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SUMMARY

A 1/8-scale model of the X-29A airplane was tested in the Ames 12-Foot Pressure Wind Tunnel at a Mach number of 0.20 and Reynolds numbers of 0.13×10^6 to 2.00×10^6 based on a fuselage forebody depth of 0.4 ft. For the test series presented herein, the angle of attack ranged from 40° to 90° and the angle of sideslip ranged from -10° to 30° for the erect attitude. Tests with the model inverted covered angles of attack from -40° to -90° and angles of sideslip from -30° to 10°. Data were obtained for the basic design and for several forebody strakes. An alternate forebody design was also tested. The results provided information for selection of forebody strakes for compensation of Reynolds number effect on the 1/25-scale free-spinning model tested in the Langley Spin Tunnel.

INTRODUCTION

Reynolds number effects on the high angle of attack, crossflow characteristics of a fuselage forebody on a small-scale model can cause appreciably different side forces, yawing moments, and pitching moments from those obtained on a full-scale airplane. (See refs. 1 and 2.) In the course of conducting free-spinning investigations in the Langley Spin Tunnel on small-scale models, the Reynolds number effects for some configurations have been so marked that the spin recovery characteristics determined from model tests were not representative of the full-scale airplane. The F-5A airplane, which has essentially the same forebody as the X-29A, exhibited these effects. (See ref. 3.)

Spinning is an aerodynamic phenomenon in which dynamic forces and moments are extremely important. Methods for the prediction of Reynolds number effects on dynamic data are, however, very limited at best, so experimental methods are employed to develop the necessary information. Typically, a wind-tunnel Reynolds number investigation is conducted to determine whether there are Reynolds number effects on the static data which could significantly influence the spin-tunnel results. When such effects are identified, various forebody modifications are tested on the model in an attempt to make the pertinent data at low Reynolds numbers representative of data at high Reynolds numbers. Such information is then used to design a forebody modification to be used on the spin-tunnel model.

In this investigation, a 1/8-scale X-29A forward-swept-wing airplane model was tested in the Ames 12-Foot Pressure Wind Tunnel to determine static longitudinal and lateral-directional aerodynamic characteristics over a range of Reynolds number from subcritical to supercritical conditions. The angle-of-attack ranges tested were 40° to 90° and -40° to -90°. The corresponding angle-of-sideslip ranges tested were -10° to 30° and 10° to -30°, respectively.

The approach used in this study was to identify the Reynolds number effects on the basic configurations and then to conduct tests using the component buildup technique to isolate the source of the effects. On the basis of this information, tests were conducted on various forebody modifications, including strakes and an alternate forebody shape, to give the desired results. The data are presented with minimum analysis and discussion.

BL		butt-line station
C_A		body-axis axial-force coefficient
C_l		body-axis rolling-moment coefficient
C_m		pitching-moment coefficient
C_N		body-axis normal-force coefficient
C_n		body-axis yawing-moment coefficient
C_Y		body-axis side-force coefficient
$\bar{c}$		wing reference chord, in.
FS		fuselage station
L,R		left, right
q	(Q in computer-generated appendix)	dynamic pressure, psf
R_N	(RN in computer-generated appendix)	Reynolds number per foot
$\bar{V}$		free-stream velocity
WL		waterline station
x,y,z		body axes
α	(ALPHA in computer-generated appendix)	angle of attack, deg
β	(BETA in computer-generated appendix)	angle of sideslip, deg
δ_a		left or right flaperon deflection, deg
δ_c		left or right canard deflection, deg
δ_R		rudder deflection, deg
δ_s		strake flap deflection, deg

TEST FACILITY

The Ames 12-Foot Pressure Wind Tunnel is a variable-density, low-turbulence, continuous-flow wind tunnel that operates in the Mach number range of 0.10 to 0.94. The wind tunnel is powered by a two-stage, axial-flow fan driven by electric motors

2

totaling 12 000 hp. Airspeed in the test section is controlled by varying the rotation speed of the fan. Eight fine-mesh screens in the settling chamber, together with a contraction ratio of 25:1, provide an airstream of exceptionally low turbulence level.

MODEL DESCRIPTION

The model was a 1/8-scale version of the X-29A airplane. The geometry of the model is given in table I and figure 1, and model-sting installation is shown in figure 2. Details of the forebody strakes are shown in figures 3 and 4, and the alternate forebody is shown in figure 5. Photographs of the model are shown in figure 6.

The X-29A airplane is a forward-swept-wing flight-demonstrator aircraft designed by the Grumman Aerospace Corporation for the Defense Advanced Research Projects Agency. In addition to incorporating a forward wing sweep of 29.3°, geometric features include horizontal canard control surfaces capable of symmetric and asymmetric deflections of the left- and right-hand surfaces; twin side-mounted external compression inlets with a bifurcated internal-flow duct feeding a single engine with the engine nozzle at the rear of the fuselage; strakes mounted on the side of the fuselage aft of the wing-body juncture, including trailing-edge deflectable strake flaps; single centerline-mounted vertical tail and rudder; and wing trailing-edge flaps, flaperons, and ailerons. The canards, rudder, fuselage strakes, and wing trailing-edge flaps on the model have deflection capabilities for determining the control effectiveness of these surfaces. The canards incorporate independent remote-control actuation for deflections ranging from -60° to +30°. The cruise wing trailing edge incorporates double-hinged ailerons and flaperons, and control-surface deflections are variable as a result of using common-flap-segment hardware. Simulated flap actuator fairings provide structural support for the control surfaces. Individual mounting brackets are used to provide rudder and strake flap deflection capability.

The cruise and maneuver wings have common geometries from the root out to BL 64 (39-percent span), with the exception that the maneuver wing has a smooth cambered trailing edge. The outboard panels of the cruise and maneuver wings differ only in twist and trailing-edge design.

Boundary-layer transition strips were not applied for this test. The forward fuselage section is removable at FS 283 and was modified to incorporate Langley designed lateral and ventral strakes. Model mounting at the aft end required a deviation from the true aircraft contours to accommodate the sting.

INSTRUMENTATION

Model forces and moments were measured with a six-component strain-gage balance. Prior to the test, static loads in each plane and combined static loads were applied to the balance to simulate the range of loads and center-of-pressure locations anticipated during the test. Remote actuation of the canards was accomplished by means of a control console located in the tunnel control room and two standard feedback potentiometers (one per canard) mounted within the model. Potentiometer output

was indicated on a digital voltmeter in the control console. An angle-of-attack transmitter was installed within the model and was used for primary angle-of-attack measurements.

TESTING AND PROCEDURE

The investigation was performed at a Mach number of 0.20 over a range of fuselage-forebody depth Reynolds numbers from 0.13×10^6 to 2.00×10^6. Data were obtained at angles of attack from 40° to 90° and at angles of sideslip from -10° to 30°, with the model erect and rolled 180°.

Forces and moments were sensed by an internally mounted six-component strain-gage balance. No axial-force corrections were applied for base and cavity pressure. An angle transducer mounted on the support system was used to measure model angles of attack. The effects of control-surface deflections were investigated.

DATA REDUCTION

The six-component force and moment data were reduced about the model moment reference center in the body-axis system. The axis system is defined in figure 7, and the moment reference center was at $-0.05\bar{c}$, FS 56.78, WL 8.25, BL 0 (full scale: FS 454.27, WL 66, BL 0). The balance center was at FS 56.78, WL 8.96, BL 0. The model was sting-mounted on a turntable in the test-section floor; therefore, angle of attack and angle of sideslip could be varied. For any specific sting-support arrangement, the model angle of attack could be varied 50°, and angle of sideslip could be varied 40°. Angle-of-attack measurements were made using an angle-of-attack transmitter mounted in the model and a tilt sensor mounted on the base of the support system. Angle-of-sideslip measurements were made using a potentiometer to measure turntable rotation angle. Computed angles included corrections to account for elastic deflection of the balance and sting.

For these tests, the model ducts were blocked, so that no airflow passed through the inlets or duct exit. Also, because no measurements were made of base or cavity pressure, no adjustments were made to the measured data to account for any effects due to these pressures. These tests were conducted with natural boundary-layer transition; that is, transition was not induced artificially.

Although it is known that large flow angles are induced by the turntable bump (fig. 2), no attempt was made to assess these flow angles, and no flow-angle corrections were made to the test results. Using the method described in reference 4, angle of attack and the longitudinal aerodynamic coefficients were corrected for the effects of tunnel-wall interference.

Blockage corrections based on the methods described in references 5 and 6 were computed and applied to determine corrected free-stream Mach number and dynamic pressure. For large angles, the blockage corrections include not only the incremental effects of model volume, model support-system drag, and model zero-lift drag but also an increment due to the separated wake as computed by the method of reference 6. These blockage corrections were applied to clear-tunnel calibrations based on the measurement of settling-chamber total pressure and wall static pressure upstream of the location of the model in the test section.

RESULTS AND DISCUSSION

Presentation of Data

To expedite publishing the results of the investigation, the data are presented with limited analysis. The model attitude schedules and an outline of the associated data run schedules are presented in tables II and III, respectively. Selected data are presented in figures 8 and 9 for the baseline configuration, in figures 10 and 11 for the forebody modifications, in figures 12 and 13 for negative angles of attack, and in figures 14 through 17 for the component buildup. The complete test results are tabulated in the appendix.

Longitudinal Characteristics

Figure 8 shows the effects of Reynolds number variation on the longitudinal characteristics of the basic configuration. Some effect on normal-force coefficient is observed, but much more significant changes are apparent in the pitching-moment-coefficient data. This effect consists of large positive increments of pitching-moment coefficients above approximately $\alpha \approx 50°$ for the low Reynolds number tests compared with the data for the high Reynolds number tests. For most canard deflections, this pitching-moment increment is sufficiently large to produce a change in sign of the model pitching-moment coefficient. The change in the data from low Reynolds number behavior to high Reynolds number behavior occurs between $R_N = 0.6 \times 10^6$ and 0.9×10^6 per foot.

Results of component buildup tests with fuselage and canards (fig. 14) and fuselage alone (fig. 16) show similar effects of Reynolds number to those for the complete model. These effects indicate that the fuselage is the source of the observed phenomenon.

Lateral-Directional Characteristics

Figure 9 shows the effects of Reynolds number variation on the lateral-directional characteristics for the basic configuration at angles of attack from 40° to 90°. The data show that the rolling-moment coefficient is relatively insensitive to Reynolds number; however, the side-force and yawing-moment coefficients are greatly affected above $\alpha = 50°$. For spin analysis, the yawing-moment coefficient is the more significant parameter. Except for the lowest Reynolds number tests, the slope of C_n versus β is negative through zero sideslip from $\alpha = 50°$ to 75°. (See figs. 9(a) through 9(f).) At $\alpha = 80°$ and 85° (figs. 9(g) and 9(h) and appendix), the change in slope of C_n versus β from positive to negative occurs between Reynolds numbers of about 1.3 and 2.2×10^6 per foot. The side-force and yawing-moment data for component tests shown in figure 15 (body plus canard) and in figures 16 and 17 (body alone) are more erratic, which indicates interactions between the various components.

Forebody Modifications

Dynamic free-spinning tests are conducted at low Reynolds numbers. When investigations such as reported herein indicate significant Reynolds number effects at high angles of attack, particularly on yawing-moment data, an attempt is made to

modify the model to compensate for these effects. From past experience, typical modifications consist of strakes attached to the forebody. For this test series, in addition to evaluating several forebody strake configurations, an alternate forebody shape was designed based on the two-dimensional work of Polhamus (ref. 2). This alternate forebody shape was expected to exhibit the desired characteristics.

Figures 10 and 11 show the test results for the forebody modifications at low Reynolds number compared with the baseline configuration at high Reynolds number. Plots of yawing-moment coefficient versus sideslip show that the ventral strake is effective at all angles of attack tested. The alternate forebody provides a reasonable match at $\alpha > 70°$, and the lateral strake performs acceptably at $\alpha > 80°$. The pitching-moment coefficient is also best matched by the ventral strake. The alternate forebody is less satisfactory but is much better than the angled or lateral strakes.

Negative Angle of Attack

Figures 12 and 13 present the results of Reynolds number variation on the baseline configuration for high negative angles of attack. Effects analogous to those observed in the positive high-angle-of-attack tests are shown. The increments in pitching-moment coefficient at low Reynolds number are slightly smaller beyond $\alpha = -65°$ than those for the high Reynolds number data. The reversals in the slope of C_n versus sideslip data at low Reynolds number are evident at $\alpha = -80°$ and $-60°$. (See figs. 13(a) and 13(b).) Forebody modifications were not tested at negative angles of attack.

CONCLUSIONS

Results of wind-tunnel tests of a 1/8-scale model of the X-29A airplane at high positive and negative angles of attack in the Ames 12-Foot Pressure Wind Tunnel have led to the following observations:

1. Significant Reynolds number effects on pitching-moment characteristics are observed above 50° angle of attack. The fuselage is the primary source of these effects.

2. Significant Reynolds number effects on yawing-moment characteristics are observed above 50° angle of attack.

3. A ventral strake mounted on the forebody produces results at low Reynolds number similar to those obtained for the baseline configuration at high Reynolds number.

4. Reynolds number effects on pitching and yawing moments at high negative angles of attack are analogous to those observed at high positive angles of attack.

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6

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TABLE I.- DIMENSIONAL DATA

	Airplane	Model
Length, ft	48	6
Wing:		
Reference area, ft^2	185	2.89
Exposed area, ft^2	160	3.50
Span, ft	27.2	3.4
Aspect ratio	4.0	4.0
Mean aerodynamic chord, in.	86.6	10.83
Leading-edge sweep, deg	-29.27	-29.27
1/4-chord sweep, deg	-33.73	-33.73
Taper ratio	0.4	0.4
Airfoil section:		
Root chord thickness, percent	6.7	6.7
Root thickness (side of body), percent	6.2	6.2
Tip chord thickness, percent	5.0	5.0
Canard:		
Reference area, ft^2	37.00	0.58
Aspect ratio	1.47	1.47
Leading-edge sweep, deg	42	42
1/4-chord sweep, deg	23.08	23.08
Taper ratio	0.319	0.319
Airfoil section:		
Root chord thickness, percent	5	5
Tip chord thickness, percent	3.5	3.5
Vertical tail:		
Reference area, ft^2	34	0.53
Aspect ratio	2.68	2.68
Leading-edge sweep, deg	47	47
Taper ratio	0.30	0.30
Airfoil section:		
Root chord thickness, percent	4	4
Tip chord thickness, percent	4	4

TABLE II.- MODEL ATTITUDE SCHEDULES

[See table III]

Schedule	α, deg	β, deg
A1	40, 50, 60, 65, 70, 75, 80, 85, 90	
A2	40, 50, 60, 70, 80, 90	
A3	-40, -50, -60, -70, -80, -90	
A4	-40, -50, -60, -65, -70, -75, -80, -85, -90	
B1		-10, -8, -4, 0, 4, 8, 10, 15, 20, 30
B2		-10, -5, 0, 5, 10, 15, 20
B3		10, 8, 4, 0, -4, -8, -10, -15, -20, -30

TABLE III.- RUN SCHEDULE

Run	R_N, per foot	α	β	δ_C, deg	δ_a, deg	δ_s, deg	δ_R, deg	Configuration
6	Atm	A2	0	Off	0	0	0	Canards off
7	↓	40	B2					
8		60	B2					
9	3.0×10^6	A2	0					
10		40	B2					
11	↓	60	B2					
12		80	B2					
13	5.0×10^6	A2	0					
14		80	B2					
15	↓	60	B2					
16		40	B2					
17	Atm	A2	0					
18		80	B2					
19		60	B2					
20		40	B2	↓	↓	↓		↓
21		A1	0	−60	25	30		Baseline
22		40	B1					
23		50						
24		60						
25		65						
26		70						
27		75						
28		80						
29		85						
30		90	↓					
31		A1	25	↓				
32		A2	0	−40				
33		90	B1					
34		85						
35		80						
36		75						
37		70						
38		65						
39		60						
40		50						
41		40	↓	↓				
42		A2	0	−25				
43		90	B1					
44		85						
45		80						
46		75						
47		70						
48		65						
49		60						
50		50						
51	↓	40	↓	↓	↓	↓	↓	↓

TABLE III.- Continued

Run	R_N, per foot	α	β	δ_c, deg	δ_a, deg	δ_s, deg	δ_R, deg	Configuration
52	Atm	A2	0	-20	25	30	0	Baseline
53	↓	90	B1	↓	↓	↓	↓	↓
54		85						
55		80						
56		75						
57		70						
58		65						
59		60						
60		50						
61	↓	40	↓	↓				
62	5.0 × 10⁶	A2	0	-60				
63		90	B1	↓				
64		85						
65		80						
66		75						
67		70						
68		65						
69		60						
70		50						
71		40	↓	↓				
72		A2	0	-40				
73		90	B1	↓				
74		85						
75		80						
76		75						
77		70						
78		65						
79		60						
80		50						
81		40	↓	↓				
82		A2	0	-20				
83		90	B1	↓				
84		85						
85		80						
86		75						
87		70						
88		65						
89		60						
90		50						
91	↓	40	↓	↓				
92	3.4 × 10⁶	A2	0	-60				
93		90	B1	↓				
94		85						
95		80						
96		75						
97	↓	70	↓	↓	↓	↓	↓	↓

TABLE III.- Continued

Run	R_N, per foot	α	β	δ_c, deg	δ_a, deg	δ_s, deg	δ_R, deg	Configuration
98	3.4×10^6	65	B1	−60	25	30	0	Baseline
99	↓	60	↓	↓	↓	↓	↓	↓
100	↓	50	↓					
101		40	↓					
102	2.2×10^6	A2	0					
103		90	B1					
104		85						
105		80						
106		75						
107		70						
108		65						
109		60						
110	↓	50	↓					
111		40	↓					
112	Atm	A2	0					
113	Atm	40	B1					
114	0.35×10^6	A2	0					
115		90	B1					
116		85						
117		80						
118		75						
119		70						
120		65						
121		60						
122		50						
123		40	↓					
124		A2	0	↓				
125		A2	0	−40				
126		40	B1					
127		50						
128		60						
129		65						
130		70						
131		75						
132		80						
133		85						
134		90	↓	↓				
135		A2	0	−20				
136		90	B1					
137		85						
138		80						
139		75						
140		70						
141		65						
142		60						
143	↓	50	↓	↓	↓	↓	↓	↓

TABLE III.- Continued

Run	R_N, per foot	α	β	δ_{c}, deg	δ_{a}, deg	δ_{s}, deg	δ_{R}, deg	Configuration
144	0.35×10^6	40	Bl	−20	25	30	0	Baseline
145	0.6×10^6	A2	0	−60				
146		90	Bl					
147		85						
148		80						
149		75						
150		70						
151		65						
152		60						
153		50						
154		40						
155	0.9×10^6	A2	0					
156		90	Bl					
157		85						
158		80						
159		75						
160		70						
161		65						
162		60						
163		50						
164		40						
165	1.1×10^6	A2	0					
166		90	Bl					
167		85						
168		80						
169		75						
170		70						
171		65						
172		60						
173		50						
174		40						
175	0.6×10^6	A2	0					Ventral strake (A) on
176		90	Bl					
177		85						
178		80						
179		75						
180		70						
181		65						
182		60						
183		50						
184		40						
185		A2	0					Angled strake (C) on
186		90	Bl					
187		85						
188		80						
189		75						

TABLE III.- Continued

Run	R_N, per foot	α	β	$\delta_{c'}$ deg	$\delta_{a'}$ deg	$\delta_{s'}$ deg	$\delta_{R'}$ deg	Configuration
190	0.6×10^6	70	B1	−60	25	30	0	Angled strake (C) on
191		65						
192		60						
193		50						
194		40	↓					
195		A2	0					Lateral strake (B) on
196		90	B1					
197		85						
198		80						
199		75						
200		70						
201		65						
202		60						
203		50						
204		40	↓					
205		A1	0					Nose strake off
206		90	B1					
207		85						
208		80						
209		75						
210		70						
211		65						
212		60						
213		50						
214		40	↓					
215		A1	0					Alternate forebody
216		90	B1					
217		85						
218		80						
219		75						
220		70						
221		65						
222		60						
223		50						
224		40	↓					
225	2.2×10^6	A2	0					Nose strake off
226		90	B1					
227		85						
228		80						
229		75						
230		70						
231		65						
232		60						
233		50						
234		40	↓					
235	↓	A2	0	↓	↓	↓	−30	Baseline

TABLE III.- Continued

Run	R_N, per foot	α	β	δ_c, deg	δ_a, deg	δ_s, deg	δ_R, deg	Configuration
236	2.2×10^6	90	B1	-60	25	30	-30	Baseline
237		85						
238		80						
239		75						
240		70						
241		65						
242		60						
243		50						
244		40						
245		A1	0			0	0	
246				-40				
247				-20				
248	0.6×10^6			-20				
249				-40				
250				-60				
251	2.2×10^6			-60	10			
252				-40				
253				-20				
254	0.6×10^6			-20				
255				-40				
256				-60				
257	2.2×10^6			-60	0			
258				-40				
259				-20				
260	0.6×10^6			-20				
261				-40				
262				-60				
263	2.2×10^6	A2			25L -10R	30		
264		80	B1					
265		60						
266		50						
267		40						
268		A2	0	-45L -5R	25			
269		80	B1					
270		60						
271		40						
272	0.6×10^6	A2	0					
273		80	B1					
274		60						
275		40						
276	2.2×10^6	40		0				
277		50						
278		A2	0					
279		90	B1					

TABLE III.- Continued

Run	R_N, per foot	α	β	δ_c, deg	δ_a, deg	δ_s, deg	δ_R, deg	Configuration
280	2.2×10^6	85	B1	0	.25	30	0	Baseline
281		80						
282		75						
283		70						
284		65						
285		60						
286	Atm	A1	0					
287	0.6×10^6	A2	0					
288		90	B1					
289		85						
290		80						
291		75						
292		70						
293		65						
294		60						
295		50						
296		40						
299	3.4×10^6	A3	0	0	-10	-30		
300		-80	B3					
301		-60						
302		-40						
303		A3	0	30				
304		-80	B3					
305		-60						
306		-40						
307	5.0×10^6	A3	0					
308		-80	B3					
309		-60						
310		-40						
311		A3	0	0				
312		-80	B3					
313		-60						
314		-40						
315	Atm	A3	0					
316		-80	B3					
317		-60						
318		-40						
319		A3	0	30				
320		-80	B3					
321		-60						
322		-40						
323	0.6×10^6	A3	0					
324		-80	B3					
325		-60						
326		-40						
327		A3	0	0				

TABLE III.- Continued

Run,	R_N, per foot	α	β	δ_c, deg	δ_a, deg	δ_s, deg	δ_R, deg	Configuration
328	0.6 × 10⁶	-80	B3	0	-10	-30	0	Baseline
329	↓	-60	↓	↓	↓	↓	↓	
330	↓	-40	↓					
331	0.35 × 10⁶	A3	0	↓				
332	0.35 × 10⁶	↓	↓	30			↓	
333	Atm	↓	↓				-30	
334	↓	-80	B3					
335	↓	-60	↓					
336	↓	-40	↓					
337	0.6 × 10⁶	A3	0					
338		-80	B3					
339		-60	↓					
340		-40	↓		↓		↓	
341		A3	0		25L -10R		0	
342		-80	B3					
343		-60	↓					
344		-40	↓					
345	Atm	A3	0					
346		-80	B3					
347		-60	↓					
348		-40	↓		↓			
349		A4	0		0			
350	0.6 × 10⁶	↓				↓		
351	Atm	↓				0		
352	0.6 × 10⁶	↓	↓	↓				
353		A2	↓	Off				Canards off
354		80	B1					
355		60	↓					
356		40	↓					
357	3.0 × 10⁶	A2	30					
358	Atm	A2	30					
359	2.2 × 10⁶	40	B1				Off	Canards, vertical tail off
360		60						
361	↓	80						
362	Atm	40						
363		60						
364	↓	80						
365	0.6 × 10⁶	40						
366		60						
367	↓	80		↓	↓	↓	↓	
369	2.2 × 10⁶	A1	0	-60	Off	Off		Body and canards
370		80	B1					
371		60						
372		40	↓	↓	↓	↓	↓	↓
373	↓	A1	0	-40				

17

TABLE III.- Continued

Run	R_N, per foot	α	β	δ_c, deg	δ_a, deg	δ_s, deg	δ_R, deg	Configuration
374	2.2×10^6	80	Bl	−40	Off	Off	Off	Body and canards
375		60						
376		40	↓	↓				
377		Al	0	−20				
378		80	Bl					
379		60						
380		40	↓					
381	Atm	Al	0					
382		80	Bl					
383		60						
384		40	↓	↓				
385		Al	0	−40				
386		80	Bl					
387		60						
388		40	↓	↓				
389		Al	0	−60				
390		80	Bl					
391		60						
392		40	↓					
393	0.35×10^6	Al	0					
394		80	Bl					
395		60						
396		40	↓	↓				
397		Al	0	−40				
398		80	Bl					
399		60						
400		40	↓	↓				
401		Al	0	−20				
402		80	Bl					
403		60						
404		40	↓					
405	0.6×10^6	Al	0					
406		80	Bl					
407		60						
408		40	↓	↓				
409		Al	0	−40				
410		80	Bl					
411		60		↓				
412		40	↓	↓				
413		Al	0	−60				
414		80	Bl					
415		60						
416		40	↓	↓				
417	2.2×10^6	Al	0	0				
418		80	Bl					
419		60	Bl	↓	↓	↓	↓	↓

TABLE III.- Concluded

Run	R_N, per foot	α	β	δ_c, deg	δ_a, deg	δ_s, deg	δ_R, deg	Configuration
420	2.2×10^6	40	Bl	0	Off	Off	Off	Body and canards
421	0.35×10^6	Al	0					
422		80	Bl					
423		60						
424		40						
425	0.6×10^6	Al	0					
426		80	Bl					
427		60						
428		40						
429	Atm	Al	0					
430		80	Bl					
431		60						
432		40						
433	6.3×10^6	Al	0	Off				Body alone
434		80	Bl					
435		60						
436		40						
437	5.0×10^6	Al	0					
438		80	Bl					
439		60						
440		40						
441	2.2×10^6	Al	0					
442		80	Bl					
443		60						
444		40						
445	0.35×10^6	Al	0					
446		80	Bl					
447		60						
448		40						
449	0.6×10^6	Al	0					
450		80	Bl					
451		60						
452		40						
453	Atm	Al	0					
454		80	Bl					
455		60						
456		40						

FS 117

40.8

72

Figure 1.- Three-view sketch of basic model. Moment reference point shown is FS 454.27 (-0.05c̄).
(Dimensions are in inches.)
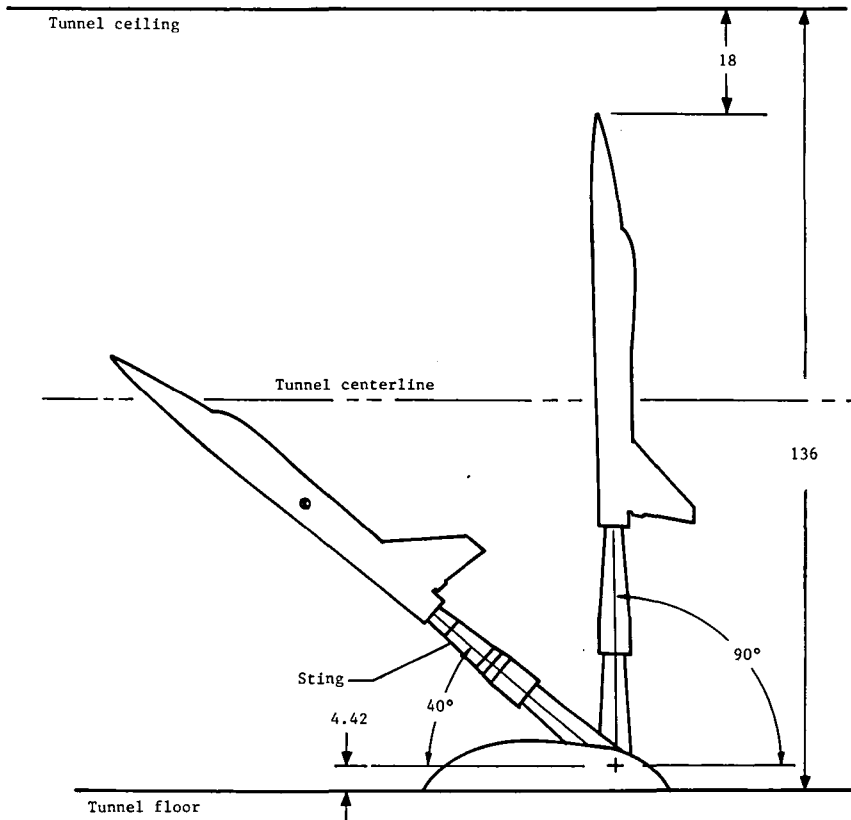
Figure 2.- Model and sting configuration for maximum and minimum angles of attack. Linear dimensions are in inches.
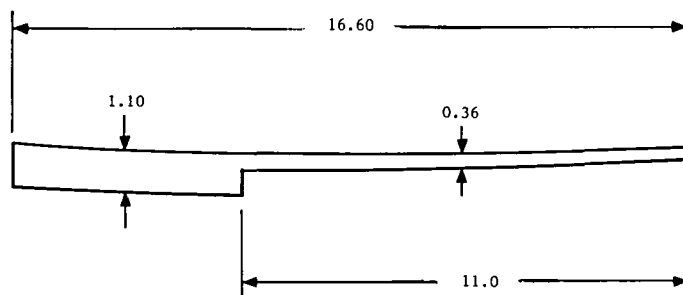
Strake A (ventral strake)
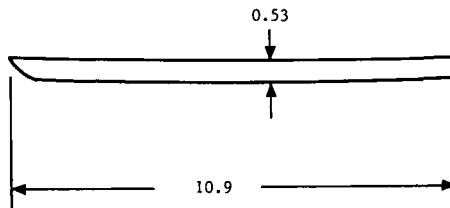
Strakes B and C

Figure 3.- Forebody strakes. Dimensions are in inches.

Section A-A Section B-B
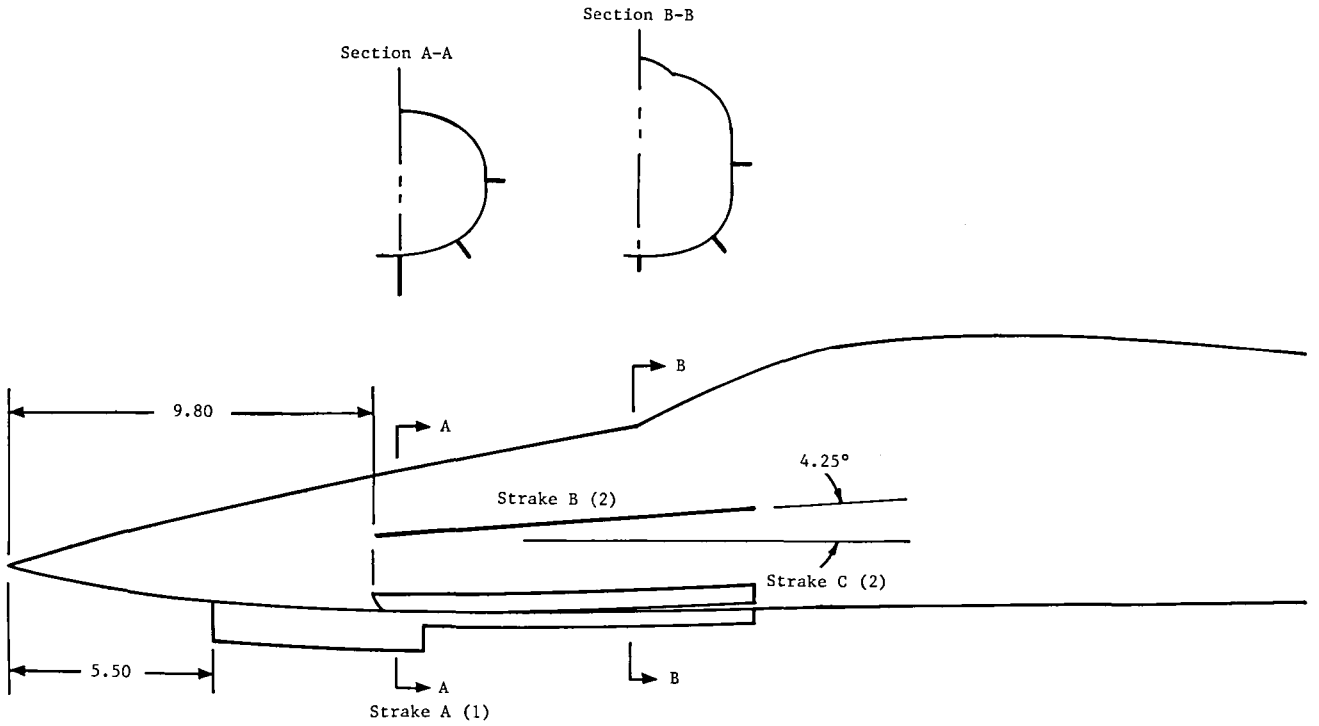
Figure 4.- Placement of various forebody strakes.
Linear dimensions are in inches.
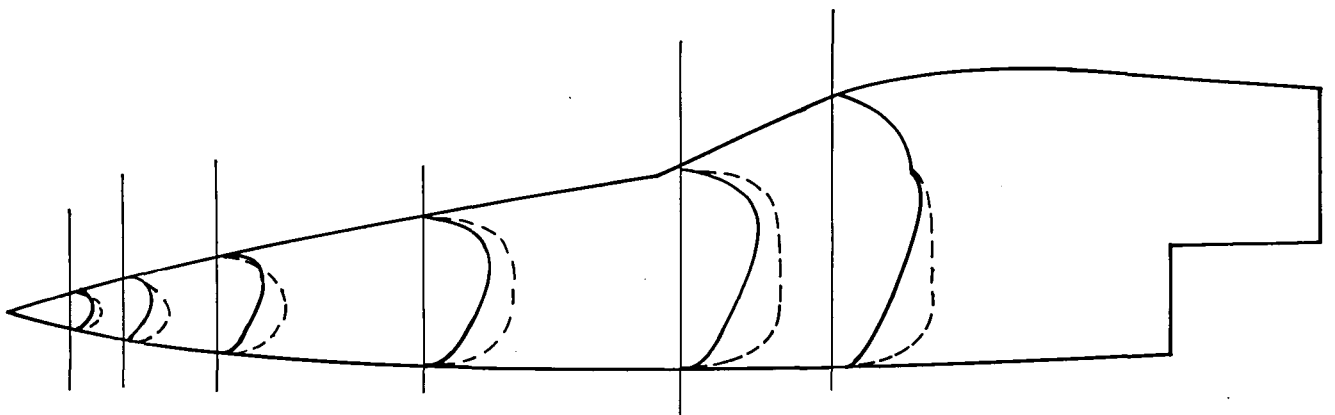
Figure 5.- Alternate forebody cross-sectional shape.
Dashed lines show basic configuration.
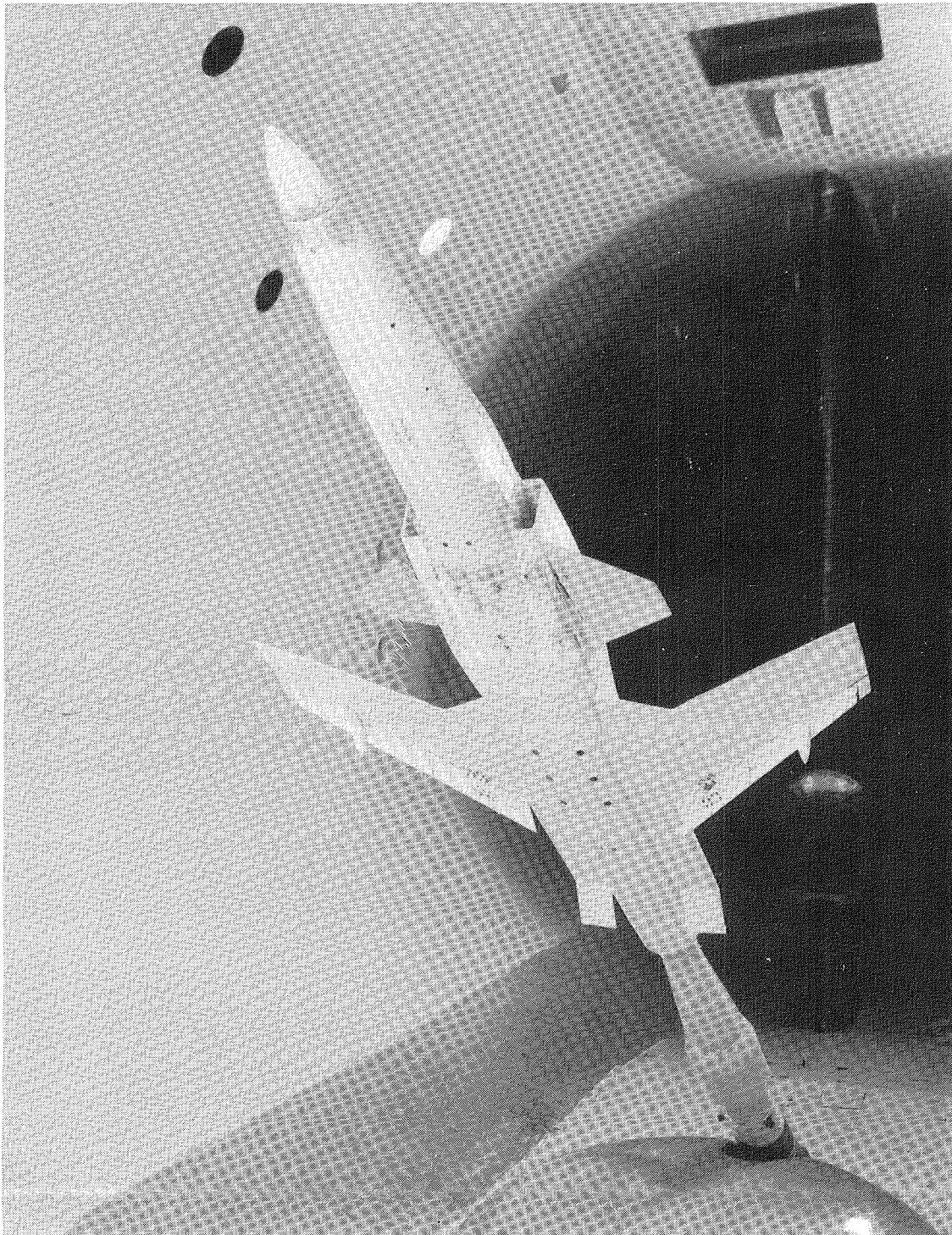
L-86-301

(a) High-angle-of-attack support system.

Figure 6.- Model installation.
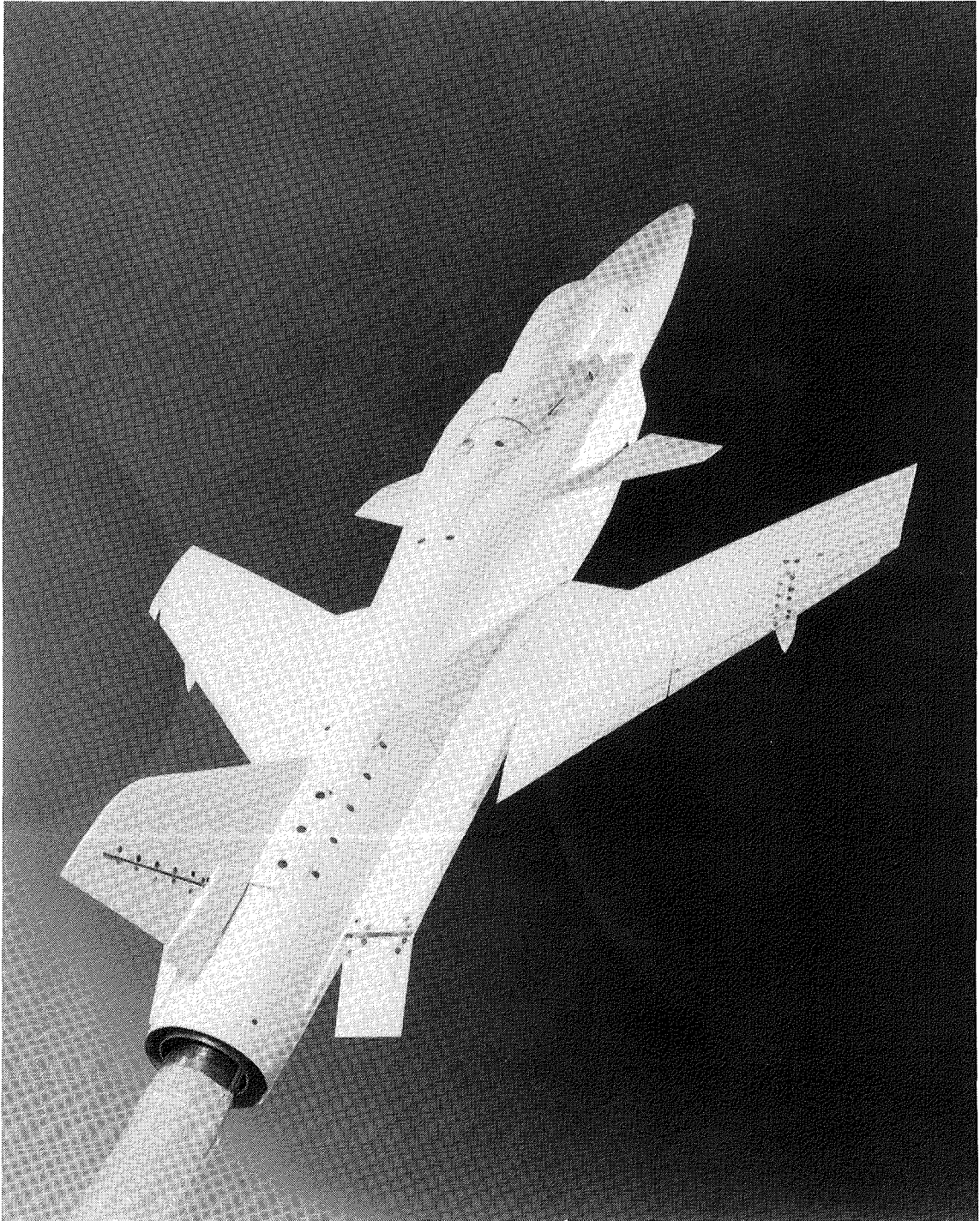
(b) Sting entry and various control surfaces deflected.

Figure 6.- Concluded.
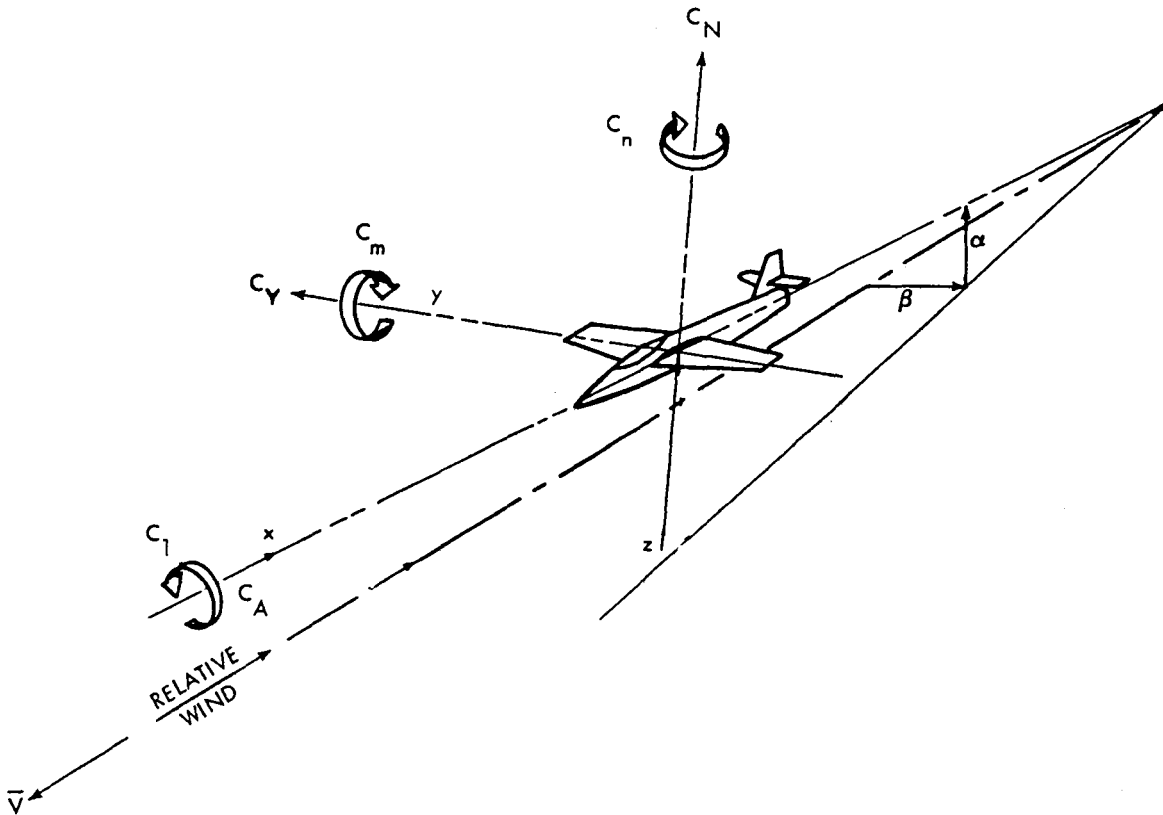
Figure 7.- Orientation of force and moment coefficients about body axes. Positive directions of force coefficients, moment coefficients, and angles are indicated by arrows.
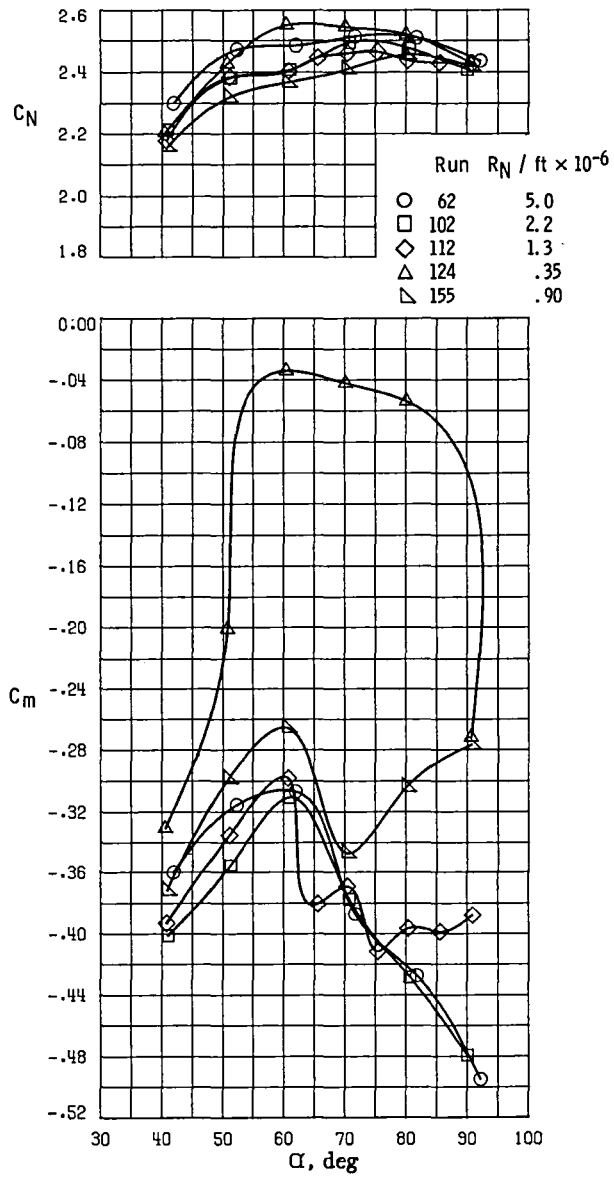
(a) $\delta_c = -60°$; $\delta_a = 25°$; $\delta_s = 30°$.

Figure 8.- Longitudinal aerodynamic characteristics at
various Reynolds numbers with $\beta = 0°$.
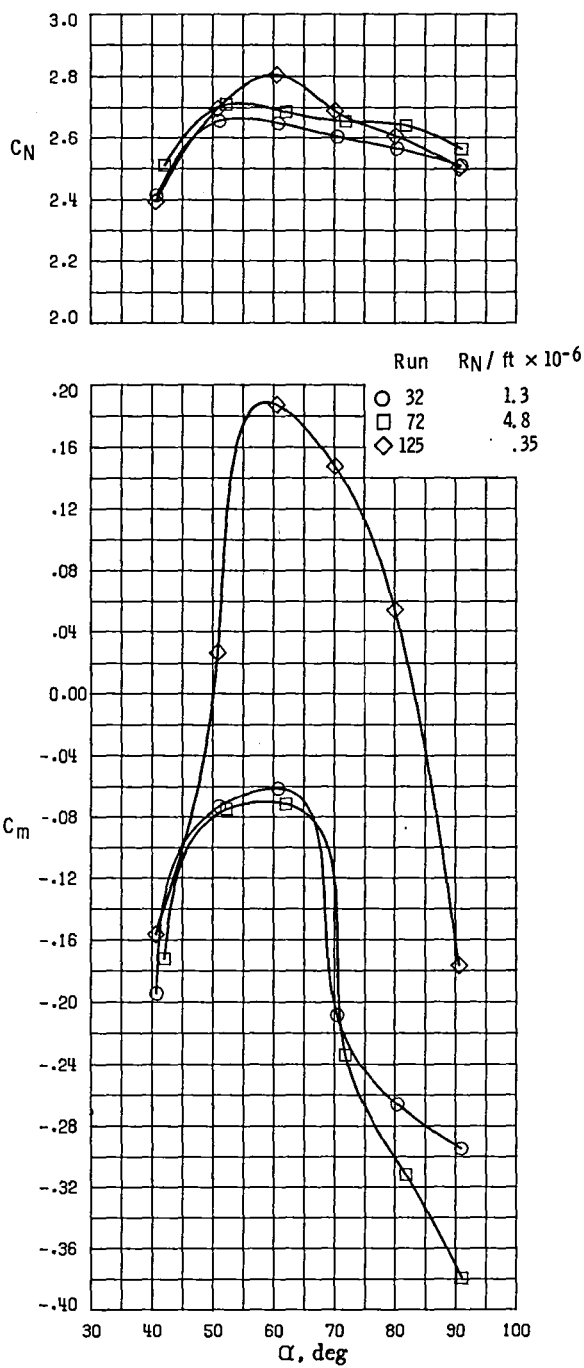
(b) $\delta_c = -40°;$ $\delta_a = 25°;$ $\delta_s = 30°.$

Figure 8.- Continued.
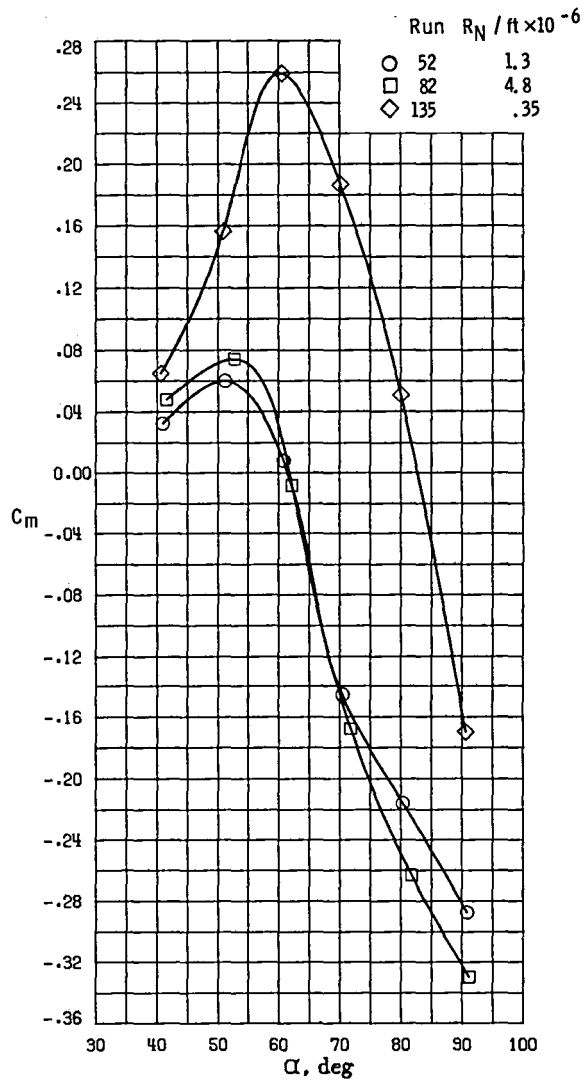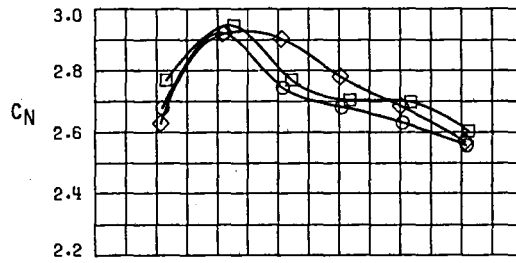
(c) $\delta_c = -20°$; $\delta_a = 25°$; $\delta_s = 30°$.

Figure 8.- Continued.
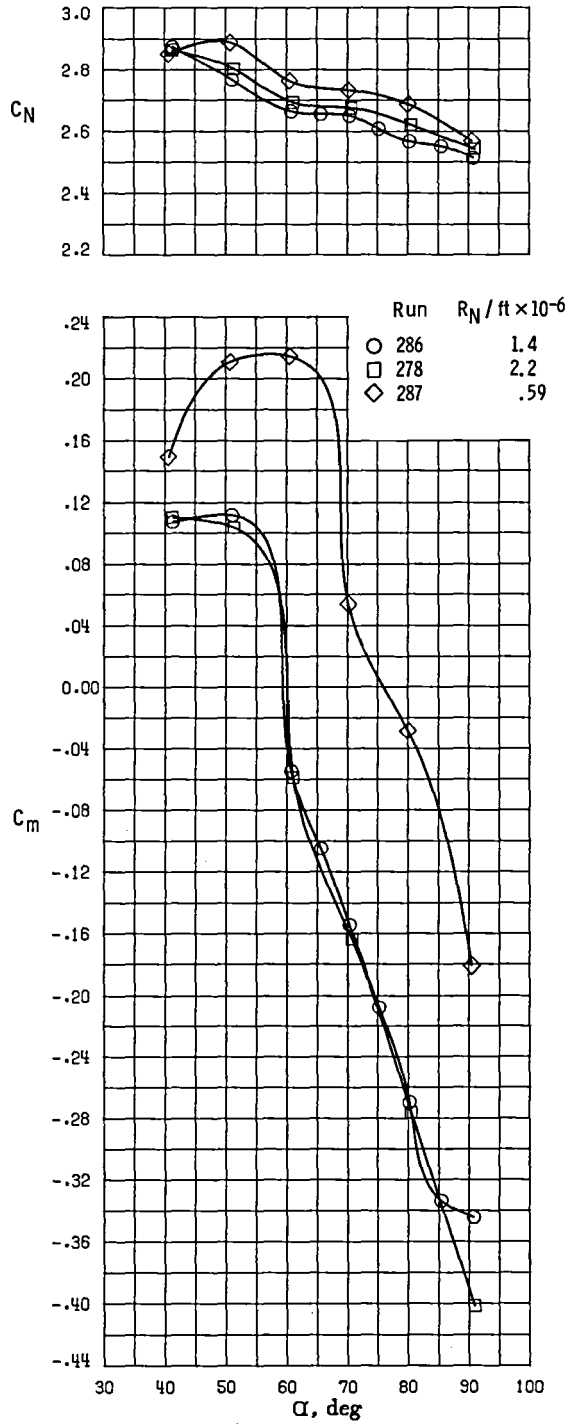
(d) $\delta_c = 0°$; $\delta_a = 25°$; $\delta_s = 30°$.

Figure 8.- Concluded.
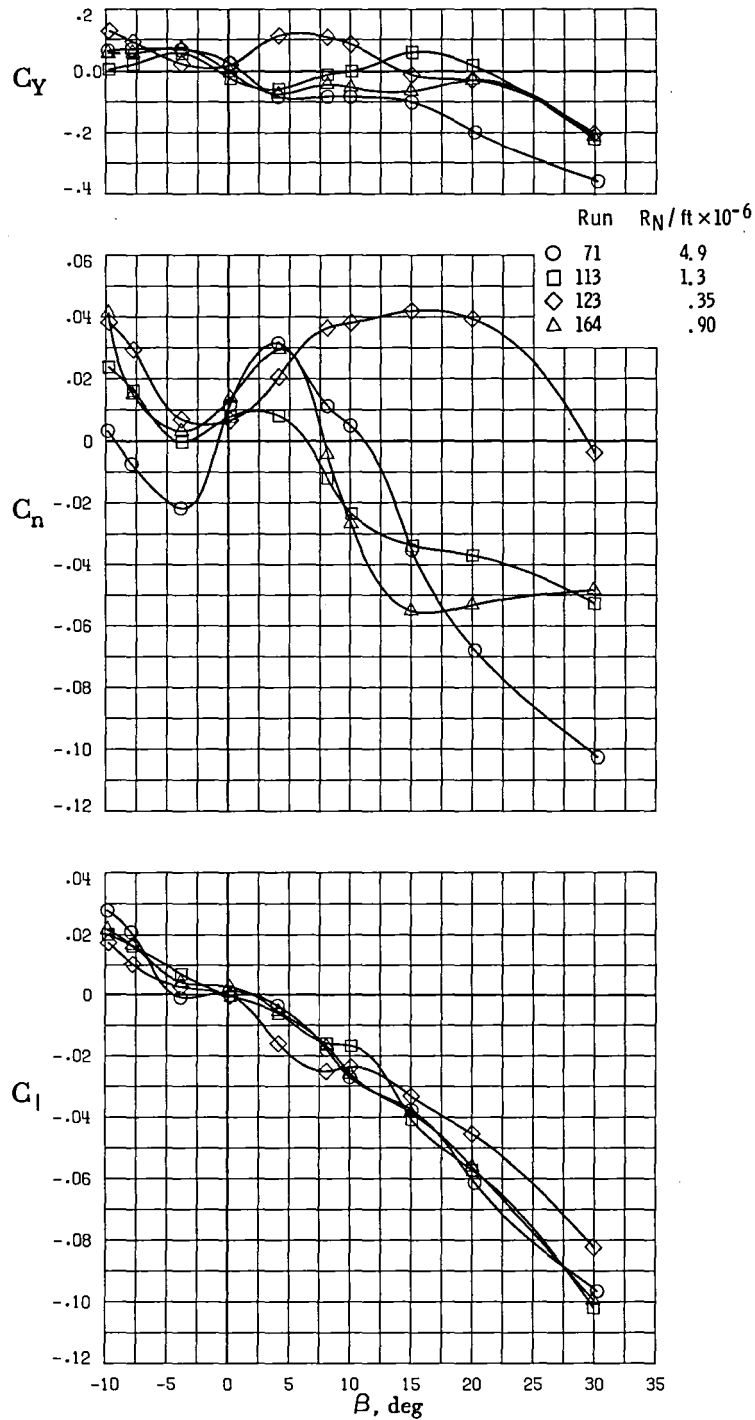
(a) α = 40°.

Figure 9.- Lateral-directional aerodynamic characteristics at various Reynolds numbers. δ_c = -60°; δ_a = 25°; δ_s = 30°.

Run $R_N / ft \times 10^{-6}$

○ 23   1.4
□ 70   4.9
◇ 122   .36
△ 163   .90

(b) $\alpha = 50°$.

Figure 9.- Continued.

Run $R_N / ft \times 10^{-6}$

	Run	$R_N / ft \times 10^{-6}$
○	24	1.4
□	69	5.0
◇	121	.35
△	162	.90
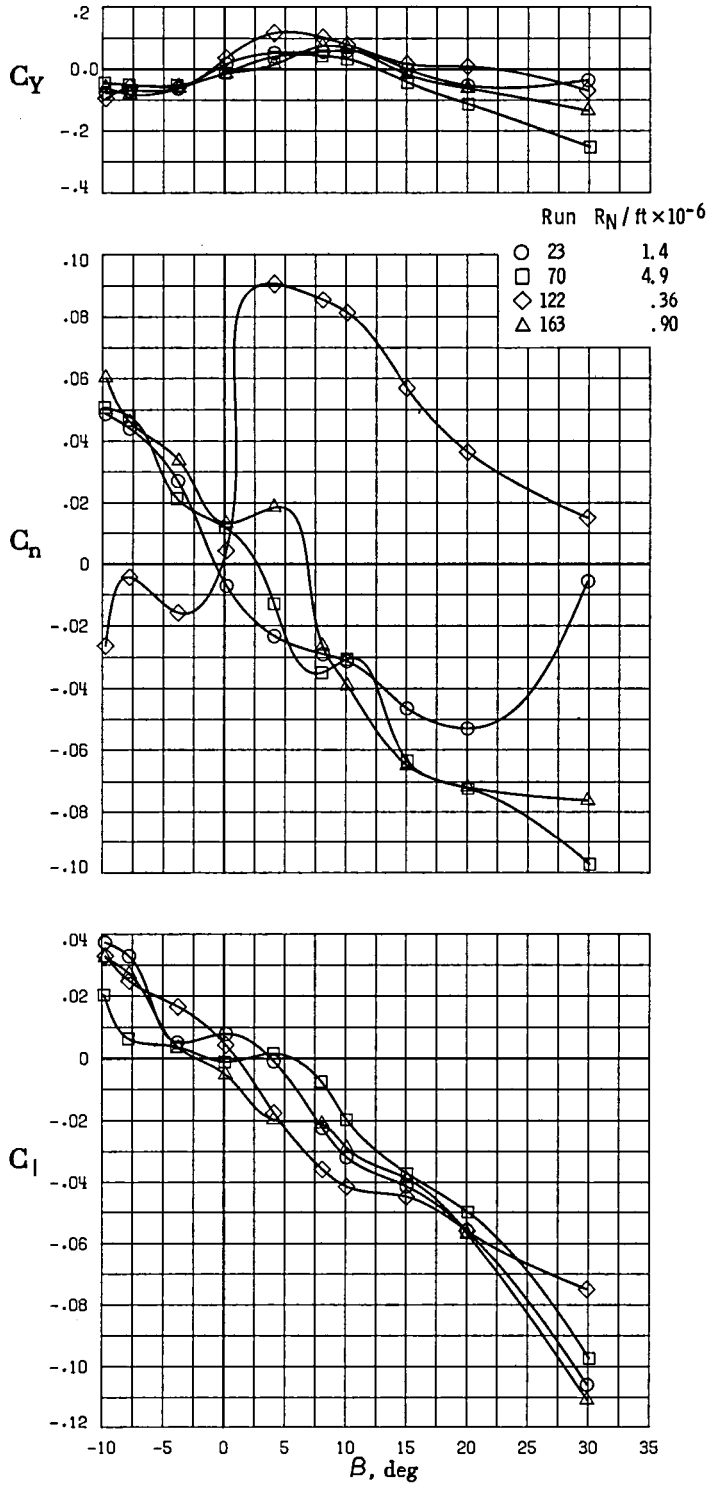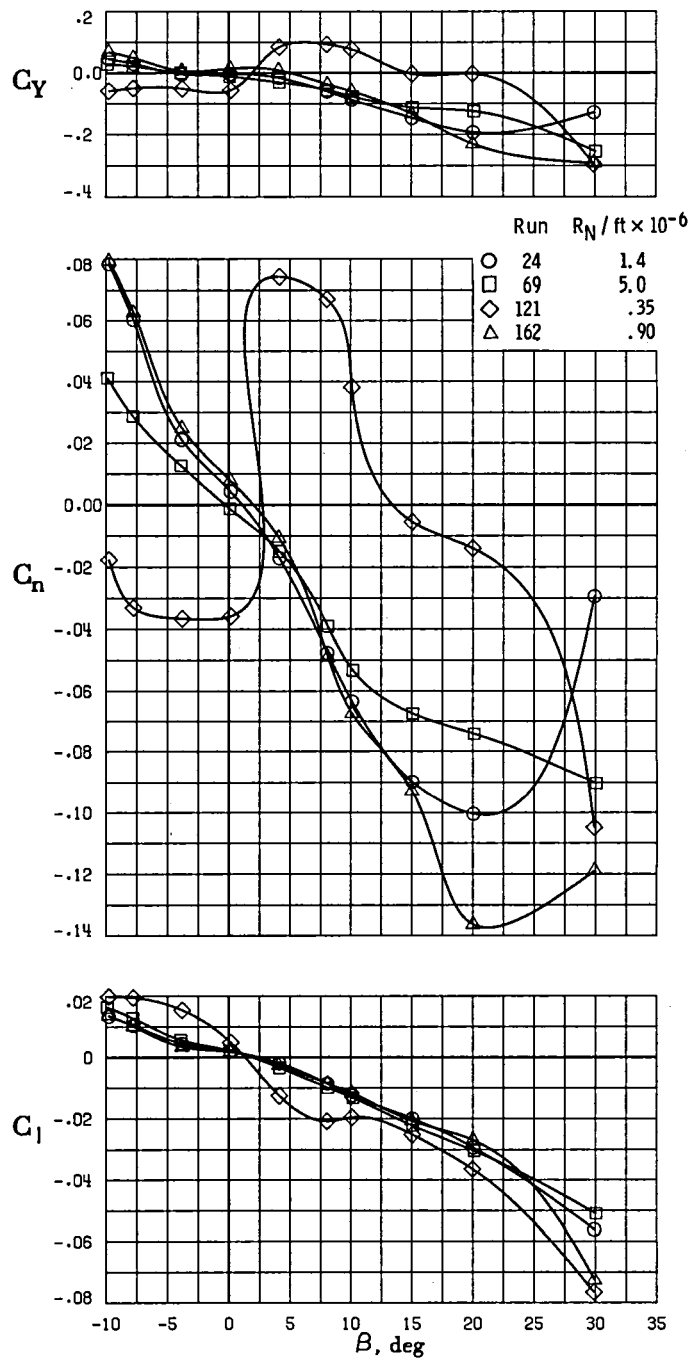
(c) $\alpha = 60°$.

Figure 9.- Continued.
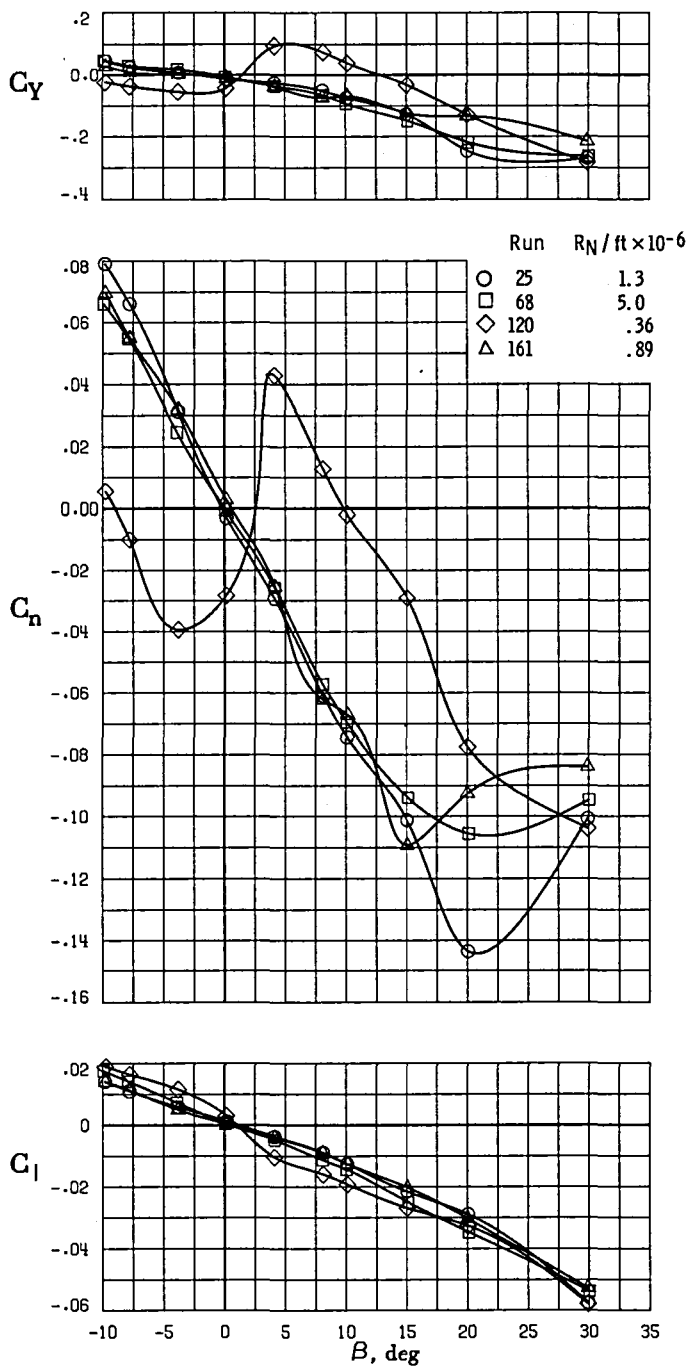
(d) α = 65°.
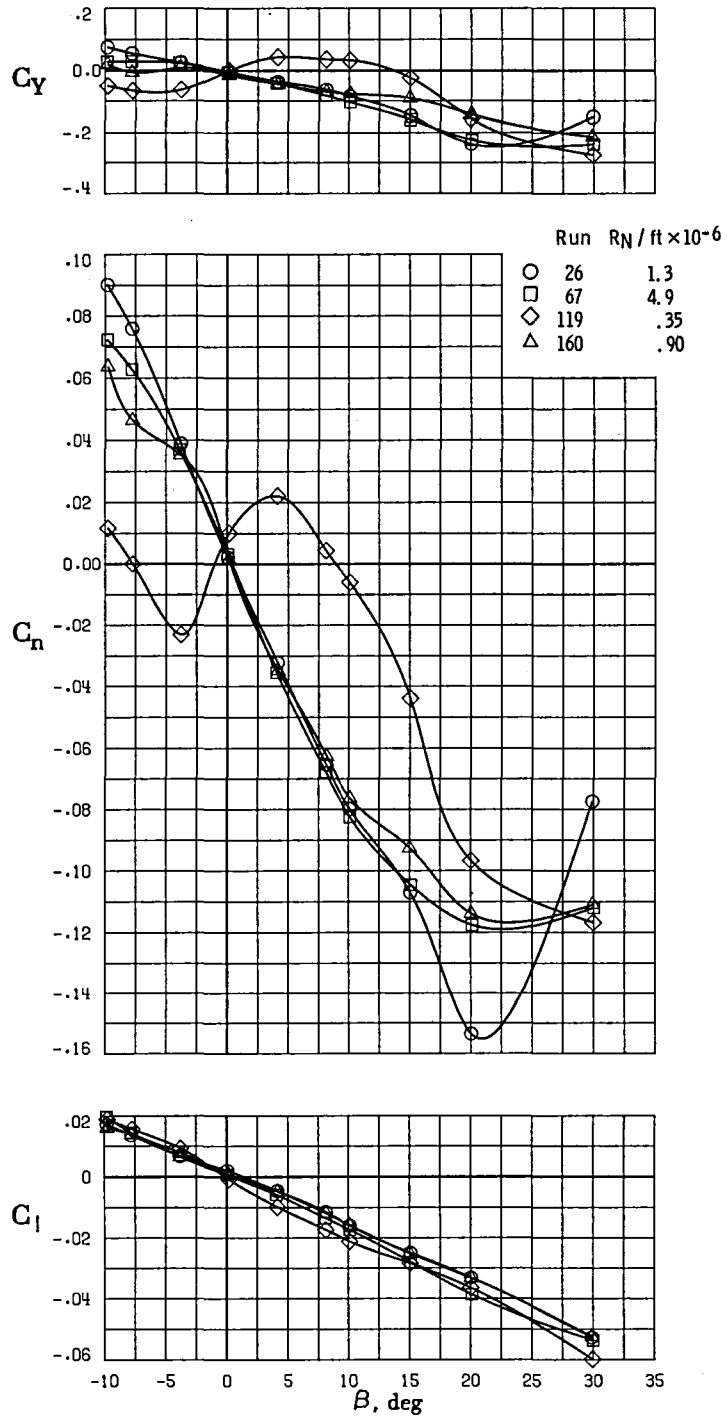
Figure 9.- Continued.

(e) $\alpha = 70°$.

Figure 9.- Continued.
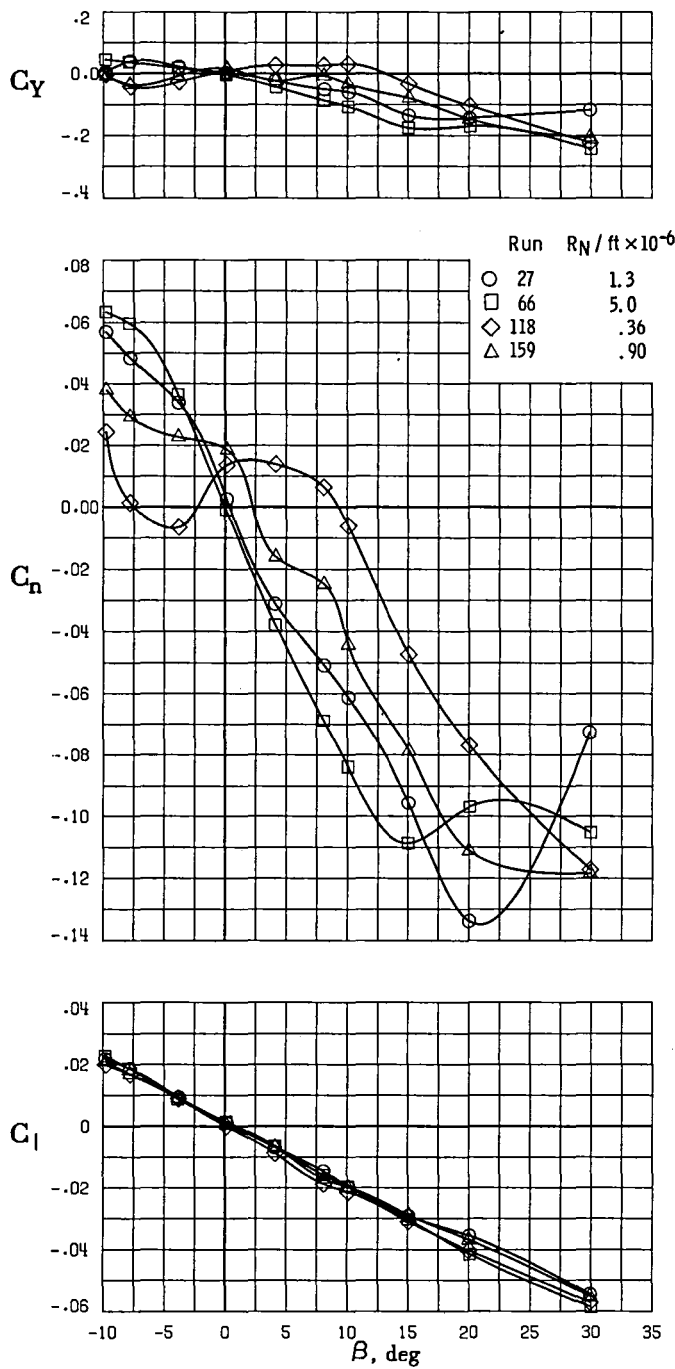
(f) $\alpha = 75°$.

Figure 9.- Continued.
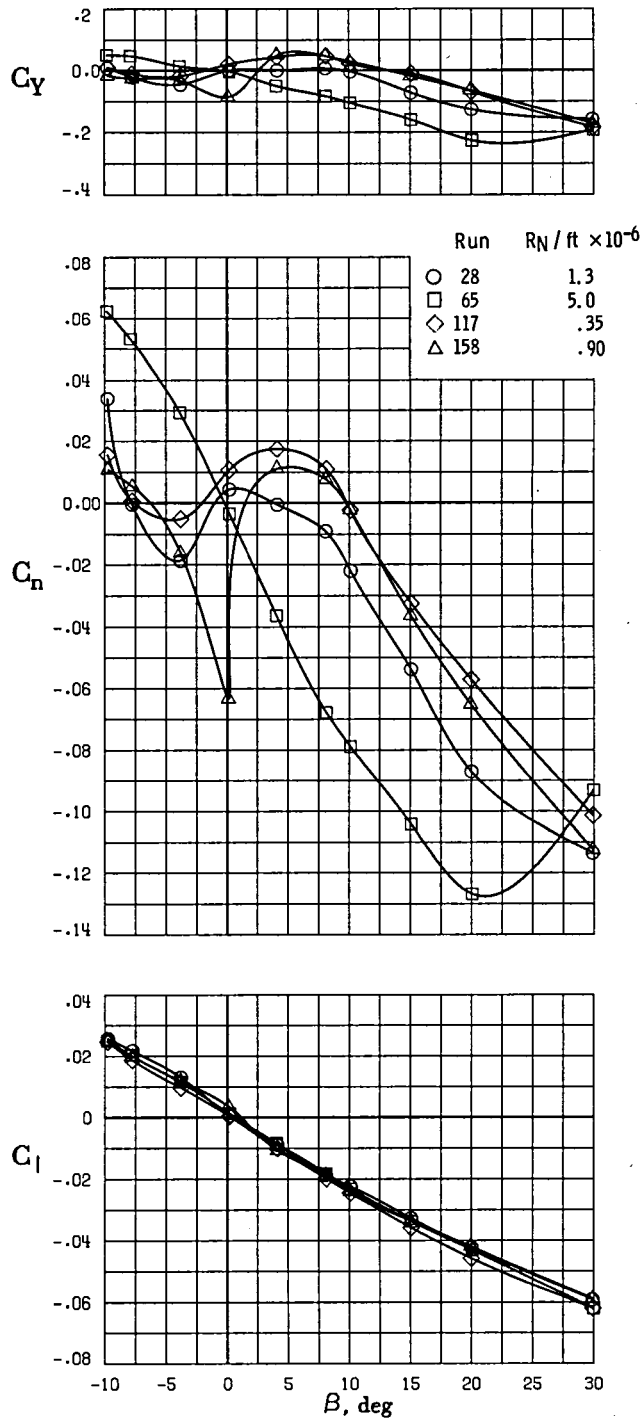
(g) $\alpha = 80°$.

Figure 9.- Continued.
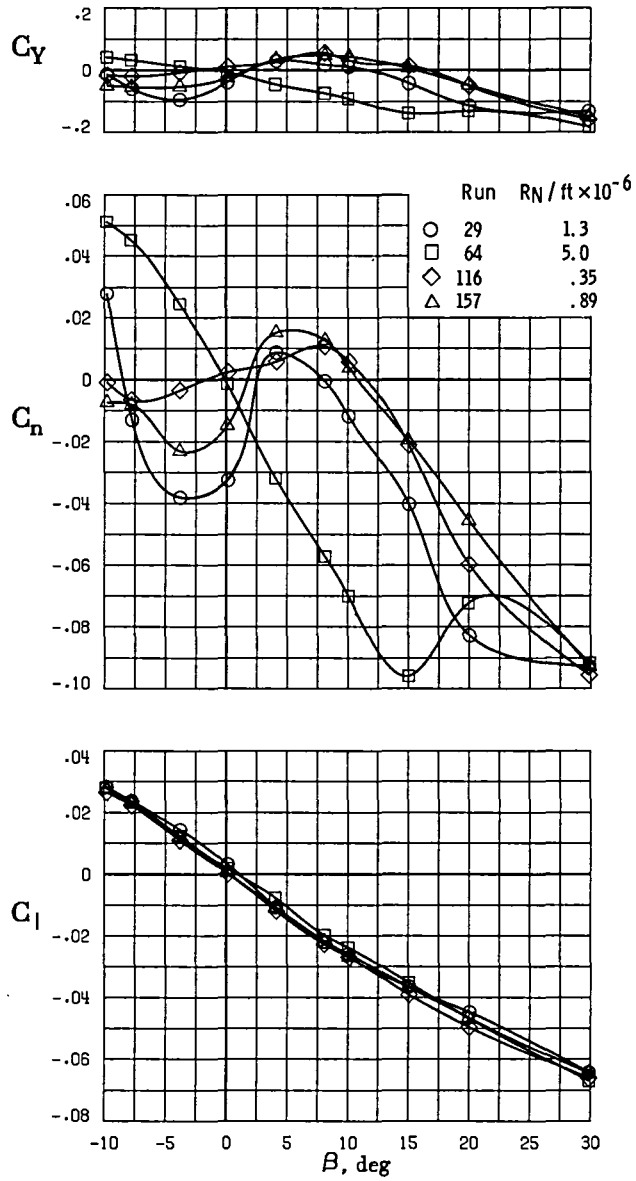
(h) α = 85°.

Figure 9.- Continued.
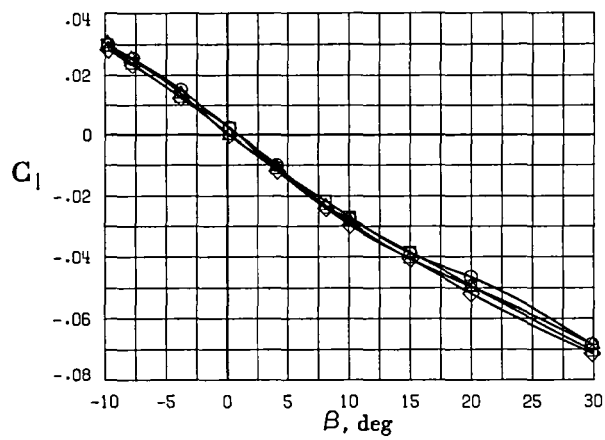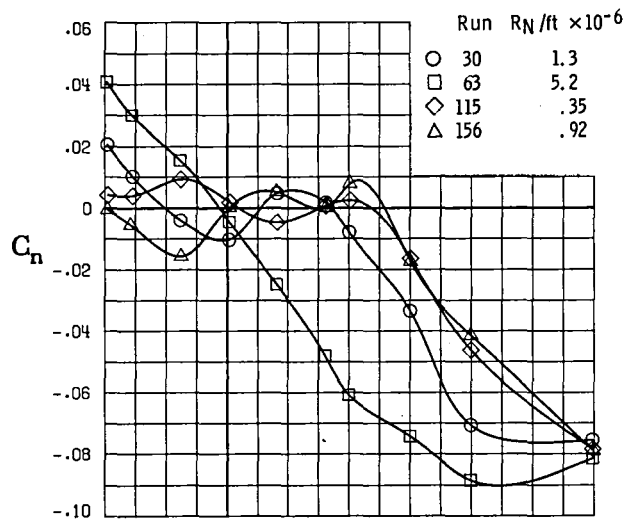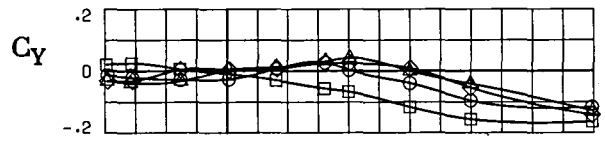
(i) $\alpha = 90°$.

Figure 9.- Concluded.
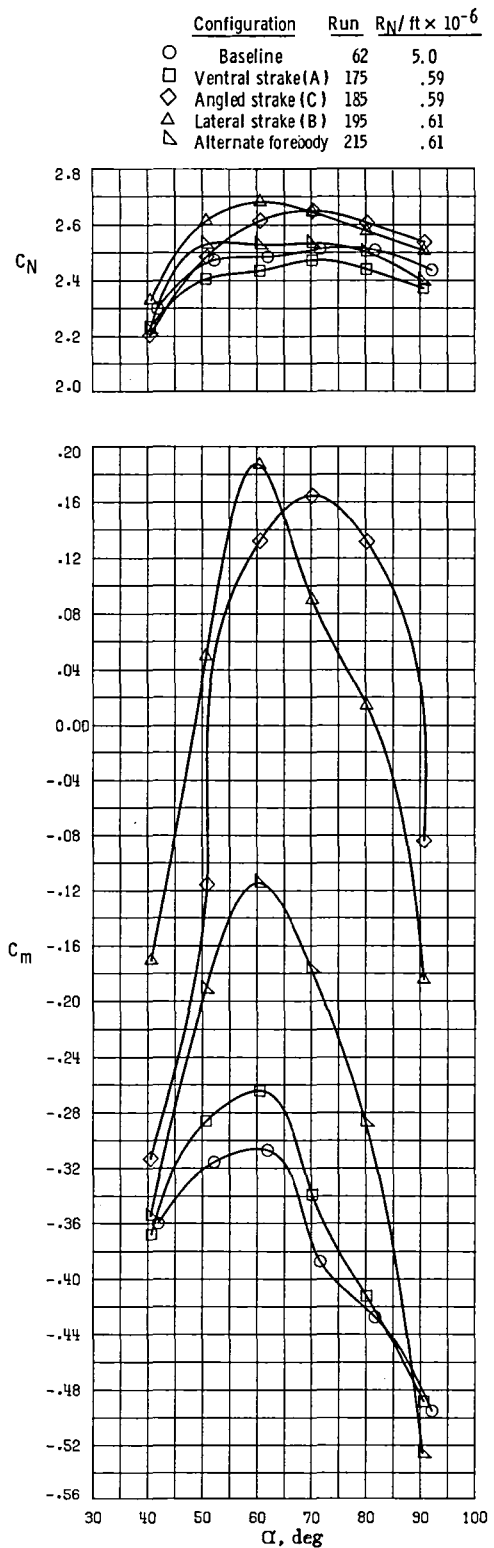
Figure 10.- Longitudinal aerodynamic characteristics of baseline configuration at high Reynolds number compared with various forebody modifications at low Reynolds number.

Configuration	Run	$R_N/ft \times 10^{-6}$
◯ Baseline	71	4.9
☐ Ventral strake (A)	184	.61
◇ Angled strake (C)	194	.60
△ Lateral strake (B)	204	.59
◺ Alternate forebody	224	.63
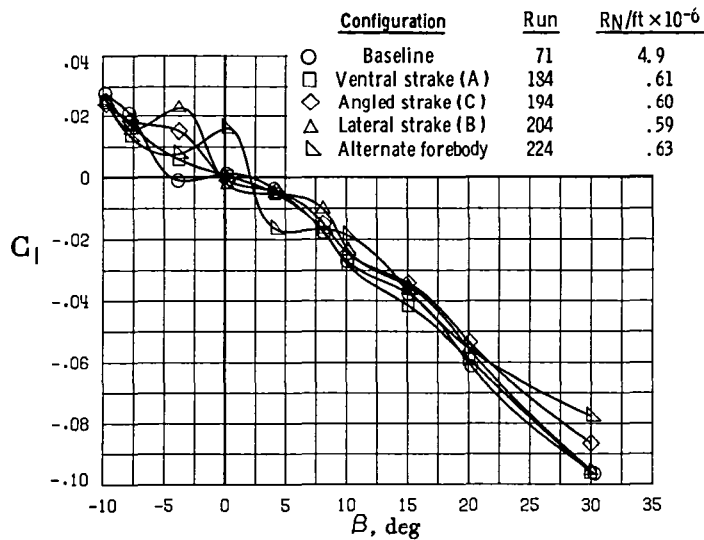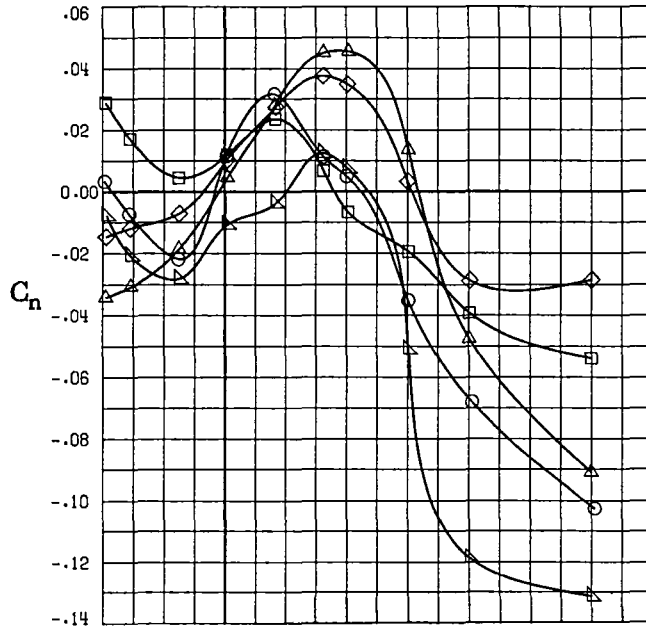
(a) $\alpha = 40°$.

Figure 11.- Lateral-directional aerodynamic characteristics of baseline configuration at high Reynolds number compared with various forebody modifications at low Reynolds number.

	Configuration	Run	$R_N/ft \times 10^{-6}$
O	Baseline	70	4.9
□	Ventral strake (A)	183	.62
◇	Angled strake (C)	193	.60
△	Lateral strake (B)	203	.60
◁	Alternate forebody	223	.65

(b) $\alpha = 50°$.

Figure 11.- Continued.

	Configuration	Run	$R_N / \text{ft} \times 10^{-6}$
○	Baseline	69	5.0
□	Ventral strake (A)	182	.62
◇	Angled strake (C)	192	.60
△	Lateral strake (B)	202	.60
◁	Alternate forebody	222	.62

(c) $\alpha = 60°$.

Figure 11.- Continued.

Configuration	Run	$R_N/ft \times 10^{-6}$
○ Baseline	67	4.9
□ Ventral strake (A)	180	.61
◇ Angled strake (C)	190	.60
△ Lateral strake (B)	200	.60
◁ Alternate forebody	220	.60

(d) $\alpha = 70°$.

Figure 11.- Continued.

Configuration	Run	$R_N/ft \times 10^{-6}$
○ Baseline	65	5.0
□ Ventral strake (A)	178	.61
◇ Angled strake (C)	188	.60
△ Lateral strake (B)	198	.60
◁ Alternate forebody	218	.60

(e) $\alpha = 80°$.

Figure 11.- Continued.

Configuration	Run	R_N / ft $\times 10^{-6}$
Baseline	63	5.2
Ventral strake (A)	176	.60
Angled strake (C)	186	.61
Lateral strake (B)	196	.60
Alternate forebody	216	.61

(f) $\alpha = 90°$.

Figure 11.- Concluded.

(a) $\delta_c = 0°$; $\delta_f = -10°$; $\delta_s = -30°$.

Figure 12.- Longitudinal aerodynamic characteristics at negative high angles of attack for various Reynolds numbers with $\beta = 0°$.
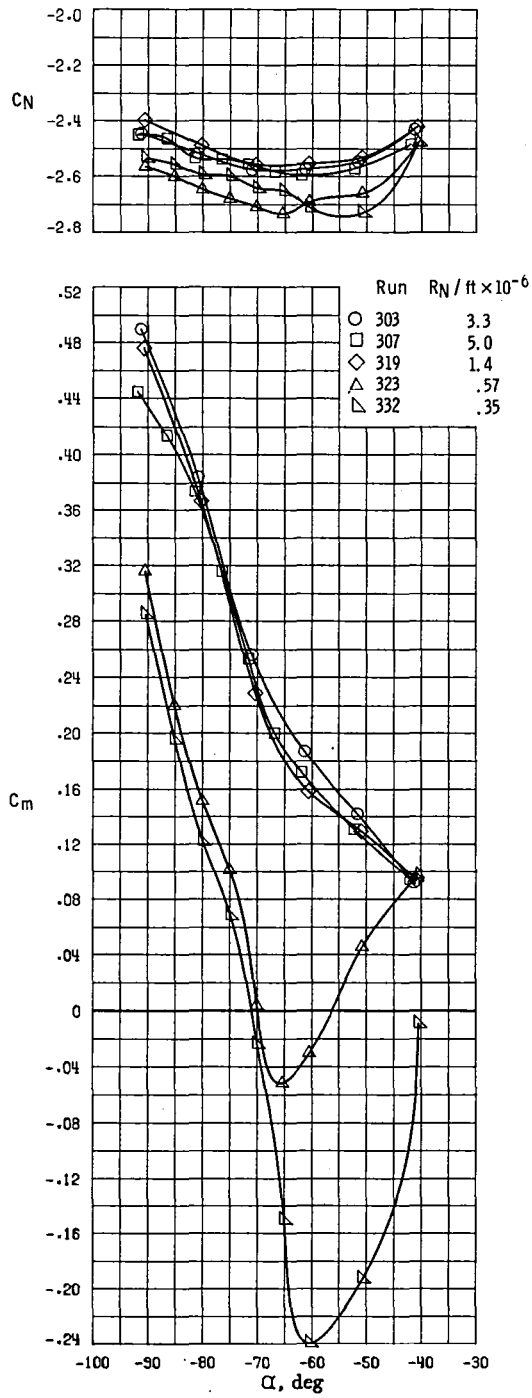
(b) $\delta_c = 30°$; $\delta_f = -10°$; $\delta_s = -30°$.

Figure 12.- Concluded.
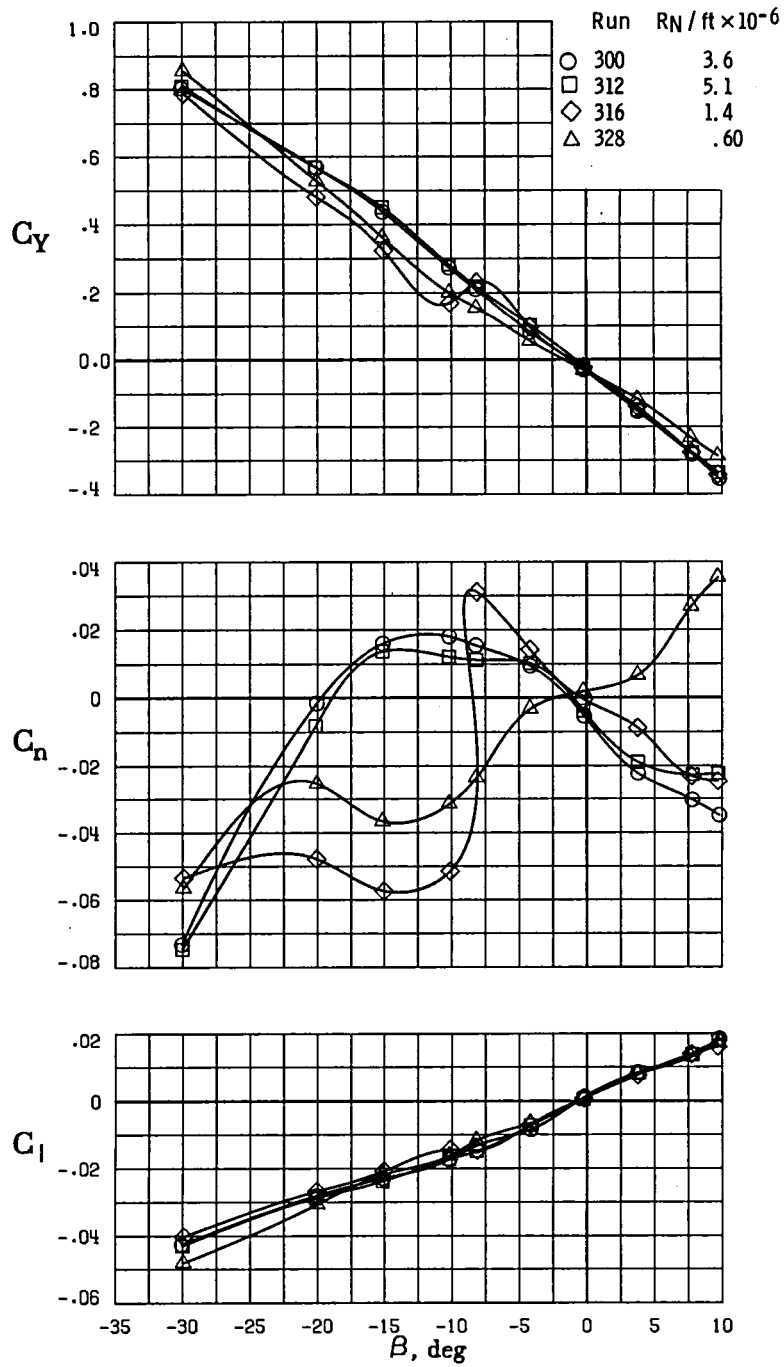
(a) $\alpha = -80°$; $\delta_c = 0°$; $\delta_f = -10°$; $\delta_s = -30°$.

Figure 13.- Lateral-directional aerodynamic characteristics
at negative high angles of attack for various Reynolds
numbers.

Run R_N/ ft $\times 10^{-6}$

O   301   3.5
□   313   4.9
◇   317   1.4
△   329   .60
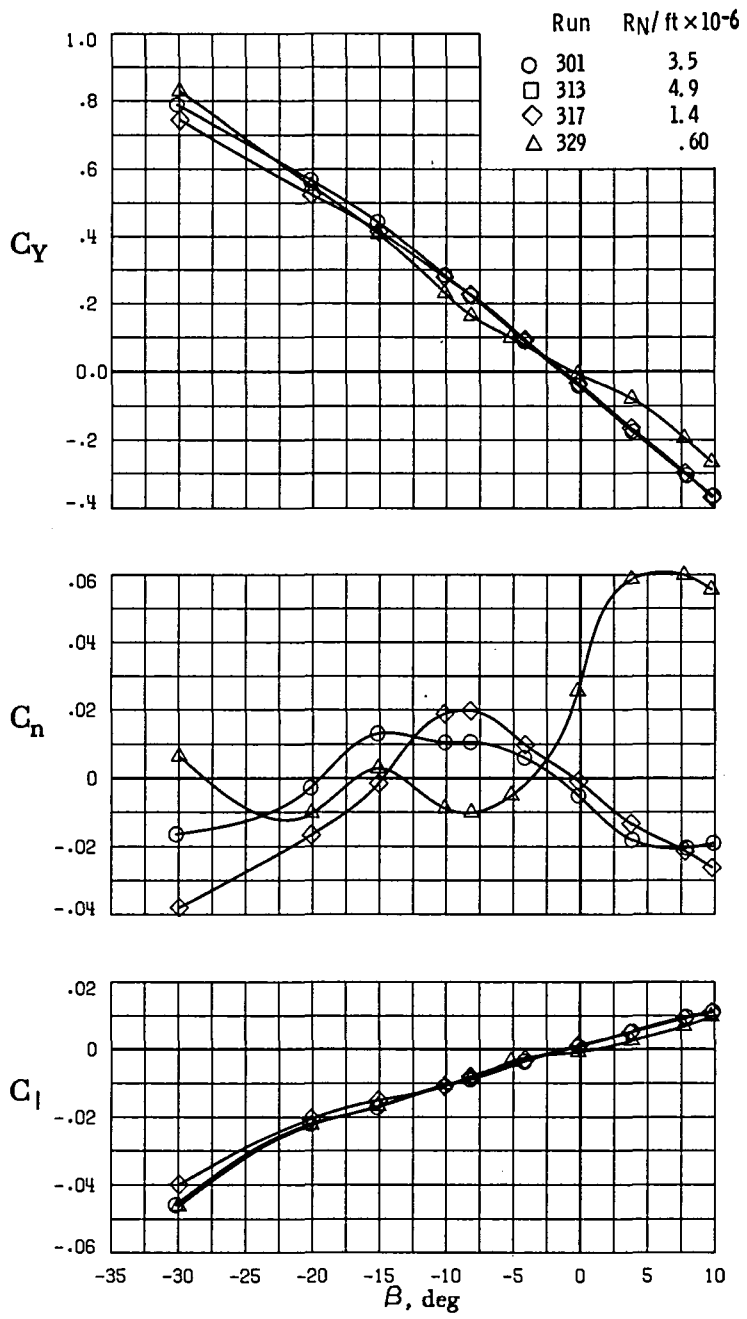
(b) $\alpha = -60°$; $\delta_c = 0°$; $\delta_f = -10°$; $\delta_s = -30°$.

Figure 13.- Continued.
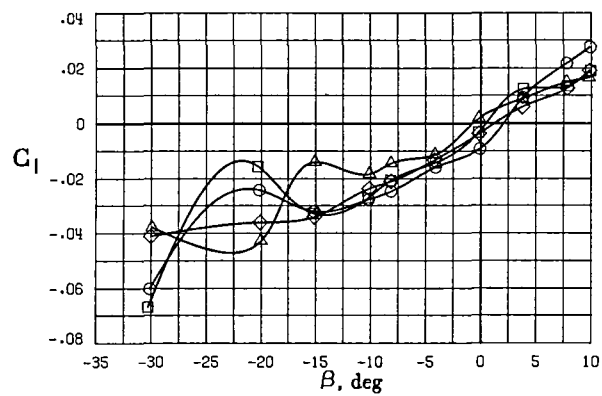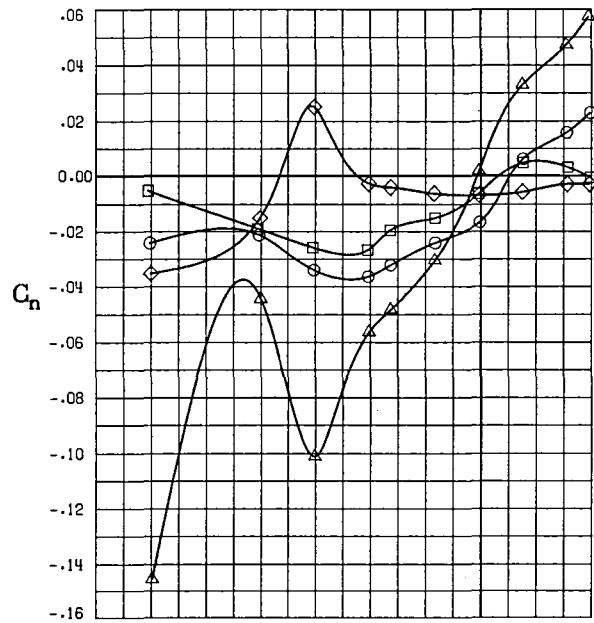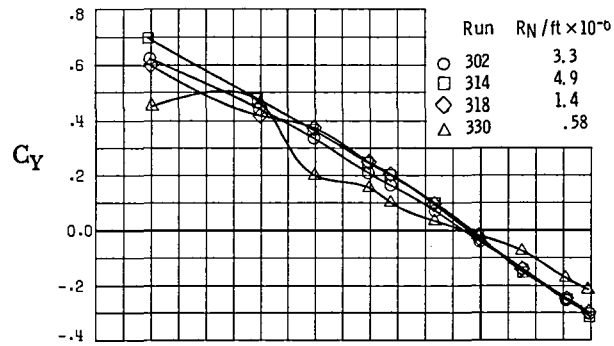
(c) $\alpha = -40°$; $\delta_c = 0°$; $\delta_f = -10°$; $\delta_s = -30°$.

Figure 13.- Continued.
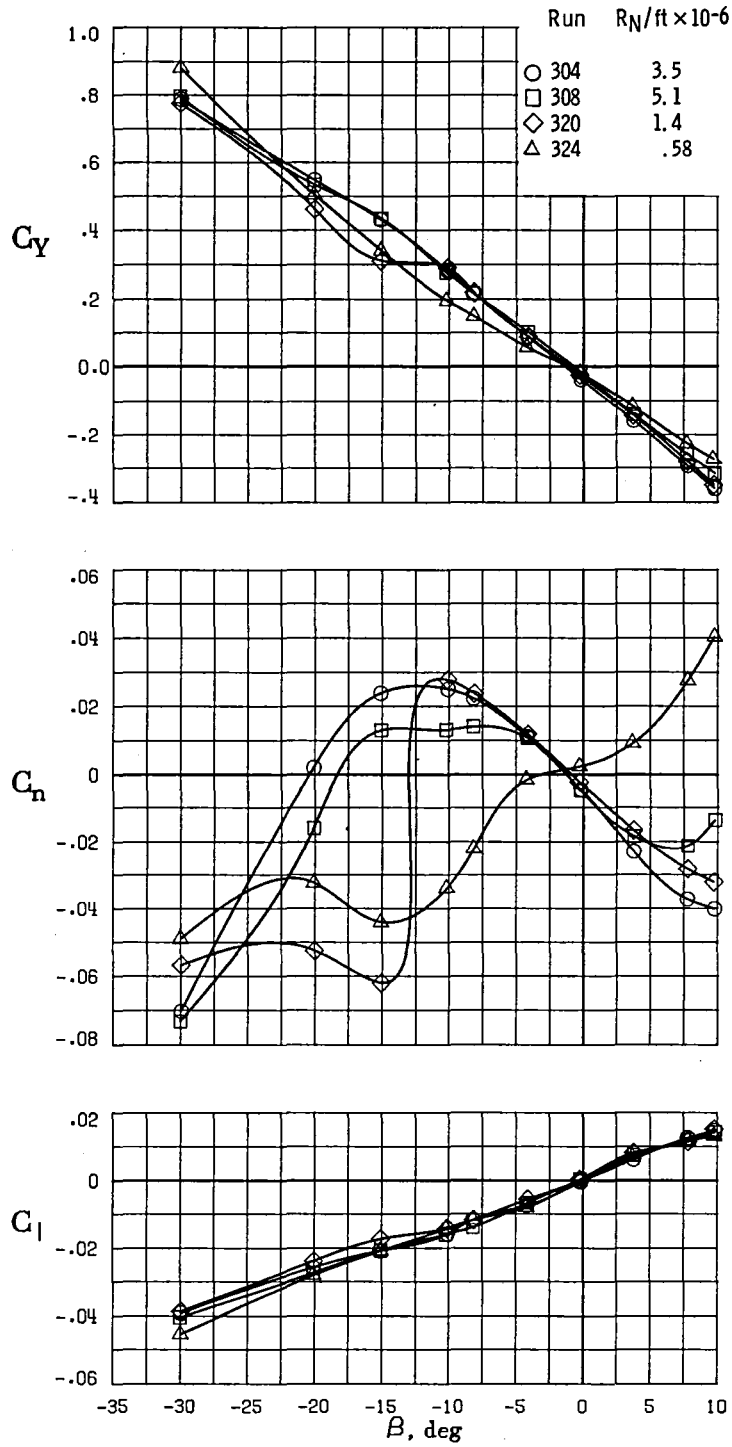
(d) $\alpha = -80°$; $\delta_c = 30°$; $\delta_f = -10°$; $\delta_s = -30°$.

Figure 13.- Continued.
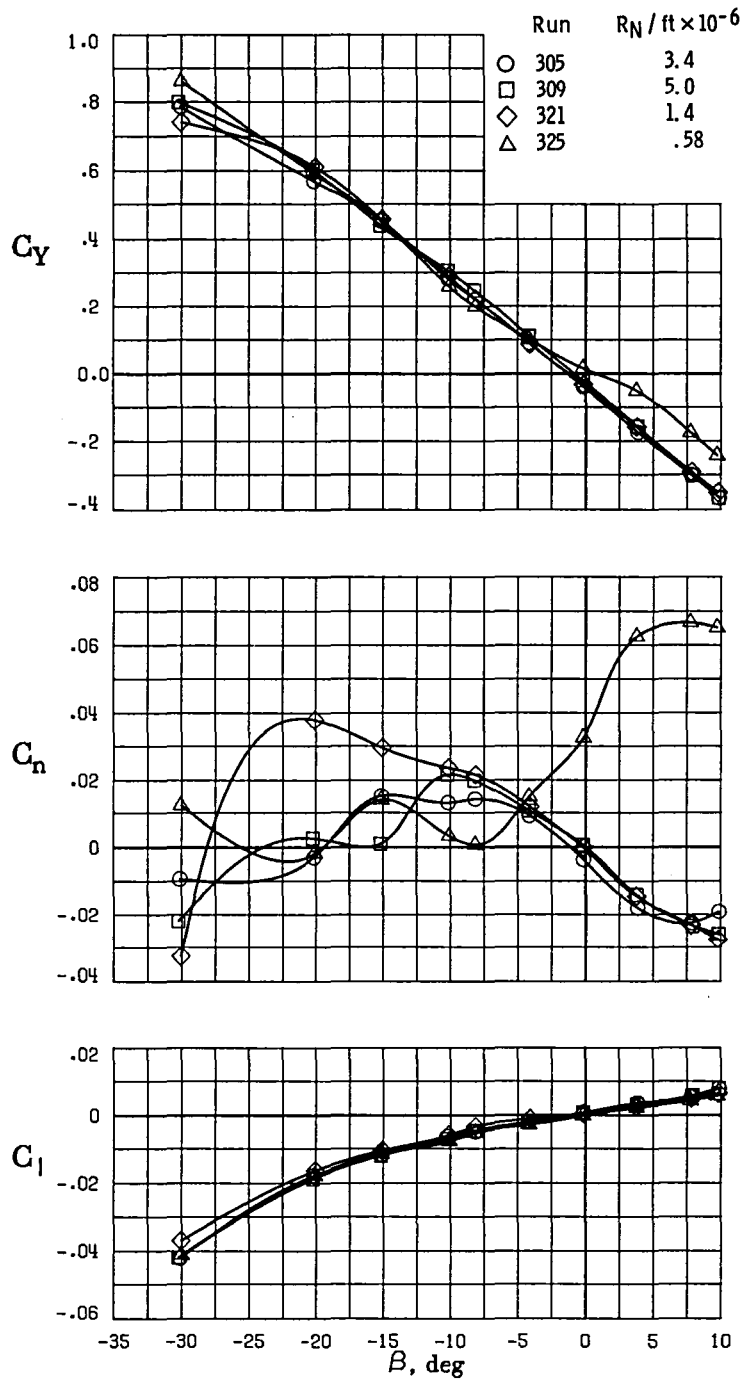
(e) $\alpha = -60°$; $\delta_c = 30°$; $\delta_f = -10°$; $\delta_s = -30°$.

Figure 13.- Continued.
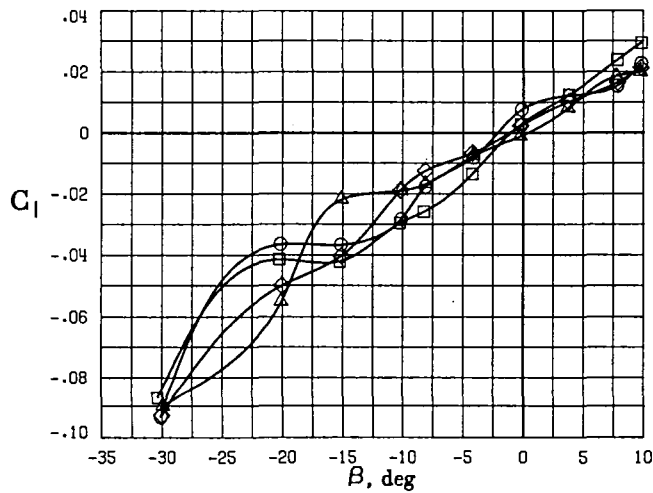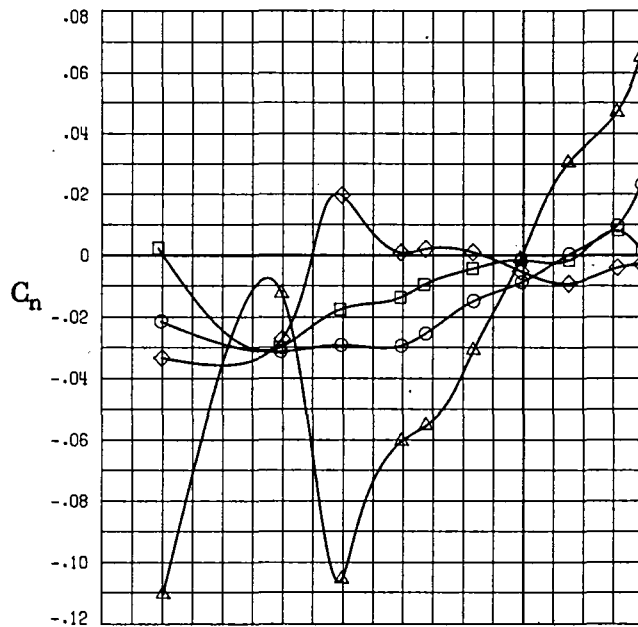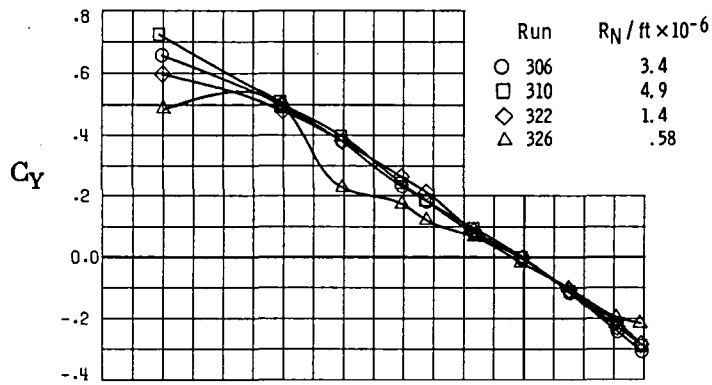
(f) $\alpha = -40°$; $\delta_c = 30°$; $\delta_f = -10°$; $\delta_s = -30°$.

Figure 13.- Concluded.
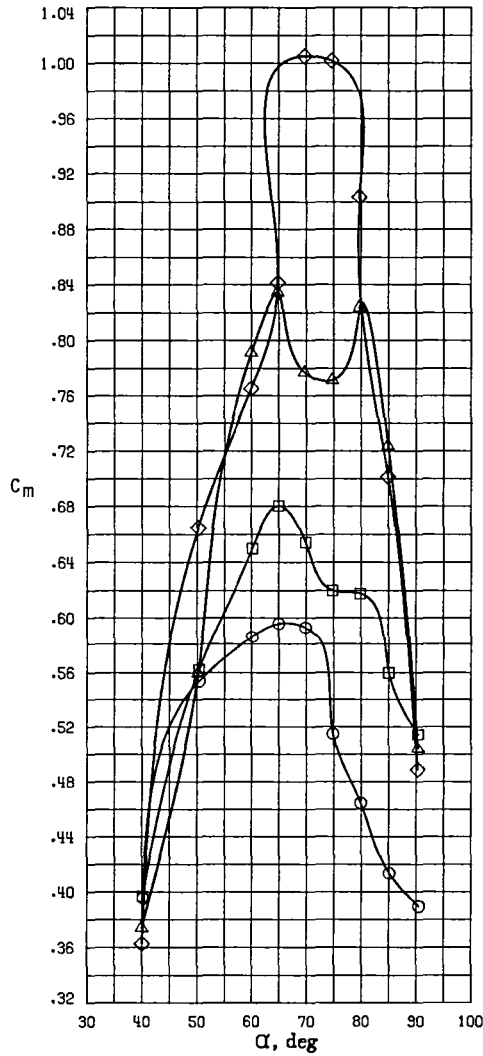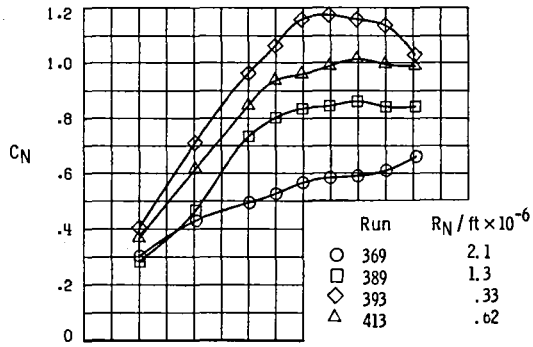
Figure 14.- Longitudinal aerodynamic characteristics
of fuselage with canards. Wing off; tail off;
strakes off for various Reynolds numbers;
$\beta = 0°$; $\delta_c = -60°$.
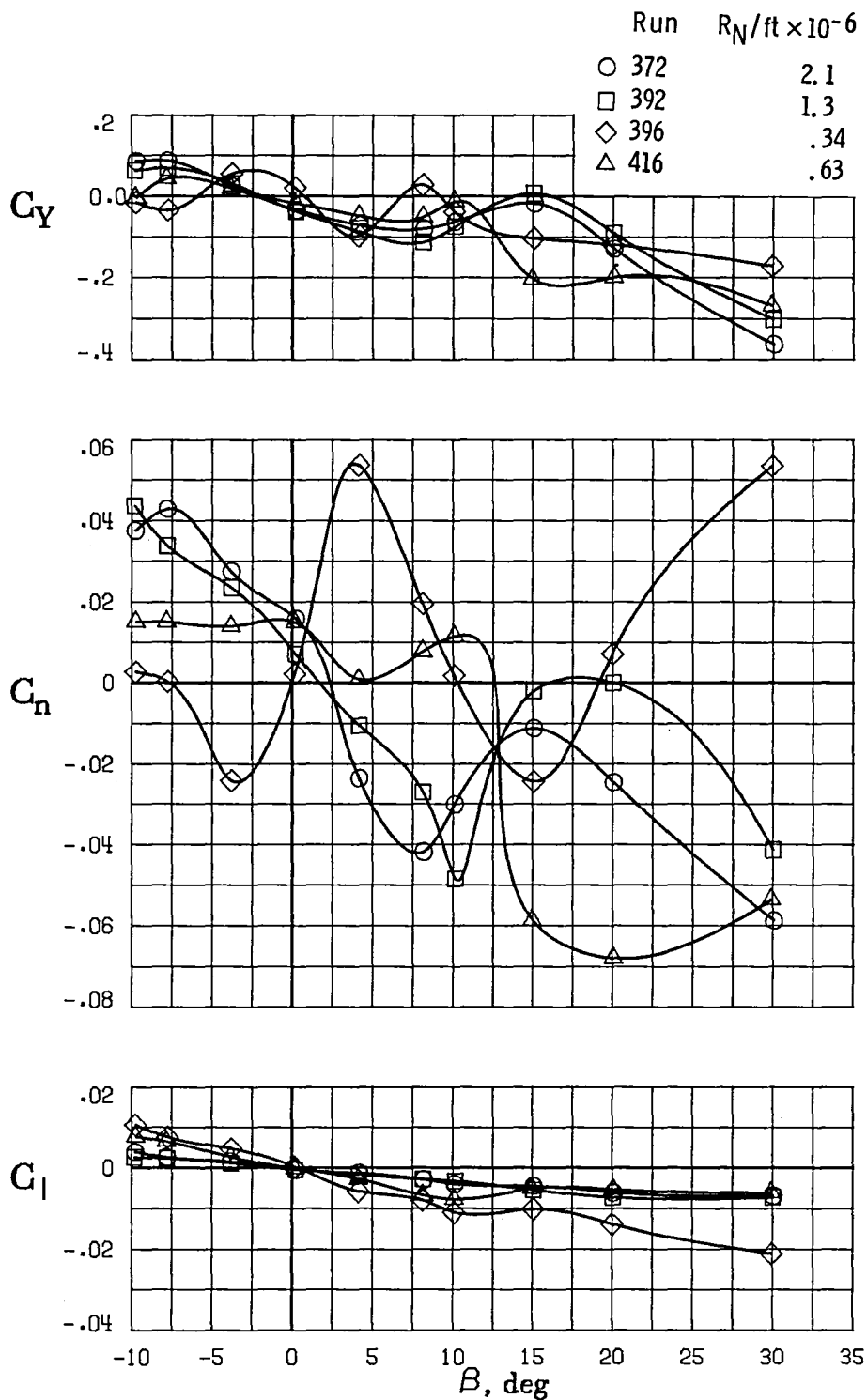
(a) $\alpha = 40°$; $\delta_c = -60°$.

Figure 15.- Lateral-directional aerodynamic characteristics of
fuselage with canards. Wing off; tail off; strakes off for
various Reynolds numbers.
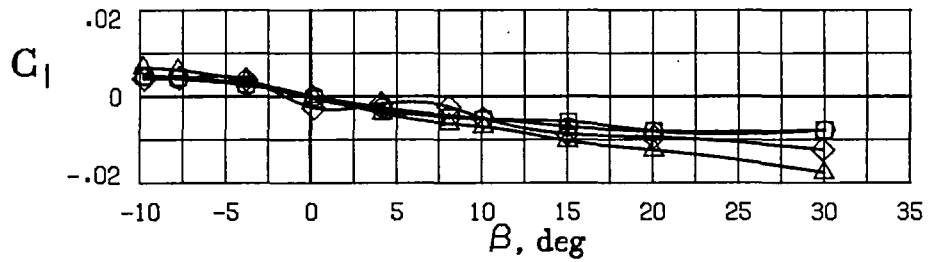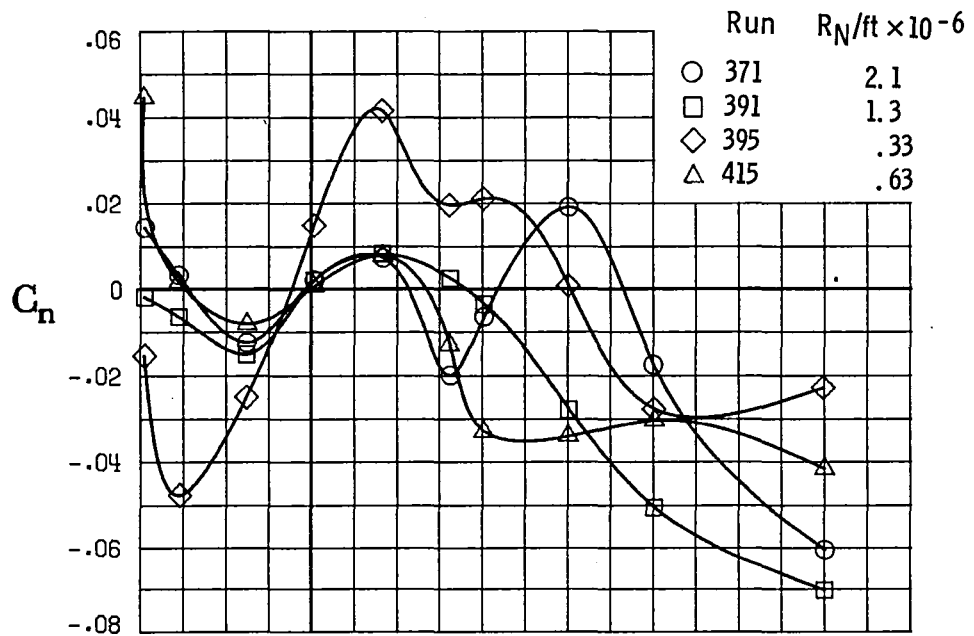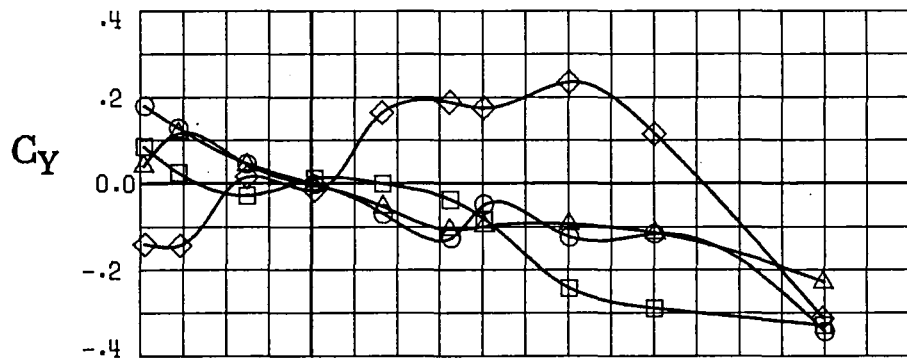
(b) $\alpha = 60°$; $\delta_c = -60°$.

Figure 15.- Continued.
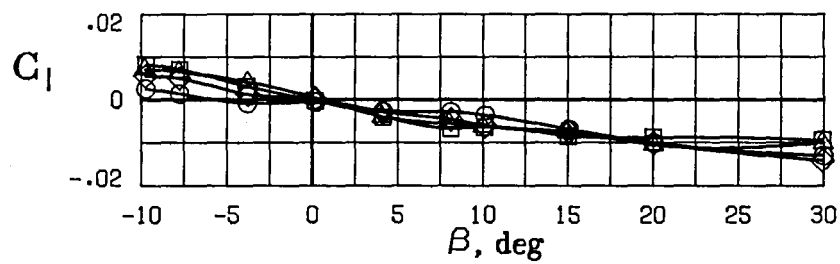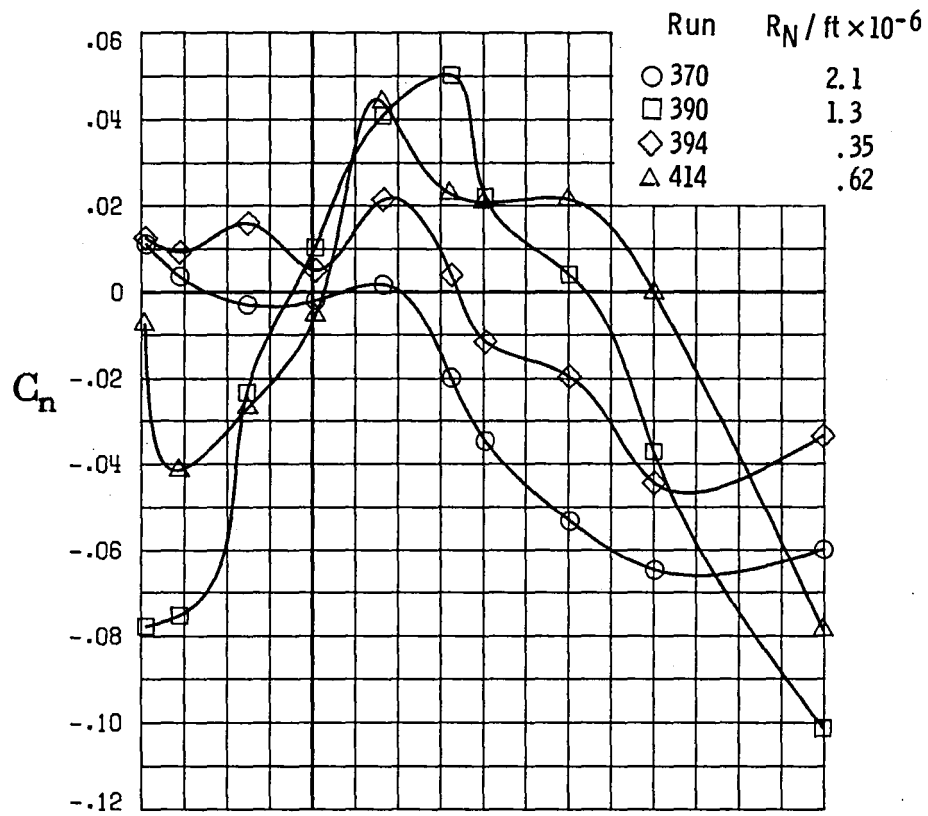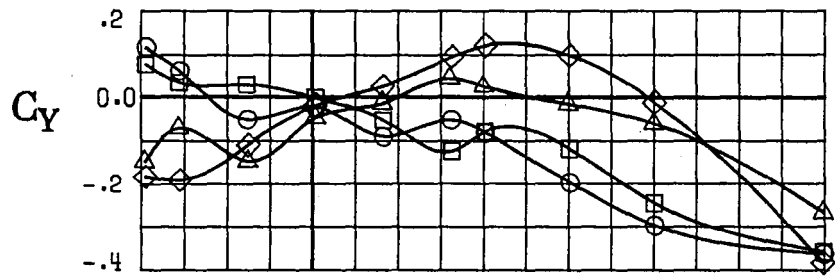
(c) $\alpha = 80°$; $\delta_c = -60°$.

Figure 15.- Concluded.
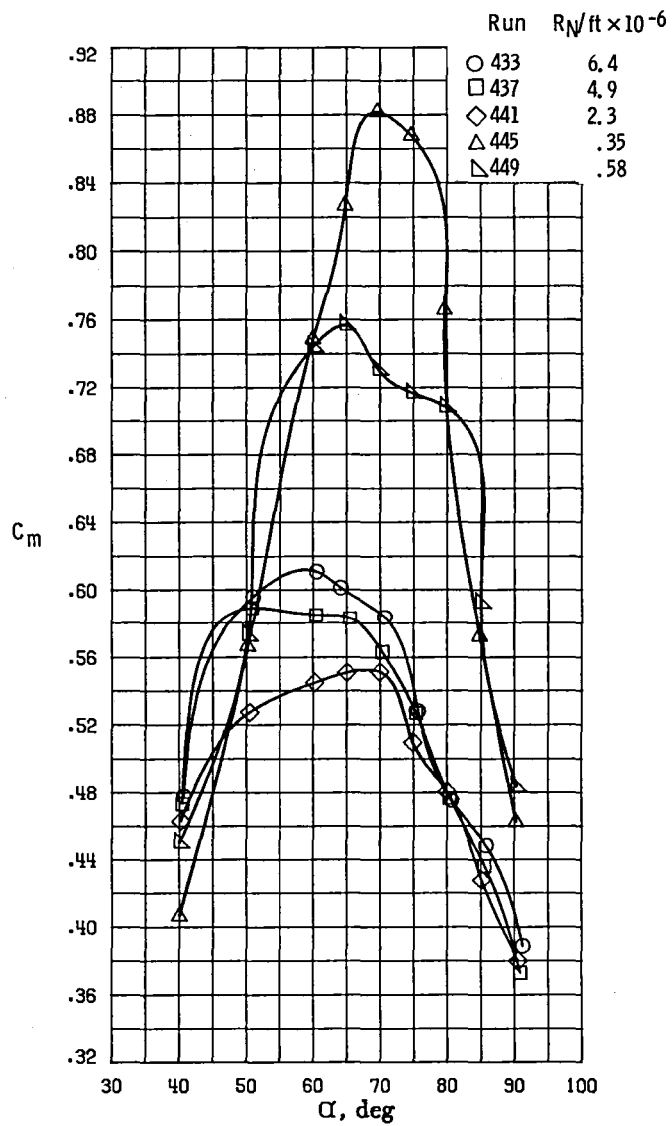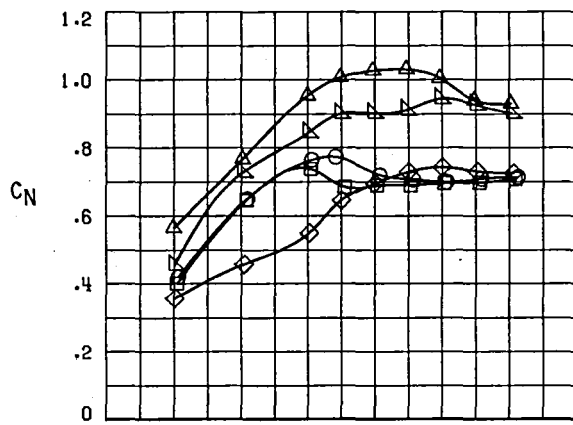
Figure 16.- Longitudinal aerodynamic characteristics
of fuselage alone for various Reynolds numbers
with β = 0°.
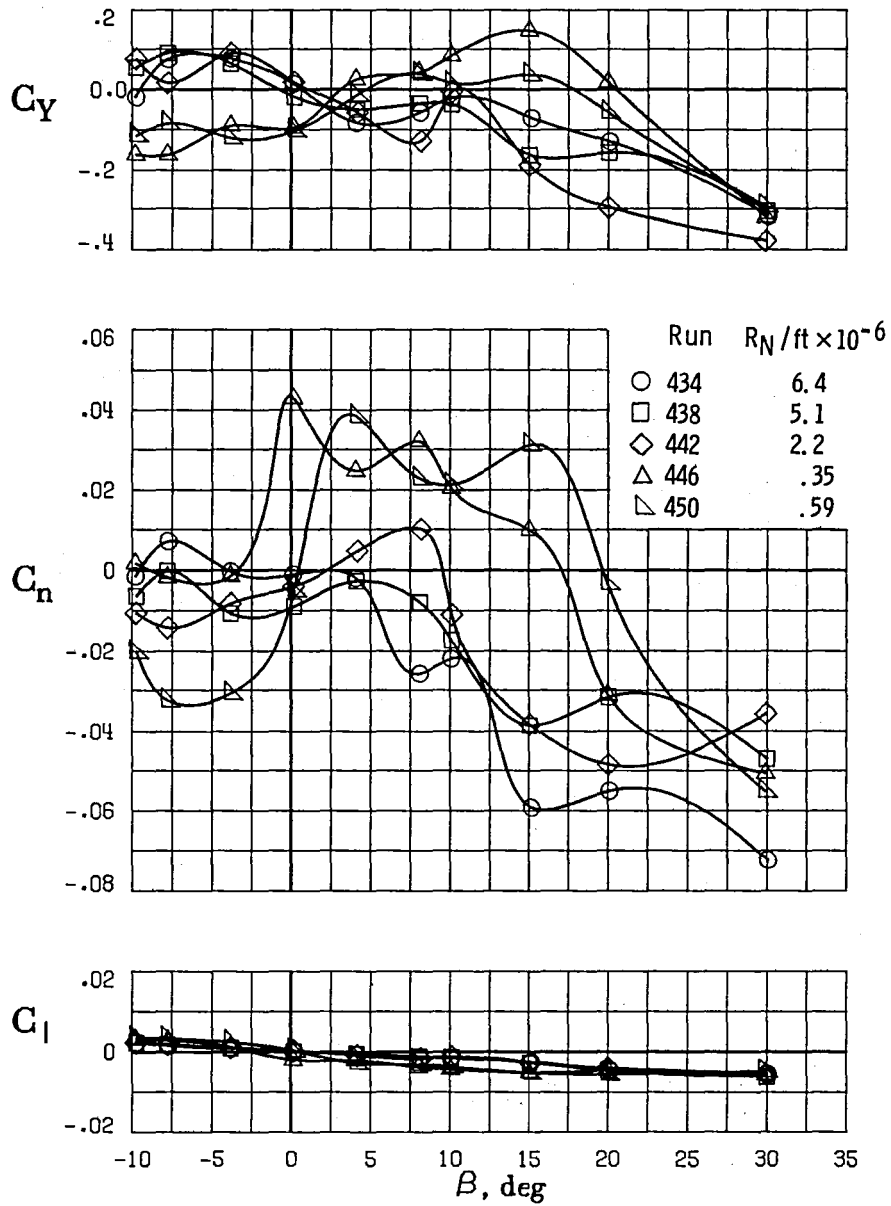
(a)   α = 80°.

Figure 17.- Lateral-directional aerodynamic characteristics
of fuselage alone for various Reynolds numbers.
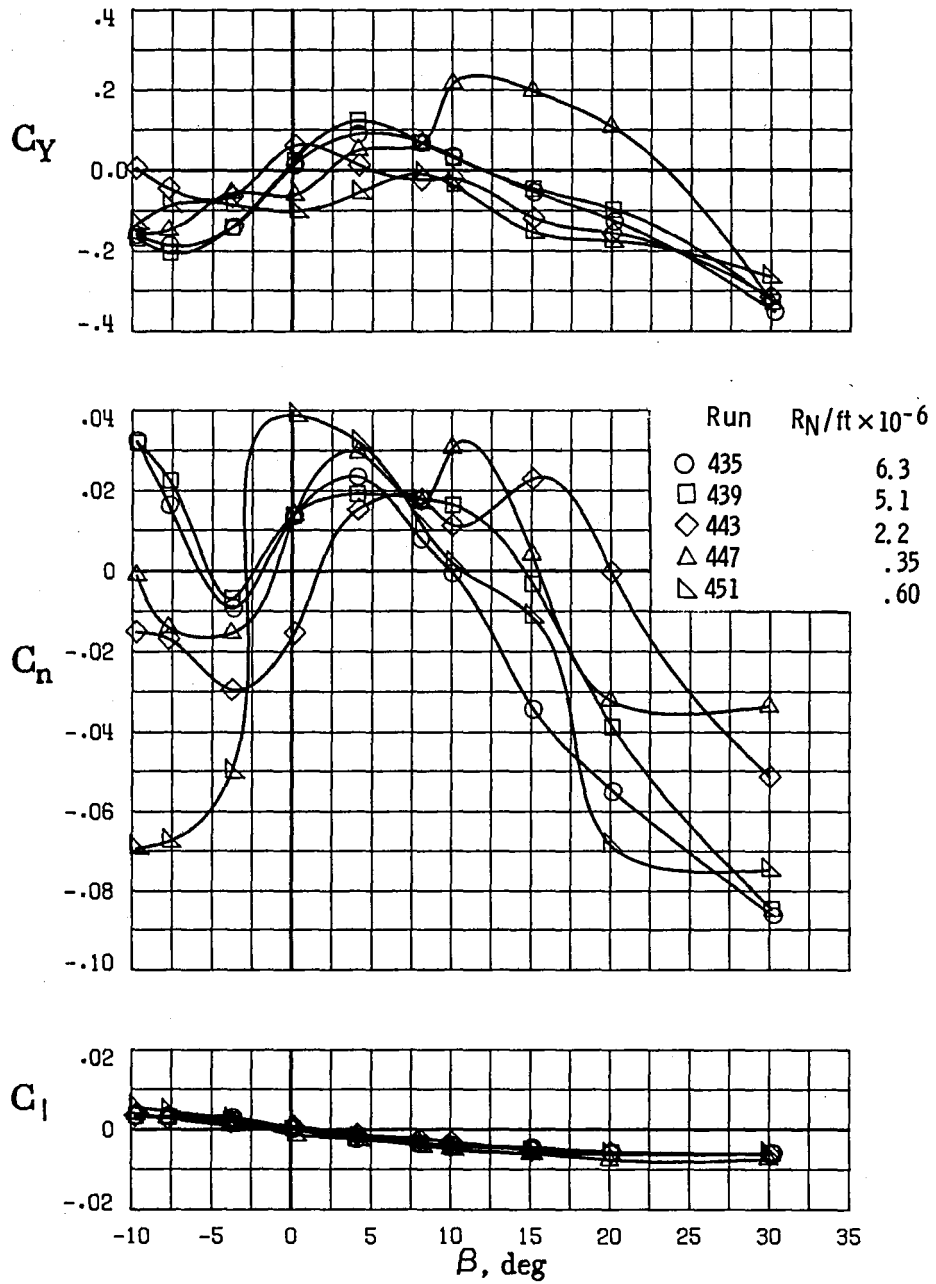
(b) α = 60°.

Figure 17.- Continued.
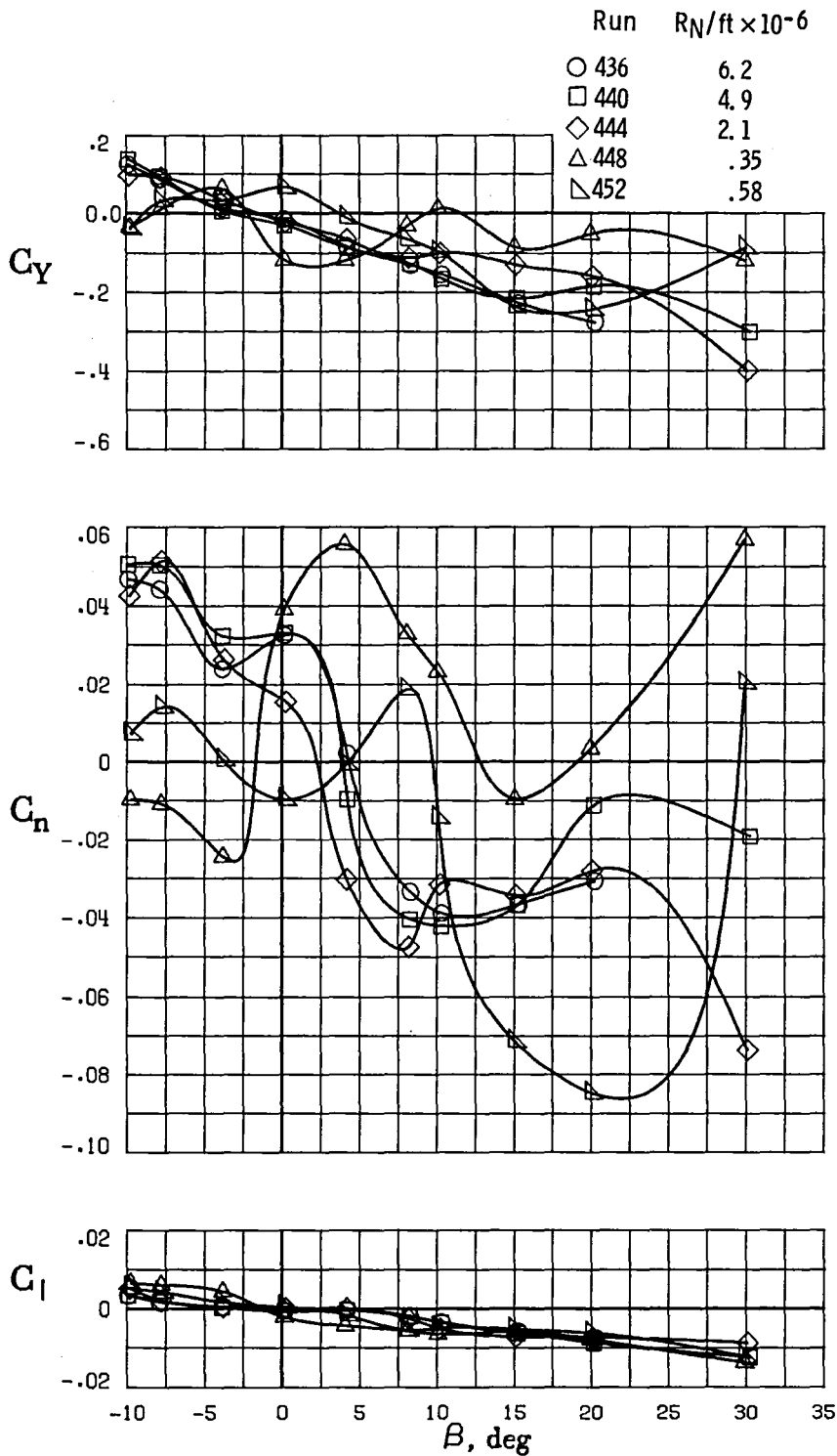
(c) $\alpha = 40°$.

Figure 17.- Concluded.

APPENDIX

TABULATED DATA

RUN   6   Q= 60.00 PSF   RN/FT= 1.407   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
40.83	-.01	1.9699	-.0631	-.2215	-.0218	.0111	-.0023
50.82	.17	2.1625	-.0870	-.2802	.0064	-.0059	.0045
60.63	.14	2.1925	-.1040	-.3651	-.0004	-.0036	.0001
70.27	.18	2.2171	-.1132	-.4683	-.0061	-.0069	-.0004
80.21	.13	2.2350	-.1199	-.5497	-.0210	-.0155	.0019
90.73	-.03	2.1470	-.1234	-.6171	-.0365	-.0347	.0007

RUN   7   Q= 52.50 PSF   RN/FT= 1.301   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
40.67	*****	2.0004	-.0704	-.1461	.0998	.0301	.0244
40.68	-5.08	1.9416	-.0662	-.1913	.0947	-.0012	.0131
40.66	.01	1.9631	-.0646	-.2180	-.0227	.0121	-.0019
40.66	5.13	1.9543	-.0645	-.1893	-.0733	.0073	-.0151
40.66	10.01	2.0118	-.0692	-.1285	-.0868	-.0320	-.0243
40.69	14.98	2.1140	-.0709	-.1393	-.0451	-.0408	-.0253
40.71	20.03	2.1112	-.0699	-.1258	-.0890	-.0485	-.0582

RUN   8   Q= 58.40 PSF   RN/FT= 1.364   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
60.63	-9.95	2.2153	-.1041	-.2503	.0288	.0477	.0109
60.62	-4.92	2.2147	-.1041	-.2963	-.0095	.0048	.0035
60.58	-.03	2.1767	-.1041	-.3620	.0052	-.0029	-.0005
60.59	5.04	2.2191	-.1045	-.3045	.0194	-.0048	-.0038
60.60	10.10	2.2279	-.1015	-.2552	-.0288	-.0430	-.0118
60.63	15.06	2.2257	-.1028	-.2016	-.1161	-.0842	-.0191

RUN   9   Q=132.50 PSF   RN/FT= 3.033   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
41.02	.18	2.0212	-.0624	-.2183	.0001	.0147	-.0005
51.32	.23	2.2085	-.0845	-.2908	-.0033	-.0008	.0019
61.08	.19	2.2145	-.1005	-.3529	.0048	.0065	.0002
70.76	.20	2.2234	-.1143	-.4633	.0078	.0032	.0009
80.66	.13	2.2080	-.1150	-.6444	.0006	-.0015	.0009
91.12	.14	2.1383	-.1219	-.7766	-.0037	-.0047	.0022

RUN 10   Q=133.40 PSF   RN/FT= 3.017   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
41.07	-9.81	2.0450	-.0702	-.1355	.0853	.0214	.0255
40.98	-4.81	1.9606	-.0635	-.1892	.0998	-.0153	.0148
40.98	.17	2.0081	-.0612	-.2153	-.0081	.0151	-.0010
40.96	5.13	1.9749	-.0613	-.1849	-.1073	.0224	-.0184
41.02	10.13	2.0606	-.0658	-.1090	-.0876	-.0138	-.0294
41.09	15.09	2.1650	-.0722	-.0997	-.0742	-.0382	-.0360
41.10	20.08	2.1687	-.0740	-.1104	-.1254	-.0510	-.0597

RUN 11   Q=139.60 PSF   RN/FT= 3.096   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
61.14	-9.71	2.2365	-.0982	-.3050	-.0048	.0346	.0114
61.10	-4.81	2.2325	-.0994	-.3409	-.0292	-.0031	.0053
61.08	.15	2.2232	-.1006	-.3563	.0018	.0048	-.0002
61.09	5.14	2.2481	-.0988	-.3155	.0241	.0044	-.0037
61.10	10.09	2.2368	-.0940	-.2984	-.0034	-.0260	-.0121
61.12	15.05	2.2594	-.0946	-.2926	-.0368	-.0532	-.0217
61.07	20.06	2.2196	-.0945	-.2781	-.0992	-.0608	-.0307

RUN 12   Q=132.70 PSF   RN/FT= 3.004   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
80.65	-9.79	2.1788	-.1126	-.6598	.1064	.0635	.0226
80.62	-4.82	2.1926	-.1145	-.6523	.0617	.0368	.0123
80.62	.12	2.2018	-.1142	-.6498	.0047	-.0008	.0013
80.62	5.11	2.2125	-.1136	-.6358	-.0418	-.0343	-.0097
80.63	10.07	2.2075	-.1109	-.6379	-.0926	-.0615	-.0204
80.62	15.05	2.1918	-.1079	-.6769	-.1677	-.0899	-.0333
80.61	20.00	2.1421	-.1059	-.6925	-.2358	-.1088	-.0420

RUN 13   Q=218.40 PSF   RN/FT= 5.012   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
41.61	.12	2.0673	-.0641	-.1947	.0100	.0159	-.0015
51.90	.15	2.2399	-.0840	-.2612	.0037	.0143	-.0058
61.75	.14	2.2940	-.1026	-.3016	.0144	.0070	.0033
71.36	.12	2.3069	-.1052	-.4808	.0464	.0198	.0019
81.26	.16	2.2530	-.1118	-.5963	.0184	.0083	.0019
91.69	.15	2.1745	-.1208	-.7101	.0115	.0046	.0014

RUN 14   Q=236.20 PSF   RN/FT= 5.187   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
81.22	-9.78	2.2301	-.1117	-.6260	.0669	.0524	.0223
81.20	-4.80	2.2466	-.1113	-.6028	.0379	.0298	.0119
81.21	.15	2.2713	-.1121	-.6023	.0249	.0087	.0016
81.17	5.08	2.2456	-.1082	-.6079	-.0043	-.0205	-.0100
81.18	10.09	2.2251	-.1068	-.6223	-.0767	-.0506	-.0204
81.26	15.09	2.2060	-.1064	-.6147	-.1434	-.0717	-.0321
81.25	20.03	2.1733	-.1052	-.6342	-.2102	-.0923	-.0423

RUN 15   Q=228.90 PSF   RN/FT= 5.091   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
61.74	-9.74	2.2543	-.0984	-.2963	-.0099	.0232	.0127
61.70	-4.78	2.2640	-.0990	-.3179	-.0342	-.0035	.0042
61.71	.19	2.2831	-.1021	-.3072	.0134	.0082	.0033
61.69	5.10	2.2646	-.0982	-.2951	.0304	.0030	-.0032
61.70	10.15	2.2630	-.0945	-.2889	-.0118	-.0317	-.0114
61.67	15.14	2.2105	-.0876	-.3228	-.0866	-.0705	-.0209
61.70	20.18	2.2114	-.0896	-.3435	-.1717	-.0947	-.0318

RUN 16   Q=218.30 PSF   RN/FT= 4.958   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
41.67	-9.83	2.0599	-.0729	-.1070	.1099	.0032	.0311
41.60	-4.77	2.0156	-.0645	-.1658	.0893	-.0244	.0122
41.70	.11	2.0677	-.0633	-.1932	.0155	.0178	-.0017
41.58	5.12	2.0268	-.0630	-.1590	-.1015	.0334	-.0169
41.64	10.12	2.0696	-.0685	-.0842	-.1200	.0101	-.0329
41.76	15.18	2.1325	-.0750	-.0473	-.1512	-.0318	-.0427
41.78	20.26	2.0729	-.0757	-.0277	-.2879	-.0578	-.0658

RUN 17   Q= 56.70 PSF   RN/FT= 1.380   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
40.57	.18	1.9600	-.0497	-.2170	.0012	.0098	-.0015
50.77	.16	2.1797	-.0749	-.2860	.0236	-.0042	.0042
70.25	.18	2.2371	-.0980	-.4735	.0111	-.0035	.0008
60.54	.16	2.1884	-.0914	-.3634	.0167	.0002	.0006
80.20	.19	2.2136	-.1057	-.5408	-.0093	-.0279	.0014
90.74	.17	2.1615	-.1104	-.5956	.0009	-.0123	.0014

RUN   18   Q= 60.50 PSF   RN/FT= 1.382   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
80.24	-9.80	2.2315	-.1036	-.4688	-.0002	-.0165	.0236
80.22	-4.80	2.2502	-.1060	-.4696	-.0291	-.0363	.0136
80.20	.16	2.2169	-.1079	-.5454	-.0341	-.0265	.0021
80.18	5.12	2.2377	-.1036	-.5246	.0181	.0109	-.0115
80.17	10.06	2.2146	-.0980	-.5201	.0185	-.0094	-.0225
80.16	15.03	2.1855	-.0943	-.5010	-.0678	-.0340	-.0328
80.16	20.00	2.1674	-.0915	-.4870	-.1586	-.0695	-.0415

RUN   19   Q= 58.30 PSF   RN/FT= 1.346   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
60.58	-9.74	2.1955	-.0932	-.2487	.0372	.0499	.0108
60.55	-4.82	2.1959	-.0937	-.2998	-.0022	.0057	.0037
60.52	.16	2.1580	-.0931	-.3566	.0125	.0008	-.0002
60.53	5.07	2.2036	-.0940	-.2918	.0334	-.0022	-.0038
60.54	10.09	2.2066	-.0921	-.2363	.0076	-.0318	-.0121
60.55	15.06	2.2316	-.0930	-.1512	-.0199	-.0437	-.0210
60.55	20.01	2.2048	-.0923	-.1824	-.1246	-.0880	-.0281

APPENDIX - Continued

RUN 20   Q= 56.70 PSF   RN/FT= 1.322   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
40.60	-9.74	1.9851	-.0586	-.1627	.0785	.0222	.0222
40.58	-4.78	1.9283	-.0571	-.1907	.0976	-.0046	.0142
40.55	.13	1.9388	-.0554	-.2159	-.0101	.0103	-.0020
40.55	5.13	1.9454	-.0554	-.1913	-.0653	.0073	-.0144
40.56	10.09	2.0029	-.0584	-.1555	-.0363	-.0220	-.0208
40.56	15.05	1.9571	-.0583	-.0575	-.0685	.0082	-.0466
40.58	20.02	1.9712	-.0689	.1644	-.0787	.0399	-.0532

RUN 21   Q= 56.60 PSF   RN/FT= 1.365   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
40.57	.16	2.1819	.0410	-.3885	-.0093	.0061	.0013
50.82	.15	2.3775	-.0666	-.3360	.0205	-.0087	.0085
60.65	.14	2.4048	-.1393	-.2927	-.0033	.0025	.0035
70.35	.15	2.4637	-.1790	-.3645	-.0073	-.0010	.0009
80.30	.17	2.4216	-.2164	-.3882	.0009	.0043	.0011
90.83	.14	2.4080	-.2551	-.3768	-.0135	-.0090	.0024

RUN 22   Q= 58.20 PSF   RN/FT= 1.361   MACH=0.20

ALPHA	BETA	c_N	c_A	c_m	c_Y	c_n	c_l
40.66	-9.74	2.2510	.0390	-.3624	.0209	.0269	.0205
40.64	-7.78	2.1924	.0405	-.3497	.0446	.0158	.0191
40.62	-3.82	2.1659	.0411	-.3702	.0727	-.0014	.0060
40.59	.14	2.1681	.0429	-.3861	-.0185	.0070	.0004
40.61	4.15	2.1737	.0410	-.3683	-.0560	.0067	-.0053
40.63	8.11	2.2273	.0408	-.3601	-.0215	-.0143	-.0142
40.66	10.08	2.2720	.0369	-.3523	-.0065	-.0254	-.0158
40.68	15.05	2.3308	.0427	-.3596	.0456	-.0333	-.0413
40.67	20.00	2.3282	.0409	-.3433	.0059	-.0367	-.0564
40.72	29.88	2.3032	.0575	.2625	.0112	.0594	-.0713

RUN 23   Q= 59.10 PSF   RN/FT= 1.364   MACH=0.20

ALPHA	BETA	c_N	c_A	c_m	c_Y	c_n	c_l
50.94	29.92	2.5197	-.0426	.0202	-.0354	-.0056	-.1057
50.94	20.03	2.5213	-.0465	-.2414	-.0531	-.0529	-.0559
50.89	15.06	2.4991	-.0475	-.2322	.0004	-.0463	-.0413
50.88	10.09	2.4630	-.0483	-.2803	.0609	-.0312	-.0317
50.86	8.11	2.4261	-.0502	-.2957	.0572	-.0289	-.0223
50.85	4.11	2.3652	-.0578	-.3292	.0528	-.0232	-.0009
50.85	.18	2.3522	-.0696	-.3284	.0171	-.0071	.0080
50.86	-3.82	2.3771	-.0594	-.3366	-.0626	.0270	.0052
50.88	-7.78	2.5177	-.0571	-.2978	-.0701	.0441	.0329
50.91	-9.75	2.5478	-.0562	-.2993	-.0770	.0488	.0373

RUN 24   Q= 59.30 PSF   RN/FT= 1.362   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
60.61	-9.76	2.3892	-.0927	-.3584	.0447	.0783	.0133
60.60	-7.76	2.3991	-.0985	-.3566	.0301	.0602	.0104
60.59	-3.83	2.4072	-.1282	-.3054	-.0042	.0211	.0045
60.60	.14	2.3957	-.1405	-.2888	-.0032	.0043	.0019
60.60	4.13	2.3952	-.1276	-.3049	-.0163	-.0171	-.0020
60.60	8.09	2.3841	-.1126	-.3274	-.0607	-.0477	-.0086
60.59	10.11	2.3924	-.1059	-.3364	-.0875	-.0634	-.0124
60.61	15.05	2.3449	-.1012	-.3176	-.1470	-.0898	-.0200
60.62	20.05	2.3345	-.1041	-.2778	-.1934	-.1004	-.0294
60.64	29.92	2.3428	-.0975	-.0295	-.1294	-.0295	-.0562

RUN 25   Q= 58.30 PSF   RN/FT= 1.347   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
65.46	29.92	2.2841	-.0993	-.1860	-.2689	-.1007	-.0574
65.47	20.05	2.3449	-.1209	-.3618	-.2447	-.1435	-.0290
65.45	15.03	2.3731	-.1302	-.3561	-.1275	-.1012	-.0216
65.46	10.09	2.4117	-.1345	-.3643	-.0735	-.0744	-.0126
65.45	8.12	2.4136	-.1339	-.3705	-.0514	-.0610	-.0089
65.45	4.12	2.4360	-.1386	-.3690	-.0269	-.0294	-.0037
65.45	.18	2.4344	-.1390	-.3632	-.0138	-.0028	.0012
65.47	-3.81	2.4315	-.1315	-.3689	.0071	.0313	.0059
65.46	-7.79	2.4279	-.1300	-.3706	.0246	.0662	.0110
65.46	-9.80	2.4127	-.1282	-.3659	.0454	.0791	.0141

RUN 26   Q= 58.60 PSF   RN/FT= 1.346   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
70.33	-9.80	2.4287	-.1755	-.3838	.0752	.0902	.0171
70.32	-7.79	2.4334	-.1777	-.3828	.0552	.0759	.0136
70.31	-3.81	2.4480	-.1783	-.3643	.0266	.0390	.0068
70.32	.05	2.4644	-.1794	-.3610	-.0036	.0022	.0020
70.31	4.14	2.4681	-.1791	-.3715	-.0365	-.0322	-.0046
70.31	8.10	2.4472	-.1736	-.3835	-.0628	-.0653	-.0114
70.30	10.10	2.4260	-.1702	-.3786	-.0842	-.0798	-.0159
70.35	15.06	2.4055	-.1599	-.3889	-.1478	-.1070	-.0249
70.36	20.03	2.3496	-.1472	-.3507	-.2377	-.1534	-.0331
70.32	29.91	2.3305	-.1360	-.1432	-.1514	-.0773	-.0527

RUN 27   Q= 57.60 PSF   RN/FT= 1.332   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
75.29	29.90	2.3517	-.1624	-.1648	-.1173	-.0727	-.0545
75.31	20.03	2.4040	-.1817	-.3238	-.1436	-.1338	-.0357
75.27	15.06	2.3841	-.1882	-.3841	-.1350	-.0956	-.0293
75.28	10.10	2.4212	-.1985	-.3700	-.0597	-.0613	-.0197
75.29	8.11	2.4467	-.1999	-.3759	-.0505	-.0508	-.0146
75.26	4.12	2.4623	-.2104	-.3933	-.0235	-.0311	-.0069
75.27	.16	2.4501	-.2096	-.3880	.0021	.0025	.0011
75.28	-3.80	2.4569	-.2114	-.3828	.0228	.0338	.0093
75.27	-7.79	2.4498	-.2076	-.3494	.0407	.0484	.0186
75.29	-9.78	2.4613	-.2076	-.3087	.0043	.0569	.0218

RUN 28   Q= 58.70 PSF   RN/FT= 1.340   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
80.33	-9.76	2.4492	-.2270	-.3449	.0085	.0338	.0257
80.32	-7.77	2.4688	-.2264	-.2969	-.0217	-.0005	.0217
80.30	-3.80	2.4573	-.2159	-.3204	-.0455	-.0187	.0130
80.27	.17	2.4390	-.2194	-.3827	.0000	.0044	.0006
80.26	4.14	2.4484	-.2152	-.3758	.0003	-.0006	-.0090
80.25	8.07	2.4453	-.2039	-.3443	.0068	-.0091	-.0187
80.25	10.11	2.4220	-.2146	-.3399	-.0043	-.0220	-.0224
80.24	15.06	2.4093	-.2113	-.3437	-.0721	-.0539	-.0327
80.23	20.00	2.3789	-.1973	-.3509	-.1265	-.0871	-.0423
80.23	29.88	2.3118	-.1825	-.2855	-.1591	-.1135	-.0592

RUN 29   Q= 57.70 PSF   RN/FT= 1.327   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
85.51	29.87	2.2982	-.2049	-.3169	-.1314	-.0928	-.0644
85.52	20.04	2.3611	-.2093	-.3815	-.1138	-.0828	-.0449
85.54	15.05	2.4050	-.2222	-.3629	-.0421	-.0403	-.0365
85.54	10.07	2.4222	-.2316	-.3722	.0112	-.0118	-.0259
85.53	8.11	2.4163	-.2305	-.3730	.0177	-.0005	-.0219
85.55	4.11	2.4234	-.2329	-.3891	.0307	.0086	-.0107
85.55	.12	2.4374	-.2352	-.3856	-.0388	-.0325	.0032
85.58	-3.79	2.4363	-.2340	-.3235	-.0939	-.0382	.0143
85.59	-7.73	2.4358	-.2369	-.3255	-.0591	-.0130	.0236
85.59	-9.78	2.4159	-.2365	-.3635	-.0144	.0279	.0281

RUN 30 Q= 58.40 PSF RN/FT= 1.332 MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
90.85	-9.77	2.3974	-.2438	-.3857	-.0134	.0207	.0300
90.86	-7.74	2.4080	-.2466	-.3857	-.0217	.0102	.0255
90.85	-3.81	2.4194	-.2521	-.3733	-.0286	-.0040	.0152
90.84	.15	2.4206	-.2571	-.3666	-.0260	-.0103	.0022
90.84	4.11	2.4213	-.2513	-.3649	.0068	.0047	-.0100
90.81	8.08	2.4084	-.2418	-.3955	.0271	.0017	-.0237
90.81	10.04	2.4066	-.2398	-.4055	.0031	-.0080	-.0276
90.80	15.02	2.3897	-.2290	-.4012	-.0392	-.0334	-.0388
90.80	19.97	2.3560	-.2138	-.4064	-.0952	-.0706	-.0466
90.79	29.86	2.2864	-.2159	-.3390	-.1168	-.0754	-.0684

RUN 31 Q= 57.30 PSF RN/FT= 1.318 MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
90.89	24.93	2.3236	-.2067	-.3842	-.1186	-.0768	-.0571
85.53	24.92	2.3497	-.2050	-.3370	-.0975	-.0765	-.0552
80.30	24.93	2.3516	-.1858	-.3076	-.1532	-.1061	-.0509
75.29	24.95	2.3689	-.1718	-.2739	-.1685	-.1202	-.0451
70.35	24.96	2.3570	-.1447	-.2445	-.1849	-.1216	-.0411
65.50	24.95	2.3457	-.1196	-.1681	-.1806	-.0952	-.0388
60.64	24.95	2.4348	-.1174	-.1433	-.1464	-.0664	-.0512
50.93	24.92	2.4735	-.0398	-.0918	-.0031	-.0037	-.0694
40.69	24.95	2.1887	.0255	.0005	-.1334	.0027	-.0595

74

RUN 32   Q= 57.70 PSF   RN/FT= 1.323   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
40.74	.17	2.4148	-.0863	-.1944	-.0014	.0011	.0040
51.04	.15	2.6562	-.1817	-.0733	.0215	-.0061	.0060
60.73	.16	2.6484	-.1945	-.0613	-.0091	-.0005	.0051
70.44	.16	2.6030	-.1697	-.2086	-.0101	.0014	.0011
80.38	.15	2.5638	-.1855	-.2662	-.0343	-.0230	.0035
90.87	.15	2.5085	-.1925	-.2946	-.0148	-.0096	.0007

RUN 33   Q= 58.10 PSF   RN/FT= 1.322   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
90.92	-9.69	2.5046	-.1885	-.3141	.0202	.0218	.0288
90.91	-7.77	2.5190	-.1922	-.3052	-.0051	.0123	.0250
90.90	-3.80	2.5217	-.1951	-.2842	-.0180	.0024	.0142
90.88	.16	2.5059	-.1944	-.3110	-.0432	-.0246	.0028
90.87	4.14	2.5149	-.1921	-.2770	-.0197	-.0029	-.0081
90.86	8.08	2.5152	-.1852	-.3105	-.0144	-.0116	-.0214
90.86	10.11	2.5076	-.1833	-.3217	-.0308	-.0163	-.0266
90.84	15.06	2.4605	-.1737	-.3279	-.0746	-.0373	-.0363
90.82	20.00	2.4242	-.1655	-.3359	-.1361	-.0682	-.0449
90.80	29.92	2.3473	-.1490	-.2642	-.1575	-.0676	-.0637

RUN 34   Q= 56.70 PSF   RN/FT= 1.305   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
85.52	29.92	2.3742	-.1540	-.2201	-.1600	-.0868	-.0615
85.52	20.00	2.4633	-.1671	-.2922	-.1446	-.0771	-.0417
85.54	15.08	2.5076	-.1756	-.2784	-.0696	-.0398	-.0339
85.56	10.12	2.5387	-.1840	-.2777	-.0088	-.0105	-.0243
85.56	8.11	2.5424	-.1865	-.2787	.0063	.0014	-.0197
85.56	4.14	2.5585	-.1898	-.2619	.0197	.0058	-.0095
85.57	.13	2.5488	-.1898	-.2695	-.0371	-.0212	.0029
85.58	-3.79	2.5615	-.1936	-.2319	-.0779	-.0449	.0141
85.60	-7.78	2.5687	-.1902	-.2303	-.0551	-.0188	.0233
85.61	-9.76	2.5508	-.1879	-.2322	-.0386	-.0090	.0280

RUN 35   Q= 57.60 PSF   RN/FT= 1.311   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
80.35	-9.76	2.5715	-.1857	-.1816	-.0324	-.0086	.0262
80.34	-7.76	2.5812	-.1872	-.1869	-.0536	-.0207	.0218
80.33	-3.79	2.5923	-.1867	-.1939	-.0782	-.0414	.0125
80.30	.20	2.5740	-.1859	-.2596	-.0616	-.0310	.0036
80.29	4.11	2.5615	-.1829	-.2624	.0078	.0129	-.0089
80.28	8.11	2.5707	-.1808	-.2436	.0056	.0006	-.0189
80.27	10.07	2.5513	-.1781	-.2428	-.0089	-.0115	-.0229
80.27	15.05	2.5166	-.1690	-.2482	-.0753	-.0424	-.0323
80.26	20.00	2.4832	-.1673	-.2449	-.1531	-.0809	-.0394
80.26	29.91	2.3968	-.1714	-.1378	-.1794	-.1083	-.0598

RUN   36   Q= 58.10 PSF   RN/FT= 1.315   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
75.35	29.93	2.4615	-.1850	.0065	-.0966	-.0761	-.0596
75.34	20.00	2.4798	-.1737	-.2118	-.1943	-.1226	-.0364
75.33	15.08	2.5062	-.1702	-.2602	-.1448	-.0835	-.0284
75.34	10.08	2.5475	-.1759	-.2412	-.0675	-.0417	-.0190
75.34	8.11	2.5536	-.1781	-.2385	-.0466	-.0389	-.0151
75.35	4.11	2.5562	-.1792	-.2554	-.0323	-.0188	-.0057
75.36	.16	2.5627	-.1792	-.2558	-.0041	.0028	.0018
75.38	-3.82	2.5634	-.1801	-.2335	.0023	.0186	.0087
75.41	-7.75	2.5867	-.1849	-.1630	.0035	.0168	.0176
75.42	-9.77	2.5749	-.1837	-.1610	.0126	.0285	.0224

RUN   37   Q= 56.70 PSF   RN/FT= 1.296   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
70.39	-9.78	2.5709	-.1735	-.2150	.0539	.0768	.0177
70.37	-7.81	2.5691	-.1718	-.2112	.0461	.0634	.0140
70.36	-3.80	2.5692	-.1694	-.2069	.0130	.0338	.0070
70.36	.18	2.5915	-.1700	-.2053	-.0144	.0014	.0012
70.35	4.15	2.5853	-.1684	-.2110	-.0395	-.0281	-.0047
70.35	8.12	2.5864	-.1705	-.2119	-.0704	-.0550	-.0123
70.35	10.13	2.5683	-.1691	-.2126	-.0930	-.0677	-.0167
70.35	15.09	2.5334	-.1681	-.2171	-.1588	-.0983	-.0269
70.36	20.05	2.5170	-.1733	-.1731	-.2434	-.1528	-.0359
70.34	29.92	2.4904	-.1865	.0318	-.1617	-.0871	-.0593

RUN 38   Q= 57.40 PSF   RN/FT= 1.303   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
65.59	29.94	2.5704	-.1903	.0533	-.1919	-.0978	-.0721
65.56	20.06	2.5443	-.1784	-.1572	-.2206	-.1472	-.0373
65.55	15.05	2.5712	-.1692	-.1589	-.1295	-.0896	-.0264
65.56	10.07	2.6050	-.1677	-.1656	-.0728	-.0663	-.0159
65.56	8.08	2.5905	-.1663	-.1660	-.0625	-.0514	-.0122
65.58	4.11	2.5785	-.1651	-.1765	-.0307	-.0266	-.0043
65.58	.18	2.6064	-.1669	-.1845	-.0136	.0015	.0018
65.60	-3.78	2.5916	-.1664	-.1808	.0155	.0338	.0071
65.61	-7.77	2.5985	-.1686	-.1773	.0423	.0637	.0140
65.63	-9.75	2.5969	-.1695	-.1746	.0498	.0767	.0175

RUN 39   Q= 57.60 PSF   RN/FT= 1.301   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
60.75	-9.76	2.6381	-.1785	-.1098	.0634	.0713	.0204
60.75	-7.78	2.6351	-.1799	-.1069	.0398	.0586	.0156
60.74	-3.81	2.6380	-.1833	-.0916	.0067	.0262	.0090
60.72	.18	2.6290	-.1923	-.0620	-.0050	-.0010	.0051
60.72	4.12	2.6278	-.1825	-.0902	-.0226	-.0207	-.0052
60.72	8.13	2.6376	-.1790	-.0965	-.0589	-.0473	-.0128
60.72	10.10	2.6396	-.1784	-.0972	-.0726	-.0594	-.0178
60.72	15.07	2.6228	-.1777	-.0910	-.1261	-.0861	-.0305
60.70	20.06	2.5949	-.1797	-.0769	-.1682	-.1030	-.0450
60.67	29.91	2.5529	-.1712	.0820	-.1176	-.0347	-.0792

RUN 40   Q= 56.40 PSF   RN/FT= 1.286   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
50.95	29.91	2.5948	-.1203	.0747	-.0453	-.0054	-.1171
51.00	20.05	2.7278	-.1456	-.0996	-.0844	-.0699	-.0660
50.99	15.06	2.6480	-.1436	-.0798	-.0581	-.0467	-.0425
50.98	10.10	2.6457	-.1558	-.0701	.0246	-.0301	-.0324
50.99	8.13	2.6582	-.1606	-.0764	.0419	-.0315	-.0254
50.99	4.13	2.6456	-.1690	-.0819	.0501	-.0249	-.0089
51.02	.17	2.6401	-.1816	-.0732	.0242	-.0079	.0061
51.02	-3.78	2.6519	-.1700	-.0820	-.0495	.0280	.0140
51.05	-7.76	2.7004	-.1685	-.0566	-.0283	.0493	.0380
51.07	-9.76	2.7280	-.1661	-.0506	.0076	.0550	.0405

RUN 41   Q= 58.50 PSF   RN/FT= 1.307   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
40.76	-9.74	2.4221	-.0782	-.1676	.0354	.0126	.0276
40.74	-7.78	2.4012	-.0798	-.1520	.0472	.0091	.0161
40.73	-3.84	2.3851	-.0821	-.1748	.0495	.0016	.0037
40.74	.18	2.4022	-.0839	-.1943	-.0078	.0011	.0041
40.71	4.12	2.3658	-.0816	-.1754	-.0498	.0059	-.0004
40.71	8.14	2.3981	-.0779	-.1661	-.0285	-.0072	-.0165
40.72	10.08	2.4306	-.0727	-.1793	-.0082	-.0096	-.0269
40.71	15.04	2.4524	-.0639	-.1974	.0042	-.0246	-.0514
40.67	20.03	2.4012	-.0539	-.2014	-.0432	-.0274	-.0639
40.73	29.91	2.4121	-.0577	.2196	-.1555	.0179	-.0866

RUN 42 Q= 57.40 PSF RN/FT= 1.300 MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
40.85	.18	2.6474	-.1173	.0335	.0044	-.0014	0.0000
51.07	.15	2.8534	-.1400	.0380	.0018	-.0051	.0060
60.75	.17	2.7163	-.1339	-.0128	-.0209	-.0043	.0059
70.39	.15	2.6605	-.1245	-.1481	-.0166	.0014	.0018
80.32	.16	2.6253	-.1292	-.2214	-.0590	-.0333	.0031
90.84	.17	2.5551	-.1344	-.2569	-.0243	-.0044	.0035

RUN 43 Q= 58.10 PSF RN/FT= 1.302 MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
90.88	-9.73	2.5486	-.1312	-.2781	.0191	.0287	.0275
90.87	-7.77	2.5588	-.1339	-.2780	.0061	.0156	.0241
90.86	-3.80	2.5606	-.1349	-.2494	-.0210	.0084	.0141
90.85	.17	2.5610	-.1370	-.2522	-.0435	-.0136	.0022
90.84	4.13	2.5684	-.1309	-.2548	-.0240	-.0111	-.0116
90.83	8.09	2.5620	-.1263	-.2851	-.0160	-.0206	-.0233
90.82	10.09	2.5524	-.1253	-.2903	-.0510	-.0211	-.0253
90.80	15.06	2.5094	-.1197	-.3085	-.0891	-.0439	-.0354
90.80	20.01	2.4840	-.1126	-.3241	-.1567	-.0683	-.0448
90.78	29.92	2.3569	-.0995	-.2568	-.1777	-.0698	-.0647

RUN   44   Q= 57.80 PSF   RN/FT= 1.298   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
85.47	-9.72	2.5874	-.1283	-.1925	-.0309	-.0024	.0272
85.47	-7.76	2.6054	-.1300	-.1897	-.0422	-.0142	.0235
85.47	-3.78	2.6275	-.1343	-.1944	-.0776	-.0344	.0146
85.45	.19	2.6081	-.1329	-.2092	-.0422	-.0186	.0023
85.45	4.11	2.6062	-.1303	-.2151	-.0001	.0041	-.0094
85.44	8.11	2.5883	-.1265	-.2324	-.0108	-.0061	-.0195
85.43	10.10	2.5765	-.1220	-.2544	-.0355	-.0170	-.0235
85.50	15.02	2.5613	-.1181	-.2464	-.0869	-.0436	-.0333
85.49	19.99	2.4975	-.1136	-.2636	-.1535	-.0769	-.0405
85.47	29.87	2.3993	-.1022	-.2092	-.1824	-.0795	-.0598

RUN   45   Q= 57.40 PSF   RN/FT= 1.292   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
80.33	-9.75	2.6095	-.1277	-.1473	-.0189	-.0086	.0252
80.33	-7.76	2.6225	-.1277	-.1484	-.0372	-.0186	.0217
80.31	-3.81	2.6250	-.1296	-.1596	-.0695	-.0394	.0127
80.29	.15	2.6286	-.1307	-.2168	-.0667	-.0340	.0033
80.28	4.14	2.6176	-.1269	-.2137	.0103	.0162	-.0091
80.28	8.09	2.6221	-.1222	-.2052	-.0163	-.0021	-.0179
80.27	10.09	2.6145	-.1198	-.2107	-.0240	-.0152	-.0222
80.27	15.06	2.5614	-.1156	-.2034	-.0903	-.0418	-.0308
80.26	20.00	2.5418	-.1147	-.1489	-.1178	-.0586	-.0390
80.25	29.91	2.4288	-.1064	-.1546	-.2078	-.1088	-.0558

RUN 46   Q= 56.40 PSF   RN/FT= 1.279   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
75.32	-9.73	2.6419	-.1294	-.1012	.0230	.0173	.0228
75.31	-7.76	2.6537	-.1301	-.1031	-.0023	.0084	.0190
75.30	-3.81	2.6406	-.1287	-.1576	-.0028	.0009	.0106
75.28	.18	2.6418	-.1266	-.2066	-.0231	.0015	.0019
75.28	4.15	2.6288	-.1226	-.1949	-.0124	-.0086	-.0075
75.27	8.08	2.6297	-.1201	-.1683	-.0227	-.0147	-.0160
75.26	10.12	2.6245	-.1190	-.1661	-.0400	-.0244	-.0201
75.25	15.07	2.5775	-.1159	-.1927	-.1246	-.0736	-.0276
75.27	20.05	2.5545	-.1186	-.1074	-.1609	-.0947	-.0360
75.33	29.94	2.4912	-.1136	.0090	-.1508	-.0698	-.0541

RUN 47   Q= 57.20 PSF   RN/FT= 1.287   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
70.39	-9.72	2.6175	-.1215	-.1642	.0892	.0711	.0194
70.38	-7.76	2.6353	-.1230	-.1656	.0646	.0623	.0155
70.36	-3.80	2.6475	-.1230	-.1524	.0263	.0348	.0073
70.36	.16	2.6524	-.1228	-.1501	-.0168	.0008	.0015
70.35	4.15	2.6420	-.1214	-.1563	-.0528	-.0285	-.0058
70.34	8.13	2.6312	-.1194	-.1690	-.0888	-.0554	-.0130
70.34	10.09	2.6195	-.1172	-.1704	-.1085	-.0662	-.0170
70.34	15.07	2.5758	-.1138	-.1800	-.1741	-.0986	-.0258
70.34	20.06	2.5460	-.1152	-.1195	-.2465	-.1479	-.0316
70.33	29.89	2.5111	-.1134	.0382	-.1826	-.0766	-.0528

RUN 48   Q= 56.00 PSF   RN/FT= 1.272   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
65.52	-9.74	2.6324	-.1154	-.1174	.0710	.0729	.0162
65.52	-7.76	2.6406	-.1170	-.1228	.0489	.0598	.0130
65.51	-3.80	2.6553	-.1159	-.1224	.0157	.0315	.0068
65.50	.15	2.6588	-.1161	-.1235	-.0099	.0001	.0010
65.50	4.15	2.6479	-.1145	-.1202	-.0427	-.0266	-.0041
65.50	8.14	2.6580	-.1132	-.1188	-.0809	-.0509	-.0111
65.49	10.14	2.6487	-.1125	-.1193	-.0958	-.0666	-.0148
65.49	15.07	2.6140	-.1098	-.1161	-.1547	-.0939	-.0230
65.49	20.07	2.5789	-.1129	-.1072	-.2412	-.1457	-.0314
65.56	29.93	2.5399	-.1088	.0463	-.2159	-.0884	-.0672

RUN 49   Q= 54.40 PSF   RN/FT= 1.252   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
60.74	-9.76	2.6692	-.1172	-.0569	.0869	.0728	.0164
60.72	-7.79	2.6654	-.1170	-.0675	.0581	.0633	.0122
60.75	-3.82	2.6999	-.1239	-.0502	.0226	.0306	.0052
60.76	.19	2.7514	-.1353	-.0086	-.0143	-.0055	.0062
60.73	4.13	2.7039	-.1213	-.0568	-.0416	-.0285	-.0026
60.72	8.14	2.6821	-.1172	-.0573	-.0602	-.0535	-.0102
60.72	10.10	2.6663	-.1151	-.0526	-.0869	-.0613	-.0135
60.72	15.07	2.6452	-.1124	-.0420	-.1560	-.0925	-.0236
60.71	20.01	2.6319	-.1193	-.0020	-.1804	-.0952	-.0335
60.71	29.91	2.6545	-.1281	.1401	-.0917	-.0248	-.0688

RUN 50   Q= 55.10 PSF   RN/FT= 1.259   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
51.08	-9.77	2.9053	-.1455	.1649	.0332	.0394	.0410
51.10	-7.79	2.8990	-.1424	.1292	-.0197	.0413	.0357
51.07	-3.81	2.8496	-.1353	.0705	-.0253	.0247	.0132
51.07	.15	2.8557	-.1416	.0412	.0029	-.0050	.0069
51.06	4.12	2.8401	-.1309	.0717	.0216	-.0211	-.0132
51.06	8.13	2.8974	-.1305	.0960	.0555	-.0311	-.0301
51.07	10.08	2.9316	-.1327	.1104	.0571	-.0308	-.0378
51.07	15.06	2.9119	-.1404	.1389	-.0260	-.0473	-.0456
51.06	20.04	2.8933	-.1450	.1197	-.0863	-.0566	-.0672
51.00	29.90	2.7690	-.1305	.1824	-.0552	-.0055	-.1244

RUN 51   Q= 57.30 PSF   RN/FT= 1.283   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
40.84	-9.75	2.5716	-.1078	.0557	.0827	.0085	.0325
40.85	-7.78	2.5747	-.1110	.0715	.0768	.0101	.0206
40.85	.19	2.6418	-.1165	.0303	.0054	.0003	-.0011
40.83	4.14	2.5952	-.1111	.0509	-.0278	-.0037	-.0051
40.81	8.12	2.5701	-.1055	.0620	-.0513	-.0044	-.0200
40.81	10.12	2.5849	-.1035	.0543	-.0500	-.0024	-.0323
40.80	15.04	2.6040	-.0992	.0111	-.0478	-.0087	-.0549
40.77	20.02	2.5746	-.0917	-.0331	-.0562	-.0199	-.0692
40.82	29.91	2.5819	-.1024	.3840	-.1391	.0172	-.0937

RUN 52   Q= 56.30 PSF   RN/FT= 1.278   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
40.96	.17	2.6796	-.0920	.0326	.0146	-.0034	-.0001
51.14	.12	2.9221	-.1240	.0599	-.0062	-.0061	.0086
60.78	.13	2.7446	-.1129	.0081	-.0070	-.0051	.0067
70.40	.14	2.6819	-.1073	-.1457	-.0141	.0019	.0024
80.33	.16	2.6307	-.1106	-.2158	-.0595	-.0338	.0041
90.82	.15	2.5574	-.1171	-.2874	-.0492	-.0341	.0017

RUN 53   Q= 58.30 PSF   RN/FT= 1.296   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
90.86	-9.80	2.5868	-.1102	-.2531	-.0059	-.0027	.0285
90.85	-7.82	2.5824	-.1134	-.2429	-.0300	-.0026	.0257
90.83	-3.85	2.6055	-.1166	-.2253	-.0540	-.0188	.0152
90.82	.17	2.5609	-.1179	-.2755	-.0496	-.0244	.0027
90.81	4.08	2.5863	-.1116	-.2550	-.0108	-.0132	-.0109
90.80	8.05	2.5937	-.1066	-.2934	-.0295	-.0196	-.0229
90.79	11.03	2.5640	-.1043	-.3048	-.0485	-.0304	-.0279
90.79	14.99	2.5520	-.0993	-.3143	-.0847	-.0440	-.0360
90.77	19.93	2.4935	-.0941	-.3244	-.1418	-.0696	-.0443
90.75	29.81	2.3874	-.0830	-.2533	-.1722	-.0682	-.0641

RUN 54   Q= 58.10 PSF   RN/FT= 1.294   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
85.52	-9.77	2.6148	-.1103	-.1912	-.0274	-.0043	.0271
85.51	-7.81	2.6137	-.1127	-.1813	-.0317	-.0188	.0226
85.50	-3.84	2.6287	-.1140	-.1882	-.0688	-.0352	.0138
85.49	.14	2.6181	-.1126	-.2068	-.0438	-.0174	.0022
85.47	4.13	2.6061	-.1101	-.2053	-.0012	.0009	-.0110
85.46	8.06	2.6279	-.1086	-.2358	-.0025	-.0085	-.0194
85.46	10.00	2.5781	-.1051	-.2433	-.0313	-.0167	-.0238
85.45	15.01	2.5572	-.1020	-.2429	-.0812	-.0428	-.0319
85.44	19.96	2.5067	-.0963	-.2592	-.1630	-.0775	-.0408
85.47	29.84	2.4011	-.0865	-.1863	-.1765	-.0732	-.0598

RUN 55   Q= 57.90 PSF   RN/FT= 1.291   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
80.35	-9.80	2.6207	-.1068	-.1516	-.0197	-.0052	.0260
80.35	-7.85	2.6394	-.1108	-.1457	-.0375	-.0204	.0212
80.33	-3.85	2.6384	-.1099	-.1566	-.0752	-.0394	.0138
80.32	.14	2.6259	-.1113	-.2103	-.0601	-.0326	.0037
80.31	4.13	2.6421	-.1087	-.2011	.0221	.0159	-.0101
80.30	8.03	2.6113	-.1037	-.1974	-.0108	-.0031	-.0184
80.30	10.05	2.6072	-.1016	-.2067	-.0298	-.0139	-.0217
80.29	15.00	2.5843	-.0986	-.1994	-.0892	-.0429	-.0307
80.30	19.96	2.5013	-.0944	-.2089	-.1653	-.0798	-.0381
80.29	29.89	2.4223	-.0903	-.1392	-.1995	-.1015	-.0557

RUN   56   Q= 57.10 PSF   RN/FT= 1.282   MACH=0.20

ALPHA	BETA	c_N	c_A	c_m	c_Y	c_n	c_1
75.32	-9.77	2.6604	-.1125	-.0900	.0145	.0132	.0232
75.32	-7.81	2.6535	-.1117	-.0930	-.0101	.0026	.0176
75.30	-3.86	2.6557	-.1118	-.1342	-.0244	-.0027	.0100
75.27	.16	2.6460	-.1093	-.2016	-.0032	.0015	.0019
75.28	4.08	2.6518	-.1056	-.1806	-.0078	-.0084	-.0086
75.28	8.04	2.6408	-.1016	-.1523	-.0208	-.0098	-.0162
75.27	10.07	2.6305	-.1018	-.1489	-.0395	-.0228	-.0196
75.26	14.97	2.5785	-.0986	-.1691	-.1299	-.0651	-.0273
75.27	19.95	2.5605	-.1017	-.1050	-.1662	-.0939	-.0353
75.29	29.85	2.4877	-.0989	.0051	-.1358	-.0700	-.0533

RUN   57   Q= 56.60 PSF   RN/FT= 1.275   MACH=0.20

ALPHA	BETA	c_N	c_A	c_m	c_Y	c_n	c_1
70.36	-9.78	2.6224	-.1053	-.1446	.0698	.0694	.0182
70.35	-7.76	2.6297	-.1050	-.1562	.0602	.0592	.0154
70.35	-3.85	2.6529	-.1070	-.1465	.0306	.0320	.0080
70.34	.11	2.6547	-.1060	-.1405	-.0132	.0016	.0025
70.33	4.06	2.6520	-.1057	-.1467	-.0580	-.0283	-.0049
70.32	8.11	2.6238	-.1012	-.1587	-.0890	-.0540	-.0132
70.32	10.07	2.6340	-.1011	-.1640	-.1180	-.0652	-.0166
70.31	15.04	2.5817	-.0968	-.1644	-.1739	-.0961	-.0254
70.33	19.97	2.5592	-.0977	-.1271	-.2431	-.1482	-.0317
70.30	29.89	2.5034	-.1003	-.0046	-.2042	-.1013	-.0505

RUN 58   Q= 55.70 PSF   RN/FT= 1.265   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
65.55	29.90	2.5523	-.1008	.0920	-.1742	-.0847	-.0566
65.55	20.04	2.5630	-.0968	-.0931	-.2621	-.1467	-.0301
65.54	15.02	2.6024	-.0930	-.1081	-.1626	-.0966	-.0230
65.55	10.09	2.6426	-.0955	-.1064	-.0944	-.0650	-.0148
65.56	8.06	2.6663	-.0978	-.1100	-.0740	-.0508	-.0108
65.56	4.11	2.6534	-.0979	-.1148	-.0390	-.0267	-.0044
65.60	.11	2.6815	-.0999	-.1172	-.0127	.0000	.0017
65.62	-3.80	2.6522	-.0987	-.1191	.0144	.0313	.0064
65.63	-7.79	2.6472	-.0990	-.1171	.0517	.0605	.0134
65.64	-9.85	2.6502	-.0993	-.1156	.0709	.0744	.0162

RUN 59   Q= 58.50 PSF   RN/FT= 1.294   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
60.73	-9.85	2.6700	-.0959	-.0663	.0856	.0729	.0159
60.72	-7.82	2.6760	-.0965	-.0723	.0621	.0639	.0118
60.71	-3.84	2.6987	-.1015	-.0537	.0272	.0323	.0048
60.71	.14	2.7293	-.1123	.0025	-.0168	-.0033	.0043
60.68	4.11	2.6885	-.0975	-.0672	-.0423	-.0302	-.0029
60.68	8.10	2.6716	-.0952	-.0613	-.0709	-.0525	-.0096
60.68	10.04	2.6674	-.0937	-.0630	-.0914	-.0630	-.0131
60.69	15.03	2.6377	-.0918	-.0474	-.1640	-.0971	-.0226
60.68	20.02	2.6143	-.0957	-.0299	-.1892	-.1035	-.0310
60.67	29.88	2.6285	-.1004	.1226	-.0995	-.0264	-.0660

RUN 60   Q= 57.40 PSF   RN/FT= 1.282   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
51.04	29.86	2.7712	-.1072	.2083	-.0369	.0041	-.1200
51.09	20.00	2.8927	-.1210	.1333	-.0810	-.0588	-.0627
51.09	15.08	2.8919	-.1174	.1357	-.0310	-.0500	-.0381
51.11	10.02	2.9523	-.1162	.1187	.0474	-.0302	-.0295
51.11	8.08	2.9434	-.1164	.1102	.0412	-.0299	-.0219
51.11	4.13	2.8823	-.1164	.0908	.0172	-.0218	-.0065
51.12	.14	2.8829	-.1227	.0602	-.0036	-.0068	.0085
51.12	-3.86	2.8783	-.1164	.0880	-.0195	.0263	.0099
51.16	-7.87	2.9542	-.1233	.1391	-.0303	.0455	.0284
51.18	-9.83	2.9575	-.1257	.1645	-.0014	.0445	.0364

RUN 61   Q= 57.20 PSF   RN/FT= 1.280   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
40.87	-9.86	2.5805	-.0945	.0848	.0736	.0084	.0316
40.86	-7.85	2.6267	-.0943	.0889	.0566	.0098	.0210
40.85	-3.84	2.6026	-.0864	.0476	-.0082	.0079	.0149
40.87	.12	2.6621	-.0921	.0316	.0113	-.0031	-.0002
40.83	4.09	2.6135	-.0873	.0540	-.0044	-.0071	-.0091
40.83	8.10	2.5935	-.0855	.0723	-.0481	-.0050	-.0200
40.84	10.04	2.6018	-.0884	.0764	-.0585	-.0037	-.0320
40.82	14.98	2.6392	-.0909	.0607	-.0604	-.0085	-.0563
40.80	19.96	2.6317	-.0865	.0125	-.0599	-.0200	-.0690
40.74	29.89	2.4383	-.0785	.1734	-.1836	-.0133	-.1155

RUN 62   Q=225.90 PSF   RN/FT= 5.013   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
41.89	.12	2.3000	.0346	-.3601	.0225	.0100	.0019
52.19	.10	2.4723	-.0691	-.3156	-.0112	.0130	-.0047
61.95	.12	2.4846	-.1413	-.3070	-.0101	0.0000	.0026
71.64	.11	2.5131	-.1747	-.3871	-.0007	.0023	.0009
81.69	.10	2.5085	-.2384	-.4275	-.0100	-.0008	.0013
92.10	.08	2.4364	-.2702	-.4951	-.0103	-.0024	.0018

RUN 63   Q=244.60 PSF   RN/FT= 5.189   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
92.18	-9.84	2.4378	-.2630	-.4905	.0206	.0408	.0298
92.15	-7.81	2.4420	-.2669	-.4818	.0251	.0300	.0241
92.12	-3.85	2.4416	-.2679	-.4931	.0055	.0155	.0129
92.07	.18	2.4521	-.2722	-.5023	-.0105	-.0046	.0021
92.08	4.07	2.4353	-.2626	-.5058	-.0300	-.0248	-.0110
91.97	8.04	2.4399	-.2616	-.5212	-.0567	-.0481	-.0216
91.99	10.01	2.4227	-.2614	-.5244	-.0671	-.0608	-.0270
91.95	15.00	2.3919	-.2520	-.5381	-.1163	-.0742	-.0384
91.93	19.96	2.3828	-.2406	-.5569	-.1560	-.0885	-.0494
91.95	29.87	2.2905	-.2393	-.5203	-.1642	-.0816	-.0704

RUN   64   Q=226.10 PSF   RN/FT= 4.983   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
86.61	29.90	2.3214	-.2213	-.5049	-.1830	-.0916	-.0670
86.68	19.97	2.4003	-.2350	-.4560	-.1303	-.0723	-.0467
86.66	15.03	2.4229	-.2433	-.5029	-.1378	-.0959	-.0352
86.69	10.05	2.4545	-.2529	-.4716	-.0904	-.0700	-.0238
86.68	8.11	2.4649	-.2544	-.4608	-.0733	-.0571	-.0198
86.68	4.04	2.4731	-.2557	-.4511	-.0458	-.0319	-.0076
86.69	.08	2.4705	-.2599	-.4424	-.0074	-.0014	.0019
86.71	-3.80	2.4850	-.2583	-.4447	.0123	.0244	.0122
86.72	-7.82	2.4777	-.2581	-.4623	.0334	.0452	.0233
86.73	-9.82	2.4618	-.2546	-.4682	.0424	.0513	.0279

RUN   65   Q=227.30 PSF   RN/FT= 4.985   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
81.50	-9.81	2.4710	-.2381	-.4438	.0514	.0624	.0249
81.49	-7.89	2.4845	-.2384	-.4419	.0482	.0532	.0202
81.47	-3.87	2.4836	-.2384	-.4341	.0134	.0293	.0115
81.47	.17	2.5019	-.2413	-.4287	-.0047	-.0035	.0012
81.46	4.06	2.4926	-.2369	-.4372	-.0508	-.0364	-.0085
81.46	8.11	2.4769	-.2320	-.4553	-.0837	-.0678	-.0183
81.46	10.10	2.4668	-.2304	-.4593	-.1051	-.0790	-.0232
81.45	15.07	2.4369	-.2251	-.4841	-.1607	-.1043	-.0337
81.45	20.05	2.3850	-.2120	-.5435	-.2261	-.1269	-.0432
81.42	29.97	2.3100	-.1943	-.4662	-.1925	-.0933	-.0621

RUN 66   Q=228.30 PSF   RN/FT= 4.986   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
76.44	30.01	2.2919	-.1619	-.4875	-.2440	-.1052	-.0586
76.48	20.10	2.4092	-.1826	-.4517	-.1698	-.0969	-.0415
76.46	15.05	2.4323	-.1948	-.4867	-.1757	-.1087	-.0303
76.47	10.06	2.4750	-.2043	-.4500	-.1064	-.0838	-.0196
76.49	8.10	2.4899	-.2078	-.4357	-.0863	-.0688	-.0158
76.47	4.15	2.4930	-.2111	-.4156	-.0433	-.0379	-.0065
76.50	.12	2.5090	-.2129	-.4022	-.0037	-.0009	.0015
76.50	-3.85	2.5109	-.2165	-.4119	.0180	.0365	.0087
76.52	-7.87	2.4939	-.2164	-.4327	.0373	.0597	.0187
76.53	-9.81	2.4844	-.2154	-.4305	.0462	.0635	.0228

RUN 67   Q=224.40 PSF   RN/FT= 4.930   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
71.52	-9.81	2.4770	-.1821	-.4238	.0290	.0723	.0197
71.52	-7.82	2.4936	-.1842	-.4153	.0299	.0628	.0145
71.50	-3.91	2.5065	-.1819	-.3989	.0245	.0371	.0081
71.51	.07	2.5322	-.1800	-.3996	-.0052	.0033	.0007
71.54	4.05	2.5146	-.1773	-.4023	-.0415	-.0355	-.0058
71.55	8.08	2.4955	-.1748	-.4108	-.0822	-.0678	-.0134
71.55	10.12	2.4897	-.1724	-.4243	-.1046	-.0824	-.0173
71.53	15.10	2.4298	-.1615	-.4646	-.1597	-.1045	-.0280
71.50	20.11	2.3647	-.1410	-.5196	-.2246	-.1176	-.0387
71.51	30.01	2.2690	-.1342	-.4733	-.2387	-.1120	-.0537

RUN 68   Q=233.90 PSF   RN/FT= 5.022   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
66.76	30.04	2.2704	-.1080	-.3791	-.2621	-.0947	-.0537
66.72	20.12	2.3512	-.1137	-.4692	-.2184	-.1056	-.0346
66.71	15.12	2.4111	-.1256	-.4360	-.1496	-.0939	-.0251
66.81	10.05	2.4726	-.1388	-.4145	-.0928	-.0695	-.0144
66.79	8.09	2.4654	-.1384	-.4016	-.0650	-.0572	-.0113
66.79	4.12	2.4898	-.1498	-.3784	-.0365	-.0257	-.0048
66.79	.06	2.4967	-.1589	-.3616	-.0069	-.0003	.0005
66.81	-3.89	2.4785	-.1571	-.3800	.0177	.0246	.0073
66.82	-7.89	2.4705	-.1496	-.4088	.0299	.0548	.0141
66.83	-9.91	2.4680	-.1476	-.4196	.0467	.0661	.0175

RUN 69   Q=230.70 PSF   RN/FT= 4.975   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
61.88	-9.87	2.4294	-.1231	-.3581	.0289	.0412	.0163
61.87	-7.80	2.4381	-.1270	-.3480	.0214	.0287	.0128
61.87	-3.89	2.4571	-.1309	-.3338	.0010	.0127	.0057
61.87	.09	2.4679	-.1418	-.3107	-.0111	-.0012	.0022
61.86	4.14	2.4634	-.1258	-.3334	-.0305	-.0149	-.0034
61.86	8.14	2.4528	-.1141	-.3656	-.0558	-.0390	-.0099
61.85	10.19	2.4260	-.1078	-.3799	-.0769	-.0533	-.0132
61.85	15.09	2.4070	-.0959	-.3887	-.1121	-.0674	-.0223
61.95	20.12	2.4478	-.1302	-.2930	-.1256	-.0742	-.0304
61.95	30.07	2.3329	-.1111	-.2588	-.2545	-.0902	-.0510

RUN 70   Q=227.20 PSF   RN/FT= 4.941   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
52.27	30.10	2.4927	-.0343	-.2868	-.2527	-.0973	-.0973
52.25	20.09	2.5884	-.0439	-.2796	-.1128	-.0723	-.0499
52.25	15.10	2.6051	-.0511	-.2762	-.0427	-.0634	-.0370
52.20	10.10	2.5214	-.0580	-.2712	.0335	-.0306	-.0196
52.08	8.03	2.4976	-.0536	-.3013	.0441	-.0350	-.0075
52.04	4.09	2.4553	-.0547	-.3259	.0407	-.0129	.0016
52.07	.08	2.4394	-.0663	-.3155	-.0122	.0118	-.0011
52.08	-3.90	2.4686	-.0669	-.3126	-.0530	.0214	.0038
52.08	-7.83	2.4889	-.0589	-.3187	-.0517	.0480	.0064
52.21	-9.83	2.5492	-.0661	-.3041	-.0457	.0508	.0204

RUN 71   Q=223.70 PSF   RN/FT= 4.920   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
41.83	-9.83	2.2951	.0269	-.2689	.0647	.0033	.0278
41.79	-7.87	2.2663	.0326	-.2897	.0695	-.0074	.0209
41.79	-3.86	2.2677	.0391	-.3363	.0672	-.0218	-.0010
42.03	.12	2.2985	.0413	-.3659	.0269	.0115	.0011
41.91	4.06	2.2573	.0384	-.3421	-.0838	.0315	-.0037
41.73	8.13	2.2662	.0403	-.2971	-.0830	.0112	-.0180
41.85	10.03	2.2802	.0386	-.2674	-.0841	.0049	-.0271
42.03	15.05	2.4123	.0256	-.2329	-.1011	-.0351	-.0377
41.99	20.23	2.4142	.0356	-.2665	-.1990	-.0680	-.0614
42.07	30.25	2.4594	.0419	-.4074	-.3592	-.1026	-.0965

RUN 72   Q=208.90 PSF   RN/FT= 4.849   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
42.04	.09	2.5096	-.0977	-.1722	.0435	.0081	-.0024
52.23	.11	2.7098	-.1898	-.0751	.0006	.0095	.0002
62.06	.12	2.6855	-.2028	-.0717	-.0089	.0002	.0034
71.80	.10	2.6542	-.1753	-.2339	-.0035	.0008	.0014
81.80	.08	2.6394	-.2095	-.3121	-.0024	-.0008	.0013
91.07	.09	2.5624	-.2200	-.3794	-.0090	-.0008	.0017

RUN 73   Q=233.20 PSF   RN/FT= 5.127   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
91.09	-9.79	2.5394	-.2118	-.3925	.0364	.0419	.0286
91.05	-7.76	2.5552	-.2124	-.3898	.0326	.0361	.0251
91.04	-3.82	2.5542	-.2176	-.3762	.0080	.0133	.0149
91.04	.15	2.5555	-.2173	-.3837	-.0010	-.0008	.0029
91.03	4.06	2.5570	-.2164	-.3789	-.0373	-.0224	-.0086
91.02	8.09	2.5489	-.2116	-.4081	-.0657	-.0453	-.0213
90.99	10.08	2.5380	-.2086	-.4192	-.0797	-.0568	-.0259
90.94	15.01	2.4890	-.2026	-.4336	-.1290	-.0717	-.0360
90.95	19.94	2.4544	-.1938	-.4659	-.1877	-.0853	-.0460
90.86	29.82	2.3263	-.1809	-.4620	-.2138	-.0761	-.0655

RUN 74   Q=223.60 PSF   RN/FT= 5.022   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
86.70	29.87	2.3618	-.1808	-.4282	-.1989	-.0875	-.0634
86.77	19.97	2.4845	-.1952	-.3763	-.1623	-.0736	-.0436
86.75	15.04	2.5061	-.1965	-.4178	-.1450	-.0818	-.0335
86.79	9.93	2.5555	-.2060	-.3904	-.0951	-.0608	-.0232
86.83	8.05	2.5887	-.2114	-.3730	-.0801	-.0482	-.0193
86.83	4.03	2.5946	-.2133	-.3584	-.0371	-.0220	-.0080
86.85	.10	2.5949	-.2163	-.3549	-.0033	-.0001	.0024
86.85	-3.87	2.5909	-.2143	-.3660	.0121	.0235	.0129
86.87	-7.82	2.5723	-.2111	-.3510	.0427	.0317	.0226
86.88	-9.83	2.5747	-.2068	-.3657	.0538	.0435	.0267

RUN 75   Q=224.50 PSF   RN/FT= 5.024   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
81.61	-9.84	2.5946	-.2002	-.3364	.0592	.0519	.0250
81.61	-7.84	2.5987	-.2036	-.3293	.0493	.0422	.0202
81.58	-3.87	2.6207	-.2072	-.3182	.0204	.0201	.0111
81.59	.14	2.6252	-.2091	-.3183	-.0079	-.0010	.0012
81.59	4.10	2.6248	-.2061	-.3208	-.0305	-.0276	-.0090
81.59	8.10	2.6167	-.2010	-.3366	-.0754	-.0526	-.0172
81.64	10.05	2.5911	-.1973	-.3421	-.0925	-.0639	-.0212
81.62	15.00	2.5434	-.1908	-.3817	-.1584	-.0889	-.0316
81.60	20.00	2.4651	-.1871	-.4210	-.2142	-.1081	-.0404
81.57	29.97	2.3898	-.1813	-.3658	-.1993	-.0904	-.0611

RUN 76   Q=228.50 PSF   RN/FT= 5.060   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
76.66	29.95	2.3874	-.1876	-.3261	-.2221	-.1004	-.0609
76.68	20.05	2.5048	-.1851	-.3036	-.1654	-.0810	-.0405
76.67	15.07	2.5459	-.1831	-.3532	-.1617	-.0940	-.0307
76.70	10.08	2.5851	-.1845	-.3157	-.1082	-.0711	-.0197
76.69	8.04	2.5874	-.1853	-.2988	-.0833	-.0580	-.0147
76.71	4.13	2.6232	-.1892	-.2777	-.0453	-.0309	-.0069
76.72	.11	2.6365	-.1921	-.2650	-.0063	.0004	.0027
76.63	-3.90	2.6147	-.1903	-.2823	.0219	.0303	.0105
76.63	-7.86	2.6044	-.1903	-.3058	.0506	.0478	.0189
76.65	-9.86	2.5992	-.1904	-.3105	.0477	.0545	.0232

RUN 77   Q=222.30 PSF   RN/FT= 4.980   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
71.67	-9.86	2.5920	-.1816	-.2539	.0402	.0573	.0212
71.67	-7.79	2.6220	-.1818	-.2448	.0252	.0501	.0165
71.65	-3.85	2.6321	-.1795	-.2357	.0034	.0288	.0091
71.64	.10	2.6398	-.1765	-.2330	-.0058	.0008	.0015
71.65	4.10	2.6374	-.1743	-.2317	-.0256	-.0269	-.0058
71.65	8.12	2.6301	-.1762	-.2379	-.0654	-.0531	-.0142
71.64	10.09	2.6105	-.1771	-.2427	-.0862	-.0653	-.0177
71.63	15.10	2.5710	-.1793	-.2905	-.1468	-.0894	-.0297
71.64	20.11	2.5009	-.1791	-.3437	-.1954	-.1060	-.0404
71.75	29.99	2.4175	-.1945	-.2977	-.2313	-.1095	-.0623

RUN 78 Q=218.20 PSF RN/FT= 4.929 MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
66.88	30.01	2.4800	-.1895	-.1946	-.2095	-.0984	-.0709
66.83	20.08	2.5506	-.1834	-.2488	-.1569	-.0912	-.0407
66.83	15.11	2.5981	-.1791	-.2238	-.1084	-.0821	-.0292
66.82	10.11	2.6305	-.1743	-.2033	-.0611	-.0586	-.0177
66.81	8.11	2.6291	-.1719	-.2005	-.0513	-.0483	-.0137
66.81	4.07	2.6451	-.1713	-.2002	-.0292	-.0244	-.0051
66.79	.14	2.6418	-.1739	-.2034	-.0045	.0028	.0018
66.82	-3.85	2.6356	-.1762	-.2023	.0118	.0256	.0077
66.84	-7.84	2.6372	-.1788	-.2131	.0206	.0475	.0168
66.93	-9.85	2.6367	-.1796	-.2183	.0302	.0555	.0215

RUN 79 Q=215.70 PSF RN/FT= 4.908 MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
62.05	-9.82	2.6811	-.1946	-.1531	.0341	.0406	.0228
62.06	-7.84	2.7005	-.1958	-.1386	.0191	.0334	.0181
62.08	-3.85	2.6895	-.1970	-.1121	-.0093	.0134	.0086
62.09	.16	2.6962	-.2034	-.0739	-.0095	-.0003	.0032
62.03	4.14	2.6854	-.1926	-.1103	-.0197	-.0167	-.0058
62.05	8.14	2.6686	-.1868	-.1416	-.0565	-.0430	-.0145
62.04	10.12	2.6644	-.1831	-.1634	-.0618	-.0529	-.0197
62.03	15.13	2.6496	-.1872	-.1720	-.0974	-.0682	-.0320
62.06	20.05	2.6360	-.1897	-.1619	-.1319	-.0688	-.0455
61.95	30.05	2.4861	-.1678	-.1843	-.2174	-.1029	-.0705

RUN 80   Q=211.80 PSF   RN/FT= 4.869   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
52.33	30.09	2.5580	-.1206	-.1709	-.2459	-.0938	-.1053
52.35	20.07	2.6516	-.1433	-.1200	-.1505	-.0654	-.0578
52.38	15.09	2.6574	-.1492	-.1311	-.0876	-.0508	-.0408
52.35	10.04	2.6825	-.1613	-.1184	-.0135	-.0254	-.0284
52.41	8.08	2.6899	-.1646	-.1131	.0175	-.0248	-.0208
52.42	4.09	2.6758	-.1762	-.0889	.0380	-.0108	-.0057
52.42	.12	2.7019	-.1894	-.0727	-.0009	.0059	.0027
52.41	-3.83	2.6904	-.1859	-.0720	-.0399	.0160	.0109
52.37	-7.85	2.6818	-.1714	-.1063	-.0410	.0302	.0237
52.41	-9.86	2.6679	-.1692	-.1105	-.0109	.0325	.0310

RUN 81   Q=206.50 PSF   RN/FT= 4.811   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
41.90	-9.85	2.3999	-.0876	-.1031	.0713	-.0028	.0312
41.88	-7.77	2.4021	-.0883	-.1194	.0652	-.0093	.0221
41.87	-3.79	2.3980	-.0896	-.1413	.0242	-.0209	.0045
41.91	.10	2.4977	-.0938	-.1776	.0425	.0079	-.0025
41.86	4.08	2.4159	-.0880	-.1387	-.0567	.0274	-.0012
41.89	8.10	2.4094	-.0808	-.1168	-.0758	.0147	-.0194
41.85	10.09	2.4193	-.0788	-.0912	-.0787	.0095	-.0294
41.94	15.07	2.5021	-.0820	-.0899	-.1291	-.0263	-.0432
41.96	20.11	2.5251	-.0710	-.1379	-.1704	-.0540	-.0657
41.90	30.18	2.3803	-.0366	-.2884	-.3179	-.0990	-.1160

RUN 82   Q=208.40 PSF   RN/FT= 4.839   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
41.55	.11	2.7697	-.1102	.0477	.0292	.0119	-.0007
52.66	.11	2.9453	-.1364	.0743	.0105	.0055	.0041
62.19	.14	2.7699	-.1278	-.0082	-.0068	-.0046	.0049
71.79	.12	2.7034	-.1199	-.1678	-.0064	.0010	.0025
81.75	.13	2.6970	-.1357	-.2631	-.0083	-.0015	.0020
91.11	.12	2.6045	-.1411	-.3298	-.0080	-.0005	.0027

RUN 83   Q=231.10 PSF   RN/FT= 5.087   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
91.07	-9.78	2.5841	-.1415	-.3483	.0419	.0501	.0294
91.08	-7.82	2.5985	-.1407	-.3447	.0393	.0391	.0246
91.04	-3.86	2.6147	-.1426	-.3321	.0087	.0179	.0151
91.03	.10	2.6162	-.1417	-.3313	-.0123	-.0022	.0022
91.04	4.07	2.6020	-.1376	-.3430	-.0402	-.0301	-.0106
91.02	8.04	2.5980	-.1352	-.3762	-.0979	-.0480	-.0194
90.99	10.00	2.5869	-.1330	-.3883	-.1070	-.0598	-.0244
90.97	14.99	2.5594	-.1306	-.4113	-.1426	-.0706	-.0349
90.94	19.96	2.5071	-.1287	-.4190	-.1833	-.0763	-.0437
90.91	29.85	2.3875	-.1215	-.4048	-.1994	-.0684	-.0659

RUN 84   Q=230.60 PSF   RN/FT= 5.073   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
86.86	29.88	2.4182	-.1195	-.3523	-.1970	-.0713	-.0627
86.93	19.99	2.5307	-.1255	-.3746	-.2092	-.0849	-.0427
86.86	14.98	2.5801	-.1260	-.3765	-.1580	-.0717	-.0337
86.88	10.04	2.5950	-.1293	-.3641	-.1126	-.0599	-.0229
86.89	8.03	2.6097	-.1314	-.3448	-.0760	-.0524	-.0191
86.86	4.11	2.6296	-.1355	-.3323	-.0550	-.0267	-.0085
86.80	.09	2.6187	-.1397	-.3107	-.0041	-.0021	.0020
86.83	-3.83	2.6443	-.1403	-.3191	.0293	.0205	.0120
86.84	-7.84	2.6136	-.1359	-.3242	.0483	.0356	.0219
86.86	-9.80	2.5955	-.1364	-.3226	.0526	.0414	.0265

RUN 85   Q=221.40 PSF   RN/FT= 4.965   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
81.57	-9.79	2.6177	-.1311	-.2942	.0820	.0521	.0231
81.55	-7.85	2.6460	-.1337	-.2890	.0681	.0461	.0187
81.57	-3.86	2.6732	-.1352	-.2771	.0235	.0252	.0115
81.57	.12	2.6691	-.1355	-.2634	-.0012	-.0027	.0007
81.59	4.09	2.6686	-.1322	-.2807	-.0511	-.0308	-.0078
81.60	8.09	2.6515	-.1274	-.2967	-.0843	-.0557	-.0172
81.59	10.10	2.6256	-.1253	-.3031	-.1176	-.0628	-.0210
81.59	15.04	2.5948	-.1240	-.3263	-.1637	-.0867	-.0303
81.56	20.00	2.5202	-.1218	-.3643	-.2158	-.1056	-.0402
81.58	29.88	2.4437	-.1170	-.2992	-.1876	-.0756	-.0596

RUN 86   Q=217.10 PSF   RN/FT= 4.916   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
76.55	29.91	2.4379	-.1135	-.2689	-.2074	-.0838	-.0569
76.61	20.04	2.5635	-.1185	-.2429	-.1640	-.0728	-.0393
76.60	15.09	2.5948	-.1185	-.2950	-.1637	-.0884	-.0293
76.62	10.09	2.6423	-.1206	-.2613	-.1076	-.0670	-.0197
76.62	8.11	2.6560	-.1220	-.2573	-.0922	-.0561	-.0152
76.60	4.09	2.6875	-.1258	-.2373	-.0535	-.0299	-.0075
76.64	.10	2.6946	-.1295	-.2289	-.0101	-.0007	.0019
76.65	-3.86	2.6877	-.1287	-.2401	.0186	.0258	.0102
76.64	-7.86	2.6522	-.1269	-.2520	.0547	.0448	.0186
76.62	-9.86	2.6361	-.1260	-.2494	.0697	.0512	.0215

RUN 87   Q=217.30 PSF   RN/FT= 4.917   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
71.68	-9.87	2.6656	-.1207	-.2025	.0596	.0549	.0219
71.67	-7.86	2.6717	-.1216	-.1931	.0464	.0479	.0180
71.67	-3.89	2.6890	-.1225	-.1720	.0167	.0303	.0099
71.66	.12	2.7068	-.1228	-.1666	-.0054	.0022	.0028
71.67	4.11	2.7106	-.1210	-.1681	-.0449	-.0286	-.0054
71.65	8.09	2.6760	-.1175	-.1848	-.0801	-.0547	-.0142
71.68	10.11	2.6855	-.1177	-.1923	-.1042	-.0642	-.0180
71.72	15.07	2.6207	-.1129	-.2368	-.1502	-.0839	-.0278
71.66	20.07	2.5498	-.1084	-.2826	-.2003	-.0954	-.0368
71.65	29.97	2.4410	-.1098	-.2646	-.2330	-.0975	-.0551

RUN 88   Q=218.60 PSF   RN/FT= 4.931   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
66.87	29.97	2.5137	-.1125	-.1753	-.1995	-.0923	-.0537
66.84	20.06	2.5903	-.1047	-.1964	-.1621	-.0819	-.0354
66.86	15.06	2.6344	-.1066	-.1668	-.1109	-.0708	-.0259
66.89	10.09	2.6969	-.1104	-.1467	-.0678	-.0547	-.0155
66.95	8.12	2.7165	-.1114	-.1407	-.0652	-.0486	-.0117
66.93	4.09	2.7267	-.1142	-.1317	-.0300	-.0234	-.0046
66.93	.09	2.7220	-.1160	-.1338	-.0042	.0033	.0031
66.95	-3.89	2.7136	-.1159	-.1430	.0169	.0269	.0090
66.94	-7.87	2.6964	-.1146	-.1537	.0367	.0458	.0161
66.96	-9.88	2.6812	-.1144	-.1579	.0379	.0536	.0201

RUN 89   Q=220.10 PSF   RN/FT= 4.943   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
62.09	-9.87	2.6904	-.1131	-.0960	.0409	.0397	.0189
62.08	-7.89	2.7074	-.1141	-.0930	.0332	.0361	.0151
62.15	-3.90	2.7309	-.1166	-.0845	.0223	.0226	.0078
62.21	.12	2.7857	-.1309	-.0098	-.0023	-.0072	.0061
62.14	4.11	2.7298	-.1133	-.0825	-.0317	-.0242	-.0031
62.13	8.10	2.7294	-.1081	-.1042	-.0478	-.0451	-.0115
62.14	10.10	2.7099	-.1055	-.1159	-.0494	-.0525	-.0152
62.14	15.07	2.6842	-.1043	-.1174	-.1023	-.0638	-.0249
62.12	20.07	2.6405	-.1060	-.1213	-.1467	-.0707	-.0347
62.19	30.00	2.5578	-.1133	-.1261	-.2147	-.0879	-.0624

RUN 90   Q=218.80 PSF   RN/FT= 4.924   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
52.58	30.07	2.7169	-.1323	.0010	-.2479	-.0827	-.1076
52.63	20.06	2.8649	-.1268	.0450	-.1103	-.0543	-.0549
52.66	15.07	2.9387	-.1341	.0790	-.0563	-.0487	-.0426
52.68	10.09	2.9776	-.1333	.0652	.0002	-.0269	-.0306
52.69	8.06	2.9539	-.1293	.0730	.0067	-.0146	-.0241
52.66	4.07	2.9329	-.1294	.0802	.0205	-.0066	-.0063
52.68	.08	2.9440	-.1372	.0757	.0043	.0054	.0023
52.66	-3.85	2.9366	-.1347	.0851	-.0092	.0060	.0152
52.68	-7.80	2.9567	-.1310	.0730	-.0329	.0249	.0216
52.72	-9.85	2.9611	-.1331	.0735	-.0405	.0314	.0285

RUN 91   Q=213.90 PSF   RN/FT= 4.866   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
42.45	-9.86	2.6633	-.1170	.1413	.0581	.0010	.0352
42.26	-7.83	2.6591	-.1130	.1269	.0264	-.0032	.0284
42.34	-3.78	2.6781	-.1066	.0867	-.0463	-.0198	.0197
41.93	.05	2.7639	-.1117	.0489	.0326	.0145	-.0012
42.28	4.04	2.6685	-.1033	.1021	.0139	.0211	-.0135
42.25	8.10	2.6762	-.1105	.1358	-.0468	.0044	-.0250
42.27	10.04	2.6544	-.1106	.1536	-.0676	.0045	-.0307
42.30	15.07	2.6644	-.1081	.1449	-.1510	-.0122	-.0517
42.24	20.12	2.6594	-.1012	.0800	-.2044	-.0432	-.0712
42.25	30.17	2.5622	-.0855	-.0880	-.3238	-.0977	-.1188

RUN   92   Q=139.50 PSF   RN/FT= 3.321   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
41.21	.15	2.2506	.0471	-.3821	.0062	.0090	.0008
51.49	.15	2.4081	-.0623	-.3409	-.0044	-.0008	.0049
61.31	.16	2.4173	-.1419	-.3122	-.0150	-.0046	.0005
71.02	.14	2.5047	-.1787	-.4091	-.0032	.0037	.0015
81.00	.15	2.4866	-.2409	-.4390	-.0078	-.0014	.0021
91.49	.14	2.4303	-.2709	-.5083	-.0056	.0028	.0014

RUN   93   Q=151.50 PSF   RN/FT= 3.431   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
91.50	-9.79	2.4310	-.2717	-.5345	.0429	.0613	.0286
91.48	-7.80	2.4135	-.2706	-.5363	.0460	.0561	.0232
91.44	-3.82	2.4210	-.2690	-.5166	.0287	.0301	.0137
91.42	.13	2.4177	-.2695	-.5117	-.0048	.0019	.0021
91.42	4.09	2.4196	-.2663	-.5128	-.0496	-.0301	-.0093
91.41	8.04	2.4050	-.2672	-.5311	-.0619	-.0544	-.0209
91.40	10.08	2.4090	-.2675	-.5431	-.0831	-.0650	-.0263
91.40	15.00	2.3944	-.2626	-.5585	-.1169	-.0780	-.0372
91.37	19.94	2.3422	-.2418	-.5889	-.1581	-.1027	-.0477
91.37	29.83	2.2725	-.2419	-.5204	-.1463	-.0706	-.0700

RUN 94   Q=145.30 PSF   RN/FT= 3.353   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
86.07	29.86	2.2957	-.2232	-.5264	-.1534	-.0861	-.0646
86.10	19.99	2.3542	-.2295	-.5783	-.2128	-.1249	-.0450
86.12	15.00	2.4127	-.2476	-.5260	-.1464	-.1046	-.0348
86.15	10.01	2.4408	-.2543	-.4822	-.0985	-.0683	-.0237
86.16	8.05	2.4619	-.2589	-.4691	-.0758	-.0582	-.0183
86.16	4.08	2.4612	-.2587	-.4588	-.0345	-.0324	-.0077
86.17	.08	2.4732	-.2591	-.4533	-.0112	.0002	.0022
86.17	-3.85	2.4596	-.2586	-.4581	.0178	.0314	.0127
86.19	-7.87	2.4371	-.2598	-.4708	.0507	.0617	.0215
86.20	-9.84	2.4412	-.2587	-.4806	.0625	.0763	.0270

RUN 95   Q=147.00 PSF   RN/FT= 3.365   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
80.91	-9.84	2.4426	-.2383	-.4580	.0610	.0749	.0252
80.92	-7.83	2.4717	-.2415	-.4482	.0579	.0605	.0206
80.89	-3.86	2.4907	-.2443	-.4376	.0122	.0306	.0115
80.88	.17	2.4801	-.2415	-.4387	-.0018	-.0021	.0011
80.88	4.15	2.4761	-.2391	-.4445	-.0478	-.0331	-.0077
80.86	8.06	2.4634	-.2339	-.4495	-.0659	-.0599	-.0184
80.86	10.10	2.4522	-.2313	-.4582	-.0902	-.0746	-.0216
80.84	15.02	2.4179	-.2223	-.5046	-.1583	-.1017	-.0320
80.81	20.06	2.3531	-.2095	-.5518	-.2219	-.1272	-.0426
80.78	29.92	2.3132	-.1921	-.5149	-.1596	-.0838	-.0610

RUN 96   Q=143.10 PSF   RN/FT= 3.316   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
75.83	29.95	2.2872	-.1613	-.5066	-.1739	-.0890	-.0565
75.87	20.06	2.3520	-.1762	-.5597	-.2219	-.1245	-.0388
75.90	15.03	2.4154	-.1914	-.5020	-.1509	-.1026	-.0305
75.93	10.08	2.4566	-.2055	-.4544	-.0886	-.0709	-.0197
75.92	8.08	2.4682	-.2085	-.4441	-.0661	-.0594	-.0158
75.89	4.10	2.4859	-.2121	-.4404	-.0467	-.0345	-.0064
75.91	.10	2.5015	-.2153	-.4294	-.0061	-.0009	.0013
75.93	-3.87	2.4920	-.2170	-.4383	.0175	.0318	.0091
75.93	-7.77	2.4678	-.2154	-.4452	.0342	.0601	.0177
75.94	-9.86	2.4582	-.2130	-.4578	.0605	.0732	.0217

RUN 97   Q=144.60 PSF   RN/FT= 3.326   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
70.91	-9.86	2.4608	-.1810	-.4472	.0486	.0734	.0188
70.91	-7.84	2.4698	-.1823	-.4329	.0253	.0615	.0144
70.89	-3.86	2.4829	-.1807	-.4106	.0102	.0345	.0074
70.89	.12	2.4843	-.1780	-.4058	-.0032	.0012	.0014
70.90	4.14	2.5010	-.1766	-.4140	-.0395	-.0353	-.0052
70.89	8.05	2.4780	-.1753	-.4304	-.0661	-.0607	-.0124
70.88	10.12	2.4589	-.1704	-.4391	-.0802	-.0712	-.0174
70.85	15.02	2.4106	-.1573	-.4791	-.1348	-.0967	-.0263
70.80	20.07	2.3355	-.1404	-.5388	-.2006	-.1150	-.0367
70.89	29.95	2.2534	-.1316	-.4804	-.2045	-.0933	-.0525

RUN 98   Q=141.00 PSF   RN/FT= 3.278   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
66.06	29.96	2.2538	-.1081	-.4130	-.2489	-.0888	-.0528
66.06	20.02	2.3235	-.1138	-.4723	-.1681	-.0885	-.0330
66.12	15.11	2.3931	-.1230	-.4479	-.1342	-.0872	-.0243
66.16	10.07	2.4420	-.1399	-.4133	-.0744	-.0597	-.0142
66.17	8.08	2.4550	-.1445	-.4012	-.0619	-.0471	-.0110
66.17	4.09	2.4419	-.1592	-.3626	-.0367	-.0204	-.0045
66.17	.11	2.4506	-.1712	-.3472	-.0084	-.0019	.0008
66.18	-3.85	2.4598	-.1641	-.3632	.0151	.0187	.0068
66.17	-7.83	2.4533	-.1507	-.4112	.0319	.0506	.0133
66.18	-9.89	2.4297	-.1472	-.4179	.0381	.0650	.0170

RUN 99   Q=146.30 PSF   RN/FT= 3.331   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
61.27	-9.87	2.4125	-.1219	-.3695	.0229	.0449	.0157
61.26	-7.81	2.4137	-.1262	-.3579	.0130	.0326	.0117
61.26	-3.89	2.4361	-.1356	-.3403	-.0134	.0077	.0058
61.26	.15	2.4421	-.1455	-.3163	-.0175	-.0034	.0011
61.25	4.13	2.4351	-.1281	-.3338	-.0085	-.0096	-.0040
61.24	8.11	2.4175	-.1134	-.3569	-.0271	-.0265	-.0098
61.22	10.11	2.4145	-.1061	-.3707	-.0501	-.0404	-.0135
61.21	15.05	2.3955	-.1000	-.3727	-.0885	-.0474	-.0235
61.19	20.06	2.3308	-.0976	-.3492	-.1362	-.0535	-.0310
61.27	29.97	2.3389	-.1073	-.2930	-.2274	-.0865	-.0513

RUN 100   Q=143.00 PSF   RN/FT= 3.288   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
51.62	30.00	2.4899	-.0412	-.3513	-.2023	-.0848	-.0986
51.65	20.04	2.5883	-.0417	-.2971	-.0623	-.0552	-.0517
51.65	15.04	2.5682	-.0592	-.2731	-.0072	-.0396	-.0372
51.64	10.00	2.5399	-.0697	-.2899	.0291	-.0337	-.0190
51.61	8.09	2.4814	-.0681	-.3021	.0410	-.0270	-.0060
51.54	4.08	2.4023	-.0522	-.3485	.0568	-.0101	.0016
51.56	.11	2.4151	-.0648	-.3395	-.0031	.0014	.0030
51.58	-3.82	2.4277	-.0633	-.3510	-.0672	.0188	.0027
51.65	-7.83	2.5122	-.0707	-.3177	-.0714	.0267	.0212
51.70	-9.81	2.5641	-.0774	-.3015	-.0563	.0383	.0237

RUN 101   Q=144.00 PSF   RN/FT= 3.292   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
41.33	-9.83	2.3294	.0294	-.3072	.0380	.0228	.0272
41.26	-7.76	2.2442	.0366	-.3217	.0713	-.0006	.0252
41.22	-3.86	2.2157	.0425	-.3626	.0773	-.0168	.0051
41.24	.13	2.2583	.0468	-.3804	.0045	.0090	.0017
41.18	4.11	2.2063	.0467	-.3614	-.0856	.0242	-.0090
41.21	8.09	2.2580	.0441	-.3157	-.0725	.0040	-.0226
41.27	10.12	2.3110	.0371	-.2931	-.0486	-.0123	-.0282
41.33	15.00	2.4398	.0296	-.3020	-.0154	-.0367	-.0354
41.33	20.06	2.4338	.0337	-.3254	-.0828	-.0532	-.0557
41.38	30.05	2.3931	.0337	-.3788	-.2994	-.0750	-.0997

RUN 102   Q= 92.10 PSF   RN/FT= 2.211   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
41.00	.19	2.2142	.0496	-.4012	-.0196	.0069	-.0008
51.20	.19	2.3808	-.0612	-.3553	.0111	-.0081	.0081
60.99	.18	2.4074	-.1453	-.3107	-.0223	-.0047	.0003
70.72	.17	2.4942	-.1758	-.3776	-.0133	-.0022	.0015
80.58	.16	2.4748	-.2435	-.4285	-.0081	-.0018	.0014
90.00	.17	2.4079	-.2662	-.4792	-.0059	.0004	.0004

RUN 103   Q= 93.20 PSF   RN/FT= 2.210   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
90.02	-9.75	2.4051	-.2640	-.5192	.0611	.0742	.0270
90.02	-7.75	2.4125	-.2638	-.5103	.0586	.0579	.0221
90.00	-3.77	2.4145	-.2646	-.5018	.0168	.0295	.0126
90.00	.17	2.4327	-.2688	-.4842	-.0058	.0016	.0012
90.01	4.10	2.4334	-.2624	-.4801	-.0417	-.0283	-.0097
89.99	8.13	2.4064	-.2530	-.4880	-.0592	-.0548	-.0211
89.99	10.11	2.3978	-.2522	-.5030	-.0746	-.0678	-.0260
89.98	15.02	2.3713	-.2498	-.5447	-.1314	-.0985	-.0372
89.96	20.01	2.3438	-.2393	-.5627	-.1405	-.0951	-.0474
89.96	29.90	2.2392	-.2400	-.6220	-.2471	-.1448	-.0675

RUN 104   Q= 92.40 PSF   RN/FT= 2.195   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
85.78	29.94	2.2301	-.2193	-.6670	-.3021	-.1736	-.0627
85.79	20.05	2.3430	-.2293	-.5600	-.1980	-.1220	-.0461
85.81	15.07	2.3986	-.2408	-.5119	-.1397	-.1086	-.0353
85.82	10.12	2.4302	-.2480	-.4807	-.0904	-.0746	-.0233
85.76	8.10	2.4522	-.2510	-.4623	-.0725	-.0577	-.0197
85.77	4.16	2.4604	-.2553	-.4439	-.0438	-.0285	-.0081
85.78	.16	2.4451	-.2574	-.4377	-.0012	-.0005	.0012
85.79	-3.82	2.4432	-.2575	-.4535	.0269	.0297	.0117
85.80	-7.81	2.4383	-.2579	-.4598	.0489	.0646	.0213
85.80	-9.76	2.4181	-.2550	-.4715	.0799	.0767	.0255

RUN 105   Q= 93.60 PSF   RN/FT= 2.202   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
80.67	-9.76	2.4324	-.2306	-.4595	.0693	.0812	.0235
80.66	-7.77	2.4580	-.2352	-.4472	.0482	.0644	.0201
80.65	-3.79	2.4749	-.2395	-.4260	.0159	.0323	.0109
80.63	.15	2.4602	-.2410	-.4290	-.0065	.0006	.0007
80.62	4.13	2.4690	-.2397	-.4263	-.0294	-.0314	-.0089
80.62	8.10	2.4559	-.2316	-.4459	-.0727	-.0604	-.0172
80.61	10.14	2.4375	-.2288	-.4633	-.0984	-.0783	-.0223
80.59	15.06	2.4022	-.2191	-.5126	-.1614	-.1090	-.0324
80.57	20.06	2.3513	-.2069	-.5608	-.2103	-.1290	-.0420
80.56	29.96	2.2446	-.1899	-.6546	-.3162	-.1751	-.0583

RUN 106   Q= 92.20 PSF   RN/FT= 2.181   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
75.53	29.99	2.2165	-.1516	-.6476	-.3245	-.1790	-.0549
75.54	20.09	2.3330	-.1754	-.5481	-.1999	-.1148	-.0394
75.58	15.06	2.4040	-.1876	-.5013	-.1629	-.1094	-.0298
75.59	10.14	2.4439	-.2010	-.4606	-.0934	-.0800	-.0190
75.59	8.15	2.4627	-.2052	-.4527	-.0684	-.0633	-.0148
75.61	4.15	2.4799	-.2084	-.4314	-.0389	-.0344	-.0070
75.62	.18	2.4658	-.2091	-.4213	-.0051	-.0013	.0011
75.63	-3.80	2.4745	-.2128	-.4292	.0149	.0307	.0091
75.65	-7.77	2.4658	-.2100	-.4514	.0557	.0678	.0164
75.64	-9.76	2.4469	-.2078	-.4639	.0736	.0857	.0201

RUN 107   Q= 93.50 PSF   RN/FT= 2.190   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
70.67	-9.79	2.4501	-.1771	-.4217	.0607	.0855	.0160
70.66	-7.80	2.4648	-.1772	-.4104	.0389	.0699	.0126
70.66	-3.78	2.4894	-.1780	-.3917	.0133	.0337	.0066
70.66	.19	2.4798	-.1744	-.3791	-.0066	.0012	.0005
70.65	4.16	2.4907	-.1743	-.3881	-.0353	-.0351	-.0058
70.64	8.13	2.4705	-.1723	-.4167	-.0627	-.0663	-.0123
70.64	10.11	2.4481	-.1673	-.4225	-.0840	-.0809	-.0169
70.62	15.11	2.3979	-.1559	-.4466	-.1352	-.1000	-.0267
70.58	20.04	2.3284	-.1399	-.5045	-.1831	-.1062	-.0364
70.56	30.02	2.2038	-.1162	-.6042	-.3286	-.1567	-.0551

RUN 108   Q= 92.40 PSF   RN/FT= 2.172   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
65.76	30.02	2.2468	-.1019	-.4168	-.2593	-.0980	-.0528
65.78	20.07	2.3277	-.1169	-.4392	-.1471	-.0817	-.0326
65.82	15.09	2.3937	-.1210	-.4239	-.1332	-.0917	-.0236
65.84	10.17	2.4387	-.1311	-.4035	-.0751	-.0722	-.0133
65.84	8.17	2.4464	-.1330	-.4002	-.0584	-.0572	-.0104
65.86	4.15	2.4768	-.1295	-.3947	-.0382	-.0324	-.0043
65.86	.15	2.4486	-.1339	-.3823	-.0228	-.0068	.0004
65.87	-3.78	2.4596	-.1293	-.3916	-.0118	.0221	.0060
65.90	-7.77	2.4708	-.1338	-.4128	.0182	.0627	.0115
65.90	-9.77	2.4372	-.1325	-.4099	.0401	.0798	.0139

RUN 109   Q= 92.90 PSF   RN/FT= 2.171   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
60.98	-9.79	2.4118	-.1102	-.3800	.0527	.0693	.0139
60.97	-7.78	2.4136	-.1180	-.3572	.0316	.0493	.0107
60.96	-3.81	2.4219	-.1313	-.3383	-.0161	.0082	.0050
60.96	.19	2.4225	-.1465	-.3118	-.0115	-.0045	.0004
60.95	4.13	2.4243	-.1273	-.3341	-.0099	-.0101	-.0040
60.94	8.12	2.4151	-.1169	-.3450	-.0482	-.0424	-.0091
60.93	10.12	2.4083	-.1111	-.3553	-.0721	-.0577	-.0127
60.92	15.12	2.3819	-.0995	-.3795	-.1165	-.0672	-.0228
60.88	20.04	2.3048	-.0857	-.3799	-.1430	-.0601	-.0302
60.92	30.00	2.2953	-.0988	-.3112	-.2814	-.0970	-.0597

RUN 110   Q= 91.40 PSF   RN/FT= 2.148   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
51.29	30.01	2.4933	-.0331	-.3347	-.1826	-.0887	-.1080
51.29	20.02	2.5240	-.0384	-.2743	-.0120	-.0357	-.0535
51.29	15.07	2.4938	-.0432	-.2752	.0372	-.0277	-.0391
51.28	10.10	2.4390	-.0403	-.3044	.0437	-.0221	-.0269
51.26	8.13	2.4317	-.0431	-.3178	.0485	-.0287	-.0175
51.25	4.17	2.3718	-.0468	-.3494	.0520	-.0158	-.0004
51.26	.17	2.3707	-.0619	-.3550	.0108	-.0094	.0096
51.26	-3.78	2.3753	-.0534	-.3611	-.0713	.0170	.0028
51.32	-7.73	2.4710	-.0434	-.3263	-.0596	.0250	.0240
51.34	-9.75	2.4665	-.0450	-.3141	-.0430	.0259	.0329

RUN 111   Q= 92.00 PSF   RN/FT= 2.150   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
41.06	-9.77	2.2957	.0407	-.3592	.0180	.0330	.0201
41.02	-7.79	2.2430	.0460	-.3565	.0530	.0155	.0226
40.97	-3.80	2.1695	.0503	-.3860	.0831	-.0118	.0093
40.97	.17	2.2123	.0537	-.4045	-.0255	.0090	-.0018
40.96	4.16	2.1921	.0523	-.3888	-.0826	.0097	-.0098
40.99	8.17	2.2454	.0510	-.3647	-.0404	-.0179	-.0177
41.00	10.11	2.2752	.0477	-.3643	-.0048	-.0240	-.0180
41.05	15.07	2.4023	.0410	-.3559	.0114	-.0409	-.0322
41.06	20.09	2.4298	.0487	-.3982	-.0423	-.0554	-.0558
41.13	30.04	2.3677	.0383	-.3930	-.2650	-.0641	-.0983

RUN 112   Q= 54.90 PSF   RN/FT= 1.325   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
40.77	.21	2.1772	.0536	-.3932	-.0198	.0072	.0005
51.00	.19	2.3835	-.0554	-.3351	.0016	-.0020	.0015
60.74	.18	2.4023	-.1272	-.2983	.0049	.0034	.0018
65.53	.20	2.4467	-.1138	-.3805	-.0082	-.0019	.0010
70.40	.19	2.4607	-.1579	-.3693	-.0098	-.0017	.0015
75.31	.18	2.4653	-.2021	-.4118	.0061	.0035	.0008
80.31	.18	2.4370	-.2213	-.3966	.0234	.0087	-.0001
85.50	.21	2.4299	-.2321	-.3988	-.0359	-.0291	.0020
90.83	.19	2.4273	-.2490	-.3880	-.0259	-.0129	.0025

RUN 113   Q= 57.40 PSF   RN/FT= 1.338   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
40.83	-9.74	2.2436	.0515	-.3638	.0071	.0237	.0202
40.84	-7.76	2.2207	.0531	-.3615	.0237	.0162	.0163
40.80	-3.78	2.1747	.0546	-.3771	.0572	-.0003	.0070
40.78	.20	2.1850	.0543	-.3977	-.0232	.0079	-.0004
40.76	4.15	2.1642	.0549	-.3788	-.0580	.0081	-.0062
40.78	8.14	2.2071	.0551	-.3659	-.0099	-.0121	-.0159
40.79	10.12	2.2548	.0527	-.3678	.0010	-.0236	-.0168
40.82	15.10	2.3543	.0532	-.3656	.0593	-.0337	-.0409
40.82	20.04	2.3626	.0516	-.3543	.0184	-.0369	-.0572
40.79	29.98	2.2904	.0460	-.3515	-.2214	-.0527	-.1021

RUN 114   Q= 13.00 PSF   RN/FT=   .318   MACH≈0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
40.54	.18	2.2803	.0418	-.3235	.0291	.0069	.0003
50.71	.17	2.4986	-.0652	-.1840	.0355	.0066	.0035
60.46	.17	2.6212	-.1533	-.0159	.0127	-.0078	.0010
80.00	.18	2.5279	-.2323	-.0386	.0090	.0082	.0009
90.50	.18	2.4283	-.2625	-.2589	-.0052	.0018	0.0000
70.06	.19	2.5251	-.1968	-.0099	.0115	.0262	-.0030
70.09	.18	2.5354	-.1954	-.0154	.0086	.0202	-.0013

RUN 115   Q= 14.50 PSF   RN/FT=   .348   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
90.57	-9.75	2.3960	-.2512	-.3037	-.0312	.0042	.0283
90.58	-7.73	2.3941	-.2549	-.2971	-.0323	.0039	.0234
90.57	-3.80	2.4126	-.2587	-.2695	.0038	.0092	.0124
90.56	.20	2.4282	-.2608	-.2610	.0032	.0018	-.0001
90.55	4.15	2.4289	-.2568	-.2732	.0066	-.0048	-.0120
90.53	8.11	2.4115	-.2491	-.3053	.0246	.0007	-.0242
90.53	10.10	2.3976	-.2465	-.3071	.0247	.0024	-.0297
90.52	15.04	2.3894	-.2332	-.3126	.0078	-.0165	-.0408
90.52	19.98	2.3578	-.2155	-.3333	-.0542	-.0463	-.0519
90.50	29.89	2.2342	-.1959	-.3599	-.1429	-.0785	-.0714

RUN 116   Q= 14.60 PSF   RN/FT= .349   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
85.18	29.89	2.2742	-.1878	-.3205	-.1586	-.0956	-.0661
85.21	20.02	2.3951	-.2082	-.2831	-.0500	-.0597	-.0496
85.22	15.07	2.4142	-.2247	-.2490	.0144	-.0211	-.0391
85.21	10.13	2.4356	-.2352	-.2516	.0319	.0057	-.0270
85.21	8.10	2.4363	-.2389	-.2381	.0571	.0107	-.0227
85.23	4.14	2.4741	-.2425	-.2147	.0290	.0058	-.0119
85.24	.16	2.4968	-.2482	-.1919	.0117	.0024	.0002
85.25	-3.80	2.4811	-.2456	-.2295	-.0078	-.0035	.0109
85.27	-7.76	2.4331	-.2439	-.2633	-.0196	-.0066	.0223
85.27	-9.76	2.4204	-.2435	-.2639	-.0171	-.0009	.0265

RUN 117   Q= 14.70 PSF   RN/FT= .352   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
80.05	-9.76	2.4792	-.2286	-.1589	.0094	.0154	.0246
80.05	-7.77	2.4782	-.2272	-.1515	-.0116	.0006	.0186
80.04	-3.80	2.5128	-.2311	-.1234	-.0192	-.0052	.0096
80.02	.15	2.5380	-.2356	-.0580	.0202	.0106	.0003
80.01	4.12	2.5138	-.2304	-.1178	.0444	.0173	-.0102
80.00	8.13	2.4955	-.2271	-.1390	.0475	.0108	-.0199
79.99	10.09	2.4904	-.2249	-.1533	.0217	-.0024	-.0246
79.98	15.07	2.4745	-.2161	-.1791	-.0105	-.0326	-.0358
79.97	19.99	2.4231	-.1993	-.2251	-.0696	-.0573	-.0459
79.95	29.92	2.2950	-.1773	-.2764	-.1858	-.1015	-.0619

RUN 118   Q= 15.00 PSF   RN/FT= .356   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
75.00	29.93	2.2916	-.1630	-.2135	-.2234	-.1174	-.0571
75.02	20.02	2.4375	-.1765	-.1737	-.1032	-.0768	-.0403
75.04	15.07	2.4940	-.1923	-.1259	-.0331	-.0473	-.0311
75.03	10.09	2.5117	-.2094	-.1136	.0320	-.0061	-.0215
75.03	8.10	2.5165	-.2121	-.1053	.0276	.0064	-.0188
75.05	4.16	2.5295	-.2174	-.0683	.0282	.0140	-.0088
75.06	.17	2.5456	-.2231	-.0180	.0094	.0138	-.0001
75.07	-3.80	2.5450	-.2232	-.0428	-.0266	-.0065	.0089
75.08	-7.77	2.5088	-.2180	-.1027	-.0424	.0013	.0167
75.09	-9.76	2.4939	-.2173	-.1165	-.0030	.0243	.0199

RUN 119   Q= 14.50 PSF   RN/FT= .351   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
70.07	-9.75	2.4972	-.1774	-.0956	-.0502	.0117	.0189
70.06	-7.73	2.5104	-.1823	-.0891	-.0660	0.0000	.0156
70.07	-3.77	2.5481	-.1930	-.0471	-.0631	-.0231	.0093
70.06	.17	2.5350	-.2029	-.0296	-.0006	.0101	-.0008
70.04	4.14	2.5368	-.1859	-.0839	.0435	.0221	-.0098
70.09	8.11	2.5226	-.1751	-.1003	.0364	.0044	-.0173
70.09	10.10	2.5308	-.1714	-.1091	.0333	-.0062	-.0211
70.08	15.05	2.4867	-.1582	-.1208	-.0243	-.0439	-.0284
70.08	20.02	2.4470	-.1536	-.1601	-.1563	-.0967	-.0365
70.06	29.95	2.3147	-.1391	-.1162	-.2750	-.1168	-.0598

RUN 120   Q= 15.00 PSF   RN/FT= .358   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
65.26	29.93	2.3537	-.1211	.0092	-.2826	-.1039	-.0579
65.27	20.05	2.4292	-.1406	-.0496	-.1291	-.0776	-.0326
65.29	15.05	2.4891	-.1430	-.0654	-.0327	-.0292	-.0270
65.30	10.11	2.5385	-.1393	-.0927	.0388	-.0018	-.0192
65.30	8.13	2.5349	-.1415	-.1066	.0747	.0129	-.0160
65.30	4.11	2.5255	-.1469	-.1237	.0944	.0428	-.0104
65.34	.16	2.5844	-.1900	.0168	-.0425	-.0283	.0030
65.32	-3.80	2.5698	-.1669	-.0360	-.0550	-.0394	.0115
65.33	-7.77	2.5509	-.1428	-.0870	-.0372	-.0100	.0164
65.33	-9.76	2.5366	-.1420	-.0877	-.0240	.0055	.0189

RUN 121   Q= 14.40 PSF   RN/FT= .352   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
60.47	-9.75	2.6382	-.1725	.1144	-.0583	-.0176	.0198
60.46	-7.76	2.5958	-.1698	.0930	-.0494	-.0331	.0195
60.43	-3.78	2.5706	-.1497	-.0377	-.0509	-.0366	.0154
60.43	.18	2.5756	-.1620	-.0252	-.0562	-.0358	.0049
60.41	4.14	2.5427	-.1486	-.0228	.0848	.0742	-.0125
60.45	8.08	2.5537	-.1548	.0864	.0936	.0672	-.0208
60.44	10.12	2.5188	-.1317	.0377	.0769	.0382	-.0195
60.45	15.06	2.5390	-.1422	.0857	-.0028	-.0055	-.0252
60.47	20.00	2.6115	-.1516	.1809	-.0022	-.0139	-.0364
60.44	29.91	2.4432	-.1037	.0623	-.2940	-.1048	-.0765

RUN 122   Q= 15.00 PSF   RN/FT= .360   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
50.73	29.88	2.3823	-.0485	.3674	-.0690	.0150	-.0749
50.73	20.03	2.5005	-.0754	.2354	.0090	.0365	-.0559
50.74	15.05	2.4936	-.0765	.2218	.0176	.0570	-.0448
50.74	10.11	2.4852	-.0761	.1271	.0799	.0814	-.0414
50.73	8.11	2.4786	-.0768	.0540	.1023	.0856	-.0357
50.73	4.12	2.4575	-.0774	-.0754	.1165	.0906	-.0175
50.74	.16	2.4364	-.0939	-.1903	.0363	.0044	.0044
50.76	-3.78	2.4715	-.0830	-.1437	-.0576	-.0158	.0166
50.78	-7.76	2.5185	-.0823	-.0491	-.0584	-.0043	.0249
50.80	-9.72	2.5519	-.0745	.0149	-.0951	-.0263	.0329

RUN 123   Q= 14.00 PSF   RN/FT= .349   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
40.55	-9.72	2.2584	.0144	-.2240	.1288	.0383	.0175
40.53	-7.76	2.2418	.0187	-.2611	.0921	.0294	.0103
40.51	-3.81	2.2150	.0209	-.3213	.0247	.0070	.0027
40.50	.18	2.2147	.0206	-.3278	.0225	.0067	-.0003
40.48	4.13	2.2071	.0299	-.2738	.1126	.0206	-.0160
40.48	8.11	2.2274	.0418	-.1529	.1080	.0365	-.0251
40.47	10.09	2.2101	.0424	-.1029	.0848	.0381	-.0237
40.48	15.03	2.1784	.0300	-.0183	-.0107	.0420	-.0332
40.52	20.01	2.1932	.0400	.0676	-.0284	.0394	-.0455
40.50	29.94	2.0870	.0450	.1369	-.2026	-.0037	-.0823

RUN 124   Q= 14.30 PSF   RN/FT= .354   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
40.56	.16	2.2034	.0174	-.3306	.0309	.0066	-.0007
50.68	.17	2.4267	-.0888	-.2014	.0318	.0068	.0043
60.43	.17	2.5490	-.1614	-.0343	-.0461	-.0426	.0059
70.13	.17	2.5431	-.1998	-.0422	.0114	.0152	-.0003
80.06	.16	2.5183	-.2385	-.0542	.0155	.0080	.0005
90.58	.17	2.4293	-.2640	-.2721	.0023	-.0003	.0004

RUN 125   Q= 14.70 PSF   RN/FT= .348   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
90.56	.17	2.5037	-.2257	-.1767	-.0027	.0020	.0007
80.03	.17	2.6060	-.2206	.0542	.0031	.0059	-.0002
70.09	.16	2.6887	-.2311	.1476	.0237	.0251	-.0023
60.54	.19	2.8060	-.2515	.1873	-.0463	-.0350	-.0008
50.78	.16	2.6959	-.2125	.0270	.0497	.0103	-.0008
40.59	.17	2.3942	-.1051	-.1564	.0228	.0048	-.0015

RUN 126   Q= 14.10 PSF   RN/FT= .341   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
40.61	-9.75	2.3335	-.1027	-.0504	.1514	.0294	.0246
40.60	-7.77	2.3463	-.1027	-.0731	.1073	.0220	.0193
40.59	-3.79	2.3688	-.1024	-.1299	-.0207	.0039	.0205
40.58	.16	2.4133	-.1007	-.1566	.0251	.0051	-.0024
40.57	4.10	2.3866	-.0949	-.0897	.1309	.0248	-.0264
40.57	8.11	2.3988	-.0954	.0100	.1301	.0359	-.0288
40.57	10.06	2.4178	-.0887	.0615	.1245	.0389	-.0323
40.57	15.04	2.3391	-.0860	.1215	.0037	.0377	-.0391
40.56	20.01	2.3304	-.0738	.1913	-.0259	.0371	-.0499
40.54	29.88	2.2282	-.0474	.2986	-.1427	.0188	-.0822

RUN 127   Q= 15.00 PSF   RN/FT= .354   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
50.76	29.88	2.5476	-.1429	.4599	-.0963	.0041	-.0965
50.78	20.02	2.6064	-.1913	.4210	-.0474	.0338	-.0576
50.80	15.05	2.6618	-.2084	.4589	-.0066	.0552	-.0478
50.81	10.08	2.7125	-.2071	.3906	.1079	.0830	-.0381
50.82	8.09	2.7080	-.2035	.3342	.1385	.0793	-.0292
50.83	4.09	2.7063	-.2074	.1980	.1755	.0753	-.0068
50.83	.21	2.7228	-.2147	.0211	.0536	.0093	-.0002
50.85	-3.80	2.7355	-.2074	.0749	-.0122	-.0198	.0237
50.86	-7.80	2.7257	-.2057	.1692	.0202	-.0173	.0363
50.88	-9.72	2.7497	-.2037	.2394	-.0292	-.0435	.0383

RUN 128   Q= 15.50 PSF   RN/FT= .361   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
60.54	-9.69	2.7457	-.2300	.2785	-.0037	-.0319	.0320
60.54	-7.75	2.7720	-.2348	.2574	-.0265	-.0368	.0297
60.53	-3.82	2.7649	-.2352	.1854	-.0552	-.0396	.0197
60.52	.18	2.7940	-.2443	.1781	-.0258	-.0405	-.0019
60.51	4.11	2.7682	-.2375	.2266	.0955	.0898	-.0134
60.50	8.10	2.7508	-.2323	.3320	.0981	.0777	-.0245
60.50	10.10	2.7328	-.2256	.2885	.0670	.0447	-.0273
60.50	15.06	2.7298	-.2191	.2926	-.0085	.0015	-.0352
60.49	19.99	2.7176	-.2126	.2901	-.0508	-.0247	-.0509
60.44	29.89	2.5492	-.1706	.2137	-.2551	-.1080	-.0956

RUN 129   Q= 15.30 PSF   RN/FT= .359   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
65.31	29.89	2.5593	-.1973	.1933	-.1971	-.1137	-.0713
65.31	20.03	2.6557	-.2175	.1482	-.1570	-.0891	-.0417
65.32	15.07	2.6792	-.2227	.1654	-.0647	-.0375	-.0317
65.32	10.14	2.6874	-.2154	.1425	.0341	.0162	-.0235
65.32	8.12	2.6472	-.2099	.1024	.0545	.0309	-.0194
65.33	4.18	2.6463	-.2201	.0996	.0952	.0614	-.0124
65.37	.13	2.7617	-.2441	.1993	-.0426	-.0283	.0024
65.34	-3.79	2.7102	-.2314	.1690	-.0500	-.0349	.0115
65.34	-7.75	2.6698	-.2206	.1675	-.0382	-.0277	.0205
65.34	-9.75	2.6781	-.2212	.1827	-.0128	-.0119	.0234

RUN 130   Q= 15.50 PSF   RN/FT= .362   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
70.12	-9.76	2.6404	-.2145	.0965	-.0331	.0003	.0212
70.12	-7.77	2.6294	-.2112	.0961	-.0378	-.0143	.0177
70.10	-3.80	2.6540	-.2254	.1291	-.0508	-.0297	.0108
70.09	.22	2.6838	-.2329	.1518	.0224	.0189	-.0016
70.07	4.18	2.6480	-.2184	.0774	.0427	.0305	-.0111
70.05	8.10	2.5986	-.2099	.0754	.0397	.0159	-.0181
70.06	10.14	2.6207	-.2124	.0803	.0047	.0031	-.0222
70.11	15.03	2.6101	-.2139	.0950	-.0660	-.0386	-.0313
70.11	20.04	2.5423	-.2076	.0310	-.1870	-.1098	-.0398
70.07	29.92	2.3984	-.1892	.0412	-.2981	-.1177	-.0754

RUN 131   Q= 14.10 PSF   RN/FT= .346   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
74.99	29.91	2.3485	-.1874	-.0953	-.2483	-.1334	-.0620
75.02	20.02	2.5102	-.2050	-.0179	-.1503	-.0860	-.0414
75.03	15.06	2.5615	-.2137	.0151	-.0688	-.0446	-.0317
75.04	10.06	2.5951	-.2199	.0421	-.0011	-.0008	-.0225
75.03	8.14	2.5926	-.2182	.0420	.0352	.0124	-.0185
75.05	4.15	2.6291	-.2216	.0706	.0322	.0170	-.0091
75.07	.17	2.6449	-.2277	.1096	.0264	.0149	-.0014
75.08	-3.80	2.6445	-.2262	.0909	-.0075	-.0099	.0080
75.10	-7.78	2.6134	-.2239	.0443	-.0108	-.0001	.0169
75.10	-9.77	2.6057	-.2233	.0336	.0254	.0192	.0207

RUN 132   Q= 14.40 PSF   RN/FT= .351   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
80.04	-9.77	2.5454	-.2173	-.0609	-.0110	.0015	.0230
80.06	-7.71	2.5640	-.2191	-.0575	-.0176	-.0054	.0185
80.04	-3.76	2.5643	-.2154	-.0180	-.0095	-.0111	.0095
80.03	.21	2.6045	-.2185	.0549	.0032	.0059	-.0002
80.02	4.18	2.5802	-.2154	-.0197	.0436	.0243	-.0101
80.01	8.10	2.5676	-.2170	-.0449	.0423	.0161	-.0193
80.00	10.14	2.5690	-.2146	-.0508	.0127	.0065	-.0241
80.00	15.01	2.5237	-.2020	-.0770	-.0136	-.0193	-.0344
79.99	20.04	2.4849	-.1932	-.0875	-.0949	-.0519	-.0432
79.96	29.94	2.3514	-.1714	-.1786	-.1939	-.1068	-.0631

RUN 133   Q= 14.50 PSF   RN/FT= .353   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
85.18	29.94	2.2878	-.1661	-.2501	-.1982	-.0956	-.0649
85.20	20.02	2.4473	-.1901	-.1910	-.0815	-.0513	-.0445
85.21	15.05	2.4978	-.2015	-.1810	-.0132	-.0193	-.0359
85.21	10.07	2.5357	-.2127	-.1763	.0297	.0064	-.0255
85.22	8.06	2.5340	-.2169	-.1704	.0425	.0118	-.0205
85.23	4.14	2.5668	-.2205	-.1359	.0122	-.0055	-.0091
85.23	.16	2.5593	-.2234	-.1268	.0186	-.0004	.0012
85.25	-3.80	2.5653	-.2221	-.1497	-.0039	.0037	.0109
85.26	-7.77	2.5310	-.2185	-.1774	-.0085	-.0071	.0222
85.26	-9.73	2.5195	-.2195	-.1715	-.0178	-.0023	.0255

RUN 134   Q= 14.60 PSF   RN/FT= .356   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
90.53	-9.73	2.4834	-.2168	-.2507	.0137	.0106	.0274
90.54	-7.71	2.4974	-.2204	-.2190	.0086	.0120	.0219
90.53	-3.80	2.4824	-.2234	-.1995	.0064	.0094	.0126
90.52	.18	2.4890	-.2255	-.1903	.0016	.0031	.0010
90.50	4.17	2.4977	-.2217	-.1865	.0006	-.0052	-.0112
90.49	8.10	2.4843	-.2157	-.2180	.0001	-.0079	-.0228
90.48	10.12	2.4721	-.2119	-.2423	-.0081	-.0069	-.0279
90.48	15.10	2.4359	-.2028	-.2464	-.0474	-.0279	-.0380
90.47	20.00	2.3777	-.1891	-.2660	-.1111	-.0503	-.0487
90.44	29.91	2.2164	-.1633	-.3083	-.2165	-.0746	-.0689

RUN 135   Q= 14.60 PSF   RN/FT= .349   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
40.65	.21	2.6296	-.1184	.0648	.0464	.0126	-.0002
50.83	.20	2.9196	-.1605	.1564	.0286	.0067	.0123
60.52	.19	2.9035	-.1691	.2593	-.0217	-.0270	-.0052
70.13	.19	2.7810	-.1554	.1866	.0283	.0278	-.0026
80.05	.19	2.6842	-.1496	.0506	-.0027	.0025	-.0002
90.62	.19	2.5691	-.1458	-.1698	-.0169	.0035	.0028

RUN 136   Q= 14.80 PSF   RN/FT= .352   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
90.52	-9.73	2.5412	-.1416	-.2138	.0286	.0143	.0275
90.53	-7.76	2.5542	-.1414	-.2002	.0308	.0176	.0230
90.52	-3.82	2.5605	-.1437	-.1725	.0082	.0148	.0141
90.50	.20	2.5414	-.1452	-.1551	.0000	.0022	.0015
90.50	4.13	2.5821	-.1417	-.1739	.0029	-.0082	-.0112
90.49	8.10	2.5498	-.1352	-.1945	-.0021	-.0119	-.0222
90.51	10.08	2.5554	-.1332	-.2224	-.0019	-.0142	-.0288
90.51	15.02	2.5129	-.1253	-.2236	-.0562	-.0296	-.0375
90.52	20.02	2.4629	-.1165	-.2465	-.1098	-.0476	-.0478
90.48	29.95	2.2933	-.0998	-.2768	-.1891	-.0669	-.0669

RUN 137   Q= 15.00 PSF   RN/FT= .356   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
85.19	29.94	2.3532	-.1095	-.1702	-.1612	-.0771	-.0627
85.21	19.98	2.5047	-.1225	-.1719	-.0839	-.0493	-.0443
85.22	15.05	2.5550	-.1302	-.1547	-.0231	-.0228	-.0348
85.21	10.06	2.5841	-.1377	-.1411	.0069	-.0015	-.0247
85.22	8.11	2.6022	-.1394	-.1391	.0164	.0056	-.0199
85.22	4.17	2.6225	-.1413	-.1043	.0107	-.0088	-.0100
85.24	.15	2.6142	-.1451	-.1019	.0124	.0019	.0024
85.25	-3.76	2.6199	-.1438	-.1241	.0145	.0051	.0120
85.26	-7.77	2.6141	-.1428	-.1523	-.0083	.0010	.0223
85.25	-9.77	2.5961	-.1420	-.1483	.0177	.0072	.0255

RUN 138   Q= 14.90 PSF   RN/FT= .355   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
80.01	-9.75	2.6163	-.1447	-.0379	-.0055	-.0047	.0238
80.02	-7.72	2.6227	-.1455	-.0283	-.0173	-.0115	.0200
80.00	-3.80	2.6485	-.1456	-.0219	-.0284	-.0154	.0107
79.99	.15	2.6457	-.1493	.0479	-.0064	.0036	.0002
79.98	4.16	2.6363	-.1467	-.0048	.0411	.0234	-.0099
79.96	8.15	2.6126	-.1426	-.0231	.0358	.0200	-.0199
79.95	10.09	2.5937	-.1397	-.0375	.0154	.0128	-.0240
79.94	15.08	2.5403	-.1346	-.0417	-.0294	-.0136	-.0332
79.93	20.08	2.4791	-.1282	-.0678	-.1052	-.0435	-.0414
79.91	29.93	2.3921	-.1154	-.1029	-.1870	-.0878	-.0604

RUN 139   Q= 14.50 PSF   RN/FT= .352   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
74.97	29.93	2.4102	-.1198	-.0368	-.2248	-.1154	-.0568
75.00	20.08	2.5487	-.1347	.0198	-.1392	-.0682	-.0398
74.99	15.07	2.5965	-.1416	.0464	-.0618	-.0339	-.0310
75.00	10.08	2.6524	-.1526	.0824	-.0069	-.0005	-.0213
75.00	8.13	2.6289	-.1531	.0853	.0327	.0127	-.0172
75.01	4.17	2.6790	-.1572	.1201	.0302	.0193	-.0086
75.02	.17	2.6805	-.1613	.1589	.0121	.0114	-.0010
75.04	-3.77	2.6794	-.1597	.1406	-.0126	-.0109	.0073
75.05	-7.75	2.6629	-.1561	.0814	-.0074	.0023	.0170
75.05	-9.77	2.6471	-.1537	.0551	.0240	.0188	.0204

RUN 140 Q= 14.20 PSF RN/FT= .349 MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
70.11	-9.76	2.6959	-.1511	.1453	-.0088	.0037	.0213
70.11	-7.72	2.7092	-.1494	.1537	-.0141	-.0129	.0179
70.11	-3.82	2.7394	-.1527	.1799	-.0218	-.0268	.0104
70.10	.23	2.7768	-.1578	.1955	.0301	.0245	-.0020
70.09	4.17	2.7516	-.1491	.1446	.0353	.0308	-.0098
70.08	8.16	2.7173	-.1423	.1360	.0207	.0121	-.0174
70.08	10.08	2.7118	-.1426	.1341	-.0045	-.0096	-.0196
70.07	15.04	2.6671	-.1381	.1180	-.0707	-.0541	-.0272
70.07	20.06	2.5831	-.1307	.0653	-.1695	-.1053	-.0345
70.04	29.92	2.5031	-.1177	.0200	-.2265	-.1276	-.0557

RUN 141 Q= 14.50 PSF RN/FT= .354 MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
65.26	29.91	2.5611	-.1218	.1845	-.2084	-.1018	-.0569
65.28	20.03	2.6542	-.1350	.1773	-.1560	-.0957	-.0335
65.27	15.05	2.6871	-.1396	.1656	-.0738	-.0532	-.0261
65.28	10.06	2.7220	-.1426	.1953	.0337	.0114	-.0199
65.28	8.13	2.7352	-.1432	.1703	.0565	.0286	-.0172
65.29	4.12	2.7146	-.1467	.1438	.0871	.0577	-.0123
65.33	.13	2.8024	-.1665	.2713	-.0120	-.0279	.0024
65.34	-3.71	2.7818	-.1521	.2144	-.0368	-.0370	.0119
65.34	-7.76	2.7742	-.1458	.2046	-.0169	-.0243	.0188
65.35	-9.72	2.7446	-.1453	.2080	.0109	-.0070	.0213

RUN 142   Q= 14.20 PSF   RN/FT= .352   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
60.51	-9.69	2.8413	-.1560	.3275	-.0040	-.0273	.0248
60.50	-7.77	2.8555	-.1576	.3099	-.0181	-.0369	.0234
60.49	-3.81	2.8502	-.1580	.2557	-.0546	-.0352	.0160
60.50	.18	2.8943	-.1659	.2513	-.0147	-.0298	-.0044
60.48	4.13	2.8114	-.1555	.2613	.0929	.0920	-.0106
60.46	8.10	2.7883	-.1479	.3235	.0749	.0796	-.0201
60.45	10.06	2.7558	-.1428	.2830	.0357	.0323	-.0195
60.42	15.06	2.7611	-.1433	.3349	-.0206	.0020	-.0284
60.51	20.04	2.7470	-.1418	.3420	-.0806	-.0252	-.0415
60.42	29.89	2.5878	-.1165	.2719	-.2537	-.0900	-.0835

RUN 143   Q= 14.00 PSF   RN/FT= .350   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
50.78	29.91	2.6818	-.1495	.6513	-.1037	.0149	-.0970
50.79	19.99	2.7691	-.1607	.5841	.0174	.0535	-.0620
50.79	15.06	2.8001	-.1654	.6370	.0263	.0665	-.0441
50.81	10.09	2.8476	-.1627	.5508	.1128	.0906	-.0357
50.81	8.09	2.8358	-.1615	.5030	.1516	.0900	-.0288
50.81	4.14	2.7997	-.1600	.3593	.1683	.0825	-.0119
50.82	.15	2.8838	-.1657	.1622	.0271	.0046	.0133
50.85	-3.78	2.9257	-.1657	.2402	-.0363	-.0191	.0192
50.86	-7.76	2.9146	-.1648	.3406	-.0269	-.0346	.0321
50.87	-9.73	2.9225	-.1673	.4273	-.0661	-.0566	.0341

RUN 144   Q= 13.40 PSF   RN/FT= .343   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
40.62	-9.75	2.5287	-.1284	.2007	.1520	.0331	.0309
40.61	-7.76	2.5429	-.1228	.1605	.1016	.0282	.0268
40.61	-3.75	2.6139	-.1189	.0931	-.0260	.0041	.0215
40.61	.15	2.6198	-.1198	.0691	.0512	.0122	.0000
40.62	4.14	2.7130	-.1232	.1320	.1395	.0270	-.0226
40.61	8.09	2.7909	-.1288	.2386	.1572	.0368	-.0310
40.62	10.10	2.8155	-.1301	.2994	.1435	.0433	-.0392
40.59	15.06	2.6113	-.1179	.3805	.0222	.0502	-.0525
40.61	20.01	2.6078	-.1199	.4461	-.0134	.0553	-.0655
40.60	29.88	2.4182	-.0986	.3648	-.1598	-.0052	-.1048

RUN 145   Q= 24.90 PSF   RN/FT= .595   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
40.62	.22	2.2314	.0537	-.3744	.0101	.0146	.0006
50.79	.20	2.4226	-.0526	-.2859	-.0149	.0244	-.0077
60.51	.21	2.5093	-.1115	-.1757	.0340	.0378	-.0046
70.21	.22	2.5105	-.1573	-.2486	-.0010	.0091	.0001
80.13	.20	2.5444	-.2153	-.1292	-.0313	-.0093	.0010
90.61	.20	2.4878	-.2474	-.2827	-.0015	.0026	.0005

RUN 146   Q= 25.30 PSF   RN/FT= .604   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
90.64	-9.75	2.4471	-.2362	-.3329	-.0568	.0001	.0309
90.65	-7.75	2.4396	-.2366	-.3340	-.0382	-.0030	.0241
90.66	-3.79	2.4573	-.2421	-.2974	-.0063	.0102	.0119
90.65	.16	2.4662	-.2453	-.2811	-.0132	.0033	.0004
90.64	4.15	2.4710	-.2414	-.2961	.0066	-.0060	-.0129
90.63	8.11	2.4661	-.2366	-.3358	.0110	-.0022	-.0238
90.63	10.06	2.4552	-.2320	-.3414	.0128	-.0016	-.0295
90.61	15.06	2.4264	-.2184	-.3372	.0036	-.0146	-.0414
90.61	19.97	2.4104	-.2015	-.3378	-.0313	-.0372	-.0510
90.59	29.89	2.2931	-.1824	-.3668	-.1506	-.0796	-.0710

RUN 147   Q= 24.50 PSF   RN/FT= .599   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
85.24	29.88	2.3279	-.1756	-.3386	-.1560	-.0994	-.0662
85.27	20.00	2.4438	-.1953	-.2859	-.0440	-.0454	-.0491
85.27	15.06	2.4647	-.2101	-.2542	.0271	-.0124	-.0397
85.27	10.09	2.4787	-.2184	-.2656	.0567	.0134	-.0280
85.28	8.09	2.5020	-.2217	-.2627	.0652	.0157	-.0226
85.29	4.14	2.5124	-.2215	-.2447	.0328	.0076	-.0121
85.29	.14	2.5402	-.2276	-.1989	.0007	-.0020	.0005
85.31	-3.80	2.5091	-.2234	-.2493	-.0336	-.0127	.0119
85.32	-7.74	2.4864	-.2225	-.2815	-.0478	-.0145	.0225
85.33	-9.73	2.4757	-.2213	-.2729	-.0366	-.0031	.0287

RUN 148   Q= 24.40 PSF   RN/FT= .601   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
80.11	-9.72	2.5223	-.2114	-.1824	-.0021	.0167	.0253
80.12	-7.74	2.5177	-.2117	-.1717	-.0307	.0068	.0203
80.11	-3.79	2.5360	-.2135	-.1585	-.0222	-.0011	.0099
80.09	.22	2.5339	-.2147	-.1142	-.0015	-.0073	.0019
80.08	4.12	2.5380	-.2174	-.1921	.0366	.0145	-.0101
80.06	8.11	2.5178	-.2069	-.1815	.0256	.0052	-.0193
80.06	10.13	2.4991	-.2046	-.1823	.0156	-.0051	-.0241
80.04	15.07	2.4991	-.2003	-.2161	-.0294	-.0373	-.0344
80.04	19.99	2.4590	-.1871	-.2344	-.0554	-.0549	-.0451
80.02	29.94	2.3467	-.1623	-.2903	-.1898	-.1115	-.0616

RUN 149   Q= 24.10 PSF   RN/FT= .587   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
75.06	29.95	2.3426	-.1455	-.2350	-.2392	-.1229	-.0578
75.10	20.06	2.4860	-.1642	-.2340	-.1133	-.0919	-.0395
75.12	15.04	2.5118	-.1735	-.1892	-.0546	-.0687	-.0306
75.12	10.13	2.5328	-.1848	-.1702	-.0117	-.0338	-.0192
75.12	8.10	2.5515	-.1886	-.1709	.0040	-.0242	-.0145
75.12	4.15	2.5525	-.1905	-.1802	-.0130	-.0204	-.0059
75.13	.16	2.5771	-.1957	-.1533	.0155	-.0020	.0013
75.15	-3.79	2.5699	-.1928	-.1392	-.0054	.0121	.0079
75.17	-7.75	2.5543	-.1895	-.1543	-.0081	.0249	.0156
75.17	-9.77	2.5490	-.1915	-.1617	.0075	.0443	.0201

RUN 150   Q= 24.80 PSF   RN/FT=   .596   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
70.15	-9.77	2.5439	-.1516	-.1788	.0205	.0638	.0167
70.15	-7.76	2.5438	-.1550	-.1696	.0060	.0387	.0134
70.15	-3.82	2.5624	-.1595	-.1571	.0065	.0227	.0059
70.13	.15	2.5303	-.1562	-.2420	.0210	.0179	.0001
70.11	4.14	2.5240	-.1544	-.2200	-.0123	-.0213	-.0052
70.11	8.07	2.5443	-.1516	-.2041	-.0385	-.0469	-.0120
70.11	10.14	2.5341	-.1510	-.2046	-.0500	-.0632	-.0152
70.11	15.06	2.4895	-.1405	-.2040	-.0994	-.0935	-.0260
70.11	20.05	2.4577	-.1310	-.2200	-.1696	-.1154	-.0355
70.08	29.95	2.3332	-.1187	-.1226	-.2766	-.1107	-.0602

RUN 151   Q= 24.70 PSF   RN/FT=   .595   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
65.33	29.96	2.3817	-.0947	-.0164	-.2690	-.0967	-.0564
65.34	20.03	2.4587	-.1181	-.0959	-.1466	-.0919	-.0321
65.32	15.04	2.4729	-.1096	-.2149	-.1181	-.1122	-.0210
65.32	10.07	2.5064	-.1200	-.2401	-.0682	-.0776	-.0127
65.32	8.15	2.5067	-.1155	-.2423	-.0363	-.0551	-.0104
65.32	4.16	2.5173	-.1104	-.2549	.0402	.0130	-.0070
65.34	.23	2.5089	-.1111	-.2695	.0614	.0394	-.0022
65.37	-3.79	2.5357	-.1166	-.2126	.0373	.0386	.0042
65.38	-7.79	2.5196	-.1141	-.2088	.0358	.0570	.0118
65.38	-9.75	2.5155	-.1132	-.2122	.0481	.0745	.0145

RUN 152   Q= 25.20 PSF   RN/FT= .602   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
60.51	-9.75	2.4941	-.0975	-.1910	.0631	.0733	.0158
60.50	-7.73	2.4787	-.1054	-.1825	.0346	.0542	.0123
60.49	-3.78	2.4639	-.1078	-.2012	.0150	.0316	.0036
60.48	.17	2.5024	-.1134	-.1723	.0320	.0389	-.0044
60.47	4.15	2.5052	-.1144	-.1082	.0666	.0568	-.0141
60.47	8.09	2.5037	-.1123	-.1220	.0461	.0131	-.0143
60.44	10.17	2.4735	-.0857	-.2385	-.0565	-.0582	-.0138
60.46	15.09	2.4626	-.1014	-.1279	-.1504	-.0986	-.0212
60.47	20.07	2.4491	-.1056	-.0833	-.2055	-.1207	-.0281
60.47	29.95	2.4264	-.0804	.0175	-.3082	-.1131	-.0786

RUN 153   Q= 25.50 PSF   RN/FT= .607   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
50.85	29.96	2.6059	-.0251	-.0919	-.2289	-.1205	-.1125
50.86	20.03	2.7011	-.0297	-.0928	-.0683	-.0751	-.0618
50.86	15.06	2.7257	-.0406	-.1138	.0419	-.0654	-.0494
50.82	10.11	2.5295	-.0539	.0393	.0564	.0657	-.0349
50.81	8.11	2.4728	-.0500	.0104	.0754	.0894	-.0376
50.81	4.14	2.4789	-.0550	-.1410	.1180	.0747	-.0153
50.81	.18	2.4306	-.0555	-.2808	-.0084	.0235	-.0070
50.83	-3.80	2.4779	-.0548	-.2833	-.0493	.0299	.0092
50.89	-7.79	2.6403	-.0539	-.2335	-.0563	.0739	.0276
50.90	-9.75	2.6697	-.0465	-.2440	-.0418	.0889	.0314

RUN 154   Q= 23.50 PSF   RN/FT= .583   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
40.62	-9.75	2.3308	.0478	-.2934	.1012	.0537	.0238
40.59	-7.76	2.2737	.0512	-.3086	.0916	.0367	.0158
40.58	-3.82	2.2368	.0531	-.3567	.0635	.0072	.0043
40.56	.21	2.2328	.0557	-.3770	.0180	.0157	.0011
40.55	4.12	2.2028	.0565	-.3072	-.0090	.0319	.0023
40.56	8.13	2.2451	.0648	-.1945	.0674	.0384	-.0236
40.55	10.13	2.2396	.0666	-.1484	.0546	.0415	-.0238
40.57	15.05	2.2874	.0549	-.1598	-.0503	-.0072	-.0401
40.59	20.04	2.3301	.0625	-.2323	-.1546	-.0533	-.0641
40.58	29.93	2.3112	.0670	-.2525	-.2659	-.0595	-.1060

RUN 155   Q= 39.20 PSF   RN/FT= .903   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
40.92	.18	2.1576	.0463	-.3720	-.0069	.0151	.0026
50.90	.21	2.3182	-.0554	-.2988	-.0170	.0110	-.0035
60.58	.22	2.3655	-.1184	-.2659	.0015	.0067	.0006
70.30	.21	2.4092	-.1545	-.3470	-.0129	.0030	.0006
80.13	.20	2.4562	-.2100	-.3042	-.0869	-.0412	.0018
90.68	.21	2.4182	-.2419	-.2767	-.0001	-.0008	.0002

RUN 156　　　Q= 39.40 PSF　　　RN/FT= .915　　　MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
90.64	29.96	2.2272	-.1916	-.3525	-.1302	-.0792	-.0686
90.64	20.01	2.3423	-.1991	-.3469	-.0423	-.0416	-.0497
90.64	15.06	2.3929	-.2185	-.3479	-.0014	-.0175	-.0408
90.68	10.10	2.4101	-.2306	-.3491	.0414	.0077	-.0287
90.69	8.13	2.4252	-.2350	-.3391	.0310	.0001	-.0234
90.72	4.10	2.4257	-.2428	-.3076	.0115	.0050	-.0107
90.72	.17	2.4173	-.2431	-.2798	.0024	.0001	-.0004
90.73	-3.75	2.4257	-.2424	-.3246	-.0331	-.0158	.0137
90.72	-7.84	2.4065	-.2348	-.3416	-.0393	-.0057	.0254
90.74	-9.76	2.3946	-.2323	-.3427	-.0331	-.0005	.0302

RUN 157　　　Q= 37.00 PSF　　　RN/FT= .892　　　MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
85.35	-9.75	2.4344	-.2198	-.2722	-.0496	-.0075	.0277
85.35	-7.73	2.4222	-.2183	-.3056	-.0544	-.0082	.0234
85.34	-3.77	2.4277	-.2200	-.3168	-.0529	-.0232	.0119
85.34	.13	2.4674	-.2240	-.2288	-.0248	-.0148	.0005
85.32	4.12	2.4385	-.2216	-.3032	.0361	.0152	-.0109
85.31	8.15	2.4244	-.2167	-.3218	.0489	.0126	-.0219
85.31	10.13	2.4297	-.2166	-.3222	.0447	.0037	-.0271
85.30	15.03	2.4119	-.2079	-.3046	.0059	-.0196	-.0367
85.29	20.00	2.3775	-.1953	-.2930	-.0482	-.0456	-.0467
85.28	29.93	2.2807	-.1815	-.3265	-.1494	-.0928	-.0646

RUN 158   Q= 37.70 PSF   RN/FT= .904   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
80.21	29.94	2.2964	-.1646	-.2939	-.1747	-.1127	-.0591
80.22	19.96	2.3958	-.1851	-.2702	-.0661	-.0653	-.0421
80.23	15.05	2.4160	-.1971	-.2488	-.0198	-.0365	-.0336
80.23	10.09	2.4543	-.1968	-.2654	.0290	-.0024	-.0242
80.24	8.13	2.4494	-.1971	-.2669	.0467	.0075	-.0190
80.26	4.14	2.4689	-.2046	-.2584	.0505	.0110	-.0109
80.25	.11	2.4649	-.2135	-.2996	-.0868	-.0634	.0034
80.25	-3.79	2.4545	-.2028	-.2672	-.0349	-.0163	.0118
80.27	-7.72	2.4487	-.2058	-.2614	-.0277	.0053	.0198
80.27	-9.71	2.4428	-.2071	-.2155	-.0185	.0107	.0248

RUN 159   Q= 37.10 PSF   RN/FT= .899   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
75.16	-9.70	2.4821	-.1939	-.1748	-.0085	.0379	.0209
75.16	-7.76	2.4702	-.1881	-.2046	-.0361	.0292	.0167
75.15	-3.81	2.4801	-.1895	-.2593	-.0078	.0226	.0090
75.12	.21	2.4384	-.1892	-.3125	.0165	.0185	.0002
75.12	4.19	2.4513	-.1884	-.2740	-.0234	-.0161	-.0068
75.12	8.15	2.4522	-.1847	-.2499	-.0073	-.0249	-.0172
75.13	10.10	2.4409	-.1794	-.2692	-.0343	-.0444	-.0199
75.16	15.12	2.4343	-.1803	-.2529	-.0799	-.0788	-.0290
75.14	20.05	2.3688	-.1618	-.2859	-.1468	-.1112	-.0370
75.12	29.95	2.2798	-.1400	-.2404	-.2065	-.1185	-.0552

RUN 160   Q= 37.10 PSF   RN/FT= .901   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
70.24	29.94	2.3010	-.1207	-.1291	-.2146	-.1110	-.0525
70.25	20.06	2.3642	-.1360	-.2418	-.1439	-.1140	-.0333
70.26	15.03	2.4119	-.1508	-.2471	-.0912	-.0926	-.0251
70.25	10.16	2.4221	-.1593	-.3073	-.0769	-.0764	-.0159
70.25	8.15	2.4406	-.1564	-.3289	-.0702	-.0626	-.0119
70.24	4.19	2.4144	-.1526	-.3559	-.0454	-.0349	-.0049
70.24	.16	2.4428	-.1569	-.3534	-.0156	.0015	.0007
70.25	-3.78	2.4278	-.1567	-.3479	.0103	.0353	.0065
70.28	-7.75	2.4508	-.1579	-.2396	-.0059	.0464	.0138
70.30	-9.75	2.4351	-.1550	-.2214	.0201	.0636	.0159

RUN 161   Q= 36.10 PSF   RN/FT= .892   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
65.38	-9.73	2.4090	-.1129	-.2618	.0277	.0696	.0138
65.39	-7.75	2.4144	-.1118	-.2915	.0085	.0549	.0112
65.36	-3.78	2.3889	-.1122	-.3704	.0022	.0319	.0049
65.35	.18	2.3968	-.1106	-.3718	-.0109	.0026	.0003
65.34	4.18	2.3881	-.1092	-.3701	-.0393	-.0255	-.0041
65.34	8.14	2.3877	-.1055	-.3568	-.0739	-.0623	-.0091
65.35	10.17	2.3937	-.1166	-.3120	-.0689	-.0673	-.0127
65.37	15.10	2.3814	-.1084	-.2674	-.1249	-.1093	-.0203
65.38	20.06	2.3710	-.1071	-.1785	-.1348	-.0926	-.0304
65.38	29.95	2.3348	-.1051	.0250	-.2156	-.0839	-.0527

RUN 162   Q= 36.50 PSF   RN/FT= .899   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
60.66	29.97	2.3776	-.0924	-.0174	-.2912	-.1189	-.0725
60.63	20.06	2.3360	-.0829	-.2023	-.2305	-.1364	-.0270
60.62	15.05	2.3655	-.0935	-.2353	-.1339	-.0929	-.0207
60.60	10.14	2.3713	-.0750	-.3403	-.0599	-.0674	-.0117
60.61	8.16	2.3796	-.0808	-.3453	-.0371	-.0490	-.0086
60.61	4.12	2.3686	-.1088	-.3059	.0086	-.0107	-.0026
60.63	.15	2.4060	-.1222	-.2793	.0149	.0078	.0018
60.64	-3.78	2.3684	-.1056	-.3042	.0067	.0248	.0034
60.66	-7.73	2.3585	-.0765	-.3350	.0488	.0628	.0101
60.66	-9.73	2.3650	-.0805	-.2898	.0682	.0793	.0136

RUN 163   Q= 36.10 PSF   RN/FT= .897   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
50.90	-9.71	2.5390	-.0436	-.2676	-.0608	.0602	.0323
50.89	-7.73	2.4817	-.0458	-.2735	-.0820	.0460	.0271
50.84	-3.71	2.3496	-.0448	-.3147	-.0615	.0336	.0034
50.83	.16	2.3228	-.0535	-.3039	-.0152	.0132	-.0053
50.82	4.12	2.3605	-.0555	-.2517	.0157	.0185	-.0197
50.83	8.10	2.4204	-.0479	-.2539	.0753	-.0265	-.0211
50.84	10.14	2.4878	-.0403	-.2548	.0677	-.0392	-.0289
50.86	15.10	2.4971	-.0331	-.2130	-.0178	-.0648	-.0388
50.88	20.07	2.5269	-.0232	-.1999	-.0626	-.0719	-.0570
50.83	29.94	2.4519	-.0080	-.2029	-.1353	-.0764	-.1108

RUN 164   Q= 36.40 PSF   RN/FT= .903   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
40.73	29.94	2.1944	.0524	-.2622	-.2134	-.0484	-.0995
40.78	20.03	2.3591	.0539	-.3506	-.0285	-.0532	-.0562
40.75	15.04	2.2611	.0432	-.2968	-.0653	-.0551	-.0387
40.72	10.10	2.1814	.0511	-.2953	-.0530	-.0269	-.0261
40.71	8.14	2.1558	.0500	-.3102	-.0427	-.0043	-.0168
40.70	4.15	2.1191	.0488	-.3525	-.0747	.0295	-.0055
40.72	.18	2.1610	.0488	-.3737	-.0035	.0139	.0028
40.73	-3.79	2.1412	.0463	-.3527	.0712	.0032	.0043
40.76	-7.77	2.1673	.0452	-.3147	.0578	.0149	.0166
40.77	-9.78	2.2266	.0442	-.3051	.0579	.0413	.0217

RUN 165   Q= 43.70 PSF   RN/FT= 1.067   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
40.70	.18	2.1319	.0483	-.3767	-.0164	.0136	.0024
50.85	.17	2.3124	-.0577	-.3169	-.0030	.0012	.0001
60.66	.16	2.3411	-.1241	-.2824	.0123	.0047	.0020
70.34	.15	2.4148	-.1563	-.3542	-.0180	.0013	.0009
80.34	.17	2.3958	-.2100	-.3337	-.0569	-.0394	.0019
90.79	.16	2.3826	-.2425	-.3176	-.0289	-.0157	.0011

RUN 166   Q= 44.60 PSF   RN/FT= 1.078   MACH=0.20

ALPHA	BETA	c_N	c_A	c_m	c_Y	c_n	c_l
90.81	-9.74	2.3797	-.2362	-.3463	-.0417	-.0037	.0302
90.79	-7.77	2.3738	-.2382	-.3484	-.0505	-.0122	.0251
90.79	-3.79	2.4070	-.2443	-.3398	-.0570	-.0229	.0150
90.78	.17	2.3882	-.2429	-.3113	-.0314	-.0136	.0002
90.77	4.14	2.3850	-.2396	-.3531	-.0089	-.0079	-.0115
90.75	8.11	2.3597	-.2321	-.3895	-.0027	-.0109	-.0226
90.75	10.13	2.3613	-.2308	-.3932	-.0127	-.0180	-.0288
90.74	15.05	2.3376	-.2201	-.4003	-.0524	-.0393	-.0392
90.73	20.05	2.3204	-.2013	-.3601	-.0708	-.0516	-.0484
90.70	29.93	2.2160	-.1982	-.3500	-.1198	-.0742	-.0677

RUN 167   Q= 43.60 PSF   RN/FT= 1.067   MACH=0.20

ALPHA	BETA	c_N	c_A	c_m	c_Y	c_n	c_l
85.43	29.93	2.2782	-.1868	-.3293	-.1449	-.0919	-.0644
85.44	20.04	2.3347	-.2008	-.3040	-.0548	-.0496	-.0455
85.45	15.10	2.3845	-.2143	-.2937	.0016	-.0198	-.0365
85.46	10.13	2.3944	-.2203	-.2999	.0423	.0070	-.0264
85.45	8.10	2.3800	-.2211	-.3439	.0306	-.0036	-.0222
85.46	4.15	2.3949	-.2293	-.3057	.0461	.0180	-.0103
85.48	.19	2.4235	-.2294	-.2893	-.0141	-.0197	.0009
85.49	-3.79	2.3941	-.2247	-.3244	-.0638	-.0294	.0125
85.49	-7.77	2.3802	-.2269	-.3188	-.0487	-.0088	.0234
85.50	-9.71	2.3750	-.2267	-.3137	-.0319	.0001	.0263

RUN 168   Q= 43.30 PSF   RN/FT= 1.062   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
80.22	-9.70	2.4062	-.2195	-.2639	-.0297	.0074	.0248
80.21	-7.76	2.4067	-.2157	-.2741	-.0397	-.0038	.0199
80.20	-3.81	2.4198	-.2124	-.2747	-.0677	-.0264	.0106
80.19	.16	2.4025	-.2128	-.3249	-.0731	-.0384	.0017
80.19	4.16	2.3922	-.2126	-.2960	.0032	-.0029	-.0105
80.17	8.13	2.3977	-.1985	-.3352	-.0064	-.0065	-.0195
80.18	10.12	2.3706	-.1955	-.3386	-.0222	-.0330	-.0223
80.18	15.04	2.4077	-.2009	-.2497	-.0388	-.0417	-.0348
80.17	20.05	2.3529	-.1897	-.2746	-.0941	-.0743	-.0412
80.15	29.93	2.2719	-.1684	-.2927	-.1652	-.1103	-.0588

RUN 169   Q= 44.10 PSF   RN/FT= 1.072   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
75.22	29.95	2.2902	-.1515	-.1774	-.1534	-.0926	-.0547
75.23	20.01	2.3588	-.1671	-.3010	-.1478	-.1120	-.0367
75.25	15.05	2.3957	-.1837	-.2600	-.0714	-.0747	-.0287
75.23	10.11	2.3702	-.1832	-.3658	-.0732	-.0638	-.0190
75.24	8.09	2.4011	-.1851	-.3582	-.0449	-.0511	-.0141
75.25	4.16	2.4070	-.1899	-.3514	-.0082	-.0219	-.0062
75.25	.14	2.4063	-.1953	-.3518	.0145	.0253	.0006
75.28	-3.80	2.4464	-.1944	-.2897	-.0386	.0102	.0093
75.29	-7.75	2.4299	-.1964	-.2696	-.0197	.0263	.0176
75.31	-9.78	2.4299	-.1978	-.2294	.0047	.0356	.0215

RUN 170   Q= 43.80 PSF   RN/FT= 1.069   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
70.32	-9.77	2.4166	-.1568	-.2803	.0314	.0631	.0166
70.31	-7.79	2.3893	-.1546	-.3339	.0208	.0609	.0127
70.29	-3.80	2.3875	-.1569	-.3611	.0124	.0378	.0062
70.28	.17	2.3924	-.1561	-.3526	-.0157	.0006	.0012
70.27	4.17	2.4018	-.1553	-.3606	-.0527	-.0360	-.0049
70.25	8.15	2.3807	-.1594	-.3720	-.0782	-.0646	-.0119
70.25	10.12	2.3826	-.1588	-.3827	-.0868	-.0820	-.0155
70.25	15.04	2.3670	-.1495	-.3087	-.1369	-.1041	-.0248
70.25	20.04	2.3476	-.1369	-.2483	-.1683	-.1125	-.0332
70.25	29.96	2.3169	-.1315	-.0419	-.1626	-.0714	-.0530

RUN 171   Q= 43.70 PSF   RN/FT= 1.067   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
65.47	29.97	2.2932	-.1118	-.0068	-.2022	-.0866	-.0504
65.47	20.07	2.3183	-.1114	-.2134	-.1742	-.1230	-.0285
65.46	15.06	2.3257	-.1123	-.2700	-.1096	-.1004	-.0213
65.45	10.09	2.3554	-.1191	-.3463	-.0664	-.0697	-.0124
65.45	8.10	2.3614	-.1212	-.3599	-.0531	-.0553	-.0099
65.44	4.14	2.3469	-.1129	-.3661	-.0382	-.0326	-.0046
65.44	.15	2.3713	-.1159	-.3739	-.0205	.0018	.0004
65.45	-3.79	2.3601	-.1143	-.3754	-.0033	.0350	.0040
65.48	-7.79	2.3538	-.1130	-.3612	.0170	.0624	.0100
65.50	-9.74	2.3615	-.1144	-.3332	.0355	.0741	.0128

RUN 172		Q= 43.40 PSF		RN/FT= 1.064		MACH=0.20	
ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
60.59	-9.73	2.3296	-.0789	-.3370	.0524	.0755	.0125
60.58	-7.79	2.3369	-.0781	-.3525	.0386	.0623	.0095
60.57	-3.78	2.3233	-.1054	-.3028	-.0024	.0208	.0032
60.58	.17	2.3374	-.1267	-.2818	.0116	.0042	.0017
60.56	4.12	2.3316	-.1093	-.3067	-.0005	-.0132	-.0020
60.57	8.12	2.3389	-.0833	-.3434	-.0430	-.0454	-.0094
60.57	10.15	2.3324	-.0756	-.3459	-.0582	-.0640	-.0117
60.58	15.07	2.3098	-.0828	-.2965	-.1595	-.0946	-.0205
60.60	20.05	2.3085	-.0802	-.2299	-.2580	-.1375	-.0266
60.62	29.95	2.3212	-.1001	-.0169	-.3130	-.1188	-.0541

RUN 173		Q= 43.60 PSF		RN/FT= 1.067		MACH=0.20	
ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
50.92	29.93	2.4253	-.0205	-.2079	-.1302	-.0703	-.1070
50.93	10.11	2.4346	-.0401	-.2658	.0580	-.0322	-.0288
50.91	8.13	2.4005	-.0424	-.2891	.0661	-.0289	-.0190
50.90	4.16	2.3331	-.0507	-.3282	.0520	-.0258	-.0002
50.90	.16	2.3302	-.0598	-.3212	-.0048	.0003	.0005
50.91	-3.77	2.3450	-.0481	-.3254	-.0599	.0311	.0046
50.96	-7.74	2.4726	-.0489	-.2795	-.0757	.0393	.0297
50.98	-9.74	2.4817	-.0450	-.2842	-.0843	.0446	.0329
50.96	20.07	2.5133	-.0344	-.2279	-.0754	-.0667	-.0570
50.95	15.07	2.4795	-.0376	-.2341	-.0069	-.0550	-.0393

RUN 174　　　　Q= 44.30 PSF　　　　RN/FT= 1.076　　　　MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
40.76	-9.75	2.2078	.0462	-.3486	.0040	.0274	.0201
40.74	-7.73	2.1483	.0471	-.3422	.0221	.0118	.0161
40.73	-3.79	2.1150	.0470	-.3605	.0496	.0023	.0045
40.71	.16	2.1172	.0485	-.3781	-.0258	.0150	.0012
40.68	4.13	2.0943	.0479	-.3595	-.0830	.0171	-.0051
40.69	8.16	2.1410	.0505	-.3370	-.0343	-.0116	-.0183
40.71	10.13	2.1913	.0502	-.3473	.0053	-.0199	-.0165
40.74	15.04	2.2759	.0467	-.3420	-.0251	-.0474	-.0345
40.76	20.04	2.3262	.0526	-.3395	.0018	-.0418	-.0568
40.74	29.96	2.2250	.0475	-.3142	-.2176	-.0490	-.1017

RUN 175　　　　Q= 23.70 PSF　　　　RN/FT= .590　　　　MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
40.64	.21	2.2365	.0520	-.3683	-.0110	.0094	-.0003
50.74	.21	2.4047	-.0584	-.2863	.0069	-.0002	.0052
60.51	.20	2.4342	-.1186	-.2643	.0234	.0136	.0023
70.18	.20	2.4724	-.1564	-.3392	.0001	.0124	-.0001
80.13	.21	2.4390	-.2110	-.4125	-.0057	.0024	.0006
90.62	.22	2.3704	-.2557	-.4884	-.0040	.0062	.0008

RUN 176   Q= 25.00 PSF   RN/FT= .604   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
90.65	-9.71	2.3552	-.2406	-.4954	.0845	.0925	.0248
90.66	-7.75	2.3578	-.2426	-.4832	.0630	.0809	.0215
90.66	-3.79	2.3716	-.2503	-.4519	.0417	.0502	.0098
90.64	.19	2.3679	-.2535	-.4921	-.0085	.0067	.0002
90.63	4.17	2.3865	-.2509	-.4792	-.0227	-.0218	-.0120
90.63	8.14	2.3816	-.2405	-.4612	-.1141	-.0799	-.0210
90.63	10.10	2.3819	-.2399	-.4759	-.1180	-.0887	-.0256
90.62	15.04	2.3522	-.2238	-.5054	-.1626	-.1066	-.0362
90.62	20.05	2.3148	-.2079	-.5332	-.1988	-.1266	-.0468
90.60	29.96	2.2047	-.1924	-.5462	-.2701	-.1388	-.0661

RUN 177   Q= 24.40 PSF   RN/FT= .598   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
85.27	29.97	2.2519	-.1824	-.5308	-.2747	-.1609	-.0617
85.29	20.03	2.3460	-.2040	-.5174	-.2013	-.1375	-.0439
85.31	15.07	2.3926	-.2179	-.4803	-.1539	-.1128	-.0341
85.31	10.10	2.4041	-.2258	-.4546	-.1011	-.0810	-.0237
85.31	8.11	2.4321	-.2282	-.4437	-.0875	-.0703	-.0178
85.31	4.16	2.4238	-.2306	-.4257	-.0427	-.0379	-.0088
85.31	.17	2.4312	-.2344	-.4168	.0052	.0018	.0009
85.33	-3.77	2.4187	-.2328	-.4243	.0321	.0370	.0091
85.35	-7.78	2.4099	-.2267	-.4503	.0866	.0770	.0178
85.35	-9.77	2.4003	-.2255	-.4614	.0896	.0932	.0227

RUN 178   Q= 25.10 PSF   RN/FT= .606   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
80.10	-9.77	2.4208	-.2112	-.4236	.0992	.1003	.0208
80.11	-7.75	2.4252	-.2102	-.4127	.0726	.0819	.0159
80.10	-3.77	2.4292	-.2123	-.4109	.0347	.0414	.0080
80.09	.17	2.4370	-.2095	-.4123	-.0007	.0037	.0006
80.07	4.14	2.4442	-.2117	-.4013	-.0314	-.0365	-.0077
80.07	8.10	2.4390	-.2058	-.4042	-.0980	-.0743	-.0160
80.06	10.13	2.4327	-.2038	-.4191	-.1244	-.0967	-.0200
80.06	15.10	2.3969	-.1999	-.4686	-.1846	-.1291	-.0299
80.06	20.04	2.3602	-.1881	-.4745	-.2120	-.1420	-.0396
80.03	29.95	2.2450	-.1621	-.4889	-.3066	-.1725	-.0566

RUN 179   Q= 25.30 PSF   RN/FT= .610   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
75.09	29.96	2.2419	-.1410	-.4397	-.3304	-.1739	-.0539
75.12	20.05	2.3482	-.1619	-.4605	-.2736	-.1709	-.0341
75.12	15.10	2.4147	-.1692	-.4430	-.2022	-.1432	-.0263
75.11	10.12	2.4621	-.1789	-.4020	-.1334	-.1041	-.0171
75.12	8.15	2.4566	-.1785	-.3972	-.1140	-.0840	-.0130
75.12	4.14	2.4697	-.1843	-.3815	-.0574	-.0404	-.0052
75.13	.18	2.4695	-.1857	-.3718	-.0031	.0101	.0006
75.15	-3.80	2.4548	-.1855	-.3776	.0323	.0452	.0068
75.17	-7.76	2.4496	-.1835	-.3999	.0749	.0865	.0129
75.17	-9.76	2.4188	-.1853	-.4099	.0942	.1054	.0184

RUN 180   Q= 25.30 PSF   RN/FT= .610   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
70.18	-9.76	2.4267	-.1456	-.3747	.0845	.1008	.0143
70.18	-7.75	2.4469	-.1491	-.3731	.0561	.0828	.0111
70.17	-3.77	2.4585	-.1517	-.3594	.0277	.0488	.0046
70.16	.16	2.4743	-.1568	-.3463	-.0001	.0121	.0007
70.14	4.15	2.4646	-.1535	-.3608	-.0475	-.0388	-.0040
70.13	8.12	2.4625	-.1439	-.3728	-.0954	-.0766	-.0107
70.13	10.09	2.4486	-.1438	-.3769	-.1198	-.0986	-.0137
70.13	15.08	2.3976	-.1384	-.3978	-.2019	-.1515	-.0221
70.13	20.06	2.3442	-.1281	-.4175	-.2979	-.1764	-.0313
70.11	29.97	2.2571	-.1173	-.3131	-.3601	-.1614	-.0557

RUN 181   Q= 25.00 PSF   RN/FT= .608   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
65.32	29.97	2.2887	-.0934	-.1565	-.3314	-.1325	-.0527
65.34	20.06	2.3650	-.1187	-.2844	-.2920	-.1604	-.0277
65.33	15.06	2.3976	-.1072	-.3509	-.1809	-.1415	-.0185
65.32	10.12	2.4387	-.1126	-.3519	-.1015	-.0900	-.0104
65.32	8.13	2.4269	-.1141	-.3489	-.0635	-.0689	-.0083
65.32	4.15	2.4638	-.1061	-.3523	-.0106	-.0217	-.0047
65.33	.13	2.4576	-.1090	-.3459	.0141	.0164	-.0008
65.35	-3.79	2.4401	-.1108	-.3490	.0225	.0483	.0034
65.37	-7.76	2.4221	-.1077	-.3714	.0343	.0814	.0082
65.37	-9.78	2.4039	-.1067	-.3683	.0600	.0971	.0110

RUN 182   Q= 25.60 PSF   RN/FT= .615   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
60.49	-9.77	2.3837	-.0738	-.3296	.0520	.0785	.0112
60.49	-7.73	2.3896	-.0709	-.3557	.0385	.0736	.0078
60.48	-3.76	2.4091	-.1010	-.2998	.0068	.0310	.0028
60.47	.20	2.3933	-.1179	-.2391	.0082	.0082	.0010
60.45	4.16	2.3922	-.1046	-.2837	.0081	-.0047	-.0035
60.44	8.11	2.3874	-.0784	-.3263	-.0482	-.0467	-.0091
60.44	10.11	2.3795	-.0747	-.3236	-.0823	-.0753	-.0107
60.47	15.11	2.4193	-.1156	-.1177	-.1773	-.0961	-.0216
60.47	20.04	2.3483	-.1013	-.1760	-.2561	-.1310	-.0274
60.46	29.94	2.3407	-.0956	.0180	-.3230	-.1252	-.0579

RUN 183   Q= 25.60 PSF   RN/FT= .617   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
50.81	29.96	2.5464	-.0255	-.1381	-.2506	-.1258	-.1082
50.83	20.06	2.6123	-.0392	-.1313	-.0783	-.0677	-.0503
50.81	15.07	2.5521	-.0405	-.1769	-.0254	-.0692	-.0328
50.80	10.10	2.5071	-.0617	-.1787	.0280	-.0464	-.0130
50.81	8.13	2.5132	-.0709	-.1531	.0517	-.0213	-.0140
50.78	4.15	2.4177	-.0616	-.2575	.0333	-.0125	-.0104
50.79	.16	2.4007	-.0600	-.2883	.0037	.0010	.0036
50.81	-3.77	2.4280	-.0534	-.3114	-.0674	.0370	.0040
50.85	-7.75	2.5639	-.0525	-.2885	-.0675	.0611	.0228
50.86	-9.78	2.5826	-.0490	-.2927	-.0534	.0718	.0261

RUN 184   Q= 25.30 PSF   RN/FT= .614   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
40.63	-9.76	2.2777	.0404	-.2961	.0587	.0287	.0252
40.61	-7.76	2.2339	.0439	-.3139	.0650	.0170	.0171
40.59	-3.78	2.1908	.0475	-.3582	.0590	.0045	.0057
40.57	.19	2.1839	.0494	-.3679	-.0157	.0118	.0004
40.55	4.15	2.1631	.0499	-.3458	-.0821	.0235	-.0052
40.55	8.14	2.1680	.0490	-.2816	-.0758	.0067	-.0178
40.57	10.10	2.2300	.0467	-.2652	-.0735	-.0068	-.0283
40.59	15.05	2.2839	.0371	-.2235	-.0623	-.0195	-.0416
40.60	20.03	2.2872	.0511	-.2032	-.1450	-.0392	-.0591
40.57	29.95	2.1962	.0607	-.2073	-.2560	-.0540	-.0962

RUN 185   Q= 25.00 PSF   RN/FT= .594   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
40.59	.22	2.2048	.0617	-.3132	.0338	.0102	.0002
50.84	.21	2.4847	-.0456	-.1157	.0111	.0042	.0028
60.55	.22	2.6146	-.1391	.1321	-.0179	-.0002	.0050
70.28	.20	2.6499	-.1744	.1646	-.0592	-.0327	.0006
80.21	.21	2.6061	-.2132	.1315	-.0225	-.0084	.0006
90.74	.20	2.5372	-.2484	-.0841	-.0108	-.0003	.0005

RUN 186   Q= 25.90 PSF   RN/FT= .606   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
90.75	-9.75	2.5122	-.2407	-.0994	-.0266	.0153	.0290
90.76	-7.79	2.5256	-.2419	-.0851	-.0166	.0133	.0240
90.75	-3.79	2.5197	-.2458	-.0791	-.0132	.0088	.0118
90.74	.17	2.5400	-.2510	-.0795	-.0110	.0008	.0010
90.72	4.16	2.5256	-.2504	-.0789	-.0094	-.0043	-.0107
90.71	8.15	2.5119	-.2412	-.0993	-.0065	-.0140	-.0233
90.71	10.11	2.5137	-.2393	-.0958	-.0005	-.0146	-.0288
90.69	15.06	2.4768	-.2232	-.1143	.0251	-.0092	-.0426
90.68	20.06	2.4350	-.2042	-.1497	.0216	.0012	-.0539
90.65	29.90	2.3410	-.1917	-.1519	-.0492	-.0231	-.0708

RUN 187   Q= 25.70 PSF   RN/FT= .605   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
85.29	29.91	2.3742	-.1819	-.1193	-.0621	-.0375	-.0672
85.31	20.00	2.4634	-.2002	-.1031	.0314	-.0021	-.0510
85.34	15.05	2.5351	-.2154	-.0717	.0085	-.0192	-.0392
85.34	10.09	2.5460	-.2252	-.0433	.0034	-.0199	-.0261
85.34	8.11	2.5491	-.2254	-.0344	.0013	-.0175	-.0224
85.35	4.11	2.5785	-.2334	-.0285	.0145	-.0043	-.0096
85.34	.20	2.5776	-.2344	-.0286	-.0058	-.0019	.0001
85.36	-3.77	2.5590	-.2344	-.0275	-.0144	.0068	.0104
85.37	-7.74	2.5441	-.2338	-.0390	-.0068	.0180	.0205
85.38	-9.77	2.5431	-.2337	-.0413	-.0132	.0231	.0265

RUN 188   Q= 25.40 PSF   RN/FT= .602   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
80.14	-9.75	2.5478	-.2126	.0805	-.0145	.0239	.0245
80.16	-7.72	2.5834	-.2167	.1005	-.0185	.0203	.0193
80.15	-3.79	2.5868	-.2216	.1369	-.0240	.0065	.0095
80.13	.17	2.5868	-.2206	.1410	-.0296	-.0080	.0005
80.12	4.13	2.5739	-.2137	.1181	-.0516	-.0260	-.0086
80.11	8.16	2.5661	-.2080	.0899	-.0514	-.0355	-.0189
80.10	10.12	2.5480	-.2042	.0725	-.0576	-.0366	-.0227
80.09	15.09	2.5060	-.2003	.0086	-.0034	-.0048	-.0365
80.07	20.07	2.4620	-.1926	-.0144	.0097	.0002	-.0467
80.04	29.91	2.3675	-.1743	-.0319	-.0957	-.0481	-.0624

RUN 189   Q= 25.90 PSF   RN/FT= .608   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
75.10	29.92	2.3607	-.1555	.0321	-.1287	-.0588	-.0587
75.12	20.02	2.5009	-.1685	.0196	-.0122	-.0207	-.0422
75.13	15.07	2.5254	-.1755	.0337	-.0005	-.0181	-.0316
75.14	10.05	2.5805	-.1838	.1006	-.0656	-.0600	-.0203
75.15	8.08	2.5921	-.1873	.1091	-.0680	-.0560	-.0156
75.16	4.14	2.6294	-.1981	.1443	-.0598	-.0442	-.0073
75.17	.18	2.6310	-.2012	.1686	-.0549	-.0324	.0005
75.19	-3.78	2.6362	-.2019	.1823	-.0609	-.0238	.0091
75.19	-7.76	2.6293	-.1961	.1690	-.0338	.0005	.0174
75.19	-9.75	2.6310	-.1942	.1615	-.0404	.0056	.0207

RUN 190   Q= 25.00 PSF   RN/FT= .599   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
70.20	-9.74	2.5910	-.1682	.1311	-.0296	.0156	.0204
70.21	-7.77	2.6061	-.1705	.1394	-.0443	.0143	.0166
70.22	-3.78	2.6514	-.1775	.1940	-.0806	-.0443	.0093
70.20	.18	2.6485	-.1772	.1715	-.0629	-.0367	.0005
70.18	4.17	2.6311	-.1712	.1454	-.0898	-.0631	-.0046
70.17	8.16	2.6100	-.1636	.1102	-.1097	-.0759	-.0134
70.16	10.16	2.5930	-.1568	.0885	-.0941	-.0748	-.0177
70.14	15.05	2.5335	-.1442	.0271	-.0327	-.0370	-.0283
70.15	20.06	2.5092	-.1549	.0752	-.0445	-.0370	-.0382
70.13	29.94	2.4111	-.1385	.1787	-.1826	-.0535	-.0619

RUN 191   Q= 26.00 PSF   RN/FT= .610   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
65.38	29.94	2.4570	-.1268	.2854	-.2016	-.0648	-.0565
65.39	20.06	2.5101	-.1341	.1337	-.0804	-.0556	-.0340
65.39	15.07	2.5266	-.1546	.1194	-.0583	-.0395	-.0269
65.39	10.13	2.5736	-.1666	.1199	-.0512	-.0518	-.0188
65.40	8.10	2.6095	-.1771	.1455	-.0643	-.0607	-.0145
65.42	4.14	2.6560	-.1845	.1720	-.0575	-.0644	-.0065
65.42	.18	2.6468	-.1790	.1854	-.0575	-.0380	.0003
65.43	-3.79	2.6275	-.1665	.1929	-.0472	-.0077	.0116
65.44	-7.77	2.6005	-.1544	.2088	-.0542	-.0177	.0186
65.44	-9.77	2.5818	-.1471	.1786	-.0438	-.0093	.0215

RUN 192   Q= 25.00 PSF   RN/FT= .599   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
60.57	-9.75	2.5489	-.1335	.2025	-.0785	-.0409	.0300
60.57	-7.79	2.5792	-.1245	.1930	-.0932	-.0467	.0275
60.56	-3.76	2.5694	-.1321	.1564	-.0491	-.0279	.0201
60.55	.18	2.6315	-.1429	.1386	.0297	.0410	-.0044
60.54	4.10	2.6338	-.1451	.1334	-.0085	-.0239	-.0068
60.52	8.13	2.5955	-.1428	.0790	-.0557	-.0587	-.0103
60.55	10.15	2.5792	-.1411	.0899	-.0623	-.0524	-.0156
60.55	15.06	2.5520	-.1335	.1521	-.0281	-.0344	-.0265
60.56	20.06	2.5431	-.1311	.1966	-.0515	-.0529	-.0305
60.55	29.96	2.5244	-.0980	.3336	-.1520	-.0385	-.0631

RUN 193   Q= 25.20 PSF   RN/FT= .603   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
50.84	29.98	2.6010	-.0118	.1228	-.1008	-.0578	-.1086
50.84	20.04	2.6256	-.0230	.0231	.0070	-.0393	-.0581
50.83	15.11	2.6585	-.0409	-.0289	.0292	-.0598	-.0438
50.81	10.11	2.5720	-.0546	-.0207	-.0195	-.0301	-.0378
50.79	8.10	2.4782	-.0457	.0022	-.0035	.0444	-.0330
50.80	4.11	2.4709	-.0512	-.0336	.0624	.0621	-.0206
50.80	.16	2.4853	-.0486	-.1039	.0026	.0031	.0035
50.82	-3.76	2.4788	-.0555	-.0162	-.0703	-.0471	.0206
50.84	-7.79	2.5016	-.0501	.0721	-.0953	-.0577	.0311
50.85	-9.72	2.4975	-.0463	.1134	-.1111	-.0546	.0351

RUN 194   Q= 25.20 PSF   RN/FT= .604   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
40.60	-9.73	2.1826	.0582	-.1090	-.0139	-.0147	.0239
40.59	-7.76	2.1555	.0562	-.1493	.0024	-.0120	.0184
40.57	-3.79	2.1718	.0540	-.2304	-.0004	-.0072	.0151
40.57	.19	2.2075	.0557	-.3024	.0351	.0103	-.0010
40.59	4.19	2.1763	.0587	-.2199	.0181	.0274	-.0045
40.59	8.08	2.1736	.0656	-.1371	.0268	.0375	-.0150
40.59	10.07	2.1710	.0696	-.1133	.0147	.0347	-.0245
40.61	15.03	2.2385	.0599	-.0939	-.0760	.0033	-.0342
40.62	20.06	2.2334	.0571	-.0520	-.1103	-.0287	-.0534
40.60	29.98	2.1552	.0600	.0539	-.2495	-.0285	-.0866

RUN 195   Q= 25.80 PSF   RN/FT= .605   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
40.69	.17	2.3269	.0553	-.1710	.0193	.0042	-.0004
50.76	.19	2.6137	-.0517	.0494	.0032	.0024	.0033
60.56	.18	2.6805	-.1435	.1867	.0234	.0238	-.0068
70.25	.18	2.6440	-.1674	.0898	-.0261	-.0101	.0015
80.15	.16	2.5767	-.2097	.0139	-.0022	-.0029	.0010
90.69	.17	2.5059	-.2426	-.1846	.0079	.0047	.0007

RUN 196   Q= 25.20 PSF   RN/FT= .596   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
90.72	-9.76	2.4865	-.2333	-.2378	.0649	.0721	.0285
90.72	-7.81	2.5141	-.2364	-.2205	.0657	.0591	.0233
90.72	-3.80	2.5064	-.2389	-.1993	.0422	.0329	.0115
90.71	.22	2.5186	-.2429	-.1894	-.0051	.0064	.0010
90.70	4.16	2.5237	-.2404	-.1993	-.1720	-.0341	-.0134
90.69	8.16	2.5086	-.2360	-.2242	-.0535	-.0512	-.0235
90.69	10.14	2.5056	-.2307	-.2393	-.0806	-.0608	-.0286
90.68	15.06	2.4584	-.2183	-.2557	-.1265	-.0853	-.0385
90.66	20.05	2.4218	-.2000	-.2906	-.1600	-.1085	-.0504
90.63	29.94	2.3087	-.1867	-.3173	-.2201	-.1138	-.0700

RUN 197   Q= 25.60 PSF   RN/FT= .601   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
85.27	29.93	2.3370	-.1734	-.2964	-.2344	-.1328	-.0656
85.29	20.09	2.4497	-.1952	-.2686	-.1822	-.1199	-.0474
85.31	15.03	2.5009	-.2088	-.2170	-.1224	-.0970	-.0360
85.32	10.11	2.5228	-.2180	-.1654	-.0643	-.0713	-.0261
85.32	8.10	2.5305	-.2175	-.1440	-.0572	-.0561	-.0204
85.32	4.17	2.5368	-.2224	-.1383	-.0234	-.0258	-.0095
85.31	.17	2.5383	-.2253	-.1461	.0097	.0032	.0011
85.33	-3.81	2.5387	-.2241	-.1513	.0330	.0359	.0117
85.35	-7.83	2.5182	-.2217	-.1799	.0677	.0665	.0201
85.35	-9.77	2.5119	-.2221	-.1803	.0783	.0780	.0252

RUN 198   Q= 25.10 PSF   RN/FT= .597   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
80.15	-9.77	2.5289	-.2106	-.0963	.0826	.0833	.0235
80.16	-7.74	2.5460	-.2124	-.0664	.0517	.0721	.0195
80.16	-3.83	2.5814	-.2157	.0058	.0211	.0314	.0115
80.15	.15	2.5845	-.2148	.0136	-.0010	-.0004	.0014
80.13	4.21	2.5979	-.2109	-.0236	-.0498	-.0465	-.0079
80.12	8.14	2.5522	-.2040	-.0600	-.1105	-.0775	-.0177
80.12	10.09	2.5488	-.2038	-.0867	-.1173	-.0905	-.0220
80.11	15.03	2.4927	-.1945	-.1575	-.1280	-.1047	-.0338
80.10	20.07	2.4533	-.1819	-.2139	-.1775	-.1223	-.0432
80.08	29.95	2.3404	-.1574	-.2546	-.2496	-.1438	-.0601

RUN 199   Q= 25.20 PSF   RN/FT= .599   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
75.12	29.94	2.3430	-.1383	-.1930	-.2820	-.1491	-.0584
75.14	20.10	2.4669	-.1606	-.1760	-.2442	-.1536	-.0388
75.15	15.09	2.5224	-.1731	-.0986	-.1937	-.1379	-.0280
75.15	10.10	2.5687	-.1845	-.0360	-.1566	-.1104	-.0177
75.15	8.12	2.5744	-.1871	-.0127	-.1283	-.0942	-.0136
75.16	4.17	2.6044	-.1965	.0357	-.0705	-.0514	-.0053
75.17	.16	2.6210	-.2008	.0532	-.0348	-.0199	.0011
75.18	-3.79	2.6270	-.2001	.0768	-.0285	.0047	.0104
75.19	-7.79	2.5953	-.1964	.0743	.0026	.0420	.0183
75.21	-9.73	2.5818	-.1930	.0441	.0229	.0640	.0221

RUN 200   Q= 25.50 PSF   RN/FT= .603   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
70.20	-9.74	2.5749	-.1773	.1169	.0053	.0415	.0209
70.19	-7.78	2.5786	-.1708	.0815	-.0107	.0279	.0173
70.19	-3.75	2.5979	-.1883	.1306	-.0315	-.0087	.0096
70.17	.20	2.6046	-.1721	.0937	-.0355	-.0098	.0009
70.16	4.17	2.6185	-.1671	.0670	-.0916	-.0596	-.0041
70.15	8.14	2.5762	-.1579	.0228	-.1414	-.1019	-.0111
70.14	10.11	2.5557	-.1533	.0005	-.1698	-.1162	-.0142
70.14	15.12	2.5081	-.1484	-.0681	-.2011	-.1458	-.0266
70.11	20.06	2.4166	-.1369	-.1108	-.2649	-.1597	-.0349
70.09	29.95	2.3463	-.1205	-.0401	-.3172	-.1302	-.0608

RUN 201   Q= 25.00 PSF   RN/FT= .598   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
65.35	29.94	2.4044	-.1119	.0789	-.3243	-.1349	-.0582
65.36	20.04	2.4630	-.1132	.0076	-.2024	-.1246	-.0318
65.36	15.08	2.5352	-.1172	.0072	-.1868	-.1281	-.0235
65.37	10.12	2.6019	-.1295	.0413	-.1285	-.1097	-.0134
65.38	8.17	2.6166	-.1362	.0492	-.1215	-.0971	-.0107
65.39	4.15	2.6225	-.1741	.1488	-.0580	-.0455	-.0056
65.41	.16	2.6436	-.1634	.1727	-.0082	.0202	-.0008
65.43	-3.76	2.6529	-.1737	.1930	-.0826	-.0409	.0142
65.44	-7.75	2.6126	-.1499	.1954	-.0362	.0007	.0196
65.45	-9.76	2.6158	-.1489	.1703	-.0087	.0171	.0226

RUN 202   Q= 24.80 PSF   RN/FT= .597   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
60.58	-9.75	2.6633	-.1561	.3253	-.0497	-.0125	.0209
60.57	-7.70	2.6029	-.1337	.2494	-.0292	-.0147	.0231
60.56	-3.72	2.6505	-.1403	.1903	-.0889	-.0486	.0224
60.55	.20	2.6822	-.1475	.1768	.0202	.0252	-.0050
60.53	4.16	2.6600	-.1428	.1800	.0018	.0102	-.0132
60.53	8.17	2.6642	-.1416	.2154	-.0345	-.0615	-.0165
60.53	10.12	2.6650	-.1355	.2200	-.0454	-.0727	-.0191
60.50	15.09	2.5455	-.0895	.0933	-.1484	-.1001	-.0220
60.49	20.05	2.4709	-.0853	.0420	-.2101	-.1196	-.0282
60.48	29.95	2.4683	-.0819	.1354	-.2995	-.1222	-.0759

RUN 203   Q= 24.70 PSF   RN/FT= .596   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
50.85	29.97	2.6736	-.0264	.0283	-.2693	-.1440	-.1133
50.87	19.97	2.7572	-.0459	.0911	-.0960	-.1007	-.0624
50.86	15.06	2.6897	-.0591	.1254	-.1161	-.0678	-.0535
50.84	10.13	2.6346	-.0567	.1273	.0358	.0067	-.0361
50.82	8.12	2.5562	-.0563	.1326	.0238	.0648	-.0317
50.83	4.09	2.5385	-.0582	.1348	.1002	.0698	-.0204
50.85	.21	2.6197	-.0568	.0480	.0020	.0031	.0021
50.86	-3.78	2.5709	-.0626	.1324	-.0958	-.0666	.0243
50.86	-7.75	2.5059	-.0615	.1513	-.0310	-.0603	.0390
50.87	-9.74	2.5120	-.0538	.1476	.0101	-.0426	.0405

160

RUN 204   Q= 24.20 PSF   RN/FT= .591   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
40.60	-9.73	2.2012	.0497	-.0864	.0498	-.0341	.0254
40.61	-7.69	2.2493	.0512	-.0751	-.0003	-.0307	.0155
40.61	-3.78	2.2825	.0505	-.1051	-.0687	-.0187	.0226
40.61	.22	2.3287	.0526	-.1749	.0245	.0046	-.0024
40.58	4.11	2.2500	.0557	-.0972	.0680	.0279	-.0053
40.57	8.13	2.2576	.0568	-.0881	-.0308	.0450	-.0104
40.55	10.18	2.2228	.0577	-.0937	-.0713	.0454	-.0239
40.55	15.09	2.2089	.0452	-.0660	-.1336	.0134	-.0354
40.59	20.05	2.2599	.0426	-.0788	-.2155	-.0476	-.0557
40.64	29.98	2.4191	.0547	-.1769	-.3440	-.0911	-.0956

RUN 205   Q= 25.50 PSF   RN/FT= .604   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
40.57	.20	2.1458	.0488	-.3624	.0196	.0065	.0010
50.78	.19	2.4016	-.0667	-.3049	-.0150	.0418	-.0052
60.48	.17	2.4529	-.1320	-.2277	.0473	.0276	-.0013
65.29	.17	2.4794	-.1246	-.2491	.0579	.0542	-.0044
70.18	.17	2.4910	-.1702	-.2214	.0796	.0739	-.0043
75.10	.17	2.5164	-.2110	-.1177	.0377	.0338	-.0001
80.14	.18	2.5146	-.2298	-.1266	-.0402	-.0167	.0024
85.30	.17	2.4820	-.2377	-.1539	-.0183	.0013	-.0002
90.65	.17	2.4312	-.2462	-.3043	-.0059	.0019	.0007

RUN 206   Q= 25.10 PSF   RN/FT= .600   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
90.64	-9.72	2.3976	-.2358	-.3620	-.0237	.0043	.0293
90.65	-7.76	2.4045	-.2365	-.3640	-.0347	.0020	.0237
90.65	-3.77	2.4362	-.2430	-.3104	-.0135	.0077	.0124
90.63	.16	2.4363	-.2453	-.2950	-.0086	.0025	.0009
90.63	4.13	2.4354	-.2432	-.3067	-.0015	-.0013	-.0131
90.62	8.10	2.4254	-.2399	-.3409	.0434	.0142	-.0248
90.62	10.11	2.4304	-.2345	-.3436	.0473	.0115	-.0299
90.60	15.04	2.4053	-.2192	-.3372	.0164	-.0033	-.0417
90.62	20.02	2.3724	-.2005	-.3475	-.0291	-.0306	-.0514
90.61	29.90	2.2452	-.1849	-.3631	-.1489	-.0756	-.0698

RUN 207   Q= 25.40 PSF   RN/FT= .605   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
85.30	29.90	2.3011	-.1784	-.3438	-.1731	-.0966	-.0655
85.31	20.00	2.4097	-.1977	-.2967	-.0454	-.0462	-.0486
85.33	15.03	2.4327	-.2150	-.2686	.0125	-.0121	-.0393
85.33	10.10	2.4409	-.2232	-.2530	.0439	.0157	-.0284
85.33	8.11	2.4459	-.2247	-.2652	.0498	.0214	-.0231
85.34	4.14	2.4635	-.2287	-.2602	.0414	.0219	-.0113
85.35	.16	2.4976	-.2372	-.1578	-.0017	.0019	.0007
85.36	-3.80	2.4712	-.2288	-.2564	-.0363	-.0214	.0128
85.34	-7.80	2.4415	-.2249	-.3333	-.0393	.0005	.0232
85.29	-9.74	2.4331	-.2232	-.3275	-.0196	.0095	.0269

RUN 208 $\quad$ Q= 25.00 PSF $\quad$ RN/FT= .602 $\quad$ MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
80.12	-9.72	2.4953	-.2227	-.1829	-.0245	.0189	.0258
80.13	-7.76	2.4971	-.2231	-.1624	-.0309	.0031	.0209
80.12	-3.80	2.5249	-.2290	-.1491	-.0423	-.0108	.0115
80.11	.19	2.5146	-.2311	-.1270	-.0234	-.0177	.0018
80.10	4.14	2.5052	-.2250	-.1563	-.0025	-.0035	-.0086
80.11	8.12	2.5092	-.2199	-.1731	.0177	-.0068	-.0179
80.15	10.10	2.4983	-.2171	-.1736	.0104	-.0115	-.0229
80.14	15.03	2.4663	-.2097	-.2051	-.0349	-.0444	-.0345
80.13	20.03	2.4170	-.1900	-.2545	-.0760	-.0600	-.0444
80.10	29.92	2.3052	-.1649	-.2907	-.1931	-.1081	-.0605

RUN 209 $\quad$ Q= 25.00 PSF $\quad$ RN/FT= .602 $\quad$ MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
75.12	29.92	2.3222	-.1569	-.2060	-.2317	-.1270	-.0556
75.14	20.03	2.4398	-.1737	-.1872	-.0956	-.0829	-.0390
75.11	15.06	2.4891	-.1860	-.1631	-.0559	-.0606	-.0298
75.10	10.11	2.5268	-.1971	-.1697	-.0259	-.0322	-.0200
75.11	8.11	2.5324	-.2005	-.1749	-.0061	-.0260	-.0142
75.11	4.17	2.5396	-.2069	-.1716	-.0005	-.0198	-.0058
75.13	.18	2.5531	-.2128	-.1265	.0619	.0157	.0011
75.14	-3.79	2.5543	-.2072	-.1548	-.0803	-.0315	.0119
75.17	-7.75	2.5536	-.2023	-.1513	-.0541	-.0021	.0194
75.17	-9.75	2.5060	-.1982	-.1401	-.0459	.0119	.0234

RUN 210   Q= 24.80 PSF   RN/FT= .601   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
70.18	-9.74	2.5028	-.1655	-.1181	-.0734	-.0088	.0215
70.18	-7.77	2.5273	-.1715	-.1290	-.0965	-.0261	.0180
70.17	-3.78	2.5212	-.1784	-.1605	-.0791	-.0247	.0106
70.15	.16	2.4860	-.1725	-.2105	.0921	.0747	-.0038
70.13	4.12	2.5098	-.1695	-.1563	.0960	.0642	-.0103
70.15	8.10	2.5203	-.1669	-.1568	.0338	.0060	-.0146
70.15	10.11	2.4928	-.1615	-.2057	-.0569	-.0591	-.0152
70.15	15.07	2.4736	-.1591	-.2027	-.1025	-.0861	-.0255
70.14	20.05	2.4272	-.1465	-.1759	-.1253	-.0881	-.0359
70.12	29.95	2.3451	-.1284	-.1085	-.2686	-.1081	-.0596

RUN 211   Q= 24.10 PSF   RN/FT= .593   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
65.32	29.95	2.3355	-.1049	-.0090	-.2564	-.0867	-.0559
65.31	20.08	2.4468	-.1275	-.0765	-.2350	-.0936	-.0351
65.30	15.05	2.4814	-.1295	-.0361	-.0058	-.0214	-.0257
65.31	10.07	2.5244	-.1377	-.0487	.0748	.0208	-.0184
65.31	8.10	2.5237	-.1371	-.0875	.0989	.0391	-.0155
65.32	4.12	2.5100	-.1319	-.1054	-.0027	.0746	-.0136
65.31	.15	2.4514	-.1285	-.2453	.0666	.0561	-.0039
65.35	-3.79	2.4984	-.1782	-.0974	-.0679	-.0344	.0126
65.38	-7.72	2.5529	-.1515	-.0017	-.1646	-.0574	.0180
65.37	-9.75	2.5139	-.1455	-.0296	-.1334	-.0374	.0200

RUN 212   Q= 25.30 PSF   RN/FT= .610   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
60.50	-9.74	2.5058	-.1257	.0794	-.1357	-.0528	.0210
60.50	-7.75	2.5337	-.1213	.0475	-.1631	-.0572	.0162
60.49	-3.78	2.4812	-.1497	-.0997	-.0976	-.0354	.0093
60.48	.14	2.4158	-.1326	-.2121	.0141	.0239	-.0043
60.48	4.13	2.4684	-.1371	-.1387	.0640	.0528	-.0146
60.49	8.08	2.5034	-.1324	.0633	.1206	.0867	-.0189
60.48	10.05	2.4865	-.1141	.0221	.0902	.0637	-.0201
60.51	15.07	2.5497	-.1461	.0667	.0008	-.0200	-.0273
60.52	20.05	2.5315	-.1319	.0563	-.1028	-.0736	-.0371
60.48	29.93	2.4129	-.0940	.0456	-.2926	-.1055	-.0712

RUN 213   Q= 24.10 PSF   RN/FT= .596   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
50.80	29.94	2.5830	-.0206	-.1421	-.2364	-.1172	-.1110
50.83	20.07	2.6733	-.0371	-.1212	-.1265	-.1023	-.0641
50.83	15.10	2.6705	-.0430	-.1257	-.0291	-.0914	-.0462
50.78	10.09	2.4501	-.0451	-.0180	.0385	.0574	-.0360
50.79	8.10	2.4453	-.0487	-.0135	.0864	.0802	-.0345
50.78	4.11	2.4373	-.0611	-.1617	.0900	.0768	-.0209
50.78	.14	2.4041	-.0728	-.3054	-.0106	.0401	-.0040
50.79	-3.79	2.4445	-.0651	-.1779	-.1226	-.0408	.0151
50.78	-7.72	2.4630	-.0338	-.0360	-.1404	-.0507	.0252
50.79	-9.74	2.5015	-.0514	.0387	-.0922	-.0676	.0373

RUN 214   Q= 25.70 PSF   RN/FT= .616   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
40.64	-9.72	2.2081	.0583	-.1577	-.1159	-.0290	.0277
40.63	-7.74	2.2242	.0526	-.2144	-.1000	-.0248	.0299
40.58	-3.77	2.1652	.0428	-.3166	.0012	-.0104	.0109
40.58	.16	2.1934	.0461	-.3755	.0183	.0069	.0007
40.61	4.13	2.1485	.0462	-.3338	-.0418	.0152	.0058
40.64	8.09	2.2528	.0640	-.2156	.1202	.0152	-.0269
40.63	10.07	2.2096	.0659	-.1488	.1229	.0263	-.0267
40.64	15.10	2.2746	.0446	-.2928	-.1809	-.0625	-.0441
40.65	20.01	2.2907	.0575	-.2904	-.1596	-.0632	-.0641
40.64	29.97	2.2688	.0596	-.2596	-.2757	-.0645	-.1040

RUN 215   Q= 25.20 PSF   RN/FT= .612   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
40.50	.21	2.2243	.0442	-.3549	-.1379	-.0118	.0171
50.70	.18	2.5294	-.0728	-.1914	-.0504	-.0955	-.0080
60.45	.17	2.5279	-.1244	-.1145	-.0899	-.0350	.0064
70.06	.16	2.5332	-.1753	-.1767	-.0313	-.0135	.0013
79.98	.16	2.5007	-.2337	-.2872	-.0126	.0017	.0003
90.46	.16	2.3970	-.2573	-.5260	-.0119	.0034	.0015

RUN 216   Q= 24.70 PSF   RN/FT= .607   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
90.50	-9.72	2.3690	-.2471	-.5711	.0690	.0895	.0257
90.52	-7.77	2.3906	-.2480	-.5547	.0418	.0739	.0219
90.50	-3.81	2.4047	-.2553	-.5261	.0234	.0392	.0123
90.49	.18	2.4191	-.2593	-.5123	-.0009	.0035	-.0003
90.48	4.14	2.4110	-.2578	-.5264	-.0477	-.0308	-.0103
90.48	8.12	2.3916	-.2504	-.5413	-.0911	-.0630	-.0193
90.47	10.11	2.3753	-.2443	-.5618	-.1139	-.0782	-.0238
90.47	15.05	2.3505	-.2345	-.5984	-.1854	-.1215	-.0337
90.47	20.00	2.2865	-.2227	-.6749	-.2899	-.1713	-.0429
90.45	29.94	2.1409	-.2181	-.8719	-.4318	-.2396	-.0596

RUN 217   Q= 24.70 PSF   RN/FT= .607   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
85.18	29.95	2.1451	-.1997	-.8401	-.4480	-.2571	-.0561
85.21	20.02	2.3266	-.2155	-.6298	-.3123	-.1898	-.0397
85.22	15.06	2.4072	-.2263	-.5093	-.1936	-.1341	-.0312
85.23	10.12	2.4282	-.2387	-.4538	-.1272	-.0878	-.0207
85.23	8.09	2.4401	-.2377	-.4484	-.0926	-.0736	-.0185
85.23	4.12	2.4643	-.2410	-.4181	-.0541	-.0363	-.0068
85.23	.12	2.4537	-.2374	-.4377	-.0073	.0034	.0013
85.24	-3.77	2.4318	-.2340	-.4457	.0307	.0415	.0111
85.26	-7.75	2.4203	-.2351	-.4562	.0697	.0785	.0188
85.26	-9.75	2.4050	-.2385	-.4640	.0858	.0959	.0240

RUN 218   Q= 24.10 PSF   RN/FT= .600   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
80.00	-9.75	2.4687	-.2354	-.3423	.0909	.1025	.0204
80.00	-7.77	2.4767	-.2278	-.3250	.0734	.0818	.0167
79.99	-3.81	2.5069	-.2361	-.2854	.0366	.0429	.0091
79.99	.19	2.5019	-.2353	-.2850	-.0135	.0018	.0014
79.99	4.16	2.5051	-.2293	-.3300	-.0600	-.0456	-.0065
79.97	8.10	2.4506	-.2187	-.3576	-.1022	-.0824	-.0141
79.97	10.09	2.4362	-.2306	-.3742	-.1420	-.1005	-.0189
79.96	15.07	2.3908	-.2200	-.4375	-.2216	-.1446	-.0270
79.94	20.03	2.3172	-.2048	-.5843	-.3312	-.1984	-.0363
79.96	29.93	2.1397	-.1772	-.8389	-.4897	-.2695	-.0526

RUN 219   Q= 24.70 PSF   RN/FT= .609   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
74.98	20.05	2.3303	-.1779	-.5142	-.3270	-.1894	-.0327
75.00	15.10	2.4240	-.1909	-.3679	-.2135	-.1403	-.0249
74.97	10.11	2.4615	-.1960	-.3298	-.1245	-.0785	-.0182
74.97	8.12	2.4841	-.2023	-.3298	-.1226	-.0923	-.0109
74.98	4.17	2.4972	-.2004	-.2915	-.0678	-.0463	-.0048
74.99	.18	2.5057	-.2033	-.2602	-.0182	-.0021	.0011
75.01	-3.82	2.5105	-.2068	-.2608	.0179	.0422	.0065
74.99	-7.76	2.5084	-.2121	-.2771	.0524	.0843	.0137
75.00	-9.78	2.4955	-.2123	-.3024	.0697	.1058	.0170

RUN 220   Q= 24.20 PSF   RN/FT= .603   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
70.06	-9.77	2.4897	-.1782	-.2578	.0718	.0990	.0148
70.06	-7.77	2.5197	-.1831	-.2342	.0473	.0783	.0114
70.06	-3.82	2.5379	-.1821	-.1825	.0040	.0308	.0056
70.05	.15	2.5427	-.1781	-.1775	-.0267	-.0138	.0013
70.03	4.13	2.5528	-.1810	-.1918	-.0498	-.0442	-.0026
70.04	8.12	2.5068	-.1703	-.3157	-.1001	-.0900	-.0067
70.03	10.10	2.4758	-.1654	-.2984	-.0803	-.0683	-.0150
70.07	15.05	2.4655	-.1624	-.3204	-.1904	-.1374	-.0227
70.06	20.05	2.3604	-.1497	-.4113	-.2769	-.1746	-.0306
70.02	29.92	2.1437	-.1219	-.6716	-.5002	-.2386	-.0525

RUN 221   Q= 25.00 PSF   RN/FT= .613   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
65.20	29.94	2.1944	-.1044	-.4503	-.4469	-.1980	-.0501
65.25	20.06	2.3986	-.1299	-.3109	-.2513	-.1568	-.0255
65.24	15.04	2.4692	-.1303	-.2879	-.1599	-.1218	-.0197
65.25	10.12	2.5358	-.1315	-.1991	-.0930	-.0797	-.0135
65.24	8.11	2.5045	-.1679	-.2324	-.0899	-.0503	-.0135
65.26	4.14	2.5556	-.1432	-.1591	-.0639	-.0522	.0003
65.28	.19	2.5894	-.1437	-.0779	-.0163	-.0065	.0032
65.22	-3.80	2.5364	-.1368	-.1626	-.0029	.0240	.0056
65.23	-7.78	2.5150	-.1347	-.1962	.0263	.0691	.0099
65.24	-9.78	2.4902	-.1340	-.2146	.0417	.0876	.0122

RUN 222   Q= 25.80 PSF   RN/FT=   .623   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
60.45	-9.77	2.5175	-.1169	-.1237	.0857	.0877	.0144
60.45	-7.78	2.5499	-.1275	-.0932	.0382	.0644	.0126
60.45	-3.80	2.5627	-.1360	-.0712	-.0399	.0016	.0101
60.43	.20	2.5381	-.1294	-.1041	-.0882	-.0374	.0063
60.41	4.14	2.5031	-.1169	-.1908	-.1083	-.0758	.0016
60.41	8.12	2.4980	-.1444	-.1714	-.0588	-.0360	-.0047
60.39	10.09	2.4824	-.1116	-.1813	-.0119	-.0258	-.0166
60.40	15.05	2.4694	-.0991	-.2013	-.1786	-.1154	-.0192
60.41	20.06	2.4242	-.1279	-.2153	-.2702	-.1558	-.0245
60.38	29.96	2.2502	-.1148	-.2267	-.4099	-.1756	-.0496

RUN 223   Q= 27.90 PSF   RN/FT=   .648   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
50.80	29.99	2.4522	-.0329	-.3632	-.4036	-.2151	-.1013
50.84	20.07	2.6850	-.0419	-.2250	-.2409	-.1560	-.0585
50.83	15.11	2.6707	-.0626	-.1395	-.0686	-.1050	-.0447
50.75	10.09	2.3880	-.0598	-.1299	-.0397	.0249	-.0348
50.76	8.11	2.4310	-.0569	-.1375	.0851	.0344	-.0264
50.77	4.14	2.4009	-.0760	-.1907	-.2244	-.0621	-.0198
50.79	.18	2.5104	-.0746	-.1925	-.0631	-.0980	-.0063
50.79	-3.79	2.4368	-.0677	-.1558	-.0630	-.0757	.0275
50.79	-7.75	2.3861	-.0702	-.0980	.0229	-.0243	.0302
50.80	-9.70	2.3891	-.0744	-.0909	.0737	.0063	.0304

RUN 224   Q= 25.90 PSF   RN/FT= .626   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
40.46	-9.70	2.0758	.0383	-.2904	.0711	-.0079	.0240
40.47	-7.75	2.1163	.0409	-.2790	-.0027	-.0209	.0133
40.46	-3.77	2.1513	.0415	-.2794	-.1283	-.0281	.0076
40.46	.16	2.1883	.0418	-.3559	-.1450	-.0108	.0159
40.46	4.16	2.2030	.0460	-.3419	.0676	-.0039	-.0168
40.44	8.10	2.1451	.0467	-.2736	.0565	.0123	-.0167
40.42	10.12	2.0898	.0478	-.2903	-.0523	.0074	-.0189
40.45	15.06	2.1754	.0323	-.2842	-.2257	-.0511	-.0365
40.49	20.07	2.3178	.0502	-.3891	-.2748	-.1188	-.0555
40.48	30.01	2.2332	.0504	-.4401	-.4428	-.1314	-.0778

RUN 225   Q= 91.40 PSF   RN/FT= 2.218   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
40.91	.25	2.2303	.0373	-.4206	-.0249	-.0113	.0011
51.14	.23	2.4208	-.0855	-.3746	-.0052	-.0196	.0069
60.89	.21	2.5002	-.1742	-.3342	.0029	.0067	-.0031
70.57	.19	2.4871	-.2234	-.3813	.0232	.0159	-.0001
80.54	.21	2.4829	-.2616	-.4310	.0041	.0069	.0013
91.05	.20	2.4133	-.2760	-.5364	.0033	-.0013	.0015

171

RUN 226   Q= 93.60 PSF   RN/FT= 2.231   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
91.03	-9.75	2.3995	-.2677	-.5643	.0471	.0606	.0279
91.00	-7.72	2.4028	-.2717	-.5501	.0393	.0508	.0232
91.00	-3.77	2.3991	-.2695	-.5432	.0205	.0244	.0123
90.98	.19	2.4202	-.2795	-.5374	-.0058	-.0005	.0016
90.97	4.18	2.3978	-.2641	-.5390	-.0123	-.0257	-.0107
90.96	8.15	2.4058	-.2705	-.5521	-.0567	-.0514	-.0207
90.96	10.10	2.4145	-.2716	-.5713	-.0703	-.0651	-.0276
90.97	15.04	2.3625	-.2616	-.5951	-.1317	-.0928	-.0373
90.94	20.01	2.3053	-.2443	-.6498	-.1835	-.1145	-.0483
90.95	29.93	2.2119	-.2462	-.6887	-.2599	-.1487	-.0675

RUN 227   Q= 94.20 PSF   RN/FT= 2.230   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
85.64	29.95	2.2362	-.2290	-.6680	-.2790	-.1596	-.0636
85.62	20.02	2.3083	-.2353	-.6047	-.1778	-.1088	-.0454
85.64	15.09	2.3710	-.2499	-.5612	-.1379	-.1024	-.0354
85.65	10.10	2.4065	-.2555	-.5214	-.0837	-.0704	-.0256
85.65	8.15	2.4019	-.2559	-.5077	-.0677	-.0576	-.0199
85.67	4.16	2.4195	-.2596	-.4818	-.0277	-.0315	-.0091
85.63	.16	2.4275	-.2685	-.4606	-.0065	-.0060	.0018
85.63	-3.80	2.4211	-.2624	-.4827	.0188	.0281	.0115
85.64	-7.77	2.4135	-.2608	-.5080	.0475	.0555	.0209
85.64	-9.75	2.4017	-.2593	-.5158	.0481	.0687	.0271

RUN 228   Q= 91.40 PSF   RN/FT= 2.191   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
80.45	-9.75	2.4505	-.2497	-.4687	.0496	.0564	.0246
80.44	-7.74	2.4162	-.2488	-.4579	.0358	.0446	.0186
80.43	-3.79	2.4493	-.2526	-.4576	.0048	.0201	.0107
80.43	.16	2.4644	-.2578	-.4331	.0017	.0109	.0011
80.43	4.17	2.4741	-.2534	-.4177	-.0241	-.0262	-.0097
80.42	8.11	2.4637	-.2470	-.4484	-.0684	-.0585	-.0176
80.48	10.11	2.4381	-.2408	-.4686	-.0881	-.0756	-.0228
80.45	15.09	2.3934	-.2341	-.5167	-.1366	-.1004	-.0332
80.43	20.08	2.3437	-.2205	-.5706	-.1788	-.1123	-.0431
80.40	29.94	2.2695	-.2001	-.5485	-.1650	-.0869	-.0621

RUN 229   Q= 92.50 PSF   RN/FT= 2.199   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
75.44	29.95	2.2754	-.1713	-.4871	-.1624	-.0855	-.0576
75.47	20.06	2.3499	-.1908	-.5366	-.1794	-.1075	-.0402
75.49	15.08	2.3927	-.2055	-.4896	-.1100	-.0833	-.0316
75.52	10.14	2.4467	-.2245	-.4007	-.0398	-.0444	-.0207
75.53	8.13	2.4906	-.2292	-.4040	-.0264	-.0315	-.0170
75.53	4.14	2.4671	-.2307	-.4040	.0139	-.0012	-.0081
75.53	.13	2.4660	-.2354	-.4268	.0035	.0028	.0016
75.55	-3.77	2.4829	-.2369	-.4415	.0116	.0252	.0095
75.57	-7.75	2.4634	-.2334	-.4447	.0276	.0414	.0166
75.58	-9.73	2.4474	-.2284	-.4355	.0369	.0506	.0211

RUN 230   Q= 92.40 PSF   RN/FT= 2.191   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
70.54	-9.72	2.4615	-.1969	-.4057	.0046	.0350	.0181
70.52	-7.78	2.4670	-.1976	-.4187	.0054	.0330	.0142
70.52	-3.83	2.4837	-.1985	-.4180	.0031	.0179	.0079
70.52	.14	2.4847	-.2224	-.3880	.0166	.0162	.0002
70.49	4.13	2.4970	-.1958	-.4163	.0175	-.0003	-.0062
70.49	8.14	2.4970	-.1889	-.4064	.0157	-.0176	-.0142
70.50	10.12	2.4813	-.1865	-.3928	.0155	-.0246	-.0179
70.49	15.10	2.4259	-.1772	-.3855	-.0586	-.0592	-.0266
70.45	20.04	2.3787	-.1688	-.4107	-.1021	-.0560	-.0372
70.38	29.97	2.2337	-.1450	-.4537	-.2011	-.0848	-.0549

RUN 231   Q= 90.50 PSF   RN/FT= 2.166   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
65.69	29.98	2.2384	-.1173	-.3635	-.2010	-.0673	-.0538
65.69	22.11	2.3321	-.1316	-.3631	-.0837	-.0401	-.0372
65.74	15.10	2.4451	-.1420	-.3686	-.0311	-.0405	-.0271
65.78	10.08	2.4639	-.1490	-.3855	.0290	-.0217	-.0166
65.80	4.16	2.4737	-.1512	-.3549	.0387	.0088	-.0082
65.82	.14	2.4871	-.1919	-.3401	.0198	.0114	-.0020
65.82	-3.79	2.4924	-.1521	-.3619	-.0696	-.0258	.0098
65.84	-7.80	2.4854	-.1530	-.3562	-.0640	-.0010	.0156
65.85	-9.77	2.4689	-.1524	-.3592	-.0411	.0160	.0186

RUN 232   Q= 92.00 PSF   RN/FT= 2.179   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
60.87	-9.75	2.4606	-.1130	-.3532	-.0341	.0079	.0176
60.87	-7.70	2.4621	-.1163	-.3477	-.0835	-.0195	.0150
60.88	-3.77	2.4794	-.1613	-.2610	-.1052	-.0522	.0111
60.88	.19	2.4792	-.1717	-.3346	-.0055	.0076	-.0039
60.86	4.08	2.4665	-.1569	-.2581	.1141	.0592	-.0091
60.84	8.08	2.4712	-.1398	-.3298	.0806	.0258	-.0135
60.82	10.10	2.4309	-.1182	-.3556	.0302	-.0055	-.0158
60.80	15.07	2.3652	-.1027	-.3462	-.0624	-.0360	-.0238
60.78	20.10	2.3352	-.1011	-.3438	-.1228	-.0601	-.0308
60.80	30.01	2.3133	-.1012	-.2952	-.2329	-.0677	-.0725

RUN 233   Q= 89.60 PSF   RN/FT= 2.148   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
51.26	29.96	2.5641	-.0579	-.0499	-.0506	-.0069	-.1015
51.24	20.02	2.5743	-.0562	-.2829	.0421	-.0194	-.0431
51.22	15.01	2.5389	-.0557	-.2919	.1007	.0039	-.0408
51.20	10.09	2.4834	-.0599	-.3246	.1641	.0233	-.0255
51.20	8.06	2.4556	-.0716	-.3068	.1454	.0348	-.0127
51.18	4.15	2.3629	-.0643	-.3308	-.0087	.0543	-.0261
51.21	.15	2.4162	-.0870	-.3769	-.0023	-.0225	.0087
51.20	-3.75	2.3735	-.0671	-.3286	-.0068	-.0540	.0279
51.23	-7.74	2.4423	-.0705	-.3074	-.1545	-.0374	.0162
51.25	-9.68	2.4609	-.0644	-.3071	-.1557	-.0284	.0247

RUN 234   Q= 91.20 PSF   RN/FT= 2.164   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
40.83	-9.69	2.1150	.0396	-.3802	.0505	-.0337	.0246
40.83	-7.73	2.1185	.0410	-.3901	.0785	-.0351	.0200
40.85	-3.75	2.1850	.0400	-.4194	.0389	-.0358	.0082
40.87	.18	2.2028	.0395	-.4198	-.0297	-.0150	.0021
40.84	4.18	2.1960	.0401	-.4255	-.0407	.0219	-.0011
40.81	8.10	2.1520	.0456	-.4030	-.0690	.0361	-.0197
40.80	10.08	2.1155	.0436	-.3775	-.0798	.0316	-.0245
40.80	15.11	2.1004	.0339	-.3199	-.1246	.0141	-.0328
40.84	20.07	2.1676	.0224	-.2391	-.1097	-.0033	-.0407
40.87	29.95	2.1637	.0376	.0212	-.1301	.0118	-.0776

RUN 235   Q= 93.20 PSF   RN/FT= 2.214   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
40.92	.19	2.2134	.0433	-.3945	-.0305	.0148	.0007
51.16	.20	2.4082	-.0673	-.3554	.0193	-.0080	.0076
60.95	.18	2.4323	-.1471	-.3089	-.0139	-.0076	.0000
70.59	.17	2.4792	-.1796	-.3935	-.0020	.0007	.0009
80.57	.17	2.4877	-.2467	-.4242	-.0041	.0013	.0005
91.06	.17	2.4124	-.2727	-.4957	-.0098	.0026	.0019

RUN 236   Q= 97.80 PSF   RN/FT= 2.259   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
91.06	-9.75	2.3920	-.2614	-.5295	.0527	.0669	.0272
91.05	-7.75	2.4045	-.2631	-.5192	.0442	.0582	.0226
91.01	-3.80	2.4220	-.2655	-.5121	.0135	.0291	.0120
90.99	.21	2.4258	-.2741	-.4919	-.0078	.0046	.0014
90.98	4.13	2.4080	-.2605	-.4926	-.0288	-.0266	-.0116
90.97	8.14	2.4006	-.2656	-.5184	-.0658	-.0561	-.0211
90.97	10.11	2.4006	-.2646	-.5232	-.0876	-.0676	-.0254
91.02	15.03	2.3803	-.2590	-.5610	-.1325	-.0970	-.0374
90.99	20.01	2.3170	-.2448	-.6027	-.1662	-.1030	-.0485
90.95	29.94	2.2484	-.2420	-.5919	-.1343	-.0695	-.0703

RUN 237   Q= 95.80 PSF   RN/FT= 2.233   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
85.64	29.96	2.2633	-.2238	-.5536	-.1434	-.0788	-.0656
85.67	20.01	2.3458	-.2346	-.5570	-.1815	-.1074	-.0462
85.63	15.07	2.4060	-.2496	-.5031	-.1361	-.0966	-.0364
85.63	10.13	2.4231	-.2535	-.4665	-.0958	-.0708	-.0246
85.63	8.10	2.4145	-.2536	-.4535	-.0713	-.0561	-.0206
85.64	4.16	2.4549	-.2586	-.4319	-.0332	-.0306	-.0091
85.65	.16	2.4402	-.2607	-.4249	-.0004	.0000	.0007
85.66	-3.80	2.4689	-.2627	-.4409	.0316	.0318	.0114
85.69	-7.76	2.4464	-.2616	-.4503	.0527	.0648	.0211
85.69	-9.77	2.4213	-.2557	-.4649	.0614	.0777	.0251

RUN 238   Q= 96.60 PSF   RN/FT= 2.239   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
80.47	-9.77	2.4343	-.2348	-.4519	.0691	.0800	.0228
80.47	-7.77	2.4621	-.2375	-.4433	.0526	.0673	.0185
80.45	-3.79	2.4797	-.2425	-.4301	.0173	.0350	.0097
80.45	.17	2.4640	-.2454	-.4252	-.0122	.0021	.0008
80.48	4.13	2.4862	-.2406	-.4199	-.0365	-.0327	-.0103
80.47	8.15	2.4507	-.2344	-.4388	-.0807	-.0610	-.0179
80.51	15.09	2.3942	-.2245	-.4913	-.1500	-.1003	-.0326
80.47	20.07	2.3542	-.2158	-.5319	-.1906	-.1110	-.0440
80.45	29.93	2.2848	-.1928	-.5382	-.1591	-.0846	-.0623
80.51	10.11	2.4436	-.2330	-.4597	-.1005	-.0762	-.0221

RUN 239   Q= 95.70 PSF   RN/FT= 2.223   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
75.44	29.93	2.2622	-.1609	-.5505	-.1863	-.0956	-.0577
75.47	20.04	2.3439	-.1795	-.5525	-.2003	-.1128	-.0398
75.45	15.06	2.3970	-.1933	-.5036	-.1559	-.1060	-.0304
75.47	10.12	2.4604	-.2070	-.4630	-.0977	-.0790	-.0196
75.48	8.13	2.4554	-.2072	-.4435	-.0721	-.0604	-.0153
75.49	4.13	2.4803	-.2142	-.4243	-.0323	-.0325	-.0068
75.49	.15	2.4846	-.2168	-.4208	-.0036	.0001	.0009
75.50	-3.81	2.4677	-.2156	-.4245	.0178	.0338	.0085
75.51	-7.79	2.4612	-.2108	-.4510	.0578	.0686	.0156
75.52	-9.80	2.4395	-.2081	-.4616	.0711	.0845	.0202

RUN 240   Q= 94.70 PSF   RN/FT= 2.207   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
70.58	-9.80	2.4507	-.1760	-.4340	.0570	.0813	.0164
70.57	-7.79	2.4643	-.1782	-.4218	.0375	.0676	.0132
70.56	-3.80	2.4855	-.1815	-.4021	.0122	.0324	.0061
70.56	.17	2.4708	-.1805	-.3921	-.0046	-.0002	.0003
70.56	4.12	2.4906	-.1762	-.3891	-.0215	-.0298	-.0060
70.56	8.13	2.4929	-.1733	-.4142	-.0496	-.0578	-.0123
70.56	10.09	2.4837	-.1719	-.4336	-.0666	-.0739	-.0168
70.54	15.10	2.4643	-.1634	-.4684	-.1313	-.0980	-.0266
70.51	20.07	2.4107	-.1473	-.5344	-.1800	-.1029	-.0380
70.51	29.96	2.3346	-.1358	-.5604	-.2373	-.1039	-.0566

RUN 241   Q= 93.20 PSF   RN/FT= 2.186   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
65.70	29.97	2.3511	-.1082	-.4778	-.2599	-.0929	-.0576
65.71	20.07	2.3538	-.1184	-.4538	-.1489	-.0763	-.0336
65.73	15.11	2.3944	-.1248	-.4395	-.1253	-.0849	-.0243
65.74	10.10	2.4543	-.1347	-.4267	-.0560	-.0697	-.0149
65.75	8.16	2.4652	-.1372	-.4188	-.0393	-.0539	-.0114
65.75	4.16	2.4643	-.1549	-.3794	-.0251	-.0237	-.0041
65.75	.20	2.4743	-.1405	-.3830	-.0240	-.0052	.0004
65.77	-3.78	2.4514	-.1352	-.3919	-.0066	.0213	.0060
65.73	-7.82	2.4509	-.1305	-.4174	.0224	.0602	.0112
65.74	-9.81	2.4426	-.1307	-.4173	.0303	.0748	.0141

RUN 242   Q= 93.70 PSF   RN/FT= 2.187   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
60.86	-9.81	2.4023	-.1003	-.3923	.0435	.0663	.0132
60.86	-7.80	2.4278	-.1090	-.3799	.0192	.0517	.0105
60.85	-3.83	2.4529	-.1290	-.3330	-.0303	.0085	.0043
60.87	.21	2.4205	-.1457	-.3045	-.0196	-.0090	.0003
60.87	4.17	2.4336	-.1353	-.3418	-.0060	-.0095	-.0037
60.90	8.18	2.4173	-.1226	-.3594	-.0373	-.0395	-.0098
60.90	10.17	2.4264	-.1107	-.3854	-.0629	-.0602	-.0131
60.87	15.11	2.3826	-.1034	-.3961	-.1081	-.0600	-.0231
60.85	20.04	2.3366	-.0940	-.3770	-.1235	-.0505	-.0315
60.88	29.99	2.3247	-.1090	-.3154	-.2230	-.0817	-.0604

RUN 243   Q= 94.30 PSF   RN/FT= 2.191   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
51.25	30.02	2.4816	-.0349	-.3667	-.1767	-.0779	-.1027
51.26	20.07	2.5391	-.0408	-.3138	-.0119	-.0389	-.0513
51.26	15.04	2.5233	-.0480	-.3188	.0330	-.0296	-.0416
51.27	10.08	2.5299	-.0457	-.3198	.0461	-.0263	-.0332
51.27	8.12	2.4981	-.0463	-.3284	.0606	-.0251	-.0260
51.25	.21	2.4095	-.0677	-.3562	.0245	-.0093	.0075
51.26	4.16	2.4342	-.0523	-.3600	.0599	-.0117	-.0038
51.25	-3.80	2.3948	-.0574	-.3628	-.0530	.0202	.0031
51.28	-7.83	2.4209	-.0453	-.3305	-.0492	.0307	.0197
51.23	-9.75	2.4707	-.0471	-.3225	-.0637	.0313	.0276

RUN 244   Q= 95.80 PSF   RN/FT= 2.205   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
40.99	-9.76	2.2979	.0439	-.3606	-.0138	.0398	.0160
40.95	-7.77	2.2453	.0433	-.3709	.0444	.0254	.0189
40.90	-3.82	2.1894	.0449	-.3794	.0570	-.0002	.0073
40.91	.19	2.2239	.0460	-.3987	-.0475	.0167	.0005
40.89	4.17	2.1999	.0467	-.3753	-.0861	.0097	-.0096
40.91	8.15	2.2335	.0458	-.3512	-.0585	-.0081	-.0187
40.94	10.12	2.2856	.0447	-.3553	-.0299	-.0036	-.0187
40.97	15.07	2.3618	.0461	-.3668	-.0283	-.0138	-.0356
40.98	20.09	2.3959	.0540	-.4082	-.0580	-.0330	-.0579
41.04	30.06	2.3329	.0476	-.5000	-.3051	-.0728	-.0964

RUN 245   Q= 91.30 PSF   RN/FT= 2.196   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
40.93	.19	2.1164	.0232	-.2658	-.0233	.0144	-.0016
51.15	.19	2.3478	-.0882	-.2639	.0212	-.0079	.0100
60.90	.19	2.3926	-.1692	-.2449	-.0176	-.0074	-.0006
65.74	.18	2.4145	-.1687	-.3212	-.0150	-.0054	-.0003
70.57	.17	2.4598	-.2071	-.3448	-.0032	.0013	.0008
75.49	.16	2.4692	-.2454	-.3929	.0022	.0010	.0006
80.54	.17	2.4728	-.2776	-.4090	.0047	.0018	.0013
85.68	.16	2.4608	-.2923	-.4222	.0026	.0006	.0009
91.02	.16	2.4221	-.3020	-.5018	.0005	.0039	.0013

RUN 246   Q= 91.80 PSF   RN/FT= 2.192   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
41.05	.19	2.2924	-.1102	-.0637	-.0125	.0069	.0056
51.31	.17	2.5546	-.2093	-.0041	.0259	-.0074	.0070
61.05	.16	2.6383	-.2373	-.0112	-.0048	.0007	.0011
65.81	.16	2.5896	-.2003	-.1378	.0023	.0023	.0008
70.68	.17	2.5910	-.2083	-.1727	-.0058	.0002	.0015
75.62	.16	2.5906	-.2202	-.2404	.0005	-.0006	.0008
80.62	.16	2.5880	-.2297	-.2827	.0070	.0009	.0008
85.75	.17	2.5655	-.2403	-.3388	.0052	.0045	.0013
91.02	.17	2.5162	-.2441	-.4082	.0002	.0060	.0023

RUN 247   Q= 92.10 PSF   RN/FT= 2.190   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
41.21	.18	2.5569	-.1232	.1785	.0101	.0007	-.0011
51.42	.19	2.8087	-.1510	.1579	.0118	-.0105	.0081
61.12	.19	2.7329	-.1535	.0695	-.0061	-.0070	.0058
65.82	.17	2.6462	-.1375	-.0686	-.0069	.0022	.0016
70.68	.17	2.6598	-.1478	-.1127	-.0083	.0002	.0009
75.56	.16	2.6413	-.1493	-.1891	-.0079	.0005	.0019
80.62	.17	2.6307	-.1577	-.2327	-.0039	.0019	.0018
85.69	.17	2.5809	-.1613	-.3048	-.0073	.0030	.0015
91.01	.17	2.5744	-.1677	-.3676	.0018	-.0005	.0011

RUN 248 Q= 23.60 PSF RN/FT= .587 MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
40.63	.18	2.5678	-.1076	.1890	.0350	.0086	-.0026
50.79	.19	2.8843	-.1519	.2269	.0323	.0169	.0034
60.51	.16	2.8298	-.1593	.2476	.0498	.0360	-.0067
65.31	.17	2.7549	-.1482	.1636	-.0506	-.0197	-.0003
70.14	.18	2.7451	-.1518	.0916	-.0852	-.0486	.0035
75.05	.17	2.7384	-.1576	.0579	-.0951	-.0512	.0039
80.04	.16	2.7025	-.1580	.0554	-.0110	-.0032	.0025
85.20	.17	2.6677	-.1548	-.0731	-.0071	-.0014	.0010
90.54	.17	2.6087	-.1586	-.1422	-.0116	.0006	.0009

RUN 249 Q= 24.20 PSF RN/FT= .592 MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
40.57	.17	2.3031	-.0956	-.0268	.0247	.0105	.0003
50.77	.18	2.6337	-.2018	.0987	.0142	.0233	-.0015
60.51	.17	2.7517	-.2430	.1823	.0429	.0487	-.0038
65.30	.16	2.7188	-.2364	.1711	.0662	.0577	-.0026
70.13	.16	2.6644	-.2179	.0330	-.0786	-.0446	.0036
75.04	.16	2.6426	-.2227	-.0067	-.0960	-.0544	.0046
80.07	.17	2.6415	-.2329	.0233	-.0372	-.0158	.0030
85.20	.16	2.6230	-.2369	-.0993	-.0036	.0016	.0012
90.58	.17	2.5758	-.2413	-.1849	-.0105	.0019	.0010

RUN 250   Q= 23.90 PSF   RN/FT= .590   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
40.48	.17	2.1159	.0286	-.2189	.0111	.0161	-.0011
50.67	.18	2.3990	-.0906	-.1445	-.0216	.0250	-.0007
60.46	.16	2.5034	-.1642	-.0366	.0392	.0437	-.0083
65.27	.17	2.5308	-.1880	-.0036	.0534	.0559	-.0032
70.10	.17	2.5530	-.2010	-.0189	-.0045	.0143	-.0011
75.03	.19	2.5223	-.2266	-.1192	-.0899	-.0459	.0033
80.05	.16	2.5210	-.2527	-.0805	-.0284	-.0180	.0022
85.21	.17	2.5014	-.2653	-.1741	-.0093	.0015	.0008
90.55	.17	2.4653	-.2922	-.2542	-.0067	.0033	.0011

RUN 251   Q= 93.80 PSF   RN/FT= 2.259   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
40.87	.19	2.0695	-.0205	-.2650	-.0178	.0117	-.0008
51.13	.19	2.3118	-.1320	-.2664	.0264	-.0110	.0120
60.93	.19	2.3934	-.2180	-.2512	-.0148	-.0092	.0006
65.73	.17	2.4160	-.2169	-.3321	-.0134	-.0077	.0006
70.62	.17	2.4606	-.2549	-.3534	.0030	-.0007	.0012
75.45	.17	2.4470	-.2930	-.3907	.0028	-.0008	.0007
80.55	.16	2.4596	-.3240	-.4085	-.0016	-.0001	.0025
85.68	.15	2.4485	-.3378	-.4340	-.0017	.0008	.0018
91.00	.17	2.4082	-.3479	-.5052	-.0011	.0033	.0017

RUN 252   Q= 88.30 PSF   RN/FT= 2.173   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
40.97	.17	2.2463	-.1567	-.0726	-.0218	.0053	.0059
51.28	.18	2.5462	-.2583	-.0144	.0216	-.0094	.0105
61.07	.17	2.6131	-.2878	-.0109	-.0083	.0008	.0001
65.82	.17	2.5685	-.2487	-.1465	-.0041	.0005	.0017
70.64	.17	2.5911	-.2564	-.1787	-.0122	-.0017	.0019
75.55	.17	2.5695	-.2672	-.2465	-.0063	-.0008	.0016
80.59	.17	2.5738	-.2755	-.2856	-.0056	.0006	.0018
85.70	.17	2.5367	-.2823	-.3515	.0110	.0058	.0018
91.01	.17	2.4917	-.2856	-.4092	.0055	.0043	.0022

RUN 253   Q= 89.30 PSF   RN/FT= 2.172   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
41.17	.17	2.5185	-.1753	.1738	-.0058	-.0007	.0018
51.45	.16	2.7978	-.2030	.1564	.0102	-.0146	.0108
61.15	.16	2.7077	-.2001	.0658	-.0152	-.0057	.0045
65.85	.17	2.6461	-.1845	-.0761	-.0023	.0009	.0021
70.68	.17	2.6493	-.1944	-.1120	-.0126	-.0005	.0029
75.56	.17	2.6405	-.1959	-.1915	-.0025	-.0017	.0017
80.60	.17	2.6414	-.2027	-.2412	.0002	-.0006	.0020
85.72	.17	2.5853	-.2026	-.3124	-.0047	.0045	.0025
91.04	.17	2.5556	-.2090	-.3623	.0057	.0051	.0033

RUN 254   Q= 24.30 PSF   RN/FT= .586   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
40.65	.19	2.5182	-.1574	.1860	.0393	.0109	-.0030
50.80	.19	2.8781	-.2064	.2380	.0323	.0184	.0042
60.50	.16	2.8440	-.2145	.2586	.0202	.0442	.0115
65.26	.17	2.8033	-.2060	.2304	.0548	.0446	-.0020
70.13	.18	2.7649	-.2083	.1859	-.0054	-.0096	.0013
75.06	.17	2.7350	-.2047	.0871	-.0676	-.0391	.0046
80.04	.16	2.7121	-.2024	.0459	-.0079	-.0010	.0024
85.21	.15	2.6875	-.2018	-.0805	-.0019	.0014	.0015
90.56	.15	2.6276	-.2028	-.1532	.0004	.0000	.0014

RUN 255   Q= 24.10 PSF   RN/FT= .588   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
40.55	.18	2.2815	-.1414	-.0372	.0296	.0122	.0012
50.76	.16	2.6390	-.2537	.0950	.0225	.0207	.0014
60.50	.16	2.7410	-.2957	.1800	.0555	.0512	-.0039
65.31	.14	2.7253	-.2879	.1734	.0702	.0567	-.0014
70.16	.15	2.6867	-.2722	.0788	-.0367	-.0225	.0016
75.05	.16	2.6604	-.2711	.0076	-.0783	-.0466	.0049
80.07	.16	2.6421	-.2796	.0237	-.0272	-.0128	.0037
85.22	.16	2.6244	-.2842	-.1143	.0062	.0029	.0021
90.55	.16	2.5749	-.2873	-.1900	.0007	.0029	.0030

RUN 256   Q= 24.20 PSF   RN/FT= .593   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
40.52	.16	2.0935	-.0137	-.2191	.0128	.0187	.0000
50.70	.17	2.3889	-.1367	-.1465	-.0156	.0284	.0016
60.44	.16	2.5017	-.2072	-.0390	.0547	.0448	-.0086
65.24	.16	2.5501	-.2358	-.0041	.0685	.0565	-.0021
70.12	.16	2.5739	-.2486	-.0103	.0268	.0222	.0000
75.03	.15	2.5501	-.2734	-.1022	-.0600	-.0366	.0033
80.04	.17	2.5413	-.2979	-.0802	-.0259	-.0148	.0033
85.22	.15	2.5277	-.3104	-.1881	.0049	.0015	.0012
90.57	.16	2.4748	-.3324	-.2678	.0065	.0060	.0029

RUN 257   Q= 89.30 PSF   RN/FT= 2.174   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
40.81	.18	1.9938	-.0398	-.2340	-.0214	.0113	-.0012
51.09	.18	2.2756	-.1557	-.2376	.0252	-.0092	.0117
60.89	.17	2.3623	-.2416	-.2211	.0002	-.0018	-.0015
65.70	.16	2.3897	-.2328	-.3121	-.0104	-.0029	-.0001
70.57	.16	2.4096	-.2773	-.3356	-.0006	.0007	.0004
75.49	.16	2.4281	-.3192	-.3739	.0027	.0015	.0005
80.50	.16	2.4321	-.3496	-.3887	.0081	.0021	.0007
85.64	.16	2.4316	-.3642	-.4102	.0056	.0018	.0016
91.02	.16	2.4115	-.3769	-.4938	.0071	.0051	.0012

RUN 258   Q= 89.90 PSF   RN/FT= 2.167   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
40.96	.18	2.1672	-.1790	-.0388	-.0183	.0088	.0030
51.22	.17	2.4865	-.2832	.0194	.0282	-.0087	.0108
61.04	.17	2.5660	-.3132	.0204	-.0007	.0015	.0026
65.82	.17	2.5652	-.2792	-.1239	-.0008	.0034	.0006
70.66	.18	2.5381	-.2811	-.1586	-.0069	.0000	.0012
80.54	.16	2.5468	-.3016	-.2613	.0036	.0051	.0016
85.67	.17	2.5079	-.3076	-.3282	.0058	.0063	.0007
91.03	.16	2.4925	-.3133	-.3936	.0030	.0056	.0018
75.50	.17	2.5291	-.2931	-.2238	-.0043	.0006	.0010

RUN 259   Q= 90.50 PSF   RN/FT= 2.167   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
41.13	.18	2.4277	-.2015	.2015	.0060	.0038	-.0004
51.36	.18	2.7583	-.2337	.1954	.0050	-.0137	.0113
61.05	.18	2.6741	-.2266	.1021	-.0096	-.0067	.0057
65.81	.17	2.5983	-.2103	-.0443	-.0012	.0017	.0010
70.68	.16	2.6118	-.2194	-.0925	-.0088	-.0002	.0013
75.56	.17	2.6119	-.2201	-.1722	-.0060	.0011	.0008
80.56	.16	2.5800	-.2249	-.2177	-.0021	.0040	.0011
85.70	.17	2.5754	-.2298	-.2883	.0090	.0031	.0004
91.01	.16	2.5394	-.2324	-.3579	.0029	.0043	.0025

RUN 260   Q= 22.40 PSF   RN/FT= .566   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
40.64	.20	2.4397	-.1804	.2223	.0436	.0087	-.0028
50.83	.17	2.8416	-.2354	.2667	.0267	.0147	.0024
60.47	.16	2.7696	-.2315	.2658	.0671	.0370	-.0090
65.30	.17	2.7364	-.2257	.2094	-.0024	-.0071	-.0008
70.13	.17	2.6464	-.2207	.1075	-.0776	-.0483	.0033
75.01	.17	2.6503	-.2253	.0856	-.0790	-.0452	.0031
80.00	.16	2.6632	-.2273	.0665	-.0003	-.0032	.0016
85.19	.16	2.6333	-.2249	-.0663	.0038	.0006	.0002
90.52	.15	2.5905	-.2276	-.1387	.0057	.0000	.0007

RUN 261   Q= 24.00 PSF   RN/FT= .584   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
40.54	.19	2.1738	-.1618	-.0029	.0261	.0132	-.0004
50.75	.16	2.5583	-.2784	.1251	.0174	.0184	-.0018
60.52	.15	2.6503	-.3142	.1968	.0611	.0495	-.0080
65.30	.16	2.6522	-.3090	.1823	.0522	.0302	-.0025
70.16	.15	2.5907	-.2900	.0512	-.0609	-.0419	.0025
75.03	.17	2.5825	-.2932	.0216	-.0784	-.0489	.0043
80.02	.15	2.5858	-.3019	.0413	-.0257	-.0137	.0020
85.20	.15	2.5638	-.3065	-.0961	.0057	.0028	.0020
90.56	.16	2.5402	-.3117	-.1669	-.0007	.0024	.0014

RUN 262   Q= 24.10 PSF   RN/FT= .585   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
40.45	.18	1.9929	-.0330	-.1842	.0053	.0200	-.0029
50.67	.16	2.3085	-.1595	-.1087	-.0043	.0235	.0002
60.48	.16	2.4475	-.2353	-.0096	.0617	.0483	-.0099
65.22	.15	2.4695	-.2537	.0115	.0660	.0549	-.0034
70.09	.15	2.4773	-.2631	-.1011	-.0727	-.0396	.0025
74.98	.17	2.4931	-.2970	-.0778	-.0552	-.0377	.0020
80.01	.17	2.5044	-.3202	-.0690	-.0284	-.0153	.0031
85.18	.15	2.4907	-.3390	-.1736	.0033	.0018	.0009
90.54	.17	2.4341	-.3579	-.2477	.0104	.0040	.0014

RUN 263   Q= 92.50 PSF   RN/FT= 2.217   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
40.88	.22	2.1088	.0089	-.3515	-.0595	-.0004	.0215
51.10	.19	2.3464	-.1026	-.3069	.0021	-.0118	.0240
60.89	.18	2.3737	-.1843	-.2719	-.0519	-.0056	.0155
70.60	.17	2.4398	-.2185	-.3703	-.0480	-.0038	.0148
80.51	.18	2.4256	-.2876	-.4012	-.0460	.0009	.0100
91.05	.17	2.3951	-.3169	-.4763	-.0386	.0008	.0078

RUN 264   Q= 96.90 PSF   RN/FT= 2.257   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
80.51	-9.77	2.3826	-.2736	-.4244	.0423	.0771	.0345
80.50	-7.77	2.3951	-.2762	-.4153	.0168	.0651	.0296
80.49	-3.80	2.4158	-.2837	-.4040	-.0101	.0318	.0206
80.48	.16	2.4358	-.2905	-.4007	-.0475	.0010	.0102
80.48	4.17	2.4370	-.2891	-.4022	-.0849	-.0341	.0005
80.48	8.15	2.4204	-.2864	-.4138	-.1301	-.0630	-.0089
80.51	10.12	2.3966	-.2810	-.4377	-.1488	-.0803	-.0141
80.49	15.12	2.3642	-.2720	-.4813	-.2045	-.1033	-.0270
80.49	20.07	2.3460	-.2662	-.5386	-.2422	-.1242	-.0376
80.45	29.97	2.2446	-.2494	-.5685	-.2304	-.1044	-.0586

RUN 265   Q= 95.40 PSF   RN/FT= 2.234   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
60.95	30.02	2.3254	-.1605	-.3734	-.2924	-.0925	-.0649
60.86	20.08	2.2576	-.1306	-.3966	-.1591	-.0650	-.0189
60.86	15.09	2.3155	-.1478	-.3744	-.1401	-.0683	-.0074
60.89	10.14	2.3545	-.1504	-.3627	-.1203	-.0636	.0043
60.89	8.13	2.3603	-.1624	-.3361	-.0941	-.0440	.0079
60.90	4.14	2.3725	-.1723	-.3100	-.0485	-.0114	.0139
60.91	.16	2.3639	-.1821	-.2775	-.0468	.0012	.0151
60.87	-3.78	2.3291	-.1599	-.2876	-.0605	.0040	.0227
60.87	-7.78	2.3224	-.1438	-.3274	-.0281	.0429	.0311
60.88	-9.78	2.3179	-.1376	-.3431	-.0146	.0598	.0348

RUN 266   Q= 93.60 PSF   RN/FT= 2.208   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
51.13	-9.75	2.3577	-.0824	-.2624	-.1021	.0317	.0519
51.09	-7.75	2.2943	-.0795	-.2750	-.0846	.0291	.0385
51.08	-3.79	2.2724	-.0906	-.2991	-.0893	.0123	.0199
51.10	.19	2.3359	-.1014	-.3077	-.0003	-.0133	.0235
51.15	4.09	2.3956	-.0950	-.3190	.0514	-.0100	.0030
51.17	8.12	2.4502	-.0908	-.2972	.0122	-.0221	-.0109
51.19	10.11	2.4914	-.0932	-.2944	.0121	-.0249	-.0173
51.20	15.03	2.5283	-.0961	-.3092	.0010	-.0306	-.0307
51.21	20.05	2.5507	-.0930	-.3154	-.0481	-.0551	-.0412
51.19	30.05	2.4929	-.0925	-.3854	-.2302	-.0845	-.0929

RUN 267   Q= 94.70 PSF   RN/FT= 2.218   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
41.02	30.09	2.2920	-.0048	-.4847	-.3460	-.0833	-.0776
41.01	20.07	2.3601	.0017	-.4042	-.1020	-.0500	-.0365
40.99	15.07	2.2464	-.0032	-.3673	-.0631	-.0402	-.0074
40.96	10.13	2.1749	.0012	-.3384	-.0686	-.0261	.0093
40.93	8.14	2.1219	.0048	-.3328	-.1025	-.0199	.0073
40.87	4.18	2.0782	.0080	-.3336	-.1298	-.0020	.0178
40.89	.18	2.0949	.0103	-.3486	-.0676	.0001	.0206
40.84	-3.78	2.0155	.0154	-.3231	.0499	-.0192	.0350
40.88	-7.77	2.0527	.0114	-.2779	.0495	.0048	.0459
40.93	-9.79	2.1429	.0052	-.2867	-.0030	.0245	.0451

192

RUN 268   Q= 92.70 PSF   RN/FT= 2.200   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
41.13	.20	2.5822	-.0418	-.0797	-.0816	.0076	-.0116
51.37	.18	2.7339	-.1003	-.0185	-.0659	.0127	-.0286
60.06	.17	2.6451	-.1116	-.0966	-.0581	.0045	-.0115
70.69	.17	2.6429	-.1117	-.2036	-.0514	-.0074	-.0107
80.56	.16	2.6062	-.1209	-.2984	-.0233	.0078	-.0074
91.04	.17	2.5214	-.1310	-.4031	-.0279	.0162	-.0024

RUN 269   Q= 98.10 PSF   RN/FT= 2.259   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
80.59	-9.75	2.6156	-.1429	-.3159	.0438	.0660	.0152
80.59	-7.74	2.6322	-.1428	-.3125	.0222	.0557	.0106
80.57	-3.80	2.6170	-.1342	-.2895	-.0081	.0320	.0016
80.54	.17	2.6089	-.1216	-.2996	-.0265	.0073	-.0068
80.53	4.16	2.6054	-.1166	-.3010	-.0608	-.0173	-.0157
80.51	8.14	2.5666	-.1114	-.3190	-.0929	-.0421	-.0236
80.51	10.12	2.5425	-.1074	-.3303	-.1137	-.0571	-.0284
80.49	15.14	2.5004	-.1001	-.3823	-.1639	-.0825	-.0382
80.47	20.04	2.4164	-.0934	-.4114	-.1855	-.0904	-.0474
80.42	29.95	2.3113	-.0753	-.4449	-.2017	-.0841	-.0678

RUN 270   Q= 94.90 PSF   RN/FT= 2.219   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
61.01	29.99	2.3987	-.0492	-.2277	-.2040	-.0775	-.0666
61.02	20.10	2.4584	-.0656	-.1701	-.1592	-.0454	-.0448
61.07	15.13	2.5357	-.0753	-.1698	-.1701	-.0523	-.0368
61.10	10.12	2.5853	-.0822	-.1592	-.1693	-.0607	-.0259
61.11	8.15	2.6223	-.0887	-.1538	-.1435	-.0507	-.0216
61.13	4.17	2.6376	-.0975	-.1369	-.1055	-.0244	-.0149
61.16	.16	2.6618	-.1097	-.1285	-.0759	.0004	-.0091
61.18	-3.74	2.7033	-.1165	-.1488	-.0816	.0211	-.0023
61.19	-7.79	2.6704	-.1213	-.1501	-.0556	.0472	.0035
61.20	-9.79	2.6643	-.1251	-.1512	-.0385	.0574	.0080

RUN 271   Q= 93.30 PSF   RN/FT= 2.193   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
41.26	-9.75	2.7143	-.0451	-.0560	-.0640	.0198	.0076
41.22	-7.73	2.6346	-.0416	-.0602	-.0698	.0101	.0055
41.18	-3.77	2.5840	-.0438	-.0826	-.1028	.0051	.0070
41.13	.21	2.5932	-.0413	-.0834	-.0886	.0069	-.0116
41.10	4.24	2.5443	-.0402	-.0810	-.1415	.0062	-.0176
41.10	8.15	2.4946	-.0336	-.0799	-.1445	.0022	-.0311
41.10	10.21	2.5375	-.0289	-.0900	-.0967	-.0063	-.0292
41.07	15.08	2.5600	-.0187	-.1486	-.0225	-.0328	-.0457
41.08	20.01	2.5759	-.0099	-.1958	-.0059	-.0455	-.0759
40.97	30.06	2.3739	.0046	-.3412	-.2677	-.0697	-.1354

194

RUN 272   Q= 23.80 PSF   RN/FT= .596   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
40.68	.20	2.5910	-.0258	-.0483	-.0162	.0130	-.0148
50.81	.16	2.7700	-.0940	.0657	-.0388	.0262	-.0229
60.45	.17	2.7387	-.1269	.1060	-.0107	.0405	-.0134
70.11	.18	2.6660	-.1118	-.0197	-.1234	-.0549	-.0064
80.03	.17	2.6264	-.1156	-.0236	-.0204	.0094	-.0075
90.50	.17	2.5720	-.1188	-.1931	-.0165	.0130	-.0039

RUN 273   Q= 26.10 PSF   RN/FT= .618   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
80.04	-9.72	2.6250	-.1272	-.0713	-.0573	-.0099	.0168
80.06	-7.68	2.6498	-.1270	-.0729	-.0729	-.0185	.0118
80.05	-3.80	2.6454	-.1196	-.0759	-.0601	-.0119	.0022
80.04	.17	2.6422	-.1153	-.0285	-.0071	.0114	-.0078
80.02	4.12	2.6125	-.1103	-.0767	.0214	.0252	-.0180
80.01	8.15	2.5849	-.1089	-.0691	.0259	.0264	-.0277
80.01	10.14	2.5624	-.1027	-.0823	.0184	.0216	-.0330
80.00	15.01	2.5638	-.0938	-.0684	-.0175	-.0047	-.0431
79.98	20.04	2.5019	-.0806	-.0924	-.0602	-.0342	-.0514
79.95	29.96	2.3692	-.0552	-.1485	-.1747	-.0876	-.0674

RUN 274   Q= 25.30 PSF   RN/FT=   .607   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
60.43	29.96	2.5309	-.0443	.1887	-.2050	-.0797	-.0746
60.46	19.98	2.6217	-.0663	.1159	-.2006	-.0908	-.0454
60.45	15.06	2.6245	-.0754	.0702	-.2004	-.0905	-.0353
60.46	10.14	2.6940	-.0870	.0187	-.1617	-.0815	-.0247
60.46	8.11	2.6634	-.0922	.0267	-.1222	-.0541	-.0213
60.47	4.19	2.7098	-.1055	.0642	-.0377	.0125	-.0195
60.51	.11	2.7419	-.1289	.1104	-.0014	.0426	-.0133
60.54	-3.79	2.8059	-.1401	.2610	-.1392	-.0758	.0003
60.55	-7.76	2.7917	-.1370	.2690	-.1519	-.0577	.0120
60.56	-9.72	2.8032	-.1379	.2287	-.1219	-.0237	.0138

RUN 275   Q= 23.80 PSF   RN/FT=   .589   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
40.69	-9.72	2.8098	-.0606	.1273	-.1224	.0061	.0096
40.66	-7.72	2.6639	-.0536	.0802	-.0790	.0046	.0107
40.60	-3.80	2.6223	-.0412	-.0219	-.0920	.0006	-.0002
40.58	.18	2.5738	-.0271	-.0475	-.0098	.0152	-.0159
40.56	4.13	2.5036	-.0166	.0345	.0361	.0299	-.0339
40.56	8.12	2.5540	-.0125	.1138	.0699	.0319	-.0514
40.56	10.17	2.5648	-.0109	.1525	.0840	.0383	-.0550
40.55	15.04	2.4894	-.0147	.2491	.0263	.0465	-.0604
40.53	20.05	2.4733	-.0087	.1927	-.0773	.0100	-.0672
40.47	30.00	2.3674	.0177	-.0914	-.2145	-.0451	-.1327

RUN 276   Q= 92.00 PSF   RN/FT= 2.189   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
41.29	-9.71	2.8043	.0209	.1189	-.0341	.0276	.0211
41.28	-7.72	2.7957	.0203	.1304	-.0411	.0146	.0254
41.27	-3.79	2.7690	.0215	.1243	-.0614	-.0001	.0235
41.30	.19	2.8638	.0209	.1110	-.0146	.0009	-.0007
41.25	4.15	2.8216	.0253	.1275	.0049	-.0028	-.0138
41.31	8.14	2.8523	.0275	.1144	.0263	-.0145	-.0206
41.30	10.09	2.8198	.0282	.0961	.0511	-.0202	-.0205
41.30	15.08	2.8686	.0280	.0565	.0871	-.0454	-.0318
41.30	20.04	2.8726	.0235	.0369	.0681	-.0497	-.0422
41.26	29.98	2.7700	.0181	-.1074	-.1414	-.0713	-.0853

RUN 277   Q= 95.20 PSF   RN/FT= 2.224   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
51.33	29.95	2.6470	.0126	-.0696	-.1023	-.0534	-.0976
51.38	20.06	2.7252	.0198	-.0079	-.0202	-.0423	-.0385
51.41	15.07	2.7979	.0189	-.0076	.0221	-.0515	-.0289
51.41	10.14	2.8760	.0137	.0190	.0203	-.0629	-.0199
51.40	8.14	2.8349	.0120	.0313	.0169	-.0564	-.0162
51.39	4.14	2.7922	.0093	.0681	.0250	-.0282	-.0066
51.42	.18	2.8206	.0057	.1038	.0135	-.0070	.0005
51.41	-3.79	2.7988	.0078	.0950	-.0276	.0168	.0086
51.40	-7.78	2.7838	.0092	.0334	-.0224	.0501	.0144
51.40	-9.73	2.7626	.0097	.0275	-.0268	.0539	.0174

RUN 278   Q= 92.10 PSF   RN/FT= 2.219   MACH=0.20

ALPHA	BETA	c_N	c_A	c_m	c_Y	c_n	c_l
41.28	.19	2.8654	.0208	.1104	-.0051	.0003	-.0002
51.39	.19	2.8032	.0063	.1037	.0114	-.0075	.0007
61.06	.17	2.6930	-.0027	-.0588	.0062	.0012	.0009
70.66	.17	2.6753	-.0115	-.1635	-.0045	.0007	.0014
80.52	.16	2.6206	-.0183	-.2764	.0012	.0049	.0007
90.98	.17	2.5433	-.0262	-.4016	-.0024	.0045	.0031

RUN 279   Q= 91.10 PSF   RN/FT= 2.192   MACH=0.20

ALPHA	BETA	c_N	c_A	c_m	c_Y	c_n	c_l
91.01	-9.73	2.5332	-.0253	-.4326	.0710	.0583	.0256
91.00	-7.76	2.5368	-.0246	-.4235	.0490	.0524	.0207
91.00	-3.80	2.5644	-.0256	-.4053	.0378	.0242	.0111
90.98	.17	2.5430	-.0252	-.4012	-.0007	.0035	.0015
90.98	4.16	2.5426	-.0217	-.4076	-.0322	-.0189	-.0113
90.96	8.11	2.5378	-.0197	-.4282	-.0624	-.0419	-.0195
90.96	10.12	2.5325	-.0190	-.4320	-.0757	-.0559	-.0248
90.94	15.04	2.4883	-.0151	-.4594	-.1320	-.0745	-.0361
90.95	20.02	2.4605	-.0148	-.4655	-.1744	-.1020	-.0458
90.93	29.94	2.3436	-.0091	-.5466	-.2461	-.1283	-.0659

RUN 280   Q= 90.90 PSF   RN/FT= 2.180   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
85.67	29.94	2.3670	-.0074	-.4963	-.2505	-.1354	-.0613
85.67	20.06	2.4901	-.0129	-.4304	-.1577	-.0946	-.0437
85.68	15.11	2.5224	-.0131	-.3948	-.1292	-.0880	-.0338
85.70	10.13	2.5500	-.0150	-.3689	-.0733	-.0570	-.0226
85.70	8.10	2.5710	-.0173	-.3539	-.0573	-.0452	-.0184
85.71	4.16	2.5790	-.0198	-.3420	-.0245	-.0208	-.0079
85.72	.17	2.5697	-.0224	-.3449	-.0024	.0038	.0016
85.73	-3.75	2.5763	-.0224	-.3435	.0392	.0201	.0084
85.73	-7.74	2.5725	-.0224	-.3601	.0624	.0518	.0188
85.74	-9.74	2.5679	-.0220	-.3740	.0694	.0642	.0241

RUN 281   Q= 90.40 PSF   RN/FT= 2.168   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
80.49	-9.74	2.5787	-.0199	-.3065	.0698	.0644	.0207
80.48	-7.74	2.6061	-.0205	-.2890	.0600	.0517	.0167
80.48	-3.83	2.6159	-.0195	-.2856	.0284	.0303	.0088
80.46	.19	2.6122	-.0184	-.2785	-.0057	.0038	.0008
80.46	4.15	2.6139	-.0175	-.2727	-.0407	-.0219	-.0071
80.45	8.13	2.5989	-.0145	-.2911	-.0718	-.0446	-.0169
80.45	10.14	2.5940	-.0139	-.3031	-.0957	-.0600	-.0201
80.43	15.09	2.5501	-.0111	-.3334	-.1407	-.0858	-.0299
80.42	20.05	2.5112	-.0095	-.3622	-.1427	-.0854	-.0413
80.43	29.95	2.4093	-.0084	-.4667	-.2513	-.1382	-.0584

RUN 282   Q= 92.90 PSF   RN/FT= 2.191   MACH=0.20

ALPHA	BETA	c_N	c_A	c_m	c_Y	c_n	c_l
75.51	29.98	2.4147	-.0024	-.4295	-.2338	-.1291	-.0550
75.53	20.06	2.5230	-.0045	-.3293	-.1342	-.0851	-.0385
75.54	15.10	2.5710	-.0063	-.2973	-.1377	-.0841	-.0275
75.56	10.15	2.5883	-.0077	-.2651	-.0854	-.0575	-.0185
75.57	8.11	2.6177	-.0098	-.2512	-.0648	-.0432	-.0154
75.59	4.14	2.6494	-.0122	-.2352	-.0287	-.0186	-.0072
75.60	.19	2.6559	-.0139	-.2368	.0028	.0023	.0014
75.61	-3.78	2.6417	-.0153	-.2267	.0348	.0248	.0087
75.63	-7.79	2.6189	-.0145	-.2538	.0701	.0488	.0145
75.63	-9.74	2.6209	-.0145	-.2715	.0791	.0628	.0191

RUN 283   Q= 92.60 PSF   RN/FT= 2.179   MACH=0.20

ALPHA	BETA	c_N	c_A	c_m	c_Y	c_n	c_l
70.61	-9.72	2.6217	-.0088	-.2207	.0646	.0607	.0175
70.60	-7.80	2.6374	-.0095	-.2021	.0490	.0476	.0141
70.59	-3.82	2.6608	-.0106	-.1754	.0223	.0207	.0069
70.61	.16	2.6723	-.0107	-.1629	-.0056	.0001	.0004
70.60	4.17	2.6682	-.0079	-.1757	-.0318	-.0227	-.0067
70.59	8.12	2.6543	-.0054	-.1945	-.0554	-.0445	-.0137
70.59	10.10	2.6447	-.0047	-.2076	-.0838	-.0552	-.0168
70.58	15.08	2.6014	-.0011	-.2407	-.1215	-.0798	-.0270
70.55	20.06	2.5512	.0014	-.3002	-.1295	-.0855	-.0360
70.51	29.98	2.4531	.0038	-.3540	-.1569	-.0883	-.0560

RUN 284   Q= 93.20 PSF   RN/FT= 2.178   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
65.77	29.99	2.4811	.0048	-.2485	-.1582	-.0772	-.0575
65.79	20.09	2.5509	.0045	-.2070	-.1107	-.0701	-.0360
65.81	15.11	2.6070	0.0000	-.1604	-.1024	-.0743	-.0253
65.82	10.12	2.6471	-.0028	-.1262	-.0765	-.0530	-.0153
65.81	8.16	2.6431	-.0034	-.1222	-.0553	-.0416	-.0122
65.83	4.15	2.6544	-.0061	-.1030	-.0284	-.0192	-.0046
65.84	.20	2.6827	-.0069	-.1111	.0011	.0002	.0015
65.89	-3.80	2.6737	-.0068	-.1214	.0222	.0219	.0072
65.90	-7.75	2.6648	-.0068	-.1334	.0495	.0461	.0133
65.91	-9.78	2.6309	-.0058	-.1425	.0673	.0574	.0164

RUN 285   Q= 93.50 PSF   RN/FT= 2.172   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
60.97	-9.79	2.6383	0.0000	-.1056	.0433	.0589	.0145
60.96	-7.79	2.6469	.0002	-.1001	.0335	.0499	.0114
60.96	-3.81	2.6775	-.0008	-.0819	.0100	.0223	.0066
60.95	.18	2.6905	-.0019	-.0585	.0049	.0003	.0011
60.95	4.15	2.6558	.0001	-.0651	-.0181	-.0182	-.0052
60.95	8.11	2.6720	.0026	-.0805	-.0459	-.0429	-.0106
60.95	10.12	2.6565	.0041	-.0904	-.0678	-.0560	-.0142
60.93	15.12	2.6347	.0073	-.1206	-.0904	-.0600	-.0239
60.89	20.06	2.5586	.0094	-.1399	-.0975	-.0461	-.0335
60.89	29.98	2.4831	.0088	-.1751	-.1605	-.0696	-.0589

RUN 286   Q= 57.60 PSF   RN/FT= 1.390   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
41.30	.21	2.8749	.0233	.1076	.0138	.0035	.0015
51.08	.21	2.7674	.0093	.1120	.0076	.0001	-.0010
60.74	.19	2.6644	.0004	-.0546	.0048	.0003	.0006
65.58	.20	2.6559	-.0042	-.1049	.0022	.0010	.0012
70.33	.21	2.6504	-.0088	-.1544	.0001	.0035	.0007
75.24	.21	2.6083	-.0129	-.2078	.0039	.0090	.0008
80.22	.21	2.5682	-.0160	-.2697	.0049	.0111	.0012
85.42	.18	2.5525	-.0181	-.3337	.0057	.0037	-.0010
90.72	.21	2.5140	-.0234	-.3443	.0230	.0208	.0011

RUN 287   Q= 24.40 PSF   RN/FT= .590   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
40.66	.20	2.8543	.0224	.1493	.0386	.0098	.0020
50.76	.20	2.8898	0.0000	.2108	.0208	.0073	.0059
60.50	.19	2.7634	-.0228	.2145	.0356	.0468	-.0025
70.13	.20	2.7327	-.0272	.0540	-.0686	-.0448	.0020
79.99	.20	2.6871	-.0266	-.0285	-.0094	.0002	.0011
90.48	.20	2.5697	-.0269	-.1810	-.0143	.0023	.0011

RUN 288   Q= 24.80 PSF   RN/FT= .593   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
90.50	-9.71	2.5664	-.0235	-.2034	-.0333	.0050	.0277
90.50	-7.77	2.5556	-.0250	-.2030	-.0246	.0030	.0217
90.48	-3.82	2.5495	-.0249	-.1963	-.0155	.0041	.0115
90.47	.17	2.5487	-.0266	-.1921	-.0160	.0016	.0006
90.46	4.13	2.5489	-.0250	-.2067	-.0016	-.0018	-.0100
90.45	8.11	2.5440	-.0222	-.1994	.0024	.0002	-.0222
90.47	10.10	2.5363	-.0203	-.2173	.0022	-.0023	-.0289
90.46	15.04	2.5110	-.0178	-.2188	-.0243	-.0136	-.0383
90.45	20.02	2.4682	-.0124	-.2319	-.0911	-.0394	-.0486
90.47	29.93	2.3324	-.0005	-.2460	-.1366	-.0596	-.0680

RUN 289   Q= 25.20 PSF   RN/FT= .597   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
85.12	29.92	2.3696	-.0057	-.1689	-.1350	-.0692	-.0637
85.15	20.03	2.5006	-.0118	-.1564	-.0554	-.0361	-.0468
85.16	15.06	2.5390	-.0169	-.1378	-.0032	-.0095	-.0361
85.16	10.11	2.5899	-.0198	-.1422	.0269	.0031	-.0255
85.17	8.13	2.5907	-.0210	-.1449	.0233	.0047	-.0203
85.16	4.13	2.5976	-.0235	-.1295	-.0025	-.0014	-.0087
85.18	.16	2.6052	-.0262	-.1187	-.0087	-.0006	.0001
85.19	-3.79	2.6011	-.0257	-.1362	-.0201	.0045	.0112
85.17	-7.77	2.6046	-.0244	-.1505	-.0343	-.0062	.0205
85.17	-9.76	2.5872	-.0237	-.1521	-.0442	.0019	.0261

RUN 290   Q= 25.10 PSF   RN/FT= .596   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
80.00	-9.76	2.6297	-.0255	-.0707	-.0464	-.0086	.0238
80.00	-7.78	2.6072	-.0241	-.0715	-.0569	-.0174	.0180
80.00	-3.80	2.6407	-.0238	-.0699	-.0583	-.0140	.0104
79.99	.17	2.6584	-.0267	-.0264	-.0161	.0000	.0003
79.99	4.13	2.6400	-.0232	-.0667	.0248	.0117	-.0096
79.97	8.10	2.6352	-.0226	-.0773	.0379	.0160	-.0184
79.97	10.12	2.6297	-.0207	-.0665	.0324	.0157	-.0239
79.96	15.03	2.5967	-.0190	-.0578	.0033	-.0025	-.0334
79.95	20.06	2.5595	-.0145	-.0655	-.0287	-.0265	-.0430
79.93	29.92	2.4436	-.0081	-.1128	-.1424	-.0806	-.0600

RUN 291   Q= 25.30 PSF   RN/FT= .599   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
74.99	29.91	2.4784	-.0098	-.0497	-.1673	-.0940	-.0566
75.00	20.02	2.5765	-.0163	.0034	-.0348	-.0401	-.0396
75.02	15.03	2.6190	-.0225	.0201	-.0185	-.0223	-.0293
75.02	10.09	2.6578	-.0250	.0165	.0210	.0056	-.0204
75.03	8.14	2.6722	-.0250	.0160	.0423	.0111	-.0169
75.04	4.13	2.6867	-.0284	.0306	.0143	.0079	-.0080
75.05	.16	2.6976	-.0338	.0719	-.0285	-.0200	.0017
75.06	-3.78	2.6970	-.0297	.0428	-.0606	-.0318	.0099
75.07	-7.75	2.6797	-.0287	.0475	-.0566	-.0233	.0187
75.08	-9.75	2.6738	-.0295	.0547	-.0518	-.0148	.0220

RUN 292   Q= 25.10 PSF   RN/FT= .597   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
70.12	-9.74	2.6969	-.0289	.1273	-.0375	-.0128	.0193
70.13	-7.75	2.7029	-.0284	.1201	-.0521	-.0199	.0166
70.11	-3.76	2.7015	-.0274	.0641	-.0851	-.0437	.0104
70.10	.20	2.6946	-.0274	.0437	-.0853	-.0469	.0029
70.09	4.10	2.7133	-.0283	.0753	-.0228	-.0128	-.0059
70.08	8.12	2.6780	-.0265	.0621	-.0211	-.0171	-.0128
70.08	10.07	2.6842	-.0263	.0639	-.0372	-.0255	-.0165
70.08	15.05	2.6573	-.0217	.0651	-.0698	-.0546	-.0273
70.07	20.04	2.6281	-.0184	.0499	-.1263	-.0837	-.0366
70.03	29.93	2.5271	-.0099	.0380	-.1810	-.1009	-.0574

RUN 293   Q= 25.40 PSF   RN/FT= .602   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
65.28	29.94	2.5597	-.0130	.1748	-.1765	-.0866	-.0569
65.32	20.01	2.6575	-.0234	.1823	-.1315	-.0835	-.0361
65.31	15.09	2.6756	-.0179	.0701	-.1226	-.0918	-.0249
65.30	10.09	2.7002	-.0201	.0634	-.0735	-.0583	-.0148
65.31	8.10	2.6989	-.0212	.0661	-.0529	-.0443	-.0112
65.31	4.15	2.7139	-.0213	.0609	-.0361	-.0363	-.0045
65.33	.17	2.7195	-.0240	.0925	-.0619	-.0375	.0007
65.35	-3.76	2.7194	-.0250	.1223	-.0650	-.0458	.0094
65.36	-7.74	2.7387	-.0262	.1850	-.0451	-.0324	.0161
65.37	-9.73	2.7189	-.0249	.1845	-.0285	-.0179	.0187

RUN 294   Q= 25.10 PSF   RN/FT= .600   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
60.47	-9.73	2.7493	-.0241	.3066	-.0408	-.0270	.0188
60.48	-7.74	2.7750	-.0267	.3033	-.0676	-.0493	.0175
60.48	-3.79	2.7999	-.0291	.2385	-.1020	-.0761	.0089
60.45	.18	2.7578	-.0200	.1426	.0263	.0491	-.0040
60.42	4.14	2.7136	-.0140	.0502	-.0342	-.0342	-.0046
60.41	8.12	2.6818	-.0126	.0438	-.0707	-.0580	-.0112
60.41	10.14	2.7083	-.0115	.0453	-.1006	-.0806	-.0150
60.41	15.07	2.6630	-.0142	.1154	-.1358	-.0915	-.0249
60.41	20.06	2.6319	-.0132	.1387	-.1804	-.0959	-.0352
60.39	29.93	2.5674	-.0079	.1936	-.2030	-.0946	-.0658

RUN 295   Q= 25.20 PSF   RN/FT= .602   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
50.79	29.94	2.7743	.0065	.2800	-.0502	-.0389	-.1153
50.82	20.07	2.8690	.0053	.3161	.0186	-.0447	-.0606
50.82	15.07	2.8670	.0073	.1511	.0065	-.0816	-.0358
50.83	10.11	2.8950	-.0023	.2778	.0263	-.0463	-.0292
50.84	8.10	2.8973	-.0080	.3388	.0027	.0016	-.0268
50.85	4.14	2.9314	-.0207	.3610	.1095	.0548	.0016
50.83	.19	2.8282	-.0015	.2011	.0170	.0077	.0048
50.86	-3.76	2.8715	-.0119	.3108	-.0795	-.0278	-.0084
50.91	-7.75	2.9476	-.0266	.5001	-.1118	-.0535	.0129
50.91	-9.73	2.9227	-.0294	.5492	-.1033	-.0600	.0229

RUN 296   Q= 25.80 PSF   RN/FT= .609   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
40.71	-9.73	2.9195	.0043	.3287	-.1320	.0086	.0187
40.70	-7.73	2.8680	.0092	.2807	-.0964	.0110	.0269
40.66	-3.78	2.7841	.0205	.1836	-.0838	.0011	.0142
40.64	.17	2.7981	.0200	.1404	.0306	.0100	.0009
40.63	4.12	2.7802	.0211	.2057	.1287	.0155	-.0193
40.64	8.13	2.8572	.0131	.3100	.1417	.0129	-.0305
40.62	10.11	2.7754	.0213	.1912	-.0034	-.0296	-.0253
40.61	15.07	2.7252	.0230	.1698	.0114	-.0483	-.0398
40.61	20.01	2.7323	.0191	.2212	.0241	-.0503	-.0558
40.58	29.95	2.7120	.0281	.0428	-.1312	-.0552	-.0954

RUN 299   Q=165.40 PSF   RN/FT= 3.613   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
-42.01	-.15	-2.8204	.1090	-.1700	-.0372	-.0126	-.0065
-51.88	-.16	-2.6647	.1055	-.0474	-.0399	-.0069	-.0028
-61.51	-.16	-2.6285	.1012	.1245	-.0383	-.0061	.0005
-71.19	-.16	-2.6224	.0937	.2787	-.0372	-.0055	.0007
-81.01	-.15	-2.5831	.0792	.3246	-.0413	-.0066	.0008
-91.47	-.17	-2.5469	.0668	.4173	-.0330	-.0019	-.0002

RUN 300   Q=165.80 PSF   RN/FT= 3.601   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
-81.02	9.80	-2.5365	.0825	.3698	-.3550	-.0350	.0184
-81.02	7.80	-2.5560	.0802	.3461	-.2827	-.0304	.0138
-81.01	3.79	-2.5822	.0807	.3332	-.1541	-.0223	.0084
-81.00	-.19	-2.5851	.0772	.3176	-.0288	-.0053	.0012
-80.99	-4.16	-2.5810	.0793	.3256	.0822	.0094	-.0085
-81.00	-8.19	-2.5721	.0813	.3369	.2108	.0154	-.0133
-80.98	-10.17	-2.5386	.0809	.3425	.2735	.0180	-.0174
-80.96	-15.09	-2.4705	.0813	.3749	.4371	.0160	-.0230
-80.93	-20.04	-2.3612	.0820	.3412	.5681	-.0016	-.0281
-80.82	-30.06	-2.0678	.0759	.1672	.8037	-.0732	-.0426

RUN 301   Q=159.80 PSF   RN/FT= 3.525   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
-61.36	-30.19	-2.0228	.0793	.0468	.7884	-.0164	-.0459
-61.44	-20.17	-2.3402	.0934	.1473	.5683	-.0028	-.0220
-61.42	-15.17	-2.4282	.0963	.1746	.4430	.0131	-.0171
-61.47	-10.12	-2.5414	.0988	.1494	.2844	.0105	-.0108
-61.49	-8.21	-2.5680	.0983	.1346	.2245	.0106	-.0089
-61.51	-4.19	-2.6096	.0982	.1266	.0894	.0060	-.0036
-61.51	-.16	-2.6329	.0986	.1315	-.0417	-.0051	.0008
-61.51	3.85	-2.6112	.0993	.1277	-.1742	-.0181	.0053
-61.53	7.89	-2.5741	.0999	.1406	-.3055	-.0204	.0097
-61.53	9.88	-2.5301	.0993	.1470	-.3641	-.0190	.0112

RUN 302   Q=141.80 PSF   RN/FT= 3.311   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
-41.66	9.86	-2.6400	.1106	-.1878	-.3042	.0229	.0276
-41.70	7.74	-2.6871	.1113	-.1938	-.2542	.0159	.0218
-41.74	3.80	-2.7830	.1111	-.1786	-.1391	.0062	.0093
-41.73	-.09	-2.7905	.1126	-.1581	-.0395	-.0166	-.0092
-41.67	-4.13	-2.7186	.1112	-.1657	.0713	-.0240	-.0158
-41.64	-8.17	-2.6759	.1077	-.1742	.1644	-.0322	-.0247
-41.63	-10.20	-2.6465	.1053	-.1715	.2097	-.0364	-.0277
-41.61	-15.14	-2.5807	.0990	-.1982	.3361	-.0340	-.0321
-41.61	-20.19	-2.5725	.0933	-.2358	.4426	-.0212	-.0242
-41.41	-30.12	-2.1956	.0786	-.2242	.6238	-.0241	-.0601

RUN 303   Q=140.70 PSF   RN/FT= 3.282   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
-41.41	-.20	-2.4298	.0224	.0922	-.0086	-.0094	.0081
-51.67	-.18	-2.5463	.0049	.1420	-.0406	-.0062	-.0029
-61.34	-.20	-2.5728	-.0029	.1872	-.0322	-.0041	.0009
-71.05	-.19	-2.5752	-.0206	.2565	-.0321	-.0038	.0004
-80.90	-.19	-2.5161	-.0445	.3845	-.0338	-.0039	.0002
-91.33	-.19	-2.4443	-.0640	.4900	-.0331	-.0026	.0007

RUN 304   Q=158.10 PSF   RN/FT= 3.471   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
-80.93	9.76	-2.4433	-.0363	.4201	-.3604	-.0402	.0146
-80.93	7.74	-2.4840	-.0409	.4070	-.2929	-.0373	.0125
-80.93	3.76	-2.4993	-.0425	.3913	-.1579	-.0230	.0062
-80.93	-.17	-2.5203	-.0456	.3832	-.0362	-.0045	-.0004
-80.92	-4.20	-2.5181	-.0442	.3876	.0895	.0112	-.0074
-80.92	-8.19	-2.4870	-.0412	.3951	.2170	.0223	-.0117
-80.90	-10.09	-2.4608	-.0385	.4026	.2826	.0250	-.0158
-80.87	-15.13	-2.3722	-.0314	.4225	.4311	.0238	-.0208
-80.85	-20.09	-2.2733	-.0195	.3841	.5483	.0020	-.0258
-80.79	-29.96	-2.0229	-.0059	.2100	.7872	-.0703	-.0393

RUN 305   Q=149.70 PSF   RN/FT= 3.379   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
-61.23	-30.10	-2.0067	.0036	.1400	.7851	-.0094	-.0422
-61.30	-20.17	-2.2850	.0007	.1931	.5688	-.0032	-.0179
-61.35	-15.14	-2.4105	-.0052	.2014	.4515	.0151	-.0117
-61.40	-10.18	-2.4916	-.0054	.1844	.2819	.0130	-.0064
-61.41	-8.18	-2.5376	-.0054	.1821	.2209	.0141	-.0049
-61.43	-4.18	-2.5887	-.0041	.1852	.0915	.0092	-.0020
-61.47	-.15	-2.5814	-.0038	.1894	-.0395	-.0038	.0007
-61.48	3.84	-2.5710	-.0036	.1822	-.1753	-.0181	.0035
-61.49	9.85	-2.5010	-.0049	.1800	-.3668	-.0192	.0079
-61.44	7.81	-2.5212	-.0040	.1808	-.3011	-.0226	.0054

210

RUN 306   Q=149.40 PSF   RN/FT= 3.380   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
-41.52	9.81	-2.3794	.0150	.0642	-.3070	.0231	.0227
-41.48	7.80	-2.4045	.0198	.0534	-.2434	.0096	.0153
-41.47	3.82	-2.4186	.0223	.0798	-.1168	.0003	.0122
-41.46	-.14	-2.4306	.0228	.0932	-.0027	-.0088	.0076
-41.45	-4.15	-2.4017	.0193	.0640	.0783	-.0149	-.0082
-41.45	-8.12	-2.4102	.0136	.0494	.1810	-.0255	-.0178
-41.43	-10.14	-2.3942	.0017	.0513	.2302	-.0295	-.0284
-41.38	-15.16	-2.3030	.0054	.0705	.3772	-.0293	-.0368
-41.34	-20.17	-2.1838	.0036	.0131	.4958	-.0314	-.0366
-41.24	-30.11	-1.9779	-.0055	-.0168	.6571	-.0215	-.0934

RUN 307   Q=212.40 PSF   RN/FT= 4.986   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
-42.02	-.19	-2.4833	.0105	.0948	-.0051	-.0012	.0011
-52.23	-.18	-2.5713	.0044	.1310	-.0106	.0026	.0005
-61.95	-.18	-2.5943	-.0038	.1722	-.0140	.0006	.0003
-66.81	-.18	-2.5827	-.0123	.2001	-.0200	-.0019	-.0003
-71.66	-.18	-2.5561	-.0216	.2537	-.0171	-.0015	.0001
-76.50	-.16	-2.5378	-.0331	.3162	-.0169	-.0044	.0005
-81.43	-.16	-2.5338	-.0440	.3738	-.0214	-.0046	.0002
-86.57	-.16	-2.4634	-.0559	.4140	-.0189	-.0052	.0012
-91.84	-.17	-2.4494	-.0626	.4448	-.0123	.0012	.0016

APPENDIX - Continued

RUN 308   Q=228.90 PSF   RN/FT= 5.142   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
-81.48	9.79	-2.4659	-.0353	.3582	-.3161	-.0137	.0142
-81.47	7.78	-2.4941	-.0397	.3567	-.2594	-.0213	.0120
-81.45	3.79	-2.5085	-.0425	.3812	-.1400	-.0185	.0074
-81.43	-.21	-2.5261	-.0460	.3685	-.0157	-.0047	.0004
-81.42	-4.14	-2.5127	-.0448	.3712	.1019	.0108	-.0066
-81.38	-8.18	-2.4822	-.0388	.3675	.2164	.0142	-.0138
-81.37	-10.19	-2.4748	-.0367	.3755	.2777	.0132	-.0160
-81.35	-15.07	-2.3910	-.0295	.3923	.4345	.0131	-.0207
-81.31	-20.09	-2.2968	-.0166	.3243	.5347	-.0160	-.0274
-81.24	-30.01	-2.0104	-.0068	.1880	.7963	-.0733	-.0405

RUN 309   Q=216.10 PSF   RN/FT= 4.984   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
-61.78	-30.21	-2.0403	-.0003	.0113	.7978	-.0220	-.0420
-61.83	-20.23	-2.2984	-.0005	.1613	.6025	.0026	-.0189
-61.90	-15.20	-2.4230	-.0033	.1678	.4386	.0009	-.0120
-61.96	-10.22	-2.5051	-.0055	.1762	.3052	.0216	-.0071
-61.99	-8.23	-2.5327	-.0046	.1769	.2480	.0198	-.0047
-61.99	-4.18	-2.5640	-.0047	.1762	.1100	.0106	-.0022
-62.00	-.18	-2.5778	-.0048	.1759	-.0211	.0006	.0008
-62.03	3.80	-2.5901	-.0046	.1641	-.1578	-.0142	.0031
-61.96	7.89	-2.5325	-.0046	.1566	-.3011	-.0235	.0058
-61.94	9.85	-2.5010	-.0040	.1596	-.3661	-.0259	.0080

212

RUN 310   Q=206.70 PSF   RN/FT= 4.857   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
-42.05	9.84	-2.4905	.0204	-.0181	-.2887	.0017	.0293
-42.01	7.85	-2.4592	.0200	.0101	-.2170	.0080	.0238
-41.95	3.81	-2.4366	.0208	.0512	-.1118	-.0017	.0124
-41.98	-.20	-2.4964	.0116	.0993	-.0010	-.0016	.0028
-41.97	-4.23	-2.4615	.0183	.0556	.0954	-.0044	-.0136
-42.01	-8.25	-2.4856	.0122	.0394	.1856	-.0096	-.0259
-42.04	-10.23	-2.4685	.0094	.0405	.2422	-.0138	-.0296
-42.03	-15.24	-2.3820	.0014	.0255	.3963	-.0176	-.0422
-42.00	-20.26	-2.2872	.0016	-.0488	.5062	-.0301	-.0415
-41.91	-30.33	-2.0163	-.0049	-.0668	.7248	.0023	-.0873

RUN 311   Q=218.00 PSF   RN/FT= 4.973   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
-42.58	-.16	-2.8939	.1059	-.1916	-.0205	-.0060	-.0033
-52.40	-.15	-2.7085	.1038	-.0525	-.0290	-.0042	-.0031
-62.06	-.16	-2.6381	.1009	.1134	-.0290	-.0039	.0012
-66.83	-.16	-2.6317	.0969	.1959	-.0270	-.0024	.0011
-71.66	-.15	-2.6202	.0946	.2735	-.0230	-.0027	.0005
-76.59	-.14	-2.5858	.0876	.2941	-.0229	-.0033	.0016
-81.55	-.15	-2.5933	.0773	.3050	-.0220	-.0037	.0008
-86.63	-.16	-2.5472	.0681	.3324	-.0266	-.0023	.0013
-91.96	-.16	-2.5487	.0634	.3297	-.0165	.0016	.0006

RUN 312   Q=229.80 PSF   RN/FT= 5.101   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
-81.57	9.73	-2.5482	.0842	.3215	-.3371	-.0223	.0179
-81.56	7.83	-2.5633	.0833	.3255	-.2766	-.0227	.0137
-81.52	3.79	-2.5772	.0781	.3104	-.1501	-.0189	.0083
-81.52	-.22	-2.5768	.0765	.3020	-.0186	-.0038	.0006
-81.46	-4.13	-2.5671	.0774	.3091	.1022	.0102	-.0072
-81.38	-8.15	-2.5705	.0797	.3062	.2184	.0112	-.0149
-81.36	-10.18	-2.5381	.0810	.3290	.2824	.0121	-.0172
-81.34	-15.11	-2.4702	.0808	.3474	.4500	.0137	-.0238
-81.33	-20.12	-2.3768	.0834	.3149	.5695	-.0082	-.0288
-81.22	-30.01	-2.0731	.0762	.1505	.8108	-.0746	-.0430

RUN 313   Q = 211.50 PSF   RN/FT = 4.899   MACH = 0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
-61.81	-30.19	-2.0515	.0766	-.0332	.8064	-.0190	-.0460
-61.86	-20.23	-2.3516	.0927	.1249	.6024	.0042	-.0231
-61.92	-15.26	-2.4456	.0948	.1480	.4453	.0077	-.0164
-61.91	-10.20	-2.5637	.0974	.1384	.3042	.0164	-.0107
-61.94	- 8.22	-2.5683	.0973	.1249	.2390	.0171	-.0090
-61.98	- 4.15	-2.6255	.0979	.1165	.1045	.0087	-.0036
-62.00	-.14	-2.6297	.0989	.1165	-.0259	-.0024	.0008
-61.99	3.87	-2.6303	.1003	.1126	-.1673	-.0168	.0052
-61.98	7.90	-2.5660	.1003	.1228	-.3055	-.0263	.0107
-61.98	9.90	-2.5477	.1000	.1270	-.3736	-.0277	.0122

RUN 314   Q=212.70 PSF   RN/FT= 4.910   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
-42.41	9.89	-2.7555	.1068	-.2754	-.3156	-.0006	.0192
-42.41	7.86	-2.7910	.1067	-.2352	-.2482	.0032	.0135
-42.41	3.83	-2.8245	.1075	-.2146	-.1518	.0049	.0125
-42.43	-.19	-2.8848	.1044	-.1898	-.0187	-.0061	-.0032
-42.35	-4.14	-2.7934	.1053	-.2001	.0995	-.0150	-.0141
-42.36	-8.20	-2.7793	.1027	-.2072	.2022	-.0195	-.0206
-42.35	-10.24	-2.7052	.1014	-.2018	.2484	-.0266	-.0271
-42.33	-15.23	-2.6291	.0956	-.2316	.3682	-.0257	-.0328
-42.38	-20.30	-2.6150	.0908	-.3031	.4773	-.0190	-.0155
-42.07	-30.28	-2.1916	.0755	-.2576	.6975	-.0051	-.0669

RUN 315   Q= 57.40 PSF   RN/FT= 1.386   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
-41.01	-.25	-2.7440	.1098	-.1466	-.0249	-.0074	-.0056
-51.03	-.23	-2.6135	.1054	-.0576	-.0326	-.0058	-.0026
-60.67	-.22	-2.5957	.1042	.1117	-.0318	-.0016	.0009
-70.32	-.22	-2.5661	.0975	.2465	-.0231	.0014	.0007
-80.27	-.22	-2.5500	.0866	.3161	-.0248	.0001	0.0000
-90.72	-.22	-2.4744	.0726	.4089	-.0289	.0034	.0008

RUN 316   Q= 55.20 PSF   RN/FT= 1.353   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
-80.18	9.71	-2.4884	.0875	.3326	-.3430	-.0247	.0160
-80.17	7.77	-2.4852	.0876	.3280	-.2759	-.0232	.0138
-80.17	3.78	-2.5336	.0883	.3079	-.1400	-.0088	.0077
-80.18	-.22	-2.5422	.0856	.3065	-.0219	-.0005	.0009
-80.17	-4.17	-2.5491	.0873	.3158	.0973	.0142	-.0070
-80.16	-8.11	-2.5004	.0901	.3193	.2305	.0311	-.0146
-80.19	-10.09	-2.5369	.0992	.1575	.1704	-.0515	-.0144
-80.19	-15.00	-2.4972	.1032	.1683	.3237	-.0574	-.0208
-80.19	-20.04	-2.3792	.1049	.1258	.4806	-.0478	-.0268
-80.15	-29.89	-2.0788	.1011	.0648	.7879	-.0535	-.0402

RUN 317   Q= 56.90 PSF   RN/FT= 1.369   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
-60.63	-29.93	-2.0837	.0918	-.2394	.7433	-.0379	-.0399
-60.67	-20.09	-2.3677	.1007	-.0903	.5247	-.0166	-.0205
-60.70	-15.07	-2.4643	.1005	-.0233	.4147	-.0015	-.0151
-60.70	-10.13	-2.5278	.1015	.0976	.2779	.0188	-.0109
-60.62	-8.18	-2.5540	.1012	.1080	.2267	.0197	-.0080
-60.65	-4.12	-2.5949	.1021	.1162	.0924	.0098	-.0031
-60.66	-.15	-2.6218	.1030	.1147	-.0349	-.0009	.0011
-60.68	3.77	-2.6008	.1029	.1161	-.1643	-.0134	.0049
-60.68	7.79	-2.5429	.1012	.1070	-.2989	-.0214	.0092
-60.68	9.79	-2.5320	.1003	.1087	-.3682	-.0263	.0110

RUN 318   Q= 57.60 PSF   RN/FT= 1.374   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
-40.92	9.80	-2.6424	.1059	-.2248	-.2984	-.0029	.0192
-40.93	7.79	-2.6659	.1062	-.2056	-.2472	-.0029	.0127
-40.92	3.75	-2.7185	.1081	-.1710	-.1399	-.0056	.0060
-40.92	-.16	-2.7459	.1072	-.1494	-.0272	-.0066	-.0037
-40.90	-4.23	-2.7063	.1076	-.1720	.0955	-.0061	-.0132
-40.89	-8.17	-2.6868	.1057	-.2163	.2048	-.0040	-.0209
-40.88	-10.15	-2.6537	.1041	-.2308	.2496	-.0027	-.0236
-40.95	-15.13	-2.6501	.1022	-.2648	.3746	.0251	-.0340
-40.91	-20.10	-2.5338	.0959	-.2597	.4191	-.0150	-.0360
-40.86	-30.02	-2.3229	.0816	-.3550	.5984	-.0352	-.0410

RUN 319   Q= 59.00 PSF   RN/FT= 1.387   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
-40.86	-.18	-2.4205	.0128	.0937	-.0187	-.0051	.0042
-50.94	-.17	-2.5311	.0087	.1295	-.0350	-.0033	-.0035
-60.69	-.16	-2.5540	-.0017	.1587	-.0293	-.0018	.0007
-70.35	-.17	-2.5574	-.0180	.2292	-.0319	-.0016	-.0001
-80.27	-.16	-2.4876	-.0369	.3667	-.0278	-.0027	.0003
-90.72	-.18	-2.3973	-.0543	.4763	-.0319	-.0011	.0006

RUN 320   Q= 60.70 PSF   RN/FT= 1.406   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
-80.24	9.71	-2.4258	-.0298	.3714	-.3496	-.0322	.0151
-80.23	7.77	-2.4381	-.0324	.3634	-.2807	-.0283	.0114
-80.23	3.75	-2.4754	-.0357	.3614	-.1433	-.0167	.0082
-80.22	-.26	-2.4783	-.0382	.3605	-.0234	-.0022	.0003
-80.21	-4.13	-2.4568	-.0363	.3563	.0881	.0119	-.0055
-80.19	-8.13	-2.4383	-.0309	.3751	.2190	.0237	-.0117
-80.19	-10.11	-2.4158	-.0305	.3794	.2903	.0278	-.0142
-80.19	-15.08	-2.4077	-.0133	.1946	.3106	-.0620	-.0173
-80.17	-20.03	-2.3186	.0028	.1704	.4615	-.0525	-.0238
-80.18	-29.97	-2.0062	.0191	.1153	.7760	-.0568	-.0388

RUN 321   Q= 59.40 PSF   RN/FT= 1.390   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
-60.66	-30.02	-2.0833	.0113	-.1941	.7409	-.0327	-.0370
-60.70	-20.07	-2.3230	.0014	.0454	.6099	.0378	-.0164
-60.70	-15.10	-2.3917	-.0001	.1051	.4554	.0295	-.0105
-60.72	-10.16	-2.4671	-.0021	.1341	.2887	.0236	-.0060
-60.72	-8.15	-2.5150	-.0023	.1394	.2225	.0215	-.0035
-60.74	-4.11	-2.5437	-.0024	.1530	.0873	.0117	-.0011
-60.76	-.15	-2.5404	-.0017	.1575	-.0326	-.0002	.0004
-60.77	3.76	-2.5380	-.0023	.1531	-.1594	-.0146	.0026
-60.78	7.82	-2.5104	-.0025	.1435	-.2918	-.0233	.0050
-60.72	9.79	-2.4925	-.0034	.1425	-.3522	-.0275	.0065

RUN 322   Q= 56.50 PSF   RN/FT= 1.355   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
-40.86	9.78	-2.3796	.0163	.0135	-.2858	-.0029	.0212
-40.85	7.80	-2.3895	.0173	.0339	-.2293	-.0041	.0164
-40.83	3.77	-2.4091	.0174	.0670	-.1072	-.0093	.0102
-40.83	-.21	-2.4079	.0105	.0977	-.0046	-.0053	.0023
-40.82	-4.21	-2.3877	.0156	.0559	.0864	.0009	-.0067
-40.82	-8.13	-2.3980	.0161	.0129	.2106	.0020	-.0126
-40.83	-10.18	-2.4260	.0157	-.0062	.2630	.0008	-.0189
-40.84	-15.13	-2.4398	.0168	-.0350	.3786	.0195	-.0404
-40.83	-20.06	-2.1922	.0134	-.0318	.4802	-.0273	-.0500
-40.78	-30.03	-2.0370	.0078	-.1315	.5962	-.0335	-.0929

RUN 323   Q= 23.00 PSF   RN/FT=   .573   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
-40.62	-.20	-2.4792	-.0044	.0979	-.0341	-.0010	-.0011
-50.74	-.18	-2.6597	-.0020	.0457	-.0317	-.0019	-.0017
-60.45	-.17	-2.6906	-.0075	-.0302	.0121	.0333	.0001
-65.31	-.17	-2.7334	-.0115	-.0516	-.0139	.0190	-.0005
-70.09	-.17	-2.7091	-.0124	.0038	-.0303	.0039	.0004
-74.99	-.16	-2.6795	-.0151	.1011	-.0285	.0033	.0004
-80.01	-.17	-2.6462	-.0227	.1516	-.0293	.0022	.0001
-85.14	-.17	-2.6011	-.0297	.2201	-.0335	.0029	-.0012
-90.50	-.17	-2.5653	-.0341	.3161	-.0303	.0046	-.0001

RUN 324   Q= 24.00 PSF   RN/FT=   .582   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
-79.96	9.74	-2.5536	-.0071	.1872	-.2739	.0402	.0130
-79.98	7.78	-2.5893	-.0126	.1804	-.2277	.0274	.0117
-79.98	3.72	-2.6300	-.0183	.1670	-.1162	.0092	.0068
-79.97	-.22	-2.6264	-.0219	.1461	-.0195	.0024	.0002
-79.96	-4.19	-2.6267	-.0175	.1623	.0568	-.0015	-.0080
-79.95	-8.15	-2.5844	-.0145	.1817	.1484	-.0221	-.0117
-79.94	-10.15	-2.5504	-.0088	.1895	.1948	-.0340	-.0143
-79.92	-15.06	-2.4748	.0028	.1855	.3401	-.0442	-.0208
-79.90	-20.05	-2.3521	.0137	.1521	.5039	-.0325	-.0281
-79.97	-29.96	-1.9827	.0226	.0061	.8806	-.0491	-.0455

RUN 325   Q= 23.70 PSF   RN/FT= .577   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
-60.39	-29.99	-2.0428	.0012	-.3184	.8605	.0122	-.0413
-60.42	-20.06	-2.3884	.0063	-.1290	.5890	-.0019	-.0179
-60.46	-15.14	-2.4983	.0024	-.0693	.4505	.0139	-.0114
-60.48	-10.08	-2.6077	.0008	-.0339	.2589	.0032	-.0077
-60.49	-8.13	-2.6203	-.0012	-.0215	.1974	.0006	-.0053
-60.50	-4.16	-2.6570	-.0027	-.0336	.1006	.0148	-.0029
-60.46	-.16	-2.6968	-.0088	-.0343	.0145	.0324	-.0002
-60.46	3.79	-2.6565	-.0040	-.0285	-.0524	.0624	.0022
-60.47	7.76	-2.5900	-.0018	-.0761	-.1770	.0666	.0043
-60.48	9.74	-2.6121	.0015	-.0966	-.2426	.0651	.0057

RUN 326   Q= 23.80 PSF   RN/FT= .579   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
-40.63	9.73	-2.4146	.0072	-.1500	-.2168	.0648	.0198
-40.63	7.75	-2.4168	.0079	-.0901	-.1974	.0468	.0185
-40.60	3.75	-2.4119	.0075	.0036	-.1008	.0303	.0082
-40.60	-.22	-2.4444	.0013	.0945	-.0184	-.0012	-.0011
-40.59	-4.13	-2.4119	.0115	.0166	.0653	-.0310	-.0076
-40.59	-8.09	-2.4159	.0114	-.0973	.1206	-.0555	-.0169
-40.58	-10.13	-2.3801	.0071	-.1363	.1712	-.0605	-.0191
-40.59	-15.10	-2.3803	.0151	-.3385	.2256	-.1058	-.0219
-40.58	-20.09	-2.3463	.0099	-.2189	.4965	-.0125	-.0552
-40.54	-29.92	-2.2167	.0334	-.5860	.4868	-.1107	-.0900

RUN 327   Q= 23.10 PSF   RN/FT= .582   MACH=0.20

ALPHA	BETA	c_N	c_A	c_m	c_Y	c_n	c_1
-40.65	-.19	-2.7552	.0997	-.1778	-.0171	.0025	.0031
-50.70	-.16	-2.7020	.0993	-.1630	-.0262	-.0047	.0001
-60.42	-.18	-2.7022	.1035	-.0944	.0113	.0243	.0007
-70.05	-.17	-2.6921	.1066	.0190	-.0136	.0026	.0009
-79.96	-.16	-2.6666	.0988	.1187	-.0247	.0015	.0005
-90.46	-.17	-2.6081	.0854	.2514	-.0277	.0047	-.0007

RUN 328   Q= 24.80 PSF   RN/FT= .601   MACH=0.20

ALPHA	BETA	c_N	c_A	c_m	c_Y	c_n	c_1
-79.98	9.72	-2.5909	.1037	.1461	-.2872	.0353	.0170
-79.99	7.74	-2.6013	.1024	.1425	-.2321	.0269	.0129
-79.99	3.80	-2.6507	.1013	.1311	-.1175	.0067	.0079
-79.98	-.19	-2.6449	.0985	.1308	-.0298	.0019	.0010
-79.97	-4.14	-2.6506	.1005	.1294	.0555	-.0032	-.0065
-79.95	-8.13	-2.6294	.1030	.1515	.1554	-.0236	-.0117
-79.94	-10.13	-2.6099	.1033	.1524	.2006	-.0315	-.0162
-79.93	-15.08	-2.5265	.1038	.1514	.3621	-.0367	-.0218
-79.91	-19.99	-2.4245	.1091	.1390	.5277	-.0254	-.0306
-79.88	-29.90	-2.0817	.0982	-.0466	.8561	-.0565	-.0481

RUN 329   Q= 24.90 PSF   RN/FT= .602   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
-60.35	-29.95	-2.0672	.0879	-.3059	.8282	.0063	-.0463
-60.39	-20.07	-2.4008	.0985	-.1490	.5502	-.0104	-.0223
-60.41	-15.07	-2.5362	.0966	-.1319	.4063	.0028	-.0168
-60.43	-10.08	-2.6306	.0988	-.0830	.2295	-.0090	-.0105
-60.43	-8.09	-2.6500	.0986	-.0745	.1618	-.0102	-.0085
-60.44	-5.14	-2.6853	.0989	-.0713	.0978	-.0051	-.0036
-60.46	-.15	-2.7082	.0996	-.0820	-.0079	.0255	-.0009
-60.48	3.83	-2.6580	.0990	-.0604	-.0797	.0586	.0025
-60.49	7.76	-2.6337	.0989	-.1064	-.1961	.0598	.0068
-60.49	9.78	-2.6004	.0980	-.1359	-.2679	.0555	.0097

RUN 330   Q= 23.10 PSF   RN/FT= .581   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
-40.66	9.77	-2.7564	.0927	-.4526	-.2149	.0574	.0166
-40.64	7.75	-2.7396	.0955	-.3926	-.1735	.0472	.0149
-40.65	3.77	-2.8055	.0983	-.3007	-.0751	.0330	.0089
-40.62	-.15	-2.7730	.1003	-.1768	-.0179	.0019	.0019
-40.61	-4.12	-2.7494	.0982	-.2554	.0340	-.0304	-.0112
-40.61	-8.12	-2.7696	.0931	-.3973	.1004	-.0482	-.0143
-40.60	-10.08	-2.7269	.0925	-.4238	.1540	-.0564	-.0182
-40.63	-15.03	-2.7720	.0865	-.6278	.1997	-.1010	-.0139
-40.49	-20.00	-2.4197	.0974	-.4531	.4611	-.0443	-.0427
-40.56	-29.89	-2.4569	.0778	-.9550	.4512	-.1453	-.0378

RUN 331　　　Q= 13.10 PSF　　　RN/FT= .328　　　MACH=0.20

SEQ	ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
4	-40.57	-.17	-2.8208	.0903	-.2880	-.0166	-.0005	-.0031
5	-50.65	-.15	-2.8878	.0921	-.3963	-.0260	.0214	-.0097
6	-60.33	-.15	-2.7732	.0881	-.3265	-.0219	.0242	-.0012
7	-65.11	-.13	-2.7427	.1019	-.1378	-.0383	.0024	-.0001
8	-69.97	-.14	-2.7086	.1084	.0063	-.0548	.0007	-.0004
9	-74.83	-.13	-2.6860	.1042	.0616	-.0526	.0007	-.0009
10	-79.85	-.13	-2.6880	.0990	.1076	-.0542	.0010	-.0016
11	-85.01	-.14	-2.6779	.0901	.1478	-.0567	.0020	-.0014
12	-90.32	-.12	-2.6644	.0828	.2185	-.0506	.0038	-.0022

RUN 332　　　Q= 15.00 PSF　　　RN/FT= .354　　　MACH=0.20

SEQ	ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
1	-90.35	-.15	-2.5351	-.0293	.2847	-.0437	.0031	.0010
2	-85.04	-.14	-2.5590	-.0266	.1955	-.0406	.0021	.0006
3	-79.88	-.12	-2.5943	-.0164	.1221	-.0414	.0007	.0001
4	-74.88	-.12	-2.6000	-.0065	.0684	-.0427	.0015	-.0006
5	-69.99	-.13	-2.6421	-.0017	-.0238	-.0359	.0015	.0006
6	-65.13	-.12	-2.6519	-.0053	-.1503	-.0312	.0020	.0002
7	-60.38	-.13	-2.7122	-.0233	-.2395	-.0073	.0341	-.0023
8	-50.68	-.14	-2.7297	-.0163	-.1927	-.0051	.0179	-.0026
9	-40.48	-.14	-2.4739	-.0065	-.0089	-.0286	-.0009	.0027

RUN 333   Q= 56.40 PSF   RN/FT= 1.357   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
-40.83	-.15	-2.4064	.0254	.1127	-.0622	.0260	-.0043
-50.96	-.16	-2.5315	.0216	.1403	-.0791	.0275	-.0100
-60.68	-.14	-2.5493	.0131	.1671	-.0785	.0259	-.0075
-65.50	-.13	-2.5812	.0036	.2023	-.0785	.0235	-.0068
-70.34	-.15	-2.5584	-.0048	.2399	-.0687	.0221	-.0068
-75.20	-.15	-2.5252	-.0147	.2859	-.0604	.0166	-.0046
-80.21	-.14	-2.4968	-.0265	.3740	-.0587	.0122	-.0043
-85.33	-.13	-2.4466	-.0382	.4248	-.0550	.0106	-.0027
-90.67	-.12	-2.4135	-.0422	.4974	-.0526	.0116	-.0055

RUN 334   Q= 56.60 PSF   RN/FT= 1.346   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
-80.18	9.72	-2.4073	-.0189	.3775	-.3587	-.0248	.0119
-80.17	7.73	-2.4439	-.0212	.3732	-.2955	-.0166	.0089
-80.16	3.78	-2.4648	-.0229	.3733	-.1685	-.0010	.0021
-80.14	-.19	-2.4917	-.0267	.3708	-.0558	.0120	-.0047
-80.14	-4.14	-2.4760	-.0242	.3738	.0561	.0271	-.0105
-80.13	-8.13	-2.4356	-.0210	.3810	.1849	.0396	-.0176
-80.12	-10.14	-2.4169	-.0197	.3852	.2612	.0457	-.0195
-80.12	-15.08	-2.4141	-.0058	.1797	.2760	-.0428	-.0236
-80.10	-20.03	-2.2982	.0098	.1444	.4374	-.0372	-.0310
-80.05	-29.97	-2.0261	.0235	.1106	.7434	-.0389	-.0452

RUN 335   Q= 55.20 PSF   RN/FT= 1.325   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
-60.62	-30.01	-2.0776	.0177	-.2582	.6983	-.0235	-.0426
-60.65	-20.08	-2.3179	.0062	.0267	.5877	.0621	-.0224
-60.65	-15.14	-2.4072	.0075	.1037	.4373	.0481	-.0159
-60.69	-10.11	-2.4828	.0082	.1363	.2471	.0427	-.0120
-60.69	-8.14	-2.5172	.0117	.1512	.1772	.0452	-.0115
-60.71	-4.15	-2.5431	.0141	.1642	.0457	.0364	-.0094
-60.73	-.19	-2.5357	.0146	.1680	-.0848	.0248	-.0081
-60.75	3.79	-2.5501	.0110	.1634	-.2017	.0106	-.0047
-60.71	7.79	-2.5183	.0102	.1560	-.3318	.0003	-.0023
-60.71	9.78	-2.4759	.0098	.1469	-.3862	-.0086	.0007

RUN 336   Q= 57.50 PSF   RN/FT= 1.345   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
-40.84	9.78	-2.4078	.0320	.0307	-.3354	.0203	.0159
-40.84	7.79	-2.4191	.0323	.0510	-.2905	.0264	.0085
-40.82	3.82	-2.4153	.0322	.0803	-.1654	.0209	.0030
-40.80	-.17	-2.3997	.0269	.1129	-.0626	.0252	-.0053
-40.80	-4.15	-2.4021	.0328	.0783	.0321	.0301	-.0158
-40.80	-8.17	-2.4142	.0315	.0289	.1669	.0262	-.0198
-40.79	-10.13	-2.3963	.0273	.0102	.2216	.0186	-.0243
-40.77	-15.07	-2.3272	.0209	-.0188	.3412	.0085	-.0491
-40.74	-20.06	-2.2251	.0021	-.0756	.4497	-.0108	-.0522
-40.67	-30.00	-2.0166	.0170	-.1416	.5659	-.0123	-.0999

226

RUN 337   Q= 23.70 PSF   RN/FT= .580   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
-40.57	-.19	-2.4338	.0096	.1062	-.0727	.0252	-.0083
-50.72	-.18	-2.5807	.0110	.0664	-.0658	.0249	-.0080
-60.42	-.17	-2.6476	.0025	-.0271	-.0244	.0514	-.0056
-65.26	-.16	-2.6674	.0003	-.0516	-.0453	.0379	-.0056
-70.06	-.16	-2.6831	-.0002	.0048	-.0563	.0245	-.0049
-74.94	-.15	-2.6432	-.0036	.1046	-.0563	.0205	-.0040
-79.95	-.15	-2.6098	-.0129	.1600	-.0521	.0167	-.0046
-85.09	-.16	-2.5841	-.0212	.2217	-.0500	.0144	-.0032
-90.48	-.16	-2.5480	-.0285	.3145	-.0432	.0138	-.0023

RUN 338   Q= 25.10 PSF   RN/FT= .593   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
-79.94	9.75	-2.5161	-.0011	.1848	-.2709	.0484	.0122
-79.95	7.75	-2.5515	-.0040	.1810	-.2310	.0400	.0089
-79.94	3.79	-2.5912	-.0106	.1666	-.1410	.0237	.0020
-79.95	-.17	-2.6068	-.0130	.1567	-.0518	.0177	-.0039
-79.95	-4.14	-2.5834	-.0104	.1673	.0377	.0126	-.0123
-79.93	-8.10	-2.5637	-.0084	.1882	.1262	-.0069	-.0158
-79.93	-10.09	-2.5339	-.0065	.1874	.1753	-.0178	-.0185
-79.92	-15.06	-2.4570	.0034	.1736	.3186	-.0258	-.0256
-79.94	-19.99	-2.3333	.0147	.1420	.4917	-.0179	-.0322
-79.90	-29.94	-1.9576	.0219	.0020	.8523	-.0314	-.0497

RUN 339   Q= 25.50 PSF   RN/FT=   .600   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
-60.37	-29.97	-1.9948	.0049	-.3070	.8447	.0328	-.0445
-60.44	-20.06	-2.3623	.0064	-.1392	.5461	.0175	-.0214
-60.45	-15.09	-2.4951	.0078	-.0602	.4204	.0336	-.0165
-60.46	-10.11	-2.5941	.0061	-.0247	.2345	.0216	-.0124
-60.46	-8.12	-2.6297	.0067	-.0132	.1601	.0227	-.0116
-60.46	-4.14	-2.6723	.0086	-.0211	.0503	.0384	-.0106
-60.46	-.17	-2.6772	.0008	-.0280	-.0345	.0539	-.0059
-60.45	3.78	-2.6394	.0045	-.0147	-.1012	.0867	-.0038
-60.42	7.76	-2.6177	.0070	-.0575	-.2275	.0907	-.0022
-60.43	9.73	-2.5901	.0075	-.0797	-.2836	.0820	.0001

RUN 340   Q= 26.20 PSF   RN/FT=   .611   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
-40.61	9.72	-2.3991	.0171	-.1181	-.2804	.0783	.0162
-40.60	7.75	-2.3842	.0178	-.0681	-.2527	.0723	.0115
-40.58	3.79	-2.3973	.0165	.0136	-.1614	.0609	.0007
-40.58	-.07	-2.4374	.0120	.1119	-.0737	.0253	-.0102
-40.56	-4.13	-2.3764	.0216	.0397	.0270	.0006	-.0122
-40.59	-8.09	-2.3857	.0165	-.0682	.1034	-.0288	-.0218
-40.60	-10.11	-2.3851	.0129	-.1087	.1686	-.0339	-.0253
-40.60	-15.04	-2.3549	.0100	-.2369	.2802	-.0511	-.0357
-40.59	-20.05	-2.3280	.0045	-.1979	.4927	.0132	-.0538
-40.55	-29.94	-2.1681	.0249	-.5266	.5085	-.0695	-.0918

228

RUN 341   Q= 25.00 PSF   RN/FT= .593   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
-40.54	-.19	-2.1688	.0133	-.0106	-.0714	.0046	.0365
-50.70	-.17	-2.3947	.0083	-.0711	-.0796	.0031	.0330
-60.47	-.17	-2.5047	.0010	-.1316	-.0415	.0316	.0363
-70.13	-.16	-2.5282	-.0056	-.0876	-.0721	.0091	.0308
-79.99	-.17	-2.4883	-.0174	.0638	-.0655	.0065	.0256
-90.49	-.16	-2.3947	-.0362	.2199	-.0716	.0097	.0185

RUN 342   Q= 27.40 PSF   RN/FT= .619   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
-80.00	9.72	-2.3583	-.0064	.0668	-.3176	.0540	.0384
-80.01	7.74	-2.4041	-.0083	.0715	-.2700	.0416	.0355
-80.01	3.80	-2.4503	-.0120	.0679	-.1706	.0179	.0308
-80.01	-.17	-2.4749	-.0173	.0564	-.0714	.0074	.0255
-79.99	-4.13	-2.4694	-.0175	.0772	.0224	.0018	.0194
-79.98	-8.13	-2.4545	-.0156	.1158	.1076	-.0232	.0160
-79.97	-10.09	-2.4297	-.0133	.1174	.1634	-.0326	.0152
-79.95	-15.03	-2.3514	-.0096	.1155	.3162	-.0412	.0074
-79.93	-20.05	-2.2492	-.0024	.1157	.4915	-.0302	-.0007
-79.90	-29.95	-1.8882	.0010	-.0262	.8660	-.0438	-.0223

RUN 343   Q= 27.90 PSF   RN/FT= .627   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
-60.38	-29.98	-1.9120	-.0107	-.3360	.8415	.0157	-.0145
-60.42	-20.07	-2.2465	-.0004	-.1741	.5512	.0026	.0176
-60.44	-15.08	-2.3607	.0009	-.1113	.4092	.0191	.0206
-60.45	-10.11	-2.4370	.0009	-.0820	.2243	.0126	.0255
-60.45	-8.11	-2.4696	.0002	-.0786	.1604	.0108	.0280
-60.47	-4.17	-2.5097	.0015	-.0929	.0441	.0223	.0315
-60.48	-.18	-2.4999	.0004	-.1119	-.0522	.0402	.0353
-60.48	3.75	-2.4541	.0038	-.1213	-.1291	.0674	.0382
-60.50	7.74	-2.4439	.0074	-.1744	-.2618	.0703	.0410
-60.50	9.70	-2.4047	.0105	-.1936	-.3305	.0679	.0427

RUN 344   Q= 26.60 PSF   RN/FT= .616   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
-40.56	9.72	-2.1280	.0180	-.2599	-.3505	.0563	.0561
-40.55	7.77	-2.1313	.0192	-.2057	-.3004	.0430	.0527
-40.55	3.83	-2.1686	.0193	-.1022	-.1810	.0340	.0467
-40.54	-.15	-2.2054	.0133	-.0038	-.0806	.0043	.0357
-40.53	-4.13	-2.1990	.0195	-.0604	.0242	-.0210	.0325
-40.55	-8.10	-2.2086	.0122	-.1644	.1101	-.0406	.0207
-40.54	-10.12	-2.1944	.0093	-.1919	.1666	-.0410	.0125
-40.53	-15.03	-2.1533	.0100	-.2993	.2707	-.0673	.0161
-40.51	-20.05	-2.0695	.0174	-.2453	.4826	.0045	-.0118
-40.51	-29.96	-2.0632	.0178	-.5118	.5300	-.0794	-.0374

230

RUN 345   Q= 56.90 PSF   RN/FT= 1.319   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
-40.74	-.21	-2.1475	.0308	-.0181	-.0676	-.0025	.0458
-50.87	-.20	-2.3260	.0252	.0029	-.0775	.0004	.0461
-60.64	-.21	-2.3724	.0171	.0690	-.0744	.0025	.0446
-70.30	-.19	-2.4221	-.0027	.1437	-.0707	.0024	.0391
-80.22	-.21	-2.3703	-.0295	.2711	-.0643	-.0010	.0314
-90.69	-.20	-2.3204	-.0504	.4071	-.0628	.0028	.0229

RUN 346   Q= 61.60 PSF   RN/FT= 1.367   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
-80.18	9.73	-2.2725	-.0191	.2589	-.4042	-.0286	.0451
-80.18	7.75	-2.3100	-.0201	.2574	-.3356	-.0263	.0428
-80.18	3.81	-2.3546	-.0239	.2648	-.1927	-.0133	.0371
-80.17	-.14	-2.3719	-.0291	.2732	-.0625	-.0010	.0322
-80.17	-4.21	-2.3834	-.0317	.2817	.0618	.0149	.0247
-80.16	-8.13	-2.3484	-.0322	.3054	.1978	.0275	.0185
-80.15	-10.14	-2.3225	-.0312	.3163	.2672	.0343	.0155
-80.19	-15.05	-2.3200	-.0219	.1538	.3239	-.0453	.0105
-80.15	-20.04	-2.2261	-.0104	.1482	.4840	-.0364	.0019
-80.08	-29.92	-1.9514	-.0011	.0817	.7906	-.0533	-.0175

RUN 347   Q= 57.00 PSF   RN/FT= 1.314   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
-60.64	-29.95	-1.9967	-.0018	-.3131	.7450	-.0357	-.0138
-60.67	-20.06	-2.1943	-.0014	-.0087	.6069	.0399	.0195
-60.66	-15.07	-2.2556	.0054	.0486	.4414	.0348	.0284
-60.65	-10.13	-2.3392	.0118	.0651	.2611	.0256	.0355
-60.65	-8.12	-2.3588	.0145	.0682	.1883	.0234	.0383
-60.67	-4.12	-2.3763	.0189	.0695	.0484	.0147	.0432
-60.67	-.17	-2.3674	.0208	.0674	-.0822	.0035	.0465
-60.68	3.79	-2.3620	.0189	.0557	-.2162	-.0097	.0479
-60.69	7.79	-2.3269	.0137	.0362	-.3436	-.0192	.0468
-60.70	9.79	-2.3193	.0125	.0306	-.4141	-.0262	.0487

RUN 348   Q= 56.80 PSF   RN/FT= 1.310   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
-40.74	9.78	-2.0997	.0344	-.1150	-.3644	.0019	.0568
-40.74	7.77	-2.1073	.0341	-.0937	-.3093	.0018	.0519
-40.75	3.83	-2.1231	.0357	-.0558	-.1834	-.0048	.0423
-40.74	-.18	-2.1587	.0323	-.0138	-.0616	-.0013	.0473
-40.73	-4.15	-2.1249	.0334	-.0318	.0362	.0070	.0413
-40.73	-8.11	-2.1302	.0370	-.0702	.1513	.0082	.0338
-40.72	-10.17	-2.1148	.0379	-.0778	.2080	.0012	.0256
-40.71	-15.07	-2.1017	.0231	-.1024	.3510	-.0008	.0072
-40.70	-20.08	-1.9818	.0224	-.0867	.4543	-.0222	-.0169
-40.69	-29.90	-1.9084	.0141	-.1253	.5706	-.0259	-.0475

RUN 349   Q= 57.10 PSF   RN/FT= 1.331   MACH=0.20

ALPHA	BETA	CN	CA	CLM	CY	CLN	CLL
-40.79	-.20	-2.3053	-.0099	.0563	-.0051	-.0045	.0010
-50.93	-.16	-2.4408	-.0124	.0865	-.0258	-.0025	-.0062
-60.64	-.16	-2.5052	-.0223	.1256	-.0271	-.0014	-.0010
-65.50	-.16	-2.5178	-.0311	.1543	-.0251	-.0013	-.0010
-70.34	-.16	-2.5190	-.0402	.1949	-.0299	.0005	-.0014
-75.22	-.16	-2.4708	-.0491	.2396	-.0268	.0001	-.0020
-80.23	-.15	-2.4429	-.0599	.3292	-.0265	-.0026	-.0005
-85.32	-.16	-2.4186	-.0681	.3975	-.0255	-.0004	-.0004
-90.68	-.15	-2.3832	-.0739	.4638	-.0229	.0028	.0004

RUN 350   Q= 24.50 PSF   RN/FT= .577   MACH=0.20

ALPHA	BETA	CN	CA	CLM	CY	CLN	CLL
-40.45	-.21	-2.3179	-.0178	.0506	-.0090	-.0016	-.0011
-50.76	-.17	-2.5000	-.0202	-.0010	-.0237	-.0069	-.0028
-60.46	-.17	-2.5994	-.0261	-.0686	.0218	.0281	-.0003
-65.28	-.18	-2.6108	-.0276	-.1006	-.0001	.0129	-.0006
-70.05	-.17	-2.6107	-.0312	-.0354	-.0169	.0028	-.0003
-74.97	-.17	-2.5759	-.0347	.0633	-.0122	.0020	-.0008
-80.02	-.16	-2.5664	-.0437	.1126	-.0128	.0016	0.0000
-85.11	-.16	-2.5279	-.0496	.1875	-.0183	.0016	-.0004
-90.45	-.17	-2.4912	-.0589	.2667	-.0258	.0046	.0004

RUN 351   Q= 56.40 PSF   RN/FT= 1.324   MACH=0.20

ALPHA	BETA	CN	CA	CLM	CY	CLN	CLL
-40.76	-.19	-2.1580	-.0342	-.0761	-.0035	-.0041	-.0005
-50.91	-.18	-2.3656	-.0390	.0005	-.0199	-.0026	-.0045
-60.70	-.16	-2.4443	-.0505	.0587	-.0240	-.0017	-.0009
-65.51	-.17	-2.4747	-.0588	.1036	-.0240	-.0014	-.0011
-70.34	-.17	-2.4678	-.0674	.1555	-.0249	.0019	-.0018
-75.19	-.16	-2.4637	-.0777	.2124	-.0248	-.0002	-.0014
-80.15	-.16	-2.4240	-.0885	.3100	-.0241	-.0024	.0000
-85.34	-.17	-2.3898	-.0987	.3745	-.0234	.0004	.0002
-90.67	-.17	-2.3765	-.1062	.4501	-.0253	.0026	.0008

RUN 352   Q= 24.70 PSF   RN/FT= .587   MACH=0.20

ALPHA	BETA	CN	CA	CLM	CY	CLN	CLL
-40.59	-.20	-2.2092	-.0447	-.0844	-.0115	-.0015	-.0021
-50.74	-.16	-2.4734	-.0506	-.0806	-.0248	-.0071	-.0023
-60.44	-.18	-2.5444	-.0561	-.1377	.0156	.0274	-.0008
-65.23	-.17	-2.5822	-.0586	-.1414	-.0115	.0160	-.0011
-70.09	-.17	-2.6103	-.0618	-.0723	-.0232	.0027	-.0008
-74.92	-.16	-2.5692	-.0652	.0346	-.0195	.0022	.0002
-79.98	-.17	-2.5587	-.0723	.0904	-.0227	.0029	-.0013
-85.11	-.15	-2.5342	-.0803	.1740	-.0234	.0033	-.0003
-90.42	-.16	-2.4901	-.0869	.2777	-.0241	.0046	-.0005

RUN 353   Q= 24.70 PSF   RN/FT= .597   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
40.45	.18	2.0249	-.0532	-.1748	.0132	.0214	-.0046
50.63	.16	2.2468	-.0827	-.2020	.0131	.0389	-.0089
60.38	.18	2.3741	-.1115	-.1272	.0559	.0370	-.0111
70.06	.15	2.3918	-.1326	-.0602	.0387	.0188	-.0021
79.92	.16	2.3711	-.1228	-.2967	.0036	-.0013	.0003
90.42	.17	2.2306	-.1227	-.4657	.0102	.0004	-.0003

RUN 354   Q= 24.00 PSF   RN/FT= .586   MACH=0.20

ALPHA	BETA	CN	CA	CLM	CY	CLN	CLL
79.92	-9.71	2.3338	-.1183	-.3620	-.0127	-.0132	.0242
79.93	-7.76	2.3535	-.1191	-.3670	-.0134	-.0187	.0190
79.93	-3.80	2.3525	-.1199	-.3498	-.0128	-.0115	.0092
79.92	.16	2.3824	-.1250	-.2997	.0092	.0008	-.0004
79.91	4.16	2.3639	-.1189	-.3510	.0463	.0118	-.0110
79.90	8.13	2.3369	-.1154	-.3654	.0546	.0138	-.0196
79.89	10.08	2.3267	-.1148	-.3566	.0509	.0140	-.0245
79.92	15.05	2.2865	-.1119	-.3425	.0054	-.0006	-.0354
79.91	20.01	2.2421	-.1027	-.3295	-.0589	-.0230	-.0444
79.89	29.92	2.1503	-.0929	-.3104	-.2171	-.0803	-.0617

RUN 355   Q= 25.30 PSF   RN/FT= .604   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
60.44	29.95	2.3591	-.1067	.1526	-.2351	-.0720	-.0782
60.43	20.00	2.3892	-.1146	.1039	-.0315	-.0359	-.0356
60.43	15.03	2.3892	-.1157	.0645	.0675	.0067	-.0272
60.44	10.05	2.4387	-.1243	.0362	.1039	.0385	-.0178
60.43	8.11	2.4174	-.1253	.0131	.1109	.0446	-.0134
60.44	4.14	2.4017	-.1208	-.0351	.1125	.0708	-.0179
60.45	.15	2.3619	-.1171	-.1247	.0605	.0356	-.0114
60.45	-3.79	2.4172	-.1216	-.0792	-.0870	-.0549	.0156
60.47	-7.75	2.4375	-.1241	.0486	-.0900	-.0641	.0182
60.48	-9.72	2.4529	-.1251	.0335	-.0472	-.0273	.0155

RUN 356   Q= 25.60 PSF   RN/FT= .611   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
40.53	-9.73	2.0625	-.0665	-.0077	.0289	-.0236	.0322
40.51	-7.73	2.0323	-.0656	-.0511	.0630	-.0158	.0205
40.47	-3.79	1.9655	-.0608	-.1390	.0644	-.0209	.0086
40.47	.13	2.0114	-.0627	-.1773	.0151	.0232	-.0047
40.45	4.15	1.9815	-.0649	-.1177	-.0334	.0429	-.0039
40.53	8.12	2.0050	-.0654	-.0185	-.0018	.0468	-.0235
40.53	10.11	2.0295	-.0660	.0230	.0012	.0512	-.0286
40.53	15.06	2.0198	-.0695	.1357	-.0532	.0562	-.0425
40.54	20.02	2.0369	-.0751	.2500	-.0974	.0408	-.0498
40.59	29.90	2.1326	-.0943	.4773	-.1551	.0340	-.0860

RUN 357   Q=130.40 PSF   RN/FT= 3.013   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
41.29	30.13	2.0947	-.0880	-.1464	-.3702	-.0762	-.0971
51.46	30.07	2.3064	-.1039	-.2368	-.2729	-.0924	-.0965
61.18	30.00	2.2320	-.1012	-.2546	-.2402	-.0828	-.0734
70.72	29.98	2.0658	-.1001	-.4566	-.2607	-.0928	-.0560
80.62	29.93	2.1179	-.1045	-.5337	-.2192	-.0703	-.0617
91.06	29.88	2.1146	-.1090	-.6223	-.1866	-.0414	-.0702

RUN 358   Q= 57.00 PSF   RN/FT= 1.376   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
40.68	30.01	1.8322	-.0808	-.1324	-.3737	-.0694	-.1004
50.91	29.96	2.2637	-.0978	-.2057	-.2127	-.0840	-.1007
60.65	29.94	2.2105	-.0974	-.1810	-.2296	-.0783	-.0744
70.24	29.97	2.0536	-.0987	-.4357	-.3614	-.1674	-.0553
80.11	29.92	2.0777	-.0903	-.4192	-.2480	-.0983	-.0595
90.60	29.89	2.0811	-.0897	-.5074	-.2198	-.0663	-.0677

RUN 359   Q= 89.60 PSF   RN/FT= 2.171   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
40.93	-9.76	2.0728	-.0685	-.1841	.0703	.0346	.0214
40.86	-7.80	1.9880	-.0664	-.1810	.1046	.0142	.0239
40.84	-3.81	1.9491	-.0619	-.2232	.0765	-.0048	.0091
40.83	.17	1.9979	-.0619	-.2333	-.0256	.0093	-.0014
40.82	4.12	1.9768	-.0620	-.2098	-.0723	.0027	-.0127
40.85	8.15	2.0191	-.0654	-.1712	-.0864	-.0173	-.0223
40.87	10.15	2.0715	-.0664	-.1767	-.0485	-.0254	-.0213
40.89	15.09	2.1332	-.0686	-.1798	-.0516	-.0342	-.0348
40.88	20.05	2.0906	-.0674	-.1891	-.1258	-.0531	-.0642
40.87	30.07	2.0171	-.0851	-.2197	-.3276	-.1073	-.1017

RUN 360   Q= 94.00 PSF   RN/FT= 2.213   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
60.87	30.00	2.2173	-.0974	-.2872	-.2524	-.0731	-.0786
60.87	20.06	2.2670	-.0972	-.2641	-.1135	-.0373	-.0381
60.86	15.05	2.2690	-.0961	-.2690	-.0701	-.0307	-.0272
60.87	10.14	2.2447	-.0970	-.2688	-.0462	-.0213	-.0137
60.87	8.14	2.2585	-.0980	-.2855	-.0154	-.0080	-.0100
60.85	4.14	2.2371	-.0991	-.3298	.0240	.0107	-.0038
60.84	.16	2.2100	-.1011	-.3799	-.0023	-.0056	-.0010
60.86	-3.78	2.2240	-.1003	-.3775	-.0062	-.0117	.0044
60.90	-7.78	2.2662	-.1002	-.3114	.0259	.0102	.0094
60.92	-9.80	2.2668	-.1002	-.2925	.0370	.0203	.0135

RUN 361   Q= 98.30 PSF   RN/FT= 2.252   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
80.34	-9.78	2.2153	-.1149	-.6226	.1060	.0528	.0216
80.33	-7.78	2.2164	-.1149	-.6278	.0849	.0458	.0178
80.31	-3.80	2.1974	-.1162	-.6364	.0579	.0282	.0090
80.32	.14	2.2268	-.1160	-.6063	.0245	.0069	.0004
80.30	4.12	2.2206	-.1125	-.6175	-.0397	-.0207	-.0099
80.30	8.11	2.2117	-.1107	-.6216	-.0913	-.0411	-.0170
80.31	10.10	2.2217	-.1098	-.6160	-.1181	-.0502	-.0226
80.29	15.07	2.1931	-.1070	-.6416	-.1831	-.0709	-.0348
80.28	20.04	2.1540	-.1053	-.6656	-.2414	-.0827	-.0461
80.27	29.98	2.0730	-.0997	-.5709	-.2449	-.0558	-.0637

RUN 362   Q= 57.60 PSF   RN/FT= 1.431   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
40.95	-9.75	2.0496	-.0707	-.1640	.0754	.0351	.0223
40.93	-7.76	1.9882	-.0684	-.1676	.0940	.0157	.0214
40.90	-3.81	1.9560	-.0647	-.2147	.0652	-.0004	.0104
40.89	.15	1.9662	-.0637	-.2295	-.0287	.0091	-.0027
40.90	4.13	1.9716	-.0643	-.1996	-.0565	.0040	-.0134
40.90	8.11	2.0045	-.0688	-.1319	-.0858	-.0165	-.0232
40.91	10.12	2.0478	-.0707	-.1214	-.0829	-.0303	-.0258
40.93	15.07	2.1283	-.0701	-.1633	-.0291	-.0327	-.0281
40.91	20.05	2.1032	-.0703	-.1616	-.0823	-.0464	-.0613
40.86	30.04	1.8702	-.0865	-.1520	-.3237	-.0951	-.0989

RUN 363   Q= 59.20 PSF   RN/FT= 1.393   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
60.61	30.00	2.1874	-.1000	-.1709	-.2467	-.0733	-.0728
60.60	20.10	2.1673	-.0936	-.2510	-.2163	-.0913	-.0362
60.62	15.11	2.2447	-.1027	-.1781	-.1416	-.0694	-.0238
60.62	10.07	2.2690	-.1030	-.2278	-.0563	-.0311	-.0139
60.61	8.13	2.2378	-.1019	-.2515	-.0251	-.0170	-.0098
60.62	4.16	2.2414	-.1021	-.2931	.0204	.0043	-.0033
60.61	.18	2.2064	-.1012	-.3478	.0037	-.0043	-.0010
60.63	-3.81	2.2478	-.1021	-.3203	-.0089	-.0081	.0014
60.65	-7.81	2.2549	-.1026	-.2810	.0250	.0151	.0083
60.66	-9.79	2.2400	-.1027	-.2515	.0519	.0273	.0122

RUN 364   Q= 59.40 PSF   RN/FT= 1.385   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
80.15	-9.76	2.2686	-.1127	-.4550	-.0181	-.0253	.0251
80.14	-7.77	2.2697	-.1125	-.4658	-.0330	-.0326	.0200
80.12	-3.80	2.2393	-.1120	-.4978	-.0003	-.0132	.0094
80.10	.17	2.2345	-.1168	-.5563	.0040	.0087	-.0007
80.09	4.13	2.2372	-.1133	-.5689	-.0407	-.0195	-.0101
80.09	8.14	2.2442	-.1073	-.5037	.0025	.0109	-.0208
80.08	10.08	2.2336	-.1071	-.5003	-.0247	.0019	-.0230
80.07	15.08	2.2171	-.1042	-.4828	-.0983	-.0238	-.0339
80.07	20.04	2.1982	-.1009	-.4820	-.1984	-.0606	-.0437
80.08	29.95	2.1023	-.0926	-.3968	-.2788	-.0805	-.0611

RUN 365   Q= 24.20 PSF   RN/FT= .590   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
40.53	-9.70	2.0978	-.0592	-.0042	.0054	-.0211	.0324
40.52	-7.77	2.0679	-.0606	-.0443	.0391	-.0157	.0217
40.49	-3.80	2.0163	-.0541	-.1345	.0317	-.0155	.0112
40.49	.16	2.0283	-.0537	-.1754	.0161	.0199	-.0051
40.48	4.12	2.0178	-.0548	-.1243	-.0135	.0375	-.0062
40.48	8.10	2.0413	-.0558	-.0172	.0150	.0419	-.0238
40.49	10.10	2.0504	-.0569	.0255	.0233	.0459	-.0294
40.50	15.08	2.0777	-.0625	.0450	-.1087	-.0071	-.0441
40.50	20.06	2.0731	-.0609	.0207	-.2013	-.0558	-.0679
40.49	29.93	1.9894	-.0754	.3072	-.2742	-.0252	-.0867

RUN 366   Q= 25.60 PSF   RN/FT= .600   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
60.43	29.95	2.3419	-.1012	.1565	-.2682	-.0788	-.0763
60.40	20.03	2.3062	-.1040	-.0027	-.1745	-.0728	-.0377
60.41	15.06	2.3476	-.1041	-.0302	-.0792	-.0395	-.0267
60.41	10.06	2.3561	-.1073	-.0752	.0001	-.0077	-.0144
60.42	8.09	2.4020	-.1139	-.0315	.0560	.0416	-.0121
60.42	4.16	2.3721	-.1126	-.0287	.0943	.0709	-.0178
60.42	.15	2.3929	-.1136	-.1102	.0657	.0374	-.0098
60.45	-3.74	2.4139	-.1166	-.0699	-.1136	-.0594	.0148
60.47	-7.75	2.4486	-.1190	.0661	-.0967	-.0699	.0195
60.47	-9.74	2.4180	-.1204	.0518	-.0359	-.0402	.0169

RUN 367   Q= 25.70 PSF   RN/FT= .599   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
79.93	-9.76	2.3147	-.1167	-.3525	-.0361	-.0232	.0253
79.95	-7.73	2.3039	-.1175	-.3592	-.0478	-.0274	.0200
79.93	-3.79	2.3151	-.1186	-.3479	-.0409	-.0149	.0104
79.92	.19	2.3327	-.1222	-.3119	-.0227	-.0010	.0000
79.92	4.12	2.3221	-.1193	-.3439	.0120	.0131	-.0109
79.90	8.12	2.3111	-.1153	-.3644	.0198	.0235	-.0219
79.90	10.09	2.3033	-.1139	-.3570	.0068	.0247	-.0266
79.89	15.05	2.2743	-.1119	-.3256	-.0323	.0121	-.0373
79.88	20.03	2.2368	-.1039	-.3211	-.1003	-.0075	-.0466
79.87	29.91	2.1298	-.0931	-.2901	-.2817	-.0665	-.0642

RUN 369   Q= 90.60 PSF   RN/FT= 2.147   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
40.19	.22	.3030	.1084	.3954	-.0362	.0163	-.0006
50.39	.20	.4316	.0153	.5539	.0106	.0027	-.0002
60.17	.20	.4949	-.0157	.5857	-.0089	.0038	-.0004
65.02	.20	.5271	-.0159	.5959	-.0039	-.0021	-.0001
69.90	.18	.5677	-.0275	.5930	-.0022	-.0015	-.0002
74.88	.19	.5843	-.0199	.5150	-.0161	-.0021	-.0003
79.89	.20	.5908	-.0334	.4647	-.0252	-.0030	-.0006
85.05	.20	.6102	-.0517	.4136	-.0073	-.0007	-.0008
90.49	.19	.6610	-.0550	.3893	-.0167	-.0013	-.0005

RUN 370 Q= 91.70 PSF RN/FT= 2.144 MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
79.98	-9.73	.7512	-.1336	.5487	.1154	.0111	.0025
79.97	-7.76	.7506	-.1332	.5667	.0611	.0036	.0013
79.94	-3.83	.7209	-.1221	.5661	-.0500	-.0030	-.0009
79.88	.15	.5997	-.0270	.4652	-.0212	-.0020	-.0007
79.90	4.11	.6179	-.0583	.4847	-.0902	.0017	-.0027
79.95	8.10	.7675	-.1108	.5163	-.0511	-.0199	-.0029
79.96	10.10	.7855	-.1166	.4987	-.0811	-.0346	-.0037
79.97	15.06	.7899	-.1272	.4891	-.1976	-.0532	-.0070
79.98	20.04	.8051	-.1359	.4459	-.2972	-.0647	-.0101
80.01	29.95	.7782	-.1339	.4268	-.3640	-.0599	-.0130

RUN 371 Q= 91.50 PSF RN/FT= 2.133 MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
60.33	30.01	.7264	-.0596	.4996	-.3437	-.0605	-.0080
60.34	20.02	.8380	-.0649	.5975	-.1161	-.0175	-.0082
60.32	15.06	.7703	-.0509	.6728	-.1242	.0191	-.0072
60.30	10.09	.7295	-.0322	.6462	-.0487	-.0064	-.0052
60.25	8.15	.6525	-.0097	.5712	-.1264	-.0199	-.0045
60.21	4.16	.5371	-.0087	.6016	-.0703	.0073	-.0027
60.21	.14	.4962	-.0131	.5957	-.0018	.0022	0.0000
60.23	-3.81	.5279	-.0060	.5936	.0455	-.0124	.0026
60.29	-7.80	.5931	-.0107	.5939	.1285	.0033	.0041
60.30	-9.77	.6279	-.0147	.5760	.1803	.0144	.0048

RUN 372   Q= 90.00 PSF   RN/FT= 2.109   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
40.21	-9.77	.4180	.0902	.3739	.0859	.0375	.0039
40.17	-7.80	.3922	.1040	.3215	.0868	.0429	.0026
40.13	-3.83	.3509	.1147	.3214	.0243	.0275	.0015
40.11	.20	.2945	.1116	.3923	-.0336	.0158	-.0005
40.13	4.16	.3730	.1167	.3337	-.0712	-.0236	-.0013
40.13	8.17	.4022	.1026	.3412	-.0796	-.0418	-.0029
40.14	10.11	.4201	.0936	.3725	-.0617	-.0301	-.0040
40.29	15.07	.5971	.0719	.4130	-.0171	-.0112	-.0045
40.31	20.05	.6215	.0592	.4090	-.1290	-.0246	-.0061
40.32	30.04	.6313	.0415	.3172	-.3630	-.0588	-.0069

RUN 373   Q= 89.20 PSF   RN/FT= 2.092   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
40.21	.20	.4163	-.0280	.5763	-.0148	.0155	-.0005
50.48	.19	.5777	-.0732	.7368	.0023	.0034	-.0008
60.30	.20	.6630	-.0843	.7341	-.0119	.0027	-.0010
65.10	.19	.6772	-.0809	.7408	-.0101	-.0038	-.0004
69.97	.18	.6810	-.0590	.6614	-.0157	-.0048	-.0001
74.90	.18	.6798	-.0518	.5860	-.0040	-.0005	-.0002
79.97	.19	.6999	-.0554	.5656	-.0038	.0013	-.0006
85.16	.17	.7186	-.0575	.5226	-.0058	.0015	-.0007
90.55	.18	.7488	-.0614	.4957	-.0013	.0031	-.0007

RUN 374   Q= 91.00 PSF   RN/FT= 2.107   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
79.99	-9.75	.7321	-.0632	.5641	.2943	.0080	.0079
79.98	-7.75	.7112	-.0593	.5761	.2657	.0018	.0062
79.96	-3.84	.7025	-.0568	.5734	.1356	-.0001	.0029
79.95	.16	.7071	-.0563	.5740	-.0034	.0012	-.0003
79.95	4.17	.7024	-.0544	.5734	-.1481	.0041	-.0042
79.94	8.11	.7490	-.0571	.5105	-.2091	-.0321	-.0064
79.95	10.11	.7560	-.0590	.4978	-.2632	-.0370	-.0078
79.97	15.06	.8187	-.0716	.4435	-.3229	-.0600	-.0106
79.98	20.05	.8237	-.0837	.4036	-.3795	-.0671	-.0141
80.01	29.91	.8718	-.1370	.4980	-.3239	-.0454	-.0209

RUN 375   Q= 91.00 PSF   RN/FT= 2.101   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
60.41	29.96	.9194	-.1238	.6321	-.2365	-.0520	-.0240
60.36	20.04	.8499	-.1073	.6659	-.1569	-.0456	-.0201
60.34	15.13	.8095	-.0958	.6368	-.1520	-.0569	-.0174
60.33	10.14	.7664	-.0963	.7350	-.1751	-.0176	-.0133
60.32	8.12	.7268	-.0898	.7344	-.1568	-.0104	-.0119
60.29	4.15	.6685	-.0825	.7269	-.1000	.0050	-.0067
60.30	.20	.6588	-.0850	.7336	-.0096	.0010	-.0007
60.32	-3.81	.6710	-.0832	.7317	.0602	-.0079	.0056
60.34	-7.80	.7018	-.0847	.7113	.1491	.0079	.0108
60.38	-9.80	.7723	-.0976	.7189	.1406	.0189	.0121

RUN 376   Q= 90.10 PSF   RN/FT= 2.083   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
40.27	-9.78	.5322	-.0280	.5412	.0474	.0238	.0082
40.23	-7.79	.4967	-.0274	.5198	.0739	.0272	.0050
40.21	-3.82	.4699	-.0270	.5225	.0359	.0126	.0023
40.15	.18	.4155	-.0277	.5757	-.0166	.0154	-.0006
40.18	4.16	.4737	-.0272	.5228	-.0548	-.0120	-.0020
40.19	8.14	.4998	-.0279	.5270	-.0654	-.0269	-.0064
40.19	10.16	.5070	-.0243	.5238	-.0662	-.0190	-.0087
40.20	15.13	.5414	-.0208	.5082	-.1222	-.0278	-.0119
40.20	20.11	.5187	-.0134	.4586	-.2303	-.0455	-.0145
40.26	30.04	.6471	-.0253	.3625	-.3633	-.0613	-.0136

RUN 377   Q= 89.90 PSF   RN/FT= 2.075   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
40.43	.17	.6610	-.0714	.7961	-.0071	.0144	-.0005
50.55	.17	.7062	-.0512	.8358	.0032	.0036	-.0002
60.35	.17	.7790	-.0328	.7318	.0009	.0019	-.0001
65.12	.15	.7864	-.0298	.7279	.0030	-.0040	.0002
70.04	.16	.7979	-.0299	.6974	.0058	-.0033	.0002
74.96	.15	.8072	-.0327	.6484	.0096	.0019	-.0005
80.02	.16	.8309	-.0374	.6226	.0046	.0014	-.0006
85.19	.16	.8468	-.0408	.5865	-.0032	-.0004	-.0003
90.66	.16	.8776	-.0444	.5699	.0039	.0030	-.0001

RUN 378   Q= 89.60 PSF   RN/FT= 2.067   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
80.01	-9.73	.8223	-.0387	.6327	.2918	-.0008	.0063
80.02	-7.77	.8372	-.0404	.6397	.2231	.0008	.0052
79.99	-3.78	.8290	-.0387	.6255	.1174	-.0001	.0024
79.98	.06	.8338	-.0368	.6236	.0048	.0003	.0001
79.98	4.14	.8283	-.0373	.6312	-.1165	.0046	-.0030
79.98	8.16	.8609	-.0402	.5747	-.1598	-.0248	-.0053
79.97	10.13	.8569	-.0397	.5558	-.1928	-.0316	-.0064
79.98	15.09	.8826	-.0437	.5206	-.2940	-.0535	-.0089
79.98	20.01	.8838	-.0480	.4596	-.3848	-.0665	-.0113
79.99	29.96	.9222	-.0599	.4593	-.3446	-.0365	-.0167

RUN 379   Q= 89.20 PSF   RN/FT= 2.055   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
60.39	30.01	.8841	-.0855	.6333	-.2993	-.0651	-.0253
60.37	20.06	.8949	-.0613	.6730	-.2114	-.0345	-.0168
60.36	15.07	.8757	-.0441	.6529	-.2456	-.0275	-.0133
60.36	10.13	.8446	-.0409	.6952	-.1770	-.0273	-.0092
60.35	8.11	.7936	-.0361	.7486	-.1768	.0026	-.0080
60.34	4.17	.7860	-.0343	.7348	-.0817	.0097	-.0048
60.33	.15	.7832	-.0335	.7364	.0030	.0016	.0000
60.35	-3.80	.7886	-.0345	.7351	.0799	-.0112	.0046
60.37	-6.89	.7923	-.0360	.7376	.1493	-.0040	.0071
60.38	-7.79	.7948	-.0368	.7401	.1651	-.0012	.0079
60.40	-9.80	.8291	-.0408	.7130	.1745	.0175	.0091

RUN 380   Q= 88.30 PSF   RN/FT= 2.040   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
40.39	-9.78	.7056	-.0656	.7429	.0446	.0174	.0137
40.37	-7.79	.6946	-.0657	.7403	.0399	.0157	.0105
40.35	-3.80	.6726	-.0638	.7464	.0091	.0055	.0046
40.33	.16	.6586	-.0706	.7943	-.0050	.0148	-.0006
40.34	4.16	.6837	-.0638	.7430	-.0154	-.0079	-.0041
40.33	8.12	.6966	-.0674	.7507	-.0433	-.0162	-.0109
40.33	10.09	.6989	-.0678	.7439	-.0461	-.0110	-.0136
40.32	15.09	.7174	-.0664	.7251	-.0854	-.0108	-.0179
40.31	20.07	.7034	-.0627	.6706	-.1701	-.0264	-.0205
40.29	30.02	.6903	-.0513	.4509	-.3086	-.0630	-.0219

RUN 381   Q= 56.10 PSF   RN/FT= 1.336   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
40.24	.21	.6530	-.0687	.7952	-.0022	.0108	-.0003
50.40	.19	.7350	-.0522	.8368	-.0037	.0031	-.0003
60.20	.20	.8145	-.0338	.7569	.0026	-.0019	.0000
65.01	.19	.8282	-.0305	.7212	.0043	-.0035	.0000
69.89	.17	.8265	-.0289	.6842	.0029	-.0029	.0001
74.84	.20	.8398	-.0322	.6465	.0142	.0103	-.0007
79.89	.20	.8601	-.0360	.6191	.0096	.0084	-.0007
85.07	.19	.8795	-.0391	.6021	-.0005	.0031	-.0006
90.47	.19	.9256	-.0392	.6660	-.0173	-.0105	.0003

RUN 382   Q= 56.30 PSF   RN/FT= 1.295   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
79.92	-9.74	.9291	-.0353	.7647	.1600	-.0750	.0092
79.89	-7.75	.9232	-.0358	.7516	.1133	-.0755	.0081
79.87	-3.82	.9126	-.0359	.7099	.0278	-.0621	.0052
79.85	.20	.8817	-.0348	.6698	-.0483	-.0351	.0015
79.84	4.13	.8787	-.0361	.6875	-.0532	.0428	-.0044
79.83	8.09	.8932	-.0384	.6970	-.1488	.0480	-.0072
79.89	10.09	.9306	-.0415	.7764	-.1236	.0831	-.0105
79.90	15.02	.9845	-.0486	.7775	-.1696	.0480	-.0126
79.90	20.03	.9605	-.0455	.6470	-.3360	-.0292	-.0119
79.92	29.95	1.0047	-.0560	.5824	-.3548	-.0713	-.0141

RUN 383   Q= 56.60 PSF   RN/FT= 1.293   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
60.24	29.96	.9225	-.0869	.7722	-.2921	-.0587	-.0237
60.22	20.08	.8924	-.0599	.8256	-.3920	-.0603	-.0169
60.22	15.10	.9088	-.0531	.8035	-.3041	-.0614	-.0124
60.20	10.13	.8323	-.0420	.8216	-.2194	-.0151	-.0088
60.19	8.11	.8252	-.0396	.7977	-.1800	-.0039	-.0074
60.19	4.12	.8152	-.0349	.7651	-.0884	.0009	-.0041
60.20	.17	.8033	-.0339	.7541	.0045	-.0022	.0000
60.21	-3.81	.8106	-.0344	.7539	.0951	-.0058	.0039
60.24	-7.81	.8180	-.0356	.7769	.2064	-.0054	.0078
60.25	-9.79	.8144	-.0373	.7945	.2485	.0038	.0090

RUN 384   Q= 56.60 PSF   RN/FT= 1.288   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
40.22	-9.75	.6873	-.0658	.7474	.0684	.0150	.0127
40.22	-7.78	.7016	-.0668	.7349	.0236	.0243	.0096
40.19	-3.81	.6804	-.0649	.7360	-.0062	.0178	.0045
40.17	.17	.6452	-.0687	.7903	.0001	.0123	-.0005
40.17	4.12	.6812	-.0655	.7387	-.0157	-.0141	-.0035
40.17	8.11	.6957	-.0676	.7510	-.0492	-.0205	-.0101
40.17	10.10	.6893	-.0684	.7532	-.0762	-.0202	-.0134
40.17	15.03	.7125	-.0661	.7444	-.0945	-.0027	-.0187
40.15	20.04	.6938	-.0624	.7037	-.1723	-.0154	-.0208
40.17	29.94	.7177	-.0567	.5778	-.2492	-.0463	-.0223

RUN 385   Q= 56.40 PSF   RN/FT= 1.285   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
40.16	.21	.4102	-.0268	.5670	-.0146	.0092	-.0003
50.35	.20	.5985	-.0744	.7304	-.0102	.0000	-.0003
60.17	.20	.8325	-.1229	.8069	.0085	-.0008	-.0008
65.04	.19	.8923	-.1195	.7716	.0009	-.0022	-.0002
69.88	.19	.8599	-.0922	.6898	.0193	-.0045	.0005
74.79	.18	.7428	-.0552	.5847	-.0135	.0081	-.0010
79.84	.18	.7610	-.0587	.5675	.0031	.0113	-.0009
85.07	.18	.7925	-.0568	.6094	-.0376	-.0188	0.0000
90.46	.19	.8108	-.0583	.5921	-.0212	-.0076	-.0004

RUN 386   Q= 56.10 PSF   RN/FT= 1.281   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
79.87	-9.77	.9107	-.0740	.6428	-.0219	-.0338	.0094
79.87	-7.73	.8929	-.0712	.6263	-.0689	-.0338	.0079
79.85	-3.78	.8620	-.0655	.5808	-.1243	-.0205	.0046
79.81	.19	.7576	-.0582	.5785	-.0249	-.0047	-.0005
79.79	4.12	.7740	-.0550	.6178	-.0590	.0443	-.0055
79.80	8.11	.8587	-.0668	.5836	-.0126	.0140	-.0082
79.82	10.07	.9119	-.0795	.7032	.0094	.0497	-.0113
79.84	15.05	.9211	-.0868	.7139	-.0924	.0311	-.0135
79.89	19.99	.9160	-.0914	.6813	-.2504	-.0154	-.0148
79.93	29.92	.9317	-.1263	.6200	-.3584	-.0837	-.0179

RUN 387   Q= 56.60 PSF   RN/FT= 1.286   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
60.25	29.95	.8909	-.1157	.7154	-.2775	-.0777	-.0206
60.23	20.09	.8344	-.1054	.7947	-.3568	-.0775	-.0192
60.21	15.09	.7893	-.0981	.7932	-.2934	-.0751	-.0162
60.21	10.13	.8106	-.1012	.8324	-.1940	-.0198	-.0124
60.21	8.09	.8167	-.1051	.8330	-.1221	-.0126	-.0097
60.21	4.12	.8322	-.1135	.8222	-.0379	-.0061	-.0060
60.22	.15	.8348	-.1236	.8067	.0067	.0003	-.0009
60.24	-3.80	.8139	-.1131	.8013	.0142	-.0024	.0054
60.25	-7.79	.7954	-.1021	.8050	.1059	.0057	.0092
60.26	-9.78	.7937	-.1023	.8098	.1581	.0123	.0113

RUN 388   Q= 56.40 PSF   RN/FT= 1.282   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
40.17	-9.78	.5305	-.0329	.5394	.0393	.0341	.0062
40.16	-7.78	.5149	-.0325	.5283	.0171	.0375	.0042
40.14	-3.81	.4537	-.0265	.5218	.0245	.0190	.0017
40.17	.15	.4123	-.0264	.5671	-.0166	.0086	-.0003
40.17	4.13	.4518	-.0269	.5301	-.0515	-.0140	-.0018
40.17	8.13	.5103	-.0323	.5390	-.0483	-.0363	-.0049
40.17	10.10	.5497	-.0293	.5378	-.0412	-.0381	-.0072
40.17	15.05	.5276	-.0182	.5254	-.1253	-.0196	-.0132
40.16	20.06	.5093	-.0107	.4838	-.2407	-.0336	-.0151
40.22	29.97	.6795	-.0312	.5139	-.2567	-.0615	-.0127

RUN 389   Q= 56.10 PSF   RN/FT= 1.279   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
40.11	.18	.2832	.1061	.3970	-.0338	.0067	-.0004
50.33	.16	.4678	.0120	.5620	.0003	.0031	-.0002
60.14	.16	.7343	-.0589	.6500	.0114	.0032	-.0008
65.02	.16	.8027	-.0835	.6804	.0020	-.0035	-.0008
69.87	.17	.8361	-.0880	.6543	-.0149	-.0083	-.0003
74.82	.16	.8452	-.1127	.6200	-.0095	-.0023	-.0003
79.86	.15	.8618	-.1461	.6177	-.0054	.0057	.0001
85.07	.15	.8419	-.1094	.5598	-.0084	-.0081	.0004
90.45	.16	.8431	-.0623	.5142	.0011	-.0114	.0004

RUN 390   Q= 55.90 PSF   RN/FT= 1.277   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
79.89	-9.72	.8942	-.1408	.7627	.0770	-.0778	.0082
79.89	-7.77	.9073	-.1384	.7522	.0330	-.0753	.0070
79.87	-3.84	.8775	-.1436	.6450	.0281	-.0233	.0030
79.85	.15	.8639	-.1454	.6157	-.0031	.0103	-.0003
79.84	4.13	.8835	-.1389	.6585	-.0519	.0409	-.0041
79.84	8.13	.8686	-.1267	.6740	-.1234	.0502	-.0067
79.87	10.10	.8823	-.1185	.6251	-.0783	.0221	-.0064
79.87	15.03	.8577	-.1245	.6306	-.1179	.0041	-.0085
79.88	20.02	.8765	-.1362	.6832	-.2460	-.0371	-.0088
79.90	29.93	.8766	-.1328	.5468	-.3587	-.1013	-.0094

RUN 391   Q= 56.50 PSF   RN/FT= 1.282   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
60.18	29.97	.7731	-.0550	.6264	-.3292	-.0703	-.0079
60.18	20.06	.8187	-.0440	.7695	-.2898	-.0505	-.0082
60.19	15.08	.7819	-.0461	.7776	-.2433	-.0279	-.0060
60.17	10.10	.7547	-.0350	.7335	-.0833	-.0035	-.0054
60.16	8.13	.7318	-.0315	.7087	-.0384	.0025	-.0049
60.16	4.14	.7394	-.0367	.6725	-.0014	.0082	-.0035
60.16	.16	.7327	-.0592	.6490	.0111	.0021	-.0006
60.17	-3.80	.7379	-.0482	.6590	-.0284	-.0151	.0028
60.18	-7.79	.7155	-.0340	.6784	.0242	-.0064	.0045
60.20	-9.79	.7150	-.0340	.6933	.0852	-.0018	.0049

RUN 392   Q= 56.60 PSF   RN/FT= 1.284   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
40.14	-9.79	.4273	.0869	.3677	.0626	.0436	.0026
40.12	-7.77	.4057	.0992	.3656	.0688	.0338	.0023
40.08	-3.79	.3325	.1086	.3497	.0308	.0234	.0011
40.11	.20	.2860	.1072	.3983	-.0376	.0071	-.0005
40.11	4.18	.3166	.1087	.3781	-.0882	-.0106	-.0017
40.12	8.14	.3966	.0982	.3982	-.1129	-.0271	-.0028
40.13	10.15	.4449	.0881	.4074	-.0741	-.0485	-.0033
40.16	15.08	.6017	.0728	.4467	.0067	-.0021	-.0055
40.18	20.05	.6537	.0639	.4686	-.0910	-.0001	-.0073
40.20	30.01	.6622	.0338	.4635	-.3030	-.0413	-.0073

RUN 393   Q= 13.70 PSF   RN/FT= .332   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
40.05	.19	.4054	.1204	.3629	.0179	.0012	-.0001
50.22	.17	.7108	.0194	.6648	-.1075	.0660	-.0040
59.98	.16	.9629	-.0251	.7652	-.0163	.0141	-.0030
64.83	.15	1.0639	-.0624	.8415	-.0827	.0415	-.0019
69.72	.16	1.1585	-.1312	1.0051	-.0061	.0415	-.0016
74.65	.16	1.1740	-.1526	1.0018	.0089	.0236	-.0010
79.74	.15	1.1578	-.1526	.9037	-.0185	.0052	-.0002
84.92	.17	1.1365	-.1496	.7014	-.0868	.0287	-.0012
90.26	.16	1.0306	-.0804	.4889	-.0286	.0076	-.0003

254

APPENDIX - Continued

RUN 394   Q= 15.30 PSF   RN/FT= .349   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
79.72	-9.75	1.1188	-.1425	.7532	-.1833	.0125	.0055
79.71	-7.77	1.0955	-.1423	.7390	-.1912	.0092	.0049
79.71	-3.78	1.1321	-.1513	.8557	-.1094	.0159	.0012
79.70	.17	1.1455	-.1545	.9059	-.0183	.0050	.0001
79.69	4.12	1.1285	-.1550	.8328	.0247	.0214	-.0030
79.71	8.13	1.1413	-.1443	.7726	.0942	.0039	-.0047
79.70	10.11	1.1209	-.1394	.7649	.1210	-.0116	-.0062
79.69	15.05	1.0810	-.1229	.7180	.0973	-.0196	-.0075
79.68	20.02	1.0701	-.1349	.7122	-.0113	-.0444	-.0101
79.69	29.91	1.0171	-.1476	.7109	-.3837	-.0334	-.0141

RUN 395   Q= 15.20 PSF   RN/FT= .348   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
60.03	29.90	1.1023	-.0763	.9790	-.3126	-.0228	-.0124
60.00	20.05	1.1402	-.0705	.9796	.1143	-.0277	-.0095
60.00	15.03	1.1151	-.0750	.9886	.2337	.0008	-.0088
60.02	10.07	1.0887	-.0924	1.0290	.1748	.0211	-.0052
60.03	8.08	1.0800	-.0761	.9736	.1884	.0196	-.0025
60.02	4.10	.9941	-.0239	.8208	.1644	.0415	-.0017
60.03	.14	.9778	-.0292	.7719	-.0160	.0149	-.0027
60.05	-3.81	.9824	-.0134	.7907	.0151	-.0249	.0039
60.07	-7.73	1.0197	-.0288	.9686	-.1433	-.0476	.0043
60.08	-9.78	1.0733	-.0729	1.0307	-.1406	-.0154	.0041

RUN 396   Q= 14.50 PSF   RN/FT= .342   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
40.09	-9.75	.5679	.1320	.5246	-.0153	.0027	.0106
40.07	-7.76	.5233	.1094	.4933	-.0336	.0003	.0076
40.05	-3.81	.4690	.1126	.3752	.0548	-.0242	.0047
40.04	.15	.4168	.1114	.3732	.0202	.0022	.0002
40.04	4.12	.4475	.1192	.4146	-.0973	.0537	-.0058
40.04	8.11	.5370	.1195	.5031	.0276	.0195	-.0080
40.04	10.06	.5655	.1464	.4761	-.0374	.0018	-.0109
40.06	15.06	.6318	.1413	.4944	-.1034	-.0244	-.0101
40.07	19.99	.7164	.1292	.5473	-.1193	.0072	-.0138
40.09	29.93	.8451	.0988	.9576	-.1722	.0535	-.0212

RUN 397   Q= 14.60 PSF   RN/FT= .345   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
40.05	.19	.5349	-.0119	.5460	.0144	.0225	-.0009
50.22	.19	.7889	-.0662	.8013	-.0038	.0518	-.0028
60.03	.18	1.0685	-.1103	.9373	-.0918	.0329	.0003
64.84	.19	1.0874	-.0978	.8889	-.1183	.0488	.0011
69.75	.19	1.0965	-.0796	.8326	-.0107	.0204	.0010
74.68	.17	1.1468	-.0923	.8490	-.0666	.0371	-.0012
79.73	.17	1.1115	-.0789	.6736	-.0939	.0366	-.0010
84.89	.19	1.0783	-.0685	.5714	-.0831	.0325	-.0009
90.28	.17	1.0586	-.0672	.5137	-.0406	.0146	-.0005

RUN 398   Q= 15.30 PSF   RN/FT= .354   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
79.70	-9.74	1.0591	-.0778	.6448	-.1236	.0356	.0075
79.70	-7.77	1.0579	-.0715	.6267	-.1578	.0386	.0057
79.69	-3.81	1.0597	-.0678	.6561	-.1792	.0529	.0017
79.71	.12	1.1038	-.0772	.6594	-.0978	.0331	-.0009
79.70	4.16	1.0873	-.0757	.6441	-.0259	.0013	-.0039
79.68	8.10	1.0220	-.0665	.6217	.0899	-.0122	-.0072
79.68	10.14	1.0402	-.0710	.6246	.0517	-.0156	-.0089
79.69	14.96	1.0832	-.0894	.6499	.0024	-.0390	-.0105
79.69	20.05	1.0995	-.1052	.7051	-.0934	-.0552	-.0137
79.69	29.94	1.0585	-.1362	.7541	-.3892	-.0258	-.0212

RUN 399   Q= 15.50 PSF   RN/FT= .359   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
60.07	29.95	1.2009	-.1350	1.0388	-.2499	-.0255	-.0248
60.04	20.03	1.1736	-.1302	1.0694	.0629	-.0411	-.0208
60.05	15.07	1.1296	-.1303	1.0724	.1505	-.0179	-.0172
60.06	10.08	1.1621	-.1461	1.1349	.2100	.0079	-.0090
60.06	8.11	1.1594	-.1474	1.1307	.2621	.0254	-.0074
60.06	4.18	1.0453	-.0995	.8722	.0753	.0332	-.0017
60.07	.15	1.0445	-.1126	.9530	-.0875	.0478	-.0006
60.06	-3.84	1.0187	-.0928	.8428	-.0146	-.0161	.0024
60.09	-7.78	1.0696	-.1237	1.0355	-.1307	-.0052	.0042
60.10	-9.77	1.2080	-.1564	1.1787	-.1713	-.0089	.0064

RUN 400   Q= 14.80 PSF   RN/FT= .352   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
40.11	-9.76	.6530	-.0149	.6457	.0581	-.0091	.0129
40.09	-7.80	.6158	-.0171	.6344	.0191	-.0078	.0110
40.08	-3.77	.5573	-.0218	.5941	-.0288	.0030	.0051
40.07	.17	.5241	-.0137	.5469	.0177	.0257	-.0005
40.06	4.13	.5701	-.0176	.5962	.0237	.0264	-.0053
40.06	8.12	.6162	-.0122	.6691	.0017	.0307	-.0107
40.06	10.14	.6410	-.0074	.6903	-.0216	.0261	-.0121
40.08	15.05	.7044	-.0086	.6255	-.1010	-.0137	-.0112
40.08	20.05	.7553	-.0014	.6188	-.2360	.0133	-.0160
40.09	29.93	.7578	.0085	.9526	-.4047	.0469	-.0245

RUN 401   Q= 15.10 PSF   RN/FT= .357   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
40.11	.19	.7311	-.0591	.7620	.0371	.0267	-.0011
50.27	.20	.8771	-.0465	.9210	-.0125	.0402	.0021
60.02	.20	.9886	-.0433	1.0049	.0218	.0362	.0041
64.85	.18	1.0296	-.0386	1.0125	.0007	.0189	.0030
69.72	.17	1.0432	-.0339	.9796	.0123	.0085	.0014
74.69	.17	1.0544	-.0281	.8789	-.0133	.0012	.0005
79.70	.18	1.0756	-.0238	.7063	-.0523	.0138	.0000
84.92	.17	1.0769	-.0270	.6232	-.0097	.0120	.0006
90.28	.17	1.1000	-.0340	.5672	-.0700	.0340	-.0005

RUN 402   Q= 15.00 PSF   RN/FT= .357   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
79.70	-9.71	1.0887	-.0341	.6170	.0077	.0131	.0072
79.70	-7.77	1.0685	-.0323	.6207	-.0037	.0121	.0063
79.69	-3.81	1.0647	-.0270	.6351	-.0176	.0357	.0023
79.67	.12	1.0460	-.0252	.7017	-.0325	.0167	.0003
79.66	4.17	1.0540	-.0325	.6512	.0081	-.0398	-.0020
79.65	8.12	1.0639	-.0340	.6079	.0280	-.0213	-.0053
79.73	10.12	1.0786	-.0370	.6064	.0155	-.0248	-.0063
79.71	15.07	1.0816	-.0422	.6247	-.0877	-.0333	-.0091
79.71	20.04	1.0822	-.0461	.6298	-.2200	-.0332	-.0121
79.71	29.95	1.0697	-.0758	.7065	-.4095	-.0239	-.0169

RUN 403   Q= 15.20 PSF   RN/FT= .360   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
60.02	29.96	1.1508	-.1061	1.0122	-.3465	-.0284	-.0275
60.05	20.02	1.0672	-.0643	.9838	-.1803	-.0158	-.0179
60.04	15.07	1.0537	-.0572	.9768	-.0550	-.0008	-.0146
60.04	10.09	1.0311	-.0521	.9411	.0047	.0166	-.0112
60.03	8.13	1.0164	-.0495	.9594	.0352	.0388	-.0099
60.04	4.06	.9564	-.0473	1.0216	-.0316	.0721	-.0009
60.04	.18	.9602	-.0480	1.0161	.0100	.0364	.0036
60.05	-3.81	1.0012	-.0502	.9068	-.0569	-.0062	-.0006
60.06	-7.72	1.1023	-.0667	1.0486	-.0549	-.0208	.0047
60.05	-9.75	1.0673	-.0614	1.0395	-.0911	-.0235	.0110

RUN 404   Q= 15.20 PSF   RN/FT= .361   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
40.08	-9.73	.8514	-.0703	.9494	-.0636	-.0267	.0117
40.07	-7.74	.7868	-.0691	.9138	-.0711	-.0158	.0086
40.06	-3.78	.7219	-.0677	.8318	-.0750	.0099	.0025
40.04	.21	.7179	-.0645	.7750	.0214	.0268	-.0016
40.09	4.15	.7769	-.0665	.8518	.0579	.0208	-.0055
40.09	10.14	.8821	-.0724	1.0118	.0716	.0417	-.0125
40.09	15.07	.8814	-.0732	.9766	-.0017	.0097	-.0140
40.09	8.12	.8458	-.0714	.9670	.0758	.0407	-.0104
40.08	20.00	.9763	-.0795	.9653	-.0483	.0107	-.0178
40.10	29.91	1.0030	-.0848	1.2249	-.1838	.0574	-.0271

RUN 405   Q= 24.30 PSF   RN/FT= .569   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
40.16	.20	.7061	-.0606	.7875	.0235	.0149	-.0006
50.32	.19	.7991	-.0503	.8796	.0041	.0278	-.0006
60.05	.18	.8924	-.0377	.8925	.0232	.0272	-.0008
64.88	.19	.9209	-.0300	.8591	-.0564	-.0293	-.0001
69.76	.18	.9588	-.0323	.8621	-.0597	-.0358	.0009
74.73	.17	1.0056	-.0329	.8770	-.0181	-.0091	.0003
79.76	.18	1.0180	-.0285	.7635	.0083	-.0054	.0003
84.97	.17	1.0307	-.0301	.6873	.0267	-.0137	.0009
90.38	.17	1.0718	-.0384	.6266	.0181	-.0098	.0004

RUN 406 Q= 25.90 PSF RN/FT= .595 MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
79.76	-9.77	1.0730	-.0384	.6133	-.0019	.0083	.0078
79.76	-7.77	1.0732	-.0350	.6049	-.0222	.0071	.0068
79.75	-3.83	1.0178	-.0270	.7155	.0490	.0000	.0040
79.74	.20	1.0092	-.0283	.7567	.0081	-.0054	.0006
79.74	4.19	.9993	-.0309	.7532	-.0580	.0114	-.0035
79.77	8.12	1.0463	-.0356	.6593	.0188	.0058	-.0062
79.78	10.09	1.0540	-.0372	.6625	-.0059	.0088	-.0074
79.78	15.07	1.0677	-.0437	.6889	-.0960	.0048	-.0102
79.78	20.03	1.0765	-.0449	.6746	-.1978	-.0170	-.0121
79.78	29.94	1.0656	-.0656	.6412	-.3832	-.0348	-.0152

RUN 407 Q= 25.80 PSF RN/FT= .598 MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
60.11	29.96	1.1299	-.1011	.9969	-.2766	-.0543	-.0252
60.08	20.07	1.0144	-.0630	.9383	-.2905	-.0691	-.0156
60.05	15.07	.9581	-.0488	.8841	-.2861	-.0482	-.0123
60.03	10.10	.9020	-.0405	.8825	-.2489	-.0145	-.0091
60.04	8.16	.8917	-.0384	.8648	-.1963	-.0098	-.0073
60.05	4.16	.8707	-.0332	.8329	-.1003	-.0022	-.0034
60.06	.13	.8895	-.0378	.8790	.0163	.0180	-.0006
60.08	-3.79	.9270	-.0457	.9544	.0211	-.0499	.0008
60.11	-7.80	.9784	-.0496	1.0139	-.0197	-.0765	.0109
60.11	-9.77	.9937	-.0506	1.0196	.0316	-.0609	.0124

RUN 408   Q= 25.90 PSF   RN/FT= .605   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
40.14	-9.76	.7902	-.0742	.9257	-.0283	-.0099	.0102
40.13	-7.69	.7418	-.0686	.8763	-.0099	.0003	.0062
40.11	-3.77	.6870	-.0581	.8004	-.0197	-.0074	.0030
40.09	.18	.6722	-.0574	.7625	.0074	.0112	-.0031
40.08	4.15	.7001	-.0553	.8126	-.0206	.0291	-.0076
40.10	8.08	.7504	-.0705	.9047	.0144	.0211	-.0090
40.13	10.10	.7094	-.0613	.7660	-.0773	-.0410	-.0119
40.12	15.03	.7070	-.0590	.7521	-.1436	-.0478	-.0161
40.12	20.06	.7529	-.0644	.7673	-.1556	-.0691	-.0170
40.15	29.96	.9101	-.0839	1.0146	-.1770	-.0096	-.0218

RUN 409   Q= 25.90 PSF   RN/FT= .609   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
40.10	.21	.4602	-.0210	.5596	-.0017	.0123	-.0002
50.31	.21	.6689	-.0738	.7556	-.0200	.0274	-.0008
60.07	.15	.9215	-.1121	.8576	.0056	.0566	.0005
64.90	.15	.9938	-.1276	.8840	-.0996	.0020	-.0010
69.76	.14	1.0042	-.1177	.8528	-.2060	-.0237	-.0005
74.70	.15	1.0294	-.1141	.8244	-.0853	-.0436	.0010
79.82	.14	1.0288	-.0865	.7288	-.0073	-.0016	.0000
84.93	.16	1.0219	-.0746	.5929	.0014	-.0091	.0001
90.35	.20	1.0181	-.0752	.5238	.0081	-.0092	.0002

RUN 410   Q= 25.60 PSF   RN/FT= .608   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
79.73	-9.72	1.0023	-.0829	.6184	-.1149	.0176	.0082
79.79	-7.77	.9880	-.0753	.6065	-.1146	.0058	.0070
79.78	-3.81	.9707	-.0747	.6764	-.0829	-.0010	.0041
79.79	.15	1.0369	-.0848	.7293	.0065	-.0032	.0004
79.76	4.14	1.0089	-.0826	.6720	-.0316	.0113	-.0039
79.75	8.10	.9579	-.0713	.6605	.0466	.0158	-.0079
79.75	10.05	.9532	-.0747	.6738	.0032	.0256	-.0099
79.75	15.05	.9810	-.0893	.7293	-.0863	.0310	-.0131
79.76	20.06	1.0182	-.1103	.7871	-.0933	.0001	-.0126
79.76	29.94	1.0338	-.1355	.6396	-.2911	-.0708	-.0176

RUN 411   Q= 26.20 PSF   RN/FT= .620   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
60.10	29.94	1.0909	-.1287	.9708	-.2265	-.0668	-.0221
60.06	19.97	.9617	-.1156	.9319	-.2192	-.0902	-.0191
60.05	14.99	.9177	-.1053	.8794	-.1898	-.0735	-.0168
60.04	10.01	.8829	-.0959	.8583	-.1249	-.0512	-.0122
60.04	8.05	.9007	-.1035	.8815	-.0716	-.0426	-.0104
60.05	4.14	.9480	-.1194	.8701	.0008	-.0125	-.0046
60.06	.16	.9141	-.1152	.8840	-.0337	.0039	-.0019
60.07	-3.81	.9100	-.0960	.8943	-.0888	-.0470	.0043
60.11	-7.75	1.0441	-.1432	1.1240	-.0954	-.0479	.0073
60.12	-9.79	1.0650	-.1490	1.1535	-.1106	-.0406	.0106

RUN 412   Q= 24.70 PSF   RN/FT= .605   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
40.09	-9.77	.5731	-.0268	.6601	.0368	.0060	.0104
40.07	-7.78	.5542	-.0276	.6206	.0385	.0140	.0078
40.05	-3.78	.5032	-.0233	.5724	.0124	.0021	.0036
40.04	.14	.4731	-.0206	.5505	.0106	.0113	.0001
40.04	4.09	.5170	-.0233	.5829	-.0362	.0134	-.0031
40.04	8.15	.5554	-.0236	.6433	-.0259	.0103	-.0080
40.04	10.13	.5713	-.0199	.6497	-.0366	.0152	-.0100
40.04	15.04	.6436	-.0137	.6572	-.1233	.0102	-.0118
40.04	20.03	.6003	-.0222	.5924	-.2270	-.0743	-.0112
40.06	29.97	.7214	-.0089	.7673	-.3044	-.0215	-.0191

RUN 413   Q= 25.40 PSF   RN/FT= .621   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
40.03	.09	.3672	.1048	.3742	-.0129	.0128	-.0002
50.22	.09	.6160	.0119	.5598	.0162	.0239	.0007
60.01	.14	.8466	-.0644	.7914	-.1112	.0549	-.0006
64.88	.14	.9372	-.1045	.8345	-.0712	.0472	-.0013
69.73	.16	.9600	-.1058	.7768	-.1790	-.0188	.0012
74.77	.15	.9884	-.1241	.7711	-.1796	-.0223	.0021
79.76	.14	1.0135	-.1462	.8235	-.0633	-.0009	.0006
84.91	.15	.9944	-.1447	.7237	-.0156	-.0057	.0004
90.36	.16	.9881	-.0850	.5040	.0095	-.0142	.0004

RUN 414   Q= 25.20 PSF   RN/FT= .622   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
79.81	-9.78	1.0432	-.1453	.7224	-.1477	-.0076	.0071
79.80	-7.79	1.0071	-.1395	.7359	-.0706	-.0416	.0064
79.80	-3.78	1.0216	-.1472	.7578	-.1471	-.0270	.0040
79.79	.18	.9992	-.1441	.8328	-.0464	-.0055	.0003
79.77	4.09	.9601	-.1365	.7679	-.0134	.0439	-.0041
79.76	8.04	1.0168	-.1382	.6991	.0424	.0227	-.0057
79.76	10.01	1.0142	-.1358	.6973	.0240	.0207	-.0063
79.76	14.98	.9773	-.1155	.7083	-.0150	.0214	-.0076
79.76	20.03	.9564	-.1377	.7595	-.0611	-.0003	-.0105
79.76	29.94	.9757	-.1454	.5848	-.2678	-.0787	-.0100

RUN 415   Q= 25.90 PSF   RN/FT= .634   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
60.06	29.96	.9914	-.0673	.8750	-.2840	-.0671	-.0097
60.03	20.03	.9079	-.0578	.8682	-.2199	-.0598	-.0072
60.02	15.07	.8613	-.0536	.8545	-.1432	-.0076	-.0070
60.02	10.05	.8725	-.0517	.8272	-.0319	.0109	-.0056
60.03	8.12	.8951	-.0564	.8159	-.0064	.0306	-.0053
60.04	4.09	.9028	-.0804	.8883	-.0546	.0841	-.0038
60.04	.15	.8546	-.0668	.7915	-.1149	.0558	-.0003
60.05	-3.77	.8495	-.0258	.8113	-.1469	-.0401	.0036
60.08	-7.77	.9265	-.0670	.9855	-.1395	-.0464	.0046
60.09	-9.84	.8953	-.0763	1.0199	-.0520	-.0692	.0061

RUN 416   Q= 25.10 PSF   RN/FT= .629   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
40.08	-9.72	.4807	.0990	.5131	-.0042	.0150	.0077
40.07	-7.80	.4265	.1039	.4593	.0431	.0150	.0065
40.05	-3.82	.3964	.1067	.3781	.0182	.0139	.0026
40.03	.16	.3600	.1044	.3801	-.0177	.0148	-.0002
40.03	4.14	.3952	.1148	.3880	-.0479	.0008	-.0028
40.02	8.13	.4233	.1092	.4694	-.0505	.0078	-.0068
40.03	10.10	.4655	.1066	.5080	-.0126	.0114	-.0078
40.04	20.07	.5880	.0644	.5297	-.2000	-.0680	-.0054
40.06	29.91	.6865	.0257	.6229	-.2689	-.0536	-.0062
40.02	15.01	.4971	.0772	.4741	-.2049	-.0588	-.0051

RUN 417   Q= 92.30 PSF   RN/FT= 2.182   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
40.37	.09	.7832	.0138	.8083	.0345	.0137	-.0025
50.58	.09	.8650	.0180	.8580	-.0038	.0042	-.0010
60.39	.09	.9072	.0206	.7585	-.0065	.0001	-.0002
65.22	.09	.9116	.0210	.7740	.0047	-.0035	.0000
70.09	.09	.9103	.0191	.7375	-.0021	-.0029	-.0002
75.01	.12	.9185	.0198	.6703	-.0050	.0025	-.0006
80.09	.13	.9345	.0180	.6593	-.0072	.0029	-.0006
85.26	.14	.9465	.0163	.6267	-.0067	.0042	-.0006
90.68	.16	.9455	.0164	.5940	-.0029	.0054	-.0006

RUN 418   Q= 94.30 PSF   RN/FT= 2.208   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
80.07	-9.74	.9199	.0145	.6540	.2191	.0067	.0052
80.07	-7.78	.9212	.0150	.6652	.1809	.0011	.0042
80.06	-3.79	.9360	.0171	.6650	.0905	.0002	.0019
80.05	.14	.9311	.0181	.6550	-.0021	.0028	-.0006
80.06	4.15	.9282	.0177	.6686	-.1029	.0080	-.0034
80.09	8.12	.9418	.0154	.6422	-.1496	-.0091	-.0052
80.09	10.08	.9507	.0137	.6141	-.1787	-.0251	-.0060
80.08	15.08	.9547	.0122	.5762	-.2813	-.0348	-.0084
80.08	20.06	.9522	.0057	.5260	-.3190	-.0470	-.0115
80.09	29.98	.9554	-.0067	.5267	-.3183	-.0216	-.0161

RUN 419   Q= 93.30 PSF   RN/FT= 2.195   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
60.44	29.99	.9750	-.0047	.6910	-.2293	-.0417	-.0178
60.44	20.10	1.0372	.0024	.7299	-.1150	-.0303	-.0125
60.43	15.06	1.0304	.0086	.7395	-.0939	-.0340	-.0104
60.43	10.12	.9937	.0146	.7434	-.0985	-.0330	-.0072
60.42	8.10	.9565	.0168	.7711	-.1071	-.0130	-.0065
60.40	4.17	.9155	.0203	.7734	-.0550	.0077	-.0040
60.39	.14	.9155	.0206	.7702	-.0053	.0007	-.0001
60.41	-3.78	.9196	.0200	.7733	.0427	-.0081	.0035
60.44	-7.78	.9373	.0171	.7801	.1163	.0016	.0061
60.48	-9.81	1.0205	.0107	.7366	.0397	.0446	.0067

RUN 420   Q= 91.60 PSF   RN/FT= 2.172   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
40.43	-9.80	.8495	.0096	.8103	-.0671	.0188	.0096
40.42	-7.80	.8093	.0096	.8020	-.0140	.0113	.0064
40.40	-3.82	.8021	.0127	.8112	-.0189	.0026	.0030
40.37	.13	.7910	.0128	.8085	.0383	.0118	-.0018
40.36	4.13	.7918	.0131	.8011	.0111	-.0019	-.0030
40.35	8.12	.8217	.0096	.8142	.0524	-.0115	-.0070
40.38	10.12	.8509	.0097	.8183	.0779	-.0067	-.0092
40.46	15.05	.9283	.0096	.7982	.0851	.0026	-.0142
40.47	20.01	.9697	.0057	.7974	-.0037	.0112	-.0179
40.43	29.99	.9102	.0014	.5965	-.2076	-.0397	-.0224

RUN 421   Q= 15.20 PSF   RN/FT= .363   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
40.09	.17	.8767	.0218	.7907	.0384	.0214	-.0012
50.23	.16	1.0205	.0186	.9048	-.0226	.0205	.0034
60.04	.15	1.0943	.0131	1.0368	.0069	.0282	.0028
64.90	.13	1.1155	.0114	1.0396	-.0158	.0187	.0019
69.75	.15	1.1312	.0117	1.0044	-.0167	.0094	.0005
74.75	.16	1.1416	.0140	.8957	-.0258	.0130	.0000
79.76	.17	1.1384	.0252	.7167	-.0306	.0118	.0002
84.95	.16	1.1572	.0234	.6533	-.0993	.0337	-.0014
90.42	.16	1.1622	.0213	.5885	-.0537	.0192	-.0006

RUN 422   Q= 14.20 PSF   RN/FT= .348   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
79.78	-9.75	1.1926	.0124	.6646	-.0895	.0179	.0060
79.78	-7.77	1.1671	.0163	.6563	-.0592	.0090	.0047
79.77	-3.78	1.1605	.0198	.6581	-.0399	.0313	.0018
79.75	.16	1.1256	.0253	.7301	-.0270	.0029	-.0001
79.74	4.12	1.1376	.0185	.6660	.0155	-.0339	-.0020
79.73	8.14	1.1441	.0153	.6359	.0401	-.0130	-.0052
79.72	10.10	1.1482	.0112	.6541	.0081	-.0037	-.0076
79.72	15.07	1.1685	-.0021	.6928	.0126	-.0132	-.0097
79.73	19.98	1.1764	-.0078	.6768	-.0737	-.0306	-.0120
79.71	29.94	1.1379	-.0217	.6468	-.2941	-.0286	-.0155

RUN 423   Q= 14.30 PSF   RN/FT= .351   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
60.04	29.94	1.2168	-.0331	1.0643	-.2491	-.0173	-.0200
60.03	20.04	1.2418	-.0228	1.1134	.0383	-.0407	-.0138
60.03	15.06	1.2155	-.0224	1.1299	.1303	-.0229	-.0111
60.04	8.05	1.2048	-.0148	1.1006	.1648	.0114	-.0072
60.05	4.12	1.1032	.0049	1.0045	-.0044	.0551	-.0006
60.06	.18	1.0763	.0060	1.0390	.0151	.0278	.0029
60.08	-3.79	1.1395	.0018	.9390	-.0602	-.0052	-.0008
60.10	-7.78	1.2472	-.0171	1.1444	-.1747	-.0204	.0055
60.11	-9.74	1.2648	-.0230	1.1863	-.2020	-.0070	.0077

RUN 424   Q= 14.30 PSF   RN/FT= .352   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
40.12	-9.75	1.0548	0.0000	1.0466	-.1276	-.0105	.0084
40.11	-7.77	.9889	-.0005	1.0059	-.0930	.0040	.0049
40.09	-3.83	.9082	.0069	.9000	.0272	.0163	.0001
40.08	.16	.8892	.0127	.7871	.0461	.0204	-.0007
40.08	4.09	.9323	.0066	.8964	.0745	.0150	-.0023
40.08	8.07	.9989	.0037	1.0262	.1462	.0172	-.0063
40.08	10.07	1.0585	.0036	1.0663	.1602	.0305	-.0098
40.07	15.04	1.0693	-.0036	1.0896	.1281	.0306	-.0117
40.08	20.00	1.1251	-.0107	1.1451	.1328	.0233	-.0140
40.07	29.93	1.2100	-.0256	1.3487	-.0837	.0851	-.0239

RUN 425   Q= 24.60 PSF   RN/FT= .594   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
40.13	.19	.8112	.0163	.8172	.0471	.0130	-.0015
50.26	.18	.9205	.0183	.9222	.0180	.0084	.0009
60.10	.17	1.0154	.0136	.9405	.0256	.0304	-.0009
64.89	.20	1.0166	.0148	.8986	-.0598	-.0362	-.0002
69.80	.17	1.0291	.0121	.9981	-.0645	-.0391	.0006
74.77	.17	1.0746	.0132	.9249	-.0220	-.0119	.0005
79.79	.18	1.0730	.0206	.8050	.0061	-.0067	-.0003
85.01	.17	1.1002	.0204	.7347	.0175	-.0167	.0000
90.43	.17	1.1247	.0173	.6541	.0189	-.0095	-.0002

RUN 426   Q= 24.80 PSF   RN/FT= .602   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
79.85	-9.80	1.1365	.0107	.6725	-.0421	-.0059	.0067
79.84	-7.81	1.0962	.0140	.6954	-.0200	-.0220	.0054
79.82	-3.84	1.0610	.0211	.7954	.0416	-.0303	.0032
79.82	.17	1.0607	.0192	.8014	.0060	-.0066	-.0005
79.80	4.10	1.0412	.0203	.7835	-.0534	.0175	-.0040
79.80	8.11	1.0920	.0159	.6927	.0142	.0147	-.0067
79.80	10.11	1.1041	.0119	.7055	-.0114	.0225	-.0082
79.80	15.01	1.1034	.0017	.7952	-.0849	.0463	-.0118
79.80	19.98	1.1188	-.0061	.8080	-.1047	.0098	-.0125
79.68	29.96	-.0065	-.2736	.2693	-.1606	-.0272	.0465

RUN 427   Q= 25.40 PSF   RN/FT= .612   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
60.10	20.03	1.1190	-.0111	1.0112	-.1761	-.0677	-.0135
60.09	15.04	1.1084	-.0032	.9826	-.1229	-.0640	-.0101
60.07	10.10	1.0717	.0041	.9551	-.0848	-.0470	-.0075
60.06	8.16	1.0393	.0098	.9250	-.1006	-.0311	-.0065
60.06	4.14	.9827	.0172	.8698	-.0976	-.0051	-.0032
60.07	.11	1.0034	.0137	.9279	.0060	.0130	-.0011
60.10	-3.79	1.0423	.0063	.9989	.0124	-.0547	.0008
60.15	-7.73	1.1092	-.0048	1.1034	-.0921	-.0571	.0083
60.16	-9.78	1.1682	-.0111	1.1455	-.0908	-.0313	.0082

RUN 428   Q= 25.20 PSF   RN/FT= .609   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
40.13	-9.77	.9754	-.0029	1.0249	-.0762	-.0026	.0070
40.11	-7.75	.9365	-.0012	.9779	-.0674	.0048	.0062
40.08	-3.81	.8583	.0119	.8790	-.0804	-.0020	.0051
40.07	.14	.8167	.0140	.8245	.0405	.0114	-.0014
40.07	4.10	.8775	.0104	.8989	.1082	.0175	-.0048
40.07	8.09	.8920	.0013	.9284	.0026	-.0163	-.0040
40.06	10.12	.8843	.0074	.8552	.0589	-.0372	-.0082
40.06	15.05	.9174	.0040	.8488	.0284	-.0320	-.0128
40.07	20.04	.9611	.0001	.8755	-.0065	-.0428	-.0145
40.08	29.91	1.1052	-.0276	1.1244	-.0399	.0107	-.0198

RUN 429   Q= 54.10 PSF   RN/FT= 1.287   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
40.28	.19	.7605	.0157	.8251	.0337	.0085	-.0019
50.43	.20	.8514	.0193	.8613	-.0058	.0023	-.0007
60.22	.18	.9164	.0221	.7770	-.0073	-.0033	-.0002
65.10	.19	.9175	.0221	.7527	.0007	-.0034	-.0001
69.92	.18	.9170	.0227	.7127	-.0023	-.0023	-.0004
74.90	.17	.9226	.0208	.6693	-.0049	.0031	-.0008
79.92	.17	.9311	.0191	.6414	-.0051	.0053	-.0009
85.11	.19	.9372	.0178	.6133	-.0078	.0029	-.0002
90.56	.19	.9601	.0181	.6198	.0003	.0174	-.0014

RUN 430   Q= 59.20 PSF   RN/FT= 1.369   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
79.98	-9.69	.9916	.0166	.7908	.1137	-.0842	.0084
80.00	-7.76	.9954	.0179	.7782	.0700	-.0814	.0072
79.97	-3.80	.9742	.0203	.7176	.0384	-.0475	.0037
79.94	.17	.9386	.0199	.6501	-.0032	.0058	-.0009
79.93	4.14	.9394	.0213	.6732	-.0779	.0207	-.0036
79.94	8.09	.9622	.0210	.7427	-.1435	.0546	-.0074
79.93	10.09	.9920	.0179	.6933	-.1194	.0262	-.0079
79.94	15.04	1.0163	.0123	.6839	-.1874	.0139	-.0102
79.94	20.04	1.0103	.0073	.6713	-.2725	-.0197	-.0113
79.95	29.94	1.0292	-.0067	.6662	-.3125	-.0531	-.0140

RUN 431   Q= 59.00 PSF   RN/FT= 1.365   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
60.29	29.96	.9555	-.0018	.7043	-.2488	-.0448	-.0167
60.32	20.05	.9894	.0052	.8878	-.2999	-.0320	-.0131
60.31	15.01	.9846	.0076	.8641	-.2431	-.0453	-.0096
60.29	10.09	.9571	.0156	.8464	-.1635	-.0226	-.0072
60.28	8.11	.9310	.0187	.8252	-.1406	-.0060	-.0061
60.27	4.15	.9204	.0209	.7960	-.0721	-.0008	-.0036
60.27	.15	.9073	.0216	.7741	-.0030	-.0031	-.0002
60.29	-3.80	.9080	.0210	.7784	.0549	-.0041	.0027
60.32	-7.78	.9264	.0178	.8092	.1252	.0046	.0053
60.33	-9.80	.9501	.0133	.8138	.1003	.0277	.0060

RUN 432   Q= 57.50 PSF   RN/FT= 1.344   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
40.25	-9.75	.8268	.0081	.8136	-.0758	.0185	.0086
40.23	-7.77	.8010	.0088	.8144	-.0435	.0173	.0061
40.21	-3.82	.7835	.0122	.8104	-.0264	.0078	.0028
40.20	.14	.7566	.0145	.8272	.0276	.0076	-.0016
40.20	4.12	.7923	.0120	.8096	.0082	-.0051	-.0032
40.21	8.12	.8274	.0083	.8333	.0440	-.0213	-.0068
40.22	10.09	.8526	.0084	.8282	.0773	-.0256	-.0095
40.23	15.43	.9209	.0107	.8081	.0580	.0047	-.0141
40.25	19.97	.9523	.0066	.8125	.0071	.0102	-.0181
40.23	29.89	.9334	0.0000	.7416	-.0952	-.0354	-.0218

RUN 433   Q=277.90 PSF   RN/FT= 6.370   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
40.65	.12	.4201	.0060	.4778	-.0361	.0423	-.0010
50.94	.20	.6504	-.0006	.5960	-.1382	.0367	.0003
60.51	.14	.7648	-.0072	.6109	.0180	.0183	-.0004
64.10	.17	.7737	-.0036	.6013	-.0112	.0168	.0001
70.63	.18	.7196	.0097	.5837	.0102	.0014	-.0002
75.61	.17	.7066	.0132	.5282	.0069	.0027	.0000
80.62	.19	.6993	.0140	.4753	.0116	-.0010	.0001
85.79	.17	.7089	.0145	.4484	.0185	-.0027	.0003
91.20	.18	.7132	.0280	.3887	.0032	-.0028	.0002

RUN 434   Q=280.50 PSF   RN/FT= 6.370   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
80.60	-9.78	.7338	.0111	.4687	-.0192	-.0015	.0023
80.59	-7.76	.7353	.0077	.4594	.0750	.0071	.0015
80.55	-3.83	.7038	.0124	.4748	.0765	-.0004	.0008
80.53	.11	.7001	.0144	.4735	.0137	-.0011	.0002
80.53	4.07	.6973	.0154	.4747	-.0831	-.0020	-.0008
80.51	8.09	.7244	.0159	.3889	-.0574	-.0258	-.0014
80.49	10.05	.7254	.0143	.3942	-.0212	-.0220	-.0017
80.66	15.14	.7857	.0021	.3831	-.0713	-.0593	-.0026
80.76	20.09	.8184	-.0146	.4639	-.1304	-.0552	-.0046
80.85	30.04	.7845	-.0299	.4684	-.3170	-.0724	-.0056

RUN 435   Q=273.20 PSF   RN/FT= 6.257   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
61.34	30.23	.8591	-.0258	.6323	-.3536	-.0863	-.0060
61.25	20.16	.9126	-.0113	.6643	-.1263	-.0550	-.0058
61.22	15.15	.8634	-.0032	.6504	-.0543	-.0344	-.0046
61.05	10.07	.7949	.0023	.6794	.0337	-.0006	-.0040
61.06	8.04	.7679	.0032	.6847	.0683	.0078	-.0036
61.00	4.08	.7663	-.0001	.6568	.0900	.0234	-.0025
60.25	.10	.7608	-.0059	.6079	.0129	.0136	.0000
61.09	-3.68	.7591	-.0029	.6476	-.1398	-.0092	.0030
60.98	-7.73	.8019	-.0038	.6560	-.1870	.0163	.0033
61.15	-9.76	.8175	-.0041	.6438	-.1604	.0325	.0034

RUN 436   Q=267.10 PSF   RN/FT= 6.154   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
40.73	-9.94	.5523	.0047	.3925	.1240	.0467	.0033
40.71	-7.92	.5538	.0084	.3665	.0863	.0442	.0017
40.64	-3.86	.4801	.0106	.4092	.0127	.0240	.0005
40.58	.10	.4074	.0074	.4815	-.0160	.0324	-.0006
40.68	4.18	.4576	.0122	.4736	-.0836	.0021	-.0004
40.77	8.27	.5386	.0086	.4091	-.1317	-.0335	-.0020
40.78	10.29	.5550	.0036	.4321	-.1566	-.0390	-.0036
40.81	15.27	.6071	-.0016	.4792	-.2282	-.0366	-.0060
40.92	20.24	.6341	-.0099	.5541	-.2773	-.0307	-.0076

RUN 437   Q=210.40 PSF   RN/FT= 4.949   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
40.47	.10	.4001	.0074	.4731	-.0193	.0315	-.0005
50.82	.14	.6455	-.0039	.5895	-.1272	.0226	.0002
60.38	.12	.7380	-.0059	.5850	.0250	.0147	.0004
65.47	.15	.6846	.0049	.5830	.0046	.0067	.0003
70.35	.15	.6891	.0107	.5630	.0040	.0008	.0003
75.33	.15	.6902	.0133	.5269	.0120	.0005	.0002
80.36	.16	.6960	.0171	.4766	-.0159	-.0093	.0002
85.57	.16	.6981	.0230	.4363	.0399	.0000	.0000
90.89	.15	.7086	.0270	.3731	.0376	-.0047	.0001

RUN 438   Q=225.50 PSF   RN/FT= 5.072   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
80.36	-9.74	.6800	.0113	.4568	.0547	-.0064	.0022
80.39	-7.78	.7057	.0104	.4732	.0907	-.0002	.0017
80.36	-3.82	.6864	.0147	.4749	.0646	-.0107	.0009
80.36	.16	.6916	.0167	.4754	-.0191	-.0090	.0000
80.36	4.12	.7030	.0215	.4700	-.0499	-.0027	-.0006
80.31	8.09	.7077	.0197	.4003	-.0346	-.0080	-.0012
80.31	10.09	.7106	.0178	.3689	-.0368	-.0174	-.0014
80.36	15.05	.7355	.0090	.3461	-.1636	-.0386	-.0028
80.53	20.04	.7920	-.0092	.4678	-.1576	-.0316	-.0049
80.62	29.97	.7865	-.0275	.4677	-.3053	-.0470	-.0062

RUN 439   Q=227.90 PSF   RN/FT= 5.073   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
61.02	30.13	.8352	-.0250	.5817	-.3274	-.0846	-.0061
61.01	20.11	.8919	-.0113	.6205	-.0970	-.0387	-.0058
60.93	15.08	.8222	-.0020	.6189	-.0458	-.0032	-.0050
60.82	10.06	.7671	.0045	.6335	.0304	.0163	-.0042
60.78	8.07	.7507	.0046	.6477	.0671	.0178	-.0036
60.79	4.05	.7296	.0021	.6357	.1233	.0191	-.0022
60.38	.10	.7447	-.0047	.5862	.0233	.0138	.0003
60.64	-3.79	.6821	-.0011	.5607	-.1418	-.0068	.0025
60.77	-7.67	.7857	-.0035	.6035	-.2047	.0225	.0031
60.80	-9.72	.8191	-.0022	.6019	-.1690	.0320	.0035

RUN 440   Q=215.20 PSF   RN/FT= 4.913   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
40.60	-9.90	.5288	.0050	.3899	.1370	.0505	.0034
40.56	-7.86	.5261	.0079	.3600	.0939	.0504	.0018
40.52	-3.86	.4704	.0100	.3996	.0063	.0322	.0003
40.48	.17	.4022	.0073	.4760	-.0308	.0330	-.0006
40.52	4.20	.4486	.0114	.4517	-.0875	-.0097	-.0004
40.53	8.25	.5263	.0097	.3794	-.1286	-.0405	-.0020
40.54	10.29	.5273	.0055	.4083	-.1673	-.0422	-.0037
40.63	15.21	.5713	-.0011	.4733	-.2161	-.0368	-.0064
40.72	20.18	.6246	-.0126	.6267	-.1855	-.0112	-.0088
40.15	30.25	.7437	-.0394	.9272	-.3014	-.0193	-.0123

RUN 441   Q= 98.60 PSF   RN/FT= 2.254   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
40.21	.12	.3564	.0125	.4631	-.0255	.0201	-.0002
50.42	.15	.4581	.0097	.5275	.0256	-.0008	-.0007
60.22	.17	.5505	.0111	.5448	.0431	-.0127	.0005
65.04	.18	.6455	.0054	.5507	.0624	-.0053	.0006
69.94	.17	.6951	-.0003	.5511	.0160	-.0037	.0004
74.91	.18	.7295	.0027	.5097	-.0095	-.0138	.0000
79.94	.19	.7437	-.0016	.4805	.0181	-.0041	.0001
85.14	.18	.7306	-.0054	.4279	.0245	-.0019	.0002
90.55	.19	.7254	-.0023	.3800	.0195	-.0005	-.0002

RUN 442   Q= 92.10 PSF   RN/FT= 2.156   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
79.96	-9.75	.6597	.0032	.4797	.0757	-.0106	.0022
79.97	-7.77	.6606	.0049	.4704	.0162	-.0143	.0018
79.99	-3.85	.7381	-.0054	.4787	.0900	-.0083	.0010
79.98	.14	.7395	-.0021	.4796	.0176	-.0041	.0002
79.97	4.15	.7376	-.0010	.4823	-.0578	.0047	-.0010
79.97	8.17	.7415	-.0003	.4875	-.1287	.0101	-.0018
79.95	10.11	.7194	.0064	.4328	-.0063	-.0111	-.0013
79.94	15.05	.6998	.0027	.3856	-.1891	-.0384	-.0027
79.95	20.01	.6993	-.0018	.3525	-.2972	-.0485	-.0041
79.96	29.91	.6917	-.0121	.3658	-.3784	-.0356	-.0056

RUN 443   Q= 92.70 PSF   RN/FT= 2.155   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
60.34	30.00	.7554	-.0101	.5187	-.3154	-.0514	-.0063
60.32	20.06	.7890	-.0035	.5743	-.1566	-.0003	-.0058
60.31	15.10	.7544	.0049	.6366	-.1187	.0229	-.0052
60.31	10.07	.7440	.0068	.6396	-.0210	.0112	-.0032
60.28	8.08	.6810	.0117	.6129	-.0231	.0178	-.0025
60.23	4.14	.5789	.0158	.5856	.0125	.0152	-.0013
60.23	.15	.5637	.0090	.5429	.0612	-.0154	.0007
60.27	-3.78	.5784	.0160	.5851	-.0648	-.0295	.0019
60.32	-7.76	.6840	.0097	.6013	-.0443	-.0169	.0028
60.31	-9.79	.7029	.0076	.6127	.0059	-.0151	.0035

RUN 444   Q= 90.50 PSF   RN/FT= 2.123   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
40.24	-9.83	.4546	.0059	.4306	.0959	.0425	.0051
40.22	-7.80	.4654	.0104	.3539	.0909	.0513	.0020
40.19	-3.77	.4170	.0145	.3838	.0342	.0263	.0004
40.17	.22	.3474	.0117	.4625	-.0230	.0153	.0000
40.20	4.17	.4272	.0135	.3897	-.0670	-.0304	.0000
40.23	8.17	.4610	.0099	.3724	-.1133	-.0475	-.0027
40.23	10.19	.4467	.0075	.4234	-.1007	-.0316	-.0052
40.25	15.10	.4890	.0050	.4179	-.1315	-.0344	-.0073
40.35	20.06	.6365	-.0017	.4550	-.1607	-.0282	-.0075
40.33	30.08	.6137	-.0048	.3211	-.4004	-.0737	-.0088

RUN 445   Q= 14.70 PSF   RN/FT= .347   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
40.04	.15	.5647	.0291	.4062	-.1237	.0416	-.0023
50.24	.15	.7674	.0152	.5664	-.0423	.0130	-.0014
60.01	.16	.9535	.0005	.7483	-.0501	.0130	.0008
64.86	.15	1.0070	-.0171	.8265	-.1106	.0312	-.0005
69.69	.16	1.0271	-.0347	.8817	-.0909	.0616	-.0025
74.69	.15	1.0302	-.0370	.8676	-.0716	.0477	-.0022
79.68	.17	1.0038	-.0297	.7655	-.0966	.0458	-.0018
84.87	.15	.9388	-.0072	.5721	-.0881	.0199	-.0010
90.25	.15	.9300	.0087	.4623	-.0437	.0091	-.0008

RUN 446 Q= 14.50 PSF RN/FT= .345 MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
79.70	-9.76	.9537	-.0189	.6374	-.1629	.0016	.0029
79.69	-7.75	.9451	-.0171	.6281	-.1630	-.0018	.0027
79.70	-3.80	.9474	-.0184	.6653	-.0904	-.0015	.0011
79.70	.14	.9816	-.0290	.7560	-.0958	.0428	-.0021
79.69	4.09	.9422	-.0191	.6922	.0245	.0246	-.0022
79.68	8.06	.9583	-.0195	.6726	.0421	.0320	-.0040
79.68	10.07	.9532	-.0171	.6640	.0835	.0203	-.0045
79.69	15.05	.9006	-.0112	.6271	.1460	.0098	-.0053
79.69	20.01	.9332	-.0198	.6205	.0167	-.0312	-.0047
79.69	29.92	.8842	-.0251	.5231	-.3201	-.0508	-.0058

RUN 447 Q= 14.80 PSF RN/FT= .349 MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
60.00	29.93	1.0250	-.0339	.8898	-.3212	-.0338	-.0075
60.05	19.99	1.0737	-.0224	.9191	.1079	-.0323	-.0077
60.05	15.06	.9923	-.0197	.9272	.1966	.0040	-.0062
60.03	10.06	.9912	-.0232	.9119	.2153	.0306	-.0049
60.03	8.13	.9911	-.0282	.9107	.0670	.0167	-.0034
60.04	4.13	.9823	-.0181	.8172	.0495	.0294	-.0019
60.00	.14	.9502	-.0041	.7443	-.0611	.0138	.0003
60.01	-3.80	.9713	-.0088	.7553	-.0566	-.0155	.0009
60.02	-7.74	.9856	-.0210	.8846	-.1497	-.0141	.0029
60.01	-9.73	.9803	-.0258	.9258	-.1576	-.0011	.0038

RUN 448 Q= 14.70 PSF RN/FT= .348 MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
40.03	-9.75	.6248	.0051	.6655	-.0366	-.0098	.0065
40.02	-7.77	.5575	.0110	.5940	.0109	-.0109	.0060
40.00	-3.81	.4963	.0162	.4867	.0617	-.0246	.0043
40.05	.15	.5538	.0208	.4134	-.1190	.0390	-.0022
40.04	4.08	.5524	.0201	.4884	-.1194	.0555	-.0045
40.04	8.09	.6000	.0167	.5716	-.0331	.0327	-.0059
40.04	10.08	.6389	.0105	.6510	.0115	.0232	-.0066
40.05	15.05	.6902	.0049	.6158	-.0861	-.0097	-.0060
40.05	19.98	.7920	-.0106	.7477	-.0531	.0033	-.0080
40.07	29.92	1.0017	-.0336	1.1140	-.1206	.0567	-.0137

RUN 449 Q= 24.80 PSF RN/FT= .575 MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
40.07	.20	.4550	.0172	.4501	.0889	-.0150	.0008
50.24	.18	.7283	.0064	.5727	-.0735	.0146	.0005
60.08	.20	.8458	-.0087	.7441	-.1013	.0429	-.0009
64.88	.20	.9016	-.0143	.7568	-.0850	.0181	-.0012
69.78	.19	.9028	-.0139	.7305	-.1556	-.0126	.0003
74.72	.19	.9123	-.0165	.7166	-.1697	-.0208	.0012
79.78	.19	.9451	-.0166	.7080	-.1234	.0035	.0004
84.97	.17	.9267	-.0079	.5924	-.0821	.0009	.0001
90.35	.17	.9022	.0069	.4834	-.0563	.0239	-.0010

RUN 450   Q= 25.50 PSF   RN/FT= .589   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
79.75	-9.74	.9281	-.0200	.6386	-.1145	-.0204	.0034
79.75	-7.76	.9210	-.0179	.6375	-.0847	-.0325	.0032
79.75	-3.82	.9252	-.0160	.6621	-.1210	-.0308	.0023
79.74	.17	.9293	-.0178	.7067	-.1031	-.0051	.0002
79.78	4.12	.8581	-.0051	.6562	-.0146	.0383	-.0029
79.77	8.08	.8927	-.0096	.5939	.0380	.0227	-.0032
79.76	10.09	.9027	-.0122	.6116	.0147	.0212	-.0038
79.77	15.05	.8456	-.0103	.6734	.0363	.0311	-.0054
79.77	19.98	.8714	-.0134	.6810	-.0579	-.0034	-.0057
79.76	29.89	.8815	-.0254	.5275	-.2937	-.0553	-.0049

RUN 451   Q= 26.20 PSF   RN/FT= .597   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
60.07	29.91	.9677	-.0284	.8411	-.2655	-.0748	-.0062
60.09	20.02	.9077	-.0121	.8462	-.1765	-.0685	-.0063
60.05	15.04	.8221	-.0007	.8301	-.1543	-.0114	-.0060
60.04	10.09	.8087	-.0002	.7940	-.0376	.0018	-.0050
60.04	8.11	.8127	-.0023	.7680	-.0102	.0114	-.0042
60.05	4.13	.8306	-.0074	.7085	-.0559	.0321	-.0025
60.06	.19	.8323	-.0130	.7460	-.1014	.0387	-.0014
60.04	-3.77	.8678	-.0134	.7857	-.0855	-.0502	.0023
60.06	-7.73	.8695	-.0210	.9554	-.0883	-.0676	.0045
60.04	-9.74	.8700	-.0194	.9774	-.1324	-.0693	.0055

RUN 452   Q= 24.80 PSF   RN/FT= .581   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
40.08	-9.75	.5475	-.0018	.6301	-.0397	.0071	.0052
40.06	-7.75	.4862	.0057	.5491	.0323	.0140	.0041
40.04	-3.81	.4277	.0142	.4931	.0342	.0004	.0016
40.03	.15	.4341	.0133	.4549	.0661	-.0098	.0004
40.03	4.15	.5079	.0177	.4598	-.0123	-.0007	-.0017
40.07	8.08	.4974	.0125	.5714	-.0664	.0186	-.0056
40.07	10.10	.5257	.0096	.5610	-.0981	-.0144	-.0051
40.07	15.04	.5421	-.0003	.5251	-.2373	-.0715	-.0054
40.08	20.04	.6038	-.0082	.5782	-.2442	-.0849	-.0064
40.13	29.93	.9227	-.0279	.9936	-.0873	.0202	-.0122

RUN 453   Q= 55.90 PSF   RN/FT= 1.295   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_1
40.12	.18	.3353	.0131	.4692	-.0223	.0084	.0001
50.32	.17	.4302	.0125	.5447	.0029	-.0005	-.0003
60.14	.17	.6912	.0009	.5845	.0005	-.0011	-.0001
64.97	.16	.6993	.0011	.5710	.0006	-.0044	.0002
69.90	.16	.7381	.0014	.5692	-.0124	-.0069	.0001
74.79	.15	.7411	.0005	.5217	-.0087	-.0045	0.0000
79.87	.15	.7426	-.0046	.4849	.0128	.0059	0.0000
85.04	.16	.7459	-.0063	.4516	.0066	.0085	-.0005
90.44	.16	.7532	.0016	.4575	-.0372	-.0226	.0006

RUN 454   Q= 57.40 PSF   RN/FT= 1.335   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
79.86	-9.73	.7643	-.0037	.6437	.0916	-.0786	.0045
79.88	-7.74	.7811	-.0041	.6194	.0621	-.0772	.0040
79.84	-3.81	.7454	-.0043	.4971	.0783	-.0051	.0006
79.83	.16	.7470	-.0041	.4882	.0099	.0064	-.0004
79.82	4.18	.7445	-.0020	.5039	-.0679	.0280	-.0022
79.83	8.09	.7555	-.0020	.5531	-.1222	.0496	-.0038
79.83	10.10	.7609	-.0013	.5639	-.1643	.0488	-.0044
79.83	15.02	.7611	.0061	.5498	-.1076	.0232	-.0048
79.85	20.00	.7381	-.0052	.5889	-.2823	-.0184	-.0040
79.87	29.98	.7527	-.0121	.4606	-.3933	-.0861	-.0032

RUN 455   Q= 58.30 PSF   RN/FT= 1.347   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
60.18	30.00	.7335	-.0124	.5571	-.3059	-.0593	-.0051
60.20	20.03	.7740	0.0000	.6914	-.2658	-.0466	-.0047
60.19	15.06	.7550	.0025	.7188	-.1991	-.0121	-.0043
60.18	10.12	.7485	.0061	.6927	-.0477	.0033	-.0037
60.17	8.13	.7307	.0073	.6637	.0123	.0104	-.0033
60.16	4.14	.7257	.0040	.6126	.0507	.0118	-.0021
60.16	.16	.6899	.0014	.5793	.0151	.0007	.0001
60.19	-3.81	.6926	.0044	.5879	-.0084	-.0129	.0024
60.21	-7.81	.6834	.0096	.6390	.0204	-.0105	.0032
60.22	-9.76	.7087	.0073	.6732	.0302	-.0108	.0034

RUN 456   Q= 57.60 PSF   RN/FT= 1.339   MACH=0.20

ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
40.16	-9.79	.4804	.0057	.4333	.0428	.0405	.0036
40.13	-7.77	.4399	.0086	.4184	.0684	.0351	.0022
40.10	-3.82	.3647	.0142	.4517	.0836	.0047	.0010
40.11	.18	.3364	.0129	.4705	-.0157	.0068	.0002
40.13	4.14	.4034	.0130	.4304	-.0628	-.0177	-.0003
40.14	8.18	.4910	.0050	.4275	-.1007	-.0487	-.0018
40.15	10.14	.5081	.0011	.4799	-.0925	-.0457	-.0036
40.18	15.10	.6366	.0054	.4872	-.0033	-.0115	-.0064
40.20	20.04	.6746	.0018	.4980	-.1081	-.0098	-.0080
40.20	30.00	.6341	-.0097	.4785	-.2958	-.0790	-.0079

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16. Abstract

A 1/8-scale model of the X-29A airplane was tested in the Ames 12-Foot Pressure Wind Tunnel at a Mach number of 0.20 and Reynolds numbers of 0.13×10^6 to 2.00×10^6 based on a fuselage forebody depth of 0.4 ft.   For the test series presented herein, the angle of attack ranged from 40° to 90° and the angle of sideslip ranged from -10° to 30° for the erect attitude. Tests with the model inverted covered angles of attack from -40° to -90° and angles of sideslip from -30° to 10°.   Data were obtained for the basic design and for several forebody strakes.   An alternate forebody design was also tested.   The results provided information for selection of forebody strakes for compensation of Reynolds number effect on the 1/25-scale free-spinning model tested in the Langley Spin Tunnel.

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