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A STUDY OF OPTIMUM COWL SHAPES AND FLOW
PORT LOCATIONS FOR MINIMUM DRAG WITH
EFFECTIVE ENGINE COOLING - VOLUME II

Stan R. Fox and Frederick O. Smetana

NORTH CAROLINA STATE UNIVERSITY
Raleigh, North Carolina 27650

NASA Grant NSG-1584
November 1980

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National Aeronautics and
Space Administration

Langley Research Center
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ABSTRACT

The successful prediction of the performance of a new or modified aircraft depends heavily on an accurate estimation of its lift and drag. This report consists of the listings, user's instructions, sample inputs, and sample outputs of two computer programs which are especially useful in obtaining an approximate solution of the viscous flow over an arbitrary non-lifting three-dimensional body. The first program performs a potential flow solution by a well-known panel method and readjusts this initial solution to account for the effects of the boundary-layer displacement thickness, a nonuniform but unidirectional onset flow field, and the presence of air intakes and exhausts. The second program is effectually a geometry package which allows the user to change or refine the shape of a body to satisfy particular needs without a significant amount of human intervention.

The report represents in part an effort to reduce the cruise drag of light aircraft through an analytical study of the contributions to the drag arising from the engine cowl shape and the forward fuselage area and also that resulting from the cooling air mass flowing through intake and exhaust sites on the nacelle. The programs may be effectively used to determine the appropriate body modifications or flow port locations to reduce the cruise drag as well as to provide sufficient air flow for cooling the engine.

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INTRODUCTION

For the past contract year a research program has been conducted for the purpose of reducing the cruise drag of light aircraft for better performance and fuel economy through studying the effects arising from modifications to body shape and the surrounding flow field. The procedures have been described [1] and coded into two FORTRAN computer programs.

The purpose of this report is to present these programs with their complete user's instructions. Sample inputs and outputs are also given to provide references for proper program executions at other computing installations.

The first program - FLOWBODY - performs a potential flow solution by the Hess low-speed panel method [1], [2], [3] and readjusts this initial solution to account for the effects of the boundary-layer displacement thickness, a nonuniform but unidirectional onset flow field, and the presence of air intakes and exhausts. The logic of the program can conveniently be described by the following steps:

- (1) The surface of the isolated fuselage is represented by a sufficiently large number of quadrilaterals or four-sided panels.
- (2) All four corners of the panel are moved into the same plane through a procedure which determines the direction of the normal.
- (3) A nonuniform onset flow field may be superimposed onto the uniform onset flow field.

- (4) A source of undetermined strength is placed on each panel, and the prescribed normal boundary condition is required to be satisfied.
- (5) The resulting system of equations are solved for the source strengths from which the velocity and pressures over the body surface are calculated.
- (6) The system of equations may be resolved for the source strengths to account for the presence of air intakes and exhausts.
- (7) Two-dimensional, momentum-integral-type boundary layer computations are performed along the streamlines to find the local values of displacement thickness and wall shear.
- (8) The wall shear is integrated over the surface to find the skin friction drag.
- (9) The body shape is modified by attaching a wake-body toward the trailing edge and by accounting for the displacement thickness effects.
- (10) A new set of source strengths and surface pressures corresponding to the wake-body shape is calculated.
- (11) The surface pressures are integrated to find the lift and pressure drag.
- (12) The total drag is determined from the sum of the skin friction drag and the pressure drag.

The second program = GRIDPLOT - is a geometry package which may be used to correct body misrepresentations, to change the body geometry, to refine the network or grid of the panels or quadrilaterals that form the surface of the body, and to plot various orthographic, perspective, and stereoscopic views of the

original and the modified body. The workhorse of this program is a cubic-spline curve-fitting method coupled to a coordinate-system rotation-translation technique that is very effective in modeling body shapes with regions of high curvature or changes in slope.

The U. S. customary units used in this report reflect those most commonly used in this country by engineers and scientists in the General Aviation field. The reader may choose to use S.I. units in lieu of U. S. customary units in both FLOWBODY and GRIDPLOT programs with only one restriction in the FLOWBODY program. If locations for air intakes and exhausts are to be specified, U. S. customary units must be used throughout FLOWBODY since the constants in the derivations for internal mass flow obtain from U. S. customary units. Otherwise, S.I. units are completely permissible.

USER'S INSTRUCTIONS - FLOWBODY PROGRAM

The program is written in FORTRAN IV and is designed to execute in single precision on an IBM 370/165 computer with an average execution time of 4 minutes 40 seconds for typically large data set. An average execution requires approximately 426,000 bytes of core storage. The program accepts multiple data sets.

Given a data set describing the half-body* under consideration, the program may be instructed to calculate an approximate solution of the three-dimensional viscous flow over an arbitrary body and to estimate the body lift and drag coefficients with or without

- (a) a simulated propeller slipstream, and
- (b) mass flow through the body.

The orientation of the body with respect to the body reference axes for the programs is shown in Figure 1.

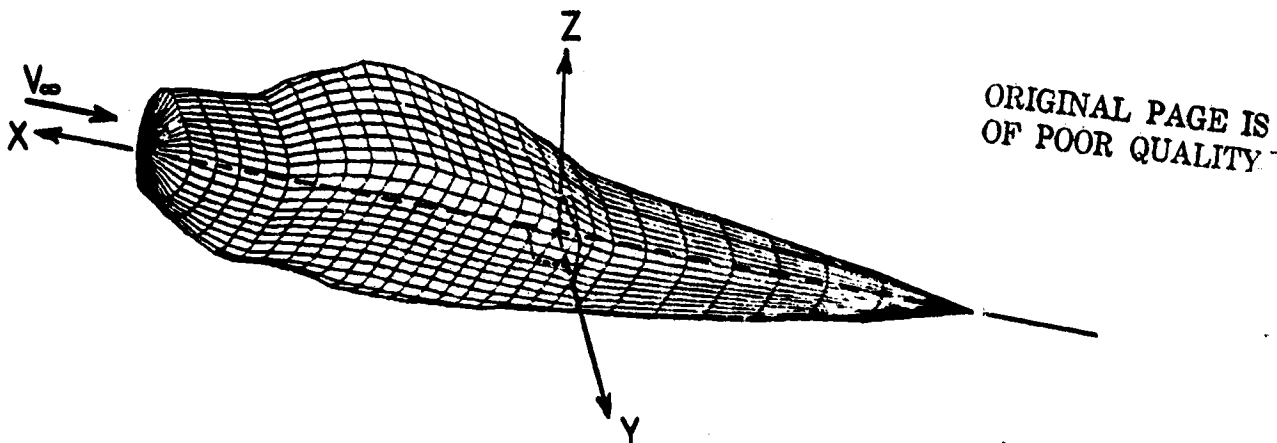


Figure 1: Orientation of the body with respect to the body reference axes

*Since the body is considered to be symmetrical about the X-Z plane, only half of the body is needed to describe the entire body.

The program requires the specification of the following input in the indicated order:

CARD 1:

The read unit number IDS: _

IDS is a right-adjusted integer number occupying columns 1-5 and specifying that the data is to be read from cards, magnetic tape, disk, etc. The user must supply the suitable job control cards for the specific reads. The IDS parameter controls only the reading of CARD 2, CARD 7, and the Body Description cards.

CARD 2: _

The title array TITLE: _____

The 80 characters of the array TITLE are used for identifying output. The reading of TITLE is controlled by the read unit number IDS.

**** The Flow Control Variables ****

CARD 3:

Columns	FORTTRAN Name	Description
1-20	VINF	Reference free-stream velocity (ft/sec)
21-40	VO	Kinematic viscosity of the fluid in which the body is moving (ft ² /sec)
41-60	ROE	Density of the fluid in which the body is moving (slug/ft ³)
61-80	REFA	Reference area upon which the aerodynamic coefficients will be based (ft ²)

Parameters VINF, VO, ROE, and REFA are single-precision floating-point numbers in E20 fields.

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CARD 4:

Columns	FORTRAN Name	Description
1-20	HVF	Heat of combustion of the fuel being used to develop engine power (BTU/lb _m)
21-40	SFC	Specific fuel consumption of the engine (lb _m /ft-lb _f)
41-60	DEP	Developed engine power or power into airstream (ft-lb _f /sec)
61-80	CPHA	Specific heat at constant pressure for air (BTU/lb _m °R)

Parameters HVF, SFC, DEP, and CPHA are single-precision floating-point numbers in E20 fields.

CARD 5:

Columns	FORTRAN Name	Description
1-20	TINF	Reference free-stream temperature (°R)
21-40	EOA	Effective orifice area-representative of that area seen by the cooling fluid passing through the body and about the body (ft ²)
41-45	IWRITE	Control variable which denotes the amount of output the user desires. IWRITE = 0 yields the normal maximum output ever desired by the user. IWRITE = 1 deletes information given for each input point. IWRITE = 2 deletes streamline and boundary layer information as well as input point information. IWRITE < 0 generates an enormous amount of output dealing with the streamline calculations, and therefore this option should be used with caution.
46-50	IPCH1	Control variable which denotes the punching of the input cards in a form compatible to the NCSU PLOT program of Reference 3. IPCH1 = 0 yields no punched cards, while IPCH1 = 1 produces punched cards.

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CARD 5 (continued):

Columns	FORTRAN Name	Description
51-55	IPCH2	Control variable which denotes the punching of cards of the body after the addition of the wake-body in a form compatible to the NCSU PLOT program of Reference 3. IPCH2 = 0 yields no punched cards, while IPCH2 = 1 produces punched cards.
56-60	IMATCH	Control variable which denotes the matching of the simulated slipstream's power to the specified power into the airstream. With IMATCH = 0, the matching is performed. With IMATCH = 1, no matching occurs and the program utilizes the user-supplied values. Normally, IMATCH = 0 should be specified for an overall program compatibility.

Parameters TINF and EOA are single-precision floating-point numbers in E20 fields, while parameters IWRITE, IPCH1, IPCH2, and IMATCH are right-adjusted integer numbers in I5 fields.

**** Conversion and Test Parameters ****

CARD 6:

Columns	FORTRAN Name	Description
1-10	CF	Conversion factor to change the units of the body coordinates points to units of feet. If CF = 0.0, the program automatically sets CF = 1.0. If CF = 1.0, the program assumes that the data units are compatible.
11-15	ITEST	Control parameter which allows only sufficient information of the propeller-slipstream (or series of vortex rings) calculation to be performed for the plotting of the location and diameter of the vortex rings and the induced velocity of such an arrangement of rings. (See Figure 2). ITEST = 0 produces no plots, while ITEST = 1 does.

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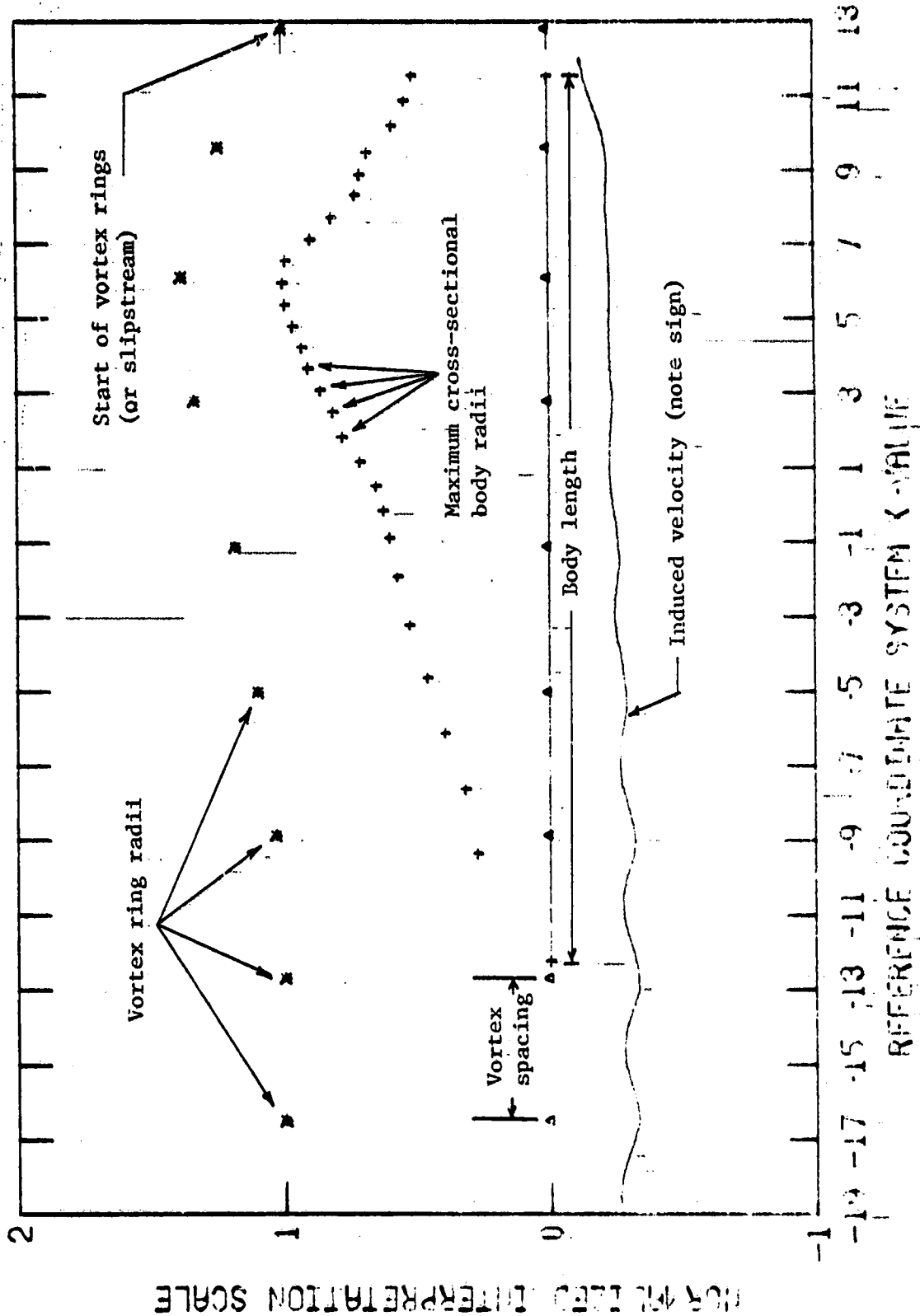


Figure 2: Typical plot of the location and radii of the vortex rings as well as the induced velocity of such an arrangement of rings

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CARD 6 (continued):

Columns	FORTTRAN Name	Description
16-20	NODE	Control parameter--equal in value to the node or panel number in question-- that generates additional output in that portion of the streamline calculation near the specified node or panel. NODE = 0 produces no additional output, while NODE = "panel number" does.

Parameter CF is a single-precision floating-point number in a F10 field.

Parameters ITEST and NODE are right-adjusted integer numbers in I5 fields.

CARD 7:

The number NQE of quadrilaterals or panels of the input half-body data:

Occupying columns 1-4 in an I4 field, NQE is a right-adjusted integer number determined by the product

$(\text{maximum MI} - 1) * (\text{maximum NI} - 1)$

where MI and NI are defined later. NQE should be restricted in value to approximately 600 because of the array dimensions in the program. The resulting of NQE is controlled by the read unit number IDS.

CARD 8: ** Ring Vortex Systems--Propeller Slipstream **

Columns	FORTTRAN Name	Description
1-5	NSRV	Number of independent ring-vortex systems. Normally NSRV = 1 or 0.
6-10	ISPACE	Generation parameter for ring vortices. If ISPACE = 0, no automatic generation and spacing of ring vortices are performed. If NSRV > 1, ISPACE must be equal to zero. If ISPACE > 0, NSRV is set equal to 1 and the program is permitted to generate a system of ring vortices.
11-20	XCRP(1)	The approximate vortex spacing along the x-axis before the x-position of maximum body diameter (ft).

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CARD 8 (continued):

Columns	FORTTRAN Name	Description
21-30	XCRP(2)	The approximate vortex spacing along the x-axis aft of the x-position of maximum body diameter (ft). $X_i = X_{i-1} - XCRP(1) * EXP(-AEXP(1) * (R-RMX)/RMX)$ where X_i, X_{i-1} = x-locations R = body radius at X_i RMX = maximum body radius for vortex spacing before the x-location of the maximum body diameter.
31-40	AEXP(1)	Factor in the exponential of the equation
41-50	AEXP(2)	Factor in the exponential of the equation $X_i = X_{i-1} - XCRP(2) * EXP(-AEXP(2) * (R-RMX)/RMX)$ where X_i, X_{i-1} = x-locations R = body radius at X_i RMX = maximum body radius for vortex spacing aft of the x-location of the maximum body diameter.
51-60	XRM	Limiting downstream x-location of the axially-spaced vortices (ft).

NSRV and ISPACE are right-adjusted integer numbers in I5 fields, while XCRP(1), XCRP(2), AEXP(1), AEXP(2) and XRM are single-precision floating-point numbers in F10 fields.

**** Ring Vortex Parameters' Cards ****

Two cards are necessary to specify the information about the location and orientation of the starting vortex (or vortices) of a generated system of vortices or an individual independent ring vortex. It should be noted that if NSRV = 0,

no cards are specified under this section. If NSRV \neq 0, the user must specify NSRV set(s) of these two cards in the order indicated in the section Circulation Variation Cards.

The first card contains

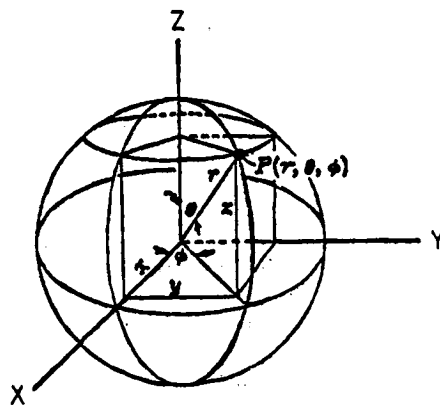
Columns	FORTTRAN Name	Description
1-10	XCV	x-coordinate of the center of the vortex ring (ft).
11-20	YCV	y-coordinate of the center of the vortex ring (ft).
21-30	ZCV	z-coordinate of the center of the vortex ring (ft).
31-40	RDM	Maximum vortex radius (ft). RDM is usually considered to be the boundary of the propeller slipstream. If NSRV = 1, ISPACE > 0, and if XCV, YCV, and ZCV correspond to the propeller's center of rotation, RDM is the propeller radius.
41-50	CA	Initial central angle, degrees (See Figure 3).
51-60	PHI	Rotation angle, degrees (See Figure 3).
61-65	NCA	Central angle increment number. NCA is that number dividing 360 degrees into NCA equal parts from which NCA segments are determined to approximate the perimeter of a circle.
66-70	NVPHI	Rotation tilt parameter. NVPHI = 0: Plane of the vortex ring(s) is perpendicular to the x-axis of body (Set PHI = 90.0). NVPHI = 1: Plane of the vortex ring(s) is not perpendicular to the x-axis of the body. Parameter allows PHI to change at the same rate as CA so that initial choices of PHI and CA determine the path taken by point P of Figure 3.

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first card (continued):

Columns	FORTRAN Name	Description
71-75	NRS	Number of radial stations or concentric vortex rings.
76-80	NPTS	Number of (circulation vs. radial distance) points (≤ 50).

The parameters XCV, YCV, ZCV, RDM, CA, and PHI are single-precision floating-point numbers in F10 fields. The parameters NCA, NVPHI, NRS, and NPTS are right-adjusted integer numbers in I5 fields.



$$CA = \theta$$

$$PHI = \phi$$

Figure 3: Definition of angles for specification of vortex ring(s) orientation (Point P described in Cartesian coordinates by $x = r \sin \theta \cos \phi$, $y = r \sin \theta \sin \phi$, and $z = r \cos \theta$)

The second card contains

Columns	FORTRAN Name	Description
1-10	GFACT	The circulation-strength scale factor. If GFACT = 0.0, the program automatically sets GFACT = 1.0. Since an arbitrary normalized circulation variation may be specified that may not be compatible to the-specified DEP, GFACT provides an easy means to adjust power into the air-stream by changing the magnitude of the circulation variation. If IMATCH = 0, GFACT is automatically adjusted to match

second card (continued):

the simulated slipstream's power to the specified power into the air-stream. GFACT is a single-precision floating-point number in an F10 field.

**** Circulation Variation Cards ****

For each independent vortex system, a set of NPTS cards must be specified in this section. Each card of the set contains

Columns	FORTRAN Name	Description
1-10	RAD	The radius at which the circulation (or strength) of the vortex ring is to be specified (ft).
11-20	GAM	The circulation (or strength) of the vortex ring at radius RAD.

The parameters RAD and GAM are single-precision floating-point numbers in F10 fields.

Ordering of cards: For each of the NSRV vortex systems, the user must supply the two cards from the Ring-Vortex-Parameters section first and, secondly, the NPTS cards of this section. For every independent ring-vortex system, the user must repeat this sequence.

**** Body Description Cards ****

Each card contains the information to specify one half-body point. Each card contains

Columns	FORTRAN Name	Description
1-12	XI	x-coordinate
13-24	YI	y-coordinate
25-36	ZI	z-coordinate

Body Description Cards (continued):

Columns	FORTRAN Name	Description
37-40	NI	N-station index (See Figure 4)
41-44	MI	M-station index (See Figure 4)
45-48	NS	Body number

XI, VI and ZI are single-precision floating-point numbers in F12 fields, while NI, MI and NS are right-adjusted integer numbers in I4 fields. The maximum value of NI or MI must be restricted to less than or equal to 30 because of the array dimensions of the program. NS should be a constant for a given data set, which must be greater than zero but not equal to 1000. A blank card must be supplied at the end of these cards to signal the end of the body description cards. The reading of the body description cards is controlled by the read unit number IDS.

**** Inlet and Exhaust Panel Cards ****

Each card contains the information to specify one panel or quadrilateral either as an inlet (flow into the body) panel or as an exhaust (flow out of the body) panel. Each card contains

Columns	FORTRAN Name	Description
1-5	MS1	1st reference M-station index [MS1 \geq 1]
6-10	MS2	2nd reference M-station index [MS1 < MS2 \leq max (MI)]
11-15	NS1	1st reference N-station index [NS1 \geq 1]
16-20	NS2	2nd reference N-station index [NS1 < NS2 \leq max (NI)]

Columns	FORTTRAN Name	Description
21-25	IPNS	Parameter which denotes the panel enclosed by the M- and N-station indexes as an inlet or exhaust panel. If IPNS = -1, the panel is designated as an inlet panel, while the panel is designated as an exhaust panel if IPNS = +1. If IPNS = 0, the panel is bypassed as being impermeable to mass flow.

The panels are designated by the order in which the data cards are encountered. It must be true—with the exception of a blank card—that

$$(MS2 - MS1) = 1$$

and

$$(NS2 - NS1) = 1$$

since only one panel specification is allowed per card. Since stagnation flows are not permitted in the program, at least one exhaust panel is required if at least one inlet panel is specified, and vice versa. MS1, MS2, NS1, NS2, and IPNS are right-adjusted integer numbers in I5 fields. A blank or zero card must be supplied to serve either of two purposes. If no inlet and exhaust panels are specified, the blank card terminates the attempt to read more cards. If inlet and exhaust panels are specified, the blank card signals the end of this information.

Specification of the cards above represent a complete set of data for a particular body. Additional data sets are programmed similarly starting again at CARD 1.

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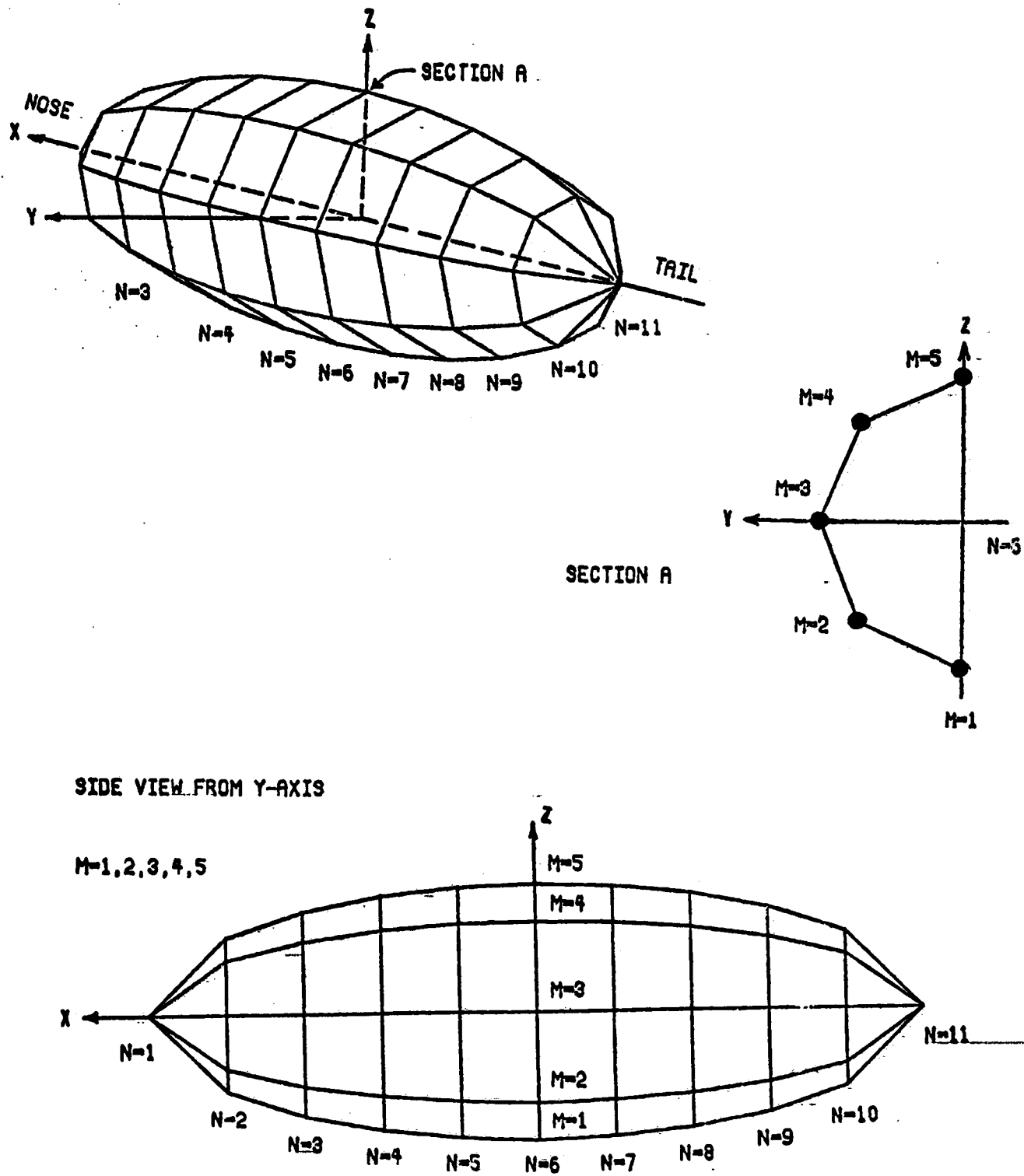


Figure 4: Schematic of indexing scheme

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38 PF1
39 PF1
40 PF1
41 PF1
42 PF1
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44 PF1
45 PF1
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47 PF1
48 PF1
49 PF1
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51 PF1
52 PF1
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72 PF1
73 PF1
74 PF1
75 PF1
76 PF1
77 PF1
78 PF1
79 PF1

COMMON /SIK/SN(650),VNP(650),IPN(650)
COMMON /RING/VTX(3,650)
COMMON /VCK/HVF,SFC,DEP,CPHA,TINF,ADUT,AIN,EOA
COMMON /BL/VOV(75),SS(75),VINP,VO,ROE,DELS(150),CFI(150),THT(150),
1 STOTAL,KKK
COMMON /INOUT/JREAD,JWRITE,KFILE,KFILE1,KFILE2,KFILE3,KFILE4,KFILE
15
COMMON /CANCEL/ICANCL,NODE
INTEGER P,P1,P2,P3,P4,PC,P5,P6,P7,P8,P9
C*** SET CARRIAGE CONTROL PARAMETERS FOR INSTALLATION
JREAD=1
JPUNCH=2
JWRITE=3
KFILE1=7
KFILE2=8
KFILE3=9
KFILE4=10
KFILE5=11
C*** SET INITIAL PARAMETERS
PI=3.1415927
IPL0T=0
LINE=0
PXLIN=50
READ DATA CARDS
C*** 1 READ (JREAD,2, END=173) IDS
2 FORMAT (I5)
ICANCL=0
READ (IDS,3) (TITLE(I),I=1,20)
3 FORMAT (20A4)
WRITE (JWRITE,4)
4 FORMAT (1H1,/,10X,105HNC SU FLOWBODY PROGRAM: POTENTIAL FLOW + BD
1 UNIFORM SLIPSTREAM FLOW + INTERIOR MASS FLOW.//)
1 KFILE=KFILE1
REWIND KFILE1
REWIND KFILE2
REWIND KFILE3
REWIND KFILE4
REWIND KFILE5
KNFW=1
ICK=3
```

```

KWRITE=0
JPOLD=0
QHOLD=1.0E44
J=0
5  FORMAT (1X,20A4) (TITLE(I),I=1,20)
   SA=.0
   LMATCH=0
C***
   DEFINE AND READ PERTINENT GEOMETRIC & FLOW CONTROL PARAMETERS
   PEAD (JREAD,6) VINP,VO,ROE,REFA,HVF,SFC,DEP,CPHA,TINF,EOA,IWRITE,I
1  IPCH1,IPCH2,IMATCH
6  FCRMAT (4E20,13./,4E20,13./,2E20,13,415)
7  READ (JREAD,7) CF,ITFST,NODE
   IF (CF.EQ.0.0E0)CF=1.0E0
8  FCRMAT (14)
   NSF=1
   MIX=150
   ISM=1
   EPS=0.0001
   ISP=0
   WRITE (JWRITE,9) NOE,NSF,MIX
9  FORMAT (17HNO. OF QUADS. =,14/17H NO. OF SECTIONS=,14/31H MAX. N
   10. OF ITERATIONS X FLOW ,I3)
   WRITE (JWRITE,10) VINP,VO,ROE,REFA,HVF,SFC,DEP,CPHA,TINF,EOA,IWRIT
10 FCRMAT (//,2X,7HVINF = ,E14.7,3X,5HVD = ,E14.7,3X,6HROE = ,E14.7,3
   1X,7HREFA = ,E14.7,3X,7HCPHA = ,E14.7,3X,6HVF = ,F14.7,7./,2X,6HDEP
   1 = ,E14.7,3X,8HIPC1 = ,E14.7,3X,7HTINF = ,E14.7,3X,6HEOA = ,E14.7,
   1/.,2X,9HWRITE = ,I2,3X,8HIPC2 = ,I2,3X,8HIPC2 = ,I2,3X,9HIMATCH
   1 = ,I2,3X,6HIDS = ,I2,3X,8HITEST = ,I2,3X,7HNCDE = ,I4)
C***
   PRINT COORDINATE CONVERSION FACTOR
   WRITE (JWRITE,11) CF
11 FCRMAT (1X,/,2X,29HCOORDINATE CONVERSION FACTOR,.,1X,F12.7./)
   WRITE (JWRITE,12) ISM,EPS
12 FORMAT (1X,/,2X,11,18H PLANE OF SYMMETRY,/,2X,22HCCNVERGENCE CRITE
   1RIA ,F8.5)
   LINE=LINE+23
   NGES=NOE
C***
   READ PERTINENT DATA FOR THE VORTEX FLOW(S)

```

```

PF1 80
PF1 81
PF1 82
PF1 83
PF1 84
PF1 85
PF1 86
PF1 87
PF1 88
PF1 89
PF1 90
PF1 91
PF1 92
PF1 93
PF1 94
PF1 95
PF1 96
PF1 97
PF1 98
PF1 99
PF1 100
PF1 101
PF1 102
PF1 103
PF1 104
PF1 105
PF1 106
PF1 107
PF1 108
PF1 109
PF1 110
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PF1 120
PF1 121

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PF1 176
PF1 177
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PF1 188
PF1 189
PF1 190
PF1 191
PF1 192
PF1 193
PF1 194
PF1 195
PF1 196
PF1 197
PF1 198
PF1 199
PF1 200
PF1 201
PF1 202
PF1 203
PF1 204
PF1 205

```

LINE=LINE+7
CA(LL)=CA(LL)*PI/180.0
PHI(LL)=PHI(LL)*PI/180.0
IF (NPPTS(LL).EQ.0) GO TO 23
C*** READ SPLINE POINTS FOR CIRCULATIONS
MNPTS=NPPTS(LL)
DO 22 I=1,MNPTS
READ (JREAD,21) RAD(I),GAM(I)
21 FCRMAT (2F10.0)
GAM(I)=GAM(I)*GFACT
22 CONTINUE
CALL SPLINE (MNPTS,GAM,RAD,LL)
23 CONTINUE
24 K=0
IF (NSRV.EQ.1) LMATCH=1
XMIN=0.0
XMAX=0.0
MM=0
P=1
Q=1.0
DO 25 I=1,31
DC 25 J=1,31
25 ID(I,J)=0
J=0
C*** READ INPUT POINTS--AN ODD NUMBER MUST BE USED FOR BOTH NI AND MI
READ (IDS,26) XI,YI,ZI,NI,MI,NS,NE,VN
26 FCRMAT (3F12.9,4I4,F12.9)
MMAX=MI
MMIN=MI
NMAX=NI
NMIN=NI
NSS=NS
PC=1
GO TO 31
27 READ (IDS,26) XI,YI,ZI,NI,MI,NS,ME,VN
GO TO 30
28 MI=MI+1
IF (MI.LE.MMAX) GO TO 29
NI=NI+1
IF (NI.EQ.6) NS=J
IF (NI.EQ.6) GO TO 35

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29 XI=XNEW(PC+1)
   YI=YNEW(PC+1)
   ZI=ZNEW(PC+1)
30 PC=PC+1
31 IF (NS.NE.NSS) GO TO 35
   IF (KNEW.EQ.1.AND.NE.EQ.0) GO TO 32
   IF (KNEW.NF.1.AND.NE.EQ.0) GO TO 33
   IW=NI
   NI=NI
   NI=IW
C** CONVERT BODY COORDINATES TO COMPATIBLE UNITS
32 XI=XI*CF
   YI=YI*CF
   ZI=ZI*CF
C** STORE INPUT POINTS IN POINT ARRAY
33 X(PC)=XI
   Y(PC)=YI
   Z(PC)=ZI
   IF (KNEW.NE.1) GO TO 34
   XS(PC)=X(PC)
   YS(PC)=Y(PC)
   ZS(PC)=Z(PC)
34 ID(MI,NI)=PC
   MMAX=MAXO(MMAX,MI)
   MMIN=MINO(MMIN,MI)
   NMAX=MAXO(NMAX,NI)
   NMIN=MINO(NMIN,NI)
   IF (XMIN.GE.XI) XMIN=XI
   IF (XMAX.LE.XI) XMAX=XI
   GO TO (27,28).KNEW
35 IF ((LINE+3).LE.MXLINE) GO TO 36
   WRITE (JWRITE,18)
   LINE=0
36 WRITE (JWRITE,37) NSS
37 FCFRMT (/,10H0 SECTION ,I4)
   PC=PC-1
C** DEFINE CENTERLINE OF BODY
   X21=X(PC)-X(1)
   Y21=Y(PC)-Y(1)
   Z21=Z(PC)-Z(1)
   RCDC=SQ2(X21,Y21,Z21)

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```
XCCS=X21/BCDC
YCCS=Y21/BCDC
ZCCS=Z21/BCDC
WRITE (JWRITE,33) XDCS,YDCS,ZDCS
28 FORMAT (1X,/,10X,35HBODY-CENTERLINE DIRECTION COSINES( ,F7.4,3H .
1 ,F7.4,3H , ,F7.4,2H ) )
IF (ITEST.FO.O) GC TO 39
XGRD(2,1)=X(1)
XCRD(2,2)=X(PC)
YCRD(2,1)=O.O
YCRD(2,2)=O.O
KIND(2)=-1
KIND(3)=3
C** 39 FOR EACH N-STATIC, DETERMINE CROSS-SECTIONAL AREA AND MAX RADIUS
LPT=1
XMR=X(1)
RMR=O.OEO
MMAXM1=MMAX-1
LZF=O
DC 41 JN=MIN,P MAX
LZF=LZP+1
X3=X(LPT)
XOPD(3,JN)=X3
Y3=Y(1)+(X3-X(1))*Y21/X21
Z3=Z(1)+(X3-X(1))*Z21/X21
AREAS=O.OEO
DC 40 JM=MIN,M MAXM1
Y4=Y(LPT)
Z4=Z(LPT)
IF (JM.FO.MMIN) RMX=SQ2F(O.O,O.O,Y3,Y4,Z3,Z4)
Y5=Y(LPT+1)
Z5=Z(LPT+1)
AREAS=AREAS+2.OEO*AREA
RMX1=SQ2F(O.O,O.O,Y3,Y5,Z3,Z5)
IF (RMX1.GT.RMX) RMX=RMX1
IF (RMX.GT.RXMR) RXMR=RMX
IF (RMX.EO.RXMR) XMR=X3
40 LPT=LPT+1
LPT=LPT+1
SVV(JN,1)=AREAS
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SVV(JN,2)=RMX
41 CONTINUE
   IROUND=0
   IF (ITEST.EQ.0) GO TO 43
   DO 42 JN=1,LZP
42 YORD(3,JN)=SVV(JN,2)/RXMR
43 IF (ISPACE.EQ.0) GO TO 45
C** COMPUTE LOCATION CF VORTICES
   CALL SPACE(NSRV,SVV,XCV,NMIN,NMAX,X- MMAX,XCRP,AEXP,XRM,ISPACE,RXMR
1,XMR)
   INSRV=NSRV
   DO 44 JV=2,NSRV
   NRS(JV)=1
   NPTS(JV)=0
   CA(JV)=CA(1)
   PHI(JV)=PHI(1)
   NCA(JV)=NCA(1)
   RDM(JV)=0.0
44 NVPHI(JV)=NVPHI(1)
45 IF ((LINE+25).LE.MXLINE) GO TO 46
   WRITE (JWRITE,19)
46 LINE=0
   IF (LMATCH.NE.1) GO TO 47
   IF (IMATCH.FQ.0) GO TO 49
47 WRITE (JWRITE,48)
48 FCRMAT (1X,/,5X,24HRING VORTEX INFORMATION:/,6X,6HNUMBER,9X,18H
1CENTER COORDINATES,8X,6HRADIUS,3X,11HCIRCULATICN,/,19X,1HX,9X,1HY,
19X,1HZ,/)
   IROUND=1
49 DO 60 JV=1,NSRV
   IF (JV.GT.1) GO TO 51
   COMPUTE A TOTAL CIRCULATICN
   PDR=RDM(JV)
   NR=NRS(JV)
   GGDR=0.0
   DO 50 MV=1,NR
   RVX=F(NR,MV,PDR,DRX)/PDR
   GGDR=GGDR+G(JV,RVX)/RVX
   CIRC(JV)=GGDR
50 IF (RDM(JV).NE.0.0.AND.JV.NE.1.AND.IMATCH.NE.0) GO TO 60
C** CENTER VORTEX CN BODY CENTERLINE
   X3=XCV(JV)
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IF (ITEST.EQ.0) GO TO 52
XDRD(1,JV)=XCV(JV)
YDRD(1,JV)=0.0
KIND(1)=2
52 YCV(JV)=Y(1)+(X3-X(1))*Y21/X21
ZCV(JV)=Z(1)+(X3-X(1))*Z21/X21
IF (JV.EQ.1) GO TO 56
C*** SCAN N-STATIONS FOR VORTEX LOCATION
LPT=1
NMAXMI=NMAX-1
DO 53 JN=NMIN,NMAXI
LC1=JN+1
LC2=JN+1
IF (XCV(JV).LE.X(LPT).AND.XCV(JV).GE.X(LPT+MMAX)) GO TO 54
53 RDM(JV)=RDM(1)
GO TO 55
C*** VORTEX LOCATED. DETERMINE RADIUS
RXTL=(X(LPT)-XCV(JV))/(X(LPT)-X(LPT+MMAX))
54 RDM(JV)=SVV(LC1,2)+RXTL*(SVV(LC2,2)-SVV(LC1,2))
RAV1=SQRT(SVV(LC1,1)/PI)
RAV2=SQRT(SVV(LC2,1)/PI)
RAV=RAV1+RXTL*(RAV2-PAV1)
RAVD=SQRT(PDR**2+RAV**2)
IF (RAVD.GT.RDM(JV))RDM(JV)=RAVD
55 CIRC(JV)=GGDR/(RDM(JV)/PDR)
GO TO 57
56 IF (ITEST.EQ.0) GO TO 57
XDRD(4,JV)=XCV(JV)
YDRD(4,JV)=RDM(JV)/PDR
KIND(4)=6
57 IF (LMATCH.NE.1) GO TO 58
IF (IMATCH.EQ.0.AND.IFOUND.EQ.0) GO TO 60
58 WRITE (JWRITE,59) JV,XCV(JV),YCV(JV),ZCV(JV),RDM(JV),CIRC(JV)
59 FORMAT (BX.12.5X,F9.5,1X,F9.5,1X,F9.5,1X,F9.5,2X,F11.7)
60 CCNTINUE
IF (IROUND.EQ.1) GO TO 64
IROUND=1
CALL RGVRTX(XCV,YCV,ZCV,XCV(1),YCV(1),ZCV(1),RDM,NCA,CA,PHI,NVPHI,
1NRS,N'RV,VX,VY,VZ,IM,NPTS)
VI=SQ2(VX,VY,VZ)
IF (IMATCH.NF.0.OR.LMATCH.NE.1) GO TO 64
DELV=VINE*(1.0+VI)
```

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PNET=ROE*PI*(RDM(1))*VINFL**2*DELV
GFACT=DFP/PNET
WRITE (JWRITE,61) VI
61 FORMAT (1X,/,5X,29HREFERENCE INDUCED VELOCITY = ,E16.9)
WRITE (JWRITE,62) GFACT
62 FORMAT (1X,/,5X,80HMATCHING OF AIRSTREAM POWER TO DEVELOPED ENGIN
1E POWER(DFP) REQUIRED GFACT TO BE ,E16.9,20H TIMES THE ORIGINAL.)
DC 63 I=1,MNPTS
63 GAM(I)=GAM(I)*GFACT
CALL SPLINE(MNPTS,GAM,RAD,1)
GO TO 47
64 WRITE (JWRITE,65)
65 FORMAT (1X,/)
IF (I TEST.EQ.0) GO TO 66
DETERMINE PARAMETERS FOR PLOT OF EXTENT OF VORTICES
XKEEP=ABS(X21)
XHOLD=ABS(XRM-X(1))
IF (XHOLD.GT.XKEEP) XKEEP=XHOLD
IKEEP1=FIX(XRM-1.0)
IKEEP2=FIX(X(1)+2.0)
IF (((2*IKEEP1)/2).NE.IKEEP1) IKEEP1=IKEEP1+1
IF (((2*IKEEP2)/2).NE.IKEEP2) IKEEP2=IKEEP2+1
LTEST=IABS(IKEEP1)+IABS(IKEEP2)
XINC=2.0
XKEEP1=FLOAT(IKEEP1)
XKEEP2=FLOAT(IKEEP2)
IHLD1=FIX(X(1))
IHLD2=FIX(XKEEP)
XHLD=FLOAT(IHLD1)+1.0
LL1=1
LL2=2*(IABS(IHLD1)+IABS(IHLD2))+1
GO TO 111
66 IF (IWRITE.GT.0) GO TO 68
C*** SET LINE COUNTER
WRITE (JWRITE,18)
LINE=0
WRITE (JWRITE,67)
67 FORMAT (4H ,M,7X,2HX1,12X,2HX2,12X,2HX3,12X,2HX4,12X,2HXC,12X,2HX
1N,12X,1MA,13X,3HCZ4/4H N,7X,2HY1,12X,2HY2,12X,2HY3,12X,2HY4,12X,
12HXC,12X,2HYN,12X,2HFL,12X,3HCZ5/4H P,7X,2HZ1,12X,2HZ2,12X,2HZ3,
112X,2HZ4,12X,2HZC,12X,2HZN,12X,4HCZ1,10X,3HCZ6/)
LINE=LINE+5

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68 IF (KNEW.EQ.2) GO TO 69
   STCTAL=XMAX-XMIN
   PEBODY=VINE*STOTAL/VO
69   MMAXQD=MMAX
   IF (KNEW.NE.1) GO TO 70
   NMX=NMAX+2
70   IDD=(NMAXQD-3)*(MMAXQD-1)/12
   N1=NMIN
   NM2=MMAX-MMIN
   NN2=NMAX-NMIN
   IF (MOD(MM2,2).EQ.0.AND.MOD(NN2,2).EQ.0) GO TO 71
   ISP=1
71   MM2=MM2/2
   NN2=NN2/2
   IF ((KNEW.EQ.1.AND.IPCH1.EQ.0).OR.(KNEW.EQ.2.AND.IPCH2.EQ.0)) GO T
10 72
C** PUNCH CARDS FOR PLOTTING
C** CALL PUNCH(NMIN,NMX,MMIN,MMAX,XS,YS,ZS,JPUNCH,JWRITE)
72 DO 110 NN=1,NN2
   M1=MMIN
   DO 109 MM=1,MM2
   NQ=1
   IT=ID(M1,N1)*ID(M1+1,N1)*ID(M1+2,N1)*ID(M1,N1+1)*ID(M1+1,N1+1)*ID(
M1+1,N1+2)*ID(M1,N1+2)*ID(M1+1,N1+2)*ID(M1+2,N1+2)
   IF (IT.EQ.0) GO TO 109
   M2=M1+1
   DO 108 M=M1,M2
   N2=N1+1
   DC 108 N=N1,N2
73   GC TO (73,74,75,76),NG
   P1=ID(M,N)
   P2=ID(M+1,N)
   P3=ID(M+1,N+1)
   P4=ID(M,N+1)
   P5=ID(M+2,N)
   P6=ID(M+2,N+1)
   P7=ID(M+1,N+2)
   P8=ID(M,N+2)
   P5=P1
   IF ((X(P1).NE.X(P2)).OR.Y(P1).NE.Y(P2)).OR.Z(P1).NE.Z(P2)).AND.(X(P1
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1) .NE.X(P4).OR.Y(P1).NE.Y(P4).OR.Z(P1).NE.Z(P4))) GO TO 77
P9=ID(M+2,N+2)
GO TO 77
74 P1=ID(M,N+1)
P2=ID(M,N)
P3=ID(M+1,N)
P4=ID(M+1,N+1)
P5=ID(M,N-1)
P6=ID(M+1,N-1)
P7=ID(M+2,N)
P8=ID(M+2,N+1)
P9=P1
IF ((X(P1).NE.X(P2).OR.Y(P1).NE.Y(P2).OR.Z(P1).NE.Z(P2)).AND.(X(P1
1) .NE.X(P4).OR.Y(P1).NE.Y(P4).OR.Z(P1).NE.Z(P4))) GO TO 77
GC TO 77
75 P1=ID(M+1,N)
P2=ID(M+1,N+1)
P3=ID(M,N+1)
P4=ID(M,N)
P5=ID(M+1,N+2)
P6=ID(M,N+2)
P7=ID(M-1,N+1)
P8=ID(M-1,N)
P9=P1
IF ((X(P1).NE.X(P2).OR.Y(P1).NE.Y(P2).OR.Z(P1).NE.Z(P2)).AND.(X(P1
1) .NE.X(P4).OR.Y(P1).NE.Y(P4).OR.Z(P1).NE.Z(P4))) GO TO 77
GC TO 77
76 P1=ID(M+1,N+1)
P2=ID(M,N+1)
P3=ID(M,N)
P4=ID(M+1,N)
P5=ID(M-1,N+1)
P6=ID(M-1,N)
P7=ID(M,N-1)
P8=ID(M+1,N-1)
P9=P1
IF ((X(P1).NE.X(P2).OR.Y(P1).NE.Y(P2).OR.Z(P1).NE.Z(P2)).AND.(X(P1
1) .NE.X(P4).OR.Y(P1).NE.Y(P4).OR.Z(P1).NE.Z(P4))) GO TO 77
P9=ID(M-1,N-1)
77 IP(1)=P1
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IP(2)=P2
IP(3)=P3
IP(4)=P4
IP(5)=P5
IP(6)=P6
IP(7)=P7
IP(8)=P8
IP(9)=P9
STORE CORNER POINTS TO PANEL NUMBER
DC 78 JX=1.4
IDD(P,JX)=IP(JX)
C*** COMPUTE NORMAL VECTOR TO PANEL (IN TERMS OF REFERENCE COORDINATE
C*** SYSTEM)
X1=X(P3)-X(P1)
X2=X(P4)-X(P2)
Y1=Y(P3)-Y(P1)
Y2=Y(P4)-Y(P2)
Z1=Z(P3)-Z(P1)
Z2=Z(P4)-Z(P2)
XN=Y2*Z1-Y1*Z2
YN=X1*Z2-X2*Z1
R=SQ2(XN.YN.ZN)
XN=XN/R
YN=YN/R
ZN=ZN/R
AO=.5*R
C*** COMPUTE PANEL CENTROID (IN TERMS OF REFERENCE COORDINATE SYSTEM)
X1=X(P3)-X(P2)
Y1=Y(P3)-Y(P2)
Z1=Z(P3)-Z(P2)
X5=Y1*Z2-Y2*Z1
Y5=Z1*X2-Z2*X1
Z5=X1*Y2-X2*Y1
A1=SQ2(X5.Y5.Z5)
A2=R-A1
IT=1
XC=(X(P2)+X(P4)+(A1*X(P3)+A2*X(P1)))/3.
YC=(Y(P2)+Y(P4)+(A1*Y(P3)+A2*Y(P1)))/3.
ZC=(Z(P2)+Z(P4)+(A1*Z(P3)+A2*Z(P1)))/3.
X4=YN*Z1-Y1*ZN
Y4=ZN*X1-Z1*XN
  
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Z4=XN*Y1-X1*YN
A=1./SQ2(X4.Y4.Z4)
X4=X4*A
Y4=Y4*A
Z4=Z4*A
X3=ZN*Y4-Z4*YN
Y3=XN*Z4-X4*ZN
Z3=YN*X4-Y4*XN
C** COMPUTE POINTS IN QUAD SYSTEM (I.E.. ELEMENT COORDINATE SYSTEM)
DO 80 I=1,9
L=IP(I)
XP(I)=X3*(X(L)-XC)+Y3*(Y(L)-YC)+Z3*(Z(L)-ZC)
YP(I)=X4*(X(L)-XC)+Y4*(Y(L)-YC)+Z4*(Z(L)-ZC)
ZP(I)=XN*(X(L)-XC)+YN*(Y(L)-YC)+ZN*(Z(L)-ZC)
C** COMPUTE MATRIX COEFFICIENTS TO FIND LOCAL BODY SURFACE EQUATION
DO 81 I=2,9
C(I,1)=1.
C(I,2)=XP(I)
C(I,3)=YP(I)
C(I,4)=XP(I)**2
C(I,5)=YP(I)**2
C(I,6)=XP(I)*YP(I)
D(I)=ZP(I)
DO 82 I=1,6
C(1,I)=C(9,I)
C(5,I)=C(5,I)+C(6,I)
C(6,I)=C(7,I)+C(8,I)
D(I)=D(9)+D(6)
D(6)=D(7)+D(8)
C** SOLVE MATRIX EQ. C*CZ=D FOR CZ
CALL MATINS(C,9,6,FF,6,1,DETERN,IDM,INDEX)
IF (IDM.EQ.1) GO TO (84,85).IT
WRITE (JWRITE,83)
FORMAT (33H ERROR IN INPUT - SINGULAR MATRIX)
LINE=LINE+1
ISP=1
GO TO 85
84 IT=2
C** COMPUTE NEW NORMAL VECTORS
XN=XN-CZ(2)*X3-CZ(3)*X4
YN=YN-CZ(2)*Y3-CZ(3)*Y4

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ZN=ZN-CZ(2)*Z3-CZ(3)*Z4
A=1./SQ2(XN,YN,ZN)

XN=XN*A
YN=YN*A
ZN=ZN*A

GO TO 79

C** STORE DATA IN ARRAY TO BE WRITTEN ON TAPE

85

B(J+1)=XP(1)
B(J+2)=YP(1)
B(J+3)=XP(2)
B(J+4)=YP(2)
B(J+5)=XP(3)
B(J+6)=YP(3)
B(J+7)=XP(4)
B(J+8)=YP(4)
B(J+9)=X3
B(J+10)=Y3
B(J+11)=Z3
B(J+12)=X4
B(J+13)=Y4
B(J+14)=Z4

XCP(K+1)=XC
YCP(K+1)=YC
ZCP(K+1)=ZC
XNP(K+1)=XN
YNP(K+1)=YN
ZNP(K+1)=ZN
AQP(K+1)=AQ

C** COMPUTE QUADRUPOLE MOMENTS

XI1=XP(1)+XP(2)
XI2=XP(1)+XP(4)
XI3=XP(3)+XP(2)
XI4=XP(3)+XP(4)
XI5=XP(2)+XP(4)
YI1=YP(1)+YP(2)
YI2=YP(1)+YP(4)
YI3=YP(3)+YP(2)
YI4=YP(3)+YP(4)
YI5=YP(2)+YP(4)
R1=A1/24.
R2=A2/24.
R3=AQ/12.
AXX=(XI1**2+XI2**2)*R1+(XI3**2+XI4**2)*R2+XI5**2*R3


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C**
AXY=(X11*Y11+X12*Y12)*R1+(X13*Y13+X14*Y14)*R2+X15*Y15*R3
AVY=(Y11**2+Y12**2)*R1+(Y13**2+Y14**2)*R2+Y15**2*R3
COMPUTE BODY SOLID ANGLE
X1=XC*X3+YC*Y3+ZC*Z3
Y1=XC*X4+YC*Y4+ZC*Z4
Z1=XC*XN+YC*YN+ZC*ZN
RD=1./SQ2(X1,Y1,Z1)
RCU=RD**3
RSV=RCU**2*RD
SA=SA+Z1*(A0*RCU-((AXX*(Y1**2+Z1**2-4.*X1**2)+AVY*(X1**2+Z1**2-4.*
1Y1**2))*1.5-15.*X1*Y1*AXY)*RSV)
B(J+14)=AXY
B(J+15)=AXY
B(J+16)=AYY
BODY ERROR TESTS
D1=SQ2((XP(3)-XP(1))*(YP(3)-YP(1)),0.)
D2=SQ2((XP(4)-XP(2))*(YP(4)-YP(2)),0.)
FL=.5*MAX1(D1,D2)
CZ3=ABS(CZ(2))+ABS(CZ(3))
IF (ABS(CZ(2))+ABS(CZ(3)).GT.FL*.001) GO TC 86
IF (ABS(CZ(1)).LT.FL*.3) GO TO 88
IF (IWRITE.GT.0) GO TO 88
86 IF (IWRITE.GT.0) GO TO 88
87 WRITE (JWRITE,87) CZ23
FCRMT (29H QUESTIONABLE PCINT -POOR FIT,6E14.3)
LINE=LINE+1
88 IF (XP(4).LT.XP(1)) GO TO 89
IF ((YP(4)-YP(3))*(YP(1)-YP(2)).GE.0.) GO TO 92
89 IF (IWRITE.GT.0) GO TO 91
WRITE (JWRITE,90) (XP(I),YP(I),I=1,4)
90 FORMAT (30H ERROR IN INPUT - CROSSED QUAD,4(2F10.5,3X))
LINE=LINE+1
91 ISP=1
92 CRCF=SQ2((XP(2)-XP(1))*(YP(2)-YP(1)),0.)+XP(3)-XP(2)+SQ2((XP(1)-XP
1(4))*(YP(1)-YP(4)),0.)+SQ2((XP(4)-XP(3))*(YP(4)-YP(3)),0.)
IF (36.*A0.GT.CRCF**2) GO TO 94
IF (IWRITE.GT.0) GO TO 104
LINE=LINE+1
WRITE (JWRITE,93)
93 FCRMT (24H WARNING LONG THIN QUAD.)
94 IF (IWRITE.GT.0) GO TO 104
IF (Z1.GE.0.) GO TO 96
WRITE (JWRITE,95)

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95 FORMAT (35H QUESTIONABLE POINT - INWARD NORMAL)
LINE=LINE+1
C*** EDIT QUADRILATERAL INFORMATION
96 GO TO (97,98,99,100),NO
97 WRITE (JWRITE,101) M,X(P1),X(P2),X(P3),X(P4),XC,XN,AQ,CZ(4),N,Y(P1)
1),Y(P2),Y(P3),Y(P4),YC,YN,FL,CZ(5),P,Z(P1),Z(P2),Z(P3),Z(P4),ZC,ZN
1,CZ(1),CZ(6)
GO TO 102
98 WRITE (JWRITE,101) M,X(P2),X(P3),X(P4),X(P1),XC,XN,AQ,CZ(4),N,Y(P2)
1),Y(P3),Y(P4),Y(P1),YC,YN,FL,CZ(5),P,Z(P2),Z(P3),Z(P4),Z(P1),ZC,ZN
1,CZ(1),CZ(6)
GO TO 102
99 WRITE (JWRITE,101) M,X(P4),X(P1),X(P2),X(P3),XC,XN,AQ,CZ(4),N,Y(P4)
1),Y(P1),Y(P3),Y(P2),Y(P4),YC,YN,FL,CZ(5),P,Z(P4),Z(P1),Z(P2),Z(P3),ZC,ZN
1,CZ(1),CZ(6)
GO TO 102
100 WRITE (JWRITE,101) M,X(P3),X(P4),X(P1),X(P2),XC,XN,AQ,CZ(4),N,Y(P3)
1),Y(P4),Y(P1),Y(P2),YC,YN,FL,CZ(5),P,Z(P3),Z(P4),Z(P1),Z(P2),ZC,ZN
1,CZ(1),CZ(6)
101 FORMAT (1H,13,8E14.5/1X,13,8E14.5/1X,13,8E14.5/)
102 LINE=LINE+4
IF (LINE.LT.MXLINE) GO TO 104
WRITE (JWRITE,103)
103 FORMAT (4H1,12X,2HX1,12X,2HX2,12X,2HX3,12X,2HX4,12X,2HXC,12X,2HX
1N,12X,1HA,13X,3HCZ4/4H N,7X,2HY1,12X,2HY2,12X,2HY3,12X,2HY4,12X,
12HXC,12X,2HYN,12X,2HFL,12X,3HCZ5/4H P,7X,2HZ1,12X,2HZ2,12X,2HZ3,
112X,2HZ4,12X,2HZC,12X,2HZN,12X,4HCZ1,10X,3HCZ6/)
LINE=0
104 J=J+16
IF (KNEW.NE.1.AND.P.LE.NOES) GO TO 105
C*** INITIALIZE ARRAYS
VNP(P)=0.0
IFN(P)=0
105 I=P
P=P+1
NC=NO+1
K=K+1
C*** WRITE B ARRAY CONTAINING INFORMATION FOR 12 QUADRILATERALS
IF (J.LT.102) GO TO 108
IF (KNEW.EQ.1)KWRITE=KWRITE+1
WRITE (KFILE)Q,(E(I),I=1,192)
IF (KNF*.NF.1) GC TO 107

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119 MC=MC+1
    IPT(MC)=LC
    IF (NX.EQ.NS2.AND.MX.EQ.MS2) GO TO 121
120 CCNTINUE
C*** CORNER POINTS LOCATED. NOW FIND CORRESPONDING PANEL NUMBER
121 DC 124 JX=1,NQE
    NPL=JX
    LC=0
    DO 123 MX=1,4
    DO 122 NX=1,4
    IF (IPT(MX).EQ.IDD(JX,NX))LC=LC+1
122 CONTINUE
123 CONTINUE
    IF (LC.EQ.4) GO TO 125
124 CONTINUE
C*** PANEL NUMBER FOUND. STORE INDICATION OF NONZERO NORMAL VELOCITY
125 IPN(NPL)=IFNS
    IF (IPNS.LT.0) GO TO 127
    WRITE (JWRITE,126) MSI,MS2,NS1,NS2,NPL
126 FORMAT (2X,4(I5,1X),2X,6HPANEL,14,2X,75HHAS BEEN DESIGNATED TO HA
1VE A NONZERO OUTWARD NORMAL COMPONENT OF VELOCITY.)
    LINE=LINE+1
    GO TO 112
127 WRITE (JWRITE,128) MSI,MS2,NS1,NS2,NPL
128 FORMAT (2X,4(I5,1X),2X,6HPANEL,14,2X,74HHAS BEEN DESIGNATED TO HA
1VE A NONZERO INWARD NORMAL COMPONENT OF VELOCITY.)
    LINE=LINE+1
    GO TO 112
C*** SET UP FOR NEXT SECTION
129 IF (ITFST.NE.0) GO TO 150
    DC 130 M=MMIN,MMAX
    DO 130 N=MMIN,NMAX
130 IC(M,N)=0
131 ASS=NS
    PC=1
    MMAX=MI
    YMIN=MI
    NMIN=NI
    NMAX=NI
    NE=ME
    IF (NS.GT.0) GO TO 31
    JHOLD=((NMAXQD-3)*(MMAXQD-1))-12*IDD)*16

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IF (J.EQ.192) GO TO 133
IF (KNEW.EQ.1) KWRITE=KWRITE+1
WRITE (KFILE)0,(B(I),I=1,192)
IF (KNEW.NE.1) GO TO 133
IF (KWRITE.NE.IDD+1) GO TO 133
QHOLD=0
DO 132 I=1,192
132 BHCLD(I)=B(I)
133 NP=K
      NGUAD=NP
      ISMP=ISM+1
      GO TO (137,136,135,134),ISMP
134 SA=SA+SA
135 SA=SA+SA
136 SA=SA+SA
137 J=1
C*** CHECK SOLID ANGLE
      IF (ABS(SA-12.566).LT..05) GO TO 138
      IF (ABS(SA).LF..05) GO TO 140
138 WRITE (JWRITE,139) SA
139 FORMAT (40HOPROBABLE ERROR IN INPUT - SOLIC ANGLE =,2F12.3)
140 REWIND KFILE
C*** CHECK NO. OF QUADRILATERALS
      IF (NP.FQ.NQE) GO TO 143
      WRITE (JWRITE,141) NP,NQE
141 FCRMAT (IX,I4,27H QUADRILATERALS GIVEN, NOT ,I4)
142 FCRMAT (//,IX,11HEXIT CALLED,/)
      GO TO 172
143 IF (ISP.LE.0) GO TO 144
      WRITE (JWRITE,142)
      GO TO 172
C*** CALL REMAINING SECTIONS OF THE POTENTIAL FLOW PROGRAM
144 CALL PFP2(ISM,K)
      IF (ICANCL.NE.0) GO TO 172
      NSRV=INSRV
145 IF (NSRV.LF.0) GO TO 158
      LL1=1
      LL2=NP
      IF (KNEW.NE.2) GO TO 146
      LL1=LL1S
      LL2=LL2S
```

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146 IF (KNEW.EQ.1) WRITE (JWRITE,147)
147 FCRMAT (1H1,/,1X,67HINDUCED VELOCITY BY RING VORTICES AT ORIGINAL
    1-BODY PANEL CENTROIDS:./)
    IF (KNEW.EQ.2) WRITE (JWRITE,148)
148 FCRMAT (1H1,/,1X,63HINDUCED VELOCITY BY RING VORTICES AT WAKE-BOD
    1Y PANEL CENTROIDS:./)
    WRITE (JWRITE,149)
149 FCRMAT (2X,5HPANEL,3X,10(.-),1X,23HPANEL CENTROID LOCATION,1X,11(
    1.-),4X,12(.-),1X,19HVELOCITY COMPONENTS,1X,13(.-),/.1X,6HNNUMBER
    1,9X,1HX,15X,1HY,15X,1HZ,17X,1HX,15X,1HY,15X,1HZ,/)
    LINE=0
    GC TO 153
150 WRITE (JWRITE,151)
151 FCRMAT (1H1,/,1X,63HINDUCED VELOCITY BY RING VORTICES ALONG BODY-
    1CENTERLINE POINTS:./)
    WRITE (JWRITE,152)
152 FCRMAT (1X,5HPOINT,3X,15(.-),1X,14HPOINT LOCATION,1X,15(.-),4X,1
    12(.-),1X,19HVELOCITY COMPONENTS,1X,13(.-),/.1X,6HNNUMBER,9X,1HX,1
    15X,1HY,15X,1HZ,17X,1HX,15X,1HY,15X,1HZ,/)
153 DC 157 LL=LL1,LL2
    IF (ITEST.EQ.0) GO TO 154
    FCR ITEST=1, SET AXIAL STATIONS FOR VORTEX INDUCED VELOCITIES
    ZCP(LL)=0.0
    ZCP(1L)=0.0
    IF (LL.EG.1) XCP(LL)=XHLD
    IF (LL.GT.1) XCP(LL)=XCP(LL-1)-0.5E0
    XORD(5,LL)=XCP(LL)
    C** COMPUTE INDUCED VELOCITY COMPONENTS AT PANEL CENTROIDS BY THE RING
    C** VORTICES
    154 CALL RGVRTX(XCV,YCV,ZCV,XCP(LL),YCP(LL),ZCP(LL),FDY,NCA,CA,PHI,NVP
    1HI,NRS,NRSV,VX,VY,VZ,IM,PIPTS)
    VTX(1,LL)=VX
    VTX(2,LL)=VY
    VTX(3,LL)=VZ
    IF (ITEST.NE.0) YCRD(5,LL)=VTX(1,LL)
    IF ((LINE+1).LE.MXLINE) GO TO 155
    WRITE (JWRITE,13)
    IF (ITEST.EQ.0) WRITE (JWRITE,149)
    IF (ITEST.NE.0) WRITE (JWRITE,152)
    LINE=0
155 WRITE (JWRITE,156) LL,XCP(LL),YCP(LL),ZCP(LL),(VTX(1S,LL)),IS=1,3)
156 FCRMAT (2X,14,3X,1H(.1PE14.7,2H, .1PE14.7,2H, .1PE14.7,4H) .1PE1

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14 7.2X,1PE14.7,2X,1PE14.7)
LINE=LINE+1
157 CCNTINUE
C** WARNING: THE FOLLOWING PLOT CARDS MAY BE INSTALLATION-DEPENDENT.
KIND(5)=-1
IPLOT=1
CALL PICSIZ(10,0,10,0)
CALL GRAFF(7.5,XKEEP1,XKEEP2,XINC,0,'REFERENCE COORDINATE SYSTEM X
1-VALUE ,XORD,XDUM,5.0,-1.0,2.0,1.0,0.0,NORMALIZED INTERPRETATION S
1CALE ,YORD,YDUM,1.5,5.200,NSRV,2,NMAX,NSRV,LL2,KIND,1.,. .)
158 IF (ITEST.EQ.0) GO TO 172
CALL PFP3(EPS,MIX)
CALL PFP4(CLPA,CDPA,ICK)
COMPUTE INTERIOR PRESSURE COEFFICIENT AND NORMAL VELOCITIES
IF (ICK.EQ.1) CALL VINOUT(JWRITE,VINF,ROE,NQE,VI)
IF (ICANCL.NE.0) GO TO 172
NSRV=0
ICK=ICK+1
IF (ICK.FQ.2) GO TO 145
IF (KNEW.NE.2) GO TO 160
C** ON SECOND PASS THROUGH COMPUTE LIFT & DRAG COEFFICIENTS
CL=CLPA/REFA
CD=(CDPA+CDFA)/REFA
WRITE (JWRITE,159) CL,CD,REFA,REBODY,STOTAL
FCRMT (///,31X,23HTOTAL BODY COEFFICIENTS///,28X,29(1H*))/30X,16H
159 TOTAL BODY CL = ,F11.5,/30X,16HTOTAL BODY CD = ,F11.5,/29X,17HREFE
1RENCE APEA = ,F11.5,/28X,18HREYNOLDS NUMBER = ,E11.4,/32X,14HBODY
1LENGTH = ,F11.5,/28X,29(1H*),//
GO TO 172
160 CALL PFP5(MMAXQD,NMAXQD,AREAAV,AVDELS,AVXCG,CDFA)
IF (ICANCL.NE.0) GO TO 172
C** REMAINING CARDS COMPUTE NECESSARY INFORMATION FOR WAKE-BODY
KNEW=2
NOFS=NOF
NI=1
NI=1
NS=1000
K=(NMAXQD-3)*(MMAXQD-1)
MF=0
NOE=NOE+2*(MMAXQD-1)
LL1S=K
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LL2S=NQE
REWIND KFILE1
DC 161 I=1,I DO
READ (KFILE1)Q,(B(IJK),IJK=1,192)
WRITE (KFILE2)Q,(B(IJK),IJK=1,192)
161 CONTINUE
KFILE=KFILE2
J=JHOLD
IF (J.EQ.0) GO TO 163
DO 162 I=1,J
B(I)=RHOLD(I)
162 Q=QHOLD
JP=JHOLD/16
QADD=QHOLD+.5
P=QADD+JP
I START=(NMAXQD-3)*MMAXQD
IST=I START+MMAXQD
XHOLD1=X(I START+1)
XHOLD2=X(I ST+1)
Y REFERENCE LINE MUST BE 0.0
C** ZAV=0.0
DC 164 I=1,MMAXQD
XNEW(I)=X(I START+I)
YNEW(I)=Y(I START+I)
ZNEW(I)=Z(I START+I)
ZAV=ZAV+ZNEW(I)
THEIA=-90.0*3.14159/180.0
ZAV=ZAV/MMAXQD
RAV=0.0
DC 165 I=1,MMAXQD
PNEW=SQRT((YNEW(I))**2+(ZNEW(I)-ZAV)**2)
PAV=RAV+RNEW
RAV=RAV/MMAXQD
FAC=(AVXCG-XHOLD1)/(XHOLD2-XHOLD1)
AVSLOP=0.0
DO 166 I=1,MMAXQD
YCG=YNEW(I)-(YNEW(I)-Y(I ST+I))*FAC
ZCG=ZNEW(I)-(ZNEW(I)-ZAV)**2*(ZNEW(I)-ZAV)**2)
P1=SQRT((YNEW(I))**2+(ZNEW(I)-ZAV)**2)+2.0*AVDELS
R2=SQRT((YCG)**2+(ZCG-ZAV)**2)+2.0*AVDELS
SLOPF=(R2-R1)/(XHOLD1-AVXCG)
166 AVSLOP=AVSLOP+SLOPE

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AVSLOP=AVSLOP/MMAXXD
AREAT=4.0*AREA*AV*2.0*MMA*XD
XINF=XHOLD1-AREAT/(3.14159*RAV)
CHECK TO MAKE SURE BODY SLOPE IS DECREASING
IF (AVSLOP.GE.0.)AVSLOP=-ABS(RAV/(XINF-XHOLD1))
WRITE (JWRITE,167) AVSLOP,AREAAV,AVXCG,XINF
FORMAT (IHI/50X,24HBEGIN WAKE BODY GEOMETRY//,17H AVERAGE SLOPE =
167 F8.5,3X,22H AVERAGE PANEL AREA = ,F8.5,3X,22H AVERAGE X-CENTROID
1 = ,F10.5,3X,20H END OF BODY AT X = ,F10.5)
DELTAZ=.01
KK=1
XX1=XHOLD1
ZZ2=0.0
RR1=RAV
168 ZZ2=ZZ2+DFLTAZ
XX2=ZZ2*(XINF-XHOLD1)+XHOLD1
RR2=RAV*EXP(AVSLOP*ZZ2)*(1.0-ZZ2)
DTHETA=3.14159/(MMA*XD-1)
AREA2=((RR2+RR1)*SIN(DTHETA/2.0))*SQRT((RR2-RR1)**2+(XX2-XX1)**2)
IF (AREA2.LT.AREAAV) GO TO 168
XK(KK)=XX2
RK(KK)=RR2
XX1=XX2
RR1=RR2
KK=KK+1
IF (KK.GE.4) GO TO 169
GO TO 168
169 XK(4)=XINF
RK(4)=0.0
X1=XK(1)
X2=XK(2)
X3=XK(3)
X4=XK(4)
R1=RK(1)
R2=RK(2)
R3=RK(3)
R4=RK(4)
NSTRT1=MMA*XD
NSTRT2=2*MMA*XD
NSTRT3=3*MMA*XD
NSTRT4=4*MMA*XD
YFAC=(-Y(1))/(XINF-XHOLD1)

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ZFAC=(ZAV-Z(I))/(XINF-XHOLDI)
DO 170 I=1,MMAXQD
  CCSTHT=COS(THETA)
  SINHT=SIN(THETA)
  XNEW(NSRT1+I)=X1
  XNEW(NSRT2+I)=X2
  XNEW(NSRT3+I)=X3
  XNEW(NSRT4+I)=X4
  YNEW(NSRT1+I)=R1*CCSTHT-(XNEW(NSRT1+I)-XHOLDI)*YFAC
  YNEW(NSRT2+I)=R2*CCSTHT-(XNEW(NSRT2+I)-XHOLDI)*YFAC
  YNEW(NSRT3+I)=R3*CCSTHT-(XNEW(NSRT3+I)-XHOLDI)*YFAC
  YNEW(NSRT4+I)=R4*CCSTHT-(XNEW(NSRT4+I)-XHOLDI)*YFAC
  ZNEW(NSRT1+I)=R1*SINHT+ZAV-(XNEW(NSRT1+I)-XHOLDI)*ZFAC
  ZNEW(NSRT2+I)=R2*SINHT+ZAV-(XNEW(NSRT2+I)-XHOLDI)*ZFAC
  ZNEW(NSRT3+I)=R3*SINHT+ZAV-(XNEW(NSRT3+I)-XHOLDI)*ZFAC
  ZNEW(NSRT4+I)=R4*SINHT+ZAV-(XNEW(NSRT4+I)-XHOLDI)*ZFAC
  THETA=THETA+DTHETA
170 STCRE COORDINATES FOR PUNCHING
C** KPI=5*MMAXQD
DO 171 I=1,KPI
  XS(I,START+I)=XNEW(I)
  YS(I,START+I)=YNEW(I)
  ZS(I,START+I)=ZNEW(I)
  XI=XNEW(I)
  YI=YNEW(I)
  ZI=ZNEW(I)
GO TO 131
C** PREPARE FOR NEXT DATA SET
172 IF (IDS.NE.JREAD) REWIND IDS
GO TO 1
C** WARNING: THE FOLLOWING PLOT CARD MAY BE INSTALLATION-DEPENDENT.
173 IF (IPL0T.NE.0) CALL PICSIZ(0.0,0.0)
STOP
END

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FUNCTION SQ2(X,Y,Z)
C** FUNCTION SQ2 CALCULATES THE SQUARE ROOT OF R**2
C RS=X**2+Y**2+Z**2

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7 IF (IROW-ICOLUMN) 7,11,7
  DETERM=-DETERM
  DO 8 L=1,N
    SWAP=A(IROW,L)
    A(IROW,L)=A(ICOLUMN,L)
    A(ICOLUMN,L)=SWAP
  8 IF (M) 11,11,9
  9 DO 10 L=1,M
    SWAP=B(IROW,L)
    B(IROW,L)=B(ICOLUMN,L)
  10 B(ICOLUMN,L)=SWAP
  C** DIVIDE PIVOT ROW BY PIVOT ELEMENT
  11 PIVOT=A(ICOLUMN,ICOLUMN)
  DETERM=DETERM*PIVOT
  A(ICOLUMN,ICOLUMN)=1.0
  DO 12 L=1,N
    A(ICOLUMN,L)=A(ICOLUMN,L)/PIVOT
  12 IF (M) 15,15,13
  13 DO 14 L=1,M
    B(ICOLUMN,L)=B(ICOLUMN,L)/PIVOT
  14 B(ICOLUMN,L)=B(ICOLUMN,L)/PIVOT
  C** REDUCE NON-PIVOT ROWS
  15 DO 20 LI=1,N
    IF (LI-ICOLUMN) 16,20,16
    T=A(LI,ICOLUMN)
    A(LI,ICOLUMN)=0.0
    DO 17 L=1,N
      A(LI,L)=A(LI,L)-A(ICOLUMN,L)*T
  17 IF (M) 20,20,19
  18 DO 19 L=1,M
    B(LI,L)=B(LI,L)-B(ICOLUMN,L)*T
  19 B(LI,L)=B(LI,L)-B(ICOLUMN,L)*T
  20 CONTINUE
  C** INTERCHANGE COLUMNS
  DO 23 I=1,N
    L=N+1-I
    IF (INDEX(L,1)-INDEX(L,2)) 21,23,21
  21 JROW=INDEX(L,1)
  JCCOL=INDEX(L,2)
  DO 22 K=1,N
    SWAP=A(K,JROW)
    A(K,JROW)=A(K,JCCOL)
    A(K,JCCOL)=SWAP
  22 CCNTINUE

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ZNO=ZNP(I)
C*** COMPUTE DISTANCE BETWEEN CENTROID OF REFERENCE QUADRILATERAL AND
C*** CENTROID OF ANOTHER QUADRILATERAL
26 RPO=SQ2F(XC,XCQ,YC,YCQ,ZC,ZCQ)
C*** IF (RPO-ST#4) 27,27,39
C*** TRANSFORM POINT FROM REFERENCE COORDINATE SYSTEM TO ELEMENT(QUAD)
C*** COORDINATE SYSTEM
27 X=(XCQ-XC)*XX+(YCO-YC)*YX+(ZCQ-ZC)*ZX
Y=(XCQ-XC)*XY+(YCO-YC)*YY+(ZCQ-ZC)*ZY
Z=(XCQ-XC)*XN+(YCO-YC)*YN+(ZCQ-ZC)*ZN
C*** IF (RPO-ST#2,0) 28,28,37
C*** COMPUTE VELOCITY COEFFICIENTS BY EXACT METHOD (QUAD SYSTEM)
28 R1=SQ2F(X,X1,Y,Y1,Z,0.)
R2=SQ2F(X,X2,Y,Y2,Z,0.)
R3=SQ2F(X,X3,Y,Y3,Z,0.)
R4=SQ2F(X,X4,Y,Y4,Z,0.)
IF ((R1+R2).LE.D12) GO TO 75
IF ((R2+R3).LE.D23) GO TO 75
IF ((R3+R4).LE.D34) GO TO 75
IF ((R4+R1).LE.D41) GO TO 75
CLA1=ALOG((R1+R2-D12)/(R1+R2+D12))
CLA2=ALOG((R2+R3-D23)/(R2+R3+D23))
CLA3=ALOG((R3+R4-D34)/(R3+R4+D34))
CLA4=ALOG((R4+R1-D41)/(R4+R1+D41))
TVX=CX12*CLA1+CY23*CLA2+CX34*CLA3+CY41*CLA4
TVY=CX12*CLA1+CX23*CLA2+CX34*CLA3+CX41*CLA4
TVZ=0.
IF (ABS(Z/ST)-.010) 38,29,29
29 Z5Q=Z**2
E1=Z5Q+(X-X1)**2
E2=Z5Q+(X-X2)**2
E3=Z5Q+(X-X3)**2
E4=Z5Q+(X-X4)**2
H1=(Y-Y1)*(X-X1)
H2=(Y-Y2)*(X-X2)
H3=(Y-Y3)*(X-X3)
H4=(Y-Y4)*(X-X4)
IF (CI12) 30,30,31
30 WS1=(CM12*FI-H1)/(Z*R1)
WS2=(CM12*E2-H2)/(Z*R2)
TV7=ATAN(WS1)-ATAN(WS2)
31 IF (CI23) 32,32,33

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32 TVZ=TVZ+ATAN((CM23*E2-H2)/(Z*R2))-ATAN((CM23*E3-H3)/(Z*R3))
 33 IF (CI34) 34,34,35
 34 TVZ=TVZ+ATAN((CM24*E3-H3)/(Z*R3))-ATAN((CM34*E4-H4)/(Z*R4))
 35 IF (CI41) 36,36,38
 36 TVZ=TVZ+ATAN((CM41*E4-H4)/(Z*R4))-ATAN((CM41*E1-H1)/(Z*R1))

GO TO 38
 C*** COMPUTE VELOCITY COEFFICIENTS BY QUADRAPOLE METHOD (QUAD SYSTEM)

37 RPQ3=RPQ**3
 RPQ7=(RPQ3**2)*RPQ
 WS1=X/RPQ3
 XSQ=X**2
 YSQ=Y**2
 ZSQ=Z**2
 PS=YSQ+ZSQ-4.*XSQ
 QS=XSQ+ZSQ-4.*YSQ
 WS2=X*(9.*PS+30.*XSQ)/RPQ7
 WS3=3.*Y*PS/RPQ7
 WS4=3.*X*QS/RPQ7
 TVX=A*WS1-CIXY*WS3-CIXX*WS2-CIYY*WS4
 WS1=Y/RPQ3
 WS2=Y*(9.*QS+30.*YSQ)/RPQ7
 TVY=A*WS1-CIXX*WS3-CIXY*WS4-CIYY*WS2
 TVZ=Z*(A/RPQ3-3.*(CIXX*PS-5.*CIXY*X*Y+CIYY*GS)/RPQ7)
 C*** TRANSFORM FROM ELEMENT TO REFERENCE COORDINATE SYSTEM

38 VX(I5)=TVX*XX+TVY*XY+TVZ*XN
 VY(I5)=TVX*YX+TVY*YY+TVZ*YN
 VZ(I5)=TVX*ZX+TVY*ZY+TVZ*ZN
 GO TO 40
 C*** COMPUTE VELOCITY COEFFICIENTS BY MONOPOLE METHOD (DIRECTLY IN THE
 C*** REFERENCE COORDINATE SYSTEM)

39 ARPQ3=A/(RPQ**3)
 VX(I5)=(XCQ-XC)*ARPQ3
 VY(I5)=(YCQ-YC)*ARPQ3
 VZ(I5)=(ZCQ-ZC)*ARPQ3
 C*** REFLECT CENTROID POINT IN PLANE OF SYMMETRY

40 GO TO (41,43,45,46,48,49,50,51),IS
 C*** DC LOOPS SET UP TO FORCE USE OF INDEX REGISTERS
 41 J1=JV
 J2=JC
 V1(J1)=VX(1)
 V1(J1+1)=VY(1)
 V1(J1+2)=VZ(1)

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42 IF (ISM) 54.54.42
C*** IS=2
XZ SYMMETRY
YCO=-YCO
GO TO 26
43 IF (ISM-1) 53.53.44
C*** XY SYMMETRY
IS=3
ZCO=-ZCO
GO TO 26
45 IS=4
YCO=-YCO
GO TO 26
46 IF (ISM-2) 52.52.47
C*** YZ SYMMETRY
IS=5
XCO=-XCO
GO TO 26
48 IS=6
YCO=-YCO
GO TO 26
49 IS=7
ZCO=-ZCO
GO TO 26
50 IS=8
YCO=-YCO
GO TO 26
C*** ADD CONTRIBUTIONS OF ALL REFLECTIONS TO OBTAIN NET INDUCED
C*** VELOCITY COMPONENTS IN REFERENCE COORDINATE SYSTEM
51 V1(J1)=V1(J1)+VX(8)+VX(7)+VX(6)+VX(5)
V1(J1+1)=V1(J1+1)-VY(8)+VY(7)+VY(6)-VY(5)
V1(J1+2)=V1(J1+2)-VZ(8)-VZ(7)+VZ(6)+VZ(5)
52 V1(J1)=V1(J1)+VX(4)+VX(3)
V1(J1+1)=V1(J1+1)+VY(4)-VY(3)
V1(J1+2)=V1(J1+2)-VZ(4)-VZ(3)
53 V1(J1)=V1(J1)+VX(2)
V1(J1+1)=V1(J1+1)-VY(2)
V1(J1+2)=V1(J1+2)+VZ(2)
C*** CALCULATE THE NORMAL VELOCITY INDUCED AT THE CONTROL POINT OF THE
C*** 1-TH ELEMENT BY A UNIT SOURCE DENSITY ON THE J-TH ELEMENT (STORED
C*** BY COLUMNS)
54 C1(J2)=XNQ*V1(J1)+YNO*V1(J1+1)+ZNO*V1(J1+2)

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JV=JV+3
55 JC=JC+1
C** WRITE COEFFICIENTS ON TAPE
    IF (JV-1001) 61,56,56
56 JV=2
    VI(1)=BLK
    IF (BLK-636.0) 57,58,59
57 WRITE (KFILE3)BLK,VI
    GO TO 60
58 REWIND KFILE3
59 WRITE (KFILES)BLK,VI
60 BLK=BLK+1.
61 IF (JC-901) 63,62,62
62 IDW=IDW+1
    WRITE (KFILE4)IDW,C1
    JC=1
63 KO=KQ+1
    L=L+1
    END OF LOOP OVER CENTROIDS
C** IF (KO-KM) 25,25,64
64 C1(JC)=0
65 P=P+1
    IF (KO-KMM) 55,65,65
    K=K+1
    J=J+16
    IF (K-KM) 66,66,70
C** IF (OF LOOP OVER QUADRILATERALS
C** READ NEXT BLOCK OF B ARRAY IF NEEDED
66 IF (J-193) 4,67,67
67 READ (KFILE)(B(I),I=1,193)
    J=2
    IF (B(1)-P) 68,4,68
68 WRITE (JWRITE,69) B(1),P
69 FORMAT (28H0 POINTS OUT OF ORDER B(1)=,1F4.0,4H P=,1F4.0)
    RETURN
70 IF (BLK-636.0) 71,72,73
C** WRITE REMAINING COEFFICIENTS ON TAPE
71 WRITE (KFILE3)BLK,VI
    GO TO 74
72 REWIND KFILE3

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73 WRITE (KFILES)BLK,V1
74 REWIND KFILES
74 WRITE (KFILES4)IDM,C1
74 REWIND KFILES4
74 REWIND KFILE
75 GO TO 77
75 WRITE (JWRITE,76) L,P
76 FORMAT (3H L=.15,20X,3H P=,F5.1)
77 RETURN
77 END

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```

C***
C FUNCTION SQ2F(X1,X2,Y1,Y2,Z1,Z2)
C
FUNCTION SQ2F(X1,X2,Y1,Y2,Z1,Z2)
FUNCTION SQ2F CALCULATES THE DISTANCE BETWEEN TWO POINTS
X=X1-X2
Y=Y1-Y2
Z=Z1-Z2
RS=Z**2+Y**2+X**2
SQ2F=SQRT(RS)
RETURN
END

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SUBROUTINE PFP3(EPS,MIX)
SUBROUTINE PFP3 SOLVES FOR SOURCE DENSITY
DIMENSION VIP(650),S(5,650),COEF(900),VTX(650)
COMMON TITLF(20),XCP(650),YCP(650),ZCP(650),XNP(650),YNP(650),ZNP(
1650),AQP(650),REFA,RFRCDY,NQUAD,IWRITE,NP,KNEW
COMMON /INOUT/JREAD,JWRITE,KFILE,KFILE1,KFILE2,KFILE3,KFILE4,KFILE
15
COMMON /SIK/SN(650),VNP(650),IPN(650)
COMMON /RING/VXX(3,650)
WRITE (JWRITE,1)
1 FCRMAT(1H1,/,/,2,4H0SOURCE DENSITY SOLUTION)
WRITE (JWRITE,2) (TITLE(I),I=1,20)

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2  FORMAT (1H0,20A4)
   K1=1
   K2=NP
   SET CONDITIONS FOR CNSET FLOW OF -1.0+VXX(1,K) IN X DIRECTION.
   ZFPO IN Y AND Z DIRECTIONS
   FX=-1.0
   CCMPUTE (1) DOT PRODUCT OF PANEL NORMAL TO CNSET FLOW, VIP(K),
   (2) DOT PRODUCT OF PANEL NORMAL TO NONUNIFORM FLOW, VIX(K),
   (3) INITIAL SOURCE DENSITY. AND SET PARTIAL SUM VECTOR TO ZERO
   DO 3 K=1,NP
   VIP(K)=XNP(K)*FX
   VIX(K)=XNP(K)*VXX(1,K)
   S(5,K)=- (VIP(K)+VIX(K)-VNP(K))* .11936
3  SN(K)=0.
   SN(NP+1)=0.
   SN(NP+2)=0.
   SN(NP+3)=0.
   SN(NP+4)=0.
   WRITE (JWRITE,30) FX
   WRITE (JWRITE,4)
4  FORMAT (/,12X,37HITERATIVE MATRIX SOLUTION INFORMATION.,/ ,27H0ITERA
   TION SUM OF CHANGES,9X,1HA,10X,2HB1,10X,2HB2)
   IT=1
   IC=5
   START ITERATION, READ FIRST BLOCK OF COEFS., START LOOP OVER QUADS.
5  READ (KFILE4)IDW,COEF
   (DO LOOP 40) CALCULATES THE SUM OF THE PRODUCTS OF THE INDUCED
   VELOCITIES AND THE SOURCE DENSITIES
   J=0
   DO 8 K=1,NP
   PICK UP SOURCE DENSITY & START LOOP OVER CENTROID POINTS
   SP=S(IC,K)
   DO 8 KP=1,NP,5
   IF (J-9)GO 7,6,6
6  READ (KFILE4)IDW,COFF
   J=0
   CCMPUTE PARTIAL SUMS FOR NEXT 5 POINTS
7  SN(KP)=SN(KP)+COEF(J+1)*SP
   SN(KP+1)=SN(KP+1)+COEF(J+2)*SP
   SN(KP+2)=SN(KP+2)+COEF(J+3)*SP
   SN(KP+3)=SN(KP+3)+COEF(J+4)*SP
   SN(KP+4)=SN(KP+4)+COEF(J+5)*SP

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C***      J=J+5      END LOOP OVER CENTROID POINTS & END LOOP OVER QUADS.
          CCNTINUE
C***      CCOMPUTE NEW SOURCE DENSITIES
          REWIND KFILE4
          PASS=1.0
          SUM=0.
          DC 9 K=K1,K2
          SN(K)=-(SN(K)+VIP(K)-VNP(K)+VTX(K))/6.283185308
          TEST=ABS(SN(K)-S(IC,K))
          SUM=SUM+TEST
          IF (TEST.GT.EPS)PASS=-1.0
          CCNTINUE
          WRITE (JWRITE,29) IT,SUM
          IF (PASS.EQ.1.0) GO TO 27
          IF (IT.EG.MIX) GC TO 27
          IT=IT+1
          IC=IC-1
          IF (IC.EQ.0) GO TO 11
          DO 10 K=K1,K2
          S(IC,K)=SN(K)
          SN(K)=0.
          GC TO 5
10      A=0.
11      B1=0.
          B2=0.
          DA=0.
          D1=0.
          D2=0.
          DC 17 K=K1,K2
          DS9=2*S(1,K)-SN(K)-S(2,K)
          IF (DS9.GT.0.) GO TO 12
          A=A+S(2,K)-S(1,K)
          CA=DA-DS9
          GC TO 13
12      A=A+S(1,K)-S(2,K)
          DA=DA+DS9
13      DS1=S(4,K)-S(3,K)
          DS2=S(3,K)-S(2,K)
          DS3=DS1-DS2
          DSS=S(2,K)-S(1,K)
          DSS=DS2-DSS

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PF3 140
PF3 141

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DS6=DS1-DSS
DS4=DS2-S(1,K)+SN(K)
DS7=DS3+DS4-DSS*DS6
DS8=DS6+DS5-DS4*DS3
IF (DS7.GT.0.) GO TO 14
BI=B1-DS1+DS4+DS2*DS6
DI=D1-DS7
GC TO 15
14 BI=B1+DS1*DS4-DS2*DS6
15 IF (DS8.GT.0.) GC TO 16
16 B2=B2-DS1*DS5+DS2*DS3
17 D2=D2-DS8
GO TO 17
18 B2=B2+DS1*DS5-DS2*DS3
D2=D2+DS8
A=A/DA
BI=B1/D1
B2=B2/D2
IF (IT.EQ.6) GO TO 23
AA=ABS(A-AS)
IF (AA.GT..02) GO TO 20
DC 18 K=K1,K2
S(S,K)=A*(SN(K)-S(1,K))+S(1,K)
SN(K)=0.
18 WRITE (JWRITE,19)
19 FCRMAT (29X,17HA EXTRAPCLATION )
GC TO 25
20 BB1=50.*ABS(B1-BS1)
BB2=50.*ABS(B2-BS2)
BBB=ABS(B1)+ABS(B2)
IF ((BB1.GT.BBB).OR.(BB2.GT.BBB)) GO TO 23
DC 21 K=K1,K2
S(S,K)=S(2,K)+B1*(S(1,K)-S(2,K))+B2*(SN(K)-S(2,K))
SN(K)=0.
21 WRITE (JWRITE,22)
22 FCRMAT (29X,17H3 EXTRAPCLATION )
GC TO 25
23 DO 24 K=K1,K2
24 S(S,K)=SN(K)
SN(K)=0.

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PF3 142
 PF3 143
 PF3 144
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 PF3 147
 PF3 148
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 PF3 152
 PF3 153
 PF3 154
 PF3 155

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25 IC=5
   WRITE (JWRITE,26) A,B1,B2
26 FORMAT (29X,3E12.3)
   AS=A
   BS1=B1
   BS2=B2
   GC TO 5
27 DC 28 K=K1,K2
28 S(1,K)=SN(K)
29 FFORMAT (4X,I3,E18.5)
30 FFORMAT (/,13H0 X VELOCITY=.F4.1,24H+VXX(1,K)
   Z VELOCITY=.4H 0.0)
   Y VELOCITY=.4H 0.0
   RETURN
   FND
  
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C***
C***
C
SUBROUTINE PFP4(CLPA,CDPA,ICK)
SUBROUTINE PFP4 COMPUTES VELOCITIES AND PRESSURE COEFFICIENTS AT
THE PANEL CENTROID POINTS
DIMENSION CV1(1000)
COMMON YITLE(20),XCP(650),YCP(650),ZCP(650),XNP(650),YNP(650),ZNP(
1650),AQP(650),REFA,REBODY,NQUAD,IWRITE,NP,KNEW
CCMMGN /RING/VTX(3,650)
COMMON /SIK/SI(650),VNP(650),IPNI(650)
COMMON /VCK/HVF,SFC,DEP,CPHA,TINF,ADUT,AIN,EDA
COMMON /CFXS/CPS(650),CPIN,CPOUT
COMMON /VXYZ/VX1(650),VY1(650),VZ1(650),VABS(650)
COMMON /HOLD/XNH(650),ZNH(650),AOPH(650)
COMMON /INOUT/JREAD,JWRITE,KFILE,KFILE1,KFILE2,KFILE3,KFILE4,KFILE
15
C
WRITE (JWRITE,1)
CFRMT (1H1,/,/,1X,75H COMPUTATION OF VELOCITIES AND PRESSURE COEFF
1 IICENTS AT THE PANFL CENTROIDS)
INITIALIZE PARAMETERS
D=-.5/3.14159265
J=1
KI=1
IF (KNEW.EQ.1) K HOLD=NP
C***
C***
  
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67 PF4

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K2=NP
BBR=1.0
CD=0.0
CL=0.0
AREA=0.0
C*** READ FIRST BLOCK OF COEFFICIENTS
      ITAPE=KFILE3
      IF (BB-BBR) 45,2,45
C*** CALCULATE VELOCITY COMPONENTS DUE TO ENTIRE FLOW FIELD
      DO 3 I=K1,K2
        VX1(I)=-1.0+VTX(1,I)+VNP(I)*XNP(I)-S1(I)*XNP(I)/D
        VY1(I)=VTX(2,I)+VNP(I)*YNP(I)-S1(I)*YNP(I)/D
        VZ1(I)=VTX(3,I)+VNP(I)*ZNP(I)-S1(I)*ZNP(I)/D
      3 CCNTINUE
C*** SFT UP LOOP OVER QUADS. PICK UP SOURCE, SET UP LOOP OVER CENTROIDS
C*** TO SUM THE PRODUCTS OF THE VELOCITY REFLECTIONS AND THE SOURCE
C*** DENSITIES
      JC=2
      4 SIJ=S1(J)
      DO 10 JP=K1,K2
        COMPUTE PARTIAL SUM FOR 3 COMPONENTS OF 3 VELOCITIES
        VX1(JP)=VX1(JP)+SIJ*CV1(JC)
        VY1(JP)=VY1(JP)+SIJ*CV1(JC+1)
        VZ1(JP)=VZ1(JP)+SIJ*CV1(JC+2)
      JC=JC+3
C*** READ MORE COEFFICIENTS IF NEEDED
      IF (JC-1000) 10,5,5
      5 JC=2
      IF (BBR-635.0) 6,7,8
      6 READ (KFILE3)BB,CV1
      GO TO 9
      7 REWIND KFILE3
      8 READ (KFILE5)BB,CV1
      9 BBR=BBR+1.
      IF (BBR-BB) 45,10,45
C*** END OF LOOP OVER CENTROIDS THEN END OF LOOP OVER QUADS.
      10 CCNTINUE
      J=J+1
      11 IF (J-NP) 4,4,11
      12 REWIND KFILE3

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GO TO 14
13 REWIND KFILES
14 IP=K1+49
C*** THE VELOCITIES AT THE CONTROL POINTS ON THE BODY SURFACE HAVE BEEN
C*** CALCULATED
IS=K1
IPAGE=1
IIN=0
ICUT=0
CPIN=0.0
CPOUT=0.0
ACUT=0.0
AIN=0.0
15 IF (IP-K2) 16,16,28
C*** COMPUTE PRESSURE COEFFICIENT, ABSOLUTE VALUE OF VELOCITY, CL, & CD
16 IF (IPAGE.EQ.1) WRITE (JWRITE,17) (TITLE(1),I=1,20),IPAGE
17 FORMAT (//,1H0,20A4,8H PAGE =,I5)
18 IF (IPAGE.NE.1) WRITE (JWRITE,18) (TITLE(1),I=1,20),IPAGE
19 IF (IPAGE.EQ.1) WRITE (JWRITE,19)
19 WRITE (JWRITE,19)
19 FORMAT (8H0 X FLOW)
20 WRITE (JWRITE,20)
20 FORMAT (4H PT.,10X,2HXC,8X,2HYC,8X,2HZC,12X,2HVX,8X,2HVV,8X,2HVZ,9
1X,5HABS.V,8X,2HCP,6X,6HSOURCE,5X,8HV NORMAL,5X,4HAREA)
DO 27 I=1,IP
VSO=VX1(I)**2+VY1(I)**2+VZ1(I)**2
VM=SQRT(VSQ)
VARS(I)=VM
CP=1.-VSO
CPS(I)=CP
VNR=VX1(I)*XNP(I)+VY1(I)*YNP(I)+VZ1(I)*ZNP(I)
IF (KNEW.EQ.2.OR.ICK.GE.2) GO TO 23
CHECK INDICATOR FOR A NONZERO NORMAL VFLOCITY SPECIFICATION
IF (IPN(I).EQ.0) GO TO 23
IF ((1+IPN(I))/ABS(IPN(I))).EQ.0) GO TO 21
GO TO 22
21 CPIN=CPIN+CP*AQP(I)
AIN=AIN+AQP(I)
IIN=IIN+1
GC TO 23
22 CPOUT=CPOUT+CP*AQP(I)
ACUT=ACUT+AQP(I)

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ICUT=IOUT+1
23 IF (I.GT.KHOLD) GO TO 25
   IF (KNEW.EQ.2) GO TO 24
   CL=CL+CP*AQP(I)*ZNP(I)
   CD=CD+CP*AQP(I)*XNP(I)
   AREA=AREA+AQP(I)
   GO TO 25
C**  COMPUTE CL, CD, AND AREA FOR WAKE-BODY PORTION
24 CL=CL+CP*AOPH(I)*ZNH(I)
   CD=CD+CP*AOPH(I)*XNH(I)
   AREA=AREA+AOPH(I)
C**  WRITE CENTROID POINTS, VFLOCITIES, CP'S, CL-PRESSURE, & CD-PRESSURE
25 WRITE (JWRITE,25) I,XCP(I),YCP(I),VZ1(I),VY1(I),VM,C
26 FORMAT (1X,13,4X,3F10.5,2F11.5,E12.2,2X,E10.3)
27 CCNTINUE
   IS=IS+50
   IP=IP+50
   IPAGE=IPAGE+1
   IF (K2-IS) 29,28,15
28 IP=K2
   GO TO 16
C**  ADJUST AND REFERENCE CL AND CD DUE TO SYMMETRY AND REFERENCE AREA
29 CLPA=2.0*CL
   CLP=CLPA/REFA
   CDP=CJPA/REFA
   WRITE (JWRITE,30) CLP,CDP,REFA,REBODY
30 FCRMAT (1H,///,18X,35HPRESSURE LIFT AND DRAG COEFFICIENTS,/,2
   11X,29(1H*),/,25X,14HPRESSURE CL = ,F11.5,/,25X,14HPRESSURE CD = ,F
   11.5,/,22X,17HREFERENCE AREA = ,F11.5,/,21X,18HREYNOLDS NUMBER = ,
   1E11.4,/,21X,29(1H*),///)
   IF (KNEW.EQ.2) GO TO 35
   WRITE (JWRITE,31)
31 FCRMAT (1H,///,2X,2HPT,5X,3HXNH,6X,3HYNH,6X,3FZNH,6X,2HCP,5X,6HVX*
   1XNH,3X,6HVV*YNH,3X,6HVZ*ZNH,5X,4HAQP1,3X,13H2*CP-AOPH*ZNH,3X,13H2*
   1CP*AOPH*XNH,4X,2HPT,///)
   LINE=)
DC 34 I=1,NP
VXXN=VX1(I)*XNP(I)
VYYN=VY1(I)*YNP(I)
VZZN=VZ1(I)*ZNP(I)

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CAZ=2.0*CPS(I)*AQP(I)*ZNP(I)
CAX=2.0*CPS(I)*AQP(I)*XNP(I)
LINE=LINE+1
IF (LINE.LE.50) GO TO 32
LINE=0
WRITE (JWRITE,31)
WRITE (JWRITE,33) I,XNP(I),YNP(I),ZNP(I),CPS(I),VXXN,VYYN,VZZN,AQP
32 1(I),CAZ,CAX,I
33 FORMAT (1X,I4,7F9.5,F8.3,X,F10.7,6X,F10.7,5X,I4)
34 CCONTINUE
GO TO 41
35 WRITE (JWRITE,36)
36 FORMAT (1H1,/,2X,2HPT,5X,3HXNP,6X,3HYNP,6X,3HZNP,6X,2HCP,5X,6HVX*,
1XNP,3X,6HVV*YNP,3X,6HVZ*ZNP,5X,4HAQP,3X,13H2*CP*AGPH*ZNH,3X,13H2*
1CP*AOPH*XNH,4X,2HPT,/)
LINE=0
DO 40 I=1,NP
VXXN=VX1(I)*XNP(I)
VYYN=VY1(I)*YNP(I)
VZZN=VZ1(I)*ZNP(I)
LINE=LINE+1
IF (LINE.LE.50) GO TO 37
LINE=0
WRITE (JWRITE,36)
37 IF (I.GT.KHOLD) GO TO 38
CAZ=2.0*CPS(I)*ACPH(I)*ZNH(I)
CAX=2.0*CPS(I)*AQP(I)*XNH(I)
WRITE (JWRITE,33) I,XNP(I),YNP(I),ZNP(I),CPS(I),VXXN,VYYN,VZZN,AQP
1(I),CAZ,CAX,I
GC TO 40
38 WRITE (JWRITE,39) I,XNP(I),YNP(I),ZNP(I),CPS(I),VXXN,VYYN,VZZN,AQP
1(I),I
39 FCRMAT (1X,I4,7F9.5,F8.3,34X,I4)
40 CONTINUE
41 IF (KNEW.EQ.0.OR.ICK.GE.2) GO TO 47
C***
TEST FOR ERRORS
IF (IIN.EQ.0.OR.IOUT.EQ.0) ICK=2
IF (ICK.EQ.1) GO TO 44
WRITE (JWRITE,42)
42 FCRMAT (1X,/,1X,131HAT LEAST ONE INLET(OUTLET) WAS SPECIFIED WIT
1HCUT AT LEAST ONE OUTLET(INLET)...ASSUMING NO INLETS OR OUTLETS...
1EXECUTION PROCEEDING.../)

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PF4 193


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5 FORMAT (12X,32HCPX > CPIN OR CPX < CPXX. STOP.//)
6 ICANCL=1
7 RETURN
7 IF (CPXX.LE.CPX.AND.CPXX.GE.CPOUT) GO TO 9
8 WRITE (JWRITE,8)
8 FORMAT (12X,34HCPXX > CPX OR CPXX < CPOUT. STOP.//)
GO TO 6
C*** ADJUST EFFECTIVE ORIFICE AREA EFFECT
9 IPASS=IPASS+1
IF (IPASS.GT.1) GO TO 14
PNET=DEP*(778.0+HVF*SFC-1.0)
IF (PNET) 10,10,12
10 WRITE (JWRITE,11) PNET
11 FFORMAT (12X,23HDEP*(778.0+HVF*SFC-1) =,1PE16.9./)
IF (PNET.LT.0.0) GO TO 6
GO TO 14
12 TR=PNET/(ROE*32.2*AIN*CPHA*778.0*TINF*VIN*VINF*SQR(CPIN-CPX))+1.0
TR=SQR(1.0/TR)
ECA=EOA*TR
WRITE (JWRITE,13) TR,ECA
13 FFORMAT (9X,58HADJUSTMENT DUE TO HEATING OF FLOW: TEMPERATURE RATIO
1 =,1PE16.9./,44X,23HEFFECTIVE ORIFICE AREA=,1PE16.9./)
GO TO 2
C*** CALCULATE NORMAL VELOCITIES
14 DC 24 I=1,NQE
ITEST=3
IF (IPN(I).EQ.0) GO TO 24
IF ((1+IPN(I))/ABS(IPN(I))).EQ.0) GO TO 15
GO TO 16
15 X1=CPS(I)-CPX
IF (X1.LT.0.0) ITEST=1
VNP(I)=-SQR(ABS(X1))
GO TO 17
16 X1=CPXX-CPS(I)
IF (X1.LT.0.0) ITEST=2
VNP(I)=SQR(ABS(X1))
GO TO (18,20,22),ITEST
18 WRITE (JWRITE,19) I,VNP(I),I
19 FFORMAT (10X,24HNORMAL VELOCITY AT PANEL,14,3H = ,E14.7,10X,11HNOTE
1 : ( CP(,14,11H)-CPX )<0.0./)
GO TO 24
20 WRITE (JWRITE,21) I,VNP(I),I

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VNT 70

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21 FORMAT (10X,24HNORMAL VELOCITY AT PANEL,I4,3H = ,E14.7,10X,16HNOTE
1: ( CPXX-CP(.I4,6H))<0.0./)
   VC TO 24
22 WRITE (JWRITE,23) I,VNP(I)
23 FORMAT (10X,24HNORMAL VELOCITY AT PANEL,I4,3H = ,E14.7./)
24 CONTINUE
   RETURN
   END
VNT 71
VNT 72
VNT 73
VNT 74
VNT 75
VNT 76
VNT 77
VNT 78

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SUBROUTINE PUNCH(NMIN,NMAX,MMIN,MMAX,X,Y,Z,JPUNCH,JWRITE)
1 2 3 4 5 6 7 8 9
PCH 10 11 12
PCH 13 14 15 16
PCH 17 18 19
PCH 20 21 22
PCH 23 24 25 26
PCH 27 28 29
PCH 30 31
SUBROUTINE PUNCH CONVERTS AND PUNCHES THE (BODY+WAKEBODY) DATA
BACK TO A COMPATIBLE PLOT PROGRAM DATA SET FOR THE FUSELAGE
DIMENSION X(651),Y(651),Z(651),XX(31,31),YY(31,31),ZZ(31,31)
SET INITIAL PARAMETERS
NS=1
L=G
LMN=1
CONVERT TO ORIGINAL AXIS SYSTEM
ZMAX=-1000.0
ZMIN=1000.0
DO 1 N=NMIN,NMAX
DC 1 M=MMIN,MMAX
L=L+1
IF (M.GT.MMIN.AND.M.LT.MMAX) GO TO 1
IF (ZMAX.LT.Z(L)) ZMAX=Z(L)
IF (ZMIN.GT.Z(L)) ZMIN=Z(L)
CONTINUE
ZORG=ABS(ZMIN)+ABS(ZMAX)
L=0
DO 3 N=NMIN,NMAX
XP=X(1)-X(LMN)
DC 2 M=MMIN,MMAX
L=L+1
YP=Y(L)
ZP=Z(L)
XX(N,M)=XP
YY(N,M)=YP

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43 PCH
44 PCH

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ZZ(N,M)=ZP+ZORG
CONTINUE
LMN=LMN+MMAX
CONTINUE
C***
PUNCH CARDS FOR NEW FUSELAGE
WRITE (JPUNCH,4) (XX(J,1),J=NMIN,NMAX)
DO 5 I=NMIN,NMAX
WRITE (JPUNCH,4) (YY(I,J),J=MMIN,MMAX)
WRITE (JPUNCH,4) (ZZ(I,J),J=MMIN,MMAX)
CONTINUE
RETURN
END
  
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SUBROUTINE PFP5(MM,NN,AREAAV,AVDELS,AVXCG,CDFA)
SUBROUTINE PFP5 COMPUTES ON-BODY STREAMLINES
DIMENSION XC1(650),YC1(650),XC2(650),YC2(650),XC3(650),XC4(650),YC
14(650),X3(650),Y3(650),Z3(650),X4(650),Y4(650),Z4(650),DMX(650),XL
1(75),YL(75),ZL(75),YC3(650),SF(5),XCR(5),YCR(5),STML(75),UABS(75),
1SKJN(650),DSTAR(650),NQTST(5)
EQUIVALENCE (YC3(1),YC2(1)),(XL(1),XNH(1)),(YL(1),AQPH(1)),(ZL(1),
1ZNH(1))
COMMON /HOLD/XNH(650),ZNH(650),AQPH(650)
COMMON TITLF(20),XCP(650),YCP(650),ZCP(650),XNP(650),YNP(650),ZNP(
1650),AQP(650),REFA,REBODY,NQUAD,IWRITE,NP,KNEW
COMMON /VXY7/VX1(650),VY1(650),VZ1(650),VABS(650)
COMMON /BL/VOV(75),SS(75),VINP,VO,ROE,DELS(150),CFI(150),THT(150),
1STOTAL,KKK
COMMON /INDUT/JREAD,JWRITE,KFILE,KFILE1,KFILE2,KFILE3,KFILE4,KFIL5
COMMON /RING/VIX(3,650)
COMMON /CANCEL/ICANCL,NGDE
COMMON /NAMI/NP,NG,DMX/NAM2/II,NSTART,NEND,NDEL/NAM3/LL,MID,DIRT
1,J1/NAM4/AF,UX,UY,UZ,CP,NQ,NCP,LNO,JSTOP,J,JL,XYL,YL,ZL/NAM
15/NQ,IQT,NR,NU,LXQ,UYQ,UZQ,JXR,UZR,UXU,UZU,UQ,VQ,CSR,UI,VT
1,XXR,XYR,UR,YXR,VR,UU,CSU,VU,XD,YD,ZD,XI,YTI,ZI,YT,XR,YR/NAM6/
1XD,YD,ZD,XU,YT,ZT,YU,DEN,U1,U2,V1,V2,USL,VSL,UXP,UYP,USQD/NAM7
1/DEN,CXY,CY,CX,CG,NQ,XCR,SF,TEST/NAM8/N,XM,YM,SFM,AC,BC/NAM9
1/XNTP,YNTP,TESTP/NAM10/TEST,XNT,YNT/NAM11/UX,UY,UZ,CP,UABS/NAM12/J
  
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1L.J.JI.USL.VSL.UX.UY.UZ.VSQD.CORD.STML.CP.AF.LNQ/NAM13/KMOD.NTEST.
1NQ.NOTEST.M/NAM14/M.I.TEST.DS1.DS2.DS3.DS4.XLT.YLT.ZLT.ZSQ/NAM15/T
1EST.RC1.RC2.RC3.RC4/NAM16/TEST/NAM17/TEST/NAM18/TEST/NAM19/DIRT.JI
1.JMIN/NAM20/JMAX.SSS.STML/NAM21/KEY.JJ.KK.JMIN/NAM22/XL.YL.ZL.UABS
1/NAM23/KEY.KK.JJ.JMAX/NAM24/JMN.JMX.AF.L/NAM25/J.L.STML.UABS.AF.MI
1D/NAM26/L.K.STML.UABS/NAM27/L.JMAX.JMIN.STML.XL.YL.ZL.UABS
COMMON /SIK/SN(650),VNP(650),IPN(650)

WRITE (JWRITE,1)
1 FORMAT (1H1,///.35HOCALCULATION OF ON-BODY STREAMLINES)
NB=(NP+11)/12
NLIN=NQUAD
DO 2 I=1,NB
IFN=I*12
IS=IFN-11
READ PANEL GEOMETRY FROM TAPE
RFAD (KFILF)O,(XC1(J),YC1(J),XC2(J),YC2(J),XC3(J),XC4(J),YC4(J),X3
1(J),Y3(J),Z3(J),X4(J),Y4(J),Z4(J),(SKIP,K=1,3),J=IS,IFN)
NQ=Q
IF (NQ.NE.IS) GO TO 68
2 CCNTINUE
NCD1=NP+1
NCD2=NOD1
IWRTS=IWRITE
IF (NODE.GT.NP)NOD2=0
IF (NOD2.LF.0) GO TO 3
NOD1=NODE-2
NCD2=NODE+2
IF (NCD1.LE.0)NJD1=1
IF (NOD2.GT.NP):NOD2=NP
FOR EACH QUAD, COMPUTE SQUARE OF THE RADIUS OF A CIRCLE ABOUT THE
CENTROID WHICH ENCLOSES THE QUAD WITH 1% TO SPARE
3 DC 4 I=1,NP
D1=(XC1(I)**2+YC1(I)**2)*1.01
D2=(XC2(I)**2+YC2(I)**2)*1.01
D3=(XC3(I)**2+YC3(I)**2)*1.01
D4=(XC4(I)**2+YC4(I)**2)*1.01
IF (I.GT.75) GO TO 4
XL(I)=0.0
YL(I)=0.0
ZL(I)=0.0
STML(I)=0.0

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UABS(I)=0.0
VCV(I)=0.0
SS(I)=0.0
4 DMX(I)=AMAX1(D1,D2,D3,D4)
  IF (NODE.NE.0) WRITE (JWRITE,NAM1)
  MID=70
  MAXJ=75
  MINJ=1
  VXI=-1.0
  IF (NLINE.EQ.0) GO TO 70
  WRITE (JWRITE,5) (ITITL(I),I=1,20)
  5 FORMAT (//,.1H0,20A4)
  IF (IWRITE.GT.1) GO TO 7
  WRITE (JWRITE,6) NLINE
  6 FORMAT (1X,47HFOR V INFINITY = -1.0+VXX(1,K),0.0,0.0,
  7 COMPUTE,14.5
  8 OH STREAMLINES STARTING AT EACH PANEL CENTROID POINT)
  9 CALCULATE STREAMLINES FOR EACH PANEL CENTROID OMITTING TRIANGULAR
  10 PANELS AT ENDS. LINES FOUND FROM NOSE TO 3 PTS PAST PANE_ CENTROID
  11 IUPPER=NLINE+1-2*(MM-1)
  12 ILCWER=2*(MM-1)
  NLINE=NLINE-1
  DO 61 II=1,3
  IF (II-2) 8,9,10
  8 NSTART=2
  NEND=2*(MM-1)
  NDEL=2
  IWRITS=IWRITE
  GO TO 11
  9 NSTART=NEND+1
  NEND=(NN-3)*(MM-1)
  NDEL=1
  GO TO 11
  10 NSTART=NEND+1
  NEND=(NN-1)*(MM-1)-1
  NDEL=2
  11 IF (NODE.NE.0) WRITE (JWRITE,NAM2)
  IWRITS=IWRITS
  IF (LL.LY.NOD1) GO TO 12
  IF (UL.GT.NOD2) GO TO 12
  IWRITE=-1
  12 MID=70

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DIRT=-1.  
JI=-1  
IF (IWRITE.LT.0) WRITE (JWRITE,NAM3)  
13 AF=1.  
UX=0.  
UY=0.  
UZ=0.  
CP=0.  
STML(MID)=0.  
NQ=LL  
NCP=LL  
LNQ=NG  
XL(MID)=XCP(LL)  
YL(MID)=YCP(LL)  
ZL(MID)=ZCP(LL)  
JSTOP=MID+3  
J=MID  
JL=J  
XLT=(XL(J)-XCP(NQ))*X3(NQ)+(YL(J)-YCP(NQ))*Y3(NQ)+(ZL(J)-ZCP(NQ))*  
1 Z3(NQ)  
YL=(XL(J)-XCP(NQ))*X4(NQ)+(YL(J)-YCP(NQ))*Y4(NQ)+(ZL(J)-ZCP(NQ))*  
1 Z4(NQ)  
XL(J)=XLT*X3(NQ)+YLT*X4(NQ)+XCP(NQ)  
YL(J)=XLT*Y3(NQ)+YLT*Y4(NQ)+YCP(NQ)  
ZL(J)=XLT*Z3(NQ)+YLT*Z4(NQ)+ZCP(NQ)  
IF (IWRITE.LT.0) WRITE (JWRITE,NAM4)  
14 IQT=MOD(NQ,4)+1  
GO TO (18,15,16,17),IQT  
15 NR=NQ+1  
NU=NQ+2  
GO TO 19  
16 NF=NG+2  
NU=NQ-1  
GO TO 19  
17 NR=NG-2  
NU=NQ+1  
GC TO 19  
18 NR=NG-1  
NU=NQ-2  
19 UXC=- (VXI*VXI(NQ))  
UYQ=- (VXI*VXI(NQ))  
UZQ=- (VXI*VZI(NQ))
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UXR=((VXI*VXI(NR))
 UYR=((VXI*VYI(NR))
 UZR=((VXI*VZI(NR))
 UXU=((VXI*VXI(NU))
 UYU=((VXI*VYI(NU))
 UZU=((VXI*VZI(NU))
 TRANSFORM VELOCITIES TO QUAD. SYSTEM
 UO=UXQ*X3(NQ)+UYQ*Y3(NQ)+UZQ*Z3(NQ)
 VO=UXQ*X4(NQ)+UYQ*Y4(NQ)+UZQ*Z4(NQ)
 CSR=1./((XNP(NQ)*XNP(NR))+UZR*Z3(NR))
 UT=UXR*X3(NR)+UYR*Y3(NR)+UZR*Z3(NR)*CSR
 VT=((UXR*X4(NR)+UYR*Y4(NR)+UZR*Z4(NR))*Z3(NQ)
 XXR=((X3(NR)*X3(NQ)+Y3(NR)*Y3(NQ)+Z3(NR)*Z3(NQ))
 XYR=((X4(NR)*X4(NQ)+Y4(NR)*Y4(NQ)+Z4(NR)*Z4(NQ))
 UR=UT*XXR+VT*XYR
 YRF=((X3(NR)*X4(NQ)+Y3(NR)*Y4(NQ)+Z3(NR)*Z4(NQ))
 YR=((X4(NR)*X4(NQ)+Y4(NR)*Y4(NQ)+Z4(NR)*Z4(NQ))
 VR=UT*VXR+VT*VYR
 UU=UXU*X3(NQ)+UYU*Y3(NQ)+UZU*Z3(NQ)
 UUU=(XNP(NQ)*XNP(NU))+YNP(NQ)*YNP(NU)+ZNP(NQ)*ZNP(NU)
 VU=(UXU*X4(NQ)+UYU*Y4(NQ)+UZU*Z4(NQ))/CSU
 FIND RELATIVE COORDINATES OF NEIGHBORING QUADS.
 XD=XCP(NR)-X3(NQ)
 YD=YCP(NR)-Y3(NQ)
 ZD=ZCP(NR)-Z3(NQ)
 XT=XD*X3(NR)+YD*Y3(NR)+ZD*Z3(NR)
 YTT=XD*X4(NR)+YD*Y4(NR)+ZD*Z4(NR)
 ZT=XD*XNP(NR)+YD*YNP(NR)+ZD*ZNP(NR)
 YT=(-4.*SQRT(YTT**2+ZT**2))+YTT*CSR+YTT)*CSR*.16666667
 XR=XT*XXR+YT*XYR
 YF=XT*YXR+YT*YFR
 IF (IMRIF.LT.0) WRITF (JWRITF,NAMS)
 XD=XCP(NU)-XCP(NQ)
 YD=YCP(NU)-YCP(NQ)
 ZD=ZCP(NU)-ZCP(NQ)
 XU=XD*X3(NQ)+YD*Y3(NQ)+ZD*Z3(NQ)
 YU=XD*X4(NQ)+YD*Y4(NQ)+ZD*Z4(NQ)
 ZU=XD*XNP(NQ)+YD*YNP(NQ)+ZD*ZNP(NQ)
 YU=14.*SQRT(YU**2+ZU**2)+YU/CSU+YU)*.16666667
 FIND COEFFICIENTS OF VELOCITY FUNCTIONS
 DEN=1./((UR*UQ)+YU-(LU-UQ)*YR)*DFN
 UI=((UR-UQ)*YU-(LU-UQ)*YR)*DFN

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U2=--((UR-UQ)*XU-(UU-UQ)*XR)*DEN
V1=((VR-VQ)*YU-(VU-VQ)*YR)*DEN
V2=--((VR-VQ)*XU-(VU-VQ)*XR)*DEN
FIND VELOCITY AT STREAMLINE POINT
USL=UQ+U1*XLT+U2*YLT
VSL=VQ+V1*XLT+V2*YLT
UXP=USL*X3(NQ)+VSL*X4(NQ)
UYP=USL*Y3(NQ)+VSL*Y4(NQ)
UZP=USL*Z3(NQ)+VSL*Z4(NQ)
VSQD=USL**2+VSL**2
IF (IWRITE.LT.0) WRITE (JWRITE,NAM6)
DEN=VSQD*SQRT(VSQD)
FIND LOCAL STREAM FUNCTION
CXY=(U1*VQ**2-V2*UQ**2)/VSQD
CYY=U2-UQ*VQ*(U1+V2)/VSQD
CXX=U2-CYY-V1
CC=XLT*VQ-YLT*UQ-CXY*XLT-CYY*YLT**2-CXX*XLT**2
FIND STREAM FUNCTION AT CORNER POINTS
XCR(1)=XC1(NQ)
XCR(2)=XC2(NQ)
XCR(3)=XC3(NQ)
XCR(4)=XC4(NQ)
XCR(5)=XCR(1)
YCR(1)=YC1(NQ)
YCR(2)=YC2(NQ)
YCR(3)=YC3(NQ)
YCR(4)=YC4(NQ)
YCR(5)=YCR(1)
DO 20 N=1,4
20 SF(N)=CO-VQ*XCR(N)+UQ*YCR(N)+CXY*XCR(N)*YCR(N)+CYY*YCR(N)**2+CXX*X
1CR(N)**2
SF(5)=SF(1)
TEST=0.
IF (IWRITE.LT.0) WRITE (JWRITE,NAM7)
DO 23 N=1,4
IF (SF(N)*SF(N+1).GF.0.) GO TO 23
XM=(XCR(N)+XCR(N+1))*5
YM=(YCR(N)+YCR(N+1))*5
FIND INTERSECTION WITH SIDE OF QUAD.
SFM=CO-VQ*XM+UG*YM+CXY*XM*YM+CYY*YM**2+CXX*XM**2
AC=2.*(SF(N)-2.*SFM+SF(N+1))
BC=3.*SF(N)-4.*SFM+SF(N+1)

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IF (IWRITE.LT.0) WRITE (JWRITE,NAM8)
IF (AC.EQ.0) GO TO 21
SR=SQRT(BC**2-4.*AC*SF(N))
TP=(BC+SR)/(2.*AC)
IF (TP.LE.1.)AND.(TP.GE.0.) GO TO 22
TP=(RC-SR)/(2.*AC)
IF (TP.LE.1.)AND.(TP.GE.0.) GO TO 22
21 TP=SF(N)/BC
IF (TP.GT.1.)OR.(TP.LT.0.) GO TO 23
XNTP=(1.-TP)*XCR(N)+TP*XCR(N+1)
22 YNTP=(1.-TP)*YCR(N)+TP*YCR(N+1)
IF (IWRITE.LT.0) WRITE (JWRITE,NAM9)
TESTP=((XNTP-XLT)*UG+(YNTP-YLT)*VQ)*DIRT
IF (TESTP.LE.TEST) GO TO 23
TEST=TESTP
XNT=XNTP
YNT=YNTP
IF (IWRITE.LT.0) WRITE (JWRITE,NAM10)
23 CONTINUE
IF (TEST.EQ.0.) GO TO 34
AVERAGE LAST VELOCITY AND CURVATURE
UX=(UY+UXP)*AF
UY=(UZ+UZP)*AF
UZ=(UX**2+UY**2+UZ**2)
CP=1.-((UX**2+UY**2+UZ**2)/UABS(J)=SQRT(1.-CP)
IF (IWRITE.LT.0) WRITE (JWRITE,NAM11)
IF (J.GE.JSTOP) GO TO 35
C*** COMPUTE VELOCITY AT NEXT POINT
JL=J
J=J+JI
USL=UQ+XNT*U1+YNT*U2
VSL=VQ+XNT*V1+YNT*V2
UX=USL*X3(NQ)+VSL*X4(NQ)
UY=USL*Y3(NQ)+VSL*Y4(NQ)
UZ=USL*Z3(NQ)+VSL*Z4(NQ)
VSQD=USL**2+VSL**2
CCRD=SQRT((XNT-XLT)**2+(YNT-YLT)**2)*DIRT
STML(J)=STML(JL)+CORD
CF=1.-VSQD
UABS(J)=SQRT(1.-CF)

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AF=.5
LNQ=NO
IF (IWRITE.LT.C) WRITE (JWRITE,NAM12)
XL(J)=XNT*X3(NQ)+YNT*X4(NQ)+XCP(NQ)
YL(J)=XNT*Y3(NQ)+YNT*Y4(NQ)+YCP(NQ)
ZL(J)=XNT*Z3(NQ)+YNT*Z4(NQ)+ZCP(NQ)
IF (J.LE.MINJ.OR.J.GE.MAXJ) GO TO 54
C*** PROCEDURE FOR FINDING NEXT QUAD. WAS MODIFIED SO THAT, DEPENDING
C*** ON THE DIRECTION. THERE ARE ONLY 5 POSSIBLE QUADS. TO TEST
KMOD=MOD(NQ,2)
NTEST=5
IF (DIRT) 26,24,29
24 WRITE (JWRITE,25) DIRT
25 FORMAT (1H1,1X,7HDIRT = ,F10.7,26HPROGRAM TERMINATED IN PF5)
ICANCL=1
RETURN
26 IF (KMOD) 27,28,27
C*** LAST QUAD. IS ODD & WE ARE TESTING AGAINST THE STREAM DIRECTION
27 NQTEST(1)=NQ-2*(MM-1)+1
   NQTEST(2)=NQ+2
   NQTEST(3)=NQ-2
   NQTEST(4)=NQTEST(1)+2
   NQTEST(5)=NQTEST(1)-2
   IF (NQ.NE.NLIM1) GO TO 32
   NQTEST(2)=NQTEST(5)
   NTEST=3
   GO TO 32
C*** LAST QUAD. IS EVEN & WE ARE TESTING AGAINST THE STREAM DIRECTION
28 NQTEST(1)=NQ-1
   NQTEST(2)=NQ+2
   NQTEST(3)=NQ-2
   NQTEST(4)=NQ+1
   NQTEST(5)=NQ-3
   IF (NQ.GT.ILOWER) GO TO 32
   NQTEST(1)=NQTEST(2)
   NQTEST(2)=NQTEST(3)
   NTEST=2
   IF (NQ.EQ.2) NTEST=1
   GO TO 32
29 IF (KMOD) 30,31,30
C*** LAST QUAD IS ODD & WE ARE TESTING IN THE STREAM DIRECTION
30 NQTEST(1)=NQ+1

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NGTEST(2)=NQ+2
NGTEST(3)=NQ-2
NGTEST(4)=NQ+3
NGTEST(5)=NQ-1
IF (NQ.LT.IUPPER) GO TO 32
NTEST=2
NGTEST(1)=NGTEST(3)
IF (NQ.EQ.NLINM1)NTEST=1
GO TO 32
C** LAST QUAD IS EVEN & WE ARE TESTING IN THE STREAM DIRECTION
31 NGTEST(1)=NQ+2*(MM-1)-1
NGTEST(2)=NQ+2
NGTEST(3)=NQ-2
NGTEST(4)=NGTEST(1)+2
NGTEST(5)=NGTEST(1)-2
IF (NQ.NE.2) GO TO 32
NTEST=4
NGTEST(3)=NGTEST(5)
32 M=1
IF (IWRITE.LT.0) WRITE (JWRITE,NAM13)
33 I=NGTEST(M)
NG=I
TFST=(XL(J)-XCP(I))*2+(YL(J)-YCP(I))*2+(ZL(J)-ZCP(I))*2-DMX(I)
IF (TEST.GT.0.) GO TO 34
DS1=(XC1(I)-XC2(I))*2+(YC1(I)-YC2(I))*2
DS2=(XC2(I)-XC3(I))*2+(YC2(I)-YC3(I))*2
DS3=(XC3(I)-XC4(I))*2+(YC3(I)-YC4(I))*2
DS4=(XC4(I)-XC1(I))*2+(YC4(I)-YC1(I))*2
XLT=(XL(J)-XCP(I))*X3(I)+(YL(J)-YCP(I))*Y3(I)+(ZL(J)-ZCP(I))*Z3(I)
YLT=(XL(J)-XCP(I))*X4(I)+(YL(J)-YCP(I))*Y4(I)+(ZL(J)-ZCP(I))*Z4(I)
ZLT=(XL(J)-XCP(I))*XNP(I)+(YL(J)-YCP(I))*YNP(I)+(ZL(J)-ZCP(I))*ZNP(I)
1(I)
ZSQ=ZLT**2
IF (IWRITE.LT.0) WRITE (JWRITE,NAM14)
TEST=ZSQ-.1*DMX(I)
IF (TEST.GT.0.) GO TO 34
RC1=SQRT(ZSQ+(XLT-XC1(I))*2+(YLT-YC1(I))*2)
RC2=SQRT(ZSQ+(XLT-XC2(I))*2+(YLT-YC2(I))*2)
RC3=SQRT(ZSQ+(XLT-XC3(I))*2+(YLT-YC3(I))*2)
RC4=SQRT(ZSQ+(XLT-XC4(I))*2+(YLT-YC4(I))*2)
TEST=((RC1+RC2)**2)-DS1*1.3
IF (IWRITE.LT.0) WRITE (JWRITE,NAM15)

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IF (TEST.LT.0.) GC TO 14
TEST=((RC2+RC3)**2)-DS2*1.3
IF (IWRITE.LT.0) WRITE (JWRITE,NAM16)
IF (TEST.LT.0.) GO TO 14
TEST=((RC3+RC4)**2)-DS3*1.3
IF (IWRITE.LT.0) WRITE (JWRITE,NAM17)
IF (TEST.LT.0.) GO TO 14
TEST=((RC4+RC1)**2)-DS4*1.3
IF (IWRITE.LT.0) WRITE (JWRITE,NAM18)
MEM+1
34 IF (M.LE.NTEST) GO TO 33
35 IF (DIRT.GT.0.) GC TO 36
C** CHANGE THE DIRECTION IN WHICH THE STREAMLINE IS TRACED
DIRT=1.
JI=1
JMIN=J
IF (IWRITE.LT.0) WRITE (JWRITE,NAM19)
GO TO 13
36 JMAX=J
SSS=STML(JMIN)
DO 37 J=JMIN,JMAX
37 STML(J)=STML(J)-SSS
IF (IWRITE.LT.0) WRITE (JWRITE,NAM20)
IF ((STML(JMIN+3)-STML(JMIN)).LT.8.*(STML(JMIN+1)-STML(JMIN))) GO
1 TO 39
KEY=1
JJ=JMIN
KK=JMIN+1
JMIN=JMIN+1
IF (IWRITE.LT.0) WRITE (JWRITE,NAM21)
38 XL(KK)=(XL(JJ)+XL(KK))/2.0
YL(KK)=(YL(JJ)+YL(KK))/2.0
ZL(KK)=(ZL(JJ)+ZL(KK))/2.0
UABS(KK)=(UABS(JJ)+UABS(KK))/2.0
IF (IWRITE.LT.0) WRITE (JWRITE,NAM22)
IF (KEY.FO.1) GO TO 39
GO TO 40
39 IF ((STML(JMAX)-STML(JMAX-3)).LT.8.*(STML(JMAX)-STML(JMAX-1))) GO
1 TO 40
KEY=2
KK=JMAX-1

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JJ=JMAX
JMAX=JMAX-1
IF (IWRITE.LT.0) WRITE (JWRITE,NAM23)
GO TO 38
JMN=JMIN+1
JMX=JMAX-2
AF=1.
L=JMN
IF (IWRITE.LT.0) WRITE (JWRITE,NAM24)
IF (IWRITE.GT.1) GO TO 42
WRITE (JWRITE,41) NCP
FORMAT (//,37H0 LINE PASSING THROUGH QUADRILATERAL ,I4)
DO 46 J=JMN,JMX
  IF ((STML(J+2)-STML(L-1)).LT.8.*(STML(J+1)-STML(L))) GO TO 45
  IF (IWRITE.GT.1) GO TO 44
  WRITE (JWRITE,43) XL(L),YL(L),ZL(L),XL(J+1),YL(J+1),ZL(J+1)
  FORMAT (14H POINT DELETED,10X,3F12.5,10X,3F12.5)
  STML(L)=(AF*STML(L)+STML(J+1))/(AF+1.)
  XL(L)=(AF*XL(L)+XL(J+1))/(AF+1.)
  YL(L)=(AF*YL(L)+YL(J+1))/(AF+1.)
  ZL(L)=(AF*ZL(L)+ZL(J+1))/(AF+1.)
  UABS(L)=(AF*UABS(L)+UABS(J+1))/(AF+1.0)
  AF=AF+1.
  IF (IWRITE.LT.0) WRITE (JWRITE,NAM25)
  IF (L.LE.MID)MID=MID-1
  GO TO 46
45 AF=1.
  L=L+1
  K=J+1
  STML(L)=STML(K)
  XL(L)=XL(K)
  YL(L)=YL(K)
  ZL(L)=ZL(K)
  UABS(L)=UABS(K)
  IF (IWRITE.LT.0) WRITE (JWRITE,NAM26)
  GO TO 46
46 CONTINUE
  L=L+1
  STML(L)=STML(JMAX)
  XL(L)=XL(JMAX)
  YL(L)=YL(JMAX)
  ZL(L)=ZL(JMAX)
  UABS(L)=UABS(JMAX)
  
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IF (IWRITE.LT.0) WRITE (JWRITE,NAM27)
JMAX=L
IF (IWRITE.GT.1) GO TO 48
WRITE (JWRITE,47)
FORMAT (3H0 1.6X,1HX,9X,1HY,9X,1HZ,13X,2HCP,8X,2HSL,7X,4HUABS)
47 K=0
48 LOHO=0
LOGO=0
IF ((JMAX-JMIN).LE.4)LOGO=1
DO 51 I=JMIN,JMAX
K=K+1
VOV(K)=UABS(I)
SS(K)=STML(I)
IF (LOGO.EQ.0) GO TO 49
SSTEST=1000.0
IF (K.GT.1)SSTEST=(SS(K)-SS(K-1))
IF (SSTEST.LF.0.0)LOHO=LOHO+1
IF (IWRITE.GT.1) GO TO 51
49 WRITE POINTS,VELOCITIES,&CP'S FOR THE STREAMLINE POINTS CALCULATED
C***
CP=1.0-UABS(I)*2
WRITE (JWRITE,50) K,XL(I),YL(I),ZL(I),CP,STML(I),UABS(I)
50 FORMAT (1X,13,3F10.5,4X,3F10.5)
51 CONTINUE
IF (LOHO.GT.0) GO TO 52
CALL ROUTINE TO CALCULATE BOUNDARY LAYER OVER THE STREAMLINE
C***
CALL BLCNT(K,IWRITE)
IF (ICANCL.NE.0) RETURN
K2=(MID-JMIN)*K+1
HOLD THE DISPLACEMENT THICKNESS & THE WALL SHEAR VALUES AT THE
C***
CENTROID POINT FOR WHICH THE STREAMLINE WAS CALCULATED
C***
SKIN(LL)=CFI(K2)
DSTAR(LL)=DELS(K2)
HSK=SKIN(LL)
HDS=DSTAR(LL)
GC TO 56
52 SKIN(LL)=HSK
DSTAR(LL)=HDS
WRITE (JWRITE,53) LL
53 FORMAT (1X,7.2X,6SHVALUES OF WALL SHEAR AND DISPLACEMENT THICKNESS
1 AT QUADRILATERAL,13.40H WAS SET DUE TO STREAMLINE DIFFICULTIES..
1/)
GO TO 56

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54 WRITE (JWRITE,41) NCP
55 WRITE (JWRITE,55)
56 FORMAT (35H PROBABLE ERROR - LINE IS VERY LCNG)
57 GC TO 35
58 CONTINUE
59 IWRITE=IWRTS
60 IF (II-2) 57,61,59
61 JEND=NEND-1
62 ESTIMATE DSTAR & SKIN FOR TRIANGLES AT THE NOSE AND TAIL OF BODY
C** DO 58 J=1,JFND,2
63 DSTAR(J)=DSTAR(J+1)/3.0
64 SKIN(J)=SKIN(J+1)/3.0
65 GO TO 61
66 JSTART=NSTART+1
67 DO 60 J=JSTART,NLIN,2
68 DSTAR(J)=DSTAR(J-1)
69 SKIN(J)=SKIN(J-1)
70 CONTINUE
71 END OF LOOP ON PANEL CENTROIDS EXCEPT TRIANGLES
72 WRITE (JWRITE,62)
73 FORMAT (///,1X,56H SUMMARY OF BOUNDARY LAYER INFORMATION FOR QUADRI
74 LATERALS//2X,5HNQUAD,6X,1HX,9X,1HY,9X,1HZ,11X,5HDSTAR,5X,4H SKIN/)
75 CDF=0.0
76 AREA=0.0
77 WRITE POINTS,DSTAR,& SKIN FOR EACH CENTROID. COMPUTE FRICTION CO
78 DC 64 J=1,NLIN
79 IF (SKIN(J).GT.900.0) SKIN(J)=0.0
80 WRITE (JWRITE,63) J,XCP(J),YCP(J),ZCP(J),DSTAR(J),SKIN(J)
81 FCFRMT (4X,13,3F10.5,4X,2F10.5)
82 CDF=CDF-SKIN(J)*AQP(J)*VX1(J)/(0.5*VABS(J))
83 AREA=AREA+AGP(J)
84 CONTINUE
85 APEAAV=AREA/NLIN
86 CCFA=2.0*CDF
87 CDF=CCFA/REFA
88 WRITE (JWRITE,65) CDF,REFA,REBODY,STOTAL
89 FCFRMT (///,15X,25H FRICTION DRAG COEFFICIENT,/,13X,29(1H*),/17X,1
90 14H FRICTION CD = ,F11.5,/14X,17H REFERENCE AREA = ,F11.5,/13X,18H REY
91 1 INCLDS NUMBER = ,F11.4/17X,14H BODY LENGTH = ,F11.5/13X,29(1H*),///
92 1)
93 REWIND KFILE3
94 REWIND KFILE4

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```

REWRITE KFILES
SUMA=0.0
AVXCG=0.0
AVAREA=0.0
AVDELS=0.0
NDC=NLINE-2*MM+4
CALCULATE AVERAGE DSTAR, AVERAGE PANEL AREA, AND AVERAGE X-ORDINATE
FOR THE THIRD STATION OF INPUT POINTS FROM THE END OF BODY. THESE
QUANTITIES ARE USED TO CALCULATE THE WAKE-BODY COORDINATES.
DO 66 I=ND0,NLINE,2
AVXCG=AVXCG+XCP(I-1)*AQP(I-1)
AVDELS=AVDELS+DSTAR(I-1)*AQP(I-1)
AVAREA=AVAREA+AQP(I-1)
SUMA=SUMA+AQP(I)
AVDELS=AVDELS/AVAREA
AVXCG=AVXCG/AVAREA
SUMA=SUMA/(MM-1)
AREA=AV*SORT(AREA*SUMA)
DO 67 I=1,NLINE
XNH(I)=XNP(I)
ZNH(I)=ZNP(I)
AOPH(I)=AQP(I)
RETURN
66 WRITE (JWRITE,69) IS,NQ
69 FORMAT (14H TAPE 04 ERROR, 2I 4)
70 REWRITE KFILES
70 RETURN
END

```

BLC 1
BLC 2
BLC 3
BLC 4
BLC 5
BLC 6
BLC 7
BLC 8
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BLC 10
BLC 11

```

SUBROUTINE BLCONT(KNP,IWRITE)
BOUNDARY LAYER CONTROL ROUTINE WHICH CALLS LAMINR & TURB2, THE
LAMINAR AND TURBULENT ROUTINES WHICH USE MOMENTUM INTEGRAL METHOD
DIMENSION V(150),S(150),DUDS(150)
COMMON /BOUND/TAW(150),HMEAN(150),NP
COMMON /SPLN/VCOFF(4,75)
COMMON /BL/VOV(75),SS(75),VIN,VO,ROE,DELS(150),CFI(150),THT(150),
ISTOTAL,KKK
COMMON /INOUT/JREAD,JWRITE,KFILE,KFILE1,KFILE2,KFILE3,KFILE4,KFILE

```

```

15 COMMON /CANCEL/ICANCL,NODE
C
C***
C***
STRAN=.05
NP=KNP
SPLINE IS CALLED TO CURVE FIT THE STREAMLINE VALUES OF ABSOLUTE
VELOCITY VERSUS SURFACE DISTANCE FROM THE NCSE OF THE BODY
CALL SPLINE(NP,V0V,SS,0)
M=NP-1
SEND=SS(NP)
KKK=2
K=1
S(1)=SS(1)
V(1)=V0V(1)
DUDS(1)=VCDEF(3,1)
DO 1 I=1,M
H=(S(I+1)-SS(I))/KKK
DC 1 J=1,KKK
K=K+1
S(K)=S(K-1)+H
V(K)=(VCOFF(1,1)*S(K)+VCDEF(2,1))*S(K)+VCDEF(3,1)+VCDEF(4,1)
1)
DUDS(K)=(3.0D0*VCDEF(1,1)*S(K)+2.0D0*VCDEF(2,1))*S(K)+VCDEF(3,1)
NPP=KKK*(NP-1)+1
CONTINUE
DC 2 I=1,NPP
S(I)=S(I)/STOTAL
DUDS(I)=DUDS(I)*STOTAL
2)
CALL LAMINR(S,V,DUDS,STRAN,II,NPP,IWRITE)
IF (ICANCL.NE.0) RETURN
IF (I.EQ.NPP) GO TO 3
CALL TURB2(S,V,DUDS,SEND,II,NPP)
3)
WRITE (JWRITE,4)
4)
FORMAT (/,6X,1HS,13X,1HV,10X,4HDUDS,9X,5HHMEAN,8X,6HDELTA S,7X,6HTH
1FIAS,8X,3HTAW,9X,3HCFI/)
5)
DO 6 I=1,NPP
S(I)=S(I)*STOTAL
V(I)=V(I)*VINP
DUDS(I)=DUDS(I)*VINP/STOTAL
6)
DELS(I)=DELS(I)*STOTAL
IF (IWRITE.GT.1) RETURN

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```
HMEAN(II)=2.308
II=2
GO TO 3
2 II=II+1
H=X(II)-X(II-1)
GO TO 4
3 AMI=H*(-0.0652*D2UDX0/(DUDX0**2))
GO TO 5
4 AKD=Z*DUDX(II-1)
CALL FFK(AKD,FD,FID,F2D)
IF (ICANCL.NE.0) RETURN
AMI=H*FD/UDEL(II-1)
UDEL=0.5*(UDEL(II-1)+UDEL(II))
DUDXP=0.5*(DUDX(II-1)+DUDX(II))
AKD=(Z+AMI/2.0)*DUDXP
CALL FFK(AKD,FD,FID,F2D)
IF (ICANCL.NE.0) RETURN
AM2=H*FD/UDEL(II)
AKD=(Z+AM2/2.0)*DUDXP
CALL FFK(AKD,FD,FID,F2D)
IF (ICANCL.NE.0) RETURN
AM3=H*FD/UDEL(II)
AKD=(Z+AM3)*DUDX(II)
CALL FFK(AKD,FD,FID,F2D)
IF (ICANCL.NE.0) RETURN
AM4=H*FD/UDEL(II)
Z=(AMI+2.0*AM2+2.0*AM3+AM4)/6.0
AKD=Z*DUDX(II)
CALL FFK(AKD,FD,FID,F2D)
IF (ICANCL.NE.0) RETURN
THT(II)=SORT(Z*VO/(VIN*STOTAL))
DELS(II)=THT(II)*FID
CFI(II)=2.0*F2D*UDEL(II)/(THT(II)*VIN*STOTAL/VO)
TAW(II)=CFI(II)*0.5*ROE*VIN*VIN*VIN
HMEAN(II)=DELS(II)/THT(II)
IF (TAW(II).LT.0.0) GO TO 8
IF (X(II).GE.XTRAN) GO TO 6
IF (II.EQ.NPP) GO TO 6
GO TO 2
6 IF (IMWRITE.GT.1) RETURN
WRITE (JWRITE,7) X(II),II
7 FORMAT (/IX,18HTTRANSITION AT X = .F10.5.17H FOR STEP NUMBER ,I3)
```


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      RETURN
      IF (IWRITE.GT.1) RETURN
      IK=II/KKK
      WRITE (JWRITE,9) TA(II),IK
      FORMAT (/,27H NEGATIVE VALUE OF TAWST = ,E14.7,21H AT OR AFTER STA
      TION ,I3.19H ON THE STREAMLINE.,38H FOR MORE INFORMATION ON THE LO
      CATION,/,108H OF LAMINAR SEPARATION USE IWRITE = 0 PRINT OPTION. T
      HE TURBULENT ROUTINE IS CALLED AT THE SEPARATION POINT.)
      RETURN
      END
  
```

LAM 76
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```

SUBROUTINE FFK(AKD,FD,FID,F2D)
C***
C  ROUTINE FOR NUMERICAL INTERPOLATION OF LAMINAR B.L. FUNCTIONS
C
      DIMENSION AK(55),F(55),F1(55),F2(55)
      COMMON /INOUT/JREAD,JWRITE,KFILE,KFILE1,KFILE2,KFILE3,KFILE4,KFILE
      15
      COMMON /CANCEL/ICANCEL,NODE
      DATA AK/0.094815,0.094632,0.094083,0.093166,0.091882,0.090234,0.08
      1823,0.085855,0.083134,0.080068,0.076664,0.072930,0.068877,0.06451
      16,0.059857,0.054912,0.049697,0.044223,0.038506,0.032562,0.026405,0
      1,0.20054,0.013524,0.006833,0.000000,-0.006957,-0.014321,-0.021170,-
      10,0.28387,-0.035651,-0.042943,-0.050244,-0.057532,-0.064789,-0.0719
      195,-0.079129,-0.086171,-0.093104,-0.099906,-0.106558,-0.113043,-0.
      1119341,-0.124434,-0.131304,-0.136935,-0.142309,-0.147411,-0.152224
      11,-0.156735,-0.160927,-0.164789,-0.168307,-0.171470,-0.174267,-0.17
      16687/
      DATA F/-0.094815,-0.093915,-0.091177,-0.086542,-0.079963,-0.071400
      1,-0.060818,-0.048195,-0.033512,-0.016759,0.002068,0.022964,0.04591
      19,0.070916,0.097532,0.126938,0.157897,0.190770,0.225538,0.262060,0
      1,300369,0.340371,0.391999,0.425181,0.469841,0.515896,0.563264,0.61
      11853,0.661571,0.712321,0.764004,0.816516,0.869752,0.923601,0.97795
      12,1.032691,1.087700,1.142862,1.198055,1.253157,1.308043,1.362589,1
      1,416665,1.470145,1.522902,1.574802,1.625719,1.675522,1.724079,1.77
      11259,1.816936,1.860975,1.903251,1.943633,1.981994/
      DATA F1/2.250000,2.250686,2.252684,2.255924,2.260349,2.265904,2.27
      12545,2.280231,2.288928,2.298609,2.309248,2.320828,2.333333,2.34675
      11,2.361073,2.376291,2.392406,2.409414,2.427320,2.446130,2.465849,2
      1,486485,2.508057,2.530574,2.554053,2.578518,2.603995,2.630480,2.65
  
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FFK 1
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18031.2.686666.2.716418.2.747321.2.779412.2.812734.2.847327.2.88324
12.2.920529.2.959246.2.999447.3.041200.3.084570.3.129634.3.176471.3
1.225166.3.275810.3.328505.3.383357.3.440479.3.499999.3.562056.3.62
16788.3.694360.3.764940.3.838720.3.915905/
DATA F2/0.355556.0.355293.0.354515.0.353236.0.351470.0.349229.0.34
16528.0.343380.0.339800.0.335801.0.331397.0.326601.0.321428.0.31589
12.0.310005.0.303782.0.297237.0.290383.0.283234.0.275804.0.268107.0
1.260156.0.251966.0.243549.0.234921.0.226093.0.217082.0.207899.0.19
18559.0.189077.0.179464.0.169736.0.159906.0.149987.0.139995.0.12994
11.0.119841.0.109708.0.099555.0.089397.0.079247.0.069120.0.059028.0
1.048985.0.039007.0.029105.0.019294.0.009588.0.000000.0.009455.0.
1018765.-0.027914.-0.036890.-0.045678.-0.054266/

```

C
IF (AKD.LE.AK(1)) GO TO 1
FD=F(1)
F1D=F1(1)
F2D=F2(1)
AKD=AK(1)
RETURN
1 IF (AKD.GT.AK(55)) GO TO 2
FD=F(55)
F1D=F1(55)
F2D=F2(55)
AKD=AK(55)
RETURN
2 DC 3 I=1.54
IF (AKD.LE.AK(I).AND.AK.GT.AK(I+1)) GO TO 5
3 CCNTINUE
WRITE (JWRITE,4) AKD
4 FORMAT (IX,6HAKD = .E12.5,22H EXCEEDS ALLOWED RANGE)
ICANCL=1
RETURN
5 FD=F(I)+(F(I+1)-F(I))*(AKD-AK(I))/(AK(I+1)-AK(I))
F1D=F1(I)+(F1(I+1)-F1(I))*(AKD-AK(I))/(AK(I+1)-AK(I))
F2D=F2(I)+(F2(I+1)-F2(I))*(AKD-AK(I))/(AK(I+1)-AK(I))
RETURN
END

```

TRB 1
TRB 2

SUBROUTINE TURB2(SUMS,UE,DUE DX,SEND,N1,NPP)

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C** ROUTINE FOR TURBULENT BOUNDARY LAYER USING MCMENTUM INTEGRAL
C
C** COMMON /BOUND/TAW(150),HMEAN(150),NP
COMMON /BL/VOV(75),SS(75),VINP,VO,ROE,DELS(150),CFI(150),THT(150),
1STOTAL,KKK
C** DIMENSION HVMEAN(2),SUMS(150),UE(150),DUEDX(150)
C
DC 1 L=N1,NPP
DUEDX(L)=VINP*DUEDX(L)/STOTAL
SUMS(L)=SUMS(L)+STOTAL
UE(L)=VINP*UE(L)
THT(N1)=THT(N1)+STOTAL
DELS(N1)=1.45*THT(N1)
C1=0.56
C2=.1667
C3=1.65
C4=0.246
C5=0.678
C6=0.268
HMEAN(N1)=1.45
HVMEAN(1)=1.269*HMEAN(N1)/(HMEAN(N1)-.379)
F1=3.+2.*C2
E2=1.+C2
E3=3.+3.*C2
T1=0.02*C1/C3*E2
IREG=N1+1
DO 7 I=IBFG,NPP
HMEAN(I)=0.0
HVMEAN(2)=0.0
UETR=(UE(I-1))/UE(I)**E3
UEINT=0.5*(SUMS(I)-SUMS(I-1))+F2*UFTR+T1*VO**C2/(UE(I)**E3)*UEINT)**(1./E2)
THT(I)=(THT(I-1)**F2*UFTR+T1*VO**C2/(UE(I)**E3)*UEINT)**(1./E2)
YERMA=(0.02*C1)/(UE(I)*THT(I))/VO**C2*1.1
T2=THT(I)/UE(I)*DUEDX(I)
HV=HVMEAN(I-1)
DO 6 J=1,6
TERMB=-HV*C4*10.0**(-C5*HH)*(UE(I)*THT(I)/VO)**(-C6)
TERMB=TERMB/2.
TERMC=(HH-1.01)*HV*T2
PHVDX=(TERMA+TERMB+TERMC)/THT(I-1)
HVI TR=HVMEAN(1)+DHVDX*(SUMS(I)-SUMS(I-1))

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69 TRB

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IF (HVITR-1.85) 3.2.2
HVITR=1.85
IF (HVITR-1.55) 4.4.5
HVITR=1.55
HITR=0.379*HVITR/(HVITR-1.269)
HVMEAN(2)=HVMEAN(2)+HVITR
HMEAN(1)=HMEAN(1)+HITR
HV=HVITR
H=HITR
HVMEAN(1)=HVMEAN(2)/6
HMFAN(1)=HMEAN(1)/6
DELS(I)=THI(I)*HMEAN(1)
CFI(I)=C4*10.0**(-C5*HMFAN(1))*(UE(I)*THI(I)/VO)**(-C6)*(UE(I)/VIN
1F)**2
TAM(I)=CFI(I)*0.5*ROE*VIN*VINF
IF (SFND-SUMS(I)) 8.8.7
7 CCNTINUE
8 DO 9 L=NI,NP
DELS(L)=DELS(L)/STOTAL
THI(L)=THI(L)/STOTAL
DUEX(L)=DUEX(L)*STOTAL/VINF
SUMS(L)=SUMS(L)/STOTAL
9 UE(L)=UE(L)/VINF
RETURN
END

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SUBROUTINE RGVRTX(XC,YC,ZC,X0,Y0,Z0,RD,NTHETA,THEIA,PHI,NVPHI,NRS,
INSRV,VX,VY,VZ,IM,NPTS)
C***
C*** SUBROUTINE RGVRTX CALCULATES THE INDUCED VELOCITIES DUE TO THE
C*** RING VORTICES
C
DIMENSION XC(40),YC(40),ZC(40),RD(40),NTHETA(40),THEIA(40),PHI(40)
1,NVPHI(40),NRS(40),UC(360),VC(360),TX(360),NPTS(40)
C
C*** DEFINE INITIAL PARAMETERS
PI=3.1415927
C=1.0/(4.0*PI)
VXX=0.0
VYY=0.0

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```

C***
VZZ=0.0
SET UP LOOP OVER SYSTEMS OF VORTICES
DO 8 L=1,NSRV
  TINC=2.0*PI/FLOAT(NTHETA(L))-1)
  NR=NRS(L)
  ISFE=0
  IF (NPTS(L).EQ.0.AND.NRS(L).EQ.1) ISEE=1
DC 7 M=1, NR
DETERMINE RADIAL STATION AND CIRCULATION
IF (ISEE.EQ.0) GO TO 1
GAMMA=CIRC(L)
R=RD(L)
DR=R
GO TO 2
1 R=F(NR,M,RD(L),DR)
  XR=R/RD(L)
  GAMMA=G(L,XR)
  T=THETA(L)
  PHX=PHI(L)
  NTH=THETA(L)
C***
TEST FOR FLOW SIMPLICATION BY DOUBLET
TEST=SQRT((X0-XC(L))**2+(Y0-YC(L))**2+(Z0-ZC(L))**2)
FACTOP=1.5
DISX=FACTOR*(2.0*RD(L))
IF (TEST.LT.DISX) GO TO 3
FACX=0.00932
CALCULATE DOUBLET STRENGTH AND FLOW
GAM=FACX*GAMMA**2
CALL DBLET(NVPHI,R,T,PHX,GAM,L,X0,Y0,Z0,XC,YC,ZC,VX,VY,VZ)
IM=1
GO TO 6
3 DC 5 I=1,NTH
  DEFINE PARAMETRIC EQNS FOR POINT ON VORTEX RING
  XI=XC(L)+R*SIN(T)*COS(PHX)
  ETA=YC(L)+R*SIN(T)*SIN(PHX)
  ZETA=ZC(L)+R*COS(T)
  DEFINE DERIVATIVES OF PARAMETRIC EQNS WRT T
  DXI=R*COS(T)*COS(PHX)
  DETA=R*COS(T)*SIN(PHX)
  DZETA=-R*SIN(T)
  INITIALIZE OR DEFINE PARAMETER
  TX(I)=T

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UC(I)=0.0
VC(I)=0.0
WC(I)=0.0
C**  CCMPUTE DISTANCE FROM FILAMENT TO ARBITRARY PCINT
RHO=SQRT((XI-XO)**2+(ETA-YO)**2+(ZETA-ZO)**2)
IF (RHO.LE.1.0E-10) GO TO 4
C**  COMPUTE VELOCITY CONTRIBUTIONS AROUND THE RING VORTEX UPON AN
C**  ARBITRARY POINT
DENOM=RHO**3*RD(L)/(C*DR)
UC(I)=(DELTA*(ZO-ZETA)-DZETA*(YO-ETA))/DENOM*GAMMA
VC(I)=(DELTA*(XO-XI)-DXI*(ZO-ZETA))/DENOM*GAMMA
WC(I)=(DXI*(YO-ETA)-DELTA*(XO-XI))/DENOM*GAMMA
4 IF (I.EQ.NTH) GO TO 5
T=T+TINC
IF (NVPHI(L).NE.0)PHX=PHX+TINC
5 CONTINUE
C**  INTEGRATE TO FIND VX, VY, VZ
IM=0
CALL TRAP(NTH,IX,UC,VX)
CALL TRAP(NTH,IX,VC,VY)
CALL TRAP(NTH,IX,WC,VZ)
6 VXX=VXX+VX
VYY=VYY+VY
VZZ=VZZ+VZ
7 CONTINUE
8 CCNTINF TOTAL INDUCED VELOCITY COMPONENTS
C**  VX=VXX
VY=VYY
VZ=VZZ
MODIFY, IF NECESSARY, FOR PRECISION PROBLEMS
C**  VMX=ABS(VX)
VMY=ABS(VY)
VMZ=ABS(VZ)
IF (ABS(VY).GT.VMX)VMX=ABS(VY)
IF (ABS(VZ).GT.VMX)VMX=ABS(VZ)
FVMX=1.0E-4*VMX
IF (ABS(VX).LT.FVMX)VX=0.0
IF (ABS(VY).LT.FVMX)VY=0.0
IF (ABS(VZ).LT.FVMX)VZ=0.0
RETURN
END

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C*** FUNCTION F(N,M,R,RD)
C
C
FUNCTION F(N,M,R,RD)
FUNCTION F CALCULATES THE RADIAL STATION OF THE VORTEX RING
RD=R/FLJAT(N)
RX=R+RD
DO 1 I=1,M
RX=RX-RD
F=RX
RETURN
END
1

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C*** FUNCTION G(L,R)
C
C
FUNCTION G(L,R)
FUNCTION G COMPUTES THE CIRCULATION AS A FUNCTION OF RADIAL
DISTANCE FROM THE VORTEX'S CENTER
CALL GAMMA(L,R,B)
G=B
RETURN
END

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C*** FUNCTION CIRC(L)
C
C
FUNCTION CIRC(L)
FUNCTION CIRC SETS THE VORTEX STRENGTH
COMMON /S2V/CIRCV(40)
CIRC=CIRCV(L)
RETURN
END

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SPN
SPN

```

C*** SUBROUTINE SPLINE(N,Y,X,IC)
C
C
SUBROUTINE SPLINE(N,Y,X,IC)
THIS SUBROUTINE PERFORMS A SPLINE FIT ON THE TABULATED

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D=3.0*((YP-YY)/HH-(YY-YM)/HM)/(HH+HM)
C=0.5*HH/(HH+HM)
A=0.5-C
P=A*(I-1)+1.0
Q(I)=-C/P
U(I)=(D-A*U(I-1))/P
M=HH
YM=YY
3 YY=YP
*** MODIFIED RIGHT HAND END CONDITION THAT ALLEVIATES THE NEED
*** TO SPECIFY THE X-DERIVATIVE OF Y AT POINT N
C***
A=31.0/32.0
P=A*Q(N-1)+1.0
H1=H(NM1)
H2=H(NM1-1)
H3=H(NM1-2)
D=Y(N)*(32.0*H1+42.0*H2+21.0*H3)/(H1+H2)/(H1+H2+H3)-Y(NM1)*(11.0*H
1+42.0*H2+21.0*H3)/(H2+H3)/H2+Y(NM1-1)*H1*(11.0*H1+21.0*(H2+H3))/(
1H1+H2)/H2/H3-Y(NM1-2)*H1*(11.0*H1+21.0*H2)/(H2+H3)/(H1+H2+H3)/H3
D=3.0*D/H1/16.0
U(N)=(D-A*U(N-1))/P
SOLVE FOR THE SPLINE COEFFICIENTS CORRESPONDING TO AHLBERG'S
M(0) TO M(N) AND STORE THEM IN THE U(I).
DO 4 J=1,NM1
I=N-J
4 U(I)=Q(I)*U(I+1)+U(I)
C*** FORM THE AA(J,I) COEFFICIENTS FOR THE CONVENTIONAL FORM OF
C*** A CUBIC POLYNOMIAL FROM THE U(I)
UU=U(I)
XX=X(I)
YY=Y(I)
DO 5 I=1,NM1
UP=U(I+1)
XP=X(I+1)
YP=Y(I+1)
HM=H(I)
AA(1,I)=(UP-UU)/HH/6.0
AA(2,I)=0.5*(XP*UU-XX*UP)/HH
AA(3,I)=0.5*(UP*XX*XP-UU*XP*XP)/HH+(UU-UP)*HH/6.0+(UP*XP-
AA(4,I)=(UU*XP*XP-UP*XX*XX)/HH/6.0+(UF*XX-UU*XP)*HH/6.0+(YY*
1 XP-YP*XX)/HH
XX=XP

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UU=UP
5 YY=YP
  IF (IC.EQ.0) GO TO 7
  DO 6 I=1,NM1
  DO 6 J=1,4
 6 CF(IC,J,I)=AA(J,I)
 7 RETURN

C
  ENTRY GAMMA(IC,T,Z)
  IF (T.GT.X(1)) GO TO 8
  I=1
  GO TO 10
 8 DO 9 I=1,NM1
  IF (X(I).LE.T.AND.X(I+1).GT.T) GO TO 10
 9 CCNTINUE
  I=NM1
 10 Z=((CF(IC,1,I)+T+CF(IC,2,I))+T+CF(IC,3,I))+T+CF(IC,4,I)
  RETURN
  FND

```

```

SUBROUTINE TRAP(ND,X,DY,Y)
C*** SUBROUTINE TRAP PERFORMS TRAPEZOIDAL INTEGRATION
C
C
C DIMENSION X(ND),DY(ND)
C
C INITIALIZE PARAMETER
S2=0.0
IF (ND-1) 4,3,1
C INTEGRATE OVER INTERVAL AND SUM
C*** 1 DC 2 I=2,ND
  S1=S2
  S2=S2+.5*(X(I)-X(I-1))*(Y(I)+DY(I-1))
 2 CCNTINUE
 3 YES2
 4 RETURN
  END

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SUBROUTINE DBLET(N,R,T,PHX,GAM,L,X0,Y0,Z0,XC,YC,ZC,VX,VY,VZ)
SUBROUTINE DBLET CALCULATES DOUBLET FLOW
DIMENSION N(40),XC(40),YC(40),ZC(40)
PI=3.1415927
DETERMINE DOUBLET AXIS VECTOR
X1=R*SIN(T)*COS(PHX)
Y1=R*SIN(T)*SIN(PHX)
Z1=R*COS(T)
PI2=0.5*PI
X2=R*SIN(T+PI2)*COS(PHX+N(L)*PI2)
Y2=R*SIN(T+PI2)*SIN(PHX+N(L)*PI2)
Z2=R*COS(T+PI2)
X3=Y1*Z2-Z1*Y2
Y3=X1*Y2-Y1*X2
RD=SQRT(X3**2+Y3**2+Z3**2)
X3=X3/RD
Y3=Y3/RD
Z3=Z3/RD
DETERMINE DOUBLET STRENGTH VECTOR COMPONENTS
XMU=GAM*X3
YMU=GAM*Y3
ZMU=GAM*Z3
PI4=-0.5*PI2
DETERMINE DOUBLET-TO-ARBITRARY POINT VECTOR
X1=X0-XC(L)
Y1=Y0-YC(L)
Z1=Z0-ZC(L)
DETERMINE VELOCITY COMPONENTS
RD=X1**2+Y1**2+Z1**2
F=PI4/RD**1.5
VX=F*XMU*(1.0-3.0*X1**2/RD)
VY=F*YMU*(1.0-3.0*Y1**2/RD)
VZ=F*ZMU*(1.0-3.0*Z1**2/RD)
RETURN
END

```

```

1 SUBROUTINE SPACE(NSRV, SVV, XCV, NMIN, NMAX, X, MMAX, XCRP, AEXP, XRM, ISPC)
2 1E, FXMR, XMR)
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40 SPC

C*** SUBROUTINE SPACE CALCULATES VORTEX LOCATION VIA EXPONENTIAL
C*** FUNCTION
C
C DIMENSION SVV(31,2), XCV(40), X(650), XCRP(2), AEXP(2)
C
C MAX=(NMAX-1)*(MMAX-1)
C NMAXMI=NMAX-1
C JV=1
C SET MAXIMUM RADIUS
C RMX=RXMR
C 1 JV=JV+1
C*** GUESS A LOCATION
C J=1
C IF (XCV(JV-1), LT, XMR) J=2
C XCV(JV)=XCV(JV-1)-XCRP(J)
C LPT=1
C SCAN N-STATIONS
C DO 2 JN=NMIN, NMAXMI
C LC1=JN
C LC2=JN+1
C IF (XCV(JV), LE, X(LPT), AND, XCV(JV), GE, X(LPT+MMAX)) GO TO 3
C 2 LPT=LPT+MMAX
C IF (ISPACE.EQ.2) GO TO 4
C JV=JV-1
C GO TO 5
C*** COMPUTE EXPONENTIAL LOCATION
C RXTL=(X(LPT)-XCV(JV))/(X(LPT)-X(LPT+MMAX))
C R=SVV(LC1,2)+RXTL*(SVV(LC2,2)-SVV(LC1,2))
C XCV(JV)=XCV(JV-1)-XCRP(J)*EXP(-AEXP(J))*(R-RMX)/RMX
C IF (XCV(JV), LE, X(MAX), AND, ISPACE.EQ.1 .OR. JV.EQ.40) GO TO 5
C GO TO 1
C 4 R=0.0
C XCV(JV)=XCV(JV-1)-XCRP(J)*EXP(-AEXP(J))*(R-RMX)/RMX
C IF (XCV(JV), GT, XRM, AND, JV.LT.40) GO TO 1
C 5 NSRV=JV
C RETURN
C END

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12.2085000	0.0000000	-0.4271002	1	10	1
12.2085000	0.0000000	-0.4271002	1	11	1
12.2085000	0.0000000	-0.4271002	1	12	1
12.2085000	0.0000000	-0.4271002	1	13	1
12.2085000	0.0000000	-0.4271002	1	14	1
12.2085000	0.0000000	-0.4271002	1	15	1
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12.2085000	0.0000000	-0.4271002	1	17	1
12.2085000	0.0000000	-0.4271002	1	18	1
12.2085000	0.0000000	-0.4271002	1	19	1
12.2085000	0.0000000	-0.4271002	1	20	1
12.2085000	0.0000000	-0.4271002	1	21	1
11.5418000	0.0000000	-1.6353990	1	2	1
11.5418000	0.1833000	-1.5978990	1	3	1
11.5418000	0.3583000	-1.5430990	1	4	1
11.5418000	0.5146000	-1.5439990	1	5	1
11.5418000	0.6708000	-1.2520990	1	6	1
11.5418000	0.8197000	-1.1270990	1	7	1
11.5418000	0.9686000	-0.9958000	1	8	1
11.5418000	1.1083000	-0.8436995	1	9	1
11.5418000	1.2645995	-0.6520995	1	10	1
11.5418000	1.4083000	-0.4271002	1	11	1
11.5418000	1.5160990	-0.1854000	1	12	1
11.5418000	1.5707990	0.0723998	1	13	1
11.5418000	1.5625000	0.3223994	1	14	1
11.5418000	1.4917000	0.5229000	1	15	1
11.5418000	1.3291990	0.6729002	1	16	1
11.5418000	1.1062000	0.7506502	1	17	1
11.5418000	0.8933000	0.7708998	1	18	1
11.5418000	0.6667000	0.7771000	1	19	1
11.5418000	0.4437000	0.7513005	1	20	1
11.5418000	0.2167000	0.7813005	1	21	1
11.5418000	0.0000000	-1.9271000	1	22	1
11.3755000	0.6520995	-1.9229000	1	23	1
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-5.1344990	0.8958000	0.9593000	26	25	1
-5.1344990	0.8958000	0.9593000	26	26	1
-5.1344990	0.8958000	0.9593000	26	27	1
-5.1344990	0.8958000	0.9593000	26	28	1
-5.1344990	0.8958000	0.9593000	26	29	1
-5.1344990	0.8958000	0.9593000	26	30	1
-5.1344990	0.8958000	0.9593000	26	31	1
-5.1344990	0.8958000	0.9593000	26	32	1
-5.1344990	0.8958000	0.9593000	26	33	1
-5.1344990	0.8958000	0.9593000	26	34	1
-5.1344990	0.8958000	0.9593000	26	35	1
-5.1344990	0.8958000	0.9593000	26	36	1
-5.1344990	0.8958000	0.9593000	26	37	1
-5.1344990	0.8958000	0.9593000	26	38	1
-5.1344990	0.8958000	0.9593000	26	39	1
-5.1344990	0.8958000	0.9593000	26	40	1
-5.1344990	0.8958000	0.9593000	26	41	1
-5.1344990	0.8958000	0.9593000	26	42	1
-5.1344990	0.8958000	0.9593000	26	43	1
-5.1344990	0.8958000	0.9593000	26	44	1
-5.1344990	0.8958000	0.9593000	26	45	1
-5.1344990	0.8958000	0.9593000	26	46	1
-5.1344990	0.8958000	0.9593000	26	47	1
-5.1344990	0.8958000	0.9593000	26	48	1
-5.1344990	0.8958000	0.9593000	26	49	1
-5.1344990	0.8958000	0.9593000	26	50	1
-5.1344990	0.8958000	0.9593000	26	51	1
-5.1344990	0.8958000	0.9593000	26	52	1
-5.1344990	0.8958000	0.9593000	26	53	1
-5.1344990	0.8958000	0.9593000	26	54	1
-5.1344990	0.8958000	0.9593000	26	55	1
-5.1344990	0.8958000	0.9593000	26	56	1
-5.1344990	0.8958000	0.9593000	26	57	1
-5.1344990	0.8958000	0.9593000	26	58	1
-5.1344990	0.8958000	0.9593000	26	59	1
-5.1344990	0.8958000	0.9593000	26	60	1
-5.1344990	0.8958000	0.9593000	26	61	1
-5.1344990	0.8958000	0.9593000	26	62	1
-5.1344990	0.8958000	0.9593000	26	63	1
-5.1344990	0.8958000	0.9593000	26	64	1
-5.1344990	0.8958000	0.9593000	26	65	1
-5.1344990	0.8958000	0.9593000	26	66	1
-5.1344990	0.8958000	0.9593000	26	67	1
-5.1344990	0.8958000	0.9593000	26	68	1
-5.1344990	0.8958000	0.9593000	26	69	1
-5.1344990	0.8958000	0.9593000	26	70	1
-5.1344990	0.8958000	0.9593000	26	71	1
-5.1344990	0.8958000	0.9593000	26	72	1
-5.1344990	0.8958000	0.9593000	26	73	1
-5.1344990	0.8958000	0.9593000	26	74	1
-5.1344990	0.8958000	0.9593000	26	75	1
-5.1344990	0.8958000	0.9593000	26	76	1
-5.1344990	0.8958000	0.9593000	26	77	1
-5.1344990	0.8958000	0.9593000	26	78	1
-5.1344990	0.8958000	0.9593000	26	79	1
-5.1344990	0.8958000	0.9593000	26	80	1
-5.1344990	0.8958000	0.9593000	26	81	1
-5.1344990	0.8958000	0.9593000	26	82	1
-5.1344990	0.8958000	0.9593000	26	83	1
-5.1344990	0.8958000	0.9593000	26	84	1
-5.1344990	0.8958000	0.9593000	26	85	1
-5.1344990	0.8958000	0.9593000	26	86	1
-5.1344990	0.8958000	0.9593000	26	87	1
-5.1344990	0.8958000	0.9593000	26	88	1
-5.1344990	0.8958000	0.9593000	26	89	1
-5.1344990	0.8958000	0.9593000	26	90	1
-5.1344990	0.8958000	0.9593000	26	91	1
-5.1344990	0.8958000	0.9593000	26	92	1
-5.1344990	0.8958000	0.9593000	26	93	1
-5.1344990	0.8958000	0.9593000	26	94	1
-5.1344990	0.8958000	0.9593000	26	95	1
-5.1344990	0.8958000	0.9593000	26	96	1
-5.1344990	0.8958000	0.9593000	26	97	1
-5.1344990	0.8958000	0.9593000	26	98	1
-5.1344990	0.8958000	0.9593000	26	99	1
-5.1344990	0.8958000	0.9593000	26	100	1

ORIGINAL PAGE IS
OF POOR QUALITY

SAMPLE OUTPUT - FLOWBODY

NEW FLOWBODY PROGRAM: POTENTIAL FLOW + BOUNDARY LAYER + NONUNIFORM SLIPSTREAM FLOW + INTERIOR FLOW

REST CASES 100 WITH NEW; AND NEW VIERING 000 PANELS -- FUELBODY ONLY

NO. OF QUADS = 000
NO. OF SECTIONS = 1
NO. OF ITERATIONS = 100

VIMP = 0.100000E+02 VU = 0.100000E+02 RDE = 0.257000E+02 DEPL = 0.170000E+03 MIP = -0.100000E+01
SDC = 0.200000E+00 DEP = 0.700000E+00 CRW = 0.200000E+00 TWP = 0.200000E+00 LDA = 0.500000E+00
INITE = 0 INCH = 0 INCH = 0 INCH = 0 INCH = 0 INCH = 0 INCH = 0 INCH = 0 INCH = 0 INCH = 0 INCH = 0 INCH = 0
COORDINATE CONVERSION FACTOR: 1.000000

1 PLANE OF SYMMETRY
CONVERGENCE CRITERIA: 0.00010

1 VORTEX SYSTEM(S) SPECIFIED

SPACE 2
XMP(1) 0.00000 XMP(2) 0.00000
XMP(1) 0.00000 XMP(2) 0.00000

FOR VORTEX SYSTEM 1
XCV = 12.00000 YCV = 0.0 ZCV = -0.00710
RHO = 2.50000 CPO = 0.0 SWR = 0.00000
XW = 100 YW = 0 ZW = 0
GW = 0.100000000E+00

SECTION 1

NON-CENTERLINE DIRECTION COSINES: -0.9990, 0.0, 0.0210

COVERING INCREASED VELOCITY = 0.00000000E+00

PATCHING OF AIRSTREAM FROM TO DEVELOPED ENGINE POWERPLANT REQUIRED GREAT TO BE 0.00000000E+00 TIMES THE ORIGINAL.

RING VORTEX INFORMATION:

NUMBER	X	Y	Z	RADIUS	CIRCULATION
1	12.00000	0.0	-0.00470	2.50000	0.4100720
2	0.01100	0.0	-0.20070	2.10000	0.0002270
3	0.11007	0.0	-0.20007	2.00000	0.3000001
4	0.70000	0.0	-0.20000	2.00000	0.0110000
5	-0.11000	0.0	-0.10000	2.00000	0.0110000
6	-0.01100	0.0	-0.20000	2.00000	0.0110000
7	-0.00700	0.0	-0.20000	2.00000	0.0110000
8	-0.00700	0.0	-0.10000	2.00000	0.0110000
9	-0.00700	0.0	-0.10000	2.00000	0.0110000
10	-0.00700	0.0	-0.20000	2.00000	0.0110000

0	01	02	03	04	05	06	07	08	09	10
X	X1	X2	X3	X4	X5	X6	X7	X8	X9	X10
Y	Y1	Y2	Y3	Y4	Y5	Y6	Y7	Y8	Y9	Y10
Z	Z1	Z2	Z3	Z4	Z5	Z6	Z7	Z8	Z9	Z10

QUESTIONABLE POINT - FROM PIT 0.0100E+00
WARNING LONG THIS QUAD:
1 0.11000E+02 0.11000E+02 0.11000E+02 0.11000E+02 0.11000E+02 0.11000E+02 0.11000E+02 0.11000E+02 0.11000E+02 0.11000E+02
2 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
3 -0.00000E+00 -0.00000E+00 -0.00000E+00 -0.00000E+00 -0.00000E+00 -0.00000E+00 -0.00000E+00 -0.00000E+00 -0.00000E+00 -0.00000E+00

QUESTIONABLE POINT - FROM PIT 0.0000E+00
WARNING LONG THIS QUAD:
1 0.11000E+02 0.11000E+02 0.11000E+02 0.11000E+02 0.11000E+02 0.11000E+02 0.11000E+02 0.11000E+02 0.11000E+02 0.11000E+02
2 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
3 -0.00000E+00 -0.00000E+00 -0.00000E+00 -0.00000E+00 -0.00000E+00 -0.00000E+00 -0.00000E+00 -0.00000E+00 -0.00000E+00 -0.00000E+00

QUESTIONABLE POINT - FROM PIT 0.0370E-01
WARNING LONG THIS QUAD:
1 0.11000E+02 0.11000E+02 0.11000E+02 0.11000E+02 0.11000E+02 0.11000E+02 0.11000E+02 0.11000E+02 0.11000E+02 0.11000E+02
2 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
3 -0.00000E+00 -0.00000E+00 -0.00000E+00 -0.00000E+00 -0.00000E+00 -0.00000E+00 -0.00000E+00 -0.00000E+00 -0.00000E+00 -0.00000E+00

QUESTIONABLE POINT - FROM PIT 0.0200E-02
WARNING LONG THIS QUAD:
1 0.11000E+02 0.11000E+02 0.11000E+02 0.11000E+02 0.11000E+02 0.11000E+02 0.11000E+02 0.11000E+02 0.11000E+02 0.11000E+02
2 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
3 -0.00000E+00 -0.00000E+00 -0.00000E+00 -0.00000E+00 -0.00000E+00 -0.00000E+00 -0.00000E+00 -0.00000E+00 -0.00000E+00 -0.00000E+00

QUESTIONABLE POINT - FROM PIT 0.2000E+00
WARNING LONG THIS QUAD:
1 0.11000E+02 0.11000E+02 0.11000E+02 0.11000E+02 0.11000E+02 0.11000E+02 0.11000E+02 0.11000E+02 0.11000E+02 0.11000E+02
2 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
3 -0.00000E+00 -0.00000E+00 -0.00000E+00 -0.00000E+00 -0.00000E+00 -0.00000E+00 -0.00000E+00 -0.00000E+00 -0.00000E+00 -0.00000E+00

QUESTIONABLE POINT - FROM PIT 0.0100E-02
WARNING LONG THIS QUAD:
10 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00
20 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00
30 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00

QUESTIONABLE POINT - FROM PIT 0.0000E+00
WARNING LONG THIS QUAD:
20 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00
30 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00
40 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00

QUESTIONABLE POINT - FROM PIT 0.2000E-01
WARNING LONG THIS QUAD:
20 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00
30 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00
40 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00 0.00000E+00

*** CALCULATION OF INTERIOR PRESSURE COEFFICIENTS AND NORMAL VELOCITIES ***

AVERAGE CD ON INLET PANELS = 7.0222807 E-01 INLET AREA = 7.7047707 E-01
 AVERAGE CD ON EXHAUST PANELS = 1.00007207 E-01 EXHAUST AREA = 6.00007070 E-01
 CPE = 0.00003728 E-01
 CPHE = 3.00101200 E-01
 ADJUSTMENT FOR HEATING OR COOLING TEMPERATURE RATIO = 7.70000020 E-01
 EFFECTIVE EXHAUST AREA = 3.07000070 E-01

CPE = 0.00000007 E-01
 CPHE = 2.00100000 E-01
 NORMAL VELOCITY AT PANEL 1 = -0.1000012E+00
 NORMAL VELOCITY AT PANEL 6 = -0.2010012E+00
 NORMAL VELOCITY AT PANEL 7 = -0.2000000E+00
 NORMAL VELOCITY AT PANEL 9 = -0.2100017E+00
 NORMAL VELOCITY AT PANEL 11 = -0.2700070E+00
 NORMAL VELOCITY AT PANEL 12 = -0.1210070E+00
 NORMAL VELOCITY AT PANEL 15 = -0.2700007E+00
 NORMAL VELOCITY AT PANEL 115 = 0.0000012E+00
 NORMAL VELOCITY AT PANEL 117 = 0.2700000E+00
 NORMAL VELOCITY AT PANEL 119 = 0.2010012E+00

ORIGINAL PAGE IS
 OF POOR-QUALITY

SOURCE DENSITY SOLUTION

REST COEFFS ARE WITH PANEL AND AREA YIELDING 500 PANELS -- FUSELAGE ONLY

X VELOCITY=1.0 Y VELOCITY=0.0 Z VELOCITY=0.0

ITERATIVE MATRIX SOLUTION INFORMATION

ITERATION	SUM OF CHANGES	A	B1	B2
1	0.42070E+01			
2	0.20701E+01			
3	0.02070E+01			
4	0.00000E+00			
5	0.00000E+00			
6	0.00000E+00			
7	0.00000E+00			
8	0.00000E+00			
9	0.00000E+00			
10	0.00000E+00			
11	0.00000E+00			
12	0.00000E+00			
13	0.00000E+00			
14	0.00000E+00			
15	0.00000E+00			
16	0.00000E+00			
17	0.00000E+00			
18	0.00000E+00			
19	0.00000E+00			
20	0.00000E+00			
21	0.00000E+00			
22	0.00000E+00			
23	0.00000E+00			
24	0.00000E+00			
25	0.00000E+00			
26	0.00000E+00			
27	0.00000E+00			
28	0.00000E+00			
29	0.00000E+00			
30	0.00000E+00			
31	0.00000E+00			
32	0.00000E+00			
33	0.00000E+00			
34	0.00000E+00			
35	0.00000E+00			
36	0.00000E+00			
37	0.00000E+00			
38	0.00000E+00			
39	0.00000E+00			
40	0.00000E+00			
41	0.00000E+00			
42	0.00000E+00			
43	0.00000E+00			
44	0.00000E+00			
45	0.00000E+00			
46	0.00000E+00			
47	0.00000E+00			
48	0.00000E+00			
49	0.00000E+00			
50	0.00000E+00			

COMPUTATION OF VELOCITIES AND PRESSURE COEFFICIENTS AT THE PANEL CENTERS

REST COEFFS ARE WITH PANEL AND AREA YIELDING 500 PANELS -- FUSELAGE ONLY

PAGE 1

P. NO.	XC	YC	ZC	UX	UY	UZ	ABS.V	CP	SOURCE	V NORMAL	AREA
01	11.20170	0.00110	-1.02012	-0.00222	0.10007	-0.10030	0.06766	7.00000	3.00000	-0.222E+00	3.111E+00
02	11.20000	0.10000	-1.77702	-0.00000	0.00200	-0.02202	1.00000	-0.10700	3.07010	-0.070E+00	3.100E+00
03	11.20170	0.10000	-1.00002	-0.00000	0.00000	-0.00000	0.00000	0.00000	0.00000	0.000E+00	0.000E+00
04	11.20000	0.20000	-1.77700	-0.00000	0.00000	-0.00000	1.00000	-0.10700	3.07010	-0.070E+00	3.100E+00
05	11.20170	0.20000	-1.00002	-0.00000	0.00000	-0.00000	0.00000	0.00000	0.00000	0.000E+00	0.000E+00
06	11.20000	0.30000	-1.77700	-0.00000	0.00000	-0.00000	1.00000	-0.10700	3.07010	-0.070E+00	3.100E+00
07	11.20170	0.30000	-1.00002	-0.00000	0.00000	-0.00000	0.00000	0.00000	0.00000	0.000E+00	0.000E+00
08	11.20000	0.40000	-1.77700	-0.00000	0.00000	-0.00000	1.00000	-0.10700	3.07010	-0.070E+00	3.100E+00
09	11.20170	0.40000	-1.00002	-0.00000	0.00000	-0.00000	0.00000	0.00000	0.00000	0.000E+00	0.000E+00
10	11.20000	0.50000	-1.77700	-0.00000	0.00000	-0.00000	1.00000	-0.10700	3.07010	-0.070E+00	3.100E+00
11	11.20170	0.50000	-1.00002	-0.00000	0.00000	-0.00000	0.00000	0.00000	0.00000	0.000E+00	0.000E+00
12	11.20000	0.60000	-1.77700	-0.00000	0.00000	-0.00000	1.00000	-0.10700	3.07010	-0.070E+00	3.100E+00
13	11.20170	0.60000	-1.00002	-0.00000	0.00000	-0.00000	0.00000	0.00000	0.00000	0.000E+00	0.000E+00
14	11.20000	0.70000	-1.77700	-0.00000	0.00000	-0.00000	1.00000	-0.10700	3.07010	-0.070E+00	3.100E+00
15	11.20170	0.70000	-1.00002	-0.00000	0.00000	-0.00000	0.00000	0.00000	0.00000	0.000E+00	0.000E+00
16	11.20000	0.80000	-1.77700	-0.00000	0.00000	-0.00000	1.00000	-0.10700	3.07010	-0.070E+00	3.100E+00
17	11.20170	0.80000	-1.00002	-0.00000	0.00000	-0.00000	0.00000	0.00000	0.00000	0.000E+00	0.000E+00
18	11.20000	0.90000	-1.77700	-0.00000	0.00000	-0.00000	1.00000	-0.10700	3.07010	-0.070E+00	3.100E+00
19	11.20170	0.90000	-1.00002	-0.00000	0.00000	-0.00000	0.00000	0.00000	0.00000	0.000E+00	0.000E+00
20	11.20000	1.00000	-1.77700	-0.00000	0.00000	-0.00000	1.00000	-0.10700	3.07010	-0.070E+00	3.100E+00
21	11.20170	1.00000	-1.00002	-0.00000	0.00000	-0.00000	0.00000	0.00000	0.00000	0.000E+00	0.000E+00
22	11.20000	1.10000	-1.77700	-0.00000	0.00000	-0.00000	1.00000	-0.10700	3.07010	-0.070E+00	3.100E+00
23	11.20170	1.10000	-1.00002	-0.00000	0.00000	-0.00000	0.00000	0.00000	0.00000	0.000E+00	0.000E+00
24	11.20000	1.20000	-1.77700	-0.00000	0.00000	-0.00000	1.00000	-0.10700	3.07010	-0.070E+00	3.100E+00
25	11.20170	1.20000	-1.00002	-0.00000	0.00000	-0.00000	0.00000	0.00000	0.00000	0.000E+00	0.000E+00
26	11.20000	1.30000	-1.77700	-0.00000	0.00000	-0.00000	1.00000	-0.10700	3.07010	-0.070E+00	3.100E+00
27	11.20170	1.30000	-1.00002	-0.00000	0.00000	-0.00000	0.00000	0.00000	0.00000	0.000E+00	0.000E+00
28	11.20000	1.40000	-1.77700	-0.00000	0.00000	-0.00000	1.00000	-0.10700	3.07010	-0.070E+00	3.100E+00
29	11.20170	1.40000	-1.00002	-0.00000	0.00000	-0.00000	0.00000	0.00000	0.00000	0.000E+00	0.000E+00
30	11.20000	1.50000	-1.77700	-0.00000	0.00000	-0.00000	1.00000	-0.10700	3.07010	-0.070E+00	3.100E+00
31	11.20170	1.50000	-1.00002	-0.00000	0.00000	-0.00000	0.00000	0.00000	0.00000	0.000E+00	0.000E+00
32	11.20000	1.60000	-1.77700	-0.00000	0.00000	-0.00000	1.00000	-0.10700	3.07010	-0.070E+00	3.100E+00
33	11.20170	1.60000	-1.00002	-0.00000	0.00000	-0.00000	0.00000	0.00000	0.00000	0.000E+00	0.000E+00
34	11.20000	1.70000	-1.77700	-0.00000	0.00000	-0.00000	1.00000	-0.10700	3.07010	-0.070E+00	3.100E+00
35	11.20170	1.70000	-1.00002	-0.00000	0.00000	-0.00000	0.00000	0.00000	0.00000	0.000E+00	0.000E+00
36	11.20000	1.80000	-1.77700	-0.00000	0.00000	-0.00000	1.00000	-0.10700	3.07010	-0.070E+00	3.100E+00
37	11.20170	1.80000	-1.00002	-0.00000	0.00000	-0.00000	0.00000	0.00000	0.00000	0.000E+00	0.000E+00
38	11.20000	1.90000	-1.77700	-0.00000	0.00000	-0.00000	1.00000	-0.10700	3.07010	-0.070E+00	3.100E+00
39	11.20170	1.90000	-1.00002	-0.00000	0.00000	-0.00000	0.00000	0.00000	0.00000	0.000E+00	0.000E+00
40	11.20000	2.00000	-1.77700	-0.00000	0.00000	-0.00000	1.00000	-0.10700	3.07010	-0.070E+00	3.100E+00
41	11.20170	2.00000	-1.00002	-0.00000	0.00000	-0.00000	0.00000	0.00000	0.00000	0.000E+00	0.000E+00
42	11.20000	2.10000	-1.77700	-0.00000	0.00000	-0.00000	1.00000	-0.10700	3.07010	-0.070E+00	3.100E+00
43	11.20170	2.10000	-1.00002	-0.00000	0.00000	-0.00000	0.00000	0.00000	0.00000	0.000E+00	0.000E+00
44	11.20000	2.20000	-1.77700	-0.00000	0.00000	-0.00000	1.00000	-0.10700	3.07010	-0.070E+00	3.100E+00
45	11.20170	2.20000	-1.00002	-0.00000	0.00000	-0.00000	0.00000	0.00000	0.00000	0.000E+00	0.000E+00
46	11.20000	2.30000	-1.77700	-0.00000	0.00000	-0.00000	1.00000	-0.10700	3.07010	-0.070E+00	3.100E+00
47	11.20170	2.30000	-1.00002	-0.00000	0.00000	-0.00000	0.00000	0.00000	0.00000	0.000E+00	0.000E+00
48	11.20000	2.40000	-1.77700	-0.00000	0.00000	-0.00000	1.00000	-0.10700	3.07010	-0.070E+00	3.100E+00
49	11.20170	2.40000	-1.00002	-0.00000	0.00000	-0.00000	0.00000	0.00000	0.00000	0.000E+00	0.000E+00
50	11.20000	2.50000	-1.77700	-0.00000	0.00000	-0.00000	1.00000	-0.10700	3.07010	-0.070E+00	3.100E+00

ORIGINAL PAGE IS
OF POOR QUALITY

PRESSURE LIST AND DRAG COEFFICIENTS

PRESSURE CL = 0.00000
PRESSURE CR = 0.01700
APPROXIMATE AREA = 174.00000
SPYNOID NUMBER = 0.2279E+00

BY	SYM	SYM	SYM	CP	VELOCITY	VELOCITY	VELOCITY	ADPH	ZOCP40000000	ZOCP40000000	BT
1	0.77628	0.09277	-0.00000	0.00000	-0.00000	0.00100	0.00070	0.111	-0.0010752	0.0000100	1
2	0.77628	0.09277	-0.00000	0.00000	-0.00000	0.00100	0.00070	0.100	-0.0000250	-0.0190000	2
3	0.77628	0.09277	-0.00000	0.00000	-0.00000	0.00100	0.00070	0.089	-0.0001020	0.0000000	3
4	0.77628	0.09277	-0.00000	0.00000	-0.00000	0.00100	0.00070	0.150	-0.0000000	0.0000000	4
5	0.77628	0.09277	-0.00000	0.00000	-0.00000	0.00100	0.00070	0.101	-0.0000000	0.0000000	5
6	0.77628	0.09277	-0.00000	0.00000	-0.00000	0.00100	0.00070	0.100	-0.0000000	0.0000000	6
7	0.77628	0.09277	-0.00000	0.00000	-0.00000	0.00100	0.00070	0.100	-0.0000000	0.0000000	7
8	0.77628	0.09277	-0.00000	0.00000	-0.00000	0.00100	0.00070	0.100	-0.0000000	0.0000000	8
9	0.77628	0.09277	-0.00000	0.00000	-0.00000	0.00100	0.00070	0.101	-0.0000000	0.0000000	9
10	0.77628	0.09277	-0.00000	0.00000	-0.00000	0.00100	0.00070	0.101	-0.0000000	0.0000000	10
11	0.77628	0.09277	-0.00000	0.00000	-0.00000	0.00100	0.00070	0.101	-0.0000000	0.0000000	11
12	0.77628	0.09277	-0.00000	0.00000	-0.00000	0.00100	0.00070	0.101	-0.0000000	0.0000000	12
13	0.77628	0.09277	-0.00000	0.00000	-0.00000	0.00100	0.00070	0.101	-0.0000000	0.0000000	13
14	0.77628	0.09277	-0.00000	0.00000	-0.00000	0.00100	0.00070	0.101	-0.0000000	0.0000000	14
15	0.77628	0.09277	-0.00000	0.00000	-0.00000	0.00100	0.00070	0.101	-0.0000000	0.0000000	15
16	0.77628	0.09277	-0.00000	0.00000	-0.00000	0.00100	0.00070	0.101	-0.0000000	0.0000000	16
17	0.77628	0.09277	-0.00000	0.00000	-0.00000	0.00100	0.00070	0.101	-0.0000000	0.0000000	17
18	0.77628	0.09277	-0.00000	0.00000	-0.00000	0.00100	0.00070	0.101	-0.0000000	0.0000000	18
19	0.77628	0.09277	-0.00000	0.00000	-0.00000	0.00100	0.00070	0.101	-0.0000000	0.0000000	19
20	0.77628	0.09277	-0.00000	0.00000	-0.00000	0.00100	0.00070	0.101	-0.0000000	0.0000000	20
21	0.77628	0.09277	-0.00000	0.00000	-0.00000	0.00100	0.00070	0.101	-0.0000000	0.0000000	21
22	0.77628	0.09277	-0.00000	0.00000	-0.00000	0.00100	0.00070	0.101	-0.0000000	0.0000000	22
23	0.77628	0.09277	-0.00000	0.00000	-0.00000	0.00100	0.00070	0.101	-0.0000000	0.0000000	23
24	0.77628	0.09277	-0.00000	0.00000	-0.00000	0.00100	0.00070	0.101	-0.0000000	0.0000000	24
25	0.77628	0.09277	-0.00000	0.00000	-0.00000	0.00100	0.00070	0.101	-0.0000000	0.0000000	25

26	0.77628	0.09277	-0.00000	0.00000	-0.00000	0.00100	0.00070	0.101	-0.0000000	0.0000000	26
27	0.77628	0.09277	-0.00000	0.00000	-0.00000	0.00100	0.00070	0.101	-0.0000000	0.0000000	27
28	0.77628	0.09277	-0.00000	0.00000	-0.00000	0.00100	0.00070	0.101	-0.0000000	0.0000000	28
29	0.77628	0.09277	-0.00000	0.00000	-0.00000	0.00100	0.00070	0.101	-0.0000000	0.0000000	29
30	0.77628	0.09277	-0.00000	0.00000	-0.00000	0.00100	0.00070	0.101	-0.0000000	0.0000000	30

CALCULATION OF CURVED STREAMLINES

SPYR CURVED 100 WITH 1001 AND 1002 YIELDING 500 PANELS -- FUSELAGE ONLY
FOR V INFINITE. COMPUTE 500 STREAMLINES STARTING AT EACH PANEL CENTROID POINT

LINE PASSING THROUGH QUADRILATERAL 2

1	2	3	4	CP	SL	UABS
1	11.20000	0.00000	-1.00000	0.00000	0.0	0.00000
2	11.20000	0.10000	-1.77740	-0.10700	0.27032	1.00000
3	10.07201	0.00000	-1.00000	-0.27000	0.73007	1.17001
4	10.07200	0.00000	-2.11070	-0.07300	1.00000	1.00000
5	0.07032	0.00000	-2.07300	-0.00000	2.10770	1.00000

TRANSITION AT 2 0 0.00010 PER STEP NUMBER 2

S	V	UBS	MEAN	DELTA S	THETA S	YAS	CFI
0.0	100.00000	0.00000	0.00000	0.0	0.0	1000.00000	1000.00000
0.27032	170.01001	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
0.54064	181.00000	12.00000	2.00000	0.00107	0.00000	0.00000	0.00000
0.81096	180.99000	12.00000	1.00000	0.00000	0.00000	0.00000	0.00000
1.08128	170.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000

LINE PASSING THROUGH QUADRILATERAL 4

1	2	3	4	CP	SL	UABS
1	11.20100	0.21000	-1.00000	0.12210	0.0	0.00000
2	11.20100	0.20000	-1.73000	-0.12200	0.20000	1.00000
3	10.07000	0.00000	-1.00000	-0.20000	0.73000	1.17000
4	10.07000	0.00000	-2.10000	-0.07000	1.00000	1.00000
5	0.00000	0.00000	-2.10000	-0.07000	2.07000	1.00000

TRANSITION AT 4 0 0.00010 PER STEP NUMBER 4

S	V	UBS	MEAN	DELTA S	THETA S	YAS	CFI
0.0	100.00000	0.00000	0.00000	0.0	0.0	1000.00000	1000.00000
0.20000	180.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
0.40000	180.00000	10.00000	2.00000	0.00100	0.00000	0.00000	0.00000
0.60000	180.00000	10.00000	1.00000	0.00000	0.00000	0.00000	0.00000
0.80000	170.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000

ORIGINAL PAGE IS
OF POOR QUALITY

ST	END	VSD	END	CP	VSDND	VSDND	VSDND	ASP	PCDPCDPCDPCDPCD	PCDPCDPCDPCD	ST
1	0.77420	0.00377	-0.00422	0.00007	-0.40020	0.00147	0.17002	0.111	-0.0010000	0.0000000	1
2	0.73077	0.00001	-0.01012	0.10700	-0.30000	0.00010	0.20000	0.100	0.0000000	-0.0100000	2
3	0.71000	0.01300	0.00000	0.00000	-0.20100	0.00000	0.00000	0.100	-0.0000000	0.0000000	3
4	0.61000	0.10000	-0.00170	-0.10000	-0.00000	-0.00000	0.00000	0.100	0.0000000	-0.0100000	4
5	0.60000	0.20000	-0.00000	0.00000	-0.00000	-0.00000	0.00000	0.101	-0.0100000	0.0000000	5
6	0.00000	0.00000	-0.00000	0.00000	-0.00000	-0.00000	0.00000	0.100	0.0000000	-0.0000000	6
7	0.00000	0.00000	-0.10000	0.00000	-0.00000	-0.00000	0.00000	0.100	-0.0100000	0.0000000	7
8	0.00000	0.00000	-0.00000	0.00000	-0.00000	-0.00000	0.00000	0.100	0.0000000	-0.0000000	8
9	0.00000	0.00000	-0.00000	0.00000	-0.00000	-0.00000	0.00000	0.101	-0.0000000	0.0000000	9
10	0.00000	0.00000	-0.00000	0.00000	-0.00000	-0.00000	0.00000	0.100	-0.0000000	0.0000000	10
11	0.00000	0.00000	-0.00000	0.00000	-0.00000	-0.00000	0.00000	0.100	0.0000000	-0.0000000	11
12	0.00000	0.00000	-0.00000	0.00000	-0.00000	-0.00000	0.00000	0.100	0.0000000	-0.0000000	12
13	0.00000	0.00000	-0.00000	0.00000	-0.00000	-0.00000	0.00000	0.100	0.0000000	-0.0000000	13
14	0.00000	0.00000	-0.00000	0.00000	-0.00000	-0.00000	0.00000	0.100	0.0000000	-0.0000000	14
15	0.00000	0.00000	-0.00000	0.00000	-0.00000	-0.00000	0.00000	0.100	0.0000000	-0.0000000	15
16	0.00000	0.00000	-0.00000	0.00000	-0.00000	-0.00000	0.00000	0.100	0.0000000	-0.0000000	16
17	0.00000	0.00000	-0.00000	0.00000	-0.00000	-0.00000	0.00000	0.100	0.0000000	-0.0000000	17
18	0.00000	0.00000	-0.00000	0.00000	-0.00000	-0.00000	0.00000	0.100	0.0000000	-0.0000000	18
19	0.00000	0.00000	-0.00000	0.00000	-0.00000	-0.00000	0.00000	0.100	0.0000000	-0.0000000	19
20	0.00000	0.00000	-0.00000	0.00000	-0.00000	-0.00000	0.00000	0.100	0.0000000	-0.0000000	20
21	0.00000	0.00000	-0.00000	0.00000	-0.00000	-0.00000	0.00000	0.100	0.0000000	-0.0000000	21
22	0.00000	0.00000	-0.00000	0.00000	-0.00000	-0.00000	0.00000	0.100	0.0000000	-0.0000000	22
23	0.00000	0.00000	-0.00000	0.00000	-0.00000	-0.00000	0.00000	0.100	0.0000000	-0.0000000	23
24	0.00000	0.00000	-0.00000	0.00000	-0.00000	-0.00000	0.00000	0.100	0.0000000	-0.0000000	24
25	0.00000	0.00000	-0.00000	0.00000	-0.00000	-0.00000	0.00000	0.100	0.0000000	-0.0000000	25
26	0.00000	0.00000	-0.00000	0.00000	-0.00000	-0.00000	0.00000	0.100	0.0000000	-0.0000000	26

260	0.00000	0.00000	-0.11010	-0.20110	0.00000	-0.00000	0.00000	0.100	-0.0000000	0.0000000	260
261	0.00000	0.00000	-0.00000	-0.00000	0.00000	-0.00000	-0.00000	0.100	0.0000000	-0.0000000	261
262	0.00000	0.00000	-0.00000	-0.00000	0.00000	-0.00000	-0.00000	0.100	0.0000000	-0.0000000	262
263	0.00000	0.00000	-0.00000	-0.00000	0.00000	-0.00000	-0.00000	0.100	0.0000000	-0.0000000	263
264	0.00000	0.00000	-0.00000	-0.00000	0.00000	-0.00000	-0.00000	0.100	0.0000000	-0.0000000	264
265	0.00000	0.00000	-0.00000	-0.00000	0.00000	-0.00000	-0.00000	0.100	0.0000000	-0.0000000	265
266	0.00000	0.00000	-0.00000	-0.00000	0.00000	-0.00000	-0.00000	0.100	0.0000000	-0.0000000	266
267	0.00000	0.00000	-0.00000	-0.00000	0.00000	-0.00000	-0.00000	0.100	0.0000000	-0.0000000	267
268	0.00000	0.00000	-0.00000	-0.00000	0.00000	-0.00000	-0.00000	0.100	0.0000000	-0.0000000	268
269	0.00000	0.00000	-0.00000	-0.00000	0.00000	-0.00000	-0.00000	0.100	0.0000000	-0.0000000	269
270	0.00000	0.00000	-0.00000	-0.00000	0.00000	-0.00000	-0.00000	0.100	0.0000000	-0.0000000	270
271	0.00000	0.00000	-0.00000	-0.00000	0.00000	-0.00000	-0.00000	0.100	0.0000000	-0.0000000	271
272	0.00000	0.00000	-0.00000	-0.00000	0.00000	-0.00000	-0.00000	0.100	0.0000000	-0.0000000	272
273	0.00000	0.00000	-0.00000	-0.00000	0.00000	-0.00000	-0.00000	0.100	0.0000000	-0.0000000	273
274	0.00000	0.00000	-0.00000	-0.00000	0.00000	-0.00000	-0.00000	0.100	0.0000000	-0.0000000	274
275	0.00000	0.00000	-0.00000	-0.00000	0.00000	-0.00000	-0.00000	0.100	0.0000000	-0.0000000	275
276	0.00000	0.00000	-0.00000	-0.00000	0.00000	-0.00000	-0.00000	0.100	0.0000000	-0.0000000	276
277	0.00000	0.00000	-0.00000	-0.00000	0.00000	-0.00000	-0.00000	0.100	0.0000000	-0.0000000	277
278	0.00000	0.00000	-0.00000	-0.00000	0.00000	-0.00000	-0.00000	0.100	0.0000000	-0.0000000	278
279	0.00000	0.00000	-0.00000	-0.00000	0.00000	-0.00000	-0.00000	0.100	0.0000000	-0.0000000	279
280	0.00000	0.00000	-0.00000	-0.00000	0.00000	-0.00000	-0.00000	0.100	0.0000000	-0.0000000	280

TOTAL BODY CHEMICALS

TOTAL BODY CL = 0.00107
TOTAL BODY CD = 0.00000
REPLACEMENT AREA = 170.00000
BODY LENGTH = 23.70000

USER'S INSTRUCTIONS - GRIDPLOT PROGRAM

The program is written in FORTRAN IV and is designed to execute in single _____ precision on an IBM 370/165 computer with an average execution time of 1 minute for each data set. An average execution requires approximately 320,000 bytes of core storage. The program accepts multiple data sets. _____

Given a data set describing the half-body* under consideration, the program may be instructed to perform the following:

- (a) Generate a properly-indexed data set with additional body (M,N) stations,
- (b) Modify the input data by a simple averaging technique, a linear-interpolation technique, and/or user-specified data-point change information,
- (c) Plot various orthographic, perspective, and/or stereoscopic views of the input data and/or the modified data,
- (d) Refine the grid network by either an equal-line augmentation scheme or a user-specified line augmentation scheme,
- (e) Punch properly-indexed data sets of the input and/or modified data set(s) for input into the NCSU PLOT program of NASA CR-2523 and/or into the FLOWBODY program of this report, and
- (f) Convert the data into different units.

* Since the body is considered to be symmetrical about the X-Z plane, only half of the body is needed to describe the entire body.

The program requires the specification of the following input in the indicated order: _____

CARD 1:

- (a) The maximum number N of N-stations present in any input data set to be tried:

N is a right-adjusted positive integer number occupying columns 1-5.

- (b) The maximum number M of M-stations present in any input data set to be tried:

M is a right-adjusted positive integer number occupying columns 6-10.

- (c) The maximum number NADD of additional N-stations present in any input data set to be tried:

NADD is a right-adjusted positive integer number occupying columns 11-15.

- (d) The maximum number MADD of additional M-stations present in any input data set to be tried:

MADD is a right-adjusted positive integer number occupying columns 16-20.

- (e) The horizontal (x-direction) length PXL of the plotting picture:

PXL is a single-precision floating-point number occupying columns 21-30 in an F10.0 field. The units of PXL must be appropriate to the installation. At NCSU, PXL must be in inches.

- (f) The width (y-direction) PYL of the plotting picture:

PYL is a single-precision floating-point number occupying columns 31-40 in a F10.0 field. The units of PYL must be appropriate to the installation. At NCSU, PYL must be in inches.

Important: Only one "Card 1" is permitted per execution.

CARD 2:

- (a) The read unit number IDS:

IDS is a right-adjusted integer number occupying columns 1-5 and specifying that the data is to be read from cards, magnetic tape, disk, etc. The user must supply the suitable job control cards for the tape and/or disk reads. The IDS parameter controls only the reading of CARD 3, CARD 4, and the Body Description cards.

- (b) The desired number INPTM of additional interior M-stations:

INPTM is a right-adjusted integer number occupying columns 6-10. INPTM may be negative, zero, or positive. If INPTM is negative, no grid refinement of the M-station is performed. If INPTM is zero, no equal-line augmentation is performed but allows for refinement by the user-specified line-augmentation scheme. If INPTM is positive, the equal-line augmentation scheme may (to be explained later) be used with the number of additional M-stations between each two successive input M-stations equal to INPTM.

- (c) The desired number INPTN of additional interior N-stations:

INPTN is a right-adjusted integer number occupying columns 11-15. INPTN may be negative, zero, or positive. If INPTN is

negative, no grid refinement of the N-stations is performed. If INPTN is zero, no equal-line augmentation is performed but allows for refinement by the user-specified line-augmentation scheme. If INPTN is positive, the equal-line augmentation scheme may (to be explained later) be used with the number of additional N-stations between each two successive input M-stations equal to INPTN.

(d) The punch option IPUNCH:

IPUNCH is a right-adjusted nonnegative integer number, occupying columns 16-20, that specifies the punching of the data set with the additional body (M,N) stations. If IPUNCH = 0, no cards are punched. If IPUNCH = 1, cards are punched.

(e) The input-data plot option IPLOT1:

IPLOT1 is a right-adjusted nonnegative integer number occupying columns 21-25. If IPLOT1 = 0, no plots are produced. If IPLOT1 = 1, plots are produced.

(f) The modified-data plot option IPLOT2:

IPLOT2 is a right-adjusted nonnegative integer number occupying columns 26-30. If IPLOT2 = 0, no plots are produced. If IPLOT2 = 1, plots are produced.

(g) The input-data punch option LPCH1:

LPCH1 is a right-adjusted nonnegative integer number, occupying columns 31-35, that specifies the punching of the input data in a compatible form for the PLOT program given in NASA CR-2523 [Reference 3]. If LPCH1 = 0, no cards are punched. If LPCH1 = 1, cards are punched.

(h) The modified-data punch option LPCH2: —

LPCH2 is a right-adjusted nonnegative integer number, occupying columns 36-40, that specifies the punching of the modified data in a compatible form for the PLOT program given in NASA CR-2523 [Reference 3]. If LPCH2 = 0, no cards are punched. If LPCH2 = 1, cards are punched.

(i) The write option IWRITE: —

IWRITE is a right-adjusted nonnegative integer number, occupying columns 41-45, that specifies the amount of desired output. If IWRITE = 0, maximum printout is produced. If IWRITE = 2, minimum printout is produced. If IWRITE = 1, the amount of printout is between the minimum and maximum.

(j) The conversion factor CF: —

CF is a single-precision floating-point number, occupying columns 51-60 in an F10.0 field, that may be used to convert the data of CARD 5 through CARD (K + 4) from one set of units to another.

CARD 3:

The title array TITLE:

The 80 characters of the array TITLE are used for identifying output. The reading of TITLE is controlled by the read unit number IDS.

CARD 4:

The number NQE of quadrilaterals of the input half-body data: —

NQE is a right-adjusted integer number occupying columns 1-4. The reading of NQE is controlled by the read unit number IDS.

**** Body Description Cards ****

Each card contains the information to specify one half-body point. Each card contains

Columns	FORTTRAN Name	Description
1-12	XI	x-coordinate
13-24	YI	y-coordinate
25-36	ZI	z-coordinate
37-40	NI	N-station index (See Figure 4)
41-44	MI	M-station index (See Figure 4)
45-48	NS	Body number

XI, YI, and ZI are single-precision floating-point numbers in F-fields. NI, MI, and NS are right-adjusted integer numbers. NS should be a constant for a given data set, which must be greater than zero but not equal to 1000. A blank card must be supplied at the end of these cards to signal the end of the body description cards. The reading of the body description cards are controlled by the read unit number IDS.

**** Point Modification Cards ****

1. Additional Input Point Change Information:

A single card contains the information to change one input point to the given values.

Columns	FORTTRAN Name	Description
1-20	XP	New X-value at (N,M)
21-40	YP	New Y-value at (N,M)
41-60	ZP	New Z-value at (N,M)
61-65	N	Reference N-station (\leq max NI)
66-70	M	Reference M-station (\leq max MI)

XP, YP, and ZP are single-precision floating-point numbers in F-fields. N and M are right-adjusted integer numbers that denote the N and M station for the application of XP, YP, and ZP. A blank card must be supplied to serve either of two purposes. If no additional point change information is to be supplied, the blank card terminates the attempt to read more cards. If point

change information is supplied, the blank card signals the end of this information.

2. Simple Averaging of Points or Linear Interpolation:

A single card contains the information to change one input point in a prescribed manner. The user may specify a two-point average, four-point average, two-point linear interpolation, or four-point linear interpolation.

Columns	FORTRAN Name	Description
1-5	M1	1st reference M-station $[0 \leq M1 \leq \max(MI)]$
6-10	M2	2nd reference M-station $[1 \leq M2 \leq \max(MI)+1]$
11-15	N1	1st reference N-station $[0 \leq N1 \leq \max(NI)]$
16-20	N2	2nd reference N-station $[1 \leq N2 \leq \max(NI)+1]$
21-25	IMETH	Method: IMETH = 0 → simple average IMETH = 1 → linear interpolation

It should be noted that points are changed by the order in which the data cards are encountered. It must be true that

$$|M2 - M1| = 0 \text{ or } 2$$

and

$$|N2 - N1| = 0 \text{ or } 2 .$$

Consider a representative (plane) portion of the grid of the original input data below. Suppose it is desired to modify the original input point (e).

Three schemes of each method are available (See Figure 5):

1. Two-point scheme of the points (a) and (c): $M2 = (m+1)$, $M1 = (m-1)$,
 $N2 = (n+2)$, $N1 = (n)$
2. Two-point scheme of the points (b) and (d): $M2 = (m+2)$, $M1 = (m)$,
 $N2 = (n+1)$, $N1 = (n+1)$
3. Four-point scheme of the points (a), (b), (c), and (d): $M2 = (m+2)$,
 $M1 = (m)$, $N2 = (n+2)$, $N1 = (n)$.

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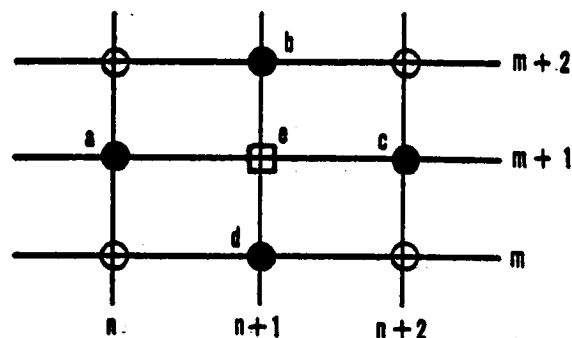


Figure 5: Illustration of points used in averaging and interpolating schemes

M_2 , M_1 , N_2 , and N_1 are right-adjusted integer numbers. A blank card must be supplied to serve either of two purposes. If no averaging (or linear interpolation) information is to be supplied, the blank card terminates the attempt to read more cards. If averaging (or linear interpolation) information is supplied, the blank card signals the end of this information.

**** Console Message LABEL Card ****

The 80 characters of the array LABEL is used to provide information to the operator on the console typewriter about specific forms for plotting. Important: Only one LABEL card is permitted per execution.

**** Plot Cards ****

A single card contains all the necessary information for one plot. The available options and the necessary input for each are described in the succeeding sections. Reading of these cards are controlled by nonzero values of IPLOT1 and/or IPLOT2. Although the various plot cards, applicable to both the input and modified data, are presently discussed, only the plot card(s) pertaining to the plotting of the input data (i.e., if IPLOT1 \neq 0) must be included at this time.

Orthographic projections. - For orthographic projections, the card should be set up as follows (See Figure 6):

Columns	FORTTRAN Name	Description
1	HORZ	"X", "Y", or "Z" for horizontal axis
3	VERT	"X", "Y", or "Z" for vertical axis
5 to 7	TEST1	Word "OUT" for deletion of hidden lines; otherwise, leave blank
8 to 12	PHI	Roll angle, degrees (See Figure 7)
13 to 17	THETA	Pitch angle, degrees (See Figure 7)
18 to 22	PSI	Yaw angle, degrees (See Figure 7)
48 to 52	PLOTSZ	PLOTSZ determines the size of plot (scale factor is computed using PLOTSZ and maximum dimension of configuration)
53 to 55	TYPE	Word "ORT"
72	KODE	If KODE = 0, continue reading plot cards If KODE = 1, after processing this plot, continue with the remaining non-plotting portion of the program

An attempt is made to center the given-configuration within the specified field. If the desired plot size is greater than 28 inches, centering is attempted within 28 inches so care must be taken in choosing the view. Minimum values are adjusted so that body axis lines with no rotation angles coincide with grid lines on the plotter paper. Therefore, the plotter pen should always be positioned exactly 1 inch from the side of the plotting space and on the intersection of heavy grid lines at the start of plotting.

Plan, front, and side views (stacked). - For plan, front, and side views, the card should be set up as follows (See Figure 8):

Columns	FORTTRAN Name	Description
8 to 12	PHI	y-origin on paper of plan view, inches
13 to 17	THETA	y-origin on paper of side view, inches
18 to 22	PSI	y-origin on paper of front view, inches

Columns	FORTRAN Name	Description
48 to 52	PLOTSZ	PLOTSZ determines size of plot (a scale factor is computed using PLOTSZ and maximum dimension of configuration)
53 to 55	TYPE	Word "VU3"
72	KODE	If KODE = 0, continue reading plot cards If KODE = 1, after processing this plot, continue with the remaining non-plotting portion of the program

Perspective views. - For perspective views, the card should be set up as follows (See Figure 9):

Columns	FORTRAN Name	Description
8 to 12	PHI	x of view point (location of viewer) in data coordinate system
13 to 17	THETA	y of view point in data coordinate system
18 to 22	PSI	z of view point in data coordinate system
23 to 27	XF	x of focal point (determines direction and focus) in data coordinate system
28 to 32	YF	y of focal point in data coordinate system
33 to 37	ZF	z of focal point in data coordinate system
38 to 42	DIST	Distance from eye to viewing plane, inches
43 to 47	FMAG	Viewing-plane magnification factor; it controls size of projected image
48 to 52	PLOTSZ	Diameter of viewing plane, inches; DIST and PLOTSZ together determine a cone which is field of vision; PLOTSZ value is also relative to type of viewer which is to be used.
53 to 55	TYPE	Word "PER"
72	KODE	If KODE = 0, continue reading plot cards If KODE = 1, after processing this plot, continue with the remaining non-plotting portion of the program

Stereo frames suitable for viewing in a stereoscope. - For stereo frames suitable for viewing in a stereoscope, the input is identical to that for the perspective views except that the word "STE" is used in columns 53 to 55. (See Figure 10). _____

IMPORTANT: If $IPLOT1 \neq 0$, at least one plot card must be supplied. Similarly, if $IPLOT2 \neq 0$, at least one plot card must be supplied.

**** User-Specified Line-Augmentation Cards ****

A single card contains the information to specify additional M-lines or N-lines between the "referenced" input M- or N-line.

Columns	FORTRAN Name	Description
1-4	NAME	Line of reference (M or N or END)
6-10	K1	Reference line number
11-15	NL	Number of additional lines

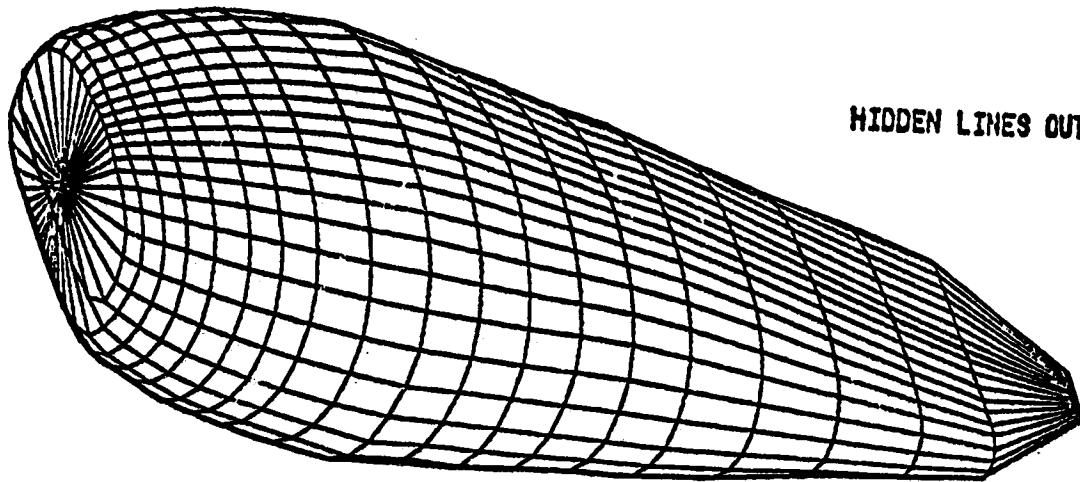
NAME is a character array, occupying columns 1-4 in an A4 field. If NAME = M, the number NL of additional lines is supplied between M-line (K1) and M-line (K1+1). If NAME = N, the number NL of additional lines is supplied between N-line (K1) and N-line (K1+1). Cards of this type is continued until NAME = END is encountered. Since NAME is a character array, the specification of M, N, or END must be left-adjusted.

**** Plot Cards for Modified Data ****

The plot cards described earlier must be now included for the plotting of the modified body, if and only if $IPLOT2 \neq 0$.

Specification of the cards above represent a complete set of data for a particular body. Additional data sets are programmed similarly starting again at CARD 2. A blank card should be supplied at the end of the last data set to terminate the program.

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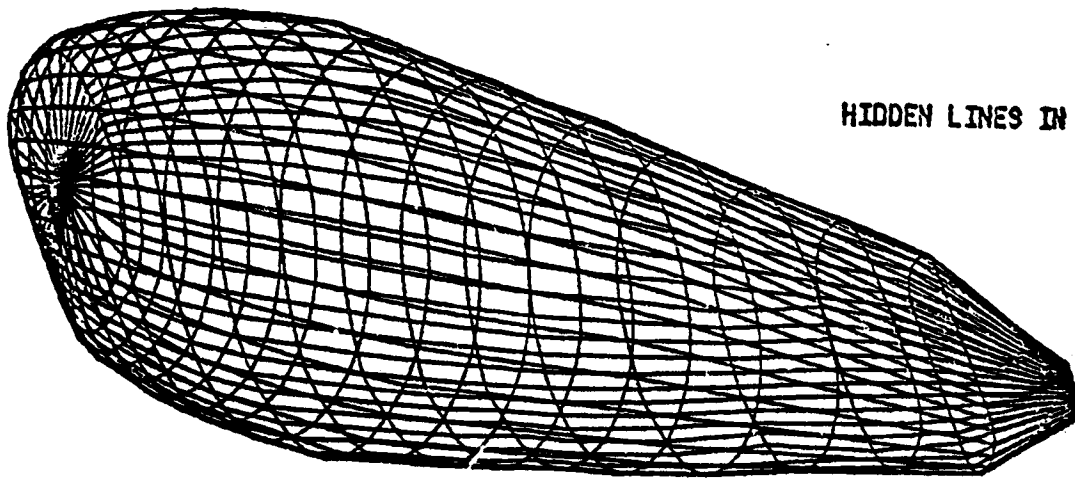
HIDDEN LINES OUT

NEW FAT NACELLE FOR LESS DRAG WITH N=21 AND M=21 YIELDING 400 PANELS —

X Z OUT 45. 10. 30.

6.0 ORT

0



HIDDEN LINES IN

NEW FAT NACELLE FOR LESS DRAG WITH N=21 AND M=21 YIELDING 400 PANELS —

X Z 45. 10. 30. _____

6.0 ORT

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Figure 6: Example of orthographic projection

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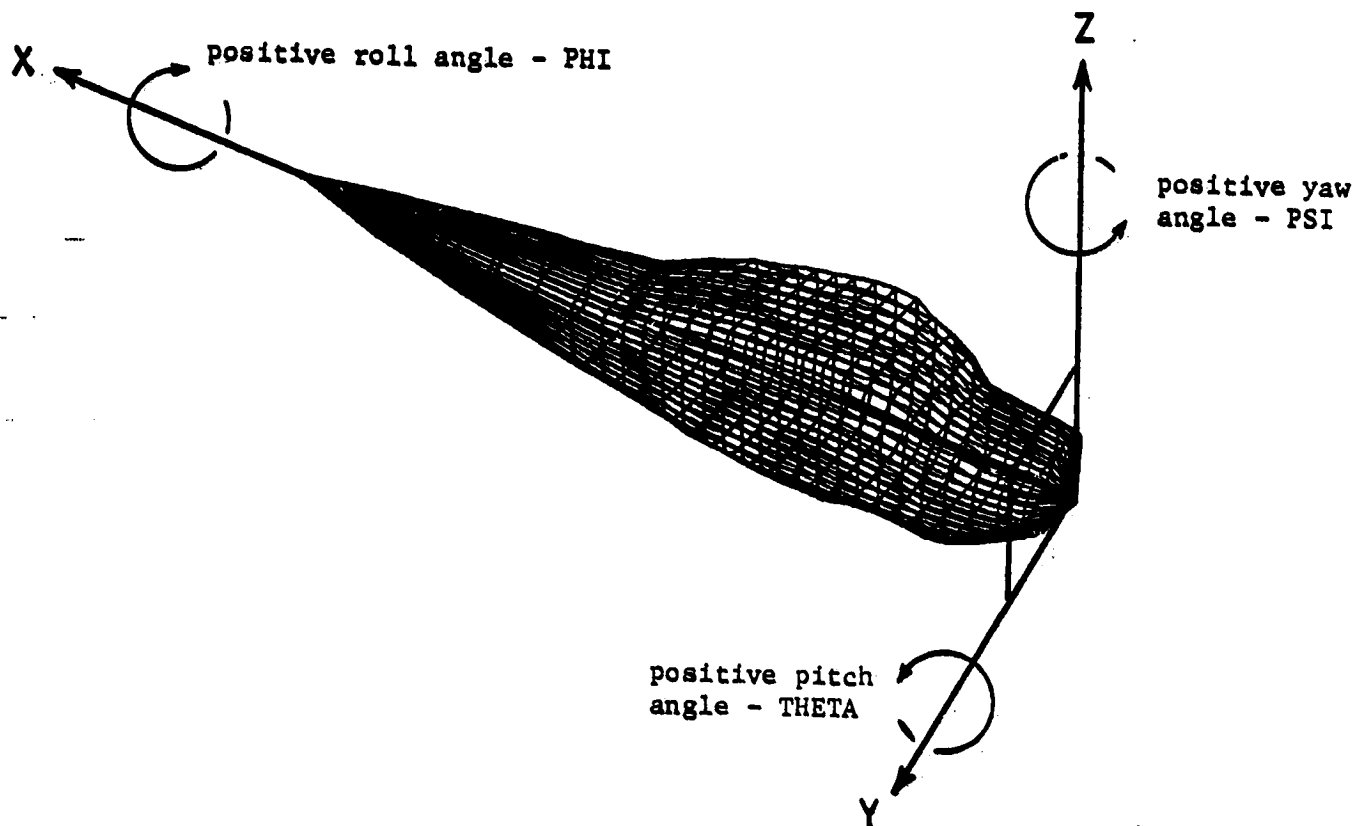


Figure 7: Orientation of body with respect to body reference axes for plotting angles

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BEST CESSNA 182 WITH M=21 AND N=29

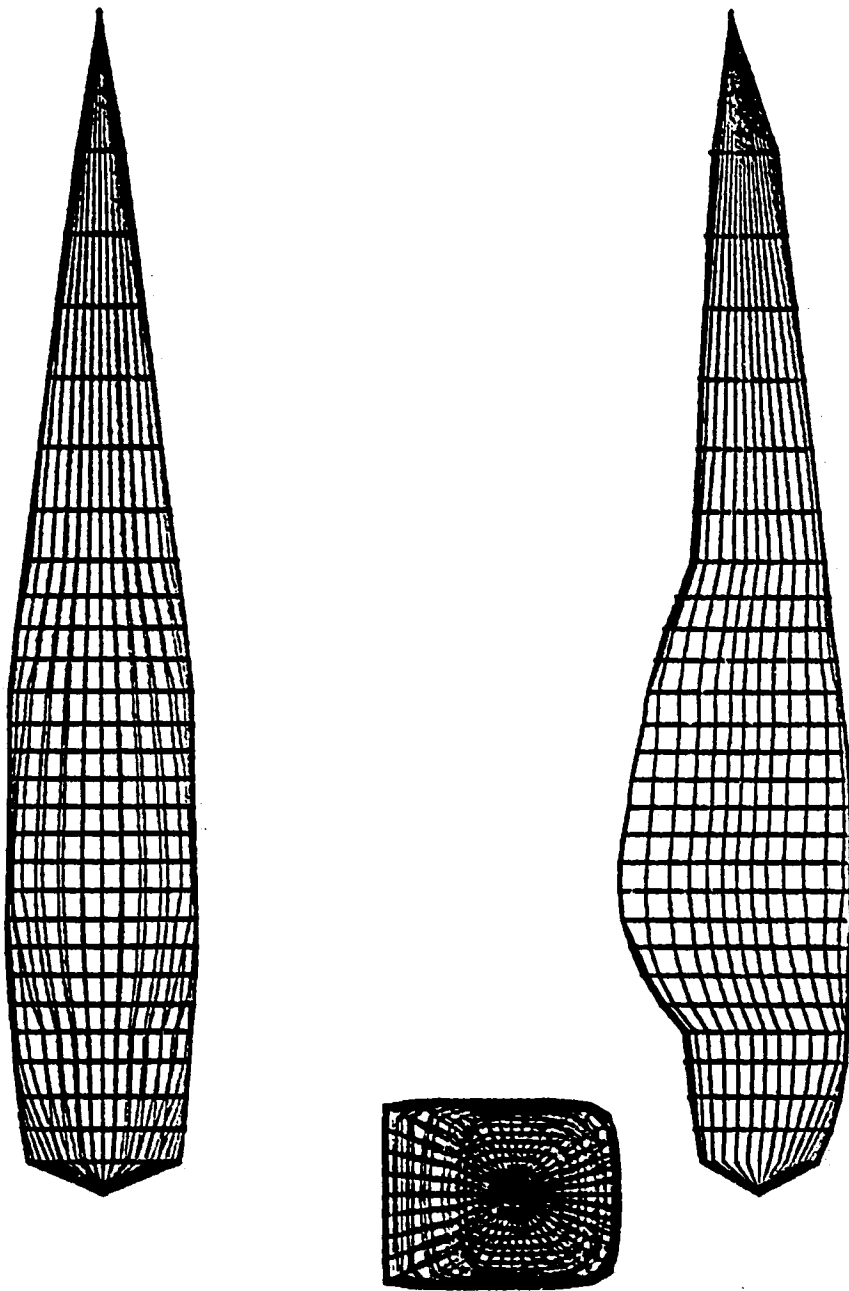
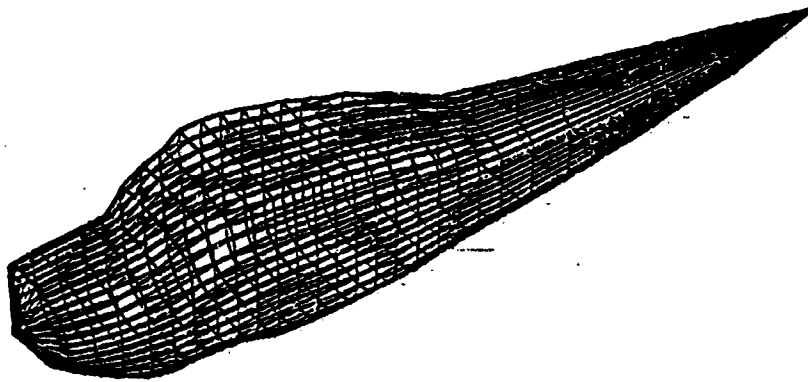


Figure 8: Example of 3-view plot

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BEST CESSNA 182 WITH M=21 AND N=29 YIELDING 560 PANELS -- FUSELAGE ONLY

-20. -50. 50. 12. 0.0 0.0 14. 1.0 8.0 PER 1

Figure 9: Example of perspective view

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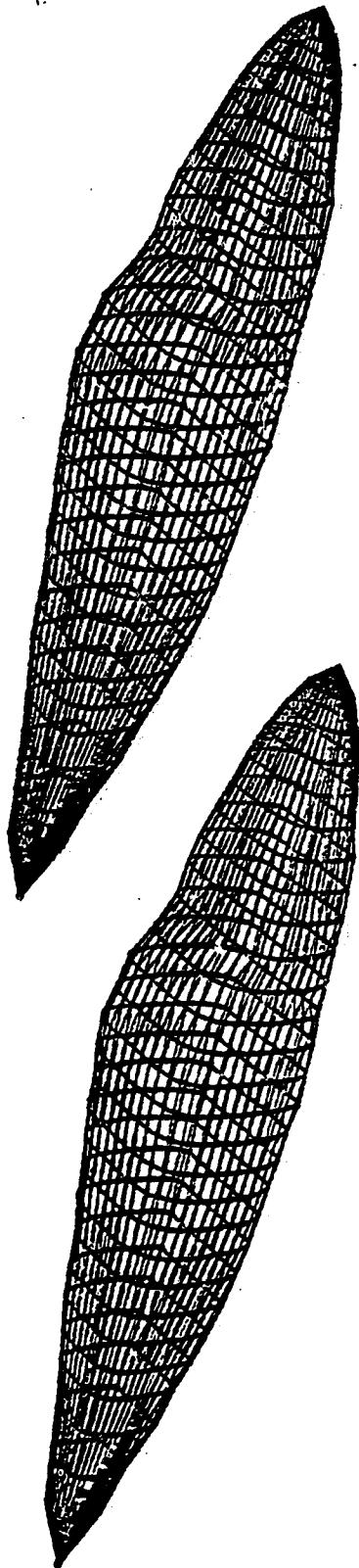


Figure 10: Example of stereo frames of stereoscopic view

PROGRAM LISTING - GRIDPLOT

PROGRAMMER:

STAN R. FOX
2406 BROUGHTON BDLG
DEPT ME ENGRG, NCSU
RALEIGH, N.C. 27650
PHONE: 919/737-2374

FOR A COMPLETE DESCRIPTION OF NECESSARY INPUT AND THE AVAILABLE
OPTIONS, CONSULT THE USER'S INSTRUCTIONS.

```

DIMENSION P(29,21,3),X(29),Y(29),Z(29),XN(89),YN(89),Q(29,81,3),R(
19,81,3),XFUS(89),SFUS(89,81,2),BS(2,81,3),C(4,29),D(29),DIAG(29),
1MP(21,2),NP(29,2)
DIMENSION XAME1(4),XAME2(4),LABEL(80)
COMMON /INPUT/JREAD,JWRITE,JPUNCH,KFILE1,KFILE2,KFILE3,KFILE4,IMRI
ITE
COMMON /TRANS/TITLE(20)
COMMON /CODE/ICODE,IBP1,IBP2
COMMON /PCODE/LCODE
DATA XAME1/4HINPU,4HT PL,4HOT D,4HATA /,XAME2/4HNEW ,4HPLOT,4H DAT
1,4HA /

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JREAD=1
JPUNCH=2
JWRITE=3
KFILE1=4
KFILE2=5
KFILE3=6
KFILE4=7
NCOUNT=1

```

```

READ DATA CARDS
READ (JREAD,1) N,M,NADD,MADD,PXL,PYL
1 FORMAT (4I5,2F10,0)
J1=M
J2=N

```

C**

```

N1=N+IABS(NADD)
M1=M+IABS(MADD)
J3=MAX0(N1,M1)
J4=MAX0(N,M)
2 READ (JREAD,3) IDS,IPPTM,INPTN,IPUNCH,IPLOT1,IPLOT2,LPCCH1,LPCCH2,IW
WRITE,CF

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3 FORMAT (9I5,5X,F10.5)
  ICAN=0
  IF (CF.EQ.0.0E0)CF=1.0E0
  IF ((IDS.GT.0.AND.IDS.NE.JPUNCH).AND.(IDS.NE.JWRITE.AND.IDS.NE.KFI
1L1).AND.(IDS.NE.KFILE2.AND.IDS.NE.KFILE3).AND.IDS.NE.KFILE4) GO TO
1 5
  IF (IDS.LE.0) GO TO 97
  WRITE (JWRITE,4)
4 FORMAT (1X,///.3X,28HERROR IN IDS ... TERMINATING.//)
  GO TO 97
5 INPTN=IABS(INPTN)
  INPTM=IABS(INPTM)
  INPTNS=INPTN
  INPTMS=INPTM
  READ (IDS,6) (TITLE(I),I=1,20)
6 FORMAT (20A4)
  WRITE (JWRITE,7) (TITLE(I),I=1,20)
7 FORMAT (1H1,/,5X,8HINPUT**.,/,10X,20A4,/)
  WRITE (JWRITE,9) IDS,INPTM,INPTN,IPUNCH,IPLGT1,IPLGT2,LPCH1,LPCH2.
  IWRITE,CF
8 FORMAT (1X,/,10X,4HIDS=,13,3X,6HINPTM=,13,4X,6HINPTN=,13,4X,7HIPUN
1CH=,13,4X,7HIPLOT1=,13,3X,7HIPLOT2=,13,/,10X,6HLPCH1=,13,2X,6HLPCH
12=,13,3X,7HIWRITE=,13,3X,3HCF=,E16.9,/)
  READ (IDS,9) NQE
9 FORMAT (14)
  WRITE (JWRITE,10) NQE
10 FORMAT (10X,25HNUMBER OF QUADRILATERALS.,14,/)
  IF (IWRITE.EQ.0) WRITE (JWRITE,11)
11 FORMAT (15X,2HX1,12X,2HY1,12X,2HZ1,8X,2HNI,5X,2HMI,5X,2HNS,/)
12 READ (IDS,12) XI,YI,ZI,NI,MI,NS
  FORMAT (3F12.8,3I4)
  MMAX=MI
  MMIN=MI
  NMAX=NI
  NMIN=NI
  NSS=NS
  L=1
  GO TO 14
13 READ (IDS,12) XI,YI,ZI,NI,MI,NS
  IF (NS.NE.NSS) GO TO 16
  L=L+1
14 IF (IWRITE.EQ.0) WRITE (JWRITE,15) XI,YI,ZI,NI,MI,NS

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15 FORMAT (10X,3(F12.8,2X),3(15.2X))
P(NI,MI,1)=XI*CF
P(NI,MI,2)=YI*CF
P(NI,MI,3)=ZI*CF
MMAX=MAXO(MMAX,MI)
MMIN=MINO(MMIN,MI)
NMAX=MAXO(NMAX,NI)
NMIN=MINO(NMIN,NI)
GC TO 13
16 NC=(MMAX-MMIN)*(NMAX-NMIN)
IF (NO.EQ.NQE) GO TO 18
WRITE (JWRITE,17) NO.NQE
17 FORMAT (1X,/,/,5X,30HNUMBER OF QUADRILATERALS READ(.14,56H) DOES N
1 NOT EQUAL THE NUMBER OF SPECIFIED QUADRILATERALS(.14,1H))
ICAN=1
GO TO 96
C** INPUT READING COMPLETED, CHECK FOR ERRORS
18 IF (((MMAX.EQ.(2*(MMAX/2)).OR.MMAX.LT.4)).OR.(MMIN.EQ.(2*(MMIN/2)).
1 OR.MMIN.LE.1)).OR.((NMAX.EQ.(2*(NMAX/2)).OR.NMAX.LT.4)).OR.(NMIN.EQ
1.(2*(NMIN/2)).OR.NMIN.LE.1))) GO TO 19
GO TO 21
19 WRITE (JWRITE,20) MMAX,MMIN,NMAX,NMIN
20 FORMAT (1X,/,/,5X,23HERROR DETECTED IN INPUT,3X,6HMMAX =.13,3X,6HMM
1 IN =.13,/,31X,6HNMAX =.13,3X,6HNMIN =.13)
ICAN=1
GO TO 56
C** ENACT POINT MODIFICATIONS
21 CALL PNT1(J1,J2,P,JREAD,JWRITE,CF)
CALL PNT2(J1,J2,P,JREAD,JWRITE,MMAX,NMAX)
IF (NCCUNT.NE.1) GO TO 23
IF (IPLJTI.EQ.0.AND.IPLOT2.EQ.0) GO TO 23
CALL PICSIZ(PXL,PYL)
READ (JREAD,22) (LABEL(NN),NN=1,80)
22 FCFORMAT (30A1)
CALL PENMSG(LABEL)
23 IF (IPLOT1.EQ.0.AND.LPCH1.EQ.0) GO TO 38
LCODE=1
CONVERT TO PLOT AXIS SYSTEM
ZMAX=-1000.0
ZMIN=1000.0
DO 24 NN=1,NMAX
XFUS(NN)=P(1,1,1)-P(NN,1,1)

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37 P(NN,MM,3)=P(NN,MM,3)-ZORG
38 IF (INPTM.LT.0.AND.INPTN.LT.0.AND.IPLOT2.EQ.0.AND.LPCH2.EQ.0) GO TO 206
10 96
CALL TEST(MAC1,MAC2,MP,NP,J1,J2,KM1,KM2,KN1,KN2,MMAX,NMAX)
KN=NMAX
IF ((INPTM.EQ.0.AND.INPTN.EQ.0).AND.(MAC1.EQ.0.AND.MAC2.EQ.0)) GO
  TO 79
C*** FOR EACH N-STATION, CURVE FIT THE M-STATIONS
  IBP1=0
  IBP2=0
  K=0
  DO 54 N=1,NMAX
  IF (N.EQ.1.OR.N.EQ.NMAX) GO TO 39
  GO TO 46
39 IF (MAC1.NE.0) GO TO 40
  NPTS=MMAX+(MMAX-1)*INPTM
  GO TO 41
40 NPTS=MAC1
C*** FOR FIRST AND LAST N-STATIONS
41 DO 42 M=1,NPTS
42 Q(N,M,1)=P(N,1,1)
  IQ=1
  IP=1
  Q(N,IQ,2)=P(N,IP,2)
  Q(N,IQ,3)=P(N,IP,3)
43 IQMX=IQ+1+INPTM
  IF (IP.GT.MMAX) GO TO 54
  IF (MAC1.EQ.0) GO TO 44
  ICODE=0
  IF ((IP-1).GE.KM1)ICCODE=1
  IF (ICCODE.EQ.0)INPTM=MP(IP-1,1)
  IF (ICCODE.EQ.1)INPTM=MP(IP-KM1,2)
  IF (ICCODE.EQ.0)IBP1=IBP1+INPTM
  IF (ICCODE.EQ.1)IBP2=IBP2+INPTM
  IQMX=IQ+1+INPTM
44 X1=(P(N,IP,2)-P(N,IP-1,2))/FLOAT(INPTM+1)
  X2=(P(N,IP,3)-P(N,IP-1,3))/FLOAT(INPTM+1)
  IQF1=IQ+1
  DC 45 ML=IQF1,IQMX
  Q(N,ML,2)=Q(N,ML-1,2)+X1
  Q(N,ML,3)=Q(N,ML-1,3)+X2

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46 IQ=IQMX
   GO TO 43
   MID=(MMAX+1)/2
   KNS=MID+(MID-1)*INPTMS
   SLP1=P(N,1,2)/P(N,1,3)
   SLP2=(P(N,MID,2)-P(N,1,2))/(P(N,MID,3)-P(N,1,3))
   M1=1
   M2=MID
   ICCDF=0
   MADD=0
   MD=0
   Y0=P(N,MID,2)
   Z0=P(N,MID,3)
47 DO 48 M=M1,M2
   Z(M+MADD)=(P(N,M,3)-Z0)*COS(A)+(P(N,M,2)-Y0)*SIN(A)
   Y(M+MADD)=(P(N,M,2)-Y0)*COS(A)-(P(N,M,3)-Z0)*SIN(A)
48 CONTINUE
   IF (MAC1.EQ.0) GO TO 49
   KNS=KM2+IBP2
   IF (ICDF.EQ.3) KNS=KM1+IBP1
49 CALL PCS(MID,Y,Z,XN,YN,INPTM,KN,C,D,DIAG,JWRITE,J4,J3,MAC1,MP,J1,K
1)
   IF (KN.NE.KNS) GO TO 50
   GO TO 52
50 WRITE (JWRITE,51) N,ICDF,KN,KNS
51 FORMAT (1X,52HPCS DID NOT FIND CORRECT NO. OF POINTS AT N-STATION
1,13,12H WITH ICDF=.12,/,1X,6HFOUND .13,18H POINTS(SHOULD BE .13,1
1H))
52 DO 53 M=1,KN
   Q(N,M+MD,1)=P(N,1,1)
   Q(N,M+MD,2)=XN(M)*SIN(A)+YN(M)*COS(A)+Y0
   Q(N,M+MD,3)=XN(M)*COS(A)-YN(M)*SIN(A)+Z0
53 CONTINUE
   IF (ICDF.NE.0.OR.MID.EQ.MMAX) GO TO 54
   SLP1=P(N,MMAX,2)/P(N,1,3)
   SLP2=(P(N,MMAX,2)-P(N,MID,2))/(P(N,MMAX,3)-P(N,MID,3))
   A=ATAN((SLP2-SLP1)/(1.0+SLP1*SLP2))
   ICCDF=1
   M1=MID

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M2=MMAX
MADD=1-MID
MD=KN-1
GO TO 47
54 INPTM=INPTMS
C** SET INITIAL AND FINAL VALUES
DO 55 LL=1,2
N=1
IF (LL.EQ.2)N=NMAX
DO 55 M=1,NPTS
DO 55 JJ=1,3
BS(LL,M,JJ)=Q(N,M,JJ)
NMAX=NPTS
C** FOR EACH M-STATION. CURVE FIT EACH SET OF N-STATIENS
MID=(NMAX+1)/2
IF (NMAX.LI.7)MID=NMAX
KNS=MID+(MID-1)*INPTN
KS=NMAX+(NMAX-1)*INPTN
IF (MAC2.EQ.0) GO TO 57
K=1
IBP1=0
IBP2=0
JD2=NMAX
IF (NMAX.GE.7)JD2=(NMAX+1)/2
DO 56 J=1,NMAX
IF (J.LT.JD2)IBP1=IBP1+NP(J,1)
IF (J.GE.JD2)IBP2=IBP2+NP(J-JD2+1,2)
56 CONTINUE
DO 64 M=1,MMAX
X0=Q(MID,M,1)
Y0=Q(MID,M,2)
Z0=Q(MID,M,3)
SAX=0.0
ICGDE=0
M1=1
M2=MID
MADD=0
MD=0
54 SLP1=(Q(M1,M,2)-Q(M2,M,2))/(Q(M1,M,1)-Q(M2,M,1))
SLP2=(Q(M1,M,3)-Q(M2,M,3))/(Q(M1,M,1)-Q(M2,M,1))
ALP1=ATAN((SLP1-SAX)/(1.0+SAX*SLP1))
ALP2=ATAN((SLP2-SAX)/(1.0+SAX*SLP2))

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DO 59 N=M1,M2
IP=M2+M1-N
X(N+MADD)=(Q(IP,M,1)-X0)*COS(ALP1)+(Q(IP,M,2)-Y0)*SIN(ALP1)
Y(N+MADD)=(Q(IP,M,2)-Y0)*COS(ALP1)-(Q(IP,M,1)-X0)*SIN(ALP1)
59 CONTINUE
IF (MAC2.EQ.0) GO TO 60
KNS=KN2+IBP2
IF (ICODE.EQ.0)KNS=KN1+IBP1
60 CALL PCS(MID,Y,X,XN,YN,INPTN,KN,C,D,DIAG,JWRITE,J4,J3,MAC2,NP,J2,K
1)
IF (KN.NE.KNS) GO TO 77
DO 61 N=1,KN
IP=KN+1-N+MD
R(IP,M,1)=XN(N)*COS(ALP1)-YN(N)*SIN(ALP1)+X0
R(IP,M,2)=XN(N)*SIN(ALP1)+YN(N)*COS(ALP1)+Y0
61 DC 62 N=M1,M2
IP=N2+M1-N
X(N+MADD)=(Q(IP,M,1)-X0)*COS(ALP2)+(Q(IP,M,3)-Z0)*SIN(ALP2)
Z(N+MADD)=(Q(IP,M,3)-Z0)*COS(ALP2)-(Q(IP,M,1)-X0)*SIN(ALP2)
62 CONTINUE
CALL PCS(MID,Z,X,XN,YN,INPTN,KN,C,D,DIAG,JWRITE,J4,J3,MAC2,NP,J2,K
1)
IF (KN.NE.KNS) GO TO 77
DO 63 N=1,KN
IP=KN+1-N+MD
R(IP,M,3)=XN(N)*SIN(ALP2)+YN(N)*COS(ALP2)+Z0
63 CONTINUE
IF (ICODE.EC.1.OR.MID.EQ.NMAX) GO TO 64
ICODE=1
H1=M1)
M2=MMAX
MADD=1-MID
MD=KN-1
GC TO 58
64 CONTINUE
KN=KS
IF (MAC2.EQ.0) GO TO 65
KN=MAC2
DO 67 LL=1,2
N=1
IF (LL.EQ.2)N=KN
DJ 66 N=1,MMAX
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DD 66 JJ=1.3
66 R(N,M,JJ)=BS(LL,M,JJ)
67 CONTINUE
DD 76 N=1,KN
X0=0.0
DD 68 M=1,MMAX
X0=X0+R(N,M,1)
68 CONTINUE
X0=X0/FLOAT(MMAX)
IF (N.EQ.1) GO TO 70
IF (X0.LT.F(N-1,1,1)) GO TO 70
X0=0.0
LK=0
DD 69 N=1,MMAX
IF (R(N,M,1).GT.R(N-1,1,1)) GO TO 69
LK=LK+1
X0=X0+R(N,M,1)
69 CONTINUE
IF (LK.EQ.0) ICAN=1
IF (ICAN.EQ.1) GO TO 72
X0=X0/LCAT(LK)
70 DD 71 M=1,MMAX
71 R(N,M,1)=X0
IF (N.EQ.1) GO TO 76
IF (X0.GT.R(N-1,1,1)) GO TO 72
GO TO 76
72 NM1=N-1
IF (ICAN.EQ.1) GO TO 74
WRITE (JWRITE,73) N,NM1
73 FORMAT (1X,/,/,10X,29H AVERAGE X-VALUE AT N-STATION .I2,46H IS GRE
ATER THAN AVERAGE X-VALUE AT N-STATION .I2,38H. MUST BE LESS THAN
YOUR EXACTLY EQUAL.//)
GO TO 96
74 WRITE (JWRITE,75) N,NM1
75 FORMAT (1X,/,/,10X,25H ALL COMPUTED X-VALUES AT N-STATION .I2,51H A
RE GREATER THAN THE AVERAGE X-VALUE AT N-STATION .I2,//)
GO TO 56
76 CONTINUE
GO TO 81
77 WRITE (JWRITE,78) M,ICLDE,KN,KNS
78 FORMAT (1X,52H PCS DID NOT FIND CORRECT NO. OF POINTS AT M-STATION
.I,13,12H WITH ICODE=.I2,/,1X,6H FOUND .I3,18H POINTS(SHOULD BE .I3,1

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GRD 457

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1H))
ICAN=1
GO TO 96
79 DO 80 N=1,KN
DC 80 M=1,MMAX
DO 80 J=1,3
80 R(N,M,J)=P(N,M,J)
C*** NOW PRINT RESULTS
81 NNCE=(MMAX-1)*(KN-1)
82 IF (IMWRITE.NE.2) WRITE (JWRITE,82) MMAX,KN,NNCE
82 FORMAT (1H1,/,5X,11HNEW DATA**/,5X,6HMMAX =,13,3X,6HNNCE =,13,
12X,5H---->,15,15H QUADRILATERALS,/,15X,2HXI,12X,2HZI,8X,
12HN1,5X,2HMI,5X,2HNS,/)
83 IF (IPUNCH.NE.0) WRITE (JPUNCH,83) NNCE
83 FORMAT (14)
NS=1
DO 85 N=1,KN
DO 85 M=1,MMAX
DO 85 J=1,3
84 IF (ABS(R(N,M,J)).LT.1.0E-04)R(N,M,J)=0.0E0
84 IF (IPUNCH.NE.0) WRITE (JWRITE,15) (R(N,M,J),J=1,3),N,M,NS
84 IF (IPUNCH.NE.0) WRITE (JPUNCH,12) (R(N,M,J),J=1,3),N,M,NS
85 CONTINUE
85 IF (IPLOT2.EQ.0.AND.LPCH2.EQ.0) GO TO 96
LCGL=2
CONVERT TO PLOT AXIS SYSTEM
ZMAX=-1000.0
ZMIN=1000.0
DO 87 NN=1,KN
XFUS(NN)=R(1,1,1)-R(NN,1,1)
DO 86 MM=1,MMAX
IF (MM.GT.1.AND.MM.LT.MMAX) GO TO 86
IF (ZMAX.LT.R(NN,MM,3))ZMAX=R(NN,MM,3)
IF (ZMIN.GT.R(NN,MM,3))ZMIN=R(NN,MM,3)
86 CONTINUE
87 CONTINUE
ZORG=ABS(ZMIN)+ABS(ZMAX)
DO 88 NN=1,KN
DO 88 MM=1,MMAX
88 R(NN,MM,3)=R(NN,MM,3)+ZORG
C*** NEW DATA
88 IF (LPCH2.EQ.0) GO TO 92

```



```

WRITE (JPUNCH,26) (XAME2(I),I=1,4)
WRITE (JPUNCH,27) (XFUS(NN),NN=1,KN)
DO 89 NN=1,KN
WRITE (JPUNCH,27) (R(NN,MM,2),MM=1,MMAX)
IF (IWRITE.GT.1) GO TO 92
WRITE (JWRITE,93)
90 FORMAT (1X,///,10X,14HNEW PLOT DATA:./)
WRITE (JWRITE,30) (XFUS(NN),NN=1,KN)
DC 91 NN=1,KN
WRITE (JWRITE,30) (R(NN,MM,2),MM=1,MMAX)
WRITE (JWRITE,31)
WRITE (JWRITE,30) (R(NN,MM,3),MM=1,MMAX)
91 WRITE (JWRITE,31)
92 IF (IPLOT2.EQ.0) GO TO 94
REWIND KFILE4
WRITE (KFILE4) (XFUS(NN),NN=1,KN)
DO 93 NN=1,KN
WRITE (KFILE4) (R(NN,MM,2),MM=1,MMAX)
WRITE (KFILE4) (R(NN,MM,3),MM=1,MMAX)
CALL XYZPLT(MMAX,KN,XFUS,SFUS)
C*** RESET Z-VALUES
DO 95 NN=1,KN
DO 95 MM=1,MMAX
95 R(NN,MM,3)=R(NN,MM,3)-ZCRG
96 IF (IPLOT1.NE.0.OR.IPLOT2.NE.0) NCOUNT=NCOUNT+1
IF (IDS.NE.JREAD) REWIND IDS
GO TO 2
NCOUNT=NCOUNT+1
97 IF (NCOUNT.GT.1) CALL PICSIZ(0.0,0.0)
STOP
END

```

```

SUBROUTINE PNT1(J2,J1,R,JREAD,JWRITE,CF)
C*** POINT MODIFICATION BY ADDITIONAL INPUT POINT CHANGE INFORMATION
C DIMENSION R(J1,J2,3)
PNS 1
PNS 2
PNS 3
PNS 4
PNS 5

```

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PNS 6
PNS 7
PNS 8
PNS 9
PNS 10
PNS 11
PNS 12
PNS 13
PNS 14
PNS 15
PNS 16
PNS 17
PNS 18
PNS 19
PNS 20
PNS 21
PNS 22
PNS 23

```

K=0
1 READ (JREAD,2) XP,YP,ZP,N,M
2 FORMAT (3F20.0,2I5)
  IF (N.LE.0.OR.M.LE.0) GO TO 5
  K=K+1
  IF (K.EQ.1) WRITE (JWRITE,3)
3 FORMAT (1X,///.5X,63HPPOINT MODIFICATION BY ADDITIONAL INPUT POINT
1 CHANGE INFORMATION,///.15X,2HXI.12X,2HYI.12X,2HZI,8X,2HNI,5X,2HMI,/)
1) WRITE (JWRITE,4) XP,YP,ZP,N,M
4) FORMAT (10X,3(F12.8,2X),2(15,2X))
  R(N,M,1)=XP*CF
  R(N,M,2)=YP*CF
  R(N,M,3)=ZP*CF
  GO TO 1
5) RETURN
  FND

```

PNT 1
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```

SUBROUTINE PNT2(J2,J1,R,JREAD,JWRITE,MMAX,NMAX)
  POINT MODIFICATION BY SIMPLE AVERAGE OR LINEAR INTERPOLATION
  DIMENSION R(J1,J2,3)
  K=0
  ICCDF1=0
  ICCDF2=0
1) READ (JREAD,2) M1,M2,N1,N2,IMETH
2) FORMAT (5I5)
  IF ((M1.LE.3.AND.M2.LE.6).AND.(N1.LE.0.AND.N2.LE.0)) GO TO 31
  IF ((M1.LE.0.OR.M2.LE.3).OR.(N1.LE.0.OR.N2.LE.0)) GO TO 1
  N=K+1
  IF (K.EQ.1) WRITE (JWRITE,3)
3) FORMAT (1X,///.5X,38HPPOINT MODIFICATION BY SPECIFIED METHOD)
  JS=42
  IF (M1.LE.M2) G) TO 4
  JS=41
  M1=JS
  JS=N2
4)

```

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IF (N1.LE.N2) GO TO 5
N2=N1
N1=J5
L1=M2-M1
L2=N2-N1
5 IF (M2-MMAX-1) 6,6,1
6 IF (1-M1) 7,7,1
7 IF (N2-NMAX-1) 8,8,1
8 IF (1-N1) 9,9,1
9 IF ((L1.EQ.1.OR.L1.GT.2).OR.(L2.EQ.1.OR.L2.GT.2)).OR.(L1.EQ.0.AND
1.L2.FG.0) GO TO 1
IF (IMETH.LT.0)IMETH=0
IF (IMETH.GT.1)IMETH=1
AVN=0.OE0
AZN=0.OE0
AZM=0.OE0
AZME=0.OE0
IM=IMETH+1
IF (L1.NE.0.AND.L2.NE.0) GO TO 19
IF (L1.EC.0.AND.L2.NE.0) GO TO 13
IF (M2.GT.MMAX) GO TO 10
IF (M1.L1) GO TO 11
AYM=(R(N1,M1,2)+R(N1,M2,2))/2.OE0
AZM=(R(N1,M1,3)+R(N1,M2,3))/2.OE0
GO TO 12
10 AYM=(N1,M1+1,2)
AZM=(N1,M1,3)
GO TO 12
11 AYM=(N1,M2-1,2)
AZM=(N1,M2,3)
12 M=N1+1
D=1.OE0
GO TO 28
13 GC TO (14,15),IM
14 AYM=(R(N1,M1,2)+R(N2,M1,2))/2.OE0
AZM=(R(N1,M1,3)+R(N2,M1,3))/2.OE0
GC TO 18
15 IF (N2.GT.NMAX) GO TO 16
IF (N1.LT.1) GO TO 17
A=(R(N1,M1,2)-R(N2,M1,2))/(R(N1,M1,1)-R(N2,M1,1))
B=(R(N1,M1,2)-A*(R(N1,M1,1)))
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AYN=A*(R(N1+1,M1,1)+B
A=(R(N1,M1,3)-R(N2,M1,3))/(R(N1,M1,1))-R(N2,M1,1))
B=(N1,M1,3)-A*(R(N1,M1,1)
AZN=A*(R(N1+1,M1,1)+B
GO TO 18
16 AYN=R(N1,M1,2)
   AZN=R(N1,M1,3)
   ICODE1=1
   GC TO 18
17 AYN=R(N2,M1,2)
   AZN=R(N2,M1,3)
   ICODE2=1
18 N=N1+1
   M=M1
   DE=1.OF0
   GC TO 28
19 IF (M2.GT.MMAX) GO TO 20
   IF (M1.LT.1) GO TO 21
   AYM=(R(N1+1,M1,2)+R(N1+1,M2,2))/2.OE0
   AZM=(R(N1+1,M1,3)+R(N1+1,M2,3))/2.OE0
   GO TO 22
20 AYN=R(N1+1,M1+1,2)
   AZM=R(N1+1,M1+1,3)
   GC TO 22
21 AYM=R(N1+1,M2-1,2)
   AZM=R(N1+1,M2,3)
   GO TO (23,24),IM
22 IF (N2.GT.NMAX) GO TO 25
23 IF (N1.LT.1) GO TO 26
   AYN=(R(N1,M1+1,2)+R(N2,M1+1,2))/2.OE0
   AZN=(R(N1,M1+1,3)+R(N2,M1+1,3))/2.OE0
   GO TO 27
24 IF (N2.GT.NMAX) GO TO 25
   IF (N1.LT.1) GO TO 26
   A=(R(N1,M1+1,2)-R(N2,M1+1,2))/(R(N1,M1+1,1))-R(N2,M1+1,1))
   B=(R(N1,M1+1,2)-A*(R(N1,M1+1,1)
   AYN=A*(R(N1+1,M1+1,1)+B
   A=(R(N1,M1+1,3)-R(N2,M1+1,3))/(R(N1,M1+1,1))-R(N2,M1+1,1))
   B=(R(N1,M1+1,3)-A*(R(N1,M1+1,1)
   AZN=A*(R(N1+1,M1+1,1)+B
   GO TO 27
25 AYN=R(N1,M1+1,2)

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AZN=R(N1,M1+1,3)
ICDDE1=1
GO TO 27
26 AYN=R(N2,M1+1,2)
   AZN=R(N2,M1+1,3)
   ICDDE2=1
27 N=N1+1
   M=M1+1
   D=2.0E0
   AVY=(AYM+AYN)/D
   AVZ=(AZM+AZN)/D
   IF (IMETH.EQ.0) WRITE (JWRITE,29) N,M,R(N,M,2),AVY,R(N,M,3),AVZ
29 FORMAT (1X,/,12,/,M=,12,/,Y=,1PE14.7,/,-->,1PE14
1.7,/,22X,/,7=,1PE14.7,/,-->,1PE14.7,5X,14F5.1MPLA AVERAGE)
   IF (IMETH.EQ.1) WRITE (JWRITE,30) N,M,R(N,M,2),AVY,R(N,M,3),AVZ
30 FORMAT (1X,/,12,/,M=,12,/,Y=,1PE14.7,/,1PE14
1.7,/,22X,/,Z=,1PE14.7,/,-->,1PE14.7,5X,20HLINER INTERPOLATION)
   R(N,M,2)=AVY
   R(N,M,3)=AVZ
   GO TO 1
31 IF (ICDDE2.NE.0) WRITE (JWRITE,32)
32 FORMAT (1X,///,5X,67HWARNING...DATA NOT COMPATIBLE AS INPUT TO 'FL
LOWBODY: PROGRAM DUE TO,/,15X,39HPOINT MODIFICATION(S) AT FRONT OF
1BCDY.)
   IF (ICDDE1.NE.0) WRITE (JWRITE,33)
33 FORMAT (1X,///,5X,67HWARNING...DATA NOT COMPATIBLE AS INPUT TO 'FL
LOWBODY: PROGRAM DUE TO,/,15X,38HPOINT MODIFICATION(S) AT REAR OF B
1OEY.)
   RETURN
   END

```

C*** SUBROUTINE TEST(M1,M2,MF,NP,J1,J2,KM1,KM2,KN1,KN2,MX,NX)
C*** SUBROUTINE TEST ALLOWS THE SPECIFICATION OF ARBITRARY ADDITIONAL
C*** STATISTICS
C DIMENSION MP(J1,2),NP(J2,2)
COMMON /INPUT/JREAD,JWRITE,JPUNCH,KK(5)
DATA N/4HM /,N/4HN /,N/4HN /

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C*** INITIALIZE PARAMETERS
M1=0
M2=0
KM1=0
KN2=0
KN1=0
KN2=0
L1=0
L2=0
WRITE (JWRITE,1)
1 FORMAT (1H1,/,13X,43H ADDITIONAL ARBITRARY STATION SPECIFICATIONS
1,/,10X,48H REFERENCE M-STATIONS N-STATIONS |,/,11X,
19H STATION |,18X,1H |,/,19X,39H |TST HALF 2ND HALFTST HALF
1 2ND HALF |,/)
DO 2 J=1,J1
MP(J,1)=0
2 MF(J,2)=0
DO 3 J=1,J2
NP(J,1)=0
3 NP(J,2)=0
IF (MX.GE.7) GO TO 4
4 IF (NX.GE.7) GO TO 5
KN1=NX
KN1=NX
5 IF (MX.LT.7) GO TO 6
KM1=(MX+1)/2
KM2=KM1
6 IF (NX.LT.7) GO TO 7
KN1=(NX+1)/2
KN2=KN1
READ DATA CARDS
7 READ (JREAD,8) NAME,K1,NL
8 FORMAT (A4,1X,2I5)
IF (NAME.EQ.MN) GO TO 11
IF (NAME.EQ.M) GO TO 9
IF (NAME.EQ.N) GO TO 10
GO TO 12
9 IF (K1.LE.0.OR.K1.GE.MX) GO TO 7
IF (K1.LT.KM1) MP(K1,1)=IABS(NL)
IF (K1.GE.KM1) MP(K1-KM1+1,2)=IABS(NL)
L1=L1+IABS(NL)
GO TO 7

```

```

10 IF (K1.LE.0.OR.K1.GE.NX) GO TO 7
   IF (K1.LT.KNI) NP(K1,1)=IABS(NL)
   IF (K1.GE.KNI) NP(K1-KNI+1,2)=IABS(NL)
   L2=L2+IABS(NL)
   GO TO 7
11 M1=MX+L1
   M2=NX+L2
   IF ((2*(M1/2)).EQ.M1.OR.(2*(M2/2)).EQ.M2) GO TO 14
   GO TO 16
12 WRITE (JWRITE,13)
13 FORMAT (1X,///,1X,57HEFRROR... DATA CARD IN TEST ROUTINE HAS NO DIR
14 CALL EXIT
   RETURN
14 WRITE (JWRITE,15) M1,M2
15 FORMAT (1X,///,1X,38HWARNING... TOTAL NUMBER OF M-STATIONS(.13,16H
16 IF (M1.EQ.MX) M1=0
   IF (M2.EC.NX) M2=0
   K=KMI
   IF (KNI.GT.K) K=KNI
   DO 23 J=1,K
   IF (J.LE.KMI.AND.J.LE.KNI) GO TO 17
   IF (J.LE.KMI.AND.J.GT.KNI) GO TO 19
   IF (J.GT.KMI.AND.J.LF.KNI) GO TO 21
   WRITE (JWRITE,16) J,MP(J,1),MP(J,2),NP(J,1),NP(J,2)
17 FORMAT (12X,13,7X,13,7X,13,6X,13,7X,13)
   GO TO 23
19 WRITE (JWRITE,20) J,MP(J,1),MP(J,2)
20 FORMAT (12X,13,7X,13,7X,13)
   GO TO 23
21 WRITE (JWRITE,22) J,MP(J,1),NP(J,2)
22 FORMAT (12X,13,26X,13,7X,13)
23 CONTINUE
   WRITE (JWRITE,24)
24 FORMAT (1X,///)
   RETURN
   END

```

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SUBROUTINE PCS(K,F,X,XY,Y,INPIS,KN,C,D,DIAG,JWRITE,J4,J3,M1,N,J,KK PCS 1

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43 PCS

```

1) CONTROL ROUTINE FOR PIECEWISE CUBIC SPLINE
C*** DIMENSION F(J4),X(J4),XY(J3),Y(J3),C(4,J4),D(J4),DIAG(J4),N(J,2)
C COM'ON /CODE/ICODE,IBP1,IBP2
C KN=K+(K-1)*INPTS
  JPID2=K
  IF (M1.EQ.0) GO TO 1
  IF (ICODE.EQ.0)KN=JPID2+IBP1
  IF (ICODE.EQ.1)KN=JPID2+IBP2
  1 IF (KN.EQ.K) GO TO 2
  DF=1.0E-4
  GO TO 4
  2 D9 3 I=1,K
  Y(I)=F(I)
  3 XY(I)=X(I)
  GO TO 9
  4 C(2,1)=(F(2)-F(1))/(X(2)-X(1))
  C(2,K)=(F(K)-F(K-1))/(X(K)-X(K-1))
  DF 5 I=1,K
  C(1,I)=F(I)
  5 CALL SPLINE(K,X,C,D,DIAG,J4)
  XX=X(1)
  XXH=X(K)
  XINC=0.0E0
  M=C
  L=1
  6 M=M+1
  IF (M.GT.KN) GO TO 13
  XX=XX+XINC
  IF (ABS(XX-XXH).LT.DF)XX=XXH
  IF (XX.EQ.XXH) GO TO 7
  IF (ABS(XX-X(L)).LT.DF)XX=X(L)
  IF (ABS(XX-X(L+1)).LT.DF)XX=X(L+1)
  IF (XX.EQ.X(L+1)).AND.(XX.NE.X(K))L=L+1
  7 XY(M)=CUBIC(XX,X,C,K,J4)
  IF (XX.EC.XXH) GO TO 9
  IF (M1.EQ.0) GO TO 8
  IF (M.EQ.0)IMPIS=N(L,ICODE+1)

```


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44 PCS
45 PCS
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52 PCS

1 SPL
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```

IF (KK.EQ.1.AND.(JPID2-L).NE.0)INPTS=N(JPID2-L,ICODE+1)
8 IF (L.LT.K)XINC=(X(L+1)-X(L))/(INPTS+1)
GO TO 6
9 RETURN
10 WRITE (JWRITE,11) M,KN
11 FORMAT (3X,16HERROR IN PCS: M=,I4.6H > KN=,I4)
CALL EXIT
RETURN
END

```

```

SUBROUTINE SPLINE(NP1,XI,C,D,DIAG,J)
C*** PIECEWISE CUBIC SPLINE
C
C DIMENSION XI(J),C(4,J),D(J),DIAG(J)
C

```

```

D(1)=0.OE0
DIAG(1)=1.OE0
N=NP1-1
DO 1 M=2,NP1
D(M)=XI(M)-XI(M-1)
DIAG(M)=(C(1,M)-C(1,M-1))/D(M)
DO 2 M=2,N
C(2,M)=3.OE0*(D(M)+DIAG(M+1)+D(M+1))*DIAG(M)
DIAG(M)=2.OE0*(D(M)+D(M+1))
DO 3 M=2,N
G=-D(M+1)/DIAG(M-1)
DIAG(M)=DIAG(M)+G*D(M-1)
C(2,M)=C(2,M)+G*C(2,M-1)
NJ=NP1
DO 4 M=2,N
NJ=NJ-1
C(2,NJ)=C(2,NJ)-D(NJ)*C(2,NJ+1)/DIAG(NJ)
DX=XI(1+1)-XI(1)
DF1=(C(1,1+1)-C(1,1))/DX
DF3=C(2,1)+C(2,1+1)-2.OE0*DF1
C(3,1)=(DF1-C(2,1)-DF3)/DX
C(4,1)=DF3/DX/DX
5 RETURN

```

ORIGINAL PAGE IS
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SPL 31
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PCB 2
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PCB 13
PCB 14
PCB 15
PCB 16
PCB 17
PCB 18
PCB 19
PCB 20
PCB 21

XYZ 1
XYZ 2
XYZ 3
XYZ 4
XYZ 5
XYZ 6
XYZ 7
XYZ 8
XYZ 9
XYZ 10
XYZ 11
XYZ 12
XYZ 13
XYZ 14

```

END
FUNCTION PCUBIC(XBAR,XI,C,NP1,J)
C*** FUNCTION EVALUATION OF PIECEWISE CUBIC SPLINE
C
C DIMENSION XI(J),C(4,J)
C
I=1
DX=XBAR-XI(I)
IF (DX) 1,4,3
1 IF (1.EQ.1) GO TO 4
I=I-1
DX=XBAR-XI(I)
IF (DX) 1,4,4
2 I=I+1
DX=DDX
3 IF (1.EQ.(NP1-1)) GO TO 4
DDX=XBAR-XI(I+1)
IF (DDX) 4,2,2
4 PCUBIC=C(1,I)+DX*(C(2,I)+DX*(C(3,I)+DX*C(4,I)))
RETURN
END

```

```

SUBROUTINE XYZPLT(M,N,XFUS,SFUS)
C*** CONTROL ROUTINE FOR CONFIGURATION PLOTS
C
DIMENSION FIRST(7),XFUS(N),SFUS(N,M,2)
COMMON /PASS/ABC(20),ABCDE(20),HORZ,VERT,TEST1,PHI,THETA,PSI,XF,YF
1 ZF,DIST,FMAG,PLOTSZ,TYPE,XMIN,XMAX,YMIN,YMAX,ZMIN,ZMAX,XMID,YMID,
2 ZMID,BIGD,KODE,ISP
COMMON /INOUT/JREAD,JWRITE,JPUNCH,KFILE1,KFILE2,KFILE3,KFILE4,IMRI
1 IF
COMMON /PCODE/LCODE
COMMON /TRANS/TITLE(20)
DATA FIRST/4HNEW,4HBODY,4H WIT,4HH IM,4HPRCV,4HED G,4HHRID /,TAME/
14H /

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43 XYZ

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DO 1 I=1,20
IF (LCODE.EQ.1)ABC(I)=TITLE(I)
IF (LCODE.EQ.2.AND.1.LE.7)ABC(I)=FIRST(I)
IF (LCODE.EQ.2.AND.1.GT.7)ABC(I)=TAME
1 WRITE (JWRITE,2) (ABC(I),I=1,20)
2 FORMAT (28X25HCONFIGURATION DESCRIPTION//1X20A//)
C*** INPUT CONFIGURATION DESCRIPTION AND INITIALIZE
CALL CBC10(M,N,XFUS,SFUS)
C*** PLOT CONFIGURATION
WRITE (JWRITE,3)
3 FORMAT (//36X9HPLOT DATA//)
4 READ (JREAD,5) (ABCDE(I),I=1,20)
5 FORMAT (20A4)
WRITE (KFILE3,5) (ABCDE(I),I=1,20)
REWIND KFILE3
1LCYSZ,TYPE,KODE
PF WIND KFILE3
6 FORMAT (2A2,A3,9F5.3,A3,16X,11)
WRITE (JWRITE,7) HORZ,VERT,TEST1,PHI,THETA,PSI,XF,YF,ZF,DIST,FMAG,
1PLOTSZ,TYPE,KODE
7 FORMAT (1X,2A2,A3,9(1X,F10.5),A3,16X,11)
CALL CBC20(M,N)
IF (KODE.EQ.0) GO TO 4
WRITE (JWRITE,8)
8 FORMAT (1X,/,1X,127(0-))
RTUPN
END

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```

SUBROUTINE CBC10(NRADX,NFORX,XFUS,SFUS)
C*** INPUTS AND INITIALIZES CONFIGURATION DESCRIPTION
COMMON /PASS/ABC(20),ABCDE(20),HORZ, VERT,TEST1,PHI,THETA,PSI,XF,YF,
1ZF,DIST,FMAG,PLOTSZ,TYPE,XMIN,XMAX,YMIN,YMAX,ZMIN,ZMAX,XMID,YMID,
1ZMID,BIGD,KODE,ISP
COMMON /INGUT/JREAD,JWRITE,JPUNCH,KFILE1,KFILE2,KFILE3,KFILE4,IWRI
1TE
1 DIMENSION XFUS(NFORX),SFUS(NFORX,2)

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C
COMMON /AV/ALRT(212,3,2),VECRT(211,3)
COMMON /PCODE/LCODE
REWIND KFILE1
REWIND KFILE2
REWIND KFILE4
LREAD=KFILE1
IF (LCODE.NE.1) LREAD=KFILE4
NRAD=NRADX
NFUSOR=NFORX
N=NFUSCR
READ (LREAD)(XFUS(1),I=1,N)
IF (IWRITE.EQ.0) WRITE (JWRITE,1) (XFUS(I),I=1,N)
1 FORMAT (1X,F10.5,1X,F10.5,1X,F10.5,1X,F10.5,1X,F10.5,1X,F10.5)
IF (IWRITE.EQ.0) WRITE (JWRITE,2)
2 FORMAT (1X,/)
DO 4 NN=1,N
DO 3 K=1,2
READ (LREAD)(SFUS(NN,MM,K),MM=1,NRAD)
IF (IWRITE.EQ.0) WRITE (JWRITE,1) (SFUS(NN,MM,K),MM=1,NRAD)
3 CONTINUE
IF (IWRITE.EQ.0) WRITE (JWRITE,2)
4 CONTINUE
XMIN=XFUS(1)
XMAX=XFUS(1)
YMAX=SFUS(1,1,1)
ZMIN=SFUS(1,1,2)
ZMAX=SFUS(1,1,2)
XMIN=AMINI(XMIN,XFUS(1))
XMAX=AMAXI(XMAX,XFUS(NFUSOR))
DO 5 NN=1,NFUSOR
DO 5 NR=1,NRAD
YMAX=AMAXI(YMAX,SFUS(NN,NR,1))
ZMIN=AMINI(ZMIN,SFUS(NN,NR,2))
ZMAX=AMAXI(ZMAX,SFUS(NN,NR,2))
5 SETUP 1ST LINE IN STREAMWISE DIRECTION
C***
NL1=NFUSOR-1
NAN=NRAD
DO 6 N=1,NFUSOR
ALRT(N,1,2)=XFUS(N)
ALRT(N,2,2)=SFUS(N,1,1)
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YSAV=YMIN
ZSAV=ZMIN
XMSAV=XMAX
YMSAV=YMAX
ZMSAV=ZMAX
IF (TYPE.NE.TYPEV) GO TO 5
SCALF=BIGD/PLOTSZ
ORG(1)=PHI
ORG(2)=THETA
ORG(3)=PSI
PHI=0.
THETA=0.
PSI=0.
YBIG=ORG(1)
YORG=FLD(1,IFIX(YMAX/SCALE))+ORG(1)
IF (YBIG.GT.ORG(2)) GO TO 1
YBIG=ORG(2)
YORG=FLD(2,IFIX(ZMAX/SCALE))+ORG(2)
IF (YBIG.GT.ORG(3)) GO TO 2
YBIG=ORG(3)
YORG=FLD(3,IFIX(ZMAX/SCALE))+ORG(3)
CALL CALPL1(2.0,YORG,-3)
NOTATE ON 3VIEW PLOTS
NCHAR=IFIX(6.*PLOTSZ)
IF (NCHAR.GT.80) GO TO 3
X=0.
GO TO 4
3 ND IF=(NCHAR-8)/2
X=FLC(1,NDIF)/5.
NCHAR=80
4 CALL NOTATE(X,0.,.2,ASC,0.,NCHAR)
YMIN=0.
ZMIN=0.
HORIZ=X1
VERT=Y1
YORG=CRG(1)-YORG-1
CALL CALPL1(0.,YORG,-3)
CALL CDC21(NRADX,NFORX)
REWIND KFILE2
VERT=Z1
YORG=ORG(2)-ORG(1)

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CALL CALPLT(0.,YORG,-3)
CALL CBC21(NRADX,NFORX)
REWIND KFILE2
HORZ=Y1
YORG=ORG(3)-ORG(2)
YMIN=FLOAT(IFIX(YSAV/SCALE))*SCALE
CALL CALPLT(0.,YORG,-3)
CALL CBC21(NRADX,NFORX)
X=FLOAT(IFIX(PLOTSZ+6.))
Y=1.-ORG(3)
GO TO 9
5 IF (TYPE.EQ.TYPES) GO TO 7
C*** NOTATE ID CN PLOT
X=0.
NCHAR=IFIX(11.*PLOTSZ)+3
IF (NCHAR.LE.80) GO TO 6
ND IF=(NCHAR-80)/2
X=FLOAT(NDIF)/11.
NCHAR=80
6 CALL NOTATE(X,.5..1,ABC.0.,NCHAR)
CALL NOTATE(X,0..1,ABCDE.0.,NCHAR)
7 IF (TYPE.EQ.TYPES.OR.TYPE.EQ.TYPES) GO TO 8
C*** ORTHOGRAPHIC
CALL CBC21(NRADX,NFORX)
X=FLOAT(IFIX(PLOTSZ+2.))
Y=-3.
GO TO 9
8 ISPE=1
IF (TYPE.EQ.TYPES) ISPE=2
C*** PERSPECTIVE OR STEREO
CALL CBC22(NRADX,NFORX)
X=PLOTSZ+2.
IF (TYPE.EQ.TYPES) X=X+PLOTSZ
Y=-3.
END OF COMPLETE PLOT
9 CALL CALPLT(X,Y,-3)
C*** RESTORE MIN AND MAX
XMIN=XSAV
YMIN=YSAV
ZMIN=ZSAV
XMAX=XMSAV

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C20 101
C20 102
C20 103
C20 104

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YMAX=ZMSAV
ZMAX=ZMSAV
RETURN
END

SUBROUTINE CBC21(NRADX,NFORX)

CONTROL ROUTINE FOR ORTHOGRAPHIC PROJECTIONS

COMMON /PASS/ABC(20),ABCDE(20),HORZ,VERT,TEST1,PHI,THETA,PSI,XF,YF,
1,ZF,DIST,FMAG,PLOTSZ,TYPE,XMIN,XMAX,YMIN,YMAX,ZMIN,ZMAX,XMID,YMID,
2,MID,BIGD,KCDE,ISP
DIMENSION C(3)
COMMON /DPLT/ALINE(212,3),RLINE(212,2),RVEC(211,2),PLINE(212,2),A(
12,3),NNUM(10)
DATA XSEE/2HX /,YSEE/2HY /,XINTST/3HOUT/,CCNV/.017453293/
DATA HVU3/3HVU3/

INITIALIZE
ITEST1=1
DMAX=BIGD
ITEST2=1
IF (XINTST.NE.TEST1)ITEST1=0
IF (PSI.EQ.0..AND.THETA.EQ.0..AND.PHI.EQ.0..)ITEST2=0
SCALF=DMAX/PLOTSZ

PHI=CCNV*PHI
THETA=CCNV*THETA
PSI=CCNV*PSI
IF (TYPE.EC.HVU3) GO TO 1
XDIS=XMAX-XMIN
YDIS=YMAX-YMIN
ZDIS=ZMAX-ZMIN
XFIX=.5*(DMAX-XDIS)
XMIN=XMIN-XFIX
YFIX=.5*(DMAX-YDIS)
YMIN=YMIN-YFIX
ZFIX=.5*(DMAX-ZDIS)
ZMIN=ZMIN-ZFIX

C**
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C**
C

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I TEST=2
C(1)=COSTHE*SINPSI
C(2)=COSPSI*COSPHI+SINTHE*SINPSI*SINPHI
C(3)=-COSPSI*SINPHI+SINTHE*SINPSI*COSPHI
GO TO 16
15 ITEST=1
C(1)=COSTHE*COSPSI
C(2)=-SINPSI*COSPHI+SINTHE*COSPSI*SINPHI
C(3)=SINPSI*SINPHI+SINTHE*COSPSI*COSPHI
C** CENTER WITHIN PAGE SIZE IF SIZE GREATER THAN 28 INCHES
16 IF (PLTJZ.GT.28..AND.TYPE.NE.FVU3)VMIN=-13.*SCALE+FLOAT(IFIX(VMID
1/SCALE))*SCALE
C** ROTATE MIDPOINT TO PLACE ROTATED VIEW CORRECTLY
IF (ITEST2.FO.0) GO TO 17
AMID1=A(1,1)*XMID+A(1,2)*YMID+A(1,3)*ZMID
AMID2=A(2,1)*XMID+A(2,2)*YMID+A(2,3)*ZMID
HMIN=HMIN-HMID+AMID1
VMIN=VMIN-VMID+AMID2
C** BEGIN PLOTTING LINES
17 CALL PLOTTI(NRADX,NFORX,ITEST,ITEST1,ITEST2,IHORZ,IVERT,HMIN,VMIN,
1SCALE,C)
CALL PLOTTI(NFORX,NRADX,ITEST,ITEST1,ITEST2,IHORZ,IVERT,HMIN,VMIN,
1SCALE,C)
RETURN
END

```

```

SUBROUTINE PLOTTI(NL,NPT,ITEST,ITEST1,ITEST2,IHORZ,IVERT,HMIN,VMIN
1,SCALE,C)
C** READS LINES OF POINTS DEFINING A SURFACE FROM DISK, MANIPULATES IN
C** SPECIFIED MANNER, AND PLOTS
C
COMMON /INOUT/JREAD,JWRITE,JPUNCH,KFILF1,KFILE2,KFILF3,KFILE4,IWRI
1TE
DIMENSION VECRI(211,3,2),VECLF(211,3,2),XLINC(214,2),C(3)
COMMON /DPLT/ALINE(212,3),RLINE(212,2),RVFC(211,2),PLINE(212,2),A(
12,3),NNUM(10)
C
NVFC=NPT-1
DO 31 N=1,NL

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C21 120
C21 121
C21 122
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C21 124
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C21 143
C21 144

PLT 1
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26 RVEC(M,N2)=-RVEC(M,N2)
27 IF (NSET.EQ.0) GO TO 30
C*** SCALE AND PLOT
NIT=0
DG 29 NI=1,NSET
NN=NNUM(N1)
DG 28 NN1=1,NN
NIT=NIT+1
XLINE(NN1,1)=PLINE(NIT,1)
XLINE(NN1,2)=PLINE(NIT,2)
28 CONTINUE
XLINE(NN+1,1)=HMIN
XLINE(NN+1,2)=VMIN
XLINE(NN+2,1)=SCALE
XLINE(NN+2,2)=SCALE
CALL LINE(XLINE(1,1),XLINE(1,2),NN,1,0,0,0)
29 CONTINUE
30 CONTINUE
31 RETURN
END

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SUBROUTINE VISTST(KUDE,NPT,NSET)
C*** TESTS A LINE OF POINTS FOR VISIBILITY
COMMON /DPLT/ALINE(212,3),RLINE(212,2),RVEC(211,2),PLINE(212,2),A(
12,3),NNUM(13)
C
IWRITE=0
IF (NPT.EQ.81.OR.NPT.EQ.85)IWRITE=1
NVEC=NPT-1
NPLT=0
NSET=0
ICOUNT=0
GO TO (1,2,3),KUDE
1 N1=1
N2=2
GO TO 4
2 N1=1

```


ORIGINAL PAGE IS
OF POOR QUALITY

19 VIS
20 VIS
21 VIS
22 VIS
23 VIS
24 VIS
25 VIS
26 VIS
27 VIS
28 VIS
29 VIS
30 VIS
31 VIS
32 VIS
33 VIS
34 VIS
35 VIS
36 VIS
37 VIS
38 VIS
39 VIS
40 VIS
41 VIS
42 VIS
43 VIS
44 VIS
45 VIS
46 VIS
47 VIS
48 VIS
49 VIS
50 VIS
51 VIS
52 VIS
53 VIS

1 PTR
2 PTR
3 PTR
4 PTR

```

N2=1
GO TO 4
3 N1=2
  N2=2
  DO 13 N=1,NPT
  IF (N.EQ.1) GO TO 6
  IF (N.EQ.NPT) GO TO 8
  DO 5 NN=N1,N2
  IF ((RVFC(N-1,NN).GT.0.).OR.(RVFC(N,NN).GT.0.)) GO TO 12
5 CONTINUE
GO TO 10
6 DO 7 NN=N1,N2
  IF (RVFC(1,NN).GT.0.) GO TO 12
7 CONTINUE
GO TO 10
8 DO 9 NN=N1,N2
  IF (RVFC(NVFC,NN).GT.0.) GO TO 12
9 CONTINUE
POINT NOT VISIBLE
C** 10 IF (ICOUNT.LE.1) GO TO 11
  NSET=NSET+1
  NNUM(NSSET)=ICOUNT
11 ICOUNT=0
  GO TO 13
C** 12 POINT IS VISIBLE
  NPLT=NPLT+1
  ICOUNT=ICOUNT+1
  PLINE(NPLT,1)=RLINE(N,1)
  PLINF(NPLT,2)=RLINE(N,2)
13 CONTINUE
  IF (ICOUNT.LE.1) GO TO 14
  NSET=NSET+1
  NNUM(NSSET)=ICOUNT
14 RETURN
END

```

SUBROUTINE PIRGT(NPT)
ROTATES AND PROJECTS A SET OF 3-D POINTS

ORIGINAL PAGE IS
OF POOR QUALITY

```

COMMON /DPLT/ALINE(212,3),RLINE(212,2),RVEC(211,2),PLINE(212,2),A(
12,3),NNUM(10)
DO 2 N=1,NPT
PLINE(N,1)=0.
RLINE(N,2)=0.
DO 1 I=1,2
DO 1 J=1,3
RLINE(N,1)=RLINE(N,1)+A(I,J)*ALINE(N,J)
1 CONTINUE
2 RETURN
END

```

5 PTR
6 PTR
7 PTR
8 PTR
9 PTR
10 PTR
11 PTR
12 PTR
13 PTR
14 PTR
15 PTR
16 PTR
17 PTR

```

SUBROUTINE VECROT(NVEC,C,FVEC,RVEC)
TRANSFORMS VECTORS
DIMENSION C(3),FVEC(211,3),RVEC(211)
DO 2 N=1,NVEC
SUM=0.
DO 1 NN=1,3
SUM=SUM+C(NN)*FVEC(N,NN)
2 RVEC(N)=SUM
RETURN
END

```

1 VEC
2 VEC
3 VEC
4 VEC
5 VEC
6 VEC
7 VEC
8 VEC
9 VEC
10 VEC
11 VEC
12 VEC
13 VEC

```

SUBROUTINE CBC22(NRADX,NFORX)
CONTROL ROUTINE FOR PERSPECTIVE AND STEREO
COMMON /PASS/ABC(20),ABCDF(20),HORZ,VERT,TEST1,PHI,THETA,PSI,XF,YF,
1,ZF,DIST,FMAG,PLCTSZ,TYPE,XMIN,XMAX,YMIN,YMAX,ZMIN,ZMAX,XMID,YMID,
1ZMID,BIGC,KODE,ISP
COMMON /INCUT/JREAD,JWRITE,JPUNCH,KFILE1,KFILE2,KFILE3,KFILE4,IWRI
1TE
DIMENSION XINIT(2),YINIT(2),ZINIT(2)

```

1 C22
2 C22
3 C22
4 C22
5 C22
6 C22
7 C22
8 C22
9 C22
10 C22

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C22

```

XINIT(1)=PHI
XINIT(2)=XF
YINIT(1)=YHETA
YINIT(2)=YF
ZINIT(1)=PSI
ZINIT(2)=ZF
CALL STERPT(XINIT,YINIT,ZINIT,0.1,0.3, PLOTSZ,DIST,FMAG)
LOOP FOR RIGHT AND LEFT FRAMES
DO 1 IC=1,ISP
  REWIND KFILE2
  NCI=-IC
  BEGIN PLOTTING LINES
  CALL PLOT3(NRADX,NFORX,PHI,THETA,PSI,XF,YF,ZF,PLOTSZ,DIST,FMAG,NC
1)
  CALL PLOT3(NRADX,NRADX,PHI,THETA,PSI,XF,YF,ZF,PLOTSZ,DIST,FMAG,NC
1)
1) CONTINUE
1) RETURN
END
  
```

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STE
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SUBROUTINE STERPT(X,Y,Z,N,K,NC,IP,PAG,PLA,XPR)
PLOTS STEREO      (PROGRAMMER - GEORGE C. SALLEY)
DIMENSION VP(3),TRAN(3),SANG(3),CANG(3),ADJ(3),PT(4),XLP(2),ZLP(2)
DIMENSION X(1),Y(1),Z(1)
DIMENSION PLX(4),PLY(4),PLZ(2)
DIMENSION PIX(4),PIY(4),PIZ(2)
DIMENSION ILP(4),IPL(4)
DATA PI,PI2,PI32,PI42/3.1415926,1.5707963,4.7123889,6.2831952/
DATA PAP/1.125/
DATA NPG/0/
DATA NPT/1/
DATA FRAME/9.80/
DATA TJRN/11.01/
NC=1
KK=K
II=IP
  
```

ORIGINAL PAGE IS
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20 STE
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49 STE
50 STE
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52 STE
53 STE
54 STE
55 STE
56 STE
57 STE
58 STE
59 STE
60 STE
61 STE

```
IF (NC) 16.1.22
1 NP=N*K+1
  NR=NP+K
  PLIM=PAG/2.
  SF=XPR
  VPL=PLA
  DO 2 I=1.4
    PLX(I)=0.
    PLY(I)=0.
    PIX(I)=0.
    PIY(I)=0.
  IPL(I)=0
2 DO 3 I=1.2
  PLZ(I)=0.
3 PIZ(I)=0.
  VPX=X(NP)
  VPY=Y(NP)
  VPZ=Z(NP)
  FPX=X(NR)
  FPY=Y(NR)
  FPZ=Z(NR)
  VX=VPX-FPX
  VY=VPY-FPY
  VZ=VPZ-FPZ
  VP(2)=SQRT((VX**2)+(VY**2))
  VP(3)=SQRT((VZ**2)+(VP(2)**2))
  TRAN(1)=VPX-(VPL*(VX/VP(2)))
  TRAN(2)=VPY-(VPL*(VY/VP(2)))
  TRAN(3)=VPZ-(VPL*(VZ/VP(3)))
  VANG=ATAN(PAR/VP(3))
  IF (VX) 11.4.7
  IF (VY) 6.6.5
4 PANG=PI/2
5 GO TO 15
6 PANG=PI/32
7 GC TO 15
8 IF (VY) 10.8.9
9 PANG=0.
10 PANG=ATAN((VY/VX))
11 GO TO 15
```

ORIGINAL PAGE IS
OF POOR QUALITY

62 STE
63 STE
64 STE
65 STE
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67 STE
68 STE
69 STE
70 STE
71 STE
72 STE
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74 STE
75 STE
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77 STE
78 STE
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80 STE
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82 STE
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101 STE
102 STE
103 STE

```
10 PANG=PI42-ATAN(((ABS(VY))/VX))
11 GO TO 15
12 IF (VY) 14,12,13
13 PANG=PI
14 GO TO 15
15 PANG=PI-ATAN((VY/(ABS(VX))))
16 PANG=PI+ATAN(((ABS(VY))/ABS(VX))))
17 PANG=PI32-PANG
18 UANG=PANG*(2.*VANG)
19 SANG(1)=SIN(UANG)
20 SANG(2)=COS(UANG)
21 CANG(1)=COS(UANG)
22 CANG(2)=SIN(UANG)
23 SANG(3)=VP(2)/VP(3)
24 CANG(3)=VPL
25 XLP(1)=0.
26 ZLP(1)=0.
27 XLP(2)=FRAME
28 ZLP(2)=0.
29 ADJ(1)=PLIM
30 ADJ(2)=PLIM
31 ADJ(3)=ADJ(2)+FRAME
32 IF (N) 60,60,22
33 M=IABS(NC)
34 L=M
35 IF (NPG+NC) 23,17,23
36 IF (2+NC) 60,19,18
37 NPG=2
38 GO TO 20
39 NPG=1
40 DO 21 I=1,L
41 CALL CALPLT(TURN,0.,-3)
42 CONTINUE
43 CALL CALPLT(XLP(M),ZLP(M),3)
44 M=1
45 L=2
46 DO 59 I=M,L
47 IF (NPG) 60,24,30
48 IF (NC) 25,29,29
```

104 STE 104
105 STE 105
106 STE 106
107 STE 107
108 STE 108
109 STE 109
110 STE 110
111 STE 111
112 STE 112
113 STE 113
114 STE 114
115 STE 115
116 STE 116
117 STE 117
118 STE 118
119 STE 119
120 STE 120
121 STE 121
122 STE 122
123 STE 123
124 STE 124
125 STE 125
126 STE 126
127 STE 127
128 STE 128
129 STE 129
130 STE 130
131 STE 131
132 STE 132
133 STE 133
134 STE 134
135 STE 135
136 STE 136
137 STE 137
138 STE 138
139 STE 139
140 STE 140
141 STE 141
142 STE 142
143 STE 143
144 STE 144
145 STE 145

```

25 IF (NPT+NC) 30,26,30
26 IF (2+NC) 60,28,27
27 NPT=2
28 GO TO 29
29 NPT=1
30 CALL CALPLY(XLP(1),ZLP(1),3)
31 DO 58 J=1,N
32 PT(1)=((X(NO)-TRAN(1))*CANG(1))-((Y(NO)-TRAN(2))*SANG(1))
33 PT(2)=((X(NO)-TRAN(1))*SANG(1))+((Y(NO)-TRAN(2))*CANG(1))
34 PT(3)=((PT(4)*CANG(3))-((Z(NO)-TRAN(3))*SANG(3)))
35 PT(4)=((PT(4)*SANG(3))+((Z(NO)-TRAN(3))*CANG(3)))
36 IF (PT(2)) 31,36,36
37 IF (ILP(1)) 60,32,35
38 IF (I1-3) 33,34,60
39 VX=PLX(1)-PT(1)
40 VY=PLY(1)-PT(2)
41 VZ=PLZ(1)-PT(3)
42 VP(1)=SQRT((VX**2)+(VY**2))
43 VP(2)=SQRT((VZ**2)+(VP(1)**2))
44 VPL=PLY(1)/(VY/VP(1))
45 PT(4)=PLX(1)-((VX/VP(1))*VPL)
46 PLX(1)=PT(1)
47 PT(1)=PT(4)
48 PLY(1)=PT(2)
49 PT(2)=0.
50 PT(4)=PLZ(1)-((VZ/VP(2))*VPL)
51 PLZ(1)=PT(3)
52 PT(3)=PT(4)
53 ILP(1)=1
54 GO TO 41
55 ILP(1)=1
56 PLX(1)=PT(1)
57 PLY(1)=PT(2)
58 PLZ(1)=PT(3)
59 GO TO 54
60 IF (ILP(1)) 60,40,37
61 IF (I1-3) 38,39,60
62 I1=3
63 IPL(1)=1
64 PIX(1)=PT(1)
65 PIY(1)=PT(2)
66 PIZ(1)=PT(3)

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ORIGINAL PAGE IS
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146 STE 146
147 STE 147
148 STE 148
149 STE 149
150 STE 150
151 STE 151
152 STE 152
153 STE 153
154 STE 154
155 STE 155
156 STE 156
157 STE 157
158 STE 158
159 STE 159
160 STE 160
161 STE 161
162 STE 162
163 STE 163
164 STE 164
165 STE 165
166 STE 166
167 STE 167
168 STE 168
169 STE 169
170 STE 170
171 STE 171
172 STE 172
173 STE 173
174 STE 174
175 STE 175
176 STE 176
177 STE 177
178 STE 178
179 STE 179
180 STE 180
181 STE 181
182 STE 182
183 STE 183
184 STE 184
185 STE 185
186 STE 186
187 STE 187

```
VX=PT(1)-PLX(1)
VY=PT(2)-PLY(1)
VZ=PT(3)-PLZ(1)
VP(1)=SQRT((VX**2)+(VY**2))
VPL=PT(2)/(VY/VP(1))
PT(2)=0.
PT(1)=PT(1)-((VX/VP(1))*VPL)
PT(3)=PT(3)-((VZ/VP(2))*VPL)
39 ILP(1)=0
40 PLX(1)=PT(1)
41 PLY(1)=PT(2)
42 PLZ(1)=PT(3)
43 XP=(PT(1)+(PT(2)*(-PT(1))/(PT(2)+VP(3))))*SF
44 ZP=(PT(3)+(PT(2)*(-PT(3))/(PT(2)+VP(3))))*SF
45 VPL=SQRT((XP**2)+(ZP**2))
46 IF (VPL-PLIM) 47,47,42
47 IF (ILP(1+2)) 60,43,46
48 IF (I1-3) 44,45,60
49 PLY(1+2)=XP
XP=PLIM*(XP/VPL)
ZP=PLIM*(ZP/VPL)
ILP(1+2)=1
60 TO 53
45 ILP(1+2)=1
46 PLX(1+2)=XP
47 PLY(1+2)=ZP
60 TO 54
47 IF (ILP(1+2)) 60,51,48
48 IF (I1-3) 49,53,63
49 I1=3
IPL(1+2)=1
PLX(1+2)=XP
PLY(1+2)=ZP
VPL=SQRT((PLX(1+2)**2)+(PLY(1+2)**2))
XP=PLIM*(PLX(1+2)/VPL)
ZP=PLIM*(PLY(1+2)/VPL)
50 ILP(1+2)=0
60 TO 52
51 IF ((SQRT((PLX(1+2)**2)+(PLY(1+2)**2)))-PLIM) 52,52,48
52 PLX(1+2)=XP
```

ORIGINAL PAGE IS
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STE 188
STE 189
STE 190
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STE 207
STE 208
STE 209
STE 210

```

PLY(I+2)=ZP
53 XPT=XP+ADJ(I+1)
   YPT=ZP+ADJ(I)
   CALL CALPLT(XPT,YPT,II)
54 II=2      (IPL(I+2)) 60,56,55
55 IPL(I+2)=0
   ZP=PIY(I+2)
   GO TO 51
56 IF (IPL(I)) 60,58,57
57 IPT(1)=PIX(I)
   IPT(2)=PIY(I)
   IPT(3)=PIZ(I)
   GO TO 40
58 NC=NO+KK
   XLP(I)=XPT
   ZLP(I)=YPT
   NN=1
59 II=IP
60 RETURN
   END

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```

SUBROUTINE PLTIT3(NL,NPT,PHI,THETA,PSI,XF,YF,ZF,PLOTSZ,DIST,FMAG,N
1 CI)
C** READS LINES OF POINTS DEFINING A SURFACE FROM DISK
C COMMON /INOUT/JREAD,JWRITE,JPUNCH,KFILE1,KFILE2,KFILE3,KFILE4,IWRI
1TF
C DIMENSION ALINE(214,3)
C
C ALINE(NPT+1,1)=PHI
C ALINE(NPT+2,1)=XF
C ALINE(NPT+1,2)=THETA
C ALINE(NPT+2,2)=YF
C ALINE(NPT+1,3)=PSI
C ALINE(NPT+2,3)=ZF
C DO 5 N=1,NL

```


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C***      READ (KFILE2)((ALINE(NN,N3),NN=1,NPT),N3=1,3)
C***      IF (N.EQ.NL) GO TO 1
C***      SKIP VECTORS
C***      READ (KFILE2)VEC
C***      LOOP FOR RIGHT AND LEFT SIDE OF BODY
C***      DO 4 NN2=1,2
C***      IF (NN2.EQ.1) GO TO 3
C***      DO 2 NN=1,NPT
C***      ALINE(NN,2)=-ALINE(NN,2)
C***      CALL STERPT(ALINE(1,1),ALINE(1,2),ALINE(1,3),NPT,1,NCI,3,PLOTSZ,DI
C***      1ST.FMAG)
C***      4 CCNTINUE
C***      5 RETURN
C***      END

```

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PL3 17
PL3 18
PL3 19
PL3 20
PL3 21
PL3 22
PL3 23
PL3 24
PL3 25
PL3 26
PL3 27
PL3 28
PL3 29
PL3 30
PL3 31

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```

C***      SUBROUTINE CALPLT(A,B,I)
C***      IMPORTANT??
C***      THIS SUBROUTINE USES THE PLOTTER SOFTWARE AVAILABLE AT N. C. STATE
C***      UNIVERSITY (SUBROUTINES PLOT AND ORIGIN) TO REPRODUCE THE ACTIONS
C***      OF THE CALCOMP SOFTWARE SUBROUTINE CALPLT.
C***      IF THE USER DOES NOT HAVE THE ORIGINAL CALCOMP ROUTINE CALPLT
C***      AVAILABLE TO HIM, HE MUST WRITE A DUMMY SUBROUTINE, USING THE
C***      PLOTTER SOFTWARE AVAILABLE AT HIS INSTALLATION, WHICH WILL
C***      REPRODUCE THE ACTION OF CALPLT.
C***      DIMENSION A(1),B(1)
C***      IF (I.LT.0) GO TO 1
C***      J=I-2
C***      CALL PLOT(A,B,J)
C***      RETURN
C***      J=IABS(I)
C***      J=J-2
C***      CALL PLJT(A,B,J)
C***      CALL ORIGIN(A,B,1,0)
C***      RETURN

```

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CAL 1
CAL 2
CAL 3
CAL 4
CAL 5
CAL 6
CAL 7
CAL 8
CAL 9
CAL 10
CAL 11
CAL 12
CAL 13
CAL 14
CAL 15
CAL 16
CAL 17
CAL 18
CAL 19
CAL 20
CAL 21
CAL 22
CAL 23
CAL 24

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END
SUBROUTINE NOTATE(A,B,C,D,E,I)
  IMPORTANT??
  THIS SUBROUTINE USES THE PLOTTER SOFTWARE AVAILABLE AT N. C. STATE
  UNIVERSITY (SUBROUTINE SYMBOL) TO REPRODUCE THE ACTIONS OF THE
  CALCCMP SOFTWARE SUBROUTINE NOTATE.
  IF THE USER DOES NOT HAVE THE ORIGINAL CALCCMP ROUTINE NOTATE
  AVAILABLE TO HIM, HE MUST WRITE A DUMMY SUBROUTINE, USING THE
  PLOTTER SOFTWARE AVAILABLE AT HIS INSTALLATION, WHICH WILL
  REPRODUCE THE ACTION OF NOTATE.
  DIMENSION D(1),DD(21)
  DATA STOP/4H /
  J=1/4
  XI=1
  XE=XI/4
  IF ((XR-J).GT.0.1)J=J+1
  DO 1 K=1,J
  DD(K)=D(K)
  DD(J+1)=STOP
  CALL SYMGL(A,B,C,DD,E)
  RETURN
  END
  C
  C***
  C***
  C***
  C***
  C***
  C***
  C***
  C***
  C***
  C***
  C

```

CAL 25
 NOT 1
 NOT 2
 NOT 3
 NOT 4
 NOT 5
 NOT 6
 NOT 7
 NOT 8
 NOT 9
 NOT 10
 NOT 11
 NOT 12
 NOT 13
 NOT 14
 NOT 15
 NOT 16
 NOT 17
 NOT 18
 NOT 19
 NOT 20
 NOT 21
 NOT 22
 NOT 23
 NOT 24
 NOT 25
 NOT 26

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SUBROUTINE LINE(A,B,I,J,K,L,S)
  IMPORTANT??
  THIS SUBROUTINE USES THE PLOTTER SOFTWARE AVAILABLE AT N. C. STATE
  UNIVERSITY (SUBROUTINE PLOT) TO REPRODUCE THE ACTIONS OF THE
  CALCCMP SOFTWARE SUBROUTINE LINE.
  IF THE USER DOES NOT HAVE THE ORIGINAL CALCCMP ROUTINE LINE
  C
  C***
  C***
  C***
  C***
  C***
  C***
  C***
  C***
  C***
  C

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LIN 1
 LIN 2
 LIN 3
 LIN 4
 LIN 5
 LIN 6
 LIN 7
 LIN 8
 LIN 9

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AVAILABLE TO HIM, HE MUST WRITE A DUMMY SUBROUTINE, USING THE
PLCTTER SOFTWARE AVAILABLE AT HIS INSTALLATION, WHICH WILL
REPRODUCE THE ACTION OF LINE.

```
C**  
C***  
C***  
C  
C  
DIMENSION A(1),B(1),X(212),Y(212)  
XMIN=A(I+1)  
XSCALF=A(I+2)  
YMIN=B(I+1)  
YSCALE=B(I+2)  
DO 1 II=1,1  
X(II)=(A(II)-XMIN)/XSCALE  
Y(II)=(B(II)-YMIN)/YSCALE  
1 CALL PLOT(X,Y,1)  
RETURN  
END
```


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OF POOR QUALITY.

11.54179382	1.562499905	0.07289881	1	13	2	0
11.54179382	1.49169731	0.32289863	1	14	2	0
11.54179382	1.32915884	0.52289993	1	15	2	0
11.54179382	1.10619926	0.67290115	1	16	2	0
11.54179382	0.88330030	0.73960114	1	17	2	0
11.54179382	0.66670161	0.77089977	1	18	2	0
11.54179382	0.44370186	0.77710056	1	19	2	0
11.54179382	0.21670252	0.78129959	1	20	2	0
11.54179332	0.0	0.78129864	1	21	2	0
11.54179332	0.0	-1.87437125	1	1	3	3
10.87548828	0.21348673	-1.85611057	1	2	3	3
10.87548828	0.42911345	-1.81024837	1	3	3	3
10.87548828	0.63553590	-1.74978733	1	4	3	3
10.87548828	0.85405535	-1.66543198	1	5	3	3
10.87548828	1.24672909	-1.54464340	1	6	3	3
10.87548828	1.22386456	-1.37801647	1	7	3	3
10.87548828	1.35816660	-1.18529987	1	8	3	3
10.87548828	1.47383976	-0.97383112	1	9	3	3
10.87548828	1.56031990	-0.73745412	1	10	3	3
10.87548828	1.62289333	-0.48950770	1	11	3	3
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ADDITIONAL ARBITRARY STATION SPECIFICATIONS

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5	0	0	0	0
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7	0	0	0	0
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11	0	0	0	0
12	0	0	0	0
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16	0	0	0	0

NEW DATAD00

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OF POOR QUALITY

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