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TESTS WITH THREE-DIMENSIONAL ADJUSTMENTS IN THE RECTANGULAR
WORKING SECTION OF THE FRENCH T2 WIND TUNNEL, WITH AN
AS 07-TYPE SWEEPED-BACK WING MODEL

A. Blanchard, M. J. Payry, J. F. Breil

Translation of "Essais 'd'adaptation tridimensionnelle' de la
veine rectangulaire de la soufflerie T2, en presence d'une
maquette d'aile en fleche du type AS 07," Rapport Technique OA
34/3075 (DERAT 12/5015 DN), O.N.E.R.A., Centre d'Etudes et de
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16. Abstract This report presents the results obtained on the AS 07 wing and the working section walls for three types of configurations. The first, called "non-adapted," corresponds to the divergent upper and lower rectilinear walls which compensate for limit layer thickening. It can serve as a basis for com- plete flow calculations. The second configuration corresponds to wall shapes determined from calculations which tend to minimize interference at the level of the fuselage. Finally, the third configuration, called "two-dimensional adapta- tion," uses the standard method for T2 profile tests. This case was tested to determine the influence of wall shape and error magnitude. These results are not sufficient to validate the three-dimensional adaptation; they must be coor- dinated with calculations or with unlimited atmosphere tests.			
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NOTATION

$\left. \begin{array}{l} X_p \\ Y_p \\ Z_p \end{array} \right\}$ Cartesian coordinates in the reference working section
 (porthole axis)

$\left. \begin{array}{l} X \\ Y \\ Z \end{array} \right\}$ Cartesian coordinates in the wing reference (leading
 edge to socket)

C Profile chord of the wing section considered

α Angle of the model (fuselage axis)

M_0 Infinite Mach upstream of the flow

M Local Mach (wing or wall)

$$K_p = \frac{p - p_0}{\frac{1}{2} \rho_0 V_0^2} \quad \text{Pressure coefficient}$$

C_z Local or complete-wing lift coefficient

$$\left\{ \begin{array}{l} C_{z \text{ local}} = \int_{\text{profil}} K_p \cdot d\left(\frac{x}{C_{\text{local}}}\right) \\ C_z = \frac{F_z}{\frac{1}{2} \rho_0 V_0^2 \cdot S_{\text{aile}}} \end{array} \right.$$

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1 - INTRODUCTION

/7*

This test series follows a study done in the T2 wind tunnel with the goal of defining a shape for the adaptable walls which would minimize their influence on three-dimensional objects placed in the center of the section or fastened on the side.

The present configuration of the working section does not allow obtaining a shape identical to that of the layer of current existing around a three-dimensional model in unlimited atmosphere (two completely rectilinear and parallel lateral walls, two flexible and bendable upper and lower walls). The planned solution thus consists of using the two bendable walls to minimize the influence of the walls on the model.

The method implemented uses solutions developed by "E. Wedemeyer and L. Lamarche" [5]. A first series of tests was done in cooperation with the University of Berlin on various existing models [6]:

- a C5 revolving body 166 mm long, 0.3% blockage;
- a civil F4 airplane model with 120-mm wingspan and three-component balance;
- a duck-type military airplane model with the same balance.

Another series of tests was then done on a bigger model [7]:

- a C5 body 400 mm long, 1.8% blockage.

*Numbers in the margin indicate pagination in the foreign text.

The results and calculations were compared.

The calculation method was optimized for revolving bodies placed in the center of the section; an extrapolation was tried which placed a half-wing at the wall. In this case, calculation is done as if the section were twice its actual width, using the Mach distribution at the wall measured near the plane of symmetry.

The results obtained on the "16/1000-scale" AS 07 are discussed in this report. They can be divided into two groups: control tests and systematic tests.

Included in the first group is control of wing angling by rotating the walls. The path of the jacks would not permit the displacements required by calculation for angling the model to +2°; we thus used this artificial method after having verified its validity.

The three-dimensional adaptation method supplies the optimal shape of the walls from the first calculation, whatever the initial position of the walls; this was verified in 8 several test configurations. Finally, an adaptation called "two-dimensional" was tested; it uses the normal method for T2 profile tests. This case, without theoretical justification, was tried to see the influence of the shape of the walls and the size of errors which can be made.

The second part of this study corresponds to systematic tests: four configurations were chosen which gave different lift coefficients, without making highly supersonic zones appear on the profiles. For each configuration, three wall positions were tested:

- The first, called "unadapted," corresponds to the upper and lower divergent rectilinear walls compensating for

thickening of the limit layers; it served as our basis for beginning three-dimensional adaptation calculations. These particularly simple limit conditions can also be used for complete calculation of the flow in the working section.

- The second wall shape comes from the three-dimensional adaptation calculation; the flexible sheets are positioned before the gust.

- Finally, the last case corresponds to "two-dimensional adaptation"; the iterative process converges on a single gust.

For each type of test, three gusts are necessary to obtain readings from the six rows of pressure recorders spread along the AS 07 wing.

The experimental results gathered during this series are not sufficient to validate the three-dimensional adaptation method used. Additional calculations must be made to estimate residual corrections. In these tests, a negligible influence of the walls is observed for low lift values or low Mach numbers; inversely, for 2 degrees of incidence or for Mach 0.8, the gaps become significant and can in part be interpreted as variations in aerodynamic incidence.

2 - ADAPTATION PRINCIPLE

The purpose of the adaptable walls is to create an unlimited flow around a model in a working section with finite dimensions; this can be done by controlling the wall conditions, either by their shape in the case of solid walls or by flows of mass through porous walls. The first solution has been chosen at T2, where flexible sheets moved by jacks form the upper and lower plates of the working section [3].

In the case of a three-dimensional body, it is necessary to bend the walls located around the model to arrive at a shape near the layer of current existing around the model in unlimited atmosphere. This solution is not at present possible at T2, but on the other hand it is possible to use the two flexible /9 walls to minimize residual corrections due to the influence of the walls on the object.

2.1 Two-dimensional adaptation

The details of the process will be found in [2] and [4]; it uses a coupling between the real flow in the working section (internal field) and a calculated virtual flow outside the wind tunnel (external field). Coupling occurs on a control surface near the walls through speed vector components. Adaptation is achieved by an iterative process acting on the shape of the walls: the components of the speed on the control surface become available at each iteration; they are extrapolated from the pressure measurements at the wall. The velocities needed on the control surface to achieve an unlimited external flow are calculated by the Green function following an inverse method. A method of optimized relaxation between the internal and external flows for the vertical velocity component, followed by an integration along each flexible wall, supplies the new shape of the wall. The real shape needed is obtained by adding the thickness displacement of the four wall limit layers.

2.2 Three-dimensional adaptation

For three-dimensional adaptation, the process is different [5]: it uses schematization of the model through distribution of sources and vortices in a narrow horseshoe placed on the section axis. This schematization gives a good representation of axisymmetrical bodies mounted in the middle of the working section.

The originality of the method lies in then doing a linear transformation, which permits passing directly from distribution of velocities at the walls to the adapted form without needing to determine the intensity of singularities. The optimized shape of the walls is thus theoretically obtained from the first calculation; this shape, which is not exactly "adapted," minimizes residual corrections on the model caused by the influence of the walls.

Using this method for a half-wing at the wall is abusive, because the base schematization does not represent a wingspan; it has nonetheless been tried here by replacing the lateral door by a plane of symmetry leading to a fictional double section width, and taking the Mach distribution of the flexible walls near the plane of symmetry as reference.

3 - EXPERIMENTAL EQUIPMENT

The T2 transonic wind tunnel is pressurizable and can function at low temperatures; only minimum-pressure and ambient-temperature tests were done during this series.

3.1 Working section equipment

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The working section has an almost square section of $0.39 \times 0.37 \text{ mm}^2$ at the entrance. Flexible sheets of Invar make up the upper and lower walls, equipped with three rows of pressure recorders whose coordinates are given in figures 7 and 8. The sheet-positioning mechanism is described in [2], [3], and [4].

The left lateral door has three portholes with pressure recorders placed along horizontal and vertical lines whose coordinates are shown in figures 7 and 9.

The pressure recorders are linked to the Scanivalves, each of whose head can observe 48 positions in 5 seconds.

The position of the wing in the working section is given in figure 6.

The Mach number of the flow is set by a second neck controlled by the computer which controls the gust.

No other equipment or wind tunnel measurement method was used.

3.2 Mounting the wing

The AS 07 wing model with a scale of "16/1000" is shown by the photographs in figure 5. The method of mounting the wing on the wall is shown (figure 6), the plane of the wing and its specifications are given (figures 10 and 11), and the shape of the profiles which compose it and the positions of the pressure recorders are indicated (figures 12 and 13).

There are six rows, each with 16 recorders on the inner and outer sections and one on the leading edge; they are placed across the wingspan so as to form lines with constant chord percentages. These recorders communicate with tubes placed in grooves along the wingspan; each tube communicates with three recorders (either on the external wing or on the internal wing). When one of the three rows of recorders is used to measure pressure, the other two are covered with thin (0.05-mm) adhesive strips. It is thus possible to simultaneously measure pressure on two sections of the wing (one internal and one external); measurement of velocities over the entire wing thus requires three different gusts.

The wing is mounted on a half-fuselage linked to a porthole, whose rotation ensures the angling of the wing-

fuselage assembly; the angular reference is the rectilinear part on the back of the fuselage [1].

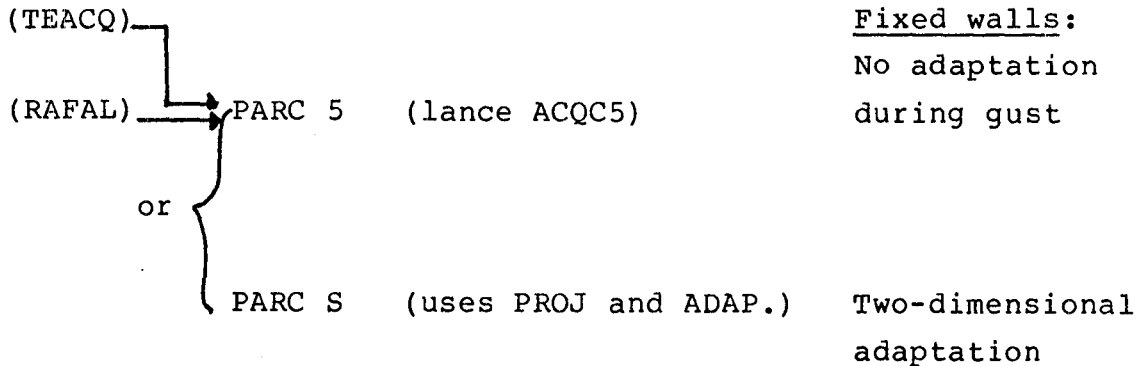
3.3 Acquisition and examination program

The T2 wind tunnel is linked to a team of two computers, one concerned with creating and regulating the gust and the other with obtaining data and storing measurements to disk at the end of the gust.

These tests are pursuant to the series done on the /11 C5 body and use its principal elements.

Disk cartridge LU 26, Program
 LU 34, Test files, calculation files

Acquisition program



Initialization of programs { with (TR,) RINC 5 (For PARC 5)
 { or (TR,) RINC S (For PARC S)

Test file

AD --- test number from AD 100 to AD 173

Wall positioning file

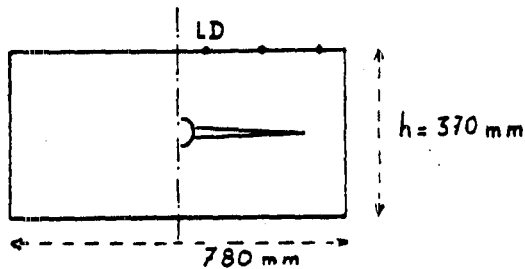
- any test file AD---
- or calculation file AD 9 ---
- or special file { AD 4: Divergent rectilinear walls of symmetrical limit layers.
AD 444: AD 4 + 10' rotation upward
AD 445: AD 4 + 30' rotation upward

Three-dimensional adaptation calculation

Calculation from a test file AD ---

VKJ 43 Calculation of wall shapes without rotation

VKI M Calculation of wall shapes with rotation



- section length 780 mm
- ratio $c = h/b = 2.1081$
- reference recorders:
right lateral RL
- weighting coefficients
file VKJ - R (cartridge
LU 43)

→ Filing to disk

File for new calculated wall shapes

AD 9 --- beginning test number for the calculation

Programs for examination of AD--- files

LTCS:

- graphs local profile Mach numbers
- graphs K_p
- lists AD file
- calculates C_z

LTC 51:

- graphs wall Mach numbers
- graphs wall shapes
- starts LTC 52 (does an RP, LTC 52)

LTC VK:

- graphs only wall shapes calculated by VKI 43 or VKIM (from AD 9---).

4 - SUMMARY OF TESTS PERFORMED

A previous study was done on the AS 07 wing [1]. We verified in one case that the same results would occur, although the working section was modified when the T2 wind tunnel was adapted for cryogenics.

The first control tests were done by measuring rows 2 and 5 of pressure recorders for the Mach numbers and incidences indicated below:

α	M_0		
	0,6	0,7	0,8
+2°	X	X	X
0	X	X	X
-2°	X	X	

Four configurations were selected for systematic tests: /13

α	M_0		
	0,6	0,7	0,8
+2°	X		
0°	X		X
-2°	X		

They correspond to a sampling of lift coefficients and to an infinite Mach effect upstream, while limiting the supersonic zones which appear on the profiles.

Figure 1 shows the list of tests in chronological order, and figures 2, 3, and 4 classify them by configuration.

We first showed that rotation of the upper and lower walls was equivalent to angling the model at the same angle. This artifice was made necessary because the path of the jacks did not permit the displacements required by calculation of three-dimensional adaptation for a model incidence of +2°.

- Divergent rectilinear walls

α gened.	α Display	Wall Start	M_0	
			0,6	0,8
+2°	+2°	AD 4	AD 120	
	+1,5°	AD 445	AD 122	
0°	0°	AD 4	AD 107 - AD 109	AD 108 - AD 132
	-0,5°	AD 445	AD 137	AD 139

M_0

$\alpha_{\text{aérod.}} = 0^\circ$	(α CALCUL	0,6	:	0,8)
	(:)
	(0° VKI 43	117	:	AD 119)
	($-0,5^\circ$ VKI M	138	:	AD 141)
	(:)

The three-dimensional adaptation method theoretically supplies the optimal shape of the walls from the first calculation, whatever the initial position of the flexible sheets. Controls were done in this respect for the following configurations:

M_0

(α	0,7	:	0,8)
(<i>display</i>		:)
($+1,5^\circ$:	AD 127 (1))
(:	AD 128 (2))
(:	AD 129 (3))
(:)
(0°	AD 115 (1)	:	AD 118 (1))
(AD 116 (2)	:	AD 119 (2))
(:)
($-0,5^\circ$:	AD 140 (1))
(:	AD 141 (2))
(:)

The figure in parentheses after the file number indicates the order of the iteration; the wall-positioning file thus results from calculation of the preceding test. (Iteration (0) is the test done with rectilinear walls.)

We also verified that the tests called "two-dimensional adaptation" converged rapidly, as is the case for the profile tests; it is sufficient for that to compare the wall position of

the 3rd and 4th iterations done during the same gust; the two positions are always close. In general, the beginning shape chosen is near the adapted shape, but we have tested this convergence in the two particular cases when the beginning shape was far from the adapted shape. The beginning file chosen was AD 4: rectilinear walls divergent from limit layers and symmetrical.

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Configuration: $Mo = 0.7$ $\alpha = +1.5^\circ$ File AD 130 (1)

Configuration: $Mo = 0.8$ $\alpha = 0^\circ$ File AD 133 (1)

followed by File AD 134 (2)

Comparisons were made between the various wall positions; they are noted:

- "Non," for divergent rectilinear walls
- "2D," for two-dimensional adaptation done with the PARCS program
- "3d," for positioning of the walls in the shape calculated by the VKI 43 or VKI M program

It was decided to do systematic tests for the three cases of "adaptation," the non-adapted case serving as a basis for three-dimensional calculation (any wall shape will work); this case can also serve as a basis for complete flow calculations, because here the limit conditions are particularly simple. The two-dimensional adaptation, a priori outside the subject of the study, was systematically tested to use as a comparison with the assumed optimal shape.

Finally, four configurations for three cases of adaptation, reproduced three times to have the velocity field on all of the wing, were tested; these 36 gusts make up the systematic tests listed in figure 26a.

5 - CONTROL TESTS

We will not present all the tests done, but only a selection of cases judged most interesting, since the goal of this series is not to evaluate the AS 07 wing.

5.1 Angling by wall rotation

Of the five configurations tested (paragraph 4), three are presented. The first corresponds to $M_0 = 0.6$ and $\alpha = +2^\circ$ for rectilinear walls (figure 14); this is the configuration which obliged us to use this artifice, as the three-dimensional case could not be tested.

Figure 15 shows the comparison of Mach numbers on the walls and on the wing, for an aerodynamic incidence equal to 0° and a Mach number equal to 0.8, in the case of rectilinear walls. Figure 16 presents the same configurations but for wall shapes coming respectively from calculations VKI 43 and VKI M.

The results of figures 14 and 15 show that the high Mach case is the most recordable, but the correspondence of the tests remains good. Figure 16 shows that the VKI M calculation makes perfect allowance for total rotation.

It is thus possible to display a model incidence /16 different from that desired and to compensate by rotating the walls.

5.2 Convergences of iterations

5.2.1 Three-dimensional adaptation

Several calculations for optimization of wall shape were connected for one configuration. The last test is always recalculated, leading to a wall shape which by definition

will not be used, but which will in fact constitute an additional iteration.

Of the four tested cases, two are presented in figures 17 and 18; the first ($Mo = 0.7$ and $\alpha = 0^\circ$) shows that the adapted shape is practically obtained from the first iteration; in the second case--much more difficult ($Mo = 0.8$ and $\alpha = +2^\circ$)--it is necessary to wait for the second calculation. This second case corresponds to a freely supersonic regime of the wing which will not be studied systematically herein.

5.2.2 Two-dimensional adaptation

In all tests done, the 3rd iteration is always identical to the 4th and last iteration of the gust, even when the upper and lower walls have been repositioned in a shape very different from the "adapted" shape. This is the case shown in figure 19 corresponding to $Mo = 0.8$ and $\alpha = 0^\circ$.

To confirm the validity of this statement, a second test was done, positioning the flexible sheets on the preceding shape; the values obtained can thus be considered to correspond to the 4th, 5th, 6th, and 7th iterations of the test; they are all identical (figure 20), which confirms that the convergence was well obtained.

5.3 Non/2-D/3-D comparison

Two cases are presented here, one of which is not part of the systematic tests:

- $Mo = 0.7$ $\alpha = 0^\circ$
- $Mo = 0.8$ $\alpha = 0^\circ$

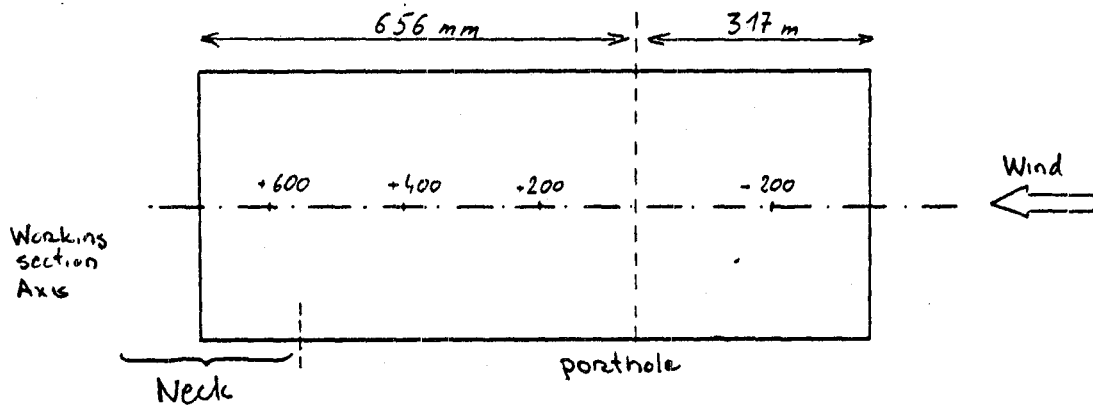
The gaps observed following the types of "adaptation" will become more significant as lift and Mach number upstream increase. The adaptation called "two-dimensional" gives results nearer to the non-adapted case; in fact, everything happens as if the aerodynamic incidence of the two-dimensional case were higher than that of the tests with a wall shape adapted in three dimensions. On the other hand, rectilinear walls lead to a higher effective Mach number upstream (blockage effect).

In the first case (figure 21), the gaps are moderate; they are more significant in the second case (figure 22). Observation of the direction of the walls leaving the convergent (figure 21) shows that effectively the direction of the flow upstream is no longer horizontal in the "2-D" case, unlike the "3-D" case; the angular reference was given by the "non-adapted" case. The effect produced is incontestable, because we /17 previously demonstrated that rotation of the wall assembly modified the aerodynamic incidence of the model; however, this is not sufficient to prove that the 2-D case is erroneous, because the direction of the current lines in unlimited atmosphere is not known. We note also the very different shapes of the walls downstream; they go downward for the "3-D" cases, which is logical allowing for the chosen schematization (horseshoe vortex) and the calculation made (in the plane of symmetry). But once more, that does not prove that the shape obtained is optimum.

Finally, one can observe on the last figure (23) that the effect produced by modifying the shape of the walls is not constant across the wingspan. This was predictable due to the working section geometry itself, allowing for twist of the wing and for three-dimensional effects.

5.4 Visualizations

For three configurations, oil visualizations were done on the left door of the working section, giving the direction of the current lines 55.4 mm from the end of the wing. Reference marks were made, making it possible to locate the positions relative to the current lines and to measure their deviations.



The end of the wing is located between the abscissas 91.06 mm and 135.86 mm from the porthole (figure 6) and very near to the section axis (function of the incidence).

The maximum deviations noticed are located on the section axis slightly behind the tip of the wing (figures 24, 25, and 26).

M_0	α	Walls	δ_{\max}
0,6	+2°	"Non-adapted" AD 4	(5°.....6°)
0,6	+2°	'Adapted 2-D	(5°.....6°)
0,6	-2°	"Non-adapted" AD 4	~ 0,5°

Figure 24

Figure 25

Figure 26

The photos taken from behind clearly show the deviations of the current lines.

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6 - SYSTEMATIC TESTS

For the 36 gusts that made up the systematic tests (paragraph 4 and figure 26a), the following information is given: wall shape (figures 27 and 28), Mach numbers of the three rows of recorders on the adaptable walls (figures 29, 30, 31, and 32), Mach numbers of the left lateral door (figures 33, 34, 35, and 36) following the horizontal axis or the three verticals, and finally spread of K_p on the AS 07 wing (figures 37 to 44).

Numerical values for these curves are given in the attached test listings. File numbers corresponding in chronological order to the experiments were kept in the interests of clarity.

Here will be found a systematic comparison of the three cases of adaptation--"Non/2-D/3-D"--and their influence on the speed distributions whose principal characteristics were seen in paragraph 5.3.

Finally, integration of K_p for each section supplies local lift coefficient C_z . The values are tabulated in figure 45; they were traced along the wingspan of the various configurations tested (figures 46 and 47). It is observed that the internal wing changes less rapidly than the external wing with incidence (figure 46) or Mach number upstream (figure 47).

On the other hand, the gap between the "non-adapted" and "adapted 3-D" cases increases with the lift.

Local C_z were multiplied by the chord of the profile in the section considered; the product $C_z \cdot C$ represents local /19 contribution to wing lift. The values obtained were traced in this representation (figures 48 and 49); this weighting modifies the appearance of the curves ("elliptic" distribution plane), but the observed tendencies are the same.

Finally, integration of the curves in this last representation supplies the overall lift coefficient of the wing, which was reported as a function of incidence (figure 50). We have also reported the lift measured during the preceding series [1], done between rectilinear walls for a Mach number upstream of 0.47. The effect of compressibility is felt more as supersonic zones develop on the wing.

7 - CONCLUSION

This series of tests on the AS 07 wing is registered as a study on three-dimensional adaptation of the T2 wind tunnel. It uses the two flexible walls to minimize residual corrections in the presence of a three-dimensional model. It implements the "E. Wedemeyer and L. Lamarche" method where schematization of the model by a distribution of singularities adequately represents an axisymmetrical body. Extrapolation of these methods in the case of a half-wing at the wall has no ultimate goal; it serves merely as a preliminary phase, to observe the influence of wall shape in various sections of the wing, to study the convergence of the method, and to make adjustments (rotation of walls, incidence, etc.).

On the other hand, these experiments can serve as a basis for calculating potential three-dimensional flow around the model. Then, a three-dimensional object placed in the section

could be more elaborately schematicized; it would lead to development, as for axisymmetrical bodies, of a method of adaptation minimizing the influence of the walls on the model.

At present, it is difficult to know if the shape called "adapted 3-D" is nearer to the values of unlimited atmosphere than the shape "adapted 2-D," but it is definitely not the optimum shape.

The tests will next be completed by directional limit layer readings on the lateral wall at the level of the end of the wing. The direction of the current lines in this area will be an important element in the reality-calculation comparison.

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- First control ($\alpha = +2^\circ$, $Mo = 0.6$ Non-adaptable) Wall shape Wall Mach Profile Mach	14
- Second control ($\alpha = 0^\circ$, $Mo = 0.8$ Non-adaptable) Wall shape Wall Mach Profile Mach	15
- Third control ($\alpha = 0^\circ$, $Mo = 0.8$ 3-D) Wall shape Wall Mach Profile Mach	16
3.2 <u>Convergence of iterations</u>	
a - 3-D	
- First case ($\alpha = 0^\circ$, $Mo = 0.7$) Wall shape Profile Mach	17
- Second case ($\alpha = +2^\circ$, $Mo = 0.8$) Wall shape Profile Mach	18

- b - 2-D ($\alpha = 0^\circ$, $Mo = 0.8$)
 - Beginning of AD 4 (File AD 133)
 - Wall shape
 - Profile Mach 19
 - Beginning of a similar shape: AD 133 (File AD 134)
 - Wall shape
 - Profile Mach 20

3.3 Non/2-D/3-D comparison

- ($\alpha = 0^\circ$, $Mo = 0.7$)
 - Wall shape
 - Wall Mach 21
- ($\alpha = 0^\circ$, $Mo = 0.7$)
 - Profile Mach (2)
 - Profile Mach (3) 21
- ($\alpha = 0^\circ$, $Mo = 0.8$)
 - Wall shape
 - Wall Mach 22
- ($\alpha = 0^\circ$, $Mo = 0.8$)
 - Profile Mach (2)
 - Profile Mach (3) 22
- ($\alpha = 0^\circ$, $Mo = 0.8$) Kp 23

4. Visualization, left lateral door

- ($\alpha = +2^\circ$, $Mo = 0.6$) Non
 - front
 - Visu (2) - back 24
- ($\alpha = +2^\circ$, $Mo = 0.6$) 2-D
 - front
 - Visu (1) - back 25
- ($\alpha = +2^\circ$, $Mo = 0.6$) Non
 - front
 - Visu (3) - back 26

5. Use in 4 base cases

5.1 Wall shape

- $\alpha = -2^\circ$ $Mo = 0.6$
- $\alpha = +2^\circ$ $Mo = 0.6$ 27
- $\alpha = 0^\circ$ $Mo = 0.6$
- $\alpha = 0^\circ$ $Mo = 0.8$ 28

5.2 Adaptable wall Mach

- ($\alpha = -2^\circ$ $Mo = 0.6$)
 - Non
 - 2-D
 - 3-D 29

- ($\alpha = 0^\circ$ Mo = 0.6)	- Non - 2-D - 3-D	30
- ($\alpha = +2^\circ$ Mo = 0.6)	- Non - 2-D - 3-D	31
- ($\alpha = 0^\circ$ Mo = 0.8)	- Non - 2-D - 3-D	32

5.3 Lateral wall Mach

- ($\alpha = -2^\circ$ Mo = 0.6)	- Non - 2-D - 3-D	33
- ($\alpha = 0^\circ$ Mo = 0.6)	- Non - 2-D - 3-D	34
- ($\alpha = +2^\circ$ Mo = 0.6)	- Non - 2-D - 3-D	35
- ($\alpha = 0^\circ$ Mo = 0.8)	- Non - 2-D - 3-D	36

5.4 Kp

- ($\alpha = -2^\circ$ Mo = 0.6)	Non adaptable	37
- ($\alpha = -2^\circ$ Mo = 0.6)	- Non - 2-D - 3-D	38
- ($\alpha = 0^\circ$ Mo = 0.6)	Non adaptable	39
- ($\alpha = 0^\circ$ Mo = 0.6)	- Non - 2-D - 3-D	40
- ($\alpha = +2^\circ$ Mo = 0.6)	Non adaptable	41
- ($\alpha = +2^\circ$ Mo = 0.6)	- Non - 2-D - 3-D	42
- ($\alpha = 0^\circ$ Mo = 0.8)	Non adaptable	43

- ($\alpha = 0^\circ$ Mo = 0.8)	- Non	
	- 2-D	
	- 3-D	44

5.5 Cz

- Cz recapitulative		45
- Cz Mo = 0.6 (3 inc.)		46
- Cz $\alpha = 0^\circ$ (2 Mach)		47
- Cz X chord Mo = 0.6 (3 inc.)		48
- Cz X chord $\alpha = 0^\circ$ (2 Mach)		49
- Cz (α)		50

TEST TABLES
FIGURES 1 TO 4

Figure 1

List of "AS 07 wing" tests

File AD4 : Divergent rectilinear walls
 AD445 : Idem + 30° rotation (upward)
 AD--- : Test file No. ---
 AD9---- : 3-D calculation of new wall position

A File	B	C	D	E
* A	INC.	RANGÉES	FICHER	ROT.
* FICHER	AFF.	DE PRISES	DE DEPART	PAROIS
* NB.	MACH	DE	ADAPT.	D'ITER.
* AD105	0	2 - 5	AD4	0
* AD107	0	"	"	0
* AD109	0	"	"	0
* AD110	-2	"	"	0
* AD115	0	"	AD9105	0
* AD116	0	"	AD9115	0
* AD117	0	"	AD9107	0
* AD118	0	"	AD9108	0
* AD119	0	"	AD9118	0
* AD120	+2	"	AD4	0
* AD122	+1.5	"	AD445	30'
* AD123	+1.5	"	AD9122	30'
* AD124	+1.5	"	AD445	30'
* AD125	+1.5	"	AD9124	30'
* AD126	+1.5	"	AD445	30'
* AD127	+1.5	"	AD9126	30'
* AD128	+1.5	"	AD9127	30'
* AD129	+1.5	"	AD9128	30'
* AD130	+1.5	"	AD4	0
* AD131	+1.5	"	AD130	0
* AD133	0	"	AD4	0
* AD134	0	"	AD133	0
* AD135	0	"	AD134	0
* AD136	0	"	AD135	0
* AD137	-0.5	"	AD445	30'
* AD138	-0.5	"	AD9137	30'
* AD139	-0.5	"	AD445	30'
* AD140	-0.5	"	AD9139	30'
* AD141	-0.5	"	AD9140	30'
* AD142	-2	"	AD4	0
* AD143	-2	"	AD9142	0
* AD144	-2	"	AD136	0
* AD145	+2	"	AD131	0
* AD146	+2	1 - 4	AD145	0
* AD147	+1.5	"	AD445	30'
* AD148	+1.5	"	AD9122	30'
* AD149	0	"	AD136	0
* AD150	0	"	AD4	0
* AD151	0	"	AD9107	0
* AD152	0	"	AD134	0
* AD153	0	"	AD4	0
* AD154	0	"	AD9118	0
* AD155	-2	"	AD144	0
* AD156	-2	"	AD4	0
* AD157	-2	"	AD9142	0
* AD158	-2	3 - 6	AD144	0
* AD159	-2	"	AD4	0
* AD160	-2	"	AD9142	0
* AD161	0	"	AD136	0
* AD162	0	"	AD4	0
* AD163	0	"	AD9107	0
* AD164	0	"	AD134	0
* AD165	0	"	AD4	0
* AD166	0	"	AD9118	0
* AD167	+1.5	"	AD445	30'
* AD168	+1.5	"	AD9122	30'
* AD169	+2	"	AD145	0

Figure 2

Rows of recorders : 1-4

NON ADAPTE				
Incidence		Mach		
Affichee	Aerodynamique	0.6	0.7	0.8
+1.5	+2	147		
0	0	150		153
-2	-2	156		

ADAPTE 3-D				
Incidence		Mach		
Affichee	Aerodynamique	0.6	0.7	0.8
+1.5	+2	148		
0	0	151		154
-2	-2	157		

ADAPTE 2-D				
Incidence		Mach		
Affichee	Aerodynamique	0.6	0.7	0.8
+2	---	146		
0	---	149		152
-2	---	155		

Affichee = Displayed

Figure 3

Rows of recorders : 2-5

NON ADAPTE				
Incidence		Mach		
Affichee	Aerodynamique	0.6	0.7	0.8
+2	+2.17	121		
	+2	120		
+1.5	+2	122	124	126
0	0	107 109	105	108 132
-0.5	0	137		139
-2	-2	142	110	

ADAPTE 3-D				
Incidence		Mach		
Affichee	Aerodynamique	0.6	0.7	0.8
+1.5	+2	123	125	127(1) 128(2) 129(3)
0	0	117	115(1) 116(2)	118(1) 119(2)
-0.5	0	138		140(1) 141(2)
-2	-2	143		

ADAPTE 2-D				
Incidence		Mach		
Affichee	Aerodynamique	0.6	0.7	0.8
+2	---	145		
+1.5	---	131	130	
0	---	136	135	134
-2	---	144		

Figure 4

Rows of recorders : 3-6

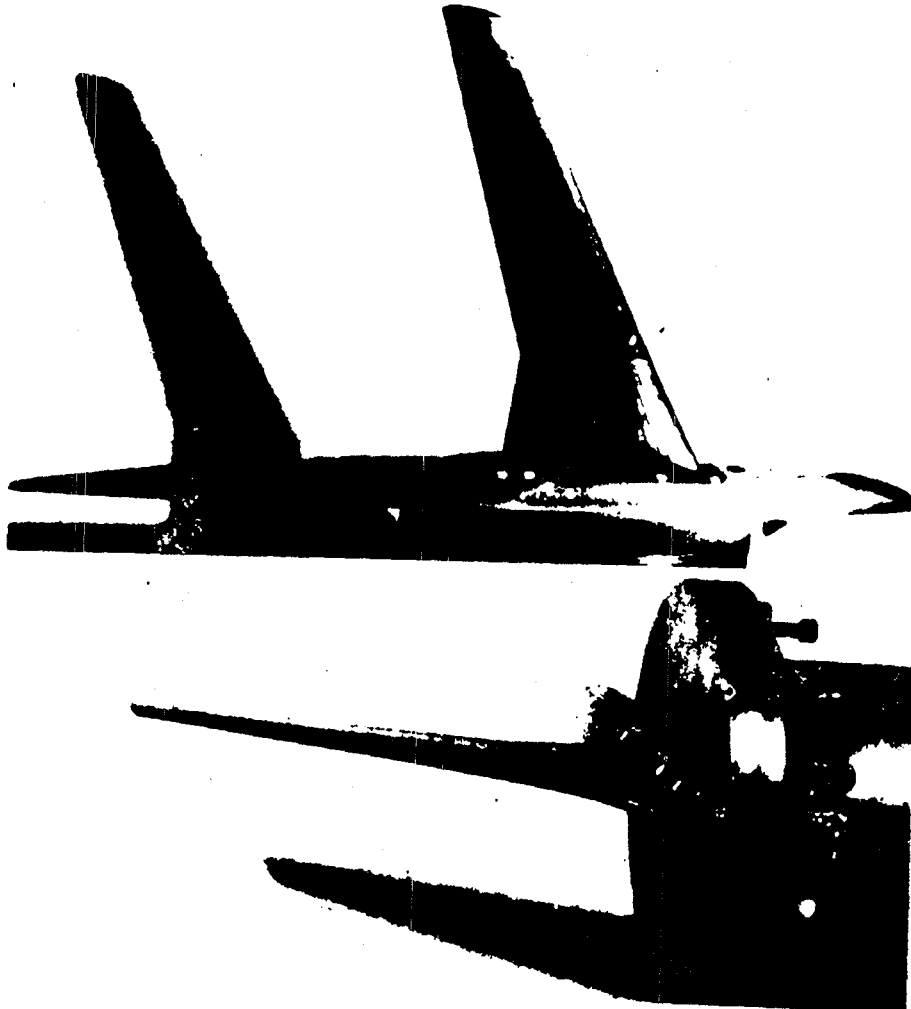
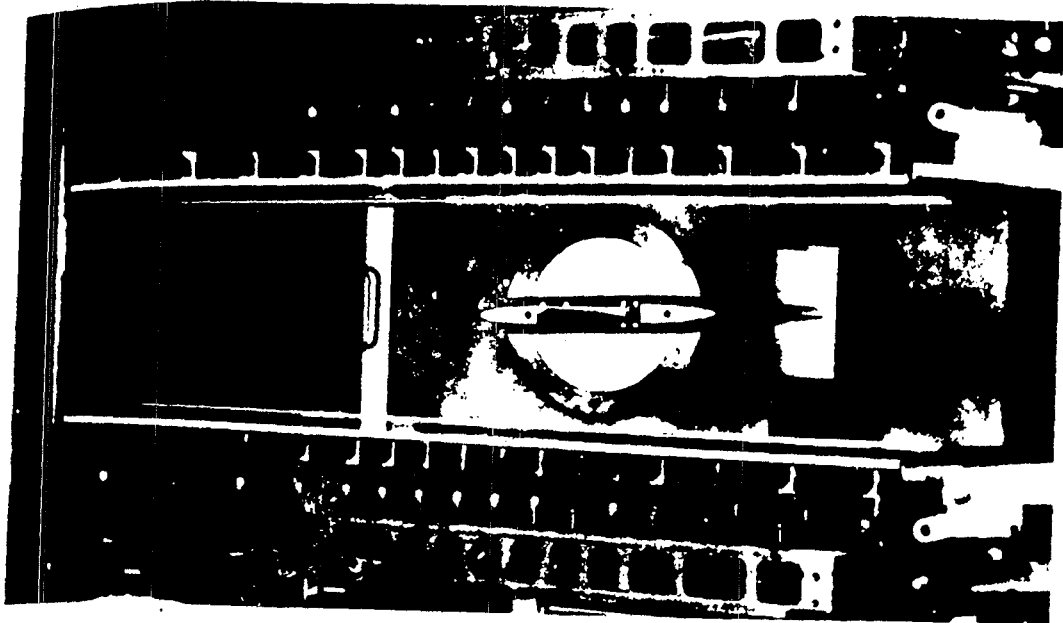
NON ADAPTE				
Incidence		Mach		
Affichee	Aerodynamique	0.6	0.7	0.8
+1.5	+2	167		
0	0	162		165
-2	-2	159		

ADAPTE 3-D				
Incidence		Mach		
Affichee	Aerodynamique	0.6	0.7	0.8
+1.5	+2	168		
0	0	163		166
-2	-2	160		

ADAPTE 2-D				
Incidence		Mach		
Affichee	Aerodynamique	0.6	0.7	0.8
+2	---	169		
0	---	161		164
-2	---	158		

Affichee = Displayed

Presentation of mounting



WING MOUNTING

FIGURES 5 TO 13

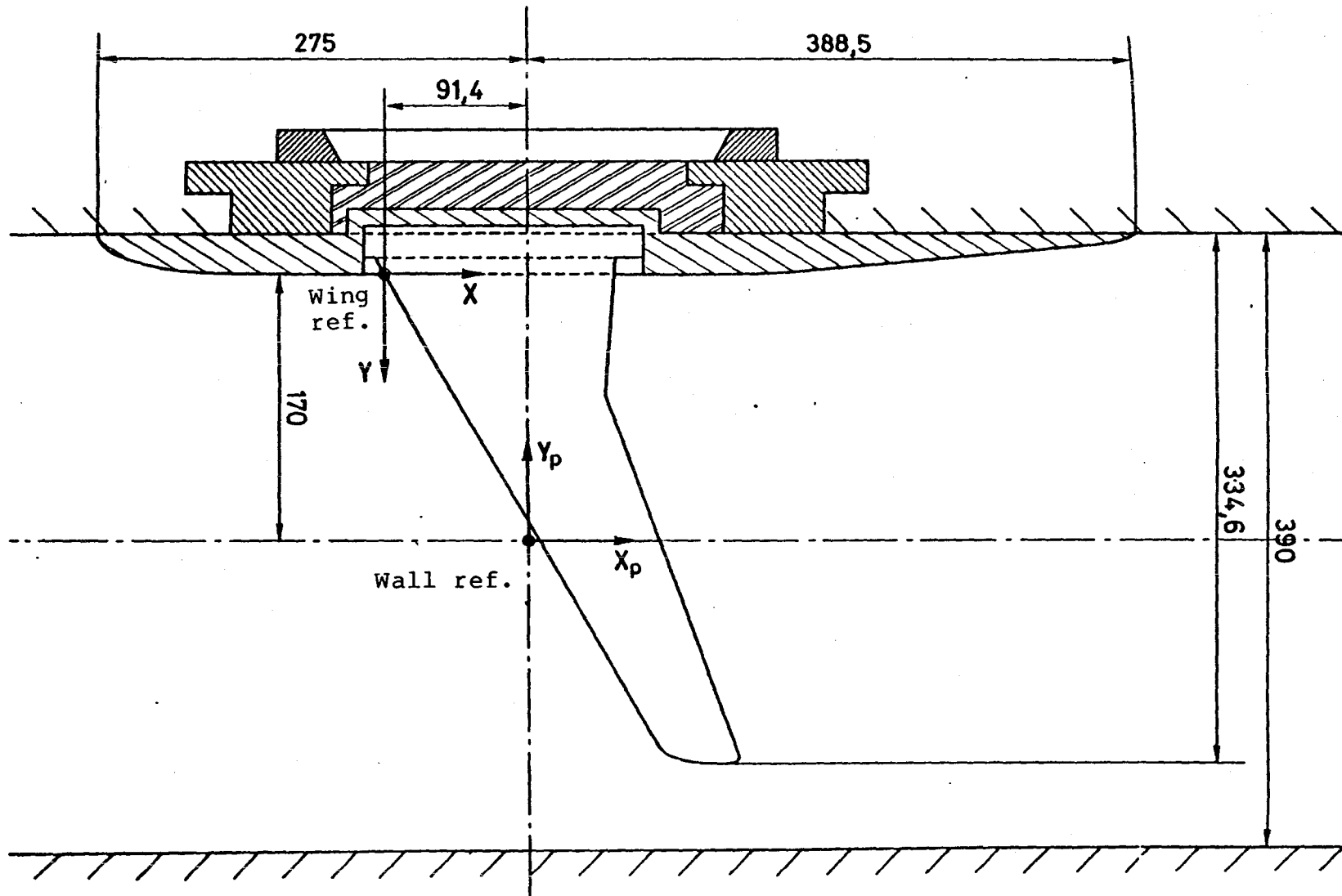


Diagram of wing mounting

Figure 6

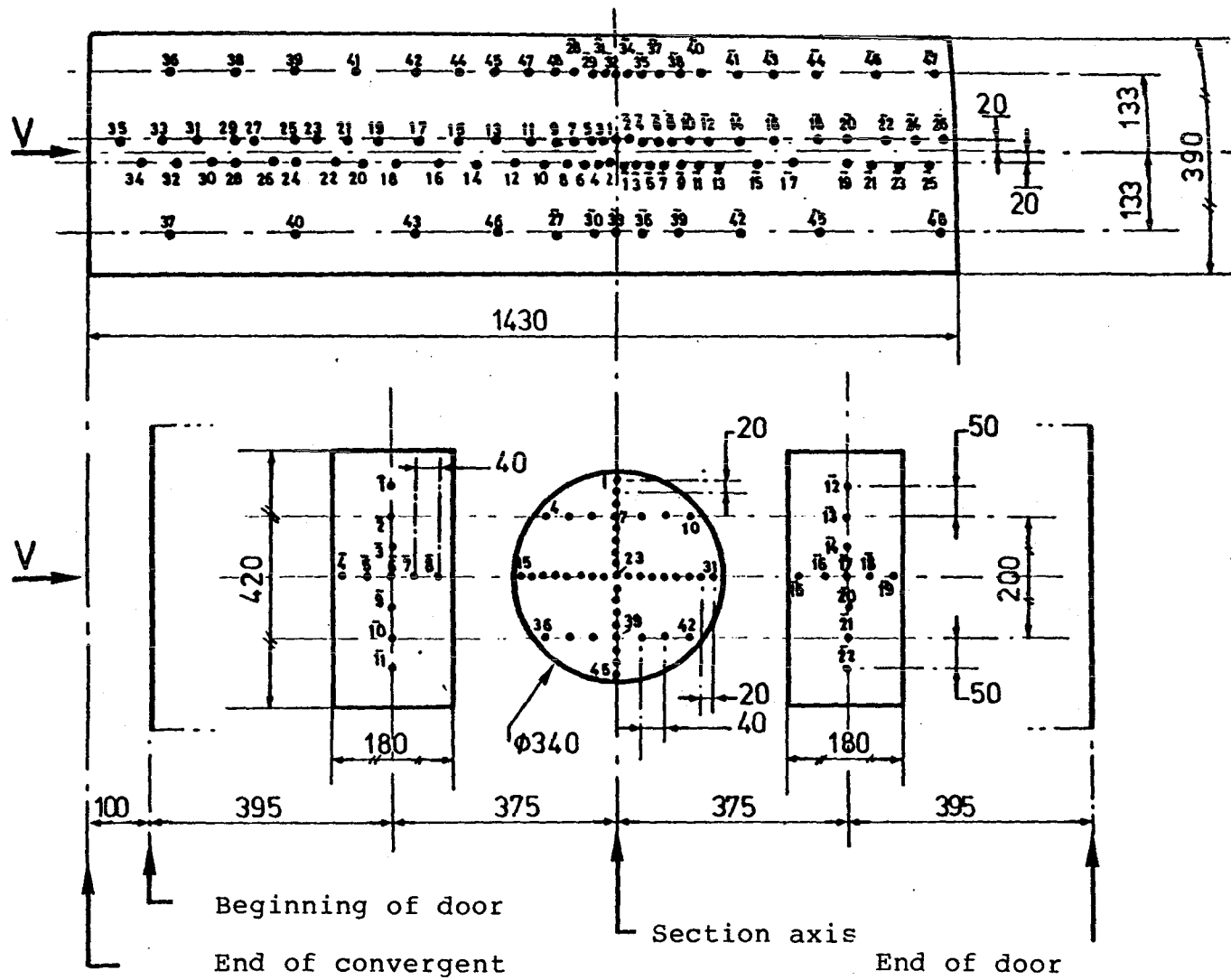


Diagram of wall pressure recorders

Figure 7

Figure 8

Equipment of adaptable cryogenic walls: specs of
pressure recorders, jacks, and thermocouples

Wall pressure recorders							Jacks		
I	XPH	XPB	ZP	I	XPH	KPB	ZP	I	XV
1	-812.5	-812.5	20.0	49	260.0	260.0	20.0	1	-705.0
2	-797.5	-797.5	-20.0	50	290.0	290.0	-20.0	2	-575.0
3	-747.5	-747.5	20.0	51	330.0	330.0	20.0	3	-460.0
4	-722.5	-722.5	-20.0	52	380.0	380.0	-20.0	4	-355.0
5	-692.5	-692.5	20.0	53	417.5	417.5	-20.0	5	-275.0
6	-667.5	-667.5	-20.0	54	442.5	442.5	20.0	6	-215.0
7	-630.0	-630.0	-20.0	55	467.5	467.5	-20.0	7	-155.0
8	-592.5	-592.5	20.0	56	492.5	492.5	20.0	8	-95.0
9	-567.5	-567.5	-20.0	57	517.5	517.5	-20.0	9	-35.0
10	-530.0	-530.0	-20.0	58	542.5	542.5	20.0	10	25.0
11	-492.5	-492.5	20.0	59	-630.0	-630.0	20.0	11	85.0
12	-467.5	-467.5	-20.0	60	-530.0	-530.0	20.0	12	145.0
13	-442.5	-442.5	20.0	61	380.0	380.0	20.0	13	205.0
14	-417.5	-417.5	-20.0	62	-735.0	-735.0	-133.0	14	285.0
15	-392.5	-392.5	20.0	63	-530.0	-530.0	-133.0	15	390.0
16	-367.5	-367.5	-20.0	64	-330.0	-330.0	-133.0	16	505.0
17	-330.0	-330.0	20.0	65	-200.0	-200.0	-133.0		
18	-290.0	-290.0	-20.0	66	-100.0	-100.0	-133.0		
19	-260.0	-260.0	20.0	67	-40.0	-40.0	-133.0		
20	-230.0	-230.0	-20.0	68	0.0	0.0	-133.0		
21	-200.0	-200.0	20.0	69	40.0	40.0	-133.0		
22	-170.0	-170.0	-20.0	70	100.0	100.0	-133.0		
23	-145.0	-145.0	20.0	71	200.0	200.0	-133.0		
24	-120.0	-120.0	-20.0	72	330.0	330.0	-133.0		
25	-100.0	-100.0	20.0	73	530.0	530.0	-133.0		
26	-85.0	-85.0	-20.0	74	-735.0	-735.0	133.0		
27	-70.0	-70.0	20.0	75	-630.0	-630.0	133.0		
28	-55.0	-55.0	-20.0	76	-530.0	-530.0	133.0		
29	-40.0	-40.0	20.0	77	-430.0	-430.0	133.0		
30	-30.0	-30.0	-20.0	78	-330.0	-330.0	133.0		
31	-20.0	-20.0	20.0	79	-260.0	-260.0	133.0		
32	-10.0	-10.0	-20.0	80	-200.0	-200.0	133.0		
33	0.0	0.0	20.0	81	-145.0	-145.0	133.0		
34	10.0	10.0	-20.0	82	-100.0	-100.0	133.0		
35	20.0	20.0	20.0	83	-70.0	-70.0	133.0		
36	30.0	30.0	-20.0	84	-40.0	-40.0	133.0		
37	43.0	40.0	20.0	85	-20.0	-20.0	133.0		
38	55.0	55.0	-20.0	86	0.0	0.0	133.0		
39	70.0	70.0	20.0	87	20.0	20.0	133.0		
40	78.8	78.8	-20.0	88	40.0	40.0	133.0		
41	91.3	91.3	20.0	89	70.0	70.0	133.0		
42	100.0	100.0	-20.0	90	100.0	100.0	133.0		
43	123.0	120.0	20.0	91	138.8	138.8	133.0		
44	138.8	138.8	-20.0	92	200.0	200.0	133.0		
45	151.3	151.3	20.0	93	260.0	260.0	133.0		
46	170.0	170.0	-20.0	94	330.0	330.0	133.0		
47	200.0	200.0	20.0	95	430.0	430.0	133.0		
48	230.0	230.0	-20.0	96	530.0	530.0	133.0		

THERM.	
I	XTH
8	-737.0
7	0.0
9	475.0
XTB	
6	-737.0
4	-427.0
2	-180.0
1	0.0
3	179.0
5	479.0

XPH-XPB-XV-XTH-XTB IN MM/AXIS PORTHOLE

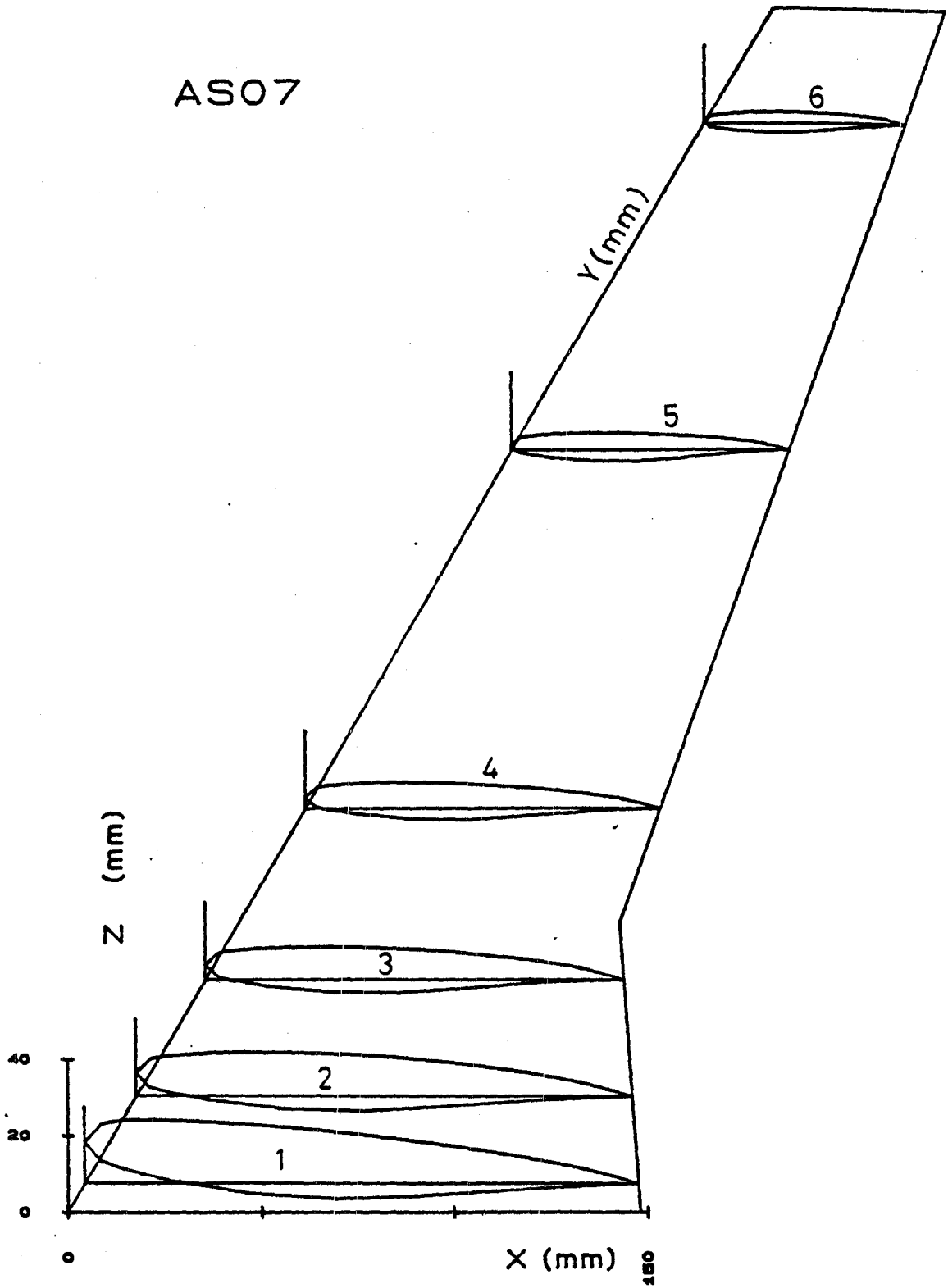
Z in mm/section axis

Figure 9

Pressure recorder specifications - lateral walls (mm)

upstream hole			central hole			downstream hole		
N	X	Z	N	X	Z	N	X	Z
1		+150	1		+160	1		+150
2	-375	+100	2	0	+140	2	+375	+100
3		+ 50	3		+120	3		+ 50
4	-455		4	-120		4	+295	
5	-410		5	- 80		5	+335	
6	-375	0	6	- 40		6	+375	0
7	-335		7	0	+100	7	+415	
8	-295		8	+ 40		8	+455	
9		- 50	9	+ 80		9		- 50
10	-375	-100	10	+120		10	+375	-100
11		-150	11		+ 80	11		-150
			12	0	+ 60			
			13		+ 40			
			14		+ 20			
			15	-160				
			16	-140				
			17	-120				
			18	-100				
			19	- 80				
			20	- 60				
			21	- 40				
			22	- 20				
			23	0	0			
			24	+ 20				
			25	+ 40				
			26	+ 60				
			27	+ 80				
			28	+100				
			29	+120				
			30	+140				
			31	+160				
			32		- 20			
			33	0	- 40			
			34		- 60			
			35		- 80			
			36	-120				
			37	- 80				
			38	- 40				
			39	0	-100			
			40	+ 40				
			41	+ 80				
			42	+120				
			43		-120			
			44	0	-140			
			45		-160			

Diagram of the wing



Specifications of the AS 07 wing

		A			
		Y	B.A. X	B.F. X	corde
B	Emplanture	0	0	148,112	148,112
C	rangee 1	7,56	4,46	147,62	143,16
	rangee 2	30,34	17,88	146,12	128,24
	rangee 3	60,40	35,6	144,15	108,55
	rupture	75,227	44,335	143,18	98,845
	rangee 4	104,301	61,47	153,61	92,14
	rangee 5	196,41	115,75	186,66	70,91
	rangee 6	279,87	164,94	216,60	51,66
D	Saumon	309,60	182,464	227,264	44,80

(mm)

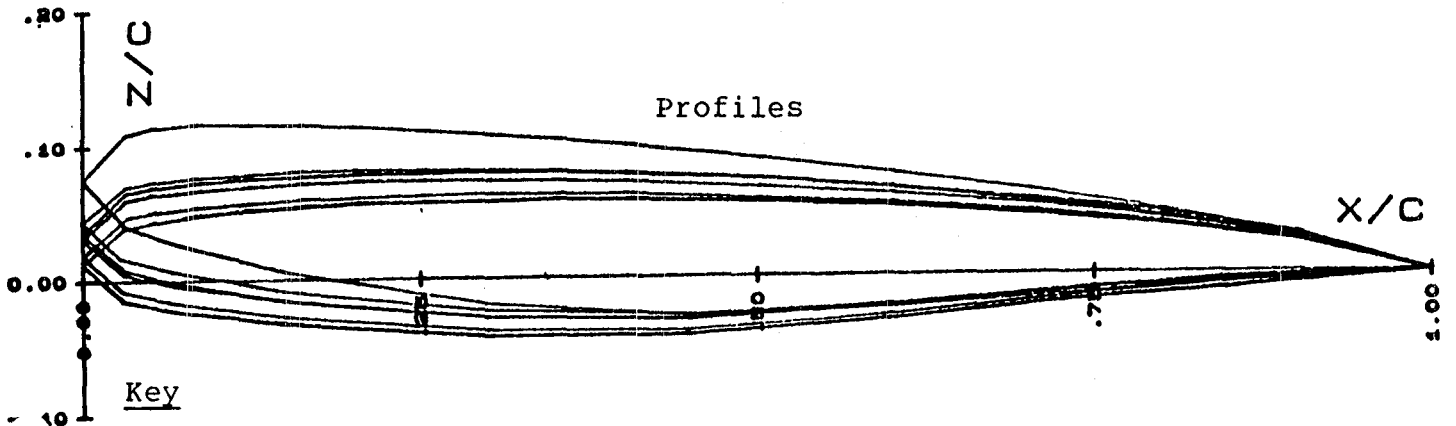
Key

- A - chord
- B - root
- C - row
- C - tip

Figure 12

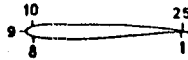
Position of pressure recorders for each section

A	B.A.	1 prise	0 %								
B	Extrados	16 prises	3	5	8	12	16	20	25	30 %	
			35	40	50	60	70	75	80	90 %	
C	Intrados	8 prises	3	7	15	30	45	60	75	85 %	



- A - B.A. 1 recorder
- B - Outer section 16 recorders
- C - Inner section 8 recorders

Specifications of pressure recorders on "Airbus" AS07 wing



A Aile Interne						B Aile Externe						
rangee 1		rangee 2		rangee 3		rangee 4		rangee 5		rangee 6		
Y = 7.560mm		Y = 30.340mm		Y = 60.400mm		Y = 104.301mm		Y = 198.410mm		Y = 279.870mm		
B.A. = 4.295mm		B.A. = 17.715mm		B.A. = 35.498mm		B.A. = 61.392mm		B.A. = 115.701mm		B.A. = 164.943mm		
B.F. = 147.620mm		B.F. = 146.120mm		B.F. = 144.150mm		B.F. = 153.610mm		B.F. = 166.660mm		B.F. = 216.600mm		
C corde 143.160mm		C corde 128.240mm		C corde 108.550mm		C corde 92.140mm		C corde 70.910mm		C corde 51.660mm		
X (mm)	Z (mm)	X (mm)	Z (mm)	X (mm)	Z (mm)	X (mm)	Z (mm)	X (mm)	Z (mm)	X (mm)	Z (mm)	
11	125.979	-1.060	126.753	-0.812	127.744	-0.477	139.796	-0.427	176.014	-0.529	208.802	-0.611
21	111.652	-2.030	113.946	-1.603	116.860	-1.104	130.546	-1.059	168.883	-1.062	203.655	-0.940
31	90.225	-3.393	94.643	-3.043	100.606	-2.349	116.608	-2.047	158.182	-2.085	195.877	-1.686
41	68.703	-4.100	75.476	-4.026	84.444	-3.416	102.910	-2.941	147.676	-2.836	188.110	-2.244
51	47.066	-2.670	56.069	-3.411	68.084	-3.155	89.086	-2.683	137.029	-2.739	180.378	-2.234
61	25.741	0.833	36.785	-1.156	51.753	-1.680	75.279	-1.404	126.444	-1.933	172.775	-1.685
71	14.624	3.784	26.560	0.924	43.091	-1.189	67.809	-0.344	120.661	-1.160	168.532	-1.158
81	8.751	5.783	21.249	2.395	38.873	0.869	64.174	0.458	117.768	-0.531	166.487	-0.742
91	4.295	10.800	17.715	6.327	35.498	3.823	61.392	2.909	115.701	1.302	164.943	0.631
101	8.723	15.493	21.770	9.986	38.940	7.078	64.267	5.467	117.973	3.323	166.547	2.025
111	11.585	16.199	24.358	10.487	41.105	7.486	66.108	5.843	119.417	3.598	167.634	2.203
121	15.846	16.647	28.129	10.923	44.283	7.849	68.897	6.110	121.501	3.835	169.065	2.442
131	21.618	16.604	33.252	11.253	48.640	8.184	72.644	6.408	124.422	4.057	171.278	2.676
141	27.277	16.489	38.412	11.529	52.991	8.315	76.313	6.598	127.290	4.257	173.375	2.808
151	32.911	16.259	43.567	11.634	57.393	8.490	80.039	6.745	129.993	4.320	175.430	2.922
161	40.345	15.832	50.130	11.621	62.771	8.539	84.700	6.784	133.473	4.440	177.931	2.954
171	47.378	15.325	56.415	11.552	68.203	8.599	89.220	6.738	137.156	4.498	180.642	2.974
181	54.600	14.779	62.367	11.373	73.628	8.559	93.797	6.674	140.619	4.442	183.036	3.024
191	61.817	14.109	69.275	11.123	79.051	8.330	98.353	6.557	144.214	4.438	185.851	2.985
201	76.080	12.593	81.970	10.477	89.905	7.886	107.621	6.118	151.250	4.116	190.836	2.862
211	90.393	10.871	94.843	9.268	100.707	7.162	116.809	5.564	158.243	3.824	196.000	2.648
221	104.729	8.981	107.703	7.823	111.669	6.098	126.168	4.814	165.501	3.331	201.100	2.312
231	111.839	7.869	114.070	6.961	117.001	5.560	130.641	4.311	168.927	3.009	203.841	2.056
241	119.020	6.701	120.482	5.980	122.467	4.846	135.204	3.747	172.367	2.629	206.349	1.850
251	133.269	3.920	133.311	3.626	133.304	3.071	144.355	2.427	179.552	1.684	211.614	1.181

Key

- A - Internal wing
- B - External wing
- C - Row
- D - B.A.
- E - B.F.
- F - Chord

CONTROL TESTS

Wall incidence and rotation: Figures 14 to 16
Convergence of iterations: Figures 17 to 20
Non/2-D/3-D comparison: Figures 21 to 23

Key to figures 14, 15, and 16

- A - Non-adapted
- B - Wall shapes
- C - Row
- D - Upper wall
- E - Lower wall
- F - Central rows of pressure recorders

$M=0,6$
 $\alpha=+2^\circ$

A non adapté

○ — AD120
 + — AD122

Rotation: First control

C Rangée ⑤

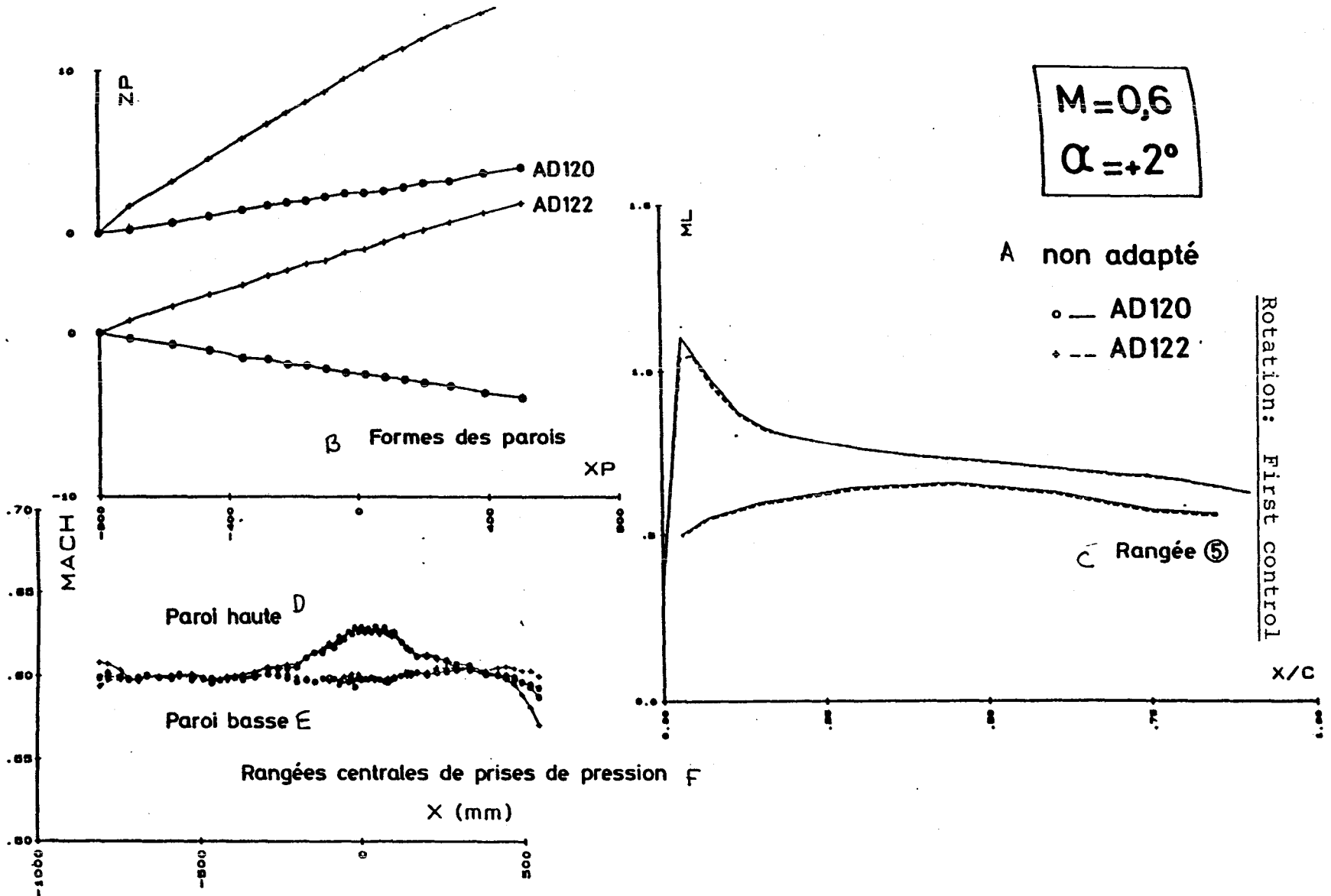


Figure 14

$M=0,8$
 $\alpha=0^\circ$

A non adapté

○ — AD108
 + --- AD139

Rotation: Second control

Rangée ⑤
 C

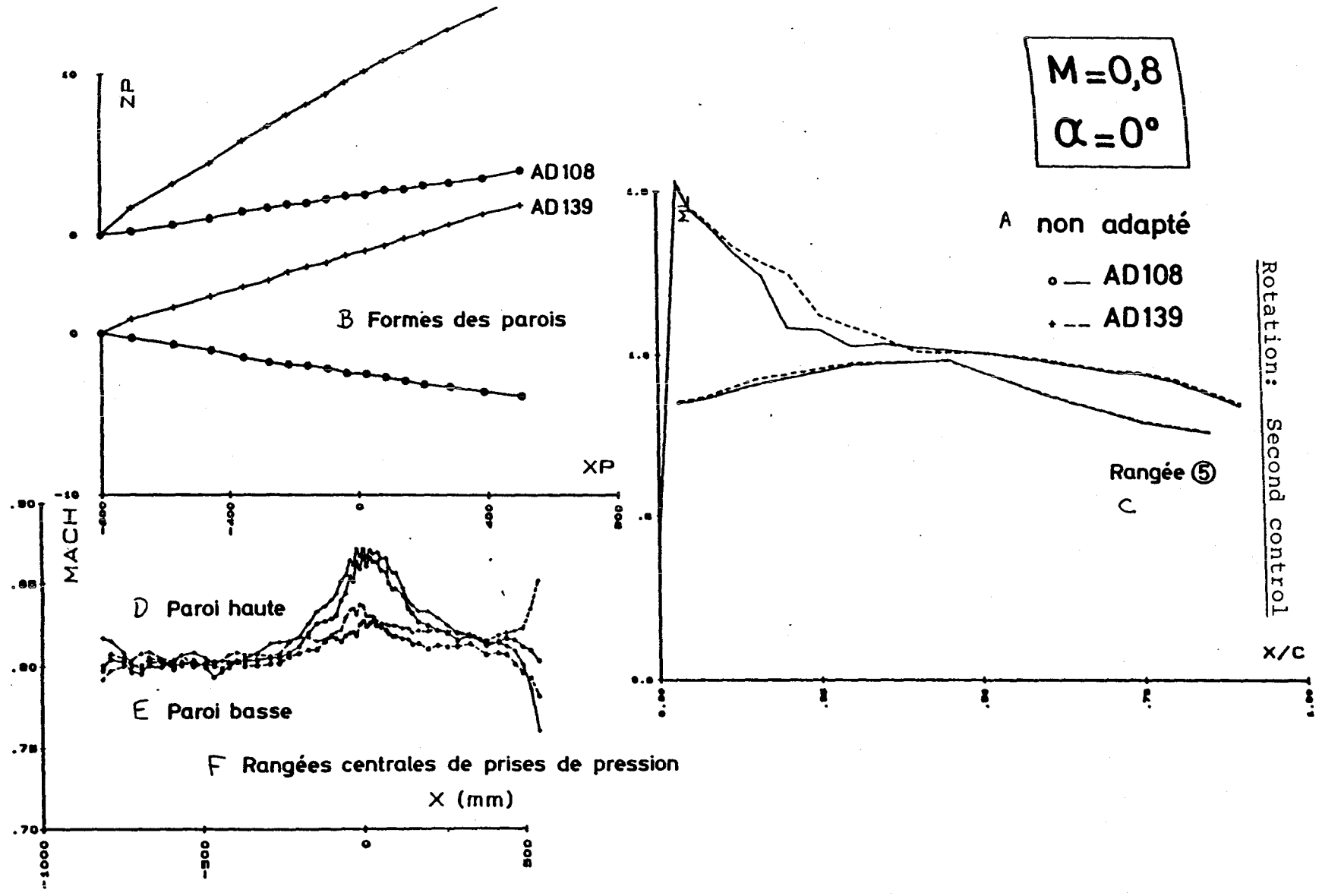


Figure 15

$M=0,8$
 $\alpha=0^\circ$

A adapté 3_D

○ — AD119
 ◆ --- AD141

Rotation: Third control

C Rangée ⑤

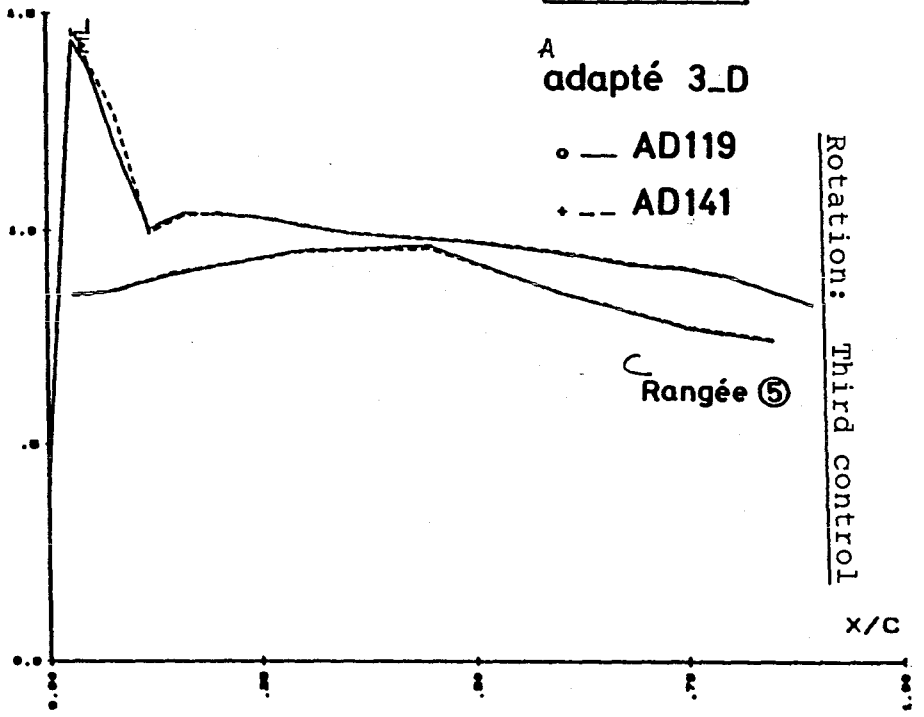
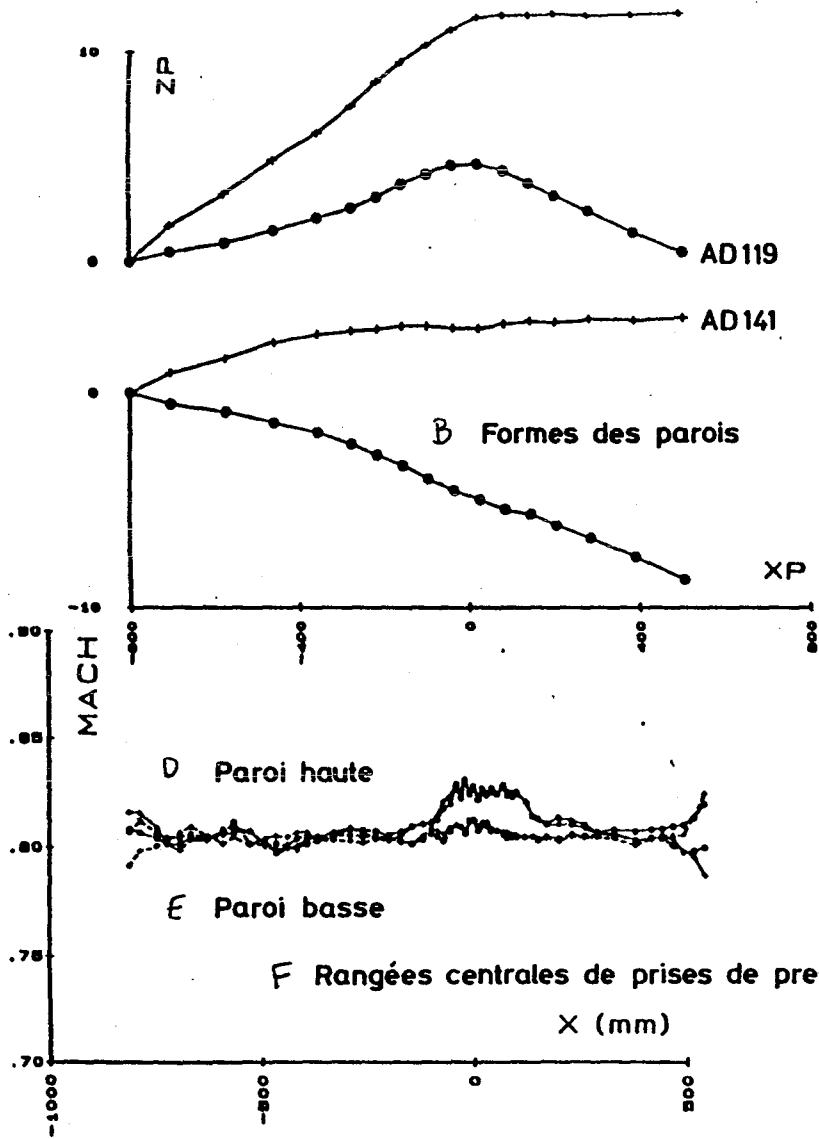
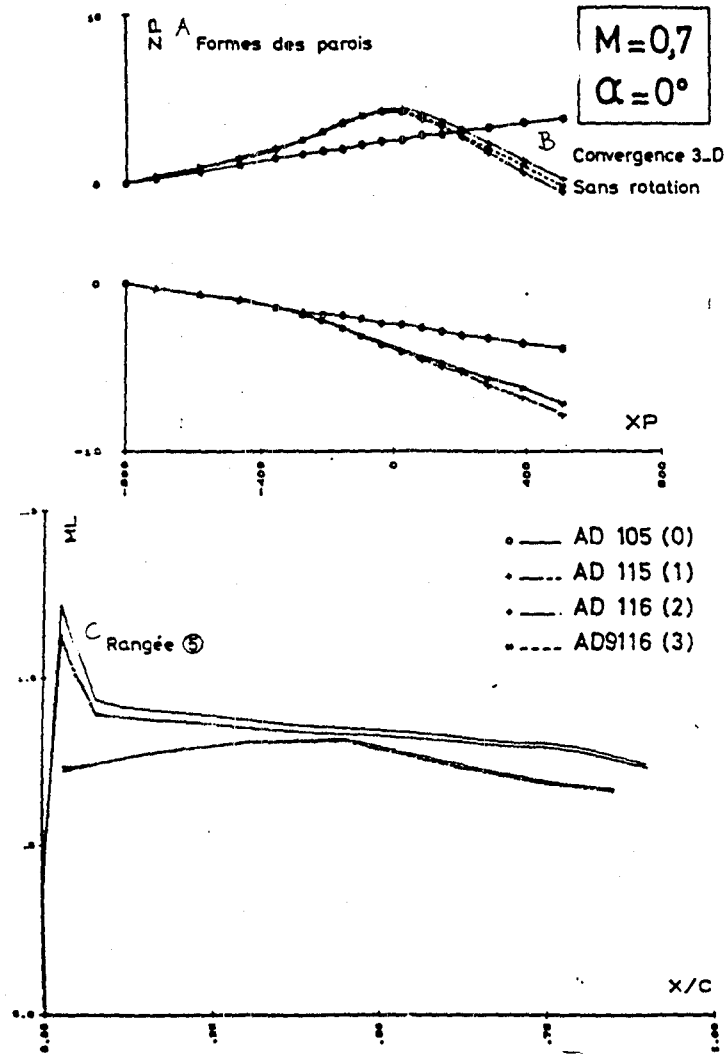


Figure 16

First case

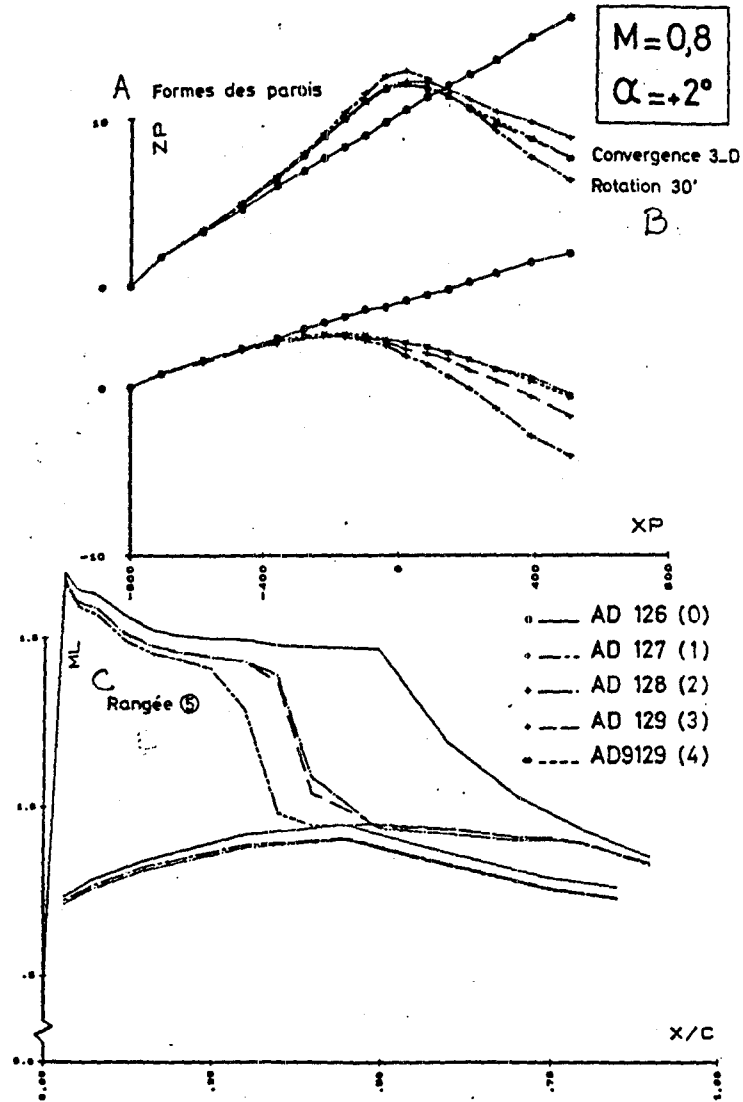


Key

- A - Wall shapes
- B - 3-D convergence, no rotation
- C - Row

Figure 18

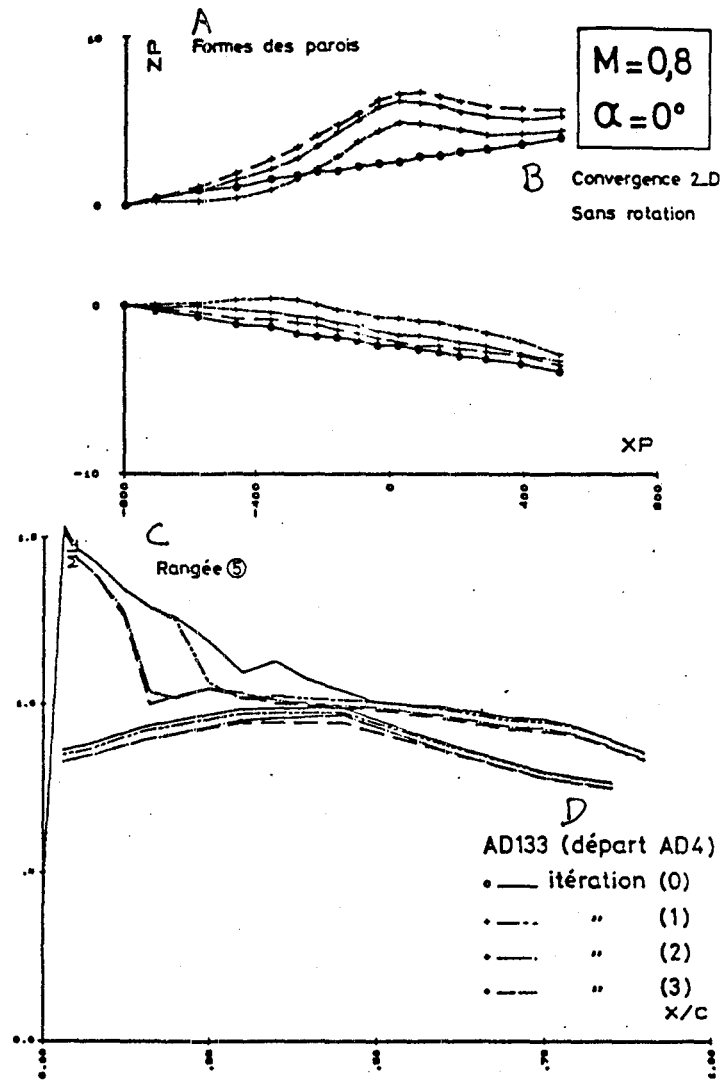
Second case



Key

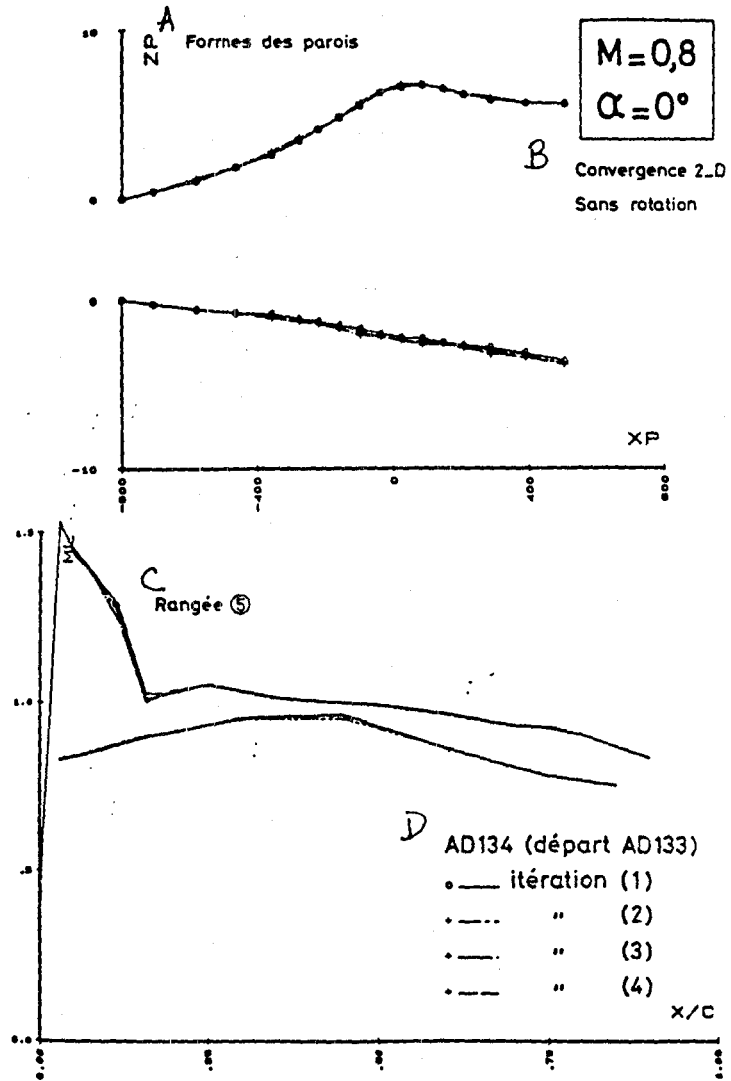
- A - Wall shapes
- B - Row

Figure 19



Key

- A - Wall shapes
- B - 2-D convergence, no rotation
- C - Row
- D - Beginning



Key

- A - Wall shapes
- B - 2-D convergence, no rotation
- C - Row
- D - Beginning

Key to figures 21 and 22

- A - Wall shapes
- B - Row
- C - Upper wall
- D - Lower wall
- E - Central rows of pressure recorders

Non/2-D/3-D comparison

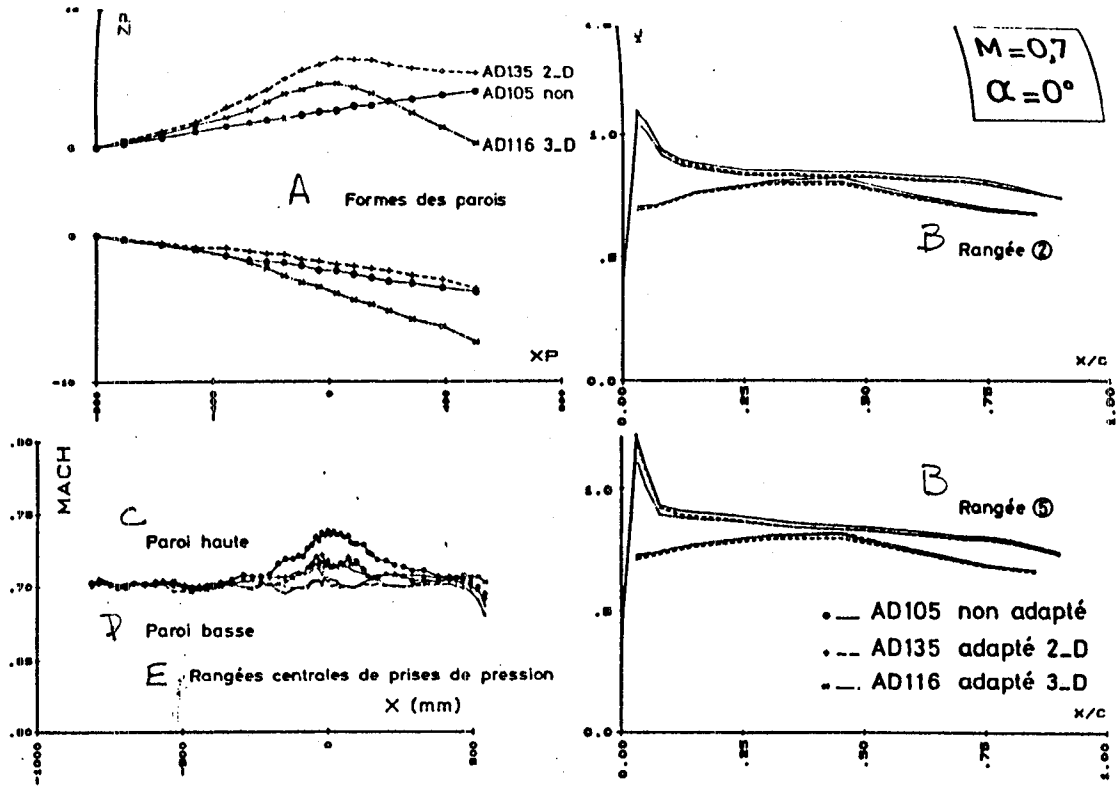
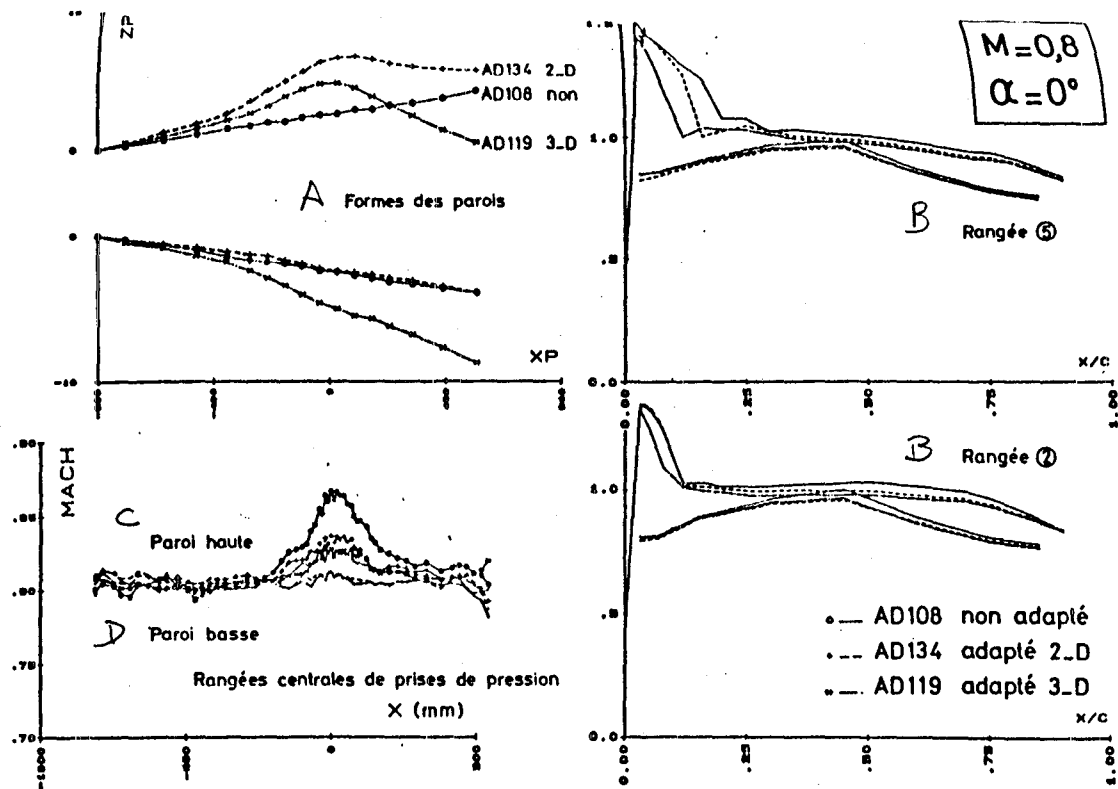
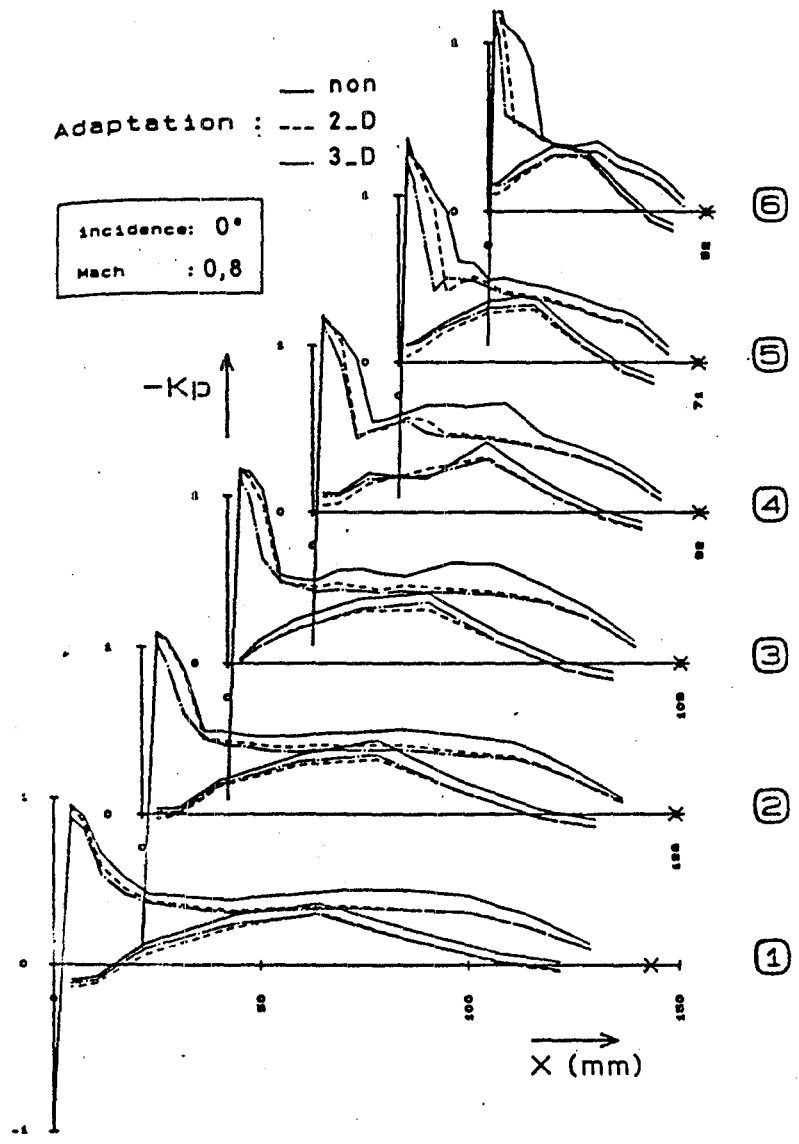


Figure 22

Non/2-D/3-D comparison



Non/2-D/3-D comparison

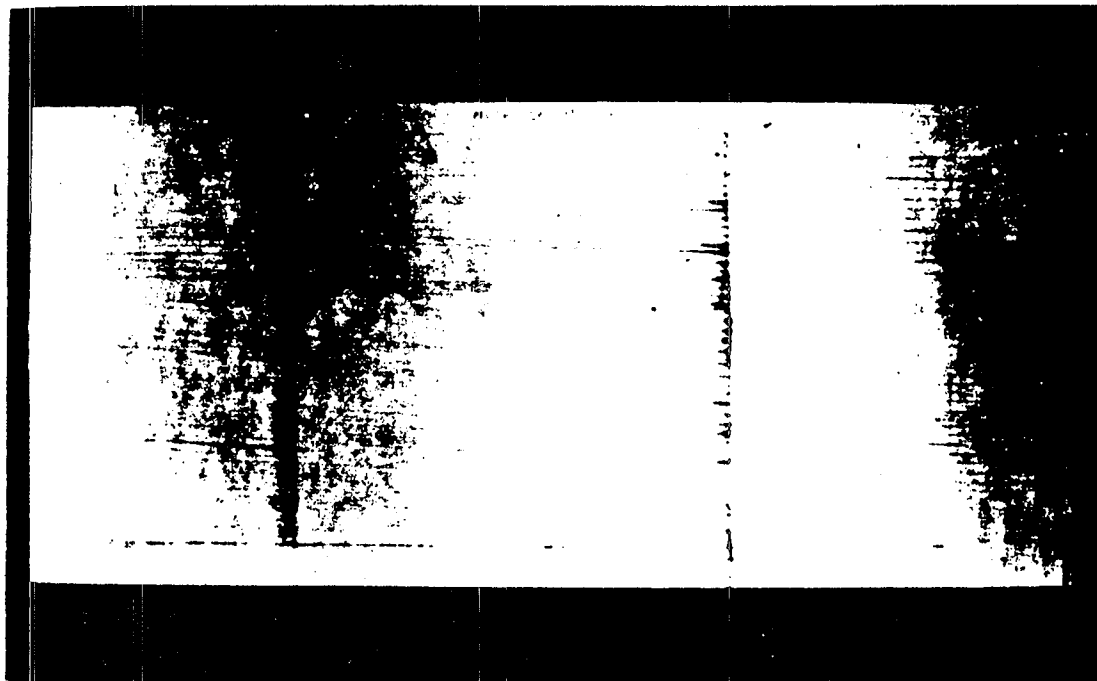
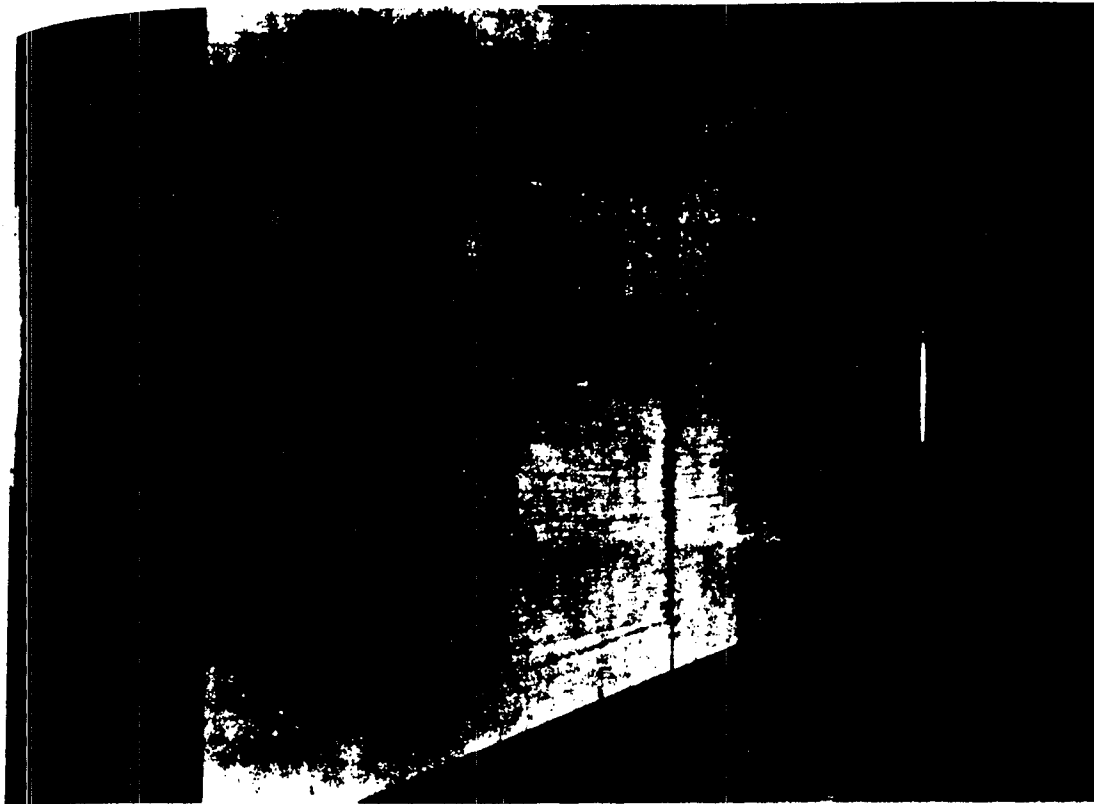


VISUALIZATION OF CURRENT LINES

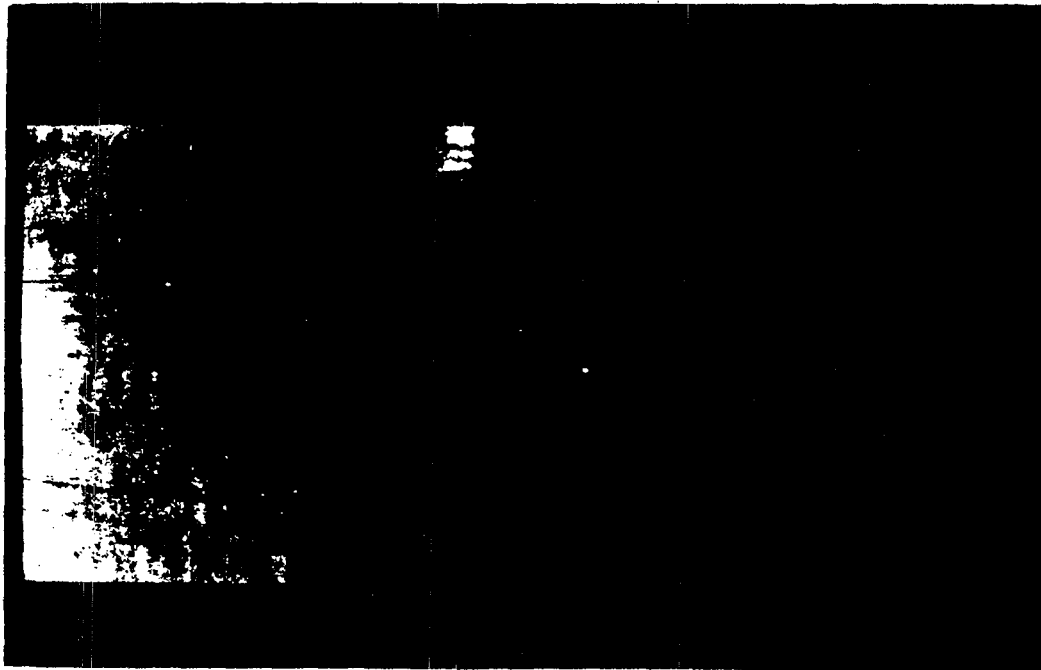
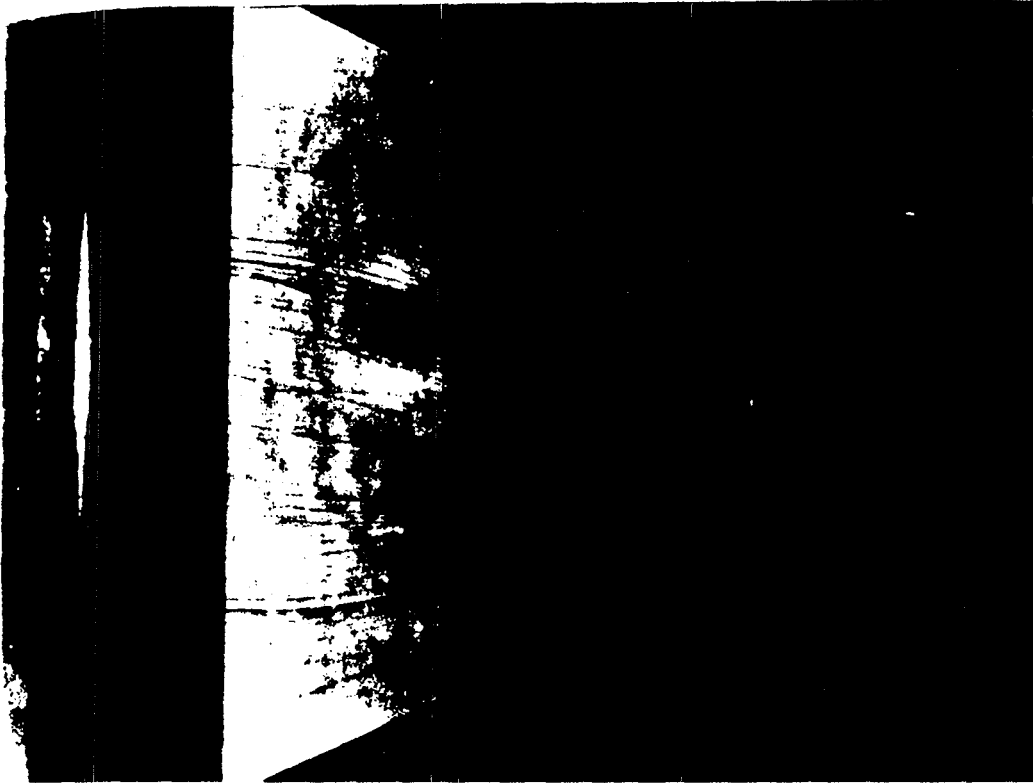
ON THE LEFT LATERAL WALL

Mo = 0.6	$\alpha = +2^\circ$	Non-adapted	Figure 24
Mo = 0.6	$\alpha = +2^\circ$	2-D	Figure 25
Mo = 0.6	$\alpha = -2^\circ$	Non-adapted	Figure 26

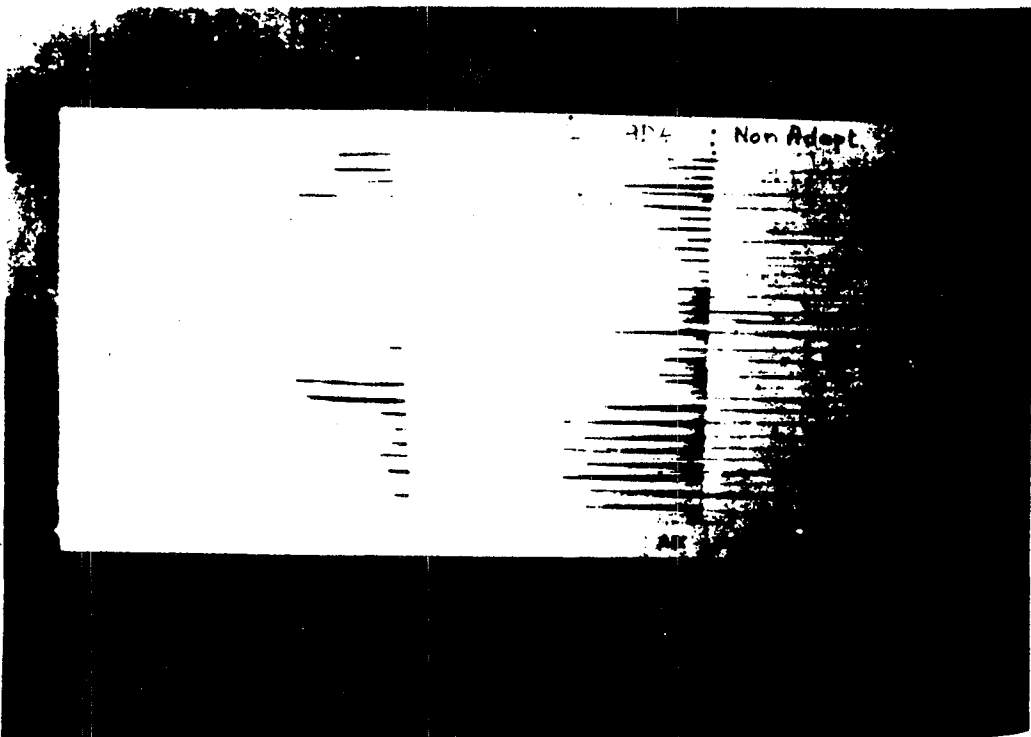
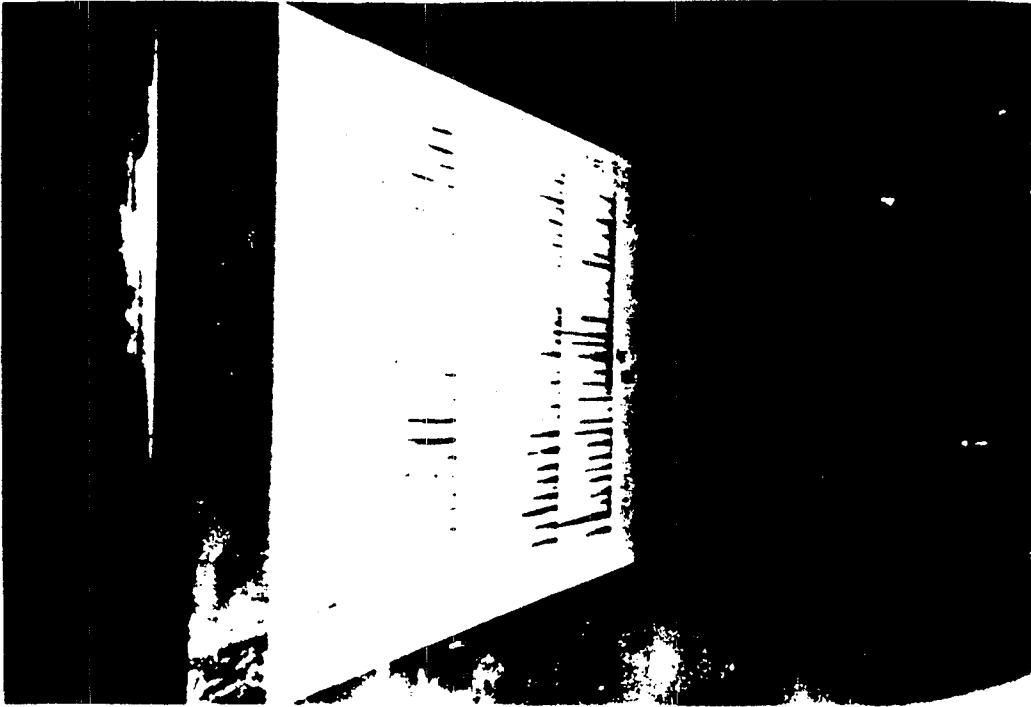
Left lateral door visualization $\alpha = +2^\circ$ $M = 0.6$ non-adapted



[illegible]



Left lateral door visualization $\alpha = -2^\circ$ $M = 0.6$ non-adapted



Use of four base cases

		M=0,6	0,8	NON ADAPTE
+2		147 (*)		(*) ranges 1-4
		122 (**)		(**) ranges 2-5
		167 (***)		(***) ranges 3-6
0		150 (*)	153 (*)	
		107 (**)	108 (**)	
		162 (***)	165 (***)	
-2		156 (*)		
		142 (**)		
		159 (***)		

		M=0,6	0,8	ADAPTE 2-D
+2		146 (*)		
		145 (**)		
		132 (***)		
0		149 (*)	152 (*)	
		136 (**)	134 (**)	
		161 (***)	164 (***)	
-2		155 (*)		
		144 (**)		
		158 (***)		

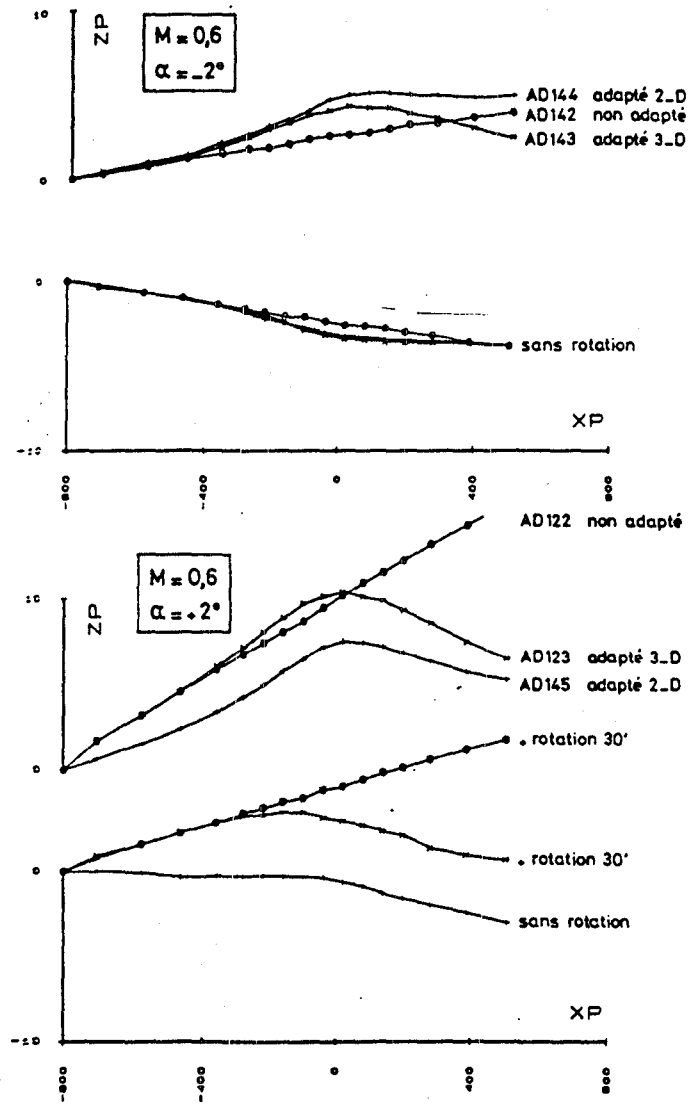
		M=0,6	0,8	ADAPTE 3-D
+2		148 (*)		
		123 (**)		
		182 (***)		
0		151 (*)	154 (*)	
		117 (**)	119 (**)	
		163 (***)	166 (***)	
-2		157 (*)		
		143 (**)		
		150 (***)		

Shape of walls
 Mach on adaptable walls
 Mach on lateral wall
 Kp distribution
 Lift coefficient

Figures 27-28
 Figures 29-32
 Figures 33-36
 Figures 37-44
 Figures 45-50

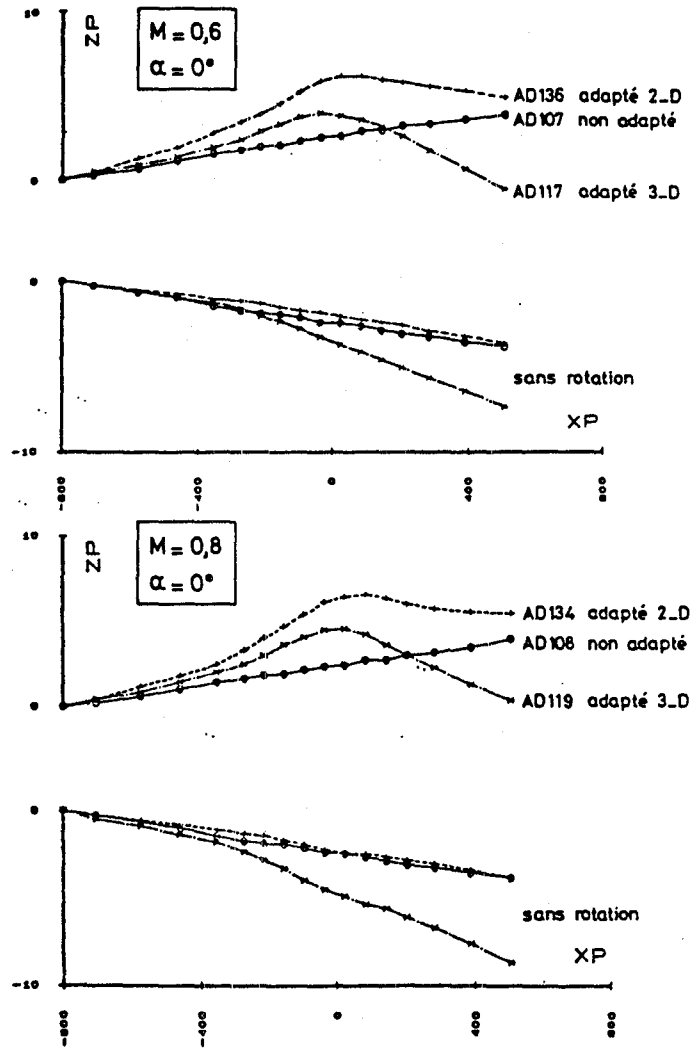
Figure 27

Use of the four base cases - Wall shape



"Sans rotation" = No rotation

Use of the four base cases - Wall shape



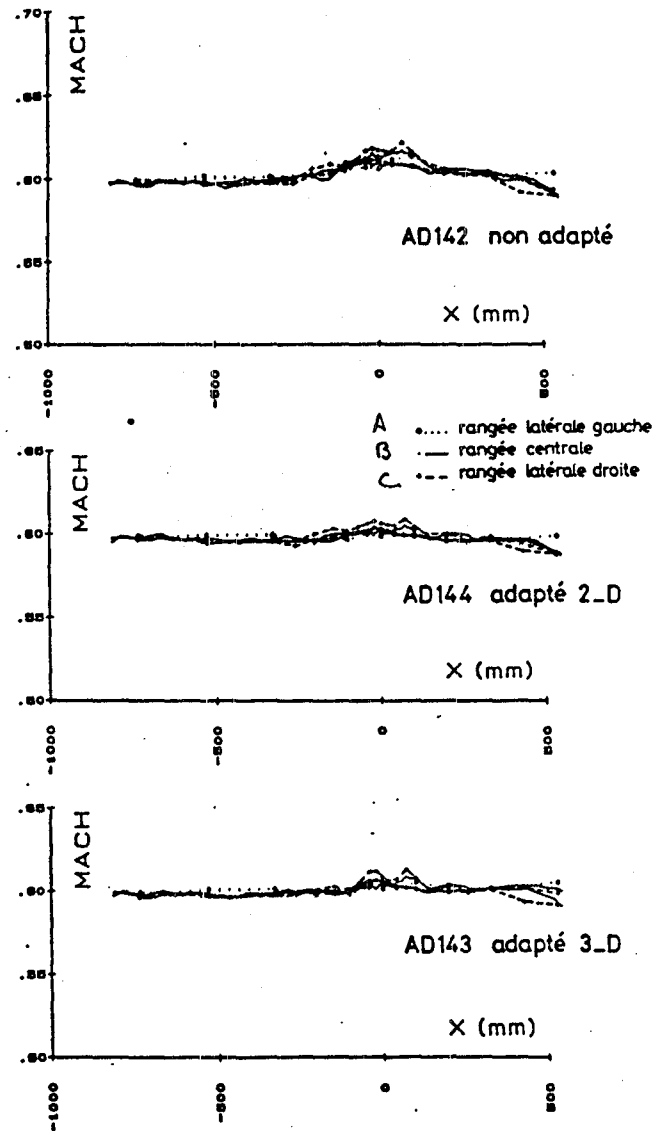
"Sans rotation" = No rotation

Key to Figures 29, 30, 31, and 32:

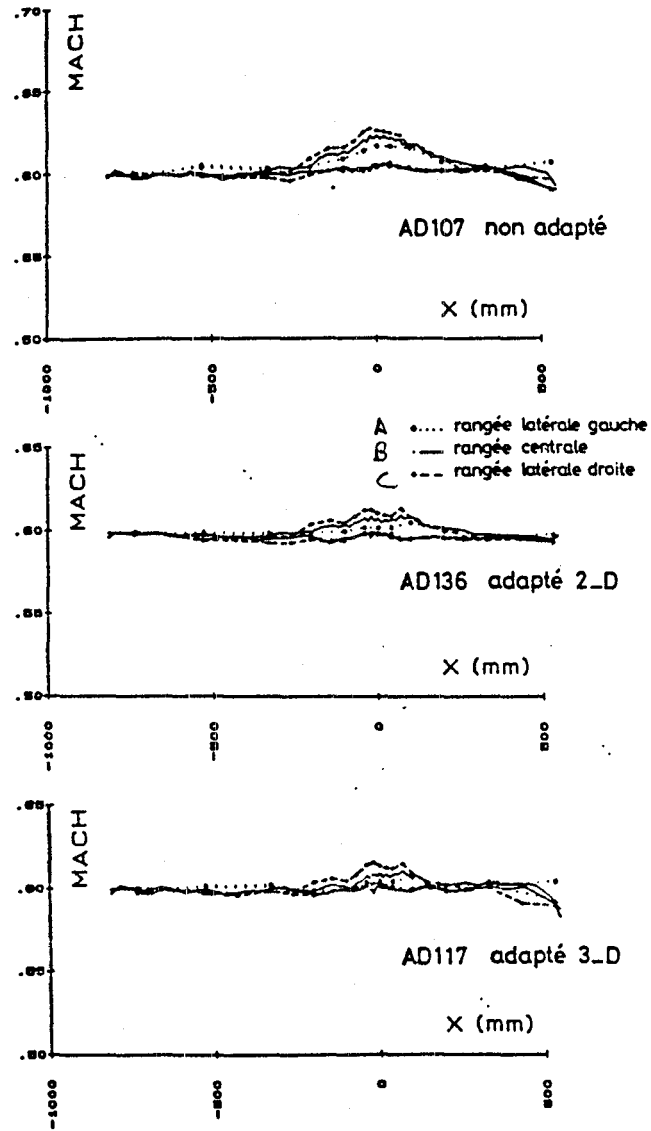
- A - Left lateral row
- B - Central row
- C - Right lateral row

Figure 29

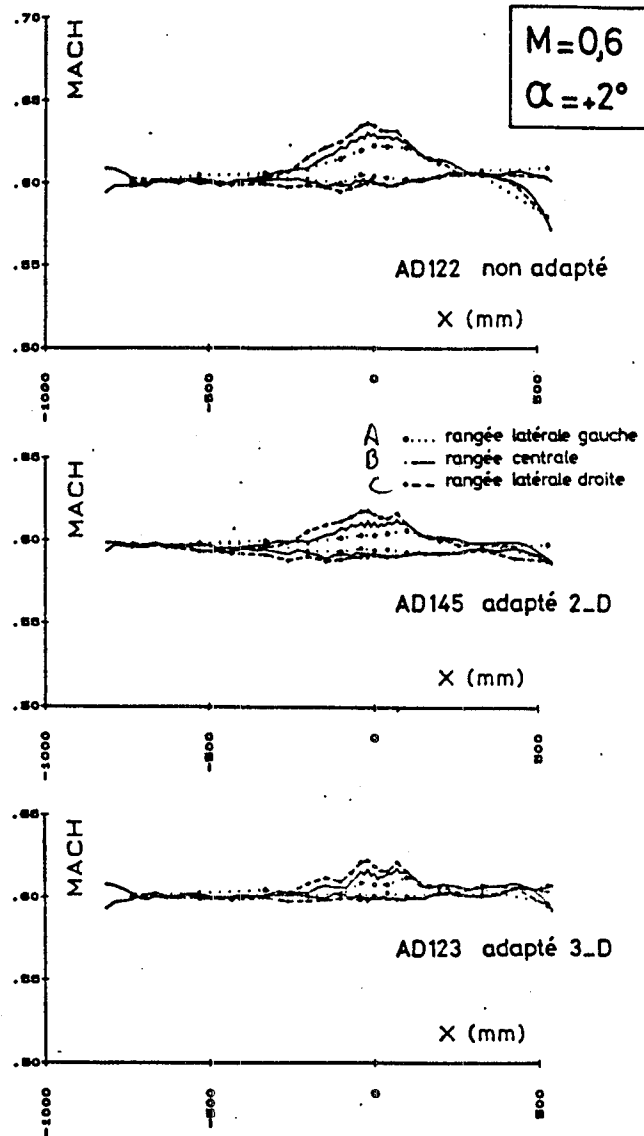
Use of the four base cases - Mach of adaptable walls



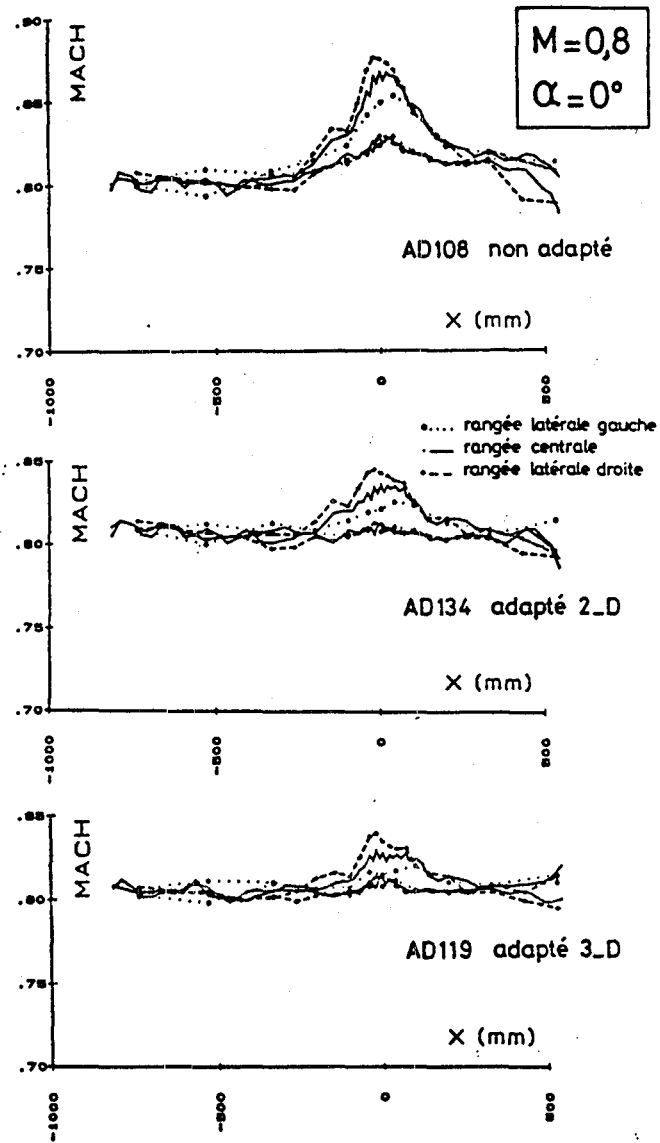
Use of the four base cases - Mach of adaptable walls



Use of the four base cases - Mach of adaptable walls



Use of the four base cases - Mach of adaptable walls



Key to Figures 33, 34, 35, and 36:

A - Vertical rows

° upstream
— middle
· downstream

B - Horizontal rows

° upper
— middle
· lower

Figure 33

Use of the four base cases - Mach of lateral walls

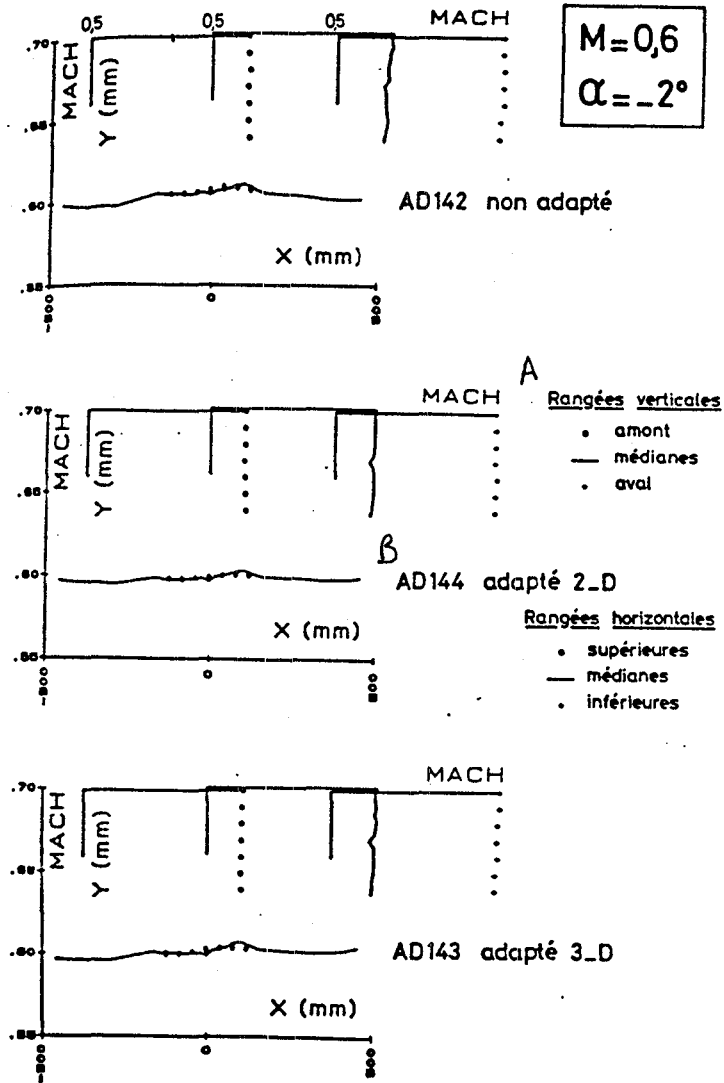


Figure 34

Use of the four base cases - Mach of lateral walls

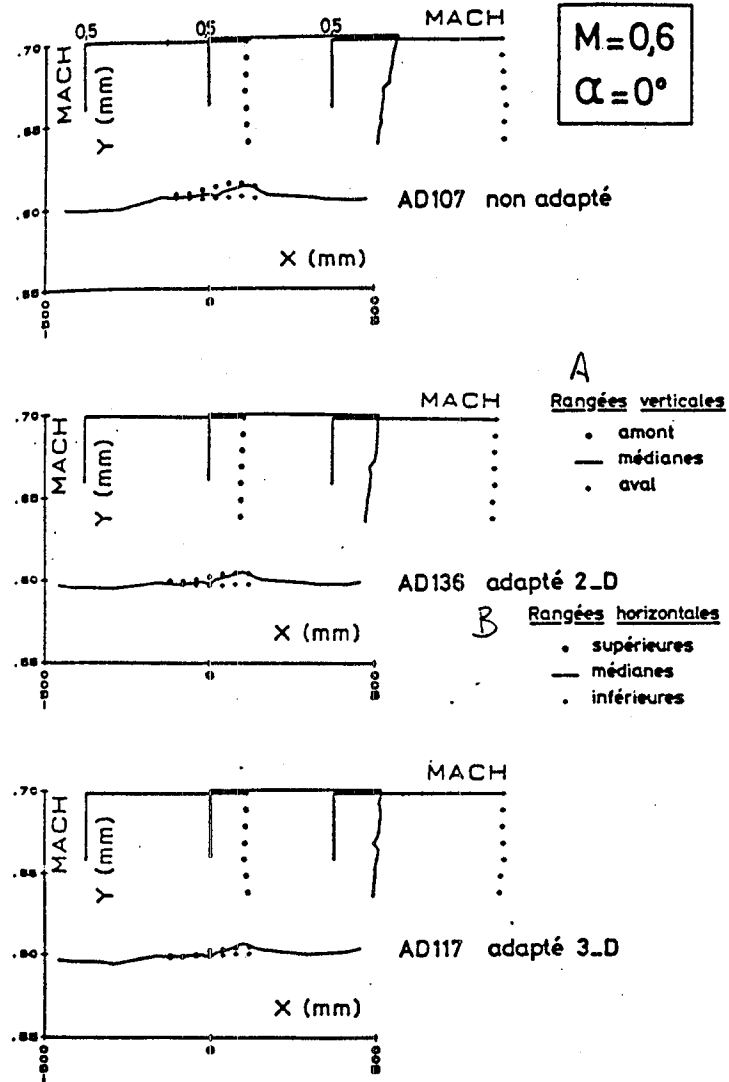
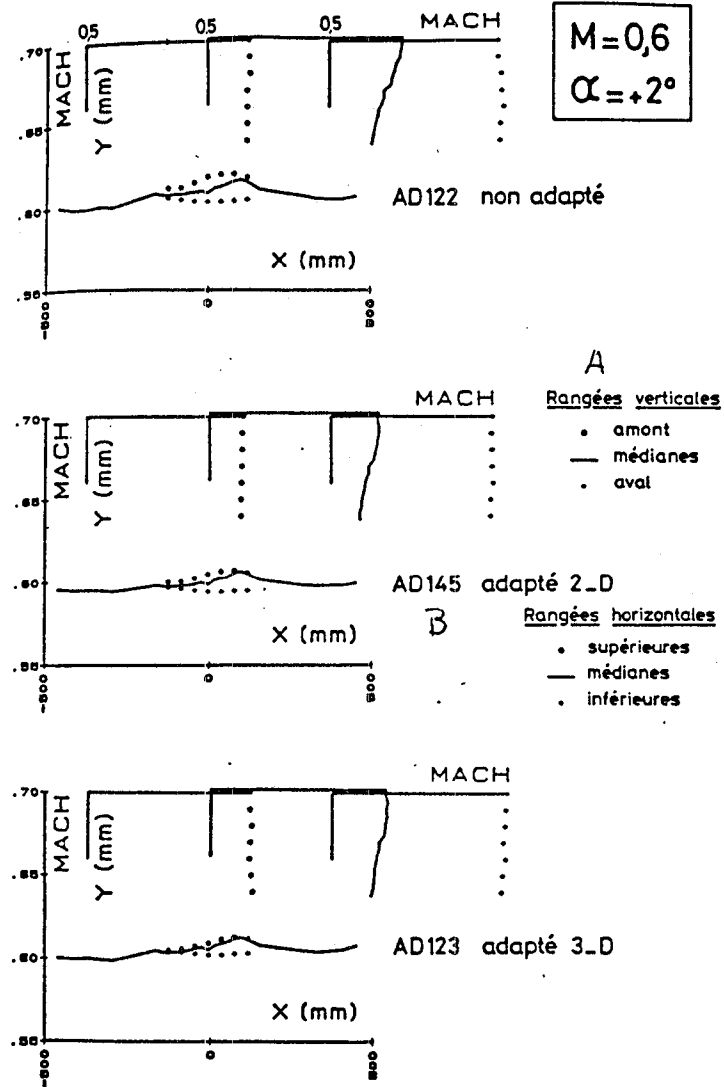


Figure 35

Use of the four base cases - Mach of lateral walls



Use of the four base cases - Mach of lateral walls

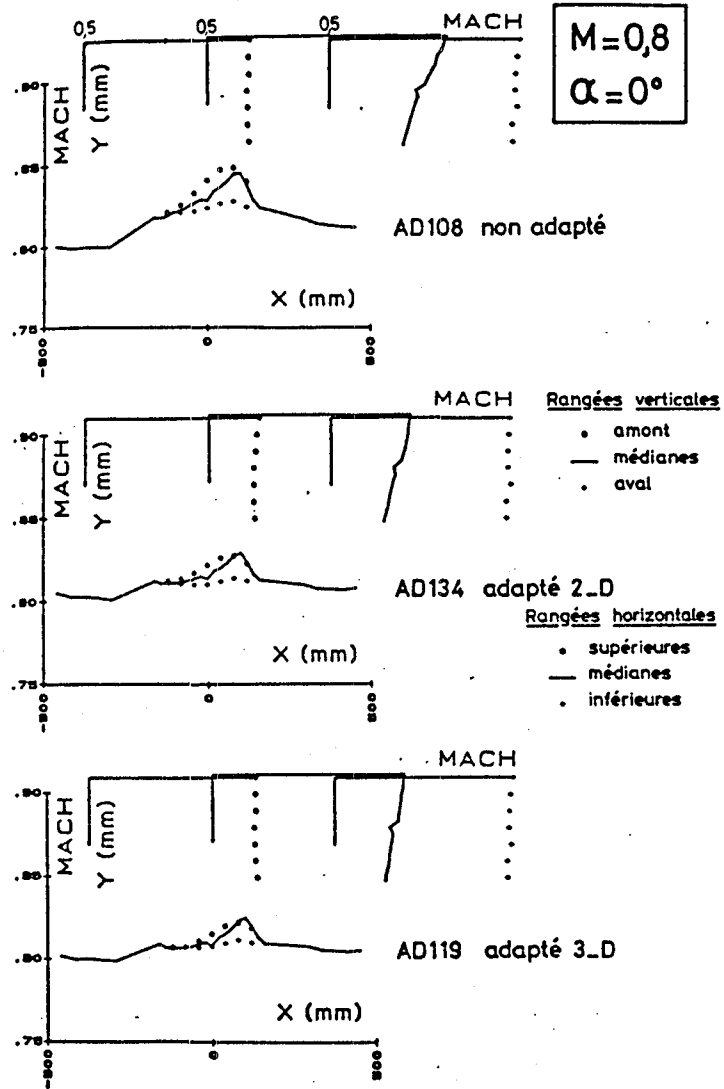


Figure 37

Use of the four base cases - Kp

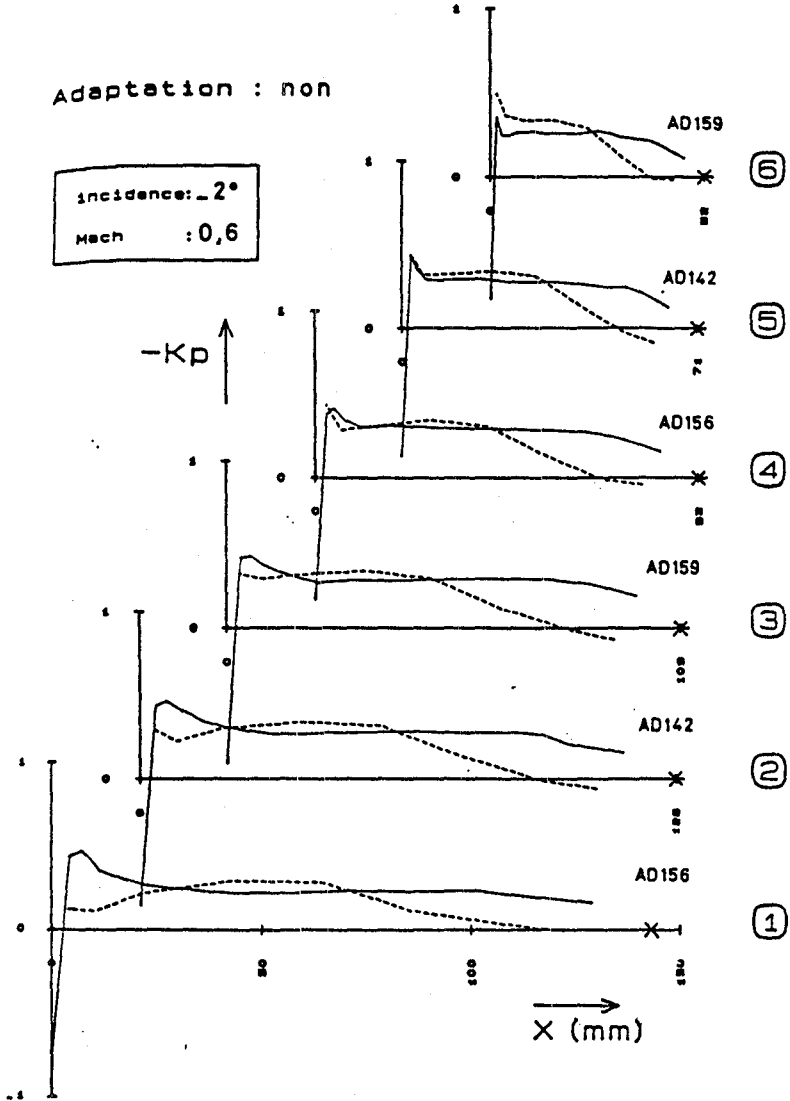


Figure 38

Use of the four base cases - Kp

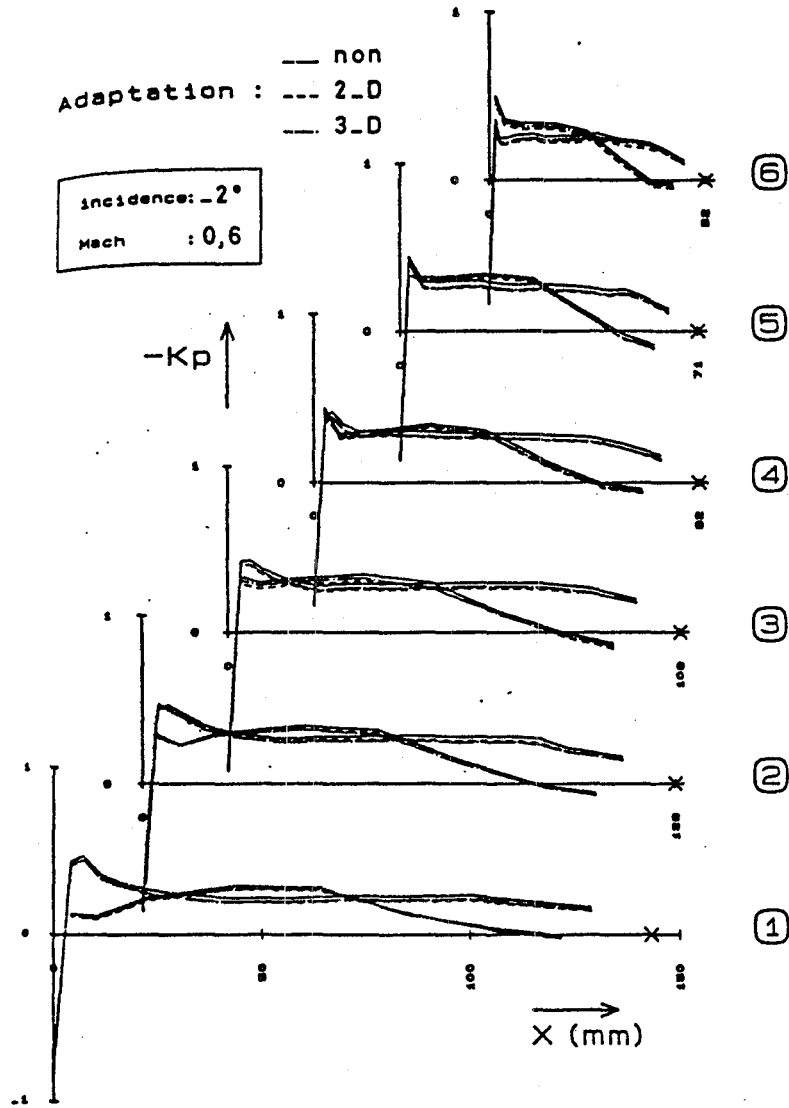


Figure 39

Use of the four base cases - Kp

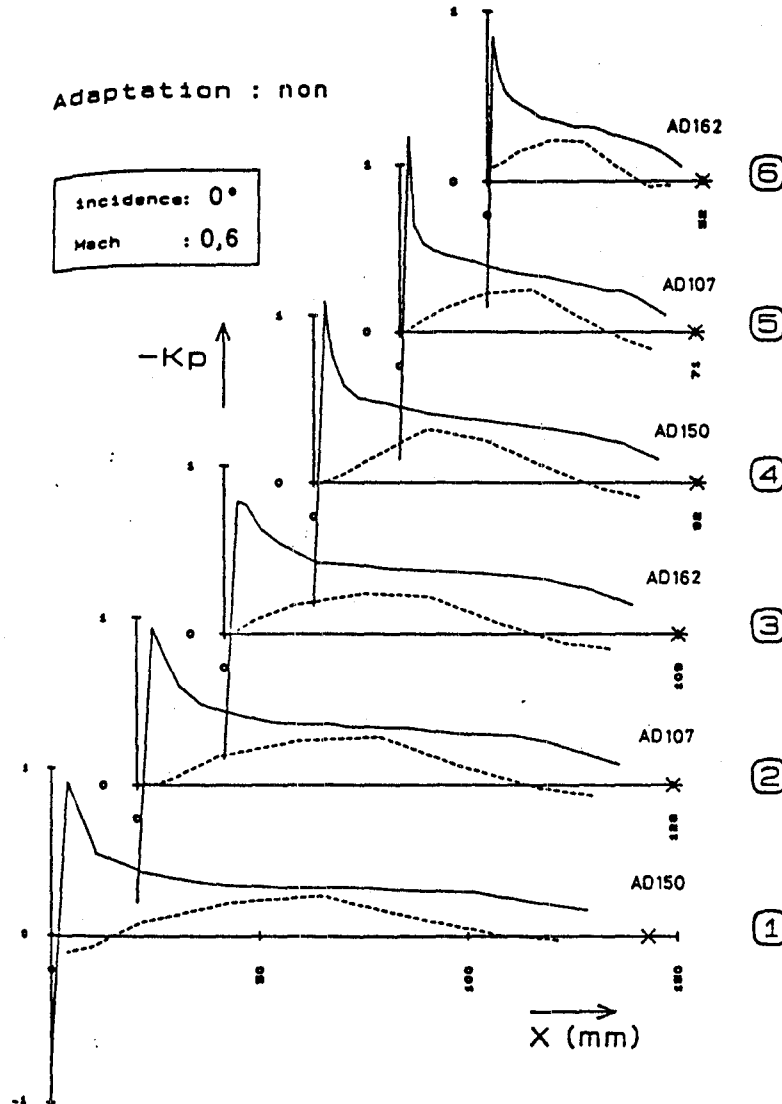


Figure 40

Use of the four base cases - Kp

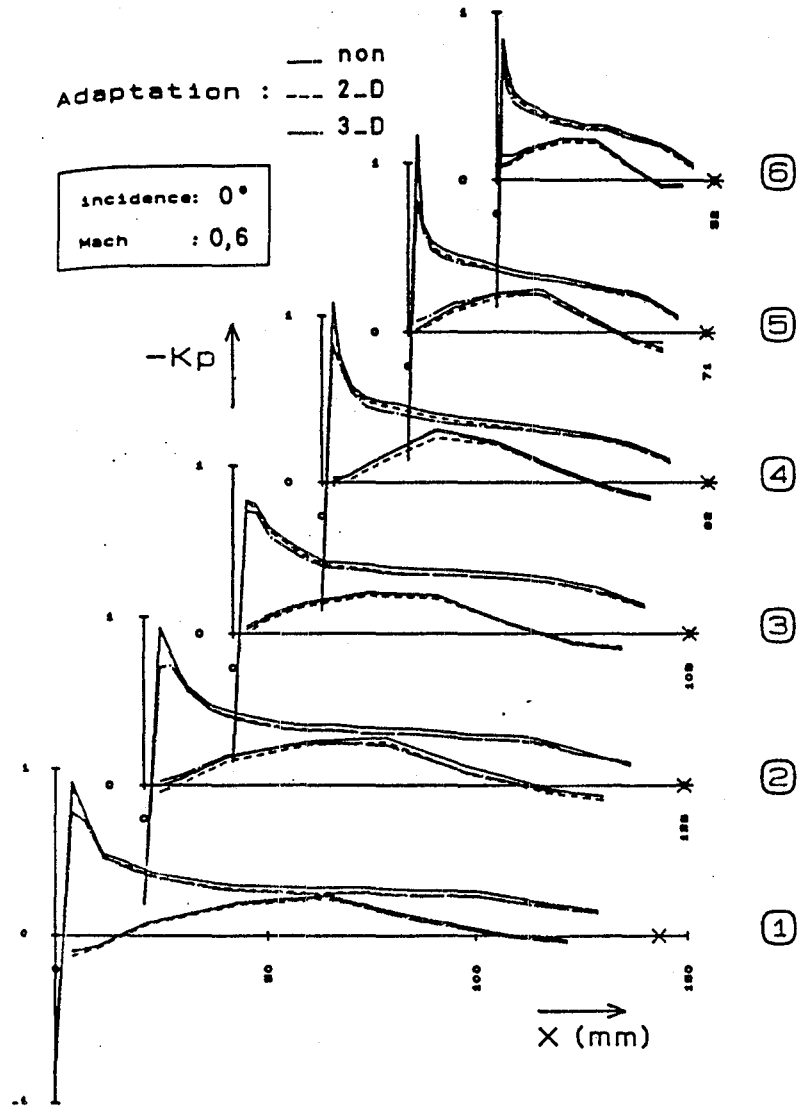


Figure 41

Use of the four base cases - Kp

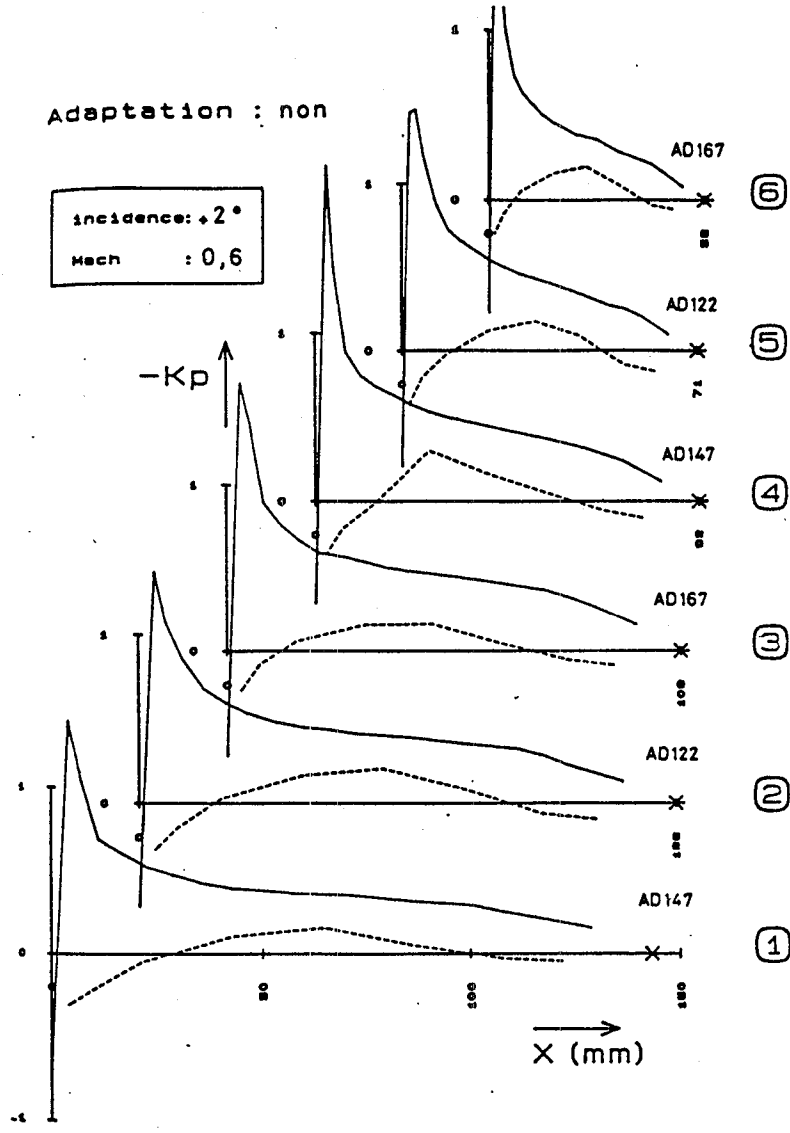


Figure 42

Use of the four base cases - Kp

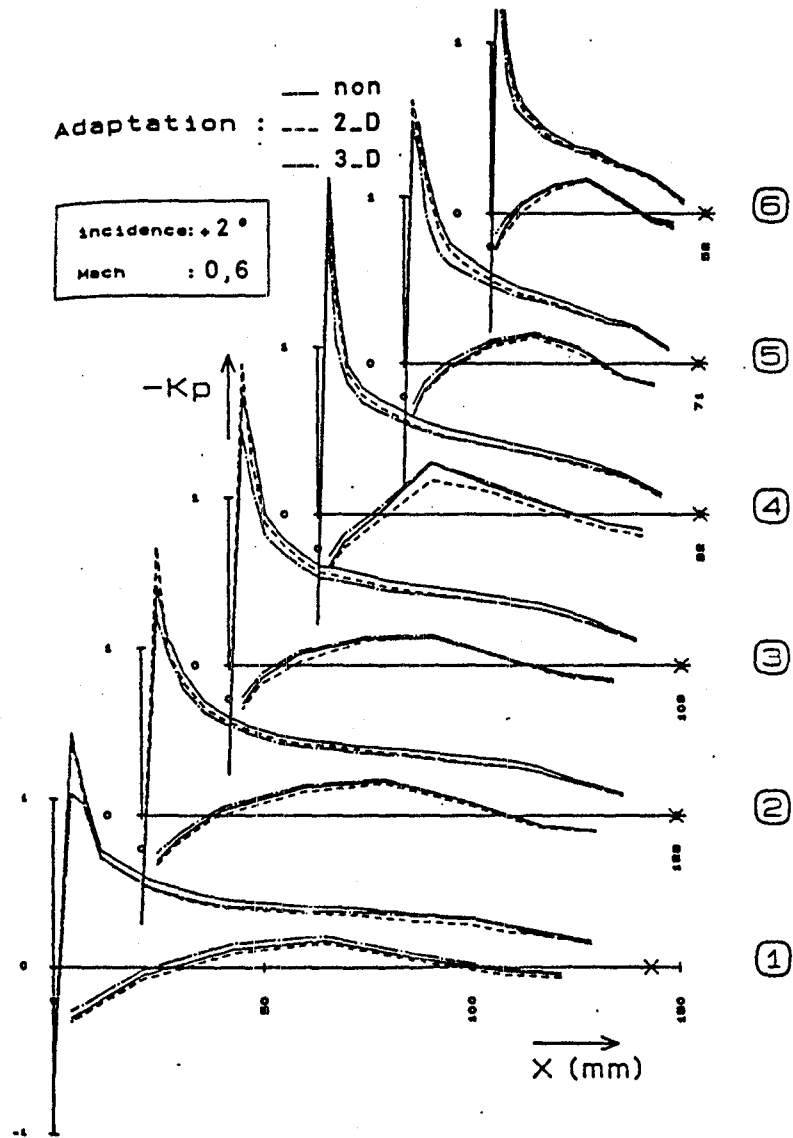


Figure 43

Use of the four base cases - Kp

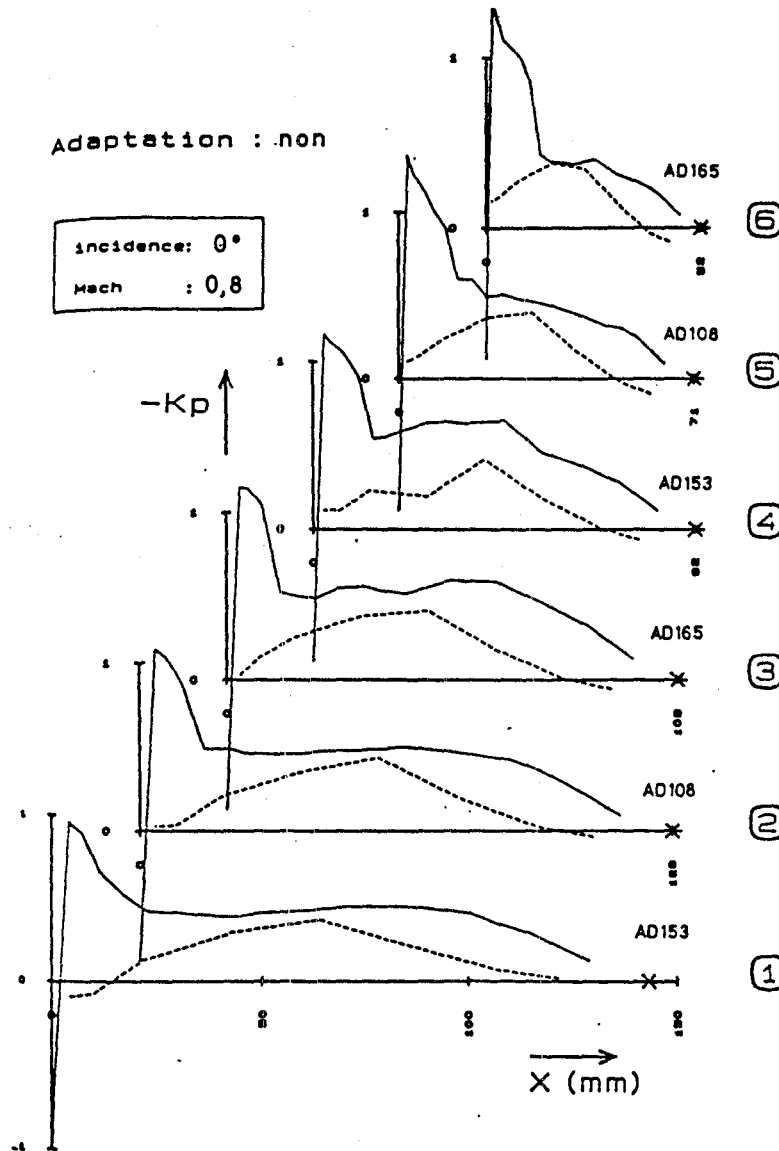
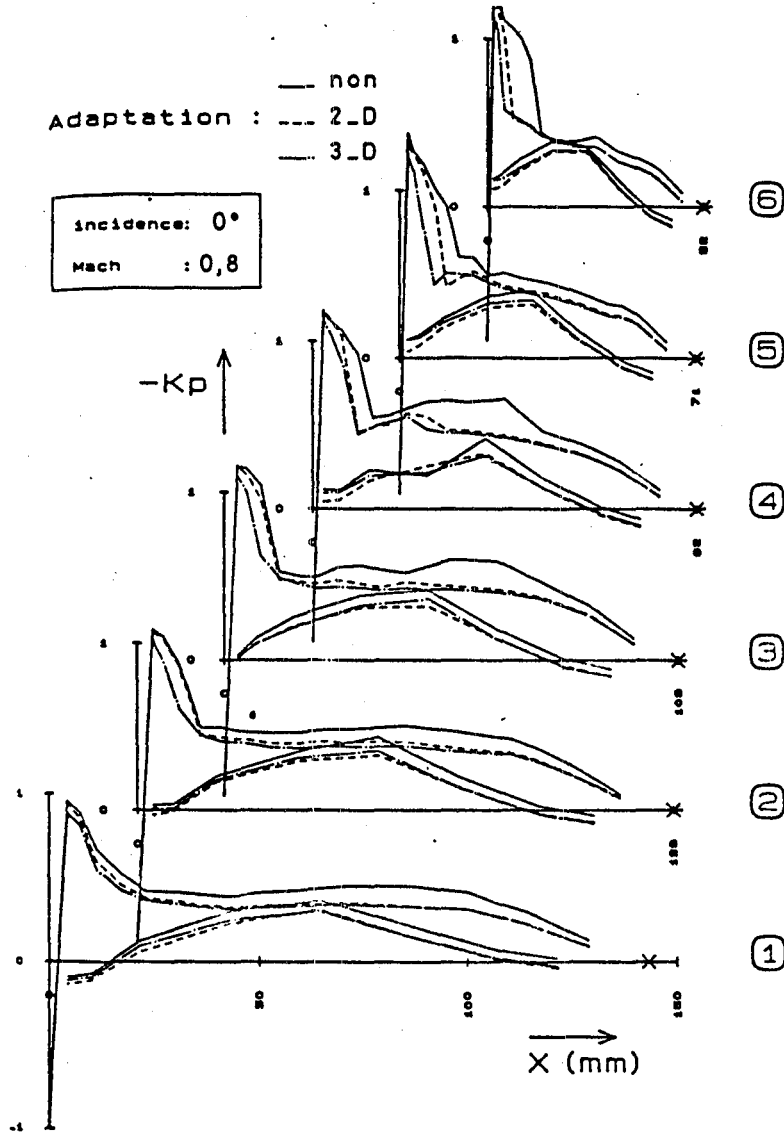


Figure 44

Use of the four base cases - Kp



Use of the four base cases - Cz
Cz recapitulative

Local lift coefficients

	NON ADAPTE	ADAPTE 2-D	ADAPTE 3-D
I = +2 M = 0.6	R 1 : 0.3600	R 1 : 0.3405	R 1 : 0.3027
	R 2 : 0.3726	R 2 : 0.3687	R 2 : 0.3229
	R 3 : 0.4388	R 3 : 0.4237	R 3 : 0.3752
	R 4 : 0.4740	R 4 : 0.4715	R 4 : 0.3861
	R 5 : 0.5091	R 5 : 0.4948	R 5 : 0.4127
	R 6 : 0.4348	R 6 : 0.4250	R 6 : 0.3658
	Aile : 0.448	Aile : 0.438	Aile : 0.371
I = 0 M = 0.6	R 1 : 0.2081	R 1 : 0.1995	R 1 : 0.1865
	R 2 : 0.2154	R 2 : 0.2198	R 2 : 0.1984
	R 3 : 0.2711	R 3 : 0.2537	R 3 : 0.2411
	R 4 : 0.2418	R 4 : 0.2419	R 4 : 0.2076
	R 5 : 0.2351	R 5 : 0.2337	R 5 : 0.1984
	R 6 : 0.1993	R 6 : 0.1926	R 6 : 0.1647
	Aile : 0.231	Aile : 0.227	Aile : 0.200
I = -2 M = 0.6	R 1 : 0.0798	R 1 : 0.0661	R 1 : 0.0687
	R 2 : 0.0888	R 2 : 0.0819	R 2 : 0.0799
	R 3 : 0.0989	R 3 : 0.0949	R 3 : 0.0945
	R 4 : 0.0665	R 4 : 0.0632	R 4 : 0.0607
	R 5 : 0.0561	R 5 : 0.0440	R 5 : 0.0486
	R 6 : 0.0232	R 6 : 0.0207	R 6 : 0.0174
	Aile : 0.066	Aile : 0.059	Aile : 0.052
I = 0 M = 0.8	R 1 : 0.2400	R 1 : 0.2253	R 1 : 0.2034
	R 2 : 0.2545	R 2 : 0.2509	R 2 : 0.2128
	R 3 : 0.3082	R 3 : 0.2842	R 3 : 0.2488
	R 4 : 0.3755	R 4 : 0.3341	R 4 : 0.3026
	R 5 : 0.4150	R 5 : 0.3825	R 5 : 0.2853
	R 6 : 0.4162	R 6 : 0.3193	R 6 : 0.2555
	Aile : 0.353	Aile : 0.315	Aile : 0.263

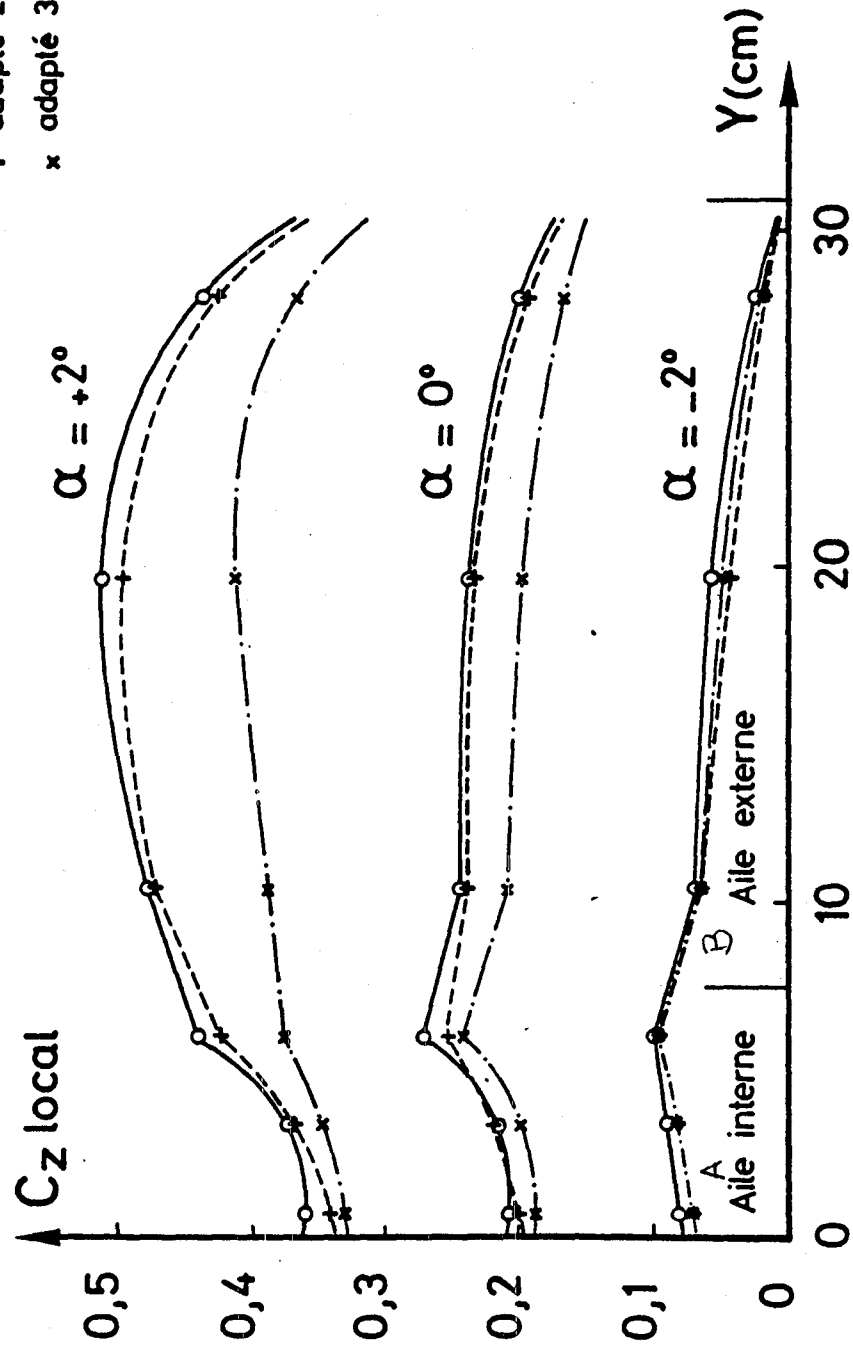
"Aile" = wing

Figure 46

Use of the four base cases - Cz

- o non adapté
- + adapté 2-D
- x adapté 3-D

$M = 0,6$



Key

- A - Internal wing
- B - External wing

Figure 47

Use of the four base cases - C_z

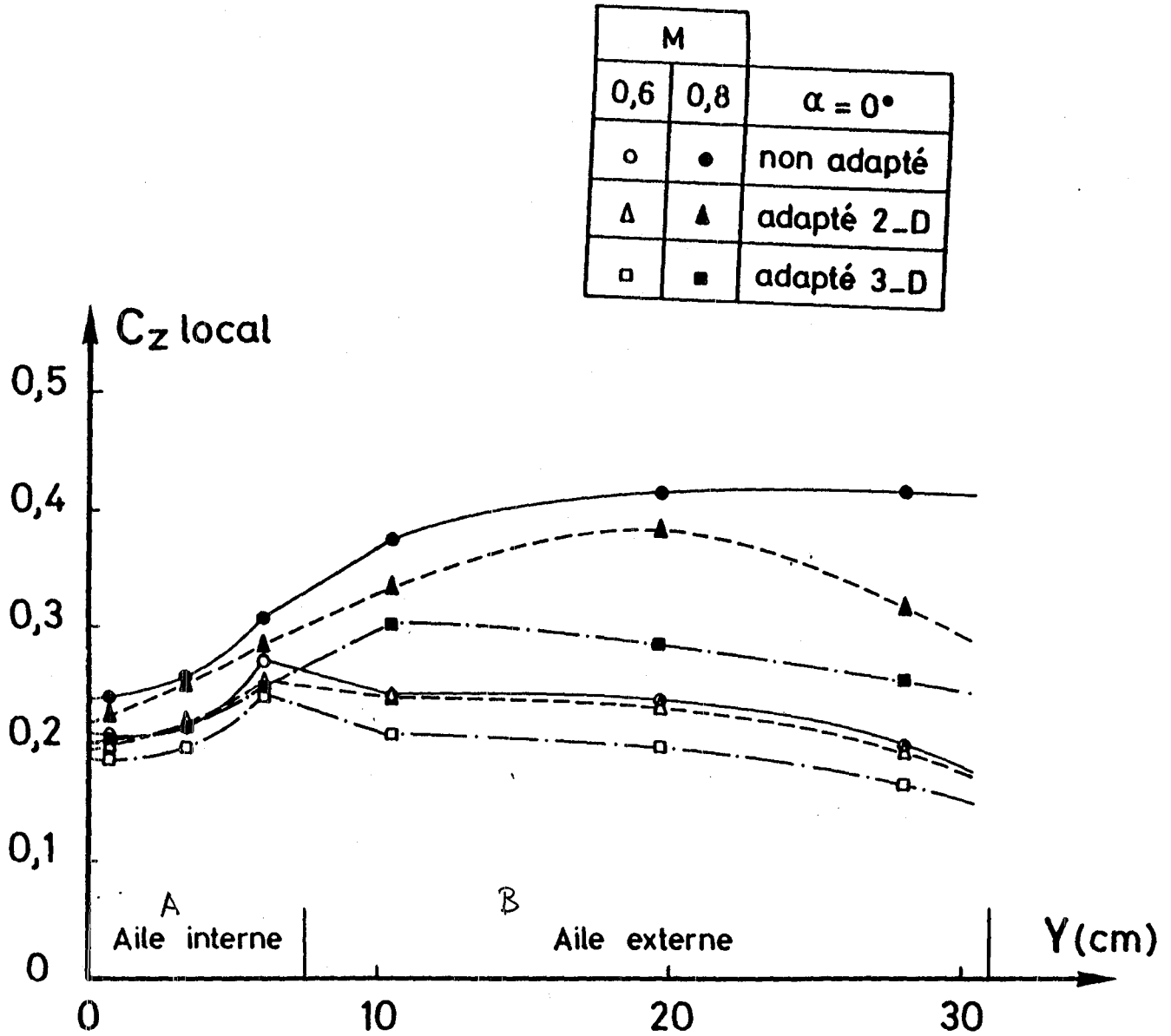
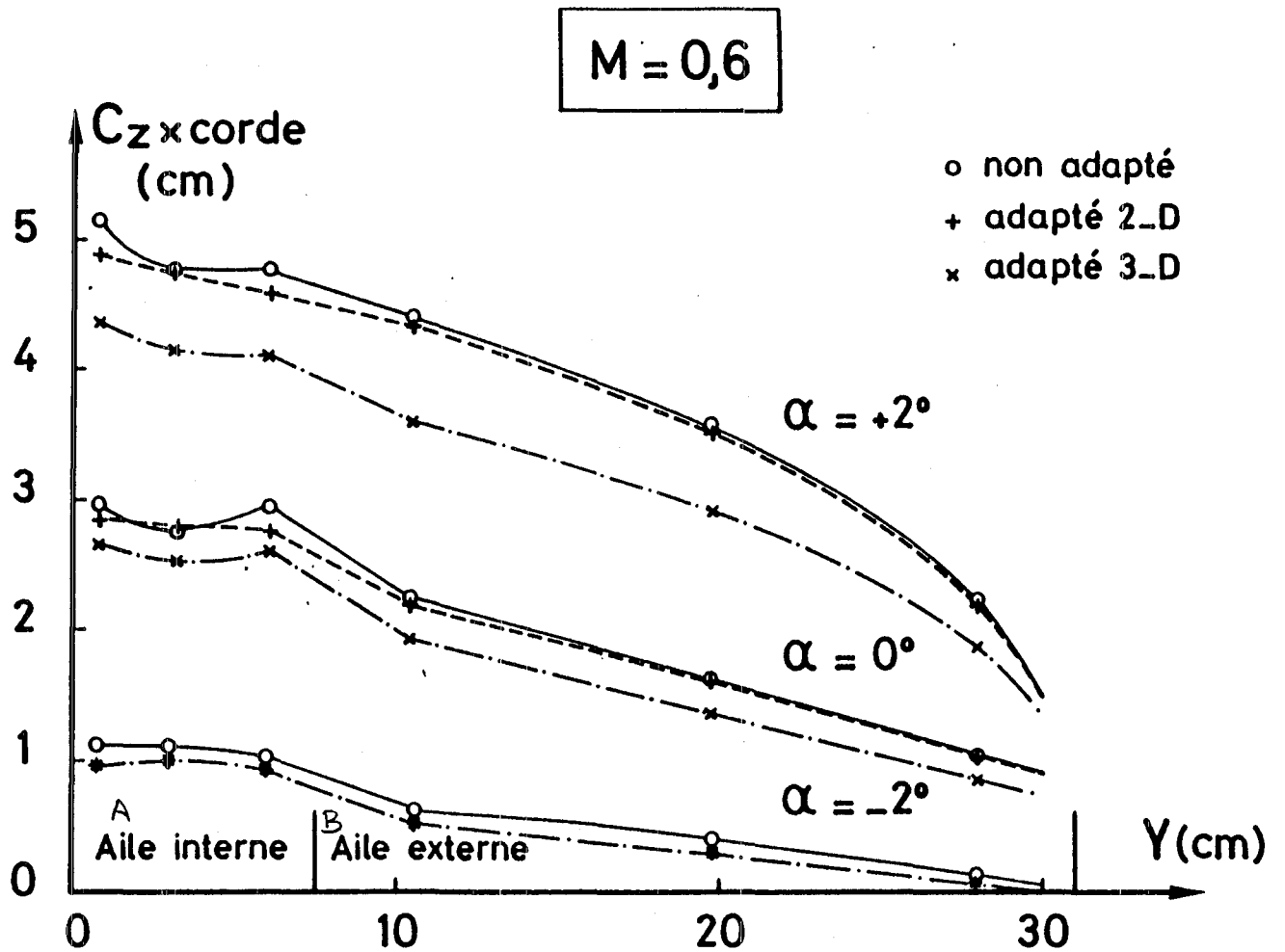


Figure 48

Use of the four base cases - Cz

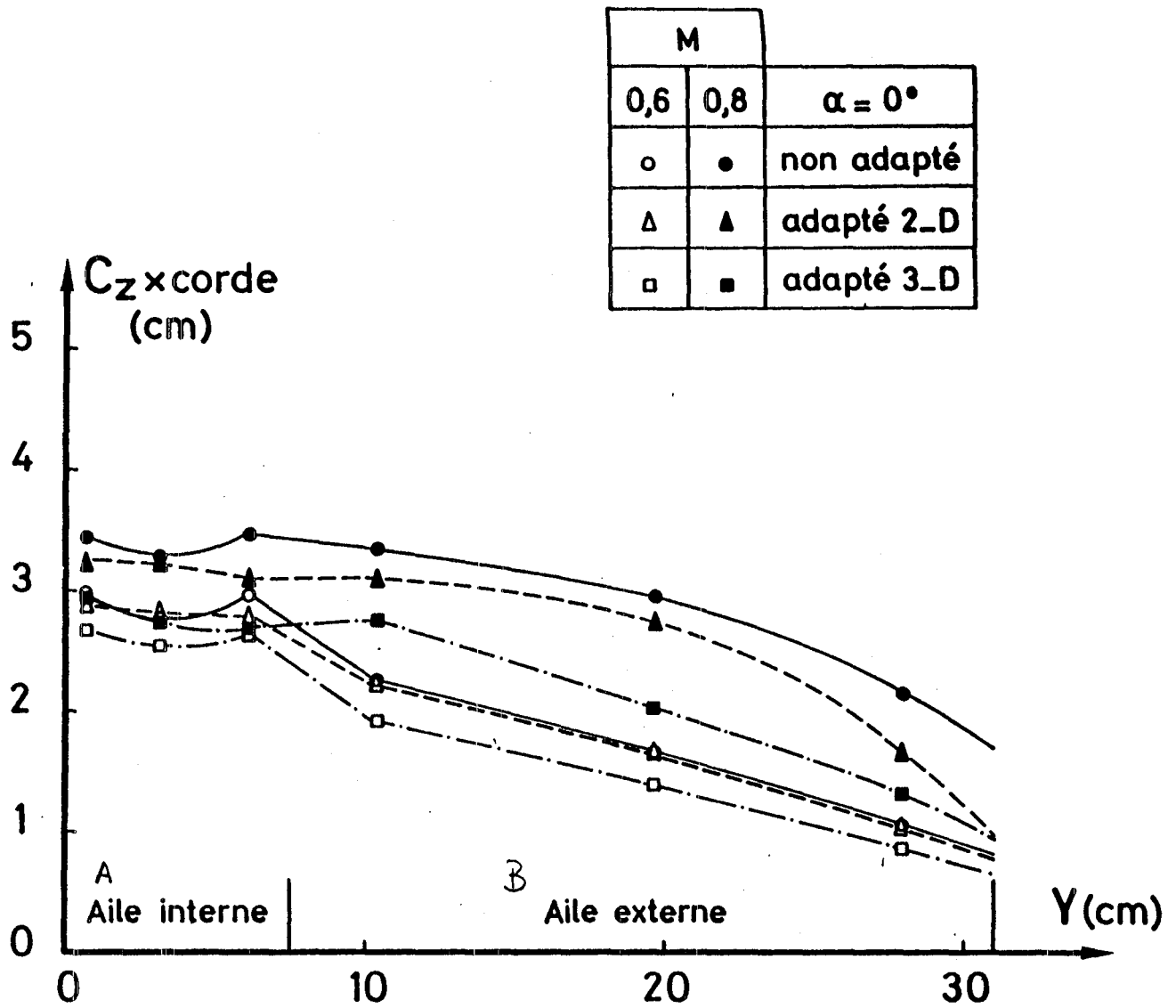


Key

- A - Internal wing
- B - External wing
- C - $C_z \times \text{chord}$

Figure 49

Use of the four base cases - Cz

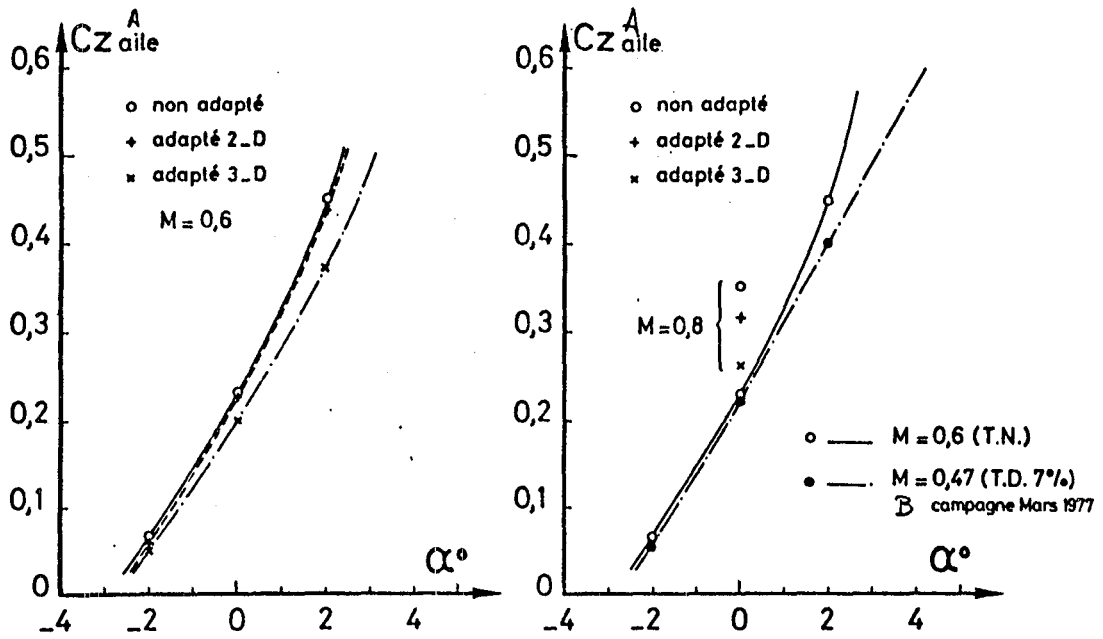


Key

- A ~ Internal wing
- B ~ External wing
- C ~ Cz x chord

Figure 50

Use of the four base cases - Cz



Key

- A - Wing
- B - March 1977 series

Listing of Cz

Key

Fichier = File
Rangee = Row
Corde = Chord

```
*****FICHIER : AD105 **** MACH = .702  INCIDENCE = 0.00  NON
* RANGE : 2      CZ= 2.310E-01  CORDE*CZ= 2.963E+01
* RANGE : 5      CZ= 2.790E-01  CORDE*CZ= 1.978E+01
*****

*****FICHIER : AD107 **** MACH = .599  INCIDENCE = 0.00  NON
* RANGE : 2      CZ= 2.154E-01  CORDE*CZ= 2.763E+01
* RANGE : 5      CZ= 2.351E-01  CORDE*CZ= 1.667E+01
*****

*****FICHIER : AD108 **** MACH = .801  INCIDENCE = 0.00  NON
* RANGE : 2      CZ= 2.545E-01  CORDE*CZ= 3.264E+01
* RANGE : 5      CZ= 4.150E-01  CORDE*CZ= 2.942E+01
*****

*****FICHIER : AD110 **** MACH = .697  INCIDENCE = -2.00  NON
* RANGE : 2      CZ= 6.918E-02  CORDE*CZ= 8.872E+00
* RANGE : 5      CZ= 3.999E-02  CORDE*CZ= 2.835E+00
*****

*****FICHIER : AD115 **** MACH = .702  INCIDENCE = 0.00  3D(1)
* RANGE : 2      CZ= 2.063E-01  CORDE*CZ= 2.645E+01
* RANGE : 5      CZ= 2.215E-01  CORDE*CZ= 1.570E+01
*****

*****FICHIER : AD116 **** MACH = .701  INCIDENCE = 0.00  3D(2)
* RANGE : 2      CZ= 2.050E-01  CORDE*CZ= 2.629E+01
* RANGE : 5      CZ= 2.270E-01  CORDE*CZ= 1.610E+01
*****

*****FICHIER : AD117 **** MACH = .598  INCIDENCE = 0.00  3D(1)
* RANGE : 2      CZ= 1.984E-01  CORDE*CZ= 2.545E+01
* RANGE : 5      CZ= 1.961E-01  CORDE*CZ= 1.390E+01
*****

*****FICHIER : AD118 **** MACH = .806  INCIDENCE = 0.00  3D(1)
* RANGE : 2      CZ= 2.070E-01  CORDE*CZ= 2.655E+01
* RANGE : 5      CZ= 2.732E-01  CORDE*CZ= 1.937E+01
*****

*****FICHIER : AD119 **** MACH = .805  INCIDENCE = 0.00  3D(2)
* RANGE : 2      CZ= 2.128E-01  CORDE*CZ= 2.729E+01
* RANGE : 5      CZ= 2.853E-01  CORDE*CZ= 2.023E+01
*****

*****FICHIER : AD120 **** MACH = .599  INCIDENCE = 2.00  NON
* RANGE : 2      CZ= 3.802E-01  CORDE*CZ= 4.876E+01
* RANGE : 5      CZ= 5.198E-01  CORDE*CZ= 3.685E+01
*****

*****FICHIER : AD122 **** MACH = .600  INCIDENCE = 2.00  NON
* RANGE : 2      CZ= 3.726E-01  CORDE*CZ= 4.779E+01
* RANGE : 5      CZ= 5.091E-01  CORDE*CZ= 3.609E+01
*****
```

*****FICHIER : AD123 **** MACH = .600 INCIDENCE = 2.00 3D(1)
* RANGE : 2 CZ= 3.229E-01 CORDE*CZ= 4.141E+01
* RANGE : 5 CZ= 4.127E-01 CORDE*CZ= 2.926E+01

*****FICHIER : AD124 **** MACH = .703 INCIDENCE = 2.00 NON
* RANGE : 2 CZ= 4.071E-01 CORDE*CZ= 5.221E+01
* RANGE : 5 CZ= 6.103E-01 CORDE*CZ= 4.327E+01

*****FICHIER : AD125 **** MACH = .703 INCIDENCE = 2.00 3D(1)
* RANGE : 2 CZ= 3.361E-01 CORDE*CZ= 4.310E+01
* RANGE : 5 CZ= 4.750E-01 CORDE*CZ= 3.368E+01

*****FICHIER : AD126 **** MACH = .806 INCIDENCE = 2.00 NON
* RANGE : 2 CZ= 5.214E-01 CORDE*CZ= 6.687E+01
* RANGE : 5 CZ= 7.394E-01 CORDE*CZ= 5.242E+01

*****FICHIER : AD127 **** MACH = .806 INCIDENCE = 2.00 3D(1)
* RANGE : 2 CZ= 3.792E-01 CORDE*CZ= 4.863E+01
* RANGE : 5 CZ= 7.103E-01 CORDE*CZ= 5.036E+01

*****FICHIER : AD128 **** MACH = .806 INCIDENCE = 2.00 3D(2)
* RANGE : 2 CZ= 4.116E-01 CORDE*CZ= 5.278E+01
* RANGE : 5 CZ= 7.521E-01 CORDE*CZ= 5.333E+01

*****FICHIER : AD129 **** MACH = .806 INCIDENCE = 2.00 3D(3)
* RANGE : 2 CZ= 3.977E-01 CORDE*CZ= 5.101E+01
* RANGE : 5 CZ= 7.435E-01 CORDE*CZ= 5.272E+01

*****FICHIER : AD130 **** MACH = .707 INCIDENCE = 1.50 2D
* RANGE : 2 CZ= 3.491E-01 CORDE*CZ= 4.477E+01
* RANGE : 5 CZ= 4.996E-01 CORDE*CZ= 3.542E+01

*****FICHIER : AD131 **** MACH = .602 INCIDENCE = 1.50 2D
* RANGE : 2 CZ= 3.210E-01 CORDE*CZ= 4.117E+01
* RANGE : 5 CZ= 4.168E-01 CORDE*CZ= 2.954E+01

*****FICHIER : AD134 **** MACH = .809 INCIDENCE = 0.00 2D
* RANGE : 2 CZ= 2.509E-01 CORDE*CZ= 3.217E+01
* RANGE : 5 CZ= 3.825E-01 CORDE*CZ= 2.712E+01

*****FICHIER : AD135 **** MACH = .702 INCIDENCE = 0.00 2D
* RANGE : 2 CZ= 2.384E-01 CORDE*CZ= 3.058E+01
* RANGE : 5 CZ= 2.758E-01 CORDE*CZ= 1.956E+01

```
*****FICHIER : AD136 **** MACH = .597  INCIDENCE = 0.00  2D
* RANGE : 2      CZ= 2.198E-01  CORDE*CZ= 2.819E+01
* RANGE : 5      CZ= 2.337E-01  CORDE*CZ= 1.657E+01
*****
*****FICHIER : AD137 **** MACH = .598  INCIDENCE = 0.00  NON
* RANGE : 2      CZ= 2.260E-01  CORDE*CZ= 2.898E+01
* RANGE : 5      CZ= 2.451E-01  CORDE*CZ= 1.738E+01
*****
*****FICHIER : AD138 **** MACH = .599  INCIDENCE = 0.00  3D(1)
* RANGE : 2      CZ= 2.004E-01  CORDE*CZ= 2.570E+01
* RANGE : 5      CZ= 1.968E-01  CORDE*CZ= 1.395E+01
*****
*****FICHIER : AD139 **** MACH = .804  INCIDENCE = 0.00  NON
* RANGE : 2      CZ= 2.686E-01  CORDE*CZ= 3.445E+01
* RANGE : 5      CZ= 4.513E-01  CORDE*CZ= 3.199E+01
*****
*****FICHIER : AD140 **** MACH = .804  INCIDENCE = 0.00  3D(1)
* RANGE : 2      CZ= 2.067E-01  CORDE*CZ= 2.651E+01
* RANGE : 5      CZ= 2.645E-01  CORDE*CZ= 1.876E+01
*****
*****FICHIER : AD141 **** MACH = .804  INCIDENCE = 0.00  3D(2)
* RANGE : 2      CZ= 2.222E-01  CORDE*CZ= 2.850E+01
* RANGE : 5      CZ= 2.991E-01  CORDE*CZ= 2.120E+01
*****
*****FICHIER : AD142 **** MACH = .598  INCIDENCE = -2.00  NON
* RANGE : 2      CZ= 8.875E-02  CORDE*CZ= 1.138E+01
* RANGE : 5      CZ= 5.611E-02  CORDE*CZ= 3.978E+00
*****
*****FICHIER : AD143 **** MACH = .598  INCIDENCE = -2.00  3D(1)
* RANGE : 2      CZ= 7.990E-02  CORDE*CZ= 1.025E+01
* RANGE : 5      CZ= 4.859E-02  CORDE*CZ= 3.445E+00
*****
*****FICHIER : AD144 **** MACH = .596  INCIDENCE = -2.00  2D
* RANGE : 2      CZ= 8.189E-02  CORDE*CZ= 1.050E+01
* RANGE : 5      CZ= 4.395E-02  CORDE*CZ= 3.116E+00
*****
*****FICHIER : AD145 **** MACH = .596  INCIDENCE = 2.00  2D
* RANGE : 2      CZ= 3.687E-01  CORDE*CZ= 4.729E+01
* RANGE : 5      CZ= 4.948E-01  CORDE*CZ= 3.508E+01
*****
*****FICHIER : AD146 **** MACH = .594  INCIDENCE = 2.00  2D
* RANGE : 1      CZ= 3.405E-01  CORDE*CZ= 4.872E+01
* RANGE : 4      CZ= 4.715E-01  CORDE*CZ= 4.344E+01
*****
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*****FICHIER : AD147 **** MACH = .593  INCIDENCE = 2.00  NON
* RANGE : 1      CZ= 3.600E-01  CORDE*CZ= 5.151E+01
* RANGE : 4      CZ= 4.740E-01  CORDE*CZ= 4.367E+01
*****

*****FICHIER : AD148 **** MACH = .594  INCIDENCE = 2.00  3D(1)
* RANGE : 1      CZ= 3.027E-01  CORDE*CZ= 4.332E+01
* RANGE : 4      CZ= 3.861E-01  CORDE*CZ= 3.557E+01
*****

*****FICHIER : AD149 **** MACH = .594  INCIDENCE = 0.00  2D
* RANGE : 1      CZ= 1.995E-01  CORDE*CZ= 2.855E+01
* RANGE : 4      CZ= 2.419E-01  CORDE*CZ= 2.228E+01
*****

*****FICHIER : AD150 **** MACH = .595  INCIDENCE = 0.00  NON
* RANGE : 1      CZ= 2.081E-01  CORDE*CZ= 2.978E+01
* RANGE : 4      CZ= 2.418E-01  CORDE*CZ= 2.228E+01
*****

*****FICHIER : AD151 **** MACH = .594  INCIDENCE = 0.00  3D(1)
* RANGE : 1      CZ= 1.865E-01  CORDE*CZ= 2.669E+01
* RANGE : 4      CZ= 2.076E-01  CORDE*CZ= 1.913E+01
*****

*****FICHIER : AD152 **** MACH = .802  INCIDENCE = 0.00  2D
* RANGE : 1      CZ= 2.253E-01  CORDE*CZ= 3.225E+01
* RANGE : 4      CZ= 3.341E-01  CORDE*CZ= 3.078E+01
*****

*****FICHIER : AD153 **** MACH = .803  INCIDENCE = 0.00  NON
* RANGE : 1      CZ= 2.400E-01  CORDE*CZ= 3.434E+01
* RANGE : 4      CZ= 3.755E-01  CORDE*CZ= 3.460E+01
*****

*****FICHIER : AD154 **** MACH = .803  INCIDENCE = 0.00  3D(1)
* RANGE : 1      CZ= 2.034E-01  CORDE*CZ= 2.911E+01
* RANGE : 4      CZ= 3.026E-01  CORDE*CZ= 2.788E+01
*****

*****FICHIER : AD155 **** MACH = .595  INCIDENCE = -2.00  2D
* RANGE : 1      CZ= 6.814E-02  CORDE*CZ= 9.751E+00
* RANGE : 4      CZ= 6.321E-02  CORDE*CZ= 5.824E+00
*****

*****FICHIER : AD156 **** MACH = .596  INCIDENCE = -2.00  NON
* RANGE : 1      CZ= 7.980E-02  CORDE*CZ= 1.142E+01
* RANGE : 4      CZ= 6.654E-02  CORDE*CZ= 6.131E+00
*****

*****FICHIER : AD157 **** MACH = .596  INCIDENCE = -2.00  3D(1)
* RANGE : 1      CZ= 6.874E-02  CORDE*CZ= 9.836E+00
* RANGE : 4      CZ= 6.066E-02  CORDE*CZ= 5.589E+00
*****
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```
****FICHIER : AD158 **** MACH = .595  INCIDENCE =-2.00  2D
* RANGE  : 3      CZ= 9.486E-02  CORDE*CZ= 1.030E+01
* RANGE  : 6      CZ= 2.071E-02  CORDE*CZ= 1.070E+00
*****

****FICHIER : AD159 **** MACH = .596  INCIDENCE =-2.00  NON
* RANGE  : 3      CZ= 9.893E-02  CORDE*CZ= 1.074E+01
* RANGE  : 6      CZ= 2.323E-02  CORDE*CZ= 1.200E+00
*****

****FICHIER : AD160 **** MACH = .596  INCIDENCE =-2.00  3D(1)
* RANGE  : 3      CZ= 9.454E-02  CORDE*CZ= 1.026E+01
* RANGE  : 6      CZ= 1.742E-02  CORDE*CZ= 8.998E-01
*****

****FICHIER : AD161 **** MACH = .597  INCIDENCE = 0.00  2D
* RANGE  : 3      CZ= 2.537E-01  CORDE*CZ= 2.754E+01
* RANGE  : 6      CZ= 1.926E-01  CORDE*CZ= 9.945E+00
*****

****FICHIER : AD162 **** MACH = .598  INCIDENCE = 0.00  NON
* RANGE  : 3      CZ= 2.711E-01  CORDE*CZ= 2.943E+01
* RANGE  : 6      CZ= 1.993E-01  CORDE*CZ= 1.029E+01
*****

****FICHIER : AD163 **** MACH = .598  INCIDENCE = 0.00  3D(1)
* RANGE  : 3      CZ= 2.411E-01  CORDE*CZ= 2.617E+01
* RANGE  : 6      CZ= 1.647E-01  CORDE*CZ= 8.506E+00
*****

****FICHIER : AD164 **** MACH = .807  INCIDENCE = 0.00  2D
* RANGE  : 3      CZ= 2.842E-01  CORDE*CZ= 3.085E+01
* RANGE  : 6      CZ= 3.193E-01  CORDE*CZ= 1.649E+01
*****

****FICHIER : AD165 **** MACH = .805  INCIDENCE = 0.00  NON
* RANGE  : 3      CZ= 3.082E-01  CORDE*CZ= 3.346E+01
* RANGE  : 6      CZ= 4.162E-01  CORDE*CZ= 2.150E+01
*****

****FICHIER : AD166 **** MACH = .804  INCIDENCE = 0.00  3D(1)
* RANGE  : 3      CZ= 2.488E-01  CORDE*CZ= 2.701E+01
* RANGE  : 6      CZ= 2.555E-01  CORDE*CZ= 1.320E+01
*****

****FICHIER : AD167 **** MACH = .599  INCIDENCE = 2.00  NON
* RANGE  : 3      CZ= 4.388E-01  CORDE*CZ= 4.763E+01
* RANGE  : 6      CZ= 4.348E-01  CORDE*CZ= 2.246E+01
*****

****FICHIER : AD168 **** MACH = .599  INCIDENCE = 2.00  3D(1)
* RANGE  : 3      CZ= 3.752E-01  CORDE*CZ= 4.074E+01
* RANGE  : 6      CZ= 3.658E-01  CORDE*CZ= 1.889E+01
*****

****FICHIER : AD169 **** MACH = .599  INCIDENCE = 2.00  2D
* RANGE  : 3      CZ= 4.237E-01  CORDE*CZ= 4.600E+01
* RANGE  : 6      CZ= 4.250E-01  CORDE*CZ= 2.195E+01
*****
```

Listing of Adaptable Wall Shapes

Listing of adaptable wall shapes (rows 2-5)

ADAPT.:	FORME	MACH	INCIDENCE
:	DEPART	0,6 : 0,8	:
NON	AD445	122	
2-D		145	+2
3-D	AD9122	123	
NON	AD4 AD4	107 : 108	
2-D		136 : 134	0
3-D	AD9107 AD9118	117 : 119	
NON	AD4	142	
2-D		144	-2
3-D	AD9142	143	

Forme depart = Beginning shape

File: AD136
Lines of current (mm)

File: AD134
Lines of current (mm)

N	Absc	1/2 L.C.	Haut	1/2 L.C.	Bas
1	-800.1	0.00	0.00		
2	-784.7	0.07	0.04		
3	-711.4	0.14	0.09		
4	-670.0	0.22	0.14		
5	-630.4	0.30	0.19		
6	-582.6	0.38	0.23		
7	-556.5	0.48	0.28		
8	-522.0	0.57	0.32		
9	-489.0	0.67	0.35		
10	-457.6	0.78	0.38		
11	-427.5	0.90	0.40		
12	-399.7	1.04	0.42		
13	-371.2	1.19	0.46		
14	-345.0	1.32	0.48		
15	-319.9	1.46	0.51		
16	-295.9	1.59	0.52		
17	-273.0	1.72	0.52		
18	-251.2	1.84	0.52		
19	-230.3	1.99	0.53		
20	-210.3	2.11	0.54		
21	-191.2	2.26	0.57		
22	-174.4	2.40	0.60		
23	-159.3	2.52	0.62		
24	-145.6	2.63	0.63		
25	-132.8	2.72	0.62		
26	-120.9	2.81	0.61		
27	-109.7	2.89	0.60		
28	-99.08	2.97	0.59		
29	-89.09	3.05	0.59		
30	-79.09	3.13	0.59		
31	-69.60	3.20	0.58		
32	-60.39	3.27	0.57		
33	-51.39	3.34	0.56		
34	-42.57	3.39	0.55		
35	-33.99	3.43	0.55		
36	-25.33	3.47	0.55		
37	-16.94	3.49	0.54		
38	-8.41	3.51	0.53		
39	0.00	3.51	0.52		
40	8.41	3.51	0.52		
41	16.84	3.51	0.52		
42	25.43	3.51	0.52		
43	33.89	3.51	0.52		
44	42.57	3.50	0.53		
45	51.39	3.49	0.53		
46	60.39	3.49	0.53		
47	69.60	3.46	0.54		
48	79.09	3.43	0.54		
49	88.99	3.38	0.54		
50	99.08	3.33	0.53		
51	109.73	3.27	0.53		
52	120.94	3.18	0.52		
53	132.83	3.08	0.52		
54	145.56	2.97	0.51		
55	159.33	2.86	0.49		
56	174.43	2.75	0.48		
57	191.23	2.67	0.47		
58	210.31	2.57	0.46		
59	230.27	2.45	0.45		
60	251.17	2.31	0.44		
61	273.05	2.15	0.44		
62	295.94	1.99	0.44		
63	319.90	1.84	0.43		
64	344.99	1.70	0.43		
65	371.23	1.55	0.43		
66	398.70	1.40	0.41		
67	427.46	1.25	0.38		
68	457.55	1.11	0.36		
69	489.05	0.99	0.33		
70	522.01	0.87	0.30		

N	Absc	1/2 L.C.	Haut	1/2 L.C.	Bas
1	-800.1	0.00	0.00		
2	-784.7	0.06	0.04		
3	-711.4	0.13	0.07		
4	-670.0	0.20	0.10		
5	-630.4	0.28	0.14		
6	-582.6	0.36	0.17		
7	-556.5	0.45	0.20		
8	-522.0	0.54	0.24		
9	-489.0	0.63	0.28		
10	-457.6	0.74	0.32		
11	-427.5	0.83	0.35		
12	-399.7	0.97	0.38		
13	-371.2	1.11	0.41		
14	-345.0	1.27	0.44		
15	-319.9	1.43	0.46		
16	-295.9	1.60	0.48		
17	-273.0	1.76	0.49		
18	-251.2	1.91	0.49		
19	-230.3	2.07	0.49		
20	-210.3	2.24	0.48		
21	-191.2	2.42	0.47		
22	-174.4	2.60	0.46		
23	-159.3	2.75	0.45		
24	-145.6	2.89	0.44		
25	-132.8	3.00	0.43		
26	-120.9	3.09	0.42		
27	-109.7	3.18	0.41		
28	-99.08	3.27	0.40		
29	-89.09	3.37	0.39		
30	-79.09	3.46	0.38		
31	-69.60	3.55	0.37		
32	-60.39	3.64	0.36		
33	-51.39	3.73	0.35		
34	-42.57	3.82	0.34		
35	-33.99	3.92	0.33		
36	-25.33	3.99	0.32		
37	-16.94	4.07	0.31		
38	-8.41	4.05	0.30		
39	0.00	4.07	0.29		
40	8.41	4.09	0.28		
41	16.84	4.09	0.27		
42	25.43	4.09	0.26		
43	33.89	4.09	0.25		
44	42.57	4.09	0.24		
45	51.39	4.08	0.23		
46	60.39	4.06	0.22		
47	69.60	4.03	0.21		
48	79.09	3.99	0.20		
49	88.99	3.92	0.19		
50	99.08	3.85	0.18		
51	109.73	3.76	0.17		
52	120.94	3.65	0.16		
53	132.83	3.53	0.15		
54	145.56	3.41	0.14		
55	159.33	3.29	0.13		
56	174.43	3.19	0.12		
57	191.23	3.09	0.11		
58	210.31	2.97	0.10		
59	230.27	2.83	0.09		
60	251.17	2.66	0.08		
61	273.05	2.48	0.07		
62	295.94	2.31	0.06		
63	319.90	2.17	0.05		
64	344.99	2.03	0.04		
65	371.23	1.91	0.03		
66	398.70	1.81	0.02		
67	427.46	1.71	0.01		
68	457.55	1.60	0.00		
69	489.05	1.50	0.00		
70	522.01	1.40	0.00		

Key: Haut = high
Bas = low

File: AD144
Lines of current (mm)

File: AD145
Lines of current (mm)

N	Absc.	Z L.C. Haut	Z L.C. Bas
1	-900.1	0.00	0.00
2	-754.7	.02	0.00
3	-711.4	.05	.01
4	-670.0	.08	.01
5	-630.4	.11	.01
6	-592.6	.15	.01
7	-556.5	.19	.01
8	-522.0	.24	0.00
9	-489.0	.29	0.00
10	-457.6	.35	-.02
11	-427.5	.42	-.04
12	-398.7	.50	-.07
13	-371.2	.59	-.09
14	-345.0	.68	-.11
15	-319.9	.79	-.15
16	-295.9	.89	-.19
17	-273.0	.94	-.23
18	-251.2	1.05	-.27
19	-230.3	1.13	-.31
20	-210.3	1.21	-.35
21	-191.2	1.29	-.38
22	-174.4	1.40	-.40
23	-158.3	1.49	-.42
24	-145.6	1.58	-.45
25	-132.8	1.63	-.49
26	-120.9	1.68	-.53
27	-109.7	1.75	-.56
28	-99.08	1.81	-.60
29	-89.89	1.87	-.63
30	-79.09	1.94	-.65
31	-69.60	2.00	-.68
32	-60.39	2.07	-.71
33	-51.39	2.13	-.74
34	-42.57	2.18	-.77
35	-33.89	2.22	-.78
36	-25.33	2.26	-.78
37	-16.84	2.29	-.79
38	-8.41	2.30	-.80
39	0.00	2.31	-.80
40	8.41	2.32	-.79
41	16.84	2.32	-.78
42	25.33	2.33	-.76
43	33.89	2.34	-.75
44	42.57	2.35	-.73
45	51.39	2.35	-.71
46	60.39	2.35	-.68
47	69.60	2.35	-.66
48	79.09	2.33	-.63
49	89.89	2.31	-.60
50	99.08	2.28	-.58
51	109.73	2.24	-.55
52	120.94	2.19	-.51
53	132.83	2.11	-.48
54	145.56	2.02	-.44
55	159.33	1.94	-.41
56	174.43	1.87	-.37
57	191.23	1.80	-.34
58	210.31	1.73	-.31
59	230.27	1.65	-.28
60	251.17	1.56	-.25
61	273.05	1.49	-.21
62	295.94	1.39	-.16
63	319.90	1.31	-.11
64	344.98	1.22	-.03
65	371.23	1.12	.03
66	398.70	1.02	.09
67	427.46	.92	.13
68	457.55	.82	.17
69	489.05	.74	.20
70	522.01	.66	.23

N	Absc.	Z L.C. Haut	Z L.C. Bas
1	-900.1	0.00	0.00
2	-754.7	.12	.10
3	-711.4	.25	.21
4	-670.0	.38	.32
5	-630.4	.51	.42
6	-592.6	.65	.55
7	-556.5	.80	.69
8	-522.0	.95	.84
9	-489.0	1.10	.98
10	-457.6	1.27	1.12
11	-427.5	1.44	1.00
12	-398.7	1.61	1.06
13	-371.2	1.80	1.14
14	-345.0	1.99	1.22
15	-319.9	2.20	1.30
16	-295.9	2.42	1.48
17	-273.0	2.62	1.46
18	-251.2	2.80	1.51
19	-230.3	2.98	1.55
20	-210.3	3.17	1.64
21	-191.2	3.36	1.73
22	-174.4	3.57	1.81
23	-158.3	3.75	1.88
24	-145.6	3.89	1.94
25	-132.8	4.01	1.94
26	-120.9	4.11	1.94
27	-109.7	4.22	1.94
28	-99.08	4.32	1.95
29	-89.89	4.41	1.97
30	-79.09	4.51	1.99
31	-69.60	4.60	2.01
32	-60.39	4.69	2.03
33	-51.39	4.76	2.04
34	-42.57	4.83	2.05
35	-33.89	4.88	2.05
36	-25.33	4.93	2.07
37	-16.84	4.96	2.07
38	-8.41	4.98	2.06
39	0.00	5.00	2.05
40	8.41	5.00	2.05
41	16.84	5.00	2.04
42	25.33	5.00	2.03
43	33.89	5.00	2.02
44	42.57	5.00	2.02
45	51.39	4.99	2.01
46	60.39	4.97	2.00
47	69.60	4.94	1.99
48	79.09	4.90	1.98
49	89.89	4.83	1.94
50	99.08	4.76	1.91
51	109.73	4.67	1.88
52	120.94	4.55	1.84
53	132.93	4.41	1.80
54	145.56	4.27	1.76
55	159.33	4.13	1.72
56	174.43	3.99	1.66
57	191.23	3.85	1.61
58	210.31	3.70	1.55
59	230.27	3.53	1.53
60	251.17	3.34	1.49
61	273.05	3.13	1.43
62	295.94	2.91	1.36
63	319.90	2.69	1.29
64	344.98	2.47	1.24
65	371.23	2.24	1.19
66	398.70	2.02	1.14
67	427.46	1.81	1.09
68	457.55	1.60	1.03
69	489.05	1.41	.96
70	522.01	1.23	.88

Key: Haut = high
Bas = low

Fichier : AD142
Cotes des parois (mm)

N	Absc.	Z Pl. Haut	Z Pl. Bas
1	-705.0	.24	-.34
2	-575.0	.66	-.72
3	-460.0	1.13	-1.00
4	-355.0	1.45	-1.42
5	-275.0	1.69	-1.70
6	-215.0	1.76	-1.87
7	-155.0	1.98	-2.11
8	-95.02	2.24	-2.13
9	-35.02	2.41	-2.40
10	24.99	2.46	-2.64
11	84.99	2.59	-2.69
12	144.99	2.82	-2.83
13	204.99	3.07	-3.05
14	284.99	3.16	-3.23
15	399.99	3.43	-3.62
16	504.99	3.79	-3.83

M = 0,6
 $\alpha = -2^\circ$

Non adapté

Fichier : AD144
Cotes des parois (mm)

N	Absc.	Z Pl. Haut	Z Pl. Bas
1	-705.0	.37	-.21
2	-575.0	.97	-.70
3	-460.0	1.39	-1.11
4	-355.0	2.09	-1.48
5	-275.0	2.55	-1.94
6	-215.0	3.06	-2.29
7	-155.0	3.46	-2.52
8	-95.02	3.92	-2.77
9	-35.02	4.51	-3.06
10	24.99	4.79	-3.29
11	84.99	4.91	-3.35
12	144.99	4.91	-3.48
13	204.99	4.82	-3.49
14	284.99	4.78	-3.56
15	399.99	4.64	-3.59
16	504.99	4.77	-3.78

Fichier : AD143
Cotes des parois (mm)

N	Absc.	Z Pl. Haut	Z Pl. Bas
1	-705.0	.45	-.40
2	-575.0	.83	-.70
3	-460.0	1.25	-1.00
4	-355.0	1.86	-1.43
5	-275.0	2.32	-1.71
6	-215.0	2.82	-2.07
7	-155.0	3.23	-2.49
8	-95.02	3.67	-2.95
9	-35.02	3.68	-3.23
10	24.99	4.12	-3.47
11	84.99	4.06	-3.53
12	144.99	4.05	-3.64
13	204.99	3.72	-3.68
14	284.99	3.48	-3.68
15	399.99	2.87	-3.72
16	504.99	2.34	-3.97

Key

Fichier = File
Cotes des parois =
Wall specifications
Haut = High
Bas = Low

Fichier : AD107
Cotes des parois (mm)

N	Absc.	Z Pl. Haut	Z Pl. Bas
1	-705.0	.24	-.26
2	-575.0	.63	-.66
3	-460.0	1.05	-.98
4	-355.0	1.45	-1.45
5	-275.0	1.69	-1.73
6	-215.0	1.89	-1.88
7	-155.0	1.98	-1.94
8	-95.02	2.23	-2.13
9	-35.02	2.43	-2.41
10	24.98	2.50	-2.46
11	94.98	2.79	-2.56
12	144.98	2.83	-2.30
13	204.98	3.08	-3.11
14	294.93	3.23	-3.26
15	389.98	3.53	-3.55
16	504.93	3.39	-3.93

M
r

Non adapté

Fichier : AD136
Cotes des parois (mm)

N	Absc.	Z Pl. Haut	Z Pl. Bas
1	-705.0	.19	-.21
2	-575.0	1.13	-.51
3	-460.0	1.92	-.72
4	-355.0	2.71	-1.03
5	-275.0	3.38	-1.12
6	-215.0	3.90	-1.29
7	-155.0	4.43	-1.50
8	-95.02	4.13	-1.79
9	-35.02	5.77	-1.51
10	24.98	6.04	-1.04
11	94.98	6.02	-2.27
12	144.98	5.89	-2.45
13	204.98	5.54	-3.60
14	294.93	5.42	-2.94
15	389.98	5.13	-3.21
16	504.93	4.82	-3.50

2-D

Fichier : AD117
Cotes des parois (mm)

N	Absc.	Z Pl. Haut	Z Pl. Bas
1	-705.0	.44	-.29
2	-575.0	.84	-.66
3	-460.0	1.26	-1.00
4	-355.0	1.86	-1.25
5	-275.0	2.31	-1.56
6	-215.0	2.82	-2.07
7	-155.0	3.23	-2.36
8	-95.02	3.63	-2.77
9	-35.02	3.89	-3.24
10	24.98	3.74	-3.70
11	94.98	3.45	-4.14
12	144.98	3.03	-4.63
13	204.98	2.47	-5.11
14	294.93	1.85	-5.70
15	389.98	.56	-6.47
16	504.98	-.58	-7.38

3-D

Key

Fichier = File
Cotes des parois =
Wall specifications
Haut = High
Bas = Low

Fichier : AD122
Cotes des parois (mm)

N	Abac.	IZ Pl. Haut	IZ Pl. Bas
1	-705.0	1.67	1.76
2	-575.0	3.15	1.60
3	-460.0	4.55	2.30
4	-355.0	5.82	2.80
5	-275.0	6.70	3.43
6	-215.0	7.42	3.76
7	-155.0	8.05	4.11
8	-95.02	8.70	4.33
9	-35.02	9.52	4.83
10	24.98	10.22	5.03
11	84.98	10.96	5.44
12	144.98	11.58	5.87
13	204.98	12.28	6.13
14	264.98	13.25	6.66
15	329.98	14.37	7.21
16	504.98	15.71	7.73

M=0,6
 $\alpha = +2^\circ$

Non adapte

Fichier : AD145
Cotes des parois (mm)

N	Abac.	IZ Pl. Haut	IZ Pl. Bas
1	-705.0	1.55	1.01
2	-575.0	1.50	-1.18
3	-460.0	2.38	-1.28
4	-355.0	3.25	-1.23
5	-275.0	4.19	-1.28
6	-215.0	4.92	-1.23
7	-155.0	5.74	-1.27
8	-95.02	6.43	-1.17
9	-35.02	7.20	-1.34
10	24.98	7.42	-1.58
11	84.98	7.44	-1.51
12	144.98	7.21	-1.24
13	204.98	6.35	-1.53
14	264.98	6.37	-1.90
15	329.98	5.75	-2.36
16	504.98	5.30	-2.45

2-D

Fichier : AD123
Cotes des parois (mm)

N	Abac.	IZ Pl. Haut	IZ Pl. Bas
1	-705.0	1.58	1.95
2	-575.0	3.13	1.62
3	-460.0	4.54	2.32
4	-355.0	6.02	2.87
5	-275.0	7.12	3.23
6	-215.0	8.03	3.35
7	-155.0	8.89	3.50
8	-95.02	9.74	3.50
9	-35.02	10.16	3.20
10	24.98	10.41	2.99
11	84.98	10.16	2.76
12	144.98	9.93	2.43
13	204.98	9.33	2.17
14	264.98	8.62	1.42
15	329.98	7.50	1.02
16	504.98	6.55	1.75

3-D

Key

Fichier = File
Cotes des parois =
Wall specifications
Haut = High
Bas = Low

Fichier : AD108
Cotes des parois (mm)

N	Absc.	IZ Pl. Haut	IZ Pl. Bas
1	-705.0	.23	-.26
2	-575.0	.63	-.66
3	-460.0	1.04	-1.09
4	-355.0	1.46	-1.45
5	-275.0	1.89	-1.74
6	-215.0	1.97	-1.88
7	-155.0	1.97	-1.94
8	-95.02	2.22	-2.13
9	-35.02	2.43	-2.40
10	24.98	2.50	-2.46
11	84.98	2.79	-2.67
12	144.98	2.82	-2.89
13	204.98	3.08	-3.11
14	264.98	3.23	-3.27
15	389.98	3.52	-3.55
16	504.98	4.00	-3.82

M = 0,8
α = 0°

Non adapté

Fichier : AD104
Cotes des parois (mm)

N	Absc.	IZ Pl. Haut	IZ Pl. Bas
1	-705.0	.42	-.26
2	-575.0	1.21	-.54
3	-460.0	1.33	-.77
4	-355.0	2.52	-1.09
5	-275.0	3.35	-1.30
6	-215.0	4.03	-1.44
7	-155.0	4.63	-1.49
8	-95.02	5.13	-1.91
9	-35.02	6.13	-2.19
10	24.98	6.44	-2.43
11	84.98	6.57	-2.48
12	144.98	6.34	-2.61
13	204.98	6.01	-2.84
14	264.98	5.74	-3.03
15	389.98	5.55	-3.40
16	504.98	5.47	-3.91

2-D

Fichier : AD119
Cotes des parois (mm)

N	Absc.	IZ Pl. Haut	IZ Pl. Bas
1	-705.0	.44	-.51
2	-575.0	.67	-.89
3	-460.0	1.47	-1.39
4	-355.0	2.06	-1.84
5	-275.0	2.53	-2.33
6	-215.0	3.03	-2.88
7	-155.0	3.64	-3.36
8	-95.02	4.11	-3.98
9	-35.02	4.51	-4.52
10	24.98	4.98	-4.93
11	84.98	4.25	-5.32
12	144.98	3.45	-5.60
13	204.98	3.08	-5.11
14	264.98	2.37	-6.71
15	389.98	1.26	-7.60
16	504.98	.45	-8.68

3-D

Key

Fichier = File
Cotes des parois =
Wall specifications
Haut = High
Bas = Low

Listing of Test Files

Key to Annex 3

Fichier = File
Parois rectilignes = Rectilinear walls
Symetriques = Symmetrical

Page format:

MACH HIGH AND LOW WALLS	MACH LATERAL WALLS	AS07 WING
I HIGH LOW	I HIGH LOW	I MACH
	DBL. RECORDERS	UPSTM PTHOLE

LFT. LAT. RECORDERS

DNSTRM PTHOLE RT. PTHOLE

RT. LAT. RECORDERS

LFT. PTHOLE

NECK RECORDERS

LISTE DES ESSAIS "AILE AS07"

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*****
* FICHER AD4 : PAROIS RECTILIGNES DIVERGENTES
* AD445 : IDEM + ROTATION DE 30° (VERS LE HAUT)
* AD___ : FICHER DE L'ESSAI N = ___
* AD9___ : CALCUL 3-D DE LA NOUVELLE POSITION DES PAROIS
*****
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* FICHER	INC. AFF.	MACH	RANGÉES DE PRISES	FICHER DE DEPART	ROT. PAROIS	ADAPT.	NB. D'ITER.
* AD105	0	.7	2 - 5	AD4	0	NON	1
* AD107	0	.7		"	0	"	1
* AD108	0	.7		"	0	"	1
* AD110	-2	.7		"	0	"	1
* AD115	0	.7		AD9105	0	3-D (1)	1
* AD116	0	.7		AD9115	0	3-D (2)	1
* AD117	0	.6		AD9107	0	3-D	1
* AD118	0	.6		AD9108	0	3-D (1)	1
* AD119	0	.6		AD9118	0	3-D (2)	1
* AD120	+2	.5		AD4	0	NON	1
* AD122	+1.5	.6		AD445	30'	NON	1
* AD123	+1.5	.6		AD9122	30'	3-D	1
* AD124	+1.5	.7		AD445	30'	NON	1
* AD125	+1.5	.6		AD9124	30'	3-D	1
* AD126	+1.5	.6		AD445	30'	NON	1
* AD127	+1.5	.6		AD9126	30'	3-D (1)	1
* AD129	+1.5	.6		AD9127	30'	3-D (2)	1
* AD129	+1.5	.6		AD9128	30'	3-D (3)	1
* AD130	+1.5	.7		AD4	0	2-D	4
* AD131	+1.5	.6		AD130	0	2-D	4
* AD133	0	.6		AD4	0	2-D	4
* AD134	0	.6		AD133	0	2-D	4
* AD135	0	.6		AD134	0	2-D	4
* AD136	0	.6		AD135	0	2-D	4
* AD137	-0.5	.6		AD445	30'	NON	1
* AD138	-0.5	.6		AD9137	30'	3-D	1
* AD139	-0.5	.6		AD445	30'	NON	1
* AD140	-0.5	.6		AD9139	30'	3-D (1)	1
* AD141	-0.5	.6		AD9140	30'	3-D (2)	1
* AD142	-2	.6		AD4	0	NON	1
* AD143	-2	.6		AD9142	0	3-D	1
* AD144	-2	.6		AD136	0	2-D	4
* AD145	+2	.6		AD131	0	2-D	4

* AD146	+2	.6	1 - 4	AD145	0	2-D	4
* AD147	+1.5	.6		AD445	30'	NON	1
* AD148	+1.5	.6		AD9122	30'	3-D	1
* AD149	0	.6		AD136	0	2-D	4
* AD150	0	.6		AD4	0	NON	1
* AD151	0	.6		AD9107	0	3-D	1
* AD152	0	.6		AD134	0	2-D	4
* AD153	0	.6		AD4	0	NON	1
* AD154	0	.6		AD9118	0	3-D	1
* AD155	-2	.6		AD144	0	2-D	4
* AD156	-2	.6		AD4	0	NON	1
* AD157	-2	.6		AD9142	0	3-D	1

* AD158	-2	.6	3 - 6	AD144	0	2-D	4
* AD159	-2	.6		AD4	0	NON	1
* AD160	-2	.6		AD9142	0	3-D	1
* AD161	0	.6		AD136	0	2-D	4
* AD162	0	.6		AD4	0	NON	1
* AD163	0	.6		AD9107	0	3-D	1
* AD164	0	.6		AD134	0	2-D	4
* AD165	0	.6		AD4	0	NON	1
* AD166	0	.6		AD9118	0	3-D	1
* AD167	+1.5	.6		AD445	30'	NON	1
* AD168	+1.5	.6		AD9122	30'	3-D	1
* AD169	+2	.6		AD145	0	2-D	4

***** FICHER AD105 NOCITE= 1
 14/ 8/85 11H40 AS07 M=.7 I=0 R 2-5 NON ADAPTE AD105
 DE AD4 1'ITE. PAROIS RECTILIGNES SYMETRIQUES

MACH DE REFERENCE= .7019 UINF= 231.103 M/S
 TIV=299.6 K PIV= 1557 MB

MACH PAROIS HAUTE ET BASSE						MACH PAROIS LATER.				AILE AS4	
I	HAUT	BAS	I	HAUT	BAS	I	MACH	I	MACH	I	MACH
1	.702	.701	PRISES DOUBLES			HUB. AMONT	33	.715	1	.702	
2	.702	.705					34	.714	2	.702	
3	.701	.702	59	.701	.701	1	.702	35	.713	3	.702
4	.700	.701	60	.703	.704	2	.702	36	.712	4	.702
5	.700	.702	61	.706	.705	3	.701	37	.712	5	.702
6	.702	.703				4	.701	38	.712	6	.702
7	.702	.702	PRISES LAT. GAUCHES			5	.701	39	.713	7	.702
8	.704	.702				6	.701	40	.714	8	.702
9	.703	.705	62	.700	.703	7	.701	41	.715	9	.702
10	.703	.700	63	.701	.707	8	.701	42	.714	10	.702
11	.700	.701	64	.708	.707	9	.701	43	.712	11	.702
12	.698	.701	65	.709	.706	10	.701	44	.712	12	.702
13	.699	.700	66	.717	.709	11	.702	45	.711	13	.702
14	.700	.702	67	.725	.710					14	.702
15	.701	.703	68	.729	.713	HUB. AVAL		HUB. DROIT		15	.702
16	.703	.703	69	.730	.715	1	.703	1	.702	16	.702
17	.705	.703	70	.727	.711	2	.703	2	.702	17	.702
18	.703	.703	71	.715	.703	3	.703	3	.701	18	.702
19	.707	.703	72	.711	.709	4	.711	4	.702	19	.702
20	.707	.705	73	.698	.710	5	.703	5	.703	20	.702
21	.709	.705				6	.703	6	.703	21	.702
22	.716	.707	PRISES LAT. DROITES			7	.703	7	.702	22	.702
23	.719	.706				8	.703	8	.702	23	.702
24	.719	.709	74	.701	.704	9	.703	9	.702	24	.702
25	.721	.711	75	.701	.702	10	.703	10	.702	25	.702
26	.721	.710	76	.702	.701	11	.707	11	.702	26	.702
27	.726	.703	77	.700	.699					27	.702
28	.729	.711	78	.703	.700	HUB. GAUCHE				28	.702
29	.734	.711	79	.705	.699	13	.702	13	.702	29	.702
30	.731	.711	80	.715	.704	14	.702	14	.702	30	.702
31	.737	.703	81	.724	.707	1	.723	1	.702	31	.702
32	.735	.713	82	.725	.710	2	.725	2	.702	32	.702
33	.733	.714	83	.732	.710	3	.724	3	.702	33	.702
34	.735	.713	84	.742	.710	4	.714	4	.702	34	.702
35	.733	.715	85	.745	.713	5	.715	5	.702	35	.702
36	.735	.715	86	.743	.715	6	.720	6	.702	36	.702
37	.736	.714	87	.742	.715	7	.723	7	.702	37	.702
38	.734	.714	88	.740	.714	8	.725	8	.702	38	.702
39	.735	.713	89	.736	.712	9	.725	9	.702	39	.702
40	.730	.712	90	.729	.711	10	.723	10	.702	40	.702
41	.739	.711	91	.725	.709	11	.722	11	.702	41	.702
42	.739	.710	92	.717	.703	12	.722	12	.702	42	.702
43	.729	.709	93	.709	.707	13	.720	13	.702	43	.702
44	.734	.703	94	.713	.705	14	.719	14	.703	44	.702
45	.722	.707	95	.705	.695	15	.713	15	.702	45	.702
46	.719	.703	96	.698	.692	16	.712	16	.703	46	.702
47	.713	.703				17	.712	17	.702	47	.702
48	.715	.709				18	.713	18	.702	48	.702
49	.714	.703				19	.713	19	.702	49	.702
50	.711	.703				20	.714	20	.702	50	.702
51	.712	.703				21	.715	21	.702		
52	.707	.705	PRISES COL			22	.715	22	.702		
53	.707	.705				23	.714	23	.702		
54	.707	.705				24	.713	24	.702		
55	.705	.704	.764	1.155		25	.720	25	.702		
56	.703	.701	.813	1.250		26	.723	26	.702		
57	.700	.698	.874	.941		27	.723	27	.702		
58	.695	.687	.931	.795		28	.723	28	.702		
			1.099	.738		29	.723	29	.702		
						30	.713	30	.702		
						31	.713	31	.702		
						32	.715	32	.702		

***** FICHER AD107 NOKIT= 1
 14 3 35 11H55 A307 M=.6 I=0 R 2-5 NON ADAPTE AD107
 DE AD4 1'ITE. PAROIS RECTILIGNES SYMETRIQUES

MACH DE REFERENCE= .5983 UINF= 231.103 M/S
 TIV=296.8 K PIV= 1534 MB

MACH PAROIS HAUTE ET BASSE						MACH PAROIS LATER.				AILE A307	
I	HAUT	BAS	I	HAUT	BAS	I	MACH	I	MACH	I	MACH
1	.599	.598	PRISES DOUBLES			HUB. AMONT	33	.605	1	.579	
2	.599	.602				34	.605	2	.593		
3	.599	.599	59	.598	.597	1	.598	35	.604	3	.605
4	.597	.597	60	.599	.600	2	.598	36	.604	4	.608
5	.597	.598	61	.599	.601	3	.598	37	.604	5	.602
6	.599	.600				4	.598	38	.604	6	.652
7	.599	.599	PRISES LAT. GAUCHES			5	.597	39	.604	7	.612
8	.599	.598				6	.597	40	.605	8	.598
9	.600	.601	62	.598	.600	7	.597	41	.605	9	.645
10	.600	.597	63	.604	.603	8	.597	42	.605	10	.685
11	.597	.598	64	.603	.601	9	.599	43	.603	11	.639
12	.596	.599	65	.603	.600	10	.598	44	.602	12	.719
13	.597	.598	66	.608	.601	11	.599	45	.602	13	.747
14	.598	.600	67	.613	.601					14	.735
15	.599	.600	68	.616	.603	HUB. AVAL	HUB. DROIT			15	.725
16	.600	.599	69	.616	.606	1	.602	1	.599	16	.714
17	.601	.599	70	.615	.603	2	.602	2	.599	17	.711
18	.603	.599	71	.605	.601	3	.603	3	.599	18	.711
19	.602	.599	72	.603	.602	4	.603	4	.599	19	.706
20	.603	.600	73	.590	.606	5	.605	5	.599	20	.704
21	.603	.600				6	.603	6	.599	21	.694
22	.608	.601	PRISES LAT. DROITES			7	.603	7	.599	22	.691
23	.611	.600				8	.603	8	.599	23	.682
24	.610	.602	74	.599	.600	9	.603	9	.599	24	.687
25	.612	.603	75	.599	.599	10	.604	10	.599	25	.686
26	.612	.603	76	.599	.598	11	.603	11	.599	26	.682
27	.614	.601	77	.597	.597					27	.680
28	.616	.603	78	.599	.597	HUB. GAUCHE				28	.673
29	.619	.603	79	.601	.595	13	.609	13	.599	29	.644
30	.618	.603	80	.608	.599	14	.611	14	.599	30	.619
31	.622	.601	81	.615	.601	15	.615	15	.599	31	.603
32	.620	.605	82	.615	.603	16	.614	16	.599	32	.616
33	.622	.605	83	.618	.601	17	.612	17	.599	33	.616
34	.620	.604	84	.624	.601	18	.606	18	.599	34	.616
35	.622	.605	85	.626	.602	19	.607	19	.599	35	.614
36	.620	.605	86	.625	.604	20	.609	20	.599	36	.614
37	.621	.604	87	.624	.605	7	.611	21	.599	37	.614
38	.619	.604	88	.623	.604	8	.613	22	.599	38	.614
39	.620	.604	89	.622	.603	9	.613	23	.599	39	.613
40	.617	.603	90	.616	.603	10	.612	24	.599	40	.613
41	.617	.603	91	.614	.601	11	.611	25	.599	41	.614
42	.617	.602	92	.608	.601	12	.610	26	.599	42	.603
43	.617	.601	93	.602	.600	13	.609	27	.599	43	.602
44	.613	.601	94	.604	.601	14	.609	28	.599	44	.610
45	.612	.600	95	.596	.598	15	.605	29	.599	45	.610
46	.609	.601	96	.590	.596	16	.604	30	.599	46	.617
47	.609	.601				17	.605	31	.599	47	.603
48	.607	.602				18	.605	32	.599	48	.606
49	.606	.602				19	.605	33	.599	49	.606
50	.604	.602				20	.606	34	.599	50	.601
51	.604	.602				21	.606	35	.599		
52	.601	.602	PRISES COL			22	.607	36	.599		
53	.599	.603				23	.605	37	.599		
54	.598	.603	.666	1.064		24	.608	38	.599		
55	.596	.602	.606	1.063		25	.609	39	.599		
56	.593	.600	.600	.681		26	.610	40	.599		
57	.591	.599	.666	.791		27	.611	41	.599		
58	.590	.593	1.027	.725		28	.612	42	.599		
						29	.610	43	.599		
						30	.608	44	.599		
						31	.606	45	.599		
						32	.606				

***** FICHER AD100 NO(IT)= 1
14 8 35 12H AS07 M=8 I=0 P 2-5 NON ADAPTE AD100
DE AD4 L'ITE PAROIS RECTILIGNES SYMETRIQUES

MACH DE REFERENCE= .8012 UINF= 231.108 M/S
TIV=293.5 K PIV= 1604 MB

MACH PAROIS HAUTE ET BASSE						MACH PAROIS LATÉR.				FILE AS07	
I	HAUT	BAS	I	HAUT	BAS	I	MACH	I	MACH	I	MACH
1	.801	.799									
2	.804	.808									
3	.803	.805	59	.803	.802	1	.801	35	.827	1	.789
4	.797	.801	60	.803	.805	2	.800	36	.826	2	.813
5	.796	.801	61	.811	.807	3	.800	37	.824	3	.822
6	.803	.805				4	.800	38	.819	4	1.006
7	.803	.804				5	.793	39	.820	5	.852
8	.802	.799				6	.799	40	.821	6	.864
9	.801	.803	62	.800	.803	7	.799	41	.822	7	.819
10	.804	.800	63	.793	.809	8	.799	42	.825	8	.814
11	.799	.802	64	.808	.806	9	.799	43	.827	9	.409
12	.794	.800	65	.814	.808	10	.799	44	.824	10	1.051
13	.797	.799	66	.823	.812	11	.800	45	.822	11	1.023
14	.799	.803	67	.841	.813				.821	12	1.025
15	.803	.803	68	.848	.823				.820	13	1.029
16	.803	.800	69	.852	.828					14	1.023
17	.804	.801	70	.845	.819					15	1.017
18	.806	.802	71	.822	.812	1	.815	1	.801	16	1.015
19	.805	.802	72	.813	.814	2	.814	2	.801	17	1.016
20	.809	.806	73	.807	.813	3	.813	3	.802	18	1.024
21	.812	.808				4	.817	4	.802	19	1.025
22	.820	.810				5	.814	5	.801	20	1.005
23	.826	.810				6	.813	6	.801	21	1.013
24	.823	.815	74	.801	.808	7	.812	7	.801	22	.897
25	.829	.813	75	.804	.803	8	.811	8	.801	23	.853
26	.831	.817	76	.802	.801	9	.814	9	.802	24	.751
27	.840	.815	77	.798	.799	10	.811	10	.802	25	.879
28	.844	.819	78	.800	.797	11	.811	11	.802	26	.868
29	.855	.821	79	.803	.797				.801	27	.879
30	.852	.821	80	.813	.806				.801	28	.803
31	.854	.819	81	.832	.811				.801	29	.863
32	.859	.826	82	.831	.815	1	.845	15	.801	30	.849
33	.867	.828	83	.848	.816	2	.844	16	.801	31	.820
34	.861	.824	84	.868	.819	3	.843	17	.801	32	1.523
35	.866	.826	85	.875	.823	4	.821	18	.802	33	1.445
36	.864	.828	86	.874	.829	5	.825	19	.801	34	1.394
37	.864	.825	87	.872	.833	6	.823	20	.801	35	1.398
38	.859	.824	88	.863	.834	7	.843	21	.801	36	1.242
39	.857	.822	89	.857	.819	8	.845	22	.801	37	1.332
40	.850	.820	90	.842	.813	9	.847	23	.801	38	1.079
41	.847	.813	91	.833	.817	10	.869	24	.801	39	1.023
42	.847	.819	92	.825	.812	11	.839	25	.801	40	1.035
43	.843	.817	93	.813	.811	12	.837	26	.801	41	1.023
44	.833	.816	94	.820	.813	13	.835	27	.801	42	1.007
45	.832	.813	95	.813	.813	14	.833	28	.801	43	.831
46	.827	.814	96	.807	.808	15	.817	29	.801	44	.847
47	.825	.811				16	.817	30	.801	45	.841
48	.822	.813				17	.813	31	.801	46	.801
49	.820	.812				18	.821	32	.802	47	.844
50	.816	.812				19	.821	33	.802	48	.817
51	.819	.814				20	.824	34	.802	49	.843
52	.813	.808				21	.826	35	.802		
53	.815	.808				22	.823	36	.802		
54	.817	.807				23	.827	37	.801		
55	.816	.802				24	.834	38	.801		
56	.812	.796				25	.836	39	.801		
57	.810	.793				26	.839	40	.801		
58	.804	.782				27	.844	41	.801		
						28	.844	42	.801		
						29	.837	43	.801		
						30	.828	44	.801		
						31	.822	45	.801		
						32	.829				

***** FICHER AD110 NOCIT)= 1
 14 3 35 15H50 AS07 M=7 I=-2 R 2-5 NON ADAPTE AD110
 DE AD4 1'ITE. PAROIS RECTILIGNES SYMETRIQUES

MACH DE REFERENCE= .6974 UINF= 231.108 M/S
 TIV=299.3 K PIV= 1553 MB

MACH PAROIS HAUTE ET BASSE						MACH PAROIS LATER.				AILE AS07	
I	HAUT	BAS	I	HAUT	BAS	I	MACH	I	MACH	I	MACH
1	.698	.697	PRISES DOUBLES			HUB. AMONT		33	.712	1	.681
2	.699	.702						34	.712	2	.706
3	.699	.699	59	.697	.697	1	.697	35	.712	3	.770
4	.696	.697	60	.699	.700	2	.697	36	.709	4	.649
5	.696	.699	61	.701	.700	3	.697	37	.710	5	.649
6	.699	.699	PRISES LAT. GAUCHES			4	.696	38	.711	6	.801
7	.697	.698				5	.695	39	.712	7	.779
8	.698	.697				6	.695	40	.714	8	.819
9	.699	.701	62	.696	.699	7	.696	41	.714	9	.869
10	.699	.695	63	.698	.704	8	.695	42	.712	10	.910
11	.696	.693	64	.702	.702	9	.696	43	.711	11	.873
12	.694	.698	65	.705	.701	10	.695	44	.711	12	.854
13	.695	.695	66	.708	.708	11	.696	45	.710	13	.826
14	.696	.698	67	.716	.711	HUB. AVANT		HUB. DROIT		14	.819
15	.697	.698	68	.718	.714	1	.703	1	.698	15	.811
16	.698	.696	69	.719	.713	2	.703	2	.699	16	.804
17	.698	.699	70	.717	.711	3	.702	3	.698	17	.805
18	.701	.702	71	.708	.707	4	.704	4	.698	18	.812
19	.700	.702	72	.705	.704	5	.702	5	.697	19	.810
20	.703	.702	73	.695	.705	6	.704	6	.698	20	.815
21	.704	.702	PRISES LAT. DROITES			7	.702	7	.697	21	.809
22	.703	.704				8	.702	8	.697	22	.812
23	.709	.705	74	.698	.700	9	.702	9	.697	23	.803
24	.709	.709	75	.699	.699	10	.703	10	.697	24	.804
25	.710	.712	76	.699	.697	11	.701	11	.697	25	.804
26	.710	.711	77	.698	.695	12	.702	12	.697	26	.805
27	.714	.711	78	.696	.695	13	.702	13	.697	27	.805
28	.716	.712	79	.697	.697	14	.702	14	.697	28	.805
29	.720	.715	80	.699	.699	HUB. GAUCHE		15	.697	29	.841
30	.718	.714	81	.709	.702	1	.710	15	.697	30	.840
31	.723	.713	82	.713	.709	2	.715	16	.697	31	.803
32	.722	.718	83	.711	.714	3	.715	17	.697	32	.858
33	.724	.720	84	.717	.715	4	.715	18	.697	33	.894
34	.721	.717	85	.725	.717	5	.707	19	.697	34	.815
35	.724	.719	86	.728	.720	6	.708	20	.697	35	.811
36	.722	.719	87	.727	.721	7	.711	21	.697	36	.812
37	.723	.718	88	.727	.721	8	.714	22	.697	37	.814
38	.720	.716	89	.725	.713	9	.715	23	.697	38	.813
39	.721	.715	90	.725	.715	10	.715	24	.698	39	.819
40	.718	.713	91	.718	.712	11	.714	25	.698	40	.815
41	.718	.712	92	.718	.708	12	.713	26	.698	41	.811
42	.719	.711	93	.710	.707	13	.713	27	.698	42	.810
43	.718	.709	94	.703	.704	14	.713	28	.698	43	.812
44	.714	.703	95	.707	.702	15	.707	29	.698	44	.804
45	.714	.705	96	.700	.691	16	.706	30	.698	45	.794
46	.710	.707	97	.695	.689	17	.707	31	.698	46	.795
47	.710	.705				18	.708	32	.698	47	.787
48	.708	.705				19	.708	33	.698	48	.780
49	.707	.704				20	.709	34	.698	49	.787
50	.705	.703				21	.709	35	.698	50	.747
51	.706	.703				22	.711	36	.698		
52	.703	.701	PRISES COL			23	.709	37	.698		
53	.702	.701				24	.713	38	.698		
54	.702	.702	757	1.149		25	.714	39	.698		
55	.692	.699	816	1.270		26	.715	40	.698		
56	.699	.695	937	.937		27	.718	41	.698		
57	.697	.693	927	.790		28	.719	42	.698		
58	.692	.685	1.091	.730		29	.717	43	.697		
						30	.712	44	.697		
						31	.710	45	.697		
						32	.712				

***** FICHER AD115 NOÛT= 1
 20/ 8/85 11H15 AS07 M=.7 I=0 R 2-5 ADAPTE 3D L'ITE AD115
 DE AD9105 L'ITE.

MACH DE REFERENCE= .7013 UINF= 231.109 M/S
 TIV=298.7 K PIV= 1517 MB

MACH PAROIS HAUTE ET BASSE						MACH PAROIS LATÉR.				FILE AS	
I	HAUT	BAS	I	HAUT	BAS	I	MACH	I	MACH	I	MACH
1	.703	.701	*	PRISES DOUBLES		*	HUB. AMONT	33	.705	*	1
2	.702	.705	**			**		34	.704	**	2
3	.701	.702	**	59	.700	.699	1	.702	.704	**	3
4	.699	.701	**	60	.703	.704	2	.701	.705	**	4
5	.698	.701	**	61	.706	.704	3	.701	.704	**	5
6	.701	.702	**				4	.701	.704	**	6
7	.700	.700	**	PRISES LAT. GAUCHES		**	5	.699	.704	**	7
8	.703	.700	**			**	6	.700	.705	**	8
9	.704	.705	**	62	.699	.703	7	.699	.707	**	9
10	.704	.701	**	63	.700	.707	8	.699	.706	**	10
11	.702	.703	**	64	.707	.705	9	.700	.704	**	11
12	.699	.704	**	65	.702	.701	10	.700	.703	**	12
13	.701	.703	**	66	.703	.702	11	.700	.703	**	13
14	.702	.703	**	67	.710	.704				**	14
15	.703	.702	**	68	.708	.704	HUB. AVAL	HUB. DROIT	**	15	
16	.704	.701	**	69	.708	.706	1	.707	1	**	16
17	.704	.702	**	70	.715	.703	2	.706	2	**	17
18	.705	.704	**	71	.708	.704	3	.706	3	**	18
19	.702	.703	**	72	.707	.706	4	.706	4	**	19
20	.702	.701	**	73	.712	.710	5	.705	5	**	20
21	.702	.701	**				6	.705	6	**	21
22	.705	.702	**	PRISES LAT. DROITES		**	7	.705	7	**	22
23	.707	.703	**			**	8	.707	8	**	23
24	.707	.703	**	74	.700	.704	9	.705	9	**	24
25	.707	.704	**	75	.700	.701	10	.704	10	**	25
26	.707	.702	**	76	.702	.701	11	.705	11	**	26
27	.711	.701	**	77	.702	.701	12	.702	12	**	27
28	.713	.704	**	78	.702	.699	HUB. GAUCHE	13	.702	**	28
29	.717	.705	**	79	.701	.699	14	.702	14	**	29
30	.715	.705	**	80	.708	.700	15	.702	15	**	30
31	.719	.703	**	81	.712	.704	16	.702	16	**	31
32	.715	.707	**	82	.710	.703	17	.702	17	**	32
33	.716	.707	**	83	.716	.703	18	.702	18	**	33
34	.712	.705	**	84	.724	.705	19	.702	19	**	34
35	.714	.706	**	85	.725	.707	20	.702	20	**	35
36	.713	.706	**	86	.730	.707	21	.702	21	**	36
37	.715	.704	**	87	.718	.706	22	.702	22	**	37
38	.716	.704	**	88	.718	.704	23	.702	23	**	38
39	.720	.703	**	89	.723	.702	24	.702	24	**	39
40	.717	.702	**	90	.717	.703	25	.702	25	**	40
41	.719	.703	**	91	.709	.705	26	.702	26	**	41
42	.719	.703	**	92	.712	.705	27	.702	27	**	42
43	.714	.704	**	93	.704	.702	28	.702	28	**	43
44	.708	.704	**	94	.707	.703	29	.702	29	**	44
45	.707	.704	**	95	.707	.693	30	.702	30	**	45
46	.707	.705	**	96	.711	.690	31	.702	31	**	46
47	.711	.704	**				32	.702	32	**	47
48	.710	.704	**				33	.702	33	**	48
49	.709	.703	**				34	.702	34	**	49
50	.705	.703	**				35	.702	35	**	50
51	.707	.704	**				36	.702	36	**	
52	.707	.705	**				37	.702	37	**	
53	.709	.706	**				38	.702	38	**	
54	.710	.706	**				39	.702	39	**	
55	.711	.702	**				40	.702	40	**	
56	.710	.699	**				41	.702	41	**	
57	.712	.695	**				42	.702	42	**	
58	.713	.688	**				43	.702	43	**	
			**				44	.702	44	**	
			**				45	.702	45	**	
			**				46	.702	46	**	
			**				47	.702	47	**	
			**				48	.702	48	**	
			**				49	.702	49	**	
			**				50	.702	50	**	
			**				51	.702	51	**	
			**				52	.702	52	**	
			**				53	.702	53	**	
			**				54	.702	54	**	
			**				55	.702	55	**	
			**				56	.702	56	**	
			**				57	.702	57	**	
			**				58	.702	58	**	
			**				59	.702	59	**	
			**				60	.702	60	**	
			**				61	.702	61	**	
			**				62	.702	62	**	

***** FICHER AD115 NOCITE= 1
 20/ 8/85 11H30 A507 M=7 I=0 R 2-5 ADAPTE 3D 2'ITE. AD116
 DE AD115 1'ITE.

 MACH DE REFERENCE= .7014 UINF= 331.108 M/S
 TIV=300.2 K PIV= 1517 MB

MACH PAROIS HAUTE ET BASSE						MACH PAROIS LATÉR.				HILE A507	
I	HAUT	BAS	I	HAUT	BAS	I	MACH	I	MACH	I	MACH
1	.703	.701	PRISES DOUBLES			HUB. AMONT		33	.705	1	.675
2	.704	.705						34	.704	2	.690
3	.702	.703	59	.702	.701	1	.700	35	.703	3	.747
4	.699	.701	60	.704	.703	2	.699	36	.703	4	.810
5	.699	.701	61	.702	.703	3	.699	37	.703	5	.807
6	.702	.703				4	.699	38	.703	6	.770
7	.702	.702	PRISES LAT. GAUCHES			5	.697	39	.703	7	.714
8	.703	.700				6	.698	40	.704	8	.707
9	.703	.704	62	.700	.703	7	.698	41	.705	9	.884
10	.704	.700	63	.700	.706	8	.697	42	.705	10	1.055
11	.701	.701	64	.704	.705	9	.698	43	.703	11	1.009
12	.697	.701	65	.701	.701	10	.698	44	.702	12	.914
13	.698	.700	66	.705	.700	11	.699	45	.702	13	.875
14	.699	.701	67	.710	.705					14	.861
15	.699	.702	68	.708	.705	HUB. AVAL		HUB. DROIT		15	.849
16	.700	.701	69	.709	.705	1	.705	1	.702	16	.837
17	.701	.701	70	.712	.702	2	.705	2	.702	17	.833
18	.705	.700	71	.705	.701	3	.704	3	.702	18	.835
19	.704	.700	72	.706	.704	4	.705	4	.701	19	.831
20	.703	.702	73	.706	.708	5	.704	5	.701	20	.828
21	.702	.701				6	.704	6	.702	21	.816
22	.702	.699	PRISES LAT. DROITES			7	.704	7	.702	22	.812
23	.703	.696				8	.705	8	.702	23	.801
24	.706	.698	74	.700	.704	9	.705	9	.701	24	.657
25	.708	.700	75	.702	.701	10	.704	10	.701	25	.632
26	.708	.700	76	.702	.700	11	.703	11	.701	26	.741
27	.713	.701	77	.698	.699	12	.704	12	.701	27	.812
28	.713	.704	78	.699	.699	HUB. GAUCHE				28	.805
29	.715	.705	79	.702	.696	13	.702	13	.702	29	.777
30	.713	.705	80	.707	.699	14	.702	14	.702	30	.738
31	.717	.702	81	.709	.698	1	.710	15	.702	31	.729
32	.713	.707	82	.712	.699	2	.708	16	.702	32	.662
33	.716	.707	83	.713	.702	3	.708	17	.702	33	1.132
34	.712	.705	84	.704	.705	4	.703	18	.702	34	1.011
35	.714	.705	85	.725	.708	5	.703	19	.701	35	.893
36	.713	.704	86	.721	.708	6	.706	20	.701	36	.883
37	.715	.702	87	.719	.705	7	.709	21	.701	37	.875
38	.714	.701	88	.719	.703	8	.710	22	.702	38	.871
39	.718	.701	89	.721	.699	9	.712	23	.702	39	.854
40	.716	.700	90	.714	.701	10	.710	24	.702	40	.852
41	.715	.700	91	.708	.706	11	.707	25	.702	41	.844
42	.716	.701	92	.708	.702	12	.707	26	.702	42	.837
43	.712	.703	93	.702	.699	13	.708	27	.702	43	.829
44	.707	.704	94	.706	.702	14	.707	28	.702	44	.813
45	.706	.704	95	.705	.698	15	.704	29	.702	45	.795
46	.706	.705	96	.704	.696	16	.703	30	.702	46	.792
47	.708	.701				17	.703	31	.702	47	.781
48	.708	.701				18	.703	32	.702	48	.747
49	.707	.700				19	.702	33	.702	49	.737
50	.704	.701				20	.703	34	.702	50	.720
51	.705	.703				21	.704	35	.702		
52	.703	.704	PRISES COL			22	.705	36	.702		
53	.705	.705				23	.703	37	.701		
54	.707	.704				24	.707	38	.702		
55	.708	.700				25	.709	39	.702		
56	.707	.696				26	.710	40	.702		
57	.707	.691				27	.713	41	.702		
58	.703	.691				28	.714	42	.702		
			1.096	.711		29	.712	43	.702		
						30	.709	44	.702		
						31	.707	45	.702		
						32	.705				

***** FICHER AD117 N0(ITE)= 1
 20/ 8/85 11H50 AS07 M=.6 I=0 R 2-5 ADAPTE 30 1'ITE. AD117
 DE AD9107 1'ITE

MACH DE REFERENCE= .5983 UNF= 231.108 M/S
 TIV=300.1 K PIV= 1386 MB

MACH PAROIS HAUTE ET BASSE						MACH PAROIS LATÉR.				AILÉ
I	HAUT	BAS	I	HAUT	BAS	I	MACH	I	MACH	I
1	.599	.597	PRISES DOUBLES			HUB. AMONT	33	.601		1
2	.600	.602					34	.600		2
3	.599	.600	59	.599	.599	1	.599	35	.599	3
4	.597	.599	60	.599	.598	2	.597	36	.599	4
5	.596	.600	61	.601	.599	3	.597	37	.600	5
6	.599	.601				4	.597	38	.599	6
7	.599	.600	PRISES LAT. GAUCHES					39	.599	7
8	.599	.597				5	.596	40	.600	8
9	.598	.599	62	.597	.599	6	.596	41	.601	9
10	.600	.596	63	.601	.602	7	.595	42	.601	10
11	.598	.597	64	.601	.602	8	.596	43	.598	11
12	.595	.596	65	.599	.597	9	.597	44	.599	12
13	.597	.596	66	.599	.599	10	.597	45	.598	13
14	.598	.598	67	.604	.601	11	.598			14
15	.599	.599	68	.604	.602	HUB. AVANT		HUB. DROIT		15
16	.598	.598	69	.604	.601					16
17	.599	.600	70	.607	.600	1	.602	1	.599	17
18	.601	.601	71	.601	.598	2	.601	2	.600	18
19	.599	.599	72	.602	.602	3	.601	3	.600	19
20	.599	.597	73	.598	.604	4	.600	4	.600	20
21	.598	.596				5	.601	5	.600	21
22	.601	.595	PRISES LAT. DROITES					6	.602	22
23	.602	.597				7	.602	7	.600	23
24	.602	.599	74	.598	.601	8	.604	8	.600	24
25	.601	.599	75	.599	.599	9	.602	9	.600	25
26	.600	.598	76	.598	.597	10	.600	10	.599	26
27	.604	.599	77	.597	.595	11	.599	11	.599	27
28	.604	.600	78	.598	.598			12	.600	28
29	.607	.601	79	.599	.595	HUB. GAUCHE		13	.600	29
30	.605	.600	80	.604	.598			14	.600	30
31	.603	.597	81	.606	.598	1	.604	15	.600	31
32	.607	.601	82	.604	.600	2	.603	16	.599	32
33	.609	.601	83	.608	.601	3	.602	17	.599	33
34	.606	.600	84	.614	.601	4	.599	18	.599	34
35	.608	.600	85	.615	.602	5	.599	19	.599	35
36	.607	.599	86	.613	.603	6	.601	20	.599	36
37	.609	.599	87	.612	.602	7	.603	21	.599	37
38	.608	.599	88	.611	.600	8	.604	22	.600	38
39	.610	.599	89	.614	.599	9	.605	23	.600	39
40	.608	.598	90	.609	.600	10	.595	24	.600	40
41	.607	.598	91	.604	.601	11	.603	25	.600	41
42	.608	.598	92	.602	.599	12	.602	26	.600	42
43	.606	.600	93	.599	.598	13	.602	27	.600	43
44	.604	.601	94	.604	.600	14	.601	28	.600	44
45	.602	.599	95	.601	.598	15	.600	29	.600	45
46	.601	.600	96	.599	.599	16	.599	30	.600	46
47	.602	.598				17	.599	31	.600	47
48	.602	.598				18	.600	32	.600	48
49	.603	.599				19	.599	33	.600	49
50	.602	.600				20	.600	34	.600	50
51	.603	.601				21	.601	35	.600	51
52	.602	.599				22	.600	36	.600	52
53	.603	.600	PRISES COL					37	.599	53
54	.602	.600		.601	1.000			38	.600	54
55	.601	.597		.604	.909			39	.600	55
56	.598	.594		.799	.799			40	.600	56
57	.594	.591		.866	.809			41	.600	57
58	.583	.587		1.023	.629			42	.600	58
								43	.600	
								44	.600	
								45	.600	
								46	.600	
								47	.600	
								48	.600	
								49	.600	
								50	.600	

***** FICHER AD113 NOCIT= 1
 20/3/85 14H35 AS07 M=3 I=0 R 2-5 ADAPTE 3D L'ITE, AD113
 DE AD9108 L'ITE.

MACH DE REFERENCE= .3059 UINFA 231.198 M/S
 TIV=300.9 K PIV= 1549 MB

MACH PAROIS HAUTE ET BASSE				MACH PAROIS LAT.ER.				FILE AS07					
I	HAUT	BAS		I	HAUT	SBS		I	MACH	I	MACH	I	MACH
1	.308	.305	* PRISES DOUBLES	* HUB. AMONT	33	.815	* HUB. AVAL	HUB. DROIT	1	.815	1	.775	
2	.306	.311	* 59	.304	.303	* 1	.307	1	.315	2	.815	2	.799
3	.303	.305	* 50	.310	.311	* 2	.305	3	.314	3	.815	3	.300
4	.300	.303	* 51	.314	.318	* 3	.305	4	.305	4	.814	4	.308
5	.304	.305	* PRISES LAT. GAUCHES*	* 4	.307	* 4	.307	5	.313	5	.813	5	.364
6	.304	.304	* 52	.301	.305	* 5	.305	6	.314	6	.814	6	.302
7	.309	.305	* 53	.301	.305	* 7	.304	7	.317	7	.817	7	.309
8	.310	.313	* 54	.314	.313	* 8	.304	8	.312	8	.812	8	.309
9	.311	.305	* 55	.312	.313	* 9	.307	9	.314	9	.814	9	.422
10	.307	.308	* 56	.308	.311	* 10	.305	10	.313	10	.813	10	1.315
11	.303	.308	* 57	.323	.312	* 11	.305	11	.313	11	.813	11	1.257
12	.303	.302	* 58	.320	.314	* 12	.303	12	.308	12	.813	12	1.120
13	.305	.311	* 59	.321	.320	* 13	.325	13	.312	13	.812	13	1.317
14	.305	.311	* 60	.317	.317	* 14	.320	14	.308	14	.812	14	1.302
15	.307	.309	* PRISES LAT. DROITES*	* HUB. AVAL	HUB. DROIT	15	.315	15	.807	15	.807	15	.307
16	.308	.309	* 74	.303	.305	* 16	.315	16	.807	16	.807	16	.307
17	.309	.308	* 75	.304	.305	* 17	.314	17	.807	17	.807	17	.305
18	.312	.309	* 76	.308	.307	* 18	.317	18	.807	18	.807	18	.305
19	.310	.309	* 77	.317	.317	* 19	.320	19	.807	19	.807	19	.309
20	.310	.312	* 78	.320	.325	* 20	.319	20	.805	20	.805	20	.309
21	.311	.313	* 79	.309	.303	* 21	.319	21	.805	21	.805	21	.307
22	.315	.311	* 80	.309	.303	* 22	.315	22	.805	22	.805	22	.307
23	.313	.310	* 81	.304	.311	* 23	.315	23	.805	23	.805	23	.307
24	.314	.312	* 82	.315	.313	* 24	.315	24	.805	24	.805	24	.307
25	.312	.315	* 83	.315	.313	* 25	.315	25	.805	25	.805	25	.307
26	.314	.314	* 84	.315	.315	* 26	.315	26	.805	26	.805	26	.307
27	.321	.311	* 85	.317	.316	* 27	.315	27	.805	27	.805	27	.307
28	.325	.313	* 86	.317	.320	* 28	.315	28	.805	28	.805	28	.307
29	.334	.315	* 87	.317	.320	* 29	.315	29	.805	29	.805	29	.307
30	.330	.315	* 88	.317	.317	* 30	.315	30	.805	30	.805	30	.307
31	.337	.312	* 89	.317	.317	* 31	.315	31	.805	31	.805	31	.307
32	.331	.319	* 90	.317	.317	* 32	.315	32	.805	32	.805	32	.307
33	.324	.320	* 91	.317	.317	* 33	.315	33	.805	33	.805	33	.307
34	.329	.320	* 92	.317	.317	* 34	.315	34	.805	34	.805	34	.307
35	.329	.319	* 93	.317	.317	* 35	.315	35	.805	35	.805	35	.307
36	.332	.319	* 94	.317	.317	* 36	.315	36	.805	36	.805	36	.307
37	.331	.319	* 95	.317	.317	* 37	.315	37	.805	37	.805	37	.307
38	.335	.317	* 96	.317	.317	* 38	.315	38	.805	38	.805	38	.307
39	.331	.315	* 97	.317	.317	* 39	.315	39	.805	39	.805	39	.307
40	.331	.315	* 98	.317	.317	* 40	.315	40	.805	40	.805	40	.307
41	.331	.315	* 99	.317	.317	* 41	.315	41	.805	41	.805	41	.307
42	.325	.312	* 100	.317	.317	* 42	.315	42	.805	42	.805	42	.307
43	.318	.311	* 101	.317	.317	* 43	.315	43	.805	43	.805	43	.307
44	.317	.307	* 102	.317	.317	* 44	.315	44	.805	44	.805	44	.307
45	.315	.308	* 103	.317	.317	* 45	.315	45	.805	45	.805	45	.307
46	.320	.305	* 104	.317	.317	* 46	.315	46	.805	46	.805	46	.307
47	.319	.308	* 105	.317	.317	* 47	.315	47	.805	47	.805	47	.307
48	.319	.308	* 106	.317	.317	* 48	.315	48	.805	48	.805	48	.307
49	.319	.310	* 107	.317	.317	* 49	.315	49	.805	49	.805	49	.307
50	.317	.315	* 108	.317	.317	* 50	.315	50	.805	50	.805	50	.307
51	.315	.313	* 109	.317	.317	* 51	.315	51	.805	51	.805	51	.307
52	.319	.321	* 110	.317	.317	* 52	.315	52	.805	52	.805	52	.307
53	.319	.319	* 111	.317	.317	* 53	.315	53	.805	53	.805	53	.307
54	.320	.312	* 112	.317	.317	* 54	.315	54	.805	54	.805	54	.307
55	.319	.312	* 113	.317	.317	* 55	.315	55	.805	55	.805	55	.307
56	.313	.305	* 114	.317	.317	* 56	.315	56	.805	56	.805	56	.307
57	.320	.303	* 115	.317	.317	* 57	.315	57	.805	57	.805	57	.307
58	.323	.303	* 116	.317	.317	* 58	.315	58	.805	58	.805	58	.307
59	.323	.303	* 117	.317	.317	* 59	.315	59	.805	59	.805	59	.307
60	.323	.303	* 118	.317	.317	* 60	.315	60	.805	60	.805	60	.307
61	.323	.303	* 119	.317	.317	* 61	.315	61	.805	61	.805	61	.307
62	.323	.303	* 120	.317	.317	* 62	.315	62	.805	62	.805	62	.307
63	.323	.303	* 121	.317	.317	* 63	.315	63	.805	63	.805	63	.307
64	.323	.303	* 122	.317	.317	* 64	.315	64	.805	64	.805	64	.307
65	.323	.303	* 123	.317	.317	* 65	.315	65	.805	65	.805	65	.307
66	.323	.303	* 124	.317	.317	* 66	.315	66	.805	66	.805	66	.307
67	.323	.303	* 125	.317	.317	* 67	.315	67	.805	67	.805	67	.307
68	.323	.303	* 126	.317	.317	* 68	.315	68	.805	68	.805	68	.307
69	.323	.303	* 127	.317	.317	* 69	.315	69	.805	69	.805	69	.307
70	.323	.303	* 128	.317	.317	* 70	.315	70	.805	70	.805	70	.307
71	.323	.303	* 129	.317	.317	* 71	.315	71	.805	71	.805	71	.307
72	.323	.303	* 130	.317	.317	* 72	.315	72	.805	72	.805	72	.307
73	.323	.303	* 131	.317	.317	* 73	.315	73	.805	73	.805	73	.307
74	.323	.303	* 132	.317	.317	* 74	.315	74	.805	74	.805	74	.307
75	.323	.303	* 133	.317	.317	* 75	.315	75	.805	75	.805	75	.307
76	.323	.303	* 134	.317	.317	* 76	.315	76	.805	76	.805	76	.307
77	.323	.303	* 135	.317	.317	* 77	.315	77	.805	77	.805	77	.307
78	.323	.303	* 136	.317	.317	* 78	.315	78	.805	78	.805	78	.307
79	.323	.303	* 137	.317	.317	* 79	.315	79	.805	79	.805	79	.307
80	.323	.303	* 138	.317	.317	* 80	.315	80	.805	80	.805	80	.307
81	.323	.303	* 139	.317	.317	* 81	.315	81	.805	81	.805	81	.307
82	.323	.303	* 140	.317	.317	* 82	.315	82	.805	82	.805	82	.307
83	.323	.303	* 141	.317	.317	* 83	.315	83	.805	83	.805	83	.307
84	.323	.303	* 142	.317	.317	* 84	.315	84	.805	84	.805	84	.307
85	.323	.303	* 143	.317	.317	* 85	.315	85	.805	85	.805	85	.307
86	.323	.303	* 144	.317	.317	* 86	.315	86	.805	86	.805	86	.307
87	.323	.303	* 145	.317	.317	* 87	.315	87	.805	87	.805	87	.307
88	.323	.303	* 146	.317	.317	* 88	.315	88	.805	88	.805	88	.307
89	.323	.303	* 147	.317	.317	* 89	.315	89	.805	89	.805	89	.307
90	.323	.303	* 148	.317	.317	* 90	.315	90	.805	90	.805	90	.307
91	.323	.303	* 149	.317	.317	* 91	.315	91	.805	91	.805	91	.307
92	.323	.303	* 150	.317	.317	* 92	.315	92	.805	92	.805	92	.307
93	.323	.303	* 151	.317	.317								

***** FICHER AD119 NOCIT)= I
30/3/85 15H10 AS07 M=3 I=0 R 2-5 ADAPTE 3D 2' ITC. AD119
DE AD118 1' ITC.

MACH DE REFERENCE= 3049 UINF= 231.103 M/S
TIV=301.4 K PIV= 1648 MB

MACH PAROIS HAUTE ET BASSE * * MACH PAROIS LAT. * * HILE AS07

I	HAUT	BAS	I	HAUT	BAS	I	MACH	AMONT	I	MACH	I	MACH	I	MACH
1	.308	.307	*	PRISES DOUBLES	*	*	HUB.	33	*	.310	*	.310	1	.799
2	.307	.312	*	*	*	*	34	*	*	.309	*	.309	2	.793
3	.304	.305	*	59	.303	*	35	*	1	.303	*	.303	3	.367
4	.301	.304	*	60	.305	*	36	*	2	.301	*	.301	4	.359
5	.302	.305	*	61	.305	*	37	*	3	.301	*	.307	5	.350
6	.305	.305	*	PRISES LAT. GAUCHES	*	*	38	*	4	.302	*	.307	6	.357
7	.304	.305	*	*	*	*	39	*	5	.300	*	.303	7	.319
8	.303	.312	*	62	.305	*	40	*	6	.300	*	.310	8	.319
9	.309	.312	*	63	.799	*	41	*	7	.799	*	.312	9	.743
10	.302	.301	*	64	.309	*	42	*	8	.799	*	.310	10	1.233
11	.799	.302	*	65	.305	*	43	*	9	.301	*	.307	11	1.244
12	.300	.301	*	66	.307	*	44	*	10	.301	*	.305	12	1.233
13	.799	.304	*	67	.303	*	45	*	11	.302	*	.305	13	1.311
14	.301	.304	*	68	.315	*	HUB.	46	*	.310	*	.308	14	.345
15	.303	.305	*	69	.317	*	HUB.	47	*	.305	*	.305	15	.330
16	.305	.305	*	70	.320	*	1	*	1	.305	*	.305	16	.373
17	.308	.305	*	71	.310	*	2	*	2	.305	*	.305	17	.375
18	.308	.305	*	72	.309	*	3	*	3	.305	*	.305	18	.372
19	.307	.305	*	73	.303	*	4	*	4	.305	*	.305	19	.373
20	.307	.305	*	74	.314	*	5	*	5	.305	*	.305	20	.331
21	.305	.304	*	PRISES LAT. DROITES	*	*	6	*	6	.305	*	.305	21	.366
22	.307	.302	*	*	*	*	7	*	7	.305	*	.305	22	.375
23	.310	.302	*	74	.304	*	8	*	8	.305	*	.305	23	.375
24	.311	.305	*	75	.305	*	9	*	9	.305	*	.305	24	.475
25	.313	.305	*	76	.305	*	10	*	10	.305	*	.305	25	.372
26	.313	.303	*	77	.300	*	11	*	11	.304	*	.305	26	.375
27	.320	.307	*	78	.301	*	HUB.	12	*	.305	*	.305	27	.375
28	.327	.310	*	79	.305	*	13	*	12	.305	*	.305	28	.391
29	.322	.309	*	80	.313	*	14	*	13	.305	*	.305	29	.393
30	.330	.307	*	81	.315	*	15	*	14	.305	*	.305	30	.374
31	.324	.312	*	82	.314	*	16	*	15	.305	*	.305	31	.374
32	.323	.313	*	83	.315	*	17	*	16	.305	*	.305	32	.374
33	.323	.309	*	84	.305	*	18	*	17	.305	*	.305	33	.374
34	.327	.311	*	85	.310	*	19	*	18	.305	*	.305	34	.374
35	.325	.311	*	86	.313	*	20	*	19	.305	*	.305	35	.374
36	.327	.309	*	87	.318	*	21	*	20	.305	*	.305	36	.374
37	.324	.309	*	88	.322	*	22	*	21	.305	*	.305	37	.374
38	.329	.305	*	89	.303	*	23	*	22	.305	*	.305	38	.374
39	.323	.304	*	90	.304	*	24	*	23	.305	*	.305	39	.374
40	.323	.305	*	91	.315	*	25	*	24	.305	*	.305	40	.374
41	.324	.305	*	92	.314	*	26	*	25	.305	*	.305	41	.374
42	.321	.305	*	93	.305	*	27	*	26	.305	*	.305	42	.374
43	.314	.305	*	94	.304	*	28	*	27	.305	*	.305	43	.374
44	.313	.304	*	95	.304	*	29	*	28	.305	*	.305	44	.374
45	.311	.305	*	96	.313	*	30	*	29	.305	*	.305	45	.374
46	.314	.304	*	97	.304	*	31	*	30	.305	*	.305	46	.374
47	.311	.305	*	98	.313	*	32	*	31	.305	*	.305	47	.374
48	.312	.305	*	99	.307	*	33	*	32	.305	*	.305	48	.374
49	.311	.305	*	100	.304	*	34	*	33	.305	*	.305	49	.374
50	.309	.305	*	101	.305	*	35	*	34	.305	*	.305	50	.374
51	.309	.303	*	102	.303	*	36	*	35	.305	*	.305	51	.374
52	.309	.305	*	103	.305	*	37	*	36	.305	*	.305	52	.374
53	.309	.304	*	104	.303	*	38	*	37	.305	*	.305	53	.374
54	.310	.799	*	105	1.133	*	39	*	38	.305	*	.305	54	.374
55	.311	.799	*	106	.301	*	40	*	39	.305	*	.305	55	.374
56	.314	.799	*	107	.310	*	41	*	40	.305	*	.305	56	.374
57	.320	.300	*	108	.318	*	42	*	41	.305	*	.305	57	.374
58	.320	.300	*	109	.310	*	43	*	42	.305	*	.305	58	.374
59	.320	.300	*	110	.310	*	44	*	43	.305	*	.305	59	.374
60	.320	.300	*	111	.310	*	45	*	44	.305	*	.305	60	.374
61	.320	.300	*	112	.310	*	46	*	45	.305	*	.305	61	.374
62	.320	.300	*	113	.310	*	47	*	46	.305	*	.305	62	.374
63	.320	.300	*	114	.310	*	48	*	47	.305	*	.305	63	.374
64	.320	.300	*	115	.310	*	49	*	48	.305	*	.305	64	.374
65	.320	.300	*	116	.310	*	50	*	49	.305	*	.305	65	.374
66	.320	.300	*	117	.310	*	51	*	50	.305	*	.305	66	.374
67	.320	.300	*	118	.310	*	52	*	51	.305	*	.305	67	.374
68	.320	.300	*	119	.310	*	53	*	52	.305	*	.305	68	.374
69	.320	.300	*	120	.310	*	54	*	53	.305	*	.305	69	.374
70	.320	.300	*	121	.310	*	55	*	54	.305	*	.305	70	.374
71	.320	.300	*	122	.310	*	56	*	55	.305	*	.305	71	.374
72	.320	.300	*	123	.310	*	57	*	56	.305	*	.305	72	.374
73	.320	.300	*	124	.310	*	58	*	57	.305	*	.305	73	.374
74	.320	.300	*	125	.310	*	59	*	58	.305	*	.305	74	.374
75	.320	.300	*	126	.310	*	60	*	59	.305	*	.305	75	.374
76	.320	.300	*	127	.310	*	61	*	60	.305	*	.305	76	.374
77	.320	.300	*	128	.310	*	62	*	61	.305	*	.305	77	.374
78	.320	.300	*	129	.310	*	63	*	62	.305	*	.305	78	.374
79	.320	.300	*	130	.310	*	64	*	63	.305	*	.305	79	.374
80	.320	.300	*	131	.310	*	65	*	64	.305	*	.305	80	.374
81	.320	.300	*	132	.310	*	66	*	65	.305	*	.305	81	.374
82	.320	.300	*	133	.310	*	67	*	66	.305	*	.305	82	.374
83	.320	.300	*	134	.310	*	68	*	67	.305	*	.305	83	.374
84	.320	.300	*	135	.310	*	69	*	68	.305	*	.305	84	.374
85	.320	.300	*	136	.310	*	70	*	69	.305	*	.305	85	.374
86	.320	.300	*	137	.310	*	71	*	70	.305	*	.305	86	.374
87	.320	.300	*	138	.310	*	72	*	71	.305	*	.305	87	.374
88	.320	.300	*	139	.310	*	73	*	72	.305	*	.305	88	.374
89	.320	.300	*	140	.310	*	74	*	73	.305	*	.305	89	.374
90	.320	.300	*	141	.310	*	75	*	74	.305	*	.305	90	.374
91	.320	.300	*	142	.310	*	76	*	75	.305	*	.305	91	.374
92	.320	.300	*	143	.310	*	77	*	76	.305	*	.305	92	.374
93	.320	.300	*	144	.310	*	78	*	77	.305	*	.305	93	.374
94	.320	.300	*	145	.310	*	79	*	78	.305	*	.305	94	.374
95	.320	.300	*	146	.310	*	80	*	79	.305	*	.305	95	.374
96	.320	.300	*	147	.310	*	81	*	80	.305	*	.305	96	.374
97	.320	.300	*	148	.310	*	82	*	81	.305	*	.305	97	.374
98	.320	.300	*	149	.310	*	83	*	82	.305	*	.305	98	.374
99	.320	.300	*	150	.310	*	84	*	83	.305	*	.305	99	.374
100	.320	.300	*	151	.310	*	85	*	84	.305	*	.305	100	.374
101	.320	.300	*	152	.310	*	86	*	85	.305	*	.305	101	.374
102	.320	.300	*	153	.310	*	87	*	86	.305	*	.305	102	.374
103	.320	.300	*	154	.310	*	88	*	87	.305	*	.305	103	.374
104	.320	.300	*	155	.310	*	89	*	88	.305	*	.305	104	.374
105	.320	.300	*	156	.310	*	90	*	89	.305	*	.305	105	.374
106	.320	.300	*	157	.310	*	91	*	90	.305	*	.305	106	.374
107	.320	.300	*	158	.310	*	92	*	91	.305	*	.305	107	.374
108	.320	.300	*	159	.310	*	93	*	92	.305	*	.305	108	.374
109	.320	.300	*	160	.310	*	94	*	93	.305	*	.305	109	.374
110	.320	.300	*	161	.310	*	95	*	94	.305	*	.305	110	.374
111	.320	.300	*	162	.310	*	96	*	95	.305	*	.305	111	.374
112	.320	.300	*	163	.310	*	97	*	96	.305	*	.305	112	.374
113	.320	.300	*	164	.310	*	98	*	97	.305	*	.305	113	.374
114	.320	.300	*	165	.310	*	99	*	98	.305	*	.305	114	.374
115	.320	.300	*	166	.310	*	100							

***** FICHER AD120 NACTI= 1
 30/ 3/85 16H 0 AS07 M=15 I=+2 R 2-5 NON ADAPTE AD120
 DE AD4 L'ITE. PAROIS RECTILIGNES SYMETRIQUES

MACH DE REFERENCE= .5993 UNF= 281.103 M/S
 TIV=301.9 K .PIV= 1395 MB

MACH PAROIS HAUTE ET BASSE				MACH PAROIS LAT. R.				MACH PAROIS LAT. L.				MACH PAROIS LAT. R.				MACH PAROIS LAT. L.											
I	HAUT	BAS		I	HAUT	BAS		I	HAUT	BAS		I	HAUT	BAS		I	HAUT	BAS		I	HAUT	BAS		I	HAUT	BAS	
1	.500	.599																									
2	.500	.502																									
3	.599	.599																									
4	.598	.599																									
5	.598	.599																									
6	.599	.599																									
7	.599	.599																									
8	.599	.599																									
9	.599	.599																									
10	.598	.599																									
11	.596	.599																									
12	.598	.599																									
13	.598	.599																									
14	.598	.599																									
15	.599	.599																									
16	.599	.599																									
17	.599	.599																									
18	.599	.599																									
19	.599	.599																									
20	.599	.599																									
21	.599	.599																									
22	.599	.599																									
23	.599	.599																									
24	.599	.599																									
25	.599	.599																									
26	.599	.599																									
27	.599	.599																									
28	.599	.599																									
29	.599	.599																									
30	.599	.599																									
31	.599	.599																									
32	.599	.599																									
33	.599	.599																									
34	.599	.599																									
35	.599	.599																									
36	.599	.599																									
37	.599	.599																									
38	.599	.599																									
39	.599	.599																									
40	.599	.599																									
41	.599	.599																									
42	.599	.599																									
43	.599	.599																									
44	.599	.599																									
45	.599	.599																									

***** FICHER AD122 NO(IT)= 1
 20/ 3/85 16H50 AS07 M=.6 I=+2(+1.5+ROT.30') R 2-5 NON ADAPTE AD122
 DE AD445 1'ITE. PAROIS RECTILIGNES + 30'

MACH DE REFERENCE= .6002 UINF= 231.108 M/S
 TIV=302.0 K PIV= 1393 MB

MACH PAROIS HAUTE ET BASSE						MACH PAROIS LATÉR.				HALE AS07				
I	HAUT	BAS	I	HAUT	BAS	I	MACH	I	MACH	I	MACH			
1	.608	.594	*	PRISES DOUBLES		*	HUB. AMONT	33	.607	*	1	.579		
2	.608	.598	*			*		34	.605	*	2	.581		
3	.604	.598	*	59	.600	.599	*	35	.605	*	3	.629		
4	.599	.597	*	60	.601	.601	*	36	.605	*	4	.666		
5	.597	.598	*	61	.601	.603	*	37	.604	*	5	.653		
6	.600	.601	*				*	38	.604	*	6	.609		
7	.600	.600	*	PRISES LAT. GAUCHES		*	39	.603	*	7	.555			
8	.601	.598	*			*	40	.603	*	8	.510			
9	.600	.601	*	62	.601	.598	*	41	.604	*	9	.381		
10	.602	.598	*	63	.603	.604	*	42	.605	*	10	1.023		
11	.599	.599	*	64	.605	.603	*	43	.603	*	11	.338		
12	.597	.599	*	65	.607	.601	*	44	.602	*	12	.362		
13	.599	.598	*	66	.613	.599	*	45	.601	*	13	.309		
14	.600	.600	*	67	.619	.604	*			*	14	.754		
15	.601	.600	*	68	.621	.603	*	HUB. AVAL	HUB. DROIT	*	15	.765		
16	.601	.599	*	69	.621	.602	*			*	16	.758		
17	.603	.600	*	70	.620	.601	*	1	.602	*	17	.741		
18	.606	.601	*	71	.611	.603	*	2	.602	*	18	.706		
19	.606	.601	*	72	.604	.606	*	3	.604	*	19	.723		
20	.607	.601	*	73	.579	.608	*	4	.607	*	20	.723		
21	.607	.599	*				*	5	.605	*	21	.711		
22	.611	.599	*	PRISES LAT. DROITES		*	5	.605	*	22	.792			
23	.615	.597	*			*	6	.605	*	23	.630			
24	.616	.598	*	74	.602	.600	*	7	.605	*	24	.568		
25	.620	.597	*	75	.601	.600	*	8	.606	*	25	.573		
26	.620	.598	*	76	.601	.609	*	9	.606	*	26	.623		
27	.624	.598	*	77	.599	.607	*	10	.604	*	27	.656		
28	.624	.600	*	78	.601	.608	*	11	.604	*	28	.639		
29	.627	.600	*	79	.605	.606	*	HUB. GAUCHE		*	29	.593		
30	.626	.602	*	80	.614	.597	*	12	.600	*	30	.549		
31	.630	.603	*	81	.620	.596	*	1	.600	*	31	.487		
32	.627	.602	*	82	.624	.594	*	2	.620	*	32	.349		
33	.629	.599	*	83	.628	.595	*	3	.619	*	33	1.042		
34	.626	.599	*	84	.633	.598	*	4	.611	*	34	1.045		
35	.627	.598	*	85	.635	.599	*	5	.611	*	35	.350		
36	.626	.599	*	86	.633	.599	*	6	.615	*	36	.363		
37	.627	.597	*	87	.631	.598	*	7	.613	*	37	.382		
38	.625	.597	*	88	.630	.597	*	8	.620	*	38	.304		
39	.627	.598	*	89	.631	.598	*	9	.620	*	39	.335		
40	.625	.599	*	90	.624	.600	*	10	.613	*	40	.767		
41	.624	.599	*	91	.617	.601	*	11	.615	*	41	.754		
42	.624	.600	*	92	.612	.603	*	12	.615	*	42	.741		
43	.620	.600	*	93	.605	.604	*	13	.614	*	43	.726		
44	.617	.600	*	94	.605	.603	*	14	.613	*	44	.706		
45	.615	.600	*	95	.598	.603	*	15	.608	*	45	.684		
46	.613	.602	*	96	.578	.602	*	16	.607	*	46	.579		
47	.613	.603	*				*	17	.607	*	47	.671		
48	.612	.605	*				*	18	.608	*	48	.642		
49	.609	.605	*				*	19	.608	*	49	.667		
50	.605	.605	*				*	20	.608	*	50	.638		
51	.604	.605	*				*	21	.609	*				
52	.602	.604	*	PRISES COL		*	22	.610	*	35	.601	*		
53	.600	.605	*			*	23	.608	*	36	.601	*		
54	.598	.606	*	.673	1.073	*	24	.612	*	37	.601	*		
55	.595	.605	*	.632	.896	*	25	.613	*	38	.600	*		
56	.589	.603	*	.806	.791	*	26	.614	*	39	.600	*		
57	.582	.603	*	.873	.692	*	27	.616	*	40	.600	*		
58	.571	.600	*	1.032	.632	*	28	.617	*	41	.600	*		
			*			*	29	.615	*	42	.600	*		
			*			*	30	.613	*	43	.600	*		
			*			*	31	.610	*	44	.600	*		
			*			*	32	.609	*	45	.600	*		

***** FICHER AD124 MOXITE= 1
 21/3/95 9H35 AS07 M=7 I=2+1.5*ROT.30'> R 2-5 NON ADAPTE AD124
 DE AD+5 L'ITE. PAROIS RECTILIGNES + 30'

MACH DE REFERENCE= .7034 . VINP= 231.109 M/S
 TIV=302.4 K PIV= 1521 MB

MACH PAROIS HAUTE ET BASSE				MACH PAROIS LATIER.				AILLE #337							
I	HAUT	BAS		I	HAUT	BAS		I	MACH	I	MACH	I	MACH	I	MACH
1	.713	.695	* PRISES DOUBLES	*			* HUB. AMONT	*	33	*	.715	*	1		
2	.712	.699			.702	.702			34		.714		2		
3	.707	.700			.705	.705			35		.712		3		
4	.702	.700			.705	.705			36		.712		4		
5	.700	.703			.706	.711			37		.712		5		
6	.702	.705	* PRISES LAT. GAUCHES*	*			* HUB. AVANT	*	38		.711		6		
7	.705	.703			.703	.703			39		.711		7		
8	.705	.705			.707	.707			40		.712		8		
9	.705	.701			.708	.708			41		.713		9		
10	.701	.702			.713	.707			42		.703		10		
11	.699	.702			.713	.707			43		.703		11		
12	.701	.701			.715	.715			44		.703		12		
13	.702	.705			.716	.716			45		.703		13		
14	.704	.705			.717	.710							14		
15	.704	.705			.717	.710			HUB. DROIT				15		
16	.705	.705			.717	.709							16		
17	.709	.705			.717	.709							17		
18	.712	.705			.719	.709							18		
19	.713	.705			.714	.714							19		
20	.713	.707			.715	.715							20		
21	.714	.705			.715	.715							21		
22	.711	.705	* PRISES LAT. DROITES*	*			* HUB. DROIT	*	1		.709		1		
23	.711	.702			.705	.705			2		.710		2		
24	.709	.702			.707	.707			3		.711		3		
25	.709	.705			.709	.709			4		.711		4		
26	.704	.705			.714	.714			5		.712		5		
27	.704	.705			.715	.715			6		.712		6		
28	.704	.705			.715	.715			7		.712		7		
29	.704	.705			.715	.715			8		.712		8		
30	.704	.705			.715	.715			9		.712		9		
31	.704	.705			.715	.715			10		.712		10		
32	.704	.705			.715	.715			11		.712		11		
33	.704	.705			.715	.715							12		
34	.704	.705			.715	.715			HUB. GAUCHE				13		
35	.704	.705			.715	.715							14		
36	.704	.705			.715	.715							15		
37	.704	.705			.715	.715							16		
38	.704	.705			.715	.715							17		
39	.704	.705			.715	.715							18		
40	.704	.705			.715	.715							19		
41	.704	.705			.715	.715							20		
42	.704	.705			.715	.715							21		
43	.704	.705			.715	.715							22		
44	.704	.705			.715	.715							23		
45	.704	.705			.715	.715							24		
46	.704	.705			.715	.715							25		
47	.704	.705			.715	.715							26		
48	.704	.705			.715	.715							27		
49	.704	.705			.715	.715							28		
50	.704	.705			.715	.715							29		
51	.704	.705			.715	.715							30		
52	.704	.705			.715	.715							31		
53	.704	.705			.715	.715							32		
54	.704	.705			.715	.715							33		
55	.704	.705			.715	.715							34		
56	.704	.705			.715	.715							35		
57	.704	.705			.715	.715							36		
58	.704	.705			.715	.715							37		
59	.704	.705			.715	.715							38		
60	.704	.705			.715	.715							39		
61	.704	.705			.715	.715							40		
62	.704	.705			.715	.715							41		
63	.704	.705			.715	.715							42		
64	.704	.705			.715	.715							43		
65	.704	.705			.715	.715							44		
66	.704	.705			.715	.715							45		
67	.704	.705			.715	.715							46		
68	.704	.705			.715	.715							47		
69	.704	.705			.715	.715							48		
70	.704	.705			.715	.715							49		
71	.704	.705			.715	.715							50		
72	.704	.705			.715	.715							51		
73	.704	.705			.715	.715							52		
74	.704	.705			.715	.715							53		
75	.704	.705			.715	.715							54		
76	.704	.705			.715	.715							55		
77	.704	.705			.715	.715							56		
78	.704	.705			.715	.715							57		
79	.704	.705			.715	.715							58		
80	.704	.705			.715	.715							59		
81	.704	.705			.715	.715							60		
82	.704	.705			.715	.715							61		
83	.704	.705			.715	.715							62		
84	.704	.705			.715	.715							63		
85	.704	.705			.715	.715							64		
86	.704	.705			.715	.715							65		
87	.704	.705			.715	.715							66		
88	.704	.705			.715	.715							67		
89	.704	.705			.715	.715							68		
90	.704	.705			.715	.715							69		
91	.704	.705			.715	.715							70		
92	.704	.705			.715	.715							71		
93	.704	.705			.715	.715							72		
94	.704	.705			.715	.715							73		
95	.704	.705			.715	.715							74		
96	.704	.705			.715	.715							75		
97	.704	.705			.715	.715							76		
98	.704	.705			.715	.715							77		
99	.704	.705			.715	.715							78		
100	.704	.705			.715	.715							79		

PRISES COL
 1 .704
 2 .705
 3 .705
 4 .705
 5 .705
 6 .705
 7 .705
 8 .705
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***** FICHER AD125 NOCITE= 1
 85 9H50 AS07 M=.7 I=+3(+1.5+ROT.30') R 2-5 ADAPTE 3D 1'ITE. AD125
 9124 1'ITE.

 MACH DE REFERENCE= .7031 UINF= 331.103 M/S
 TIV=300.7 K PIV= 1522 MB

MACH PAROIS HAUTE ET BASSE					MACH PAROIS LATÉR.					FILE AS07	
HAUT	BAS	I	HAUT	BAS	I	MACH	I	MACH	I	MACH	
.713	.694	*	PRISES DOUBLES		*	HUB. AMONT	33	.705	*	1	.668
.712	.699	**			**		34	.704	**	2	.683
.707	.700	**	59	.701	.702	1	.702	.703	**	3	.701
.702	.702	**	60	.705	.704	2	.701	.705	**	4	.708
.700	.705	**	61	.706	.696	3	.701	.705	**	5	.707
.702	.706	**			**	4	.702	.704	**	6	.707
.702	.704	**	PRISES LAT. GAUCHES		**	5	.700	.703	**	7	.663
.704	.702	**			**	6	.700	.703	**	8	.622
.705	.705	**	62	.704	.702	7	.700	.704	**	9	.414
.706	.700	**	63	.703	.706	8	.699	.704	**	10	1.391
.703	.702	**	64	.707	.705	9	.700	.702	**	11	1.395
.700	.702	**	65	.702	.702	10	.700	.702	**	12	.669
.702	.702	**	66	.703	.702	11	.702	.701	**	13	.663
.701	.704	**	67	.713	.706				**	14	.610
.701	.704	**	68	.713	.704	HUB. AVANT		HUB. DROIT		15	.684
.702	.702	**	69	.711	.704	1	.706	1	.704	15	.675
.704	.702	**	70	.713	.701	2	.705	2	.704	17	.663
.708	.703	**	71	.709	.703	3	.704	3	.703	18	.665
.707	.702	**	72	.706	.701	4	.705	4	.703	19	.657
.705	.703	**	73	.701	.703	5	.704	5	.703	20	.649
.703	.702	**			**	6	.704	6	.703	21	.682
.706	.702	**	PRISES LAT. DROITES		**	7	.704	7	.703	22	.631
.703	.701	**			**	8	.703	8	.704	23	.606
.706	.701	**	74	.705	.704	9	.704	9	.703	24	.675
.703	.700	**	75	.702	.702	10	.704	10	.703	25	.671
.703	.701	**	76	.704	.702	11	.700	11	.703	26	.679
.715	.700	**	77	.701	.700	12	.699	12	.703	27	.701
.716	.703	**	78	.702	.700	13	.703	13	.703	28	.716
.722	.703	**	79	.705	.697	HUB. GAUCHE		13	.703	29	.716
.719	.704	**	80	.710	.699	1	.714	14	.703	30	.666
.725	.700	**	81	.713	.699	2	.713	15	.703	31	.623
.721	.704	**	82	.712	.697	3	.713	16	.703	32	.663
.723	.703	**	83	.721	.699	4	.705	17	.703	33	1.166
.719	.701	**	84	.731	.701	5	.705	18	.703	34	1.166
.721	.700	**	85	.732	.703	6	.706	19	.703	35	1.168
.718	.701	**	86	.733	.702	7	.709	20	.703	36	1.024
.719	.699	**	87	.735	.701	8	.713	21	.703	37	.699
.717	.699	**	88	.732	.699	9	.716	22	.703	38	.691
.720	.699	**	89	.734	.698	10	.716	23	.703	39	.611
.717	.700	**	90	.716	.699	11	.714	24	.703	40	.693
.716	.699	**	91	.712	.699	12	.713	25	.703	41	.676
.716	.699	**	92	.709	.703	13	.712	26	.704	42	.664
.715	.698	**	93	.703	.702	14	.711	27	.704	43	.647
.713	.699	**	94	.709	.698	15	.710	28	.704	44	.629
.712	.699	**	95	.706	.695	16	.707	29	.703	45	.600
.709	.701	**	96	.700	.692	17	.705	30	.703	46	.624
.710	.703	**			**	18	.705	31	.703	47	.703
.710	.705	**			**	19	.705	32	.703	48	.740
.709	.704	**			**	20	.705	33	.703	49	.773
.707	.702	**			**	21	.706	34	.703	50	.701
.703	.700	**			**	22	.706	35	.703		
.707	.697	**	PRISES COL		**	23	.707	36	.703		
.703	.699	**			**	24	.706	37	.703		
.707	.701	**	.760	1.154	**	25	.710	38	.703		
.706	.700	**	.780	1.086	**	26	.713	39	.703		
.705	.699	**	.873	.962	**	27	.714	40	.703		
.703	.697	**	.929	.767	**	28	.717	41	.703		
.701	.691	*	1.096	.713	*	29	.718	42	.703		
						30	.715	43	.703		
						31	.711	44	.703		
						32	.709	45	.702		
							.707				

***** FICHER AD136 N0(1T)= 1
 21/ 3/85 10H 5 A307 M=.3 I=+2(+1.5+ROT.30') R 2-5 NON ADAPTE AD136
 DE AD445 1'ITE. PAROIS RECTILIGNES + 30'

MACH DE REFERENCE= .8060 UINF= 231.108 M/S
 TIV=300.3 K PIV= 1553 MB

MACH PAROIS HAUTE ET BASSE						MACH PAROIS LATER.				AILE A307		
I	HAUT	BAS	I	HAUT	BAS	I	MACH	I	MACH	I	MACH	
1	.819	.795	*	PRISES DOUBLES		HUB. AMONT	33	.839	*	1	.794	
2	.818	.800	*				34	.835	*	2	.811	
3	.811	.801	*	59	.801	.804	*	35	.832	*	3	.879
4	.804	.803	*	60	.810	.809	*	36	.827	*	4	.854
5	.800	.806	*	61	.820	.825	*	37	.823	*	5	.803
6	.802	.808	*				38	.820	*	6	.847	
7	.801	.806	*	PRISES LAT. GAUCHES			39	.831	*	7	.757	
8	.807	.806	*				40	.835	*	8	.713	
9	.809	.812	*	62	.806	.802	*	41	.849	*	9	.745
10	.811	.804	*	63	.801	.813	*	42	.840	*	10	1.458
11	.808	.806	*	64	.816	.815	*	43	.829	*	11	1.504
12	.805	.807	*	65	.824	.816	*	44	.827	*	12	1.483
13	.807	.806	*	66	.846	.824	*	45	.825	*	13	1.443
14	.806	.809	*	67	.871	.825	*			14	1.390	
15	.807	.809	*	68	.883	.825	*	HUB. AVANT	HUB. DROIT	15	1.123	
16	.808	.808	*	69	.897	.832	*			16	1.389	
17	.811	.809	*	70	.887	.831	*	1	.827	1	.805	
18	.817	.812	*	71	.847	.829	*	2	.827	2	.805	
19	.818	.813	*	72	.832	.835	*	3	.828	3	.807	
20	.820	.815	*	73	.788	.835	*	4	.835	4	.805	
21	.824	.815	*				5	.831	5	5	.805	
22	.833	.814	*	PRISES LAT. DROITES			6	.830	6	6	.805	
23	.842	.813	*				7	.828	7	7	.805	
24	.847	.819	*	74	.808	.804	*	8	.830	8	.805	
25	.853	.821	*	75	.802	.806	*	9	.832	9	.805	
26	.858	.821	*	76	.808	.805	*	10	.830	10	.805	
27	.872	.817	*	77	.807	.804	*	11	.830	11	.805	
28	.877	.821	*	78	.808	.806	*			12	.805	
29	.895	.820	*	79	.817	.806	*	HUB. GAUCHE	13	.805		
30	.891	.821	*	80	.833	.811	*			14	.805	
31	.911	.816	*	81	.851	.818	*	1	.830	15	.805	
32	.904	.824	*	82	.860	.819	*	2	.877	16	.805	
33	.920	.823	*	83	.888	.814	*	3	.874	17	.805	
34	.911	.822	*	84	.928	.816	*	4	.836	18	.805	
35	.934	.822	*	85	.934	.821	*	5	.844	19	.805	
36	.919	.826	*	86	.932	.823	*	6	.855	20	.805	
37	.932	.823	*	87	.929	.824	*	7	.871	21	.805	
38	.914	.825	*	88	.928	.822	*	8	.887	22	.805	
39	.908	.824	*	89	.902	.822	*	9	.895	23	.805	
40	.900	.824	*	90	.877	.825	*	10	.876	24	.805	
41	.893	.823	*	91	.858	.827	*	11	.867	25	.805	
42	.888	.824	*	92	.848	.830	*	12	.863	26	.805	
43	.871	.824	*	93	.831	.829	*	13	.858	27	.805	
44	.860	.827	*	94	.830	.829	*	14	.853	28	.805	
45	.855	.825	*	95	.818	.850	*	15	.828	29	.805	
46	.851	.828	*	96	.789	.848	*	16	.828	30	.805	
47	.848	.828	*				17	.830	31	.805		
48	.843	.831	*				18	.832	32	.805		
49	.838	.830	*				19	.834	33	.805		
50	.832	.831	*				20	.838	34	.805		
51	.830	.830	*				21	.841	35	.805		
52	.823	.827	*	PRISES COL			22	.845	36	.805		
53	.823	.829	*				23	.845	37	.805		
54	.822	.831	*	.881	1.233	*	24	.853	38	.805		
55	.820	.832	*	.873	.907	*	25	.859	39	.805		
56	.811	.833	*	.957	.862	*	26	.868	40	.805		
57	.798	.845	*	.999	.812	*	27	.882	41	.805		
58	.775	.864	*	1.157	.776	*	28	.891	42	.805		
			*				29	.874	43	.805		
			*				30	.856	44	.805		
			*				31	.848	45	.805		
			*				32	.843				

***** FICHER AD127 HQ(ITE)= 1
 31/ 3/95 10H20 AS07 M=9 I=+2(+1.5+ROT.30') R 2-5 ADAPTE 3D 1'ITE. AD127
 DE AD9126 1'ITE.

MACH DE REFERENCE= .3056 UINF= 231.108 M=8
 TIV=299.9 K PIV= 1551 MB

MACH PAROIS HAUTE ET BASSE						MACH PAROIS LATER.				FILE AS07			
I	HAUT	BAS	I	HAUT	BAS	I	MACH	I	MACH	I	MACH		
1	.320	.796	*	PRISES DOUBLES		*	HUB. AMONT	33	.305	*	1	.754	
2	.319	.801	+			+		34	.304	+	2	.775	
3	.312	.800	+	59	.301	.305	1	.304	.302	+	3	.341	
4	.305	.803	+	60	.307	.307	2	.303	.307	+	4	.313	
5	.301	.806	+	61	.304	.799	3	.302	.305	+	5	.338	
6	.303	.808	+				4	.304	.304	+	6	.336	
7	.301	.307	+	PRISES LAT. GAUCHES		+	5	.302	.302	+	7	.749	
8	.306	.307	+			+	6	.301	.302	+	8	.713	
9	.303	.812	+	62	.307	.302	7	.301	.303	+	9	.438	
10	.303	.302	+	63	.799	.310	8	.300	.303	+	10	1.456	
11	.305	.803	+	64	.311	.312	9	.303	.301	+	11	1.474	
12	.302	.302	+	65	.307	.306	10	.303	.301	+	12	1.433	
13	.304	.302	+	66	.306	.302	11	.305	.300	+	13	1.365	
14	.304	.306	+	67	.310	.307				+	14	1.315	
15	.305	.303	+	68	.308	.302		HUB. AVAL	HUB. DROIT	+	15	1.315	
16	.306	.303	+	69	.312	.302	1			+	16	1.307	
17	.307	.307	+	70	.313	.799	2	.304	1	.306	+	17	1.313
18	.309	.304	+	71	.307	.799	3	.302	2	.306	+	18	1.321
19	.309	.303	+	72	.304	.796	4	.301	3	.306	+	19	1.313
20	.309	.306	+	73	.309	.797	5	.302	4	.306	+	20	1.303
21	.307	.305	+				6	.300	5	.306	+	21	.330
22	.303	.302	+	PRISES LAT. DROITES		+	7	.300	6	.306	+	22	.969
23	.312	.799	+			+	8	.300	7	.306	+	23	.934
24	.312	.301	+	74	.310	.304	9	.301	8	.306	+	24	.730
25	.314	.303	+	75	.302	.307	10	.300	9	.306	+	25	.733
26	.313	.302	+	76	.306	.304	11	.796	10	.307	+	26	.323
27	.319	.799	+	77	.304	.300	12	.794	11	.306	+	27	.303
28	.313	.304	+	78	.303	.304	13		12	.306	+	28	.333
29	.325	.305	+	79	.308	.797		HUB. GAUCHE	13	.306	+	29	.324
30	.319	.305	+	80	.316	.301	1		14	.306	+	30	.713
31	.326	.799	+	81	.319	.793	2	.313	15	.306	+	31	.723
32	.320	.304	+	82	.313	.796	3	.312	16	.306	+	32	.419
33	.325	.303	+	83	.329	.793	4	.314	17	.306	+	33	1.364
34	.319	.799	+	84	.328	.302	5	.306	18	.306	+	34	1.334
35	.323	.799	+	85	.328	.304	6	.306	19	.306	+	35	1.382
36	.321	.793	+	86	.332	.303	7	.309	20	.306	+	36	1.437
37	.324	.796	+	87	.329	.300	8	.315	21	.306	+	37	1.430
38	.322	.796	+	88	.326	.795	9	.321	22	.306	+	38	1.430
39	.326	.794	+	89	.329	.793	10	.324	23	.306	+	39	1.403
40	.323	.794	+	90	.313	.794	11	.313	24	.305	+	40	1.293
41	.322	.794	+	91	.310	.797	12	.315	25	.305	+	41	.332
42	.323	.795	+	92	.309	.300	13	.314	26	.305	+	42	.345
43	.317	.795	+	93	.799	.799	14	.313	27	.305	+	43	.330
44	.310	.795	+	94	.306	.793	15	.311	28	.306	+	44	.337
45	.303	.795	+	95	.303	.796	16	.303	29	.306	+	45	.312
46	.306	.797	+	96	.308	.793	17	.306	30	.305	+	46	.311
47	.309	.799	+				18	.306	31	.305	+	47	.332
48	.303	.302	+				19	.306	32	.305	+	48	.331
49	.306	.300	+				20	.305	33	.305	+	49	.331
50	.304	.799	+				21	.306	34	.306	+	50	.329
51	.306	.795	+				22	.307	35	.305	+		
52	.306	.790	+	PRISES COL		+	23	.303	36	.306	+		
53	.303	.792	+			+	24	.306	37	.305	+		
54	.307	.793	+	.348	1.213	+	25	.311	38	.306	+		
55	.303	.793	+	.363	1.213	+	26	.314	39	.306	+		
56	.303	.793	+	.336	.327	+	27	.313	40	.306	+		
57	.313	.793	+	.331	.321	+	28	.323	41	.306	+		
58	.315	.777	+	1.141	.730	+	29	.325	42	.306	+		
							30	.313	43	.306	+		
							31	.310	44	.306	+		
							32	.306	45	.306	+		

***** FICHER AD123 N0CIT= 1
 21/ 8/85 10H35 AS07 M=.3 I=+2(+1.5+RDT.30') R 2-5 ADAPTE 3D 2'ITE. AD123
 DE AD9127 1'ITE.

MACH DE REFERENCE= .3058 UINF= 231.108 M/S
 TIV=299.3 K PIV= 1549 MB

MACH PAROIS HAUTE ET BASSE						MACH PAROIS LATER.				HAIE
I	HAUT	BAS	I	HAUT	BAS	I	MACH	I	MACH	I
1	.319	.795	PRISES DOUBLES			HUB. AMONT	33	.309		1
2	.313	.801					34	.307		2
3	.311	.801	59	.305	.306	1	.302	35	.305	3
4	.303	.802	60	.310	.308	2	.301	36	.307	4
5	.300	.805	61	.303	.305	3	.301	37	.305	5
6	.305	.809				4	.304	38	.304	6
7	.305	.803	PRISES LAT. GAUCHES			5	.301	39	.303	7
8	.309	.805				6	.301	40	.304	8
9	.309	.809	62	.306	.301	7	.300	41	.307	9
10	.311	.803	63	.301	.311	8	.799	42	.307	10
11	.306	.804	64	.308	.310	9	.301	43	.303	11
12	.300	.803	65	.308	.303	10	.301	44	.302	12
13	.302	.802	66	.309	.300	11	.303	45	.300	13
14	.302	.805	67	.322	.305					14
15	.303	.807	68	.325	.304	HUB. AVAL		HUB. DROIT		15
16	.303	.805	69	.331	.305	1	.303	1	.306	16
17	.304	.805	70	.331	.302	2	.307	2	.306	17
18	.306	.803	71	.314	.301	3	.307	3	.305	18
19	.305	.800	72	.311	.309	4	.310	4	.305	19
20	.307	.802	73	.305	.315	5	.309	5	.306	20
21	.309	.802				6	.309	6	.305	21
22	.313	.803	PRISES LAT. DROITES			7	.308	7	.305	22
23	.317	.800				8	.309	8	.306	23
24	.316	.800	74	.308	.304	9	.310	9	.306	24
25	.317	.799	75	.305	.307	10	.307	10	.306	25
26	.313	.799	76	.308	.304	11	.308	11	.305	26
27	.326	.795	77	.302	.300					27
28	.328	.801	78	.300	.301	HUB. GAUCHE				28
29	.338	.801	79	.304	.794	13	.305	13	.305	29
30	.333	.802	80	.317	.798	14	.306	14	.306	30
31	.344	.797	81	.325	.798	1	.325	15	.305	31
32	.338	.803	82	.322	.793	2	.325	16	.305	32
33	.345	.802	83	.338	.794	3	.325	17	.307	33
34	.339	.799	84	.354	.798	4	.310	18	.306	34
35	.344	.799	85	.357	.802	5	.311	19	.306	35
36	.342	.800	86	.353	.302	6	.317	20	.305	36
37	.344	.793	87	.350	.300	7	.325	21	.305	37
38	.341	.799	88	.347	.797	8	.333	22	.305	38
39	.342	.799	89	.343	.797	9	.336	23	.305	39
40	.337	.793	90	.329	.799	10	.329	24	.305	40
41	.334	.793	91	.319	.301	11	.324	25	.305	41
42	.334	.799	92	.316	.303	12	.322	26	.305	42
43	.327	.800	93	.307	.301	13	.320	27	.305	43
44	.319	.801	94	.310	.305	14	.317	28	.305	44
45	.317	.800	95	.303	.305	15	.309	29	.305	45
46	.315	.801	96	.304	.302	16	.308	30	.305	46
47	.316	.801				17	.308	31	.305	47
48	.316	.804				18	.308	32	.305	48
49	.316	.803				19	.308	33	.305	49
50	.312	.805				20	.309	34	.305	50
51	.311	.807				21	.311	35	.305	
52	.305	.805	PRISES COL			22	.312	36	.305	
53	.307	.310				23	.312	37	.305	
54	.308	.310	.858	1.220		24	.317	38	.305	
55	.309	.303	.866	.989		25	.321	39	.305	
56	.307	.305	.942	.981		26	.325	40	.305	
57	.307	.305	.995	.319		27	.333	41	.305	
58	.305	.303	1.147	.777		28	.335	42	.305	
						29	.327	43	.305	
						30	.318	44	.305	
						31	.313	45	.305	
						32	.311			

***** FICHER AD129 NO(IT)= 1
 21/ 2/85 10450 AS07 M=3 I=+2(+1.5+ROT.30') R 2-5 ADAPTE 3D 3'ITE. AD129
 DE AD9128 1'ITE.

MACH DE REFERENCE= .3059 UINF= 231.108 M/S
 TIV=299.3 K PIV= 1649 MB

MACH PAROIS HAUTE ET BASSE						MACH PAROIS LATÉR.				RILE AS07				
I	HAUT	BAS		I	HAUT	BAS	I	MACH	I	MACH	I	MACH		
1	.820	.797	+	PRISES DOUBLES			HUB. AMONT		33	.810	+	1	.763	
2	.820	.803	+						34	.809	+	2	.781	
3	.814	.803	+	59	.803	.805	+	1	.805	35	.807	+	3	.845
4	.806	.804	+	60	.807	.808	+	2	.803	36	.809	+	4	.832
5	.802	.806	+	61	.808	.805	+	3	.803	37	.809	+	5	.800
6	.805	.810	+					4	.805	38	.807	+	6	.827
7	.803	.806	+	PRISES LAT. GAUCHES			5	.802	39	.806	+	7	.747	
8	.805	.803	+					6	.802	40	.807	+	8	.712
9	.806	.808	+	62	.809	.805	+	7	.801	41	.809	+	9	.441
10	.808	.803	+	63	.799	.812	+	8	.800	42	.809	+	10	1.475
11	.805	.806	+	64	.812	.809	+	9	.802	43	.804	+	11	1.479
12	.801	.807	+	65	.807	.806	+	10	.802	44	.803	+	12	1.434
13	.804	.805	+	66	.806	.805	+	11	.803	45	.802	+	13	1.364
14	.805	.808	+	67	.824	.809	+						14	1.059
15	.807	.807	+	68	.824	.804	+	HUB. AVAL		HUB. DROIT		15	1.333	
16	.807	.804	+	69	.829	.805	+					16	1.014	
17	.807	.803	+	70	.832	.805	+	1	.811	1	.805	+	17	1.024
18	.810	.805	+	71	.815	.802	+	2	.809	2	.806	+	18	1.040
19	.808	.805	+	72	.812	.810	+	3	.809	3	.806	+	19	1.039
20	.807	.807	+	73	.810	.814	+	4	.811	4	.806	+	20	1.029
21	.808	.805	+					5	.809	5	.806	+	21	1.001
22	.812	.802	+	PRISES LAT. DROITES			6	.809	6	.806	+	22	.974	
23	.816	.799	+					7	.809	7	.806	+	23	.946
24	.813	.803	+	74	.811	.806	+	8	.810	8	.805	+	24	.723
25	.814	.805	+	75	.804	.808	+	9	.811	9	.806	+	25	.761
26	.815	.805	+	76	.806	.805	+	10	.807	10	.806	+	26	.832
27	.825	.802	+	77	.804	.803	+	11	.807	11	.806	+	27	.809
28	.829	.805	+	78	.805	.801	+			12	.806	+	28	.809
29	.849	.805	+	79	.807	.798	+	HUB. GAUCHE		13	.806	+	29	.823
30	.835	.805	+	80	.816	.801	+			14	.806	+	30	.756
31	.845	.799	+	81	.824	.797	+	1	.825	15	.806	+	31	.723
32	.838	.805	+	82	.819	.800	+	2	.825	16	.806	+	32	.437
33	.844	.803	+	83	.826	.799	+	3	.825	17	.806	+	33	1.576
34	.837	.800	+	84	.854	.801	+	4	.810	18	.806	+	34	1.504
35	.841	.799	+	85	.857	.804	+	5	.812	19	.807	+	35	1.501
36	.839	.800	+	86	.851	.803	+	6	.817	20	.806	+	36	1.510
37	.842	.798	+	87	.847	.801	+	7	.825	21	.806	+	37	1.474
38	.840	.800	+	88	.844	.798	+	8	.833	22	.806	+	38	1.455
39	.843	.799	+	89	.845	.799	+	9	.835	23	.806	+	39	1.440
40	.838	.800	+	90	.831	.802	+	10	.823	24	.806	+	40	1.423
41	.835	.800	+	91	.817	.804	+	11	.824	25	.806	+	41	1.383
42	.835	.801	+	92	.816	.803	+	12	.823	26	.806	+	42	1.039
43	.826	.802	+	93	.807	.803	+	13	.820	27	.806	+	43	.944
44	.817	.802	+	94	.813	.806	+	14	.818	28	.805	+	44	.892
45	.815	.802	+	95	.808	.791	+	15	.810	29	.806	+	45	.913
46	.813	.802	+	96	.808	.787	+	16	.808	30	.806	+	46	.913
47	.816	.801	+					17	.809	31	.806	+	47	.911
48	.817	.804	+					18	.810	32	.806	+	48	.896
49	.815	.805	+					19	.810	33	.806	+	49	.895
50	.812	.807	+					20	.811	34	.806	+	50	.835
51	.813	.809	+					21	.812	35	.806	+		
52	.811	.806	+	PRISES COL			22	.814	36	.806	+			
53	.811	.809	+					23	.812	37	.806	+		
54	.812	.810	+	.860	1.219		+	24	.818	38	.806	+		
55	.813	.806	+	.868	.867		+	25	.822	39	.806	+		
56	.811	.802	+	.843	.876		+	26	.827	40	.806	+		
57	.811	.796	+	.895	.817		+	27	.833	41	.806	+		
58	.811	.776	+	1.146	.777		+	28	.835	42	.806	+		
								29	.827	43	.806	+		
								30	.819	44	.806	+		
								31	.814	45	.806	+		
								32	.812					

***** FICHER AD130 NO(CIT)= 4
 21/3/35 12H20 AS07 M=7 I=1.5 R 2-5 ADAPTE 2D AD130
 DE AD4 L'ITE. PAROIS RECTILIGNES SYMETRIQUES

MACH DE REFERENCE= .7071 UINF= 231.109 M/S
 TIV=294.0 K PIV= 1525 MB

MACH PAROIS HAUTE ET BASSE						MACH PAROIS LATER.				FILE AS0		
I	HAUT	BAS	I	HAUT	BAS	I	MACH	I	MACH	I	MACH	
1	.706	.702	PRISES DOUBLES			HUB. AMONT	33	.707	34	.706	1	.706
2	.707	.707								2	.706	
3	.707	.705	59	.705	.704	1	.705	35	.705	3	.705	
4	.704	.704	60	.709	.703	2	.704	36	.706	4	.706	
5	.704	.705	61	.705	.703	3	.704	37	.706	5	.706	
6	.707	.707								6	.705	
7	.706	.705	PRISES LAT. GAUCHES			4	.704	38	.705	7	.704	
8	.705	.702								8	.703	
9	.706	.705	62	.705	.705	5	.703	39	.704	9	.705	
10	.708	.700	63	.705	.709	6	.703	40	.705	10	.705	
11	.707	.701	64	.710	.709	7	.703	41	.705	11	.705	
12	.705	.703	65	.710	.704	8	.702	42	.705	12	.705	
13	.706	.705	66	.710	.701	9	.703	43	.704	13	.703	
14	.707	.709	67	.719	.706	10	.703	44	.703	14	.703	
15	.707	.711	68	.716	.705	11	.703	45	.703	15	.703	
16	.707	.706	69	.715	.705	HUB. AVAL		HUB. DROIT		16	.703	
17	.707	.704	70	.720	.703	1	.708	1	.705	17	.703	
18	.710	.704	71	.714	.703	2	.707	2	.705	18	.703	
19	.709	.703	72	.709	.707	3	.707	3	.705	19	.703	
20	.709	.704	73	.693	.710	4	.709	4	.705	20	.703	
21	.711	.703								21	.705	
22	.715	.702	PRISES LAT. DROITES			5	.707	5	.705	22	.705	
23	.713	.700								23	.705	
24	.716	.701	74	.706	.707	6	.707	6	.705	24	.705	
25	.717	.701	75	.705	.705	7	.708	7	.705	25	.705	
26	.717	.701	76	.707	.699	8	.708	8	.705	26	.705	
27	.723	.700	77	.706	.703	9	.705	9	.705	27	.705	
28	.724	.703	78	.705	.699	10	.705	10	.705	28	.705	
29	.730	.704	79	.707	.698	11	.705	11	.705	29	.705	
30	.726	.704	80	.713	.709	HUB. GAUCHE				30	.705	
31	.731	.700	81	.725	.699	1	.713	1	.705	31	.705	
32	.726	.705	82	.722	.697	2	.713	2	.705	32	.705	
33	.728	.704	83	.730	.693	3	.713	3	.705	33	.705	
34	.723	.702	84	.738	.701	4	.711	4	.705	34	.705	
35	.725	.702	85	.739	.703	5	.711	5	.705	35	.705	
36	.733	.703	86	.733	.703	6	.714	6	.705	36	.705	
37	.735	.701	87	.729	.702	7	.717	7	.705	37	.705	
38	.724	.702	88	.722	.700	8	.720	8	.705	38	.705	
39	.727	.701	89	.731	.700	9	.721	9	.705	39	.705	
40	.724	.701	90	.724	.703	10	.719	10	.705	40	.705	
41	.724	.702	91	.713	.704	11	.717	11	.705	41	.705	
42	.724	.702	92	.715	.703	12	.716	12	.705	42	.705	
43	.721	.703	93	.705	.703	13	.715	13	.705	43	.705	
44	.718	.704	94	.707	.704	14	.713	14	.705	44	.705	
45	.717	.703	95	.705	.704	15	.713	15	.705	45	.705	
46	.715	.704	96	.691	.701	16	.708	16	.705	46	.705	
47	.716	.703								47	.705	
48	.715	.705								48	.705	
49	.713	.705								49	.705	
50	.708	.706								50	.705	
51	.709	.706								51	.705	
52	.708	.704	PRISES COL			22	.710	25	.705	52	.705	
53	.708	.706								53	.705	
54	.708	.707	781	1.155		23	.709	26	.705	54	.705	
55	.707	.705	795	1.062		24	.713	27	.705	55	.705	
56	.702	.703	875	.883		25	.714	28	.705	56	.705	
57	.696	.703	931	.771		26	.717	29	.705	57	.705	
58	.685	.703	1.096	.713		27	.719	30	.705	58	.705	
						28	.721	31	.705			
						29	.718	32	.705			
						30	.714	33	.705			
						31	.711	34	.705			
						32	.709					

***** FICHER AD131 NO(IT)= 4
 21/ 3/85 14H50 AS07 M=.6 I=1.5 R 2-5 ADAPTE 3D AD131
 DE AD130 4'ITE.

MACH DE REFERENCE= .6019 UINF= 231.108 M/S
 TIV=296.4 K PIV= 1393 MB

MACH PAROIS HAUTE ET BASSE						MACH PAROIS LATER.				AILE AS07	
I	HAUT	BAS	I	HAUT	BAS	I	MACH	I	MACH	I	MACH
1	.604	.600	PRISES DOUBLES			HUB. AMONT	33	.603	1	.572	
2	.604	.603					34	.602	2	.581	
3	.603	.601	59	.602	.600	1	.602	35	.601	3	.623
4	.601	.601	60	.604	.600	2	.601	36	.602	4	.669
5	.601	.602	61	.602	.599	3	.601	37	.602	5	.658
6	.603	.603				4	.601	38	.601	6	.617
7	.602	.601	PRISES LAT. GAUCHES			5	.600	39	.600	7	.566
8	.603	.601				6	.600	40	.601	8	.529
9	.602	.602	62	.602	.602	7	.600	41	.601	9	.675
10	.604	.598	63	.605	.604	8	.599	42	.601	10	1.021
11	.602	.597	64	.603	.603	9	.600	43	.599	11	.886
12	.601	.599	65	.605	.601	10	.599	44	.599	12	.823
13	.602	.600	66	.606	.599	11	.600	45	.599	13	.784
14	.601	.602	67	.609	.602					14	.755
15	.602	.605	68	.609	.601	HUB. AVAL	HUB. DROIT	15	.750		
16	.602	.601	69	.609	.602			16	.735		
17	.601	.598	70	.612	.599	1	.604	1	.602	17	.723
18	.603	.598	71	.607	.600	2	.603	2	.602	18	.726
19	.603	.598	72	.604	.602	3	.604	3	.601	19	.719
20	.605	.601	73	.596	.603	4	.604	4	.602	20	.711
21	.605	.600				5	.603	5	.602	21	.699
22	.607	.599	PRISES LAT. DROITES			6	.603	6	.602	22	.691
23	.608	.597				7	.603	7	.602	23	.682
24	.608	.597	74	.603	.603	8	.605	8	.601	24	.680
25	.610	.597	75	.602	.602	9	.603	9	.602	25	.675
26	.609	.597	76	.602	.597	10	.602	10	.602	26	.632
27	.613	.596	77	.602	.603	11	.602	11	.602	27	.661
28	.613	.599	78	.600	.595			12	.602	28	.646
29	.616	.599	79	.602	.594	HUB. GAUCHE	13	.601	13	.604	
30	.614	.599	80	.612	.598			14	.602	30	.566
31	.617	.596	81	.613	.595	1	.610	15	.602	31	.621
32	.614	.599	82	.614	.595	2	.609	16	.602	32	.640
33	.616	.599	83	.618	.596	3	.609	17	.601	33	1.108
34	.613	.599	84	.622	.597	4	.605	18	.602	34	.986
35	.615	.598	85	.623	.599	5	.605	19	.602	35	.861
36	.613	.599	86	.620	.599	6	.608	20	.601	36	.806
37	.615	.598	87	.619	.599	7	.609	21	.602	37	.785
38	.615	.598	88	.618	.598	8	.611	22	.602	38	.773
39	.617	.598	89	.621	.598	9	.612	23	.602	39	.760
40	.615	.598	90	.616	.599	10	.611	24	.602	40	.746
41	.615	.598	91	.618	.600	11	.609	25	.602	41	.734
42	.615	.599	92	.608	.599	12	.609	26	.601	42	.727
43	.613	.599	93	.602	.599	13	.607	27	.602	43	.713
44	.610	.599	94	.603	.600	14	.607	28	.601	44	.697
45	.608	.599	95	.601	.595	15	.604	29	.601	45	.678
46	.607	.599	96	.593	.593	16	.603	30	.602	46	.674
47	.609	.599				17	.603	31	.602	47	.665
48	.608	.600				18	.603	32	.602	48	.638
49	.606	.600				19	.604	33	.602	49	.663
50	.603	.600				20	.603	34	.602	50	.635
51	.604	.601				21	.604	35	.602		
52	.603	.600	PRISES COL			22	.605	36	.602		
53	.604	.601				23	.603	37	.602		
54	.604	.601	.663	1.060		24	.607	38	.602		
55	.602	.599	.698	.912		25	.608	39	.601		
56	.608	.598	.799	.797		26	.608	40	.602		
57	.597	.596	.865	.694		27	.611	41	.602		
58	.593	.593	1.024	.634		28	.611	42	.602		
						29	.609	43	.601		
						30	.608	44	.601		
						31	.606	45	.602		
						32	.604				

***** FICHER AD133 HAUT= 4
 21/3x35 SH55 AS07 M=3 I=0 R=25 ADAPTE 2D AD133
 DE AD4 LITE. PAROIS RECTILIGNES SYMETRIQUES

MACH DE REFERENCE= .3073 UNIF= 231.103 M/S
 TIV=295.2 K PIV= 1553 MB

MACH PAROIS HAUTE ET BASSE		MACH PAROIS LATÉR.		AILS AS07		
I	HAUT	BAS	I	MACH	I	MACH
1	.309	.304	PRISES DOUBLES	HUB. AMONT	33	.313
2	.311	.312	59 .310 .310	1 .303	34	.312
3	.309	.305	60 .310 .304	2 .303	35	.311
4	.304	.307	61 .304 .304	3 .302	36	.311
5	.303	.312	PRISES LAT. GAUCHES	4 .302	37	.311
6	.310	.312	62 .310 .310	5 .301	38	.311
7	.310	.307	63 .305 .305	6 .301	39	.312
8	.303	.303	64 .302 .312	7 .300	40	.313
9	.311	.798	65 .311 .313	8 .300	41	.312
10	.306	.797	66 .311 .303	9 .301	42	.310
11	.300	.798	67 .315 .306	10 .301	43	.303
12	.302	.303	68 .321 .310	11 .302	44	.303
13	.303	.312	69 .321 .310	HUB. HVALL HUB. DROIT	45	.303
14	.305	.319	70 .321 .312	1 .302		
15	.306	.303	71 .324 .306	2 .307		
16	.307	.302	72 .314 .310	3 .307		
17	.310	.302	73 .312 .310	4 .309		
18	.303	.307	PRISES LAT. DROITES	5 .307		
19	.309	.306	74 .307 .311	6 .307		
20	.313	.303	75 .311 .311	7 .307		
21	.317	.305	76 .311 .311	8 .307		
22	.319	.305	77 .311 .311	9 .309		
23	.320	.309	78 .312 .312	10 .306		
24	.321	.307	79 .312 .312	11 .307		
25	.326	.310	80 .315 .315	HUB. GAUCHE		
26	.326	.311	81 .312 .312	1 .302		
27	.327	.311	82 .312 .312	2 .302		
28	.335	.303	83 .303 .303	3 .302		
29	.335	.314	84 .311 .311	4 .312		
30	.331	.310	85 .315 .315	5 .312		
31	.334	.311	86 .315 .315	6 .312		
32	.336	.305	87 .314 .314	7 .315		
33	.332	.308	88 .313 .313	8 .315		
34	.334	.306	89 .303 .303	9 .315		
35	.327	.304	90 .305 .305	10 .312		
36	.327	.304	91 .317 .317	11 .307		
37	.3215	.304	92 .317 .317	12 .310		
38	.317	.305	93 .317 .317	13 .310		
39	.316	.306	94 .319 .319	14 .311		
40	.310	.306	95 .319 .319	15 .310		
41	.311	.305	96 .319 .319	16 .311		
42	.306	.303	97 .319 .319	17 .311		
43	.306	.303	98 .319 .319	18 .311		
44	.306	.303	99 .319 .319	19 .312		
45	.305	.303	100 .319 .319	20 .312		
46	.305	.303	101 .319 .319	21 .312		
47	.305	.303	102 .319 .319	22 .312		
48	.305	.303	103 .319 .319	23 .312		
49	.305	.303	104 .319 .319	24 .312		
50	.305	.303	105 .319 .319	25 .312		
51	.305	.303	106 .319 .319	26 .312		
52	.305	.303	107 .319 .319	27 .312		
53	.305	.303	108 .319 .319	28 .312		
54	.305	.303	109 .319 .319	29 .312		
55	.305	.303	110 .319 .319	30 .312		
56	.305	.303	111 .319 .319	31 .312		
57	.305	.303	112 .319 .319	32 .312		
58	.305	.303	113 .319 .319	33 .312		
59	.305	.303	114 .319 .319	34 .312		
60	.305	.303	115 .319 .319	35 .312		

***** FICHER AD134 NO(IT)= 4
 21/ 3/85 17H15 AS07 M=3 I=0 R 2-5 ADAPTE 2D AD134
 DE AD133 4'ITE

 MACH DE REFERENCE= .8085 UINF= 231.108 M/S
 TIV=297.1 K PIV= 1552 MB

MACH PAROIS HAUTE ET BASSE						MACH PAROIS LATER.				FILE AS07			
I	HAUT	BAS	I	HAUT	BAS	I	MACH	I	MACH	I	MACH		
1	.811	.805	*	PRISES DOUBLES		*	HUB. AMONT	33	.813	*	1	.774	
2	.814	.814	*			*		34	.812	*	2	.797	
3	.812	.812	*	59	.809	.810	*	1	.806	35	.811	* 3	.872
4	.806	.808	*	50	.809	.807	*	2	.804	36	.811	* 4	.950
5	.805	.809	*	61	.804	.800	*	3	.803	37	.810	* 5	.944
6	.811	.813	*				*	4	.804	38	.810	* 6	.885
7	.809	.811	*	PRISES LAT. GAUCHES		*	5	.802	39	.810	* 7	.804	
8	.807	.804	*				*	6	.802	40	.812	* 8	.795
9	.806	.806	*	62	.809	.809	*	7	.802	41	.814	* 9	.424
10	.810	.802	*	63	.800	.812	*	8	.800	42	.812	* 10	1.359
11	.806	.805	*	64	.813	.807	*	9	.802	43	.809	* 11	1.332
12	.801	.805	*	65	.809	.807	*	10	.802	44	.808	* 12	1.233
13	.803	.805	*	66	.815	.806	*	11	.802	45	.807	* 13	1.019
14	.805	.809	*	67	.820	.809	*					* 14	1.012
15	.807	.808	*	68	.822	.809	*	HUB. AVAL	HUB. DROIT	15	1.806		
16	.808	.802	*	69	.825	.811	*			16	.895		
17	.809	.801	*	70	.824	.809	*	1	.808	1	.808	* 17	.895
18	.811	.803	*	71	.814	.804	*	2	.808	2	.808	* 18	1.001
19	.808	.804	*	72	.810	.807	*	3	.807	3	.808	* 19	.998
20	.807	.808	*	73	.797	.815	*	4	.810	4	.808	* 20	1.000
21	.807	.807	*				*	5	.807	5	.808	* 21	.981
22	.814	.804	*	PRISES LAT. DROITES		*	6	.807	6	.808	* 22	.957	
23	.819	.801	*				*	7	.807	7	.808	* 23	.944
24	.820	.805	*	74	.810	.814	*	8	.808	8	.808	* 24	.749
25	.821	.809	*	75	.810	.811	*	9	.809	9	.808	* 25	.779
26	.821	.809	*	76	.807	.803	*	10	.806	10	.808	* 26	.860
27	.826	.807	*	77	.804	.805	*	11	.806	11	.808	* 27	.957
28	.826	.810	*	78	.807	.798	*			12	.808	* 28	.947
29	.832	.811	*	79	.806	.799	*	HUB. GAUCHE	13	.808	* 29	.891	
30	.827	.811	*	80	.814	.805	*		14	.808	* 30	.843	
31	.835	.807	*	81	.827	.802	*	1	.823	15	.808	* 31	.826
32	.831	.813	*	82	.824	.807	*	2	.823	16	.808	* 32	.410
33	.837	.813	*	83	.824	.807	*	3	.822	17	.808	* 33	1.523
34	.832	.809	*	84	.844	.810	*	4	.812	18	.808	* 34	1.454
35	.836	.809	*	85	.846	.814	*	5	.813	19	.808	* 35	1.380
36	.834	.810	*	86	.843	.813	*	6	.817	20	.808	* 36	1.266
37	.836	.808	*	87	.842	.810	*	7	.822	21	.808	* 37	1.005
38	.833	.809	*	88	.839	.808	*	8	.825	22	.808	* 38	1.029
39	.835	.809	*	89	.838	.807	*	9	.827	23	.808	* 39	1.050
40	.839	.808	*	90	.825	.808	*	10	.823	24	.808	* 40	1.029
41	.837	.808	*	91	.817	.807	*	11	.821	25	.808	* 41	1.008
42	.828	.807	*	92	.817	.804	*	12	.820	26	.808	* 42	1.000
43	.822	.807	*	93	.807	.805	*	13	.819	27	.808	* 43	.887
44	.816	.806	*	94	.810	.804	*	14	.818	28	.808	* 44	.959
45	.815	.804	*	95	.805	.796	*	15	.812	29	.808	* 45	.927
46	.813	.805	*	96	.795	.793	*	16	.810	30	.808	* 46	.921
47	.816	.803	*				*	17	.810	31	.808	* 47	.912
48	.816	.806	*				*	18	.811	32	.808	* 48	.840
49	.815	.806	*				*	19	.811	33	.808	* 49	.900
50	.810	.806	*				*	20	.812	34	.808	* 50	.830
51	.810	.805	*				*	21	.813	35	.808	*	
52	.806	.801	*	PRISES COL		*	22	.815	36	.808	*		
53	.809	.807	*				*	23	.813	37	.808	*	
54	.810	.810	*	.859	1.217	*	24	.818	38	.808	*		
55	.810	.807	*	.873	1.189	*	25	.820	39	.808	*		
56	.805	.803	*	.942	.895	*	26	.823	40	.808	*		
57	.801	.799	*	.985	.823	*	27	.827	41	.808	*		
58	.793	.797	*	1.144	.792	*	28	.829	42	.808	*		
			*			*	29	.824	43	.808	*		
			*			*	30	.816	44	.808	*		
			*			*	31	.812	45	.808	*		
			*			*	32	.814			*		

***** FICHER AD135 N0(1T)= 4
 22/ 8/85 9H30 AS07 M=.7 I=0 R 2-5 ADAPTE 2D AD135
 DE AD134 4'ITE

MACH DE REFERENCE= .7021 UINF= 231.108 M/S
 TIV=297.2 K PIV= 1521 MB

MACH PARDIS HAUTE ET BASSE						MACH PARDIS LAT.				FILE AS07		
I	HAUT	BAS	I	HAUT	BAS	I	MACH	I	MACH	I	MACH	
1	.703	.700	*	PRISES DOUBLES		*	HUB. AMONT	33	.704	*	1	.672
2	.704	.704	*			*		34	.703	*	2	.639
3	.703	.702	*	59	.700	.701	*	35	.702	*	3	.742
4	.700	.702	*	60	.703	.700	*	36	.703	*	4	.600
5	.699	.703	*	61	.702	.701	*	37	.702	*	5	.797
6	.702	.704	*				*	38	.702	*	6	.752
7	.701	.702	*	PRISES LAT. GAUCHES		*		39	.702	*	7	.707
8	.702	.700	*				*	40	.703	*	8	.691
9	.702	.702	*	62	.701	.703	*	41	.704	*	9	.696
10	.704	.697	*	63	.701	.704	*	42	.704	*	10	1.033
11	.702	.697	*	64	.704	.705	*	43	.702	*	11	1.054
12	.699	.698	*	65	.706	.701	*	44	.701	*	12	.935
13	.701	.698	*	66	.703	.696	*	45	.700	*	13	.897
14	.701	.700	*	67	.713	.702	*			*	14	.870
15	.701	.702	*	68	.710	.701	*	HUB. AVAIL	HUB. DROIT	*	15	.858
16	.701	.702	*	69	.710	.702	*			*	16	.845
17	.701	.702	*	70	.715	.702	*	1	.704	1	.702	.842
18	.704	.699	*	71	.707	.700	*	2	.703	2	.702	.843
19	.704	.698	*	72	.703	.702	*	3	.703	3	.702	.838
20	.707	.700	*	73	.695	.705	*	4	.704	4	.702	.835
21	.706	.701	*				*	5	.702	5	.702	.822
22	.707	.701	*	PRISES LAT. DROITES		*		6	.703	6	.702	.813
23	.707	.700	*				*	7	.702	7	.702	.803
24	.706	.699	*	74	.702	.704	*	8	.703	8	.702	.657
25	.708	.699	*	75	.701	.703	*	9	.704	9	.702	.690
26	.708	.699	*	76	.702	.697	*	10	.702	10	.702	.738
27	.714	.699	*	77	.701	.697	*	11	.702	11	.702	.795
28	.716	.703	*	78	.699	.698	*				.702	.792
29	.721	.704	*	79	.703	.695	*	HUB. GAUCHE			.702	.759
30	.718	.704	*	80	.712	.699	*				.702	.725
31	.722	.701	*	81	.712	.701	*	1	.711	15	.701	.707
32	.717	.704	*	82	.711	.698	*	2	.711	16	.702	.698
33	.719	.704	*	83	.719	.698	*	3	.710	17	.702	1.195
34	.714	.701	*	84	.723	.701	*	4	.704	18	.702	1.075
35	.715	.701	*	85	.723	.704	*	5	.705	19	.702	.922
36	.714	.701	*	86	.723	.703	*	6	.707	20	.702	.894
37	.717	.700	*	87	.720	.702	*	7	.710	21	.702	.886
38	.717	.700	*	88	.719	.700	*	8	.712	22	.702	.979
39	.721	.700	*	89	.725	.699	*	9	.713	23	.702	.869
40	.718	.700	*	90	.718	.701	*	10	.711	24	.702	.856
41	.718	.700	*	91	.708	.703	*	11	.710	25	.701	.844
42	.718	.700	*	92	.709	.701	*	12	.709	26	.701	.838
43	.713	.701	*	93	.702	.699	*	13	.708	27	.701	.829
44	.708	.702	*	94	.704	.700	*	14	.708	28	.701	.812
45	.706	.701	*	95	.701	.698	*	15	.704	29	.701	.799
46	.705	.702	*	96	.699	.695	*	16	.703	30	.701	.790
47	.709	.700	*				*	17	.704	31	.701	.781
48	.709	.701	*				*	18	.704	32	.702	.743
49	.708	.700	*				*	19	.704	33	.702	.777
50	.705	.700	*				*	20	.704	34	.702	.729
51	.704	.701	*				*	21	.705	35	.702	
52	.704	.701	*	PRISES COL		*		22	.705	36	.702	
53	.704	.702	*				*	23	.704	37	.702	
54	.703	.700	*	.753	1.148	*		24	.707	38	.702	
55	.703	.699	*	.739	1.098	*		25	.708	39	.702	
56	.700	.697	*	.869	.863	*		26	.710	40	.702	
57	.697	.696	*	.926	.767	*		27	.712	41	.702	
58	.692	.697	*	1.092	.711	*		28	.714	42	.702	
			*			*		29	.711	43	.702	
			*			*		30	.707	44	.702	
			*			*		31	.706	45	.702	
			*			*		32	.705			

***** FICHER AD136 NO(IT)= 4
 22/ 3/85 9H55 AS07 M=.6 I=0 R 2-5 ADAPTE 2D AD136
 DE AD135 4'ITE

MACH DE REFERENCE= .5972 UINF= 231.108 M/S
 TIV=295.8 K PIV= 1393 MB

MACH PAROIS HAUTE ET BASSE						MACH PAROIS LATER.				AILE AS07	
I	HAUT	BAS	I	HAUT	BAS	I	MACH	I	MACH	I	MACH
1	.598	.596	PRISES DOUBLES			HUB. AMONT	33	.598	1	.589	
2	.598	.599					34	.598	2	.583	
3	.599	.598	59	.597	.597	1	.596	35	.597	3	.589
4	.598	.598	60	.598	.597	2	.596	36	.598	4	.590
5	.598	.598	61	.596	.596	3	.596	37	.597	5	.573
6	.599	.599	PRISES LAT. GAUCHES			4	.596	38	.595	6	.542
7	.597	.597				5	.595	39	.595	7	.591
8	.597	.596				6	.595	40	.595	8	.584
9	.598	.597	62	.598	.598	7	.595	41	.597	9	.593
10	.598	.594	63	.598	.598	8	.594	42	.597	10	.581
11	.597	.596	64	.599	.597	9	.595	43	.596	11	.585
12	.596	.596	65	.599	.596	10	.595	44	.595	12	.583
13	.597	.596	66	.600	.595	11	.595	45	.595	13	.738
14	.596	.596	67	.602	.598	HUB. AVAL		HUB. DROIT		14	.7124
15	.596	.596	68	.602	.598					15	.715
16	.596	.594	69	.602	.598	1	.598	1	.588	16	.705
17	.597	.595	70	.605	.595	2	.598	2	.598	17	.701
18	.599	.595	71	.600	.595	3	.597	3	.598	18	.701
19	.598	.596	72	.597	.596	4	.598	4	.598	19	.696
20	.599	.597	73	.594	.598	5	.597	5	.598	20	.693
21	.600	.597	PRISES LAT. DROITES			6	.597	6	.598	21	.693
22	.602	.594				7	.597	7	.598	22	.680
23	.603	.593				8	.598	8	.598	23	.671
24	.602	.595	74	.599	.599	9	.598	9	.598	24	.659
25	.603	.596	75	.597	.597	10	.598	10	.598	25	.678
26	.602	.596	76	.597	.594	11	.596	11	.598	26	.670
27	.605	.596	77	.596	.594	12	.598	12	.598	27	.670
28	.605	.598	78	.596	.592	HUB. GAUCHE				28	.664
29	.608	.598	79	.597	.592	13	.598	13	.598	29	.695
30	.606	.598	80	.604	.595	14	.597	14	.597	30	.510
31	.608	.596	81	.606	.593	1	.603	15	.597	31	.595
32	.606	.599	82	.605	.594	2	.602	16	.597	32	.610
33	.607	.599	83	.609	.596	3	.602	17	.597	33	.719
34	.605	.597	84	.612	.598	4	.599	18	.597	34	.719
35	.606	.597	85	.613	.599	5	.599	19	.597	35	.719
36	.606	.598	86	.610	.598	6	.600	20	.597	36	.719
37	.607	.596	87	.609	.598	7	.602	21	.597	37	.719
38	.606	.596	88	.609	.596	8	.604	22	.597	38	.719
39	.610	.595	89	.614	.595	9	.604	23	.597	39	.719
40	.608	.595	90	.608	.595	10	.604	24	.597	40	.711
41	.608	.595	91	.604	.595	11	.602	25	.597	41	.703
42	.609	.595	92	.602	.595	12	.602	26	.597	42	.698
43	.607	.596	93	.607	.595	13	.601	27	.597	43	.692
44	.604	.596	94	.608	.598	14	.600	28	.598	44	.698
45	.603	.596	95	.605	.595	15	.598	29	.600	45	.669
46	.602	.597	96	.603	.593	16	.598	30	.597	46	.666
47	.602	.596				17	.597	31	.597	47	.668
48	.601	.596				18	.597	32	.598	48	.668
49	.600	.595				19	.597	33	.598	49	.697
50	.598	.595				20	.598	34	.598	50	.624
51	.598	.595				21	.598	35	.596		
52	.597	.596	PRISES COL			22	.599	36	.598		
53	.597	.596				23	.597	37	.598		
54	.597	.595				24	.600	38	.597		
55	.597	.594				25	.601	39	.597		
56	.596	.594				26	.602	40	.597		
57	.595	.594				27	.604	41	.597		
58	.597	.593	1.014	.632		28	.605	42	.597		
						29	.603	43	.597		
						30	.601	44	.597		
						31	.600	45	.597		
						32	.598				

***** FICHER AD138 NOCIT= 1
 22/ 3/85 10H45 AS07 M=6 I=0(-30'+ROT.30') R 2-5 ADAPTE 3D AD138
 DE AD9137 L'ITE

MACH DE REFERENCE= .5985 UINF= 231.108 M/S
 TIV=300.6 K PIV= 1392 MB

MACH PAROIS HAUTE ET BASSE						MACH PAROIS LATER.				FILE AS07		
I	HAUT	BAS	I	HAUT	BAS	I	MACH	I	MACH	I	MACH	
1	.606	.591	*	PRISES DOUBLES		HUB. AMONT	33	.601	*	1	.570	
2	.605	.595	*				34	.601	*	2	.581	
3	.601	.595	*	59	.597	.599	1	.600	35	.601	* 3	.623
4	.597	.597	*	60	.600	.600	2	.599	36	.601	* 4	.631
5	.596	.599	*	61	.601	.599	3	.598	37	.601	* 5	.630
6	.597	.601	*				4	.598	38	.601	* 6	.651
7	.597	.599	*	PRISES LAT. GAUCHES		5	.598	39	.600	* 7	.611	
8	.598	.599	*				6	.598	40	.601	* 8	.599
9	.599	.601	*	62	.598	.596	7	.598	41	.601	* 9	.600
10	.600	.597	*	63	.600	.602	8	.597	42	.601	* 10	.652
11	.598	.597	*	64	.602	.603	9	.598	43	.600	* 11	.622
12	.597	.597	*	65	.600	.599	10	.598	44	.600	* 12	.754
13	.599	.597	*	66	.602	.601	11	.599	45	.598	* 13	.732
14	.600	.599	*	67	.604	.601					* 14	.720
15	.600	.599	*	68	.603	.601	HUB. AVAL	HUB. DROIT			* 15	.712
16	.600	.599	*	69	.604	.602					* 16	.703
17	.599	.600	*	70	.606	.599	1	.602	1	.599	* 17	.699
18	.599	.600	*	71	.601	.601	2	.602	2	.599	* 18	.698
19	.599	.600	*	72	.602	.599	3	.602	3	.598	* 19	.693
20	.602	.602	*	73	.591	.604	4	.602	4	.598	* 20	.692
21	.601	.600	*				5	.601	5	.598	* 21	.682
22	.602	.597	*	PRISES LAT. DROITES		6	.601	6	.599	* 22	.680	
23	.602	.596	*				7	.602	7	.599	* 23	.672
24	.603	.600	*	74	.600	.598	8	.604	8	.599	* 24	.651
25	.606	.603	*	75	.597	.599	9	.604	9	.599	* 25	.681
26	.605	.602	*	76	.598	.597	10	.602	10	.600	* 26	.627
27	.607	.602	*	77	.598	.596	11	.601	11	.599	* 27	.613
28	.607	.602	*	78	.598	.598					* 28	.672
29	.608	.601	*	79	.598	.597	HUB. GAUCHE	13	.599	* 29	.649	
30	.606	.601	*	80	.605	.598					* 30	.626
31	.609	.598	*	81	.605	.596	1	.605	13	.598	* 31	.617
32	.607	.602	*	82	.607	.601	2	.605	15	.598	* 32	.603
33	.608	.602	*	83	.610	.602	3	.604	17	.598	* 33	.699
34	.606	.601	*	84	.613	.601	4	.601	18	.598	* 34	.717
35	.607	.601	*	85	.614	.602	5	.601	19	.598	* 35	.740
36	.606	.601	*	86	.611	.603	6	.603	20	.599	* 36	.730
37	.607	.600	*	87	.610	.602	7	.605	21	.599	* 37	.724
38	.607	.600	*	88	.610	.601	8	.606	22	.599	* 38	.721
39	.610	.600	*	89	.614	.599	9	.607	23	.600	* 39	.716
40	.609	.600	*	90	.609	.599	10	.606	24	.599	* 40	.707
41	.609	.599	*	91	.604	.598	11	.604	25	.599	* 41	.699
42	.609	.599	*	92	.603	.600	12	.605	26	.599	* 42	.695
43	.607	.598	*	93	.600	.600	13	.604	27	.598	* 43	.690
44	.604	.598	*	94	.603	.598	14	.604	28	.598	* 44	.680
45	.603	.598	*	95	.598	.603	15	.602	29	.599	* 45	.687
46	.602	.599	*	96	.589	.601	16	.601	30	.599	* 46	.686
47	.604	.601	*				17	.601	31	.599	* 47	.660
48	.604	.602	*				18	.601	32	.599	* 48	.649
49	.604	.601	*				19	.601	33	.599	* 49	.660
50	.602	.600	*				20	.602	34	.599	* 50	.627
51	.602	.599	*				21	.602	35	.599		
52	.600	.598	*	PRISES COL		22	.593	36	.599			
53	.601	.601	*				23	.601	37	.598		
54	.600	.602	*	.656	1.064		24	.604	38	.599		
55	.600	.602	*	.632	.987		25	.604	39	.598		
56	.597	.602	*	.602	.795		26	.605	40	.598		
57	.594	.603	*	.668	.692		27	.607	41	.598		
58	.589	.605	*	1.028	.632		28	.608	42	.598		
			*				29	.606	43	.598		
			*				30	.604	44	.598		
			*				31	.604	45	.598		
			*				32	.602				

***** FICHER AD139 N0(1T)= 1
 22/ 8/85 11H 0 AS07 M=3 I=0(-30'+ROT.30') R 2-5 NON ADAPTE AD139
 DE AD445 1'ITE PAROIS RECTILIGNES + 30'

MACH DE REFERENCE= .8043 UINF= 231.108 M/S
 TIV=301.2 K PIV= 1651 MB

MACH PAROIS HAUTE ET BASSE						MACH PAROIS LATÉR.				AILE A30-	
I	HAUT	BAS	I	HAUT	BAS	I	MACH	I	MACH	I	MACH
1	.817	.792	PRISES DOUBLES			HUB. AMONT	33	.834		1	.750
2	.816	.798					34	.833		2	.816
3	.809	.800	59	.799	.805	1	.805	35	.832	3	.809
4	.802	.804	60	.807	.806	2	.805	36	.825	4	.802
5	.798	.808	61	.812	.815	3	.805	37	.827	5	.798
6	.800	.809				4	.805	38	.830	6	.800
7	.800	.805	PRISES LAT. GAUCHES			5	.803	39	.831	7	.800
8	.805	.803				6	.804	40	.833	8	.805
9	.807	.807	62	.804	.803	7	.805	41	.835	9	.807
10	.809	.800	63	.799	.809	8	.807	42	.832	10	.809
11	.805	.802	64	.813	.813	9	.805	43	.830	11	.805
12	.802	.804	65	.819	.818	10	.804	44	.829	12	.802
13	.804	.804	66	.835	.817	11	.806	45	.827	13	.804
14	.803	.807	67	.851	.832					14	.803
15	.804	.809	68	.855	.831	HUB. AVAL		HUB. DROIT		15	.804
16	.805	.808	69	.859	.832	1	.817	1	.804	16	.805
17	.808	.808	70	.854	.827	2	.817	2	.805	17	.808
18	.814	.807	71	.832	.821	3	.818	3	.805	18	.814
19	.815	.808	72	.820	.823	4	.823	4	.805	19	.815
20	.816	.815	73	.776	.827	5	.820	5	.804	20	.816
21	.813	.813				6	.819	6	.804	21	.813
22	.826	.819	PRISES LAT. DROITES			7	.817	7	.804	22	.826
23	.833	.815				8	.818	8	.805	23	.833
24	.836	.817	74	.806	.805	9	.821	9	.805	24	.836
25	.841	.820	75	.800	.806	10	.820	10	.805	25	.841
26	.844	.821	76	.806	.802	11	.820	11	.805	26	.844
27	.852	.822	77	.804	.803					27	.852
28	.855	.830	78	.806	.804	HUB. GAUCHE				28	.855
29	.865	.834	79	.812	.801	13	.804	13	.804	29	.865
30	.862	.835	80	.826	.815	14	.804	14	.804	30	.862
31	.872	.831	81	.840	.816	1	.854	15	.805	31	.872
32	.867	.837	82	.842	.817	2	.852	16	.805	32	.867
33	.872	.837	83	.860	.823	3	.851	17	.805	33	.872
34	.866	.830	84	.873	.834	4	.829	18	.804	34	.866
35	.871	.831	85	.883	.839	5	.833	19	.804	35	.871
36	.869	.830	86	.879	.838	6	.841	20	.804	36	.869
37	.870	.828	87	.875	.833	7	.849	21	.804	37	.870
38	.865	.826	88	.872	.828	8	.856	22	.804	38	.865
39	.866	.825	89	.869	.825	9	.856	23	.804	39	.866
40	.860	.825	90	.853	.825	10	.847	24	.805	40	.860
41	.857	.825	91	.841	.823	11	.847	25	.804	41	.857
42	.857	.825	92	.834	.823	12	.845	26	.805	42	.857
43	.848	.823	93	.819	.819	13	.843	27	.805	43	.848
44	.839	.823	94	.819	.818	14	.841	28	.804	44	.839
45	.837	.821	95	.809	.839	15	.825	29	.804	45	.837
46	.834	.822	96	.775	.836	16	.829	30	.804	46	.834
47	.833	.821				17	.828	31	.804	47	.833
48	.830	.823				18	.828	32	.804	48	.830
49	.825	.821				19	.829	33	.804	49	.825
50	.820	.821				20	.831	34	.804	50	.820
51	.819	.820				21	.834	35	.804		
52	.815	.816	PRISES COL			22	.836	36	.804		
53	.814	.819				23	.835	37	.804		
54	.813	.821	.869	1.221		24	.842	38	.804		
55	.810	.822	.868	.878		25	.845	39	.804		
56	.801	.823	.849	.881		26	.843	40	.805		
57	.786	.835	.882	.819		27	.853	41	.804		
58	.761	.852	1.150	.779		28	.854	42	.805		
						29	.846	43	.804		
						30	.836	44	.804		
						31	.831	45	.804		
						32	.836				

***** FICHER ADI40 N0(17)= 1
 22/ 8/85 11H15 AS07 M=.8 I=0(-30'ROT.30') R 2-5 ADAPTE 3D 1'ITE. ADI40
 DE AD9139 1'ITE

MACH DE REFERENCE= .8039 UINF= 231.109 M/S
 TIV=300.8 K PIV= 1649 MB

MACH PAROIS HAUTE ET BASSE				MACH PAROIS LAT.ER.				MACH PAROIS LAT.ER.				MACH PAROIS LAT.ER.					
I	HAUT	BAS	I	HAUT	BAS	I	HUB. AMONT	I	MACH	I	MACH	I	MACH	I	MACH	I	MACH
1	.817	.792	+	PRISES	DOUBLES	+	HUB. AMONT	33	.809	+	.809	+	.809	+	.809	+	.809
2	.815	.793	+	59	.801	.805	*	34	.809	+	.809	+	.809	+	.809	+	.809
3	.810	.800	+	50	.807	.805	*	35	.808	+	.808	+	.808	+	.808	+	.808
4	.802	.804	+	51	.804	.793	*	36	.802	+	.802	+	.802	+	.802	+	.802
5	.799	.807	+	+	+	+	*	37	.807	+	.807	+	.807	+	.807	+	.807
6	.802	.809	+	+	+	+	*	38	.804	+	.804	+	.804	+	.804	+	.804
7	.801	.805	+	PRISES	LAT. GAUCHES*	+	5	.802	.807	+	.807	+	.807	+	.807	+	.807
8	.804	.802	+	63	.805	.802	*	6	.801	.810	+	.810	+	.810	+	.810	
9	.806	.806	+	53	.797	.808	*	7	.801	.811	+	.811	+	.811	+	.811	
10	.808	.801	+	53	.809	.808	*	8	.800	.802	+	.802	+	.802	+	.802	
11	.803	.803	+	54	.809	.809	*	9	.801	.800	+	.800	+	.800	+	.800	
12	.800	.804	+	55	.806	.807	*	10	.801	.802	+	.802	+	.802	+	.802	
13	.804	.804	+	55	.802	.802	*	11	.803	.805	+	.805	+	.805	+	.805	
14	.804	.806	+	57	.814	.807	*	+	+	+	+	+	+	+	+	+	+
15	.807	.806	+	58	.810	.809	*	HUB. AVAL	HUB. DROIT	+	+	+	+	+	+	+	+
16	.807	.803	+	59	.813	.812	*	1	.805	+	.804	+	.804	+	.804	+	.804
17	.806	.804	+	70	.819	.805	*	2	.805	+	.804	+	.804	+	.804	+	.804
18	.804	.805	+	71	.806	.803	*	3	.804	+	.804	+	.804	+	.804	+	.804
19	.802	.805	+	72	.808	.802	*	4	.805	+	.804	+	.804	+	.804	+	.804
20	.804	.808	+	73	.797	.805	*	5	.805	+	.804	+	.804	+	.804	+	.804
21	.805	.807	+	+	+	+	*	6	.805	+	.804	+	.804	+	.804	+	.804
22	.809	.805	+	PRISES	LAT. DROITES*	+	7	.805	.804	+	.804	+	.804	+	.804	+	.804
23	.810	.803	+	74	.807	.805	*	8	.804	+	.804	+	.804	+	.804	+	.804
24	.808	.803	+	75	.801	.805	*	9	.805	+	.804	+	.804	+	.804	+	.804
25	.807	.806	+	76	.805	.802	*	10	.805	+	.804	+	.804	+	.804	+	.804
26	.808	.805	+	77	.804	.802	*	11	.801	+	.804	+	.804	+	.804	+	.804
27	.814	.804	+	78	.802	.800	*	+	+	+	+	+	+	+	+	+	+
28	.816	.808	+	79	.801	.800	*	HUB. GAUCHE	HUB. DROIT	+	+	+	+	+	+	+	+
29	.822	.810	+	80	.813	.805	*	1	.814	+	.804	+	.804	+	.804	+	.804
30	.819	.810	+	81	.817	.804	*	2	.813	+	.804	+	.804	+	.804	+	.804
31	.824	.807	+	82	.809	.804	*	3	.813	+	.804	+	.804	+	.804	+	.804
32	.819	.812	+	83	.820	.806	*	4	.813	+	.804	+	.804	+	.804	+	.804
33	.822	.815	+	84	.833	.811	*	5	.815	+	.804	+	.804	+	.804	+	.804
34	.817	.810	+	85	.833	.815	*	6	.815	+	.804	+	.804	+	.804	+	.804
35	.819	.812	+	86	.828	.816	*	7	.816	+	.804	+	.804	+	.804	+	.804
36	.813	.812	+	87	.824	.814	*	8	.813	+	.804	+	.804	+	.804	+	.804
37	.822	.811	+	88	.824	.811	*	9	.813	+	.804	+	.804	+	.804	+	.804
38	.821	.810	+	89	.821	.807	*	10	.813	+	.804	+	.804	+	.804	+	.804
39	.827	.809	+	90	.821	.805	*	11	.813	+	.804	+	.804	+	.804	+	.804
40	.824	.807	+	91	.809	.801	*	12	.813	+	.804	+	.804	+	.804	+	.804
41	.823	.806	+	92	.809	.804	*	13	.812	+	.804	+	.804	+	.804	+	.804
42	.823	.805	+	93	.802	.804	*	14	.811	+	.804	+	.804	+	.804	+	.804
43	.816	.802	+	94	.803	.800	*	15	.809	+	.804	+	.804	+	.804	+	.804
44	.808	.801	+	95	.803	.815	*	16	.807	+	.804	+	.804	+	.804	+	.804
45	.805	.799	+	96	.794	.812	*	17	.806	+	.804	+	.804	+	.804	+	.804
46	.804	.801	+	+	+	+	*	18	.807	+	.804	+	.804	+	.804	+	.804
47	.808	.802	+	+	+	+	*	19	.807	+	.804	+	.804	+	.804	+	.804
48	.810	.806	+	+	+	+	*	20	.807	+	.804	+	.804	+	.804	+	.804
49	.810	.807	+	+	+	+	*	21	.809	+	.804	+	.804	+	.804	+	.804
50	.809	.805	+	+	+	+	*	22	.809	+	.804	+	.804	+	.804	+	.804
51	.807	.794	+	+	+	+	*	23	.810	+	.804	+	.804	+	.804	+	.804
52	.807	.797	+	+	+	+	*	24	.809	+	.804	+	.804	+	.804	+	.804
53	.807	.800	+	.853	1.215	+	*	25	.809	+	.804	+	.804	+	.804	+	.804
54	.806	.802	+	.855	1.125	+	*	26	.815	+	.803	+	.803	+	.803	+	.803
55	.806	.805	+	.838	.835	+	*	27	.813	+	.803	+	.803	+	.803	+	.803
56	.803	.805	+	.830	.823	+	*	28	.824	+	.804	+	.804	+	.804	+	.804
57	.812	.812	+	1.143	.790	+	*	29	.819	+	.804	+	.804	+	.804	+	.804
58	.796	.824	+	+	+	+	*	30	.811	+	.804	+	.804	+	.804	+	.804
			+				*	31	.806	+	.803	+	.803	+	.803	+	.803
			+				*	32	.810	+	.803	+	.803	+	.803	+	.803

***** FICHER ADI41 NO(ITE)= 1
 22/ 8/85 11H35 A307 M=3 I=0(-30)+ROT.30) R 2-5 ADAPTE 3D 2'ITE. ADI41
 DE AD9140 1'ITE

MACH DE REFERENCE= .3043 UINF= 231.108 M/S
 TIV=299.3 K. PIV= 1551 MB

MACH PAROIS HAUTE ET BASSE				MACH PAROIS LAT.ER.				MILE 450					
I	HAUT	BAS		I	HAUT	BAS		I	MACH	I	MACH	I	MACH
1	.315	.792	* PRISES DOUBLES	* HUB. AMONT	33	.309		* HUB. DROIT	1	.304			
2	.316	.793	* 59	.303	.305		34	.308	2	.305			
3	.309	.800	* 60	.305	.305		35	.308	3	.308			
4	.301	.802	* 61	.300	.300		36	.307	4	.307			
5	.799	.807	* PRISES LAT. GAUCHES*	5	.302		37	.307	5	.307			
6	.303	.810	* 63	.304	.301		38	.307	6	.307			
7	.306	.802	* 64	.797	.310		39	.307	7	.307			
8	.307	.805	* 65	.812	.309		40	.812	8	.308			
9	.307	.801	* 66	.304	.304		41	.307	9	.308			
10	.301	.804	* 67	.808	.305		42	.306	10	.306			
11	.777	.805	* 68	.815	.306		43	.304	11	.304			
12	.799	.807	* 69	.817	.310		44	.304	12	.304			
13	.301	.803	* 70	.821	.307		45	.304	13	.304			
14	.304	.802	* 71	.809	.302		14	.304	14	.304			
15	.304	.803	* 72	.808	.303		15	.305	15	.305			
16	.305	.803	* 73	.792	.310		16	.305	16	.305			
17	.307	.803	* PRISES LAT. DROITES*	74	.305		17	.305	17	.305			
18	.309	.802	* 74	.306	.305		18	.305	18	.305			
19	.307	.803	* 75	.304	.305		19	.305	19	.305			
20	.304	.803	* 76	.304	.302		20	.304	20	.304			
21	.303	.803	* 77	.300	.304		21	.304	21	.304			
22	.306	.803	* 78	.304	.300		22	.304	22	.304			
23	.309	.802	* 79	.305	.795		23	.304	23	.304			
24	.311	.805	* 80	.310	.302		24	.304	24	.304			
25	.312	.805	* 81	.317	.302		25	.305	25	.305			
26	.314	.808	* 82	.314	.305		26	.305	26	.305			
27	.311	.808	* 83	.327	.307		27	.305	27	.305			
28	.313	.809	* 84	.340	.310		28	.304	28	.304			
29	.315	.809	* 85	.340	.314		29	.304	29	.304			
30	.315	.807	* 86	.340	.317		30	.304	30	.304			
31	.321	.805	* 87	.329	.310		31	.305	31	.305			
32	.325	.812	* 88	.327	.305		32	.305	32	.305			
33	.321	.807	* 89	.322	.304		33	.305	33	.305			
34	.319	.807	* 90	.324	.306		34	.304	34	.304			
35	.325	.805	* 91	.315	.305		35	.304	35	.304			
36	.323	.805	* 92	.311	.305		36	.304	36	.304			
37	.325	.807	* 93	.307	.303		37	.304	37	.304			
38	.324	.807	* 94	.300	.317		38	.304	38	.304			
39	.325	.805	* 95	.790	.315		39	.304	39	.304			
40	.325	.804	* PRISES COL				40	.304	40	.304			
41	.325	.804	* 858	1.213			41	.304	41	.304			
42	.325	.805	* 859	1.165			42	.304	42	.304			
43	.321	.804	* 860	.940			43	.304	43	.304			
44	.321	.804	* 861	.935			44	.304	44	.304			
45	.321	.804	* 862	1.145			45	.304	45	.304			
46	.320	.803	* 863				46	.304	46	.304			
47	.320	.803	* 864				47	.304	47	.304			
48	.320	.803	* 865				48	.304	48	.304			
49	.320	.803	* 866				49	.304	49	.304			
50	.320	.803	* 867				50	.304	50	.304			
51	.320	.803	* 868				51	.304	51	.304			
52	.320	.803	* 869				52	.304	52	.304			
53	.320	.803	* 870				53	.304	53	.304			
54	.320	.803	* 871				54	.304	54	.304			
55	.320	.803	* 872				55	.304	55	.304			
56	.320	.803	* 873				56	.304	56	.304			
57	.320	.803	* 874				57	.304	57	.304			
58	.320	.803	* 875				58	.304	58	.304			

***** FICHER AD142 M80ITD= 1
 22/ 8.35 14H25 AS07 M=6 I=-2 R 2.5 NON ADAPTE AD142
 DE AD4 VITE. PAROIS RECTILIGNES SYMETRIQUES

MACH DE REFERENCE= .5976 UINF= 231.109 M/S
 TIV=02.5 K PIV= 1.990 MB

MACH PAROIS HAUTE ET BASSE		MACH PAROIS LAT. HUB. AVAL		MACH PAROIS LAT. HUB. DROIT		MACH PAROIS LAT. HUB. GAUCHE		MACH PAROIS LAT. HUB. DROIT									
I	HAUT	BAS	I	HAUT	BAS	I	HAUT	BAS	I	HAUT	BAS	I	HAUT	BAS	I	HAUT	BAS
1	.597	.596	*			*			*			*			*		
2	.597	.599	*			*			*			*			*		
3	.597	.597	*	59	.597	.597	*		*			*			*		
4	.595	.596	*	60	.597	.598	*	1	.597	.598	*	1	.597	.598	*		
5	.595	.597	*	61	.600	.597	*	3	.598	.595	*	3	.598	.595	*		
6	.597	.599	*	*			*	4	.598	.596	*	4	.598	.596	*		
7	.598	.596	*				*	5	.597	.597	*	5	.597	.597	*		
8	.598	.598	*	62	.597	.598	*	7	.597	.597	*	7	.597	.597	*		
9	.598	.595	*	63	.599	.601	*	8	.597	.597	*	8	.597	.597	*		
10	.596	.597	*	64	.601	.600	*	9	.597	.597	*	9	.597	.597	*		
11	.594	.597	*	65	.602	.601	*	10	.597	.597	*	10	.597	.597	*		
12	.595	.597	*	66	.604	.604	*	11	.597	.597	*	11	.597	.597	*		
13	.595	.599	*	*			*	11	.599	.605	*	11	.599	.604	*		
14	.596	.599	*				*	12	.609	.605	*	12	.609	.605	*		
15	.597	.599	*	67	.609	.605	*	13	.609	.605	*	13	.609	.605	*		
16	.598	.598	*	68	.610	.607	*	14	.609	.605	*	14	.609	.605	*		
17	.598	.598	*	69	.612	.605	*	15	.609	.605	*	15	.609	.605	*		
18	.601	.598	*	70	.603	.602	*				*				*		
19	.600	.598	*	71	.603	.602	*				*				*		
20	.602	.602	*	72	.602	.602	*				*				*		
21	.601	.601	*	*			*				*				*		
22	.604	.599	*				*				*				*		
23	.605	.599	*				*				*				*		
24	.605	.603	*	74	.597	.599	*	1	.601	.601	*	1	.601	.601	*		
25	.606	.607	*	75	.599	.598	*	2	.601	.602	*	2	.601	.602	*		
26	.606	.606	*	76	.597	.596	*	3	.602	.602	*	3	.602	.602	*		
27	.608	.608	*	77	.595	.597	*	4	.603	.603	*	4	.603	.603	*		
28	.609	.608	*	78	.597	.596	*	5	.602	.602	*	5	.602	.602	*		
29	.612	.609	*	79	.599	.599	*	6	.601	.601	*	6	.601	.601	*		
30	.611	.608	*	80	.605	.602	*	7	.601	.601	*	7	.601	.601	*		
31	.611	.608	*	81	.609	.602	*	8	.609	.609	*	8	.609	.609	*		
32	.611	.608	*	82	.607	.609	*	9	.609	.609	*	9	.609	.609	*		
33	.613	.609	*	83	.610	.610	*	10	.609	.609	*	10	.609	.609	*		
34	.611	.609	*	84	.615	.610	*	11	.609	.609	*	11	.609	.609	*		
35	.613	.607	*	85	.617	.610	*	12	.607	.607	*	12	.607	.607	*		
36	.614	.608	*	86	.615	.610	*	13	.607	.607	*	13	.607	.607	*		
37	.614	.607	*	87	.615	.609	*	14	.609	.609	*	14	.609	.609	*		
38	.616	.607	*	88	.615	.608	*	15	.609	.609	*	15	.609	.609	*		
39	.614	.607	*	89	.615	.608	*	16	.609	.609	*	16	.609	.609	*		
40	.614	.606	*	90	.615	.607	*	17	.609	.609	*	17	.609	.609	*		
41	.613	.606	*	91	.615	.607	*	18	.609	.609	*	18	.609	.609	*		
42	.614	.605	*	92	.615	.607	*	19	.609	.609	*	19	.609	.609	*		
43	.614	.605	*	93	.615	.607	*	20	.609	.609	*	20	.609	.609	*		
44	.614	.605	*	94	.615	.607	*	21	.609	.609	*	21	.609	.609	*		
45	.615	.605	*	95	.615	.607	*	22	.609	.609	*	22	.609	.609	*		
46	.615	.605	*	96	.615	.607	*	23	.609	.609	*	23	.609	.609	*		
47	.615	.605	*	97	.615	.607	*	24	.609	.609	*	24	.609	.609	*		
48	.615	.605	*	98	.615	.607	*	25	.609	.609	*	25	.609	.609	*		
49	.615	.605	*	99	.615	.607	*	26	.609	.609	*	26	.609	.609	*		
50	.615	.605	*	100	.615	.607	*	27	.609	.609	*	27	.609	.609	*		
51	.615	.605	*				*	28	.609	.609	*	28	.609	.609	*		
52	.615	.605	*				*	29	.609	.609	*	29	.609	.609	*		
53	.615	.605	*				*	30	.609	.609	*	30	.609	.609	*		
54	.615	.605	*				*	31	.609	.609	*	31	.609	.609	*		
55	.615	.605	*				*	32	.609	.609	*	32	.609	.609	*		
56	.615	.605	*				*	33	.609	.609	*	33	.609	.609	*		
57	.615	.605	*				*	34	.609	.609	*	34	.609	.609	*		
58	.615	.605	*				*	35	.609	.609	*	35	.609	.609	*		
59	.615	.605	*				*	36	.609	.609	*	36	.609	.609	*		

***** FICHER AD143 NO(IT)= 1
 22/ 8/85 14H40 AS07 M=.6 I=-2 R 2-5 ADAPTE 3D AD143
 DE AD9142 1'ITE.

MACH DE REFERENCE= .5982 UINF= 231.109 M/S
 TIV=301.5 K PIV= 1391 MB

MACH PAROIS HAUTE ET BASSE						MACH PAROIS LATÉR.				AILE AS07	
I	HAUT	BAS	I	HAUT	BAS	I	MACH	I	MACH	I	MACH
1	.599	.597	PRISES DOUBLES			HUB. AMONT	33	.501	1	.575	
2	.599	.599						2	.592		
3	.598	.598	59	.598	.599	1	.597	35	.501	3	.536
4	.596	.598	60	.599	.599	2	.596	36	.501	4	.536
5	.595	.598	61	.602	.600	3	.596	37	.501	5	.536
6	.598	.600				4	.596	38	.501	6	.536
7	.598	.599	PRISES LAT. GAUCHES			5	.596	39	.501	7	.536
8	.599	.599				6	.595	40	.502	8	.536
9	.599	.599	62	.595	.598	7	.595	41	.503	9	.536
10	.599	.596	63	.600	.601	8	.595	42	.502	10	.536
11	.597	.596	64	.601	.601	9	.595	43	.501	11	.536
12	.595	.597	65	.598	.600	10	.595	44	.500	12	.536
13	.596	.597	66	.599	.598	11	.595	45	.500	13	.536
14	.597	.599	67	.605	.602	HUB. AVANT		HUB. DROIT		14	.536
15	.597	.599	68	.602	.601	1	.603	1	.599	15	.536
16	.598	.598	69	.602	.603	2	.602	2	.598	16	.536
17	.599	.599	70	.605	.601	3	.601	3	.598	17	.536
18	.601	.599	71	.602	.599	4	.601	4	.598	18	.536
19	.599	.600	72	.602	.602	5	.600	5	.599	19	.536
20	.599	.601	73	.600	.605	6	.601	6	.599	20	.536
21	.598	.601	PRISES LAT. DROITES			7	.601	7	.599	21	.536
22	.601	.599				8	.601	8	.599	22	.536
23	.600	.597				9	.603	9	.599	23	.536
24	.599	.598	74	.597	.600	10	.600	10	.599	24	.536
25	.600	.601	75	.599	.599	11	.601	11	.599	25	.536
26	.600	.600	76	.599	.595	12	.600	12	.598	26	.536
27	.603	.601	77	.597	.597	13	.599	13	.598	27	.536
28	.605	.603	78	.597	.595	HUB. GAUCHE		14	.599	28	.536
29	.607	.604	79	.598	.597	1	.604	1	.599	29	.536
30	.606	.603	80	.601	.600	2	.602	2	.598	30	.536
31	.607	.601	81	.603	.600	3	.602	3	.598	31	.536
32	.606	.604	82	.600	.602	4	.602	4	.598	32	.536
33	.606	.605	83	.605	.605	5	.602	5	.598	33	.536
34	.604	.603	84	.612	.606	6	.603	6	.599	34	.536
35	.604	.603	85	.613	.606	7	.603	7	.599	35	.536
36	.603	.603	86	.609	.606	8	.601	8	.599	36	.536
37	.605	.602	87	.606	.605	9	.603	9	.598	37	.536
38	.606	.602	88	.607	.603	10	.603	10	.598	38	.536
39	.609	.602	89	.613	.602	11	.604	11	.598	39	.536
40	.607	.602	90	.608	.601	12	.603	12	.598	40	.536
41	.607	.602	91	.601	.600	13	.602	13	.598	41	.536
42	.608	.601	92	.604	.599	14	.603	14	.598	42	.536
43	.604	.599	93	.599	.599	15	.602	15	.598	43	.536
44	.600	.599	94	.602	.601	16	.602	16	.598	44	.536
45	.601	.599	95	.602	.599	17	.601	17	.598	45	.536
46	.601	.600	96	.599	.591	18	.600	18	.598	46	.536
47	.604	.599				19	.600	19	.598	47	.536
48	.603	.601				20	.600	20	.598	48	.536
49	.602	.600				21	.600	21	.598	49	.536
50	.600	.601				22	.600	22	.598	50	.536
51	.602	.601				23	.600	23	.598	51	.536
52	.603	.600	PRISES COL			24	.600	24	.598	52	.536
53	.603	.601				25	.598	25	.598	53	.536
54	.603	.601	.603	1.059		26	.602	26	.598	54	.536
55	.603	.599	.601	.917		27	.603	27	.598	55	.536
56	.602	.597	.799	.796		28	.604	28	.598	56	.536
57	.601	.595	.855	.692		29	.606	29	.598	57	.536
58	.599	.590	1.023	.631		30	.607	30	.598	58	.536
						31	.606	31	.598	59	.536
						32	.604	32	.598	60	.536
							.602				
							.601				

***** FICHER AD144 N0(1T)= 4
 22/ 8/85 15H10 AS07 M=1.6 I=-2 R 2-5 ADAPTE 2D AD144
 DE AD136 1'ITE.

MACH DE REFERENCE= .5964 UINF= 231.100 M/S
 TIV=296.8 K PIV= 1392 MB

MACH PAROIS HAUTE ET BASSE						MACH PAROIS LATER.				AILE AS07	
I	HAUT	SAS	I	HAUT	SAS	I	MACH	I	MACH	I	MACH
1	.598	.595	PRISES DOUBLES			HUB. AMONT	33	.599	1	.575	
2	.599	.599				34	.599	2	.591		
3	.597	.598	59	.596	.597	35	.599	3	.639		
4	.596	.598	60	.597	.597	36	.599	4	.690		
5	.596	.599	61	.596	.595	37	.599	5	.697		
6	.598	.600	PRISES LAT. GAUCHES			38	.599	6	.686		
7	.597	.597				39	.599	7	.667		
8	.597	.596	62	.597	.598	40	.600	8	.681		
9	.597	.597	63	.597	.599	41	.600	9	.617		
10	.598	.594	64	.599	.600	42	.600	10	.737		
11	.597	.595	65	.596	.595	43	.598	11	.736		
12	.595	.596	66	.599	.597	44	.598	12	.718		
13	.595	.595	67	.600	.599	45	.597	13	.699		
14	.596	.597	68	.599	.598	HUB. AVAL HUB. DROIT		14	.687		
15	.599	.597	69	.601	.599	1	.598	15	.682		
16	.595	.596	70	.602	.598	2	.598	16	.676		
17	.596	.597	71	.599	.596	3	.598	17	.675		
18	.599	.595	72	.597	.597	4	.598	18	.678		
19	.597	.595	73	.589	.598	5	.597	19	.677		
20	.597	.596	PRISES LAT. DROITES			6	.597	20	.679		
21	.595	.595				7	.597	21	.675		
22	.599	.598	74	.597	.599	8	.597	22	.675		
23	.599	.598	75	.597	.597	9	.598	23	.670		
24	.599	.599	76	.597	.594	10	.598	24	.667		
25	.599	.599	77	.595	.595	11	.597	25	.678		
26	.599	.599	78	.595	.595	12	.597	26	.694		
27	.599	.599	79	.596	.593	HUB. GAUCHE		27	.686		
28	.599	.599	80	.600	.596	1	.600	28	.688		
29	.599	.599	81	.603	.598	14	.597	29	.688		
30	.599	.599	82	.602	.601	15	.597	30	.683		
31	.599	.599	83	.604	.601	16	.597	31	.683		
32	.599	.599	84	.606	.602	17	.597	32	.682		
33	.599	.599	85	.607	.604	18	.597	33	.685		
34	.599	.599	86	.606	.603	19	.597	34	.685		
35	.599	.599	87	.605	.602	20	.597	35	.685		
36	.599	.599	88	.605	.600	21	.597	36	.685		
37	.599	.599	89	.609	.599	22	.597	37	.685		
38	.599	.599	90	.604	.600	23	.597	38	.685		
39	.599	.599	91	.600	.598	24	.597	39	.685		
40	.599	.599	92	.600	.596	25	.597	40	.685		
41	.599	.599	93	.596	.595	26	.597	41	.685		
42	.599	.599	94	.599	.595	27	.597	42	.685		
43	.599	.599	95	.594	.598	28	.597	43	.685		
44	.599	.599	96	.587	.588	29	.597	44	.685		
45	.599	.599				30	.597	45	.685		
46	.599	.599				31	.597	46	.685		
47	.599	.599				32	.597	47	.685		
48	.599	.599				33	.597	48	.685		
49	.599	.599				34	.597	49	.685		
50	.599	.599				35	.597	50	.685		
51	.599	.599				36	.597				
52	.597	.595	PRISES COL			37	.597				
53	.597	.595				38	.597				
54	.596	.594	.658	1.053		39	.597				
55	.596	.592	.695	.925		40	.597				
56	.593	.592	.794	.801		41	.597				
57	.598	.599	.861	.693		42	.597				
58	.587	.598	1.019	.632		43	.597				
						44	.597				
						45	.597				

***** FICHER AD145 NO(IT)= 4
 22/ 8/85 17H15 AS07 M=.6 I=+2 R 2-5 ADAPTE 2D AD145
 DE AD131 4'ITE.

MACH DE REFERENCE= .5959 UINF= 231.109 M/S
 TIV=297.1 K PIV= 1391 MB

MACH PAROIS HAUTE ET BASSE						MACH PAROIS LATER.				FILE AS07		
I	HAUT	BAS	I	HAUT	BAS	I	MACH	I	MACH	I	MACH	
1	.598	.593	*	PRISES DOUBLES		*	HUB. AMONT	33	.597	*	1	.580
2	.599	.597	**			**		34	.595	**	2	.571
3	.598	.596	**	59	.596	.596	1	.596	.595	**	3	.581
4	.596	.596	**	60	.598	.596	2	.595	.596	**	4	.586
5	.595	.597	**	61	.597	.595	3	.595	.596	**	5	.586
6	.598	.598	**			**	4	.595	.595	**	6	.587
7	.597	.596	**	PRISES LAT. GAUCHES		**	5	.595	.594	**	7	.584
8	.597	.595	**			**	6	.595	.594	**	8	.584
9	.597	.596	**	62	.596	.596	7	.595	.594	**	9	.584
10	.598	.593	**	63	.599	.598	8	.594	.594	**	10	1.093
11	.596	.594	**	64	.599	.597	9	.594	.594	**	11	.836
12	.594	.594	**	65	.599	.594	10	.594	.592	**	12	.839
13	.596	.593	**	66	.592	.593	11	.594	.593	**	13	.736
14	.596	.594	**	67	.593	.595	*			*	14	.733
15	.596	.595	**	68	.593	.594	HUB. AVAL	HUB. DROIT		15	.750	
16	.597	.594	**	69	.595	.595	1	.598	1	.597	15	.736
17	.598	.594	**	70	.596	.593	2	.597	2	.596	17	.728
18	.600	.593	**	71	.599	.592	3	.597	3	.596	18	.724
19	.599	.592	**	72	.598	.596	4	.598	4	.597	19	.718
20	.600	.594	**	73	.599	.599	5	.597	5	.597	20	.709
21	.599	.593	**			**	6	.597	6	.597	21	.696
22	.601	.591	**	PRISES LAT. DROITES		**	7	.598	7	.597	22	.686
23	.603	.589	**			**	8	.598	8	.597	23	.675
24	.604	.591	**	74	.597	.598	9	.599	9	.597	24	.662
25	.608	.592	**	75	.597	.595	10	.598	10	.597	25	.657
26	.606	.592	**	76	.597	.595	11	.597	11	.596	26	.645
27	.609	.591	**	77	.595	.592	*		*		27	.645
28	.608	.593	**	78	.595	.591	HUB. GAUCHE			28	.633	
29	.611	.592	**	79	.598	.598	13	.596	13	.597	29	.620
30	.608	.593	**	80	.596	.599	14	.596	14	.596	30	.609
31	.612	.589	**	81	.599	.593	1	.605	15	.596	31	.469
32	.608	.592	**	82	.612	.599	2	.604	16	.596	32	.349
33	.611	.592	**	83	.614	.599	3	.605	17	.596	33	1.079
34	.608	.591	**	84	.618	.598	4	.608	18	.596	34	1.011
35	.610	.590	**	85	.618	.592	5	.608	19	.596	35	.924
36	.609	.592	**	86	.616	.591	6	.602	20	.596	36	.899
37	.611	.590	**	87	.614	.591	7	.604	21	.596	37	.891
38	.610	.591	**	88	.613	.590	8	.606	22	.597	38	.832
39	.613	.591	**	89	.617	.591	9	.607	23	.597	39	.755
40	.610	.591	**	90	.610	.592	10	.606	24	.597	40	.749
41	.610	.591	**	91	.604	.593	11	.604	25	.597	41	.735
42	.610	.591	**	92	.602	.593	12	.603	26	.596	42	.725
43	.607	.592	**	93	.597	.593	13	.602	27	.596	43	.711
44	.604	.593	**	94	.598	.594	14	.601	28	.597	44	.693
45	.603	.592	**	95	.596	.599	15	.598	29	.597	45	.671
46	.601	.592	**	96	.597	.598	16	.597	30	.597	46	.657
47	.603	.592	**			**	17	.597	31	.597	47	.650
48	.602	.592	**			**	18	.597	32	.597	48	.633
49	.601	.593	**			**	19	.598	33	.597	49	.617
50	.599	.595	**			**	20	.598	34	.597	50	.601
51	.599	.595	**			**	21	.599	35	.597		
52	.599	.594	**	PRISES COL		**	22	.599	36	.596		
53	.599	.595	**			**	23	.598	37	.596		
54	.599	.595	**	.598	1.057	**	24	.601	38	.596		
55	.598	.593	**	.606	.988	**	25	.602	39	.596		
56	.594	.592	**	.726	.793	**	26	.603	40	.596		
57	.591	.591	**	.963	.691	**	27	.605	41	.596		
58	.596	.588	**	1.021	.621	**	28	.606	42	.596		
			**			**	29	.605	43	.596		
			**			**	30	.603	44	.596		
			**			**	31	.601	45	.596		
			**			**	32	.598				

***** FICHER AD146 N0CIT= 4
 23/ 3/85 9H50 AS07 M=6 I=+2 R 1-4 ADAPTE 2D AD146
 DE AD145 4'ITE.

MACH DE REFERENCE= .5936 UINF= 231.109 M/S
 TIV=297.0 K PIV= 1393 MB

MACH PAROIS HAUTE ET BASSE						MACH PAROIS LATÉR.				FILE AS07	
I	HAUT	BAS	I	HAUT	BAS	I	MACH	I	MACH	I	MACH
1	.595	.591	PRISES DOUBLES			HUB. AMONT	33	.594	1	.573	
2	.596	.595					34	.593	2	.573	
3	.595	.593	59	.593	.593	1	.594	35	.592	3	.573
4	.593	.592	60	.596	.594	2	.594	36	.593	4	.573
5	.592	.593	61	.595	.590	3	.593	37	.593	5	.573
6	.594	.594				4	.593	38	.592	6	.573
7	.594	.593	PRISES LAT. GAUCHES			5	.592	39	.592	7	.573
8	.594	.593				6	.592	40	.591	8	.573
9	.594	.594	62	.594	.592	7	.592	41	.592	9	.573
10	.596	.591	63	.597	.596	8	.591	42	.593	10	1.010
11	.595	.591	64	.597	.593	9	.592	43	.591	11	.598
12	.593	.591	65	.596	.593	10	.592	44	.590	12	.799
13	.595	.591	66	.598	.599	11	.592	45	.590	13	.552
14	.594	.592	67	.603	.592					14	.735
15	.594	.592	68	.591	.591	HUB. AVAL	HUB. DROIT	15	.594	15	.723
16	.594	.591	69	.601	.591	1	.596	1	.594	16	.709
17	.595	.591	70	.604	.590	2	.596	2	.594	17	.700
18	.597	.591	71	.600	.592	3	.596	3	.594	18	.697
19	.597	.591	72	.595	.593	4	.596	4	.594	19	.692
20	.598	.593	73	.587	.595	5	.595	5	.594	20	.689
21	.597	.592				6	.595	6	.594	21	.689
22	.599	.591	PRISES LAT. DROITES			7	.595	7	.594	22	.689
23	.601	.589				8	.595	8	.594	23	.689
24	.601	.589	74	.595	.595	9	.597	9	.594	24	.689
25	.604	.603	75	.594	.593	10	.596	10	.594	25	.689
26	.603	.603	76	.595	.591	11	.594	11	.594	26	.689
27	.607	.587	77	.594	.590					27	.689
28	.608	.590	78	.593	.599	HUB. GAUCHE	12	.594	12	.600	
29	.611	.589	79	.597	.588	13	.594	13	.594	29	.600
30	.608	.590	80	.603	.599	14	.594	14	.594	30	.600
31	.611	.586	81	.606	.597	1	.603	15	.594	31	.600
32	.608	.590	82	.608	.595	2	.602	16	.594	32	.600
33	.609	.589	83	.612	.596	3	.602	17	.594	33	1.013
34	.605	.588	84	.617	.597	4	.603	18	.594	34	.603
35	.607	.588	85	.617	.599	5	.603	19	.594	35	.603
36	.605	.588	86	.613	.598	6	.600	20	.594	36	.603
37	.607	.587	87	.610	.599	7	.602	21	.594	37	.603
38	.606	.587	88	.609	.596	8	.604	22	.594	38	.603
39	.609	.587	89	.613	.593	9	.604	23	.594	39	.603
40	.607	.587	90	.608	.599	10	.603	24	.594	40	.603
41	.607	.588	91	.601	.592	11	.602	25	.594	41	.603
42	.607	.588	92	.602	.593	12	.601	26	.594	42	.603
43	.604	.590	93	.595	.591	13	.600	27	.594	43	.603
44	.600	.591	94	.596	.591	14	.600	28	.594	44	.603
45	.600	.591	95	.594	.595	15	.600	29	.594	45	.603
46	.599	.593	96	.595	.593	16	.599	30	.593	46	.603
47	.602	.592				17	.599	31	.593	47	.603
48	.602	.593				18	.599	32	.594	48	.603
49	.599	.593				19	.599	33	.594	49	.603
50	.595	.592				20	.598	34	.594	50	.603
51	.595	.592				21	.598	35	.593	51	.603
52	.596	.593	PRISES COL			22	.597	36	.594	52	.603
53	.596	.593				23	.596	37	.594	53	.603
54	.596	.593	.593	1.048		24	.593	38	.594	54	.603
55	.595	.591	.593	.911		25	.599	39	.594	55	.603
56	.592	.589	.732	.933		26	.601	40	.594	56	.603
57	.589	.586	.659	.889		27	.602	41	.594	57	.603
58	.584	.582	1.015	.928		28	.604	42	.594	58	.603
						29	.602	43	.594		
						30	.600	44	.594		
						31	.599	45	.594		
						32	.595				

***** FICHER AD147 NO(IT)= 1
 23/ 8/ 85 10H25 AS07 M= 6 I=+2(+1.5+ROT.30') R 1-4 NON ADAPTE AD147
 DE AD445 1'ITE PAROIS RECTILIGNES + 30'

MACH DE REFERENCE= .5931 UINF= 231.108 M/S
 TIV=301.2 K PIV= 1393 MB

MACH PAROIS HAUTE ET BASSE						MACH PAROIS LATÉR.				FILE AS07		
I	HAUT	BAS	I	HAUT	BAS	I	MACH	I	MACH	I	MACH	
1	.601	.597	*	PRISES DOUBLES		*	HUB. AMONT	33	.590	*	1	.584
2	.600	.590	*			*		34	.593	*	2	.585
3	.596	.591	*	59	.593	.593	1	.595	.597	*	3	.591
4	.593	.593	*	60	.594	.593	2	.594	.598	*	4	.592
5	.591	.594	*	61	.592	.597	3	.595	.597	*	5	.585
6	.593	.595	*				4	.594	.596	*	6	.593
7	.593	.593	*	PRISES LAT. GAUCHES		*	5	.593	.595	*	7	.593
8	.594	.592	*				6	.593	.595	*	8	.593
9	.594	.594	*	62	.594	.592	7	.594	.595	*	9	.592
10	.594	.590	*	63	.595	.595	8	.594	.594	*	10	1.017
11	.591	.591	*	64	.599	.595	9	.593	.594	*	11	.591
12	.590	.591	*	65	.599	.593	10	.593	.593	*	12	.593
13	.591	.591	*	66	.600	.595	11	.593	.592	*	13	.776
14	.592	.592	*	67	.612	.594				*	14	.751
15	.593	.593	*	68	.614	.594		HUB. AVANT	HUB. DROIT	*	15	.723
16	.594	.593	*	69	.614	.594	1	.597	.593	*	16	.723
17	.596	.593	*	70	.613	.594	2	.597	.594	*	17	.714
18	.599	.594	*	71	.604	.595	3	.597	.594	*	18	.710
19	.599	.594	*	72	.598	.593	4	.598	.594	*	19	.705
20	.590	.594	*	73	.574	.600	5	.600	.594	*	20	.701
21	.601	.593	*				6	.600	.594	*	21	.591
22	.605	.592	*	PRISES LAT. DROITES		*	7	.599	.593	*	22	.593
23	.600	.590	*				8	.599	.593	*	23	.592
24	.609	.593	*	74	.609	.594	9	.599	.593	*	24	.592
25	.613	.593	*	75	.600	.593	10	.600	.593	*	25	.595
26	.612	.593	*	76	.593	.591	11	.599	.593	*	26	.591
27	.616	.591	*	77	.591	.590	12	.599	.593	*	27	.595
28	.617	.592	*	78	.593	.590	13	.599	.594	*	28	.597
29	.620	.590	*	79	.599	.589	14	.599	.594	*	29	.597
30	.619	.591	*	80	.605	.589	15	.599	.594	*	30	.591
31	.623	.593	*	81	.613	.593	16	.613	.594	*	31	.591
32	.619	.591	*	82	.615	.590	17	.611	.594	*	32	.594
33	.621	.590	*	83	.609	.590	18	.611	.593	*	33	1.220
34	.618	.590	*	84	.609	.593	19	.604	.593	*	34	1.000
35	.620	.590	*	85	.608	.593	20	.605	.593	*	35	.593
36	.619	.592	*	86	.609	.593	21	.608	.593	*	36	.590
37	.621	.591	*	87	.624	.592	22	.610	.593	*	37	.591
38	.618	.591	*	88	.629	.590	23	.612	.593	*	38	.593
39	.620	.591	*	89	.624	.590	24	.613	.593	*	39	.591
40	.617	.590	*	90	.617	.590	25	.610	.593	*	40	.591
41	.617	.591	*	91	.619	.595	26	.610	.593	*	41	.591
42	.616	.592	*	92	.605	.595	27	.609	.593	*	42	.593
43	.613	.593	*	93	.599	.595	28	.608	.593	*	43	.594
44	.610	.595	*	94	.597	.595	29	.606	.593	*	44	.593
45	.609	.596	*	95	.599	.601	30	.601	.594	*	45	.592
46	.607	.596	*	96	.573	.599	31	.600	.594	*	46	.590
47	.607	.595	*				32	.599	.594	*	47	.592
48	.605	.595	*				33	.600	.594	*	48	.591
49	.602	.596	*				34	.600	.593	*	49	.599
50	.603	.597	*				35	.601	.594	*	50	.601
51	.597	.597	*				36	.602	.594	*		
52	.593	.597	*				37	.603	.593	*		
53	.592	.590	*	PRISES COL		*	38	.601	.593	*		
54	.590	.590	*				39	.604	.593	*		
55	.587	.590	*	.861	1.060		40	.605	.593	*		
56	.594	.590	*	.592	.990		41	.607	.593	*		
57	.579	.601	*	.797	.791		42	.607	.593	*		
58	.570	.605	*	.865	.689		43	.609	.593	*		
			*	1.022	.629		44	.610	.593	*		
			*				45	.603	.593	*		
			*				46	.606	.593	*		
			*				47	.604	.593	*		
			*				48	.602	.593	*		

***** FICHER AD148 NQ(IT)= 1
 23/ 8/95 10H40 AS07 M=.6 I=+2(1.5+ROT.30') R 1-4 ADAPTE 3D AD148
 DE AD9122 1'ITE.

MACH DE REFERENCE= .5936 UINF= 231.109 M/S
 TIV=300.6 K PIV= 1392 MB

MACH PAROIS HAUTE ET BASSE						MACH PAROIS LATÉR.				FILE AS07	
I	HAUT	BAS	I	HAUT	BAS	I	MACH	I	MACH	I	MACH
1	.500	.586	PRISES DOUBLES			HUB. AMONT	33	.595	1	.582	
2	.599	.589				34	.595	2	.590		
3	.595	.590	59	.592	.592	1	.594	35	.594		
4	.592	.593	60	.595	.594	2	.593	36	.595		
5	.591	.594	61	.590	.592	3	.594	37	.595		
6	.593	.595				4	.594	38	.595		
7	.593	.592	PRISES LAT. GAUCHES			5	.593	39	.594		
8	.595	.592				6	.593	40	.594		
9	.596	.594	62	.593	.592	7	.593	41	.595		
10	.596	.591	63	.595	.595	8	.593	42	.595		
11	.594	.594	64	.597	.597	9	.593	43	.594		
12	.592	.595	65	.595	.594	10	.593	44	.594		
13	.593	.594	66	.595	.596	11	.594	45	.593		
14	.593	.595	67	.592	.593						
15	.593	.594	68	.590	.595	HUB. AVAL		HUB. DROIT			
16	.594	.593	69	.591	.593	1	.599	1	.594		
17	.595	.594	70	.595	.592	2	.599	2	.594		
18	.597	.595	71	.599	.595	3	.599	3	.595		
19	.596	.594	72	.590	.595	4	.598	4	.595		
20	.596	.594	73	.593	.597	5	.598	5	.595		
21	.596	.593				6	.598	6	.594		
22	.599	.592	PRISES LAT. DROITES			7	.599	7	.594		
23	.600	.592				8	.600	8	.594		
24	.599	.595	74	.594	.593	9	.599	9	.594		
25	.600	.595	75	.592	.592	10	.599	10	.594		
26	.599	.594	76	.594	.591	11	.597	11	.594		
27	.603	.591	77	.592	.592						
28	.604	.592	78	.594	.592	HUB. GAUCHE	13	.593			
29	.608	.591	79	.596	.590	14	.593	14	.593		
30	.607	.592	80	.601	.590	15	.593	15	.593		
31	.610	.589	81	.605	.591	16	.602	16	.593		
32	.607	.593	82	.602	.592	17	.602	17	.593		
33	.608	.593	83	.608	.591	18	.602	18	.593		
34	.604	.594	84	.615	.590	19	.592	19	.594		
35	.606	.594	85	.615	.591	20	.597	20	.593		
36	.605	.596	86	.611	.592	21	.594	21	.594		
37	.607	.595	87	.609	.595	22	.602	22	.594		
38	.607	.594	88	.609	.594	23	.604	23	.594		
39	.610	.593	89	.614	.592	24	.603	24	.594		
40	.608	.592	90	.608	.592	25	.604	25	.594		
41	.609	.592	91	.601	.591	26	.602	26	.594		
42	.609	.592	92	.600	.594	27	.601	27	.594		
43	.605	.591	93	.596	.596	28	.601	28	.594		
44	.601	.592	94	.600	.593	29	.600	29	.594		
45	.599	.591	95	.598	.596	30	.597	30	.594		
46	.598	.593	96	.591	.595	31	.595	31	.594		
47	.600	.594				32	.595	32	.593		
48	.600	.596				33	.595	33	.593		
49	.600	.596				34	.595	34	.593		
50	.599	.596				35	.597	35	.593		
51	.600	.594				36	.598	36	.593		
52	.600	.592	PRISES COL			37	.599	37	.593		
53	.601	.594				38	.597	38	.593		
54	.600	.596	.659	1.059		39	.601	39	.593		
55	.600	.596	.631	.707		40	.601	40	.593		
56	.598	.596	.797	.746		41	.603	41	.593		
57	.595	.597	.364	.591		42	.604	42	.593		
58	.592	.599	1.021	.830		43	.605	43	.593		
						44	.604	44	.593		
						45	.600	45	.593		

***** FICHER ADI49 MACHIT= 4
 23/8/85 11H10 AS07 M=6 I=0 R 1-4 ADAPTE 2D ADI49
 DE ADI36 4 ITE.

MACH DE REFERENCE= .5936 UINF= 231.108 M/S
 TIV=295.8 K PIV= 1394 MB

MACH PAROIS HAUTE ET BASSE		MACH PAROIS LATER.		ALLE AS07		
I	HAUT	BAS	I	MACH	I	MACH
1	.595	.592	33	.595	1	.593
2	.595	.595	34	.594	2	.591
3	.594	.594	35	.594	3	.591
4	.592	.594	36	.593	4	.596
5	.594	.594	37	.594	5	.591
6	.594	.596	38	.593	6	.592
7	.594	.593	39	.592	7	.595
8	.595	.592	40	.594	8	.595
9	.595	.593	41	.594	9	.597
10	.595	.590	42	.594	10	.597
11	.592	.592	43	.594	11	.594
12	.590	.592	44	.592	12	.595
13	.592	.591	45	.594	13	.595
14	.592	.593			14	.593
15	.594	.593			15	.595
16	.595	.592			16	.595
17	.594	.593			17	.597
18	.594	.591			18	.597
19	.594	.590			19	.594
20	.595	.592			20	.595
21	.595	.592			21	.593
22	.597	.591			22	.594
23	.598	.590			23	.594
24	.599	.590			24	.590
25	.601	.592			25	.597
26	.600	.592			26	.597
27	.602	.592			27	.597
28	.602	.594			28	.597
29	.604	.594			29	.597
30	.606	.594			30	.597
31	.603	.595			31	.597
32	.605	.595			32	.597
33	.602	.593			33	.595
34	.604	.594			34	.595
35	.604	.592			35	.595
36	.603	.594			36	.595
37	.603	.593			37	.595
38	.603	.592			38	.595
39	.603	.592			39	.595
40	.603	.591			40	.595
41	.603	.591			41	.595
42	.603	.591			42	.595
43	.602	.592			43	.595
44	.602	.592			44	.595
45	.602	.592			45	.595
46	.602	.592			46	.595
47	.603	.592			47	.595
48	.603	.592			48	.595
49	.603	.592			49	.595
50	.603	.592			50	.595
51	.603	.592			51	.595
52	.603	.592			52	.595
53	.603	.592			53	.595
54	.603	.592			54	.595
55	.603	.592			55	.595
56	.603	.592			56	.595
57	.603	.592			57	.595
58	.603	.592			58	.595
59	.603	.592			59	.595
60	.603	.592			60	.595
61	.603	.592			61	.595
62	.603	.592			62	.595

***** FICHER AD150 NOCIT>= 1
 33/ 3/85 11H25 AS07 M.F.6 I=0 R 1-4 NON ADAPTE AD150
 DE AD4 L'ITE. PAROIS RECTILIGNES SYMETRIQUES

MACH DE REFERENCE .5247 UNF= 231.108 M/S
 TIV=300.1 K PIV= 1321 MB

MACH PAROIS HAUTE ET BASSE		MACH PAROIS LAT. HUB. DROIT		MACH PAROIS LAT. HUB. GAUCHE		MACH PAROIS LAT. HUB. DROIT	
I	HAUT	BAS	I	HAUT	BAS	I	HAUT
1	.535	.534	33	.594	.593	33	.594
2	.535	.537	34	.594	.596	34	.594
3	.535	.536	35	.594	.597	35	.594
4	.533	.535	36	.594	.597	36	.594
5	.532	.535	37	.594	.596	37	.594
6	.532	.537	38	.594	.597	38	.594
7	.535	.536	39	.594	.597	39	.594
8	.535	.534	40	.594	.596	40	.594
9	.535	.535	41	.594	.596	41	.594
10	.535	.532	42	.593	.593	42	.593
11	.533	.533	43	.593	.593	43	.593
12	.531	.533	44	.593	.593	44	.593
13	.531	.534	45	.593	.593	45	.593
14	.533	.535					
15	.534	.536					
16	.535	.534					
17	.535	.534					
18	.538	.534					
19	.537	.534					
20	.539	.535					
21	.500	.535					
22	.503	.536					
23	.503	.537					
24	.505	.533					
25	.505	.533					
26	.510	.534					
27	.513	.533					
28	.517	.533					
29	.516	.533					
30	.520	.535					
31	.517	.535					
32	.514	.535					
33	.515	.535					
34	.514	.535					
35	.515	.535					
36	.515	.535					
37	.517	.535					
38	.514	.535					
39	.515	.535					
40	.518	.537					
41	.518	.537					
42	.511	.538					
43	.508	.537					
44	.508	.537					
45	.506	.535					
46	.504	.535					
47	.504	.535					
48	.502	.535					
49	.502	.535					
50	.500	.535					
51	.500	.535					
52	.500	.535					
53	.500	.535					
54	.500	.535					
55	.501	.535					
56	.501	.535					
57	.500	.535					
58	.500	.535					
59	.500	.535					
60	.500	.535					
61	.500	.535					
62	.500	.535					
63	.500	.535					
64	.500	.535					
65	.500	.535					
66	.500	.535					
67	.500	.535					
68	.500	.535					
69	.500	.535					
70	.500	.535					
71	.500	.535					
72	.500	.535					
73	.500	.535					
74	.500	.535					
75	.500	.535					
76	.500	.535					
77	.500	.535					
78	.500	.535					
79	.500	.535					
80	.500	.535					
81	.500	.535					
82	.500	.535					
83	.500	.535					
84	.500	.535					
85	.500	.535					
86	.500	.535					
87	.500	.535					
88	.500	.535					
89	.500	.535					
90	.500	.535					
91	.500	.535					
92	.500	.535					
93	.500	.535					
94	.500	.535					
95	.500	.535					
96	.500	.535					
97	.500	.535					
98	.500	.535					
99	.500	.535					
100	.500	.535					

***** FICHER AD151 NO(IT)= 1
 23/ 3/85 11H40 AS07 M=6 I=0 R 1-4 ADAPTE 3D AD151
 DE AD9107 1'ITE.

MACH DE REFERENCE= .5943 UINF= 231.108 M/S
 TIV=300.0 K PIV= 1391 MB

MACH PAROIS HAUTE ET BASSE						MACH PAROIS LATÉR.				AILE AS07		
I	HAUT	BAS	I	HAUT	BAS	I	MACH	I	MACH	I	MACH	
1	.595	.594	PRISES DOUBLES			HUB. AMONT	33	.597	1	.581		
2	.595	.597					34	.596	2	.592		
3	.594	.595	59	.594	.595	1	.594	35	.596	3	.584	
4	.593	.594	60	.594	.594	2	.594	36	.596	4	.585	
5	.593	.595	61	.599	.594	3	.594	37	.596	5	.585	
6	.595	.596					4	.595	38	.596	6	.579
7	.594	.595	PRISES LAT. GAUCHES				5	.594	39	.596	7	.574
8	.595	.593					6	.594	40	.596	8	.567
9	.594	.594	62	.593	.595	7	.593	41	.597	9	.580	
10	.595	.592	63	.596	.597	8	.593	42	.597	10	.583	
11	.592	.592	64	.598	.599	9	.593	43	.596	11	.583	
12	.590	.593	65	.595	.595	10	.594	44	.595	12	.573	
13	.592	.593	66	.595	.594	11	.595	45	.595	13	.577	
14	.592	.595	67	.599	.596	HUB. AVAL		HUB. DROIT		14	.584	
15	.593	.595	68	.600	.597					15	.583	
16	.594	.595	69	.601	.598	1	.600	1	.594	16	.577	
17	.595	.595	70	.603	.595	2	.599	2	.594	17	.575	
18	.597	.594	71	.607	.595	3	.599	3	.595	18	.572	
19	.596	.593	72	.608	.596	4	.599	4	.595	19	.573	
20	.596	.595	73	.606	.599	5	.598	5	.595	20	.568	
21	.595	.595	PRISES LAT. DROITES				6	.598	6	.595	21	.567
22	.594	.594					7	.598	7	.595	22	.569
23	.599	.594	74	.594	.597	8	.600	8	.594	23	.569	
24	.597	.595	75	.596	.599	9	.598	9	.594	24	.569	
25	.597	.595	76	.594	.599	10	.597	10	.594	25	.561	
26	.597	.595	77	.592	.599	11	.596	11	.595	26	.563	
27	.600	.595	78	.595	.599	HUB. GAUCHE				27	.569	
28	.602	.597	79	.595	.599					28	.561	
29	.604	.597	80	.600	.599	1	.600	13	.594	29	.563	
30	.603	.597	81	.603	.594	2	.600	14	.594	30	.561	
31	.603	.597	82	.600	.599	3	.600	15	.594	31	.563	
32	.605	.597	83	.604	.599	4	.599	16	.594	32	.561	
33	.603	.596	84	.609	.599	5	.597	17	.594	33	.563	
34	.603	.595	85	.609	.599	6	.597	18	.594	34	.563	
35	.605	.595	86	.611	.599	7	.597	19	.594	35	.564	
36	.604	.597	86	.609	.599	8	.598	20	.594	36	.564	
37	.606	.596	87	.609	.599	9	.599	21	.594	37	.565	
38	.605	.597	88	.609	.599	10	.601	22	.594	38	.561	
39	.608	.596	89	.611	.599	11	.602	23	.594	39	.563	
40	.605	.595	90	.606	.599	12	.601	24	.594	40	.567	
41	.604	.595	91	.601	.599	13	.600	25	.594	41	.561	
42	.605	.594	92	.609	.599	14	.600	26	.594	42	.563	
43	.603	.593	93	.597	.599	15	.600	27	.594	43	.563	
44	.600	.593	94	.601	.599	16	.599	28	.595	44	.566	
45	.600	.593	95	.609	.599	17	.597	29	.595	45	.566	
46	.600	.594	96	.604	.599	18	.596	30	.595	46	.566	
47	.600	.595					19	.596	31	.595	47	.566
48	.600	.595					20	.596	32	.595	48	.566
49	.600	.595					21	.596	33	.595	49	.566
50	.600	.594					22	.596	34	.595	50	.566
51	.600	.595					23	.596	35	.595		
52	.600	.594	PRISES COL				24	.597	36	.595		
53	.601	.596					25	.596	37	.595		
54	.601	.596	.587	1.048		26	.599	38	.595			
55	.600	.599	.590	.919		27	.600	39	.595			
56	.603	.599	.595	.866		28	.600	40	.595			
57	.607	.604	.601	.808		29	.602	41	.594			
58	.604	.605	1.018	.809		30	.603	42	.595			
						31	.602	43	.595			
						32	.599	44	.594			
						33	.598	45	.595			

***** FICHER AD152 NOCIT)= 4
 23/ 8/85 11H55 AS07 M=.8 I=0 R 1-4 ADAPTE 2D AD152
 DE AD134 4'ITE.

MACH DE REFERENCE= .8022 UINF= 231.108 M/S
 TIV=295.3 K PIV= 1552 MB

MACH PAROIS HAUTE ET BASSE			MACH PAROIS LAT. HAUTE ET BASSE			MACH PAROIS LAT. BASSE			AILE AS07			
I	HAUT	BAS	I	HAUT	BAS	I	MACH	I	MACH	I	MACH	
1	.804	.800	PRISES DOUBLES			HUB. AMONT			32	.807	1	.784
2	.804	.806							34	.805	2	.808
3	.803	.802	59	.803	.802	1	.797	35	.805	3	.871	
4	.799	.801	60	.805	.803	2	.796	36	.804	4	.944	
5	.800	.802	61	.799	.796	3	.796	37	.804	5	.903	
6	.804	.805							38	.804	6	.829
7	.803	.802	PRISES LAT. GAUCHES						39	.804	7	.752
8	.805	.801							40	.805	8	.741
9	.805	.804	62	.801	.801	4	.798	41	.808	9	.834	
10	.806	.798	63	.796	.807	5	.796	42	.807	10	1.271	
11	.801	.799	64	.806	.804	6	.796	43	.803	11	1.213	
12	.796	.799	65	.803	.801	7	.796	44	.802	12	1.078	
13	.793	.799	66	.810	.800	8	.796	45	.801	13	1.010	
14	.797	.801	67	.814	.804	HUB. AVANT			HUB. DROIT			
15	.799	.802	68	.816	.802	1	.802	1	.802	14	.976	
16	.799	.799	69	.820	.805	2	.802	2	.802	15	.969	
17	.802	.798	70	.813	.804	3	.801	3	.802	16	.958	
18	.806	.797	71	.808	.799	4	.804	4	.802	17	.951	
19	.804	.798	72	.805	.802	5	.802	5	.802	18	.956	
20	.802	.802	73	.800	.807	6	.801	6	.802	19	.955	
21	.801	.801	PRISES LAT. DROITES						7	.801	20	.954
22	.808	.797							8	.801	21	.952
23	.813	.796	74	.802	.805	9	.803	9	.802	22	.944	
24	.814	.799	75	.804	.803	10	.800	10	.802	23	.921	
25	.815	.803	76	.803	.799	11	.800	11	.802	24	.754	
26	.815	.803	77	.798	.798	HUB. GAUCHE						
27	.820	.801	78	.799	.795	1	.815	12	.802	25	.783	
28	.820	.804	79	.799	.792	2	.815	13	.802	26	.859	
29	.825	.805	80	.802	.799	3	.815	14	.802	27	.854	
30	.821	.804	81	.809	.799	4	.806	15	.802	28	.919	
31	.823	.800	82	.821	.797	5	.807	16	.802	29	.879	
32	.823	.805	83	.818	.801	6	.811	17	.802	30	.825	
33	.823	.805	84	.829	.801	7	.815	18	.802	31	.821	
34	.824	.801	85	.837	.804	8	.820	19	.802	32	.817	
35	.828	.802	86	.839	.807	9	.821	20	.802	33	1.421	
36	.827	.803	87	.836	.807	10	.817	21	.802	34	1.379	
37	.830	.801	88	.835	.805	11	.815	22	.802	35	1.315	
38	.826	.802	89	.833	.802	12	.814	23	.802	36	1.014	
39	.828	.801	90	.832	.800	13	.813	24	.802	37	1.328	
40	.823	.801	91	.821	.802	14	.812	25	.802	38	1.037	
41	.821	.801	92	.811	.804	15	.806	26	.802	39	1.070	
42	.821	.802	93	.812	.799	16	.805	27	.802	40	1.059	
43	.816	.802	94	.802	.798	17	.804	28	.802	41	1.019	
44	.810	.803	95	.804	.799	18	.805	29	.802	42	1.018	
45	.809	.801							30	.802	43	1.003
46	.807	.801							31	.802	44	.961
47	.812	.798							32	.802	45	.951
48	.810	.799							33	.802	46	.928
49	.809	.799							34	.802	47	.903
50	.805	.800							35	.802	48	.845
51	.804	.801							36	.802	49	.805
52	.802	.797	PRISES COL						37	.802	50	.806
53	.801	.800							38	.802		
54	.801	.801	849	1.211		21	.808	39	.802			
55	.802	.800	869	1.186		22	.809	40	.802			
56	.801	.798	886	.899		23	.807	41	.802			
57	.800	.799	881	.823		24	.812	42	.802			
58	.797	.797	1.140	.780		25	.814	43	.802			
						26	.817	44	.802			
						27	.821	45	.802			
						28	.823					
						29	.818					
						30	.811					
						31	.807					
						32	.808					

***** FICHER AD153 NO(IT)= 1
 23/ 8/85 14H40 AS07 M=8 I=0 R 1-4 NON ADAPTE AD153
 DE AD4 1'ITE. PAROIS RECTILIGNES SYMETRIQUES

MACH DE REFERENCE= .8029 UINF= 231.108 M/S
 TIV=302.4 K PIV= 1650 MB

MACH PAROIS HAUTE ET BASSE						MACH PAROIS LATÉR.				AILE AS07	
I	HAUT	BAS	I	HAUT	BAS	I	MACH	I	MACH	I	MACH
1	.802	.801	PRISES DOUBLES			HUB. AMONT		33	.822	1	.811
2	.801	.805						34	.831	2	.833
3	.801	.802	59	.800	.801	1	.803	35	.829	3	.808
4	.800	.803	60	.803	.804	2	.802	36	.822	4	.872
5	.800	.804	61	.813	.811	3	.802	37	.825	5	.837
6	.802	.805				4	.801	38	.825	6	.859
7	.800	.801	PRISES LAT. GAUCHES			5	.801	39	.829	7	.771
8	.804	.802				6	.801	40	.832	8	.762
9	.805	.807	62	.800	.802	7	.801	41	.834	9	.827
10	.804	.799	63	.796	.809	8	.802	42	.830	10	1.277
11	.800	.801	64	.812	.810	9	.801	43	.829	11	1.238
12	.798	.802	65	.819	.814	10	.801	44	.827	12	1.115
13	.800	.803	66	.829	.821	11	.803	45	.825	13	1.043
14	.799	.805	67	.848	.824					14	.896
15	.802	.806	68	.855	.828	HUB. AVAL		HUB. DROIT		15	.894
16	.804	.804	69	.860	.834	1	.817	1	.803	16	.987
17	.805	.803	70	.851	.826	2	.816	2	.803	17	.880
18	.810	.805	71	.828	.819	3	.816	3	.803	18	.892
19	.812	.807	72	.821	.818	4	.820	4	.803	19	.897
20	.817	.813	73	.815	.823	5	.817	5	.804	20	1.012
21	.818	.813				6	.815	6	.804	21	1.011
22	.820	.809	PRISES LAT. DROITES			7	.813	7	.803	22	.893
23	.825	.809				8	.813	8	.803	23	.861
24	.829	.817	74	.801	.805	9	.816	9	.803	24	.779
25	.824	.824	75	.801	.803	10	.814	10	.803	25	.806
26	.838	.823	76	.802	.801	11	.815	11	.803	26	.887
27	.847	.821	77	.801	.802			12	.803	27	.896
28	.842	.825	78	.803	.801	HUB. GAUCHE		13	.803	28	.892
29	.853	.827	79	.819	.802	1	.854	13	.803	29	.809
30	.858	.826	80	.826	.811	2	.851	14	.803	30	.871
31	.871	.823	81	.832	.811	3	.849	15	.803	31	.855
32	.857	.831	82	.838	.822	4	.824	16	.803	32	.821
33	.875	.833	83	.855	.822	5	.820	17	.803	33	1.411
34	.869	.830	84	.876	.825	6	.808	18	.803	34	1.079
35	.875	.831	85	.883	.831	7	.808	19	.803	35	1.341
36	.871	.832	86	.883	.833	8	.847	20	.803	36	1.057
37	.871	.829	87	.881	.833	9	.853	21	.803	37	1.056
38	.866	.829	88	.874	.838	10	.845	22	.803	38	1.064
39	.854	.827	89	.866	.825	11	.846	23	.803	39	1.069
40	.858	.824	90	.859	.824	12	.843	24	.803	40	1.105
41	.853	.823	91	.841	.826	13	.841	25	.803	41	1.108
42	.854	.823	92	.832	.819	14	.839	26	.803	42	1.100
43	.847	.823	93	.819	.816	15	.832	27	.803	43	1.113
44	.840	.824	94	.820	.819	16	.821	28	.803	44	1.016
45	.837	.821	95	.812	.803	17	.821	29	.803	45	.879
46	.833	.822	96	.813	.799	18	.824	30	.803	46	.855
47	.830	.818				19	.824	31	.803	47	.807
48	.826	.818				20	.826	32	.803	48	.860
49	.824	.816				21	.831	33	.803	49	.830
50	.820	.815				22	.834	34	.803	50	.864
51	.819	.813				23	.833	35	.803		
52	.815		PRISES COL			24	.839	36	.803		
53	.817	.815				25	.842	37	.803		
54	.816	.817		.855	1.211	26	.846	38	.804		
55	.816	.813		.866	1.036	27	.851	39	.804		
56	.814	.809		.938	.882	28	.852	40	.804		
57	.815	.805		.982	.816	29	.843	41	.804		
58	.818	.794		1.142	.775	30	.834	42	.804		
						31	.829	43	.804		
						32	.834	44	.804		

***** FICHER AD154 NOKIT= 1
 23/ 8/85 14H50 AS07 M=18 I=0 R 1-4 ADAPTE 3D AD154
 DE ADP113 1'ITE.

MACH DE REFERENCE= .3025 UINF= 231.108 M/S
 TIV=301.5 K PIV= 1652 MB

MACH PAROIS HAUTE ET BASSE						MACH PAROIS LATÉR.				AILE AS07		
I	HAUT	BAS	I	HAUT	BAS	I	MACH	I	MACH	I	MACH	
1	.305	.303	PRISES DOUBLES			HUB. AMONT	33	.307	1	.787		
2	.302	.305					34	.305	2	.311		
3	.301	.304	59	.799	.302	1	.798	35	.305	3	.371	
4	.300	.305	60	.303	.302	2	.797	36	.305	4	.340	
5	.300	.307	61	.304	.799	3	.797	37	.305	5	.314	
6	.301	.305					4	.798	38	.305	6	.345
7	.300	.302	PRISES LAT. GAUCHES				5	.796	39	.305	7	.750
8	.305	.303					6	.796	40	.307	8	.752
9	.303	.303	62	.300	.304	7	.796	41	.309	9	.303	
10	.304	.795	63	.795	.305	8	.795	42	.308	10	1.232	
11	.799	.795	64	.307	.303	9	.797	43	.304	11	1.193	
12	.796	.798	65	.304	.300	10	.797	44	.303	12	1.353	
13	.797	.799	66	.305	.305	11	.799	45	.302	13	.394	
14	.795	.301	67	.314	.303	HUB. AVAL		HUB. DROIT		14	.369	
15	.798	.303	68	.312	.303	1	.305	1	.302	15	.351	
16	.300	.302	69	.314	.303	2	.303	2	.303	16	.350	
17	.302	.302	70	.313	.305	3	.303	3	.303	17	.345	
18	.305	.302	71	.308	.300	4	.305	4	.302	18	.349	
19	.304	.302	72	.305	.304	5	.303	5	.302	19	.350	
20	.304	.302	73	.313	.303	6	.303	6	.302	20	.357	
21	.303	.300	PRISES LAT. DROITES			7	.303	7	.302	21	.351	
22	.305	.798				8	.302	8	.302	22	.344	
23	.307	.303	74	.301	.307	9	.303	9	.302	23	.323	
24	.308	.303	75	.300	.303	10	.304	10	.303	24	.798	
25	.309	.305	76	.301	.793	11	.301	11	.303	25	.360	
26	.310	.303	77	.797	.798	HUB. GAUCHE				26	.347	
27	.315	.303	78	.799	.799	1	.314	12	.302	27	.301	
28	.317	.305	79	.799	.799	2	.314	13	.302	28	.392	
29	.324	.305	80	.301	.795	3	.314	14	.303	29	.345	
30	.319	.304	81	.311	.798	4	.314	15	.303	30	.345	
31	.327	.301	82	.314	.799	5	.314	16	.303	31	.345	
32	.322	.305	83	.312	.305	6	.314	17	.303	32	1.415	
33	.325	.307	84	.323	.305	7	.313	18	.302	33	1.382	
34	.320	.304	85	.305	.305	8	.304	19	.302	34	1.323	
35	.324	.306	86	.307	.309	9	.305	20	.302	35	1.231	
36	.322	.307	87	.302	.309	10	.309	21	.302	36	1.005	
37	.324	.305	88	.300	.309	11	.313	22	.302	37	1.000	
38	.321	.304	89	.307	.305	12	.317	23	.302	38	1.044	
39	.325	.304	90	.329	.303	13	.319	24	.302	39	1.059	
40	.321	.303	91	.319	.305	14	.315	25	.303	40	1.322	
41	.320	.303	92	.312	.306	15	.313	26	.303	41	1.312	
42	.321	.303	93	.311	.300	16	.312	27	.303	42	1.310	
43	.317	.303	94	.301	.301	17	.311	28	.303	43	.393	
44	.311	.303	95	.305	.302	18	.310	29	.303	44	.377	
45	.310	.301	96	.302	.797	19	.305	30	.303	45	.349	
46	.307	.301	97	.313	.734	20	.304	31	.303	46	.329	
47	.311	.799					21	.304	32	.303	47	.301
48	.308	.301					22	.304	33	.303	48	.344
49	.308	.302					23	.304	34	.303	49	.304
50	.305	.304					24	.305	35	.303	50	.305
51	.305	.303	PRISES COL				25	.305	36	.303		
52	.306	.300					26	.307	37	.303		
53	.307	.302					27	.305	38	.303		
54	.306	.302	344	1.207		28	.311	39	.303			
55	.309	.799	357	1.134		29	.314	40	.303			
56	.311	.795	332	.395		30	.317	41	.303			
57	.317	.792	377	.321		31	.321	42	.303			
58	.327	.799	1.135	.799		32	.322	43	.303			
						33	.317	44	.303			
						34	.310	45	.303			
						35	.307					
						36	.309					

***** FICHER AD155 N0(1T)= 4
 23/ 3/85 15H20 AS07 M=6 I=-2 R 1-4 ADAPTE 2D AD155
 DE AD144 4'ITE

MACH DE REFERENCE= .5951 UNF= 231.108 M/S
 TIV=296.6 K PIV= 1394 MB

MACH PAROIS HAUTE ET BASSE						MACH PAROIS LATER.				FILE AS07	
I	HAUT	BAS	I	HAUT	BAS	I	MACH	I	MACH	I	MACH
1	.596	.594	PRISES DOUBLES			HUB.	AMONT	33	.597	1	.598
2	.596	.598						34	.597	2	.598
3	.595	.595	59	.594	.595	1	.594	35	.597	3	.598
4	.593	.594	60	.596	.595	2	.594	36	.597	4	.598
5	.593	.595	61	.594	.594	3	.594	37	.597	5	.598
6	.595	.597	PRISES LAT. GAUCHES			4	.595	38	.597	6	.598
7	.594	.595						39	.597	7	.598
8	.595	.595						40	.598	8	.598
9	.596	.597	62	.594	.595	4	.594	41	.598	9	.598
10	.597	.593	63	.597	.598	5	.593	42	.597	10	.598
11	.595	.593	64	.597	.598	6	.593	43	.597	11	.598
12	.593	.593	65	.594	.594	7	.593	44	.596	12	.598
13	.594	.593	66	.596	.595	8	.594	45	.596	13	.598
14	.594	.595	67	.599	.598	9	.594			14	.598
15	.594	.595	68	.599	.599	10	.593	HUB.	RVAL	HUB.	DROIT
16	.593	.593	69	.598	.598	11	.594	1	.596	1	.598
17	.594	.594	70	.598	.598	12	.596	2	.595	2	.598
18	.597	.595	71	.597	.598	13	.595	3	.595	3	.598
19	.595	.595	72	.596	.598	14	.596	4	.595	4	.598
20	.595	.595	73	.596	.598	15	.596	5	.595	5	.598
21	.593	.595	74			16	.596	6	.595	6	.598
22	.596	.595	PRISES LAT. DROITES			17	.596	7	.595	7	.598
23	.597	.595	75	.595	.595	18	.597	8	.595	8	.598
24	.597	.595	76	.595	.595	19	.597	9	.595	9	.598
25	.597	.596	77	.594	.594	20	.597	10	.595	10	.598
26	.599	.597	78	.593	.593	21	.596	11	.595	11	.598
27	.601	.599	79	.593	.593	22	.596	12	.595	12	.598
28	.602	.600	80	.594	.594	23	.596	13	.595	13	.598
29	.601	.599	81	.599	.598	24	.596	14	.595	14	.598
30	.603	.598	82	.598	.598	25	.599	15	.595	15	.598
31	.601	.600	83	.598	.598	26	.598	16	.595	16	.598
32	.602	.601	84	.591	.591	27	.598	17	.595	17	.598
33	.604	.600	85	.596	.596	28	.598	18	.595	18	.598
34	.601	.601	86	.597	.595	29	.598	19	.595	19	.598
35	.601	.600	87	.595	.595	30	.598	20	.595	20	.598
36	.601	.600	88	.593	.593	31	.598	21	.595	21	.598
37	.601	.600	89	.593	.593	32	.598	22	.595	22	.598
38	.601	.600	90	.593	.593	33	.598	23	.595	23	.598
39	.603	.600	91	.593	.593	34	.598	24	.595	24	.598
40	.601	.600	92	.593	.593	35	.598	25	.595	25	.598
41	.601	.600	93	.594	.594	36	.598	26	.595	26	.598
42	.602	.600	94	.594	.594	37	.598	27	.595	27	.598
43	.600	.600	95	.593	.593	38	.598	28	.595	28	.598
44	.600	.600	96	.593	.593	39	.598	29	.595	29	.598
45	.600	.600	97	.593	.593	40	.598	30	.595	30	.598
46	.600	.600	98	.593	.593	41	.598	31	.595	31	.598
47	.600	.600	99	.593	.593	42	.598	32	.595	32	.598
48	.600	.600	100	.593	.593	43	.598	33	.595	33	.598
49	.600	.600	101	.593	.593	44	.598	34	.595	34	.598
50	.600	.600	102	.593	.593	45	.598	35	.595	35	.598
51	.600	.600	103	.593	.593	46	.598	36	.595	36	.598
52	.600	.600	104	.593	.593	47	.598	37	.595	37	.598
53	.600	.600	105	.593	.593	48	.598	38	.595	38	.598
54	.600	.600	106	.593	.593	49	.598	39	.595	39	.598
55	.600	.600	107	.593	.593	50	.598	40	.595	40	.598
56	.600	.600	108	.593	.593	51	.598	41	.595	41	.598
57	.600	.600	109	.593	.593	52	.598	42	.595	42	.598
58	.600	.600	110	.593	.593	53	.598	43	.595	43	.598
59	.600	.600	111	.593	.593	54	.598	44	.595	44	.598
60	.600	.600	112	.593	.593	55	.598	45	.595	45	.598
61	.600	.600	113	.593	.593	56	.598	46	.595	46	.598
62	.600	.600	114	.593	.593	57	.598	47	.595	47	.598
63	.600	.600	115	.593	.593	58	.598	48	.595	48	.598
64	.600	.600	116	.593	.593	59	.598	49	.595	49	.598
65	.600	.600	117	.593	.593	60	.598	50	.595	50	.598
66	.600	.600	118	.593	.593	61	.598	51	.595	51	.598
67	.600	.600	119	.593	.593	62	.598	52	.595	52	.598
68	.600	.600	120	.593	.593	63	.598	53	.595	53	.598
69	.600	.600	121	.593	.593	64	.598	54	.595	54	.598
70	.600	.600	122	.593	.593	65	.598	55	.595	55	.598
71	.600	.600	123	.593	.593	66	.598	56	.595	56	.598
72	.600	.600	124	.593	.593	67	.598	57	.595	57	.598
73	.600	.600	125	.593	.593	68	.598	58	.595	58	.598
74	.600	.600	126	.593	.593	69	.598	59	.595	59	.598
75	.600	.600	127	.593	.593	70	.598	60	.595	60	.598
76	.600	.600	128	.593	.593	71	.598	61	.595	61	.598
77	.600	.600	129	.593	.593	72	.598	62	.595	62	.598
78	.600	.600	130	.593	.593	73	.598	63	.595	63	.598
79	.600	.600	131	.593	.593	74	.598	64	.595	64	.598
80	.600	.600	132	.593	.593	75	.598	65	.595	65	.598
81	.600	.600	133	.593	.593	76	.598	66	.595	66	.598
82	.600	.600	134	.593	.593	77	.598	67	.595	67	.598
83	.600	.600	135	.593	.593	78	.598	68	.595	68	.598
84	.600	.600	136	.593	.593	79	.598	69	.595	69	.598
85	.600	.600	137	.593	.593	80	.598	70	.595	70	.598
86	.600	.600	138	.593	.593	81	.598	71	.595	71	.598
87	.600	.600	139	.593	.593	82	.598	72	.595	72	.598
88	.600	.600	140	.593	.593	83	.598	73	.595	73	.598
89	.600	.600	141	.593	.593	84	.598	74	.595	74	.598
90	.600	.600	142	.593	.593	85	.598	75	.595	75	.598
91	.600	.600	143	.593	.593	86	.598	76	.595	76	.598
92	.600	.600	144	.593	.593	87	.598	77	.595	77	.598
93	.600	.600	145	.593	.593	88	.598	78	.595	78	.598
94	.600	.600	146	.593	.593	89	.598	79	.595	79	.598
95	.600	.600	147	.593	.593	90	.598	80	.595	80	.598
96	.600	.600	148	.593	.593	91	.598	81	.595	81	.598
97	.600	.600	149	.593	.593	92	.598	82	.595	82	.598
98	.600	.600	150	.593	.593	93	.598	83	.595	83	.598
99	.600	.600	151	.593	.593	94	.598	84	.595	84	.598
100	.600	.600	152	.593	.593	95	.598	85	.595	85	.598
101	.600	.600	153	.593	.593	96	.598	86	.595	86	.598
102	.600	.600	154	.593	.593	97	.598	87	.595	87	.598
103	.600	.600	155	.593	.593	98	.598	88	.595	88	.598
104	.600	.600	156	.593	.593	99	.598	89	.595	89	.598
105	.600	.600	157	.593	.593	100	.598	90	.595	90	.598
106	.600	.600	158	.593	.593	101	.598	91	.595	91	.598
107	.600	.600	159	.593	.593	102	.598	92	.595	92	.598
108	.600	.600	160	.593	.593	103	.598	93	.595	93	.598
109	.600	.600	161	.593	.593	104	.598	94	.595	94	.598
110	.600	.600	162	.593	.5						

***** FICHER AD156 NOKIT= 1
 23/ 8-85 15H40 AS07 M=5 I=-3 R 1-4 NON ADAPTE AD156
 DE AD4 1'ITE. PAROIS RECTILIGNES SYMETRIQUES

 MACH DE REFERENCE= .5950 UINF= 231.109 M/S
 TIV=301.1 K PIV= 1395 MB

MACH PAROIS HAUTE ET BASSE						MACH PAROIS LATER.				FILE AS07	
I	HAUT	BAS	I	HAUT	BAS	I	MACH	I	MACH	I	MACH
1	.596	.595	PRISES DOUBLES			HUB. AMONT	33	.604		1	.594
2	.596	.598					34	.604		2	.597
3	.596	.595	59	.596	.596	1	.596	35	.604	3	.592
4	.594	.595	60	.597	.598	2	.598	36	.602	4	.593
5	.594	.596	61	.599	.598	3	.596	37	.603	5	.597
6	.596	.598				4	.596	38	.603	6	.594
7	.596	.596	PRISES LAT. GAUCHES			5	.595	39	.604	7	.591
8	.597	.595				6	.595	40	.605	8	.595
9	.597	.598	62	.594	.595	7	.595	41	.605	9	.596
10	.597	.595	63	.597	.599	8	.596	42	.605	10	.591
11	.595	.596	64	.599	.599	9	.595	43	.604	11	.591
12	.593	.596	65	.600	.599	10	.596	44	.603	12	.595
13	.594	.595	66	.603	.601	11	.596	45	.603	13	.599
14	.594	.597	67	.607	.603					14	.593
15	.595	.597	68	.608	.605	HUB. AVANT		HUB. DROIT		15	.593
16	.595	.595	69	.609	.608	1	.599	1	.595	16	.594
17	.596	.596	70	.610	.608	2	.598	2	.596	17	.594
18	.598	.596	71	.602	.601	3	.599	3	.595	18	.594
19	.597	.597	72	.601	.600	4	.601	4	.595	19	.598
20	.599	.598	73	.588	.600	5	.599	5	.595	20	.598
21	.599	.600	PRISES LAT. DROITES			6	.599	6	.595	21	.595
22	.603	.601				7	.599	7	.595	22	.595
23	.603	.601	74	.595	.598	8	.600	8	.595	23	.595
24	.603	.603	75	.595	.596	9	.601	9	.595	24	.595
25	.604	.605	76	.595	.595	10	.601	10	.595	25	.595
26	.604	.604	77	.594	.594	11	.600	11	.595	26	.595
27	.605	.603	78	.595	.595					27	.595
28	.607	.604	79	.596	.594	HUB. GAUCHE	12	.595	12	.595	
29	.609	.605	80	.594	.599	13	.595	13	.595	29	.595
30	.608	.604	81	.606	.603	1	.608	14	.595	30	.595
31	.612	.604	82	.604	.605	2	.607	15	.595	31	.595
32	.610	.607	83	.609	.606	3	.606	16	.595	32	.595
33	.611	.608	84	.614	.607	4	.601	17	.595	33	.595
34	.609	.606	85	.615	.608	5	.602	18	.595	34	.595
35	.611	.608	86	.614	.609	6	.604	19	.595	35	.595
36	.611	.609	87	.614	.610	7	.603	20	.595	36	.595
37	.612	.606	88	.613	.608	8	.607	21	.595	37	.595
38	.611	.605	89	.618	.604	9	.608	22	.595	38	.595
39	.613	.604	90	.613	.604	10	.607	23	.595	39	.595
40	.611	.603	91	.607	.604	11	.605	24	.595	40	.595
41	.611	.603	92	.604	.602	12	.605	25	.595	41	.595
42	.613	.603	93	.608	.609	13	.605	26	.595	42	.595
43	.609	.603	94	.601	.599	14	.605	27	.595	43	.595
44	.606	.603	95	.607	.606	15	.603	28	.595	44	.595
45	.605	.602	96	.606	.608	16	.601	29	.595	45	.595
46	.603	.603				17	.601	30	.595	46	.595
47	.603	.601				18	.601	31	.595	47	.595
48	.602	.600				19	.601	32	.595	48	.595
49	.601	.598				20	.602	33	.595	49	.595
50	.599	.598				21	.603	34	.595	50	.595
51	.599	.599				22	.604	35	.595		
52	.599	.597	PRISES COL			23	.605	36	.595		
53	.600	.598				24	.605	37	.595		
54	.599	.598	.595	1.049		25	.606	38	.595		
55	.598	.595	.594	.995		26	.607	39	.595		
56	.594	.593	.594	.901		27	.606	40	.595		
57	.591	.592	.590	.894		28	.609	41	.595		
58	.586	.589	1.017	.833		29	.608	42	.595		
						30	.608	43	.595		
						31	.604	44	.595		
						32	.604	45	.595		

***** FICHER AD157 NOKIT= 1
 23/ 8/89 16H10 AS07 M#6 I=-2 R 1-4 ADAPTE 3D AD157
 DE AD9142 1'ITE.

MACH DE REFERENCE= .5961 UINF= 231.108 M/S
 TIV=301.3 K PIV= 1395 MB

MACH PAROIS HAUTE ET BASSE						MACH PAROIS LATÉR.				AILE AS07		
I	HAUT	BAS	I	HAUT	BAS	I	MACH	I	MACH	I	MACH	
1	.597	.596	*	PRISES DOUBLES		HUB.	AMONT	33	.599	1	.589	
2	.597	.599	**					34	.599	2	.582	
3	.597	.597	**	59	.595	.595	1	.595	35	.599	3	.585
4	.595	.596	**	60	.597	.599	2	.595	36	.599	4	.588
5	.594	.596	**	61	.598	.598	3	.595	37	.599	5	.581
6	.596	.598	**				4	.595	38	.598	6	.560
7	.596	.596	**	PRISES LAT. GAUCHES		5	.595	39	.599	7	.527	
8	.596	.595	**			6	.595	40	.599	8	.533	
9	.597	.598	**	62	.595	.595	7	.595	41	.590	9	.578
10	.597	.595	**	63	.599	.599	8	.595	42	.599	10	.724
11	.595	.596	**	64	.599	.599	9	.595	43	.599	11	.703
12	.593	.595	**	65	.596	.597	10	.595	44	.598	12	.698
13	.595	.595	**	66	.595	.595	11	.595	45	.598	13	.633
14	.594	.596	**	67	.599	.599					14	.671
15	.594	.596	**	68	.591	.590	HUB.	AVAL	HUB.	DROIT	15	.655
16	.595	.595	**	69	.590	.591					16	.650
17	.596	.596	**	70	.590	.599	1	.599	1	.596	17	.657
18	.599	.597	**	71	.599	.599	2	.599	2	.597	18	.657
19	.596	.597	**	72	.599	.591	3	.599	3	.597	19	.657
20	.596	.598	**	73	.598	.594	4	.599	4	.599	20	.661
21	.595	.598	**				5	.599	5	.599	21	.650
22	.598	.596	**	PRISES LAT. DROITES		6	.590	6	.590	6	.592	
23	.598	.596	**			7	.590	7	.590	7	.597	
24	.598	.597	**	74	.596	.599	8	.591	8	.597	8	.577
25	.597	.599	**	75	.599	.599	9	.591	9	.599	9	.587
26	.597	.598	**	76	.595	.595	10	.590	10	.599	10	.591
27	.590	.599	**	77	.595	.595	11	.590	11	.599	11	.584
28	.590	.590	**	78	.595	.595			12	.596	12	.702
29	.595	.592	**	79	.595	.595	HUB.	GAUCHE	13	.596	13	.685
30	.593	.591	**	80	.599	.599	14	.599	14	.599	14	.680
31	.596	.590	**	81	.591	.599	1	.590	15	.599	15	.726
32	.594	.592	**	82	.599	.598	2	.590	16	.599	16	.629
33	.593	.592	**	83	.592	.591	3	.590	17	.599	17	.705
34	.590	.590	**	84	.590	.593	4	.597	18	.599	18	.717
35	.592	.592	**	85	.590	.594	5	.597	19	.599	19	.694
36	.591	.591	**	86	.597	.594	6	.599	20	.599	20	.683
37	.593	.590	**	87	.595	.593	7	.599	21	.599	21	.683
38	.593	.599	**	88	.595	.592	8	.590	22	.599	22	.685
39	.596	.599	**	89	.590	.590	9	.591	23	.599	23	.684
40	.594	.599	**	90	.596	.599	10	.591	24	.599	24	.682
41	.594	.599	**	91	.599	.599	11	.590	25	.599	25	.680
42	.595	.590	**	92	.590	.590	12	.599	26	.599	26	.678
43	.592	.598	**	93	.596	.599	13	.599	27	.599	27	.678
44	.598	.597	**	94	.599	.599	14	.599	28	.599	28	.675
45	.597	.596	**	95	.599	.599	15	.598	29	.599	29	.673
46	.597	.597	**	96	.599	.599	16	.597	30	.599	30	.669
47	.591	.597	**				17	.597	31	.599	31	.651
48	.591	.598	**				18	.597	32	.599	32	.641
49	.590	.599	**				19	.595	33	.599	33	.659
50	.597	.598	**				20	.597	34	.599	34	.659
51	.598	.599	**				21	.599	35	.599	35	.640
52	.599	.598	**	PRISES COL		22	.599	36	.599			
53	.591	.590	**			23	.597	37	.599			
54	.590	.590	**			24	.591	38	.599			
55	.590	.599	**	.550	1.004	25	.599	39	.599			
56	.596	.598	**	.594	.920	26	.591	40	.597			
57	.591	.599	**	.797	.802	27	.592	41	.599			
58	.580	.590	**	.859	.594	28	.593	42	.599			
			+	1.020	.633	29	.594	43	.599			
						30	.592	44	.599			
						31	.591	45	.599			
						32	.599					

***** FICHER AD158 NOKIT= 4
 26/ 8/85 10H35 AS07 M=6 I=-2 R 3-5 ADAPTE 2D AD158
 DE AD144 4'ITE.

MACH DE REFERENCE= .5955 UINF= 331.109 M/S
 TIV=294.7 K PIV= 1393 MB

MACH PAROIS HAUTE ET BASSE						MACH PAROIS LATER.				AILE AS07	
I	HAUT	SAS	I	HAUT	SAS	I	MACH	I	MACH	I	MACH
1	.596	.594	PRISES DOUBLES			HUB. AMONT	33	.598	1	.564	
2	.596	.598					34	.598	2	.565	
3	.596	.597	59	.595	.595	1	.595	35	.598	3	.561
4	.595	.597	60	.596	.596	2	.595	36	.597	4	.560
5	.595	.598	61	.594	.594	3	.594	37	.598	5	.562
6	.595	.598	PRISES LAT. GAUCHES			4	.594	38	.598	6	.564
7	.595	.594	62	.595	.597	5	.594	39	.598	7	.565
8	.596	.596	63	.597	.598	6	.594	40	.600	8	.579
9	.596	.593	64	.597	.597	7	.594	41	.600	9	.579
10	.595	.594	65	.597	.597	8	.594	42	.600	10	.579
11	.594	.595	66	.596	.594	9	.594	43	.598	11	.580
12	.594	.595	67	.600	.596	10	.594	44	.597	12	.582
13	.595	.595	68	.599	.597	11	.594	45	.596	13	.583
14	.595	.594	69	.599	.600	HUB. AVANT		HUB. DROIT		14	.573
15	.596	.594	70	.601	.597	1	.595	1	.595	15	.574
16	.595	.594	71	.598	.596	2	.597	2	.595	16	.573
17	.596	.595	72	.597	.595	3	.597	3	.595	17	.575
18	.594	.595	73	.600	.597	4	.597	4	.595	18	.575
19	.595	.598	PRISES LAT. DROITES			5	.597	5	.595	19	.577
20	.596	.594	74	.596	.599	6	.597	6	.595	20	.577
21	.600	.593	75	.595	.595	7	.598	7	.595	21	.577
22	.599	.599	76	.595	.594	8	.598	8	.595	22	.577
23	.598	.598	77	.595	.593	9	.598	9	.595	23	.577
24	.597	.598	78	.594	.593	10	.597	10	.595	24	.577
25	.599	.598	79	.593	.593	11	.597	11	.595	25	.577
26	.601	.599	80	.593	.593	HUB. GAUCHE		12	.595	26	.577
27	.600	.600	81	.601	.600	13	.595	13	.595	27	.577
28	.602	.599	82	.602	.595	14	.600	14	.595	28	.577
29	.604	.598	83	.598	.600	15	.600	15	.595	29	.577
30	.602	.601	84	.601	.599	16	.599	16	.595	30	.577
31	.603	.601	85	.607	.600	17	.597	17	.595	31	.577
32	.603	.598	86	.608	.601	18	.597	18	.595	32	.577
33	.604	.599	87	.605	.601	19	.597	19	.595	33	.577
34	.601	.598	88	.605	.601	20	.598	20	.595	34	.577
35	.602	.599	89	.604	.600	21	.598	21	.595	35	.577
36	.602	.598	90	.604	.600	22	.600	22	.595	36	.577
37	.603	.597	91	.603	.598	23	.600	23	.595	37	.577
38	.604	.597	92	.605	.598	24	.600	24	.595	38	.577
39	.603	.596	93	.600	.597	25	.599	25	.595	39	.577
40	.603	.596	94	.600	.596	26	.599	26	.595	40	.577
41	.603	.595	95	.597	.594	27	.599	27	.595	41	.577
42	.603	.595	96	.597	.593	28	.599	28	.595	42	.577
43	.601	.595	97	.597	.593	29	.599	29	.595	43	.577
44	.601	.595	98	.597	.593	30	.599	30	.595	44	.577
45	.599	.595	99	.597	.593	31	.599	31	.595	45	.577
46	.598	.595	100	.597	.593	32	.599	32	.595	46	.577
47	.599	.595	101	.597	.593	33	.599	33	.595	47	.577
48	.600	.595	102	.597	.593	34	.599	34	.595	48	.577
49	.600	.595	103	.597	.593	35	.599	35	.595	49	.577
50	.597	.595	104	.597	.593	36	.599	36	.595	50	.577
51	.595	.594	PRISES COL			37	.598	37	.595	51	.577
52	.595	.594	105	.603	1.047	38	.599	38	.595	52	.577
53	.595	.594	106	.606	.600	39	.600	39	.595	53	.577
54	.592	.593	107	.604	.604	40	.601	40	.595	54	.577
55	.590	.593	108	.603	.603	41	.602	41	.595	55	.577
56	.595	.595	109	1.014	.602	42	.603	42	.595	56	.577
						43	.603	43	.595		
						44	.603	44	.595		
						45	.603	45	.595		

***** FICHER AD159 NOCIT= 1
 26/ 8/85 11H 0 AS07 M=6 I=-2 R 3-5 NON ADAPTE AD159
 DE AD4 1'ITE. PAROIS RECTILIGNES SYMETRIQUES

MACH DE REFERENCE= .5958 UINF= 331.108 M/S
 TIV=398.9 K PIV= 1392 MB

MACH PAROIS HAUTE ET BASSE						MACH PAROIS LATÉR.				RILE AS07	
I	HAUT	BAS	I	HAUT	BAS	I	MACH	I	MACH	I	MACH
1	.596	.595	PRISES DOUBLES			HUB. AMONT	33	.595	1	.574	
2	.597	.599				34	.594	2	.593		
3	.596	.596	59	.595	.595	35	.594	3	.594		
4	.595	.595	59	.597	.598	36	.592	4	.593		
5	.594	.595	61	.597	.595	37	.593	5	.704		
6	.596	.597				38	.593	6	.597		
7	.596	.595	PRISES LAT. GAUCHES			39	.594	7	.599		
8	.597	.599				40	.595	8	.599		
9	.597	.599	62	.595	.595	41	.595	9	.592		
10	.597	.595	63	.597	.599	42	.595	10	.598		
11	.595	.595	64	.599	.599	43	.594	11	.700		
12	.592	.593	65	.599	.599	44	.597	12	.713		
13	.593	.595	66	.592	.599	45	.593	13	.700		
14	.594	.595	67	.611	.601	HUB. AVAL		HUB. DROIT			
15	.595	.597	68	.610	.603	1	.591	1	.596		
16	.596	.595	69	.597	.605	2	.590	2	.596		
17	.597	.597	70	.610	.601	3	.590	3	.595		
18	.599	.597	71	.591	.599	4	.592	4	.595		
19	.598	.597	72	.601	.599	5	.591	5	.595		
20	.599	.599	73	.599	.599	6	.590	6	.595		
21	.599	.599	PRISES LAT. DROITES			7	.590	7	.595		
22	.593	.599				8	.590	8	.595		
23	.594	.594	74	.596	.593	9	.590	9	.595		
24	.593	.594	75	.596	.596	10	.599	10	.595		
25	.593	.595	76	.595	.595	11	.599	11	.595		
26	.593	.593	77	.594	.594	HUB. GAUCHE		12	.595		
27	.596	.594	78	.595	.595	13	.595	13	.595		
28	.590	.595	79	.597	.595	14	.595	14	.595		
29	.594	.595	80	.594	.599	15	.595	15	.595		
30	.594	.594	81	.595	.593	16	.597	16	.595		
31	.594	.594	82	.594	.596	17	.596	17	.595		
32	.592	.593	83	.599	.593	18	.596	18	.595		
33	.590	.595	84	.597	.594	19	.595	19	.595		
34	.590	.595	85	.595	.596	20	.595	20	.595		
35	.590	.595	86	.595	.597	21	.595	21	.595		
36	.590	.595	87	.595	.593	22	.595	22	.595		
37	.591	.595	88	.593	.595	23	.595	23	.595		
38	.591	.594	89	.599	.592	24	.597	24	.595		
39	.591	.594	90	.593	.592	25	.597	25	.595		
40	.591	.592	91	.597	.592	26	.597	26	.595		
41	.591	.592	92	.590	.599	27	.595	27	.595		
42	.592	.592	93	.590	.597	28	.595	28	.595		
43	.590	.593	94	.591	.597	29	.595	29	.595		
44	.597	.593	95	.596	.599	30	.595	30	.595		
45	.595	.591	96	.596	.597	31	.595	31	.595		
46	.593	.591				32	.595	32	.595		
47	.593	.593									
48	.593	.593									
49	.593	.593									
50	.592	.593									
51	.591	.593									
52	.593	.595	PRISES COL								
53	.593	.597									
54	.593	.593	.554	1.045							
55	.597	.595	.592	.595							
56	.594	.593	.793	.801							
57	.592	.591	.860	.992							
58	.593	.599	1.015	.592							

FICHER AD160 NOKIT= 1
28/3/85 11H25 A907 M=6 I=-2 R 3-5 ADAPTE 3D AD160
DE AD9142 1'ITE.

MACH DE REFERENCE= .5964 UINF= 231.103 M/S
TIV=297.3 K PIV= 1390 MB

MACH PAROIS HAUTE ET BASSE						MACH PAROIS LATER.				AILE A907	
I	HAUT	BAS	I	HAUT	BAS	I	MACH	I	MACH	I	MACH
***** PRISES DOUBLES *****											
1	.598	.596				HUB. AMONT	33		.599	1	.570
2	.597	.599					34		.599	2	.589
3	.596	.597	59	.595	.595	1	.595	35	.599	3	.600
4	.594	.597	60	.598	.599	2	.594	36	.599	4	.601
5	.594	.597	61	.600	.597	3	.594	37	.599	5	.599
6	.595	.598				4	.595	38	.599	6	.599
7	.595	.598	***** PRISES LAT. GAUCHES *****			5	.594	39	.599	7	.599
8	.597	.598				6	.594	40	.600	8	.599
9	.598	.598	62	.595	.597	7	.594	41	.601	9	.600
10	.598	.598	63	.599	.601	8	.593	42	.601	10	.600
11	.595	.597	64	.600	.599	9	.594	43	.599	11	.600
12	.594	.598	65	.597	.598	10	.594	44	.599	12	.600
13	.596	.597	66	.597	.595	11	.595	45	.598	13	.600
14	.595	.597	67	.603	.598					14	.600
15	.596	.598	68	.601	.598	HUB. AVAL		HUB. DROIT		15	.675
16	.597	.597	69	.600	.599					16	.679
17	.598	.597	70	.604	.597	1	.600	1	.597	17	.600
18	.598	.598	71	.600	.597	2	.600	2	.596	18	.670
19	.598	.599	72	.601	.599	3	.600	3	.598	19	.679
20	.597	.598	73	.594	.602	4	.600	4	.597	20	.681
21	.596	.599				5	.599	5	.597	21	.682
22	.599	.599	***** PRISES LAT. DROITES *****			6	.599	6	.597	22	.681
23	.598	.599				7	.600	7	.597	23	.675
24	.597	.599	74	.596	.599	8	.601	8	.596	24	.686
25	.598	.599	75	.596	.597	9	.600	9	.596	25	.688
26	.598	.599	76	.597	.596	10	.599	10	.596	26	.685
27	.598	.598	77	.595	.596	11	.599	11	.596	27	.681
28	.598	.598	78	.596	.596					28	.685
29	.596	.600	79	.596	.596	HUB. GAUCHE				29	.685
30	.594	.602	80	.600	.599	13	.597	13	.597	30	.684
31	.596	.600	81	.601	.599	1	.601	14	.597	31	.684
32	.594	.602	82	.599	.600	2	.600	15	.599	32	.684
33	.604	.600	83	.603	.600	3	.600	16	.599	33	.689
34	.601	.600	84	.609	.602	4	.598	17	.597	34	.689
35	.602	.600	85	.610	.603	5	.598	18	.596	35	.685
36	.602	.600	86	.607	.603	6	.599	19	.596	36	.680
37	.603	.600	87	.605	.602	7	.600	20	.596	37	.670
38	.603	.600	88	.605	.601	8	.601	21	.596	38	.670
39	.605	.600	89	.610	.599	9	.602	22	.596	39	.670
40	.604	.609	90	.607	.598	10	.602	23	.596	40	.670
41	.604	.609	91	.603	.596	11	.600	24	.597	41	.671
42	.605	.608	92	.602	.598	12	.600	25	.597	42	.670
43	.604	.609	93	.607	.597	13	.600	26	.597	43	.674
44	.602	.609	94	.601	.597	14	.600	27	.597	44	.674
45	.601	.609	95	.600	.594	15	.600	28	.597	45	.681
46	.600	.609	96	.592	.592	16	.598	29	.597	46	.680
47	.602	.608				17	.598	30	.597	47	.680
48	.601	.608				18	.598	31	.597	48	.680
49	.600	.608				19	.598	32	.597	49	.680
50	.600	.608				20	.598	33	.597	50	.680
51	.600	.608				21	.598	34	.597		.680
52	.601	.608	***** PRISES COL *****			22	.598				
53	.601	.608				23	.597				
54	.601	.608	97	.601	1.0055	24	.600				
55	.600	.608	98	.601	.600	25	.601				
56	.600	.608	99	.603	.600	26	.600				
57	.600	.608	100	.603	.600	27	.604				
58	.600	.608	101	.604	.602	28	.604				
59	.600	.608	102	.604	.602	29	.604				
60	.600	.608	103	.604	.602	30	.600				
61	.600	.608	104	.604	.602	31	.600				
62	.600	.608	105	.604	.602	32	.600				

***** FICHER AD162 NOKIT= 1
 26/ 8/85 14H20 AS07 M=.5 I=0 R 3-6 NON ADAPTE AD162
 DE AD4 L'ITE. PAROIS RECTILIGNES SYMETRIQUES

MACH DE REFERENCE= .5979 UINF= 231.108 M/S
 TIV=299.4 K PIV= 1391 MB

MACH PAROIS HAUTE ET BASSE						MACH PAROIS LATÉR.				AILE AS07	
I	HAUT	BAS	I	HAUT	BAS	I	MACH	I	MACH	I	MACH
1	.597	.596	PRISES DOUBLES			HUB. AMONT		33	.604	1	.559
2	.597	.600						34	.604	2	.580
3	.597	.598	59	.597	.598	1	.598	35	.603	3	.620
4	.596	.597	60	.599	.599	2	.599	36	.602	4	.659
5	.596	.597	61	.602	.599	3	.599	37	.603	5	.674
6	.598	.599				4	.599	38	.602	6	.653
7	.598	.598	PRISES LAT. GAUCHES			5	.597	39	.603	7	.625
8	.598	.597				6	.597	40	.603	8	.606
9	.598	.599	62	.596	.597	7	.598	41	.605	9	.622
10	.599	.599	63	.600	.601	8	.598	42	.604	10	.640
11	.598	.598	64	.600	.601	9	.598	43	.603	11	.633
12	.596	.598	65	.603	.599	10	.598	44	.603	12	.7190
13	.598	.598	66	.607	.600	11	.598	45	.602	13	.7164
14	.598	.600	67	.611	.600					14	.7146
15	.599	.600	68	.613	.601	HUB. AVAL		HUB. DROIT		15	.7229
16	.598	.598	69	.614	.604	1	.602	1	.597	16	.7207
17	.599	.598	70	.615	.600	2	.603	2	.599	17	.724
18	.601	.593	71	.605	.600	3	.603	3	.599	18	.719
19	.600	.597	72	.602	.601	4	.603	4	.598	19	.717
20	.603	.599	73	.599	.603	5	.603	5	.598	20	.714
21	.604	.599				6	.603	6	.598	21	.709
22	.607	.599	PRISES LAT. DROITES			7	.603	7	.598	22	.701
23	.609	.599				8	.603	8	.598	23	.692
24	.609	.602	74	.597	.599	9	.604	9	.598	24	.690
25	.611	.602	75	.597	.598	10	.604	10	.598	25	.688
26	.610	.602	76	.597	.596	11	.602	11	.602	26	.627
27	.613	.603	77	.599	.597			12	.598	27	.673
28	.614	.601	78	.597	.596	HUB. GAUCHE		13	.598	28	.654
29	.617	.601	79	.600	.595	1	.613	13	.598	29	.654
30	.616	.601	80	.609	.598	2	.613	14	.598	30	.634
31	.620	.599	81	.612	.600	3	.612	15	.598	31	.625
32	.618	.603	82	.613	.602	4	.612	16	.598	32	.621
33	.619	.603	83	.617	.600	5	.612	17	.599	33	.655
34	.617	.602	84	.623	.600	6	.615	18	.599	34	.600
35	.620	.603	85	.625	.601	7	.615	19	.599	35	.7161
36	.619	.604	86	.623	.602	8	.611	20	.598	36	.7145
37	.620	.602	87	.622	.603	9	.611	21	.598	37	.7135
38	.619	.602	88	.621	.602	10	.613	22	.598	38	.7128
39	.621	.601	89	.624	.601	11	.613	23	.598	39	.7119
40	.618	.601	90	.619	.601	12	.612	24	.598	40	.709
41	.619	.601	91	.612	.600	13	.611	25	.598	41	.7085
42	.618	.601	92	.607	.599	14	.610	26	.598	42	.699
43	.615	.600	93	.601	.599	15	.609	27	.598	43	.697
44	.612	.600	94	.603	.600	16	.608	28	.598	44	.6882
45	.610	.599	95	.599	.591	17	.608	29	.598	45	.6771
46	.608	.600	96	.606	.588	18	.604	30	.598	46	.664
47	.607	.599				19	.605	31	.598	47	.6583
48	.606	.600				20	.605	32	.598	48	.6553
49	.605	.600				21	.605	33	.598	49	.6524
50	.604	.601				22	.605	34	.598	50	.6497
51	.604	.601				23	.606	35	.597		
52	.603	.600	PRISES OCL			24	.606	36	.597		
53	.602	.600				25	.606	37	.597		
54	.601	.600		.600	1.055	26	.608	38	.597		
55	.599	.597		.992	.912	27	.609	39	.597		
56	.595	.595		.797	.738	28	.610	40	.598		
57	.591	.592		.650	.592	29	.611	41	.598		
58	.584	.597		1.319	.630	30	.612	42	.598		
						31	.610	43	.598		
						32	.608	44	.598		
								45	.598		

***** FICHER AD163 NO(IT)= 1
 26/ 3/85 14H40 AS07 M=.6 I=0 R 3-6 ADAPTE 3D AD163
 DE AD9107 1'ITE.

MACH DE REFERENCE= .5980 UNF= 231.108 M/S
 TIV=298.8 K PIV= 1390 MB

MACH PAROIS HAUTE ET BASSE						MACH PAROIS LATÉR.				FILE AS07	
I	HAUT	BAS	I	HAUT	BAS	I	MACH	I	MACH	I	MACH
1	.599	.597	PRISES DOUBLES			HUB. AMONT	33	.601	1	.601	.601
2	.599	.601					34	.600	2	.600	.600
3	.598	.599	59	.598	.599	1	.599	35	.600	3	.600
4	.596	.598	60	.598	.598	2	.598	36	.600	4	.600
5	.596	.599	61	.603	.599	3	.598	37	.600	5	.600
6	.599	.600				4	.598	38	.600	6	.600
7	.598	.598	PRISES LAT. GAUCHES			5	.598	39	.600	7	.600
8	.599	.597				6	.598	40	.600	8	.600
9	.598	.598	62	.597	.598	7	.598	41	.601	9	.601
10	.599	.596	63	.600	.601	8	.597	42	.600	10	.600
11	.598	.597	64	.601	.602	9	.597	43	.599	11	.600
12	.596	.597	65	.598	.597	10	.597	44	.598	12	.598
13	.597	.597	66	.599	.598	11	.598	45	.598	13	.598
14	.598	.599	67	.603	.601					14	.598
15	.598	.600	68	.604	.600	HUB. AVAL		HUB. DROIT		15	.598
16	.599	.599	69	.604	.602					16	.598
17	.599	.600	70	.606	.599	1	.604	1	.598	17	.598
18	.602	.598	71	.600	.597	2	.604	2	.598	18	.598
19	.600	.597	72	.603	.599	3	.603	3	.598	19	.598
20	.599	.598	73	.598	.602	4	.603	4	.598	20	.598
21	.599	.598				5	.602	5	.599	21	.598
22	.601	.598	PRISES LAT. DROITES			6	.603	6	.599	22	.598
23	.602	.597				7	.603	7	.599	23	.598
24	.601	.599	74	.598	.600	8	.605	8	.598	24	.598
25	.602	.600	75	.598	.599	9	.604	9	.598	25	.598
26	.601	.599	76	.598	.596	10	.602	10	.598	26	.598
27	.604	.599	77	.597	.596	11	.601	11	.600	27	.598
28	.605	.601	78	.597	.597			12	.600	28	.598
29	.603	.601	79	.598	.594	HUB. GAUCHE		13	.600	29	.598
30	.606	.600	80	.603	.596			14	.600	30	.598
31	.609	.598	81	.605	.597	1	.604	15	.600	31	.598
32	.607	.601	82	.603	.599	2	.603	16	.600	32	.598
33	.609	.601	83	.608	.600	3	.603	17	.600	33	.598
34	.607	.599	84	.613	.600	4	.600	18	.600	34	.598
35	.608	.600	85	.615	.601	5	.600	19	.600	35	.598
36	.607	.600	86	.613	.601	6	.602	20	.600	36	.598
37	.609	.599	87	.612	.601	7	.604	21	.600	37	.598
38	.609	.600	88	.612	.600	8	.605	22	.600	38	.598
39	.611	.600	89	.615	.600	9	.605	23	.600	39	.598
40	.610	.599	90	.609	.600	10	.604	24	.600	40	.598
41	.609	.599	91	.605	.597	11	.603	25	.600	41	.598
42	.608	.598	92	.603	.598	12	.603	26	.600	42	.598
43	.606	.597	93	.609	.598	13	.603	27	.600	43	.598
44	.603	.597	94	.604	.597	14	.602	28	.600	44	.598
45	.602	.596	95	.602	.597	15	.601	29	.600	45	.598
46	.602	.597	96	.595	.584	16	.600	30	.600	46	.598
47	.603	.597				17	.600	31	.600	47	.598
48	.603	.599				18	.600	32	.600	48	.598
49	.603	.599				19	.600	33	.600	49	.598
50	.603	.599				20	.600	34	.600	50	.598
51	.605	.600				21	.601	35	.600	51	.598
52	.604	.600	PRISES COL			22	.601	36	.600	52	.598
53	.605	.600				23	.600	37	.600	53	.598
54	.605	.600	.660	1.004		24	.602	38	.600	54	.598
55	.604	.597	.641	.916		25	.603	39	.600	55	.598
56	.601	.593	.797	.766		26	.604	40	.600	56	.598
57	.609	.609	.664	.691		27	.606	41	.600	57	.598
58	.605	.602	1.021	.630		28	.606	42	.600	58	.598
						29	.606	43	.600		
						30	.604	44	.600		
						31	.603	45	.600		
						32	.601				

***** FICHER AD164 NOCIT= 4
 25/08/85 15H 5 A907 M=.8 I=0 R 3-6 ADAPTE 3D AD164
 DE AD134 4'ITE.

MACH DE REFERENCE= .3067 UINF= 231.108 M/S
 TIV=294.0 K PIV= 1653 MB

MACH PAROIS HAUTE ET BASSE						MACH PAROIS LATÉR.				AILE A907	
I	HAUT	BAS	I	HAUT	BAS	I	MACH	I	MACH	I	MACH
1	.305	.302	PRISES DOUBLES			HUB. AMONT	33	.311	1	.753	
2	.306	.303					34	.310	2	.789	
3	.307	.306	59	.304	.304	1	.304	35	.309	3	.865
4	.305	.306	60	.305	.305	2	.302	36	.308	4	.855
5	.305	.303	61	.307	.302	3	.301	37	.308	5	.950
6	.307	.303				4	.302	38	.307	6	.899
7	.304	.304	PRISES LAT. GAUCHES			5	.300	39	.308	7	.851
8	.305	.302				6	.300	40	.310	8	.817
9	.305	.306	62	.305	.305	7	.300	41	.312	9	.406
10	.305	.300	63	.797	.309	8	.799	42	.310	10	1.414
11	.303	.302	64	.310	.305	9	.300	43	.307	11	1.376
12	.300	.304	65	.311	.307	10	.300	44	.307	12	1.285
13	.303	.303	66	.311	.302	11	.300	45	.305	13	1.030
14	.303	.305	67	.323	.305					14	1.025
15	.305	.304	68	.319	.303	HUB. AVAL		HUB. DROIT		15	1.013
16	.306	.300	69	.321	.313					16	1.028
17	.306	.300	70	.325	.305	1	.308	1	.305	17	1.018
18	.306	.303	71	.310	.302	2	.307	2	.305	18	1.010
19	.306	.304	72	.303	.305	3	.306	3	.305	19	1.023
20	.310	.307	73	.305	.310	4	.307	4	.305	20	1.012
21	.311	.307				5	.306	5	.304	21	1.303
22	.312	.305	PRISES LAT. DROITES			6	.305	6	.305	22	.380
23	.314	.302				7	.305	7	.305	23	.355
24	.314	.303	74	.306	.309	8	.306	8	.305	24	.753
25	.315	.305	75	.304	.304	9	.307	9	.304	25	.719
26	.313	.303	76	.303	.300	10	.305	10	.305	26	.859
27	.325	.301	77	.302	.302	11	.305	11	.305	27	.956
28	.327	.305	78	.302	.795					28	.958
29	.335	.306	79	.304	.798	HUB. GAUCHE				29	.903
30	.330	.307	80	.313	.304					30	.863
31	.337	.304	81	.320	.303	1	.322	13	.305	31	.855
32	.331	.311	82	.319	.302	2	.321	14	.305	32	.416
33	.334	.313	83	.333	.303	3	.321	15	.305	33	1.512
34	.327	.310	84	.346	.306	4	.310	16	.305	34	1.433
35	.330	.312	85	.347	.310	5	.311	17	.305	35	1.334
36	.323	.313	86	.340	.313	6	.316	18	.305	36	1.051
37	.332	.310	87	.335	.313	7	.320	19	.305	37	1.043
38	.329	.309	88	.333	.310	8	.325	20	.305	38	1.034
39	.333	.307	89	.337	.304	9	.326	21	.305	39	1.005
40	.330	.305	90	.327	.304	10	.322	22	.305	40	.894
41	.329	.304	91	.317	.305	11	.320	23	.305	41	.906
42	.330	.304	92	.314	.303	12	.319	24	.305	42	.371
43	.324	.304	93	.303	.302	13	.318	25	.305	43	.370
44	.317	.304	94	.307	.303	14	.316	26	.305	44	.327
45	.317	.303	95	.306	.300	15	.310	27	.305	45	.306
46	.312	.304	96	.302	.797	16	.309	28	.305	46	.393
47	.313	.303				17	.309	29	.305	47	.331
48	.311	.304				18	.309	30	.305	48	.350
49	.313	.304				19	.310	31	.305	49	.375
50	.307	.305				20	.310	32	.304	50	.322
51	.303	.304				21	.312	33	.304		
52	.310	.303	PRISES COL			22	.313	34	.304		
53	.310	.305				23	.311	35	.304		
54	.309	.304	.352	1.213		24	.317	36	.304		
55	.309	.303	.371	1.213		25	.319	37	.304		
56	.306	.301	.307	.300		26	.322	38	.304		
57	.306	.302	.382	.325		27	.326	39	.304		
58	.306	.798	1.141	.793		28	.328	40	.304		
						29	.322	41	.304		
						30	.325	42	.304		
						31	.322	43	.304		
						32	.315	44	.304		
						33	.311	45	.304		
						34	.313				

***** FICHER AD166 NO(IT)= 1
 26/ 3/95 15H45 AS07 M=.3 I=0 R 3-6 ADAPTE 3D AD166
 DE AD9118 1'ITE.

MACH DE REFERENCE= .3039 UINF= 231.109 M/S
 TIV=298.3 K PIV= 1649 MB

MACH PAROIS HAUTE ET BASSE						MACH PAROIS LATÉR.				AILE A907			
I	HAUT	BAS	I	HAUT	BAS	I	MACH	I	MACH	I	MACH		
1	.306	.303	PRISES DOUBLES			HUB. AMONT		33	.306	1	.758		
2	.307	.311						34	.305	2	.786		
3	.305	.307	59	.305	.305	1	.799	35	.305	3	.862		
4	.300	.304	60	.306	.305	2	.798	36	.304	4	.973		
5	.799	.305	61	.303	.301	3	.798	37	.303	5	.953		
6	.304	.303						38	.303	6	.892		
7	.305	.306	PRISES LAT. GAUCHES					39	.303	7	.849		
8	.306	.303						40	.305	8	.307		
9	.306	.306	62	.302	.304	5	.798	41	.303	9	.425		
10	.307	.300	63	.797	.303	6	.797	42	.307	10	1.375		
11	.302	.301	64	.305	.306	7	.795	43	.303	11	1.301		
12	.796	.300	65	.303	.300	8	.799	44	.302	12	1.097		
13	.798	.300	66	.304	.798	9	.799	45	.301	13	1.030		
14	.798	.303	67	.313	.303	10	.799	46	.302	14	1.015		
15	.799	.304	68	.312	.303	HUB. AVAL		HUB. DROIT		15	1.001		
16	.799	.301	69	.314	.307	1	.307	1	.304	15	1.006		
17	.301	.302	70	.316	.306	2	.306	2	.304	17	1.003		
18	.305	.302	71	.306	.797	3	.305	3	.304	18	.997		
19	.304	.300	72	.303	.307	4	.305	4	.304	19	1.003		
20	.304	.301	73	.306	.310	5	.305	5	.304	20	.998		
21	.303	.301	PRISES LAT. DROITES					6	.305	6	.304	21	.991
22	.305	.799						7	.305	7	.971		
23	.307	.799	74	.303	.309	8	.306	8	.304	23	.948		
24	.308	.799	75	.305	.306	9	.306	9	.304	24	.751		
25	.308	.302	76	.305	.306	10	.303	10	.304	25	.777		
26	.309	.300	77	.304	.301	11	.303	11	.304	26	.857		
27	.315	.799	78	.799	.799	12	.304	12	.304	27	.957		
28	.317	.304	79	.797	.798	HUB. GAUCHE				28	.959		
29	.323	.305	80	.302	.796	13	.304	13	.304	29	.309		
30	.319	.304	81	.310	.798	14	.304	14	.304	30	.375		
31	.326	.301	82	.313	.799	1	.314	15	.304	31	.373		
32	.321	.306	83	.311	.300	2	.313	16	.304	32	.416		
33	.325	.307	84	.322	.301	3	.312	17	.304	33	1.403		
34	.320	.303	85	.304	.305	4	.303	18	.304	34	1.336		
35	.323	.304	86	.306	.308	5	.304	19	.304	35	1.373		
36	.321	.305	87	.332	.303	6	.303	20	.304	36	1.356		
37	.323	.303	88	.329	.307	7	.312	21	.304	37	1.343		
38	.321	.305	89	.327	.304	8	.316	22	.304	38	1.326		
39	.325	.305	90	.329	.303	9	.318	23	.304	39	1.000		
40	.320	.305	91	.319	.305	10	.315	24	.304	40	.991		
41	.319	.305	92	.311	.304	11	.312	25	.304	41	.382		
42	.320	.305	93	.309	.797	12	.311	26	.304	42	.958		
43	.317	.305	94	.301	.300	13	.311	27	.304	43	.956		
44	.311	.304	95	.308	.305	14	.310	28	.304	44	.924		
45	.311	.301	96	.304	.796	15	.304	29	.304	45	.904		
46	.307	.301		.303	.794	16	.303	30	.304	46	.892		
47	.309	.797				17	.303	31	.304	47	.925		
48	.307	.799				18	.304	32	.304	48	.947		
49	.308	.302				19	.304	33	.304	49	.370		
50	.306	.305				20	.304	34	.304	50	.313		
51	.308	.307				21	.305	35	.304				
52	.307	.302	PRISES COL					22	.307	36	.304		
53	.307	.303						23	.305	37	.304		
54	.308	.304	.343	1.210		24	.311	38	.304				
55	.310	.301	.355	1.123		25	.313	39	.304				
56	.308	.798	.336	.394		26	.315	40	.303				
57	.308	.798	.381	.319		27	.320	41	.303				
58	.304	.798	1.141	.780		28	.322	42	.303				
						29	.317	43	.303				
						30	.310	44	.304				
						31	.307	45	.304				
						32	.307						

***** FICHER AD167 NO<IT>= 1
 26/3/85 16H15 AS07 M=5 I=2(1.5+ROT.30) R 3-6 NON ADAPTE AD167
 DE AD45 1/ITE. PAROIS RECTILIGNES + 30'

MACH DE REFERENCE= .5991 UINF= 231.198 M/S
 TIV=398.7 K PIV= 1391 MB

MACH PAROIS HAUTE ET BASSE		MACH PAROIS LAT. DROIT		MACH PAROIS LAT. GAUCHE		MACH PAROIS LAT. HUB.		MACH PAROIS LAT. HUB. DROIT		MACH PAROIS LAT. HUB. GAUCHE	
I	HAUT	BAS	I	HAUT	BAS	HUB.	AMONT	I	MACH	I	MACH
1	.597	.593						33	.595		.597
2	.595	.596						34	.594		.595
3	.593	.597				1	.599	35	.593		.595
4	.599	.599		59	.599	2	.599	36	.593		.592
5	.597	.591		50	.599	3	.599	37	.592		.590
6	.593	.592		51	.599	4	.599	38	.592		.594
7	.598	.599		52	.599	5	.599	39	.591		.594
8	.599	.598		53	.599	6	.599	40	.591		.593
9	.599	.597		54	.599	7	.599	41	.592		.599
10	.598	.598		55	.599	8	.599	42	.593		.592
11	.598	.598		56	.599	9	.599	43	.591		.592
12	.596	.598		57	.599	10	.598	44	.599		.592
13	.598	.597		58	.599	11	.599	45	.599		.592
14	.598	.599		59	.599						
15	.599	.599		60	.599						
16	.599	.599		61	.599						
17	.599	.599		62	.599						
18	.595	.599		63	.599						
19	.595	.599		64	.599						
20	.595	.599		65	.599						
21	.595	.599		66	.599						
22	.597	.599		67	.599						
23	.595	.599		68	.599						
24	.595	.599		69	.599						
25	.595	.599		70	.599						
26	.595	.599		71	.599						
27	.595	.599		72	.599						
28	.595	.599		73	.599						
29	.595	.599		74	.599						
30	.595	.599		75	.599						
31	.595	.599		76	.599						
32	.595	.599		77	.599						
33	.595	.599		78	.599						
34	.595	.599		79	.599						
35	.595	.599		80	.599						
36	.595	.599		81	.599						
37	.595	.599		82	.599						
38	.595	.599		83	.599						
39	.595	.599		84	.599						
40	.595	.599		85	.599						
41	.595	.599		86	.599						
42	.595	.599		87	.599						
43	.595	.599		88	.599						
44	.595	.599		89	.599						
45	.595	.599		90	.599						
46	.595	.599		91	.599						
47	.595	.599		92	.599						
48	.595	.599		93	.599						
49	.595	.599		94	.599						
50	.595	.599		95	.599						
51	.595	.599		96	.599						
52	.595	.599		97	.599						
53	.595	.599		98	.599						
54	.595	.599		99	.599						
55	.595	.599		100	.599						
56	.595	.599		101	.599						
57	.595	.599		102	.599						
58	.595	.599		103	.599						
59	.595	.599		104	.599						
60	.595	.599		105	.599						

PRISES COL

.699 1.069
 .699 .892
 .893 .791
 .893 .893
 1.099 .691

***** FICHER AD168 NO(IT)= 1
 26/ 8/85 16H25 AS07 M=6 I=+2(1.5+ROT.30') R 3-6 ADAPTE 3D AD168
 DE AD9122 1'ITE.

MACH DE REFERENCE= .5994 UINF= 231.109 M/S
 TIV=298.4 K PIV= 1391 MB

MACH PAROIS HAUTE ET BASSE						MACH PAROIS LATÉR.				AILE AS07	
I	HAUT	BAS	I	HAUT	BAS	I	MACH	I	MACH	I	MACH
			PRISES DOUBLES			HUB.	AMONT	33	.602	1	.563
1	.607	.592						34	.601	2	.573
2	.606	.595						35	.600	3	.577
3	.603	.597	59	.598	.599	1	.599	36	.602	4	.583
4	.599	.598	60	.600	.600	2	.598	37	.601	5	.584
5	.597	.599	61	.604	.599	3	.598	38	.600	6	.585
6	.599	.601				4	.599	39	.600	7	.584
7	.598	.600	PRISES LAT. GAUCHES			5	.599	40	.600	8	.583
8	.599	.599	62	.600	.597	6	.598	41	.601	9	.583
9	.600	.601	63	.602	.603	7	.598	42	.601	10	1.004
10	.601	.597	64	.603	.604	8	.598	43	.599	11	.989
11	.599	.598	65	.601	.600	9	.598	44	.599	12	.987
12	.597	.598	66	.599	.601	10	.598	45	.598	13	.984
13	.598	.597	67	.607	.600	11	.599			14	.979
14	.598	.599	68	.606	.600	HUB. AVANT		HUB. DROIT		15	.961
15	.599	.600	69	.606	.601			1	.599	16	.955
16	.599	.599	70	.611	.600	1	.603	2	.599	17	.947
17	.601	.600	71	.604	.599	2	.604	3	.599	18	.938
18	.603	.601	72	.605	.602	3	.604	4	.599	19	.933
19	.602	.600	73	.605	.605	4	.604	5	.600	20	.926
20	.602	.600				5	.604	6	.600	21	.916
21	.602	.599	PRISES LAT. DROITES			6	.604	7	.600	22	.914
22	.605	.599	74	.601	.599	7	.604	8	.599	23	.909
23	.605	.597	75	.600	.599	8	.605	9	.599	24	.905
24	.603	.600	76	.600	.599	9	.605	10	.599	25	.903
25	.604	.600	77	.600	.597	10	.603	11	.599	26	.900
26	.604	.600	78	.599	.598	11	.602	12	.600	27	.898
27	.608	.598	79	.602	.596	HUB. GAUCHE		13	.600	28	.898
28	.610	.599	80	.607	.597	14	.600	14	.600	29	.891
29	.614	.598	81	.611	.607	15	.607	15	.600	30	.887
30	.612	.598	82	.608	.598	16	.607	16	.600	31	.886
31	.615	.594	83	.613	.597	17	.607	17	.600	32	1.000
32	.612	.598	84	.620	.596	18	.603	18	.599	33	.889
33	.613	.597	85	.620	.597	19	.603	19	.599	34	.889
34	.609	.597	86	.617	.598	20	.603	20	.599	35	.888
35	.611	.597	87	.615	.599	21	.603	21	.599	36	.887
36	.609	.598	88	.614	.597	22	.609	22	.599	37	.887
37	.613	.597	89	.620	.597	23	.610	23	.599	38	.886
38	.613	.598	90	.618	.598	24	.608	24	.599	39	.886
39	.616	.598	91	.607	.598	25	.607	25	.599	40	.885
40	.614	.597	92	.606	.599	26	.607	26	.599	41	.885
41	.613	.597	93	.602	.600	27	.606	27	.599	42	.885
42	.613	.598	94	.606	.601	28	.605	28	.599	43	.885
43	.609	.597	95	.604	.599	29	.603	29	.599	44	.885
44	.606	.598	96	.594	.597	30	.602	30	.599	45	.885
45	.604	.598				31	.602	31	.599		
46	.606	.598				32	.602	32	.600		
47	.606	.601									
48	.606	.601									
49	.606	.601									
50	.604	.601									
51	.605	.601									
52	.605	.599	PRISES COL			33	.600	35	.600		
53	.606	.601				34	.602	36	.600		
54	.605	.602				35	.602	37	.600		
55	.604	.601	.671	1.072		36	.605	38	.600		
56	.601	.600	.691	.901		37	.606	39	.600		
57	.598	.599	.686	.793		38	.607	40	.600		
58	.591	.596	.672	.691		39	.609	41	.600		
			1.002	.633		40	.610	42	.600		
						41	.608	43	.600		
						42	.607	44	.600		
						43	.605	45	.600		
						44	.603				
						45	.603				

***** FICHER AD169 N00IT= 4
 26/ 8/85 16H50 AS07 M=.6 I=+2 R 3-5 ADAPTE 2D AD169
 DE AD145 4'ITE.

 MACH DE REFERENCE= .5991 UINF= 231.108 M/S
 TIV=294.2 K PIV= 1391 MB

MACH PAROIS-HAUTE ET BASSE						MACH PAROIS LATER.				RILE AS07	
I	HAUT	BAS	I	HAUT	BAS	I	MACH	I	MACH	I	MACH
1	.601	.596	PRISES DOUBLES				HUB. AMONT	33	.599	1	.596
2	.601	.600						34	.598	2	.597
3	.600	.599	59	.600	.598	1	.600	35	.597	3	.596
4	.597	.599	60	.602	.599	2	.599	36	.598	4	.594
5	.597	.600	61	.600	.597	3	.599	37	.597	5	.596
6	.600	.601				4	.599	38	.597	6	.594
7	.600	.598	PRISES LAT. GAUCHES			5	.598	39	.595	7	.592
8	.601	.597				6	.598	40	.595	8	.592
9	.602	.599	62	.598	.599	7	.598	41	.597	9	.592
10	.602	.596	63	.602	.601	8	.597	42	.597	10	.594
11	.599	.598	64	.603	.599	9	.598	43	.596	11	.594
12	.596	.598	65	.602	.596	10	.597	44	.595	12	.594
13	.598	.597	66	.602	.595	11	.597	45	.595	13	.593
14	.599	.597	67	.606	.597					14	.593
15	.600	.597	68	.607	.596	HUB. AVAL		HUB. DROIT		15	.593
16	.600	.596	69	.607	.597	1	.601	1	.600	16	.593
17	.601	.596	70	.609	.595	2	.602	2	.600	17	.593
18	.603	.603	71	.604	.595	3	.601	3	.600	18	.593
19	.603	.597	72	.602	.598	4	.602	4	.600	19	.593
20	.604	.596	73	.592	.600	5	.601	5	.600	20	.593
21	.604	.595				6	.601	6	.600	21	.593
22	.606	.596	PRISES LAT. DROITES			7	.601	7	.600	22	.593
23	.608	.595				8	.601	8	.600	23	.593
24	.608	.595	74	.599	.601	9	.602	9	.600	24	.593
25	.608	.594	75	.600	.598	10	.601	10	.600	25	.593
26	.607	.594	76	.601	.597	11	.599	11	.600	26	.593
27	.611	.593	77	.598	.596					27	.593
28	.611	.595	78	.599	.594	HUB. GAUCHE		12	.600	28	.593
29	.615	.595	79	.602	.593	1	.603	1	.600	29	.593
30	.613	.596	80	.609	.592	2	.602	2	.600	30	.593
31	.616	.593	81	.613	.594	3	.603	3	.600	31	.593
32	.613	.596	82	.611	.591	4	.602	4	.600	32	.593
33	.615	.595	83	.615	.591	5	.603	5	.600	33	.593
34	.612	.594	84	.621	.593	6	.602	6	.600	34	.593
35	.613	.594	85	.621	.593	7	.603	7	.600	35	.593
36	.613	.594	86	.619	.593	8	.603	8	.600	36	.593
37	.615	.593	87	.617	.593	9	.607	9	.600	37	.593
38	.615	.593	88	.615	.592	10	.609	10	.600	38	.593
39	.616	.593	89	.619	.592	11	.619	11	.600	39	.593
40	.614	.594	90	.614	.594	12	.607	12	.600	40	.593
41	.613	.594	91	.607	.595	13	.605	13	.600	41	.593
42	.613	.595	92	.605	.595	14	.606	14	.600	42	.593
43	.611	.595	93	.600	.596	15	.604	15	.600	43	.593
44	.603	.595	94	.602	.596	16	.601	16	.600	44	.593
45	.607	.595	95	.609	.596	17	.600	17	.600	45	.593
46	.604	.596	96	.601	.599	18	.600	18	.600	46	.593
47	.606	.596				19	.600	19	.600	47	.593
48	.605	.596				20	.600	20	.600	48	.593
49	.605	.597				21	.600	21	.600	49	.593
50	.602	.597				22	.600	22	.600	50	.593
51	.603	.598				23	.601	23	.600		
52	.601	.598	PRISES COL			24	.601	24	.600		
53	.601	.598				25	.600	25	.600		
54	.600	.597	1.061	1.057		26	.603	26	.600		
55	.600	.595	1.064	.995		27	.604	27	.600		
56	.597	.593	1.099	.794		28	.606	28	.600		
57	.594	.591	1.065	.631		29	.607	29	.600		
58	.589	.600	1.023	.622		30	.608	30	.600		
						31	.607	31	.600		
						32	.600	32	.600		

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ADAPTATIONS
TESTS WITH THREE-DIMENSIONAL ADJUSTMENTS IN THE RECTANGULAR
WORKING SECTION OF THE FRENCH T2 WIND TUNNEL, WITH AN
TYPE AS 07-TYPE SWEPT-~~BACK~~ WING^{HALL} MODEL INSTALLED

A. Blanchard, M. J. Payry, J. F. Breil

Translation of "Essais 'd'adaptation tridimensionnelle' de la
veine rectangulaire de la soufflerie T2, en presence d'une
maquette d'aile en fleche du type AS 07," Rapport Technique OA
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TESTS WITH THREE-DIMENSIONAL ADJUSTMENTS IN THE
RECTANGULAR WORKING SECTION OF THE FRENCH T2
WIND TUNNEL WITH AN AS 07-TYPE SWEPT-BACK WING
MODEL

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The results obtained on the AS 07 wing and the working
section walls for three types of configurations are reported. The
first, called non-adapted, corresponds to the divergent upper and
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It can serve as a basis for complete flow calculations. The second
configuration corresponds to wall shapes determined from calcula-
tions which tend to minimize interference at the level of the
fuselage. Finally, the third configuration, called two-dimensional
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case was tested to determine the influence of wall shape and
error magnitude. These results are not sufficient to validate the
three-dimensional adaptation; they must be coordinated with
calculations or with unlimited atmosphere tests.

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ACCO

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NASA TECHNICAL MEMORANDUM

NASA TM-88442

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ADAPTATIONS
TESTS WITH THREE-DIMENSIONAL ADJUSTMENTS IN THE RECTANGULAR
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TYPE AS 07-TYPE SWEEP ~~WING~~ WING MODEL INSTALLED

A. Blanchard, M. J. Payry, J. F. Breil

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adaptation

NOTATION

$\left. \begin{array}{l} X_p \\ Y_p \\ Z_p \end{array} \right\}$ Cartesian coordinates in the reference working section
 (porthole axis)

$\left. \begin{array}{l} X \\ Y \\ Z \end{array} \right\}$ Cartesian coordinates in the wing reference (leading edge to socket)

C Profile chord of the wing section considered

α Angle of the model (fuselage axis)

M_o ~~Infinite Mach~~ ^{Test} ~~upstream of the flow~~ ^{number} ~~number~~

M Local Mach (wing or wall)

$$K_p = \frac{p - p_o}{\frac{1}{2} \rho V_o^2} \quad \text{Pressure coefficient}$$

C_z Local or complete-wing lift coefficient

$$\left\{ \begin{array}{l} C_z \text{ local} = \int_{\text{profil}} K_p \cdot d\left(\frac{x}{C_{\text{local}}}\right) \\ C_z = \frac{F_z}{\frac{1}{2} \rho V_o^2 \cdot S_{\text{aile}}} \end{array} \right.$$

ADAPTATIONS
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TYPE AS 07 ~~TYPE~~ SWEPT-BACK WING MODEL INSTALLED.

A. Blanchard, M. J. Payry, J. F. Breil

1 - INTRODUCTION

/7*

This test series follows a study done in the T2 wind tunnel with the goal of defining a shape for the adaptable walls which would minimize their influence on three-dimensional ~~objects~~ ^{models} placed in the center of the ^{test} section or fastened on the sidewall.

flow flow
The present configuration of the working section does not allow obtaining a shape ^{to be set which are} identical to that of the layer of the ^{streamlines} ~~current~~ existing around a three-dimensional model in unlimited ^{fixed} atmosphere (two completely ~~rectilinear~~ ^{fixed} and parallel lateral walls, two flexible and bendable upper and lower walls). The planned solution thus consists of using the two bendable walls to minimize the influence of the walls on the model. ^{unconfined}

The method implemented uses solutions developed by "E. Wedemeyer and L. Lamarche" [5]. A first series of tests was done in cooperation with the ^{technical} University of Berlin on various existing models [6]:

- a C5 revolving body 166 mm long, 0.3% blockage;
- a civil F4 airplane model with 120-mm wingspan and three-component balance;
- a duck-type military airplane model with the same balance.

Another series of tests was then done on a bigger model [7]:

- a C5 body 400 mm long, 1.8% blockage.

*Numbers in the margin indicate pagination in the foreign text.

The results and calculations were compared.

The calculation method was optimized for revolving bodies of revolution placed in the center of the ^{test} section; an extrapolation was tried which placed a half-wing at the wall. In this case, calculations are done as if the section were twice its actual width, using the Mach distribution at the wall measured near the plane of symmetry.

The results obtained on the "16/1000-scale" AS 07 are discussed in this report. They can be divided into two groups: control tests and systematic tests.

Included in the first group is control of wing angling by rotating the walls. The ^{power} path of the jacks would not permit the displacements ~~required by calculation~~ for ~~angling the model to~~ ^{flow angle} ^{low angle} ^{angle of attack of} $+2^\circ$; we thus used this "artificial" method after ~~having verified~~ ^{ed} its validity.

The three-dimensional adaptation method supplies the ^{own} optimal shape of the walls from the first calculation, whatever the initial position of the walls; this was verified in 18 several test configurations. Finally, an adaptation called ^{2D} "two-dimensional" was tested; it uses the normal method for ~~2D~~ ^{model} profile tests. This case, without theoretical justification, was tried to see the influence of the ~~shape of the walls~~ ^{shapes} and the ~~size of errors which can be made.~~ ^{magnitude of the corresponding interferences}

The second part of this study corresponds to systematic tests: four configurations were chosen which gave different lift coefficients, without making highly supersonic zones appear on the profiles. For each configuration, three wall positions were tested:

- The first, called "unadapted," corresponds to the upper and lower divergent ~~rectilinear~~ walls compensating for

boundary
boundary

thickening of the ~~limit~~ layers; it served as our basis for beginning three-dimensional adaptation calculations. These particularly simple limit conditions can also be used for complete calculation of the flow in the working section.

- The second wall shape comes from the three-dimensional adaptation calculation; the flexible ^{walls} sheets are positioned before the ~~gust~~ tunnel is ^{run} run.
- Finally, the last case corresponds to "two-dimensional adaptation"; the iterative process converges ⁱⁿ on a single ~~gust~~ tunnel ^{run} run.

For each type of test, three ^{tunnel runs} gusts are necessary to obtain readings from the six rows of pressure recorders spread along the AS 07 wing.

The experimental results gathered during this series are not sufficient to validate the three-dimensional adaptation method used. Additional calculations must be made to estimate residual corrections. In these tests, ^{the small} a negligible influence of the walls is observed for low lift values or low Mach numbers; inversely, for 2 degrees of incidence or for Mach 0.8, the ~~influence~~ become significant and can in part be interpreted as variations in aerodynamic incidence.

2 - ADAPTATION PRINCIPLE

^{unconfined} The purpose of the adaptable walls is to create an unlimited flow around a model, in a working section with finite dimensions; this can be done by controlling the wall conditions, either by their shape in the case of solid walls or by flows of mass through porous walls. The first solution has been chosen at T2, where flexible sheets moved by jacks form the upper and lower ^{walls} plates of the working section [3].

meaningful flow

In the case of a three-dimensional body, it is necessary to bend the walls located around the model to arrive at a shape *corresponding* near ~~the layer of current~~ ^{to a streamtube} existing around the model in ~~unlimited~~ ⁱⁿ atmosphere. This solution is not at present possible ~~at~~ ⁱⁿ T2, but on the other hand it is possible to use the two flexible 19 walls to minimize residual corrections due to the influence of the walls on the ~~object~~ *model*.

2.1 Two-dimensional adaptation

The details of the process will be found in [2] and [4]; it uses a coupling between the real flow in the working section (internal field) and a calculated ^{imaginary} ~~virtual~~ flow outside the wind tunnel (external field). Coupling occurs on a control surface near the walls through speed vector components. Adaptation is achieved by an iterative process acting on the shape of the walls: the components of ^{velocity} ~~the speed~~ ^{at} on the control surface ~~becomes~~ available at each iteration; they are extrapolated from the pressure measurements at the wall. The velocities needed on the control surface to achieve an unlimited external flow are calculated by the Green function following an inverse method. A method of optimized relaxation between the internal and external flows for the vertical velocity component, followed by an integration along each flexible wall, supplies the new shape of the wall. The real shape needed is obtained by adding the thickness displacement of the four wall limit layers.

2.2 Three-dimensional adaptation

For three-dimensional adaptation, the process is different [5]: it uses ^{a representation} ~~schematization~~ of the model ^{by} a distribution of sources and vortices in a narrow horseshoe, placed on the ^{test} section axis. This ^{centerline} ~~schematization~~ ^{representation} ~~gives~~ ^{is} a good ^{approximation} ~~representation~~ of axisymmetrical bodies mounted in the middle of the working section. *centerline*

The originality of the method lies in then doing a linear transformation, which permits passing directly from distribution of velocities at the walls to the adapted form without needing to determine the intensity of singularities. The optimized shape of the walls is thus theoretically obtained from the first calculation; this shape, which is not exactly "adapted," minimizes residual corrections on the model caused by the influence of the walls.

Using this method for a half-wing at the wall is ^{not quite} ~~correct~~ abusive, because the ^{basic representation} ~~base schematization~~ does not ^{rearrange} represent a wingspan; it has nonetheless been tried here by replacing the ~~one~~ lateral ^{sidewall} ~~door~~ by a plane of symmetry leading to a ~~fictional~~ ^{fictitious} double section width, and taking the Mach distribution of the flexible walls near the plane of symmetry as reference. ^{fictitious}

3 - EXPERIMENTAL EQUIPMENT

The T2 transonic wind tunnel ^{can be} ~~is~~ ^{ed} pressurizable and can function at low temperatures; only minimum-pressure and ambient-temperature tests were ~~done~~ ^{used} during this series.

3.1 Working section equipment

/10

The working section has an almost square section of $0.39 \times 0.37 \text{ mm}^2$ at the entrance. Flexible sheets of Invar make up the upper and lower walls, equipped with three rows of pressure recorders whose coordinates are given in figures 7 and 8. The ~~sheet~~ ^{wall}-positioning mechanism is described in [2], [3], and [4].

The left lateral ^{sidewall} ~~door~~ ^{sidewall} has three portholes with pressure recorders placed along horizontal and vertical lines whose coordinates are shown in Figures 7 and 9.

The pressure recorders are linked to ~~the~~ Scanivalves, each of ~~whose head~~ ^{which} can observe 48 positions in 5 seconds.

The position of the wing in the working section is given in figure 6.

The Mach number of the flow is set by a ~~second neck~~ ^{secondary throat} ~~throat~~ ^{secondary throat} controlled by the computer which controls the ~~gust~~ ^{gust} tunnel run.

No other equipment or wind tunnel measurement method ~~were~~ was used.

3.2 Mounting the wing

The AS 07 ^{half-} wing model with a scale of "16/1000" is shown by the photographs in figure 5. The method of mounting the wing on the wall is shown (figure 6), the plane of the wing and its specifications are given (figures 10 and 11), and the shape of the profiles ^{at different spanwise locations are shown} ~~which compose it~~, and the positions of the pressure recorders are indicated (figures 12 and 13).

^{at different spanwise locations are shown}

There are six rows, each with 16 recorders on the inner and outer sections and one on the leading edge; they are placed across the wingspan so as to form lines with constant chord percentages. These recorders communicate with tubes placed in grooves along the wingspan; each tube communicates with three recorders (either on the external wing or on the internal wing). When one of the three rows of recorders is used to measure pressure, the other two are covered with thin (0.05-mm) adhesive strips. It is thus possible to simultaneously measure pressure on two sections of the wing (one internal and one external); measurement of velocities over the entire wing thus requires three different ~~gusts~~ ^{runs} tunnel runs.

The wing is mounted on a half-fuselage linked to a porthole, whose rotation ~~ensures the angling of the wing-~~

^{which rotates} ~~ensures the angling of the wing-~~ ^{so to change the angle of attack of}

fuselage assembly; the angular reference is the ^{straight} ~~rectilinear~~ part on the back of the fuselage [1].

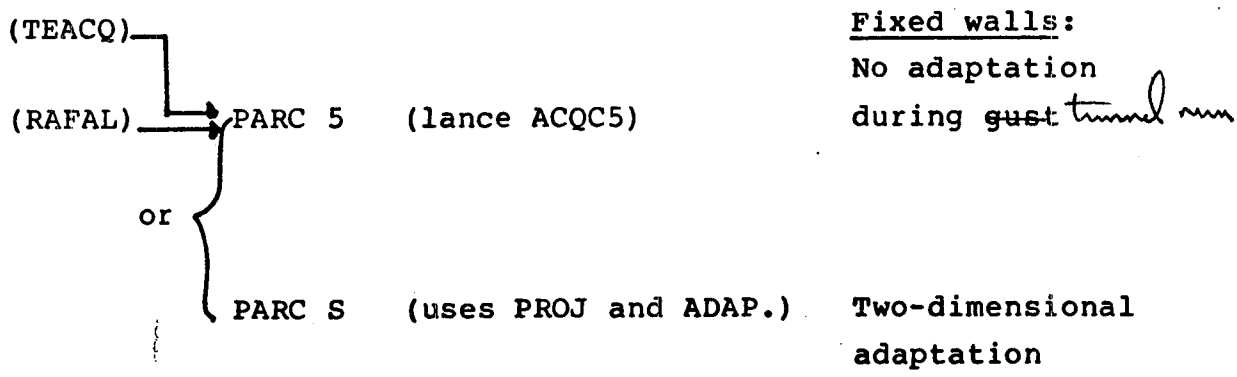
3.3 Acquisition and examination programs ^{graphics}

The T2 wind tunnel is linked to a team of two computers, one concerned with creating and ^{controlling} ~~regulating~~ the ^{tunnel run} ~~gust~~ and the other with obtaining data and storing measurements to disk at the end of ^{each} ~~the~~ ^{tunnel run} ~~gust tunnel run~~.

These tests are ^{similar} ~~pursuant~~ to the series done on the /11 C5 body and use its principal elements.

Disk cartridge LU 26, Program
LU 34, Test files, calculation files

Acquisition program



Initialization of programs { with (TR,) RINC 5 (For PARC 5)
or (TR,) RINC S (For PARC S)

Test file

AD --- test number from AD 100 to AD 173

Wall positioning file

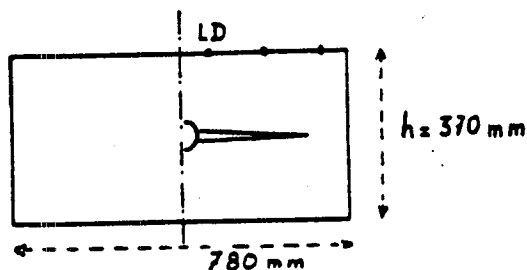
- any test file AD---
- or calculation file AD 9 ---
- or special file { AD 4: Divergent ~~rectilinear~~ walls ^{of inth} ~~symmetrical~~ ^{boundary} limit layers.
- AD 444: AD 4 + 10' ^{axis} rotation upward
- AD 445: AD 4 + 30' ^{axis} rotation upward

Three-dimensional adaptation calculation

Calculation from a test file AD ---

VKJ 43 Calculation of wall shapes without rotation

VKI M Calculation of wall shapes with rotation



- section length 780 mm
- ratio $c = h/b = 2.1081$
- reference recorders:
right lateral RL
- weighting coefficients
file VKJ - R (cartridge
LU 43)

→ Filing to disk

File for new calculated wall shapes

AD 9 --- beginning test number for the calculation

Programs for examination of AD--- files

LTCS:

- graphs local profile Mach numbers
- graphs K_p
- lists AD file
- calculates C_z

LTC 51:

- graphs wall Mach numbers
- graphs wall shapes
- starts LTC 52 (does an RP, LTC 52)

LTC VK:

- graphs only wall shapes calculated by VKI 43 or VKIM (from AD 9---).

4 - SUMMARY OF TESTS PERFORMED

A previous study was done on the AS 07 wing [1]. We verified in one case that the same results would occur, although the working section was modified when the T2 wind tunnel was *modified* adapted for cryogenics.

The first control tests were done by measuring rows 2 and 5 of pressure recorders for the Mach numbers and incidences indicated below:

α \ M_0)		
	0,6	0,7	0,8
(+2°	X	X	X
(0	X	X	X
(-2°	X	X	

Four configurations were selected for systematic tests: /13

$\alpha \backslash M_0$	0,6	0,7	0,8
+2°	X		
0°	X		X
-2°	X		

They correspond to a sampling of lift coefficients and ~~to an~~ ^{numbers} infinite Mach effect ^{numbers} upstream, while limiting the supersonic zones which appear on the profiles.

Figure 1 shows the list of tests in chronological order, and figures 2, 3, and 4 classify them by configuration.

We first showed that rotation of the upper and lower walls was equivalent to ^{changing the angle of attack of} angling the model at the same ^{geometric} angle. This ^{technique} ~~artifice~~ was made necessary because the ^{power} path of the jacks did ^{power} not permit the displacements required by calculation of three-dimensional adaptation for a model incidence of +2°.

- Divergent rectilinear walls

α accid.			M_0	
	α Display	Wall Start	0,6	0,8
+2°	+2°	AD 4	AD 120	
	+1,5°	AD 445	AD 122	
0°	0°	AD 4	AD 107 - AD 109	AD 108 - AD 132
	-0,5°	AD 445	AD 137	AD 139

		M_0	
$\alpha_{a\acute{e}rod.} = 0^\circ$	α CALCUL	0,6	: 0,8
	0° VKI 43	117	: AD 119
	-0,5° VKI M	138	: AD 141

The three-dimensional adaptation method theoretically supplies the optimal ^{sum} shape of the walls from the first calculation, whatever the initial position of the flexible ^{walls} sheets. ^{Tests} Controls were done in this respect for the following configurations:

		M_0	
α <i>(display)</i>		0,7	: 0,8
+1,5°			: AD 127 (1) : AD 128 (2) : AD 129 (3)
0°	AD 115 (1) AD 116 (2)		: AD 118 (1) : AD 119 (2)
-0,5°			: AD 140 (1) : AD 141 (2)

The figure in parentheses after the file number indicates the order of the iteration; the wall-positioning file thus results from calculation of the preceding test. (Iteration (0) is the test done with ~~rectilinear~~ ^{straight} walls.)

We also verified that the tests called "two-dimensional adaptation" converged rapidly, as is the case for the ^{2D model} profile ^{2D Model} tests; it is sufficient ~~for that~~ to compare the wall positions of

the 3rd and 4th iterations, ^{performed} ~~done~~ during the same ~~gust~~; the two positions are always close. In general, the beginning shape chosen is near the adapted shape, but we have tested this convergence in the two particular cases when the beginning shape was far from the adapted shape. The beginning file chosen was AD 4: ~~rectilinear walls divergent from limit layers and symmetrical.~~ ^{straight} ~~symmetrical.~~ ^{performed} ~~symmetrically~~ ^{tunnel run} ~~tunnel run~~ ^{for boundary layers.} ~~for boundary layers.~~

/15

Configuration: $Mo = 0.7 \quad \alpha = +1.5^\circ$ File AD 130 (1)
Configuration: $Mo = 0.8 \quad \alpha = 0^\circ$ File AD 133 (1)
followed by File AD 134 (2)

Comparisons were made between the various wall positions; they are noted:

- "Non," for divergent ^{straight} rectilinear walls
- "2D," for two-dimensional adaptation done with the PARCS program
- "3d," for positioning of the walls in the shape calculated by the VKI 43 or VKI M program

It was decided to do systematic tests for the three cases of "adaptation," the non-adapted case serving as a basis for three-dimensional calculation (any wall shape will work); this case can also serve as a basis for complete flow calculations, because here the limit conditions are particularly simple. The two-dimensional adaptation, ~~is not~~ ^{beyond} ~~outside~~ the subject of the study, was systematically tested to use as a comparison with the ^{assumed} optimal shape.

Finally, four configurations for three cases of adaptation, reproduced three times to have the velocity field on all of the wing, were tested; these 36 ^{tunnel runs.} gusts make up the systematic tests listed in figure 26a.

5 - CONTROL TESTS

We will not present all the tests done, but only a selection of cases judged most interesting, since the goal of this series ^{was} ~~is~~ not to evaluate the AS 07 wing.

5.1 Angling by wall rotation *Change of flow angle* *change of flow angle*

Of the five configurations tested (^{section} paragraph 4), three are presented. The first corresponds to $Mo = 0.6$ and $\alpha = +2^\circ$ for ~~rectilinear~~ ^{straight} walls (figure 14); this is the configuration which obliged us to use this ^{technique} ~~artifice~~, as the three-dimensional case could not be tested.

Figure 15 shows the comparison of Mach numbers on the walls and on the wing, for an aerodynamic incidence equal to 0° and a Mach number equal to 0.8, in the case of ~~rectilinear~~ ^{straight} walls. Figure 16 presents the same configurations but for wall shapes coming respectively from ^{3D} ~~2D~~ calculations VKI 43 and VKI M.

The results of figures 14 and 15 show that the high Mach case is the most ^{interesting} ~~recordable~~, but the ^{quality} ~~correspondence~~ of the tests remains good. Figure 16 shows that the VKI M calculation makes perfect allowance for ^{axis} ~~total~~ rotation.

It is thus possible to ^{set} ~~display~~ a model incidence /16 different from that desired and to compensate by rotating the walls.

5.2 Convergence of iterations *Adaptation*

5.2.1 Three-dimensional adaptation

Several calculations for optimization of wall shape were ^{made} ~~connected~~ for one configuration. The last test is always recalculated, leading to a wall shape which by definition

will not be used, but which will in fact constitute an additional iteration.

Of the four tested cases, two are presented in figures 17 and 18; the first ($M_o = 0.7$ and $\alpha = 0^\circ$) shows that the adapted shape is practically obtained from the first iteration; in the second case--much more difficult ($M_o = 0.8$ and $\alpha = +2^\circ$)--it is necessary to wait for the second calculation. This second case corresponds to a ~~freely~~ *influenced by the ?* supersonic regime of the wing which will not be studied systematically herein.

5.2.2 Two-dimensional adaptation

In all tests done, the 3rd iteration is always identical to the 4th and last iteration of the ~~test~~ ^{tunnel run}, even when the upper and lower walls have been prepositioned in a shape very different from the "adapted" shape. This is the case shown in figure 19 corresponding to $M_o = 0.8$ and $\alpha = 0^\circ$.

To confirm the validity of this statement, a second test was done, positioning the flexible ~~sheets on the~~ ^{walls} preceding shapes; the values obtained can thus be considered to correspond to the 4th, 5th, 6th, and 7th iterations of the test; they are all identical (figure 20), which confirms that the convergence was well obtained.

5.3 Non/2-D/3-D comparison

Two cases are presented here, one of which is not part of the systematic tests:

- $M_o = 0.7$ $\alpha = 0^\circ$
- $M_o = 0.8$ $\alpha = 0^\circ$

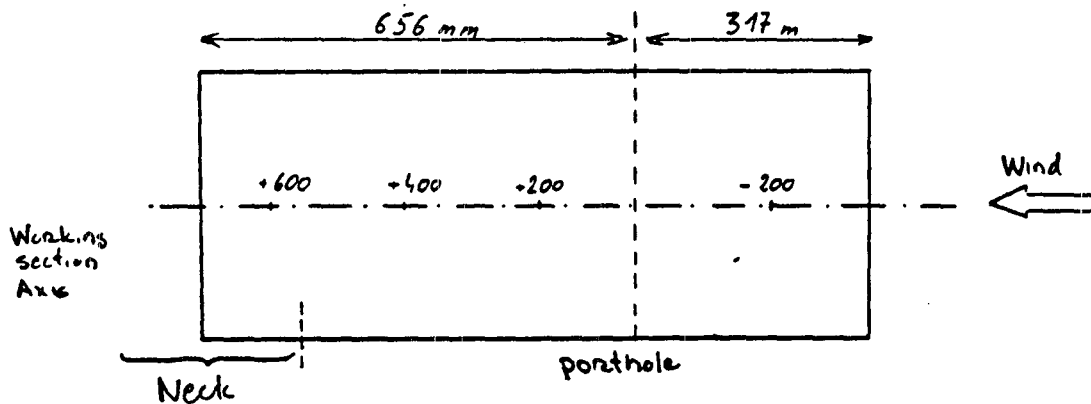
The ^{differences} gaps, observed following the ^{various} types of "adaptation" ~~will~~ become more significant as lift ^{and} Mach number ~~upstream~~ increase. The adaptation called "two-dimensional" gives results nearer to the non-adapted case; in fact, everything happens as if the aerodynamic incidence of the two-dimensional case were higher than that of the tests with a wall shape adapted in three dimensions. On the other hand, ^{straight} ~~rectilinear~~ walls lead to a higher effective Mach number upstream (blockage effect).

In the first case (figure 21), the ^{differences} gaps are moderate; they are more significant in the second case (figure 22). Observation of the ^{slope} ~~direction~~ of the walls leaving the ^{contraction} ~~convergent~~ (figure 21) shows that, effectively, the direction of the flow upstream is no longer horizontal in the "2-D" case, unlike the "3-D" case; the angular reference was given by the "non-adapted" case. The effect produced is ^{indisputable} ~~incontestable~~, because we /17 previously demonstrated that rotation of the walls ~~assembly~~ modified the aerodynamic incidence of the model; however, this is not sufficient to prove that the 2-D case is ^{in error} ~~erroneous~~, because the direction of the ^{stream} ~~current~~ lines in ~~unlimited~~ the ^{unconfined flow} ~~unconfined~~ atmosphere ^{are} ~~is~~ not known. We note also the very different shapes of the walls downstream; they go downward for the "3-D" cases, which is logical allowing for the chosen ^{schematization} ~~representation~~ (horseshoe vortex) and the calculation made (in the plane of symmetry). But once more, that does not prove that the shape obtained is optimum.

Finally, one can observe on the last figure (23) that the effect ^{at} ~~produced by~~ modifying the shape of the walls is not constant across the wingspan. This was predictable due to the working section geometry itself, allowing for twist of the wing and for three-dimensional effects.

5.4 Visualizations

For three configurations, oil visualizations were done on the left ^{sidewall} ~~door~~ of the working section, giving the direction of the ^{stream} ~~current~~ lines 55.4 mm from the end of the wing. Reference marks were made, making it possible to locate the positions relative to the ^{stream} ~~current~~ lines and to measure their deviations.



The end of the wing is located between the abscissas 91.06 mm and 135.86 mm from the porthole (figure 6) and very near to the section axis (function of the incidence).

The maximum deviations noticed are located on the ^{test} section axis slightly behind the tip of the wing (figures 24, 25, and 26).

Mo	α	Walls	δ_{max}
0,6	+2°	"Non-adapted" AD 4	(5°.....6°)
0,6	+2°	'Adapted 2-D	(5°.....6°)
0,6	-2°	"Non-adapted" AD 4	~ 0,5°

Figure 24

Figure 25

Figure 26

The photos taken from behind clearly show the deviations of the ^{stream}current-lines.

/18

6 - SYSTEMATIC TESTS

For the 36 ^{tunnel runs}gusts that made up the systematic tests (paragraph 4 and figure 26a), the following information is given: wall shape (figures 27 and 28), Mach numbers of the three rows of recorders on the adaptable walls (figures 29, 30, 31, and 32), Mach numbers of the left lateral ^{side wall}door (figures 33, 34, 35, and 36) following the horizontal axis or the three verticals, and finally spread of Kp on the AS 07 wing (figures 37 to 44).

Numerical values for these curves are given in the attached test listings. File numbers corresponding in chronological order to the experiments were kept in the interests of clarity.

Here will be found a systematic comparison of the three cases of adaptation--"Non/2-D/3-D"--and their influence on the ^{velocity}speed distributions. ^{velocity}whose principal characteristics ^{of which}were seen in paragraph 5.3.

Finally, integration of Kp for each section supplies local lift coefficient Cz. The values are tabulated in figure 45; they were traced along the wingspan of the various configurations tested (figures 46 and 47). It is observed that the internal wing changes less rapidly than the external wing with incidence (figure 46) or, ^{test}Mach number ^{upstream} (figure 47).

On the other hand, the ^{difference}between the "non-adapted" and adapted 3-D" cases increases with the lift.

Local C_z s were multiplied by the chord of the profile in the section considered; the product $C_z \cdot C$ represents local /19 contribution to wing lift. The values obtained were traced in this representation (figures 48 and 49); this weighting modifies the appearance of the curves ("elliptic" distribution plane), but the observed tendencies are the same.

Finally, integration of the curves in this last representation supplies the overall lift coefficient of the wing, which ^{is} was reported as a function of incidence (figure 50). We have also reported the lift measured during the preceding series [1], ^{performed} done between ^{straight} rectilinear walls for a Mach number upstream of 0.47. The effect of compressibility is felt more as supersonic zones develop on the wing.

- CONCLUSION

This series of tests on the AS 07 wing is ^{recorded} registered as a study on three-dimensional adaptation of the T2 wind tunnel. It uses the two flexible walls to minimize residual corrections in the presence of a three-dimensional model. It implements the "E. Wedemeyer and L. Lamarche" method where ^{the representation} schematization of the model by a distribution of singularities adequately represents an axisymmetrical body. Extrapolation of these methods in the case of a half-wing ^{model mounted on the sidewall} at the wall has no ultimate goal; it serves merely as a preliminary phase, to observe the influence of wall shape ^{on} in various sections of the wing, to study the convergence of the method, and to make adjustments ^{to} (rotation of walls, incidence, etc.).

On the other hand, these experiments can serve as a basis for calculating potential three-dimensional flow around the model. Then, a three-dimensional ^{test} object placed in the section ^{model}

theoretically
theoretically represented
could be more elaborately ~~schematicized~~; it would lead to development, as for axisymmetrical bodies, of a method of adaptation minimizing the influence of the walls on the model.

At present, it is difficult to know if the shape called "adapted 3-D" is nearer to the values of ~~unlimited atmosphere~~ *unconfined flow* than the shape "adapted 2-D," but it is definitely not the optimum shape.

The tests will ~~next~~ *continue with* be completed by directional ~~limit~~ *boundary* layer ~~layer~~ *boundary* ~~readings~~ *measurements* on the lateral ~~wall~~ *side* at the level of ~~the end~~ *with* of the wing tip. The direction of the ~~current~~ *stream* lines in this area will be an important element in the reality-calculation comparisons

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PAPER 14

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- 2-D
- 3-D 32

side

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