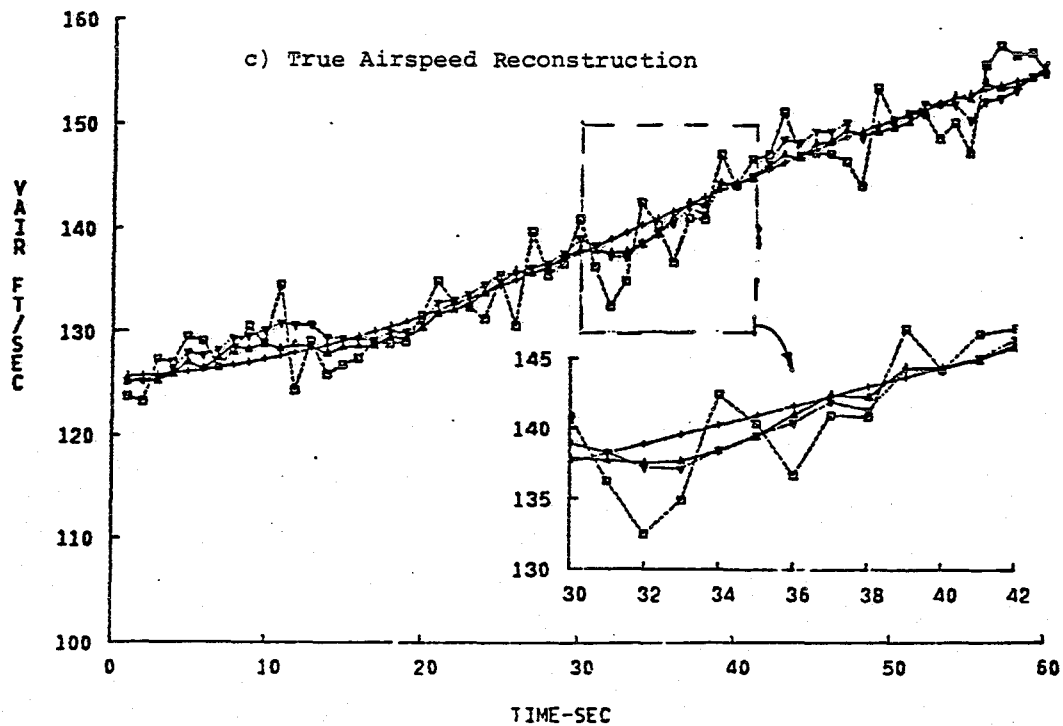


Figure 3-7: Examples of application of the optimal flight path reconstruction algorithm to the climbing turn pseudo-flight-test data.

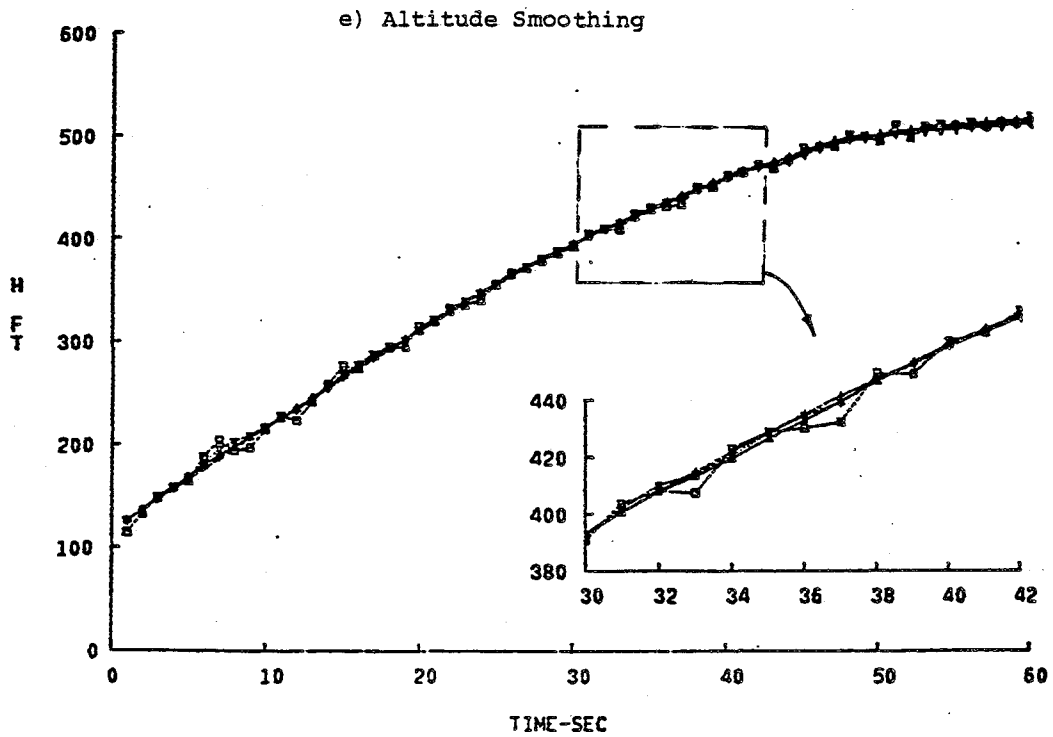


Figure 3-7: Examples of application of the optimal flight path reconstruction algorithm to the climbing turn pseudo-flight-test data.

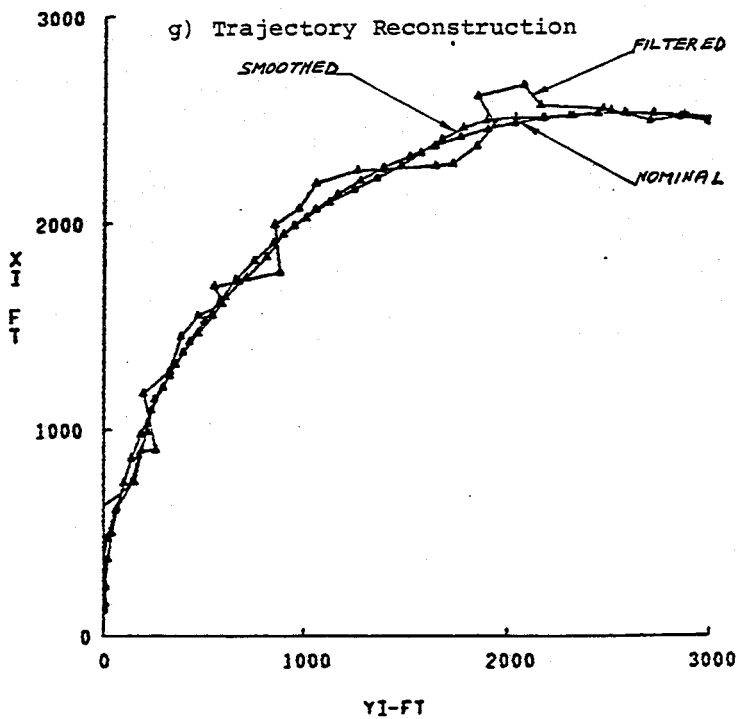
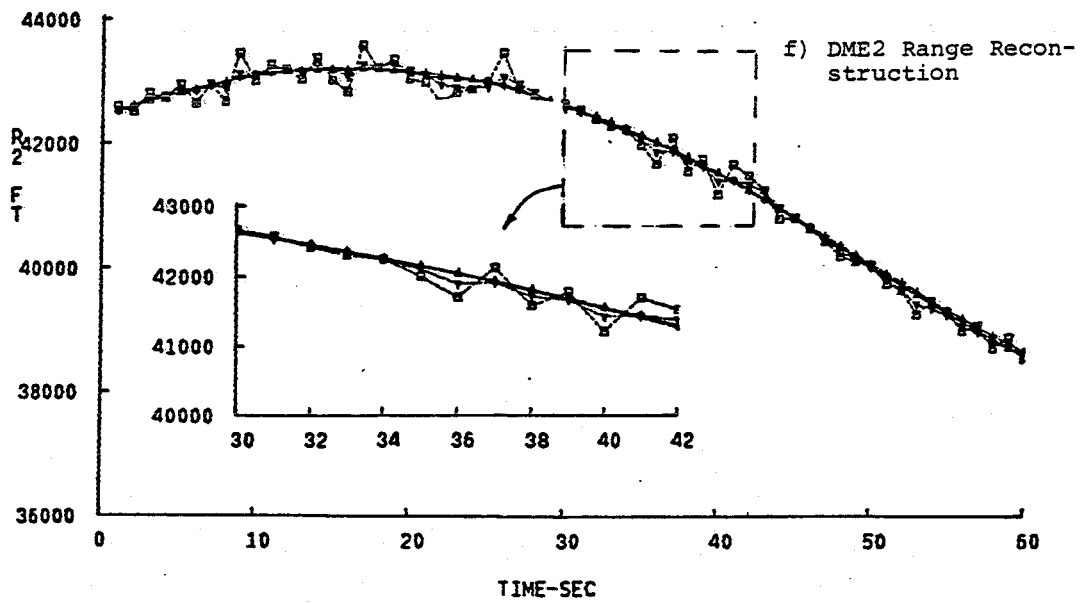


Figure 3-7: Examples of application of the optimal flight path reconstruction algorithm to the climbing turn pseudo-flight-test data.

4.

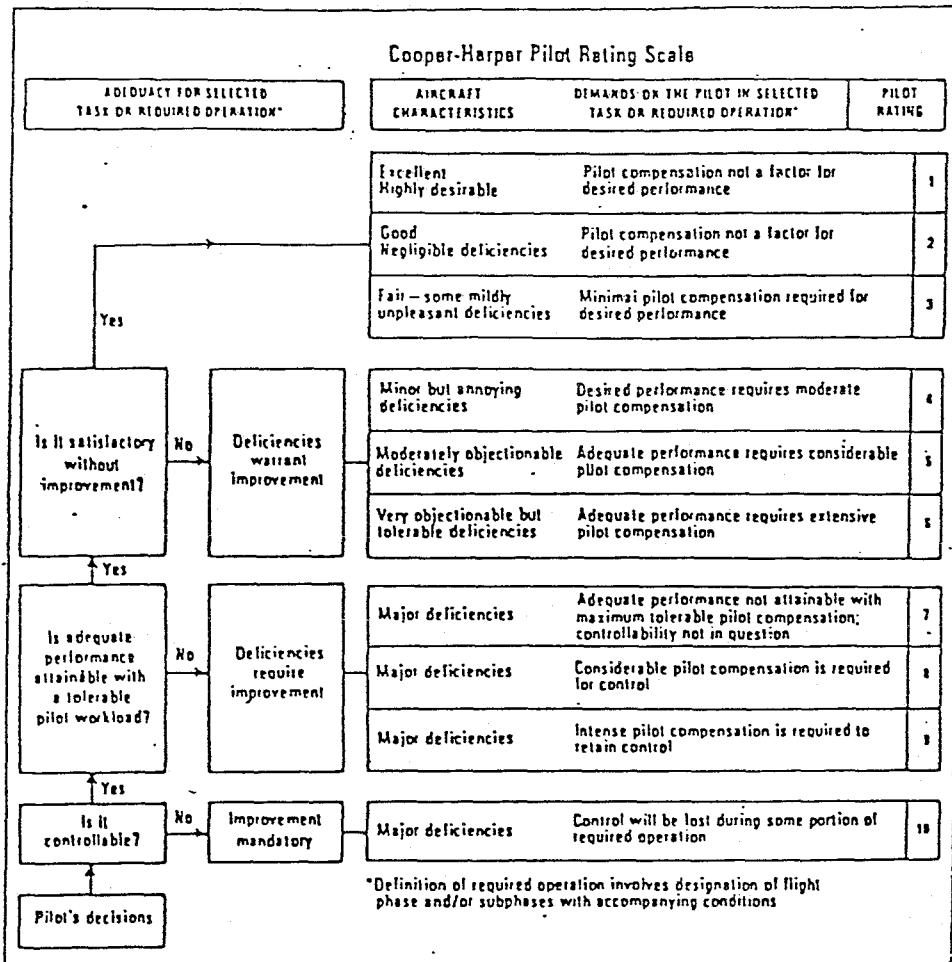
PRELIMINARY FLIGHTS

Flight test results are the important objectives of the SPIFR program. As the human operator is an integral part of the control and guidance loop, Pilot Opinion Ratings (POR) constitute important experimental results. Both the Cooper-Harper Rating (CHR), which is a performance rating (Ref. 15) and the workload rating (M.I.T. scale, Ref. 15) are significant. As we debrief the evaluation pilot with regard to both the complete mission and to its specific segments, knee-pad-size versions of both scales and of the grading sheet have been prepared (Fig. 4-1).

To test the complete SPIFR-mission-simulation concept, a series of preliminary flights has been carried out. Its main objectives were to verify the realism of simulation of SPIFR regime environment, the in-flight configuration matching capability and the data acquisition and reduction process.

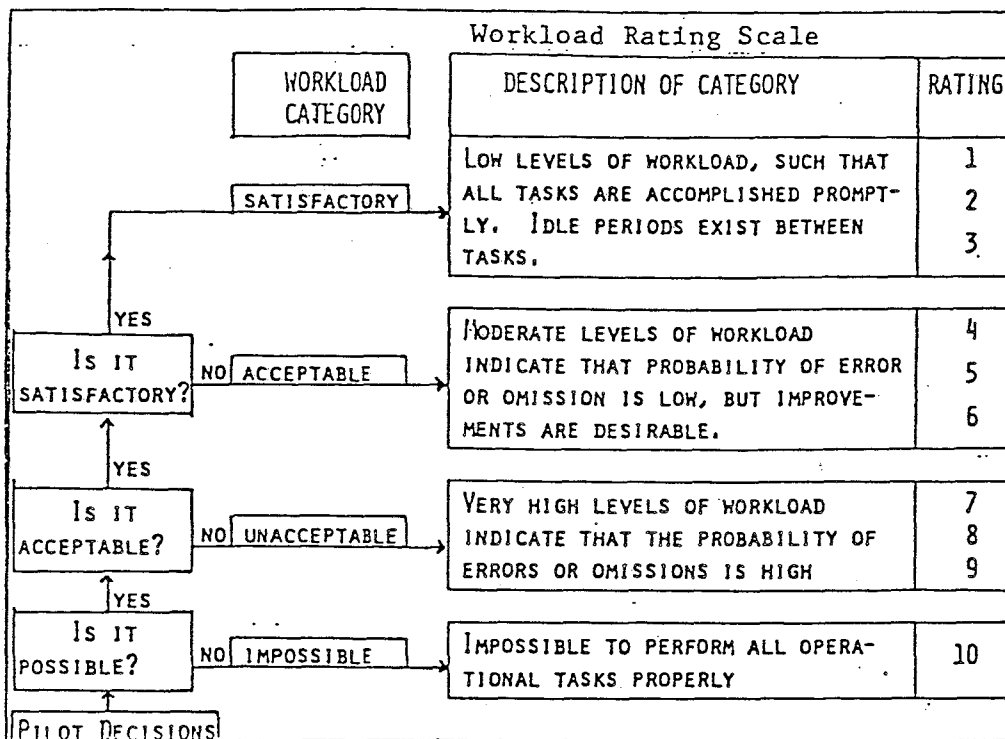
After extensive hangar checks of the aircraft system modifications, of the new navigation/communication package and of the onboard experimental setup, the proposed instrument tracks (Fig. 3-2 to 3-5) were flown - totalling to about 10 flight hours.

These preliminary flights have shown that the tasks appear to simulate SPIFR missions, which are realistic in both geometry and workload. Using the knee-pad-size POR scales and grading sheet the in-flight debriefing can be carried out without interfering with the mission. The in-flight configuration matching capability with regard to each



a) Performance POR Scale

Figure 4-1: Knee-pad Versions of the Performance and Workload PORs and of the Evaluation Sheet.



b) Workload POR Scale

Figure 4-1: Knee-pad Versions of the Performance and Workload PORs and of the Evaluation Sheet.

EVALUATION SHEET

MISSION VARIANT #

CONFIGURATION #

PILOT

DATE

SPEED RETRIMMING

CHR

WORKLOAD

COMMENTS

HOLDING PATTERN

CHR

WORKLOAD

COMMENTS

GLIDE SLOPE TRACKING

CHR

WORKLOAD

COMMENTS

OVERALL MISSION

CHR

WORKLOAD

COMMENTS

c) Evaluation Sheet.

Figure 4-1: Knee-pad Versions of the
(cont.) Performance and Workload
PORs and of the Evaluation
Sheet.

of the priority configurations has been confirmed. The data collection and reduction process has been verified by comparison of timings and directions of deflection of various controls reported by the safety pilot to those obtained by recorded data processing.

5.

CONCLUSION

This report summarizes the first phase of the SPIFR project, which constitutes an integrated theoretical and flight-test research effort, which addresses stability-and-control, avionics and human factor effects in single pilot IFR situations. The first phase activities were aimed at basic research system preparation and, consequently, at conducting the first flight test series of the SPIFR four-year program.

Most of the goals of the first phase of the SPIFR program have been achieved. The basic research system has been put together and successfully flight-tested, including the ARA aircraft modifications and the onboard digital data acquisition system. A modern navigation/communication system has been installed, and a new instrument panel has been designed to accommodate flexibility in introduction of additional instrumentation and workload devices. The data collection system has been built around the Z-80 microprocessor. The microprocessor performs the analog channels sampling, preliminary processing and transfer of the data records to the digital recorder. The software required for these onboard manipulations has been developed, debugged and flight-tested. In parallel, the post-flight data preprocessing software and procedure development has been completed and tried out with actual in-flight recorded data. Mission planning and experimental matrix design have been carried out accounting for navigational accuracy and the "learning curve effect" and for the amount-of-flight-hours-constraint. Applying theoretical algorithms the aerodynamic configurations for the

SPIFR program have been obtained and implemented on the ARA aircraft. A preliminary flight-test series has been conducted to check whether realistic SPIFR conditions are obtained and to verify the in-flight configurations matching. These flight tests have confirmed that the SPIFR mission simulation is realistic both in geometry and in workload.

During the second phase of the SPIFR project, the first flight series will be completed and the collected data will be analysed, including the subjective PORs. Finally, statistical regression analysis will be applied to render flying qualities criteria for Single Pilot Instrument Flight Rule operations.

The structure of the research program as summarized in this report will render quantitative criteria with regard to the effects of airframe dynamic response, workload level, and pilot experience on the SPIFR flight regime. Furthermore, the ARA is now ready to conduct a broad range of additional flight experiments associated with single-pilot instrument flight.

APPENDIX A

DERIVATION OF THE LINEARIZED VERSIONS OF THE SIMPLIFIED AND THE IMPROVED KINEMATIC MODELS

A.1 IMPROVED WIND MODEL

The kinematic state model B (eq.(3-50)) assumes that ideal, constant wind measurements \underline{w}_I are available along the flight path. Although we may disregard the high-frequency turbulence disturbances, it is difficult to obtain wind measurements along a flight path with an acceptable degree of reliability. A solution is to adjoin a wind model to state model B, estimating its parameters along with \underline{x}_B . A reasonable low-frequency wind model may constitute of a constant component and a linear variation with altitude,

$$\underline{w}_I(h) = \underline{w}_{I_0} + \frac{\partial \underline{w}_I}{\partial z_I} (z_I - z_{I_0}) \quad (A-1)$$

where \underline{w}_{I_0} is a constant wind vector at reference altitude $-z_{I_0}$ and $\frac{\partial \underline{w}_I}{\partial z_I}$ is a vector of slope of wind variation with altitude. Adjoining eq. (A-1) to eq. (3-50), we obtain:

$$\begin{bmatrix} \dot{x}_I \\ \dot{y}_I \\ \dot{z}_I \end{bmatrix} = \hat{H}_B^I(t) \begin{bmatrix} u \\ v \\ w \end{bmatrix} + \begin{bmatrix} w_{x_{I_0}} + \frac{\partial w_{x_I}}{\partial z_I} (z_I - z_{I_0}) \\ w_{y_{I_0}} + \frac{\partial w_{y_I}}{\partial z_I} (z_I - z_{I_0}) \\ w_{z_{I_0}} + \frac{\partial w_{z_I}}{\partial z_I} (z_I - z_{I_0}) \end{bmatrix} \quad (A-2)$$

$$\begin{bmatrix} \dot{u} \\ \dot{v} \\ \dot{w} \end{bmatrix} = \hat{\omega}(t) \begin{bmatrix} u \\ v \\ w \end{bmatrix} + \begin{bmatrix} a_x - s\hat{\theta}g \\ a_y + c\hat{\theta}s\hat{\phi}g \\ a_z + c\hat{\theta}c\hat{\phi}g \end{bmatrix} + \begin{bmatrix} n_{a_x} \\ n_{a_y} \\ n_{a_z} \end{bmatrix} + \hat{H}_I^B(t) * \frac{\partial w_I}{\partial z_I} * [\dot{z}_I] \quad (A-3)$$

Carrying through the mathematical steps necessary to transfer the state variable z_I derivative to the left-hand side, we obtain the state model B in the following form:

$$\begin{bmatrix} \dot{x}_I \\ \dot{y}_I \\ \dot{z}_I \end{bmatrix} = \hat{H}_B^I(t) \begin{bmatrix} u \\ v \\ w \end{bmatrix} + \begin{bmatrix} w_{x_{I_0}} + \frac{\partial w_{x_I}}{\partial z_I} (z_I - z_{I_0}) \\ w_{y_{I_0}} + \frac{\partial w_{y_I}}{\partial z_I} (z_I - z_{I_0}) \\ w_{z_{I_0}} + \frac{\partial w_{z_I}}{\partial z_I} (z_I - z_{I_0}) \end{bmatrix} \quad (A-4)$$

$$\begin{bmatrix} \dot{u} \\ \dot{v} \\ \dot{w} \end{bmatrix} = \hat{\omega}(t) \begin{bmatrix} u \\ v \\ w \end{bmatrix} + \begin{bmatrix} a_x - s\hat{\theta} g \\ a_y + c\hat{\theta}s\hat{\phi}g \\ a_z + c\hat{\theta}c\hat{\phi}g \end{bmatrix} + \begin{bmatrix} n_{a_x} \\ n_{a_y} \\ n_{a_z} \end{bmatrix} + H_{uvw} \hat{H}_I^B(t) \frac{\partial w_I}{\partial z_I}$$

(A-5)

$$\begin{bmatrix} \dot{w}_{x_{I_0}} \\ \dot{w}_{y_{I_0}} \\ \dot{w}_{z_{I_0}} \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix}$$

(A-6)

$$\begin{bmatrix} \frac{\partial \dot{w}_{x_I}}{\partial z_I} \\ \frac{\partial \dot{w}_{y_I}}{\partial z_I} \\ \frac{\partial \dot{w}_{z_I}}{\partial z_I} \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix}$$

(A-7)

$$H_{uvw} \triangleq \begin{bmatrix} \hat{H}_{B_{31}}^I & \hat{H}_{B_{32}}^I & \hat{H}_{B_{33}}^I \end{bmatrix} \begin{bmatrix} u \\ v \\ w \end{bmatrix}$$

(A-8)

The kinematic state model B of eq. (A-2) to (A-8) renders improved flight path reconstruction and an estimate of constant wind and of wind gradient along the flight path.

A.2 LINEARIZATION OF THE SIMPLIFIED KINEMATIC MODEL

To apply the extended Kalman filter algorithm the non-linear kinematic model has to be linearized. The linearized version of the simplified kinematic model has been derived analytically and is presented in this section. The result for state model A [eq. (3-40)] is:

$$\begin{aligned}
 \begin{bmatrix} \dot{p} \\ \dot{q} \\ \dot{r} \\ \dot{\phi} \\ \dot{\theta} \\ \dot{\psi} \end{bmatrix} &= \begin{bmatrix} 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 \\ 1 & \text{tg}\theta\text{s}\phi & \text{tg}\theta\text{c}\phi & \text{qtg}\theta\text{c}\phi - \text{rtg}\theta\text{s}\phi & (\text{qs}\phi + \text{rc}\phi)/\text{c}^2\theta \\ 0 & \text{c}\phi & -\text{s}\phi & -\text{qs}\phi - \text{rc}\phi & 0 \\ 0 & \text{s}\phi/\text{c}\theta & \text{c}\phi/\text{c}\theta & \text{qc}\phi/\text{c}\theta - \text{rs}\phi/\text{c}\theta & (\text{qs}\phi + \text{rc}\phi)\frac{\text{s}\theta}{\text{c}^2\theta} \end{bmatrix} \begin{bmatrix} p \\ q \\ r \\ \phi \\ \theta \\ \psi \end{bmatrix} + \begin{bmatrix} \dot{p} \\ \dot{q} \\ \dot{r} \\ 0 \\ 0 \\ 0 \end{bmatrix} \quad (\text{A-9}) \\
 \dot{\underline{x}}_A & \qquad \qquad \qquad \underline{F}_A \qquad \qquad \qquad \underline{x}_A \qquad \underline{w}_A
 \end{aligned}$$

Rearranging eq. (3-50) of state model B:

$$\begin{aligned}
 \begin{bmatrix} \dot{x}_I \\ \dot{y}_I \\ \dot{z}_I \\ \dot{u} \\ \dot{v} \\ \dot{w} \end{bmatrix} &= \begin{bmatrix} 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \end{bmatrix} + \begin{bmatrix} \hat{H}_B^I(t) \\ \hat{\omega}(t) \end{bmatrix} \begin{bmatrix} x_I \\ y_I \\ z_I \\ u \\ v \\ w \end{bmatrix} + \begin{bmatrix} w_{x_I} \\ w_{y_I} \\ w_{z_I} \\ a_x - \hat{s}\hat{\theta}g \\ a_y + \hat{c}\hat{\theta}\hat{s}\hat{\phi}g \\ a_z + \hat{c}\hat{\theta}\hat{c}\hat{\phi}g \end{bmatrix} + \begin{bmatrix} 0 \\ 0 \\ 0 \\ n_{a_x} \\ n_{a_y} \\ n_{a_z} \end{bmatrix} \quad (\text{A-10}) \\
 \dot{\underline{x}}_B & \qquad \underline{F}_B \qquad \qquad \underline{x}_B \qquad \underline{G}_B \qquad \underline{u}_B \qquad \underline{w}_B
 \end{aligned}$$

The linearized version of measurement model B [eq. (3-51)]:

$$\underbrace{\begin{bmatrix} |V_{air}| \\ \alpha \\ \beta \\ h \\ r_{DME_{s1}} \\ r_{DME_{s2}} \\ \theta_{VOR_{s1}} \\ \theta_{VOR_{s2}} \end{bmatrix}}_{z_B} = \underbrace{\begin{bmatrix} 0 & 0 & 0 & \frac{u}{a_0^{1/2}} & \frac{v}{a_0^{1/2}} & \frac{w}{a_0^{1/2}} \\ 0 & 0 & 0 & \frac{-w}{a_0^{-v^2}} & 0 & \frac{u}{a_0^{-v^2}} \\ 0 & 0 & 0 & \frac{-v}{a_0^{-w^2}} & \frac{u}{a_0^{-w^2}} & 0 \\ 0 & 0 & -1 & 0 & 0 & 0 \\ \frac{x_I - x_{s1}}{a_{31}^{1/2}} & \frac{y_I - y_{s1}}{a_{31}^{1/2}} & \frac{z_I - z_{s1}}{a_{31}^{1/2}} & 0 & 0 & 0 \\ \frac{x_I - x_{s2}}{a_{32}^{1/2}} & \frac{y_I - y_{s2}}{a_{32}^{1/2}} & \frac{z_I - z_{s2}}{a_{32}^{1/2}} & 0 & 0 & 0 \\ \frac{-(y_I - y_{s1})}{a_{31} - (z_I - z_{s1})^2} & \frac{x_I - x_{s1}}{a_{31} - (z_I - z_{s1})^2} & 0 & 0 & 0 & 0 \\ \frac{-(y_I - y_{s2})}{a_{32} - (z_I - z_{s2})^2} & \frac{x_I - x_{s2}}{a_{32} - (z_I - z_{s2})^2} & 0 & 0 & 0 & 0 \end{bmatrix}}_{H_B} \underbrace{\begin{bmatrix} x_I \\ y_I \\ z_I \\ u \\ v \\ w \end{bmatrix}}_{x_B} + \underbrace{\begin{bmatrix} n_v \\ n_\alpha \\ n_\beta \\ n_h \\ n_{DME_1} \\ n_{DME_2} \\ n_{VOR_1} \\ n_{VOR_2} \end{bmatrix}}_{v_B} \quad (A-11)$$

$$\left. \begin{aligned} \text{with: } a_0 &= u^2 + v^2 + w^2 \\ a_{3i} &= (x_I - x_{si})^2 + (y_I - y_{si})^2 + (z_I - z_{si})^2 \end{aligned} \right\} (A-12)$$

A.3 LINEARIZATION OF THE IMPROVED KINEMATIC MODEL.

The improvement to the kinematic model elaborated in the first section of this appendix refers to state model B. The linearized version of (A-3) is:

$$\begin{bmatrix} \dot{x}_I \\ \dot{y}_I \\ \dot{z}_I \\ \dot{u} \\ \dot{v} \\ \dot{w} \\ \dot{w}_{x_{I_0}} \\ \dot{w}_{y_{I_0}} \\ \dot{w}_{y_{I_0}} \\ \frac{\partial \dot{w}_{x_I}}{\partial z_I} \\ \frac{\partial \dot{w}_{y_I}}{\partial z_I} \\ \frac{\partial \dot{w}_{z_I}}{\partial z_I} \end{bmatrix} = \begin{bmatrix} F_{11} & F_{12} & F_{13} & F_{14} \\ F_{21} & F_{22} & F_{23} & F_{24} \\ F_{31} & F_{32} & F_{33} & F_{34} \\ F_{41} & F_{42} & F_{43} & F_{44} \end{bmatrix} \begin{bmatrix} x_I \\ y_I \\ z_I \\ u \\ v \\ w \\ w_{x_{I_0}} \\ w_{y_{I_0}} \\ w_{z_{I_0}} \\ \frac{\partial w_{x_I}}{\partial z_I} \\ \frac{\partial w_{y_I}}{\partial z_I} \\ \frac{\partial w_{z_I}}{\partial z_I} \end{bmatrix} + \begin{bmatrix} 0 \\ 0 \\ 0 \\ a_x - s\theta g \\ a_y + c\hat{\theta}s\hat{\phi}g \\ a_z + c\hat{\theta}c\hat{\phi}g \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \end{bmatrix} + \begin{bmatrix} 0 \\ 0 \\ 0 \\ n_{a_x} \\ n_{a_y} \\ n_{a_z} \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \end{bmatrix} \quad (A-13)$$

$\dot{\underline{x}}_B$ F_B \underline{x}_B

where each F_{ij} stands for a 3x3 matrix:

$$F_{21} = F_{31} = F_{41} = F_{32} = F_{42} = F_{23} = F_{33} = F_{43} = F_{34} = F_{44} = [0] \quad (\text{A-14})$$

$$F_{13} = [I] \quad (\text{A-15})$$

$$F_{14} = (z_I - z_{I_0}) [I] \quad (\text{A-16})$$

$$F_{11} = \begin{bmatrix} 0 & 0 & \frac{\partial w_{x_I}}{\partial z_I} \\ 0 & 0 & \frac{\partial w_{y_I}}{\partial z_I} \\ 0 & 0 & \frac{\partial w_{z_I}}{\partial z_I} \end{bmatrix} \quad (\text{A-17})$$

$$F_{12} = \hat{H}_B^I(t) \quad (\text{A-18})$$

$$F_{22} = \begin{bmatrix} \hat{H}_{B31}^I \left(\hat{H}_I^B \frac{\partial w_I}{\partial z_I} \right)_1 & \hat{r} + \hat{H}_{B32}^I \left(\hat{H}_I^B \frac{\partial w_I}{\partial z_I} \right)_1 & -\hat{q} + \hat{H}_{B33}^I \left(\hat{H}_I^B \frac{\partial w_I}{\partial z_I} \right)_1 \\ -\hat{r} + \hat{H}_{B31}^I \left(\hat{H}_I^B \frac{\partial w_I}{\partial z_I} \right)_2 & \hat{H}_{B32}^I \left(\hat{H}_I^B \frac{\partial w_I}{\partial z_I} \right)_2 & \hat{p} + \hat{H}_{B33}^I \left(\hat{H}_I^B \frac{\partial w_I}{\partial z_I} \right)_2 \\ \hat{q} + \hat{H}_{B31}^I \left(\hat{H}_I^B \frac{\partial w_I}{\partial z_I} \right)_3 & -\hat{p} + \hat{H}_{B32}^I \left(\hat{H}_I^B \frac{\partial w_I}{\partial z_I} \right)_3 & \hat{H}_{B33}^I \left(\hat{H}_I^B \frac{\partial w_I}{\partial z_I} \right)_3 \end{bmatrix} \quad (\text{A-19})$$

$$F_{24} = H_{uvw} * \hat{H}_I^B(t) \quad (\text{A-20})$$

APPENDIX B
PROGRAM LISTINGS

B.1 ONBOARD ASSEMBLY PROGRAMMING

The microprocessor prepares the data in block units. Each block unit is a memory buffer of 1024 data words (each data word contains two bytes or 16 bits). For 38 information channels, for example, taken every second such a block can be filled with 26-sec worth of data (plus 36 dummy words: $38 \times 26 + 36 = 1024$). A data block is written into the digital cartridge recordwise. Each record contains 128 data words, i.e., under normal conditions eight records complete a block transfer. Occasionally, to make sure that no data is missed, a record may be written repeatedly onto the cartridge. Thus, the first task for the preprocessing software (Appendix C) is to reconstruct the original data blocks, each constituting of eight records of $\frac{8 \times 128 - 36}{38} = 26$ information-seconds.

B.2 GENERIC SPIFR FLIGHT PATH AND IN-FLIGHT MEASUREMENTS SIMULATION (FORTRAN)

This program creates a generic SPIFR mission trajectory, simulates the associated in-flight measurements and corrupts them with pseudo-random noise. Knowing the uncorrupted values of the measured variables, the algorithm for optimal smoothing and flight path reconstruction may be verified.

B.3 OPTIMAL SMOOTHING AND FLIGHT PATH RECONSTRUCTION ALGORITHM (FORTRAN)

As demonstrated in the following listings, one of the key issues in optimal smoothing and flight path reconstruction is computer storage management -- in particular, between the forward and the backward passes over the measured data records. The smoothing algorithm, which consists of eq. (3-60) to (3-63), requires knowledge of the state-vector before and after each measurement update and of the corresponding covariance matrices. For state model A, e.g., the state vector has six components. This means that following the filtering pass 84 values have to be stored for each measurement instant. A SPIFR mission simulation is about 30 minutes long and after preprocessing the measurement update interval is standardized to be 1 sec for all variables. Thus, the temporary storage facility has to "remember" 84x30x60 values.

228035	326188	64	STA	FLAG		
228038	3E24	65	MVI	A,''		
22803A	CD4182	66	CALL	BO		
22803D	C31F80	67	JMP	BB		
22		68	;LAG:	DB	0	
22		69	FILLMEM:			
228040	F5	70	PUSH	PSW		
228041	E5	71	PUSH	H		
228042	110090	72	LXI	D,BUFF0	;BASE ADDRESS FOR FILLING IS BUFF0	
228045	210000	73	LXI	H,0	;COUNT STARTS WITH 0	
228048	7D	74	FILLAG:	MOV	A,L	;LOWER BYTE INTO ACC
228049	12	75	STAX	D	;STORE IT TO MEMORY	
22804A	13	76	INX	D	;MOVE TO NEXT BYTE LOCATION	
22804B	7C	77	MOV	A,H	;UPPER BYTE INTO ACC	
22804C	12	78	STAX	D	;STORE IT TO MEMORY	
22804D	13	79	INX	D	;POINT TO NEXT BYTE LOCATION	
22804E	23	80	INX	H	;SIZE OF INTEGER UP BY 1	
22804F	7C	81	MOV	A,H	;CHECK FOR AN UPPER BOUND	
228050	FE28	82	CPI	28H	;	
228052	C24880	83	JNZ	FILLAG	;REPEAT IF BELOW UPPER BOUND	
228055	E1	84	POP	H		
228056	F1	85	POP	PSW		
228057	C9	86	RET			
22		87	UEBUFS:			
228058	F5	88	PUSH	PSW		
228059	E5	89	PUSH	H		
22805A	C5	90	PUSH	B		
22805B	2A6688	91	LHLD	EREMAIN		
22805E	010001	92	LXI	B,256	;256 BYTES EMPYIED AT A TIME	
228061	AF	93	XRA	A	;CARRY=0	
228062	ED42	94	DSEC	B		
228064	226688	95	SHLD	EREMAIN	;EREMAIN=EREMAIN-256	
22		96			;	
22		97			;IS EREMAIN >= 256 ?	
22		98			;	
228067	AF	99	XRA	A	;CARRY=0	
228068	ED42	100	DSEC	B		
22806A	F29D80	101	JP	EROOH	;IF S=0, HL >= BC	
22		102			;	
22		103			;CAN NOT EMPTY	
22		104			; ANOTHER BLOCK OF 256	
22		105			; FROM CURRENT BUFFER OF 2048	
22		106			;	
22806D	CD6887	107	CALL	SETEMPY	;MARK CURRENT BUFFER EMPTY	
22		108			;SET UP INDICES FOR DUMPING NEXT 2048 BLOCK	
228070	210008	109	LXI	H,2048	;	
228073	226688	110	SHLD	EREMAIN	;EREMAIN=2048	
22		111			;	
228076	3A6888	112	LDA	EMHICB	;SWITCH TO NEXT BUFFER	
228079	3C	113	INR	A	;	
22807A	326888	114	STA	EMHICB	;	
22807D	FE0A	115	CPI	10		
22807F	C29280	116	JNZ	ESW	;	
228082	76	117	HLT			
22		118			;	
22		119			;WE ARE NOW BEYOND TENTH BUFFER	
22		120			; NOTE EMHICB HAS RANGE 0 TO 9	
22		121			; SWITCH TO BUFFER 0	
22		122			;	
228083	3E00	123	MVI	A,0		
228085	326888	124	STA	EMHICB	;EMHICB=0	
22		125			;	
22		126			;ECLRRBUF CONTAINS THE STARTING	
22		127			; LOCATION OF THE CURRENT 2048 BLOCK	
22		128			; BEING EMPTYIED	
22		129			;	

```

LL8086 110090 130 LXI D,BUFFO ;BUFFO IS STARTING LOCATION OF
LL 131 ; BLOCK 0 OR BUFFER 0
LL8088 ED537488 132 SDED ECURRBUF ;NOTE THAT DE POINTS WHERE ECURRBUF POINTS
LL80AF C39D80 133 JMP EROOM
LL 134 ESM:
LL 135 ;
LL 136 ;WE ARE GOING TO EMPTY A BUFFER
LL 137 ; 2048 BYTES HIGHER IN CORE THAN THE
LL 138 ; PREVIOUS BUFFER.
LL 139 ;
LL8092 2A7488 140 LHL ECURRBUF ;
LL8095 010008 141 LXI B,2048
LL8098 09 142 DAD B
LL8099 227488 143 SHLD ECURRBUF
LL809C EB 144 XCHG ;DE POINTING WHERE ECURRBUF POINTS.
LL 145 EROOM:
LL809D C1 146 POP B
LL809E E1 147 POP H
LL809F F1 148 POP PSM
LL80A0 C9 149 RET
LL 150 ;
LL 151 WRITE:
LL 152 ;THE ONLY ERROR ALLOWED FOR NOW
LL 153 ;IS TRYING TO WRITE BEYOND EOT
LL 154 ;WRITE ON LEFT TAPE OR RIGHT TAPE
LL 155 ;DEPENDING ON THE SETTING OF TSM
LL 156 ;TSM='L' OR 'R'.
LL 157 ;IF END OF TAPE OR HARD ERROR ON ONE TAPE,
LL 158 ;SWITCH TO ANOTHER TAPE
LL 159 ;
LL80A1 F5 160 PUSH PSM
LL80A2 E5 161 PUSH H
LL80A3 C5 162 PUSH B
LL80A4 ED537888 163 SDED TEMPDE ;SAVE DE PAIR IN CASE OF RETRY
LL 164 ; LXI H,TEMPDE
LL 165 ; CALL HOMP2
LL80A8 3A6988 166 LDA TSM ;WHICH TAPE DO WE USE?
LL80AB FE4C 167 CPI 'L'
LL80AD C2C280 168 JNZ WRITR
LL 169 WRITL:
LL80B0 CD3481 170 CALL LCTUM ;IF YOU COME TO EDT SWITCH TO NEXT UNIT
LL 171 ;((((((((MORE CODE HERE))))))))))))))))
LL 172 ;((((((((ABOUT SWITCHING LOGIC))))))))))))))))
LL80B3 CAE80 173 JZ RETML
LL80B6 3E52 174 MVI A,'R'
LL80B8 326988 175 STA TSM
LL 176 ;((((((((RETRANSMIT LAST RECORD ONTO RIGHT TAPE))))))))))))
LL80BB C3C280 177 JMP WRITR ; AND REWRITE RECORD ON RIGHT TAPE
LL80BE C1 178 RETML: POP B
LL80BF E1 179 POP H
LL80C0 F1 180 POP PSM
LL80C1 C9 181 RET
LL 182 WRITR:
LL80C2 CD0581 183 CALL RETUM ;IF YOU COME TO EDT SWITCH TO NEXT UNIT
LL 184 ;((((((((MORE CODE HERE))))))))))))))))
LL 185 ;((((((((ABOUT SWITCHING LOGIC))))))))))))))))
LL80C5 CAD080 186 JZ RETMR
LL80C8 3E4C 187 MVI A,'L'
LL80CA 326988 188 STA TSM
LL 189 ;((((((((RETRANSMIT LAST RECORD USING))))))))))))
LL80CD C3B080 190 JMP WRITL ; AND REWRITE RECORD ON LEFT TAPE
LL80D0 C1 191 RETMR: POP B
LL80D1 E1 192 POP H
LL80D2 F1 193 POP PSM
LL80D3 C9 194 RET
LL 195 INITMR:

```


LL80D4	F5	196	PUSH	PSW	
LL80D5	E5	197	PUSH	H	
LL80D6	3E00	198	MVI	A,0	
LL80D8	326888	199	STA	EMHIC8B	
LL80DB	210008	200	LXI	H,2048	
LL80DE	226688	201	SHLD	EREMAIN	
LL80E1	3E4C	202	MVI	A,'L'	
LL80E3	326988	203	STA	TSM	
LL80E6	210090	204	LXI	H,BUFF0	
LL80E9	227488	205	SHLD	ECURRBUF	
LL80EC	110090	206	LXI	D,BUFF0	
LL80EF	E1	207	POP	H	
LL80F0	F1	208	POP	PSW	
LL80F1	C9	209	RET		
LL		210	DEH256:		
LL80F2	E5	211	PUSH	H	
LL		212			;
LL		213			;DE (= DE - 256
LL		214			;
LL80F3	62	215	MOV	H,D	
LL80F4	6B	216	MOV	L,E	;HL (= DE
LL80F5	010001	217	LXI	B,256	
LL80F8	AF	218	XRA	A	;CARRY=0
LL80F9	ED42	219	DSBC	B	;HL - 256
LL80FB	54	220	MOV	D,H	
LL80FC	5D	221	MOV	E,L	;DE (= HL
LL80FD	E1	222	POP	H	
LL80FE	C9	223	RET		
LL		224	LCTUF:		
LL		225			;WRITE AN EOF MARK ON LCTU
LL80FF	3E1B	226	MVI	A,ESC	
LL8101	CD4182	227	CALL	BO	
LL8104	3E26	228	MVI	A,'&	
LL8106	CD4182	229	CALL	BO	
LL8109	3E70	230	MVI	A,'p'	
LL810B	CD4182	231	CALL	BO	
LL810E	3E31	232	MVI	A,'1'	;ADDRESS OF LCTU
LL8110	CD4182	233	CALL	BO	
LL8113	3E75	234	MVI	A,'u'	
LL8115	CD4182	235	CALL	BO	
LL8118	3E35	236	MVI	A,'5'	;WRITE FILEMARK COMMAND IS ASCII CHAR 5
LL811A	CD4182	237	CALL	BO	
LL811D	3E43	238	MVI	A,'C'	
LL811F	CD4182	239	CALL	BO	
LL8122	3E11	240	MVI	A,DC1	
LL8124	CD4182	241	CALL	BO	
LL8127	CD5782	242	CALL	BI	
LL812A	326288	243	STA	SAVE	
LL812D	CD5782	244	CALL	BI	
LL8130	326388	245	STA	SAVE+1	
LL8133	C9	246	RET		
LL		247	LCTUM:		
LL8134	ED5B7888	248	LDSD	TEMPDE	
LL8138	3E1B	249	MVI	A,ESC	
LL813A	CD4182	250	CALL	BO	
LL813D	3E26	251	MVI	A,'&	
LL813F	CD4182	252	CALL	BO	
LL8142	3E70	253	MVI	A,'p'	
LL8144	CD4182	254	CALL	BO	
LL8147	3E31	255	MVI	A,'1'	
LL8149	CD4182	256	CALL	BO	
LL814C	3E64	257	MVI	A,'d'	
LL814E	CD4182	258	CALL	BO	
LL8151	3E32	259	MVI	A,'2'	
LL8153	CD4182	260	CALL	BO	
LL8156	3E35	261	MVI	A,'5'	

228158	CD4182	262	CALL	BO	
22815B	3E36	263	MVI	A,'6'	
22815D	CD4182	264	CALL	BO	
228160	3E57	265	MVI	A,'W'	
228162	CD4182	266	CALL	BO	
228165	3E05	267	MVI	A,ENG	
228167	CD4182	268	CALL	BO	
22816A	CD5782	269	CALL	BI	
22816D	326488	270	STA	SAV	
228170	FE06	271	CPI	ACK	
228172	CA7881	272	JZ	NEXT	
228175	C39481	273	JMP	LCTUM	
22		274			
228178	010001	275	NEXT:	LXI	B,256
22817B	CD7482	276		CALL	SEND
22817E	3E11	277		MVI	A,DC1
228180	CD4182	278		CALL	BO
228183	CD5782	279		CALL	BI
228186	DA3481	280		JC	LCTUM
228189	326288	281		STA	SAVE
22818C	CD5782	282		CALL	BI
22818F	DA3481	283		JC	LCTUM
228192	326388	284		STA	SAVE+1
228195	3A6288	285		LDA	SAVE
228198	FES3	286		CPI	'S'
22819A	C8	287		RZ	
22819B	ED5B7888	288		LDED	TEMPDE
22819F	C9	289		RET	
22		290			
22		291	RTUF:		
2281A0	3E1B	292		MVI	A,ESC
2281A2	CD4182	293		CALL	BO
2281A5	3E26	294		MVI	A,'8'
2281A7	CD4182	295		CALL	BO
2281AA	3E70	296		MVI	A,'p'
2281AC	CD4182	297		CALL	BO
2281AF	3E32	298		MVI	A,'2'
2281B1	CD4182	299		CALL	BO
2281B4	3E75	300		MVI	A,'u'
2281B6	CD4182	301		CALL	BO
2281B9	3E35	302		MVI	A,'5'
2281BB	CD4182	303		CALL	BO
2281BE	3E43	304		MVI	A,'C'
2281C0	CD4182	305		CALL	BO
2281C3	3E11	306		MVI	A,DC1
2281C5	CD4182	307		CALL	BO
2281C8	CD5782	308		CALL	BI
2281CB	326288	309		STA	SAVE
2281CE	CD5782	310		CALL	BI
2281D1	326388	311		STA	SAVE+1
2281D4	C9	312		RET	
22		313			
2281D5	ED5B7888	314	RTUM:	LDED	TEMPDE
2281D9	3E1B	315		MVI	A,ESC
2281DB	CD4182	316		CALL	BO
2281DE	3E26	317		MVI	A,'8'
2281E0	CD4182	318		CALL	BO
2281E3	3E70	319		MVI	A,'p'
2281E5	CD4182	320		CALL	BO
2281E8	3E32	321		MVI	A,'2'
2281EA	CD4182	322		CALL	BO
2281ED	3E64	323		MVI	A,'d'
2281EF	CD4182	324		CALL	BO
2281F2	3E32	325		MVI	A,'2'
2281F4	CD4182	326		CALL	BO
2281F7	3E35	327		MVI	A,'5'

;DE POINTS TO LOCATION TO BE EMPTIED
;READ S OF F
;READ CR
;EITHER S OR F
;RETURN Z SET ON 'S', Z RESET ON 'F'
;WRITE AN EOF MARK ON LCTU
;ADDRESS OF RCTU
;WRITE FILEMARK COMMAND IS ASCII CHAR 5
;ADDRESS OF RCTU

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0001F9 CD4182 328 CALL BO
0001FC 3E36 329 MVI A,'6'
0001FE CD4182 330 CALL BO
000201 3E57 331 MVI A,'W'
000203 CD4182 332 CALL BO
000206 3E05 333 MVI A,END
000208 CD4182 334 CALL BO
00020B CD5782 335 CALL BI
00020E 326488 336 STA SAV
000211 FE06 337 CPI ACK
000213 CA1982 338 JZ NEXT
000216 C3D581 339 JMP RCTUM
000218 340 NEXT:
000219 341 ;DE POINTS TO LOCATION TO BE EMPTIED
000219 010001 342 LXI B,256
00021C CD7482 343 CALL SEND
00021F 3E11 344 MVI A,DC1
000221 CD4182 345 CALL BO
000224 CD5782 346 CALL BI ; READ S OR F
000227 DAD581 347 JC RCTUM
00022A 326288 348 STA SAVE
00022D CD5782 349 CALL BI ; READ CR
000230 DAD581 350 JC RCTUM
000233 326388 351 STA SAVE+1
000236 3A6288 352 LDA SAVE ;EITHER S OR F
000239 FE53 353 CPI 'S' ;RETURN WITH Z SET ON S, Z RESET ON F
00023B CA 354 RZ
00023C ED5B7888 355 LDED TEMPDE
000240 C9 356 RET
000242 357 ;*****
000243 358 ; CHARACTER OUTPUT ROUTINE
000244 359 ; CD OUTPUTS ONE CHARACTER FROM ACC TO TERMINAL
000245 360 ; VIA THE USART. ALL REGISTERS AND FLAGS ARE
000246 361 ; PRESERVED. THE CHARACTER IT OUTPUTS IS IN THE ACC.
000247 362 ;*****
000248 363 BO: PUSH PSM
000249 364 PUSH B
000250 365 MOV C,A ;SAVE A REG
000251 366 BOO:
000252 367 NOP
000253 368 NOP
000254 369 IN S8251A ;GET USART STATUS
000255 370 ANI TXRDYA ;CHECK TRANSMIT READY FLAG
000256 371 JZ BOO ;NOT READY
000257 372 NOP
000258 373 NOP
000259 374 NOP
000260 375 NOP
000261 376 MOV A,C ;READY TO TRANSMIT , RESTORE CHAR TO A REG
000262 377 OUT D8251A ;SEND IT
000263 378 POP B
000264 379 POP PSM
000265 380 RET
000266 381 ;*****
000267 382 ; CHARACTER INPUT ROUTINE
000268 383 ; BI INPUTS ONE CHARACTER FROM TERMINAL INTO ACC
000269 384 ; VIA THE USART. THE FLAGS AND THE ACC ARE CHANGED.
000270 385 ; THE CHARACTER IT READS IS RETURNED IN THE ACC.
000271 386 ; IF NO TIMEOUT OCCURS, THE CARRY IS SET.
000272 387 ; IF TIMEOUT OCCURS, THE CARRY IS RESET.
000273 388 ; THE CHAR READ IS RETURNED IN THE ACC.
000274 389 ;*****
000275 390 BI: NOP ;
000276 391 PUSH B
000277 392 LXI B,OFFFH
000278 393 BIO:

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22A25C	08	394	DCX	B	
22A25D	78	395	MOV	A,B	
22A25E	B1	396	ORA	C	
22A25F	CA6F82	397	JZ	TIMEDOUT	
22A262	DBED	398	IN	S&251A	;GET USART STATUS
22A264	E602	399	ANI	R0R0YA	;CHECK RECIEVER READY
22A266	CAS0&2	400	JZ	B10	;
22A269	DBEC	401	IN	D&251A	;GET CHAR
22A268	37	402	STC		
22A26C	3F	403	CNC		
22A26D	C1	404	POP	B	
22A26E	C9	405	RET		
22A26F	00	406	TIMEDOUT: NOP		
22A270	37	407	STC		
22A271	C1	408	POP	B	
22A272	C9	409	RET		
22A273	76	410	HLT		
22		411	SEND:		
22A274	1A	412	LDAX	D	
22A275	CD41&2	413	CALL	BO	
22A278	13	414	INX	D	
22A279	08	415	DCX	B	
22A27A	78	416	MOV	A,B	
22A27B	B1	417	ORA	C	
22A27C	C274&2	418	JNZ	SEND	
22A27F	C9	419	RET		
22		420	STATUS:		
22A280	F5	421	PUSH	PSW	
22A281	E5	422	PUSH	H	
22A282	21FC&9	423	LXI	H,STAT	
22A285	3E18	424	MVI	A,ESC	;START ESCAPE SEQUENCE
22A287	CD41&2	425	CALL	BO	
22A28A	3E5E	426	MVI	A,'''	
22A28C	CD41&2	427	CALL	BO	
22A28F	3E11	428	MVI	A,DC1	
22A291	CD41&2	429	CALL	BO	
22A294	CD57&2	430	CALL	BI	;EAT ESC
22A297	CD57&2	431	CALL	BI	;EAT BACKSLASH
22A29A	CD57&2	432	CALL	BI	;BYTE 0
22A29D	CD0B&8	433	CALL	CO	
22A2A0	CD57&2	434	CALL	BI	;BYTE 1
22A2A3	CD0B&8	435	CALL	CO	
22A2A6	CD57&2	436	CALL	BI	;BYTE 2
22A2A9	CD0B&8	437	CALL	CO	
22A2AC	CD57&2	438	CALL	BI	;BYTE 3
22A2AF	CD0B&8	439	CALL	CO	
22A2B2	CD57&2	440	CALL	BI	;BYTE 4
22A2B5	CD0B&8	441	CALL	CO	
22A2B8	CD57&2	442	CALL	BI	;BYTE 5
22A2BB	CD0B&8	443	CALL	CO	
22A2BE	CD57&2	444	CALL	BI	;BYTE 6
22A2C1	CD0B&8	445	CALL	CO	
22A2C4	CD57&2	446	CALL	BI	;GET CR
22A2C7	CD0B&8	447	CALL	CO	
22A2CA	E1	448	POP	H	
22A2CB	F1	449	POP	PSW	
22A2CC	C9	450	RET		
22		451	LCTUST:		
22A2CD	F5	452	PUSH	PSW	
22A2CE	E5	453	PUSH	H	
22A2CF	3E18	454	MVI	A,ESC	
22A2D1	CD0B&8	455	CALL	CO	
22A2D4	3E26	456	MVI	A,'&'	
22A2D6	CD0B&8	457	CALL	CO	
22A2D9	3E70	458	MVI	A,'p'	
22A2DB	CD0B&8	459	CALL	CO	

LL82DE	3E31	460	MVI	A,'1'
LL82E0	CD0B88	461	CALL	CO
LL82E3	3E5E	462	MVI	A,'''
LL82E5	CD0B88	463	CALL	CO
LL82E8	3E11	464	MVI	A,DC1
LL82EA	CD0B88	465	CALL	CO
LL82ED	CD5782	466	CALL	BI ;ESC READ
LL82F0	CD5782	467	CALL	BI ;BACKSLASH READ
LL82F3	CD5782	468	CALL	BI ;P READ
LL82F6	CD5782	469	CALL	BI ;DEVICE CODE DIGIT READ
LL82F9	CD5782	470	CALL	BI ;BYTE 0 READ
LL82FC	CD5782	471	CALL	BI ;BYTE 1 READ
LL82FF	CD5782	472	CALL	BI ;BYTE 2 READ
LL8302	CD5782	473	CALL	BI ;CR READ
LL8305	E1	474	POP	H
LL8306	F1	475	POP	PSW
LL8307	C9	476	RET	
LL		477	;	
LL		478	;	DELAY ONE MILLISECOND
LL		479	;	
LL		480	DIMS:	
LL8308	C5	481	PUSH	B
LL8309	F5	482	PUSH	PSW
LL830A	019800	483	LXI	B,152
LL830B	0B	484	DIMS:	DCX B
LL830E	78	485	MOV	A,B
LL830F	B1	486	ORA	C
LL8310	C20D83	487	JNZ	DIMS0
LL8313	F1	488	POP	PSW
LL8314	C1	489	POP	B
LL8315	C9	490	RET	
LL001B		491	ESC	EDU 1BH
LL000D		492	CR	EDU 0DH
LL00ED		493	S&Z51A	EDU 0EDH
LL00EE		494	D&Z51A	EDU 0ECH
LL0002		495	R&R&YA	EDU 0ZH
LL0001		496	T&R&YA	EDU 01H
LL000A		497	LF	EDU 0AH
LL0005		498	ENQ	EDU 05H
LL0006		499	ACK	EDU 06H
LL0011		500	DC1	EDU 11H
LL8316	F5	501	CNTR1:	PUSH PSW
LL8317	3E74	502	MVI	A,074H
LL8319	D3DF	503	OUT	ODFH
LL831B	3E10	504	MVI	A,TLOW
LL831D	D3DD	505	OUT	ODDH
LL831F	3E27	506	MVI	A,THIGH
LL8321	D3DD	507	OUT	ODDH
LL8323	E3	508	XTHL	
LL8324	E3	509	XTHL	
LL8325	F1	510	POP	PSW
LL8326	C9	511	RET	
LL8327	F5	512	CNTR0:	PUSH PSW
LL8328	3E36	513	MVI	A,036H
LL832A	D3DF	514	OUT	ODFH
LL832C	3E0A	515	MVI	A,0AH
LL832E	D3DC	516	OUT	ODCH
LL8330	3E00	517	MVI	A,00H
LL8332	D3DC	518	OUT	ODCH
LL8334	E3	519	XTHL	
LL8335	E3	520	XTHL	
LL8336	F1	521	POP	PSW
LL8337	C9	522	RET	
LL		523	STINT:	
LL8338	F5	524	PUSH	PSW
LL8339	E5	525	PUSH	H

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LL          526 ;
LL          527 ;
LL          528 ;
LL833A 3EC3      529      MVI    A,00H
LL833C 32E3FF    530      STA    INT75
LL833F 214F83    531      LXI    H,BREAK
LL8342 22E4FF    532      SHLD   INT75+1
LL          533 ;
LL          534 ;
LL          535 ;
LL8345 3B03      536      MVI    A,03H      ;BIT 7=0 FOR MODE 0
LL          537 ;
LL          538 ;
LL8347 0307      539      OUT   007H      ;BIT 0 TO 3 DEFINE INTERRUPT PRIORITY
LL          540 ;
LL          541 ;
LL          542 ;
LL8349 ED46      543      INM   H
LL834B E1        544      POP   H
LL834C F1        545      POP   PSM
LL          546 ;
LL          547 ;
LL          548 ;
LL834D FB        549      EI
LL834E C9        550      RET
LL          551 ;
LL          552 ;
LL          553 ;
LL834F 00        554      BREAK: NOP
LL8350 F5        555      PUSH  PSM
LL8351 E5        556      PUSH  H
LL8352 C5        557      PUSH  B
LL8353 D5        558      PUSH  D
LL          559 ;
LL8354 3A6188    560      LDA   FLAG
LL8357 30        561      DCR   A
LL8358 326188    562      STA   FLAG
LL          563 ;
LL835B 3EFF      564      MVI    A,0FFH    ;MAKE OUTPUT OF
LL835D 03E8      565      OUT   0E8H      ; ZERO VOLTS
LL835F ED5B5788  566      LDED  ;RESTORE BUFFER POINTER TO DE PAIR
LL8363 CD4A87    567      CALL  TSTFULL   ;IS BUFFER EMPTY
LL          568 ;
LL          569 ;
LL          570 ;
LL8366 CDC383    571      CALL  FAST      ;COLLECT FAST DATA
LL          572 ;
LL          573 ;
LL          574 ;
LL8369 3A5E88    575      LDA   CNT
LL836C FE04      576      CPI   4
LL836E C27483    577      JNZ   NOT4
LL8371 CD2484    578      CALL  SLOW
LL          579      NOT4:
LL          580 ;
LL          581 ;
LL          582 ;
LL          583 ;
LL8374 3A5E88    584      LDA   CNT
LL8377 FED9      585      CPI   9
LL8379 C2A783    586      JNZ   NOT9
LL          587 ;
LL837C 213400    588      LXI    H,2*26
LL837E 19        589      DAD   D      ;ADD 2*26 TO DE PAIR TO POINT BEYOND
LL8380 50        590      MOV   E,L
LL8381 54        591      MOV   D,H      ;PUT HL IN DE

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228382	CDCA86	592	CALL	DISPLAY	;IF THERE IS TWO DIGIT PAIR READY, DISPLAY MEMORY
228385	CD484	593	CALL	UPBLIPS	;THERE ARE TWO BUFFER POINTERS AND COUNTER
228388	CD5785	595	CALL	UCLK	; TO UPDATE
22838B	CD486	596	CALL	FLIP	;TIC THE CLOCK
22838E	CD7A88	597	CALL	AVG	;TOGGLE LITE 3
228391	CD3885	598	CALL	UINTS	
228394	CD4785	599	CALL	RINTS	
228397	ED535788	600	SEED	SAVEDE	
22839B	AF	601	XRA	A	
22839C	D3E8	602	OUT	OE8H	
22839E	CD9785	603	CALL	STATE	
2283A1	CD7886	604	CALL	INTWODIG	
2283A4	C38983	605	JMP	MODISP	
2283A7	CD7A88	609	CALL	AVG	;AVERAGE FAST CHANNELS
2283AA	CD3885	610	CALL	UINTS	;UPDATE INTERRUPT COUNT
2283AD	CD4785	612	CALL	RINTS	;RESET INTERRUPT COUNT WHEN NECESSARY
2283B0	AF	613	XRA	A	;MAKE OUTPUT OF
2283B1	D3E8	614	OUT	OE8H	; FIVE VOLTS
2283B3	CD9785	617	CALL	STATE	; PLAY WITH PBS + LITES ON CONTROL PANEL
2283B6	CD7886	618	CALL	INTWODIG	;LOOK FOR FOR TWO DIGIT PAIR
2283B9	3E03	620	MVI	A,03H	
2283BB	D3D7	621	OUT	0D7H	
2283BD	D1	622	POP	D	
2283BE	C1	623	POP	B	
2283BF	E1	624	POP	H	
2283C0	F1	625	POP	PSW	
2283C1	FB	626	EI		
2283C2	C9	627	RET		
2283C3	3E00	629	MVI	A,0	
2283C5	CD6185	630	CALL	ADCO	
2283C8	CDEB84	631	CALL	STORE	
2283CB	3E00	633	MVI	A,0	;DELE COLUMN CHANNEL
2283CD	CD6185	634	CALL	ADCO	; READ ADC CHANNEL
2283D0	CDEB84	635	CALL	STORE	; PUT IN BUFFER RAM
2283D3	3E05	637	MVI	A,5	;THETADOT CHANNEL
2283D5	CD6185	638	CALL	ADCO	; READ ADC CHANNEL
2283D8	CDEB84	639	CALL	STORE	; PUT IN BUFFER RAM
2283DB	3E07	641	MVI	A,7	;HZ-NORMAL ACCEL CHANNEL
2283DD	CD6185	642	CALL	ADCO	; READ ADC CHANNEL
2283E0	CDEB84	643	CALL	STORE	; PUT IN RAM BUFFER
2283E3	3E08	645	MVI	A,8	;DELA-ROOLL WHEEL
2283E5	CD6185	646	CALL	ADCO	; READ ADC CHANNEL
2283E8	CDEB84	647	CALL	STORE	; PUT IN RAM BUFFER
2283EB	3E09	649	MVI	A,9	;DELTA-PEDALS CHANNEL
2283ED	CD6185	650	CALL	ADCO	; READ ADC CHANNEL
2283F0	CDEB84	651	CALL	STORE	; PUT IN RAM BUFFER
2283F3	3E0B	653	MVI	A,11	;BETA-SIDESLIP CHANNEL
2283F5	CD6185	654	CALL	ADCO	; READ ADC CHANNEL
2283F8	CDEB84	655	CALL	STORE	; PUT IN RAM BUFFER
2283FB	3E0D	657	MVI	A,13	;P-ROLL RATE CHANNEL

2283FD	CD6185	658	CALL	ADCO	; READ ADC CHANNEL
228400	CDEB84	659	CALL	STORE	; PUT IN RAM BUFFER
22		660			
228403	3E0E	661	MVI	A,14	;R-YAW RATE CHANNEL
228405	CD6185	662	CALL	ADCO	; READ ADC CHANNEL
228408	CDEB84	663	CALL	STORE	; PUT IN RAM BUFFER
22		664			
22840B	3E0F	665	MVI	A,15	;RY-LATERAL ACCEL CHANNEL
22840D	CD6185	666	CALL	ADCO	; READ ADC CHANNEL
228410	CDEB84	667	CALL	STORE	; PUT IN RAM BUFFER
22		668			
228413	3E15	669	MVI	A,21	;RX-LONGITUDINAL ACCEL CHANNEL
228415	CD6185	670	CALL	ADCO	; READ ADC CHANNEL
228418	CDEB84	671	CALL	STORE	; PUT IN RAM BUFFER
22		672			
22841B	3E19	673	MVI	A,25	;ALPHA-ANGLE OF ATTACK CHANNEL
22841D	CD6185	674	CALL	ADCO	; READ ADC CHANNEL
228420	CDEB84	675	CALL	STORE	; PUT IN RAM BUFFER
228423	C9	676	RET		
22		677			
22		678			
228424	CD7E85	679	CALL	DME	;DME DISTANCE
228427	CDEB84	680	CALL	STORE	; PUT IN BUFFER RAM
22		681			
22842A	3E01	682	MVI	A,1	;DELTA-THROTTLE HANDLE
22842C	CD6185	683	CALL	ADCO	; READ ADC CHANNEL
22842F	CDEB84	684	CALL	STORE	; PUT IN RAM BUFFER
22		685			
228432	3E02	686	MVI	A,2	;DELTA-FLAP LEVER CHANNEL
228434	CD6185	687	CALL	ADCO	; READ ADC CHANNEL
228437	CDEB84	688	CALL	STORE	; PUT IN RAM BUFFER
22		689			
22843A	3E03	690	MVI	A,3	;DELTA-ELEVATOR TRIM CHANNEL
22843C	CD6185	691	CALL	ADCO	; READ ADC CHANNEL
22843F	CDEB84	692	CALL	STORE	; PUT IN RAM BUFFER
22		693			
228442	3E04	694	MVI	A,4	;THETA-PITCH ANGLE CHANNEL
228444	CD6185	695	CALL	ADCO	; READ ADC CHANNEL
228447	CDEB84	696	CALL	STORE	; PUT IN RAM BUFFER
22		697			
22844A	3E06	698	MVI	A,6	;U-VELOCITY CHANNEL
22844C	CD6185	699	CALL	ADCO	; READ ADC CHANNEL
22844F	CDEB84	700	CALL	STORE	; PUT IN RAM BUFFER
22		701			
228452	3E0A	702	MVI	A,10	;PSI-HEADING ANGLE CHANNEL
228454	CD6185	703	CALL	ADCO	; READ ADC CHANNEL
228457	CDEB84	704	CALL	STORE	; PUT IN RAM BUFFER
22		705			
22845A	3E0C	706	MVI	A,12	;PHI-ROLL ANGLE CHANNEL
22845C	CD6185	707	CALL	ADCO	; READ ADC CHANNEL
22845F	CDEB84	708	CALL	STORE	; PUT IN RAM BUFFER
22		709			
228462	3E10	710	MVI	A,16	;DELTA-RUDDER TRIM CHANNEL
228464	CD6185	711	CALL	ADCO	; READ ADC CHANNEL
228467	CDEB84	712	CALL	STORE	; PUT IN RAM BUFFER
22		713			
22846A	3E11	714	MVI	A,17	;DELTA-AILERON TRIM CHANNEL
22846C	CD6185	715	CALL	ADCO	; READ ADC CHANNEL
22846F	CDEB84	716	CALL	STORE	; PUT IN RAM BUFFER
22		717			
228472	3E12	718	MVI	A,18	;DELTA-ELEVATOR POSITION CHANNEL
228474	CD6185	719	CALL	ADCO	; READ ADC CHANNEL
228477	CDEB84	720	CALL	STORE	; PUT IN RAM BUFFER
22		721			
22847A	3E13	722	MVI	A,19	;DELTA-THROTTLE POSITION CHANNEL
22847C	CD6185	723	CALL	ADCO	; READ ADC CHANNEL

22B47F	CDEB84	724	CALL	STORE	;	PUT IN RAM BUFFER
22		725			;	
22B482	3E14	726	MVI	A,20	;	DELFL-FLAP POSIYION CHANNEL
22B484	CD6185	727	CALL	ADCO	;	READ ADC CHANNEL
22B487	CDEB84	728	CALL	STORE	;	PUT IN RAM BUFFER
22		729			;	
22B48A	3E16	730	MVI	A,22	;	DELA-AILERON POSITION CHANNEL
22B48C	CD6185	731	CALL	ADCO	;	READ ADC CHANNEL
22B48F	CDEB84	732	CALL	STORE	;	PUT IN RAM BUFFER
22		733			;	
22B492	3E17	734	MVI	A,23	;	DELRL-RUDDER POSITION CHANNEL
22B494	CD6185	735	CALL	ADCO	;	READ ADC CHANNEL
22B497	CDEB84	736	CALL	STORE	;	PUT IN RAM BUFFER
22		737			;	
22B49A	3E18	738	MVI	A,24	;	H1LOC-N1 LOCALISER CHANNEL
22B49C	CD6185	739	CALL	ADCO	;	READ ADC CHANNEL
22B49F	CDEB84	740	CALL	STORE	;	PUT IN RAM BUFFER
22		741			;	
22B4A2	3E1A	742	MVI	A,26	;	ALPHAP-PORT ALPHA CHANNEL
22B4A4	CD6185	743	CALL	ADCO	;	READ ADC CHANNEL
22B4A7	CDEB84	744	CALL	STORE	;	PUT IN RAM BUFFER
22		745			;	
22B4AA	3E1B	746	MVI	A,27	;	ALPHAS-STARBOARD ALPHA CHANNEL
22B4AC	CD6185	747	CALL	ADCO	;	READ ADC CHANNEL
22B4AF	CDEB84	748	CALL	STORE	;	PUT IN RAM BUFFER
22		749			;	
22B4B2	3E1C	750	MVI	A,28	;	LOCMLS-MLS LOCALIZER CHANNEL
22B4B4	CD6185	751	CALL	ADCO	;	READ ADC CHANNEL
22B4B7	CDEB84	752	CALL	STORE	;	PUT IN RAM BUFFER
22		753			;	
22B4BA	3E1D	754	MVI	A,29	;	GSMLS-MLS GLIDE SLOPE CHANNEL
22B4BC	CD6185	755	CALL	ADCO	;	READ ADC CHANNEL
22B4BF	CDEB84	756	CALL	STORE	;	PUT IN RAM BUFFER
22		757			;	
22B4C2	3E1E	758	MVI	A,30	;	LOCN2-N2 LOCALIZER CHANNEL
22B4C4	CD6185	759	CALL	ADCO	;	READ ADC CHANNEL
22B4C7	CDEB84	760	CALL	STORE	;	PUT IN RAMBUFER
22		761			;	
22B4CA	3E1F	762	MVI	A,31	;	IDELFL-FLAP COMMAND CHANNEL
22B4CC	CD6185	763	CALL	ADCO	;	READ ADC CHANNEL
22B4CF	CDEB84	764	CALL	STORE	;	PUT IN RAM BUFFER
22		765			;	
22B4D2	CD6385	766	CALL	DIGH	;	H
22B4D5	CDEB84	767	CALL	STORE	;	PUT IN RAM BUFFER
22		768			;	
22B4D8	CD6985	769	CALL	DIGLI	;	LIGHTS
22B4DB	CDEB84	770	CALL	STORE	;	PUT IN RAM BUFFER
22		771			;	
22B4DE	CD8D85	772	CALL	DIGMOD	;	MODE SWITCHES
22B4E1	CDEB84	773	CALL	STORE	;	PUT IN RAM BUFFER
22		774			;	
22B4E4	CD9385	775	CALL	DIGTIM	;	TIME
22B4E7	CDEB84	776	CALL	STORE	;	PUT IN RAM BUFFER
22B4EA	C9	777	CALL	RET		
22		778	STORE:			
22		779			;	
22		780			;	
22		781			;	
22		782			;	
22		783			;	
22		784			;	
22B4EB	F5	785	PUSH	PSW		
22B4EC	7D	786	MOV	A,L		
22B4ED	12	787	STAX	D		
22B4EE	13	788	INX	D		
22B4EF	7C	789	MOV	A,H		

TAKE CONTENTS OF HL REGISTER
STORE AT DOUBLE BYTE POINTED
TO BY DE REGISTER.

2284F0	12	790	STAX	D	
2284F1	13	791	INX	D	
2284F2	F1	792	POP	PSW	
2284F3	C9	793	RET		
22		794			;
22		795			;
22		796	URBUFS:		
22		797			;
22		798			;
22		799			;
22		800			;
22		801			;
22		802			;
22		803			;
22		804			;
22		805			;
22		806			;
22		807			;
22		808			;
22		809			;
22		810			;
22		811			;
22		812			;
22		813			;
22		814			;
2284F4	F5	815	PUSH	PSW	
2284F5	E5	816	PUSH	H	
2284F6	C5	817	PUSH	B	
2284F7	2A5988	818	LHLD	REMAIN	;
2284FA	014C00	819	LXI	B, BYTPERSEC	; BYTPERSEC BYTES FILLED PER SECOND
2284FD	AF	820	XRA	A	; CARRY=0
2284FE	ED42	821	DSBC	B	
228500	225988	822	SHLD	REMAIN	; REMAIN=REMAIN-BYTPERSEC
22		823			;
22		824			;
22		825			;
228503	AF	826	XRA	A	; CARRY=0
228504	ED42	827	DSBC	B	
228506	F23985	828	JP	ROOM	; IF S=0, HL >= BC
22		829			;
22		830			;
22		831			;
22		832			;
22		833			;
22		834			;
228509	CD9487	835	CALL	SETFULL	; MARK CURRENT BUFFER FULL
22		836			;
22850C	210008	837	LXI	H, 2048	
22850F	225988	838	SHLD	REMAIN	; REMAIN=2048
22		839			;
228512	3A5B88	840	LDA	FMHICB	; SWITCH TO NEXT BUFFER
228515	3C	841	INR	A	;
228516	325B88	842	STA	FMHICB	;
228519	FEDA	843	CPI	10	
22851B	C22D85	844	JNZ	SW	
22		845			;
22		846	HLT		;
22851E	3E00	847	MVI	A, 0	
228520	325B88	848	STA	FMHICB	
228523	110090	849	LXI	D, BUFF0	
228526	ED537688	850	SDED	CURRBUF	
22852A	C33985	851	JMP	ROOM	
22		852			;
22852D	2A7688	853	SW: LHLD	CURRBUF	; BASE ADDRESS OF CURRENT BUFFER
228530	010008	854	LXI	B, 2048	
228533	09	855	DAD	B	; INCREMENT BY 2048

228534	227688	856		SHLD	CURRBUF	;UPDATED BASE ADDRESS SAVED
228537	54	857		MOV	D,H	;AND PUT INTO
228538	5D	858		MOV	E,L	; THE DE PAIR
228539	C1	861	ROOM:	POP	B	
22853A	E1	862		POP	H	
22853B	F1	863		POP	PSW	
22853C	C9	864		RET		
22853D	F5	866	UINITS:	PUSH	PSW	
22853E	3A5E88	867		LDA	CNT	
228541	3C	868		INR	A	
228542	325E88	869		STA	CNT	
228545	F1	870		POP	PSW	
228546	C9	871		RET		
228547	F5	873	RINTS:	PUSH	PSW	
228548	3A5E88	874		LDA	CNT	
22854B	F60A	875		CPI	10	
22854D	C25385	876		JNZ	NOT10	
228550	3E00	877		MVI	A,0	
228552	325E88	878		STA	CNT	
228555	F1	880	NOT10:	POP	PSW	
228556	C9	881		RET		
228557	E5	883	UCLK:	PUSH	H	
228558	2A5C88	884		LHLD	TIM	
22855B	Z3	885		INX	H	
22855C	225C88	886		SHLD	TIM	
22855F	E1	887		POP	H	
228560	C9	888		RET		
228561	320130	890	ADCO:	STA	ADDAM+01H	
228564	3E01	891		MVI	A,01	
228566	320030	892		STA	ADDAM+00H	
228569	3A0030	893	BUSY	LDA	ADDAM+00H	
22856C	07	894		RLC		
22856D	026985	895		JNC	BUSY	
228570	2A0430	896		LHLD	ADDAM+04H	
228573	C9	897		RET		
228574	6F	899	CDCO:	MOV	L,A	
228575	2600	901		MVI	H,0	
228577	C9	902		RET		
228578	6F	904	BDCO:	MOV	L,A	
228579	3A5E88	905		LDA	CNT	
22857C	67	906		MOV	H,A	
22857D	C9	907		RET		
22857E	2E00	909	DNE:	MVI	L,0	
228580	2600	910		MVI	H,0	
228582	C9	911		RET		
228583	DBE4	915	DIGH:	IN	ALTPORT	;ALTIMETER READING
228585	6F	916		MOV	L,A	
228586	2600	917		MVI	H,0	
228588	C9	918		RET		
228589		919	DIGLI:			
228590		920		MVI	L,35	
228591		921		MVI	H,0	

2A5288	2A5288	922	LHLD	LIGHTS	
2A528C	C9	923	RET		
		924	DIGMOD:		
DBES	DBES	925	IN	PUSHPORT	
6F	6F	926	MOV	L,A	
2600	2600	927	MVI	H,0	
		928	; MVI	L,36	
		929	; MVI	H,0	
C9	C9	930	RET		
		931	DIGTIM:		
2A5C88	2A5C88	932	LHLD	TIM	
C9	C9	933	RET		
		934	STATE:		
		935	; THISMACHINE HAS TWO STATES		
		936	; STATE 0	THE MACHINE STAYS IN THIS STATE FOR 30 SECS.	
		937	; AFTER 30 SECS. ELAPSE, IT TURNS ON THE PROPER LIGHT		
		938	; AND SHIFTS TO STATE 1.		
		939	; STATE 1	THE MACHINE STAYS IN STATE 1 UNTIL THE PROPER	
		940	; PUSHBUTTON IS DEPRESSED. (LIGHT X GOES WITH PB X, ETC)		
		941	; THE CORRESPONDING LIGHT IS TURNED OFF AND THE		
		942	; MACHINE SHIFTS TO STATE 0.		
		943	; STATE 0	THE MACHINE STAYS IN THIS STATE FOR 30 SECS.	
F5	F5	944	PUSH	PSW	
E5	E5	945	PUSH	H	
C5	C5	946	PUSH	B	
3A4E88	3A4E88	947	LDA	ST	
B7	B7	948	ORA	A	;SET THE FLAGS
C2C185	C2C185	949	JNZ	STATE1	
		950	STATE0:		
212C01	212C01	951	LXI	H,THSEDY	;LOAD THE NUMBER OF TIMER CLICKS NEEDED FOR 30 SEC
AF	AF	952	XRA	A	;CLEAR CARRY
ED4B5088	ED4B5088	953	LBCD	PTIM	
ED42	ED42	954	DSEC	B	
C2B785	C2B785	955	JNZ	BPTIM	
CDDA85	CDDA85	956	CALL	TONL	
CD3D86	CD3D86	957	CALL	TONS	;STATE=1
C3D485	C3D485	958	JMP	BACK	
		959	BPTIM:		
2A5088	2A5088	960	LHLD	PTIM	
23	23	961	INX	H	
225088	225088	962	SHLD	PTIM	
C3D485	C3D485	963	JMP	BACK	
		964	STATE1:		
CD2586	CD2586	965	CALL	PB	;RETURN PUSHBUTTON STATUS IN Z FLAG
C2D485	C2D485	966	JNZ	BACK	
		967	PBON:		
CDFB85	CDFB85	968	CALL	TOFFL	;TURN OFF LITE
CD4586	CD4586	969	CALL	TOFFS	;STATE=0
CD1C86	CD1C86	970	CALL	CPTIM	;PTIM = 0
CD5C86	CD5C86	971	CALL	SMPFLITE	;SWITCH TO NEXT PUSHBUTTON + LITE SET
C3D485	C3D485	972	JMP	BACK	
		973	BACK:		
C1	C1	974	POP	B	
E1	E1	975	POP	H	
F1	F1	976	POP	PSW	
C9	C9	977	RET		
		978	TONL:		
F5	F5	979	PUSH	PSW	
3A5488	3A5488	980	LDA	BINRY	
FE00	FE00	981	CPI	0	
C2EF85	C2EF85	982	JNZ	ON2	
3A5288	3A5288	983	LDA	LIGHTS	
E6FE	E6FE	984	ANI	OFFH	
D3C5	D3C5	985	OUT	LITEPORT	;BIT 0 PORT B 5 VOLTS
325288	325288	986	STA	LIGHTS	
F1	F1	987	POP	PSW	

2285EE	C9	988		RET	
22		989	DN2:		
2285EF	3A5288	990		LDA	LIGHTS
2285F2	E6FD	991		ANI	02H ;
2285F4	D3C5	992		OUT	LITEPORT ;BIT 1 PORT B 5 VOLTS
2285F6	325288	993		STA	LIGHTS
2285F9	F1	994		POP	PSW
2285FA	C9	995		RET	
22		996	TUFFL:		
2285FB	F5	997		PUSH	PSW
2285FC	3A5688	998		LDA	BINRY
2285FF	FE00	999		CPI	0
228601	C21086	1000		JNZ	OFF2
228604	3A5288	1001		LDA	LIGHTS
228607	F601	1002		ORI	01H ;
228609	D3C5	1003		OUT	LITEPORT ;BIT 0 PORT B 0 VOLTS
22860B	325288	1004		STA	LIGHTS
22860E	F1	1005		POP	PSW
22860F	C9	1006		RET	
22		1007	OFF2:		
228610	3A5288	1008		LDA	LIGHTS ;
228613	F602	1009		ORI	02H
228615	D3C5	1010		OUT	LITEPORT ;BIT 0 PORT B 0 VOLTS
228617	325288	1011		STA	LIGHTS
22861A	F1	1012		POP	PSW
22861B	C9	1013		RET	
22		1014	CPTIM:		
22861C	E5	1015		PUSH	H
22861D	210000	1016		LXI	H,0
228620	225088	1017		SHLD	PTIM ;CLEAR PTIM
228623	E1	1018		POP	H
228624	C9	1019		RET	
22		1020	PB:		
228625	3A5688	1021		LDA	BINRY
228628	FE00	1022		CPI	0
22862A	C23586	1023		JNZ	PB2
22862D	D8E5	1024		IN	PUSHPORT ;PUSHBUTTON STATUS
22862F	325488	1025		STA	MODES
228632	E601	1026		ANI	01H ;BIT 0 PORT B
228634	C9	1027		RET	;STATUS RETURNED IN Z FLAG
22		1028	PB2:		
228635	D8E5	1029		IN	PUSHPORT
228637	325488	1030		STA	MODES
22863A	E602	1031		ANI	02H ;BIT 1 PORT B
22863C	C9	1032		RET	
22		1033	TONS:		
22863D	F5	1034		PUSH	PSW
22863E	3E01	1035		MVI	A,01H ;
228640	324E88	1036		STA	ST ;STATE=1
228643	F1	1037		POP	PSW
228644	C9	1038		RET	
22		1039	TOFFS:		
228645	F5	1040		PUSH	PSW
228646	3E00	1041		MVI	A,0
228648	324E88	1042		STA	ST
22864B	F1	1043		POP	PSW
22864C	C9	1044		RET	
22		1045	FLIP:		
22		1046			;TOGGLE LIGHT 3, TOGGLE LIGHT 4 TOGETHER
22864D	F5	1047		PUSH	PSW
22864E	3A5288	1048		LDA	LIGHTS
228651	EE04	1049		XRI	04H ;FLIP BIT 2
228653	EE08	1050		XRI	08H ;FLIP BIT 3
228655	325288	1051		STA	LIGHTS
228658	D3C5	1052		OUT	LITEPORT
22865A	F1	1053		POP	PSW

22865B	C9	1054	RET		
22		1055	SMPBLITE:		
22		1056	;	IF YOU ARE USING PBO AND LITE0,	
22		1057	;	USE PBI AND LITE1.	
22		1058	;	IF YOU ARE USING PBI AND LITE1,	
22		1059	;	USE PBO AND LITE0.	
22		1060	;		
22865C	F5	1061	PUSH	PSW	
22865D	3A5688	1062	LDA	BINRY	
228660	EE01	1063	XRI	01H	
228662	325688	1064	STA	BINRY	
228665	F1	1065	POP	PSW	
228666	C9	1066	RET		
22		1067	CTIM:		
228667	ES	1068	PUSH	H	
228668	210000	1069	LXI	H,0	HL=0
228668	225C88	1070	SHLD	TIM	SECOND COUNTER = 0
22866E	E1	1071	POP	H	
22866F	C9	1072	RET		
22		1073	SETCDIG:		
22		1074	;		
22		1075	;	SET DIGIT COUNTER CNTDIG	
22		1076	;		
228670	F5	1077	PUSH	PSW	
228671	3E00	1078	MVI	A,0	
228673	324D88	1079	STA	CNTDIG	CNTDIG=0
228676	F1	1080	POP	PSW	
228677	C9	1081	RET		
22		1082	INTMODIG:		
228678	ES	1083	PUSH	H	
228679	CS	1084	PUSH	B	
22867A	D5	1085	PUSH	D	
22		1086			CHECK TO SEE IF THERE IS
22		1087			A TWO DIGIT INPUT READY
22		1088			
22		1089			IF THERE IS NOT,
22		1090			RETURN WITH Z SET
22		1091			
22		1092			IF THERE IS,
22		1093			RETURN WITH Z RESET
22		1094			
22		1095			
22867B	CDB186	1096	CALL	DI	GET DIGIT IF WAITING
22867E	CAAD86	1097	JZ	INPUTR	IF Z SET, NOTHING WAITING
22		1098	;		
22		1099	;		
22		1100			Z NOT SET, SO DIGIT IN ACC
228681	E60F	1101	ANI	0FH	CONVERT ASCII DIGIT TO BINARY DIGIT
22		1102	CALL	HMNP	
22		1103	CALL	CRLF	
228683	57	1104	MOV	D,A	SAVE DIGIT IN D
228684	3A4D88	1105	LDA	CNTDIG	CNTDIG IS DIGIT COUNTER
228687	3C	1106	INR	A	
228688	324D88	1107	STA	CNTDIG	
22868B	FE02	1108	CPI	02H	
22868D	CA9886	1109	JZ	INPUTE	IF Z SET, COUNT IS 2
22		1110	;		
22		1111	;		
22		1112			HAVE INPUT IN D, SAVE IN B
228690	7A	1113	MOV	A,D	
228691	324B88	1114	STA	INPUTS	SAVE FIRST INPUT DIGIT
228694	AF	1115	XRA	A	Z IS SET
228695	C3AD86	1116	JMP	INPUTR	
22		1117	INPUTE:		
228698	3A4B88	1118	LDA	INPUTS	MOVE FIRST INPUT DIGIT IN ACC
22869B	07	1119	RLC		

22869C	07	1120	RLC		
22869D	07	1121	RLC		
22869E	47	1122	MOV	B,A	;(B)=8*(INPUTS)
22869F	3A4B88	1123	LDA	INPUTS	;
2286A2	87	1124	ADD	A	;(A)=2*(INPUTS)
2286A3	80	1125	ADD	B	;(A)=2*(INPUTS)+8*(INPUTS)=10*(INPUTS)
2286A4	82	1126	ADD	D	;ADD IN SECOND INPUT DIGIT
2286A5	324C88	1127	STA	TWODIG	
2286A8	3E00	1128	MVI	A,0	
2286AA	324D88	1129	STA	CNTDIG	;CLEAR THE COUNTER
22		1130	INPUTR:		
2286AD	D1	1131	POP	D	
2286AE	C1	1132	POP	B	
2286AF	E1	1133	POP	H	
2286B0	C9	1134	RET		
22		1135	DI:		
22		1136	;		ACC AND FLAGS ARE CHANGED
22		1137	;		GET INPUT IF WAITING
22		1138	;		OTHERWISE RETURN WITH Z SET
22		1139	;		
22		1140	;		SEE IF INPUT IS ADECIMAL DIGIT,
22		1141	;		IF NOT RETURN WITH Z SET
22		1142	;		
22		1143	;		IF INPUT IS A DECIMAL DIGIT,
22		1144	;		ECHO IT AND RETURN IN ACC
22		1145	;		
22		1146	;		
2286B1	DBCD	1147	IN	S8251	
2286B3	E602	1148	ANI	RXR0Y	;IS THERE INPUT DATA YET
2286B5	CB	1149	RZ		;IF Z IS SET, RETURN
22		1150	;		
22		1151	;		READ THE CHAR
22		1152	;		
2286B6	DBCC	1153	IN	D8251	;GET CHAR
2286B8	E67F	1154	ANI	07FH	; CHOP OFF PARITY
22		1155	;		
22		1156	;		TEST FOR DIGIT FROM 0 TO 9
22		1157	;		
2286BA	FE30	1158	CPI	30H	; COMPARE WITH ASCII 0
2286BC	FAC886	1159	JM	DINODIG	; JUMP IF LESS THAN
2286BF	FE3A	1160	CPI	3AH	;COMPARE WITH ASCII COLON
2286C1	F2C886	1161	JP	DINODIG	; JUMP IF GREATER OR EQUAL
2286C4	CD0B88	1162	CALL	CD	;HAVE LEGAL DIGIT IN ACC, Z IS RESET
2286C7	C9	1163	RET		
22		1164	;		
22		1165	;		
22		1166	DINODIG:		
2286C8	AF	1167	XRA	A	;Z IS SET
2286C9	C9	1168	RET		
22		1169	DISPLAY:		
2286CA	F5	1170	PUSH	PSW	
2286CB	E5	1171	PUSH	H	
2286CC	CS	1172	PUSH	B	
22		1173			;DISPLAY MEMORY LOCATION
22		1174			;CORRESPONDING TO TWODIG ADDRESS
22		1175			;
2286CD	3A5E88	1176	LDA	CNT	;INTERRUPT COUNT LOADED IN ACC
2286D0	FE09	1177	CPI	9	; IS THIS THE NINTH INTERRUPT
2286D2	C2F386	1178	JNZ	DISPLAYR	; RETURN IF NOT NINE
22		1179			;
22		1180			;
2286D5	3A4C88	1181	LDA	TWODIG	;LOAD TWO DIGIT NUMBER
2286D8	FE00	1182	CPI	0	; IF IT IS ZERO, NOTHING TO DISPLAY YET
2286DA	CAF386	1183	JZ	DISPLAYR	; SO RETURN
22		1184			;
22		1185			;

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2286DD 87      1186      ADD      A      ;FORM BYTE OFFSET IN ACC
2286DE D602    1187      SUI      2      ; VALUE OF 1 IS AN OFFSET OF ZERO
;
;
2286E0 2600    1189      MVI      H,0    ;MOVE ACC OFFSET
2286E2 6F      1190      MOV      L,A    ; HL HAS ACC OFFSET
2286E3 ED4B5788 1191      LBCD     SAVEDE ; BASE ADDRESS OF CURRENT STORAGE IN BC
2286E7 09      1192      DAD      B      ;
;
;
;
;
2286E8 CD2A87    1195      CALL     CRLF
2286EB CDF786    1196      CALL     HDMP2  ;
;
;
;
22      1198
22      1199      ; CALL     CRLF
22      1200      ; LDA      TWODIG
22      1201      ; CALL     HDMP
22      1202      ; CALL     CRLF
22      1203      ; LXI     H,SAVEDE
22      1204      ; CALL     HDMP2
22      1205      ; CALL     CRLF
2286EE 3E00    1206      MVI      A,0    ;ZERO
2286F0 324C88    1207      STA     TWODIG ; TWODIG
;
;
;
22      1209
22      1210      DISPLAY:
2286F3 C1      1211      POP     B
2286F4 E1      1212      POP     H
2286F5 F1      1213      POP     PSM
2286F6 C9      1214      RET
;
;
; DUMP THE CONTENTS OF MEMORY IN HEX
; H HOLDS STARTING ADDRESS OF DUMP
; A REG IS USED IN HDMP
22      1215
22      1216
22      1217
HDMP2: 2286F7 F5      1218      PUSH    PSM
2286F8 E5      1219      PUSH    H
2286F9 23      1220      INX     H
2286FA 7E      1221      MOV     A,H
2286FB CD0987    1222      CALL    HDMP
2286FE 2B      1223      DCX     H
2286FF 7E      1224      MOV     A,H
228700 CD0987    1225      CALL    HDMP
228703 CD2A87    1226      CALL    CRLF
228706 E1      1227      POP     H
228707 F1      1228      POP     PSM
228708 C9      1229      RET
;
;
; HDMP USES THE A REG
;SAVE ACC
; TWICE
;ISOLATE THE HIGH ORDER NYBBLE
228709 F5      1231      HDMP:  PUSH    PSM
22870A F5      1232      PUSH    PSM
22870B E6F0    1233      ANI     OFCH
22870D 0F      1234      RRC
22870E 0F      1235      RRC
22870F 0F      1236      RRC
228710 0F      1237      RRC
;HI DIG SHIFTED RIGHT BY 4
;PRINT HIGH ORDER DIGIT
228711 CD2287    1238      CALL    BINHE
228714 CD0B88    1239      CALL    CO      ;PRINT ASCII FORM OF HIGH DIGIT
228717 F1      1240      POP     PSM     ;RESTORE THE ACC TO VALUE AT ENTRY
;ISOLATE THE LOW ORDER NYBBLE
228718 E60F    1241      ANI     OFH
22871A CD2287    1242      CALL    BINHE
;
;
;
22871D CD0B88    1243      CALL    CO
228720 F1      1244      POP     PSM
228721 C9      1245      RET
;
;
;
;
228722 C630    1246      BINHE:  ADI     30H
228724 FE3A    1247      CPI     3AH
;
;
228726 D8      1248      RC
228727 C607    1249      ADI     7H
228729 C9      1250      RET
;
;
;
;
22      1251      ; CRLF USES ONLY THE AREG

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22872A F5      1252  CRLF:  PUSH  PSW
22872B 3E0D    1253      MVI  A,0DH
22872D CD0B88  1254      CALL CD
228730 3E0A    1255      MVI  A,0AH
228732 CD0B88  1256      CALL CD
228735 F1      1257      POP  PSW
228736 C9      1258      RET
22          1259  ;DATAOVRUN:
22          1260  ; ARE WE FILLING FASTER THAN WE ARE EMPTYING
22          1261  ;   PUSH  PSW
22          1262  ;   PUSH  B
22          1263  ;   LDA  BHIHCB
22          1264  ;   MOV  B,A
22          1265  ;   LDA  FHIHCB
22          1266  ;   CMP  B
22          1267  ;   JNZ  D1
22          1268  ;
22          1269  ;   MVI  A,'0'
22          1270  ;   CALL BO
22          1271  ;   HLT
22          1272  ;D1:
22          1273  ;   POP  B
22          1274  ;   POP  PSW
22          1275  ;   RET
22          1276  ;VALIDMP:
22          1277  ; LET THE FILLER CATCHUP WITH EMPTIER
22          1278  ;   PUSH  PSW
22          1279  ;   PUSH  B
22          1280  ;   LDA  FILLONE
22          1281  ;   CPI  0
22          1282  ;   JNZ  V1
22          1283  ;
22          1284  ;V2:  LDA  FHIHCB
22          1285  ;   CPI  0
22          1286  ;   MVI  A,'W'
22          1287  ;   CALL CD
22          1288  ;   JZ   V2
22          1289  ;
22          1290  ;   MVI  A,1
22          1291  ;   STA  FILLONE
22          1292  ;V1:
22          1293  ;
22          1294  ;   LDA  BHIHCB
22          1295  ;   MOV  B,A
22          1296  ;   LDA  FHIHCB
22          1297  ;   CMP  B
22          1298  ;   LDA  FHIHCB
22          1299  ;   ADI  30H
22          1300  ;   CALL CD
22          1301  ;   JZ   V1
22          1302  ;   POP  B
22          1303  ;   POP  PSW
22          1304  ;   RET
22          1305  INITSEMA:
22          1306  ;
22          1307  ;MARK ALL BUFFERS EMPTI
228737 F5      1307      PUSH  PSW
228738 C5      1308      PUSH  B
228739 E5      1309      PUSH  H
22873A 216A88  1310      LXI  H,SEMAPHORE
22873D 060A    1311      MVI  B,10
22873F 3645    1312  S1:  MVI  M,'E'
228741 23      1313      INX  H
228742 05      1314      DCR  B
228743 C23F87  1315      JNZ  S1
228746 E1      1316      POP  H
228747 C1      1317      POP  B

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008748	F1	1318	POP	PSW	
008749	C9	1319	RET		
00		1320	TSTFULL:		
00		1321			;WAIT UNTIL BUFFER EMPTY (INFINITE LOOP!)
00874A	F5	1322	PUSH	PSW	
00874B	C5	1323	PUSH	B	
00874C	E5	1324	PUSH	H	
00874D	216A88	1325	LXI	H,SEMAPHORE	
008750	3A5B88	1326	LDA	FMHICB	
008753	0600	1327	MVI	B,0	
008755	4F	1328	MOV	C,A	
008756	09	1329	DAD	B	; (HL) := SEMAPHORE+(FMHICB)
008757	7E	1330	MOV	A,H	; (A) := (SEMAPHORE+(FMHICB))
008758	FE46	1331	CPI	'F'	;SEE IF BUFFER FULL
00875A	CC6187	1332	CZ	OVRUN	;WAIT TIL EMPTY
00875D	E1	1333	POP	H	
00875E	C1	1334	POP	B	
00875F	F1	1335	POP	PSW	
008760	C9	1336	RET		
00		1337	OVRUN:		
008761	3E4F	1338	MVI	A,'O'	
008763	CD0B88	1339	CALL	CD	
008766	3E56	1340	MVI	A,'V'	
008768	CD0B88	1341	CALL	CD	
00876B	3A5B88	1342	LDA	FMHICB	
00876E	C641	1343	ADI	'A'	
008770	CD0B88	1344	CALL	CD	
008773	C30000	1345	JMP	0	
00		1346	TSTEMPTY:		
00		1347			;WAIT UNTIL BUFFER FULL
008776	F5	1348	PUSH	PSW	
008777	C5	1349	PUSH	B	
008778	E5	1350	PUSH	H	
008779	216A88	1351	LXI	H,SEMAPHORE	
00877C	3A6888	1352	LDA	EMHICB	
00877F	0600	1353	MVI	B,0	
008781	4F	1354	MOV	C,A	
008782	09	1355	DAD	B	
008783	7E	1356	MOV	A,H	; (A) := (SEMAPHORE+(EMHICB))
008784	FE45	1357	CPI	'E'	;SEE IF BUFFER EMPTY
008786	F5	1358	PUSH	PSW	;SAVE Z FLAG
008787	3A6888	1359	LDA	EMHICB	
00878A	C630	1360	ADI	'0'	;CONVERT TO ASCII
00		1361	CALL	CD	
00878C	F1	1362	POP	PSW	;RESTORE Z FLAG
00878D	CA8387	1363	JZ	EMPTY1	;WAIT UNTIL FULL
008790	E1	1364	POP	H	
008791	C1	1365	POP	B	
008792	F1	1366	POP	PSW	
008793	C9	1367	RET		
00		1368	SETFULL:		
00		1369			;MARK BUFFER FULL
008794	F5	1370	PUSH	PSW	
008795	C5	1371	PUSH	B	
008796	E5	1372	PUSH	H	
008797	216A88	1373	LXI	H,SEMAPHORE	
00879A	3A5B88	1374	LDA	FMHICB	
00879D	0600	1375	MVI	B,0	
00879F	4F	1376	MOV	C,A	; (BC) := (FMHICB)
0087A0	09	1377	DAD	B	; (HL) := SEMAPHORE+(FMHICB)
0087A1	3E46	1378	MVI	A,'F'	;MARK IT FULL
0087A3	77	1379	MOV	H,A	; (SEMAPHORE+(FMHICB)) := 'F'
0087A4	E1	1380	POP	H	
0087A5	C1	1381	POP	B	
0087A6	F1	1382	POP	PSW	
0087A7	C9	1383	RET		

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LL      1384  SETEMPTY:
LL      1385                                ;MARK BUFFER EPTY
LL87A8  F5    1386      PUSH   PSW
LL87A9  C5    1387      PUSH   B
LL87AA  E5    1388      PUSH   H
LL87AB  216A88 1389      LXI    H,SEMAPHORE
LL87AE  3A6888 1390      LDA    EWHICHB
LL87B1  0600   1391      MVI    B,0
LL87B3  4F    1392      MOV    C,A          ;(BC)=(EWHICHB)
LL87B4  09    1393      DAD    B          ;(HL)=(SEMAPHORE+(EWHICHB))
LL87B5  3E45   1394      MVI    A,'E'      ;MARK IT EMPTY
LL87B7  77    1395      MOV    M,A          ;(SEMAPHORE+(EWHICHB))='E'
LL87B8  E1    1396      POP    H
LL87B9  C1    1397      POP    B
LL87BA  F1    1398      POP    PSW
LL87BB  C9    1399      RET

LL      1400  INITRE:
LL87BC  CD7086 1401      CALL  SETDIG   ;ZERO DIGIT COUNTER, CNTDIG
LL87BF  CD2783 1402      CALL  CNTR0
LL87C2  CD1683 1403      CALL  CNTR1
LL87C5  3E0A   1404      MVI    A,10
LL87C7  326188 1405      STA   FLAG
LL87CA  3E80   1406      MVI    A,80H      ;FORMAT 8255 AS MODE 0,
LL87CC  D3EB   1407      OUT   0EBH      ; ALL THREE PORTS OUTPUT ON J-2 8004
LL87CE  110090 1408      LXI    D,BUFF0   ; SAVEDE POINTER =
LL87D1  ED535788 1409      SDED  SAVEDE    ; SET TO BASE ADDRESS OF ALL TEN BUFFERS
LL87D5  3E00   1410      MVI    A,00H      ; POINTER THAT TELLS WHICH BUFFER
LL87D7  325B88 1411      STA   FWHICHB   ; IS BEING FILLED = 0
LL87DA  210008 1412      LXI    H,2048   ;COUNTER TO TELL HOW MUCH
LL87DD  225988 1413      SHLD  REMAIN    ; OF A BUFFER IS UNFILLED.
LL87E0  110090 1414      LXI    D,BUFF0   ; POINTER TO BASE ADDRESS OF CURRENT
LL87E3  210000 1415      LXI    H,0       ;ZERO OUT
LL87E6  225E88 1416      SHLD  CNT       ; INTERRUPT COUNTER
LL87E9  ED537688 1417      SDED  CURRBUF   ; BUFFER BEING FILLED
LL      1418      ; MVI    A,0
LL      1419      ; STA   FILLONE ;FILLONE=0, MEANS ALL BUFFERS ARE EMPTY
LL      1420      ; OF DATA.
LL87ED  3E80   1421      MVI    A,080H
LL87EF  D3C7   1422      OUT   LITECTRL  ;FORMAT LIGHTS
LL87F1  3E9B   1423      MVI    A,09BH
LL87F3  D3E7   1424      OUT   J18004    ;FORMAT PUSHBUTTONS.
LL87F5  3EFF   1425      MVI    A,0FFH    ;TURN OFF LIGHTS
LL87F7  D3C5   1426      OUT   LITEPORT
LL87F9  325288 1427      STA   LIGHTS    ; SAVE LIGHT STATUS
LL87FC  CD4586 1428      CALL  TOFFS     ;STATE=0
LL87FF  CD1C86 1429      CALL  CPTIM     ;PTIM=0
LL8802  CD6786 1430      CALL  CTIM      ;CLEAR SECOND COUNTER
LL8805  3E00   1431      MVI    A,0
LL8807  325688 1432      STA   BINRY     ;BINRY=0, PBO AND LITEO FIRST
LL880A  C9    1433      RET

LL      1434  ;*****
LL      1435  ; CHARACTER OUTPUT ROUTINE
LL      1436  ; CO OUTPUTS ONE CHARACTER FROM ACC TO TERMINAL
LL      1437  ; VIA THE USART. ALL REGISTERS AND FLAGS ARE
LL      1438  ; PRESERVED. THE CHARACTER IT OUTPUTS IS IN THE ACC.
LL      1439  ;*****
LL880B  F5    1440  CO:  PUSH   PSW
LL880C  C5    1441      PUSH   B
LL880D  4F    1442      MOV    C,A      ;SAVE A REG
LL880E  00    1443  COO:  NOP        ;DELAY
LL880F  00    1444      NOP
LL8810  1E0B  1445      IN     00251    ;GET USART STATUS
LL8812  E901  1446      ANI   0001     ;CHECK TRANSMIT READY FLAG
LL8814  0001  1447      JZ    0001     ;IF READY
LL8817  00    1448      NOP
LL8818  00    1449      NOP

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228819 00      1450      NOP
22881A 00      1451      NOP
22881B 79      1452      MOV      A,C      ;READY TO TRANSMIT , RESTORE CHAR TO A REG
22881C D3CC     1453      OUT      D8251    ;SEND IT
22881E C1      1454      POP      B
22881F F1      1455      POP      PSM
228820 C9      1456      RET
22      1457      INITUSART:
228821 CD2B88 1458      CALL     RUSART   ;MASTER RESET SEQUENCE
228824 CD3C88 1459      CALL     MUSART   ;SET MODE IN USART
228827 CD4388 1460      CALL     CUSART   ;SET COMMAND IN USART
22882A C9      1461      RET
22882B 3E80     1462      RUSART: MVI      A,80H  ;RESET 8251
22882D D3CD     1463      OUT      C8251    ;
22882F E3      1464      XTHL
228830 E3      1465      XTHL
228831 D3CD     1466      OUT      C8251
228833 E3      1467      XTHL
228834 E3      1468      XTHL
228835 3E40     1469      MVI      A,40H   ;
228837 D3CD     1470      OUT      C8251   ;
228839 E3      1471      XTHL
22883A E3      1472      XTHL
22883B C9      1473      RET
22883C 3E4E     1474      MUSART: MVI      A,USMODE
22883E D3CD     1475      OUT      C8251
228840 E3      1476      XTHL
228841 E3      1477      XTHL
228842 C9      1478      RET
228843 3E37     1479      CUSART: MVI      A,USCMD  ;REST ERROR FLAGS
22      1480      ;      ENABLE TRANSMIT
22      1481      ;      ENABLE RECIEVE
22      1482      ;      READY DATA SET
22      1483      ;
22      1484      ;
228845 D3CD     1485      OUT      C8251 ;GIVE COMMAND
228847 E3      1486      XTHL
228848 E3      1487      XTHL
228849 C9      1488      RET
22884A C9      1489      RET
22      1490      ;
22004C      1491      BYTPERSEC EDU 2*38  ; HOW MANY BYTES PER SEC OF DATA
22012C      1492      TSEBY: EDU 300    ;NUMBER OF TIMER CLICKS NEEDED FOR 30 DELAY
22      1493      ;300 FOR .1 SEC TIMER CLICKS
22      1494      ;150 FOR .2 SEC TIMER CLICKS
220010      1495      TLOW EDU 010H    ;
220027      1496      THIGH EDU 027H   ;2710H=100000
22      1497      ;TLOW EDU 020H   ;
22      1498      ;THIGH EDU 04EH  ;4E20H=200000
22004E      1499      USMODE: EDU 04EH  ;
220037      1500      USCMD: EDU 037H  ;
22884B 00      1501      INPUTS: DB 0
22884C 00      1502      TMODIG: DB 0
22884D 00      1503      ONTDIG: DB 0
2200CD      1504      S8251 EDU 0CDH
2200CD      1505      C8251 EDU S8251
2200CC      1506      D8251 EDU 0CCH
220002      1507      RORDY EDU 02H
220001      1508      TXRDY EDU 01H
22884E 0000    1509      ST: DW 0
228850 0000    1510      PTIH: DW 0
228852 0000    1511      LIGHTS: DW 0
228854 0000    1512      MODES: DW 0
228856 00      1513      BINRY: DB 0
228857 0090    1514      SAVEDE: DW BUFFO
228859 0008    1515      REMAIN: DW 2048

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22885B	00	1516	FMICB: DB	0	;FILL WHICH BUFFER
22885C	0000	1517	TIN: DM	0	
22885E	0000	1518	CNT: DM	0	
228860	00	1519	FILLONE: DB	0	
228861	00	1520	FLAG: DB	0	
228862	0000	1521	SAVE: DM	0	
228864	0000	1522	SAV: DM	0	
228866	0000	1523	EREMAIN: DM	0	
228868	00	1524	EMICB: DB	0	;EMPTY WHICH BUFFER
228869	00	1525	TSW: DB	0	
22886A	4545454545	1526	SEMAPHORE:	DB	'EEEEEEEE' ;TEN BUFFER SEMAPHORES ALL 'E'
22	4545454545				
228874	0000	1527	EDURBUF: DM	0	
228876	0090	1528	CURRBUF: DM	0	BUFFO
228878	0000	1529	TEMPDE: DM	0	
22		1530	AVG:		
22887A	F5	1531		PUSH	PSW
22887B	E5	1532		PUSH	H
22887C	C5	1533		PUSH	B
22887D	D5	1534		PUSH	D
22887E	DDE5	1535		PUSHX	
228880	FDE5	1536		PUSHY	
228882	3A5E88	1537		LDA	CNT ;
228885	FE00	1538		CPI	0
228887	C29688	1539		JNZ	AVG1
22		1540	; ;	MVI	A,'1'
22		1541	; ;	CALL	CO
22888A	CDE388	1542		CALL	PART1
22888D	FDE1	1543		POPY	
22888F	DDE1	1544		POPX	
228891	D1	1545		POP	D
228892	C1	1546		POP	B
228893	E1	1547		POP	H
228894	F1	1548		POP	PSW
228895	C9	1549		RET	
228896	FE09	1550	AVG1:	CPI	9
228898	C2A788	1551		JNZ	AVG2
22889B	CDFA88	1552		CALL	PART3
22889E	FDE1	1553		POPY	
2288A0	DDE1	1554		POPX	
2288A2	D1	1555		POP	D
2288A3	C1	1556		POP	B
2288A4	E1	1557		POP	H
2288A5	F1	1558		POP	PSW
2288A6	C9	1559		RET	
2288A7	CD8C88	1560	AVG2:	CALL	PART2
2288AA	FDE1	1561		POPY	
2288AC	DDE1	1562		POPX	
2288AE	D1	1563		POP	D
2288AF	C1	1564		POP	B
2288B0	E1	1565		POP	H
2288B1	F1	1566		POP	PSW
2288B2	C9	1567		RET	
22		1568	PART1		
2288B3	21A68A	1569		LXI	H,432
2288B6	013000	1570		LXI	B,48
2288B9	CDF489	1571		CALL	CLEAR
22		1572	PART2:		
22		1573	; ;	MVI	A,'2'
22		1574	; ;	CALL	CO
22		1575	; ;	CALL	CRLF
2288BC	AF	1576		XRA	A
2288BD	32888A	1577		STA	ITER
22		1578	TP1:		
22		1579	; ;	CALL	PORTAOFF
2288C0	DB215788	1580		LXIX	PNTA16

LL88C4	FD21888A	1581	LXIY	ITER	
LL88C8	CDBF89	1582	CALL	LD2BCDE	; (BCDE):=(A16(ITER))
LL		1583	CALL	WBCDE	; DUMP BCDE REGISTERS
LL		1584			
LL88CB	CD4D89	1585	CALL	DSTACK	; PUT(BCDE) ONTO 32 BIT STACK
LL88CE	DD21A68A	1586	LXIX	A32	
LL88D2	FD21888A	1587	LXIY	ITER	
LL88D6	CD8B89	1588	CALL	LD4BCDE	; (BCDE):=(A32(ITER))
LL		1589	CALL	WBCDE	; DUMP BCDE REGISTERS
LL88D9	CD4D89	1590	CALL	DSTACK	
LL88DC	CD7189	1591	CALL	FIXADD	
LL88DF	CD5F89	1592	CALL	UDSTACK	; (BCDE):=RESULT OF 32BIT INTEGER ADD
LL		1593	CALL	WBCDE	; DUMP BCDE REGISTERS
LL88E2	DD21A68A	1594	LXIX	A32	
LL88E6	FD21888A	1595	LXIY	ITER	
LL88EA	CDA389	1596	CALL	ST4BCDE	; (A32(ITER)):= (BCDE)
LL		1597	LDA	ITER	
LL		1598	CALL	HDMF	
LL		1599	CALL	CRLF	
LL88ED	3A888A	1600	LDA	ITER	; CHECK ITERATION COUNT
LL88F0	3C	1601	INR	A	
LL88F1	32888A	1602	STA	ITER	
LL88F4	FEOC	1603	CPI	12	
LL88F6	C2C088	1604	JNZ	TP1	
LL		1605	CALL	PORTA0N	
LL88F9	C9	1606	RET		
LL		1607			
LL88FA	AF	1608	XRA	A	
LL88FB	32888A	1609	STA	ITER	
LL		1610			
LL88FE	DD215788	1611	LXIX	PNTA16	
LL8902	FD21888A	1612	LXIY	ITER	
LL8906	CDBF89	1613	CALL	LD2BCDE	; (BCDE):=(A16(ITER))
LL8909	CD4D89	1614	CALL	DSTACK	; (BCDE) ONTO 32 BIT STACK OF T9511
LL890C	DD21A68A	1615	LXIX	A32	
LL8910	FD21888A	1616	LXIY	ITER	
LL8914	CD8B89	1617	CALL	LD4BCDE	; (BCDE):=(A32(ITER))
LL8917	CD4D89	1618	CALL	DSTACK	; (BCDE) ONTO 32 BIT STACK OF T9511
LL891A	CD7189	1619	CALL	FIXADD	; ADD 32 BIT INTEGERS TOGETHER
LL891D	110A00	1620	LXI	D,10	
LL8920	010000	1621	LXI	B,0	
LL8923	CD4D89	1622	CALL	DSTACK	
LL8926	CD7E89	1623	CALL	FIXDIV	; DIVIDE BY TEN
LL8929	CD5F89	1624	CALL	UDSTACK	; (BCDE) HAS AVERAGE OF TEN VALUES
LL892C	DD215788	1625	LXIX	PNTA16	
LL8930	FD21888A	1626	LXIY	ITER	
LL8934	CD8989	1627	CALL	ST2BCDE	; (BCDE):=(A16(ITER))
LL8937	3A888A	1628	LDA	ITER	; CHECK ITERATION COUNT
LL893A	3C	1629	INR	A	
LL893B	32888A	1630	STA	ITER	
LL893E	FEOC	1631	CPI	12	
LL8940	C2FE88	1632	JNZ	TP2	
LL8943	C9	1633	RET		
LL		1634			
LL8944	F5	1635			
LL8945	DB05	1636	T95BUSY:	PUSH	PSW
LL8947	B7	1637	T95BUSY1:	IN	T9511CTRLPORT
LL8948	FA4589	1638		ORA	A
LL894B	F1	1639		JM	T95BUSY1
LL894C	C9	1640		POP	PSW
LL		1641		RET	
LL894D	F5	1642	DSTACK:		
LL894E	CD4489	1643		PUSH	PSW
LL8951	7B	1644		CALL	T95BUSY
LL8952	B3D4	1645		MOV	A,E
LL8954	7A	1646		OUT	T9511DATAPORT
				MOV	A,D

LL8955	D3D4	1647	OUT	T9511DATAPORT	
LL8957	79	1648	MOV	A,C	;NEXT SIG BYTE TO STACK OF T9511
LL8958	D3D4	1649	OUT	T9511DATAPORT	
LL895A	78	1650	MOV	A,B	;MSB BYTE TO STACK OF T9511
LL895B	D3D4	1651	OUT	T9511DATAPORT	
LL895D	F1	1652	POP	PSW	
LL895E	C9	1653	RET		
LL		1654			
LL895F	F5	1655	PUSH	PSW	
LL8960	CD4489	1656	CALL	T95BUSY	;WAIT UNTIL T9511 NOT BUSY
LL8963	D8D4	1657	IN	T9511DATAPORT	;MSB FROM STACK OF T9511
LL8965	47	1658	MOV	B,A	
LL8966	D8D4	1659	IN	T9511DATAPORT	;NEXT BYTE FROM STACK OF T9511
LL8968	4F	1660	MOV	C,A	
LL8969	D8D4	1661	IN	T9511DATAPORT	;NEXT BYTE FROM STACK OF T9511
LL896B	57	1662	MOV	D,A	
LL896C	D8D4	1663	IN	T9511DATAPORT	
LL896E	5F	1664	MOV	E,A	
LL896F	F1	1665	POP	PSW	
LL8970	C9	1666	RET		
LL		1667			
LL8971	F5	1668	PUSH	PSW	
LL8972	CD4489	1669	CALL	T95BUSY	
LL8975	3E2C	1670	MVI	A,02CH	;32 BIT FIX POINT ADD
LL8977	D3D5	1671	OUT	OD5H	;
LL8979	CDFC89	1672	CALL	STAT	
LL897C	F1	1673	POP	PSW	
LL897D	C9	1674	RET		
LL		1675			
LL897E	F5	1676	PUSH	PSW	
LL897F	CD4489	1677	CALL	T95BUSY	
LL8982	3E2F	1678	MVI	A,02FH	;32 BIT FIX POINT DIVIDE
LL8984	D3D5	1679	OUT	OD5H	;
LL8986	CDFC89	1680	CALL	STAT	
LL8989	F1	1681	POP	PSW	
LL898A	C9	1682	RET		
LL		1683			
LL		1684			
LL		1685			;THIS SUBROUTINE LOADS A 32 BIT ARRAY ELEMENT INTO
LL		1686			;THE REGISTERS BCDE, REGISTER B HAS MOST SIGNIFICANT BYTE,
LL		1687			;REGISTER E HAS THE LEAST SIGNIFICANT BYTE.
LL		1688			;
LL		1689			;THIS SUBROUTINE HAS A CALLING SEQUENCE
LL		1690	;	LXIX	A32
LL		1691	;	LXIY	ITER
LL		1692	;	CALL	LD4BCDE
LL898B	F5	1693	PUSH	PSW	
LL898C	ES	1694	PUSH	H	
LL		1695			
LL898D	FD6E00	1696	MOVRY	L,0	
LL8990	FD6601	1697	MOVRY	H,1	;(HL)=CONTENTS(ITER)
LL		1698			
LL8993	29	1699	DAD	H	
LL8994	29	1700	DAD	H	;(HL)=4*CONTENTS(ITER)
LL		1701			
LL8995	DDES	1702	PUSHX		
LL8997	C1	1703	POP	B	;(BC)=(DX)
LL		1704			
LL8998	09	1705	DAD	B	;(HL)=A32(ITER)
LL		1706			
LL		1707			
LL8999	5E	1708	MOV	E,M	
LL899A	23	1709	INX	H	
LL899B	56	1710	MOV	D,M	
LL899C	23	1711	INX	H	
LL899D	4E	1712	MOV	C,M	

```

LL899E 23      1713      INX      H
LL899F 46      1714      MOV      B,M      ;(BCDE):=(4 BYTES OF A32(I))
;;          1715
LL89A0 E1      1716      POP      H
LL89A1 F1      1717      POP      PSM
LL89A2 C9      1718      RET
;;          1719      ST4BCDE:
;;          1720      ;
;;          1721      ;THIS SUBROUTINE STORES THE REGISTERS BCDE INTO A 32 BIT ARRAY ELEMENT
;;          1722      ; REGISTER B HAS MOST SIGNIFICANT BYTE,
;;          1723      ;REGISTER E HAS THE LEAST SIGNIFICANT BYTE.
;;          1724      ;
;;          1725      ;THIS SUBROUTINE HAS A CALLING SEQUENCE
;;          1726      ;      LXIX      A32
;;          1727      ;      LXIY      ITER
;;          1728      ;      CALL      ST4BCDE
LL89A3 F5      1729      PUSH     PSM
LL89A4 E5      1730      PUSH     H
LL89A5 C5      1731      PUSH     B
LL89A6 D5      1732      PUSH     D
;;          1733
LL89A7 FD6E00  1734      MOVRY   L,0
LL89A8 FD6601  1735      MOVRY   H,1      ;(HL):=CONTENTS(ITER)
;;          1736
LL89A9 29      1737      DAD     H
LL89AA 29      1738      DAD     H      ;(HL):=4*CONTENTS(ITER)
;;          1739
LL89AF D0E5    1740      PUSHX
LL89B1 C1      1741      POP     B      ;(BC):=(IX)
;;          1742
LL89B2 09      1743      DAD     B      ;(HL):=A32(ITER)
;;          1744
LL89B3 D1      1745      POP     D
LL89B4 73      1746      MOV     M,E
LL89B5 23      1747      INX     H
LL89B6 72      1748      MOV     M,D
LL89B7 23      1749      INX     H
;;          1750
LL89B8 C1      1751      POP     B
LL89B9 71      1752      MOV     M,C
LL89BA 23      1753      INX     H
LL89BB 70      1754      MOV     M,B
;;          1755
LL89BC E1      1756      POP     H
LL89BD F1      1757      POP     PSM
LL89BE C9      1758      RET
;;          1759
;;          1760      LD2BCDE:
;;          1761      ;
;;          1762      ;THIS SUBROUTINE LOADS A 16 BIT ARRAY ELEMENT INTO THE REGISTERS BCDE.
;;          1763      ;REGISTER BC HAS 16 BIT ZERO
;;          1764      ;REGISTER DE HAS THE 16 BIT INTEGER.
;;          1765      ;
;;          1766      ;THIS SUBROUTINE HAS A CALLING SEQUENCE
;;          1767      ;      LXIX      PNTA16
;;          1768      ;      LXIY      ITER
;;          1769      ;      CALL      LD2BCDE
LL89BF F5      1770      PUSH     PSM
LL89C0 E5      1771      PUSH     H
;;          1772
LL89C1 DD6E00  1773      MOVX    L,0
LL89C4 DD6601  1774      MOVX    H,1      ;(HL):=ADDR(A16)
;;          1775
LL89C7 EB      1776      XCHG   ;(DE):=ADDR(A16)
;;          1777
LL89C8 FD6E00  1778      MOVRY   L,0

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LL89CB	FD6601	1779	MOVY	H,1	; (HL):=CONTENTS(ITER)
;;		1780			
LL89CE	29	1781	DAD	H	; (HL):=2*CONTENTS(ITER)
;;		1782			
LL89CF	19	1783	DAD	D	; (HL):=ADDR(A16)+2*CONTENTS(ITER)
;;		1784			
;;		1785			
LL89D0	5E	1786	MOV	E,M	
LL89D1	23	1787	INX	H	
LL89D2	56	1788	MOV	D,M	; (DE) LOADED WITH 16 BIT INTEGER
;;		1789			; WHOSE ADDRESS IS IN (HL)
;;		1790			
LL89D3	010000	1791	LXI	B,0	; (BC) SET TO 0
;;		1792			
LL89D6	E1	1793	POP	H	
LL89D7	F1	1794	POP	PSW	
LL89D8	C9	1795	RET		
;;		1796			STZBCDE:
;;		1797			;
;;		1798			; THIS SUBROUTINE LOADS THE REGISTERS BCDE INTO A 16 BIT ARRAY ELEMENT.
;;		1799			; REGISTER BC HAS 16 BIT ZERO
;;		1800			; REGISTER DE HAS THE 16 BIT INTEGER.
;;		1801			;
;;		1802			; THIS SUBROUTINE HAS A CALLING SEQUENCE
;;		1803	;	LXIX	PMTA16
;;		1804	;	LXIY	ITER
;;		1805	;	CALL	LDZBCDE
LL89D9	F5	1806		PUSH	PSW
LL89DA	ES	1807		PUSH	H
LL89DB	CS	1808		PUSH	B
LL89DC	D5	1809		PUSH	D
;;		1810			;
;;		1811			
LL89DD	DD6E00	1812	MOVX	L,0	
LL89DE	DD6601	1813	MOVX	H,1	; (HL):=ADDR(A16)
;;		1814			
LL89E3	EB	1815	XCHG		; (DE):=ADDR(A16)
;;		1816			
LL89E4	FD6E00	1817	MOVY	L,0	
LL89E7	FD6601	1818	MOVY	H,1	; (HL):=CONTENTS(ITER)
;;		1819			
LL89EA	29	1820	DAD	H	; (HL):=2*CONTENTS(ITER)
;;		1821			
LL89EB	19	1822	DAD	D	; (HL):=2*CONTENTS(ITER)+ADDR(A16)
;;		1823			
LL89EC	D1	1824	POP	D	; RESTORE DE PAIR AS IT WAS ON ENTERING
;;		1825			
;;		1826			
LL89ED	73	1827	MOV	M,E	;
LL89EE	23	1828	INX	H	
LL89EF	72	1829	MOV	M,D	; (DE) STORED AT ADDRESS CONTAINED IN (HL)
;;		1830			
LL89F0	C1	1831	POP	B	; RESTORE BC
LL89F1	E1	1832	POP	H	
LL89F2	F1	1833	POP	PSW	
LL89F3	C9	1834	RET		
;;		1835			CLEAR:
;;		1836			;
;;		1837			; THIS SUBROUTINE HAS A CALLING SEQUENCE
;;		1838	;	LXI	H,A32
;;		1839	;	LXI	B,48
;;		1840	;	CALL	CLEAR
;;		1841			;
;;		1842			; THIS SUBROUTINE CLEARS AN ARRAY OF 32 BIT ELEMENTS.
;;		1843			; HL IS THE BASE ADDRESS
;;		1844			; BC IS HOW MANY BYTES TO ZERO


```

LL      1911  ;
LL      1912  ;
LL      1913  ;
LL      1914  ;
LL      1915  ;
LL      1916  ;
LL      1917  ;
LL      1918  ;
LL      1919  ;
LL      1920  ;
LL      1921  ;
LL      1922  ;
LL8A4A F5    1923  MSG:  PUSH  PSM  ;SAVE STATUS AND A REG
LL8A4B E5    1924          PUSH H
LL8A4C D5    1925          PUSH D
LL8A4D 1A    1926          LDAX  D      ;GET LENGTH OF MESSAGE
LL8A4E 67    1927          MOV   H,A    ;SAVE IT IN H
LL8A4F 13    1928          INX   D      ;POINT TO FIRST BYTE OF MESSAGE
LL      1929  ;
LL8A50 1A    1930  MSG:  LDAX  D      ;BYTE OF MESSAGE INTO A
LL8A51 CD0B88 1931          CALL  CD      ; OUTPUT CHAR
LL8A54 13    1932          INX   D      ;POINT TO NEXT BYTE
LL8A55 25    1933          DCR   H      ; NUMBER OF CHARS TO BE OUTPUT
LL      1934  ;
LL8A56 C2508A 1935          JNZ   MSGO   ;BRANCH IF THERE ARE
LL8A59 D1    1936          POP   D
LL8A5A E1    1937          POP   H
LL8A5B F1    1938          POP   PSM
LL8A5C C9    1939          RET
LL      1940  ;
LL8A5D F5    1941  MSG:  PUSH  PSM
LL8A5E 78    1942          MOV   A,B
LL8A5F CD0987 1943          CALL  HDMP
LL8A62 79    1944          MOV   A,C
LL8A63 CD0987 1945          CALL  HDMP
LL8A66 7A    1946          MOV   A,D
LL8A67 CD0987 1947          CALL  HDMP
LL8A6A 7B    1948          MOV   A,E
LL8A6B CD0987 1949          CALL  HDMP
LL8A6E CD2A87 1950          CALL  CRLF
LL8A71 F1    1951          POP   PSM
LL8A72 C9    1952          RET
LL      1953  ;
LL8A73 F5    1954  INITPORTA:  PUSH  PSM
LL8A74 3E80  1955          MVI   A,080H
LL8A76 D3EB  1956          OUT  OEBH
LL8A78 F1    1957          POP  PSM
LL8A79 C9    1958          RET
LL      1959  ;
LL8A7A F5    1960  PORTAON:   PUSH  PSM
LL8A7B 3E00  1961          MVI   A,00H
LL8A7D D3EB  1962          OUT  OEBH
LL8A7F F1    1963          POP  PSM
LL8A80 C9    1964          RET
LL      1965  ;
LL8A81 F5    1966  PORTAOFF:  PUSH  PSM
LL8A82 3EFF  1967          MVI   A,0FFH
LL8A84 D3EB  1968          OUT  OEBH
LL8A86 F1    1969          POP  PSM
LL8A87 C9    1970          RET
LL8A88 0000  1971  ITER:    DW   0
LL8A8A 0000  1972  I:      DW   0
LL8A8C A68A  1973  PNTA32: DW   A32
LL8A87 1974  PNTA16: DW   SAVEDE
LL8A8E 0100  1975  A16:   DW   01H,02H,03H,04H,05H,06H,07H,08H,09H,0AH,0BH,0CH
LL8A90 0200

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LLBA92 0300
LLBA94 0400
LLBA96 0500
LLBA98 0600
LLBA9A 0700
LLBA9C 0800
LLBA9E 0900
LLBAA0 0A00
LLBAA2 0B00
LLBAA4 0C00
LLBAA6          1976  A32:      DS      4*20
LLBAA8          1977  T9511CTRLPORT EDU 005H
LLBAAA          1978  T9511DATAPORT EDU 004H
LLBAAC 04          1979  OKAY:   DB      4,'OK',CR,LF
LLBAAE 4F4B
LLBAAF 0D
LLBAAG 0A
LLBAAH 06          1980  DONEE:  DB      6,'DONE',CR,LF
LLBAAI 444F4E45
LLBAAJ 0D
LLBAAK 0A
LLBAAL          1981          ORG      9000H
LLBAAM          1982  BUFF0:  DS      2048*10
LLBAAN          1983          END
LL      0 ERRORS
&
&R; T=0.53/3.15 09:23:38
&

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GENERIC TRAJECTORY (B.2)

FILE: GTRAJ1 FORTRAN A1 PRINCETON UNIVERSITY TIME-SHARING SYSTEM

```

COMMON/COM/C(2000)
COMMON/DEGREE/DUMMY2(5)
COMMON/RK/DUMMY4(112)
COMMON/RUNOUT/DUMMY8(1)
C
235 CONTINUE
CALL MYINIT
CALL MYRUN
GOTO 235
END
SUBROUTINE MYINIT
CALL INPT
CALL INIT
CALL DYNAMI
RETURN
END
SUBROUTINE MYRUN
COMMON/COM/C(2000)
COMMON/RUNOUT/DAN
COMMON/SINAV/XST(7), YST(7), ZST(7), DIREQ(7), ISTDME, ISTVCR
1, R1(40), NOYES(40), SIGMA(40)
COMMON/DOUBLE/DSEED, DDS
DOUBLE PRECISION DSEED, DDS
EQUIVALENCE (C(203), TIME), (C(207), NSTEP)
EQUIVALENCE (C(211), TIMPR), (C(212), TIMPLT), (C(213), TIMITY)
EQUIVALENCE (C(241), J1), (C(244), TINSOF)
C
C*****TEMPORARILY:
DO 259 I=1,40
259 R1(I)=0.
C
DAN=0.
C
CALL ERROR
C
242 CONTINUE
IF (TIME.LT.TINSOF) GOTO 82
DAN=2.
CALL OUTPT
CALL FINI
GOTO 100
C
82 CONTINUE
C
C***NOISE HAS TO BE DRAWN FROM RANDOM GEN FOR EACH CHANN EVERY DT AND
C***BE AVAILABLE FOR SUBROUTINE OUTPT AT WHATEVER REQUIRED RECORDING
C***INSTANTS.
C*****CALL GGNPM (DSEED, 30, R1)
DSEED=DSEED+DDS
C
CALL LOGIC
C***R.K. LOOP
C
DO 246 J=1,4
J1=J

```

```

CALL ROTAT
CALL DYNAM
C
IF (TIME.LE.0.) CALL OUTPT
CALL RKG
246 CONTINUE
C
C
NSIEP=NSTEP+1
IF (TIME.LE.TIMPR.AND.TIME.LE.TIMPLT.AND.TIME.LE.TIMTTY) GOTO 242
CALL OUTPT
GOTO 242
100 CONTINUE
RETURN
END
BLOCK DATA
COMMON/DEGREE/TETO,QO(50),PSIOJ,PHIOJ,WPOJ(50),WROJ(50)
COMMON/PROG/TACCX(50),TACCY(50),TACCZ(50),TACCG(50),
1WPC(50),WRC(50),WQC(50),NTIME,TSWTCH(15),ISWTCH
COMMON/COM/C(2000)
COMMON/ALBET/XBETA,ZBETA,XALPHA,YALPHA
COMMON/STNAV/XST(7),YST(7),ZST(7),DIREQ(7),ISTDME,ISTVOR
1,R1(40),NOYES(40),SIGMA(40)
COMMON/DOUBLE/DSEED,DDS
DOUBLE PRECISION DSEED,DDS
C
EQUIVALENCE (C(202),NRATE)
EQUIVALENCE (C(214),DTPR),(C(215),DTPLT),(C(216),DTTTY)
EQUIVALENCE (C(220),IPR),(C(244),TIMSCF)
EQUIVALENCE (C(341),HO),(C(347),XEO),(C(348),YEO)
EQUIVALENCE (C(277),USPEDO),(C(278),VSPEDO),(C(279),WSPEDO)
C
DATA HO/116./,TIMSCF/60./,TETO/10./,PSIOJ/0./,PHIOJ/12.7/,
1NTIME/15/,USPEDO/125./,VSPEDO/0./,WSPEDO/12./
2,TACCG/0.,60.,61.,100.,101.,160.,161.,43*600./,
600/2*.6,2*0.,2*.6,44*0./,
7WPOJ/2*-.5,2*0.,2*.5,44*0./,
9WROJ/2*2.86,2*0.,2*-2.86,44*0./,
BTACCX/2*.179,2*.096,2*.179,2*-.206,42*.2/,
CTACCY/40*0.,10*0./,
DTACCZ/2*-1.003,2*-.994,2*-1.003,2*-.985,42*-1./
DATA NRATE/20/,DTPR/400./,DTPLT/400./,DTTTY/1./,
1IPR/1/
2,XBETA/0./,ZBETA/0./,XALPHA/0./,YALPHA/0./
3,XST/7*120000./
4,YST/7*120000./
5,ZST/7*0./
6,DIREQ/7*32./
7,ISTDME/1/,ISTVOR/1/
DATA DSEED/1.D0/,DDS/1.D0/,NOYES/40*0/,SIGMA/40*0./
DATA ISWTCH/1/,TSWTCH/15*600./
1,XEO/0./,YEO/0./
END
SUBROUTINE INPT
INTEGER FILE(6),GO

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```

LOGICAL SOF
DIMENSION NAME(8), LNAME(4)
C
COMMON/COM/C(2000)
COMMON/DEGREE/TETO, QO(50), PSIOJ, PHIOJ, WPOJ(50), WROJ(50)
COMMON/PROG/TACCX(50), TACCY(50), TACCZ(50), TPROG(50),
1WPC(50), WRC(50), WQC(50), NTIME, TSWTCH(15), ISWTCH
COMMON/ALBET/ XBETA, ZBETA, XALPHA, YALPHA
COMMON/STNAV/XST(7), YST(7), ZST(7), DIREQ(7), ISTDME, ISTVOR
1, R1(40), NOYES(40), SIGMA(40)
COMMON/DOUBLE/DSEED, DDS
DOUBLE PRECISION DSEED, DDS
C
EQUIVALENCE (C(202), NRATE)
EQUIVALENCE (C(214), DTPR), (C(215), DTPLT), (C(216), DTTY)
EQUIVALENCE (C(220), IPR), (C(243), IF2), (C(244), TMSOF)
EQUIVALENCE (C(341), HO), (C(347), XE0), (C(348), YE0)
EQUIVALENCE (C(277), USPED0), (C(278), VSPED0), (C(279), WSPED0)
C
NAMELIST/INP/FILE
NAMELIST/INCN/HO, TETO, QO, TMSOF, PSIOJ, PHIOJ, WPOJ, WROJ,
1TACCX, TACCY, TACCZ, NTIME, TPROG, USPED0, VSPED0, WSPED0
2, XBETA, ZBETA, XALPHA, YALPHA
3, XST, YST, ZST, DIREQ, ISTDME, ISTVOR
4, TSWTCH, XE0, YE0
NAMELIST/PARM/NRATE, DTTY, DTPR, DTPLT, IPR, DSEED, DDS, NOYES, SIGMA
C
DATA NAME/4HINCN, 4HPARM, 4H      ,4H      ,4H      ,4H      ,4H      ,4H      /
235 CONTINUE
PRINT 502
502 FORMAT(1H, 'TO CONTINUE ENTER F, TO STOP ENTER T')
READ 503, SCF
503 FORMAT(L1)
IF(SOF) STOP
PRINT 500
500 FORMAT(1H, 'ENTER DESIRED FILES IN NAMELIST INP', '/')
READ(5, INP)
IF1=FILE(1)
IF2=FILE(2)
IF3=FILE(3)
IF4=FILE(4)
IF5=FILE(5)
IF6=FILE(6)
DO 220 I=1, 2
LNAME(I)=NAME(I)
220 CONTINUE
C
IF(IF1.EQ.5) PRINT 501, LNAME
501 FORMAT(1H, 'ENTER NAMELISTS ', A4, A4, 'IN THIS ORDER', '/')
IF(IF3.NE.0) READ(IF1, INCN)
IF(IF4.NE.0) READ(IF1, PARM)
C
PRINT 504
504 FORMAT(1H, 'TO RUN ENTER 1, TO MODIFY INPUT DATA ENTER 0')
READ 505, GO

```

```

505 FORMAT (I1)
IF(GO.NE.1) GCTO 235
RETURN
END
SUBROUTINE INIT
DIMENSION IPL(100),IPD(100)
COMMON/COM/C(2000)
COMMON/DEGREE/TETO,QO(50),PSIOJ,PHIOJ,WPOJ(50),WROJ(50)
COMMON/PROG/TACCX(50),TACCY(50),TACCZ(50),TPROG(50),WPC(50),
1WRC(50),WQC(50),NTIME,TSWTCH(15),ISWTCH
COMMON/RK/ARK(4),BRK(4),CRK(4),QRK(100)
C
EQUIVALENCE (C(201),N)
EQUIVALENCE (C(202),NRATE), (C(203),TIME), (C(204),TIMED)
EQUIVALENCE (C(205),DT), (C(207),NSTEP)
EQUIVALENCE (C(211),TIMPR), (C(212),TIMPLT), (C(213),TIMTTY)
EQUIVALENCE (C(214),DTPR), (C(215),DTPLT), (C(216),DTTTY)
EQUIVALENCE (C(217),LINE), (C(218),NPRINT), (C(219),NPLOT)
EQUIVALENCE (C(222),NSQ2)
EQUIVALENCE (C(242),CRAD), (C(370),GRAV1), (C(319),THETO)
EQUIVALENCE (C(318),PHIO), (C(320),PSIO)
C
GRAV1=32.17
C
ARK(1)=.5
ARK(2)=1.-1./SQRT(2.)
ARK(3)=1.+1./SQRT(2.)
ARK(4)=1./6.
BRK(1)=2.
BRK(2)=1.
BRK(3)=1.
BRK(4)=2.
CRK(1)=ARK(1)
CRK(2)=ARK(2)
CRK(3)=ARK(3)
CRK(4)=ARK(1)
DO 229 I=1,100
229 QRK(I)=0.
C
NSQ2=1
C
PI=4.*ATAN(1.)
CRAD=180./PI
THETO=TETO/CRAD
PSIO=PSIOJ/CRAD
PHIO=PHIOJ/CRAD
DO 248 I=1,NTIME
WPC(I)=WPOJ(I)/CRAD
WQC(I)=QO(I)/CRAD
248 WRC(I)=WROJ(I)/CRAD
C
IPL(1)=203
IPD(1)=204
N=1
C(1)=IPL(1)

```



```

C (101)=IPD (1)
TIME=0.
TIMED=1.
NSTEP=0
NRAT=NRATE
  DT=1./FLOAT (NRAT)
C
NPRINT=0
NPIOT=0
LINE=60
TIMPR=DTPR-.5*DT
TIMPLT=DTPLT-.5*DT
TIMTTY=DTTTY-.5*DT
IF (DTTTY.GT.50.)          TIMTTY=1000.
C
RETURN
END
SUBROUTINE ERROR
PRINT 507
507 FORMAT (1H , 'RUNNING NOW' , /)
RETURN
END
SUBROUTINE DYNAMI
DIMENSION IPL (100) , IPD (100)
COMMON/COM/C (2000)
EQUIVALENCE (C (201) , N)
EQUIVALENCE (C (205) , DT)
EQUIVALENCE (C (311) , TET) , (C (319) , THET0) , (C (312) , PHI)
EQUIVALENCE (C (318) , PHI0) , (C (310) , PSI) , (C (320) , PSIO)
EQUIVALENCE (C (334) , XE) , (C (335) , YE) , (C (336) , ZE)
EQUIVALENCE (C (341) , H0) , (C (343) , HM) , (C (347) , XE0) , (C (348) , YE0)
EQUIVALENCE (C (271) , USPEED) , (C (277) , USPED0) , (C (272) , VSPEED)
EQUIVALENCE (C (278) , VSPED0) , (C (273) , WSPEED) , (C (279) , WSPED0)
C
N=N+1
  IPL (N) = 310
  IPD (N) = 314
N=N+1
  IPL (N) = 311
  IPD (N) = 315
N=N+1
  IPL (N) = 312
  IPD (N) = 316
N=N+1
  IPL (N) = 271
  IPD (N) = 274
N=N+1
  IPL (N) = 272
  IPD (N) = 275
N=N+1
  IPL (N) = 273
  IPD (N) = 276
N=N+1
  IPL (N) = 334
  IPD (N) = 337

```

```

N=N+1
IPL(N)=335
IPD(N)=338
N=N+1
IPL(N)=336
IPD(N)=339
C
TET=THETO
PSI=PSIO
PHI=PHIO
XE=XEO
YE=YEO
ZE=-HO
HM=HO
C
USPEED=USPEEO
VSPEED=VSPEEO
WSPEED=WSPEEO
C
DO 111 I=2,N
C(I)=IPL(I)
111 C(100+I)=IPL(I)
C
RETURN
END
SUBROUTINE LOGIC
COMMON/COM/C(2000)
COMMON/PROG/TACCX(50),TACCZ(50),TPROG(50),
1WPC(50),WRC(50),WQC(50),NTIME,TSWTCH(15),ISWTCH
EQUIVALENCE (C(302),WQ),(C(303),WR),(C(301),WP)
EQUIVALENCE (C(531),ACCX),(C(532),ACCY),(C(533),ACCZ)
EQUIVALENCE (C(203),TIME),(C(311),TET)
EQUIVALENCE (C(312),PHI),(C(272),VSPEED),(C(205),DT)
IF(TIME.LT.TSWTCH(ISWTCH))GOTO 11
IF(ISWTCH.EQ.1)GOTO 12
IF(ISWTCH.EQ.2)GOTO 13
PHI=0.
TET=-.1745
ISWTCH=ISWTCH+1
GOTO 11
13 PHI=12.7*.01745
TET=.1745
ISWTCH=ISWTCH+1
GOTO 11
12 PHI=0.
TET=.096
ISWTCH=ISWTCH+1
11 CONTINUE
C***FOR THIS N.L. MODEL TRANSITION BETWEEN COMPUTATIONALLY PREDICTED
C***STEADY STATES WILL ANYWAY BE ARTIFICIAL. THUS, THE TSWTCH-OPTION
C***IS DEFERRED AND ONLY THE FIRST SQUINT-SEGMENT IS USED IN EACH RUN.
C***RESULTS OF ALL RUNS APPEND TO EACH OTHER ON FILE 10('DISP MOD'-
C***OPTION OF FILEDEF-BEFORE THE CONSECUTIVE RUNS OF THE JOB).
C***THE CREATED FILE HAS ALL DATA-VARIABLES OF A GIVEN INSTANT AS A
C***RECORD.IT'S COMPATIBLE WITH APL-LINPLOT(BLANKS BETWEEN VALUES),

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C***AND A SEPARATE PROGRAM CONVERTS IT TO A TIME-VECTOR-RECORD FILE.
WQ=SQUINT (TIME,TPROG,WQC,NTIME,1)
WP=SQUINT (TIME,TPROG,WPC,NTIME,1)
WR=SQUINT (TIME,TPROG,WRC,NTIME,1)
ACCX=SQUINT (TIME,TPROG,TACCX,NTIME,1)
ACCY=SQUINT (TIME,TPROG,TACCY,NTIME,1)
AC CZ=SQUINT (TIME,TPROG,TAC CZ,NTIME,1)
RETURN
END
SUBROUTINE LYNAM
COMMON/COM/C (2000)
C
EQUIVALENCE (C (302),WQ), (C (311),TET), (C (315),DTET)
EQUIVALENCE (C (321),VX), (C (323),VZ)
EQUIVALENCE (C (334),XE), (C (336),ZE), (C (337),XED), (C (339),ZED)
EQUIVALENCE (C (351),CEB11)
EQUIVALENCE (C (353),CEB13), (C (357),CEB31), (C (359),CEB33)
EQUIVALENCE (C (310),PSI), (C (312),PHI), (C (314),DPSI), (C (316),DPHI)
EQUIVALENCE (C (301),WP), (C (303),WR)
EQUIVALENCE (C (322),VY), (C (335),YE), (C (338),YED)
EQUIVALENCE (C (439),CSF), (C (440),SNF), (C (441),CST), (C (442),SNT)
EQUIVALENCE (C (352),CEB12), (C (354),CEB21), (C (355),CEB22)
EQUIVALENCE (C (356),CEB23), (C (358),CEB32)
EQUIVALENCE (C (531),ACCX), (C (532),ACCY), (C (533),ACCZ)
EQUIVALENCE (C (271),USPEED), (C (272),VSPEED), (C (273),WSPEED)
EQUIVALENCE (C (274),DUSPED), (C (275),DVSPEED), (C (276),DWSPEED)
EQUIVALENCE (C (370),GRAV1)
C
DPSI=(WR*CSF+WQ*SNF)/CST
DTET=WQ*CSF-WR*SNF
DPHI=WP+DPSI*SNT
CALL DBTOI (USPEED,VSPEED,WSPEED,CEB11,CEB12,CEB13
1,CEB21,CEB22,CEB23,CEB31,CEB32,CEB33,VX,VY,VZ)
XED=VX
ZED=VZ
YED=VY
DUSPED=-WQ*WSPEED+WR*VSPEED-GRAV1*SNT +ACCX*GRAV1
C*****DVSPEED=-WR*USPEED+WP*WSPEED+GRAV1*CST*SNF+ACCY*GRAV1-ASSUME COORD.
DVSPEED=0.
DWSPEED=+WQ*USPEED-WP*VSPEED+GRAV1*CST*CSF+ACCZ*GRAV1
C
C
RETURN
END
SUBROUTINE FINISH
COMMON/COM/C (2000)
COMMON/REC/A3 (2000,20)
C
EQUIVALENCE (C (203),TIME), (C (217),LINE), (C (218),NPRINT)
EQUIVALENCE (C (219),NPLOT), (C (220),IPR), (C (243),IF2), (C (242),CRAD)
EQUIVALENCE (C (212),TIMPLT)
C
ENTRY FINI
WRITE (IF2,516)
516 FORMAT (1H , 'TIME IS OVER', ///)

```

C

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IF (NPLOT.LT.2) GOTO 518
DO 121 I=1,NPLOT
121 WRITE (10,531) (A3(I,J),J=1,16)
531 FORMAT (1H,16(F9.2,X))
ENDFILE 10
WRITE (IF2,517) NPLOT
517 FORMAT (1H,I15)
518 CONTINUE
RETURN
END
SUBROUTINE CUPPT
COMMON/COM/C(2000)
COMMON/RUNCUT/DAN
COMMON/REC/A3(2000,20)
DIMENSION RDME(7),VOR(7)
COMMON/ALBET/XBETA,ZBETA,XALPHA,YALPHA
COMMON/STNAV/XST(7),YST(7),ZST(7),DIREQ(7),ISTDME,ISTVOR
1,R1(40),NOYES(40),SIGMA(40)
EQUIVALENCE (C(336),ZE)
EQUIVALENCE (C(203),TIME),(C(211),TIMPR),(C(212),TIMPLT)
EQUIVALENCE (C(213),TIMTTY),(C(214),DTPR),(C(215),DIPLT)
EQUIVALENCE (C(216),DETTY),(C(217),LINE),(C(218),NPRINT)
EQUIVALENCE (C(219),NPLOT),(C(242),CRAD),(C(243),IF2)
EQUIVALENCE (C(302),WQ),(C(321),VX),(C(323),VZ),(C(334),XE)
EQUIVALENCE (C(343),HM),(C(311),TET)
EQUIVALENCE (C(310),PSI),(C(312),PHI)
EQUIVALENCE (C(301),WP),(C(303),WR),(C(322),VY),(C(335),YE)
EQUIVALENCE (C(531),ACCX),(C(532),ACCY),(C(533),AC CZ)
EQUIVALENCE (C(271),USPEED),(C(272),VSPEED),(C(273),WSPEED)

```

C
C

```

WPJ=CRAD*WP+NOYES(1)*SIGMA(1)*R1(1)
WQJ=CRAD*WQ+NOYES(2)*SIGMA(2)*R1(2)
WRJ=CRAD*WR+NOYES(3)*SIGMA(3)*R1(3)
PSIJ=CRAD*PSI+NOYES(4)*SIGMA(4)*R1(4)
THETJ=CRAD*TET+NOYES(5)*SIGMA(5)*R1(5)
PHIJ=CRAD*PHI+NOYES(6)*SIGMA(6)*R1(6)
VAIR=SQRT(USPEED**2+VSPEED**2+WSPEED**2)+NOYES(7)*SIGMA(7)*R1(7)
VRP=VSPEED+WR*XBETA-WP*ZBETA
USPD=USPEED
BETA=ATAN2(VRP,USPD)
BETAJ=CRAD*BETA+NOYES(8)*SIGMA(8)*R1(8)
WQR=WSPEED-WQ*XALPHA+WP*YALPHA
ALPHA=ATAN2(WQR,USPD)
ALPHAJ=CRAD*ALPHA+NOYES(9)*SIGMA(9)*R1(9)
HM=-ZE+NOYES(10)*SIGMA(10)*R1(10)
DO 301 I=1,ISTDME
301 RDME(I)=SQRT((XE-XST(I))**2+(YE-YST(I))**2+(ZE-ZST(I))**2)+
1NOYES(10+I)*SIGMA(10+I)*R1(10+I)
DO 302 I=1,ISTVOR
YVOR=YE-YST(I)
XVOR=XE-XST(I)
REQ=DIREQ(I)/CRAD
RUNITX=COS(REQ)

```

```

RUNITY=SIN(REQ)
VCOS=ABS((XVCR*RUNITY+YVOR*VCOS)/SQRT(XVOR**2+YVOR**2))
RVOR1=ARCCOS(VCOS)
RVOR=CRAD*RVOR1+NOYES(10+ISTDME+I)*SIGMA(10+ISTDME+I)*
1R1(10+ISTDME+I)
302 VOR(I)=SATF(RVOR,10.)
VXY=SQRT(VX*VX+VY*VY)
VZN=-VZ
GAMV=ATAN2(VZN,VXY)
GAMVJ=CRAD*GAMV
GAMH=ATAN2(VY,VX)
GAMHJ=CRAD*GAMH
ACCX=ACCX+NOYES(10+ISTDME+ISTVOR+1)*SIGMA(10+ISTDME+ISTVOR+1)*
1R1(10+ISTDME+ISTVOR+1)
ACCY=ACCY+NOYES(10+ISTDME+ISTVOR+2)*SIGMA(10+ISTDME+ISTVOR+2)*
1R1(10+ISTDME+ISTVOR+2)
ACCZ=ACCZ+NOYES(10+ISTDME+ISTVOR+3)*SIGMA(10+ISTDME+ISTVOR+3)*
1R1(10+ISTDME+ISTVOR+3)
C***NOW,IF TRIGGERED-CONTAMINATION BY NOISE;IF NOT-BYPASSED.
C
C***OUTPUT OPTIONS:
C*** 1.SHORT(TERMINAL) PRINTOUT;
C*** 2.LONG PRINTOUT OF FIRST BUNCH,SECOND OR BOTH;
C*** 3.CREATION OF 1SEC-INTERVAL-FILE OF DATA(SAME AS FLIGHT FILE)-
C*** -TO BE PRINTED,PLOTTED OR FURTHER PROCESSED.
C
IF(TIME.GT.0..AND.DAN.LT.1.)GOTO 879
PRINT 508
WRITE(IF2,511)TIME,VAIR,GAMVJ,GAMHJ,HM,XE,YE,PSIJ,THETJ,
1PHIJ,VOR(1),RDME(1),ALPHAJ,BETAJ
879 CONTINUE
IF(TIME.LE.TIMPR)GOTO 241
IF(LINE.NE.60)GOTO 259
WRITE(IF2,508)
508 FORMAT(1H1,' TIME VAIR GAMVJ GAMEJ HM XE
1YE PSIJ THETJ PHIJ VOR(1) RDME(1) ALPHAJ BETAJ')
NPRINT=NPRINT+1
LINE=1
259 CONTINUE
WRITE(IF2,511)TIME,VAIR,GAMVJ,GAMHJ,HM,XE,YE,PSIJ,THETJ,PHIJ,
1VOR(1),RDME(1),ALPHAJ,BETAJ
511 FORMAT(1H ,5F7.1,2F10.1,4F7.1,F11.1,2F7.1)
NPRINT=NPRINT+1
TIMPR=TIMPR+ITPR
LINE=LINE+1
241 IF(TIME.LE.TIMPLT.OR.NPLOT.GE.2000)GOTO 247
NPLOT=NPLOT+1
A3(NPLOT,1)=TIME
A3(NPLOT,2)=WPJ
A3(NPLOT,3)=WQJ
A3(NPLOT,4)=WRJ
A3(NPLOT,5)=ACCX
A3(NPLOT,6)=ACCY
A3(NPLOT,7)=ACCZ
A3(NPLOT,8)=HM

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A3 (NPLOT,9) =VAIR
A3 (NPLOT,10) =PSIJ
A3 (NPLOT,11) =THETJ
A3 (NPLOT,12) =PHIJ
A3 (NPLOT,13) =VOR (1)
A3 (NPLOT,14) =RDME (1)
A3 (NPLOT,15) =ALPHAJ
A3 (NPLOT,16) =BETAJ
    TIMPLT=TIMPLT+DTPLT
247    IF (TIME.LE.TIMTTY) GOTO 240
    IF (TIME.LT. (1.5*DTTTY)) PRINT 510
510  FORMAT (1H1, ' TIME          VAIR          GAMVJ          GAMHJ          XE          YE
1      HM' )
    PRINT 513, TIME, VAIR, GAMVJ, GAMHJ, XE, YE, HM
513  FORMAT (1H ,7F10.1)
    TIMTTY=TIMTTY+DTTTY
240  CONTINUE
C
RETURN
END
FUNCTION SATF (X11, XM11)
SATF=SIGN (AMIN1 (ABS (X11), XM11), X11)
RETURN
END
SUBROUTINE RCTAT
COMMON/COM/C (2000)
EQUIVALENCE (C (311), TET), (C (351), CEB11), (C (353), CEB13)
EQUIVALENCE (C (357), CEB31), (C (359), CEB33)
EQUIVALENCE (C (441), CST), (C (442), SNT)
EQUIVALENCE (C (310), PSI), (C (312), PHI), (C (352), CEE12)
EQUIVALENCE (C (354), CEB21), (C (355), CEB22), (C (356), CEB23)
EQUIVALENCE (C (358), CEB32), (C (443), CSP), (C (444), SNP)
EQUIVALENCE (C (439), CSF), (C (440), SNF)
C
SNT=SIN (TET)
CST=COS (TET)
SNP=SIN (PSI)
CSF=COS (PSI)
SNF=SIN (PHI)
CSF=COS (PHI)
C
CEE11=CST*CSP
CEB13=-SNT
CEB31=+SNT*CSF*CSP+SNF*SNP
CEB33=CST*CSF
CEB12=CST*SNP
CEB21=SNF*SNT*CSP-CSF*SNP
CEB22=SNF*SNT*SNP+CSF*CSP
CEB23=SNF*CST
CEB32=CSF*SNT*SNP-SNF*CSP
RETURN
END
SUBROUTINE DITOB (XI, YI, ZI, A11, A12, A13, A21, A22, A23, A31, A32, A33,
1XO, YO, ZO)
XO=A11*XI+A13*ZI+A12*YI

```

```

ZO=A31*XI+A33*ZI+A32*YI
YO=A21*XI+A22*YI+A23*ZI
RETURN
ENTRY DBTCI (XI, YI, ZI, A11, A12, A13, A21, A22, A23, A31, A32, A33,
1XO, YO, ZO)
XO=A11*XI+A31*ZI+A21*YI
ZO=A13*XI+A33*ZI+A23*YI
YO=A12*XI+A22*YI+A32*ZI
RETURN
END
SUBROUTINE RKG
DIMENSION IPL (100), IPD (100)
COMMON/CGM/C (2000)
COMMON/RK/ARK (4), BRK (4), CRK (4), QRK (100)
C
EQUIVALENCE (C (201), N)
EQUIVALENCE (C (205), H), (C (241), J)
C
DO 100 I=1, N
IL=C (I)
ID=C (100+I)
X1=C (ID) *H
X2=(X1-BRK (J) *QRK (I)) *ARK (J)
C (IL)=C (IL) +X2
100 QRK (I) =QRK (I) +3. *X2-CRK (J) *X1
C
RETURN
END
FUNCTION SQUINT (X, TABX, TABY, NTAB, N)
DIMENSION TABX (NTAB), TABY (NTAB)
IF (NTAB.NE.1) GOTO 1
SQUINT=TABY (NTAB)
RETURN
1 IF (X-TABX (N)) 2, 3, 4
2 N=N-1
IF (N) 9, 9, 1
3 SQUINT=TABY (N)
FACTOR=0.
RETURN
4 IF ((N+1).GT.NTAB) GOTO 10
IF (X-TABX (N+1)) 5, 6, 7
6 N=N+1
GOTO 3
7 N=N+1
GOTO 4
5 FACTOR=(X-TABX (N)) / (TABX (N+1) -TABX (N))
SQUINT=(TABY (N+1) -TABY (N)) *FACTOR+TABY (N)
RETURN
9 PRINT 1000, X, TABX (1)
Y=SQRT (-1.)
STOP
1000 FORMAT (1H, 10 ('$'), 'SQUINT UNDERFLOW - INPUT =', E15.8, ' LESS THAN
1N FIRST ARG. TABLE ENTRY (', E15.8, ') ')
10 PRINT 2000, X, TABX (NTAB)
Y=SQRT (-1.)

```

FILE: GTRAJ1 FCRIRAN A1 PRINCETON UNIVERSITY TIME-SHARING SYSTEM

```
STCP
2000 FORMAT(1H ,10('$'), 'SQUINT OVERFLOW -INPUT =',E15.8 ,' GREATER
1 THAN LAST ARG. TABLE ENTRY (' ,E15.8 ,' ) ' )
END
```

GTR
GTR
GTR
GTR

OPTIMAL FLIGHT PATH RECONSTRUCTION (B.3)

FILE: OPTFILT FORTRAN A

PRINCETON UNIVERSITY TIME-SHARING

```

C*
C*OPTIMAL FILTERING PROGRAM
C*
  IMPLICIT REAL*8(A-H,O-$)
  REAL*4 PREDCT(6)
  DIMENSION SUM(6),H112(11,6),H111(6,6)
  COMMON/DAT0/S2LIAC,S2XYZR,TIMSOF,X00(11),S2WIND,S2WNDZ,S2WNDY
  1,S2V,S2ALF,S2BET,S2H,S2DME,S2VOR,S2BDME,S2ZR,PERCNT,OMEGA,AGLOBE
  4,OUTL1,OUTL2,S2QA,S2QB
  2,EPS2,TLAM0,SMEW0,XST,YST,ZST,DIREQ,KDME(20),NDME1(20),NDME2(20)
  3,KDME2(20),NXP,NRATE,NSTEP,IDGT,ISTDME,ISTVOR,SOF
  LOGICAL GO,SOF
  NAMELIST/INP/FILE
  INTEGER FILE(2)
  NAMELIST/OK/GO
  NAMELIST/DAT/SOF,NXP,S2LIAC,S2XYZR,NRATE,TIMSOF,X00,NSTEP,IDGT
  1,S2V,S2ALF,S2BET,S2H,S2DME,S2VOR,PERCNT,OMEGA,AGLOBE
  4,OUTL1,OUTL2,S2QA,S2QB
  2,EPS2,ISTDME,ISTVOR,XST,YST,ZST,DIREQ,KDME,NDME1,NDME2,S2WIND
  3,TLAM0,SMEW0,S2WNDZ,S2BDME,S2ZR,S2WNDY,KDME2
  DIMENSION P(11,11),PO(11,11),HB(6,11),X0(11),XOUT(11)
  1,RES(6),RK(6,6),HBT(11,6),PHT(11,6),HPHT(6,6),HPHTR(6,6)
  2,HPHTRI(6,6),WKAREA(110),CKALM(11,6),DELX(11,1),RES1(6,1)
  3,XPLUS(11),AIDEN(11,11),CH(11,11),UNMKH(11,11),PPLUS(11,11)
  4,CKALMT(6,11),UNMKHT(11,11),STABK1(11,11),STABK2(11,11)
  5,STABK3(6,11),STABK4(11,11)
  DIMENSION XST(7),YST(7),ZST(7),DIREQ(7)
  1,XST7(7),YST7(7),ZST7(7),DIREQ7(7)
C***
  DEFINE FILE 12(60,2112,L,KSTEPS)
C***
  1 CONTINUE
  PRINT 1002
  1002 FORMAT(1H,'TYPE &INP FILE= &END')
  READ(5,INP)
  INF1=FILE(1)
  INF2=FILE(2)
  PRINT 2000,FILE
  2000 FORMAT(2I10)
  PRINT 1004
  1004 FORMAT(1H,'TYPE &DAT DATA= &END')
  READ(INF1,DAT)
  IF(SOF)GOTO 92
  PRINT 1003
  1003 FORMAT(1H,'IF EVERYTHING O.K. TYPE &OK GO=.TRUE.&END')
  GO=.TRUE.
  READ(5,OK)
  IF(GO)GOTO 10
  GOTO 1
  10 CONTINUE
C***
  DO 331 I=1,6
  331 SUM(I)=0.0D0
C***
  PI=4.0D0*DATAN(1.0D0)

```

```

CRAD=180.000/PI
DO 17 I=1,NXP
17 X0(I)=X00(I)
KSTEP=0
KSTEP1=0
DO 101 I=1,NXP
DO 102 J=1,NXP
AIDEN(I,J)=0.000
102 P0(I,J)=0.000
101 CONTINUE
C*****
DO 109 I=1,NXP
109 AIDEN(I,I)=1.000
DO 104 I=1,6
DO 105 J=1,6
105 RK(I,J)=0.000
104 CONTINUE
RK(1,1)=S2V
RK(2,2)=S2ALF
RK(3,3)=S2BET
RK(4,4)=S2H
RK(5,5)=S2DME
RK(6,6)=S2DME
C***
DO 461 I=1,7
XST7(I)=XST(I)
YST7(I)=YST(I)
ZST7(I)=ZST(I)
461 DIREQ7(I)=DIREQ(I)
ISTV07=ISTVOR
ISTDM7=ISTDME
NRAT7=NRATE
TIMS7=TIMSOF
NXP7=NXP
S2LI7=S2LIAC
C***
IDME2=1
IDME=1
301 CONTINUE
KSTEP=KSTEP+1
KSTEP1=KSTEP1+1
C*
IFLAG=1
C***
IF(KDME(IDME).GT.KSTEP)GOTO 807
C*
DO 817 I=1,NXP7
DO 817 J=1,NXP7
817 IF(I.NE.J)P0(I,J)=0.000
IFLAG=5
C*
XST7(1)=XST(NDME1(IDME))
YST7(1)=YST(NDME1(IDME))
ZST7(1)=ZST(NDME1(IDME))
IDME=IDME+1

```

```

807 CONTINUE
C*
  IF (KDME2 (IDME2) .GT. KSTEP) GOTO 827
  DO 828 I=1, NXP7
  DO 828 J=1, NXP7
828 IF (I.NE. J) P0 (I, J) = 0.0D0
  IFLAG=5
  XST7 (2) = XST (NDME2 (IDME2))
  YST7 (2) = YST (NDME2 (IDME2))
  ZST7 (2) = ZST (NDME2 (IDME2))
  IDME2=IDME2+1
827 CONTINUE
C*
C*CALLING THE PROPAGATION-BETWEEN-MEASUREMENTS SUBROUTINE
C***
  CALL PROP27 (TIMS7, PERCNT, OMEGA, AGLOBE, EPS2, S2WNDY, TLAM0
  1, SMEW0, S2WIND, S2WNDZ, X0, P0, XST7, YST7, ZST7, DIREQ7, S2ZR, S2BDME
  3, OUTL1, OUTL2, S2QA, S2QB
  2, S2LI7, S2XYZR, XOUT, P, HB, RES, IFLAG, NRAT7, NXP7, ISTD7, ISTVO7, KSTEP)
  DO 201 I=1, 6
  DO 202 J=1, NXP
202 HBT (J, I) = HB (I, J)
201 CONTINUE
  CALL VMULFF (P, HBT, NXP, NXP, 6, NXP, NXP, PHT, NXP, IER1)
  CALL VMULFF (HB, PHT, 6, NXP, 6, 6, NXP, HPHT, 6, IER2)
  DO 211 I=1, 6
  DO 212 J=1, 6
212 HPHTR (I, J) = HPHT (I, J) + RK (I, J)
211 CONTINUE
C***
  DO 341 I=1, 6
341 SUM (I) = SUM (I) + HPHTR (I, I)
C***
  CALL LINV1F (HPHTR, 6, 6, HPHTRI, IDGT, WKAREA, IER3)
  CALL VMULFF (PHT, HPHTRI, NXP, 6, 6, NXP, 6, CKALM, NXP, IER4)
  DO 221 I=1, 6
221 RES1 (I, 1) = RES (I)
  CALL VMULFF (CKALM, RES1, NXP, 6, 1, NXP, 6, DELX, NXP, IER5)
  DO 231 I=1, NXP
231 XPLUS (I) = XOUT (I) + DELX (I, 1)
  CALL VMULFF (CKALM, HB, NXP, 6, NXP, NXP, 6, CH, NXP, IER6)
  DO 241 I=1, NXP
  DO 242 J=1, NXP
242 UNMKH (I, J) = AIDEN (I, J) - CH (I, J)
241 CONTINUE
C-OLD CALL VMULFF (UNMKH, P, NXP, NXP, NXP, NXP, NXP, PPLUS, NXP, IER7)
  DO 281 I=1, NXP
  DO 281 J=1, NXP
281 UNMKHT (J, I) = UNMKH (I, J)
  DO 283 I=1, NXP
  DO 283 J=1, 6
283 CKALMT (J, I) = CKALM (I, J)
  CALL VMULFF (P, UNMKHT, NXP, NXP, NXP, NXP, NXP, STABK1, NXP, IER7)
  CALL VMULFF (UNMKH, STABK1, NXP, NXP, NXP, NXP, NXP, STABK2, NXP, IER8)
  CALL VMULFF (RK, CKALMT, 6, 6, NXP, 6, 6, STABK3, 6, IER9)

```

```

CALL VMULFF(CKALM,STABK3,NXP,6,NXP,NXP,6,STABK4,NXP,IER10)
DO 282 I=1,NXP
DO 282 J=1,NXP
282 PPLUS(I,J)=STABK2(I,J)+STABK4(I,J)
C***
C***
IF(KSTEP1.LT.5)GOTO 253
KSTEP1=0
DO 251 I=1,NXP
DO 252 J=1,NXP
IF(I.LE.J)GOTO 252
PPLUS(I,J)=.5D0*(PPLUS(I,J)+PPLUS(J,I))
PPLUS(J,I)=PPLUS(I,J)
252 CONTINUE
251 CONTINUE
253 CONTINUE
C*****
DO 741 I=1,NXP
741 X0(I)=XPLUS(I)
DO 742 I=1,NXP
DO 742 J=1,NXP
742 P0(I,J)=PPLUS(I,J)
C***
KSTEPSA=KSTEP
C***
WRITE(12,KSTEPSA)(XPLUS(I),I=1,NXP)
1,(XOUT(I),I=1,NXP),((PPLUS(I,J),I=1,NXP),J=1,NXP)
2,((P(I,J),I=1,NXP),J=1,NXP)
C***
IF(KSTEP.EQ.NSTEP)GOTO 311
C***
GOTO 301
C***
311 CONTINUE
C***
IF(NSTEP.GT.60)GOTO 1
DO 342 I=1,6
342 PREDCT(I)=DSQRT(SUM(I)/59)
PREDCT(2)=57.3*PREDCT(2)
PREDCT(3)=57.3*PREDCT(3)
PRINT 343,(PREDCT(I),I=1,6)
343 FORMAT(' ',F12.0,2F12.1,3F12.0)
C***
GOTO 1
92 CONTINUE
STOP
END
BLOCK DATA
IMPLICIT REAL*8(A-H,O-$)
COMMON/DAT0/S2LIAC,S2XYZR,TIMSOF,X00(11),S2WIND,S2WNDZ,S2WNDY
1,S2V,S2ALF,S2BET,S2H,S2DME,S2VOR,S2BDME,S2ZR,PERCNT,OMEGA,AGLOBE
4,OUTL1,OUTL2,S2QA,S2QB
2,EPS2,TLAM0,SMEW0,XST,YST,ZST,DIREQ,KDME(20),NDME1(20),NDME2(20)
3,KDME2(20),NXP,NRATE,NSTEP,IDGT,ISTDME,ISTVOR,SOF
DIMENSION XST(7),YST(7),ZST(7),DIREQ(7)

```

```
LOGICAL SOP
DATA SOP/ .FALSE. /,NXP/11/,S2LIAC/.4D0/,NRATE/20/,TMSOF/1.0D0/
1,X00/0.0D0,0.0D0,-116.0D0,125.0D0,0.0D0,12.0D0,5*0.0D0/
2,S2V/6.25D0/,S2ALF/.000076D0/,S2WIND/.10D0/,S2WNDZ/.000001D0/
3,S2BET/.000076D0/,S2H/25.0D0/,S2DME/40000.0D0/,S2VOR/.000004D0/
4,NSTEP/60/,IDGT/3/,S2XYZR/25.0D0/,S2ZR/.10D0/
6,ISTDME/2/,ISTVOR/2/,S2BDME/.000025D0/,S2WNDY/-.10D0/
7,XST/.703D0, .6985D0,5*.706D0/
8,YST/-1.297D0,-1.2985D0,5*-1.294D0/
9,ZST/7*0.0D0/
A,DIREQ/32.0D0,32.0D0,0.0D0,0.0D0,0.0D0,0.0D0,0.0D0/
B,KDME/1,19*2500/,NDME1/1,2,3,1,4,15*2/,NDME2/2,3,1,4,16*3/
C,OMEGA/.0000728D0/,AGLOBE/20940000.0D0/,EPS2/.0067D0/
D,TLAM0/.700D0/,SMEW0/-1.300D0/
DATA PERCNT/.000001D0/
1,KDME2/1,19*2600/
2,OUTL1/20000.0D0/,OUTL2/20000.0D0/,S2QA/.81D0/,S2QB/.81D0/
END
```

```

C*
C***STATE AND COVARIANCE MATRIX PROPAGATION BETWEEN MEASUREMENTS.
C*
SUBROUTINE PROP27 (TIMSOP, PERC1, OMEG1, AGLOB1, EPS1, S2W0Y
1, TLAM00, SMEW00, S2W0, S2WZ, X0, P0, XST, YST, ZST, DIREQ, S2ZR1, S2BDM
3, OUTL1T, OUTL2T, S2QAT, S2QBT
2, S2LIAC, S2XYZR, XOUT, P, HB, RES, IFLAG7, NRATE, NXP, ISTDME, ISTVOR, KSTEP)
IMPLICIT REAL*8 (A-H, O-S)
EQUIVALENCE (IC (202), NRATE1), (C (311), TIMSF)
DIMENSION P0 (11, 11), X0 (11), P01 (11, 11), P1 (11, 11), HB1 (8, 11), X01 (11)
EQUIVALENCE (C (467), S2LIA), (C (373), S2XYZ)
EQUIVALENCE (IC (251), NXP1), (C (551), X01 (1)), (C (593), P01 (1, 1))
EQUIVALENCE (C (993), HB1 (1, 1)), (C (793), P1 (1, 1))
DIMENSION HB (6, 11), XOUT (11), P (11, 11), RES (6), Z (11), ZCAL (8)
EQUIVALENCE (C (469), XE), (C (471), YE), (C (473), ZE)
EQUIVALENCE (C (481), USPEED), (C (483), VSPEED), (C (485), WSPEED)
EQUIVALENCE (C (571), Z (1)), (C (1235), ZCAL (1))
DIMENSION XST (7), YST (7), ZST (7), DIREQ (7), XST1 (7), YST1 (7), ZST1 (7)
1, DIREQ1 (7)
EQUIVALENCE (C (1257), XST1 (1)), (C (1271), YST1 (1))
EQUIVALENCE (C (1299), DIREQ1 (1)), (C (1285), ZST1 (1))
EQUIVALENCE (IC (252), ISTD1), (IC (253), ISTV1)
EQUIVALENCE (IC (259), KSTEP1)
EQUIVALENCE (C (505), OMEGA), (C (507), AGLOBE), (C (509), EPS2)
EQUIVALENCE (C (511), TLAM0), (C (513), SMEW0)
EQUIVALENCE (C (470), S2WNDZ)
C***
EQUIVALENCE (C (482), WX), (C (484), WY), (C (486), WZ)
EQUIVALENCE (C (468), S2WIND)
COMMON/COM/C (2000)
COMMON/INCOM/IC (500)
C***
EQUIVALENCE (C (312), PERCNT), (C (381), S2ZR), (C (382), S2BDME)
1, (C (494), BDME1), (C (498), BDME2), (C (474), S2WNDY)
2, (IC (261), IFLAG), (C (502), OUTL1), (C (504), OUTL2)
3, (C (506), S2QA), (C (508), S2QB)
OUTL1=OUTL1T
OUTL2=OUTL2T
S2QA=S2QAT
S2QB=S2QBT
IFLAG=IFLAG7
S2WNDY=S2W0Y
S2ZR=S2ZR1
S2BDME=S2BDM
PERCNT=PERC1
C***
OMEGA=OMEG1
AGLOBE=AGLOB1
EPS2=EPS1
TLAM0=TLAM00
SMEW0=SMEW00
KSTEP1=KSTEP
NRATE1=NRATE
TIMSF=TIMSOP
S2LIA=S2LIAC

```

```

S2XYZ=S2XYZR
S2WIND=S2W0
S2WNDZ=S2WZ
NXP1=NXP
DO 61 I=1,NXP1
61 X01(I)=X0(I)
DO 62 I=1,NXP1
DO 62 J=1,NXP1
P01(I,J)=P0(I,J)
62 CONTINUE
DO 64 I=1,7
XST1(I)=XST(I)
YST1(I)=YST(I)
ZST1(I)=ZST(I)
64 DIREQ1(I)=DIREQ(I)
ISTDM1=ISTDME
ISTV01=ISTVOR

```

C

```

CALL MYINIT
CALL MYRUN

```

C***

```

DO 101 I=1,NXP1
DO 102 J=1,NXP1
IF(I.LT.J)GOTO 101
102 P1(J,I)=P1(I,J)
101 CONTINUE
XOUT(1)=XE
XOUT(2)=YE
XOUT(3)=ZE
XOUT(4)=USPEED
XOUT(5)=VSPEED
XOUT(6)=WSPEED
XOUT(7)=WX
XOUT(8)=WY
XOUT(9)=WZ

```

C*

```

XOUT(10)=BDME1
XOUT(11)=BDME2

```

C***K-TH VECTOR Z TRANSFERRED FROM INIT AND VECTOR ZCAL--FROM OUTPT

```

DO 111 I=1,6
111 RES(I)=Z(I+3)-ZCAL(I)

```

C*

```

RES(5)=RES(5)-BDME1
RES(6)=RES(6)-BDME2

```

C***

```

DO 52 I=1,NXP1
DO 52 J=1,NXP1
52 P(I,J)=P1(I,J)
DO 63 I=1,6
DO 63 J=1,NXP1
63 HB(I,J)=HB1(I,J)

```

C

```

RETURN
END
SUBROUTINE MYINIT

```

```

IMPLICIT REAL*8 (A-H,O-$)
CALL INIT
CALL DYNAMI
RETURN
END
SUBROUTINE MYRUN
IMPLICIT REAL*8 (A-H,O-$)
COMMON/COM/C (2000)
COMMON/INCOM/IC (500)
EQUIVALENCE (C (305), TIME), (IC (207), NSTEP)
EQUIVALENCE (IC (241), J1), (C (311), TIMSF)
C
242 CONTINUE
IF (TIME.LT.TIMSF) GOTO 82
CALL OUTPT
GOTO 100
C
82 CONTINUE
C
C***R.K. LOOP
C
DO 246 J=1,4
J1=J
CALL DYNAM
C
CALL RKG
246 CONTINUE
C
C
NSTEP=NSTEP+1
GOTO 242
100 CONTINUE
RETURN
END
SUBROUTINE INIT
IMPLICIT REAL*8 (A-H,O-$)
REAL*4 Z1 (11), XA1 (6)
DIMENSION IPL (100), IPD (100)
COMMON/COM/C (2000)
COMMON/INCOM/IC (500)
COMMON/RK/ARK (4), BRK (4), CRK (4), QRK (100)
C
EQUIVALENCE (IC (251), NXP1), (C (467), S2LIA), (C (373), S2XYZ)
COMMON/PQ/FB (11, 11), QB (11, 11)
EQUIVALENCE (C (993), HB1 (1, 1)), (C (571), Z (1))
DIMENSION HB1 (8, 11), XA (6), Z (11)
EQUIVALENCE (IC (259), KSTEP1)
C
EQUIVALENCE (IC (201), N)
EQUIVALENCE (IC (202), NRATE1), (C (305), TIME), (C (307), TIMED)
EQUIVALENCE (C (303), DT), (IC (207), NSTEP)
EQUIVALENCE (C (309), CRAD), (C (301), GRAV1)
EQUIVALENCE (C (493), ACCX), (C (495), ACCY), (C (497), ACCZ)
EQUIVALENCE (C (313), WP), (C (315), WQ), (C (317), WR)
EQUIVALENCE (C (329), PHI), (C (327), TET), (C (325), PSI)

```



```

EQUIVALENCE (C(351),CEB11), (C(353),CEB12), (C(355),CEB13)
EQUIVALENCE (C(357),CEB21), (C(359),CEB22), (C(361),CEB23)
EQUIVALENCE (C(363),CEB31), (C(365),CEB32), (C(367),CEB33)
EQUIVALENCE (IC(1),IPL(1)), (IC(101),IPD(1))
EQUIVALENCE (C(468),S2WIND), (C(470),S2WINDZ)
1, (C(381),S2ZR), (C(382),S2BDME), (C(474),S2WNDY)
2, (IC(261),IFLAG), (C(502),OUTL1), (C(504),OUTL2)
3, (C(506),S2QA), (C(508),S2QB)

```

```

C
GRAV1=32.17D0

```

```

C
ARK(1)=.5D0
ARK(2)=1.0D0-1.0D0/DSQRT(2.0D0)
ARK(3)=1.0D0+1.0D0/DSQRT(2.0D0)
ARK(4)=1.0D0/6.0D0
BRK(1)=2.0D0
BRK(2)=1.0D0
BRK(3)=1.0D0
BRK(4)=2.0D0
CRK(1)=ARK(1)
CRK(2)=ARK(2)
CRK(3)=ARK(3)
CRK(4)=ARK(1)
DO 229 I=1,100
229 QRK(I)=0.0D0

```

```

C
PI=4.0D0*DATAN(1.0D0)
CRAD=180.0D0/PI

```

```

C
IPL(1)=305
IPD(1)=307
N=1
TIME=0.0D0
TIMED=1.0D0
NSTEP=0
NRAT=NRATE1
DT=1.0D0/DFLOAT(NRAT)

```

```

C***

```

```

C
DO 306 I=1,NXP1
DO 307 J=1,NXP1
307 FB(I,J)=0.0D0
306 CONTINUE
DO 308 I=1,8
DO 309 J=1,NXP1
309 HB1(I,J)=0.0D0
308 CONTINUE
HB1(4,3)=-1.0D0

```

```

C*
HB1(5,10)=1.0D0
HB1(6,11)=1.0D0
DO 311 I=1,NXP1
DO 312 J=1,NXP1
312 QB(I,J)=0.0D0
311 CONTINUE

```

```

QB(4,4)=S2LIA
QB(5,5)=S2QA
QB(6,6)=S2QB
DO 314 I=1,2
314 QB(I,I)=S2XYZ
QB(3,3)=S2ZR
QB(7,7)=S2WIND
QB(8,8)=S2WNDY
QB(9,9)=S2WNDZ
C*
QB(10,10)=S2BDME
QB(11,11)=S2BDME
C***
C***READ IN SMOOTHED VECTOR X OF MODEL A AND VECTOR Z AT K-TH TIME
C***POINT.Z COSTITUTES OF INPUT(ACCEL MEASUREMENTS) AND MEASUREMENT
C***MATRICES.FIRST NEEDED IN DYNAM AND SECOND--IN MAIN.
C
IF(KSTEP1.EQ.2)GOTO 319
READ(10)(XA1(I),I=1,6)
319 CONTINUE
READ(9)(Z1(I),I=1,11)
Z(5)=Z1(5)/CRAD
Z(6)=Z1(6)/CRAD
Z(10)=Z1(10)/CRAD
Z(11)=Z1(11)/CRAD
Z(4)=Z1(4)
Z(7)=Z1(7)
Z(8)=Z1(8)
Z(9)=Z1(9)
C***
WP=XA1(1)
WQ=XA1(2)
WR=XA1(3)
PHI=XA1(4)
TET=XA1(5)
PSI=XA1(6)
CALL ROTAT
ACCX=Z1(1)
ACCY=Z1(2)
ACCZ=Z1(3)
C*
C* IFLAG=5 FOR FIRST STEP
IF(IFLAG.NE.5)GOTO 837
OOR1=Z(8)
ONR1=Z(8)
OOR2=Z(9)
ONR2=Z(9)
GOTO 838
837 CONTINUE
IF(DABS(Z(8)-ONR1).LT.OUTL1)GOTO 839
Z(8)=ONR1+(ONR1-OOR1)
839 CONTINUE
OOR1=ONR1
ONR1=Z(8)
IF(DABS(Z(9)-ONR2).LT.OUTL2)GOTO 840

```

```

      Z(9)=ONR2+(ONR2-00R2)
840  CONTINUE
      00R2=ONR2
      ONR2=Z(9)
838  CONTINUE

```

C*

```

      RETURN
      END
      SUBROUTINE DYNAMI
      IMPLICIT REAL*8 (A-H,O-S)
      DIMENSION IPL(100),IPD(100)
      COMMON/COM/C(2000)
      COMMON/INCOM/IC(500)

```

C***

```

      DIMENSION X01(11),P01(11,11),P1(11,11)
      EQUIVALENCE (C(337),CSF),(C(339),SNF),(C(341),CST),(C(343),SNT)
1, (C(505),OMEGA),(C(507),AGLOBE),(C(509),EPS2)
2, (C(511),TLAM0)
3, (C(351),CEB11),(C(352),CEB12),(C(353),CEB13)
4, (C(354),CEB21),(C(355),CEB22),(C(356),CEB23)
5, (C(357),CEB31),(C(358),CEB32),(C(359),CEB33)
6, (C(494),BDME1),(C(498),BDME2),(C(312),PERCNT),(C(311),TIMSF)
7, (C(313),WP),(C(315),WQ),(C(317),WR)
      COMMON/PQ/FB(11,11),QB(11,11)
      DIMENSION B60(11,11),FKDT(11,11),SUME(11,11),SUME1(11,11)
1, TMAT(11,11),TNATT(11,11),PTMATT(11,11),TMPMT(11,11)
      EQUIVALENCE (IC(251),NXP1),(C(551),X01(1)),(C(593),P01(1,1))
      EQUIVALENCE (C(793),P1(1,1))

```

C***

```

      EQUIVALENCE (IC(201),N)
      EQUIVALENCE (C(303),DT)
      EQUIVALENCE (C(327),TET),(C(325),PSI),(C(329),PHI)
      EQUIVALENCE (C(469),XE),(C(471),YE),(C(473),ZE)
      EQUIVALENCE (C(481),USPEED),(C(485),WSPEED),(C(483),VSPRED)
      EQUIVALENCE (IC(1),IPL(1)),(IC(101),IPD(1))
      EQUIVALENCE (C(482),WX),(C(484),WY),(C(486),WZ)

```

C

```

      N=N+1
      IPL(N)=469
      IPD(N)=475
      N=N+1
      IPL(N)=471
      IPD(N)=477
      N=N+1
      IPL(N)=473
      IPD(N)=479
      N=N+1
      IPL(N)=481
      IPD(N)=487
      N=N+1
      IPL(N)=483
      IPD(N)=489
      N=N+1
      IPL(N)=485
      IPD(N)=491

```



```

DO 101 I=1, NXP1
DO 102 J=1, NXP1
IF (I.LT.J) GOTO 101
102 P1(J,I)=P1(I,J)
101 CONTINUE

```

C***

```

TLAM=TLAM0+XE/AGLOBE
COST=DCOS(TLAM)
SINT=DSIN(TLAM)
TANT=SINT/COST
SIN2T=2*SINT*COST
COS2T=COST*COST-SINT*SINT
C1111=1.0D0-ZE/AGLOBE-.5D0*EPS2*COS2T
C112=1/C1111

```

C
C

```

C141=C112*(ZE/AGLOBE+.5*EPS2*COS2T)
C111=(CEB11*USPEED+CEB21*VSPEED+CEB31*WSPEED+WX)/AGLOBE
C211=(CEB12*USPEED+CEB22*VSPEED+CEB32*WSPEED+WY)/AGLOBE
C241=-C112*YE*TANT/AGLOBE
C341=C112*EPS2*SIN2T
C56=OMEGA*(CEB11*COST-CEB13*SINT)
C64=OMEGA*(CEB21*COST-CEB23*SINT)
C45=OMEGA*(CEB31*COST-CEB33*SINT)

```

C***

```

C413=OMEGA*(CEB11*SINT+CEB13*COST)
C412=OMEGA*(CEB21*SINT+CEB23*COST)
C411=OMEGA*(CEB31*SINT+CEB33*COST)
CENT1=-OMEGA**2*AGLOBE*C1111*.5*SIN2T
CENT2=-OMEGA**2*AGLOBE*C1111*COST**2
C47=2*(+WR*CEB21-WQ*CEB31)+OMEGA*CEB12*SINT
C48=2*(+WR*CEB22-WQ*CEB32)-C413
C49=2*(+WR*CEB23-WQ*CEB33)-OMEGA*CEB12*COST
C57=2*(-WR*CEB11+WP*CEB31)+OMEGA*CEB22*SINT
C58=2*(-WR*CEB12+WP*CEB32)-C412
C59=2*(-WR*CEB13+WP*CEB33)-OMEGA*CEB22*COST
C67=2*(+WQ*CEB11-WP*CEB21)+OMEGA*CEB32*SINT
C68=2*(+WQ*CEB12-WP*CEB22)-C411
C69=2*(+WQ*CEB13-WP*CEB23)-OMEGA*CEB32*COST

```

C

C***

```

C1122=C112*C112
C2112=C211*C1122
C13=C111*C1122
C11=-EPS2*SIN2T*C13
C31=C111*C112*EPS2*(2*COS2T-C112*EPS2*SIN2T*SIN2T)
C33=C13*EPS2*SIN2T
C21=-EPS2*SIN2T*C2112+C13*(-C1111+.5D0*EPS2*SIN2T*SIN2T)*YE/
1 AGLOBE/COST/COST
C22=-C111*C112*TANT
C23=C2112-C13*TANT*YE/AGLOBE
C14=C141*CEB11
C15=C141*CEB21
C16=C141*CEB31
C24=C241*CEB11+C141*CEB12

```

```

C25=C241*CEB21+C141*CEB22
C26=C241*CEB31+C141*CEB32
C34=C341*CEB11
C35=C341*CEB21
C36=C341*CEB31
C17=C141
C27=C241
C28=C141
C37=C341
C411=OMEGA*(CEB31*SINT+CEB33*COST)
C412=OMEGA*(CEB21*SINT+CEB23*COST)
C413=OMEGA*(CEB11*SINT+CEB13*COST)
C433=OMEGA*COST
C43=C433*C413
C53=C433*C412
C63=C433*C411
COST1=COST*OMEGA/AGLOBE
SINT1=SINT*OMEGA/AGLOBE
C4111=(C1111*COS2T+.5D0*EPS2*SIN2T*SIN2T)*OMEGA*OMEGA
C4112=(C1111*SIN2T- EPS2*SIN2T*COST*COST)*OMEGA*OMEGA
C41=(WSPEED*C412-VSPEED*C411)/AGLOBE
1-CEB11*C4111+CEB13*C4112+COST1*(WX*CEB12-WY*CEB11)+SINT1*(
2 WY*CEB13+WZ*CEB12)
C51=(USPEED*C411-WSPEED*C413)/AGLOBE
1-CEB21*C4111+CEB23*C4112+COST1*(WX*CEB22-WY*CEB21)+SINT1*(
2 WY*CEB23+WZ*CEB22)
C61=(VSPEED*C413-USPEED*C412)/AGLOBE
1-CEB31*C4111+CEB33*C4112+COST1*(WX*CEB32-WY*CEB31)+SINT1*(
2 WY*CEB33+WZ*CEB32)
C65=-C56
C46=-C64
C54=-C45
FB(1,1)=C11
FB(2,1)=C21
FB(3,1)=C31
FB(4,1)=C41
FB(5,1)=C51
FB(6,1)=C61
FB(2,2)=C22
FB(1,3)=C13
FB(2,3)=C23
FB(3,3)=C33
FB(4,3)=C43
FB(5,3)=C53
FB(6,3)=C63
FB(1,4)=CEB11+C14
FB(2,4)=CEB12+C24
FB(3,4)=+CEB13+C34
FB(1,5)=CEB21+C15
FB(2,5)=CEB22+C25
FB(3,5)=+CEB23+C35
FB(1,6)=CEB31+C16
FB(2,6)=CEB32+C26
FB(3,6)=+CEB33+C36
FB(5,4)=-WR+C54

```

```

FB(6,4)=WQ+C64
FB(4,5)=WR+C45
FB(6,5)=-WP+C65
FB(4,6)=-WQ+C46
FB(5,6)=WP+C56
FB(1,7)=1.0D0+C17
FB(2,8)=1.0D0+C141
FB(3,9)=1.0D0
FB(2,7)=C27
FB(3,7)=C37
FB(4,7)=C47
FB(4,8)=C48
FB(4,9)=C49
FB(5,7)=C57
FB(5,8)=C58
FB(5,9)=C59
FB(6,7)=C67
FB(6,8)=C68
FB(6,9)=C69

```

C****

C

```

CALL CSTM (FB, PERCNT, TIMSF, TMAT, B60, FKDT, SUME, SUME1, NXP1, NTERMS)
DO 600 I=1, NXP1
DO 600 J=1, NXP1
600 TMATT(J, I)=TMAT(I, J)
DO 610 I=1, NXP1
DO 610 J=1, NXP1
610 TMPTMT(I, J)=P1(I, J)+QB(I, J)
CALL VMULPF(TMPTMT, TMATT, NXP1, NXP1, NXP1, NXP1, NXP1, PTMATT, NXP1, I1)
CALL VMULPF(TMAT, PTMATT, NXP1, NXP1, NXP1, NXP1, NXP1, P1, NXP1, I2)

```

C

```

RETURN
END
SUBROUTINE DYNAM
IMPLICIT REAL*8 (A-H, O-$)
COMMON/COM/C(2000)
COMMON/INCOM/IC(500)

```

C***

```

EQUIVALENCE (IC(251), NXP1)
COMMON/FQ/FB(11, 11), QB(11, 11)
EQUIVALENCE (C(494), BDME1), (C(496), DBDME1)
1, (C(498), BDME2), (C(500), DBDME2)
EQUIVALENCE (C(793), P1(1, 1))
EQUIVALENCE (C(401), DP11), (C(402), DP21), (C(403), DP31)
EQUIVALENCE (C(404), DP41), (C(405), DP51), (C(406), DP61)
EQUIVALENCE (C(407), DP71), (C(408), DP81), (C(409), DP91)
EQUIVALENCE (C(410), DP22), (C(411), DP32), (C(412), DP42)
EQUIVALENCE (C(413), DP52), (C(414), DP62), (C(415), DP72)
EQUIVALENCE (C(416), DP82), (C(417), DP92)
EQUIVALENCE (C(418), DP33), (C(419), DP43), (C(420), DP53)
EQUIVALENCE (C(421), DP63), (C(422), DP73), (C(423), DP83)
EQUIVALENCE (C(424), DP93)
EQUIVALENCE (C(425), DP44), (C(426), DP54), (C(427), DP64)
EQUIVALENCE (C(428), DP74), (C(429), DP84), (C(430), DP94)
EQUIVALENCE (C(431), DP55), (C(432), DP65), (C(433), DP75)

```

```

EQUIVALENCE (C(434),DP85), (C(435),DP95), (C(436),DP66) OP
EQUIVALENCE (C(437),DP76), (C(438),DP86), (C(439),DP96) OP
EQUIVALENCE (C(440),DP77), (C(441),DP87), (C(442),DP97) OP
EQUIVALENCE (C(443),DP88), (C(444),DP98), (C(445),DP99) OP
EQUIVALENCE (C(319),WPD), (C(321),WQD), (C(323),WRD) OP
DIMENSION DPM(11,11),FP(11,11),P1(11,11) OP

```

C***

```

EQUIVALENCE (C(482),WX), (C(484),WY), (C(486),WZ) OP
EQUIVALENCE (C(488),DWX), (C(490),DWY), (C(492),DWZ) OP

```

C

```

EQUIVALENCE (C(315),WQ), (C(327),TET), (C(333),DTET) OP
EQUIVALENCE (C(499),VX), (C(503),VZ) OP
EQUIVALENCE (C(469),XE), (C(473),ZE), (C(475),XED), (C(479),ZED) OP
EQUIVALENCE (C(351),CEB11) OP
EQUIVALENCE (C(355),CEB13), (C(363),CEB31), (C(367),CEB33) OP
EQUIVALENCE (C(325),PSI), (C(329),PHI), (C(331),DPSI), (C(335),DPHI) OP
EQUIVALENCE (C(313),WP), (C(317),WR) OP
EQUIVALENCE (C(501),VY), (C(471),YE), (C(477),YED) OP
EQUIVALENCE (C(337),CSF), (C(339),SNF), (C(341),CST), (C(343),SNT) OP
EQUIVALENCE (C(353),CEB12), (C(357),CEB21), (C(359),CEB22) OP
EQUIVALENCE (C(361),CEB23), (C(365),CEB32) OP
EQUIVALENCE (C(493),ACCX), (C(495),ACCY), (C(497),ACCZ) OP
EQUIVALENCE (C(481),USPEED), (C(483),VSPEED), (C(485),WSPEED) OP
EQUIVALENCE (C(487),DUSPED), (C(489),DVSPED), (C(491),DWSPED) OP
EQUIVALENCE (C(301),GRAV1) OP
EQUIVALENCE (C(511),TLAM0) OP
EQUIVALENCE (C(505),OMEGA), (C(507),AGLOBE), (C(509),EPS2) OP

```

C***

-C

```

CALL DBTOI(USPEED,VSPEED,WSPEED,CEB11,CEB12,CEB13
1,CEB21,CEB22,CEB23,CEB31,CEB32,CEB33,VX,VY,VZ) OP

```

C***

```

DO 101 I=1,NXP1 OP
DO 102 J=1,NXP1 OP
IF(I.LT.J)GOTO 101 OP
102 P1(J,I)=P1(I,J) OP
101 CONTINUE OP
TLAM=TLAM0+XE/AGLOBE OP
COST=DCOS(TLAM) OP
SINT=DSIN(TLAM) OP
TANT=SINT/COST OP
SIN2T=2*SINT*COST OP
COS2T=COST*COST-SINT*SINT OP
C1111=1.0D0-ZE/AGLOBE-.5D0*EPS2*COS2T OP
C112=1/C1111 OP

```

C

-C

```

C141=C112*(ZE/AGLOBE+.5*EPS2*COS2T) OP
C111=(CEB11*USPEED+CEB21*VSPEED+CEB31*WSPEED+WX)/AGLOBE OP
C211=(CEB12*USPEED+CEB22*VSPEED+CEB32*WSPEED+WY)/AGLOBE OP
C241=-C112*YE*TANT/AGLOBE OP
C341=C112*EPS2*SIN2T OP
C56=OMEGA*(CEB11*COST-CEB13*SINT) OP
C64=OMEGA*(CEB21*COST-CEB23*SINT) OP
C45=OMEGA*(CEB31*COST-CEB33*SINT) OP

```



```

XED=VX+WX+C141*C111*AGLOBE
ZED=+VZ+WZ+C341*C111*AGLOBE
YED=VY+WY+C141*C211*AGLOBE+C241*C111*AGLOBE

```

C***

```

C413=OMEGA*(CEB11*SINT+CEB13*COST)
C412=OMEGA*(CEB21*SINT+CEB23*COST)
C411=OMEGA*(CEB31*SINT+CEB33*COST)
CENT1=-OMEGA**2*AGLOBE*C1111*.5*SIN2T
CENT2=-OMEGA**2*AGLOBE*C1111*COST**2
C47=2*(+WR*CEB21-WQ*CEB31)+OMEGA*CEB12*SINT
C48=2*(+WR*CEB22-WQ*CEB32)-C413
C49=2*(+WR*CEB23-WQ*CEB33)-OMEGA*CEB12*COST
C57=2*(-WR*CEB11+WP*CEB31)+OMEGA*CEB22*SINT
C58=2*(-WR*CEB12+WP*CEB32)-C412
C59=2*(-WR*CEB13+WP*CEB33)-OMEGA*CEB22*COST
C67=2*(+WQ*CEB11-WP*CEB21)+OMEGA*CEB32*SINT
C68=2*(+WQ*CEB12-WP*CEB22)-C411
C69=2*(+WQ*CEB13-WP*CEB23)-OMEGA*CEB32*COST

```

C

C***

```

DUSPED=-WQ*WSPEED+WR*VSPEED+ACCX*GRAV1
1+C45*VSPEED-C64*WSPEED
2+C47*WX+C48*WY+C49*WZ+CENT1*CEB11+CENT2*CEB13

```

C*

C*

```

DVSPED=-WR*USPEED+WP*WSPEED+ACCY*GRAV1
1-C45*USPEED+C56*WSPEED
2+C57*WX+C58*WY+C59*WZ+CENT1*CEB21+CENT2*CEB23
DWSPED=+WQ*USPEED-WP*VSPEED+ACCZ*GRAV1
1+C64*USPEED-C56*VSPEED
2+C67*WX+C68*WY+C69*WZ+CENT1*CEB31+CENT2*CEB33

```

C

```

DWX=0.0D0
DWY=0.0D0
DWZ=0.0D0

```

C*

```

DBDME1=0.0D0
DBDME2=0.0D0

```

C***

C

```

RETURN
END
SUBROUTINE OUTPT
IMPLICIT REAL*8(A-H,O-$)
COMMON/COM/C(2000)
COMMON/INCOM/IC(500)
DIMENSION RDME(7),VOR(7)

```

C***

```

DIMENSION XST1(7),YST1(7),ZST1(7),DIREQ1(7)
EQUIVALENCE (C(1257),XST1(1)),(C(1271),YST1(1)),(C(1285),ZST1(1))
EQUIVALENCE (C(1299),DIREQ1(1)),(IC(252),ISTDM1),(IC(253),ISTVO1)
EQUIVALENCE (C(993),HB1(1,1))
EQUIVALENCE (C(1235),ZCAL(1))
DIMENSION ZCAL(8),HB1(8,11)

```

C

```

EQUIVALENCE (C(309),CRAD)
EQUIVALENCE (C(473),ZE)
EQUIVALENCE (C(305),TIME)
EQUIVALENCE (C(315),WQ), (C(499),VX), (C(503),VZ), (C(469),XE)
EQUIVALENCE (C(327),TET)
EQUIVALENCE (C(325),PSI), (C(329),PHI)
EQUIVALENCE (C(313),WP), (C(317),WR), (C(501),VY), (C(471),YE)
EQUIVALENCE (C(493),ACCX), (C(495),ACCY), (C(497),ACCZ)
EQUIVALENCE (C(481),USPEED), (C(483),VSPEED), (C(485),WSPEED)
EQUIVALENCE (C(507),AGLOBE), (C(509),EPS2)
EQUIVALENCE (C(511),TLAM0), (C(513),SMEW0)
DIMENSION XDME(7), YDME(7), ZDME(7)
C***
TLAM=TLAM0+XE/AGLOBE
COST=DCOS(TLAM)
SINT=DSIN(TLAM)
TANT=SINT/COST
SMEW=SMEW0+YE/AGLOBE/COST
SIN2T=2*SINT*COST
COS2T=COST*COST-SINT*SINT
C1111=1.0D0-.5D0*EPS2*COS2T-ZE/AGLOBE
AC1111=AGLOBE*C1111
COSS=DCOS(SMEW)
SINS=DSIN(SMEW)
RX1=EPS2*SIN2T*COST*COSS-C1111*SINT*COSS-C1111*TANT*SINS*YE/AGLOBE
RX2=EPS2*SIN2T*COST*SINS-C1111*SINT*SINS+C1111*TANT*COSS*YE/AGLOBE
RX3=EPS2*SIN2T*SINT+C1111*COST
C
C***VECTORS X OF MODEL A AND Z(K-TH TIME POINT) OF MODEL B(WITHOUT
C***ACCEL) TRANSFERRED FROM INIT
C
VAIR2=USPEED**2+VSPEED**2+WSPEED**2
VAIR=DSQRT(VAIR2)
VRP=VSPEED
USPD=USPEED
BETA=DATAN2(VRP,USPD)
WQR=WSPEED
ALPHA=DATAN2(WQR,USPD)
DO 301 I=1,ISTDM1
XDME(I)=AC1111*COST*COSS-DCOS(XST1(I))*DCOS(YST1(I))*
1 (-ZST1(I)+AGLOBE*(1.0D0-.5D0*EPS2*DCOS(2*XST1(I))))
YDME(I)=AC1111*COST*SINS-DCOS(XST1(I))*DSIN(YST1(I))*
1 (-ZST1(I)+AGLOBE*(1.0D0-.5D0*EPS2*DCOS(2*XST1(I))))
ZDME(I)=AC1111*SINT-DSIN(XST1(I))*
1 (-ZST1(I)+AGLOBE*(1.0D0-.5D0*EPS2*DCOS(2*XST1(I))))
C***XST,YST ARE LATITUDE AND LONGITUDE
301 RDME(I)=DSQRT(XDME(I)**2+YDME(I)**2+ZDME(I)**2)
C
C*301 RDME(I)=DSQRT((XE-XST1(I))**2+(YE-YST1(I))**2+(ZE-ZST1(I))**2)
C
DO 302 I=1,ISTVO1
302 VOR(I)=1.
C***
ZCAL(1)=VAIR
ZCAL(2)=ALPHA

```

```

ZCAL (3) =BETA
ZCAL (4) =-ZE
ZCAL (5) =RDME (1)
ZCAL (6) =RDME (2)
ZCAL (7) =VOR (1)
ZCAL (8) =VOR (2)

```

```

C
HB1 (5, 1) = (RX1*XDME (1) +RX2*YDME (1) +RX3*ZDME (1)) /RDME (1)
HB1 (6, 1) = (RX1*XDME (2) +RX2*YDME (2) +RX3*ZDME (2)) /RDME (2)
HB1 (5, 2) = (-C1111*SINS*XDME (1) +C1111*COSS*YDME (1)) /RDME (1)
HB1 (6, 2) = (-C1111*SINS*XDME (2) +C1111*COSS*YDME (2)) /RDME (2)
HB1 (5, 3) = (-COST*COSS*XDME (1) -COST*SINS*YDME (1) -SINT*ZDME (1))
1/RDME (1)
HB1 (6, 3) = (-COST*COSS*XDME (2) -COST*SINS*YDME (2) -SINT*ZDME (2))
1/RDME (2)
HB1 (7, 1) = -(YE-YST1 (1)) / (RDME (1) **2 - (ZE-ZST1 (1)) **2)
HB1 (8, 1) = -(YE-YST1 (2)) / (RDME (2) **2 - (ZE-ZST1 (2)) **2)
HB1 (7, 2) = (XE-XST1 (1)) / (RDME (1) **2 - (ZE-ZST1 (1)) **2)
HB1 (8, 2) = (XE-XST1 (2)) / (RDME (2) **2 - (ZE-ZST1 (2)) **2)
HB1 (1, 4) =USPEED/VAIR
HB1 (2, 4) =-WSPEED/(VAIR2-VSPEED**2)
HB1 (3, 4) =-VSPEED/(VAIR2-WSPEED**2)
HB1 (1, 5) =VSPEED/VAIR
HB1 (3, 5) =USPEED/(VAIR2-WSPEED**2)
HB1 (1, 6) =WSPEED/VAIR
HB1 (2, 6) =USPEED/(VAIR2-VSPEED**2)

```

```

C
RETURN
END

```

```

FUNCTION SATF (X11, XM11)
IMPLICIT REAL*8 (A-H, O-$)
SATF=DSIGN (DMIN1 (DABS (X11), XM11), X11)
RETURN
END

```

```

SUBROUTINE ROTAT
IMPLICIT REAL*8 (A-H, O-$)
COMMON/COM/C (2000)
EQUIVALENCE (C (327), TET), (C (351), CEB11), (C (355), CEB13)
EQUIVALENCE (C (363), CEB31), (C (367), CEB33)
EQUIVALENCE (C (341), CST), (C (343), SNT)
EQUIVALENCE (C (325), PSI), (C (329), PHI), (C (353), CEB12)
EQUIVALENCE (C (357), CEB21), (C (359), CEB22), (C (361), CEB23)
EQUIVALENCE (C (365), CEB32), (C (345), CSP), (C (347), SNP)
EQUIVALENCE (C (337), CSF), (C (339), SNF)

```

```

C
SNT=DSIN (TET)
CST=DCOS (TET)
SNP=DSIN (PSI)
CSP=DCOS (PSI)
SNF=DSIN (PHI)
CSF=DCOS (PHI)

```

```

C
CEB11=CST*CSP
CEB13=-SNT
CEB31=+SNT*CSF*CSP+SNF*SNP

```

```

CEB33=CST*CSF
CEB12=CST*SNP
CEB21=SNF*SNT*CSP-CSF*SNP
CEB22=SNF*SNT*SNP+CSF*CSP
CEB23=SNF*CST
CEB32=CSP*SNT*SNP-SNF*CSP
RETURN
END
SUBROUTINE DITOB(XI, YI, ZI, A11, A12, A13, A21, A22, A23, A31, A32, A33,
1XO, YO, ZO)
IMPLICIT REAL*8(A-H, O-$)
XO=A11*XI+A13*ZI+A12*YI
ZO=A31*XI+A33*ZI+A32*YI
YO=A21*XI+A22*YI+A23*ZI
RETURN
ENTRY DBTOI(XI, YI, ZI, A11, A12, A13, A21, A22, A23, A31, A32, A33,
1XO, YO, ZO)
XO=A11*XI+A31*ZI+A21*YI
ZO=A13*XI+A33*ZI+A23*YI
YO=A12*XI+A22*YI+A32*ZI
RETURN
END
SUBROUTINE RKG
IMPLICIT REAL*8(A-H, O-$)
DIMENSION IPL(100), IPD(100)
COMMON/COM/C(2000)
COMMON/RK/ARK(4), BRK(4), CRK(4), QRK(100)
COMMON/INCOM/IC(500)
C
EQUIVALENCE (IC(201), N)
EQUIVALENCE (C(303), H), (IC(241), J)
EQUIVALENCE (IC(1), IPL(1)), (IC(101), IPD(1))
C
DO 100 I=1, N
IL=IPL(I)
ID=IPD(I)
X1=C(ID)*H
X2=(X1-BRK(J)*QRK(I))*ARK(J)
C(IL)=C(IL)+X2
100 QRK(I)=QRK(I)+3.0D0*X2-CRK(J)*X1
C
RETURN
END

```

```

C*
C*OPTIMAL SMOOTHING PROGRAM
C*
  IMPLICIT REAL*8(A-H,O-$)
  REAL*4 XS1(11),PS1(9,9),XAS(6,1)
  COMMON/DAT0/PERCNT,DT,TLAM0,OMEGA,AGLOBE,EPS2,IDGT,NSTEP,NXP,SOF
  LOGICAL GO,SOF
  NAMELIST/INP/FILE
  INTEGER FILE(2)
  NAMELIST/OK/GO
  NAMELIST/DAT/SOF,NSTEP,NXP,PERCNT,DT,IDGT,TLAM0
  1,OMEGA,AGLOBE,EPS2
C***
  DEFINE FILE 17( 150,368,L,KSTEPG)
  DEFINE FILE 12( 150,2112,L ,KSTEPSA)
  DIMENSION XPK12(11),XMK12(11),PPK12(11,11),PMK12(11,11)
C*
  DIMENSION XPK1(6),XMK1(6),XPK(6),XMK(6)
  1,PPK1(6,6),PMK1(6,6),PPK(6,6),PMK(6,6)
  2,FK(6,6),TMAT(6,6),TMATT(6,6),PTMATT(6,6)
  3,PINV(6,6),WKAREA(60),AK(6,6),AKT(6,6)
  4,DELX(6,1),DELP(6,6),DELXES(6,1),XS(6)
  5,AKDELP(6,6),ADPAT(6,6),PS(6,6)
  6,PMK2(6,6)
C***
  DIMENSION B60(6,6),FKDT(6,6),SUME(6,6),SUME1(6,6)
C***
  1 CONTINUE
  PRINT 1002
  1002 FORMAT(1H,'TYPE &INP FILE= &END')
  READ(5,INP)
  INF1=FILE(1)
  INF2=FILE(2)
  PRINT 2000,FILE
  2000 FORMAT(2I10)
  PRINT 1004
  1004 FORMAT(1H,'TYPE &DAT DATA= &END')
  READ(INF1,DAT)
  IF(SOF)GOTO 92
  PRINT 1003
  1003 FORMAT(1H,'IF EVERYTHING O.K. TYPE &OK GO=.TRUE.&END')
  GO=.TRUE.
  READ(5,OK)
  IF(GO)GOTO 10
  GOTO 1
  10 CONTINUE
C***
C***
  KSTEP=NSTEP
  KSTEP1=0
C***
  KSTEPSA=KSTEP
C*
  PI=4.000*DATAN(1.000)
  CRAD=180.000/PI

```

```

C***
  READ (10) (XAS (I, 1), I=1, 6)
  READ (12' KSTEPSA) (XPK12 (I), I=1, 11)
  1, (XMK12 (I), I=1, 11), ((PPK12 (I, J), I=1, 11), J=1, 11)
  2, ((PMK12 (I, J), I=1, 11), J=1, 11)

C*
  DO 431 I=1, NXP
    XPK1 (I) =XPK12 (I)
  431 XMK1 (I) =XMK12 (I)
    DO 432 I=1, NXP
      DO 432 J=1, NXP
        PPK1 (I, J) =PPK12 (I, J)
  432 PMK1 (I, J) =PMK12 (I, J)

C***
  DO 581 I=1, NXP
  581 XS (I) =XPK1 (I)
    DO 582 I=1, NXP
      DO 582 J=1, NXP
  582 PS (I, J) =PPK1 (I, J)
    KSTEPG=KSTEP
    DO 709 I=1, NXP
  709 XS1 (I) =XS (I)
    DO 710 I=1, NXP
      DO 710 J=1, NXP
  710 PS1 (I, J) =PS (I, J)
    XS1 (7) =XPK12 (7)
    XS1 (8) =XPK12 (8)
    XS1 (9) =XPK12 (9)
    DO 801 I=7, 9
      DO 801 J=1, 9
  801 PS1 (I, J) =PPK12 (I, J)
    DO 802 I=1, 6
      DO 802 J=7, 9
  802 PS1 (I, J) =PPK12 (I, J)

C***
  XS1 (10) =XPK12 (10)
  XS1 (11) =XPK12 (11)
  WRITE (17' KSTEPG) (XS1 (I), I=1, 11)
  1, ((PS1 (I, J), I=1, 9), J=1, 9)

C***
  DO 591 I=1, NXP
    DO 591 J=1, NXP
  591 FK (I, J) =0.

C***
C***
  301 CONTINUE
    KSTEP=KSTEP-1
    IF (KSTEP.LT.1) GOTO 311
    KSTEP1=KSTEP+1

C***
  KSTEPSA=KSTEP

C***
  READ (10) (XAS (I, 1), I=1, 6)
  READ (12' KSTEPSA) (XPK12 (I), I=1, 11)
  1, (XMK12 (I), I=1, 11), ((PPK12 (I, J), I=1, 11), J=1, 11)

```

2, ((PMK12(I,J),I=1,11),J=1,11)

C*

```
DO 441 I=1,NXP
  XPK(I)=XPK12(I)
441 XMK(I)=XMK12(I)
DO 442 I=1,NXP
DO 442 J=1,NXP
  PPK(I,J)=PPK12(I,J)
442 PMK(I,J)=PMK12(I,J)
```

C***

C***FK-MATRIX COMPUTATION

```
WP=XAS(1,1)
WQ=XAS(2,1)
WR=XAS(3,1)
PHI=XAS(4,1)
TET=XAS(5,1)
PSI=XAS(6,1)
SNT=DSIN(TET)
CST=DCOS(TET)
SNF=DSIN(PHI)
CSF=DCOS(PHI)
SNP=DSIN(PSI)
CSP=DCOS(PSI)
```

C***

```
CEB11=CST*CSP
CEB12=CST*SNP
CEB13=-SNT
CEB21=SNF*SNT*CSP-CSF*SNP
CEB22=SNF*SNT*SNP+CSF*CSP
CEB23=+SNF*CST
CEB31=SNT*CSF*CSP+SNF*SNP
CEB32=CSF*SNT*SNP-SNF*CSP
CEB33=+CST*CSF
```

C***

```
XE=XPK(1)
YE=XPK(2)
ZE=XPK(3)
USPEED=XPK(4)
VSPEED=XPK(5)
WSPEED=XPK(6)
```

C***

```
WX=XPK12(7)
WY=XPK12(8)
WZ=XPK12(9)
```

C***

```
TLAM=TLAM0+XE/AGLOBE
COST=DCOS(TLAM)
SINT=DSIN(TLAM)
TANT=SINT/COST
SIN2T=2*SINT*COST
COS2T=COST*COST-SINT*SINT
C1111=1.0D0-ZE/AGLOBE-.5D0*EPS2*COS2T
C112=1/C1111
```

C*

C*

```

C141=C112*(ZE/AGLOBE+.5*EPS2*COS2T)
C111=(CEB11*USPEED+CEB21*VSPEED+CEB31*WSPEED+WX)/AGLOBE
C211=(CEB12*USPEED+CEB22*VSPEED+CEB32*WSPEED+WY)/AGLOBE
C241=-C112*YE*TANT/AGLOBE
C341=C112*EPS2*SIN2T
C56=OMEGA*(CEB11*COST-CEB13*SINT)
C64=OMEGA*(CEB21*COST-CEB23*SINT)
C45=OMEGA*(CEB31*COST-CEB33*SINT)
C***
C413=OMEGA*(CEB11*SINT+CEB13*COST)
C412=OMEGA*(CEB21*SINT+CEB23*COST)
C411=OMEGA*(CEB31*SINT+CEB33*COST)
CENT1=-OMEGA**2*AGLOBE*C1111*.5*SIN2T
CENT2=-OMEGA**2*AGLOBE*C1111*COST**2
C47=2*(+WR*CEB21-WQ*CEB31)+OMEGA*CEB12*SINT
C48=2*(+WR*CEB22-WQ*CEB32)-C413
C49=2*(+WR*CEB23-WQ*CEB33)-OMEGA*CEB12*COST
C57=2*(-WR*CEB11+WP*CEB31)+OMEGA*CEB22*SINT
C58=2*(-WR*CEB12+WP*CEB32)-C412
C59=2*(-WR*CEB13+WP*CEB33)-OMEGA*CEB22*COST
C67=2*(+WQ*CEB11-WP*CEB21)+OMEGA*CEB32*SINT
C68=2*(+WQ*CEB12-WP*CEB22)-C411
C69=2*(+WQ*CEB13-WP*CEB23)-OMEGA*CEB32*COST
C*
C1122=C112*C112
C2112=C211*C1122
C13=C111*C1122
C11=-EPS2*SIN2T*C13
C31=C111*C112*EPS2*(2*COS2T-C112*EPS2*SIN2T*SIN2T)
C33=C13*EPS2*SIN2T
C21=-EPS2*SIN2T*C2112+C13*(-C1111+.5D0*EPS2*SIN2T*SIN2T)*YE/
1. AGLOBE/COST/COST
C22=-C111*C112*TANT
C23=C2112-C13*TANT*YE/AGLOBE
C14=C141*CEB11
C15=C141*CEB21
C16=C141*CEB31
C24=C241*CEB11+C141*CEB12
C25=C241*CEB21+C141*CEB22
C26=C241*CEB31+C141*CEB32
C34=C341*CEB11
C35=C341*CEB21
C36=C341*CEB31
C17=C141
C27=C241
C28=C141
C37=C341
C411=OMEGA*(CEB31*SINT+CEB33*COST)
C412=OMEGA*(CEB21*SINT+CEB23*COST)
C413=OMEGA*(CEB11*SINT+CEB13*COST)
C433=OMEGA*COST
C43=C433*C413
C53=C433*C412
C63=C433*C411
COST1=COST*OMEGA/AGLOBE

```



```

SINT1=SINT*OMEGA/AGLOBE
C4111=(C1111*COS2T+.5D0*EPS2*SIN2T*SIN2T)*OMEGA*OMEGA
C4112=(C1111*SIN2T-      EPS2*SIN2T*COST*COST)*OMEGA*OMEGA
C41=(WSPEED*C412-VSPEED*C411)/AGLOBE
1-CEB11*C4111+CEB13*C4112+COST1*(WX*CEB12-WY*CEB11)+SINT1*(
2 WY*CEB13+WZ*CEB12)
  C51=(USPEED*C411-WSPEED*C413)/AGLOBE
1-CEB21*C4111+CEB23*C4112+COST1*(WX*CEB22-WY*CEB21)+SINT1*(
2 WY*CEB23+WZ*CEB22)
  C61=(VSPEED*C413-USPEED*C412)/AGLOBE
1-CEB31*C4111+CEB33*C4112+COST1*(WX*CEB32-WY*CEB31)+SINT1*(
2 WY*CEB33+WZ*CEB32)
C65=-C56
C46=-C64
C54=-C45
FK(1,1)=C11
FK(2,1)=C21
FK(3,1)=C31
FK(4,1)=C41
FK(5,1)=C51
FK(6,1)=C61
FK(2,2)=C22
FK(1,3)=C13
FK(2,3)=C23
FK(3,3)=C33
FK(4,3)=C43
FK(5,3)=C53
FK(6,3)=C63
FK(1,4)=CEB11+C14
FK(2,4)=CEB12+C24
FK(3,4)=+CEB13+C34
FK(1,5)=CEB21+C15
FK(2,5)=CEB22+C25
FK(3,5)=+CEB23+C35
FK(1,6)=CEB31+C16
FK(2,6)=CEB32+C26
FK(3,6)=+CEB33+C36
FK(5,4)=-WR+C54
FK(6,4)=WQ+C64
FK(4,5)=WR+C45
FK(6,5)=-WP+C65
FK(4,6)=-WQ+C46
FK(5,6)=WP+C56

```

C*

C*CALLING THE SUBROUTINE FOR COMPUTATION OF THE STATE TRANSITION MATRIX

C***

```
CALL CSTM(FK,PERCNT,DT,TMAT,B60,FKDT,SUME,SUME1,NXP,NTERMS)
```

```
DO 600 I=1,NXP
```

```
DO 600 J=1,NXP
```

```
600 THATT(J,I)=TMAT(I,J)
```

C***

```
DO 701 I=1,NXP
```

```
DO 701 J=1,NXP
```

```
701 PMK2(I,J)=PMK1(I,J)
```

C***

```

CALL LINV1F(PMK2,NXP,NXP,PINV,IDGT,WKAREA,IER1)
CALL VMULFF(PPK,TMATT,NXP,NXP,NXP,NXP,NXP,PTMATT,NXP,IER2)
CALL VMULFF(PTMATT,PINV,NXP,NXP,NXP,NXP,NXP,AK,NXP,IER3)
DO 601 I=1,NXP
DO 601 J=1,NXP
601 AKT(J,I)=AK(I,J)
DO 602 I=1,NXP
602 DELX(I,1)=XS(I)-XMK1(I)
DO 603 I=1,NXP
DO 603 J=1,NXP
603 DELP(I,J)=PS(I,J)-PMK1(I,J)
CALL VMULFF(AK,DELX,NXP,NXP,1,NXP,NXP,DELXES,NXP,IER4)
DO 604 I=1,NXP
604 XS(I)=XPK(I)+DELXES(I,1)
CALL VMULFF(AK,DELP,NXP,NXP,NXP,NXP,NXP,AKDELP,NXP,IER5)
CALL VMULFF(AKDELP,AKT,NXP,NXP,NXP,NXP,NXP,ADPAT,NXP,IER6)
DO 605 I=1,NXP
DO 605 J=1,NXP
605 PS(I,J)=PPK(I,J)+ADPAT(I,J)
C***
IF(KSTEP1.LT.5) GOTO 253
KSTEP1=0
DO 251 I=1,NXP
DO 252 J=1,NXP
IF(I.LE.J) GOTO 252
PS(I,J)=.5D0*(PS(I,J)+PS(J,I))
PS(J,I)=PS(I,J)
252 CONTINUE
251 CONTINUE
253 CONTINUE
C***
DO 711 I=1,NXP
711 XS1(I)=XS(I)
DO 712 I=1,NXP
DO 712 J=1,NXP
712 PS1(I,J)=PS(I,J)
KSTEPG=KSTEP
XS1(7)=XPK12(7)
XS1(8)=XPK12(8)
XS1(9)=XPK12(9)
DO 803 I=7,9
DO 803 J=1,9
803 PS1(I,J)=PPK12(I,J)
DO 804 I=1,6
DO 804 J=7,9
804 PS1(I,J)=PPK12(I,J)
XS1(10)=XPK12(10)
XS1(11)=XPK12(11)
WRITE(17,KSTEPG)(XS1(I),I=1,11)
1,((PS1(I,J),I=1,9),J=1,9)
C***COPY K-AREAS INTO (K+1)-AREAS I.E. INTO 'PREVIOUS' AREA,
C***--GOING FROM END TO BEGINNING OF FILE.
DO 631 I=1,NXP
DO 631 J=1,NXP
631 PMK1(I,J)=PMK(I,J)

```

```
DO 632 I=1,NXP
632 XMK1(I)=XMK(I)
C***
      GOTO 301
C***
C***
311 CONTINUE
C***
C***
      GOTO 1
92 CONTINUE
STOP
END
BLOCK DATA
IMPLICIT REAL*8 (A-H,O-$)
COMMON/DAT0/PERCNT,DT,TLAM0,OMEGA,AGLOBE,EPS2,IDGT,NSTEP,NXP,SOF
LOGICAL SOF
DATA SOF/ .FALSE. /,NSTEP/60/,NXP/6/
1,PERCNT/.000001D0/,DT/1.0D0/
2,IDGT/3/
3,TLAM0/.700D0/
4,OMEGA/.0000728D0/,AGLOBE/20940000.0D0/,EPS2/.0067D0/
END
```

C***THIS PROGRAM CREATES A NON-DIRECT-ACCESS-DATA-FILE FOR XAS OR
 C***XBS FOR OUTPUT OR FURTHER PROCESSING

```

C*
  DIMENSION J(15),Z(11)
1  ,RDME(7),XDME(7),YDME(7),ZDME(7)
  COMMON/DAT0/SOF,J,NSTEP,N,NAMES,TLAM0,AGLOBE
1  ,EPS2,SMEW0,ISTDME,XST(7),YST(7),ZST(7)
  INTEGER FILE(2)
  DIMENSION NAMES(38),NAMES1(38),XS(11),PS(9,9),SUM(14),STDZ(10)
1  ,BIAS(11),SUM1(14),TEMP(14)
  LOGICAL GO,SOF
  NAMELIST/INP/FILE
  NAMELIST/OK/GO
  NAMELIST/DAT/SOF,J,NSTEP,N,TLAM0,AGLOBE
1  ,EPS2,SMEW0,ISTDME,XST,YST,ZST
C***
  DEFINE FILE 10(60,368,L,KSTEP1)
C***
1 CONTINUE
  PRINT 1002
1002 FORMAT(1H,'TYPE &INP FILE= &END')
  READ(5,INP)
  INF1=FILE(1)
  INF2=FILE(2)
  PRINT 2000,FILE
2000 FORMAT(2I10)
  PRINT 1004
1004 FORMAT(1H,'TYPE &DAT DATA= &END')
  READ(INF1,DAT)
  IF(SOF)GOTO 92
  PRINT 1003
1003 FORMAT(1H,'IF EVERYTHING O.K. TYPE &OK GO=.TRUE.&END')
  GO=.TRUE.
  READ(5,OK)
  IF(GO)GOTO 10
  GOTO 1
10 CONTINUE
C***
  DO 331 I=1,14
  SUM1(I)=0.
331 SUM(I)=0.
C***
  DO 991 J1=1,NSTEP
  KSTEP1=J1
  READ(10,KSTEP1)(XS(I),I=1,11)
1,((PS(I,J7),I=1,9),J7=1,9)
C***
  COST=COS(TLAM0+XS(1)/AGLOBE)
  XS(2)=XS(2)/COST
C***
  DO 302 I=1,9
  DO 302 J8=1,9
  IF(PS(I,J8).LT.0.)PS(I,J8)=100.
302 PS(I,J8)=SQRT(PS(I,J8))
C***

```

```

WRITE(11) (XS(I), I=1, 9)
C***
READ(14) (Z(I3), I3=1, 11)
IF(NSTEP.GT.150) GOTO 923
WRITE(12, 903) J1, (XS(I), I=1, 6), (PS(I, I), I=1, 6)
903 FORMAT(' ', I10, 12F10.3)
WRITE(12, 905) J1, (XS(I), I=7, 9), (PS(I, I), I=7, 9)
905 FORMAT(' ', I10, 6F20.3)
923 CONTINUE
C***NOT TO WASTE TDISK SPACE, WHILE ACTUALLY PROCESSING
C****
... USPD=XS(4)
... VSPD=XS(5)
... WSPD=XS(6)
... XE=XS(1)
... YE=XS(2)*COST
C***XS(2) HAS BEEN REDEFINED AT THE BEGINNING OF THIS PROGRAM.
ZE=XS(3)
VAIR=SQRT(USPD**2+VSPD**2+WSPD**2)
ALPHA=57.3*ATAN2(WSPD, USPD)
BETA=57.3*ATAN2(VSPD, USPD)
HM=-ZE
C***
IF(J1.EQ.1) PRINT 931, XS(1), XS(2)
931 FORMAT(' ', 2F10.0)
C***
IF(NSTEP.GT.150) GOTO 921
C***
TLAM=TLAM0+XE/AGLOBE
COST=COS(TLAM)
SINT=SIN(TLAM)
SMEW=SMEW0+YE/AGLOBE/COST
COSS=COS(SMEW)
SINS=SIN(SMEW)
C1111=1.-.5*EPS2*COS(2*TLAM)
AC1111=AGLOBE*C1111
DO 301 I=1, ISTDME
XDME(I)=AC1111*COST*COSS-(-ZST(I)+AGLOBE*(1.-.5*EPS2*COS(2*XST(I)
1)))*COS(XST(I))*COS(YST(I))
YDME(I)=AC1111*COST*SINS-(-ZST(I)+AGLOBE*(1.-.5*EPS2*COS(2*XST(I)
1))*COS(XST(I))*SIN(YST(I))
ZDME(I)=AC1111*SINT-(-ZST(I)+AGLOBE*(1.-.5*EPS2*COS(2*XST(I)
1))*SIN(XST(I))
RDME(I)=SQRT(XDME(I)**2+YDME(I)**2+ZDME(I)**2)
C*
C* RDME(I)=SQRT((XE-XST(I))**2+(YE-YST(I))**2+(ZE-ZST(I))**2)
C*
301 CONTINUE
C***
WRITE(15, 912) J1, Z(4), VAIR, Z(5), ALPHA, Z(6), BETA, Z(7), HM
1, Z(8), RDME(1), Z(9), RDME(2), XS(7), XS(8), (PS(I, I), I=1, 6)
C*****PRINT 911, J1, Z(4), VAIR, Z(5), ALPHA, Z(6), BETA, Z(7), HM
C****1, Z(8), RDME(1), Z(9), RDME(2), XS(7), XS(8)
911 FORMAT(I4, F4.0, F4.0, 4F4.1, 2F6.0, 4F8.0, 2F4.0)
912 FORMAT(' ', I5, 2F5.0, 4F4.1, 2F6.0, 4F8.0, 2F4.0, 4X, 3F6.0, 4X, 3F5.1)

```

```

C***
TEMP ( 1)=Z ( 4)-VAIR
TEMP ( 2)=Z ( 5)-ALPHA
TEMP ( 3)=Z ( 6)-BETA
TEMP ( 4)=Z ( 7)-HM
TEMP ( 9)=Z ( 8)-RDME(1)
TEMP(10)=Z ( 9)-RDME(2)
TEMP ( 5)=XS(7)
TEMP ( 6)=XS(8)
TEMP ( 7)=XS(10)
TEMP ( 8)=XS(11)
DO 951 I51=1,10
SUM1(I51)=SUM1(I51)+TEMP(I51)
951 SUM (I51)=SUM (I51)+TEMP(I51)**2
GOTO 922
921 CONTINUE
WRITE (15,913) J1, Z(4), VAIR, Z(5), ALPHA, Z(6), BETA, Z(7), HM
1, Z(8), XS(1), Z(9), XS(2), XS(7), XS(8)
913 FORMAT(' ', I5, 2F5.0, 4F4.1, 2F6.0, 4F8.0, 2F4.0, 4X, 18X, 4X, 15X)
C*****PRINT 911, J1, Z(4), VAIR, Z(5), ALPHA, Z(6), BETA, Z(7), HM
C*****1, Z(8), XS(1), Z(9), XS(2), XS(7), XS(8)
922 CONTINUE
C****
C*****PRINT 996, J1, (XS(I), I=1,6)
996 FORMAT(' ', I7, 6F10.3)
C*****PRINT 997, J1, (XS(I), I=7,9)
997 FORMAT(' ', I7, 3F20.3)
991 CONTINUE
C***
IF(NSTEP.GT.60)GOTO 953
DO 952 I=1,8
BIAS(I)=SUM1(I)/60
TEMP2=SUM(I)/59-BIAS(I)**2
IF(TEMP2.LT.0.)TEMP2=100.
952 STDZ(I)=SQRT(TEMP2)
BIAS(9)=SUM(9)/60
BIAS(10)=SUM(10)/60
TEMP3=SUM(9)/59-(BIAS(9)+BIAS(7))**2
TEMP4=SUM(10)/59-(BIAS(10)+BIAS(8))**2
IF(TEMP3.LT.0.)TEMP3=100.
IF(TEMP4.LT.0.)TEMP4=100.
STDZ(9)=SQRT(TEMP3)
STDZ(10)=SQRT(TEMP4)
WRITE(15,914)(PS(I,I),I=1,6),(STDZ(I1),I1=1,4),STDZ(9),STDZ(10)
914 FORMAT(' ', F10.0, 2F10.1, 3F10.0, 4X, F10.0, 2F10.1, 3F10.0)
PRINT 915, (BIAS(I), I=1,4), BIAS(9), BIAS(10), (STDZ(I1), I1=1,4)
1, STDZ(9), STDZ(10)
915 FORMAT(' ', F6.0, 2F6.1, 3F6.0, 7X, F6.0, 2F6.1, 3F6.0)
953 CONTINUE
ENDFILE 12
ENDFILE 15
C***
PRINT 995, (PS(I,I), I=1,6)
995 FORMAT(' ', 6F10.3)
C*** IS THERE ANOTHER RUN TO BE GENERATED?

```

```
GOTO 1
92 CONTINUE
STOP
END
BLOCK DATA
COMMON/DAT0/SOF,J,NSTEP,N,NAMES,TLAM0,AGLOBE
1 ,EPS2,SMEWO,ISTDME,XST(7),YST(7),ZST(7)
DIMENSION J(15),NAMES(38)
LOGICAL SOF
DATA SOF/.FALSE./,J/38,2,23,5,26,6,27,14,24,15,25,29,18,2*0/,
ANSTEP/60/,N/13/
B,TLAM0/.700/,AGLOBE/20940000./
C,ISTDME/2/,XST/.703,.6985,5*.706/,YST/-1.297,-1.2985,5*-1.294/
D,ZST/7*0./,EPS2/.0067/,SMEWO/-1.300/
1,NAMES/'DME1','CLDE',' Q ',' NZ ',' WHDA',' PEDR',' BETA',' P '
2,' R ',' NY ',' NX ',' ALFA',' DME2',' HADT',' LEDF',' TRDE',' THET'
3,' V ',' PSI ',' PHI ',' TRDR',' TRDA',' PODE',' PODT',' PODF',' PODA'
4,' PODR',' VOR1',' HBAR',' ALS ',' LMLS',' GMLS',' VOR2',' INDF',' HDIG'
5,' LGHT',' MDSW',' TIME'/
END
```

APPENDIX C

COMPUTER SYSTEMS FOR PREPROCESSING
AND POST-FLIGHT DATA REDUCTION

Post-flight data handling begins using the HP 1000 digital computer located at Princeton University's Gas Dynamics Laboratory. The raw data is transferred to a 9-track, 1600 BPI magnetic tape that can be processed on either the IBM 4341 or the IBM 3033 computer. The following block-diagram summarizes the described procedure:

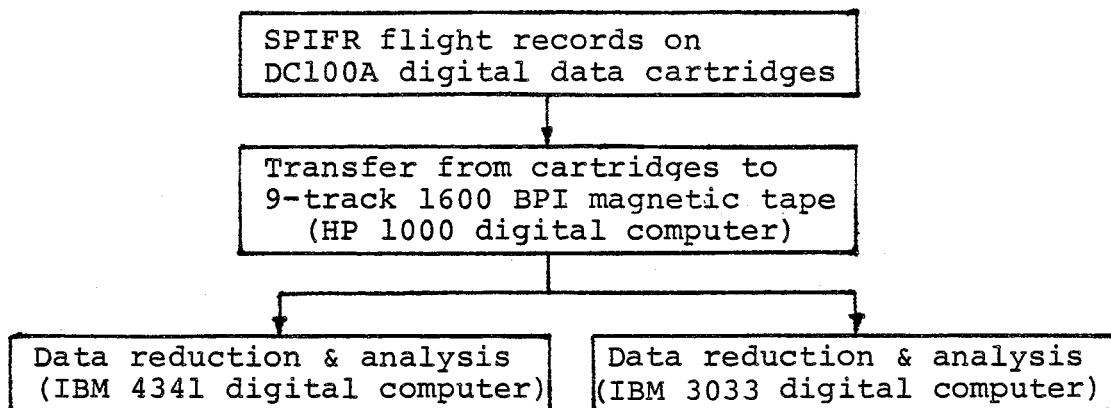


Figure C-1. Data Reduction Procedure.

The FORTRAN program CAT9 controls the transfer from the DC100A cartridges to the 9-track magnetic tape. The FORTRAN program RAWY1 converts 16-bit binary-formatted data into IBM-compatible decimal integer format and arranges the data in physical time vectors. The FORTRAN program SPIFY1 completes the preprocessing by converting the decimal integer time vectors into voltage and then into engineering units, also

converting Indicated Air Speed (IAS) to True Air Speed (TAS).

The SPIFR data storage policy is to preserve both the raw flight-test data and the preprocessed data on magnetic tapes (9-track, 1600 BPI), which makes it compatible for further analysis on both the IBM 4341 and the IBM 3033 machines. Thus, two copies of the raw integer data (RAWY1 output file) and one copy with engineering unit time-vectors (SPIFY1 output file)-for further processing (analysis, tabular printouts or plotting) are preserved.

TRANSFER FROM CARTRIDGES TO TAPE

&CAT9 T=00004 IS ON CR00005 USING 00012 BLKS R=0000

```
0001 FTN4,L
0002 PROGRAM CAT9(3,99), VERSION OF 4 JUNE 1981
0003 C
0004 C PROGRAM TO COPY BINARY DATA FROM CASSETTE TO IBM COMPATIBLE
0005 C TAPE DRIVE.
0006 C
0007 C LOADING THE PROGRAM
0008 C :RU,LOADR,*F4X,%CAT9
0009 C
0010 C RUNNING THE PROGRAM
0011 C :RU,CAT9,P1,P2
0012 C WHERE P1 - IS THE LOGICAL UNIT NUMBER OF YOUR TERMINAL
0013 C P2 - IS THE LOGICAL UNIT NUMBER OF THE MAG TAPE
0014 C
0015 C
0016 C INTEGER Ibuff(128),IMORE,ISTAT,ITLOG,PARMS(5),NBLCK
0017 C EQUIVALENCE (PARMS(1),LUCRT),(PARMS(2),MTLU)
0018 C CALL RMPAR(PARMS)
0019 C NBLCK=0
0020 C***READ FROM LEFT CARTRIDGE LU 4
0021
0022 21 CONTINUE
0023 CALL EXEC(1,100B+4,IBUFF,128)
0024 C GET STATUS
0025 CALL ABREG(ISTAT,ITLOG)
0026 WRITE(LUCRT,47)ITLOG
0027 47 FORMAT(I10)
0028 C CHECK FOR END OF FILE
0029 IF(IAND(ISTAT,200B).EQ.200B) GO TO 22
0030 C CHECK FOR END OF TAPE
0031 IF(IAND(ISTAT,40B).EQ.40B) GO TO 22
0032 C CHECK FOR END OF DATA
0033 IF(IAND(ISTAT,2).EQ.2)GO TO 22
0034 C***WRITE TO TAPE
0035 CALL EXEC(2,100B+MTLU,IBUFF,128)
0036 NBLCK=NBLCK+1
0037 WRITE(LUCRT,31)NBLCK
0038 31 FORMAT(I7)
0039 GOTO 21
0040 22 CONTINUE
0041 IF(ITLOG.LT.128) GO TO 41
0042 CALL EXEC(2,100B+MTLU,IBUFF,128)
0043 NBLCK=NBLCK+1
0044 WRITE(LUCRT,31)NBLCK
0045 41 WRITE(LUCRT,23)
0046 23 FORMAT('PLUG IN NEXT CARTRIDGE AND TYPE 1 OR IF LAST-TYPE 0')
0047 READ(LUCRT,*)IMORE
0048 IF(IMORE.EQ.1)GOTO 21
0049 C WRITE TWO CONSECUTIVE END OF FILE MARKS
0050 CALL EXEC(3,0100B+MTLU)
0051 CALL EXEC(3,0100B+MTLU)
0052 STOP
```

PREPROCESSING - STEP I

FILE: RAWY1 FORIRAN A1 PRINCETON UNIVERSITY TIME-SHARING SYSTEM

```

COMMON/DAT0/SOF,NB
LOGICAL GO,SCF
NAMelist/INP/FILE
INTEGER*2 A3(1200),A2(1700,38)
INTEGER*2 DATA(128)
LOGICAL*1 DALOG(256)
LOGICAL*1 SWLOG(256)
INTEGER*2 DATA1(128)
INTEGER*2 DATA2(128)
EQUIVALENCE (DATA(1),DALOG(1)),(SWLOG(1),DATA1(1))
INTEGER FILE(2)
NAMelist/OK/GO
NAMelist/DAI/SCF,NB
C***
  1 CONTINUE
  PRINT 1002
1002 FORMAT(1H,'TYPE &INP FILE= &END')
  READ(5,INP)
  INF1=FILE(1)
  INF2=FILE(2)
  PRINT 2000,FILE
2000 FORMAT(2I10)
  PRINT 1004
1004 FORMAT(1H,'TYPE &DAT DATA= &END')
  READ(INF1,DAT)
  IF(SOF)GOTO 92
  PRINT 1003
1003 FORMAT(1H,'IF EVERYTHING O.K. TYPE SOK GO=.TRUE.&END')
  GO=.TRUE.
  READ(5,OK)
  IF(GO)GOTO 10
  GOTO 1
10 CONTINUE
C***
  I1=0
  I2=0
C***
  READ(15,17)DATA
  DO 28 I=1,255,2
    SWLOG(I)=DALCG(I+1)
    SWICG(I+1)=DALOG(I)
28 CONTINUE
  GOTO 32
C***
  99 CONTINUE
  DO 30 I=1,128
  30 DATA2(I)=DATA1(I)
  READ(15,17,END=100)DATA
  17 FORMAT(128A2)
  DO 29 I=1,255,2
    SWLOG(I)=DALCG(I+1)
    SWICG(I+1)=DALOG(I)
  29 CONTINUE
C***
  DO 31 I=1,128

```

```

IF (DATA2(I) .NE. DATA1(I)) GOTO 32
31 CONTINUE
GOTO 99
32 CONTINUE
C***
I1=I1+1
IF (I1.EQ.8) GOTO 417
DO 421 M=1,128
M3=M+(I1-1)*128
421 A3(M3)=DATA1(M)
GOTO 99
417 DO 418 M=1,92
M3=M+(I1-1)*128
418 A3(M3)=DATA1(M)
C***M3=1-(128*8-36);I1=0-8;I2=NC. OF 2048-BYTE BLCCKS,
C***READ FROM TAPE INTO A3(EACH OVERWRITING THE PREVIOUS).
I2=I2+1
K1=26*(I2-1)+1
K2=K1+25
C*K HAS A SPAN OF 26 AS 1024=38*26+36
C***
J7=0
DO 431 K=K1,K2
IF (K.GT.NB) GOTO 437
DO 432 J=1,38
432 A2(K,J)=A3(J7+J)
J7=J7+38
431 CONTINUE
I1=0
GOTO 99
100 CONTINUE
C***
PRINT 441
441 FORMAT(1H , 'EOT; DECREASE NB AND RERUN AS A NEW JOB')
C***
437 CONTINUE
KSCF=K-1
27 FORMAT(1H , I10)
PRINT 27, KSCF
DO 531 J=1,38
531 WRITE(9) (A2(K0,J) , K0=1, KSCF)
ENDFILE 9
C***
GOTO 1
92 CONTINUE
STCP
END
BLCK DATA
COMMON/DATC/SOF,NB
LOGICAL SOF
DATA SOF/ .FALSE. /, NB/256/
END

```

PREPROCESSING - STEP II

FILE: SPIFY1 FORTRAN A1 PRINCETON UNIVERSITY TIME-SHARING SYSTEM

```

COMMON/DAT0/SOF,V Slope,VCONST,PHSLOP,PHCONS,N11,DPNSTD
INTEGER FILE(2)
DIMENSION A3(1700,38),PHSLOP(55),PHCONS(55)
INTEGER*2 A2(1700,38)
LOGICAL GO,SCF
NAMELIST/INP/FILE
NAMELIST/OK/GO
NAMELIST/DAT/SOF,V Slope,VCONST,PHSLOP,PHCONS,N11,DPNSTD
1 CONTINUE
PRINT 1002
1002 FORMAT(1H,'TYPE &INP FILE= &END')
READ(5,INP)
INF1=FILE(1)
INF2=FILE(2)
PRINT 2000,FILE
2000 FORMAT(2I10)
PRINT 1004
1004 FORMAT(1H,'TYPE &DAT DATA= &END')
READ(INF1,DAT)
IF(SCF)GOTO 92
PRINT 1003
1003 FORMAT(1H,'IF EVERYTHING O.K. TYPE &OK GO=.TRUE.&END')
GO=.TRUE.
READ(5,OK)
IF(GO)GOTO 10
GOTO 1
10 CONTINUE
C***
DO 501 J=1,38
501 READ(9)(A2(I,J),I=1,N11)
C***NOW-INTO REAL PHYSICAL DATA.
DO 512 I=1,N11
ISIGN=0
IF(A2(I,1).LT.0)ISIGN=1
C***65535=2**16-1, BECAUSE IF LEFTMOST OF THE 16-ZEROS-AND-ONES-FIELD
C***IS ONE, IT ITSELF IS INTERPRETTED AS MINUS AND EACH OF THE OTHER
C***15 BITS IS CHANGED(ONES TO ZEROS AND ZEROS TO ONES).
C***THUS, E.G., A 16-ONES-FIELD IS INTERPRETTED AS -0 INSTEAD OF 2**16-1
C***AND A ONE FOLLOWED BY 15 ZEROS IS -(2**15-1) INSTEAD OF 2**15
512 A3(I,1)=A2(I,1)+ISIGN*65535
DO 502 I=1,N11
DO 503 J=2,12
ISIGN=0
IF(A2(I,J).LT.0)ISIGN=1
503 A3(I,J)=((A2(I,J)+ISIGN*65535)*VSLOPE/16.+VCONST)*PHSLOP(J)+
1PHCONS(J)
502 CONTINUE
C***
DO 521 I=1,N11
ISIGN=0
IF(A2(I,13).LT.0)ISIGN=1
521 A3(I,13)=A2(I,13)+ISIGN*65535
DO 522 I=1,N11
DO 523 J=14,34
ISIGN=0

```

```

        IF (A2 (I,J) .LT.0) ISIGN=1
523  A3 (I,J) =(((A2 (I,J) +ISIGN*65535) *VSLOPE/16. +VCONST) *PHSLOP (J) +
        1PHCONS (J))
522  CONTINUE
C***
        DO 514 I=1,N11
        DO 515 J=35,38
        ISIGN=0
        IF (A2 (I,J) .LT.0) ISIGN=1
515  A3 (I,J) =A2 (I,J) +ISIGN*65535
514  CONTINUE
C***
        DO 591 I=1,N11
591  IF (A3 (I, 19) .LT.0.) A3 (I, 19) =A3 (I, 19) +360.
C***
        DO 601 I=2,N11,2
601  A3 (I, 1) =A3 (I, 13)
        DO 602 I=3,N11,2
602  A3 (I, 1) =.5*(A3 (I-1, 1) +A3 (I+1, 1))
        A3 (1, 1) =A3 (2, 1)
        N111=N11-2
        DO 603 I=2,N111,2
603  A3 (I, 13) =.5*(A3 (I-1, 13) +A3 (I+1, 13))
        A3 (N11, 13) =A3 (N11-1, 13)
C***
C***PRAT=PRATIO;RRAT=RRATIO
        DO 611 I=1,N11
        PRAT= (A3 (I, 29) +DPNSTD) /1013.3
        RRAT=PRAT**.81
        A3 (I, 18) =1.689*A3 (I, 18) /SQRT (RRAT)
        HCONST=EXP (ALOG (PRAT) /5.256)
        A3 (I, 29) = (1-HCONST) /.00000689
611  CONTINUE
C***
C***NOT TO LOSE ACCURACY,THE TIME VECTORS ARE STORED UNFORMATTED,I.E.
C***USING UNFORMATTED READ(AND WRITE WHEN RETRIEVING FOR FURTHER
C***PROCESSING).
        DO 121 J=1,38
121  WRITE (10) (A3 (I,J) ,I=1,N11)
        ENDFILE 10
C***IS THERE ANOTHER RUN TO BE GENERATED?
        GOTC 1
92  CONTINUE
        STOP
        END
        BLOCK DATA
        COMMON/DAT0/SOF,VSLOPE,VCONST,PHSLOP,PHCONS,N11,DPNSTD
        DIMENSION PHSLOP (55) ,PHCONS (55)
        LOGICAL SOF
        DATA SOF/ .FALSE. /,VSLOPE/.004884/,VCONST/-10./,
        1PHSLOP/1.,1.6583,-2.7604,-.20555,-8.2085,.2557,
        2-3.0754,4.0811,-3.4664,-.05184,.05519,2.8611,
        31.,.0508,.1020,-5.,3.1338,5.0623,
        418.2787,-8.1864,5.,-5.,2.4703,.0513,
        55.1310,-1.9589,2.4074,1.,15.275,2.8611,

```

```
6.25,.10,1.,.1,1.,3*1., SE
717*1./, SI
8PHCONS/0.,-3.2009,.458,-.02467,-.5304,.1055, SE
9-,1019,-.0427,-.2048,-.0019,-.01233,13.7125, SI
A0.,.492,-.0017,0.,.3805,99.9689, SE
B.0984,-.4821,0.,0.,-4.0193,.513, SI
C-23.8869,1.5698,3.5703,0.,950.,13.7125, SI
D0.,0.,0.,0.,0.,0.,0.,0., SI
E17*0./, SI
FN11/10/ SE
G,DENSTL/0./ SE
END SE
```

APPENDIX D

INTEGRATION OF DISTANCE MEASURING EQUIPMENT (DME) INTO THE DATA COLLECTION SYSTEM

The DME component of the navigation/communication system has been integrated into the onboard experimental setup with the capability to sequence automatically available navigation stations and process the distance information using microprocessor control. The navigation/communication (NAV/COM) and the DME are part of the Bendix "BX-2000" product line of aircraft avionics. A digital information format is used in the Bendix NAV/COM and DME for frequency tuning. The DME receiver output to the pilot's indicator is a pulse-width signal which is compatible with digital processing techniques.

This appendix is sub-divided into sections relating to the external (microprocessor) tuning, distance signal decoding, and an overview of the DME system and specifications. The first two sections are specific to the Bendix system.

D-1. EXTERNAL DME TUNING

The Bendix DM-2031A DME receiver/transmitter has provisions for both "2 out of 5" tuning which is compatible with other manufacturers systems and a serial binary-coded-decimal (BCD) tuning. The serial tuning method is used by the Bendix NAV/COM and is implemented in the microprocessor tuning for compatibility. When the Bendix DME is installed with the Bendix NAV/COM, the DME serial tuning signal is the same one which is used for tuning the NAV receivers. As shown in Figure D-1, a switch located on the NAV/COM (Bendix CN-2011A) permits the pilot to select DME tuning paired with either NAV 1 or NAV 2. In the center-off or hold (H) position, no tuning signal is sent to the DME. Under this condition the DME continues to hold the last tuning selection and station frequency. The tuning signal contains a BCD format of the paired NAV frequency. (The NAV frequency is not the actual frequency used in the DME system, as will be explained in the overview section.)

The tuning signal is in the form of a twenty-bit asynchronous pulse-width modulated serial word. The serial data word format is shown in Figure D-2. The basic period of each word is 4.0 msec, and when supplied by the NAV/COM; the word rate is 250 Hz. However, a single word is sufficient to tune the DME. Note that the same format is used for the COM, NAV, DME and GS (glide slope) units in the Bendix product line. The first bit in the word is the synchronizing pulse. Each bit after the first is dedicated to a specific piece of information. The value of bits 2 through 7 is ignored in the current DME, but future units may use these bits as a device code.

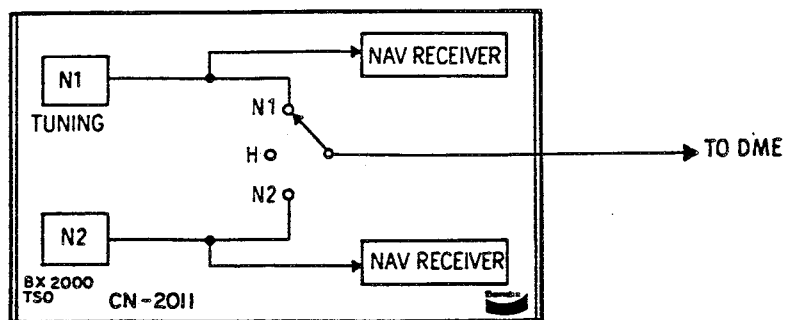


Figure D-1. DME Tuning Via NAV/COM.

	SYN _C	ES _T	X	TX	X	X	X	10MHz		1 MHz		0.1 MHz				0.25 MHz (COM ONLY)				
COM								2	1	8	4	2	1	8	4	2	1	4	2	1
NAV/GS		X	X	X	X	X	X	2	1	8	4	2	1	8	4	2	1	4	2	1
DME		X	X	X	X	X	X	2	1	8	4	2	1	8	4	2	1	4	2	1
	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20

4.0 MILLISECONDS

Figure D-2. Serial Data Word Format.

The bit format is shown in Figure D-3. Synchronization, logic "1", and logic "0" bits correspond to 150-, 100- and 50-microsecond duration pulses respectively. The decoder inside the DME (as well as NAV, COM and GS) is relatively tolerant of the actual pulse width (and word length) of the incoming signal. As mentioned previously, the synchronizing pulse (bit 1) indicates the beginning of the serial data word. During the synchronizing pulse, the signal level stays at logic 1 for 150 microseconds (nominal). The Bendix circuitry samples each bit at 125 microseconds to determine if that bit is the synchronizing pulse. A similar sample is made at 75 microseconds to differentiate logic 1 and logic 0 pulses. Hence, the minor variation in the pulse widths of the tuning signal will not compromise the proper functioning of the system.

A microprocessor software program which generates the bit pulses and data word format to tune the DME was written using simple software timing loops. This program was verified using an oscilloscope to check the pulse widths and data word format. Software programming of the station sequencing was not completed in time for implementation on the test program. The alternative tuning method to be described latter is an interim solution.

Electrical (hardware) interfacing for microprocessor tuning output to the DME input is shown in Figure D-4. A signal inversion is employed at the NAV/COM's DME tuning signal output (this was not shown in Figure D-1 for clarity) and the signal is again inverted at the DME. Thus, the signals on the interconnecting wires are inverted with respect to Figure D-3. The high level (pull-up) voltage

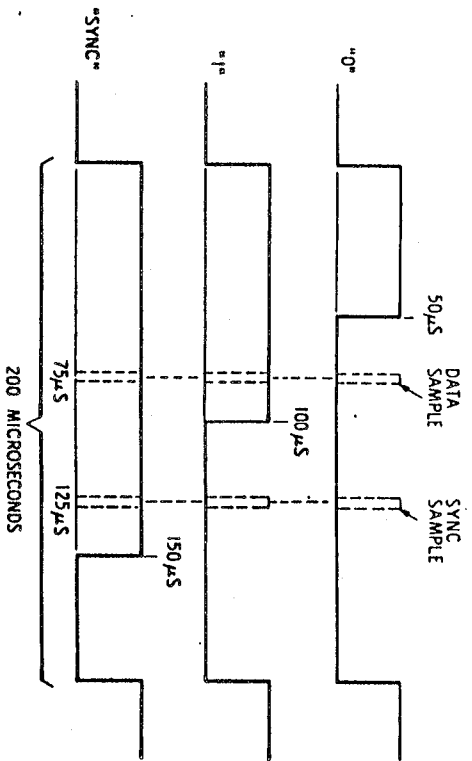


Figure D-3. Bit Format.

is 12 to 15 volts. An open collector buffer, preferably with a 12 volt pull-up, may be used at the microprocessor side of the interface.

The alternative tuning method used in the current testing also is shown in Figure D-4. A switch located on the avionics section of the instrument panel allows the pilot to select normal NAV/COM (N) tuning or remote microprocessor (EXT) tuning. In the EXT position either the NAV 1 or NAV 2 tuning signal is routed to the DME, depending on the position of the relay shown. The relay is driven by a discrete digital output of the microprocessor. No changes in software logic were required for this implementation since the relay was driven in parallel with the "computer functioning" light on the instrument panel. The present rate of 0.5 Hz allows sufficient time for DME station lock-on and measurement of distance.

The selection switch N/EXT provides an additional function. In the EXT position, the displayed DME distance available on the one pilot's electronic course deviation instrument (ECDI) is blanked. The primary center panel DME indicator is not blanked, and the microprocessor station tuning of the DME can be verified by the safety pilot. The primary DME indicator can be switched by the safety pilot to display elapsed time or other function during flight tests.

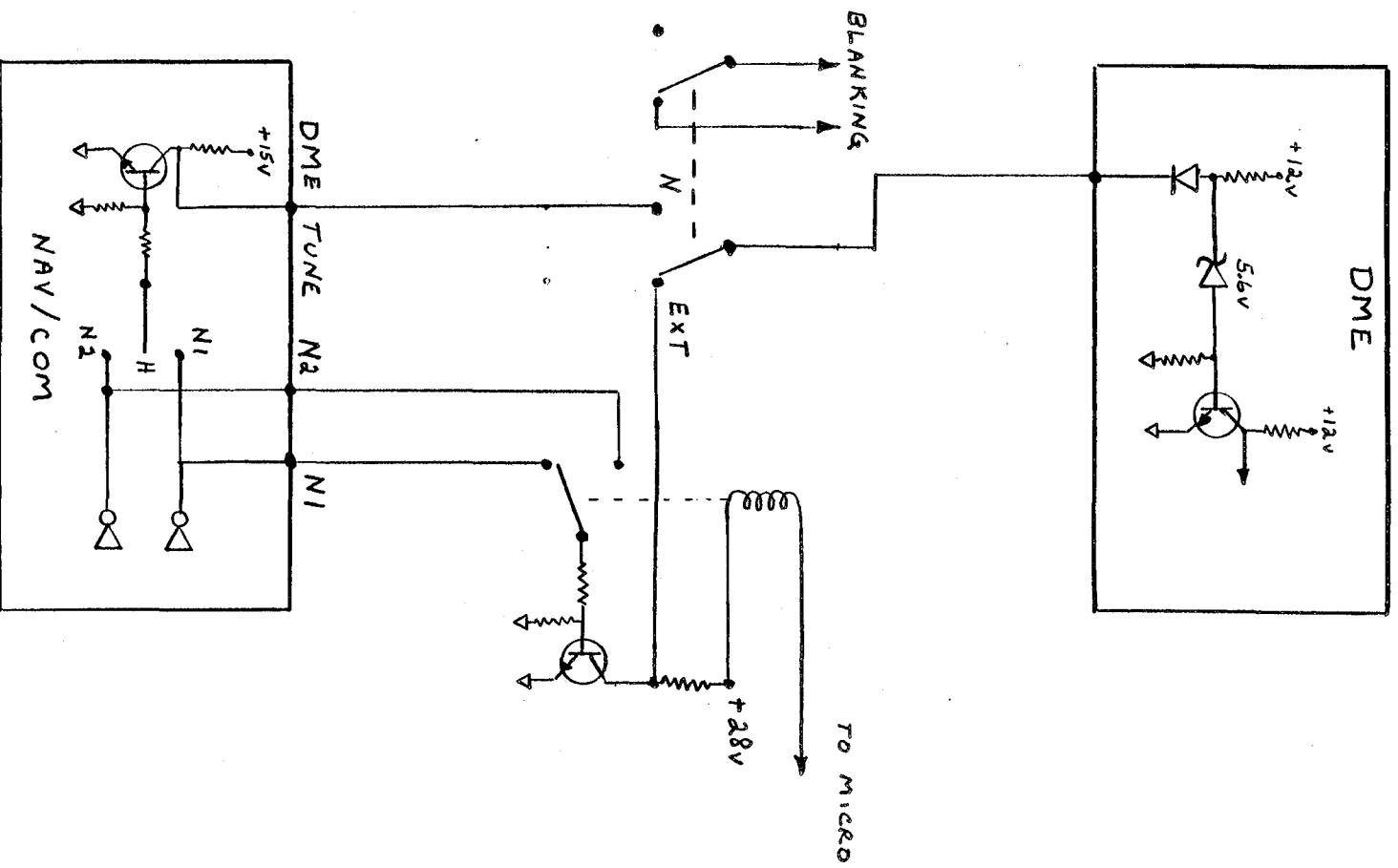


Figure D-4. DME Tuning Electrical Interface.

D-2. DME DISTANCE SIGNAL DECODING

Three signal outputs are generated by the Bendix DM-2031A DME receiver/transmitter: a pulse pair (RP1 and RP2) and a status signal (SEARCH). The time interval between RP1 and RP2 represents the slant range distance to the DME ground station. The digital logic interface, shown in Figure D-5, processes these three signals upon a DATA READ signal from the microprocessor. The distance represented the difference (RP2 - RP1) is presented to the microprocessor as a 16-bit (2-byte) word. The high-order bit of this data word is used to indicate the DME status (SEARCH).

The difference (RP2 - RP1) is measured by a 16-bit digital counter using a crystal controlled oscillator which operates at a frequency of 18 MHZ. Using the principle that RF energy travels one nautical mile and returns in 12.359 microseconds, the slant range from the aircraft to the ground station can be determined. Since the high-order bit is used for the status SEARCH signal, the maximum distance reading (15 bits) is 147 nautical miles. Although the interface clock frequency of 18 MHZ would suggest a measurement (counter) bit resolution of 27 feet, the actual resolution is determined by the processing within the Bendix DM-2031A. The LSI (large-scale-integration) chip that generates these pulses uses a 1.6 MHZ clock (actually 1.61825 MHZ) which limits the (RP2 - RP1) difference increments to the equivalent of 0.05 nautical miles. Some other factors influencing measurement accuracy are discussed in the overview section.

The digital logic interface is presented in a simplified block diagram form in Figure D-6 for discussion of interface

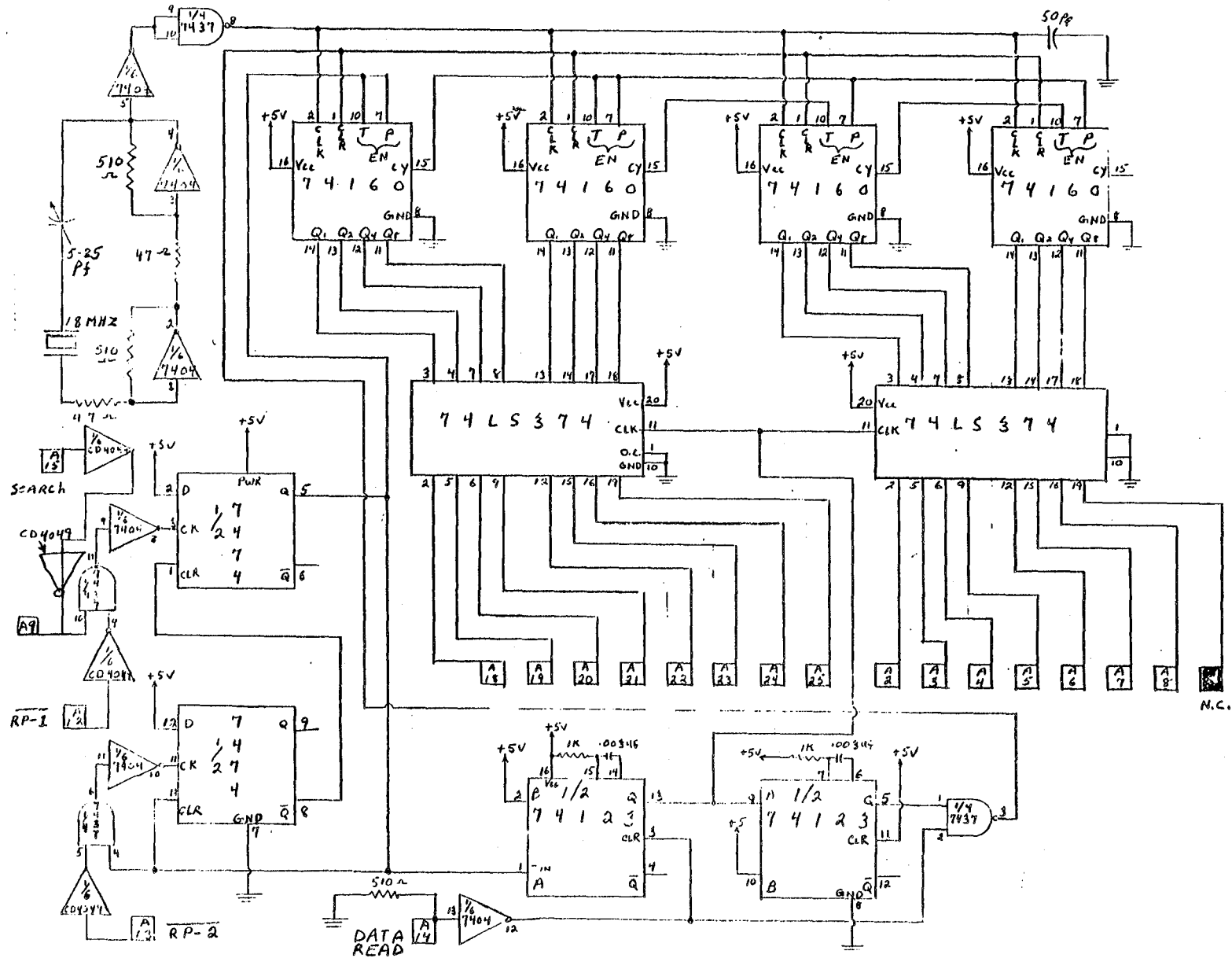


Figure D-5. DME - Microprocessor Electrical Interface.

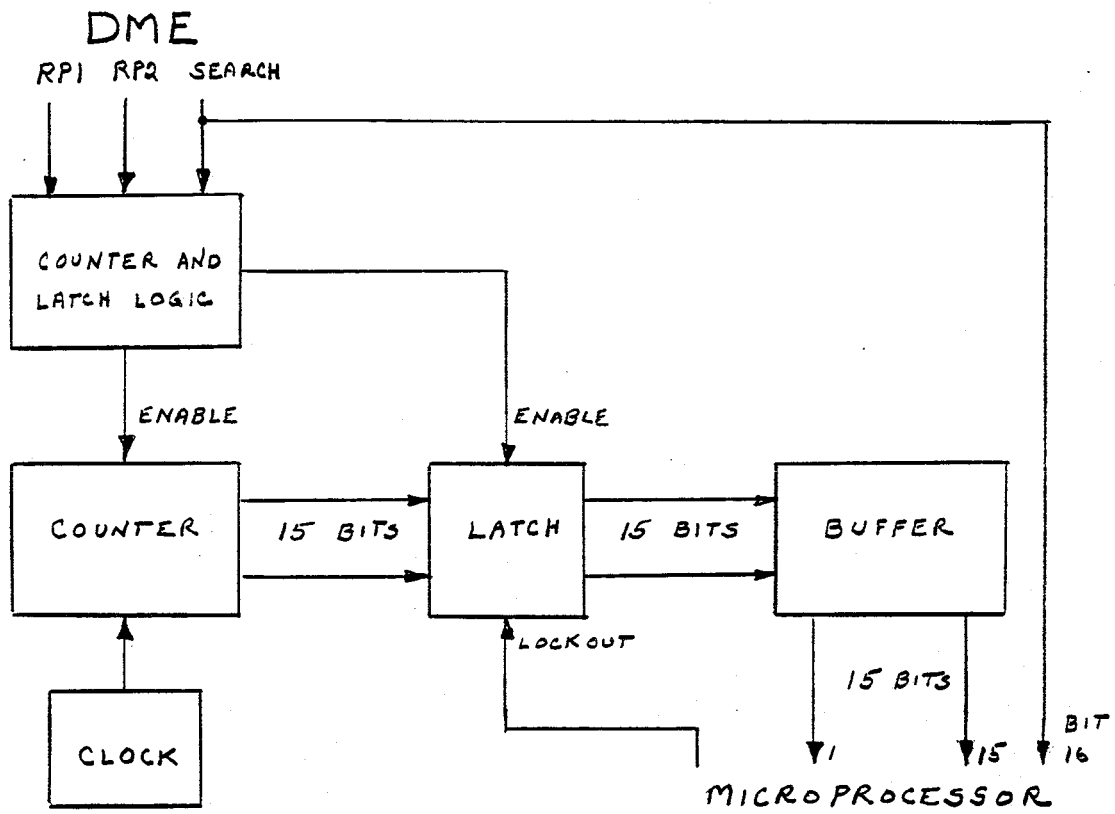


Figure D-6. DME Interface Block Diagram.

operation. The status of SEARCH is used to enable the counter as a precaution, although the absence of pulses RP1 and RP2 would preclude counter operation. The counter is started from a previously cleared (zero) value by the RP1 pulse from the DME. As noted previously, the counter rate is determined by the 18 MHz reference clock. The count is stopped by the RP2 pulse.

Two other events occur after receipt of RP2. After a very short delay, the count is transferred to the buffer via the latch control; when this operation is completed, the counter is reset or cleared. This chain of events continues to cycle as long as the signal DATA READ is not asserted by the microprocessor data collection system. Counter and buffer updates will take place at a 21 Hz rate during normal DME operation. When the microprocessor generates a DATA READ request, transfer of counter information to the buffer is inhibited. This signal is maintained by the microprocessor until the buffer has been read. This mode of operation guarantees that some data will be available so that the microprocessor will not "hang" in a wait state. The data in the buffer will normally be valid distance information measured within the last .05 sec of receipt of DATA READ. The signals RP1 and RP2 are not the raw pulses used by the DME interrogating a ground station; rather, they are generated by a sophisticated LSI chip. Corrections for delays in turnaround at the ground station and within the Bendix unit are applied so that the (RP2 - RP1) difference has no bias for true zero distance. Upon loss of the DME station, the (RP2 - RP1) pulses will continue to be sent by the LSI chip for up to 10 sec. A correction also is made to maintain the same rate of change (groundspeed) as observed

prior to station signal loss. The correction is 80% of the preobserved groundspeed to prevent a "backing up" indication on the pilot's indicator when the signal is reacquired. The consequences of the above and other effects are discussed in the following overview section.

D-3. DME/DATA COLLECTION OVERVIEW

The purpose of the DME system is to provide the pilot with slant range distance information from the aircraft to a selected DME ground facility. The system transmits interrogation signals in the form of pulse pairs to the selected ground station. The DME ground facility receives the interrogation signal and returns a reply signal (again a pulse pair) for each interrogation received. Multiple aircraft may interrogate the DME ground station.

The DME system operates in the frequency range of 978 MHz to 1212 MHz. There are 200 DME channels which are paired with VHF NAV frequencies between 108.00 MHz and 117.95 MHz (100 "X" channels and 100 "Y" channels). For example DME channel 85X is paired with NAV frequency 113.80 MHz. The aircraft transmits the interrogation pulses at 1109 MHz and receives the reply offset by 63 MHz at 1172 MHz. (Some X channels are offset below the transmission frequency.) On the .05 spacing VHF frequencies such as 113.85 MHz (paired DME channel 85Y) the same transmission frequency is used but the reply is offset opposite to that used for the X channel (1046 MHz). Since some electrical processing delay will take place from receipt of interrogation signal to reply signal, all replies are adjusted to a specific delay to permit accurate measurement of the elapsed time by the airborne distance measuring circuits. This delay is 50 μ sec for "X" stations and 56 μ sec for Y stations (measured between the first pulse of interrogation to the first pulse of reply).

The interrogation pulse pairs are spaced at 12 μ sec for X channels and 36 μ sec for Y channels. The reply pulse

pairs are 12 μ sec and 30 μ sec for X and Y respectively.

The DME ground facility continuously transmits a nominal 2700 pulse pairs per second squitter signal with a 1350 Hz identification morse code signal at 30-second intervals. The 1350 Hz identification signal consists of groups of evenly spaced pulse pairs. The ground station provides a reply pulse pair that replaces a squitter pulse pair 50 μ sec after receiving an interrogation. The identification signal is available to the pilot as an audio tone to verify tuning and station selection.

When the DME is first tuned to a ground station, it must determine which reply pulses are to its interrogation pulses as opposed to those meant for other aircraft. Old model DME equipment frequently took 20 seconds or longer to achieve a lock-on and track. The Bendix DM-2031A specification for lock-on is less than 1 second. During the search period the interrogation rate is increased to 140 pulse pairs/sec to improve the detection time. This is reduced to 21 interrogations per sec during track. All DME units also use a variable pulse repetition rate to prevent synchronization of distance replies between other DME aircraft interrogators. A random jitter of the interrogation rate about the nominal of $\pm 1\%$ is used in the Bendix DM-2031A.

The specification measurement accuracy of the Bendix DM-2031A is ± 0.1 nautical mile or .15 percent, whichever is larger. The minimum indication on the pilot's display of the Bendix DME system is 0.1 nautical mile. The output resolution of the signal to the indicator (RP1 - RP2) pulses is 0.05 nautical mile.

A possible source of error, both at the ground station and in the aircraft processing circuits, is proper pulse delay processing. The DME ground station error specification is ± 0.1 nautical miles indicating that the pulse delay (50 μ sec on channel X) is within 1.2 μ sec. This type of error, at a given ground station, and airborne unit should be predictable and could be removed from the data. Determination of this error is predicated on range measurement of multiple DME stations by the aircraft. A small dynamic error occurs with the data collection system since the measurement time may be in error by the update period (approximately 0.05 sec). In the implementation discussed here, an error due to signal loss is possible. Time difference information can continue up to 10 seconds after signal loss as mentioned previously. With the present scheme of sequencing stations every 2 seconds, the memory circuit is only partially charged, and it is unlikely that a memory generated signal will be obtained.

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