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# THE 12 MICRON BAND OF ETHANE: A SPECTRAL CATALOG FROM 765 CM<sup>-1</sup> TO 900 CM<sup>-1</sup>

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# Abstract

This document is concerned with the high resolution laboratory absorption spectrum of the  $12\mu$ m band of ethane gas. The data were obtained using the McMath Solar Telescope 1-metre Fourier Transform interferometer at Kitt Peak National Observatory and tunable diode laser spectrometers at the University of Tennessee and NASA/Goddard Space Flight Center. Over 2000 individual vibration-rotation transitions were analyzed taking into account many higher order effects including torsional splitting. Line positions were reproduced to better than 0.001 cm<sup>-1</sup>. Both ground and upper state molecular constants were determined in the analysis.

Part I of this document contains a discussion of the experimental details, the analysis procedures and the results. A list of ethane transitions occurring near  $^{14}\text{CO}_2$  laser lines needed for heterodyne searches for  $\text{C}_2\text{H}_6$  in extraterrestrial sources is also included.

Part II contains a spectral catalogue of the ethane  $v_9$  fundamental from 765 cm<sup>-1</sup> to 900 cm<sup>-1</sup>. The contents include: (a) a high dispersion (1 cm<sup>-1</sup>/12 in.) plot of both the Kitt Peak interferometric data and a simulated spectrum with Doppler-limited resolution using the model of Part I; (b) a table of over 8500 calculated transitions listing quantum number assignments, frequencies and intensities.

- 1 -

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# TABLE OF CONTENTS

<u>Part I</u>		5
	les and figures describing the analysis of the 12 micron band	7
Part II		1
Figure 1.	Plot of observed and simulated 12 micron spectra of ethane 6	5
<u>Table 1</u> .	List of quantum number assignments, calculated transition frequencies and relative intensities for the ethane vibration-rotation fundamental at 12 microns	1

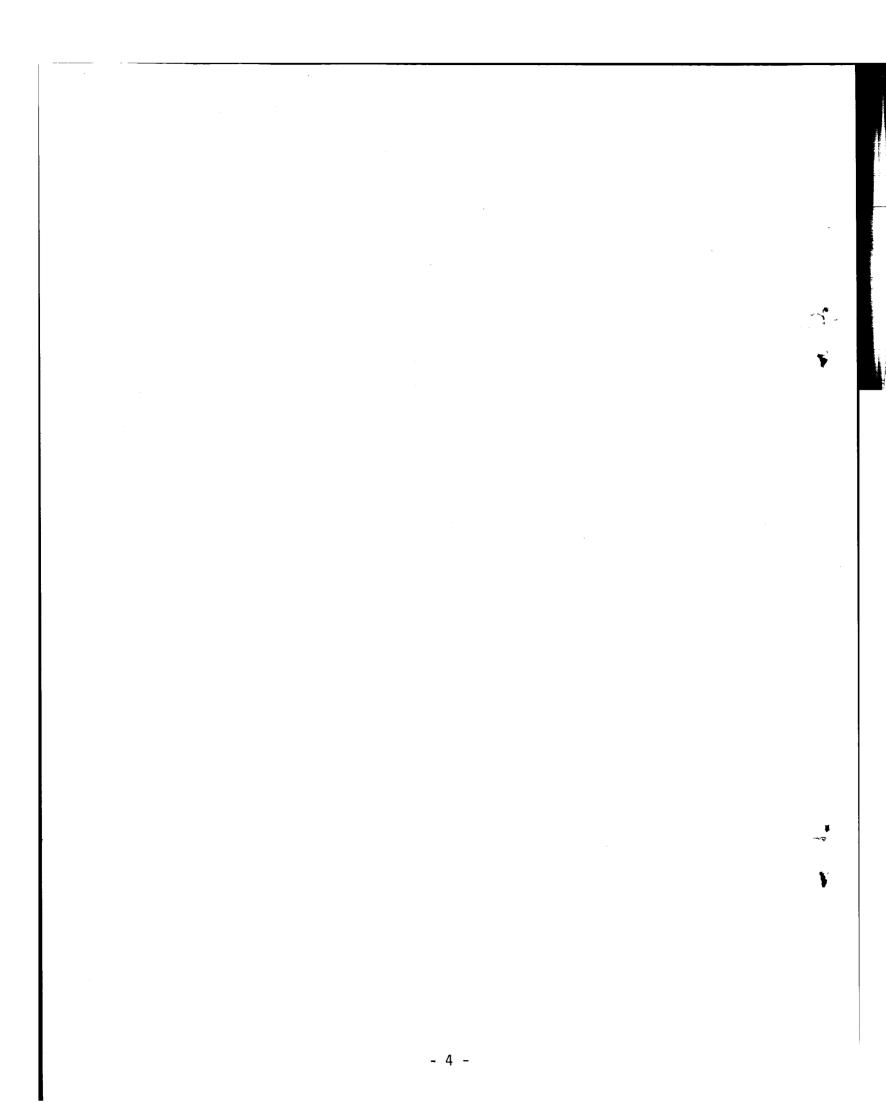
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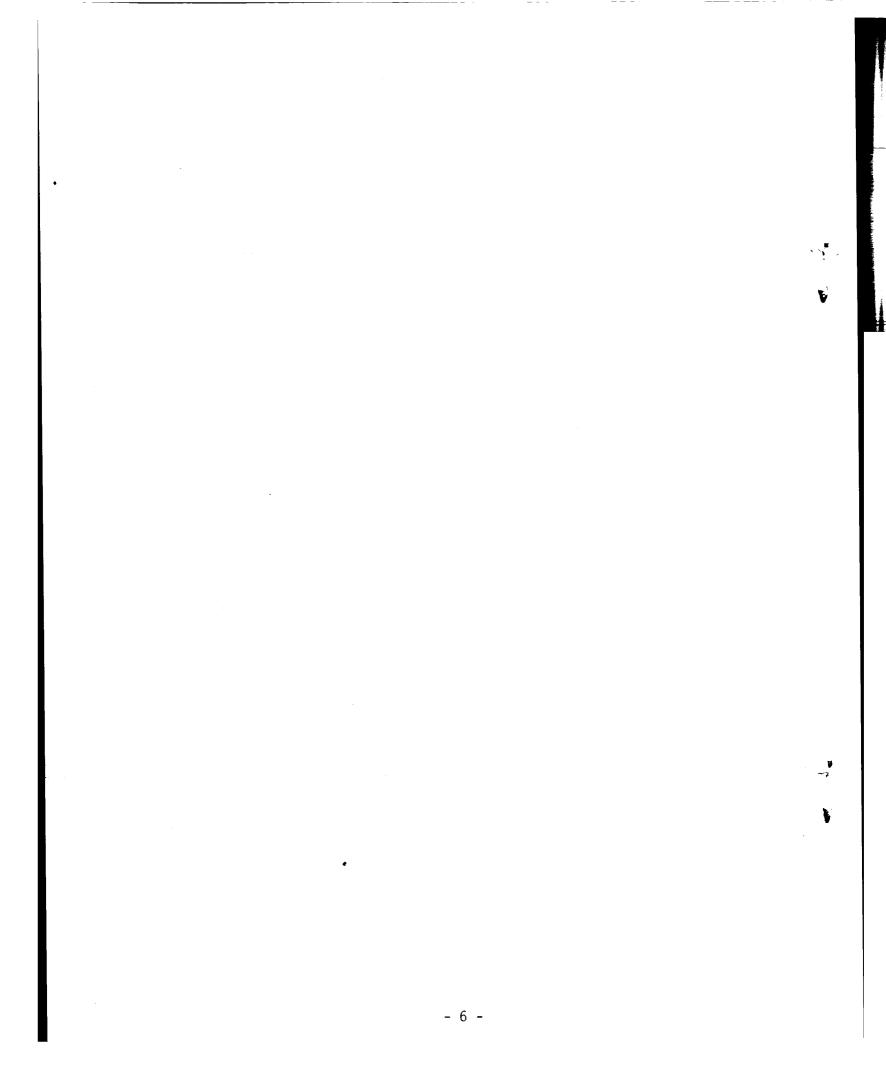
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The 12µm Band of Ethane: High Resolution Laboratory Analysis with Candidate Lines for Infrared Heterodyne Searches<sup>\*</sup>

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#### ABSTRACT

Several groups have reported emission from the  $v_9$  band of ethane at  $12\mu m$ in the spectra of Jupiter, Saturn, Neptune and Titan. This paper reports the results of a laboratory study of  $v_9$  using both high resolution Fourier Transform and diode laser absorption spectroscopy. Approximately 2000 transitions in this band have been subjected to an analysis that includes the normal rovibrational terms as well as the higher-order effects of *e*-doubling,  $\ell$ -resonance, internal rotation and a Coriolis resonance with the  $3v_{\mu}$  state. A model for this band capable of reproducing observed  $v_9$  features to better than  $0.001 \text{ cm}^{-1}$  is presented. High precision values of the primary ground state constants have also been determined:  $B_0 = 0.6630279(24) \text{ cm}^{-1}$ ,  $D_0^J =$  $1.0324(23) \times 10^{-6} \text{ cm}^{-1}$  and  $D_0^{JK} = 2.651(88) \times 10^{-6} \text{ cm}^{-1}$ . A list of v<sub>9</sub> transitions occuring near  $^{14}$ CO $_2$  laser lines that are good candidates for laser heterodyne searches has been compiled. An atlas is available from the authors that includes: (1) plots of the observed and simulated  $\nu_9$  spectra between 750 and 900  $\rm cm^{-1}$  and (2) a list of over 8500 calculated transitions and intensities.

- 9 -

# I. INTRODUCTION

The  $v_9$  fundamental band of ethane occurs in the  $12\mu m$  wavelength region and has recently received a great deal of attention in molecular astrophysics. It is the strongest band of ethane in a terrestrial window and therefore has always provided the best opportunity for identification and characterization of ethane in planetary atmospheres and molecular clouds.

Spectra recorded from the outer solar system bodies of Jupiter, Saturn, Neptune and Titan show  $12_{\mu}m$  emission from ethane (Ridgway 1974; Gillett and Forrest, 1974; Combes et al., 1974; Tokunaga, Knacke and Owen, 1976; Encrenaz, Combes and Zéau, 1978; Tokunaga et al., 1979; Tokunaga, Knacke and Orton, 1975; Gillett, 1975; Gillett and Rieke, 1977; Macy and Sinton, 1977; Gillett, Forrest and Merrill, 1973; Hanel et al., 1981). The observed  $v_9$  emission has been used to determine ethane abundances and to map planetary ethane (Gillett and Orton, 1975; Tokunaga et al., 1978; Hanel et al., 1981). All of these studies provide information needed for the construction of planetary atmospheric models (Danielseon, et al, 1973; Hunten, 1974; Strobel, 1974; Caldwell, 1977). In low resolution spectra the emission is seen as a single  $\sim$ 70 cm $^{-1}$  wide feature while its appearance in medium resolution spectra is as a series of unresolved Q-branches separated by  $^{2.7}$  cm<sup>-1</sup>. Very recently, however, high resolution laser heterodyne spectroscopy has detected individual vibration-rotation lines of  $v_{q}$  in emission from Jupiter's stratosphere (Kostiuk et al., 1981 and 1983). This laser heterodyne astronomy program was a major reason for undertaking the present laboratory study.

Although  $C_2H_6$  has not been detected in molecular sources outside the solar system, the  $12\mu m$  band is again the best candidate for a search. Ethane

- 10 -

cannot be detected in the radio region because it has no permanent dipole moment<sup>1</sup>. However, infrared laser heterodyne spectroscopy has recently provided the 10µm detection of the similarly nonpolar ethylene molecule ( $C_2H_4$ ) in the circumstellar cloud of IRC + 10216 (Betz, 1981). Two other non-polar hydrocarbons, methane and acetylene, have already been identified in the infrared spectrum of this source (Hall and Ridgway, 1978; Ridgway <u>et al</u>., 1976). The overlap of the <sup>14</sup>C<sup>16</sup>O<sub>2</sub> laser with the R-side of v<sub>9</sub> means that laser heterodyne searches can be made for ethane in IRC + 10216 and other infrared molecular sources.

The application of infrared laser heterodyne spectroscopy to observations of high-altitude ethane on Jupiter and the possibility that this technique will be used to search for ethane line emission in other planets and molecular clouds makes a new laboratory analysis of  $v_9$  important at this time. In the previous study (Daunt <u>et al.</u>, 1981) the rotational structure in the Q-branches was not resolved. In particular, line-splittings due to torsional effects and frequency shifts and intensity anomalies due to higher order Coriolis effects were not observed. Absolute line frequencies measured in that work were only accurate to about 0.01 cm<sup>-1</sup>. The narrow bandwidth, high resolution and frequency precision of laser heterodyne techniques requires individual line positions to be known to better than 0.001 cm<sup>-1</sup>.

<sup>&</sup>lt;sup>1</sup>Pure rotational transitions are made weakly allowed through interactions between the torsional mode and dipole allowed vibrations as discussed by Rosenberg and Susskind (1979). They have predicted frequencies and intensities for  $\Delta K = 0$ ,  $\Delta J = \pm 1$  transitions which would occur in the millimeter wave region. There has been no experimental detections of these lines reported to date.

A new study of the  $v_9$  band of ethane was therefore undertaken using both high resolution Fourier transform and tunable diode laser spectra. The combination of these two types of spectroscopy yielded complete coverage of the band with high absolute frequency precision and complete resolution (to the Doppler linewidth and beyond) in dense spectral regions. The results of a full vibration-rotation analysis including higher order effects is reported here. This analysis allowed accurate line frequencies and intensities to be calculated. An independent study of  $v_9$  by Henry <u>et al</u>. (1983) has yielded results similar to those reported in the present paper.

#### II. EXPERIMENTAL DETAILS

The ethane spectra were recorded with the one-meter Fourier transform spectrometer (FTS) located at the McMath solar telescope at Kitt Peak National Observatory. This instrument is a dual, moving cat's-eye interferometer capable of 0.005 cm<sup>-1</sup> unapodized resolution when operated in the asymmetric interferogram mode. The beamsplitters used for this work were made of KBr and the detector was a liquid helium cooled Arsenic-doped Silicon photoconductor. A 450 Watt glower was used as a continuum source. The reference signal for this instrument is provided by a stabilized HeNe laser. Thirty-two interferograms were averaged during a period of 103 minutes to produce a S/N ratio of approximately 400/1.

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The ethane was a research-grade sample (99.99%) obtained from Matheson Gas Products and used without purification. The gas was contained in a 30 cm straight-path cell with  $BaF_2$  windows. The sample pressure was 4.01 Torr, as measured with a capacitance manometer. The temperature of the sample cell was 22°C. Absolute frequency calibration was established by recording the  $C_2H_6$ spectrum simultaneously with a spectrum of  $CO_2$ . Carbon dioxide at a pressure of 0.5 Torr was contained in a White-type multiple traversal cell set for a path length of 193m. The source radiation beam was passed simultaneously through both cells before entering the spectrometer. The  $10\mu m {}^{12}C^{16}O_2$  laser frequencies of Petersen <u>et al</u>. (1974) were used as standards, and errors introduced by extrapolating the calibration to  $12\mu m$  are estimated to be less than 2 x  $10^{-4}$  cm<sup>-1</sup>.

The line splittings due to torsional and torsional-Coriolis effects were studied using tunable diode laser spectra. The experimental details of that

- 13 -

portion of the work have been described in a separate paper (Susskind <u>et al.</u>, 1982). The diode laser results were used in the present work to measure absolute line intensities and to model the splittings and line shifts which were not sufficiently resolved in the FTS spectra.

## III. ANALYSIS

# (a) Assignment of Spectra

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The FTS spectra were assigned by taking the molecular parameters determined for  $v_9$  from the previous study of Daunt <u>et al.</u> (1981) and generating a simulated spectrum with programs described in that work. A list of quantum number assignments, wavenumbers and relative intensities was generated along with a computer plot of the spectrum. This calculated spectrum with assignments was then used to identify the features in the observed spectrum. The earlier work had clearly resolved only the  $P_{P}$  and  $R_{R}$ lines of  $v_9$ . The new FTS data resolved the  $R_Q$  and  $P_Q$  branches as well as the  $^{R}$  P and  $^{P}$  R lines in addition to the  $^{P}$  P and  $^{R}$  R structure. Despite the limited selection of lines in the previous study the parameters determined there gave an excellent prediction of the FTS spectrum. The upper trace of Figure 1 shows the  $^{R}Q_{\Delta}$  region of  $v_{9}$  as recorded by the Kitt Peak FTS instrument. The lower trace is a simulation at  $0.005 \text{ cm}^{-1}$  resolution using the constants from Daunt et al. (1981). The structure of this Q-branch had not been resolved in the earlier work (see Fig. 2 of Daunt et al., 1981), yet the prediction was excellent, enabling assignments to be made in a straightforward manner. Any questionable assignments were checked by the traditional method of combination differences.

# (b) Theoretical Model

The vibration-rotation Hamiltonian for the ethane molecule can be written to first order as

- 15 -

$$H = H_{VIB} + H_{ROT} + H_{VR}$$
(1)

where  $H_{VIB}$  and  $H_{ROT}$  are the vibration and rotation Hamiltonians for a symmetric rotor (Herzberg, 1945; Allen and Cross, 1963). The term  $H_{VR}$  represents vibration-rotation coupling contributions including the usual Coriolis interactions described by Mills (1972). The rovibrational Hamiltonian, Eq. (1), used in this work contained all terms through  $h_3^{\dagger}$  plus the  $\beta$  terms of  $h_4^{\dagger}$  as described by Blass and Nielsen (1974) and Daunt <u>et al</u>. (1981):

$$\langle J, K, \ell_{9} | H | J, K, \ell_{9} \rangle = v_{0} + (A_{0}^{-}B_{0}^{-})K^{2} - 2A_{e}\varsigma_{9}^{Z}K\ell_{9}$$

$$+ B_{0}^{-}J(J+1) - (\alpha_{9}^{A} - \alpha_{9}^{B})K^{2} - \alpha_{9}^{B}^{-}J(J+1) - D_{0}^{J}^{-}J^{2}(J+1)^{2}$$

$$- D_{0}^{JK}K^{2} J(J+1) - D_{0}^{K}K^{4} + n_{9}^{J}^{-}J(J+1)K\ell_{9}$$

$$+ n_{9}^{K}K^{3}\ell_{9} + \beta^{J}J^{2}(J+1)^{2} + \beta^{JK}K^{2}^{-}J(J+1) + \beta^{K}K^{4}$$

$$(2)$$

The previous study of Daunt <u>et al</u>. (1981) showed that  $\ell$ -doubling and  $\ell$ -resonance interactions were necessary for understanding the observed features of  $v_9$ . The necessary matrix elements have been given by Amat, Nielsen and Tarrago (1971) as:

$$\langle J, K+1, \ell_{9} = +1 | H| J, K-1, \ell_{9} = -1 \rangle = -\frac{1}{2} \left[ q_{9}^{(+)} + \delta q_{9}^{J} J(J+1) + \delta q_{9}^{K} (2K)^{2} \right]$$

$$\left[ \{ J(J+1) - K(K+1) \} \{ J(J+1) - K(K-1) \} \right]^{\frac{1}{2}}$$

$$(3)$$

where the following definitions relative to Amat, Nielsen and Tarrago (1971, Table XXXVI) have been used in the present work:

$$q_{t}^{(+)} = -4F_{t}^{t}$$

$$\delta q_{t}^{J} = -4F_{22+}^{t,J+} \qquad (4)$$

$$\delta q_{t}^{K} = -8F_{22+}^{t,K+} \qquad (4)$$

The sign convention used for the  $\ell$ -doubling constant  $q_t^{(+)}$  is the generally accepted one of Cartwright and Mills (1970).

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The earlier lower resolution study (Daunt <u>et al.</u>, 1981) required only those terms described by Eqs. (2)-(4). Torsional splittings and higher order effects were not needed to account for the observed data and were therefore not included in the model.

The characteristics of torsional spectral features in ethane were first referred to by Wilson (1938) and later were discussed in more detail by Susskind (1974) and Hougen (1980). Observed ethane torsional splittings were first reported by Flicker <u>et al</u>. (1977) in the  $v_9$  band but went unanalyzed at that time. Pine and Lafferty (1982) observed torsional splittings in the  $3\mu$ m bands but the strong interactions among the many vibration-rotation states prevented a quantitative upper state analysis. Patterson <u>et al</u>. (1981) correctly interpreted the observed intensity anomalies in the diode laser spectrum of the  ${}^{R}Q_{0}$  branch of  $v_9$  as due to the effects of torsional splittings. Diode laser spectra recorded by the present authors across a wide range of the  $v_9$  band and described in more detail elsewhere (Susskind <u>et al</u>., 1982) clearly showed torsional splittings plus the effects of a Coriolis interaction with the  $3v_4$  torsional state.

These newest observations indicated that the high resolution FTS data needed to be analyzed with a model that included torsional effects. This changed the Hamiltonian of Eq. (1) to

- 17 -

$$H = H_{VIB} + H_{ROT} + H_{VR} + H_{TOR} + H_{TV}$$
(5)

where the details of the new terms  $H_{TOR}$  and  $H_{TV}$  are described elsewhere (Susskind <u>et al.</u>, 1982; Susskind, 1974; Hougen, 1980). Only the most important effects of these terms on the appearance of the spectra will be discussed here.

The torsional term  $H_{TOR}$  causes each  $|J,K,\ell\rangle$  vibration-rotation state to be split into four torsional substates denoted by the torsional symmetry number  $\sigma = 0$ , 1, 2 or 3. As shown in Fig. 2 the allowed levels in the ground vibrational state have the following value relationship: even  $\sigma$  for K even and odd  $\sigma$  for K odd. In the  $v_9 = 1$  state the reverse is true. The overall selection rules for  $v_9$  transitions are  $\Delta K = \pm 1$ ,  $\Delta \ell = \pm 1$ ,  $\Delta J = 0$ ,  $\pm 1$  and  $\Delta \sigma =$ 0. The  $H_{TV}$  term allows each vibrational state to have a different value for the barrier to internal rotation. To the extent that this barrier changes, the spacings of the  $\sigma$  torsional levels will differ for each vibrational state.

Fig. 2 also shows the splitting  $(\Delta_9)$  between the allowed torsional levels in  $v_9$  to be less than that in the ground state  $(\Delta_G)$ . If such a difference between the torsional level splittings in lower and upper states exists, then each normally allowed transition, denoted by the spectroscopic symbol  $\Delta K[\Delta J]_K(J)$ , will be split into a torsional doublet. The first order torsional model given by Susskind (1974) predicts that <u>all</u>  $v_9$  doublets should have essentially the same splitting of  $S_{0,9} \equiv |\Delta_9 - \Delta_G|$ . One torsional component is shifted  $\Delta S (=S_{0,9})$  from the unsplit position while the other component is shifted 2 $\Delta S$  in the opposite direction. The sense of the shifts depend on the appropria<sup>+</sup> round state K values as given in Table I. The

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diode laser spectra (Susskind <u>et al</u>. 1982) showed that the torsional doublets at low J and K values were indeed split by a constant value of  $-2.2 \times 10^{-3}$  cm<sup>-1</sup> but that lines with higher J and K values sometimes had splittings of more than 0.05 cm<sup>-1</sup>. This observation could not be accounted for using only the terms H<sub>TOR</sub> and H<sub>TV</sub>. An accidental Coriolis resonance with the nearby torsionally excited state  $3v_4$  was shown to account for the observed J,K-dependent splitting in excess of the intrinsic torsional splitting, S<sub>0,9</sub>. This had the effect of perturbing each component of a doublet by a different amount, thereby altering the apparent splitting. A final model Hamiltonian including all the important effects is then given by

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$$H = H_{VIB} + H_{ROT} + H_{VR} + H_{TOR} + H_{TV} + H_{COR}$$
(6)

where  $H_{COR}$  is described in detail in Susskind <u>et al.</u> (1982). The energy levels involved in this resonance are schematically shown in Fig. 3. The  $3v_4$ state has four torsional  $\sigma$  substates with the vibrational origin energies shown in the figure. The energy separations from the origin of the  $v_9$  state are given by  $\Delta_{\sigma} = v_9 - (3v_4)_{\sigma} = \Delta_0$ ,  $\Delta_1$ ,  $\Delta_2$  and  $\Delta_3$ . It should be noted from this figure that the  $|v_9, J, K-1, -1\rangle$  levels (- $\ell$  states, see Herzberg, 1945) are closer to the  $3v_4$  levels than the  $|v_9, J, K+1, +1\rangle$  levels (+ $\ell$  states). Since the selection rule for the Coriolis interaction is  $K_{v_9} - K_3 v_4 = \ell_{v_9}$  the perturbations are expected to be greater for the - $\ell$  levels than for the + $\ell$ levels. The observed diode laser spectra of the  ${}^PQ_K(J)$  branch ( $\Delta K=\Delta \ell=-1, \Delta J=0$ ) lines showed splittings that were much more perturbed than those for the  ${}^Rq_K(J)$  branches ( $\Delta K=\Delta \ell=+1, \Delta J=0$ ) in agreement with this model. A diagram of how the individual vibration-rotation-torsion states are coupled through the Coriolis resonance is given in Fig. 4 for the case of K"=6. The magnitude of the perturbation to any  $|v_9, J, K+\ell, \ell, \sigma >$  level through  $H_{COR}$  is given by second-order perturbation theory as

$$\Delta E = \frac{C^{2}[J(J+1)-K(K+\ell)]}{\Delta_{\sigma} + E_{J,K}^{\vee 9} - E_{J,K}^{3\nu_{4}}}$$
(7)

where C is a coupling constant described in Susskind <u>et al</u>. (1982) and found to have the value 0.032 cm<sup>-1</sup>. The perturbation is different for each  $\sigma$ torsional state. Therefore the total splitting for a transition to an upper state |J,K+ℓ,ℓ> is given by

$$S_{J,K+\ell,\ell} = S_{0,9} + C^2 [J(J+1) - K(K+\ell)]F(J,K,\ell)$$
 (8)

where

$$F(J,K,\ell) = \frac{1}{\Delta_{\sigma} + E_{J,K}^{\vee 9} - E_{J,K}^{3\nu_{4}}} - \frac{1}{\Delta_{\sigma+2} + E_{J,K}^{\vee 9} - E_{J,K}^{3\nu_{4}}} . (9)$$

The rotational contribution to each denominator in Eq. (9) is given to first order by

$$E_{J,K+\ell,\ell}^{\vee 9} - E_{J,K}^{3\nu_{\mu}} = 2[A(1-\zeta_{9}^{Z})-B]K\ell + [A(1-2\zeta_{9}^{Z})-B]$$
  
= 2.617KAK + 0.619 cm<sup>-1</sup> (10)

The primary source of any observed splitting is given by the first term on the r.h.s. of Eq. (8) i.e., the intrinsic splitting:  $S_{0,9}$ . The second factor affecting the observed splittings comes from the difference in the Coriolis perturbations to each component as given by the second term on the r.h.s. of Eq. (8). The intrinsic splitting  $S_{0,9}$  ( $\approx 2.2 \times 10^{-3} \text{ cm}^{-1}$ ) dominates far from

resonance, i.e., for lines having large K" $\Delta$ K values or those near the subband origins (J=K). For lines with either larger (J-K) or more negative K" $\Delta$ K values the Coriolis effects become progressively greater. This results in frequency shifts which <u>enlarge</u> the torsional component splittings to values sometimes exceeding 0.050 cm<sup>-1</sup>. The Coriolis perturbation is positive and always greater for the  $\sigma$  (=0 for K even and =1 for K odd) levels than for the  $\sigma$  + 2 levels provided the interacting v<sub>9</sub> and 3v<sub>4</sub> states do not cross. This is in the same sense as the first order torsional splitting, S<sub>0,9</sub>, assuming a barrier in v<sub>9</sub> greater than that in the ground state. Since all the lines treated in this paper were not near the level crossing (K" $\Delta$ K=-17) the Coriolis perturbation <u>always increased</u> the splittings.

# (c) <u>Correction of the Data Set</u>

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The original FTS data set consisted of over 2000 assigned lines having quantum number values of  $-13 \le K^* \Delta K \le +18$  and  $J^* \le 40$ . These lines covered the spectral region between 765 cm<sup>-1</sup> and 900 cm<sup>-1</sup> and at first inspection did not show torsional splittings. This is understandable since in the previous section it was seen that the first order splitting,  $S_{0,9}$ , was 0.0022 cm<sup>-1</sup> and the unapodized resolution of the FTS data was 0.005 cm<sup>-1</sup>. Lines with high J and K quantum numbers have observable splittings greater than the resolution only when the Coriolis contribution of Eq. (8) is sufficiently large. These enhanced splittings are visible on careful inspection of the data. However, the resolution and S/N ratio of the data set used for the present study was such that most of the torsional doublets were either unresolved or the weaker component was not reliably measured.

- 21 -

The very high frequency precision of the FTS data meant that some correction for the combined instrumental and torsional effects (splittings and shifts) had to be carried out before a complete analysis would yield reliable molecular constants free of systematic model errors. All the terms of Eq. (6) can be treated simultaneously using a global model Hamiltonian but this was deemed unnecessary since the torisonal terms are essentially independent of the rest of the terms in Eq. (6). Therefore an alternative method to full diagonalization was used. The effects of torsional splitting and the Coriolis resonance with  $3v_4$  were calculated using Table I and Eq. (7), respectively. These calculations were then used, together with the instrumental response, to deperturb the observed data yielding "corrected" frequencies which could be fitted with Eqs. (2) and (3). The clearest way to describe this procedure is to refer the reader to Fig. 5. The torsional splitting from the unperturbed and unsplit position ( $v_0$ ) was calculated according to Table I using the results from Susskind <u>et al</u>. (1982) (Fig. 5a). The effects of the Coriolis resonance with  $3v_4$  on each torsional component was then calculated using Eq. (7) and added to the first order torsional result (Fig. 5b). This was followed by giving each component transition a Doppler width profile ( $\Delta v_D$  =  $1.8 \times 10^{-3} \text{ cm}^{-1}$  FWHM) in the proper intensity ratio (Table I) and adding the result in the case of overlap (Fig. 5c). The next step was a convolution with the appropriate instrument profile. This was followed by a peak finding routine that located maxima in the final profile and calculated the shift(s) from the origin  $\boldsymbol{\nu}_0$  (Fig. 5d). These shifts were then subtracted from the observed transition frequencies to yield a corrected data set. The modified data set then corresponds to the spectrum of  $v_9$  which would be observed if torsion and the  $3v_4$  resonance did not exist. This corrected data set does not represent any physically observable spectrum but it allows the fitting of the band to a standard model that simplifies both the analysis and subsequent

- 22 -

simulation of the spectrum for astrophysical modeling. Simulated spectra for comparison with observed data are easily obtained by adding the calculated torsional and Coriolis effects to the unsplit line positions to predict the final spectrum.

# (d) Fitting Procedure

The data analysis procedure followed the iterative scheme listed below:

- (1) each 2x2 Hamiltonian (Cartwright and Mills, 1970) was evaluated for a molecular parameter set of 1 parameters  $[\gamma_1, \gamma_2, \ldots, \gamma_1]_n = \tilde{\gamma}_n$  (n = 0 for the initial set) to obtain the upper state energies;
- (2) the residuals (obs.-calc.) were computed as

and Wilson, 1975);

$$\Delta_{o-c} (J+\Delta J, K+\Delta K, \ell+\Delta \ell) = [\nu_{OBS}(J+\Delta J, K+\Delta K, \ell+\Delta \ell) + E_{gs}(J, K, \ell=0)] - E_{calc}^{n}(J+\Delta J, K+\Delta K, \ell+\Delta \ell)$$
(11)

where  $E_{gs}$  is the ground state energy and  $E_{calc}^{n}$  came from step (1); (3) the derivatives  $\delta E/\delta \gamma_{m}$ , where  $\gamma_{m}$  is a particular molecular parameter such as  $\alpha_{9}^{B}$ , were calculated using the Hellman-Feynman theorem (Rowe

(4) the residuals,  $\Delta_{o-c}$ , were fitted to a Taylor series expansion of the energy retaining only the terms linear in  $\delta\gamma$ , i.e.

$$\Delta_{o-c} = \sum_{m} \frac{\delta E}{\delta \gamma_{m}} \Big|_{\gamma_{n}} \delta \gamma_{m} ; \qquad (12)$$

(5) the molecular parameter set  $\widehat{\boldsymbol{\gamma}}_n$  was corrected according to

$$\left(\gamma_{m}\right)_{n+1} = \left(\gamma_{m}\right)_{n} + \delta\gamma_{m}$$
(13)

- 23 -

The series of steps from 1 through 5 continued until the stepwise regression (Efrymonson, 1960) produced no significant reduction in the sum square error of the remaining  $\Delta_{0-C}$  of step 2. At that point, the data, which had been originally weighted uniformly (wt.=1), was reweighted according to the method of bi-weights (Beaton and Tukey, 1974) as in the previous  $v_9$  study (Daunt <u>et al.</u>, 1981). The procedure was terminated using a modified  $\chi^2$  test (Lin <u>et al.</u>, 1980).

# (e) <u>Results</u>

Several parameter sets, corresponding to model Hamiltonians limited to lower order terms than those presented in Eqs. (2) and (3), were also tried in the analysis procedure described above. In all, four parameter sets were determined involving inclusion and exclusion of  $\{\beta^J, \beta^{JK}, \beta^K\}$  and  $\{\delta q_{q}^J, \delta q_{q}^K\}$  in various combinations. Each parameter set was used to synthesize plots of selected 2 cm<sup>-1</sup> segments of the spectrum on a 1 cm<sup>-1</sup>/meter scale. These were then compared with the observed spectrum plotted on the same scale. Based on these visual comparisons, the best parameter set was judged to be the full set described by Eqs. (2) and (3) and listed in Table II. The analysis of 1609 corrected transitions yielded a standard deviation of 0.7 x  $10^{-3}$  cm<sup>-1</sup>. The overall agreement between the  $v_9$  molecular constants of the present study and those reported by Daunt et al. (1981) and Henry et al. (1983) is very good. The only notable discrepancy occurs in the band origin  $\boldsymbol{\nu}_0$  which appears to be ~0.001  $\text{cm}^{-1}$  too low in Henry et al. (1983). The fact that their interferometer has to be operated in air at present is probably responsible for this small but significant wavelength offset.

- 24 -

A ground state constant determination was also carried out as in Lin <u>et</u> <u>al</u>. (1980) using 893 ground state combination differences. Results of this analysis and comparison with previous work are shown in Table III. The excellent agreement with the analyses of laser difference frequency data by Pine and Lafferty (1982) and recent FTS data by Henry <u>et al</u>. (1983) indicates that the ground state constants for ethane are now very precisely determined.

The quality of the analysis is best demonstrated by examination of Figures 6-9 which show the  ${}^{R}Q_{K}(J)$ , K = 1, 2, 3 and 4 branch regions of  $v_{9}$ . Panel A of each figure shows the FTS data and panel B a corresponding diode laser scan of the same region.

3

The Doppler limited diode laser data was computer deconvoluted using the techniques described by Blass and Halsey (1981) in order to clearly resolve the torsional splittings at low J and K values. These results are shown in panel C of each figure. The intrinsic torsional splitting of  $S_{0,9} = 2.2 \text{ x}$  $10^{-3}$  cm<sup>-1</sup> is now readily visible. The parameters of Tables II and III for the deperturbed  $v_9$  plus the torsional/Coriolis parameters of Susskind <u>et al</u>. (1982) were then used to simulate the deconvoluted spectra. The results for a calculated line width of 0.001  $\rm cm^{-1}$  are shown in panel D of each figure. The agreement is most pleasing in each case. Features not reproduced are attributed to the hot band  $v_9 + v_4 - v_4$  which has not been included in the simulation. It is evident from Figs. 6-9 that the present model can reproduce essentially all the observed vo features in the present data with good frequency accuracy (better than 0.001  $\text{cm}^{-1}$ ). The relative intensities of the torsional doublets in Figs. 6-9 appear to deviate from the calculated because the scans available for deconvolution were not recorded under conditions necessary for accurate absolute intensity measurements. Additional diode

- 25 -

laser spectra recorded for the purpose of intensity measurements gave excellent agreement with the theoretical predictions of Table I.

## **IV. DISCUSSION**

One of the most important features of the  $v_9$  band is the  ${}^{R}Q_0(J)$  branch. This band head has been used to evaluate the ethane abundance in the Jovian atmosphere (Tokunaga, Knacke and Owen, 1976; Tokunaga <u>et al.</u>, 1979) because it stood out clearly from the remainder of the band. It was noted, however, by Tokunaga and Varanasi (1976) that it was impossible to simultaneously fit  ${}^{R}Q_0$ and the rest of the  $v_9$  band to a standard model. These workers obtained effective molecular parameters for  ${}^{R}Q_0$  and made laboratory intensity measurements which were then used to extract mixing ratios and abundances from the astrophysical spectra.

The anomalous behavior of  ${}^{R}Q_{0}$  is due to i-doubling effects (Daunt <u>et al.</u>, 1981) induced by the Coriolis interaction of  $v_{9}$  with  $v_{4}$ ,  $v_{5}$  and  $v_{6}$  (Susskind <u>et al.</u>, 1982). This explains the difference between  ${}^{R}Q_{0}$  and the other  ${}^{P,R}Q_{K}$ branches reported by Tokunaga and co-workers (1976, 1979). The detailed line pattern of  ${}^{R}Q_{0}$  was partially resolved in the diode laser spectra of Flicker <u>et</u> <u>al</u>. (1977) and interpreted correctly later by Patterson <u>et al</u>. (1981). Only when taking the torsional effects into account could the unexpected intensity pattern of the lines be understood. The effect of the Coriolis interaction on the component splitting is a factor of two larger for  ${}^{R}Q_{0}$  than for most other branches (the exceptions being  ${}^{R}R_{0}$  and  ${}^{R}P_{0}$  where there is no torsional-Coriolis interaction). The combination of this enlarged torsional splitting and the narrowing of J-line spacings caused by the *i*-doubling are responsible for the anomalous appearance of  ${}^{R}Q_{0}$ . This feature is the final test for the present model. Figure 10A shows the FTS spectrum where the line spacings are so close that very little is resolved. A Doppler limited diode laser scan of <sup>R</sup>Q<sub>0</sub> is shown in Fig. 10B where more structure is visible but still not enough for a detailed line-by-line analysis. If the spectrum in Fig. 10B is deconvoluted, then complete resolution of all the torsional features is obtained as seen in Fig. 10C. The peculiar pattern is due to the lower frequency torsional component of each J falling into close coincidence with the high frequency component of the next higher J. The complete model for  $v_9$ predicts the pattern plotted in Fig. 10D and is in good agreement with the deconvoluted laser data. The extra lines appearing in Fig. 10C are assumed to be transitions of the hot band  $v_9 + v_4 - v_4$ .

An accurate model of the line positions and relative intensities of  ${}^{R}Q_{0}$  is now available. The uncertainty of earlier astrophysical studies caused by a lack of understanding of the structure of this feature has been removed.

There have been several attempts to obtain absolute intensity values for the entire v<sub>9</sub> band (Varanasi, Cess and Bangaru, 1974) and for the  ${}^{R}Q_{0}$  branch alone (Tokunaga and co-workers, 1976; 1979). A combination of our calculated relative line strengths and diode laser absolute line strength determinations has allowed us to derive a value of 0.53 (±0.05) cm<sup>-2</sup> atm<sup>-1</sup> at 296°K for the  ${}^{R}Q_{0}$ branch. The integrated strength from the FTS data for the  ${}^{R}Q_{0}$  region gave S = 0.56 (±0.03) cm<sup>-2</sup> atm<sup>-1</sup>. These values are much lower than the S = 0.74 (±0.09) cm<sup>-2</sup> atm<sup>-1</sup> obtained by Tokunaga and Varanasi (1976) from unresolved medium resolution data. The value of 0.70 cm<sup>-2</sup> atm<sup>-1</sup> derived from diode laser data reported in Henry <u>et al</u>. (1983) is more problematic. They used a rigid rotor model and measured only  ${}^{R}Q$  type transitions with low K and high J quantum numbers. These are the lines, however, whose intensities are the most perturbed by the  $\mathfrak{L}(2,2)$  resonance. The extent of this perturbation is quite pronounced as shown in Table IV and Figure 11. The  ${}^{R}Q_{1}(25)$  and  ${}^{R}Q_{1}(30)$  lines are 22% and 31% stronger than normal (rigid rotor model) and will appear to be 44% and 62% stronger than the respective  ${}^{P}Q_{1}(25)$  and  ${}^{P}Q_{1}(30)$  lines (see Fig. 11).

The K and J dependence of this effect accounts for the problems reported in Henry <u>et al</u>. (1983) in trying to derive a consistent transition dipole moment as K and J changed. These types of intensity effects have been described in more detail in Mills (1969), Cartwright and Mills (1970) and Masri and Blass (1971). In short, the overall intensity effect of the resonance (for the case of  $v_9$  of  $C_2H_6$ ) is to enhance  ${}^RQ$ ,  ${}^PP$  and  ${}^PR$  type transitions while depleting the  ${}^PQ$ ,  ${}^RR$  and  ${}^RP$  type transitions. Unless one samples all sets of transitions for wide values of K and J the derivation of a band strength will be in error. It would be possible to derive strengths from a few selected lines but only if the resonances have been rigorously taken into account. The particular case of  $v_9$  of  $C_2H_6$  strongly illustrates the inadequacy of using rigid rotor models for the study of perturbed bands.

In comparing the two diode laser line intensities studies where measurements overlap the present study obtained experimental strength values about 40% lower than those reported in Henry <u>et al</u>. (1983). This disagreement is independent of the model problem discussed above. Since large discrepancies still exist, further work on the absolute intensity problem is required before  ${}^{R}Q_{0}$  or any other features of  $v_{9}$  can be used as precise probes for ethane abundances. It should also be remembered that a large proportion of the observed intensity in the 12µm region is attributable to the as yet unanalyzed hot bands ( $v_{9} + nv_{4} - nv_{4}$ ), the  $3v_{4}$  band, and isotopic bands. Work on these problems is presently underway.

Recently Bjoraker <u>et al</u>. reported a detection of ethane on Saturn in the  $3\mu$ m region through a band strikingly similar in appearance to  $v_9$  (Q-branch

-29 -

spacings ~2.7 cm<sup>-1</sup> apart). There is also the possibility of using the  $v_9$  +  $v_{12}$  band (Lin, Blass and Gailar, 1980) as a probe for ethane as suggested by Treffers <u>et al</u>. (1978). However,  $v_9$  would still appear to be the strongest feature of  $C_2H_6$  in the usual atmospheric windows and therefore the best candidate for extraterrestrial searches.

The suitability of the  $v_9$  band for laser heterodyne searches in molecular sources was a primary motivation of the present study. The R side of the  $v_{q}$ band overlaps the I-band P-branch of the  $^{14}$ CO<sub>2</sub> laser lines and provides the best opportunities for heterodyne studies. Assuming a Doppler shift for a source of  $\pm 3$ GHz (as for Jupiter) and a filter bank width of  $\pm 3$ GHz, candidate coincidences within  $\pm 6$ GHz ( $\pm .2$  cm<sup>-1</sup>) between the stronger transitions of  $v_9$ and the  $^{14}CO_2$  laser lines are listed in Table V. The quality of the reported offsets have been checked recently by laboratory heterodyne measurements by Weaver et al. (1983). Comparisons with the predictions in Table V for the eight lines studied show an average difference of only 6MHz. Several of these predicted coincident ethane transitions have recently been observed in the Jovian stratosphere by Kostiuk et al. (1983). The relative intensities listed in Table IV can be converted to absolute intensities by applying the multiplicative conversion factor 7.1(0.7) x  $10^{-3}$  cm<sup>-2</sup> atm<sup>-1</sup> This factor was derived from diode laser intensity measurements of  $v_9$  transitions and corresponds to a sample temperature of 296°K.

The lines listed in Table V have been taken from an atlas of calculated  $v_9$  transitions compiled from the present study and covering the region from 750 to 900 cm<sup>-1</sup>. This atlas consists of two sections: Part I - plots of the observed FTS spectrum and a simulated spectrum calculated at Doppler width for 300°K (1.8 x 10<sup>-4</sup> cm<sup>-1</sup>); and Part II - a list of over 8500 calculated

- 30 -

transition frequencies, quantum number assignments and relative intensities. A page from Part I of this atlas for the 837.5 to 840.0 cm<sup>-1</sup> region is shown in Fig. 12. The corresponding page list of Part II for the plots in Fig. 12 is given in Table VI. The intensity conversion factor discussed above applies to the entire  $v_9$  atlas. Copies of this atlas may be obtained by writing to the authors (S.J.D., D.E.J. or W.E.B.).

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#### FIGURE CAPTIONS

- Figure 1. Upper panel: part of the FTS spectrum of the  $v_9$  band of  $C_2H_6$  near  $^{R}Q_4$  recorded with  $\Delta v = 0.005 \text{ cm}^{-1}$ . Lower panel: simulated spectrum of the same region using the parameters from Daunt <u>et al.</u> (1981). No torsional effects were included in this calculation.
- Figure 2. Selection rules, first order torsional splittings, predicted splitting patterns and intensities for an internal rotation barrier in  $v_9$  greater than that in the ground vibrational state. The allowed and forbidden levels are shown by horizontal solid and dashed lines, respectively.
- Figure 3. Energy origins of the  $3v_4$  state (including torsional effects) relative to  $v_9$ . Note that the (- $\ell$ ) states of  $v_9$  are closer to the  $3v_4$  levels than the (+ $\ell$ ) states. Since transitions with  $\Delta K = -1$ ( $^{P}P$ ,  $^{P}Q$ ,  $^{P}R$ ) terminate in the (- $\ell$ ) levels, they will be the most perturbed by  $3v_4$ .
- Figure 4. Energy levels involved in transitions from the ground state (K" = 6, J") to  $v_9$ . Torsional level splittings are shown for the lower  $(+2S_0, +S_0, -S_0, -2S_0$  where  $S_0 = \Delta_G/3$  and upper states  $(+2S_1, +S_1, -S_1, -2S_1$  where  $S_1 = \Delta_g/3$ . The allowed torsional levels are shown by solid lines and the forbidden levels by dashed lines. The  $3v_4$ levels perturb the  $v_9$  levels through the Coriolis interaction matrix shown in the upper left corner (the interacting levels are connected by the lines  $\bullet - \bullet \bullet$ ). Allowed  $v_9$  transitions are shown by the slanting vertical arrows.
- Figure 5. Method used for obtaining corrective shifts for the FTS data.

(a) Calculate the first order torsional splittings for each  $v_9$  transition (unperturbed frequency =  $v_0$ ). The pattern is given by Table I where  $S_{0,9} = |3\Delta S| = |3(S_1 - S_0)| = |\Delta_9 - \Delta_G| = 2.282 \times 10^{-3} \text{ cm}^{-1}$ . (b) The  $3v_4$  Coriolis resonance contributions are calculated with Eq. (7) and these additional shifts are added to each torsional component.

(c) Each line is given a Doppler line shape  $(\Delta v_D = 1.8 \times 10^{-3} \text{ cm}^{-1} \text{ FWHM})$  and intensities are summed. (d) The results from part (c) are convoluted with an instrument function to yield a final contour. This profile is then searched for maxima and shifts relative to  $v_0$  are calculated. These shift values are then merged with the observed measurements to create an "unsplit and unshifted" set of frequencies that can be fitted with the standard model of Eqs. (2)-(3).

- Figure 6. The <sup>R</sup>Q<sub>1</sub> region of v<sub>9</sub>. (A) FTS spectrum; (B) diode laser scan;
  (C) deconvoluted diode laser data; (D) simulated spectra including torsion and Coriolis effects (full model).
- Figure 7. The  $^{R}Q_{2}$  region of  $v_{9}$ . (A) FTS spectrum; (B) diode laser scan; (C) deconvoluted diode data showing full resolution of the complex feature near 827.610 cm<sup>-1</sup>; (D) simulated spectrum using full model.
- Figure 8. The  ${}^{R}Q_{3}$  region of  $v_{9}$ . (A) FTS spectrum; (B) diode laser scan where the torsional splitting is only evident as shoulders; (C) deconvoluted diode laser data with torsional splitting now completely resolved even at J = 4; (D) simulated spectrum using full model.
- Figure 9. The  $R_{Q_4}$  region of  $v_9$ . (A) FTS spectrum; (B) diode laser spectrum;

- 38 -

(C) deconvoluted diode data showing complete resolution of the torsional splittings even at J = 6; (D) simulated spectra using full model.

- Figure 10. The  ${}^{R}Q_{0}$  branch of  $v_{9}$ . (A) FTS spectrum; (B) diode laser scan showing that even at Doppler limited resolution the fine structure is still unresolved; (C) deconvoluted diode data illustrating complete resolution of the unusual structure of  ${}^{R}Q_{0}$ . This is a result of a two-fold torsional effect for  ${}^{R}Q_{0}$  caused by the  $3v_{4}$  resonance and the strong  $\ell$ -doubling that is quite common in the  ${}^{R}Q_{0}$  branch of perpendicular bands of symmetric top molecules; (D) simulated spectra using the full model. Unassigned peaks are assumed to belong to the hot band  $v_{9} + v_{4} - v_{4}$ .
  - Figure 11.Effects of  $\ell$ -resonance on the (A)  ${}^{R}Q_{1}(J)$  branch and (B)  ${}^{P}Q_{1}(J)$ branch of  $v_{9}$ . The J values are numbered and both plots are on the same frequency and absolute intensity scales. Note the enhanced intensity of the  ${}^{R}Q_{1}(J)$  lines relative to the  ${}^{P}Q_{1}(J)$  with the same J value. The effect increases with J. A rigid rotor model would have the intensities approximately equal.
- Figure 12.A page from Part I of the  $v_9$  Band Atlas that covers 837.5 to 840.0 cm<sup>-1</sup>. The upper trace in each row is the FTS data (the  $^{R}Q_6$  region in this case). The lower trace is the simulated spectrum using the full model. The torsional splittings are clearly seen for all transitions. The calculated resolution is  $1.8 \times 10^{-1}$  cm<sup>-1</sup> at T =  $300^{\circ}$ K (i.e., Doppler limited).

K"	Int. <sup>(a)</sup>	Int.RATIO	σ	Tor. Shift <sup>(b)</sup>
<u> </u>	1	1		
$K^{n} = 3p$ K even	levels, all S	2:1	0	(2/3)S <sub>0,9</sub>
	W		2	-(1/3)S <sub>0,9</sub>
K odd	S	2:1	3	-(2/3)S <sub>0,9</sub>
	W	<b>t</b> • 1	1	(1/3)S <sub>0,9</sub>
VH 4 25 1		1		
<u>K <del>7</del> 3p</u>	levels, all	<u> </u>		
K even	S	4:1	2	-(1/3)S <sub>0,9</sub>
	W		0	<sup>(2/3)S</sup> 0,9
K odd	S	4:1	1	(1/3)S <sub>0,9</sub>
	W		3	-(2/3)S <sub>0,9</sub>
K" = 0 ]e	avel			
Jeven	S	6:2	0	(2/3)S <sub>0,9</sub>
	W		2	-(1/3)S <sub>0,9</sub>
J odd	S	10:6	0	(2/3)S <sub>0,9</sub>
	W		2	-(1/3)S <sub>0,9</sub>

TABLE I. TORSIONAL SPLITTINGS IN  $\nu_9$  OF  $\text{C}_2\text{H}_6$ 

 $(a)_{S} = stronger and W = weaker component$ 

 ${}^{(b)}S_{0,9} \equiv |\Delta_9 - \Delta_6|$  is the difference in torsional level splittings between the ground and  $v_9$  vibrational states.

	Present Study	Daunt, et al. <sup>(a)</sup>
ν <sub>0</sub>	821.7234	821.727(6)
Α α <sub>9</sub>	-7.90722(59)×10 <sup>-3</sup>	-7.837(30)x10 <sup>-3</sup>
B αg	1.27454(13)×10 <sup>-3</sup>	1.259(15)x10 <sup>-3</sup>
Ας <mark>2</mark>	0.694742(13)	0.6950(5)
ე უყ	-2.410(28)×10 <sup>-6</sup>	-2.42(1.30)×10 <sup>-6</sup>
K Ng	3.0758(49)×10 <sup>-5</sup>	3.448(1.300)×10 <sup>-5</sup> -
β <sub>9</sub>	-1.66(13)×10 <sup>-9</sup>	<sub>ND</sub> (c)
β <sub>9</sub> JK	-5.58(12)×10 <sup>-8</sup>	ND
β <sup>K</sup> β <sub>9</sub>	-1.810(38)x10 <sup>-7</sup>	ND
9 <sup>+</sup>	-1.8169(14)×10 <sup>-3</sup>	-1.832(30)×10 <sup>-3</sup>
ل وpۂ	1.98(16)x10 <sup>-8</sup> ,	ND
۵qg ۶	-8.80(33)×10 <sup>-7</sup>	ND
σ(S.D.)	$0.7 \times 10^{-3}$	6.7x10 <sup>-3</sup>
N/N <sub>0</sub> (b)	1342/1609	549/569

TABLE II. WHOLE BAND ANALYSIS OF  $v_9$  OF  $C_2H_6^+$ 

<sup>+</sup>All quantities in units of cm<sup>-1</sup>; error limits are 95% confidence limits.
<sup>(a)</sup>Daunt, S.J., Blass, W.E., Halsey, G.W., Fox K. and Lovell, R.J., 1981, J.
Mol. Spectrosc. <u>86</u>, 327.

 $(b)_{N/N_0}$  is the ratio of lines included without zero weight (N) to the total number of assigned lines(N<sub>0</sub>).

(c)<sub>Not</sub> determined.

TABLE III.	COMPARISON OF	TABLE III. COMPARISON OF RECENT DETERMINATIONS OF THE GROUND STATE CONSTANTS FOR ETHANE <sup>†</sup>	THE GROUND STATE CO	ONSTANTS FOR ETHANE <sup>†</sup>
	PRESENT WORK	PINE AND LAFFERTY(a)	LIN, ET AL. (b)	COLE, ET AL. (c)
BO	0.6630279(24)	0.6630271(14)	0.6630353(152)	0.663089(24)
D <sup>J</sup> (×10 <sup>-6</sup> )	1.0324(23)	1.0312(26)	1.0406(16)	1.084(35)
D <sup>JK</sup> (×10 <sup>-6</sup> )	2.651(88)	2.660(29)	2.575(274)	5.00(66)
σ(x10 <sup>-3</sup> )	0.87	0.55	2.2	ı
(p) <sup>0</sup> N/N	760/893	766 <sup>(e)</sup>	230/285	<sub>184</sub> (e)
<sup>†</sup> All quantities are		in units of cm <sup>-1</sup> .		
(a) <sub>Pine</sub> , A.	S. and Lafferty	(a) <sub>Pine</sub> , A.S. and Lafferty, W.J., 1982, J. Res. Natl. Bur. Stand., <u>87</u> 237; uncertainties	tl. Bur. Stand., <u>87</u>	237; uncertainties
are one	are one standard deviation.	cion.		
<sup>(D)</sup> Lin, K.F	., Blass, W.E.	<pre>(<sup>D)</sup>Lin, K.F., Blass, W.E. and Gailar, N.M., 1980, J. Mol. Spectrosc. 79, 151.</pre>	J. Mol. Spectrosc.	
<sup>(c)</sup> Cole, A.	.R.H., Cross, K.	<sup>(c)</sup> Cole, A.R.H., Cross, K.J., Cugley, J.A. and Heise, H.M., 1980, J. Mol. Spectrosc.	se, H.M., 1980, J.	Mol. Spectrosc. 233;
uncertai	inties are two s	uncertainties are two standard deviations.		
$(d)_{See N/N_0}$ comment		in Table II.		
(e) <sub>These ca</sub>	ns	performed with standard fixed weighting methods.	d weighting methods	·

- 42 -

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<u>K"</u>	<u>j"</u>	Relative <sup>a</sup> Increase in R-type (ΔK=+1) Transitions	Relative <sup>b</sup> Decrease in P-type (ΔK=-1) Transitions	Percent Intensity Over(under) estima- tion for R(P) Transitions
1 1 1 1 1 1	10 15 20 25 30 35 40	1.048 1.084 1.145 1.221 1.309 1.403 1.497	0.962 0.917 0.855 0.779 0.691 0.597 0.503	4 8 15 22 31 40 50
2	10	1.018	0.982	2
2	15	1.072	0.928	7
2	20	1.112	0.888	11
2	25	1.160	0.840	16
2	30	1.215	0.785	21
3	10	1.012	0.988	1
3	20	1.048	0.952	5
3	30	1.107	0.893	10
4	10	1.008	0.992	1
4	20	1.035	0.965	3
4	30	1.080	0.920	8
5	10	1.006	0.994	0
5	20	1.028	0.972	3
5	30	1.063	0.937	6

# TABLE IV. INTENSITY EFFECTS OF &-RESONANCE

<sup>a</sup> Intensity ratio of R(perturbed)/R(unperturbed)

<sup>b</sup> Intensity ratio of P(perturbed)/P(unperturbed)

141

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COINCIDENCES	
LIST OF <sup>14</sup> CO <sub>2</sub> LASER LINES AND NEARBY COINCIDENCES WITH v <sub>9</sub> <sup>2</sup> of C <sub>2</sub> H <sub>6</sub> TRANSITIONS	r c
DF 14 WITH	
LIST (	
TABLE	

Relative Intensity		1.50784 0.37696 0.25736 0.30736	.4287	anne.		. 796	0.39827 1.41936 0.65653	995	.372	205	542	577	304 456	397	394	2/2 //2	417 383	534 364
Assignment ΔΚΔJ(K"J"σ")		RR(2,2,2) RR(2,2,0) RQ(4,33,2) RO(4,32,2)		, <sup>ر</sup> کر , +		3,15,	PR(3,15,1) RQ(5,18,1) RR(0,9,2)	0,9,0 2,13,	5,17,		, 16, 16,	5,15,	1,7,1	5,14,	5,13, 5,13,	2,5,2	2,5,0 5,12,	5,1 2
1) <u>Δν(MHz)</u>		-5224 -5156 -4428 -2019	324 2602 4815			-5445 -5387	-5315 -5281 -5129	-5062 -4564	- 3996 - 3895	- 3535 - 3436	-2583 -2583	- 1344	-471	-272 -183	815 901	1229	1305	1911 2765
$\frac{2002}{5}(cm^{-1})$	831.81368	831.63944 .64171 .66598 .74632	.82449 .90048 .27430	833.68367	835.53734	835.35570 .35764	.36005 .36119 .36626	.36848 .38511	.40403	.41944 .42271	.44/94 .45119 /8020	.49250	.52163	.52825	.56453 56740	.57835	.59834	.62957
CO <sub>2</sub> Laser 21ine	P(40)			P(38)	P(36)													
Relative Intensity		0.70824 0.81464 0.92992		. <b>- 1</b> - 9 - 9			0.26504 0.39225				1.75055 0.71817 1.55853							
Assignment <u>^KoJ(K"J"~")</u>		RQ(1,29,1) RQ(1,28,1) RQ(1,27,1)		<u> </u>	Î –Î –Î		RQ(2,34,2) RR(0,2,0)			$-\underline{\mathbb{C}}$	RQ(3,21,1) RQ(3,21,1) RD(3,20,3)	$\mathbb{C}$	$\sum_{i=1}^{n}$		$\mathbb{C}\mathbb{C}$	. <u> </u>	$2 \odot C$	<u> </u>
) <u>^</u> (MHz) <sup>†</sup>		-4648 -2868 -1122	394 583 2071	2250 3703 3874	5289 5451		4542 5965			-5903 -4401	-4268 -2834	-2706 -1331	-1210	213	1457 1567	2743 2848	3958 3058	5101
<sup>vCO2</sup> (cm <sup>-</sup> 1) <u>vC2H</u> 6	824.16974	824.01469 .07408 .13232	.18289 .18919 .23882	.24480 .29327 .29897	.34615	826.10540	826.25690 .30437	828.02458	829.92733	829.73042 .78052	.83281	.83705	.88696	.93442	.97594	830.01883 02233	.05935 .05935	.09749
CO <sub>2</sub> Laser	P(48)					P(46)	- 44: -	P(44)	P(42)									

	1.06952 0.25704 1.02816 0.95792 0.85480 0.71400 0.53000	0.28760 0.42568 0.28312 0.62275 1.86825 0.60527	0.26798 1.07192 0.33640 1.34560 1.66984 0.41746	0.48053 2.13296 0.53324 0.53324 0.55380 0.59226 0.59226 0.59226 0.59226 0.53126 0.65315 0.65315 0.65315 0.33217 0.65315 0.33217 0.33217
•	RQ(7,14,1) RQ(7,13,3) RQ(7,13,1) RQ(7,12,1) RQ(7,11,1) RQ(7,10,1) RQ(7,9,1)	PR(5,25,1) PR(4,23,2) RQ(8,29,2) RR(0,15,2) RR(0,15,0) PR(3,21,3)	PR(1,18,3) PR(1,18,1) RR(1,14,3) RR(1,14,3) RR(2,12,2) RR(2,12,0) RR(2,12,0)	RQ(9,23,3) RR(4,9,2) RR(4,9,2) RQ(9,22,3) RQ(9,22,1) RQ(9,22,1) RQ(9,22,1) RQ(9,22,1) RQ(9,20,1) RQ(9,19,1) RQ(9,19,1) RQ(9,11,3) RQ(9,11,3) RQ(9,11,3) RQ(9,11,1) RQ(9,11,1) RQ(9,11,1) RQ(9,11,1) RQ(9,11,1) RQ(9,11,1)
ø	998 2020 2101 3130 4076 4948 5740	3022 4253 4621 4993 5847 5847	-5448 -5304 648 756 3406 3518	-5050 -3866 -3780 -3780 -3223 -1471 -145 -145 -145 -73 -73 -73 -73 -73 -73 -73 -73 -73 -73
	.03395 .06806 .07075 .10507 .13663 .13663 .16571 .19212 842.78930	842.89010 .93118 .94345 .95586 .95808 .95808 .98434 .98434	844.38000 .38479 .58335 .58693 .67534 .67908 846.31794	846.14949 18960 19187 21043 21402 26888 27232 31310 31549 3112 38112 38112 47560 47660 47660 47952 47952 47952
	V. CONT'D.) P(28)	P(26)	P(24)	
	(TABLE 1.45792 1.97080 0.98540 0.33594 1.34376 0.29692 1.18768 0.98464 0.72768	0.28507 0.33533 0.39147 0.45340 0.26047 0.52093	0.25713 0.37960 0.53712 0.50554 0.84256 0.72953	
	RQ(5,11,1) RR(3,3,3) RR(3,3,1) RQ(5,10,1) RQ(5,9,1) RQ(5,9,1) RQ(5,8,1) RQ(5,8,1) RQ(5,7,1)	RQ(6,31,0) RQ(6,30,0) RQ(6,29,0) RQ(6,28,0) RQ(6,27,0) RQ(6,27,0)	PR(6,24,0) PR(5,22,1) PR(4,20,2) RR(0,12,2) RR(0,12,0) PR(3,18,3) PR(3,18,3)	$\begin{pmatrix} (2) \\ (1) \\ (1) \\ (1) \\ (2$
	2844 3213 3213 3624 4408 4483 5182 5807	-2999 -660 1612 3813 5740 5943	-2559 -2168 -1427 -412 -346 -342	
⊾'	.63222 .64452 .64452 .64677 .66077 .68829 .68687 .71019	837.37471 837.27466 .35270 .42847 .50189 .56619 .57294	839.19581 839.11044 .12348 .14821 .18206 .18428 .18439	223040 223040 223040 223040 223040 223040 223040 223040 223040 23040000000000
		P(34)	(26) - 45 -	P(30)

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848.05797	847.92096 92318 92795 848.00364 08787 .17249	P(20) 849.78182	849.70794 .71233 .81382 .81866 .93555	. 23009 851 48950	51.3569 51.3569 .5023	.59406	.65981	853.18100	853.07035 .11888	.12122 .16677	854.85631	854.80056 .81380 .6613	.90904 .90904 .91979 855.04873
	-4107 -4041 -3898 -1629 896 3433		-2215 -2083 959 1104 4609		-3973 -3865 385	3135	5027 5027 5106		-3317 -1862	-1792 -427		-1671 -1274 354	1581 1903 5769
	RR(0,19,2) RR(0,19,0) PR(4,27,2) PR(3,25,3) PR(2,23,2) PR(1,21,1)		RR(1,18,3) RR(1,18,1) RR(2,16,2) RR(2,16,2) RR(3,14,3) RR(3,14,3)	6 T T 6 0	RR(4,13,2) RR(4,13,0) RR(5,11,3) RR(5,11,3)	0,22,	6,9,2 6,9,0		PR(2,27,2) RR(7,8,3)	7,8,1	• •	1,22,12,20	RR(2,20,2) RR(2,18,0) RR(3,18,3) BR(3,18,3)
(TABLE	0.48790 1.46370 0.27408 0.41340 0.60376 0.87912		0.25402 1.01608 1.35968 0.33992 1.65467	•	1.82808 0.45702 0.51668	• •	• • •		0.38280 0.58980	.599		0,0,0	0.96312 0.25820 1.24067
V., CONT'D.		P(10)		P(8)		P(6)				P(4)			<u> </u>
(	.32425 .42528 .47923 .48383 .64585	858.15839	858.09157 .10651 .10996 .29436 .29704	859.78513	859.78340 .78606 .85442 .96172	861.39566	861.21833 .28594 28830	.37669	5554	862.98995	862.81721 863.00960 .01367	rem moral dram way	
	-5732 -2703 -1086 -948 3909 4007		-2003 -1555 -1452 4076 4157		-52 28 2077 5294		-5316 -3289 2210	-56 -56	4790		-5179 589 711		
	RR(3,19,1) RR(0,26,0) RR(4,17,2) RR(4,17,0) RR(5,15,3) RR(5,15,1)		PR(1,29,1) RR(6,14,2) RR(6,14,0) RR(7,12,3) RR(7,12,3)		RR(8,11,2) RR(8,11,0) RR(1,26,1) RR(2,24,2)		25 10	3, 23, 3, 23,	4,21,		RR(4,22,2) RR(5,20,3) RR(5,20,1)		x 10 <sup>10</sup> cm/sec.
	0.56583 0.28556 1.39280 0.34820 0.40944 1.63776		0.36008 0.86760 1.73520 0.47878 1.91512		1.93760 0.48440 0.37184 0.59776		0.52000 1.92180	0.72447	0.9406		0.83688 0.26128 1.04512		n

(TABLE V., CONT'D.)

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P(12)

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TABLE VI. SAMPLE PAGE FROM PART II OF THE  $\nu_{9}$  ETHANE BAND ATLAS

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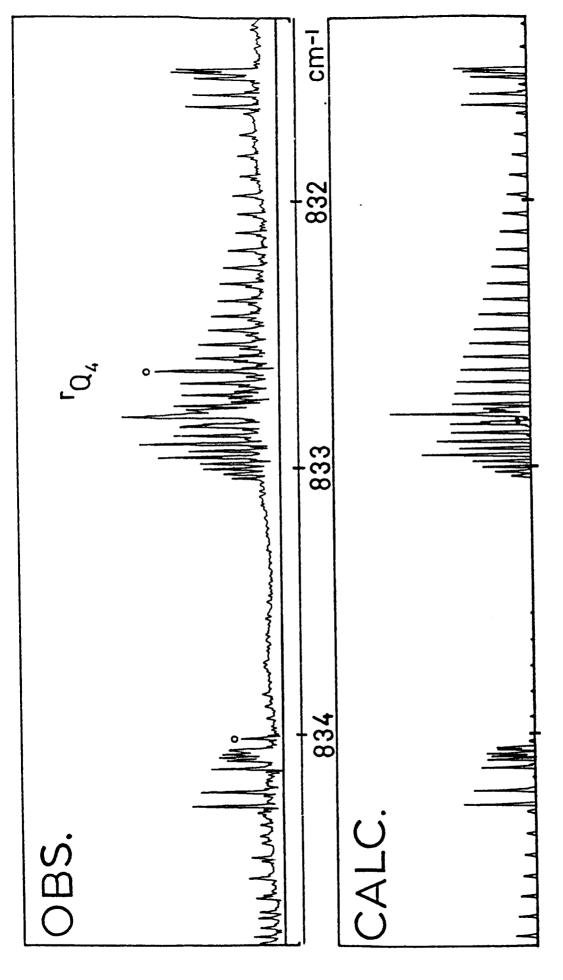
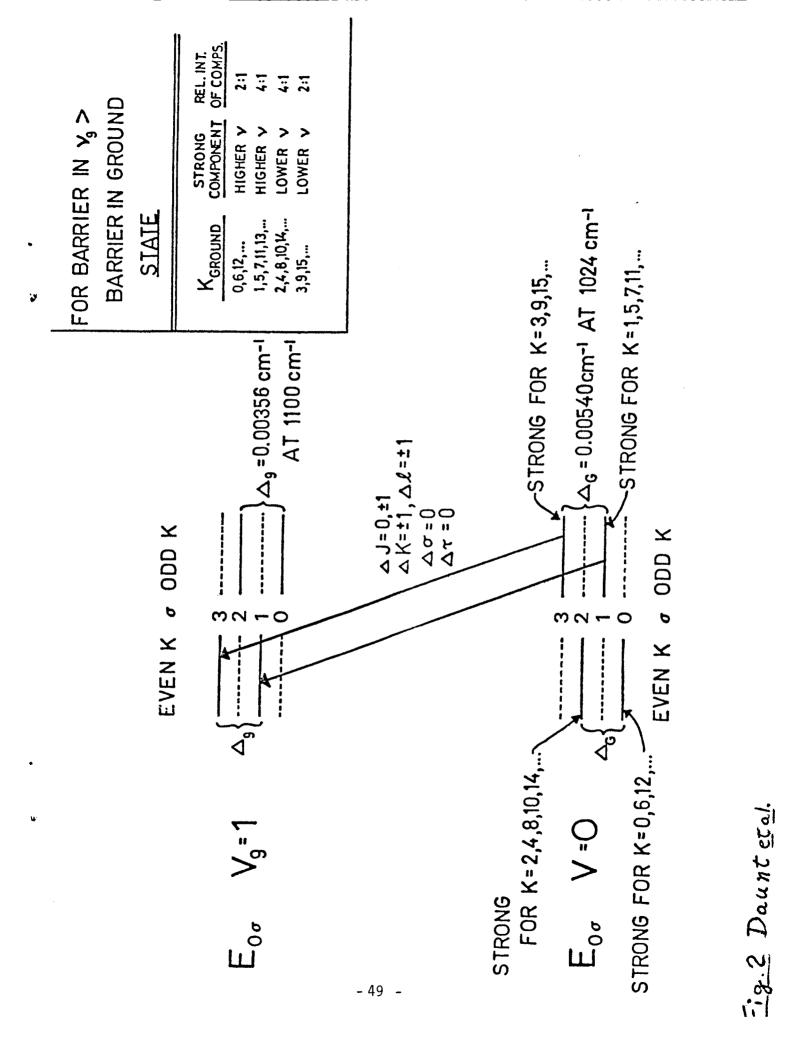
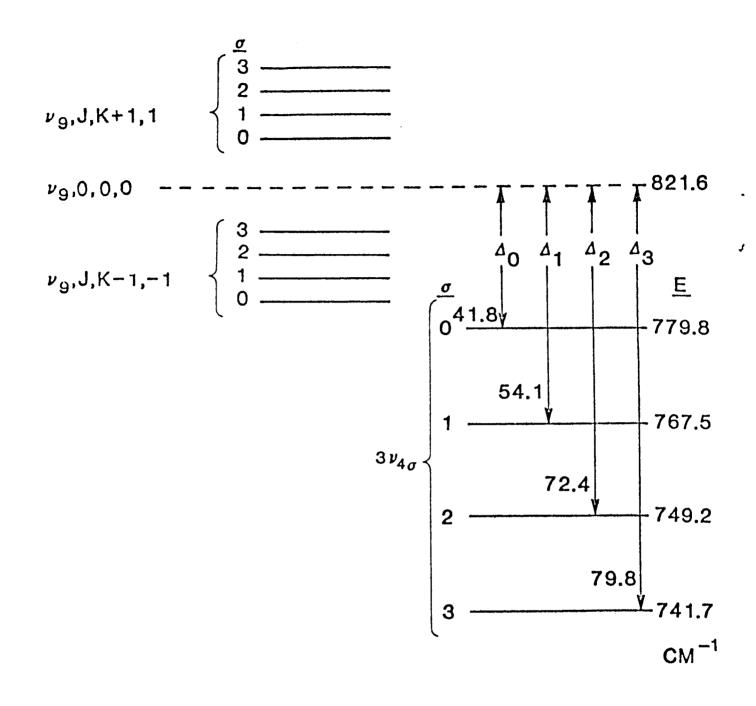
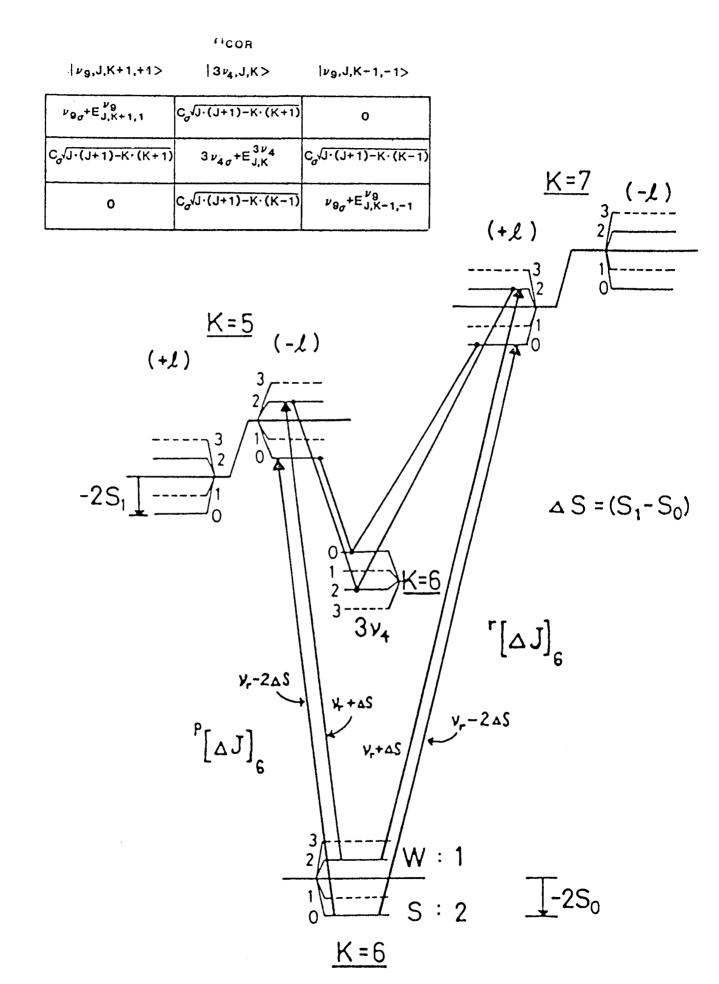


Fig. I Dant et al

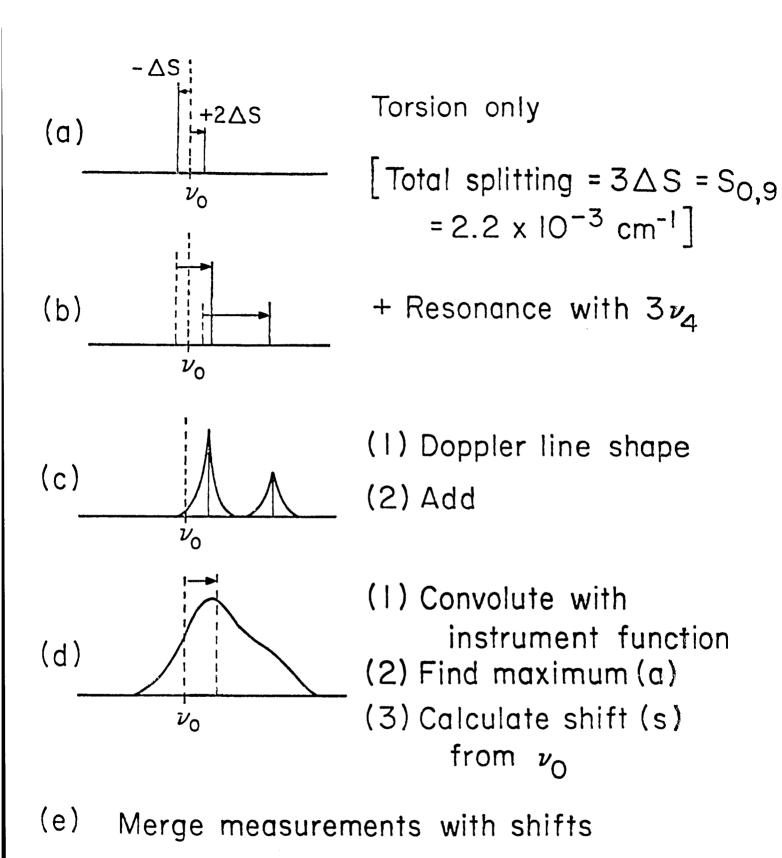






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(f) Use standard model +l - resonance

Fig.5 Dountetal.

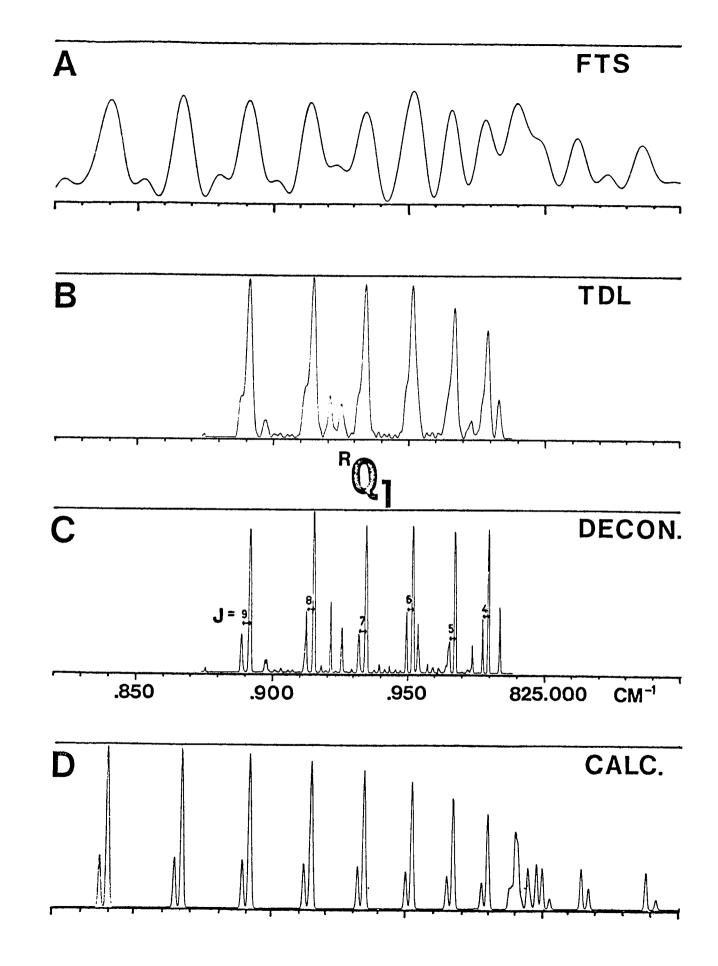
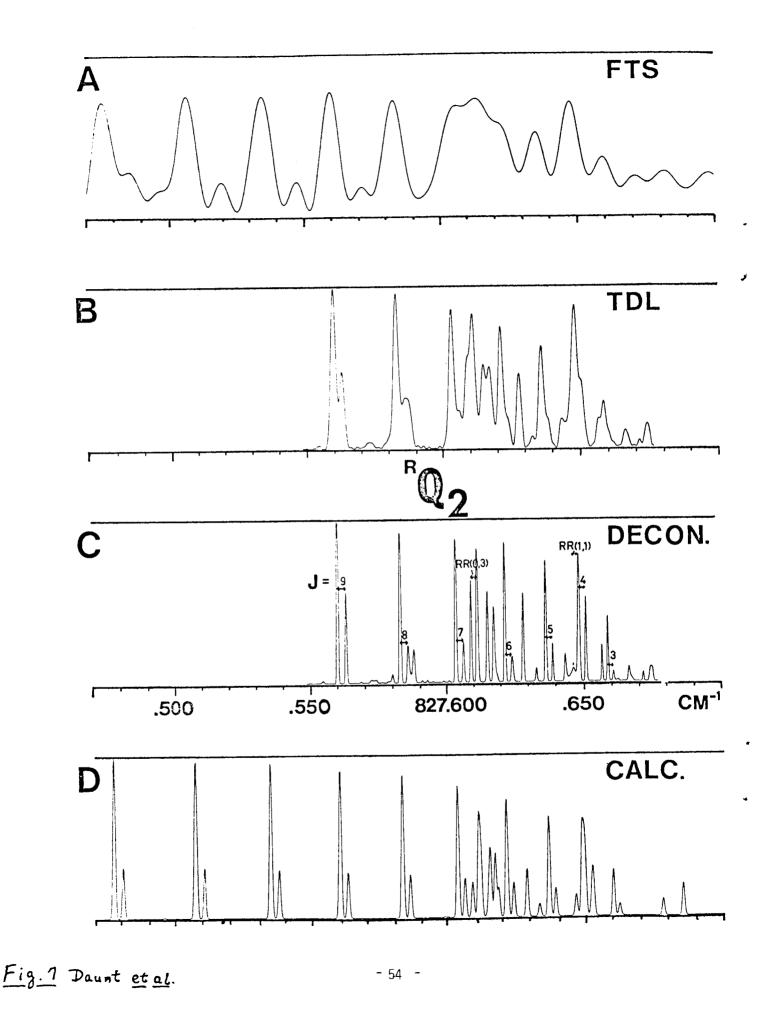


Fig. 6 Daunt et al.

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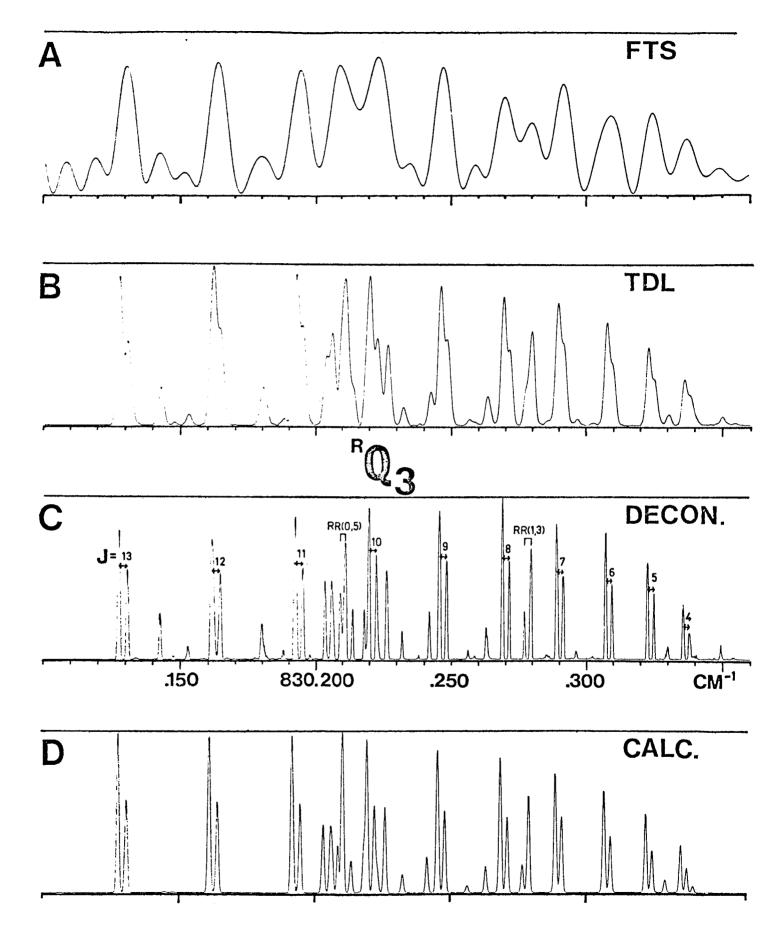


Fig. 8 Dauxt et al.

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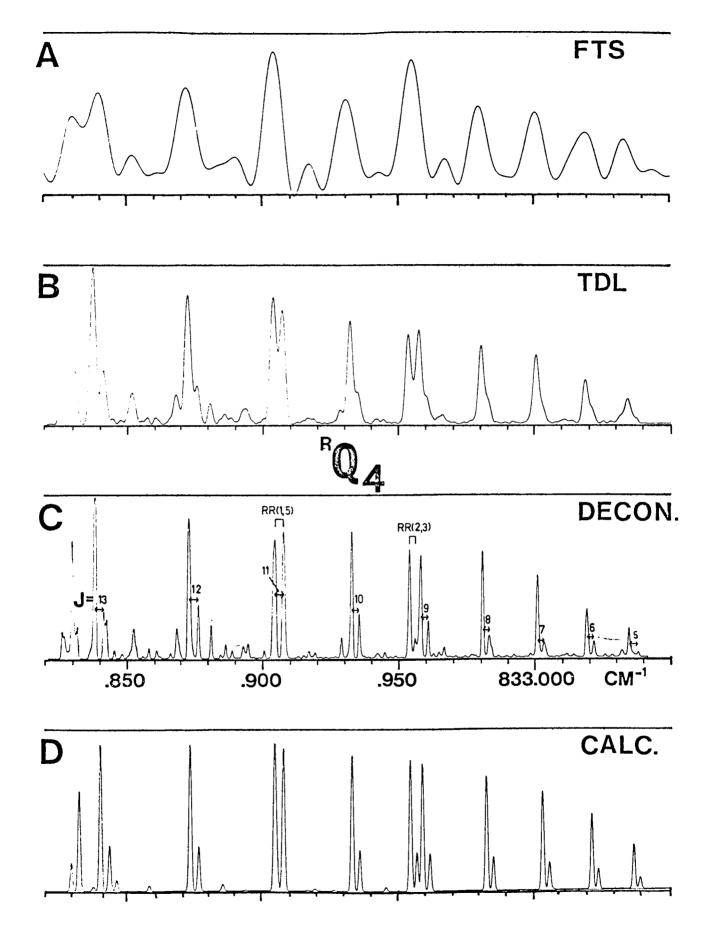


Fig. 9 Daunt et al.

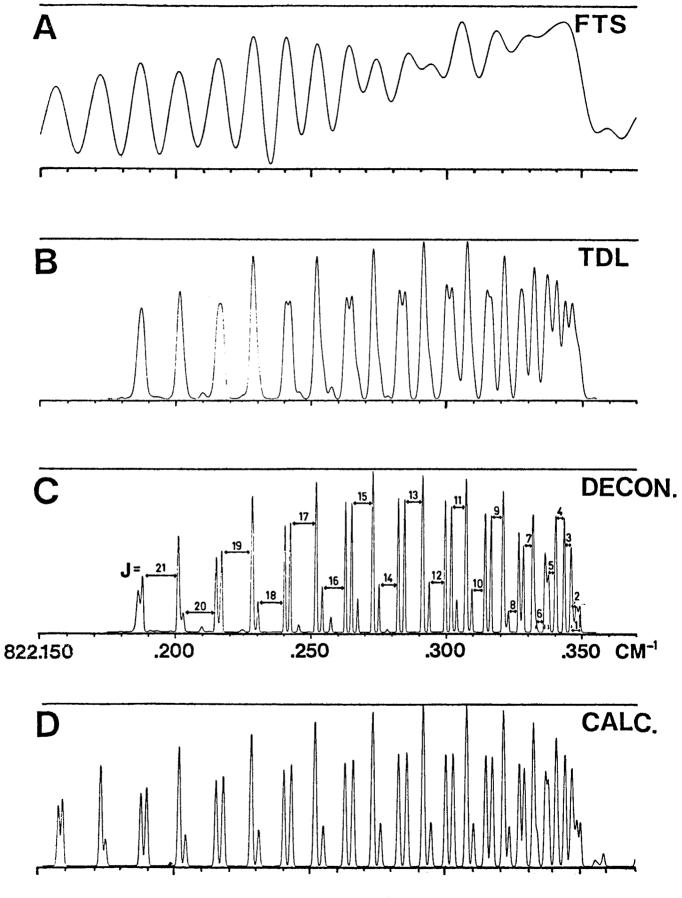
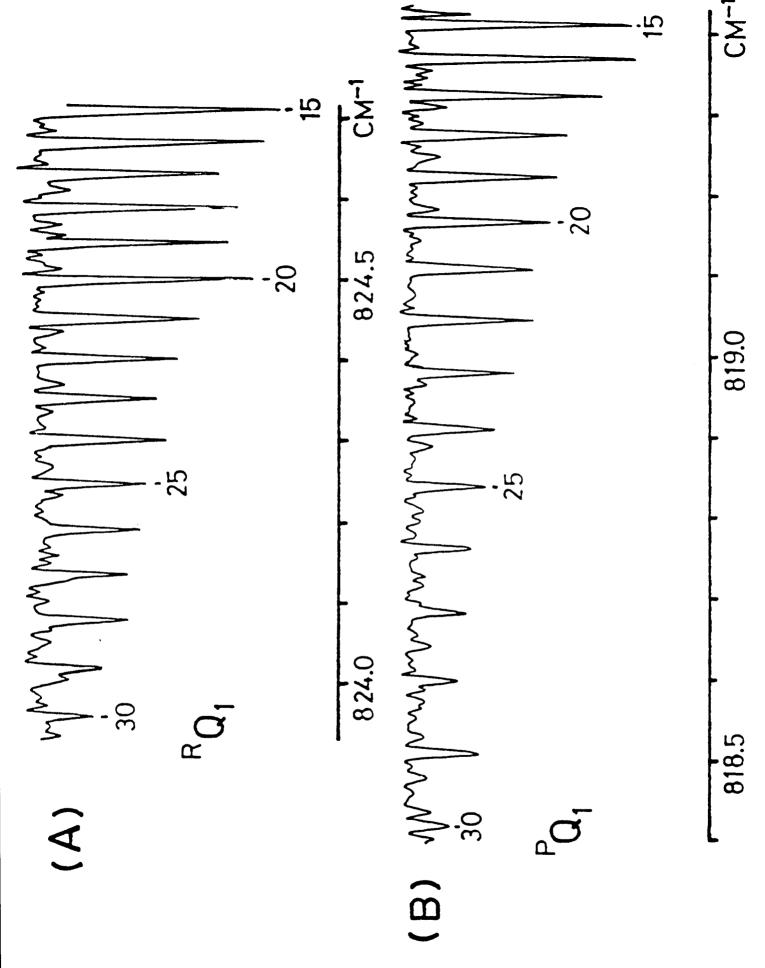
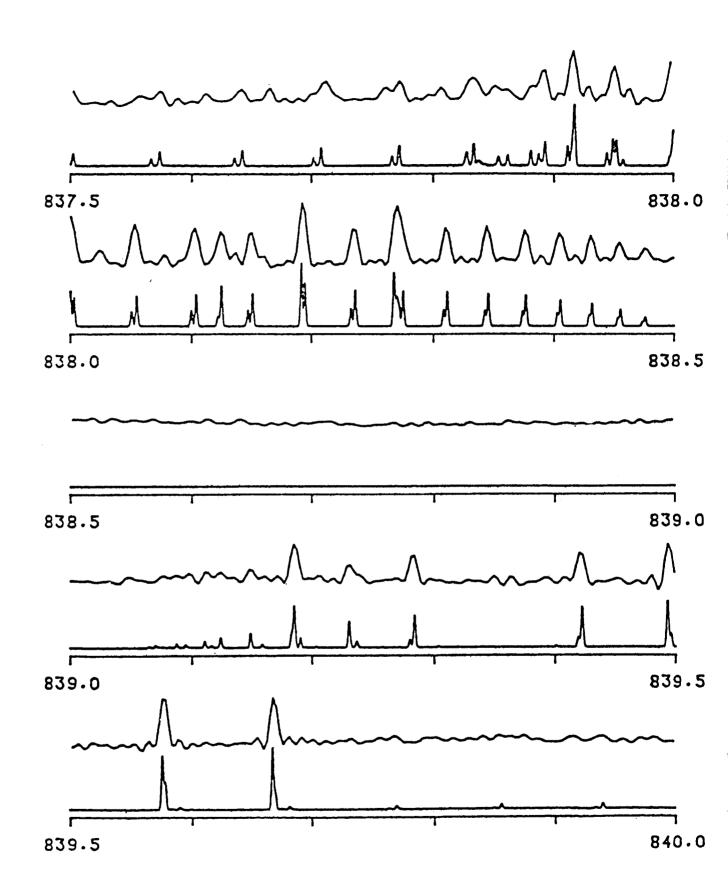


Fig. 10 Douxt et al.

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<u>PART\_II</u>

### The 12µm Band of Ethane

A Spectral Catalog from 765  $\rm cm^{-1}$  to 900  $\rm cm^{-1}$ 

#### A.K. Atakan, W.E. Blass, S.J. Daunt and G.W. Halsey The University of Tennessee Molecular Spectroscopy Laboratory

## D.E. Jennings, D.C. Reuter and J. Susskind NASA/Goddard Space Flight Center

and

#### J.W. Brault Kitt Peak National Observatory

Prepared	:	Under NASA Contract #NAS5-26896 to The University of Tennessee
Ву	:	A.K. Atakan and W.E. Blass
Principal Investigators	:	W.E. Blass and S.J. Daunt

December 1982

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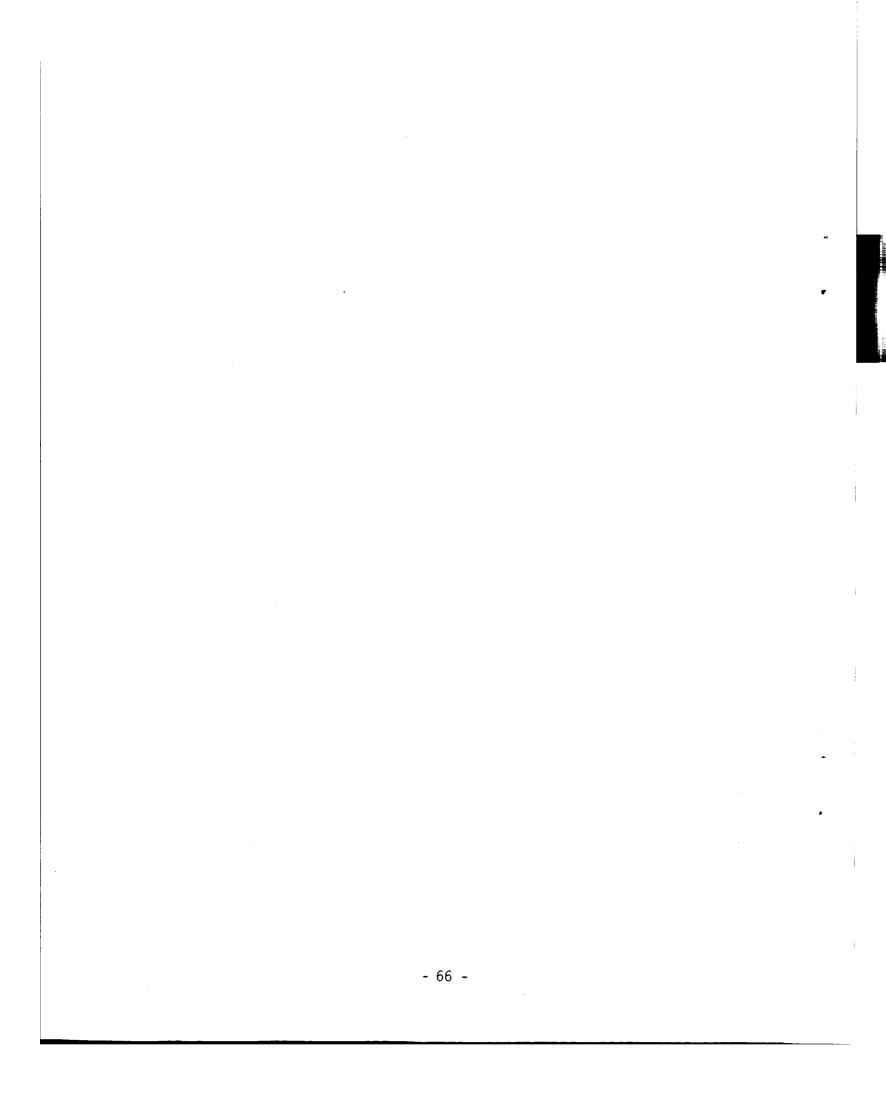
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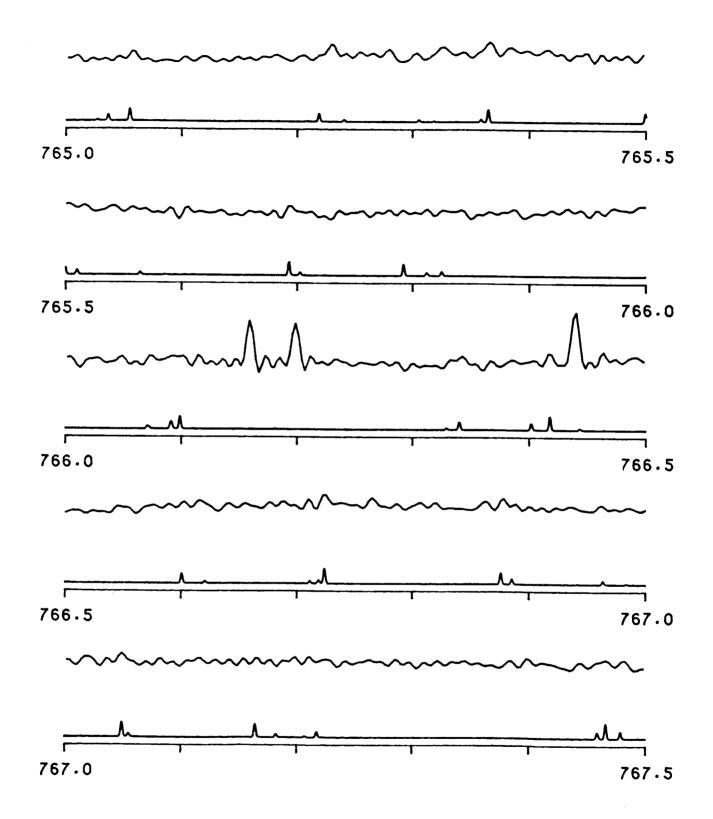
#### Figure 1

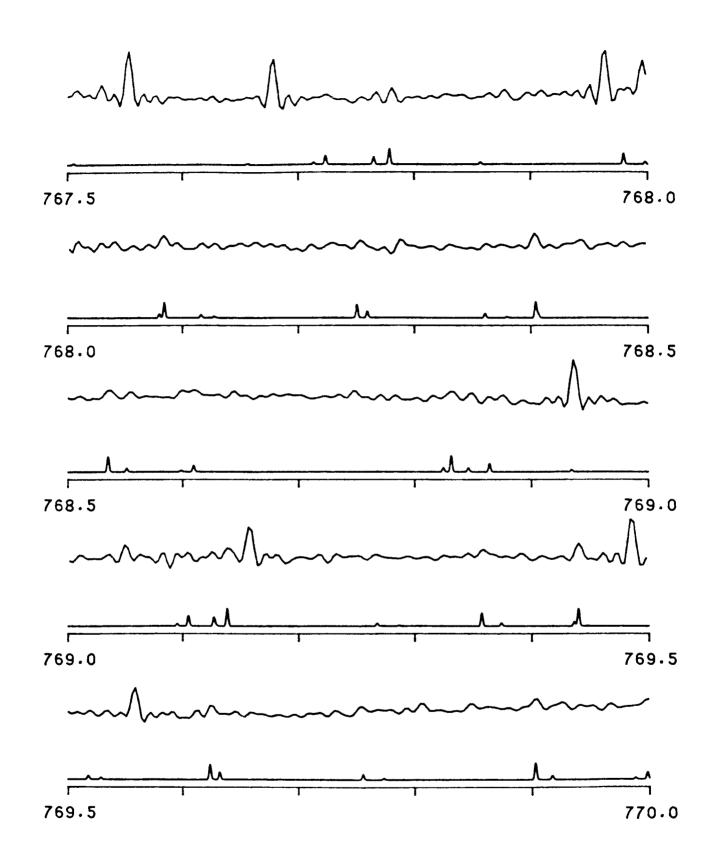
The observed 0.005 cm<sup>-1</sup> resolution spectrum taken at KPNO on the McMath Interferometer is presented in the upper trace of each panel, the calculated spectrum<sup>+</sup> (at an effective resolution of 0.0018 cm<sup>-1</sup>) is presented in the lower trace of each panel. The relative intensities correspond to  $300^{\circ}$ K ethane and the apparent line width corresponds to an infinitely high resolution spectrum of Doppler limited  $300^{\circ}$ K ethane.

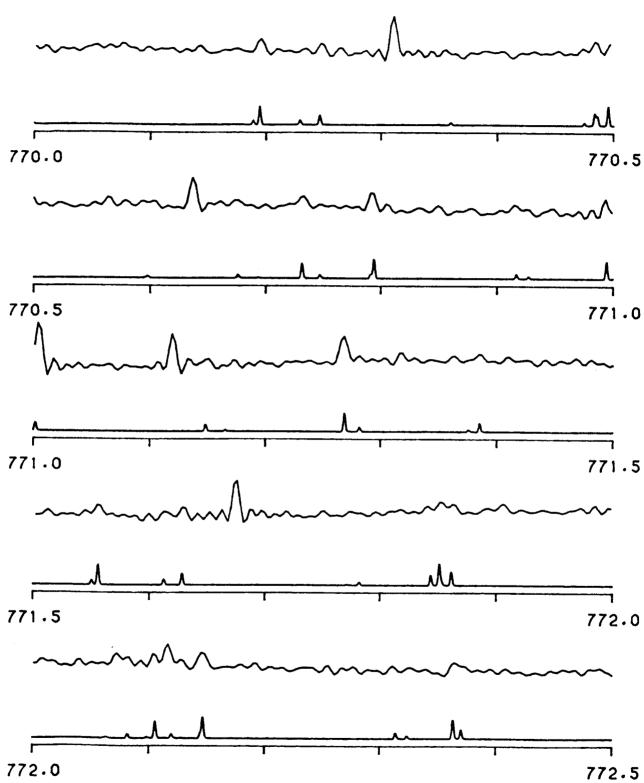
<sup>†</sup>The calculated spectrum is based upon the results of:

- (1) "Diode laser spectra of the torsional splittings in the  $v_9$  band of ethane: Torsion-vibration-rotation interactions and the barrier to internal rotation", J. Susskind, D.C. Reuter, D.E. Jennings, S.J. Daunt, W.E. Blass and G.W. Halsey, J. Chem. Phys., 77, 2728 (1982).
- (2) "The 12µm Band of Ethane: High Resolution Laboratory Analysis with Candidate Lines for Infrared Heterodyne Searches", S.J. Daunt, A.K. Atakan, W.E. Blass, G.W. Halsey, D.E. Jennings, D.C. Reuter, J. Susskind and J.W. Brault, submitted to Ap. J.; Part I of this memorandum.



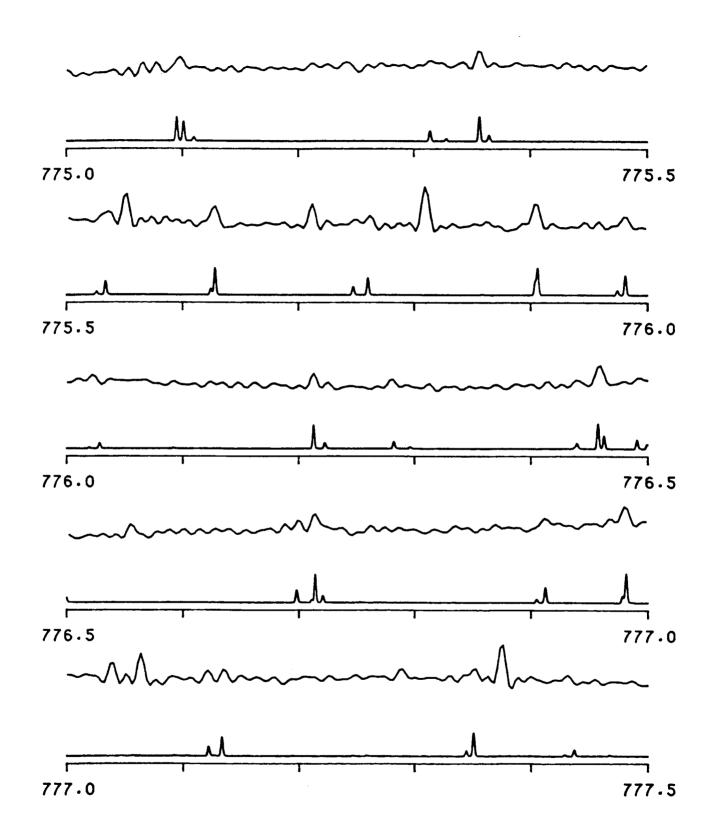


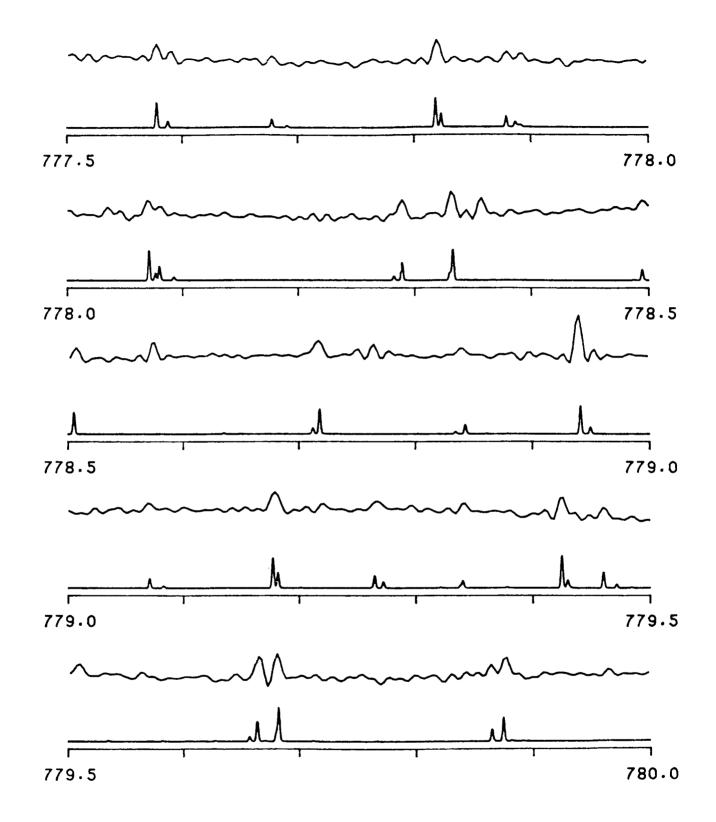


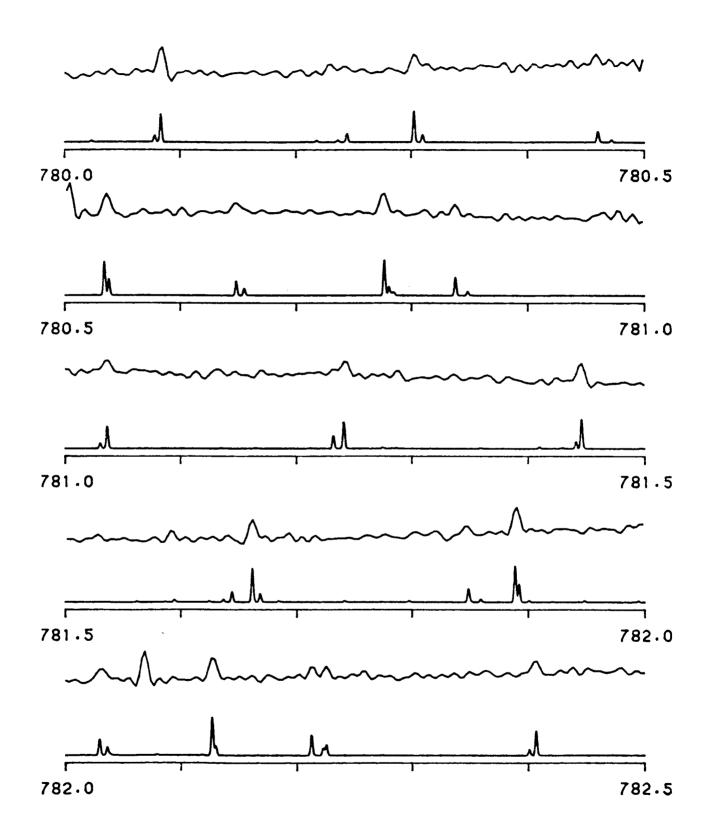


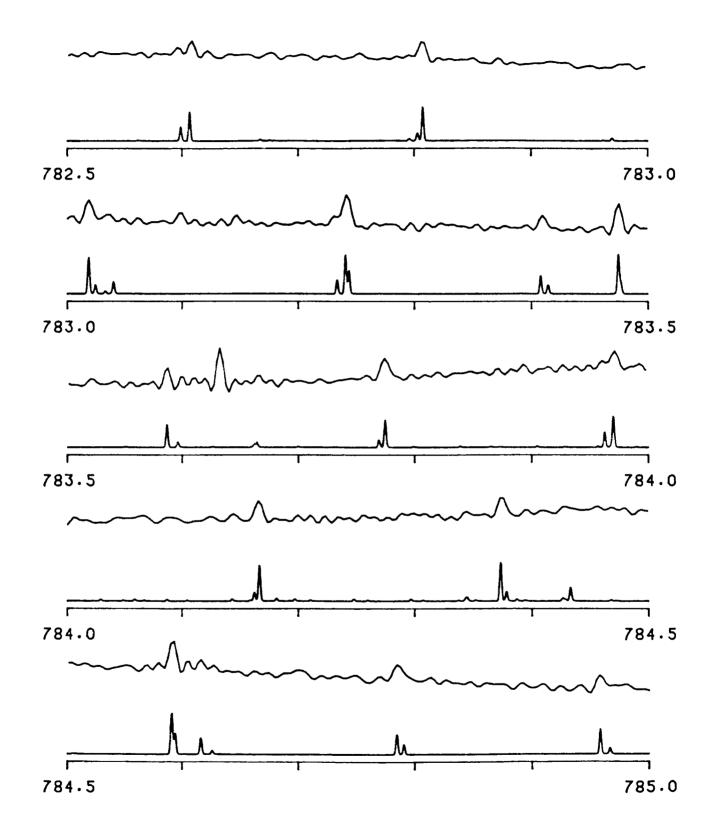


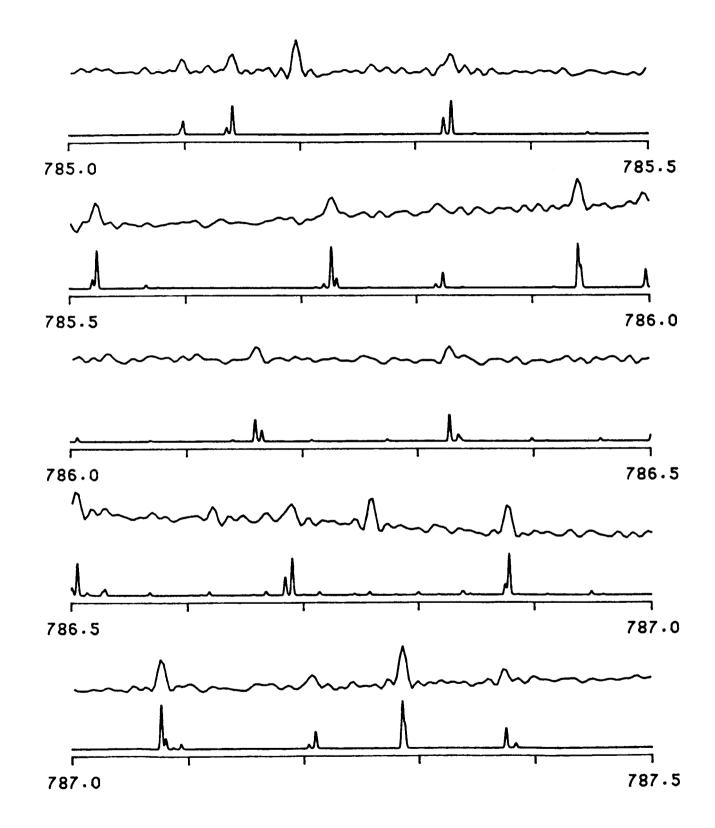




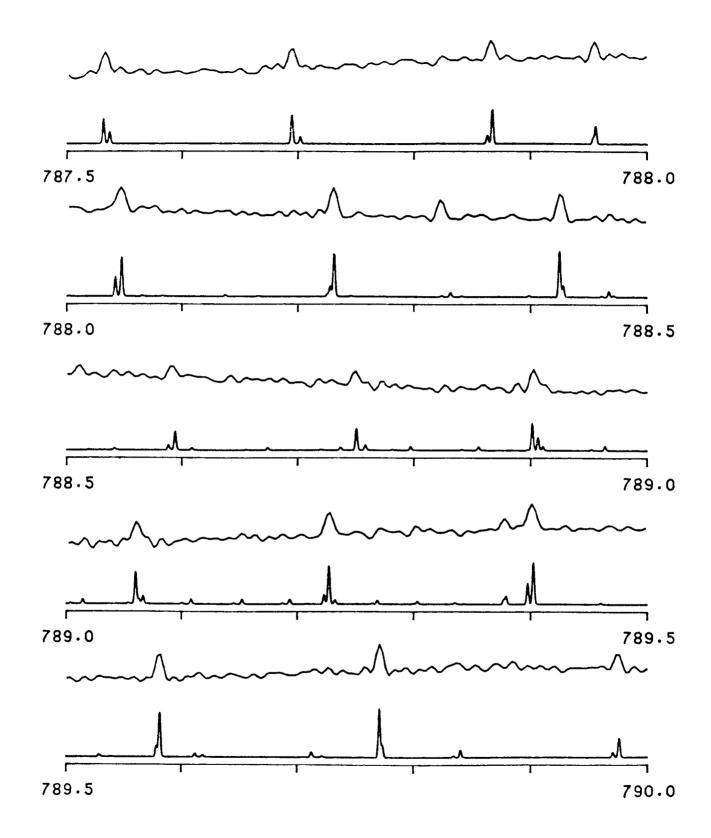


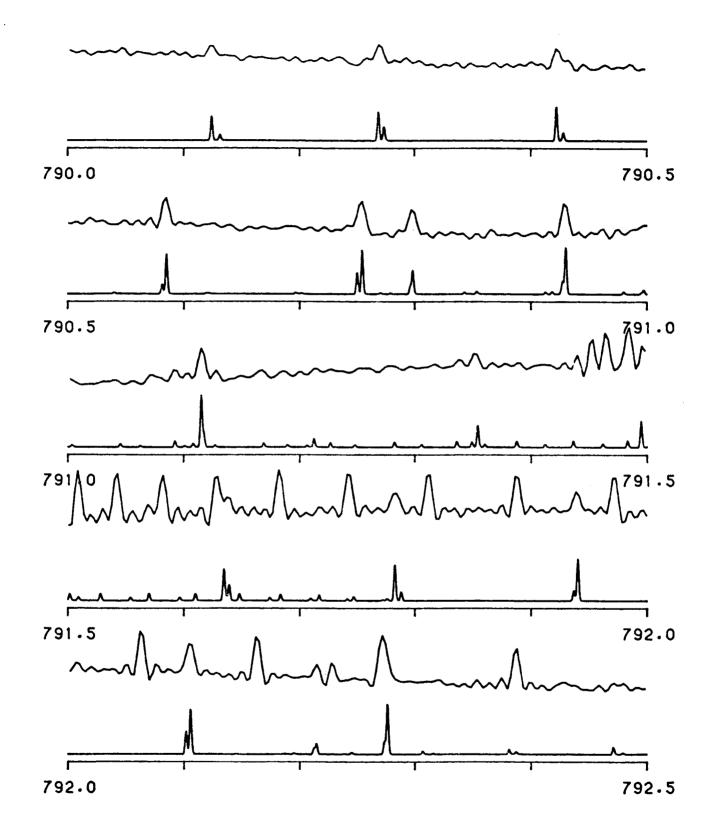


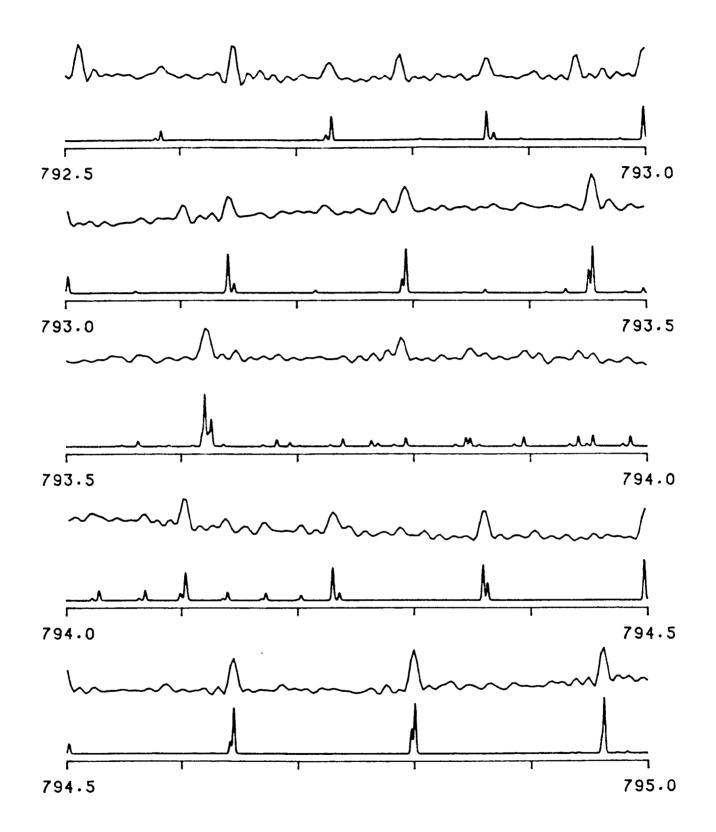


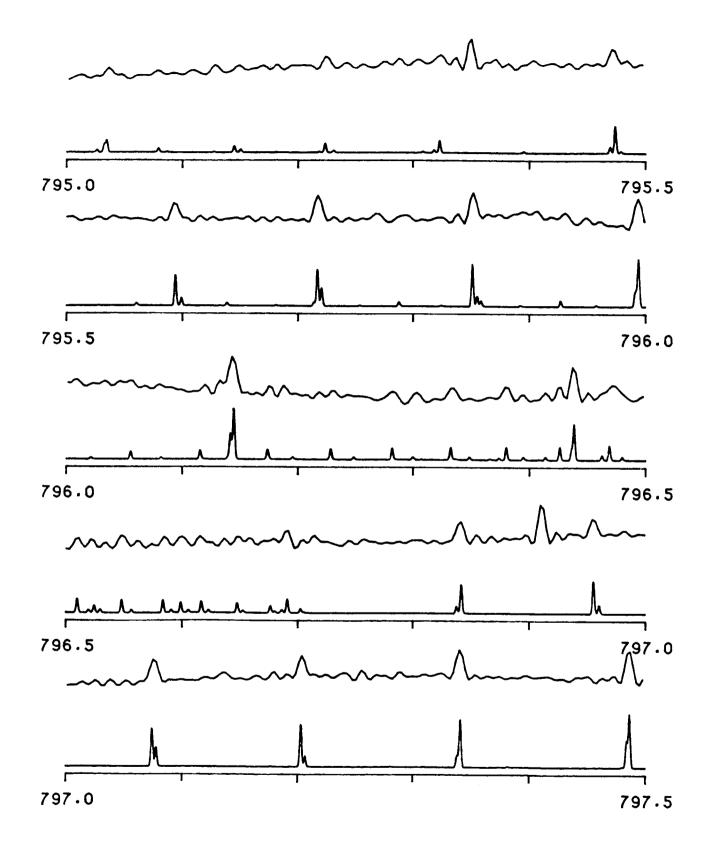


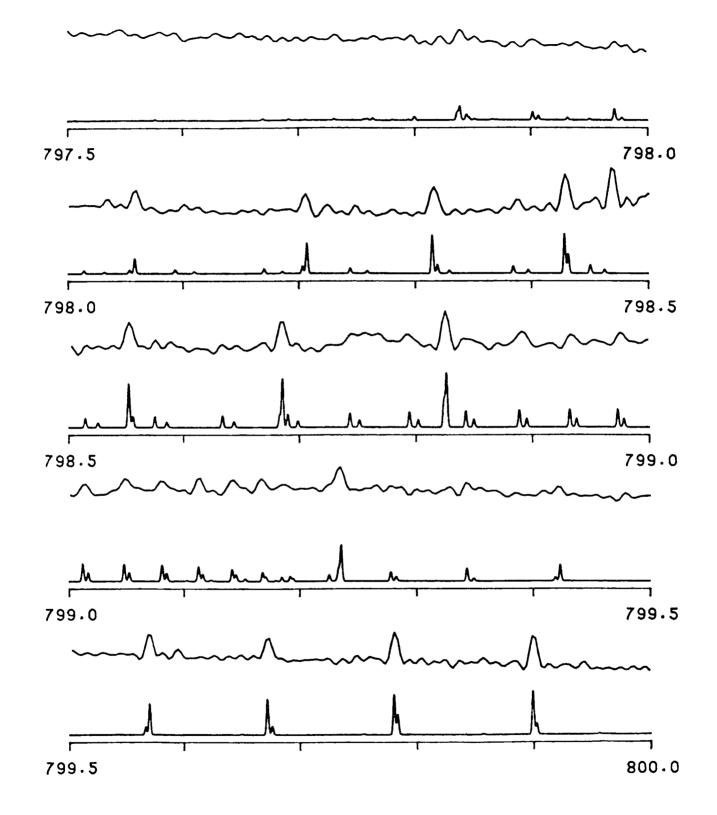
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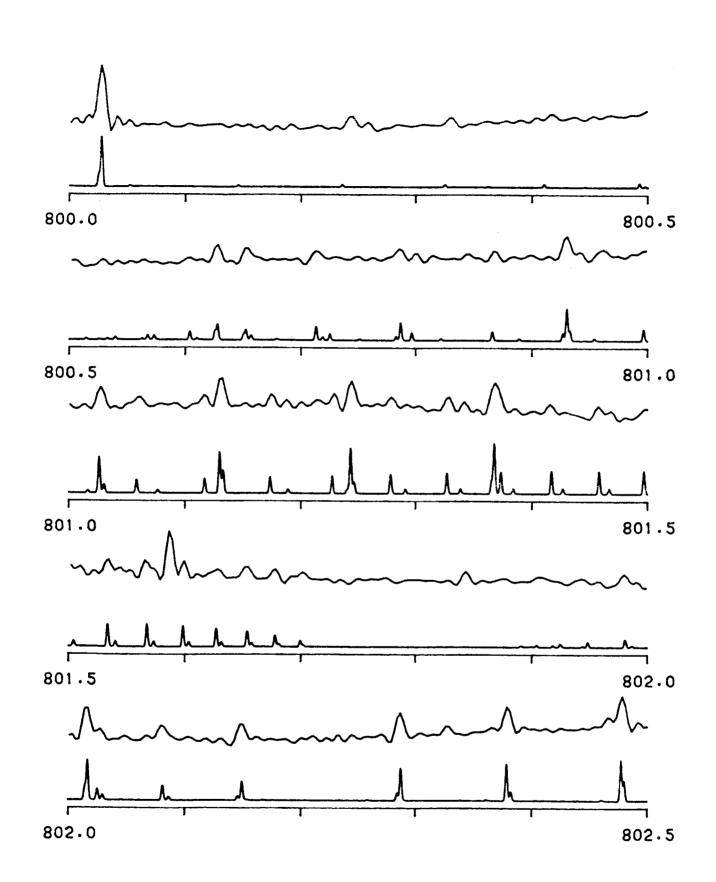


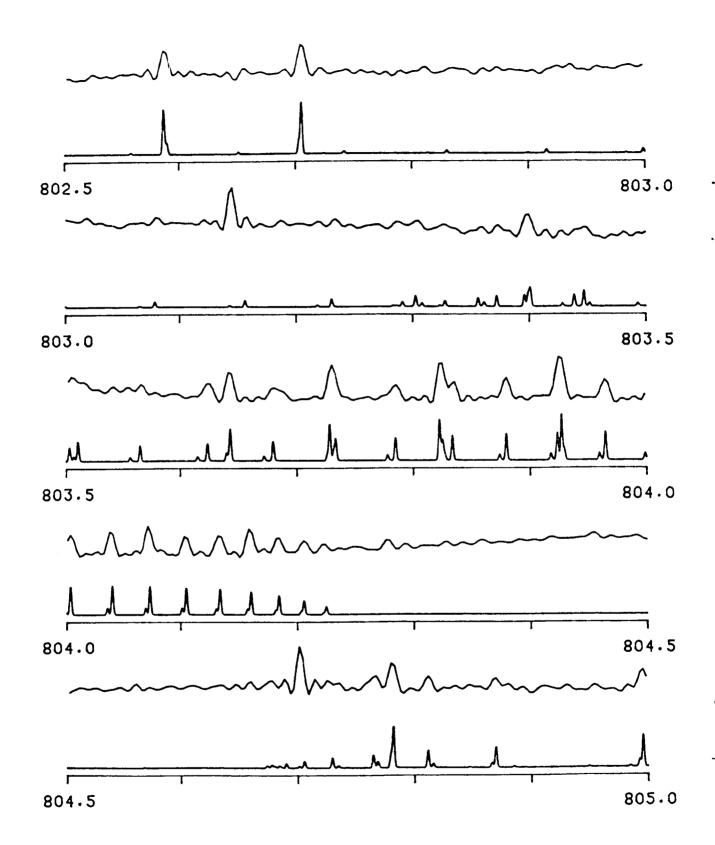


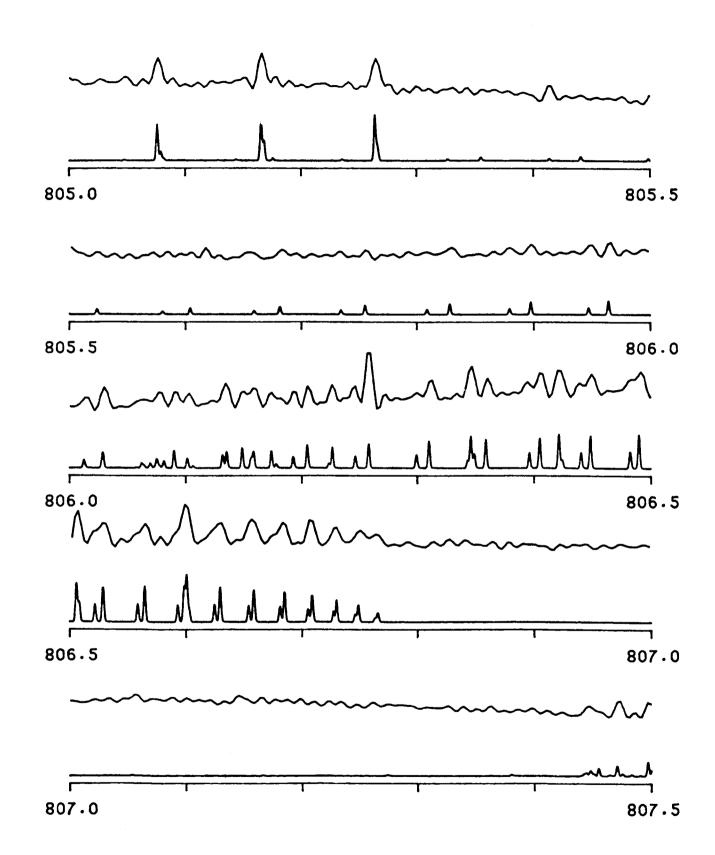


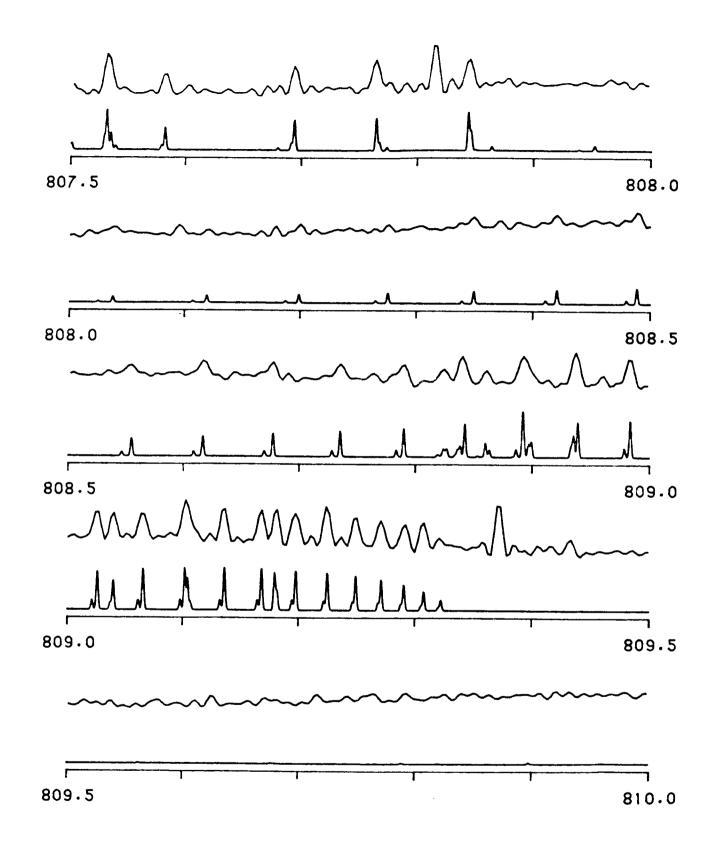


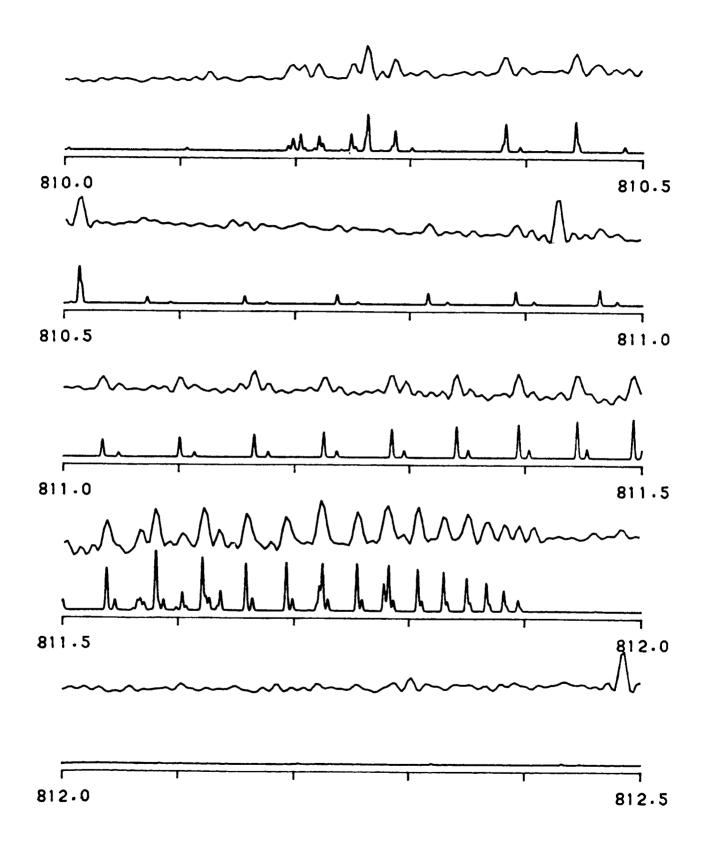


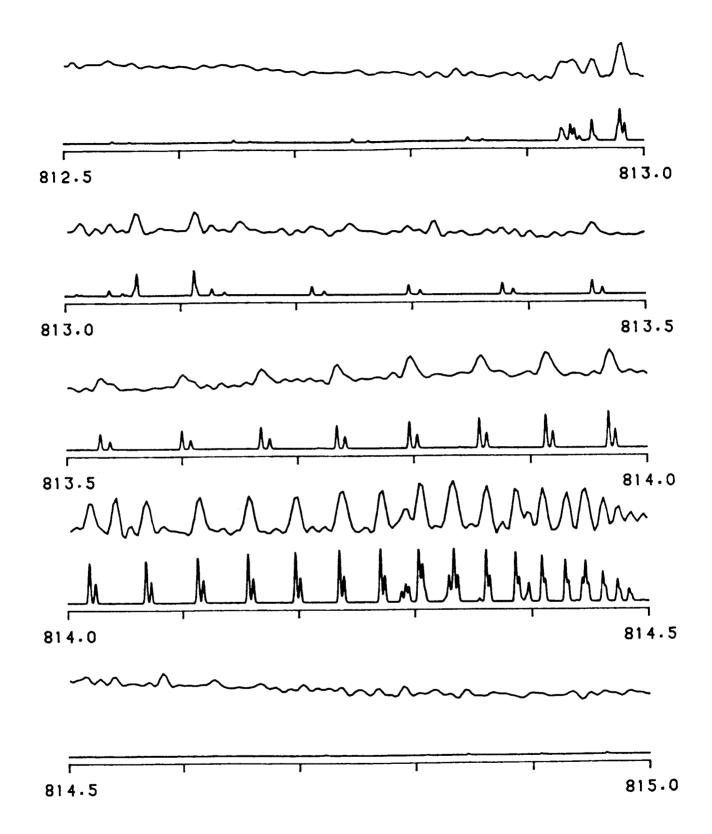


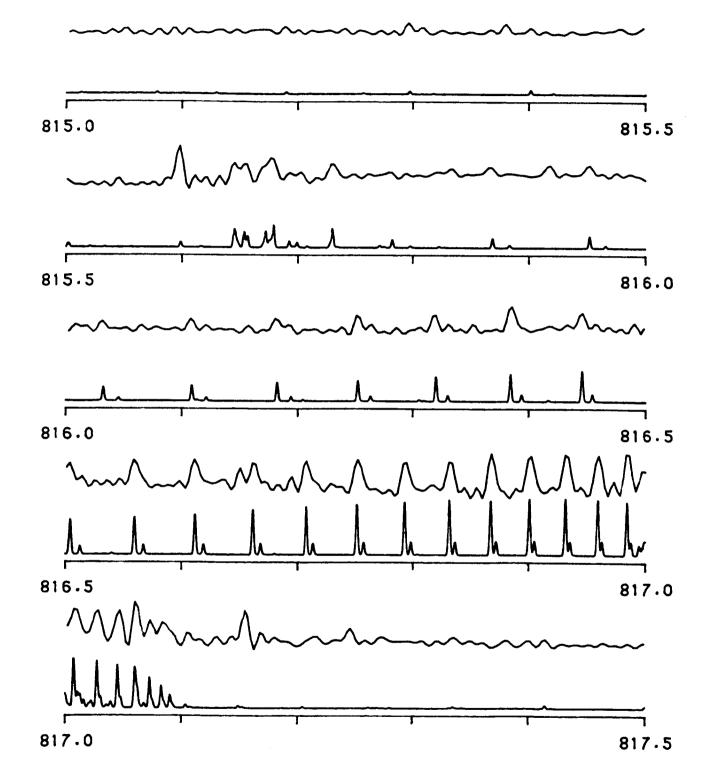


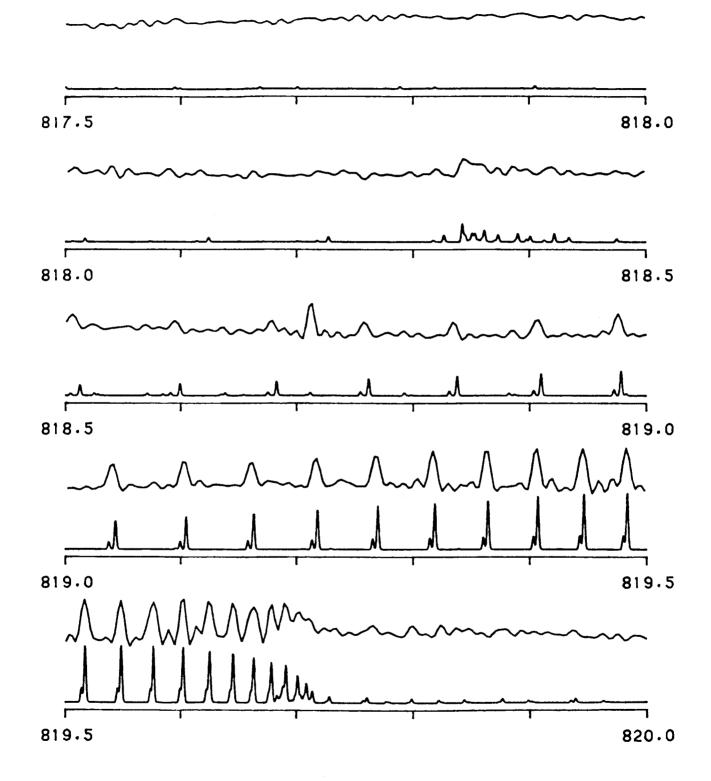


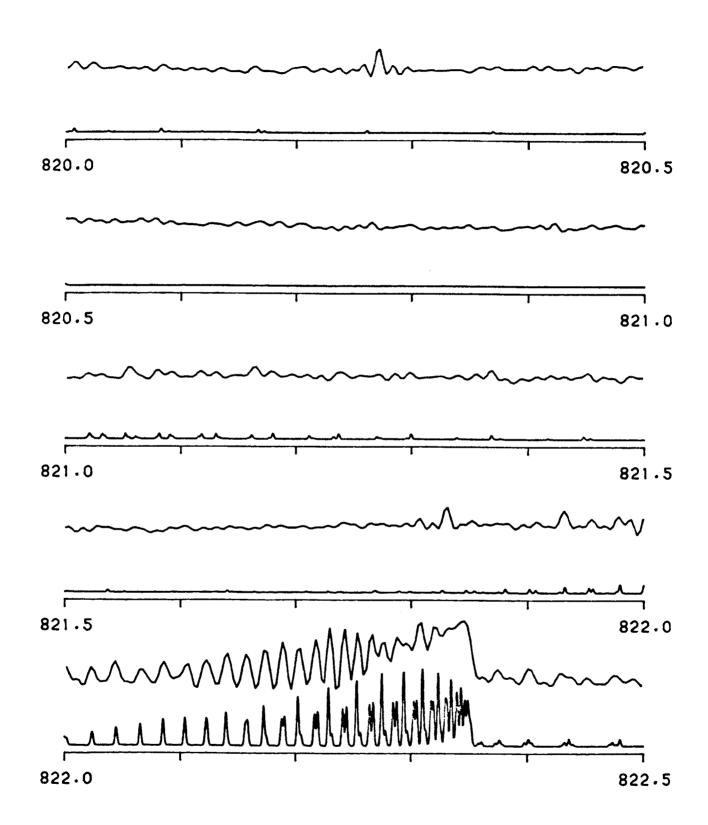


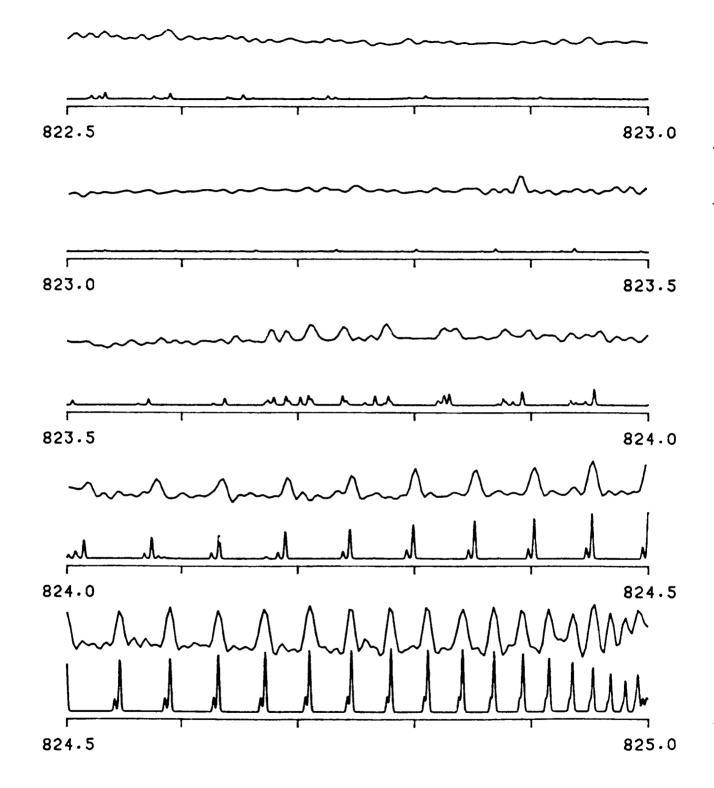


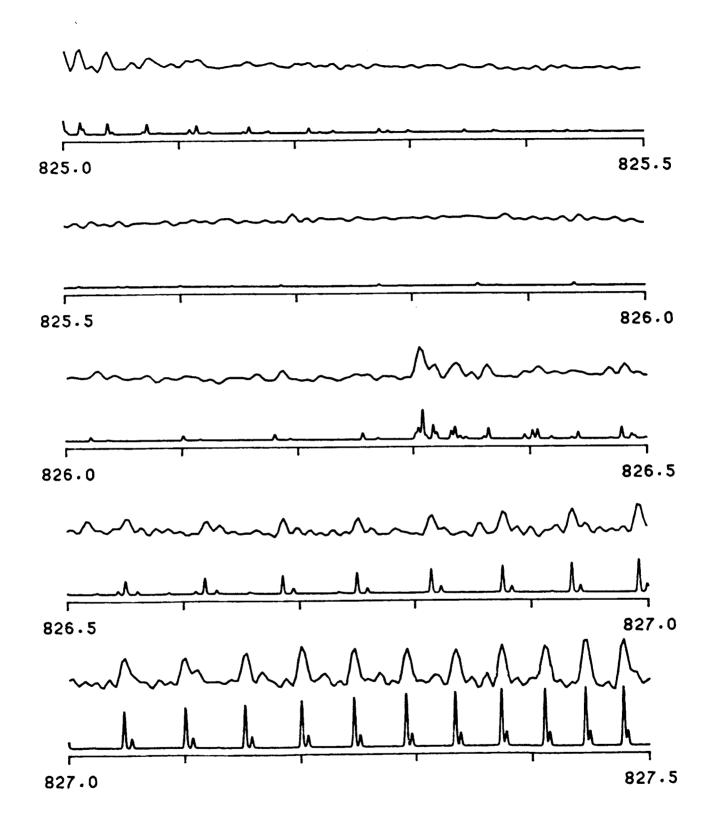


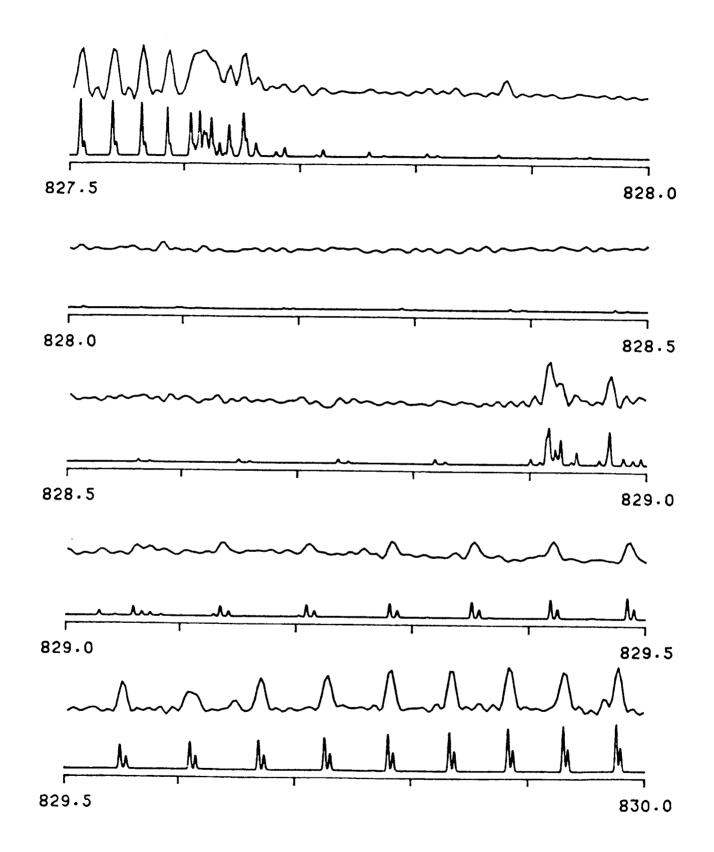


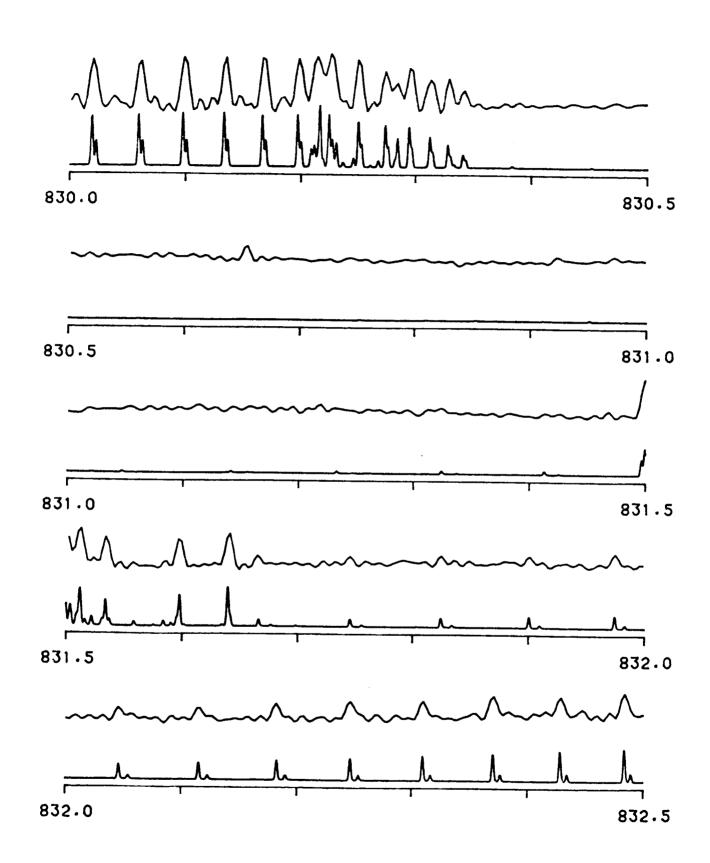


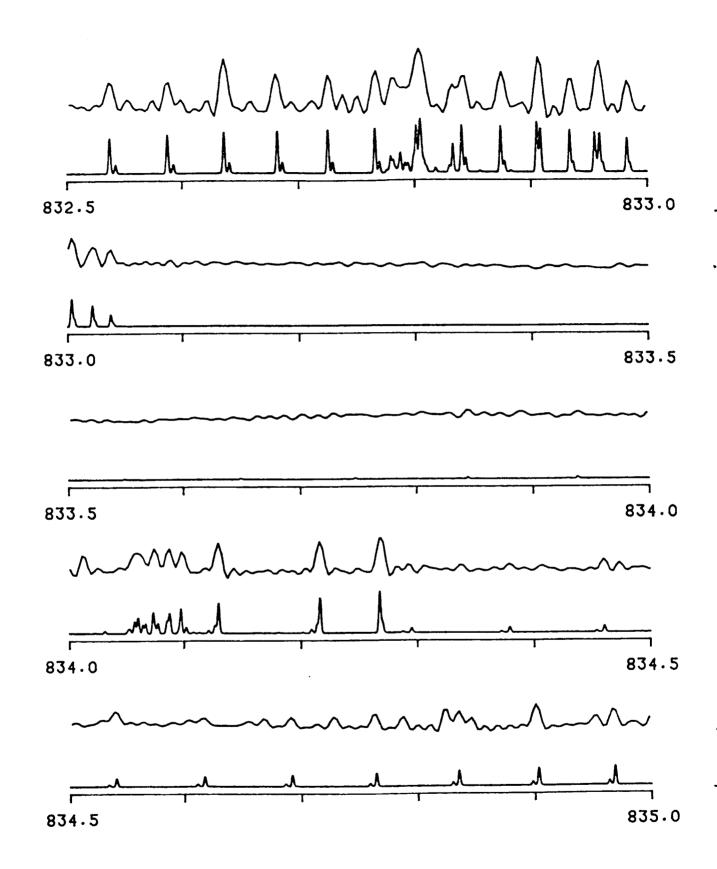


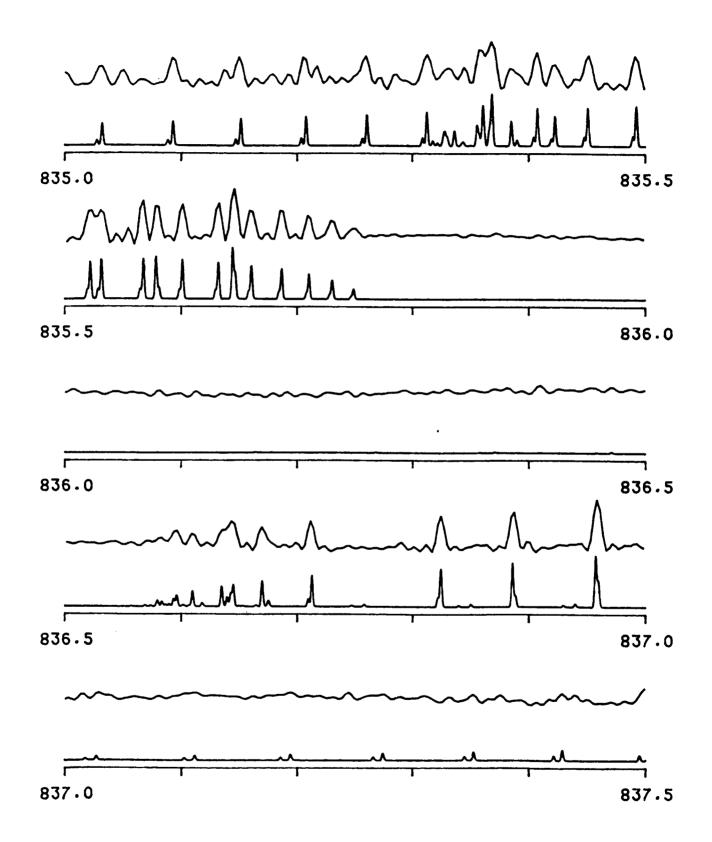


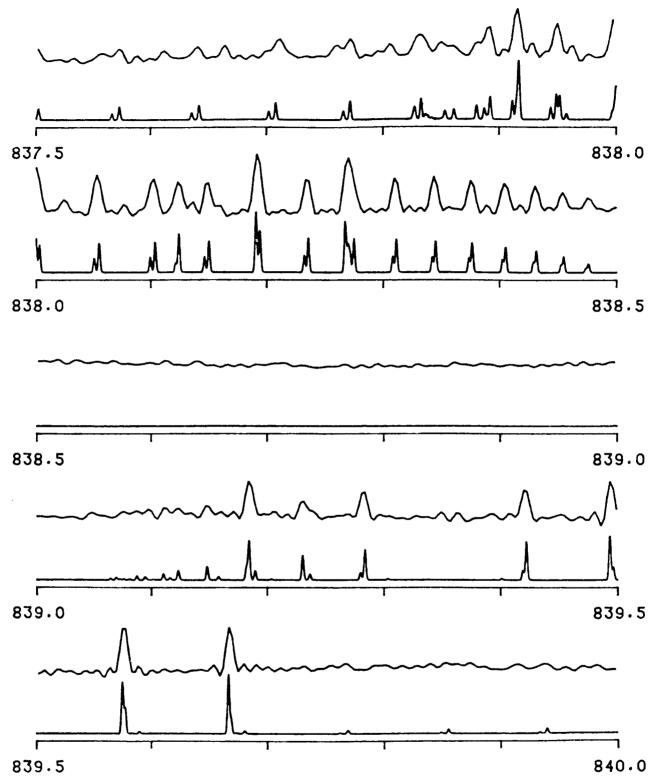




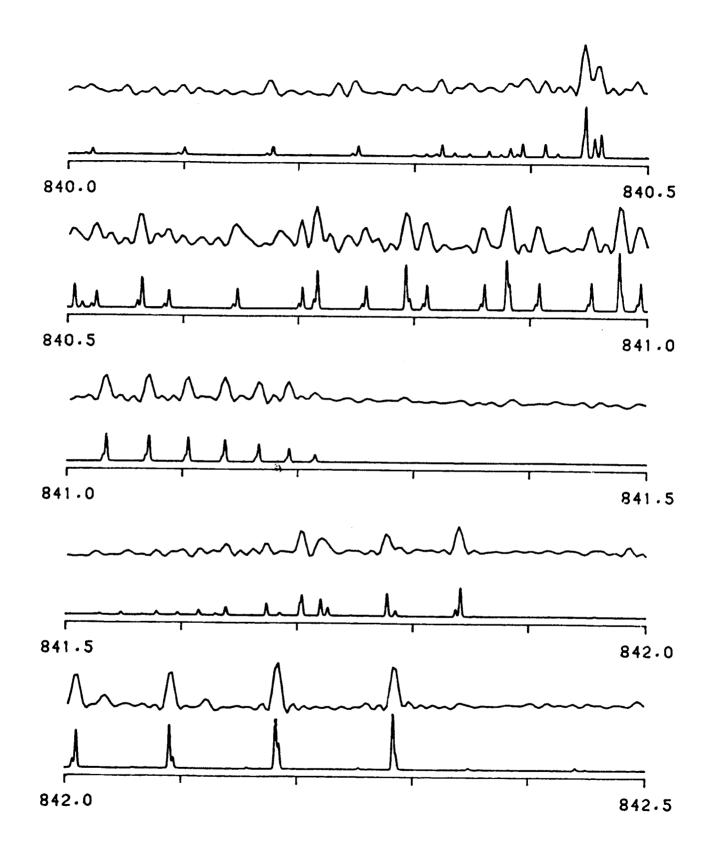




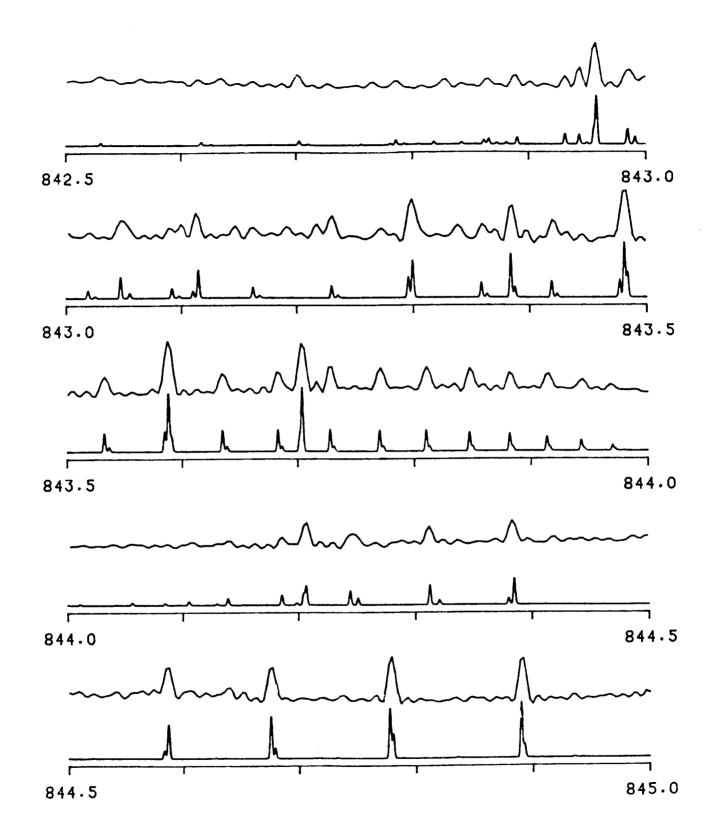


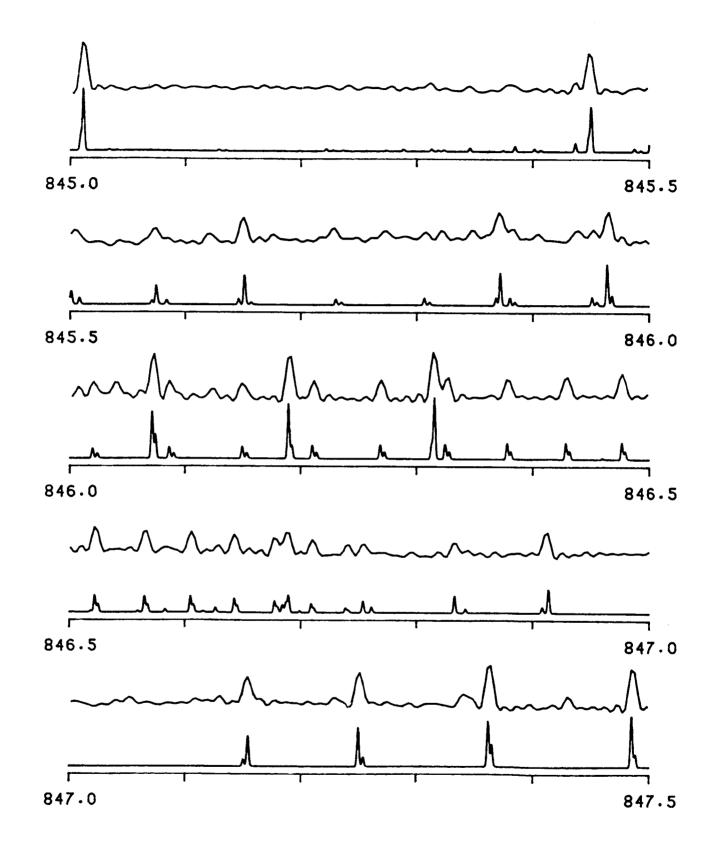






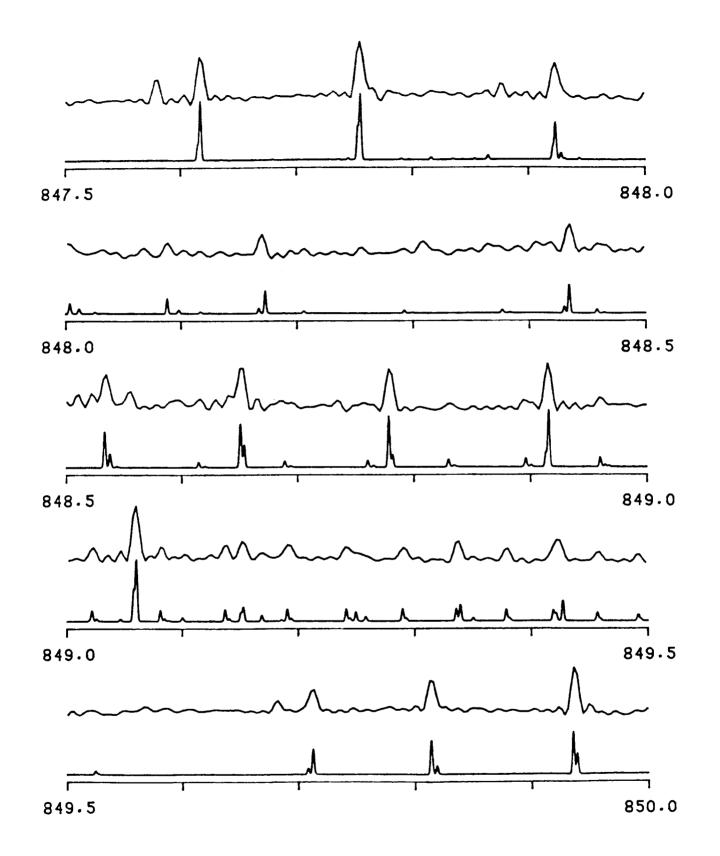
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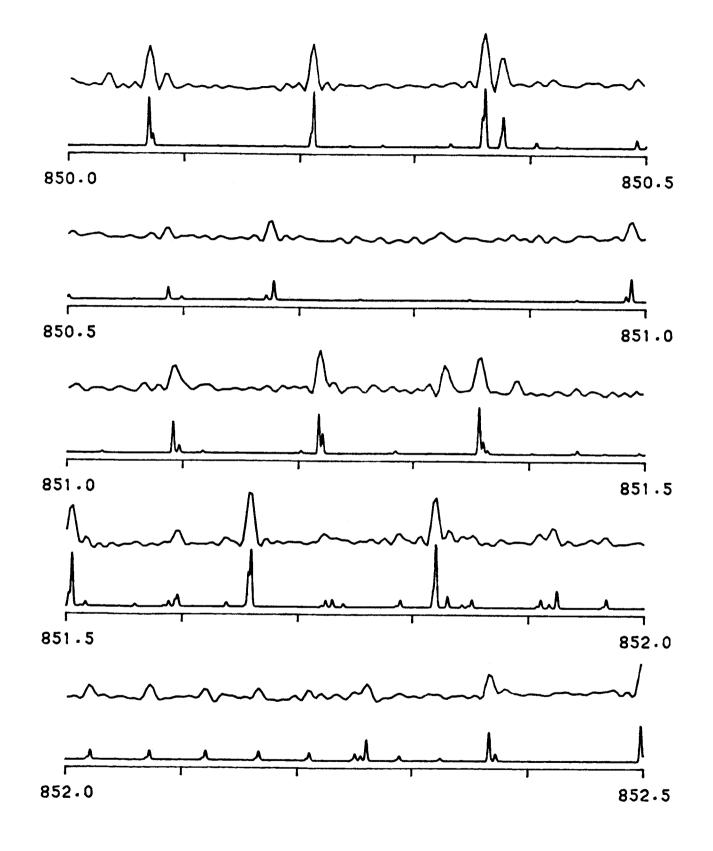


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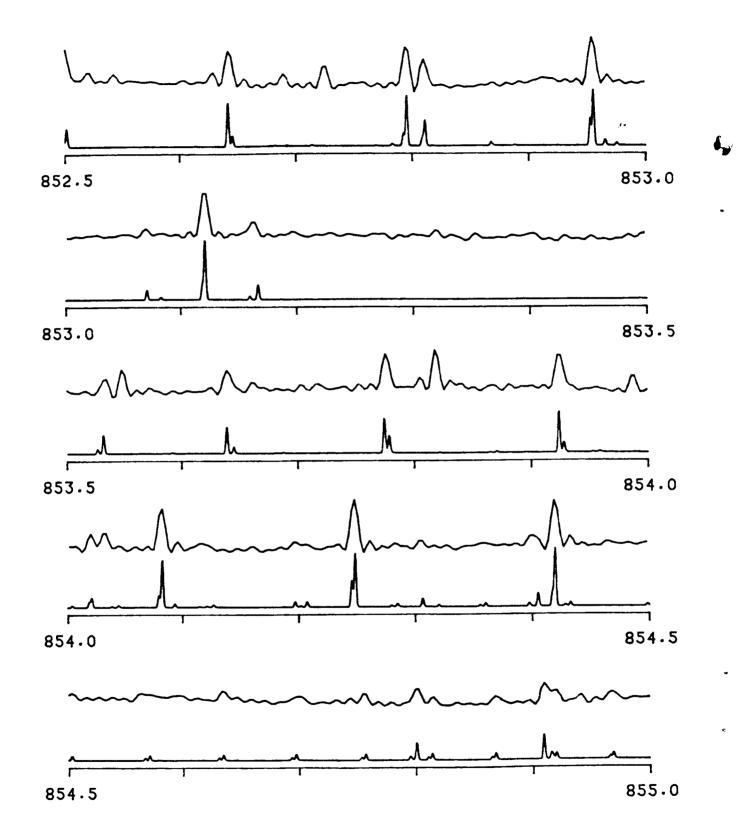
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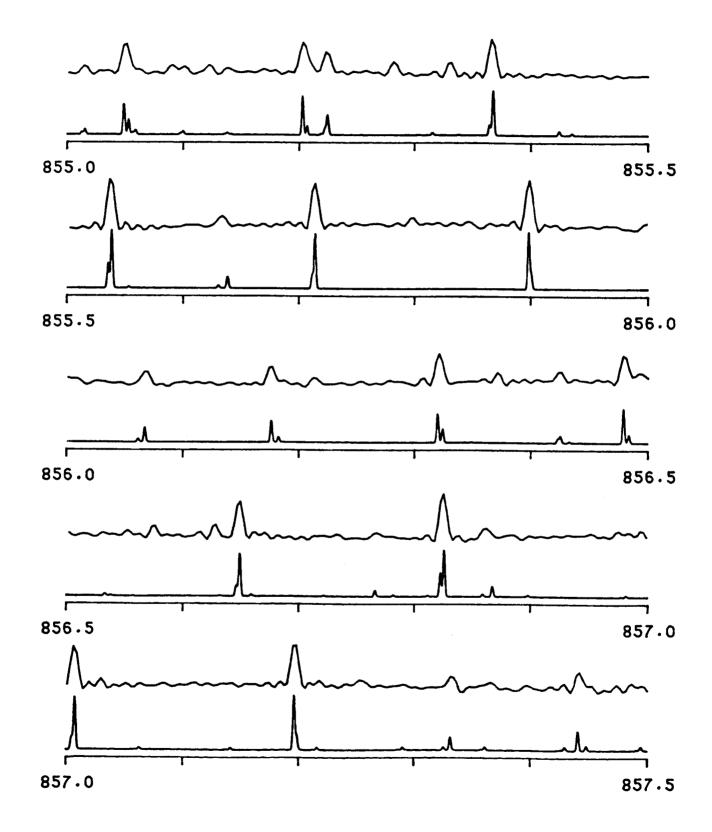




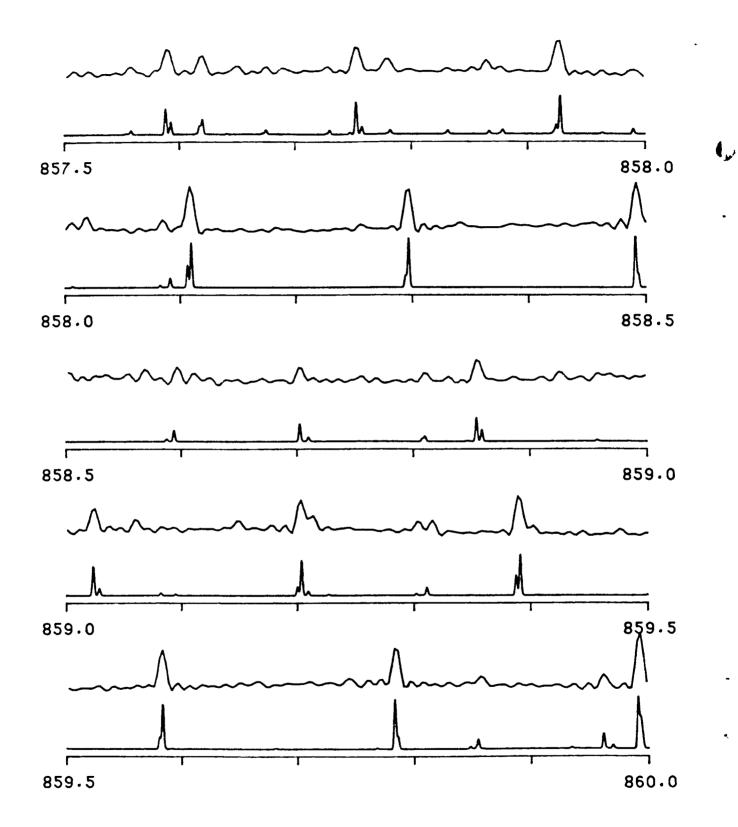


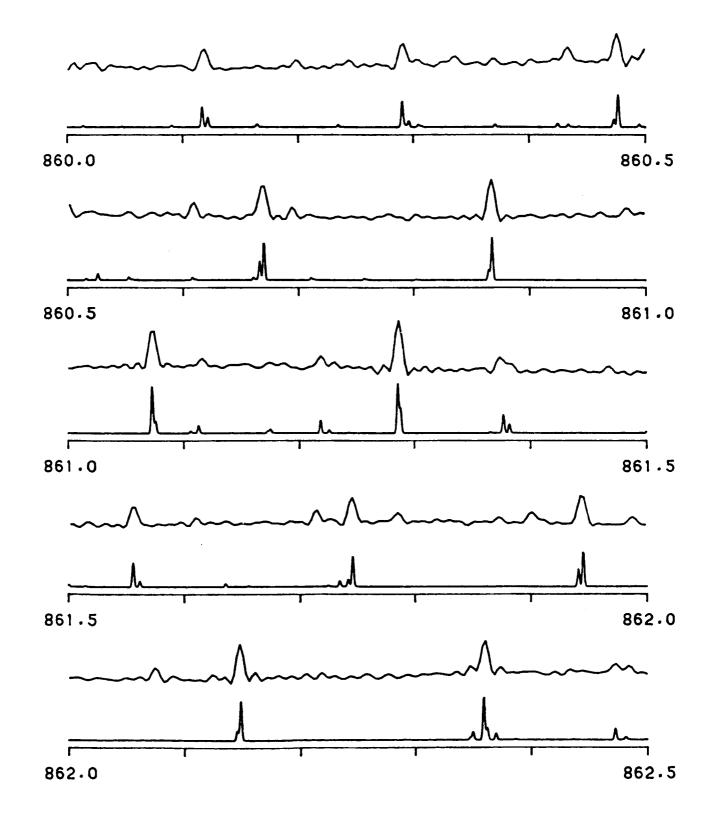
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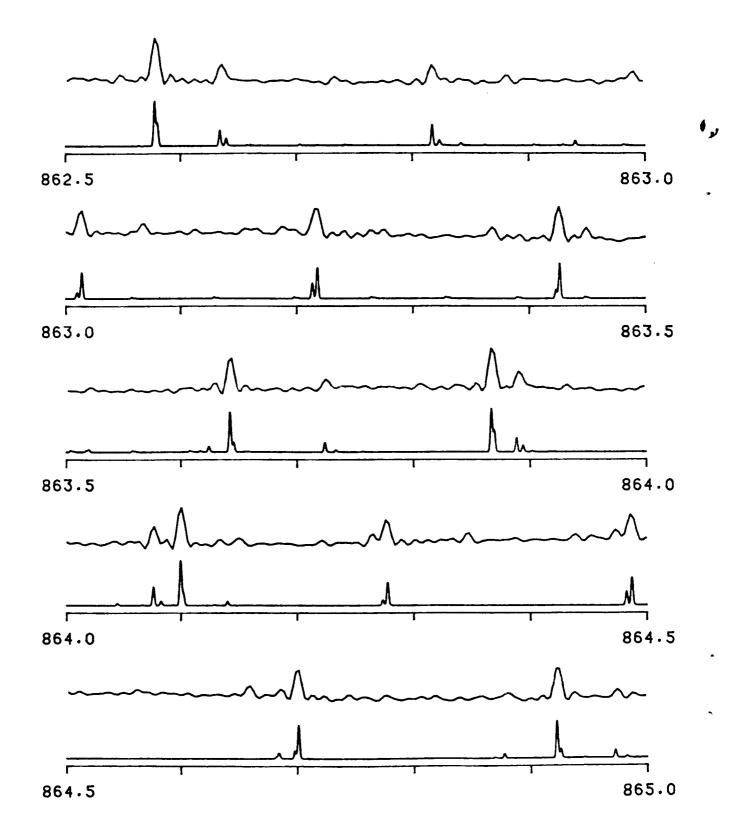
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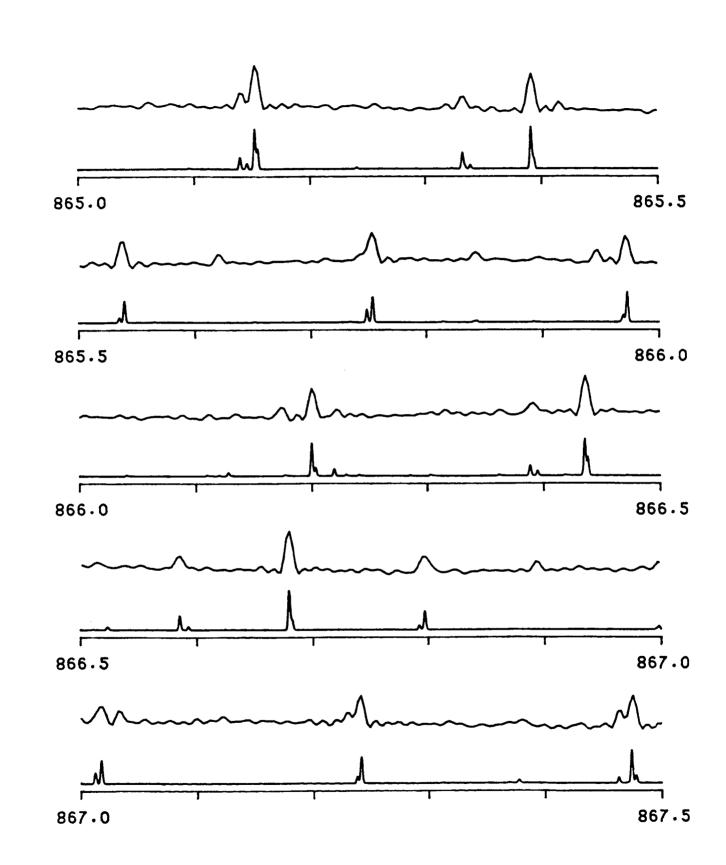


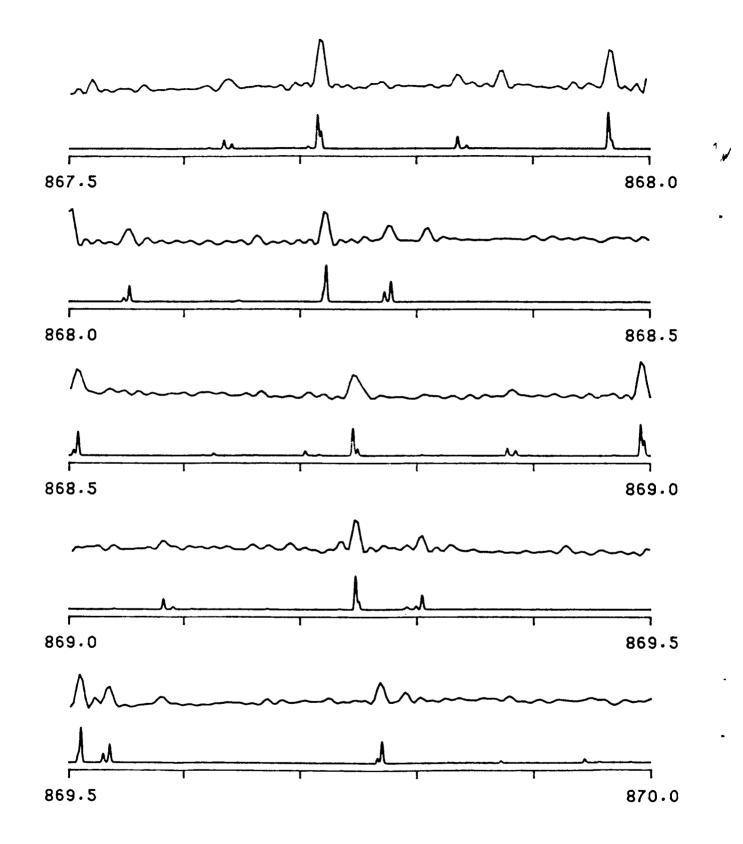


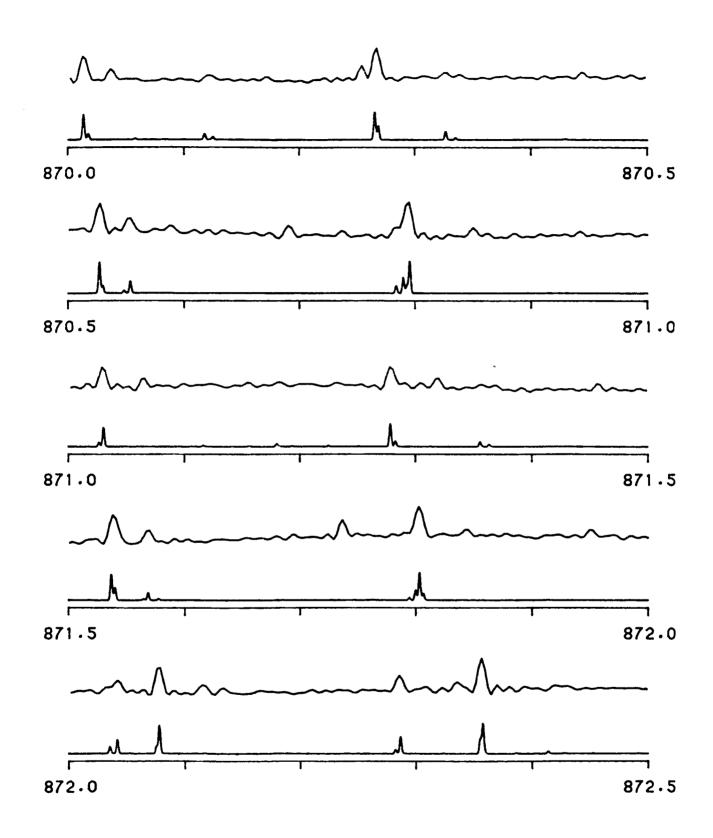
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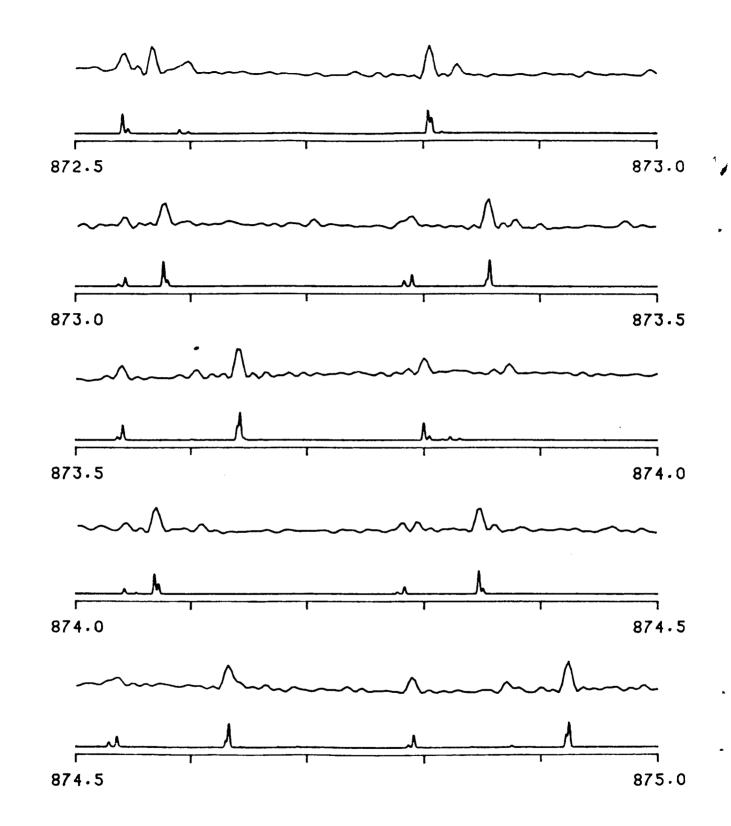


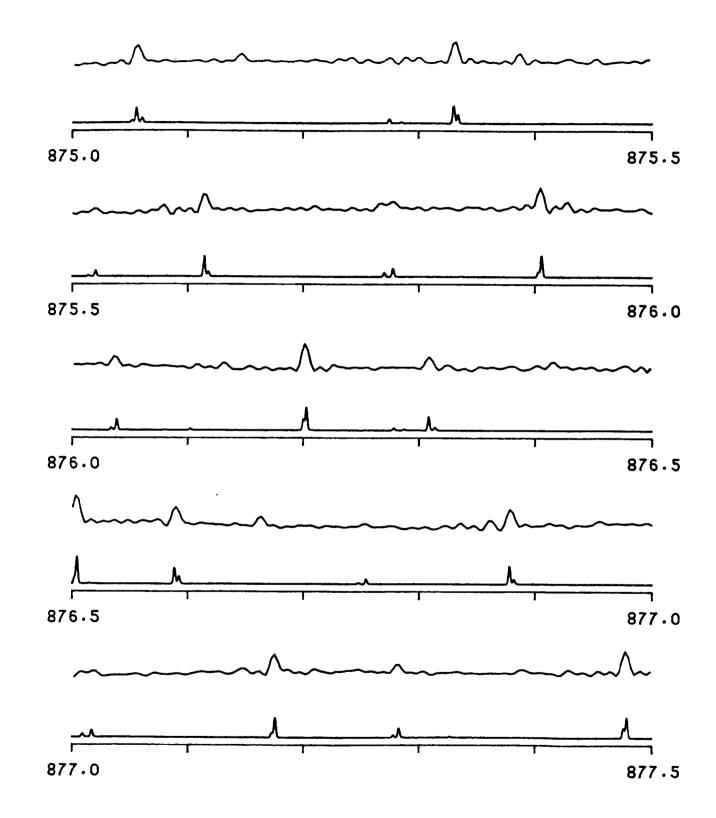




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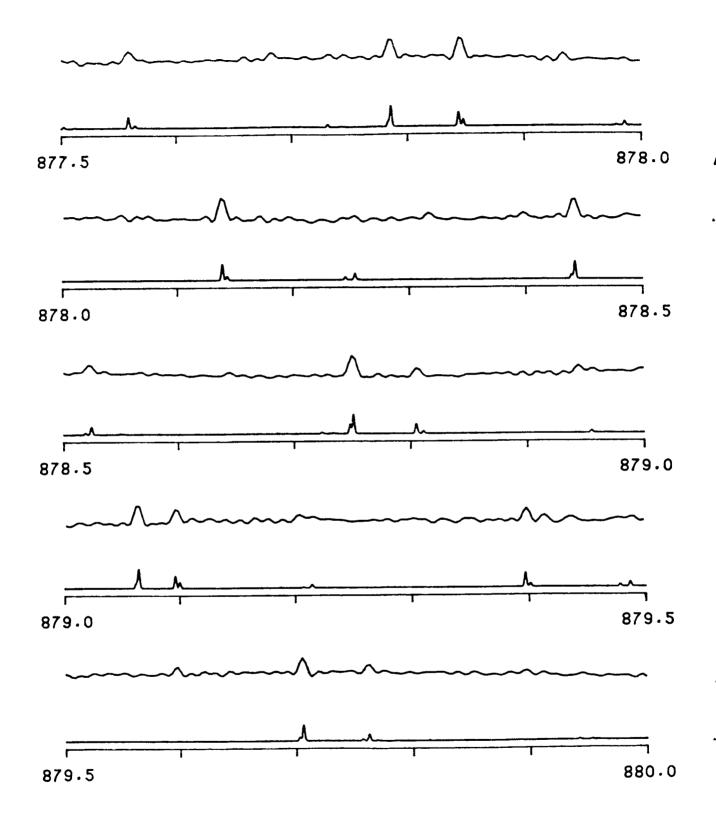


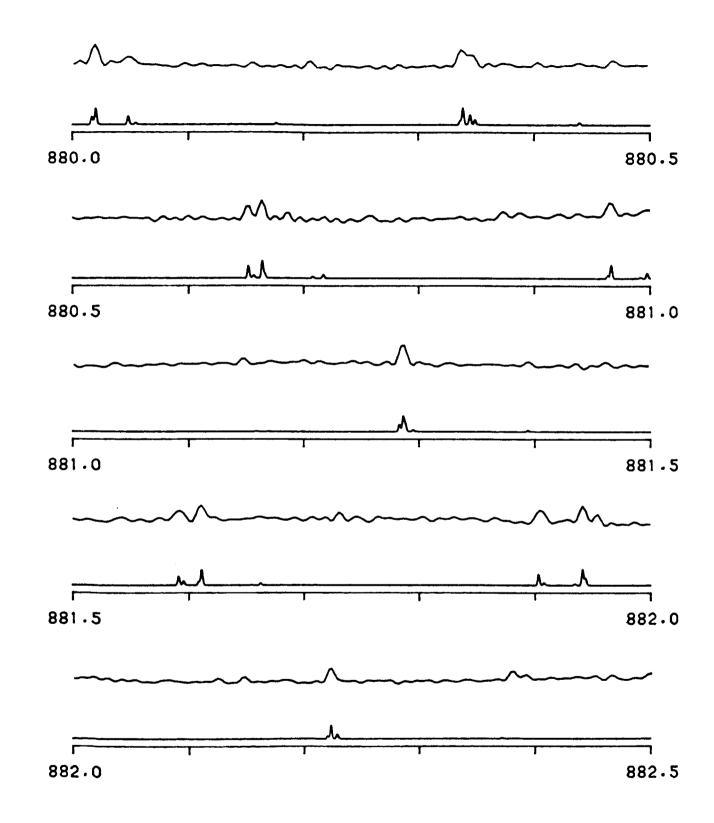


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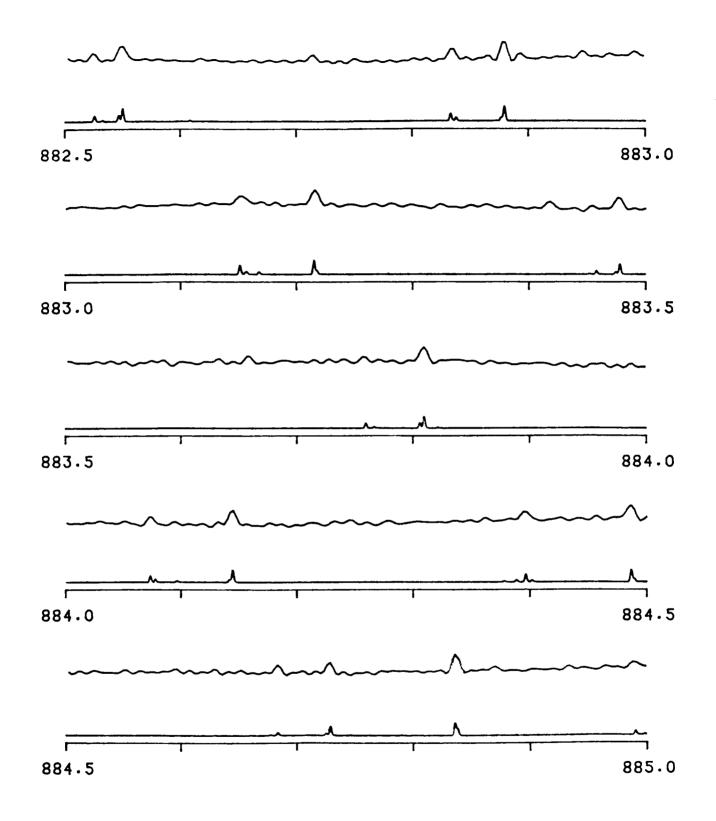


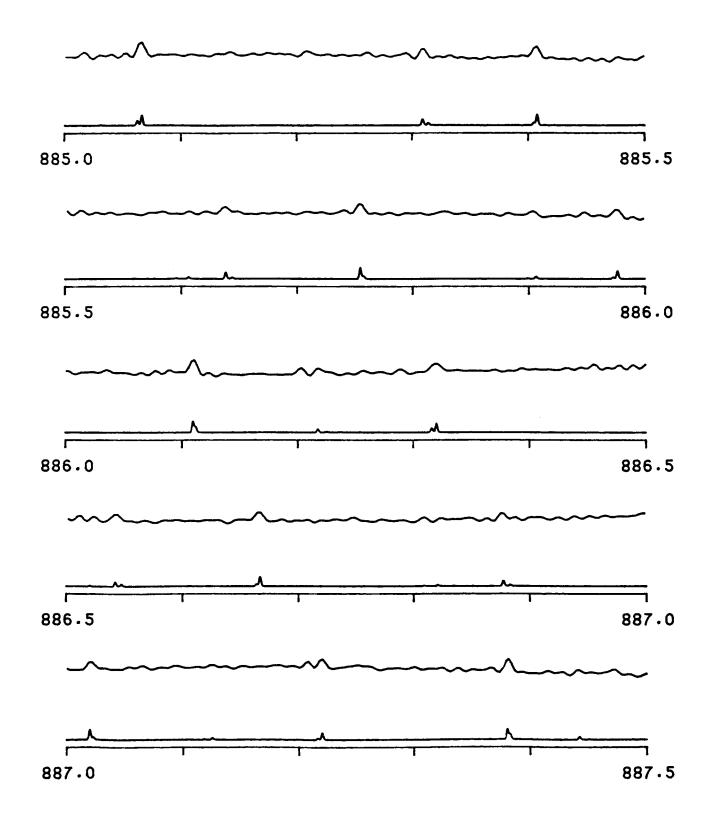


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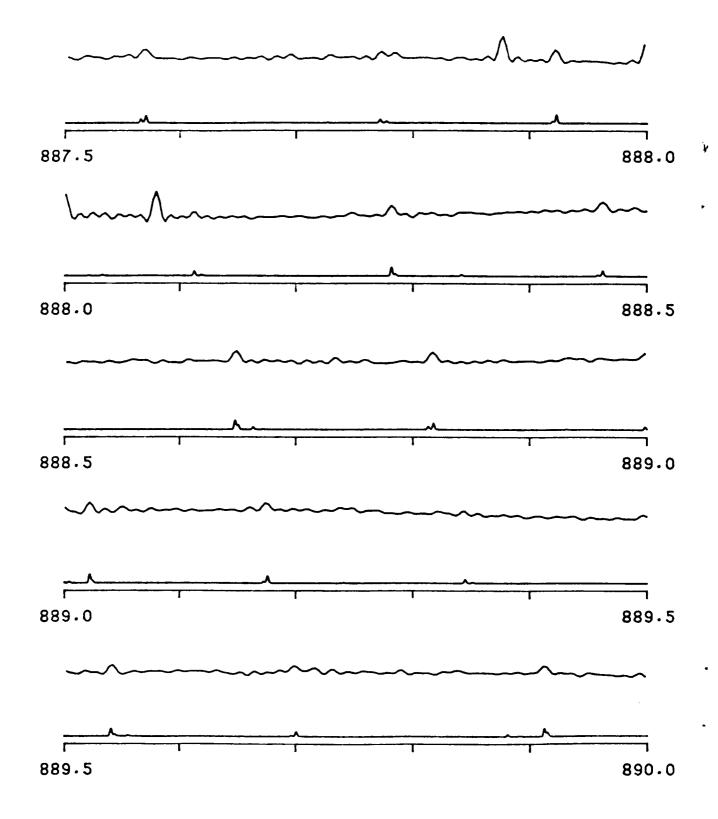
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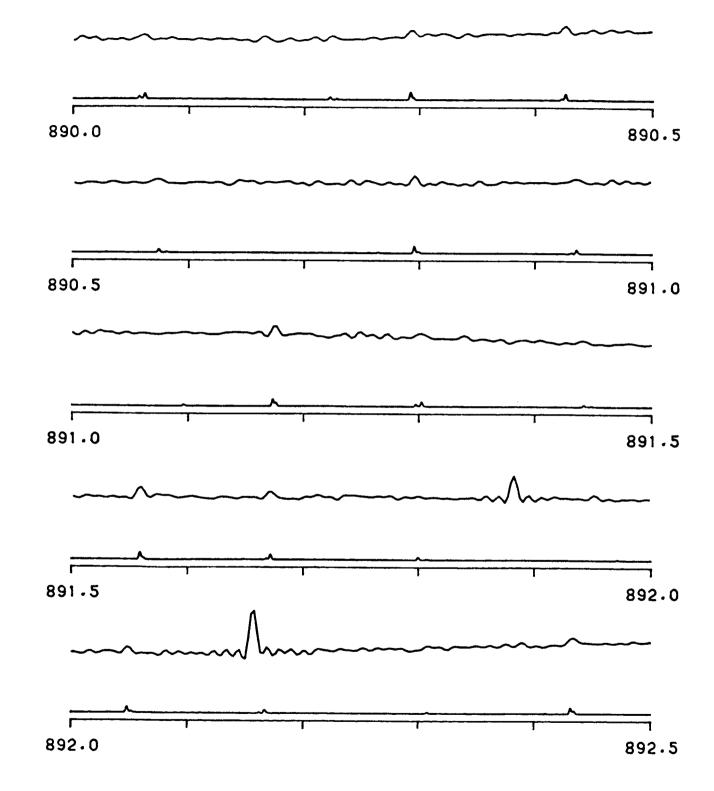
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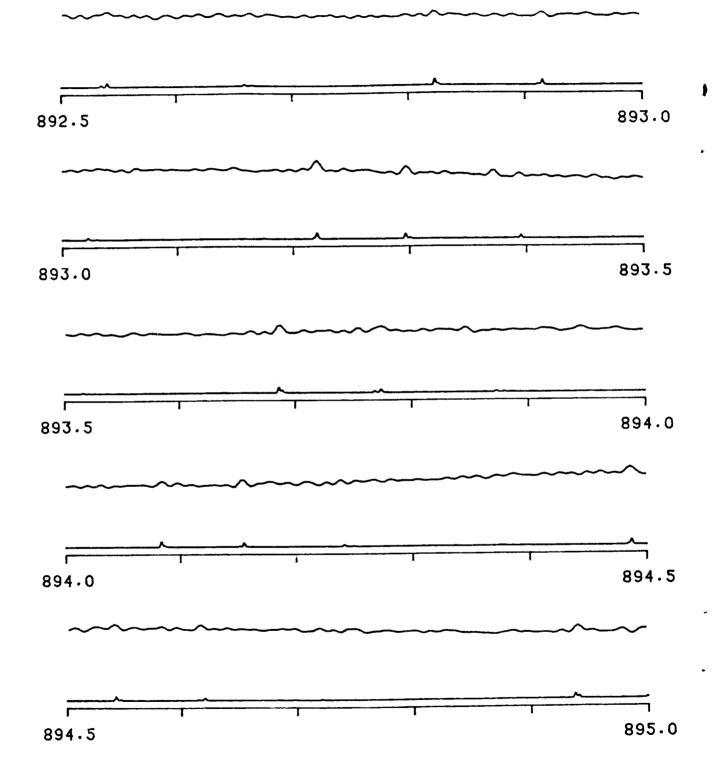
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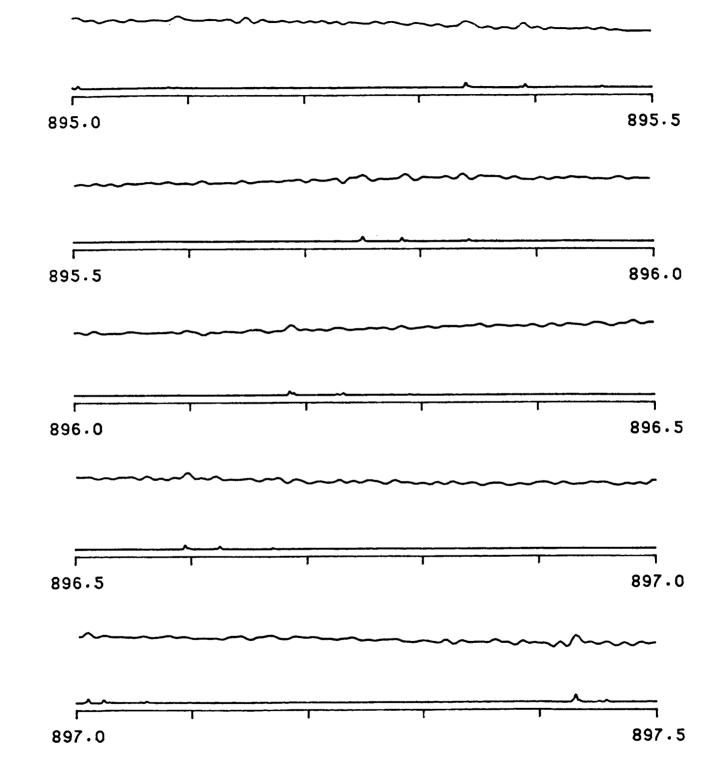




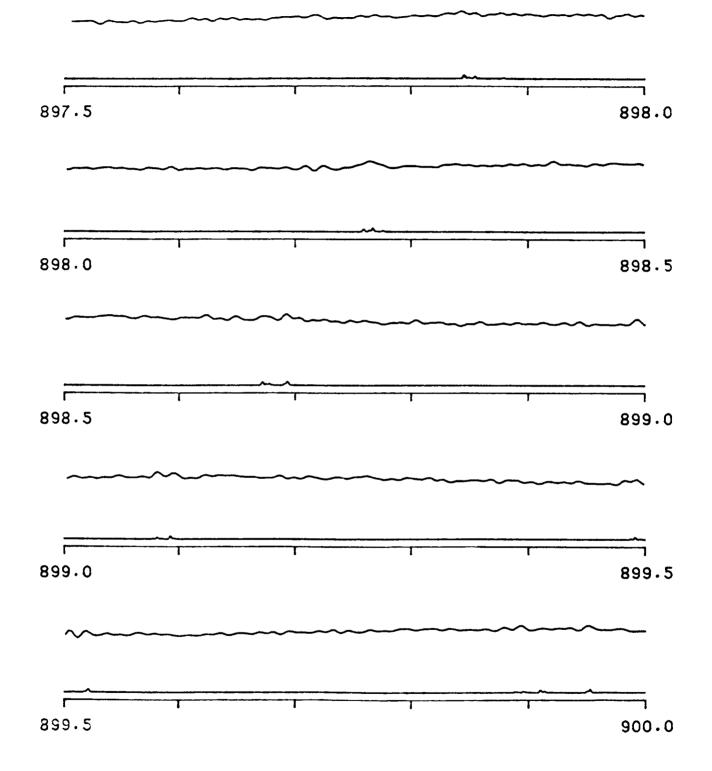
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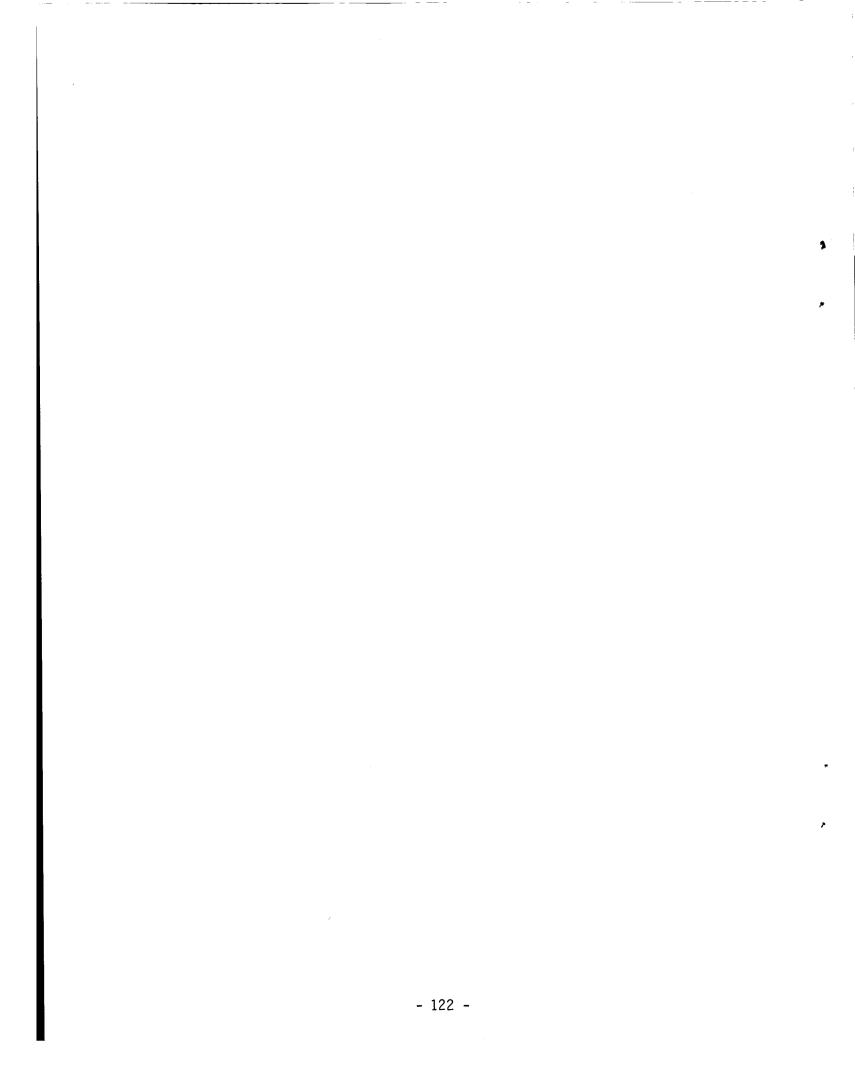
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## Table 1

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Assignment, calculated transition  $(cm^{-1})$  and calculated relative intensity from 765 cm<sup>-1</sup> to 900 cm<sup>-1</sup> for all transitions such that K < 30 and J < 50. The analysis used transitions -14 < K $\Delta$ K < +19 and J < 41. Extrapolation beyond the experimental transitions are included since some added verifications have been obtained -14 < K $\Delta$ K and since the calculated transition frequencies are probably better than any other current "guesses".



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MAVE NO	10     PP     5     26     3     77414448       24     PP     5     26     1     77415294     0       24     RP     4     43     2     77415409     0       54     PQ     19     35     1     77415409     0       56     PQ     19     35     1     77418026     0       56     PQ     19     33     3     77421110     0       14     PQ     19     34     1     7742136     0       13     PP     11     15     77422644     0       13     PP     11     15     77427264     0       00     PQ     19     32     3     77427264     0	C C C C C C C C C C C C C C C C C C C	RP       2       3       774, 48473         P       13       23       774, 50115       0         P       19       29       3       774, 50115       0         P       12       13       2       774, 50115       0         R       PP       12       13       2       774, 50115       0         R       PP       12       13       2       774, 55642       0         R       PP       12       13       2       774, 55642       0         R       PP       12       13       2       774, 55642       0         R       PP       12       13       774, 56638       0       0         PP       12       13       774, 56638       0       0       0         PP       12       13       774, 660988       0       <	H     PP     8     20     774.85744     0       8     PQ     19     23     3     774.85744     0       6     PP     2     31     2     774.85744     0       2     PP     2     31     2     774.85744     0       2     PP     2     31     2     774.88474     0       2     PQ     19     23     1     774.88873     0       2     PQ     19     23     1     774.88973     0       0     PP     2     31     0     774.899946     0       0     PP     2     31     0     774.999944     0
T K J S WAVE NO I	.00010     PP     5     3     77414448       .00474     PP     5     26     1     77415294       .00224     RP     4     43     2     77415294       .03864     PQ     19     35     1     77415294       .03864     PQ     19     35     1     77416409       .03864     PQ     19     35     1     77416409       .03864     PQ     19     35     1     77416409       .15456     PQ     19     33     77418026       .15456     PQ     19     33     77421110       .154407     RP     4     43     77421364       .15456     PQ     19     34     1       .15456     PQ     19     34     1       .15456     PQ     19     34     1       .11     15     3     77422644       .15500     PQ     19     32     3	000132 KP 3 41 3 774 30019 0 00016 PQ 19 31 774 31082 0 02480 PQ 19 31 774 3117 0 02480 PQ 19 31 3 774 3108 0 00040 PP 6 24 2 774 37144 0 00022 PQ 19 32 1 774 38480 0 00026 PP 6 24 2 774 38480 0 1744 38480 0 138452 PQ 19 30 3 774 43243 0 19968 PQ 19 31 1 774 44274 0	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	00264 PP 8 20 0 774.85744 0. 00108 PQ 19 23 3 774.86292 0. 00096 PP 2 31 2 774.88474 0. 00432 PQ 19 23 1 774.88474 0. 00320 PP 2 31 0 774.89946 0. 00320 PP 2 31 0 774.90594 0.
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ENO INT KJSWAVENO I	73.09324       0.00010       PP       5       26       774.14448       0         73.09580       0.00474       PP       5       26       774.15294       0         73.19959       0.00024       RP       4       43       774.15294       0         73.19979       0.03864       PQ       19       35       774.16409       0         73.19979       0.03864       PQ       19       35       774.17162       0         73.19920       0.45407       RP       4       43       774.18026       0         73.19920       0.45407       RP       4       33       774.21710       0         73.20140       0.00014       PQ       19       33       774.24236       0         73.20546       0.90014       PQ       19       34       174.22264       0         73.22658       0.62800       PP       11       15       374.22644       0         73.22658       0.62800       P       19       32       374.22644       0	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{c} 73.50837 \ 0.00028 \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \$	4.02435       0.00264       PP       8       20       774.85744       0         4.04012       0.00108       PQ       19       23       3       774.86292       0         4.05093       0.00096       PP       2       31       2       744.86744       0         4.05093       0.00096       PP       2       31       2       774.88474       0         4.05116       0.000432       PQ       19       23       1       774.88873       0         4.05116       0.001320       PP       2       31       774.88873       0         4.05837       0.00320       PP       2       31       774.88873       0         4.05837       0.003220       PP       2       31       774.899946       0         4.13228       0.001116       PQ       18<45
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J S WAVE NO INT K J S WAVE NO I	19       45       3       773.09324       0.00010       PP       5       6       3       774.14448       0         2       40       773.09580       0.00474       PP       5       26       1       774.15294       0         19       47       1       773.09580       0.00024       RP       4       43       774.15294       0         13       4       7       3       773.19929       0.03864       PQ       19       35       774.16409       0         12       14       2       773.19920       0.45407       RP       4       43       774.18026       0         12       14       2       773.19920       0.45407       RP       4       33       774.21710       0         13       4       1       773.20085       0.15456       PQ       19       34       174.24236       0         19       44       3       774.24236       0.00014       PQ       19       34       174.24236       0         12       14       3       774.2423       0.15456       PQ       19       11       15       374.226140         12       14       0	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$ \begin{array}{c} 3 & 773.50837 0.00028 \\ 6 & 773.55247 0.00026 \\ 7 & 773.55247 0.00064 \\ 8 & 774.50115 0 \\ 7 & 774.50544 0 \\ 7 & 774.50544 0 \\ 7 & 774.50544 0 \\ 7 & 774.50564 0 \\ 7 & 774.55642 0 \\ 7 & 774.55642 0 \\ 7 & 774.55642 0 \\ 7 & 774.55642 0 \\ 7 & 773.525266 0 \\ 7 & 773.525266 0 \\ 7 & 773.525266 0 \\ 7 & 774.55642 0 \\ 7 & 774.55642 0 \\ 7 & 774.56657 0 \\ 7 & 773.73091 0 \\ 7 & 773.73091 0 \\ 7 & 773.73091 0 \\ 7 & 773.73091 0 \\ 7 & 773.73091 0 \\ 7 & 774.60988 0 \\ 7 & 774.60988 0 \\ 7 & 774.60988 0 \\ 7 & 774.60988 0 \\ 7 & 773.73642 0 \\ 1 & 773.73642 0 \\ 1 & 773.73642 0 \\ 1 & 773.73642 0 \\ 7 & 773.73642 0 \\ 7 & 773.73642 0 \\ 7 & 773.73642 0 \\ 7 & 773.73642 0 \\ 7 & 773.73642 0 \\ 7 & 773.73642 0 \\ 7 & 774.60988 0 \\ 7 & 774.60988 0 \\ 7 & 774.60988 0 \\ 7 & 774.65679 0 \\ 7 & 774.65928 0 \\ 7 & 774.65928 0 \\ 7 & 774.65928 0 \\ 7 & 774.65928 0 \\ 7 & 774.65928 0 \\ 7 & 774.65928 0 \\ 7 & 774.75168 0 \\ 7 & 774.75168 0 \\ 7 & 774.75168 0 \\ 7 & 774.75168 0 \\ 7 & 774.7668 0 \\ 7 & 774.7668 0 \\ 7 & 774.77068 0 \\ 7 & 774.77068 0 \\ 7 & 7 & 774.84957 0 \\ 7 & 7 & 7 & 7 & 7 \\ 7 & 7 & 7 & 7 & 7$	19       37       774.02435       0.00264       PP       8       20       774.85744       0         5       45       3       774.04012       0.00108       PQ       19       23       3       774.86292       0         19       35       3       774.04012       0.00108       PQ       19       23       3       774.86292       0         19       35       3       774.05093       0.00096       PP       2       31       2       774.88474       0         5       45       1       774.05116       0.00432       PQ       19       23       1       774.88873       0         19       36       1       774.09897       0.00320       PP       2       31       0       774.89976       0         19       34       3       774.13228       0.00116       PQ       18       45       0       774.90594       0

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I ON	3       781.8857         1       781.8857         1       781.89294         0       781.89993         2       781.891.90074         2       781.91084         0       781.91084         0       781.91084         0       781.91084         0       781.91084         1       781.91084	0 781.96349 0 781.96629 3 781.97552 0 781.99046 0 781.99046	2 (81.99458 0 0 782.01506 0 3 782.02932 0 1 782.03599 0 782.03795 0	0 782.03959 0 0 782.04119 0 0 782.06408 0 1 782.07715 0	2 782.07909 0. 0 782.08810 0. 3 782.09456 0. 0 782.11169 0.	2 782, 15691 1, 2 782, 12691 1, 0 782, 12994 0, 0 782, 13446 0, 782, 15273 0, 2 782, 15273 0,	782,15938 0,0 782,16938 0,0 3 782,16938 0,0 3 782,19411 0,1 1 782,20352 0,0	3 782.21077 0. 2 782.21361 0. 0 782.22328 0. 2 782.22416 0. 2 782.22638 0.	Z 782.24780 0. 782.26089 0. 782.30735 0. 782.30735 0. 782.31640 0. 782.31640 0. 782.31640 0. 782.39493 0. 782.40088 0. 782.40088 0.	· 0 CI014.701 1
J S WAVE NO I	13       3       781.8857       1         13       1       781.8857       0         26       0       781.89993       0         21       2       781.89793       0         21       2       781.99074       0         34       0       781.91084       0         25       0       781.91084       0         24       0       781.91084       0         24       781.91084       0       281.91084         25       2       781.91084       0         25       781.91084       92056       0         24       781.9423       0       781.9423         24       781.94878       94.291       0	35 0 781.96349 0 23 0 781.96629 0 48 3 781.97552 0 22 0 781.97552 0	19 2 181.99458 0 21 0 782.01506 0 24 3 782.02532 0 24 782.03595 0	20 0 782.03959 0. 36 0 782.04119 0. 19 0 782.06408 0. 48 1 782.0715 0.	17 2 782.07909 0. 18 0 782.08810 0. 47 3 782.09456 0. 17 0 782.11169 0.	11 2 782.12691 1. 11 2 782.12691 1. 11 0 782.13994 0. 16 0 782.15273 0. 13 0 782.15273 0.	49 6 7001 1000 1000 1000 1000 1000 1000 10	46 3 782.21077 0. 22 2 782.21361 0. 22 0 782.22328 0. 29 2 782.22416 0. 29 0 782.22638 0.	45 2 782.24780 0. 45 0 782.26089 0. 45 3 782.30735 0. 43 3 782.30735 0. 44 1 782.31640 0. 44 1 2 782.31640 0. 44 1 2 782.39493 0. 44 1 0 782.39493 0. 45 1 782.40068 0. 20 3 782.40068 0.	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
J S WAVE NO I	P 9 13 3 781.88857 1 P 9 13 1 781.89204 0 0 16 26 0 781.89993 0 0 16 21 2 781.90074 0 0 16 24 0 781.91084 0 0 16 24 0 781.91084 0 0 16 24 0 781.94291 0 0 15 29 2 781.94878 0 0 15 49 1 781.94888 0 0 15 49 1 781.9488 0 0 18 49 1 8888 0 0 18 49 18 18 18 18 18 18 18 18 18 18 18 18 18	16         35         0         781.96349         0           2         16         23         0         781.96529         0           2         15         48         3         781.97552         0           2         15         48         3         781.99046         0           2         15         22         0         781.99046         0	1     1 <td>0 16 20 0 782.03959 0. 0 16 36 0 782.04119 0. 0 16 19 0 782.06408 0. 15 48 1 782.07715 0.</td> <td>a 16 17 2 782.07909 0. a 16 18 0 782.08810 0. a 15 47 3 782.09456 0. a 16 17 0 782.11169 0.</td> <td>P     10     10     2     10     11     2     10     11     2     12     12     12     12     12     12     11     1</td> <td>P 10 49 2 402.10038 0. P 10 49 2 782.16038 0. P 9 47 3 782.19411 0. P 9 47 1 782.20352 0.</td> <td>7 15 46 3 782.210// 0. P 4 22 2 782.21361 0. P 0 29 2 782.22416 0. P 0 29 0 782.22438 0.</td> <td>8     45     2     782.24/80     0.       8     45     0     782.26089     0.       15     46     1     782.30175     0.       15     46     1     782.30175     0.       15     46     1     782.30175     0.       15     45     3     782.30175     0.       16     183     3     782.30175     0.       15     45     3     782.31640     0.       15     45     3     782.32414     0.       15     45     3     782.39493     0.       15     41     782.39493     0.       16     41     782.39493     0.       17     10     782.39493     0.       18     782.39493     0.     0.       17     782.340088     0.     0.       18     782.400688     0.     0.       19     782.400688     0.     0.</td> <td>0 C1014:201 1 CH C1 X</td>	0 16 20 0 782.03959 0. 0 16 36 0 782.04119 0. 0 16 19 0 782.06408 0. 15 48 1 782.07715 0.	a 16 17 2 782.07909 0. a 16 18 0 782.08810 0. a 15 47 3 782.09456 0. a 16 17 0 782.11169 0.	P     10     10     2     10     11     2     10     11     2     12     12     12     12     12     12     11     1	P 10 49 2 402.10038 0. P 10 49 2 782.16038 0. P 9 47 3 782.19411 0. P 9 47 1 782.20352 0.	7 15 46 3 782.210// 0. P 4 22 2 782.21361 0. P 0 29 2 782.22416 0. P 0 29 0 782.22438 0.	8     45     2     782.24/80     0.       8     45     0     782.26089     0.       15     46     1     782.30175     0.       15     46     1     782.30175     0.       15     46     1     782.30175     0.       15     45     3     782.30175     0.       16     183     3     782.30175     0.       15     45     3     782.31640     0.       15     45     3     782.32414     0.       15     45     3     782.39493     0.       15     41     782.39493     0.       16     41     782.39493     0.       17     10     782.39493     0.       18     782.39493     0.     0.       17     782.340088     0.     0.       18     782.400688     0.     0.       19     782.400688     0.     0.	0 C1014:201 1 CH C1 X
J S WAVE NO I	P 9 13 3 781.88857 1 P 9 13 1 781.89204 0 0 16 26 0 781.89993 0 0 16 21 2 781.90074 0 0 16 24 0 781.91084 0 0 16 24 0 781.91084 0 0 16 24 0 781.94291 0 0 15 29 2 781.94878 0 0 15 49 1 781.94888 0 0 15 49 1 781.9488 0 0 18 49 1 8888 0 0 18 49 18 18 18 18 18 18 18 18 18 18 18 18 18	16         35         0         781.96349         0           2         16         23         0         781.96529         0           2         15         48         3         781.97552         0           2         15         48         3         781.99046         0           2         15         22         0         781.99046         0	1     1 <td>0 16 20 0 782.03959 0. 0 16 36 0 782.04119 0. 0 16 19 0 782.06408 0. 15 48 1 782.07715 0.</td> <td>a 16 17 2 782.07909 0. a 16 18 0 782.08810 0. a 15 47 3 782.09456 0. a 16 17 0 782.11169 0.</td> <td>P     10     10     2     10     11     2     10     11     2     12     12     12     12     12     12     11     1</td> <td>P 10 49 2 402.10038 0. P 10 49 2 782.16038 0. P 9 47 3 782.19411 0. P 9 47 1 782.20352 0.</td> <td>7 15 46 3 782.210// 0. P 4 22 2 782.21361 0. P 0 29 2 782.22416 0. P 0 29 0 782.22438 0.</td> <td>45 2 782.24780 0. 45 0 782.26089 0. 45 3 782.30735 0. 43 3 782.30735 0. 44 1 782.31640 0. 44 1 2 782.31640 0. 44 1 2 782.39493 0. 44 1 0 782.39493 0. 45 1 782.40068 0. 20 3 782.40068 0.</td> <td>0 C1014:201 1 CH C1 X</td>	0 16 20 0 782.03959 0. 0 16 36 0 782.04119 0. 0 16 19 0 782.06408 0. 15 48 1 782.07715 0.	a 16 17 2 782.07909 0. a 16 18 0 782.08810 0. a 15 47 3 782.09456 0. a 16 17 0 782.11169 0.	P     10     10     2     10     11     2     10     11     2     12     12     12     12     12     12     11     1	P 10 49 2 402.10038 0. P 10 49 2 782.16038 0. P 9 47 3 782.19411 0. P 9 47 1 782.20352 0.	7 15 46 3 782.210// 0. P 4 22 2 782.21361 0. P 0 29 2 782.22416 0. P 0 29 0 782.22438 0.	45 2 782.24780 0. 45 0 782.26089 0. 45 3 782.30735 0. 43 3 782.30735 0. 44 1 782.31640 0. 44 1 2 782.31640 0. 44 1 2 782.39493 0. 44 1 0 782.39493 0. 45 1 782.40068 0. 20 3 782.40068 0.	0 C1014:201 1 CH C1 X
J S WAVE NO I	0.00200 PP 9 13 3 781.88857 1 0.71328 PP 9 13 1 781.89294 0 0.17832 PQ 16 26 0 781.89993 0 0.0050 PQ 16 21 2 781.90074 0 0.00984 PQ 16 24 0 781.91084 0 0.00106 PQ 16 24 0 781.91084 0 0.00424 PQ 16 24 0 781.94291 0 0.00423 PQ 15 24 0 781.94873 0 0.00413 PQ 15 49 1 781.94873 0	0.00827 Pq 16 35 0 781.96349 0 0.21896 Pq 16 23 0 781.96629 0 0.87584 Pq 15 48 3 781.95629 0 0.01448 Pq 15 22 0 781.99046 0	0.00390 Pq 16 19 2 (81.99458 0) 0.01560 Pq 16 21 0 782.01506 0) 0.01728 PP 3 24 3 782.03599 0) 0.02792 PP 3 24 1 782.03599 0)	0.02040 PQ 16 20 0 782.03959 0. 0.51947 PQ 16 36 0 782.04119 0. 1.03893 PQ 16 19 0 782.06408 0. 0.04720 PQ 15 48 1 782.07715 0.	0.02360 PQ 16 17 2 782.07909 0. 0.02392 PQ 16 18 0 782.08810 0. 0.02784 PQ 15 47 3 782.09456 0. 0.07416 PQ 16 17 0 782.11169 0.	0.01624 Fu 10 10 2 102.11177 0 0.03192 PP 10 11 2 782.12694 0 0.29750 PP 10 11 0 782.12994 0 1.19000 PQ 16 16 0 782.15273 0 0.03632 PQ 16 37 782.15273 0	0.024050 NP 10 49 2 702.12290 0 0.028462 NP 10 49 2 782.15038 0 0.094520 NP 9 47 3 782.190411 0 0.04520 NP 9 47 1 782.20352 0	0.40328 PQ 15 46 3 782.210// 0. 1.31816 PP 4 22 2 782.21361 0. 0.04944 RP 0 29 2 782.22416 0. 0.05328 RP 0 29 0 782.22638 0.	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	
T K J S WAVE NO I	535       0.00200       PP       9       13       781.8857       1         796       0.71328       PP       9       13       781.8857       1         839       0.71328       PQ       16       26       781.89993       0         839       0.17832       PQ       16       26       781.89993       0         899       0.00050       PQ       16       26       781.90074       0         858       0.000984       PQ       16       21       781.91084       0         858       0.00984       PQ       16       24       781.91084       0         828       0.00106       PQ       16       25       781.91084       0         771       0.00424       PQ       16       26       781.94291       0         771       0.00424       PQ       15       271.94278       0       693       0         783       0.01200       PQ       15       2781.94678       0       60783       0	022 0.00827 PQ 16 35 0 781.96349 0 001 0.21896 PQ 16 23 0 781.96629 0 616 0.87584 PQ 15 48 3 781.97552 0 428 0.01448 PQ 16 22 0 781.99046 0	21/ 0.00390 Pq 16 19 2 /81.99458 0 121 0.01560 Pq 16 21 0 782.01506 0 435 0.01728 PP 3 24 1 782.03599 0 389 0.02792 PP 3 24 1 782.03599 0 577 0.06688 PD 16 18 2 03795 0	181         0.02040         PQ         16         20         782.03959         0.           282         0.51947         PQ         16         36         782.04119         0.           171         1.03893         PQ         16         19         782.06408         0.           496         0.04720         PQ         15         48         1         782.07715         0.	355 0.02360 Pq 16 17 2 782.07909 0. 683 0.02392 Pq 16 18 0 782.08810 0. 925 0.02784 Pq 15 47 3 782.09456 0. 975 0.07416 Pq 15 17 0 782.11169 0.	923     0.03192     PP     10     10     2     102 <td>102     0.04000     KF     10     49     2     102110238     0       617     0.02462     RP     15     47     1     782.16978     0       422     0.094520     RP     9     47     1     782.199411     0       423     0.04520     RP     9     47     1     782.199411     0       6448     0.10082     RP     9     47     1     782.20352     0</td> <td>391 0.40328 PQ 15 46 3 782.210// 0. 147 1.31816 PP 4 22 2 782.21361 0. 431 0.31994 PP 4 22 2 782.22361 0. 430 0.04944 PP 0 29 2 782.22476 0. 206 0.05328 PP 0 29 0 782.22638 0.</td> <td>728 0.05632 RP 8 45 2 782.24780 0.835 0.00596 RP 8 45 0 782.26089 0.846 0.49880 PQ 15 46 1 782.26089 0.963 0.17 0.05938 PQ 15 46 1 782.30733 0.973 0.973 0.0593 PQ 15 45 3 782.3073 0.973 0.978 PQ 15 45 3 782.37414 0.772 0.00798 PQ 15 45 3 782.39493 0.727 0.00432 PP 5 20 3 782.40668 0.557 0.00432 PP 5 20 3 782.40662 0.5577 0.557 0.557 0.557 0.557 0.557 0.5577 0.557 0.557 0.5577 0.557 0.5577 0.5577 0.557</td> <td>140 0.01020 1 (4 (1 M) 07010.0</td>	102     0.04000     KF     10     49     2     102110238     0       617     0.02462     RP     15     47     1     782.16978     0       422     0.094520     RP     9     47     1     782.199411     0       423     0.04520     RP     9     47     1     782.199411     0       6448     0.10082     RP     9     47     1     782.20352     0	391 0.40328 PQ 15 46 3 782.210// 0. 147 1.31816 PP 4 22 2 782.21361 0. 431 0.31994 PP 4 22 2 782.22361 0. 430 0.04944 PP 0 29 2 782.22476 0. 206 0.05328 PP 0 29 0 782.22638 0.	728 0.05632 RP 8 45 2 782.24780 0.835 0.00596 RP 8 45 0 782.26089 0.846 0.49880 PQ 15 46 1 782.26089 0.963 0.17 0.05938 PQ 15 46 1 782.30733 0.973 0.973 0.0593 PQ 15 45 3 782.3073 0.973 0.978 PQ 15 45 3 782.37414 0.772 0.00798 PQ 15 45 3 782.39493 0.727 0.00432 PP 5 20 3 782.40668 0.557 0.00432 PP 5 20 3 782.40662 0.5577 0.557 0.557 0.557 0.557 0.557 0.5577 0.557 0.557 0.5577 0.557 0.5577 0.5577 0.557	140 0.01020 1 (4 (1 M) 07010.0
ENO INT KJSWAVENO I	.83535       0.00200       PP       9       13       781.88557       1         .83796       0.71328       PP       9       13       781.88557       1         .83796       0.71328       PP       9       13       781.8857       1         .84899       0.17832       PQ       16       26       781.89993       0         .84899       0.00050       PQ       16       21       2       781.99074       0         .88658       0.00984       PQ       16       21       2       781.91084       0         .89828       0.00984       PQ       16       24       781.91084       0         .89828       0.00126       PQ       16       25       781.92084       0         .99771       0.00424       PQ       16       24       781.94039       0         .97169       0.01200       PQ       15       271.94037       0       <	.99022 0.00827 PQ 16 35 0 781.96349 0 .03001 0.21896 PQ 16 23 0 781.96629 0 .03616 0.87584 PQ 15 48 3 781.97552 0 .05428 0.01448 PQ 16 22 0 781.99046 0	.0621/ 0.00390 Pq 16 19 2 /81.99458 0 .07121 0.01560 Pq 16 21 0 782.01506 0 .13435 0.01728 PP 3 24 3 782.02932 0 .15389 0.02792 PP 3 24 1 782.03599 0 .1577 0.00698 P0 16 18 2 782 03795 0	21181 0.02040 PQ 16 20 0 782.03959 0. 23282 0.51947 PQ 16 36 0 782.04119 0. 24171 1.03893 PQ 16 19 0 782.06408 0. 27496 0.04720 PQ 15 48 1 782.07715 0.	.28355 0.02360 PQ 16 17 2 782.07909 0. .28683 0.02392 PQ 16 18 0 782.08810 0. .35925 0.02784 PQ 15 47 3 782.09456 0. .40975 0.07416 PQ 16 17 0 782.11169 0.	.42210 0.01004 FY 10 10 2 102.11119 0. 42223 0.03192 PP 10 11 2 782.12694 0. 444132 0.29750 PP 10 11 0 782.12994 0. 44630 1.19000 PQ 16 16 0 782.15273 0. 49669 0.03632 PQ 16 37 782.15273 0.	.20102 0.04000 NF 10 49 2 702.12290 0. .59457 0.028462 PQ 15 47 1 782.19678 0. .62423 0.04520 RP 9 47 3 782.19411 0. .63648 0.10082 RP 9 47 1 782.20352 0.	.64391 0.40328 PQ 15 46 3 782.210// 0. .66147 1.31816 PP 4 22 2 782.21361 0. .68430 0.04944 RP 0 29 2 782.22416 0. .74206 0.05328 RP 0 29 0 782.22638 0.	79728 0.05632 RP 8 45 2 782.24780 0. 84835 0.00696 RP 8 45 0 782.26089 0. 84946 0.49880 PQ 15 46 1 782.30775 0. 85017 0.05932 PQ 15 45 3 782.30733 0. 85473 0.00533 RP 7 43 1 782.30733 0. 85473 0.00598 PQ 15 45 3 782.37640 0. 85547 0.00510 RP 6 41 2 782.39493 0. 85617 0.00908 PP 5 20 3 782.40088 0. 87697 0.00432 PP 5 20 3 782.40068 0. 87697 0.00432 PP 5 20 3 782.40068 0. 87697 0.00432 PP 5 20 3 782.40068 0.	00140 0.01020 1 (4 (1 NJ 07010.0 04100)
NO INT KJSWAVENO I	80.83535       0.00200       PP       9       13       781.88557       1         80.83796       0.71328       PP       9       13       781.88557       1         80.83796       0.71328       PP       9       13       781.88557       1         80.84839       0.17832       PQ       16       26       0       781.89993       0         80.84899       0.00050       PQ       16       26       0       781.99074       0         80.88658       0.000984       PQ       16       21       2       781.91084       0         80.88658       0.00106       PQ       16       24       781.91084       0         80.9771       0.00126       PQ       16       27       781.94291       0         80.9771       0.00424       PQ       16       20       781.94291       0         80.977169       0.01200       PQ       15       49       1781.94033       0	80.99022 0.00827 PQ 16 35 0 781.96349 0 81.03001 0.21896 PQ 16 23 0 781.96629 0 81.03616 0.87584 PQ 15 48 3 781.97552 0 81.05428 0.01448 PQ 16 22 0 781.99046 0	B1.06217 0.00390 Pq 16 19 2 781.99458 0 B1.07121 0.01560 Pq 16 21 0 782.01506 0 B1.13435 0.01728 PP 3 24 1 782.02932 0 B1.16389 0.02792 PP 3 24 1 782.03599 0 B1.17677 0.00698 P0 16 18 2 782.03795 0	81.21181 0.02040 PQ 16 20 0 782.03959 0. 81.23282 0.51947 PQ 16 36 0 782.04119 0. 81.24171 1.03893 PQ 16 19 0 782.06408 0. 81.27496 0.04720 PQ 15 48 1 782.07715 0.	81.28355       0.02360       Pq       16       17       2       782.07909       0.         81.28683       0.02392       Pq       16       18       0       782.08810       0.         81.35925       0.02784       Pq       15       47       3       782.09456       0.         81.40975       0.07416       Pq       15       17       0       782.11169       0.	B1.42210 0.01034 FU 10 10 2 762.11779 0. B1.42923 0.03192 PP 10 11 2 782.12691 1. B1.44630 1.19000 PQ 16 16 0 782.15294 0. B1.49669 0.03632 PQ 16 37 0 782.15273 0. B1.49669 0.003632 PQ 16 37 0 782.15273 0.	B1.50102 U.04000 RF 10 49 2 702.15330 U B1.59427 0.02462 RP 9 47 1 782.15936 0. B1.62423 0.04520 RP 9 47 3 782.19411 0. B1.63648 0.10082 RP 9 47 1 782.20352 0.	B1.64391 0.40328 PQ 15 46 3 782.210// 0. B1.66147 1.31816 PP 4 22 2 782.21361 0. B1.66430 0.04944 RP 0 29 2 782.22416 0. B1.74206 0.05328 RP 0 29 0 782.22638 0.	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1.00140 0.01020 1 CH CI NJ 07010.00 04100.10
ENO INT KJSWAVENO I	2       780.83535       0.00200       PP       9       13       781.88557       1         2       780.83796       0.71328       PP       9       13       781.88557       1         0       780.84839       0.17832       PQ       16       26       0       781.89993       0         0       780.84839       0.17832       PQ       16       26       0       781.89993       0         0       780.84899       0.00050       PQ       16       21       271.90074       0         2       780.88658       0.00984       PQ       16       24       781.91084       0         3       780.89828       0.00106       PQ       16       24       781.92056       0         1       780.99771       0.00424       PQ       16       24       781.94291       0         2       780.977159       0.00424       PQ       15       49       1781.94231       0	0     780.99022     0.00827     Pq     16     35     0     781.96349     0       3     781.03001     0.21896     Pq     16     23     0     781.96629     0       1     781.03616     0.87584     Pq     15     48     3     781.97552     0       2     781.05428     0.01448     Pq     15     22     0     781.99046     0	3 (81.06217 0.00390 PG 16 19 2 (81.99458 0 1 781.07121 0.01560 PQ 16 21 0 782.01506 0 2 781.13435 0.01728 PP 3 24 1 782.02932 0 2 781.16389 0.02792 PP 3 24 1 782.03599 0 0 781 7777 0 00698 PO 16 18 2 782.03795 0	2 781.21181 0.02040 PQ 16 20 0 782.03959 0. 2 781.23282 0.51947 PQ 16 36 0 782.04119 0. 0 781.24171 1.03893 PQ 16 19 0 782.06408 0. 3 781.27496 0.04720 PQ 15 48 1 782.07715 0.	1       781.28355       0.02360       Pq       16       17       2       782.07909       0.         2       781.28683       0.02392       Pq       16       18       0       782.08810       0.         2       781.35925       0.02784       Pq       15       47       3       782.09456       0.         2       781.40975       0.07416       Pq       15       47       3       782.11169       0.	0       781.442210       0.01604       79       10       10       2       782.12691       11         2       781.442923       0.03192       PP       10       11       2       782.12694       0         3       781.44132       0.229750       PP       10       11       0       782.12694       0         1       781.44630       1.19000       PQ       16       16       782.13294       0         2       781.44669       0.03632       PQ       16       16       782.15273       0         2       781.44669       0.03632       PQ       16       37       782.15273       0	Z 781.59402 U.04060 NF 10 49 Z 762.15939 U 3 781.59422 0.02462 RP 10 47 1 782.16938 0. 2 781.62423 0.04520 RP 9 47 3 782.19411 0. 3 781.63648 0.10082 RP 9 47 1 782.20352 0.	1       281.64391       0.40328       PQ       15       46       3       782.210/1       0.         2       781.66147       1.31816       PP       4       22       782.21361       0.         2       781.66810       0.04944       RP       4       22       782.22346       0.         2       781.66830       0.04944       RP       0       29       2       782.22416       0.         2       781.74206       0.05328       RP       0       29       782.22638       0.	2       781.79728       0.05632       RP       8       45       7       82.24780       0.05632         0       781.84835       0.00696       RP       8       45       0       782.26089       0.         2       781.84845       0.00596       RP       8       45       0       782.30179       0.         2       781.84845       0.00593       RP       7       43       3       782.3073       0.         2       781.85355       0.00593       RP       7       43       3       782.31640       0.         3       781.85355       0.00593       RP       7       43       1       782.31640       0.         3       781.85355       0.00593       RP       7       43       1       782.31640       0.         3       781.85355       0.00593       RP       7       43       1       782.32414       0.         0       781.85727       0.00510       RP       6       41       7782.3493       0.         0       781.85528       0.12470       RP       5       20       3782.34949       0.         0       781.85528       0.00510       RP	U (1014.201 1 (4 (1 MJ 07010.0 04100.101 0
WAVE NO INT K J S WAVE NO I	46       2       780.83535       0.00200       PP       9       13       781.88857       1         23       2       780.83796       0.71328       PP       9       13       781.8857       1         23       0       780.84839       0.17832       PQ       16       26       781.89993       0         23       0       780.84899       0.00050       PQ       16       26       781.89993       0         36       780.84899       0.00050       PQ       16       21       2781.90074       0         36       780.88658       0.00984       PQ       16       21       2781.91084       0         36       2       780.88658       0.001964       PQ       16       26       781.91084       0         36       2       780.89828       0.00126       PQ       16       26       781.92056       0         44       1       780.997169       0.00126       PQ       16       24       781.94291       0         35       780.97169       0.01200       PQ       15       2781.94633       0       781.94633       0	42       0       780.99022       0.00827       Pq       16       35       0       781.96349       0         21       3       781.03001       0.21896       Pq       16       23       0       781.96629       0         21       781.03616       0.87584       Pq       15       23       781.97552       0         21       781.05428       0.01448       Pq       15       48       3       781.99046       0         34       2       781.05428       0.01448       Pq       16       22       0       781.99046       0	40 3 781.06217 0.00390 PQ 16 19 2 781.99458 0 40 1 781.07121 0.01560 PQ 16 21 0 782.01506 0 33 2 781.13435 0.01728 PP 3 24 1 782.02932 0 38 2 781.16389 0.02792 PP 3 24 1 782.03599 0	32 2 781.21181 0.02040 PQ 16 20 0 782.03959 0. 19 2 781.23282 0.51947 PQ 16 36 0 782.04119 0. 19 0 781.24171 1.03893 PQ 16 19 0 782.06408 0. 36 3 781.27496 0.04720 PQ 15 48 1 782.07715 0.	36 1 781.28355 0.02360 PQ 16 17 2 782.07909 0. 31 2 781.28683 0.02392 PQ 16 18 0 782.08810 0. 30 2 781.35925 0.02784 PQ 15 47 3 782.09456 0. 34 2 781.40975 0.07416 PQ 16 17 0 782.11169 0.	34       0       181.442210       0.01604       19       2       10.2       10.2       122.12694       0         17       3       781.44132       0.29750       PP       10       11       2       782.12694       0         17       3       781.44132       0.29750       PP       10       11       0       782.12694       0         17       1       781.444630       1.19000       PQ       16       16       0       782.12594       0         17       1       781.44630       1.19000       PQ       16       16       0       782.15273       0         23       2       281.446569       0.03632       PQ       16       16       0       782.15273       0         23       2       281.5275       0.03632       PD       10       16       37       782.15273       0	21 2 181.280102 0.04000 NF 10 49 2 102.12298 0.32 3 781.58617 0.02462 NF 10 49 0 782.16978 0.26 2 781.59422 0.09848 PQ 15 47 1 782.19078 0.26 2 781.62423 0.04520 NP 9 47 3 782.19411 0.28 3 781.63648 0.10082 NP 9 47 1 782.20352 0.	28       1       28       1       28       164391       0.40328       PQ       15       2       782.21361       0.         15       2       781.66147       1.31816       PP       4       22       2       782.22328       0.         15       0       781.664310       0.32954       PP       4       22       2       782.22328       0.         15       0       781.664310       0.032954       RP       0.29       2       782.22328       0.         29       2       781.68430       0.049444       RP       0       29       782.22638       0.         24       2       781.74206       0.05328       RP       0       29       782.22638       0.	23       2       781.79728       0.05632       RP       8       45       7       82.24780       0.0         30       781.84846       0.49880       PQ       15       46       7       82.30770       0.0593       0.0         26       781.84846       0.49880       PQ       15       46       7       82.30770       0.0593       0.0       18       30733       0.0	21 0 101.00140 0.010 CL 01 01 02010.0 00100.101 0.12
WAVE NO INT K J S WAVE NO I	8       46       2       780.83535       0.00200       PP       9       13       781.88557       1         4       23       2       780.83796       0.71328       PP       9       13       781.88557       1         4       23       0       780.83796       0.71328       PP       9       13       781.89204       0         4       23       0       780.84839       0.17832       PQ       16       26       0       781.89993       0         8       46       0       780.84899       0.00050       PQ       16       21       2       781.90074       0         16       36       2       780.88658       0.00984       PQ       16       24       781.91084       0         7       44       3       780.89828       0.00106       PQ       16       24       781.94256       0         7       44       1       780.99771       0.00424       PQ       16       26       781.94256       0         7       44       1       780.99774       0       16       26       781.942976       0         7       44       1       780.99774	6       42       0       780.99022       0.00827       Pq       16       35       0       781.96349       0         5       21       3       781.03001       0.21896       Pq       16       23       0       781.96629       0         5       21       1       781.03001       0.21896       Pq       16       23       0       781.96629       0         16       34       2       781.03616       0.87584       Pq       15       48       3       781.97552       0         16       34       2       781.05428       0.01448       Pq       16       22       781.99046       0	5 40 3 781.06217 0.00390 PG 16 19 2 781.99458 0 5 40 1 781.07121 0.01560 PQ 16 21 0 782.01506 0 16 33 2 781.13435 0.01728 PP 3 24 1 782.02932 0 4 38 0 781.16389 0.02792 PP 3 24 1 782.03599 0	16 32 2 781.21181 0.02040 PQ 16 20 0 782.03959 0. 6 19 2 781.23282 0.51947 PQ 16 36 0 782.04119 0. 6 19 0 781.24171 1.03893 PQ 16 19 0 782.06408 0. 3 36 3 781.27496 0.04720 PQ 15 48 1 782.07715 0.	3 36 1 781.28355 0.02360 PQ 16 17 2 782.07909 0. 16 31 2 781.28683 0.02392 PQ 16 18 0 782.08810 0. 16 30 2 781.35925 0.02784 PQ 15 47 3 782.09456 0. 2 34 2 781.40975 0.07416 PQ 15 17 0 782.11169 0.	c       34       0       1	10       21       2       181.20102       0.04000       07       10       49       2       1021.10390       0         1       32       3       781.59422       0.028462       RP       10       49       0       782.16936       0         1       32       3       781.59422       0.028462       RP       10       49       0       782.19036       0         1       56       2       781.59423       0.098462       RP       9       47       1       782.19046       0         16       26       2       781.62423       0.04520       RP       9       47       3       782.19411       0         12       28       781.63648       0.100822       RP       9       47       1       782.203522       0	1       28       1       281.64391       0.40328       PQ       15       46       3       782.210/1       0.         8       15       2       781.66147       1.31816       PP       4       22       782.22338       0.         8       15       2       781.66810       0.34816       PP       4       22       782.22328       0.         16       25       781.66810       0.04944       RP       0       29       2       782.22348       0.         16       22       781.67043       0.05328       RP       0       29       782.22638       0.	6 23 2 781.79728 0.05632 RP 8 45 2 782.24780 0. 6 30 0 781.84835 0.00696 RP 8 45 0 782.26089 0. 6 31 0 781.84863 0.49880 PQ 15 46 1 782.30739 0. 6 31 0 781.84863 0.49880 RP 7 43 1 782.30733 0. 6 22 781.85077 0.05932 RP 7 43 1 782.31640 0. 6 29 0 781.85577 0.00533 RP 7 43 1 782.31640 0. 6 32 0 781.85577 0.00538 PQ 15 45 3 782.39493 0. 6 32 0 781.85528 0.12470 RP 6 41 2 782.39493 0. 6 32 0 781.85528 0.12470 RP 6 41 0 782.39493 0. 6 31 0 781.85528 0.12470 RP 5 20 3 782.39493 0. 6 31 0 781.85617 0.00908 PP 5 20 1 782.400688 0. 6 31 0 781.87697 0.00432 PP 5 20 3 782.40068 0. 7 7 7 7 7 782.40068 0.	0 CIDI+1201 1 CH CI NJ 0701010 04100101 0 12 01

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WAVE NO	784. 25985       0.04527       PP         784. 23674       0.09080       RP         784. 33737       0.03640       RP         784. 34718       0.03640       RP         784. 34718       0.03640       RP         784. 34718       0.03640       RP         784. 34718       0.001681       RQ         784. 34718       0.0018813       RP         784. 34768       0.00173       RP         784. 35781       0.00173       RP         784. 42641       0.13074       RP         784. 45980       0.00158       PQ         784. 45980       0.00158       PQ         784. 59070       0.65413<
E NO	1       784, 25985       0.04527       PP         0       784, 25985       0.09080       PP         0       784, 23737       0.03640       RP         0       3784, 33737       0.03640       RP         0       3784, 33737       0.03640       RP         0       3784, 33737       0.03640       RP         0       3784, 337318       1.52296       PQ         1       784, 42870       0.01010873       RP         7       3784, 42841       0.145667       PQ         7       3784, 42847       0.03100       PQ         7       784, 45309       0.03100       PQ         7       784, 45309       0.03100       PQ         7       784, 45910       0.01650       PQ         7       784, 45985       0.00108       PQ         7       784, 459850       0.001650       PQ         7       784, 459850       0.001650       PQ         7       784, 459850
WAVE NO	<pre>5 21 1 784.25985 0.04527 PP 5 20 3 784.29674 0.09080 PP 1 30 3 784.33737 0.03640 PP 5 30 3 784.34514 0.09080 PP 5 19 2 784.3468 0.14467 PP 8 13 2 784.34714 0.088173 PP 7 17 1 784.35181 0.04407 RP 7 17 1 784.35181 0.04407 RP 7 17 1 784.35181 0.04407 RP 7 17 1 784.4541 0.13074 RP 7 17 1 784.4549 0.08173 PP 7 17 1 784.45641 0.13074 RP 7 17 1 784.45980 0.00128 RP 7 17 1 784.45980 0.00128 RP 7 17 7 784.5608 0.15956 PP 7 17 7 784.5608 0.15956 PP 7 18 2 784.5608 0.15956 PP 7 19 7 784.5608 0.15956 PP 7 19 7 784.959810 0.00216 PP 1 40 7 784.95679 0.00024 PP 1 40 7 784.95679 0.00024 PP 1 40 7 784.95689 0.00024 PP 1 40 7 784.95679 0.00024 PP 1 4 20 784.95679 0.00024 PP 1 4 20 785.01388 0.00026 PP 1 4 17 785.01388 0.00026 PP 1 4 10 785.01388 0.00026 PP 1 4 10 785.01388 0.00026 PP 1 4 11 7785.01388 0.0000000000000000000000000000000000</pre>
J S WAVE NO	21       784.25985       0.04527       PP         20       784.25985       0.09080       PP         20       784.259674       0.090806       PP         30       3784.33737       0.03640       RP         310       784.33737       0.03640       RP         30       3784.33737       0.03640       RP         319       784.33737       0.03640       RP         313       784.3478       0.14566       PP         30       784.3478       0.14566       PP         313       784.3478       0.14566       PP         317       284.37318       1.52296       PQ       PP         317       284.42641       0.13074       RP       PP         317       3784.42641       0.13074       PP       PP <t< td=""></t<>

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T K J S WAVE NO I	343       RP       12       46       2792.05450       0.00168         104       RP       11       44       792.05756       0.00168         104       RP       10       42       792.05756       0.00168         687       RP       11       44       792.05756       0.00168         5687       RP       13       46       0.0036       0.0036         5680       RP       13       46       0.00032       0.00037         5707       RP       10       42       0.792.0549       0.00036         540       RP       10       42       0.792.0549       0.00037         540       RP       9       40       1792.0549       0.00036         541       RP       9       40       1792.0549       0.00148         5513       RP       9       40       1792.10573       0.90367         5513       RP       6       11       2792.08445       0.001432         5513       RP       11       43       792.11276       0.00366         5513       RP       13       792.11376       0.00366       0.00366         5513       RP       14	33       RP       24       792.58346       0.37335         55       PQ       11       38       792.58346       0.37335         56       PQ       11       37       792.58346       0.00668         56       PQ       11       37       792.58346       0.00668         56       PQ       11       37       792.56867       0.00832         51       PQ       11       37       792.75940       0.0832         51       PP       120       792.77540       0.03328         72       PQ       11       36       792.77540       0.01026         70       PQ       11       36       792.77540       0.94648         72       PQ       11       36       792.77540       0.94648         72       PQ       11       36       792.77839       0.91026         70       PQ       11       36       792.86362       1.11096         71       PP       2       18       792.86586       0.01258         71       PP       2       18       792.86586       0.01258         71       PP       2       18       792.86586       0.050322
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O INT K J S WAVE NO I	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	0.1533       R       1       24       792.58346       0.37336         0.04483       P       1       38       792.58346       0.37336         1.44056       P       11       37       792.58346       0.00668         1.44056       P       11       37       792.58346       0.00668         0.00360       P       11       37       792.58346       0.00658         0.00360       P       11       37       792.56897       0.00832         0.00360       P       11       37       792.56897       0.00832         0.00360       P       11       37       792.568697       0.00832         0.00360       P       11       37       792.77640       0.33328         0.001118       P       1       203       792.77839       0.01026         0.001118       P       1       203       792.86736       0.04104         1.63440       P       1       203       792.86536       0.04104         1.63440       P       1       3       792.86536       0.04104         0.40860       P       2       18       792.86536       0.04104         1.63440
ENO INT KJSWAVENO I	13909 $0.0343$ RP       12       46       272       05939 $0.00036$ 221217 $0.33104$ RP       11 $44$ 792       05939 $0.00036$ 221217 $0.33104$ RP       11 $44$ 792       05939 $0.00036$ 221217 $0.33104$ RP       11 $44$ 792       05939 $0.00036$ 221517 $0.33104$ RP       11 $44$ 792       05949 $0.00038$ 221560 $0.10353$ RP       13 $48$ 792       05949 $0.000336$ 231560 $0.20707$ RP       144       792       072450 $0.003367$ 34924 $0.21366$ P       1143       792       072456 $0.003367$ 34924 $0.21303$ RP       940       1143       792       0143 $0.003367$ 34924 $0.21303$ RP       940       1143       792       0143 $0.003367$ 34924 $0.21303$ RP       940       1143       792       0.003367         349260	74744       0.15873       R       1       792.58346       0.37936         77245       0.04483       Pq       11       38       792.58346       0.37936         77245       0.04483       Pq       11       38       792.58346       0.00668         77621       0.08967       Pq       11       37       3       792.582421       0.02672         78281       1.44056       Pq       11       37       3       792.58497       0.00832         78735       0.00360       Pq       11       37       3       792.77540       0.03328         78826       0.36014       P       1       20       792.77839       0.010332         85585       0.00172       Pq       11       37       792.77839       0.03328         90157       0.00172       Pq       1       20       792.77839       0.01026         936957       0.004172       Pq       1       3       792.86716       0.01258         94048       1.63440       Pq       1       36       792.865362       11096         94048       1.63440       Pq       1       37       792.86736       0.04104         94048
AVE NO INT K J S WAVE NO I	$\begin{array}{c} 1.18909 & 0.09343 & \mathrm{RP} & 12 & 46 & 2 & 792 & 05450 & 0.00058 \\ 1.20547 & 0.08276 & \mathrm{RP} & 11 & 44 & 1 & 792 & 05936 & 0.00058 \\ 1.20547 & 0.08276 & \mathrm{RP} & 11 & 44 & 1 & 792 & 05497 & 0.00073 \\ 1.20556 & 0.11340 & \mathrm{RP} & 10 & 42 & 792 & 05497 & 0.00073 \\ 1.20556 & 0.11340 & \mathrm{RP} & 13 & 48 & 3 & 792 & 06477 & 0.00073 \\ 1.20556 & 0.11340 & \mathrm{RP} & 13 & 48 & 1 & 792 & 05493 & 0.00350 \\ 1.20556 & 0.11340 & \mathrm{RP} & 13 & 48 & 1 & 792 & 05493 & 0.00356 \\ 1.20556 & 0.11340 & \mathrm{RP} & 13 & 48 & 1 & 792 & 05493 & 0.00356 \\ 1.20556 & 0.11340 & \mathrm{RP} & 13 & 48 & 1 & 792 & 07240 & 0.000356 \\ 1.20552 & 0.225680 & \mathrm{RP} & 13 & 48 & 1 & 792 & 08417 & 0.000356 \\ 1.35452 & 0.225680 & \mathrm{RP} & 18 & 48 & 1 & 792 & 0.02564 \\ 1.357199 & 0.20038 & \mathrm{RP} & 8 & 38 & 2 & 792 & 10183 & 0.903367 \\ 1.357199 & 0.00038 & \mathrm{RP} & 8 & 38 & 2 & 792 & 10183 & 0.903367 \\ 1.35720 & 0.225680 & 0.24493 & \mathrm{RP} & 8 & 38 & 0 & 792 & 10183 & 0.0035664 \\ 1.42756 & 0.00152 & \mathrm{RP} & 1 & 43 & 1 & 792 & 13760 & 0.001666 \\ 1.42756 & 0.00152 & \mathrm{RP} & 1 & 33 & 0 & 792 & 11276 & 0.000356 \\ 1.42756 & 0.00152 & \mathrm{RP} & 1 & 43 & 1 & 792 & 13760 & 0.00132 \\ 1.45760 & 0.256187 & \mathrm{RP} & 5 & 34 & 2 & 792 & 19451 & 0.01032 \\ 1.42750 & 0.20038 & \mathrm{RP} & 6 & 34 & 2 & 792 & 19451 & 0.00132 \\ 1.42750 & 0.00038 & \mathrm{RP} & 5 & 34 & 2 & 792 & 19451 & 0.00132 \\ 1.42750 & 0.00038 & \mathrm{RP} & 5 & 34 & 2 & 792 & 19451 & 0.00132 \\ 1.42750 & 0.00038 & \mathrm{RP} & 5 & 37 & 22764 & 0.00132 \\ 1.49198 & 1.03344 & 0.1367 & \mathrm{RP} & 5 & 37 & 227560 & 1.96108 \\ 1.550104 & 0.25843 & \mathrm{RP} & 4 & 30 & 0 & 792 & 279560 & 0.002564 \\ 1.55044 & 0.13570 & \mathrm{RP} & 7 & 9 & 7 & 9 & 3 & 792 & 279560 & 0.00132 \\ 1.61002 & 0.20353 & \mathrm{RP} & 1 & 3 & 1 & 792 & 230560 & 0.002564 \\ 1.61020 & 0.20353 & \mathrm{RP} & 1 & 3 & 1 & 792 & 230580 & 0.00132 \\ 1.61020 & 0.20353 & \mathrm{RP} & 1 & 3 & 1 & 292 & 2795760 & 0.00132 \\ 1.61020 & 0.11467 & \mathrm{RP} & 3 & 28 & 1 & 792 & 279560 & 0.00132 \\ 1.61020 & 0.10363 & \mathrm{RP} & 1 & 1 & 1 & 792 & 330580 & 0.001325 \\ 1.61020 & 0.10363 & \mathrm{RP} & 1 & 1 & 1 & 792 & 330580 & 0.0013$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
WAVE NO INT K J S WAVE NO I	791.21809 0.09343 RP 12 46 2 792.05456 0.00038 791.21217 0.08376 RP 11 44 1 792.054756 0.00038 791.21862 0.113407 RP 13 48 3 792.06472 0.00073 791.21862 0.113407 RP 13 48 3 792.06472 0.00073 791.218662 0.113407 RP 13 48 3 792.06472 0.00073 791.31650 0.113407 RP 13 48 3 792.07260 0.000320 791.31650 0.113407 RP 13 48 1 792.07260 0.000320 791.31624 0.21866 RP 9 40 1 792.07260 0.0003367 791.31624 0.12270 PP 6 11 2 792.10183 0.903367 791.31624 0.12270 PP 6 11 2 792.10183 0.903367 791.31625 0.13393 RP 13 48 1 792.2172 0.003367 791.31626 0.26187 RP 7 36 1 792.19171 0.00733 791.31626 0.26187 RP 7 36 1 792.191810 0.00733 791.43560 0.26187 RP 7 36 1 792.19180 0.00466 791.41232 0.13093 RP 6 11 4 3 792.191810 0.004565 791.43560 0.26187 RP 7 36 1 792.191810 0.004265 791.45760 0.003344 PP 6 11 42 7 792.19145 0.02365 791.45760 0.003344 PP 6 11 42 7 792.19445 0.002365 791.4560 0.26187 RP 7 36 1 792.19445 0.002365 791.4560 0.26187 RP 7 3 6 1 1 42 7 792.3372 0.03325 791.45760 0.002608 RP 6 34 2 792.79453 0.049102 791.55095 0.14467 RP 7 3 792.23927 0.002328 791.55040 0.14167 RP 7 9 1 792.23927 0.003328 791.55040 0.13567 RP 7 9 1 792.23951 0.00422 791.55040 0.13567 RP 7 9 1 792.23951 0.00422 791.55040 0.13567 RP 7 9 1 792.23660 0.013228 791.55040 0.13567 RP 7 9 1 792.23660 0.013228 791.55040 0.13567 RP 7 9 1 792.23660 0.013228 791.55040 0.13567 RP 7 9 26 6 792.47132 0.003328 791.56040 0.13567 RP 7 9 26 6 792.47132 0.003328 791.56040 0.13567 RP 7 9 26 6 792.47132 0.003328 791.56040 0.13567 PP 7 9 1 792.33688 0.013228 791.561062 0.22833 PP 1 40 1 792.33688 0.013228 791.561062 0.22833 PP 1 40 1 792.33688 0.013228 791.561060 0.22658 PP 1 7 9 1792.23666 0.000658 791.561060 0.226758 PP 1 9 272 2 792.214314 0.01688 791.561060 0.226758 PP 1 9 272 2 792.214314 0.01688 791.577400 0.21027 PP 1 1 40 3 792.25766 0.00352 791.561060 0.22675 PP 1 2 9 272.27660 0.00352 791.561060 0.22675 PP 1 2 9 272.27660 0.003572 791.561060 0.22675 PP 1 2 9 272.27660 0.003572 791.561060 0.22757660 0.002772 PP 10 1140 7 792.32688 0.013268 791.57757 PP 100120772	791.74744       0.15873       RP       1       24       772.58346       0.37336         791.77245       0.04483       PQ       11       38       3       792.59346       0.37336         791.77245       0.044483       PQ       11       37       3       792.59279       0.00668         791.77245       0.044483       PQ       11       37       3       792.59279       0.00668         791.78245       0.08967       PQ       11       37       3       792.62421       0.02672         791.78235       0.00360       PQ       11       37       3       792.62421       0.003328         791.78735       0.00360       PQ       11       37       3       792.75540       0.033328         791.98585       0.00118       PP       1       20       3       792.75440       0.94648         791.99057       0.00118       PP       1       20       3       792.75462       0.04104         791.99055       0.40860       PQ       11       36       792.77549       0.94648         791.94048       1.63440       PQ       11       36       792.86342       0.11046         791.94048
AVE NO INT K J S WAVE NO I	$ \begin{array}{c} 791 & 10809 & 0.09343 \\ 3 & 791 & 205766 & 0.00068 \\ 3 & 791 & 206477 & 0.00073 \\ 3 & 791 & 206477 & 0.00073 \\ 2 & 791 & 20660 & 0.18687 \\ 8 & 713 & 48 & 1792 & 06497 & 0.00073 \\ 2 & 791 & 20560 & 0.10353 \\ 8 & 792 & 06497 & 0.00032 \\ 1 & 791 & 20560 & 0.10353 \\ 8 & 792 & 06497 & 0.00032 \\ 1 & 791 & 20560 & 0.10353 \\ 1 & 791 & 20560 & 0.11340 \\ 1 & 792 & 0791 & 30502 \\ 1 & 791 & 30523 & 0.221660 \\ 1 & 1 & 2 & 792 & 0792 & 06497 & 0.00030 \\ 1 & 791 & 30562 & 0.10353 \\ 1 & 791 & 30562 & 0.10353 \\ 1 & 791 & 30562 & 0.10353 \\ 1 & 791 & 3702 & 0.791 & 3104 \\ 1 & 1 & 792 & 0791 & 300367 \\ 1 & 791 & 3709 & 0.00152 \\ 1 & 791 & 47360 & 0.20152 \\ 1 & 791 & 47360 & 0.20152 \\ 1 & 791 & 47360 & 0.20152 \\ 1 & 791 & 47360 & 0.20152 \\ 1 & 791 & 47360 & 0.20152 \\ 1 & 791 & 47360 & 0.20152 \\ 1 & 791 & 47360 & 0.20152 \\ 1 & 791 & 47360 & 0.20152 \\ 1 & 791 & 47360 & 0.20152 \\ 1 & 791 & 47360 & 0.00152 \\ 1 & 791 & 47360 & 0.20152 \\ 1 & 791 & 47360 & 0.00152 \\ 1 & 791 & 47360 & 0.00152 \\ 1 & 791 & 5792 & 0.13757 \\ 1 & 791 & 5792 & 0.149178 \\ 1 & 792 & 192433 & 0.224557 \\ 1 & 791 & 5793 & 0.00030 \\ 1 & 41 & 1 & 792 & 239261 & 0.001328 \\ 1 & 791 & 5792 & 27493 & 0.0033250 \\ 1 & 791 & 5791 & 0.002008 \\ 1 & 41 & 1 & 792 & 239281 & 0.013228 \\ 1 & 791 & 5792 & 0.003328 \\ 1 & 41 & 1 & 792 & 239281 & 0.013228 \\ 1 & 791 & 5792 & 0.003328 \\ 1 & 41 & 1 & 792 & 239281 & 0.013228 \\ 1 & 791 & 53440 & 0.14467 \\ 1 & 791 & 53450 & 0.20037 \\ 2 & 791 & 514673 \\ 1 & 791 & 53450 & 0.12337 \\ 1 & 791 & 53450 & 0.003328 \\ 1 & 41 & 1 & 792 & 23792 & 0.003328 \\ 1 & 41 & 1 & 792 & 23792 & 0.003328 \\ 1 & 791 & 53440 & 0.14467 \\ 1 & 792 & 13528 & 0.003328 \\ 1 & 91 & 61002 & 0.28433 \\ 1 & 91 & 61002 & 0.28433 \\ 1 & 91 & 792 & 239281 & 0.013228 \\ 1 & 791 & 53450 & 0.00328 \\ 1 & 91 & 792 & 23792 & 0.003328 \\ 1 & 91 & 772 & 2562 & 792 & 491128 \\ 1 & 792 & 497134 & 0.01688 \\ 1 & 792 & 792 & 529119 & 0.00528 \\ 1 & 792 & 792 & 529119 & 0.00528 \\ 1 & 91 & 792 & 529119 & 0.00528 \\ 1 & 91 & 792 & 529119 & 0.00528 \\ 1 & 1 & 91 & 792 & 529119 & 0.00528 \\ 1 & 1 & 91$	791.774744       747444       77245       90.00668       792.59279       0.00668       791.77245       792.69677       0.00668       791.77245       792.616877       0.00668       791.77245       792.616877       0.003328       792.616877       0.003328       792.71662       0.033328       792.71662       0.033328       791.791762       791.78735       0.003328       792.71662       0.033328       791.791762       791.77837       791.791762       791.77837       791.79176       791.77845       791.77845       791.77845       791.77845       791.77845       791.77846       791.77846       791.77846       791.7744       791.99167       0.01126       791.77846       791.77845       791.99167       791.7744       791.99167       791.77845       791.79166       791.77845       791.79166       791.7046       791.79166       791.7046       791.79166       791.71096       791.7926       791.91096       791.71096       791.7926       791.91096       77774       7792.019303       0.001258 <td< td=""></td<>
J S WAVE NO INT K J S WAVE NO I	$ \begin{array}{c} \textbf{791.5} \textbf{791.18909} \textbf{0.09343} \textbf{RP} \textbf{12} \textbf{46} \textbf{2} \textbf{792.05447} \textbf{0.00168} \textbf{792.5} \textbf{791.26447} \textbf{0.00168} \textbf{792.05756} \textbf{0.00168} \textbf{25} \textbf{1} \textbf{791.27647} \textbf{0.033704} \textbf{RP} \textbf{13} \textbf{48} \textbf{3} \textbf{792.05476} \textbf{0.00168} \textbf{25} \textbf{1} \textbf{791.27647} \textbf{0.033704} \textbf{RP} \textbf{13} \textbf{48} \textbf{3} \textbf{792.05756} \textbf{0.00168} \textbf{25} \textbf{1} \textbf{791.27647} \textbf{0.033704} \textbf{RP} \textbf{13} \textbf{48} \textbf{3} \textbf{792.05447} \textbf{0.00073} \textbf{26} \textbf{27} $	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$
S WAVE NO INT K J S WAVE NO I	$ \begin{array}{c} \textbf{791.5} \textbf{791.18009} \textbf{0.09343} \textbf{RP} \textbf{12} \textbf{46} \textbf{2} \textbf{792.05447} \textbf{0.000168} \textbf{25} \textbf{791.2047} \textbf{0.033704} \textbf{RP} \textbf{10} \textbf{42} \textbf{2} \textbf{792.05756} \textbf{0.000168} \textbf{25} \textbf{791.2047} \textbf{0.033704} \textbf{RP} \textbf{10} \textbf{42} \textbf{2} \textbf{792.05476} \textbf{0.000168} \textbf{25} \textbf{1} \textbf{791.20247} \textbf{0.033704} \textbf{RP} \textbf{10} \textbf{42} \textbf{2} \textbf{792.05476} \textbf{0.000168} \textbf{25} \textbf{1} \textbf{791.20247} \textbf{0.033704} \textbf{RP} \textbf{10} \textbf{42} \textbf{2} \textbf{792.05476} \textbf{0.000168} \textbf{25} \textbf{1} \textbf{791.20247} \textbf{0.033704} \textbf{26} \textbf{1} \textbf{2} \textbf{2} \textbf{2} \textbf{2} \textbf{2} \textbf{2} \textbf{2} 2$	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$

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J S WAVE NO I	PQ 16 45 0 795.31180 0.000 RP 1 22 3 795.31809 0.120 RP 1 22 1 795.32297 0.483 PQ 10 35 0 795.34409 0.015 PQ 10 34 0 795.44699 0.015 PQ 10 34 0 795.44699 0.015	PP 1 18 3 795.46958 0.27014 PP 1 18 1 795.47387 1.08056	PQ 10 33 2 795.47891 0.09216 PQ 10 33 0 795.52750 0.02304 PO 10 32 2 795 56007 0.11048	PP 2 16 2 795.59378 1.25184 PP 2 16 0 705.59308 0 31264	PQ 10 32 0 795.60539 0.02762 PQ 10 32 0 705.62867 0 13136	PC 10 31 2 792.03001 0.13130 PO 10 31 0 795.68089 0.03284 PO 10 30 2 795 71453 0 15488	PP 3 14 3 795.71768 1.45447	PP 3 14 1 795.72131 0.72723 PQ 10 30 0 795.75377 0.03872	PQ 10 29 2 795.78784 0 18112 PO 10 29 0 795 82423 0 04528	PP 4 12 2 795.85109 1.65304	PQ 10 28 2 795.85851 0.21000	PQ 10 28 0 199.89211 0.02200	PQ 10 27 0 795.95777 0.06034 PP 5 10 3 795.99112 0.45960	PQ 10 26 2 795.99228 0.27488 PP 5 10 1 795.99401 1.83840	PQ 10 26 0 796.02085 0.068 PO 10 25 2 706 05528 0 310	PQ 10 25 0 796.08150 0.077	PQ 10 24 2 796.11365 0.346 PQ 10 24 0 796.13960 0.086	PP 6 8 2 796.14194 1.005	PQ 10 23 2 796.17365 0.383	PQ 10 23 0 796.19547 0.095 PQ 10 22 2 796.22910 0.419	PQ 9 49 3 796.23788 0.002 PQ 10 22 0 796.24889 0.104	PQ 9 49 1 796.28114 0.00110	PQ 10 21 2 796.28201 0.45360 RP 10 39 2 796.28546 0.00712	RP 11 41 3 796.28678 0.000	RP 11 41 1 796.29356 0.003	RP 10 39 0 796.29433 0.001 RP 9 37 1 796.29633 0.006	PQ 10 21 0 796.29987 0.113 RP 12 43 2 796.30105 0.000
J S WAVE NO I	90 PQ 16 45 0 795.31180 0.000 82 RP 1 22 3 795.31809 0.120 92 RP 1 22 1 795.32297 0.483 48 PQ 10 35 0 795.36409 0.016 80 PQ 10 34 2 795.44699 0.0176 82 PQ 10 34 0 795.44699 0.016	28 PP 1 18 3 795,46958 0.27014 20 PP 1 18 1 795,47387 1.08056	10 PQ 10 33 2 795.47891 0.09216 37 PQ 10 33 0 795.55750 0.02304 38 P0 10 32 2 795 56007 0.11048	10 PP 2 16 2 795.59378 1.25184 10 PP 2 16 0 705.59908 0 31264	58 PQ 10 32 0 795.60539 0.02762 58 PQ 10 32 0 795.60539 0.02762	72 PG 10 31 2 792.05000 0.03284 32 PG 10 31 0 795.6809 0.03284 33 PG 10 30 2 795 71463 0 15488	53 PP 3 14 3 795.71768 1.45447	42 PP 3 14 1 795.72131 0.72723 57 Pq 10 30 0 795.75377 0.03872	27 PQ 10 29 2 795.78784 0.18112 14 PQ 10 29 0 795.82423 0.04528	22 PP 4 12 2 795.85109 1.65304	56 PQ 10 28 2 795.85851 0.21000	24 PQ 10 27 2 795.92672 0.24136	74 PQ 10 27 0 795.95777 0.06034 40 PP 5 10 3 795.99112 0.45960	96 PQ 10 26 2 795.99228 0.27488 06 PP 5 10 1 795.99401 1.83840	70 PQ 10 26 0 796.02085 0.068	73 PQ 10 25 0 796.08150 0.077	47 PQ 10 24 2 796.11365 0.346	36 PP 6 8 2 796.14194 1.009	70 PQ 10 23 2 796.17365 0.383	20 PQ 10 23 0 796.19547 0.095 50 PQ 10 22 2 796.22910 0.419	50 PQ 9 49 3 796.23788 0.002 90 PQ 10 22 0 796.24889 0.104	30 PQ 9 49 1 796.28114 0.00110	28 PQ 10 21 2 796.28201 0.45360 50 RP 10 39 2 796.28546 0.00712	00 RP 11 41 3 796.28678 0.000	2 RP 11 41 1 796.29356 0.003	08 RP 10 39 0 796.29433 0.001 28 RP 9 37 1 796.29633 0.006	8 PQ 10 21 0 796.29987 0.113 4 RP 12 43 2 796.30105 0.000
J S WAVE NO I	00190 PQ 16 45 0 795.31180 0.000 39782 RP 1 22 3 795.31809 0.120 00992 RP 1 22 1 795.32297 0.483 00248 PQ 10 35 0 795.36409 0.019 01280 PQ 10 34 2 795.39500 0.076 444482 PQ 10 34 0 795.44699 0.019	77928 PP 1 18 3 795.46958 0.27014 00320 PP 1 18 1 795.47387 1.08056	01640 PQ 10 33 2 795.47891 0.09216 97697 PQ 10 33 0 795.55750 0.02304 85337 P0 10 32 795.56007 0.11048	00410 PP 2 16 2 795.59378 1.25184 00088 PP 2 16 0 795.59378 0 312964	00068 PG 10 21 0 795.0539 0.02762 00068 PG 10 22 0 795.60539 0.02762 00568 PG 10 21 0 705 52867 0 12136	00272 PG 10 31 2 795.68089 0.03284 00272 PG 10 31 0 795.68089 0.03284	00063 PP 3 14 3 795.71768 1.45447	00142 PP 3 14 1 795.72131 0.72723 00567 PQ 10 30 0 795.75377 0.03872	00127 PQ 10 29 2 795.78784 0.18112 00014 PQ 10 29 0 795 82423 0.04528	02152 PP 4 12 2 795.85109 1.65304	00056 PQ 10 28 2 795.85851 0.21000	00024 Pq 10 27 2 795.92672 0.24136	00974 PQ 10 27 0 795.95777 0.06034 02640 PP 5 10 3 795.99112 0.45960	03896 PQ 10 26 2 795.99228 0.27488 00006 PP 5 10 1 795.99401 1.83840	53470 PQ 10 26 0 796.02085 0.068	03373 PQ 10 25 0 796.08150 0.077	06/47 PQ 10 24 2 796.11565 0.346 00660 PQ 10 24 0 796.13960 0.086	02786 PP 6 8 2 796.14194 1.009	29070 PQ 10 23 2 796.17365 0.383	03320 PQ 10 23 0 796.19547 0.095 48450 PQ 10 22 2 796.22910 0.419	17560 PQ 9 49 3 796.23788 0.002 04390 PQ 10 22 0 796.24889 0.104	00830 PQ 9 49 1 796.28114 0.00110	04128 PQ 10 21 2 796.28201 0.45360 26360 RP 10 39 2 796.28546 0.00712	13180 RP 11 41 3 796.28678 0.000	1032 RP 11 41 1 796.29356 0.003	37408 RP 10 39 0 796.29433 0.001 09352 RP 9 37 1 796.29633 0.006	)1278 PQ 10 21 0 796.29987 0.113 06264 RP 12 43 2 796.30105 0.000
T K J S WAVE NO I	0.00190 PQ 16 45 0 795.31180 0.000 0.39782 RP 1 22 3 795.31809 0.120 0.00992 RP 1 22 1 795.32297 0.483 0.00248 PQ 10 35 0 795.36409 0.019 0.01280 PQ 10 34 0 795.44699 0.019 0.44482 PQ 10 34 0 795.44699 0.019	1.77928 PP 1 18 3 795.46958 0.27014 0.00320 PP 1 18 1 795.47387 1.08056	0.01640 PQ 10 33 2 795.47891 0.09216 0.97697 PQ 10 33 0 795.55750 0.02304 1 65332 PO 10 32 0 795 56007 0.11048	0.00410 PP 2 16 2 795.59378 1.25184 0.0048 PP 2 16 0 795.59378 1.25184	0.00068 PQ 10 32 0 795.60539 0.02762 0.00068 PQ 10 32 0 795.60539 0.02762	0.00272 PQ 10 31 2 725.68089 0.03284 0.00272 PQ 10 31 0 795.68089 0.03284	0.00063 PP 3 14 3 795.71768 1.45447	0.00142 PP 3 14 1 795.72131 0.72723 0.00567 PQ 10 30 0 795.75377 0.03872	0.00127 PQ 10 29 2 795.78784 0.18112 0.00014 PO 10 29 0 795 82423 0.04528	0.02152 PP 4 12 2 795.85109 1.65304	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	0.00024 PQ 10 27 2 795.92672 0.24136	0.00974 PQ 10 27 0 795.95777 0.06034 0.02640 PP 5 10 3 795.99112 0.45960	0.03896 PQ 10 26 2 795.99228 0.27488 0.00006 PP 5 10 1 795.99401 1.83840	0.53470 PQ 10 26 0 796.02085 0.068	0.03373 PQ 10 25 0 796.08150 0.077	0.06/47 PQ 10 24 2 796.11565 0.346 0.00660 PQ 10 24 0 796.13960 0.086	0.02786 PP 6 8 2 796.14194 1.009 0 11144 PP 6 8 0 796 14470 2 019	0.29070 PQ 10 23 2 796.17365 0.383	0.03320 PQ 10 23 0 796.19547 0.095 0.48450 PQ 10 22 2 796.22910 0.419	0.17560 PQ 9 49 3 796.23788 0.002 0.04390 PQ 10 22 0 796.24889 0.104	0.00830 PQ 9 49 1 796.28114 0.00110	0.04128 PQ 10 21 2 796.28201 0.45360 0.26360 RP 10 39 2 796.28546 0.00712	0.13180 RP 11 41 3 796.28678 0.000	0.05112 RP 11 41 1 796.29356 0.003	0.37408 RP 10 39 0 796.29433 0.001 0.09352 RP 9 37 1 796.29633 0.006	0.01278 PQ 10 21 0 796.29987 0.113 0.06264 RP 12 43 2 796.30105 0.000
O INT K J S WAVE NO I	120         0.00190         PQ         16         45         0         795.31180         0.000           175         0.39782         RP         1         22         3         795.31809         0.120           761         0.00992         RP         1         22         1         795.32297         0.483           758         0.00248         PQ         10         35         795.356409         0.016           528         0.01280         PQ         10         34         795.4999         0.016           93         0.44482         PQ         10         34         0         795.44699         0.016	502 1.77928 PP 1 18 3 795.46958 0.27014 124 0.00320 PP 1 18 1 795.47387 1.08056	209 0.01640 PQ 10 33 2 795.47891 0.09216 143 0.97697 PQ 10 33 0 795.52750 0.02304 153 1 05332 P0 10 32 0 765 55007 0 11048	235 0.00410 PP 2 16 2 795.59378 1.25184 601 0.0088 PP 2 16 0 705.59008 0 31296	X79         0.00068         Pq         10         21         <	283 0.00272 PQ 10 31 0 795.68089 0.03284 517 0 0133 PO 10 37 0 795.68089 0.03284	575 0.00063 PP 3 14 3 795.71768 1.45447	73/0.00142 PP 3 14 1 795.72131 0.7273 286 0.00567 PQ 10 30 0 795.75377 0.03872	540 0.00127 PQ 10 29 2 795.78784 0.18112 355 0.00014 PQ 10 29 0 795.82423 0.04528	721 0.02152 PP 4 12 2 795.85109 1.65304	000 0.00056 PQ 10 28 2 795.85851 0.21000	401 0.00024 PQ 10 27 2 795.92672 0.24136	119 0.00974 PQ 10 27 0 795.95777 0.06034 519 0.02640 PP 5 10 3 795.99112 0.45960	049 0.03896 PQ 10 26 2 795.99228 0.27488 101 0.00006 PP 5 10 1 795.99401 1.83840	332 0.53470 PQ 10 26 0 796.02085 0.068	295 0.03373 PQ 10 25 0 796.08150 0.077	226 0.06/47 PQ 10 24 2 796.11565 0.346 552 0.00660 PQ 10 24 0 796.13960 0.086	997 0.02786 PP 6 8 2 796.14194 1.009 584 0 11144 PP 6 8 0 796 14470 2 019	206 0.29070 PQ 10 23 2 796.17365 0.383	272 0.03320 PQ 10 23 0 796.19547 0.095 128 0.48450 PQ 10 22 2 796.22910 0.419	383 0.17560 PQ 9 49 3 796.23788 0.002 556 0.04390 PQ 10 22 0 796.24889 0.104	185 0.00830 PQ 9 49 1 796.28114 0.00110	731 0.04128 PQ 10 21 2 796.28201 0.45360 159 0.26360 RP 10 39 2 796.28546 0.00712	099 0.13180 RP 11 41 3 796.28678 0.000	25 0.05112 RP 11 41 1 796.29356 0.003	137 0.37408 RP 10 39 0 796.29433 0.001 42 0.09352 RP 9 37 1 796.29633 0.006	50 0.01278 PQ 10 21 0 796.29987 0.113 56 0.06264 RP 12 43 2 796.30105 0.000
ENO INT KJSWAVENO I	50120 0.00190 PQ 16 45 0 795.31180 0.000 50175 0.39782 RP 1 22 3 795.31809 0.120 51761 0.00992 RP 1 22 1 795.32297 0.483 60758 0.00248 PQ 10 35 0 795.36409 0.016 62622 0.01280 PQ 10 34 2 795.44699 0.016 64193 0.444482 PQ 10 34 0 795.44699 0.016	64502 1.77928 PP 1 18 3 795.46958 0.27014 71124 0.00320 PP 1 18 1 795.47387 1.08056	/3209 0.01640 PQ 10 33 2 795.47891 0.09216 20743 0.97697 PQ 10 33 0 795.52750 0.02304 20653 PO 10 32 2 795 56007 0 11048	81235 0.00410 PP 2 16 2 795.59378 1.25184 81501 0.0088 PP 2 16 0 795 59908 0 31296	87579 0.00068 PQ 10 22 0 795.60539 0.02762 87819 0.00068 PQ 10 32 0 795.60539 0.02762	8611 0.00209 FG 10 31 2 727.0301 0.0319 88283 0.00272 PQ 10 31 0 795.68089 0.03284 88617 0 01132 PO 10 30 2 795 71453 0 15488	88675 0.00063 PP 3 14 3 795.71768 1.45447	88/3/ 0.00142 PP 3 14 1 /95./2131 0./2/23 89286 0.00567 Pq 10 30 0 795.75377 0.03872	89640 0.00127 PQ 10 29 2 795.78784 0.18112 90355 0.00014 PQ 10 29 0 795.82423 0.04528	90721 0.02152 PP 4 12 2 795.85109 1.65304	91090 0.00056 Pq 10 28 2 795.85851 0.21000	93401 0.00024 PQ 10 27 2 795.92672 0.24136	93419 0.00974 PQ 10 27 0 795.95777 0.06034 93519 0.02640 PP 5 10 3 795.99112 0.45960	94049 0.03896 PQ 10 26 2 795.99228 0.27488 94401 0.00006 PP 5 10 1 795.99401 1.83840	96032 0.53470 PQ 10 26 0 796.02085 0.068	97395 0.03373 PQ 10 25 0 796.08150 0.077	98226 0.06/47 PQ 10 24 2 796.11565 0.346 00652 0.00660 PQ 10 24 0 796.13960 0.086	01997 0.02786 PP 6 8 2 796.14194 1.009 02580 0 11100 PP 6 8 0 796 10070 2 019	03206 0.29070 Pq 10 23 2 796.17365 0.383	03272 0.03320 PQ 10 23 0 796.19547 0.095 03428 0.48450 PQ 10 22 2 796.22910 0.419	0/883 0.17560 PQ 9 49 3 796.23788 0.002 08656 0.04390 PQ 10 22 0 796.24889 0.104	09985 0.00830 PQ 9 49 1 796.28114 0.00110	12731 0.04128 PQ 10 21 2 796.28201 0.45360 14459 0.26360 RP 10 39 2 796.28546 0.00712	14999 0.13180 RP 11 41 3 796.28678 0.000	21925 0.05112 RP 11 41 1 796.29356 0.003	22437 0.37408 RP 10 39 0 796.29433 0.001 23142 0.09352 RP 9 37 1 796.29633 0.006	27850 0.01278 PQ 10 21 0 796.29987 0.113 30856 0.06264 RP 12 43 2 796.30105 0.000
NO INT K J S WAVE NO I	94.50120 0.00190 PQ 16 45 0 795.31180 0.000 94.50175 0.39782 RP 1 22 3 795.31809 0.120 94.51761 0.00992 RP 1 22 1 795.32297 0.483 94.60758 0.00248 PQ 10 35 0 795.36409 0.015 94.62622 0.01280 PQ 10 34 0 795.44699 0.015 94.64193 0.444482 PQ 10 34 0 795.44699 0.015	94. 64502 1. 77928 PP 1 18 3 795. 46958 0. 27014 94. 71124 0.00320 PP 1 18 1 795. 47387 1.08056	94.73209 0.01640 Pq 10 33 2 795.47891 0.09216 94.79743 0.97697 Pq 10 33 0 795.52750 0.02304 94.8065 1 6533 P0 10 32 0 795 55007 0 11048	94.81235 0.00410 PP 2 16 2 795.59378 1.25184 04.81535 0.00410 PP 2 16 2 795.59378 1.25184	94.87579 0.00068 PQ 10 22 0 795.6539 0.02762 04.87579 0.00068 PQ 10 32 0 795.6539 0.02762 04.87811 0 00568 PQ 10 31 0 755 5387 0 13135	94.0601 0.00000 Fq 10 31 2 727.03001 0.03204 94.88283 0.00272 Pq 10 31 0 795.68089 0.03284 94.88617 0 01133 PD 10 30 2 795 71453 0 15488	94.88675 0.00063 PP 3 14 3 795.71768 1.45447	94.88/3/ 0.00142 PP 3 14 1 795.72131 0.72723 94.89286 0.00567 PQ 10 30 0 795.75377 0.03872	94.89640 0.00127 PQ 10 29 2 795.78784 0.18112 94.90355 0.00014 PQ 10 29 0 795.82423 0.04528	94.90721 0.02152 PP 4 12 2 795.85109 1.65304	94.91090 0.00056 PQ 10 28 2 795.85851 0.21000	94.91003 0.00024 PQ 10 27 2 795.92672 0.02220	94.93419 0.00974 PQ 10 27 0 795.95777 0.06034 94.93519 0.02640 PP 5 10 3 795.99112 0.45960	94.94049 0.03896 PQ 10 26 2 795.99228 0.27488 94.94401 0.00006 PP 5 10 1 795.99401 1.83840	94.96032 0.53470 PQ 10 26 0 796.02085 0.068	94.97395 0.03373 PQ 10 25 0 796.08150 0.077	94.98226 0.06747 PQ 10 24 2 796.11565 0.346 95.00652 0.00660 PQ 10 24 0 796.13960 0.086	95.01997 0.02786 PP 6 8 2 796.14194 1.009 25 02584 0 11144 PP 6 8 0 796 14470 2 019	95.03206 0.29070 Pq 10 23 2 796.17365 0.383	95.03272 0.03320 PQ 10 23 0 796.19547 0.095 95.03428 0.48450 PQ 10 22 2 796.22910 0.419	95.07883 0.17560 PQ 9 49 3 796.23788 0.002 95.08656 0.04390 PQ 10 22 0 796.24889 0.104	95.09985 0.00830 PQ 9 49 1 796.28114 0.00110	95.12731 0.04128 PQ 10 21 2 796.28201 0.45360 35 14459 0.26360 RP 10 39 2 796.28546 0.00712	75.14999 0.13180 RP 11 41 3 796.28678 0.000	95.21925 0.05112 RP 11 41 1 796.29356 0.003	95.22437 0.37408 RP 10 39 0 796.29433 0.001 95.23142 0.09352 RP 9 37 1 796.29633 0.006	95.27850 0.01278 PQ 10 21 0 796.29987 0.113 95.30856 0.06264 RP 12 43 2 796.30105 0.000
ENO INT KJSWAVENO I	794.50120         0.00190         PQ         16         45         0         795.31180         0.000           794.50175         0.39782         RP         1         22         3         795.31809         0.120           794.51761         0.00992         RP         1         22         3         795.32297         0.483           794.51761         0.00992         RP         1         22         1         795.32297         0.483           794.60758         0.002948         PQ         10         35         795.36409         0.0143           794.62622         0.01280         PQ         10         34         7795.39500         0.076           794.64193         0.44482         PO         10         34         7795.44699         0.0126	794.64502 1.77928 PP 1 18 3 795.46958 0.27014 794.71124 0.00320 PP 1 18 1 795.47387 1.08056	794.73209 0.01640 PQ 10 33 2 795.47891 0.09216 794.79743 0.97697 PQ 10 33 0 795.52750 0.02304 794.80053 1 6533 P0 10 32 0 765.56007 0.11048	794.81235 0.00410 PP 2 16 2 795.59378 1.25184 704.83550 0.00410 PP 2 16 2 795.59378 1.25184	794.87579 0.00068 PQ 10 22 0 795.60539 0.02762 704.87579 0.00068 PQ 10 32 0 795.60539 0.02762	794.86283 0.00272 FQ 10 31 0 795.68089 0.03284 794.88283 0.00272 PQ 10 31 0 795.68089 0.03284	794.88675 0.00063 PP 3 14 3 795.71768 1.45447	794.88737 0.00142 PP 3 14 1 795.72131 0.72723 794.89286 0.00567 PQ 10 30 0 795.75377 0.03872	794.89640 0.00127 PQ 10 29 2 795.78784 0.18112 794.90355 0.00014 PQ 10 29 0 795.82423 0.04528	794,90721 0.02152 PP 4 12 2 795.85109 1.65304	794.91090 0.00056 PQ 10 28 2 795.85851 0.21000	794.91603 0.00024 PQ 10 27 2 795.92672 0.24136	794.93419 0.00974 PQ 10 27 0 795.95777 0.06034 794.93519 0.02640 PP 5 10 3 795.99112 0.45960	794.94049 0.03896 PQ 10 26 2 795.99228 0.27488 794.94401 0.00006 PP 5 10 1 795.99401 1.83840	794,96032 0.53470 PQ 10 26 0 796.02085 0.068 700.06258 2 13880 PQ 10 25 2 706 05528 0 310	794.97395 0.03373 PQ 10 25 0 796.08150 0.077	794.98226 0.06747 PQ 10 24 2 796.11565 0.346 795.00652 0.00660 PQ 10 24 0 796.13960 0.086	795.01997 0.02786 PP 6 8 2 796.14194 1.009 705 02584 0 11144 PP 6 8 0 796 14470 2 019	795.03206 0.29070 PQ 10 23 2 796.17365 0.383	795.03272 0.03320 PQ 10 23 0 796.19547 0.095 795.03428 0.48450 PQ 10 22 2 796.22910 0.419	795.07883 0.17560 PQ 9 49 3 796.23788 0.002 795.08656 0.04390 PQ 10 22 0 796.24889 0.104	795.09985 0.00830 Pq 9 49 1 796.28114 0.00110	795.12731 0.04128 PQ 10 21 2 796.28201 0.45360 795.14459 0.26360 RP 10 39 2 796.28546 0.00712	795.14999 0.13180 RP 11 41 3 796.28678 0.000	795.21925 0.05112 RP 11 41 1 796.29356 0.003	795.22437 0.37408 RP 10 39 0 796.29433 0.001 795.23142 0.09352 RP 9 37 1 796.29633 0.006	795.27850 0.01278 PQ 10 21 0 796.29987 0.113 795.30856 0.06264 RP 12 43 2 796.30105 0.000
WAVENO INT KJSWAVENO I	4       0       794,50120       0.00190       PQ       16       45       0       795.31180       0.001         3       0       794,50175       0.39782       RP       1       22       3       795.31809       0.120         3       2       794,51761       0.00992       RP       1       22       7795.32297       0.418         3       2       794,60758       0.00248       PQ       10       35       775.32597       0.418         2       794,60758       0.00248       PQ       10       34       775.39500       0.076         3       7794,6173       0.44482       PQ       10       34       775.44699       0.016	1         794.64502         1.77928         PP         1         18         795.46958         0.27014           2         0         794.71124         0.00320         PP         1         18         1         795.46958         0.27014           2         0         794.71124         0.00320         PP         1         18         1         795.47387         1.08056	1 2 /94./3209 0.01640 PQ 10 33 2 /95.4/891 0.09216 9 2 794.79743 0.97697 PQ 10 33 0 795.52750 0.02304 1 794.80053 1 0532 PO 10 32 755.5607 0 1104.8	1 0 794.81235 0.00410 PP 2 16 2 795.59378 1.25184 3 2 704.83501 0.00410 PP 2 16 2 795.59378 1.25184	2 2 794.87579 0.00068 PQ 10 22 0 795.60539 0.02762 2 3 794.87579 0.00068 PQ 10 32 0 795.60539 0.02762	2 2 794.0101 0.00272 PQ 10 31 2 797.0501 0.0310 2 1 794.88283 0.00272 PQ 10 31 0 795.68089 0.03284 3 3 794 88617 0.0132 PO 10 30 2 795 71453 0 15488	4 2 794.88675 0.00063 PP 3 14 3 795.71768 1.45447	0 0 794.88737 0.00142 PP 3 14 1 795.72131 0.72723 8 1 794.89286 0.00567 PQ 10 30 0 795.75377 0.03872	4 0 794 89640 0.00127 PQ 10 29 2 795 78784 0.18112 6 3 794 90355 0.00014 PQ 10 29 0 795 82423 0.04528	6 2 794.90721 0.02152 PP 4 12 2 795.85109 1.65304	6 1 794.91090 0.00056 PQ 10 28 2 795.85351 0.21000	8 2 794.91603 0.00024 PQ 10 27 2 795.92672 0.24136	4 3 794.93419 0.00974 PQ 10 27 0 795.95777 0.06034 9 2 794.93519 0.02640 PP 5 10 3 795.99112 0.45960	4 1 794.94049 0.03896 PQ 10 26 2 795.99228 0.27488 8 0 794.94401 0.00006 PP 5 10 1 795.99401 1.83840	7 3 794.96032 0.53470 PQ 10 26 0 796.02085 0.068 7 1 701 06251 2 13880 PO 10 25 2 706 05528 0 310	2 2 794.97395 0.03373 PQ 10 25 0 796.08150 0.077	2 0 794.98226 0.06747 PQ 10 24 2 796.11565 0.346 9 0 795.00652 0.00660 PQ 10 24 0 796.13960 0.086	0 3 795.01997 0.02786 PP 6 8 2 796.14194 1.009 0 1 705 02584 0 11144 PP 6 8 0 796 14470 2 019	0 2 795.03206 0.29070 PQ 10 23 2 796.17365 0.383	8 2 795.03272 0.03320 PQ 10 23 0 796.19547 0.095 0 795.03428 0.48450 PQ 10 22 2 796.22910 0.419	3 2 795.07883 0.17560 PQ 9 49 3 796.23788 0.002 3 0 795.08656 0.04390 PQ 10 22 0 796.24889 0.104	3 0 795.09985 0.00830 PQ 9 49 1 796.28114 0.00110	7 2 795.12731 0.04128 PQ 10 21 2 796.28201 0.45360 5 3 795.14459 0.26360 RP 10 39 2 796.28546 0.00712	1 795.14999 0.13180 RP 11 41 3 796.28678 0.000	5 2 795.21925 0.05112 RP 11 41 1 796.29356 0.003	+ 2 795.22437 0.37408 RP 10 39 0 796.29433 0.001 + 0 795.23142 0.09352 RP 9 37 1 796.29633 0.006	0 795.27850 0.01278 PQ 10 21 0 796.29987 0.113 2 795.30856 0.06264 RP 12 43 2 796.30105 0.000
S WAVE NO INT K J S WAVE NO I	0 44 0 794.50120 0.00190 PQ 16 45 0 795.31180 0.000 4 13 0 794.50175 0.39782 RP 1 22 3 795.31809 0.120 0 43 2 794.51761 0.00992 RP 1 22 1 795.32297 0.483 0 43 0 794.66758 0.00248 PQ 10 35 0 795.36409 0.015 0 42 2 794.66758 0.00248 PQ 10 34 0 795.39500 0.076 5 11 3 794.66193 0.44482 PO 10 34 0 795.44699 0.015	5 11 1 794.64502 1.77928 PP 1 18 3 795.46958 0.27014 0 42 0 794.71124 0.00320 PP 1 18 1 795.47387 1.08056	0 41 2 /94./3209 0.01640 PQ 10 33 2 /95.4/891 0.09216 6 9 2 794.79743 0.97697 PQ 10 33 0 795.52750 0.02304 6 9 0 794.8063 1 95332 PO 10 32 755 56007 0.11048	0 41 0 794.81235 0.00410 PP 2 16 2 795.59378 1.25184 0 40 2 794.81235 0.00410 PP 2 16 2 795.59378 1.25184	0 42 2 794.87579 0.00068 PQ 10 22 0 795.60539 0.02762 0 42 3 794.87579 0.00068 PQ 10 32 0 795.60539 0.02762	0 40 2 794.0601 0.00000 74 0 31 2 797.08089 0.03284 1 42 1 794.88283 0.00272 90 10 31 0 795.68089 0.03284 0 38 3 704 88617 0 01133 90 10 30 2 795 71453 0 15488	2 44 2 794.88675 0.00063 PP 3 14 3 795.71768 1.45447	0 40 0 794.88737 0.00142 PP 3 14 1 795.72131 0.72723 9 38 1 794.89286 0.00567 Pq 10 30 0 795.75377 0.03872	2 44 0 794 89640 0.00127 PQ 10 29 2 795 78784 0 18112 3 46 3 794 90355 0.00014 PQ 10 29 0 795 82423 0.04528	8 36 2 794,90721 0.02152 PP 4 12 2 795.85109 1.65304	3 46 1 794.91090 0.00056 PQ 10 28 2 795.85351 0.21000	8 36 0 194.91603 0.00338 PU 10 28 0 193.89217 0.02290 4 48 2 794.93401 0.00024 PQ 10 27 2 795.92672 0.24136	7 34 3 794.93419 0.00974 PQ 10 27 0 795.95777 0.06034 0 39 2 794.93519 0.02640 PP 5 10 3 795.99112 0.45960	7 34 1 794.94049 0.03896 PQ 10 26 2 795.99228 0.27488 4 48 0 794.94401 0.00006 PP 5 10 1 795.99401 1.83840	7 7 3 794,96032 0.53470 PQ 10 26 0 796.02085 0.068	32 2 794.97395 0.03373 PQ 10 25 0 796.08150 0.077	32 0 794.98226 0.06747 PQ 10 24 2 796.11565 0.346 39 0 795.00652 0.00660 PQ 10 24 0 796.13960 0.086	30 3 795.01997 0.02786 PP 6 8 2 796.14194 1.009 30 1 795 02584 0 11144 PP 6 8 0 796 14470 2 019	20 2 795.03206 0.29070 PQ 10 23 2 796.17365 0.383	<b>38</b> 2 795.03272 0.03320 PQ 10 23 0 796.19547 0.095 20 0 795.03428 0.48450 PQ 10 22 2 796.22910 0.419	28 2 795.07883 0.17560 PQ 9 49 3 796.23788 0.002 28 0 795.08656 0.04390 PQ 10 22 0 796.24889 0.104	0 38 0 795.09985 0.00830 PQ 9 49 1 796.28114 0.00110	0 37 2 795.12731 0.04128 PQ 10 21 2 796.28201 0.45360 3 26 3 795.14459 0.26360 RP 10 39 2 796.28546 0.00712	26 1 795.14999 0.13180 RP 11 41 3 796.28678 0.000 37 7 755.14999 0.13180 RP 11 41 3 796.28678 0.000	36 2 795.21925 0.05112 RP 11 41 1 796.29356 0.003	24 2 795.22437 0.37408 RP 10 39 0 796.29433 0.001 24 0 795.23142 0.09352 RP 9 37 1 796.29633 0.006	36 0 795.27850 0.01278 PQ 10 21 0 796.29987 0.113 35 2 795.30856 0.06264 RP 12 43 2 796.30105 0.000
J S WAVE NO INT K J S WAVE NO I	44       0       794.50120       0.00190       PQ       16       45       0       795.31180       0.001         13       0       794.50175       0.39782       RP       1       22       3       795.31809       0.120         43       2       794.51761       0.00992       RP       1       22       795.32297       0.485         43       2       794.60758       0.00248       PQ       10       35       795.326409       0.015         42       794.60758       0.001280       PQ       10       34       795.39500       0.076         41       3       794.64193       0.44482       PQ       10       34       795.44699       0.015	P 5 11 1 794.64502 1.77928 PP 1 18 3 795.46958 0.27014 2 10 42 0 794.71124 0.00320 PP 1 18 1 795.47387 1.08056	1 10 41 2 /94./3209 0.01640 PQ 10 33 2 /95.4/891 0.09216 P 6 9 2 794.79743 0.97697 PQ 10 33 0 795.52750 0.02304 P 6 9 7 794 80053 1 0533 PO 10 32 755 56007 0 11048	<b>3</b> 10 41 0 794.81235 0.00410 PP 2 16 2 795.59378 1.25184 10 40 2 794.81235 0.00410 PP 2 16 2 795.59378 1.25184	P 11 42 2 794.87579 0.00068 PQ 10 32 0 795.60539 0.02762 P 11 42 3 794.87579 0.00068 PQ 10 32 0 795.60539 0.02762 P 10 40 3 704.87519 0.00668 PQ 10 31 0 756.5387 0 13136	P 10 40 2 794.0001 0.00200 Pq 10 31 2 797.0001 0.0310 P 11 42 1 794.88283 0.00272 Pq 10 31 0 795.68089 0.03284 P 0 3 8 3 704 88617 0.0132 P0 10 30 2 705 71453 0 15488	P 12 44 2 794.88675 0.00063 PP 3 14 3 795.71768 1.45447	P 10 40 0 794.88737 0.00142 PP 3 14 1 795.72131 0.72723 P 9 38 1 794.89286 0.00567 PQ 10 30 0 795.75377 0.03872	P 12 44 0 794 89640 0.00127 PQ 10 29 2 795 78784 0.18112 P 13 46 3 794 90355 0.00014 PO 10 29 0 795 82423 0.04528	P 8 36 2 794,90721 0.02152 PP 4 12 2 795.85109 1.65304	P 13 46 1 794.91090 0.00056 PQ 10 28 2 795.85851 0.21000	P 14 48 2 794.91003 0.00024 PQ 10 27 2 795.92672 0.24136	P 7 34 3 794.93419 0.00974 PQ 10 27 0 795.95777 0.06034 2 10 39 2 794.93519 0.02640 PP 5 10 3 795.99112 0.45960	P 7 34 1 794.94049 0.03896 PQ 10 26 2 795.99228 0.27488 P 14 48 0 794.94401 0.00006 PP 5 10 1 795.99401 1.83840	P 7 7 3 794,96032 0.53470 PQ 10 26 0 796.02085 0.068	P 6 32 2 794.97395 0.03373 PQ 10 25 0 796.08150 0.077	P 6 32 0 794.98226 0.06747 PQ 10 24 2 796.11565 0.346 3 10 39 0 795.00652 0.00660 PQ 10 24 0 796.13960 0.086	P 5 30 3 795.01997 0.02786 PP 6 8 2 796.14194 1.009 P 5 30 1 795 02584 0 11144 PP 6 8 0 796 14470 2 019	0 20 2 795.03206 0.29070 PQ 10 23 2 796.17365 0.383	<b>10 38 2 795.03272 0.03320 PQ 10 23 0 796.19547 0.095</b> <b>0 20 0 795.03428 0.48450 PQ 10 22 2 796.22910 0.419</b>	2 4 28 2 795.07883 0.17560 PQ 9 49 3 796.23788 0.002 2 4 28 0 795.08656 0.04390 PQ 10 22 0 796.24889 0.104	1 10 38 0 795.09985 0.00830 Pq 9 49 1 796.28114 0.00110	2 10 37 2 795.12731 0.04128 PQ 10 21 2 796.28201 0.45360 2 3 26 3 795.14459 0.26360 RP 10 39 2 796.28546 0.00712	2 2 2 1 795.14999 0.13180 RP 11 41 3 796.28678 0.000	10 36 2 795.21925 0.05112 RP 11 41 1 796.29356 0.003	2 24 2 795.22437 0.37408 RP 10 39 0 796.29433 0.001 2 24 0 795.23142 0.09352 RP 9 37 1 796.29633 0.006	2 10 36 0 795.27850 0.01278 PQ 10 21 0 796.29987 0.113 2 10 35 2 795.30856 0.06264 RP 12 43 2 796.30105 0.000

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J S WAVE NO 1	17         44         1         809.32841         0.           4         44         0         809.35843         0.           18         46         2         809.42197         0.           18         46         0         809.42197         0.           18         46         0         809.4232         0.           14         43         2         809.44234         0.           15         18         3         809.44274         0.	21 29 3 809.51325 0. 4 42 2 809.56108 0. 4 42 0 809.59556 0. 23 33 1 809.67342 0.	th         ti         1         2         809         67646         0           16         20         2         809         68114         0           22         31         0         809         68510         0           44         41         0         809         68510         0	21 29 1 809.72330 0. 22 31 2 809.76775 0. 4 40 2 809.78859 0.	16 20 0 809.79546 0 4 40 0 809.81978 0 17 22 3 809.87886 0	4 39 2 809.89745 0 17 22 1 809.89802 0 1 30 809 92709 0	18 24 0 809.95374 0. 4 38 2 810.00316 0. 23 33 3 810 00827 0.	L 38 0 810.03128 0 18 24 2 810.09003 0 11 11 3 810.09745 0	11 11 1 810, 10056 0. 4 37 2 810, 10570 0. 4 37 0 810, 13238 0.	5 19 3 810.19344 0. 6 21 2 810.19346 0. 5 19 1 810.19699 0.	7 23 3 810.19994 0. 7 23 3 810.19992 0.	4 17 2 810.20405 0.	4 17 0 810.20811 0. 8 25 2 810.21719 0. 2 15 2 810.21720 0.	3 15 1 810.222448 0.	4 36 0 810.23035 0. 9 27 3 810.24062 0. 9 27 1 810.24487 0.	2 13 2 810.24918 0. 12 13 2 810.25190 0. 2 13 0 810.25271 0.
J S WAVE NO 1	48144       RP       17       44       1       809.35841       0.         00130       PQ       4       44       0       809.35841       0.         38758       RP       18       46       2       809.42197       0.         38750       RP       18       46       2       809.42197       0.         0520       RP       18       46       0       809.4232       0.         55032       PQ       4       43       2       809.412334       0.         28604       PQ       4       43       3       809.44574       0.         28604       PR       15       18       3       809.445724       0.         144415       PR       15       18       3       809.445724       0.	.40068 PR 21 29 3 809.51325 0. .60272 PQ 4 42 2 809.56108 0. .00928 PQ 4 42 0 809.59556 0. .00248 PR 23 33 1 809.67342 0.	00062 PQ 4 41 2 809.67646 0. 00128 PR 16 20 2 809.68114 0. 40878 PR 22 31 0 809.68510 0. 63512 P0 4 41 0 809.70927 0.	25472 PR 21 29 1 809.72330 0. 31368 PR 22 31 2 809.76775 0. 00232 PO 4 40 2 809.78750 0.	00158 PR 16 20 0 809.79546 0. 00632 PQ 4 40 0 809.81978 0. 41098 PR 17 22 3 809.87886 0.				.57640 PR 11 11 1 810.10056 0. .00018 PQ 4 37 2 810.10570 0. .37334 PQ 4 37 0 810.13238 0.	49336 RP 5 19 3 810.19344 0. 00308 RP 6 21 2 810.19346 0. 00048 RP 5 19 1 810.19699 0.		.30272 RP 4 17 2 810.20405 0. 21088 PQ 4 36 2 810.20509 0.	.00072 RP 4 17 0 810.20811 0. .25076 RP 8 25 2 810.21719 0.	.00696 RP 8 25 0 810.22227 0. 18552 RP 3 15 1 810.222448 0.	.74208 PQ 4 36 0 810.23035 0. .10396 RP 9 27 3 810.24062 0. .01624 RP 9 27 1 810.24487 0.	.41584 RP 2 13 2 810.24918 0. .00174 PR 12 13 2 810.25190 0. .00006 RP 2 13 0 810.25271 0.
O INT K J S WAVE NO I	72 1.48144 RP 17 44 1809.32841 0. 73 0.00130 PQ 4 44 0 809.35843 0. 07 0.38758 RP 18 46 2 809.42197 0. 82 0.00520 RP 18 46 0 809.42197 0. 75 1.55032 PQ 4 43 2 809.44234 0. 78 0.28604 PQ 4 43 8 809.447834 0. 33 1.14416 PR 15 18 1 809.445724 0.	77 0.40068 PR 21 29 3 809.51325 0. 12 1.60272 PQ 4 42 2 809.56108 0. 27 0.00928 PQ 4 42 0 809.59556 0. 04 0.00248 PR 23 33 1 809.67342 0.	69 0.00062 PQ 4 41 2 809.67646 0. 77 0.00128 PR 16 20 2 809.68114 0. 00 0.40878 PR 22 31 0 809.68510 0. 06 1.63512 PQ 4 41 0 809.70927 0.	70 1.25472 PR 21 29 1 809.72330 0. 27 0.31368 PR 22 31 2 809.76775 0. 01 0 00232 PO 4 40 2 809 78559 0.	99 0.00158 PR 16 20 0 809.79546 0 42 0.00632 PQ 4 40 0 809.81978 0 76 0 41098 PR 17 22 3 809.87886 0	54 1.64392 PQ 4 39 2 809.89745 0 01 0.00113 PR 17 22 1 809.89802 0 30 0 00057 PO 4 30 0 809.89802 0	85 0.40638 PR 18 24 0 809.95374 0. 39 1.62552 PQ 4 38 2 810.00316 0. 51 1 14007 PR 23 3 3 2 810.00877 0.	77 0.72023 PQ 4 38 0 810.03128 0 47 0.39410 PR 18 24 2 810.09003 0 08 0.01232 PR 11 11 3 810.09745 0.	78 1.57640 PR 11 11 1 810.10056 0. 21 0.00018 PQ 4 37 2 810.10570 0. 63 0.37334 PQ 4 37 0 810.13238 0.	72 1 49336 RP 5 19 3 810 19344 0. 92 0.00308 RP 6 21 2 810 19346 0. 53 0.00048 RP 5 19 1 810 19699 0.	55 0.00012 RP 6 21 0 810.19804 0. 32 0.34318 RP 7 23 3 810.19992 0.	43 0.30777 RP 4 17 2 810.20005 0. 16 1.21088 Pq 4 36 2 810.20509 0.	46 0.00072 RP 4 17 0 810.20811 0. 09 0.25076 RP 8 25 2 810.21719 0.	75 0.00696 RP 8 25 0 810.22227 0. 27 0.18552 RP 3 15 1 810.222448 0.	69 0.74208 PQ 4 36 0 810.23035 0. 98 0.10396 RP 9 27 3 810.24062 0. 44 0.01624 RP 9 27 1 810.24487 0.	29 0.41584 RP 2 13 2 810.24918 0. 53 0.00174 PR 12 13 2 810.25190 0. 75 0.00006 RP 2 13 0 810.25271 0.
ENO INT KJSWAVENO I	.48144 RP 17 44 1 809.32841 0. .00130 PQ 4 44 0 809.35843 0. .38758 RP 18 46 2 809.42197 0. .00520 RP 18 46 0 809.42324 0. .55032 PQ 4 43 2 809.44734 0. .28604 PQ 4 43 0 809.44724 0. .14415 18 3 809.44724 0. .14412 PR 15 18 3 809.49724 0.	06077 0.40068 PR 21 29 3 809.51325 0. 06512 1.60272 PQ 4 42 2 809.56108 0. 06627 0.00928 PQ 4 42 0 809.59556 0. 08404 0.00248 PR 23 33 1 809.67342 0.	00069 0.00062 PQ 4 41 2 809.67646 0. 09177 0.00128 PR 16 20 2 809.68114 0. 09800 0.40878 PR 22 31 0 809.68510 0. 0206 1 63512 PQ 4 41 0 809.70927 0.	10470 1.25472 PR 21 29 1 809.72330 0. 10727 0.31368 PR 22 31 2 809.76775 0. 10801 0 00232 P0 4 40 2 809 78559 0.	12799 0.00158 PR 16 20 0 809.79546 0. 13242 0.00632 PQ 4 40 0 809.81978 0. 13246 0.41098 PR 17 22 3 809.87886 0.	13654 1.64392 PQ 4 39 2 809.89745 0. 15401 0.00113 PR 17 22 1 809.89802 0. 1503 0.00013 PR 17 22 1 809.89802 0.	16485 0.40638 PR 18 24 0 809.95374 0. 16839 1.62552 PQ 4 38 2 810.00316 0. 7051 1 144047 PR 23 3 3 810 00827 0.	18177 0.72023 PQ 4 38 0 810.03128 0 9447 0.39410 PR 18 24 2 810.09003 0 19508 0.01232 PR 11 11 3 810.09745 0	9778 1.57640 PR 11 11 1 810.10056 0. 0571 0.00018 PQ 4 37 2 810.10570 0. 27163 0.37334 PQ 4 37 0 810.13238 0.	22472 1.49336 RP 5 19 3 810.19344 0. 33492 0.00308 RP 6 21 2 810.19346 0. 33553 0.00048 RP 5 19 1 810.19699 0.	24255 0.00012 RP 6 21 0 810.19804 0. 24632 0.34318 RP 7 23 3 810.19992 0.	Contract         Contract	28246 0.00072 RP 4 17 0 810.20811 0. 28809 0.25076 RP 8 25 2 810.21719 0. 2000 0.25076 RP 8 25 2 810.21719 0.	9005 1.00304 AF 3 12 3 910.22227 0.0475 0.00696 RP 8 25 0 810.22227 0.0527 0.18552 RP 3 15 1 810.22448 0.	0769 0.74208 PQ 4 36 0 810.23035 0. 1998 0.10396 RP 9 27 3 810.24062 0. 2044 0.01624 RP 9 27 1 810.24487 0.	2229 0.41584 RP 2 13 2 810.24918 0. 2253 0.00174 PR 12 13 2 810.25190 0. 2275 0.00006 RP 2 13 0 810.25271 0.
NO INT K J S WAVE NO I	08.98372 1.48144 RP 17 44 1 809.32841 0. 09.01973 0.00130 PQ 4 44 0 809.35843 0. 09.02107 0.38758 RP 18 46 2 809.42197 0. 09.02482 0.00520 RP 18 46 0 809.4232 0. 09.02575 1.55032 PQ 4 43 2 809.447934 0. 09.03578 0.28604 PQ 4 43 2 809.447934 0. 09.03938 1.44412 PQ 4 43 0 809.447724 0. 09.03738 1.44416 P2 809.445724 0.	09.06077 0.40068 PR 21 29 3 809.51325 0. 09.06512 1.60272 PQ 4 42 2 809.56108 0. 09.06627 0.00928 PQ 4 42 0 809.59556 0. 09.08404 0.00248 PR 23 33 1 809.67342 0.	09.09069 0.00062 PQ 4 41 2 809.67646 0. 09.09177 0.00128 PR 16 20 2 809.68114 0. 09.09800 0.40878 PR 22 31 0 809.68510 0. 09.10206 1.63512 PO 4 41 0 809.70927 0.	09.10470 1.25472 PR 21 29 1 809.72330 0. 09.10727 0.31368 PR 22 31 2 809.76775 0. 09.1081 0 00232 PO 4 40 2 809 78559 0.	09.12799 0.00158 PR 16 20 0 809.79546 0. 09.13242 0.00632 PQ 4 40 0 809.81978 0. 09.13276 0 41008 PR 17 22 3 809.87886 0.	09.13654 1.64392 PQ 4 39 2 809.89745 0 09.15401 0.00113 PR 17 22 1 809.89802 0 09.15030 0.00157 PO 4 30 0 809 02709 0	09.16485 0.40638 PR 18 24 0 809.95374 0. 09.16839 1.62552 PQ 4 38 2 810.00316 0. 01.7051 1.04047 PR 23 33 3.810.00877 0.	09.18177 0.72023 PQ 4 38 0 810.03128 0 09.19147 0.39410 PR 18 24 2 810.09003 0 09.19568 0.01232 PR 11 11 3 810.09745 0	09.19778 1.57640 PR 11 11 1 810.10056 0. 09.20521 0.00018 PQ 4 37 2 810.10570 0. 09.22163 0.37334 PQ 4 37 0 810.13238 0.	09.22472 1.49336 RP 5 19 3 810.19344 0. 09.23492 0.00308 RP 6 21 2 810.19346 0. 09.23553 0.00048 RP 5 19 1 810.19699 0.	0.24255 0.00012 RP 6 21 0 810.19804 0. 09.24632 0.34318 RP 7 23 3 810.19992 0.	09.26843 0.30272 RP 4 17 2 810.20405 0. 09.26843 0.30288 PQ 4 36 2 810.20405 0.	09.28246 0.00072 RP 4 17 0 810.20811 0. 09.28809 0.25076 RP 8 25 2 810.21719 0.	79.29007 1.00304 AF 3 12 3 910.2221 9. 39.30475 0.00696 RP 8 25 0 810.22227 0. 39.30527 0.18552 RP 3 15 1 810.22448 0.	09.30769 0.74208 PQ 4 36 0 810.23035 0. 09.31998 0.10396 RP 9 27 3 810.24062 0. 09.32044 0.01624 RP 9 27 1 810.24487 0.	09.32229 0.41584 RP 2 13 2 810.24918 0. 09.32253 0.00174 PR 12 13 2 810.25190 0. 09.32275 0.00006 RP 2 13 0 810.25271 0.
MAVE NO INT K J S WAVE NO I	808.98372         1.48144         RP         17         44         1         809.32841         0.           809.01973         0.00130         PQ         44         0         809.35843         0.           809.02107         0.38758         RP         18         46         809.42197         0.           809.02482         0.00520         RP         18         46         809.42197         0.           809.02482         0.00520         RP         18         46         809.4232         0.           809.02575         1.55032         PQ         4         43         2         809.44234         0.           809.03548         0.28604         PQ         4         43         2         809.447234         0.           809.03338         0.14413         P         15         18         3         809.44574         0.	809.06077 0.40068 PR 21 29 3 809.51325 0. 809.06512 1.60272 PQ 4 42 2 809.56108 0. 809.06627 0.00928 PQ 4 42 0 809.59556 0. 809.08404 0.00248 PR 23 33 1 809.67342 0.	809.09069 0.00062 PQ 4 41 2 809.67646 0. 809.09177 0.00128 PR 16 20 2 809.68114 0. 809.09800 0.40878 PR 22 31 0 809.68510 0. 809.10206 1 63512 PQ 4 41 0 809.70927 0.	809.10470 1.25472 PR 21 29 1 809.72330 0. 809.10727 0.31368 PR 22 31 2 809.76775 0. 809.1081 0.00232 PO 4 40 2 809.78559 0.	809.12799 0.00158 PR 16 20 0 809.79546 0. 809.13242 0.00032 PQ 4 40 0 809.81978 0. 809.13245 0.01098 PR 17 22 3 809.87886 0.	809.13654 1.64392 PQ 4 39 2 809.89745 0 809.15401 0.00113 PR 17 22 1 809.89802 0 800 15030 0.00157 P0 4 30 0 809 02709 0	809.16485 0.40638 PR 18 24 0 809.95374 0. 809.16839 1.62552 PQ 4 38 2 810.00316 0. 809.17051 1.0447 PF 23 33 3.810.00877 0.	809.18177 0.72023 PQ 4 38 0 810.03128 0 809.19147 0.39410 PR 18 24 2 810.09003 0 809.19548 0.01232 PR 11 11 3 810.09745 0.	809.19778 1.57640 PR 11 11 1 810.10056 0. 809.20521 0.00018 PQ 4 37 2 810.10570 0. 809.22163 0.37334 PQ 4 37 0 810.13238 0.	809.22472 1.49336 RP 5 19 3 810.19344 0. 809.23492 0.00308 RP 6 21 2 810.19346 0. 800.23553 0.00048 RP 5 19 1 810.19699 0.	809.24255 0.00012 RP 6 21 0 810.19804 0. 809.24632 0.34318 RP 7 23 3 810.19992 0.	809.26843 0.30272 RP 4 17 2 810.20405 0. 809.27116 1.21088 PQ 4 36 2 810.20509 0.	809.28246 0.00072 RP 4 17 0 810.20811 0. 809.28809 0.25076 RP 8 25 2 810.21719 0.	809.30475 0.00696 RP 8 25 0 810.22227 0.809.30527 0.18552 RP 3 15 1 810.222448 0.	809.30769 0.74208 PQ 4 36 0 810.23035 0. 809.31998 0.10396 RP 9 27 3 810.24062 0. 809.32044 0.01624 RP 9 27 1 810.24487 0.	809.32229 0.41584 RP 2 13 2 810.24918 0. 809.32253 0.00174 PR 12 13 2 810.25190 0. 809.32275 0.00006 RP 2 13 0 810.25271 0.
ENO INT KJSWAVENO I	7 1 808.98372 1.48144 RP 17 44 1 809.32841 0. 6 3 809.01973 0.00130 PQ 4 44 0 809.35843 0. 6 3 809.02107 0.38758 RP 18 46 2 809.42197 0. 6 1 809.02482 0.00520 RP 18 46 0 809.42329 0. 6 1 809.02482 0.00520 RP 18 46 0 809.42324 0. 8 3 809.03578 1.555032 PQ 4 43 0 809.44734 0. 8 3 809.03578 0.28604 PQ 4 43 0 809.44724 0. 5 3 809.0378 0.28604 PQ 4 43 0 809.44724 0. 5 3 809.04797 0.00015 PR 15 18 1 809.445724 0.	5 3 809.06077 0.40068 PR 21 29 3 809.51325 0. 5 1 809.06512 1.60272 PQ 4 42 2 809.56108 0. 6 2 809.06627 0.00928 PQ 4 42 0 809.59556 0. 8 2 809.08404 0.00248 PR 23 33 1 809.67342 0.	8         0         809,09069         0.00062         PQ         4         41         2         809,67646         0.           5         1         809,09177         0.00128         PR         16         20         2         809,68114         0.           4         3         809,09800         0.40878         PR         22         31         0         809,68510         0.           4         3         809,09800         0.40878         PR         22         31         0         809,68510         0.           4         1         809         10206         1         63512         P0         4         41         0         809,70927         0.	6 2 809.10470 1.25472 PR 21 29 1 809.72330 0. 6 0 809.10727 0.31368 PR 22 31 2 809.76775 0. 6 0 809.10727 0.31368 PR 22 31 2 809.76775 0.	4     3     809.12799     0.00158     PR     16     20     809.79546     0.       4     1     809.13242     0.00632     PQ     4     40     0     809.81978     0.       3     3     809.13242     0.00632     PR     17     27     3     809.81978     0.	3 1 809.13654 1.64392 PQ 4 39 2 809.89745 0 0 3 809.15401 0.00113 PR 17 22 1 809.89802 0 0 1 809 1592 0.00057 PO 4 39 0 809 92709 0	2 3 809.16485 0.40638 PR 18 24 0 809.95374 0. 2 1 809.16839 1.62552 PQ 44 38 2 810.00316 0. 4 3 809.16839 1.404047 PR 23 3 3 3 10 00877 0.	1         809,18177         0.72023         P0         4.38         0.810,03128         0.3324           1         3         809,19147         0.39410         PR         18         24         2810,09003         0.           5         809,19508         0.01732         PR         11         3         810,09745         0.	1         1         809.19778         1.57640         PR         11         1         810.10056         0           7         0         809.20521         0.00018         PQ         4         37         2         810.10570         0           0         3         809.22163         0.37334         PQ         4         37         0         810.13238         0	0 1 809.22472 1.49336 RP 5 19 3 810.19344 0. 5 0 809.23492 0.00308 RP 6 21 2 810.19346 0. 5 2 809 23553 0 00048 RP 5 19 1 810.19699 0.	2 0 809.24255 0.00012 RP 6 21 0 810.19804 0. 9 3 809.24632 0.34318 RP 7 23 3 810.19992 0. 9 3 809.24632 0.34318 RP 7 23 3 810.19992 0.	3 809.26843 0.37272 RP 4 17 2 810.20405 0. 1 809.26844 1.21088 PQ 4 36 2 810.20405 0.	7 2 809.28246 0.00072 RP 4 17 0 810.20811 0. 7 3 809.28809 0.25076 RP 8 25 2 810.21719 0. 7 3 202.22020 1.25076 RP 8 25 2 810.21719 0.	1       1       0.09, 29000       1.00304       Nr       3       1.0       3       0.0       2.1       3       0.0       2.1       0.0	6 1 809.30769 0.74208 PQ 4 36 0 810.23035 0. 5 3 809.31998 0.10396 RP 9 27 3 810.24062 0. 4 2 809.32044 0.01624 RP 9 27 1 810.24487 0.	5 1 809.32229 0.41584 RP 2 13 2 810.24918 0. 6 0 809.32253 0.00174 PR 12 13 2 810.25190 0. 4 3 809.32275 0.00006 RP 2 13 0 810.25271 0.
MAVE NO INT K J S WAVE NO I	5       17       1       808.98372       1.48144       RP       17       44       1       809.32841       0.         3       36       3       809.01973       0.00130       PQ       4       44       0       809.35841       0.         5       16       3       809.01973       0.00130       PQ       4       44       0       809.35843       0.         5       16       3       809.02107       0.38758       RP       18       46       2       809.42197       0.         3       36       1       809.022107       0.38758       RP       18       46       0       809.42197       0.         5       16       1       809.02275       1.55032       PQ       4       43       2       809.44234       0.         1       8       3       809.04728       0.025032       PQ       4       4       3       809.447234       0.         1       8       3       809.04775       1.55032       PQ       4       4       3       3       809.447234       0.         1       8       3       809.044776       1.77454       0.       2       3 <td>5 15 3 809.06077 0.40068 PR 21 29 3 809.51325 0. 5 15 1 809.06512 1.60272 PQ 4 42 2 809.56108 0. 4 46 2 809.06627 0.00928 PQ 4 42 0 809.59556 0. 4 38 2 809.08404 0.00248 PR 23 33 1 809.67342 0.</td> <td>u       38       0       809.09069       0.00062       PQ       u       u1       2       809.67646       0.         9       25       1       809.09177       0.00128       PR       16       20       2       809.68114       0.         5       1       4       3       809.09800       0.40878       PR       22       31       0       809.68510       0.         5       1       1       3       809.09800       0.40878       PR       22       31       0       809.68510       0.</td> <td>6 2 809.10470 1.25472 PR 21 29 1 809.72330 0. 6 0 809.10727 0.31368 PR 22 31 2 809.76775 0. 46 0 809.10801 0 00232 P0 4 40 2 809.78859 0.</td> <td>14 3 809.12799 0.00158 PR 16 20 0 809.79546 0. 14 1 809.13242 0.00632 PQ 4 40 0 809.81978 0. 13 3 809.13242 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WAVE	RP       12       25       0       821.50235       0         RQ       0       49       0       821.50541       0         RQ       0       47       2       821.50541       0         RQ       0       47       2       821.55203       0         PR       10       18       2       821.55203       0         PR       10       18       2       821.55106       0         PR       10       18       2       821.55137       0         PR       10       18       0       821.55137       0         PR       19       35       1       821.55380       0         PR       19       35       1       821.55736       0	RP 13 27 3 821.58867 0 RP 13 27 1 821.59225 0 RQ 0 45 2 821.59454 0 RQ 0 46 0 821.61109 0	PK 20 3/ 2 821.62395 0 RQ 0 44 2 821.62945 0 PR 11 20 3 821.64046 0 PR 11 20 1 821.64046 0 PR 0 45 0 821.64046 0	RQ 0 413 2 821.66332 0 RQ 0 444 0 821.67712 0 RP 14 29 2 821.68890 0 RP 14 29 0 821.69331 0	RQ 0 42 2 821.69617 0 RQ 0 43 0 821.70879 0 RQ 0 41 2 821.72820 0 PR 12 22 2 821.73710 0	PR 12 22 0 821.75938 0 PR 12 22 0 821.75772 0 PR 21 39 3 821.76944 0 PR 21 39 3 821.78300 0	RQ 0 39 2 821.78554 0. RP 15 31 3 821.79454 0. RP 15 31 3 821.79454 0. RQ 0 31 821.79832 0. RQ 0 38 2 821.81887 0.	RQ 0 39 0 821.82684 0. PR 13 24 3 821.84601 0. RQ 0 37 2 821.84726 0. RQ 0 38 0 821.85428 0. PR 13 24 1 821 8545 0.	RQ 0 36 2 821.87492 0. RQ 0 37 0 821.88085 0. RQ 0 35 2 821.90154 0. RP 16 33 2 821.90174 0. RP 16 33 2 821.91018 0. RP 16 33 0 821.91018 0. RP 16 33 0 821.91044 0.	RQ 0 32 0 821.93168 0. RQ 0 33 2 821.95249 0. RQ 0 34 0 821.95593 0. PR 14 26 2 821.95682 0. RQ 0 32 2 821.97662 0.
WAVE	0024     RP     12     25     0     821.50235     0       0568     RQ     0     49     0     821.50541     0       0153     RQ     0     47     2     821.50541     0       0153     RQ     0     47     2     821.50541     0       2528     PR     10     18     2     821.51706     0       0112     RQ     0     48     0     821.53706     0       0112     RQ     0     48     0     821.55137     0       154     RQ     0     46     821.55136     0       0100     RQ     0     47     0     821.57736     0	0002         RP         13         27         3         821.58867         0           0350         RP         13         27         1         821.59256         0           2344         RQ         0         45         2         821.59454         0           5586         RQ         0         46         0         821.59454         0	2528 RQ 0 44 2 821.62395 0 2528 RQ 0 44 2 821.62945 0 5452 PR 11 20 3 821.64046 0 1808 PR 11 20 1 821.64046 0 1808 PR 0 45 0 821.64046 0	3300         RQ         0         43         2         821.66332         0           9817         RQ         0         44         0         821.67712         0           9633         RP         14         29         821.66332         0           9633         RP         14         29         821.66333         0           9633         RP         14         29         821.66333         0           9076         RP         14         29         0         821.69333         0	0672 RQ 0 42 2 821.69617 0 5168 RQ 0 43 0 821.70879 0 4116 RQ 0 41 2 821.72820 0 5464 PR 12 22 2 821.73710 0	2320 RQ 0 42 0 621.75949 0 2320 RQ 0 40 2 821.75772 0 2944 RQ 0 41 0 821.76944 0 2944 RQ 0 41 0 821.76944 0 2944 RQ 1 39 3 821.78300 0	089/ RQ 0 39 2 821.78554 0. 1793 RP 15 31 3 821.79454 0. 0010 RP 15 31 1 821.79832 0. 1790 RQ 0 38 2 821.81887 0. 4790 RQ 0 38 2 821.81887 0.	0077 RQ 0 39 0 821.82684 0. 1908 PR 13 24 3 821.84601 0. 1632 RQ 0 37 2 821.84726 0. 1674 RQ 0 38 0 821.85428 0.	5480 RQ 0 36 2 821.87492 0. 1120 RQ 0 37 0 821.88085 0. 1108 RQ 0 37 0 821.90154 0. 1432 RQ 0 35 0 821.90154 0. 1432 RP 16 33 2 821.91018 0. 0018 RP 16 33 0 821.910494 0. 0018 RP 16 33 0 821.910494 0.	2980 Kg U 55 U 821.93168 U. 4490 Rg O 33 2 821.95249 O. 1142 Rg O 34 0 821.95593 O. 1388 PR 14 26 2 821.95622 O. 390 Rg O 32 2 821.97662 O.
T K J S WAVE	.00024       RP       12       25       0       821.50235       0         .00568       RQ       0       49       0       821.50241       0         .00153       RQ       0       49       0       821.50241       0         .00153       RQ       0       47       2       821.52203       0         .00153       RQ       0       47       2       821.51516       0         .10112       RQ       0       48       0       821.55137       0         .16116       PR       10       18       0       821.55137       0         .04154       R       0       47       0       821.55736       0         .20700       RQ       0       47       0       821.57536       0	.00002 RP 13 27 3 821.58867 0 .10350 RP 13 27 1 821.59225 0 .22344 RQ 0 45 2 821.59454 0 .05586 RQ 0 46 0 821.61109 0	.10112 PK 20 3/ 2 821.62395 0 .02528 RQ 0 44 2 821.62945 0 .05452 PR 11 20 3 821.63126 0 .21808 PR 11 20 1 821.64046 0 16600 R0 0 45 0 821.64046 0	.08300 RQ 0 43 2 821.66332 0 .09817 RQ 0 44 0 821.67712 0 .19633 RP 14 29 2 821.68890 0 .00076 RP 14 29 0 821.69331 0	.20672 RQ 0 42 2 821.69617 0 .05168 RQ 0 43 0 821.70879 0 .04116 RQ 0 41 2 821.72820 0 .16464 PR 12 22 2 821.73710 0		.1089/ KQ 0 39 2 821.78954 0. 21793 RP 15 31 3 821.79454 0. 00010 RP 15 31 1 821.79854 0. 00580 RP 0 40 0 821.79852 0. 04790 RQ 0 38 2 821.81887 0.	.00077 RQ 0 39 0 821.82684 0. 04908 PR 13 24 3 821.84601 0. .19632 RQ 0 37 2 821.84726 0. .06704 RQ 0 38 0 821.85428 0.	.16480 RQ 0 36 2 821.87492 0. 04120 RQ 0 37 0 821.88085 0. 01108 RQ 0 35 2 821.90154 0. 00008 RP 16 33 2 821.910675 0. 00018 RP 16 33 0 821.91018 0. 000420 RQ 0 34, 2 821.91194 0.	.12980 KG 0 35 0 821.95168 0. 06490 RQ 0 33 2 821.95249 0. 00142 RQ 0 34 0 821.95593 0. 00188 PR 14 26 2 821.95622 0. 01390 RQ 0 32 2 821.97662 0.
O INT K J S WAVE	17       0.00024       RP       12       25       0       821.50235       0         19       0.00568       RQ       0       49       0       821.50541       0         19       0.00153       RQ       0       47       2       821.50541       0         27       0.00153       RQ       0       47       2       821.52203       0         21       0.01112       RQ       0       47       2       821.53706       0         21       0.10112       RQ       0       48       821.551370       0         25       0.16616       PR       10       18       821.55137       0         35       0.16616       PR       19       35       1       821.55380       0         37       0.00008       RQ       0       47       0       821.57536       0	12 0.00002 RP 13 27 3 821.58867 0 14 0.10350 RP 13 27 1 821.59225 0 22 0.22344 RQ 0 45 2 821.59454 0 21 0.05586 RQ 0 46 0 821.61109 0	22 0.10112 PK 20 3/ 2 821.62395 0 36 0.02528 RQ 0 44 2 821.62945 0 52 0.05452 PR 11 20 3 821.63126 0 18 0.21808 PR 11 20 1 821.64046 0 17 0 16600 R0 0 45 0 821 64446 0	88 0.08300 RQ 0 43 2 821.66332 0 11 0.09817 RQ 0 44 0 821.67712 0 33 0.19633 RP 14 29 2 821.68890 0 12 0.00076 RP 14 29 0 821.69331 0	20         0.20672         RQ         0         42         821.69617         0           13         0.05168         RQ         0         43         0         821.70879         0           16         0.04116         RQ         0         41         821.72820         0           15         0.16464         PR         12         821.72820         0	0         1         0	U3 0.1089/ KQ 0 39 2 821.79694 0. 10 0.21793 RP 15 31 3 821.79454 0. 27 0.00010 RP 15 31 1 821.79839 0. 17 0.09580 RQ 15 31 2821.79832 0. 11 0.04790 RQ 0 38 2 821.81887 0.	50 0.00077 RQ 0 39 0 821.82684 0. 9 0.04908 PR 13 24 3 821.84601 0. 88 0.19632 RQ 0 37 2 821.84726 0. 44 0.06704 RQ 0 38 0 821.85428 0. 0.0.01775 PR 13 24 1 821.85428 0.	7 0.16480 RQ 0 36 2 821.87492 0. 0 0.04120 RQ 0 37 0 821.88085 0. 0 0.01108 RQ 0 37 0 821.90154 0. 20 0.004432 RQ 0 35 0 821.90154 0. 20 0.004438 RP 16 33 2 821.91018 0. 7 0.00018 RP 16 33 0 821.91494 0. 22 0.00420 RQ 0 34 2 821.92744 0.	4 0.12980 Kg 0 35 0 821.95168 0. 0 0.06490 Rg 0 33 2 821.95249 0. 5 0.00142 Rg 0 34 0 821.95593 0. 4 0.00138 PR 14 26 2 821.95682 0. 1 0.01390 Rg 0 32 2 821.97662 0.
ENO INT KJSWAVE	88917       0.00024       RP       12       25       0       821.50235       0         98875       0.00568       RQ       0       49       0       821.50541       0         99319       0.00153       RQ       0       47       2       821.52203       0         01797       0.02528       PR       10       18       2       821.53706       0         02021       0.10112       RQ       0       48       0       821.53706       0         02021       0.10112       RQ       0       48       0       821.53706       0         02155       0.10616       PR       10       18       2       821.55137       0         02155       0.10616       PR       19       18       0       821.55837       0         02154       0.004154       RR       19       35       1821.55786       0         023178       0.20700       RQ       0       47       0       821.5765       0	03312 0.00002 RP 13 27 3 821.58867 0 03414 0.10350 RP 13 27 1 821.59225 0 05192 0.22344 RQ 0 45 2 821.59454 0 05451 0.05586 RQ 0 46 0 821.61109 0	000022 0.10112 PK 20 3/ 2 821.62395 0 06286 0.02528 RQ 0 44 2 821.62945 0 07862 0.05452 PR 11 20 3 821.64046 0 08118 0.21808 PR 11 20 1 821.64046 0 00017 0 16600 PC 0 0 45 0 821.64044 0	00288 0.08300 RQ 0 43 2 821.66332 0 11511 0.09817 RQ 0 44 0 821.67712 0 11803 0.19633 RP 14 29 2 821.68890 0 13012 0.00076 RP 14 29 0 821.69331 0	13020       0.20672       RQ       0       42       2       821.69617       0         13313       0.05168       RQ       0       43       0       821.70879       0         15816       0.04116       RQ       0       41       2       821.72820       0         15816       0.04116       RQ       0       41       2       821.72820       0         16095       0.16464       PR       12       22       2       821.73710       0	1794         0.02750         Nu         0.42         0.621.75978         0.12172         0.121	2303 0.1089/ KQ 0 39 2 821.79454 0. 23740 0.21793 RP 15 31 3 821.79454 0. 24827 0.09580 RP 15 31 821.79839 0. 27007 0.09580 RQ 0 40 0 821.79832 0. 27311 0.04790 RQ 0 38 2 821.81887 0.	29160 0.00077 RQ 0 39 0 821.82684 0. 29579 0.04908 PR 13 24 3 821.84601 0. 29968 0.19632 RQ 0 37 2 821.84726 0. 33884 0.106744 RR 13 24 1 821.85428 0. 34250 0.01674 PR 13 24 1 821.86457 0.	36877 0.16480 RQ 0 36 2 821.87492 0. 37627 0.04120 RQ 0 37 0 821.88085 0. 41370 0.01108 RQ 0 37 2 821.90154 0. 13702 0.01108 RQ 0 35 0 821.90154 0. 43503 0.00403 RP 16 33 2 821.91018 0. 44562 0.00420 RP 16 33 0 821.91494 0.	14/24 0.12980 Kg 0 52 0 821.93168 0. 15330 0.06490 Rg 0 33 2 821.95249 0. 17785 0.00142 Rg 0 34 0 821.95593 0. 18434 0.00188 PR 14 26 2 821.95622 0. 19831 0.01390 Rg 0 32 2 821.97662 0.
NO INT KJSWAVE	20.88917       0.00024       RP       12       25       0       821.50235       0         20.98875       0.00568       RQ       0       49       0       821.50541       0         20.99319       0.00153       RQ       0       49       0       821.55243       0         21.01797       0.00153       RQ       0       47       2       821.52203       0         21.02021       0.10112       RQ       0       47       2       821.552706       0         21.02021       0.10112       RQ       0       48       821.554156       0         21.02155       0.16616       PR       10       18       821.55437       0         21.02155       0.16616       PR       19       35       1       821.55580       0         21.02184       0.004154       R       19       35       1       821.57536       0         21.02170       RQ       0       47       0       821.57536       0	21.03312 0.00002 RP 13 27 3 821.58867 0 21.03414 0.10350 RP 13 27 1 821.59225 0 21.05192 0.22344 RQ 0 445 2 821.59454 0 21.05451 0.05586 RQ 0 46 0 821.61109 0	Z1.06052 0.10112 PK Z0 3/ Z 821.62395 0 21.06286 0.02528 RQ 0 44 2 821.62945 0 21.07862 0.05452 PR 11 20 3 821.63126 0 21.08118 0.21808 PR 11 20 1 821.64046 0 21.08118 0.21808 PR 11 20 1 821.64046 0	21.09288 0.08300 RQ 0 43 2 821.66332 0 21.11511 0.09817 RQ 0 44 0 821.67712 0 21.11803 0.19633 RP 14 29 2 821.68890 0 21.13012 0.00076 RP 14 29 0 821.69331 0	21.13020 0.20672 RQ 0 42 2 821.69617 0 21.13313 0.05168 RQ 0 43 0 821.70879 0 21.15816 0.04116 RQ 0 41 2 821.72820 0 21.16095 0.16464 PR 12 22 2 821.73710 0	21.17941 0.022320 NG 0 42 0 021.75938 0 21.17941 0.22320 NG 0 41 0 821.75938 0 21.1892 0.00304 PR 12 22 0 821.76772 0 21.21099 0.12944 RQ 0 41 0 821.76944 0 21.21429 0.03236 PR 21 39 3 821.78300 0	21.23303 0.1089/ KQ 0 39 2 821.78954 0. 21.23740 0.21793 RP 15 31 3 821.79454 0. 21.24827 0.0010 RP 15 31 1 821.79854 0. 21.24877 0.09580 RQ 0 41 0 1 821.79852 0. 21.27311 0.04790 RQ 0 38 2 821.81887 0.	21.29160 0.00077 RQ 0 39 0 821.82684 0. 21.29579 0.04908 PR 13 24 3 821.84601 0. 21.29968 0.19632 RQ 0 37 2 821.84726 0. 21.33884 0.06704 RQ 0 38 0 821.85428 0. 21.33650 0.0676 PR 13 24 1 871.86167 0.	21.36877 0.16480 RQ 0 36 2 821.87492 0. 21.37627 0.04120 RQ 0 37 0 821.88085 0. 21.41370 0.01108 RQ 0 35 2 821.90154 0. 1.413230 0.00108 RP 16 33 2 821.910675 0. 21.44347 0.00018 RP 16 33 0 821.91094 0. 21.44562 0.00420 RQ 0 34 2 821.91494 0.	21.44754 0.12980 Kg 0 35 0 821.95168 0. 21.45330 0.06490 Rg 0 33 2 821.95249 0. 21.47785 0.00182 PR 14 26 2 821.95593 0. 21.49831 0.01390 Rg 0 32 2 821.97662 0.
AVE NO INT K J S WAVE	0.88917       0.00024       RP       12       25       0       821.50235       0         0.99319       0.00153       RQ       0       49       0       821.52203       0         0.99319       0.00153       RQ       0       47       2       821.52203       0         1.01797       0.02528       PR       10       18       2       821.53706       0         1.01797       0.02528       PR       10       18       2       821.53706       0         1.02021       0.10112       RQ       0       48       0       821.55137       0         1.022155       0.16616       PR       10       18       2       821.55837       0         1.022155       0.16616       PR       10       18       0       821.55837       0         1.022157       0.04154       R       19       35       1821.55780       0         1.02747       0.004154       R       0       47       0       821.5765       0         1.023178       0.20700       RQ       0       47       0       821.5765       0	821.03312 0.00002 RP 13 27 3 821.58867 0 821.03414 0.10350 RP 13 27 1 821.59225 0 821.05192 0.22344 RQ 0 45 2 821.59454 0 821.05451 0.05586 RQ 0 46 0 821.61109 0	821.06052 0.10112 PK 20 3/ 2 821.62395 0 821.06286 0.02528 RQ 0 44 2 821.62945 0 821.07862 0.05452 PR 11 20 3 821.63126 0 821.08118 0.21808 PR 11 20 1 821.64046 0 821.08118 0.21808 PR 11 20 1 821.64046 0	821.09288 0.08300 RQ 0 43 2 821.66332 0 821.11511 0.09817 RQ 0 44 0 821.67712 0 821.11803 0.19633 RP 14 29 2 821.68890 0 821.13012 0.00076 RP 14 29 0 821.69331 0	821.13020 0.20672 RQ 0 42 2 821.69617 0 821.13313 0.05168 RQ 0 43 0 821.70879 0 821.15816 0.04116 RQ 0 41 2 821.72820 0 821.16095 0.16464 PR 12 22 2 821.73710 0	821.17941 0.022320 NG 0 42 0 621.75938 0 821.17941 0.22320 NG 0 41 0 821.75938 0 821.1829 0.03304 PR 12 22 0 821.76772 0 821.21099 0.12944 RQ 0 41 0 821.76944 0 821.21429 0.03236 PR 21 39 3 821.78300 0	821.23303 0.1089/ KQ 0 39 2 821.78954 0. 821.23740 0.21793 RP 15 31 3 821.79454 0. 821.24827 0.0010 RP 15 31 1 821.79854 0. 821.27311 0.09580 RQ 0 40 0 821.79852 0. 821.27311 0.04790 RQ 0 38 2 821.81887 0.	821.29160 0.00077 RQ 0 39 0 821.82684 0. 821.29579 0.04908 PR 13 24 3 821.84601 0. 821.29968 0.19632 RQ 0 37 2 821.84726 0. 821.33884 0.06704 RQ 0 38 0 821.85428 0. 821.33650 0.06776 PR 13 24 1 871.85458 0.	821.36877 0.16480 RQ 0 36 2 821.87492 0. 821.37627 0.04120 RQ 0 37 0 821.88085 0. 821.41370 0.01108 RQ 0 35 2 821.90154 0. 821.413230 0.004132 RQ 0 35 2 821.90154 0. 821.4337 0.00008 RP 16 33 2 821.91094 0. 821.44347 0.00018 RP 16 33 0 821.91094 0. 821.44562 0.00420 RQ 0 34 2 821.91494 0.	821.444/54 0.12980 Kg 0 35 0 821.95168 0. 821.45330 0.06490 Rg 0 33 2 821.95249 0. 821.4789 0.00188 PR 14 26 2 821.95693 0. 821.49831 0.01390 Rg 0 32 2 821.97662 0.
WAVE NO INT K J S WAVE	0       1       820.88917       0.00024       RP       12       25       0       821.50235       0         3       0       820.99319       0.00568       RQ       0       49       0       821.50541       0         3       0       820.99319       0.00153       RQ       0       47       2       821.52203       0         3       0       820.93319       0.00153       RQ       0       47       2       821.52203       0         3       0       0.01797       0.02528       PR       10       18       2       821.53706       0         3       1       821.02175       0.10112       RQ       0       48       0       821.55137       0         5       2       821.02389       0.004154       RR       19       18       0       821.55780       0         5       2       821.02389       0.004154       RR       19       35       1       821.575680       0         5       2       821.02389       0.004154       RQ       0       47       0       821.575680       0         7       3       821.023178       0       0       <	0 821.03312 0.00002 RP 13 27 3 821.58867 0 1 821.03414 0.10350 RP 13 27 1 821.59225 0 2 821.05192 0.22344 RQ 0 45 2 821.59454 0 0 821.05451 0.05586 RQ 0 46 0 821.61109 0	Z 821.06052 0.10112 PK 20 3/ 2 821.62395 0 0 821.06286 0.02528 RQ 0 44 2 821.62945 0 3 821.07862 0.05452 PR 11 20 3 821.63126 0 1 821.08118 0.21808 PR 11 20 1 821.64046 0 3 821.09117 0 16600 R0 0 45 0 821.64046 0	1         821.09288         0.08300         RQ         0         43         2         821.65332         0           2         821.11511         0.09817         RQ         0         44         0         821.67712         0           0         821.11511         0.09817         RQ         0         44         0         821.67712         0           0         821.11803         0.19633         RP         14         29         821.68890         0           3         821.13012         0.00076         RP         14         29         821.69331         0	6 2 821.13020 0.20672 RQ 0 42 2 821.69617 0 6 0 821.13313 0.05168 RQ 0 43 0 821.70879 0 5 3 821.15816 0.04116 RQ 0 41 2 821.72820 0 5 1 821.16095 0.16464 PR 12 22 2 821.73710 0	3       5       1	0 2 821.23303 0.1089/ RQ 0 39 2 821.79494 0. 0 0 821.23740 0.21793 RP 15 31 3 821.79494 0. 9 3 821.24827 0.00010 RP 15 31 1 821.79839 0. 9 3 821.27007 0.09500 RQ 0 40 0 821.79832 0. 9 1 821.27311 0.04790 RQ 0 38 2 821.81887 0.	3 2 821.29160 0.00077 RQ 0 39 0 821.82684 0. 2 3 821.29579 0.04908 PR 13 24 3 821.84601 0. 2 1 821.29968 0.19632 RQ 0 37 2 821.84726 0. 1 2 821.33884 0.06704 RQ 0 38 0 821.85428 0. 1 2 831.33884 0.06704 RR 13 24 1 871 86167 0.	2 821.36877 0.16480 RQ 0 36 2 821.87492 0. 0 821.37627 0.04120 RQ 0 37 0 821.88085 0. 3 821.41370 0.01108 RQ 0 35 2 821.90154 0. 8 821.413230 0.004132 RQ 0 35 2 821.90154 0. 0 821.4332 0.00008 RP 16 33 2 821.91094 0. 3 821.44347 0.00018 RP 16 33 0 821.91094 0. 2 821.44562 0.00420 RQ 0 34 2 821.91494 0.	5 8 21.44774 0.12980 Kg 0 57 0 821.95168 0. 6 1 821.45330 0.06490 Rg 0 33 2 821.95249 0. 9 0 821.47785 0.00142 Rg 0 34 0 821.95593 0. 8 2 821.49831 0.01390 Rg 0 32 2 821.97662 0. 5 2 821.49831 0.01390 Rg 0 32 2 821.97662 0.
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S WAVE NO INT K J S WAVE NO I	$ \begin{array}{c} 7 & 1 & 824, 9553 & 1.94648 & Rq & 2 & 46 & 0 & 825. 26594 & 0 \\ 6 & 3 & 824, 95647 & 0.00744 & Rq & 20 & 33 & 8 & 825. 27376 & 0 \\ 5 & 3 & 824, 95658 & 0.000744 & Rq & 2 & 19 & 3 & 825. 27376 & 0 \\ 5 & 3 & 824, 95658 & 0.00040 & Rq & 20 & 3 & 8 & 825. 27376 & 0 \\ 5 & 1 & 824, 956796 & 1.49040 & Rq & 9 & 19 & 1 & 825. 27376 & 0 \\ 5 & 1 & 824, 956796 & 1.49040 & Rq & 1 & 1 & 825. 238129 & 0 \\ 6 & 3 & 824, 97610 & 0.00040 & Rq & 10 & 2 & 12 & 825. 33739 & 0 \\ 4 & 3 & 824, 97610 & 0.00040 & Rq & 10 & 2 & 14 & 2 & 825. 33713 & 0 \\ 5 & 2 & 824, 99761 & 0.00040 & Rq & 10 & 2 & 15 & 825. 37173 & 0 \\ 1 & 3 & 824, 99956 & 0.00080 & Rq & 2 & 14 & 2 & 825. 37173 & 0 \\ 3 & 3 & 824, 99956 & 0.01770 & Rq & 11 & 21 & 2 & 825. 44444 & 0 \\ 3 & 3 & 824, 99950 & 0.01770 & Rq & 11 & 21 & 2 & 825. 444357 & 0 \\ 3 & 3 & 824, 99950 & 0.01723 & 0.22310 & Rq & 2 & 14 & 2 & 825. 444357 & 0 \\ 3 & 3 & 824, 99950 & 0.01770 & Rq & 11 & 21 & 2 & 825. 444357 & 0 \\ 3 & 3 & 824, 99950 & 0.01770 & Rq & 11 & 21 & 2 & 825. 444357 & 0 \\ 3 & 3 & 824, 99950 & 0.01770 & Rq & 11 & 21 & 3 & 825. 444357 & 0 \\ 3 & 3 & 824, 99950 & 0.01804 & Rq & 2 & 44 & 2 & 825. 444357 & 0 \\ 3 & 3 & 824, 99950 & 0.01904 & Rq & 2 & 44 & 2 & 825. 444357 & 0 \\ 3 & 3 & 824, 99950 & 0.01904 & Rq & 2 & 42 & 2 & 825. 444357 & 0 \\ 3 & 3 & 825, 01440 & 0.46466 & Rq & 12 & 24 & 2 & 825. 444357 & 0 \\ 3 & 3 & 825, 01440 & 0.46466 & Rq & 1 & 2 & 12 & 2 & 825. 54429 & 0 \\ 3 & 3 & 825, 01440 & 0.46466 & Rq & 1 & 2 & 12 & 2 & 825. 5441357 & 0 \\ 3 & 3 & 825, 01440 & 0.46466 & Rq & 1 & 2 & 12 & 2 & 2 & 825. 5441357 & 0 \\ 3 & 3 & 825, 01440 & 0.46466 & Rq & 1 & 2 & 12 & 2 & 2 & 825. 544139 & 0 \\ 3 & 825, 01440 & 0.00320 & Rq & 1 & 2 & 2 & 2 & 825. 544139 & 0 \\ 3 & 3 & 825, 01430 & 0.003040 & Rq & 1 & 2 & 2 & 2 & 2 & 2 & 2 & 2 & 2 & 2$	2 4 5 5 5 5 5 5 4 5 3 0.09 / 2 4 7 2 3 8 2 8 2 9 5 9 5 9 1 0. 2 4 6 2 8 5 5 2 4 1 2 3 0.01 7 2 8 7 2 3 8 0 8 2 5 9 5 5 1 3 0. 2 4 0 2 8 2 5 2 5 9 7 8 0.00016 8 P 1 5 2 8 3 8 2 5 9 7 6 4 1 0.

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AVE NO INT K J S WAVE NO I	$\begin{array}{c} 827, 12894 & 0.01880 & \text{Rq} & 2 & 6 & 2 & 827, 62365 & 0 \\ 827, 15167 & 1.69920 & \text{Rq} & 4 & 11 & 0 & 827, 653486 & 0 \\ 827, 15905 & 0.42568 & \text{Rq} & 1 & 3 & 3 & 27, 64081 & 0 \\ 827, 24437 & 0.01176 & \text{Rp} & 1 & 3 & 3 & 27, 64081 & 0 \\ 827, 24437 & 0.01176 & \text{Rp} & 1 & 3 & 3 & 27, 64081 & 0 \\ 827, 24437 & 0.01176 & \text{Rp} & 1 & 3 & 827, 64081 & 0 \\ 827, 24437 & 0.00294 & \text{Rg} & 1 & 3 & 827, 64081 & 0 \\ 827, 24437 & 0.00294 & \text{Rg} & 1 & 3 & 827, 64081 & 0 \\ 827, 24437 & 0.00294 & \text{Rg} & 1 & 3 & 827, 64081 & 0 \\ 827, 24437 & 0.00294 & \text{Rg} & 1 & 3 & 827, 64081 & 0 \\ 827, 24471 & 0.00294 & \text{Rg} & 1 & 1 & 3 & 827, 65449 & 0 \\ 827, 29152 & 2.05208 & \text{Rq} & 2 & 3 & 0 & 827, 65449 & 0 \\ 827, 29152 & 2.05208 & \text{Rq} & 2 & 3 & 0 & 827, 65449 & 0 \\ 827, 29152 & 2.05508 & \text{Rq} & 2 & 3 & 0 & 827, 65449 & 0 \\ 827, 34518 & 0.00347 & \text{Rg} & 7 & 17 & 3 & 827, 65347 & 0 \\ 827, 34518 & 0.00347 & \text{Rg} & 7 & 17 & 3 & 827, 65347 & 0 \\ 827, 34518 & 0.00347 & \text{Rg} & 7 & 17 & 3 & 827, 65347 & 0 \\ 827, 31382 & 0.00347 & \text{Rg} & 7 & 17 & 3 & 827, 65347 & 0 \\ 827, 410481 & 0.554565 & \text{PR} & 9 & 19 & 0 & 827, 77346 & 0 \\ 827, 410481 & 0.554565 & \text{PR} & 9 & 19 & 2 & 827, 65347 & 0 \\ 827, 410481 & 0.554565 & \text{PR} & 7 & 17 & 3 & 827, 65347 & 0 \\ 827, 410494 & 0.554565 & \text{PR} & 7 & 17 & 3 & 827, 79373 & 0 \\ 827, 410494 & 0.554565 & \text{PR} & 1 & 7 & 3 & 827, 79373 & 0 \\ 827, 410494 & 0.554565 & \text{PR} & 1 & 9 & 2 & 1 & 827, 793749 & 0 \\ 827, 410494 & 0.554565 & \text{PR} & 1 & 9 & 27, 78343 & 0 \\ 827, 410494 & 0.554565 & \text{PR} & 1 & 9 & 27, 73374 & 0 \\ 827, 59251 & 0.00384 & \text{PR} & 1 & 827, 793759 & 0 \\ 827, 59251 & 0.00384 & \text{PR} & 1 & 9 & 27, 73374 & 0 \\ 827, 59424 & 0.047976 & \text{RP} & 1 & 2 & 827, 939522 & 0 \\ 827, 59424 & 0.047976 & \text{RP} & 1 & 1 & 25 & 3 & 827, 939528 & 0 \\ 827, 59424 & 0.04933 & \text{PR} & 1 & 2 & 827, 939728 & 0 \\ 827, 59424 & 0.04933 & \text{PR} & 1 & 2 & 827, 939362 & 0 \\ 827, 59424 & 0.04933 & \text{PR} & 1 & 2 & 827, 939362 & 0 \\ 827, 59424 & 0.049375 & 0 & 0 & 921 & 3 & 827, 939349 & 0 \\ 827, 59424 & 0.04$	827.61629 0.18308 RP 8 12 0 828.01497 0. 827.61657 0.17144 PR 12 27 0 828.06277 0. 827.61694 0.62473 PR 13 29 3 828.09082 0. 827.61879 0.73232 RP 9 14 3 828.09505 0. 827.61998 0.31237 RP 20 37 2 828.09669 0.
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NO INT KJSWAVENO I	3337       0.05567       RQ       9       29       1       845.73516         1005       0.02783       RQ       9       28       3       845.80644         0054       0.00020       RQ       9       28       3       845.80644         0317       0.00020       RQ       9       28       3       845.80544         0317       0.00010       RP       18       20       2       845.81107         1222       0.00013       RP       18       20       845.84058       107         1222       0.000142       RP       18       20       845.841291       107         2036       0.000142       RP       15       3       845.87193       16         2891       0.06833       RQ       9       27       1       845.88197       3         2853       0.034177       RQ       9       26       3       845.95122       3         1929       0.001177       RQ       9       26       3       845.95122       3	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	4.51 $0.02700$ $RI$ $9.21$ $846.2723$ $4.51$ $0.22800$ $RR$ $5$ $3$ $846.28655$ $692$ $0.12120$ $RR$ $5$ $3$ $846.28655$ $73$ $846.38955$ $0$ $796$ $0.56155$ $RR$ $5$ $7$ $846.30895$ $796$ $0.56155$ $RR$ $5$ $7$ $846.30895$ $018$ $1.68465$ $RR$ $5$ $7$ $846.31549$ $018$ $1.68465$ $RR$ $5$ $7$ $846.31549$ $026$ $0.96022$ $RR$ $9$ $20$ $846.33534$ $026$ $0.08692$ $RR$ $9$ $20$ $846.35734$ $026$ $0.08692$ $RR$ $9$ $20$ $846.35734$ $0093$ $0.50927$ $RR$ $144$ $846.389716$ $0093$ $0.50927$ $RR$ $19$ $846.387794$ $0069$ $0.7200$ $PR$ $1140$ $846.389779$ $0069$ $0.7200$ $800$ $0.25463$ $RQ$ $910$ $846.338738$ $946.438779$ $109$ $0.00018$ $RQ$ $919$ $846.338789$ $109$ $0.00018$ $RQ$ $919$ $846.438779$ $112$ $0.720378$ $RQ$ $919$ $846.415712$ $112$ $1.01232$ $RQ$ $918$ $846.42857$ $0069$ $0.17023$ $RR$ $934$ $446.445770$ $112$ $0.25308$ $RQ$ $918$ $846.428570$ $558$ $0.25308$ $RQ$
AVE NO INT K J S WAVE NO I	5.03337       0.05567       Rq       9       29       845.73516         5.10054       0.002783       Rq       9       28       345.80644         5.10054       0.00220       Rq       9       28       345.80644         5.10054       0.00020       Rq       9       28       345.80644         5.10317       0.00010       RP       18       20       845.81107         5.11222       0.00010       RP       18       20       845.84058         5.11222       0.000133       RP       18       20       845.84058         5.125036       0.000142       RR       15       3 845.861616       3         5.125036       0.000142       RR       15       3 845.88191       3         5.12503       0.030177       RQ       9       27       3 845.88197       3         5.13523       0.034177       RQ       9       26       3 845.95122       3       3	$\begin{array}{c} 0.17602 \ 0.01456 \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
ENO INT KJSWAVENO I	45.03337       0.05567       RQ       9       29       1       845.3516         45.04005       0.02783       RQ       9       28       3       845.80644         45.10054       0.00020       RQ       9       28       3       845.80644         45.10054       0.00020       RQ       9       28       3       845.80644         45.10317       0.00020       RP       18       20       845.81107       10         45.11222       0.00010       RP       18       20       845.84058       10       10         45.11222       0.000033       RP       18       20       845.841291       10       15       3       845.861616       15         45.1223       0.000042       RR       1       15       3       845.881616       16       15       15       15       15       15       16       15       16       15       13       16       15       16       16       15       16       16       17       16       16       16       16       16       16       16       16       17       16       16       16       16       16       16       16       16	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
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J S WAVE NO INT K J S WAVE NO I	37       3 845.03337       0.05567       RQ       9 29       845.03337         37       3 845.04005       0.02783       RQ       9 28       3 845.80644         27       3 845.10054       0.00020       RQ       9 28       3 845.80644         27       3 845.10054       0.00020       RQ       9 28       3 845.80644         27       1 845.10317       0.00010       RP       18 20       8 45.81107         27       1 845.11222       0.000133       RP       18 20       8 45.12936         45       8445.12036       0.00042       RR       1 15       3 845.86816         45       845.12891       0.06833       RQ       9 27       3 845.87193         36       1 845.12833       0.034177       RQ       9 27       3 845.95122	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$ \begin{array}{c} 277 & 3495.37457 \\ 373 & 3495.40692 \\ 373 & 3495.40692 \\ 373 & 3495.40692 \\ 373 & 346.38451 \\ 172 & 345.40692 \\ 0.06060 \\ 0 \\ 0.12120 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\$
S WAVE NO INT K J S WAVE NO I	9       37       3       845.03337       0.05567       RQ       9       29       1       845.73516         9       37       3       845.04005       0.02783       RQ       9       29       3       845.80644         21       27       3       845.10054       0.00020       RQ       9       28       3       845.80644         21       27       3       845.10317       0.00020       RQ       9       28       3       845.8107         21       27       1       845.10317       0.00010       RP       18       20       2       845.84058         15       47       3       845.1222       0.000033       RP       18       20       2       845.84058       10         14       45       3       845.1220       0.000042       RR       115       3       845.88167       3         9       36       1       845.1250       0.000042       RR       115       3       845.88167       3         9       36       1       845.1353       0.034177       RQ       9       2       3       445.95122       3       3       3       9       3 <t< td=""><td><math display="block"> \begin{array}{cccccccccccccccccccccccccccccccccccc</math></td><td><math display="block">\begin{array}{cccccccccccccccccccccccccccccccccccc</math></td></t<>	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
J S WAVE NO INT K J S WAVE NO I	0       9       37       8 445.03337       0.05567       RQ       9       29       1       8 45.03337       0.002783       RQ       9       28       3       8 45.03337       0.002783       RQ       9       28       3       8 45.80644       0.00278       RQ       9       28       1       8 45.80544       0.00278       RQ       9       28       1       8 45.81057       0.0027       RP       18       20       8 45.81057       0.0033       RP       18       20       0       8 45.1226       0.00033       RP       18       20       8 45.81657       0.0033       RP       18       27       3       8 45.86167       0.003416       11       15       3       445.86167       0.003416       11       15       3       445.86170       0.00042       RR       11       15       3       445.86170       0.00042       RR       11       15       3       445.86170       0.00042       18       15       16       17       18<	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$ \begin{array}{c} 277 & 3495.37457 \\ 373 & 3495.40692 \\ 373 & 3495.40692 \\ 373 & 3495.40692 \\ 373 & 346.38451 \\ 172 & 345.40692 \\ 0.06060 \\ 0 \\ 0.12120 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\$

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WAVE NO	849.49428 849.52661 849.52661 849.52661 849.52661 849.55603 849.55603 849.55603 849.55603 849.55603 849.55603 849.55618 849.55618 849.55618 849.95653 849.9733 849.97332 850.07444 850.07444 850.07734 850.07734 850.07734 850.07734 850.07734 850.07734 850.07734 850.07734 850.07734 850.07734 850.07734 850.07734 850.07734 850.0728 850.07237 850.73873 850.73873 850.73873 850.73873 850.73734 850.73873 850.73734 850.73734 850.73734 850.73734 850.73737 850.7734 850.7734 850.77347 850.77387 850.7737 850.77387 850.7747 870.7747 870.7747 870.7747 870.7747 870.7747 870.7747 870.7747 870.7747 870.7747 870.7747 870.7747 870.7747 870.7747 870.7747 870.7747 870.774
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WAVE NO	<ul> <li>8.896055</li> <li>8.91588</li> <li>8.91588</li> <li>8.91588</li> <li>8.91588</li> <li>8.91588</li> <li>8.95555</li> <li>8.955555</li> <li>8.955555</li> <li>8.955555</li> <li>8.955555<!--</td--></li></ul>
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х ш	<b>863.60729</b> <b>863.60729</b> <b>1863.60729</b> <b>1863.61646</b> <b>1863.62493</b> <b>1863.62493</b> <b>1863.62493</b> <b>1863.65493</b> <b>0863.61214</b> <b>1863.65499</b> <b>1863.65499</b> <b>1863.65499</b> <b>2863.72385</b> <b>0863.72385</b> <b>0863.72385</b> <b>0863.72385</b> <b>0863.72385</b> <b>0863.72385</b> <b>0863.72385</b> <b>0863.73326</b> <b>0863.73326</b> <b>0863.73326</b> <b>0863.73326</b> <b>0863.73326</b> <b>0863.73326</b> <b>0863.73326</b> <b>0863.73326</b> <b>0863.73326</b> <b>0863.73326</b> <b>0863.73326</b> <b>0863.73326</b> <b>0863.73326</b> <b>0863.73326</b> <b>0863.73326</b> <b>0863.73326</b> <b>0863.73326</b> <b>0863.73326</b> <b>0863.73326</b> <b>0863.73326</b> <b>0863.73326</b> <b>0863.73326</b> <b>0863.73326</b> <b>0863.735666</b> <b>000</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b> <b>100</b>	<ul> <li>2 863.78947</li> <li>2 863.84965</li> <li>3 863.849657</li> <li>3 863.849657</li> <li>3 863.86557</li> <li>3 863.865956</li> <li>3 863.985906</li> <li>3 863.987906</li> <li>3 863.91695</li> <li>3 863.91695</li> <li>3 863.9148</li> <li>3 863.9148</li> <li>3 863.914378</li> <li>0 864.014378</li> <li>0 864.09828</li> <li>0 864.09828</li> <li>0 864.09828</li> <li>0 864.09828</li> <li>0 864.109373</li> <li>0 864.109373</li> <li>0 864.109373</li> <li>0 864.109373</li> <li>0 864.2193</li> <li>0 864.2193</li> <li>0 864.2193</li> <li>0 864.2193</li> <li>0 864.2193</li> <li>0 864.23550</li> <li>0 864.27350</li> <li>0 864.27350</li> </ul>	<ul> <li>2 864, 45374</li> <li>2 864, 45374</li> <li>3 864, 45372</li> <li>0 864, 48117</li> <li>0 864, 48117</li> <li>0 864, 48724</li> <li>1 864, 5144724</li> <li>1 864, 57394</li> <li>0 864, 68378</li> </ul>
WAVE N	17       3       863.60729         29       3       863.60729         29       3       863.61046         29       3       863.61046         29       3       863.61046         29       3       863.6113         14       863.6113       0         14       863.6124       1         14       863.6124       1         14       863.6124       1         14       863.6124       1         15       863.6124       1         16       863.6124       1         16       863.7519       0         16       863.77385       0         16       863.72385       0         17       2       863.73307         27       2       863.73307         20       863.733327       0         21       2       863.73307	40       863.78947         47       2863.85557         12       863.85557         12       863.8557         12       863.8557         12       863.8557         12       863.8557         12       863.8557         12       863.8557         12       863.8557         12       863.8557         12       863.8557         12       863.8557         12       863.85657         12       863.9505         138       863.9505         138       863.970         138       863.970         138       864.0554         146       864.0554         136       864.0554         145       864.0554         15       864.10571         16       864.10571         170       864.10571         19       864.27695         10       864.27936         110       864.27936         12       864.27936	443       6       644, 34574       0         443       6       644, 45341       0         442       0       864, 45341       0         442       0       864, 45341       0         442       0       864, 45341       0         19       2       864, 45341       0         19       2       864, 45341       0         19       2       864, 45341       0         19       2       864, 45172       1         11       2       864, 51472       1         14       1       864, 57394       0         441       0       864, 51372       1         133       2       864, 633792       0         333       2       864, 633792       0         333       2       864, 633792       0
WAVE N	15       17       3       863.60729       0         15       17       3       863.60766       0         15       17       3       863.60766       0         1       29       3       863.60769       0         1       29       3       863.60769       0         1       29       3       863.61244       0         5       42       1       863.62493       0         8       14       2       863.61214       1         8       14       2       863.61214       1         8       14       2       863.657490       0         15       16       3       863.657490       0         15       16       3       863.72183       0         15       16       1       863.72183       0         16       48       2       863.72183       0         16       48       0       863.73307       0         2       2       0       863.73307       0         16       49       2       863.73307       0         2       2       0       863.73307       0	4       40       0       863.78947       0         16       47       2       863.84963       0         9       12       3       853.84963       0         9       12       3       853.8555       0         9       12       3       853.85655       0         9       12       3       853.85655       0         3       25       3       863.8555       0         3       25       3       853.9515       0         3       25       3       853.9516       0         3       38       3       3       3       3         3       38       3       3       3       3         3       38       3       3       3       3         3       38       3       3       3       3       3         3       38       3       3       3       3       3       3         3       38       38       0       3       3       3       3       3       3       3       3       3       3       3       3       3       3       3       3 <t< td=""><td>16       43       5       504, 345, 14         16       42       2       864, 45, 345, 14         16       42       2       864, 46072       0         16       42       2       864, 48117       0         7       47       3       864, 48117       0         6       19       2       864, 48117       0         6       19       2       864, 48117       0         16       41       2       864, 56693       0         16       41       2       864, 56693       0         16       41       2       864, 57394       0         16       41       2       864, 633792       0         16       45       2       864, 633792       0         16       45       2       864, 633792       0         0       33       2       864, 633792       0         0       33       2       864, 633792       0         0       33       2       864, 633792       0         0       33       2       864, 633792       0</td></t<>	16       43       5       504, 345, 14         16       42       2       864, 45, 345, 14         16       42       2       864, 46072       0         16       42       2       864, 48117       0         7       47       3       864, 48117       0         6       19       2       864, 48117       0         6       19       2       864, 48117       0         16       41       2       864, 56693       0         16       41       2       864, 56693       0         16       41       2       864, 57394       0         16       41       2       864, 633792       0         16       45       2       864, 633792       0         16       45       2       864, 633792       0         0       33       2       864, 633792       0         0       33       2       864, 633792       0         0       33       2       864, 633792       0         0       33       2       864, 633792       0
WAVE N	15       17       3       863.60729       0         15       17       3       863.60766       0         15       17       3       863.60766       0         1       29       3       863.60769       0         1       29       3       863.60769       0         1       29       3       863.61946       0         5       42       1       863.62493       0         8       14       2       863.61214       1         8       14       2       863.61214       1         8       14       2       863.657490       0         15       16       3       863.657490       0         15       16       3       863.72183       0         15       16       1       863.72183       0         16       48       2       863.72183       0         16       48       0       863.73307       0         2       2       0       863.73307       0         16       49       2       863.73307       0         2       2       0       863.73307       0	4       40       863.78947         6       47       2       863.84963         6       47       2       863.84963       0         9       12       3       853.84963       0         9       12       3       863.84963       0         9       12       3       863.84963       0         3       3       3       853.86655       1         3       25       3       863.86905       1         3       25       3       863.86805       0         3       25       3       863.98822       0         3       25       3       863.99148       0         3       25       3       863.99148       0         3       38       3       863.99148       0         3       38       3       863.99148       0         3       38       3       863.99148       0         3       38       3864.04378       0       0         2       36       364.04378       0       0         2       36       364.06540       0       0         2       364.0709828 <td>16       43       5       504, 345, 14         16       42       2       864, 45, 345, 14         16       42       2       864, 46072       0         16       42       2       864, 48117       0         7       47       3       864, 48117       0         6       19       2       864, 48117       0         6       19       2       864, 48117       0         16       41       2       864, 56693       0         16       41       2       864, 56693       0         16       41       2       864, 57394       0         16       41       2       864, 633792       0         16       45       2       864, 633792       0         16       45       2       864, 633792       0         0       33       2       864, 633792       0         0       33       2       864, 633792       0         0       33       2       864, 633792       0         0       33       2       864, 633792       0</td>	16       43       5       504, 345, 14         16       42       2       864, 45, 345, 14         16       42       2       864, 46072       0         16       42       2       864, 48117       0         7       47       3       864, 48117       0         6       19       2       864, 48117       0         6       19       2       864, 48117       0         16       41       2       864, 56693       0         16       41       2       864, 56693       0         16       41       2       864, 57394       0         16       41       2       864, 633792       0         16       45       2       864, 633792       0         16       45       2       864, 633792       0         0       33       2       864, 633792       0         0       33       2       864, 633792       0         0       33       2       864, 633792       0         0       33       2       864, 633792       0
WAVE N	0.03407       RQ       15       17       3       863.60729       0         0.01703       RQ       15       17       3       863.60729       0         0.05040       RR       15       17       3       863.60729       0         0.03020       RR       1       29       3       863.60729       0         0.03020       RR       1       29       3       863.61646       0         0.033020       RR       1       29       3       863.62493       0         0.03940       PR       5       42       1       863.62493       0         0.03940       PR       8       14       2       863.644940       0         0.03368       RR       8       14       2       863.654990       0         0.039527       RQ       15       16       863.654990       0         0.02650       RR       2       27       2       863.72385       0         0.02650       RR       16       48       863.772385       0       0       0         0.10600       RR       2       27       2       863.772385       0       0       0 </td <td>0.04782       PR       4       0       663.78947         0.19128       RQ       16       47       2       863.8555       1         0.05720       RQ       16       47       0       863.8555       1         0.02860       RR       9       12       863.8555       1         0.26128       RR       9       12       863.8555       1         0.26128       RR       9       12       863.8555       1         0.03160       RR       9       12       863.8555       1         0.03160       PR       3       25       3       863.91695       0         0.03160       PR       3       25       3       863.9149       0       0         0.03161       PR       3       38       3       3833.91695       0       0         0.03143       RQ       16       46       864.04378       0<td><math display="block">\begin{array}{cccccccccccccccccccccccccccccccccccc</math></td></td>	0.04782       PR       4       0       663.78947         0.19128       RQ       16       47       2       863.8555       1         0.05720       RQ       16       47       0       863.8555       1         0.02860       RR       9       12       863.8555       1         0.26128       RR       9       12       863.8555       1         0.26128       RR       9       12       863.8555       1         0.03160       RR       9       12       863.8555       1         0.03160       PR       3       25       3       863.91695       0         0.03160       PR       3       25       3       863.9149       0       0         0.03161       PR       3       38       3       3833.91695       0       0         0.03143       RQ       16       46       864.04378       0 <td><math display="block">\begin{array}{cccccccccccccccccccccccccccccccccccc</math></td>	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
T K J S WAVE N	718       0.03407       RQ       15       17       3       863.60729       0         309       0.01703       RQ       15       17       3       863.60729       0         309       0.006040       RR       15       17       3       863.60729       0         784       0.03940       RR       1       29       3       863.61946       0         784       0.03940       PR       1       29       3       863.6193       0         6519       0.03940       PR       5       42       1       863.6193       0         721       0.3540       PR       8       14       2       863.64214       1         723       0.3568       RR       8       14       2       863.64214       1         731       0.01970       RR       8       14       2       863.64214       1         733       0.2257       RQ       15       16       1       863.65719       0         433       0.02257       RQ       15       16       1       863.72385       0         239       0.02550       RQ       15       16       2       <	965       0.04782       PR       4       40       0       863.78947       0         221       0.19128       RQ       16       47       2       863.84965       1         201       0.05720       RQ       16       47       0       863.84965       1         367       1.04512       RR       9       12       3       863.85906       0         367       1.04512       RR       9       12       3       863.86906       0         367       1.04512       RR       9       12       3       863.86906       0         367       1.04512       RR       3       25       3       863.99169       0         367       1.04512       RR       3       25       3       863.99169       0         367       1.04512       RR       3       25       3       863.99169       0         367       0.05807       RR       3       25       3       863.99169       0         370       0       0.05307       RR       16       46       863.99169       0         371       0       0.01688       RQ       16       66	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
ENO INT KJSWAVEN	<ul> <li>.65718 0.03407 RQ 15 17 3 863.60729 0</li> <li>.65718 0.01703 RQ 15 17 1 863.60729 0</li> <li>.70309 0.06040 RR 1 29 3 863.61646 0</li> <li>.71784 0.03020 RR 1 29 1 863.62493 0</li> <li>.74234 0.03940 PR 5 42 1 863.62493 0</li> <li>.74619 0.01970 RR 8 14 2 863.64293 0</li> <li>.74619 0.01970 RR 8 14 2 863.64293 0</li> <li>.81721 0.83688 RR 8 14 0 863.64293 0</li> <li>.82481 0.01970 RR 8 14 0 863.65499 0</li> <li>.82481 0.0257 RQ 15 16 1 863.65499 0</li> <li>.82481 0.02257 RQ 15 48 2 863.72385 0</li> <li>.82239 0.02650 RR 2 72 863.73328 0</li> <li>.90470 0.05107 RR 2 27 0 863.73328 0</li> </ul>	$\begin{array}{c} .92965 \ 0.04782 \\ .94021 \ 0.19128 \\ RQ \ 16 \ 47 \ 2863.84963 \\ .98201 \ 0.05720 \\ RQ \ 16 \ 47 \ 2863.84965 \\ .98206 \\ .99964 \ 0.02860 \\ RR \ 912 \\ .863.8655 \\ .91367 \ 1.04512 \\ RR \ 912 \\ .863.98822 \\ .912 \\ .91389 \\ .912 \\ .91389 \\ .912 \\ .91389 \\ .912 \\ .91389 \\ .912 \\ .91389 \\ .912 \\ .913 \\ .914 \\ .913 \\ .913 \\ .913 \\ .914 \\ .913 \\ .913 \\ .914 \\ .913 \\ .913 \\ .914 \\ .913 \\ .914 \\ .913 \\ .914 \\ .913 \\ .914 \\ .913 \\ .914 \\ .913 \\ .914 \\ .913 \\ .914 \\ .913 \\ .914 \\ .913 \\ .914 \\ .913 \\ .914 \\ .9$	$\begin{array}{c} 1000000000000000000000000000000000000$
NO INT KJSWAVEN	62.65718       0.03407       RQ       15       17       3       863.60729       0         622.65718       0.01703       RQ       15       17       3       863.60729       0         622.65718       0.01703       RQ       15       17       3       863.60729       0         622.70309       0.06040       RR       1       29       3       863.61646       0         52.71784       0.03020       RR       1       29       3       863.61493       0         52.71784       0.03020       RR       1       29       3       863.61493       0         52.74234       0.03320       RR       1       29       1       863.62493       0         52.74639       0.0352       RR       8       14       2       863.64490       0         52.74639       0.0352       RR       1       2       863.64490       0 <td>52.92965       0.04782       PR       4       0       0       663.78947       0         52.98201       0.05720       RQ       16       47       2       863.84963       0         52.98201       0.05720       RQ       16       47       2       863.84965       1         52.98201       0.05260       RQ       16       47       0       863.855       1         53.09544       0.02860       RR       9       12       863.8655       1         53.01367       1.04512       RR       9       12       863.8655       1         53.05984       0.03160       PR       3       25       3       863.9916       0         53.05984       0.03160       PR       3       25       3       863.9140       0         53.05984       0.03160       PR       3       25       3       863.9140       0         53.19760       0.03161       PR       3       25       864.06540       0         53.13761       0.00142       PR       2       3       863.916950       0         53.137761       0.00142       PR       2       864.06540       0       0<td><math display="block">\begin{array}{c} 3.47223 &amp; 1.47292 &amp; 704 &amp; 104 &amp; 306 &amp; 134702 \\ 3.414818 &amp; 0.07880 &amp; 704 &amp; 164 &amp; 36444 &amp; 34502 \\ 3.45087 &amp; 0.03867 &amp; 70334 &amp; 1642 &amp; 2864457341 &amp; 0.\\ 3.45087 &amp; 0.00367 &amp; 70333 &amp; 747 &amp; 386446072 &amp; 0.\\ 3.550648 &amp; 0.03367 &amp; 787 &amp; 619 &amp; 286446072 &amp; 0.\\ 3.550648 &amp; 0.0333 &amp; 747 &amp; 196451417 &amp; 0.\\ 3.551229 &amp; 0.00733 &amp; 7747 &amp; 18644514420 &amp; 1.\\ 3.55701 &amp; 0.06593 &amp; 7747 &amp; 1864457394 &amp; 0.\\ 3.55701 &amp; 0.063360 &amp; 704 &amp; 1641 &amp; 286465693 &amp; 0.\\ 3.55701 &amp; 0.063360 &amp; 704 &amp; 1641 &amp; 286465693 &amp; 0.\\ 3.55946 &amp; 0.03180 &amp; 787 &amp; 645 &amp; 286466693 &amp; 0.\\ 3.55946 &amp; 0.03180 &amp; 786 &amp; 1641 &amp; 28646673794 &amp; 0.\\ 3.55946 &amp; 0.03180 &amp; 786 &amp; 1641 &amp; 28646673794 &amp; 0.\\ 3.55946 &amp; 0.03180 &amp; 786 &amp; 16447 &amp; 28646673794 &amp; 0.\\ 3.55946 &amp; 0.00318 &amp; 716 &amp; 10286466666 &amp; 0.\\ 3.55946 &amp; 0.00318 &amp; 716 &amp; 1028646667806 &amp; 0.\\ 3.55946 &amp; 0.00310 &amp; 78 &amp; 0 &amp; 33 &amp; 2864667806 &amp; 0.\\ 3.60125 &amp; 0.00010 &amp; 78 &amp; 0 &amp; 33 &amp; 2864667806 &amp; 0.\\ 3.60125 &amp; 0.00010 &amp; 78 &amp; 0 &amp; 33 &amp; 2864667806 &amp; 0.\\ 3.60125 &amp; 0.00010 &amp; 78 &amp; 0 &amp; 33 &amp; 2864667806 &amp; 0.\\ 3.60125 &amp; 0.00010 &amp; 78 &amp; 0 &amp; 33 &amp; 08646633766 &amp; 0.\\ 3.60125 &amp; 0.00010 &amp; 78 &amp; 0 &amp; 33 &amp; 0864667806 &amp; 0.\\ 3.60125 &amp; 0.00010 &amp; 78 &amp; 0 &amp; 33 &amp; 0864663378 &amp; 0.\\ 3.60125 &amp; 0.00010 &amp; 78 &amp; 0 &amp; 33 &amp; 0864663378 &amp; 0.\\ 3.60125 &amp; 0.00010 &amp; 78 &amp; 0 &amp; 33 &amp; 0864663378 &amp; 0.\\ 3.60125 &amp; 0.00010 &amp; 78 &amp; 0 &amp; 33 &amp; 0864663378 &amp; 0.\\ 3.60125 &amp; 0.00010 &amp; 78 &amp; 0 &amp; 33 &amp; 08646633766 &amp; 0.\\ 3.60125 &amp; 0.00010 &amp; 78 &amp; 0 &amp; 33 &amp; 0864663378 &amp; 0.\\ 3.60125 &amp; 0.00010 &amp; 78 &amp; 0 &amp; 33 &amp; 0864663378 &amp; 0.\\ 3.60125 &amp; 0.00010 &amp; 76 &amp; 0 &amp; 33 &amp; 0864663378 &amp; 0.\\ 3.60125 &amp; 0.00010 &amp; 76 &amp; 0 &amp; 33 &amp; 0864663378 &amp; 0.\\ 3.60125 &amp; 0.00010 &amp; 76 &amp; 000000 &amp; 76 &amp; 0000000 &amp; 000000 &amp; 000000 &amp; 000000 &amp; 000000</math></td></td>	52.92965       0.04782       PR       4       0       0       663.78947       0         52.98201       0.05720       RQ       16       47       2       863.84963       0         52.98201       0.05720       RQ       16       47       2       863.84965       1         52.98201       0.05260       RQ       16       47       0       863.855       1         53.09544       0.02860       RR       9       12       863.8655       1         53.01367       1.04512       RR       9       12       863.8655       1         53.05984       0.03160       PR       3       25       3       863.9916       0         53.05984       0.03160       PR       3       25       3       863.9140       0         53.05984       0.03160       PR       3       25       3       863.9140       0         53.19760       0.03161       PR       3       25       864.06540       0         53.13761       0.00142       PR       2       3       863.916950       0         53.137761       0.00142       PR       2       864.06540       0       0 <td><math display="block">\begin{array}{c} 3.47223 &amp; 1.47292 &amp; 704 &amp; 104 &amp; 306 &amp; 134702 \\ 3.414818 &amp; 0.07880 &amp; 704 &amp; 164 &amp; 36444 &amp; 34502 \\ 3.45087 &amp; 0.03867 &amp; 70334 &amp; 1642 &amp; 2864457341 &amp; 0.\\ 3.45087 &amp; 0.00367 &amp; 70333 &amp; 747 &amp; 386446072 &amp; 0.\\ 3.550648 &amp; 0.03367 &amp; 787 &amp; 619 &amp; 286446072 &amp; 0.\\ 3.550648 &amp; 0.0333 &amp; 747 &amp; 196451417 &amp; 0.\\ 3.551229 &amp; 0.00733 &amp; 7747 &amp; 18644514420 &amp; 1.\\ 3.55701 &amp; 0.06593 &amp; 7747 &amp; 1864457394 &amp; 0.\\ 3.55701 &amp; 0.063360 &amp; 704 &amp; 1641 &amp; 286465693 &amp; 0.\\ 3.55701 &amp; 0.063360 &amp; 704 &amp; 1641 &amp; 286465693 &amp; 0.\\ 3.55946 &amp; 0.03180 &amp; 787 &amp; 645 &amp; 286466693 &amp; 0.\\ 3.55946 &amp; 0.03180 &amp; 786 &amp; 1641 &amp; 28646673794 &amp; 0.\\ 3.55946 &amp; 0.03180 &amp; 786 &amp; 1641 &amp; 28646673794 &amp; 0.\\ 3.55946 &amp; 0.03180 &amp; 786 &amp; 16447 &amp; 28646673794 &amp; 0.\\ 3.55946 &amp; 0.00318 &amp; 716 &amp; 10286466666 &amp; 0.\\ 3.55946 &amp; 0.00318 &amp; 716 &amp; 1028646667806 &amp; 0.\\ 3.55946 &amp; 0.00310 &amp; 78 &amp; 0 &amp; 33 &amp; 2864667806 &amp; 0.\\ 3.60125 &amp; 0.00010 &amp; 78 &amp; 0 &amp; 33 &amp; 2864667806 &amp; 0.\\ 3.60125 &amp; 0.00010 &amp; 78 &amp; 0 &amp; 33 &amp; 2864667806 &amp; 0.\\ 3.60125 &amp; 0.00010 &amp; 78 &amp; 0 &amp; 33 &amp; 2864667806 &amp; 0.\\ 3.60125 &amp; 0.00010 &amp; 78 &amp; 0 &amp; 33 &amp; 08646633766 &amp; 0.\\ 3.60125 &amp; 0.00010 &amp; 78 &amp; 0 &amp; 33 &amp; 0864667806 &amp; 0.\\ 3.60125 &amp; 0.00010 &amp; 78 &amp; 0 &amp; 33 &amp; 0864663378 &amp; 0.\\ 3.60125 &amp; 0.00010 &amp; 78 &amp; 0 &amp; 33 &amp; 0864663378 &amp; 0.\\ 3.60125 &amp; 0.00010 &amp; 78 &amp; 0 &amp; 33 &amp; 0864663378 &amp; 0.\\ 3.60125 &amp; 0.00010 &amp; 78 &amp; 0 &amp; 33 &amp; 0864663378 &amp; 0.\\ 3.60125 &amp; 0.00010 &amp; 78 &amp; 0 &amp; 33 &amp; 08646633766 &amp; 0.\\ 3.60125 &amp; 0.00010 &amp; 78 &amp; 0 &amp; 33 &amp; 0864663378 &amp; 0.\\ 3.60125 &amp; 0.00010 &amp; 78 &amp; 0 &amp; 33 &amp; 0864663378 &amp; 0.\\ 3.60125 &amp; 0.00010 &amp; 76 &amp; 0 &amp; 33 &amp; 0864663378 &amp; 0.\\ 3.60125 &amp; 0.00010 &amp; 76 &amp; 0 &amp; 33 &amp; 0864663378 &amp; 0.\\ 3.60125 &amp; 0.00010 &amp; 76 &amp; 000000 &amp; 76 &amp; 0000000 &amp; 000000 &amp; 000000 &amp; 000000 &amp; 000000</math></td>	$\begin{array}{c} 3.47223 & 1.47292 & 704 & 104 & 306 & 134702 \\ 3.414818 & 0.07880 & 704 & 164 & 36444 & 34502 \\ 3.45087 & 0.03867 & 70334 & 1642 & 2864457341 & 0.\\ 3.45087 & 0.00367 & 70333 & 747 & 386446072 & 0.\\ 3.550648 & 0.03367 & 787 & 619 & 286446072 & 0.\\ 3.550648 & 0.0333 & 747 & 196451417 & 0.\\ 3.551229 & 0.00733 & 7747 & 18644514420 & 1.\\ 3.55701 & 0.06593 & 7747 & 1864457394 & 0.\\ 3.55701 & 0.063360 & 704 & 1641 & 286465693 & 0.\\ 3.55701 & 0.063360 & 704 & 1641 & 286465693 & 0.\\ 3.55946 & 0.03180 & 787 & 645 & 286466693 & 0.\\ 3.55946 & 0.03180 & 786 & 1641 & 28646673794 & 0.\\ 3.55946 & 0.03180 & 786 & 1641 & 28646673794 & 0.\\ 3.55946 & 0.03180 & 786 & 16447 & 28646673794 & 0.\\ 3.55946 & 0.00318 & 716 & 10286466666 & 0.\\ 3.55946 & 0.00318 & 716 & 1028646667806 & 0.\\ 3.55946 & 0.00310 & 78 & 0 & 33 & 2864667806 & 0.\\ 3.60125 & 0.00010 & 78 & 0 & 33 & 2864667806 & 0.\\ 3.60125 & 0.00010 & 78 & 0 & 33 & 2864667806 & 0.\\ 3.60125 & 0.00010 & 78 & 0 & 33 & 2864667806 & 0.\\ 3.60125 & 0.00010 & 78 & 0 & 33 & 08646633766 & 0.\\ 3.60125 & 0.00010 & 78 & 0 & 33 & 0864667806 & 0.\\ 3.60125 & 0.00010 & 78 & 0 & 33 & 0864663378 & 0.\\ 3.60125 & 0.00010 & 78 & 0 & 33 & 0864663378 & 0.\\ 3.60125 & 0.00010 & 78 & 0 & 33 & 0864663378 & 0.\\ 3.60125 & 0.00010 & 78 & 0 & 33 & 0864663378 & 0.\\ 3.60125 & 0.00010 & 78 & 0 & 33 & 08646633766 & 0.\\ 3.60125 & 0.00010 & 78 & 0 & 33 & 0864663378 & 0.\\ 3.60125 & 0.00010 & 78 & 0 & 33 & 0864663378 & 0.\\ 3.60125 & 0.00010 & 76 & 0 & 33 & 0864663378 & 0.\\ 3.60125 & 0.00010 & 76 & 0 & 33 & 0864663378 & 0.\\ 3.60125 & 0.00010 & 76 & 000000 & 76 & 0000000 & 000000 & 000000 & 000000 & 000000$
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JSWAVENO INT KJSWAVEN	<b>31 3 862.65718 0.03407 RQ 15 17 3 863.60729 0</b> <b>37 3 862.65718 0.01703 RQ 15 17 3 863.60729 0</b> <b>37 3 862.70309 0.06040 RR 1 29 3 863.61646 0</b> <b>37 3 862.71784 0.03020 RR 1 29 1 863.62493 0</b> <b>30 3 862.74234 0.03940 PR 5 42 1 863.62493 0</b> <b>30 3 862.74234 0.03940 PR 5 42 1 863.62493 0</b> <b>30 3 862.74619 0.01970 RR 8 14 2 863.64214 1</b> <b>22 2 862.81721 0.83688 RR 8 14 2 863.64290 0</b> <b>22 862.81721 0.83688 RR 8 14 0 863.64290 0</b> <b>23 862.82380 0.209222 RQ 15 16 3 863.65490 0</b> <b>29 3 862.82381 0.029222 RQ 15 16 3 863.65490 0</b> <b>29 1 862.82851 0.02257 RQ 15 48 2 863.72385 0</b> <b>35 2 862.84187 0.10600 RR 2 863.72385 0</b> <b>38 62.84187 0.10600 RR 2 27 2 863.73328 0</b> <b>38 62.90420 0.02553 PR 4 40 2 863.73328 0</b> <b>28 1 862.90420 0.02553 PR 4 40 2 863.7336560 0</b> <b>29 1 862.90420 0.02553 PR 4 40 2 863.7336560 0</b> <b>20 862.90420 0.02553 PR 4 40 2 863.7336560 0</b> <b>29 1 862.90420 0.02553 PR 4 40 2 863.7336560 0</b> <b>20 862.90420 0.02553 PR 4 40 2 863.73328 0</b> <b>20 1 862.90420 0.02553 PR 4 40 2 863.73365660 0</b> <b>20 1 862.90420 0.02553 PR 4 40 2 863.73365660 0</b> <b>20 1 862.90420 0.02553 PR 4 40 2 863.73365</b>	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$
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## **BIBLIOGRAPHIC DATA SHEET**

<b>1. Report No.</b> TM-85108	2. Government Accession No.	3. Recipient's Catalog No.			
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Infrared and Radio Greenbelt, Maryland	Astronomy Branch	14. Sponsoring Agency Code 693			
Solar Telescope 1-metre Fourier Transform interferometer at Kitt Peak National Observatory and tunable diode laser spectrometers at the University of Tennessee and NASA/Goddard Space Flight Center. Over 2000 individual vibration-rotation transitions were analyzed taking into account many higher order effects including torsional splitting. Line positions were reproduced to better than 0.001 cm <sup>-1</sup> . Both ground and upper state molecular constants were determined in the analysis. Part I of this document contains a discussion of the experimental details, the analysis procedures and the results. A list of ethane transitions occurring					
near $^{14}CO_2$ laser lines needed for heterodyne searches for $C_2H_6$ in extraterrestria sources is also included.					
Part II contains a spectral catalogue of the ethane $v_9$ fundamental from 765 cm <sup>-1</sup> to 900 cm <sup>-1</sup> . The contents include: (a) a high dispersion (1 cm <sup>-1</sup> / 12 in.) plot of both the Kitt Peak interferometric data and a simulated spectrum with Doppler-limited resolution using the model of Part I; (b) a table of over 8500 calculated transitions listed quantum number assignments, frequencies and intensities.					
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