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DEVELOPMENT OF COMPUTERIZED ANALYSIS FOR  
SOLID PROPELLANT COMBUSTION (ISAP-2)

NAG8-627

by

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## ABSTRACT

This report is an improvement to ISAP-1, "SRB Vorticity-Acoustic Coupled Instability Analysis", September, 1986.

Included in this report are the automatic generation of all input data for grid configuration, boundary conditions for coupled acoustic and vortical field calculations, transformation of all dimensions to a parametric form, resulting in flexibility for the user to define the size of the problem (geometric configurations) with reduction in storage (15-65%) and computer time (50-75%).

Additional research is required for the following areas:

- (1) effects of turbulence, (2) nonlinear wave oscillations, and
- (3) chemistry upon combustion instability.

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## I. INTRODUCTION

This report represents an improved version of "SRB Vorticity-Acoustic Coupled Instability Analysis - ISAP-1, September, 1986. The many basic changes to the original code include the automatic generation of all the input data for grid structure, boundary conditions, and coupling between the flow field and the acoustic/vortical field. In addition, all the dimensions in the program were transformed into a parametric form. These new parameters will enable the user to control the computer memory storage and the program execution time by specifying different sets of parameters and different geometric configurations. Also presented is the comparison between the results of the original program and those of the new one, along with recommendations to the user and additional research requirements.

As noted in the earlier report (ISAP-1), unstable waves may occur as a result of acoustic and/or vortical (hydrodynamic) oscillations. If these two different types of waves are coupled together, their physical interactions lead to extremely complicated phenomena. Theoretically, there exists an infinite number of frequencies for both acoustic and vortical oscillations. Realistically, however, only a limited number of combined frequencies are excited. Our objective is to determine the combined nature of acoustic and vortical frequencies at which instabilities may arise. This subject is important in rocket motor combustion chambers when the vortical field is coupled with

acoustic pressure oscillations. In the past, the acoustic combustion instability was studied independently of the vortical instability induced by vortex motions. This report is intended to combine the two different sources of energy everywhere within the spatial domain and to determine the effect of one upon the other. This can be achieved by calculating the mean flow velocities and vorticities and their fluctuating parts of velocities and vortices, as well as the fluctuating pressure.

To elucidate this coupling mechanism, the acoustic wave equation and the perturbed vortical transport equation are solved, being combined with the results of mean flow calculations from the Navier-Stokes system by means of finite elements. With these data, growth constants are calculated and stability boundaries determined. Contributions to stability and/or instability from various sources such as combustion, convection (flow turning), and viscous damping on propellant surfaces and energy convection, momentum convection, momentum viscous damping, and dissipative energy from the interior domain are separately identified. It is also found that stability boundaries for coupled acoustic and vortical oscillations are somewhat similar to the classical hydrodynamic stability boundaries, but they occur in the form of multiple islands.

## II. MESH GENERATION

In the original version of the program, the input data was read externally, and this procedure required extensive preparation for any changes in the input constants and/or the configuration of the field. This process is complex and time consuming. Consequently, a mesh generation routine is added to the program.

The program has two major parts: (1) the flow field calculations and (2) the acoustic and vortical calculations from which the stability integrals and growth constants are derived. Therefore, a complete set of input data is required for each part.

### A. Flow Field

The flow field calculations include velocities and pressure with grid configurations coarser than those in ISAP-1. Figure 1a shows the original grid in ISAP-1. It is apparent that the element sizes are smaller near boundaries (4), (5), and (6) in Fig. 2, but these reductions were set arbitrarily. The mesh generation routine has a much better approach. It reduces the grid size logarithmically near the same boundaries. This will enhance the flexibility of the program. The generated arrays are the following:

- (a) NENN - the element connectivity matrix; it sets the global nodal values of the nodes of each element.
- (b) XX, YY - the coordinates of each global node.



- (c) NU, NV, and ND - the global nodes for the Dirichlet boundary condition adjustment for the U, V velocities and pressure, respectively.
- (d) UB, VB, and PB - the boundary values associated with NU, NV, and ND, respectively.
- (e) UU, VV, PP - the velocities in the x-direction, y-direction, and the pressure, respectively.

#### B. Acoustic and Vortical Field

This is the smaller grid shown in Fig. 2b,d. The two grids are interconnected through the ICON matrix. Again this connectivity was previously set arbitrarily. While in the mesh generation routine, the new grid is set through ICON, such that the distances between the nodes at each boundary are as equal as possible. The arrays for this field are:

- (a) NENL - the element connectivity matrix for the smaller grid.
- (b) ICON - the interconnectivity matrix between the flow field and the acoustic/vortical field.
- (c) NODE - the adjustment matrix for the boundary conditions in the computation of vortical modes.
- (d) FFNX, FFNY - the direction cosines at the boundaries in the x and y directions, respectively.
- (e) NBQ - the number of elements at each boundary.
- (f) ABN, ANN - the admittance at the burning surface and nozzle, respectively.
- (g) NC - the connectivity matrix of the boundary elements.

### C. Initial and Flow Constants

For each problem, there are some basic constants that are needed to define it. They deal with the geometry, flow properties, error, time-step, and convergence parameters. Many of these constants, such as REN, GAMMA, DT, ERROR, ITMAX, and NPT, have already been defined in the original report. In order to enhance the flexibility of the program, a few additional constants dealing with the geometry of the problem were utilized in the mesh generation routine. They are the following:

- (a) XMIN, XMAX, YMIN, YMAX - the limiting values of the domain.
- (b) X0, Y0 - the coordinates of the corner node (see Fig. 1).

These geometric values must be redefined by the user every time the configuration of the problem changes.

### III. PARAMETRIC DIMENSIONS

The original program was bounded by a set of fixed parameters which controls the memory storage requirements. For the flow field, the program used 832 grid points and 767 elements; for the acoustic/vortical field, it used 40 grid points and 27 elements.

In order to make the programs more flexible, parametric dimensions were added. This addition will allow the user to choose the memory storage needed for different executions. This procedure requires the definition of the parameters and the respective arrays.

#### A. Parameters

A total of 10 parameters is needed to maximize the flexibility of the program. All but two of these parameters are geometric; they will generate both grids. Of the remaining two parameters, one is fixed and the other is floating (not fixed).

##### (a) Geometric Parameters:

Four parameters are needed for each grid.

##### 1. Flow field:

The four parameters, shown in Fig. 2, are defined as follows:

- NELF1 - the number of boundary elements above the corner node in the y-direction.
- NELF2 - the number of boundary elements below the corner node in the y-direction.

NETP1 - the number of boundary elements left of the corner node in the x-direction.

NETP2 - the number of boundary elements right of the corner node in the x-direction.

## 2. Acoustic/vortical field:

The four parameters associated with this field are similar to those of the flow field with their respective positions.

NALF1, NALF2, NATP1, and NATP2 are the number of elements on boundaries (5), (1), (6), and (4), respectively (see Fig. 2).

### (b) Floating Parameter:

The parameter MI is affected by other parameters and constants and is a direct result of the calculations. In the original code, the value of MI was set at 65. However, this value can be much lower (see Table 3).

From the program, the needed value of MI is augmented for each St (Strouhal number)  $\geq .01$ . Those values of St  $< .01$  will produce oscillations which are negligible relative to the acoustic oscillations and, therefore, are eliminated to avoid unnecessary calculations. As the Reynolds number increases, the vortical oscillations expand further in the field, resulting in higher values of St at additional nodes; therefore, the needed value of MI will increase.

However, in order to limit the memory storage requirements, MI must be minimized. This procedure will be achieved by changing MI relative to the changes in REN and the geometric parameters (see Section V for the recommended values of MI).

(c) Fixed Parameter:

The parameter NBP, which is always equal to 6, represents the 6 boundaries of the domain. It must be noted that the remaining parameters are derived directly from the 10 preset parameters already defined.

B. Arrays

The size of all the different arrays can be set either by a DIMENSION statement or by a COMMON block. When the parameters were added to the program, two other steps had to be taken:

- (1) All the COMMON blocks were eliminated from the code. This step required a change in the way the subroutines are called, by including all the variable arrays that were otherwise included in the COMMON statements.
- (2) All the arrays must be referenced in the MAIN program. This step was required because the dimensions of all the arrays are generated in the PARAMETER statements in the MAIN program.

#### IV. COMPARISON OF RESULTS

The computer memory storage and the execution time are the important outcome of this study. Therefore, to compare these effects, the results will be displayed in two ways: (1) by comparing the original code and the revised code and (2) by comparing the original grids' results with those of the reduced ones.

First of all, the basic assumptions and flow constants are presented:

1. The Reynolds number,  $REN = 10^3, 10^4, 10^5$  for different runs.
2. The specific heat ratio,  $GAMMA = 1.2$ .
3. The time step for the calculation of the mean flow field,  $DT = 1$ .
4. The convergence error for mean flow,  $ERROR = .001$ .
5. The maximum number of iterations for flow field calculations,  $ITMAX = 30$ .
6. The domain of calculations:  $XMIN = 0, XMAX = 10, YMIN = 0, YMAX = 1.5$ .
7. The corner node coordinates:  $X0 = 2, Y0 = 1$ .
8. Boundary and initial conditions: With reference to Fig. 1, burning takes place only on boundary (6); therefore, an instantaneous flux normal to this boundary appears at time  $T = 0$ . Then, the velocity in the negative y-direction is set at a dimensionless value of  $v = -.01$ , only at the nodes of boundary (6), and excluding the end points of this boundary. All other flow variables are set equal to zero

everywhere in the domain. (The value of  $-.01$  was taken from the original code and is a function of the burning rate at the surface of the solid fuel).

9. The normal vectors at the boundaries: At boundaries (1) - (6), the values of the normal vectors are  $FFNX = 1., 0., 1., 0., 1., 0.$ ;  $FFNY = 0., 1., 0., 1., 0., 1.$ , respectively.
10. Admittance: Only at the burning surface (boundary 6),  $ABN = 1.$ ; otherwise, it is equal to zero. Only at the nozzle (boundary 3),  $AAN = 1.$ ; otherwise, it is equal to zero.

These assumptions and flow constants were kept fixed (except for  $REN$ ) throughout the calculations. Now, we can proceed to the comparison of the results.

#### A. Original Grids

It is clear that with the original grids (ISAP-1), the storage required to generate the data in the revised code will exceed the storage needed to read the data from an outside source. Therefore, the total memory requirements for the revised code exceed that of the original code by about 2%.

Concerning the run time requirements, on the other hand, the revised code used about 2% less time than that of the original code, even though it went through 5 additional values of Strouhal numbers, i.e., vortical calculations (see Table 1).

NOTE: The value of  $MI$  has been defined earlier, but this value is also dependent on the systems on which these programs are running. The original code gave a value of  $MI = 15$  on the IBM

3084 and a value of  $MI = 16$  on the UNIVAC. This phenomenon is a result of the eigenvalue solver routine. This routine is very sensitive to any small variations in its input data. To eliminate the sensitivity problem, these codes should be transformed to operate in double-precision, while reducing the ERROR value and increasing ITMAX. These new additions will increase the storage requirements and run time by over 50%.

The flow field results, as shown in Fig. 3, prove that the revised code presents the same exact flow field as that of the original code. In the figure, the original code results are displayed in the upper half of each section for (a) the pressure, (b) the velocity in the x-direction, and (c) the velocity in the y-direction. These results were expected because of the linearity of the solution. However, the difference between the values of MI was not expected to be as large.

Even though the revised version of the program made it more flexible and easy to operate, it still has not made any major contribution to reduce the memory requirements nor the necessary run time. Therefore, we will present the other aspects of possible improvements which reduce the memory storage and run time. But, as we will see, they will slightly affect the computational results.

## B. Reduced Grids

As a part of the flexibility of the revised code, the user has the option of changing the number of nodes and elements used in the program. Figure 1 shows the different grids used for



comparison purposes. The number of nodes and elements are tabulated in Table 2. As seen in Table 2, if the number of elements at the boundaries is reduced by 1/4, the total number of nodes and elements is reduced by about 1/2. As a result of the reduced grids, the required memory storage and run time will definitely be reduced. Then, there is a need to find what percentage reduction is achieved and how it will affect the results.

Table 3 shows the different reductions achieved for required memory and run time at different Reynolds numbers. The storage requirement is reduced by 14% and 66% with coarser grids for the flow field and the flow and A/V fields, respectively, while the execution time is reduced between 56% and 76%. From these values, we can conclude that the flow field calculations affect mostly the run time required, while the acoustic/vortical (A/V) field affects the storage size of the program. On the other hand, the computational results of such reductions are slightly affected. Figures 4-6 show the flow field variables for the reduced grid (the lower part of each section), as compared to the original grid, for  $Re = 10^3$ ,  $10^4$ , and  $10^5$ , respectively. The difference between the results becomes more obvious as  $Re$  gets larger. Consequently, at high values of the Reynolds number ( $Re$ ), the coarse mesh does not produce accurate results.

## V. RECOMMENDATIONS

Two types of recommendations are necessary to conclude this report: (1) those directed towards the users of the program and (2) those needed for a more realistic modeling of the problem at hand.

### A. To the user:

- (1) **Grids:** This program does not contain a turbulent flow model to accommodate for the higher values of  $Re$ . Also, there is a limit, in reducing the grids, at which the results would become insignificant. Therefore, a coarse mesh, such as (6, 9, 13, 20), may be used at  $Re \leq 10^3$ ; but, at higher values of  $Re$ , a more refined mesh is needed. Recommended values for the parameters:  $NELF1 \geq 6$ ,  $NELF2 \geq 9$ ,  $NETP1 \geq 13$ ,  $NETP2 \geq 20$ ,  $2 \leq NALF1, NALF2, NATP1, NATP2 \leq 4$ . It is imperative that the last 4 parameters be  $\geq 2$ ; otherwise, the calculations will become senseless.
- (2) **The value of MI:** As stated earlier, the needed value of MI is calculated within the program. The maximum allowable value of MI is equal to the number of A/V modes:  $MI_{max} = NT$ . In order to control the memory storage requirements, MI can be specified smaller than NT. As shown in Table 3, the needed values of MI increase as the Reynolds number increases.

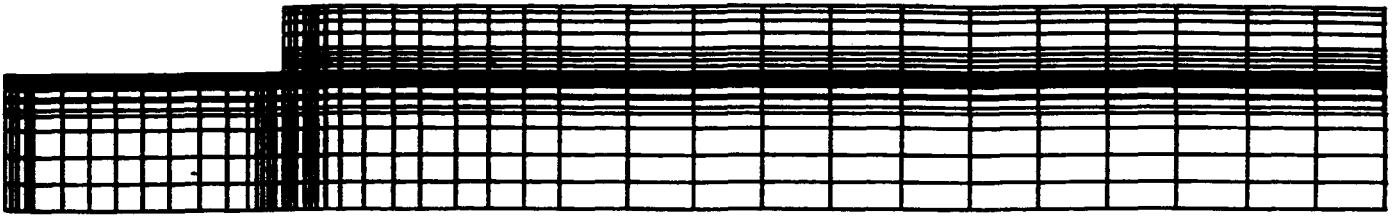
Therefore, it is recommended that the user adjust the value of MI, as needed, to correspond with the values of the Reynolds

number and the appropriate geometric parameters. The recommended values of MI are:  $MI_{(needed)} < MI \leq NT$ , where  $MI_{(needed)}$  are the values listed in Table 3.

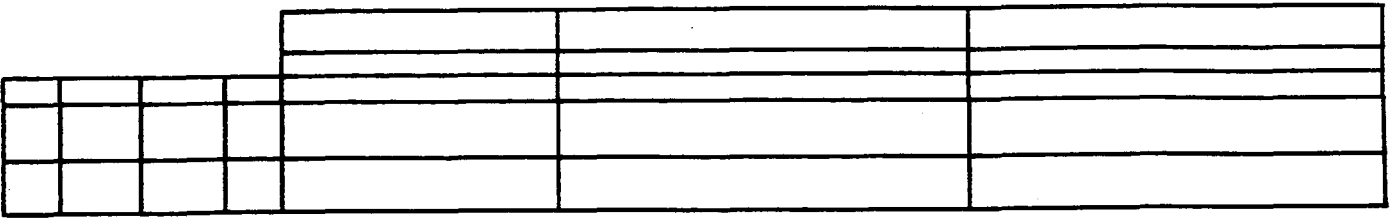
B. Additional Recommendations:

There are many areas where this program can be improved, some of which can be done in the near future, others will be the topics of further study and research.

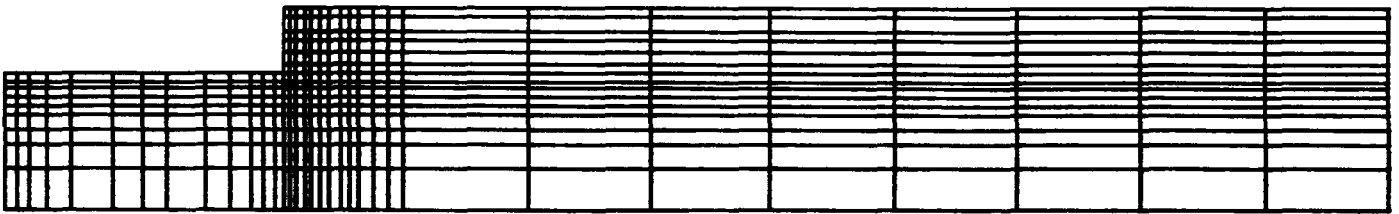
- (1) Double precision, smaller DT, smaller ERROR, and larger ITMAX: these extra steps are needed for accuracy and to avoid the sensitivity in the eigenvalue solver.
- (2) Turbulent model: this model will be used for the relatively high values of Re.
- (3) Higher order approximations of the pressure and the vorticity.
- (4) The study of the effect of compressibility.
- (5) The addition of chemistry to the model by adding the species and energy equations.



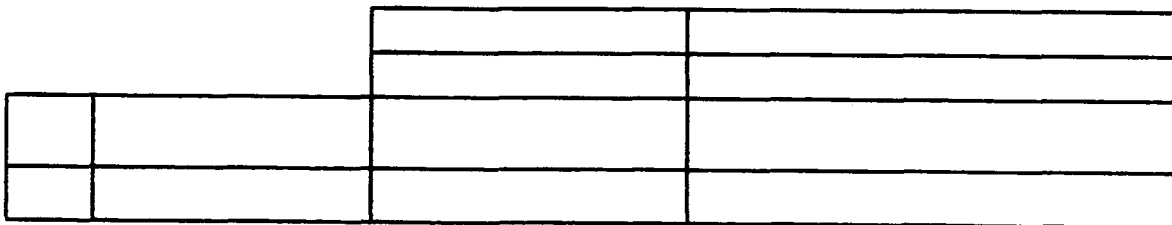
(a)



(b)



(c)



(d)

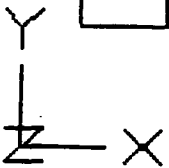


Fig 1. The grids: a) for the original flow calculations, b) for the original A/V calculations, c) for the reduced flow calculations, and d) for the reduced A/V calculations.

NELF1, NALF1  
 NELF2, NALF2

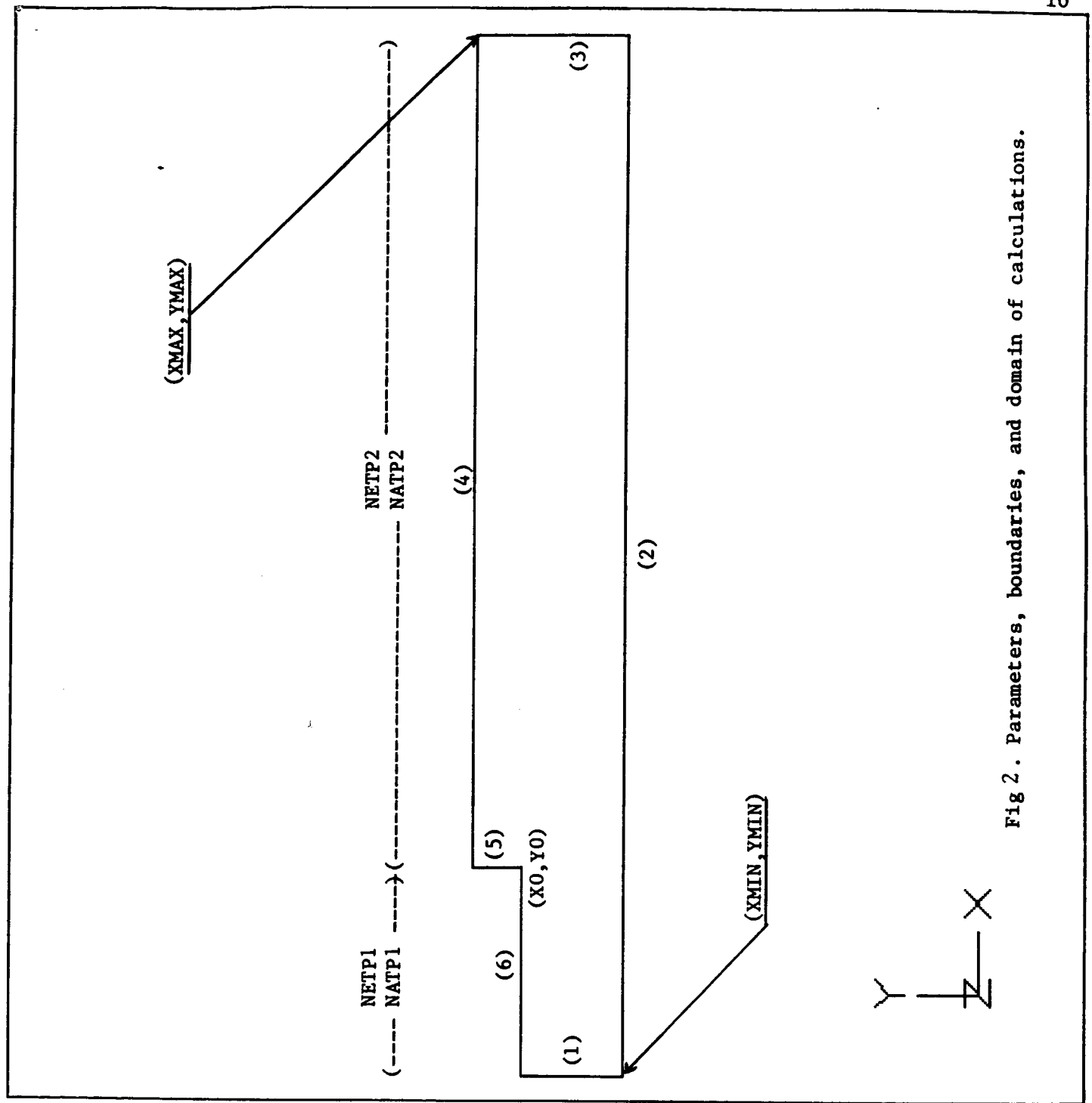
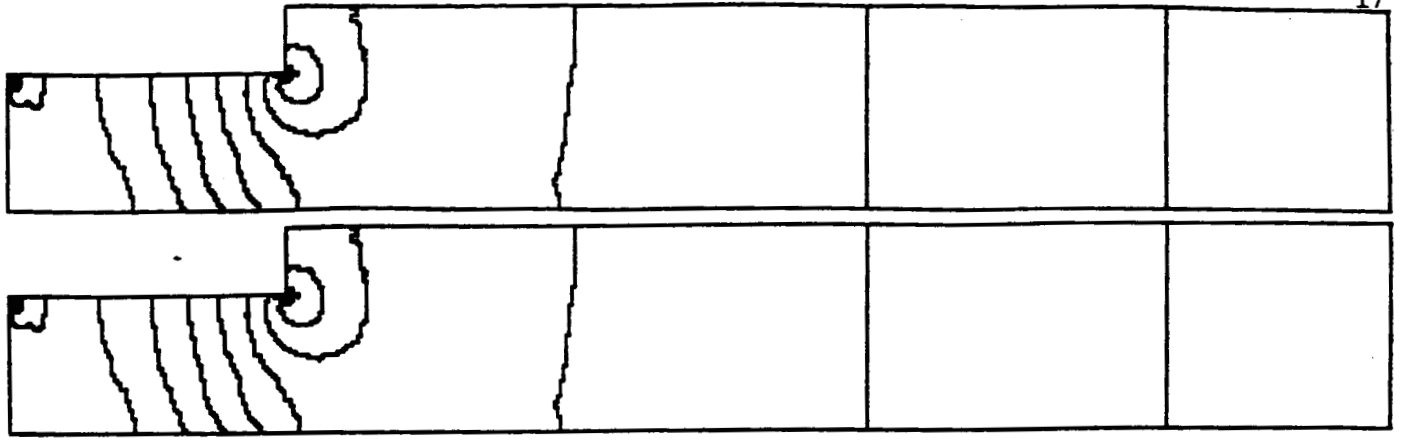
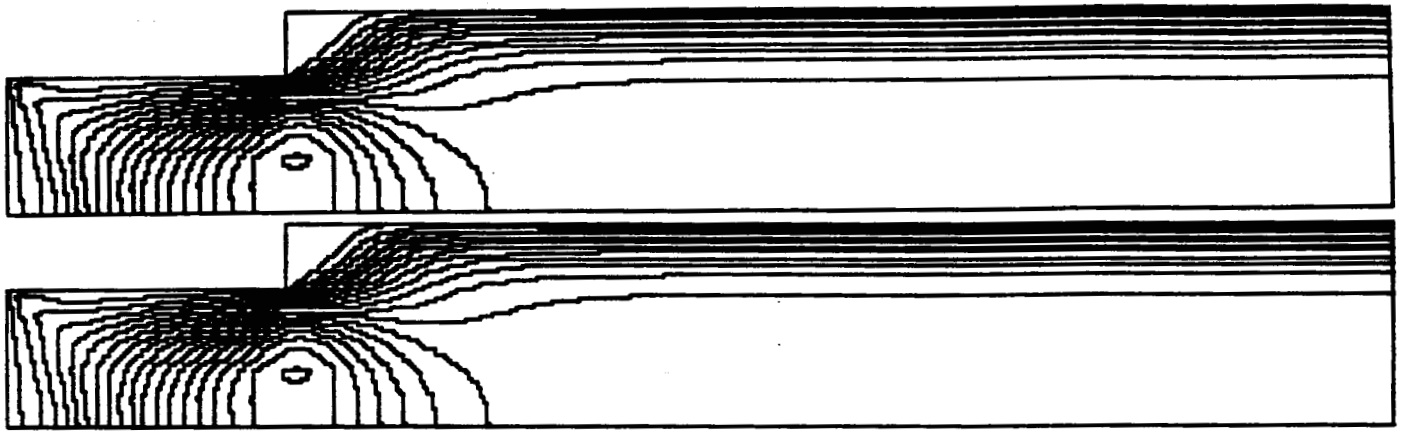


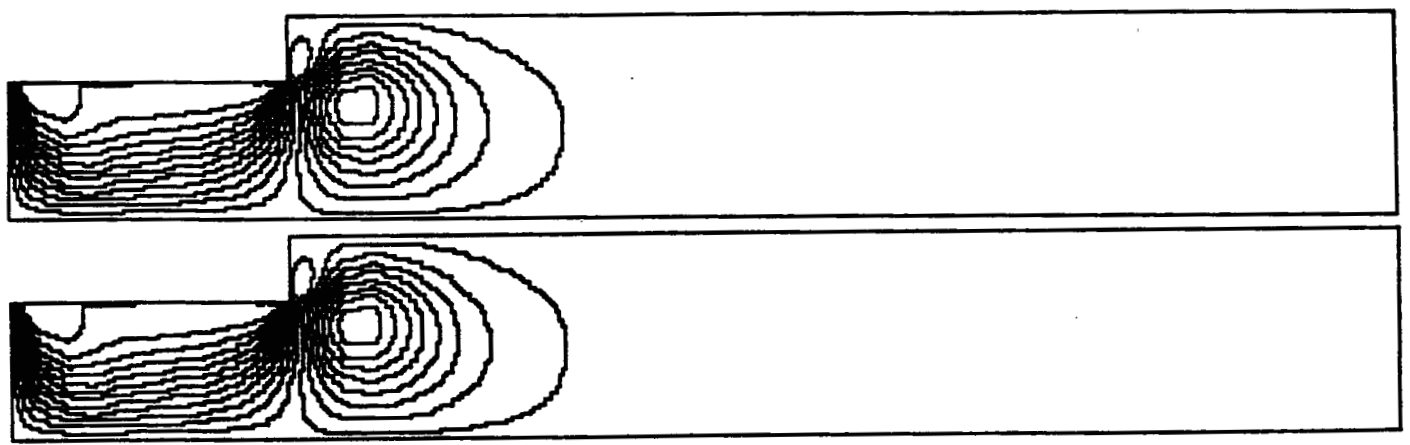
Fig 2. Parameters, boundaries, and domain of calculations.



(a)

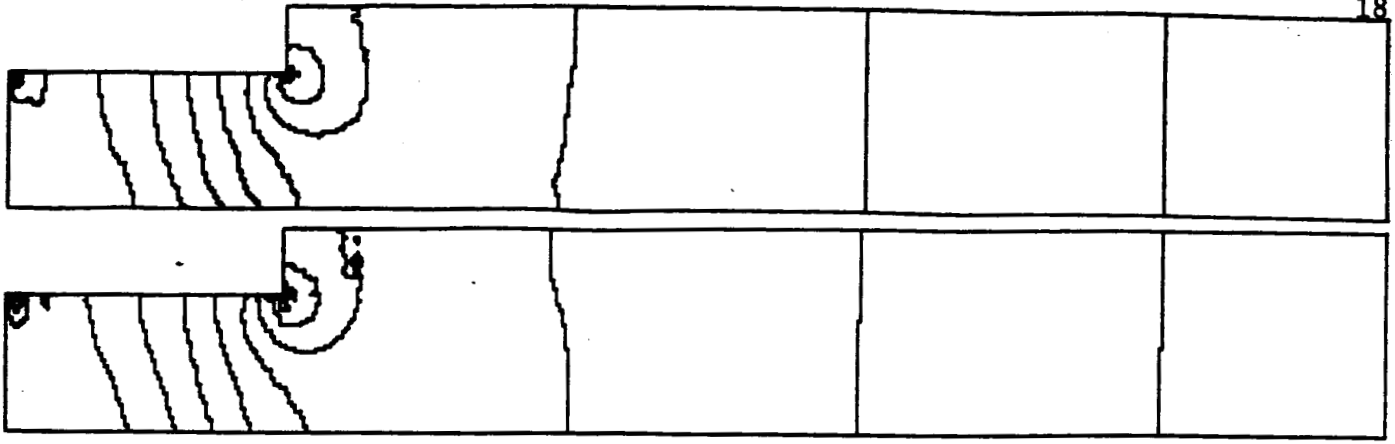


(b)

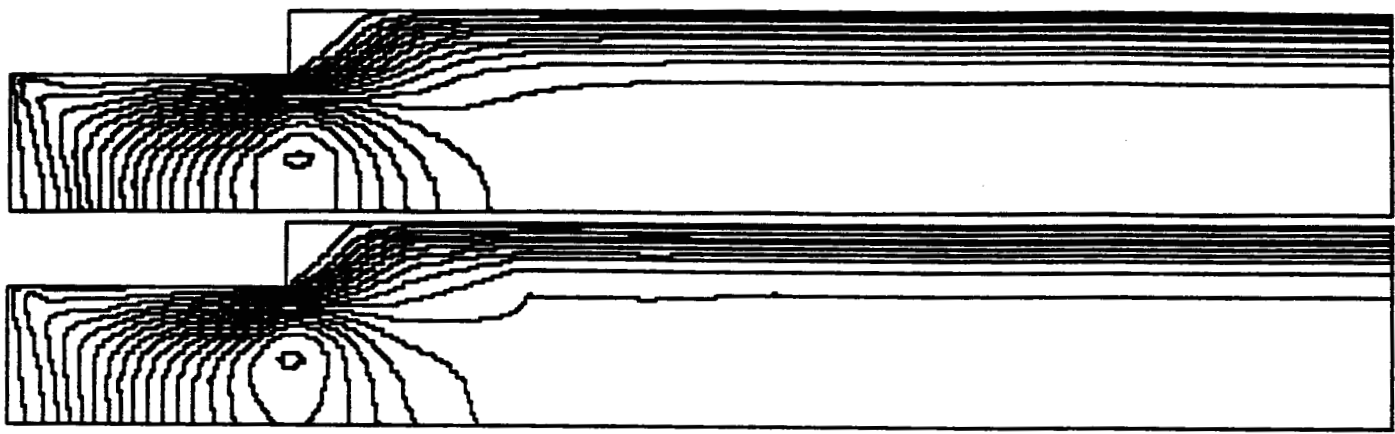


(c)

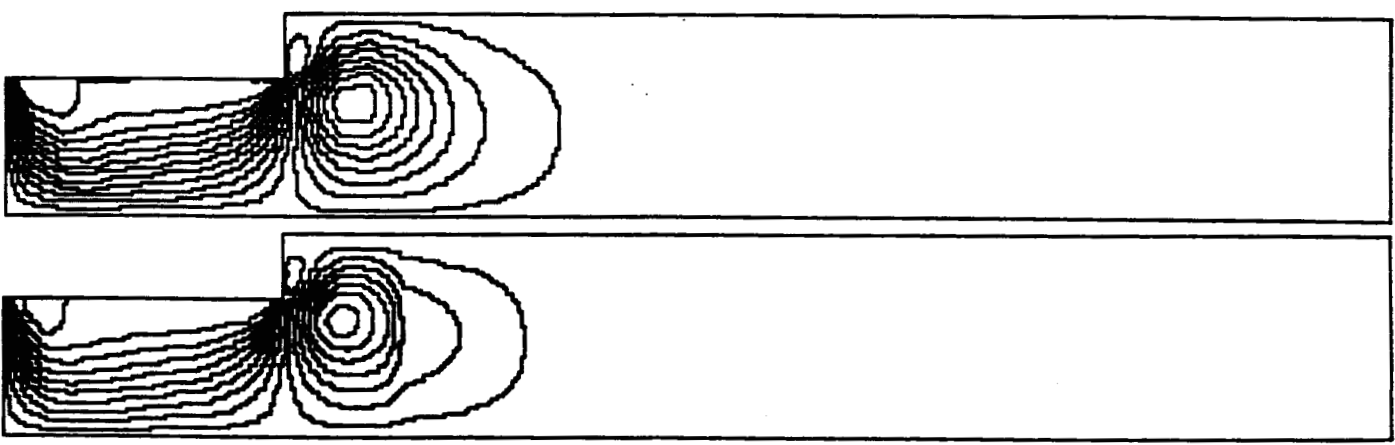
Fif 3. Comparison between the flow field results of the original code (upper part) and those of the revised code (lower part), for (a) the pressure, (b) the U-velocity, and (c) the V-velocity. (Re=1000.)



(a)

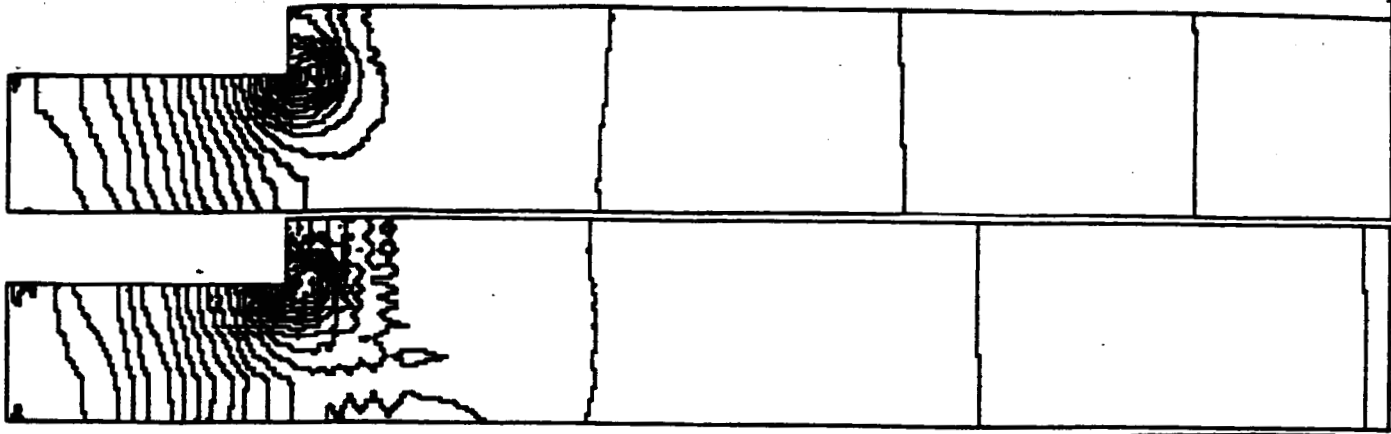


(b)

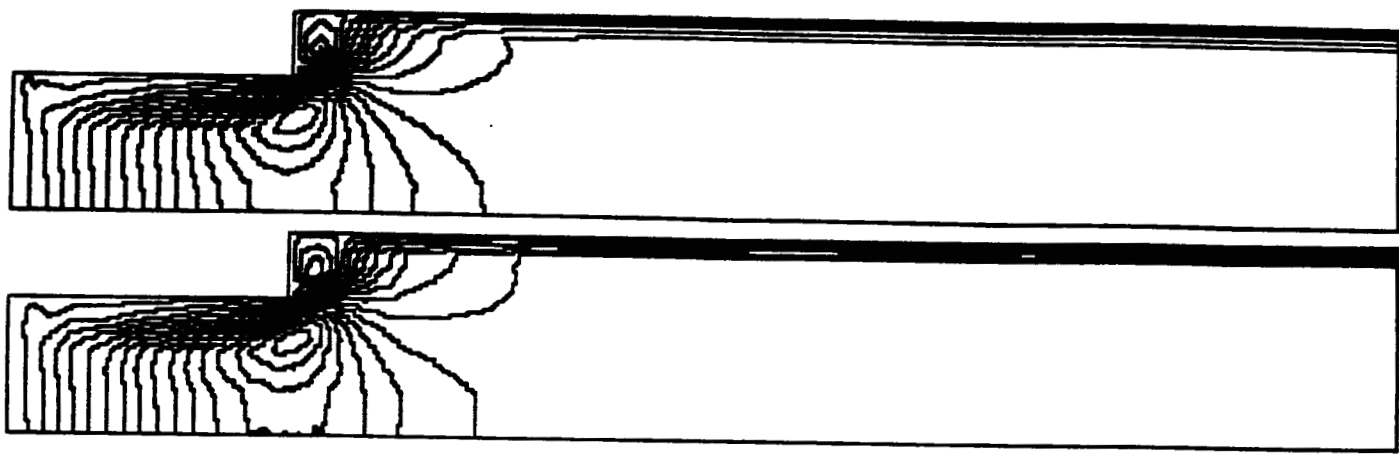


(c)

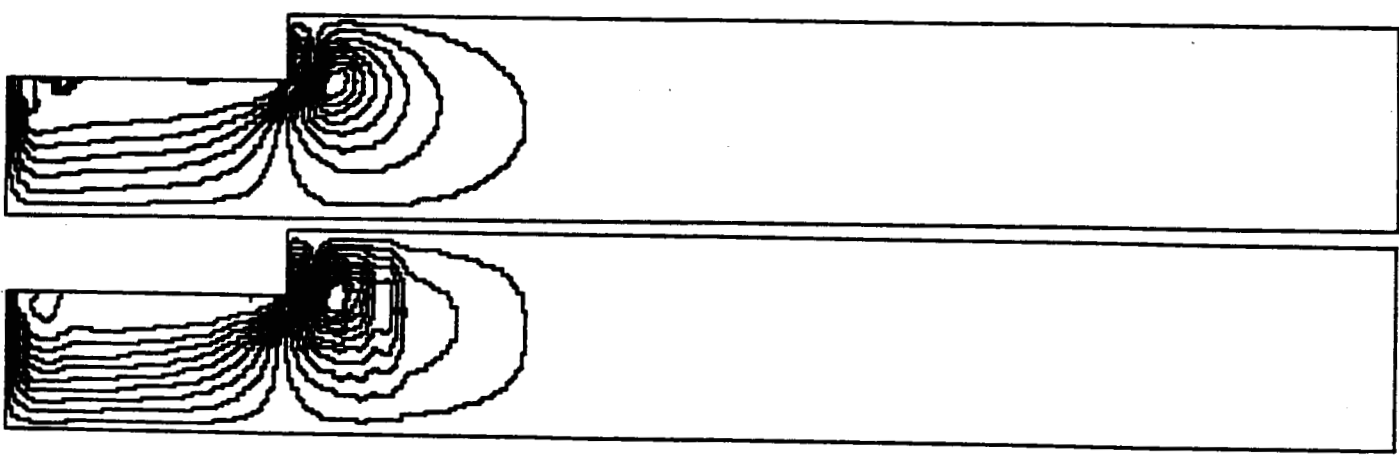
Fig 4. Comparison of the flow field variables between the original mesh (upper part) and the reduced mesh (lower part) : (a) the pressure, (b) the U-velocity, (c) the V-velocity;  $Re = 1000$ .



(a)



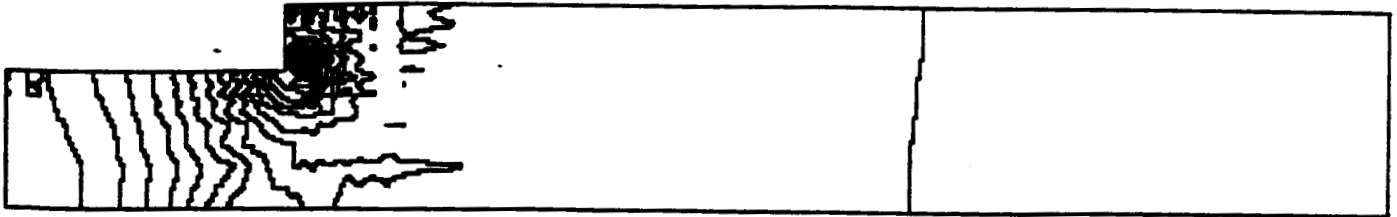
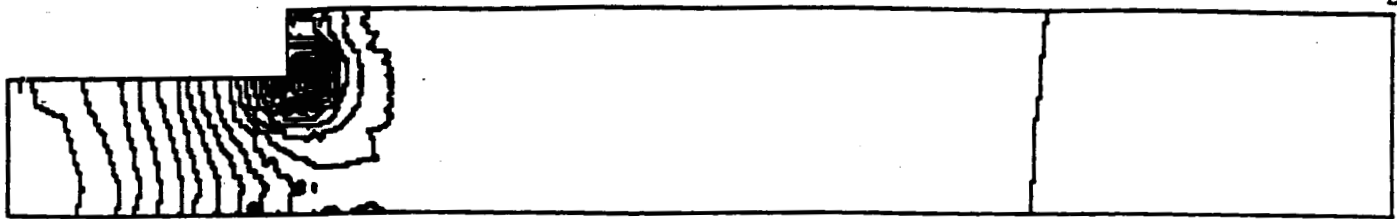
(b)



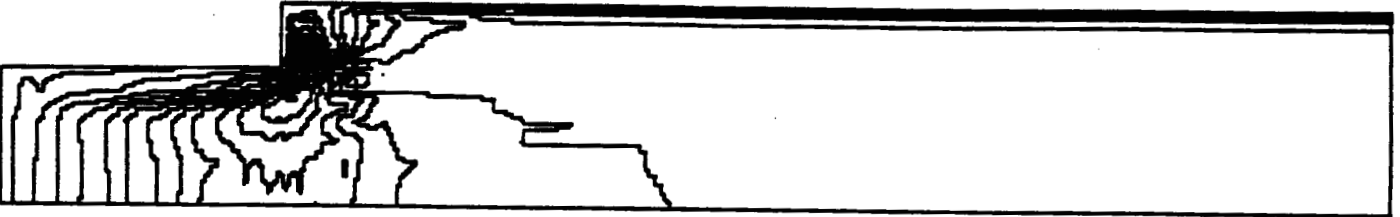
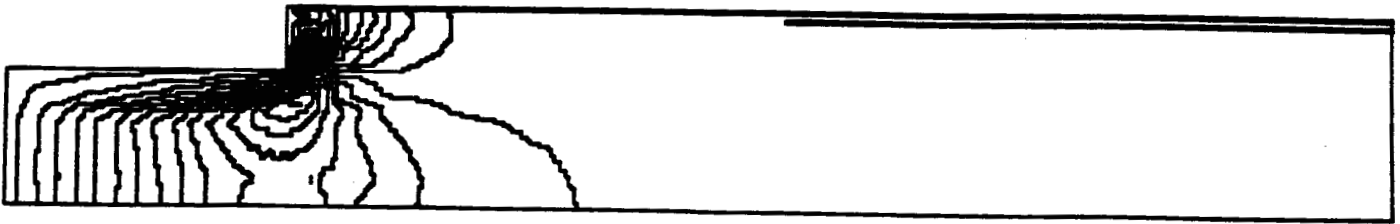
(c)

Fig 5. Comparison of the flow field variables between the original mesh (upper part) and the reduced mesh (lower part) : (a) the pressure, (b) the U-velocity, (c) the V-velocity;  $Re = 10000$ .

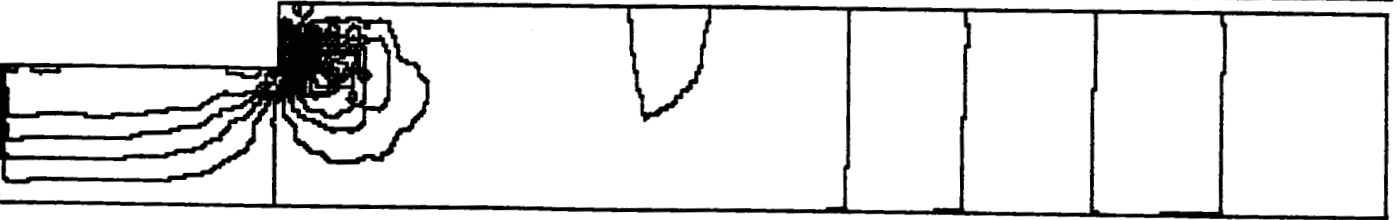
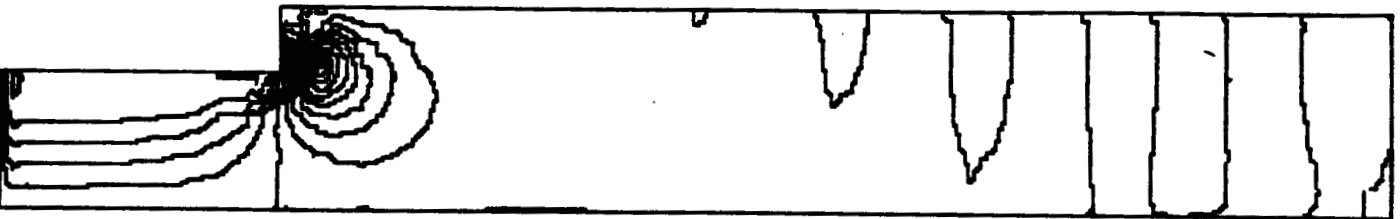




(a)



(b)



(c)

Fig 6. Comparison of the flow field variables between the original mesh (upper part) and the reduced mesh (lower part) : (a) the pressure, (b) the U-velocity, (c) the V-velocity;  $Re = 100000$ .

Table 1. Comparison between the storage and runtime of the original code and the revised one, at  $Re = 10^3$ .  
(original grids)

	Memory Requirement Bytes	Fraction of the original	Run-time (UNIVAC) min	Fraction of the original	MI (needed)
ORIGINAL	3023004	1	226	1	16
REVISED	3109452	1.02	223	.98	21

Table 2. The reduced grids.

		Parameters	No. of Nodes	No. of Elements
Flow Field	Original	(8,13,17,26)	832	767
	Reduced	(6,9,13,20)	466	417
A/V Field	Original	(2,3,4,3)	40	27
	Reduced	(2,2,2,2)	21	12

Table 3. Storage and run-time comparison between the original grids and the reduced ones. (MI was set at 65 as an initial assumption).

	Re	Memory Requirement Bytes	Fraction of the Original	Run-time (UNIVAC) min	Fraction of the Original	MI (needed)
Original GRID	$10^3$	3109452	1.	223	1.	21
	$10^4$	3109452	1.	240	1.	30
	$10^5$	3109452	1.	242	1.	33
Flow field reduced (only)	$10^3$	2682808	.86	80	.358	19
	$10^4$	2682808	.86	100	.420	27
	$10^5$	2682808	.86	105	.434	33
Flow & A/V fields reduced	$10^3$	1077816	.34	52	.233	7
	$10^4$	1077816	.34	64	.267	12
	$10^5$	1077816	.34	65	.270	14

APPENDIX

Listing of the Revised Code.

MAIN2

DATE: 87/09/24  
TIME: 12:02  
PAGE: 01 OF 50

MEMBER: MAIN2  
LEVEL: 01.00  
USERID: CTJC197

PROJECT: CTJC197  
GROUP: STB1  
TYPE: FORT

START COL 1-----2-----3-----4-----5-----6-----7-----8

1 C PROGRAM ISAP1  
1 C VIRTUAL A,A2,B,B2,C,CZ22,D,SI,SR  
1 C VIRTUAL PAA,PAH,PAT,UUI,UUR,VVI,VVR  
1 C PPROGRAM FOR SRB VORTICALLY-COUPLED COMBUSTION INSTABILITY  
1 C ANALYSIS BY FINITE ELEMENTS

7 PARAMETER (NELF1=6,NELF2=9,NETP1=13,NETP2=20)  
1 PARAMETER (NELF1=8,NELF2=13,NETP1=17,NETP2=26)  
1 C PARAMETER (NALF1=2,NALF2=3,NATP1=4,NATP2=3)  
1 C PARAMETER (NALF1=2,NALF2=2,NATP1=2,NATP2=2)

7 PARAMETER (MI=65,NC1=20,NBP=6,  
6 &NERGT=NELF1+NELF2,NEBOT=NETP1+NETP2,  
6 &NEL=NETP2\*NERGT+NETP1+NELF2,NBO=2\*NERGT+7,  
6 &NARGT=NALF1+NALF2,NABOT=NATP1+NATP2,  
6 &NPT1A=(NALF2+1)\*NATP1,NPT2A=(NATP2+1)\*(NARGT+1),  
6 &NL=NATP2\*NARGT+NATP1\*NALF2,NT=NPT1A+NPT2A,MII=4\*NT,  
6 &NT1=NT-NALF1-NALF2-NATP2-2,NTT=3\*NT1+NT,  
6 &NPT1=(NELF2+1)\*NETP1,NPT2=(NETP2+1)\*(NERGT+1),  
6 &NGPT=NPT1+NPT2,NDP=NERGT+1,  
6 &NUX=NELF1+NELF2+NETP1+NETP2+3,NVY=NUX+NDP+NEBOT+1)

1 C DIMENSION NENN(NEL,4),NENL(NL,4),ICON(NT),NC(NBP,NC1,2),FRE(NT),  
6 &PRESS(NT,NT),FVE(MI),UUR(NT,MI),UUI(NT,MI),VVR(NT,MI),  
6 &VVI(NT,MI)  
7 DIMENSION NBN1(NELF2+1),NBN2(NELF1+NETP1+1),NBN3(NETP2+1),  
6 &NBN4(NERG+1),NBN5(NEBOT+1)

1 C DIMENSION NODE(NTT),NBQ(NBP),FFNX(NBP),FFNY(NBP),ABN(NBP)  
7 DIMENSION ANNI(NBP)  
7 DIMENSION XI(NT),YT(NT),UT(NT),VT(NT)  
11 DIMENSION NU(NUX),NV(NVY),ND(NDP),UB(NUX),VB(NVY),PB(NDP)  
11 DIMENSION XX(NGPT),YY(NGPT),UU(NGPT),VV(NGPT),PP(NGPT)  
11 DIMENSION PFR(NT),PFV(MI),PAA(NT,MI),PAH(NT,MI),PAT(NT,MI)  
7 DIMENSION US(NGPT),VS(NGPT),DPP(NGPT),DELU(NGPT),DELV(NGPT),  
6 \*A(NGPT,NBO),B(NGPT,NBO),FU(NGPT),FV(NGPT),TARR1(NT),  
6 \*ITER(NT),SR(MII,NTT),SI(MII,NTT),FV1(MII),ITER2(NTT)  
7 COMPLEX A1(NT,NT),B1(NT,NT),CZ1(NT,NT),EIGAV(NT),EIGBV(NT),  
6 \*EIGV(NT),A2(MII,MII),B2(MII,MII),C(NTT,NTT),D(NTT,NTT),  
6 \*CZ22(NTT,NTT),EIGAV2(NTT),EIGBV2(NTT),EIGV2(NTT)

1 C DATA XMIN,XMAX,YMIN,YMAX/O..10..O..1.5/  
7 DATA XO,YO/2..1.1/

7 REN=1000.  
7 GAMMA=1.2  
7 DT=1.  
7 ERROR=.001  
7 ITMAX=30  
7 NPT=4

1 C  
1 C

ORIGINAL FILE IS  
OF POOR QUALITY

PROJECT: CTJJC197  
GROUP: STB1  
TYPE: FORT

MEMBER: MAIN2  
LEVEL: 01.00  
USERID: CTJJC197

DATE: 87/09/24  
TIME: 12:02  
PAGE: 02 OF 50

START COL 1-----2-----3-----4-----5-----6-----7-----8

CT=SPEED OF SOUND(IN/SEC)/CHARACTERISTIC LENGTH(IN)

CT=40000.0/24.0

INPUT DATA

CALL DINPUT(NELF1,NELF2,NETP1,NETP2,NALF1,NALF2,  
&NATP1,&NATP2,NERGT,NERGT,NAROT,NAROT,NPT1A,NPT1,  
&NEL,NGPT,NPT,NBW1,NBW1,NBW1,NVY,NDP,NBP,NTT,NODE,  
&NENN,NENL,ICON,NC,NBN1,NBN2,NBN3,NBN4,NBN5,NT1,NC1,  
\* XMIN,XMAX,YMIN,YMAX,XO,YO,  
\* NBO,XX,YY,UU,VV,PP,NU,NV,ND,UB,VB,PB,FFNX,  
\* FFNY,ABN,ANN,REN,GAMMA,DT,ERROR,ITMAX,NL,NT)

COMPUTATION OF MEAN FLOW FIELDS

CALL VELOT(NEL,NGPT,NPT,NBW1,NBW1,NBW1,XX,YY,UU,VV,PP,REN,DT,ERROR,  
\* NENN,ICON,XT,YT,UT,VT,NBO,US,VS,DPP,DELU,DELV,FU,FV,  
\* A,B,NUX,NVY,NDP,NU,NV,ND,UB,VB,PB,NT,ITMAX)

COMPUTATION OF ACOUSTIC MODES

CALL EIPRE(NL,NT,NPT,NENL,FRE,PRESS,  
\* XT,YT,TARR1,A1,B1,CZ1,EIGAV,EIGV,EIGV,ITER)

IF(NEL1.GT.1)GOTO 100

COMPUTATION OF VERTICAL MODES

CALL EIVOR(NL,NT,NPT,REN,NTT,NODE,MVP,MI,MI1,  
\* SR,SI,FV1,A2,B2,C,D,CZ2,EIGAV2,EIGBV2,EIGV2,ITER2,  
\* NENL,FVE,UUR,UUI,VVR,VVI,XT,YT,UT,VT)

WRITE(6,1000)

DO LOOP FOR EACH ACOUSTIC MODE

DO 1 IK=2,NT

FR=CT\*FRE(1K)  
PFR(1K)=FR

DO LOOP FOR EACH VERTICAL MODE

DO 1 IG=1,MVP

STABILITY INTEGRAL AT THE BOUNDARY

CALL SURFCE(1K,IG,NBP,FFNX,FFNY,ABN,ANN,NC1,  
\* NC,FRE,PRESS,FVE,UUR,UUI,VVR,VVI,  
\* NT,AAA,AAB,AHB,AHC,REN,GAMMA,NBQ,MI,  
\* XT,YT,UT,VT)

STABILITY INTEGRAL IN THE VOLUME

ORIGINAL  
OF POOR QUALITY

DATE: 87/09/24  
TIME: 12:02  
PAGE: 03 OF 50

ORIGINAL PAGE IS  
OF POOR QUALITY

MEMBER: MAIN2  
LEVEL: 01.00  
USERID: CTJC197

PROJECT: CTJC197  
GROUP: STB1  
TYPE: FORT

START COL 1-----2-----3-----4-----5-----6-----7-----+-----8

```

1 C
11 CALL VOLUME(IK,IG,NPT,NL,NT,EN,AAD,AAE,AAF,
* NENL,FRE,PRESS,UUR,UUI,VVR,VVI,
* AHE,AHF,AHG,REN,GAMMA,MI,XT,YT,UT,VT)
1 C
1 C
1 C
1 C
11 FV2 =FVE(IG)
11 PFV(IG)=FV2
9 CTOEN=CT/EN
11 AAA=CTOEN*AAA
11 AAB=CTOEN*AAB
11 AAC=CTOEN*AAC
11 AAD=CTOEN*AAD
11 AAE=CTOEN*AAE
11 AAF=CTOEN*AAF
1 C
11 AHB=CTOEN*AHB
11 AHC=CTOEN*AHC
11 AHE=CTOEN*AHE
11 AHF=CTOEN*AHF
11 AHG=CTOEN*AHG
1 C
11 AA=AAA+AAB+AAC+AAD+AAE+AAF
11 AH=AHB+AHC+AHE+AHF+AHG
11 AT=AA+AH
1 C
11 PAA(IK,IG)=AA
11 PAH(IK,IG)=AH
11 PAT(IK,IG)=AT
1 C
11 WRITE(6,1001) FR,FV2
11 WRITE(6,1002) AT,AA,AH
11 WRITE(6,1012)
11 WRITE(6,1003) AAA,AAB,AAC,AAD,AAE,AAF
11 WRITE(6,1004) AHB,AHC,AHE,AHF,AHG
1 C
1 CONTINUE
1 I
1 C
11 WRITE(6,1006)
11 DO 100 IK=1,NT
11 DO 100 IG=1,MVP
11 WRITE(6,1005) PFR(IK),PFV(IG),PAA(IK,IG),PAH(IK,IG),
* PAT(IK,IG)
1 100 CONTINUE
1 C
1 C
11 STOP
11 FORMAT(////,5X,'STABILITY INTEGRALS',/)
1 1000 FORMAT(//,10X,'ACOUSTIC FREQ =',E10.5,'HZ',5X,
* 'STRAUHAL NO. =',E10.5,/)
6 1001 *
1 1002 *
6 1003 *
1 1012 *
1 1012 *
1 1012 *

```

MAIN2

DATE: 87/09/24  
TIME: 12:02  
PAGE: 04 OF 50

MEMBER: MAIN2  
LEVEL: 01.00  
USERID: CTJJC197

PROJECT: CTJJC197  
GROUP: STB1  
TYPE: FORT

START COL 1 2 3 4 5 6 7 8

1003 14X,'F',14X,'G')  
1004 FORMAT(6X,'ALPA',6E15.5)  
1005 FORMAT(6X,'ALPH',15X.2E15.5,15X.3E15.5)  
1006 FORMAT(5X,5E12.3)  
FORMAT(//////)  
END

SUBROUTINE DINPUT(NELF1,NELF2,NETP1,NETP2,NALF1,NALF2,  
&NATP1,&NATP2,&NERGT,&NEBOT,&NARGT,&NABOT,&NPT1A,&NPT1,  
&NEL,&NGPT,&NPT,&NBW1,&NBW2,&NBW3,&NBW4,&NBW5,&NT1,&NC1,  
\* XMIN,XMAX,YMIN,YMAX,XO,YO,  
\* NBQ,XX,YY,UU,VV,PP,NU,NV,ND,UB,VB,PB,FFNX,  
\* FFFNY,ABN,ANN,REN,GAMMA,DT,ERROR,ITMAX,NL,NT)

GENERATION OF INPUT DATA

NEL : NUMBER OF FINITE ELEMENTS  
NGPT : NUMBER OF GLOBAL NODES  
NPT : NUMBER OF LOCAL NODES IN EACH FINITE ELEMENT  
NBW1 : HALF BAND WIDTH + 1 OF THE STIFFNESS MATRIX  
NBW2 : TOTAL BAND WIDTH OF THE STIFFNESS MATRIX  
NBW3 : NUMBER OF BOUNDARY CONDITIONS OF U-VELOCITY  
NBW4 : NUMBER OF BOUNDARY CONDITIONS OF V-VELOCITY  
NBW5 : NUMBER OF BOUNDARY CONDITIONS OF PRESSURE  
NTT : NUMBER OF TITAL EQUATIONS FOR THE COMPUTATION OF VERTICAL MODE  
NODE(NTT) : ADJUSTMENT MATRIX FOR THE BOUNDARY CONDITIONS OF THE COMPUTATION OF VERTICAL MODES  
NBP : NUMBER OF BOUNDARY FACES OF DOMAIN  
NBQ(NBP) : BOUNDARY ELEMENT MATRIX  
XX(NGPT) : X-COORDINATE  
YY(NGPT) : Y-COORDINATE  
UU(NGPT) : INITIAL CONDITIONS OF U-VELOCITY  
VV(NGPT) : INITIAL CONDITIONS OF V-VELOCITY  
PP(NGPT) : INITIAL CONDITIONS OF PRESSURE  
NU(NUX) : GLOBAL NODES OF BOUNDARY CONDITIONS OF U-VELOCITY  
NV(NVY) : GLOBAL NODES OF BOUNDARY CONDITIONS OF V-VELOCITY  
ND(NDP) : GLOBAL NODES OF BOUNDARY CONDITIONS OF PRESSURE  
FFNX(NBP) : X-DIRECTION NORMAL VECTORS AT EACH BOUNDARY  
FFNY(NBP) : Y-DIRECTION NORMAL VECTORS AT EACH BOUNDARY  
ABN(NBP) : ADMITTANCE AT THE BURNING SURFACE



PROJECT: CTJC197 MEMBER: MAIN2 DATE: 87/09/24  
GROUP: STB1 LEVEL: 01.00 TIME: 12:02  
TYPE: FORT USERID: CTJC197 PAGE: 05 OF 50

START COL 1 2 3 4 5 6 7 8

1 C ANN(NBP) : ADMITTANCE AT THE NOZZLE  
1 C REN : REYNOLDS NUMBER  
1 C GAMMA : SPECIFIC HEAT RATIO  
1 C DT : TIME STEP FOR THE COMPUTATION OF MEAN FLOW  
1 C ERROR : CONVERGENCE ERROR CRITERIA OF THE  
1 C ITMAX : COMPUTATION OF MEAN FLOW  
1 C : MAXIMUM NUMBER OF ITERATIONS OF THE  
1 C : COMPUTATION OF MEAN FLOW

7 DIMENSION NENN(NEL,4),NENL(NL,4),ICON(NT),NC(NBP,NC1,2)  
11 DIMENSION XX(NGPT),YY(NGPT),NU(NUX),NV(NVY),ND(NDP),  
\* UB(NUX),VB(NVY),PB(NDP)  
11 DIMENSION UU(NGPT),VV(NGPT),PP(NGPT)  
11 DIMENSION NODE(NT),NBQ(NBP),FFNX(NBP),FFNY(NBP),ABN(NBP),  
• ANN(NBP)  
7 DIMENSION NBN1(NELF2+1),NBN2(NELF1+NETP1+1),NBN3(NETP2+1),  
&NBN4(NERG1+1),NBN5(NEBOT+1)

CONSTANTS FOR BAND MATRIX

NBW=NERGT+3  
NBW1=NBW+1  
NBWT=NBW\*2+1

DO 10 J=1,NETP1  
DO 10 I=1,NELF2  
K=(J-1)\*NELF2+I  
NNZ=0  
IF(J.EQ.NETP1)NNZ=NELF1  
NENN(K,1)=(J-1)\*(NELF2+1)+I+1  
NENN(K,2)=J\*(NELF2+1)+I+1+NNZ  
NENN(K,3)=NENN(K,2)-1  
NENN(K,4)=NENN(K,1)-1  
CONTINUE

NEL1=NETP1\*NELF2  
DO 20 J=1,NETP2  
DO 20 I=1,NERGT  
K=(J-1)\*NERGT+I+NEL1  
NENN(K,1)=(J-1)\*(NERGT+1)+I+1+NPT1  
NENN(K,2)=J\*(NERGT+1)+I+1+NPT1  
NENN(K,3)=NENN(K,2)-1  
NENN(K,4)=NENN(K,1)-1  
CONTINUE

DO 40 I=1,NETP1  
K=(I-1)\*(NELF2+1)  
YY(K+1)=YO  
DO 40 J=1,NELF2-1  
YY(K+J+1)=(YO-YMIN)+ALOG10(10.\*(1.-FLOAT(J)/FLOAT(NELF2+1)))  
YY(K+J+2)=YMIN  
CONTINUE

ORIGINAL PAGE IS  
OF POOR QUALITY

DATE: 87/09/24  
TIME: 12:02  
PAGE: 06 OF 50

MEMBER: MAIN2  
LEVEL: 01.00  
USERID: CTJC197

PROJECT: CTJC197  
GROUP: STB1  
TYPE: FORT

START COL -----1-----2-----3-----4-----5-----6-----7-----8

```

7 DY11=(YMAX-YO)/FLOAT(NELF1)
7 DO 50 I=1,NETP2+1
7 K=(I-1)*(NERGT+1)
7 YY(NPT1+K+1)=YMAX
7 DO 45 I1=1,NELF1-1
7 YY(NPT1+K+I1+1)=YMAX-DY11*FLOAT(I1)
1 CONTINUE
1 45
7 DO 50 J=1,NELF2+1
7 YY(NPT1+K+NELF1+J)=YY(J)
1 CONTINUE
1 50
1 C
7 DO 60 I=1,NELF2+1
7 XX(I)=XMIN
1 CONTINUE
1 60
1 C
7 NO=NELF2+1
1 C
11 DX12=(XO-XMIN)*.5
11 NTP22=INT(.5*FLOAT(NETP1-1)+.1)
11 PINV22=1./FLOAT(NTP22)
11 PINV33=1./FLOAT(NETP1-NTP22)
1 C
11 DO 75 J=2,NETP1
11 N1=NO
7 IF(J.EQ.NTP22+1)GOTO 72
11 IF(J.GT.NTP22)GOTO 73
11 DUMMY=1.-PINV22*FLOAT(J-1)
11 DX22=DX12*(1.-ALOG10(10.*DUMMY))
11 XXOO=XMIN
11 GOTO 74
11 72
11 XXOO=XMIN
11 DX22=DX12
11 GOTO 74
7 DUMMY=PINV33*FLOAT(J-1-NTP22)
11 DX22=DX12*ALOG10(10.*DUMMY)
11 XXOO=XMIN+DX12
1 74
11 NO=NO+1
11 XX(N1+1)=XXOO+DX22
11 CONTINUE
1 75
1 C
11 DX33=XO-XMIN
11 PINV44=1./FLOAT(NETP1+NTP22)
11 DO 77 J=1,NETP1
11 N1=NO
11 DUMMY=1.-PINV44*FLOAT(J-1)
11 DX34=DX33*(1.-ALOG10(10.*DUMMY))
11 DO 77 I=1,NERGT+1
11 NO=NO+1
11 XX(N1+I)=XO+DX34
11 CONTINUE
1 77
1 C
11 NTP44=NETP2-NETP1
11 DX44=(XMAX-XX(NO))/FLOAT(NTP44+1)
11

```

MAIN2

ORIGINAL PAGE IS  
OF POOR QUALITY

PROJECT: CTJC197  
GROUP: STB1  
TYPE: FORT

MEMBER: MAIN2  
LEVEL: 01.00  
USERID: CTJC197

DATE: 87/09/24  
TIME: 12:02  
PAGE: 07 OF 50

START COL 1-----2-----3-----4-----5-----6-----7-----8

```

11 DO 79 J=1,NTP44+1
11 N1=NO
11 DO 79 I=1,NERGT+1
11 NO=NO+1
11 XX(N1+I)=XX(N1)+DX44
1 79 CONTINUE
1 C
11 DO 80 I=1,NGPT
11 PP(I)=O.
11 UU(I)=O.
11 VV(I)=O.
1 80 CONTINUE
11 DO 90 I=2,NETP1
11 J=(I-1)*(NELF2+1)
11 VV(J+1)=-O.O1
1 90 CONTINUE
1 C
7 DO 101 I=1,NELF2+1
7 NBN1(I)=1
7 CONTINUE
7 DO 102 I=1,NELF1+1
7 NBN2(I)=NPT1+I
7 CONTINUE
7 DO 103 I=1,NETP1
7 J=I+NELF1+1
7 NBN2(J)=NPT1+1-I*(NELF2+1)
7 CONTINUE
7 DO 104 I=1,NETP2+1
7 NBN3(I)=NGPT+1-I*(NERGT+1)
7 CONTINUE
7 DO 105 I=1,NERGT+1
7 NBN4(I)=NGPT-I+1
7 CONTINUE
7 NN=NELF2+1
7 NBN5(1)=NN
7 DO 106 I=2,NEBOT+1
7 IF(I.GT.NETP1)NN=NERGT+1
7 NBN5(I)=NBN5(I-1)+NN
7 CONTINUE
7 N2=O
7 N3=O
7 DO 110 I=1,NELF2+1
7 N2=N2+1
7 N3=N3+1
7 NU(I)=NBN1(I)
7 NV(I)=NBN1(I)
7 CONTINUE
7 N4=N2
7 DO 111 I=1,NEBOT+1
7 N2=N2+1
7 NV(N4+I)=NBN5(I)
7 CONTINUE
7 111

```

MAIN2

PROJECT: CTJC197  
GROUP: STB1  
TYPE: FORT

MEMBER: MAIN2  
LEVEL: 01.00  
USERID: CTJC197

DATE: 87/09/24  
TIME: 12:02  
PAGE: 08 OF 50

START COL 1-----2-----3-----4-----5-----6-----7-----8

```

1 C      N4=N2
7      DO 112 I=1,NERGT+1
7      N2=N2+1
7      NV(N4+I)=NBN4(I)
7      ND(I)=NBN4(I)
1 112   CONTINUE
1 C
7      N4=N2
7      N5=N3
7      DO 113 I=1,NETP2+1
7      N2=N2+1
7      N3=N3+1
7      NV(N4+I)=NBN3(I)
7      NJ(N5+I)=NBN3(I)
1 113   CONTINUE
1 C
7      N6=NELF1+NETP1+1
7      DO 114 I=1,N6
7      NV(N2+I)=NBN2(I)
7      NJ(N3+I)=NBN2(I)
1 114   CONTINUE
1 C
7      DO 116 I=1,NJX
7      J=NJ(I)
7      UB(I)=UU(J)
1 116   CONTINUE
1 C
7      DO 117 I=1,NVY
7      J=NJ(I)
7      VB(I)=VV(J)
1 117   CONTINUE
1 C
7      DO 118 I=1,NDP
7      J=ND(I)
7      PB(I)=PP(J)
1 118   CONTINUE
1 C
7      DO 120 J=1,NATP1
7      DO 120 I=1,NALF2
7      K=(J-1)*NALF2+I
7      NNZ=0
7      IF(J.EQ.NATP1)NNZ=NALF1
7      NENL(K,1)=(J-1)*(NALF2+1)+I+1
7      NENL(K,2)=J*(NALF2+1)+I+1+NNZ
7      NENL(K,3)=NENL(K,2)-1
7      NENL(K,4)=NENL(K,1)-1
1 120   CONTINUE
1 C
7      NAL1=NATP1*NALF2
7      DO 121 J=1,NATP2
7      DO 121 I=1,NARGT
7      K=(J-1)*NARGT+I+NAL1
7      NENL(K,1)=(J-1)*(NARGT+1)+I+1+NPT1A

```

MAIN2

DATE: 87/09/24  
TIME: 12:02  
PAGE: 09 OF 50

MEMBER: MAIN2  
LEVEL: 01.00  
USERID: CTJC197

PROJECT: CTJC197  
GROUP: STB1  
TYPE: FORT

START COL -----1-----2-----3-----4-----5-----6-----7-----+-----8

```

7 NENL(K,2)=J*(NARGT+1)+I+1+NPT1A
7 NENL(K,3)=NENL(K,2)-1
7 NENL(K,4)=NENL(K,1)-1
1 121 CONTINUE
1 C
1 C
7 YDY=(YO-YMIN)/FLOAT(NALF2)
7 ICON(1)=1
7 ICON(NALF2+1)=NELF2+1
7 DO 525 I=2,NALF2
7 YDY1=(NALF2+1-I)*YDY
7 DO 520 J=2,NELF2
7 YINC1=YDY1-YY(J)+YMIN
7 YINC2=YDY1-YY(J+1)+YMIN
7 IF(YINC2.LT.O.)GOTO 520
7 IF(ABS(YINC2).GE.ABS(YINC1))GOTO 521
7 IF(ABS(YINC2).LT.ABS(YINC1))GOTO 522
1 520 CONTINUE
1 521 ICON(I)=J
7 GOTO 525
1 522 ICON(I)=J+1
1 525 CONTINUE
7 IF(NALF2.LE.2)GOTO 526
7 DO 526 I=3,NALF2
7 IF(ICON(I).EQ.ICON(I+1))ICON(I)=ICON(I)-1
7 CONTINUE
1 526
1 C
7 XMID=(XO-XMIN)/2.
7 XDX=(XO-XMIN)/FLOAT(NATP1)
7 DO 535 I=2,NATP1
7 XDX1=(I-1)*XDX
7 DO 530 J=1,NETP1-1
7 JJ1=J*(NELF2+1)+1
7 JJ2=(J+1)*(NELF2+1)+1
7 XINC1=XX(JJ1)-XDX1-XMIN
7 XINC2=XX(JJ2)-XDX1-XMIN
7 IF(XINC2.LT.O.)GOTO 530
7 IF(ABS(XINC2).GE.ABS(XINC1))GOTO 531
7 IF(ABS(XINC2).LT.ABS(XINC1))GOTO 532
1 530 CONTINUE
1 531 JJ=JJ1
7 GOTO 533
1 532 JJ=JJ2
1 533 IF(NATP1.LE.2)GOTO 534
7 LL=-1
7 IF(XX(JJ).GT.XMID)LL=1
7 JK=(I-2)*(NALF2+1)+1
7 IF(ICON(JK).EQ.JJ)JJ=JJ+LL*(NELF2+1)
1 534 ICON((I-1)*(NALF2+1)+1)=JJ
7 DO 535 K=2,NALF2+1
7 KK=(I-1)*(NALF2+1)+K
7 ICON(KK)=ICON(K)+JJ-1
1 535 CONTINUE
1 C

```

START COL -----1-----2-----3-----4-----5-----6-----7-----+-----8

```

7 ICON(NPT1A+1)=NPT1+1
7 ICON(NPT1A+NALF1+1)=NPT1+NELF1+1
7 YDY2=(YMAX-YO)/FLOAT(NALF1)
7 DO 545 I=2,NALF1
7 YDY3=(NALF1+1-I)*YDY2
7 DO 540 J=1,NELF1-1
7 YINC3=YDY3-YY(NPT1+J)+YO
7 YINC4=YDY3-YY(NPT1+J+1)+YO
7 IF(YINC4.LT.O.)GOTO 540
7 IF(ABS(YINC4).GE.ABS(YINC3))GOTO 541
7 IF(ABS(YINC4).LT.ABS(YINC3))GOTO 542
1 CONTINUE
1 540 ICON(NPT1A+I)=NPT1+J
1 541 GOTO 545
7 542 ICON(NPT1A+I)=NPT1+J+1
1 545 CONTINUE
7 IF(NALF1.LE.2)GOTO 546
7 DO 546 I=2,NALF1
7 J=NPT1A+I
7 IF(ICON(J).EQ.ICON(J+1))ICON(J)=ICON(J)-1
1 CONTINUE
1 546 DO 547 I=2,NALF2+1
7 547 ICON(NPT1A+NALF1+I)=NPT1+NELF1+ICON(I)
1 CONTINUE
1 547 C
7 XDX2=(XMAX-XO)/FLOAT(NATP2)
7 DO 555 I=2,NATP2
7 XDX3=(I-1)*XDX2
7 DO 550 J=2,NETP2
7 JJ3=NPT1+J*(NERGT+1)+1
7 JJ4=NPT1+(J+1)*(NERGT+1)+1
7 XINC3=XX(JJ3)-XDX3-XO
7 XINC4=XX(JJ4)-XDX3-XO
7 IF(XINC4.LT.O.)GOTO 550
7 IF(ABS(XINC4).GE.ABS(XINC3))GOTO 551
7 IF(ABS(XINC4).LT.ABS(XINC3))GOTO 552
1 CONTINUE
1 550 JJ=JJ3
1 551 GOTO 553
7 JJ=JJ4
1 552 IF(NATP2.LE.2)GOTO 554
1 553 IF(NPT1A+(I-1)*(NARGT+1)
7 IF(ICON(JK).EQ.JJ)JJ=JJ-(NERGT+1)
1 554 ICON(NPT1A+(I-1)*(NARGT+1)+1)=JJ
7 DO 555 K=2,NARGT+1
7 KK=NPT1A+(I-1)*(NARGT+1)+K
7 ICON(KK)=ICON(NPT1A+K)+JJ-NPT1-1
1 CONTINUE
1 555 C
7 ICON(NT)=NGPT
7 ICON(NT-NARGT)=NGPT-NERGT
7 DO 556 I=2,NARGT
7 J=NT-(NARGT+1)+I
7 JDD=ICON(NPT1A+I)-ICON(NPT1A+I-1)

```

START COL 1-----2-----3-----4-----5-----6-----7-----+-----8

```

7 1 556  ICON(J)=ICON(J-1)+JDD
1 1 C      CONTINUE
1 1 C      :
7 1 1      J1=0
7 1 1      DO 320 J=2,NATP1
7 1 1      DO 320 I=1,NALF2+1
7 1 1      J1=J1+1
7 1 1      NODE(J1)=(J-1)*(NALF2+1)+I
1 1 320    CONTINUE
7 1 1      DO 321 I=1,NALF2
7 1 1      J1=J1+1
7 1 1      NODE(J1)=NPT1A+NALF1+1+I
1 1 321    CONTINUE
7 1 1      DO 322 J=2,NATP2+1
7 1 1      DO 322 I=2,NARGT+1
7 1 1      J1=J1+1
7 1 1      J2=0
7 1 1      IF(I.EQ.2)J2=1
7 1 1      NODE(J1)=NODE(J1-1)+1+J2
1 1 322    CONTINUE
7 1 1      DO 323 I=1,2
7 1 1      DO 323 J=1,NT1
7 1 1      K=I*NT1+J
7 1 1      NODE(K)=NODE(J)+I*NT
1 1 323    CONTINUE
7 1 1      DO 324 I=1,NT
7 1 1      J=3*NT1+I
7 1 1      NODE(J)=NODE(J-1)+1
1 1 324    CONTINUE
1 1 C
1 1 C
7 1 350    DO 350 I=1,6
7 1 1      FFNX(I)=0.
7 1 1      FFNY(I)=0.
7 1 1      ABN(I)=0.
7 1 1      ANN(I)=0.
1 1 350    CONTINUE
7 1 1      NBQ(1)=NALF2
7 1 1      NBQ(2)=NABOT
7 1 1      NBQ(3)=NARGT
7 1 1      NBQ(4)=NATP2
7 1 1      NBQ(5)=NALF1
7 1 1      NBQ(6)=NATP1
7 1 1      DO 360 I=1,6,2
7 1 1      FFNX(I)=1.
7 1 1      FFNY(I+1)=1.
1 1 360    CONTINUE
7 1 1      ABN(6)=1.
7 1 1      ANN(3)=1.
1 1 C
1 1 C
7 1 371    DO 371 J=1,NBQ(1)
7 1 1      NC(1,J,1)=J

```

MAIN2

PROJECT: CTJJC197  
GROUP: STB1  
TYPE: FORT

MEMBER: MAIN2  
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START COL 1 2 3 4 5 6 7 8

```

7 1 371 NC(1,J,2)=J+1
1 1 C CONTINUE
7 K=O
7 NBDQ2=NALF2+1
7 DO 372 J=1,NBQ(2)
7 K=K+NBDQ2
7 IF(J.GE.NATP1)NBDQ2=NARGT+1
7 NC(2,J,1)=K
7 NC(2,J,2)=K+NBDQ2
1 1 372 CONTINUE
1 1 C
7 DO 373 J=1,NBQ(3)
7 NC(3,J,1)=NT+1-J
7 NC(3,J,2)=NT-J
1 1 373 CONTINUE
1 1 C
7 DO 374 J=1,NBQ(4)
7 NC(4,J,1)=NT-J*(NARGT+1)+1
7 NC(4,J,2)=NC(4,J,1)-(NARGT+1)
1 1 374 CONTINUE
1 1 C
7 DO 375 J=1,NBQ(5)
7 NC(5,J,1)=NPT1A+J
7 NC(5,J,2)=NPT1A+J+1
1 1 375 CONTINUE
1 1 C
7 DO 376 J=1,NBQ(6)
7 NBDQ6=O
7 IF(J.EQ.1)NBDQ6=NALF1
7 NC(6,J,1)=NPT1A+1-(J-1)*(NALF2+1)+NBDQ6
7 NC(6,J,2)=NPT1A+1-J*(NALF2+1)
1 1 376 CONTINUE
1 1 C PRINT INPUT DATA
1 1 C
11 WRITE(6,2000)
11 WRITE(6,2001) REN,GAMMA
11 WRITE(6,2002) DT,ERROR,ITMAX
11 WRITE(6,2003) NEL,NGPT,NPT,NBW,NBW1,NBWT
1 1 C
11 WRITE(6,2004)
11 DO 1 I=1,NEL
11 WRITE(6,1003) (NENN(I,J),J=1,NPT)
1 1 C CONTINUE
11 WRITE(6,2005)
11 WRITE(6,2006)
11 DO 11 I=1,NGPT
11 WRITE(6,1004) I,XX(I),YY(I),JU(I),VV(I),PP(I)
1 1 11 CONTINUE
1 1 C
11 WRITE(6,2007)
11 DO 12 I=1,NUX
11 WRITE(6,1005) NU(I),UB(I)

```



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GROUP: S1B1  
TYPE: FORT

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START COL 1-----2-----3-----4-----5-----6-----7-----8

```

1 12 CONTINUE
11 WRITE(6,2008)
11 DO 13 I=1,NVY
11 WRITE(6,1005) NV(I),VB(I)
1 13 CONTINUE
11 WRITE(6,2009)
11 DO 14 I=1,NDP
11 WRITE(6,1005) ND(I),PB(I)
1 14 CONTINUE
1 C
11 WRITE(6,2010)
11 DO 15 I=1,NTT
11 WRITE(6,1006) I,NODE(I)
1 15 CONTINUE
1 C
11 WRITE(6,2011)
11 WRITE(6,2012)
11 DO 16 I=1,NBP
11 WRITE(6,1007) I,NBQ(I),FFNX(I),FFNY(I),ABN(I),ANN(I)
1 16 CONTINUE
1 C
11 WRITE(6,2013)
11 DO 17 I=1,NBP
11 NB=NBQ(I)
11 DO 17 J=1,NB
11 WRITE(6,1008) (NC(I,J,K),K=1,2)
1 17 CONTINUE
1 C
11 FORMAT(4I5)
11 FORMAT(15,5F10.5)
11 FORMAT(15,F10.5)
11 FORMAT(2I5)
11 FORMAT(2I5,4F10.5)
11 FORMAT(2I5)
11 RETURN
1 2000 FORMAT(///,10X,'INPUT DATA',///)
1 2001 FORMAT(5X,'REN=',E10.5,5X,'GAMMA=',F10.5)
1 2002 FORMAT(5X,'DT=',F10.5,2X,'ERROR=',F10.5,2X,'ITMAX=',I5)
1 2003 FORMAT(5X,'NEL=',I5,2X,'NGPT=',I5,2X,'NPT=',I5,2X,
6 'NBW=',I5,2X,'NBWT=',I5,2X,'NBWT=',I5)
1 2004 FORMAT(///,10X,'ELEMENT CONNECTIVITY MATRIX',/)
1 2005 FORMAT(///,10X,'COORDINATE VALUE AT EACH GLOBAL NODE',/)
1 2006 FORMAT(1X,'NO',7X,'XX',7X,'YY',7X,'UU',7X,'VV',7X,'PP',/)
1 2007 FORMAT(///,10X,'BOUNDARY CONDITIONS FOR MEAN FLOW FIELDS',/)
1 2008 FORMAT(//)
1 2009 FORMAT(//)
1 2010 FORMAT(///,10X,'ADJUSTMENT FOR BOUNDARY CONDITIONS',/)
1 2011 FORMAT(///,10X,'NORMAL VECTORS AND ADMITTANCES',/)
1 2012 FORMAT(1X,'NO',3X,'NEQ',6X,'FFNX',6X,'FFNY',7X,'ABN',
6 7X,'ANN',/)
1 2013 FORMAT(///,10X,'BOUNDARY ELEMENT CONNECTIVITY MATRIX',/)
11 END
1 C
1 C

```

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GROUP: STB1  
TYPE: FORT

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START COL -----1-----2-----3-----4-----5-----6-----7-----8

1 C

SUBROUTINE VELOT(NEL,NGPT,NPT,NBW1,NBWT,XX,YY, UU,VV,PP,REN,DT,ERROR,

\* NENN,ICON,XT,YT,UT,VT,NBO,US,VS,DPP,DELU,DELV,FU,FV, A,B,NUX,NVY,NDP,NU,NV,NO,UB,VB,PB,NT,ITMAX)

VIRTUAL

SUBROUTINE FOR MEAN VELOCITY CALCULATIONS

A(NGPT,NBWT) : GLOBAL BAND STIFFNESS MATRIX  
B(NGPT,NBWT) : GLOBAL BAND STIFFNESS MATRIX  
FN(NGPT) : GLOBAL FORCE MATRIX  
FV(NGPT) : GLOBAL FORCE MATRIX  
US(NGPT) : ESTIMATED U-VELOCITY  
VS(NGPT) : ESTIMATED V-VELOCITY  
DPP(NGPT) : PRESSURE CORRECTIONS  
DELU(NGPT) : ACCELERATIONS IN X-DIRECTION  
DELV(NGPT) : ACCELERATIONS IN Y-DIRECTION  
ST(4) : GAUSSIAN POINTS OF GAUSSIAN QUADRATURE  
WS(4) : WEIGHTING FUNCTIONS OF GAUSSIAN QUADRATURE  
ANM(NPT,NPT) : LOCAL STIFFNESS MATRIX  
BNM(NPT,NPT) : LOCAL STIFFNESS MATRIX  
CNM(NPT,NPT) : LOCAL STIFFNESS MATRIX  
FNU(NPT) : LOCAL FORCE MATRIX  
FNV(NPT) : LOCAL FORCE MATRIX  
GN(NPT) : LOCAL FORCE MATRIX  
HNU(NPT) : LOCAL FORCE MATRIX  
HNV(NPT) : LOCAL FORCE MATRIX  
SUM : CONVERGENCE ERROR IN EACH ITERATION  
ITER : COUNTER OF ITERATION

DIMENSION XX(NGPT),YY(NGPT),UU(NGPT),VV(NGPT),PP(NGPT)  
DIMENSION UB(NUX),VB(NVY),PB(NDP),WS(4),ST(4)  
DIMENSION NU(NUX),NV(NVY),ND(NDP)  
DIMENSION XT(NT),YT(NT),UT(NT),VT(NT)  
DIMENSION US(NGPT),VS(NGPT),DPP(NGPT),DELU(NGPT),DELV(NGPT)  
DIMENSION ANM(4,4),BNM(4,4),CNM(4,4),FNU(4),FNV(4),GN(4),  
HNU(4),HNV(4),A(NGPT,NBO),B(NGPT,NBO),  
FU(NGPT),FV(NGPT),NENN(NEL,4),ICON(NT)

CALL THE VALUES FOR GAUSSIAN QUADRATURE INTEGRATIONS

CALL GAUSS(4,WS,ST)

ITER=0

CONTINUE

1 C 2000

ITER=ITER+1

ESTIMATED VELOCITIES

DO 100 I=1,NGPT

11

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GROUP: STB1  
TYPE: FORT

START COL -----1-----2-----3-----4-----5-----6-----7-----8

```

11 FU(I)=0.0
11 FV(I)=0.0
11 DO 100 J=1,NBWT
11 A(I,J)=0.0
11 B(I,J)=0.0
11 CONTINUE
1 100
1 C
11 DO 200 I=1,NEL
11 CALL ELEUV(I,NPT,NGPT,XX,YY,UU,VV,PP,REN,DT,NENN,
6 ANM,FNU,FNV,WS,ST,NEL)
11 DO 200 J=1,NPT
11 JJ=NENN(I,J)
11 FU(JJ)=FU(JJ)+FNU(J)
11 FV(JJ)=FV(JJ)+FNV(J)
11 DO 200 K=1,NPT
11 KK=NENN(I,K)
11 KKJJ=KK-JJ+NBW1
11 A(JJ,KKJJ)=A(JJ,KKJJ)+ANM(J,K)
11 B(JJ,KKJJ)=A(JJ,KKJJ)
11 CONTINUE
1 200
1 C
11 CALL ADJUST(NUX,NGPT,NU,A,UB,FU,NBW1,NBWT)
11 CALL ADJUST(NVY,NGPT,NV,B,VB,FV,NBW1,NBWT)
11 C
11 CALL GAUSU(A,FU,US,NGPT,NBW1,NBWT)
11 CALL GAUSU(B,FV,VS,NGPT,NBW1,NBWT)
11 C
11 C
11 C
11 C
11 DO 300 I=1,NGPT
11 FU(I)=0.0
11 DO 300 J=1,NBWT
11 A(I,J)=0.0
11 CONTINUE
1 300
1 C
11 DO 400 I=1,NEL
11 CALL ELEPR(I,NPT,NGPT,XX,YY,US,VS,DT,BNM,GN,
6 WS,ST,NEL,NENN)
11 DO 400 J=1,NPT
11 JJ=NENN(I,J)
11 FU(JJ)=FU(JJ)+GN(J)
11 DO 400 K=1,NPT
11 KK=NENN(I,K)
11 KKJJ=KK-JJ+NBW1
11 A(JJ,KKJJ)=A(JJ,KKJJ)+BNM(J,K)
11 CONTINUE
1 400
1 C
11 CALL ADJUST(NDP,NGPT,ND,A,PB,FU,NBW1,NBWT)
11 CALL GAUSU(A,FU,DPP,NGPT,NBW1,NBWT)
11 C
11 C
11 C
11 C
11 DO 500 I=1,NGPT

```





START COL 1-----2-----3-----4-----5-----6-----7-----8

```

1 190 CONTINUE
1 C
1 C ASSEMBLY OF GLOBAL MATRICES
1 C
11 DO 200 I=1,NL
11 CALL ELEMPI(I,NPT,ANM,BNM,WS,ST,NL,NT,NENL,
6 * XT,YT)
1 C
11 DO 200 J=1,NPT
11 JJ=NENL(I,J)
11 DO 200 K=1,NPT
11 KK=NENL(I,K)
11 A1(JJ,KK)=A1(JJ,KK)+CPLX(ANM(J,K),O.O)
11 B1(JJ,KK)=B1(JJ,KK)+CPLX(BNM(J,K),O.O)
1 200 CONTINUE
1 C
1 C APPLY EIGENVALUE SUBROUTINE IN IMSL
1 C
11 CALL CONVRT(NT,A1,NT,B1,NT,CZZ1,NT)
11 CALL SOLVE(NT,A1,NT,B1,NT,CZZ1,NT,ITER,EIGAV,EIGBV)
1 C
1 C OBTAIN EIVENVALUES AND EIGENVECTORS
1 C
11 DO 220 IEG=1,NT
11 IF(EIGBV(IEG).EQ.O.O) GO TO 220
11 EIGV(IEG)=EIGAV(IEG)/EIGBV(IEG)
11 FRE(IEG)=SORT(ABS(REAL(EIGV(IEG))))
11 DO 221 IEF=1,NT
11 PRESS(IEF,IEG)=REAL(CZZ1(IEF,IEG))
11 CONTINUE
1 221 CONTINUE
1 220
1 C
1 C SORTING PROCESS
1 C
11 NN=NT-1
11 DO 4000 K=1,NN
11 JJ=NT-K
11 DO 410 L=1,JJ
11 IF(FRE(L).LE.FRE(L+1)) GO TO 410
11 TEMP=FRE(L)
11 FRE(L)=FRE(L+1)
11 FRE(L+1)=TEMP
11 DO 420 NP=1,NT
11 TARR1(NP)=PRESS(NP,L)
11 PRESS(NP,L)=PRESS(NP,L+1)
11 PRESS(NP,L+1)=TARR1(NP)
11 CONTINUE
1 420 CONTINUE
1 410 CONTINUE
1 4000 CONTINUE
1 C
1 C OUTPUT FOR ACOUSTIC FREQUENCIES AND THEIR MODES
1 C
11 WRITE(6,1000)
11 DO 500 I=1,NT

```



MAIN2

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PROJECT: CTJC197  
GROUP: STB1  
TYPE: FORT

START COL 1-----2-----3-----4-----5-----6-----7-----+-----8

```

11 DIMENSION ANM(4,4,4,4),BNM(4,4,4,4),FV1(MII),NENL(NL,4),
6 * FVE(MI),UUR(NT,MI),UUI(NT,MI),VVR(NT,MI),VVI(NT,MI)
11 COMPLEX A2(MII,MII),B2(MII,MII),C(NT,NTT),D(NTT,NTT),
6 * CZZ2(NTT,NTT),EIGAV2(NTT),EIGBV2(NTT),EIGV2(NTT)
11 INTEGER ITER2(NTT)

```

```

11 CALL GAUSS(4,WS,ST)

```

INITIALIZATION OF GLOBAL MATRICES

```

7 NT4=NT*4
7 NT2=NT*2
11 DO 1 I=1,NT4
11 DO 1 J=1,NT4
11 A2(I,J)=(O.O,O.O)
11 B2(I,J)=(O.O,O.O)
11 CONTINUE

```

```

11 DO 111 I=1,NTT
11 DO 111 J=1,NT
11 C(I,J)=(O.O,O.O)
11 D(I,J)=(O.O,O.O)
11 CONTINUE

```

```

11 DO 112 I=1,NT4
11 DO 112 J=1,NTT
11 SR(I,J)=O.O
11 SI(I,J)=O.O
11 CONTINUE

```

ASSEMBLY OF GLOBAL MATRICES

```

11 DO 2 I=1,NL
11 CALL ELEVR(I,NPT,ANM,BNM,WS,ST,REN,NL,NT,NENL,
6 * XT,YT,UT,VT)

```

```

7 DO 2 L=1,4
7 LNT=(L-1)*NT
11 DO 2 J=1,NPT
11 JJ=NENL(I,J)+LNT
11 DO 2 LL=1,4
11 LLNT=(LL-1)*NT

```

```

11 DO 2 K=1,NPT
11 KK=NENL(I,K)+LLNT
11 A2(JJ,KK)=A2(JJ,KK)+CMPLX(ANM(L,LL,J,K),O.O)
11 B2(JJ,KK)=B2(JJ,KK)+CMPLX(BNM(L,LL,J,K),O.O)
11 CONTINUE

```

APPLY BOUNDARY CONDITIONS

```

11 DO 20 I=1,NTT
11 DO 20 J=1,NTT
11 C(I,J)=A2(NODE(I),NODE(J))
11 D(I,J)=B2(NODE(I),NODE(J))
11 CONTINUE

```

1 20



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GROUP: STB1  
TYPE: FORT

START COL 1-----2-----3-----4-----5-----6-----7-----8

```

1 C
11 CALL CONVRT(NTT,C,NTT,D,NTT,CZZ2,NTT)
11 CALL SOLVE(NTT,C,NTT,D,NTT,CZZ2,NTT,ITER2,EIGAV2,EIGBV2)
1 C
1 C
1 C
1 C
11 DO 3 IEG=1,NTT
11 IF(EIGBV2(IEG).EQ.0.0) GO TO 3
11 EIGV2(IEG)=EIGAV2(IEG)/EIGBV2(IEG)
11 FV1(IEG)=AIMAG(EIGV2(IEG))
11 DO 4 IEF=1,NTT
11 SR(NODE(IEF),IEG)=REAL(CZZ2(IEF,IEG))
11 SI(NODE(IEF),IEG)=AIMAG(CZZ2(IEF,IEG))
11 CONTINUE
1 4 CONTINUE
1 3
1 C
1 C
1 C
1 C
11 SORTING PROCESS
11 NN=NTT-1
11 DO 5 K=1,NN
11 JJ=NTT-K
11 DO 6 L=1,JJ
11 IF(FV1(L).LT.FV1(L+1)) GO TO 6
11 TEMP=FV1(L)
11 FV1(L)=FV1(L+1)
11 FV1(L+1)=TEMP
11 DO 7 NP=1,NT4
11 TR=SR(NP,L)
11 TI=SI(NP,L)
11 SR(NP,L)=SR(NP,L+1)
11 SI(NP,L)=SI(NP,L+1)
11 SR(NP,L+1)=TR
11 SI(NP,L+1)=TI
11 CONTINUE
1 7 CONTINUE
1 6 CONTINUE
1 5 CONTINUE
1 C
11 IP=0
11 DO 8 I=1,NTT
11 IF(FV1(I).LT.0.01) GO TO 8
11 IP=IP+1
11 FVE(IP)=FV1(I)
11 DO 9 J=1,NT
11 UUR(J,IP)=SR(NT2+J,I)
11 UUI(J,IP)=SI(NT2+J,I)
11 VVR(J,IP)=-SR(NT+J,I)
11 VVI(J,IP)=-SI(NT+J,I)
11 CONTINUE
1 9 CONTINUE
1 8 CONTINUE
1 C
11 MVP=IP
11 OUTPUT FOR VORTICAL MODES
1 C
1 C

```

START COL 1-----2-----3-----4-----5-----6-----7-----8

```

11 WRITE(6,999)
11 DO 10 I=1,20
11 WRITE(6,1000) I,FVE(I)
11 WRITE(6,1010)
11 DO 11 J=1,NF
11 WRITE(6,1001) J,XT(J),YT(J),UUR(J,I),UUI(J,I),
* VVR(J,I),VVI(J,I)
1 11 CONTINUE
1 10 CONTINUE
1 C
11 RETURN
1 999 FORMAT(//////,10X,'LOWEST TWENTY VORTICAL MODES',/)
1 1000 FORMAT(//////,15,'-TH VORTICAL MODE',5X,
* 'STROUHAL NO. ',E10.5,/)
1 1010 FORMAT(3X,'NO',5X,'XT',8X,'YT',9X,'UUR',12X,'UUI',
* 12X,'VVR',12X,'VVI')
1 1001 FORMAT(15,2F9.5,4E14.5)
11 END

```

```

11 SUBROUTINE SURFCE(IK,IG,NBP,FFNX,FFNY,ABN,ANN,NC1,
* NC,FRE,PRESS,FVE,UUR,UUI,VVR,VVI,
* NT,AAA,AAB,
* AHB,AHC,REN,GAMMA,NBQ,MI,
* XT,YT,UT,VT)

```

STABILITY INTEGRALS AT THE SURFACES

- IK : COUNTER OF ACOUSTIC MODES
- IG : COUNTER OF VIRTICAL MODES
- AAA : (A)-TERM OF ACOUSTIC GROWTH CONSTANT
- AAB : (B)-TERM OF ACOUSTIC GROWTH CONSTANT
- AHB : (B)-TERM OF VORTICALLY COUPLED ACOUSTIC GROWTH CONSTANT
- AHC : (C)-TERM OF VORTICALLY COUPLED ACOUSTIC GROWTH CONSTANT
- X(2) : LOCAL BOUNDARY X-COORDINATES
- Y(2) : LOCAL BOUNDARY Y-COORDINATES
- U(2) : LOCAL BOUNDARY MEAN VELOCITY IN X-DIRECTION
- V(2) : LOCAL BOUNDARY MEAN VELOCITY IN Y-DIRECTION
- P(2) : LOCAL BOUNDARY ACOUSTIC MODES
- UR(2) : LOCAL BOUNDARY VALUE OF REAL PART OF VORTICAL DISTURBANCES IN X-DIRECTION
- VR(2) : LOCAL BOUNDARY VALUE OF REAL PART OF VORTICAL DISTURBANCES IN Y-DIRECTION
- UI(2) : LOCAL BOUNDARY VALUE OF IMAGINARY PART OF VORTICAL DISTURBANCES IN X-DIRECTION
- VI(2) : LOCAL BOUNDARY VALUE OF IMAGINARY PART OF VORTICAL DISTURBANCES IN Y-DIRECTION
- FI(2) : INTERPOLATION FUNCTIONS IN BOUNDARY ELEMENT
- DS(2) : FIRST DERIVATIVES OF INTERPOLATION FUNCTIONS

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START COL -----1-----2-----3-----4-----5-----6-----7-----8

```

1 C      IN BOUNDARY ELEMENT
1 C
7 DIMENSION XT(NT),YT(NT),UI(NT),VI(NT)
11 DIMENSION FFNX(NBP),FFNY(NBP),ABN(NBP),ANN(NBP),NBQ(NBP)
11 DIMENSION U(2),V(2)
6 *      WS(4),ST(4),X(2),Y(2),P(2),UI(2),VI(2),FI(2),OS(2)
11 DIMENSION UR(2),VR(2),NC(NBP,NC1,2),FRE(NT),PRESS(NT,NT),
6 * FVE(MI),UUR(NT,MI),UUI(NT,MI),VVR(NT,MI),VVI(NT,MI)
1 C      CALL GAUSS(4,WS,ST)
11
1 C      FR=FRE(IK)
11 FRINV=1./FR
7 FR2INV=FRINV*FRINV
7 RFRINV=FRINV/REN
11 FV3=FVE(IG)
1 C
1 C      INITIALIZATIONS
1 C
11 AAA=0.0
11 AAB=0.0
11 AHB=0.0
11 AHC=0.0
1 C
1 C      REPEAT INTEGRATION IN EACH BOUNDARY AREA
1 C      DO 1 IB=1,NBP
11 IF(IB.EQ.2) GO TO 1
1 C
1 C      NECESSARY INFORMATION IN EACH BOUNDARY AREA
1 C
11 FFNX=FFNX(IB)
11 FFNY=FFNY(IB)
11 NB = NBQ(IB)
11 AB = ABN(IB)
11 AN = ANN(IB)
1 C
11 DO 2 IC=1,NB
1 C
11 DO 10 N=1,2
11 NN=NC(IB,IC,N)
11 X(N)=XT(NN)
11 Y(N)=YT(NN)
11 U(N)=UT(NN)
11 V(N)=VT(NN)
11 P(N)=PRESS(NN,IK)
11 UR(N)=UUR(NN,IG)
11 VR(N)=VVR(NN,IG)
11 UI(N)=UUI(NN,IG)
11 VI(N)=VVI(NN,IG)
11 CONTINUE
1 10
1 C
11 IF(FNX .EQ. 0.0) DTA=0.5*ABS(X(2))-X(1)

```

PROJECT: CTJJC197  
GROUP: STB1  
TYPE: FORT

MEMBER: MAIN2  
LEVEL: 01.00  
USERID: CTJJC197

DATE: 87/09/24  
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PAGE: 24 OF 50

START COL -----1-----2-----3-----4-----5-----6-----7-----8

11 IF (FNY .EQ. 0.0) DTA=0.5\*ABS(Y(2))-Y(1))  
7 DTINV5=-.5/DTA

1 C  
11 DO 100 K=1,4  
11 XI=ST(K)  
11 ACOF=WS(K)

INTERPOLATION FUNCTIONS AT THE BOUNDARY ELEMENT

11 FI(1)=0.5\*(1.0-XI)  
11 FI(2)=0.5\*(1.0+XI)

11 DS(1)=DTINV5  
11 DS(2)=-DS(1)

1 C  
11 YP=0.0  
11 SU=0.0  
11 SV=0.0  
11 PN=0.0  
11 PS=0.0  
11 SUI=0.0  
11 SUIV=0.0  
11 SVIS=0.0

1 C  
11 DO 110 N=1,2  
11 YP=YP+FI(N)\*Y(N)  
11 SU=SU+FI(N)\*U(N)  
11 SV=SV+FI(N)\*V(N)  
11 PN=PN+FI(N)\*P(N)  
11 PS=PS+DS(N)\*P(N)  
11 SUI=SUI+FI(N)\*UI(N)  
11 SUIV=SUI+FI(N)\*VI(N)  
11 SVIS=SVIS+DS(N)\*VI(N)  
11 CONTINUE

1 C  
11 C=3.14159\*YP\*ACOF\*DTA

1 C  
11 AAA=AAA+C\*((AB-AN)\*PN\*PN+(GAMMA+1.0)\*(SU\*FNX+SV\*FNY)\*PN\*PN)  
11 AAB=AAB-C\*(SU\*FNX+SV\*FNY)\*PS\*PS\*FR2INV  
11 AHB=AHB+C\*GAMMA\*(2.0\*(SU\*SUI\*PS\*FNX+SV\*SUI\*PS\*FNY)  
6 \* + (SU\*SUI+SV\*SUI)\*PS\*(FNX+FNY))\*FRINV

11 AHC=AHC+C\*(SVIS\*PS\*FNX+SUIS\*PS\*FNY)\*RFRINV  
11 CONTINUE

1 C  
1 100  
1 C  
1 2  
1 1  
1 1  
1 C  
11 RETURN  
11 END

11 SUBROUTINE VOLUME(IK,IG,NPT,NL,NT,EN,AAD,AAE,AAF.





MAIN2

DATE: 87/09/24  
TIME: 12:02  
PAGE: 27 OF 50

MEMBER: MAIN2  
LEVEL: 01.00  
USERID: CTJJC197

PROJECT: CTJJC197  
GROUP: STB1  
TYPE: FORT

START COL 1-----2-----3-----4-----5-----6-----7-----8

```

11 VNN=O.O
11 VNX=O.O
11 VNY=O.O
11 URN=O.O
11 URX=O.O
11 URY=O.O
11 VRN=O.O
11 VRX=O.O
11 VRY=O.O
11 UIN=O.O
11 UIX=O.O
11 UIY=O.O
11 VIN=O.O
11 VIX=O.O
11 VIY=O.O
1 C
11 DO 30 N=1,NPT
11 YP=YP+FI(N)*Y(N)
11 PRN=PRN+FI(N)*P(N)
11 PRX=PRX+DX(N)*P(N)
11 PRY=PRY+DY(N)*P(N)
11 PRXX=PRXX+DXX(N)*P(N)
11 PRXY=PRXY+DXY(N)*P(N)
11 PRYY=PRYY+DYY(N)*P(N)
11 UNN=UNN+FI(N)*U(N)
11 UNX=UNX+DX(N)*U(N)
11 UNY=UNY+DY(N)*U(N)
11 VNN=VNN+FI(N)*V(N)
11 VNX=VNX+DX(N)*V(N)
11 VNY=VNY+DY(N)*V(N)
11 URN=URN+FI(N)*UR(N)
11 URX=URX+DX(N)*UR(N)
11 URY=URY+DY(N)*UR(N)
11 VRN=VRN+FI(N)*VR(N)
11 VRX=VRX+DX(N)*VR(N)
11 VRY=VRY+DY(N)*VR(N)
11 UIN=UIN+FI(N)*UI(N)
11 UIX=UIX+DX(N)*UI(N)
11 UIY=UIY+DY(N)*UI(N)
11 VIN=VIN+FI(N)*VI(N)
11 VIX=VIX+DX(N)*VI(N)
11 VIY=VIY+DY(N)*VI(N)
11 CONTINUE

```

```

1 30
1 C
11 C=3.14159*YP*ACOF*DTA
11 EN=EN+C*2.O*PRN*PRN
11 AAD=AAD-C*(2.O*GAMMA+1.O)*PRN*(UNN*PRX+VNN*PRY)
11 AAE=AAE+C*(-(UNN*PRX+VNN*PRY)*PRN
11 +2.O*(UNN*PRX+PRXX+VNN*PRY*PRY
11 +(UNN*PRX+VNN*PRY)*PRY)*FR21INV)
11 *
11 *
11 AAF=AAF-C*((PRXX*PRXX+2.O*PRXY*PRXY+PRYY*PRYY)*RF21INV
11 +FR*FR*PRN*PRN*RN31INV)
11 *
11 AHE=AHE+2.O*C*GAMMA*(UNN*UIN+PRXX+VNN*VIN*PRY
11

```

-----1-----2-----3-----4-----5-----6-----7-----8

```

6 *          *(UNN*VIN+VNN*UIN)*PRXY)*FRINV
11 AHF=AHF-C*GAMMA*(UIX*PRXX+VIX*PRYY+(UIV+VIX)*PRXY)*RFRINV
11 AHG=AHG+2.0*C*GAMMA*(GAMMA-1.0)
6 *          *(2.0*(URX*URX+VNY*VRY)
6 *          *(UNY+VNX)*(URY+VRX))*RENINV
1 20
1 C
1 1
1 C
11 RETURN
11 END
1 C
1 C
1 C

```

```

11 SUBROUTINE ELEUV(MMM,NPT,NGPT,XX,YY,UU,VV,PP,
6 *          REN,DT,NENN,ANM,FNU,FNV,WS,ST,NEL)
1 C
1 C
1 C

```

```

11 LOCAL MATRICES FOR VELOCITIES
11 DIMENSION XX(NGPT),YY(NGPT),UU(NGPT),VV(NGPT),PP(NGPT)
11 DIMENSION ANM(4,4),FNU(4),FNV(4),WS(4),ST(4)
11 DIMENSION X(4),Y(4),FI(4),DX(4),DY(4),AA(4),AB(4),
6 *          U(4),V(4),P(4),NENN(NEL,4)
1 C

```

```

7 RENINV=1./REN
7 DTINV=1./DT
1 C
11 DO 1 N=1,NPT
11 NN=NENN(MMM,N)
11 X(N)=XX(NN)
11 Y(N)=YY(NN)
11 U(N)=UU(NN)
11 V(N)=VV(NN)
11 P(N)=PP(NN)
11 CONTINUE
1 1
1 C

```

```

11 DO 2 N=1,NPT
11 FNU(N)=0.0
11 FNV(N)=0.0
11 DO 2 M=1,NPT
11 ANM(N,M)=0.0
11 CONTINUE
1 2
1 C
11 DO 300 K=1,4
11 DO 300 L=1,4
11 XI=ST(K)
11 ETA=ST(L)
11 ACOF=WS(K)*WS(L)
11 C

```

```

11 CALL INTER(XI,ETA,NPT,X,Y,DX,DY,FI,DTA,AA,AB)
11 C
11 SSU=0.0
11 SSV=0.0
11 SXP=0.0
11

```



PROJECT: CTJJC197  
GROUP: STB1  
TYPE: FORT

MEMBER: MAIN2  
LEVEL: 01.00  
USERID: CTJJC197

DATE: 87/09/24  
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PAGE: 29 OF 50

START COL -----1-----2-----3-----4-----5-----6-----7-----8

```

11 SYP=0.0
11 YP=0.0
1 C
11 DO 301 N=1,NPT
11 SSU=SSU+FI(N)*U(N)
11 SSV=SSV+FI(N)*V(N)
11 SXP=SXP+DX(N)*P(N)
11 SYP=SYP+DY(N)*P(N)
11 YP =YP +FI(N)*Y(N)
11 CONTINUE
1 301
1 C
11 C=ACOF*DTA*YP
1 C
11 DO 500 N=1,NPT
11 CFIN=C*FI(N)
11 FNU(N)=FNU(N)+CFIN*(SSU*DTINV-SXP)
11 FNV(N)=FNV(N)+CFIN*(SSV*DTINV-SYP)
11 DO 500 M=1,NPT
11 ANM(N,M)=ANM(N,M)+CFIN*(FI(M)*DTINV+SSU*DX(M)+SSV*DY(M))
11 +C*(DX(N)*DX(M)+DY(N)*DY(M))*RENINV
6 *
1 500 CONTINUE
1 300 CONTINUE
1 C
11 RETURN
11 END
1 C
11 SUBROUTINE ELEPR(MMM,NPT,NGPT,XX,YY,US,VS,
* DT,BNM,GN,WS,ST,NEL,NENN)
11 LOCAL MATRICES FOR PRESSURE CORRECTIONS
1 C
11 DIMENSION XX(NGPT),YY(NGPT),US(NGPT),VS(NGPT)
11 DIMENSION BNM(4,4),GN(4),WS(4),ST(4),NENN(NEL,4)
11 DIMENSION X(4),Y(4),FI(4),DX(4),DY(4),AA(4),AB(4),U(4),V(4)
1 C
11 DTINV=1./DT
11 DO 1 N=1,NPT
11 NN=NENN(MMM,N)
11 X(N)=XX(NN)
11 Y(N)=YY(NN)
11 U(N)=US(NN)
11 V(N)=VS(NN)
11 CONTINUE
1 1 C
11 DO 2 N=1,NPT
11 GN(N)=0.0
11 DO 2 M=1,NPT
11 BNM(N,M)=0.0
11 CONTINUE
1 2 C
11 DO 300 K=1,4
11 DO 300 L=1,4
11 XI=ST(K)

```

PROJECT: CTJJC197  
GROUP: STB1  
TYPE: FORT

MEMBER: MAIN2  
LEVEL: 01.00  
USERID: CTJJC197

DATE: 87/09/24  
TIME: 12:02  
PAGE: 30 OF 50

START COL -----1-----2-----3-----4-----5-----6-----7-----8

```

11      ETA=ST(L)
11      ACOF=WS(K)*WS(L)
1      C
11      CALL INTER(XI,ETA,NPT,X,Y,DX,DY,FI,DTA,AA,AB)
1      C
11      SXU=0.0
11      SYV=0.0
11      YP =0.0
1      C
11      DO 301 N=1,NPT
11      SXU=SXU+DX(N)*U(N)
11      SYV=SYV+DY(N)*V(N)
11      YP =YP +FI(N)*Y(N)
11      CONTINUE
1      301
1      C
11      C=ACOF*DTA*YP
1      C
11      DO 500 N=1,NPT
11      GN(N)=GN(N)-C*FI(N)*(SXU+SYV)*DTINV
11      DO 500 M=1,NPT
11      BNM(N,M)=BNM(N,M)+C*(DX(N)*DX(M)+DY(N)*DY(M))
11      CONTINUE
1      500
1      300
1      C
11      RETURN
11      END
11      *
11      SUBROUTINE ELEAC(MMM,NPT,NGPT,XX,YY,DPP,CNM,
11      HNU,HNV,WS,ST,NEL,NENN)
11      C
11      C
11      C
11      LOCAL MATRICES FOR ACCELERATIONS
11      DIMENSION XX(NGPT),YY(NGPT),DPP(NGPT),NENN(NEL,4)
11      DIMENSION CNM(4,4),HNU(4),HNV(4),WS(4),ST(4)
11      DIMENSION X(4),Y(4),DP(4),FI(4),DX(4),DY(4),AA(4),AB(4)
11      C
11      DO 1 N=1,NPT
11      NW=NENN(MMM,N)
11      X(N)=XX(NN)
11      Y(N)=YY(NN)
11      DP(N)=DPP(NN)
11      CONTINUE
11      DO 2 N=1,NPT
11      HNU(N)=0.0
11      HNV(N)=0.0
11      DO 2 M=1,NPT
11      CNM(N,M)=0.0
11      CONTINUE
11      2
11      C
11      DO 300 K=1,4
11      DO 300 L=1,4
11      XI=ST(K)

```

PROJECT: CTJC197  
GROUP: STB1  
TYPE: FORT

MEMBER: MAIN2  
LEVEL: 01.00  
USERID: CTJC197

DATE: 87/09/24  
TIME: 12:02  
PAGE: 31 OF 50

START COL -----1-----2-----3-----4-----5-----6-----7-----8

```

11      ETA=ST(L)
11      ACOF=WS(K)*WS(L)
1   C
11      CALL INTER(XI,ETA,NPT,X,Y,DX,DY,FI,DTA,AA,AB)
11      SDPX=0.0
11      SDPY=0.0
11      YP =0.0
1   C
11      DO 310 N=1,NPT
11      SDPX=SDPX+DX(N)*DP(N)
11      SDPY=SDPY+DY(N)*DP(N)
11      YP =YP +FI(N)*Y(N)
1   C
11      CONTINUE
1   C
11      C=ACOF*DTA*YP
11      DO 500 N=1,NPT
11      CFIN=C*FI(N)
11      HNJ(N)=HNJ(N)-CFIN*SDPX
11      HNV(N)=HNV(N)-CFIN*SDPY
11      DO 500 M=1,NPT
11      CNM(N,M)=CNM(N,M)+CFIN*FI(M)
1   C
11      CONTINUE
1   C
11      RETURN
11      END
1   C
11      SUBROUTINE ELEMP(MMM,NPT,ANM,BNM,WS,ST,NL,NT,NENL,
6      XT,YT)
1   C
11      DIMENSION XT(NT),YT(NT)
11      DIMENSION ANM(4,4),BNM(4,4),WS(4),ST(4),NENL(NL,4)
11      DIMENSION X(4),Y(4),FI(4),DX(4),DY(4),AA(4),AB(4)
1   C
11      DO 100 N=1,NPT
11      NN=NENL(MMM,N)
11      X(N)=XT(NN)
11      Y(N)=YT(NN)
11      CONTINUE
1   C
11      DO 110 I=1,NPT
11      DO 110 J=1,NPT
11      ANM(I,J)=0.0
11      BNM(I,J)=0.0
11      CONTINUE
1   C
11      DO 300 K=1,4
11      DO 300 L=1,4
11      XI=ST(K)
11      ETA=ST(L)
11      ACOF=WS(K)*WS(L)

```

START COL -----1-----2-----3-----4-----5-----6-----7-----+-----8

```

1 C
11 CALL INTER(XI,ETA,NPT,X,Y,DX,DY,FI,DTA,AA,AB)
1 C
11 YP=O.O
11 DO 310 N=1,NPT
11 YP=YP+FI(N)*Y(N)
11 CONTINUE
1 310
1 C
11 C=@CDF*DTA*YP
1 C
11 DO 500 N=1,NPT
11 CFIN=C*FI(N)
11 DO 500 M=1,NPT
11 ANM(N,M)=ANM(N,M)+C*(DX(N)*DX(M)+DY(N)*DY(M))
11 BNM(N,M)=BNM(N,M)+CFIN*FI(M)
11 CONTINUE
1 500
1 300
1 C
11 RETURN
11 END
1 C
11 *
11 SUBROUTINE ELEVR(MMM,NPT,ANM,BNM,WS,ST,REN,NL,NT,NENL,
11 XT,YT,UT,VT)
1 C
11 LOCAL ELEMENT FOR VERTICAL EIGENMODES
1 C
11 DIMENSION XT(NT),YT(NT),UT(NT),VT(NT)
11 DIMENSION X(4),Y(4),U(4),V(4),ANM(4,4,4,4),BNM(4,4,4,4),
11 * WS(4),ST(4),PI(4,4),DPX(4,4),DPY(4,4),
11 * DPXX(4,4),DPXY(4,4),DPYY(4,4),NENL(NL,4)
1 C
11 RENINV=1./REN
1 C
11 DO 100 N=1,NPT
11 NN=NENL(MMM,N)
11 X(N)=XT(NN)
11 Y(N)=YT(NN)
11 U(N)=UT(NN)
11 V(N)=VT(NN)
11 CONTINUE
1 100
1 C
11 DO 110 L=1,4
11 DO 110 N=1,NPT
11 DO 110 LL=1,4
11 DO 110 M=1,NPT
11 ANM(L,LL,N,M)=O.O
11 BNM(L,LL,N,M)=O.O
11 CONTINUE
1 110
1 C
11 DA=ABS(X(2)-X(1))*0.5
11 DB=ABS(Y(4)-Y(1))*0.5
11
11 C

```

MAIN2

DATE: 87/09/24  
TIME: 12:02  
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MEMBER: MAIN2  
LEVEL: 01.00  
USERID: CTJC197

PROJECT: CTJC197  
GROUP: STB1  
TYPE: FORT

START COL -----1-----2-----3-----4-----5-----6-----7-----8

```

11 DO 300 K=1,4
11 DO 300 L=1,4
11 XI=ST(K)
11 ETA=ST(L)
11 ACOF=WS(K)*WS(L)
1 C
11 CALL HERMT(XI,ETA,DA,DB,PI,DPX,DPY,DPXX,DPXY,DPYY)
1 C
11 SU=0.0
11 SV=0.0
11 SUX=0.0
11 SUY=0.0
11 SVX=0.0
11 SVY=0.0
11 SUXX=0.0
11 SUXY=0.0
11 SUYY=0.0
11 SVXX=0.0
11 SVXY=0.0
11 SVYY=0.0
11 YP=0.0
1 C
11 DO 310 N=1,NPT
11 SU=SU+PI(1,N)*U(N)
11 SV=SV+PI(1,N)*V(N)
11 SUX=SUX+DPX(1,N)*U(N)
11 SUY=SUY+DPY(1,N)*U(N)
11 SVX=SVX+DPX(1,N)*V(N)
11 SVY=SVY+DPY(1,N)*V(N)
11 SUXX=SUXX+DPXX(1,N)*U(N)
11 SUXY=SUXY+DPXY(1,N)*U(N)
11 SUYY=SUY+DPYY(1,N)*U(N)
11 SVXX=SVXX+DPXX(1,N)*V(N)
11 SVXY=SVXY+DPXY(1,N)*V(N)
11 SVYY=SVYY+DPYY(1,N)*V(N)
11 YP=YP+PI(1,N)*Y(N)
11 CONTINUE
1 310
1 C
11 C=ACOF*DA*DB*YP
1 C
11 DO 500 IL=1,4
11 DO 500 N=1,NPT
11 DO 500 JL=1,4
11 DO 500 M=1,NPT
11 ANM(IL,JL,N,M)=ANM(IL,JL,N,M)+C*(
* PI(IL,N)*(SVXX*DPY(JL,M)-SVXY*DPX(JL,M)
* -SUXY*DPY(JL,M)+SUY*DPX(JL,M))
* +(SU*DPX(IL,N)+SV*DPY(IL,N))*(DPXX(JL,M)+DPYY(JL,M))
* -(DPXX(IL,N)*DPXX(JL,M)+2.0*DPXY(IL,N)*DPXY(JL,M))
* +DPY(IL,N)*DPY(JL,M))*RENINV
11 BNM(IL,JL,N,M)=BNM(IL,JL,N,M)+C*(
* DPX(IL,N)*DPX(JL,M)+DPY(IL,N)*DPY(JL,M))
11 CONTINUE
1 500
1 300

```



MAIN2

PROJECT: CTJC197  
GROUP: STB1  
TYPE: FORT

MEMBER: MAIN2  
LEVEL: 01.00  
USERID: CTJC197

DATE: 87/09/24  
TIME: 12:02  
PAGE: 35 OF 50

START COL 1-----2-----3-----4-----5-----6-----7-----8

11 B(K)=B(K)+FACT\*B(I)  
1 CONTINUE  
1 5 CONTINUE  
1 C

11 X(N)=B(N)/A(N,NBW1)  
11 NP1=N+1  
11 DO 2 K=1,NM1  
11 SUM=0.0  
11 NMK=N-K  
11 DO 3 J=1,K  
11 JJ=(NP1-J)-NMK+NBW1  
11 IF(JJ.LE.0 .OR. JJ.GT.NBWT) GO TO 3  
11 SUM=SUM+A(NMK,JJ)\*X(NP1-J)  
1 3 CONTINUE  
11 X(NMK)=(B(NMK)-SUM)/A(NMK,NBW1)  
1 2 CONTINUE  
1 C

11 RETURN  
11 END

SUBROUTINE GAUSS(NGG,W,ST)  
DIMENSION W(NGG),ST(NGG)

IF(NGG.EQ.1) GO TO 10  
IF(NGG.EQ.2) GO TO 20  
IF(NGG.EQ.3) GO TO 30  
IF(NGG.EQ.4) GO TO 40  
IF(NGG.EQ.5) GO TO 50  
IF(NGG.EQ.6) GO TO 60

W(1)=2.0  
ST(1)=0.0  
GO TO 70

W(1) = 1.0  
W(2) = W(1)  
ST(1) = -0.577350269  
ST(2) = -ST(1)  
GO TO 70

W(1) = 0.5555555555  
W(2) = 0.8888888888  
W(3) = W(1)  
ST(1) = -0.7745966692  
ST(2) = 0.0  
ST(3) = -ST(1)  
GO TO 70

W(1) = 0.3478548451  
W(2) = 0.6521451548

MAIN2

PROJECT: CTJJC197  
GROUP: STB1  
TYPE: FORT

MEMBER: MAIN2  
LEVEL: 01.00  
USERID: CTJJC197

DATE: 87/09/24  
TIME: 12:02  
PAGE: 36 OF 50

START COL 1-----2-----3-----4-----5-----6-----7-----8

```

7 W(3) = W(2)
7 W(4) = W(1)
7 ST(1) = -0.8611363115
7 ST(2) = -0.3399810435
7 ST(3) = -ST(2)
7 ST(4) = -ST(1)
7 GO TO 70
1 C
2 50 W(1) = 0.2369268850
7 W(2) = 0.478628674
7 W(3) = 0.5688888888
7 W(4) = W(2)
7 W(5) = W(1)
7 ST(1) = -0.9061798459
7 ST(2) = -0.5384693101
7 ST(3) = 0.0
7 ST(4) = -ST(2)
7 ST(5) = -ST(1)
7 GO TO 70
1 C
2 60 W(1) = 0.1713244923
7 W(2) = 0.3607615730
7 W(3) = 0.4679139345
7 W(4) = W(3)
7 W(5) = W(2)
7 W(6) = W(1)
7 ST(1) = -0.9324695142
7 ST(2) = -0.6612093864
7 ST(3) = -0.2386191860
7 ST(4) = -ST(3)
7 ST(5) = -ST(2)
7 ST(6) = -ST(1)
1 C
2 70 CONTINUE
1 C
7 RETURN
7 END
1 C
1 C
1 C
1 C

```

```

11 SUBROUTINE INTER(XX,YY,NPT,X,Y,DX,DY,FT,DTA,AA,AB)
1 C
1 C LINEAR INTERPOLATION FUNCTIONS AND THEIR FIRST DERIVATIVES
1 C
1 C DIMENSION X(NPT),Y(NPT),DX(NPT),DY(NPT),FT(NPT)
1 C DIMENSION AA(NPT),AB(NPT),DTJ(2,2)
1 C
1 C FT(1)=0.25*(1.0-XX)*(1.0-YY)
1 C FT(2)=0.25*(1.0+XX)*(1.0-YY)
1 C FT(3)=0.25*(1.0+XX)*(1.0+YY)
1 C FT(4)=0.25*(1.0-XX)*(1.0+YY)
1 C
1 C AA(1)=0.25*(-1.0+YY)
1 C AA(2)=0.25*(1.0-YY)
1 C

```



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MEMBER: MAIN2  
LEVEL: 01.00  
USERID: CTJC197

PROJECT: CTJC197  
GROUP: STB1  
TYPE: FORT

START COL 1-----2-----3-----4-----5-----6-----7-----8

1 C AA(3)=0.25\*( 1.0+YY)  
1 C AA(4)=0.25\*(-1.0-YY)  
1 C  
1 C AB(1)=0.25\*(-1.0+XX)  
1 C AB(2)=0.25\*(-1.0-XX)  
1 C AB(3)=0.25\*( 1.0+XX)  
1 C AB(4)=0.25\*( 1.0-XX)  
1 C

7 XXP1=XX+1.  
7 XXM1=XX-1.  
7 YYP1=YY+1.  
7 YYM1=YY-1.

1 C  
7 AA(1)=.25\*YYM1  
7 AA(2)=-AA(1)  
7 AA(3)=.25\*YYP1  
7 AA(4)=-AA(3)

1 C  
7 AB(1)=.25\*XXM1  
7 AB(3)=.25\*XXP1  
7 AB(2)=-AB(3)  
7 AB(4)=-AB(1)

1 C  
7 FT(1)=AB(1)\*YYM1  
7 FT(2)=AB(2)\*YYM1  
7 FT(3)=AB(3)\*YYP1  
7 FT(4)=AB(4)\*YYP1

1 DO 4 I=1,2  
1 DO 4 J=1,2  
1 DTJ(I,J)=0.0

1 DO 5 N=1,NPT  
1 DTJ(1,1)=DTJ(1,1)+AA(N)\*X(N)  
1 DTJ(1,2)=DTJ(1,2)+AA(N)\*Y(N)  
1 DTJ(2,1)=DTJ(2,1)+AB(N)\*X(N)  
1 DTJ(2,2)=DTJ(2,2)+AB(N)\*Y(N)

1 DTA=DTJ(1,1)\*DTJ(2,2)-DTJ(1,2)\*DTJ(2,1)  
1 DTAINV=1./DTA

1 DO 7 N=1,NPT  
1 DX(N)=( DTJ(2,2)\*AA(N)-DTJ(1,2)\*AB(N))\*DTAINV  
1 DY(N)=(-DTJ(2,1)\*AA(N)+DTJ(1,1)\*AB(N))\*DTAINV  
1 CONTINUE

1 RETURN  
1 END

1 SUBROUTINE QUADR(AA,AB,X,Y,DX,DY,DXX,DXY,DYY,NPT)  
1 SECOND DERIVATIVES OF INTERPOLATION FUNCTIONS



MAIN2

PROJECT: CTJC197  
GROUP: STB1  
TYPE: FORT

MEMBER: MAIN2  
LEVEL: 01.00  
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START COL -----1-----2-----3-----4-----5-----6-----7-----8

```

2 8 CONTINUE
1 C
11 D11=(DXX1*DY11+DXY1*DYX1)*DY11-2.*DY11*DY11-2.*DYX1*DY11+DXY1*DY11
11 D12=2.*DYX1*DY11+DY11*DY11-2.*DXX1*DY11+DY11*DY11
11 D13=2.*DXX1*DY11+DXY1*DY11-DXX1*DY11*(DXX1*DY11+DXY1*DY11)
11 D21=DXY1*DY11+DXY1*DYX1-DXX1*DY11*DY11+DY11*DY11
11 D22=DXX1*DXX1*DY11+DY11-DXY1*DY11*DY11+DY11*DY11
11 D23=DXY1*DY11+DXX1*DY11-DXY1*DY11*DY11
11 D31=2.*DXX1*DY11+DXY1*DY11-DXY1*DY11*(DXX1*DY11+DXY1*DY11)
11 D32=DXY1*DY11+DXX1*DY11-DXX1*DY11*DY11
11 D33=DXX1*DXX1*(DXX1*DY11+DY11+DXX1)-2.*DXX1*DY11+DXX1*DY11
1 C
1 C
DO 9 N=1,NPT
11 DXX(N)=(D11*DUMXX(N)+D12*DUMXY(N)+D13*DUMYY(N))*DDDINV
11 DXY(N)=(D21*DUMXX(N)+D22*DUMXY(N)+D23*DUMYY(N))*DDDINV
11 DYY(N)=(D31*DUMXX(N)+D32*DUMXY(N)+D33*DUMYY(N))*DDDINV
2 9 CONTINUE
1 C
1 C
RETURN
END
SUBROUTINE HERMT(XI,ETA,DA,DB,PI,DPX,DPY,DPXX,DPXY,DPYY)
HERMITE POLYNOMIAL INTERPOLATION FUNCTIONS
DIMENSION PI(4,4),DPX(4,4),DPY(4,4),DPXX(4,4),DPXY(4,4),
DPYY(4,4)
DAINV4=.25/DA
DBINV4=.25/DB
DA2INV4=DAINV4/DA
DB2INV4=DBINV4/DB
F1X=(2.-3.*XI+XI*XI)*.25
F2X=(2.+3.*XI-XI*XI)*.25
G1X=DA*(1.-XI-XI*XI+XI*XI)*.25
G2X=DA*(-1.-XI+XI*XI+XI*XI)*.25
F1Y=(2.-3.*ETA+ETA*ETA)*.25
F2Y=(2.+3.*ETA-ETA*ETA)*.25
G1Y=DB*(1.-ETA-ETA*ETA+ETA*ETA)*.25
G2Y=DB*(-1.-ETA+ETA*ETA+ETA*ETA)*.25
DF1X=(-3.+3.*XI*XI)*DAINV4
DF2X=(3.-3.*XI*XI)*DAINV4
DG1X=(-1.-2.*XI+3.*XI*XI)*.25
DG2X=(-1.+2.*XI+3.*XI*XI)*.25
DF1Y=(-3.+3.*ETA*ETA)*DBINV4
DF2Y=(3.-3.*ETA*ETA)*DBINV4
DG1Y=(-1.-2.*ETA+3.*ETA*ETA)*.25
DG2Y=(-1.+2.*ETA+3.*ETA*ETA)*.25
DOF1X=6.*XI*DA2INV4

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MAIN2

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LEVEL: 01.00  
USERID: CTJUC197

PROJECT: CTJUC197  
GROUP: STB1  
TYPE: FORT

START COL 1-----2-----3-----4-----5-----6-----7-----8

11 DDF2X=-6.\*XI\*DA2IN4  
11 DDG1X=(-2.+6.\*XI)\*DAINV4  
11 DDG2X=( 2.+6.\*XI)\*DAINV4  
1 C

11 DDF1Y=6.\*ETA\*DB2IN4  
11 DDF2Y=-6.\*ETA\*DB2IN4  
11 DDG1Y=(-2.+6.\*ETA)\*DBINV4  
11 DDG2Y=( 2.+6.\*ETA)\*DBINV4  
1 C

11 PI(1,1)=F1X\*F1Y  
11 PI(1,2)=F2X\*F1Y  
11 PI(1,3)=F2X\*F2Y  
11 PI(1,4)=F1X\*F2Y  
11 PI(2,1)=G1X\*F1Y  
11 PI(2,2)=G2X\*F1Y  
11 PI(2,3)=G2X\*F2Y  
11 PI(2,4)=G1X\*F2Y  
11 PI(3,1)=F1X\*G1Y  
11 PI(3,2)=F2X\*G1Y  
11 PI(3,3)=F2X\*G2Y  
11 PI(3,4)=F1X\*G2Y  
11 PI(4,1)=G1X\*G1Y  
11 PI(4,2)=G2X\*G1Y  
11 PI(4,3)=G2X\*G2Y  
11 PI(4,4)=G1X\*G2Y  
1 C

11 DPX(1,1)=DF1X\*F1Y  
11 DPX(1,2)=DF2X\*F1Y  
11 DPX(1,3)=DF2X\*F2Y  
11 DPX(1,4)=DF1X\*F2Y  
11 DPX(2,1)=DG1X\*F1Y  
11 DPX(2,2)=DG2X\*F1Y  
11 DPX(2,3)=DG2X\*F2Y  
11 DPX(2,4)=DG1X\*F2Y  
11 DPX(3,1)=DF1X\*G1Y  
11 DPX(3,2)=DF2X\*G1Y  
11 DPX(3,3)=DF2X\*G2Y  
11 DPX(3,4)=DF1X\*G2Y  
11 DPX(4,1)=DG1X\*G1Y  
11 DPX(4,2)=DG2X\*G1Y  
11 DPX(4,3)=DG2X\*G2Y  
11 DPX(4,4)=DG1X\*G2Y  
1 C

11 DPY(1,1)=F1X\*DF1Y  
11 DPY(1,2)=F2X\*DF1Y  
11 DPY(1,3)=F2X\*DF2Y  
11 DPY(1,4)=F1X\*DF2Y  
11 DPY(2,1)=G1X\*DF1Y  
11 DPY(2,2)=G2X\*DF1Y  
11 DPY(2,3)=G2X\*DF2Y  
11 DPY(2,4)=G1X\*DF2Y  
11 DPY(3,1)=F1X\*DG1Y  
11 DPY(3,2)=F2X\*DG1Y  
11 DPY(3,3)=F2X\*DG2Y  
11

START COL -----1-----2-----3-----4-----5-----6-----7-----8

11	DPY(3,4)=F1X*DG2Y
11	DPY(4,1)=G1X*DG1Y
11	DPY(4,2)=G2X*DG1Y
11	DPY(4,3)=G2X*DG2Y
11	DPY(4,4)=G1X*DG2Y
11	DPXX(1,1)=DDF1X*F1Y
11	DPXX(1,2)=DDF2X*F1Y
11	DPXX(1,3)=DDF2X*F2Y
11	DPXX(1,4)=DDF1X*F2Y
11	DPXX(2,1)=DDG1X*F1Y
11	DPXX(2,2)=DDG2X*F1Y
11	DPXX(2,3)=DDG2X*F2Y
11	DPXX(2,4)=DDG1X*F2Y
11	DPXX(3,1)=DDF1X*G1Y
11	DPXX(3,2)=DDF2X*G1Y
11	DPXX(3,3)=DDF2X*G2Y
11	DPXX(3,4)=DDF1X*G2Y
11	DPXX(4,1)=DDG1X*G1Y
11	DPXX(4,2)=DDG2X*G1Y
11	DPXX(4,3)=DDG2X*G2Y
11	DPXX(4,4)=DDG1X*G2Y
11	DPYY(1,1)=F1X*DDF1Y
11	DPYY(1,2)=F2X*DDF1Y
11	DPYY(1,3)=F2X*DDF2Y
11	DPYY(1,4)=F1X*DDF2Y
11	DPYY(2,1)=G1X*DDF1Y
11	DPYY(2,2)=G2X*DDF1Y
11	DPYY(2,3)=G2X*DDF2Y
11	DPYY(2,4)=G1X*DDF2Y
11	DPYY(3,1)=F1X*DDG1Y
11	DPYY(3,2)=F2X*DDG1Y
11	DPYY(3,3)=F2X*DDG2Y
11	DPYY(3,4)=F1X*DDG2Y
11	DPYY(4,1)=G1X*DDG1Y
11	DPYY(4,2)=G2X*DDG1Y
11	DPYY(4,3)=G2X*DDG2Y
11	DPYY(4,4)=G1X*DDG2Y
11	DPXY(1,1)=DF1X*DF1Y
11	DPXY(1,2)=DF2X*DF1Y
11	DPXY(1,3)=DF2X*DF2Y
11	DPXY(1,4)=DF1X*DF2Y
11	DPXY(2,1)=DG1X*DF1Y
11	DPXY(2,2)=DG2X*DF1Y
11	DPXY(2,3)=DG2X*DF2Y
11	DPXY(2,4)=DG1X*DF2Y
11	DPXY(3,1)=DF1X*DG1Y
11	DPXY(3,2)=DF2X*DG1Y
11	DPXY(3,3)=DF2X*DG2Y
11	DPXY(3,4)=DF1X*DG2Y
11	DPXY(4,1)=DG1X*DG1Y
11	DPXY(4,2)=DG2X*DG1Y

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MEMBER: MAIN2  
GROUP: STB1  
LEVEL: 01.00  
TYPE: FORT  
USERID: CTJC197

PROJECT: CTJC197  
MEMBER: MAIN2  
GROUP: STB1  
LEVEL: 01.00  
TYPE: FORT  
USERID: CTJC197

START COL 1-----2-----3-----4-----5-----6-----7-----8

```

11      DPXY(4,3)=DG2X+DG2Y
11      DPXY(4,4)=DG1X+DG2Y
1   C      RETURN
11      END
7   SUBROUTINE CONVRT
6   $( N, A, NA, B, NB, X, NX )
7   COMPLEX A(NA,N)
7   COMPLEX B(NB,N)
7   COMPLEX W
7   COMPLEX X(NX,N)
7   COMPLEX Y
7   COMPLEX Z
1   C      REAL C
7   REAL D
1   C      INTEGER I
7   INTEGER II
7   INTEGER IMJ
7   INTEGER IMI
7   INTEGER IP1
7   INTEGER J
7   INTEGER JM2
7   INTEGER JP1
7   INTEGER K
7   INTEGER N
7   INTEGER NA
7   INTEGER NB
7   INTEGER NM1
7   INTEGER NM2
7   INTEGER NX
1   C      LUWT = 6
7   NM1 = N - 1
7   DO 80 I=1,NM1
7   D = O.O
7   IP1 = I + 1
7   DO 10 K=IP1,N
7   Y = B(K,I)
7   C = ABS(REAL(Y)) + ABS(AIMAG(Y))
7   IF( C.LE.D ) GO TO 9
7   D = C
7   II = K
5   CONTINUE
10  CONTINUE
7   IF( D.EQ.O.O ) GO TO 78
7   Y = B(I,I)
7   IF( D.LE.ABS(REAL(Y)) + ABS(AIMAG(Y)) ) GO TO 40
7   DO 20 J=1,N
7   Y = A(I,J)
7   A(I,J) = A(II,J)
7   A(II,J) = Y

```

530970  
530980  
530990  
531000  
531010  
531020  
531030  
531040  
531050  
531060  
531070  
531080  
531090  
531100  
531110  
531120  
531130  
531140  
531150  
531160  
531170  
531180  
531190  
531200  
531210  
531220  
531230  
531240  
531250  
531260  
531270  
531280  
531290  
531300  
531310  
531320  
531330  
531340  
531350  
531360  
531370  
531380  
531390  
531400  
531410  
531420  
531430  
531440  
531450

PROJECT: CTJC197  
GROUP: STB1  
TYPE: FORT

MEMBER: MAIN2  
LEVEL: 01.00  
USERID: CTJC197

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START COL -----1-----2-----3-----4-----5-----6-----7-----8

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4 20 CONTINUE
7 DO 30 J=1,N
7 Y = B(I,J)
7 B(I,J) = B(II,J)
7 B(II,J) = Y
4 30 CONTINUE
4 40 CONTINUE
7 DO 70 J=IP1,N
7 Y = B(J,I)/B(I,I)
7 IF( REAL(Y).EQ.O.O .AND. AIMAG(Y).EQ.O.O ) GO TO 68
7 DO 50 K=1,N
7 A(J,K) = A(J,K) - Y*A(I,K)
4 50 CONTINUE
7 DO 60 K=IP1,N
7 B(J,K) = B(J,K) - Y*B(I,K)
4 60 CONTINUE
4 68 CONTINUE
4 70 CONTINUE
7 B(IP1,I) = CMPLX(O.O,O.O)
4 78 CONTINUE
4 80 CONTINUE
1 C
7 DO 100 I=1,N
7 DO 90 J=1,N
7 X(I,J) = CMPLX(O.O,O.O)
4 90 CONTINUE
7 X(I,I) = CMPLX(1.O,O.O)
3 100 CONTINUE
1 C
7 NM2 = N - 2
7 IF( NM2.LT.1 ) GO TO 270
7 DO 260 J=1,NM2
7 JM2 = NM1 - J
7 JP1 = J + 1
7 DO 250 II=1,JM2
7 I = N + 1 - II
7 IM1 = I - 1
7 IMJ = I - J
1 C
7 W = A(I,J)
7 Z = A(IM1,J)
7 IF( ABS(REAL(W)) + ABS(AIMAG(W)).LE.
6 $ ABS(REAL(Z)) + ABS(AIMAG(Z)) ) GO TO 140
7 DO 120 K=J,N
7 Y = A(I,K)
7 A(I,K) = A(IM1,K)
7 A(IM1,K) = Y
3 120 CONTINUE
7 DO 130 K=IM1,N
7 Y = B(I,K)
7 B(I,K) = B(IM1,K)
7 B(IM1,K) = Y
3 130 CONTINUE
3 140 CONTINUE
531460
531470
531480
531490
531500
531510
531520
531530
531540
531550
531560
531570
531580
531590
531600
531610
531620
531630
531640
531650
531660
53167
531680
531690
531700
531710
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531800
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531910
531920
531930
531940
531950
531960
531970
531980
531990

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PROJECT: CTJC197  
GROUP: STB1  
TYPE: FORT

MEMBER: MAIN2  
LEVEL: 01.00  
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START COL 1 2 3 4 5 6 7 8

```

1 C
7 Z = A(I,J)
7 IF( REAL(Z).EQ.O.O .AND. AIMAG(Z).EQ.O.O ) GO TO 170
7 Y = Z/A(IM1,J)
7 DO 150 K=JP1,N
7 A(I,K) = A(I,K) - Y*A(IM1,K)
7 150 CONTINUE
7 DO 160 K=IM1,N
7 B(I,K) = B(I,K) - Y*B(IM1,K)
7 160 CONTINUE
7 170 CONTINUE
7 C
7 W = B(I,IM1)
7 Z = B(I,I)
7 IF( ABS(REAL(W)) + ABS(AIMAG(W)) .LE.
6 $ ABS(REAL(Z)) + ABS(AIMAG(Z)) ) GO TO 210
7 DO 180 K=1,I
7 Y = B(K,I)
7 B(K,I) = B(K,IM1)
7 B(K,IM1) = Y
7 180 CONTINUE
7 DO 190 K=1,N
7 Y = A(K,I)
7 A(K,I) = A(K,IM1)
7 A(K,IM1) = Y
7 190 CONTINUE
7 DO 200 K=IMJ,N
7 Y = X(K,I)
7 X(K,I) = X(K,IM1)
7 X(K,IM1) = Y
7 200 CONTINUE
7 210 CONTINUE
7 C
7 Z = B(I,IM1)
7 IF( REAL(Z).EQ.O.O .AND. AIMAG(Z).EQ.O.O ) GO TO 249
7 Y = Z/B(I,I)
7 DO 220 K=1,IM1
7 B(K,IM1) = B(K,IM1) - Y*B(K,I)
7 220 CONTINUE
7 B(I,IM1) = CMPLX(O.O,O.O)
7 DO 230 K=1,N
7 A(K,IM1) = A(K,IM1) - Y*A(K,I)
7 230 CONTINUE
7 DO 240 K=IMJ,N
7 X(K,IM1) = X(K,IM1) - Y*X(K,I)
7 240 CONTINUE
7 249 CONTINUE
7 C
7 250 CONTINUE
7 A(JP1+1,J) = CMPLX(O.O,O.O)
7 260 CONTINUE
7 270 CONTINUE
7 C
7 RETURN

```

532000  
532010  
532020  
532030  
532040  
532050  
53767  
532070  
532080  
532090  
532100  
532110  
532120  
532130  
532140  
532150  
532160  
532170  
532180  
532190  
532200  
532210  
532220  
532230  
532240  
532250  
532260  
532270  
532280  
532290  
532300  
532310  
532320  
532330  
532340  
532350  
532360  
532370  
532380  
532390  
532400  
532410  
532420  
532430  
532440  
532450  
532460  
532470  
532480  
532490  
532500  
532510  
532520  
532530





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START COL -----1-----2-----3-----4-----5-----6-----7-----8-----
7 IF( BNI.GT.BNORM ) BNORM = BNI 533080
4 30 CONTINUE 533090
1 C 533100
7 IF( ANORM.EQ.O.O ) ANORM = 1.0 533110
7 IF( BNORM.EQ.O.O ) BNORM = 1.0 533120
7 EPSA = ANORM 533130
7 EPSB = BNORM 533140
4 40 CONTINUE 533150
7 EPSA = EPSA/2.0 533160
7 EPSB = EPSB/2.0 533170
7 C = ANORM + EPSA 533180
7 IF( C.GT.ANORM ) GO TO 40 533190
7 IF( N.LE.1 ) GO TO 320 533200
4 50 CONTINUE 533210
7 ITS = 0 533220
7 NM1 = NN - 1 533230
4 60 CONTINUE 533240
7 D2 = ABS(REAL(A(NN,NN))) + ABS(AIMAG(A(NN,NN))) 533250
7 DO 70 LB=2,NN 533260
7 L = NN + 2 - LB 533270
7 SS = D2 533280
7 Y = A(L-1,L-1) 533290
7 D2 = ABS(REAL(Y)) + ABS(AIMAG(Y)) 533300
7 SS = SS + D2 533310
7 Y = A(L,L-1) 533320
7 R = SS + ABS(REAL(Y)) + ABS(AIMAG(Y)) 533330
7 IF( R.EQ.SS ) GO TO 80 533340
4 70 CONTINUE 533350
7 L = 1 533360
4 80 CONTINUE 533370
7 IF( L.EQ.NN ) GO TO 320 533380
7 IF( ITS.LT.30 ) GO TO 90 533390
7 ITER(NN) = -1 533400
7 IF( ABS(REAL(A(NN,NN))) + ABS(AIMAG(A(NN,NN))) .GT. 533410
6 $.8*ABS(REAL(ANNM1)) + ABS(AIMAG(ANNM1)) ) GO TO 999 533420
4 90 CONTINUE 533430
7 IF( ITS.EQ.10 .OR. ITS.EQ.20 ) GO TO 110 533440
1 C 533450
7 ANNM1 = A(NN,NNM1) 533460
7 ANM1M1 = A(NM1,NNM1) 533470
7 S = A(NN,NN)*B(NM1,NNM1) - ANNM1*B(NM1,NN) 533480
7 W = ANNM1*B(NN,NN)* 533490
6 $ (A(NM1,NN)*B(NM1,NNM1) - ANM1M1*B(NM1,NN)) 533500
7 Y = (ANNM1*B(NN,NN) - S)/2.0 533510
7 Z = CSQRT(Y*Y + W) 533520
7 IF( REAL(Z).EQ.O.O .AND. AIMAG(Z).EQ.O.O ) GO TO 100 533530
7 DO = REAL(Y/Z) 533540
7 IF( DO.LT.O.O ) Z = -Z 533550
3 100 CONTINUE 533560
7 DEN = (Y + Z)*B(NM1,NNM1)*B(NN,NN) 533570
7 IF( REAL(DEN).EQ.O.O .AND. 533580
6 $ AIMAG(DEN).EQ.O.O ) 533590
6 $DEN = CMPLX(EPSA,O.O) 533600
7 NUM = (Y + Z)*S - W 533610

```

MAIN2

PROJECT: CTJJC197  
GROUP: STB1  
TYPE: FORT

MEMBER: MAIN2  
LEVEL: 01.00  
USERID: CTJJC197

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START  
GOL -----1-----2-----3-----4-----5-----6-----7-----+-----8

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7 GO TO 120
3 110 CONTINUE
7 Y = A(NM1,NN-2)
7 NUM = CMPLX(ABS(REAL(ANNM1)) + ABS(AIMAG(ANNM1)),
6 $ ABS(REAL(Y)) + ABS(AIMAG(Y)))
7 DEN = CMPLX(1.0,0.0)
3 120 CONTINUE
7 IF( NV.EQ.L+1 ) GO TO 140
7 D1 = ABS(REAL(A(NN,NN))) + ABS(AIMAG(A(NN,NN)))
7 D2 = ABS(REAL(A(NM1,NN1))) + ABS(AIMAG(A(NM1,NN1)))
7 E1 = ABS(REAL(ANNM1)) + ABS(AIMAG(ANNM1))
7 NL = NN - (L + 1)
7 DD 130 MB=1,NL
7 M = NN - MB
7 EO = E1
7 Y = A(M,M-1)
7 E1 = ABS(REAL(Y)) + ABS(AIMAG(Y))
7 DO = D1
7 D1 = D2
7 Y = A(M-1,M-1)
7 D2 = ABS(REAL(Y)) + ABS(AIMAG(Y))
7 Y = A(M,M)*DEN - B(M,M)*NUM
7 DO = (DO + D1 + D2)*( ABS(REAL(Y)) + ABS(AIMAG(Y)) )
7 EO = EO*E1*( ABS(REAL(DEN)) + ABS(AIMAG(DEN)) ) + DO
7 IF( EO.EQ.DO ) GO TO 150
3 130 CONTINUE
3 140 CONTINUE
7 M = L
3 150 CONTINUE
7 ITS = ITS + 1
7 W = A(M,M)*DEN - B(M,M)*NUM
7 Z = A(M+1,M)*DEN
7 D1 = ABS(REAL(Z)) + ABS(AIMAG(Z))
7 D2 = ABS(REAL(W)) + ABS(AIMAG(W))
7 LOR1 = 1
7 NNORN = N
7 DO 310 I=M,NN1
7 J = I + 1
7 IF( I.EQ.M ) GO TO 170
7 W = A(I,I-1)
7 Z = A(J,I-1)
7 D1 = ABS(REAL(Z)) + ABS(AIMAG(Z))
7 D2 = ABS(REAL(W)) + ABS(AIMAG(W))
7 IF( D1.EQ.O.O ) GO TO 60
3 170 CONTINUE
7 IF( D2.GT.D1 ) GO TO 190
7 DO 180 K=I,NNORN
7 Y = A(I,K)
7 A(I,K) = A(J,K)
7 A(J,K) = Y
7 Y = B(I,K)
7 B(I,K) = B(J,K)
7 B(J,K) = Y
3 180 CONTINUE

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PROJECT: CTJC197  
GROUP: STB1  
TYPE: FORT

MEMBER: MAIN2  
LEVEL: 01.00  
USERID: CTJC197

DATE: 87/09/24  
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7 IF( I.GT.M ) A(I,I-1) = A(J,I-1)
7 IF( D2.EQ.O.O ) GO TO 220
7 Y = CMPLX( REAL(W)/D1, AIMAG(W)/D1 )/
6 $ CMPLX( REAL(Z)/D1, AIMAG(Z)/D1 )
7 GO TO 200
3 190 CONTINUE
7 Y = CMPLX( REAL(Z)/D2, AIMAG(Z)/D2 )/
6 $ CMPLX( REAL(W)/D2, AIMAG(W)/D2 )
3 200 CONTINUE
7 DO 210 K=I,NNORN
7 A(J,K) = A(J,K) - Y*A(I,K)
7 B(J,K) = B(J,K) - Y*B(I,K)
3 210 CONTINUE
3 220 CONTINUE
7 IF( I.GT.M ) A(J,I-1) = CMPLX(O.O.O.O)
7 Z = B(J,I)
7 W = B(J,J)
7 D1 = ABS(REAL(Z)) + ABS(AIMAG(Z))
7 D2 = ABS(REAL(W)) + ABS(AIMAG(W))
7 IF( D1.EQ.O.O ) GO TO 60
7 IF( D2.GT.D1 ) GO TO 270
7 DO 230 K=LOR1,J
7 Y = A(K,J)
7 A(K,J) = A(K,I)
7 A(K,I) = Y
7 Y = B(K,J)
7 B(K,J) = B(K,I)
7 B(K,I) = Y
3 230 CONTINUE
7 IF( I.EQ.NM1 ) GO TO 240
7 Y = A(J+1,J)
7 A(J+1,J) = A(J+1,I)
7 A(J+1,I) = Y
3 240 CONTINUE
7 DO 250 K=1,N
7 Y = X(K,J)
7 X(K,J) = X(K,I)
7 X(K,I) = Y
3 250 CONTINUE
7 B(J,I) = CMPLX(O.O.O.O)
7 IF( D2.EQ.O.O ) GO TO 310
7 Z = CMPLX( REAL(W)/D1, AIMAG(W)/D1 )/
6 $ CMPLX( REAL(Z)/D1, AIMAG(Z)/D1 )
7 GO TO 280
3 270 CONTINUE
7 Z = CMPLX( REAL(Z)/D2, AIMAG(Z)/D2 )/
6 $ CMPLX( REAL(W)/D2, AIMAG(W)/D2 )
3 280 CONTINUE
7 DO 290 K=LOR1,J
7 A(K,I) = A(K,I) - Z*A(K,J)
7 B(K,I) = B(K,I) - Z*B(K,J)
3 290 CONTINUE
7 B(J,I) = CMPLX(O.O.O.O)
7 IF( I.LT.NM1 ) A(I+2,I) = A(I+2,I) - Z*A(I+2,J)

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MAIN2

PROJECT: CTJJC197  
GROUP: STB1  
TYPE: FORT

MEMBER: MAIN2  
LEVEL: 01.00  
USERID: CTJJC197

DATE: 87/09/24  
TIME: 12:02  
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7 DO 300 K=1,N
7 X(K,I) = X(K,I) - Z*X(K,J)
3 300 CONTINUE
3 310 CONTINUE
3 GO TO 60
3 320 CONTINUE
7 EIGA(NN) = A(NN,NN)
7 EIGB(NN) = B(NN,NN)
7 IF( NN.EQ.1 ) GO TO 330
7 ITER(NN) = ITS
7 NN = NN1
7 IF( NN.GT.1 ) GO TO 50
7 ITER(1) = 0
7 GO TO 320
3 330 CONTINUE
7 M = N
3 340 CONTINUE
7 ALFM = A(M,M)
7 BETM = B(M,M)
7 B(M,M) = CMPLX(1.0,0.0)
7 L = M - 1
7 IF( L.EQ.0 ) GO TO 370
3 350 CONTINUE
7 L1 = L + 1
7 SL = CMPLX(0.0,0.0)
7 DO 360 J=L1,M
7 SL = SL + B(J,M)*(BETM*A(L,J) - ALFM*B(L,J))
3 360 CONTINUE
7 Y = BETM*A(L,L) - ALFM*B(L,L)
7 IF( REAL(Y).EQ.0.0 .AND.
6 $ AIMAG(Y).EQ.0.0 )
6 $ Y = CMPLX( (EPSA+EPSB)/2.0, 0.0 )
7 B(L,M) = -SL/Y
7 L = L - 1
3 370 CONTINUE
7 IF( L.GT.0 ) GO TO 350
7 M = M - 1
7 IF( M.GT.0 ) GO TO 340
7 M = N
3 380 CONTINUE
7 DO 400 I=1,N
7 S = CMPLX(0.0,0.0)
7 DO 390 J=1,M
7 S = S + X(I,J)*B(J,M)
3 390 CONTINUE
7 X(I,M) = S
3 400 CONTINUE
7 M = M - 1
7 IF( M.GT.0 ) GO TO 380
7 M = N
3 410 CONTINUE
7 SS = 0.0
7 DO 420 I=1,N
7 R = ABS(REAL(X(I,M))) + ABS(AIMAG(X(I,M)))

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MAIN2

PROJECT: CTJC197  
GROUP: STB1  
TYPE: FORT

MEMBER: MAIN2  
LEVEL: 01.00  
USERID: CTJC197

DATE: 87/09/24  
TIME: 12:02  
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START COL 1-----2-----3-----4-----5-----6-----7-----8

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7 IF( R.LT.SS ) GO TO 418
7 SS = R
7 D = X(I,M)
3 418 CONTINUE
3 420 CONTINUE
7 IF( SS.EQ.O.O ) GO TO 440
7 DO 430 I=1,N
7 X(I,M) = X(I,M)/D
3 430 CONTINUE
3 440 CONTINUE
7 M = M - 1
7 IF( M.GT.O ) GO TO 410
3 999 CONTINUE
7 RETURN
7 END
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