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LONG DURATION EXPOSURE FACILITY (LDEF) STRUCTUP & VERIFICATION TEST REPORT

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LONG DURATION EXPOSURE FACILITY (LDEF) STRUCTURAL VERIFICATION TEST REPORT

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SUMMAR Y

A series of structural load tests on the Long Duration Exposure Facility's (LDEF) primary structure have been conducted. These tests had a three-fold purpose: (1) demonstrate structural adequacy of the assembled LDEF primary structure when subjected to anticipated flight loads; (2) verify analytical models and methods used in loads and stress analysis; and (3) perform tests to comply with the Space Transportation System (STS) requirements.

Test loads were based on predicted limit loads considering all flight events. Simulation of these limit loads on specified structural elements was accomplished by applying discrete load sets to the LDEF. Monitored data consisted of load, both applied and reacted, strain, and deflection measurements.

Evaluation of the test results shows good agreement between predicted and observed load, strain, and deflection data. In addition, test data show that the LDEF structure was subjected to 1.2 times limit load to meet the STS requirements. The structural adequacy of the LDEF is demonstrated as a result of this test.

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INTRODUCTION

The LDEF has been developed by the NASA Office of Aeronautics and Space Technology and the Langley Research Center to accommodate a set of experiments which require a free-flying exposure in space. The experiments are totally self-contained in trays which are mounted on the facility structure.

The LDEF is delivered to Earth orbit by the Space Transportation System (STS) and placed in a gravity-gradient stabilized attitude by the STS remote manipulator system. After approximately 1 year in orbit, the LDEF is retrieved on a subsequent STS flight. After it is returned from space, the trays with experiments are removed and returned to the respective experimenters for post-flight inspection and analysis.

The design of the LDEF began in the mid-seventies, with a deployable weight of approximately 13,750 lbs. During this period, the size and arrangement of elements of the primary structure were selected. The majority of experiments consisted of relatively light debris experiments. More recently, the LDEF experiment manifest has changed to the current flight complement of many different types of experiments which, in general, weigh considerably more than the debris experiments. The current deployable weight is in excess of 21,000 lbs. During this time period, the load environments have matured. Coupled STS/LDEF transient analyses (references 1 and 2) have been performed which have allowed the structure to be evaluated from a loads/stress standpoint.

Structural testing is, in general, a convincing way to demonstrate structural adequacy. For LDEF, it is a culmination of activities, all of which were directed towards establishing confidence in the integrity of the structure. There are three interrelated verification test objectives. The first is to demonstrate that the LDEF structure can withstand anticipated flight loads. The second is to verify analytical models and methods used in

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the loads and stress analyses. The third is to comply with the Space Transportation System (STS) requirement which states, "Static test a flight article or equivalent to 1.2 times limit load and design to an ultimate factor of safety, such that detrimental permanent deformation is precluded."

Simulation of 1.2 times limit load on specified structural elements was accomplished by analytically investigating the application of discrete load sets. Four test set-ups which simulated the maximum flight loadings during lift-off, maneuvering, and landing were developed. The magnitude, direction, and placement of the applied test loads were determined for each.

All four test set-ups had similar instrumentation. Reacted and applied loads were recorded for all tests, and strain gage data were recorded for selected structural elements. Deflections were recorded at the LDEF/test support interface and at selected locations on the LDEF structure.

TEST ORGANIZATIONAL STRUCTURE

The organizational structure for the test, indicating the major responsibilities for each activity, is shown on figure 1.

The deployable LDEF consists of two distinct parts: (1) the primary structure (or facility) and (2) the trays containing the experiments. The structural verification test described herein was performed on the primary structure.

TEST ARTICLE

The LDEF facility consists of a structural framework whose cross-section is a 12-sided regular polygon. It is approximately 30 feet long and 14 feet in diameter. The structure (shown in fig. 2) is designed to house 72 tray/ experiments around its circumference and a total of 14 tray/experiments on the ends. The primary structure is made of aluminum, except for the steel trunnions and fasteners, and weighs about 8,500 pounds.

A schematic of the primary structure showing the basic structural components is shown in figure 3. The LDEF has five mechanical interfaces with the STS. There are two main trunnions reacting loads in the longitudinal and vertical directions. A keel trunnion reacts loads in the lateral direction. Finally, there are two end support beam trunnions reacting loads in the vertical direction.

The end frames are similar and consist of mechanically fastened 6-inch extruded I-beams. Tubular diagonal members (not shown) are mechanical links between the end frames and the center ring providing additional structural stiffness in both the vertical and horizontal planes. The end support beam (ESB), which consists of welded tubes and machined fittings, is on one end of the primary structure. It is free to rotate about a center spindle.

The center ring is fabricated in sections from two 10-inch extruded channels joined by welding 1/2-inch thick plates to form a "box." Sections of this box are welded to forgings, which provide structural ties for 24 mechanically fascened longerons, 12 on either side of the center ring. The two main trunnions are

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mechanically fastened to the center ring 14 inches above the horizontal plane of symmetry. In the plane of the center ring, 7-inch extruded I-beams (not shown) are used to provide rigidity. A 12-inch extruded I-beam (not shown) provides a mechanical link between the two main trunnions.

The twenty-four longerons are 7-inch extruded I-beams mechanically fastened to the end frames and center ring. They provide the mounting surface for the experiment trays in the longitudinal direction. The "T" sections, or intercostals, are mechanically fastened to the longerons and are the mounting surfaces for experiment trays in the circumferential direction.

TEST SET-UP DESCRIPTION

A special test support frame (fig. 4) was designed, fabricated, and erected in the LaRC Structures Dynamics Research Laboratory, Building 1293B. This frame, with the LDEF in place (fig. 5), simulated the LDEF/STS interfaces and was located over a massive test floor adjacent to a backstop. Figure 6 illustrates the general layout of the LDEF test facility and associate. equipment. The hydraulic load maintainers (fig. 7) and data acquisition system (DAS) (fig. 8) were operated from the adjacent Control Room. The hydraulic load maintainers were operated from a single control point by a single operator. A pneumatically operated load dump control was provided to facilitate emergency shutdown of the system. The pallet-mounted hydraulic pump (fig. 9) was located in the test bay with hard lines connecting it to the load maintainers in the Control Room. Remote controls for the pump were located at a single point in the Control Room. Flex hoses connected the hydraulic load maintainers, through interface manifolds, to the appropriate hydraulic loading cylinders. The majority of these cylinders were attached directly to the floor and to the floor-mounted center beam (fig. 10). The DAS, located in the Control Room,

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was connected to the LDEF instrumentation sensors through interface boxes (fig. 11) located in the test cell. The acoustic emission monitoring system (fig. 12) was separately located. Visual monitoring of the tests was performed using two remotely operated TV systems and through a shatter-proof window in the Control Room. Two-way voice communication was provided between seven of the test team members.

LOAD APPLICATION TRAIN

A typical test load application train for dual tension type load inputs to the LDEF structure is depicted on figure 13. It consisted of a hydraulic cylinder attached to the floor or backstop with a swivel eye and connected to a load cell or load link with an appropriate adapter. The load cell was connected to a yoke arrangement by structural chain, the latter used primarily to preclude rotation under load as would be encountered when using steel cable. The yoke arrangemment consisted of cable or structural chain attached to a spreader bar and polyester straps wrapped around specific LDEF joints and attached to the spreader bar. Rubber pads were placed between the polyester straps and the LDEF structure to protect the surface finish, eliminate slippage, and better distribute the load. This loading arrangement precluded the need for any structural modifications to the LDEF. Where necessary, adjustable reinforcing blocks were utilized to prevent the load strap from overloading unsupported flanges on some structural elements.

Various quantities, types, and sizes of hydraulic cylinder and load cell/ load link were used during the tests as specified in tables I(a) through I(d). These tables illustrate locations of the LDEF load input by symbol and instrumentation signal conditioner channel number. Details of the load input and application trains are also listed. All elements of the load application

trains were certified prior to test initiation. Each hydraulic cylinder and load cell/load link combination was calibrated in a vertical position prior to test initiation to establish pressure levels used in each load maintainer channel. Since some of these load application trains were inclined to the vertical when in use, the actual load readings provided by the DAS were used for controlling and individually adjusting loads. Hydraulic pump supply pressure was adjusted as necessary during incremental loading to maintain a pressure 200-300 psig above that required at a given loading step.

INSTRUMENTATION

The instrumentation objectives included assuring that the proper loading conditions on the LDEF structure were achieved; that resulting loads, stresses, strains, deflections, and angular displacements were accurately measured; and that the information was permanently recorded. All instrumentation, except the strain gages, were separately calibrated against known, traceable standards. Standard gage factors were used for the stain gage instrumentation.

Deflectometers

The deflectometers used were MOXON Inc. model 1111-703-031 linear potentiometers precalibrated at 10-VDC over a range of 3 or 6 inches depending on the intended location. They were mounted in the test facility (typical mounting shown in fig. 14(a)) at various locations and attached (fig. 14(b)) to the LDEF or its support structure by cable, swivel-eye arrangements to measure x, y, and z displacements resulting from application of loads. Table II illustrates the attachment points on the LDEF and lists the instrumentation signal conditioner channel number and measurement direction. Also listed are the locations of attachments per the LDEF standard location designation (fig. 15), gage identification number, and reference voltage at the gage. For example,

from table II, the location of signal conditioner channel number D-7 is stated as "920 FL-A x." This represents LDEF location 920F (fig. 15) at the mid-point between L and A (end view) with movement measured in the x-direction. Also listed are instrumentation channels D-37 through 48 which represent the reference deflectometers used to measure any movement of the test structure near the four trunnion mounts. To avoid any modifications of the LDEF structure, deflectometers were attached to bolts placed in existing experiment tray mounting holes nearest the desired measurement location.

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Load Cells

The number, type, and range of load cells varied for each of the four tests. Each load cell was precalibrated at 10-VDC in tension and/or compression. Tables I(a) through I(d) illustrate the load input/output locations that utilized load cells. Dual load inputs resulted from single hydraulically produced and monitored load sources that were equally split through a bridle arrangement (fig. 13). The angular direction at each load input was mechanically measured at the 20 or 40 percent loading steps during each test so that its force components could be correctly resolved by the computer. Figures 16(a) through 16(d) illustrate the approximate LDEF test facility load input attachment points for the four tests. The position of the backstop with relation to LDEF is also depicted along with the location of the beams on the floor. The numbered symbols relate to the instrumentation signal conditioner "A" channel numbers.

Table I(a) shows, that for the landing load test, 22 load cells were used to measure 34 load inputs and 2 reactions. Tabulated are the channel numbers for instrumentation hook-up; type, location on LDEF, and orientation of input load; load cell capacity, identification, and supply voltage; and type and size of hydraulic cylinder. Maximum hydraulic pump supply pressure is also stated for the 100 percent test loading condition. For example, signal

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conditioner channel A-29 represents a single load input where location is stated as "911CH xz." From figure 15, this corresponds, to ocation 911C at joint H (end view) loaded toward the ESB in the x-z plane. The angle of this load, as measured from the horizontal, was 70° in the x-z plane and 85° in the y-z plane. A 10K tension measuring load link, identified as L10-6, was used to measure a maximum anticipated load of 7.2K. It had a measured reference voltage of 10.534 VDC. Signal conditioner channel A-47 is A-29's counterpart on the opposite side of the LDEF structure.

Strain Gages

All strain gages used were single axis Micro-Measurement model CEA-13-250UW-350. In only eleven instances, (center ring and diagonals) were the output of two gages combined to provide a single measurement.

<u>Main trunnions</u>. - Four strain gages were attached 90° apart on the two main trunnions, as shown in figure 17, to measure LDEF reaction loads. Each main trunnion was separately calibrated in bending in a special set-up (fig. 18) using a calibrated load cell. The trunnion being tested was rotated (0°, 90°, 180°, and 270°) in the fixture such that scrain gages were calibrated in tension, compression, and a neutral position depending on their orientation relative the load input. These calibration values were input to the DAS computer program to calculate trunnion reaction loads during the four tests. The trunnion was also oriented at an angle and calibrated to simulate combined x-z loading.

LDEF structure. - The remaining 81 strain gages were located on representative LDEF members where analytical analysis indicated higher strains could be anticipated (e.g., center ring members adjacent to the main trunnions, longeron sections near the center ring and main trunnions, diagonal sections near the center ring, and portions of the ESB). These lucations are noted on figures 19(a) through 19(h). Specific values for dimensions A through F shown

on figures 19(a) through 19(d) are listed in table III. The figures list the LDEF member on which particular gages are located, the strain gage number, the instrumentation signal conditioner channel number, and the LDEF location identifier. In this instance, the location identifier (fig. 15) becomes more complex. For example, from figure 19(a), strain gage number 37 is located on the side of the center ring (station 911D) away from the ESB, between joints C and B. It is at section "A" on the outside face (0) of the member.

Angle of Attack Indicators

The four angle-of-attack indicators (AOAI's) used were Sundstrand model no. 2000, capable of routinely measuring up to 30° angular change about their longitudinal axis with an accuracy of \pm .J1°. One pair, oriented 90° to each other, were mounted on a plate attached to the end of the right main trunnion (fig. 17) to measure LDEF pitching motions and apparent bending of the main trunnions in the vertical plane. A reference pair of AOAI's, similarly oriented, were mounted on the test support structure, as close to the first pair as possible, to indicate any test structure induced motions.

Pressure Gages

Up to 20 hydraulic cylinders were simultaneously used to provide load inputs to the LDEF structure. Heise MDL H dial pressure gages (fig. 7), calibrated to 3000 psi, were attached in the lines connecting the hydraulic load maintainers to the tension and compression sides of each hydraulic cylinder. Anticipated maximum pressure for maximum load was marked on each gage during pre-test calibration and checkout operations. Pressure was monitored, but not recorded, during test operations.

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Acoustic Emission Monitoring

The major components of the acoustic emission monitoring system are depicted on figure 12. During the first three tests, an interlocking series of acoustic arrays was established around the exterior circumference of the center ring. Each array consisted of four high-sensitivity sensors with a center resonant frequency of 150 kHz. A typical installation is shown on figure 20. The risetime, duration, peak amplitude, and location of acoustic events were recorded. For the last test, some of the sensors were repositioned to monitor the ESB.

DATA ACQUISITION SYSTEM DESCRIPTION

The DAS (fig. 21) consisted of 200 data channels feeding four identical 50-channel signal conditioning chassis, each of which had its own regulated power supply. These four units were connected to two HP-3497A 100-channel data acquisition control units (scanners). The scanners, in t m, were attached to a HP-9845 computer combined with a HP-9872A plotter. During test operations, the computer could activate two separate alarms through a HP-59306A relay actuator to indicate either an out-of-limits condition (buzzer) or an overload condition (horn). In the run mode, the HP-9845's cathode ray tube (CRT) continuously displayed an update of 40 consecutively-scanned channels of selected information. These 40 channels included all input and interface reaction loads plus selected strain gage and deflectometer signals. During any scanning process, if the scanned channel were determined to be in an outof-limit condition, its associated data would be presented on the CRT in a flashing mode and the buzzer would sound. If an overload condition were found to exist during the scan function, that data would appear on the CRT in inverse video and the horn would sound. When scanning all 200 channels, if cut-of-limit or overload conditions were found to exist, again the buzzer or horn would

sound. The anticipated levels for out-of-limit and overload conditions were preprogrammed. The out-of-limit level incorporated a sliding set-point which was always greater than the expected test reading by an amount equal to 10 percent of the expected maximum test value. The overload level was set at 110 percent of maximum expected load value. Several out-of-limit indications occurred and these required assessment and adjustment as necessary of the loading method, instrumentation installation, or anticipated load. An overload condition required immediate dumping of the load followed by an adjustment.

At the maximum condition and incremental loading steps, the DAS operator would command the computer's thermal printer to provide a permanent copy of the 40-channel or the complete 200-channel data, and command the computer to store the raw and reduced data on the computer's two data tapes. The printouts also presented a bar chart showing the data as a percent of maximum anticipated value. The computer also presented compari ons between input and reaction loads for total resolved components and moments about each LDEF axis. The 200 channels consisted of 78 deflectometers, up to 22 load cells, 89 strain gages, 4 angle-of-attack indicators, 4 signal conditioning chassis power supply voltages, and 3 spares. Tables IV(a) through IV(d) list the 200-channel instrumentation hook-up for each test showing signal conditioner and scanner channel numbers, function being measured, LDEF position designator, sensor identifier, and measured reference voltage at the scasor.

One problem encountered with this DAS arrangement resulted from the differences in impedance between the various load cells and the total number used for each test. The effect was to change the reference voltage applied to all instrumentation connected to signal conditioning chassis "A" from the 10-VDC level at which they were calibrated. This included all load cells and 27 of the deflectometers. For each test, it was necessary to measure the

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reference supply voltage at the sensor and to correct the calibration factor used in the computer accordingly by the ratio of voltages.

A contractor generated computer program¹ was used to access the instrumentation, convert values and display them in appropriate engineering units, provide permanent printouts, store raw and reduced data on tape, and compare actual instrumentation levels with predetermined values for status checks and appropriate warnings. As a further check, the computer also compared forces and moments summed about the various LDEF axes. The computer scan channel numbers 0-49 correspond to signal conditioner channels A-1 through A-50; likewise, scan channels 50-99, 100-149, and 150-199 correspond accordingly to 1 through 50 for B, C, and D. The program was readily accessible to provide the operator the ability to correct input values as deemed appropriate.

TEST LOADS

Internal forces and moments of the LDEF primary structure were calculated considering both ground handling and flight events. In general, the limit loads result from the transient STS events of lift-off and landing. The finite element model, which is used to determine limit load at the structural element level, includes stiffness and mass representations of the primary structure and the trays/experiments. These limit loads were developed by performing transient dynamic analyses using acceleration-time histories representing both lift-off and landing conditions supplied by the Rockwell International Corporation (ref. 2). Twelve lift-off and five landing transients were considered for each of the two specific locations of the LDEF in the STS Orbiter Bay.

¹ Wyle Laboratories, Scientific Services and Systems Group: Operating Instructions for the Long Duration Exposure Facility (LDEF). Document Number SD63145-115R0-D3, April 1982. (Unpublished)

Verification test loads were defined as 1.2 times limit loads and is equal to the applied test loads which include those resulting from a 1G environment. These verification test loads were determined by iterative static analyses. Load sets were altered until internal forces and moments of selected structural elements were similar to 1.2 times flight loads. In addition, reaction loads were required to be at least 1.2 times flight induced reaction loads. Four tests were required to load all selected members to verification levels. The four tests were labeled as, (I) landing, (II) lift-off, (III) maneuvering, k(z), and (IV) landing, ESB. A stress analysis using test loads was performed to show that no structure would be damaged as a result of testing.

Table I(a) locates the points where the test loads were applied for Test I - Landing. The loads from this configuration induced verification loading of the center ring, diagonals, trunnions, and longerons. This test used 20 hydraulic cylinders and 34 load input points. The second test is shown in a schematic in table I(b). Twelve hydraulic cylinders were used to apply 14 loads. Verification test loads were applied to the center ring, diagonals, trunnions, and longerons. The third test. representing a flight maneuver, was relatively simple. It required that discrete loads be applied at six locations on the center ring, as shown on table I(c), to achieve the verification test loaded the ESB and end frame members to 1.2 times the limit load which represented a landing condition. Table I(d) locates the three applied loads used in this test.

RESULTS AND DISCUSSION

The success of the LDEF Structural Verification Test is based on an examination of load, strain, and deflection test data which show agreement with analytical predictions. During the four tests, selected elements of the LDEF structure were subjected to 120 percent of anticipated limit load. In achieving the test load on certain elements, others were subjected to levels other than limit, but in no case to levels that would cause structural damage.

Loads

The integrated loads listed in table V for the four tests consist of the applied load, 120 percent of limit load, and reacted load. Figure 3 identifies and locates components of the LDEF primary structure with respect to the longitudinal, vertical, and lateral directions. The desired 120 percent of limit load was met for all tests as shown by an examination of the applied and reacted loads. For all test configurations, the applied and reactive loads should be of equal magnitude. The largest difference occurred in Test III. The instrumentation for this test configuration did not allow measurement of the lateral frictional loads at the main trunnion. Inclusion of frictional loads would tend to reduce the difference in these measured loads.

Stresses

Table VI summarizes predicted and measured stresses for the most severely loaded member of each type of LDEF structural element. The first column represents 120 percent of the predicted stress due to the limit load condition. The second column represents the actual measured stress at the same point due to applied test loads. The third column represents the computed stresses using the applied test load.

<u>Diagonals</u>. - The eight LDEF diagonals have ball-joints at each end to minimize the transfer of moment. Of the eight, four were strain-gaged to define axial load. The resulting tensile stress of 5304 psi (table VI) was within 1/2 percent of the 120 percent tensile limit stress value. Using the applied load from Test I, the predicted stress for this member exceeded the measured (S.G. #94 on fig. 19-G) stress of 5304 psi by 6 psi. The limit compressive stress times 120 percent was -3372 psi. The measured test stress of -4111 psi exceeded the anticipated compressive stress by 21.9 percent. The predicted compressive stress based on the applied loads for this member was -4140 psi.

End Support Beam. - The ESB was instrumented to define both bending moment and axial force in two of the four hollow aluminum tubular members. The limit stress times 120 percent for the lower tube was 12,090 psi and was measured at 10,697 psi (S.G. #114 on fig. 19-H).

<u>Center Ring</u>. - The most highly stressed members of the center ring are directly above and below the main trunnions. The limit stress times 1.2 for the member below the main trunnion was 5,292 psi (S.G. #53 on fig. 19-D) which includes the contribution from axial force and two bending moments. The measured stress was 127.3 percent of 1.2 times limit stress. At this same point, the predicted stress based on the applied Toaus was 88.9 percent of the measured. The limit stress times 1.2 for the center ring members above the main trunnions was -5,412 psi compared with a corresponding measured stress of -5,505 psi (S.G. #37 on fig. 19-A). The predicted stress at this same point was -5,240 psi.

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<u>Longerons</u>. - The limit stress for the longeron above the main trunnion has an axial compressive stress times 120 percent of -268 psi. The peak predicted axial stress of -312 psi was 2 percent greater in magnitude than the measured value (S.G.'s #73 through #80 on fig. 19-E).

Deflections

Vertical deflection versus length of the LDEF is shown on figures 22(a) through 22(d). The first two of these figures show deflections resulting from Test J. Figure 22(a) shows those deflections along the length of a longeron directly above the main trunnion and figure 22(b) shows those deflections along the bottom-most longeron. Applied loads for Test I are principally in the vertical direction. Examination of the resulting measured deflection data does not suggest a need for either a significant translational or rotational rigid body correction. Figures 22(c) and 22(d) refer to the vertical deflections of the same longerons due to Test II. For this test, the applied load components in the vertical and longitudinal directions were more nearly equal than in Test I. Mausured deflection at the support locations, while small, is not consistent and therefore can not be used as a correction for rigid body motion. Examination of the deflection data shown on figure 22(c) does suggest that a rigid body translation and rotation has taken place. A rigid body correction obtained by enforcing like displacements equal at the main trunnion (LDEF length - 200 inches) and the longeron at the ESB end (LDEF length -360 inches) substantially improves the predicted and measured deflection data for both longerons.

or all test loadings, the deflection along the length of LDEF, both above and below the main trunnion, show good agreement between measured and computed. The test data consistently indicated a slightly stiffer structure than was predicted by the analysis.

72

Post-Flight Inspection

During Test II, the acoustic monitoring instrumentation indicated a localized activity in the region of the right main trunnion. Post-test inspection did reveal a weld imperfection in a fillet weld on a gusset which was repaired by local surface grinding. Post-test visual, eddy current, and dye penetrant examinations of the center ring and ESB welds indicated no additional anomalies.

CONCLUSIONS

All test objectives were achieved. A review of test data and post-test inspection of the flight hardware shows that the LDEF structure is adequate to survive all flight induced loads. Test data comparisons with analyses demonstrate good agreement when examining load, strain, and deflection data. This agreement verifies the analytical models and methods used in the loads and stress analyses. Since the test loads were at least equal to 1.2 times anticipated flight loads, the fina¹ test objective, "Static test a flight article to 1.2 times limit load and design to an ultimate factor of safety such that detrimental permanent deformation is precluded as a result of test," was also met.

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|---------------------|---------------------------------------|------------|----------|------------------|--------------------|----------|---|--------------|-----------------|
| CVM | CHAN. N | 10. | | LOAD | INPUT | LO | AD CELL | ну | D. CYL. |
| Sin, | SIG. CONUT. | SCANNER | TYPE OF | LOCATION | MEAS . XZ/YZ | IDENT. # | VOLT. @ GAGE | TYPE | PISTON AREA IN2 |
| 4 | A-29 | 28 | SGL | 911CH XZ | 70/85 | L10-6 | 10.534 | P/HBB2HLS14 | 4.125 |
| 0 | ۸-30 | 29 | SGL | 916AI Z | 90/87 | 1.5-1 | 9.984 | HYDRO N2C | 2.35 |
| 0 | A-31 | 30 | SGL | 916AD Z | 89/93 | L5-2 | 9.980 | HYDRO N2C | 2.357 |
| | A-32 | 31 | DUAL | 916AF-G Z | 87/89 | 5-77 | 10.529 | P/HBB2HLS14 | 1.460 |
| | A-33 | ′32 | DUAL | 936EA-L Z | 86/90 | L5-4 | 9.993 | P/HBB2HLS14 | 1.460 |
| | A-34 | 33 | DUAL | 936EE-H Z | 89/91 | 5-38 | 10.517 | P/HBB2HLS14 | 1.460 |
| | A-35 | 34 | DUAL | 936DB-K Z | 86/92 | 5-39 | 10.519 | P/HBB2HLS14 | 1.460 |
| | A-36 | 35 | DUAL | 936DF-G Z | 90/90 | 5-40 | 10.513 | P/HBB2HLS14 | 1.460 |
| | A-37 | 36 | DUAL | 936CB-К Z | 81/90 | 5-41 | 10.561 | P/HBB201 514 | 1.460 |
| 1 | A-38 | 37 | DUAL | 936CF-G Z | 87/90 | 5-43 | 10.518 | P/HBB2HLS14 | 1.460 |
| ' J | A-39 | 38 | DUAL | 936BA-L Z | 83/90 | 5-45 | 10.517 | P/HBB2HLS14 | ۰.460 |
| . 🖸 | A-40 | 39 | DUAL | 936bE-н Z | 80/90 | 5-46 | 10.513 | P/HBB2HLS14 | 1.460 |
| | A-41 | 40 | SGL | RESETTUN Z | | L10-5 | 9.877 | | |
| | A-42 | 41 | SGL | LESBTRUN Z | | L12-10 | 10.532 | | |
| | A-43 | 42 | SGL | 911CI XZ | 61.5/92 | L10 7 | 10.531 | P/HBB2HLS14 | 4.125 |
| | Λ-44 | 43 | SGL | 911CD XZ | 62.5/81 | LICA | 10,532 | P/HBB2HLS14 | 4.125 |
| $\overline{\Delta}$ | A-45 | 44 | DUAL | 911CA-L XZ | 62/90 | 20-58 | 9.967 | P/HTC2HLS33 | 7.660 |
| | A-46 | 45 | DUAL | 91JCE-K XZ | 70/90 | 20-59 | 9.928 | P/HTC2HLS33 | 7.660 |
| | ۸-47 | 46 | SGL | 911CE XZ | 70/93 | L10-9 | 10,532 | P/HBB2HLS14 | 4.125 |
| | A-48 | 47 | DUAL | 911CF-G XZ | 58.25/90 | 20-73 | 9.965 | P/HIC2HLS33 | 7.660 |
| D | <i>⊾</i> –49 | 48 | DUAL | 920FA-L XZ | 47.5/90 | 20-77 | 9.965 | P/HTC2HLS33 | 7.660 |
| | A-50 | 49 | DUAL | 920FF-G XZ | 48.5/90 | 20-76 | 9.929 | P/HTC2HLS33 | 7.660 |
| * R | EACTION LOAD | | . | 4 ,,,,,,, | Above @ 20% Loa | d | | | * |

3000 psi PUMP PRESS MAX.

TABLE I A.- LOAD INPUT LOCATION AND INFORMATION FOR "LANDING" TEST

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NUMBERS SHOWN ARE SIGNAL CONDITIONER CHANNEL "A" NUMBERS

| 0.24 | CHAN. 1 | NO. | | LOAD | INPUT | LO | AD CELL | ну | D. CYL. |
|--|---|--|--|--|---|---|---|---|--|
| 511 | SIG. CONDT. | SCANNER | TYPE OF | LOCATION | MEASZ XZ/YZ | IDENT. # | VOLT. @ GACE | TYPE | PISTON AREA IN2 |
| 00000000000000000000000000000000000000 | $ \begin{array}{c} A-30 \\ A-31 \\ A-29 \\ A-47 \\ A-41 \\ A-42 \\ A-43 \\ A-44 \\ A-45 \\ A-46 \\ A-32 \\ A-46 \\ A-32 \\ A-48 \\ A-48 \\ A-40 \\ A-48 \\ A-40 \\ A$ | 29 30 28 46 40 41 42 43 44 45 31 47 | SGL SGL SGL SGL SGL SGL SGL SGL SGL SGL | 920F1 Z 920FD Z 916AG XZ 916AF XZ RESBTRUN Z LESBTRUN Z 916AL XZ 916AL XZ 911CK XZ 911CB XZ 911CT XZ 911CD XZ | 90° 90° 40° 39° 28°/ 25°/ 55°/9° 55°/10° 60°/4° 60°/3° | L5-4 L5-2 L10-6 L10-9 L10-5 L12-10 L10-7 L10-8 20-58 20-59 20-65 20-73 | 9.985 9.982 10.534 10.534 9.983 10.530 10.538 10.538 10.534 9.967 9.928 9.900 9.965 | HYDRO N2C HYDRO N2C P/HBB2HLS14 P/HBB2HLS14 P/HBB2HLS14 P/HBB2HLS14 P/HBB2HLS14 P/HTC2HLS33 P/HTC2HLS33 P/HTC2HLS33 P/HTC2HLS33 | 2.357 2.357 4.125 4.125 4.125 4.125 4.125 7.660 7.660 7.660 7.660 7.660 |
| ŏ | A-50 | 40 | DUAL | 920FF-G XZ | 50/ | 20-76 | 9.933 | P/HTC2HLS33 | 7.660 |

21

2500 psi PUMP PRESS MAX

* REACTION LOAD

TABLE I B. - LOAD INPUT LOCATION AND INFORMATION FOR "LIFTOFF" TEST

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| | | ~ | | 150(| D psi PUMP PR | ESS MAX. | | | |
|---------------|-----------------|-------------|---------------|----------------|----------------|----------|--------------|--------------|-----------------------------|
| | CHAN. | NO. | | (IA) | INPUT | ΓΟΊ | AD CELL | Ч | D. CYL. |
| S | SIG. CONDT | . SCANNER | TYPE OF | LOCATION | NEAS XZ/YZ | IDENT. # | VOLT. @ GAGE | TYPE | PISTON AREA IN ² |
| – * | J A-36 | 35 | SGL | KEEL Y | | 50-23 | 10.518 | 1 | - |
| * | A-41 | 40 | SGL | RESBTRI'V Z | | L10-5 | 9.982 | 1 | |
| * | A-42 | 41 | SGL | LESBTRUN Z | | L12-10 | 10.529 | 1 | |
| _ | 0 A-43 | 42 | SGL | 911CDD Y | 00 | 110-E | 10.525 | P/HBB2HLS14 | 4.125 |
| _ | 0 A-44 | 43 | SGL | 911CDF Y | .5°DWN | L10-6 | 10.531 | P/HBB2HLS14 | 4.125 |
| * | O A-45 | 77 | SGL | Y Idile | 2°DWN | L10-7 | 10.534 | P/HBB2HI.S14 | 4.125 |
| * | S A-46 | . 45 | SGL | 911CI Y | 2°DWN | L10-9 | 10.530 | P/HBB2HLS14 | 4.125 |
| × * | > A−47 | 46 | SGL | 911DG Y | 1°DWN | L5-4 | 9.977 | P/HBJ2HLS14 | 4.125 |
| × * | S A-48 | 47 | SGL | 911CC Y | NMODI | L5-2 | 9.968 | P/HBE2HLS14 | 4.125 |
|], | * REACTION LOAL | | | | Above | | | | |
| * | * Ea. Located t | 8.4" Either | : Side of Cnt | r. of Chir. Kl | Ing TC 40% Lo. | ad | | | |

TABLE I C.- LOAD INPUT LOCATION AND INFORMATION FOR "KEEL" TEST

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| | CILAN. N | 0. | | LOAD | INPUT | TO' | AD CELL | Н | D. CYL. |
|-----------|--------------|-----------|---------|------------|------------|----------|--------------|-------------|-----------------|
| | SIG. CONDT. | SCANNER | TYPE OF | LOCATION | NEAS XZ/YZ | IDENT. # | VOLT. @ CAGE | TYPE | PISTON AREA IN2 |
| 0 | A -36 | 35 | SGL | FESS Z | 06/06 | 50-10 | 10.533 | P/HBB2HLS14 | 19.640 |
| \$ | A-41 | 40 | SGL | RESBTRUN Z | 1 | 50-98 | 10.543 | - | 1 |
| \$ | A-42 | , 41 , | SGL | LESBTRUN Z | 1 | 50-34 | 9.982 | 1 | |
| | A-43 | 42 | DUAL | 916AA-L Z | 06/06 | L12-10 | 10.538 | P/HTC2HLS33 | 7.660 |
| | A-44 | 43 | DUAL | 916AF-G Z | 06/06 | L10-7 | 10.580 | P/HTC2HLS33 | 7.660 |

* REACTION LOAD

TABLE I D.- LOAD INPUT LOCATION AND INFORMATION FOR "END SUPPORT BEAM" TEST

dat. 1 .

ORIGINAL PAGE IS OF POOR QUALITY



RIGHT MAIN TRUNNION

CONTROL ROOM SIDE

| SIG. CONDT. CH. # | LTR/ / DIR | LOCATION | IDENT. NO. | VOLT. @ GACE | | SIG. CONDT. CH. # | LTR/ | DIR | LOCATION | IDENT. NO. | VOLT. @ GAGE |
|-------------------------|---------------|-------------|---------------|--------------------|-----|-------------------------|------|-----|---------------|---------------|--------------------|
| D-7 | AX | 920FL-A X | D 01 | 9 9 76 | 1 1 | D-26 | D | v | 036CF V | D 44 | 0 006 |
| D-8 | AY | 920FL-A Y | D 02 | 10,000 | | D=20 | R | 7 | 936CF 7 | D 44 | 9.996 |
| D-9 | AZ | 920FL-A Z | D 21 | 9,495 | | n-16 | S | v | 936BC Y | D 46 | 10,002 |
| D-10 | вх | 920FC · X | b 03 | 9,988 | | D-17 | S | ż | 936BC 7 | D 47 | 0 995 |
| D-11 | BY | 920FC Y | D 04 | 9,985 | | D-24 | т | Ŷ | 936BF Y | D 48 | 9,991 |
| D-12 | Вz | 920FC Z | D 22 | 9,993 | | 1)-25 | Ť | 7 | 936BF 2 | 0.80 | 9,999 |
| A-26 | l c x | 920FF X | D 05 | 10.641 | | A-17 | E E | x | 916AL ¥ | D 50 | 10.651 |
| D-2 | CY | 920FF Y | D 06 | 9.992 | | A-18 | ŭ | Ŷ | 916AL-A Y | D 51 | 10,523 |
| A-27 | C Z | 926FF Z | D 23 | 10.650 | | A-19 | U | ż | 916AL-A Z | D 52 | 10.652 |
| C-49 | | 936EC-920FB | D 07 | 9.714 | | D-13 | v | x | 916AC X | D 53 | 10,000 |
| C-50 | E | 936EC-920FD | D 08 | 9.705 | | D-14 | v | Ŷ | 916AC Y | D 54 | 9,993 |
| D-22 | FY | 936EC Y | D 09 | 9.990 | | D-15 | v | Z | 916AC Z | D 55 | 9,993 |
| D-23 | FZ | 936EC Z | D 24 | 9,990 | | A-24 | Ŵ | x | 916AF X | D 56 | 10,532 |
| D-30 | GY | 936EF Y | D 83 | 10.000 | | A-20 | Ŵ | Y | 916AF Y | D 57 | 10.581 |
| D-31 | GZ | 936EF Z | D 25 | 9,993 | | A-25 | W | z | 916AF Z | D 58 | 10.646 |
| D-20 | HY | 936DC Y | D 11 | 9.999 | | A-8 | X | x | LESB TRUN X | D 59 | 10.517 |
| D-21 | нz | 936DC Z | D 26 | 9.995 | | A-9 | x | Y | LESB TRUN Y | D 60 | 10.582 |
| D-28 | IY | 936DF Y | D 12 | 10.000 | | A-10 | X | Z | LESB TRUN Z | D 61 | 10.645 |
| D-29 | ΙZ | 936DF Z | D 27 | 9.995 | | A-11 | Y | X | RESB TRUN X | D 62 | 10,534 |
| D-4 | JX | 911C/DL-A X | D 13 | 9.997 | | A-12 | Y | Y | RESB TRUN Y | D 63 | 10.530 |
| D-5 | JY | 911C/DL-A Y | D 14 | 10.018 | 1 | A-13 | Y | Z | RESB TRUN Z | D 64 | 10.644 |
| D-6 | JZ | 911C/DL-A Z | D 15 | 9.993 | | A-21 | Z | X | ESBS X | D 65 | 10.527 |
| A 2 | КХ | LM TRUN X | D 16 | 10.561 | | A-22 | z | Y | ESBS Y | D 66 | 10.612 |
| A3 | Кү | LM TRUN Y | D 17 | 10.523 | | A-23 | Z | Z | ESBS Z | D 67 | 10.645 |
| A-4 | KZ | LM TRUN Z | D 18 | 10.642 | 1 | C-47 | cc | | 936BCBI | D 29 | 9.706 |
| D-32 | LY | 911C/DD Y | D 19 | 9.993 | | C-48 | BB | | 936EC-E1 | D 30 | 9.704 |
| D-33 | ĽΖ | 911C/DD Z | D 20 | 10.002 | | D-37 | | | LMTEST STRU X | D 70 | 9.983 |
| C-45 | МҮ | 911C/DE Y | D 31 | 10.558 | | D-38 | | | LMTEST STRU Y | D 71 | 9.991 |
| C-46 | M 7. | JIC/DE Z | D 68 | 9.707 | | D-39 | | | LMTEST STRU Z | D 72 | 9.990 |
| D-3 | NX | 911C-, F X | D 33 | 10.010 | | D-40 | | | RMTEST STRU X | D 73 | 9.995 |
| A-28 | N Y | 911C-DF Y | D 34 | 10.581 | | D-41 | | i | RMTEST STRU Y | D 74 | 9.998 |
| D-34 | N 7. | 911C-DF Z | D 35 | 9.989 | | D-42 | | | KMTEST STRU Z | D 75 | 10,000 |
| A-14 | 0 X (| KEEL X | D 36 | 10.641 | | D-43 | | | LETEST SIRU X | D 76 | 9.996 |
| A-15 | 0 Y | KEEL Y | D 37 | 10.642 | | D-44 | | | LETEST STRU Y | D 77 | 9.997 |
| A-16 | 0 Z | KEEL Z | D 38 | 10.651 | | D-45 | | | LETEST STRU Z | D 78 | 9.995 |
| A-5 | РХ | RM TRUN X | D 39 | 10.256 | | D-46 | | | RETEST STRU X | D 32 | 10.005 |
| A-6 | Рү | RM TRUN Y | D 40 | 10.526 | | D-47 | | | RETEST STRU Y | D 69 | 10.002 |
| A-7 | Ρz | RM TRUN Z | D 41 | 10.643 | | D-48 | | | RETEST STRU Z | D 79 | 10.002 |
| D-18 | QY | 936CC Y | D 42 | 9.994 | | | | | | 1 | |
| D-19 | Q Z | 936CC Z | D 43 | 9.996 | | | | | | | |

TABLE II. - DEFLECTOMETER DESIGNATION AND LOCATION

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| LOCATION CODES | A | В | с | D | E | F |
|--|--------------------------------------|--------------------------------------|--------------|----------------|---------------------------------|--------------------------------------|
| Bay 9/Sec A fwd Sec A aft Sec B fwd Sec B aft & hole inboard fwd | | | 3.06 3.09 | 3.032 3.032 | 5.957 | 16.817 |
| inboard aft out aft | | | | | 6.007 8.567 | 19.387 16.797 19.387 |
| 2" above gusset inboard fwd out fwd inboard aft out aft | | 8.517 11.097 8.567 11.127 | | | | |
| Tang top hole inboard fwd out fwd inboard aft out aft | 18.817 21.387 18.797 21.387 | | | | | |
| Bay 10/Sec A fwd Sec A aft Sec B fwd Sec B aft | | | 3.06 2.98 | 3.02 3.00 | | |
| <pre></pre> | 8.357 11.087 8.467 11.177 | 25.037 27.767 25.162 27.864 | | | | |
| Bay 3/Sec A fwd Sec A aft Sec B fwd Sec B aft | | | 3.06 3.06 | 3.08 3.06 | | |
| G hole inboard fwd out fwd inboard aft out aft | | | | | 5.96 8.567 5.887 8.597 | 16.787 19.387 16.777 19.407 |
| 2" above gusset inhoard fwd out fwd inboard aft out aft | | 8.79 11.397 8.819 11.427 | | | | |
| Tang top hole inboard fwd out fwd inboard aft out aft | 18.787 21.387 18.777 21.407 | | | | | |
| Bay 2/Sec A fwd Sec A aft Sec B fwd Sec B aft | | | 3.00 3.00 | 3.01 3.01 | | |
| G hole inboard fwd out fwd inboard aft out aft | 8.537 11.193 8.380 11.047 | 25.217 27.902 25.117 27.807 | | | | |

TABLE III. - STRAIN GAGE LOCATION CODE DIMENSIONS

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| CHAN | NO. | | l | r | l | 1 | CHAN | NO | | · · · · · · · · · · · · · · · · · · · | | |
|-------|------|-------------------|---------------|----------|--------|-----|--------------|------|----------|---------------------------------------|-------|--------|
| | | | | | VOLT | | | | | | | VOLT |
| SIG. | SCAN | FUNCT. | LOCATION | IDEN1. | e | 1 | SIC. | SCAN | FUNC . | LOCATION | IDENT | 6 |
| CONDT | | | | NO. | GAGE |] | CONDT | | | | NO. | GAGE |
| A-1 | | PWR SUPP | A REF Vo | | 10.850 | I | 8-1 | 50 | PUR SUPP | B REF VO | | 10,000 |
| A-2 | 1 1 | DEFL | LM TRUN K-X | D-16 | 10.561 | | B-2 | 51 | Str. Ga. | LM TRUN +Z | 89 | 9,9655 |
| A-3 | 2 | DEFL | LM TRUN K-Y | D-17 | 10.523 | 1 | B-3 | 52 | Str. Ga. | LM TRUN +X | 92 | 9,9657 |
| A-4 | 3 | DEFL | LM TRUN K-Z | D-18 | 10.642 | 1 | B4 | 53 | Str. Ga. | RM TRUN +2 | 29 | 9,9559 |
| A-5 | 4 | DEFL | RM TRUN P-X | D-39 | 10.256 | | B5 | 54 | Str. Ga. | RM TRUN +X | 30 | 9.9658 |
| A-6 | 5 | DEFL | MA TRUN P-Y | D-40 | 10.526 | 1 | B-6 | 55 | Str. Ga. | 911DC-DB0 | 33 | 10.000 |
| A-7 | 6 | DEFL | RM TRUN P-Z | D-41 | 10.643 | | B-7 | 56 | Str. Ca. | 911CC-DB0 | 34 | 10.000 |
| A-8 | 7 | DEFL | LESB TRUN X-X | D~59 | 10.517 | 1 | B-8 | 57 | St⁻. Ga. | 911DC-DBI | 35 | 10.000 |
| A-9 | 8 | DEFL | LESB TRUN X-Y | D-60 | 10.582 | | B9 | 58 | Str. Ga. | 911CC-DBI | 36 | 10.000 |
| A-10 | 9 | DEFL | LESE TRUN X-2 | D-61 | 10.645 | | B-10 | 59 | Str. Ga. | 911DC-BAO | 37 | 10.000 |
| A-11 | 10 | DEFL | RECE TRUN Y-X | D-62 | 10.534 | 1 | 6-11 | 60 | Str. Ga. | 911CC-BAO | 38 | 10.000 |
| A-12 | 11 | DEFL. | RE. TRUN Y-Y | D-63 | 10.530 | | B-12 | 61 | Str. Ga. | 911DC-BAI | 39 | 10.000 |
| A-13 | 12 | DEFL | RESB TRUN Y-Z | D-64 | 10.644 | [| B-13 | 62 | Str. Ga. | 911CC-BAI | 40 | 10.000 |
| A-14 | 13 | DEFL | KEEL 0-X | D-36 | 10.641 | 1 | B-14 | 63 | Str. Ga. | 911C-DJ-IAO | 0 | 10.000 |
| A-15 | 14 | DEFL | KEEL O-Y | D-37 | 10.642 | 1 | 8-15 | 64 | Str. Ga. | 911C-DC-DBOI | 41* | 10.000 |
| A-16 | 15 | DEFL | KEEL 0-2 | D-38 | 10.651 | ! | B-16 | 65 | for. Ga. | 911C-DC-BAOI | 42* | 10.000 |
| A-17 | 16 | DEFL | 916AL-A U-X | D~50 | 10.651 | [| B-17 | 66 | Str. Ga. | 911DC-DA0 | 43 | 10.000 |
| A-18 | 17 | DEFL | 916AL-A U-Y | D-51 | 10.523 | | B-18 | 67 | Str. Ga. | 911CC-DA0 | 44 | 10.000 |
| A-19 | 18 | DEFL | 916AL-A U-Z | D-52 | 10.652 | 1 | B-19 | 68 | Str. Ga. | 911DC-DAI | 45 | 10.000 |
| A-20 | 19 | DEFL | 916AF W-Y | D-57 | 10.581 | 1 | B-20 | 69 | Str. Ga. | 911CC-DAI | 46 | 10.000 |
| A-21 | 20 | DEFL | ESBS Z-Å | D-65 | 10.527 | 1 | B-21 | 70 | Str. Ga. | 911C-DC-DAOI | 47* | 10.000 |
| A-22 | 21 | DEFL | ESBS Z-Y | D-66 | 10.612 | 1 | B-22 | 71 | Str. Ga. | 911DC-BBO | 48 | 10.000 |
| A-23 | 22 | DEF'. | ESBS Z-Z | D-67 | 10.645 | ł | B-23 | 72 | Str. Ga. | 911CC-BBO | 49 | 10.000 |
| A-24 | 23 | DEFL | 916AF W-X | D-36 | 10.532 | 1 | 8-24 | 73 | Str. Ga. | 911DC-BBI | 50 | 10.000 |
| A-25 | 24 | DEFL | 910AF W-Z | D-28 | 10.040 | | 8-25 | 14 | Str. Ga. | 91100-881 | 21 | 10.000 |
| A-20 | 25 | DEFL | 920FF C-X | D-05 | 10.041 | ł | B-20 | 13 | Str. Ga. | 911C-DC-BDOI | 52* | 10.000 |
| A-2/ | 20 | DEFL | | D-23 | 10.000 | ĺ – | D-2/ | 70 | Str. Ga. | 91101-180 | 55 | 10.000 |
| A-20 | 21 | DEFL LOAD CELL | | 1 1-10-6 | 10.501 | 1 | D-20 B-20 | 74 | Str. Ga. | STICJ-IBU | 54 | |
| A-27 | 20 | LOAD CELL | 9110H AL | 15-1 | 10.334 | | B-27 | 70 | Str. Ga. | ALLOJ-BL | 55 | 10.000 |
| A-31 | 30 | LOAD CELL | 916AD 2 | 15-2 | 0 980 | } | R_31 | 80 | Str Ca | 911C-DI-TROT | 57* | 10.000 |
| A-32 | 31 | LOAD CELL | 9164F-C 7 | 5-77 | 10 529 | ł | B-32 | 81 | Str. Ca | 911D - KRO | 58 | 10,000 |
| A-33 | 32 | LOAD CELL | 936EA-L Z | 1.5-4 | 0.993 | ĺ | B-33 | 82 | Str. Ga. | 911CI-KB0 | 59 | 10.000 |
| A-34 | 33 | LOAD CELL | 936EE-H Z - | 5-38 | 10.517 | 1 | B-34 | 83 | Str. Ga. | 911DI-KBT | 60 | 10,000 |
| A-35 | 34 | LOAD CELL | 936DB-K Z | 5-39 | 10.519 | | 8-35 | 84 | Str. Ga. | 911CJ-KB(| 61 | 10.000 |
| A-36 | 35 | LOAD CELL | 936DF-G Z | 5-40 | 10.513 | | B-36 | 85 | Str. Ga. | 911C-DJ-KBUI | 62* | 10.000 |
| A-37 | 36 | LOAD CELL | 936CB-K Z | 5-41 | 10.561 | | B-37 | 86 | Str. Ca. | 911DJ-IA0 | 63 | 10.000 |
| A38 | 37 | LOAD CELL | 936CF-G Z | 5-43 | 10.518 | 1 | B-38 | 87 | Str. Ga. | 911CJ-IA0 | 64 | 10.000 |
| A-39 | 38 | LOAD CELL | 936BA-L Z | 5-45 | 10.517 | | E-39 | 88 | Str. Ga. | 911DJ-IAI | 65 | 10.000 |
| A -40 | 39 | LOAD CELL | 936BE-H Z | 5-46 | 10.513 | | B-40 | 89 | Str. Ga. | 911CJ-IAI | 66 | 10.000 |
| A-41 | 40 | LOAD CELL | RESB TRUN Z | L10-5 | 9.877 | | B-41 | 90 | Str. Ga. | 911C-DJ-IAI | 67 | 10.000 |
| A-42 | 41 | LOAD CELL | LESB TRUN Z | 112-10 | 10.532 | | B-42 | 91 | Str. Ga. | 911DJ-KAO | 68 | 10.000 |
| A-43 | 42 | LOAD CELL | 911CI XZ | L10-7 | 10.531 |] | B-43 | 92 | Str. Ga. | 911CJ-KAO | 69 | 10.000 |
| A-44 | 43 | LOAD CELI. | 911CD XZ | L10-8 | 10.532 | | B-44 | 93 | Str. Ga. | 911DJ-KAI | 70 | 10.000 |
| A-45 | 44 | LOAD CELL | 911CA-L XZ | 20-58 | 9.967 | ł | B-45 | 94 | Str. Ga. | 911CJ-KAI | 71 | 10.000 |
| A-46 | 45 | LOAD CELL | 911CB-K XZ | 20-59 | 9.928 | | B-46 | 95 | Str. Ga. | 911C-DJ-KAOI | 72* | 10.000 |
| A-47 | 46 | LOAD CELL | 911CE XZ | L10-9 | 10.532 | 1 | B-47 | 96 | Str. Ga. | 911DC-920FCAOU | 73 | 10.000 |
| A-48 | 47 | LOAD CELL | 920CF-G XZ | 20-73 | 9.965 | 1 | B-48 | 97 | Str. Ga. | 911DC-920FCAOL | 74 | 10.000 |
| ·A-49 | 48 | LOAD CELL | 920FA-L XZ | 20-77 | 9,965 | | B-49 | 98 | Str. Ga. | 911DC-920FCAIU | 73 | 10.000 |
| A-50 | 49 | LOAD CELL | 920FF-G XZ | 2076 | 9.929 | | B-50 | 99 | Str. Ga. | 911DC-920FCAIL | 76 | 10.000 |

*Combined Gages

Channels A-24 through B-13 were used for 40 channel scan of selected information.

TABLE IV A. - INSTRUMENTATION HOOK-UP, "LANDING" TEST

| CHAN | NO. | | | | | CHAN | NO. | | | | |
|-------|------|-----------|-----------------|-------------|----------|-------|-------------|-----------|----------------|--------|--------|
| | | | | | VOLT | | · · · · · · | | | | VOLT |
| SIG. | SCAN | FUNCT. | LOCATION | IDENT. | e | SIG. | SCAN | FUNCT. | LOCATION | IDENT. | e |
| CONDT | | | | NO. | GAGE | CONDI | | | | NO. | CAGE |
| (-1 | 100 | PUN SHIPP | C REE Vo | | 10.004 | n., 1 | 1.0 | PUD CIIPP | D PEE Vo | | 10.240 |
| C-2 | 101 | Str. Ga. | 911DC-920FCB0U | 77 | 10.004 | 0-1 | 151 | DEFL | 920FF C-Y | D-06 | 9,992 |
| C-3 | 102 | Str. Ga. | 911DC-920FCB01. | 78 | 10.004 | D-3 | 152 | DEFL | 911C-DF N-X | D-33 | 10.010 |
| C-4 | 103 | Str. Ga. | 911DC-920FCB1U | 79 | 10.004 | D-4 | 153 | DEFL | 911C/DL-A J-X | D-13 | 9,997 |
| C-5 | 104 | Str. Ga. | 911DC-920FCBIL | 80 | 10.004 | D-* | 14 | DEFL | 911C/DL-A J-Y | D-14 | 10.018 |
| C6 | 105 | Str. Ga. | 911DF-920FFA0U | 81 | 10.004 | D6 | 155 | DEFL | 911C/DL-A J-Z | D-15 | 9.993 |
| C-7 | 106 | Str. Ga. | 911DF-920FFADL | 82 | 10.004 | D-7 | 156 | DEFL | 920FL-A A-X | D01 | 9.976 |
| C8 | 107 | Str. Ga. | 911DF-920FFAIU | 83 | 10.004 | D-8 | 157 | DEFL | 920FL-A A-Y | D-02 | 10.000 |
| C-9 | 108 | Str. Ga. | 911DF-920FFAIL | 84 | 10.004 | D-9 | 158 | DEFL | 920FL-A A-Z | D-21 | 9.995 |
| C-10 | 109 | Str. Ga. | 911DF-920FFBOU | 85 | 10.004 | D-10 | 159 | DEFL | 920FC B-X | D03 | 9.988 |
| C-11 | 110 | Str. Ga. | 911DF-920FFBOL | 86 | 10.004 | D-11 | 160 | DEFL | 920FC 3-Y | D04 | 9.985 |
| C-12 | 111 | Str. Ga. | 911DF-920FFBIU | 87 | 10.004 | D-12 | 161 | DEFL | 920FC B-Z | D-22 | 9.993 |
| C-13 | 112 | Str. Ga. | 911DF-920FFBIL | 88 | 10.004 | D-13 | 162 | DEFL | 916AC V-X | D-53 | 10,000 |
| C-14 | 113 | Str. Ga. | RM TRUN -Z | 31 | 9.9615 | D-14 | 163 | DEFL | 916AC V-Y | D-54 | 9.993 |
| C-15 | 114 | Str. Ga. | RM TRUN X | 32 | 9.9614 | D-15 | 164 | DEFL | 916AC V-Z | D-55 | 9.992 |
| C-16 | 115 | Str. Ga. | LM TRUN -X | 90 | 9.9612 | D-16 | 165 | DEFL | 936BC S-Y | D-46 | 10.002 |
| C-17 | 116 | Str. Ga. | LMTI -Z | 91 | 9.9614 | D-17 | 166 | DEFL | 936BC S-Z | D-47 | 9.995 |
| C-18 | 117 | Str. Ga. | 911D920FFUL | 93* | 10.004 | D-18 | 167 | DEFL | 936CC Q-Y | D-42 | 9.994 |
| C-19 | 118 | Str. Ga. | 911cc-916AFul | 94 * | 10.004 | D-19 | 168 | DEFL | 936CC Q-Z | D-43 | 9.996 |
| C-20 | 119 | Str. Ga. | 911DC-920FAUL | 95* | 10.004 | D-20 | 169 | DEFL | 936DC H-Y | D-11 | 9.999 |
| C-21 | 120 | Str. Ga. | 911CC-916AAUL | 96* | 10.004 | D-21 | 170 | DEFL | 936DC H-Z | D-26 | 9.995 |
| C-22 | 121 | | | | | D-22 | 171 | DEFL | 936EC F-Y | D-09 | 9.990 |
| C-23 | 122 | | | | | D-23 | 172 | DEFL | 936EC F-Z | D-24 | 9.990 |
| C-24 | 123 | | | | | D-24 | 173 | DEFL | 936BF T-Y | D-48 | 9.991 |
| C-25 | 124 | | | | | D-25 | 174 | DEFL | 936BF T-Z | D-80 | 9.999 |
| C-26 | 125 | | | | | D-26 | 175 | DEFL | 936CF R-Y | D-44 | 9.996 |
| C-27 | 126 | | | | | D-27 | 176 | DEFL | 936CF R-Z | D-45 | 9.994 |
| C-28 | 127 | | | | | D-28 | 177 | DEFL | 936DF I-Y | D-12 | 10.000 |
| C-29 | 128 | | | | | D29 | 178 | DEFL | 936DF I-2 | D-27 | 9.995 |
| C-30 | 129 | | ~ | | | D-30 | 179 | DEFL | 936EF G-Y | D-10 | 10.000 |
| C-31 | 130 | Str. Ga. | TRAY | 105 | 10.004 | D-31 | 180 | DEFL | 936EF GZ | D-25 | 9.993 |
| C-32 | 131 | Str. Ga. | TRAY | 106 | 10.004 | D-32 | 181 | DEFL | 911C/DD L-Y | D-19 | 9.993 |
| C-33 | 132 | Str. Ga. | TRAY | 107 | 10.004 | D-33 | 182 | DEFL | 911C/DD L-Z | D-20 | 10.002 |
| C-34 | 133 | Str. Ga. | TRAY | 108 | 10.004 | D-34 | 183 | DEFL | 911C-DF N-Z | D-35 | 9.989 |
| C-35 | 134 | | | | | D-35 | 184 | AOAI | TEST STR PITCH | Q-10 | |
| C-35 | 135 | | | | | D-36 | 185 | AOAI | TEST STR ROLL | Q9 | |
| C-37 | 136 | | | | | D-37 | 186 | DEFL | LM TEST STRU X | D-70 | 9.983 |
| C-38 | 137 | - | | • | | D-38 | 187 | DEFL | LM TEST STRU Y | D-71 | 9,991 |
| C-39 | 138 | | | | | D-39 | 188 | DEFL | LM TEST STRU Z | D-/2 | 9.990 |
| C-40 | 139 | | | | | D-40 | 189 | DEFL | KM TEST STRU X | D-/3 | 9.995 |
| C-41 | 140 | | | | | D-41 | 190 | DEFL | KM TEST STRU Y | D-/4 | 9.998 |
| C-42 | 141 | | | | | D-42 | 1 1 3 1 | DEFL | KM TEST STRU Z | D-/5 | 10.000 |
| C-43 | 142 | | | | | D-43 | 192 | DEFL | LE TEST STRU X | D-/0 | 9.990 |
| C-44 | 143 | | | | 10 . 660 | D-44 | 133 | DEFL | LE TEST STRU I | 10-11 | 9.99/ |
| C-45 | 144 | DEFL | 911C/DE M-Y | D-31 | 10.328 | D-45 | 194 | DEFL | LE TEST STRU Z | D-70 | 10 005 |
| C-46 | 145 | DEFL | 911C/DE M-Z | D-68 | 9.707 | D-40 | 132 | DEFL | RE TEST STRU X | D-32 | 10,003 |
| U-4/ | 146 | DEFL | ANDRE-RI CC | D-29 | 9.706 | D-4/ | 170 | DEFL | KE TEST SIKU Y | D-07 | 10.002 |
| 0-48 | 14/ | DEFL | 9JOEC-EI BB | D-30 | 9.704 | U-48 | 17/ | DEFL | RE TEST SIKU Z | 0-13 | 10.002 |
| 0-49 | 148 | PEFL | 930LC-920FB D | D-07 | 9./14 | D-49 | 100 | AUAL | DM TRIN PITCH | 0-13 | |
| L-30 | 149 | DEFL | 930EC-92UFD E | 00-U | 9.705 | 0-20 | 461 | AUAI | ANT INUN KULL | 1 4-12 | l |

*Combined Gages

IABLE IV A. (CONTD.)- INSTRUMENTATION HOOK-UP, "LANDING" TEST

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and the second second

| CHAN | NO. | | | | | | CHAN | NO. | | | | |
|--------------|-------|-----------|----------------------|-----------|--------------|-----|---------------|--------|----------|----------------|--------|--------|
| erc | CC 41 | TINICE | TOCATTON | TOPME | VOLT. | | 070 | 00.411 | TRACT | 10013700 | **** | VOLT. |
| CONDT | SCAN | PUNCT. | LUCATION | IDENT. | CACE | | SIG. | SCAN | FUNCT. | LOCATION | IDENT. | CACT . |
| | | | | | UNUL | | CONDI | | | | | GADE |
| A-1 | 0 | PWR SUPP | A REF Vo | | 10.850 | | B-1 | 50 | PWR SUPP | B REF Vo | | 10.000 |
| A-2 | 1 | DEFL | LM TRUN K-X | D-16 | 10.561 | | B2 | 51 | Str. Ga. | LM TRUN +Z | 89 | 9.9655 |
| A-3 | 2 | DEFL | LM TRUN K-Y | D-17 | 10.523 | 1 1 | B-3 | 52 | Str. Ga. | LM TRUN +X | 92 | 9.9657 |
| A-4 | 3 | DEFL | LM TRUN K-Z | D-18 | 10.642 | | B-4 | 53 | Str. Ga. | RM TRUN +Z | 29 | 9.9659 |
| A-5 | 4 | DEFL | RM TRUN P-X | D-39 | 10.256 | | B-5 | 54 | Str. Ga. | RM TRUN +X | 30 | 9.9658 |
| A6 | 5 | DEFL | RM TRUN P-Y | D-40 | 10.526 | | B6 | 55 | Str. Ga. | 911DC-DBO | 33 | 10.000 |
| A-7 | 6 | DEFL | RM TRUN P-Z | D-41 | 10.643 | | B- 7 | 56 | Str. Ga. | 911CC-DB0 | 34 | 10.000 |
| A8 | | DEFL | LESB TRUN X-X | D-59 | 10.517 | | B8 | 57 | Str. Ga. | 911DC-DBI | 35 | 10.000 |
| A-9 | 8 | DEFL | LESE TRUN X-Y | D-60 | 10.582 | | B-9 | 58 | Str. Ga. | 911CC-DBI | 36 | 10.000 |
| A-10 | | DEFL | LESB TRUN X-Z | D-01 | 10.645 | | B-10 | 59 | Str. Ga. | 911DC-BAO | 3/ | 10.000 |
| A-11 | 10 | DEFL | RESE TRUN Y-X | D-62 | 10.534 | | B-11 | 60 | Str. Ca. | 911CC-BAO | 38 | 10.000 |
| A-12 | 1 | DEFL | RESB TRUN Y-Y | D-03 | 10.530 | | B-12 | 61 | Str. Ga. | 911DC-BAI | 39 | 10.000 |
| A-12 | 12 | DEFL | KESB IKUN I-Z | D-04 | 10.644 | | 8-13 | 62 | Str. Ga. | 91100-BA1 | 40 | 10.000 |
| A-14 | 12 | DEFL | KEEL U-X | D-30 | 10.641 | | B-14 | 63 | Str. Ga. | 9110-DJ-1A0 | 0 | 10.000 |
| A-15 | 14 | DEFL | KEEL U-I | D-3/ | 10.042 | | 8-13 | C4 | SET. Ga. | 9110-00-0001 | 41- | 10.000 |
| A-10 | 15 | DEFL | KEEL U-C | D-30 | 10.651 | | D-10 | 6 | Str. Ga. | 9110-DC-DAUL | 42= | 10.000 |
| A-17 | 10 | DEFL | 916AL-A U-A | D-51 | 10.631 | | D-1/ D 10 | 67 | Str. Ga. | 911DC-DAU | 43 | 10.000 |
| A-10 | 10 | DEFL | 916AL-A U-1 | D-31 | 10.323 | | B-10 | 67 | SEE. Ga. | | 44 | 10.000 |
| A-17 | 10 | DEFL | DIGAL-A U-Z | D-52 | 10.052 | | 5-19 P 20 | 60 | Str. Ga. | 9110C-DAI | · 45 | 10.000 |
| A-21 | 20 | DEFL | FCRC 7-V | D-65 | 10.501 | | D-20 P 21 | 70 | Str. Ga. | DIIC N' DAOT | 40 | 10.000 |
| A-21 | 20 | DEFL | ESDS 4-A | D-03 | 10.527 | | D~21 P 22 | 70 | Str. Ga. | SIIC-DC-DAUL | 4/- | 10.000 |
| A-23 | 22 | DEFL | E355 2-1 FCBC 7-7 | D-67 | 10.012 | | D-22 P. 22 | 71 | Str. Ga. | 9110C-550 | 40 | 10.000 |
| A-24 | 22 | DEFL | 016AF U_V | D-56 | 10.045 | | B-23 B-24 | 72 | Str Ca | GIIDC_BRT | 50 | 10.000 |
| A-25 | 26 | DEFE | 016AF 4-7 | D-58 | 10.552 | | B-24 B-25 | 75 | Str Ca | 9110C-BBI | 51 | 10.000 |
| A-26 | 25 | DEFT | 920FF (-Y | D-05 | 10 641 | 1 | B-26 | 75 | Str Ca | 911C-DC-BROT | 52# | 10.000 |
| A-27 | 26 | DEFT | 920FF C-7 | D-23 | 10 650 | | B-27 | 76 | Str Ca | 911DI_TRO | 53 | 10.000 |
| A-28 | 27 | DEFL | 911C-DF N-Y | D-34 | 10.581 | | 5-28 | 77 | Str Ca | 911CI-TBO | 54 | 10.000 |
| A-29 | 28 | LOAD CELL | 916AG XY | L-10-6 | 10,534 | | B-29 | 78 | Str. Ga. | 911nJ-IBI | 55 | 10,000 |
| A-30 | 29 | LOAD CELL | 920FI Z | L5-4 | 9,985 | | B-30 | 79 | Str. Ga. | 911CJ-IBI | 56 | 10.000 |
| A-31 | 30 | LOAD CELL | 920FD Z | L5-2 | 9.982 | | B-31 | 80 | Str. Ga. | 911C-DJ-IBOI | 57* | 10.000 |
| A-32 | 31 | LOAD CELL | 911CI XZ | 20-65 | 9.900 | | B-32 | 81 | Str. Ga. | 911DJ-KBO | 58 | 10.000 |
| A-33 | 32 | • | | | | | B-33 | 82 | Str. Ga. | 911CJ-KBO | 59 | 10.000 |
| A-34 | 33 | | | | | | B-34 | 83 | Str. Ga. | 911DJ-KBI | 60 | 10.000 |
| A-35 | 34 | | | | | | B35 | 84 | Str. Ga. | 911CJ-KBI | 61 | 10.000 |
| A36 | 35 | ••. | | 1 | | | B-36 | 85 | Str. Ga. | 911C-DJ-KBOI | 62* | 10.000 |
| ∧- 37 | 36 | Str. Ga. | RM TRUN -Z | 31 | | | B-37 | 86 | Str. Ga. | 911DJ-1A0 | 63 | 10.000 |
| A-38 | 37 | Str. Ga. | LM TRUN -Z | 91 | | | B-38 | 87 | Str. Ga. | 911CJ-IAO | 64 | 10.000 |
| A-39 | 38 | Str. Ga. | RM TRUN -X | 32 | | | B-39 | 88 | Str. Ga. | 911DJ-IAI | 65 | 10.000 |
| A-40 | 39 | Str. Ga. | LM TRUN -X | 90 | | | B-40 | 89 | Str. Ga. | 911CJ-IAI | 66 | 10.000 |
| A-41 | 40 | LOAD CELL | RESB TRUN Z | L10-5 | 9.983 | | B-41 | 90 | Str. Ga. | 911C-DJ-IAI | 67 | 10.000 |
| A-42 | 41 | LOAD CELL | LESB TRUN Z | L12-10 | 10.530 | | B-42 | 91 | Str. Ga. | 911DJ-KAO | 68 | 10.000 |
| A-43 | 42 | LOAD CELL | 916AL XZ | L10-7 | 10.538 | | B-43 | 92 | Str. Ga. | 911CJ-KAO | 69 | 10,000 |
| A-44 | 43 | LOAD CELL | 916AA XZ | L10-8 | 10.534 | | P-44 | 93 | Str. Ga. | 911DJ-KAI | 70 | 10.000 |
| A-45 | 44 | LOAD CELL | 911K XZ | 20-58 | 9.967 | | B-45 | 94 | Str. Ga. | 911CJ-KAI | 71 | 10.000 |
| A-46 | 45 | LOAD CELL | 911CB X2 | 20-59 | 9.928 | | B-46 | 95 | Str. Ga. | 911C-DJ-KAOI | 72* | 10.000 |
| A-47 | 46 | LOAD CELL | 916AF XZ | L10-9 | 10.534 | | B-47 | 96 | Str. Ga. | 911DC-920FCAOU | 73 | 10.000 |
| A-48 | 47 | LOAD CELL | 911CD XZ | 20-73 | 9.965 | | B-45 | 97 | Str. Ga. | 911DC-920FCAOL | 74 | 10.000 |
| A-49 | 48 | LUAD CELL | 920FA-L XZ | 29-77 | 9.931 | | 8-49 | 98 | Str. Ga. | 911DC-920FCAIU | | 10.000 |
| N-20 | 49 | LUAD CELL | 920FF-G XZ | 20-76 | <u>9</u> 933 | | 8-50 | 99 | Str. Ga. | 911DC-920FCAIL | /6 | 10.000 |

*Combined Gages

Channels A-24 through B-13 were used for 40 channel scan of selected information. TABLE IV B.- INSTRUMENTATION HOOK-UP, "LIFTOFF" TEST

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| CHAN | NO. | | | | <u> </u> | 1 | CHAN | NO. | | | T | |
|---------------|------|----------|----------------------------------|---------------|-------------------|---|---------------|------|--------------|--------------------------|--------------------|-------------------|
| SIG. CONDT | SCAN | FUNCT. | LOCATION | IDENT. NO. | VOLT @ GACE | | SIG. CONDT | SCAN | FUNCT. | LOCATION | IDENT. NO. | VOLT @ GAGE |
| C-1 | 100 | PWR SUPP | C REF Vo | | 10.004 | | D-1 | 150 | PWR SUPP | D REF Vo | | 10.240 |
| | 101 | Str. Ga. | 911DC-920FCB00 9110C-920FCB00 | 78 | 10.004 | | D-2 | 151 | DEFL | 920FF L-I 911C_DF N_Y | D-00 | 9.992 |
| C-4 | 103 | Str. Ga. | 911DC-920FCB1U | 70 | 10.004 | | D-4 | 153 | DEFL | 911C/DL-A J-X | D-13 | 9.997 |
| c-s | 104 | Str. Ga. | 911DC-920FCBIL | 80 | 10.004 | | D5 | 154 | DEFL | 911C/DL-A J-Y | D-14 | 10.018 |
| C-6 | 105 | Str. Ga. | 911DF-920FFAUU | 81 | 10.004 | | D-6 | 155 | DEFL | 911C/DL-A J-2 | D-15 | 9.993 |
| C-7 | 106 | Str. Ga. | 911DF-920FFAOL | 82 | 10.004 | | D-7 | 156 | DEFL | 920FL-A A-X | D-01 | 9.976 |
| C-8 | 107 | Str. Ga. | 911DF920FFALU | 83 | 10.004 | | D-8 | 157 | DEFL | 920FL-A A-Y | D02 | 10.000 |
| C-9 | 108 | Str. Ga. | 911DF-920FFA1L | 84 | 10,004 | | D9 | 158 | DEFL | 920FL-A A-Z | D-21 | 9.995 |
| C-10 | 109 | Str. Ga. | 911DF-920FFBOU | 85 | 10.004 | | D-10 | 159 | DEFL | 920FC B-X | D-03 | 9.988 |
| 0-11 | 110 | Str. Ga. | 911DF-920FFBOL | 86 | 10.004 | | 0-11 | 160 | DEFL DEFL | 920FC B-Y | D-04 | 9.985 |
| C-12 C-13 | 111 | Str. Ga. | 9110F-920FFB10 0110F 020FFB10 | 6/ 60 | 10.004 | | D-12 | 161 | DEFL | 920EC D-2 916AC V_V | D-22 | 10 000 |
| C-14 | 112 | SUL 08. | 911Dr-920ribil | 60 | 10.004 | | D-13 | 163 | DEFL | 916AC V-X | D-54 | 9,993 |
| C-15 | 114 | | | | | | D = 14 | 164 | DEFL. | 916AC V-2 | D-55 | 9,992 |
| C-16 | 115 | | | | | | D-16 | 165 | DEFL | 936BC S-Y | D-46 | 10.002 |
| C-17 | 116 | | | | | | D-17 | 166 | DEFL | 936BC S-Z | D-47 | 9.995 |
| C-18 | 117 | Str. Ga. | 911DC-920FFUL | 93* | 10.004 | | D-18 | 167 | DEFL | 936CC Q-Y | D-42 | 9.994 |
| C-19 | 118 | Str. Ga. | 911CC-916AFUL | 94* | 10.004 | | D-19 | 168 | DEFL | 936CC Q-Z | D-43 | 9.996 |
| C-20 | 119 | Str. Ga. | / 911DC-920FAUL | 95* | 10.004 | | D-20 | 169 | DEFL | 936DC HY | D-11 | 9.999 |
| C-21 | 120 | Str. Ga. | 911CC-916AAUL | 96* | 10,004 | | D-21 | 170 | DEFL | 936DC H-Z | D-26 | 9.995 |
| C-22 | 121 | | | | | 1 | D-22 | 171 | DEFL | 936EC F-Y | D-09 | 9.990 |
| C-23 | 122 | | | | | | D-23 | 1/2 | DEFL | 936EC F-2 | 1~24 | 9.990 |
| C-24 | 123 | | | | | | D-24 | 173 | DEFL | 930DF 1-1 036PF T-7 | D-48 | 9.991 |
| C-25 | 124 | | | | | | D-25 | 175 | DEFL | 936CF R-Y | D-00 | 9,996 |
| C-20 | 125 | | | | | | D-20 | 176 | DEFL | 936CF R-2 | D-45 | 9,994 |
| C-28 | 127 | | | | | | D-28 | 177 | DEFL | 936DF I-Y | D-12 | 10.000 |
| C-29 | 128 | | | | | | D-29 | 178 | DEFL | 936DF I-Z | D-27 | 9.995 |
| C-30 | 129 | | | | | | D-30 | 179 | DEFL | 936EF G-Y | D-10 | 10.000 |
| C-31 | 130 | Str. Ca. | TRAY | 105 | 10.004 | | D-31 | 180 | DEFL | 936EF G-2 | D-25 | 9.993 |
| C-32 | 131 | Str. Ga. | TRAY | 106 | 10.004 | | D-32 | 181 | DEFL | 911C/DD L-Y | D-19 | 9.993 |
| C-33 | 132 | Str. Ga. | TRAY | 107 | 10.004 | | D-33 | 182 | DEFL | 911C/DD L-Z | D-20 | 10.002 |
| C-34 | 133 | Str. Ga. | TRAY | 108 | 10.004 | | D-34 | 183 | DEFL | 911C-DF N-Z | D-35 | 9.989 |
| C-35 | 134 | | - | | | | D-35 | 184 | AUAL | TEST SIK PILC | | |
| C-30 | 135 | | | | | | D-30 D-37 | 185 | DEEL | ILDI SIK KULL | V D_70 | 9 983 |
| C-39 | 130 | | | | | | D-38 | 187 | DEFL | IM TEST STRU | | 9,991 |
| C-30 | 138 | | | | | | D-30 | 188 | DEFL | IM TEST STRU | $z = \frac{D}{12}$ | 9.990 |
| C-40 | 139 | | | | | | D-40 | 189 | DEFL | RM TEST STRU | K D-73 | 9.995 |
| C-41 | 140 | | | | | | D-41 | 190 | DEFL | RM TEST ST.U | 7 D-74 | 9.998 |
| C-42 | 141 | | | • | | | D-42 | 191 | DEFL | RM TEST STRU | z D75 | 10.000 |
| C-43 | 142 | | | | • | | D-43 | 192 | DEFL | LE TEST STRU | K D-76 | 9.996 |
| C-44 | 143 | | | | | | D-44 | 193 | DEFL | LE TEST STRU | (D-77 | 9.997 |
| C-45 | 144 | DEFL | 911C/DE M-Y | D-31 | 10.558 | | D-45 | 194 | DEFL | LE TEST STRU | Z D-78 | 9.995 |
| C-46 | 145 | DEFL | 911C/DE M-Z | D-68 | 9.707 | | D-46 | 195 | DEFL | RE TEST STRU | K D-32 | 10.005 |
| C-47 | 146 | DEFL | 936BC-BI CC | D-29 | 9.706 | | D-47 | 196 | DEFL | RE TEST STRU | (D-69 | 10.002 |
| C-48 | 14/ | DEFL | YJOEC-EL BB | U-30 70 a | 9./04 | | D-48 | 100 | | RE TEST SIKU | 0-11 | 10.002 |
| C-49 | 140 | DEFL | 930LU-920LB D | D-07 | 9.714 | | D-49 D-50 | 100 | AUAL | PM TRUN PILCH | 0-12 | |
| L | 147 | DELF | 730EC-920ED E | 000 | 9.703 | | 00 | 732 | NULL | MA INON ROLL | 1 4-12 | |

*Combined Gages

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TABLE IV B. (CONTD.)- INSTRUMENTATION HOOK-UP, "LIFTOFF" TEST

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| CHAN | NO. | | 1 | | T | 7 | CHAN | NO. | l | | 1 | [|
|---------|-------------|-----------|----------------|--------------|----------|-----|-----------------|------|----------|----------------|-------------|--------|
| | | | ļ. | | VOLT. | 1 | - | r | 4 | | | VOLT. |
| SIG. | SCAN | FUNCT. | LOCATION | IDENT. | e | 1 | SIG. | SCAN | FUNCT. | LOCATION | IDENT. | e |
| CONDT | | | 1 | NO. | GAGE | | CONDT | ļ | | | NO. | GAGE |
| 1 | | | | | | 1 | | | | | | |
| A-1 | 0 | PWR SUPP | A REF VO | | 10.850 | 1 | B-1 | 50 | PWR SUPP | B REF Vo | | 10.000 |
| A-2 | | DEFL | LA TRUN K-X | D-16 | 10.561 | | 8-2 | 51 | Str. Ga. | LM TRUN +Z | 89 | 9.9655 |
| | 1 5 | DEFL | LA IRUN K-I | D-17 | 10.523 | | B-3 | 52 | Str. Ga. | LM IKUN +X | 92 | 9.965/ |
| A-4 | | DEFL | DM WOIDE D Y | D-18 | 10.042 | 1. | 5-4 | 23 | Str. Ga. | RM TRUN +Z | 29 | 9.9659 |
| 1 | 4 | DEFL | DM TDIDY D V | D-39 | 10.250 | İ | 0-0 | 54 | Str. Ga. | KM IKUN +A | | 9.9038 |
| A-0 | | DEFL | DM TRUN P-I | D-40 | 10.520 | 1 | 8-0 | 22 | Str. Ga. | 911DC-DBO | 33 | 10.000 |
| A_8 | 7 | DEFL | I FOR TRUN F-2 | D-41 D 50 | 10.043 | | D-/ | 20 | SER. Ga. | 911CC-DBU | 34 | 10.000 |
| A_9 | | DEFL | LEGB TRUN X-X | D-59 | 10.517 | 1 | D-0 B 0 | 59 | Str. Ga. | | 25 | 10.000 |
| 4-10 | ő | DEFL | LESS INCA A-I | D-00 | 10.502 | | D-7 | 50 | Str. Ga. | OLIDO PAO | 20 | 10.000 |
| A-11 | 10 | DEFL | DESB TRIN V-Y | D-61 | 10.045 | | B-10 B-11 | 60 | Str. Ga. | 9110C-BAO | 20 | 10.000 |
| A-12 | 11 | DEFL | RESD TRUN Y-V | D=63 | 10.530 | 1 | 8_12 | 61 | str Ca | 911CC-BAU | 30 | 10.000 |
| A-13 | 12 | DEFI | PESE TRIN V-7 | D-64 | 10 644 | | B-13 | 62 | Ser Ca | 911CC_BAT | 40 | 10.000 |
| A-14 | 113 | DEFL. | KEEL O-Y | D-36 | 10 641 | 1 | B = 14 | 63 | Str Ca | 911C-DI-TAO | | 10.000 |
| A-15 | 14 | DEFL / | KEEL 0-Y | D=37 | 10.642 | | B-15 | 64 | Str. Ca | 911C-DC-DBOT | 41 ± | 10,000 |
| A-16 | 15 | DEFL | KFFL 0-7 | D-38 | 10.651 | | B-16 | 65 | Str Ga | 911C-DC-BAOT | 42* | 10.000 |
| A-17 | 16 | DEFL | 916AL-A U-X | D-50 | 10.651 | | B-17 | 66 | Str. Ga. | 911DC-DAO | 43 | 10.000 |
| A-18 | 17 | DEFL | 916AL-A U-Y | D-51 | 10.523 | | B-18 | 67 | Str. Ga. | 911CC-DAO | 44 | 10.000 |
| A-19 | 18 | DEFL | 916AL-A U-Z | D-52 | 10.652 | | B-19 | 68 | Str. Ga. | 911DC-DAI | 45 | 10.000 |
| A-20 | 19 | DEFL | 916AF W-Y | D-57 | 10.581 | | B-20 | 69 | Str. Ga. | 911CC-DAI | 46 | 10.000 |
| A-21 | 20 | DEFL | ESBS Z-X | D-65 | 10.527 | 1 | 5-21 | 70 | Str. Ga. | 911C-DC-DAOI | 47* | 10.000 |
| A-22 | 21 | DEFL | ESBS Z-Y | D-66 | 10.612 | | B-22 | 71 | Str. Ga. | 911DC-BBO | 48 | 10.000 |
| A-23 | 22_ | DEFL | ESES Z-Z | D-67 | 10.645 | | B-23 | 72 | Str. Ga. | 911CC-BBO | 49 | 10.000 |
| A-24 | 23 | DEFL | 916AF W-X | D-56 | 10.532 |] | B-24 | 73 | Str. Ga. | 911DC-BBI | 50 | 10.000 |
| A25 | 24 | DEFL | 916AF W-2 | D-58 | 10.646 | [[| B-25 | 74 | Str. Ga. | 911CC-BBI | 51 | 10.000 |
| A-26 | 25 | DEFL | 920FF C-X | D-05 | 10.641 | | B-26 | 75 | Str. Ga. | 911C-DC-BB01 | 52* | 10.000 |
| A-27 | 26 | DEFL | 920FF C-Z | D-23 | 10.650 | () | B-27 | 76 | Str. Ga. | 911DJ-IBO | 53 | 10.000 |
| A-28 | 27 | DEFL | 911C-DF N-Y | D-34 | 10.581 | | B-28 | 77 | Str. Ga. | 911CJ-IBO | 54 | 10.000 |
| A-29 | 28 | | - | | | ((| B-29 | 78 | Str. Ga. | 911DJ-IBI | 55 | 10.000 |
| A-30 | 29 | | | | | | B-3 0 | 79 | Str. Ga. | 911CJ-IBI | 56 | 10.000 |
| A-31 | 30 | | | | | | B-31 | 80 | Str. Ga. | 911C-DJ-IBOI | 57* | 10.000 |
| A-32 | 31 | | | | | | B-32 | 81 | Str. Ga. | 911DJ-KBO | 58 | 10.000 |
| A-33 | 32 | | | | | | B-33 | 82 | Str. Ga. | 911CJ-KBO | 59 | 10.000 |
| A-34 | 33 | | | | | | B-34 | 83 | Str. Ga. | 911DJ-KBI | 60 | 10.000 |
| A-35 | 34 | | | | | | B-35 | 84 | Str. Ga. | 911CJ-KBI | 61 | 10.000 |
| A-36 | 35 | LOAD CELL | KEEL Y | 50-23 | 10.518 | [] | B-36 | 85 | Str. Ga. | 911J-DJ-KBOI | 62* | 10.000 |
| A-37 | 36 | Str. Ga. | KM TRUN -Z | 31 | | 1 | B-37 | 86 | Str. Ga. | 911DJ-IAO | 63 | 10.000 |
| 86-A | 3/ | str. Ga. | LM TRUN -Z | 31 | | | B-38 | 87 | Str. Ga. | 911CJ-IA0 | 64 | 10.000 |
| A-39 | 30 | STT. Ga. | KMITKUN ~X | 32 | | | 5-39 | 88 | Str. Ga. | YI IDJ-IAI | 65 | 10.000 |
| A-40 | 39 | STT. GA. | LAT TRUN -X | 90 1 10 F | 0.000 | | 5-40 | 89 | Str. Ga. | 911CJ-IAL | 66 | 10.000 |
| A-41 | 40 | LOAD CELL | KLOB IKUN Z | 110-5 | 9.982 | | 5-41 5 / 1 | 90 | Str. Ga. | 9110-DJ-1A1 | 6/ | 10.000 |
| A-42 | 41 | LOAD CELL | LLOB TRUN Z | L12-10 | 10.529 | | B-42 | 91 | Str. Ga. | 911DJ-KAU | 68 | TO 000 |
| A-43 | 42 | LOAD CELL | | 110-6 | 10.020 | | B-43 | 62 | SET. Ga. | 911CJ-KAU | 70 | 10.000 |
| A-45 | 44 | LOAD CELL | 011D, V | 110-7 | 10.534 | | B-44 | 0/ | 51". Ga. | 9110J-KAL | 70 | 10.000 |
| A-46 | 25 | LOAD CELL | | 110_0 | 10.530 | | B-46 | 05 | Str Ca | 911C-DI-KAOT | 72 | 10.000 |
| A-47 | 46 | LOAD CELL | 9110C V | 15-4 | 9 9 9 77 | | B_47 | 96 | Str Ca | 911DC_920ECA01 | 72 | 10,000 |
| A-48 | 47 | LOAD CELL | 911CG Y | 1.5-2 | 9,968 | | R-49 | 97 | Str. Ca | 911DC_920FCA00 | 73 | 10.000 |
| A-49 | 48 | | | | | | B-49 | 98 | Str. Ca. | 9110C-920FCATH | 75 | 10,000 |
| A-50 | 49 | | | | | | B-50 | 99 | Str. Ca. | 911DC-920FCATI | 76 | 10,000 |
| · · · · | | | | | | | | | | | | |

*Combined Gages

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Channels A-24 through B-13 were used for 40 channel scan of selected information.

TABLE IV C. - INSTRUMENTATION HOOK-UP, "KEEL" TEST

STATE CONTRACT OF STATE

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| CHAN | NO. | | 1 | | [| } | CHAN | NO. | 1 | | | |
|------------|------|----------|----------------|---------|--------|-----|--------|-------|----------|-------------------------|--------------|---------|
| | | | | | VOLT | | | | | 1001770 | | VOLT |
| SIG. | SCAN | FUNCT. | LOCATION | IDENT. | GACE | | SIG. | SCAN | FUNCT. | LOCATION | IDENI. | GAGE |
| | | | | | - ONGL | { | | | | | | |
| C-1 | 100 | PWR SUPP | C REF Vo | | 10.004 | ĺ | D-1 | 150 | PWR SUPP | D REF Vo | | 10.240 |
| C-2 | 101 | Sor. Ga. | 911DC-920FCBOU | 77 | 10.004 | | D-2 | 151 | DEFL | 920FF C-Y | D-06 | 9.992 |
| C-3 | 102 | Str. Ga. | 911DC-920FCBOL | 78 | 10.004 | | D-3 | 152 | DEFL | 911C-DF N-X | D-33 | 10.010 |
| C-4 | 103 | Str. Ga. | 911DC-920FCBIU | 79 | 10,004 | | D-4 | 153 | DEFL | 911C/LL-A J-X | D-13 | 9.997 |
| C-5 | 104 | Str. Ga. | 911DC-920FCBIL | 80 | 10.004 |] | D5 | 154 | DEFL | 911C/DL-A J-Y | D-14 | 10.018 |
| C-6 | 105 | Str. Ga. | 911DF-920FFA0U | 81 | 10.004 | | D-6 | 155 | DEFL | 911C/DL-A J-Z | D-15 | 9.993 |
| C7 | 106 | Str. Ga. | 911DF-920FFAOL | 82 | 10.004 | ļ | D-7 | 156 | DEFL | 920FL-A A-X | D-01 | 9.976 |
| C-8 | 107 | Str. Ga. | 911DF-920FFAIU | 83 | 10.004 | | D-8 | 157 | DEFL | 920FL-A A-Y | D-02 | 10.000 |
| C-9 | 108 | Str. Ga. | 911DF-920FFA1L | 84 | 10.004 | 1 | D-9 | 158 | DEFL | 920°L-A A-Z | D-21 | 9.995 |
| 0-10 | 109 | Str. Ga. | 911DF-920FFBOU | 85 | 10.004 | | D-10 | 159 | DEFL | 920rC B-X | 0-03 | 9.388 1 |
| C-11 | 110 | Str. Ga. | 911DF-920FF80L | 86 | 10.034 | | D-11 | 160 | DEFL | 920FC B-Y | D-04 | 9.985 |
| | 111 | Str. Ga. | 911DF-929FFB10 | 8/ | 10.004 | | 1 2 12 | 1 161 | DEFL | 920FC B-Z | 0-22 | 9.993 |
| | 112 | Str. Ga. | 9110F-920FFB1L | 88 | 10.004 | ļ | D-13 | 162 | DEFL | 916AC V-X | D-53 | 10.000 |
| 1 - 14 | 113 | | | | | 1 | D-14 | 103 | DEFL | 1910AL V-I | D-34 | 1 2.223 |
| C 16 | 114 | i | | : | | | 0-13 | 164 | DEFL | 910AC V-2 | D-33 | 10.002 |
| 10^{-10} | 115 | | | | | Į į | D-10 | 102 | DEFL | 193080 5-1 10360 C.7 | 0-40 | 10.002 |
| 0.19 | 110 | s - c | 01100 020000 | 024 | 10 004 | | D-17 | 100 | DEFL | 9305 5-2 036cc 0 V | D-47 | 9.995 |
| | 11/ | S E. GL. | 911 C-920FFUL | 93* | 10.004 | 1 | D-18 | 16/ | DEFL | 930LL Q-1 | D-42 | 9.554 |
| C-20 | 110 | Str. Ja. | OILDC OCOFAUL | 94* | 10.004 | | D-19 | 160 | DEFL | 9360C Q-2 | D-45 | 0 000 |
| C_{-21} | 120 | Str. (1. | 911DC-920FAUL | 93* | 10.004 | 1 | D-20 | 170 | DEFL | 936DC H-1 | D-11 D-26 | 0 005 |
| 0-21 | 120 | SLL. Ud. | JIICC-JIVAAUL | 90* | 10.004 | ł | D-21 | 170 | DEFL | 936DC R-2 | D-20 | 0.000 |
| C-22 | 122 | | | | | | D-22 | 172 | DEFL | 936EC F-1 | D-05 | 0 000 |
| C-24 | 122 | | | | | | D-23 | 173 | DEFL | 9368F T_Y | D-24 | 9,991 |
| C-25 | 124 | | | | | | D-24 | 174 | DEFL | 936BF T-Z | D-80 | 9.999 |
| C-26 | 125 | | | | | | D-26 | 175 | DEFT. | 936CF R-Y | D-44 | 9,996 |
| C-27 | 126 | | | | | i | D-27 | 176 | DEFL | 936CF R-Z | D-45 | 9.994 |
| C-28 | 127 | | | | | | D-28 | 177 | DEFL | 936DF I-Y | D-12 | 10.000 |
| C-29 | 128 | | | | | | D-29 | 178 | DEFL | 936DF I-Z | D-27 | 9.995 |
| C-30 | 129 | | | | | [| D-30 | 179 | DEFL | 936EF G-Y | D-10 | 10.000 |
| C-31 | 130 | Str. Ga. | TRAY | 105 | 10.004 | | D-31 | 180 | DEFL | 936EF G-Z | D-25 | 9.993 |
| C-32 | 131 | Str. Ga. | TRAY | 106 | 10.004 | | D-32 | 181 | DEFL | 911C/DD L-Y | D-19 | 9.993 |
| C-33 | 132 | Str. Ga. | TRAY | 107 | 10.004 | | D-33 | 182 | DEFL | 911C/DD L-2 | D-20 | 10.002 |
| C-34 | 133 | Str. Ga. | TRAY | 108 | 10.004 | | D-34 | 183 | DEFL | 911C-DF N-Z | D-35 | 9.989 |
| C-35 | 134 | | | | | | D-35 | 184 | AOAI | TEST STR PITCH | Q-10 | |
| C-36 | 135 | | | | | | D-36 | 185 | AOAI | TEST STR ROLL | Q-9 | |
| C-37 | 136 | | | | | | D-37 | 186 | DEFL | LM TEST STRU X | D70 | 9.983 |
| C-38 | 137 | 1 | | | | | D-38 | 187 | DEFL | LM TEST STRU Y | D-71 | 9.991 |
| C-39 | 138 | | | | | | D-39 | 188 | DEFL | LM TEST STRU Z | D-72 | 9.990 |
| C-40 | 139 | • | | | | | D-40 | 189 | DEFL | RM TEST STRU X | D-73 | 9.995 |
| C-41 | 140 | | | | | | D-41 | 190 | DEFL | RM TEST STRU Y | D-74 | 9.998 |
| C-42 | 141 | | | | | | D-42 | 191 | DEFL | RM TEST STRU Z | D-75 | 10.000 |
| C-43 | 142 | | | | | | D-43 | 192 | DEFL | LE TEST STRU X | D-76 | 9.996 |
| C-44 | 143 | | | | | | D-44 | 193 | DEFL | LE TEST STRU Y | D-77 | 9.997 |
| C-45 | 144 | DEFL | 911C/DE M-Y | D-31 | 10.558 | | D-45 | 194 | DEFL | LE TEST STRU Z | D-78 | 9.995 |
| C-46 | 145 | DEFL | 911C/DE M-Z | D-68 | 9.707 | | D-46 | 195 | DEFL | RE TEST STRU X | D-32 | 10.005 |
| C-47 | 146 | DEFL | 936BC-BI CC | D-29 | 9.706 | | D-47 | 196 | DEFL | RE TEST STRU Y | D-69 | 10.002 |
| C-48 | 147 | DEFL | 936EC-EI BB | D-30 | 9.704 | | D-48 | 197 | DEFL | RE TEST STRU Z | 10-79 | 10.002 |
| C-49 | 148 | DEFL | 936EC-920FB D | D-07 | 9.714 | | D-49 | 198 | AOAL | KM TRUN PITCH | 10-11 | |
| C-20 | 149 | DEFL | 936EC-920FD E | 008 | 9.705 | | D-20 | 1793 | AUAI | KM TRUN KULL | 14-12 | 1 [|

*Combined Gages

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TABLE IV C. (CONTD.)- INSTRUMENTATION HOOK-UP, "KEEL" TEST

| CHAN | NO. | | | 1 | 1 |] [| CHAN | NO. | | | 1 | <u> </u> |
|----------|----------|-----------|---------------|---------------|--------|-----|--------------|-----------|----------|----------------|--------|----------|
| L | | | { | { | VOLT. | | | | | 1 | Í | VOLT. |
| SIG. | SCAN | FUNCT. | LOCATION | IDENT. | e | 11 | SIG. | SCAN | FUNCT. | LOCATION | IDENT. | l e |
| CONDT | } . | | 1 | NO. | GAGE | | CONDT | | | ļ | NO. | GAGE |
| | | | ····· | } | | 1 | | | | <u> </u> | f | |
| A-1 | 0 | PWR SUPP | A REF Vo | | 10.850 | | B-1 | 50 | PWR SUPP | B REF Vo | | 10,000 |
| A-2 | | DEFL | LM TRUN K-X | D-16 | 10.561 | | B-2 | 51 | Str. Ga. | LM TRUN +Z | 89 | 9.9655 |
| A-3 | 2 | DEFL | LH TRUN K-Y | D-17 | 10.523 | 1 1 | B-3 | 52 | Str. Ga. | LM TRUN +X | 92 | 9.9657 |
| A-4 | 3 | DEFL | LM TRUN K-Z | <u>1</u> 2–18 | 10.642 | | B-4 | 53 | Str. Ga. | RM TRUN +Z | 29 | 9,9659 |
| A-3 | 4 | DEFL | RM TRUN P-X | D-39 | 10.256 | 1 1 | 8-5 | 54 | Str. Ga. | RM TRUN +X | 30 | 9.9658 |
| A-0 | 2 | DEFL | RM TRUN P-Y | 0-40 | 10.526 | 1 | 8-0 | 22 | Str. Ga. | 911DC-DBO | 33 | 10.000 |
| A-/ | 0 | DEFL | KM TKUN P-Z | D-41 | 10.643 | | 8-/ | 20 | Str. Ga. | 911CC-DB0 | 34 | 10.000 |
| A-0 | | DEFL | LESB IKUN A-A | D-39 | 10.517 | } } | D-0 | 5/ | S.r. Ga. | 911DC-DB1 | ~ 33 | 10.000 |
| A-9 | , a | DEFL | LESB IKUN A-I | D=00 | 10.582 | | 5-9 | 20 | Str. Ga. | 91100-081 | 00 | 1 10.000 |
| A-10 | | DEFL | LESS IKUN A-2 | D-01 | 10.045 | 1 1 | B-10 | 29 | Str. Ga. | 911DC-BAU | 1 37 | 10.000 |
| A-11 | 10 | DEFL | RESE IKUN I-A | D-02 | 10.534 | 1 1 | D-11 D-11 | 60 | Str. Ga. | 911CC-BAU | 20 | 10.000 |
| A-12 | 11 | DEFL | RESS IRUN 1-1 | D-03 | 10.550 | | D-12 | 01 | Str. Ga. | DILCC BAT | 33 | 10.000 |
| A-14 | 12 | DEFL | RESE INUN I-L | D-04 | 10.644 | | B-13 | 62 | Str. Ga. | 911CL-BAL | 40 | 10,000 |
| A-14 | 14 | DEFL | KEEL U-A | 0-30 | 10.641 | | B-14 B 16 | 60 | Str. Ga. | 911C-DJ-IAU | 1 41+ | 10.000 |
| A-16 | 14 | DEFL | KEEL 0-1 | D-37 | 10.042 | | B-12 B-16 | 64 | Str. Ga. | | 41. | 10,000 |
| A-10 | 15 | DEFL | (01641_A U-V | D50 | 10.031 | | B-10 B-17 | 66 | Str. Ga. | ALLOC DAG | 42 | 10,000 |
| A-19 | 17 | DEFL | OIGAL-X U-A | D-30 D 51 | 10.001 | | 9 19 | 60 | Str. Ga. | 9110C-040 | 43 | 10.000 |
| A-10 | 19 | DEFL | | D-52 | 10.525 | | B-10 B-10 | 40 | Str. Ca. | 911CC-DAU | 45 | 10.000 |
| A-20 | 10 | DEFL | | p-57 | 10.032 | | B-20 | 60 | Str. Ga. | 9110C-DAT | 45 | 10,000 |
| A-20 | 20 | DEFL | FSRS 7-Y | D-65 | 10.501 | | B-20 | 70 | Str. Ca. | 911C-DC-DAI | 47 | 10,000 |
| A-22 | 20 | DEFL | ESBS L-A | D-65 | 10.527 | | 8-22 | 70 | Str. Ca. | 9110-DC-DRUI | 48 | 10,000 |
| A-23 | 22 | DEFL | FSBS 7_7 | D-67 | 10.645 | | B-23 | 72 | Str. Ca. | 911CC_880 | 40 | 10,000 |
| A-24 | 23 | DEFL | 916AF W-X | D-56 | 10.532 | | B-24 | 71 | Str. Ga. | 911DC-BBT | 50 | 10,000 |
| A-25 | 24 | DEFL | 916AF W-Z | D-58 | 10.646 | | B-25 | 74 | Str. Ga. | 911CC-BBT | 51 | 10,000 |
| A-26 | 25 | DEFL | 920FF C-X | D-05 | 10.641 | | B-26 | 75 | Str. Ga. | 911C-DC-BBOT | 52* | 10.000 |
| A-27 | 26 | DEFL | 920FF C-Z | D-23 | 10.650 | | B-27 | 76 | Str. Ga. | 911DJ-1BO | 53 | 10.000 |
| A-28 | 27 | DEFL | 911C-DF N-Y | D-34 | 10.581 | | B-28 | 77 | Str. Ga. | 911CJ-1BO | 54 | 10.000 |
| A-29 | 28 | | | | | | B-29 | 78 | Str. Ga. | 911DJ-1BI | 55 | 10.000 |
| A-30 | 29 | | | | | | B-30 | 79 | Str. Ga. | 911CJ-IBI | 56 | 10.000 |
| A-31 | 30 | | | | | | B-31 | 80 | Str. Ga. | 911C-DJ-IBOI | 57* | 10.000 |
| A-32 | 31 | | - | | | | B-32 | 81 | Str. Ga. | 911DJ-KBO | 58 | 10.000 |
| A-33 | 32 | • | | | | | B-33 | 82 | Str. Ga. | 911CJ-KBO | 59 | 10.000 |
| A34 | 33 | | | | | | B-34 | 83 | Str. Ga. | 911DJ-KBI | 60 | 10.000 |
| A~35 | 34 | | | | | | B-35 | 84 | Str. Ga. | 911CJ-KBI | 61 | 10.000 |
| A36 | 35 | LOAD CELL | FESS Z | 50- 10 | 10.533 | 1 | B-36 | 85 | Str. Ga. | 911C-DJ-KBOI | 62* | 10.000 |
| A-37 | 36 | Str. Ga. | RM TRUN -2 | 31 | | | B-37 | 86 | Str. Ga. | 911DJ-IAO | 63 | 10.000 |
| A-38 | 37 | Str. Ga. | LM TRUN -Z | 91 | | | B-38 | 87 | Str. Ga. | 911CJ-IAO | 64 | 10.000 |
| A-39 | 38 | Str. Ga. | RM TRUN -X | 32 | | | B-39 | 88 | Str. Ga. | 911DJ-IAI | 65 | 10,000 |
| A-40 | 39 | Str. Ga. | LM TRUN -X | 90 | | | B-40 | 89 | Str. Ga. | 911CJ-IAI | 66 | 10,000 |
| A-41 | 40 | LOAD CELL | RESB TRUN Z | 50~98 | 10.543 | | B-41 | 90 | Str. Ga. | 911C-DJ-IAI | 67 | 10.000 |
| A-42 | 41 | LOAD CELL | LESB TRUN Z | 50-34 | 9.982 | | B-42 | 91 | Str. Ga. | 911DJ-KAO | 68 | 10,000 |
| A-43 | 42 | LOAD CELL | 916AA-L Z | L12-10 | 10.538 | | B-43 | 92 | Str. Ga. | 911CJ-KAO | 69 | 10.000 |
| A44 | 43 | LOAD CELL | 916AF-G Z | L10-7 | 10.580 | | B-44 | 93 | Str. Ga. | 911DJ-KA1 | 70 | 10.000 |
| A-45 | 44 | | | | | | B-45 | 94 | Str. Ga. | 911CJ-KAI | 71 | 10.000 |
| A-46 | 45 | | | | | . | B-46 | 95 | Str. Ga. | 911C-DJ-KAOI | 72* | 10.000 |
| A-47 | 46 | | | | | 1 | B-47 | 96 | Str. Ga. | 911DC-920FCAOU | 73 | 10.000 |
| A-48 | 47 | | | | | | B-48 | 97 | Str. Ga. | 911DC-920FCAOL | 74 | 10.000 |
| A-49 | 48 | | | _ | | . 1 | 8-49 | 98 | Str. Ga. | 911DC-920FCATU | 75 | 10.000 |
| A-50 | 49 | | | | | | B-20 | 99 | Str. Ga. | 911DC-920FCAIL | /6 | 10.000 |

*Combined Gages

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Channels A-24 through B-13 were used for 40 channel scan of selected information.

TABLE IV D.- INSTRUMENTATION HOOK-UP, "END SUPPORT BEAM" TEST

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| CHAN | NO. | | | [| 1 |] | CHAN | NO. | [| | | 1 |
|--------------|------|-----------------|----------------|-------------|--------|----------|--------------|-----------------|----------|----------------------------------|--------------|-----------|
| SIG. | SCAN | FUNCT. | LOCATION | IDENT. | VOLT | | \$1G. | SCAN | FUNCT. | LOCATION | IDENT. | VOLT e |
| CONDT | | | | NO. | CAGE | ļ | CONDI | | | | NO. | GAGE |
| C-1 | 100 | PWR SUPP | C REF Vo | | 10.004 | 1 1 | D-1 | 150 | PWR SUPP | D REF Vo | | 10.240 |
| C-2 | 101 | Str. Ga. | 911DC-920FCBOU | 77 | 10.004 | | D-2 | 151 | DEFI. | 920FF C-Y | D-06 | 9.992 |
| C-3 | 102 | Str. Ga. | 911DC-920FCBOL | 78 | 10.004 | i | D-3 | 152 | DEFL | 911C-DF N-X | D-33 | 10.010 |
| C-4 | 103 | Str. Ga. | 911DC-920FCBIU | 79 | 10.004 | | D-4 | 153 | DEFL | 911C/DL-A J-X | D-13 | 9.997 |
| C-5 | 104 | Str. Ga. | 911DC-920FCBIL | 80 | 10.004 | | D-5 | 154 | DEFL | 911C/DL-A J-Y | D-14 | 10.018 |
| C-6 | 105 | Str. Ga. | 911DF-920FFA0U | 81 | 10.004 | | D-6 | 155 | DEFL | 911C/DL-A J-Z | D-15 | 9.993 |
| C-7 | 106 | Str. Ga. | 911DF-920FFAOL | 82 | 10.004 | | D-7 | 156 | DEFL | 920FL-A A-X | D01 | 9.976 |
| C-8 | 107 | Str. Ga. | 911DF-920FFAIU | 83 | 10.004 | | D-8 | 157 | DEFL | 920FL-A A-Y | D-02 | 10.000 |
| C 10 | 108 | Str. Ga. | 911DF-920FFAIL | 84 | 10.004 | 1 | D-9 | 158 | DEFL | 920FL-A A-Z | D-21 | 9.995 |
| C-10 | 109 | Str. Ga. | 911DF-920FFBOU | 85 | 10.004 | | D-10 | 159 | DEFL | 920FC B-X | D-03 | 9.988 |
| C-12 | 110 | Str. Ga. | 911DF-920FFBUL | 00 97 | 10.004 | | D-11 D 12 | 160 | DEFL | | D-04 | 9.903 |
| C-12 C-13 | 112 | Str Ca | 911DF-920FFB10 | 89 | 10.004 | | D-12 D-13 | 162 | DEFL | 920FC D-2 916AC V-V | D-72 D-53 | 10 000 |
| C-14 | 113 | JUL. 04. | JIIDE-JEGEEDIL | | 10.004 | | D-13 | 163 | DEFL | | D=55 | 9,993 |
| C-15 | 114 | | | | | | D=15 | 164 | DEFT. | 916AC V-2 | D-55 | 9.992 |
| C-16 | 115 | | 1 | | 1 | 1 1 | D-16 | 165 | DEFL | 936BC S-Y | D-46 | 10.002 |
| C-17 | 116 | | | | | | D-17 | 166 | DEFL | 936BC S-Z | D-47 | 9.995 |
| C-18 | 117 | Str. Ga. | 911DC-920FFUL | 93* | 10.004 | | D-18 | 167 | DEFL | 936CC Q-Y | D-42 | 9.994 |
| C-19 | 118 | Str. Ga. | 911CC-916AFUL | 94* | 10.004 | | D-19 | 168 | DEFL | 936CC Q-Z | D-43 | 9.996 |
| C-20 | 119 | Str. Ga. | 911DC-920FAUL | 95 * | 10.004 | | D-20 | 16 [^] | DEFL | 936DC H-Y | D-11 | 9.999 |
| C-21 | 120 | Str. Ga. | 911CC-916AAUL | 96* | 10.004 | | D-21 | 170 | DEFL | 936DC H-Z | D-26 | 9.995 |
| C-22 | 121 | Str. Ga. | ESB | 97 | 10.004 | | D-22 | 171 | DEFL | 936EC F-Y | D-09 | 9.990 |
| C-23 | 122 | Str. Ga. | ESB | 98 | 10.004 | | D-23 | 172 | DEFL | 936EC F-Z | D-24 | 9.990 |
| C-24 | 123 | Str. Ga. | ESB | 99 | 10.004 | | D-24 | 173 | CEFL | 936BF T-Y | D-48 | 9.991 |
| C-25 | 124 | Str. Ga. | ESB | 100 | 10.004 | [| D-25 | 174 | DEFL | 936BF T-Z | D-60 | 9.995 |
| C-20 | 123 | Str. Ga. | ESB | 101 | 10.004 | | D-26 | 1/5 | DEFL | 936CF R-Y | D-44 | 9.996 |
| C-27 | 120 | Str. Ua. | LOD FCD | 102 | 10.004 | | D-27 | 170 | DEFL | 9300F K-2 | D-45 D-12 | 9.994 |
| C-29 | 128 | Str Ca. | FSB | 105 | 10.004 | | D-20 D-29 | 178 | DEFL | 936DF 1-1 | D-12 D-27 | 9,995 |
| C-30 | 129 | Str. Ga. | ESB | 104 | 10.004 | | D-29 | 170 | DEFL | 936FF C-Y | D=10 | 10.000 |
| C-31 | 130 | Str. Ga. | ESB - | ĩió | 10.004 | | D-31 | 180 | DEFL | 936EF G-Z | D-25 | 9,993 |
| C-32 | 131 | Str. Ga. | ESB | 111 | 10.004 | | D-32 | 181 | DEFL | 911C/DD L-Y | D-19 | 9.993 |
| C-33 | 132 | Str. Ga. | ESB | 112 | 10.004 | | D-33 | 182 | DEFL | 911C/DD L-Z | D-20 | 10.002 |
| C-34 | 133 | Str. Ga. | ESB | 113 | 10.004 | 1 | D-34 | 183 | DEFL | 911C-DF N-2 | D-35 | 9.989 |
| C-35 | 134 | Str. Ga. | ESB | 114 | 10.004 | | D-35 | 184 | IAOA | TEST STR PITC | Q-10 | |
| C-36 | 135 | Str. Ga. | ESB | 115 | 10.004 | | D-36 | 185 | AOAI | TEST STR ROLL | Q-9 | _ |
| C-37 | 136 | Str. Ga. | ESB | 116 | 10.004 | | D-37 | 186 | DEFL | LM TEST STRU λ | D70 | 9.983 |
| C-38 | 137 | Str. Ga. | TRAY | 105 | 10.004 | | D-38 | 187 | DEFL | LM TEST STRU Y | D-71 | 9.991 |
| C-39 | 138 | Str. Ga. | TRAY | 106 | 10.004 | | D-39 | 188 | DEFL | LM TEST STRU Z | D-/2 | 9.990 |
| C-40 | 139 | Str. Ga. | | 107 | 10.004 | | D-40 | 189 | DEFL | KM TEST STRU X | D-/3 | 9.995 |
| C-41 | 140 | στι. 68. | INAL | 108 | 10.004 | | D-41 D-42 | 101 | DEFL | NELIESI SIKU I DM TECT CTDH 7 | D-74 | 3.330 |
| C_/2 | 1/2 | | | | | | D=42 | 102 | DEFL | IF TEST CTON V | D-75 | 0 004 |
| C=43 | 142 | | | | | | D-43 | 103 | DEFL | IF TEST SIRU A | D-77 | 0 007 |
| C-45 | 144 | DEFL | 911C/DE M_V | D-31 | 10.558 | | D-45 | 194 | DEFL | LE TEST STRIL 7 | D-78 | 9,995 |
| C-46 | 145 | DEFL | 911C/DE M-7 | D-68 | 9,707 | | D-46 | 195 | DEFL | RE TEST STRU X | D-32 | 10.005 |
| C-47 | 146 | DEFL | 936BC-B1 CC | D-29 | 9,706 | | D-47 | 196 | DEFL | RE TEST STRU Y | D-69 | 10,002 |
| C-48 | 147 | DEFL | 936EC-EI BB | D-30 | 9,704 | i | D-48 | 197 | DEFL | RE TEST STRU Z | D-79 | 10.002 |
| C-49 | 148 | DEFL | 936EC-920FB D | D-07 | 9.714 | | D-49 | 198 | AOAI | RM TRUN PITCH | Q-11 | |
| C-50 | 149 | DEFL | 936EC-920FD E | D-08 | 9.705 | - 1 | D-50 | 199 | AOAI | RM TRUN ROLL | Q-12 | |
| | | | | | | . L | | | | | | |

*Combined Gages

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TABLE IV D. (CONTD.)- INSTRUMENTATION HOOK-UP, "END SUPPORT BEAM" TEST

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when have a second s

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| _ | | | _ | _ | _ | | |
|----------------|-------------|--------------|---------------------|----------------|---|------------------------|--------------------------|
| | KEE | LATERAL | I | 1 | | 23,045 | 1 |
| *(,sa)) | ESB | VERTICAL | 1 | 1 | | ł | 43,515 |
| REACTED LOAD | TRUNNION | LONGITUDINAL | 46,625 | 86. 310 | | ł | ł |
| | MAIN | VERTICAL | 145,810 | FR F/F | | 1 | 1 |
| | ÆÐ | LATERAL | 1 | 1 | | 22,050 | 1 |
| *('BS') | E 33 | VERTICAL | 1 | 1 | | I | 45,030 |
| APPLIED LOAD | TRUNNION | LONGITUDINAL | 47,230 | 5 | 22.2000 | ł | ! |
| | NIM | VERTICAL | 139,600 | (ITR / | 2 | ł | I |
| | Æ | LATERAL | 1 | 1 | | 21,460 | 1 |
| ("BS") (M | ESB | VERFICAL | ł | | | 1 | 43,350 |
| L.2 × LIMIT LO | TRUNION | LONGITUDINAL | 41,620 | 84.330 | 2222 | 1 | 1 |
| | MAIN | VERTICAL | 138,650 | 63. % E | | I | 1 |
| | | | Test I (Landing) | Test II | (LIFT-OFF) Teer 111 | Officerence - Keel) | Test IV (Landing-ESB) |

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Table V.- LDEF Verification Test Loads

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| | | | STRESS-PS | I |
|-------------------------------|----------------|--------------|-----------|------------------|
| STRUCTURAL | TYPE OF | 120% OF | MEASURED | PREDICTED STRESS |
| ELEMENT | SI'RESS | LIMIT STRESS | STRESS | FROM TEST LOADS |
| DIAGONAL (TENSILE) | AXIAL | 5,328 | 5,304 | 5,310 |
| DIAGONAL (COMPRESSIVE) | AXIAL | -3,372 | -4,111 | -4,140 |
| END SUPPORT BEAM | COMBINED | 12,090 | 10,697 | 12,136 |
| CENTER RING (BELOW TRUNNION) | COMBINED | 5,292 | 6,737 | 5,990 |
| CETTER RING (ABOVE TRUNNION) | COMBINED | -5,412 | -5,505 | -5,240 |
| LONGERON | AXIAL | -268 | -307 | -312 |
| | | | | |

TABLE VI.- LDEF STRUCTURAL ELEMENT STRESSES

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| | | S/C Eng | r. & Ops. Mgr. | | |
|-------|---|-------------------------------|--------------------------|--|--------------|
| | | | | | |
| - | | | | | |
| | L D E F Stru. Analy. Mgr. | Test M | L D E F gr./Conductor | L D E Structure | F Mgr. |
| | | | | | |
| | Systems Engineering | Instrumentarion | Fabrication | Support Contracts | |
| | • Stru/Test Data Analy. | • Instrumentation/Calib. | • Hdwr. Fab. | • Wyle Labs | |
| | • Hydraulic Design | Strain Gages | • Hydraulic Fab. | Software | |
| | • Hardware Design | Load Cells | • Inspection | Instr. Oper. | |
| | • GSE Design | Press. Gages | • NDT | • Modern Mach. | |
| 36 | Load Cyl./Maintainers | Deflectometers | Acoustics | Instr. Calib. | orig of I |
| | Load Maintainer Ops. | AOAI's | X-ray | S/G Install. | inai Poo |
| | • Test Plans/Procedures | Software | • TV Surveil. | Klate Holt | r Pr R Qi |
| | • DAS Oper. | • Electronic Equip./Ops. | | Rigging | uge Jali |
| | Report Preparation | | | Transportation | IS TY |
| | | | | • Old Dominion Elev. | |
| | | | | Load Certification Testi | ng |
| | | | | • DEI | |
| | | | | Test Stru. Des. | |
| | | | | | |
| Rel Q | Safety Faci. uality Engind iability | lities Operat eering Suppo | ions Mana ort Sup | igement Acquisition | uo |
| | • Fa | tc. Mods. • Me | ch. Set Up | Transportation Procur | ir emen t s |
| | • 2b | reader Bar Design | • | Property Mgmt. | |
| Figur | e 1 Test Organization | NAL STRUCTURE | | | |

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Figure 4.- Test Support Frame

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FIGURE 6. - LDEF TEST FACILITY TOP VIEW

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FIGURE 7.- HYDRAULIC LOAD MAINTAINERS

SIGNAL CONDITIONING CHASSIS EXCEPTER AND HP 3497A DATA ACQUISITION CONTROL UNITS MON TORS 2 HP 9845 COMPUTER

ORIGINAL PAGE BLACK AND WHITE PHOTOGRAPH





Figure 10.- Typical Installation of Hydraulic Cylinders and Load Cells





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FIGURE 13.- TYPICAL LOAD APPLICATION TRAIN



FIGURE 14 A.- DEFLECTOMETER MOUNTING



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FIGURE 15. - LDEF STANDARD LOCATION DESIGNATION (JOINT NUMBERING SYSTEM)

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FIGURE 17.- MAIN TRUNNION INSTRUMENTATION

Contract Theory of the



FIGURE 18. - MAIN TRUNNION CALIBRATION TEST



FIGURE 19 A.- STRAIN GAGE LOCATION, CENTER RING, BAY 2

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FIGURE 19 B.- STRAIN GAGE LOCATION, CENTER RING, BAY 10

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FIGURE 19 C. - STRAIN GAGE LOCATION, CENTER RING, BAY 3

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911C-DC-DB0I

B-15

41-1 (41-0 (

911C-DC-DA01

B-21

47-1 | 47-0

s o

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911CC-DAI 911DC-DAI

911CC-DBI 911DC-DBI

B-9 B-8

60

3

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| OF POOR QUALITY | | LDEF LOCATION IDENTIFIER | 911DJ-IBO 911CJ-IBO 911CJ-IBI 911DJ-IBI 911DJ-IBI |
|-----------------------------------|-------------|---------------------------------|---|
| of 911 | SECTION 'B" | SIG. CONDT. CHAN. NO. | B-27 B-28 B-30 B-29 B-29 B-31 |
| Z (INSIDE) Z (INSIDE) SECT. | | STRAIN GAGE NUMBER | 53 54 56 57-0 57-0 |
| | | 1.DEF LOCATION 1DENTIFIER | 911DJ-1A0 911CJ-1A0 911CJ-1A1 911DJ-1A1 911C-DJ-1A1 911C-DJ-1A1 911C-DJ-1A0 |
| C SI | SECTION "A" | SIG. CONDT. CHAN. NO. | B-37 B-38 B-40 B-40 B-39 B-41 B-41 B-14 |
| , ž | | STRAIN GAGE NUMBER | 63 64 66 65 67-I 0 |
| Section | | POSITION NUMBER | 0 0 4 0 9 F |
| FOR DIMENSIONS A-F | | 1.55 | 1.25 DIA. |

Figure 19 D.- Strain Gage Location, Center Ring, Bay 9

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FIGURE 19 E.- STRAIN GAGE LOCATION, LONGERON

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| OF FUCK NUCK ITY | | LDEF LOCATION IDENTIFIER | 911DF-920FFBOU 911DF-920FFBOL 911DF-920FFBIL 911DF-920FFB1U |
|-------------------------------|-------------|--------------------------------|--|
| | SECTION "B" | SIG. CONDT. CHAN. NO. | C-10 C-11 C-13 C-12 |
| 920FI | | STRAIN GAGE NUMBER | 85 86 88 7 |
| IBER 911DF TO | | LDEF LOCATION IDENTIFIER | 911DF-920FFAOU 911DF-920FFAOL 911DF-920FFAIL 911DF-920FFAIU |
| | SECTION "A" | SIG. CONDT. CHAN. NO. | C-6 C-7 C-8 C-8 |
| | | STRAIN GAGE NUMBER | 81 82 84 83 |
| | TYP.) | POSITION NUMBER | 4 0 0 H |
| 33,66 43 HBD. (oursibe) | | | Uluside) Z TYP. SECT. |

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FIGURE 19 F.- STRAIN GAGE LOCATION, LONGERON

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| | SIG. CONDT. LDEF | C-18 911DC-920FF | C-19 911CC-916AF | C-20 911DC-920FA | C-21 911CC-916AA |
|-------------------------|----------------------|------------------|------------------|------------------|------------------|
| | CHAN. NO. IDENTIFIER | (AFT) | (FWD) | (AFT) | (FWD) |
| | AIN GAGE | (63U) | (96L) | (97U) | (1001) |
| | UMBER | (94L) | (95U) | (98L) | (166) |
| | STI N | 6 | 76 | 56 | 8 |
| GAGES 90° FROM HOLES | 5.0 | | | | |

FIGURE 19 G. STRAIN GAGE LOCATION, DIAGONAL

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| POSITION NUMBER | SEC STRAIN GAGE NO. | TION "A" SIG. CONDT. CHAN. NO. TEST 4 | SEC STRAIN GAGE NO. | rion "b" Sig. condr. chan. nc. Test 4 | SEC STRAIN GAGE NO. | f fon "C" SIG. CONDT. CHAN. NO. TEST 4 | SEC STRAIN GAGE NO. | rion "d" Sig. condr. Chan. no. Test 4 |
|--------------------|------------------------------|--|------------------------------|--|------------------------------|---|------------------------------|--|
| 4004 | 103 | C-28 | 101 | C26 | 99 | с-24 | 97 | C-22 |
| | 104 | C-29 | 102 | C-27 | 100 | С-25 | 98 | C-23 |
| | 115 | C-36 | 113 | C-34 | 111 | С-33 | 109 | C-30 |
| | 116 | C-37 | 114 | C-35 | 112 | С-33 | 110 | C-31 |

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TYP. SECT.

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FIGURE 19 H.- STRAIN GAGE LOCATION, END SUPPORT BEAM

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> POSITION NUMBER

> > 65



FIGURE 20.- TYPICAL ACOUSTIC EMISSION TRANSDUCER INSTALLATION



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UATA ACQUISITION SYSTEM





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OR HILL PROLERS OF PUGA COMPLEX

FIGURE 22 C.- DEFLECTIONS OF LDEF VS LENGTH OF LONGERON ABOVE TRUNNION FOR "LIFTOFF" TEST

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