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# Turbofan Noise Generation Volume 2: Computer Programs

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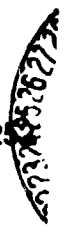
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National Aeronautics and  
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VOLUME 2: COMPUTER PROGRAMS

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## SUMMARY OF VOLUME 2

The computations for three different noise mechanisms - mean rotor wake, inlet turbulence, and rotor wake turbulence - described in Volume 1 of this report are coded as three separate computer program "packages." This arrangement was deemed reasonable because of differences in the required input data (e.g., rotor vs stator geometries), because of interest in the role of each separate noise mechanism, and for economy of execution during parametric studies. The computer codes are described by means of block diagrams, tables of data and variables, and example program executions. Reference to Volume 1 will be made via equation or figure number. FORTRAN listings of the programs appear in the appendix to Volume 2.

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## CHAPTER 1

### MEAN ROTOR WAKE PROGRAM

The computer program described in Fig. 1\* computes the sound power of each propagating mode for the first three harmonics of the blade passage frequency. The data required to run the program and the program results are described in Table 1.\* Important FORTRAN variables used in the program are given in Table 2. Function subroutines utilized in the program are described in Table 3.

The terminal output from a sample execution of the Mean Rotor Wake Program is shown in Table 4 for the rotor/stator data provided by NASA Lewis. The mean flow velocity entering the stator is specified from measured data. The pressure amplitude and sound power of each mode for each harmonic number of the blade passage frequency are listed. Note that for a propagating mode  $(m,n)$  at harmonic  $s$ , another mode  $(-m,n)$  of equal amplitude propagates with frequency  $-s$ . Thus the total sound power for the mode shape  $(|m|, n)$  at frequency  $|s|x$  (blade passage frequency) is the sum of the two components.

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\*Note: Because of the number and complexity of the figures and tables, they have been collected at the end of each section of this volume. The 9 text figures and 12 tables appear before the appendix.

## CHAPTER 2

### TURBULENCE PROGRAMS

The calculations for two types of turbulence noise are considerably more time-consuming than for the tones of the mean-wake interaction because 1) all modes that are not cut off by the duct may be excited, i.e., there is no selection rule, as is the case for the mean-wake interaction, and 2) the noise is broadband rather than tonal, requiring the sound power at many frequencies to be calculated. For these reasons, the turbulence programs are each broken into two subsections. The method used is, first, to calculate and store, for a given number of blade radii, the pressure distributions across the rotor blades or stator vanes at a small number of frequencies over the range of interest. The power spectral density is essentially a spatial integral containing the pressure distribution and acoustic mode shape as factors in the integrand. The pressure distributions are slowly varying functions of frequency and duct radius when compared with the acoustic mode shapes. Thus it is reasonable to interpolate the pressure distribution for a specific frequency and radius from a look-up table of stored pressure values. All other variables that change with radius (or frequency) are calculated explicitly for that given radius (frequency). In this manner, convergence of the radial integration is improved by using more integration steps than there are stored pressure values. The pressure distributions are stored in binary form in a disc file for later use so that, for example, turbulence parameter values may be varied without recomputing the pressures.

#### 2.1 Inlet Turbulence Program

The pressure distributions across the rotor blades are computed and stored as described in Fig. 2. The sound power calculation is diagrammed in Fig. 3. Input and output data for the programs are listed in Table 5. Additional program variables of possible interest to the user are given in Table 6.



Output from sample executions of the two program sections is shown in Tables 7 and 8. The input data relating to rotor geometry and performance are first entered as listed in Table 7. The pressure distributions are computed (as evidenced by the error code returned from LEQTIC; see Table 3), and the data are stored on a disc. The power spectral density for all propagating modes at a frequency of 15 times shaft rate (blade passage frequency in this 15-blade fan) is then computed, and the results are given in Table 8.

## 2.2 Rotor Wake Turbulence Program

The two-stage method of calculation described above is repeated for the Rotor Wake Turbulence problem. The calculation of pressure distributions across the stator vanes proceeds as shown in Fig. 4. The sound power calculation is explained in Fig. 5. Input and output data for the programs are listed in Table 9. Additional program variables are given in Table 10.

The output from sample program executions is shown in Tables 11 and 12. The mean flow into the stator may be specified as for the Mean Wake case. (Note that the print-out shown in Table 12 has been stripped of all messages other than the power spectral density per mode to minimize the amount of paper delivered for high frequencies (many modes). The standard program version would contain diagnostic messages, cut-off ratios, etc., as for Table 8.

## CHAPTER 3

### EXECUTION PARAMETERS AND PROGRAM LIMITATIONS

#### A. General Remarks

1. Specifying blade or vane geometries: Geometrical data are stored in matrix VGEOM. The number of radial positions at which data may be specified (NDAT) is presently limited to 10 by DIMENSION statements. This limitation may be lifted by increasing the size of VGEOM *in all main and subprograms*. The geometrical data are specified by proceeding radially *from hub to tip*, and *must include these two end points*. These data are linearly interpolated for integration stations between the data points.

2. Specifying mean flow distributions: Variable IVOR is a switch controlling whether a free vortex distribution (IVOR=0) or input data (IVOR=1) are used in stator calculations. Input data are stored in matrix VELOCV. The number of radial positions at which data are specified (NVELO) is presently limited to 10. This limitation may be lifted by increasing the size of VELOCV *in all main and subprograms*. The velocity data are specified by proceeding radially *from hub to tip* and *must include these two endpoints*. These data are also linearly interpolated for intermediate points in the radial integration.

3. Specifying Bessel function accuracies: The absolute accuracies for all Bessel function calculations (EB) and root convergence (EC) have been left as input parameters. Values of 0.001 and 0.0001, respectively, have been sufficient for these calculations.

4. Specifying the number of chordwise integration points: The number of chordwise integration points (NCHORD) is an input variable. DIMENSION statements currently limit the value of NCHORD to 20 in all programs. A value of 8 has yielded sufficient accuracy in the cases checked to date. Execution time increases radically for increases in NCHORD, so its value should be minimized. For cases where the acoustic wavelength is considerably less than the blade or stator chord, it may be necessary to increase NCHORD beyond 8. If NCHORD must be increased beyond 20, the following array sizes must be inspected and/or increased: CASCET, PHASE, DELTAP, F, A, WA, and B.

5. Specifying the number of radial integration points: The number of radial integration points (NRAD in Mean Wake, or NRADNU in the turbulence programs) is an input variable. The value must be large enough to achieve convergence of the result, yet small enough to minimize program execution time. A value of 7 has yielded adequate accuracy ( $\pm 1$  dB) for the acoustic power levels in cases checked to date. The value of 20 must not be exceeded without inspecting and/or increasing the sizes of arrays PSISTO, BJ, RR, RRNU, and CASCET.

## B. Turbulence Programs

1. Specifying the number of radial positions for pressure calculations: Both turbulence programs compute and store pressure distributions at a number (NRAD) of radial positions. Acoustic calculations are later performed by using NRADNU ( $>$ NRAD) integration points. This arrangement minimizes the execution time needed for pressure calculations while maintaining good accuracy in the radial integral. NRAD values of 5 have been used for the test cases cited here. NRAD may not be increased beyond 20 without violating DIMENSION statements, as discussed in Sec. A.5.

2. Range of Mode Number  $m$ : The turbulence programs that compute power spectral densities contain a summation of autocorrelation functions that vary with mode number  $m$ . If the annular duct/turbofan arrangement were to allow propagation of modes with mode number  $|m|$  greater than 49 at a given frequency, then program execution would be terminated with an error message. This range may be increased by increasing the size of arrays ISUMTC and SUMTOT and by changing the decision value in the associated IF statement.

3. Selection of frequency values for data storage: The turbulence programs compute and store pressure distributions for a range of frequencies for later interpolation. The most useful frequencies to calculate in the subject spectrum of, for example, from 1 to 3 times the blade passage frequency (BPF), are probably the first, second, and third harmonics of BPF. This range is straightforwardly specified for the wake turbulence program. An important qualification to this procedure must be invoked for inflow turbulence, as explained below.

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The sound power calculations for the inflow turbulence routine require pressure distribution data for frequencies up to an equivalent frequency

$$(\omega^*/\Omega) = (\omega/\Omega)_{\max} + |m_{\max}| + m_{\text{sum}},$$

where  $(\omega/\Omega)_{\max}$  is the highest frequency of interest,  $m_{\max}$  is the largest value of  $m$  which can propagate at frequency  $(\omega/\Omega)$ , and  $m_{\text{sum}} = -|m_{\max}| + (\ell B)$  for some integer  $\ell$  such that  $0 \leq m_{\text{sum}} \leq B-1$ , for  $B$ =number of rotor blades. Thus, before computing the pressure distribution, the user must know what modes can propagate for the turbofan under discussion. The utility program MAPIN/MAPPER (see appendix) will yield the propagating modes for a given geometry, frequency, and turbofan speed. As an example, suppose that the turbulence noise spectrum between BPF and 3BPF is desired for NASA Rotor 55 with the operating conditions: Number of blades = 15,  $M_t = 0.508$ ,  $M = 0.323$ , and  $\sigma_r = 0.484$ . Pressure data will be needed from the lowest frequency of interest ( $\omega/\Omega = \text{BPF} = 15$ ) to the highest equivalent frequency ( $\omega^*/\Omega$ ). Program MAPIN/MAPPER reveals that  $|m_{\max}| = 21$  for  $(\omega/\Omega) = 3\text{BPF} = 45$ . Thus,

$$(\omega^*/\Omega) = (\omega/\Omega)_{\max} + |m_{\max}| + m_{\text{sum}}$$

$$(\omega^*/\Omega) = 45 + 21 + 9 = 75,$$

$$\text{where } m_{\text{sum}} = -21 + (2 \cdot 15) = 9.$$

In the example,  $(\omega^*/\Omega)$  conveniently falls at the fifth multiple of blade passage frequency (5BPF) or  $\omega/\Omega=75$ . The frequency range for pressure distribution calculations is then from  $(\omega/\Omega)=15$  to  $(\omega/\Omega) = 75$  in steps of  $(\omega/\Omega) = 15$ . The results of calculations for that case are shown in Table 7. If programs INSRCH/INTURB were to be executed without pressure data of sufficiently high equivalent frequency, the program execution would be terminated with an error message.

4. DIMENSION of storage matrix CASCET: Pressure distributions are stored on the disc in matrix CASCET. It is desirable to keep this matrix as small as possible to minimize core and disc file requirements. The DIMENSION of CASCET should therefore be adjusted as follows to suit the data: DIMENSION CASCET (NCHORD, NRAD, NBLADE, PRANGE), where NCHORD = number of chordwise integration points, NRAD = number of radial positions for pressure calculations, NBLADE = number of rotor blades, or, for the Rotor Wake Turbulence Program, use NVANE = number of stator vanes. PRANGE = number of frequencies for pressure calculations.

FIGURES

Calculate the sound power of each propagating mode for the first 3 harmonics of the blade passage frequency.

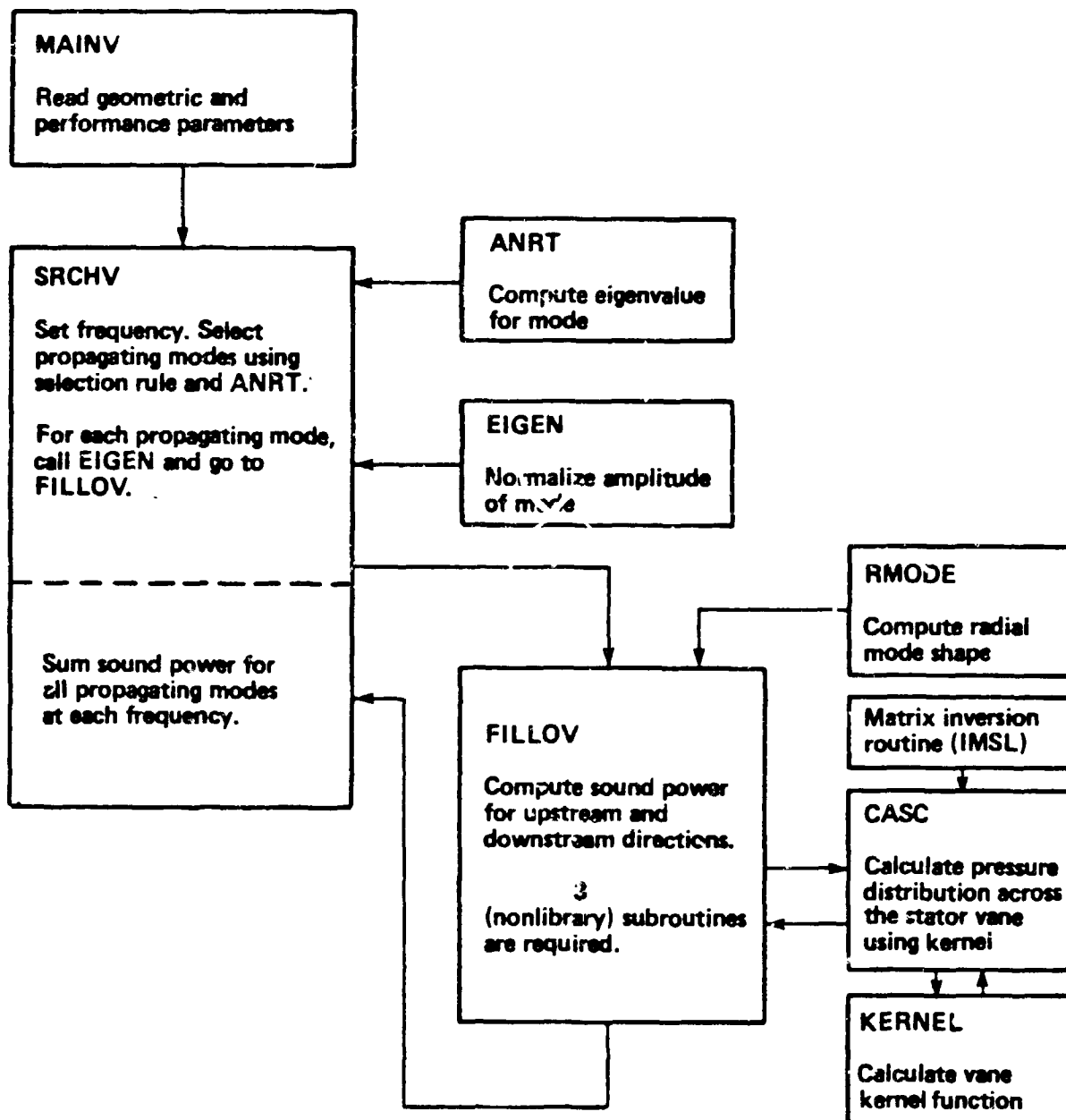


Figure 1. Block Diagram of Mean Rotor Wake Program

A. Calculate pressure distributions across the rotor blades and store data on the disk.

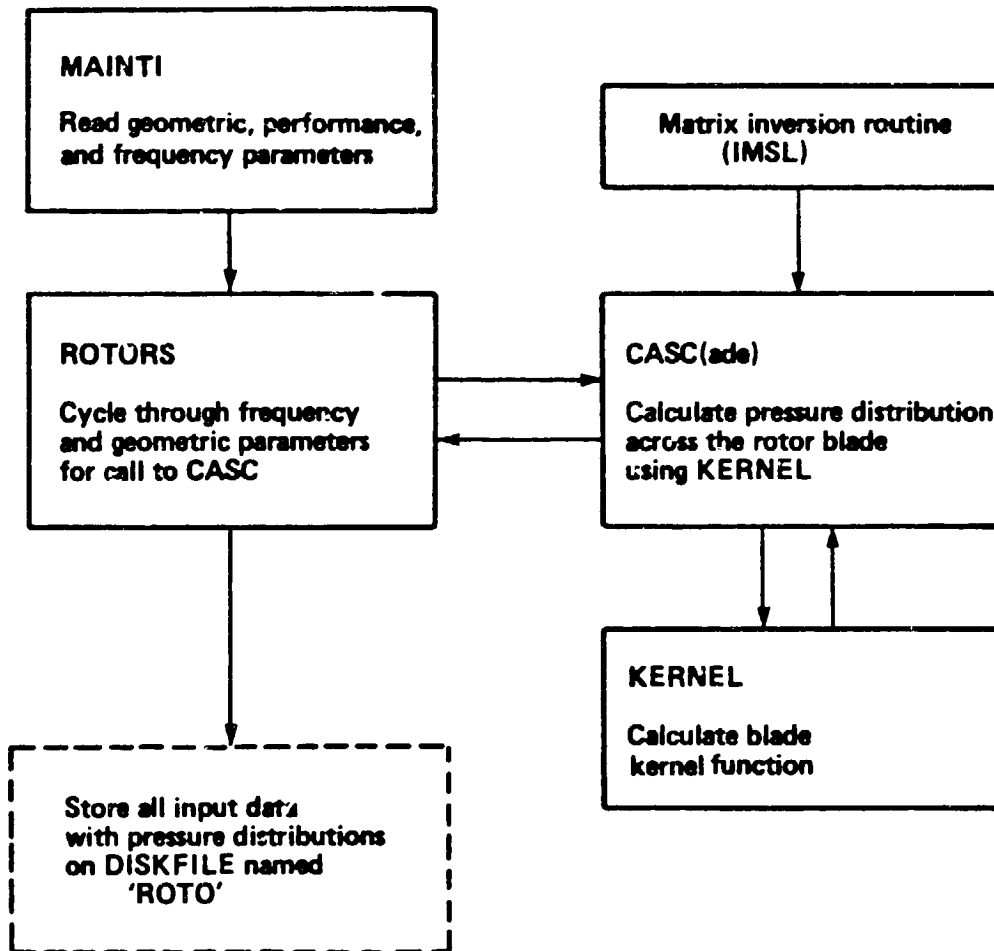


Figure 2. Block Diagram of Inlet Turbulence Program; Part A: Data Storage



B. Calculate the power spectral density of each propagating mode at a given frequency and the total PSD for all modes.

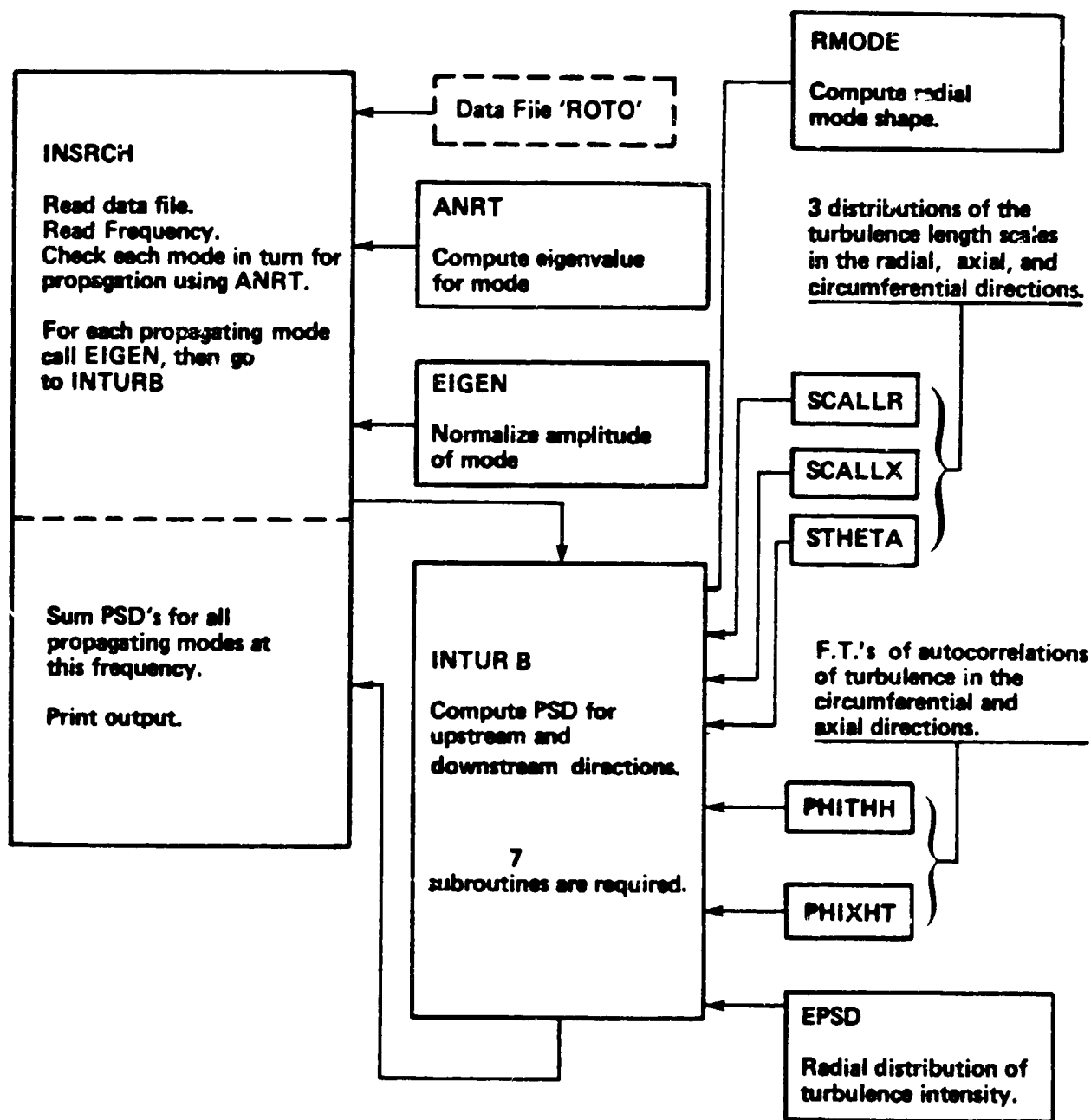


Figure 3. Block Diagram of Inlet Turbulence Program; Part B: Noise Calculation

A. Calculate pressure distributions across the stator vanes and store data on the disk.

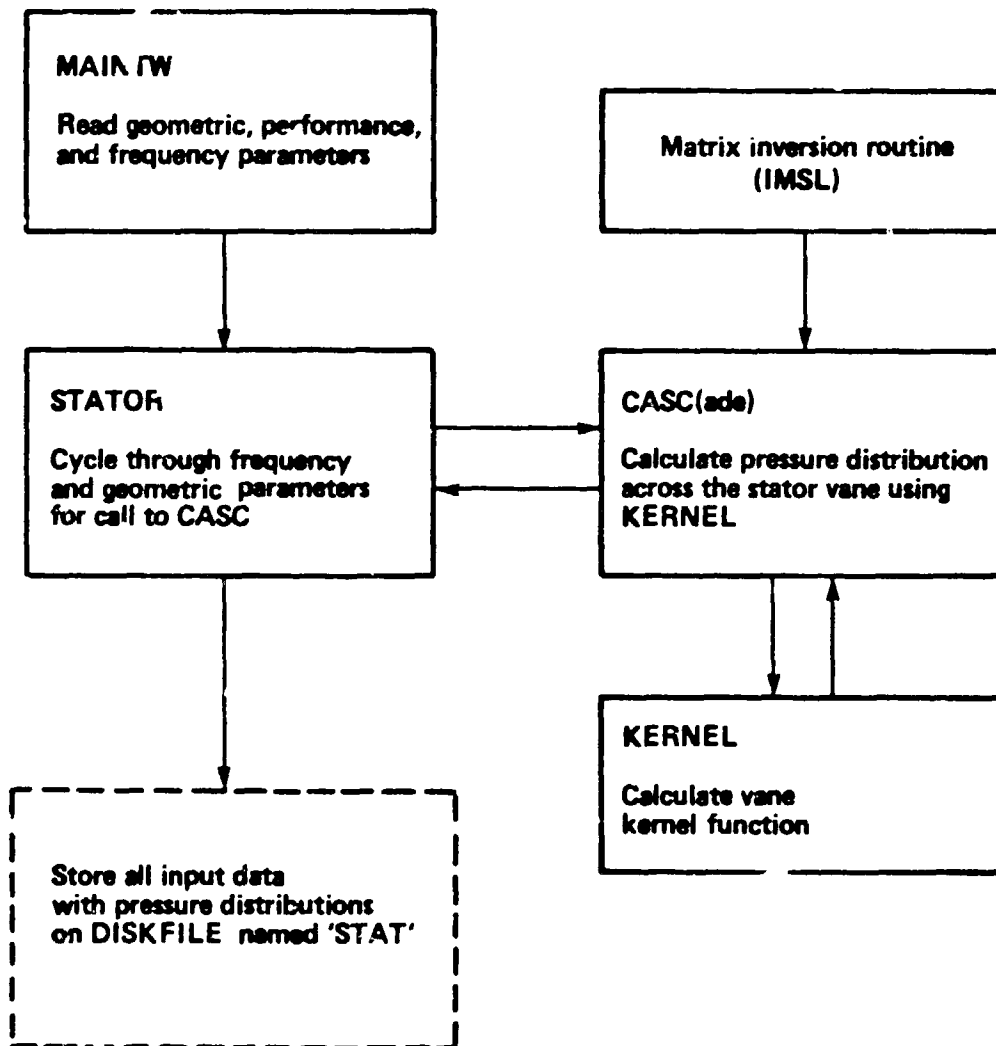


Figure 4. Block Diagram of Rotor Wake Turbulence Program; Part A: Data Storage

B. Calculate the power spectral density of each propagating mode at a given frequency and the total PSD for all modes.

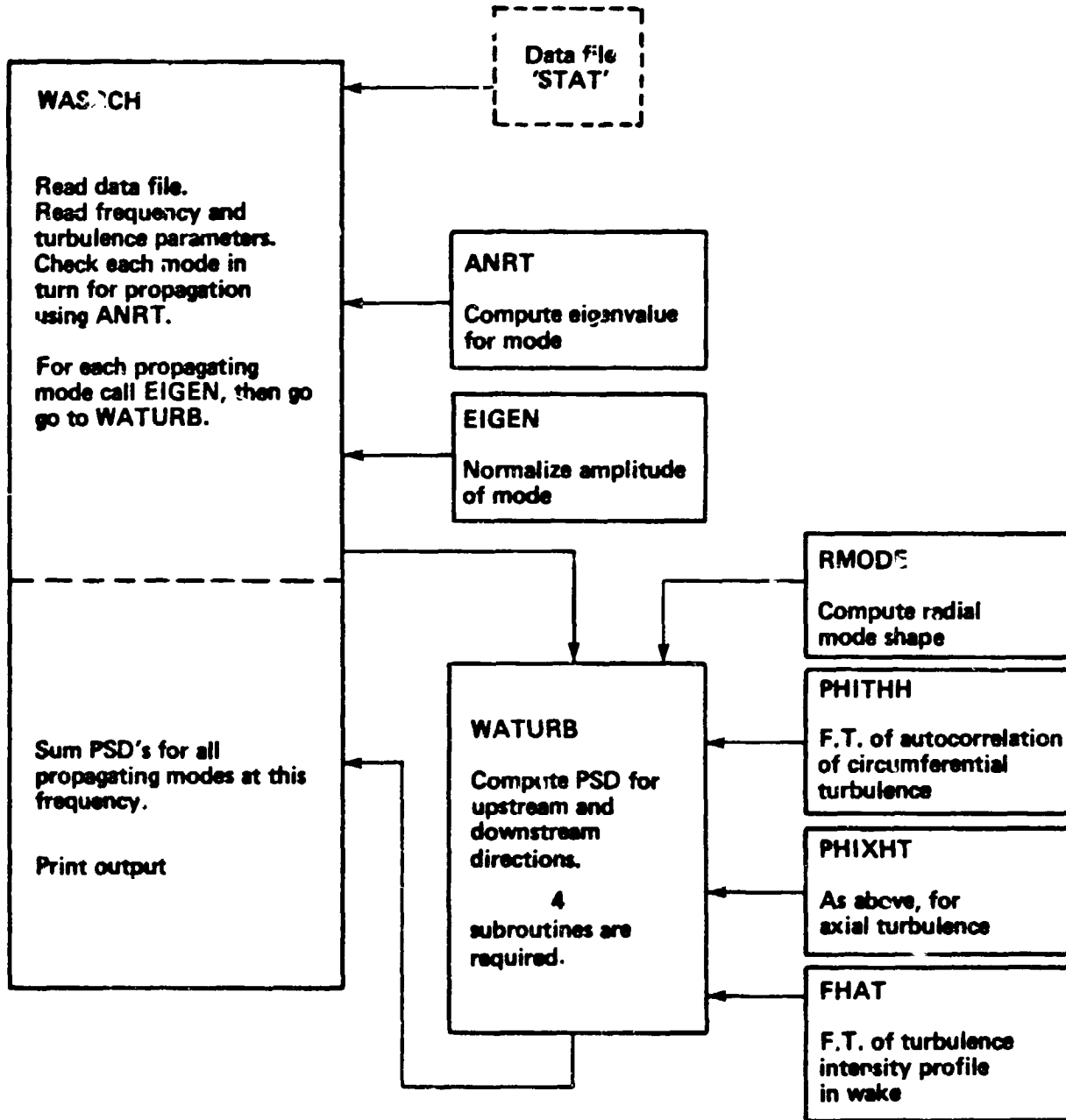


Figure 5. Block Diagram of Rotor Wake Turbulence Program; Part B: Noise Calculation

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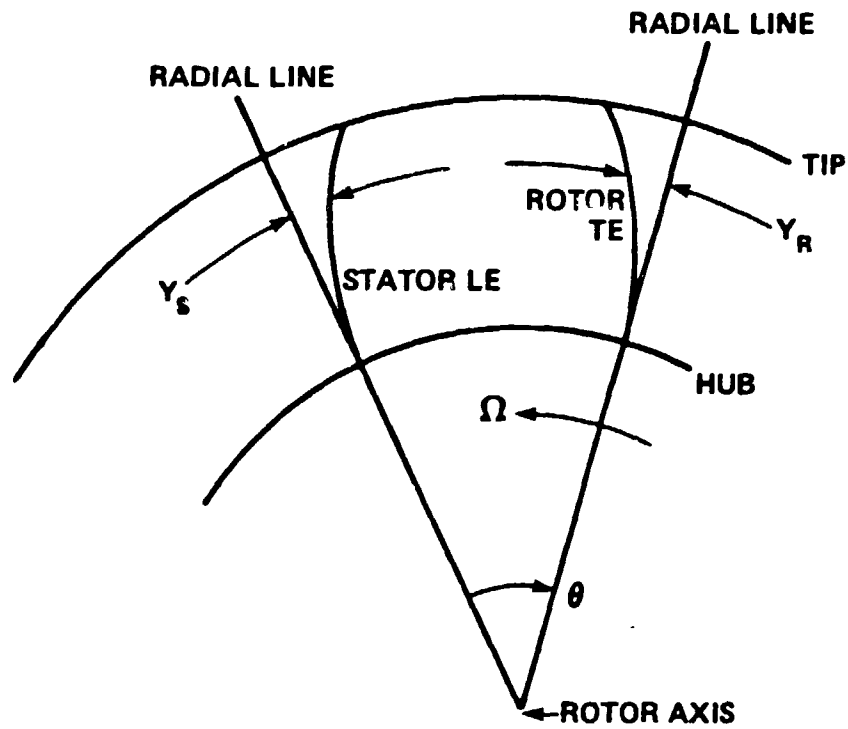


Figure 6. Schematic View of a Rotor Blade TE and Stator Vane LE Looking Down the Turbofan X Axis, in Stator-Fixed Coordinates

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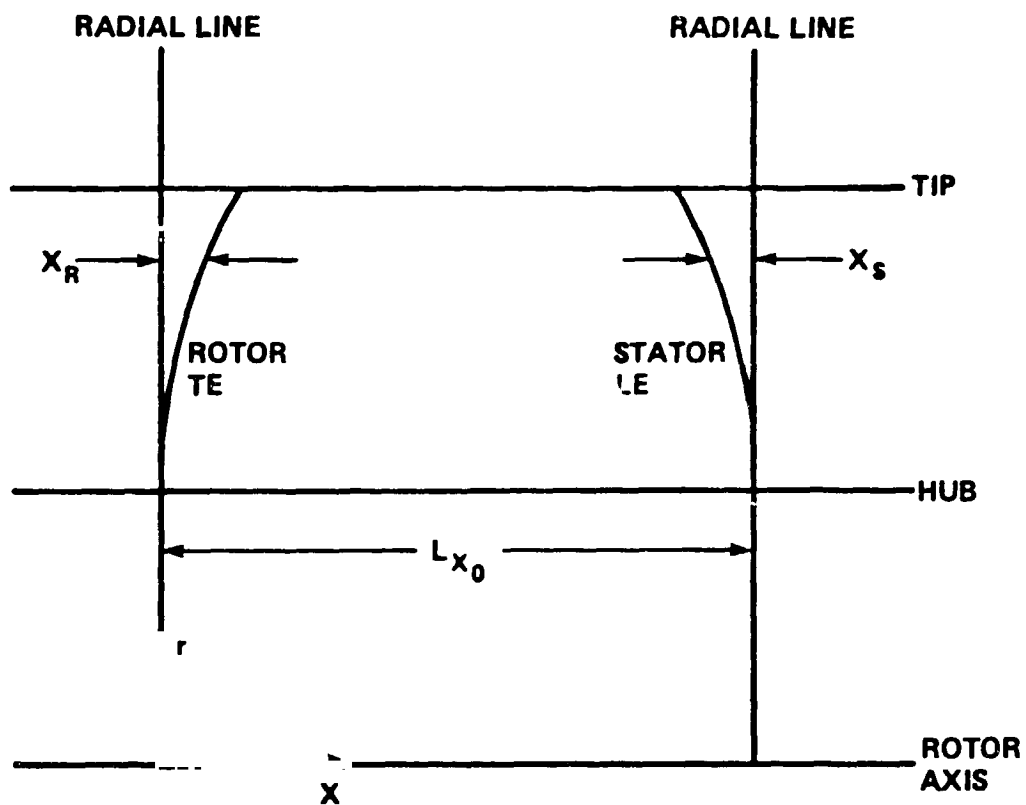


Figure 7. Schematic View of a Rotor Blade TE and Stator Vane LE Looking Perpendicular to the Rotor Axis

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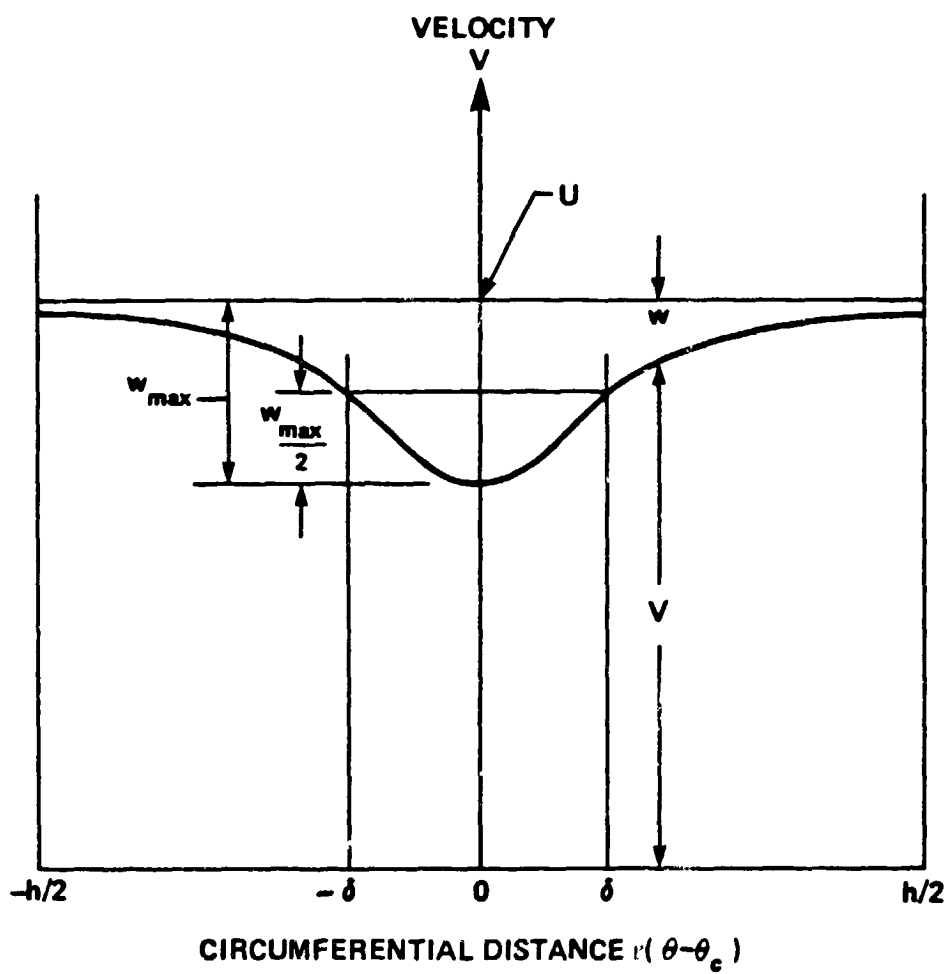


Figure 8. Typical Wake Profile

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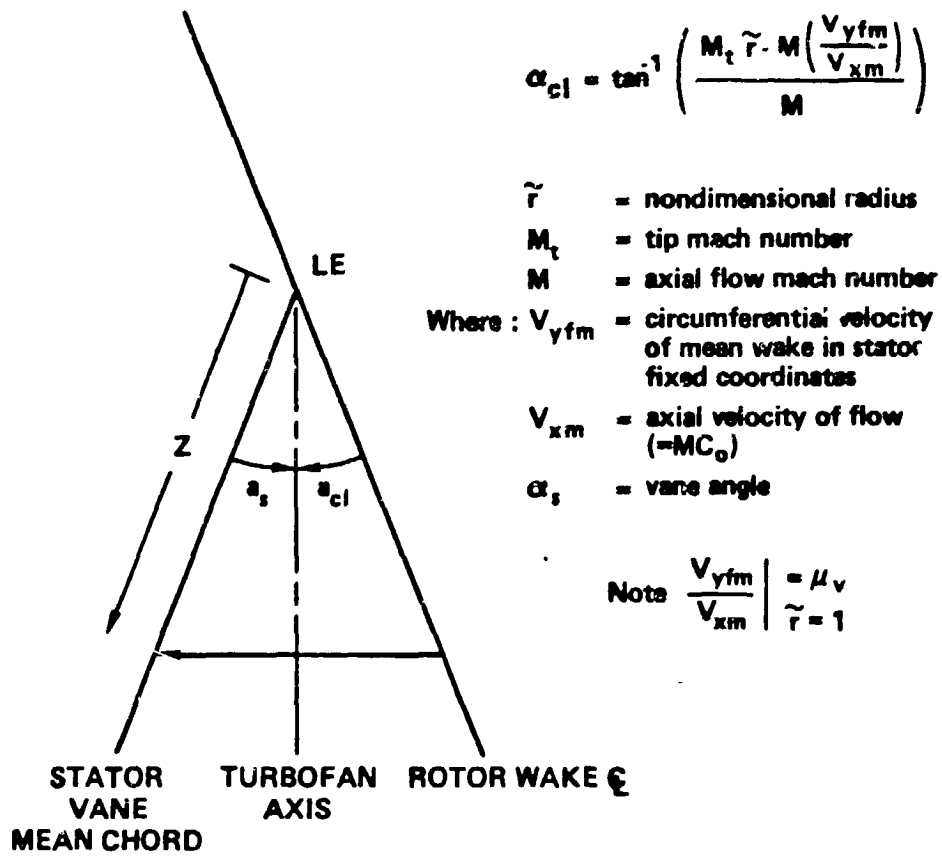


Figure 9. Schematic Diagram of the Stator Vane Mean Chord at the Instant When the Wake Centerline Intersects the Leading Edge

TABLES



TABLE 1. INPUT/OUTPUT DATA FOR THE MEAN ROTOR WAKE PROGRAM

This program calculates the complex modal amplitude and the modal sound power generated by the interaction of the mean rotor wakes with the stator vanes. All input and output data are nondimensional. The input data consist of geometric, performance, and computational parameters.

A. Geometric Data

	FORTTRAN NAME	SYMBOL	VARIABLE	FORTTRAN VARIABLE TYPE
1.	NBLADE	B	No. of rotor blades	Integer
2.	NVANE	V	No. of stator vanes	Integer
3.	SIGMAR	$\sigma_r$	Ratio of hub radius to duct radius	Floating Point
4.	SIGMAC	$\sigma_c$	Ratio of tip chord of <i>stator</i> vane to duct radius	Floating Point
5.	LXO	$d/r_{duct}$	Ratio of rotor-stator spacing to duct radius	Floating Point
6.			Vector of data for a number, NDAT (an integer variable) of <i>stator</i> vane radii	
a.	R	$\bar{r}$	Nondimensional radius = $r/r_{duct}$	Floating Point
b.	C	$\bar{c}$	Nondimensional vane chord = $c/c_{tip}$	Floating Point
c.	ALPHAS	$\alpha_s$	Vane angle (degrees)	Floating Point
d.	YS*	$\bar{y}_s$	Nonradial variation of <i>stator</i> leading edge = $Y_s/c_{tip}$	Floating Point
e.	YR*	$\bar{y}_r$	Nonradial variation of <i>rotor</i> trailing edge = $Y_r/c_{tip}$	Floating Point
f.	XS**	$\bar{x}_s$	Axial variation of <i>stator</i> leading edge = $X_s/c_{tip}$	Floating Point
g.	XR**	$\bar{x}_r$	Axial variation of <i>rotor</i> trailing edge = $X_r/c_{tip}$	Floating Point

\*See Figure 6

\*\*See Figure 7

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TABLE 1. (Cont.)

b. Performance Data

	FORTRAN NAME	SYMBOL	DEFINITION	FORTRAN VARIABLE TYPE
1.	MT	$M_t$	Tot Mach number	Floating Point
2.	MA	M	Axial flow Mach number	Floating Point
3.	IVOR	-	Switch for rotor wake specification = 0 for free vortex distribution = 1 for specified input velocity distribution	Integer
4.			(for IVOR = 1) Vector of data for a number, NVELO, (an integer variable) of <i>vane</i> radii	
	R	$\bar{r}$	a. Nondimensional radius	Floating Point
	XVEL	$\frac{V_{yfm}}{V_{xm}}$	b. Ratio of circumferential velocity to axial flow velocity of the mean wake (See Fig. 9)	Floating Point
5.	MUV	$\mu_v$	(for IVOR = 0) Ratio of circumfer- ential velocity at the duct radius to the axial flow velocity	Floating Point
6.	WWIDTH	$\delta/h$	Ratio of wake half-width to wake spacing (See Fig. 8)	Floating Point
7.	VELDEF	$w_{max}/U$	Ratio of maximum wake velocity deficit to the streamwise flow velocity (assumed constant with radius). (See Fig. 8)	Floating Point

TABLE 1. (Cont.)

C. Computational Data

These data set the number of integration stations in the chordwise and spanwise directions (and, indirectly, the accuracy of the results). The required accuracy for the Bessel functions used in the mode shape and eigenvalue routines are also specified.

	FORTRAN NAME	VARIABLE	FORTRAN VARIABLE TYPE
1.	NRAD	No. of integration stations in the radial direction (odd number)	Integer
2.	NCHORD	No. of integration stations in the chordwise direction (even number)	Integer
3.	EB	Absolute accuracy of all Bessel function calculations	Floating Point
4.	EC	Absolute accuracy of convergence to root of eigenvalue equation	Floating Point

Program Output

The output lists the complex nondimensional pressure amplitude for each propagating mode. The amplitude is nondimensionalized by the dynamic pressure of the mean axial flow  $\rho_0 U^2/2$ . Also given is the *relative* modal sound power level. To recover the conventional sound power level (dB re  $10^{-12}$  watt) add

$$10 \log_{10} \left[ \frac{\rho_0 c_0^3 M^4 r_{\text{duct}}^2}{8 \cdot 10^{-12}} \right]$$

to the computed relative power. This step is required because all computations performed in the program are nondimensional with absolute values of  $\rho_0$ ,  $c_0$ , and  $r_{\text{duct}}$  unknown.

TABLE 2. IMPORTANT INTERNAL PROGRAM VARIABLES  
MEAN ROTOR WAKE PROGRAM

(Used in addition to the INPUT/OUTPUT variables.)

FORTRAN NAME	SYMBOL	VARIABLE
AMN*	$A_{m,n}$	Weighting factors of mode shape $\psi = A_{m,n} J_m + B_{m,n} Y_m$
BMN*	$B_{m,n}$	
ARG*	$X_{m,n}$	Argument of the mode shape function $\psi$ ( $=\kappa_{m,n} r$ )
B*	$b$	Nondimensional vane semi-chord = $c/2c_{tip}$
BETASQ*	$\beta^2$	$1-M^2$ , where M is the axial flow Mach no.
DELTAP	$\Delta \bar{p}$	Nondimensional complex pressure along vane chord
DELTAR*	$\Delta \bar{r}$	Discrete radial interval for integration
GAMMA	$\Gamma$	Nondimensional wave number of the convected gust
GMNS*	$\tilde{\gamma}_{m,n,s}$	Nondimensional acoustic wavenumber for moving medium (See Eq. 87 of Vol. 1)
H1	$h_1$	Nondimensional stator vane spacing in direction parallel to vane (See Fig. B-1 of Vol. 1)
H2	$h_2$	Nondimensional stator vane spacing in direction perpendicular to vane (See Fig. B-1 of Vol. 1)
IER*, IERPS1	-	Error codes from Bessel function subroutines
IR*	-	Counter for integration stations in radial direction
IZ*	-	Counter for integration stations in chordwise direction
KMNS*	$K_{m,n,s}$	Nondimensional acoustic wavenumber = $r_{duct} \cdot K_{m,n,s}$ (See Eq. 88 of Vol. 1)

TABLE 2. (Cont.)

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KX	$k_x$	Nondimensional gust wavenumber in the axial direction
MM*	m	Circumferential mode number
MR	$M_r$	Relative Mach number of mean wake (vector sum of rotational and axial components)
MYM	-	Relative circumferential Mach no. of mean wake at $\bar{r}$ .
NN*	n	Radial mode number
PMNS	-	Sum of terms comprising the radial integral
PSI*, OR PSISTO*	$\psi$	Nondimensional radial mode shape as a function of radius
QMNS	-	Sum of terms comprising the chordwise integral
R*	$\bar{r}$	Nondimensional radius = $r/r_{\text{duct}}$
RELPRL	-	Relative modal sound power level at harmonic s
REPLWR, SPWR	-	Relative modal sound power at harmonic s
SB	sB	Product of harmonic number and no. of blades
SS	s	Harmonic number (=1,2,3) multiple of the rotor blade passage frequency
WH	$\hat{w}$	Complex nondimensional amplitude of gust velocity impinging on stator vane
WHTC	-	Weighting factor for Simpson Integration method used in chordwise integral
XMN*	$k_{m,n} r_{\text{duct}}$	Nondimensional root of duct eigenvalue equation (See Eq. 6 of Vol. 1)

\*These variables are also used in the inlet and wake turbulence programs, but are listed here only.

TABLE 3. UTILITY SUBROUTINES

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A. Subroutines common to the Mean Wake, Inlet, and Wake Turbulence programs.

1. ANRT (ANNular RooT), ANFU (ANNular FUNction), ISIGN  
Programs find the roots  $\kappa_{m,n}$  of the boundary value equation for the annular duct:

$$J'_m(\kappa_{m,n} r_{duct}) Y'_m(\kappa_{m,n} r_{hub}) - J'_m(\kappa_{m,n} r_{hub}) Y'_m(\kappa_{m,n} r_{duct}) = 0$$

2. FLSJ, BESY (BESSel functions of the first [J] and the second [i] kind)

BESJ computes the mth order Bessel function of the first kind,  $J_m(x)$ .

BESY computes the mth order Bessel function of the second kind,  $Y_m(x)$ .

An error code is returned along with each answer. The error code is:

- ERR = 0 No error (answer is correct to given accuracy)
- = 1 m was negative (must be  $\geq 0$ )
- = 2 Argument was negative (must be  $\geq 0$ )
- = 3 Required accuracy not obtained
- = 4 Range of n compared to the argument was not correct (see program listing).

3. EIGEN

The program normalizes the weighting factors  $A_{m,n}$  and  $B_{m,n}$  used in the mode function.

$$\psi = A_{m,n} J_m + B_{m,n} Y_m.$$

The orthogonality condition is

$$\int_A \psi_{i,j} \psi_{m,n}^* dA = \begin{cases} \Gamma_{m,n} & \text{if } i = m \text{ and } j = n \\ 0 & \text{otherwise} \end{cases}$$

The normalizing condition used is that

$$\bar{\Gamma}_{m,n} \equiv \frac{\Gamma_{m,n}}{\pi(r_{duct}^2 - r_{hub}^2)} = 1 \text{ (non-dimensional).}$$

TABLE 3. (Cont.)

4. RMODE  
Program computes the radial mode shape  $\psi$  for the  $m$ ,  $n$ th mode of the annular duct. (See Eq. 4 of Vol. 1)
  5. KERNEL  
Program computes the kernel for the Green's function formulation of the cascade routine. (See Eqs. B-25 and B-26 of Vol. 1)  
Used in conjunction with PRES or CASC.
- B. Subroutine used specifically for the Mean Wake Routine
1. PRES (PRESSure distribution)  
The program specifies the complex pressure distribution across the stator vane chord as produced by a velocity gust. The input parameters include the gust wavenumber, the wake velocity, and the stator vane spacings.
- C. Subroutines used specifically for the Inlet Turbulence Routine
1. SCALLX (SCALE Length, X direction)  
Program yields the turbulence length scale in the axial direction as a function of radial position. The routine is actually a program input whereby a particular turbulence distribution is loaded.
  2. SCALLR (SCALE Length, Radial direction)  
Program yields the turbulence length scale in the radial direction as a function of radial position. The routine is an input parameter.
  3. STHETA (Scale length, THETA direction)  
Program yields the turbulence length scale in the circumferential direction as a function of radial position. The routine is an input parameter.
  4. EPSD ( $\epsilon_D$ )  
Program yields the inlet RMS turbulence intensity as a function of radial position. The routine is an input parameter.
  5. PHITHH ( $\hat{\phi}_\theta$ )  
The program computes the Fourier transform of the correlation function in the circumferential direction. This transform is usually a fairly simple analytic function such as an exponential.

TABLE 3. (Cont.)

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6. PHIXHT ( $\hat{\phi}_x$ )

The program computes the Fourier transform of the correlation function in the axial direction.

D. Subroutines used for the Inlet and Wake Turbulence Routines

1. CASC (CASCade function.)

The program calculates the complex pressure distribution across a blade chord as produced by a velocity gust. The input parameters include the gust wavenumber, the wake velocity, and the blade spacings. This program is a version of PRES (listed above) specialized for use with the extended range of arguments in the turbulence routines.

E. Subroutine used specifically for the Wake Turbulence Routine

1. FHAT ( $\hat{f}$ )

The program computes the Fourier transform of the modulating function for the turbulent wake. The transform is usually a simple analytic function depending on the turbulence model in use.

F. IMSL Library Subroutine called by Subroutine KERNEL

IMSL Library routine LEQTIC is called by KERNEL to solve a set of simultaneous equations. The documentation provided by IMSL follows on the next three pages.



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TABLE 3. (Cont.) DESCRIPTION OF IMSL LIBRARY ROUTINE LEQ1C.

IMSL ROUTINE NAME - LEQ1C

PURPOSE - LINEAR EQUATION SOLUTION - COMPLEX MATRIX -  
SPACE ECONOMIZER SOLUTION

USAGE - CALL LEQ1C (A,N,IA,B,M,IB,IJOB,WA,IER)

ARGUMENTS

A - INPUT COMPLEX N BY N MATRIX CONTAINING THE  
COMPLEX COEFFICIENTS OF THE EQUATION  $AX = B$ .  
ON OUTPUT, A CONTAINS THE L-U DECOMPOSITION OF  
A ROWWISE PERMUTATION OF THE INPUT MATRIX A.

N - ORDER OF MATRIX A. (INPUT)

IA - ROW DIMENSION OF MATRIX A EXACTLY AS  
SPECIFIED IN THE DIMENSION STATEMENT IN THE  
CALLING PROGRAM. (INPUT)

B - INPUT COMPLEX N BY M MATRIX CONTAINING THE  
COMPLEX VALUED RIGHT HAND SIDES OF THE  
EQUATION  $AX = B$ .  
ON OUTPUT, THE SOLUTION MATRIX X REPLACES B.  
IF IJOB=1, B IS NOT USED.

M - NUMBER OF RIGHT HAND SIDES (COLUMNS IN B).  
(INPUT)

IB - ROW DIMENSION OF MATRIX B EXACTLY AS SPECIFIED  
IN THE DIMENSION STATEMENT IN THE CALLING  
PROGRAM. (INPUT)

IJOB - INPUT OPTION PARAMETER. IJOB=I IMPLIES WHEN  
I=0, FACTOR THE MATRIX AND SOLVE THE  
EQUATION  $AX=B$ .  
I=1, FACTOR THE MATRIX A.  
I=2, SOLVE THE EQUATION  $AX=B$ . THIS  
OPTION IMPLIES THAT LEQ1C HAS ALREADY  
BEEN CALLED USING IJOB=0 OR 1 SO THAT  
THE MATRIX HAS ALREADY BEEN FACTORED. IN  
THIS CASE OUTPUT MATRIX A MUST HAVE BEEN  
SAVED FOR REUSE IN THE CALL TO LEQ1C.

WA - WORK AREA OF LENGTH N CONTAINING THE PIVOT  
INDICES.

IER - ERROR PARAMETER. (OUTPUT)  
TERMINAL ERROR  
IER=129 INDICATES THAT MATRIX A IS  
ALGORITHMICALLY SINGULAR. (SEE THE  
CHAPTER L PRELUDE.)

PRECISION/HARDWARE - SINGLE AND DOUBLE/H32  
- SINGLE/H36,H48,H60

REQD. IMSL ROUTINES - UERTST,UGETIO

NOTATION - INFORMATION ON SPECIAL NOTATION AND  
CONVENTIONS IS AVAILABLE IN THE MANUAL  
INTRODUCTION OR THROUGH IMSL ROUTINE UHELP

REMARKS

1. WHEN IJOB=1, ARGUMENTS B, M AND IB ARE NOT USED BY  
LEQ1C.
2. INPUT MATRIX A IS DESTROYED WHEN IJOB=0 OR 1. WHEN  
IJOB=0 OR 2, B IS REPLACED WITH THE SOLUTION X.

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TABLE 3. (Cont.) DESCRIPTION OF IMSL LIBRARY ROUTINE LEQ1C.

3. LEQ1C CAN BE USED TO COMPUTE THE INVERSE OF A COMPLEX MATRIX. THIS IS DONE BY CALLING LEQ1C WITH M=N, B=THE N BY N IDENTITY MATRIX AND IJOB=0. WHEN N IS LARGE, IT MAY BE MORE PRACTICAL TO COMPUTE THE INVERSE A COLUMN AT A TIME. TO DO THIS, FIRST CALL LEQ1C WITH IJOB=1 TO FACTOR A. MAKE SUCCEEDING CALLS WITH M=1, B=A COLUMN OF THE IDENTITY MATRIX AND IJOB=2. B WILL BE REPLACED BY THE CORRESPONDING COLUMN OF A INVERSE.
4. THE DETERMINANT OF A CAN BE COMPUTED AFTER LEQ1C HAS BEEN CALLED AS FOLLOWS

```
DET = (1.0,0.0)
DO 5 I = 1,N
  IPVT = WA(I)
  IF (IPVT .NE. I) DET = -DET
  DET = DET*A(I,I)
5 CONTINUE
```

Algorithm

For a given N by N complex matrix A and an N by M complex matrix B, LEQ1C computes an LU decomposition of a rowwise permutation of A and solves the system of equations AX=B. Row equilibration and partial pivoting are used.

See reference:

Forsythe, George and Moler, Cleve B., Computer Solution of Linear Algebraic Systems, Prentice-Hall, Inc., Englewood Cliffs, New Jersey, 1967.

Example

This example shows how to solve a system of 3 equations in 3 unknowns using LEQ1C.

The equations are

$$\begin{aligned}(1.+i3.)X(1) + (2.5-i3.5)X(2) + (1.+i)X(3) &= (1.-i2.) \\ (6.+i2.)X(1) + (-4.+i3.)X(2) &= (3.-i4.) \\ (5.-i) X(1) + (1.+i) X(2) + (3.+i3.)X(3) &= (5.-i6.)\end{aligned}$$

and the unknowns are X(1),X(2), and X(3).

In this case, N=3 (A is 3 by 3), and M=1. (B is 3 by 1, one right hand side).

Input:

```
INTEGER N,IA,M,IB,IJOB,IER
COMPLEX A(3,3),B(3)
REAL WA(3)
IA = 3
IB = 3
N = 3
```

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TABLE 3. (Cont.) DESCRIPTION OF IMSL LIBRARY ROUTINE LEQTIC.

```
A =      (1.,3.)  (2.5,-3.5)  (1.,1.)  
          (6.,2.)  (-4.,2.)  (0.,0.)  
          (5.,-1.) (1.,1.)  (3.,3.)
```

```
M = 1
```

```
B =      (1.,-2.)  
          (3.,-4.)  
          (5.,-6.)
```

```
IJOB=0
```

```
CALL LEQTIC (A,N,IA,B,M,IB,IJOB,WA,IER)
```

```
  .  
  .  
END
```

```
Output:
```

```
IER = 0
```

```
B =      (-.32881, -.68795)  
          (-.48127, -.55729)  
          (.90092, -1.5177)
```

```
Hence the solution is
```

```
X(1) = -.32881 -i0.68795  
X(2) = -.48127 -i0.55729  
X(3) = .90092 -i1.5177
```

TABLE 4. SAMPLE EXECUTION OF THE MEAN ROTOR WAKE PROGRAM

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```
NVANE=
11
NVANE= 11
NBLADE=
15
NBLADE= 15
HUB RADIUS DIVIDED BY DUCT RADIUS =
.484
SIGMAR= 0.48400000E+00
VANE TIP CHORD DIVIDED BY DUCT RADIUS =
.408
SIGMAC= 0.40800000E+00
LX0 =
.6201
LX0= 0.62010000E+00
NDAT =
7
NDAT= 7
VANE GEOMETRY MATRIX INPUT
FEED MATRIX IN ONE ROW AT A TIME, FROM HUB TO TIP
ROW= 1 R/RDUCT =
.484
C/CTIP =
1.
ALPHAS (DEGREES)=
16.3
YS/CTIP =
0.
YR/CTIP =
0.
XS/CTIP =
0.
XR/CTIP =
0.
ROW= 2 R/RDUCT =
.56
C/CTIP =
1.
ALPHAS (DEGREES)=
15.67
YS/CTIP =
.027
YR/CTIP =
-.033
XS/CTIP =
-.001
XR/CTIP =
-.02
```

TABLE 4. (Cont.)

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ROW= 3 R/RDUCT =  
 .739  
 C/CTIP =  
 1.  
 ALPHAS (DEGREES)=  
 14.07  
 YS/CTIP =  
 .093  
 YR/CTIP =  
 -.118  
 XS/CTIP =  
 -.005  
 XR/CTIP =  
 -.057  
 ROW= 4 R/RDUCT =  
 .92  
 C/CTIP =  
 1.  
 ALPHAS (DEGREES)=  
 12.57  
 YS/CTIP =  
 .158  
 YR/CTIP =  
 -.213  
 XS/CTIP =  
 -.008  
 XR/CTIP =  
 -.073  
 ROW= 5 R/RDUCT =  
 .946  
 C/CTIP =  
 1.  
 ALPHAS (DEGREES)=  
 12.36  
 YS/CTIP =  
 .163  
 YR/CTIP =  
 -.226  
 XS/CTIP =  
 -.008  
 XR/CTIP =  
 -.07  
 ROW= 6 R/RDUCT =  
 .973  
 C/CTIP =  
 1.

TABLE 4. (Cont.)

OPTIONAL PAGE 13  
OF PROGRAM

ALPHAS (DEGREES)=

12.15

YS/CTIP =

.177

YR/CTIP =

-.242

XS/CTIP =

-.009

XR/CTIP =

-.067

ROW= 7 R/RDUCT =

1.

C/CTIP =

1.

ALPHAS (DEGREES)=

11.92

YS/CTIP =

.187

YR/CTIP =

-.262

XS/CTIP =

-.009

XR/CTIP =

-.064

WANE GEOMETRY MATRIX IS

0.484E+00	0.100E+01	0.284E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
0.560E+00	0.100E+01	0.273E+00	0.270E-01	-0.330E-01	-0.100E-02	-0.200E-01	
0.739E+00	0.100E+01	0.246E+00	0.930E-01	-0.118E+00	-0.500E-02	-0.570E-01	
0.920E+00	0.100E+01	0.219E+00	0.158E+00	-0.213E+00	-0.800E-02	-0.730E-01	
0.946E+00	0.100E+01	0.216E+00	0.163E+00	-0.226E+00	-0.800E-02	-0.700E-01	
0.973E+00	0.100E+01	0.212E+00	0.177E+00	-0.242E+00	-0.900E-02	-0.670E-01	
0.100E+01	0.100E+01	0.208E+00	0.187E+00	-0.262E+00	-0.900E-02	-0.640E-01	

TYPE 1 TO INPUT ROTOR FLOW VELOCITY, 0 FOR FREE VORTEX

1

IVOR= 1

NUMBER OF RADII FOR SPECIFYING MEAN ROTOR FLOW=

8

NVELO= 8

INPUT MATRIX FOR MEAN ROTOR FLOW

FEED MATRIX IN ONE ROW AT A TIME, FROM HUB TO TIP

ROW= 1 R/RDUCT=

.484

MEAN CIRCUMFERENTIAL VELOCITY RATIO=

.808

ROW= 2 R/RDUCT=

.533

TABLE 4. (Cont.)

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MEAN CIRCUMFERENTIAL VELOCITY RATIO=  
 .700  
 ROW= 3 R/RDUCT=  
 .612  
 MEAN CIRCUMFERENTIAL VELOCITY RATIO=  
 .784  
 ROW= 4 R/RDUCT=  
 .834  
 MEAN CIRCUMFERENTIAL VELOCITY RATIO=  
 .712  
 ROW= 5 R/RDUCT=  
 .918  
 MEAN CIRCUMFERENTIAL VELOCITY RATIO=  
 .688  
 ROW= 6 R/RDUCT=  
 .946  
 MEAN CIRCUMFERENTIAL VELOCITY RATIO=  
 .686  
 ROW= 7 R/RDUCT=  
 .974  
 MEAN CIRCUMFERENTIAL VELOCITY RATIO=  
 .713  
 ROW= 8 R/RDUCT=  
 1.  
 MEAN CIRCUMFERENTIAL VELOCITY RATIO=  
 .713  
 MEAN ROTOR FLOW VELOCITY MATRIX IS  
 .4840E+00 .8080E+00  
 .5330E+00 .7880E+00  
 .6120E+00 .7840E+00  
 .8340E+00 .7120E+00  
 .9180E+00 .6880E+00  
 .9460E+00 .6860E+00  
 .9740E+00 .7130E+00  
 .1000E+01 .7130E+00  
 MT =  
 .508  
 MT= 0.50800000E+00  
 MA =  
 .323  
 MA = 0.32300000E+00  
 WAKE WIDTH =  
 .172  
 WWIDTH= 0.17200000E+00  
 MAX VEL DEFICIT DIVIDED BY UBAR  
 .27  
 VELDEF= 0.27000000E+00

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TABLE 4. (Cont.)

NUMBER OF RADIAL STATIONS =  
7  
NRAD= 7  
NUMBER OF CHORDWISE STATIONS =  
8  
NCHORD= 8  
ACCURACY OF BESSEL FN =  
.001  
EB= 0.10000000E-02  
ACCURACY OF CONVERGENCE TO ROOT XMN =  
.0001  
EC= 0.10000000E-03

S = 3  
XMN(MAX) FOR PROPAGATION = 0.24154718E+02  
%FRSAPR Floating underflow PC= 6115  
  
%FRSAPR Floating underflow PC= 6163

MODE DATA

S = 3 M = 1 N = 1 XMN = 0.13709056E+01  
CUTOFF RATIO FOR MODE= .1762E+02  
SUM OF BESSEL FUNCTION ERROR CODES = 0  
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0  
AMN = 0.15152305E+01 BMN = -0.42119466E+00  
ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M = 1 N = 1 S = 3  
ERROR CODE FROM INVERSION ROUTINE= 0  
ERROR CODE FROM INVERSION ROUTINE= 0  
ERROR CODE FROM INVERSION ROUTINE= 0  
ERROR CODE FROM INVERSION ROUTINE= 0  
ERROR CODE FROM INVERSION ROUTINE= 0  
ERROR CODE FROM INVERSION ROUTINE= 0  
ERROR CODE FROM INVERSION ROUTINE= 0

UPSTREAM

GAMMA M,N,SB = 0.33725477E+02  
MODE AMPLITUDE = 0.13613387E-03 0.33358998E-04  
SUM OF ALL ERRORS IN PSI CALCULATIONS = 0  
RELATIVE SOUND POWER LEVEL FOR MODE(0B)= -0.7364E+02

DOWNSTREAM

GAMMA M,N,SB = -0.17237771E+02  
MODE AMPLITUDE = -0.47378941E-04 -0.72085580E-05  
SUM OF ALL ERRORS IN PSI CALCULATIONS = 0  
RELATIVE SOUND POWER LEVEL FOR MODE(0B)= -0.7715E+02



TABLE 4. (Cont.)

M= -1 N= 1 S= -3

UPSTREAM  
RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.7364E+02

DOWNSTREAM  
RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.7715E+02

MODE DATA

S = 3 M = 1 N = 2 XMN = 0.63900327E+01  
CUTOFF RATIO FOR MODE= .3780E+01  
SUM OF BESSEL FUNCTION ERROR CODES = 0  
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0  
AMN = 0.19356938E+01 BMN = 0.32269858E+01  
ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M = 1 N = 2 S = 3

UPSTREAM  
GAMMA M,N,SB = 0.32857319E+02  
MODE AMPLITUDE = -0.11049067E-03 -0.91503578E-04  
SUM OF ALL ERRORS IN PSI CALCULATIONS = 0  
RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.7351E+02

DOWNSTREAM  
GAMMA M,N,SB = -0.16369614E+02  
MODE AMPLITUDE = 0.56242548E-04 0.26364856E-04  
SUM OF ALL ERRORS IN PSI CALCULATIONS = 0  
RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.7519E+02

M= -1 N= 2 S= -3

UPSTREAM  
RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.7351E+02

DOWNSTREAM  
RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.7519E+02

MODE DATA

S = 3 M = 1 N = 3 XMN = 0.12724612E+02  
CUTOFF RATIO FOR MODE= .1960E+01  
SUM OF BESSEL FUNCTION ERROR CODES = 0  
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0  
AMN = 0.43514410E+01 BMN = 0.30726765E+01  
ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

TABLE 4. (Cont.)

ORIGINAL PAGE 13  
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M = 1 N = 3 S = 3

UPSTREAM

GAMMA M,N,SB = 0.30194305E+02  
MODE AMPLITUDE = -0.67274867E-04 -0.89817303E-06  
SUM OF ALL ERRORS IN PSI CALCULATIONS = 0  
RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.8036E+02

DOWNSTREAM

GAMMA M,N,SB = -0.13706599E+02  
MODE AMPLITUDE = 0.39056430E-04 0.46102940E-04  
SUM OF ALL ERRORS IN PSI CALCULATIONS = 0  
RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.7634E+02

M= -1 N= 3 S= -3

UPSTREAM

RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.8036E+02

DOWNSTREAM

RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.7634E+02

MODE DATA

S = 3 M = 1 N = 4 XMN = 0.18362274E+02  
CUTOFF RATIO FOR MODE= .1315E+01  
SUM OF BESSEL FUNCTION ERROR CODES = 0  
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0  
AMN = 0.61381751E+01 BMN = 0.22116971E+01  
ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M = 1 N = 4 S = 3

UPSTREAM

GAMMA M,N,SB = 0.24825892E+02  
MODE AMPLITUDE = 0.88119635E-06 0.55164443E-06  
SUM OF ALL ERRORS IN PSI CALCULATIONS = 0  
RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.1173E+03

DOWNSTREAM

GAMMA M,N,SB = -0.83381859E+01  
MODE AMPLITUDE = 0.10458061E-04 0.45172844E-04  
SUM OF ALL ERRORS IN PSI CALCULATIONS = 0  
RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.8064E+02

TABLE 4. (Cont.)

M= -1 N= 4 S= -3

UPSTREAM  
RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.1173E+03

DOWNSTREAM  
RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.8064E+02

LARGEST PROPAGATING N FOR THIS M = 4

MODE DATA

S = 3 M = -10 N = 1 XMN = 0.11769701E+02  
CUTOFF RATIO FOR MODE= .2052E+01  
SUM OF BESSEL FUNCTION ERROR CODES = 0  
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0  
AMN = 0.54257755E+01 BMN = -0.30348594E-02  
ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M = -10 N = 1 S = 3

UPSTREAM  
GAMMA M,N,SB = 0.30531741E+02  
MODE AMPLITUDE = -0.90896823E-04 0.41207877E-04  
SUM OF ALL ERRORS IN PSI CALCULATIONS = 0  
RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.7690E+02

DOWNSTREAM  
GAMMA M,N,SB = -0.14044035E+02  
MODE AMPLITUDE = -0.64741460E-03 -0.25779423E-03  
SUM OF ALL ERRORS IN PSI CALCULATIONS = 0  
RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.5498E+02

M= 10 N= 1 S= -3

UPSTREAM  
RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.7690E+02

DOWNSTREAM  
RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.5498E+02

MODE DATA

S = 3 M = -10 N = 2 XMN = 0.16348282E+02  
CUTOFF RATIO FOR MODE= .1478E+01  
SUM OF BESSEL FUNCTION ERROR CODES = 0  
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0  
AMN = 0.48044727E+01 BMN = -0.37694076E+00  
ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

TABLE 4. (Cont.)

ORIGINAL PAGE 13  
OF POOR QUALITY

M = -10 N = 2 S = 3

UPSTREAM

GAMMA M,N,SB = 0.27032509E+02  
MODE AMPLITUDE = 0.36213808E-04 0.13253067E-04  
SUM OF ALL ERRORS IN PSI CALCULATIONS = 0  
RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.8559E+02

DOWNSTREAM

GAMMA M,N,SB = -0.10544803E+02  
MODE AMPLITUDE = 0.54190425E-03 0.25744146E-03  
SUM OF ALL ERRORS IN PSI CALCULATIONS = 0  
RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.5754E+02

M = 10 N = 2 S = -3

UPSTREAM

RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.8559E+02

DOWNSTREAM

RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.5754E+02

MODE DATA

S = 3 M = -10 N = 3 XMN = 0.19710760E+02  
CUTOFF RATIO FOR MODE = .1225E+01  
SUM OF BESSEL FUNCTION ERROR CODES = 0  
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0  
AMN = 0.45357506E+01 BMN = -0.21469782E+01  
ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M = -10 N = 3 S = 3

UPSTREAM

GAMMA M,N,SB = 0.22996575E+02  
MODE AMPLITUDE = 0.50912282E-05 0.44796741E-04  
SUM OF ALL ERRORS IN PSI CALCULATIONS = 0  
RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.8492E+02

DOWNSTREAM

GAMMA M,N,SB = -0.65088688E+01  
MODE AMPLITUDE = -0.32015018E-03 -0.56725690E-03  
SUM OF ALL ERRORS IN PSI CALCULATIONS = 0  
RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.5844E+02

TABLE 4. (Cont.)

ORIGINAL PAGE IS  
OF POOR QUALITY

M= 10 N= 3 S= -3

UPSTREAM

RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.8492E+02

DOWNSTREAM

RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.5844E+02

MODE DATA

S = 3 M = -10 N = 4 XMN = 0.23588640E+02  
 CUTOFF RATIO FOR MODE= .1024E+01  
 SUM OF BESSEL FUNCTION ERROR CODES = 0  
 ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0  
 AMN = 0.62652037E+01 BMN = -0.98372497E+00  
 ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M = -10 N = 4 S = 3

UPSTREAM

GAMMA M,N,SB = 0.13736991E+02  
 MODE AMPLITUDE = -0.50110748E-03 -0.29130448E-03  
 SUM OF ALL ERRORS IN PSI CALCULATIONS = 0  
 RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.6613E+02

DOWNSTREAM

GAMMA M,N,SB = 0.27507146E+01  
 MODE AMPLITUDE = -0.34158767E-03 0.85520260E-03  
 SUM OF ALL ERRORS IN PSI CALCULATIONS = 0  
 RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.6090E+02

M= 10 N= 4 S= -3

UPSTREAM

RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.6613E+02

DOWNSTREAM

RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.6090E+02

LARGEST PROPAGATING N FOR THIS M = 4

MODE DATA

S = 3 M = 12 N = 1 XMN = 0.13878611E+02  
 CUTOFF RATIO FOR MODE= .1740E+01  
 SUM OF BESSEL FUNCTION ERROR CODES = 0  
 ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0  
 AMN = 0.60892918E+01 BMN = -0.63711792E-03  
 ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

TABLE 4. (Cont.)

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OF POOR QUALITY

M = 12 N = 1 S = 3

UPSTREAM

GAMMA M,N,SB = 0.25133072E+02  
MODE AMPLITUDE = 0.88696711E-04 0.15987079E-05  
SUM OF ALL ERRORS IN PSI CALCULATIONS = 0  
RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.7808E+02

DOWNSTREAM

GAMMA M,N,SB = -0.12645367E+07  
MODE AMPLITUDE = 0.95047415E-04 0.45870526E-03  
SUM OF ALL ERRORS IN PSI CALCULATIONS = 0  
RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.5892E+02

M= -12 N= 1 S= -3

UPSTREAM

RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.7808E+02

DOWNSTREAM

RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.5892E+02

MODE DATA

S = 3 M = 12 N = 2 XMN = 0.18713666E+02  
CUTOFF RATIO FOR MODE= .1291E+01  
SUM OF BESSEL FUNCTION ERROR CODES = 0  
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0  
AMN = 0.53619937E+01 BMN = -0.12842323E+00  
ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M = 12 N = 2 S = 3

UPSTREAM

GAMMA M,N,SB = 0.24381333E+02  
MODE AMPLITUDE = 0.31973551E-03 -0.67991251E-04  
SUM OF ALL ERRORS IN PSI CALCULATIONS = 0  
RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.6745E+02

DOWNSTREAM

GAMMA M,N,SB = -0.78936267E+01  
MODE AMPLITUDE = 0.14232207E-03 -0.40642054E-03  
SUM OF ALL ERRORS IN PSI CALCULATIONS = 0  
RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.6146E+02



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TABLE 4. (Cont.)

M= -12 N= 2 S= -3

UPSTREAM  
RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.6745E+02

DOWNSTREAM  
RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.6146E+02

MODE DATA

S = 3 M = 12 N = 3 XMN = 0.22297030E+02  
CUTOFF RATIO FOR MODE= .1083E+01  
SUM OF BESSEL FUNCTION ERROR CODES = 0  
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0  
AMN = 0.50662141E+01 BMN = -0.14574338E+01  
ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M = 12 N = 3 S = 3

UPSTREAM  
GAMMA M,N,SB = 0.18059368E+02  
MODE AMPLITUDE = -0.38293325E-03 -0.15805489E-03  
SUM OF ALL ERRORS IN PSI CALCULATIONS = 0  
RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.6696E+02

DOWNSTREAM  
GAMMA M,N,SB = -0.15716621E+01  
MODE AMPLITUDE = -0.11038813E-02 0.41711175E-03  
SUM OF ALL ERRORS IN PSI CALCULATIONS = 0  
RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.5569E+02

M= -12 N= 3 S= -3

UPSTREAM  
RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.6696E+02

DOWNSTREAM  
RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.5569E+02

LARGEST PROPAGATING N FOR THIS M = 3

MODE DATA

S = 3 M = -21 N = 1 XMN = 0.23254819E+02  
CUTOFF RATIO FOR MODE= .1039E+01  
SUM OF BESSEL FUNCTION ERROR CODES = 0  
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0  
AMN = 0.85042393E+01 BMN = -0.38116337E-05  
ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0



TABLE 4. (Cont.)

M = -21 N = 1 S = 3

UPSTREAM

GAMMA M,N,SB = 0.15145542E+02  
MODE AMPLITUDE = 0.63165623E-03 -0.10433352E-02  
SUM OF ALL ERRORS IN PSI CALCULATIONS = 0  
RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.5882E+02

DOWNSTREAM

GAMMA M,N,SB = 0.13421642E+01  
MODE AMPLITUDE = -0.18827030E-02 0.30355092E-02  
SUM OF ALL ERRORS IN PSI CALCULATIONS = 0  
RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.4796E+02

M= 21 N= 1 S= -3

UPSTREAM

RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.5882E+02

DOWNSTREAM

RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.4796E+02

LARGEST PROPAGATING N FOR THIS M = 1  
NO MORE PROPAGATING MODES FOR THIS VALUE OF S

S = 2  
XMN(MAX) FOR PROPAGATION = 0.16103146E+02

MODE DATA

S = 2 M = -3 N = 1 XMN = 0.39866274E+01  
CUTOFF RATIO FOR MODE= .4039E+01  
SUM OF BESSEL FUNCTION ERROR CODES = 0  
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0  
AMN = 0.26023450E+01 BMN = -0.32589376E+00  
ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M = -3 N = 1 S = 2  
ERROR CODE FROM INVERSION ROUTINE= 0  
ERROR CODE FROM INVERSION ROUTINE= 0  
ERROR CODE FROM INVERSION ROUTINE= 0  
ERROR CODE FROM INVERSION ROUTINE= 0  
ERROR CODE FROM INVERSION ROUTINE= 0  
ERROR CODE FROM INVERSION ROUTINE= 0  
ERROR CODE FROM INVERSION ROUTINE= 0



TABLE 4. (Cont.)

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## UPSTREAM

GAMMA M,N,SB = 0.21981403E+02  
 MODE AMPLITUDE = 0.13526694E-03 -0.11438489E-03  
 SUM OF ALL ERRORS IN PSI CALCULATIONS = 0  
 RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.7167E+02

## DOWNSTREAM

GAMMA M,N,SB = -0.10989599E+02  
 MODE AMPLITUDE = -0.12497451E-04 -0.25469007E-03  
 SUM OF ALL ERRORS IN PSI CALCULATIONS = 0  
 RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.6288E+02

M= 3 N= 1 S= -2

## UPSTREAM

RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.7167E+02

## DOWNSTREAM

RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.6288E+02

## MODE DATA

S = 2 M = -3 N = 2 XMN = 0.77467003E+01  
 CUTOFF RATIO FOR MODE= .2079E+01  
 SUM OF BESSEL FUNCTION ERROR CODES = 0  
 ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0  
 AMN = 0.35705322E+01 BMN = -0.89511162E+00  
 ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M = -3 N = 2 S = 2

## UPSTREAM

GAMMA M,N,SB = 0.20412827E+02  
 MODE AMPLITUDE = -0.62938154E-04 0.18019367E-03  
 SUM OF ALL ERRORS IN PSI CALCULATIONS = 0  
 RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.7126E+02

## DOWNSTREAM

GAMMA M,N,SB = -0.94210234E+01  
 MODE AMPLITUDE = -0.56493354E-03 0.30607513E-03  
 SUM OF ALL ERRORS IN PSI CALCULATIONS = 0  
 RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.5566E+02

TABLE 4. (Cont.)

M= 3 N= 2 S= -2

UPSTREAM

RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.7126E+02

DOWNSTREAM

RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.5566E+02

MODE DATA

S = 2 M = -3 N = 3 XMN = 0.13008803E+02  
CUTOFF RATIO FOR MODE= .1238E+01  
SUM OF BESSEL FUNCTION ERROR CODES = 0  
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0  
AMN = -0.18754296E+00 BMN = 0.53089865E+01  
ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M = -3 N = 3 S = 2

UPSTREAM

GAMMA M,N,SB = 0.15524623E+02  
MODE AMPLITUDE = -0.87384578E-05 -0.13593062E-03  
SUM OF ALL ERRORS IN PSI CALCULATIONS = 0  
RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.7526E+02

DOWNSTREAM

GAMMA M,N,SB = -0.45328195E+01  
MODE AMPLITUDE = 0.50005592E-03 0.24067449E-03  
SUM OF ALL ERRORS IN PSI CALCULATIONS = 0  
RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.5971E+02

M= 3 N= 3 S= -2

UPSTREAM

RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.7526E+02

DOWNSTREAM

RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.5971E+02

LARGEST PROPAGATING N FOR THIS M = 3

MODE DATA

S = 2 M = 8 N = 1 XMN = 0.96413107E+01  
CUTOFF RATIO FOR MODE= .1670E+01  
SUM OF BESSEL FUNCTION ERROR CODES = 0  
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0  
AMN = 0.48101923E+01 BMN = -0.14625735E-01  
ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

TABLE 4. (Cont.)

ORIGINAL PAGE IS  
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M = 8 N = 1 S = 2

## UPSTREAM

GAMMA M,N,SB = 0.19124322E+02  
 MODE AMPLITUDE = -0.15710355E-02 0.39986281E-02  
 SUM OF ALL ERRORS IN PSI CALCULATIONS = 0  
 RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.4444E+02

## DOWNSTREAM

GAMMA M,N,SB = -0.81325179E+01  
 MODE AMPLITUDE = 0.66697707E-03 -0.60581600E-04  
 SUM OF ALL ERRORS IN PSI CALCULATIONS = 0  
 RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.5598E+02

M = -8 N = 1 S = -2

## UPSTREAM

RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.4444E+02

## DOWNSTREAM

RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.5598E+02

## MODE DATA

S = 2 M = 8 N = 2 XMN = 0.13862791E+02  
 CUTOFF RATIO FOR MODE= .1122E+01  
 SUM OF BESSEL FUNCTION ERROR CODES = 0  
 ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0  
 AMN = 0.41234860E+01 BMN = -0.85984376E+00  
 ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M = 8 N = 2 S = 2

## UPSTREAM

GAMMA M,N,SB = 0.14153511E+02  
 MODE AMPLITUDE = -0.50227789E-02 -0.46086625E-02  
 SUM OF ALL ERRORS IN PSI CALCULATIONS = 0  
 RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.4172E+02

## DOWNSTREAM

GAMMA M,N,SB = -0.31617076E+01  
 MODE AMPLITUDE = -0.18333959E-02 -0.37698765E-03  
 SUM OF ALL ERRORS IN PSI CALCULATIONS = 0  
 RELATIVE SOUND POWER LEVEL FOR MODE(DB)= -0.5006E+02

TABLE 4. (Cont.)

ORIGINAL PAGE IS  
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M = -8 N = 2 S = -2

UPSTREAM

RELATIVE SOUND POWER LEVEL FOR MODE(DB) = -0.4172E+02

DOWNSTREAM

RELATIVE SOUND POWER LEVEL FOR MODE(DB) = -0.5006E+02

LARGEST PROPAGATING N FOR THIS M = 2

MODE DATA

S = 2 M = -14 N = 1 XMN = 0.15975402E+02

CUTOFF RATIO FOR MODE = .1008E+01

SUM OF BESSEL FUNCTION ERROR CODES = 0

ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0

AMN = 0.66675895E+01 BMN = -0.10554324E-03

ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M = -14 N = 1 S = 2

UPSTREAM

GAMMA M,N,SB = 0.76348570E+01

MODE AMPLITUDE = -0.15299872E-01 0.33717128E-01

SUM OF ALL ERRORS IN PSI CALCULATIONS = 0

RELATIVE SOUND POWER LEVEL FOR MODE(DB) = -0.3212E+02

DOWNSTREAM

GAMMA M,N,SB = 0.33569469E+01

MODE AMPLITUDE = 0.13580878E-01 0.28533771E-01

SUM OF ALL ERRORS IN PSI CALCULATIONS = 0

RELATIVE SOUND POWER LEVEL FOR MODE(DB) = -0.3279E+02

M = 14 N = 1 S = -2

UPSTREAM

RELATIVE SOUND POWER LEVEL FOR MODE(DB) = -0.3212E+02

DOWNSTREAM

RELATIVE SOUND POWER LEVEL FOR MODE(DB) = -0.3279E+02

LARGEST PROPAGATING N FOR THIS M = 1  
NO MORE PROPAGATING MODES FOR THIS VALUE OF S

S = 1

XMN(MAX) FOR PROPAGATION = 0.80515728E+01

## TABLE 4. (Cont.)

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## MODE DATA

S = 1 M = 4 N = 1 XMN = 0.51995376E+01  
 CUTOFF RATIO FOR MODE = .1549E+01  
 SUM OF BESSEL FUNCTION ERROR CODES = 0  
 ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0  
 AMN = 0.31336383E+01 BMN = -0.20930871E+00  
 ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M = 4 N = 1 S = 1  
 ERROR CODE FROM INVERSION ROUTINE = 0  
 ERROR CODE FROM INVERSION ROUTINE = 0  
 ERROR CODE FROM INVERSION ROUTINE = 0  
 ERROR CODE FROM INVERSION ROUTINE = 0  
 ERROR CODE FROM INVERSION ROUTINE = 0  
 ERROR CODE FROM INVERSION ROUTINE = 0  
 ERROR CODE FROM INVERSION ROUTINE = 0

## UPSTREAM

GAMMA M,N,SB = 0.92437007E+01  
 MODE AMPLITUDE = -0.16022921E-01 -0.12244703E-01  
 SUM OF ALL ERRORS IN PSI CALCULATIONS = 0  
 RELATIVE SOUND POWER LEVEL FOR MODE(DB) = -0.3113E+02

## DOWNSTREAM

GAMMA M,N,SB = -0.37477989E+01  
 MODE AMPLITUDE = -0.10714520E-02 0.23857642E-02  
 SUM OF ALL ERRORS IN PSI CALCULATIONS = 0  
 RELATIVE SOUND POWER LEVEL FOR MODE(DB) = -0.4450E+02

M = -4 N = 1 S = -1

## UPSTREAM

RELATIVE SOUND POWER LEVEL FOR MODE(DB) = -0.3113E+02

## DOWNSTREAM

RELATIVE SOUND POWER LEVEL FOR MODE(DB) = -0.4450E+02

LARGEST PROPAGATING N FOR THIS M = 1  
 NO MORE PROPAGATING MODES FOR THIS VALUE OF S  
 PROBLEM COMPLETED

RELATIVE POWER LEVEL UPSTREAM S = 1 -0.2812E+02  
 RELATIVE POWER LEVEL UPSTREAM S = 2 -0.2843E+02  
 RELATIVE POWER LEVEL UPSTREAM S = 3 -0.5381E+02  
 RELATIVE POWER LEVEL DOWNSTREAM S = 1 -0.4149E+02  
 RELATIVE POWER LEVEL DOWNSTREAM S = 2 -0.2964E+02  
 RELATIVE POWER LEVEL DOWNSTREAM S = 3 -0.4253E+02  
 STOP

## END OF EXECUTION

CPU TIME: 4:39.68  
 EXIT.

ELAPSED TIME: 20:51.21

TABLE 5. INPUT/OUTPUT DATA FOR THE INLET TURBULENCE PROGRAMS

This program calculates the modal power spectral density for noise generated by a turbofan rotor subjected to inlet turbulence. All input and output data are nondimensional. The input variables are defined in order to parallel as closely as possible the variables used in the Mean Wake Program. The input data consist of geometric, performance, turbulence, and computational parameters.

A. Geometric Data

	FORTRAN NAME	SYMBOL	VARIABLE	FORTRAN VARIABLE TYPE
1.	NBLADE	B	No. of rotor blades	Integer
2.	SIGMAR	$\sigma_r$	Ratio of hub radius to duct radius	Floating Point
3.	SIGMAC	$\sigma_c$	Ratio of tip chord of rotor blade to duct radius	Floating Point
4.			Vector of data for a number, NDAT (an integer variable) of rotor blade radii	
a.	R	$\bar{r}$	Nondimensional radius = $r/r_{duct}$	Floating Point
b.	C	$\bar{c}$	Nondimensional blade chord = $c/c_{tip}$	Floating Point
c.	CHI	X	Blade angle (degrees) [See Fig. 3 of Vol. 1]	Floating Point

B. Performance Data

	FORTRAN NAME	SYMBOL	VARIABLE	FORTRAN VARIABLE TYPE
1.	MT	$M_t$	Tip Mach number	Floating Point
2.	MA	M	Axial flow Mach number	Floating Point
3.			Frequency range data: Pressure distributions are calculated and stored for the range of frequencies from PSTART to PEND in steps of PSTEP. These data are interpolated for calculations at the frequency of interest OMEGA.	

TABLE 5. (Cont.)

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	FORTRAN NAME	SYMBOL	VARIABLE	FORTRAN VARIABLE TYPE
a.	PSTART	-	First frequency for pressure calculation. Must be an integer multiple of shaft frequency. (Usually = NBLADE)	Integer
b.	PEND	-	Final frequency for pressure calculation. See text for description of value required.	Integer
c.	PSTEP	-	Frequency step size in pressure calculation. (Usually = NBLADE)	Integer
d.	OMEGA	$\omega/\Omega$	Noise frequency of interest (nondimensionalized on the rotor shaft frequency)	Floating Point

## C. Turbulence Data

The inlet turbulence data are loaded into separate function subroutines. This arrangement allows rather complicated radial distributions of turbulence to be modeled.

	FORTRAN FUNCTION NAME	SYMBOL	VARIABLE
1.	SCALLX	$\tilde{L}_x(\bar{r})$	Axial turbulence length scale (nondimensionalized on the duct radius) as a function of nondimensionalized radius.*
2.	SCALLR	$\tilde{L}_r(\bar{r})$	Radial turbulence length scale (nondimensionalized on the duct radius) as a function of nondimensionalized radius.
3.	STHETA	$\tilde{L}_\theta(\bar{r})$	Circumferential turbulence length scale (nondimensionalized on the duct radius) as a function of nondimensionalized radius.*
4.	EPSD	$\epsilon_D(\bar{r})$	RMS turbulence velocity (nondimensionalized on the mean axial velocity) as a function of nondimensionalized radius. (See Eq. 94 of Vol. 1)

\*See page 48 of Vol. 1.

TABLE 5. (Cont.)

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## D. Computational Data

These data set the number of integration stations in the chordwise and spanwise directions (and, indirectly, the accuracy of the results). The required accuracy for the Bessel functions used in the mode shape and eigenvalue routines are also specified.

FORTRAN NAME	VARIABLE	FORTRAN VARIABLE TYPE
1. NRAD	No. of radial stations at which pressure distributions are calculated (odd number)	Integer
2. NRADNU	No. of integration stations in the chordwise direction (odd number)	Integer
3. NCHORD	No. of integration stations in the chordwise direction (even number)	Integer
4. EB	Absolute accuracy of all Bessel function calculations	Floating Point
5. EC	Absolute accuracy of convergence to annular root for boundary value problem	Floating Point

## Program Output

The output consists of the *relative* power spectral density for each propagating mode and for the sum of all propagating modes at the frequency of interest. The output is given in terms of the nondimensional quantity

$$10 \log_{10} \left[ \frac{S_{mn}}{\rho_0 c_0^2 r_{duct}^3} \right]$$

where  $S_{mn}$  is the spectral density (watt/Hz),  $\rho_0$  is the ambient air density,  $c_0$  is the small-signal speed of sound and  $r_{duct}$  is the (dimensional) duct radius. To recover the conventional spectral density (dB re  $10^{-12}$  watt/Hz) one must add

$$10 \log_{10} \left[ \frac{\rho_0 c_0^2 r_{duct}^3}{10^{-12} \text{ watt}} \right]$$

to the output of the program. This step is required because all computations performed in the program are nondimensional with absolute values of  $\rho_0$ ,  $c_0$ , and  $r_{duct}$  unknown.



TABLE 6. IMPORTANT INTERNAL VARIABLES FOR THE INLET TURBULENCE PROGRAM

(Used in addition to INPUT/OUTPUT Variables)

FORTRAN NAME	SYMBOL	VARIABLE
BJ(N) <sup>+</sup>	$J_N(X)$	Nth order Bessel function of the first kind
CASCET <sup>+</sup>	$\Delta\bar{p}$	Stored values of the chordwise pressure distribution
H <sup>+</sup>	-	Vector length of blade spacing between corresponding points on any two neighboring blades (See Fig. B.1)
AB <sup>+</sup>	-	Nondimensional gust wave number [ $=M_t b \sigma_c (\frac{\omega}{\Omega} - m) / M_r$ ]
LR <sup>+</sup>	$\tilde{L}_r(\bar{r})$	Ratio of radial turbulence length scale to duct radius
LTHETA	$\tilde{L}_\theta(\bar{r})$	Ratio of circumferential turbulence length scale to duct radius
LX <sup>+</sup>	$\tilde{L}_x(\bar{r})$	Ratio of axial turbulence length scale to duct radius
OMEGA <sup>+</sup>	$\omega/\Omega$	Ratio of noise frequency to rotor shaft frequency
OMEGBC <sup>+</sup>	-	Nondimensional acoustic wavenumber for reduced frequency [ $=M_t \sigma_c b (\frac{\omega}{\Omega} - m)$ ]
PHIARG <sup>+</sup>	-	Argument of $\hat{\phi}_x$ (Argument)
PMNS	-	Sum of terms comprising the radial integral
QMNS	-	Sum of terms comprising the chordwise integral
RELPRL <sup>+</sup>	-	Relative modal power spectral density level at a given frequency
RELPCR <sup>+</sup> or SPWR <sup>+</sup>	-	Relative modal power spectral density at given frequency
RRRS <sup>+</sup>	$R_g$	Weighting factor for Bessel-type integration in chordwise direction
SIGMA <sup>+</sup>	$\sigma$	Interblade phase angle (See page 52 of Vol. 1)
THEARG <sup>+</sup>	-	Argument of $\hat{\phi}_\theta$ (Argument)
WHTR <sup>+</sup>	-	Weighting factor for Simpson integration in radial direction

<sup>+</sup>These variables are also used in the wake turbulence routine, but are listed here only.

TABLE 7. SAMPLE EXECUTION OF THE INLET TURBULENCE DATA STORAGE ROUTINE

```

@ROTORS
NBLADE=
15
NBLADE= 15
HUB RADIUS DIVIDED BY DUCT RADIUS =
.46
SIGNAR= 0.46000000E+00
BLADE TIP CHORD DIVIDED BY DUCT RADIUS=
.374
SIGNAC= 0.37400000E+00
NDAT =
10
NDAT= 10
BLADE GEOMETRY MATRIX INPUT
FEED MATRIX IN ONE ROW AT A TIME, FROM HUB TO TIP
ROW= 1 R/RDUCT =
.46
C/CTIP =
.628
CHI (DEGREES)=
5.61
ROW= 2 R/RDUCT =
.514
C/CTIP =
.662
CHI (DEGREES)=
9.73
ROW= 3 R/RDUCT =
.541
C/CTIP =
.68
CHI (DEGREES)=
11.74
ROW= 4 R/RDUCT =
.622
C/CTIP =
.735
CHI (DEGREES)=
17.48
ROW= 5 R/RDUCT =
.73
C/CTIP =
.811
CHI (DEGREES)=
24.22
ROW= 6 R/RDUCT =
.838

```

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TABLE 7. (Cont.)

C/CTIP =  
.887  
CHI (DEGREES)=  
30.66  
ROW= 7 R/RDUCT =  
.919  
C/CTIP =  
.945  
CHI (DEGREES)=  
35.44  
ROW= 8 R/RDUCT =  
.946  
C/CTIP =  
.959  
CHI (DEGREES)=  
37.05  
ROW= 9 R/RDUCT =  
.973  
C/CTIP =  
.976  
CHI (DEGREES)=  
38.96  
ROW= 10 R/RDUCT =  
1.  
C/CTIP =  
1.  
CHI (DEGREES)=  
41.14  
BLADE GEOMETRY MATRIX IS  
0.460E+00 0.628E+00 0.979E-01  
0.514E+00 0.662E+00 0.170E+00  
0.541E+00 0.680E+00 0.205E+00  
0.622E+00 0.735E+00 0.305E+00  
0.730E+00 0.811E+00 0.423E+00  
0.838E+00 0.887E+00 0.535E+00  
0.919E+00 0.945E+00 0.619E+00  
0.946E+00 0.959E+00 0.647E+00  
0.973E+00 0.976E+00 0.680E+00  
1.100E+01 0.100E+01 0.718E+00  
MT =  
.508  
MT= 0.50800000E+00  
MA =  
.323  
MA = 0.32300000E+00  
NUMBER OF RADIAL STATIONS =  
5  
NRAD= 5

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TABLE 7. (Cont.)

NUMBER OF CHORDWISE STATIONS =  
8  
NCHORD= 8  
START FREQUENCY(HARMONIC NO. OF SHAFT) =  
15  
PSTART= 15  
END FREQUENCY(HARMONIC NO. OF SHAFT) =  
75  
P END= 75  
FREQUENCY STEP SIZE (HARMONIC ORDERS) =  
15  
PSTEP= 15  
ENTER TITLE FOR DATA FILE(MAX 72 CHARACTERS)  
NASA ROTOR 55,NCHORD=8,NRAD=580Z DESIGN SPEED/9-25-9\180  
ERROR CODE FROM INVERSION ROUTINE= 0

*(Note: Edited for brevity -- Error Code  
repeated for 375 inversions.)*

ERROR CODE FROM INVERSION ROUTINE= 0  
STOP

END OF EXECUTION  
CPU TIME: 52:32.72      ELAPSED TIME: 1:32:28.46  
EXIT.

TABLE 8. SAMPLE EXECUTION OF THE INLET TURBULENCE NOISE  
CALCULATION

@INSRCH

USER-ASSIGNED TITLE OF DATA SET FROM FILE "ROTO" IS  
NASA ROTOR 55, NCHORD=8, MRAD=580% DESIGN SPEED/9-25-80  
NOISE FREQUENCY/SHAFT FREQUENCY=

15.

OMEGA= .1500E+02

NUMBER OF RADIAL POSITIONS FOR ACOUSTIC COMP.=

7

NRADNU= 7

ACCURACY OF BESSEL FNS=

.001

EB= .1000E-02

ACCURACY OF CONVERGENCE TO ROOT XNM=

.0001

EC= .1000E-03

XNM(MAX) FOR PROPAGATION = 0.80515728E+01

*WARNING: This sample is for  
illustration purposes only.  
The input data for this  
execution did not correspond  
with Table 7 above.*

MODE DATA

OMEGA= .1500E+02 M= 0 N= 1 XNM= .0000E+00

PLANE WAVE MODE: CUTOFF RATIO IS + INFINITE

SUM OF BESSEL FUNCTION ERROR CODES = 0

ERROR CODE FOR CONVERGENCE TO ROOT XNM = 0

AMN = 0.10000000E+01 BMN = 0.00000000E+00

ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M= 0 N= 1 OMEGA= .1500E+02

UPSTREAM

GAMMA M,N,SB = 0.11255539E+02

REL. MODAL SOUND POWER SPECTRAL DENSITY=-.2031E-08

SUM OF ALL ERRORS IN PSI CALCULATIONS = 0

SUM OF ALL ERRORS IN RS CALCULATIONS= 0

REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.8692E+02

DOWNSTREAM

GAMMA M,N,SB = -0.57596368E+01

REL. MODAL SOUND POWER SPECTRAL DENSITY= .4316E-08

SUM OF ALL ERRORS IN PSI CALCULATIONS = 0

SUM OF ALL ERRORS IN RS CALCULATIONS= 0

REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.8365E+02

MODE DATA

OMEGA= .1500E+02 M= 0 N= 2 XNM= .5944E+01

CUTOFF RATIO FOR MODE= .1354E+01

SUM OF BESSEL FUNCTION ERROR CODES = 0

ERROR CODE FOR CONVERGENCE TO ROOT XNM = 0

AMN = -0.17828589E+01 BMN = 0.31951480E+01

ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

TABLE 8. (Cont.)

M= 0 N= 2 OMEGA= .1500E+02

UPSTREAM

GAMMA M,N,SB = 0.84861763E+01  
REL. MODAL SOUND POWER SPECTRAL DENSITY=-.4482E-08  
SUM OF ALL ERRORS IN PSI CALCULATIONS = 0  
SUM OF ALL ERRORS IN RS CALCULATIONS= 0  
REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.8349E+02

DOWNSTREAM

GAMMA M,N,SB = -0.29907743E+01  
REL. MODAL SOUND POWER SPECTRAL DENSITY= .2133E-08  
SUM OF ALL ERRORS IN PSI CALCULATIONS = 0  
SUM OF ALL ERRORS IN RS CALCULATIONS= 0  
REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.8671E+02

LARGEST PROPAGATING N FOR THIS M = 2

ZFRSAPR Floating underflow PC= 17366

ZFRSAPR Floating underflow PC= 17433

MODE DATA

OMEGA= .1500E+02 M= 1 N= 1 XMN= .1396E+01  
CUTOFF RATIO FOR MODE= .5769E+01  
SUM OF BESSEL FUNCTION ERROR CODES = 0  
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0  
AMN = 0.15347161E+01 BMN = -0.40872429E+00  
ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M= 1 N= 1 OMEGA= .1500E+02

UPSTREAM

GAMMA M,N,SB = 0.11126733E+02  
REL. MODAL SOUND POWER SPECTRAL DENSITY=-.3481E-07  
SUM OF ALL ERRORS IN PSI CALCULATIONS = 0  
SUM OF ALL ERRORS IN RS CALCULATIONS= 0  
REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.7458E+02

DOWNSTREAM

GAMMA M,N,SB = -0.56308314E+01  
REL. MODAL SOUND POWER SPECTRAL DENSITY= .6363E-07  
SUM OF ALL ERRORS IN PSI CALCULATIONS = 0  
SUM OF ALL ERRORS IN RS CALCULATIONS= 0  
REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.7196E+02

TABLE 8. (Cont.)

ORIGINAL PAGE IS  
OF POOR QUALITY

M= -1 N= 1 OMEGA= .1500E+02

M= -1 N= 1 OMEGA= .1500E+02

UPSTREAM

GAMMA M,N,SB = 0.11126733E+02

REL. MODAL SOUND POWER SPECTRAL DENSITY=-.1139E-09

SUM OF ALL ERRORS IN PSI CALCULATIONS = 0

SUM OF ALL ERRORS IN RS CALCULATIONS= 0

REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.9943E+02

DOWNSTREAM

GAMMA M,N,SB = -0.56308314E+01

REL. MODAL SOUND POWER SPECTRAL DENSITY= .2030E-09

SUM OF ALL ERRORS IN PSI CALCULATIONS = 0

SUM OF ALL ERRORS IN RS CALCULATIONS= 0

REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.9492E+02

MODE DATA

OMEGA= .1500E+02 M= 1 N= 2 XMN= .6150E+01

CUTOFF RATIO FOR MODE= .1309E+01

SUM OF BESSEL FUNCTION ERROR CODES = 0

ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0

AMN = 0.25524893E+01 BMN = 0.26060464E+01

ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M= 1 N= 2 OMEGA= .1500E+02

UPSTREAM

GAMMA M,N,SB = 0.82391651E+01

REL. MODAL SOUND POWER SPECTRAL DENSITY=-.5133E-07

SUM OF ALL ERRORS IN PSI CALCULATIONS = 0

SUM OF ALL ERRORS IN RS CALCULATIONS= 0

REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.7290E+02

DOWNSTREAM

GAMMA M,N,SB = -0.27432631E+01

REL. MODAL SOUND POWER SPECTRAL DENSITY= .3747E-07

SUM OF ALL ERRORS IN PSI CALCULATIONS = 0

SUM OF ALL ERRORS IN RS CALCULATIONS= 0

REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.7426E+02

M= -1 N= 2 OMEGA= .1500E+02

M= -1 N= 2 OMEGA= .1500E+02

TABLE 8. (Cont.)

ORIGINAL PAGE IS  
OF POOR QUALITY

UPSTREAM

GAMMA M,N,SB = 0.82391651E+01  
REL. MODAL SOUND POWER SPECTRAL DENSITY=-.3109E-09  
SUM OF ALL ERRORS IN PSI CALCULATIONS = 0  
SUM OF ALL ERRORS IN RS CALCULATIONS= 0  
REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.9507E+02

DOWNSTREAM

GAMMA M,N,SB = -0.27432631E+01  
REL. MODAL SOUND POWER SPECTRAL DENSITY= .4165E-10  
SUM OF ALL ERRORS IN PSI CALCULATIONS = 0  
SUM OF ALL ERRORS IN RS CALCULATIONS= 0  
REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.1038E+03

LARGEST PROPAGATING N FOR THIS M = 2

MODE DATA

OMEGA= .1500E+02 M= 2 N= 1 XMN= .2748E+01  
CUTOFF RATIO FOR MODE= .2930E+01  
SUM OF BESSEL FUNCTION ERROR CODES = 0  
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0  
AMN = 0.21049825E+01 BMN = -0.38973734E+00  
ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M= 2 N= 1 OMEGA= .1500E+02

UPSTREAM

GAMMA M,N,SB = 0.10744835E+02  
REL. MODAL SOUND POWER SPECTRAL DENSITY=-.2065E-06  
SUM OF ALL ERRORS IN PSI CALCULATIONS = 0  
SUM OF ALL ERRORS IN RS CALCULATIONS= 0  
REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.6665E+02

DOWNSTREAM

GAMMA M,N,SB = -0.52489328E+01  
REL. MODAL SOUND POWER SPECTRAL DENSITY= .7372E-06  
SUM OF ALL ERRORS IN PSI CALCULATIONS = 0  
SUM OF ALL ERRORS IN RS CALCULATIONS= 0  
REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.6132E+02

M= -2 N= 1 OMEGA= .1500E+02

M= -2 N= 1 OMEGA= .1500E+02



TABLE 8. (Cont.)

ORIGINAL PAGE IS  
OF POOR QUALITY

## UPSTREAM

GAMMA M,N,SB = 0.10744835E+02  
 REL. MODAL SOUND POWER SPECTRAL DENSITY=-.7070E-11  
 SUM OF ALL ERRORS IN PSI CALCULATIONS = 0  
 SUM OF ALL ERRORS IN RS CALCULATIONS= 0  
 REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.1115E+03

## DOWNSTREAM

GAMMA M,N,SB = -0.52489328E+01  
 REL. MODAL SOUND POWER SPECTRAL DENSITY= .6529E-11  
 SUM OF ALL ERRORS IN PSI CALCULATIONS = 0  
 SUM OF ALL ERRORS IN RS CALCULATIONS= 0  
 REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.1119E+03

## MODE DATA

OMEGA= .1500E+02 M= 2 N= 2 XMN= .6738E+01  
 CUTOFF RATIO FOR MODE= .1195E+01  
 SUM OF BESSEL FUNCTION ERROR CODES = 0  
 ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0  
 AMN = 0.36099485E+01 BMN = 0.11001426E+01  
 ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M= 2 N= 2 OMEGA= .1500E+02

## UPSTREAM

GAMMA M,N,SB = 0.74045386E+01  
 REL. MODAL SOUND POWER SPECTRAL DENSITY=-.1927E-06  
 SUM OF ALL ERRORS IN PSI CALCULATIONS = 0  
 SUM OF ALL ERRORS IN RS CALCULATIONS= 0  
 REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.6715E+02

## DOWNSTREAM

GAMMA M,N,SB = -0.19086367E+01  
 REL. MODAL SOUND POWER SPECTRAL DENSITY= .3230E-06  
 SUM OF ALL ERRORS IN PSI CALCULATIONS = 0  
 SUM OF ALL ERRORS IN RS CALCULATIONS= 0  
 REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.6491E+02

M= -2 N= 2 OMEGA= .1500E+02

M= -2 N= 2 OMEGA= .1500E+02

## UPSTREAM

GAMMA M,N,SB = 0.74045386E+01  
 REL. MODAL SOUND POWER SPECTRAL DENSITY=-.2280E-10  
 SUM OF ALL ERRORS IN PSI CALCULATIONS = 0  
 SUM OF ALL ERRORS IN RS CALCULATIONS= 0  
 REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.1064E+03

## DOWNSTREAM

GAMMA M,N,SB = -0.19086367E+01  
 REL. MODAL SOUND POWER SPECTRAL DENSITY= .2400E-12  
 SUM OF ALL ERRORS IN PSI CALCULATIONS = 0  
 SUM OF ALL ERRORS IN RS CALCULATIONS= 0  
 REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.1262E+03

LARGEST PROPAGATING N FOR THIS M = 2

TABLE 8. (Cont.)

ORIGINAL PAGE IS  
OF POOR QUALITY

MODE DATA

OMEGA= .1500E+02 M= 3 N= 1 XMN= .4027E+01  
CUTOFF RATIO FOR MODE= .2000E+01  
SUM OF BESSEL FUNCTION ERROR CODES = 0  
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0  
AMN = 0.26815693E+01 BMN = -0.27568805E+00  
ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M= 3 N= 1 OMEGA= .1500E+02

UPSTREAM

GAMMA M,N,SB = 0.10115297E+02  
REL. MODAL SOUND POWER SPECTRAL DENSITY=-.8401E-06  
SUM OF ALL ERRORS IN PSI CALCULATIONS = 0  
SUM OF ALL ERRORS IN RS CALCULATIONS= 0  
REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.6076E+02

DOWNSTREAM

GAMMA M,N,SB = -0.46193948E+01  
REL. MODAL SOUND POWER SPECTRAL DENSITY= .7621E-05  
SUM OF ALL ERRORS IN PSI CALCULATIONS = 0  
SUM OF ALL ERRORS IN RS CALCULATIONS= 0  
REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=- 5118E+02

M= -3 N= 1 OMEGA= .1500E+02

M= -3 N= 1 OMEGA= .1500E+02

UPSTREAM

GAMMA M,N,SB = 0.10115297E+02  
REL. MODAL SOUND POWER SPECTRAL DENSITY=-.5393E-12  
SUM OF ALL ERRORS IN PSI CALCULATIONS = 0  
SUM OF ALL ERRORS IN RS CALCULATIONS= 0  
REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.1227E+03

DOWNSTREAM

GAMMA M,N,SB = -0.46193948E+01  
REL. MODAL SOUND POWER SPECTRAL DENSITY= .6330E-13  
SUM OF ALL ERRORS IN PSI CALCULATIONS = 0  
SUM OF ALL ERRORS IN RS CALCULATIONS= 0  
REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.1320E+03

MODE DATA

OMEGA= .1500E+02 M= 3 N= 2 XMN= .7642E+01  
CUTOFF RATIO FOR MODE= .1054E+01  
SUM OF BESSEL FUNCTION ERROR CODES = 0  
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0  
AMN = 0.33544744E+01 BMN = -0.11908489E+01  
ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0



TABLE 8. (Cont.)

ORIGINAL PAGE IS  
OF POOR QUALITY

M= 3 N= 2 OMEGA= .1500E+02

UPSTREAM

GAMMA M,N,SB = 0.54275270E+01  
REL. MODAL SOUND POWER SPECTRAL DENSITY=-.2364E-06  
SUM OF ALL ERRORS IN PSI CALCULATIONS = 0  
SUM OF ALL ERRORS IN RS CALCULATIONS= 0  
REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.6626E+02

DOWNSTREAM

GAMMA M,N,SB = 0.68375036E-01  
REL. MODAL SOUND POWER SPECTRAL DENSITY= .1706E-05  
SUM OF ALL ERRORS IN PSI CALCULATIONS = 0  
SUM OF ALL ERRORS IN RS CALCULATIONS= 0  
REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.5768E+02

M= -3 N= 2 OMEGA= .1500E+02

M= -3 N= 2 OMEGA= .1500E+02

UPSTREAM

GAMMA M,N,SB = 0.54275270E+01  
REL. MODAL SOUND POWER SPECTRAL DENSITY=-.2331E-11  
SUM OF ALL ERRORS IN PSI CALCULATIONS = 0  
SUM OF ALL ERRORS IN RS CALCULATIONS= 0  
REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.1163E+03

DOWNSTREAM

GAMMA M,N,SB = 0.68375036E-01  
REL. MODAL SOUND POWER SPECTRAL DENSITY= .9788E-12  
SUM OF ALL ERRORS IN PSI CALCULATIONS = 0  
SUM OF ALL ERRORS IN RS CALCULATIONS= 0  
REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.1201E+03

LARGEST PROPAGATING N FOR THIS M = 2

MODE DATA

OMEGA= .1500E+02 M= 4 N= 1 XMN= .5230E+01  
CUTOFF RATIO FOR MODE= .1539E+01  
SUM OF BESSEL FUNCTION ERROR CODES = 0  
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0  
AMN = 0.32237284E+01 BNN = -0.16030403E+00  
ERROR CODE FOR BESSEL FNS IN AMN AND BNN CALC = 0 0 0 0 0 0 0 0

M= 4 N= 1 OMEGA= .1500E+02



TABLE 8. (Cont.)

UPSTREAM

GAMMA M,N,SB = 0.92161443E+01  
REL. MODAL SOUND POWER SPECTRAL DENSITY=-.2038E-05  
SUM OF ALL ERRORS IN PSI CALCULATIONS = 0  
SUM OF ALL ERRORS IN RS CALCULATIONS= 0  
REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.5691E+02

DOWNSTREAM

GAMMA M,N,SB = -0.37202422E+01  
REL. MODAL SOUND POWER SPECTRAL DENSITY= .6538E-04  
SUM OF ALL ERRORS IN PSI CALCULATIONS = 0  
SUM OF ALL ERRORS IN RS CALCULATIONS= 0  
REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.4185E+02

M= -4 N= 1 OMEGA= .1500E+02

M= -4 N= 1 OMEGA= .1500E+02

UPSTREAM

GAMMA M,N,SB = 0.92161443E+01  
REL. MODAL SOUND POWER SPECTRAL DENSITY=-.5114E-13  
SUM OF ALL ERRORS IN PSI CALCULATIONS = 0  
SUM OF ALL ERRORS IN RS CALCULATIONS= 0  
REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.1329E+03

DOWNSTREAM

GAMMA M,N,SB = -0.37202422E+01  
REL. MODAL SOUND POWER SPECTRAL DENSITY= .3263E-14  
SUM OF ALL ERRORS IN PSI CALCULATIONS = 0  
SUM OF ALL ERRORS IN RS CALCULATIONS= 0  
REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.1449E+03

LARGEST PROPAGATING N FOR THIS M = 1

MODE DATA

OMEGA= .1500E+02 M= 5 N= 1 XMN= .6376E+01  
CUTOFF RATIO FOR MODE= .1263E+01  
SUM OF BESSEL FUNCTION ERROR CODES = 0  
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0  
AMN = 0.37079083E+01 BMN = -0.81471940E-01  
ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M= 5 N= 1 OMEGA= .1500E+02

UPSTREAM

GAMMA M,N,SB = 0.79436739E+01  
REL. MODAL SOUND POWER SPECTRAL DENSITY=-.1669E-05  
SUM OF ALL ERRORS IN PSI CALCULATIONS = 0  
SUM OF ALL ERRORS IN RS CALCULATIONS= 0  
REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.5778E+02

TABLE 8. (Cont.)

ORIGINAL PAGE IS  
OF POOR QUALITY

DOWNSTREAM

GAMMA M,N,SB = -0.24477719E+01  
REL. MODAL SOUND POWER SPECTRAL DENSITY= .4521E-03  
SUM OF ALL ERRORS IN PSI CALCULATIONS = 0  
SUM OF ALL ERRORS IN RS CALCULATIONS= 0  
REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.3345E+02

M= -5 N= 1 OMEGA= .1500E+02

M= -5 N= 1 OMEGA= .1500E+02

UPSTREAM

GAMMA M,N,SB = 0.79436739E+01  
REL. MODAL SOUND POWER SPECTRAL DENSITY=-.4608E-14  
SUM OF ALL ERRORS IN PSI CALCULATIONS = 0  
SUM OF ALL ERRORS IN RS CALCULATIONS= 0  
REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.1434E+03

DOWNSTREAM

GAMMA M,N,SB = -0.24477719E+01  
REL. MODAL SOUND POWER SPECTRAL DENSITY= .1763E-14  
SUM OF ALL ERRORS IN PSI CALCULATIONS = 0  
SUM OF ALL ERRORS IN RS CALCULATIONS= 0  
REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.1475E+03

LARGEST PROPAGATING N FOR THIS M = 1

MODE DATA

OMEGA= .1500E+02 M= 6 N= 1 XMN= .7484E+01  
CUTOFF RATIO FOR MODE= .1076E+01  
SUM OF BESSEL FUNCTION ERROR CODES = 0  
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0  
AMN = 0.41370714E+01 BMN = -0.38730478E-01  
ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M= 6 N= 1 OMEGA= .1500E+02

UPSTREAM

GAMMA M,N,SB = 0.58865744E+01  
REL. MODAL SOUND POWER SPECTRAL DENSITY=-.4244E-04  
SUM OF ALL ERRORS IN PSI CALCULATIONS = 0  
SUM OF ALL ERRORS IN RS CALCULATIONS= 0  
REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.4372E+02

DOWNSTREAM

GAMMA M,N,SB = -0.39067242E+00  
REL. MODAL SOUND POWER SPECTRAL DENSITY= .2657E-02  
SUM OF ALL ERRORS IN PSI CALCULATIONS = 0  
SUM OF ALL ERRORS IN RS CALCULATIONS= 0  
REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.2576E+02

TABLE 8. (Cont.)

ORIGINAL PAGE IS  
OF POOR QUALITY

M= -6 N= 1 OMEGA= .1500E+02

M= -6 N= 1 OMEGA= .1500E+02

UPSTREAM

GAMMA M,N,SB = 0.58865744E+01

REL. MODAL SOUND POWER SPECTRAL DENSITY=-.3327E-15

SUM OF ALL ERRORS IN PSI CALCULATIONS = 0

SUM OF ALL ERRORS IN RS CALCULATIONS= 0

REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.1548E+03

DOWNSTREAM

GAMMA M,N,SB = -0.39067242E+00

REL. MODAL SOUND POWER SPECTRAL DENSITY= .2438E-15

SUM OF ALL ERRORS IN PSI CALCULATIONS = 0

SUM OF ALL ERRORS IN RS CALCULATIONS= 0

REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.1561E+03

LARGEST PROPAGATING N FOR THIS M = 1

NO MORE PROPAGATING MODES FOR THIS OMEGA

PROBLEM COMPLETED

RELATIVE POWER SPECTRAL DENSITY LEVEL UPSTREAM=-.4321E+02

REL. POWER SPECTRAL DENSITY LEVEL DOWNSTREAM=-.2497E+02

STOP

END OF EXECUTION

CPU TIME: 3:0.55

ELAPSED TIME: 11:11.94

EXIT.

TABLE 9. INPUT/OUTPUT DATA FOR THE ROTOR WAKE TURBULENCE PROGRAM

This program calculates the modal power spectral density for noise generated by the interaction of rotor wake turbulence with the stator vanes. All input and output data are nondimensional. The input variables are defined in order to parallel as closely as possible the variables used in the Mean Wake and Inlet Turbulence programs. The input data consist of geometric, performance, turbulence, and computational parameters.

A. Geometric Data

FORTTRAN NAME	SYMBOL	VARIABLE	FORTTRAN VARIABLE TYPE
1. NVANE	V	No. of stator vanes	Integer
2. NBLADE	B	No. of rotor blades	Integer
3. SIGMAR	$\sigma_r$	Ratio of hub radius to duct radius	Floating Point
4. SIGMAC	$\sigma_c$	Ratio of tip chord of stator vane to duct radius	Floating Point
5.		Vector of data for a number, NDAT (an integer variable) of stator vane radii	
a. R	$\bar{r}$	Nondimensional radius = $r/r_{duct}$	Floating Point
b. C	$\bar{c}$	Nondimensional vane chord = $c/c_{tip}$	Floating Point
c. THETA	$\theta$	Vane angle (degrees)	Floating Point

B. Performance Data

FORTTRAN NAME	SYMBOL	VARIABLE	FORTTRAN VARIABLE TYPE
1. MT	$M_t$	Tip Mach number	Floating Point
2. MA	M	Axial flow Mach number	Floating Point
3.		Frequency range data: Pressure distributions are calculated and stored for the range of frequencies from PSTART to PEND in steps of PSTEP. These data are interpolated for calculations at the frequency of interest OMEGA. See text.	

TABLE 9. (Cont.)

ORIGINAL P...  
OF POOR QUALITY

	FORTTRAN NAME	SYMBOL	VARIABLE	FORTTRAN VARIABLE TYPE
a.	PSTART	-	First frequency for pressure calculation. Must be an integer multiple of shaft frequency. (Usually = NBLADE)	Integer
b.	PEND	-	Final frequency for pressure calculation. (Usually = 3x NBLADE)	Integer
c.	PSTEP	-	Frequency step size in pressure calculations. (Usually = NBLADE)	Integer
d.	OMEGA	$\omega/\Omega$	Noise frequency of interest (non-dimensionalized on the rotor shaft frequency)	Floating Point
4.	IVOR	-	Switch for rotor wake specification = 0 for free vortex distribution = 1 for specified input velocity distribution	Integer
5.		(for IVOR = 1)	Vector of data for a number, NVELO (an integer variable) of vane radii	
	R	$\bar{r}$	a. Nondimensional radius	Floating Point
	XVEL	$\frac{V_{yfm}}{V_{xm}}$	b. Ratio of circumferential velocity of mean wake to axial flow velocity (See Fig. 9)	Floating Point
6.	MUV	$u_v$	(for IVOR = 0) Ratio of circumferential velocity at the duct radius to the axial flow velocity	Floating Point

C. Turbulence Data

The wake turbulence data are assumed to be constant across the duct.

	FORTTRAN NAME	SYMBOL	VARIABLE	FORTTRAN VARIABLE TYPE
1.	LX	$\bar{L}_x$	Axial turbulence length scale (nondimensionalized on the duct radius)	Floating Point



TABLE 9. (Cont.)

ORIGINAL PAGE IS  
OF POOR QUALITY

FORTTRAN NAME	SYMBOL	VARIABLE	FORTTRAN VARIABLE TYPE
2. LR	$\bar{L}_r$	Radial turbulence length scale (nondimensionalized on the duct radius)	Floating Point
3. LPHETA	$\bar{L}_\theta$	Circumferential turbulence length scale (nondimensionalized on the duct radius)	Floating Point
4. EPSW	$\epsilon_w$	RMS turbulence velocity at wake centerline (nondimensionalized on the mean axial velocity), [see Eq. 138 of Vol. 1]	Floating Point
5. WWIDTH	$\bar{\delta}$	Ratio of turbulent wake width to duct radius (See Eq. 140 of Vol. 1)	Floating Point

## D. Computational Data

The computational input data are identical to those used for the inlet turbulence routine.

## Program Output

The output consists of the *relative* power spectral density for all propagating modes at the frequency of interest. The nondimensionalization used here is identical to that used for the inlet turbulence routine.

TABLE 10. IMPORTANT INTERNAL PROGRAM VARIABLES FOR THE ROTOR  
WAKE TURBULENCE PROGRAM

(Used in addition to INPUT/OUTPUT variables)

FORTRAN NAME	SYMBOL	VARIABLE
OMEGA	$\omega/\Omega$	Ratio of noise frequency to rotor shaft frequency
FARG		Argument of $\hat{f}$ (argument)
-THETA		Stator vane angle (radius)
QSUM	-	Sum of correlation function contributions multiplying pressure distribution. Value must exceed QTESTR (input variable) before pressure distribution is actually calculated.
MTHETA	-	Circumferential wake Mach number at a given radius
MYM	-	Relative circumferential wake Mach number at a given radius

TABLE 11. SAMPLE EXECUTION OF THE ROTOR WAKE TURBULENCE  
DATA STORAGE ROUTINE

ORIGINAL PAGE IS  
OF POOR QUALITY

QSTATOR  
NVANE=  
11  
NVANE= 11  
NBLADE=  
15  
NBLADE= 15  
HUB RADIUS DIVIDED BY DUCT RADIUS =  
.484  
SIGMAR= 0.48400000E+00  
VANE TIP CHORD DIVIDED BY DUCT RADIUS=  
.408  
SIGNAC= 0.40800000E+00  
NDAT =  
7  
NDAT= 7  
VANE GEOMETRY MATRIX INPUT  
FEED MATRIX IN ONE ROW AT A TIME, FROM HUB TO TIP  
ROW= 1 R/RDUCT =  
.484  
C/CTIP =  
1.  
THETA (DEGREES)=  
16.3  
ROW= 2 R/RDUCT =  
.56  
C/CTIP =  
1.  
THETA (DEGREES)=  
15.67  
ROW= 3 R/RDUCT =  
.739  
C/CTIP =  
1.  
THETA (DEGREES)=  
14.07  
ROW= 4 R/RDUCT =  
.92  
C/CTIP =  
1.  
THETA (DEGREES)=  
12.57  
ROW= 5 R/RDUCT =  
.946  
C/CTIP =  
1.

TABLE 11. (Cont.)

THETA (DEGREES)=

12.36

ROW= 6 R/RDUCT =

.973

C/CTIP =

1.

THETA (DEGREES)=

12.15

ROW= 7 R/RDUCT =

1.

C/CTIP =

1.

THETA (DEGREES)=

11.92

VANE GEOMETRY MATRIX IS

0.484E+00 0.100E+01 0.284E+00

0.560E+00 0.100E+01 0.273E+00

0.739E+00 0.100E+01 0.246E+00

0.920E+00 0.100E+01 0.219E+00

0.946E+00 0.100E+01 0.216E+00

0.973E+00 0.100E+01 0.212E+00

0.100E+01 0.100E+01 0.208E+00

TYPE 1 TO INPUT ROTOR WAKE VELOCITY; 0 FOR FREE VORTEX

1

IVOR= 1

NUMBER OF RADII FOR SPECIFYING MEAN ROTOR FLOW=

8

NVELO= 8

INPUT MATRIX FOR MEAN ROTOR FLOW

FEED MATRIX IN ONE ROW AT A TIME, FROM HUB TO TIP

ROW= 1 R/RDUCT=

.484

MEAN CIRCUMFERENTIAL VELOCITY RATIO(U CIRCUM/U AXIAL)=

.808

ROW= 2 R/RDUCT=

.533

MEAN CIRCUMFERENTIAL VELOCITY RATIO(U CIRCUM/U AXIAL)=

.788

ROW= 3 R/RDUCT=

.612

MEAN CIRCUMFERENTIAL VELOCITY RATIO(U CIRCUM/U AXIAL)=

.784

ROW= 4 R/RDUCT=

.834

MEAN CIRCUMFERENTIAL VELOCITY RATIO(U CIRCUM/U AXIAL)=

.712

TABLE 11. (Cont.)

ORIGINAL PAGE IS  
OF POOR QUALITY

ROW= 5 R/RDUCT=  
.918  
MEAN CIRCUMFERENTIAL VELOCITY RATIO(U CIRCUM/U AXIAL)=  
.688  
ROW= 6 R/RDUCT=  
.946  
MEAN CIRCUMFERENTIAL VELOCITY RATIO(U CIRCUM/U AXIAL)=  
.686  
ROW= 7 R/RDUCT=  
.974  
MEAN CIRCUMFERENTIAL VELOCITY RATIO(U CIRCUM/U AXIAL)=  
.713  
ROW= 8 R/RDUCT=  
1.  
MEAN CIRCUMFERENTIAL VELOCITY RATIO(U CIRCUM/U AXIAL)=  
.713  
MEAN ROTOR FLOW VELOCITY MATRIX IS  
    .4840E+00 .8080E+00  
    .5330E+00 .7880E+00  
    .6120E+00 .7840E+00  
    .8340E+00 .7120E+00  
    .9180E+00 .6880E+00  
    .9460E+00 .6860E+00  
    .9740E+00 .7130E+00  
    .1000E+01 .7130E+00  
MT =  
.508  
MT= 0.50800000E+00  
MA =  
.323  
MA = 0.32300000E+00  
NUMBER OF RADIAL STATIONS =  
5  
NRAD= 5  
NUMBER OF CHORDWISE STATIONS (.LE.20) =  
8  
NCHORD= 8  
START FREQUENCY(HARMONIC NO. OF SHAFT )=  
15  
PSTART= 15  
END FREQUENCY(HARMONIC NO. OF SHAFT)=  
45  
P END= 45  
FREQUENCY STEP SIZE (HARMONIC ORDERS)=  
15  
PSTEP= 15

TABLE 11. (Cont.)

ENTER TITLE FOR DATA FILE (MAX 72 CHARACTERS)  
NASA ROTOR/STATOR 55/15 BLADES, 11 VANES/WAKE TURBULENCE STORAGE  
ERROR CODE FROM INVERSION ROUTINE= 0  
ERROR CODE FROM INVERSION ROUTINE= 0  
ERROR CODE FROM INVERSION ROUTINE= 0  
ERROR CODE FROM INVERSION ROUTINE= 0  
ERROR CODE FROM INVERSION ROUTINE= 0  
ERROR CODE FROM INVERSION ROUTINE= 0  
ERROR CODE FROM INVERSION ROUTINE= 0

*(Note: Edited for brevity -- Error Code  
repeated 165 times.)*

ERROR CODE FROM INVERSION ROUTINE= 0  
STOP

END OF EXECUTION  
CPU TIME: 21:28.07      ELAPSED TIME: 1:16:29.97  
EXIT.  
^C

TABLE 12. SAMPLE EXECUTION OF THE ROTOR WAKE TURBULENCE  
NOISE CALCULATION

ORIGINAL PAGE IS  
OF POOR QUALITY

WASRCH  
USER-ASSIGNED TITLE OF DATA SET FROM FILE "STAT" IS  
NASA ROTOR/STATOR 55/15 BLADES, 11 VANES/WAKE TURBULENCE STORAGE  
NOISE FREQUENCY/SHAFT FREQUENCY=

15.  
OMEGA= .1500E+02  
NUMBER OF RADIAL POSITIONS FOR ACOUSTIC COMP.=  
7  
NRADNU= 7  
ACCURACY OF BESSEL FNS=  
.001  
EB= .1000E-02  
ACCURACY OF CONVERGENCE TO ROOT XMW=  
.0001  
EC= .1000E-03  
WAKE WIDTH=  
.072  
WWIDTH= .7200E-01  
TURBULENCE INTENSITY(RMS FLUCTUATING U/U BAR)=  
.01  
EPSU= .1000E-01  
TURBULENCE LENGTH SCALE IN AXIAL DIRECTION=  
.5  
LX= .5000E+00  
TURBULENCE LENGTH SCALE IN RADIAL DIRECTION=  
.5  
LR= .5000E+00  
TURBULENCE LENGTH SCALE IN CIRCUMFERENTIAL DIRECTION=  
.5  
LTHETA= .5000E+00

M= 0 N= 1 OMEGA= .1500E+02  
XFRSAPR Floating underflow PC= 17374  
XFRSAPR Floating underflow PC= 17374

UPSTREAM  
REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.9627E+02

DOWNSTREAM  
REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.9577E+02

M= 0 N= 2 OMEGA= .1500E+02

UPSTREAM  
REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.9546E+02

DOWNSTREAM  
REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.1009E+03

TABLE 12. (Cont.)

M= 1 N= 1 OMEGA= .1500E+02

UPSTREAM  
REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.8998E+02

DOWNSTREAM  
REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.1116E+03

M= -1 N= 1 OMEGA= .1500E+02

UPSTREAM  
REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.1050E+03

DOWNSTREAM  
REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.9336E+02

M= 1 N= 2 OMEGA= .1500E+02

UPSTREAM  
REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.8850E+02

DOWNSTREAM  
REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.9785E+02

M= -1 N= 2 OMEGA= .1500E+02

UPSTREAM  
REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.1071E+03

DOWNSTREAM  
REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.9508E+02

M= 2 N= 1 OMEGA= .1500E+02

UPSTREAM  
REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.8758E+02

DOWNSTREAM  
REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.9249E+02

M= -2 N= 1 OMEGA= .1500E+02

UPSTREAM  
REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.1222E+03

DOWNSTREAM  
REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.9020E+02



TABLE 12. (Cont.)

M= 2 N= 2 OMEGA= .1500E+02

UPSTREAM  
REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.8410E+02

DOWNSTREAM  
REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.8596E+02

M= -2 N= 2 OMEGA= .1500E+02

UPSTREAM  
REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.1090E+03

DOWNSTREAM  
REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.9225E+02

M= 3 N= 1 OMEGA= .1500E+02

UPSTREAM  
REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.8632E+02

DOWNSTREAM  
REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.8503E+02

M= -3 N= 1 OMEGA= .1500E+02

UPSTREAM  
REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.1081E+03

DOWNSTREAM  
REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.8705E+02

M= 3 N= 2 OMEGA= .1500E+02

UPSTREAM  
REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.7849E+02

DOWNSTREAM  
REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.7829E+02

M= -3 N= 2 OMEGA= .1500E+02

UPSTREAM  
REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.9483E+02

DOWNSTREAM  
REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.9060E+02

TABLE 12. (Cont.)

ORIGINAL PAGE IS  
OF POOR QUALITY

M= 4 N= 1 OMEGA= .1500E+02

UPSTREAM  
REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.8833E+02

DOWNSTREAM  
REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.8132E+02

M= -4 N= 1 OMEGA= .1500E+02

UPSTREAM  
REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.1006E+03

DOWNSTREAM  
REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.8528E+02

M= 5 N= 1 OMEGA= .1500E+02

UPSTREAM  
REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.8864E+02

DOWNSTREAM  
REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.8005E+02

M= -5 N= 1 OMEGA= .1500E+02

UPSTREAM  
REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.9498E+02

DOWNSTREAM  
REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.8460E+02

M= 6 N= 1 OMEGA= .1500E+02

UPSTREAM  
REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.8764E+02

DOWNSTREAM  
REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.8147E+02

M= -6 N= 1 OMEGA= .1500E+02

UPSTREAM  
REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.8544E+02

DOWNSTREAM  
REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=-.8534E+02  
PROBLEM COMPLETED

RELATIVE POWER SPECTRAL DENSITY LEVEL UPSTREAM=-.7473E+02  
REL. POWER SPECTRAL DENSITY LEVEL DOWNSTREAM=-.7218E+02  
STOP

END OF EXECUTION  
CPU TIME: 1:59.28  
EXIT.

ELAPSED TIME: 4:6.50

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PROGRAM MAINV

This is the calling program  
controlling the computation of  
mean wake/stator interaction  
noise.

```
PROGRAM MAINV
  DIMENSION IDATA(10),FDATA(72),VGFORM(12,7),VELOCV(12,2)
  REAL XT, XA, XUV, LXZ
```

C  
C

```
2001 WRITE(5,2001)
  FORMAT(' NVANE=')
  READ(5,1001) NVANE
1001 FORMAT(20.0)
  WRITE(5,2101) NVANE
2101 FORMAT(' NVANE=',I3)
  WRITE(5,2002)
2002 FORMAT(' NBLADE=')
  READ(5,1001) NBLADE
  WRITE(5,2102) NBLADE
2102 FORMAT(' NBLADE=',I3)
  WRITE(5,2003)
2003 FORMAT(' HUB RADIUS DIVIDED BY DUCT RADIUS =')
  READ(5,1001) SIGMAR
  WRITE(5,2103) SIGMAR
2103 FORMAT(' SIGMAR=',E16.8)
  WRITE(5,2004)
2004 FORMAT(' VANE TIP CHORD DIVIDED BY DUCT RADIUS =')
  READ(5,1001) SIGMAC
  WRITE(5,2104) SIGMAC
2104 FORMAT(' SIGMAC=',E16.8)
  WRITE(5,2005)
2005 FORMAT(' LXZ =')
  READ(5,1001) LXZ
  WRITE(5,2105) LXZ
2105 FORMAT(' LXZ=',E16.8)
C
C
  WRITE(5,2006)
2006 FORMAT(' NDAT =')
  READ(5,1001) NDAT
  WRITE(5,2106) NDAT
2106 FORMAT(' NDAT=',I3)
  WRITE(5,2007)
2007 FORMAT(' VANE GEOMETRY MATRIX INPUT')
  WRITE(5,2008)
2008 FORMAT(' FEED MATRIX IN ONE ROW AT A TIME, FROM HUB TO TIP')
C
C
  DO 10 IPDM=1,NDAT
  WRITE(5,2009) IPDM
2009 FORMAT(' PDM=',I3,' R/RDUCT =')
  READ(5,1001) VGFORM(IROW,1)
  WRITE(5,2010)
2010 FORMAT(' C/CTIP =')
  READ(5,1001) VGFORM(IROW,2)
  WRITE(5,2011)
```

ORIGINAL PAGE IS  
OF POOR QUALITY

```

2011   FORMAT(' ALPHAS (DEGREES)=' )
      READ(5,1001) VGEOM(IFOR,3)
      VGEOM(IFOR,3)=VGEOM(IFOR,3)*.21*.533
      WRITE(5,2012)
2012   FORMAT(' VS/CTIP =' )
      READ(5,1001) VGEOM(IFOR,4)
      WRITE(5,2013)
2013   FORMAT(' VE/CTIP =' )
      READ(5,1001) VGEOM(IFOR,5)
      WRITE(5,2014)
2014   FORMAT(' VS/CTIP =' )
      READ(5,1001) VGEOM(IFOR,6)
      WRITE(5,2015)
2015   FORMAT(' VE/CTIP =' )
      READ(5,1001) VGEOM(IFOR,7)
10    CONTINUE
C
C
      WRITE(5,2020)
2020   FORMAT(' VANE GEOMETRY MATRIX IS')
      DO 11 IFOR=1,NDAT
      WRITE(5,2120) (VGEOM(IROW,ICOLN),ICOLN=1,7)
2120   FORMAT(' ',7E13.3)
11    CONTINUE
      WRITE(5,5000)
5000   FORMAT(' TYPE 1 TO INPUT ROTOR FLOW VELOCITY, 0 FOR FREE VORTEX')
      READ(5,1001) IVOR
      WRITE(5,5010) IVOR
5010   FORMAT(' IVOR=',I3)
      IF (IVOR.EQ.0) NVELO=C
      IF (IVOR.EQ.1) GO TO 4005
C
C
      WRITE(5,3000)
3000   FORMAT(' NUMBER OF RADII FOR SPECIFYING MEAN ROTOR FLOW=' )
      READ(5,1001) NVELO
      WRITE(5,3010) NVELO
3010   FORMAT(' NVELO=',I3)
      WRITE(5,3014)
3014   FORMAT(' INPUT MATRIX FOR MEAN ROTOR FLOW')
      WRITE(5,3016)
3016   FORMAT(' FEED MATRIX IN ONE ROW AT A TIME, FROM HUB TO TIP')
      DO 4010 IROW=1,NVELO
      WRITE(5,3008) IROW
3008   FORMAT(' ROW=',I3,' R/RDUCT=' )
      READ(5,1001) VELOCV(IROW,1)
      WRITE(5,3012)
3012   FORMAT(' MEAN CIRCUMFERENTIAL VELOCITY RATIO=' )
      READ(5,1001) VELOCV(IROW,2)
4010   CONTINUE
C

```

ORIGINAL PAGE IS  
OF POOR QUALITY





```

C
3814 WRITE(5,2014)
      FORMAT(' MAY FORTN FLOW VELOCITY MATRIX IS')
      DO 4022 IROW=1,NVFLD
3816 WRITE(5,2015) (VLLDGV(IROW,ICOLMN),ICOLMN=1,2)
4022 CONTINUE

```

```

C
C
4025 CONTINUE

```

ORIGINAL PAGE IS  
OF POOR QUALITY

```

C
2030 WRITE(5,2030)
      FORMAT(' MT =')
      READ(5,1071) MT
      WRITE(5,2137) MT
2137 FORMAT(' MT=',E16.8)
      WRITE(5,2031)
2031 FORMAT(' MA =')
      READ(5,1071) MA
      WRITE(5,2131) MA
2131 FORMAT(' MA=',F16.8)
      IF(IWORD.EQ.1) GO TO 6022
      WRITE(5,2032)
2032 FORMAT(' VYF4/VX4 & PRODUCT =')
      READ(5,1071) VUV
      WRITE(5,2132) VUV
2132 FORMAT(' VUV=',F16.8)
6022 CONTINUE

```

```

      IF(IWORD.EQ.1) VUV=2.
      WRITE(5,2033)
2033 FORMAT(' WAKE WIDTH =')
      READ(5,1071) WWIDTH
      WRITE(5,2133) WWIDTH
2133 FORMAT(' WWIDTH=',E16.8)
      WRITE(5,2034)
2034 FORMAT(' MAY VEL DEFICIT DIVIDED BY UBAF')
      READ(5,1071) VELDEF
      WRITE(5,2134) VELDEF
2134 FORMAT(' WELDEF=',E16.8)

```

```

C
C
2035 WRITE(5,2135)
      FORMAT(' NUMBER OF RADIAL STATIONS =')
      READ(5,1071) NRPAD
      WRITE(5,2135) NRPAD
2135 FORMAT(' NRPAD=',I4)
      WRITE(5,2736)
2036 FORMAT(' NUMBER OF CROSSWISE STATIONS =')
      READ(5,1071) NCHORD
      WRITE(5,2136) NCHORD

```



```
2136  FORMAT(' NCHORD=',I4)
      WRITE(5,2037)
2037  FORMAT(' ACCURACY OF BESSEL FN =')
      READ(5,1001) EB
      WRITE(5,2137) EB
2137  FORMAT(' EB=',E16.8)
      WRITE(5,2038)
2038  FORMAT(' ACCURACY OF CONVERGENCE TO ROOT XMN =')
      READ(5,1001) EC
      WRITE(5,2138) EC
2138  FORMAT(' EC=',E16.8)
```

ORIGINAL PAGE IS  
OF POOR QUALITY

C  
C

```
IDATA(1)=NVANE
IDATA(2)=NBLADE
IDATA(3)=NRAD
IDATA(4)=NCHORD
IDATA(5)=NDAT
IDATA(9)=IVOR
IDATA(10)=NVELO
```

C  
C

```
RDATA(1)=MT
RDATA(2)=MA
RDATA(3)=LX0
RDATA(4)=SIGMAC
RDATA(5)=SIGMAR
RDATA(6)=MUV
RDATA(7)=WWIDTH
RDATA(8)=VELDEF
RDATA(9)=EB
RDATA(10)=EC
```

C  
C

```
CALL SRCHV(IDATA,RDATA,VGEOM,VELOCV)
STOP
END
```

## PROGRAM SRCHV

Program determines which modes propagate for the mean wake/stator interaction and enables the noise calculation.

```
SUBROUTINE SPOHV(IDATA,RDATA,VGEOM,VELOCV)
  INTEGER S,P1
  DIMENSION IER(9),IDATA(12),M(12)
  DIMENSION RDATA(27),VGEOM(17,7),POWER(3,2),SPWR(2),RELEP(3,2)
  DIMENSION VELOCV(15,2)
  REAL VT,VA
```

```
C
C      DATA((POWER(I,J),I=1,3),J=1,2)/6*8.8/
```

```
C
C      S=4
10      S=S-1
C      IF(S.LE.2) GO TO 9888
```

```
C
C      WRITE(5,2007) S
2007      FORMAT('S =',I2)
```

ORIGINAL PAGE IS  
OF POOR QUALITY

```
C
C      NVANE=IDATA(1)
C      NBLADE=IDATA(2)
C      VT=PDATA(1)
C      VA=PDATA(2)
C      SIGMAF=PDATA(5)
C      SF=PDATA(9)
C      SC=PDATA(10)
```

```
C
C      XVAX=S*VBLADE*VT/(1.-VA**2)**.5
```

```
C
C      WRITE(5,2001) XVAX
2001      FORMAT('XVAX(MAX) FOR PROPAGATION =',E16.8)
```

```
C
C      P1=(S*NBLADE)/NVANE
C      MTEST=2*S*NBLADE-(2*P1+1)*NVANE
C      IF(MTEST.GT.0) P1=P1+1
```

```
C
C      J=1
C      M(1)=S*NBLADE-P1*NVANE
```

```
C
C      N=1
15      N=N+1
20
```

```
C
C      MABS=M(J)
C      IF(M(J).LT.0) MABS=-MABS
```

```
C
```

C

CALL ANPT (MABS,N,SIGMAP,BE,EC,XMN,IEB,IEC)

C

C

IF(XMN.GE.XMAX) GO TO 6003

C

C

ORIGINAL PAGE IS  
OF POOR QUALITY

WRITE(5,3000)

3000

FORMAT('2MODE DATA')

WRITE(5,3001) S,'(J)',N,XMN

3001

FORMAT('S =',I3,' N =',I3,' XMN =',E16.8)

IF(XMN.EQ.0.) GO TO 1000

COEFFR=XMAX/XMN

WRITE(5,4000) COEFFR

4000

FORMAT(' CUTOFF RATIO FOR MODE=',E12.4)

GO TO 1005

1005

CONTINUE

WRITE(5,4005)

4005

FORMAT(' PLANE WAVE MODE: CUTOFF RATIO IS + INFINITE')

1005

CONTINUE

WRITE(5,3002) IEB

3002

FORMAT(' SUM OF BESSEL FUNCTION ERROR CODES =',I3)

WRITE(5,3003) IEC

3003

FORMAT(' ERROR CODE FOR CONVERGENCE TO ROOT XMN =',I3)

C

C

CALL EIGEN (MABS,SIGMAR,XMN,AMN,BMN,BE,IER)

C

C

WRITE(5,3004) AMN,BMN

3004

FORMAT(' AMN =',E16.8,' BMN =',E16.8)

WRITE(5,3005) IER

3005

FORMAT(' ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC =',I3)

C

C

RDATA(11)=XMN

RDATA(12)=AMN

RDATA(13)=BMN

IDATA(6)=N(J)

IDATA(7)=N

IDATA(8)=S

C

C

CALL FLEW(IDATA,RDATA,VGEOM,VELOCV,SPWR)

II=IABS(IDATA(8))

POWER(II,1)=POWER(II,1)+SPWR(1)

POWER(II,2)=POWER(II,2)+SPWR(2)

C

C

IDATA(6)=-IDATA(6)

IDATA(8)=-IDATA(8)

C  
C

```

8300 WRITE(5,8300) IDATA(6),IDATA(7),IDATA(8)
      FORMAT('Mx=',I5,' N=',I5,' S=',I5)
      RFLUP=17.*ALOG10(SPWR(1))
8400 WRITE(5,8400)
      FORMAT('UPSTREAM ')
      WRITE(5,8600) RFLUP
8600 FORMAT(' RELATIVE SOUND POWER LEVEL FOR MODE(02)=' ,F16.4)
      RFLDN=14.*ALOG10(SPWR(2))
8200 WRITE(5,8200)
      FORMAT('DOWNSTREAM ')
      WRITE(5,8600) RFLDN
      II=IABS(IDATA(8))
      POWER(II,1)=POWER(II,1)+SPWR(1)
      POWER(II,2)=POWER(II,2)+SPWR(2)

```

C  
C

```

      IDATA(6)=-IDATA(6)
      IDATA(8)=-IDATA(8)

```

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C  
C

```

      GO TO 2

```

C  
C

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C  
C

C  
C

```

6100 IF(N.EQ.1) GO TO 7000

```

```

      NMAX=N-1
      WRITE(5,6100) NMAX
6200 FORMAT('LARGEST PROPAGATING N FOR THIS M =' ,I3)

```

```

      IF(J.EQ.1) GO TO 6100

```

```

      IF(V(1).EQ.7) GO TO 6200

```

```

      IF(V(J-1).LT.8) W(J+1)=V(J-1)-NVAVE

```

```

      IF(V(J-1).GT.8) W(J+1)=V(J-1)+NVAVE
      J=J+1
      GO TO 1

```

```
6100 CONTINUE
      IF(M(1).LT.Z) M(2)=M(1)+NVAVE
      IF(M(1).GT.Z) M(2)=M(1)-NVAVE
C
C
C                                     ORIGINAL PAGE IS
C                                     OF POOR QUALITY
      J=2
      GO TO 15
C
C
6200 V(J+1)=M(J)+NVAVE
      J=J+1
      GO TO 15
C
C
7000 IF(J.EQ.1) GO TO 3000
C
C
7001 WRITE(5,7001)
      FORMAT(' NO MORE PROPAGATING MODES FOR THIS VALUE OF S')
      GO TO 10
8000 CONTINUE
      WRITE(5,8001)
8001 FORMAT(' NO PROPAGATING MODES FOR THIS VALUE OF S')
      GO TO 10
C
C
9000 CONTINUE
      WRITE(5,9001)
8001 FORMAT(' PROBLEM COMPLETED')
      DO 550 II=1,3
        DO 550 JJ=1,2
          IF(POWER(II,JJ).EQ.Z) GO TO 5215
          RELPR(II,JJ)=17.*ALOG10(POWER(II,JJ))
          GO TO 550
5215 RELPR(II,JJ)=1.F+35
550 CONTINUE
      DO 600 II=1,3
        IF(RELPR(II,1).EQ.1.E+35) GO TO 5315
        WRITE(5,610) II,RELPR(II,1)
        GO TO 600
5315 WRITE(5,5610) II
5610 FORMAT(' S=',I2,' HARMONIC IS UNEXCITED')
600 CONTINUE
610 FORMAT(' RELATIVE POWER LEVEL UPSTREAM S=',I2,5X,E16.4)
      DO 620 II=1,3
        IF(RELPR(II,2).EQ.1.E+35) GO TO 5415
        WRITE(5,600) II,RELPR(II,2)
        GO TO 620
5415 WRITE(5,5610) II
620 CONTINUE
630 FORMAT(' RELATIVE POWER LEVEL DOWNSTREAM S=',I2,5X,E16.4)
      RETURN
      END
```

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### PROGRAM FILLOV

Program computes the noise  
generated by the mean wake/  
stator interaction in a sub-  
sonic turbofan.



```

SUBROUTINE FILLOV(IDATA,RDATA,VGSDM,VELOCV,SPWR)
DIMENSION VGSDM(14,7),RDATA(27),IDATA(12),XX(6),IERPSI(2),SPWR(2)
DIMENSION PHASE(42),VELOCV(14,2)
DIMENSION PSISTD(2)
INTEGER SS,SB
REAL KX,K,KVNS,AR,AT,VA,MUV,NVA,LYZ
REAL MTHETA,MTHRJB
COMPLEX I,AF,DELTA(142),PMNS,FMNS,AMNS,AMNS
COMPLEX FVN(42)
COMPLEX QNSTA(52,52)
COMPLEX CASCT(22,32)
DATA ISS/3/
I=(0.,1.)
PI=3.1415926

```

C  
C

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OF POOR QUALITY

```

NVA=IDATA(1)
NPLAGE=IDATA(2)
NPA=IDATA(3)
NCHORD=IDATA(4)
ADAT=IDATA(5)
MV=IDATA(6)
AV=IDATA(7)
SS=IDATA(8)
IVP=IDATA(9)
NVELO=IDATA(10)

```

C  
C

8306  
7224

```

NPI(5,6,7) MV,AV,SS
FORMAT('M'=' ',I5,' ' N=' ',I5,' ' S=' ',I5)
FORMAT(' NPA=' ',I3,' ' NCHORD=' ',I3)

```

C  
C

```

MT=RDAT(1)
M2=RDAT(2)
LYE=RDAT(3)
SIGMAC=RDAT(4)
SIGMAR=RDAT(5)
MUV=RDAT(6)
NWIDTH=RDAT(7)
VELOCV=RDAT(2)
ER=RDAT(9)
EC=RDAT(12)
XUN=RDAT(11)
AMN=RDAT(12)
BMN=RDAT(13)

```

C  
C

```

SP=SS*VELAD

```

C

```
C
      BPT*SQ=1.-V1**2
      K'NS=((((SP*MT)**2-2*BTASQ*XW**2)**.5)*ABS(1.*SS))/(1.*SS)
7016      FORMAT(' K'NS=',F10.4)
```

```
C
      C
      WETA=EXP(14.738879*W*IDTH**2)
      SU=2.
      ERROR=.1E-5
      INDEX=0
100      INDEX=INDEX+1
      DSUM=1./(W*IDTH**2*(INDEX**2))
      SUM=SUM+DSUM
      IF(DSUM.LT.ERROR) GO TO 110
      GO TO 100
```

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```
C
      C
110      XSIGN=1.
111      GVNS=(SP*MT+XSIGN*X'NS)/WETA*SQ
      PMS=(2.,P.)
      DELTA=(1.-SIGNAR)/(N*AD-1)
      IF=0
      IDAT=0
      IDOT=2
```

```
C
      C
      S*TR=-1.
      DO 200 YR=1,N*AD
```

```
C
      C
      R=SIGNAR*(IF-1.)*(1.-SIGNAR)/(N*AD-1.)
      IF(P.LE.VGROW(IDAT,1)) GO TO 221
      IDAT=IDAT+1
      IF(IDAT.GT.NDAT) IDAT=NDAT
201      DFLTA=(P-VGROW(IDAT,1))/(VGROW(IDAT,1)-VGROW(IDAT-1,1))
      DO 210 IX=2,7
210      XY(IX-1)=VGROW(IDAT,IX)+DFLTA*(VGROW(IDAT,IX)-VGROW(IDAT-1,IX))
```

```
C
      C
      P=XY(1)/2.
      ALPHAS=XX(2)
      YS=XX(3)
      YR=XX(4)
      XS=XX(5)
      XP=XX(5)
7011      FORMAT(' B,ALPHAS,YS,YR,YS,XP OF R IS')
7012      FORMAT(6F10.4)
```

```
C
      C
      IF(TVOR.EQ.7) GO TO 4127
      C
```

C  
C INTERPOLATE TO GET MEAN CIRCUMFERENTIAL WACH NUMBERS AT THIS #  
C

IF(F.LS.VELOCV(IDOT,1)) GO TO 4021

IDOT=IDOT+1

IF(IDOT.GT.NVFLD) IDOT=NVFLD

4021

DELTA=(P-VELOCV(IDOT,1))/(VELOCV(IDOT,1)-VELOCV(IDOT-1,1))

XVEL=VELOCV(IDOT,2)+DELTA\*(VELOCV(IDOT,2)-VELOCV(IDOT-1,2))

MTHETA=XVEL\*\*2

C  
C  
C  
C

4025

FORMAT(' R=',E11.4,' MTHETA=',E11.4)

C  
C

4028

IF(IR.EQ.1) MTHETA=MTHETA

CONTINUE

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C  
C

MY=DELTA-M\*WV/R

IF(IWOR.EQ.1) MY=MTHETA-MTHETA

ACL=ATAN2(MY,1)

C  
C

COSAS=COS(ALPHAS)

SINAS=SIN(ALPHAS)

C  
C

PART1=LX\*\*2\*WV\*(1./SIGMA\*\*2-1./R\*\*2)

IF(IWOR.EQ.1) PART1=LX\*\*2\*(MTHETA/M/SGR-MTHETA/VA/R)

PART2=SIGMAC\*(YS+YF)/R

PART3=SIGMAC\*(XS+XR)\*(SGR/VA-MV/R\*\*2)

IF(IWOR.EQ.1) PART3=SIGMAC\*(XS+XR)\*(M/VA-MTHETA/VA/R)

C  
C

PHASE1=90\*(PART1-PART2-PART3)

C  
C

PHASE2=90\*SIGMAC\*(SINAS+COSAS\*MY/M)/R

C  
C

W=(VELDFP/SIGMA)\*SIN(ACL+ALPHAS)\*WBETA\*\*(-SS\*\*2)

WV=V\*CEVP(-I\*(PHASE1+PHASE2))

C  
C

KV=-PHASE2

C  
C

MR=VA\*(1.+(WV/R)\*\*2)\*\*.5

IF(IWOR.EQ.1) MR=(M\*\*2+MTHETA\*\*2)\*\*.5

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$$K=SP*VT*B*SIGMAC/(1.-VR**2)$$

$$GAMMA=(2.*SP*PI/NVAND)*(1.+VT*VR*K*SINAS/(1.-VR**2))$$

$$H1=-2.*PI*K*SINAS/(NVAND*B*SIGMAC)$$

$$H2=2.*PI*K*COSAS/(NVAND*B*SIGMAC)$$

SKIP CALL AND STOP OF PRES FOR DOWNSTREAM  
IF(YSTGR.FO.-1.) GO TO 308

SKIP PRES CALL AFTER NRD CALLS FOR THIS VALUE OF S(=SS)  
IF(SS.EQ.ISS) GO TO 308

307 FORMAT('INPUT TO SUBROUTINE PRES')

307 FORMAT(' W4=',E16.4)

304 FORMAT(' WY=',E16.4, ' W=',E16.4, ' GAMMA=',E16.4)

WRITE(21,305) W4,W1,W2,NCHORD

306 FORMAT(' W4=',E16.4, ' W1=',E16.4, ' W2=',E16.4, ' NCRD=',I3)

CALL PRES((1.,W.),WY,W,GAMMA,W4,W1,W2,NCHORD,DELTA,IERP)

IF(YR.EQ.NRD) ISS=SS  
DO 310 ICK=1,NCHORD  
CASCET(IE,ICK)=DELTA(ICK)  
CONTINUE

312 WRITE(5,7500) IERR

7500 FORMAT(' ERROR CODE FROM INVERSION ROUTINE=',I3)

7025 FORMAT(' OUTPUT FROM PRES:(DELTA(I2),I2=1,NCHORD)  
(DELTA(I1),I2=1,NCHORD)

308 CONTINUE  
Z'UD=SIGMAC\*B\*(GAMMA\*COSAS-WY\*SINAS/P)

Q'NS=CASCET(IE,NCHORD)/Z.  
Q'NST'(IE,NCHORD)=Q'NS  
S'IC=1.

```

C
NFIN=NCHORD-1
DO 227 IZ=1,NFIN
  WHIC=1.+SWTC/R.
  SWTC=-SWTC
  THETA=(I2*PI)/NCHORD
  QUNSTV(IF,IZ)=CISSET(IM,IZ)*CEXP(I*ZMOL*(1.+COS(THETA)))
228 QUNSS=QUNSTV+WHIC*CAASCT(IF,IZ)*CEXP(I*ZMOL*(1.+COS(THETA)))
  QUNSS=QUNSS*(1.+(I2/R)**2)*PI/NCHORD

```

```

7022  FORMAT(' IF=',IZ,' QUNSS(P)=' ,2E12.4,' WH(R)=' ,2E12.4)
      QUNSS=QUNSS*V

```

C  
C  
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C  
C

```

SKIP PHOD CALL AND STORE FOR DOWSTREAM
IF(XSIGN.DQ.-1.) GO TO 7021

```

```

ARG=XAN*W

```

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```

CALL PHOD (M,ARG,MUN,PMN,PSI,FB,IEP,PSI)
PSISTO(IE)=PSI
7020  FORMAT(' PSI(?)=' ,F16.5)

```

C  
C  
C  
C

```

IEP=IEP+IE*PSI(1)+IE*PSI(2)

```

```

7021  CONTINUE
      CR=QUNSS*SIAS+4*CORAS/R
      CP=(M*YS/R-QUNSS*XS)*SIGNAC
      PHAS=(QUNSS*PSISTO(IE)/KUNSS)*CA
      PHA(IF)=PHAS
      PHASE(IF)=CP-PHASE1-PHASE2

```

200  
2001  
2004

```

CONTINUE
DO 2004 J=1,NFAD
  FORMAT(I4,3E14.5)
CONTINUE
PHAS=?.
DO 277 N=1,NRAD-1
  GP=.5*(PHASE(N)+PHASE(N+1))
  X=.5*(PHASE(N+1)-PHASE(N))
  IF(ABS(X).LT.F.001) GO TO 268
  W1=SIN(X)/(2.*X)
  W2=(SIN(X)/X-COS(X))/(2.*X)
  GO TO 269

```

268  
269

```

  W3=.5*(1.-X**2/6.)
  W4=W3*(1.-X**2/12.)/6.
269  CONTINUE
      PHAS=PHAS+DELTA*CEXP(I*GP)*((W3-I*W1)*PHAS(N)+(W3+I*W1)*PHAS(N+1))

```

```

270 CONTINUE
   AMNS=-PMNS*WAVE*SIGMAC/(PI*(1.-SIGMA**2))
C
   POWNUM=2.*AMNS*SL*AT*(CABS(PMNS)*PETA*WAVE*SIGMAC)**2
   POWDEN=PI*(1.-SIGMA**2)*((SE*MT)+XSIGMA*MA*PMNS)**2
   RELPWR=POWNUM/POWDEN
   RELPEL=12.*ALOG10(RELPWR)

```

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```

C
CC
C
   IF(XSIGV.LT.E.) GO TO 9200

C
C
   WRITE(5,8200)
   FORMAT('UPSTREAM')
   WRITE(5,8101) GUNS
   FORMAT(' GAMMA W,N,SE =',E16.8)
   WRITE(5,8122) AMNS
   FORMAT(' MODE AMPLITUDE =',2E16.8)
   WRITE(5,8522) IER
   FORMAT(' SUM OF ALL ERRORS IN PSI CALCULATIONS =',I5)
   WRITE (5,8622) RELPEL
   FORMAT(' RELATIVE SOUND POWER LEVEL FOR MODE(OB)=' ,E16.4)
   DO 7000 IF=1,NRAD
      P=SIGMA*(IF-1.)*(1.-SIGMA)/(NRAD-1.)
   7002   FORMAT(5X,E12.4)
   7006   CONTINUE
   7200   FORMAT(' END OF UPSTREAM INTEGRATION')
      YSIGV=-1.
      SPWR(1)=RELPWR
      GO TO 111
   9000   WRITE(5,8200)
   8200   FORMAT('DOWNSTREAM')
   WRITE(5,8201) GUNS
   FORMAT(' GAMMA W,N,SE =',E16.8)
   WRITE(5,8222) AMNS
   FORMAT(' MODE AMPLITUDE =',2E16.8)
   WRITE(5,8422) IER
   FORMAT(' SUM OF ALL ERRORS IN PSI CALCULATIONS =',I5)
   WRITE(5,8622) RELPEL
   SPWR(2)=RELPWR
   7202   FORMAT(' END OF DOWNSTREAM INTEGRATION')
   RETURN
   END

```

## PROGRAM MAINTI

This is a calling program to control the computation of pressure data for the inlet turbulence case.

```

      PROGRAM MAINTI
      DIMENSION IDATA(10),RDATA(20),VGEOM(10,7)
      REAL MT,MA
      INTEGER PSTART,PEND,P,PRANGE,PSTEP
      DATA (IDATA(J),J=1,10)/10*0/
      DATA (RDATA(J),J=1,20)/20*.0.0/

```

ROTOR INFLOW TURBULENCE -- MATRIX STORAGE PROGRAM

THIS PROGRAM GRUPO CALCULATES AND STORES VECTORS OF THE COMPLEX PRESSURE DISTRIBUTION ACROSS THE ROTOR BLADE.

DATA REQUIRED TO EXECUTE THIS ROUTINE INCLUDE:

1. BLADE GEOMETRY
2. ROTOR OPERATING SPEEDS
3. NUMBER OF RADIAL AND CHORDWISE POSITIONS AT WHICH THE PRESSURES ARE CALCULATED
4. FREQUENCY RANGE OF INTEREST (EXPRESSED IN TERMS OF HARMONIC ORDER OF SHAFT ROTATION).

THE RANGE OF CIRCUMFERENTIAL MODE NUMBER M IS 0 TO NBLADE-1.

NCHORD MUST BE NO GREATER THAN 20.

```

1001  FORMAT(G20.8)
      WRITE(5,2002)
2002  FORMAT(' NBLADE=')
      READ(5,1001) NBLADE
      WRITE(5,2102) NBLADE
2102  FORMAT(' NBLADE=',I3)
      WRITE(5,2003)
2003  FORMAT(' HUB RADIUS DIVIDED BY DUCT RADIUS =')
      READ(5,1001) SIGMAR
      WRITE(5,2103) SIGMAR
2103  FORMAT(' SIGMAR=',E16.8)
      WRITE(5,2004)
2004  FORMAT(' BLADE TIP CHJRD DIVIDED BY DUCT RADIUS=')
      READ(5,1001) SIGMAC
      WRITE(5,2104) SIGMAC
2104  FORMAT(' SIGMAC=',E16.8)
      WRITE(5,2006)
2006  FORMAT(' NDAT =')
      READ(5,1001) NDAT
      WRITE(5,2106) NDAT
2106  FORMAT(' NDAT=',I3)
      WRITE(5,2007)

```

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```
2007 FORMAT(' BLADE GEOMETRY MATRIX INPUT')
WRITE(5,2008)
2008 FORMAT(' FEED MATRIX IN ONE ROW AT A TIME, FROM HUB TO TIP')
```

C  
C

```
DO 10 IROW=1,NDAT
WRITE(5,2009) IROW
2009 FORMAT(' ROW=',I3,' R/RDUCT =')
READ(5,1001) VGEOM(IRJW,1)
WRITE(5,2010)
2010 FORMAT(' C/CTIP =')
READ(5,1001) VGEOM(IRJW,2)
WRITE(5,2011)
2011 FORMAT(' CHI (DEGREES)=')
READ(5,1001) VGEOM(IRJW,3)
VGEOM(IROW,3)=VGEOM(IRJW,3)*.0174533
10 CONTINUE
```

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10  
C  
C

```
WRITE(5,2020)
2020 FORMAT(' BLADE GEOMETRY MATRIX IS')
DO 11 IROW=1,NDAT
WRITE(5,2120) (VGEOM(IROW,ICOLMN),ICOLMN=1,3)
2120 FORMAT(' ',7E10.3)
11 CONTINUE
```

C  
C

```
WRITE(5,2030)
2030 FORMAT(' MT =')
READ(5,1001) MT
WRITE(5,2130) MT
2130 FORMAT(' MT=',E16.8)
WRITE(5,2031)
2031 FORMAT(' MA =')
READ(5,1001) MA
WRITE(5,2131) MA
2131 FORMAT(' MA =',E16.8)
```

C  
C

```
WRITE(5,2035)
2035 FORMAT(' NUMBER OF RADIAL STATIONS =')
READ(5,1001) NRAD
WRITE(5,2135) NRAD
2135 FORMAT(' NRAD=',I4)
WRITE(5,2036)
2036 FORMAT(' NUMBER OF CHORDWISE STATIONS =')
READ(5,1001) NCHORD
WRITE(5,2136) NCHORD
2136 FORMAT(' NCHORD=',I4)
```

C

```
C
WRITE(5,100)
100 FORMAT(' START FREQUENCY(HARMONIC NO. OF SHAFT)=' )
READ(5,1001) PSTART
WRITE(5,110) PSTART
110 FORMAT(' PSTART=',I4)
WRITE(5,120)
120 FORMAT(' END FREQUENCY(HARMONIC NO. OF SHAFT)=' )
READ(5,1001) PEND
WRITE(5,130) PEND
130 FORMAT(' P END=',I4)
```

```
C
WRITE(5,140)
140 FORMAT(' FREQUENCY STEP SIZE (HARMONIC ORDERS)=' )
READ(5,1001) PSTEP
WRITE(5,150) PSTEP
150 FORMAT(' PSTEP=',I4)
PRANGE=(PEND-PSTART)/PSTEP+1
IDATA(2)=NBLADE
IDATA(3)=NRAD
IDATA(4)=NCHORD
IDATA(5)=NDAT
IDATA(6)=PSTART
IDATA(7)=PEND
IDATA(8)=PSTEP
```

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```
C
RDATA(1)=MT
RDATA(2)=MA
KDATA(4)=SIGMAC
RDATA(5)=SIGNAR
```

```
C
CALL ROTOKS(IDATA,RDATA,VGEOM)
STOP
END
```

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### PROGRAM ROTORS

Program calculates and stores  
the pressures generated on a  
turbofan rotor by inlet tur-  
bulence.

SUBROUTINE ROTORS(IUATA, RDATA, VGEOM)

C  
C  
C  
C  
C  
C  
C  
C

ADJUSTABLE DIMENSION STATEMENTS USED TO MINIMIZE STORAGE  
REQUIREMENTS OF MATRIX CASSET

DIMENSION OF DELTAP=20  
DIMENSION OF CASSET=(NCHORD, NRAU, NBLADE, PRANGE)

NOTE NCHORD MUST BE NO GREATER THAN 20  
DIMENSION DELTAP(20)  
DIMENSION VGEOM(10,7), RDATA(20), IUATA(10), AA(6)  
DIMENSION CASSET(0,0,10,0)  
DIMENSION A(72)  
REAL KD, MP, MA, MT  
COMPLEX L, DELTAP, CASSET  
INTEGER PSTART, PENU, P, PRANGE, PDISP  
L=(0.,1.)  
PI=3.1415926

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OF POOR QUALITY

NBLADE=IUATA(2)  
NRAU=IUATA(3)  
NCHORD=IUATA(4)  
NRA1=IUATA(5)  
PSTART=IUATA(6)  
PENU=IUATA(7)  
PSTEP=IUATA(8)

C  
C

M1=RDATA(1)  
M2=RDATA(2)  
SIGNAC=RDATA(4)  
SIGNAR=RDATA(5)

C  
C  
C  
C

INITIALIZE IUAT FOR GEOMETRIC DATA

IUAT=2

WRITE(5,100)  
100 FORMAT(' ENTER TITLE FOR DATA FILE(MAX 72 CHARACTERS)')  
READ(5,1000) A  
1003 FORMAT(72A1)

C

START LOOPS TO CALL CASSET=BEGIN WITH LOOP ON RADIAL  
POSITION TO MINIMIZE INTERPOLATION.

C  
C  
C

DO 330 IK=1, NRAU

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```

C
R=SIGMAR*(IR-1.)/(1.-SIGMAR)/(NRAD-1.)
IF(R.LE.VGEUM(IDAT,1)) GO TO 201
IDAT=IDAT+1
IF(IDAT.GT.NDAT) IDAT=NDAT
201 DELTA=(K-VGEUM(IDAT,1))/(VGEUM(IDAT,1)-VGEUM(IDAT-1,1))
DO 210 IA=2,3
210 XX(IA-1)=VGEUM(IDAT,IA)+DELTA*(VGEUM(IDAT,IA)-VGEUM(IDAT-1,IA))

```

C  
C

```

O=XX(1)/2.
CHI=XX(2)
WRITE(21,7010) B,CHI,R
7010 FORMAT(' B=',E10.4,' CHI=',E10.4,' R=',E10.4)

```

C  
C  
C  
C

```

COSCHI=COS(CHI)
SINCHI=SIN(CHI)

```

C  
C  
C

BEGIN LOOPS ON MODE NUMBER M AND FREQUENCY COUNTER P

```

DO 300 M=1,NBLAUE
MM=M*COUNT-1

```

C  
C

IF IS STORAGE COUNTER FOR PARAMETER P IN MATRIX CASSET  
IP=?

C  
C

```

DO 310 P=PSTART,PEND,PSTEP
IP=IP+1

```

C  
C  
C

```

UNSUBC=PI**2*(UNAC**2*(P-MM)

```

C  
C  
C

```

MR=(MA**2+(MT*R)**2)**-.5

```

C  
C

```

AB=PI/AR**2*(UNAC**2*(P-MM)
SIGMA=-2.*PI**2*MM/NBLAUE

```

C  
C

```

B=2.*PI**2*R/NBLAUE/SIGMA/B

```

C  
C  
C

C

```

WRITE(21,300)
300  FORMAT('INPUT TO SUBROUTINE CASC')
WRITE(21,302) OMEGBC
302  FORMAT(' OMEGBC=',E12.4)
WRITE(21,304) MK,KB,SIGMA
304  FORMAT(' MK=',E12.4, ' KB=',E12.4, ' SIGMA=',E12.4)
WRITE(21,306) n,CHI,NCHORD
306  FORMAT(' n=',E12.4, ' CHI=',E12.4, ' NCHORD=',I3)

```

C  
C  
C  
C  
C  
C

```
CALL CASC(OMEGBC,MK,KB,SIGMA,H,CHI,NCHORD,DELTAP,IERP)
```

C  
C  
C  
C  
C  
C  
C  
C  
C  
C  
C

STORE RESULTS OF CASC IN STORAGE MATRIX FOR DISK FILE.  
 MATRIX POSITION DESCRIPTORS ARE (IN ORDER OF APPEARANCE):

1. CIRCUMFERENTIAL POSITION (TRAILING TO LEADING EDGES)
2. RADIAL POSITION (INNER RADIUS TO OUTER RADIUS)
3. CIRCUMFERENTIAL MODE NUMBER + 1 (M+1)
4. ORDER OF FREQUENCY COMPUTATIONS (FIRST TO LAST)

WITH: IP=1 FOR PSTART  
 IP=PRANGE FOR PEND

```

DO J=1,ICA=1,NCHORD
CASCSET(ICA,IK,NCOUNT,IP)=DELTAP(ICA)
310  CONTINUE
WRITE(5,7503) IERP
7503  FORMAT(' ERROR CODE FROM INVERSION ROUTINE=',I3)
WRITE(21,7025)
7025  FORMAT(' OUTPUT FROM CASC:(DELTAP(IQ),IQ=1,NCHORD)')
WRITE(21,7012) (DELTAP(IQ),IQ=1,NCHORD)
7002  FORMAT(5X,0E12.4)

```

C  
C  
C  
C  
C

```
320  CONTINUE
```

C  
C  
C  
C  
C

STORE MATRIX OF PRESSURE VALUES ON THE DISK FOR LATER  
 PROCESSING BY OTHER PROGRAMS.

```

CALL OFILE(23,'R0TU')
WRITE (23) A
WRITE (23) IDATA
WRITE (23) RDATA
WRITE (23) VGEOM
WRITE (23) CASCSET

```

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C

C  
C  
C  
ENDFILE 23

STOP  
END

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## PROGRAM INSRCH

Program determines which modes propagate for the case of inlet turbulence and controls the noise computation.



PROGRAM INSRCH  
DIMENSION CASCET(8,5,15,5)  
DIMENSION IER(8),IDATA(10)  
DIMENSION RDATA(20),VGEOM(10,7),POWER(2),SPWR(2),RELPR(2)  
DIMENSION NPCJN(4)  
DIMENSION A(72)  
INTEGER PRANGE,PEND,PSTART,PSTEP  
COMPLEX CASCET  
REAL MT,MA

DATA(POWER(J),J=1,2)/2\*0.0/

CALLING PROGRAM FOR INTUR3 TO SEARCH OUT AND CALCULATE  
ALL PROPAGATING MODES AT A GIVEN POSITIVE FREQUENCY.

OPEN FILE "ROTO" AND READ INPUT ARRAYS  
INCLUDING MAIN STORAGE MATRIX "CASCET".

\*\*\*\*\*NOTE THAT "ROTO" IS A SEQUENTIAL UNFORMATTED BINARY FILE--

ORDER OF STORAGE=A,IDATA,RDATA,VGEOM,CASCET

\*\*\*\*\*

CALL IFILE(23,"ROTO")  
READ (23) A  
READ (23) IDATA  
READ (23) RDATA  
READ (23) VGEOM  
READ (23) CASCET  
ENDFILE 23

WRITE(5,5)  
FORMAT(' USER-ASSIGNED TITLE OF DATA SET FROM FILE "ROTO" IS')  
WRITE(5,6) A  
FORMAT(' ',72A1)  
PSTART=IDATA(5)  
PEND=IDATA(7)  
PSTEP=IDATA(8)  
PRANGE=(PEND-PSTART)/PSTEP+1  
NPCON(1)=PSTART  
NPCON(2)=PEND  
NPCON(3)=PSTEP  
NPCON(4)=PRANGE

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C <MTHEOBALD>INSRCH.FOR;18 Mon 29-Sep-80 10:11AM PAGE 1:1

C ENTER NOISE FREQUENCY OF INTEREST(MUST BE POSITIVE FREQUENCY)

C  
1001 FORMAT(G20.0)  
WRITE(5,110)  
110 FORMAT(' NOISE FREQUENCY/SHAFT FREQUENCY=')  
READ(5,1001) OMEGA  
RDATA(8)=OMEGA  
115 FORMAT(' OMEGA=',E10.4)  
WRITE(5,115) RDATA(8)

C  
C SELECT NO. OF RADIAL POSITIONS TO INTERPOLATE PRESSURES  
C (ASSUMED THAT NRADNU.GE.NRAD)

C \*\*\*\*\*NOTE: NRADNU MUST BE .LE.30 UNLESS DIMENSION STATEMENTS IN  
C "INTURB" ARE TO BE MODIFIED

C \*\*\*\*\*  
WRITE(5,120)  
120 FORMAT(' NUMBER OF RADIAL POSITIONS FOR ACOUSTIC COMP. =')  
READ(5,1001) NRADNU  
IDATA(1)=NRADNU  
WRITE(5,130) IDATA(1)  
130 FORMAT(' NRADNU=',I4)  
WRITE(5,2037)  
2037 FORMAT(' ACCURACY OF BESSL FNS =')  
READ(5,1001) EB  
WRITE(5,2137) EB  
2137 FORMAT(' EB=',E10.4)  
WRITE(5,2038)  
2038 FORMAT(' ACCURACY OF CONVERGENCE TO ROOT XMN =')  
READ(5,1001) EC  
WRITE(5,2138) EC  
2138 FORMAT(' EC=',E10.4)  
RDATA(9)=EB  
RDATA(10)=EC  
MT=RDATA(1)  
MA=RDATA(2)  
SIGMAR=RDATA(5)

C  
C  
C  
C  
C  
C  
C  
C  
C  
C  
XMAX=OMEGA\*MT/(1.-MA\*\*2)\*\*.5

2001 WRITE(5,2001) XMAX  
FORMAT(' XMN(MAX) FOR PROPAGATION =',E16.0)

C  
C START WITH PLANE WAVE MODES (0,1). COUNT UP IN N, THEN M  
C UNTIL ALL POSSIBLE HIGHER MODES ARE CUT OFF.

J=1  
N=0

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RESTART N COUNT HERE FOR NEW M

N=0

INCREMENT N

N=N+1

MABS=IABS(M)

CALL ANRT (MABS,N,SIGMAR,EB,EC,XMN,IEB,IEC)

IF MODE IS CUT OFF, GO TO 6000

IF(XMN.GE.XMAX) GO TO 6000

WRITE(5,3000)  
3000 FORMAT('MODE DATA')  
WRITE(5,3001) OMEGA,M,N,XMN  
3001 FORMAT('OMEGA=',E10.4,' M=',I3,' N=',I3,' XMN=',E10.4)  
IF(XMN.EQ.0.) GO TO 1000  
COFFRA=XMAX/XMN  
WRITE(5,4000) COFFRA  
4000 FORMAT('CUTOFF RATIO FOR MODE=',E10.4)  
GO TO 1005  
1000 CONTINUE  
WRITE(5,4005)  
4005 FORMAT(' PLANE WAVE MODE: CUTOFF RATIO IS + INFINITE')  
1005 CONTINUE  
WRITE(5,3002) IEB  
3002 FORMAT(' SUM OF BESSEL FUNCTION ERROR CODES =',I3)  
WRITE(5,3003) IEC  
3003 FORMAT(' ERROR CODE FOR CONVERGENCE TO ROOT XMN =',I3)

NORMALIZE MODE AMPLITUDE

CALL EIGEN (MABS,SIGMAR,XMN,AMN,BMN,EB,IER)

WRITE(5,3004) AMN,BMN

```
3004 FORMAT(' AMN =',E16.8,' BMN =',E16.8)
WRITE(5,3005) IER
3005 FORMAT(' ERROR CODE FOR BESSEL PMS IN AMN AND BMN CALC =',I2)
```

C  
C

```
RDATA(11)=XMN
RDATA(12)=AMN
RDATA(13)=BMN
IDATA(6)=M
IDATA(7)=N
```

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OF POOR QUALITY

C  
C

```
CALL INTURB(IDATA,RDATA,VGEOM,SPWR,CASCET,NPCON)
POWER(1)=POWER(1)+SPWR(1)
POWER(2)=POWER(2)+SPWR(2)
```

C  
C  
C  
C  
C

```
DO NOT SWITCH SIGN ON M IF M=0
```

```
IF(M.EQ.0) GO TO 20
```

```
IDATA(6)=-IDATA(6)
```

C  
C

```
WRITE(5,8300) IDATA(6),IDATA(7),RDATA(8)
8300 FORMAT('OM=',I5,' N=',I5,' OMEGA=',E10.4)
```

C  
C  
C

```
SWITCH SIGN ON M AND RECALCULATE
```

```
CALL INTURB(IDATA,RDATA,VGEOM,SPWR,CASCET,NPCON)
POWER(1)=POWER(1)+SPWR(1)
POWER(2)=POWER(2)+SPWR(2)
```

C  
C

```
IDATA(6)=-IDATA(6)
```

```
GO TO 20
```

C  
C

```
IF MODE IS CUTOFF, DECIDE WHICH MODE TO TRY NEXT.
```

C  
C

```
IF(N.EQ.1) GO TO 7000
```

C  
C

```
NMAX=N-1
WRITE(5,6001) NMAX
```

6001 FORMAT('0LARGEST PROPAGATING N FOR THIS M =',I3)

C  
C  
C  
C  
C

J=J+1

INCREMENT M

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OF POOR QUALITY

M=M+1  
GO TO 15

C  
C  
C  
C  
C  
C

M=1 TO REACH THIS POINT

7000 CONTINUE

C  
C

WRITE(5,7001)

7001 FORMAT(' NO MORE PROPAGATING MODES FOR THIS OMEGA')

10 CONTINUE

WRITE(5,9001)

9001 FORMAT(' PROBLEM COMPLETED')

DO 550 JJ=1,2

IF(POWER(JJ).EQ.0.) GO TO 5215

RELPR(JJ)=10.\*ALOG10(ABS(POWER(JJ)))

GO TO 550

5215 RELPR(JJ)=1.E+35

550 CONTINUE

IF(RELPR(1).EQ.1.E+35) GO TO 5315

WRITE(5,610) RELPR(1)

GO TO 600

5315 WRITE(5,5610)

5610 FORMAT(' FREQUENCY IS CUT OFF')

600 CONTINUE

610 FORMAT(' RELATIVE POWER SPECTRAL DENSITY LEVEL UPSTREAM=',E10.4)

IF(RELPR(2).EQ.1.E+35) GO TO 5415

WRITE(5,630) RELPR(2)

GO TO 620

5415 WRITE(5,5610)

620 CONTINUE

630 FORMAT(' REL. POWER SPECTRAL DENSITY LEVEL DOWNSTREAM=',E10.4)

STOP

END

## PROGRAM INTURB

Program computes the noise  
generated by a turbofan rotor  
subjected to inlet turbulence.

SUBROUTINE INTURB(IDATA,RDATA,VGEOM,SPWR,CASCET,NPCON)

C  
C  
C  
C  
C  
C  
C  
C  
C  
C  
C  
C

PROGRAM COMPUTES THE SOUND POWER GENERATED BY A TURBOFAN ROTOR SUBJECTED TO INLET TURBULENCE. THIS IS A SIMPLIFIED VERSION SUITABLE FOR VERY SMALL TURBULENCE LENGTH SCALES IN THE RADIAL DIRECTION

PROGRAM INTERPOLATES IN RADIAL POSITION AND FREQUENCY FROM A STORED MATRIX OF PRESSURE DISTRIBUTIONS (NAME=CASCET)

DIMENSION VGEOM(10,7),RDATA(20),IDATA(10),XX(6),IERPSI(2),SPWR(2)  
DIMENSION BJJ(20)  
DIMENSION CASCET(8,5,15,5)  
DIMENSION PSISTO(30),NPCON(4),RR(30),RRNU(30)  
INTEGER P,PSTEP,PRANGE,PSTART,PEND  
REAL KMNS,MT,MA,LR,LTHETA,LX  
COMPLEX I,DELTAP,QMNS,CASCET  
COMPLEX Z,RRS,RRRS,QMNST  
COMPLEX Y

C  
C  
C  
C  
C

\*\*\*\*\*  
C DIMENSION OF PSISTO AND RRNU MUST BE .GE. NRADNU  
C DIMENSION OF RR MUST BE .GE. NRAD  
C \*\*\*\*\*

I=(0.,1.)  
PI=3.1415926

C  
C

NRADNU=IDATA(1)  
NBLADE=IDATA(2)  
NRAD=IDATA(3)  
NCHORD=IDATA(4)  
NDAT=IDATA(5)  
MM=IDATA(6)  
NN=IDATA(7)  
OMEGA=RDATA(8)  
PRANGE=NPCON(4)  
PSTART=NPCON(1)  
PEND=NPCON(2)  
PSTEP=NPCON(3)  
SIGMAR=RDATA(5)

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C  
C

0300 WRITE(5,0300) MM,NN,OMEGA  
FORMAT('MM=',I5,' NN=',I5,' OMEGA=',E10.4)  
WRITE(21,0300) MM,NN,OMEGA  
WRITE(21,700)

```
700      FORMAT(' INTURB EXECUTION')
WRITE(21,7204) NRAD,NCHORD
7204     FORMAT(' NRAD=',I3,' NCHORD=',I3)
```

LIST NONDIMENSIONAL RADIAL POSITIONS AVAILABLE IN STORED DATA (NEEDED FOR INTERPOLATION)

```
DO 5 IR=1,NRAD
R=SIGMAR+(IR-1.)*(1.-SIGMAR)/(NRAD-1.)
RR(IR)=R
CONTINUE
```

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```
WRITE(21,6)
FORMAT(' R VALUES FROM STORAGE ARE')
WRITE(21,8) RR
FORMAT(7E10.4)
```

```
MT=RDATA(1)
MA=RDATA(2)
SIGMAC=RDATA(4)
EB=RDATA(9)
EC=RDATA(10)
XMN=RDATA(11)
AMN=RDATA(12)
BMN=RDATA(13)
```

INITIALIZE ERROR ACCUMULATOR IN PSI CALCULATIONS  
IER=0

LIST NONDIMENSIONAL RADIAL POSITIONS TO BE USED IN INTERPOLATION

```
DO 7 IRNU=1,NRADNU
R=SIGMAR+(IRNU-1.)*(1.-SIGMAR)/(NRADNU-1.)
RRNU(IRNU)=R
```

COMPUTE AND STORE MODE SHAPE WEIGHTING AT EACH RADIUS

```
ARG=XMN*R
CALL RMODE(MN,ARG,AMN,BMN,PSI,EB,IERPSI)
PSISTO(IRNU)=PSI
IER=IER+ISRPSI(1)+IERPSI(2)
CONTINUE
```

7



C  
C

9 WRITE(21,9)  
FORMAT(' R VALUES FOR INTERPOLATION ARE')  
WRITE(21,8) RRNU  
WRITE(21,11)  
11 FORMAT(' PSISTO VALUES ARE')  
WRITE(21,3) PSISTO

C  
C

BETASQ=1.-MA\*\*2  
KMNS=((OMEGA\*MT)\*\*2-BETASQ\*XMN\*\*2)\*\*.5\*ABS(OMEGA)/OMEGA  
WRITE(21,7(18) KMNS  
7018 FORMAT(' KMNS=',310.4)

C  
C  
C  
C

CHECK TO BE SURE MODE NUMBER M IS IN RANGE OF STORED DATA

IF(MM.LT.0) GO TO 300

C  
C  
C  
C

FOR POSITIVE M, WANT 0.LE.M.LE.(NBLADE-1)

IF(0.LE.MM.AND.MM.LE.(NBLADE-1)) GO TO 310

C  
C  
C  
C

IF M POSITIVE BUT OUT OF RANGE, SUBTRACT INTEGER\*NBLADE

MTRIAL =MM  
NTRIAL=0  
320 CONTINUE  
NTRIAL=NTRIAL+1  
MSUM=NTRIAL-NTRIAL\*NBLADE  
IF(0.LE.MSUM.AND.MSUM.LE.(NBLADE-1)) GO TO 330  
GO TO 320  
330 MUSE=MSUM+1  
GO TO 340

C  
C  
C  
C

FOR NEGATIVE M, ADD INTEGER\*NBLADE TO M

350 MTRIAL=MM  
NTRIAL=0  
350 CONTINUE  
NTRIAL=NTRIAL+1  
MSUM=NTRIAL+NTRIAL\*NBLADE  
IF(0.LE.MSUM.AND.MSUM.LE.(NBLADE-1)) GO TO 360  
GO TO 350  
360 MUSE=MSUM+1  
GO TO 340

C  
C

310 MUSE=MM+1

C  
C

340 CONTINUE

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C  
C  
C  
C  
C  
C  
C  
341 WRITE(21,341) MM,MUSE  
FORMAT(' MM=',I5,' MUSE=',I5)

SEARCH HARMONIC ORDERS FOR FREQUENCY INTERPOLATION

WANT PMIN.LE.OMEGA.LE.PMAX

IF(MM.LT.0) GJ TO 400  
NUPMIN=PSTART

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NUPMAX=PEND  
DO 10 P=PSTART,PEND-PSTEP,PSTEP  
IF (OMEGA.GE.(1.\*P)) NUPMIN=P  
CONTINUE  
10 DO 20 P=PEND,PSTART,-PSTEP  
IF (OMEGA.LT.(1.\*P)) NUPMAX=P  
CONTINUE  
20 GO TO 490

C  
C  
C  
C  
C  
C  
C  
400 CONTINUE

FOR MODE NUMBER M.LT.0 MUST SHIFT FREQUENCY PARAMETER TO  
RETRIEVE CASSET DATA.

EQUIV.(OMEGA)=OMEGA+ABS(MM)+MSUM

EQOMEG=OMEGA+IABS(MM)+MSUM  
NUPMIN=PSTART  
NUPMAX=PEND  
DO 410 P=PSTART,PEND-PSTEP,PSTEP  
IF(EQOMEG.GE.(1.\*P)) NUPMIN=P  
CONTINUE  
410 DO 420 P=PEND,PSTART,-PSTEP  
IF(EQOMEG.LT.(1.\*P)) NUPMAX=P  
CONTINUE  
420

C  
C  
C  
C  
C  
C  
C  
490 CONTINUE

CONVERT TO FIND IP PARAMETER OF DATA STORAGE IN CASSET

IP=0  
DO 25 P=PSTART,PEND,PSTEP  
IP=IP+1  
IPP=P  
IF (NUPMIN.EQ.IPP) IPMIN=IP  
IF (NUPMAX.EQ.IPP) IPMAX=IP  
CONTINUE  
25

```

C
C      WRITE(21,21) NUPMIN,NUPMAX
21     FORMAT(' NUPMIN=',I5,' NUPMAX=',I5)
C      WRITE(21,22) IPMIN,IPMAX
22     FORMAT(' IPMIN=',I5,' IPMAX=',I5)

```

```

C
C
C      KILL PROGRAM IF DESIRED FREQUENCY IS OUT OF RANGE OF DATA
C      PSTARF=FLOAT(PSTART)
C      PENDF=FLOAT(PEND)
C      OMEGAT=OMEGA
C      IF (MM.LT.0) OMEGAT=EROMES
C      IF(PSTARF.LE.OMEGAT.AND.OMEGAT.LE.PENDF) GO TO 343
C      WRITE(5,342)
342    FORMAT(' FREQUENCY OUT OF RANGE OF DATA FILE')
C      STOP
343    CONTINUE

```

```

C
C
C      110    XSIGN=1.
C
C      ***** RETURN TO LINE (111) TO REPEAT FOR DOWNSTREAM
C      PROPAGATION *****

```

```

C
C      111    CMNS=(MT*MA*OMEGA+XSIGN*KMNS)/BETASQ
C
C      INITIALIZE VARIABLES
C      ISUMR IS ERROR CODE ACCUMULATOR FOR BESSEL WEIGHTING FUNCTION
C      PMNS IS RESULT OF DOUBLE INTEGRAL
C      SWTR IS WEIGHTING SIGN FUNCTION FOR RADIAL INTEGRATION
C
C      PMNS=0.
C      DELTAR=(1.-SIGMAR)/(NRADN-1)
C      ISUMR=0
C      IDAT=2

```

```

C
C      SWTR=-1.
C
C      *****START RADIAL INTEGRATION LOOP HERE *****
C
C      DO 901 IRNU=1,NRADNU

```

```

C
C      RADIAL POSITION SEARCH FOR INTERPOLATION COORDINATES
C
C      WANT RR(IRMIN).LE.RRNU(IRNU).LE.RR(IRMAX)
C      ***NOTE: RR(1)=RRNU(1)
C              RR(NRAD)=RRNU(NRADNU)

```

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```

IF (IRNU.EQ.1) GO TO 50
IF (IRNU.EQ.NRADNU) GO TO 60
IRMIN=1
IRMAX=NRAD
DO 30 IR=1, NRAD-1, 1
  IF (RRNU(IRNU).GE.RR(IR)) IRMIN=IR
30 CONTINUE
DO 40 IR=NRAD, 1, -1
  IF (RRNU(IRNU).LT.RR(IR)) IRMAX=IR
40 CONTINUE
GO TO 70
50 CONTINUE
  IRMIN=1
  IRMAX=2
GO TO 70
60 CONTINUE
  IRMIN=NRAD-1
  IRMAX=NRAD
GO TO 70
70 CONTINUE

```

```

WRITE(21,71) IRMIN,IRMAX
71 FORMAT(' IRMIN=',I5,' IRMAX=',I5)
  WRITE(21,72) RR(IRMIN),RRNU(IRNU),RR(IRMAX)
72 FORMAT(' RR(IRMIN=',E10.4,' RRNU(NU=',E10.4,' RR(IRMAX=',E10.4)

```

BLADE GEOMETRY AT RADIAL STATION OF INTEGRATION

```

R=RRNU(IRNU)
IF(R.LE.VGEOM(IDAT,1)) GO TO 201
IDAT=IDAT+1
IF(IDAT.GT.NDAT) IDAT=NDAT
201 DELTA=(R-VGEOM(IDAT,1))/(VGEOM(IDAT,1)-VGEOM(IDAT-1,1))
DO 210 IX=2,3
210 XX(IX-1)=VGEOM(IDAT,IX)+DELTA*(VGEOM(IDAT,IX)-VGEOM(IDAT-1,IX))

```

```

B=XX(1)/2.
CHI=XX(2)
WRITE(21,7010) B,CHI,R
7010 FORMAT(' B=',E10.4,' CHI=',E10.4,' R=',E10.4)

```

```

COSCHI=COS(CHI)
SINCHI=SIN(CHI)

```

```

ZMOD=SIGMAC*B*(GMNS*COSCHI+MM*SINCHI/R)

```

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CHORDWISE INTEGRATION USES BESSEL INTEGRATION METHOD

---CALCULATE BESSEL WEIGHTING FUNCTIONS  
BESJ REQUIRES POSITIVE ARGUMENT

X=ABS(ZMOD)  
CALL BESJ(X,0,BJ0,EB,IRROR1)  
CALL BESJ(X,NCHORD,BJ(NCHORD),EB,IRROR2)  
CALL BESJ(X,NCHORD-1,BJ(NCHORD-1),EB,IRROR3)  
ISERR=IRROR1+IRROR2+IRROR3  
WRITE(21,5400) ZMOD,ISERR

5400 FORMAT(' ZMOD=',E10.4,' ISERR=',I5)

IF(ZMOD.GT.0.) GO TO 5040

C BJ0 IS EVEN FUNCTION, ADJUST SIGN ON OTHERS

BJ(NCHORD)=BJ(NCHORD)\*(-1.)\*\*NCHORD  
BJ(NCHORD-1)=BJ(NCHORD-1)\*(-1.)\*\*(NCHORD-1)

5040 CONTINUE

C USE RECURSION RELATION TO COMPUTE AND STORE BESSEL FUNCTIONS.

DO 2000 N=NCHORD-1,2,-1  
BJ(N-1)=-BJ(N+1)+2.\*N\*BJ(N)/ZMOD

2000 CONTINUE

INITIALIZE INTERPOLATION TO GET PRESSURE VALUE FOR THIS  
FREQUENCY AND RADIAL POSITION FROM STORED DATA

USE 4 POINT BIVARIATE INTERPOLATION. SEE ABRAMOJITZ AND  
STEGUN 25.2.65

NOTE QQ AND PP ARE LESS THAN 1

DETERMINE FRACTIONAL PARTS OF FREQ. AND RADIAL SPACING

PP=(RRNU(IRNU)-RR(IRMIN))/(RR(IRMAX)-RR(IRMIN))  
QQ=(OMEGA-NUPMIN)/(NUPMAX-NUPMIN)  
IF(MM.LT.0) QQ=(EQOMEG-NUPMIN)/(NUPMAX-NUPMIN)

WRITE(21,912) PP,QQ  
912 FORMAT(' PP=',E10.4,' QQ=',E10.4)

QMNS=(0.,0.)

\*\*\*\*\* BEGIN CHORDWISE INTEGRATION LOOP HERE \*\*\*\*\*

DO 220 IZ=1,NCHORD

C COMPUTE R SUB S, THE WEIGHTING FUNCTION AT THE CHORDAL

C STATION

NOTE THAT Z=I\*\*IKOUNT BELOW

ORIGINAL PAGE IS  
OF POOR QUALITY

```

RRRS=(0.,0.)
Z=(1.,0.)
DO 5000 IKOUNT=0,NCHORD
BM=1.
IF(IKOUNT.EQ.0.OR.IKOUNT.EQ.NCHORD) BM=0.5
ARGU=IKOUNT*IZ*PI/NCHORD
IF(IKOUNT.GT.0) GO TO 5010
RRS=BM*Z*BJ0
GO TO 5020

```

```

5010 CONTINUE
RRS=BM*Z*BJ(IKOUNT)*COS(ARGU)

```

```

5020 CONTINUE
Z=Z*I
RRRS=RRRS+RRS

```

```

5000 CONTINUE
RRRS=RRRS*2.*PI/NCHORD
BN=1.
IF(IZ.EQ.NCHORD) BN=0.5

```

INTERPOLATE PRESSURE VALUES IN FREQUENCY AND RADIUS

```

MCOUNT=MUSE
Y=(1.-PP)*(1.-QQ)*CASCET(IZ,IRMIN,MCOUNT,IPMIN)
Y=Y+PP*(1.-QQ)*CASCET(IZ,IRMAX,MCOUNT,IPMIN)
Y=Y+QQ*(1.-PP)*CASCET(IZ,IRMIN,MCOUNT,IPMAX)
Y=Y+PP*QQ*CASCET(IZ,IRMAX,MCOUNT,IPMAX)

```

```

WRITE(21,2) CASCET(IZ,IRMIN,MCOUNT,IPMIN)
WRITE(21,2) CASCET(IZ,IRMAX,MCOUNT,IPMIN)
WRITE(21,2) CASCET(IZ,IRMIN,MCOUNT,IPMAX)
WRITE(21,2) CASCET(IZ,IRMAX,MCOUNT,IPMAX)

```

```

2 FORMAT(' CASCET=',2E10.4)

```

EVALUATE FINITE CHORDWISE SUM TO APPROX. INTEGRAL

```

QMNST=Y*RRRS*BN
QMNS=QMNS+Y*RRRS*BN
WRITE(21,5030) IZ,QMNST
5030 FORMAT(' IZ=',I5,' QMNST=',2E10.4)
220 CONTINUE

```

C \*\*\*\*\*END OF CHORDWISE INTEGRATION LOOP (220) \*\*\*\*\*

```

7022 WRITE(21,7022) IRNU,QMNS
FORMAT(' IRNU=',I3,' QMNS=',2E10.4)

```

8010 CONTINUE  
GO TO 8013

8012 CONTINUE  
SUMNU=0.

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8013 CONTINUE  
WRITE(21,8015) SUMNU,P,TURM

8015 FORMAT(' SUMNU=',E10.4,' P=',I5,' TURM=',E10.4)

C  
C  
C  
C  
C

FMNS=CB\*CC\*CD\*SUMNU/R

WHTR=1.+SWTR/3.

SWTR=-SWTR

IF(IR.EQ.1.OR.IR.EQ.NRAD) WHTR=WHTR/2.

C  
C

PMNS=PMNS+WHTR\*FMNS\*DELTAR\*SIGMAC\*SIGMAC\*2.

WRITE(21,7016) PMNS

7016 FORMAT(' PMNS SUM(R)=',E10.4)

901 CONTINUE

C  
C  
C  
C  
C

C\*\*\*\*\* END OF RADIAL INTEGRATION LOOP (901) \*\*\*\*\*

SMN=((BETAS2\*NBLADE)\*\*2)\*MA\*MT\*OMEGA\*PMNS/PI/KMNS  
SMN=SMN/(1.-SIGMAR\*\*2)/(OMEGA\*MT+XSIGN\*MA\*KMNS)\*\*2  
SMN=-XSIGN\*SMN

C  
C  
C  
C  
C

MULTIPLY OUTPUT BY 2 (ADDS +3DB) TO ACCOUNT FOR ENERGY  
IN NEGATIVE FREQUENCY

SMN=SMN\*2.

REL PWR=SMN

IPWR=1

IF(RELPWR.EQ.0.) GO TO 915

RELPR=10.\*ALJG10(ABS(RELPWR))

GO TO 920

915 IPWR=0

920 CONTINUE

C  
C  
C

IF(XSIGN.LT.0.) GO TO 9000

C  
C

WRITE(5,3000)

FORMAT('UPSTREAM ')

WRITE(5,8101) GMNS

3000

```
8101  FORMAT(' GAMMA M,N,SB =',E16.8)
      WRITE(5,8102) SMN
8102  FORMAT(' REL. MODAL SOUND POWER SPECTRAL DENSITY=',E10.4)
      WRITE(5,8500) IER
      WRITE(5,5500) ISUMR
8500  FORMAT(' SUM OF ALL ERRORS IN PSI CALCULATIONS =',I5)
      IF(IPWR.EQ.0) GO TO 970
      WRITE(5,3600) RELPRL
      GO TO 980
970   CONTINUE
      WRITE(5,952)
980   CONTINUE
8600  FORMAT(' REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=',E10.4)
      WRITE(21,7200)
7200  FORMAT(' END OF UPSTREAM INTEGRATION')
      XSIGN=-1.
      SPWR(1)=RELPWR
      GO TO 111
```

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C  
C\*\*\*\*\* RETURN TO LINE 111 TO COMPUTE DOWNSTREAM PROPAGATION  
C\*\*\*\*\*

```
C
9000  WRITE(5,8200)
8200  FORMAT('DOWNSTREAM')
      WRITE(5,8201) GMNS
8201  FORMAT(' GAMMA M,N,SB =',E16.8)
      WRITE(5,8202) SMN
8202  FORMAT(' REL. MODAL SOUND POWER SPECTRAL DENSITY=',E10.4)
      WRITE(5,8400) IER
      WRITE(5,5500) ISUMR
5500  FORMAT(' SUM OF ALL ERRORS IN RS CALCULATIONS=',I5)
8400  FORMAT(' SUM OF ALL ERRORS IN PSI CALCULATIONS =',I5)
      IF(IPWR.EQ.0) GO TO 950
      WRITE(5,8500) RELPRL
      GO TO 960
950   CONTINUE
      WRITE(5,952)
952   FORMAT(' SOUND POWER SPECTRAL DENSITY FOR MODE=0/UNEXCITED')
960   CONTINUE
      SPWR(2)=RELPWR
      WRITE(21,7202)
7202  FORMAT(' END OF DOWNSTREAM INTEGRATION')
      RETURN
      END
```



## PROGRAM MAINTW

This is a calling program to control the computation of pressure data for the wake turbulence case.



```
2006  FORMAT(' NDAT =')
      READ(5,1001) NDAT
      WRITE(5,2106) NDAT
2106  FORMAT(' NDAT=',I3)
      WRITE(5,2007)
2007  FORMAT(' VANE GEOMETRY MATRIX INPUT')
      WRITE(5,2008)
2008  FORMAT(' FEED MATRIX IN ONE ROW AT A TIME, FROM HUB TO TIP')
```

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C  
C

```
      DO 10 IROW=1,NDAT
      WRITE(5,2009) IROW
2009  FORMAT(' ROW=',I3,' R/RDUCT =')
      READ(5,1001) VGEOM(IROW,1)
      WRITE(5,2010)
2010  FORMAT(' C/CTIP =')
      READ(5,1001) VGEOM(IROW,2)
      WRITE(5,2011)
2011  FORMAT(' THETA (DEGREES) =')
      READ(5,1001) VGEOM(IROW,3)
      VGEOM(IROW,3)=VGEOM(IROW,3)*.0174533
10    CONTINUE
```

10  
C  
C

```
      WRITE(5,2020)
2020  FORMAT(' VANE GEOMETRY MATRIX IS')
      DO 11 IROW=1,NDAT
      WRITE(5,2120) (VGEOM(IROW,ICOLMN),ICOLMN=1,3)
2120  FORMAT(' ',7E10.3)
11    CONTINUE
```

C  
C  
C

```
      WRITE(5,5000)
5000  FORMAT(' TYPE 1 TO INPUT ROTOR WAKE VELOCITY; 0 FOR FREE
1  VORTEX')
      READ(5,1001) IVOR
      WRITE(5,5010) IVOR
5010  FORMAT(' IVOR=',I3)
      IF (IVOR.EQ.0) NVELO=0
      IF (IVOR.EQ.0) GO TO 4005
```

C  
C

```
      WRITE(5,3000)
3000  FORMAT(' NUMBER OF RADII FOR SPECIFYING MEAN ROTOR FLOW =')
      READ(5,1001) NVELJ
      WRITE(5,3002) NVELO
3002  FORMAT(' NVELJ=',I3)
      WRITE(5,3004)
3004  FORMAT(' INPUT MATRIX FOR MEAN ROTOR FLJ =')
      WRITE(5,3006)
```

```

3006  FORMAT(' FEED MATRIX IN ONE ROW AT A TIME, FROM HUB TO TIP')
      DO 4000 IROW=1,NVELO
      WRITE(5,3008) IROW
3008  FORMAT(' ROW=',I3,' R/RDUCT=')
      READ(5,1001) VELOCV(IROW,1)
      WRITE(5,3012)
3012  FORMAT(' MEAN CIRCUMFERENTIAL VELOCITY RATIO(0 CIRCUM/U
1 AXIAL0=')
      READ(5,1001) VELOCV(IROW,2)
4000  CONTINUE

```

C  
C

```

      WRITE(5,3014)
3014  FORMAT(' MEAN ROTOR FLOW VELOCITY MATRIX IS')
      DO 4002 IROW=1,NVELO
      WRITE(5,3016) (VELOCV(IROW,ICOLMN),ICOLMN=1,2)
3016  FORMAT(' ',2E10.4)
4002  CONTINUE

```

C  
C  
C

```

4005  CONTINUE

```

C  
C  
C  
C

```

      WRITE(5,2030)
2030  FORMAT(' MT =')
      READ(5,1001) MT
      WRITE(5,2130) MT
2130  FORMAT(' MT=',E16.8)
      WRITE(5,2031)
2031  FORMAT(' MA =')
      READ(5,1001) MA
      WRITE(5,2131) MA
2131  FORMAT(' MA =',E16.8)

```

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C  
C  
C  
C

```

      IF (IVOR.EQ.1) GO TO 6000
      WRITE(5,2032)
2032  FORMAT(' VYFM/VXM @ R=RDUCT=')
      READ(5,1001) MUV
      WRITE(5,2132) MUV
2132  FORMAT(' MUV=',E10.4)
6000  CONTINUE
      IF (IVOR.EQ.1) MUV=0.

```

C  
C  
C

```

      WRITE(5,2035)

```

```
2035  FORMAT(' NUMBER OF RADIAL STATIONS =')
      READ(5,1001) NRAD
      WRITE(5,2135) NRAD
2135  FORMAT(' NRAD=',I4)
      WRITE(5,2036)
2036  FORMAT(' NUMBER OF CHORDWISE STATIONS (.LE.20) =')
      READ(5,1001) NCHORD
      WRITE(5,2136) NCHORD
2136  FORMAT(' NCHORD=',I4)
C
C      WRITE(5,100)
100   FORMAT(' START FREQUENCY(HARMONIC NO. OF SHAFT) =')
      READ(5,1001) PSTART
      WRITE(5,110) PSTART
110   FORMAT(' PSTART=',I4)
      WRITE(5,120)
120   FORMAT(' END FREQUENCY(HARMONIC NO. OF SHAFT) =')
      READ(5,1001) PEND
      WRITE(5,130) PEND
130   FORMAT(' P END=',I4)
C
C      WRITE(5,140)
140   FORMAT(' FREQUENCY STEP SIZE (HARMONIC ORDERS) =')
      READ(5,1001) PSTEP
      WRITE(5,150) PSTEP
150   FORMAT(' PSTEP=',I4)
      PRANGE=(PEND-PSTART)/PSTEP+1
      IDATA(1)=NVANE
      IDATA(2)=NBLADE
      IDATA(3)=NRAD
      IDATA(4)=NCHORD
      IDATA(5)=NDAT
      IDATA(6)=PSTART
      IDATA(7)=PEND
      IDATA(8)=PSTEP
      IDATA(9)=IVOR
      IDATA(10)=NVELO
C
C      RDATA(1)=MT
      RDATA(2)=MA
      RDATA(4)=SIGMAC
      RDATA(5)=SIGMAR
      RDATA(6)=MUV
C
CALL STATOR(IDATA,RDATA,VGEOM,VELOCV)
STOP
END
```

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## PROGRAM STATOR

Program calculates and stores the pressures generated on a turbofan stator by wake turbulence.

SUBROUTINE STATOR(IDATA,RDATA,VGEOM,VELOCV)

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DIMENSION OF DELTAP=20  
DIMENSION JF CASCET=(NCHORD,NRAD,NVANE,PRANGE)

NOTE NCHORD MUST BE NO GREATER THAN 20

DIMENSION DELTAP(20)  
DIMENSION VGEOM(10,7),RDATA(20),IDATA(10),XX(6)  
DIMENSION CASCET(3,5,11,3)  
DIMENSION A(72),VELOCV(10,2)  
REAL KB,MR,MA,MT,MYM,MTHETA  
COMPLEX I,DELTAP,CASCET  
INTEGER PSTART,PEND,P,PRANGE,PSTEP  
I=(0.,1.)  
PI=3.1415926

NVANE=IDATA(1)  
NBLADE=IDATA(2)  
NRAD=IDATA(3)  
NCHORD=IDATA(4)  
NOAT=IDATA(5)  
PSTART=IDATA(6)  
PEND=IDATA(7)  
PSTEP=IDATA(8)  
IVOR=IDATA(9)  
NVELO=IDATA(10)

WRITE(5,160)  
160 FORMAT(' ENTER TITLE FOR DATA FILE(MAX 72 CHARACTERS)')  
READ(5,1003) A  
1003 FORMAT(72A1)

MT=RDATA(1)  
MA=RDATA(2)  
SIGMAC=RDATA(4)  
SIGMAR=RDATA(5)

IDAT=2  
IDOT=2

START LOOPS TO CALL CASC--BEGIN WITH LOOP ON RADIAL  
POSITION TO MINIMIZE INTERPOLATION.

DO 308 IK=1,NRAD

DO 300 P=PSTART,PEND,PSTEP  
IP=IP+1

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OMEGBC=MT\*SIGMAC\*B\*P

MR=(MA\*\*2+MTHETA\*\*2)\*\*.5

KB=MT/MR\*B\*SIGMAC\*P  
SIGMA=-2.\*PI\*MM/NVANE

H=2.\*PI\*R/NVANE/SIGMAC/B

ANGLE= -TnETA

```

WRITE(21,300)
300  FORMAT('0INPUT TO SUBROUTINE CASC')
    WRITE(21,302) OMEGBC
302  FORMAT(' OMEGBC=',E10.4)
    WRITE(21,304) MR,KB,SIGMA
304  FORMAT(' MR=',E10.4,' KB=',E10.4,' SIGMA=',E10.4)
    WRITE(21,306) H,ANGLE,NCHORD
306  FORMAT(' H=',E10.4,' ANGLE=',E10.4,' NCHORD=',I3)

```

CALL CASC(OMEGBC,MR,KB,SIGMA,H,ANGLE,NCHORD,DELTAP,IERP)

STORE RESULTS OF CASC IN STORAGE MATRIX FOR DISK FILE.  
 MATRIX POSITION DESCRIPTORS ARE(IN ORDER OF APPEARANCE):

1. CHORDWISE POSITION(TRAILING TO LEADING EDGES)
2. RADIAL POSITION(INNER RADIUS TO OUTER RADIUS)
3. CIRCUMFERENTIAL MODE NUMBER + 1 (M+1)
4. ORDER OF FREQUENCY COMPUTATIONS(FIRST TO LAST)

WITH: IP=1 FOR PSTART  
 IP=PRANGE FOR PEND

DO 310 ICK=1,NCHORD  
CASCET(ICK,IR,MCOUNT,IP)=DELTAP(ICK)



```

310 CONTINUE
    WRITE(5,7500) IERP
7500 FORMAT(' ERROR CODE FROM INVERSION ROUTINE=',I3)
    WRITE(21,7025)
7025 FORMAT(' OUTPUT FROM CASC:(DELTA(IQ),IQ=1,NCHORD')
    WRITE(21,7002) (DELTA(IQ),IQ=1,NCHORD)
7002 FORMAT(5X,6E10.4)

```

C  
C  
C  
C  
C  
C  
C  
C  
C  
C

```

308 CONTINUE

STORE MATRIX OF PRESSURE VALUES ON THE DISK FOR LATER
PROCESSING BY OTHER PROGRAMS.

```

```

CALL OFILE(23,'STAT')
WRITE (23) A
WRITE (23) IDATA
WRITE (23) RDATA
WRITE (23) VGEOM
WRITE (23) VELOCV
WRITE (23) CASCET

```

C  
C  
C  
C

ENDFILE 23

STOP  
END

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**PROGRAM WASXCH**

Program determines which modes propagate for the case of rotor wake turbulence and controls the noise computation.

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```

PROGRAM ASKCH
  DIMENSION CASSET(8,5,11,3)
  DIMENSION IA(8),IDATA(12)
  DIMENSION RDATA(22),VGEOM(13,7),POWER(2),SPWR(2),RELPR(2)
  DIMENSION NPCON(4),VELOCV(13,2)
  DIMENSION A(72)
  DIMENSION ISUMTO(120)
  COMPLEX CASSET
    REAL LA,LP,LT,ETA
  INTEGER PRANGE, PSTART, PSTEP, PEND
  REAL MF,MA

```

C

```

  DATA (ISUMTO(J),J=1,120)/120*F/
  DATA (POWER(J),J=1,2)/2*2.7/

```

C

C

C

C

C

C

C

C

C

C

C

C

C

CALLING PROGRAM FOR DIFURS TO SEARCH OUT AND CALCULATE ALL PROPAGATING MODES AT A GIVEN POSITIVE FREQUENCY.

C

C

C

C

C

C

C

C

C

C

C

C

C

C

C

C

C

OPEN FILE "STAT" AND READ INPUT ARRAYS INCLUDING MAIN STORAGE MATRIX "CASSET"

\*\*\*\*\*NOTE THAT "STAT" IS A SEQUENTIAL UNFORMATTED BINARY FILE--

ORDER OF STORAGE=A,IDATA,RDATA,VGEOM,VELOCV,CASSET

C

C

C

C

C

C

C

C

C

C

C

C

C

C

C

C

C

C

C

```

CALL IFILE(23,"STAT")
  READ (23) A
  READ (23) IDATA
  READ (23) RDATA
  READ (23) VGEOM
  READ (23) VELOCV
  READ (23) CASSET
ENDFILE 23

```

```

  WRITE(5,6)
  FORMAT(' USER-ASSIGNED TITLE OF DATA SET FROM FILE "STAT" IS ')
  WRITE(5,6) A

```

```

  FORMAT(' ',72A1)

```

```

  PSTART=IDATA(6)
  PEND=IDATA(7)
  PSTEP=IDATA(8)
  PRANGE=(PEND-PSTART)/PSTEP+1
  NPCON(1)=PSTART
  NPCON(2)=PEND
  NPCON(3)=PSTEP
  NPCON(4)=PRANGE

```

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C  
C  
C ENTER NOISE FREQUENCY OF INTEREST(MUST BE POSITIVE FREQUENCY)  
C

```
1001 FORMAT(G24.8)
      WRITE(5,110)
110  FORMAT(' NOISE FREQUENCY/SHAFT FREQUENCY=')
      READ(5,1001) JMEGA
      RDATA(1)=JMEGA
115  FORMAT(' MEGA=',E12.4)
      WRITE(5,115) RDATA(1)
```

C  
C SELECT NO. OF RADIAL POSITIONS TO INTERPOLATE PRESSURES  
C (ASSUMED THAT NRADNO.GE.NRAD)

C  
C \*\*\*\*\*NOTE: NRADNO MUST BE .LE.30 UNLESS DIMENSION STATEMENTS IN  
C "DIFORMS" ARE TO BE MODIFIED  
C \*\*\*\*\*

```
      WRITE(5,120)
120  FORMAT(' NUMBER OF RADIAL POSITIONS FOR ACOUSTIC COMP.=')
      READ(5,1201) NRADNO
      RDATA(13)=FLOAT(NRADNO)
      WRITE(5,130) NRADNO
130  FORMAT(' NRADNO=',I4)
      WRITE(5,2037)
2037 FORMAT(' ACCURACY OF BESSEL FNS=')
      READ(5,1001) EB
      WRITE(5,2137) EB
2137 FORMAT(' EB=',E14.4)
      WRITE(5,2038)
2038 FORMAT(' ACCURACY OF CONVERGENCE TO ROOT XFN=')
      READ(5,1001) EC
      WRITE(5,2138) EC
2138 FORMAT(' EC=',E14.4)
```

C  
C ENTER TURBULENCE CHARACTERISTICS  
C

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```
      WRITE(5,2033)
2033 FORMAT(' WAKE WIDTH=')
      READ(5,1001) WWIDTH
      WRITE(5,2133) WWIDTH
2133 FORMAT(' WWIDTH=',E14.4)
      WRITE(5,2034)
2034 FORMAT(' TURBULENCE INTENSITY(RMS FLUCTUATING U/U BAR)=')
      READ(5,1001) EPSW
2134 FORMAT(' EPSW=',E12.4)
      WRITE(5,2134) EPSW
```

C

```
      WRITE(5,6010)
0010 FORMAT(' TURBULENCE LENGTH SCALE IN AXIAL DIRECTION=')
      READ(5,1001) LX
      WRITE(5,6002) LX
```

```

0022  FORMAT(' LX=',E10.4)
      WRITE(5,0022)
0024  FORMAT(' TOLERANCE LENGTH SCALE IN RADIAL DIRECTION=')
      READ(5,1001) LR
      WRITE(5,0024) LR
0026  FORMAT(' LR=',E10.4)
      WRITE(5,0026)
0028  FORMAT(' TOLERANCE LENGTH SCALE IN CIRCUMFERENTIAL DIRECTION=')
      READ(5,1001) LTHETA
      WRITE(5,0028) LTHETA
0030  FORMAT(' LTHETA=',E10.4)
      RDATA(3)=RPSa
      RDATA(7)=RWIDTH
      RDATA(15)=LR
      RDATA(16)=Lr
      RDATA(17)=LTHETA
      RDATA(9)=EB
      RDATA(10)=EC
      X1=RDATA(1)
      X2=RDATA(2)
      SIGMA=COS(5)

```

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C  
C  
C  
C

```
XMAX=COS(5)*4/(1.-X1**2)**.5
```

2001

```

      WRITE(21,2001) XMAX
      FORMAT(' MAX(MAX) FOR PROPAGATION =',E15.5)

```

C  
C  
C  
C  
C  
C  
C  
C

START WITH PLANE WAVE MODE (0,1). COUNT UP IN N, THEN M UNTIL ALL POSSIBLE HIGHER MODES ARE CUT OFF.

```

      J=1
      M=0

```

C  
C  
C  
C  
C  
C  
C  
C  
C  
C  
C

RESTART N COUNT HERE FOR NEW M

```

      N=1
      INCREMENT N
      N=N+1

```

```
      NAPS=IABS(N)
```

C  
C  
C  
C  
C  
C  
C  
C  
C  
C

CALL ANRI (MARS, X, SIGMAR, EB, EC, XAM, IEB, IEC)

IF MODE IS CUT OFF, GO TO 6000

IF(XAM.GE.XMAX) GO TO 6700

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```

3000 WRITE(21,3000)
      FORMAT('MODE DATA')
      WRITE(21,3001) OMEGA, M, N, XAM
3001 FORMAT('OMEGA=',E12.4,'      W=',13,'      V=',13,'      XAM=',E10.4)
      IF(XAM.EQ.0.) GO TO 1200
      COEFFA=XMAX/XAM
      WRITE(21,4000) COEFFA
4000 FORMAT('CUTOFF RATIO FOR MODE=',E12.4)
      GO TO 1200
1200 CONTINUE
      WRITE(21,4000)
4005 FORMAT('PLANE WAVE MODE: CUTOFF RATIO IS + INFINITE')
1005 CONTINUE
      WRITE(21,3002) IEB
3002 FORMAT('SUM OF BESSEL FUNCTION ERROR CODES =',I3)
      WRITE(21,3003) IEC
3003 FORMAT('ERROR CODE FOR CONVERGENCE TO ROOT AMN =',I3)

```

C  
C  
C

NORMALIZE MODE AMPLITUDE

CALL EIGEN (MARS, SIGMAR, AMN, AMB, BMN, BP, IER)

C  
C

```

      WRITE(21,3004) AMN, AMB
3004 FORMAT('AMN =',E10.8,'      AMB =',E10.8)
      WRITE(21,3005) IER
3005 FORMAT('ERROR CODE FOR BESSEL FNS IN AMN AND AMB CALC =',I12)

```

C  
C

```

RDATA(11)=AMN
RDATA(12)=AMB
RDATA(13)=BMN
IDATA(6)=*
IDATA(7)=*

```

C  
C

```

CALL WATURN(IDATA, RDATA, VGEOM, VELUCV, SPWR, CASSET, WPCUN,
1 ISUMTU)
POWER(1)=POWER(1)+SPWR(1)
POWER(2)=POWER(2)+SPWR(2)

```



C  
C

```
WRITE(21,7001)
7001  FORMAT(' NO MORE PROPAGATING MODES FOR THIS OMEGA')
10    CONTINUE
      WRITE(5,9001)
9001  FORMAT(' PROBLEM COMPLETED')
      DO 500 JJ=1,2
        IF(POWER(JJ).EQ.0.) GO TO 5215
        RELPR(JJ)=10.*ALOG10(ABS(POWER(JJ)))
        GO TO 557
5215  RELPR(JJ)=1.E+35.
550    CONTINUE
        IF(RELPR(1).EQ.1.E+35) GO TO 5315
        WRITE(5,610) RELPR(1)
        GO TO 600
5315  WRITE(5,5510)
5610  FORMAT(' FREQUENCY IS CUT OFF')
600    CONTINUE
510  FORMAT(' RELATIVE POWER SPECTRAL DENSITY LEVEL UPSTREAM=',E10.4)
      IF(RELPR(2).EQ.1.E+35) GO TO 5415
      WRITE(5,630) RELPR(2)
      GO TO 620
5415  WRITE(5,5510)
520  CONTINUE
630  FORMAT(' REL. POWER SPECTRAL DENSITY LEVEL DOWNSTREAM=',E10.4)
      STOP
      END
```

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PROGRAM WATURB

Program computes the sound power  
generated by a turbofan *stator*  
subjected to wake turbulence.

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SUBROUTINE NATURH(IDATA,RDATA,VGEOM,VELOCV,SPWR,CASCET,NPCON,  
1 ISUMTU)

C  
C  
C  
C  
C  
C  
C  
C  
C  
C  
C  
C

PROGRAM COMPUTES THE SOUND POWER GENERATED BY A TURBOFAN  
STATOR SUBJECTED TO INLET TURBULENCE. THIS IS A SIMPLIFIED  
VERSION SUITABLE FOR VERY SMALL TURBULENCE LENGTH SCALES  
IN THE RADIAL DIRECTION

PROGRAM INTERPOLATES IN RADIAL POSITION AND FREQUENCY FROM A  
STORED MATRIX OF PRESSURE DISTRIBUTIONS (NAME=CASCET)

DIMENSION VGEOM(10,7),RDATA(20),IDATA(10),XX(6),IERPSI(2),SPWR(2)  
DIMENSION BJ(20)  
DIMENSION PSISTO(30),NPCON(4),RR(30),RRNU(30)  
DIMENSION VELOCV(10,2)  
DIMENSION CASCET(8,5,11,3)  
DIMENSION ISUMTU(100),SUMTJT(100,30)  
INTEGER P,PSTEP,PRANGE,PSTART,PEND,S1  
REAL KMNS,MR,MT,MA,LR,LTHETA,LX,MYM,MTHETA  
COMPLEX I,QMNS,A1,CASCET  
COMPLEX Z,RRS,RRRS,MMNST  
COMPLEX X

C  
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C  
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C  
C

\*\*\*\*\*  
C DIMENSION OF PSISTO AND RRNU MUST BE .GE. NRAONU  
C DIMENSION OF RX MUST BE .GE. NRAOU  
C\*\*\*\*\*

I=(0.,1.)  
PI=3.1415926

NRAONU=IFIX(RDATA(15))  
NVAHE=IDATA(1)  
NBLADE=IDATA(2)  
NRAU=IDATA(3)  
NCHORD=IDATA(4)  
NDAT=IDATA(5)  
MM=IDATA(6)  
NN=IDATA(7)  
LVOR=IDATA(9)  
NVELO=IDATA(10)  
OMEGA=RDATA(8)  
PRANGE=NPCON(4)  
PSTART=NPCON(1)  
PEND=NPCON(2)  
PSTEP=NPCON(3)  
SIGMAH=RDATA(5)

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C  
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```
WRITE(5,6328) M4,NN,OMEGA
8300 FORMAT('M=',15,' N=',15,' OMEGA=',E12.4)
7204 FORMAT('NRAD=',13,' NCHORD=',13)
```

C  
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C

LIST NONDIMENSIONAL RADIAL POSITIONS AVAILABLE IN STORED  
DATA (NEEDED FOR INTERPOLATION)

```
DO 5 IR=1,NRAD
R=SIGMAR+(IR-1.)*(1.-SIGMAR)/(NRAD-1.)
RR(IR)=R
CONTINUE
```

5  
C  
C  
C  
C  
6  
8  
C  
C  
C

FORMAT('R VALUES FROM STORAGE ARE')  
FORMAT(7E10.4)

```
MT=RDATA(1)
MA=RDATA(2)
EPSW=RDATA(3)
SIGNAC=RDATA(4)
MUV=RDATA(6)
WIDTH=RDATA(7)
EB=RDATA(9)
EC=RDATA(10)
XMN=RDATA(11)
AMN=RDATA(12)
BMN=RDATA(13)
LX=RDATA(15)
LR=RDATA(16)
LTHETA=RDATA(17)
```

C  
C  
C  
C  
C  
C  
C

INITIALIZE APROR CODE ACCUMULATOR IN PSI COMPUTATIONS  
IER=2

LIST NONDIMENSIONAL RADIAL POSITIONS TO BE USED IN INTERPOLATION

```
DO 7 IRNU=1,NRADNU
R=SIGMAR+(IRNU-1.)*(1.-SIGMAR)/(NRADNU-1.)
RRNU(IRNU)=R
```

C  
C  
C

COMPUTE AND STORE MODE SHAPE WEIGHTING AT EACH RADIUS

```
C
      ARG=AMN*R
      CALL KMODE(MM,ARG,AMN,SMN,PSI,EB,IERPSI)
      PSISTO(IRNU)=PSI
      IER=IER+IERPSI(1)+IERPSI(2)
```

7 CONTINUE

```
C
C
C 9      FORMAT(' R VALUES FOR INTERPOLATION ARE')
C 11     FORMAT(' PSISTO VALUES ARE')
```

C
C PERFORM SUMMATION OVER TRANSFORMS OF AUTOCORRELATION
C FUNCTIONS FOR LATER USE. THIS SUMMATION IS A
C FUNCTION OF MODE NUMBER M AND RADIUS R FOR A GIVEN SET
C OF INPUT PARAMETERS.

C CHECK TO SEE WHETHER SUM IS AVAILABLE FROM STORAGE

```
C
      MINDEX=MM+50
      IF(ISUMTO(MINDEX).EQ.1) GO TO 6040
```

C MAKE SURE STORAGE LIMITS ARE NOT EXCEEDED

```
C
      IF(MM.GT.49) WRITE(5,5010)
6010  FORMAT(' MODE NUMBER M EXCEEDS STORAGE OF MATRIX SUMTOT')
      IF(MM.GT.49) STOP
```

C COMPUTE SUMMATION AS A FUNCTION OF R AND STORE IN SUMTOT

```
C
      DO 6020 IRNU=1,NRADNU
      K=KRNU(IRNU)
      SUMTOT(MINDEX,IRNU)=0.
```

C LIMITS ON DOUBLE SUM ADAPT TO PHYSICAL PARAMETERS

```
C
      MM1MAX=INT(23.*R/NBLADE/WIDTH)
      MM1MAX=INT(1./NVANE*(16.*R/LTHETA+MM1MAX*NBLADE+20.))
      DO 6020 MM1=-MM1MAX,MM1MAX
      FARG=MM1*NBLADE*WIDTH/R
      PHIARG=HT*LX/4A*(OMEGA+MM1*NBLADE)
      TERM1=PHIXHT(PHIARG)*(ABS(PHAT(FARG)))**2
      DO 6000 MM1=-MM1MAX,MM1MAX
      THEARG=((MM1*NVANE)-(MM1*NBLADE)-MM)*LTHETA/R
      TURM1=TERM1*PHITM(THEARG)
      SUMTOT(MINDEX,IRNU)=SUMTOT(MINDEX,IRNU)+TURM1
6000  CONTINUE
      WRITE(21,6015) MM,OMEGA,R,SUMTOT(MINDEX,IRNU)
6015  FORMAT(' M4=',I5,' OMEGA=',E10.4,' R=',E10.4,' SUMTOT=',E10.4)
```

```
C
C 6020  CONTINUE
      ISUMTO(MINDEX)=1
```

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C  
6040 CONTINUE

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BETASQ=1.-MA\*\*2  
KMNS=((OMEGA\*MT)\*\*2-3BETASQ\*XMN\*\*2)\*\*.5)\*ABS(OMEGA)/OMEGA  
WRITE(21,7010) KMNS  
7010 FORMAT(' KMNS=',E10.4)

C  
C  
C  
CHECK TO BE SURE MODE NUMBER M IS IN RANGE OF STORED DATA

IF(MM.LT.0) GO TO 300

C  
C  
FOR POSITIVE M, WANT 0.LE.M.LE.(NVANE-1)

IF(0.LE.MM.AND.MM.LE.(NVANE-1)) GO TO 310

C  
C  
IF M POSITIVE BUT OUT OF RANGE, SUBTRACT INTEGER\*NVANE

MTRIAL =MM  
NTRIAL=0  
320 CONTINUE  
NTRIAL=NTRIAL+1  
MSUM=MTRIAL-NTRIAL\*NVANE  
IF(0.LE.MSUM.AND.MSUM.LE.(NVANE-1)) GO TO 330  
GO TO 320  
330 MUSE=MSUM+1  
GO TO 340

C  
C  
FOR NEGATIVE M, ADD INTEGER\*NVANE TO M

300 MTRIAL=MM  
NTRIAL=0  
350 CONTINUE  
NTRIAL=NTRIAL+1  
MSUM=MTRIAL+NTRIAL\*NVANE  
IF(0.LE.MSUM.AND.MSUM.LE.(NVANE-1)) GO TO 360  
GO TO 350  
360 MUSE=MSUM+1  
GO TO 340

C  
310 MUSE=MM+1

C  
340 CONTINUE

C  
341 FORMAT(' MM=',I5,' MUSE=',I5)

C  
C  
C  
KILL PROGRAM IF DESIRED FREQUENCY IS OUT OF RANGE  
OF STORED DATA

```

C
PSTARF=FLOAT(PSTART)
PENDF=FLOAT(PEND)
IF(PSTARF.LE.OMEGA.AND.JMEGA.LE.PENDF) GO TO 343
WRITE(5,342)
342 FORMAT(' FREQUENCY OUT OF RANGE OF DATA')
STOP
343 CONTINUE

```

```

C
C
C SEARCH HARMONIC ORDERS FOR FREQUENCY INTERPOLATION
C
C WANT PMIN.LE.OMEGA.LE.PMAX

```

```

C
C NUPMIN=PSTART
C
C NUPMAX=PEND
C DO 10 P=PSTART,PEND,PSTEP,PSTEP
C IF (OMEGA.GE.(1.*P)) NUPMIN=P
10 CONTINUE
C DO 20 P=PEND,PSTART,-PSTEP
C IF (OMEGA.LT.(1.*P)) NUPMAX=P
20 CONTINUE

```

```

C
C
C
C
C CONVERT TO FIND IP PARAMETER OF DATA STORAGE IN CASSET

```

```

C
C IP=0
C DO 25 P=PSTART,PEND,PSTEP
C IP=IP+1
C IPP=P
C IF (NUPMIN.EQ.IPP) IPMIN=IP
C IF (NUPMAX.EQ.IPP) IPMAX=IP
25 CONTINUE

```

```

C
C 21 FORMAT(' NUPMIN=',I5,' NUPMAX=',I5)
C 22 FORMAT(' IPMIN=',I5,' IPMAX=',I5)

```

```

C
C
C 110 XSIGN=1.

```

C \*\*\*\*\* RETURN TO LINE (111) TO REPEAT FOR DOWNSTREAM  
C PROPAGATION \*\*\*\*\*

```

C
C 111 GMNS=(NT*NA*OMEGA+XSIGN*K4NS)/BETASQ
C
C

```

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C INITIALIZE VARIABLES  
C ISUMR IS ERROR CODE ACCUMULATOR FOR BESSEL WEIGHTING FUNCTION  
C \*\*\*S

C PMNS IS RESULT OF DOUBLE INTEGRAL  
C  
C

C S\*TR IS WEIGHTING SIGN FUNCTION IN RADIAL INTEGRATION  
C

PMNS=0.  
DELTAR=(1.-SIGMAR)/(NRADNJ-1)  
ISUMR=0  
IDOT=2  
IDAT=2

C  
C S\*TR=-1.

C \*\*\*\*\*START RADIAL INTEGRATION LOOP HERE \*\*\*\*\*  
C

DO 901: IRNU=1, NRADNU

C  
C  
C RADIAL POSITION SEARCH FOR INTERPOLATION COORDINATES  
C  
C

WANT RR(IRMIN).LE.RRNU(IRNU).LE.RR(IRMAX)  
\*\*\*NOTE: RR(1)=RRNU(1)  
RR(NRAD)=NRNU(NRADNU)

IF (IRNU.EQ.1) GO TO 50  
IF (IRNU.EQ.NRADNU) GO TO 60  
IRMIN=1  
IRMAX=NRAD  
DO 30 IR=1, NRAD-1, 1  
IF (NRNU(IRNU).GE.NR(IR)) IRMIN=IR

30 CONTINUE

DO 40 IR=NRAD, 1, -1  
IF (RRNU(IRNU).LT.RR(IR)) IRMAX=IR

40 CONTINUE

GO TO 70

50 CONTINUE

IRMIN=1

IRMAX=2

GO TO 70

60 CONTINUE

IRMIN=NRAD-1

IRMAX=NRAD

GO TO 70

70 CONTINUE

C  
C

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```

71      FORMAT(' IRMIN=',I5,' IRMAX=',I5)
72      FORMAT(' RR(IRMIN=',E10.4,' RRNU(NU=',E10.4,' RR(IRMAX=',E10.4)

```

C  
C  
C

BLADE GEOMETRY AT RADIAL STATION OF INTEGRATION

```

      R=RRNU(IRNU)
      IF(R.LE.VGEOM(IDAT,1)) GO TO 201
      IDAT=IDAT+1
      IF(IDAT.GT.NDAT) IDAT=NDAT
201     DELTA=(V-VGEOM(IDAT,1))/(VGEOM(IDAT,1)-VGEOM(IDAT-1,1))
      DO 210 IX=2,3
210     XX(IX-1)=VGEOM(IDAT,IX)+DELTA*(VGEOM(IDAT,IX)-VGEOM(IDAT-1,IX))

```

C  
C

```

      B=XX(1)/2.
      THETA=XX(2)
      WRITE(21,7010) B,THETA,R
7010     FORMAT(' B=',E10.4,' THETA=',E10.4,' R=',E10.4)

```

C  
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```

      COSTHE=COS(THETA)
      SINTHE=SIN(THETA)

```

C  
C

```

      IF (IVOR.EQ.0) GO TO 4020

```

C  
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C  
C

INTERPOLATE TO GET MEAN CIRCUMFERENTIAL MACH NUMBERS AT THIS R

```

      IF (R.LE.VELOCV(IDOT,1)) GO TO 4001
      IDOT=IDOT+1
      IF (IDOT.GT.NVELO) IDOT=NVELO
4001     DELTA=(R-VELOCV(IDOT,1))/(VELOCV(IDOT,1)-VELOCV(IDOT-1,1))
      XVEL=VELOCV(IDOT,2)+DELTA*(VELOCV(IDOT,2)-VELOCV(IDOT-1,2))
      MTHETA=XVEL*MA

```

C  
C

```

4015     FORMAT(' R=',E10.4,' MTHETA=',E10.4)

```

C  
C

```

4020     CONTINUE

```

C  
C  
C  
C

MYM IS CIRCUMFERENTIAL MACH NUMBER OF WAKES IMPINGING ON STATOR

```

      MYM=MT*R-MA*MOV/R
      IF (IVOR.EQ.1) MYM=MT*R-MTHETA
      IF (IVOR.EQ.0) MTHETA=MA*MOV/R

```

C

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```
C CHI IS ARCTAN(CIRCUMFERENTIAL VELOCITY OF WAKE/AXIAL VELOCITY)
C CHI=ATAN2(MYM,MA)
C COSCHI=COS(CHI)
```

```
C ZMOD=SIGMAC*B*(GMNS*COSTHS-MM*SINTE/R)
```

```
C CHORDWISE INTEGRATION USES BESSEL INTEGRATION METHOD
```

```
C ---CALCULATE BESSEL WEIGHTING FUNCTIONS
```

```
C BESJ REQUIRES POSITIVE ARGUMENT
```

```
C X=ABS(ZMOD)
C CALL BESJ(X,0,BJ0,EB,ERROR1)
C CALL BESJ(X,NCHORD,BJ(NCHORD),EB,ERROR2)
C CALL BESJ(X,NCHORD-1,BJ(NCHORD-1),EB,ERROR3)
C ISERR=ERROR1+ERROR2+ERROR3
```

```
5400 FORMAT(' ZMOD=',E10.4,' ISERR=',I5)
C IF(ZMOD.GT.0.) GO TO 5040
```

```
C BJ0 IS EVEN FUNCTION, ADJUST SIGN ON OTHERS
C BJ(NCHORD)=BJ(NCHORD)*(-1)**NCHORD
C BJ(NCHORD-1)=BJ(NCHORD-1)*(-1)**(NCHORD-1)
```

```
5040 CONTINUE
```

```
C USE RECURSION RELATION TO COMPUTE AND STORE BESSEL FUNCTIONS
```

```
C DO 2000 N=NCHORD-1,2,-1
C BJ(N-1)=-BJ(N+1)+2.*N*BJ(N)/ZMOD
2000 CONTINUE
```

```
C INITIALIZE INTERPOLATION TO GET PRESSURE VALUE FOR THIS
C FREQUENCY AND RADIAL POSITION FROM STORED DATA
```

```
C USE 4 POINT BIVARIATE INTERPOLATION. SEE ABRAMOWITZ AND
C STEGUN 25.2.65
```

```
C NOTE QQ AND PP ARE LESS THAN 1
```

```
C DETERMINE FRACTIONAL PARTS OF FREQ. AND RADIAL SPACING
```

```
C PP=(RRNU(IRNU)-RR(IRMIN))/(RR(IRMAX)-RR(IRMIN))
C QQ=(OMEGA-NUPMIN)/(NUPMAX-NUPMIN)
```

```
C 912 FORMAT(' PP=',E10.4,' QQ=',E10.4)
```

```
C WMNS=(0.,0.)
```

```
C ***** BEGIN CHORDWISE INTEGRATION LOOP HERE *****
```

```
C DO 220 IZ=1,NCHORD ORIGINAL PAGE IS
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```

C COMPUTE R SUB S, THE WEIGHTING FUNCTION AT THE CHORDAL  
C STATION

C NOTE THAT Z=I\*\*IKOUNT BSLON

```
C
C      RRRS=(0.,0.)
C      Z=(1.,0.)
C      DO 5000 IKOUNT=0,NCHORD
C      BM=1.
C      IF (IKOUNT.EQ.0.OR.IKOUNT.EQ.NCHORD) BM=0.5
C      ARGU=IKOUNT*IZ*PI/NCHORD
C      IF (IKOUNT.GT.0) GO TO 5010
C      RRS=BM*Z*BJ0
C      GO TO 5020
```

```
5010 CONTINUE
      RRS=BM*Z*BJ(IKOUNT)*COS(ARGU)
```

```
5020 CONTINUE
      Z=Z*I
      RRRS=RRRS+RRS
```

```
5000 CONTINUE
```

```
C
C      RRRS=RRRS*2.*PI/NCHORD
C      BN=1.
C      IF (IZ.EQ.NCHORD) BN=0.5
```

C INTERPOLATE PRESSURE VALUES IN FREQUENCY AND RADIUS

```
C
C      MCOUNT=MUSE
C      Y=(1.-PP)*(1.-QQ)*CASCET(IZ,IRMIN,MCOUNT,IPMIN)
C      Y=Y+PP*(1.-QQ)*CASCET(IZ,IRMAX,MCOUNT,IPMIN)
C      Y=Y+QQ*(1.-PP)*CASCET(IZ,IRMIN,MCOUNT,IPMAX)
C      Y=Y+PP*QQ*CASCET(IZ,IRMAX,MCOUNT,IPMAX)
```

```
C
2   FORMAT(' CASCET=',2E10.4)
```

C EVALUATE FINITE CHORDWISE SUM TO APPROX. INTEGRAL

```
C
C      QMNST=Y*RRRS*BN
C      QMNS=QMNS+Y*RRRS*BN
5030 FORMAT(' IZ=',I5,' QMNST=',2E10.4)
220  CONTINUE
```

C \*\*\*\*\*END OF CHORDWISE INTEGRATION LOOP (220) \*\*\*\*\*

```
C
7022 FORMAT(' IRNU=',I3,' QMNS=',2E10.4)
```

```
C
C      ISUMR=ISUMR+ISERR
7021 CONTINUE
```

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C  
C

CA=MM\*COSTHE/R+GMNS\*SINHE  
CB=(CABS(LMNS)\*PSISTO(IRNU)\*CA\*B)\*\*2  
CD=((MT\*R)\*\*2+1.)\*.5

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FMNS=CB\*CD\*SUNTJT(MINDEX,IRNU)/(R\*\*2)/COSCHI

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C

WHTR=1.+SWTR/3.  
SWTR=-SWTR  
IF(IR.EQ.1.OR.IR.EQ.NRAD) WHTR=WHTR/2.

C  
C

PMNS=PMNS+WHTR\*FMNS\*DELTA/R  
7016 FORMAT(' PMNS SUM(R)=',E10.4)  
901 CONTINUE

C  
C

C\*\*\*\*\* END OF RADIAL INTEGRATION LOOP (901) \*\*\*\*\*

C  
C

CC=LR\*LIHETA\*LX\*(EPS#\*#WIDTH)\*\*2

C  
C

SMN=((BETASQ\*NBLADE\*NVANE)\*\*2)\*MT\*OMEGA\*PMNS/KMNS\*MA\*\*3  
SMN=SMN/(1.-SIGMAR\*\*2)/(OMEGA\*MT+XSIGN\*MA\*KMNS)\*\*2  
SMN=SMN\*CC\*SIGMAC\*SIGMAC\*(-XSIGN)/32./(PI\*\*4)

C  
C

MULTIPLY OUTPUT BY 2 (ADDS +3DB) TO ACCOUNT FOR ENERGY  
IN NEGATIVE FREQUENCY  
SMN=SMN\*2.

C  
C

RELPWR=SMN  
IPWR=1  
IF(RELPWR.EQ.0.) GO TO 915  
RELPR=10.\*ALJG10(ABS(RELPWR))  
GU TO 920  
915 IPWR=0  
920 CONTINUE

C  
C

IF(XSIGN.LT.0.) GO TO 9000

C  
C

WRITE(5,3000)

C  
C

```
3000  FORMAT('UPSTREAM ')
8101  FORMAT(' GAMMA M,N,SB =',E16.8)
      WRITE(21,8102) SMN
 8102  FORMAT(' REL. MODAL SOUND POWER SPECTRAL DENSITY=',E10.4)
      WRITE(21,8500) IER
      WRITE(21,5500) ISUMR
8500  FORMAT(' SUM OF ALL ERRORS IN PSI CALCULATIONS =',I5)
      IF(IP#R.EQ.0) GO TO 970
      WRITE(5,8600) RELPRL
      GO TO 980
 970   CONTINUE
      WRITE(5,952)
 980   CONTINUE
8600  FORMAT(' REL. SOUND POWER SPECTRAL DENSITY LEVEL (DB)=',E10.4)
      WRITE(21,7200)
 7200  FORMAT(' END OF UPSTREAM INTEGRATION')
      XSIGN=-1.
      SPWR(1)=RELPWR
      GO TO 111
```

```
C
C***** RETURN TO LINE 111 TO COMPUTE DOWNSTREAM PROPAGATION
C*****
```

```
C
9000  WRITE(5,8200)
8200  FORMAT('DOWNSTREAM')
8201  FORMAT(' GAMMA M,N,SB =',E16.8)
      WRITE(21,8202) SMN
 8202  FORMAT(' REL. MODAL SOUND POWER SPECTRAL DENSITY=',E10.4)
      WRITE(21,8400) IER
      WRITE(21,5500) ISUMR
 5500  FORMAT(' SUM OF ALL ERRORS IN RS CALCULATIONS=',I5)
8400  FORMAT(' SUM OF ALL ERRORS IN PSI CALCULATIONS =',I5)
      IF(IP#R.EQ.0) GO TO 950
      WRITE(5,8600) RELPRL
      GO TO 960
 950   CONTINUE
      WRITE(5,952)
 952   FORMAT(' SOUND POWER SPECTRAL DENSITY FOR MODE=0/UNEXCITED')
 960   CONTINUE
      SPWR(2)=RELPWR
      WRITE(21,7202)
 7202  FORMAT(' END OF DOWNSTREAM INTEGRATION')
      RETURN
      END
```

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**SUBROUTINE ANRT**

Program finds the roots of the  
boundary value equation for an  
annular duct.

**PRECEDING PAGE BLANK NOT FILMED**

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.....

SUBROUTINE ANRT(M,N,S,EB,EC,XMN,IEB,IEC)

(AN)NULAR FUNCTION (R)OJ(T)

PURPOSE  
 START WITH A GUESS SOLUTION FOR XM1  
 AND GET A BETTER VALUE FOR XM1.  
 GUESS EACH HIGHER ORDER ROOT FROM  
 $XM(N+1) = XMN+3.14159$   
 AND THEN REFINE IT TO GET THE (M,N)  
 ROOT TO :  $F=P(JS*Y-YS*J) = 0$

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.....

```

IF(M.EQ.0.AND.N.EQ.1) GO TO 6
XMN = M-3.14159
DO 5 NN=1,N
  DX = .31415
  IS = (-1)**(NN+1)
  X = XMN+3.14159
  J = 1

  CALL ANFU(M,X,S,EB,F,IEB)
  DX = -ISIG(F*IS)*DX
  TE = F

  IF (ABS(F) .LE. EC) GO TO 3
  IF (J .GT. 100) GO TO 2

  X = X+DX
  CALL ANFJ(M,X,S,EB,F,IEB)

  IF ((F*TE) .LT. 0.) DX = -DX/2.
  J = J+1
  TE = F
  GO TO 1

2 IEC = 1
  GO TO 4
3 IEC = 0
4 XMN = X
5 CONTINUE
RETURN
6 CONTINUE
IEB=0
IEC=0
XMN=0.
RETURN
END
    
```

(+)

C  
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C  
C  
C

.....

SUBROUTINE ANFU(M,X,S,EB,F,IEB)

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(AN)NULAR (?U)NCTION

PURPOSE

EVALUATE THE DETERMINANT  $F = P(JS*Y - YS*J)$

.....

IF (M .NE. 0) GO TO 1  
CALL BESJ( X,1,ZJ ,EB ,IE3)  
CALL BESJ(S\*X,1,ZJS ,Eb ,IE4)  
CALL BESY( X,1,ZY , IE7)  
CALL BESY(S\*X,1,ZYS , IE8)  
IEB = IE3+IE4+IE7+IE8  
GO TO 2

C

1

CALL BESJ( X,M-1,BJM ,EB ,IE1)  
CALL BESJ(S\*X,M-1,BJMS,EB ,IE2)  
CALL BESJ( X,M+1,BJP ,EB ,IE3)  
CALL BESJ(S\*X,M+1,BJPS,EB ,IE4)  
ZJ = .5\*(BJM -BJP )  
ZJS = .5\*(BJMS-BJPS)  
CALL BESY( X,M-1,BYM , IE5)  
CALL BESY(S\*X,M-1,BYMS, IE6)  
CALL BESY( X,M+1,BYP , IE7)  
CALL BESY(S\*X,M+1,BYPS, IE8)  
ZY = .5\*(BYM -BYP )  
ZYS = .5\*(BYMS-BYPS)  
IEB = IE1+IE2+IE3+IE4+IE5+IE6+IE7+IE8

C

2

F = ZJS\*ZY - ZJ\*ZYS  
RETURN  
END

~L

.....  
SUBROUTINE BESJ

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PURPOSE

COMPUTE THE J BESSEL FUNCTION FOR A GIVEN ARGUMENT AND ORDER

USAGE

CALL BESJ(X,N,BJ,D,IER)

DESCRIPTION OF PARAMETERS

X -THE ARGUMENT OF THE J BESSEL FUNCTION DESIRED

N -THE ORDER OF THE J BESSEL FUNCTION DESIRED

BJ -THE RESULTANT J BESSEL FUNCTION

D -REQUIRED ACCURACY

IER-RESULTANT ERROR CODE WHERE

IER=0 NO ERROR

IER=1 N IS NEGATIVE

IER=2 X IS NEGATIVE OR ZERO

IER=3 REQUIRED ACCURACY NOT OBTAINED

IER=4 RANGE OF N COMPARED TO X NOT CORRECT (SEE REMARKS)

REMARKS

N MUST BE GREATER THAN OR EQUAL TO ZERO, BUT IT MUST BE  
LESS THAN

$20+10*X-X**2/3$  FOR X LESS THAN OR EQUAL TO 15

$90*X/2$  FOR X GREATER THAN 15

SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED

NONE

METHOD

RECURRENCE RELATION TECHNIQUE DESCRIBED BY H. GOLDSTEIN AND  
R.M. THALER, "RECURRENCE TECHNIQUES FOR THE CALCULATION OF  
BESSEL FUNCTIONS", M.T.A.C., V.13, PP.102-108 AND I.A. STEGUN  
AND M. ABRAMOWITZ, "GENERATION OF BESSEL FUNCTIONS ON HIGH  
SPEED COMPUTERS", M.T.A.C., V.11, 1957, PP.255-257

.....  
SUBROUTINE BESJ(X,N,BJ,D,IER)

BJ=.0

IF (X .NE. 0.) GO TO 9

IER = 0

IF (N .EQ. 0) BJ = 1.

RETURN



C

```
9      IF(N)10,20,20
10     IER=1
      RETURN
20     IF(X)30,30,31
30     IER=2
      RETURN
31     IF(X-15.)32,32,34
32     NTEST=20.+10.*X-X** 2/3
      GO TO 36
34     NTEST=90.+X/2.
36     IF(N-NTEST)40,38,38
38     IER=4
      RETURN
40     IER=0
      N1=N+1
      MPREV=.0
```

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```
      COMPUTE STARTING VALUE OF M
50     IF(X-5.)50,50,60
      MA=X+6.
      GO TO 70
60     MA=1.4*X+60./X
70     MB=N+IFIX(X)/4+2
      MZERO=MAX0(MA,MB)
```

C  
C  
C

```
      SET UPPER LIMIT OF M
100    DO 190 M=MZERO,MAX,3
```

C  
C  
C

```
      SET F(M),F(M-1)
      FM1=1.0E-28
      FM=.0
      ALPHA=.0
      IF(M-(M/2)*2)120,110,120
110    JT=-1
      GO TO 130
120    JT=1
130    M2=M-2
      DO 160 K=1,M2
      MK=M-K
      BMK=2.*FLOAT(MK)*FM1/X-FM
      FM=FM1
      FM1=BMK
      IF(MK-N-1)150,140,150
140    BJ=BMK
150    JT=-JT
      S=1+JT
```

160 ALPHA=ALPHA+BMK\*S  
BMK=2.\*FM1/X-FM  
IF(N)180,170,180  
170 BJ=BMK  
180 ALPHA=ALPHA+BMK  
BJ=BJ/ALPHA  
IF(ABS(BJ-BPREV)-ABS(D\*BJ))200,200,190  
190 BPREV=BJ  
IER=3  
200 RETURN  
END

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COMPUTE Y0 AND Y1 FOR X GREATER THAN 4

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```

30 T1=4.0/X
   T2=T1*T1
   P0=((((-0.0000037043*T2+.0000173565)*T2-.0000487613)*T2
1   +.00017343)*T2-.001753062)*T2+.3989423
   Q0=((((-0.0000032312*T2-.0000142070)*T2+.0000342468)*T2
1   -.00000869791)*T2+.0004564324)*T2-.01246594
   P1=((((-0.0000042414*T2-.0000200920)*T2+.0000580759)*T2
1   -.000223203)*T2+.002921825)*T2+.3989423
   Q1=((((-0.0000035594*T2+.000016222)*T2-.0000398708)*T2
1   +.0001064741)*T2-.0005390400)*T2+.03740084
   A=2.0/SQRT(X)
   B=A*T1
   C=X-.7853982
   Y0=A*P0*SIN(C)+B*Q0*COS(C)
   Y1=-A*P1*COS(C)+B*Q1*SIN(C)
   GO TO 90

```

COMPUTE Y0 AND Y1 FOR X LESS THAN OR EQUAL TO 4

```

40 XX=X/2.
   X2=XX*XX
   T=ALOG(XX)+.5772157
   SUM=0.
   TERM=T
   Y0=T
   DO 70 L=1,15
   IF( (-1)5L,60,50
50 SUM=SUM+1./FLOAT(L-1)
60 FL=L
   TS=T-SUM
   TERM=(TERM*(-X2)/FL**2)*(1.-1./(FL*TS))
70 Y0=Y0+TERM
   TERM = XX*(T-.5)
   SUM=0.
   Y1=TERM
   DO 80 L=2,16
   SUM=SUM+1./FLOAT(L-1)
   FL=L
   FL1=FL-1.
   TS=T-SUM
   TERM=(TERM*(-X2)/(FL1*FL))*((TS-.5/FL)/(TS+.5/FL1))
80 Y1=Y1+TERM
   PI2=.6366198
   Y0=PI2*Y0
   Y1=-PI2/X+PI2*Y1

```

CHECK IF ONLY Y0 OR Y1 IS DESIRED

```

90 IF(N-1)100,100,130

```

C  
C  
C RETURN EITHER Y0 OR Y1 AS REQUIRED

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100 IF(N)110,120,110  
110 BY=Y1  
GO TO 170  
120 BY=Y0  
GO TO 170

C  
C  
C PERFORM RECURRENCE OPERATIONS TO FIND YN(X)

130 YA=Y0  
YB=Y1  
K=1  
140 T=FLOAT(2\*K)/X  
YC=T\*YB-YA  
IF(ABS(YC)-1.7E33)145,145,141  
141 IER=3  
RETURN  
145 K=K+1  
IF(K-N)150,160,150  
150 YA=YB  
YB=YC  
GO TO 140  
160 BY=YC  
170 RETURN  
180 IER=1  
RETURN  
190 IER=2  
RETURN  
END

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SUBROUTINE CASC

Program computes the complex  
pressure distribution across  
a blade chord for incident  
turbulence.

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(\*)

SUBROUTINE EIGEN

Program computes the weighting  
factors for the eigen functions  
(mode shapes).

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```

SUBROUTINE EIGEN(MM,STGMAR,XMN,MMN,BMN,D,IER)
DIMENSION IER(8)
IF(MMN.EQ.0.) GO TO 22
N=MM
IF(M.LT.0) N=-N
MMINUS=IABS(N-1)
MPLUS=N+1
XMHUB=XML*SIGMAR
S=STGMAR**2
CALL PESJ (XMM,N,BJM,D,IER(1))
CALL PESY (XMM,N,BYM,IER(2))
CALL PESJ (XMHUB,N,BJMH,D,IER(3))
CALL PESY (XMHUB,N,BYMH,IER(4))
CALL PESJ (XMM,MPLUS,BJMP,D,IER(5))
CALL PESY (XMM,MPLUS,BYMP,IER(6))
CALL PESJ (XMM,MMINUS,BJMM,D,IER(7))
CALL PESY (XMM,MMINUS,BYMM,IER(8))
IF(M.GT.0) GO TO 100
BJMV=-BJMV
BYMV=-BYMV
100 BJPRIM=(BJMV-BJMP)/2.
BYPRIM=(BYMV-BYMP)/2.
IF(ABS(BJPRIM).LT.ABS(BYPRIM)) GO TO 10
AMN=-BYPRIM/BJPRIM
BMN=1.
GO TO 20
10 AMN=1.
BMN=-BJPRIM/BYPRIM
20 PART1=(1.-(MM/XMN)**2)*(AMN*BJM+BMN*BYM)**2/(1.-S)
PART2=(S-(MM/YMN)**2)*(AMN*BJMH+BMN*BYMH)**2/(1.-S)
FACTOR=(PART1-PART2)**.5
AMN=AMN/FACTOR
BMN=BYM/FACTOR
RETURN
22 CONTINUE
AMN=1.
BMN=0.
DO 24 J=1,8
24 IFR(J)=0
RETURN
END

```

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SUBROUTINE EPSD

Program yields the inlet RMS  
turbulence intensity.

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(4)

SUBROUTINE FHAT

Program computes the Fourier  
transform of the spatial  
distribution of wake turbulence.

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## FUNCTION FHAT(FARG)

C  
C FUNCTION YIELDS THE FOURIER TRANSFORM OF THE SPATIAL  
C DISTRIBUTION OF WAKE TURBULENCE VELOCITY FOR  
C SUBROUTINE OUTURD  
C

DATA PI/3.14159/

C  
C NEED SWITCH TO AVOID UNDERFLOW ON EXPONENTIATION :  
C RANGE IS E+-38.  
C

A=(FARG\*\*2)/4./PI  
IF(A.GT.87.) GO TO 10  
B=EXP(-A)  
GO TO 20  
10 B=0.  
20 CONTINUE  
FHAT=B  
RETURN  
END

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SUBROUTINE KERNEL

Program computes the kernel  
of the Green's function.

```

SUBROUTINE KERNEL(X,K,GAMMA,MR,H1,H2,ERROR,CKF)
REAL K,MR
COMPLEX I,CKF,AN,ANP,ANM,RN,RJOT
RN(AN)=BETAR**2*H2/(2.*D**2)*(AN**2-K**2)*CEXP(I*(AN+K*MR)
1 *X)/((AN-GN*H1/D**2)*(AN+K/MR))
DATA I/(0.,1.)/,PI/3.14159/,XMIN/.001/
BETAR=SQRT(1.-MR**2)
IF(ABS(X).GT.XMIN) GO TO 10
CKF=BETAR/(2.*PI)*CEXP(-I*BETAR**2*K*X/MR)*(1./X-I*K/MR
1 *ALOG(ABS(X)))
RETURN
10 CONTINUE
D=SQRT(H1**2+(BETAR*H2)**2)
R=D*SQRT(K**2+(D*ALOG(ERROR)/(BETAR*H2*X))**2)
N1=(GAMMA-R)/(2.*PI)
N2=(GAMMA+R)/(2.*PI)
CKF=0.
IF(X.GT.0.) GO TO 50
DO 40 N=N1,N2
GN=GAMMA-2.*PI*N
S=(K*D)**2-GN**2
IF(S.GE.0.) RJOT=-SQRT(S)*ABS(K)/K
IF(S.LT.0.) RJOT=I*SQRT(-S)
ANM=(GN*H1-BETAR*H2*RJOT)/D**2
CKF=CKF+RN(ANM)
40 CONTINUE
RETURN
50 CONTINUE
DO 70 N=N1,N2
GN=GAMMA-2.*PI*N
S=(K*D)**2-GN**2
IF(S.GE.0.) RJOT=-SQRT(S)*ABS(K)/K
IF(S.LT.0.) RJOT=I*SQRT(-S)
ANP=(GN*H1+BETAR*H2*RJOT)/D**2
CKF=CKF-RN(ANP)
70 CONTINUE
CKF=CKF-BETAR**2*K/(2.*MR)*SINH(BETAR**2*K
1 *H2/MR)*CEXP(-I*BETAR**2*K*X/MR)/(COSH(BETAR**2*K*H2/MR)-
2 COS(GAMMA+K*H1/MR))
RETURN
END

```

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SUBROUTINE PHITHH

Program computes the Fourier  
transform of the correlation  
function in the circumferential  
direction.

FUNCTION PHITHH(ARGUM2)

C  
C  
C PROGRAM CALCULATES THE FOURIER TRANSFORM OF THE CORRELATION  
C FUNCTION IN THE AZIMUTHAL DIRECTION AS A FUNCTION OF  
C  
C  
C 12/14/79 VERSION USES GAUSSIAN AUTOCORRELATION FUNCTION.  
C FORM FOLLOWS EQUATION 27 IN W.D. MARK'S "ROTOR INLET  
C TURBULENCE" PAGE 10.  
C

DATA PI/3.14159/

C  
C NEED SWITCH TO AVOID UNDERFLOW IN EXPONENTIATION. RANGE  
C IS E+-38.  
C

A=ARGUM2\*\*2  
B=A/PI  
IF(B.GT.87.) GO TO 10  
C=2.\*\*EXP(-B)  
GO TO 20  
10 C=0.  
20 CONTINUE  
PHITHH=C  
RETURN  
END

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SUBROUTINE PHIXHT

Program calculates the Fourier  
transform of the correlation  
function in the axial direction.



FUNCTION PHIXHT(ARGUM1)

C  
C PROGRAM CALCULATES THE FOURIER TRANSFORM OF THE CORRELATION  
C FUNCTION IN THE AXIAL DIRECTION AS A FUNCTION OF  
C NONDIMENSIONAL FREQUENCY

C  
C 12/14/79 VERSION USES GAUSSIAN AUTOCORRELATION FUNCTION.  
C FORM FOLLOWS EQUATION 27 IN W.D. MARK'S "ROTOR INLET  
C TURBULENCE" PAGE 17.

C  
C NEED SWITCH TO AVOID UNDERFLOW ON EXPONENTIATION. RANGE  
C IS E+-38  
C

DATA PI/3.14159/  
A=ARGUM1\*\*2  
B=A/PI  
IF(B.GT.87.) GO TO 10  
C=2.\*EXP(-B)  
GO TO 20  
10 C=0.  
20 CONTINUE  
PHIXHT=C  
RETURN  
END

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(+)

(+)

SUBROUTINE PRES

Program generates the complex  
pressure distribution across  
the stator vane chord.

```
SUBROUTINE PRES(WH,X,K,GAMMA,MR,H1,H2,MSEG,F,IER)
REAL K,MR,KX
COMPLEX I,WH,F,A,CKF
COMPLEX G,G0,G1,G2,G3
DIMENSION F(100),A(100,100),WA(100),B(100)
DATA I/(0.,1.)/,ERROR/.0001/,PI/3.14159/
DATA (B(J),J=1,100)/100*1.3/
G(X)=(G0+G1*X+G2*X**2+G3*X**3)*CEXP(I*K*MR*X)
B(MSEG)=.5
BPTAR=SQRT(1.-MR**2)
G0=I*BPTAR*K/(2.*PI*MR)
G1=BPTAR*K**2/(2.*PI)*(1./MR**2-0.5)
G2=I*BPTAR*K**3/(4.*PI)*(1./(2.*MR)-1./MR**3)
G3=-BPTAR*K**4/(12.*PI)*(1./MR**4-1./(2.*MR**2)-0.125)
DO 10 M=1,MSEG
X=COS((M-.5)*PI/MSEG)
F(M)=WH*CEXP(I*KX*X)
10 CONTINUE
N=MSEG
DO 50 M=1,N
DO 50 L=1,N
S=-ALOG(2.)
DO 40 IR=1,N
S=S-2.*B(IR)/IR*COS((M-.5)*IR*PI/N)*COS(PI*IR*L/N)
40 CONTINUE
ARG=COS((M-.5)*PI/N)-COS(L*PI/N)
CALL KERNEL(ARG,K,GAMMA,MR,H1,H2,ERROR,CKF)
A(M,L)=P(L)*(CKF+G(ARG)*(S-ALOG(ABS(ARG))))*PI/N
50 CONTINUE
CALL LEQ1IC(A,MSEG,100,F,1,100,B,WA,IER)
RETURN
END
```

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SUBROUTINE RMODE

Program computes the radial  
mode shape for an annular  
duct.

Subroutine RMODE (M4,X,AMN,BMN,PSI,D,IERROR)  
DIMENSION IERROR(2)  
IF(X.EQ.0.) GO TO 300  
FACTOR=1.  
M=M4  
IF(M.LT.1) GO TO 100  
200 CONTINUE  
CALL BESJ (X,M,BJ,D,IERROR(1))  
CALL BESY (X,M,BY,IERROR(2))  
PSI=FACTOR\*(AMN\*BJ+BMN\*BY)  
RETURN  
102 M=-M  
K=M/2  
IF((1.\*M)/(2.).GT.(1.\*K)) FACTOR=-1.  
GO TO 200  
300 CONTINUE  
PSI=AMN  
IERROR(1)=0  
IERROR(2)=0  
RETURN  
END

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SUBROUTINE SCALLR

Program yields the turbulence  
length scale in the radial  
direction.

FUNCTION SCALLP(R)

C  
C PROGRAM CALCULATES THE INLET TURBULENCE LENGTH  
C SCALE IN THE RADIAL DIRECTION AS A FUNCTION OF THE MEAN RADIUS.  
C THE LENGTH SCALE IS NONDIMENSIONALIZED ON THE DUCT RADIUS.  
C NOTE SIGMA.R.LE.R.LE.1.

C  
C 12/21/79 VERSION USES A CONSTANT

R=0.50  
SCALLR=B  
RETURN  
END

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SUBROUTINE SCALLX

Program yields the turbulence  
length scale in the axial  
direction.



FUNCTION SCALLY(R)

C  
C PROGRAM CALCULATES THE INLET TURBULENCE LENGTH SCALE  
C IN THE AXIAL DIRECTION AS A FUNCTION OF THE MEAN RADIUS.  
C LENGTH SCALE IS NONDIMENSIONALIZED ON THE DUCT RADIUS.

C  
C 12/18/79 VERSTON USES A CONSTANT  
C NOTE SIGMAF.LE.R.LE.1.

R=40.  
SCALLX=8  
RETURN  
END

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SUBROUTINE STHETA

Program yields the turbulence  
length scale in the circumfer-  
ential direction.

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FUNCTION STHETA(R)

C  
C PROGRAM CALCULATES THE INLET TURBULENCE LENGTH SCALE  
C IN THE AZIMUTHAL DIRECTION AS A FUNCTION OF MEAN RADIUS.  
C THE LENGTH SCALE IS NON-DIMENSIONALIZED ON THE DUCT RADIUS.

C DATA PI/3.14159/

C  
C 12/18/79 VERSION USES A CONSTANT  
C NOTE SIGMA R.LE.R.LF.1.

B=0.5  
STHETA=B  
RETURN  
END

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PROGRAM MAPIN/  
SUBROUTINE MAPPER  
(with sample execution)

Program lists which duct modes  
will propagate for inlet turbu-  
lence noise.

DIMENSION RDATA(20)  
REAL MT,MA

C  
C  
C  
C INPUT VARIABLES TO SUBROUTINE MAPPER FOR LISTING OF ALL  
C PROPAGATING MODES FOR TURBULENCE PROGRAMS AT A  
C GIVEN FREQUENCY

C  
1001 FORMAT(G20.8)  
WRITE(5,2003)  
2003 FORMAT(' HUB RADIUS DIVIDED BY DUCT RADIUS =')  
READ(5,1001) SIGMAR  
WRITE(5,2103) SIGMAR  
2103 FORMAT(' SIGMAR=',E16.8)

C  
C  
WRITE(5,2030)  
2030 FORMAT(' MT =')  
READ(5,1001) MT  
WRITE(5,2130) MT  
2130 FORMAT(' MT=',E16.8)  
WRITE(5,2031)  
2031 FORMAT(' MA =')  
READ(5,1001) MA  
WRITE(5,2131) MA  
2131 FORMAT(' MA =',E16.8)  
WRITE(5,2037)  
2037 FORMAT(' ACCURACY OF BESSEL FN =')  
READ(5,1001) EB  
WRITE(5,2137) EB  
2137 FORMAT(' EB=',E16.8)  
WRITE(5,2038)  
2038 FORMAT(' ACCURACY OF CONVERGENCE TO ROOT XMN =')  
READ(5,1001) EC  
WRITE(5,2138) EC  
2138 FORMAT(' EC=',E16.8)

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C  
C  
C  
C  
RDATA(1)=MT  
RDATA(2)=MA  
RDATA(9)=EB  
RDATA(10)=EC

C  
C  
C  
C  
RDATA(5)=SIGMAR

CALL MAPPER(RDATA)  
STOP  
END

SUBROUTINE MAPPER(RDATA)  
DIMENSION IER(3),RDATA(20)  
REAL MT,MA

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C  
C  
C  
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C  
C  
C  
C  
C  
C  
C  
C  
C  
C  
C

PROGRAM LISTS ALL PROPAGATING MODES FOR INLET AND WAKE  
TURBULENCE PROGRAMS WITHOUT CALCULATING MODAL  
AMPLITUDES. USE THIS PROGRAM AS A PRECURSOR TO  
INTURB OR WATURB SEARCH ROUTINES TO ESTIMATE RUN TIME.

1001 FORMAT(G20.8)  
WRITE(5,110)  
110 FORMAT(' NOISE FREQUENCY/SHAFT FREQUENCY=')  
READ(5,1001) OMEGA  
RDATA(8)=OMEGA  
115 FORMAT(' OMEGA=',E10.4)  
WRITE(5,115) RDATA(8)  
MT=RDATA(1)  
MA=RDATA(2)  
SIGMAR=RDATA(5)  
EB=RDATA(9)  
EC=RDATA(10)

XMAX=OMEGA\*MT/(1.-MA\*\*2)\*\*.5

C  
C  
C  
C

WRITE(5,2001) XMAX  
2001 FORMAT(' XMN(XAX) FOR PROPAGATION =',E16.8)

C  
C  
C  
C  
C  
C  
C  
C

START WITH PLANE WAVE MODE (0,1). COUNT UP IN N, THEN M  
UNTIL ALL POSSIBLE HIGHER MODES ARE CUT OFF.

J=1  
M=0

C  
C  
C  
C  
C  
C  
C  
C  
C

RESTART N COUNT HERE FOR NEW M

N=0

C INCREMENT N

C  
20

N=N+1

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C  
C

MABS=IABS(M)

C  
C  
C

CALL ANRT (MABS,N,SIGMAR,EB,EC,XMN,IEB,IEC)

C  
C  
C  
C  
C

IF MODE IS CUT OFF GO TO 6000

C  
C

IF(XMN.GE.XMAX) GO TO 6000

C  
C

WRITE(5,3000)

3000

FORMAT('MODE DATA')

WRITE(5,3001) OMEGA,M,N,XMN

3001

FORMAT('OMEGA=',E10.4,' M=',I3,' N=',I3,' XMN=',E10.4)

IF(XMN.EQ.0.) GO TO 1000

COFFRA=XMAX/XMN

WRITE(5,4000) COFFRA

4000

FORMAT('CUTOFF RATIO FOR MODE=',E10.4)

GO TO 1005

1000

CONTINUE

WRITE(5,4005)

4005

FORMAT('PLANE WAVE MODE: CUTOFF RATIO IS + INFINITE')

1005

CONTINUE

WRITE(5,3002) IEB

3002

FORMAT('SUM OF BESSEL FUNCTION ERROR CODES =',I3)

WRITE(5,3003) IEC

3003

FORMAT('ERROR CODE FOR CONVERGENCE TO ROOT XMN =',I3)

C

NORMALIZE MODE AMPLITUDE

C

CALL EIGEN (MABS,SIGMAR,XMN,AMN,BMN,EB,IER)

C  
C

WRITE(5,3004) AMN,BMN

3004

FORMAT('AMN =',E16.8,' BMN =',E16.8)

WRITE(5,3005) IER

3005

FORMAT('ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC =',I2)

C  
C  
C  
C  
C  
C

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C  
C

MMM=M

C  
C

DO NOT SWITCH SIGN ON M IF M=0

C  
C

IF(M.EQ.0) GO TO 20

C  
C

MMM=-MMM

C  
C

WRITE(5,8300) MMM,N,RDATA(8)

8300 FORMAT('JM=',I3,' N=',I3,' OMEGA=',E10.4)

C  
C

SWITCH SIGN ON M

C  
C

C  
C

C  
C

GO TO 20

C  
C

C  
C

C  
C

IF MODE IS CUTOFF, DECIDE WHICH MODE TO TRY NEXT.

C  
C

C  
C

6000 IF(N.EQ.1) GO TO 7000

C  
C

NMAX=N-1

WRITE(5,6001) NMAX

C  
C

C  
C

J=J+1

C  
C

C  
C

INCREMENT M

M=M+1

GO TO 15

C  
C

C  
C

N=1 TO REACH THIS POINT

C  
C

C  
C

WRITE(5,7001)

C  
C

C  
C

7001 FORMAT(' NO MORE PROPAGATING MODES FOR THIS OMEGA')

CONTINUE

WRITE(5,9001)

C  
C

9001 FORMAT(' PROBLEM COMPLETED')

RETURN

END



Sample Execution of MAPIN/MAPPER

@MAPPER  
HUB RADIUS DIVIDED BY DUCT RADIUS =  
.484  
SIGMAR= 0.48400000E+00  
MT =  
.508  
MT= 0.50800000E+00  
MA =  
.323  
MA = 0.32300000E+00  
ACCURACY OF BESSEL FN =  
.0001  
EB= 0.10000000E-03  
ACCURACY OF CONVERGENCE TO ROOT XMN =  
.0001  
EC= 0.10000000E-03  
NOISE FREQUENCY/SHAFT FREQUENCY=  
15.  
OMEGA= .1500E+02  
XMN(MAX) FOR PROPAGATION = 0.80515728E+01

MODE DATA

OMEGA= .1500E+02 M= 0 N= 1 XMN= .0000E+00  
PLANE WAVE MODE: CUTOFF RATIO IS + INFINITE  
SUM OF BESSEL FUNCTION ERROR CODES = 0  
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0  
AMN = 0.10000000E+01 BMN = 0.00000000E+00  
ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

MODE DATA

OMEGA= .1500E+02 M= 0 N= 2 XMN= .6205E+01  
CUTOFF RATIO FOR MODE= .1298E+01  
SUM OF BESSEL FUNCTION ERROR CODES = 0  
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0  
AMN = -0.26166472E+01 BMN = 0.27171760E+01  
ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

LARGEST PROPAGATING N FOR THIS M = 2

%FRSAPR Floating underflow PC= 3100

%FRSAPR Floating underflow PC= 3146

ORIGINAL PAGE 13  
OF FOUR QUALITY

MODE DATA

OMEGA= .1500E+02 M= 1 N= 1 XMN= .1371E+01  
CUTOFF RATIO FOR MODE= .5873E+01  
SUM OF BESSEL FUNCTION ERROR CODES = 0  
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0  
AMN = 0.15152306E+01 BMN = -0.42119467E+00  
ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M= -1 N= 1 OMEGA= .1500E+02

MODE DATA

OMEGA= .1500E+02 M= 1 N= 2 XMN= .6390E+01  
CUTOFF RATIO FOR MODE= .1260E+01  
SUM OF BESSEL FUNCTION ERROR CODES = 0  
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0  
AMN = 0.14356938E+01 BMN = 0.32269858E+01  
ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M= -1 N= 2 OMEGA= .1500E+02

LARGEST PROPAGATING N FOR THIS M = 2

MODE DATA

OMEGA= .1500E+02 M= 2 N= 1 XMN= .2708E+01  
CUTOFF RATIO FOR MODE= .2973E+01  
SUM OF BESSEL FUNCTION ERROR CODES = 0  
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0  
AMN = 0.20525722E+01 BMN = -0.42471320E+00  
ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M= -2 N= 1 OMEGA= .1500E+02

MODE DATA

OMEGA= .1500E+02 M= 2 N= 2 XMN= .6920E+01  
CUTOFF RATIO FOR MODE= .1164E+01  
SUM OF BESSEL FUNCTION ERROR CODES = 0  
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0  
AMN = 0.36560636E+01 BMN = 0.74837045E+00  
ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

ORIGINAL PAGE IS  
OF POOR QUALITY

M= -2 N= 2 OMEGA= .1500E+02

LARGEST PROPAGATING N FOR THIS M = 2

MODE DATA

OMEGA= .1500E+02 M= 3 N= 1 XMN= .3987E+01  
CUTOFF RATIO FOR MODE= .2020E+01  
SUM OF BESSEL FUNCTION ERROR CODES = 0  
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0  
AMN = 0.26023450E+01 BNN = -0.32589376E+00  
ERROR CODE FOR BESSEL FNS IN AMN AND BNN CALC = 0 0 0 0 0 0 0 0

M= -3 N= 1 OMEGA= .1500E+02

MODE DATA

OMEGA= .1500E+02 M= 3 N= 2 XMN= .7747E+01  
CUTOFF RATIO FOR MODE= .1039E+01  
SUM OF BESSEL FUNCTION ERROR CODES = 0  
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0  
AMN = 0.35705322E+01 BNN = -0.89511162E+00  
ERROR CODE FOR BESSEL FNS IN AMN AND BNN CALC = 0 0 0 0 0 0 0 0

M= -3 N= 2 OMEGA= .1500E+02

LARGEST PROPAGATING N FOR THIS M = 2

MODE DATA

OMEGA= .1500E+02 M= 4 N= 1 XMN= .5200E+01  
CUTOFF RATIO FOR MODE= .1549E+01  
SUM OF BESSEL FUNCTION ERROR CODES = 0  
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0  
AMN = 0.31336392E+01 BNN = -0.20930877E+00  
ERROR CODE FOR BESSEL FNS IN AMN AND BNN CALC = 0 0 0 0 0 0 0 0

M= -4 N= 1 OMEGA= .1500E+02

LARGEST PROPAGATING N FOR THIS M = 1

C-3

ORIGINAL PAGE IS  
OF POOR QUALITY

MODE DATA

OMEGA= .1500E+02 M= 5 N= 1 XMN= .6355E+01  
CUTOFF RATIO FOR MODE= .1267E+01  
SUM OF BESSEL FUNCTION ERROR CODES = 0  
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0  
AMN = 0.36182370E+01 BMN = -0.11930907E+00  
ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M= -5 N= 1 OMEGA= .1500E+02

LARGEST PROPAGATING N FOR THIS M = 1

MODE DATA

OMEGA= .1500E+02 M= 6 N= 1 XMN= .7473E+01  
CUTOFF RATIO FOR MODE= .1077E+01  
SUM OF BESSEL FUNCTION ERROR CODES = 0  
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0  
AMN = 0.40542452E+01 BMN = -0.61590101E-01  
ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M= -6 N= 1 OMEGA= .1500E+02

LARGEST PROPAGATING N FOR THIS M = 1  
NO MORE PROPAGATING MODES FOR THIS OMEGA  
PROBLEM COMPLETED  
STOP

END OF EXECUTION

CPU TIME: 29.82 ELAPSED TIME: 3:4.03

EXIT.

^C

@MAPPER

HUB RADIUS DIVIDED BY DUCT RADIUS =

.484

SIGMAR= 0.48400000E+00

MT =

.508

MT= 0.50800000E+00

MA =

.323

MA = 0.32300000E+00

ACCURACY OF BESSEL FN =

.0001

EB= 0.10000000E-03

ORIGINAL PAGE  
OF POOR QUALITY

ACCURACY OF CONVERGENCE TO ROOT XMN =  
.0001  
EC= 0.10000000E-03  
NOISE FREQUENCY/SHAFT FREQUENCY=  
30.  
OMEGA= .3000E+02  
XMN(MAX) FOR PROPAGATION = 0.16103146E+02

MODE DATA

OMEGA= .3000E+02 M= 0 N= 1 XMN= .0000E+00  
PLANE WAVE MODE: CUTOFF RATIO IS + INFINITE  
SUM OF BESSEL FUNCTION ERROR CODES = 0  
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0  
AMN = 0.10000000E+01 BMN = 0.00000000E+00  
ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

MODE DATA

OMEGA= .3000E+02 M= 0 N= 2 XMN= .6205E+01  
CUTOFF RATIO FOR MODE= .2595E+01  
SUM OF BESSEL FUNCTION ERROR CODES = 0  
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0  
AMN = -0.26166472E+01 BMN = 0.27171760E+01  
ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

MODE DATA

OMEGA= .3000E+02 M= 0 N= 3 XMN= .1224E+02  
CUTOFF RATIO FOR MODE= .1316E+01  
SUM OF BESSEL FUNCTION ERROR CODES = 0  
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0  
AMN = -0.24929737E+01 BMN = 0.47091179E+01  
ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

LARGEST PROPAGATING N FOR THIS M = 3  
ZFRSAPR Floating underflow PC= 3100

ZFRSAPR Floating underflow PC= 3146

MODE DATA

OMEGA= .3000E+02 M= 1 N= 1 XMN= .1371E+01  
CUTOFF RATIO FOR MODE= .1175E+02  
SUM OF BESSEL FUNCTION ERROR CODES = 0

ORIGINAL PAGE 15  
OF PCOR QUALITY

ERROR CODE FOR CONVERGENCE TO ROOT X<sub>MN</sub> = 0  
AMN = 0.15152306E+01    BMN = -0.42119467E+00  
ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M= -1    N= 1    OMEGA= .3000E+02

MODE DATA

OMEGA= .3000E+02    M= 1    N= 2    X<sub>MN</sub>= .6390E+01  
CUTOFF RATIO FOR MODE= .2520E+01  
SUM OF BESSEL FUNCTION ERROR CODES = 0  
ERROR CODE FOR CONVERGENCE TO ROOT X<sub>MN</sub> = 0  
AMN = 0.19356938E+01    BMN = 0.32269858E+01  
ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M= -1    N= 2    OMEGA= .3000E+02

MODE DATA

OMEGA= .3000E+02    M= 1    N= 3    X<sub>MN</sub>= .1232E+02  
CUTOFF RATIO FOR MODE= .1307E+01  
SUM OF BESSEL FUNCTION ERROR CODES = 0  
ERROR CODE FOR CONVERGENCE TO ROOT X<sub>MN</sub> = 0  
AMN = 0.43514410E+01    BMN = 0.30726765E+01  
ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M= -1    N= 3    OMEGA= .3000E+02

LARGEST PROPAGATING N FOR THIS M = 3

MODE DATA

OMEGA= .3000E+02    M= 2    N= 1    X<sub>MN</sub>= .2708E+01  
CUTOFF RATIO FOR MODE= .5946E+01  
SUM OF BESSEL FUNCTION ERROR CODES = 0  
ERROR CODE FOR CONVERGENCE TO ROOT X<sub>MN</sub> = 0  
AMN = 0.20525722E+01    BMN = -0.42471320E+00  
ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M= -2    N= 1    OMEGA= .3000E+02

MODE DATA

OMEGA= .3000E+02    M= 2    N= 2    X<sub>MN</sub>= .6920E+01  
CUTOFF RATIO FOR MODE= .2327E+01  
SUM OF BESSEL FUNCTION ERROR CODES = 0

ORIGINAL PAGE IS  
OF POOR QUALITY

ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0  
AMN = 0.36560636E+01    BMN = 0.74837045E+00  
ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M= -2    N=    2    OMEGA= .3000E+02

MODE DATA

OMEGA= .3000E+02    M= 2    N= 3    XMN= .1258E+02  
CUTOFF RATIO FOR MODE= .1280E+01  
SUM OF BESSEL FUNCTION ERROR CODES = 0  
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0  
AMN = 0.44592966E+01    BMN = -0.29055613E+01  
ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M= -2    N=    3    OMEGA= .3000E+02

LARGEST PROPAGATING N FOR THIS M = 3

MODE DATA

OMEGA= .3000E+02    M= 3    N= 1    XMN= .3987E+01  
CUTOFF RATIO FOR MODE= .4039E+01  
SUM OF BESSEL FUNCTION ERROR CODES = 0  
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0  
AMN = 0.26023450E+01    BMN = -0.32589376E+00  
ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M= -3    N=    1    OMEGA= .3000E+02

MODE DATA

OMEGA= .3000E+02    M= 3    N= 2    XMN= .7747E+01  
CUTOFF RATIO FOR MODE= .2079E+01  
SUM OF BESSEL FUNCTION ERROR CODES = 0  
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0  
AMN = 0.35705322E+01    BMN = -0.89511162E+00  
ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M= -3    N=    2    OMEGA= .3000E+02

MODE DATA

OMEGA= .3000E+02    M= 3    N= 3    XMN= .1301E+02  
CUTOFF RATIO FOR MODE= .1238E+01  
SUM OF BESSEL FUNCTION ERROR CODES = 0

ORIGINAL PAGE IS  
OF POOR QUALITY

ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0  
AMN = -0.18754669E+00 BMN = 0.53089864E+01  
ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M= -3 N= 3 OMEGA= .3000E+02

LARGEST PROPAGATING N FOR THIS M = 3

MODE DATA

OMEGA= .3000E+02 M= 4 N= 1 XMN= .5200E+01  
CUTOFF RATIO FOR MODE= .3097E+01  
SUM OF BESSEL FUNCTION ERROR CODES = 0  
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0  
AMN = 0.31336392E+01 BMN = -0.20930877E+00  
ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M= -4 N= 1 OMEGA= .3000E+02

MODE DATA

OMEGA= .3000E+02 M= 4 N= 2 XMN= .8798E+01  
CUTOFF RATIO FOR MODE= .1830E+01  
SUM OF BESSEL FUNCTION ERROR CODES = 0  
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0  
AMN = 0.33061669E+01 BMN = -0.15169850E+01  
ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M= -4 N= 2 OMEGA= .3000E+02

MODE DATA

OMEGA= .3000E+02 M= 4 N= 3 XMN= .1359E+02  
CUTOFF RATIO FOR MODE= .1185E+01  
SUM OF BESSEL FUNCTION ERROR CODES = 0  
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0  
AMN = 0.34317489E+01 BMN = 0.40298049E+01  
ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M= -4 N= 3 OMEGA= .3000E+02

LARGEST PROPAGATING N FOR THIS M = 3



ORIGINAL PAGE IS  
OF POOR QUALITY

MODE DATA

OMEGA= .3000E+02 M= 5 N= 1 XMN= .6355E+01  
CUTOFF RATIO FOR MODE= .2534E+01  
SUM OF BESSEL FUNCTION ERROR CODES = 0  
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0  
AMN = 0.36182370E+01 BMN = -0.11930907E+00  
ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M= -5 N= 1 OMEGA= .3000E+02

MODE DATA

OMEGA= .3000E+02 M= 5 N= 2 XMN= .9995E+01  
CUTOFF RATIO FOR MODE= .1611E+01  
SUM OF BESSEL FUNCTION ERROR CODES = 0  
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0  
AMN = 0.32789852E+01 BMN = -0.15982724E+01  
ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M= -5 N= 2 OMEGA= .3000E+02

MODE DATA

OMEGA= .3000E+02 M= 5 N= 3 XMN= .1432E+02  
CUTOFF RATIO FOR MODE= .1125E+01  
SUM OF BESSEL FUNCTION ERROR CODES = 0  
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0  
AMN = 0.50087871E+01 BMN = 0.16051647E+01  
ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M= -5 N= 3 OMEGA= .3000E+02

LARGEST PROPAGATING N FOR THIS M = 3

MODE DATA

OMEGA= .3000E+02 M= 6 N= 1 XMN= .7473E+01  
CUTOFF RATIO FOR MODE= .2155E+01  
SUM OF BESSEL FUNCTION ERROR CODES = 0  
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0  
AMN = 0.40542452E+01 BMN = -0.61590101E-01  
ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M= -6 N= 1 OMEGA= .3000E+02

ORIGINAL PAGE IS  
OF POOR QUALITY

MODE DATA

OMEGA= .3000E+02 M= 6 N= 2 XMN= .1127E+02  
CUTOFF RATIO FOR MODE= .1429E+01  
SUM OF BESSEL FUNCTION ERROR CODES = 0  
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0  
AMN = 0.34647685E+01 BMN = -0.14296053E+01  
ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M= -6 N= 2 OMEGA= .3000E+02

MODE DATA

OMEGA= .3000E+02 M= 6 N= 3 XMN= .1518E+02  
CUTOFF RATIO FOR MODE= .1061E+01  
SUM OF BESSEL FUNCTION ERROR CODES = 0  
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0  
AMN = 0.51904865E+01 BMN = -0.42382837E+00  
ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M= -6 N= 3 OMEGA= .3000E+02

LARGEST PROPAGATING N FOR THIS M = 3

MODE DATA

OMEGA= .3000E+02 M= 7 N= 1 XMN= .8565E+01  
CUTOFF RATIO FOR MODE= .1880E+01  
SUM OF BESSEL FUNCTION ERROR CODES = 0  
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0  
AMN = 0.44478450E+01 BMN = -0.30159084E-01  
ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M= -7 N= 1 OMEGA= .3000E+02

MODE DATA

OMEGA= .3000E+02 M= 7 N= 2 XMN= .1257E+02  
CUTOFF RATIO FOR MODE= .1281E+01  
SUM OF BESSEL FUNCTION ERROR CODES = 0  
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0  
AMN = 0.37694693E+01 BMN = -0.11581721E+01  
ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M= -7 N= 2 OMEGA= .3000E+02

LARGEST PROPAGATING N FOR THIS M = 2

ORIGINAL PAGE IS  
OF POOR QUALITY

MODE DATA

OMEGA= .3000E+02 M= 8 N= 1 XMN= .9641E+01  
CUTOFF RATIO FOR MODE= .1670E+01  
SUM OF BESSEL FUNCTION ERROR CODES = 0  
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0  
AMN = 0.48101954E+01 BMN = -0.14625833E-01  
ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M= -8 N= 1 OMEGA= .3000E+02

MODE DATA

OMEGA= .3000E+02 M= 8 N= 2 XMN= .1386E+02  
CUTOFF RATIO FOR MODE= .1162E+01  
SUM OF BESSEL FUNCTION ERROR CODES = 0  
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0  
AMN = 0.41235105E+01 BMN = -0.85984372E+00  
ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M= -8 N= 2 OMEGA= .3000E+02

LARGEST PROPAGATING N FOR THIS M = 2

MODE DATA

OMEGA= .3000E+02 M= 9 N= 1 XMN= .1071E+02  
CUTOFF RATIO FOR MODE= .1504E+01  
SUM OF BESSEL FUNCTION ERROR CODES = 0  
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0  
AMN = 0.51513706E+01 BMN = -0.65555876E-02  
ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M= -9 N= 1 OMEGA= .3000E+02

MODE DATA

OMEGA= .3000E+02 M= 9 N= 2 XMN= .1512E+02  
CUTOFF RATIO FOR MODE= .1065E+01  
SUM OF BESSEL FUNCTION ERROR CODES = 0  
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0  
AMN = 0.44743524E+01 BMN = -0.59372922E+00  
ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M= -9 N= 2 OMEGA= .3000E+02

LARGEST PROPAGATING N FOR THIS M = 2

(+)

ORIGINAL PAGE IS  
OF POOR QUALITY

MODE DATA

OMEGA= .3000E+02 M= 10 N= 1 XMN= .1177E+02  
CUTOFF RATIO FOR MODE= .1368E+01  
SUM OF BESSEL FUNCTION ERROR CODES = 0  
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0  
AMN = 0.54757875E+01 BMN = -0.30348101E-02  
ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M= -10 N= 1 OMEGA= .3000E+02

LARGEST PROPAGATING N FOR THIS M = 1

MODE DATA

OMEGA= .3000E+02 M= 11 N= 1 XMN= .1283E+02  
CUTOFF RATIO FOR MODE= .1256E+01  
SUM OF BESSEL FUNCTION ERROR CODES = 0  
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0  
AMN = 0.57877752E+01 BMN = -0.13177058E-02  
ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M= -11 N= 1 OMEGA= .3000E+02

LARGEST PROPAGATING N FOR THIS M = 1

MODE DATA

OMEGA= .3000E+02 M= 12 N= 1 XMN= .1388E+02  
CUTOFF RATIO FOR MODE= .1160E+01  
SUM OF BESSEL FUNCTION ERROR CODES = 0  
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0  
AMN = 0.60893310E+01 BMN = -0.63729882E-03  
ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M= -12 N= 1 OMEGA= .3000E+02

LARGEST PROPAGATING N FOR THIS M = 1

MODE DATA

OMEGA= .3000E+02 M= 13 N= 1 XMN= .1493E+02  
CUTOFF RATIO FOR MODE= .1079E+01  
SUM OF BESSEL FUNCTION ERROR CODES = 0  
ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0  
AMN = 0.63824353E+01 BMN = -0.1813051E-03  
ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

ORIGINAL PAGE IS  
OF POOR QUALITY

M= -13 N= 1 OMEGA= .3000E+02

LARGEST PROPAGATING N FOR THIS M = 1

MODE DATA

OMEGA= .3000E+02 M= 14 N= 1 XMN= .1598E+02

CUTOFF RATIO FOR MODE= .1008E+01

SUM OF BESSEL FUNCTION ERROR CODES = 0

ERROR CODE FOR CONVERGENCE TO ROOT XMN = 0

AMN = 0.66676797E+01 BMN = -0.10550421E-03

ERROR CODE FOR BESSEL FNS IN AMN AND BMN CALC = 0 0 0 0 0 0 0 0

M= -14 N= 1 OMEGA= .3000E+02

LARGEST PROPAGATING N FOR THIS M = 1

NO MORE PROPAGATING MODES FOR THIS OMEGA

PROBLEM COMPLETED

STOP

END OF EXECUTION

CPU TIME: 1:40.60

ELAPSED TIME: 8:6.24

EXIT.