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ALESEP: A Computer Program for the Analysis of Airfoil Leading Edge Separation Bubbles

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FIGURES

APPENDIX A - SAMPLE CASE

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ALESEP: A Computer Program for the Analysis of Airfoil Leading Edge Separation Bubbles

SUMMAR Y

A program called ALESEP is presented for the analysis of the inviscidviscous interaction which occurs due to the presence of a closed laminartransitional separation bubble on an airfoil. The ALESEP code provides an iterative solution of the boundary layer equations expressed in an inverse formulation coupled to a Cauchy integral representation of the inviscid flow. This interaction analysis is treated as a local perturbation to a known solution obtained from a global airfoil analysis; hence, part of the required input to the ALESEP code are the reference displacement thickness and tangential velocity distributions. Special windward differencing may be used in the reversed flow regions of the separation bubble to accurately account for the flow direction in the discretization of the streamwise convection of momentum. The ALESEP code contains both a forced transition model based on a streamwise intermittency function and a natural transition model based on a solution of the integral form of the turbulent kinetic energy equation. Instructions for the input, output, and program usage are given herein along with a sample case.

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a	Structural coefficient
С	Airfoil chord
°f	Skin friction coefficient
D	Damping factor applied to mixing and dissipation lengths
Ĩ	Perturbation stream function
F	Velocity ratio, u/u _e
g	Total enthalpy ratio, H/H _e
H	Total enthalpy
l	Mixing length or ratio of local to edge density * molecular viscosity product
L	Reference length or dissipation length
m	Perturbation mass flow
n	Coordinate normal to reference displacement surface
N	Coordinate measured normal to reference displacement surface from the body surface
Pr	Prandtl number
PrT	Turbulent Prandtl number
q	Magnitude of fluctuating velocities
Re	Reference Reynolds number
\mathbf{Re}_{θ}	Local momentum thickness Reynolds number
κ _θ	Correlated momentum thickness Reynolds number
R _τ	Turbulent Reynolds number
s,S	Coordinates along reference displacement surface
Tu	Turbulence level
u	Velocity component parallel to reference displacement surface
v	Velocity component normal to reference displacement surface

V	Transformed normal velocity in Prandtl transposition theorem
α	Windward differencing weighting operator
β	Pressure gradient parameter
δ	Boundary layer thickness
6 *	Displacement thickness
δτ	Stress thickness
ε	Eddy viscosity coefficient
ĸ	von Karman constant
η	Transformed normal coordinate
ν	Kinematic viscosity coefficient
μ	Molecular viscosity coefficient
ξ	Transformed tangential coordinate
φ	Velocity potential
ρ	Density
ψ	Stream function
ω	Interaction relaxation parameter
Subscri	ots
e	Edge of boundary layer
I	Inviscid
ref	Reference solution
t ₁	Start of transition
t ₂	End of transition
T	Turbulent

- v Viscous
- $^{\infty}$ Free stream
- 1 Start of interaction region

ţ

End of interaction region

<u>Superscripts</u>

- Perturbation quantity
- + Inner wall non-dimensionalized coordinate
- k Global inviscid-viscous iteration counter

Introduction

It was pointed out by Tani (Ref. 1) that airfoils at moderate incidence angles, prior to either leading edge stall or thin airfoil stall, experience local separation bubbles just downstream of the peak suction (minimum pressure) regions. Figure 1 shows a schematic diagram of an airfoil leading edge bubble which occurs if the Reynolds number is sufficiently low so that the boundary layer remains laminar up to the minimum pressure point. Downstream of this point, separation occurs almost immediately since laminar boundary layers, in contrast with turbulent flows, are extremely sensitive to adverse pressure gradients. A separation bubble forms in which a recirculating streamline pattern is bounded by a shear layer. Since shear layer flows tend to be highly unstable to flow disturbances, transition from laminar to turbulent flow generally occurs in this shear layer. Further downstream, the turbulent mixing between the shear layer flow with the lower dead air region results in entrainment of higher energy air which energizes the flow near the surface thereby resulting in flow reattachment with subsequent turbulent boundary layer flow downstream. As shown in Fig. 1, the initial position of the separation bubble is characterized by a pressure plateau followed by a pressure recovery region after the transition process is initiated, but prior to flow reattachment.

Technical Approach

The approach taken in the ALESEP code for the analysis of closed leading edge separation bubbles is based on an inviscid-viscous interaction technique in which the boundary layer equations are solved iteratively with an inviscid analysis through displacement thickness coupling. Experimental studies (Refs. 2-5) have shown that these closed transitional separation bubbles occupy only a few percent of the airfoil chord. Since the resultant interaction is highly localized, the leading edge transitional bubble problem is treated as a linear perturbation to a known global airfoil solution. The use of a perturbation approach permits an accurate analysis of the flow field structure in this region in contrast with the extremely difficult problem of trying to resolve this small scale phenomena while simultaneously solving the global airfoil flow field. In contrast with previous perturbation treatments of this problem, the approach taken in ALESEP accounts for the influence of the global viscous airfoil flow on the local interaction analysis. A detailed discussion of the approach taken in the ALESEP technique can be found in Refs. 6-8.

The local inviscid analysis in the ALESEP procedure assumes that the disturbance field induced by the presence of a transitional separation bubble can be treated as a small disturbance to the global airfoil flow. An asymptotic analysis is presented in Ref. 8 which formally shows that under a particular limiting condition, the disturbance field induced by the transitional displacement surface can be represented by a distribution of sources placed along a reference displacement surface as shown in Fig. 2. The reference displacement surface is usually defined as the displacement thickness which would exist in the local region due to an attached turbulent boundary layer. It, as well as the reference velocity distribution, are obtained from an airfoil analysis code such as that presented in Refs. 9 or 10 in which instantaneous transition from laminar to turbulent flow is assumed to occur at the predicted laminar separation point. Calculation of the perturbation velocity which occurs due to the difference between the separation bubble displacement thickness and the reference displacement surface as shown in Fig. 2, is performed through a Cauchy integral of the streamwise distributed sources using potential flow considerations. Upon integration of this Cauchy integral for the perturbed velocity, the local inviscid velocity distribution, u_{eI} , due to the interaction with the separation bubble is determined by adding the perturbation velocity and the reference velocity solution.

The viscous solution technique used in ALESEP is the inverse boundary layer procedure presented by Carter (Ref. 11). In this procedure, a perturbation stream function is introduced into the boundary layer equations for the simplification of boundary conditions. The continuity equation is eliminated and the stream function definition is subsequently added to the governing equation set which also included the momentum and energy equations. The governing equations are solved for the local perturbation stream function, velocity ratio, total enthalpy ratio, and viscous edge velocity, u_{ev} , for a prescribed streamwise distribution of perturbation mass flow, $m = \rho_{ev} \delta^*$. The numerical solution of the governing equations is obtained using an implicit finite difference technique which is first order accurate in the streamwise direction and second order accurate in the normal direction.

Since the boundary layer equations are parabolic, an instability will arise when the solution marching direction is opposite to the flow direction. Reyhner and Flugge Lotz (FLARE) (Ref. 12) have shown that this instability is easily avoided by assuming that the streamwise convection terms are zero in reversed flow regions. It is apparent, however, that a loss of accuracy in the converged solution is incurred due to the negligence of the streamwise convection terms. As an improvement to the FLARE approximation, a windward finite difference operator may be used in the ALESEP code to calculate the streamwise gradient terms in reversed flow regions. The effects of using the more accurate windward differencing scheme are described in detail in Ref. 8.

The transition from laminar to turbulent flow in the separated shear layer may be modeled using one of two possible techniques available in the ALESEP code. A simple forced transition model in which the onset and length of transition are specified may be used in conjunction with either the Cebeci-Smith (Ref. 13) or the McDonald-Fish-Kreskovsky (Refs. 14 and 15) turbulence models. The forced transition model is based on the streamwise intermittency distribution which was established by Dhawan and Narasimha (Ref. 16). Alternately, the natural transition model of McDonald and Fish (Ref. 14) may be used with the McDonald-Fish-Kreskovsky turbulence model to automatically predict the transition location. Details of these transition and turbulence models in conjunction with the ALESEP inviscidviscous interaction technique may be found in Refs. 6-8.

The present interaction iteration procedure is based on the inviscidviscous iteration technique presented by Carter (Ref. 17) and is adopted to the present scheme as outlined in Fig. 3. The key feature of this iteration procedure is that the update formula permits the inverse boundary layer analysis to be directly linked to the inviscid analysis which accounts for displacement thickness effects. It was found by Kwon and Pletcher (Ref. 18) that convergence could be accelerated by making several inner loop passes through the Cauchy integral and the update formula with the boundary layer prediction of the edge velocity frozen at its current global iteration value. This technique is used in the present interaction iteration and has been found to significantly accelerate the global convergence rate of the scheme.

USER INSTRUCTIONS

Code Description

A flow chart of the ALESEP code is shown in Fig. 4. The code has been written to allow for one of two possible modes of operation to be performed. The first mode allows for a direct finite difference boundary layer calcuation for a prescribed edge velocity distribution. The second mode allows for an inviscid-viscous interaction calculation for a prescribed reference displacement surface and reference edge velocity distribution.

The ALESEP code is written in FORTRAN IV language and takes 206,000 octal word storage locations. Typically 20-40 global inviscid-viscous iterations are required to reduce residuals in inviscid-viscous edge velocities to 10^{-3} . On a Cyber 175 computer using the Cebeci-Smith turbulence model, an inviscid-viscous interaction calculation takes approximately 12 seconds per iteration. Using the McDonald-Fish-Kreskovsky turbulence model, an interaction calculation takes approximately 80 seconds per iteration. This increase in computing time is a result of the iterative solution of the turbulent kinetic energy equation required for this model.

Input Description

The input to the ALESEP code is read in five separate blocks. The first block is a namelist file, MASTER, used to define parameters which control the mode of operation, the streamwise computational grid, and input/output options. The second block of input contains the prescribed reference pressure, reference displacement surface, and free stream turbulence level distributions. The third input block is a namelist file, INPUT, which defines the controlling parameters for the boundary layer solution procedure. The fourth block is used to define experimental data which may be used in subsequent plots of the results. Finally, the last block of information required for inviscid-viscous interaction cases is the velocity ratio, perturbation stream function, total enthalpy ratio, and eddy viscosity profiles at the inital station of the interaction region and the initial guess of the perturbation mass flow distribution.

The first three blocks of input information are necessary to execute a direct boundary layer calculation. The input variable, IFIN, located in the MASTER namelist must be set to 2 and INVRSE in the INPUT namelist must be set to 0. The computational grid is determined by the following variables:

Streamwise - IGRID, AK1, AK2, DS, MMAX, SSWTCH, SPIVOT, IPIVOT, AK11, AK12, IVGINX, IMAX (namelist MASTER)

Normal - DETA, AK, NMAX1 (namelist Input)

A laminar similarity solution is used at the initial station with a freestream Mach number, AMES, and gradient, BETAS = $(1/M_{\rm p})(dM_{\rm p}/d\xi)$ prescribed in namelist INPUT. The user has a choice of transition and turbulence models through the definition of variables, STRANS, KTRAN, TRNLEN, and ITRBMD located in namelist INPUT. For ITRBMD = 0, the Cebeci-Smith turbulence model is used with forced transition occurring according to specified values of STRANS, KTRAN, and TRNLEN. For ITRBMD = 1 or 2, the McDonald-Fish or McDonald-Fish-Kreskovsky natural transition turbulence model is used and transition is predicted automatically.

For an inviscid-viscous interaction calculation, input blocks 1, 2, 3 and 5 are necessary. The input variable, IFIN, located in namelist MASTER, must be set to 3 and INVRSE in the INPUT namelist must be set to 1. A total of IQUIT global inviscid-viscous iterations are performed. The structure of the computational grid is determined by the same variables previously mentioned for a direct boundary layer calculation with some required constraints which are discussed below. Velocity ratio, perturbation stream function, total enthalpy ratio and viscosity profiles at the initial station of the interaction region are required in the fifth input block (NSTART=1 in INPUT namelist) and are obtained from a direct boundary layer calculation extending from the leading edge to the initial station of the inviscid-viscous interaction calculation located somewhat ahead of the laminar separation point. For INTERP=0 in namelist INPUT, the values of AK and NMAX1 which define the computational grid in the normal direction in namelist INPUT should be the same as that used in the direct boundary layer calculation. The value of DETA in namelist INPUT should be the value used in the direct boundary layer calculation scaled by $\sqrt{2\xi}/\rho_e u_e r_0^i \delta^*$ due to the different definitions of the normal coordinate used in the direct and inverse boundary layer formulations. This scaling is performed automatically in subroutine CONVRT at the last computational station of the direct boundary layer calculation when IPRNEW has been set to 1. The value of DETA for the interaction calculation can then be found in the converted profile information for the last station printed out at the end of the direct boundary layer calculation. The value of XCO in namelist INPUT for the interacting calculation should be defined as the value of XC at the last computational station of the direct calculation. The value of AHO also in namelist INPUT should be defined as the value of AH at the last computational station of the direct calculation scaled by the inverse over direct DETA ratio. As in the direct calculation, the user has a choice of transition and turbulence models through definition of the input variables STRANS, KTRAN, TRNLEN, and ITRBMD. In addition to the models described in the direct boundary layer calculation, a forced transition model may be used with the McDonald-Fish (Ref. 14) or McDonald-Fish-Kreskovsky (Ref. 15) turbulence models by setting KTRAN=IQUIT and defining STRANS and TRNLEN. To use the natural transition model of McDonald and Fish with these turbulence models, KTRAN must be set to 0. Special windward differencing may be used in the reverse flow region of the separation bubble through definition of IWINDD and IWINDG in namelist INPUT. Detailed results using the different turbulence models and windward differencing scheme may be found in Refs. 6-8.

Detailed Input Description

Input Block 1:

The first block of input is read in from subroutine Main in a namelist called MASTER. This information defines the streamwise computational mesh and parameters controlling input and output.

INPLT	Number of global iterations between calls to plotting routines.
IQUIT	Total number of global inviscid-viscous iterations to be computed. Set IQUIT=1 for a direct boundary layer calculation.
RFDT	Relaxation factor applied to the perturbation mass flow in the inviscid-viscous update procedure.
RFVN	Relaxation factor for the injection velocity to represent viscous effects (inactive, set = 1.0).
MMAX	Total number of streamwise grid points used in the boundary layer calculation.
SSWTCH	Arclength location measured from the nose of the body where the boundary layer calculation is initiated.
IPLOT	Value of the global iteration counter at which the plot subroutines are first called.
AK1	The ratio of adjacent grid sizes used in generating the boundary layer grid in the streamwise direction beginning at SSWTCH.
AK2	The ratio of adjacent grid sizes at SSTING where SSTING > SSWTCH.
SSTING	Location where secondary boundary layer stretching, AK2, in the streamwise direction is initiated.
DS	Increment in arclength used at start of boundary layer mesh which begins at SSWTCH.
IVT1	Index in the inviscid streamwise arrays where the tangential velocity VT is read into program (inactive, set = 0).
IVT2	Last index where VT (I) is read into program (inactive, set = 0).
ISMOTH	If equals zero, no smoothing is used; if equals 1, the smoothed VT distribution is used.

MIT2	Inactive, set = 0.
SSTOP	Arclength location measured along the reference surface where the calculation is terminated downstream.
ITEK	Inactive, set = 0.
IAXI	If equals 0, two dimensional flow; if equals 1, axisymmetric flow.
IFIN	If equals 1, program terminates after initial inviscid calcula- tion (this initial inviscid calculation is made with no boundary layer effect). If equals 2, program terminates after initial inviscid calculation and one pass thorugh boundary layer solver. If equals 3, program operates in full interactive mode and terminates after IQUIT iterations.
IFILET	If equals 1, the offset distance between the circular arc, hard surface and a cubic filet coordinate surface will be computed (set = 0).
XT1 XT2	
YSTING YSTING RADIUS THICK XLO	Inactive, set = 0.
IWRPMF	If equals 0, bypass. If equals 1, the perturbation mass flow distribution is written to unit 13 for later restart.
CHORD	Reference length which allows rescaling the original axial dis- tance measured from the nose to an alternate coordinate system measured from another location located at distance XOR from the nose.
XOR	Axial location in the original coordinate where the origin of the new coordinate X/C is located. Both XOR and CHORD are used to shift and rescale the axial coordinate used in the program.
SIO	Shift factor which allows the inviscid calculation to start at a downstream location on an open nose body where the flow is not disturbed near the nose. SIO is the distance from the original nose of the body to the downstream location where the inviscid calculation is started (set = 0).
IPLTX	If equals zero, bypass. If equals 1, then the program generates a plot file which will later generate the plots on a TEKTRONICS unit for studying the resuts of individual iterations. The user may select the global iteration(s) for which plots are to be generated.

- NDCP If equals 0, bypass. If equals 1, then experimental CP data versus X will be read into the program and plotted on CALCOMP plot from subroutine PLOTCP.
- NDDT If equals 0, bypass. If equals 1, then experimental displacement thickness distribution versus X/C will be read into the program and plotted along with the computed displacement thickness distribution.
- NDCF If equals 0, bypass. If equals 1, then experimental skin friction data versus X/C will be read into the program and plotted along with the computed skin friction distribution.
- NDUE If equals 0, bypass. If equals 1, experimental tangential velocity data versus X/C will be read in and plotted along with the tangential velocity computed solution.
- IPRINT(I) Array containing global iteration values at which station output is printed (array length = 100).

IGRID

If equals 0, inviscid and boundary layer mesh are generated by their own parameters.

If equals 1, inviscid mesh is set by its own parameters (IMAX, SINO, AKI1, AKI2, SPIVOT, IPIVOT, IVGINX - as described below) and boundary layer mesh is set equal to the inviscid mesh for S > SSWTCH.

If equals -1, inviscid mesh is set equal to the mesh at which geometry is input (i.e., X0, Y0, S0) and boundary layer mesh is set equal to inviscid mesh for S > SSWTCH.

If equals -2, inviscid mesh is set equal to the mesh at which geometry is input and boundary layer mesh is generated by its own parameters.

- IMAX Maximum number of points in streamwise direction for the inviscid mesh.
- SINO The arclength at first point in inviscid mesh, or SI(1).
- AKI1 Ratio of adjacent grid sizes used in generating the inviscid grid in the streamwise direction between SINO and SPIVOT.
- AKI2 Ratio of adjacent grid sizes used in generating the inviscid grid in the streamwise direction for S > SPIVOT.
- SPIVOT Arclength at which geometric progression constant changes from AKI1 to AKI2.
- IPIVOT Streamwise mesh index at SPIVOT.

IVGINX	If equals 0, uniform inviscid mesh; if equals 1, a variable mesh using AKI1, AKI2 is used.
LOADDT	If equals 0, reference displacement thickness, DTO = 0; if equals 1, DTO is read in the second input block.
LOADSI	If equals 0, compute arclength from X0, Y0; if equals 1, arc- length is read in the second input block.
LOADCP	If equals 0, compute CPO using Cauchy integral; if equals 1, CPO is read in the second input block.

Input Block 2:

The second block of input is read in from subroutine INVO in a formated block. This block of information contains the reference displacement surface, reference velocity distribution, and edge turbulence level distribution.

ITITLE	Card 1:	A brief title for the configuration (12A6).
IXY	Card 2:	Number of points at which inviscid input including reference solution is read in. (I3)
xo	Card 3:	Cartesian distance in horizontal direction.
YO		Cartesian distance in vertical direction.
SO		Arclength measured from stagnation point.
СРО		Pressure coefficient, $(P_0 - P_{\infty})/\frac{1}{2}\rho_{\infty}U_{\infty}^2$, from reference solution.
DTO		Displacement thickness from reference solution.
TUO		Freestream turbulence level.
NOTE: I F10.7) f	XY values o ormat.	f XO, YO, SO, CPO, DTO, TUO are read in (4F10.7, E10.5,
CAN		
GAM	Card 4:	γ, the specific heat ratio.
AMINF		M_{∞} , freestream Mach number.
NOTE: G	AM. AMINF a	re read in with 2F10.7 format.

Input Block 3:

The third block of input is read in from subroutine TURBID in a namelist called INPUT. The information in this block is used to define the computational grid in the normal direction, the reference freestream flow conditions, the transition and turbulence model, and further output parameters.

NMAX1	Total	number	of	grid	points	which	are	used	across	the	boundary
	layer	in the	nor	cmal o	direction	on.					

- NMXOLD Total number of grid points in the initial profile of the interaction calculation.
- DETA Increment in the transformed normal grid spacing, Δn , adjacent to the wall.
- AK Ratio of adjacent step sizes in the eta, n, direction which is used to generate the mesh across the boundary layer. A uniform mesh (AK=1) is not currently allowed.
- INVRSE If equals 0, then a direct boundary layer calculation is to be performed; if equals 1, then an interacting boundary layer calculation is to be performed.
- JPFMAX Total number of points used in the initial guess for the perturbation mass flow distribution, PMFIN to be read in the fifth input block. In the case of restart, i.e., if IRESTR equal to 1, then JPFMAX should be set equal to MMAX.
- IRESTR If equals 0, bypass; if equals 1, then a restart capability is used. In this case, the input array for PMFIN obtained from a previous calculation are read from unit 12.
- INTERP If equals 0, bypass; if equals 1, then profiles at the initial interaction station are to be interpolated onto the interaction grid (set = 0).
- IPRNEW If equals 0, bypass. If equals 1, the computed profiles at M=MMAX from a direct boundary layer calculation are converted from direct variables to inverse variables. Principally, this involves a change in the stream function and in the transformed normal coordinate eta, η.
- NSTART If equals 0, program is initiated with the solution of the self-similar equations. If equals 1, profiles for the velocity ratio, stream function, total enthalpy ratio, and viscosity versus eta, η , are read from the fifth input block.

NQMAX Maximum number of column iterations which can be used in the boundary layer solution procedure.

- NPRRES If equals 0, bypass; if equals 1, boundary layer residual information will be printed.
- MFIG(I) Array of index values of the streamwise stations where profiles in the boundary layer solution are printed (array length = 100).
- JMAX The maximum number of boundary layer profiles to be printed out. If JMAX equals zero, then there will be no profiles printed, in which case, MFIG is set to a hundred zeros.
- ITPRO Global iteration counter at which detailed boundary layer residual and profile information is printed out.
- PMFO Multiplicative factor which is used to rescale the perturbation mass flow.
- AHO Initial value of the static temperature integral across the boundary layer which appears explicitly in the boundary layer equations. This parameter is needed when NSTART = 1, i.e., the boundary layer solution is initiated with specified profiles instead of internally generated self-similar solutions.
- XCO Initial value of the transformed (Levy Lees) ξ variable which is needed when NSTART = 1.
- RESG Maximum change in the dependent variable allowed between successive column iterations in_4 the boundary layer calculation. Typical value used is 10 \cdot .
- IPLOT(I) Array containing an index to determine which plots are desired by the user (array length = 8). If IPLOT(I) is equal to 0, plot is bypassed; if IPLOT(I) is equal to 1, then the plot is made. The following order is used in the plotting subroutine. Plot #1 is DT (δ *, displacement thickness) versus X/C. Plot #2 is CF versus X/C. Plot #3 is UE (VT, the inviscid tangential velocity) versus X/C. Plot #4 is Beta (pressure gradient parameter) versus X/C. Plot #5 is VN versus X/C. Plots #6, 7 and 8 control the plotting of profiles across the boundary layer.
- WAKCON The Clauser constant in the Cebeci-Smith eddy viscosity law is SWK1 varied linearly from 0.0168 at S=SWK1 to 0.0168/WAKCON at S=SWK2 SWK2 (set WAKCON=1.0, SWK1=10000, SWK2=20000 to deactivate this option).
- YORIGN(I) Array containing the origin of the Y axis for each of the respective plots listed above (array length = 8).
- YSCALE(I) Array containing the scale factor for each of these plots (array length = 8). If the scale factor exceeds 1000, then the scale for these particular plots is determined automatically.

- YIN(I) Array containing the number of inches for Y axis in each of the plots listed above (array length = 8).
- XORIGN(I) Array containing the origin for X axis in each of these plots (array length = 8).
- XSCALE(I) Array containing the scale factor for X axis (array length = 8); Again if this parameter exceeds 1000, the scale factor is determined automatically.
- XIN(I) Array containing the number of inches used along the X axis in the respective plots (array length = 8).
- XL Reference dimensional length used to convert the present X to a dimensional distance.
- NDATA If equals 0, bypass; if equals 1, experimental data will be read from the fourth input block to be plotted with numerical results.
- BETAS Value of the pressure gradient parameter, (1/M)(dM/dS), which is required in the self-similar solution.
- AMES Value of the streamwise Mach number required in the self-similar solution.
- GW Value of the total enthalpy ratio at the wall.
- TINFD Reference temperature at infinity in degrees Rankine which is required in the Sutherland law for molecular viscosity.
- PRT Turbulent Prandtl number.
- PR Prandtl number.
- REINF Reynolds number based on the reference (free stream) properties and based on the length which is used to nondimensionalize the coordinate used in the calculation.
- STRANS Nondimensional distance along the body at which instantaneous transition is assumed to occur.
- KTRAN For Cebeci-Smith turbulence model (ITRBMD=0): equal to 0, fully laminar calculation; equal to 1, instantaneous transition occurs at STRANS; equal to 2, transition occurs over TRNLEN starting at STRANS. For McDonald-Fish turbulence model -(ITRBMD=1,2): KTRAN is the global iteration number when the McDonald-Fish natural transition model begins to predict the transition location. Forced transition over TRNLEN starting at STRANS is used for all global iterations prior to KTRAN.

IWINDD	Global iteration number when convection windward difference operation is effective.
IWINDG	If equals 0, do not use windward differencing in energy equation; if equals 1, use windward differencing on convection terms in energy equation starting on the IWINDD global iteration.
IWINDS	If equals 0, do not use windward differencing on stream function; if equals 1, use windward differencing on stream function in momentum and energy equations starting on the IWINDI global iteration. This option is not recommended at this time (set = 0).
ITRBMD	If equals 0, Cebeci-Smith turbulence model; if equals 1, McDonald-Fish turbulence model; equals 2, McDonald-Fish-Kreskov- sky turbulence model.

Input Block 4:

The fourth block of input is read in from subroutine TURBID in a formated block only when NDATA $\neq 0$. This block of information contains experimental data which may be plotted along with the numerical results.

IDST		
ICFST IUST	Card 1:	Number of experimental data points to be read for DTE, CFE, or Ul (I3).
J	Card 2:	Index of experimental data point (I3).
XDTE		
XCF XU1		Cartesian distance in horizontal direction for experimental values of DTE, CFE or Ul.
DTE		Experimental values of δ^* (NDDT \neq 0)
CFE		Experimental values of C_f (NDCF $\neq 0$)
U1		Experimental values of U_e^{\dagger} (NDUE \neq 0)
NOTE:	IDST, ICFST,	or IUST values of
J,	XDTE, XCF	or XU1 and
	DTE, CFE,	or Ul are read in (I3, 2F8.4) format

Input Block 5:

The fifth block of input is read in from subroutine TURBID in a formated

block only when NSTART=1. This block of information contains profiles for the velocity ratio, perturbation stream function, and total enthalpy ratio to be used at the initial station of the interaction calculation. For ITRBMD $\neq 0$, the scalar quantities necessary to initialize the turbulent kinetic energy equation as well as the eddy viscosity profiles are also read in this block. The initial guess distribution for the perturbation mass flow parameter is also read in this formated block.

Values of PSI11, PSI12, PSI31, PSI32, EMFK, ALINF, A1MFK, DTINC, DELTU, and A2MA3 are read in 5F16.8 format when ITRBMD $\neq 0$. These variables define the scalar quantities required for the McDonald-Fish-Kreskovsky turbulence model at the inital station of the interaction case. These values are stored in unit 14 of a direct boundary layer calculation when IPRNEW = 1. See the output description section for the definition of these variables.

NMAX values of YNI, EPSBB, and EPSHB in a 3E16.8 format are read next when ITRBMD $\neq 0$. These arrays define the viscosity profiles for the McDonald-Fish-Kreskovsky turbulence model at the initial station. These values are stored in unit 14 of a direct boundary layer calculation when IPRNEW = 1. See the output description for the definition of these variables.

NMXOLD values of NN, ETABD, FBD, PSI, and GBD are read in a 15, 4E16.8 format. These arrays define the velocity ratio, perturbation stream function, and total enthalpy ratio profiles at the initial station. These values are stored in unit 14 of a direct boundary layer calculation when IPRNEW = 1. See the output description section for the definition of these variables.

JPFMAX values of PMFIN in a 7F10.7 format followed by JPFMAX values of SPMF in the same format are read in to define the initial distribution of the perturbation mass flow.

Output Description

An example test case for the NACA 66_3-018 airfoil tested experimentally by Gault (Ref. 2) at a chord Reynolds number of 2×10^6 and a 0.0 degree angle of attack is given in Appendix A. A comparison between the predicted and experimental pressure distributions is shown in Fig. 5(a). The predicted displacement thickness and skin friction distributions are shown in Figs. 5(b) and 5(c), respectively. In this case, the reference pressure₇ distribution was taken to be the experimental high Reynolds number (Re = 10⁻) case in which transition naturally occurred before laminar separation could take place. A direct boundary layer calculation was run

from the leading edge stagnation point of the airfoil to an s/c = 0.5 using the reference pressure distribution as the edge boundary condition. The velocity ratio, perturbation stream function, total enthalpy ratio, and eddy viscosity profiles were taken at the s/c = 0.5 station from the direct calculation and used as initial profiles for the interacting calculation. The reference displacement thickness was held constant at that value predicted by the direct boundary layer calculation at s/c = 0.5. A total of 99 grid points were distributed evenly between s/c = 0.5 and s/c = 0.99in the interaction calculation. The McDonald-Fish turbulence model was used in this case with transition being forced to occur between s/c = .693and .703. The local edge turbulence level was calculated from a 0.2percent freestream turbulence level and the local to upstream inviscid velocity ratio using the assumption of frozen turbulence. The FLARE approximation of the streamwise convection was used in this case. Windward differencing was found to have little affect on the predicted results. Further comparisons of predicted results using the ALESEP technique with experimental data may be found in Refs. 6-8.

The notation used in the output of the ALESEP code conforms to that used in the description of the governing equations in Refs. 6-8. A dictionary of the variables used in the output can be found in the following section.

Reference Distribution Output

XO, YO XB, YB	Input Cartesian coordinates of body shape.
SO	Input arclength.
СРО	Input reference pressure coefficient.
DTO	Input reference displacement thickness.
TUO, TUB	Input boundary layer edge turbulence level.
VT	Input boundary layer edge velocity at same location as input body coordinates.
SI	Body arclength measured from stagnation point at nose of body to same location as input body coordinates.
XOC	Shifted and rescaled value of axial coordinate, XO. XOC = (XO - XOR)/CHORD
PMF PMFB	Input perturbation mass flow paramter, $m = \rho_{e} u_{e} r^{i} \delta^{*}$ (interacting case only).
S	Body arclength measured from stagnation point to boundary layer computational stations.

SPMF	Body arclength measured from stagnation point to boundary layer stations where perturbation mass flow is defined.
XOCBL	Same as XOC, but measured from stagnation point to boundary layer computational stations.
RO	If flow is axisymmetric, RO is the body radius; for 2-D flow RO=1.
VTBL	Boundary layer edge velocity at boundary layer computational

Similarity Solution Output

stations.

- NQ Boundary layer column iteration counter.
- RES1 Maximum change in dependent variable between two successive column iterations.

AHO Static temperature integral, h.

			1. S.		t ·			
FNW	Normalized	wall	shear,	$\frac{\partial F}{\partial F}$		where	F =	u/u
				- θη	n=0			e

- ETA Transformed coordinate normal to surface, n.
- F Streamwise velocity ratio, $u/u_{o} = F$.
- SF Transformed stream function, f.

G Total enthalpy ratio, $H/H_{c} = G$.

Initial Profiles

If NSTART equals 0, then the initial profile is the same as the laminar self-similar solution. If NSTART equals 1, then the initial profiles are the same as those which are read in (ETABD = ETA, FBD = F, PSI = SF, GBD = G). Note however that if INTERP equals 1, then these profiles have been interpolated onto a new η -mesh.

Station Output (Summary Chart No. 1)

M Streamwise station index

PMF	In direct calculation, this is $\sqrt{2\xi}$ where ξ is the streamwise Levy Lees variable; in an interacting case, this is the pre- scribed distribution of perturbation mass flow, $m = \rho_e u_e r_o^1 \delta^*$.
РМГСНК	This is $\rho_{ev} r_{o}^{i} \delta^{*}$; in an inverse calculation, this quantity is a check to see that the computed velocity profiles give the same displacement thickness as that prescribed and thus, in the interacting mode, we should always get PMFCHK = PMF.
BETA	Pressure gradient parameter, $\beta = (1/M_e)(dM_e/d\xi)$.
BETCHK	Calculated pressure gradient parameter (interacting case only).
UEP	Boundary layer edge velocity. In direct mode, UEP is the same as the prescribed VTBL; in the inverse mode, it is computed as part of the solution.
АМАСН	Boundary layer edge Mach number.
АН	Static temperature integral, $h = \int_{0}^{\infty} (T/T_{e} - 1)d_{\eta}$.
CF	Skin friction coefficient based on free stream dynamic head, $C_f = \tau_w^* / \frac{1}{2} \rho_{\infty}^* U_{\infty}^{*2}$ where asterisk denotes dimensional quantity.
NMCH	Index where inner and outer edge viscosity laws are matched (Cebeci-Smith turbulence model).
RTHETA	Reynolds number based on momentum thickness.

<u>McDonald-Fish-Kreskovsky Turbulence Model Output</u> (ITRBMD ≠ 0)

MREF	Reference free stream Mach number. Same as AMINF in third input block.
TREFD	Reference free stream static temperature. Same as TINFD in INPUT namelist.
TREF	Nondimensional reference free stream static temperature.
REYREF	Reference free stream Reynolds number. Same as REINF in INPUT namelist.
ME 2	Boundary layer edge Mach number at current streamwise station.
UE2	Nondimensional boundary layer edge velocity at current streamwise station.
TE2	Nondimensional boundary layer edge temperature at current streamwise station.

RHOE2	Nondimensional boundary layer edge density at current streamwise station.
TU2	Boundary layer edge turbulence level at current streamwise station.
RO2	Geometry coefficient, RO, at current streamwise station.
QE2	Boundary layer edge perturbation velocity magnitude at current streamwise station.
MUE2	Nondimensional boundary layer edge molecular viscosity at current streamwise station.
ME1	Boundary layer edge Mach number at previous streamwise station.
UE1	Nondimensional boundary layer edge velocity at previous stream- wise station.
TEl	Nondimensional boundary layer edge temperature at previous streamwise station.
RHOE1	Nondimensional boundary layer edge density at previous stream- wise station.
RO1	Geometry coefficient, RO, at previous streamwise station.
QE1	Boundary layer edge perturbation velocity magnitude at previous streamwise station.
ACLINF	Free stream dissipation length, L, at current streamwise station.
ALINFN	Free stream mixing length, 2, at current streamwise station.
ALINFO	Free stream mixing length, ℓ , at previous streamwise station.
A1MFKN	Structural coefficient, a ₁ , at current streamwise station.
A1MFKO	Structural coefficient, a ₁ , at previous streamwise station.
A2MFK	Structural coefficient, a2, at current streamwise station.
A3MFK	Structural coefficient, a3, at current streamwise station.
BLTHK	Boundary layer thickness at current streamwise station scaled by $\sqrt{R}_{e_{\infty}}$.
DELIN	Inner boundary layer thickness at current streamwise station.
DELTU2	Value of turbulent displacement thickness, δ_{τ} , at current

DELTU1	Value of turbulent displacement thickness, $\boldsymbol{\delta}_{\tau}\text{,}$ at previous streamwise station.
DTINC2	Incompressible displacement thickness at current streamwise station.
VEDGE	Nondimensional boundary layer edge normal velocity component, v _e , at current streamwise station.
NDELTU	Index of normal grid point where DELTU2 is located.
NINNER	Index of normal grid point where DELIN is located.
PSI11N	Value of first set of terms of the ϕ_1 integral in turbulent kinetic energy equation at current streamwise station.
PSI12N	Value of second set of terms of the ϕ_1 integral in the turbulent kinetic energy equation of the current streamwise station.
PSI110	Value of first set of terms of the ϕ_1 integral in the turbulent kinetic energy equation at the previous streamwise station.
PS1120	Value of second set of terms of the ϕ_1 integral in the turbulent kinetic energy equation at the previous streamwise station.
PSI21N	Value of the ϕ_2 integral in the turbulent kinetic energy equation at the current streamwise station.
PSI31N	Value of the first set of terms of the ϕ_3 integral in the turbulent kinetic energy equation at the current streamwise station.
PSI32N	Value of the second set of terms of the ϕ_3 integral in the turbulent kinetic energy equation at the current streamwise station.
EMFK	Value of the source term, E, in the turbulent kinetic energy equation at the current streamwise station.
RTAU	Value of the turbulent Reynolds number, R_{τ} , at the current streamwise station.
RTHEAT	Value of the correlated momentum thickness Reynolds number, ${\tilde R}_{\theta}^{},$ at the current streamwise station.
A2MA3N	Value of the difference of structural coefficient, $a_2^{-a_3}$, at the current streamwise station.

Profile Output

ETA	Transformed normal coordinate, n.
YBL	Nondimensional physical distance from surface.
F2	Streamwise velocity ratio, u/u _e .
SF2	Transformed stream function, f.
G2	Total enthalpy ratio, H/H _e .
EPSBAR	$1+\epsilon/\mu$ where ϵ is the eddy viscosity coefficient and μ is the molecular viscosity coefficient.
RHOMUR	$\ell = \rho \mu / \rho_e \mu_e$.
Τ	Static temperature ratio, T/T _e .
For ITRBMD	\neq 0, the following additional profiles are printed:
YN	Nondimensional physical distance from the surface scaled by $\sqrt{Re_\infty}$
YPLUS	Nondimensional scaled distance from the surface, y+ = $y\sqrt{\tau/\rho/v}$
DUDY	Nondimensional velocity normal gradient, $\partial F / \partial YN$
TAU	Shear stress, $(\mu + \mu_T) \partial u / \partial YN$
DAMP	Damping factor squared, \mathfrak{D}^2 .
FUN	Local mixing length distribution in normal direction.
FMFK	McDonald-Kreskovsky function, f_{τ} , on mixing length formula.

Station Output (Summary Chart No. 2)

М	Streamwise index.
XLE	Cartesian coordinate of station location.
DT*	Scaled displacement thickness, $\delta^* \sqrt{Re_{\infty}}$.
THETA*	Scaled momentum thickness, $\theta \sqrt{Re_{\infty}}$.
CPBL	C_{p} obtained from interacting boundary layer calculation.
UEP	u, obtained from interacting boundary layer calculation.

QW Heat transfer coefficient at the wall.

STAN Stanton number.

STRINT Intermittency parameter in streamwise direction.

CFX Scaled skin friction coefficient, $c_f \sqrt{Re_{\infty}}$.

Summary of Convergence History

INTRAC Interaction global iteration counter.

DDTMAX Maximum change in DT.

RMSDT Root mean square change in DT.

SMDT Streamwise location where DDTMAX occurs.

DUEMAX Maximum change in UE.

RMSUE Root mean square change in UE.

SMUE Streamwise location for maximum change in UE.

DSFMAX Maximum change in perturbation stream function, f.

DFMAX Maximum change in velocity ratio, F.

DGMAX Maximum change in total enthalpy ratio, G.

Brief Description of Files

The following files are used to write information for plotting, restart, and interaction purposes.

Unit	Number	Purpose
	8	Write velocity and temperature profiles to be used for plotting purposes later on (TURBID).
	9	Write stream function profile to be used for plotting purposes later on (TURBID).
	10	Write eddy viscosity coefficient profile to be used for plotting purposes later on (TURBID).
	12	Read information for restart run (TURBID).

- Write information for later restart (WR13).
- Write the profiles in inverse variables from a direct boundary layer run at the last streamwise station (CONVRT).
- 17 Write the weak interaction solution from a direct boundary layer run for use as a reference solution (TURBID).
 - 18

14

Direct access file to store information for windward differencing scheme (TURBID).

22

Write station quantities for Tektronics plotting (WR22).

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82-6-7-2

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Fig. 2 Local interaction region coordinate system



Fig. 3 Inviscid-viscous interaction procedure




Fig. 5 Predicted results for NACA 66₃-018 airfoil. (a) Pressure distribution.

83-9-99-23



Fig. 5 Predicted results for NACA 663-018 airfoil (b) Displacement thickness.

83-9-99-24



Fig. 5 Predicted results for NACA 66₃-018 airfoil. (c) Skin friction.

83-9-99-25



APPENDIX A

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INVERSE RUN CASE, REC=2.+1C++6 -- .2% TURBULENCE SMASTER INTPLT=199 10UIT=40. RFDT=1.0, RFVN=1., MMAX=199, SSWTCH=0.500001. IPLOT=199, IGRID=1, AK1=1., AKZ=1., SSTING= .6, DS=.01, IVT1=0, IVT2=0, ISMOTH=0, MIT2=25, S\$TOP=1.0, ITEK=0, IAXI=0, IFIN=3, IFILET=0, XT1= 8.44, XT2= 9.34, XSTING= 10., YSTING=0., RADIUS=0., XLD=10.,THICK=0.,SID=0.,XOR=0.,CHORD=1., IWRPMF = 1, IPLTX = 1, $\begin{array}{rcl} NDCP &= & 0 \\ NDDT &= & 0 \\ \end{array}$ NDCF = 0_{\bullet} NDUE = 1; LOADSI=0 ,LOADCP=1, LOADDT=0, IMAX=199, SINO=0., SPIVOT= 0.5, IPIVOT=101 , AKI1= 1.0 , AKI2=1.0 ,IVGINX=00 , IPRINT=10,20,30,40,96*0, \$END NACA 663018 AIRFOIL REFERENCE SOLUTION AT REC=10++7 34 .00000 0.0 0.0 1.0000 •0006568 •0006568 .002 .00496 .002 .002 0.0 0.0 .0006568 0.0 0.0 .49007 •01929 •02922 0.0 0.0 .15011 0006568 .002 .15011
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•16958192E+00	•10000276E+01	-10000209E+01
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120064166401	100103575401	100078505401
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•14075319E+CL	•10009609E+01	•10007282E+01
15350475E+01	-10008626E+01	10006538E+01
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•47248308E+01	10000000E+01	1000000E+01
-51508635E+01	-1000000E+01	-10000000E+01
561522026401	100000005401	10000005+01
• JULJEJ72ETUL	•100000000000000	•1000000E+01
•01214080E+UI	•I0000006+01	•1000000E+01
•66731333E+C1	•1000000E+01	.10000000E+01
-72745132E+01	+10000000E+01	-100000C0E+01
702001725401	100000000000000	10000000000000
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• 86445167E+UI	•1000000E+01	•1000000E+01
•94233212E+01	10000000E+01	10000000E+01
-10272218E+02	.1000000E+01	1000000F+01
111975151+02	1000000F+01	10000005+01
122040005+02	100000000000000000000000000000000000000	100000000000000000000000000000000000000
• 12200030E + 02	• 1000000E+01	• 10000000E+01
•13305436E+C2	•T0000000E+01	• 100000C0E+0]
14503723E+02	.1000000E+01	10000000E+01
-15809856F+02	-1000000E+01	100000000
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•10103331F+02	• 10000000F+01	 IOOOOOCOF+01
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99 •47886999E+02 •1000000E+01 ••29081892E-09 •1000000E+ 00 •52197755E+02 •1000000E+01 •10133663E-08 •1000000E+	5555555666666666666677777777777888888888	$\begin{array}{c} 89897596E+0\\ \circ 98081010E+0\\ \circ 10700093E+0\\ \circ 10700093E+0\\ \circ 12732141E+0\\ \circ 13887296E+0\\ \circ 12732141E+0\\ \circ 13887296E+0\\ \circ 15146416E+0\\ \circ 15146416E+0\\ \circ 136172471746E+0\\ \circ 21422764E+0\\ \circ 23360076E+0\\ \circ 23412773466E+0\\ \circ 2336076E+0\\ \circ 330282341E+0\\ \circ 33997809E+0\\ \circ 33997809E+0\\ \circ 55442529E+0\\ \circ 554425387E+0\\ \circ 11057487E+0\\ \circ 12053587E+0\\ \circ 120537587E+0\\ \circ 120537587E+0\\ \circ 120537587E+0\\ \circ 120537587E+0\\ \circ 120537587E+0\\ \circ 12057587E+0\\ \circ 12057587587E+0\\ \circ 12057587587E+0\\ \circ 12057587587E+0\\ \circ 12057587587E+0\\ \circ 12057587587E+0\\ \circ 1205758758758758758758758758758758758758758$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	-31339816E+00 -31595943E+000 -31595943E+000 -30920794E+000 -29865301E+000 -29865301E+000 -26109145E+000 -26109145E+000 -26109145E+000 -26109145E+000 -26253739E+000 -16770507E+000 -16770507E+000 -16770507E+001 -65661795E-011 -40346863E-011 -10197160E+011 -10197160E+011 -10197160E+011 -10197160E+011 -10197160E+011 -10197160E+011 -10197160E+011 -10197160E+011 -10197160E+011 -10197160E+011 -23287468E+044 -15375229E+007 -29056131E+008 -15357242E+008 -5537729E+009 -27842084E+009 -28074609E+009 -28311975E+009 -28074609E+009 -28319036E+009 -28319036E+009 -28319036E+009 -28120839E+009 -28120839E+009 -28013991E+009 -28120839E+009 -28120839E+009 -28552849E+009 -28403413E+009 -28403413E+009 -28403413E+009 -28403413E+009 -28403413E+009 -29081892E+009 -28403413E+009 -29081892E+009 -29081892E+009 -29081892E+009 -29081892E+009 -28403413E+009 -29081892E+0	<pre>.10000014E+ .10000071E+ .10000071E+ .10000105E+ .100000177E+ .100000241E+ .100000241E+ .10000262E+ .10000263E+ .10000263E+ .10000263E+ .10000263E+ .100000157E+ .10000016E+ .100000016E+ .100000016E+ .10000000E+ .10000000E+ .10000000E+ .10000000E+ .10000000E+ .10000000E+ .10000000E+ .10000000E+ .10000000E+ .10000000E+ .10000000E+ .10000000E+ .10000000E+ .10000000E+ .10000000E+ .10000000E+ .10000000E+ .10000000E+ .10000000E+ .1000000E+ .1000000E+ .1000000E+ .10000000E+ .10000000E+ .10000000E+ .10000000E+ .10000000E+ .10000000E+ .10000000E+ .10000000E+ .10000000E+ .10000000E+ .10000000E+ .10000000E+ .10000000E+ .1000000E+ .1000000E+ .1000000E+ .1000000E+ .1000000E+ .10000000E+ .10000000E+ .10000000E+ .10000000E+ .10000000E+ .10000000E+ .10000000E+ .10000000E+ .10000000E+ .10000000E+ .10000000E+ .10000000E+ .10000000E+ .10000000E+ .10000000E+ .10000000E+ .1000000E+ .1000000E+ .1000000E+ .10000</pre>
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1234567890123456789012345678901234	.00000 .00496 .0092 .01929 .02922 .07497 .13184 .251389 .348951 .49855 .345700 .49855 .6236715 .6659245 .6659245 .6659245 .73319 .773469 .6659245 .773319 .773469 .808448 .813903 .856673 .8808429 .893165 .8808429 .93155 .97960	.00000 .000000 .00000000	000496 001929 019297 0274920 131848 34598951 4494359222 671918355 66367153169 66594055 77534894 8859623659181 6656945519 77754694 8819903 885848499 885848499317560 89957960	$\begin{array}{c} 1.00000\\ .78366\\ .49007\\ .15011\\01987\\21413\\34216\\42605\\52539\\550331\\557837\\556733\\556733\\556733\\5560744\\660706\\580971\\48786\\350464\\35099\\30462\\136872\\092415\\ .006662\\ .070662\\ .17660\\ .22958\\ .27373\end{array}$		
I	51	SMOOTH	VT INPL	JT VT		
1 2 3 4 5 6 7 8 9 10 11	$\begin{array}{c} 000000\\ 005000\\ 0110000\\ 025000\\ 025000\\ 035000\\ 035000\\ 04500\\ 0400\\ 0400\\ 0400\\ 0400\\ 0400\\ 0400\\ 0400\\ 0$	• 0203 • 4258 • 6997 • 8443 • 9274 • 9771 1 • 0233 1 • 0326 1 • 0315	61 .0 75 .4 83 .1 70 .0 16 1.0 20 1.0 99 1.0 05 1.0 86 1.0)19994 67394 715935 326788 928191 972494 911455 921509 931564 931564 931672		

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. 175	000 1	1.184304	1_184299
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-220	000	L.205888	1.205889
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. 255	000	1.219425	1,219450
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265	<u>άρο '</u>	1.220066	1.220040
•207	000	1.220700	1.6550110
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376	200 C	1 3332433	1 222400
• 21 2	UUU .	1.4222421	1.222429
- 280	000	1.223173	1.223174
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200	000	1.224656	1 . 224664
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.295	600	1.225401	1.225408
- 566	000 ·	1 226 100	1 372127
• 300	000	1.550140	T#550131
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73	.360000	1.236962	1.236959
75	•370000	1.238630	1.23863
77	.380000	1.240302	1.24030
79	•390000	1.241978	1.24197
80 81	• 395 800	1.243579	1.24280
82 83	•405C00 •410000	1.244325 1.245060	1.24432
84 85	•415000 •420000	1.245794 1.246530	1.245794
86 87	•425C00 •430000	1.247267	1.24726
88 89	435000	1.248740	1.24874
90	445000	1.250220	1.250214
92	-455000	1.251667	1.25168
94 95	•465000	1.252843	1.252834
96	475000	1.253899	1.253899
98	•485000	1.254962	1.25496
100	•495000	1.256030	1.25602
102	•505000	1.257157	1.25657
103	•515000	1.257739	1.25774
105	•525000	1.258905 1.259487	1.25890
107	•530000 •535000	1.260074 1.260662	1.260069
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111	•550000 •555000	1.262088 1.262419	1.262070
113 114	•560000 •565000	1.262746	1.262744
115	•570000 •575000	1.263412	1.26341
	-580000 -585000	1.264078	1.264079
119	•590000 •595000	1.264736	1.26474
121	600000	1.265576	1.26558
123	.610000	1.266767	1.266660
125	.620000	1.267245	1.26773
127	.630000	1.263788	1.263606
129	•640000	1.258419	1.258333
131	•650000	1.250508	1.250926
133	•660000	1.235921	1.235776

134	•665000	1.227241	1.227141
136 137	•675000 •680000	1.211836 1.204989	1.211932
138 139	•685000 •690000	1.198164	1.198242
140	.695000	1.185024	1.184814
142	.705000	1.173836	1.168411
144	.715000	1.162907	1.162944
142	.725000	1.151586	1.151565
147	•735000	1.140062	1.140085
149 150	•740000 •745000	1.134182 1.128265	1.134175
151	•750000 •755000	1.122351	1.122354
153	•760000 •765000	1.110665	1.110672
155	.770000	1.099088	1.099114
157	.780000	1.087748	1.087670
159	.790000	1.077182	1.077188
161	.800000	1.066647	1.066706
162	.805000 .810000	1.055607	1.055577
164	•815000 •820000	1.050003	1.049998
166 167	•825000 •830000	1.038481 1.032595	1.038445
168 169	•835000 •840000	1.026614	1.026607
170	.845000	1.013343	1.013324
172	855000	999214	999066
174	-865000	986759	986816
176	.875000	.974959	.974969
178	•885000	•969049	•963149
180	•890000 •895000	•951663	•951657
181	•905000	•945938	•945912
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185 186	•920000 •925000	•921514 •915132	•921521 •915164
187 188	•930000 •935000	•908913 •903038	•908807 •903036
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57	•280000	•000000	•000000
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23	100000	•••••••	
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63	.310000	.000000	.000000
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97	•313000	•000000	••••••••
65	•320000	•000000	.000000
66	.325000	.000000	_000000
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69	340000	- 000000	-000000
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10	• 345000	•000000	•000000
71	.350000	.000000	.000000
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26	1120000		
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103	•510000	•000000	•000000
104	-515000	. 000000	. 000000
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108	•535000	•000000	•000000
109	- 540000	.00000	.000000
110	ELEDDO	-000000	••••••••
TTO .		•000000	•000000
111	•5500.00	.000000	.000000
112	-555000	. 000000	. 000000
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114	.565000	.000000	.000000
115	• 570000	• 000000	•000000
119	•575000 580000	-000000	-000000
118	.585000	.000000	000000
119	590000	000000	.000000
120	-595000	.000000	.000000
121	.600000	.000000	•000000
122	•605000	.000000	•000000
123	+610000	.000000	.000000
124	-620000	.000000	.000000
126	625000	.000000	.000000
127	.630000	.000000	.000000
128	•635000	.000000	•000000
129	•640000	•000000	•000000
130	.645000	.000000	.000000
112	-655000	.000000	.000000
133	.660000	.000000	.000000
134	.665000	.000000	.000000
135	.670000	.000000	•000000
136	•675000	.000000	.000000
137	+080000 685000	•000000	000000
130	-690000	-000000	.000000
14ó	695000	.000000	.000000
141	.700000	.000000	.000000
142	.705000	.000000	.000000
143	•710000	•000000	•000000
144	-715000	.000000	.000000
146	725000	.000000	.000000
147	730000	.000000	.000000
148	•735000	.000000	.000000
149	•740000	•000000	.000000
151	• 745000	•000000	.000000
152	.755000	.000000	.000000
153	760000	.000000	.000000
154	.765000	.000000	•000000
155 -	•770000	•000000	•000000
125	•775000	.000000	-000000
158	-785000	.000000	.0000000
159	790000	000000	000000
160	.795000	.000000	.000000
161	•800000	.000000	•000000
162	-805000	.000000	•000000
163	-810000	-000000	.000000
165	.820000	.000000	-000000
166	825000	.000000	.000000
167	.830000	.000000	.000000
168	.835000	.000000	•000000
169	•840000	•000000	
171	-850000	.000000	-000000
172	855000	.000000	.000000
173	.860000	.000000	.000000
174	865000	.000000	.000000

175	- 870000	-000000	-000000
176	875000		.000000
1 7 7	. 880000		. 000000
176	885000	• • • • • • • • • • • • • • • • • • • •	•••••••••
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100	• 6 9 5 0 0 0	•000000	-000000
101	.900000	.000000	.000000
182	.905000	.000000	•000000
183	•910000	•000000	•000000
184	•915000	•000000	•000000
185	•920000	•000000	•000000
186	.925000	•000000	.000000
187	•930000	•000000	.000000
188	.935000	.000000	.000000
189	.940000	.000000	.000000
190	.945000	.000000	.000000
191	950000	.000000	1000000
192	955000		
101	960000		
104	965000	.000000	
166	970000	•000000	•••••••••
104	0750000	•000000	
190	•975000	.000000	•000000
1.91	• 980000	•000000	
1.48	• 985000	•000000	.000000
199	• 440000	•000000	•000000

1999 - All

SMOOTHED REFERENCE SOLUTION ON COMPUTATIONAL MESH

I	SI	XB	YB	VT	PMFB	TUB
1	.00000	.00000	.00000	.02036	.00000	.00200
2	.00500	.00500	.00000	.42588	.00000	.00200
3	•01000	.01000	.00000	.69975	.00000	.00200
4	.01500	•01500	.00000	.84438	.00000	.00200
5	.02000	.02000	.00000	.92741	.00000	.00200
6	•02500	.02500	.00000	.97717	.00000	.00200
7	.03000	•03000	.00000	1.00792	.00000	.00200
8	• 03500	.03500	.00000	1.02332	.00000	.00200
9	• 04000	.04000	.00000	1.03270	.00000	.00200
10	.04500	.04500	.00000	1.04181	.00000	.00200
11	.05000	.05000	.00000	1.05159	.00000	.00200
12	.05500	.05500	.00000	1.06166	.00000	.00200
13	.06000	• 06000	.00000	1.07182	.00000	•00200
14	•06500	•06500	.00000	1.08206	.00000	.00200
15	07000	.07000	.00000	1.09213	.00000	.00200
16	.07500	.07500	.00000	1.10093	.00000	.00200
17	.08000	.08000	.00000	1.10720	.00000	.00200
18	.08500	.08500	.00000	1.11221	.00000	.00200
19	.09000	.09000	.00000	1.11708	.00000	.00200
20	.09500	.09500	.00000	1.12206	.00000	.00200
21	.10000	.10000	.00000	1.12709	.00000	.00200
22	.10500	.10500	.00000	1.13213	.00000	.00200
23	.11000	.11000	.00000	1.13717	.00000	.00200
24	.11500	.11500	.00000	1.14223	.00000	.00200
25	.12000	.12000	.00000	1.14733	.00000	00200
26	12500	.12500	.00000	1.15239	.00000	.00200
27	•13000	•13000	.00000	1.15704	.00000	.00200
28	13500	.13500	.00000	1.16075	.00000	• 0 C Z C O
29	-14000	.14000	.00000	1.16381	.00000	.00200

	14500	14500	00000	1.16669	. 00000	-00200
	15000	15000	.00000	1,16960	.00000	.00200
12	15500	15500	.00000	1.17253	.00000	.00200
12	16000	16000		1,17547	.00000	.ŏčžóč
14	16500	16500		1.17842	.00000	.00200
15	17000	17000	.00000	1.18136	.00000	.00200
16	17500	17500	.00000	1.18430	.00000	.00200
iž –	18000	18000	.00000	1.18727	.00000	.00200
8	.18500	.18500	.00000	1.19022	•00000	•00200
39	.19000	.19000	.00000	1.19303	.00000	•00200
0	•19500	•19500	.00000	1.19548	.00000	.00200
1	.20000	• 20000	.00000	1.19763	.00000	.00200
12	•20500	• 20500	•00000	1.19968	00000	.00200
•3	.21000	.21000	.00000	1.20174	.00000	•00200
+4	•21500	• 21500	.00000	1 20590	•00000	.00200
+2	• 22000	•22000	•00000	1,20796	.00000	.00200
19	• 22 900	-22000		1.21004	.00000	.00200
8	23500	23500	. 00000	1.21212	.00000	.00200
Lõ	24000	24000	.00000	1.21423	.00000	.00200
5ó	24500	24500	.00000	1.21633	.00000	.00200
51	.25000	.25000	.00000	1.21817	.00000	.00200
52	-25500	.25500	•00000	1.21943	.00000	•00200
53	.26000	.26000	.00000	1.22026	.00000	.00200
24	•26500	.26500	•00000	1.22097	•00000	.00200
22	•27000	• 27000	+00000	1.22109	.00000	.00200
20	• 2/ 500	• 27500	.00000	1 22217	.00000	.00200
58	28500	28500	.00000	1.22392		.00200
.a	-29000	29000		1.22466	.00000	. ŎČŽŎĊ
5ó -	29500	29500	.00000	1.22540	.00000	.00200
51	.30000	.30000	.00000	1.22619	•00000	.00200
52	.30500	.30500	•00000	1.22706	.00000	.00200
53	•31000	.31000	•00000	1.22798	•00000	.00200
54	• 31500	• 31500	.00000	1.22890	.00000	.00200
55	• 32000	.32000	.00000	1.22982	•00000	• • • • • • • • • • • • • • • • • • • •
20	• 32 300	.32300	.00000	1 22165	•00000	.0020
57 58	-33500	.33500	.00000	1.23256	.00000	.0020
šě –	34000	34000	.00000	1.23348	.00000	. ŎŎŽŎ
źó	34500	34500	.00000	1.23439	.00000	.00200
71	35000	.35000	.00000	1.23528	.00000	.00200
72	.35500	•35500	.00000	1.23613	.00000	.0020
73.	.36000	•36000	•00000	1.23696	•00000	•0020
74	•36500	• 36500	•00000	1.23780	.00000	.00200
75.	• 37000	.37000	•00000	1.23003	.00000	.0020
<u>,</u> ,	• 37500	• 37 500	•00000	1 24020	.00000	-0020
79	+ JOUUU 28500	38500	.00000	1.24114	100000	.0020
70	.39000	39000	.00000	1.24198	.00000	0020
κó –	39500	39500	.00000	1.24280	.00000	.0020
B ĭ	40000	.40000	.00000	1.24358	.00000	.0020
82	.40500	.40500	.00000	1.24433	• 00000	.0020
83	.41000	•41000	.00000	1.24506	.00000	•0020
84	•41500	• 41500	•00000	1.24579	• 00000	•0020
85	• 42000	• 42000	.00000	1.24053	+00000	•0020
80	.42500	• 42300	•00000	1 249727	00000	-0020
04 88	-43000 43500	43000	.00000	1.24974	.00000	.0020
89	-44000	• • • • • • • •	00000	1.24948	.00000	10020
ŏ'n	• • • • • • • • • • • • • • • • • • • •	44500		1 25022	00000	. 0 6 2 0

91	45000	-45000	.00000	1.25096	•00000	•00200
ó5	45500	45500		1.25167	. 00000	
74	• • • • • • • • • •	• • • • • • • • • • • • • • • • • • • •	• • • • • • • • • • • • • • • • • • • •	1 5 2 5 3 6		
93	•46000	•46000	.00000	1.27229		•00200
94	.46500	.46500	-00000	1.25284	.00000	•00200
Á É	47000	47000		1 26227	<u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u></u>	00200
92	.4/000	.4/000		1+62221	.00000	• • • • • • • • •
96	•47500	• 47500	.00000	1.25390	•00000	•00200
óž .	48000	48000		1.25443	- 00000	-00200
21	• • • • • • • • • • • • • • • • • • • •	• +0000		1 56/07	• • • • • • • • •	100500
98	•48500	•48500	•00000	1.23490	•00000	•00200
00	49000	- 49000	-00000	1.25549	<u>_00000</u>	. 00200
óó	40500	40500	00000	1 25602		00200
.00	•49500	• 49500	•00000	1.53003	• • • • • • • • • • • • • • • • • • • •	
01	•20000	.50000	.00000	1.25658	•00000	•00200°
ă.	50500	50500	00000	1.25716	- 00000	-00200
	•	• • • • • • • • • • • • • • • • • • • •		1 56756		00200
.03	• 51000		.00000	1+627774	•00000	
04	.51500	-51500	.00000	1.25832	. 00000	•00200
A 6	63000	62000	00000	1 25800	00000	.00200
.05	• 52000	• 92000		1.23070	• • • • • • • • • • • • • • • • • • • •	• • • • • • • • • •
.06	•52500	• 52500	•00000	1.23949	•00000	•00200
07	53000	-53000	0	1.26007	.00000	.00200
X.	53500	63600		1 74044	00000	00200
08	• 23200	• 2 3 2 0 0	•00000	1.20000	• • • • • • • • • • • • • • • • • • • •	• • • • • • • • • • • • • • • • • • • •
.09	• 54000	• 54000	•00000	1.20123		
10	54500	54500	.00000	1.26171	~ 00000	.00200
			• * * * * * * *	1 32 300		00200
		• > > 0 0 0 0	.00000	1.20209	• • • • • • • • • • • • • • • • • • • •	•00200
12	. 55500	• 55500	.00000	1.26242	.00000	•00200
15	56000	56000		1.26275	. 00000	00200
÷ , ,	• • • • • • • • • • • • • • • • • • • •	• • • • • • • • • • • • • • • • • • • •	• • • • • • • • • • • • • • • • • • • •	1 56266	• • • • • • • • • • • •	00200
.1.4 -			.00000	1.50200	.00000	+00200
15	.57000	.57000	.00000	1.26341	.00000	• •00200.
12	67600	67500	00000	1 26375		00200
10	• 97 900	• 57 500	• • • • • • • • • • • • • • • • • • • •	1.20313		00100
.17	•28000			1.20400	• 00000	•00200
18	- 58500	-58500		1226441	.00000	.00200
tň		50000	100000	1 26476	00000	00200
17	• 5 9 0 0 0	. 59000	• • • • • • • • • • • • • • • • • • • •	1.020717	• • • • • • • • • • • • • • • • • • • •	• • • • • • • • • • • • • • • • • • • •
.20	•59500	• 5 9 5 0 0	•00000	1.26511	•00000	•00200·
21	-60000	-60000	-00000	1.26558	.00000	.00200
55	10500	40500		1 34414	00000	00200
	. 60 50 0	.00500	• • • • • • • • • • • • • • • • • • • •	1.20017	•00000	• • • • • • • • • • • • • • • • • • • •
.23	.61000	•61000	•00000	1.20077	.00000	00200
24	61500	-61500	- 00000	1.26733	- 00000	.00200
52	6 2000	62000		1 74 776		00200
22	.02000	.02000	•00000	1.20123	• • • • • • • • • • • • • • • • • • • •	• • • • • • • • • • • • • • • • • • • •
.26	•62500	•62500	.00000	1.26587	.00000	00200
27	63000	-63000	.00000	1.26379	.00000	.00200
5.	() 5000	1 36 00		1 24122	00000	00200
.28	.03200	•03200	•00000	1.20131	• • • • • • • • • •	• • • • • • • • • • • • • • • • • • • •
.29	•64000	•64000	.00000	1.25842	•00000	•00Z00
30	.64500	-64500	-00000	1.25493	- 00000	-00200°
3.4			• • • • • • • • •	1 76061	00000	00200
131	•02000	.02000	•00000	1+22021	• • • • • • • • • • • • • • • • • • • •	• • • • • • • • • • • • • • • • • • • •
32	.65500	•65500	.00000	1.24411	•00000	•0C200
33	66000	-66000	-00000	1,23592	<u>-00000</u>	.00200
	• • • • • • • • • • • • • • • • • • • •	• • • • • • • • •	• • • • • • • • • • • • • • • • • • • •	1 22222		00200
.34 .	.66500	•60500		1.22/24	.00000	•00200
35	•67000	.67000	.00000	1.21908	.00000	•00200
36	67500	67500	. 00000	1.21184	-00000	-00200
20	.07500	• • • • • • • • • • • • • • • • • • • •	• • • • • • • • • • • • • • • • • • • •	1 5 6 6 0 7	• • • • • • • • • • • • • • • • • • • •	
.37	68000	•68000	•00000	1.20499	.00000	.00200
38	- 68500	-68500	.00000	1.19816	• 00000	• 00200
20	60000	40000	00000	1 10140	00000	00200
	.09000	•07000	• • • • • • • • • • • • • • • • • • • •	1.17172	• • • • • • • • • • • • • • • • • • • •	
140	69500	•69500	•00000	1.19205	•••••••	•00200
41	70000	.70000	.00000	1.17928	.00000	•00ZCO
4.5	70600	70500	00000	1.17384		.00200
174	• 10 500	• 10 300	• • • • • • • • • • • • • • • • • • • •	T . T . D	••••••	• • • • • • • • • • • • • • • • • • • •
43	•/1000	•/1000	•00000	1.10841	•00000	•00200
44	.71500	71500	.00000	1.16291	.00000	.00200
45	- 22000	72000		1.15729	100000	.00200
172	• 12000	• • • • • • • • • • • • • • • • • • • •	• 00000	******	• • • • • • • • • • • • • • • • • • • •	• • • • • • • • • • • • • • • • • • • •
146	•72500	. 12500	•00000	1.12124	• 00000	•00200
47	.73000	73000	.00000	1.14586	• 00000	.00200
1.0	73600	72500		1 14004	00000	00200
170	• 13200	• 13300	• • • • • • • • • • • • • • • • • • • •	1.11000	• • • • • • • • • • • • • • • • • • • •	
149	• 74000	. 74000	•00000	1.13418	• 00000	•00200
50	.74500	.74500	.00000	1.12826	.00000	.00200
i ś i	75000	25000	00000	1 12235	. ñññññ	

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152	•75500	•75500	.00000	1.11648	.00000	.00200
153	.76000	.76000	.00000	1.11067	.00000	.00200
154	.76500	.76500	.00000	1.10488	.00000	.00200
155	.77000	.77000	.00000	1.09909	.00000	.0C200
156	.77500	.77500	.00000	1.09334	.00000	.00200
ī5ž	78000	78000	.000000	1.08775	. 00000	. 00200
158	78500	78500	.00000	1.08241		
îšš	79000	79000	.00000	1.07718		
160	79500	79500		1.07196		. 00200
161	80000	80000		1.06665	. 00000	. 00200
162	80500	80500	.00000	1.06117	. 00000	. 00200
163	81000	.81000	.00000	1.05561		. 00200
164	.81500	181500	.00000	1.05000		.00200
165	82000	82000	.00000	1.04431	• • • • • • • • • • • • • • • • • • • •	.00200
166	.82500	82500		1.03848		.00200
167	83000	.83000	.00000	1.03260	. 00000	. 00200
168	.83500	83500	.00000	1.02661		00200
160	84000	000048		1 02026	• • • • • • • • • • • • • • • • • • • •	00200
176	- 84500	.84500	.00000	1.01334		.00200
1 7 ĭ	85000	85000	.000000	1.00618	000000	00200
1 22	.85500	85500		00021	• • • • • • • • • • • • • • • • • • • •	00200
172	86000	86000	.00000	00278		.00200
174	.86500	86500		98676	.00000	.00200
125	87000	87000		98086		00200
176	87500	87500	.00000	97496	. 00000	.00200
177	.88000	- 88000	.00000	96905	. 00000	00200
178	88500	88500	.00000	96318	• • • • • • • • • • • • • • • • • • • •	00200
îżă	.89000	89000	.00000	95740	. 000000	.00200
180	89500	89500	.00000	05166	. 00000	.00200
181		. 90000		94594		.00200
182	90500	. 40500	.00000	94015		.00200
โล้วั	91000	91000	.00000	93416		.00200
184	91500	91500	-00000	92790		.00200
185	92000	92000		92151	. 00000	.00200
186	92500	92500		91513	.00000	.00200
187	93000	93000	.00000	. 00.001		.00200
188	91500	93500	.00000	. 9030£	. 00000	. 00200
189	94000	94000		89740	. 00000	-00200
196 -	94500	94500		.80181		00200
îáĭ	95000	95000	. 00000	.88623		00200
192	95500	95500		88061	. 00000	. 00200
191	96000	96000	.00000	87401		.00200
194	96500	96500	.00000	86906	.00000	-00200
195	97000	97000	.00000	86309		.00200
196	97500	97500	.00000	.85738	. 00000	.00200
197	. 98000	97960	.00000	85325		00200
198	-98500	97960		85200		00200
100	.99000	97960	.00000	85220	00000	•00200
. , ,	• • • • • • • • • • • • • • • • • • • •	• 71 700	•00000	.07663	• • • • • • • • • • • • • • • • • • • •	• • • • • • • • • • • • • • • • • • • •

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*** STREAMWISE LOCATIONS OF BOUNDARY LAYER CALCULATION, BODY RADIUS, FROM SUBROUTINE XBLGRD ***

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M	S	XOCBL	RO
M 123456789012345678901234567890123456789012345678901234567	S 50000100E+00 5050000E+00 5100000E+00 5200000E+00 5200000E+00 53500000E+00 53500000E+00 5400000E+00 5500000E+00 5600000E+00 56500000E+00 57000000E+00 57500000E+00 58500000E+00 58500000E+00 59500000E+00 6000000E+00 60500000E+00 61500000E+00 61500000E+00 61500000E+00 61500000E+00 61500000E+00 61500000E+00 62500000E+00 63500000E+00 64500000E+00 64500000E+00 65500000E+00 645000000E+00 64500000E+00 64500000E+00 64500000E+00 64500000E+00 64500000E+00 64500000E+00 64500000E+00 64500000E+00 645000000E+00 64500000E+00 64500000E+00 64500000E+00 64500000E+00 64500000E+00 64500000E+00 64500000E+00 64500000E+00 64500000E+00 64500000E+00 64500000E+00 64500000E+00 64500000E+00 64500000E+00 6450000	X0CBL 50000100E+00 5100000E+00 5100000E+00 5200000E+00 52500000E+00 53500000E+00 53500000E+00 5400000E+00 5500000E+00 55500000E+00 56500000E+00 56500000E+00 57000000E+00 57500000E+00 59500000E+00 59500000E+00 6000000E+00 6000000E+00 6000000E+00 6000000E+00 6000000E+00 6000000E+00 6000000E+00 6000000E+00 60500000E+00 70000000E+00 7000000E+	R0 100000000000000000000000000000000000
4444455555 5555	• 72000000E+00 • 72500000E+00 • 7300000E+00 • 73500000E+00 • 74000000E+00 • 74500000E+00 • 7500000E+00 • 75500000E+00 • 7600000E+00	.72500000E+00 .72500000E+00 .73500000E+00 .73500000E+00 .74500000E+00 .74500000E+00 .75500000E+00 .75500000E+00 .75500000E+00 .75600000E+00	10000000000000000000000000000000000000
54 55 56 57	•76500000E+00 •77000000E+00 •77500000E+00 •78000000E+00	.76500000E+00 .77000000E+00 .77500000E+00 .78000000E+00	• 10000000E+01 • 10000000E+01 • 10000000E+01 • 10000000E+01

58	.78500000E+00	.78500000E+00	.1000000E+01
59	•7900000E+00	•7900000E+00	•1000000E+01
60	•79500000E+00	•79500000E+00	•10000000E+01
61	•8000000E+00	•8000000E+00	•1000000E+01
62	• 8 0 5 0 0 0 0 0 E + 0 0	+80500000E+00	•1000000E+01
0.5	+0100000E+00	+1500000E+00	10000000000000
65	-82000000E+00	.8200000E+00	10000000000000000000000000000000000000
66	-82500000E+00	.82500000E+00	1000000F+01
- 67	.8300000F+00	.83000000F+00	-10000000F+01
68	.83500000E+00	.83500000E+00	.10000000E+01
69	.8400000E+00	•84000000E+00	•1000000E+01
70	84500000E+00	.84500000E+00	10000000E+01
71	•8500000E+00	•85000000E+00	10000000E+01
72	•85500000E+00	•85500000E+00	•1000000E+01
(3)	•8600000E+00	•86 000000E +00	•1000000E+01
74	•86500000E+00	•86500000E+00	•10000000E+01
76	• 0700000E+00	•8700000E+00	-1000000E+01
- 49	+07500000E+00	•0750000E+00	•10000000E+01
78	-88500000E+00	.88500000E+00	10000000000000
79	-89000000F+00	-8900000E+00	-10000000E+01
80	.89500000F+00	.89500000F+00	1000000E+01
81	•90000000E+00	•9000000E+00	.1000000E+01
82	•90500000E+00	•90500000E+00	.1000000E+01
83	•9100000E+00	•9100000E+00	.1000000E+01
84	•91500000E+00	•91500000E+00	•1000000E+01
85	•9200000E+00	•9200000E+00	•10000000E+01
00	•9250000000000	•92500000E+00	*1000000E+01
89	93000000000000	•93000000E+00	•10000000E+01
80 R	-94000000E+00	-9600000E+00	10000000000000
Ğά	•94500000E+00	-94500000E+00	-10000000E+01
- 91 -	9500000E+00	9500000F+00	1000000F+01
9Ž	•95500000E+00	•95500000E+00	.1000000E+01
93	•9600000E+00	•9600000E+00	.1000000E+01
94	•96500000E+00	+9650000E+00	1000000E+01
95	•9700000E+00	•9700000E+00	1000000E+01
96	•97500000E+00	•97500000E+00	•10000000E+01
97	• 98000000E+00	•97960000E+00	•1000000E+01
40	• 98 900000E +00	9796000000000	
77	• 7 7 0 0 0 0 0 0 2 7 0 0	• 77 90000E+00	•I0000006+01
T(1).	I=1.ISTOP ++ T	ANGENTIAL SURFA	CE VELOCITY ++
. 20)361118E-01 .42	587502E+00 .6	9974665E+00 .8
.10)326985E+01 .10	418054E+01 .1	0515865E+01 .1(
.11	L071978E+01 .11	.122086E+01 .1	1170772E+01 .1

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4438338E+OC .92741105E+00 .97717037E+00 .10079155E+01 .10233201E+01 • 10820591E+01 • 11321336E+01 • 11666916E+01 • 11902215E+01 • 12079620E+01 .10718227E+01 .11270912E+01 0616646E+01 •10921312E+01 •11371735E+01 .11009306E+01 •11422303E+01 •11725311E+01 1220551E+01 •11523902E+01 •11784156E+01 •11996843E+01 •12163270E+01 •11473275E+01 •11754740E+01 .11570372E+01 .11607504E+01 11638072E+01 •11695964E+01 •11843038E+01 •12038129E+01 •11872670E+01 •12058880E+01 •12202554E+01 .11930290E+01 .12100365E+01 .11954789E+01 .12121230E+01 •11813564E+01 •12017419E+01 •11976296E+01 •12142348E+01 •12216866E+01 •12279789E+01 •12352755E+01 •12181662E+01 .īŽŽÓ9657Ē+ŎĪ .12194251E+01 12224271E+01 12163270E+01 12239169E+01 12307304E+01 12377951E+01 12443252E+01 12502202E+01 .12231732E+01 .12298158E+01 •12246563E+01 •12316450E+01 .12254010E+01 .12325609E+01 •12261896E+01 •12334778E+01 .12270632E+01 .12343887E+01 .12288992E+01 •12361266E+01 12419783E+01 12480036E+01 12533712E+01 12369616E+01 12386300E+01 -12394658E+01 +12403025E+01 .12411409E+01 12427992E+01 •12435795E+01 •12494784E+01 •12544307E+01 .12450596E+01 .12509602E+01 .12457942E+01 .12516671E+01 •12465304E+01 •12522913E+01 .12472671E+01 .12528432E+01 124874Ó2E+ŎI .12538994E+01 •12565830E+01 •12612270E+01 •12640778E+01 •12549623E+01 •12594873E+01 12554938E+01 12560301E+01 •12571569E+01 •12617113E+01 .12577395E+01 12583225E+01 .12589045E+01 .12600737E+01 .12620882E+01 •12624186E+01 •12651067E+01 •12606620E+01 •12637458E+01 12627456E+01 •12630774E+01 12634115E+01 -12644054E+01 .12647356E+01 .12673255E+01 ·12658707E+01 •12655760E+01 •12661366E+01 •12549316E+01 •12667675E+01 •12505079E+01 •12672454E+01 •12359210E+01 •12637881E+01 •12190825E+01 •12613663E+01 •12118356E+01 12584187E+01 .12441069E+01

.12272409E+01

1.14

•11850243E+01 •11400624E+01 •10933362E+01 .11684112E+01
.11223511E+01 .11629067E+01 .11913973E+01
.11458577E+01 .11792827E+01 .11738360E+01 .12049893E+01 .11981644E+01 11341824E+01 10877476E+01 .11282649E+01 .11164763E+01 •11572793E+01 11515855E+01 .10771816E+01 .10824060E+01 .10719585E+01 .11106654E+01 .11048784E+01 .10990885E+01 .10611719E+01 -10325951E+01 •10266140E+01 10500030E+01 .10443102E+01 .10384810E+01 .10556068E+01 .10666475E+01 .98675889E+00 .94015169E+00 .99921421E+00 .99277769E+00 -98086357E+00 .97495857E+00 10133428E+01 .10061831E+01 .10202646E+01 92790154E+00 •93416163E+00 •88622597E+00 .96317772E+00 .91513169E+00 •95739597E+00 •90891310E+00 -95166285E+00 -94593812E+00 .96904543E+00 .88060782E+00 90303803E+00 -89739503E+00 .89181324E+00 -92151407E+00 85222938E+00 .85325028E+00 .85200245E+00 .86906174E+00 -86308678E+00 .85737531E+0C -87490564E+00 INITIAL GUESS ON PMF .11667000E+01 .1 .12978000E+01 .12978000E+01 SPMF .6000000E+00 .8000000E+00 -10000000E+01 ONTO COMPUTATIONAL MESH INTERPOLATED PMF DISTRIBUTION FROM INITIAL GUESS .116670000E+01 .11044275E+01 .11077050E+01 .11142600E+01 .11208150E+01 11240925E+01 .111C9825E+01
.11372025E+01 .11175375E+01 •11437575E+01 •11699775E+01 11470350E+01 11732550E+01 •11503125E+01 •11765325E+01 •12027525E+01 .11404800E+01 .11273700E+01 .11306475E+01 .11339250E+01 •11601450E+01 •11863650E+01 •12125850E+01 -11535900E+01 .11667000E+01 •11568675E+01 •11830875E+01 -11634225E+01 11994750E+01 12256950E+01 12519150E+01 11896425E+01 12158625E+01 .11929200E+01 .11961975E+01 .11798100E+01 12289725E+01 .12191400E+01 .12224175E+01 .12060300E+01 12093075E+01 •12551925E+01 •12814125E+01 •12978000E+01 .12453600E+01 .12420825E+01 .12486375E+01 .12322500E+01 .12355275E+01 •12388050E+01 .12748575E+01 .12781350E+01 12683025E+01 .12715800E+01 12650250E+01 12912450E+01 12584700E+01 .12617475E+01 12978000E+01 12978000E+01 12978000E+01 .ī2978000Ē+ŎĪ .12846900E+01 .12879675E+01 .12945225E+01 .12978000E+01 12978000E+01 .12978000E+01 .12978000E+01 .12978000E+01 12978000E+01 -12978000E+01 12978000E+01 12978000E+01 .12978000E+01 .12978000E+01 12978000E+01 .12978000E+01 .12978000E+01 .12978000E+01 .12978000E+01 12978000E+01 12978000E+01 •12978000E+01 •12978000E+01 -12978000E+01 -12978000E+01 .12978000E+01 12978000E+01 .12978000E+01 .12978000E+01 .12978000E+01 .12978000E+01 12978000E+01 -12978000E+01 .12978000E+01 .12978000E+01 12978000E+01 -12978000E+01

*** INITIAL PROFILES ***

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Ν	ETA(N)	F1(N)	SF1(N)	G1(N)	T (N)	
N 12345678901234567890123456789012345678901234567890	ETA(N) .00000E+00 9.26311E-04 1.93599E-03 3.03654E-03 4.23614E-03 5.54370E-03 8.52246E-03 1.02158E-02 1.40734E-02 1.40734E-02 1.40734E-02 1.40734E-02 1.40734E-02 1.40734E-02 2.12620E-02 2.12620E-02 2.41019E-02 2.41019E-02 2.41019E-02 3.05714E-02 3.42491E-02 3.42491E-02 3.42491E-02 3.426274E-02 4.26274E-02 4.26274E-02 4.26274E-02 4.26274E-02 5.82402E-02 5.82402E-02 5.82402E-02 5.82402E-02 5.82402E-02 5.82402E-02 5.82402E-02 5.826263E-01 1.38553E-01 1.51949E-01 1.51949E-01 1.8725E-01 2.39336E-01 2.61803E-01 2.61802E-0	F1(N) .00000E+00 5.77794E-04 1.20750E-03 1.69376E-03 2.64166E-03 3.45672E-03 3.45672E-03 3.45672E-03 5.31289E-03 6.36769E-03 1.01344E-02 1.32419E-02 1.32419E-02 1.32419E-02 1.32419E-02 1.32419E-02 2.13093E-02 2.45953E-02 2.94560E-02 2.945761E-02 3.61702E-02	SF1(N) .00000E+00 6.23002E-04 1.30132E-03 2.84364E-03 3.71857E-03 4.67074E-03 5.70681E-03 6.83401E-03 6.83401E-03 8.06435E-02 1.24197E-02 1.41327E-02 1.41327E-02 1.41327E-02 1.41327E-02 1.41327E-02 2.02108E-02 2.02108E-02 2.02108E-02 2.02108E-02 2.02108E-02 2.02108E-02 2.02108E-02 2.02108E-02 3.10229E+02 3.10229E+02 3.10229E+02 3.78830E-02 4.17426E-02 3.78830E-02 4.59165E-02 5.52968E-02 5.52968E-02 5.52968E-02 5.52968E-02 5.52968E-02 5.52968E-02 7.23024E-02 7.23024E-02 7.885511E-02 7.23024E-02 7.23024E-02 7.885511E-02 7.23024E-02 7.885511E-01 1.10073E-01 1.10073E-01 1.50158E-01 1.50158E-01 1.50158E-01	$\begin{array}{c} G1(N) \\ 1.00000E+00 \\ 1.0000E+00 \\ 1.0000E+00 \\ 1.0000E+00 \\ 1.0000E+00 \\ 1.000E+00 \\ 1.00E+00 \\ 1.0$	T(N) 1.00051E+00 1.00051E+00 1.00051E+00 1.00051E+00 1.00051E+00 1.00051E+00 1.00051E+00 1.00051E+00 1.00051E+00 1.00051E+00 1.00050E+00 1.000050E+00 1.000000 1.000000E+00 1.0000000 1.0000000 1.0000000 1.00000000 1.0000000000	
39 40	2.61803E-01 2.86292E-01	1.60013E-01 1.74626E-01	1.50158E-01 1.61599E-01	9.99993E-01 9.99993E-01	1.00049E+00 1.00048E+00	
+12 423 445	3.12904E-01 3.42079E-01 3.73792E-01 4.08360E-01 4.46039E-01	2.07669E-01 2.26293E-01 2.46457E-01 2.68264E-01	1.86037E-01 1.98932E-01 2.12170E-01 2.25637E-01	9.99993E-01 9.99992E-01 9.99992E-01 9.99992E-01 9.99993E-01	1.00048E+00 1.00048E+00 1.00047E+00 1.00047E+00 1.00046E+00	
467 489	4.87109E-01 5.31875E-01 5.80670E-01 6.33856E-01	2.91822E-01 3.17235E-01 3.44603E-01 3.74012E-01	2.39185E-01 2.52621E-01 2.65709E-01 2.78154E-01	9.99993E-01 9.99993E-01 9.99994E-01 9.99994E-01 9.99995E-01	1.00046E+00 1.00045E+00 1.00044E+00 1.00043E+00	
50 51 52 53 54	6.91830E-01 7.55021E-01 8.23899E-01 8.98976E-01 9.80810E-01	4.05535E-01 4.39216E-01 4.75062E-01 5.13027E-01 5.52996E-01	2.89602E-01 2.99631E-01 3.07750E-01 3.13398E-01 3.15959E-01	9.99996E-01 9.99997E-01 9.99999E-01 1.000C0E+00	1.00042E+00 1.00041E+00 1.00039E+00 1.00037E+00 1.00036E+00	
55 56 57	1.07001E+00 1.16724E+00 1.27321E+00	5.94762E-01 6.33001E-01 6.82247E-01	3.14780E-01 3.09208E-01 2.98653E-01	1.000C1E+00 1.000C1E+00 1.000C1E+00	1.00033E+00 1.00031E+00 1.00023E+00	

				1 000035.000	1 000345400
28	1.308/3E+00	1.200095-01	2.020/45-01	1.000022400	1.000202400
59	1.51464E+00	7.710562-01	2.010916-01	1.000022+00	1.000236+00
60	1.65189E+00	8.13824E-01	2.34128E-01	L.00002E+00	1.00019E+00
61	1.80148E+00	8.54050E-01	2.02537E-01	1.00003E+00	1.00016E+00
62	1.96454E+00	8.90560E-01	1.67705E-01	1.00003E+00	1.00013E+00
63 \	2.14228E+00	9.22255E-01	1.31635E-01	1.00003E+00	1.00010E+00
64	2.33601E+00	9.48295E-01	9.67800E-02	1.00002E+00	1.00007E+00
65	2.54717E+00	9.68280E-01	6.56618E-02	1.000C2E+00	1.00005E+00
66	2.77735E+00	9.82381E-01	4.03469E-02	1.000C2E+00	1.00003E+00
67	3.02823F+00	9,91348E-01	2.19190E-02	1.000C1E+00	1.00002E+00
68	3.30170F+00	9,96362E-01	1.01972E-02	1.000C1E+00	1.00001E+00
ěå	3.59978E+00	9.98747F-01	3.885428-03	1.000C0E+00	1.00000E+00
76	3,924695+00	9.99669E-01	1.13344E-03	1.000COF+00	1.00000E+00
21	4 27884E+00	9.49941E-01	2.25148E-04	1.000C0E+00	1,00000F+00
	4.66486E+00	0 000045-01	2.328755-05	1.000COF+00	1.00000F+00
72	5 085626+00	1.000005+00	1.847575-07	1.00000E+00	1.00000E+00
7%	5 546755400	1 00000000000	-1 501226-08	1.00000000000	1.00000E+00
75	5 06616E+00	1 00000000000	2 005415-00		1.0000000000
12	6 680066400	1 00000000000	-1 125425-00	1.000005+00	1.0000000000
49	3 103000 100	1.000002.00			1 00000000000
11	7 . 10300E . 00	1.0000000000000000000000000000000000000			1 00000000000
18	7.83040E+00	1.00000000000	-3.320//E-10		
	8-536062+00	1.00000000000	-2. /21025-10		
80 .	9.30524E+00	1.00000E+00	-2.184215-10	1.0000000000000000000000000000000000000	
81	1.01436E+01	1.00000E+00	-2.83120E-10	T-00000E+00	1.00000000000
82	1.10575E+01	1.00000E+00	-2.78171E-10	1.0000000000	1.00000000000
83	1.20536E+01	1.00000E+00	-2.80746E-10	1.000C0E+00	1.00000E+00
84	1.31393E+01	1.00000E+00	-2.80964E-10	1.00000E+00	1.00000E+00
85	1.43228E+01	1.00000E+00	-2.78622E-10	1.000C0E+00	1.00000E+00
86	1.56128E+01	1.00000E+00	-2.83407E-10	1.00000E+00	1.00000E+00
87	1.70189E+01	1.00000E+00	-2.77132E-10	1.000C0E+00	1.00000E+00
88 -	1.85515E+01	1.00000E+00	-2.83190E-10	1.00000E+00	1.00000E+00
89	2.02220E+01	1.00000E+00	-2.77933E-10	1.000C0E+00	1.00000E+00
-90	2.20430E+01	1.00000E+00	-2.82266E-10	1.000COE+00	1.00000E+00
91	2.40277E+01	1.00000E+00	-2.80140E-10	1.00000E+00	1.00000E+00
9Ž	2.61912E+01	1.00000E+00	-2.81208E-10	1.000COE+00	1.00000E+00
93	2.85493E+01	1.00000E+00	-2.83951E-10	1.000COE+00	1.00000E+00
94	3.11197E+01	1.00000E+00	-2.78758E-10	1.000COE+00	1.00000E+00
95	3.39214E+01	1.00000E+00	-2.85528E-10	1.000COE+00	1.00000E+00
96	3.69752E+01	1.00000E+00	-2.79979E-10	1.000C0E+00	1.00000E+00
97	4.03039E+01	1.00000E+00	-2.87555E-10	1.000C0E+00	1.00000Ē+00
98	4.39322E+01	1.00000E+00	-2.84034E-10	1.00000000000	1.00000E+00
ģğ	4.78870F+01	1.00000F+00	-2,90819E-10	1.000COE+00	1.00000E+00
100	5.21978F+01	1.00000F+00	- 00000F+00	1.00000E+00	1.00000E+00
		2000000000000			

		*** SUMM/	ARY OF CONVER	GENCE HISTORY	***			and the second	
INTRAC	DDTMAX	RMSDT	SMDT	DUEPAX	RMSUE	SMUE	DSFMAX	DEMAX	DGMAX
2	71076E+00	.24873E-01	•99000E+00	.97713E-01	•60667E-02	.70000E+00	+15504E+01	28723E+00	17674E-04
		*** SUMMA	RY OF CONVER	GENCE HISTORY	***				
INTRAC	DDTMAX	RMSDT	SMDT	DUEMAX	RMSUE	SMUE	DSFMAX	DFMAX	DGMAX
3	27173E+00	•95139E-02	•99000E+00	45837E-01	.25718E-02	.99000E+00	•56745E+00	•12014E+00	89486E-05

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	4 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	EDGE QUAN MREF = REYREF = 2 TE2 =15 RO2 = ME1 = RHDE1 =	TITIES .04000 000000.0 62.25889 1.00000 .04880 .9996	IN VISMFK AT D TREFD D ME2 9 RH0E2 0 GE2 0 GE2 0 UE1 1 R01	STATION M= 4 = 530.00000 = .04870 = .99961 = .00346 = 1.21979 = 1.00000	4 TREF =1 UE2 = TU2 = MUE2 = TE1 =1 QE1 =	562.50000 1.21747 .00200 .99988 562.25605 .00346					
	44	MFK QUANT ACLINF = AIMFKN = DELTUZ = DTINCI = NINNER = PDI110 = PSI31N = RTAU = .71500E+0	ITIES II 2.12620 .12000 6.4498 3.8139 5 .12666 .5741 6.4552 C 11	N VISMFK AT 9 ALINFN 0 ALMFK0 10 BLTHK 3 DELTU1 2 VEDGE 7 PSI11N 8 PSI120 9 PSI32N 5 RTHEAT 45421E+01	STATION M= 44 = .15269 = .12000 = 6.44983 = 6.45033 =01328 = .11757 = .00000 = .00000 = .251.29068 45421E+013	ALINFO = A2MFK = DELIN = DTINC2 = NDELTU = PSI12N = PSI2IN = EMFK = A2MA3N = 1380E+00 - 31	$\begin{array}{r} \bullet 09019\\ \bullet 50000\\ 4\cdot 39527\\ 3\cdot 73176\\ \bullet 61\\ \bullet 0000\\ \bullet 06090\\ \bullet 00011\\ \bullet 30000\\ 371E+00 \bullet 1\end{array}$	2175E+01 •48	702E-01 •553	30E-03 -•4	3160E-03***	910.651
•.	PROF	ILES AT M=	44 S	(M)=R 7.15	000E-01 INVR	SE= 1 PMF(M)	= 4.54211	E+00 BETA(M)	-3.13798E-	01		
	N	ETA(N)	E+00	YBL(N)	F2(N)	SF2(N)	G2(N)	EPSBAI E+00 1,0000	R(N) RHOM NF+00 9,998	UR(N) 1 92F-01 1	(N) .00047E+00	
	23456789011234567890112345678901123345678901333333333333333333333333333333333333	9.293594 1.093594 3.236170 6.5962468 1.0206151 1.0226155 1.0226155 1.0226155 1.0426563 1.0426563 1.0426563 1.042656219 2.017714 3.0826979 4.02586082 7.0844735 1.0864593 1.0265553 1.026555555555555555555555555555555555555	-04 -04 -03 -03 -03 -03 -03 -03 -02 -02 -02 -02 -02 -02 -02 -02	2.44577E-06 5.11166E-06 5.11164E-06 1.1164E-06 1.11848E-05 1.46372E-05 2.25022E-05 2.25073E-05 3.18485E-05 3.715845E-05 4.29485E-05 5.61387E-05 5.636370E-05 5.636370E-05 5.636370E-05 7.1810E-05 8.07187E-05 8.07187E-05 9.04292E-04 1.255126E-04 1.255126E-04 1.3883E-04 1.383874E-04 1.383774E-04 1.383774E-04 2.51236E-04 2.51237E-04 2.51236E-04 2.51236E-04 1.36377E-04 3.33377E-04 3.65826E-04 4.39773E-04 3.65826E-04 4.39773E-04 5.27578E-04	-8.64058E-04 -1.79956E-03 -2.81174E-03 -3.90609E-03 -5.08836E-03 -6.36448E-03 -7.74056E-03 -7.74056E-03 -1.08176E-02 -1.25313E-02 -1.43699E-02 -1.43699E-02 -1.63394E-02 -2.30870E-02 -2.30870E-02 -2.30870E-02 -2.30870E-02 -3.11712E-02 -3.41691E-02 -5.88004E-02 -5.49791E-02 -6.265982E-02 -7.42479E-02 -7.79516E-02 -8.46726E-02 -8.91858E-02 -8.91858E-02	$\begin{array}{c} -3 \cdot 00618E - 0\\ -6 \cdot 25775E + 0\\ -9 \cdot 77214E - 0\\ -1 \cdot 756625E + 0\\ -2 \cdot 68296E - 0\\ -2 \cdot 68296E - 0\\ -3 \cdot 74296E - 0\\ -3 \cdot 74296E - 0\\ -4 \cdot 961587E - 0\\ -4 \cdot 961587E - 0\\ -6 \cdot 353895E - 0\\ -7 \cdot 11855E - 0\\ -7 \cdot 11855E - 0\\ -7 \cdot 93035E - 0\\ -1 \cdot 26993E - 0\\ -1 \cdot 26993E - 0\\ -1 \cdot 846523E - 0\\ -1 \cdot 84657E - 0\\ -1 \cdot 84657E - 0\\ -2 \cdot 21277E - 0\\ -2 \cdot 33279E - 0\\ -2 \cdot 56143E - 0\\ -2 \cdot 888842E - 0\\ -2 \cdot 88$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{c} +00 & 1.0000 \\ +00 & 1.000000 \\ +00 & 1.00000 \\ +00 & 1.00000 \\ +00 & 1.00000 \\ +00 & 1.00000 \\ +00 & 1.00000 \\ +00 & 1.000000 \\ +00 & 1.000000 \\ +00 & 1.000000 \\ +00 & 1.000000 \\ +00 & 1.000000 \\ +00 & 1.000000 \\ +00 & 1.000000 \\ +00 & 1.000000 \\ +00 & 1.000000 \\ +00 & 1.000000 \\ +00 & 1.000000 \\ +00 & 1.000000 \\ +00 & 1.0000000 \\ +00 & 1.000000 \\ +00 & 1.000000 \\ +00 & 1$	$\begin{array}{c} 2 + 0 \\ 9 + 9 \\ 9 \\ 2 \\ 2 \\ 2 \\ 2 \\ 2 \\ 2 \\ 2 \\ 2 \\$	92E-01 1 92E-01 1 93E-01 1 93E-01 1 93E-01 1 93E-01 1 93E-01 1 93E-01 1 93E-01 1 93E-01 1	,00047E+00 ,00047E+00	

				1 00100F 01	0 000005 01	1 001885+00	0 000025-01	1 000475400
37 -	2.18/256-01	5.//5U6E-04	-8.93890E-UZ	-2.843885-01	A.44444E-01	1.001000-00	7.770735-01	1.000472400
38	2.39336E-01	6.31927E-04	-8.64654E-02	-2.81556E-01	9.99999E-01	1.06579E+00 -	9.99893E-01	1.000476+00
5ŏ	5 618035-01	6.01246E-04	-7.938175-02	-2.630815-01	9.999995-01	1.52142E+00	9,99893F-01	1.00047E+00
27	2.010030-01			-2 412515-01	ó óóóóóé - ő î	2 945575400	0 000025-01	1 00047E+00
40	2.862926-01	1.559046-04	-/.V/408E-02	-2+41271E-UI	A+AAAADE-01	2.043375+00	7. 77073E-UL	1.000472400
41	3.12984E-01	8.26381F-04	-6.14452E-02	-2.18596E-01	9.99998E-01	4.03030E+00	9.998936-01	1.000472+00
. 5	2 4 20 20 5 - 01	0 022016-04	-5 055505-02	-1.031125-01	0.000075-01	4.89872F+00	9-99893E-01	1.00047F+00
12	3.420775-01	7.032010-07				6 640046400		1 000475400
43	3./3/922-01	9.86934E-04	-3.700046-02	-1-030516-01	3.33341E-01	3.74904E+00	4.99093E-UI	1.000472400
44	4.08360F-01	1.07820F-03	-2.01766E-02	-1.27193E-01	9.99996E-01	6.24939E+00	9.99893E-01	1.000472+00
	4 440206-01	1 177605-02	7 270055-04	-8 553 205-02	0.000055-01	6.955896+00	9,998935-01	1.00047E+00
+2	4.400396-01	1+1//090-03	1.210752-07					1 000475400
+6	4.8/1096-01	1.28613E-03	2.622896-02	-3.820608-02	A*AAAA2E-01	1+00/325+00	A. 440435-01	1.000476400
47	5-31875F-01	1.40432E-03	5.72639E-02	1.47507E-02	9.99994E-01	8.44469E+00	-9.99894E-01	1.000476+00
	5 904 70E-01	1 622146-02	a 40270E-02	7.288145-02	0.000015-01	9,28905F+00	9,99895F-01	1.00046E+00
+0	3.00070E=01	1.033105-03	7.772105-02	1.200140-02				1 00044 6400
¥9	6.338562-01	1.6/3586-03	1.907486-01	1.371936-01	4.44443E=01	1.021105-01	7.770700-01	1.000402+00
50	6-91830E-01	1.82665F-03	1.95612E-01	1.99744E-01	9.99992E-01	1.12007E+01	9.99898E-01	1.000456+00
. i	7 550215-01	1 003405-03	2 615085-01	2.631756-01	0.000036-01	1,22149F+01	9-99901F-01	1.00044F+00
<u>, </u>	1	1.773776-03				1 214445+01	0 00045-01	1 000415400
22	8.238996-01	2+1/3348-03	3.340015-01	3.202226-01	A+ 44 44 2E - 0 T	1+310776-01	7.77700L-01	1.000410.000
53	8,98976F-01	2.37356F-03	4.29741E-01	3.63547E-01	9.99999E-01	1.38956E+01	9.99912E-01	1.000346+00
	0 909105-01	2 580605-02	5 302315-01	3 84389F-01	1.00000E+00	1,41915E+01	9.99921F-01	1.00035E+00
22	3.00010E-01	2.00000000		3 747746-01	1 000015.00	1 200005101	ó óóó 22E_01	1 000296+00
לכ	1.070016+00	2.027006-03	0.307/32-01	3.14/14E-01	1.000012+00	1.3000000000	7.777336-01	
56	1.167248+00	3.08174E-03	7.41248E-01	3.31328E-01	1.00002E+00	1.256906+01	9.99947E-01	1.000236+00
E ž	1 272216400	3 361485-03	8.34760F-01	2.59426E-01	1.00002E+00	1.04835F+01	9-99962E-01	1.00017E+00
21	1.273211-00				1 000035.00	7 944765+00	0 000745-01	1.000116+00
28	1.388/3E+00	3.666.386-03	A*08312F-01	1.142006-01	1.000022+00	1.044725400	7. 777700-01	1.000112.00
59	1.51464E+00	3.99870E-03	9.574248-01	9.71536E-02	1.00002E+00	5.193176+00	A*AAA80E-01	1.0000000000
Ľ۵.	1.651895+00	4.36091E-03	9.84190F-01	4.27312E-02	1.00001E+00	3.09693E+00	9.99994E-01	1.00003E+00
yv .				1 166667 01	1 000015400	1 025155+00	0 00075-01	1.00001E+00
51	1.801486+00	4.137126-03	4.42010E-01	1.303375-02	1.000012-00	1.023136+00	7.777712-01	
52 -	1.96454E+00	5.18605E-03	9.99334E-01	2.379.40E-03	1.00000E+00	1.241656+00	A. 44444E-01	1.0000000000
53	2 14228 EADO	5.655116-03	1.00005E+00	-2.596975-04	1.00000F+00	1.04350E+00	1.00000E+00	1.00000E+00
					1 000005.00	1 000346+00	1.00000E+00	1.00000E+00
54	2.336016+00	0.100305-03	1.000025+00	-2+334405-04	1.000002+00			
65	2.54717E+00	6.72367E-03	9.999998-01	8.20406E-06	T*00000E+00	1.002452+00	1.0000000000	1.00000000000
66	2.77735E+00	7.33111F-03	9,99995F-01	3,38101E-05	1.00000E+00	1.00021E+00	1.00000E+00	1.00000E+00
22	5 0 2 9 3 2 5 4 0 0	2 002225	1 000005.00	-1 435405-06	1 000005+00	1.000236+00	1.00000E+00	1,00000F+00
01	3.020232700	1.993222-03	1.0000000000000000000000000000000000000	-1.433075-00			1 0000000 000	1 00000000000
58	3.301/0E+00	8.714936-03	T*00000E+00	-0.3/2426-00	1.000005+00	1.000032+00	1.00000000000	
69	3,59978E+00	9,50158F-03	1.00000E+00	1.04511E-06	1.00000E+00	1.00003E+00	1.00000E+00	T*00000E+00
žó	3 074405400	1 035005-03	1 000005.00	1 212728-06	1.000005400	1.00000E+00	1.00000E+00	1_00000F+00
<u>r</u> <u>v</u>	3.924092400	1.033305-02	1.000000000000	1.212720-00			1 000005+00	1 000005.00
11	4.278846+00	1.129376-02	1.00000E+00	-/.194856-0/	1.00000E+00	1.000012+00	1.000000000000	1.00000000000
72	4.66486E+00	1.23124E-02	1.00000E+00	-2.39006E-07	1.00000E+00	1.00000E+00	T*00000E+00	1.000006+00
72	5 085625+00	1.342285-02	1.0000E+00	1.97365E-07	1.00000E+00	1.00000F+00	1.00000E+00	1.00000E+00
<u>,</u> ,	J. 00 JOZE + 00	1. 172202-02				1 000005 000	1 000005+00	1.0000000+00
£9	2.24422E+UU	1.403326-02	1.00000000000	-1-204000-07	1.00000000000	1.0000000000000000000000000000000000000		
75	6.04416E+00	1.59525E-02	1.00000E+00	-1.39239E-07	1.00000E+00	T*00000E+00	T-00000E+00	1.0000000000
76	6-58906E+00	1,73905E-02	1,00000E+00	-6.12036E-09	1.00000E+00	1.00000E+00	1.00000E+00	1.00000E+00
<u>'</u>				-0.00015-09	1 000005.00	1 00000000000	1.00000E+00	1_00000F+00
(!	1.10300E+00	1.097000-02	1.00000000000	-4.00001E-00	1.00000000000			
78 -	7.83040E+00	2.06665E-02	1.00000E+00	-9.273568-08	I.00000E+00	1.000005+00	1.0000000000	1.000002+00
79	8-53606F+00	2-25288F-02	1.00000F+00	-4,98450E-08	1.00000E+00	1.00000E+00	1.00000E+00	T*00000E+00
à Á	0 205265400	2 765885-02	1 00000E+00	-9 43845E-08	1.00000E+00	1.0000E+00	1,00000F+00	1.00000E+00
20	7. 30 32 4 2 4 00	2.777000-02					1 000005+00	1 00000E+00
51	1.014368401	2.0//146-02	T.00000E+00	-/.031106-08	1.0000000000	1.00000000000	T. 00000E+00	
82	1.10575E+01	2.91831E-02	1.00000E+00	-7.39964E-08	1.00000E+00	1.00000E+00	T*00000E+00	T*00000E+00
22	1 205268+01	3 181195-02	1.00000E+00	-8.15067E-08	1,00000E+00	1,00000F+00	1.00000E+00	1.00000E+00
2.7				7 13717 00	1 0000000000000000000000000000000000000		1 00000E+00	1.00000E+00
54	1.313936+01	3.40//3E-UZ	1.00000000000	-/.12/1/2-00	1.0000000000	1.00000000000		
85	1.43228E+01	3.78005E-02	1.00000E+00	-8.00130E-08	1.00000E+00	I.00000E+00	T*00000E+00	1.00000000000
ÄÄ	1.56128E+01	4.12049F-02	1,00000E+00	-7.33403E-08	1.00000F+00	1.00000E+00	1.00000E+00	1.00000E+00
24				7 000125 09	1 000005+00	1 000005+00	1 00000E+00	1.00000E+00
5 (T . LOT 0 A F + OT	4.471702-02	1.000005+00	-1+404146-00	1.0000000000000000000000000000000000000	1.0000000000000000000000000000000000000		1 0000000000000000000000000000000000000
38	1.85515E+01	4.89604E-02	1.00000E+00	-7.29716E-08	T*00000F+00	T*00000F+00	T-000005+00	T+00000E+00
à ũ	2.02220E+01	5.336916-02	1.00000E+00	-8-01457F-08	1.00000E+00	1.00000E+00	1.00000E+00	1.00000E+00
56		5 01766E 02	1 0000000000000000000000000000000000000	- 7 10270E-00	1 00000000000	1.00000F+00	1.00000E+00	1.00000F+00
10	2.204302+01	2.01/405-02	T+00000E+00	-1+135135-00	1.0000000000000000000000000000000000000	1.0000000000000000000000000000000000000	1 000000000000	1 000005+00
91	2.40277E+01	6.34127E-02	-1+00000E+00	-8.07270E-08	T*00000F+00	T*00006+00	T+00000E+00	T+00000E+00
9ž –	2.619126+01	6-91221E-02	1.00000F+00	-7-19720E-08	1.00000E+00	1.00000E+00	1.00000E+00	T*00000F+00
5.	2 954021401	7 632525	1 000005.00	-8 013385-09	1.000005+00	1.00000F+00	1.00000F+00	1.00000E+00
7)	2.034335701	1.004045-02	1.00000E+00			1 0000000000	1 000005100	1.0000000+000
94	3.111976+01	8.212886-02	T+00000E+00	-(.296125-08	T*00000F+00	1.00000E+00	1.0000000000000000000000000000000000000	
95	3.39214F+01	8.95228E-02	1.00000E+00	-7.89910E-08	1.00000E+00	1.00000E+00	T*0000F+00	T+00000E+00
96	3.697528+01	9.758216-02	1.00000 +00	-7-41.798E-08	1.00000E+00	1.00000E+00	1.00000E+00	1.00000E+00
			1 000000000000	7 704045 00	1 000000 .000		1.000005+00	1.00000F+00
47	4 . () 1() 1() 1() + () (1.0010000000000000000000000000000000000	7		エルリリリリリモモリリ	1.0000000700		

Sec. 2

98 99 100 N	4.39322E+01 4.78870E+01 5.21978E+01 YN(N)	1.15942E-01 1.26379E-01 1.37756E-01 YPLUS(N)	1.00000E+00 1.00000E+00 1.00000E+00 DUDY(N)	-7.52281E-08 -7.741C4E-08 .000C0E+00 TAU(N)	1.00000E+00 1.00000E+00 1.00000E+00 DAMP(N)	1.00000E+00 1.00000E+00 1.00000E+00 FUN(N)	1.00000E+00 1.00000E+00 1.00000E+00 FMFK(N)	1.00000E+00 1.00000E+00 1.00000E+00 EPSBAR(N)
1 2 3 4 5 6 7 8	.00000E+00 3.45884E-03 7.22898E-03 1.13384E-02 1.58177E-02 2.07002E-02 2.60220E-02 3.18229E-02	.00000E+00 7.15787E-02 1.49073E-01 2.32916E-01 3.23557E-01 4.21465E-01 5.27124E-01 6.41031E-01	2.50733E-01 2.49009E-01 2.47259E-01 2.45353E-01 2.43277E-01 2.41018E-01 2.38560E-01 2.35887E-01	3.05334E-01 3.03235E-01 3.01106E-01 2.98789E-01 2.96268E-01 2.93527E-01 2.90547E-01 2.90547E-01	2.01996E-03 2.07795E-03 2.14242E-03 2.29428E-03 2.38370E-03 2.48373E-03 2.5581E-03	.00000E+00 9.48546E-05 4.14246E-04 1.01867E-03 1.98125E-03 3.38992E-03 5.35001E-03 7.98697E-03	.00000E+00 .00000E+00 .00000E+00 .00000E+00 .00000E+00 .00000E+00 .00000E+00	1.00000E+00 1.00000E+00 1.00001E+00 1.00002E+00 1.00004E+00 1.00008E+00 1.00013E+00 1.00020F+00
9 10 11 12 13 14 15 16	3.81458E-02 4.50377E-02 5.25499E-02 6.07383E-02 6.96636E-02 7.93921E-02 8.99963E-02 1.01555E-01	7.63687E-01 8.95598E-01 1.03726E+00 1.18915E+00 1.35174E+00 1.52543E+00 1.71058E+00 1.9750E+00	2.32981E-01 2.29826E-01 2.26402E-01 2.26402E-01 2.2690E-01 2.18671E-01 2.14326E-01 2.09636E-01 2.04582E-01	2.83800E-01 2.79992E-01 2.75869E-01 2.71409E-01 2.66591E-01 2.61397E-01 2.55807E-01 2.49805E-01	2.72158E-03 2.86296E-03 3.02214E-03 3.20164E-03 3.40435E-03 3.63358E-03 3.63358E-03 3.89311E-03 4.18722E-03	1.14495E-02 1.59125E-02 2.15805E-02 2.86905E-02 3.75140E-02 4.83588E-02 6.15678E-02 7.75158E-02	.00000E+00 .00000E+00 .00000E+00 .00000E+00 .00000E+00 .00000E+00 .00000E+00 .00000E+00	1.00029E+00 1.00042E+00 1.00060E+00 1.00083E+00 1.00113E+00 1.00153E+00 1.00270E+00
17 18 19 20 21 22 23 24	1.14154E-01 1.27886E-01 1.42855E-01 1.59171E-01 1.76955E-01 1.96339E-01 2.17469E-01 2.40500E-01	2.11637E+00 2.33727E+00 2.57014E+00 2.81476E+00 3.07068E+00 3.33722E+00 3.61342E+00 3.81792E+00	1.99150E-01 1.93325E-01 1.87098E-01 1.80464E-01 1.73424E-01 1.65989E-01 1.58175E-01 1.58008E-01	2.43375E-01 2.36506E-01 2.29191E-01 2.1426E-01 2.13215E-01 2.04563E-01 1.95485E-01 1.85999F-01	4.52077E-03 4.89916E-03 5.32839E-03 5.81495E-03 6.36582E-03 6.98818E-03 7.68914E-03 8.47520E-03	9.66026E-02 1.19240E-01 1.45833E-01 1.76754E-01 2.12304E-01 2.52672E-01 2.97885E-01 3.47754E-01	.00000E+00 .00000E+00 .00000E+00 .00000E+00 .00000E+00 .00000E+00 .00000E+00 .00000E+00	1.00353E+00 1.00460E+00 1.00593E+00 1.00757E+00 1.00959E+00 1.01201E+00 1.01488E+00 1.01488E+00
25 26 27 28 29 30 31	2.65604E-01 2.92967E-01 3.22793E-01 3.90739E-01 4.29364E-01 4.71466E-01 5.17356E-01	4.18897E+00 4.48418E+00 4.78039E+00 5.07328E+00 5.35677E+00 5.62193E+00 5.85488E+00 6.03251E+00	1.41523E-01 1.32762E-01 1.23766E-01 1.41575E-01 1.05212E-01 9.56703E-02 8.58889E-02 8.58889E-02	1.76124E-01 1.65883E-01 1.55293E-01 1.44362E-01 1.33077E-01 1.21392E-01 1.09196E-01 9.6688E-02	9.35143E-03 1.03202E-02 1.13790E-02 1.25175E-02 1.37122E-02 1.49173E-02 1.60501E-02 1.60501E-02	4.01826E-01 4.59356E-01 5.19299E-01 5.80336E-01 6.40953E-01 6.99547E-01 7.54567E-01 8.04664E-01	00000E+00 00000E+00 00000E+00 00000E+00 00000E+00 00000E+00 00000E+00 00000E+00 00000E+00 00000E+00	1.02195E+00 1.02605E+00 1.03036E+00 1.03467E+00 1.03867E+00 1.04196E+00 1.04402E+00 1.04402E+00
334 335 376 378 390	5.67377E-01 6.21900E-01 6.81330E-01 7.46108E-01 8.16716E-01 8.93680E-01 9.77569E-01	6.11209E+00 6.00884E+00 5.51945E+00 3.94680E+00 4.37856E+00 9.38607E+00 1.49291E+01	6.47817E-02 5.23775E-02 3.70819E-02 1.59759E-02 1.66804E-02 6.01834E-02 8.92527E-02 8.92527E-02	8 • 21684E -02 6 • 61013E -02 4 • 64671E -02 1 • 98133E -02 2 • 03511E -02 7 • 81039E -02 1 • 65135E -01	1.73858E-02 1.73858E-02 1.73858E-02 1.73858E-02 1.73858E-02 1.73858E-02 1.73858E-02 1.73858E-02 1.56517E-01 1.56517E-01	8.48822E-01 8.86442E-01 9.17374E-01 9.41883E-01 9.60571E-01 9.74259E-01 9.83873E-01 9.83873E-01	•00000E+00 •00000E+00 •00000E+00 •00000E+00 •00000E+00 •00000E+00 •00000E+00	1.04158E+00 1.03634E+00 1.02901E+00 1.01842E+00 1.00188E+00 1.06579E+00 1.52142E+00 2.84557E+00
41 42 445 467	1.16868E+00 1.27732E+00 1.39574E+00 1.52481E+00 1.66550E+00 1.81886E+00 1.98601E+00	2.203392+01 3.01652E+01 4.76247E+01 5.89999E+01 7.21964E+01 8.75177E+01 1.05890E+02	9.66024E-02 1.06699E-01 1.22001E-01 1.39415E-01 1.57055E-01 1.75563E-01 1.95737E-01	4.71725E-01 6.39758E-01 8.24379E-01 1.06008E+00 1.6393LE+00 2.01286E+00	8.14781E-01 9.72846E-01 9.99997E-01 1.00000E+00 1.00000E+00 1.00000E+00	9.94473E-01 9.96999E-01 9.98458E-01 9.99254E-01 9.99662E-01 9.99858E-01 9.99944E-01	•00000E+00 •00000E+00 •00000E+00 •00000E+00 •00000E+00 •00000E+00 •00000E+00	4.03030E+00 4.89872E+00 5.54904E+00 6.24939E+00 6.9589E+00 7.66735E+00 8.44469E+00
49 552 553 555 555	2 • 10021E + 00 2 • 36661E + 00 2 • 58327E + 00 2 • 81922E + 00 3 • 07640E + 00 3 • 35672E + 00 3 • 35672E + 00 3 • 94527E + 00	1.54146E+02 1.54146E+02 2.20430E+02 2.58594E+02 2.95880E+02 3.25868E+02 3.39819E+02 3.39819E+02	2.17/20E-01 2.41516E-01 2.66475E-01 2.90985E-01 3.12043E-01 3.25062E-01 3.24318E-01 3.04522E-01	2 • 462 / 5E +00 3 • 00 3 25E +00 3 • 634 60E +00 4 • 32824E +00 5 • 00216E +00 5 • 5C017E +00 5 • 60427E +00 5 • 12009E +00	1.00000E+00 1.00000E+00 1.00000E+00 1.00000E+00 1.00000E+00 1.00000E+00 1.00000E+00 1.00000E+00	9.99998-01 9.99998-01 9.99998-01 1.00000E+00 1.00000E+00 1.00000E+00	.00000E+00 .00000E+00 .00000E+00 .00000E+00 .00000E+00 .00000E+00 .00000E+00	1.02116E+01 1.12007E+01 1.22149E+01 1.31644E+01 1.38956E+01 1.41915E+01 1.38088E+01 1.38088E+01

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			A ALAAFE 61	2 /151/5.00	1 000005400	1 000005+00	000005400	1.048356401
57	4.753852+00	Z.89020E+02	と。いうガリンヒーリエ	2.017106400	1.0000000000	T*OOOOC+OO	• UUUUUE + UU	Tendagirant
E Ó	5 19506 EAOO	2 246026402	1 280615-01	1.327136+00	1.000006+00	1,00000F+00	_00000F+00	7 844752+00
20	2.102045400	20247025402	1.007010-01			5° 6 6 6 6 7 . 6 6		6 102176+00
50	5.65501F+00	1.50741E+02	7.94973E-02	5.025846-01	1.00000E+00	1.00000000000	• UUUUUE + UU	3+143115+00
		8 71635101	3 700005-02	1 209265-01	1 000005400	1.000005+00	.000006+00	3-096936+00
60	6.10/20E+UU	0.0/1736401	3.100096-02	1.340505-01	1.00000000000	1.00000000000		
<u> </u>	6.725605400	4.396826401	1.36041E-02	3,022586-02	1,00000F+00	1.00000E+00	■00000F+00	1.825156+00
01	0.123002100	4.37002LV01				1 0000000 + 00	0000000000	1 241456400
62	7.33418E+00	4.79473E+01	3.658876-03 -	3.022582-02	1.000006+00	T*000006+00	• • • • • • • • • • • • • • • • • • • •	1.241025400
73	3 007535.00	6 220 41 E + A1	5 £ 1 7 £ 7 Ē 6 £	2 022595-02	1.000006400	1.00000E+00	-00000E+00	1.04350F+00
03	1.4991335+00	2+220416401	2.017425-04	3.022305-02	1.0000000000			1 000345.00
64	8-72058F+00	5.701115+01	3,35954F~05	3.02258F-02	1.00000E+00	1.00000E+00	.00000E+00	
				3 433646 - 03	1 000005400	1 000005400	000005+00	1.002456+00
. 65	9.508702+00	0.210376401	3.930036-02	3.022305-02	1.000000400	LOUVVULVUV	••••••	
6 L	1 036785+01	6.77706E+A1	3.257516-08	3-022586-02	1_00000F+00	1.0000E+00	*00000E+00	1.000216+00
00	1.030102.01				1 22222	1 000000.000		1 000 225400
67	1.13041E+01	7.390116+01	3.20039t~U0	3.022386-02	T*00000E+00	1.000005.00	•••••••	1.000232000
4.9	1 222495401	0 067266401	2.020205-08	3.022586-02	1.00000E+00	1,00000F+00	-00000E+00	1.00003E+00
00	1.275 -05-01	0.031305-01	30720372-00					1 000025+00
69	1,34373F+01	8.78466E+01	4.14188E-07	3.022586-02	I+00000E+00	1.00000000000		T.º 00003E+00
36	1 4/4007.01	6 677476401	5 774545_09	2 022585-02	1 000005+00	1.000005400	00000E+00	1:.00000E+00
10	1.404335401	947//46ETVL	2012335-00	200222005-02	1.0000000000		••••••	
71	1.507176+01	1.044158+02	5,73687F-08	3_02258F-02	1.00000E+00	1.00000E+00	•00000E+00	T*0000TE+00
11	1	1.0111110			1 000005.00	1 000005.00	000005400	1 000005+00
72	1.741246+01	1.13834E+02	2.923226-00	3.022306-02	TODOODEADO	1.000005+00	+UUUUUE+UU	1.000002.000
5 5	1 000206101	1 241005402	A 267326_00	3.07758E-02	1_00000E+00	3,00000F+00	_00000F+00	1.000000000000
13	T+04050C+AT	1.241000402	70201322-07					1 00000000000
74	2.06945E+01	1.35291E+02	6.87889E-09	3.022586-02	T*00000F+00	T+00000E+00	+UUUUUE+UU	1.00000000000
26	5 564056401	1 474985103	1 970105-00	2 022585	1.000005+00	1.00000E+00	-00000F+00	1 • 00000E+00
(7	5 +53003E+01	T+414005405	T+014TAE-04	30022300-02	1.0000000000			1 0000000.00
76	2.459396+01	-1.60784F+02	8.76048F-10	3.02258E-02	1.00000E+00	1.0000000000000000000000000000000000000		T*00000E+00
14			1 000435-00	3 033500-03	1 000005+00	1.000005+00	-00000E+00	1_00000F+00
11	2.681076+01	1/72/02+02	T*000475-04	3.022306-02	1.00000E+00	1.00000000000	• 00000L + 00	
79	2 42260E+01	1.910725+02	3-61663F-10	3-02258F-02	1_00000F+00	1.00000E+00	_00000E+00	1.00000000000
12	2				1 00000000000	1 0000000.000	000005400	1.000006+00
79	3.186065+01	2.052902+02	/.0303/6-11	3.022305-02	1.0000000000	1.000005+00		1.0000000.000
àň	2 672125401	2 270575402	1.721606-10	3.02258F-02	1,00000E+00	1,00000E+00	+00000E+00	1.00000E+00
<u>ov</u>	3+413135401	24210312702	1.1.1.1.1.1.1.1.1					1 0000000400
81	3.78604E+01	2.47514E+02	1.165842-10	う。リムとうびヒーリン	1.000000000000	T+000005+00	• • • • • • • • • • • • • • • • • • • •	I . UUUUUE + UU
õž	L 12711E+01	2 409116402	- A 214555-11	3.022586-02	1.00000E+00	1,00000F+00	_00000F+00	1_00000E+00
02	4.15.115401	2.030116405		1.022105-02	1.000092.000			1 00000000000
83 -	4,49888F+01	2,94116E+02	-1.26455E=12	3.02258t+02	-1.00000E+00	1.00000000000	• UUUUUE + UU	T.000005400
	4 004115.01	3 206005403	1 1 26026-11	2 02268602	1 000005+00	1.000006+00	-00000E+00	1_00000E+00
04 :	4+A04TTE+0T	3.200002702	· 1+153436-11	3.022302-02	1.000002.00			1 000002.00
85	5.34580F+01	3.49484F+02	9.64632E-12	- 3_02258E-02	1.00000E+00	1.00000000000	.00000E+00	T+00000C+00
	6 033365.01	3 000 607 03	6 030505-13	3 0225PE_02	1 000005+00	1.000005+00	- 00000E+00	1_00000F+00
80	2.02/226401	3.009.395702	2.020202-12	3.022302-02	1.00000000000	1.00000000000		
87	6.35203E+01	4.152666+02	1-95789F-12	- 3_02258E-02	1.00000E+00	1.00000E+00	•00000E+00	T-000006+00
×.			ñ 116767-13	5 633696-63	1 000005+00	1 000005400	000006+00	1,00000F+00
. 88	0.924046401	9.720026702	7440272E=13	3.022305-02	1.00000000000	TODOODETOO		
80	7.547536+01	A. 03473F402	1.119256-12	3-022586-02	1_00000F+00	1.00000E+00	00000E+00	T-00000E+00
97		7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7			1 000005.00	1 0000000.000		1 00000E+00
90 .	8.ZZ/14t+01	5.3/852E+V2	1.700022-16	3.022705-02	1.000005400	1.000000-00		
<u> Ö</u> i ···	0.067016401	5 862805402	1.803505-12	3_02258F-02	1.00000F+00	1.00000E+00	-00000E+00	1.00000E+00
21	0.0707716701				1 000007.00	1 00000000000	0000E+00	1 00000E+00
92 .	9.775352+01	6.J9067E+02	1.903216-12	3.022308-02	T+00000E+00	T*000005+00	+UUUUUE+UU	1.0000001.000
· 63	1 046666403	L 04 404 E40 2	1 703875-12	3.022586-02	1.00000F+00	1.00000F+00	+00000E+00	-1.00000E+00
73	1.0000000	0.700072702	10103016-16	3.022300-02				1 000005400
94	1,16148E+02	7.59320E+02	1.3695ZE-1Z	3.022586-02	1.00000E+00	1.0000000000	••••••••	TOUCOULADO
óć.	1 362062403	A 774906403	1 766655-17	2 022585-02	1.000006+00	1.000006+00	_00000F+00	1.00000E+00
	1+200046402	0+210005+02	T+033435-15	34455305-65			100000000000	1 ÅÅÅÅÅÅÅÅÅÅÅÅÅÅÅÅÅÅÅÅÅÅÅÅÅÅÅÅÅÅÅÅÅÅÅÅ
96	1,38002F+02	9,07193E+07	7.Z1820E-13	3.02258E-02	T*00000E+00	T*00000F+00	+UUUUUE+UU	T+000005+00
63	1 60/ 160 101	0 032135.03	£ 371816.15	3 077582-07	1.000005+00	1.000006+00	-00000F+00	1_00000E+00
47	ショウリサイフヒキリイ	70037126702	フゅうしてひすたみぞう	34722305-722	1.0000000000000000000000000000000000000	*********		1 000007.00
QA	1.639675+02	1.07194F+03	2_84895F-13	3.02258E-02	1.00000E+00	I.00000F+00	.000002+00	1.000005400
~~~		1 1282200	3 348455.13	5 A3366E_A3	1 000005+00	1.00005400	-000006+00	1 -00000F+00
	1.10/2/2+02	T*T00445403	2.4 (70075713.	3.0442305-04	T TO TO TO TE TO T	1.000005.00		1 1000007 .00
100	1.948165+02	1.273625+03	-00000F+00	3.02258E-02	1.00000E+00	1.00000E+00	+00000E+00	T*00000F+00
TAA	**********	***********		sevee soe, ve				

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	MFK QUAN ACLINF = A1MFKN = DELTU2 = DTINC1 = PDI110 = PSI31N = RTAU = 98 .97960E	NTITIES IN VISH 3.02966 .12000 27.36673 5.51352 37 .00433 00223 133.57505 +00 5 .471956	K AT STATION M= ALINFN = 3.0190 ALMFKO = .1200 BLTHK = 27.3667 DELTU1 = 27.0798 VEDGE = .0129 VEDIE = .0042 VEL20 = .00000 VEL20 = .00000 VEL20 = .0000 VEL20 = .00000 VEL20 = .000000 VEL20000 VEL200000 VEL200000 VEL20000000 VEL200000000000 VEL2000000000000000000000000000000000000	98 8 ALINFD = 0 A2MFK = 3 DELIN = 9 DTINC2 = 7 NDELTU = 6 PSI21N = 0 PSI21N = 0 EMFK = 1 A2MA3N = •60510E+00 -•5894	2.97758 50000 1.18870 5.56567 .0000 .00000 .00018 .30000 89E+00 .84751E+00	•33899E-01 •4	0399E-03 .16068E-0	92*** 4490.037
	EDGE QU/ MREF = REYREF = TE2 = RO2 = ME1 = RHOE1 =	ANTITIES IN VISP .04000 T 2000000.0 P 1562.64331 R 1.00000 C .03390 U 1.00023 R	4FK AT STATION H=         7REFD       530.0000         4E2       .0337         8HDE2       1.0002         9E2       .0347         9E1       .030         8475       .000	99 0 TREF =150 8 UE2 = 3 TU2 = 6 MUE2 = 1 TE1 =150 0 QE1 =	52.50000 .84462 .00200 1.00007 52.64086 .00346			
•	MFK QUAI ACLINF = A1MFKN = DELTU2 = DTINC1 = NINNE = PDI110 = RTAU = 99 .97960E	NTITIES IN VISH 3.06774 .12000 27.71125 5.56567 .00426 00301 133.82633 .00 8.477016	K AT STATION M= ALINFN = 3.0537 ALMFKO = .1200 3LTHK = 27.7112 DELTU1 = 27.3667 VEDGE = .0184 VEDGE = .0042 VEDI1 = .0042 VEDGE = .0000 VEDGE = .00000 VEDGE = .00000 VEDGE = .00000 VEDGE = .00000 VEDGE = .00000 VEDGE = .00000 VEDGE = .000000 VEDGE = .000000 VEDGE = .000000 VEDGE = .000000000 VEDGE = .00000000000000000000000000000000000	99 3 ALINFO = 0 AZMFK = 5 DELIN = 3 DTINC2 = 6 NDELTU = 1 PSI12N = 0 PSI2IN = 0 EMFK = 2 A2MA3N = 80755E+007930	3.01908 .50000 1.19687 5.64454 73 .00000 .00000 .00019 .30000 03E+00 .84462E+00	•33783E-01 •4	0117E-03 .15770E-0	2*** 4537.856
	XC(M),M=1,MM 58400446E 63408793E 68411658E 73402934410E 83219143E 83219143E 92246307E 96434011E 10426697E 10790627E 11137709E	AX (LEVY-LEES S1 +00 .59027671E +00 .64034338E +00 .69036579E +00 .74024235 +00 .83828762E +00 .88467322E +00 .88467322E +00 .92778107E +00 .96945908E +01 .1009381E +01 .10834875E +01 .11180144E	REAMWISE COORDIN +00 .59654243E +00 .64659860E +00 .74644203E +00 .74644203E +00 .74644203E +00 .84438097E +00 .89012138E +00 .93307654E +00 .97455013E +01 .10141853E +01 .10519394E +01 .10878866E +01 .11222452E	ATE) +00 +60280417E +00 +65285341E +0C 70285846E +0C 75262698E +0C 80168150E +00 85046638E +00 93834903E +00 97961265E +01 10565314E +01 10922605E	•00       .60906308E+00         •00       .65910768E+00         •00       .70910111E+00         •00       .75879636E+00         •00       .80778763E+00         •00       .80778763E+00         •00       .9097546E+00         •00       .94359784E+00         •01       .10237935E+01         •01       .10966094E+01	.61532032E+0 .66536129E+0 .71534060E+0 .76495067E+0 .86243696E+0 .90637769E+0 .90637769E+0 .94882211E+0 .98964778E+0 .10285548E+0 .10656284E+0 .11009339E+0	0 .62157658E+00 0 .67161409E+00 0 .72157612E+00 0 .81999331E+00 0 .86815526E+00 0 .9176067E+00 0 .99461769E+00 1 .10328F+01 1 .11052346E+01	.62783236E+00 .67786593E+00 .72780638E+00 .77722187E+00 .82609328E+00 .87371792E+00 .95919384E+00 .95919384E+00 .99955534E+00 .10379927E+01 .10746117E+01 .11095128E+01
	*** INVER M XI	SE B.L. CALCULAT Le S	TIONS - SUMMARY DT+	CHART NO. 2 ** THETA* CP	+ BL UEP	OW	STAN STRINT	CFX
	23	50500 .5050 51000 .5100	00 .97191 00 .98169	• 37682 -• • 38021 -•	57331 1.25437 57112 1.25349	•08287 •08330	•00077 •00000 •00078 •00000	1.31097 1.36654

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4	.51500	.51500	.99211	.38338	56932	1.25278	.08252	.00077	.00000	1.35989
5	•52000	.52000	•99852	• 38615	56829	1.25236	•08245	•00077	•00000	1.37872
· 6	• 52500	-52500	1.00920	• 38873		1 25107	-08216	-00077	-00000	1.39932
Å	-53500	-53500	1.01405	39348		1.25191	.08197	.00077	.00000	1.40490
ğ	54000	.54000	1.01906	. 39576	- 56709	1.25189	.08170	.00076	.00000	1.40605
10	.54500	.54500	1.02463	.39803	56702	1.25186	.08130	.00076	.00000	1.40079
11	•55000	•55000	1.03095	• 40034	56685	1.25179	.08075	•00075	•00000	1.38952
12	• 5 5 5 0 0	•55500	1.03764	• 40268	56661	1.25170	•08015	•00075	-00000	1.3/000
13	• <b>56</b> 5000	•20000	1.05160	· 40303		1.25143	.07893	-00074	-00000	1.34983
15	.57000	-57000	1.05892	40979	- 56551	1.25126	07828	00073	.00000	1.33496
16	57500	57500	1.06659	41221	- 56499	1.25105	.07759	.00072	.00000	1.31841
17	.58000	.58000	1.07471	• 41 468	56434	1.25079	.07684	• 00072	.00000	1.29965
18	•58500	.58500	1.08342	•41721		1.25047	.07601	• 00071	•00000	1.27810
19	•59000	•59000	1.09286	41981		1.25008	.07510	• 00070	.00000	1.22554
20	+ 39 3 0 0	- 29200	1 11422	+42201		1.24901	.07301	00069		1,19473
22	• 60500	.60500	1.12700	42825	55830	1.24837	.07171	00067	.00000	1.15602
23	61000	.61000	1.14257	43145	55610	1.24749	.07006	.00065	.00000	1.10394
24	.61500	.61500	1.16315	43507	55315	1.24630	.06780	•00063	.00000	1.02858
25	.62000	.62000	1.19342	•43942	54898	1.24463	.06441	•00060	•00000	•91062
26	•62500	.62500	1.24019	•44489		1.24230	+05940	•00055	.00000	• 13724
21	.63000	.03000	1.30190	+47123		1 23647	•07570	.00050	.00000	36190
20	-64000	-64000	1.47900	46564	- 52119	1.23341	-04164	00039	.00000	18428
30	64500	.64500	1.60367	47322	51425	1.23059	.03536	.00033	.00000	.03322
31	.65000	.65000	1.75840	. 48064	50841	1.22822	.02927	.00027	.00000	07820
32	<b>.655</b> 00	•65500	1.95162	.48781	50395	1.22640	•02348	•00022	•00000	14433
33	•66000	.66000	2.17750	•49437	50070	1.22507	•01876	.00018	•00000	- 17200
34	•66500	•66500	2 441920	60476	- 49833	1.22336	.01306	-00012	.00000	-16949
30	-67500	67500	2.89443	-50777	- 49508	1.22277	.01145	.00011	.00000	- 16339
37	68000	68000	3.11439	.51041	- 49389	1.22229	.01029	.00010	.00000	15716
38	.68500	.68500	3.31800	.51245	49286	1.22187	.00944	.00009	•00000	15199
39	.69000	.69000	3.49881	•51402	49196	1.22150	.00884	•00008	•00000	148/5
40	• 69500	•69500	3.64759	• 51 522	49111	1.22115	.00841	-00011	·109/3 80756	- 15347
41	• 70000	70500	3. 61221	• 7 1 0 1 9	- 49029	1.22044	.00574	.00007	99876	-17396
43	71000	.71000	3.81437	51937	48780	1.21979	.00304	.00003	1.00000	- 25870
44	.71500	71500	3.73223	52905	48213	1.21747	.00393	.00004	1.00000	61038
45	.72000	.72000	3.56285	.57763	45390	1.20581	.01186	.00011	1.00000	-1.79600
46	•72500	•72500	3.17802	•76223	36165	1.16692	.00037	•00000	1.00000	-3.32501
4/	•73000	•73000	2.74561	1.00246	26491	1.10263	03428	00032	1.00000	-1.90000
48	• 73500	•73500	2 2 2 2 7 1 6	1 10558	- 20021	1.09555	01946	00018	1.00000	1,96497
50	.74500	.74500	2.11614	1.22674	-,19211	1.09184	00181	00002	1.00000	2.94961
5ĭ	75000	.75000	2.04719	1.25012	18616	1.08911	.01271	.00012	1.00000	3.59295
52	.75500	.75500	2.01200	1.27289	17988	1.08623	.02382	.00022	1.00000	4.02929
53	•76000	.76000	1.99895	1.29712	17275	1.08294	•03208	.00030	1.00000	4.32985
24	• 76500	• 76500	2.00119	1.32322	104/2	1+0/923	+03818	•00030	1.00000	4.57798
22	• 77500	77500	2.02593	1.37171	- 14665	1.07092	04577	-00043	1.00000	4.77071
57	78000	78000	2.06260	1.41236	- 13711	1.06636	04804	00045	1.00000	4.83073
58	78500	78500	2.09311	1.44412	- 12753	1.06186	.04973	.00046	1.00000	4.86925
59	.79000	.79000	2.12733	1.47677	11787	1.05729	•05081	.00047	1.00000	4.88418
60	•79500	.79500	2.16516	1.51062	10800	1.05262	•05131	• 00048	1.00000	4.07943
61	.80000	.80000	2.20668	1.54588	09784	1.04778	• 05 1 30	00040	1.00000	4.81651
63	-81000	-81000	2.30081	1.62119	07657	1.03758	.05000	00047	1.00000	4.76849
64	81500	.81500	2.35248	1.66093	06565	1.03231	04894	.00046	1.00000	4.71120

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65	.82000	.82000	2.40732 1.	.7021805453	1.02690	•04764 •(	1.00000	4.64481
- 66	.82500	.82500	2.46563 1.	.7451604316	1.02135	•04610 •0	1.00000	4.56966
67	.83000	.83000	2.52702 1	.7896903163	1.01569	•04442 •0		4.49011
68	•83500	•83500	2.59183 1.	.8359901991	1.00990	•0•279 •9		4.90432
69	•84000	-84000	2.001/1 1.	•88496 -•00774	1.00380	•04047 •0		4.10376
70	•84500	.84500	2.13803 1.		• 99740	•03007 •1		4 09643
11	• 0 2 0 0 0	•07000		04747 03070	08453	.03342		3.98701
12	+ 85 500	•0000			97840	.03161		3,90370
74	-86500	.86500	3.06128 2	15657 .05423	97251	.03001		3.82565
25	87000	.87000	3,14255 2	21147 06546	96672	02843		3.74667
76	87500	87500	3.22604 2.	26745 07657	96096	.02684 .0	00025 1.00000	3.66418
77	.88000	.88000	3.31187 2.	32459 .08755	. 95522	.02524 .0	00024 1.00000	3.58111
78	.88500	.88500	3.39981 2.	.38278 .09840	•94953	•02369 •(	1.00000	3.49918
79	•89000	•89000	3.48962 2.	•44196 •10909	•94389	+02218 +0		3.41806
80	.89500	•89500	3.58176 2.	•50232 •11965	•93827	•02070 •0		3-33824
81	•90000	•90000	3.6/6/5 2.	•56408 •13013	• 93267	•01924 •9		3-25/42
82	• 90 500	•90500	3.11530 2.	•62760 •14059	•92705	+01//6 +0		3.1/40/
83	• 91000	•91000		•07370 •17114 74774 •14190	• 72134	• 01022 • 0		2.00801
94	•91500	•91500	<b>3.70701 2.</b>	e 10220 e 2205 17244	91337	.01311		2.91058
0 J 86	92500	.92500	4.21680 2	.90525 .18292	- 90 39 3	.01167		2.82749
87	93000	93000	4,33416 2	97802 19312	89827	01038		2.75078
88	93500	93500	4.45078 3.	ó5ŏ35 2ó289		.00927	00009 1.00000	2.68269
89	.94000	.94000	4.56746 3.	12258 21231	.88753	.00827 .0	00008 1.00000	2.61764
90	.94500	.94500	4.68549 3.	.19535 .22149	.88234	.00732 .(	1.00007	2.55299
91	•95000	•95000	4-80532 3.	•26895 •23048	.87723	•00641 •0		2.48852
92	•95500	•95500	4.92699 3.	•34335 •23928	•87220	•00554 •0		2.42696
93	.96000	•96000	5.05047 3.	•41849 •24789	.86726	.00471 .0	1.00000	2.36685
94	•96500	•96500	5.17512 3	•49408 •25628	• 80241	•00395 •0		2.30,208
95	•97000	•97000	2.29918 3	• 20429 • 20433	•07//2	•00320 •0		2.22000
90	• 97 500	•97500		•04094 •2/1// 70633 37906	+ 07 3 3 0 8 4 0 4 0	•00200 •0		2 21 356
97	+9790U	• 96000	5 56722 2	-74540 -28176	84751	.00385		2.27237
40 00	.97960	99000	5.64611 3	.79843	.84462	-00382	0004 1.00000	2.23015
	• 71 700		<b>JIO4011</b> JI	• • • • • • • • • • • • • • • • • • • •		•••••••••		2023025
INTRAC=40	DT(M).M=	L.MMAX						
.656831	77E-03	.68724676E-03	.69415870E-03	•70152512E-03	•70605941E-03	.71007281E-03	•71360929E-03	.71704370E-03
.720583	29E-03	.72452408E-03	.72898921E-03	.73372409E-03	•73859319E-03	•74359262E-03	•74877030E-03	•75419029E-03
•759932	09E-03	•76609372E-03	•77277158E-03	•780C1455E-03	•78787939E-03	•79690987E-03	•80792149E-03	•82247022E-03
•843877	07E-03	•87694899E-03	•92058103E-03	•97557254E-03	-10458102E-02	•11339643E-02	•12433749E-02	•13800014E-02
+153972	335-02	•17106354E-02	•18822551E-02	•20466744E-02	•22022091E-02	•23461782E-U2	• 24 740340E-02	+27/923/05=02
• 203507	176-02	• 26963496E-02	•20971002E-02	• 263 90030E-02	+ 27193131E=U2 14134733E=03	+224/19030-02	142448915-02	143054785-02
+10019U	805-02	14800542E-02	+L4473043E=U2 15042521E=02	152000655-02	15603598E=02	159247405-02	-162691865-02	16634572E-02
170223	325+02	-174346355-02	178687445-02	-18326995E-02	-188211515-02	19360827E-02	19930079E-02	205095006-02
210803	328-02	21646495E-02	222212078-02	22811545F-02	23418435E-02	24040298E-02	24675314E-02	25326889E-02
259985	ŽŎĔ-ŎŽ	-26695383E-02	27426523F-02	-28196696E-02	-28996697E-02	29817308E-02	-30647106E-02	.31471794E-02
• 322967	99E-02	•33131440E-02	.33978774E-02	•34839055E-02	•35712207E-02	•36593596E-02	•37470837E-02	•38295899E-02
•389974	62E-02	•39366261E-02	•39924035E-02					
OUTOUT OU		FROM SHOROUTTHE	C TAINT & DMEALES					
UUIPUI UU	ANTITIES	FROM ZORKOOITNES	S INVI & PHENE					
VT DISTR	IBUTION	ON INVISCID MESH	AT INTRAC= 40					
.20361	118E-01	.40332743E+00	+67977286F+00	0 _82561002E+00	.90943079E+00	.95978430E+00	.99100538E+00	.10068074E+01
10165	274E+01	10259340E+01	.10359824F+0	1 .10463018E+01	.10566801E+01	.10671190E+01	.10773787E+01	•10863529E+01
10927	839E+01	.10979488E+01	.11029631E+C	1 .11080791E+01	.11132467E+01	.11184145E+01	•11235743E+01	.11287461E+01
•11339	538E+01	•11391229E+01	•11438725E+C	1 .11476849E+C1	11508377E+01	•11538151E+01	.11568103E+01	11598328E+01
•11628	612E+01	•11658861E+01	•11689082E+0	1 •11719349E+C1	11749757E+01	11780061E+01	11808880E+01	.11834109E+01

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.12523104E+01 .12515116E+C1 .12489383E+01 .12329343E+C1 .12216271E+C1 .12047805E+C1 .10823940E+01 .10474237E+01 .10035763E+01 .95498031E+00 .90949957E+00 .86706637E+00	.12520514E+01 .12513641E+01 .12513641E+01 .12300407E+01 .12212052E+01 .11655115E+01 .10787247E+01 .99719818E+00 .9429135E+00 .90372351E+00 .86222153E+00	.12519143E+01 .12511867E+01 .12473315E+01 .12276072E+C1 .12208249E+C1 .10372463E+01 .10372463E+01 .99068210E+00 .99806906E+00 .89806906E+00 .85753023E+00	.12518521E+01 .12509716E+01 .1257528E+C1 .12257528E+C1 .12204641E+01 .1025025E+01 .10703814E+01 .10319795E+01 .98426658E+00 .93804425E+00 .89261713E+00 .85319620E+00	.12518283E+01 .12507085E+01 .12444093E+01 .12244160E+01 .12201018E+01 .10946080E+01 .10659361E+01 .10265862E+01 .97813990E+00 .93244638E+00 .88732842E+00 .84950662E+00	.12517990E+01 .12503851E+01 .12420296E+01 .12196886E+01 .10910505E+01 .10614563E+01 .10210418E+01 .97225331E+00 .92682493E+00 .88214430E+00 .84732821E+00	•12517326E+01 •12499884E+01 •12391747E+01 •12227047E+01 •1289804E+01 •10884292E+01 •10569109E+01 •10153898E+00 •9646503E+00 •92112331E+00 •87703842E+00 •84443449E+00	.12516344E+01 .12495090E+01 .12360683E+01 .12221158E+01 .12165565E+01 .10856229E+01 .10522459E+01 .10096107E+01 .96071028E+00 .91532273E+00 .87201177E+00
INTRAC= 40 PMF( .11667000E+01 .12753236E+01 .13438474E+01 .14854446E+01 .26708310E+01 .24577244E+01 .22039405E+01 .24757387E+01 .29200704E+01 .34324784E+01 .40573514E+01 .46902391E+01	M) • M=1 • MMAX • 12186841E+01 • 12822706E+01 • 13544208E+01 • 15409521E+01 • 29649882E+01 • 46607361E+01 • 22165016E+01 • 22269407E+01 • 22269407E+01 • 29803568E+01 • 35031835E+01 • 41378694E+01 • 47224697E+01	<pre>.12301037E+01 .12901086E+01 .13658284E+01 .16142275E+01 .32604884E+01 .22351731E+01 .22534582E+01 .25534582E+01 .30411842E+01 .30411842E+01 .35769405E+01 .42191138E+01 .47731201E+01</pre>	.12424650E+01 12983921E+01 .13781455E+01 .17067762E+01 .35436004E+01 .21907537E+01 .22832051E+01 .22832051E+01 .31033078E+01 .36541826E+01 .43011249E+01	12500909E+01 13068884E+01 13914622E+01 18255005E+01 38113951E+01 21698093E+01 22161405E+01 23161405E+01 31667936E+01 37339105E+01 43839045E+01	.12569419E+01 .13155901E+01 .14066912E+01 .19752382E+01 .37228342E+01 .21646311E+01 .23523017E+01 .23544746E+01 .3314510E+01 .38151580E+01 .44669904E+01	•12630652E+01 •13245766E+01 •14251944E+01 •21619918E+01 •42792444E+01 •30988739E+01 •21706868E+01 •23911025E+01 •32970417E+01 •38967628E+01 •45491820E+01	<pre>.12690819E+01 .1339525E+01 .14495792E+01 .23962501E+01 .44601391E+01 .27001236E+01 .21846187E+01 .24322164E+01 .2858954E+01 .33639333E+01 .39773001E+01 .46258499E+01</pre>
INTRAC= 40 RHOUE( .0000000E+00 .12513173E+01 .12502230E+01 .12440838E+01 .12245827E+01 .12203361E+01 .10953728E+01 .10662383E+01 .10268581E+01 .97843393E+00 .93276878E+00 .88767817E+00 .84987955E+00	M), M=1, MMAX 12537929E+01 12512890E+01 12499072E+01 12499072E+01 12236145E+01 1219637E+01 10916771E+01 10617483E+01 10213150E+01 97255087E+00 92715087E+00 88249714E+00 88249714E+00	<pre>.12529217E+01 .12512241E+01 .12495199E+01 .12389721E+01 .1228775E+01 .12193156E+01 .10889522E+01 .10571953E+01 .10156647E+01 .96676614E+0C .926739425E+00 .84481575E+00</pre>	<pre>.12522046E+01 .12511279E+01 .12490523E+01 .12359451E+01 .12359451E+01 .12169960E+01 .10860726E+01 .1098879E+01 .10098879E+01 .905101495E+0C .91565574E+00 .87237054E+00</pre>	12517943E+01 12510077E+01 12484963E+01 12328962E+01 12218031E+01 12053720E+01 10827921E+01 10038562E+01 95528854E+00 90983609E+00 86742802E+00	.12515377E+01 .12508634E+01 .12478112E+01 .12300836E+01 .12213865E+01 .11665834E+01 .10790862E+01 .10740802E+01 .99748139E+00 .94960315E+00 .90406348E+00 .86258598E+00	.12514017E+01 .12506901E+01 .12469325E+01 .12277159E+01 .12210160E+01 .11244547E+01 .10750247E+01 .1075179E+01 .99096888E+00 .94396757E+00 .89841239E+00 .85789746E+00	.12513403E+01 12504799E+01 12457520E+01 12259018E+01 12206718E+01 1034366E+01 10706976E+01 10325509E+01 98455701E+00 93836312E+00 89296372E+00 85356609E+00

*** SUMMARY OF CONVERGENCE HISTORY ***

INTRAC	DDTMAX	RMSDT	SMDT	DUEMAX	RMSUE	SMUE	DSFMAX	DFMAX	DGMAX
40	•44969E-02	•13448E-03	•72500E+00	•14095E-02	.45920E-04	•72500E+00	.17686E-02	65451E-03	64283E-07
		*** SUMM	ARY OF CONVER	GENCE HISTORY	***				
INTRAC	DDTMAX	RMSDT	SMDT	DUEPAX	RMSUE	SMUE	DSFMAX	DFMAX	DGMAX
1 2 3 4	•35913E+01 -•71076E+00 -•27173E+00 -•56569E-01	•11701E+00 •24873E-01 •95139E-02 •18364E-02	•99000E+00 •99000E+00 •99000E+00 •99000E+00	•70411E+00 •97713E-01 •45837E-01 •20625E-01	•30850E-01 •60667E-02 •25718E-02 •83977E-03	.99000E+00 .70000E+00 .99000E+00 .70000E+00	•15504E+01 •56745E+00 •16098E+00	28723E+00 .12014E+00 .34229E-01	17674E-04 89486E-05 37457E-05

<b>E</b>	371 005 01	126225-03	000005+00	152675-01	717765-02	695005+00	206925-01	- 182005-01	- 106075-05
2		•130325-02	770002400	166115-01	42002E-02	605000000	367305-01	- 128025-01	- 120195-05
9	• 32024E-UI	•110375-05	• 700000000000	• 144115-01	• • • • • • • • • • • • • • • • • • •	•07500E+00	- 307375-01		-137102-09
1	•3/338E-01	•121/4E-02	•70000E+00	•14700E-01	•777398=03	• 0950 UE + 00	• 317005-01	!?!!!!	123005-02
8	• 37931E-01	•13132E-02	•70000E+00	•14408E-01	• 57463E-U3	+69000E+00	•19042E-UI	11227E-UI	-+110325-02
9	•36763E-01	•13124E-02	•/0000E+00	•13543E-01	+55539E-03	•04000E+00	1/521E-01	10329E-01	1120/E-U2
0	•34362E-01	.12904E-02	•70000E+00	.12309E-01	•53011E-03	•71500E+00	15959E-01	-+92950E-02	+.10419E-05
.1	•32601E-01	-12370E-02	•71500E+00	• <b>.11606E-01</b> ·	.49871E-03	•72000E+00	14199E-01	82224E-02	93521E-06
.2	.30846E-01	.11607E-02	•71500E+00	.11272E-01	•45899E-03	•72000E+00	<b>.</b> 12698E-01	72150E-02	82555E-06
3	-28753E-01	-10808E-02	•71500E+00	.10797E-01	.42061E-03	•72000E+00	.12454E−01	63217E-02	73701E-06
4.	-27811E-01	10097E-02	.72000E+00	.10195E-01	.38668E-03	•72000E+00	•11888E-01	55837E-02	65829E-06
5	26834F-01	94115E-03	72000F+00	95929F-02	.35684E-03	•72000E+00	.11046E-01	50729E-02	58908E-06
6	25518E-01	88249E-03	. 72000F+00	89118F-02	-32869E-03	72000F+00	-11266E-01	46236E-02	52969E-06
ž	24144E-01	815405-03	. 72000F+00	82517E-02	-30262E-03	72000F+00	-10800E-01	42768E-02	47811E-06
8	228765-01	75540E-03	72000E+00	766356-02	27832E-03	. 72000F+00	-96507E-02	39384E-02	43234F-06
ä	215205-01	706575-03	720005+00	-707716-02	258115-03	- 72000E+00	86351F-02	36242E-02	39763E-06
	200705-01	660515-03	720005+00	651146-02	239385-03	72500E+00	80968E-02		36725E-06
	186705-01	41700E-03	720005+00	611585-02	222846-03	725005+00	715325-02	- 307995-02	339115-06
2	•100/UE-UI	+01709E=03	720005+00	564915-02	202315-02	725005+00	747745-07	- 28243E-02	31257E-06
2	•1/10/201	• 207345-03	• 7200000000	= J0701E-02	100575-07	725005400	776205-02	- 250055-02	- 287326-06
3	•15/295-01	• 2 3 2 0 2 E = 0 3	•720002+00	+ 71073ETUZ	+10077E-03	725005400	+ 1 1 2 7 E = U 2 4 4 1 2 5 E = 0 2	- 229125-02	- 267126-06
4	·144/3E-01	•48719E-03	•72000E+00	• 407215-02	• 172045-03	• 725002+00	+001275-02		
5	•13247E-01	•44867E-03	•72000E+00	• 472325-02	·17024E-03	• 725000000	• 20 30 75 - 02		240010-00
6	•12280E-01	-41280E-03	• 72500E+00	• 42223E-02	·14514E-03	• 72500E+00	• 7 1 3 / 4 E - U Z	198295-02	219005-00
7	•11568E-01	•38134E-03	•72500E+00	• 39358E-02	•13338E-03	• 72500E+00	•40410E-02	1809/E-02	200305-00
8	•10842E-01	•35872E-03	•72500E+00	•36530E-02	•124/0E-03	• 72500E+00	•4224/E-U2	1077UE-02	103335-00
9	•98367E-02	•33623E-03	•72500E+00	•32849E-02	•11549E-03	•72500E+00	•51801E-02	1516/E-02	16/81E-06
0	•91480E-02	.30044E-03	•72500E+00	•30302E-02	•10433E-03	•72500E+00	•42259E-02	13856E-02	15358E-06
1	•85574E-02	.27128E-03	•72500E+00	.28134E-02	.94150E-04	•72500E+00	•37165E-02	12502E-02	13986E-06
12	.81339E-02	-24926E-03	•72500E+00	•26553E-02	.86780E-04	•72500E+00	•26145E-02	13246E-02	12699E-06
3	•75886E-02	-23308E-03	.72500E+00	-24611E-02	.80134E-04	•72500E+00	.30114E-02	10457E-02	11574E-06
4.	.70868E-02	-21603E-03	•72500E+00	•22844E-02	•74176E-04	•72500E+00	-26354E-02	- <b>.</b> 96796E-03	10607E-06
5	65908E-02	20105E-03	•72500E+00	•21126E-02	.68885E-04	.72500E+00	-24816E-02	88408E-03	97452E-07
6	-61362F-02	-18479E-03	-72500E+00	19566F-02	-63367E-04	.72500E+00	.24263E-02	83048E-03	89640E-07
7	57149E-02	17140F-03	72500F+00	18135E-02	-58632E-04	.72500E+00	-23070E-02	77849E-03	82478E-07
B	53196E-02	15876F-03	72500 +00	16805E-02	54246F-04	.72500E+00	20079E-02	75394E-03	75880E-07
ŏ	484015-02	14969E-03	725005+00	152285-02	-50772F-04	72500E+00	-19500F-02	64088E-03	69885E-07
	449695-07	134485-03	725006+00	140955-02	459205-04	72500E+00	17686E-02	- 65451F-03	64283F-07
	• • • • • 0 • L = 0 Z	• I J T T UL = U J				•• • • • • • • • • • • • • • • • • • •	-1.000L 0L		

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.***** JOB COMPLETE *****


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4. Title and Subtitle			Report Date April 1984
ALESEP: A Computer Program for the Analysis of Airfoil Separation Bubbles		of Airfoil 6.	Performing Organization Code
7. Author(s)		8.	Performing Organization Report No.
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9. Performing Organization Name and Address			· · · · · · · · · · · · · · · · · · ·
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Washington, D.C. 20546			
15. Supplementary Notes			
Langley Technical Monitor: Joel L. Everhart			
A program called ALESEP is presented for the analysis of the inviscid-viscous inter- action which occurs due to the presence of a closed laminar-transitional separation bubble on an airfoil. The ALESEP code provides a iterative solution of the boundary layer equations expressed in an inverse formulation coupled to a Cauchy integral representation of the inviscid flow. This interaction analysis is treated as a local perturbation to a known solution obtained from a global airfoil analysis; hence, part of the required input to the ALESEP code are the reference displacement thickness and tangential velocity distributions. Special windward differencing may be used in the reversed flow regions of the separation bubble to accurately account for the flow direction in the discretization of the streamwise convection of momentum. The ALESEP code contains both a forced transition model based on a streamwise intermittency function and a natural transition model based on a solution of the integral form of the turbulent kinetic energy equation. Instructions for the input, output, and program usage are given herein along with a sample case.			
17. Key Words (Suggested by Author(s)) Interaction, Separation Transitional, Airfoil Se	Bubble, Viscous, u paration	Distribution Statement Unclassified - Unlimited	
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