



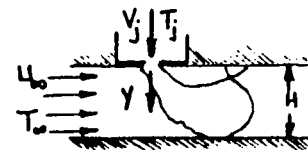
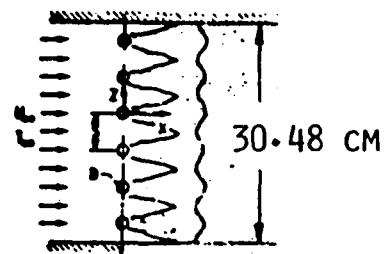
# NASA DILUTION JET MIXING - PHASE I

## OBJECTIVE:

- 0 COLLECT A DATA BASE ON MIXING OF A ROW OF JETS WITH A CONFINED CROSS FLOW
- 0 DEVELOP EMPIRICAL JET MIXING CORRELATIONS

## PARAMETERS INVESTIGATED:

- 0 MOMENTUM RATIO (J), H/D, S/D,  $q_j/q_\infty$
- 0 NON-UNIFORM CROSS-STREAM TEMPERATURE AND VELOCITY PROFILES
- 0 COLD/HOT JET INJECTION
- 0 CROSS-STREAM FLOW AREA CONVERGENCE



DILUTION JET MIXING - PHASES I and II

S. Srinivasan

Garrett Turbine Engine Company  
Phoenix, Arizona

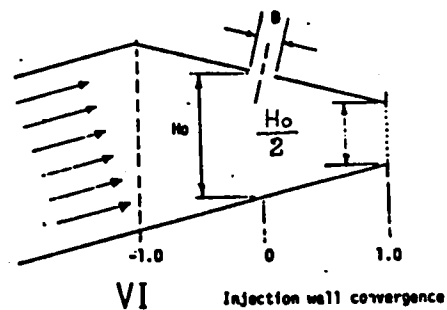
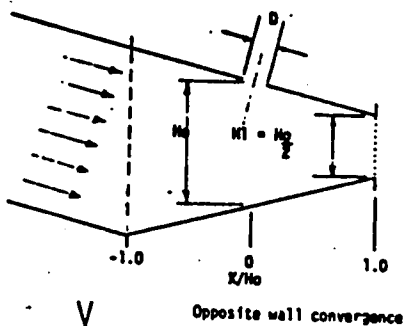
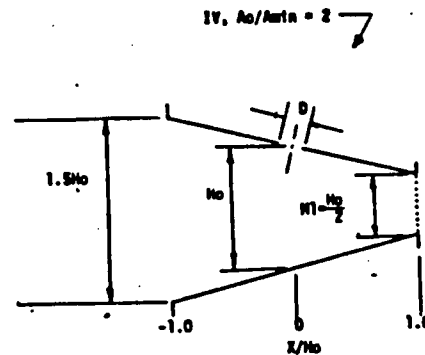
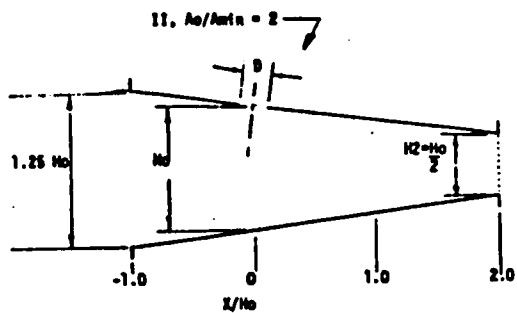
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# PHASE 1 TEST SECTION CONFIGURATIONS

TEST SECTIONS:

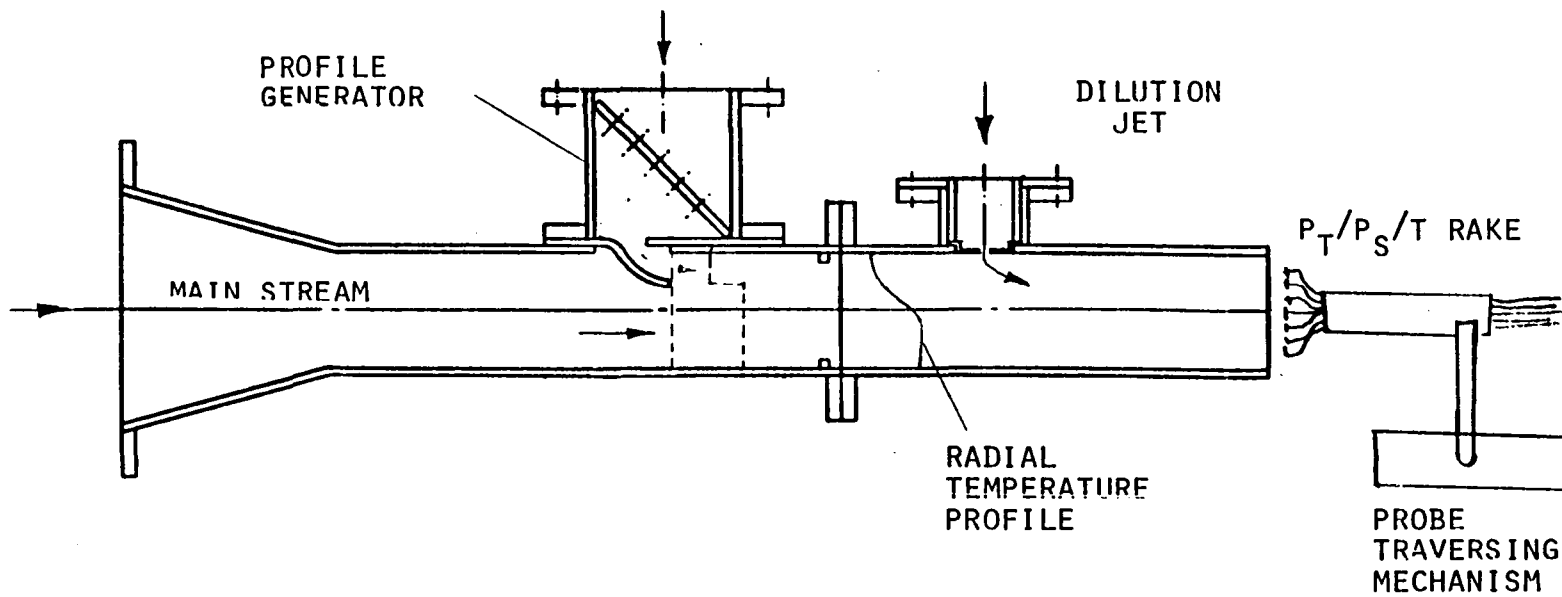
$$H_0 = 10.16 \text{ cm}$$



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# SCHMEMATIC OF THE DILUTION JET MIXING TEST RIG



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## NASA DILUTION JET MIXING - PHASE II

### OBJECTIVE:

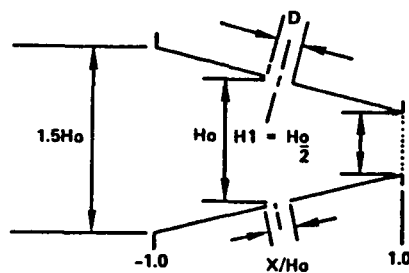
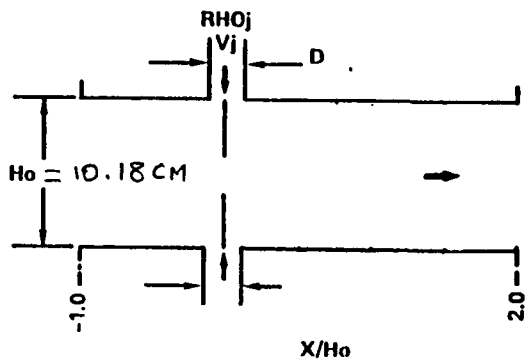
- O EXTEND THE DATA BASE ON MIXING OF SINGLE-SIDED ROW OF JETS WITH A CONFINED CROSS FLOW.
- O COLLECT DATA BASE ON MIXING OF TWO-SIDED ROW OF JETS WITH A CONFINED CROSS FLOW
- O DEVELOP EMPIRICAL JET MIXING CORRELATIONS

### PARAMETERS INVESTIGATED:

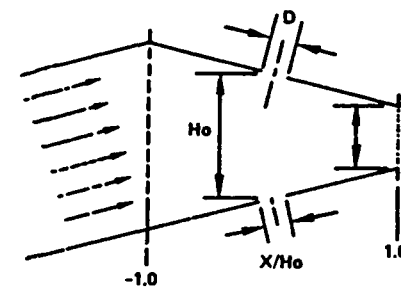
- O CIRCULAR VS SQUARE ORIFICES, TWO-DIMENSIONAL SLOT
- O MOMENTUM RATIO (J),  $H/D$ ,  $s/D$
- O IN-LINE AND STAGGERED ORIFICE CONFIGURATIONS
- O NON-UNIFORM CROSS-STREAM TEMPERATURE AND VELOCITY PROFILES
- O CORSS-STREAM FLOW AREA CONVERGENCE



# PHASE II TEST SECTIONS AND ORIFICE CONFIGURATIONS

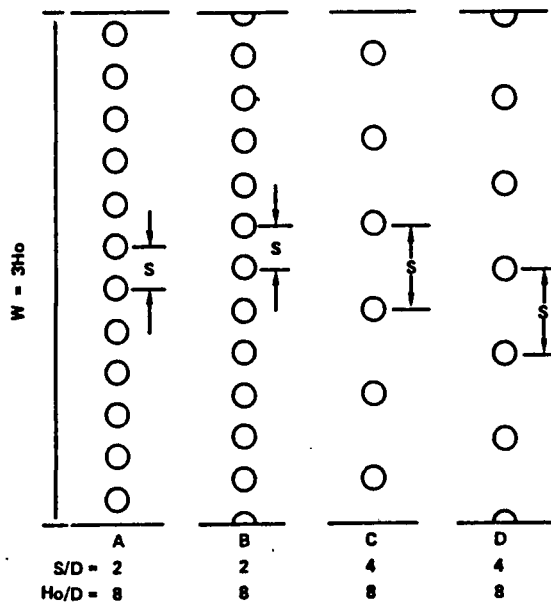


SYMMETRIC CONVERGENCE



ASYMMETRIC CONVERGENCE

Test Sections



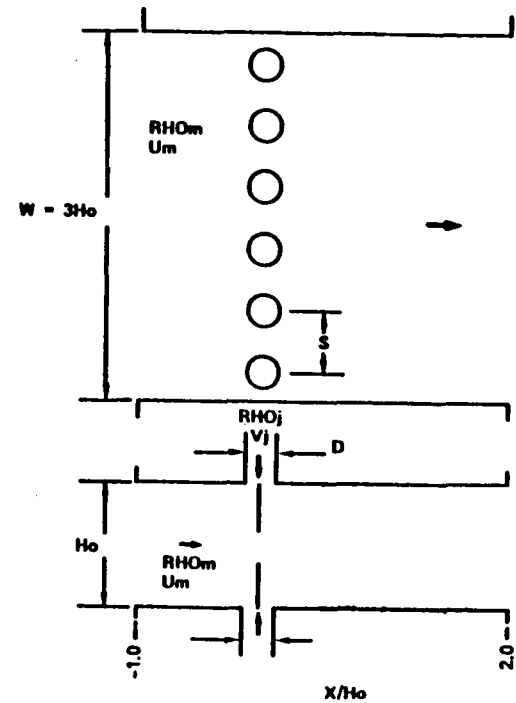
Orifice Configurations.



## PHASE II SERIES 1 TESTING

### SCOPE

- 0 COMPARE EFFECTS OF  $J$ ,  $s/D$ ,  $H/D$
- 0 TWO-SIDED AND ONE-SIDED JET INJECTION
- 0 IN-LINE AND STAGGERED ORIFICE CONFIGURATIONS
  
- 0 DEVELOP CORRELATIONS FOR TWO-SIDED JET INJECTION



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PHASE II SERIES 1 TEST CONDITIONS

UM = 15 M/S

TM = 645°K

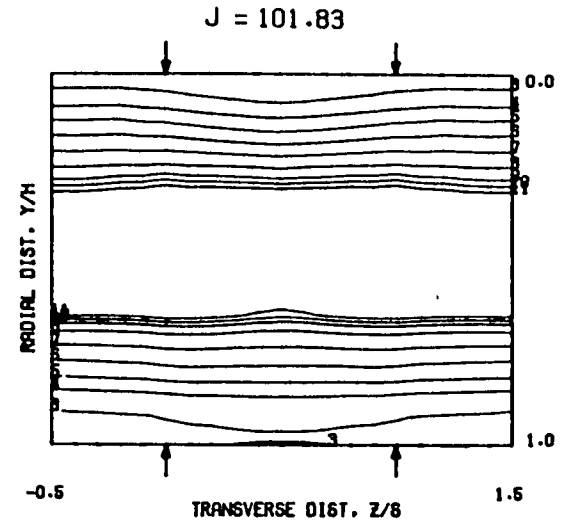
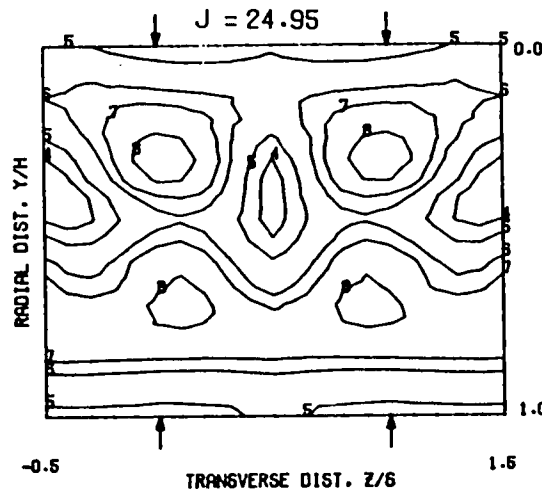
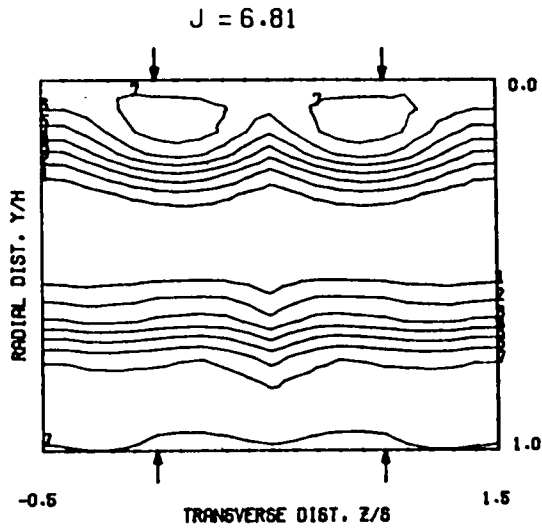
Ho = 10.16 Cm

| H/D | S/D | CONFIGURATION | JTOP          | JBOTTOM       |
|-----|-----|---------------|---------------|---------------|
| 8   | 2   | IN-LINE       | 6.81          | 6.88          |
|     |     | INJECTION     | 25.0<br>101.8 | 24.8<br>101.9 |
|     | 2   | STAGGERED     | 6.53          | 6.54          |
|     |     | INJECTION     | 25.2<br>99.3  | 24.7<br>99.6  |
|     | 4   | IN-LINE       | 7.85          | 7.81          |
|     |     | INJECTION     | 27.9<br>108.3 | 27.3<br>107.0 |
| 8   | 4   | STAGGERED     | 5.98          | 6.14          |
|     |     | INJECTION     | 25.7<br>103.1 | 25.7<br>104.3 |

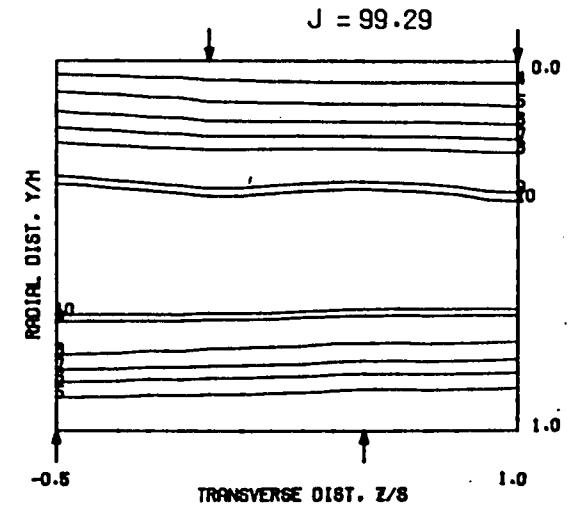
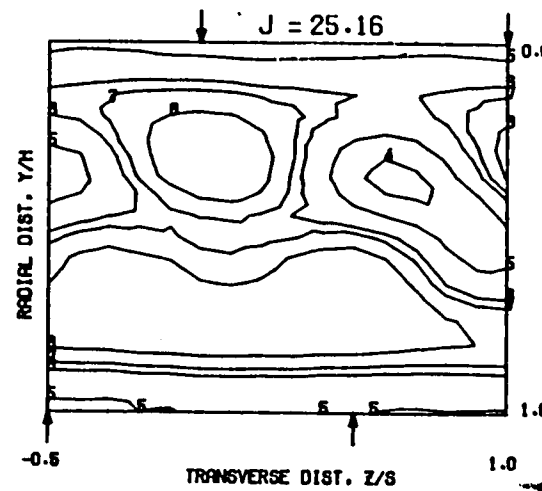
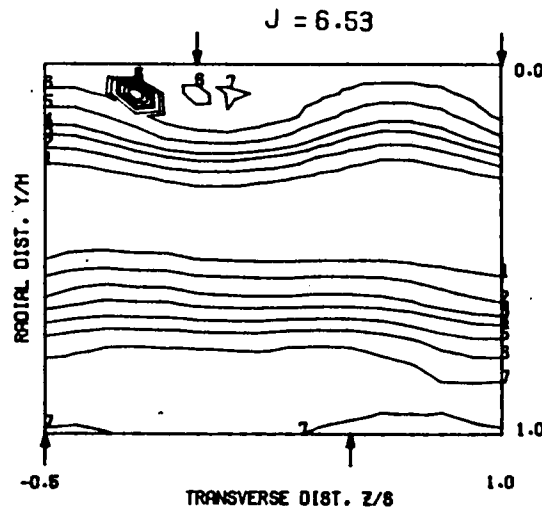


MEASURED THETA DISTRIBUTIONS FOR  $S/D = 2$ ,  $H/D = 8$ ,  $X/H_0 = 0.5$

INLINE ORIFICE CONFIGURATION



STAGGERED ORIFICE CONFIGURATION



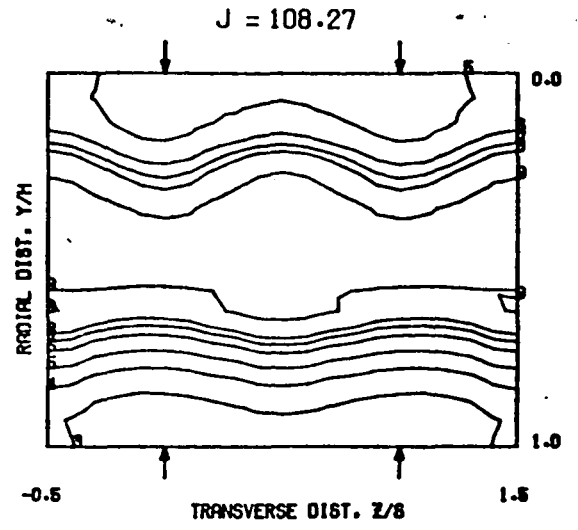
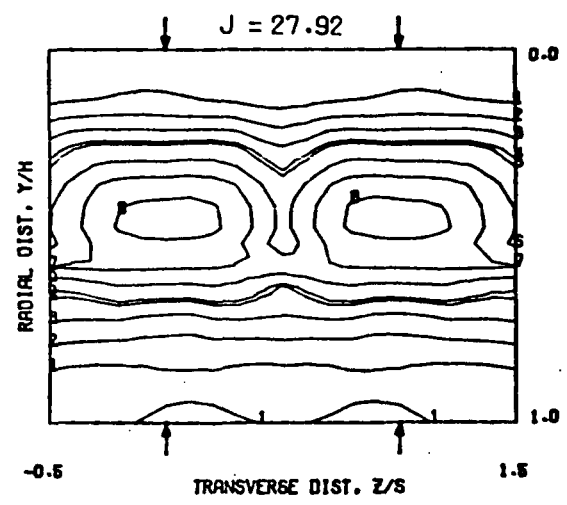
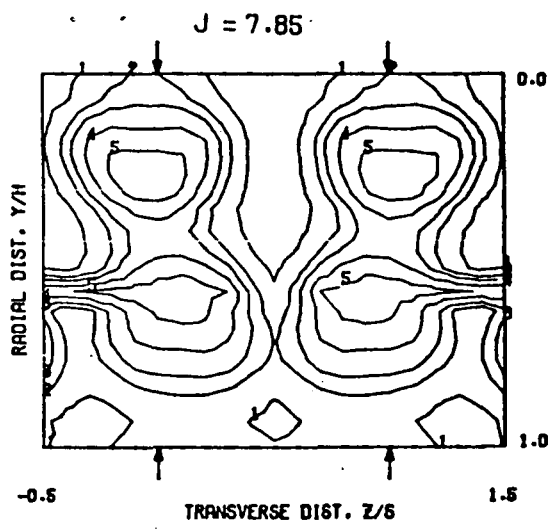
$$\theta = (T_M - T)/(T_M - T_J)$$



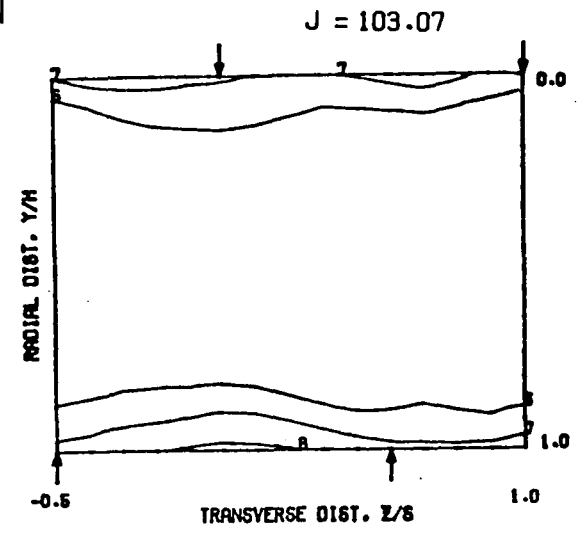
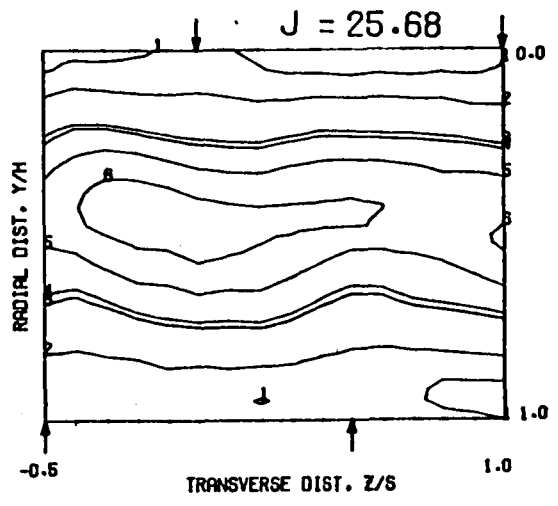
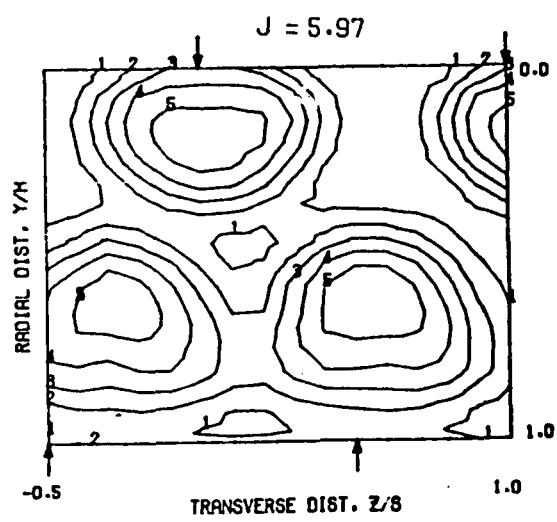


MEASURED THETA DISTRIBUTIONS FOR  $S/D = 4$ ,  $H/D = 8$ ,  $X/H_0 = 0.5$

IN-LINE ORIFICE CONFIGURATION



STAGGERED ORIFICE CONFIGURATION

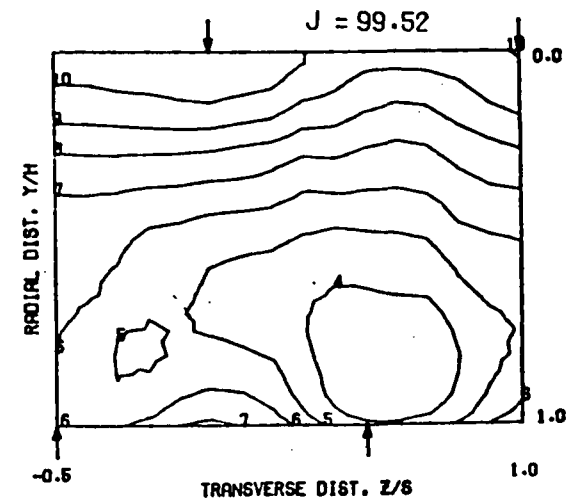
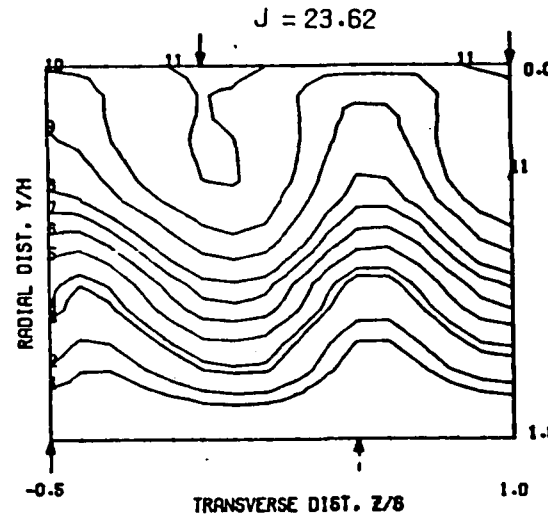
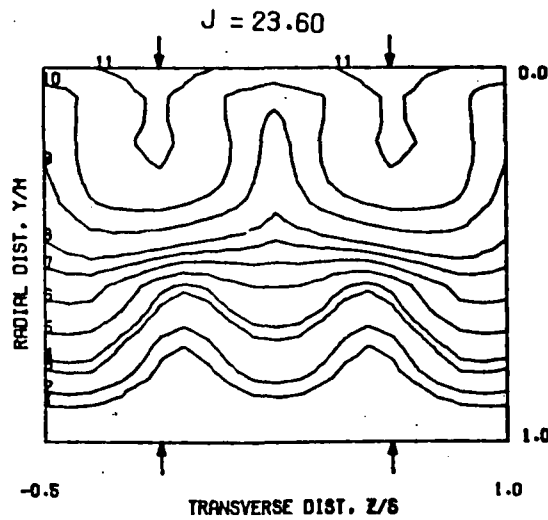
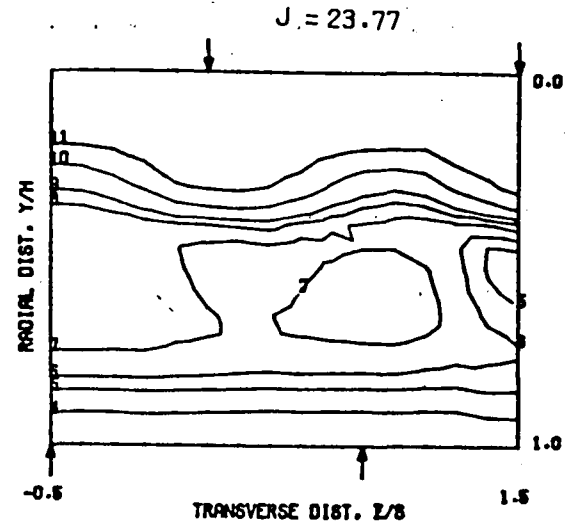
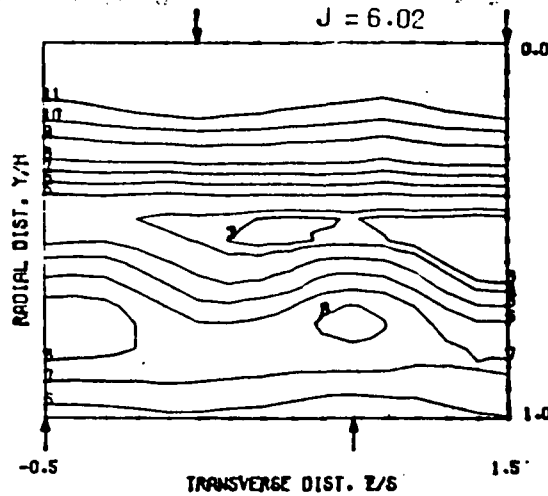
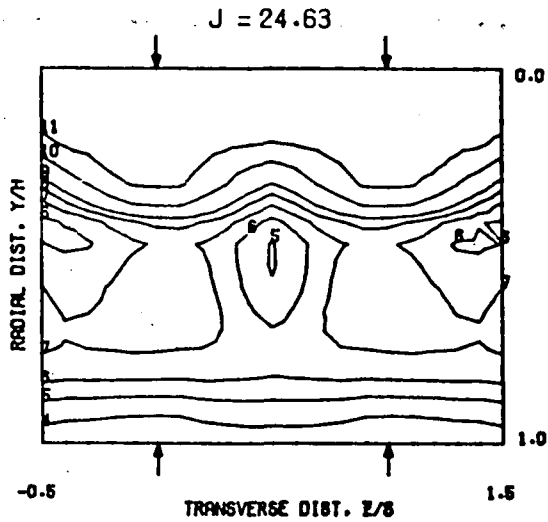


$$\theta = (T_M - T)/(T_M - T_J)$$



# MEASURED THETA DISTRIBUTION FOR PROFILED MAINSTREAM

$S/D = 2, H/D = 8$



$S/D = 4, H/D = 8$   
 $\theta = (T_{MAX} - T)/(T_{MAX} - T_J)$



PHASE II SERIES 2 TESTS

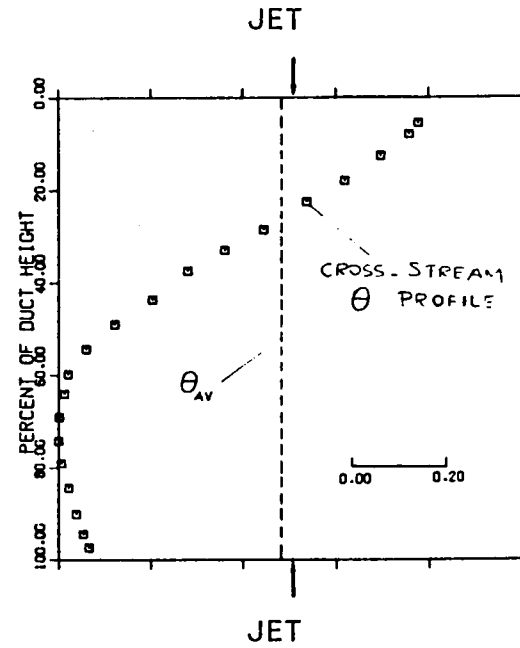
SCOPE:

O TWO-SIDED JET INJECTION WITH PROFILED  
CROSS-STREAM

TEST CONDITIONS:

$U_m = 15 \text{ M/S}$       $H = 10.16 \text{ CM}$ ,      $T_J = 300^{\circ}\text{K}$

| H/D | S/D | CONFIGURATION | J <sub>TOP</sub> | J <sub>BOTTOM</sub> |
|-----|-----|---------------|------------------|---------------------|
| 8   | 2   | IN-LINE       | 24.6             | 24.7                |
|     |     | STAGGERED     | 6.02             | 6.21                |
|     |     | STAGGERED     | 23.8             | 23.4                |
| 8   | 4   | IN-LINE       | 23.6             | 24.2                |
|     |     | STAGGERED     | 23.6             | 24.1                |
|     |     | STAGGERED     | 99.5             | 99.3                |



$$\theta = (T_{MAX} - T) / (T_{MAX} - T_J)$$



## FUTURE TEST PLAN ON PHASE II

- o ONE-SIDED JET INJECTION
  - o TWO - DIMENSIONAL SLOT
  - o SQUARE HOLES
  
- o TWO-SIDED JET INJECTION
  - o NON-UNIFORM CROSS-STREAM TEMPERATURE PROFILES
  - o UNEQUAL JET INJECTION RATES
  - o CONVERGENT TEST SECTIONS (SYMMETRIC AND ASYMMETRIC)

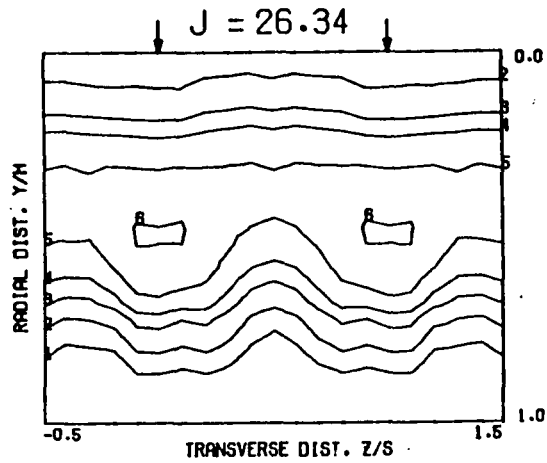
SCHEDULED COMPLETION DATE ON PHASE II TESTS: DECEMBER 1982

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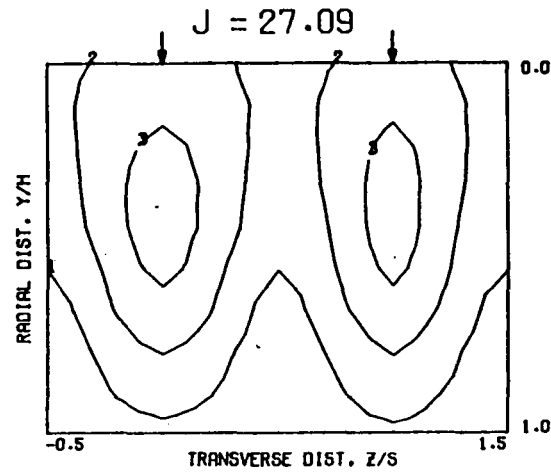


MEASURED THETA DISTRIBUTIONS WITH FLOW AREA  
CONVERGENCE FOR  $S/D = 4$ ,  $H/D = 8$  AT  $X/8 = 1$

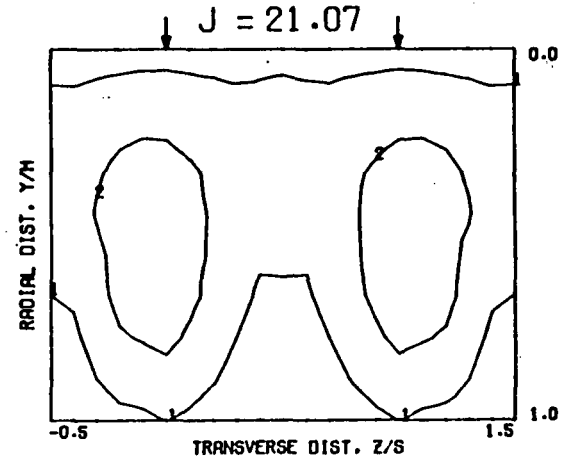
$\phi = 90^\circ$ ,  $A_1/A_2 = 1$



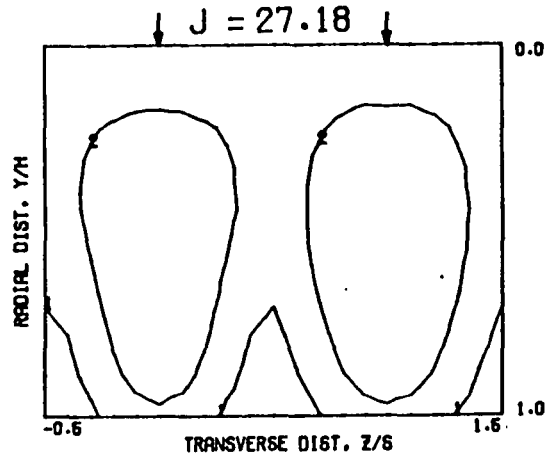
$\phi = 97^\circ$ ,  $A_1/A_2 = 1.33$



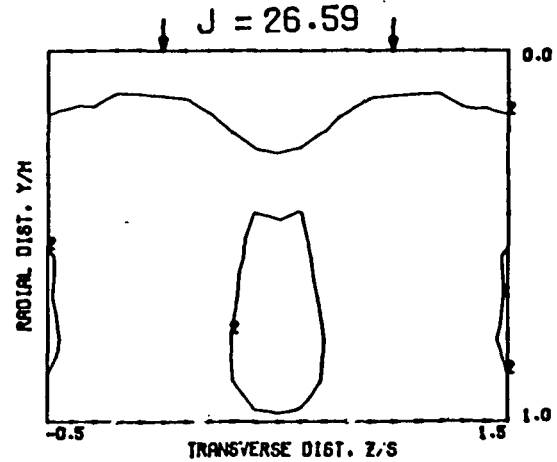
$\phi = 104^\circ$ ,  $A_1/A_2 = 2$



$\phi = 90^\circ$ ,  $A_1/A_2 = 2$



$\phi = 117^\circ$ ,  $A_1/A_2 = 2$





COMPARISON BETWEEN ONE-SIDED AND TWO-SIDED JET INJECTION

S/D = 2, H/D = 8

| PARAMETER                                       | $M_{JET}/M_{MAIN}$ | TWO-SIDED INJECTION |           | ONE-SIDED INJECTION |         |
|---|--------------------|---------------------|-----------|---------------------|---------|
|   |                    | IN-LINE             | STAGGERED | H/D = 8             | H/D = 4 |
| MOMENTUM RATIO, J                               | 0.23               | 6.81                | 6.53      | 25.3                | 5.74    |
| $\theta_{EB} = (T_M - T_{EB}) / (T_M - T_J)$    |                    | 0.198               | 0.189     | 0.169               | 0.176   |
| MAX JET PENETRATION, $Y_c/H$                    |                    | 0.2                 | 0.19      | 0.40                | 0.36    |
| JET HALF WIDTH, $W_{1/2}^+/H$ ,<br>AT $X/H = 1$ |                    | 0.33                | 0.25      | 0.28                | 0.20    |
| JET HALF WIDTH, $W_{1/2}^-/H$ ,<br>AT $X/H = 1$ |                    | 0.0                 | 0.0       | 0.12                | 0.13    |
| $\theta/\theta_{EB}$ AT $X/H = 1$               |                    | 1.82                | 1.94      | 1.89                | 2.06    |
| MOMENTUM RATIO, J                               | 0.47               | 25.0                | 25.2      | 107.8               | 22.0    |
| $\theta_{EB} = (T_M - T_{EB}) / (T_M - T_J)$    |                    | 0.318               | 0.319     | 0.302               | 0.271   |
| MAX JET PENETRATION, $Y_c/H$                    |                    | 0.35                | 0.35      | 0.66                | 0.60    |
| JET HALF WIDTH $W_{1/2}^+/H$<br>AT $X/H = 1$    |                    | 0.                  | 0.        | 0.19                | 0.24    |
| JET HALF WIDTH, $W_{1/2}^-/H$<br>AT $X/H = 1$   |                    | 0.2                 | 0.28      | 0.26                | 0.27    |
| $\theta_c/\theta_{EB}$ AT $X/H = 1$             |                    | 1.08                | 1.10      | 1.17                | 1.44    |



COMPARISON BETWEEN ONE-SIDED AND TWO-SIDED JET INJECTION

S/D = 4, H/D = 8

| PARAMETER                                       | $M_{JET}/M_{MAIN}$ | TWO-SIDED INJECTION |           | ONE-SIDED INJECTION |         |
|---|--------------------|---------------------|-----------|---------------------|---------|
|   |                    | IN-LINE             | STAGGERED | H/D = 8             | H/D = 4 |
| MOMENTUM RATIO, J                               | 0.125              | 7.85                | 5.97      | 26.3                | 6.14    |
| $\theta_{EB} = (T_M - T_{EB})/(T_M - T_J)$      |                    | 0.112               | 0.102     | 0.105               | 0.107   |
| MAX JET PENETRATION, $Y_c/H$                    |                    | 0.37                | 0.24      | 0.54                | 0.54    |
| JET HALF WIDTH, $W_{1/2}^+/H$ ,<br>AT $X/H = 1$ |                    | 0.05                | 0.13      | 0.27                | 0.20    |
| JET HALF WIDTH, $W_{1/2}^-/H$ ,<br>AT $X/H = 1$ |                    | 0.29                | 0.11      | 0.23                | 0.24    |
| $\theta/\theta_{EB}$ AT $X/H = 1$               |                    | 2.64                | 1.77      | 1.63                | 2.54    |
| MOMENTUM RATIO, J                               | 0.23               | 27.9                | 25.7      | 109.0               | 26.7    |
| $\theta_{EB} = (T_M - T_{EB})/(T_M - T_J)$      |                    | 0.190               | 0.189     | 0.181               | 0.192   |
| MAX JET PENETRATION, $Y_c/H$                    |                    | 0.50                | 0.50      | 1.0                 | 1.0     |
| JET HALF WIDTH $W_{1/2}^+/H$<br>AT $X/H = 1$    |                    | 0.0                 | 0.0       | 0.0                 | 0.0     |
| JET HALF WIDTH, $W_{1/2}^-/H$ ,<br>AT $X/H = 1$ |                    | 0.24                | 0.27      | 0.33                | 0.45    |
| $\theta_c/\theta_{EB}$ AT $X/H = 1$             |                    | 1.43                | 1.37      | 1.41                | 1.75    |