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Program: Wake Properties  
of the Galileo Probe at Mach  
Numbers From 0.25 to 0.95**

Thomas N. Canning  
*Portola Valley, California*

Thomas M. Edwards  
*Ames Research Center  
Moffett Field, California*

## GALILEO PROBE PARACHUTE TEST PROGRAM:

### WAKE PROPERTIES OF THE GALILEO PROBE AT MACH NUMBERS FROM 0.25 TO 0.95

Thomas N. Canning\* and Thomas M. Edwards

Ames Research Center

#### SUMMARY

*The results of surveys of the near and far wake of the Galileo Probe are presented for Mach numbers from 0.25 to 0.95. The trends in the data resulting from changes in Mach number, radial and axial distance, angle of attack, and a small change in model shape are shown in crossplots based on the data. A rationale for selecting an operating volume suitable for parachute inflation based on low Mach number flight results is outlined.*

#### INTRODUCTION

The deployment, inflation, performance, and stability of a parachute in the wake of a payload to which it is attached are frequently sensitive to the velocity gradients of the wake itself. This sensitivity is expected to be particularly great for cases in which the wake diameter is comparable to that of the parachute because the radial velocity gradient is largest at the periphery of the parachute before the parachute is fully open. That is to say, a very small parachute (such as a drogue) may deploy and inflate satisfactorily in a large wake (because only small differences of imposed velocity occur near it), whereas a somewhat larger parachute might inflate slowly or not at all. In contrast, the larger parachute may inflate satisfactorily in the wake of a small payload — the usual configuration employed in parachute development and structural tests. The descent parachute configuration of the Pioneer Venus Large Probe (ref. 1) is believed to have exhibited a "reluctance" to open at Mach numbers above 0.6 both for the system tests in the Earth's atmosphere and for the actual Probe during its flight in the atmosphere of Venus. The rather gradual inflation did not compromise the collection of scientific data in the Venutian atmosphere because no critical events, such as entering a recognized cloud layer, occurred before the altitude for parachute deployment and inflation. In the case of the Galileo Probe (ref. 2), on the other hand, it is most important to deploy and inflate the parachute somewhat earlier, i.e., at higher Mach number, in order to remove the instrumented descent configuration from the aeroshell and permit operation of the cloud-analysis instrument before entering the first clouds in the postulated atmosphere of Jupiter.

During Earth-based flight tests to verify adequate system behavior for the Galileo flight conditions, however, the inflation was achieved at an undesirably low Mach number; once inflation was complete, the performance and stability proved to be the same as the earlier tests and flights. Rather than accept the loss of the scientific data and the risk of even further delayed inflation for the flight in the atmosphere of Jupiter, it was decided to investigate the reasons for the marginal behavior and to seek means to ensure prompt inflation at the desired flight Mach number. In order to relate the anticipated wake-survey data to the earlier experience, tests at conditions spanning those for both Venus and Jupiter were desired. Two types of tests were believed necessary in order to guide decisions on design variations: wake-flow surveys and tests of scale model parachutes. This report describes the wake-flow study and suggests a simple rationale for employing the summary plots derived from the data. Tests of a scale model parachute are reported in reference 3.

#### TEST EQUIPMENT AND TEST FACILITY

##### Probe Models

The wakes of two one-eighth-scale models (6-in. diameter) of the Galileo Entry Probe aeroshell were surveyed in the NASA Ames 6- by 6-ft transonic wind tunnel to define the initial operating environment of the descent parachute. The principal configuration represented the expected form of the "ablated" Galileo Probe deceleration-module heat shield. The second configuration represented the "ballasted" configuration to be used in a planned system drop test to verify that parachute deployment, inflation, performance, and stability were satisfactory. The two model profiles are shown in figure 1. In addition to matching the forebody profile for the

\*Mechanical Engineer, 276 La Cuesta Drive, Portola Valley, CA 94025.

system drop test, the model in figure 1(b) also is essentially the same as that of the Pioneer Venus Large Probe; thus the results from both programs can be directly related. The principal difference between the latter model and the Pioneer Venus Large Probe is the short cylinder between the 45° half-angle cone and the base. In neither case was the form of the afterbody (from the rim of the cylinder aft) made to simulate a real configuration because of the expected insensitivity to the afterbody of the distant wake flow and most of the reverse-flow region. At high Reynolds numbers (above critical for transition), the flow separates at the cone-cylinder junction at subsonic and transonic speed.

The models were affixed to the support structures at a pivot located 0.084 model diameter ahead of the base plane. Thus, when positive angles of attack were set, the center of the model base moved slightly in the direction of negative  $Z$ .

The area surrounding the model noses was covered by a fairly densely spaced single layer of glass spheres out to a radius of 0.167 model diameter to assure early transition to turbulent boundary-layer flow. This feature in combination with the nominal test Reynolds number 1.5 million, was used to assure good simulation of full-scale flow. A brief sequence of tests was run at  $Re_D$  equal to 3 million and showed no alteration of flow patterns.

### Model Supports

Two types of support were used during the tests. All of the data reported herein were obtained with the models supported on the sting-strut assembly shown in figure 2. A few preliminary tests were run with the ablated-form model mounted conventionally on a long slender sting equipped with a fixed rake of five pitot-pressure tubes located 2.6 model diameters from the model base. Tests were conducted with and without the strut in place about 0.3 model diameter from the base. The strut reduced the size of the wake significantly at  $M = 0.95$ ; therefore, the two-diameter extension sting was installed to reduce the interference. Subsequent surveys with the traversing survey probe described later revealed a wake profile which matched that of the sting-mounted model much more closely. Directly comparable tests using only the five-tube probe were not possible, but it was concluded that support interference was reduced to a degree which would allow accurate determination of data trends with Mach number, distance downstream and angle of attack, and model profile. The strut was stabilized with guy wires to avert possible coupled torsion-bending oscillations.

### Wake Survey Apparatus

All of the data presented herein were obtained using the pitot-static probe illustrated in figure 3. Included on this

probe were forward- and aft-facing pitot tubes; the forward-facing tube incorporated a coaxial static-pressure tube as well (four orifices at 0.29 model diameter from its tip). This spacing permitted good determination of flow properties in weak and moderately strong axial pressure gradients. The aft-facing pitot tube was about 1 model diameter downstream of the static-pressure taps, so that strong gradients made interpretation of the data in the reverse-flow region difficult. After completing the far-wake survey, the forward-facing pitot-static probe was accordingly converted to aft-facing (fig. 3(b)) by bending it through 180°. The orifice nearest the inside of this bend was sealed with epoxy to avoid the strongest aerodynamic effects of the bend. Even with this alteration, the strong pressure gradients in the reverse-flow region required that the separation between pitot and static orifices be recognized in obtaining the data. This was accomplished by traversing the probe in increments of 1.75-in. (0.29 model diameter) and using the measurement in adjacent test sequence points to obtain spatially coincident measurements of pitot and static pressures.

The same procedure can, in effect, be achieved with the far-wake results by interpolation of the static-pressure data to obtain coincident determination of the pressures; this has not been done in reducing the data because the gradients there are an order of magnitude less severe than in the reverse-flow region.

Pitot and static-pressure measurements made using probes of this sort are degraded if the local flow is highly inclined (more than 10°) relative to the tube axis. Since this degradation is small for angles less than about 10°, the only regions in the wake where errors are expected to be large are well removed from the axis in the near wake. Approximate numerical analysis of the wake profiles downstream of the model by more than 5 model diameters indicated that radial inflow into the accelerating wake resulted in inclinations of less than 3°. Unsteadiness of the flow in the wake doubtless interfered with the static-pressure determination; since the goal of the present surveys was to determine the qualitative influence of Mach number, position, and angle of attack on dynamic-pressure distribution, the small and slowly changing bias on the static-pressure measurement was ignored in studying the data.

The pitot-static probe was located at the tip of the short radial arm so that as the survey assembly was rolled, the probe moved to the left or right to survey at positions other than the vertical plane of symmetry. The location of the roll mechanism is indicated in figure 4.

Vertical positioning of the survey probe was accomplished by translating the wind tunnel model-support body of revolution (BOR) by simultaneous operation of its two positioning screws. Streamwise positioning of the survey probe was effected by means of the linear-actuator mechanism connected between the probe arm and the roll mechanism. The maximum extension range of the linear actuator was slightly less than 4 model diameters; it was therefore necessary to

position the model-support strut at several stations along the test-section ceiling to achieve the full streamwise array of surveys desired.

### Deflections of Survey Apparatus

As noted above, the entire survey apparatus was cantilevered from a large floor-to-ceiling strut located in the entrance to the wind tunnel diffuser. The maximum cantilever length is approximately 12 ft. Late in the test program it was discovered that aerodynamic loads deflected the apparatus upward by an amount that is believed to be influenced by extension length, dynamic pressure, Mach number, roll position, and position relative to the model's wake. Additionally, backlash in the vertical-positioning drive may have yielded a small irregularity in vertical position, although calibration tests without airflow revealed no such effect greater than about 0.5% of the model diameter. The aerodynamic deflection, on the other hand, produced in one case a deflection of at least 8% of the model diameter. As far as could be determined, this deflection was nearly constant for a given test condition and streamwise position of the survey probe (axial and roll), so that the shapes of the vertical profiles of dynamic pressure, Mach number, etc., were preserved, but the absolute position of the survey probe relative to the model axis was not accurately known. From a study of the flow-profile plots, the effect of the elastic deflection can be seen to yield a "movement" of the wake progressively in the +Z direction as the dynamic pressure increased; i.e., increasing Mach number at constant Reynolds number. A similar lateral deflection may have occurred as well, but observation was not possible.

Interpretations of the profiles of flow properties were therefore based on the assumption that vertical deflection was constant throughout any one run, i.e., vertical traverse. Also, where effects of angle of attack were under study, it was assumed that deflection was independent of angle of attack.

### TESTS

Most of the test period was spent obtaining the complete survey of the static and pitot pressure variations in the wake of the "ablated" model configuration supported on the strut. The matrix of test conditions and survey points is detailed in table 1. The abbreviated test matrix for the second, i.e., "ballasted," model consists of runs 333 through 335. In this listing an entry is made in a column only at the run at which that parameter is changed. The special tests, designed to reveal the extent of support interference on the nominal wake properties, are not included.

The test sequence was dictated by the most efficient use of tunnel time, except that the special support interference

study was accomplished first to obtain early assurance that support interference would not be excessive.

While the test airflow conditions were being established, the survey apparatus was maneuvered into the desired position: for height, Z, by raising the BOR conventionally used for model support, for lateral position, Y, by rotating the roll positioner on the BOR and extending the survey apparatus linear actuator to the desired streamwise position, X. Each run thereafter consisted of a vertical traverse to all the points at which measurements were needed.

Succeeding runs were made at the remaining lateral positions desired for the same axial station before moving to the next axial station. Once the three linear dimensions had been adequately surveyed, the next Mach number was established and the desired spacial survey was completed. The time required to position the survey probe was sufficient to assure equilibration of the pressure sensors without additional delay.

The only occasions requiring breaks in the wind tunnel operation were those to adjust the streamwise location of the model-support strut and its guy wires, adjust the angle of attack of the model (by rotation about the pivot inside the model), or exchange the ablated model for the ballasted model. At each such break in the testing, the glass-bead boundary-layer trip area was inspected and refurbished as needed.

### RESULTS

All of the wake-survey results for both the ablated and ballasted configurations supported on the short sting with strut are provided in table 2. Table 2 has been subdivided into four sections. Sections 2a and 2c present data for the ablated model shape with the pitot-static probe facing forward. Section 2b presents data for the ballasted model profile, and section 2d presents data for the ablated shape with the pitot-static probe facing aft. Data were taken at Mach numbers of 0.25, 0.60, 0.80, 0.85, 0.90, and 0.95 at a Reynolds number of 0.75 million based on model diameter. The pitot-static surveys yielded profiles of Mach number, dynamic pressure, velocity, and static pressure as functions of vertical position relative to the horizontal axis of the small sting at selected lateral positions and several axial stations between 1 and 11 model diameters downstream from the model base.

Definitions of column headings are presented in table 2. To preserve direct accountability of the table, the actual run numbers and order of table 1 may facilitate rapid location of a desired test listing. Gaps in the number sequence represent runs made at a Mach number of 1.1; these runs were deleted because of serious disturbance of the flow by the normal-shock wave upstream of the linear actuator of the survey system.

A few unexplained anomalies have been observed in individual sequence (i.e., data-point) listings. These anomalies have not been deleted.

Selected groups of runs have been plotted and cross-plotted in figures 5 through 8 to reveal the shape, Mach number, distance, and angle-of-attack effects on the properties of the wake. In these plots attention is concentrated on the variation of the ratio of local dynamic pressure to free-stream dynamic pressure. Other parameters, such as velocity or pitot pressure, may be as meaningful in applying the results for various purposes. Sufficient information is tabulated so that such plots may be constructed.

All of the tabulated results, with the exception of runs 367 through 390, are presented with no post-test alteration. These exceptions are the tests made with the modified (reversed by a 180° bend) pitot-static tube. In these tests, very strong axial gradients resulted in a large static pressure difference between the positions of the pitot and static pressure orifices. Therefore, the  $X$  increment used in these tests was selected so that the static pressure determined at a particular sequence point could be used with the pitot pressure obtained at the previous sequence point. The tabulated data have been treated in this manner.

With considerable effort the same kind of correction can be applied to the data from surveys at 3.5 model diameters, and farther, behind the base. There is little to be gained, however, because the pressure gradients are an order of magnitude less severe than in the reverse flow near the model base.

## DISCUSSION OF RESULTS

### Far-Wake Region

The momentum defect in the wake of a simple nonlifting body is directly equivalent to the drag of the body. The wakes of the two aerodynamic models used in this study illustrate that the ballasted model has slightly less drag than the more bluff ablated model used in most of the tests. The profiles of dynamic pressure (fig. 5) show a smaller loss in the wake core of the ballasted model than in the wake core of the ablated model. The extent and precision of the surveys in this study are not sufficient to determine the absolute drag coefficients with great accuracy, but the difference is clear. While the two configurations showed only modest differences in dynamic pressure loss (and gradients of dynamic pressure), much greater changes were observed for the ablated model as Mach number and distance from the model to the survey station were changed. The lower portion of each part of figure 6 illustrates the rapid increase of dynamic pressure in the wake core as the survey station is moved downstream from the wake stagnation point — 0 dynamic

pressure. Even as far downstream as 11 model diameters, the continued recovery toward free-stream conditions is clear.

This acceleration of the wake core is achieved at the cost of deceleration of the airflow immediately outside the wake; at all times the total loss in momentum flux must represent the model drag. This redistribution of momentum is summarized in the contour plots of constant dynamic pressure presented in the upper portions of figure 6. At some distance downstream of the body, probably about 6 model diameters from the base, the profiles become "similar." That is, when normalized to the maximum loss in velocity at the core and to the local wake diameter, the profile plots will remain unchanged. Once similarity is established, the radial gradients are seen to vary as the 1.5 power of the maximum loss at the core.

### The Effects of Angle of Attack

The total drag of bodies like those tested in this study is quite insensitive to angle of attack, for angles of attack very much less than the body cone half angle; therefore the total change in loss of momentum in the wake was correspondingly slight as angle of attack increased to 20°. The generation of even a modest lift force, however, results in the discharge of a trailing vortex system which rolls up into a vortex pair at great distances downstream. This vortex system causes the wake to move in a direction opposite to that of the lift vector. This deflection of the wake is the most prominent feature in the vertical profiles of dynamic pressure ratio at angles of attack of both plus and minus 10° and 20° (fig. 7). The surveys revealed no further major changes in the dynamic pressure profiles.

### Reverse-Flow Region

In deploying the Galileo Probe parachute, it is necessary first to propel a small drogue through the near wake of the probe (where the flow moves toward the base). Further, the drogue must then remove the afterbody heat shield and drag it through the volume of reverse flow before the main parachute can be drawn aft in turn. In order to permit estimation of the performance requirements placed on the drogue, the reverse-flow region was surveyed in detail using the modified pitot-static probe (runs 367 through 390). These data are summarized as contour plots of dynamic pressure in figure 8.

The length of the reverse flow increases significantly as Mach number increases from 0.25 to 0.95. The relative severity of the reverse flow, on the other hand, diminishes.

The dynamic pressure profiles deduced (from crossplotting the data) to act along the axis of the flow core are shown in figure 8.

## APPLICATION OF RESULTS TO DESIGN OF GALILEO PROBE PARACHUTE CONFIGURATION

Experience with the Pioneer Venus Large Probe (ref. 1) and with the System Drop Test Configuration for the Galileo Probe (ref. 2) suggested a "reluctance" to inflate at Mach numbers above 0.60. In these cases the parachutes were deployed at approximately 5.5 Probe diameters behind the Probe base. The present data indicate that at this location and flight speed the loss of dynamic pressure near the wake core was severe and the wake diameter was comparable to that of the parachute itself. It is believed that these features combined to cause poor inflation. The result of increasing the Mach number was to aggravate the loss of dynamic pressure and increase the wake size. A slight aggravation was noted when the blunter shape of the Galileo (ablated form) was substituted for that of the Pioneer Venus Large Probe. In order to promote satisfactory parachute inflation for the more severe Galileo requirements, it is necessary, therefore, to find that region in the wake which appears to be more conducive to reliable inflation than that for the Pioneer Venus case at Mach 0.60.

The mixing of external-flow air with the wake is found to produce a rapidly improving wake profile with increasing distance downstream. A comparison of the appropriate profiles suggests that proper parachute inflation can be achieved for the Galileo at a Mach number of 0.80 by incorporating only a modest increase in deployment distance.

## CONCLUSIONS

The wakes of the Galileo Probe and a system drop test configuration have been surveyed to determine the variation of flow properties between the model base and a station almost 11 model diameters downstream.

It was found that (compared to the Pioneer Venus Large Probe) the wake of the more bluff configuration (the shape representative of the expected ablated heat shield after entry into Jupiter) had slightly larger dynamic pressure losses and that the severity of these losses increased markedly with Mach numbers from 0.25 to 0.95. Further, it was found that entrainment of adjacent air monotonically increased the wake size and the dynamic pressure in the core.

It was also found that the length of the reverse-flow region immediately downstream of the model increased slightly with increasing Mach number whereas the relative severity of the reverse flow diminished substantially.

A simple rationale was described whereby a region in which a parachute might be expected to inflate at high speed may be identified based on successful parachute operation at lower speed.

Ames Research Center

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## REFERENCES

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TABLE 1.— TEST CONDITION LISTING

Run No.	Mach No.	X/D <sub>B</sub>	Y/D <sub>B</sub>	Alpha	Run No.	Mach No.	X/D <sub>B</sub>	Y/D <sub>B</sub>	Alpha
144	0.95	7.0	0.02	0	194	0.95	8.5	-0.45	+20
145		8.5	-0.44		195	0.90	10.9	0	
146		0			196	0.90	8.5		
147		0.44			197	0.85	10.9		
148	0.80	7.0	0		198	0.85	8.5		
149		8.5	-0.44		199	0.80	10.9	0.41	
150		0			200			0	
151		0.44			201			-0.38	
152	0.60	7.0	0		202		8.5		-0.48
153		8.5	-0.44		203			0.43	
154		0			204			0	
155		0.44			205			-0.36	
156	0.95		-0.39		206		10.9		-0.45
157		0			207	0.60		0.41	
158		0.43			208			0	
159		10.5	0.41		209			-0.38	
160		0			210			-0.48	
161		-0.38			211		8.5	0.43	
162		-0.48			212			0	
163		10.0	0		213			-0.36	
164	0.80	10.9	0.41		214		10.9	0.45	
165		0			215	0.25		0.41	
166		-0.38			216			0	
167		-0.48			217			-0.38	
168		10.0	0		218			-0.48	
169	0.60	10.9	0.41		219		8.5	0.43	
170		0			220			0	
171		-0.38			221			-0.36	
172		-0.48			222			-0.45	
173		10.0	0		223	0.95	10.9	0.41	-20
174	0.90	10.9			224			0	
175	0.90	0.85			225			-0.38	
176	0.85	0.85			226			-0.48	
177	0.85	10.9			227		8.5	0.43	
178	0.25		0.41		228			0	
179		0			229			-0.36	
180		-0.38			230			-0.45	
181		-0.48			231	0.90	10.9	0	
182		10.0	0		232	0.90	8.5		
183		7.0	0		233	0.85	10.9		
184		8.5	-0.45		234	0.85	8.5		
185		0			235	0.80	10.9	0.41	
186		0.43			236		0	0	
187	0.95	10.9	0.41	+20	237			-0.38	
188		0			238			-0.48	
189		-0.36			239		8.5	0.43	
190		-0.48			240			0	
191		8.5	0.43		241			-0.36	
192		0			242		10.9	-0.45	
193		-0.36			243	0.60		0.41	

TABLE 1.— CONTINUED

Run No.	Mach No.	$X/D_B$	$Y/D_B$	Alpha	Run No.	Mach No.	$X/D_B$	$Y/D_B$	Alpha
244	0.60	10.9	0	-20	294	0.25	8.5	-0.45	+10
245			-0.38		295	0.95	10.9	0.41	-10
246			-0.48		296			0	
247		8.5	0.43		297			-0.38	
248			0		298			-0.48	
249			-0.36		299		8.5	0.43	
250			-0.45		300			0	
251	0.25	10.9	0.41		301			-0.36	
252			0		302			-0.45	
253			-0.38		303	0.90	10.9	0	
254			-0.48		304	0.90	8.5		
255		8.5	0.43		305	0.85	8.5		
256			0		306	0.85	10.9		
257			-0.36		307	0.80		0.41	
258			-0.45		308			0	
259	0.95	10.9	0.41	+10	309			-0.38	
260			0		310			-0.48	
261			-0.38		311		8.5	0.43	
262			-0.48		312			0	
263		8.5	0.43		313			-0.36	
264			0		314	0.60	10.9	-0.45	
265			-0.36		315			0.41	
266			-0.45		316			0	
267	0.90	10.9	0		317			-0.38	
268	0.90	8.5			318			-0.48	
269	0.85	10.9			319		8.5	0.43	
270	0.85	8.5			320			0	
271	0.80	10.9	0.41		322	0.25	10.9	-0.45	
272			0		323			0.41	
273			-0.38		324			0	
274			-0.48		325			-0.38	
275		8.5	0.43		326			-0.48	
276			0		327		8.5	0.43	
277			-0.36		328			0	
278			-0.45		329			-0.36	
279	0.60	10.9	0.41		330			-0.45	
280			0		333	0.95	5.5	0	
281			-0.38		334	0.80			
282			-0.48		335	0.25			
283		8.5	0.43		340	0.95	3.5		
284			0		341		5.5	0.44	
285			-0.36		342			0	
286			-0.45		343			-0.44	
287	0.25	10.9	0.41		344		7.0	0	
288			0		345	0.90	7.0		
289			-0.38		346		5.5		
290			-0.48		347		3.5		
291		8.5	0.43		349	0.85	7.0		
292			0		350		5.5		
293			-0.36		351		3.5		

TABLE 1.— CONCLUDED

Run No.	Mach No.	$X/D_B$	$Y/D_B$	Alpha	Run No.	Mach No.	$X/D_B$	$Y/D_B$	Alpha
352	0.80	3.5	0	0	372	0.90	0.25	0	0
353		5.5	0.44		373		0.40		
354			0		374		0.50		
355			-0.44		375	0.85	0.17		
356		7.0			376		0.25		
357	0.60	7.0			377		0.40		
358		5.5	0.44		378		0.50		
359			0		379	0.80	0.17		
360			-0.44		380		0.25		
361		3.5	0		381		0.40		
362	0.25	3.5	0		382		0.50		
363		5.5	0.44		383	0.60	0.18		
364			0		384		0.25		
365			-0.44		385		0.40		
366		7.0	0		386		0.50		
367	0.95	0.17			387	0.25	0.18		
368		0.25			388		0.25		
369		0.40			389		0.40		
370		0.50			390		0.50		
371	0.90	0.17							

TABLE 2.— MEASURED WAKE PROPERTIES

	Heading Definitions
Run:	Serial number within the test program.
Test P TN:	Identifier for the entire test program.
CONF:	Configuration of model and support system.
5	Ablated model mounted on short sting and strut supported from ceiling of wind tunnel test section; forward-facing pitot-static probe. (Sections 2a and 2c.)
6	Ballast-profile model supported as in 5. (Section 2b.)
7	Ablated model supported as in 5, except that pitot-static probe is bent to face downstream. (Section 2d.)
Mach:	Mach number in free-stream wind tunnel flow.
RN/L:	Reynolds number per unit length (1 ft) in free-stream flow.
PT:	Pressure in stagnation chamber upstream of wind tunnel test section, pounds per square foot.
Q:	Dynamic pressure of wind tunnel free-stream airflow. $Q = 0.7 M^2 \times P$ , pounds per square foot.
P:	Static pressure of wind tunnel free-stream airflow, pounds per square foot.
TT:	Temperature of air in stagnation chamber of wind tunnel, °F.
Alpha:	Inclination of model axis to an intersecting line parallel to the free-stream direction.
Seq:	Serial number of data record within run.
X/DB:	Distance from model base to streamwise station of pitot orifice on pitot-static tube, diameters of model base.
Y/DB:	Horizontal component of distance from axis of short sting to pitot orifice on pitot static tube, diameters of model base.
Z/DB:	Vertical component of distance from axis of small sting to pitot orifice of pitot-static probe, diameters of model base.
MF/M:	Ratio of Mach number determined from measured pitot and static pressures on the pitot-static probe to Mach.
MA/M:	As above, but using the pressure acting on the aft-facing pitot probe.
QF/Q:	Ratio of dynamic pressure acting on pitot-static probe to the free-stream dynamic pressure.
QA/Q:	As above, but using the pressure acting on the aft-facing pitot tube.
VF/V:	Ratio of air velocity deduced from pitot-static tube to free-stream velocity.
VA/V:	As above but using aft-facing pitot tube.
CP:	Static pressure acting on pitot-static probe minus free-stream static pressure, all divided by free-stream dynamic pressure. $CP = (PF - P)/Q$ .
PF:	Static pressure acting on static pressure orifices of pitot-static probe, pounds per square foot.
PF/P:	Ratio of static pressure acting on pitot-static probe to free-stream static pressure.

**Table 2(a)**

**Configuration 5 – Ablated model mounted on short sting and strut supported from ceiling of wind tunnel test section:  
forward-facing pitot-static probe.**

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RUN	TST	P	TN	CCNF	MACH	RN/L	PT	C	P	TT	ALPHA
SEQ	MACH	Q	X/DR	Y/DB	Z/DR	MF/N	MA/N	QF/Q	QA/Q	VF/V	V A/V
144	571	1	66	5	0.948	1.480	687	242.6	385	69.1	0.00
1	0.948	242.6	7.04	0.02	-2.02	0.891	0.804	0.905	0.905	0.021	1.013
2	0.948	242.6	7.04	0.02	-1.52	0.926	0.865	0.936	0.015	1.009	
3	0.947	242.2	7.04	0.02	-1.01	0.922	0.853	0.933	0.006	1.004	
4	0.948	242.7	7.04	0.02	-0.68	0.895	0.796	0.909	-0.012	0.993	
5	0.948	242.7	7.04	0.02	-0.52	0.866	0.744	0.883	-0.014	0.991	
6	0.948	242.7	7.04	0.02	-0.35	0.829	0.679	0.849	-0.020	0.988	
7	0.948	242.7	7.04	0.02	-0.18	0.800	0.628	0.823	-0.031	0.980	
8	0.948	242.7	7.04	0.02	-0.01	0.781	0.594	0.805	-0.043	0.973	
9	0.948	242.7	7.04	0.02	0.15	0.767	0.574	0.793	-0.041	0.974	
10	0.947	242.2	7.04	0.02	0.32	0.750	0.549	0.776	-0.036	0.977	
11	0.947	242.2	7.04	0.02	0.48	0.776	0.590	0.801	-0.033	0.979	
12	0.947	242.2	7.04	0.02	0.65	0.827	0.674	0.847	-0.023	0.986	
13	0.947	242.2	7.04	0.02	0.99	0.937	0.877	0.946	-0.002	0.999	
14	0.947	242.2	7.04	0.02	1.49	0.977	0.973	0.980	0.030	1.019	
15	0.948	242.7	7.04	0.02	1.99	0.967	0.962	0.971	0.046	1.029	

RUN	TST	P	TN	CCNF	MACH	RN/L	PT	C	P	TT	ALPHA
SEQ	MACH	G	X/DR	Y/DB	Z/DR	MF/N	MA/N	QF/Q	QA/Q	VF/V	V A/V
145	571	1	66	5	0.949	1.476	687	242.5	385	70.1	0.00
1	0.949	242.5	8.49	-0.44	-2.03	0.972	0.963	0.976	0.033	1.021	
2	0.947	241.6	8.49	-0.44	-1.52	0.978	0.969	0.981	0.021	1.013	
3	0.948	242.6	8.49	-0.44	-1.03	0.964	0.937	0.969	0.015	1.009	
4	0.947	242.1	8.49	-0.44	-0.69	0.901	0.811	0.914	0.001	1.000	
5	0.947	242.1	8.49	-0.44	-0.52	0.878	0.768	0.894	-0.006	0.996	
6	0.947	242.1	8.49	-0.44	-0.36	0.862	0.729	0.880	-0.012	0.993	
7	0.947	242.1	8.49	-0.44	-0.19	0.834	0.691	0.854	-0.012	0.992	
8	0.947	242.2	8.49	-0.44	-0.02	0.814	0.654	0.836	-0.022	0.986	
9	0.947	242.2	8.49	-0.44	0.14	0.810	0.648	0.832	-0.019	0.988	
10	0.946	241.7	8.49	-0.44	0.31	0.820	0.663	0.842	-0.023	0.986	
11	0.946	241.7	8.49	-0.44	0.48	0.826	0.688	0.856	-0.025	0.984	
12	0.946	241.7	8.49	-0.44	0.64	0.868	0.744	0.884	-0.019	0.988	
13	0.947	242.2	8.49	-0.44	0.98	0.937	0.881	0.946	0.006	1.004	
14	0.948	242.7	8.49	-0.44	1.49	0.972	0.964	0.976	0.033	1.021	
15	0.945	242.3	8.49	-0.44	1.98	0.973	0.972	0.977	0.043	1.027	

RUN	TST	P	TN	CCNF	MACH	RN/L	PT	C	P	TT	ALPHA	
SFG	MACH	Q	X/DB	Y/DA	Z/DB	MF/N	MA/M	QA/Q	VF/V	VA/V	CP	PF/P
146	571	1	66	5	0.952	1.478	688	243.5	384	70.4	0.00	
1	0.952	243.5	8.49	0.00	-2.02	0.895	0.807	0.909	0.014	1.009		
2	0.954	244.0	8.49	0.00	-1.53	0.928	0.870	0.938	0.015	1.010		
3	0.952	243.5	8.49	0.00	-1.02	0.926	0.858	0.936	0.001	1.000		
4	0.953	244.0	8.49	0.00	-0.69	0.898	0.802	0.911	-0.007	0.996		
5	0.953	244.0	8.49	0.00	-0.53	0.868	0.749	0.885	-0.011	0.993		
6	0.953	244.0	8.49	0.00	-0.36	0.852	0.720	0.871	-0.014	0.991		
7	0.951	243.5	8.49	0.00	-0.19	0.819	0.664	0.841	-0.018	0.989		
8	0.951	243.5	8.49	0.00	-0.02	0.819	0.660	0.840	-0.023	0.986		
9	0.952	244.0	8.49	0.00	0.15	0.796	0.625	0.820	-0.023	0.985		
10	0.952	244.0	8.49	0.00	0.31	0.801	0.630	0.824	-0.027	0.983		
11	0.952	244.0	8.49	c.c0	0.48	0.798	0.628	0.821	-0.020	0.987		
12	0.950	243.5	8.49	0.00	0.64	0.825	0.673	0.846	-0.017	0.990		
13	0.949	243.0	8.49	0.00	0.98	0.912	0.833	0.924	0.003	1.002		
14	0.949	243.0	8.49	0.00	1.48	0.970	0.961	0.975	0.034	1.021		
15	0.948	242.7	8.49	0.00	1.98	0.975	0.978	0.975	0.042	1.026		

RUN	TST	P	TN	CCNF	MACH	RN/L	PT	C	P	TT	ALPHA	
SFG	MACH	Q	X/DB	Y/DA	Z/DB	MF/N	MA/M	QA/Q	VF/V	VA/V	CP	PF/P
147	571	1	66	5	0.951	1.477	688	243.5	385	70.8	0.00	
1	0.951	243.5	8.49	0.44	-2.03	0.979	0.972	0.982	0.022	1.014		
2	0.951	243.5	8.49	0.44	-1.52	0.982	0.973	0.984	0.016	1.010		
3	0.953	244.0	8.49	0.44	-1.02	0.974	0.956	0.977	0.013	1.008		
4	0.952	243.5	8.49	0.44	-0.65	0.930	0.867	0.940	0.003	1.002		
5	0.952	243.5	8.49	0.44	-0.52	0.928	0.880	0.947	-0.001	1.000		
6	0.952	243.5	8.49	0.44	-0.36	0.942	0.884	0.950	-0.005	0.997		
7	0.953	244.0	8.49	0.44	-0.19	0.920	0.841	0.931	-0.009	0.994		
8	0.951	243.5	8.49	0.44	-0.02	0.898	0.797	0.912	-0.018	0.988		
9	0.951	243.5	8.49	0.44	0.14	0.887	0.776	0.901	-0.020	0.987		
10	0.952	244.0	8.49	0.44	0.31	0.872	0.750	0.889	-0.023	0.985		
11	0.952	244.0	8.49	0.44	0.48	0.874	0.754	0.891	-0.022	0.986		
12	0.951	243.5	8.49	0.44	0.65	0.906	0.809	0.918	-0.021	0.987		
13	0.951	243.5	8.49	0.44	0.98	0.961	0.921	0.967	-0.005	0.997		
14	0.951	243.5	8.49	0.44	1.48	0.981	0.980	0.984	0.028	1.018		
15	0.949	243.0	8.49	0.44	1.98	0.975	0.979	0.975	0.041	1.026		

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RUN	TST	F	TN	CCNF	MACH	RNL	PT	C	P	TT	ALPHA
					X/DR	Y/DR	Z/DR	MF/N	MA/M	QF/Q	PF/P
148	571	1	66	5	0.803	1.515	757	223.5	495	70.7	0.00
SFC	MACH	0	223.5	7.05	0.02	-2.02	0.882	0.786	0.893	0.023	1.011
1	0.	803	223.5	7.05	0.02	-1.52	0.901	0.818	0.911	0.016	1.007
2	0.	801	223.0	7.05	0.02	-1.01	0.905	0.820	0.915	0.003	1.001
3	0.	801	223.0	7.05	0.02	-0.68	0.871	0.757	0.883	-0.005	0.998
4	0.	802	223.5	7.05	0.02	-0.52	0.850	0.719	0.863	-0.009	0.996
5	0.	802	223.5	7.05	0.02	-0.34	0.815	0.661	0.831	-0.009	0.996
6	C.	802	223.5	7.05	0.02	-0.18	0.818	0.665	0.834	-0.013	0.994
7	0.	801	223.0	7.05	0.02	-0.18	0.818	0.625	0.811	-0.018	0.992
8	0.	800	222.5	7.05	0.02	-0.00	0.794	0.650	0.826	-0.020	0.991
9	0.	800	222.5	7.05	0.02	0.16	0.810	0.650	0.816	-0.011	0.995
10	0.	801	223.0	7.05	0.02	0.32	0.799	0.635	0.844	-0.015	0.993
11	0.	801	223.0	7.05	0.02	0.48	0.829	0.682	0.880	-0.003	0.999
12	0.	801	223.0	7.05	0.02	0.65	0.867	0.751	0.920	0.008	1.004
13	0.	801	223.0	7.05	0.02	0.99	0.957	0.920	0.962	0.019	1.009
14	0.	801	223.0	7.05	0.02	1.49	0.986	0.980	0.987	0.021	1.009
15	0.	801	223.0	7.05	0.02	1.99	0.986	0.982	0.988		

RUN	TST	F	TN	CCNF	MACH	RNL	PT	C	P	TT	ALPHA
					X/DR	Y/DR	Z/DR	MF/N	MA/M	QF/Q	PF/P
149	571	1	66	5	0.798	1.512	758	222.1	498	70.6	0.00
SFC	MACH	0	222.1	8.49	-0.44	-1.59	0.984	0.977	0.986	0.021	1.009
1	0.	798	222.1	8.49	-0.44	-1.09	0.968	0.944	0.971	0.018	1.008
2	0.	798	222.1	8.49	-0.44	-0.58	0.869	0.752	0.882	-0.013	0.994
3	0.	798	222.1	8.49	-0.44	-0.25	0.854	0.722	0.868	-0.025	0.989
4	0.	797	221.5	8.49	-0.44	-0.05	0.846	0.708	0.860	-0.025	0.989
5	0.	799	222.6	8.49	-0.44	-0.05	0.840	0.699	0.854	-0.020	0.991
6	0.	801	223.1	8.49	-0.44	-0.08	0.840	0.711	0.861	-0.020	0.991
7	0.	801	223.1	8.49	-0.44	-0.26	0.847	0.723	0.863	0.009	1.004
8	0.	811	226.3	8.49	-0.44	-0.42	0.848	0.784	0.900	-0.017	0.992
9	0.	801	223.0	8.49	-0.44	-0.58	0.889	0.784	0.900	-0.010	0.995
10	0.	801	223.0	8.49	-0.44	-0.75	0.931	0.862	0.938	0.007	1.003
11	0.	803	223.5	8.49	-0.44	-0.92	0.944	0.894	0.950	0.011	1.005
12	0.	802	223.0	8.49	-0.44	-1.08	0.963	0.937	0.967	0.020	1.009
13	0.	802	223.0	8.49	-0.44	-1.42	0.983	0.976	0.985	0.035	1.016
14	0.	803	223.5	8.49	-0.44	-1.92	0.977	0.969	0.979	0.023	1.010
15	0.	803	223.5	8.49	-0.44	-2.43	0.985	0.986	0.988		

RUN	TST	P	TIN	CCNF	MACH	PN/L	PT	G	P	TT	ALPHA
SFC	MACH	%		X/DB	Y/DB	Z/DR	MF/N	MA/M	QF/Q	QA/Q	VF/V
150	571	1	66	5	C.800	1.516	751	220.7	493	66.3	0.00
151	571	1	66	5	C.801	1.510	749	220.6	491	67.2	0.00
1	0.	800	220.7	8.49	0.00	-2.03	0.883	0.792	0.894	0.911	0.035 1.016
2	0.	799	220.1	8.49	0.00	-1.53	C.902	0.822	0.909	0.911	0.025 1.011
3	0.	798	219.6	8.49	0.00	-1.03	C.899	0.816	0.882	0.882	0.020 1.009
4	0.	798	219.1	8.49	0.00	-0.70	C.870	0.760	0.850	0.850	0.009 1.004
5	0.	797	219.1	8.49	0.00	-0.53	C.858	0.736	0.871	0.871	-0.000 1.000
6	0.	798	219.6	8.49	0.00	-0.36	C.841	0.706	0.856	0.856	-0.007 0.997
7	0.	798	219.6	8.49	0.00	-0.19	C.849	0.718	0.863	0.863	-0.010 0.996
8	0.	799	220.1	8.49	0.00	-0.01	C.835	0.697	0.850	0.850	-0.003 0.998
9	0.	799	220.1	8.49	0.00	0.15	C.837	0.697	0.852	0.852	-0.011 0.995
10	0.	799	220.1	8.49	0.00	0.31	C.825	0.679	0.840	0.840	-0.005 0.998
11	0.	799	220.1	8.49	0.00	0.48	C.846	0.719	0.860	0.860	0.010 1.004
12	0.	799	220.1	8.49	0.00	0.64	C.875	0.767	0.887	0.887	0.004 1.002
13	0.	799	220.1	8.49	0.00	0.98	C.942	0.892	0.948	0.948	0.014 1.006
14	0.	800	220.7	8.49	0.00	0.98	C.942	0.968	0.980	0.980	0.028 1.013
15	C.	8C1	221.2	8.49	0.00	1.48	C.982	0.978	0.984	0.984	0.029 1.013
16	0.	799	220.2	8.49	0.00	1.98	C.982	0.976	0.976	0.976	

RUN	TST	F	TIN	CCNF	MACH	PN/L	PT	G	P	TT	ALPHA
SFC	MACH	%		X/DB	Y/DR	Z/DR	MF/N	MA/M	QF/Q	QA/Q	VF/V
151	571	1	66	5	C.801	1.510	749	220.6	491	67.2	0.00
1	0.	801	220.6	8.49	0.44	-2.03	0.974	0.967	0.977	0.977	0.042 1.019
2	C.	8CC	220.6	8.49	0.44	-1.52	C.980	0.974	0.982	0.982	0.032 1.014
3	0.	799	220.1	8.49	0.44	-1.03	C.975	0.961	0.978	0.978	0.024 1.011
4	0.	799	220.1	8.49	0.44	-0.68	C.921	0.853	0.929	0.929	0.013 1.006
5	0.	798	219.6	8.49	0.44	-0.52	C.929	0.869	0.937	0.937	0.013 1.006
6	0.	798	219.6	8.49	0.44	-0.36	C.931	0.870	0.938	0.938	0.009 1.004
7	C.	797	219.1	8.49	0.44	-0.19	C.910	0.832	0.919	0.919	0.007 1.003
8	0.	797	219.1	8.49	0.44	-0.02	C.897	0.805	0.907	0.907	-0.002 0.999
9	0.	797	219.1	8.49	0.44	0.15	C.897	0.802	0.907	0.907	-0.006 0.997
10	0.	799	219.6	8.49	0.44	0.30	C.896	0.803	0.906	0.906	0.000 1.000
11	0.	800	220.1	8.49	0.44	0.48	C.900	0.810	0.910	0.910	-0.000 1.000
12	C.	8CC	220.1	8.49	0.44	0.66	C.925	0.855	0.932	0.932	0.001 1.000
13	0.	800	220.6	8.49	0.44	0.98	C.960	0.930	0.965	0.965	0.019 1.009
14	C.	800	220.6	8.49	0.44	1.48	C.981	0.972	0.983	0.983	0.022 1.010
15	0.	800	220.1	8.49	0.44	1.98	C.980	0.972	0.982	0.982	0.029 1.013

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RUN	TST	P	TN	CCNF	MACH	PN/L	PT	Q	P	TT	ALPHA
SEQ	571	1	66	5	0.599	1.513	895	176.6	702	67.0	0.00
1	0.599	176.6	7.05	X/DB	Y/CR	Z/DR	MF/N	WA/W	QF/F	0.824	0.911
2	0.599	176.6	7.05	X/DB	Y/DB	Z/DB	MF/N	WA/W	QF/F	0.834	0.916
3	0.597	175.4	7.05	X/DB	Y/DB	Z/DB	MF/N	WA/W	QF/F	0.840	0.921
4	0.597	175.4	7.05	X/DB	Y/DB	Z/DB	MF/N	WA/W	QF/F	0.786	0.893
5	0.597	175.4	7.05	X/DB	Y/DB	Z/DB	MF/N	WA/W	QF/F	0.738	0.867
6	0.597	175.4	7.05	X/DB	Y/DB	Z/DB	MF/N	WA/W	QF/F	0.834	0.843
7	0.597	175.4	7.05	X/DB	Y/DB	Z/DB	MF/N	WA/W	QF/F	0.693	0.843
8	0.598	176.0	7.05	X/DB	Y/DB	Z/DB	MF/N	WA/W	QF/F	0.667	0.827
9	0.597	175.4	7.05	X/DB	Y/DB	Z/DB	MF/N	WA/W	QF/F	0.655	0.820
10	0.597	175.4	7.05	X/DB	Y/DB	Z/DB	MF/N	WA/W	QF/F	0.711	0.852
11	0.597	175.4	7.05	X/DB	Y/DB	Z/DB	MF/N	WA/W	QF/F	0.710	0.852
12	0.598	176.0	7.05	X/DB	Y/DB	Z/DB	MF/N	WA/W	QF/F	0.726	0.862
13	0.599	176.6	7.05	X/DB	Y/DB	Z/DB	MF/N	WA/W	QF/F	0.793	0.897
14	0.600	177.2	7.05	X/DB	Y/DB	Z/DB	MF/N	WA/W	QF/F	0.939	0.971
15	0.601	177.2	7.05	X/DB	Y/DB	Z/DB	MF/N	WA/W	QF/F	0.990	0.995
				X/DB	Y/DB	Z/DB	MF/N	WA/W	QF/F	C.981	0.989

RUN	TST	P	TN	CCNF	MACH	PN/L	PT	C	P	TT	ALPHA
SEQ	571	1	66	5	0.602	1.518	896	177.8	701	67.2	0.60
1	0.602	177.8	8.49	-C.44	-2.0	C.3	C.978	C.964	0.979	0.035	1.009
2	0.599	176.0	8.49	-0.44	-1.0	52	C.984	C.972	0.985	0.019	1.005
3	0.599	176.0	8.49	-0.44	-1.0	03	C.957	C.918	0.960	0.007	1.002
4	0.598	176.0	8.49	-0.44	-0.69	0.898	C.807	0.944	0.94	0.003	1.001
5	0.601	177.2	8.49	-0.44	-0.52	0.873	C.763	0.880	0.880	0.003	1.001
6	0.601	177.2	8.49	-0.44	-0.35	0.882	C.779	0.890	0.890	-0.006	0.998
7	0.599	176.6	8.49	-0.44	-0.19	0.860	C.739	0.867	0.867	-0.002	0.999
8	0.599	176.0	8.49	-0.44	-0.02	C.857	C.735	0.865	0.865	0.006	1.001
9	0.599	176.0	8.49	-0.44	0.14	0.863	C.744	0.871	0.871	-0.005	0.999
10	0.599	176.6	8.49	-0.44	0.31	C.872	C.758	0.879	0.879	-0.006	0.998
11	0.599	176.6	8.49	-0.44	0.48	C.889	C.789	0.895	0.895	-0.006	0.998
12	0.599	176.0	8.49	-0.44	0.65	0.919	C.846	0.924	0.924	0.007	1.002
13	0.599	176.0	8.49	-0.44	0.58	C.944	C.895	0.947	0.947	0.022	1.005
14	0.600	177.2	8.49	-0.44	1.48	0.981	C.967	0.982	0.982	0.019	1.005
15	0.600	177.2	8.49	-0.44	1.98	C.982	C.971	0.983	0.983	0.027	1.007

RUN	TST	P	TN	CCNF	MACH	RN/L	PT	C	P	TT	ALPHA	
SFQ	MACH	Q		X/DR	Y/DR	Z/DR	MF/N	WA/N	QF/Q	VA/V	CP	PF/P
154	571	1	66	5	0.597	1.507	895	175.4	7C3	67.3	0.00	0.022 1.005
					8.49	0.00	-2.02	C.9C6	0.825	0.911		
1	0.597	175.4			8.49	0.00	-1.53	0.921	0.852	0.926		0.015 1.004
2	0.598	176.0			8.49	0.00	-1.02	C.926	0.858	0.930		0.003 1.001
3	0.598	176.0			8.49	0.00	-0.69	C.892	0.798	0.899		0.001 1.000
4	0.599	176.6			8.49	0.00	-0.53	C.871	0.758	0.878		-0.002 0.999
5	0.598	176.0			8.49	0.00	-0.36	C.842	0.708	0.850		-0.001 1.000
6	0.599	176.6			8.49	0.00	-0.19	0.861	0.741	0.869		-0.003 0.999
7	0.599	176.6			8.49	0.00	-0.02	0.838	0.701	0.847		-0.008 0.998
8	0.599	176.6			8.49	0.00	0.14	0.867	0.751	0.874		-0.005 0.999
9	0.599	176.6			8.49	0.00	0.31	0.864	0.744	0.872		-0.014 0.996
10	0.599	176.6			8.49	0.00	0.48	0.878	0.770	0.885		-0.010 0.998
11	0.599	176.6			8.49	0.00	0.64	0.882	0.778	0.889		-0.001 1.000
12	0.600	177.2			8.49	0.00	0.98	C.925	0.877	0.939		0.011 1.003
12	0.600	177.2			8.49	0.00	1.47	C.988	0.979	0.939		0.011 1.003
14	0.600	177.2			8.49	0.00	1.98	C.989	0.983	0.990		0.015 1.004
15	0.600	177.2			8.49	0.00	1.98	C.989	0.983	0.990		

RUN	TST	P	TN	CCNF	MACH	RN/L	PT	C	P	TT	ALPHA	
SFQ	MACH	Q		X/DR	Y/DR	Z/DR	MF/N	WA/N	QF/Q	VA/V	CP	PF/P
155	571	1	66	5	0.600	1.515	896	177.2	702	67.3	0.00	0.023 1.006
					8.49	0.44	-2.02	C.983	0.972	0.984		0.015 1.004
1	0.600	177.2			8.49	0.44	-1.52	0.988	0.981	0.989		0.022 1.005
2	0.600	177.2			8.49	0.44	-1.03	C.976	0.957	0.977		0.011 1.003
3	0.600	177.2			8.49	0.44	-0.69	C.931	0.869	0.935		0.007 1.002
4	0.600	177.2			8.49	0.44	-0.52	0.925	0.856	0.929		0.004 1.001
5	0.600	177.2			8.49	0.44	-0.36	C.920	0.848	0.925		0.007 1.002
6	0.600	177.2			8.49	0.44	-0.19	0.913	0.836	0.918		0.005 1.001
7	0.600	177.2			8.49	0.44	-0.02	C.899	0.809	0.905		0.003 1.001
8	0.600	177.2			8.49	0.44	0.44	C.9C3	0.816	0.916		0.007 1.002
9	0.600	177.2			8.49	0.44	0.14	C.9C3	0.816	0.916		0.010 1.002
10	0.600	177.2			8.49	0.44	0.31	0.882	0.780	0.889		0.023 1.006
11	0.600	177.2			8.49	0.44	0.48	C.9C3	0.816	0.908		0.023 1.006
12	0.600	177.2			8.49	0.44	0.64	0.919	0.846	0.924		0.023 1.006
13	0.600	177.2			8.49	0.44	0.98	C.957	0.959	0.959		0.007 1.002
14	0.600	177.2			8.49	0.44	1.48	C.981	0.968	0.982		0.023 1.006
15	0.600	177.2			8.49	0.44	1.98	C.986	0.978	0.987		0.023 1.006

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RUN	TST	P	TN	CCNF	MACH	RN/L	PT	C	P	TT	ALPHA
SFC	MACH	C	X/DB	Y/DB	Z/DB	MF/N	MA/M	QF/Q	QA/Q	VF/V	VA/V
156	571	1	66	5	0.954	1.482	679	241.2	378	64.8	0.00
2	0.954	241.2	8.48	-0.45	-2.03	C.966	0.957	0.971	0.041	1.026	PF/P
3	0.951	240.1	8.48	-0.45	-1.53	C.970	0.963	0.975	0.038	1.024	
4	0.952	240.7	8.48	-0.45	-1.02	0.967	0.948	0.972	0.024	1.015	
5	0.952	240.7	8.48	-0.45	-0.69	C.924	0.857	0.935	0.006	1.004	
6	C.951	240.1	8.48	-0.45	-0.52	0.897	0.807	0.911	0.003	1.002	
7	0.951	240.1	8.48	-0.45	-0.36	0.884	0.781	0.899	0.000	1.000	
8	0.950	239.6	8.48	-0.45	-0.19	0.872	0.753	0.888	-0.014	0.991	
9	0.951	240.1	8.48	-0.45	-0.03	C.850	0.714	0.869	-0.019	0.988	
10	0.954	241.7	8.48	-0.45	0.14	0.822	0.669	0.843	-0.015	0.990	
11	C.953	241.8	8.48	-0.45	0.31	0.825	0.673	0.846	-0.017	0.989	
12	0.953	241.8	8.48	-0.45	0.48	0.832	C.690	0.852	-0.005	0.997	
13	0.951	241.2	8.48	-0.45	0.64	0.863	0.744	0.881	-0.004	0.997	
14	0.949	240.8	8.48	-0.45	0.99	0.929	0.865	0.939	0.002	1.001	
15	0.950	241.3	8.48	-0.45	1.48	C.981	C.979	0.984	0.028	1.018	
16	C.949	240.8	8.48	-0.45	1.98	0.972	0.971	0.976	0.045	1.C28	

RUN	TST	P	TN	CCNF	MACH	RN/L	PT	C	P	TT	ALPHA
SFC	MACH	C	X/DB	Y/DB	Z/DB	MF/N	MA/M	QF/Q	QA/Q	VF/V	VA/V
157	571	1	66	5	0.954	1.478	681	241.7	380	66.9	0.00
1	0.954	241.7	8.48	-0.01	-2.02	C.895	0.812	0.909	0.021	1.013	PF/P
2	0.955	242.3	8.48	-0.01	-1.53	0.922	C.865	0.933	0.027	1.017	
3	0.952	241.2	8.48	-0.01	-1.02	C.920	0.856	0.931	0.016	1.010	
4	0.952	241.2	8.48	-0.01	-0.69	C.895	0.804	0.909	0.008	1.005	
5	0.950	240.7	8.48	-0.01	-0.53	0.881	0.774	0.896	-0.003	0.998	
6	0.951	241.2	8.48	-0.01	-0.36	C.859	0.732	0.877	-0.011	0.993	
7	0.951	241.2	8.48	-0.01	-0.19	C.817	0.662	0.838	-0.013	0.992	
8	0.951	241.2	8.48	-0.01	-0.02	C.809	0.646	0.831	-0.019	0.988	
9	0.951	241.2	8.48	-0.01	0.14	C.794	0.623	0.818	-0.020	0.987	
10	0.951	241.2	8.48	-0.01	0.31	0.797	0.624	0.820	-0.027	0.983	
11	0.951	241.2	8.48	-0.01	0.48	C.797	0.626	0.820	-0.022	0.986	
12	0.951	241.2	8.48	-0.01	0.64	C.811	0.652	0.833	-0.016	0.990	
13	0.951	241.2	8.48	-0.01	0.98	0.906	0.821	0.919	-0.001	0.999	
14	0.951	241.2	8.48	-0.01	1.48	0.972	C.968	0.977	0.034	1.021	
15	0.949	240.8	8.48	-0.01	1.99	C.969	0.969	0.974	0.049	1.031	

RUN	TSI	P	TN	CCNF	MACH	RN/L	PT	C	P	TT	0.00	0.00	CP	PF/P
											QA/Q	VF/V	VAV/V	
158	571	1	66	5	0.954	1.481	684	242.5	381	67.8	0.979	0.029	1.019	
	SEC	MACH	G	X/DB	Y/DB	Z/DB	MF/N	MA/M	QF/Q	0.969	0.979	0.028	1.018	
1	0.954	242.9	8.48	0.43	-2.03	C.975	0.967	0.967	0.978	0.021	1.013			
2	0.954	242.9	8.48	0.43	-1.53	C.974	0.945	0.945	0.971	0.007	1.005			
3	0.953	242.3	E.48	0.43	-1.03	C.966	0.858	0.858	0.935	0.002	1.001			
4	0.953	242.3	E.48	0.43	-0.70	C.924	0.865	0.865	0.939	0.001	1.000			
5	0.954	242.9	8.48	0.43	-0.52	0.929	0.842	0.842	0.929	-0.007	0.996			
6	0.952	242.3	E.48	0.43	-0.36	C.917	0.802	0.802	0.911	-0.010	0.993			
7	0.952	242.3	E.48	0.43	-0.19	0.898	0.754	0.754	0.888	-0.017	0.989			
8	0.953	242.9	8.48	0.43	-0.02	0.871	0.729	0.729	0.877	-0.016	0.990			
9	0.950	241.8	8.48	0.43	0.14	0.859	0.724	0.724	0.874	-0.020	0.987			
10	0.950	241.8	3.48	0.43	0.30	0.855	0.724	0.724	0.874	-0.012	0.993			
11	0.950	241.8	8.48	0.43	0.48	0.856	0.762	0.762	0.892	-0.007	0.995			
12	0.951	242.4	8.48	0.43	0.64	0.876	0.762	0.762	0.893	0.950	0.027	1.017		
13	0.950	241.9	8.48	0.43	0.98	0.942	0.833	0.833	0.977	0.963	0.024	1.027		
14	0.949	241.4	8.48	0.43	1.48	C.973	1.48	1.48	0.974	0.978	0.974			
15	0.947	241.0	8.48	0.43	1.98	C.974	1.98	1.98	0.974					

RUN	TSI	P	TN	CCNF	MACH	RN/L	PT	C	P	TT	0.00	0.00	CP	PF/P
											QA/Q	VF/V	VAV/V	
159	571	1	66	5	0.954	1.478	684	242.9	381	68.8	0.976	0.030	1.019	
	SEC	MACH	G	X/DB	Y/DB	Z/DB	WF/W	MA/M	QF/Q	0.962	0.976	0.035	1.022	
1	0.954	242.9	1C.87	0.41	-2.05	0.972	0.963	0.963	0.975	0.040	1.025			
2	0.952	241.2	10.87	C.41	-1.53	0.971	0.925	0.925	0.957	0.028	1.018			
3	0.951	242.4	1C.87	0.41	-1.04	C.950	0.856	0.856	0.929	0.020	1.013			
4	0.949	241.4	1C.87	C.41	-0.71	C.917	0.853	0.853	0.919	0.012	1.008			
5	0.947	241.0	1C.87	C.41	-0.54	C.918	0.828	0.828	0.906	0.011	1.007			
6	0.948	241.5	1C.87	C.41	-0.37	0.906	0.801	0.801	0.906	0.001	1.001			
7	0.948	241.5	1C.87	C.41	-0.19	C.892	0.802	0.802	0.895	-0.010	0.994			
8	0.946	241.1	1C.87	C.41	-0.04	C.895	0.768	0.768	0.803	-0.019	0.988			
9	0.948	241.5	1C.87	C.41	0.13	C.879	0.780	0.780	0.888	-0.014	0.991			
10	0.948	241.5	1C.87	C.41	0.29	C.888	0.754	0.754	0.888	-0.014	0.991			
11	0.949	241.4	1C.87	C.41	0.46	C.872	0.770	0.770	0.933	0.003	1.002			
12	0.949	241.4	1C.87	C.41	0.63	C.881	0.852	0.852	0.922	0.029	1.018			
13	0.949	241.4	1C.87	C.41	0.97	C.922	0.967	0.967	0.978	0.045	1.028			
14	0.949	241.4	1C.87	C.41	1.47	C.975	0.974	0.974	0.977					
15	0.949	241.4	1C.87	C.41	1.97	C.973								

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RUN	TSI	P	T <sub>N</sub>	CCNF	MACH	RN/L	PT	C	P	TT	ALPHA
160	571	1	66	5	0.950	1.473	685	241.9	383	69.6	0.00
SFC	MACH	G	X/DR	Y/DR	Z/DR	NF/N	MA/M	QF/Q	QA/Q	VF/V	VA/V
1	0.950	241.9	IC.87	-0.03	-2.04	0.899	0.821	0.912	0.939	0.869	0.921
2	0.951	242.4	IC.87	-0.03	-1.55	0.929	0.875	0.875	0.875	0.875	0.875
3	0.951	242.4	IC.87	-0.03	-1.04	0.929	0.875	0.939	0.939	0.939	0.939
4	0.953	242.9	IC.87	-0.03	-0.71	0.900	0.812	0.913	0.913	0.913	0.913
5	0.953	242.9	IC.87	-0.03	-0.54	0.880	0.776	0.895	0.895	0.895	0.895
6	0.953	242.9	IC.87	-0.03	-0.37	0.868	0.753	0.885	0.885	0.885	0.885
7	0.955	244.5	IC.87	-0.03	-0.37	0.864	0.750	0.881	0.881	0.881	0.881
8	0.953	244.0	IC.87	-0.03	-0.20	0.846	0.716	0.865	0.865	0.865	0.865
9	0.951	243.5	IC.87	-0.03	-0.03	0.826	0.685	0.847	0.847	0.847	0.847
10	0.951	243.5	IC.87	-0.03	0.12	0.824	0.681	0.845	0.845	0.845	0.845
11	0.948	242.6	IC.87	-0.03	0.29	0.832	0.689	0.852	0.852	0.852	0.852
12	0.948	242.6	IC.87	-0.03	0.46	0.822	0.676	0.843	0.843	0.843	0.843
13	0.948	242.6	IC.87	-0.03	0.63	0.834	0.699	0.854	0.854	0.854	0.854
14	0.947	242.2	IC.87	-0.02	0.97	0.888	0.795	0.903	0.903	0.903	0.903
15	0.948	242.7	IC.87	-0.03	1.46	0.959	0.941	0.965	0.965	0.965	0.965
16	0.948	242.7	IC.87	-0.03	1.97	0.972	0.974	0.976	0.976	0.976	0.976

RUN	TSI	P	T <sub>N</sub>	CCNF	MACH	RN/L	PT	C	P	TT	ALPHA
161	571	1	66	5	0.954	1.479	688	244.0	383	70.5	0.00
SEC	MACH	G	X/DR	Y/DR	Z/DR	NF/N	MA/M	QF/Q	QA/Q	VF/V	VA/V
1	0.954	244.0	IC.87	-0.38	-2.03	0.962	0.944	0.968	0.968	0.968	0.968
2	0.953	243.5	IC.87	-0.38	-1.54	0.968	0.957	0.973	0.973	0.973	0.973
3	0.953	243.5	IC.87	-0.38	-1.04	0.955	0.932	0.962	0.962	0.962	0.962
4	0.949	242.5	IC.87	-0.38	-0.71	0.916	0.849	0.927	0.927	0.927	0.927
5	0.951	243.5	IC.87	-0.38	-0.54	0.888	0.796	0.902	0.902	0.902	0.902
6	0.949	243.0	IC.87	-0.38	-0.37	0.875	0.772	0.892	0.892	0.892	0.892
7	0.948	242.7	IC.87	-0.38	-0.20	0.872	0.762	0.889	0.889	0.889	0.889
8	0.947	242.2	IC.87	-0.38	-0.04	0.857	0.737	0.875	0.875	0.875	0.875
9	0.945	241.8	IC.87	-0.38	0.14	0.848	0.719	0.867	0.867	0.867	0.867
10	0.945	241.8	IC.87	-0.38	0.30	0.844	0.712	0.863	0.863	0.863	0.863
11	0.944	241.3	IC.87	-0.38	0.47	0.847	0.720	0.866	0.866	0.866	0.866
12	0.945	241.8	IC.87	-0.38	0.63	0.858	0.739	0.876	0.876	0.876	0.876
13	0.946	242.3	IC.87	-0.38	0.96	0.908	0.830	0.921	0.921	0.921	0.921
14	0.946	242.3	IC.87	-0.38	1.47	0.963	0.945	0.968	0.968	0.968	0.968
15	0.946	242.3	IC.87	-0.38	1.97	0.973	0.974	0.977	0.977	0.977	0.977

RUN	TST	P	TN	CENF	MACH	RN/L	PT	C	P	TT	ALPHA
SEQ	MACH	G	X/CR	Y/DB	Z/DB	MF/N	MA/M	QF/Q	QA/Q	VF/V	VA/V
162	571	1	66	5	0.952	1.477	688	243.5	384	70.6	0.00
1	0.952	243.5	1C.87	-C.48	-2.04	0.971	0.963	0.975	0.975	0.035	1.022
2	0.952	243.5	1C.87	-0.48	-1.53	C.974	0.968	0.978	0.978	0.031	1.019
3	0.954	244.C	1C.87	-0.48	-1.04	C.964	0.941	0.969	0.969	0.021	1.013
4	0.954	244.C	1C.87	-C.48	-0.70	C.918	0.849	0.929	0.929	0.013	1.008
5	0.954	244.C	1C.87	-0.48	-0.54	C.906	0.825	0.919	0.919	0.008	1.005
6	0.954	244.C	1C.87	-C.48	-0.37	C.890	0.795	0.905	0.905	0.006	1.004
7	0.954	244.0	1C.87	-0.48	-0.20	C.875	0.766	0.891	0.891	0.001	1.001
8	0.954	244.C	1C.87	-C.48	-0.04	C.874	0.764	0.890	0.890	0.001	1.001
9	0.954	244.C	1C.87	-C.48	0.12	C.854	0.729	0.873	0.873	-0.001	0.999
10	0.954	244.C	1C.87	-C.48	0.30	C.847	0.715	0.866	0.866	-0.005	0.997
11	0.954	244.C	1C.87	-C.48	0.46	C.851	0.725	0.870	0.870	-0.001	0.999
12	0.952	243.5	1C.87	-C.48	0.62	C.870	0.757	0.887	0.887	0.001	1.000
13	0.953	244.C	1C.88	-C.48	0.97	C.915	0.842	0.926	0.926	0.011	1.007
14	0.953	244.0	1C.87	-C.48	1.47	C.961	0.947	0.967	0.967	0.040	1.025
15	0.950	243.C	1C.87	-0.48	1.96	C.968	0.968	0.973	0.973	0.053	1.033

RUN	TST	P	TN	CENF	MACH	RN/L	PT	C	P	TT	ALPHA
SEQ	MACH	G	X/CR	Y/DB	Z/DB	MF/N	MA/M	QF/Q	QA/Q	VF/V	VA/V
163	571	1	66	5	0.952	1.479	689	244.C	385	70.9	0.00
1	0.952	244.C	9.99	C.CC	-C.37	C.865	0.746	0.832	0.832	-0.004	0.998
2	0.949	243.C	9.99	0.00	-0.20	0.847	C.714	0.866	0.866	-0.010	0.994
3	0.949	243.C	1C.C0	C.00	-0.03	C.840	0.701	0.860	0.860	-0.011	0.993
4	0.949	243.C	9.99	C.CC	0.14	C.832	0.686	0.852	0.852	-0.014	0.991
5	0.949	243.0	1C.00	C.00	0.30	C.825	0.673	0.846	0.846	-0.019	0.988
6	0.949	243.C	1C.00	C.CC	0.46	C.832	0.688	0.853	0.853	-0.011	0.993
7	0.949	243.0	1C.00	C.00	0.64	C.840	0.702	0.859	0.859	-0.008	0.995
8	0.948	242.6	1C.00	C.00	0.97	C.890	0.796	0.905	0.905	0.006	1.004
9	0.948	242.6	1C.00	C.CC	1.46	C.967	0.954	0.972	0.972	0.031	1.019
10	0.948	242.6	1C.00	C.00	1.97	C.975	0.976	0.978	0.978	0.044	1.028

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RUN	TST	P	TN	CCNF	MACH	RNL	PT	C	P	TT	ALPHA
	164	5	571.1	66	5	0.802	1.513	757	223.0	495	70.6
SFC	MACH	G	X/D9	Y/D9	Z/D9	MF/N	MA/N	QF/Q	QA/Q	VF/V	VA/V
1	0.802	223.0	1C.88	0.41	-2.05	0.973	0.967	0.976	0.976	0.045	1.020
2	0.799	222.5	1C.88	0.41	-1.54	0.980	0.974	0.982	0.982	0.034	1.015
3	0.800	222.5	1C.88	0.41	-1.03	0.965	0.941	0.969	0.969	0.022	1.010
4	0.800	222.5	1C.88	0.41	-0.70	0.932	0.872	0.939	0.939	0.011	1.005
5	0.800	222.5	1C.88	0.41	-0.53	0.917	0.846	0.925	0.925	0.015	1.007
6	0.800	222.5	1C.88	0.41	-0.37	0.909	0.830	0.918	0.918	0.009	1.004
7	0.800	222.5	1C.88	0.41	-0.21	0.895	0.806	0.905	0.905	0.015	1.007
8	0.798	222.0	1C.88	0.41	-0.05	0.902	0.813	0.911	0.911	-0.000	1.000
9	0.800	222.5	1C.88	0.41	0.13	0.900	0.809	0.910	0.910	-0.000	1.000
10	0.801	223.1	1C.88	0.41	0.29	0.893	0.793	0.903	0.903	-0.011	0.995
11	0.802	223.5	1C.88	0.41	0.47	0.897	0.803	0.907	0.907	-0.003	0.999
12	0.803	223.5	1C.88	0.41	0.63	0.913	0.830	0.921	0.921	-0.006	0.997
13	0.803	223.5	1C.88	0.41	0.96	0.943	0.894	0.949	0.949	0.013	1.006
14	0.803	223.5	1C.88	0.41	1.47	0.982	0.972	0.984	0.984	0.020	1.009
15	0.801	223.0	1C.88	0.41	1.97	0.987	0.985	0.989	0.989	0.023	1.011

RUN	TST	P	TN	CCNF	MACH	RNL	PT	C	P	TT	ALPHA
	165	5	571.1	66	5	C.801	1.516	758	223.1	497	70.4
SFC	MACH	G	X/D9	Y/D9	Z/D9	MF/N	MA/N	QF/Q	QA/Q	VF/V	VA/V
1	0.801	223.1	1C.88	-0.03	-2.04	0.897	0.816	0.907	0.907	0.033	1.015
2	0.797	221.5	1C.88	-0.03	-1.55	0.915	0.846	0.924	0.924	0.022	1.010
3	0.798	222.1	1C.88	-0.03	-1.04	0.920	0.850	0.928	0.928	0.009	1.004
4	0.799	222.6	1C.88	-0.03	-0.71	0.897	0.804	0.907	0.907	-0.001	0.999
5	0.800	222.5	1C.88	-0.03	-0.54	0.879	0.773	0.890	0.890	0.002	1.001
6	0.800	222.5	1C.88	-0.02	-0.38	0.869	0.753	0.881	0.881	-0.006	0.997
7	0.802	223.5	1C.88	-0.03	-0.20	0.865	0.747	0.878	0.878	-0.006	0.997
8	0.802	223.5	1C.88	-0.03	-0.04	0.862	0.744	0.875	0.875	0.003	1.001
9	0.802	223.5	1C.88	-0.03	0.13	0.865	0.751	0.878	0.878	0.010	1.004
10	0.802	223.5	1C.88	-0.03	0.30	0.858	0.736	0.871	0.871	0.000	1.000
11	0.801	223.1	1C.88	-0.03	0.46	0.862	0.746	0.875	0.875	0.006	1.003
12	0.801	223.1	1C.88	-0.03	0.62	0.880	0.777	0.892	0.892	0.004	1.002
13	0.801	223.1	1C.88	-0.03	0.96	0.930	0.870	0.937	0.937	0.013	1.006
14	0.801	223.1	1C.88	-0.03	1.46	0.974	0.959	0.977	0.977	0.022	1.010
15	0.801	223.1	1C.88	-0.03	1.97	0.982	0.977	0.985	0.985	0.027	1.012

RUN	TST	P	TN	CCNF	MACH	PN/L	PT	C	P	TT	ALPHA	PF/P
SEQ	MACH	Q		X/DB	Y/DB	Z/DB	WF/N	WA/N	QA/Q	VF/V	VA/V	CP
166	571	1	66	5	C.800	1.514	757	222.5	497	70.3	0.00	0.029 1.013
1	0.800	222.5		1C.88	-0.38	-2.04	C.982	0.976	0.984	0.976	0.984	0.021 1.009
2	0.800	222.5		1C.88	-C.38	-1.54	C.982	0.972	0.984	0.972	0.984	0.015 1.007
3	0.800	222.5		1C.88	-C.38	-1.C4	C.956	0.921	0.961	0.921	0.961	0.011 1.005
4	0.800	222.5		1C.88	-0.38	-0.71	0.909	0.830	0.918	0.830	0.918	0.008 1.004
5	0.800	222.5		1C.88	-C.38	-0.54	C.880	0.777	0.891	0.777	0.891	0.013 1.006
6	0.800	222.5		1C.88	-0.38	-0.35	C.866	0.755	0.879	0.755	0.879	0.011 1.005
7	0.800	222.5		1C.88	-0.38	-0.21	0.865	0.753	0.878	0.753	0.878	0.003 0.999
8	0.799	222.6		1C.88	-C.38	-0.04	C.867	0.751	0.880	0.751	0.880	0.003 0.999
9	0.801	223.1		1C.88	-0.38	0.13	C.854	0.729	0.868	0.729	0.868	0.003 0.999
10	0.800	222.5		1C.88	-C.38	0.29	0.874	0.763	0.886	0.763	0.886	0.001 1.000
11	0.801	223.0		1C.88	-0.28	0.47	C.877	0.771	0.889	0.771	0.889	0.004 1.002
12	0.801	223.0		1C.88	-C.38	0.63	0.889	0.792	0.899	0.792	0.899	0.006 1.003
13	0.801	223.0		1C.88	-C.38	0.97	C.933	0.876	0.940	0.876	0.940	0.013 1.006
14	0.800	222.5		1C.88	-C.38	1.47	0.975	0.962	0.978	0.962	0.978	0.027 1.C12
15	0.801	223.1		1C.88	-C.38	1.97	C.981	0.976	0.983	0.976	0.983	0.030 1.014

RUN	TST	P	TN	CCNF	MACH	PN/L	PT	C	P	TT	ALPHA	PF/P
SEQ	MACH	Q		X/DB	Y/DB	Z/DB	WF/N	WA/N	QA/Q	VF/V	VA/V	CP
167	571	1	66	5	0.800	1.514	757	222.5	497	70.4	0.00	0.031 1.014
1	0.800	222.5		1C.88	-C.48	-2.04	C.980	0.974	0.983	0.974	0.983	0.020 1.009
2	0.800	222.5		1C.88	-0.48	-1.54	C.987	0.982	0.988	0.982	0.988	0.013 1.006
3	0.800	222.5		1C.88	-C.48	-1.04	C.966	0.938	0.969	0.938	0.969	0.009 1.004
4	0.801	223.0		1C.88	-0.48	-0.71	0.912	0.836	0.921	0.836	0.921	0.005 1.002
5	0.801	223.0		1C.88	-C.48	-0.52	C.892	0.797	0.902	0.797	0.902	0.004 1.002
6	0.801	223.0		1C.88	-0.48	-0.37	C.986	0.787	0.897	0.787	0.897	0.001 1.000
7	0.800	222.5		1C.88	-C.48	-0.21	0.885	0.782	0.896	0.782	0.896	-0.001 1.000
8	0.802	223.0		1C.88	-C.48	-0.04	C.886	0.786	0.897	0.786	0.897	0.002 1.001
9	0.802	223.0		1C.88	-C.48	0.12	C.872	0.764	0.884	0.764	0.884	0.010 1.004
10	0.803	223.5		1C.88	-C.48	0.29	C.880	0.775	0.892	0.775	0.892	0.001 1.001
11	0.803	223.5		1C.88	-0.48	0.47	C.891	0.797	0.902	0.797	0.902	0.008 1.004
12	0.802	223.5		1C.88	-C.48	0.63	C.902	0.818	0.912	0.818	0.912	0.010 1.C04
13	0.802	223.5		1C.88	-C.48	0.96	C.938	0.884	0.944	0.884	0.944	0.010 1.005
14	0.802	223.5		1C.88	-C.48	1.46	0.978	0.965	0.980	0.965	0.980	0.022 1.010
15	0.802	223.5		1C.88	-C.48	1.96	C.980	0.974	0.982	0.974	0.982	0.033 1.015

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RUN	TST	P	TN	CCNF	MACH	RN/L	PT	C	P	TT	ALPHA
SEQ	MACH	Q	X/DB	Y/DB	Z/DB	MF/N	MA/N	QF/Q	QA/Q	VF/V	VA/V
168	571.1	66.5	0.800	1.514	757	222.5	497	70.3	0.00	0.870	PF/P
1	0.800	222.5	1C.00	0.00	-0.37	0.857	0.736	0.864	0.852	0.723	0.006
2	0.800	222.5	1C.00	0.00	-0.20	0.850	0.701	0.852	-0.000	0.984	0.002
3	0.800	222.5	1C.00	0.00	-0.03	0.837	0.748	0.878	-0.006	0.982	1.001
4	0.800	222.5	1C.00	0.00	0.15	0.866	0.730	0.870	-0.009	0.985	1.000
5	0.800	222.5	1C.00	0.00	0.30	0.856	0.734	0.870	0.003	0.983	0.996
6	0.801	223.0	1C.00	0.00	0.47	0.857	0.773	0.890	0.006	0.980	1.003
7	0.801	223.0	1C.00	0.00	0.63	0.878	0.859	0.932	0.014	0.973	1.006
8	0.801	223.0	1C.00	0.00	0.97	0.924	0.974	0.986	0.013	0.986	1.006
9	0.801	223.0	1C.00	0.00	1.47	0.984	0.982	0.989	0.016	0.982	1.007
10	0.801	223.0	1C.00	0.00	1.97	0.988	0.982	0.989	0.016	0.982	1.007

RUN	TST	P	TN	CCNF	MACH	RN/L	PT	C	P	TT	ALPHA
SEQ	MACH	Q	X/DB	Y/DB	Z/DB	MF/N	MA/N	QF/Q	QA/Q	VF/V	VA/V
169	571.1	66.5	0.604	1.515	896	179.0	700	69.1	0.00	0.985	PF/P
1	0.604	179.0	1C.88	0.41	-2.04	0.984	0.976	0.987	0.987	0.978	0.021
2	0.603	178.4	1C.88	0.41	-1.54	0.987	0.945	0.973	0.973	0.945	1.005
3	0.603	178.4	1C.88	0.41	-1.04	0.971	0.935	0.967	0.967	0.935	1.003
4	0.603	178.4	1C.88	0.41	-0.70	0.931	0.867	0.900	0.900	0.867	1.001
5	0.602	177.8	1C.88	0.41	-0.55	0.920	0.847	0.884	0.884	0.847	0.008
6	0.602	177.8	1C.88	0.41	-0.37	0.920	0.847	0.884	0.884	0.847	1.002
7	0.603	178.4	1C.88	0.41	-0.20	0.914	0.836	0.873	0.873	0.836	1.000
8	0.603	178.4	1C.88	0.41	-0.02	0.900	0.814	0.850	0.850	0.814	0.003
9	0.603	178.4	1C.88	0.41	0.13	0.911	0.830	0.867	0.867	0.830	1.001
10	0.603	178.4	1C.88	0.41	0.29	0.896	0.806	0.843	0.843	0.806	0.012
11	0.603	178.4	1C.88	0.41	0.46	0.914	0.838	0.875	0.875	0.838	1.003
12	0.603	178.4	1C.88	0.41	0.64	0.927	0.861	0.900	0.900	0.861	0.006
13	0.603	178.4	1C.88	0.41	0.98	0.942	0.892	0.939	0.939	0.892	1.006
14	0.603	178.4	1C.88	0.41	1.46	0.971	0.950	0.988	0.988	0.950	0.030
15	0.603	178.4	1C.88	0.41	1.97	0.951	0.985	0.995	0.995	0.985	1.004

RUN	TST	P	TA	CCNF	MACH	PN/L	PT	C	P	TT	0.00	ALPHA
SEQ	MACH	0	X/DB	Y/DR	Z/DR	MF/N	MA/M	QF/Q	QA/Q	VF/V	VA/V	CP
170	571	1	66	5	0.596	1.509	890	174.1	700	64.1	0.00	DF/P
2	0.	596	174.1	1C.87	-0.03	-2.04	0.919	0.849	0.924	0.021	1.005	
3	0.	596	174.1	1C.87	-0.03	-1.54	0.925	0.859	0.929	0.020	1.005	
4	0.	598	175.3	1C.87	-C.03	-1.04	0.927	0.863	0.931	0.015	1.004	
5	0.	598	175.3	1C.87	-0.03	-0.71	0.897	0.808	0.903	0.019	1.005	
6	0.	598	175.3	1C.87	-C.C2	-0.55	0.886	0.786	0.892	0.007	1.002	
7	0.	598	175.3	1C.87	-0.03	-0.38	0.886	0.786	0.893	-0.001	1.000	
8	0.	598	175.3	1C.87	-C.C2	-0.21	0.872	0.760	0.879	0.004	1.001	
9	0.	598	175.3	1C.87	-C.C2	-0.03	0.878	0.771	0.885	-0.002	0.999	
10	0.	600	175.9	1C.87	-C.C2	0.13	0.881	0.776	0.888	-0.005	0.999	
11	0.	600	175.9	1C.87	-C.C2	0.29	0.868	0.753	0.875	0.003	1.001	
12	C.	600	175.9	1C.87	-C.C2	0.46	0.894	0.798	0.901	-0.010	0.998	
13	0.	600	175.9	1C.87	-C.C2	0.62	0.896	0.805	0.902	0.008	1.002	
14	0.	601	176.5	1C.87	-0.03	0.97	0.920	0.849	0.925	0.008	1.002	
15	0.	601	176.5	1C.87	-C.C2	1.46	0.981	0.963	0.982	0.004	1.001	
16	0.	602	177.1	1C.87	-C.C2	1.97	0.982	0.970	0.983	0.021	1.005	

RUN	TST	P	TA	CCNF	MACH	PN/L	PT	C	P	TT	0.00	ALPHA
SEQ	MACH	0	X/DB	Y/DR	Z/DR	MF/N	MA/M	QF/Q	QA/Q	VF/V	VA/V	CP
171	571	1	66	5	0.602	1.519	891	177.1	697	65.0	0.00	DF/P
1	0.	602	177.1	1C.87	-0.38	-2.04	0.968	0.948	0.970	0.044	1.011	
2	0.	602	177.1	1C.87	-C.28	-1.54	0.975	0.957	0.977	0.028	1.007	
3	0.	602	177.1	1C.87	-C.38	-1.04	0.950	0.907	0.953	0.022	1.006	
4	0.	602	177.1	1C.87	-C.38	-0.70	0.907	0.824	0.913	0.002	1.000	
5	0.	602	177.1	1C.87	-C.C2	-0.53	0.890	0.794	0.896	0.007	1.002	
6	0.	602	177.1	1C.87	-0.38	-0.36	0.886	0.784	0.892	0.000	1.000	
7	C.	6C2	177.1	1C.87	-C.C2	-0.20	0.890	0.792	0.897	-0.003	0.999	
8	0.	602	177.1	1C.87	-C.C2	-0.04	0.880	0.773	0.886	-0.002	0.999	
9	0.	604	177.1	1C.87	-0.38	0.12	0.880	0.775	0.887	0.004	1.001	
10	0.	6C4	177.1	1C.87	-C.C2	0.30	0.888	0.788	0.894	-0.001	1.000	
11	0.	602	177.1	1C.87	-C.C2	0.46	0.895	0.802	0.901	0.005	1.001	
12	0.	6C2	177.1	1C.87	-C.C2	0.63	0.894	0.801	0.900	0.007	1.002	
13	0.	600	175.9	1C.87	-C.C2	0.96	0.924	0.858	0.929	0.014	1.003	
14	0.	601	176.5	1C.87	-C.C2	1.47	0.969	0.944	0.971	0.016	1.004	
15	0.	6C1	176.5	1C.87	-C.C2	1.96	0.980	0.970	0.983	0.024	1.006	

RUN	TST	P	TN	CCNF	MACH	RN/L	PT	G	P	TT	ALPHA
SEQ	MACH	Q	X/DB	Y/DR	Z/DB	MF/N	MA/M	QF/Q	OA/Q	VF/V	VA/V
172	571	1	66	5	0.601	1.514	.891	176.5	698	65.5	0.00
											PF/P
											0.020
											1.005
											0.016
											1.004
											0.013
											1.003
											0.005
											1.001
											0.008
											1.002
											-0.003
											0.999
											-0.005
											0.999
											-0.002
											1.000
											-0.006
											0.998
											-0.008
											1.002
											-0.008
											1.002
											-0.014
											1.004
											0.001
											1.000
											-0.016
											1.004
											0.027
											1.007

RUN	TST	P	TN	CCNF	MACH	RN/L	PT	G	P	TT	ALPHA
SEQ	MACH	Q	X/DR	Y/DP	Z/DP	MF/N	MA/M	QF/Q	OA/Q	VF/V	VA/V
173	571	1	66	5	0.602	1.514	.891	177.1	697	66.2	0.00
											PF/P
											0.007
											0.998
											-0.003
											0.999
											-0.010
											0.997
											-0.006
											0.998
											-0.001
											1.000
											-0.007
											1.002
											-0.002
											1.000
											-0.022
											1.006
											0.018
											1.005
											0.015
											1.004

RUN	TST	F	TIN	CCNF	WACH	RNL	PT	C	P	TT	ALPHA
SFC	MACH	G		X/DB	Y/DB	Z/DB	NF/N	MA/N	GF/N	QA/Q	VF/V
174	571	1	66	5	0.902	1.479	699	234.7	412	68.6	0.00
1	0.902	234.7	1C.87	-0.03	-1.98	0.924	0.879	0.933	0.053	1.030	
2	0.901	234.8	1C.87	-0.03	-1.54	0.931	0.885	0.939	0.039	1.022	
3	0.902	235.3	10.88	-0.03	-1.03	0.924	0.866	0.934	0.024	1.013	
4	0.901	234.8	1C.87	-0.03	-0.70	0.894	0.805	0.907	0.012	1.007	
5	0.900	234.3	1C.87	-0.03	-0.54	0.862	0.753	0.879	0.018	1.010	
6	0.900	234.3	1C.87	-0.03	-0.36	0.847	0.724	0.865	0.014	1.008	
7	0.900	234.4	1C.87	-0.03	-0.20	0.840	0.713	0.858	0.019	1.011	
8	0.900	234.4	1C.87	-0.03	-0.04	0.840	0.709	0.858	0.006	1.003	
9	0.902	235.2	1C.87	-0.03	0.13	0.845	0.711	0.862	-0.008	0.595	
10	0.903	235.7	1C.87	-0.03	0.30	0.854	0.726	0.870	-0.007	0.996	
11	0.903	235.1	1C.87	-0.03	0.46	0.860	0.738	0.876	-0.003	0.999	
12	0.903	235.1	1C.87	-0.03	0.62	0.858	0.736	0.875	-0.001	0.999	
13	0.902	234.7	1C.87	-0.03	0.97	0.859	0.819	0.911	0.025	1.014	
14	0.902	235.1	1C.88	-0.03	1.46	0.958	0.936	0.964	0.036	1.021	
15	0.904	235.6	1C.87	-0.03	1.97	0.965	0.956	0.970	0.045	1.026	

RUN	TST	P	TIN	CCNF	WACH	RNL	PT	C	P	TT	ALPHA
SFC	MACH	Q		X/DB	Y/DB	Z/DB	NF/N	MA/N	GF/N	QA/Q	VF/V
175	571	1	66	5	0.900	1.473	697	233.8	412	69.2	0.00
1	0.900	233.8	8.49	-0.01	-2.03	0.919	0.864	0.929	0.041	1.023	
2	0.899	233.8	8.49	-0.01	-1.52	0.919	0.868	0.929	0.048	1.027	
3	0.899	233.9	8.49	-0.01	-1.03	0.924	0.866	0.933	0.026	1.015	
4	0.899	233.9	8.49	-0.01	-0.69	0.881	0.784	0.895	0.017	1.010	
5	0.899	233.9	8.49	-0.01	-0.53	0.865	0.750	0.880	0.005	1.003	
6	0.899	233.9	8.49	-0.01	-0.36	0.834	0.694	0.852	-0.005	0.997	
7	0.900	234.3	8.49	-0.01	-0.19	0.815	0.658	0.835	-0.019	0.989	
8	0.903	235.2	8.49	-0.01	-0.01	0.824	0.668	0.843	-0.028	0.984	
9	0.903	235.1	8.49	-0.01	0.14	0.811	0.650	0.831	-0.019	0.989	
10	0.904	235.1	8.49	-0.01	0.31	0.806	0.645	0.827	-0.014	0.992	
11	0.901	233.7	8.49	-0.01	0.47	0.810	0.661	0.831	0.011	1.006	
12	0.896	233.0	8.49	-0.01	0.64	0.821	0.699	0.849	0.023	1.013	
13	0.895	232.6	8.49	-0.01	0.97	0.910	0.835	0.921	0.015	1.008	
14	0.898	234.0	8.49	-0.01	1.47	0.972	0.962	0.976	0.030	1.017	

RUN	TST	P	TN	CCNF	MACH	RN/L	PT	C	TT	ALPHA
176	571	1	66	E C.852	1.498	726	229.7	452	69.8	0.00
SEG	MACH	0	X/DB	Y/DB	Z/DB	MF/N	MA/M	CF/Q	CA/Q	VF/V
1	0.852	229.7	8.49	-C.01	-2.03	0.9C4	0.830	0.915	0.030	1.C15
2	0.852	229.7	8.49	-0.01	-1.53	C.924	0.864	0.933	0.024	1.C12
3	0.853	230.1	8.49	-C.01	-1.03	C.922	0.856	0.931	0.014	1.C07
4	0.853	230.1	8.49	-C.01	-0.69	C.877	0.772	0.890	0.008	1.004
5	0.853	230.1	8.49	-0.01	-0.53	0.857	0.735	0.872	0.003	1.C01
6	0.853	230.1	8.49	-C.01	-0.36	C.827	0.685	0.844	0.003	1.C01
7	0.853	230.1	8.49	-C.01	-0.19	C.820	0.669	0.837	-0.007	0.997
8	0.853	230.1	8.49	-C.01	-0.02	C.815	0.662	0.833	-0.004	0.998
10	0.852	229.8	8.49	-C.01	0.21	C.8C5	0.646	0.823	-0.003	0.998
11	0.852	229.8	8.49	-C.01	0.48	C.827	0.684	0.844	-0.001	1.C00
12	0.852	229.8	8.49	-C.01	0.65	C.851	0.722	0.867	-0.007	0.997
13	0.853	230.1	8.49	-0.01	0.97	C.928	0.866	0.936	0.011	1.C05
14	0.853	230.1	8.49	-C.01	1.48	C.971	0.959	0.974	0.035	1.C18
15	0.851	229.3	8.49	-0.01	1.98	C.975	0.968	0.978	0.037	1.C19

RUN	TST	P	TN	CCNF	MACH	RN/L	PT	C	TT	ALPHA
177	571	1	66	5 C.850	1.497	727	229.4	453	70.0	0.00
SFQ	MACH	C	X/DB	Y/DB	Z/DB	MF/N	MA/M	CF/Q	CA/Q	VF/V
1	0.850	229.4	1C.87	-0.03	-2.05	0.920	0.858	0.930	0.026	1.C13
2	0.850	229.4	1C.87	-0.03	-1.53	C.925	0.866	0.933	0.026	1.013
3	0.850	229.4	1C.87	-0.03	-1.03	C.916	0.847	0.926	0.018	1.C09
4	0.850	229.4	1C.87	-C.03	-0.71	C.884	0.786	0.897	0.011	1.C05
5	0.850	229.0	1C.87	-C.03	-0.55	C.872	0.763	0.885	0.010	1.005
6	0.850	229.0	1C.87	-C.03	-0.38	C.865	0.750	0.879	0.006	1.C03
7	0.850	229.0	1C.87	-C.03	-0.20	C.857	0.739	0.871	0.014	1.C07
8	0.848	228.6	1C.87	-C.03	-0.03	C.859	0.738	0.873	0.002	1.C01
9	0.849	229.1	1C.87	-C.03	0.13	C.861	0.742	0.876	-0.009	1.C00
10	0.849	229.1	1C.87	-C.03	0.29	C.857	0.734	0.871	0.002	1.001
11	0.850	229.4	1C.87	-C.03	0.46	C.857	0.737	0.872	0.005	1.C02
12	0.850	229.4	1C.87	-C.03	0.63	C.875	0.765	0.888	0.002	1.C01
13	0.850	229.4	1C.87	-C.03	0.96	C.915	0.843	0.925	0.011	1.C06
14	0.852	229.8	1C.87	-C.03	1.46	C.970	0.952	0.974	0.022	1.C11
15	0.852	229.8	1C.87	-C.03	1.97	C.974	0.970	0.978	0.036	1.018

RUN	TST	P	TN	CCNF	MACH	RNL	PT	G	T	TT	ALPHA
SFG	MACH	Q	X/DR	Y/DR	Z/DR	MF/N	MA/N	GF/Q	QA/Q	VF/V	VA/V
178	571	1	66	5	C.250	1.517	1891	79.5	1811	66.4	0.00
1	0.250	79.5	10.87	0.41	-2.04	0.995	0.000	0.989	0.000	0.995	0.000
2	C.250	79.5	1C.87	C.41	-1.54	C.984	0.000	0.967	0.000	0.984	0.000
3	0.249	78.8	1C.87	C.41	-1.04	C.968	0.000	0.937	0.000	0.969	0.000
4	0.250	79.5	1C.87	C.41	-0.71	C.917	0.000	0.841	0.000	0.918	0.000
5	0.250	79.5	1C.87	C.41	-0.54	C.923	0.000	0.851	0.000	0.924	0.000
6	0.250	79.5	10.87	C.41	-0.37	C.928	0.000	0.861	0.000	0.929	0.000
7	0.250	79.5	1C.87	C.41	-0.20	C.915	0.000	0.837	0.000	0.916	0.000
8	0.250	79.5	10.87	C.41	-0.03	C.918	0.000	0.843	0.000	0.919	0.000
9	0.250	79.5	1C.87	C.41	0.13	C.919	0.000	0.844	0.000	0.920	0.000
10	0.250	79.5	1C.87	C.41	0.38	C.910	0.000	0.827	0.000	0.911	0.000
11	C.250	79.5	1C.87	C.41	0.46	C.928	0.000	0.861	0.000	0.929	0.000
12	0.250	79.5	1C.87	C.41	0.63	C.939	0.000	0.880	0.000	0.939	0.000
13	0.250	79.5	10.87	C.41	0.96	C.950	0.000	0.901	0.000	0.950	0.000
14	0.250	79.5	1C.87	C.41	1.47	C.986	0.000	0.970	0.000	0.986	0.000
15	0.250	79.5	10.87	C.41	1.96	C.955	0.000	0.989	0.000	0.995	0.000

RUN	TST	P	TN	CCNF	MACH	RNL	PT	G	T	TT	ALPHA
SFG	MACH	Q	X/DR	Y/DR	Z/DR	MF/N	MA/N	GF/Q	QA/Q	VF/V	VA/V
179	571	1	66	5	0.249	1.512	1892	78.8	1812	66.2	0.00
1	0.249	78.8	10.87	-0.03	-2.04	C.939	0.000	0.881	0.000	0.940	0.000
2	0.248	78.1	1C.87	-C.02	-1.54	C.944	0.000	0.891	0.000	0.945	0.000
3	0.248	78.1	1C.87	-C.02	-1.04	C.946	0.000	0.894	0.000	0.947	0.000
4	0.248	78.1	1C.87	-0.03	-0.71	C.911	0.000	0.829	0.000	0.912	0.000
5	0.248	78.1	1C.87	-C.C3	-0.55	C.892	0.000	0.796	0.000	0.894	0.000
6	0.248	78.1	1C.87	-0.03	-0.37	C.910	0.000	0.827	0.000	0.911	0.000
7	0.248	78.1	1C.87	-0.03	-0.20	C.890	0.000	0.792	0.000	0.891	0.000
8	0.248	78.1	1C.87	-C.02	-0.04	C.913	0.000	0.833	0.000	0.914	0.000
9	0.248	78.1	1C.87	-C.03	0.13	C.895	0.000	0.801	0.000	0.896	0.000
10	0.248	78.1	1C.87	-C.C3	0.30	C.892	0.000	0.796	0.000	0.894	0.000
11	0.248	78.1	10.87	-0.03	0.46	C.930	0.000	0.864	0.000	0.931	0.000
12	0.248	78.1	1C.87	-C.03	0.63	C.913	0.000	0.833	0.000	0.914	0.000
13	0.248	78.1	1C.87	-C.C3	0.56	C.926	0.000	0.857	0.000	0.927	0.000
14	0.249	78.8	1C.87	-0.03	1.46	C.984	0.000	0.968	0.000	0.984	0.000
15	0.249	78.8	1C.87	-C.03	1.97	C.952	0.000	0.984	0.000	0.992	0.000

RUN	TST	P	TN	CNF	MACH	RNL	PT	G	P	TT	ALPHA
SEQ	MACH	Q	X/DR	Y/DR	Z/DR	MF/N	WA/N	CF/Q	QA/Q	VF/V	VA/V
180	571	1	66	5	0.248	1.506	1.891	78.1	1812	65.9	0.00
1	0.248	78.1	1C.87	-0.38	-2.C3	C.994	0.000	C.987	C.000	0.994	0.000
2	0.249	78.8	1C.87	-C.38	-1.54	C.980	0.000	C.960	C.000	0.980	0.000
3	0.248	78.1	1C.87	-C.38	-1.C5	C.945	0.000	C.892	C.000	0.946	0.000
4	0.248	78.1	1C.87	-C.38	-0.71	0.907	0.000	C.822	C.000	0.958	0.000
5	0.248	78.1	1C.87	-C.38	-0.54	C.923	0.000	C.852	0.000	0.924	0.000
6	0.248	78.1	1C.87	-0.38	-0.37	C.906	0.000	C.820	C.000	0.907	0.000
7	0.249	78.8	1C.87	-C.38	-0.21	C.890	0.000	C.792	C.000	0.891	0.000
8	0.249	78.8	1C.87	-C.38	-0.05	C.9C1	0.000	C.811	C.000	0.902	0.000
9	0.248	78.1	1C.87	-0.38	0.13	C.910	0.000	C.827	C.000	0.911	C.000
10	0.248	78.1	1C.87	-C.38	0.30	C.900	0.000	C.810	C.000	0.901	0.000
11	0.248	78.1	1C.88	-0.38	0.46	C.9C2	0.000	C.815	C.000	0.904	0.000
12	0.248	78.1	1C.88	-C.38	0.63	C.954	0.000	C.910	0.000	0.955	0.000
13	0.249	78.8	1C.88	-C.38	0.96	C.942	0.000	C.886	C.000	0.942	0.000
14	0.249	78.8	1C.88	-C.38	1.47	C.966	0.000	C.932	C.000	0.966	0.000
15	0.249	78.8	1C.87	-C.38	1.96	C.991	0.000	C.981	C.000	0.991	0.000

RUN	TST	P	TN	CNF	MACH	RNL	PT	G	P	TT	ALPHA
SEQ	MACH	Q	X/DR	Y/DR	Z/DR	MF/N	WA/N	CF/Q	QA/Q	VF/V	VA/V
181	571	1	66	5	0.249	1.514	1.892	78.8	1812	65.7	0.00
1	0.249	78.8	1C.87	-0.48	-2.C5	C.951	0.000	C.981	C.000	0.991	0.000
2	0.249	78.8	1C.87	-0.48	-1.54	C.975	0.000	C.951	C.000	0.976	0.000
3	0.248	78.1	1C.87	-C.48	-1.C4	C.954	0.000	C.910	C.000	0.955	0.000
4	0.249	78.8	1C.87	-C.48	-0.71	C.912	0.000	C.831	C.000	0.913	0.000
5	0.250	79.5	1C.87	-C.48	-0.53	C.905	0.000	C.818	C.000	0.906	0.000
6	0.249	78.8	1C.87	-C.48	-0.38	C.9C7	0.000	C.822	C.000	0.908	0.000
7	0.249	78.8	1C.87	-C.48	-0.21	C.922	0.000	C.852	C.000	0.924	0.000
8	0.249	78.8	1C.87	-C.48	-0.04	C.914	0.000	C.834	C.000	0.915	0.000
9	0.249	78.8	1C.87	-C.48	0.12	C.899	0.000	C.8C8	C.000	0.900	0.000
10	0.250	79.5	1C.87	-C.48	0.25	C.914	0.000	C.835	C.000	0.915	0.000
11	0.250	79.5	1C.87	-C.48	0.47	C.9C8	0.000	C.823	C.000	0.909	0.000
12	0.250	79.5	1C.87	-C.48	0.63	C.927	0.000	C.858	C.000	0.927	0.000
13	0.250	79.5	1C.87	-C.48	0.96	C.951	0.000	C.905	C.000	0.952	0.000
14	0.250	79.5	1C.87	-C.48	1.46	C.990	0.000	C.979	C.000	0.990	0.000
15	0.250	79.5	1C.87	-C.48	1.97	C.991	0.000	C.979	C.000	0.990	0.000

RUN	TST	P	TN	CNF	MACH	PN/L	PT	C	P	TT	ALPHA
182	571	1	66	5	0.249	1.514	1892	78.8	1812	65.5	0.00
	SFG		MACH	0	X/DR	Y/DR	Z/DR	MF/N	MA/M	QF/Q	PF/P
1	0.249			78.8	1C.00	C.00	-0.37	C.852	0.C00	0.796	0.000
2	0.250			79.5	1C.00	C.00	-0.19	C.885	0.C00	0.782	0.000
3	0.250			79.5	1C.00	C.00	-0.04	C.885	0.C00	0.782	0.000
4	0.250			79.5	1C.00	C.00	0.13	C.891	C.000	0.792	C.000
5	0.250			79.5	C.99	C.00	0.30	C.900	C.000	0.810	0.000
6	0.250			79.5	9.99	C.00	0.46	C.905	C.000	0.818	0.000
7	0.249			78.8	9.99	C.00	0.64	C.915	0.000	0.836	0.000
8	0.249			78.8	9.99	C.00	0.96	C.958	0.000	0.918	0.000
9	0.249			78.8	9.99	0.00	1.47	C.989	C.000	0.977	0.000
10	0.249			78.8	9.99	0.00	1.97	C.997	0.000	0.993	0.000

RUN	TST	P	TN	CNF	MACH	PN/L	PT	C	P	TT	ALPHA
183	571	1	66	5	0.249	1.515	1892	78.8	1812	65.4	0.00
	SEC		MACH	C	X/DR	Y/DR	Z/DR	MF/N	MA/M	QF/Q	PF/P
1	0.249			78.8	7.C5	0.01	-2.02	0.936	0.000	0.876	0.000
2	0.248			78.1	7.C5	C.01	-1.51	C.950	0.000	0.901	C.000
3	0.248			78.1	7.C5	0.01	-1.01	C.937	0.000	0.877	C.000
4	0.249			78.8	7.05	C.01	-0.68	C.901	0.000	0.811	C.000
5	0.248			78.1	7.05	C.01	-0.52	C.849	C.000	C.720	C.000
6	0.249			78.8	7.C5	C.01	-0.35	C.853	C.000	0.727	C.000
7	0.249			78.8	7.05	C.C1	-0.19	C.812	C.000	0.659	C.000
8	0.249			78.8	7.C5	C.01	-0.01	C.832	C.000	0.690	C.000
9	0.249			78.8	7.C5	C.C1	0.15	C.885	C.000	0.782	C.000
10	0.249			78.8	7.C5	C.01	0.32	C.867	C.000	0.750	C.000
11	0.249			78.8	7.C5	C.01	0.48	C.893	C.000	0.796	C.000
12	0.249			78.8	7.C5	C.01	0.66	C.908	C.000	0.824	C.000
13	0.249			78.8	7.C5	C.01	0.95	C.947	C.000	0.895	C.000
14	0.249			78.8	7.C5	C.01	1.45	C.991	C.000	0.982	C.000
15	0.249			78.8	7.C5	C.01	1.95	C.991	C.000	0.981	C.000

RUN	TST	F	TN	CCNF	MACH	RN/L	PT	G	P	TT	ALPHA
SEQ	MACH	C	X/DB	Y/DB	Z/DB	MF/N	MA/M	QF/Q	DA/Q	VF/V	VA/V
184	571	1	66	5	0.249	1.515	1.892	78.8	1812	65.3	0.00
1	0.249	78.8	8.49	-0.45	-2.03	0.992	0.000	0.984	c.000	0.992	0.00
2	0.249	78.8	8.49	-0.45	-1.52	c.986	0.000	0.972	c.000	0.986	0.00
3	0.249	78.8	8.49	-0.45	-1.03	c.973	0.000	0.946	0.000	0.973	0.00
4	0.249	78.8	8.49	-c.45	-0.70	c.907	0.000	0.822	0.000	0.908	0.00
5	0.249	78.8	8.49	-c.45	-0.52	c.882	0.000	0.778	c.000	0.884	0.00
6	0.249	78.8	8.49	-c.45	-0.36	c.898	0.000	0.804	c.000	0.899	c.00
7	0.249	78.8	8.49	-c.45	-0.19	c.908	0.000	c.824	c.000	0.909	0.00
8	0.249	78.8	8.49	-c.45	-0.02	c.893	0.000	0.796	c.000	0.894	0.00
9	0.249	78.8	8.49	-c.45	0.14	c.896	0.000	0.801	0.000	0.897	0.00
10	0.249	78.8	8.49	-c.45	0.31	c.898	0.000	c.806	c.000	0.899	0.00
11	0.249	78.8	8.49	-c.45	0.48	c.894	0.000	c.799	c.000	0.895	0.00
12	0.250	79.5	8.49	-c.45	0.64	c.925	0.000	c.862	c.000	0.929	0.00
13	0.250	79.5	8.49	-c.45	0.98	c.928	0.000	c.861	c.000	0.929	c.00
14	0.249	78.8	8.49	-c.45	1.49	c.951	0.000	c.981	c.000	0.991	0.00
15	0.249	78.8	8.49	-c.45	1.98	c.995	0.000	c.989	c.000	0.995	0.00

RUN	TST	F	TN	CCNF	MACH	RN/L	PT	G	P	TT	ALPHA
SEQ	MACH	C	X/DB	Y/DB	Z/DB	MF/N	MA/M	QF/Q	DA/Q	VF/V	VA/V
185	571	1	66	5	0.249	1.515	1.891	78.8	1811	65.3	0.00
1	0.249	78.8	8.49	-0.01	-2.02	c.931	0.000	0.867	0.000	0.932	0.00
2	0.249	78.8	8.49	-c.01	-1.53	c.942	0.000	0.886	0.000	0.942	0.00
3	0.249	78.8	8.49	-0.01	-1.03	c.950	0.000	c.902	0.000	0.951	0.00
4	0.250	79.5	8.49	-c.01	-0.69	c.908	0.000	c.823	0.000	0.909	0.00
5	0.249	78.8	8.49	-c.01	-0.52	c.872	0.000	c.759	c.000	0.873	0.00
6	0.249	78.8	8.49	-0.01	-0.36	c.877	0.000	c.768	c.000	0.878	0.00
7	0.249	78.8	8.49	-c.01	-0.20	c.886	0.000	c.783	c.000	0.887	0.00
8	0.250	79.5	8.49	-0.01	-0.02	c.854	0.000	c.728	0.000	0.855	0.00
9	0.249	78.8	8.49	-c.01	0.15	c.875	0.000	c.764	c.000	0.876	0.00
10	0.249	78.8	8.49	-0.01	0.31	c.887	c.000	c.785	c.000	0.888	0.00
11	0.250	79.5	8.49	-c.01	0.48	c.914	0.000	c.834	c.000	c.915	0.00
12	0.250	79.5	8.49	-c.01	0.65	c.922	0.000	c.868	c.000	c.933	0.00
13	0.250	79.5	8.49	-c.01	0.98	c.949	0.000	c.900	c.000	c.949	0.00
14	0.251	80.2	8.49	-c.01	1.48	c.982	0.000	c.964	c.000	c.982	0.00
15	0.250	79.5	8.49	-c.01	1.98	c.995	0.000	c.989	c.000	c.995	0.00

RUN	TST	P	TN	CCNF	MACH	PN/L	PT	G	P	TT	ALPHA
SEC	MACH	Q	X/DR	Y/DR	Z/DR	MF/N	MA/M	QF/Q	QA/Q	VF/V	VA/V
186	571	1	66	5	0.251	1.528	1.892	80.2	1811	65.4	0.00
1	0.251	80.2	8.49	0.43	-2.03	0.993	0.000	0.986	0.000	0.993	0.00
2	0.251	80.2	8.49	0.43	-1.52	0.993	0.000	0.986	0.000	0.993	0.00
3	0.251	80.2	8.49	0.43	-1.03	0.978	0.000	0.955	0.000	0.978	0.00
4	0.251	80.2	8.49	0.43	-0.69	0.905	0.000	0.818	0.000	0.906	0.00
5	0.251	80.2	8.49	0.43	-0.52	0.912	0.000	0.832	0.000	0.913	0.00
6	0.253	80.8	8.49	0.43	-0.36	0.928	0.000	0.861	0.000	0.929	0.00
7	0.253	80.8	8.49	0.43	-0.17	0.935	0.000	0.872	0.000	0.935	0.00
8	0.251	80.2	8.49	0.43	-0.02	0.911	0.000	0.828	0.000	0.912	0.00
9	0.251	80.2	8.49	0.43	0.14	0.915	0.000	0.837	0.000	0.916	0.00
10	0.251	80.2	8.49	0.43	0.31	0.955	0.000	0.818	0.000	0.906	0.00
11	0.251	80.2	8.49	0.43	0.48	0.905	0.000	0.818.	0.000	0.906	0.00
12	0.251	80.2	8.49	0.43	0.64	0.905	0.000	0.827	0.000	0.910	0.00
13	0.251	80.2	8.49	0.43	0.99	0.944	0.000	0.890	0.000	0.944	0.00
14	0.251	80.2	8.49	0.43	1.49	0.982	0.000	0.964	0.000	0.982	0.00
15	0.251	80.2	8.49	0.42	1.98	0.988	0.000	0.976	0.000	0.988	0.00

RUN	TST	P	TN	CCNF	MACH	PN/L	PT	G	P	TT	ALPHA
SEC	MACH	Q	X/DR	Y/DR	Z/DR	MF/N	MA/M	QF/Q	QA/Q	VF/V	VA/V
187	571	1	66	5	0.952	1.484	679	240.7	379	63.8	20.00
2	0.952	240.7	1C.88	0.41	-2.04	C.966	0.962	0.971	0.971	0.971	0.049
3	0.952	240.7	1C.88	0.41	-1.54	C.966	0.960	0.942	0.960	0.960	1.031
4	0.952	240.7	1C.88	0.41	-1.04	C.960	0.960	0.854	0.929	0.929	1.029
5	0.950	240.1	1C.87	0.41	-0.71	C.918	0.854	0.854	0.929	0.929	0.933
6	0.950	240.1	1C.87	0.41	-0.53	C.922	0.861	0.933	0.933	0.933	0.933
7	0.950	239.6	1C.88	0.41	-0.37	C.935	0.884	0.884	0.944	0.944	0.944
8	0.950	240.1	1C.88	0.41	-0.20	C.919	0.852	0.852	0.930	0.930	0.930
9	0.950	239.6	1C.88	0.41	-0.04	C.922	0.855	0.855	0.932	0.932	0.932
10	0.950	239.6	1C.88	0.41	0.12	C.907	0.827	0.827	0.920	0.920	0.920
11	0.950	239.6	1C.88	0.41	0.29	C.886	0.789	0.789	0.901	0.901	0.901
12	0.947	238.8	1C.88	0.41	0.46	C.888	0.792	0.792	0.902	0.902	0.902
13	0.947	238.8	1C.88	0.41	0.63	C.879	0.775	0.775	0.895	0.895	0.895
14	0.948	239.3	1C.88	0.41	0.96	C.891	0.798	0.798	0.906	0.906	0.906
15	0.948	239.3	1C.88	0.41	1.16	C.914	0.838	0.838	0.925	0.925	0.925
16	0.949	239.7	1C.88	0.41	1.47	C.954	0.917	0.917	0.961	0.961	0.961
17	0.948	239.3	1C.87	0.41	1.96	C.969	0.963	0.963	0.974	0.974	0.974

RUN	TST	P	TA	CCNF	MACH	RN/L	PT	G	P	TT	20.00	65.3	PF/P
SEQ	MACH	G	X/DR	Y/DB	Z/DR	MF/N	MA/M	QF/Q	QA/Q	VF/V	VA/V	CP	PF/P
188	571	1	66	5	0.954	1.477	678	240.6	377	0.824	0.912	0.031	1.020
1	0.954	240.6	1C.88	-0.03	-2.04	0.899	0.856	0.926	0.040	1.026			
2	0.953	240.1	1C.88	-0.03	-1.55	C.914	0.857	0.928	0.032	1.021			
3	0.952	240.1	10.88	-0.03	-1.04	C.916	0.828	0.916	0.026	1.016			
4	0.951	240.1	1C.88	-0.03	-0.70	C.902	0.799	0.902	0.025	1.016			
5	0.951	240.1	1C.88	-0.03	-0.54	C.887	0.790	0.899	0.019	1.012			
6	0.950	239.6	1C.88	-0.03	-0.38	0.884	0.781	0.895	0.015	1.010			
7	0.950	239.6	1C.88	-0.03	-0.21	C.879	0.773	0.891	0.015	1.009			
8	0.948	239.3	10.88	-0.03	-0.04	C.875	0.771	0.891	0.012	1.008			
9	0.948	239.3	1C.88	-0.03	-0.13	C.875	0.765	0.887	0.014	1.009			
10	0.948	239.3	10.88	-0.03	-0.29	C.871	0.765	0.887	0.005	1.003			
11	0.946	238.9	1C.88	-0.03	0.46	C.880	0.776	0.895	-0.004	0.998			
12	0.946	238.9	10.88	-0.03	0.62	C.878	0.769	0.894	-0.008	0.995			
13	0.947	239.3	1C.88	-0.03	0.96	C.887	0.783	0.902	-0.004	0.998			
14	0.950	240.2	10.88	-0.03	1.16	C.894	0.797	0.903	-0.009	1.006			
15	0.950	240.2	1C.87	-C.03	1.46	C.924	0.877	0.943	0.040	1.025			
16	0.948	239.3	1C.87	-C.03	1.97	C.967	0.959	0.972					

RUN	TST	P	TA	CCNF	MACH	RN/L	PT	G	P	TT	20.00	66.3	PF/P
SEQ	MACH	G	X/DR	Y/DB	Z/DR	MF/N	MA/M	QF/Q	QA/Q	VF/V	VA/V	CP	PF/P
189	571	1	66	5	0.954	1.476	679	241.2	378	0.956	0.973	0.031	1.020
1	0.954	241.2	1C.87	-C.38	-2.04	C.968	0.958	0.975	0.028	1.018			
2	0.956	241.7	1C.87	-C.38	-1.54	C.970	0.940	0.968	0.024	1.016			
3	0.957	241.7	1C.88	-0.38	-1.05	C.962	0.926	0.936	0.022	1.014			
4	0.956	241.1	1C.87	-C.38	-0.71	C.926	0.825	0.915	0.024	1.015			
5	0.953	240.1	1C.87	-C.38	-0.54	C.901	0.816	0.910	0.027	1.017			
6	0.953	240.1	1C.87	-C.38	-0.37	C.896	0.811	0.909	0.018	1.011			
7	0.949	239.1	1C.87	-0.38	-0.21	C.895	0.818	0.912	0.021	1.013			
8	0.949	239.1	1C.88	-C.38	-0.04	C.899	0.777	0.893	0.013	1.008			
9	0.949	239.2	1C.87	-C.38	0.13	C.878	0.751	0.881	0.009	1.005			
10	0.950	239.6	1C.87	-C.38	0.30	C.864	0.773	0.894	0.005	1.003			
11	0.948	239.3	1C.87	-C.38	0.47	C.878	0.756	0.886	-0.001	0.999			
12	0.949	239.7	1C.87	-C.38	0.64	C.870	0.778	0.895	0.008	1.005			
13	0.949	239.7	1C.87	-C.38	0.97	C.880	0.830	0.922	0.005	1.003			
14	0.947	239.3	1C.87	-C.38	1.17	C.910	0.877	0.941	0.015	1.009			
15	0.947	239.3	1C.87	-C.38	1.46	C.932	0.961	0.948	0.043	1.027			
16	0.944	238.0	1C.87	-C.38	1.96	C.961	0.959	0.966					

RUN	TST	F	TN	CCNF	MACH	RN/L	PT	G	P	TT	ALPHA
SFC		MACH	Q	X/DR	Y/DR	Z/DR	MF/N	MA/N	QF/Q	QA/Q	VF/V
190	571	1	66	5	0.949	1.483	685	242.0	384	67.1	20.00
1	0.949	242.0	C	1C.87	-0.48	-2.C5	C.974	0.969	0.978	0.033	1.021
2	0.950	242.4	C	1C.87	-0.48	-1.54	C.972	0.965	0.977	0.032	1.020
3	0.952	242.9	C	1C.87	-C.48	-1.C5	C.960	0.938	0.966	0.029	1.019
4	0.952	242.9	C	1C.87	-C.48	-0.71	C.917	0.851	0.928	0.020	1.013
5	0.952	242.9	C	1C.87	-C.48	-0.54	C.910	0.836	0.922	0.015	1.009
6	0.951	242.4	C	1C.87	-0.48	-0.37	C.915	0.845	0.927	0.013	1.008
7	0.951	242.4	C	1C.87	-0.48	-0.21	C.920	0.850	0.931	0.009	1.005
8	0.951	242.4	C	1C.87	-C.48	-0.04	C.908	0.831	0.921	0.012	1.007
9	0.951	242.4	C	1C.87	-0.48	0.12	C.903	0.819	0.916	0.007	1.005
10	0.951	242.4	C	1C.87	-C.48	C.29	C.936	0.849	0.945	-0.047	0.970
11	0.951	242.4	C	1C.87	-0.48	0.47	C.880	0.775	0.895	0.002	1.001
12	0.951	242.4	C	1C.87	-0.48	0.63	C.877	0.769	0.893	-0.000	1.000
13	0.950	241.9	C	1C.87	-C.48	0.96	C.894	0.800	0.908	0.003	1.002
14	0.950	241.9	C	1C.87	-0.48	1.16	C.912	0.834	0.924	0.003	1.002
15	0.950	242.4	C	1C.87	-C.48	1.46	C.944	0.899	0.952	0.014	1.009
16	0.950	242.4	C	1C.87	-0.48	1.97	C.971	0.966	0.975	0.041	1.026

RUN	TST	F	TN	CCNF	MACH	RN/L	PT	G	P	TT	ALPHA
SFC		MACH	Q	X/DR	Y/DR	Z/DR	MF/N	MA/N	QF/Q	QA/Q	VF/V
191	571	1	66	5	0.952	1.479	684	242.3	382	68.1	20.00
1	0.952	242.3	C	8.49	0.43	-2.03	C.973	0.968	0.977	0.033	1.021
2	0.953	242.5	C	8.49	C.43	-1.52	C.970	0.963	0.974	0.037	1.023
3	0.954	243.4	C	8.49	0.43	-1.03	C.960	0.941	0.966	0.034	1.022
4	0.952	242.9	C	8.49	C.42	-0.69	C.917	0.852	0.928	0.021	1.013
5	0.952	242.9	C	8.49	C.43	-0.52	C.923	0.880	0.943	0.017	1.011
6	0.950	242.4	C	8.49	0.43	-0.36	C.930	0.872	0.940	0.012	1.008
7	0.950	242.4	C	8.49	C.43	-0.19	C.922	0.853	0.933	0.006	1.004
8	0.950	242.4	C	8.49	C.42	-0.03	C.918	0.843	0.929	-0.000	1.000
9	0.949	242.0	C	8.49	C.43	0.14	C.896	0.800	0.910	-0.007	0.996
10	0.948	241.5	C	8.49	C.43	0.30	C.886	0.777	0.901	-0.015	0.991
11	0.948	241.5	C	8.49	C.43	0.48	C.880	0.765	0.895	-0.019	0.988
12	0.948	241.5	C	8.49	C.43	0.65	C.877	0.756	0.893	-0.026	0.983
13	0.948	241.5	C	8.49	C.43	0.98	C.915	0.822	0.927	-0.031	0.981
14	0.950	241.9	C	8.49	C.43	1.18	C.929	0.855	0.939	-0.013	0.992
15	0.947	241.0	C	8.49	C.43	1.48	C.970	0.941	0.975	-0.000	1.000
16	0.948	241.5	C	8.49	C.43	1.98	C.976	0.975	0.980	0.038	1.024

RUN	TST	P	TN	MACH	CCNF	RN/L	PT	C	P	TT	ALPHA
192	571	1	66	5	0.951	1.478	685	242.4	383	68.6	20.00
SEG	MACH	G	X/DR	Y/DR	Z/DR	MF/N	MA/M	QF/Q	QA/Q	VF/V	VA/V
1	0.951	242.4	8.49	-0.01	-2.03	C.900	0.821	0.913	0.927	0.935	0.935
2	0.952	242.3	8.49	-0.01	-1.53	C.916	0.853	0.919	0.916	0.925	0.925
3	0.951	241.8	8.49	-0.01	-1.02	0.925	0.865	0.916	0.914	0.924	0.924
4	0.953	242.9	8.49	-0.01	-0.65	C.906	0.825	0.914	0.914	0.923	0.923
5	0.953	242.9	8.49	-0.01	-0.53	0.901	0.816	0.914	0.914	0.922	0.922
6	0.953	242.9	8.49	-0.01	-0.36	C.885	0.782	0.900	0.900	0.909	0.909
7	0.951	242.4	8.49	-0.01	-0.19	C.869	0.754	0.886	0.886	0.895	0.895
8	0.951	242.4	8.49	-0.01	-0.01	C.853	0.724	0.872	0.872	0.881	0.881
9	0.951	242.4	8.49	-0.01	0.15	C.868	0.744	0.885	0.885	0.894	0.894
10	0.951	242.4	8.49	-0.01	0.31	C.862	0.734	0.879	0.879	0.888	0.888
11	0.952	242.9	8.49	-0.01	0.48	C.849	0.711	0.868	0.868	0.877	0.877
12	0.952	242.9	8.49	-0.01	0.65	C.850	0.710	0.868	0.868	0.877	0.877
13	0.952	242.9	8.49	-0.01	0.98	C.875	0.759	0.891	0.891	0.900	0.900
14	0.951	242.4	8.49	-0.01	1.18	C.914	0.833	0.926	0.926	0.935	0.935
15	0.950	241.9	8.49	-0.01	1.48	0.955	0.919	0.962	0.962	0.971	0.971
16	0.950	241.9	8.49	-0.01	1.98	C.974	0.973	0.977	0.977	0.986	0.986

RUN	TST	P	TN	MACH	CCNF	RN/L	PT	C	P	TT	ALPHA
193	571	1	66	5	0.952	1.475	684	242.3	382	69.1	20.00
SFG	MACH	Q	X/DR	Y/DR	Z/DR	MF/N	MA/M	QF/Q	QA/Q	VF/V	VA/V
1	0.952	242.3	8.49	-0.26	-2.02	C.972	0.963	0.976	0.976	0.981	0.981
2	0.952	242.3	8.49	-0.36	-1.52	0.973	0.964	0.977	0.977	0.982	0.982
3	0.953	242.9	8.49	-0.36	-1.03	C.966	0.950	0.971	0.971	0.978	0.978
4	0.952	242.9	8.49	-0.36	-0.69	0.925	0.865	0.935	0.935	0.944	0.944
5	0.954	243.4	8.49	-0.36	-0.52	0.902	0.819	0.915	0.915	0.924	0.924
6	0.952	242.9	8.49	-0.26	-0.36	C.889	0.791	0.904	0.904	0.913	0.913
7	0.950	241.9	8.49	-0.36	-0.19	0.886	0.783	0.901	0.901	0.910	0.910
8	0.949	241.4	8.49	-0.36	-0.01	C.883	0.776	0.899	0.899	0.908	0.908
9	0.949	241.4	8.49	-0.36	0.14	0.877	0.763	0.893	0.893	0.902	0.902
10	0.949	241.4	8.49	-0.36	0.32	0.871	0.751	0.887	0.887	0.896	0.896
11	0.949	241.4	8.49	-0.36	0.48	0.846	0.709	0.865	0.865	0.874	0.874
12	0.947	241.0	8.49	-0.36	0.65	C.866	0.734	0.878	0.878	0.887	0.887
13	0.948	241.5	8.49	-0.36	0.98	0.888	0.785	0.903	0.903	0.912	0.912
14	0.946	241.1	8.49	-0.36	1.18	0.929	0.856	0.939	0.939	0.947	0.947
15	0.949	242.0	8.49	-0.36	1.48	0.976	0.956	0.979	0.979	0.987	0.987
16	0.948	241.5	8.49	-0.36	1.98	C.976	0.973	0.980	0.980	0.989	0.989

RUN	TST	P	TN	CCNF	MACH	RN/L	PT	C	P	TT	ALPHA
194	571	1	66	5	0.952	1.474	684	242.3	382	69.5	20.00
SFC	MACH	G		X/DR	Y/DR	Z/DR	NF/N	MA/N	QF/Q	0.979	PF/P
2	0.952	242.3	8.49	-0.45	-2.03	C.975	0.970	0.970	0.979	0.032	1.020
3	0.955	243.4	8.49	-0.45	-1.52	C.973	0.966	0.977	0.977	0.031	1.020
4	0.955	243.4	8.49	-C.45	-1.02	C.970	C.954	0.974	0.974	0.022	1.014
5	0.956	243.5	8.49	-0.45	-0.69	0.928	0.869	0.869	0.939	0.012	1.008
6	0.956	243.9	8.49	-0.45	-0.52	0.916	0.843	0.843	0.927	0.007	1.004
7	0.956	243.9	8.49	-0.45	-0.35	C.909	C.827	0.922	0.922	0.001	1.000
8	0.955	243.4	8.49	-0.45	-0.19	C.916	0.836	0.836	0.928	-0.006	0.996
9	0.955	243.4	8.49	-0.45	-0.02	C.894	0.797	0.797	0.909	-0.007	0.996
10	0.954	242.9	8.49	-C.45	0.14	C.890	0.784	0.784	0.905	-0.017	0.989
11	0.954	242.9	8.49	-0.45	0.31	C.884	0.772	0.772	0.900	-0.021	0.987
12	0.954	242.9	8.49	-0.45	0.48	C.856	0.723	0.723	0.874	-0.022	0.986
13	0.954	242.9	8.49	-C.45	0.65	C.858	0.729	0.729	0.876	-0.017	0.989
14	0.954	242.9	8.49	-C.45	0.98	C.903	C.811	0.916	0.916	-0.008	0.995
15	0.952	242.3	8.49	-0.45	1.18	C.952	0.903	0.903	0.960	-0.011	0.993
16	0.953	242.5	8.49	-C.45	1.48	C.976	0.954	0.954	0.979	0.004	1.002
17	0.954	243.4	8.49	-0.45	1.98	C.976	0.978	0.978	0.980	0.041	1.026

RUN	TST	P	TN	CCNF	MACH	RN/L	PT	C	P	TT	ALPHA
195	571	1	66	5	0.902	1.486	692	232.0	409	63.7	20.00
SEQ	MACH	G		X/DR	Y/DR	Z/DR	NF/N	MA/N	QF/Q	0.860	PF/P
2	0.902	233.0	1C.88	-C.03	-2.05	C.918	0.860	0.860	0.928	0.037	1.021
3	0.903	232.9	1C.88	-C.03	-1.54	C.924	0.869	0.869	0.933	0.032	1.018
4	0.902	232.4	1C.88	-0.03	-1.04	C.917	0.854	0.854	0.927	0.028	1.016
5	C.901	231.9	1C.88	-C.02	-0.71	C.892	0.808	0.808	0.905	0.030	1.017
6	0.901	231.9	10.88	-0.02	-0.55	C.889	0.803	0.803	0.902	0.029	1.016
7	C.901	231.9	1C.87	-C.03	-0.38	C.872	C.778	C.778	0.888	0.034	1.019
8	0.901	231.9	1C.88	-C.03	-0.21	C.869	0.763	0.763	0.884	0.020	1.011
9	0.901	231.9	1C.87	-0.03	-0.04	0.869	0.763	0.763	0.884	0.020	1.011
10	0.900	231.5	1C.87	-C.03	0.13	C.862	0.751	0.751	0.878	0.019	1.011
11	0.900	231.5	1C.87	-0.03	0.29	C.866	0.758	0.758	0.881	0.021	1.012
12	0.900	231.5	1C.87	-0.03	0.46	C.864	0.755	0.755	0.879	0.021	1.012
13	0.900	231.5	10.87	-C.03	0.63	C.859	0.747	0.747	0.875	0.023	1.013
14	0.900	231.5	1C.87	-C.03	0.97	C.882	0.786	0.786	0.896	0.020	1.011
15	C.900	231.5	1C.87	-C.03	1.17	C.908	0.835	0.835	0.919	0.023	1.013
16	C.900	231.5	1C.87	-C.03	1.46	C.927	0.880	0.880	0.937	0.042	1.024
17	0.898	231.1	1C.87	-C.03	1.96	C.959	0.949	0.949	0.965	0.054	1.031

RUN	TST	P	VN	CCNF	MACH	RN/L	PT	C	P	TT	ALPHA
				5	C.9CC	1.474	691	231.5	4C9	65.3	20.00
SEC	SFC	MACH	G	X/FR	Y/DR	Z/DR	MF/N	MA/M	QF/Q	QA/Q	VF/V
196	571	1	66	1	231.5	8.49	-0.01	-2.03	0.886	0.818	0.900
	1	0.900	232.3	8.49	-0.01	-0.69	0.910	0.830	0.921	0.842	0.912
	2	0.893	229.9	8.49	-0.01	-1.53	0.900	0.880	0.783	0.894	0.869
	3	0.895	230.9	8.49	-0.01	-1.02	0.925	0.867	0.935	0.842	0.913
	4	0.902	232.3	8.49	-0.01	-0.69	0.910	0.830	0.921	0.842	0.912
	5	0.902	231.9	8.49	-0.01	-0.53	0.880	0.835	0.783	0.894	0.869
	6	0.902	231.9	8.49	-0.01	-0.36	0.869	0.760	0.884	0.884	0.935
	7	0.902	231.9	8.49	-0.01	-0.19	0.852	0.729	0.869	0.869	0.921
	8	0.902	231.9	8.49	-0.01	-0.02	0.835	0.702	0.853	0.853	0.912
	9	0.902	231.9	8.49	-0.01	0.15	0.845	0.717	0.863	0.863	0.913
	10	0.901	233.1	8.49	-0.01	0.31	0.815	0.668	0.835	0.835	0.913
	11	0.901	233.1	8.49	-0.01	0.47	0.819	0.672	0.838	0.838	0.913
	12	0.899	232.7	8.49	-0.01	0.64	0.839	0.707	0.857	0.857	0.913
	13	0.899	232.7	8.49	-0.01	0.98	0.895	0.809	0.907	0.907	0.913
	14	0.898	232.7	8.49	-0.01	1.18	0.922	0.875	0.941	0.941	0.913
	15	0.898	232.3	8.49	-0.01	1.47	0.961	0.940	0.966	0.966	0.913
	16	0.900	233.2	8.49	-0.01	1.98	0.969	0.961	0.973	0.973	0.913

RUN	TST	P	VN	CCNF	MACH	RN/L	PT	C	P	TT	ALPHA
				5	0.850	1.500	724	228.3	451	67.2	20.00
SFC	MACH	G	X/DR	Y/DR	Z/DR	MF/N	MA/M	QF/Q	QA/Q	VF/V	VA/V
197	571	1	66	1	228.3	1C.87	-C.C2	-2.04	0.851	0.816	0.903
	1	0.850	227.9	1C.87	-C.03	-1.54	0.907	0.844	0.918	0.844	0.918
	2	0.849	227.6	1C.87	-C.02	-1.04	0.909	0.840	0.919	0.840	0.918
	3	0.847	227.6	1C.87	-C.02	-0.71	0.898	0.817	0.909	0.817	0.912
	4	0.845	226.8	1C.87	-C.03	-0.54	0.894	0.807	0.906	0.807	0.912
	5	0.845	226.8	1C.87	-C.03	-0.38	0.891	0.797	0.903	0.806	0.912
	6	0.847	227.6	1C.87	-C.03	-0.28	0.891	0.797	0.903	0.806	0.912
	7	0.848	228.0	1C.87	-C.03	-0.21	0.886	0.781	0.898	0.898	0.912
	8	0.852	229.1	1C.87	-C.03	-0.14	0.884	0.775	0.896	0.896	0.912
	9	0.854	229.4	1C.87	-C.03	0.13	0.876	0.763	0.889	0.889	0.912
	10	0.853	228.9	1C.87	-C.03	0.29	0.864	0.747	0.878	0.878	0.912
	11	0.852	228.5	1C.87	-C.03	0.46	0.871	0.765	0.884	0.884	0.912
	12	0.852	229.1	1C.87	-C.03	0.63	0.869	0.759	0.883	0.883	0.912
	13	0.852	229.1	1C.87	-C.03	0.96	0.906	0.827	0.917	0.917	0.912
	14	0.852	228.6	1C.87	-C.03	1.17	0.929	0.871	0.937	0.937	0.912
	15	0.852	228.6	1C.87	-C.03	1.47	0.967	0.948	0.971	0.971	0.912
	16	0.851	228.2	1C.87	-C.03	1.97	0.975	0.961	0.978	0.978	0.912

RUN	TST	P	TN	CCNF	VACH	PN/L	PT	G	D	TT	ALPHA	20.00
SFC	MACH	3	5	0.849	1.497	724	227.9	452	67.9		CP	DF/P
198	571.1	66	3	X/DB	Y/DR	Z/DR	MF/N	QF/Q	QA/Q	VF/V	VA/V	0.015
	SFC	MACH	3	8.49	-0.01	-2.02	0.910	0.835	0.920		0.014	1.007
1	0.849	227.9	8.49	-0.01	-1.53	0.925	0.861	0.933			0.011	1.005
2	0.852	228.6	8.49	-0.01	-1.53	0.925	0.867	0.937			0.016	1.008
3	0.854	229.2	8.49	-0.01	-1.52	0.929	0.795	0.900			0.017	1.009
4	0.853	228.9	8.49	-0.01	-0.69	0.888	0.772	0.888			0.017	1.008
5	0.852	228.5	8.49	-0.01	-0.52	0.875	0.751	0.877			0.015	1.008
6	0.853	229.0	8.49	-0.01	-0.36	0.863	0.725	0.865			0.008	1.004
7	0.852	229.1	8.49	-0.01	-0.19	0.850	0.712	0.858			0.005	1.003
8	0.852	229.1	9.49	-0.01	-0.01	0.842	0.680	0.841			0.006	1.003
9	0.852	229.1	8.49	-0.01	0.14	0.823	0.681	0.861			-0.001	0.999
10	0.851	228.7	8.49	-0.01	0.31	0.815	0.714	0.858			-0.002	0.999
11	0.853	229.5	8.49	-0.01	0.48	0.842	0.709	0.855			-0.003	0.998
12	0.853	229.5	8.49	-0.01	0.65	0.859	0.737	0.874			0.008	1.004
13	0.854	229.4	8.49	-0.01	0.97	0.910	0.831	0.920			0.008	1.004
14	0.853	229.0	8.49	-0.01	1.17	0.953	0.911	0.958			0.022	1.011
15	0.853	229.0	8.49	-0.01	1.47	0.976	0.962	0.979			0.035	1.018
16	0.854	229.4	8.49	-0.01	1.98	0.975	0.968	0.979				

RUN	TST	P	TN	CCNF	VACH	PN/L	PT	G	D	TT	ALPHA	20.00	
SFC	MACH	3	5	X/DB	Y/DR	Z/DR	MF/N	QF/Q	QA/Q	VF/V	VA/V	CP	DF/P
199	571.1	66	3	1C.87	0.41	-2.04	0.991	0.986	0.992		0.011	1.005	
	SFC	MACH	3	8C4	222.6	1C.87	C.41	-1.54	0.983	0.977	0.985	0.022	1.010
1	0.799	222.6	1C.87	0.41	-1.54	0.983	0.955	0.977			0.016	1.007	
2	0.804	224.6	1C.87	0.41	-1.04	0.974	0.942	0.888			0.004	1.002	
3	0.803	224.1	1C.87	0.41	-0.70	0.942	0.923	0.874			0.010	1.004	
4	0.802	223.5	1C.87	0.41	-0.04	0.914	0.857	0.930			0.018	1.008	
5	0.801	223.0	1C.87	0.41	-0.53	0.923	0.850	0.929			0.006	1.003	
6	0.804	224.0	1C.87	0.41	-0.37	0.922	0.821	0.948			0.004	1.002	
7	0.804	224.0	1C.87	0.41	-0.20	0.921	0.801	0.904			0.008	1.004	
8	0.804	224.0	1C.87	0.41	-0.04	0.914	0.837	0.913			0.016	1.007	
9	0.804	224.0	1C.87	0.41	0.13	0.903	0.822	0.914			0.007	1.003	
10	0.804	224.0	1C.87	0.41	0.29	0.904	0.821	0.904			0.015	1.007	
11	0.802	223.5	1C.87	0.41	0.46	0.894	0.801	0.904			0.020	1.009	
12	0.802	223.5	1C.87	0.41	0.63	0.903	0.818	0.912			0.011	1.005	
13	0.801	223.0	1C.87	0.41	0.96	0.932	0.872	0.939			0.012	1.012	
14	0.801	223.0	1C.87	0.41	1.16	0.956	0.920	0.961			0.027	1.012	
15	0.801	223.0	1C.87	0.41	1.46	0.976	0.962	0.979					
16	0.801	223.0	1C.87	0.41	1.97	0.982	0.968	0.984					

RUN	TST	P	TN	CNF	MACH	RNL	PT	G	P	TT	ALPHA
SEC	MACH	C	X/DR	Y/DB	Z/DB	MF/N	MA/M	QF/Q	QA/Q	VF/V	VA/V
200	571	1	66	5	0.758	1.520	758	222.1	498	68.6	20.00
1	0.798	222.1	1C.87	-C.03	-2.04	C.9C2	0.824	0.912	0.026	1.012	PF/P
2	0.799	222.6	1C.87	-0.03	-1.54	C.916	0.846	0.925	0.017	1.008	
3	0.801	223.1	1C.87	-C.03	-1.C4	C.923	0.855	0.931	0.008	1.004	
4	0.801	223.1	1C.87	-C.03	-0.71	C.906	0.823	0.916	0.005	1.002	
5	0.802	223.5	1C.87	-0.03	-0.54	C.898	0.807	0.908	0.004	1.002	
6	0.802	223.5	1C.87	-C.03	-0.38	C.887	0.787	0.898	-0.001	0.999	
7	0.803	223.5	1C.87	-0.03	-0.21	C.882	0.778	0.894	-0.004	0.998	
8	0.803	223.5	1C.87	-0.03	-0.03	C.870	0.757	0.882	0.001	1.000	
9	0.802	223.0	1C.87	-C.03	0.13	C.887	0.786	0.898	-0.003	0.999	
10	0.802	223.0	1C.87	-C.03	0.30	C.884	0.780	0.895	-0.006	0.997	
11	0.804	224.0	1C.87	-C.03	0.46	C.871	0.756	0.883	-0.005	0.998	
12	0.805	224.5	1C.87	-0.03	0.63	C.870	0.762	0.883	0.011	1.005	
13	0.804	224.0	1C.87	-0.03	0.96	C.902	0.821	0.911	0.022	1.010	
14	0.804	224.0	1C.87	-C.03	1.16	C.944	0.898	0.950	0.016	1.007	
15	0.803	224.1	1C.87	-0.03	1.46	0.969	0.947	0.972	0.020	1.009	
16	0.803	224.1	1C.87	-C.03	1.96	C.984	0.978	0.986	0.023	1.011	

RUN	TST	P	TN	CNF	MACH	RNL	PT	G	P	TT	ALPHA
SFG	MACH	C	X/DR	Y/DB	Z/DB	MF/N	MA/M	QF/Q	QA/Q	VF/V	VA/V
201	571	1	66	5	0.8C1	1.520	757	223.0	496	69.1	20.00
1	0.8C1	223.0	1C.87	-C.38	-2.04	C.981	0.973	0.984	0.023	1.010	PF/P
2	0.801	223.0	1C.87	-C.38	-1.54	C.983	0.975	0.985	0.019	1.009	
3	0.800	222.5	1C.87	-C.38	-1.04	C.963	0.935	0.967	0.018	1.008	
4	0.800	222.5	1C.87	-C.38	-0.70	C.926	0.861	0.934	0.009	1.004	
5	0.802	223.0	1C.87	-C.38	-0.54	C.901	0.815	0.911	0.009	1.004	
6	0.802	223.0	1C.87	-C.38	-0.37	C.894	0.800	0.905	0.001	1.000	
7	0.802	223.0	1C.87	-C.38	-0.20	C.900	0.810	0.910	0.001	1.000	
8	0.803	223.5	1C.87	-C.38	-0.04	C.877	0.774	0.889	0.012	1.005	
9	0.804	224.0	1C.87	-C.38	0.13	0.869	0.759	0.881	0.013	1.006	
10	0.804	224.0	1C.87	-C.38	0.30	C.876	0.771	0.888	0.009	1.004	
11	0.802	223.5	1C.87	-C.38	0.46	C.881	0.777	0.892	0.006	1.003	
12	0.802	223.5	1C.87	-C.38	0.62	0.887	0.791	0.898	0.011	1.005	
13	0.801	223.0	1C.87	-C.38	0.97	C.929	0.868	0.937	0.010	1.005	
14	0.801	223.0	1C.87	-C.38	1.17	C.942	0.893	0.948	0.016	1.007	
15	0.800	222.5	1C.87	-C.38	1.47	C.973	0.955	0.976	0.020	1.009	
16	0.801	223.0	1C.87	-C.38	1.96	C.982	0.977	0.984	0.028	1.013	

RUN	TST	P	TN	CCNF	MACH	RNL	PT	G	P	TT	ALPHA
SEG					X/DB	Y/DB	Z/DB	MF/M	WA/M	QF/N	VA/V
202	571	1	66	5	0.8C1	1.520	758	223.1	497	69.3	20.00
	0-801	223.1	IC.87	-C.48	-2.04	0.979	0.972	0.981	0.983	0.974	0.981
	0-800	222.5	IC.87	-C.48	-1.54	C.981	0.975	0.975	0.975	0.974	0.975
	0-800	222.5	IC.87	-0.48	-1.04	C.972	0.950	0.950	0.950	0.950	0.950
	0-802	223.5	IC.87	-0.48	-0.70	C.924	0.856	0.856	0.856	0.856	0.856
	0-802	223.5	IC.87	-C.48	-0.53	C.9C8	0.824	0.824	0.824	0.824	0.824
	0-803	223.5	IC.87	-0.48	-0.37	C.9C2	0.818	0.818	0.818	0.818	0.818
	0-803	223.5	IC.87	-C.48	-0.21	C.9C5	0.823	0.823	0.823	0.823	0.823
	0-800	222.5	IC.87	-0.48	-0.04	C.877	0.774	0.774	0.774	0.774	0.774
	0-801	223.1	IC.87	-C.48	0.13	C.880	0.777	0.777	0.777	0.777	0.777
	0-801	223.1	IC.88	-C.48	0.25	C.875	0.778	0.778	0.778	0.778	0.778
	0-802	223.6	IC.87	-0.48	0.46	C.878	0.777	0.777	0.777	0.777	0.777
	0-799	222.6	IC.87	-C.48	0.64	C.894	0.802	0.802	0.802	0.802	0.802
	0-798	222.0	IC.87	-0.48	0.96	C.929	0.866	0.866	0.866	0.866	0.866
	0-798	222.0	IC.87	-C.48	1.16	C.963	0.933	0.933	0.933	0.933	0.933
	0-800	222.5	IC.87	-C.48	1.47	C.983	0.970	0.970	0.970	0.970	0.970
	0-801	223.0	IC.87	-0.48	1.97	C.987	0.981	0.981	0.981	0.981	0.981

RUN	TST	P	TN	CCNF	MACH	RNL	PT	G	P	TT	ALPHA
SEG					X/DB	Y/DB	Z/DB	MF/M	WA/M	QF/N	VA/V
203	571	1	66	5	0.798	1.515	757	222.0	498	69.6	20.00
	0-798	222.0	IC.49	-2.03	C.980	0.975	0.983	0.983	0.983	0.975	0.983
	0-798	222.1	IC.49	-1.53	C.982	0.977	0.985	0.985	0.985	0.977	0.985
	0-798	222.1	IC.49	-1.04	C.981	0.969	0.983	0.983	0.983	0.969	0.983
	0-798	222.1	IC.49	-0.65	C.921	0.870	0.938	0.938	0.938	0.870	0.938
	0-798	222.1	IC.49	-0.53	C.920	0.853	0.928	0.928	0.928	0.853	0.928
	0-798	222.1	IC.49	-0.36	C.930	0.866	0.937	0.937	0.937	0.866	0.937
	0-798	222.1	IC.49	-0.15	C.920	0.847	0.928	0.928	0.928	0.847	0.928
	0-798	222.1	IC.49	-0.02	C.906	0.822	0.915	0.915	0.915	0.822	0.915
	0-798	222.1	IC.49	0.14	C.9C6	0.816	0.915	0.915	0.915	0.816	0.915
	0-799	222.6	IC.49	0.31	C.879	0.769	0.890	0.890	0.890	0.769	0.890
	0-799	222.6	IC.49	0.43	C.920	0.928	0.908	0.908	0.908	0.928	0.908
	0-800	222.5	IC.49	0.43	C.907	0.821	0.916	0.916	0.916	0.821	0.916
	0-800	222.5	IC.49	0.43	C.949	0.900	0.954	0.954	0.954	0.900	0.954
	0-799	222.0	IC.49	0.43	C.971	0.950	0.975	0.975	0.975	0.950	0.975
	0-799	222.0	IC.49	0.43	C.988	0.981	0.989	0.989	0.989	0.981	0.989
	0-799	222.0	IC.49	0.43	C.978	0.971	0.971	0.971	0.971	0.971	0.971

RUN	TST	P	TRN	CCNF	MACH	RN/L	PT	C	P	ALPHA		
										20.00	20.00	20.00
204	571	1	66	5	C.802	1.521	759	223.	6	497	69.6	0.022
					X/CR	Y/DR	Z/DR	WF/N	WA/N	0.812	0.907	1.010
SFC	MACH	Q			8.49	-0.C1	-2.03	C.897	0.823	0.912	0.025	1.C11
1	0.802	223.	6		8.49	-0.01	-1.53	C.902	0.858	0.930	0.019	1.C09
2	0.802	223.	6		8.49	-C.01	-1.02	C.922	0.809	0.908	0.007	1.003
3	0.799	222.	6		8.49	-0.01	-0.69	C.898	0.782	0.896	-0.001	1.000
4	0.799	222.	6		8.49	-0.C1	-0.52	C.884	0.746	0.876	0.004	1.002
5	0.799	222.	6		8.49	-C.01	-0.36	C.863	0.746	0.877	-0.006	0.997
6	0.799	222.	6		8.49	-C.01	-0.20	C.865	0.735	0.872	-0.006	0.997
7	0.798	222.	C		8.49	-0.C1	-0.02	C.859	0.709	0.856	-0.001	1.000
8	0.798	222.	C		8.49	-C.02	0.02	C.859	0.703	0.853	-0.003	0.999
9	0.800	222.	5		8.49	-0.C1	0.31	C.839	0.713	0.859	-0.006	0.997
10	0.800	222.	5		8.49	-C.01	0.47	C.845	0.760	0.885	-0.006	0.997
11	0.800	222.	5		8.49	-0.01	0.64	C.873	0.760	0.853	0.006	1.003
12	0.800	222.	5		8.49	-C.01	0.98	C.922	0.925	0.962	0.020	1.009
13	0.8C1	223.	0		8.49	-C.01	1.18	C.958	0.964	0.979	0.025	1.C11
14	0.8C1	223.	0		8.49	-C.01	1.48	C.976	0.977	0.984	0.028	1.013
15	0.799	222.	C		8.49	-C.01	1.98	C.982				
16	0.800	222.	C		8.49	-C.01	1.98	C.982				

RUN	TST	P	TRN	CCNF	MACH	RN/L	PT	C	P	ALPHA		
										20.00	20.00	20.00
205	571	1	66	5	0.8C1	1.517	757	223.	0	496	69.9	0.028
SFC	MACH	Q			X/CR	Y/DR	Z/DR	WF/N	WA/N	0.976	0.984	1.013
1	0.801	223.	0		8.49	-0.36	-2.02	C.982	0.973	0.982	0.031	1.C14
2	0.8C1	223.	0		8.49	-C.36	-1.52	C.980	0.951	0.975	0.015	1.007
3	0.801	223.	0		8.49	-C.36	-1.03	C.972	0.869	0.938	0.007	1.C03
4	0.8C1	223.	C		8.49	-0.36	-0.69	C.931	0.795	0.901	0.008	1.003
5	0.8C1	223.	0		8.49	-C.36	-0.53	C.890	0.778	0.893	0.003	1.001
6	0.801	223.	C		8.49	-0.36	-0.36	C.881	0.750	0.879	0.001	1.009
7	0.8C1	223.	C		8.49	-C.36	-0.19	C.866	0.728	0.866	0.004	1.002
8	0.801	223.	0		8.49	-C.36	-0.C2	C.852	0.734	0.871	-0.006	0.997
9	0.8C0	222.	5		8.49	-0.36	0.14	C.858	0.742	0.875	-0.005	0.998
10	0.800	222.	5		8.49	-C.36	0.31	C.862	0.740	0.873	0.002	1.001
11	0.800	222.	5		8.49	-C.36	0.48	C.860	0.790	0.898	0.007	1.003
12	0.798	222.	0		8.49	-C.36	0.64	C.887	0.869	0.939	0.002	1.001
13	0.799	222.	0		8.49	-C.36	0.98	C.932	0.957	0.979	0.007	1.C02
14	0.799	222.	C		8.49	-C.36	1.18	C.977	0.977	0.986	0.019	1.009
15	0.799	222.	C		8.49	-C.36	1.48	C.984	0.984	0.989	0.020	1.C09

RUN	TST	P	TN	CCNF	MACH	RN/L	PT	G	P	TT			ALPHA				
										X/DB	Y/DB	Z/DR	WF/N	MA/W	CF/Q	QA/Q	VF/V
206	571	1	66	5	C.800	1.515	757	222.5	496	69.8	20.00						
SFC	MACH	G		X/DB	Y/DB	Z/DR	WF/N	MA/W	CF/Q								
1	0.800	222.	5	E.49	-C.45	-2.03	0.981	0.975	0.983	0.029	1.013						
2	0.800	222.	5	E.49	-C.45	-2.C3	C.979	0.974	0.982	0.034	1.015						
3	0.801	223.	1	E.49	-0.45	-1.53	C.980	C.974	0.982	0.031	1.014						
4	0.801	223.	1	E.49	-C.45	-1.C3	C.972	0.952	0.975	0.018	1.008						
5	0.799	222.	6	E.49	-C.45	-0.68	0.921	C.852	0.929	0.011	1.005						
6	0.800	222.	5	E.49	-0.45	-0.52	0.899	0.812	0.909	0.009	1.004						
7	0.800	222.	5	E.49	-C.45	-0.36	0.879	0.776	0.891	0.007	1.003						
8	0.799	222.	0	E.49	-C.45	-0.19	0.886	C.787	0.897	0.004	1.002						
9	0.798	221.	5	E.49	-C.45	-0.03	0.883	0.779	0.894	-0.002	0.999						
10	0.798	221.	5	E.49	-C.45	0.14	0.854	0.726	0.867	-0.007	0.997						
11	0.798	221.	5	E.49	-C.45	0.31	C.859	0.736	0.872	-0.004	0.998						
12	0.799	222.	0	E.49	-C.45	0.48	0.874	0.763	0.886	-0.005	0.998						
13	0.799	222.	0	E.49	-C.45	0.64	0.899	C.808	0.909	0.001	1.001						
14	0.800	222.	5	E.49	-C.45	0.98	C.956	0.911	0.960	-0.006	0.997						
15	0.800	222.	5	E.49	-C.45	1.18	C.976	C.955	0.978	0.006	1.003						
16	0.800	222.	5	E.49	-C.45	1.48	0.986	0.979	0.987	0.017	1.008						
17	C.8C1	223.	1	E.49	-C.45	1.98	C.985	C.986	C.980	0.024	1.011						

RUN	TST	P	TN	CCNF	MACH	RN/L	PT	G	P	TT			ALPHA				
										X/DB	Y/DB	Z/DB	WF/N	MA/W	CF/Q	QA/Q	VF/V
207	571	1	66	5	C.600	1.510	896	177.2	702	68.7	20.00						
SFC	MACH	G		X/DB	Y/DB	Z/DR	WF/N	MA/W	CF/Q								
1	0.600	177.	2	1C.87	C.41	-2.C5	C.973	0.957	0.975	0.044	1.011						
2	0.600	177.	2	1C.87	C.41	-1.54	C.992	C.987	0.993	0.011	1.003						
3	0.600	177.	2	1C.87	C.41	-1.05	C.961	0.932	0.964	0.034	1.009						
4	0.600	177.	2	1C.87	C.41	-0.71	C.932	C.972	0.936	0.014	1.003						
5	0.599	176.	4	1C.88	C.41	-0.54	C.926	C.861	0.931	0.015	1.004						
6	0.600	177.	2	1C.87	C.41	-0.38	C.926	C.865	0.933	0.008	1.002						
7	0.600	177.	2	1C.87	C.41	-0.20	C.929	C.864	0.934	-0.001	1.000						
8	0.600	177.	2	1C.87	C.41	-0.04	C.921	C.849	0.926	0.004	1.001						
9	0.600	177.	2	1C.87	C.41	0.12	C.914	C.836	0.920	0.000	1.000						
10	C.600	177.	2	1C.88	C.41	0.29	C.915	C.839	0.920	0.008	1.002						
11	C.600	177.	2	1C.88	C.41	0.47	C.905	0.821	0.911	0.011	1.003						
12	C.600	177.	2	1C.88	C.41	0.63	C.923	C.854	0.923	0.010	1.002						
13	C.600	177.	2	1C.87	C.41	0.96	C.939	C.885	0.942	0.017	1.004						
14	C.600	177.	2	1C.87	C.41	1.17	C.967	C.937	0.969	0.004	1.001						
15	C.600	177.	2	1C.87	C.41	1.47	C.975	C.953	0.976	0.015	1.004						
16	C.600	177.	2	1C.88	C.41	1.97	C.982	C.971	0.983	0.027	1.007						

RUN	TST	P	TA	CCNF	MACH	RN/L	PT	C	P	TT	ALPHA	
SEQ	MACH	G	X/DB	Y/DR	Z/DB	MF/N	WA/W	QF/Q	VAF/V	VAF/V	CP	PF/P
208	571	1	66	5	0.602	1.513	896	177.8	701	68.4	20.00	
1	0.602	177.8	1C.87	-C.03	-2.04	C.970	0.851	0.925	0.019	1.005		
2	0.602	177.8	1C.87	-C.03	-1.55	C.929	0.866	0.933	0.016	1.004		
3	0.602	177.8	1C.88	-C.03	-1.04	C.925	0.859	0.929	0.019	1.005		
4	0.602	177.8	1C.87	-0.03	-0.71	0.914	0.835	0.919	0.001	1.000		
5	0.602	177.8	1C.87	-C.C2	-0.54	C.857	0.804	0.903	-0.000	1.000		
6	0.603	178.4	1C.87	-0.03	-0.38	0.888	0.792	0.895	0.012	1.003		
7	0.602	177.8	1C.87	-0.03	-0.21	0.885	0.785	0.892	0.004	1.001		
8	0.602	177.8	1C.87	-C.03	-0.02	0.883	0.780	0.890	0.003	1.001		
9	0.602	177.8	1C.87	-C.03	0.13	0.871	0.762	0.878	0.018	1.005		
10	0.602	177.8	1C.87	-C.03	0.30	0.854	0.798	0.900	-0.002	0.999		
11	0.602	177.8	1C.87	-0.03	0.46	C.885	0.786	0.891	0.016	1.004		
12	0.602	177.8	1C.87	-C.03	0.63	C.895	0.802	0.901	0.008	1.002		
13	0.602	177.8	1C.87	-C.03	0.96	C.929	0.865	0.933	0.008	1.002		
14	0.602	177.8	1C.87	-C.03	1.16	0.954	0.912	0.957	0.007	1.002		
15	0.600	177.2	1C.87	-C.03	1.46	C.969	0.941	0.971	0.011	1.003		
16	0.602	177.8	1C.87	-0.03	1.97	C.982	0.971	0.984	0.022	1.006		

RUN	TST	P	TA	CCNF	MACH	RN/L	PT	C	P	TT	ALPHA	
SEQ	MACH	G	X/DB	Y/DR	Z/DB	MF/N	WA/W	QF/Q	VAF/V	VAF/V	CP	PF/P
209	571	1	66	5	0.600	1.511	296	177.2	702	68.3	20.00	
1	0.600	177.2	1C.87	-0.38	-2.04	0.981	0.968	0.982	0.028	1.007		
2	0.600	177.2	1C.87	-C.38	-1.54	C.984	0.971	0.985	0.015	1.004		
3	0.599	176.4	1C.87	-0.38	-1.04	0.968	0.938	0.970	0.007	1.002		
4	0.601	177.2	1C.87	-0.38	-0.71	C.924	0.858	0.929	0.016	1.004		
5	0.602	177.8	1C.87	-C.38	-0.54	0.899	0.811	0.905	0.011	1.003		
6	0.602	177.8	1C.87	-C.38	-0.37	0.894	0.801	0.900	0.007	1.002		
7	0.602	177.8	1C.87	-C.38	-0.21	C.911	0.831	0.916	0.004	1.001		
8	0.602	177.8	1C.87	-0.38	-0.04	0.892	0.796	0.898	0.003	1.001		
9	0.602	177.8	1C.87	-C.38	0.13	0.889	0.792	0.895	0.012	1.003		
10	0.602	177.8	1C.88	-C.38	0.30	C.889	0.791	0.895	0.006	1.001		
11	0.600	177.2	1C.87	-C.38	0.47	C.900	0.812	0.906	0.004	1.001		
12	0.600	177.2	1C.87	-C.38	0.63	C.902	0.817	0.908	0.017	1.004		
13	0.602	177.8	1C.87	-C.38	0.96	C.927	0.863	0.931	0.019	1.005		
14	0.602	177.8	1C.87	-C.38	1.17	C.938	0.884	0.942	0.016	1.004		
15	0.600	177.2	1C.87	-C.38	1.47	C.964	0.934	0.967	0.019	1.005		
16	0.600	176.4	1C.87	-C.38	1.96	C.985	0.976	0.986	0.020	1.005		

RUN	TST	P	TA	CCNF	MACH	RNL	PT	G	P	TT	ALPHA
	210	571	1	66	5	C.599	1.5C8	895	176.6	702	68.2
SFC	MACH	G	X/DB	Y/DR	Z/DB	MF/N	WA/M	QF/Q	VA/V	CP	PF/P
1	0.599	176.6	1C.87	-C.48	-2.04	C.983	0.972	0.984	0.024	1.006	
2	0.599	176.6	1C.88	-C.48	-1.53	C.986	0.978	0.987	0.019	1.005	
3	0.600	177.2	1C.87	-0.48	-1.05	0.962	0.930	0.965	0.019	1.005	
4	0.600	177.2	1C.87	-C.48	-0.71	C.916	0.846	0.921	0.031	1.008	
5	0.602	177.8	1C.87	-0.48	-0.54	C.908	0.827	0.914	0.013	1.003	
6	C.600	177.2	1C.87	-C.48	-0.37	C.9C2	0.816	0.909	0.004	1.001	
7	0.600	177.2	1C.87	-C.48	-0.21	C.894	0.801	0.900	0.011	1.003	
8	0.600	177.2	1C.87	-0.48	-0.04	C.9CC	0.811	0.906	0.003	1.001	
9	0.600	177.2	1C.87	-C.48	0.12	C.898	0.807	0.904	0.003	1.001	
10	C.600	177.2	1C.87	-0.48	0.29	C.898	0.807	0.904	0.003	1.001	
11	0.600	177.2	1C.87	-C.48	0.47	C.895	0.803	0.901	0.010	1.002	
12	0.600	177.2	1C.87	-0.48	0.63	C.916	0.840	0.921	0.003	1.001	
13	C.599	176.6	1C.87	-C.48	0.96	C.942	0.887	0.945	0.000	1.000	
14	0.599	176.6	1C.87	-C.48	1.17	C.97C	0.943	0.972	0.011	1.003	
15	0.600	177.2	1C.87	-0.48	1.47	C.974	0.954	0.976	0.023	1.006	
16	0.600	177.2	1C.87	-C.48	1.96	C.985	0.976	0.986	0.024	1.006	

RUN	TST	P	TA	CCNF	MACH	RNL	PT	G	P	TT	ALPHA
	211	571	1	66	5	0.6C1	1.503	882	174.5	691	64.1
SFC	MACH	G	X/DB	Y/DB	Z/DB	MF/N	WA/M	QF/Q	VA/V	CP	PF/P
1	0.601	174.5	8.48	0.43	-2.03	C.952	0.988	0.993	0.010	1.002	
2	0.601	174.5	8.49	0.43	-1.53	C.989	0.983	0.990	0.015	1.004	
3	0.600	173.9	8.48	0.43	-1.03	C.968	0.945	0.970	0.031	1.008	
4	0.601	174.5	8.48	0.43	-0.70	C.924	0.858	0.928	0.020	1.005	
5	0.599	173.9	8.48	0.43	-0.52	C.926	0.862	0.931	0.019	1.005	
6	0.599	174.0	8.48	0.43	-0.36	C.926	0.859	0.931	0.004	1.001	
7	0.598	173.4	8.48	0.43	-0.19	C.918	0.843	0.923	-0.001	1.000	
8	0.600	174.6	8.48	0.43	-0.02	C.910	0.825	0.916	-0.017	0.996	
9	0.601	174.6	8.48	0.43	0.14	C.893	0.796	0.899	-0.009	0.998	
10	0.602	175.1	8.48	0.43	0.31	C.9C1	0.812	0.907	-0.002	0.999	
11	0.602	175.1	8.48	0.43	0.48	C.892	0.798	0.898	0.012	1.003	
12	0.601	174.5	8.48	0.43	0.48	C.915	0.839	0.920	0.008	1.002	
13	C.600	173.9	8.48	0.43	0.64	C.915	0.907	0.955	0.004	1.001	
14	0.600	173.9	8.48	0.43	0.97	C.952	0.929	0.964	0.016	1.004	
15	0.599	173.9	8.48	0.43	1.17	C.962	0.965	0.981	0.024	1.006	
16	0.599	173.9	8.49	0.43	1.48	C.979	0.974	0.985	0.020	1.005	
17	0.599	173.9	8.49	0.43	1.98	C.984					

RUN	TST	P	TN	CCNF	MACH	RNL	PT	C	P	TT	ALPHA
SFC	MACH	G		X/DR	Y/DR	Z/DR	MF/N	MA/M	QF/Q	QA/Q	VF/V
212	571	1	66	5	0.599	1.5C4	886	174.6	695	64.9	20.00
1	0.	599	174.6	E.49	-0.01	-2.02	0.907	0.828	0.912	0.029	1.007
2	0.	598	174.6	E.49	-0.C1	-1.53	0.928	0.862	0.932	0.006	1.001
3	0.	598	174.6	E.49	-0.01	-1.03	0.923	0.873	0.938	0.006	1.002
4	0.	599	174.6	E.49	-0.C1	-0.69	0.891	0.797	0.897	0.016	1.004
5	0.	598	174.6	E.49	-0.C1	-0.53	0.874	0.766	0.881	0.012	1.003
6	0.	598	174.6	E.49	-0.C1	-0.36	0.863	0.744	0.870	0.001	1.000
7	0.	602	175.8	E.49	-0.C1	-0.19	0.858	0.735	0.865	-0.002	0.999
8	0.	600	175.2	E.49	-0.C1	-0.02	0.859	0.738	0.866	0.002	1.000
9	0.	600	175.2	E.48	-0.C1	0.14	0.861	0.741	0.869	-0.001	1.000
10	0.	600	175.2	E.48	-0.C1	0.31	0.865	0.749	0.873	0.001	1.000
11	C.	600	175.2	E.48	-0.01	0.48	0.863	0.746	0.871	0.004	1.001
12	C.	600	175.2	E.49	-0.C1	0.64	0.883	0.779	0.889	0.002	1.000
13	C.	600	175.2	E.49	-0.01	0.98	0.934	0.872	0.938	0.003	1.001
14	0.	599	174.6	E.48	-0.C1	1.18	0.958	0.920	0.961	0.009	1.002
15	0.	600	175.2	E.49	-0.C1	1.48	0.982	0.969	0.983	0.019	1.005
16	C.	600	175.2	E.49	-0.01	1.98	0.988	0.980	0.989	0.015	1.004

RUN	TST	P	TN	CCNF	MACH	RNL	PT	C	P	TT	ALPHA
SFC	MACH	G		X/DR	Y/DR	Z/DR	MF/N	MA/M	QF/Q	QA/Q	VF/V
212	571	1	66	5	0.6C2	1.5C5	887	175.8	694	66.1	20.00
1	0.	6C2	175.8	E.49	-0.36	-2.03	0.986	0.978	0.987	0.022	1.006
2	0.	602	175.8	E.49	-0.36	-1.52	0.980	0.957	0.981	0.023	1.007
3	0.	600	175.2	E.48	-0.36	-1.03	0.972	0.948	0.974	0.012	1.003
4	0.	600	175.2	E.49	-0.36	-0.70	0.930	0.864	0.934	-0.002	0.999
5	0.	599	174.6	E.48	-0.36	-0.52	0.889	0.792	0.896	0.005	1.001
6	0.	599	174.6	E.49	-0.C6	-0.36	0.879	0.772	0.886	-0.002	0.999
7	0.	599	174.6	E.49	-0.36	-0.19	0.868	0.753	0.875	-0.002	0.999
8	0.	600	175.2	E.49	-0.36	-0.02	0.856	0.735	0.864	0.007	1.002
9	0.	601	175.8	E.49	-0.C6	0.15	0.853	0.728	0.861	0.006	1.001
10	0.	599	174.6	E.49	-0.36	0.31	0.873	0.762	0.880	0.001	1.000
11	0.	599	174.6	E.49	-0.C6	0.48	0.875	0.767	0.882	0.004	1.001
12	0.	599	174.6	E.48	-0.C6	0.65	0.903	0.815	0.908	0.001	1.000
13	0.	599	174.6	E.49	-0.C6	0.98	0.961	0.923	0.964	-0.003	0.999
14	0.	599	174.6	E.48	-0.36	1.18	0.976	0.953	0.977	0.006	1.002
15	0.	599	174.6	E.48	-0.36	1.49	0.981	0.967	0.983	0.017	1.004
16	0.	598	174.6	E.48	-0.C6	1.98	0.992	0.987	0.993	0.012	1.003

RUN	TST	P	TN	CCNF	NACH	PN/L	PT	C	P	TT	ALPHA
	214	571	1	66	5	0.600	1.503	887	175.2	695	66.2
SEQ	MACH	G		X/DB	Y/DB	Z/DB	MF/N	WA/N	GF/Q	VF/V	20.00
1	0.600	175.2	E.49	-C.45	-2.03	C.987	0.979	0.983	0.019	1.005	
2	0.599	174.6	E.49	-0.45	-1.52	C.986	0.978	0.987	0.019	1.005	
3	0.600	175.2	E.49	-C.45	-1.03	C.976	0.955	0.977	0.011	1.003	
4	0.602	175.8	E.49	-0.45	-0.69	C.921	0.851	0.926	0.007	1.002	
5	0.601	175.2	E.49	-0.45	-0.53	C.896	0.804	0.902	0.001	1.000	
6	0.602	175.8	E.49	-C.45	-0.36	C.880	0.778	0.887	0.016	1.004	
7	0.600	175.2	E.49	-0.45	-0.19	C.893	0.798	0.899	0.002	1.000	
8	0.602	175.8	E.49	-C.45	-0.02	C.872	0.762	0.879	0.010	1.002	
9	0.600	175.2	E.49	-0.45	0.14	C.882	0.779	0.888	0.006	1.001	
10	0.600	175.2	E.49	-C.45	0.31	C.879	0.773	0.886	0.002	1.000	
11	0.600	175.2	E.49	-C.45	C.48	C.881	0.777	0.888	0.007	1.002	
12	0.599	174.6	E.48	-0.45	0.64	C.904	0.817	0.910	-0.002	0.999	
13	0.599	174.6	E.48	-C.45	0.98	C.945	0.893	0.948	0.003	1.001	
14	0.599	174.6	E.49	-C.45	1.18	C.98C	0.959	0.981	-0.002	1.000	
15	0.599	174.6	E.49	-0.45	1.48	C.986	0.977	0.987	0.019	1.005	
16	0.600	175.2	E.49	-0.45	1.98	C.979	0.965	0.980	0.032	1.008	

RUN	TST	P	TN	CCNF	NACH	PN/L	PT	C	P	TT	ALPHA
	215	571	1	66	5	0.250	1.523	1892	79.5	1811	65.1
SEQ	MACH	Q		X/DB	Y/DB	Z/DB	MF/N	WA/N	GF/Q	VF/V	20.00
1	0.250	79.5	1C.87	0.41	-2.04	C.997	0.000	0.993	0.000	0.997	0.000
2	0.250	79.5	1C.87	C.41	-1.54	C.951	0.000	0.981	0.000	0.991	0.010
3	0.249	78.8	1C.87	C.41	-1.05	C.979	0.000	0.958	0.000	0.979	0.019
4	0.249	78.8	1C.87	C.41	-0.70	C.949	0.000	0.900	0.000	0.950	0.019
5	0.249	78.8	1C.87	C.41	-0.54	C.945	0.000	0.900	0.000	0.950	0.019
6	0.250	79.5	1C.88	C.41	-0.37	C.94C	0.000	0.882	0.000	0.940	0.019
7	0.250	79.5	1C.87	C.41	-0.21	C.929	0.000	0.881	0.000	0.939	0.019
8	0.250	79.5	1C.87	C.41	-C.C4	C.931	0.000	0.867	0.000	0.932	0.019
9	0.250	79.5	1C.87	O.41	0.12	C.938	0.000	0.879	0.000	0.939	0.021
10	0.250	78.8	1C.87	C.41	C.25	C.922	0.000	0.867	0.000	0.932	0.021
11	0.251	79.5	10.87	O.41	O.47	C.914	0.000	0.836	0.000	0.915	0.012
12	0.251	79.5	1C.87	C.41	O.63	C.944	0.000	0.891	0.000	0.945	0.021
13	0.249	78.1	1C.87	C.41	C.96	C.961	0.000	0.922	0.000	0.961	0.028
14	0.250	78.8	1C.87	C.41	1.16	O.970	0.000	0.941	0.000	0.971	0.019
15	0.251	79.5	1C.87	C.41	1.46	C.987	0.000	0.974	0.000	0.987	0.010
16	0.251	79.5	1C.87	O.41	1.97	C.995	0.000	0.989	0.000	0.995	0.010

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RUN	TST	P	TN	CCNF	MACH	RN/L	PT	G	P	TT	ALPHA
SFC	MACH	Q	X/DB	Y/DB	Z/DB	MF/N	MA/M	QF/Q	QA/Q	VF/V	VA/V
216	571	1	66	5	C.250	1.515	1.884	78.8	1804	64.5	20.00
1	0.250	78.8	1C.87	-0.03	-2.04	0.945	0.000	0.893	0.000	0.946	0.000
2	0.250	78.8	1C.87	-C.03	-1.54	C.950	0.000	0.902	0.000	0.951	0.000
3	0.250	78.8	1C.88	-0.03	-1.04	C.949	0.000	0.900	0.000	0.950	0.000
4	0.250	78.8	1C.88	-C.C3	-0.71	C.912	0.000	0.832	0.000	0.913	0.000
5	0.250	78.8	1C.87	-0.03	-0.54	C.902	0.000	0.815	C.000	0.904	0.000
6	0.250	78.8	1C.87	-0.03	-0.37	C.914	0.000	0.834	0.000	0.915	0.000
7	0.250	78.8	1C.87	-C.C2	-0.20	C.9C4	0.000	0.817	C.000	0.905	0.000
8	0.250	78.8	1C.87	-0.03	-2.04	C.896	0.000	0.803	C.000	0.897	0.000
9	0.250	78.8	1C.87	-C.C2	0.13	C.902	0.000	0.813	C.000	0.903	0.000
10	0.251	79.5	1C.87	-0.03	0.29	C.9C2	0.000	0.813	C.000	0.903	0.000
11	0.251	79.5	1C.87	-C.C2	0.47	C.887	0.000	0.785	C.000	0.888	0.000
12	0.251	79.5	1C.88	-0.03	0.63	C.895	0.000	0.801	C.000	0.896	0.000
13	0.251	79.5	1C.88	-C.C3	0.96	C.943	0.000	0.889	C.000	0.944	0.000
14	0.251	79.5	1C.88	-C.C2	1.16	C.959	0.000	0.919	C.000	0.959	0.000
15	0.250	78.8	1C.88	-C.C2	1.46	C.992	0.000	0.982	C.000	0.992	0.000
16	0.251	79.5	1C.87	-C.C3	1.97	C.991	0.000	0.983	C.000	0.992	0.000

RUN	TST	P	TN	CCNF	MACH	RN/L	PT	G	P	TT	ALPHA
SFC	MACH	Q	X/DB	Y/DB	Z/DB	MF/N	MA/M	QF/Q	QA/Q	VF/V	VA/V
217	571	1	66	5	C.250	1.516	1.884	78.8	1804	64.2	20.00
1	0.250	78.8	1C.87	-C.28	-2.04	1.001	0.000	1.001	0.001	0.000	-0.019 0.999
2	0.250	78.8	1C.87	-0.38	-1.53	C.992	0.000	0.984	0.000	0.992	0.000
3	0.251	79.5	1C.88	-C.28	-1.04	C.978	0.000	0.955	0.000	0.978	0.000
4	0.251	79.5	1C.87	-C.38	-0.71	C.935	0.000	0.874	C.000	0.936	0.000
5	0.251	79.5	1C.88	-C.38	-0.54	C.909	0.000	0.825	C.000	0.910	0.000
6	0.250	78.8	1C.87	-C.28	-0.37	C.899	0.000	0.808	C.000	0.900	0.000
7	0.249	78.1	1C.88	-C.38	-0.20	C.901	0.000	0.811	C.000	0.902	0.000
8	0.251	79.5	1C.88	-C.28	-0.04	C.914	0.000	0.836	C.000	0.915	0.000
9	0.251	79.5	1C.88	-C.38	0.13	C.892	0.000	0.796	C.000	0.893	0.000
10	0.251	79.5	1C.88	-C.38	0.30	C.912	0.000	0.832	C.000	0.913	0.000
11	0.250	78.8	1C.87	-C.38	0.47	C.92C	0.000	0.846	C.000	0.921	0.000
12	0.250	78.8	1C.88	-C.38	0.63	C.916	0.000	0.838	C.000	0.917	0.000
13	0.250	78.8	1C.88	-C.38	0.96	C.95C	0.000	0.902	C.000	0.951	0.000
14	0.250	78.8	1C.88	-C.28	1.16	C.976	0.000	0.951	C.000	0.976	0.000
15	0.251	79.5	1C.88	-C.38	1.46	C.990	0.000	0.979	C.000	0.990	0.000
16	0.251	79.5	1C.88	-C.28	1.96	C.592	0.000	0.984	C.000	0.992	0.000

RUN	TST	P	TN	CCNF	MACH	RNL	PT	G	P	TT	ALPHA	
SFC	MACH	0	X/DB	Y/DB	Z/DR	MF/N	WA/W	QA/Q	VF/V	VA/V	CP	DF/P
218	571	1	66	5	0.250	1.515	1883	78.8	1803	64.2	20.00	
1	0.250	78.8	10.88	-0.48	-2.05	1.000	0.000	1.000	0.000	0.000	-0.019	0.999
2	0.251	79.5	1C.88	-C.48	-1.53	0.988	0.000	0.976	0.000	0.988	-0.019	C.999
3	0.251	79.5	10.88	-C.48	-1.C4	C.960	0.000	0.922	C.000	0.961	0.000	-0.010
4	0.251	79.5	1C.87	-0.48	-0.70	C.916	0.000	0.839	C.000	0.917	0.000	-0.019
5	0.251	79.5	1C.88	-C.48	-0.54	C.922	0.000	0.849	C.000	0.923	0.000	-0.010
6	0.250	78.8	10.88	-0.48	-0.37	C.921	0.000	0.848	C.000	0.922	0.000	-0.021
7	0.250	78.8	1C.87	-0.48	-0.21	C.906	0.000	0.820	C.000	0.907	0.000	-0.021
8	0.251	79.5	1C.87	-C.48	-0.04	C.922	0.000	0.849	C.000	0.923	0.000	-0.021
9	0.251	79.5	1C.87	-0.48	0.13	C.922	0.000	0.849	C.000	0.923	0.000	-0.012
10	0.251	79.5	1C.87	-C.48	0.30	C.918	0.000	0.842	C.000	0.919	0.000	-0.010
11	0.251	79.5	1C.88	-0.48	0.46	C.924	0.000	0.953	C.000	0.925	0.000	-0.010
12	0.251	79.5	1C.88	-C.48	0.63	C.929	0.000	0.862	C.000	0.929	0.000	-0.021
13	0.251	79.5	1C.88	-C.48	0.96	C.954	0.000	0.910	C.000	0.955	0.000	-0.019
14	0.251	79.5	1C.88	-0.48	1.16	C.960	0.000	0.920	C.000	0.960	0.000	-0.019
15	0.251	79.5	1C.88	-C.48	1.47	C.995	0.000	0.989	C.000	0.995	0.000	-0.019
16	0.251	79.5	1C.88	-0.48	1.96	C.998	0.000	0.995	C.000	0.998	0.000	-0.019

RUN	TST	P	TN	CCNF	MACH	RNL	PT	G	P	TT	ALPHA	
SFC	MACH	0	X/DB	Y/DB	Z/DR	MF/N	WA/W	QA/Q	VF/V	VA/V	CP	DF/P
219	571	1	66	5	0.251	1.523	1884	79.5	1803	63.9	20.00	
1	0.251	79.5	8.49	0.43	-2.03	C.956	0.000	0.991	0.000	0.996	0.000	-0.017
2	0.251	79.5	8.49	0.43	-1.52	C.955	0.000	0.989	0.000	0.995	0.000	-0.019
3	0.251	79.5	8.49	0.43	-1.02	C.978	0.000	0.957	C.000	0.979	0.000	-0.019
4	0.251	79.5	8.49	0.43	-0.68	C.934	0.000	0.872	C.000	0.935	0.000	-0.019
5	0.251	79.5	8.49	0.43	-0.53	C.939	0.000	0.881	C.000	0.939	0.000	-0.019
6	0.251	79.5	8.49	0.43	-0.35	C.925	0.000	0.855	C.000	0.926	0.000	-0.021
7	0.251	79.5	8.49	0.43	-0.18	C.912	0.000	0.830	C.000	0.913	0.000	-0.021
8	0.251	79.5	8.49	0.43	-0.02	C.918	0.000	0.842	C.000	0.919	0.000	-0.021
9	0.251	79.5	8.49	0.43	0.14	C.902	0.000	0.813	C.000	0.903	0.000	-0.021
10	0.252	80.1	8.49	0.43	0.31	C.9C8	0.000	0.823	C.000	0.909	0.000	-0.021
11	0.252	80.1	8.49	0.43	0.48	C.912	0.000	0.830	C.000	0.913	0.000	-0.021
12	0.251	79.5	8.49	0.43	0.64	C.935	0.000	0.874	C.000	0.936	0.000	-0.021
13	0.252	80.1	8.49	0.43	0.98	C.958	0.000	0.918	C.000	0.959	0.000	-0.021
14	0.252	80.1	8.49	0.43	1.18	C.980	0.000	0.960	C.000	0.981	0.000	-0.019
15	0.252	80.1	8.49	0.43	1.48	C.992	0.000	0.983	C.000	0.992	0.000	-0.019
16	0.252	80.1	8.49	0.43	1.98	C.993	0.000	0.984	C.000	0.993	0.000	-0.019

RUN	TST	P	TN	CCNF	MACH	RN/L	PT	C	P	TT	ALPHA
220	571	1	66	5	0.251	1.523	1884	79.5	1803	63.9	20.00
SEG	MACH	Q	X/DB	Y/DB	Z/DR	MF/N	MA/M	QF/Q	QA/Q	VF/V	VA/V
1	0.251	79.5	8.49	-0.01	-2.03	0.924	0.000	0.872	0.000	0.935	0.000
2	0.251	79.5	8.49	-c.01	-1.53	0.940	0.000	0.882	0.000	0.940	0.000
3	0.251	79.5	8.49	-0.01	-1.02	0.944	0.000	0.891	c.000	0.945	0.000
4	0.252	80.1	8.49	-0.01	-0.69	0.899	0.000	0.808	0.000	0.900	0.000
5	0.251	79.5	8.49	-0.01	-0.52	0.886	0.000	0.784	0.000	0.887	0.000
6	0.251	79.5	8.49	-0.01	-0.35	0.857	0.000	0.733	0.000	0.858	0.000
7	0.251	79.5	8.49	-c.01	-0.19	0.879	c.000	0.771	c.000	0.880	c.000
8	0.251	79.5	8.49	-0.01	-0.02	0.863	0.000	0.744	0.000	0.864	0.000
9	0.251	79.5	8.49	-c.01	0.14	0.863	0.000	0.744	0.000	0.864	0.000
10	0.251	79.5	8.49	-0.01	0.31	0.896	0.000	0.801	0.000	0.897	0.000
11	0.251	79.5	8.49	-c.01	0.47	0.890	0.000	0.791	0.000	0.891	0.000
12	0.252	80.1	8.49	-0.01	0.65	0.890	0.000	0.792	0.000	0.892	0.000
13	0.251	79.5	8.49	-0.01	0.98	0.940	0.000	0.882	0.000	0.940	0.000
14	0.251	79.5	8.49	-0.01	1.18	0.980	0.000	0.960	0.000	0.981	0.000
15	0.251	79.5	8.49	-0.01	1.48	0.996	0.000	0.991	0.000	0.996	0.000
16	0.251	79.5	8.49	-0.01	1.98	0.995	0.000	0.989	0.000	0.995	0.000

RUN	TSI	P	TN	CCNF	MACH	RN/L	PT	C	P	TT	ALPHA
221	571	1	66	5	0.251	1.524	1884	79.5	1803	63.7	20.00
SFQ	MACH	Q	X/DB	Y/DB	Z/DR	MF/N	MA/M	QF/Q	QA/Q	VF/V	VA/V
1	0.251	79.5	8.49	-c.36	-2.02	0.993	0.000	0.986	0.000	0.993	0.000
2	0.251	79.5	8.49	-0.36	-1.52	0.996	0.000	0.991	0.000	0.996	0.000
3	0.251	79.5	8.49	-0.36	-1.03	0.975	0.000	0.950	0.000	0.975	0.000
4	0.251	79.5	8.49	-0.36	-0.69	0.934	0.000	0.872	c.000	0.935	0.000
5	0.251	79.5	8.49	-0.26	-0.53	0.897	0.000	0.804	0.000	0.898	0.000
6	0.251	79.5	8.49	-0.36	-0.36	0.881	0.000	0.775	c.000	0.882	0.000
7	0.251	79.5	8.49	-0.36	-0.19	0.901	0.000	0.811	c.000	0.902	0.000
8	0.251	79.5	8.49	-0.36	-0.03	0.878	0.000	0.770	c.000	0.879	c.000
9	0.251	79.5	8.49	-0.36	0.15	0.906	0.000	0.820	c.000	0.907	c.000
10	0.251	79.5	8.49	-0.36	0.31	0.892	0.000	0.796	c.000	0.894	c.000
11	0.251	79.5	8.49	-0.36	0.48	0.870	0.000	0.756	c.000	0.871	c.000
12	0.251	79.5	8.49	-0.36	0.65	0.926	0.000	0.856	c.000	0.927	c.000
13	0.251	79.5	8.49	-0.36	0.98	0.942	0.000	0.887	c.000	0.943	c.000
14	0.251	79.5	8.49	-0.36	1.18	0.981	0.000	0.962	c.000	0.981	c.000
15	0.251	79.5	8.49	-0.36	1.48	0.995	0.000	0.989	c.000	0.995	c.000
16	0.251	79.5	8.49	-0.36	1.97	0.999	0.000	0.996	c.000	0.999	c.000

RUN	TST	P	TN	CNF	MACH	RNL	PT	C	P	TT	ALPHA
222	571	1	66	5	0.252	1.531	1.884	80.1	1802	63.7	20.00
SFC	MACH	Q	X/DB	Y/DB	Z/DB	MF/N	MA/N	QF/Q	QA/Q	VF/V	VA/V
1	0.252	80.1	8.49	-0.45	-2.03	C.991	0.000	0.981	0.000	0.991	0.000
2	0.252	80.1	8.49	-0.45	-1.52	C.991	0.000	0.981	0.000	0.991	0.000
3	0.252	80.1	8.49	-C.45	-1.C3	C.975	0.000	C.950	0.000	0.975	0.000
4	0.252	80.1	8.49	-C.45	-0.70	C.902	0.000	0.813	0.000	0.903	0.000
5	0.252	80.1	8.49	-C.45	-0.51	C.913	0.000	0.834	0.000	0.914	0.000
6	0.252	80.1	8.49	-C.45	-0.36	C.896	0.000	0.803	0.000	0.897	0.000
7	0.252	80.1	8.49	-C.45	-0.18	C.879	0.000	0.772	0.000	0.880	0.000
8	0.252	80.1	8.49	-C.45	-0.03	C.882	0.000	0.777	0.000	0.883	0.000
9	0.252	80.1	8.49	-C.45	0.14	C.903	0.000	0.815	0.000	0.904	0.000
10	0.252	80.1	8.49	-C.45	0.31	C.874	0.000	0.763	0.000	0.875	0.000
11	0.252	80.1	8.49	-C.45	0.48	C.911	0.000	0.830	0.000	0.912	0.000
12	0.252	80.1	8.49	-C.45	0.64	C.929	0.000	0.882	0.000	0.940	0.000
13	0.252	80.1	8.49	-C.45	0.98	C.956	0.000	0.914	0.000	0.957	0.000
14	0.252	80.1	8.49	-C.45	1.18	C.978	0.000	0.955	0.000	0.978	0.000
15	0.252	80.1	8.49	-C.45	1.47	C.988	0.000	0.976	0.000	0.988	0.000
16	0.252	80.1	8.49	-C.45	1.98	C.991	0.000	0.981	0.000	0.991	0.000

RUN	TST	P	TN	CNF	MACH	RNL	PT	C	P	TT	ALPHA
223	571	1	66	5	0.954	1.480	681	241.7	380	66.3	-20.00
SFC	MACH	Q	X/DB	Y/DB	Z/DB	MF/N	MA/N	QF/Q	QA/Q	VF/V	VA/V
2	0.954	241.7	C.87	C.41	-2.04	0.971	0.966	0.975	0.966	0.975	0.040
3	0.957	242.8	C.88	C.41	-1.54	C.967	0.959	0.972	0.959	0.972	0.039
4	0.957	242.8	C.88	C.41	-1.04	C.954	0.927	0.961	0.927	0.961	0.030
5	0.957	242.8	C.88	C.41	-0.70	C.904	0.824	0.917	0.824	0.917	0.012
6	0.957	242.8	C.88	C.41	-0.53	C.888	0.794	0.903	0.794	0.903	0.010
7	0.957	242.8	C.88	C.41	-0.37	C.878	0.775	0.894	0.775	0.894	0.007
8	0.957	242.8	C.88	C.41	-0.20	C.866	0.753	0.883	0.753	0.883	0.007
9	0.957	242.8	C.88	C.41	-0.C4	C.874	0.768	0.890	0.768	0.890	0.008
10	0.957	242.8	C.88	C.41	0.12	C.872	0.764	0.888	0.764	0.888	0.008
11	0.957	242.8	C.88	C.41	0.29	C.871	0.763	0.887	0.763	0.887	0.010
12	0.957	242.8	C.87	C.41	0.46	C.885	0.790	0.900	0.790	0.900	0.014
13	0.954	241.7	C.87	C.41	0.62	C.905	0.827	0.918	0.827	0.918	0.016
14	0.954	241.7	C.87	C.41	0.97	C.945	0.912	0.953	0.912	0.953	0.032
15	0.955	242.3	C.87	C.41	0.97	C.963	0.942	0.969	0.942	0.969	0.024
16	0.957	242.8	C.87	C.41	1.17	C.966	0.957	0.971	0.957	0.971	0.039
17	0.957	242.8	C.87	C.41	1.47	C.968	0.966	0.972	0.966	0.972	0.050
18	0.956	242.3	C.87	C.41	1.96	C.963	0.964	0.969	0.964	0.969	0.060

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RUN	TST	P	TN	CCNF	MACH	PN/L	PT	G	P	TT	ALPHA
SEQ	MACH	0	5	0.956	1.482	684	241.4	380	68.0	-20.00	
224	571	1	66	X/DR	Y/DR	Z/DR	NF/N	WA/W	QF/Q	QA/Q	VF/V
1	0.956	243.4	1C.87	-C.03	-2.04	C.888	C.922	C.813	0.903	0.871	0.047 PF/P
2	0.955	243.4	1C.87	-C.03	-1.55	C.888	C.922	C.913	0.933	0.846	0.036 1.C30
3	0.955	243.4	1C.87	-C.03	-0.54	C.888	C.922	C.771	0.925	0.771	0.023 1.023
4	0.953	242.9	1C.87	-C.03	-0.03	C.888	C.922	C.891	0.891	0.891	0.023 1.014
5	0.953	242.9	1C.87	-C.03	-1.04	C.913	C.922	C.711	0.860	0.860	0.012 1.008
6	0.953	242.9	1C.87	-C.03	-0.71	C.874	C.922	C.704	0.848	0.848	0.008 1.C05
7	0.951	242.9	1C.87	-C.03	-0.54	C.888	C.922	C.666	0.838	0.838	0.011 1.007
8	0.951	242.4	1C.87	-C.03	-0.38	C.888	C.922	C.661	0.834	0.834	0.002 1.C01
9	0.951	242.4	1C.87	-C.03	-0.20	C.888	C.922	C.687	0.848	0.848	0.004 1.003
10	0.951	242.4	1C.87	-C.03	-0.03	C.888	C.922	C.704	0.856	0.856	0.005 1.003
11	0.950	241.9	1C.87	-C.03	0.13	C.888	C.922	C.742	0.876	0.876	0.011 1.007
12	0.949	241.4	1C.87	-C.03	0.30	C.888	C.922	C.798	0.897	0.897	0.013 1.008
13	0.949	241.4	1C.87	-C.03	0.46	C.888	C.922	C.873	0.935	0.935	0.019 1.012
14	0.949	241.4	1C.87	-C.03	0.63	C.888	C.922	C.922	0.956	0.956	0.034 1.021
15	0.947	241.0	1C.87	-C.03	0.97	C.925	C.925	C.947	0.965	0.965	0.040 1.025
16	0.947	241.0	1C.87	-C.03	1.17	C.948	C.948	C.947	0.972	0.972	0.053 1.030

RUN	TST	P	TN	CCNF	MACH	PN/L	PT	G	P	TT	ALPHA
SEQ	MACH	0	5	0.950	1.475	684	241.8	383	68.8	-20.00	
225	571	1	66	X/DR	Y/DR	Z/DR	NF/N	WA/W	QF/Q	QA/Q	VF/V
1	0.950	241.8	1C.87	-0.38	-2.04	C.964	C.970	0.949	0.969	0.957	0.034 3F/P
2	0.951	242.4	1C.87	-C.38	-1.54	C.956	C.962	0.974	0.974	0.921	0.027 1.C17
3	0.950	241.8	1C.87	-C.38	-1.04	C.956	C.962	0.788	0.902	0.913	0.028
4	0.950	241.8	1C.87	-C.38	-0.70	C.887	C.904	0.731	0.873	0.873	0.001 1.C01
5	0.952	242.3	1C.87	-C.38	-0.54	C.887	C.904	0.698	0.856	0.856	-0.000 1.000
6	0.952	242.3	1C.87	-C.38	-0.37	C.855	C.855	0.704	0.858	0.858	-0.000 1.000
7	0.952	242.3	1C.87	-C.38	-0.19	C.836	C.836	0.731	0.865	0.865	0.001 1.001
8	0.950	241.8	1C.87	-C.38	-0.04	C.839	C.839	0.698	0.869	0.869	0.004 1.002
9	0.949	243.0	1C.87	-C.38	-0.04	C.845	C.845	0.704	0.872	0.872	0.014 1.009
10	0.948	242.7	1C.87	-C.38	0.13	C.850	C.850	0.717	0.891	0.891	0.015 1.C10
11	0.949	243.1	1C.87	-C.38	0.30	C.853	C.853	0.729	0.908	0.908	0.018 1.C11
12	0.949	243.1	1C.87	-C.38	0.46	C.874	C.874	0.735	0.949	0.949	0.022 1.014
13	0.947	242.7	1C.87	-C.38	0.63	C.894	C.894	0.773	0.967	0.967	0.031 1.020
14	0.947	242.7	1C.87	-C.38	0.96	C.941	C.941	0.811	0.976	0.976	0.039 1.024
15	0.949	243.1	1C.87	-C.38	1.18	C.961	C.961	0.903	0.949	0.949	0.044 1.028
16	0.948	242.7	1C.87	-C.38	1.47	C.972	C.972	0.971	0.968	0.968	C.050 1.C32

RUN	TST	P	TN	CCNF	MACH	RN/L	PT	C	P	TT	ALPHA
SEQ	MACH	G	X/DR	Y/DR	Z/DR	NF/N	MA/M	QF/Q	QA/Q	VF/V	VA/V
226	571	1	6.6	5	0.953	1.482	688	244.	C	384	-20.00
1	0.953	244.	C	1C.	87	-C.48	-2.04	0.	968	0.959	0.972
2	0.953	244.	C	1C.	87	-C.48	-1.55	C.	968	0.959	0.972
3	0.952	243.	5	1C.	87	-C.48	-1.04	0.	953	0.919	0.959
4	0.952	243.	5	1C.	88	-C.48	-0.71	C.	890	0.798	0.904
5	0.952	243.	5	1C.	87	-C.48	-0.54	C.	860	0.745	0.878
6	0.950	243.	C	1C.	87	-C.48	-0.37	C.	860	0.742	0.878
7	0.950	243.	C	1C.	87	-C.48	-0.20	C.	841	0.709	0.860
8	0.950	243.	C	1C.	87	-C.48	-0.04	C.	855	0.734	0.873
9	0.951	243.	5	1C.	88	-C.48	0.13	C.	859	0.739	0.877
10	0.951	243.	5	1C.	88	-C.48	0.29	C.	871	0.759	0.887
11	0.951	243.	5	1C.	88	-C.48	0.46	C.	895	0.806	0.909
12	0.951	243.	5	1C.	87	-C.48	0.64	C.	907	0.832	0.919
13	0.948	242.	6	1C.	88	-C.48	0.97	C.	942	0.907	0.950
14	0.947	242.	2	1C.	87	-C.48	1.16	C.	956	0.936	0.962
15	0.947	242.	2	1C.	87	-C.48	1.47	C.	961	0.952	0.967
16	0.945	241.	8	1C.	87	-C.48	1.97	C.	965	0.962	0.970

RUN	TST	P	TN	CCNF	MACH	RN/L	PT	C	P	TT	ALPHA
SEQ	MACH	G	X/DR	Y/DR	Z/DR	NF/N	MA/M	QF/Q	QA/Q	VF/V	VA/V
227	571	1	6.6	5	0.952	1.477	688	243.	C	384	-20.00
1	0.952	243.	5	8.49	0.43	-2.03	C.	972	C.	966	0.976
2	0.953	244.	0	8.49	0.43	-1.53	C.	971	0.963	0.976	0.976
3	0.952	243.	5	8.49	0.43	-1.03	C.	966	0.948	0.971	0.971
4	0.951	243.	5	8.49	0.43	-0.69	C.	910	0.832	0.923	0.923
5	0.951	243.	5	8.49	0.43	-0.52	C.	902	0.812	0.915	0.915
6	0.952	244.	0	8.49	0.43	-0.36	C.	898	0.801	0.912	0.912
7	0.952	244.	0	8.49	0.43	-0.19	C.	868	0.748	0.885	0.885
8	0.952	244.	0	8.49	0.43	-0.03	C.	856	0.728	0.874	0.874
9	0.951	243.	5	8.49	0.43	0.14	C.	850	0.716	0.868	0.868
10	0.951	243.	5	8.49	0.42	0.31	C.	869	0.750	0.886	0.886
11	0.951	243.	5	8.49	0.43	0.49	C.	881	0.773	0.896	0.896
12	0.949	243.	0	8.49	0.43	0.65	C.	911	0.831	0.923	0.923
13	0.947	242.	2	8.49	0.42	0.98	C.	955	0.925	0.961	0.961
14	0.947	242.	2	8.49	0.42	1.18	C.	965	0.950	0.970	0.970
15	0.947	242.	2	8.49	0.43	1.48	C.	964	0.955	0.969	0.969
16	0.946	242.	3	8.49	0.43	1.98	C.	973	0.973	0.977	0.977

RUN	TST	P	TN	CCNF	MACH	RN/L	PT	C	P	TT	ALPHA
SEQ	MACH	G	X/DB	Y/DB	Z/DB	NF/N	MA/M	QF/Q	QA/Q	VF/V	V A/V
228	571	1	66	5	0.950	1.475	688	243.0	385	70.7	-20.00
			8.49	-0.01	-2.02	0.898	0.817	0.912	0.912	0.019	1.012
1	0.950	243.0	8.49	-0.01	-1.52	0.929	0.871	0.939	0.939	0.015	1.010
2	0.952	243.5	8.49	-0.01	-1.02	0.929	0.862	0.939	0.939	-0.001	0.999
3	0.952	243.5	8.49	-0.01	-1.02	0.929	0.784	0.902	0.902	-0.008	0.995
4	0.954	244.0	8.49	-0.01	-0.69	0.888	0.720	0.871	0.871	-0.015	0.991
5	0.954	244.0	8.49	-0.01	-0.53	0.852	0.639	0.826	0.826	-0.016	0.990
6	0.952	243.5	8.49	-0.01	-0.36	0.803	0.639	0.826	0.826	-0.017	0.989
7	0.952	243.5	8.49	-0.01	-0.19	0.782	0.606	0.807	0.807	-0.002	0.989
8	0.952	243.5	8.49	-0.01	-0.01	0.783	0.606	0.807	0.807	-0.018	0.989
9	0.953	244.0	8.49	-0.01	0.14	0.794	0.625	0.818	0.818	-0.013	0.992
10	0.950	243.0	8.49	-0.01	0.31	0.818	0.665	0.840	0.840	-0.010	0.994
11	0.950	243.0	8.49	-0.01	0.48	0.839	0.703	0.859	0.859	-0.002	0.999
12	0.951	243.5	8.49	-0.01	0.64	0.871	0.763	0.887	0.887	0.010	1.006
13	0.949	243.0	8.49	-0.01	0.98	0.946	0.909	0.954	0.954	0.026	1.016
14	0.949	243.0	8.49	-0.01	1.18	0.964	0.952	0.969	0.969	0.038	1.024
15	0.948	242.7	8.49	-0.01	1.48	0.960	0.951	0.966	0.966	0.049	1.031
16	0.946	242.3	8.49	-0.01	1.98	0.970	0.974	0.974	0.974	0.049	1.031

RUN	TST	F	TN	CCNF	MACH	RN/L	PT	C	P	TT	ALPHA
SEQ	MACH	G	X/DB	Y/DB	Z/DB	NF/N	MA/M	QF/Q	QA/Q	VF/V	V A/V
229	571	1	66	5	0.953	1.484	691	245.1	385	71.1	-20.00
			8.49	-0.36	-2.03	0.964	0.947	0.969	0.969	0.031	1.020
1	0.953	245.1	8.49	-0.36	-1.53	0.971	0.961	0.975	0.975	0.030	1.019
2	0.953	245.1	8.49	-0.36	-1.03	0.968	0.944	0.972	0.972	0.013	1.008
3	0.953	245.1	8.49	-0.36	-0.69	0.906	0.818	0.918	0.918	-0.004	0.998
4	0.954	245.7	8.49	-0.36	-0.52	0.847	0.713	0.866	0.866	-0.010	0.994
5	0.954	245.7	8.49	-0.36	-0.36	0.817	0.662	0.839	0.839	-0.012	0.992
6	0.954	245.7	8.49	-0.36	-0.18	0.813	0.655	0.835	0.835	-0.016	0.990
7	0.954	245.7	8.49	-0.36	-0.01	0.814	0.657	0.836	0.836	-0.013	0.992
8	0.951	244.6	8.49	-0.36	0.15	0.811	0.655	0.833	0.833	-0.008	0.995
9	0.951	244.6	8.49	-0.36	0.31	0.822	0.692	0.853	0.853	-0.004	0.997
10	0.951	244.6	8.49	-0.36	0.48	0.866	0.749	0.883	0.883	-0.001	0.999
11	0.951	244.6	8.49	-0.36	0.65	0.903	0.818	0.916	0.916	0.004	1.002
12	0.951	244.6	8.49	-0.36	0.98	0.951	0.921	0.958	0.958	0.028	1.018
13	0.951	244.6	8.49	-0.36	1.18	0.969	0.959	0.973	0.973	0.036	1.022
14	0.951	244.6	8.49	-0.36	1.48	0.966	0.959	0.971	0.971	0.044	1.028
15	0.949	244.2	8.49	-0.36	1.98	0.969	0.966	0.971	0.971	0.048	1.C30
16	0.949	244.2	8.49	-0.36	2.48	0.970	0.974	0.974	0.974	0.049	1.C30

RUN	TST	P	TN	CCNF	MACH	RN/L	PT	C	P	TT	ALPHA
										-20.00	
230	571	1	66	5	C.950	1.480	691	244.1	387	71.5	
SEC	MACH	G	X/CR	Y/DB	Z/DP	WF/N	WA/M	QF/Q	QA/Q	VF/V	CP
1	0.950	244.1	8.49	-C.45	-2.03	C.974	0.967	0.978	0.030	1.019	
2	0.952	245.1	8.49	-C.45	-1.51	C.972	C.964	0.976	0.031	1.019	
3	0.952	245.1	8.49	-C.45	-1.03	C.969	0.948	0.974	0.016	1.010	
4	0.952	245.1	8.49	-C.45	-0.65	C.910	C.828	0.923	-0.002	0.999	
5	0.952	245.1	8.49	-C.45	-0.53	C.873	0.759	0.889	-0.006	0.996	
6	0.952	245.1	8.49	-C.45	-0.36	0.841	0.701	0.860	-0.014	0.991	
7	0.952	245.1	8.49	-C.45	-0.19	C.832	C.687	0.853	-0.016	0.990	
8	0.952	245.1	8.49	-C.45	-0.02	0.838	0.696	0.858	-0.014	0.991	
9	0.952	245.1	8.49	-C.45	0.14	0.846	0.707	0.865	-0.021	0.986	
10	0.952	245.1	8.49	-C.45	0.31	C.860	0.733	0.878	-0.013	0.992	
11	0.952	245.1	8.49	-C.45	0.48	0.876	0.766	0.892	-0.004	0.997	
12	0.952	245.1	8.49	-C.45	0.65	C.915	0.837	0.926	0.001	1.000	
13	0.952	245.1	8.49	-C.45	0.98	C.960	0.934	0.966	0.021	1.013	
14	0.950	244.1	8.49	-C.45	1.18	C.968	0.957	0.973	0.032	1.020	
15	0.950	244.1	8.49	-C.45	1.49	C.966	0.959	0.971	0.044	1.028	
16	0.951	244.6	8.49	-C.45	1.98	0.969	0.969	0.974	0.049	1.031	

RUN	TST	P	TN	CCNF	MACH	RN/L	PT	C	P	TT	ALPHA
										-20.00	
231	571	1	66	5	C.902	1.483	706	237.0	417	71.6	
SEC	MACH	O	X/CR	Y/DP	Z/DP	WF/N	WA/M	QF/Q	QA/Q	VF/V	CP
1	0.902	237.0	10.87	-C.03	-2.04	C.915	0.866	0.926	0.059	1.034	
2	0.901	237.1	1C.87	-0.03	-1.55	C.923	0.873	0.932	0.046	1.026	
3	0.899	236.7	1C.87	-C.03	-1.C4	C.911	0.842	0.922	0.027	1.C15	
4	0.899	236.2	10.87	-C.02	-0.71	C.862	C.756	0.879	0.026	1.015	
5	0.897	235.8	1C.87	-C.03	-0.55	C.854	0.737	0.871	0.017	1.010	
6	0.899	236.7	1C.87	-C.03	-0.37	0.838	0.701	0.856	-0.001	0.999	
7	0.901	237.1	1C.87	-C.03	-0.21	0.828	0.684	0.846	-0.002	0.999	
8	0.902	237.5	1C.87	-C.03	-0.C4	C.842	0.706	0.860	-0.006	0.996	
9	0.903	237.5	1C.87	-C.03	0.13	C.847	0.718	0.864	0.002	1.001	
10	0.902	237.0	1C.87	-C.03	0.30	C.852	0.730	0.869	0.009	1.005	
11	0.901	236.5	1C.87	-C.03	0.47	C.869	0.767	0.884	0.030	1.017	
12	0.900	236.1	1C.87	-C.03	0.64	C.881	0.795	0.895	0.042	1.024	
13	0.899	236.1	1C.87	-C.03	0.95	C.927	0.879	0.937	0.039	1.022	
14	0.900	236.6	1C.87	-C.03	1.16	C.952	0.925	0.959	0.034	1.019	
15	0.900	236.6	1C.87	-C.03	1.45	C.962	0.950	0.967	0.046	1.026	
16	0.899	236.2	1C.87	-C.03	1.96	C.965	0.970	0.970	0.050	1.028	

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RUN	TST	P	PTN	CCNF	MACH	RNL	PT	G	P	TT	ALPHA	V	CP	PF/P
SFC	MACH	Q	X/DB	Y/DB	Z/DB	WF/N	MA/M	QF/Q	QA/Q	VF/V	VA/V	V	CP	PF/P
232	571 1	66	5	0.904	1.484	705	237.4	415	71.4	-20.00			0.035	1.020
	MACH	Q	X/DB	Y/DB	Z/DB	WF/N	MA/M	QF/Q	QA/Q	VF/V	VA/V	V	CP	PF/P
1	0.904	237.4	8.49	-0.01	-2.03	0.920	0.863	0.930				0.038	1.022	
2	0.904	237.4	8.49	-0.01	-1.53	0.923	0.870	0.932				0.012	1.007	
3	0.904	237.4	8.49	-0.01	-1.02	0.927	0.865	0.936				0.015	1.009	
4	0.904	237.4	8.49	-0.01	-0.69	0.882	0.784	0.896				0.011	1.006	
5	0.902	237.4	8.49	-0.01	-0.53	0.845	0.719	0.863				0.011	1.006	
6	0.901	236.6	8.49	-0.01	-0.26	0.803	0.649	0.824				0.011	1.006	
7	0.901	236.6	8.49	-0.01	-0.19	0.796	0.638	0.817				0.011	1.006	
8	0.900	236.6	8.49	-0.01	-0.01	0.802	0.644	0.823				0.003	1.002	
9	0.899	236.1	8.49	-0.01	0.16	0.801	0.647	0.822				0.015	1.008	
10	0.899	236.2	8.49	-0.01	0.33	0.832	0.698	0.851				0.012	1.007	
11	0.898	235.7	8.49	-0.01	0.48	0.841	0.715	0.859				0.019	1.011	
12	0.896	235.3	8.49	-0.01	0.64	0.876	0.777	0.891				0.021	1.012	
13	0.899	236.2	8.49	-0.01	0.98	0.943	0.903	0.950				0.027	1.015	
14	0.899	236.2	8.49	-0.01	1.18	0.965	0.948	0.970				0.033	1.019	
15	0.896	235.3	8.49	-0.01	1.48	0.969	0.962	0.973				0.042	1.024	
16	0.896	235.3	8.49	-0.01	1.99	0.968	0.961	0.973				0.044	1.025	

RUN	TST	P	PTN	CCNF	MACH	RNL	PT	G	P	TT	ALPHA	V	CP	PF/P
SFC	MACH	C	X/DB	Y/DB	Z/DB	WF/N	MA/M	QF/Q	QA/Q	VF/V	VA/V	V	CP	PF/P
233	571 1	66	5	0.851	1.452	726	225.3	452	71.1	-20.00			0.030	1.015
	MACH	C	X/DB	Y/DB	Z/DB	WF/N	MA/M	QF/Q	QA/Q	VF/V	VA/V	V	CP	PF/P
1	0.851	229.3	1C.87	-0.03	-2.04	0.914	0.848	0.923				0.030	1.015	
2	0.851	229.3	1C.87	-0.03	-1.54	0.923	0.864	0.931				0.019	1.010	
3	0.852	229.8	1C.87	-0.03	-1.04	0.908	0.832	0.918				0.014	1.007	
4	0.852	229.8	1C.87	-0.03	-0.71	0.883	0.785	0.896				0.016	1.008	
5	0.852	229.8	1C.87	-0.03	-0.55	0.857	0.738	0.872				0.019	1.005	
6	0.852	229.8	1C.87	-0.03	-0.37	0.850	0.728	0.866				0.014	1.007	
7	0.850	229.4	1C.87	-0.03	-0.20	0.844	0.719	0.860				0.016	1.008	
8	0.850	229.4	1C.87	-0.03	-0.04	0.853	0.731	0.868				0.010	1.005	
9	0.849	229.1	1C.87	-0.03	0.13	0.865	0.753	0.879				0.013	1.007	
10	0.850	229.5	1C.87	-0.03	0.29	0.866	0.756	0.880				0.014	1.007	
11	0.851	229.9	1C.87	-0.03	0.46	0.882	0.781	0.895				0.009	1.004	
12	0.853	230.2	1C.87	-0.03	0.63	0.897	0.809	0.908				0.011	1.006	
13	0.853	230.2	1C.87	-0.03	0.97	0.939	0.891	0.946				0.022	1.011	
14	0.853	230.1	1C.87	-0.03	1.16	0.965	0.944	0.969				0.025	1.013	
15	0.854	230.5	1C.87	-0.03	1.46	0.977	0.967	0.980				0.028	1.014	
16	0.854	230.5	1C.87	-0.03	1.96	0.972	0.964	0.976				0.039	1.020	

RUN	TST	P	TN	CCNF	MACH	RNL	PT	C	D	TT	ALPHA
SEQ	MACH	G	X/DR	Y/DB	Z/DB	MF/N	MA/M	QF/Q	QA/Q	VF/V	VA/V
234	571	1	66	5	0.854	1.497	728	230.6	452	71.0	-20.00
1	0.854	230.6	8.49	-0.01	-2.03	0.922	0.853	0.931	0.941	0.874	0.005 1.003
2	0.857	231.2	8.49	-0.01	-1.53	0.933	0.834	0.907	0.917	0.834	0.005 1.003
3	0.854	230.6	8.49	-0.01	-1.03	0.907	0.760	0.867	0.881	0.760	0.028 1.015
4	0.852	229.8	8.49	-0.01	-0.69	0.867	0.715	0.843	0.859	0.715	0.021 1.011
5	0.852	229.8	8.49	-0.01	-0.53	0.843	0.678	0.821	0.839	0.678	0.013 1.007
6	0.850	229.4	8.49	-0.01	-0.36	0.821	0.669	0.817	0.835	0.669	0.011 1.005
7	0.849	229.1	8.49	-0.01	-0.19	0.817	0.681	0.825	0.842	0.681	0.002 1.001
8	0.849	229.1	8.49	-0.01	-0.02	0.825	0.736	0.842	0.858	0.736	0.002 1.001
9	0.849	229.1	8.49	-0.01	0.14	0.824	0.711	0.842	0.858	0.711	0.003 1.001
10	0.847	228.2	8.49	-0.01	0.31	0.842	0.736	0.855	0.870	0.736	0.015 1.007
11	0.847	228.2	8.49	-0.01	0.48	0.855	0.777	0.877	0.890	0.777	0.020 1.010
12	0.846	227.9	8.48	-0.01	0.64	0.877	0.711	0.890	0.905	0.711	0.025 1.012
13	0.846	227.5	8.49	-0.01	0.99	0.949	0.912	0.955	0.969	0.912	0.021 1.010
14	0.846	227.9	8.49	-0.01	1.18	0.974	0.959	0.977	0.986	0.959	0.014 1.007
15	0.850	229.5	8.49	-0.01	1.48	0.986	0.980	0.988	0.986	0.980	0.020 1.010
16	0.853	230.2	8.49	-0.01	1.95	0.984	0.978	0.986	0.984	0.978	0.029 1.013

RUN	TST	P	TN	CCNF	MACH	RNL	PT	C	D	TT	ALPHA
SEQ	MACH	G	X/DR	Y/DB	Z/DB	MF/N	MA/M	QF/Q	QA/Q	VF/V	VA/V
235	571	1	66	5	0.801	1.513	757	223.0	496	70.9	-20.00
1	0.801	223.0	1C.87	0.41	-2.04	0.975	0.967	0.978	0.980	0.970	0.039 1.018
2	0.800	222.5	1C.87	0.41	-1.54	0.977	0.953	0.969	0.972	0.953	0.035 1.016
3	0.801	223.1	1C.87	0.41	-1.05	0.969	0.947	0.967	0.972	0.947	0.022 1.010
4	0.801	223.1	1C.87	0.41	-0.70	0.921	0.929	0.933	0.929	0.929	0.011 1.005
5	0.800	222.5	1C.87	0.41	-0.53	0.910	0.834	0.919	0.919	0.834	0.015 1.007
6	0.800	222.5	1C.87	0.41	-0.37	0.906	0.818	0.912	0.912	0.818	0.012 1.005
7	0.800	222.5	1C.87	0.41	-0.20	0.906	0.825	0.915	0.915	0.825	0.013 1.006
8	0.800	222.5	1C.87	0.41	-0.04	0.899	0.811	0.908	0.908	0.811	0.009 1.004
9	0.800	222.5	1C.87	0.41	0.12	0.905	0.821	0.915	0.915	0.821	0.006 1.003
10	0.801	223.1	1C.87	0.41	0.25	0.907	0.822	0.916	0.916	0.822	-0.000 1.000
11	0.801	223.0	1C.87	0.41	0.46	0.904	0.819	0.913	0.913	0.819	0.004 1.002
12	0.802	223.5	1C.87	0.41	0.64	0.922	0.854	0.930	0.930	0.854	0.011 1.005
13	0.801	223.0	1C.87	0.41	0.97	0.959	0.925	0.964	0.964	0.925	0.013 1.006
14	0.801	223.0	1C.87	0.41	1.16	0.967	0.941	0.970	0.970	0.941	0.016 1.007
15	0.803	223.5	1C.87	0.41	1.46	0.981	0.972	0.983	0.983	0.972	0.022 1.010
16	0.802	223.5	1C.87	0.41	1.96	0.979	0.972	0.986	0.986	0.972	0.029 1.013

RUN	TST	P	TN	CCNF	MACH	RN/L	PT	C	P	TT	ALPHA
SFC	MACH	Q	X/DR	Y/DR	Z/DB	MF/M	MA/M	QF/Q	QA/Q	VF/V	VA/V
226	571	1	66	5	C.800	1.512	757	222.5	497	70.8	-20.00
1	0.800	222.5	1C.87	-0.03	-2.04	0.897	0.817	0.907	0.847	0.925	0.034 1.015
2	0.801	223.1	1C.87	-C.03	-1.55	C.917	0.847	0.920	0.834	0.773	0.011 1.008
3	0.801	223.1	1C.87	-0.03	-1.04	C.911	0.847	0.925	0.773	0.890	0.003 1.005
4	0.801	223.1	1C.87	-0.03	-0.71	C.879	0.756	0.881	0.881	0.935	0.008 1.004
5	0.801	223.0	1C.87	-C.03	-0.54	0.868	0.746	0.875	0.886	0.916	0.006 1.003
6	0.801	223.0	1C.87	-0.03	-0.37	C.863	0.755	0.881	0.881	0.935	0.003 1.001
7	0.801	223.0	1C.87	-C.03	-0.20	0.868	0.746	0.875	0.875	0.916	0.008 1.004
8	0.801	223.0	1C.87	-0.03	-0.04	C.862	0.765	0.886	0.886	0.935	0.002 1.001
9	0.801	223.0	1C.87	-0.03	0.13	C.874	0.781	0.894	0.894	0.935	0.005 1.002
10	0.801	223.0	1C.87	-C.03	0.30	0.883	0.780	0.893	0.893	0.935	0.010 1.004
11	0.801	223.0	1C.87	-C.03	0.46	C.882	0.817	0.910	0.910	0.935	0.018 1.008
12	0.801	223.0	1C.87	-C.03	0.63	C.900	0.916	0.935	0.935	0.935	0.021 1.009
13	0.801	223.0	1C.87	-0.03	0.96	C.924	0.933	0.941	0.941	0.935	0.023 1.010
14	0.802	223.5	1C.87	-C.03	1.15	C.961	0.965	0.960	0.960	0.935	0.033 1.015
15	0.802	223.5	1C.87	-C.03	1.47	C.973	0.976	0.983	0.983	0.935	0.030 1.014
16	0.801	223.1	1C.87	-0.03	1.97	C.980	0.974	0.989	0.989	0.935	0.027 1.013

RUN	TST	P	TN	CCNF	MACH	RN/L	PT	C	P	TT	ALPHA
SFC	MACH	Q	X/DR	Y/DR	Z/DB	MF/M	MA/M	QF/Q	QA/Q	VF/V	VA/V
227	571	1	66	5	C.800	1.512	757	222.5	497	70.8	-20.00
1	0.800	222.5	1C.87	-C.04	-2.04	C.971	0.962	0.974	0.959	0.975	0.044 1.020
2	0.799	222.6	1C.87	-C.38	-1.54	C.972	0.959	0.962	0.924	0.962	0.035 1.016
3	0.798	222.6	1C.87	-0.38	-1.05	0.958	0.825	0.916	0.909	0.962	0.016 1.007
4	0.799	222.6	1C.87	-C.38	-0.71	C.906	0.778	0.893	0.893	0.935	0.004 1.002
5	0.798	222.6	1C.87	-0.38	-0.54	0.881	0.770	0.889	0.889	0.935	0.001 1.001
6	0.799	222.6	1C.87	-C.38	-0.37	0.877	0.747	0.876	0.876	0.935	0.006 1.003
7	0.800	222.5	1C.87	-0.38	-0.19	0.862	0.762	0.883	0.883	0.935	0.013 1.006
8	0.800	222.5	1C.87	-C.38	-0.03	C.870	0.754	0.878	0.878	0.935	0.018 1.008
9	0.799	222.6	1C.87	-C.38	0.13	C.865	0.777	0.891	0.891	0.935	0.007 1.003
10	0.799	222.6	1C.87	-C.38	0.30	C.880	0.787	0.894	0.894	0.935	0.023 1.010
11	0.800	223.1	1C.87	-C.38	0.47	C.883	0.828	0.916	0.916	0.935	0.016 1.007
12	0.801	223.6	1C.87	-C.38	0.63	C.907	0.828	0.916	0.916	0.935	0.022 1.010
13	0.799	222.6	1C.87	-C.38	0.96	C.939	0.891	0.946	0.946	0.935	0.015 1.007
14	0.800	222.5	1C.87	-C.38	1.17	C.964	0.968	0.981	0.981	0.935	0.013 1.006
15	0.800	222.5	1C.87	-0.38	1.47	C.987	0.982	0.989	0.989	0.935	0.016 1.007
16	0.803	223.5	1C.87	-C.28	1.96	C.988	0.982	0.989	0.989	0.935	0.016 1.007

ORIGINAL PAGE IS  
QE POOR QUALITY

RUN	TST	P	TN	CCNF	MACH	RN/L	PT	C	P	TT	ALPHA
					X/DR	Y/DR	Z/DR	MF/N	MA/M	QF/Q	-20.00
238	571	1	66	5	0.799	1.510	757	222.0	497	70.7	
SEQ	MACH	0									
1	0.799	222.0	C	10.87	-C.48	-2.04	C.978	0.971	0.980	0.035	1.016
2	0.798	222.0	C	1C.87	-0.48	-1.55	0.977	0.968	0.979	0.032	1.014
3	0.797	221.5	C	1C.87	-C.48	-1.04	C.950	0.910	0.955	0.021	1.009
4	0.797	221.5	C	1C.87	-0.48	-0.70	0.897	0.808	0.907	0.009	1.004
5	0.798	222.0	C	1C.87	-C.48	-0.54	0.887	0.791	0.898	0.011	1.005
6	0.798	222.0	C	1C.87	-C.48	-0.36	0.879	0.777	0.891	0.009	1.004
7	0.798	222.0	C	1C.87	-C.48	-0.20	0.879	0.774	0.891	0.002	1.001
8	0.800	222.5	C	1C.87	-C.48	-0.04	0.878	0.775	0.890	0.009	1.004
9	0.800	222.5	C	1C.87	-0.48	0.13	0.875	0.770	0.887	0.009	1.004
10	0.800	222.5	C	1C.87	-0.48	0.29	C.890	0.792	0.900	0.002	1.001
11	0.799	222.0	C	1C.87	-0.48	0.47	C.897	0.808	0.907	0.008	1.004
12	0.800	222.5	C	1C.87	-C.48	0.63	0.915	0.841	0.923	0.012	1.005
13	0.800	222.5	C	1C.87	-C.48	0.96	C.950	0.908	0.955	0.015	1.007
14	0.800	222.5	C	1C.87	-0.48	1.16	C.965	0.938	0.969	0.013	1.006
15	0.801	222.4	C	1C.87	-C.48	1.47	0.979	0.970	0.981	0.027	1.012
16	0.801	222.4	C	1C.87	-C.48	1.97	C.98C	0.975	0.983	0.032	1.014

RUN	TST	P	TN	CCNF	MACH	RN/L	PT	C	P	TT	ALPHA
					X/DR	Y/DR	Z/DR	MF/N	MA/M	QF/Q	-20.00
239	571	1	66	5	0.801	1.514	758	223.1	497	70.7	
SEQ	MACH	0									
1	0.801	223.1	C	8.49	0.43	-2.02	C.982	0.978	0.985	0.025	1.011
2	0.801	223.1	C	8.49	C.43	-1.52	C.988	0.982	0.989	0.016	1.007
3	0.801	223.0	C	8.48	0.43	-1.02	C.978	0.962	0.980	0.014	1.006
4	0.803	223.5	C	8.49	C.43	-0.69	0.926	0.859	0.934	0.004	1.002
5	0.803	223.5	C	8.48	C.43	-0.52	C.91C	0.870	0.919	0.003	1.001
6	0.803	223.5	C	8.48	0.43	-0.36	C.9C4	0.816	0.913	-0.001	1.000
7	0.804	224.0	C	8.49	C.43	-0.19	0.896	0.799	0.906	-0.009	0.996
8	0.804	224.0	C	8.49	C.42	-0.02	C.883	0.775	0.895	-0.014	0.993
9	0.804	224.0	C	8.49	C.43	0.14	0.872	C.760	0.884	0.001	1.001
10	0.802	223.0	C	8.49	C.43	0.30	0.886	C.790	0.897	0.014	1.006
11	0.801	223.0	C	8.49	C.43	0.48	C.899	0.812	0.909	0.010	1.004
12	0.800	222.5	C	8.49	C.43	0.65	C.919	0.848	0.927	0.009	1.004
13	0.800	222.5	C	8.49	C.42	0.98	C.956	0.922	0.961	0.019	1.009
14	0.799	222.6	C	8.49	C.43	1.19	0.975	0.961	0.978	0.023	1.010
15	0.798	222.6	C	8.48	C.43	1.48	C.984	0.977	0.966	0.022	1.010
16	0.798	222.6	C	8.48	C.43	1.98	C.982	0.978	0.985	0.025	1.011

ORIGINAL PAGE IS  
OF POOR QUALITY

RUN	TST	P	TN	CCNF	MACH	RN/L	PT	G	P	TT	ALPHA	
SFC	MACH	C	X/DB	Y/DB	Z/DB	NF/N	MA/N	QA/Q	VF/V	VA/V	CP	PF/P
240	571	1	66	5	0.799	1.510	757	222.0	497	70.6	-20.00	
1	0.799	222.0	C	8.49	-0.01	-2.02	0.892	0.806	0.903	0.030	1.013	
2	0.799	222.0	C	8.49	-C.01	-1.53	C.903	0.825	0.912	0.029	1.013	
3	0.798	221.5	E	8.49	-0.01	-1.03	0.912	0.837	0.920	0.015	1.007	
4	0.800	222.5	E	8.49	-0.01	-0.69	C.827	0.800	0.852	0.317	1.142	
5	0.800	222.5	E	8.49	-0.01	-0.53	0.866	0.751	0.879	0.003	1.001	
6	C.800	222.5	E	8.49	-0.01	-0.36	C.846	0.713	0.860	-0.010	0.996	
7	0.800	222.5	E	8.49	-0.01	-0.19	C.828	0.683	0.643	-0.006	0.997	
8	C.800	222.5	E	8.49	-0.01	-0.01	C.822	0.673	0.838	-0.010	0.996	
9	0.801	223.0	C	8.49	-C.01	0.15	C.832	0.689	0.847	-0.011	0.995	
10	0.801	223.0	C	8.49	-0.01	0.31	C.855	0.727	0.868	-0.011	0.995	
11	0.801	223.0	C	8.49	-0.01	0.48	C.864	0.745	0.877	-0.004	0.998	
12	0.801	223.0	C	8.49	-C.01	0.65	C.891	0.796	0.901	0.008	1.004	
13	0.801	223.0	C	8.49	-0.01	0.97	C.949	0.907	0.955	C.015	1.077	
14	0.801	222.0	C	8.49	-C.01	1.17	C.972	C.952	0.976	0.015	1.007	
15	0.801	223.0	C	8.49	-0.01	1.48	C.984	0.977	0.988	0.018	1.008	
16	C.800	222.5	E	8.49	-0.01	1.98	C.984	0.979	0.986	0.025	1.011	

RUN	TST	P	TN	CCNF	MACH	RN/L	PT	G	P	TT	ALPHA	
SFC	MACH	C	X/DB	Y/DB	Z/DB	NF/N	MA/N	QA/Q	VF/V	VA/V	CP	PF/P
241	571	1	66	C.800	1.513	757	222.5	497	70.5	-20.00		
1	0.800	222.5	E	8.49	-0.36	-2.03	C.978	C.970	0.980	0.032	1.014	
2	0.801	223.1	E	8.49	-0.36	-1.52	C.978	0.968	0.980	0.028	1.013	
3	0.801	223.1	E	8.49	-C.36	-1.03	C.965	0.940	0.969	0.023	1.010	
4	0.801	223.1	E	8.49	-C.36	-0.69	C.908	0.827	0.918	0.006	1.003	
5	0.801	223.1	E	8.49	-0.36	-0.52	C.869	0.755	0.881	-0.000	1.000	
6	0.801	223.1	E	8.49	-C.36	-0.36	C.851	0.723	0.864	-0.003	0.999	
7	0.801	223.1	E	8.49	-0.36	-0.19	C.829	0.684	0.844	-0.010	0.996	
8	0.800	222.5	E	8.49	-0.36	-0.02	0.845	0.711	0.859	-0.008	0.997	
9	0.801	223.0	E	8.49	-C.36	0.14	0.844	0.712	0.858	-0.003	0.999	
10	0.801	223.0	E	8.49	-C.36	0.32	0.862	0.742	0.875	-0.003	0.999	
11	0.800	222.5	E	8.49	-C.36	0.48	0.884	0.782	0.895	-0.000	1.000	
12	0.800	222.5	E	8.49	-0.36	0.65	C.906	0.821	0.915	0.003	1.001	
13	C.800	222.5	E	8.49	-C.36	0.98	C.953	0.914	0.958	0.015	1.007	
14	0.800	222.5	E	8.49	-0.36	1.19	C.971	C.950	0.974	0.019	1.009	
15	0.800	222.5	E	8.49	-0.36	1.48	C.983	C.975	0.965	0.021	1.009	
16	0.799	221.9	E	8.49	-0.36	1.98	C.984	C.979	0.986	0.025	1.011	

RUN	TST	P	TN	CCNF	MACH	PN/L	PT	C	P	TT	ALPHA
SFG	MACH	Q	X/DB	Y/DR	Z/DB	MF/N	MA/M	QF/Q	QA/Q	VF/V	VAV/V
242	571	1	66	5.0	-799	1.514	758	222.6	498	70.6	-20.00
											PF/P
1	0.799	222.6	8.48	-0.45	-2.03	0.982	0.977	0.934	0.927	1.012	
2	C.8C0	222.5	8.49	-0.45	-1.53	0.985	0.979	0.986	0.022	1.010	
3	0.799	222.0	8.48	-0.45	-1.04	0.973	0.951	0.976	0.011	1.005	
4	0.799	222.0	8.49	-0.45	-0.67	0.900	0.814	0.910	0.008	1.004	
5	0.799	222.0	8.49	-0.45	-0.53	0.872	0.761	0.884	0.004	1.002	
6	0.799	222.0	8.48	-0.45	-0.36	0.862	0.745	0.876	0.002	1.001	
7	0.799	222.0	8.49	-0.45	-0.19	0.852	0.724	0.866	-0.005	0.998	
8	0.799	222.0	8.49	-0.45	-0.02	0.850	0.723	0.863	0.004	1.002	
9	0.800	222.5	8.49	-0.45	0.14	0.859	0.735	0.872	-0.006	0.997	
10	0.800	222.5	8.49	-0.45	0.31	0.859	0.738	0.872	-0.000	1.000	
11	0.800	222.5	8.49	-0.45	0.48	0.885	0.786	0.896	-0.006	1.003	
12	0.8C0	222.5	8.49	-0.45	0.65	0.912	0.833	0.921	0.006	1.003	
13	0.800	222.5	8.49	-0.45	0.98	0.954	0.915	0.959	0.015	1.007	
14	0.798	222.0	8.49	-0.45	1.18	0.983	0.970	0.935	0.009	1.004	
15	0.800	222.5	8.49	-0.45	1.48	0.987	0.981	0.989	0.015	1.007	
16	0.800	222.5	8.49	-0.45	1.98	0.985	0.980	0.987	0.021	1.009	

RUN	TST	P	TN	CCNF	MACH	PN/L	PT	C	P	TT	ALPHA
SFG	MACH	C	X/DB	Y/DR	Z/DB	MF/N	MA/M	QF/Q	QA/Q	VF/V	VAV/V
243	571	1	66	5.0	0.601	1.511	887	175.8	695	64.8	-20.00
											PF/P
2	0.601	175.8	1C.88	C.41	-2.05	0.973	0.957	0.975	0.043	1.011	
3	0.597	174.0	1C.88	C.41	-1.54	0.971	0.955	0.973	0.046	1.012	
4	0.596	173.4	1C.88	C.41	-1.04	0.947	0.905	0.950	0.035	1.009	
5	0.596	173.5	1C.88	C.41	-0.71	0.915	0.842	0.920	0.023	1.006	
6	0.599	174.0	1C.88	C.41	-0.53	0.924	0.852	0.928	-0.005	0.999	
7	0.601	175.0	1C.88	C.41	-0.37	0.906	0.821	0.912	0.002	1.000	
8	0.600	175.2	1C.88	C.41	-0.20	0.906	0.824	0.912	0.010	1.002	
9	0.600	175.2	1C.88	C.41	-0.03	0.908	0.828	0.913	0.016	1.004	
10	0.600	175.0	1C.88	C.41	0.13	0.900	0.816	0.906	0.023	1.007	
11	0.599	174.0	1C.88	C.41	0.29	0.901	0.818	0.906	0.032	1.008	
12	0.596	173.4	1C.88	C.41	0.47	0.919	0.847	0.924	0.014	1.003	
13	0.597	174.0	1C.88	C.41	0.63	0.927	0.878	0.941	-0.001	1.000	
14	0.600	175.0	1C.88	C.41	0.97	0.960	0.922	0.962	0.003	1.001	
15	0.602	175.0	1C.88	C.41	1.16	0.976	0.955	0.978	0.007	1.002	
16	0.600	175.2	1C.88	C.41	1.47	0.986	0.975	0.987	0.015	1.004	
17	0.602	175.8	1C.88	C.41	1.96	0.977	0.961	0.978	0.032	1.008	

ORIGINAL PAGE IS  
OF POOR QUALITY

RUN	TST	P	TN	CNF	MACH	RN/L	PT	C	P	TT	ALPHA
SFC	MACH	G	X/DR	Y/DR	Z/DR	MF/N	MA/M	QF/Q	QA/Q	VF/V	VA/V
244	571	1	66	5	0.600	1.5C8	887	175.2	696	65.1	-20.00
	1	0.600	175.2	1C.88	-C.03	-2.04	C.932	0.868	0.936	-0.001	1.000
	2	0.603	175.4	10.88	-C.03	-1.54	C.929	0.865	0.934	0.005	1.001
	3	0.603	176.4	1C.88	-C.03	-1.04	C.921	0.852	0.926	0.014	1.004
	4	0.601	175.2	1C.88	-C.03	-0.71	C.886	0.789	0.893	0.015	1.004
	5	0.601	175.2	1C.88	-C.03	-0.54	C.888	0.790	0.894	0.007	1.002
	6	0.602	175.8	1C.88	-C.03	-0.37	C.865	0.752	0.873	0.020	1.005
	7	0.602	175.8	1C.88	-C.03	-0.20	C.861	0.745	0.869	0.020	1.005
	8	0.601	175.8	1C.88	-C.03	-0.04	C.873	0.765	0.880	0.010	1.002
	9	0.599	174.6	1C.88	-C.03	0.13	C.886	0.786	0.892	0.008	1.002
	10	0.598	174.0	1C.88	-C.03	0.30	C.886	0.786	0.892	0.011	1.003
	11	0.598	174.0	1C.88	-C.03	0.46	C.884	0.784	0.890	0.018	1.004
	12	0.598	174.0	1C.88	-C.03	0.63	C.911	0.833	0.916	0.013	1.003
	13	0.598	174.0	1C.88	-C.03	0.98	C.943	0.892	0.946	0.011	1.003
	14	0.599	174.6	1C.88	-C.03	1.15	C.946	0.901	0.950	0.022	1.005
	15	0.599	174.6	1C.88	-C.03	1.46	C.982	0.969	0.983	0.019	1.005
	16	0.599	174.6	1C.88	-C.03	1.96	C.977	0.963	0.978	0.038	1.010

RUN	TST	P	TN	CNF	MACH	RN/L	PT	C	P	TT	ALPHA
SFC	MACH	G	X/DR	Y/DR	Z/DR	MF/N	MA/M	QF/Q	QA/Q	VF/V	VA/V
245	571	1	66	5	0.600	1.5C6	887	175.2	695	65.3	-20.00
	1	0.600	175.2	1C.88	-C.28	-2.05	C.980	0.967	0.981	0.026	1.007
	2	0.599	174.6	1C.88	-C.03	-1.53	C.981	0.967	0.982	0.020	1.005
	3	0.602	175.8	1C.88	-C.38	-1.05	C.946	0.899	0.949	0.019	1.005
	4	0.600	175.2	1C.88	-C.38	-0.70	C.9C2	0.820	0.909	0.018	1.005
	5	0.600	175.2	1C.88	-C.38	-0.54	0.887	0.788	0.894	0.003	1.001
	6	0.600	175.2	1C.88	-C.38	-0.38	0.887	0.786	0.893	-0.002	0.999
	7	0.601	175.2	1C.88	-C.38	-0.21	0.878	0.772	0.884	0.011	1.003
	8	0.601	175.2	1C.88	-C.38	-0.05	C.910	0.771	0.916	-0.277	0.930
	9	0.602	175.8	1C.88	-C.38	0.12	C.9C2	0.816	0.909	0.003	1.001
	10	0.600	175.2	1C.88	-C.38	0.30	C.900	0.812	0.905	0.012	1.003
	11	0.600	175.2	1C.88	-C.38	0.46	C.896	0.808	0.902	0.024	1.006
	12	0.599	174.6	1C.87	-C.38	0.63	C.909	0.832	0.914	0.029	1.007
	13	0.600	175.2	1C.87	-C.38	0.96	0.929	0.869	0.933	0.027	1.007
	14	0.599	174.6	1C.87	-C.38	1.16	C.961	0.926	0.963	0.014	1.003
	15	0.601	175.8	1C.87	-C.38	1.47	0.978	0.963	0.979	0.029	1.007
	16	0.600	175.2	1C.87	-C.38	1.96	C.982	0.972	0.984	0.027	1.007

RUN	TST	P	TN	CCNF	MACH	PN/L	PT	C	P	TT	ALPHA
SFC	MACH	Q	X/DR	Y/DR	Z/DR	MF/N	MA/M	QA/Q	VF/V	VA/V	PF/P
246	571	1	66	5	0.599	1.502	887	174.6	696	65.7	-20.00
1	0.599	174.6	1C.87	-0.48	-2.04	0.980	0.967	0.981	0.028	1.007	
2	0.599	174.6	1C.88	-C.48	-1.54	0.982	0.971	0.983	0.024	1.006	
3	0.599	174.6	1C.88	-C.48	-1.05	0.958	0.921	0.961	0.014	1.003	
4	0.599	174.6	1C.88	-C.48	-0.71	0.900	0.811	0.905	0.009	1.002	
5	0.600	175.2	1C.87	-C.48	-0.54	0.890	0.796	0.897	0.018	1.005	
6	0.600	175.2	1C.87	-0.49	-0.37	0.890	0.793	0.897	0.004	1.001	
7	0.600	175.2	1C.87	-C.48	-0.20	0.889	0.792	0.895	0.009	1.002	
8	0.600	175.2	1C.88	-0.48	-0.04	0.895	0.801	0.901	0.004	1.001	
9	0.6C2	175.8	1C.88	-C.48	0.12	0.900	0.812	0.906	0.014	1.004	
10	0.602	175.8	1C.87	-0.48	0.30	0.900	0.812	0.906	0.011	1.003	
11	0.602	175.8	1C.88	-C.48	0.47	0.910	0.831	0.915	0.015	1.004	
12	0.6C2	175.8	1C.87	-C.48	0.63	0.920	0.849	0.925	0.012	1.003	
13	0.602	175.8	1C.88	-C.48	0.97	0.946	0.899	0.950	0.016	1.004	
14	0.6C2	175.8	1C.87	-C.48	1.17	0.969	0.946	0.971	0.028	1.007	
15	0.602	175.8	1C.87	-C.48	1.46	0.982	0.969	0.983	0.022	1.006	
16	0.602	175.8	1C.88	-C.48	1.97	0.984	0.974	0.985	0.024	1.006	

RUN	TST	F	TN	CCNF	MACH	PN/L	PT	C	P	TT	ALPHA
SFC	MACH	Q	X/DR	Y/DR	Z/DR	MF/N	MA/M	QA/Q	VF/V	VA/V	PF/P
247	571	1	66	5	0.6C0	1.5C0	887	175.2	695	65.1	-20.00
1	0.6C0	175.2	8.49	C.43	-2.C3	0.980	0.967	0.981	0.028	1.007	
2	0.600	175.2	8.49	C.43	-1.52	0.984	0.974	0.985	0.020	1.005	
3	0.600	175.2	8.49	0.43	-1.03	0.977	0.957	0.978	0.011	1.003	
4	0.6C0	175.2	8.49	C.43	-0.65	0.912	0.834	0.918	0.007	1.002	
5	0.600	175.2	8.49	C.43	-0.52	0.9C5	0.820	0.910	0.006	1.001	
6	0.6C0	175.2	8.49	C.43	-0.36	0.908	0.825	0.913	0.005	1.001	
7	0.600	175.2	8.49	C.43	-0.19	0.9C2	0.813	0.908	-0.003	0.999	
8	0.600	175.2	8.49	C.43	-0.02	0.890	0.793	0.896	0.097	1.002	
9	0.600	175.2	8.49	C.43	0.15	0.9C5	0.820	0.911	0.003	1.000	
10	0.600	175.2	8.49	C.43	0.31	0.892	0.799	0.899	0.014	1.003	
11	0.6C0	175.2	8.49	C.43	0.45	0.917	0.840	0.922	-0.001	1.000	
12	0.600	175.2	8.49	C.43	0.66	0.92C	0.865	0.934	0.000	1.000	
13	0.6C0	175.2	8.49	C.43	0.99	0.971	0.944	0.973	0.007	1.002	
14	0.6C0	175.2	8.49	C.43	1.18	0.985	0.972	0.986	0.007	1.002	
15	0.602	175.8	8.49	C.43	1.48	0.986	0.975	0.987	0.015	1.004	
16	0.6C2	175.8	8.49	C.43	1.98	0.987	0.979	0.988	0.019	1.005	

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RUN	TST	P	TN	CCNF	MACH	RNL	PT	G	P	TT	ALPHA	
SEQ	MACH	Q	X/DB	Y/DR	Z/DR	WF/N	MA/M	CA/Q	VF/V	VA/V	CP	PF/P
248	571	1	66	5	0.600	1.503	887	175.2	695	66.2	-20.00	
1	0.600	175.2	8.49	-c.01	-2.02	c.911	0.835	0.916	0.026	1.007		
2	0.600	175.2	8.49	-0.01	-1.53	0.926	0.861	0.931	0.011	1.003		
3	0.600	175.2	8.49	-c.01	-1.02	0.921	0.851	0.926	0.007	1.002		
4	0.600	175.2	8.49	-0.01	-0.70	0.888	0.789	0.894	0.003	1.001		
5	0.600	175.2	8.49	-c.01	-0.53	0.862	0.742	0.869	-0.004	0.999		
6	0.602	175.8	8.49	-c.01	-0.36	c.844	0.712	0.852	0.000	1.000		
7	0.602	175.8	8.49	-0.01	-0.19	c.828	0.685	0.837	0.001	1.000		
8	0.602	175.8	8.49	-c.01	-0.02	c.859	0.738	0.867	-0.003	0.999		
9	0.602	175.8	8.49	-0.01	0.14	c.856	0.734	0.864	0.003	1.001		
10	0.602	175.8	8.49	-c.01	0.32	0.854	0.729	0.862	0.000	1.000		
11	0.602	175.8	8.49	-c.01	0.47	c.873	0.763	0.880	0.002	1.000		
12	0.602	175.8	8.49	-0.01	0.64	c.897	0.804	0.903	-0.003	0.999		
13	0.602	175.8	8.49	-c.01	0.98	c.953	0.910	0.956	0.009	1.002		
14	0.602	175.8	8.49	-0.01	1.17	c.976	0.956	0.978	0.015	1.004		
15	0.602	175.8	8.49	-0.01	1.48	c.978	0.963	0.979	0.029	1.007		
16	0.602	175.8	8.49	-c.01	1.98	c.981	0.970	0.982	0.028	1.007		

RUN	TST	P	TN	CCNF	MACH	RNL	PT	G	P	TT	ALPHA	
SEQ	MACH	Q	X/DB	Y/DR	Z/DR	WF/N	MA/M	CA/Q	VF/V	VA/V	CP	PF/P
249	571	1	66	5	0.600	1.502	887	175.2	695	66.5	-20.00	
1	0.600	175.2	8.49	-0.36	-2.02	c.984	0.974	0.985	0.025	1.006		
2	0.600	175.2	8.49	-0.36	-1.52	c.982	0.971	0.983	0.025	1.006		
3	0.600	175.2	8.49	-c.36	-1.03	c.970	0.942	0.972	0.006	1.001		
4	0.600	175.2	8.49	-0.36	-0.70	c.917	0.841	0.922	0.001	1.000		
5	0.600	175.2	8.49	-c.36	-0.52	c.875	0.766	0.882	0.006	1.001		
6	0.600	175.2	8.49	-0.36	-0.36	c.857	0.735	0.865	0.003	1.001		
7	0.600	175.2	8.49	-c.36	-0.17	c.856	0.733	0.864	-0.004	0.999		
8	0.600	175.2	8.49	-c.36	-0.02	c.868	0.752	0.875	-0.007	0.998		
9	0.600	175.2	8.49	-0.36	0.15	c.863	0.745	0.871	-0.003	0.999		
10	0.600	175.2	8.49	-c.36	0.32	c.867	0.750	0.874	-0.005	0.999		
11	0.602	175.8	8.49	-0.36	0.48	c.878	0.773	0.885	0.013	1.003		
12	0.602	175.8	8.49	-c.36	0.65	c.918	0.843	0.922	0.005	1.001		
13	0.602	175.8	8.49	-0.36	0.98	c.962	0.928	0.965	0.006	1.001		
14	0.602	175.8	8.49	-c.36	1.18	c.976	0.956	0.977	0.014	1.004		
15	0.602	175.8	8.49	-c.36	1.48	c.987	0.979	0.988	0.019	1.005		
16	0.602	175.8	8.49	-0.36	1.98	c.989	0.981	0.990	0.014	1.004		

RUN	TST	P	TIN	CCNF	MACH	RN/L	PT	G	P	TT	ALPHA
SFG	MACH	G	X/DB	Y/DB	Z/DB	MF/N	MA/M	QF/Q	QA/Q	VF/V	VA/V
250	571	1	66	5	0.602	1.503	887	175.8	694	66.7	-20.00
1	0.602	175.8	8.49	-0.45	-2.03	0.984	0.974	0.985	0.985	0.984	0.984
2	0.602	175.8	8.49	-C.45	-1.52	C.983	0.972	0.972	0.972	0.972	0.972
3	0.602	175.8	8.49	-0.45	-1.02	C.963	0.930	0.965	0.965	0.965	0.965
4	0.602	175.8	8.49	-C.45	-0.69	C.915	0.840	0.920	0.920	0.920	0.920
5	0.600	175.2	8.49	-0.45	-0.52	0.878	0.772	0.885	0.885	0.885	0.885
6	C.600	175.2	8.49	-0.45	-0.35	0.879	0.774	0.886	0.886	0.886	0.886
7	0.600	175.2	8.49	-0.45	-0.18	C.870	0.757	0.877	0.877	0.877	0.877
8	0.600	175.2	8.49	-0.45	-0.03	0.878	0.771	0.885	0.885	0.885	0.885
9	C.600	175.2	8.49	-0.45	0.14	0.872	0.763	0.879	0.879	0.879	0.879
10	0.600	175.2	8.49	-C.45	0.31	0.891	0.793	0.897	0.897	0.897	0.897
11	0.600	175.2	8.49	-0.45	0.48	0.905	0.819	0.911	0.911	0.911	0.911
12	0.600	175.2	8.49	-0.45	0.65	C.912	C.833	0.917	0.917	0.917	0.917
13	0.600	175.2	8.49	-0.45	0.98	0.959	0.923	0.962	0.962	0.962	0.962
14	0.600	175.2	8.49	-0.45	1.19	C.982	0.968	0.984	0.984	0.984	0.984
15	0.600	175.2	8.49	-C.45	1.49	C.985	0.975	0.986	0.986	0.986	0.986
16	0.600	175.2	8.49	-0.45	1.98	0.981	0.969	0.983	0.983	0.983	0.983

RUN	TST	P	TIN	CCNF	MACH	RN/L	PT	G	P	TT	ALPHA
SFG	MACH	G	X/DB	Y/DB	Z/DB	MF/N	MA/M	QF/Q	QA/Q	VF/V	VA/V
251	571	1	66	5	0.251	1.515	1875	179.4	179.4	65.1	-20.00
1	0.251	79.4	1C.87	C.41	-2.05	0.995	0.000	0.990	0.000	0.995	0.000
2	0.250	78.8	1C.88	0.41	-1.53	C.956	0.000	0.991	0.000	0.996	0.000
3	0.251	79.4	1C.88	0.41	-1.04	C.948	0.000	0.898	0.000	0.948	0.000
4	0.250	78.8	1C.88	0.41	-0.70	C.935	0.000	0.874	0.000	0.936	0.000
5	0.251	79.4	1C.88	0.41	-0.54	C.912	0.000	0.832	0.000	0.913	0.000
6	0.249	78.1	1C.88	0.41	-0.38	C.928	0.000	0.859	0.000	0.928	0.000
7	0.250	78.8	1C.88	0.41	-0.22	C.908	0.000	0.824	0.000	0.909	0.000
8	0.250	78.8	1C.88	0.41	-0.04	C.945	0.000	0.892	0.000	0.945	0.000
9	0.250	78.8	1C.88	0.41	0.12	C.942	0.000	0.887	0.000	0.943	0.000
10	0.250	78.8	1C.88	0.41	0.29	0.930	0.000	0.864	0.000	0.931	0.000
11	0.250	78.8	1C.88	0.41	0.47	C.940	0.000	0.883	0.000	0.941	0.000
12	0.250	78.8	1C.88	0.41	0.63	C.949	0.000	0.899	0.000	0.949	0.000
13	0.252	79.4	1C.88	0.41	0.97	0.970	0.000	0.941	0.000	0.971	0.000
14	0.253	80.1	1C.88	C.41	1.16	C.98C	0.000	0.961	0.000	0.980	0.000
15	0.249	78.1	1C.88	0.41	1.47	C.990	0.000	0.979	0.000	0.990	0.000
16	0.250	78.8	1C.88	0.41	1.97	C.993	0.000	0.986	0.000	0.993	0.000

ORIGINAL PAGE IS  
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RUN	TST	P	TN	CNF	MACH	RN/L	PT	G	TT	ALPHA	PF/P
252	571	1	66	5 C.250	1.510	1.874	78.8	1794	64.6	-20.00	0.999
				X/DR	Y/DB	Z/DR	MF/N	MA/M	QF/Q	QA/Q	VF/V
SEG	MACH	0	0.250	78.8	10.88	-0.03	-2.04	C.938	0.000	0.880	0.000
1	0.250	78.8	10.88	-0.03	-1.54	C.944	0.000	0.890	C.000	0.944	0.000
2	0.250	78.8	10.88	-0.02	-1.03	C.937	0.000	0.878	0.000	0.938	0.000
3	0.250	78.8	10.88	-0.02	-0.71	C.947	0.000	0.822	C.000	0.908	0.000
4	0.252	79.4	10.88	-0.02	-0.71	C.947	0.000	0.766	0.000	0.877	0.000
5	0.250	78.8	10.88	-0.03	-0.54	C.875	0.000	0.755	C.000	0.871	0.000
6	0.250	78.8	10.88	-C.03	-0.37	C.870	0.000	0.894	0.000	0.898	0.000
7	0.250	78.8	10.88	-C.03	-0.20	0.897	0.000	0.824	0.000	0.909	0.000
8	0.250	78.8	10.88	-C.03	-0.04	C.948	0.000	0.811	C.000	0.902	0.000
9	0.252	79.4	10.88	-0.03	0.13	C.931	0.000	0.916	0.000	0.916	0.000
10	0.250	78.8	10.88	-C.03	0.30	C.915	0.000	C.836	C.000	0.920	0.000
11	0.250	78.8	10.88	-C.03	0.46	C.919	0.000	C.845	C.000	0.921	0.000
12	0.250	78.8	10.88	-C.03	0.62	C.920	0.000	0.846	0.000	0.921	0.000
13	0.250	78.8	10.88	-C.03	0.97	C.955	0.000	0.911	C.000	0.955	0.000
14	0.250	78.8	10.88	-C.03	1.16	C.972	0.000	0.944	0.000	0.972	0.000
15	0.250	78.8	10.88	-C.03	1.46	C.989	0.000	0.977	C.000	0.989	0.000
16	0.252	79.4	10.88	-C.03	1.97	C.952	0.000	0.984	C.000	0.992	0.000

RUN	TST	P	TN	CNF	MACH	RN/L	PT	G	TT	ALPHA	PF/P
253	571	1	66	5 C.252	1.518	1.874	79.4	1794	64.2	-20.00	0.999
SFC	MACH	G	X/DR	Y/DR	Z/DR	MF/N	MA/M	QF/Q	QA/Q	VF/V	VA/V
1	0.252	79.4	10.88	-0.38	-2.04	C.991	0.000	0.983	0.000	0.991	0.000
2	0.252	79.4	10.88	-C.38	-1.54	C.989	0.000	0.977	C.000	0.989	0.000
3	0.250	78.8	10.88	-0.38	-1.04	C.955	0.000	0.911	C.000	0.955	0.000
4	0.252	79.4	10.88	-0.38	-0.70	C.917	0.000	0.841	0.000	0.918	0.000
5	0.250	78.8	10.88	-0.38	-0.54	C.909	0.000	0.825	0.000	0.910	0.000
6	0.250	78.8	10.88	-0.38	-0.37	C.911	0.000	C.829	C.000	0.912	0.000
7	0.250	78.8	10.88	-0.38	-0.21	C.917	0.000	C.839	C.000	0.918	0.000
8	0.250	78.8	10.88	-0.38	-0.04	C.919	0.000	C.843	C.000	0.919	0.000
9	0.250	78.8	10.88	-0.38	0.13	C.915	0.000	0.836	0.000	0.916	0.000
10	0.250	78.8	10.88	-0.38	0.30	C.908	0.000	0.824	C.000	0.909	0.000
11	0.250	78.8	10.88	-0.38	0.47	C.928	0.000	0.860	C.000	0.929	0.000
12	0.250	78.8	10.88	-0.38	0.64	C.940	0.000	0.883	C.000	0.941	0.000
13	0.250	78.8	10.88	-0.38	0.97	C.942	0.000	0.888	C.000	0.943	0.000
14	0.250	78.8	10.88	-0.38	1.17	C.981	0.000	0.962	C.000	0.981	0.000
15	0.250	78.8	10.88	-0.38	1.96	C.951	0.000	0.981	C.000	0.991	0.000
16	0.250	78.8	10.88	-0.38	1.96	C.992	0.000	0.984	C.000	0.992	0.000

RUN	TST	P	TN	CCNF	MACH	RN/L	PT	C	G	P	TT	ALPHA	
SEC	MACH	Q	X/DB	Y/DB	Z/DB	MF/N	WA/M	QF/Q	QA/Q	VF/V	VA/V	CP	PF/P
254	571	1	66	5	0.252	1.519	1874	79.4	1794	63.9	-20.00		
1	0.252	79.4	10.88	-C.48	-2.05	C.982	0.000	0.965	0.000	0.983	0.000	0.002	1.000
2	0.250	78.8	10.88	-C.48	-1.53	C.986	0.000	0.972	0.000	0.986	0.000	-0.001	1.000
3	0.250	78.8	10.88	-C.48	-1.04	C.959	0.000	0.920	0.000	0.960	0.000	-0.010	1.000
4	0.249	78.1	10.88	-C.48	-0.71	C.924	0.000	0.852	0.000	0.925	0.000	-0.030	0.999
5	0.249	78.1	10.88	-C.48	-0.54	C.916	0.000	0.838	0.000	0.917	0.000	-0.030	0.999
6	0.251	78.8	10.88	-C.48	-0.37	C.911	0.000	0.829	0.000	0.912	0.000	-0.021	0.999
7	0.250	78.8	10.88	-C.48	-0.20	C.894	0.000	0.799	0.000	0.895	0.000	-0.012	0.999
8	0.250	78.8	10.88	-C.48	-0.04	C.911	0.000	0.829	0.000	0.912	0.000	-0.012	0.999
9	0.250	78.8	10.88	-C.48	0.12	C.907	0.000	0.822	0.000	0.908	0.000	-0.021	0.999
10	0.250	78.8	10.88	-C.48	0.29	C.927	0.000	0.859	0.000	0.928	0.000	-0.012	0.999
11	0.249	78.1	10.88	-C.48	0.46	C.930	0.000	0.864	0.000	0.931	0.000	-0.021	0.999
12	0.249	78.1	10.88	-C.48	0.63	C.926	0.000	0.857	0.000	0.927	0.000	-0.019	0.999
13	0.249	78.1	10.88	-C.48	0.97	C.965	0.000	0.930	0.000	0.965	0.000	-0.021	0.999
14	0.249	78.1	10.88	-C.48	1.16	C.951	0.000	0.981	0.000	0.991	0.000	-0.017	0.999
15	0.249	78.1	10.88	-C.48	1.47	C.990	0.000	0.981	0.000	0.991	0.000	-0.010	1.000
16	0.249	78.1	10.88	-C.48	1.96	C.994	0.000	0.938	0.000	0.994	0.000	-0.012	0.999

RUN	TST	P	TN	CCNF	MACH	RN/L	PT	C	G	P	TT	ALPHA	
SEC	MACH	Q	X/DB	Y/DB	Z/DB	MF/N	WA/M	QF/Q	QA/Q	VF/V	VA/V	CP	PF/P
255	571	1	66	5	0.250	1.514	1874	78.8	1794	63.5	-20.00		
1	0.250	78.8	8.49	C.43	-2.03	C.990	0.000	0.979	0.000	0.990	0.000	-0.010	1.000
2	0.249	78.1	8.49	C.43	-1.52	C.992	0.000	0.984	0.000	0.992	0.000	-0.014	0.999
3	0.250	78.8	8.49	C.43	-1.C3	C.979	0.000	0.958	0.000	0.979	0.000	-0.006	1.000
4	0.250	78.8	8.49	C.43	-0.65	C.931	0.000	0.866	0.000	0.931	0.000	-0.012	0.999
5	0.250	78.8	8.49	C.43	-0.53	C.915	0.000	0.836	0.000	0.915	0.000	-0.012	0.999
6	0.249	78.1	8.49	C.43	-0.35	C.918	0.000	0.842	0.000	0.919	0.000	-0.021	0.999
7	0.249	78.1	8.49	C.43	-0.19	C.882	0.000	0.778	0.000	0.884	0.000	-0.021	0.999
8	0.249	78.1	8.49	C.43	-0.03	C.924	0.000	0.854	0.000	0.925	0.000	-0.012	0.999
9	0.249	78.1	8.49	C.43	0.14	C.921	0.000	0.849	0.000	0.922	0.000	-0.012	0.999
10	0.249	78.1	8.49	C.43	0.31	C.927	0.000	0.859	0.000	0.928	0.000	-0.012	0.999
11	0.248	77.4	8.49	C.43	0.48	C.937	0.000	0.877	0.000	0.938	0.000	-0.021	0.999
12	0.248	77.4	8.49	C.43	0.64	C.936	0.000	0.876	0.000	0.937	0.000	-0.021	0.999
13	0.248	77.4	8.49	C.43	0.98	C.980	0.000	0.959	0.000	0.980	0.000	-0.016	0.999
14	0.249	78.1	8.49	C.43	1.19	C.987	0.000	0.974	0.000	0.987	0.000	-0.016	0.999
15	0.248	77.4	8.49	C.42	1.48	C.998	0.000	0.995	0.000	0.998	0.000	-0.016	0.999
16	0.249	78.1	8.49	C.43	1.98	C.991	0.000	0.981	0.000	0.991	0.000	-0.014	0.999

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RUN	TST	P	TN	CCNF	MACH	RN/L	PT	G	TT	ALPHA	P	63.3	-20.00
256	571	1	66	5	C.249	1.5C8	1874	78.1	1794				
SEG	MACH	G	X/DR	Y/DR	Z/DB	MF/N	MA/M	QF/Q	QA/Q	VF/V	VA/V		PF/P
1	0.249	78.1	8.49	-0.01	-2.03	0.934	0.000	0.871	0.000	0.935	0.000	-0.016	0.999
2	0.248	77.4	8.49	-0.01	-1.52	0.942	0.000	0.886	0.000	0.942	0.000	-0.014	0.999
3	0.249	78.1	8.49	-0.01	-1.01	0.941	0.000	0.884	0.000	0.941	0.000	-0.021	0.999
4	C.250	78.8	8.49	-0.01	-0.70	0.895	0.000	0.801	0.000	0.896	0.000	-0.012	0.999
5	0.249	78.1	8.49	-0.01	-0.53	C.876	0.000	0.767	0.000	0.878	0.000	-0.021	0.999
6	0.250	78.8	8.49	-0.01	-0.36	0.844	0.000	0.712	0.000	0.845	0.000	-0.012	0.999
7	0.250	78.8	8.49	-0.01	-0.19	0.855	0.000	0.731	0.000	0.857	0.000	-0.012	0.999
8	0.249	78.1	8.49	-0.01	-0.02	C.873	0.000	0.752	C.000	0.875	0.000	-0.021	0.999
9	C.250	78.8	8.49	-0.01	0.14	0.861	0.000	0.741	0.000	0.863	0.000	-0.021	0.999
10	0.250	78.8	8.49	-0.01	0.30	C.888	0.000	0.787	0.000	0.889	0.000	-0.021	0.999
11	0.250	78.8	8.49	-0.01	0.48	C.911	0.000	0.829	0.000	0.912	0.000	-0.021	0.999
12	0.252	79.4	8.49	-0.01	0.65	C.915	0.000	0.837	0.000	0.916	0.000	-0.012	0.999
13	0.252	79.4	8.49	-0.01	0.97	C.959	0.000	0.919	C.000	0.959	0.000	-0.021	0.999
14	0.252	79.4	8.49	-0.01	1.18	C.993	0.000	0.984	0.000	0.993	0.000	-0.017	0.999
15	0.252	79.4	8.49	-0.01	1.48	C.988	0.000	0.976	C.000	0.988	0.000	-0.005	1.000
16	0.250	78.8	8.49	-0.01	1.95	C.994	0.000	0.988	C.000	0.994	0.000	-0.010	1.000

RUN	TST	P	TN	CCNF	MACH	RN/L	PT	G	TT	ALPHA	P	63.1	-20.00
257	571	1	66	5	C.250	1.516	1874	78.8	1794				
SEG	MACH	G	X/DR	Y/DR	Z/DB	MF/N	MA/M	QF/Q	QA/Q	VF/V	VA/V		PF/P
1	0.250	78.8	8.49	-0.26	-2.02	C.988	0.000	0.975	0.000	0.938	0.000	-0.010	1.000
2	0.250	78.8	8.49	-0.36	-1.52	C.951	0.000	0.981	C.000	0.991	0.000	-0.015	0.999
3	0.249	78.1	8.49	-0.36	-1.03	C.954	0.000	0.908	0.000	0.954	0.000	-0.021	0.999
4	0.252	79.4	8.49	-0.36	-0.69	0.914	0.000	0.836	C.000	0.915	0.000	-0.012	0.999
5	0.250	78.8	8.49	-0.36	-0.52	C.898	0.000	0.806	C.000	0.899	0.000	-0.012	0.999
6	0.250	78.8	8.49	-0.36	-0.35	C.875	0.000	0.764	0.000	0.876	0.000	-0.021	0.999
7	0.250	78.8	8.49	-0.36	-0.19	C.889	0.000	0.790	C.000	0.891	0.000	-0.021	0.999
8	0.250	78.8	8.49	-0.36	-0.03	C.898	0.000	0.806	0.000	0.899	0.000	-0.023	0.999
9	0.252	79.4	8.49	-0.36	0.14	C.389	0.000	0.789	0.000	0.890	0.000	-0.021	0.999
10	0.252	79.4	8.49	-0.36	0.31	C.872	0.000	0.761	C.000	0.874	0.000	-0.012	0.999
11	0.252	79.4	8.49	-0.36	0.48	C.920	0.000	0.846	0.000	0.921	0.000	-0.012	0.999
12	0.251	79.4	8.49	-0.36	0.65	C.914	0.000	0.836	C.000	0.915	0.000	-0.012	0.999
13	0.251	79.4	8.49	-0.36	0.98	C.948	0.000	0.898	0.000	0.948	0.000	-0.008	1.000
14	0.248	77.4	8.49	-0.36	1.17	1.001	0.000	1.000	C.000	1.001	0.000	-0.239	0.998
15	C.250	78.8	8.49	-0.36	1.48	0.996	0.000	0.991	0.000	0.996	0.000	-0.015	0.999
16	0.250	78.8	8.49	-0.36	1.98	C.995	0.000	0.989	0.000	0.995	0.000	-0.014	0.999

RUN	TST	P	TA	CCNF	MACH	RN/L	PT	C	P	TT	ALPHA	
SEQ	MACH	0	X/DR	Y/DR	Z/DR	MF/N	MA/M	QF/Q	VA/V	VF/V	CP	PF/P
258	571	1	66	5	0.249	1.51C	1874	78.1	1794	62.9	-20.00	
1	0.249	78.1	8.49	-0.45	-2.03	C.99C	0.000	0.981	0.000	0.990	0.000	-0.007 1.000
2	0.249	78.1	8.49	-0.45	-1.52	C.99C	0.000	0.979	C.000	0.990	0.000	-0.010 1.000
3	0.250	78.8	8.49	-C.45	-1.03	C.964	0.000	0.928	0.000	0.964	0.000	-0.021 0.999
4	0.250	78.8	8.49	-C.45	-0.70	C.894	0.000	C.799	C.000	0.896	0.000	-0.021 0.999
5	0.249	78.1	8.49	-C.45	-0.52	C.879	0.000	C.773	0.000	0.881	0.000	-0.021 0.999
6	0.249	78.1	8.49	-C.45	-0.36	C.882	0.000	C.780	C.000	0.885	0.000	-0.021 0.999
7	0.249	78.1	8.49	-C.45	-0.19	C.918	0.200	C.842	C.000	0.919	0.000	-0.021 0.999
8	0.250	78.8	8.49	-C.45	-0.02	C.918	0.000	C.841	C.000	0.918	0.000	-0.021 0.999
9	0.249	78.1	8.49	-C.45	0.15	C.988	0.000	C.789	C.000	0.890	0.000	-0.021 0.999
10	0.249	78.1	8.49	-C.45	0.31	C.928	0.000	C.861	C.000	0.929	0.000	-0.021 0.999
11	0.250	78.8	8.49	-C.45	0.48	C.927	0.000	C.859	C.000	0.928	0.000	-0.021 0.999
12	0.249	78.1	8.49	-C.45	0.65	C.939	0.000	C.880	C.000	0.939	0.000	-0.012 0.999
13	0.249	78.1	8.49	-C.45	0.98	C.973	0.000	C.945	C.000	0.973	0.000	-0.017 0.999
14	0.249	78.1	8.49	-C.45	1.18	C.988	0.000	C.975	C.000	0.988	0.000	-0.008 1.000
15	0.249	78.1	8.49	-C.45	1.48	C.985	0.000	C.970	C.000	0.985	0.000	-0.003 1.000
16	0.249	78.1	8.49	-C.45	1.98	C.988	0.000	C.975	C.000	0.988	0.000	0.001 1.000

RUN	TST	P	TA	CCNF	MACH	RN/L	PT	G	P	TT	ALPHA	
SEQ	MACH	0	X/DR	Y/DR	Z/DB	MF/N	MA/M	QF/Q	VA/V	VF/V	CP	PF/P
259	571	1	66	5	0.951	1.480	682	241.2	381	66.2	10.00	0.037 1.024
2	0.951	241.2	1C.88	0.41	-2.04	0.971	0.966	0.976	0.000	0.976	0.000	0.041 1.026
3	0.954	242.3	1C.88	C.41	-1.53	C.967	0.959	0.972	0.000	0.972	0.000	0.034 1.021
4	0.954	242.3	1C.88	C.41	-1.04	C.964	0.949	0.969	0.000	0.969	0.000	0.023 1.015
5	0.956	242.8	1C.88	C.41	-0.70	0.919	0.856	0.930	0.000	0.930	0.000	0.024 1.015
6	0.956	242.8	1C.88	C.41	-0.54	C.927	0.873	0.938	0.000	0.938	0.000	0.014 1.009
7	0.955	242.3	1C.88	C.41	-0.37	C.928	0.868	0.938	0.000	0.938	0.000	0.011 1.007
8	0.955	242.3	1C.88	C.41	-0.20	C.918	0.849	0.929	0.000	0.929	0.000	0.002 0.999
9	0.955	242.3	1C.88	C.41	-0.04	C.9C9	0.831	0.921	0.000	0.921	0.000	0.001 1.006
10	0.955	242.3	1C.88	C.41	0.13	C.895	0.805	0.909	0.000	0.909	0.000	0.007 1.005
11	0.955	242.3	1C.88	C.41	0.25	C.876	0.769	0.892	0.000	0.892	0.000	0.005 1.003
12	0.953	241.8	1C.88	C.41	0.46	C.887	0.785	0.902	0.000	0.902	0.000	-0.002 0.999
13	0.953	241.8	1C.88	C.41	0.63	C.866	0.751	0.883	0.000	0.883	0.000	0.001 1.001
14	0.953	241.8	1C.88	C.41	0.96	C.885	0.786	0.900	0.000	0.900	0.000	0.005 1.003
15	0.953	241.8	1C.88	C.41	1.17	C.920	0.851	0.931	0.000	0.931	0.000	0.008 1.005
16	0.953	241.8	1C.88	C.41	1.47	C.953	0.923	0.960	0.000	0.960	0.000	0.025 1.016
17	0.951	241.2	1C.88	C.41	1.96	C.967	0.972	0.972	0.000	0.972	0.000	0.048 1.031

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RUN	TST	P	TN	CCNF	MACH	PN/L	PT	C	P	TT	ALPHA
SFC	MACH	G	X/DR	Y/DR	Z/DR	MF/N	MA/N	QF/Q	QA/Q	VF/V	VA/V
260	571	1	66	5	0.952	1.485	686	242.5	382	67.3	10.00
1	0.952	242.5	1C.88	-C.03	-2.C4	C.890	0.813	0.904	0.877	0.936	0.042
2	0.951	242.4	1C.88	-C.03	-1.55	C.926	C.877	0.928	0.857	0.031	1.027
3	0.951	242.4	1C.88	-C.03	-1.04	C.917	C.824	0.916	0.889	0.020	1.024
4	0.951	242.4	1C.88	-C.C3	-C.70	C.9C2	C.824	0.903	0.903	0.020	1.012
5	0.951	242.4	1C.88	-C.03	-0.54	C.889	C.798	0.903	0.903	0.017	1.C11
6	0.950	241.5	1C.88	-C.C3	-0.38	C.868	C.868	0.885	0.885	0.014	1.009
7	0.950	241.5	1C.88	-C.03	-0.20	C.867	C.756	0.884	0.884	0.009	1.006
8	0.950	241.5	1C.88	-C.03	-0.04	C.858	C.739	0.876	0.876	0.004	1.003
9	0.950	241.5	1C.88	-C.C3	0.13	C.852	C.729	0.871	0.871	0.004	1.003
10	0.950	241.5	1C.88	-C.03	0.30	C.841	C.709	0.860	0.860	0.003	1.002
11	0.950	241.5	1C.88	-C.C2	0.46	C.856	C.732	0.874	0.874	-0.000	1.000
12	0.948	241.5	1C.88	-C.03	0.63	C.838	C.701	0.857	0.857	-0.002	0.999
13	0.948	241.5	1C.88	-C.03	0.96	C.863	C.746	0.880	0.880	0.005	1.003
14	0.948	241.5	1C.88	-C.02	1.16	C.8E5	C.798	0.903	0.903	0.016	1.010
15	0.946	241.1	1C.88	-C.03	1.46	C.929	C.880	0.939	0.939	0.030	1.C19
16	0.946	241.1	1C.88	-C.03	1.96	C.969	C.967	0.974	0.974	0.047	1.029

RUN	TST	P	TN	CCNF	MACH	PN/L	PT	C	P	TT	ALPHA
SFC	MACH	G	X/DR	Y/DR	Z/DR	MF/N	MA/N	QF/Q	QA/Q	VF/V	VA/V
261	571	1	66	5	0.951	1.480	685	242.4	383	68.0	10.00
1	0.951	242.4	1C.88	-C.38	-2.C4	C.962	0.950	0.969	0.959	0.974	0.037
2	0.951	242.4	1C.88	-C.38	-1.54	C.970	C.941	0.969	0.969	0.022	1.014
3	0.951	242.4	1C.88	-C.38	-1.04	C.964	C.872	0.939	0.939	0.031	1.020
4	0.951	242.4	1C.88	-C.38	-0.71	C.929	C.826	0.918	0.918	0.016	1.010
5	0.951	242.4	1C.88	-C.38	-0.54	C.906	C.794	0.903	0.903	0.012	1.007
6	0.951	242.4	1C.88	-C.38	-0.37	C.889	C.788	0.901	0.901	0.008	1.005
7	0.951	242.4	1C.88	-C.38	-0.21	C.887	C.766	0.891	0.891	0.005	1.003
8	0.951	242.4	1C.88	-C.38	-0.C3	C.875	C.766	0.891	0.891	0.002	1.001
9	0.951	242.4	1C.88	-C.38	0.12	C.877	C.769	0.893	0.893	-0.001	1.000
10	0.951	242.4	1C.88	-C.38	0.30	C.871	C.756	0.868	0.868	-0.005	0.997
11	0.951	242.4	1C.88	-C.38	0.46	C.860	C.739	0.878	0.878	-0.002	0.999
12	0.951	242.4	1C.88	-C.38	0.63	C.868	C.755	0.885	0.885	0.002	1.001
13	0.951	242.4	1C.88	-C.38	0.97	C.885	C.784	0.900	0.900	0.002	1.001
14	0.950	241.9	1C.88	-C.38	1.17	C.910	C.834	0.923	0.923	0.010	1.006
15	0.949	241.4	1C.88	-C.38	1.46	C.941	C.902	0.949	0.949	0.031	1.020
16	0.947	241.1	1C.88	-C.38	1.97	C.954	C.942	0.961	0.961	0.055	1.035

RUN	TST	P	TA	CCNF	MACH	RN/L	PT	G	P	TT	ALPHA
SFG	MACH	0	5	0.951	1.478	685	242.4	383	68.6	10.00	PF/P
1	0.951	242.4	1	0.88	-0.48	-2.04	0.969	0.960	0.973	0.036	1.023
2	0.953	242.5	1	0.88	-C.48	-1.55	C.969	0.960	0.974	0.035	1.022
3	0.952	242.3	1	0.88	-C.48	-1.04	C.964	0.944	0.969	0.025	1.016
4	0.954	242.5	1	0.88	-C.48	-0.71	C.915	0.848	0.927	0.019	1.012
5	0.953	242.3	1	0.88	-C.48	-0.54	C.910	0.837	0.922	0.015	1.010
6	0.953	242.3	1	0.88	-C.48	-0.37	C.911	0.834	0.923	0.008	1.005
7	0.953	242.3	1	0.88	-C.48	-0.21	C.905	0.822	0.918	0.004	1.003
8	0.955	242.8	1	0.88	-C.48	-0.04	C.892	0.795	0.906	0.000	1.000
9	0.955	242.8	1	0.88	-C.48	0.13	C.890	0.792	0.905	-0.002	0.999
10	0.955	242.8	1	0.88	-C.48	0.29	0.866	0.749	0.883	-0.003	0.998
11	0.953	242.3	1	0.88	-0.48	0.47	0.864	0.748	0.881	0.005	1.003
12	0.955	243.4	1	0.88	-C.48	0.64	0.862	0.747	0.880	0.007	1.004
13	0.953	242.9	1	0.88	-C.48	0.96	0.888	0.794	0.902	0.012	1.008
14	0.951	242.4	1	0.88	-0.48	1.17	0.909	0.836	0.922	0.017	1.011
15	0.950	242.4	1	0.88	-C.48	1.46	C.950	0.918	0.957	0.028	1.018
16	0.949	242.6	1	0.88	-0.48	1.97	C.966	0.962	0.971	0.050	1.032

RUN	TST	P	TA	CCNF	MACH	RN/L	PT	G	P	TT	ALPHA
SFG	MACH	0	5	0.952	1.474	684	242.3	382	69.4	10.00	PF/P
1	0.952	242.3	1	0.49	-0.43	-2.03	C.973	0.967	0.977	0.032	1.020
2	0.952	242.3	1	0.49	-1.52	C.972	0.964	0.977	0.030	1.019	
3	0.952	242.3	1	0.49	-0.43	-1.03	C.966	0.946	0.971	0.023	1.015
4	0.952	242.3	1	0.49	-0.43	-0.68	C.912	0.841	0.924	0.019	1.012
5	0.951	241.8	1	0.49	-0.43	-0.52	C.928	0.866	0.938	0.008	1.005
6	0.951	241.8	1	0.49	-0.43	-0.35	C.926	0.863	0.936	0.011	1.007
7	0.950	241.8	1	0.49	-C.43	-0.19	C.913	0.838	0.925	0.007	1.005
8	0.949	241.4	1	0.49	-0.43	-0.03	C.896	0.803	0.910	0.002	1.001
9	0.950	241.9	1	0.49	-0.43	0.14	0.869	0.754	0.886	-0.003	0.998
10	0.948	241.5	1	0.49	C.43	0.31	C.856	0.729	0.874	-0.010	0.993
11	0.949	242.0	1	0.49	C.43	0.48	C.852	0.720	0.870	-0.012	0.992
12	0.948	242.0	1	0.49	C.43	0.64	C.866	0.730	0.878	-0.021	0.987
13	0.947	241.6	1	0.49	C.43	0.98	C.914	0.826	0.926	-0.020	0.987
14	0.946	241.1	1	0.49	C.43	1.17	C.952	0.902	0.959	-0.006	0.996
15	0.946	241.1	1	0.49	C.43	1.47	C.968	0.944	0.973	0.012	1.007
16	0.946	241.1	1	0.49	C.43	1.95	C.965	0.965	0.974	0.044	1.027

RUN	TST	P	TN	CCNF	MACH	RN/L	PT	C	P	TT	ALPHA	
SEQ	MACH	G	X/DB	Y/DB	Z/DB	MF/N	MA/N	QA/Q	VF/V	VA/V	CP	PF/P
264	571	1	66	5	0.951	1.482	688	243.5	385	69.6	10.00	
1	0.951	243.5	8.49	-C.01	-2.02	C.993	0.810	0.907	0.938	0.025	1.016	
2	0.951	243.5	8.49	-0.01	-1.54	C.927	C.974	0.861	0.934	0.016	1.010	
3	0.951	243.5	8.49	-0.01	-1.02	0.923	C.838	0.925	0.925	0.006	1.004	
4	0.952	244.0	E.49	-C.01	-C.69	C.914	0.800	0.909	0.893	-0.001	1.000	
5	0.952	244.0	E.49	-0.01	-0.52	0.895	0.766	0.718	0.870	-0.009	0.994	
6	0.952	244.0	E.49	-C.01	-0.36	0.877	0.650	0.688	0.854	-0.015	0.990	
7	0.952	244.0	E.49	-0.01	-0.19	C.851	0.676	0.625	0.820	-0.016	0.990	
8	0.952	244.0	E.49	-C.01	-0.01	0.832	0.691	0.688	0.847	-0.019	0.988	
9	0.951	243.5	E.49	-C.01	0.14	C.827	0.676	0.676	0.887	-0.008	0.995	
10	0.951	243.5	E.49	-C.01	0.31	C.830	0.650	0.625	0.923	0.008	1.005	
11	0.952	244.0	E.49	-C.01	0.47	C.796	0.676	0.625	0.965	0.024	1.015	
12	0.952	244.0	E.49	-C.01	0.65	C.826	0.674	0.674	0.972	0.050	1.031	
13	0.952	244.0	E.49	-C.01	0.98	C.870	0.754	0.754	0.972	0.026	1.031	
14	0.952	244.0	E.49	-C.01	1.18	C.911	0.834	0.834	0.972	0.026	1.031	
15	0.949	243.5	E.49	-C.01	1.48	C.959	0.935	0.935	0.972	0.026	1.031	
16	0.948	242.6	E.49	-C.01	1.98	C.967	0.964	0.964	0.972	0.026	1.031	

RUN	TST	P	TN	CCNF	MACH	RN/L	PT	C	P	TT	ALPHA	
SEQ	MACH	G	X/DR	Y/DR	Z/DR	MF/N	MA/N	QA/Q	VF/V	VA/V	CP	PF/P
265	571	1	66	5	0.951	1.480	688	243.5	385	69.9	10.00	
1	0.951	243.5	8.49	-0.36	-2.03	0.968	C.951	0.972	0.978	0.025	1.016	
2	0.952	243.5	E.49	-0.26	-1.52	C.974	0.964	0.956	0.977	0.026	1.017	
3	0.952	243.5	E.49	-C.26	-1.C3	C.974	C.956	0.977	0.977	0.014	1.009	
4	0.954	244.0	E.49	-0.36	-0.69	C.940	0.886	0.948	0.948	0.005	1.003	
5	0.954	244.0	E.49	-C.36	-0.53	C.914	0.834	0.925	0.925	-0.000	1.000	
6	0.954	244.0	E.49	-0.36	-0.35	C.885	0.782	0.901	0.901	-0.004	0.997	
7	0.954	244.0	E.49	-C.36	-0.19	C.874	0.761	0.890	0.890	-0.004	0.997	
8	0.952	243.5	E.49	-C.36	-0.C2	C.859	0.739	0.877	0.877	-0.018	0.989	
9	0.952	243.5	E.49	-C.36	0.15	C.837	0.692	0.857	0.857	-0.021	0.987	
10	0.952	243.5	E.49	-C.36	0.31	C.818	0.663	0.840	0.840	-0.014	0.991	
11	0.952	243.5	E.49	-C.36	0.48	C.827	0.676	0.848	0.848	-0.019	0.988	
12	0.952	243.5	E.49	-C.36	0.65	C.844	0.705	0.863	0.863	-0.016	0.990	
13	0.950	243.0	E.49	-C.36	0.98	C.895	0.796	0.909	0.909	-0.010	0.994	
14	0.950	243.0	E.49	-C.36	1.18	C.936	0.878	0.945	0.945	0.005	1.003	
15	0.950	243.0	E.49	-C.36	1.48	C.963	0.943	0.969	0.969	0.025	1.016	
16	0.948	242.6	E.49	-C.36	1.98	C.972	0.972	0.972	0.972	0.045	1.028	

RUN	TST	P	TN	CCNF	MACH	RN/L	PT	C	P	TT	ALPHA
SEC	MACH	G	X/DB	Y/DB	Z/DB	MF/N	MA/M	QF/Q	QA/Q	VF/V	VA/V
266	571	1	66	5	0.949	1.479	688	243.0	385	70.1	10.00
1	0.949	243.0	C	X/DB	Y/DB	Z/DB	MF/N	MA/M	QF/Q	QA/Q	VF/V
2	0.949	243.0	C	8.49	-0.45	-2.03	0.972	0.965	0.976	0.978	0.978
3	0.951	243.5	C	8.49	-0.45	-1.52	0.974	0.965	0.976	0.976	0.976
4	0.951	243.5	C	8.49	-0.45	-1.03	0.972	0.956	0.975	0.975	0.975
5	0.951	243.5	C	8.49	-0.45	-0.69	0.932	0.875	0.942	0.942	0.942
6	0.951	243.5	C	8.49	-0.45	-0.52	0.906	0.821	0.918	0.918	0.918
7	0.951	243.5	C	8.49	-0.45	-0.35	0.906	0.819	0.919	0.919	0.919
8	0.952	244.0	C	8.49	-0.45	-0.19	0.986	0.782	0.901	0.901	0.901
9	0.952	244.0	C	8.49	-0.45	-0.02	0.872	0.754	0.889	0.889	0.889
10	0.952	244.0	C	8.49	-0.45	0.14	0.857	0.725	0.875	0.875	0.875
11	0.952	244.0	C	8.49	-0.45	0.31	0.841	0.697	0.861	0.861	0.861
12	0.951	243.5	C	8.49	-0.45	0.48	0.843	0.699	0.863	0.863	0.863
13	0.951	243.5	C	8.49	-0.45	0.65	0.845	0.705	0.864	0.864	0.864
14	0.951	243.5	C	8.49	-0.45	0.98	0.906	0.816	0.919	0.919	0.919
15	0.950	243.0	C	8.49	-0.45	1.18	0.946	0.895	0.954	0.954	0.954
16	0.950	243.0	C	8.49	-0.45	1.47	0.966	0.947	0.971	0.971	0.971

RUN	TST	P	TN	CCNF	MACH	RN/L	PT	C	P	TT	ALPHA
SEC	MACH	G	X/DB	Y/DB	Z/DB	MF/N	MA/M	QF/Q	QA/Q	VF/V	VA/V
267	571	1	66	5	0.901	1.482	703	235.0	415	70.3	10.00
1	0.901	235.9	C	X/DB	Y/DB	Z/DB	MF/N	MA/M	QF/Q	QA/Q	VF/V
2	0.900	235.5	C	1C.88	-C.03	-2.04	0.919	0.871	0.929	0.929	0.929
3	0.897	234.6	C	1C.88	-C.03	-1.04	0.913	0.873	0.932	0.932	0.932
4	0.897	234.7	C	1C.87	-C.03	-0.71	0.885	0.853	0.923	0.923	0.923
5	0.898	235.2	C	1C.88	-C.03	-0.54	0.884	0.798	0.898	0.898	0.898
6	0.899	235.6	C	1C.88	-C.03	-0.38	0.874	0.766	0.889	0.889	0.889
7	0.900	236.0	C	1C.89	-C.03	-0.21	0.861	0.744	0.877	0.877	0.877
8	0.900	235.5	C	1C.88	-C.03	-0.04	0.862	0.744	0.878	0.878	0.878
9	0.901	235.9	C	1C.88	-C.03	0.13	0.848	0.723	0.865	0.865	0.865
10	0.901	235.9	C	1C.88	-C.03	0.29	0.856	0.735	0.872	0.872	0.872
11	0.901	235.9	C	1C.88	-C.03	0.46	0.855	0.733	0.872	0.872	0.872
12	0.902	236.4	C	1C.88	-C.03	0.63	0.861	0.746	0.877	0.877	0.877
13	0.902	236.4	C	1C.88	-C.03	0.96	0.885	0.791	0.899	0.899	0.899
14	0.900	236.0	C	1C.88	-C.03	1.17	0.906	0.832	0.917	0.917	0.917
15	0.900	236.0	C	1C.88	-C.03	1.46	0.951	0.924	0.957	0.957	0.957
16	0.900	236.0	C	1C.88	-C.03	1.97	0.971	0.971	0.975	0.975	0.975

RUN	TST	F	TN	CCNF	MACH	RNL	PT	G	P	TT	ALPHA
SFG	MACH	Q		X/DR	Y/DR	Z/DB	MF/N	QA/Q	VF/V	VA/V	PF/P
268	571	1	66	5	0.902	1.480	702	235.8	414	70.3	10.00
1	0.902	235.8		8.49	-C.C1	-2.C3	C.9C6	0.847	0.917	0.057	1.032
2	0.899	235.0		8.49	-0.01	-1.53	0.911	C.858	0.922	0.058	1.033
3	0.897	234.6		8.49	-C.C1	-1.02	0.923	0.869	0.932	0.038	1.021
4	0.897	234.7		8.49	-0.01	-0.69	0.886	0.802	0.900	0.036	1.020
5	0.897	234.7		8.49	-0.01	-0.52	0.868	0.763	0.883	0.021	1.012
6	0.897	234.7		8.49	-C.C1	-0.36	C.854	0.734	0.870	0.014	1.008
7	0.896	234.8		8.49	-0.01	-0.19	0.838	0.704	0.855	0.007	1.004
8	0.898	235.2		8.49	-C.C1	-0.C2	C.832	0.687	0.850	-0.011	0.994
9	0.900	236.1		8.49	-0.01	0.15	C.816	0.664	0.836	-0.007	0.996
10	0.900	236.1		8.49	-C.C1	0.31	0.795	0.628	0.816	-0.008	0.995
11	0.899	235.6		8.49	-C.C1	0.48	0.818	0.667	0.837	-0.004	0.998
12	0.900	236.0		8.49	-C.01	0.64	C.827	0.681	0.845	-0.005	0.997
13	0.901	235.9		8.49	-C.C1	0.58	C.902	0.813	0.914	-0.001	0.999
14	0.900	235.5		8.49	-0.01	1.18	0.922	0.857	0.932	0.011	1.006
15	0.899	235.0		8.49	-0.01	1.48	C.964	0.943	0.969	0.026	1.015
16	0.899	235.0		8.49	-C.C1	1.98	C.971	0.963	0.975	0.038	1.022

RUN	TST	F	TN	CCNF	MACH	RNL	PT	G	P	TT	ALPHA
SFG	MACH	Q		X/DR	Y/DR	Z/DB	MF/N	QA/Q	VF/V	VA/V	PF/P
269	571	1	66	5	0.853	1.499	727	230.1	452	70.0	10.00
1	0.853	230.1		10.88	-C.03	-2.04	C.9C3	0.835	0.914	0.048	1.024
2	0.852	229.8		1C.88	-C.02	-1.55	C.918	0.861	0.928	0.040	1.020
3	0.852	229.8		1C.88	-0.03	-1.C4	C.916	0.851	0.925	0.030	1.015
4	0.850	229.4		1C.88	-C.03	-0.71	0.891	0.803	0.903	0.024	1.012
5	0.850	229.4		1C.88	-C.C2	-0.53	C.872	0.769	0.885	0.025	1.013
6	0.849	229.1		10.89	-0.03	-0.38	C.864	0.753	0.878	0.017	1.009
7	0.849	229.1		1C.88	-C.C3	-0.20	C.856	0.739	0.871	0.014	1.007
8	0.849	229.1		1C.88	-C.C3	-0.C3	C.85C	0.726	0.865	0.012	1.006
9	0.849	229.1		1C.88	-0.03	0.13	C.853	0.732	0.868	0.010	1.005
10	0.849	229.1		1C.88	-C.C3	0.29	0.858	0.738	0.872	0.008	1.004
11	0.849	229.1		1C.88	-0.03	0.46	C.844	0.716	0.859	0.012	1.006
12	0.849	229.1		1C.88	-C.C3	0.63	C.855	0.737	0.870	0.015	1.008
13	0.848	228.6		10.88	-C.C3	0.56	C.9C1	0.821	0.912	0.021	1.010
14	0.848	228.6		1C.88	-0.03	1.16	C.934	0.880	0.941	0.019	1.010
15	0.849	229.1		1C.88	-C.C3	1.46	C.966	0.944	0.970	0.024	1.012
16	0.850	229.4		1C.88	-0.03	1.97	C.976	0.969	0.979	0.034	1.017

RUN	TST	P	TN	CENF	MACH	PNL	PT	G	P	TT	ALPHA
SFC										10.00	
					X/DP	Y/DP	Z/DP	MF/N	MA/M	QA/Q	VF/V
270	571	1	66	5	0.854	1.500	727	230.5	451	70.0	
	MACH	G			X/DP	Y/DP	Z/DP	MF/N	MA/M	QA/Q	VF/V
1	0.854	230.5			8.49	-0.01	-2.02	0.9C8	0.836	0.918	0.028
2	0.854	230.C			8.49	-0.01	-1.53	C.914	0.851	0.924	0.035
3	0.850	228.9			8.49	-0.01	-1.03	C.912	0.847	0.922	0.037
4	0.850	229.C			8.49	-C.C1	-0.69	C.88C	0.788	0.893	0.036
5	0.848	228.7			8.49	-0.01	-0.53	C.86C	0.747	0.874	0.020
6	0.848	228.7			8.49	-0.01	-0.26	C.846	0.721	0.862	0.014
7	0.849	229.1			8.49	-C.C1	-0.19	C.82C	0.701	0.852	0.008
8	0.849	229.1			8.49	-C.C1	-0.02	0.941	0.704	0.857	0.008
9	0.850	229.5			8.49	-C.C1	0.14	C.819	0.668	0.836	-0.005
10	0.850	229.4			8.49	-0.01	0.32	C.812	0.657	0.831	-0.011
11	C.850	229.4			8.49	-C.C1	0.48	0.826	0.680	0.843	-0.005
12	0.850	229.4			8.49	-0.01	0.64	C.848	0.717	0.863	-0.004
13	0.852	229.E			8.49	-C.C1	0.98	C.913	0.838	0.922	0.012
14	0.852	229.E			8.49	-C.C1	1.17	C.95C	0.910	0.956	0.018
15	0.852	229.E			8.49	-0.01	1.48	C.968	0.951	0.972	0.029
16	C.852	229.E			8.49	-0.01	1.98	C.977	0.972	0.980	0.034

RUN	TST	P	TN	CENF	MACH	PNL	PT	G	P	TT	ALPHA
SFC										10.00	
					X/DP	Y/DP	Z/DP	MF/N	MA/M	QA/Q	VF/V
271	571	1	66	5	0.8C2	1.519	757	222.5	495	69.7	
	MACH	G			X/DP	Y/DP	Z/DP	MF/N	MA/M	QA/Q	VF/V
1	0.803	223.5			1C.88	0.41	-2.C4	C.976	0.969	0.979	0.038
2	0.801	223.C			1C.88	0.41	-1.54	0.98C	0.975	0.983	0.030
3	0.801	223.C			1C.88	C.41	-1.04	0.974	0.959	0.977	0.023
4	0.801	223.0			1C.88	C.41	-0.72	C.919	0.854	0.927	0.026
5	0.801	223.C			1C.88	C.41	-0.54	C.922	0.857	0.930	0.020
6	0.801	223.C			1C.88	C.41	-0.27	C.923	0.853	0.931	0.006
7	0.801	223.0			1C.88	0.41	-0.21	C.918	0.845	0.926	0.006
8	0.803	223.5			1C.88	0.41	-0.04	0.896	0.807	0.907	0.010
9	0.801	223.0			1C.88	0.41	0.13	0.898	0.810	0.908	0.009
10	0.801	223.C			1C.88	0.41	0.29	C.884	0.783	0.895	0.003
11	0.802	223.5			1C.88	C.41	0.47	C.9C3	0.818	0.913	0.006
12	0.802	223.5			1C.88	0.41	0.63	C.89C	0.805	0.907	0.004
13	0.802	223.5			1C.88	C.41	0.97	C.933	0.876	0.940	0.016
14	0.802	223.5			1C.88	C.41	1.16	C.95C	0.912	0.955	0.023
15	0.800	222.5			1C.88	0.41	1.47	C.973	0.957	0.976	0.023
16	C.800	222.5			1C.88	C.41	1.96	C.977	0.970	0.980	0.036

RUN	T	S	T	N	C	MACH	P	N/L	PT	G	TT	ALPHA
272	571	1	66	5	0.800	1.516	757	222.5	497	69.6	10.00	PF/P
SFC	MACH	Q	X/DB	Y/DB	Z/DB	MF/N	MA/M	CF/Q	QA/Q	VF/V	VAV	CP
1	0.800	222.5	1C.88	-C.02	-2.C4	0.898	0.818	0.908	0.908	0.922	0.922	0.025 1.C11
2	0.799	222.6	1C.88	-0.03	-1.54	0.913	0.842	0.853	0.853	0.929	0.929	0.013 1.006
3	0.800	222.5	1C.88	-0.03	-1.04	0.921	0.853	0.877	0.877	0.911	0.911	0.013 1.006
4	0.800	222.5	1C.88	-0.03	-0.71	0.901	0.817	0.838	0.838	0.902	0.902	0.006 1.C02
5	0.800	222.5	1C.88	-0.03	-0.55	0.891	0.797	0.835	0.835	0.886	0.886	-0.001 1.000
6	0.801	223.0	1C.88	-0.03	-0.37	0.874	0.763	0.833	0.833	0.886	0.886	-0.003 0.999
7	0.801	223.0	1C.88	-0.03	-0.20	0.871	0.757	0.833	0.833	0.886	0.886	-0.003 0.999
8	0.801	223.0	1C.88	-0.03	-0.04	0.851	0.725	0.865	0.865	0.886	0.886	0.003 1.001
9	0.801	223.0	1C.88	-0.03	0.14	0.861	0.742	0.874	0.874	0.886	0.886	0.003 1.001
10	0.802	223.0	1C.88	-0.03	0.29	0.866	0.753	0.879	0.879	0.886	0.886	0.009 1.004
11	0.802	223.0	1C.88	-0.03	0.46	0.865	0.752	0.878	0.878	0.886	0.886	0.010 1.004
12	0.800	222.5	1C.88	-0.03	0.63	0.863	0.749	0.876	0.876	0.886	0.886	0.010 1.005
13	0.800	222.5	1C.88	-0.03	0.96	0.910	0.834	0.919	0.919	0.920	0.920	0.014 1.006
14	0.800	222.5	1C.88	-0.03	1.17	0.979	0.985	0.985	0.985	0.945	0.945	0.012 1.005
15	0.802	223.0	1C.88	-0.03	1.47	0.966	0.942	0.969	0.969	0.923	0.923	0.023 1.010
16	0.801	222.4	1C.88	-0.03	1.97	0.978	0.978	0.981	0.981	0.932	0.932	0.032 1.015

RUN	T	S	T	N	C	MACH	P	N/L	PT	G	TT	ALPHA
273	571	1	66	5	0.798	1.516	757	222.0	498	69.3	10.00	PF/P
SFC	MACH	Q	X/DB	Y/DB	Z/DB	MF/N	MA/M	CF/Q	QA/Q	VF/V	VAV	CP
1	0.798	222.0	1C.88	-0.38	-2.04	0.985	0.980	0.987	0.987	0.987	0.987	0.021 1.009
2	0.799	222.0	1C.88	-0.38	-1.54	0.980	0.971	0.983	0.983	0.987	0.987	0.022 1.010
3	0.799	222.0	1C.88	-0.38	-1.04	0.970	0.948	0.973	0.973	0.987	0.987	0.017 1.008
4	0.800	222.5	1C.88	-0.38	-0.71	0.911	0.840	0.920	0.920	0.987	0.987	0.025 1.C11
5	0.800	222.5	1C.88	-0.38	-0.54	0.889	0.795	0.900	0.900	0.987	0.987	0.014 1.006
6	0.800	222.5	1C.88	-0.38	-0.37	0.880	0.778	0.892	0.892	0.900	0.900	0.009 1.004
7	0.800	222.5	1C.88	-0.38	-0.21	0.881	0.778	0.892	0.892	0.900	0.900	0.006 1.003
8	0.800	222.5	1C.88	-0.38	-0.04	0.878	0.771	0.889	0.889	0.900	0.900	0.001 1.001
9	0.800	222.5	1C.88	-0.38	0.13	0.857	0.736	0.871	0.871	0.900	0.900	0.003 1.001
10	0.801	223.0	1C.88	-0.38	0.29	0.874	0.765	0.886	0.886	0.900	0.900	0.003 1.001
11	0.801	223.0	1C.88	-0.38	0.47	0.876	0.770	0.888	0.888	0.900	0.900	0.006 1.003
12	0.801	223.0	1C.88	-0.38	0.63	0.888	0.792	0.899	0.899	0.900	0.900	0.010 1.005
13	0.801	223.0	1C.88	-0.38	0.97	0.920	0.855	0.923	0.923	0.923	0.923	0.020 1.009
14	0.800	222.5	1C.88	-0.38	1.16	0.943	0.897	0.949	0.949	0.949	0.949	0.018 1.008
15	0.800	222.5	1C.88	-0.38	1.47	0.974	0.969	0.977	0.977	0.977	0.977	0.027 1.012
16	0.800	222.5	1C.88	-0.38	1.96	0.979	0.971	0.982	0.982	0.982	0.982	0.029 1.C13

RUN	TSI	P	TIN	CCLNF	MACH	RN/L	PT	G	P	TT	ALPHA
SFC	MACH	G	X/DR	Y/DR	Z/DR	MF/N	MA/M	CF/Q	QA/Q	VF/V	VA/V
274	571	1	66	5	0.799	1.519	758	222.6	498	69.1	10.00
1	0.799	222.6	1C.88	-C.48	-2.04	0.979	0.972	0.981	0.032	1.C14	
2	0.798	222.0	1C.88	-C.48	-1.54	C.981	0.974	0.983	0.028	1.012	
3	0.800	222.5	1C.88	-C.48	-1.04	C.962	0.936	0.967	0.020	1.009	
4	0.799	222.0	1C.88	-C.48	-0.71	C.917	0.844	0.925	0.011	1.005	
5	0.799	222.0	1C.88	-C.48	-0.54	C.898	0.810	0.908	0.011	1.005	
6	0.800	222.5	1C.88	-C.48	-0.38	0.892	0.799	0.903	0.010	1.005	
7	0.801	223.0	1C.88	-C.48	-0.21	C.886	0.786	0.897	0.003	1.001	
8	0.801	223.0	1C.88	-C.48	-0.04	C.882	0.781	0.894	0.006	1.003	
9	0.801	223.0	1C.88	-C.48	0.13	0.877	0.773	0.889	0.010	1.005	
10	0.801	223.0	1C.88	-C.48	0.29	0.874	0.766	0.886	0.004	1.002	
11	0.801	223.0	1C.88	-C.48	0.46	0.883	0.782	0.894	0.006	1.003	
12	0.801	223.0	1C.88	-C.48	0.63	C.890	0.796	0.901	0.009	1.004	
13	0.801	223.0	1C.88	-C.48	0.96	C.928	0.869	0.936	0.020	1.009	
14	0.801	223.0	1C.88	-C.48	1.17	C.951	0.913	0.956	0.020	1.009	
15	0.802	223.5	1C.88	-C.48	1.47	C.972	C.956	0.975	0.026	1.012	
16	0.801	223.0	1C.88	-C.48	1.97	0.979	0.972	0.981	0.031	1.C14	

RUN	TSI	P	TIN	CCLNF	MACH	RN/L	PT	G	P	TT	ALPHA
SFC	MACH	G	X/DR	Y/DR	Z/DR	MF/N	MA/M	CF/Q	QA/Q	VF/V	VA/V
275	571	1	66	5	0.800	1.518	757	222.5	497	69.1	10.00
1	0.800	222.5	8.49	C.43	-2.03	C.986	0.980	0.987	0.020	1.009	
2	0.800	222.5	8.49	0.43	-1.52	C.985	C.980	0.986	0.023	1.010	
3	0.801	223.0	8.49	0.43	-1.03	C.980	0.968	0.982	0.016	1.007	
4	0.801	223.0	8.49	C.43	-0.70	C.922	0.854	0.930	0.012	1.005	
5	0.800	222.5	8.49	0.43	-0.52	0.925	0.860	0.933	0.011	1.005	
6	0.800	222.5	8.49	0.43	-0.35	C.919	0.848	0.927	0.009	1.004	
7	0.803	223.5	8.49	0.43	-0.19	C.903	0.815	0.913	-0.003	0.999	
8	0.803	223.5	8.49	0.43	-0.01	C.880	0.775	0.892	0.001	1.000	
9	0.801	223.0	8.49	C.43	0.14	C.864	0.751	0.876	0.015	1.007	
10	0.801	223.0	8.49	C.43	0.31	C.870	0.759	0.882	0.007	1.003	
11	0.800	222.5	8.49	C.43	0.48	C.874	0.766	0.886	0.004	1.002	
12	0.800	222.5	8.49	C.43	0.64	C.899	0.811	0.909	0.008	1.004	
13	0.798	222.0	8.49	0.43	0.98	0.948	0.903	0.954	0.009	1.004	
14	0.799	222.6	8.49	C.42	1.19	C.957	0.924	0.961	0.020	1.009	
15	0.799	222.6	8.49	0.43	1.47	C.976	0.963	0.979	0.023	1.C10	
16	0.799	222.6	8.49	C.43	1.98	0.979	0.973	0.982	0.032	1.014	

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RUN	TST	P	TN	CCNF	MACH	RN/L	PT	C	P	TT	ALPHA
SEQ										10.00	
SFQ	MACH	0	0	0	C.8C2	1.513	754	222.3	493	69.2	PF/P
276	571	1	66		X/DR	Y/DB	Z/DR	MF/N	QA/Q	VF/V	CP
1	0	8C2	222.3	8.49	-C.C1	-2.02	C.8SC	0.802	0.900	0.029	1.013
2	0	801	221.8	8.49	-0.01	-1.52	C.9C6	0.830	0.915	0.028	1.C13
3	0	801	221.8	8.49	-0.01	-1.03	0.916	0.848	0.924	0.024	1.C11
4	0	8C1	221.8	8.49	-0.01	-0.69	C.893	0.803	0.903	0.015	1.C07
5	C.	801	221.8	8.49	-0.01	-0.53	0.864	0.748	0.877	0.006	1.003
6	0	801	221.8	8.49	-C.C1	-0.36	C.850	0.724	0.864	0.004	1.002
7	C.	8C1	221.8	8.49	-0.01	-0.19	C.833	0.696	0.847	0.009	1.004
8	0	8C0	221.2	8.49	-C.C1	-0.02	C.824	0.679	0.839	0.003	1.001
9	0	800	221.2	8.49	-0.01	0.14	C.838	0.700	0.853	-0.007	0.597
10	C.	800	221.2	8.49	-C.C1	-0.31	C.832	0.691	0.847	-0.006	0.997
11	0	800	221.2	8.49	-C.C1	0.47	C.839	0.704	0.854	-0.003	0.999
12	C.	8C0	221.2	8.49	-0.01	0.65	C.849	0.722	0.863	0.001	1.001
13	0	800	221.2	8.49	-0.01	0.97	C.915	0.842	0.924	0.012	1.005
14	C.	800	221.2	8.49	-0.01	1.18	C.947	0.904	0.953	0.016	1.007
15	0	800	221.2	8.49	-C.C1	1.48	C.976	0.963	0.979	0.025	1.C11
16	0	800	221.2	8.49	-C.C1	1.98	0.978	0.972	0.981	0.034	1.015

RUN	TST	P	TN	CCNF	MACH	RN/L	PT	C	P	TT	ALPHA
SEQ										10.00	
SFQ	MACH	0	0	0	C.801	1.512	754	221.8	494	69.1	PF/P
277	571	1	66		X/DR	Y/DB	Z/DR	MF/N	QA/Q	VF/V	CP
1	0	801	221.8	8.49	-0.26	-2.C2	0.979	0.971	0.982	0.029	1.013
2	0	8C1	221.8	8.49	-0.36	-1.52	C.976	0.965	0.979	0.030	1.C13
3	0	801	221.8	8.49	-C.C6	-1.C2	C.973	0.952	0.976	0.013	1.006
4	0	8C2	222.3	8.49	-0.36	-0.69	0.919	0.846	0.926	0.008	1.003
5	0	8C2	222.3	8.49	-C.C6	-0.51	0.886	0.785	0.897	-0.000	1.000
6	0	804	222.8	8.49	-0.36	-0.36	0.859	0.739	0.872	0.006	1.003
7	C.	8C1	221.8	8.49	-C.C6	-0.18	0.844	0.710	0.858	-0.006	0.997
8	0	801	221.8	8.49	-C.C6	-0.C3	C.847	0.715	0.861	-0.006	0.997
9	0	8C4	222.8	8.49	-0.36	0.14	0.854	0.727	0.867	-0.005	0.998
10	0	804	222.8	8.49	-C.C6	0.32	C.827	0.698	0.852	-0.009	0.996
11	0	804	222.8	8.49	-C.C6	0.48	0.847	0.718	0.861	0.004	1.C02
12	0	802	222.3	8.49	-0.26	0.64	0.873	0.764	0.885	0.009	1.004
13	0	802	222.2	8.49	-C.C6	0.99	C.935	0.879	0.942	0.013	1.006
14	C.	802	222.3	8.49	-0.36	1.19	C.951	0.912	0.956	0.020	1.C09
15	0	801	221.8	8.49	-C.C6	1.48	0.980	0.971	0.982	0.027	1.C12
16	0	801	221.8	8.49	-C.C6	1.98	0.979	0.972	0.981	0.032	1.C15

RUN	TST	P	TN	C	MACH	RN/L	PT	G	P	TT	ALPHA
					X/DR	Y/DR	Z/DR	MF/N	MA/M	10.00	
SFC					QA/Q	VF/V	VA/V	CP	PF/P		
278	571	1	66	5	0.800	1.510	753	221.3	494	69.1	
	MACH	C									
1	C.	800	221.3	8.49	-0.45	-2.03	0.977	0.969	0.980	0.034	1.015
2	C.	800	221.3	8.49	-0.45	-1.52	0.983	0.977	0.985	0.025	1.011
3	0.	800	221.3	8.49	-0.45	-1.03	0.974	0.957	0.977	0.020	1.009
4	0.	801	221.8	8.49	-0.45	-0.69	0.916	0.844	0.925	0.013	1.006
5	0.	801	221.8	8.49	-0.45	-0.52	0.889	0.793	0.900	0.006	1.003
6	0.	801	221.8	8.49	-0.45	-0.35	0.883	0.781	0.894	0.001	1.001
7	0.	803	222.3	8.49	-0.45	-0.18	0.865	0.748	0.878	-0.000	1.000
8	0.	803	222.3	8.49	-0.45	-0.02	0.949	0.719	0.862	-0.002	0.999
9	0.	803	222.3	8.49	-0.45	0.14	0.855	0.729	0.868	-0.006	0.997
10	0.	803	222.3	8.49	-0.45	0.30	0.857	0.732	0.870	-0.006	0.997
11	0.	803	222.3	8.49	-0.45	0.48	0.871	0.761	0.884	0.006	1.003
12	0.	803	222.3	8.49	-0.45	0.65	0.881	0.778	0.892	0.005	1.002
13	0.	803	222.3	8.49	-0.45	0.98	0.944	0.897	0.950	0.016	1.007
14	0.	804	222.8	8.49	-0.45	1.18	0.963	0.935	0.967	0.019	1.009
15	0.	802	222.3	8.49	-0.45	1.44	0.978	0.968	0.981	0.026	1.012
16	0.	802	222.3	8.49	-0.45	1.99	0.979	0.972	0.981	0.031	1.014

RUN	TST	P	TN	C	MACH	RN/L	PT	G	P	TT	ALPHA
					X/DR	Y/DR	Z/DR	MF/N	MA/M	10.00	
SFC					QA/Q	VF/V	VA/V	CP	PF/P		
279	571	1	66	5	0.598	1.508	896	176.0	C	67.8	
	MACH	C									
1	0.	598	176.0	C	1C.88	0.41	-2.04	C.978	0.965	0.980	0.033
2	0.	598	176.0	C	1C.88	0.41	-1.54	C.981	C.969	0.982	0.027
3	0.	598	176.0	C	1C.88	0.41	-1.04	C.965	0.937	0.967	0.028
4	0.	598	176.0	C	1C.88	0.41	-0.71	C.933	0.874	0.937	0.015
5	0.	598	176.0	C	1C.88	0.41	-0.54	C.930	0.867	0.934	0.010
6	0.	599	176.0	C	1C.88	0.41	-0.38	C.919	0.846	0.923	0.009
7	0.	598	176.0	C	1C.88	0.41	-0.20	C.927	0.861	0.931	0.010
8	0.	598	176.0	C	1C.88	0.41	-0.04	C.906	0.822	0.911	0.008
9	0.	599	176.0	C	1C.88	0.41	0.13	C.894	0.801	0.900	0.012
10	0.	599	176.0	C	1C.88	0.41	0.29	C.908	0.825	0.913	0.008
11	0.	599	176.0	C	1C.88	0.41	0.46	C.899	0.812	0.905	0.016
12	0.	598	176.0	C	1C.88	0.41	0.63	C.913	C.834	0.918	0.006
13	0.	599	176.0	C	1C.88	0.41	0.96	C.930	0.868	0.934	0.017
14	0.	599	176.0	C	1C.88	0.41	1.17	C.946	0.902	0.950	0.028
15	0.	600	177.2	C	1C.88	0.41	1.46	C.979	0.963	0.981	0.019
16	C.	600	177.2	C	1C.88	0.41	1.97	C.978	0.964	0.979	0.029

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RUN	TST	P	TN	CCNF	MACH	RN/L	PT	G	P	TT	10.00	ALPHA	
SFC	MACH	Q	X/DB	Y/DB	Z/DB	MF/N	MA/M	QF/Q	QA/Q	VF/V	V A/V	CP	PF/P
280	571	1	66	5	C.600	1.516	896	177.2	703	67.2			
	SFC	MACH	Q	X/DB	Y/DB	Z/DB	MF/N	MA/M	QF/Q	QA/Q	VF/V	V A/V	CP
1	0.600	177.2	1C.88	-0.03	-2.04	C.913	C.840	0.919				0.027	1.007
2	0.599	176.6	1C.88	-0.03	-1.55	C.930	0.868	0.935				0.009	1.002
3	0.599	176.6	1C.88	-C.03	-1.04	0.929	0.866	0.934				0.008	1.002
4	0.602	177.8	1C.88	-0.03	-0.71	0.901	0.816	0.907				0.019	1.005
5	0.602	177.8	1C.88	-C.03	-0.54	C.901	0.812	0.907				0.000	1.000
6	0.603	178.4	1C.88	-0.03	-0.37	C.875	0.768	0.882				0.016	1.004
7	0.602	177.8	1C.88	-0.03	-0.21	C.869	0.758	0.876				0.015	1.004
8	0.602	177.8	1C.88	-C.03	-0.03	C.872	0.765	0.880				0.017	1.004
9	0.602	177.8	1C.88	-C.03	0.13	C.882	C.780	0.889				0.008	1.002
10	0.602	177.8	1C.88	-C.03	0.30	C.893	0.798	0.899				0.004	1.001
11	0.602	177.8	1C.88	-0.03	0.46	C.880	0.777	0.867				0.015	1.004
12	0.602	177.8	1C.88	-0.03	0.64	C.891	0.796	0.897				0.011	1.003
13	0.603	178.4	1C.88	-C.03	0.96	C.912	C.836	0.917				0.019	1.005
14	0.602	177.8	1C.38	-0.03	1.16	C.946	0.900	0.950				0.019	1.005
15	0.603	178.4	1C.88	-C.03	1.46	C.967	0.941	0.970				0.020	1.005
16	0.603	178.4	1C.88	-C.03	1.96	C.972	C.954	0.974				0.036	1.009

RUN	TST	P	TN	CCNF	MACH	RN/L	PT	G	P	TT	10.00	ALPHA	
SFC	MACH	Q	X/DB	Y/DB	Z/DB	MF/N	MA/M	QF/Q	QA/Q	VF/V	V A/V	CP	PF/P
281	571	1	66	5	0.599	1.514	896	176.6	703	66.8			
	SFC	MACH	Q	X/DB	Y/DB	Z/DB	MF/N	MA/M	QF/Q	QA/Q	VF/V	V A/V	CP
1	0.599	176.6	1C.88	-0.38	-2.04	C.979	0.966	0.931				0.028	1.007
2	0.602	177.8	1C.88	-C.38	-1.54	C.984	0.971	0.985				0.014	1.004
3	0.602	177.8	1C.88	-0.38	-1.05	C.941	0.891	0.945				0.024	1.006
4	0.601	177.2	1C.88	-C.38	-0.71	C.914	0.838	0.919				0.012	1.003
5	0.602	177.8	1C.88	-C.38	-C.54	C.904	0.819	0.910				0.008	1.002
6	0.601	177.2	1C.88	-0.38	-0.37	C.878	0.773	0.885				0.015	1.004
7	0.602	177.8	1C.88	-C.38	-0.22	C.886	0.787	0.893				0.008	1.002
8	0.602	177.8	1C.88	-C.38	-0.05	C.864	0.751	0.871				0.026	1.007
9	0.603	178.4	1C.88	-C.38	0.12	C.885	0.786	0.892				0.012	1.003
10	0.603	178.4	1C.88	-C.38	0.31	C.881	0.782	0.888				0.027	1.007
11	0.603	178.4	1C.88	-C.38	0.47	C.889	0.792	0.896				0.007	1.002
12	0.602	177.8	1C.88	-C.38	0.64	C.902	0.816	0.906				0.008	1.002
13	0.601	177.2	1C.88	-C.38	0.99	C.934	0.873	0.938				0.007	1.002
14	0.601	177.2	1C.88	-C.38	1.17	C.949	0.901	0.952				0.004	1.001
15	0.602	177.8	1C.88	-C.38	1.46	C.973	0.954	0.975				0.029	1.007
16	0.602	177.8	1C.88	-C.38	1.96	C.979	0.967	0.981				0.032	1.008

RUN	TST	P	TN	CCNF	MACH	PN/L	PT	C	P	TT	ALPHA			
SFG	MACH	G		X/DB	Y/DB	Z/DB	MF/N	MA/M	QF/Q	QA/Q	VF/V	VA/V	CP	PF/P
282	571	1	66	0.6C4	1.517	891	177.7	696	66.1	10.00	0.949	0.970	0.051	1.013
2	0.604	177.7	1C.87	-C.48	-2.04	C.968	C.974	C.957	0.976	0.970	0.035	1.009	0.026	1.007
3	0.601	176.5	1C.87	-C.48	-1.54	C.974	C.977	0.962	0.927	0.960	0.022	1.005	0.013	1.003
4	0.600	175.9	1C.88	-C.48	-1.04	C.960	C.974	C.953	0.914	0.912	0.009	1.002	0.010	1.003
5	0.600	175.9	1C.88	-C.48	-0.70	C.905	C.900	C.906	0.906	0.904	0.007	1.002	0.007	1.002
6	0.598	175.3	1C.88	-C.48	-0.53	C.900	C.900	C.898	0.895	0.894	0.009	1.001	0.009	1.001
7	0.598	175.3	1C.88	-C.48	-0.37	C.898	C.895	C.884	0.883	0.882	0.007	1.001	0.007	1.001
8	0.598	175.3	1C.88	-C.48	-0.20	C.895	C.895	C.890	0.888	0.887	0.007	1.001	0.007	1.001
9	0.598	175.3	1C.88	-C.48	-0.05	C.882	C.882	C.881	0.880	0.879	0.007	1.000	0.007	1.000
10	0.600	175.9	1C.88	-C.48	0.12	C.899	C.899	C.895	0.895	0.895	0.007	1.000	0.007	1.000
11	0.600	175.9	1C.88	-C.48	0.29	C.888	C.888	C.884	0.884	0.884	0.007	1.002	0.007	1.002
12	0.600	175.9	1C.88	-C.48	0.47	C.895	C.895	C.893	0.891	0.891	0.005	1.001	0.004	1.001
13	0.600	175.9	1C.88	-C.48	0.63	C.908	C.908	C.914	0.914	0.914	0.004	1.001	0.004	1.001
14	0.600	175.9	1C.88	-C.48	0.96	C.925	C.925	C.930	0.930	0.930	0.022	1.005	0.023	1.006
15	0.600	175.9	1C.88	-C.48	1.17	C.946	C.946	C.949	0.949	0.949	0.033	1.008	0.033	1.008
16	0.600	175.9	1C.88	-C.48	1.48	C.967	C.967	C.969	0.969	0.969	0.016	1.004	0.016	1.004
17	0.6C2	177.1	1C.88	-C.48	1.96	C.987	C.987	C.979	0.979	0.979				

RUN	TST	P	TN	CCNF	MACH	PN/L	PT	C	P	TT	ALPHA			
SFG	MACH	G		X/DB	Y/DB	Z/DB	MF/N	MA/M	QF/Q	QA/Q	VF/V	VA/V	CP	PF/P
283	571	1	66	0.599	1.509	896	176.6	703	68.1	10.00	0.975	0.986	0.019	1.005
1	0.599	176.6	8.49	0.43	-2.03	C.985	C.983	C.971	0.984	0.984	0.022	1.005	0.009	1.002
2	0.600	177.2	8.49	0.43	-1.53	C.983	C.975	C.953	0.977	0.977	0.011	1.003	0.011	1.003
3	0.600	177.2	8.49	0.43	-1.03	C.975	C.969	C.858	0.929	0.929	0.004	1.001	0.004	1.001
4	0.602	177.8	8.49	0.43	-0.69	C.925	C.925	C.854	0.928	0.928	0.002	1.001	0.006	1.001
5	0.602	177.8	8.49	0.43	-0.53	C.924	C.924	C.835	0.919	0.919	0.006	1.001	0.006	1.001
6	0.603	178.4	8.49	0.43	-0.35	C.914	C.914	C.816	0.816	0.816	0.004	0.999	0.004	0.999
7	0.602	177.8	8.49	0.43	-0.19	C.903	C.903	C.816	0.809	0.809	0.003	1.001	0.003	1.001
8	0.602	177.8	8.49	0.43	-0.02	C.904	C.904	C.816	0.793	0.793	-0.004	0.999	0.004	0.999
9	0.602	177.8	8.49	0.43	0.14	C.900	C.900	C.808	0.808	0.808	-0.015	0.996	-0.015	0.996
10	0.602	177.8	8.49	0.43	0.31	C.893	C.893	C.795	0.795	0.795	-0.009	0.998	-0.009	0.998
11	0.602	177.8	8.49	0.43	0.48	C.890	C.890	C.793	0.793	0.793	-0.003	1.001	-0.003	1.001
12	0.602	177.8	8.49	0.43	0.65	C.904	C.904	C.816	0.910	0.910	-0.004	0.999	-0.004	0.999
13	0.601	177.2	8.49	0.43	0.98	C.957	C.957	C.916	0.916	0.916	-0.004	0.999	-0.004	0.999
14	0.602	177.8	8.49	0.43	1.18	C.975	C.975	C.953	0.953	0.953	-0.009	1.002	-0.009	1.002
15	0.602	177.8	8.49	0.43	1.48	C.979	C.979	C.963	0.963	0.963	-0.019	1.005	-0.019	1.005
16	0.603	178.4	8.49	0.43	1.95	C.981	C.981	C.967	0.967	0.967	-0.021	1.005	-0.021	1.005

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RUN	TST	P	TN	CCNF	MACH	RNL	PT	C	P	TT	ALPHA
SFC					X/DR	Y/DR	Z/DR	MF/N	MA/M	QF/Q	PF/P
284	571	1	66	5	0.602	1.512	896	177.8	701	68.8	10.00
1	0.6C2	177.8			8.49	-0.01	-2.03	0.901	0.819	0.907	0.031 1.008
2	0.6C1	177.2			8.49	-0.01	-1.53	0.920	0.850	0.925	0.015 1.004
3	0.601	177.2			8.49	-0.01	-1.02	0.922	0.852	0.926	0.014 1.003
4	0.601	177.2			8.49	-0.01	-0.69	0.895	0.801	0.901	0.002 1.000
5	0.601	177.2			8.49	-C-CI	-0.53	0.875	0.764	0.882	-0.011 0.997
6	0.602	177.8			8.49	-0.C1	-0.36	0.857	0.733	0.864	-0.004 0.999
7	0.6C2	177.8			8.49	-C-CI	-0.19	0.859	0.738	0.867	-0.002 0.999
8	0.601	177.2			8.49	-0.01	-0.02	0.850	0.721	0.858	-0.007 0.998
9	0.602	177.8			8.49	-0.01	0.15	0.850	0.721	0.858	-0.004 0.999
10	0.602	177.8			8.49	-0.C1	0.31	0.852	0.727	0.861	-0.001 1.000
11	0.6C2	177.8			8.49	-0.01	0.48	0.863	0.746	0.870	0.005 1.001
12	0.6C1	177.2			8.49	-C-CI	0.64	0.879	0.771	0.886	-0.006 0.998
13	0.601	177.2			8.49	-0.01	0.99	0.939	0.879	0.942	-0.008 0.998
14	0.6C1	177.2			8.49	-C-CI	1.18	0.956	0.916	0.959	0.007 1.002
15	0.602	177.8			8.49	-C-CI	1.48	0.977	0.959	0.979	0.018 1.005
16	0.6C2	177.8			8.49	-0.01	1.98	0.980	0.966	0.981	0.023 1.006

RUN	TST	P	TN	CCNF	MACH	RNL	PT	C	P	TT	ALPHA
SFC					X/DR	Y/DR	Z/DR	MF/N	MA/M	QF/Q	PF/P
285	571	1	66	5	0.6C2	1.510	896	177.8	701	69.1	10.00
1	0.602	177.8			8.49	-0.36	-2.02	0.980	0.966	0.981	0.026 1.007
2	0.602	177.8			8.49	-C-CI	-1.52	0.980	0.967	0.982	0.025 1.006
3	0.602	177.8			8.49	-0.36	-1.03	0.975	0.952	0.977	0.007 1.002
4	0.602	177.8			8.49	-C-CI	-0.69	0.914	0.837	0.919	0.011 1.003
5	0.602	177.8			8.49	-0.36	-0.52	0.885	0.784	0.891	0.004 1.001
6	0.6C0	177.2			8.49	-C-CI	-0.36	0.877	0.768	0.884	-0.002 0.999
7	0.600	177.2			8.49	-0.36	-0.19	0.858	0.735	0.866	-0.005 0.999
8	0.600	177.2			8.49	-C-CI	-0.02	0.863	0.743	0.871	-0.009 0.998
9	0.600	177.2			8.49	-C-CI	0.15	0.867	0.750	0.874	-0.007 0.998
10	0.600	177.2			8.49	-C-CI	0.32	0.856	0.733	0.864	-0.003 0.999
11	0.599	176.6			8.49	-C-CI	0.48	0.879	0.772	0.886	-0.009 0.998
12	0.600	177.2			8.49	-C-CI	0.65	0.895	0.802	0.901	-0.001 1.000
13	0.6C1	177.2			8.49	-C-CI	0.97	0.921	0.867	0.935	-0.001 1.000
14	0.601	177.2			8.49	-C-CI	1.18	0.960	0.922	0.962	0.004 1.001
15	0.6C2	177.8			8.49	-C-CI	1.48	0.983	0.969	0.984	0.014 1.004
16	0.602	177.8			8.49	-0.36	1.98	0.984	0.973	0.985	0.019 1.005

RUN	TST	P	TN	CCNF	MACH	PN/L	PT	C	P	TT	ALPHA
		SEC	MACH	0	X/DR	Y/DR	Z/DR	MF/N	MA/M	QF/Q	VA/V
286	571	1	66	5	0.600	1.507	896	177.2	702	69.4	10.00
1	C.	600	177.2	8.49	-0.45	-2.03	C.979	C.965	0.980	0.027	1.007
2	C.	600	177.2	8.49	-0.45	-1.53	0.983	0.972	0.984	0.023	1.006
3	0.	600	177.2	8.49	-0.45	-1.03	C.973	0.950	0.975	0.014	1.003
4	0.	600	177.2	8.49	-0.45	-0.69	C.917	C.843	0.922	0.010	1.002
5	C.	600	177.2	8.49	-0.45	-0.53	0.897	0.804	0.903	-0.003	0.999
6	C.	601	177.2	8.49	-0.45	-0.35	C.884	0.780	0.891	-0.011	0.997
7	0.	601	177.2	8.49	-0.45	-0.20	0.873	0.761	0.880	-0.005	0.999
8	0.	6C1	177.2	8.49	-0.45	-0.02	C.872	0.759	0.879	-0.002	0.999
9	0.	601	177.2	8.49	-0.45	0.15	C.862	C.743	0.871	-0.009	0.998
10	0.	601	177.2	8.49	-0.45	0.31	C.875	0.766	0.882	-0.001	1.000
11	0.	601	177.2	8.49	-0.45	0.48	C.889	C.789	0.895	-0.007	0.998
12	0.	601	177.2	8.49	-0.45	0.65	C.903	0.816	0.909	0.003	1.001
13	0.	6C1	177.2	8.49	-0.45	0.98	C.949	0.901	0.952	0.002	1.000
14	0.	6C2	177.8	8.49	-0.45	1.18	C.966	C.935	0.968	0.007	1.002
15	0.	6C1	177.2	8.49	-0.45	1.48	C.982	0.969	0.983	0.019	1.005
16	0.	6C2	177.8	8.49	-0.45	1.98	C.984	C.974	0.985	0.021	1.005

RUN	TST	P	TN	CCNF	MACH	PN/L	PT	C	P	TT	ALPHA
		SEC	MACH	0	X/DR	Y/DR	Z/DR	MF/N	MA/M	QF/Q	VA/V
287	571	1	66	5	0.251	1.517	1893	80.2	1811	68.4	10.00
1	0.	251	80.2	10.88	0.41	-2.05	0.994	0.000	C.988	0.000	0.013
2	C.	250	79.5	C.88	C.41	-1.54	C.984	0.000	0.967	0.000	-0.015
3	0.	250	79.5	1C.88	C.41	-1.04	C.979	0.000	0.957	0.000	-0.024
4	0.	249	78.8	1C.88	C.41	-0.70	C.953	0.000	0.907	0.000	-0.039
5	0.	250	79.5	1C.88	C.41	-0.54	C.940	0.000	0.882	0.000	-0.030
6	0.	250	79.5	1C.88	C.41	-0.36	C.906	0.000	0.820	0.000	-0.019
7	0.	250	79.5	1C.88	C.41	-0.20	C.926	0.000	0.856	0.000	-0.021
8	0.	250	79.5	1C.88	C.41	-0.04	C.927	0.000	0.858	0.000	-0.021
9	0.	250	79.5	1C.88	C.41	0.12	C.951	0.000	0.903	0.000	-0.021
10	0.	249	78.8	1C.88	C.41	0.29	C.924	0.000	0.853	0.000	-0.030
11	0.	249	78.8	1C.88	C.41	0.46	C.927	0.000	0.859	0.000	-0.030
12	C.	249	78.8	1C.88	C.41	0.63	C.935	0.000	0.872	0.000	-0.030
13	0.	249	78.8	1C.88	C.41	0.96	C.983	0.000	0.965	0.000	-0.028
14	C.	250	79.5	1C.88	C.41	1.17	C.971	0.000	0.943	C.000	-0.021
15	0.	250	79.5	1C.88	C.41	1.46	C.975	0.000	C.950	C.000	-0.022
16	0.	249	78.8	1C.88	C.41	1.96	C.997	0.000	C.993	0.000	-0.021

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RUN	TST	P	TN	CCNF	WACH	RN/L	PT	G	TT	ALPHA			
SFC	MACH	C	X/DB	Y/DB	Z/DB	MF/N	MA/M	QF/Q	QA/Q	VF/V	V/A/V	CP	PF/P
288	571.1	66	5	C.250	1.511	1892	79.5	1811	68.1	10.00			
1	0.250	79.5	1C.88	-0.03	-2.04	0.941	0.000	0.884	C.000	0.941	0.000	-0.022	0.999
2	0.250	79.5	1C.88	-C.02	-1.55	C.945	0.000	0.893	0.000	0.946	0.000	-0.022	0.999
3	0.250	79.5	1C.88	-C.03	-1.04	C.941	0.CCC	C.884	C.000	0.941	0.000	-0.022	0.999
4	0.250	79.5	1C.88	-C.C3	-0.71	C.915	0.000	C.000	0.916	0.000	-0.030	0.999	
5	0.250	79.5	1C.88	-0.03	-0.54	C.913	0.000	0.832	C.000	0.914	0.000	-0.030	0.999
6	0.250	79.5	1C.88	-C.C3	-0.38	C.901	0.000	0.811	C.000	0.902	0.000	-0.030	C.999
7	0.249	78.8	1C.88	-C.03	-0.20	C.892	0.000	0.794	C.000	0.893	0.000	-0.030	0.999
8	0.249	78.8	1C.88	-C.03	-0.03	C.890	0.000	0.790	C.000	0.891	0.000	-0.030	0.999
9	0.249	78.8	1C.88	-C.C3	0.13	C.902	0.000	0.813	C.000	0.903	0.000	-0.030	0.999
10	0.249	78.8	1C.88	-C.03	0.29	C.898	C.CCC	0.806	C.000	0.899	C.000	-0.030	0.999
11	0.249	78.8	1C.88	-C.C2	0.46	C.925	0.000	0.853	C.000	0.925	C.000	-0.039	0.998
12	0.250	79.5	1C.88	-C.02	0.63	C.913	0.000	0.834	C.000	0.914	C.000	-0.014	0.999
13	0.249	78.8	1C.88	-C.03	0.97	C.956	0.000	0.913	C.000	0.956	C.000	-0.021	0.999
14	0.248	78.1	1C.88	-C.02	1.16	C.945	0.000	C.892	C.000	0.946	C.000	-0.025	C.999
15	0.248	78.1	1C.88	-C.03	1.47	C.950	0.000	0.979	C.000	0.990	C.000	-0.026	0.999
16	0.249	78.8	1C.88	-C.03	1.96	C.991	0.000	0.981	C.000	0.991	C.000	-0.017	0.999

RUN	TST	P	TN	CCNF	WACH	RN/L	PT	G	TT	ALPHA			
SFC	MACH	Q	X/DB	Y/DB	Z/DB	MF/N	MA/M	QF/Q	QA/Q	VF/V	V/A/V	RP	PF/P
289	571.1	66	5	C.250	1.512	1892	79.5	1811	68.0	10.00			
1	0.250	79.5	1C.88	-C.38	-2.04	C.992	0.000	C.982	0.000	0.992	0.000	-0.017	0.999
2	0.250	79.5	1C.88	-C.38	-1.54	C.986	0.000	C.972	0.000	0.986	0.000	-0.019	0.999
3	0.250	79.5	1C.88	-C.28	-1.05	C.974	0.000	C.948	0.000	0.975	0.000	-0.030	0.999
4	0.250	79.5	1C.88	-C.38	-0.71	C.920	0.000	C.846	C.000	0.921	C.000	-0.030	0.999
5	0.250	79.5	1C.88	-C.38	-0.54	C.912	0.000	C.830	C.000	0.913	C.000	-0.030	0.999
6	0.250	79.5	1C.88	-C.38	-0.38	C.897	C.000	C.804	C.000	0.898	C.000	-0.021	0.999
7	0.250	79.5	1C.88	-C.38	-0.21	C.916	0.000	C.839	C.000	0.917	C.000	-0.021	0.999
8	0.250	79.5	1C.88	-C.38	-0.04	C.914	0.000	C.834	C.000	0.915	C.000	-0.021	0.999
9	0.250	79.5	1C.88	-C.38	0.13	C.917	0.000	C.839	C.000	0.917	C.000	-0.030	0.999
10	0.250	79.5	1C.88	-C.38	0.30	C.888	0.000	C.787	C.000	0.889	C.000	-0.030	0.999
11	0.250	79.5	1C.88	-C.38	0.46	C.900	0.000	C.810	C.000	0.901	C.000	-0.030	0.999
12	0.250	79.5	1C.88	-C.38	0.64	C.921	0.000	C.848	C.000	0.922	C.000	-0.030	0.999
13	0.250	79.5	1C.88	-C.38	0.96	C.950	0.000	C.901	C.000	0.951	C.000	-0.030	0.999
14	0.250	79.5	1C.88	-C.38	1.16	C.966	0.000	C.932	C.000	0.966	C.000	-0.022	0.999
15	0.250	79.5	1C.88	-C.38	1.46	C.983	0.000	C.965	C.000	0.983	C.000	-0.019	0.999
16	0.250	79.5	1C.88	-C.38	1.97	C.988	0.000	C.976	C.000	0.988	C.000	-0.006	1.000

RUN	TST	P	TA	CCNF	MACH	RNL	PT	G	P	TT	ALPHA	PF/D
291	571	1	66	5	0.250	1.512	1.892	79.5	1811	67.8	10.00	0.999
			MACH	X/CR	Y/CR	Z/DB	MF/N	NA/M	QF/D	VA/Q	VF/V	CD
1	0.250	79.5	8.49	0.43	-2.03	C.990	0.-000	0.979	0.000	0.990	0.-000	-0.017
2	0.249	78.8	8.49	0.43	-1.53	C.992	0.-000	0.986	0.000	0.993	0.-000	-0.017
3	0.250	79.5	8.49	0.43	-1.03	C.984	0.-000	0.967	C.000	0.-000	0.984	0.-024
4	0.250	79.5	8.49	C.43	-0.68	C.918	0.-000	0.841	C.000	0.-000	0.918	0.-030
5	0.250	79.5	8.49	0.43	-0.52	C.923	0.-000	0.870	C.000	0.-000	0.934	0.-030
6	0.250	79.5	8.49	0.43	-0.36	C.939	0.-000	0.881	0.-000	0.-000	0.940	0.-030
7	0.250	79.5	8.49	0.43	-0.15	C.951	0.-000	0.811	0.-000	0.-002	0.-000	0.-030
8	0.250	79.5	8.49	0.43	-0.02	C.912	0.-000	0.830	0.-000	0.-013	0.-000	-0.-021
9	0.250	79.5	8.49	0.43	0.14	C.900	0.-000	C.810	C.000	0.-001	0.-000	-0.-021
10	0.250	79.5	8.49	0.43	0.31	C.912	0.-000	C.830	C.000	0.-013	0.-000	-0.-030
11	0.250	79.5	8.49	0.43	0.49	C.928	0.-000	C.860	C.000	0.-029	0.-000	-0.-021
12	0.250	79.5	8.49	C.43	0.65	C.932	0.-000	0.868	C.000	0.-000	0.933	0.-021
13	0.250	79.5	8.49	C.43	0.98	C.968	0.-000	0.936	C.000	0.-000	0.968	0.-015
14	0.250	79.5	8.49	C.43	1.18	C.964	0.-000	0.929	C.000	0.-000	0.965	0.-014
15	0.250	79.5	8.49	0.43	1.48	C.991	0.-000	0.981	0.-000	0.-000	0.991	0.-019
16	0.250	79.5	8.49	0.43	1.98	C.993	0.-000	0.986	0.-000	0.-000	0.994	0.-024

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RUN	TST	P	TN	CCNF	MACH	PN/L	PT	C	P	TT	10.00	ALPHA
292	571	1	66	5	0.250	1.513	1892	79.5	1811	67.8		
SEG	MACH	Q	X/DB	Y/DB	Z/DB	NF/N	MA/W	QF/Q	QA/Q	VF/V	VA/V	PF/P
1	0.250	79.5	8.49	-C.01	-2.03	C.926	0.000	0.856	0.000	0.927	0.000	-0.017 0.999
2	0.250	79.5	8.49	-0.01	-1.53	C.944	0.000	0.891	0.000	0.945	0.000	-0.021 0.999
3	0.250	79.5	8.49	-0.01	-1.03	C.936	0.000	0.875	0.000	0.937	0.000	-0.022 0.999
4	0.250	79.5	8.49	-C.C1	-0.69	0.888	C.000	0.787	C.000	0.889	C.000	-0.030 0.999
5	0.250	79.5	8.49	-0.01	-0.53	C.882	0.000	0.777	C.000	0.883	C.000	-0.030 0.999
6	0.250	79.5	8.49	-0.C1	-0.36	C.862	0.000	0.742	C.000	0.863	C.000	-0.030 0.999
7	0.250	79.5	8.49	-0.01	-0.19	C.873	0.000	0.761	C.000	0.874	C.000	-0.030 0.999
8	0.250	79.5	8.49	-0.C1	-0.01	0.885	C.000	0.782	C.000	0.886	C.000	-0.030 0.999
9	0.249	78.8	8.49	-0.01	0.14	C.872	0.000	0.759	C.000	0.873	C.000	-0.030 0.999
10	0.249	78.8	8.49	-0.01	0.32	C.865	0.000	0.747	C.000	0.866	C.000	-0.030 0.999
11	0.249	78.8	8.49	-0.C1	0.47	C.858	C.000	0.806	C.000	0.899	C.000	-0.030 0.999
12	0.249	78.8	8.49	-0.01	0.65	0.911	0.000	0.829	C.000	0.912	C.000	-0.030 0.999
13	0.249	78.8	8.49	-C.01	0.98	C.943	0.000	0.888	C.000	0.944	C.000	-0.024 0.999
14	0.249	78.8	8.49	-0.01	1.17	C.979	0.000	0.958	C.000	0.980	C.000	-0.028 0.999
15	0.249	78.8	8.49	-0.01	1.48	0.987	0.000	0.974	C.000	0.987	C.000	-0.028 0.999
16	0.249	78.8	8.49	-0.01	1.98	C.957	0.000	0.993	C.000	0.997	C.000	-0.019 0.999

RUN	TST	P	TN	CCNF	MACH	PN/L	PT	C	P	TT	10.00	ALPHA
293	571	1	66	5	0.249	1.506	1891	78.8	1811	67.7		
SEG	MACH	Q	X/DB	Y/DB	Z/DR	NF/N	MA/W	QF/Q	QA/Q	VF/V	VA/V	PF/P
1	0.249	78.8	8.49	-0.36	-2.03	0.994	0.CCC	0.987	C.000	0.994	C.000	-0.226 0.999
2	0.250	79.5	8.49	-C.36	-1.52	C.980	0.000	0.960	0.000	0.980	0.000	-0.017 0.999
3	0.250	79.5	8.49	-C.36	-1.02	C.971	0.000	0.941	C.000	0.971	C.000	-0.024 0.999
4	0.249	78.8	8.49	-0.36	-0.70	C.937	0.000	0.878	C.000	0.938	C.000	-0.026 0.999
5	0.249	78.8	8.49	-C.36	-0.52	C.904	0.000	0.817	C.000	0.905	C.000	-0.030 0.999
6	0.249	78.8	8.49	-0.36	-0.36	C.898	C.000	0.806	C.000	0.899	C.000	-0.030 0.999
7	0.249	78.8	8.49	-C.36	-0.19	C.900	0.000	0.810	C.000	0.901	C.000	-0.032 0.999
8	0.249	78.8	8.49	-C.36	-0.C3	C.881	0.000	0.776	C.000	0.883	C.000	-0.021 0.999
9	0.249	78.8	8.49	-C.36	0.15	C.878	0.000	0.769	C.000	0.879	C.000	-0.021 0.999
10	0.250	79.5	8.49	-C.26	0.31	C.878	0.000	0.770	C.000	0.879	C.000	-0.021 0.999
11	0.250	79.5	8.49	-0.C6	0.48	C.901	C.000	0.811	C.000	0.902	C.000	-0.021 C.999
12	0.250	79.5	8.49	-C.36	0.64	C.916	0.000	0.839	C.000	0.917	C.000	-0.021 0.999
13	0.250	79.5	8.49	-C.36	0.98	C.960	0.000	0.920	C.000	0.960	C.000	-0.021 0.999
14	0.250	79.5	8.49	-C.36	1.18	C.984	0.000	0.967	C.000	0.984	C.000	-0.019 0.999
15	0.250	79.5	8.49	-C.36	1.45	C.985	0.000	0.970	C.000	0.985	C.000	-0.008 1.000
16	0.249	78.8	8.49	-0.36	1.98	C.993	0.000	0.986	C.000	0.993	C.000	-0.017 0.999

RUN	TST	P	TN	CCNF	MACH	PN/L	PT	G	P	TT	ALPHA	PF/P
2.294	5.166	5	0.249	1.507	1.892	78.8	1812	67.6	10.00	0.000	0.000	-0.015
MACH	C	X/FR	Y/FR	Z/DB	MF/N	MA/M	QF/Q	QA/Q	VF/V	VAV/V	CP	CP
1	0.249	78.8	8.49	-0.45	-2.03	0.993	0.000	0.986	0.000	0.993	0.	0.999
2	0.250	79.5	8.49	-0.45	-1.53	0.990	0.000	0.979	0.000	0.990	0.	0.999
3	0.250	79.5	8.49	-0.45	-1.62	0.987	0.000	0.974	0.000	0.988	0.	0.999
4	0.250	79.5	8.49	-0.45	-0.69	0.921	0.000	0.848	0.000	0.922	0.	0.999
5	0.250	79.5	8.49	-0.45	-0.52	0.901	0.000	0.811	0.000	0.902	0.	0.999
6	0.250	79.5	8.49	-0.45	-0.35	0.890	0.000	0.792	0.000	0.892	0.	0.999
7	0.251	80.2	8.49	-0.45	-0.18	0.879	0.000	0.772	0.000	0.880	0.	0.999
8	0.251	80.2	8.49	-0.45	-0.02	0.892	0.000	0.794	0.000	0.893	0.	0.999
9	0.251	80.2	8.49	-0.45	0.14	0.886	0.000	0.784	0.000	0.887	0.	0.999
10	0.250	79.5	8.49	-0.45	0.31	0.888	0.000	0.787	0.000	0.889	0.	0.999
11	0.251	80.2	8.49	-0.45	0.48	0.907	0.000	0.821	0.000	0.908	0.	0.999
12	0.250	79.5	8.49	-0.45	0.65	0.932	0.000	0.868	0.000	0.933	0.	0.999
13	0.251	80.2	8.49	-0.45	0.98	0.961	0.000	0.923	0.000	0.961	0.	0.999
14	0.250	79.5	8.49	-0.45	1.18	0.980	0.000	0.960	0.000	0.980	0.	0.999
15	0.250	79.5	8.49	-0.45	1.48	0.951	0.000	0.982	0.000	0.992	0.	0.999
16	0.251	80.2	8.49	-0.45	1.98	0.987	0.000	0.974	0.000	0.987	0.	0.999

RUN	TST	P	TN	CNF	MACH	RN/L	PT	G	P	TT	ALPHA	
SSEG	MACH	G	X/DR	Y/DR	Z/DR	MF/N	QA/M	QF/0	VF/V	VA/V	CP	PF/P
295	571	1	66	5	0.954	1.483	686	243.4	382	68.1	-10.00	
2	0.954	243.4	1C.88	C.41	-2.04	0.965	0.961	0.971	0.049	1.031		
3	0.954	243.4	1C.88	0.41	-1.53	0.966	0.959	0.971	0.043	1.027		
4	0.952	242.9	1C.88	C.41	-1.05	0.955	0.935	0.962	0.038	1.024		
5	0.950	242.4	1C.88	0.41	-0.70	0.908	0.836	0.921	0.021	1.013		
6	0.950	242.4	1C.88	0.41	-0.54	0.903	0.823	0.916	0.016	1.010		
7	0.948	241.0C	1C.88	C.41	-0.38	0.901	0.816	0.914	0.010	1.006		
8	0.950	241.9	1C.88	0.41	-0.21	0.882	0.782	0.898	0.007	1.005		
9	0.950	241.9	1C.88	0.41	-0.03	0.871	0.761	0.888	0.003	1.002		
10	0.950	241.9	1C.88	C.41	0.13	0.874	0.761	0.890	-0.006	0.997		
11	0.950	241.9	1C.88	0.41	0.29	0.859	0.736	0.877	-0.006	0.996		
12	0.950	241.9	1C.88	C.41	0.47	0.877	0.769	0.893	0.000	1.000		
13	0.950	241.9	1C.88	0.41	0.63	0.894	0.799	0.908	0.000	1.000		
14	0.950	241.9	1C.88	C.41	0.97	0.942	0.897	0.951	0.015	1.009		
15	0.950	241.9	1C.88	C.41	1.17	0.969	0.954	0.973	0.027	1.017		
16	0.950	241.9	1C.88	0.41	1.48	0.973	0.969	0.977	0.039	1.025		
17	0.949	241.4	1C.88	C.41	1.97	0.966	0.965	0.971	0.054	1.034		

RUN	TST	P	TIN	CCNF	MACH	RNL	PT	C	B	TT	ALPHA
SEQ	MACH	Q	X/DR	Y/DB	Z/DR	MF/N	MA/W	GF/Q	QA/Q	VF/V	VA/V
296	571	1	66	5	0.953	1.476	685	242.9	382	69.6	-10.00
SEQ0	MACH	Q	X/DR	Y/DB	Z/DR	MF/N	MA/W	GF/Q	QA/Q	VF/V	VA/V
1	0.953	242.9	1C.88	-0.03	-2.C4	C.892	0.815	0.907	0.036	1.023	
2	0.953	242.9	1C.88	-0.03	-1.55	C.927	0.878	0.937	0.036	1.023	
3	0.951	242.4	1C.88	-C.03	-1.04	C.923	0.863	0.934	0.021	1.013	
4	0.951	242.4	1C.88	-0.03	-0.71	C.875	0.780	0.895	0.013	1.008	
5	0.950	241.9	1C.88	-C.03	-0.54	C.858	0.741	0.876	0.010	1.006	
6	0.950	241.9	1C.88	-C.03	-0.37	C.828	0.705	0.858	0.005	1.003	
7	0.948	241.5	1C.88	-0.03	-0.20	C.826	0.684	0.846	0.005	1.003	
8	0.949	242.0	1C.88	-C.03	-0.04	C.826	0.681	0.847	-0.002	0.999	
9	0.949	242.0	1C.88	-0.03	0.13	C.831	0.686	0.851	-0.009	0.994	
10	0.949	242.0	1C.88	-C.03	0.30	C.826	0.698	0.856	-0.001	0.999	
11	0.949	242.0	1C.88	-C.02	0.46	C.845	0.715	0.864	0.003	1.002	
12	0.949	242.0	1C.88	-C.03	0.63	C.860	0.745	0.877	0.012	1.008	
13	0.946	241.1	1C.88	-C.03	0.96	C.915	0.850	0.927	0.024	1.015	
14	0.947	241.6	1C.88	-0.03	1.16	C.947	0.912	0.954	0.028	1.018	
15	0.947	241.6	1C.87	-C.03	1.46	C.974	0.971	0.978	0.038	1.024	
16	0.948	241.5	1C.88	-C.03	1.96	C.971	0.975	0.975	0.048	1.030	

RUN	TST	P	TIN	CCNF	MACH	RNL	PT	C	B	TT	ALPHA
SEQ	MACH	Q	X/DR	Y/DB	Z/DR	MF/N	MA/W	GF/Q	QA/Q	VF/V	VA/V
297	571	1	66	5	0.955	1.473	685	243.4	381	70.7	-10.00
SEQ0	MACH	Q	X/DR	Y/DB	Z/DR	MF/N	MA/W	GF/Q	QA/Q	VF/V	VA/V
1	0.955	243.4	10.87	-0.38	-2.C4	C.96C	0.944	0.966	0.039	1.025	
2	0.955	243.4	1C.87	-0.38	-1.54	C.967	0.956	0.972	0.033	1.021	
3	0.949	244.2	1C.87	-C.38	-1.C4	C.959	0.933	0.965	0.022	1.014	
4	0.950	244.7	1C.87	-C.38	-0.71	C.905	0.824	0.918	0.010	1.006	
5	0.950	244.7	1C.87	-0.28	-0.53	C.874	0.765	0.891	0.001	1.001	
6	0.950	244.7	1C.87	-C.38	-0.38	C.853	0.727	0.872	-0.001	0.999	
7	0.950	244.7	1C.87	-C.38	-0.20	C.845	0.712	0.864	-0.004	0.997	
8	0.950	244.7	1C.87	-0.38	-0.04	C.827	0.695	0.857	-0.012	0.992	
9	0.950	244.7	1C.87	-0.38	0.13	C.843	0.705	0.863	-0.013	0.992	
10	0.951	244.6	10.87	-C.38	0.30	C.841	0.703	0.861	-0.010	0.994	
11	0.950	244.1	1C.87	-C.38	0.47	C.956	0.732	0.874	-0.003	0.998	
12	0.950	244.1	1C.87	-C.28	0.63	C.878	0.774	0.894	0.006	1.004	
13	0.949	243.7	10.87	-C.38	0.96	C.931	0.877	0.940	0.020	1.013	
14	0.949	243.7	1C.87	-C.38	1.16	C.962	0.941	0.967	0.028	1.018	
15	0.951	244.6	10.87	-C.38	1.47	C.964	0.955	0.969	0.045	1.028	
16	0.951	244.6	1C.87	-0.38	1.96	C.968	0.975	0.975	0.055	1.035	

RUN	TST	P	TN	CCNF	MACH	RNL	PT	C	P	TT	ALPHA
SFC	MACH	Q	X/DB	Y/DB	Z/DB	MF/N	MA/M	QF/Q	QA/Q	VF/V	VA/V
298	571	1	66	5	0.952	1.483	692	245.1	386	71.6	-10.00
1	0.952	245.1	1C.87	-C.48	-2.C4	C.970	0.963	0.975	0.036	1.023	PF/P
2	0.952	245.1	1C.87	-0.48	-1.54	C.973	0.966	0.977	0.031	1.019	
3	0.954	245.7	1C.87	-0.48	-1.04	0.959	0.931	0.965	0.019	1.C12	
4	0.954	245.7	1C.87	-C.48	-0.71	0.904	0.820	0.917	0.007	1.005	
5	0.954	245.7	1C.87	-0.48	-0.54	0.886	0.790	0.901	0.010	1.C06	
6	0.954	245.7	1C.87	-C.48	-0.38	0.875	0.766	0.891	0.002	1.001	
7	0.954	245.7	1C.87	-C.48	-0.20	0.868	0.751	0.885	-0.004	0.998	
8	0.954	245.7	1C.87	-0.48	-0.04	0.857	0.733	0.875	-0.004	0.998	
9	0.954	245.7	1C.87	-0.48	0.12	0.859	0.736	0.876	-0.002	0.999	
10	0.954	245.7	1C.87	-0.48	0.28	C.860	0.741	0.878	0.002	1.C01	
11	0.954	245.7	1C.87	-0.48	0.46	C.869	0.757	0.886	0.005	1.C03	
12	0.952	245.1	1C.87	-C.48	0.63	0.897	C.809	0.911	0.006	1.004	
13	0.954	245.7	1C.87	-0.48	0.96	0.946	0.904	0.954	0.016	1.C10	
14	0.952	245.1	1C.87	-C.48	1.16	C.954	0.930	0.961	0.033	1.021	
15	0.951	244.6	1C.87	-0.48	1.46	C.964	0.956	0.969	0.045	1.C28	
16	0.949	244.2	1C.87	-C.48	1.97	C.968	0.969	0.973	0.053	1.C34	

RUN	TST	P	TN	CCNF	MACH	RNL	PT	C	P	TT	ALPHA
SFC	MACH	Q	X/DB	Y/DB	Z/DB	MF/N	MA/M	QF/Q	QA/Q	VF/V	VA/V
299	571	1	66	5	0.954	1.481	692	245.7	385	72.4	-10.00
1	0.954	245.7	8.48	C.43	-2.C3	C.977	0.971	0.980	0.028	1.018	PF/P
2	0.954	245.7	8.49	0.43	-1.52	C.975	0.967	0.979	0.027	1.C17	
3	0.956	246.2	8.48	C.43	-1.C3	C.971	0.955	0.975	0.020	1.013	
4	0.956	246.2	8.48	0.43	-0.69	C.915	0.840	0.926	0.007	1.004	
5	0.954	245.7	8.48	0.43	-0.52	C.914	0.835	0.926	-0.001	0.999	
6	0.953	245.1	8.48	C.43	-0.34	C.895	0.798	0.909	-0.007	0.996	
7	0.953	245.1	8.48	0.43	-0.19	C.882	0.773	0.897	-0.010	0.994	
8	0.953	245.1	8.48	C.43	-0.02	0.867	0.746	0.884	-0.010	0.993	
9	0.952	245.1	8.48	0.43	0.14	0.852	0.719	0.870	-0.013	0.992	
10	0.954	245.7	8.48	0.43	0.31	0.856	0.728	0.874	-0.011	0.993	
11	0.952	245.2	8.48	0.43	0.48	C.867	0.746	0.884	-0.010	0.994	
12	0.952	245.2	8.48	0.43	0.66	0.899	0.806	0.912	-0.003	0.998	
13	0.952	245.2	8.48	C.43	0.97	0.958	0.923	0.964	0.009	1.006	
14	0.949	244.2	8.48	0.43	1.18	C.977	0.965	0.980	0.019	1.012	
15	0.949	244.2	8.48	0.43	1.48	C.976	0.974	0.980	0.033	1.021	
16	0.950	244.7	8.48	C.43	1.98	C.971	0.971	0.976	0.047	1.079	

RUN	TST	P	TN	CNF	MACH	RNL	PT	Q	P	TT	ALPHA	-10.00
SFQ	MACH	X/DB	Y/DB	Z/DB	MF/N	MA/W	CF/Q	QA/Q	VF/V	VAV	CP	PF/P
300	571	1	66	5	0.956	1.482	693	246.2	385	72.8	0.014	1.009
											0.011	1.007
1	0.956	246.2	8.48	-0.01	-2.02	0.898	0.814	0.912	0.942	0.940	0.002	1.001
2	0.954	245.7	8.48	-0.01	-1.53	0.932	0.874	0.866	0.915	0.915	-0.009	0.994
3	0.955	245.6	8.49	-0.01	-1.02	0.930	0.866	0.886	0.910	0.910	-0.010	0.994
4	0.955	245.6	8.48	-0.01	-0.69	0.902	0.808	0.806	0.820	0.820	-0.012	0.992
5	0.953	245.1	8.48	-0.01	-0.52	0.869	0.750	0.886	0.848	0.848	-0.016	0.990
6	0.954	245.7	8.48	-0.01	-0.36	0.827	0.679	0.629	0.604	0.604	-0.018	0.989
7	0.956	246.2	8.48	-0.01	-0.19	0.797	0.629	0.615	0.615	0.615	-0.012	0.992
8	0.956	246.2	8.48	-0.01	-0.03	0.782	0.604	0.806	0.829	0.829	-0.018	0.988
9	0.954	245.7	8.48	-0.01	0.15	0.788	0.617	0.812	0.812	0.812	-0.018	0.988
10	0.952	245.1	8.48	-0.01	0.30	0.789	0.789	0.813	0.813	0.813	-0.018	0.988
11	0.952	245.1	8.48	-0.01	0.48	0.807	0.643	0.643	0.643	0.643	-0.018	0.988
12	0.951	244.6	8.48	-0.01	0.64	0.839	0.701	0.858	0.858	0.858	-0.005	0.997
13	0.951	244.6	8.48	-0.01	0.99	0.927	0.867	0.937	0.937	0.937	-0.014	1.009
14	0.951	244.6	8.48	-0.01	1.17	0.952	0.924	0.959	0.959	0.959	-0.029	1.018
15	0.949	244.2	8.48	-0.01	1.48	0.967	0.960	0.972	0.972	0.972	-0.043	1.027
16	0.948	244.3	8.48	-0.01	1.99	0.973	0.973	0.977	0.977	0.977	-0.045	1.028

RUN	TST	P	TN	CNF	MACH	RNL	PT	G	P	TT	ALPHA	-10.00
SFQ	MACH	X/DB	Y/DB	Z/DB	MF/N	MA/W	CF/Q	QA/Q	VF/V	VAV	CP	PF/P
301	571	1	66	5	0.954	1.478	692	245.7	385	73.3	-0.006	1.025
											0.029	1.018
1	0.954	245.7	8.48	-0.36	-2.02	0.960	0.945	0.966	0.966	0.966	0.008	1.005
2	0.954	245.7	8.48	-0.36	-1.52	0.973	0.964	0.977	0.977	0.977	-0.003	1.002
3	0.954	245.7	8.48	-0.36	-1.02	0.972	0.950	0.976	0.976	0.976	-0.004	0.998
4	0.954	246.8	8.48	-0.36	-0.69	0.922	0.852	0.933	0.933	0.933	-0.010	0.994
5	0.953	246.8	8.48	-0.36	-0.52	0.869	0.754	0.886	0.886	0.886	-0.016	0.990
6	0.952	246.3	8.48	-0.36	-0.36	0.840	0.701	0.859	0.859	0.859	-0.011	0.993
7	0.950	245.8	8.48	-0.36	-0.19	0.817	0.662	0.838	0.838	0.838	-0.017	0.989
8	0.950	245.8	8.48	-0.36	-0.02	0.806	0.643	0.829	0.829	0.829	-0.000	1.000
9	0.951	246.2	8.48	-0.36	0.15	0.811	0.650	0.833	0.833	0.833	-0.018	0.989
10	0.949	245.8	8.48	-0.36	0.32	0.818	0.663	0.840	0.840	0.840	-0.016	0.990
11	0.949	245.4	8.48	-0.36	0.47	0.837	0.697	0.857	0.857	0.857	-0.010	0.994
12	0.949	245.4	8.48	-0.36	0.65	0.879	0.773	0.895	0.895	0.895	-0.017	1.010
13	0.949	245.4	8.48	-0.36	0.97	0.939	0.892	0.948	0.948	0.948	-0.026	1.016
14	0.948	245.4	8.48	-0.36	1.18	0.970	0.957	0.975	0.975	0.975	-0.037	1.023
15	0.948	245.4	8.48	-0.36	1.49	0.972	0.966	0.976	0.976	0.976	-0.042	1.027
16	0.947	245.4	8.48	-0.36	1.98	0.976	0.973	0.980	0.980	0.980	-0.045	1.028

RUN	TST	P	TN	CCNF	MACH	RNL	PT	G	P	TT	ALPHA
302	571	1	66	5	0.953	1.482	695	246.3	3E7	73.6	-10.00
	SFC	MACH	G	X/CR	Y/DB	Z/DB	MF/N	WA/W	QF/Q	QA/Q	VF/V
1	0.953	246.3	8.48	-0.45	-2.03	C.970	0.961	0.974	0.033	1.021	
2	0.954	246.8	8.48	-0.45	-1.52	C.975	0.969	0.978	0.031	1.020	
3	0.954	246.8	8.48	-0.45	-1.03	C.971	0.953	0.975	0.016	1.010	
4	0.954	246.8	8.48	-0.45	-0.68	C.911	0.831	0.923	0.002	1.001	
5	0.954	246.8	8.48	-0.45	-0.52	C.881	0.774	0.897	-0.005	0.997	
6	0.953	246.8	8.48	-0.45	-0.36	C.859	0.733	0.877	-0.011	0.993	
7	0.953	246.8	8.48	-0.45	-0.18	C.845	0.707	0.864	-0.015	0.990	
8	0.952	246.3	8.48	-0.45	-0.03	C.825	0.671	0.846	-0.021	0.986	
9	0.953	246.8	8.48	-0.45	0.13	C.824	0.672	0.845	-0.018	0.988	
10	0.953	246.8	8.48	-0.45	0.31	C.842	0.701	0.862	-0.018	0.988	
11	0.953	246.8	8.48	-0.45	0.48	C.862	0.735	0.879	-0.015	0.990	
12	0.952	246.3	8.48	-0.45	0.64	C.886	0.783	0.901	-0.003	0.998	
13	C.950	245.8	8.48	-0.45	0.98	C.950	0.907	0.957	0.009	1.006	
14	0.950	245.8	8.48	-C.45	1.18	C.969	0.954	0.973	0.026	1.017	
15	0.950	245.8	8.48	-0.45	1.49	C.970	0.965	0.975	0.039	1.025	
16	0.949	245.4	8.48	-0.45	1.99	C.973	0.974	0.977	0.045	1.028	

RUN	TST	P	TN	CCNF	MACH	RNL	PT	G	P	TT	ALPHA
303	571	1	66	5	C.9CC	1.482	709	237.8	419	73.8	-10.00
	SFC	MACH	Q	X/CR	Y/DB	Z/DB	MF/N	WA/W	QF/Q	QA/Q	VF/V
1	C.900	237.8	10.87	-C.03	-2.04	C.929	0.885	0.938	0.043	1.024	
2	0.900	237.8	10.87	-C.03	-1.55	C.936	0.895	0.945	0.036	1.020	
3	0.900	237.8	10.87	-C.03	-1.04	C.922	0.862	0.932	0.023	1.C13	
4	0.901	238.3	10.87	-C.03	-0.71	C.885	0.785	0.898	0.005	1.C03	
5	0.902	238.7	10.87	-C.03	-0.54	C.860	0.744	0.870	0.013	1.007	
6	0.902	238.7	10.87	-C.03	-0.37	C.842	0.712	0.860	0.007	1.004	
7	0.902	238.7	10.87	-C.03	-0.20	C.833	0.694	0.851	0.002	1.001	
8	0.901	238.2	10.87	-C.03	-0.03	C.826	0.685	0.845	0.007	1.004	
9	0.901	238.2	10.87	-C.03	0.13	C.839	0.708	0.857	0.008	1.005	
10	0.901	238.2	10.87	-C.03	0.30	C.836	0.703	0.854	0.013	1.007	
11	0.901	238.2	10.87	-C.03	0.46	C.857	0.740	0.873	0.015	1.008	
12	0.899	237.3	10.87	-C.03	0.62	C.871	0.771	0.886	0.030	1.017	
13	0.898	236.9	10.87	-C.03	0.97	C.916	0.857	0.927	0.036	1.020	
14	0.896	236.5	10.87	-C.03	1.16	C.946	0.914	0.953	0.038	1.022	
15	0.896	236.5	10.87	-C.03	1.46	C.964	0.953	0.968	0.047	1.027	
16	0.896	236.5	10.88	-C.03	1.96	C.970	0.964	0.974	0.046	1.026	

ORIGINAL PAGE IS  
OF POOR QUALITY

RUN	TST	P	TN	CCNF	MACH	RN/L	PT	G	P	TT	ALPHA	-10.00
SEQ	MACH	Q	X/DB	Y/DR	Z/DB	MF/N	MA/M	QA/Q	VF/V	VA/V	CP	PF/P
1	0.904	23.8.5	8.49	-0.01	-2.03	0.930	0.879	0.939			0.030	1.017
2	0.904	23.8.5	8.49	-0.01	-1.52	0.933	0.885	0.941			0.030	1.017
3	0.904	23.9.0	8.49	-0.01	-1.01	0.924	0.864	0.933			0.023	1.013
4	0.904	23.9.0	8.49	-0.01	-0.69	0.878	0.775	0.893			0.099	1.005
5	0.903	23.8.6	8.49	-0.01	-0.53	0.847	0.720	0.864			0.005	1.003
6	0.903	23.8.6	8.49	-0.01	-0.25	0.816	0.668	0.835			0.009	1.005
7	0.901	23.8.2	8.49	-0.01	-0.19	0.799	0.640	0.820			0.006	1.004
8	0.900	23.7.8	8.49	-0.01	-0.01	0.814	0.665	0.834			0.006	1.003
9	0.900	23.7.8	8.49	-0.01	0.15	0.797	0.637	0.813			0.003	1.002
10	0.900	23.7.8	8.49	-0.01	0.32	0.800	0.640	0.820			0.001	1.001
11	0.899	23.7.4	8.49	-0.01	0.47	0.825	0.684	0.844			0.009	1.005
12	0.899	23.7.4	8.49	-0.01	0.65	0.856	0.743	0.873			0.023	1.013
13	0.897	23.7.0	8.49	-0.01	0.98	0.923	0.866	0.933			0.030	1.017
14	0.897	23.7.0	8.49	-0.01	1.18	0.956	0.933	0.962			0.036	1.020
15	0.896	23.6.5	8.49	-0.01	1.48	0.972	0.965	0.976			0.037	1.021
16	0.898	23.7.4	8.49	-0.01	1.98	0.977	0.971	0.980			0.031	1.017

RUN	TST	P	TN	CCNF	MACH	RN/L	PT	G	P	TT	ALPHA	-10.00
SEQ	MACH	S	X/DR	Y/DR	Z/DB	MF/N	MA/M	QA/Q	VF/V	VA/V	CP	PF/P
1	0.848	231.1	8.49	-0.01	-2.03	0.917	0.848	0.926			0.018	1.009
2	0.849	231.5	8.49	-0.01	-1.52	0.929	0.870	0.937			0.019	1.009
3	0.851	232.4	8.49	-0.01	-1.02	0.922	0.855	0.931			0.010	1.005
4	0.851	232.3	8.49	-0.01	-0.69	0.982	0.779	0.895			0.002	1.001
5	0.852	232.2	8.49	-0.01	-0.52	0.850	0.720	0.866			-0.007	0.996
6	0.852	232.2	8.49	-0.01	-0.37	0.826	0.682	0.843			-0.001	1.000
7	0.851	231.7	8.49	-0.01	-0.18	0.812	0.657	0.830			-0.007	0.996
8	0.851	231.7	8.49	-0.01	-0.02	0.814	0.659	0.831			-0.009	0.996
9	0.852	232.1	8.49	-0.01	0.14	0.919	0.670	0.837			-0.004	0.998
10	0.852	232.1	8.49	-0.01	0.31	0.836	0.696	0.852			-0.007	0.996
11	0.852	232.1	8.49	-0.01	0.47	0.843	0.710	0.859			-0.001	1.000
12	0.853	232.5	8.49	-0.01	0.65	0.874	0.766	0.887			0.005	1.003
13	0.853	232.5	8.49	-0.01	0.98	0.924	0.879	0.942			0.015	1.008
14	0.853	232.5	8.49	-0.01	1.18	0.962	0.937	0.967			0.025	1.013
15	0.851	231.6	8.49	-0.01	1.48	0.972	0.964	0.975			0.039	1.020
16	0.850	231.3	8.49	-0.01	1.98	0.976	0.972	0.980			0.042	1.021

RUN	TST	P	TN	CCNF	MACH	RN/L	PT	C	P	TT	ALPHA	
SEQ	MACH	Q	X/DB	Y/DB	Z/DB	NF/N	MA/M	QA/Q	VF/V	VA/V	CP	PF/P
306	571	1	66	5	0.851	1.497	734	231.7	457	74.0	-10.00	
1	0.851	231.7	1C.87	-C.03	-2.C4	C.921	0.860	0.930	0.027	1.C14		
2	0.850	231.3	1C.87	-C.03	-1.54	C.926	0.870	0.935	0.029	1.014		
3	0.848	230.5	1C.87	-C.03	-1.04	C.910	0.839	0.920	0.026	1.C13		
4	0.847	230.6	1C.87	-C.03	-0.71	C.877	0.775	0.890	0.015	1.007		
5	0.848	231.0	1C.87	-0.03	-0.54	C.865	0.752	0.879	0.009	1.C05		
6	0.848	231.0	1C.87	-C.C3	-0.38	C.852	0.728	0.868	0.002	1.001		
7	0.849	231.5	1C.87	-0.03	-0.21	C.853	0.728	0.868	0.000	1.000		
8	0.849	231.5	1C.87	-C.03	-0.04	C.848	0.722	0.864	0.005	1.C02		
9	0.849	231.5	1C.87	-C.03	0.13	C.869	0.758	0.883	0.006	1.003		
10	0.848	231.0	1C.87	-C.03	0.29	C.856	0.737	0.871	0.012	1.C06		
11	0.848	231.0	1C.87	-C.C3	0.47	C.876	0.771	0.889	0.009	1.005		
12	0.848	231.0	1C.87	-0.03	0.63	C.886	0.788	0.898	0.011	1.005		
13	0.849	231.4	1C.87	-C.C3	0.97	C.937	0.886	0.945	0.016	1.008		
14	0.849	231.4	1C.87	-C.03	1.17	C.962	0.933	0.966	0.019	1.009		
15	0.851	231.7	1C.87	-0.03	1.47	C.974	0.961	0.977	0.027	1.C14		
16	0.850	231.3	1C.87	-C.03	1.97	C.978	0.974	0.981	0.036	1.018		

RUN	TST	P	TN	CCNF	MACH	RN/L	PT	C	P	TT	ALPHA	
SEQ	MACH	Q	X/DB	Y/DB	Z/DB	NF/N	MA/M	QA/Q	VF/V	VA/V	CP	PF/P
307	571	1	66	5	0.796	1.512	764	223.4	503	73.8	-10.00	
1	0.796	223.4	1C.87	C.41	-2.C4	C.985	0.986	0.990	0.018	1.008		
2	0.798	223.9	1C.87	0.41	-1.54	C.950	0.986	0.991	0.015	1.C07		
3	0.799	224.4	1C.87	C.41	-1.05	C.974	0.955	0.977	0.013	1.006		
4	0.799	224.4	1C.87	0.41	-0.70	C.925	0.859	0.933	0.008	1.003		
5	0.799	224.4	1C.87	C.41	-0.55	0.912	0.834	0.921	0.004	1.C02		
6	0.799	224.4	1C.87	C.41	-0.38	C.916	0.840	0.925	0.001	1.000		
7	0.801	224.9	1C.87	0.41	-0.20	C.904	0.816	0.914	-0.003	0.999		
8	0.801	224.9	1C.87	C.41	-0.C4	C.896	0.803	0.906	0.001	1.001		
9	0.801	224.9	1C.87	0.41	0.13	C.9C1	0.812	0.911	0.002	1.001		
10	0.801	224.9	1C.87	C.41	0.29	C.899	0.810	0.909	0.003	1.001		
11	0.801	224.9	1C.87	C.41	0.47	C.9C8	0.826	0.918	0.003	1.001		
12	0.802	225.4	1C.87	C.41	0.63	C.923	0.852	0.931	0.003	1.001		
13	0.803	225.5	1C.87	C.41	0.98	C.956	0.919	0.960	0.013	1.006		
14	0.802	225.4	1C.87	0.41	1.16	C.973	0.953	0.976	0.016	1.C07		
15	0.802	225.4	1C.87	C.41	1.46	C.980	0.973	0.983	0.027	1.C12		
16	0.801	224.9	1C.87	C.41	1.97	C.985	0.980	0.986	0.024	1.011		

RUN	TST	P	TN	CCNF	MACH	PN/L	PT	G	P	TT	ALPHA
SEQ	MACH	0		X/DB	Y/DB	Z/DB	MF/N	MA/M	QF/Q	-10.00	CP
308	571.1	66	5	0.799	1.511	767	225.1	504	76.0	0.907	0.027
2	0.799	225.1	10.87	-0.03	-2.04	C.897	0.814	0.917	0.010	1.012	0.021
3	0.800	225.6	10.88	-C.03	-1.55	C.912	C.840	0.921	0.005	1.009	0.010
4	0.800	225.6	10.88	-C.03	-1.C4	C.908	0.827	0.797	0.005	1.002	0.005
5	0.800	225.6	10.87	-0.03	-0.70	0.892	0.768	0.888	-0.002	0.999	0.002
6	0.800	225.6	10.87	-C.C3	-0.54	0.877	0.745	0.877	-0.004	0.998	0.004
7	0.801	226.1	10.87	-0.03	-0.37	C.864	0.750	0.877	0.007	1.003	0.007
8	0.802	226.6	10.87	-C.03	-0.20	0.866	0.748	0.878	-0.004	0.998	0.004
9	0.802	226.6	10.88	-C.03	-0.C3	C.849	0.721	0.863	-0.001	1.000	0.003
10	0.802	226.6	10.88	-0.03	0.13	C.860	0.740	0.873	0.003	1.001	0.003
11	0.801	226.1	10.88	-C.C3	0.29	0.864	0.755	0.880	0.007	1.003	0.007
12	0.801	226.1	10.88	-0.03	0.47	0.867	0.783	0.894	0.012	1.005	0.012
13	0.800	225.6	10.88	-0.03	0.63	C.882	0.783	0.894	0.013	1.006	0.013
14	0.801	226.1	10.87	-C.C3	0.96	C.929	0.869	0.937	0.020	1.009	0.020
15	0.801	226.1	10.88	-C.03	1.17	C.951	0.912	0.956	0.023	1.010	0.023
16	0.799	225.7	10.88	-C.03	1.46	C.978	0.967	0.981	0.030	1.013	0.030
17	0.801	226.1	10.87	-0.03	1.96	C.980	0.972	0.982			

RUN	TST	P	TN	CCNF	MACH	PN/L	PT	G	P	TT	ALPHA
SEQ	MACH	0		X/DB	Y/DB	Z/DB	MF/N	MA/M	QF/Q	-10.00	CP
309	571.1	66	5	0.797	1.510	768	224.6	505	76.4	0.979	0.034
1	0.797	224.6	10.87	-0.38	-2.05	0.977	C.968	0.968	0.981	0.024	1.015
2	0.798	225.2	10.87	-C.38	-1.54	C.978	C.968	0.963	0.963	0.003	1.011
3	0.802	226.7	10.87	-C.38	-1.04	C.958	C.920	0.807	0.908	0.003	1.001
4	0.800	225.6	10.87	-C.38	-0.70	C.898	C.898	0.783	0.894	0.011	1.005
5	0.799	225.1	10.87	-C.38	-0.54	0.883	0.755	0.881	0.002	1.001	0.002
6	0.798	224.6	10.87	-C.38	-0.36	0.868	C.740	0.872	0.005	1.002	0.005
7	0.800	225.6	10.87	-C.38	-0.20	C.859	C.755	0.882	-0.005	0.998	0.001
8	0.800	225.6	10.88	-C.38	-0.04	0.870	0.749	0.878	0.001	1.000	0.001
9	0.800	225.6	10.88	-C.38	0.12	C.865	0.765	0.886	0.005	1.002	0.005
10	0.801	226.1	10.88	-C.38	0.30	C.874	0.770	0.886	0.017	1.008	0.017
11	C.801	226.1	10.87	-C.38	0.47	C.874	C.874	0.915	0.010	1.004	0.010
12	0.801	226.1	10.87	-C.38	0.63	C.906	0.824	0.915			
13	0.801	226.1	10.87	-C.38	0.96	C.943	0.896	0.949	0.015	1.007	0.015
14	0.801	226.1	10.87	-C.38	1.16	C.957	0.924	0.962	0.018	1.008	0.018
15	0.800	225.6	10.87	-C.38	1.46	C.979	0.969	0.982	0.023	1.010	0.023
16	0.801	226.1	10.87	-C.38	1.96	C.986	0.981	0.987	0.020	1.009	0.020

RUN	TST	P	TN	CCNF	MACH	PN/L	PT	G	D	TT	ALPHA	
SFC					X/DR	Y/DP	Z/DR	WF/N	MA/N	QF/Q	QA/Q	
210	571	1	66	5	0.799	1.512	769	225.7	5C5	76.7	-10.00	
1	0.799	225.7	1C.87	-C.48	-2.C4	0.979	0.971	0.981	0.031	1.014		
2	0.799	225.7	1C.87	-C.48	-1.53	0.981	0.974	0.983	0.026	1.012		
3	0.799	225.7	1C.87	-C.48	-1.04	0.965	0.935	0.969	0.008	1.003		
4	0.802	226.7	1C.87	-C.48	-0.71	0.904	0.819	0.914	0.005	1.002		
5	C.8C2	226.7	1C.87	-C.48	-0.53	0.886	0.784	0.897	-0.003	0.999		
6	0.8C3	227.2	1C.87	-C.48	-0.38	0.882	0.777	0.893	0.000	1.000		
7	0.802	226.6	1C.87	-C.48	-0.21	0.875	0.767	0.887	0.002	1.001		
8	0.802	226.6	1C.87	-C.48	-0.04	0.884	0.783	0.895	0.002	1.001		
9	0.802	226.6	1C.87	-C.48	0.13	0.885	0.783	0.896	0.002	1.001		
10	0.803	227.2	1C.87	-C.48	0.29	0.880	0.778	0.892	0.008	1.004		
11	0.8C3	227.2	1C.87	-C.48	0.46	0.882	0.792	0.899	0.010	1.005		
12	0.803	227.2	1C.87	-C.48	0.63	0.903	0.822	0.913	0.018	1.008		
13	0.8C1	226.1	1C.88	-C.48	0.97	0.945	0.897	0.951	0.009	1.004		
14	0.801	226.1	1C.88	-C.48	1.17	0.962	0.936	0.966	0.024	1.011		
15	0.801	226.1	1C.88	-C.48	1.47	0.979	0.970	0.981	0.030	1.013		
16	0.8C0	225.6	1C.87	-C.48	1.96	0.976	0.968	0.979	0.038	1.017		
311	571	1	66	5	0.8C1	1.512	769	226.1	504	76.8	-10.00	
SFC	MACH	O	X/DR	Y/DP	Z/DR	WF/N	MA/N	QF/Q	QA/Q	VF/V	VA/V	PF/P
1	0.-8C1	226.1	8.-49	C.43	-2.03	C.986	0.982	0.988	0.021	1.009		
2	0.-8C3	227.2	8.-49	C.43	-1.53	C.982	0.975	0.984	0.026	1.012		
3	0.-803	227.2	8.-49	C.43	-1.C3	C.972	0.955	0.975	0.025	1.011		
4	0.-8C3	227.2	8.-49	C.43	-0.69	C.918	0.846	0.926	0.010	1.004		
5	0.-8C2	226.7	8.-49	C.43	-0.53	C.916	0.840	0.925	0.001	1.000		
6	0.-801	227.3	8.-49	C.43	-0.26	C.888	0.795	0.899	0.019	1.009		
7	0.-8C0	226.8	8.-49	C.43	-0.19	C.882	0.778	0.893	0.002	1.001		
8	0.-800	226.8	8.-48	C.43	-0.C2	C.882	0.777	0.894	-0.004	0.998		
9	0.-8C0	226.8	8.-48	C.43	0.14	C.881	0.774	0.892	-0.004	C.998		
10	0.-800	226.8	8.-48	C.43	0.31	C.876	0.767	0.888	-0.003	0.999		
11	0.-799	226.3	8.-48	C.43	0.48	C.893	0.794	0.903	-0.007	0.997		
12	0.-798	225.8	8.-49	C.43	0.65	C.907	0.826	0.916	0.011	1.005		
13	0.-798	225.8	8.-49	C.43	0.98	C.959	0.926	0.963	0.016	1.007		
14	0.-799	226.3	8.-49	C.43	1.18	C.978	0.963	0.981	0.014	1.006		
15	0.-800	226.8	8.-49	C.43	1.49	C.984	0.977	0.986	0.021	1.009		
16	0.-801	227.3	8.-49	C.43	1.98	C.983	0.979	0.985	0.028	1.012		

RUN	TST	P	TN	CCNF	MACH	PN/L	PT	C	P	TT	ALPHA
SFC	MACH	G	X/DB	Y/DB	Z/DB	MF/N	MA/M	QF/Q	QA/Q	VF/V	VA/V
312	571	1	66	5	c.800	1.521	774	227.4	507	77.2	-10.00
1	c.800	227.4	8.49	-0.01	-2.02	0.896	0.810	0.906	0.919	1.008	
2	0.800	227.4	8.49	-c.c1	-1.53	c.912	0.839	0.922	0.015	1.007	
3	0.800	227.4	8.49	-0.01	-1.02	c.909	0.830	0.918	0.010	1.005	
4	0.800	227.4	8.49	-c.c1	-0.69	c.877	0.769	0.889	0.000	1.000	
5	0.800	227.4	8.49	-0.c1	-0.53	c.860	0.737	0.873	-0.007	0.997	
6	c.800	227.4	8.48	-0.01	-0.36	0.839	0.702	0.854	-0.009	0.996	
7	0.800	227.4	8.48	-c.c1	-0.19	c.812	0.661	0.829	0.000	1.000	
8	c.800	227.4	8.49	-0.c1	-0.02	c.827	0.683	0.842	-0.004	0.998	
9	0.800	227.4	8.48	-c.c1	0.14	c.834	0.696	0.849	-0.001	1.000	
10	0.799	226.9	8.48	-0.01	0.32	c.820	0.673	0.835	0.002	1.001	
11	c.797	226.4	8.49	-0.01	0.48	0.856	0.732	0.869	-0.002	0.999	
12	0.799	226.9	8.49	-c.c1	0.65	c.879	0.773	0.891	-0.001	1.000	
13	0.799	226.5	8.48	-0.01	0.98	0.943	0.889	0.949	0.001	1.000	
14	0.804	228.9	8.48	-c.c1	1.17	c.981	0.961	0.983	-0.001	0.999	
15	0.805	228.8	8.48	-0.01	1.48	c.986	0.975	0.988	-0.007	1.003	
16	0.804	227.7	8.48	-0.01	1.98	0.982	0.976	0.984	0.027	1.012	

RUN	TST	P	TN	CCNF	MACH	PN/L	PT	C	P	TT	ALPHA
SFC	MACH	G	X/DB	Y/DB	Z/DB	MF/N	MA/M	QF/Q	QA/Q	VF/V	VA/V
313	571	1	66	5	0.801	1.518	772	227.3	506	77.4	-10.00
1	0.801	227.3	8.48	-0.36	-2.02	c.981	0.974	0.983	0.027	1.012	
2	0.800	226.8	8.48	-0.36	-1.52	c.982	c.974	0.984	0.021	1.009	
3	c.800	226.8	8.48	-0.36	-1.03	c.960	0.929	0.964	0.018	1.008	
4	0.801	227.3	8.48	-0.36	-0.65	c.907	0.824	0.916	0.006	1.003	
5	0.801	227.3	8.48	-0.36	-0.52	c.866	0.749	0.879	-0.003	0.998	
6	0.801	227.2	8.48	-0.36	-0.36	c.857	0.732	0.870	-0.007	0.997	
7	0.801	227.3	8.48	-0.36	-0.19	c.829	0.686	0.844	-0.005	0.998	
8	0.801	227.3	8.48	-0.36	-0.03	c.833	0.690	0.848	-0.013	0.994	
9	0.800	226.8	8.48	-0.36	0.14	c.842	c.709	0.857	-0.007	0.997	
10	0.800	226.8	8.48	-0.36	0.31	c.853	0.727	0.867	-0.003	0.999	
11	0.800	226.8	8.49	-c.c6	0.48	c.878	0.767	0.890	-0.010	0.996	
12	0.801	226.8	8.48	-0.36	0.64	c.895	0.804	0.906	0.005	1.002	
13	0.801	226.8	8.48	-0.36	0.98	c.952	0.913	0.957	0.018	1.008	
14	0.800	227.4	8.48	-c.c6	1.17	c.974	0.958	0.977	0.021	1.010	
15	0.798	226.4	8.49	-0.36	1.48	c.985	0.979	0.987	0.021	1.010	
16	0.797	225.8	8.48	-0.36	1.98	c.985	0.980	0.987	0.023	1.010	

RUN	TST	P	TN	CCNF	MACH	RNL	PT	C	P	TT	ALPHA	
SEQ	MACH	Q	X/DR	Y/DR	Z/DR	NF/N	MA/N	CF/Q	QA/Q	VF/V	CP	PF/P
314	571	1	66	5	0.799	1.517	773	226.9	507	77.6	-10.00	
1	0.799	226.9	8.48	-0.45	-2.03	C.975	0.973	0.981	0.035	1.015		
2	0.799	226.9	8.48	-0.45	-1.46	C.980	0.973	0.982	0.030	1.013		
3	0.799	226.9	8.48	-0.45	-1.03	C.967	0.941	0.971	0.013	1.006		
4	0.799	226.9	8.48	-0.45	-0.69	C.905	0.824	0.915	0.013	1.006		
5	0.798	226.4	8.48	-0.45	-0.52	C.870	0.755	0.882	-0.002	0.999		
6	0.800	226.8	8.48	-0.45	-0.35	C.851	0.722	0.865	-0.007	0.997		
7	0.800	226.8	8.48	-0.45	-0.19	C.851	0.721	0.865	-0.009	0.996		
8	0.800	226.8	8.48	-0.45	-0.02	C.854	0.724	0.867	-0.015	0.993		
9	0.801	227.3	8.48	-0.45	0.14	C.852	0.723	0.865	-0.007	0.997		
10	0.801	227.3	8.48	-0.45	0.31	C.856	0.729	0.869	-0.011	0.995		
11	0.803	227.8	8.48	-0.45	0.48	C.884	0.781	0.895	-0.002	0.999		
12	0.803	227.8	8.48	-0.45	0.65	C.901	0.811	0.911	-0.001	1.000		
13	0.803	227.8	8.48	-0.45	0.98	C.956	0.917	0.961	0.007	1.003		
14	0.803	227.8	8.48	-0.45	1.17	C.976	0.958	0.978	0.015	1.007		
15	0.802	227.3	8.48	-0.45	1.48	C.983	0.977	0.985	0.026	1.012		
16	0.802	227.3	8.48	-0.45	1.98	C.979	0.971	0.981	0.039	1.014		

RUN	TST	P	TN	CCNF	MACH	RNL	PT	C	P	TT	ALPHA	
SFG	MACH	Q	X/DR	Y/DR	Z/DR	NF/N	MA/N	CF/Q	QA/Q	VF/V	CP	PF/P
315	571	1	66	5	0.602	1.521	918	182.4	718	76.5	-10.00	
1	0.602	182.4	10.87	0.41	-2.05	C.988	0.980	0.989	0.018	1.004		
2	0.602	182.4	10.87	0.41	-1.54	C.984	0.972	0.985	0.018	1.004		
3	0.602	182.4	10.87	0.41	-1.04	C.964	0.934	0.966	0.018	1.005		
4	0.601	181.8	10.87	0.41	-0.70	C.915	0.840	0.920	0.015	1.004		
5	0.600	181.2	10.87	0.41	-0.54	C.920	0.846	0.925	0.002	1.000		
6	0.600	181.2	10.87	0.41	-0.37	C.916	0.841	0.921	0.006	1.001		
7	0.600	181.2	10.87	0.41	-0.21	C.907	0.824	0.912	0.007	1.002		
8	0.600	181.2	10.87	0.41	-0.04	C.908	0.825	0.914	-0.003	0.999		
9	0.600	181.2	10.87	0.41	0.13	C.902	0.814	0.907	0.004	1.001		
10	0.600	181.2	10.87	0.41	0.29	C.901	0.814	0.906	0.014	1.003		
11	0.600	181.2	10.87	0.41	0.46	C.914	0.837	0.920	0.003	1.001		
12	0.600	181.2	10.87	0.41	0.64	C.922	0.852	0.926	0.014	1.003		
13	0.600	181.2	10.87	0.41	0.96	C.952	0.909	0.955	0.013	1.003		
14	0.600	181.2	10.87	0.41	1.16	C.970	0.945	0.972	0.018	1.004		
15	0.601	181.8	10.87	0.41	1.46	C.984	0.974	0.985	0.019	1.005		
16	0.601	181.8	10.87	0.41	1.97	C.990	0.981	0.991	0.016	1.004		

RUN	TST	P	TN	CCNF	MACH	RNV/L	PT	C	G	P	TT	ALPHA
SFCG	MACH	S		X/DB	Y/DB	Z/DB	MF/N	QA/Q	VF/V	VA/V	CP	PF/P
216	571	1	66	5	0.601	1.520	518	181.8	719	76.1	-10.00	
1	0.601	181.8	1C.87	-C.03	-2.04	C.921	0.853	0.926	0.018	1.005		
2	0.601	181.8	1C.87	-C.03	-1.54	C.932	0.872	0.937	0.014	1.003		
3	0.601	181.8	1C.87	-C.03	-1.05	C.921	0.850	0.926	0.008	1.002		
4	0.601	181.8	1C.87	-C.03	-0.71	C.892	0.797	0.899	0.003	1.001		
5	0.601	181.8	1C.87	-C.03	-0.54	C.887	0.788	0.894	0.006	1.002		
6	0.601	181.8	1C.87	-C.03	-0.38	C.877	0.771	0.884	0.010	1.002		
7	C.601	181.8	1C.87	-C.03	-0.20	C.882	0.778	0.888	0.003	1.001		
8	0.601	181.8	1C.87	-C.03	-0.03	C.888	0.778	0.894	-0.003	0.999		
9	0.601	181.8	1C.87	-C.02	0.14	C.877	0.770	0.884	0.002	1.001		
10	0.601	181.8	1C.87	-C.02	0.30	C.899	0.810	0.905	0.008	1.002		
11	0.601	181.8	1C.87	-C.03	0.47	C.902	0.812	0.907	-0.003	0.999		
12	0.601	181.8	1C.87	-C.03	0.63	C.916	0.839	0.921	0.004	1.001		
13	0.601	181.8	1C.87	-C.02	0.98	C.949	0.904	0.953	0.010	1.002		
14	0.601	181.8	1C.87	-C.03	1.16	C.958	0.919	0.960	0.006	1.002		
15	0.601	181.8	1C.87	-C.03	1.46	C.984	0.972	0.985	0.015	1.004		
16	0.601	181.8	1C.87	-C.03	1.96	C.989	0.983	0.990	0.022	1.005		

RUN	TST	P	TN	CCNF	MACH	RNV/L	PT	C	G	P	TT	ALPHA
SFCG	MACH	G		X/DB	Y/DB	Z/DB	MF/N	QA/Q	VF/V	VA/V	CP	PF/P
317	571	1	66	5	0.602	1.523	918	182.4	719	76.1	-10.00	
1	0.602	182.4	1C.87	-C.38	-2.04	C.981	0.971	0.982	0.032	1.008		
2	0.601	181.8	1C.87	-C.28	-1.54	C.984	0.974	0.985	0.022	1.005		
3	0.601	181.8	1C.87	-C.38	-1.05	C.958	0.920	0.960	0.014	1.003		
4	0.601	181.8	1C.87	-C.38	-0.71	C.916	0.841	0.921	0.006	1.002		
5	0.601	181.8	1C.87	-C.38	-0.54	C.897	0.805	0.903	0.005	1.001		
6	0.601	181.8	1C.87	-C.38	-0.38	C.897	0.804	0.903	-0.003	0.999		
7	0.601	181.8	1C.87	-C.28	-0.20	C.886	0.786	0.892	0.006	1.002		
8	0.601	181.8	1C.87	-C.38	-0.04	C.894	0.800	0.901	-0.002	1.000		
9	0.601	181.8	1C.87	-C.28	0.13	C.886	0.784	0.893	-0.007	0.998		
10	0.601	181.8	1C.87	-C.38	0.30	C.896	0.804	0.902	0.002	1.001		
11	0.601	181.8	1C.87	-C.28	0.46	C.911	0.831	0.915	0.004	1.001		
12	0.601	181.8	1C.87	-C.38	0.63	C.915	0.836	0.920	-0.002	1.000		
13	0.601	181.8	1C.87	-C.38	0.96	C.952	0.907	0.955	0.006	1.002		
14	0.601	181.8	1C.87	-C.28	1.17	C.972	0.947	0.974	0.013	1.003		
15	0.601	181.8	1C.87	-C.38	1.47	C.982	0.968	0.983	0.018	1.004		
16	0.601	181.8	1C.87	-C.28	1.96	C.985	0.976	0.986	0.026	1.007		

RUN	TST	P	TN	C	MACH	PN/L	PT	C	P	TT	ALPHA		
SFC	MACH	Q	X/DR	Y/DR	Z/DR	MF/N	MA/M	QF/Q	QA/Q	VF/V	V <sub>A</sub> /V	CP	PF/P
318	571	1	66	5	0.6C1	1.521	918	181.8	719	75.8	-10.00	0.020	1.005
1	0.6C1	181.8	IC.87	-C.48	-2.C4	C.989	0.984	0.990					
2	0.6C1	181.8	IC.87	-0.48	-1.55	C.981	0.968	0.982					
3	0.6C1	181.8	IC.87	-C.48	-1.04	C.953	0.914	0.956					
4	0.6C1	181.8	IC.87	-C.48	-0.71	C.908	0.829	0.914					
5	0.6C1	181.8	IC.87	-C.48	-0.54	0.897	0.808	0.903					
6	0.6C1	181.8	IC.87	-C.48	-0.38	0.892	0.798	0.899					
7	0.6C1	181.8	IC.87	-C.48	-0.21	0.897	0.807	0.903					
8	0.6C1	181.8	IC.88	-C.48	-0.04	0.897	0.804	0.903					
9	0.6C1	181.8	IC.88	-0.48	0.12	0.895	0.802	0.901					
10	0.6C1	181.8	IC.88	-C.48	0.29	0.903	0.817	0.908					
11	0.6C1	181.8	IC.88	-C.48	0.47	0.906	0.824	0.912					
12	0.6C1	181.8	IC.87	-C.48	0.63	0.913	0.835	0.919					
13	0.6C1	181.8	IC.87	-C.48	0.96	0.955	0.920	0.962					
14	0.6C1	181.8	IC.87	-0.48	1.17	0.962	0.930	0.965					
15	0.6C1	181.8	IC.87	-C.48	1.47	0.980	0.965	0.981					
16	0.6C1	181.8	IC.88	-C.48	1.96	0.989	0.982	0.990					

RUN	TST	P	TN	C	MACH	PN/L	PT	C	P	TT	ALPHA		
SFC	MACH	Q	X/DR	Y/DR	Z/DR	MF/N	MA/M	QF/Q	QA/Q	VF/V	V <sub>A</sub> /V	CP	PF/P
319	571	1	66	5	0.598	1.508	912	179.3	716	75.4	-10.00	0.013	1.003
1	0.598	179.3	8.49	0.43	-2.03	C.991	0.985	0.991					
2	0.595	179.5	8.49	0.43	-1.52	C.984	0.974	0.985					
3	0.599	179.9	8.49	0.42	-1.03	C.977	0.956	0.978					
4	0.598	179.3	8.49	0.43	-0.69	C.917	0.843	0.922					
5	0.598	179.3	8.49	0.43	-0.53	C.927	0.860	0.931					
6	0.598	179.3	8.49	0.42	-0.35	C.915	0.839	0.920					
7	0.599	179.5	8.49	0.43	-0.18	C.895	0.801	0.901					
8	0.599	179.5	8.49	0.43	-0.02	C.900	0.810	0.906					
9	0.599	179.5	8.49	0.42	0.14	0.877	0.770	0.883					
10	0.599	179.5	8.49	0.42	0.31	0.897	0.804	0.903					
11	0.599	179.9	8.49	0.43	0.48	C.9CS	0.827	0.915					
12	0.599	179.5	8.49	0.42	0.65	C.924	0.854	0.928					
13	0.599	179.9	8.49	0.42	0.98	C.955	0.913	0.958					
14	0.599	179.5	8.49	0.43	1.18	C.978	0.961	0.980					
15	0.598	179.2	8.49	0.43	1.48	C.951	0.986	0.992					
16	0.599	179.9	8.49	0.43	1.95	C.991	0.986	0.992					

RUN	TST	P	TN	CCNF	MACH	RN/L	PT	G	P	TT	ALPHA
SEQ	MACH	C	X/DB	Y/DB	Z/DB	WF/N	MA/M	QF/Q	VA/V	CP	PF/P
220	571.1	66	5	0.598	1.508	912	179.3	716	75.4	-10.00	
1	0.598	179.3	8.49	-0.01	-2.02	0.916	0.842	0.921	0.018	1.004	
2	0.598	179.3	8.49	-0.01	-1.53	0.928	0.865	0.933	0.012	1.003	
3	0.598	179.3	8.49	-0.01	-1.02	0.928	0.864	0.933	0.010	1.002	
4	0.598	179.3	8.49	-0.01	-0.70	0.887	0.787	0.893	0.006	1.002	
5	0.598	179.3	8.49	-0.C1	-0.52	0.871	0.759	0.879	-0.002	0.999	
6	0.598	179.3	8.49	-0.01	-0.36	0.853	0.727	0.861	-0.004	0.999	
7	0.598	179.3	8.49	-0.C1	-0.19	0.852	0.724	0.860	-0.009	0.998	
8	0.598	179.3	8.49	-0.01	-0.02	0.85C	0.722	0.858	-0.009	0.998	
9	0.598	179.3	8.49	-0.C1	0.14	0.858	0.737	0.866	-0.001	1.000	
10	0.598	179.3	8.49	-0.C1	0.31	0.867	0.750	0.874	-0.009	0.998	
11	0.598	179.3	8.49	-0.01	0.48	0.879	0.771	0.885	-0.004	0.999	
12	0.598	179.3	8.49	-0.01	0.64	0.896	0.803	0.902	0.000	1.000	
13	0.598	179.3	8.49	-0.01	0.98	0.942	0.889	0.946	0.003	1.001	
14	0.598	179.3	8.49	-0.01	1.17	0.980	0.962	0.981	0.010	1.002	
15	0.598	179.3	8.49	-0.C1	1.48	0.985	0.974	0.986	0.015	1.004	
16	0.599	179.9	8.49	-0.01	1.98	0.950	0.983	0.990	0.013	1.003	

RUN	TST	P	TN	CCNF	MACH	RN/L	PT	G	P	TT	ALPHA
SEQ	MACH	G	X/DB	Y/DB	Z/DB	WF/N	MA/M	QF/Q	VA/V	CP	PF/P
321	571.1	66	5	0.599	1.511	912	179.3	716	75.4	-10.00	
1	0.599	179.9	8.49	-0.36	-2.03	0.987	0.978	0.988	0.013	1.003	
2	0.600	180.5	8.49	-0.C6	-1.53	0.985	0.975	0.986	0.017	1.004	
3	0.599	179.9	8.49	-0.36	-1.03	0.967	0.936	0.969	0.006	1.001	
4	0.600	180.5	8.49	-0.36	-0.65	0.91C	0.830	0.916	0.004	1.001	
5	0.600	180.5	8.49	-0.36	-0.53	0.884	0.783	0.890	0.010	1.002	
6	0.600	180.5	8.49	-0.C6	-0.35	0.864	0.747	0.871	0.006	1.001	
7	0.599	179.9	8.49	-0.36	-0.19	0.866	0.749	0.873	-0.008	0.998	
8	0.599	179.9	8.48	-0.C6	-0.03	0.860	0.738	0.868	-0.006	0.998	
9	0.598	179.3	8.48	-0.36	0.14	0.862	0.741	0.869	-0.008	0.998	
10	0.599	179.9	8.48	-0.C6	0.36	0.866	0.752	0.873	0.009	1.002	
11	0.599	179.9	8.48	-0.36	0.48	0.894	0.798	0.900	-0.004	0.999	
12	0.599	179.9	8.48	-0.36	0.65	0.9C7	0.824	0.913	0.001	1.000	
13	0.600	180.5	8.48	-0.C6	0.98	0.960	0.925	0.963	0.014	1.003	
14	0.599	179.9	8.48	-0.C6	1.19	0.972	0.953	0.975	0.023	1.006	
15	0.600	180.5	8.49	-0.36	1.48	0.984	0.973	0.985	0.022	1.006	
16	0.600	180.5	8.49	-0.C6	1.98	0.987	0.980	0.988	0.019	1.005	

RUN	TST	P	TN	CNF	MACH	RN/L	PT	C	P	TT	ALPHA
SEQ					X/DB	Y/DR	Z/DR	MF/N	MA/N	QF/N	VA/V
322	571	1	66	5	0.600	1.514	913	180.5	716	75.4	-10.00
	MACH	0									
1	0.600	180.5	8.49	-0.45	-2.03	0.982		0.972	0.984	0.984	0.025 1.006
2	0.599	179.9	8.49	-0.45	-1.52	0.987		0.980	0.988	0.988	0.022 1.005
3	0.599	179.9	8.49	-0.45	-1.03	0.967		0.938	0.969	0.969	0.014 1.003
4	0.598	179.3	8.49	-0.45	-0.69	0.913		0.835	0.919	0.919	0.004 1.001
5	0.600	180.5	8.49	-0.45	-0.52	0.882		0.780	0.889	0.889	0.007 1.002
6	0.599	179.9	8.49	-0.45	-0.36	0.875		0.767	0.862	0.862	0.006 1.001
7	0.599	179.9	8.49	-0.45	-0.19	0.873		0.761	0.880	0.880	-0.006 0.998
8	0.595	179.9	8.49	-0.45	-0.02	0.884		0.779	0.891	0.891	-0.012 0.997
9	0.599	179.9	8.49	-0.45	0.14	0.894		0.798	0.900	0.900	-0.008 0.998
10	0.601	181.1	8.49	-0.45	0.30	0.878		0.772	0.885	0.885	0.001 1.000
11	0.601	181.1	8.49	-0.45	0.48	0.897		0.805	0.903	0.903	0.002 1.001
12	0.601	181.1	8.49	-0.45	0.65	0.921		0.848	0.926	0.926	-0.002 1.000
13	0.600	180.5	8.49	-0.45	0.98	0.961		0.926	0.964	0.964	0.007 1.002
14	0.600	180.5	8.49	-0.45	1.18	0.967		0.941	0.969	0.969	0.022 1.006
15	0.600	180.5	8.49	-0.45	1.48	0.988		0.979	0.989	0.989	0.012 1.003
16	0.600	180.5	8.49	-0.45	1.98	0.986		0.977	0.987	0.987	0.022 1.005

RUN	TST	P	TN	CNF	MACH	RN/L	PT	C	P	TT	ALPHA
SEQ					X/DB	Y/DR	Z/DR	MF/N	MA/N	QF/N	VA/V
323	571	1	66	5	0.249	1.502	1910	79.5	1829	72.8	-10.00
	MACH	0									
1	0.249	79.5	1C.87	0.41	-2.05	0.998	0.000	0.996	0.000	0.998	0.000
2	0.249	79.5	1C.88	0.41	-1.53	0.995	0.000	0.989	0.000	0.995	0.000
3	0.249	79.5	1C.87	0.41	-1.04	0.985	0.000	0.968	0.000	0.985	0.000
4	0.249	79.5	1C.87	0.41	-0.71	0.942	0.000	0.886	0.000	0.942	0.000
5	0.249	79.5	1C.87	0.41	-0.54	0.928	0.000	0.879	0.000	0.939	0.000
6	0.249	79.5	1C.87	0.41	-0.36	0.929	0.000	0.861	0.000	0.929	0.000
7	0.249	79.5	1C.87	0.41	-0.20	0.930	0.000	0.863	0.000	0.930	0.000
8	0.249	79.5	1C.87	0.41	-0.04	0.913	0.000	0.834	0.000	0.914	0.000
9	0.249	79.5	1C.87	0.41	0.12	0.955	0.000	0.912	0.000	0.956	0.000
10	0.249	79.5	1C.87	0.41	0.29	0.923	0.000	0.851	0.000	0.924	0.000
11	0.249	79.5	1C.88	0.41	0.46	0.937	0.000	0.877	0.000	0.938	0.000
12	0.249	79.5	1C.88	0.41	0.63	0.967	0.000	0.934	0.000	0.967	0.000
13	0.249	79.5	1C.88	0.41	0.96	0.984	0.000	0.967	0.000	0.984	0.000
14	0.249	79.5	1C.88	0.41	1.17	0.983	0.000	0.965	0.000	0.983	0.000
15	0.249	79.5	1C.88	0.41	1.46	0.995	0.000	0.989	0.000	0.995	0.000
16	0.249	79.5	1C.88	0.41	1.97	0.998	0.000	0.994	0.000	0.998	0.000

ORIGINAL PAGE IS  
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RUN	TST	P	TN	CCNF	MACH	RN/L	PT	G	P	TT	ALPHA
SFC	MACH	C	X/DR	Y/DR	Z/DB	WF/N	MA/M	QF/Q	QA/Q	VF/V	VA/V
324	571	1	66	5	0.249	1.503	1910	79.5	1829	72.5	-10.00
1	0.249	79.5	1C.87	-C.03	-2.04	0.949	0.000	0.899	0.000	0.949	0.019
2	0.250	80.2	1C.87	-C.03	-1.54	0.951	0.000	0.904	0.000	0.952	0.015
3	0.249	79.5	1C.87	-C.03	-1.04	0.932	0.000	0.870	0.000	0.934	0.024
4	0.249	79.5	1C.87	-C.02	-0.71	0.905	0.000	0.825	0.000	0.910	0.024
5	0.249	79.5	1C.87	-C.03	-0.54	0.892	0.000	0.796	0.000	0.893	0.024
6	0.249	79.5	1C.87	-C.03	-0.38	0.892	0.000	0.797	0.000	0.894	0.024
7	0.249	79.5	1C.87	-C.03	-0.21	0.889	0.000	0.790	0.000	0.891	0.024
8	0.249	79.5	1C.87	-C.03	-0.03	0.904	0.000	0.816	0.000	0.905	0.024
9	0.249	79.5	1C.87	-C.03	0.13	0.905	0.000	0.818	0.000	0.906	0.024
10	0.250	80.2	1C.87	-C.03	0.29	0.908	0.000	0.825	0.000	0.909	0.015
11	0.250	80.2	1C.87	-C.03	0.46	0.906	0.000	0.820	0.000	0.907	0.010
12	0.250	80.2	1C.87	-C.03	0.63	0.937	0.000	0.878	0.000	0.938	0.024
13	0.250	80.2	1C.87	-C.03	0.96	0.946	0.000	0.893	0.000	0.946	0.024
14	0.250	80.2	1C.87	-C.03	1.16	0.972	0.000	0.946	0.000	0.974	0.021
15	0.250	80.2	1C.87	-C.03	1.46	0.988	0.000	0.976	0.000	0.988	0.019
16	0.249	79.5	1C.87	-C.03	1.97	1.004	0.000	1.006	0.000	1.004	0.019

RUN	TST	P	TN	CCNF	MACH	RN/L	PT	G	P	TT	ALPHA
SFC	MACH	Q	X/DR	Y/DR	Z/DB	WF/N	MA/M	QF/Q	QA/Q	VF/V	VA/V
325	571	1	66	5	0.249	1.5C4	1911	79.5	1830	72.1	-10.00
1	0.249	79.5	1C.87	-C.03	-2.05	0.954	0.000	0.987	0.000	0.994	0.014
2	0.248	78.8	1C.87	-C.03	-1.54	0.958	0.000	0.996	0.000	0.998	0.017
3	0.248	78.8	1C.87	-C.03	-1.04	0.948	0.000	0.898	0.000	0.949	0.024
4	0.249	79.5	1C.87	-C.03	-0.71	0.922	0.000	0.849	0.000	0.923	0.024
5	0.249	79.5	1C.87	-C.03	-0.54	0.899	0.000	0.808	0.000	0.900	0.024
6	0.248	78.8	1C.87	-C.03	-0.37	0.891	0.000	0.794	0.000	0.892	0.024
7	0.249	79.5	1C.87	-C.03	-0.20	0.905	0.000	0.818	0.000	0.906	0.024
8	0.249	79.5	1C.87	-C.03	-0.04	0.910	0.000	0.827	0.000	0.911	0.024
9	0.248	78.8	1C.87	-C.03	0.13	0.915	0.000	0.836	0.000	0.916	0.024
10	0.248	78.8	1C.87	-C.03	0.29	0.915	0.000	0.836	0.000	0.916	0.024
11	0.249	79.5	1C.87	-C.03	0.47	0.919	0.000	0.844	0.000	0.920	0.024
12	0.249	79.5	1C.87	-C.03	0.63	0.931	0.000	0.867	0.000	0.932	0.024
13	0.248	78.8	1C.87	-C.03	0.96	0.960	0.000	0.921	0.000	0.961	0.033
14	0.249	79.5	1C.87	-C.03	1.17	0.982	0.000	0.965	0.000	0.983	0.040
15	0.249	79.5	1C.87	-C.03	1.47	0.987	0.000	0.974	0.000	0.987	0.040
16	0.249	79.5	1C.87	-C.03	1.96	0.992	0.000	0.984	0.000	0.992	0.040

RUN	TST	P	TN	CNF	MACH	PN/L	PT	C	P	TT	ALPHA
326	571	1	66	5	0.250	1.512	1911	80.2	1829	72.0	-10.00
SFG	MACH	G		X/DR	Y/DR	Z/DR	NF/N	MA/W	CF/Q	VF/V	CP
1	0.250	80.2	10.87	-0.48	-2.04	C.988	0.000	0.976	0.000	0.983	0.000
2	0.250	80.2	10.87	-C.48	-1.54	C.978	0.000	0.957	0.000	0.979	0.000
3	0.249	79.5	1C.87	-C.48	-1.04	C.949	0.000	0.899	0.000	0.949	0.000
4	0.250	80.2	1C.87	-0.48	-0.71	C.919	0.000	0.844	0.000	0.920	0.000
5	0.249	79.5	1C.87	-C.48	-0.54	C.922	0.000	0.851	0.000	0.924	0.000
6	0.250	80.2	10.87	-0.48	-0.37	C.900	0.000	0.809	0.000	0.901	0.000
7	C.250	80.2	1C.87	-C.48	-0.21	C.919	0.000	0.844	0.000	0.920	0.000
8	0.250	80.2	1C.87	-C.48	-0.04	C.916	0.000	0.838	0.000	0.917	0.000
9	0.250	80.2	1C.87	-C.48	0.12	C.910	0.000	0.826	0.000	0.911	0.000
10	0.250	8C.2	1C.87	-C.48	0.25	C.926	0.000	0.857	0.000	0.927	0.000
11	0.250	80.2	1C.87	-0.48	0.47	C.944	0.000	0.890	0.000	0.945	0.000
12	0.249	79.5	1C.87	-C.48	0.63	C.959	0.000	0.918	0.000	0.959	0.000
13	0.249	79.5	1C.87	-C.48	0.96	C.977	0.000	0.953	0.000	0.977	0.000
14	0.249	79.5	1C.87	-C.48	1.17	C.982	0.000	0.963	0.000	0.982	0.000
15	0.249	79.5	1C.87	-C.48	1.47	C.001	0.000	1.001	0.001	1.001	0.000
16	0.249	79.5	1C.87	-0.48	1.96	C.954	0.000	0.987	0.000	0.994	0.000

RUN	TST	P	TN	CNF	MACH	PN/L	PT	C	P	TT	ALPHA
227	571	1	66	5	0.249	1.506	1910	79.5	1329	71.8	-10.00
SFG	MACH	G		X/DR	Y/DR	Z/DR	NF/N	MA/M	CF/Q	VF/V	CP
1	0.249	79.5	8.49	0.43	-2.03	C.996	0.000	0.991	0.000	0.996	0.000
2	0.249	79.5	8.49	0.43	-1.52	C.994	0.000	0.987	0.000	0.994	0.000
3	0.249	79.5	8.49	0.43	-1.02	C.969	0.000	0.937	0.000	0.969	0.000
4	0.249	79.5	8.49	0.43	-0.69	C.941	0.000	0.884	0.000	0.941	0.000
5	0.249	79.5	8.49	0.43	-0.52	C.913	0.000	0.834	0.000	0.914	0.000
6	0.249	79.5	8.49	0.43	-0.35	C.931	0.000	0.867	0.000	0.932	0.000
7	0.249	79.5	8.49	0.43	-0.19	C.911	0.000	0.830	0.000	0.912	0.000
8	0.249	79.5	8.49	0.43	-0.02	C.897	0.000	0.804	0.000	0.898	0.000
9	0.249	79.5	8.49	0.42	0.14	C.897	0.000	0.804	0.000	0.898	0.000
10	0.249	79.5	8.49	0.42	0.31	C.911	0.000	0.830	0.000	0.912	0.000
11	0.249	79.5	8.49	0.43	0.48	C.923	0.000	0.851	0.000	0.924	0.000
12	0.249	79.5	8.49	0.43	0.65	C.931	0.000	0.867	0.000	0.932	0.000
13	0.249	79.5	8.49	0.43	0.98	C.974	0.000	0.948	0.000	0.974	0.000
14	0.249	79.5	8.49	0.43	1.18	C.994	0.000	0.987	0.000	0.994	0.000
15	0.249	79.5	8.49	0.43	1.49	C.985	0.000	0.977	0.000	0.989	0.000
16	0.249	79.5	8.49	0.43	1.98	C.994	0.000	0.987	0.000	0.994	0.000

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RUN	TST	P	TN	CCNF	MACH	RNL	PT	C	P	TT	ALPHA	PF/P
328	571	1	66	5	0.249	1.5C7	1910	75.5	1829	71.4	-10.00	
SEC	MACH	0	X/CR	Y/DB	Z/DP	MF/N	MA/M	QF/Q	QA/Q	VF/V	VA/V	CP
1	0.249	79.5	8.49	-0.01	-2.02	0.527	0.000	0.877	0.000	0.937	0.000	-0.010 1.000
2	0.249	79.5	8.49	-0.01	-1.53	0.947	0.000	0.896	0.000	0.948	0.000	-0.019 0.999
3	0.249	79.5	8.49	-0.01	-1.03	0.914	0.000	0.834	0.000	0.914	0.000	-0.024 0.999
4	0.249	79.5	8.49	-0.01	-0.69	0.894	0.000	0.799	0.000	0.895	0.000	-0.024 0.999
5	0.249	79.5	8.49	-0.01	-0.53	0.876	0.000	0.766	0.000	0.877	0.000	-0.024 0.999
6	0.249	79.5	8.49	-0.01	-0.36	0.867	0.000	0.750	0.000	0.868	0.000	-0.024 0.999
7	0.249	79.5	8.49	-0.01	-0.19	0.877	0.000	0.768	0.000	0.878	0.000	-0.024 0.999
8	0.250	80.2	8.49	-0.01	0.01	0.870	0.000	0.756	0.000	0.871	0.000	-0.024 0.999
9	0.250	80.2	8.49	-0.01	0.15	0.877	0.000	0.768	0.000	0.878	0.000	-0.017 0.999
10	0.250	80.2	8.49	-0.01	0.33	0.870	0.000	0.756	0.000	0.871	0.000	-0.015 0.999
11	0.250	80.2	8.49	-0.01	0.47	0.896	0.000	0.802	0.000	0.897	0.000	-0.017 0.999
12	0.250	80.2	8.49	-0.01	0.64	0.893	0.000	0.797	0.000	0.894	0.000	-0.015 0.999
13	0.250	80.2	8.49	-0.01	0.97	0.952	0.000	0.905	0.000	0.952	0.000	-0.015 0.999
14	0.250	80.2	8.49	-0.01	1.17	0.976	0.000	0.952	0.000	0.976	0.000	-0.010 1.000
15	0.249	79.5	8.49	-0.01	1.48	0.988	0.000	0.975	0.000	0.988	0.000	-0.028 0.999
16	0.250	80.2	8.49	-0.01	1.98	0.952	0.000	0.984	0.000	0.992	0.000	-0.003 1.000

RUN	TST	P	TN	CCNF	MACH	RNL	PT	C	P	TT	ALPHA	PF/P
329	571	1	66	5	0.250	1.514	1911	80.2	1829	71.1	-10.00	
SEC	MACH	0	X/DB	Y/DB	Z/DR	MF/N	MA/M	QF/Q	QA/Q	VF/V	VA/V	CP
1	0.250	80.2	8.49	-0.36	-2.03	0.589	0.000	0.977	0.000	0.939	0.000	-0.003 1.000
2	0.250	80.2	8.49	-0.36	-1.53	0.961	0.000	0.982	0.000	0.992	0.000	-0.015 0.999
3	0.249	79.5	8.49	-0.36	-1.02	0.955	0.000	0.912	0.000	0.956	0.000	-0.022 0.999
4	0.249	79.5	8.49	-0.36	-0.69	0.914	0.000	0.834	0.000	0.914	0.000	-0.024 0.999
5	0.250	80.2	8.49	-0.36	-0.52	0.900	0.000	0.809	0.000	0.901	0.000	-0.024 0.999
6	0.250	80.2	8.49	-0.36	-0.36	0.882	0.000	0.778	0.000	0.834	0.000	-0.015 0.999
7	0.250	80.2	8.49	-0.36	-0.19	0.867	0.000	0.751	0.000	0.868	0.000	-0.024 0.999
8	0.250	80.2	8.49	-0.36	-0.03	0.885	0.000	0.783	0.000	0.887	0.000	-0.015 0.999
9	0.250	80.2	8.49	-0.36	0.14	0.899	0.000	0.808	0.000	0.900	0.000	-0.024 0.999
10	0.250	80.2	8.49	-0.36	0.32	0.876	0.000	0.766	0.000	0.877	0.000	-0.024 0.999
11	0.250	80.2	8.49	-0.36	0.47	0.893	0.000	0.797	0.000	0.894	0.000	-0.024 0.999
12	0.250	80.2	8.49	-0.36	0.64	0.923	0.000	0.852	0.000	0.924	0.000	-0.015 0.999
13	0.250	80.2	8.49	-0.36	0.98	0.976	0.000	0.952	0.000	0.976	0.000	-0.024 0.999
14	0.250	80.2	8.49	-0.36	1.19	0.974	0.000	0.948	0.000	0.974	0.000	-0.017 0.999
15	0.250	80.2	8.49	-0.36	1.49	0.985	0.000	0.979	0.000	0.936	0.000	-0.013 0.999
16	0.249	79.5	8.49	-0.36	1.98	0.994	0.000	0.987	0.000	0.994	0.000	-0.012 0.999

RUN	TST	P	TN	CCNF	MACH	RN/L	PT	C	P	TT	ALPHA
SEQ	MACH	G	X/CR	Y/DB	Z/DR	MF/N	MA/M	QF/Q	QA/Q	VF/V	VA/V
330	571	1	66	5.0	250	1.514	1911	80.2	1829	71.2	-10.00
1	0.250	80.2	8.49	-0.45	-2.03	0.989	0.000	0.977	0.000	0.989	0.000
2	0.249	79.5	8.49	-0.45	-1.52	0.985	0.000	0.970	0.000	0.985	0.000
3	0.249	79.5	8.49	-0.45	-1.02	0.964	0.000	0.929	0.000	0.965	0.000
4	0.250	80.2	8.49	-0.45	-0.65	0.902	0.000	0.814	0.000	0.904	0.000
5	0.250	80.2	8.49	-0.45	-0.52	0.890	0.000	0.792	0.000	0.892	0.000
6	0.249	79.5	8.49	-0.45	-0.35	0.892	0.000	0.797	0.000	0.894	0.000
7	0.249	79.5	8.49	-0.45	-0.19	0.907	0.000	0.822	0.000	0.908	0.000
8	0.249	79.5	8.49	-0.45	-0.02	0.882	0.000	0.776	0.000	0.883	0.000
9	0.249	79.5	8.49	-0.45	0.14	0.887	0.000	0.785	0.000	0.888	0.000
10	0.249	79.5	8.49	-0.45	0.31	0.889	0.000	0.790	0.000	0.891	0.000
11	0.249	79.5	8.49	-0.45	0.48	0.915	0.000	0.837	0.000	0.916	0.000
12	0.249	79.5	8.49	-0.45	0.64	0.937	0.000	0.877	0.000	0.938	0.000
13	0.249	79.5	8.49	-0.45	0.98	0.966	0.000	0.932	0.000	0.966	0.000
14	0.249	79.5	8.49	-0.45	1.19	0.976	0.000	0.951	0.000	0.976	0.000
15	0.249	79.5	8.49	-0.45	1.48	0.998	0.000	0.994	0.000	0.998	0.000
16	0.249	79.5	8.49	-0.45	1.98	0.998	0.000	0.996	0.000	0.998	0.000

TABLE 2(b)

Configuration 6 – Ballast-profile model as supported in Configuration 5.

RUN	TST	P	TN	CCNF	MACH	RN/L	PT	G	P	ALPHA			PF/P
										X/DR	Y/DP	Z/DR	
331	571	1	66	6	1.1C4	1.513	686	272.5	320	74.4	0.00	0.856	0.282
SEG	MACH	Q											0.263
2	1.104	272.9	7.18	-C.02	1.95	0.825	0.852	0.856	0.856	0.00	0.241	0.083	1.071
3	1.105	272.7	6.93	-C.02	1.95	C.840	C.865	C.866	C.866	0.955	0.225	0.158	1.134
4	1.1C3	272.5	6.76	-C.01	1.95	C.945	0.956	0.919	0.917	0.972	0.049	1.041	0.049
5	1.101	272.2	6.60	-C.01	1.96	0.900	0.971	0.971	0.972	0.983	0.027	1.023	0.027
6	1.099	271.9	6.44	-C.01	1.96	C.966	0.967	0.967	0.967	0.983	0.980	0.034	1.029
7	1.098	271.7	6.27	-C.01	1.96	C.980	0.983	0.983	0.983	0.983	0.976	0.043	1.036
8	1.099	271.5	6.09	-C.01	1.96	C.976	0.979	0.979	0.979	0.980	0.976	0.058	1.049
9	1.101	272.2	5.94	-C.00	1.96	C.970	0.975	0.975	0.975	0.976	0.976	0.064	1.054
10	1.101	272.2	5.76	-C.00	1.96	C.960	0.967	0.967	0.967	0.967	0.967	0.079	1.067
11	1.099	271.5	5.60	-C.00	1.96	C.958	0.966	0.966	0.966	0.966	0.966	0.092	1.078
12	1.100	271.8	5.44	C.00	1.96	C.949	0.960	0.960	0.960	0.960	0.960	0.092	1.078
13	1.100	271.8	5.26	C.00	1.96	C.941	0.954	0.954	0.954	0.954	0.954	0.113	1.096
14	1.100	271.8	5.C9	C.00	1.97	0.928	0.944	0.944	0.944	0.944	0.944	0.237	1.202
15	1.102	272.1	4.92	C.01	1.97	C.875	0.898	0.898	0.898	0.898	0.898	0.205	1.174
16	1.1C4	272.3	4.76	C.01	1.97	C.858	0.882	0.882	0.882	0.882	0.882	0.233	1.199
17	1.1C2	272.1	4.59	C.01	1.97	C.855	0.879	0.879	0.879	0.879	0.879	0.237	1.202
18	1.1C4	272.3	4.42	C.01	1.97	C.845	0.874	0.874	0.874	0.874	0.874	0.250	1.213
19	1.1C4	272.3	4.25	C.01	1.97	C.842	0.867	0.867	0.867	0.867	0.867	0.260	1.222
20	1.1C2	272.1	4.10	C.01	1.97	C.839	0.863	0.863	0.863	0.863	0.863	0.266	1.226
21	1.1C2	272.1	3.94	C.02	1.97	C.834	0.857	0.857	0.857	0.857	0.857	0.275	1.234
332	571	1	66	6	1.1C5	1.507	686	272.7	319	75.7	0.00	0.921	0.037
SEG	MACH	Q											0.080
1	1.105	272.7	5.49	C.00	-1.04	C.9C4	0.843	0.818	0.818	0.748	0.748	0.078	1.067
2	1.105	272.7	5.49	C.00	-0.55	C.875	0.843	0.843	0.843	0.705	0.705	0.078	1.067
3	1.105	273.1	5.49	C.00	-0.03	C.71C	0.539	0.539	0.539	0.431	0.431	0.076	1.065
4	1.1C4	272.9	5.49	C.00	0.12	0.666	0.473	0.473	0.473	0.706	0.706	0.078	1.066
5	1.102	272.6	5.49	C.00	0.29	0.636	0.467	0.467	0.467	0.565	0.565	0.074	1.062
6	1.098	271.7	5.49	C.00	0.46	C.667	0.475	0.475	0.475	0.565	0.565	0.081	1.068
7	1.093	270.8	5.49	C.00	0.62	C.729	0.491	0.491	0.491	0.565	0.565	0.081	1.068
8	1.093	270.8	5.49	C.00	0.96	C.911	0.885	0.885	0.885	0.926	0.926	0.081	1.068

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RUN	TST	P	TN	CCNF	MACH	RN/L	PT	C	P	TT	ALPHA
333	571	1	66	6	0.949	1.482	699	247.0	392	75.8	0.00
				X/CR	Y/DP	Z/CR	MF/N	MA/M	CF/Q	QA/Q	VF/V
SEQ	MACH	Q		5.49	0.00	-1.04	C.898	0.828	0.911		0.043
1	0.949	247.0		5.49	0.00	-0.55	C.860	0.752	0.878		0.025
2	0.948	246.6		5.49	0.00	-0.04	0.683	0.465	0.712		-0.002
3	0.946	246.2		5.49	0.00	0.14	C.655	0.428	0.685		-0.004
4	0.947	246.1		5.49	0.00	0.29	0.648	0.419	0.678		-0.004
5	0.945	245.7		5.49	0.00	0.46	C.683	0.465	0.712		-0.002
6	0.945	245.7		5.49	0.00	0.63	0.742	0.553	0.768		0.007
7	0.946	246.2		5.48	0.00	0.96	C.513	0.851	0.924		0.035
8	0.945	245.8		5.49	0.00	0.96	C.513				1.022

RUN	TST	P	TN	CCNF	MACH	RN/L	PT	C	P	TT	ALPHA
334	571	1	66	6	0.800	1.519	769	226.2	505	75.4	0.00
				X/CR	Y/DP	Z/CR	MF/N	MA/M	CF/Q	QA/Q	VF/V
SEQ	MACH	Q		5.49	0.00	-1.04	0.909	0.830	0.918		0.008
1	0.800	226.2		5.49	0.00	-0.54	0.838	0.708	0.853		1.003
2	0.801	226.1		5.49	0.00	-0.04	0.723	0.521	0.744		0.015
3	0.800	226.2		5.49	0.00	0.12	0.722	0.518	0.742		0.009
4	0.800	226.2		5.49	0.00	0.29	0.729	0.531	0.749		0.996
5	0.802	226.7		5.49	0.00	0.46	0.775	0.600	0.793		0.002
6	0.802	226.7		5.49	0.00	0.63	0.825	0.686	0.844		0.001
7	0.802	226.7		5.49	0.00	0.96	0.942	0.895	0.948		1.000
8	0.801	226.1									0.018

RUN	TST	P	TN	CCNF	MACH	RN/L	PT	C	P	TT	ALPHA
235	571	1	66	6	0.251	1.521	1911	80.9	1828	71.1	0.00
				X/CR	Y/DP	Z/CR	MF/N	MA/M	CF/Q	QA/Q	VF/V
SEQ	MACH	Q		5.48	0.00	-1.04	C.9C8	0.000	0.825	0.000	0.000
1	0.251	80.9		5.49	0.00	-0.55	C.888	0.000	0.787	0.000	0.036
2	0.251	80.9		5.49	0.00	-0.03	C.817	0.000	0.667	0.000	0.045
3	0.250	80.2		5.49	0.00	0.13	0.813	0.000	0.659	0.000	0.043
4	0.251	80.9		5.48	0.00	0.29	C.857	0.000	0.726	0.000	0.036
5	0.251	80.9		5.48	0.00	0.46	C.854	0.000	0.729	0.000	0.029
6	0.251	80.9		5.49	0.00	0.63	C.891	0.000	0.792	0.000	0.026
7	0.251	80.9		5.48	0.00	0.96	C.943	0.000	0.889	0.000	0.010
8	0.251	80.9									1.000

**Table 2(c)**

**Configuration 5 – Ablated model mounted on short sting and strut supported from ceiling of wind tunnel test section:  
forward-facing pitot-static probe.**

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RUN	TST	P	TN	CCNF	MACH	RN/L	PT	G	P	TT	0.00	ALPHA	
SEQ	MACH	Q	X/DB	Y/DR	Z/DR	MF/N	MA/M	QF/Q	OA/Q	VF/V	VA/V	CP	PF/P
336	571	1	66	5	1.102	1.508	678	269.2	317	70.6	0.985	0.012	1.010
2	1.102	269.3	5.49	C.44	-1.05	C.982	0.973	0.926	0.907	0.907	0.929	0.055	1.047
3	1.106	269.9	5.49	0.44	-0.70	0.888	0.891	0.891	0.929	0.929	0.929	0.079	1.067
4	1.101	269.1	5.49	C.44	-0.54	C.914	0.832	0.832	0.901	0.901	0.901	0.083	1.071
5	1.101	269.1	5.49	0.44	-0.21	C.882	0.743	0.743	0.861	0.861	0.861	0.077	1.065
6	1.101	269.1	5.49	0.44	-0.04	0.835	0.654	0.654	0.816	0.816	0.816	0.074	1.062
7	1.098	268.4	5.49	C.44	0.12	C.785	0.610	0.610	0.791	0.791	0.791	0.074	1.063
8	1.098	268.4	5.49	0.44	0.29	0.757	0.651	0.651	0.813	0.813	0.813	0.077	1.065
9	1.096	268.1	5.49	C.44	0.46	0.782	0.63	0.63	0.824	0.824	0.824	0.083	1.070
10	1.096	268.1	5.49	0.44	0.63	0.824	0.727	0.727	0.851	0.851	0.851	0.094	1.079
11	1.094	268.0	C	5.49	0.44	0.96	0.920	0.913	0.934	0.934	0.934	0.070	1.079

RUN	TST	P	TN	CCNF	MACH	RN/L	PT	G	P	TT	0.00	ALPHA	
SEQ	MACH	Q	X/DB	Y/DR	Z/DR	MF/N	MA/M	QF/Q	OA/Q	VF/V	VA/V	CP	PF/P
337	571	1	66	5	1.100	1.512	682	270.7	319	72.0	0.902	0.076	1.065
1	1.100	270.7	5.49	0.00	-1.04	0.882	0.828	0.828	0.895	0.895	0.895	0.079	1.066
2	1.098	270.6	5.49	C..CC	-0.54	C.875	0.816	0.816	0.746	0.746	0.746	0.078	1.066
3	1.098	270.6	5.49	0.00	-0.04	0.7CS	0.536	0.536	0.707	0.707	0.707	0.072	1.061
4	1.098	270.6	5.49	C..CC	0.13	C.668	0.473	0.473	0.663	0.663	0.663	0.079	1.067
5	1.099	270.4	5.49	0.00	0.30	C.622	0.412	0.412	0.684	0.684	0.684	0.082	1.069
6	1.097	270.2	5.49	C..CC	0.47	C.644	0.444	0.444	0.757	0.757	0.757	0.083	1.069
7	1.094	269.6	5.49	C..CC	0.62	C.721	0.555	0.555	0.868	0.868	0.868	0.096	1.081
8	1.099	270.4	5.49	C..CC	0.96	0.896	0.913	0.913	0.914	0.914	0.914	0.096	1.081

RUN	TST	P	TN	CCNF	MACH	RN/L	PT	G	P	TT	0.00	ALPHA		
SEQ	MACH	Q	X/DB	Y/DR	Z/DR	MF/N	MA/M	QF/Q	OA/Q	VF/V	VA/V	CP	PF/P	
338	571	1	66	5	1.102	1.509	682	271.0	319	72.8	0.906	0.042	1.036	
1	1.102	271.0	5.49	-C.44	-1.04	C.96C	0.954	0.954	0.967	0.967	0.967	0.087	1.074	
2	1.102	271.0	5.49	-0.44	-0.71	C.919	0.906	0.906	0.933	0.933	0.933	0.085	1.073	
3	1.105	271.6	5.49	C.44	-0.54	C.855	0.785	0.785	0.879	0.879	0.879	0.091	1.078	
4	1.108	272.2	5.49	-0.44	-0.21	C.856	0.790	0.790	0.879	0.879	0.879	0.088	1.076	
5	1.110	272.4	5.49	-0.44	-0.04	C.814	0.712	0.712	0.842	0.842	0.842	0.078	1.067	
6	1.102	271.0	5.49	-0.44	0.13	C.767	0.627	0.627	0.800	0.800	0.800	0.078	1.067	
7	1.100	270.7	5.49	-0.44	0.29	C.745	0.591	0.591	0.779	0.779	0.779	0.076	1.065	
8	1.097	270.2	5.49	-0.44	0.46	C.775	0.640	0.640	0.807	0.807	0.807	0.079	1.066	
9	1.095	269.9	5.49	-0.44	0.63	C.839	0.754	0.754	0.864	0.864	0.864	0.084	1.070	
10	1.098	270.0	C	5.49	-0.44	0.96	C.920	0.918	0.934	0.934	0.934	0.934	0.101	1.085

RUN	TST	P	TN	CCNF	MACH	PN/L	PT	C	P	TT	ALPHA
339	571	1	66	5	1.103	1.513	686	272.5	320	73.9	0.00
SFC	MACH	G	X/DR	Y/DR	Z/DR	MF/N	MA/M	QF/Q	QA/Q	VF/V	VA/V
1	1.103	272.5	3.52	C.C2	-1.03	C.866	0.868	0.888	0.888	0.185	1.158
2	1.101	272.2	3.52	C.C2	-0.53	C.8C7	0.749	0.836	0.177	1.150	
3	1.098	271.7	3.52	C.02	-0.02	C.256	0.074	0.282	0.156	1.132	
4	1.099	272.1	3.52	C.C2	0.14	C.125	0.021	0.150	0.153	1.129	
5	1.100	272.3	3.52	C.C2	0.31	C.121	0.016	0.134	0.159	1.135	
6	1.100	272.2	3.52	C.C2	0.47	C.325	0.120	0.358	0.159	1.135	
7	1.098	271.7	3.52	C.C2	0.64	C.6C9	0.420	0.650	0.155	1.131	
8	1.096	271.4	3.52	C.02	0.98	0.859	0.874	0.382	0.220	1.185	

RUN	TST	P	TN	CCNF	MACH	PN/L	PT	C	P	TT	ALPHA
340	571	1	66	5	0.951	1.480	695	245.7	388	73.8	0.00
SFC	MACH	G	X/DR	Y/DR	Z/DR	MF/N	MA/M	QF/Q	QA/Q	VF/V	VA/V
1	0.951	245.7	3.52	C.02	-1.03	C.941	0.915	0.949	0.054	1.034	
2	0.951	245.7	3.52	C.C2	-0.53	C.827	0.708	0.848	0.053	1.034	
3	0.950	245.8	3.52	C.C2	-0.03	C.108	0.012	0.117	0.041	1.026	
4	0.949	245.4	3.52	C.C2	0.14	C.14	0.043	0.043	1.027		
5	0.949	245.4	3.52	C.C2	0.31	C.31	0.038	0.024			
6	0.947	245.0	3.52	C.02	0.47	C.224	0.051	0.243	0.029	1.018	
7	0.947	245.0	3.52	C.C2	0.64	C.534	0.290	0.566	0.023	1.014	
8	0.947	245.0	3.52	C.C2	0.98	C.929	0.911	0.947	0.055	1.034	

RUN	TST	P	TN	CCNF	MACH	PN/L	PT	C	P	TT	ALPHA
341	571	1	66	5	0.953	1.480	695	246.3	387	74.1	0.00
SFC	MACH	G	X/DR	Y/DR	Z/DR	MF/N	MA/M	QF/Q	QA/Q	VF/V	VA/V
1	0.953	246.3	5.49	C.44	-1.04	C.956	0.941	0.963	0.046	1.029	
2	0.954	246.8	5.49	C.44	-0.70	C.876	0.786	0.892	0.038	1.024	
3	0.952	246.3	5.49	C.44	-0.54	C.926	0.873	0.936	0.028	1.018	
4	0.951	245.7	5.49	C.44	-0.21	C.857	0.743	0.875	0.016	1.010	
5	0.951	245.7	5.49	C.44	-0.04	C.816	0.668	0.838	0.006	1.004	
6	0.951	245.7	5.49	C.44	0.12	C.777	0.602	0.802	-0.005	0.997	
7	0.951	245.7	5.49	C.44	0.29	C.757	0.573	0.783	-0.001	0.999	
8	0.949	245.3	5.49	C.44	0.46	C.782	0.612	0.806	0.001	1.001	
9	0.949	245.3	5.49	C.44	0.63	C.832	0.694	0.852	0.005	1.003	
10	0.949	245.3	5.49	C.44	0.96	C.948	0.914	0.955	0.028	1.018	

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RUN	TST	P	TN	CCNF	MACH	RN/L	PT	C	P	TT	ALPHA
342	571	1	66	5	0.952	1.480	695	246.3	388	74.4	0.00
SEQ	MACH	0	X/DB	Y/DB	Z/DR	MF/N	MA/M	CF/Q	OA/Q	VF/V	PF/P
1	0.952	246.3	5.49	0.00	-1.04	0.896	0.922	0.910	0.036	1.023	
2	0.949	245.3	5.49	0.00	-0.54	0.861	0.752	0.879	0.022	1.014	
3	0.950	245.8	5.49	0.00	-0.04	0.676	0.457	0.706	0.002	1.001	
4	0.950	245.8	5.49	0.00	0.13	0.636	0.402	0.667	-0.010	0.994	
5	0.950	245.8	5.49	0.00	0.29	0.630	0.395	0.661	-0.007	0.995	
6	0.950	245.8	5.49	0.00	0.46	0.641	0.410	0.672	-0.004	0.998	
7	0.949	245.3	5.49	0.00	0.62	0.740	0.546	0.767	-0.004	0.998	
8	0.949	245.3	5.49	0.00	0.96	0.914	0.852	0.926	0.030	1.019	

RUN	TST	P	TN	CCNF	MACH	RN/L	PT	C	P	TT	ALPHA
343	571	1	66	5	0.952	1.480	695	246.3	388	74.5	0.00
SEQ	MACH	0	X/TR	Y/DB	Z/DB	MF/N	MA/M	QF/Q	OA/Q	VF/V	PF/P
1	0.952	246.3	5.49	-C.44	-1.05	0.960	0.948	0.965	0.046	1.029	
2	0.952	246.3	5.49	-C.44	-0.70	0.924	0.870	0.934	0.032	1.020	
3	0.952	246.3	5.49	-C.44	-0.54	0.881	0.787	0.896	0.022	1.014	
4	0.952	246.3	5.49	-C.44	-0.20	0.816	0.667	0.837	0.005	1.003	
5	0.951	245.7	5.49	-0.44	-0.04	0.771	0.595	0.796	0.001	1.001	
6	0.950	245.8	5.49	-0.44	0.12	0.740	0.546	0.767	-0.004	0.998	
7	0.950	245.8	5.49	-0.44	0.29	0.727	0.529	0.755	-0.001	1.000	
8	0.949	245.3	5.49	-0.44	0.45	0.777	0.603	0.801	-0.002	0.999	
9	0.949	245.3	5.49	-0.44	0.63	0.836	0.704	0.856	0.009	1.006	
10	0.950	245.8	5.49	-0.44	0.96	0.944	0.909	0.952	0.031	1.020	

RUN	TST	P	TN	CCNF	MACH	RN/L	PT	C	P	TT	ALPHA
344	571	1	66	5	0.953	1.481	696	246.8	388	74.7	0.00
SEQ	MACH	0	X/DB	Y/DR	Z/DN	MF/N	MA/M	CF/Q	OA/Q	VF/V	PF/P
1	0.953	246.8	6.99	-0.02	-1.05	0.920	0.856	0.931	0.016	1.010	
2	0.954	246.8	6.99	-0.02	-0.55	0.862	0.747	0.880	0.008	1.005	
3	0.953	246.3	6.99	-0.02	-0.05	0.753	0.563	0.779	-0.010	0.993	
4	0.952	245.7	6.99	-0.02	0.12	0.740	0.542	0.767	-0.016	0.990	
5	0.954	246.2	6.99	-0.02	0.28	0.735	0.535	0.762	-0.015	0.991	
6	0.954	246.2	6.99	-0.02	0.44	0.735	0.539	0.763	-0.006	0.996	
7	0.953	246.3	6.98	-0.02	0.62	0.778	0.608	0.802	0.009	1.006	
8	0.952	245.7	6.98	-0.02	0.95	0.904	0.825	0.917	0.014	1.009	

RUN	TST	P	TN	CONF	MACH	RNL	PT	G	P	TT	ALPHA			
345	571	1	66	5	0.902	1.489	714	239.8	421	74.5	0.00			
SEQ	MACH	Q		X/DR	Y/DR	Z/DR	MF/N	MA/M	QF/Q	QA/Q	VF/V	VA/V	CP	PF/P
1	0.902	239.8		6.99	-0.02	-1.05	0.922	0.863	0.932		0.024	1.014		
2	0.904	240.2		6.99	-0.02	-0.55	0.854	0.731	0.870		0.006	1.004		
3	0.904	240.2		6.99	-0.02	-0.04	0.771	0.590	0.794		-0.012	0.993		
4	0.904	239.6		6.98	-0.02	0.12	0.740	0.545	0.765		-0.007	0.996		
5	0.904	239.6		6.98	-0.02	0.28	0.735	0.539	0.760		-0.003	0.998		
6	0.903	239.2		6.98	-0.02	0.45	0.755	0.570	0.779		0.001	1.001		
7	0.905	240.0		6.98	-0.02	0.63	0.817	0.670	0.837		0.008	1.005		
8	0.905	240.1		6.98	-0.02	0.95	0.911	0.848	0.922		0.036	1.021		

RUN	TST	P	TN	CONF	MACH	RNL	PT	G	P	TT	ALPHA			
346	571	1	66	5	0.897	1.485	713	238.1	423	74.4	0.00			
SEQ	MACH	Q		X/DR	Y/DR	Z/DR	MF/N	MA/M	QF/Q	QA/Q	VF/V	VA/V	CP	PF/P
1	0.897	238.1		5.49	0.00	-1.04	0.909	0.844	0.920		0.038	1.022		
2	0.896	237.6		5.49	0.00	-0.54	0.844	0.724	0.861		0.030	1.017		
3	0.896	237.6		5.49	0.00	-0.03	0.663	0.441	0.690		0.006	1.003		
4	0.898	238.0		5.49	0.00	0.13	0.663	0.440	0.691		0.003	1.001		
5	0.899	238.5		5.49	0.00	0.30	0.651	0.422	0.678		-0.005	0.997		
6	0.900	238.4		5.49	0.00	0.46	0.703	0.496	0.729		0.006	1.004		
7	0.900	238.4		5.49	0.00	0.62	0.773	0.601	0.796		0.009	1.005		
8	0.901	238.8		5.49	0.00	0.96	0.934	0.884	0.943		0.021	1.012		

RUN	TST	P	TN	CONF	MACH	RNL	PT	G	P	TT	ALPHA			
347	571	1	66	5	0.900	1.486	713	238.9	421	74.7	0.00			
SEQ	MACH	Q		X/DR	Y/DR	Z/DR	MF/N	MA/M	QF/Q	QA/Q	VF/V	VA/V	CP	PF/P
1	0.900	238.9		3.52	0.02	-1.03	0.930	0.904	0.939		0.081	1.046		
2	0.900	238.9		3.52	0.02	-0.53	0.752	0.588	0.776		0.071	1.040		
3	0.899	238.5		3.52	0.02	-0.03	0.000	0.000	0.000		0.078	1.044		
4	0.898	238.0		3.52	0.02	0.15					0.073	1.041		
5	0.898	238.0		3.52	0.02	0.30	0.105	0.115	0.115		0.065	1.037		
6	0.898	238.0		3.52	0.02	0.47	0.319	0.105	0.341		0.053	1.030		
7	0.900	238.5		3.52	0.02	0.64	0.585	0.348	0.613		0.032	1.018		
8	0.901	239.4		3.52	0.02	0.98	0.931	0.903	0.940		0.074	1.042		

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RUN	TST	P	TN	CCNF	MACH	RN/L	PT	C	P	TT	ALPHA
					X/DB	Y/DB	Z/DB	MF/N	MA/M	QF/Q	0.00
SEQ	MACH	Q			0.02	0.02	0.02	0.02	0.02	0A/Q	PF/P
348	571	1	66	5	1.098	1.510	688	272.6	323	75.8	0.279
					X/DB	Y/DB	Z/DB	MF/N	MA/M	QF/Q	0.279
	1	1.098	272.6	3.29	0.02	1.98	0.832	0.857	0.859	0.859	1.236
	2	1.099	272.5	3.34	0.02	1.98	0.823	0.858	0.859	0.859	1.236
	3	1.099	272.5	3.42	0.02	1.98	0.830	0.855	0.857	0.857	1.239
	4	1.099	272.5	3.52	0.02	1.98	0.829	0.854	0.856	0.856	1.242
	5	1.098	272.2	3.62	0.02	1.98	0.831	0.856	0.857	0.857	1.239
	6	1.098	272.6	3.71	0.02	1.98	0.832	0.857	0.858	0.858	1.238
	7	1.098	272.8	3.81	0.02	1.97	0.835	0.859	0.860	0.860	1.233
	8	1.098	273.2	3.91	0.02	1.97	0.826	0.860	0.862	0.862	1.230
	9	1.098	273.2	4.02	0.02	1.97	0.838	0.864	0.864	0.864	1.228
	10	1.097	272.5	4.12	0.01	1.97	0.844	0.869	0.869	0.869	1.220
	11	1.100	273.4	4.25	0.01	1.97	0.845	0.871	0.870	0.870	1.218

RUN	TST	P	TN	CCNF	MACH	RN/L	PT	C	P	TT	ALPHA
					X/DB	Y/DB	Z/DB	MF/N	MA/M	QF/Q	0.00
SEQ	MACH	Q			0.02	-0.02	-1.05	0.908	0.939	0.918	0.033
349	571	1	66	5	0.852	1.496	734	232.1	457	74.7	1.017
					X/DB	Y/DB	Z/DB	MF/N	MA/M	QF/Q	1.017
	1	0.852	232.1	6.99	-0.02	-1.05	0.908	0.939	0.918	0.918	0.033
	2	0.852	232.2	6.98	-0.02	-0.54	0.825	0.704	0.851	0.851	1.010
	3	0.852	232.2	6.99	-0.02	-0.05	0.763	0.585	0.784	0.784	1.004
	4	0.850	231.8	6.99	-0.02	0.12	0.750	0.562	0.772	0.772	-0.000
	5	0.849	231.4	6.99	-0.02	0.28	0.761	0.580	0.782	0.782	1.001
	6	0.848	231.0	6.99	-0.02	0.45	0.780	0.610	0.800	0.800	1.002
	7	0.848	231.0	6.99	-0.02	0.62	0.829	0.693	0.846	0.846	1.008
	8	0.847	230.7	6.99	-0.02	0.95	0.936	0.886	0.944	0.944	1.010

RUN	TST	P	TN	CCNF	MACH	RN/L	PT	C	P	TT	ALPHA
					X/DB	Y/DB	Z/DB	MF/N	MA/M	QF/Q	0.00
SEQ	MACH	Q			0.00	-1.04	0.895	0.826	0.910	0.846	0.043
350	571	1	66	5	0.849	1.492	733	230.8	457	74.3	1.022
					X/DB	Y/DB	Z/DB	MF/N	MA/M	QF/Q	1.022
	1	0.849	230.8	5.49	0.00	-1.04	0.895	0.826	0.910	0.846	0.043
	2	0.848	231.0	5.49	0.00	-0.56	0.829	0.696	0.716	0.716	1.013
	3	0.850	231.9	5.49	0.00	-0.04	0.692	0.481	0.693	0.693	1.005
	4	0.850	231.9	5.49	0.00	0.13	0.668	0.447	0.693	0.693	-0.001
	5	0.850	231.8	5.49	0.00	0.29	0.674	0.455	0.698	0.698	1.001
	6	0.849	231.4	5.49	0.00	0.46	0.728	0.533	0.751	0.751	1.005
	7	0.849	230.9	5.49	0.00	0.62	0.810	0.661	0.828	0.828	1.007
	8	0.846	230.1	5.49	0.00	0.96	0.934	0.885	0.942	0.942	1.014

RUN	TST	P	TN	CONF	MACH	RN/L	PT	C	P	TT	ALPHA	
SEC	MACH	Q	X/CR	Y/CR	Z/DR	NF/N	MA/M	QF/Q	QA/Q	VF/V	CP	PF/P
351	571.1	66	5	0.851	1.496	723	231.6	457	74.2	0.00		
1	0.851	231.6	3.52	C.02	-1.03	C.926	0.889	0.934		0.073	1.037	
2	0.851	231.6	3.52	C.02	-0.53	C.711	0.525	0.734		0.080	1.041	
3	0.851	231.6	3.52	C.02	-0.02	C.168	0.029	0.179		0.068	1.035	
4	0.850	231.3	3.52	C.02	0.14	C.054	0.003	0.057		0.072	1.036	
5	0.850	231.3	3.52	C.02	0.31	C.233	0.056	0.249		0.062	1.031	
6	0.850	231.3	3.52	C.02	0.47	C.366	0.138	0.388		0.066	1.033	
7	0.850	231.3	3.52	C.02	0.64	C.653	0.439	0.678		0.057	1.029	
8	0.849	230.9	3.52	C.02	0.98	C.934	0.910	0.942		0.083	1.042	

RUN	TST	P	TN	CONF	MACH	RN/L	PT	C	P	TT	ALPHA	
SEC	MACH	C	X/DB	Y/DB	Z/DR	NF/N	MA/M	QF/Q	QA/Q	VF/V	CP	PF/P
352	571.1	66	5	0.8C2	1.516	764	225.4	5C0	74.0	0.00		
1	0.8C2	225.4	3.52	C.02	-1.03	C.906	0.847	0.915		0.074	1.033	
2	0.8C1	224.9	3.52	C.02	-0.53	C.720	0.536	0.740		0.077	1.035	
3	0.8C0	224.4	3.52	C.02	-0.03	C.247	0.063	0.261		0.074	1.033	
4	0.8C0	224.4	3.52	C.02	0.14	C.219	0.049	0.232		0.066	1.030	
5	0.801	224.9	3.52	C.02	0.31	C.3C1	0.093	0.318		0.064	1.029	
6	0.802	225.4	3.52	C.02	0.47	C.488	0.244	0.511		0.054	1.024	
7	0.801	224.9	3.52	C.02	0.64	C.696	0.495	0.717		0.050	1.023	
8	0.800	224.4	3.52	C.02	0.97	C.934	0.901	0.940		0.076	1.034	

RUN	TST	P	TN	CONF	MACH	RN/L	PT	C	P	TT	ALPHA	
SEC	MACH	Q	X/DB	Y/DB	Z/DP	NF/N	MA/M	QF/Q	QA/Q	VF/V	CP	PF/P
353	571.1	66	5	0.802	1.517	764	225.4	5C0	73.9	0.00		
1	0.802	225.4	5.49	C.44	-1.C4	C.978	C.970	0.980		0.032	1.014	
2	0.8C2	225.4	5.49	0.44	-0.71	C.887	0.796	0.898		0.027	1.C12	
3	0.8C1	224.9	5.49	0.44	-0.54	C.912	C.840	0.921		0.020	1.009	
4	0.8C1	224.9	5.49	0.44	-0.21	C.836	0.705	0.851		0.016	1.007	
5	0.799	224.4	5.49	0.44	-0.04	C.823	0.676	0.838		-0.002	0.999	
6	0.799	224.4	5.49	C.44	0.13	C.802	0.645	0.819		0.005	1.002	
7	0.798	223.9	5.49	C.44	0.29	C.818	0.670	0.834		0.004	1.C02	
8	0.798	223.9	5.49	C.44	0.46	C.848	0.720	0.862		0.004	1.002	
9	0.798	223.9	5.49	C.44	0.63	C.897	0.809	0.907		0.012	1.005	
10	0.798	223.9	5.49	C.44	0.96	C.961	0.935	0.965		0.027	1.C12	

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RUN	TST	P	TN	CCNF	MACH	RN/L	PT	G	P	TT	ALPHA	PF/P
354	571	1	66	5	0.799	1.515	764	224.4	5C2	73.7	0.00	C.020 1.009
				X/DB	Y/DB	Z/DR	MF/N	MA/M	QF/Q	QA/Q	VF/V	CP
SEQ	MACH	G		5.49	0.00	-1.04	C.898	0.814	0.903	0.848	0.905 1.002	
1	0.799	224.4		5.49	0.49	-0.54	C.833	0.696	0.720	0.722	-0.013 0.994	
2	0.801	224.9		5.49	0.00	-0.03	C.699	0.485	0.490	0.490	-0.006 0.998	
3	0.801	224.9		5.49	0.00	0.14	C.701	0.490	0.722	0.722	-0.007 0.997	
4	0.801	224.9		5.49	0.49	C.49	C.720	0.517	0.740	0.740	-0.010 1.005	
5	0.802	225.4		5.49	0.00	0.45	C.749	0.564	0.768	0.768	-0.009 1.004	
6	0.802	225.4		5.49	0.49	C.62	C.816	0.668	0.832	0.832	-0.009 1.004	
7	C.800	225.0		5.49	0.00	0.97	C.944	0.901	0.950	0.950	0.024 1.011	
8	0.800	225.0		5.49	0.49	0.00						

RUN	TST	P	TN	CCNF	MACH	RN/L	PT	G	P	TT	ALPHA	PF/P
355	571	1	66	5	0.799	1.515	764	224.4	5C2	73.8	0.00	C.032 1.014
				X/DB	Y/DB	Z/DR	MF/N	MA/M	QF/Q	QA/Q	VF/V	CP
SEQ	MACH	Q		5.49	-0.44	-1.04	C.976	0.965	0.978	0.978	0.023 1.010	
1	0.799	224.4		5.49	-0.44	-0.71	C.931	0.876	0.938	0.938	0.010 1.005	
2	0.799	224.4		5.49	-0.44	-0.54	C.854	0.733	0.868	0.868	0.004 1.002	
3	0.801	224.9		5.49	-0.44	-0.20	C.800	0.640	0.816	0.816	0.004 1.002	
4	0.801	224.9		5.49	-0.44	-0.04	C.779	0.608	0.797	0.797	-0.006 0.997	
5	0.801	224.9		5.49	-0.44	0.12	C.760	0.576	0.779	0.779	-0.003 1.001	
6	0.798	223.9		5.49	-0.44	0.29	C.791	0.627	0.808	0.808	0.004 1.002	
7	0.799	224.4		5.49	-0.44	0.46	C.828	0.687	0.843	0.843	0.010 1.004	
8	0.798	223.9		5.49	-0.44	0.63	C.890	0.795	0.901	0.901	0.029 1.013	
9	0.799	224.4		5.49	-0.44	0.96	C.962	0.937	0.966	0.966		
10	0.799	224.4		5.49	-0.44							

RUN	TST	P	TN	CCNF	MACH	RN/L	PT	G	P	TT	ALPHA	PF/P
356	571	1	66	5	0.802	1.515	763	224.8	500	73.6	0.00	C.020 1.009
				X/DB	Y/DB	Z/DR	MF/N	MA/M	QF/Q	QA/Q	VF/V	CP
SEQ	MACH	G		6.99	-0.02	-1.06	C.905	0.825	0.914	0.914	0.005 1.002	
1	0.802	224.8		6.99	-0.02	-0.55	C.846	0.718	0.860	0.860	0.001 1.000	
2	0.799	223.8		6.99	-0.02	-0.05	C.782	0.612	0.807	0.807	-0.001 0.999	
3	0.800	224.3		6.98	-0.02	0.12	C.789	0.622	0.798	0.798	-0.002 0.999	
4	0.801	224.9		6.98	-0.02	0.28	C.780	0.608	0.819	0.819	0.007 1.003	
5	0.801	224.9		6.99	-0.02	0.45	C.802	0.646	0.854	0.854	0.009 1.004	
6	0.801	224.9		6.98	-0.02	0.61	C.840	0.708	0.919	0.919	0.010 1.005	
7	0.798	223.9		6.99	-0.02	0.96	C.941	0.95	0.95	0.95		
8	0.798	223.9		6.98	-0.02							

RUN	TST	P	TN	CCNF	MACH	RN/L	PT	C	P	TT	ALPHA	
SEQ	MACH	0	X/DB	Y/DB	Z/DB	WF/N	WA/W	QA/Q	VF/V	VA/V	CP	PF/P
357	571	1	66	5	0.597	1.510	891	174.7	700	64.6	0.00	
2	0.597	174.7	6.99	-0.02	-1.05	0.920	0.850	0.924	0.019	1.005		
3	0.597	174.7	6.99	-0.02	-0.55	0.859	0.739	0.866	0.006	1.002		
4	0.597	174.7	6.99	-0.02	-0.04	0.807	0.651	0.817	-0.004	0.999		
5	0.598	175.3	6.99	-0.02	0.12	0.807	0.650	0.817	-0.008	0.998		
6	0.601	176.5	6.99	-0.02	0.29	0.831	0.690	0.840	-0.001	1.000		
7	0.600	175.9	6.99	-0.02	0.45	0.842	0.708	0.851	-0.009	0.998		
8	0.600	175.5	6.99	-0.02	0.61	0.870	0.755	0.877	-0.010	0.998		
9	0.600	175.9	6.99	-0.02	0.96	0.928	0.863	0.932	0.013	1.003		

RUN	TST	P	TN	CCNF	MACH	RN/L	PT	C	P	TT	ALPHA	
SEQ	MACH	0	X/DB	Y/DB	Z/DB	WF/N	MA/M	QA/Q	VF/V	VA/V	CP	PF/P
358	571	1	66	5	0.602	1.515	891	177.1	697	65.0	0.00	
1	0.602	177.1	5.49	0.44	-1.04	0.980	0.965	0.982	0.017	1.004		
2	0.602	177.1	5.49	0.44	-0.71	0.903	0.817	0.909	0.006	1.002		
3	0.601	176.5	5.49	0.44	-0.54	0.917	0.841	0.922	0.002	1.000		
4	0.603	177.1	5.49	0.44	-0.21	0.862	0.741	0.869	-0.006	0.998		
5	0.603	177.1	5.49	0.44	-0.04	0.831	0.691	0.840	-0.004	0.999		
6	0.601	176.5	5.49	0.44	0.12	0.835	0.697	0.843	0.002	1.000		
7	0.600	175.9	5.49	0.44	0.29	0.829	0.689	0.838	0.014	1.003		
8	0.597	174.7	5.49	0.44	0.47	0.859	0.740	0.866	0.012	1.003		
9	0.598	175.3	5.49	0.44	0.63	0.883	0.782	0.889	0.012	1.003		
10	0.598	175.3	5.49	0.44	0.97	0.966	0.935	0.968	0.010	1.002		

RUN	TST	P	TN	CCNF	MACH	RN/L	PT	C	P	TT	ALPHA	
SEQ	MACH	0	X/DB	Y/DB	Z/DB	WF/N	MA/M	QA/Q	VF/V	VA/V	CP	PF/P
359	571	1	66	5	0.601	1.515	891	176.5	698	65.3	0.00	
1	0.601	176.5	5.49	0.00	-1.04	0.920	0.849	0.925	0.013	1.003		
2	0.601	176.5	5.49	0.00	-0.54	0.837	0.703	0.846	0.013	1.003		
3	0.601	176.5	5.49	0.00	-0.04	0.747	0.557	0.758	-0.006	0.998		
4	0.601	176.5	5.49	0.00	0.13	0.761	0.578	0.772	-0.007	0.998		
5	0.601	176.5	5.49	0.00	0.30	0.774	0.598	0.785	-0.006	0.998		
6	0.601	176.5	5.49	0.00	0.46	0.818	0.668	0.827	-0.004	0.999		
7	0.601	176.5	5.49	0.00	0.62	0.837	0.702	0.845	0.007	1.002		
8	0.601	176.5	5.49	0.00	0.96	0.949	0.903	0.953	0.008	1.002		

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RUN	TST	P	TN	CCNF	MACH	RN/L	PT	C	P	TT	ALPHA		
360	571	1	66	5	0.601	1.514	891	176.5	698	65.6	0.00		
SEQ	MACH		0	X/DR	Y/DB	Z/CR	MF/N	MA/W	QA/Q	VF/V	VA/V	CP	PF/P
1	0.601	176.5	5.49	-0.44	-1.04	C.981	0.965	0.983	0.983	0.983	0.983	0.008	1.002
2	0.602	177.1	5.49	-0.44	-0.71	C.931	0.867	0.935	0.935	0.935	0.935	0.002	1.000
3	0.602	177.1	5.49	-0.44	-0.54	C.866	0.750	0.873	0.873	0.873	0.873	0.002	1.000
4	0.601	176.5	5.49	-0.44	-0.20	C.810	0.657	0.820	0.820	0.820	0.820	-0.001	1.000
5	0.601	176.5	5.49	-0.44	-0.04	C.796	0.633	0.806	0.806	0.806	0.806	-0.003	0.999
6	0.601	176.5	5.49	-0.44	0.13	C.801	0.642	0.811	0.811	0.811	0.811	-0.002	0.999
7	0.601	176.5	5.49	-0.44	0.29	C.826	0.681	0.835	0.835	0.835	0.835	-0.004	0.999
8	0.601	176.5	5.49	-0.44	0.47	C.856	0.733	0.864	0.864	0.864	0.864	0.003	1.001
9	0.600	175.9	5.49	-0.44	0.63	C.886	0.785	0.892	0.892	0.892	0.892	0.003	1.001
10	0.600	175.9	5.49	-0.44	0.97	C.955	0.915	0.958	0.958	0.958	0.958	0.013	1.003

RUN	TST	P	TN	CCNF	MACH	RN/L	PT	C	P	TT	ALPHA		
361	571	1	66	5	0.6C2	1.515	891	177.1	697	65.9	0.00		
SEQ	MACH	G	X/DB	Y/DR	Z/DR	MF/N	MA/W	QA/Q	VF/V	VA/V	CP	PF/P	
1	0.6C2	177.1	2.52	0.02	-1.03	C.945	0.901	0.948	0.948	0.948	0.948	0.038	1.010
2	0.6C2	177.1	2.52	C.02	-0.53	C.780	0.616	0.790	0.790	0.790	0.790	0.050	1.013
3	0.6C1	176.5	3.52	0.02	-0.02	C.477	0.230	0.490	0.490	0.490	0.490	0.036	1.009
4	0.6C2	177.1	2.52	C.02	0.14	C.493	0.244	0.506	0.506	0.506	0.506	0.025	1.006
5	0.602	177.1	3.52	C.02	0.31	C.528	0.280	0.541	0.541	0.541	0.541	0.021	1.005
6	0.6C1	176.5	3.52	C.02	0.48	C.675	0.458	0.688	0.688	0.688	0.688	0.018	1.005
7	0.6C2	177.1	3.52	C.02	0.64	C.791	0.633	0.801	0.801	0.801	0.801	0.041	1.010
8	0.6C1	176.5	3.52	C.02	0.97	C.949	C.914	0.952	0.952	0.952	0.952	0.055	1.014

RUN	TST	P	TN	CCNF	MACH	RN/L	PT	C	P	TT	ALPHA		
362	571	1	66	5	0.251	1.517	1875	79.4	1794	64.8	0.00		
SEQ	MACH	G	X/DB	Y/DR	Z/DR	MF/N	MA/W	QA/Q	VF/V	VA/V	CP	PF/P	
1	0.251	79.4	2.52	C.02	-1.03	C.955	0.000	0.920	0.000	0.920	0.000	0.001	1.000
2	0.250	78.8	3.52	C.02	-0.53	C.804	0.000	0.647	0.000	0.647	0.000	-0.010	1.000
3	0.252	79.4	3.52	C.02	-0.02	C.536	0.000	0.287	0.000	0.287	0.000	-0.001	1.000
4	0.250	78.8	3.52	C.02	0.14	C.614	0.000	0.376	0.000	0.376	0.000	-0.012	0.999
5	0.250	78.8	3.52	C.02	0.31	C.668	0.000	0.445	0.000	0.445	0.000	-0.010	1.000
6	0.250	78.8	3.52	C.02	0.48	C.752	0.000	0.566	0.000	0.566	0.000	-0.008	1.000
7	0.250	78.8	3.52	C.02	0.64	C.822	0.000	0.676	0.000	0.676	0.000	-0.010	1.000
8	0.250	78.8	3.52	C.02	0.98	C.970	0.000	0.941	0.000	0.941	0.000	-0.001	1.000

RUN	TST	F	TN	CCNF	MACH	RN/L	PT	C	P	TT	ALPHA
363	571	1	66	5	C.250	1.51C	1874	78.8	1794	64.6	0.00
SEQ	MACH	G	X/CR	Y/DB	Z/CR	MF/N	MA/N	QF/Q	QA/Q	VF/V	VA/V
1	0.250	78.8	5.49	0.44	-1.04	C.975	0.000	0.951	0.000	0.976	0.000
2	0.250	78.8	5.49	0.44	-0.79	C.9C9	0.000	0.825	0.000	0.910	0.000
3	0.250	78.8	5.49	0.44	-0.54	C.914	0.000	0.834	0.000	0.915	0.000
4	0.250	78.8	5.49	0.44	-0.21	C.863	0.000	0.743	0.000	0.864	0.000
5	0.250	78.8	5.49	0.44	-0.04	C.822	0.000	0.692	0.000	0.834	0.000
6	0.250	78.8	5.49	0.44	0.12	C.836	0.000	0.698	0.000	0.837	0.000
7	0.250	78.8	5.49	0.44	0.29	C.862	0.000	0.743	0.000	0.864	0.000
8	0.250	78.8	5.49	0.44	0.47	C.888	0.000	0.787	0.000	0.889	0.000
9	0.250	78.8	5.49	0.44	0.63	C.919	0.000	0.843	0.000	0.920	0.000
10	0.250	78.8	5.49	0.44	0.96	C.946	0.000	0.894	0.000	0.946	0.000

RUN	TST	P	TN	CCNF	MACH	RN/L	PT	C	P	TT	ALPHA
364	571	1	66	5	0.252	1.517	1874	75.4	1794	64.6	0.00
SEQ	MACH	G	X/DB	Y/DB	Z/DB	MF/N	MA/N	QF/Q	QA/Q	VF/V	VA/V
1	0.252	79.4	5.49	C.CC	-1.04	C.928	0.000	0.860	0.000	0.928	0.000
2	0.252	79.4	5.49	0.00	-0.54	C.848	0.000	0.718	0.000	0.849	0.000
3	0.252	79.4	5.49	C.CC	-0.04	C.797	0.000	0.634	0.000	0.799	0.000
4	0.252	79.4	5.49	0.00	0.13	C.798	0.000	0.636	0.000	0.800	0.000
5	0.252	79.4	5.49	0.00	0.29	C.807	0.000	0.650	0.000	0.808	0.000
6	0.252	79.4	5.49	C.CC	0.46	C.821	0.000	0.690	0.000	0.833	0.000
7	0.250	78.8	5.49	0.00	0.62	C.856	0.000	0.721	0.000	0.857	0.000
8	0.249	78.1	5.49	C.CC	0.97	C.930	0.000	0.864	0.000	0.931	0.000

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RUN	TST	P	TN	CCNF	MACH	RN/L	PT	G	P	TT	ALPHA
365	571	1	66	5	0.250	1.511	1874	78.8	1794	64.5	0.00
SEC	MACH	G		X/DR	Y/DR	Z/DR	MF/N	MA/M	QF/Q	QA/Q	VF/V
1	0.250	78.8	5.48	-C.44	-1.05	C.967	0.000	0.934	0.000	0.967	0.000
2	0.250	78.8	5.48	-0.44	-0.71	C.911	0.000	C.829	0.000	0.912	0.000
3	0.250	78.8	5.49	-C.44	-0.54	C.846	0.000	C.715	C.000	0.848	0.000
4	0.250	78.8	5.49	-C.44	-0.20	C.819	C.000	C.670	C.000	0.821	C.000
5	0.252	79.4	5.49	-0.44	-0.04	C.839	0.000	C.704	C.000	0.841	0.000
6	0.250	78.8	5.49	-C.44	0.12	C.809	0.000	C.654	0.000	0.811	0.000
7	0.252	79.4	5.49	-0.44	0.29	C.848	C.000	C.718	C.000	0.849	0.000
8	0.252	79.4	5.49	-C.44	0.46	C.850	0.000	C.721	0.000	0.851	0.000
9	0.250	78.8	5.49	-C.44	0.63	C.928	0.000	C.878	C.000	0.938	0.000
10	0.250	78.8	5.48	-0.44	0.96	C.968	0.000	C.935	C.000	0.968	C.000

RUN	TST	P	TN	CCNF	MACH	RN/L	PT	G	P	TT	ALPHA
366	571	1	66	5	0.250	1.511	1874	78.8	1794	64.4	0.00
SEC	MACH	G		X/DR	Y/DR	Z/DR	MF/N	MA/M	QF/Q	QA/Q	VF/V
1	0.250	78.8	6.98	-0.02	-1.05	C.929	0.000	C.862	C.000	0.930	0.000
2	0.249	78.1	6.98	-0.02	-0.56	C.854	0.000	C.729	0.000	0.856	0.000
3	0.249	78.1	6.98	-C.02	-0.05	C.829	0.000	C.686	0.000	0.831	0.000
4	0.249	78.1	6.98	-C.02	0.12	C.828	0.000	C.684	0.000	0.830	0.000
5	0.250	78.8	6.98	-C.02	0.29	C.872	0.000	C.761	C.000	0.874	0.000
6	0.250	78.8	6.98	-C.02	0.45	C.866	0.000	C.748	C.000	0.867	0.000
7	0.250	78.8	6.98	-C.02	0.61	C.863	0.000	C.743	C.000	0.864	0.000
8	0.250	78.8	6.98	-0.02	0.95	C.924	0.000	C.871	C.000	0.935	C.000

Table 2(d)

Configuration 7 – Ablated model mounted on short sting and strut supported from ceiling of wind tunnel test section aft-facing pitot-static probe.

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RUN	TST	P	TN	CNF	MACH	RNL	PT	G	P	TT	ALPHA
367	571	1	66	7	0.951	1.480	682	241.2	381	66.2	0.00
SFG	MACH	0	X/DB	Y/DB	Z/DB	MF/N	WA/M	QF/Q	QA/Q	VF/V	VA/V
1	0.950	241.2	0.53	0.01	0.18	0.228	0.256	0.039	0.049	0.247	0.277
2	0.951	241.2	0.82	0.01	0.18	0.310	0.208	0.069	0.031	0.334	0.225
3	0.951	241.2	1.11	0.00	0.18	0.315	0.157	0.069	0.017	0.340	0.171
4	0.950	240.7	1.40	0.00	0.18	0.354	0.221	0.087	0.034	0.381	0.229
5	0.950	240.7	1.69	-0.00	0.18	0.436	0.294	0.134	0.061	0.465	0.316
6	0.949	240.3	2.05	-0.01	0.18	0.480	0.379	0.168	0.105	0.511	0.407
7	0.951	241.2	2.26	-0.01	0.17	0.430	0.346	0.147	0.095	0.460	0.372
8	0.951	241.2	2.55	-0.01	0.17	0.381	0.342	0.123	0.099	0.408	0.368
9	0.951	241.2	2.85	-0.01	0.17	0.234	0.236	0.050	0.051	0.253	0.255
10	0.951	241.2	3.13	-0.02	0.17	0.000	0.040	0.000	0.002	0.000	0.044
11	0.951	241.2	3.44	-0.02	0.17	0.000	0.000	0.000	0.000	0.000	0.000
12	0.951	241.2	3.72	-0.02	0.16	0.000	0.000	0.000	0.000	0.000	0.000
13	0.951	240.7	4.01	-0.03	0.16	0.000	0.000	0.000	0.000	0.000	0.000
14	0.952	241.2	4.29	-0.03	0.16	0.000	0.000	0.000	0.000	0.000	0.000

RUN	TST	P	TN	CNF	MACH	RNL	PT	G	P	TT	ALPHA
368	571	1	66	7	0.950	1.473	681	240.7	381	67.6	0.00
SFG	MACH	G	X/DB	Y/DB	Z/DB	MF/N	WA/M	QF/Q	QA/Q	VF/V	VA/V
1	0.950	240.7	0.53	0.01	0.25	0.257	0.247	0.048	0.045	0.277	0.267
2	0.950	240.7	0.82	0.01	0.25	0.327	0.236	0.080	0.040	0.362	0.256
3	0.950	240.7	1.11	0.00	0.25	0.285	0.164	0.056	0.019	0.308	0.178
4	0.951	241.2	1.40	0.00	0.25	0.337	0.191	0.078	0.025	0.362	0.207
5	0.951	241.2	1.68	-0.00	0.24	0.368	0.269	0.095	0.050	0.395	0.290
6	0.951	241.2	1.98	-0.01	0.24	0.439	0.346	0.140	0.087	0.469	0.372
7	0.951	241.2	2.27	-0.01	0.24	0.405	0.354	0.129	0.098	0.434	0.380
8	0.951	241.2	2.55	-0.01	0.24	0.356	0.300	0.108	0.076	0.383	0.323
9	0.950	240.7	2.85	-0.01	0.24	0.215	0.201	0.043	0.037	0.233	0.218
10	0.948	240.3	3.14	-0.02	0.23	0.000	0.041	0.000	0.002	0.000	0.045
11	0.951	241.2	3.44	-0.02	0.23	0.000	0.000	0.000	0.000	0.000	0.005
12	0.951	241.2	3.73	-0.02	0.23	0.000	0.000	0.000	0.000	0.000	0.008
13	0.950	240.7	4.01	-0.02	0.23	0.000	0.000	0.000	0.000	0.000	0.022

RUN	TST	P	TN	CCNF	MACH	RN/L	PT	G	P	TT	ALPHA
SEQ	MACH	C	X/DR	Y/DR	Z/DR	MF/N	MA/M	QF/Q	QA/Q	VF/V	V4/V
369	571	1	66	7	0.950	1.485	689	243.5	385	68.8	0.00
1	0.950	243.5	C.53	C.01	0.40	0.267	0.184	0.053	0.025	0.289	0.199
2	0.949	243.0	0.82	0.01	0.40	0.265	0.000	0.051	0.000	0.286	0.00
3	0.949	243.0	1.11	0.00	0.40	0.251	0.000	0.044	0.000	0.272	-0.441
4	0.949	243.1	1.41	C.00	0.39	0.165	0.000	0.020	0.000	0.184	-0.495
5	0.949	243.1	1.69	-0.00	0.39	0.204	0.173	0.029	0.021	0.221	-0.485
6	0.949	243.1	1.99	-C.01	0.39	0.268	0.299	0.052	0.005	0.289	-0.437
7	0.949	243.6	2.27	-C.C1	0.39	0.242	0.296	C.046	C.068	0.263	0.358
8	0.949	243.6	2.56	-C.C1	0.39	0.177	0.233	0.026	0.046	0.191	0.252
9	0.949	243.6	2.85	-C.C1	0.38	0.066	0.130	0.003	0.015	0.065	0.141
10	0.949	243.0	3.14	-0.02	0.38	C.000	C.000	0.000	0.000	0.000	-0.074
11	C.950	243.0	3.44	-C.C2	0.38	C.000	C.000	0.000	0.000	0.000	0.008
12	0.952	243.5	2.73	-C.C2	0.38	C.000	C.000	0.000	0.000	0.000	0.029
13	C.952	243.5	4.02	-C.03	0.38	C.000	C.000	0.000	0.000	0.000	1.019

RUN	TST	P	TN	CCNF	MACH	RN/L	PT	G	P	TT	ALPHA
SEQ	MACH	C	X/DR	Y/DR	Z/DR	MF/N	MA/M	QF/Q	QA/Q	VF/V	V4/V
370	571	1	66	7	0.948	1.490	688	242.7	386	69.6	0.00
1	0.948	242.7	C.53	C.01	0.50	0.196	0.053	0.029	0.019	0.212	-0.402
2	0.947	242.1	C.82	C.01	0.50	0.164	0.164	0.019	0.017	0.177	0.748
3	0.947	242.1	1.11	C.00	0.50	0.148	0.148	0.015	0.015	0.160	-0.444
4	0.947	242.1	1.41	0.00	0.50	C.000	C.000	0.000	0.000	0.000	0.696
5	0.949	243.0	1.69	-C.00	0.49	0.064	0.064	0.003	0.003	0.070	-0.495
6	0.948	242.7	1.98	-0.01	0.49	C.139	0.185	0.014	0.025	0.151	0.260
7	0.949	243.1	2.27	-C.01	0.49	0.000	0.184	0.000	0.027	0.000	0.342
8	0.950	243.5	2.56	-C.C1	0.49	C.049	0.109	0.002	0.010	0.053	0.119
9	C.949	243.0	2.85	-C.01	0.49	0.000	0.042	0.009	0.002	0.000	0.045
10	C.948	242.6	3.14	-C.C2	0.48	C.000	C.000	0.000	0.000	0.000	0.070
11	C.950	243.0	3.44	-0.02	0.48	C.000	C.000	0.000	0.000	0.000	0.993
12	C.949	242.5	3.73	-C.02	0.48	C.000	C.000	0.000	0.000	0.000	0.019
13	C.951	242.9	4.01	-C.C3	0.48	C.000	C.000	0.000	0.000	0.000	1.014

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RUN	TST	P	TIN	CCNF	MACH	RN/L	PT	G	P	TT	ALPHA
371	571	1	66	7	0.899	1.482	704	235.6	416	70.1	0.00
SEC	MACH	Q	X/DR	Y/DR	Z/DR	NF/N	MA/M	QF/Q	QA/Q	VF/V	VΔ/V
1	0.899	235.6	C.53	C.01	0.19	0.248	0.257	0.048	0.051	0.266	-0.395
2	0.902	236.4	C.82	C.C1	0.18	C.298	0.173	0.066	0.022	0.319	0.186
3	0.906	237.1	1.11	C.00	0.18	0.345	0.168	0.087	C.021	0.368	0.181
4	0.904	236.2	1.41	C.00	0.18	C.411	0.242	0.124	C.043	0.437	0.260
5	0.901	234.8	1.69	-0.00	0.18	C.474	0.300	0.168	C.067	0.502	0.321
6	0.900	234.9	1.98	-C.C1	0.18	C.484	0.386	0.181	0.115	0.512	0.411
7	0.901	235.4	2.27	-C.C1	0.17	C.456	0.359	0.174	0.108	0.484	0.383
8	0.899	235.1	2.56	-C.C1	0.17	C.352	0.301	0.111	C.081	0.375	0.322
9	0.897	234.6	2.85	-C.C1	0.17	C.207	0.201	0.041	C.038	0.222	0.216
10	0.899	235.6	3.14	-0.02	0.17	C.054	0.070	0.003	0.005	0.059	0.076
11	0.900	236.0	3.44	-0.02	0.17	C.000	0.000	0.000	0.000	0.000	0.000
12	0.902	236.4	3.73	-C.C2	0.16	C.000	0.000	0.000	0.000	0.000	0.000
13	0.903	236.8	4.01	-0.03	0.16	C.000	0.000	0.000	0.000	0.000	0.000

RUN	TST	P	TIN	CCNF	MACH	RN/L	PT	G	P	TT	ALPHA
372	571	1	66	7	0.902	1.479	702	235.8	414	70.5	0.00
SEC	MACH	Q	X/DR	Y/DR	Z/DR	NF/N	MA/M	QF/Q	QA/Q	VF/V	VΔ/V
1	0.902	235.8	C.53	C.C1	0.25	C.229	0.224	0.045	C.039	0.256	0.240
2	0.901	235.4	C.82	C.01	0.25	C.365	0.279	0.101	C.059	0.389	0.258
3	0.899	235.0	1.11	C.00	0.25	C.375	0.208	0.104	C.032	0.400	0.224
4	0.899	235.0	1.41	C.00	0.24	C.404	0.247	0.119	C.045	0.430	0.265
5	0.898	234.6	1.69	-0.00	0.24	C.453	0.313	0.151	C.072	0.480	0.325
6	0.898	234.6	1.98	-C.C1	0.24	C.442	0.328	0.150	C.082	0.469	0.351
7	0.898	234.6	2.27	-C.C1	0.24	C.428	0.339	0.150	C.094	0.455	0.362
8	0.898	234.6	2.56	-C.C1	0.24	C.357	0.306	0.112	C.082	0.381	0.328
9	0.898	234.6	2.85	-C.C1	0.24	C.173	0.126	0.028	C.015	0.186	0.125
10	0.899	235.0	3.14	-C.C2	0.23	C.023	0.083	0.001	C.007	0.025	0.050
11	0.901	235.4	3.44	-C.C2	0.23	C.000	0.000	0.000	0.000	0.000	0.000
12	0.902	235.8	3.73	-C.C2	0.23	C.000	0.000	0.000	0.000	0.000	0.000
13	0.902	235.8	4.01	-C.C3	0.23	C.000	0.000	0.000	0.000	0.000	0.000

RUN	TST	F	TN	CCNF	MACH	RN/L	PT	C	P	TT	ALPHA		
SEQ	MACH	G	X/DR	Y/DR	Z/DR	MF/N	MA/M	QF/Q	QA/Q	VF/V	VA/V	CP	DF/P
373	571	1	66	7	0.899	1.475	702	235.0	415	70.9	0.00		
1	0.899	235.5	C.53	C.01	0.40	C.279	0.184	0.061	0.027	0.299	0.158	-0.381	0.785
2	0.900	235.5	C.82	C.01	0.40	C.276		0.058		0.295		-0.419	0.762
3	0.900	235.5	1.11	0.00	0.40	C.297		0.065		0.318		-0.466	0.736
4	0.900	235.5	1.41	0.00	0.40	C.293	0.039	0.062	0.001	0.314	0.042	-0.492	0.720
5	0.900	235.5	1.69	-0.00	0.39	C.269	0.228	0.052	0.038	0.283	0.244	-0.481	0.727
6	0.902	235.5	1.98	-0.01	0.39	C.243	0.306	0.044	0.070	0.260	0.327	-0.436	0.752
7	0.900	234.9	2.27	-C.C1	0.39	C.192	0.278	C.030	0.063	0.206	0.298	-0.340	0.807
8	0.900	234.9	2.56	-C.C1	0.39	C.179	0.241	C.028	C.050	0.193	0.258	-0.229	0.870
9	0.900	234.9	2.85	-C.C1	0.39	C.000	0.113	0.000	0.012	0.000	0.122	-0.115	0.935
10	0.901	235.4	3.14	-C.C2	0.38	C.000				0.000		-0.025	0.986
11	0.901	235.4	3.44	-C.C2	0.38							0.033	1.C19
12	0.901	235.4	3.73	-C.C2	0.38							0.058	1.033
13	0.898	234.5	4.01	-C.C3	0.38	C.0CC						0.055	1.031

RUN	TST	F	TN	CCNF	MACH	RN/L	PT	C	P	TT	ALPHA		
SEQ	MACH	G	X/DR	Y/DR	Z/DR	MF/N	MA/M	QF/Q	QA/Q	VF/V	VA/V	CP	DF/P
374	571	1	66	7	0.898	1.473	701	234.5	415	71.1	0.00		
1	0.898	234.5	C.53	C.C1	0.50	0.144		0.016	0.155			-0.367	0.793
2	0.899	235.1	C.82	C.C1	0.50	C.275		C.058	0.295			-0.412	0.767
3	0.899	235.1	1.11	0.00	0.50	C.178		C.024	0.191			-0.455	0.742
4	0.899	235.1	1.41	0.00	0.50							-0.458	0.741
5	0.900	235.5	1.69	-0.00	0.49	C.082		C.005	0.088			-0.480	0.728
6	0.903	236.3	1.99	-C.01	0.49	C.130	0.147	0.013	0.016	0.140	0.159	-0.433	0.753
7	0.905	236.7	2.27	-C.C1	C.49	C.113	0.202	0.010	C.033	0.122	0.217	-0.332	0.810
8	0.902	235.8	2.56	-C.C1	0.49	C.143	0.210	0.018	C.039	0.154	0.226	-0.224	0.872
9	0.900	234.9	2.85	-C.C1	0.49	C.CCC	0.000	C.000	C.000	0.000	C.000	-0.120	0.932
10	0.902	235.5	3.14	-C.C2	0.48							-0.029	0.983
11	0.902	235.5	3.44	-C.C2	0.48							0.023	1.C13
12	0.902	235.9	3.73	-C.C2	0.48							0.043	1.025
13	0.900	235.5	4.01	-C.C3	0.48							0.035	1.C20

RUN	TST	P	TN	CCNF	MACH	RNL	PT	C	P	TT	ALPHA
375	571	1	66	7	0.850	1.497	730	230.1	455	71.5	0.00
SEQ	MACH	C	X/DB	Y/DB	Z/DB	MF/N	MA/M	QF/Q	QA/Q	VF/V	VA/V
1	0.850	230.1	0.53	0.01	0.18	0.238	0.181	0.045	0.026	0.254	0.193
2	0.852	230.8	0.82	0.01	0.18	0.297	0.189	0.068	0.028	0.316	0.202
3	0.852	230.8	1.11	0.00	0.18	0.419	0.202	0.133	0.031	0.443	0.215
4	0.852	230.9	1.40	0.00	0.18	0.441	0.242	0.149	0.045	0.466	0.257
5	0.852	230.9	1.69	-C.00	0.18	0.512	0.337	0.203	0.088	0.538	0.358
6	0.850	230.1	1.98	-C.01	0.18	0.519	0.396	0.218	0.127	0.544	0.419
7	0.847	229.4	2.27	-C.01	0.17	0.457	0.357	0.179	0.110	0.481	0.379
8	0.849	230.3	2.56	-C.01	0.17	0.342	0.276	0.107	0.069	0.364	0.294
9	0.850	230.7	2.85	-C.01	0.17	0.186	0.145	0.034	0.020	0.199	0.155
10	0.850	230.7	3.14	-C.02	0.17	0.000	0.000	0.000	0.000	0.000	0.000
11	0.849	230.2	3.44	-C.02	0.17	0.000	0.000	0.000	0.000	0.000	0.000
12	0.848	229.9	3.73	-C.02	0.16	0.000	0.000	0.000	0.000	0.000	0.000
13	0.848	229.9	4.01	-C.03	0.16	0.000	0.000	0.000	0.000	0.000	0.000

RUN	TST	P	TN	CCNF	MACH	RNL	PT	C	P	TT	ALPHA
376	571	1	66	7	0.848	1.497	731	229.9	457	71.6	0.00
SEQ	MACH	C	X/DB	Y/DB	Z/DB	MF/N	MA/M	QF/Q	QA/Q	VF/V	VA/V
1	0.848	229.9	0.53	0.01	0.25	0.254	0.254	0.052	0.052	0.270	0.271
2	0.850	230.7	0.80	0.01	0.25	0.340	0.248	0.090	0.048	0.361	0.264
3	0.851	230.6	1.11	C.00	0.25	0.365	0.169	0.101	0.022	0.387	0.181
4	0.852	230.5	1.41	C.00	0.24	0.408	0.255	0.126	0.049	0.432	0.271
5	0.851	230.6	1.69	-C.00	0.24	0.469	0.321	0.167	0.078	0.494	0.341
6	0.852	230.5	1.98	-C.01	0.24	0.457	0.338	0.164	0.090	0.481	0.359
7	0.852	230.9	2.27	-C.01	0.24	0.466	0.351	0.137	0.103	0.429	0.373
8	0.853	231.2	2.56	-C.01	0.24	0.288	0.284	0.074	0.072	0.307	0.302
9	0.854	231.2	2.85	-C.01	0.24	0.135	0.123	0.018	0.015	0.145	0.131
10	0.851	230.5	3.13	-C.02	0.22	0.000	0.040	0.000	0.000	0.043	0.012
11	0.851	230.6	3.44	-C.02	0.23	0.000	0.000	0.000	0.000	0.000	0.000
12	0.851	231.0	3.73	-C.02	0.23	0.000	0.000	0.000	0.000	0.000	0.000
13	0.851	230.6	4.01	-C.03	0.23	0.000	0.000	0.000	0.000	0.000	0.000

RUN	TST	F	TN	CENF	MACH	RA/L	PT	G	P	TT	ALPHA
SFC	MACH	0	X/DR	Y/DR	Z/DR	MF/N	MA/M	CF/Q	QA/Q	VF/V	VA/V
377	571	1	66	7	0.853	1.502	727	230.1	452	69.0	0.00
	SFC	MACH	0	X/DR	Y/DR	Z/DR	MF/N	MA/M	CF/Q	QA/Q	VF/V
2	0.853	230.1	C.53	C.C1	0.40	C.251	0.174	C.051	C.025	0.267	0.186
3	0.850	229.4	C.81	C.C1	0.40	C.222	0.000	C.039	0.000	0.237	0.000
4	0.848	228.6	1.10	C.CC	0.40	C.271	0.075	C.056	0.004	0.288	0.080
5	0.848	228.6	1.41	0.00	0.40	C.266	0.000	C.053	C.000	0.283	0.000
6	0.850	229.0	1.69	-C.00	0.39	C.320	0.145	C.078	0.016	0.340	0.155
7	0.850	229.0	1.98	-C.C1	0.29	C.3C4	0.303	C.072	C.072	0.323	0.322
8	0.850	228.9	2.27	-0.01	0.39	C.263	0.311	C.058	0.061	0.280	0.320
9	0.851	229.2	2.56	-C.01	0.39	C.140	0.243	C.018	0.018	0.150	0.258
10	0.851	229.2	2.85	-C.C1	0.28	C.84	0.168	C.007	C.027	0.039	0.180
11	0.852	229.8	3.13	-C.02	0.38						
12	0.852	229.8	3.44	-C.C2	0.28						
13	0.852	229.8	3.72	-C.02	0.38						
14	0.85C	229.0	4.01	-0.C3	0.38						

RUN	TST	F	TN	CENF	MACH	RA/L	PT	G	P	TT	ALPHA
SFC	MACH	5	X/DR	Y/DR	Z/DR	MF/N	MA/M	CF/Q	QA/Q	VF/V	VA/V
278	571	1	66	7	0.849	1.494	726	228.5	453	69.8	0.00
	SFC	MACH	5	X/DR	Y/DR	Z/DR	MF/N	MA/M	CF/Q	QA/Q	VF/V
1	0.849	228.5	C.53	C.C1	0.50	0.124	0.013	0.133	0.000	0.212	-0.368
2	0.848	228.6	C.81	C.C1	0.50	0.225	0.040	0.240	0.000	0.240	-0.414
3	0.849	229.1	1.11	C.00	0.50	0.203	0.032	0.216	0.000	0.216	-0.461
4	0.854	23C.5	1.49	C.CC	0.50	0.199	0.029	0.212	0.000	0.212	-0.500
5	0.854	23C.5	1.69	-C.CC	0.49	C.114	0.CC0	C.010	0.000	0.122	-0.474
6	0.854	23C.0	1.98	-C.C1	0.49	C.162	0.234	C.021	0.043	0.174	-0.413
7	0.852	229.7	2.27	-C.C1	0.49	C.156	0.249	C.021	0.052	0.167	-0.249
8	0.852	229.8	2.55	-C.C1	0.49	C.032	0.114	C.CC1	C.012	0.035	-0.122
9	0.852	229.7	2.85	-C.C1	0.49	0.000	0.000	0.000	0.000	0.000	-0.090
10	0.852	230.3	3.14	-C.C2	0.48						-0.011
11	0.851	230.0	3.44	-C.02	0.48						0.040
12	0.851	230.0	3.73	-C.C2	0.48						0.045
13	0.853	230.2	4.01	-C.C3	0.48						0.039

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RUN	TST	F	TN	CCNF	MACH	RN/L	PT	G	TT	ALPHA	
										P	PF/P
379	571	1	66	7	C.799	1.520	762	223.2	5CC	70.5	0.00
SFG	MACH	G	X/DB	Y/DR	Z/DR	NF/N	MF/M	QF/Q	OA/Q	VF/V	VA/V
1	0.798	223.2	0.53	C.01	0.18	C.237	0.189	0.046	0.030	0.251	0.201
2	0.799	223.8	0.82	C.01	0.18	C.371	0.203	0.110	0.033	0.390	0.216
3	C.798	223.3	1.11	0.00	0.18	C.444	0.252	0.155	C.050	0.466	0.267
4	0.797	222.8	1.41	C.00	0.18	C.475	0.306	C.177	0.073	0.497	0.323
5	0.799	223.2	1.69	-0.00	0.18	0.512	0.394	0.298	0.123	0.555	0.414
6	C.798	222.7	1.98	-C.01	0.18	0.492	0.381	0.200	0.120	0.515	0.4C1
7	C.798	222.7	2.27	-C.01	0.17	C.332	0.269	C.098	C.065	0.350	0.284
8	0.798	222.7	2.56	-C.01	0.17	0.257	0.244	0.063	0.056	0.272	0.258
9	0.798	222.7	2.85	-C.01	0.17	C.CCC	0.000	0.000	0.000	0.000	0.000
10	0.798	222.7	3.13	-C.02	0.17	C.000	0.000	0.000	0.000	0.000	0.000
11	C.798	222.7	2.44	-C.C2	0.17	C.000	0.000	0.000	0.000	0.000	0.000
12	0.798	222.7	3.73	-0.02	0.16	C.000	0.000	0.000	0.000	0.000	0.000
13	0.797	222.7	4.C1	-C.C3	0.16						

RUN	TST	P	TN	CCNF	MACH	RN/L	PT	G	TT	ALPHA	
										P	PF/P
380	571	1	66	7	0.892	1.520	760	224.2	497	70.8	0.00
SFG	MACH	G	X/DB	Y/DR	Z/DR	NF/N	MF/M	QF/Q	OA/Q	VF/V	VA/V
1	0.802	224.2	0.53	C.01	0.25	0.227	0.172	0.042	0.025	0.241	0.184
2	0.804	224.6	0.82	0.01	0.25	C.378	0.231	0.114	C.042	0.399	0.244
3	0.804	224.6	1.11	0.00	0.25	C.377	0.235	0.112	0.043	0.397	0.243
4	0.801	223.6	1.41	C.00	0.24	0.459	0.278	0.164	0.060	0.481	0.294
5	0.801	223.7	1.69	-C.00	0.24	2.445	0.343	0.157	0.093	0.467	0.361
6	0.802	224.2	1.99	-C.01	0.24	C.422	C.351	C.147	C.102	0.444	0.370
7	C.800	223.7	2.27	-C.01	0.24	0.364	0.354	0.116	0.110	0.384	0.373
8	0.801	224.2	2.55	-C.C1	0.24	C.154	0.232	0.035	C.051	0.205	0.247
9	0.799	223.2	2.85	-C.01	0.24	C.000	0.084	0.000	C.07	0.000	0.089
10	0.799	223.2	3.14	-C.02	0.23	C.000	0.000	0.000	0.000	0.000	0.000
11	0.799	223.2	3.44	-C.02	0.23	C.000	C.000	C.000	C.000	C.000	C.000
12	C.801	223.7	3.73	-C.02	0.23						
13	0.799	224.2	4.C1	-C.C3	0.23						

RUN	TST	P	TN	CCNF	MACH	RN/L	PT	C	P	TT	ALPHA
381	571	1	66	7	0.801	1.517	760	223.7	498	71.1	0.00
SEQ	MACH	Q	X/CB	Y/CB	Z/DB	MF/N	MA/M	QF/Q	QA/Q	VF/V	VA/V
1	0.8C1	223.7	C.53	C.C1	0.40	C.232	0.074	0.044	0.004	0.246	0.391
2	0.799	222.6	C.82	C.C1	0.40	C.273	0.000	0.060	0.000	0.283	0.424
3	0.799	223.2	1.11	0.00	0.40	0.346	0.000	0.093	0.000	0.364	0.488
4	0.799	223.2	1.40	0.00	0.39	C.285	0.030	0.063	0.001	0.301	0.504
5	0.799	223.2	1.69	-0.00	0.39	C.306	0.233	0.073	0.042	0.323	0.493
6	0.800	223.7	1.99	-C.01	0.39	C.241	0.312	0.047	0.080	0.255	0.408
7	0.800	223.7	2.26	-C.C1	0.39	C.146	0.259	0.019	0.059	0.155	0.274
8	0.800	223.7	2.56	-C.C1	0.39	0.000	0.127	0.000	0.015	0.000	0.134
9	0.801	224.2	2.84	-C.C1	0.38	C.CCC	0.000	0.000	0.000	0.000	0.000
10	0.800	223.7	3.14	-0.02	0.38						0.028
11	0.799	223.2	3.44	-C.02	0.38	C.000					1.012
12	0.801	223.7	3.72	-C.02	0.38	C.000					0.037
13	0.800	223.1	4.01	-C.03	0.38						1.017

RUN	TST	P	TN	CCNF	MACH	RN/L	PT	C	P	TT	ALPHA
382	571	1	66	7	0.800	1.518	761	223.7	499	71.3	0.00
SEQ	MACH	Q	X/CB	Y/CB	Z/DB	MF/N	MA/M	QF/Q	QA/Q	VF/V	VA/V
1	0.800	223.7	C.53	C.01	0.50	C.182	0.027	0.193			0.824
2	0.800	223.7	C.82	C.01	0.50	C.221	0.039	0.234			0.808
3	0.800	223.7	1.10	C.00	0.50	0.234	0.043	0.248			0.782
4	0.802	224.2	1.40	C.00	0.49	0.157	0.019	0.166			0.772
5	0.801	223.7	1.69	-0.00	0.49	C.131	0.105	0.013	0.009	0.139	0.479
6	0.801	223.7	1.98	-C.01	0.49	C.134	0.244	0.015	0.049	0.142	0.259
7	0.801	223.7	2.26	-C.C1	0.49	C.165	0.256	0.024	0.057	0.175	0.271
8	0.801	223.7	2.56	-C.C1	0.49	C.000	0.119	0.000	0.013	0.000	0.126
9	0.801	223.7	2.84	-C.C1	0.48						0.976
10	0.801	223.7	3.14	-C.C2	0.48						1.006
11	0.801	223.7	3.44	-C.02	0.48	C.000					1.016
12	0.799	223.2	3.72	-C.02	0.48						1.018
13	0.799	223.2	4.01	-C.C3	0.48						1.019

RUN	TST	P	TN	CCNF	MACH	RN/L	PT	G	P	TT	ALPHA
SFG	MACH	G	X/DR	Y/DR	Z/DB	MF/N	MA/M	QF/Q	QA/Q	VF/V	VA/V
383	571	1	66	7	0.601	1.513	900	178.5	705	70.3	0.00
	MACH	G	C.53	C.C1	0.18	0.298	0.244	0.080	0.054	0.308	0.252
1	0.601	178.5	C.82	C.C1	0.18	C.410	0.360	0.148	0.114	0.422	-0.382
2	0.599	177.3	C.01	C.00	0.18	C.502	0.370	C.221	C.120	0.515	0.466
3	0.597	176.7	1.10	C.00	0.18	C.536	0.394	0.253	0.137	0.549	-0.496
4	0.597	176.7	1.41	C.00	0.18	C.494	0.375	C.220	0.126	0.507	-0.486
5	0.597	176.7	1.69	-C.00	0.18	C.494	0.375	C.220	0.126	0.507	-0.401
6	0.597	176.7	1.99	-0.01	0.18	C.373	0.340	0.130	C.109	0.384	-0.252
7	0.600	177.9	2.26	-C.C1	0.17	C.140	0.159	0.019	0.025	0.145	0.165
8	0.599	177.3	2.56	-C.01	0.17	C.000	0.000	C.000	0.000	0.000	0.015
9	0.599	177.3	2.85	-C.C1	0.17	C.000	0.000	C.000	0.000	0.000	0.012
10	0.600	177.9	3.13	-C.C2	0.17	C.000	0.000	C.000	0.000	0.000	0.011
11	0.600	177.9	3.43	-C.02	0.17	C.000	0.000	C.000	0.000	0.000	0.006
12	0.601	178.5	3.72	-C.C2	0.16						0.030
13	0.600	177.9	4.C1	-C.03	0.16						-0.001

RUN	TST	P	TN	CCNF	MACH	RN/L	PT	G	P	TT	ALPHA
SFG	MACH	G	X/DR	Y/DR	Z/DB	MF/N	MA/M	QF/Q	QA/Q	VF/V	VA/V
384	571	1	66	7	0.600	1.511	899	177.5	705	70.0	0.00
	MACH	G	C.53	C.C1	0.25	C.271	0.191	0.066	0.032	0.280	0.197
1	0.600	177.5	C.82	C.01	0.25	C.361	0.236	0.115	C.049	0.372	-0.435
2	0.602	178.5	C.01	C.CC	0.25	C.490	0.294	0.209	0.075	0.503	0.890
3	C.6C1	178.5	1.11	C.CC	0.25	C.492	0.362	C.213	0.115	0.506	-0.474
4	0.601	178.5	1.41	C.CC	0.24	C.446	0.313	0.180	0.088	0.459	-0.510
5	0.600	177.9	1.69	-C.00	0.24	C.446	0.313	0.180	0.088	0.459	-0.510
6	0.599	177.3	1.98	-C.C1	0.24	C.324	0.331	C.098	0.103	0.334	-0.510
7	0.599	177.3	2.27	-C.C1	0.24	C.165	0.299	C.026	C.087	0.170	-0.510
8	0.597	176.7	2.56	-C.C1	0.24	C.000	0.000	C.000	0.000	0.000	0.871
9	0.600	177.9	2.85	-C.C1	0.24	C.000	0.000	C.000	0.000	0.000	0.875
10	0.600	177.9	3.13	-C.02	0.23	C.000	0.000	C.000	0.000	0.000	0.915
11	0.601	178.5	3.44	-C.C2	0.23	C.000	0.000	C.000	0.000	0.000	0.971
12	0.600	177.9	3.73	-C.C2	0.23	C.000	0.000	C.000	0.000	0.000	1.000
13	0.602	178.5	4.C1	-C.C3	0.23						1.003

RUN	TST	P	TN	RCNF	MACH	RN/L	PT	C	P	TT	ALPHA
286	571	1	66	7	0.600	1.513	900	177.9	706	69.5	0.00
SEG	MACH	G	X/FN	Y/EP	Z/DB	MF/N	MA/M	GF/Q	OA/Q	VF/V	VA/V
1	0.600	177.9	C.53	C.C1	0.50	0.214	0.041	0.221	0.216	-0.447	0.887
2	0.600	177.9	C.82	C.01	0.50	C.2C9	0.039	0.273	-0.528	0.867	
3	0.600	177.9	1.11	C.00	0.50	0.265	0.061	0.194	0.000	-0.527	0.867
4	0.600	177.9	1.40	C.00	0.50	C.188	0.000	0.031	0.000	-0.417	0.895
5	0.600	177.9	1.69	-0.09	0.49	0.025	0.218	0.001	0.042	0.036	0.225
6	0.600	177.9	1.98	-C.C1	0.49	C.000	0.198	0.000	0.037	0.000	0.205
7	0.600	177.9	2.27	-0.C1	0.49	C.000	0.075	C.000	0.006	0.000	0.078
8	0.600	177.9	2.56	-0.C1	0.49	0.000	0.000	0.000	0.000	0.002	1.000
9	0.600	177.9	2.85	-C.C1	0.49	0.000	0.000	0.000	0.000	0.019	1.005
10	0.600	177.9	3.13	-0.02	0.48	C.000	0.000	0.000	0.000	0.026	1.006
11	0.600	177.9	3.44	-C.C2	0.48	C.000	0.000	0.000	0.000	0.023	1.006
12	0.600	178.5	3.72	-C.C2	0.48	C.000	0.000	0.000	0.000	0.010	1.002
13	0.600	177.9	4.C1	-C.C3	0.48	C.000	0.000	0.000	0.000	0.006	1.001

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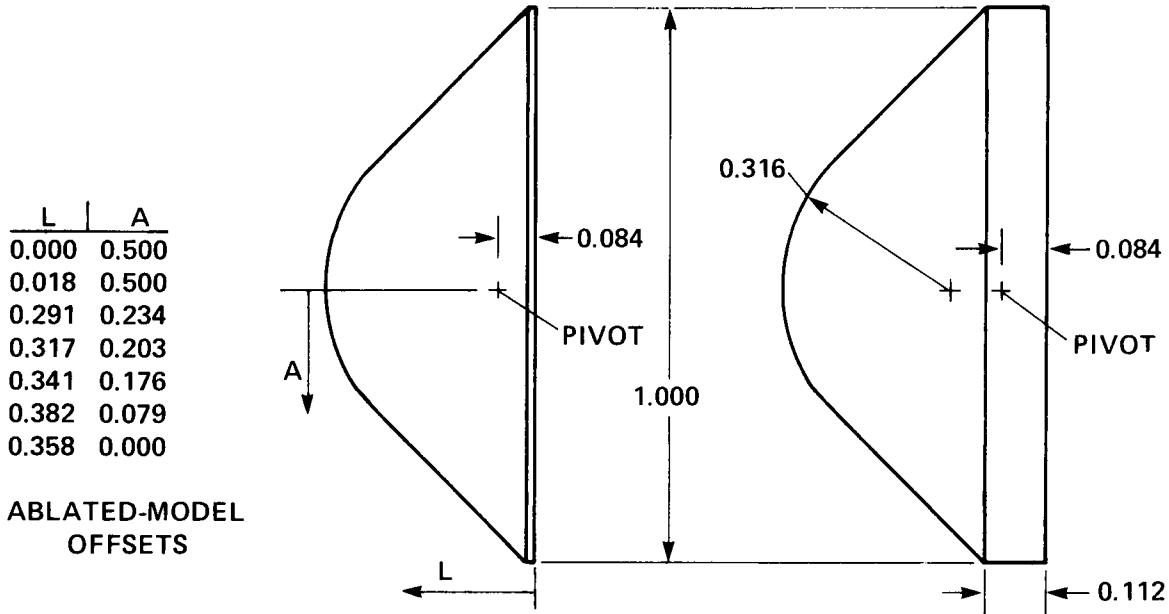
RUN	TST	P	TN	CCNF	MACH	PN/L	PT	C	P	TT	ALPHA
SEG	MACH	0	0.253	1.66	7	0.253	1.527	1884	8C.8	1802	66.4
1	0.253	80.8	0.53	c.c1	0.18	c.295	0.350	ma/n	gf/q	0a/q	vf/v
2	0.252	80.1	0.82	0.01	0.18	c.466	0.495	0.212	c.156	0.120	0.402
3	0.252	80.1	1.11	0.00	0.18	c.525	0.368	0.269	c.160	0.469	0.407
4	0.251	79.5	1.41	c.00	0.18	c.528	0.456	0.273	c.132	0.527	0.370
5	0.251	79.5	1.69	-c.cc	0.18	c.346	0.381	0.118	c.203	0.531	0.458
6	0.251	79.5	1.98	-c.01	0.18	c.002	0.136	0.000	c.018	0.000	0.127
7	0.252	80.1	2.27	-c.01	0.17	c.000	0.000	0.000	c.000	0.000	0.000
8	0.252	80.1	2.56	-c.c1	0.17	c.000	0.000	0.000	c.000	0.000	0.000
9	0.252	80.1	2.85	-c.01	0.17	c.000	0.000	0.000	c.000	0.000	0.000
10	0.252	80.1	3.13	-c.02	0.17	c.000	0.000	0.000	c.000	0.000	0.000
11	0.251	79.5	3.43	-0.02	0.17	c.000	0.000	0.000	c.000	0.000	0.000
12	0.251	79.5	3.72	-c.02	0.16	c.000	0.000	0.000	c.000	0.000	0.000
13	0.251	79.5	4.00	-c.03	0.16	c.000	0.000	0.000	c.000	0.000	0.000

RUN	TST	P	TN	CCNF	MACH	PN/L	PT	G	P	TT	ALPHA
SEG	MACH	0	0.251	1.66	7	0.251	1.516	1883	79.5	1802	65.8
1	0.251	79.5	c.53	c.01	0.25	0.245	0.334	0.059	c.109	0.246	0.000
2	0.252	80.1	c.82	c.c1	0.25	c.402	0.263	0.157	0.067	0.404	0.265
3	0.252	80.1	1.11	0.00	0.25	c.528	0.249	0.272	c.061	0.531	0.251
4	0.250	78.8	1.41	c.00	0.24	c.500	0.342	0.245	0.114	0.502	0.343
5	0.251	79.5	1.69	-c.00	0.24	c.289	0.354	0.082	0.124	0.290	0.356
6	0.250	78.8	1.98	-c.c1	0.24	c.134	0.144	0.018	c.021	0.135	0.145
7	0.251	79.5	2.26	-0.01	0.24	c.042	0.120	0.002	c.014	0.042	0.121
8	0.251	79.5	2.55	-c.01	0.24	c.000	0.000	0.000	c.000	0.000	0.000
9	0.250	78.8	2.85	-c.c1	0.24	c.073	0.000	0.005	c.000	0.074	0.000
10	0.250	78.8	3.13	-0.02	0.23	c.000	c.000	c.000	c.000	0.000	0.000
11	0.250	78.8	3.43	-c.02	0.23	c.000	c.000	c.000	c.000	0.000	0.000
12	0.251	79.5	3.73	-c.c2	0.23	c.000	c.000	c.000	c.000	0.000	0.000
13	0.251	79.5	4.01	-0.03	0.23	c.000	c.000	c.000	c.000	0.000	0.000

RUN	TST	P	TN	CENF	MACH	RN/L	PT	C	P	TT	ALPHA
389	571	1	66	7	0.252	1.524	1884	8C.1	1802	65.4	0.00
SFC	MACH	G	X/DR	Y/CP	Z/DR	MF/N	MA/N	CF/0	QA/Q	VF/V	CP
1	0.252	80.1	C.53	C.C1	0.40	C.11C	0.219	0.012	0.047	0.111	0.221
2	0.252	80.1	C.82	C.01	0.40	C.3C7	0.000	0.092	C.000	0.308	0.000
3	0.251	79.5	1.11	0.00	0.40	C.260	0.133	0.066	0.017	0.201	0.134
4	0.251	79.5	1.40	0.00	0.40	C.2CE	0.396	0.092	C.153	0.310	0.398
5	0.250	78.8	1.68	-C.00	0.39	C.204	0.371	0.041	C.136	0.206	0.373
6	0.250	78.8	1.98	-C.C1	0.39	C.120	0.232	0.014	C.053	0.121	0.233
7	0.251	79.5	2.27	-C.01	0.39	C.0CC	0.000	0.000	C.000	0.000	0.000
8	0.251	79.5	2.56	-C.C1	0.39	C.0CC	0.000	0.000	C.000	0.000	0.000
9	0.251	79.5	2.85	-C.C1	0.39	C.0CC	0.000	0.000	C.000	0.000	0.000
10	0.250	78.8	3.13	-C.02	0.38	C.0CC	0.000	0.000	C.000	0.000	0.000

RUN	TST	P	TN	CENF	MACH	RN/L	PT	C	P	TT	ALPHA
390	571	1	66	7	0.251	1.519	1884	79.5	1803	65.1	0.00
SFG	MACH	G	X/DR	Y/DR	Z/DR	MF/N	MA/N	CF/0	QA/Q	VF/V	CP
1	0.251	79.5	C.53	C.C1	0.50	C.259	0.000	0.066	C.000	0.261	0.000
2	0.251	79.5	C.82	C.C1	0.50	C.146	0.000	0.021	C.000	0.147	0.000
3	0.251	79.5	1.11	C.CC	0.50	C.221	0.000	0.048	C.000	0.223	0.000
4	0.251	79.5	1.41	0.00	0.50	C.07C	0.186	0.005	C.034	0.071	0.188
5	0.252	80.1	1.69	-C.CC	0.49	C.242	0.250	0.058	C.062	0.245	0.252
6	0.252	80.1	1.98	-0.01	0.49	C.CCC	0.000	0.000	C.000	0.000	0.000
7	0.252	80.1	2.27	-C.C1	0.49	C.CCC	0.000	0.000	C.000	0.000	0.000
8	0.252	80.1	2.56	-C.C1	0.49	C.0CC	0.000	0.000	C.000	0.000	0.000
9	0.252	80.1	2.85	-C.C1	0.49	C.0CC	0.000	0.000	C.000	0.000	0.000
10	0.252	80.1	3.13	-C.C2	0.48	C.CCC	0.000	0.000	C.000	0.000	0.000
11	0.252	80.1	3.44	-0.02	0.48	C.CCC	0.000	0.000	C.000	0.000	0.000
12	0.252	80.1	3.73	-C.C2	0.48	C.0CC	0.000	0.000	C.000	0.000	0.000
13	0.252	80.1	4.01	-C.03	0.48	C.0CC	0.000	0.000	C.000	0.000	0.000

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MODEL DIAMETER = 6 in.

Figure 1.— Scale models tested in 6-by 6-ft transonic wind tunnel. (a) Ablated configuration. (b) Ballasted configuration.

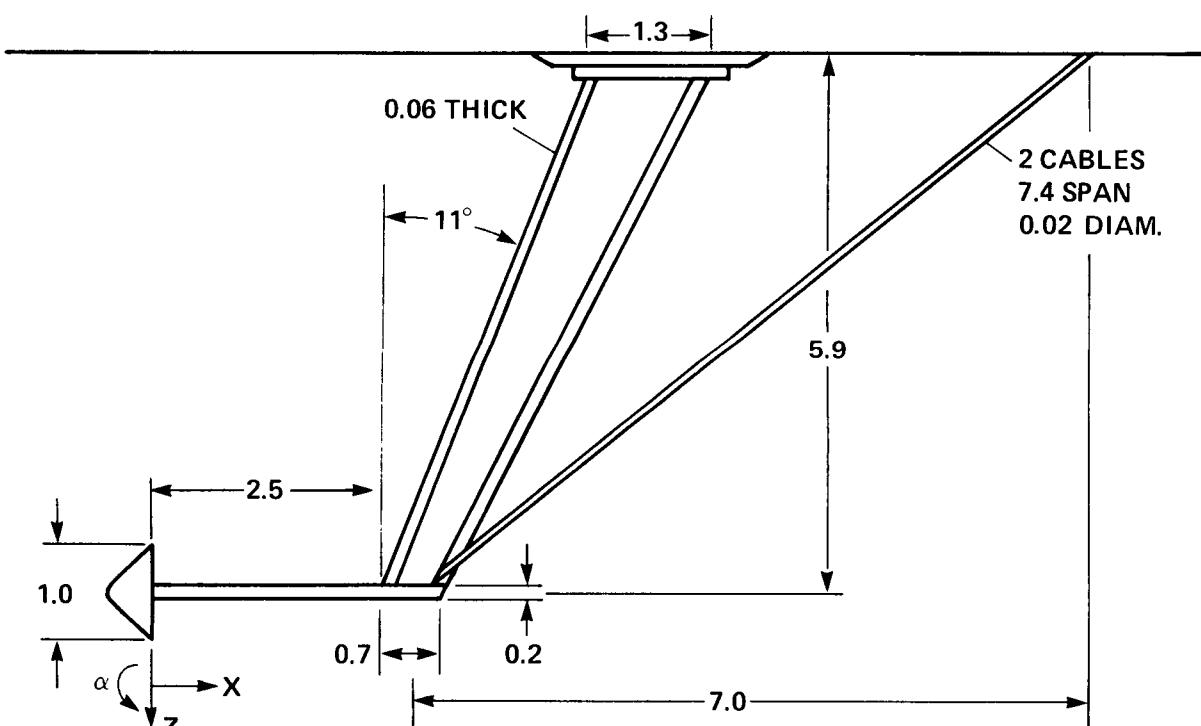
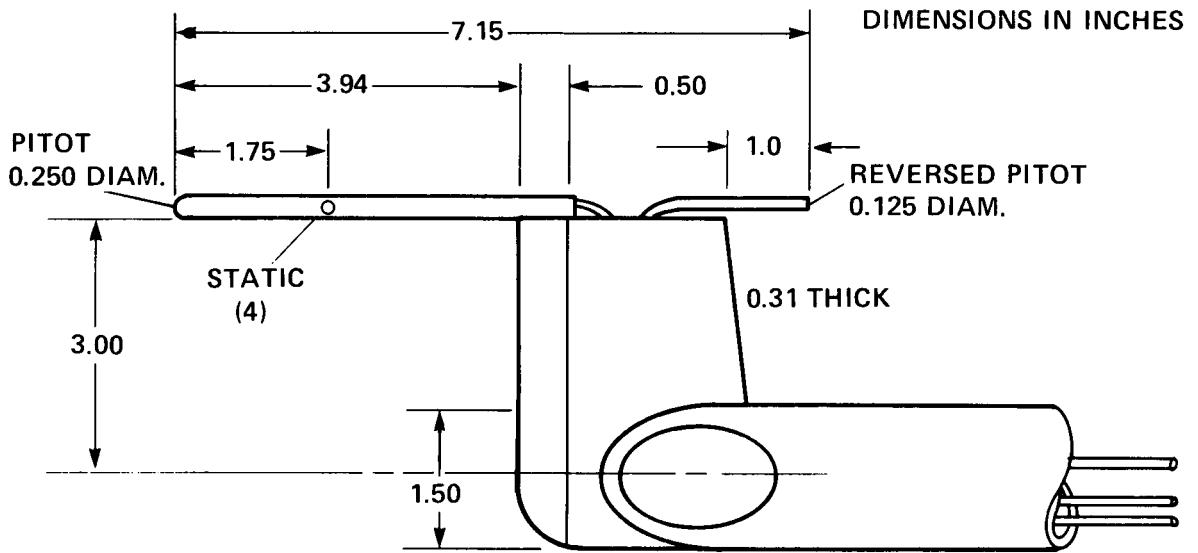
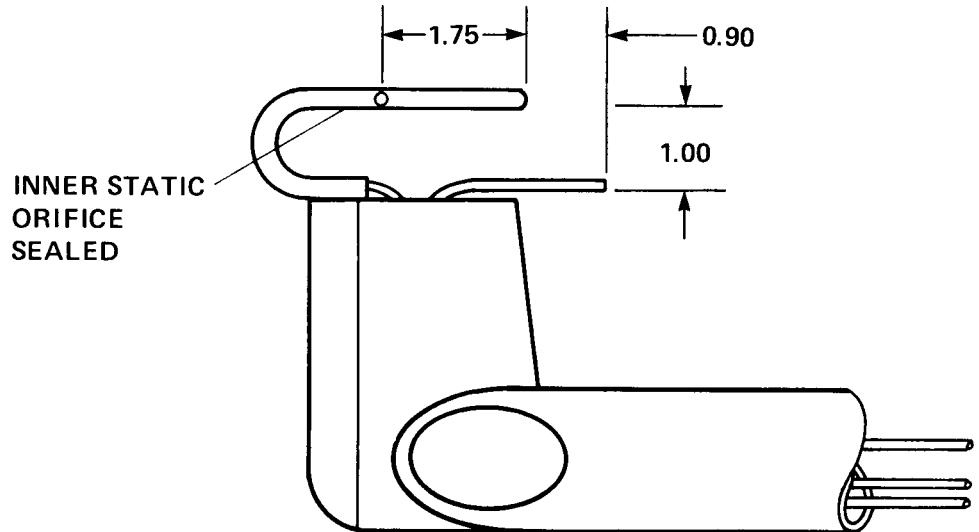


Figure 2.— Model and sting-strut support.



a) FAR-WAKE CONFIGURATION



b) NEAR-WAKE CONFIGURATION (CONFIGURATION "A" MODIFIED BY BENDING)

Figure 3.— Pitot-static probe.

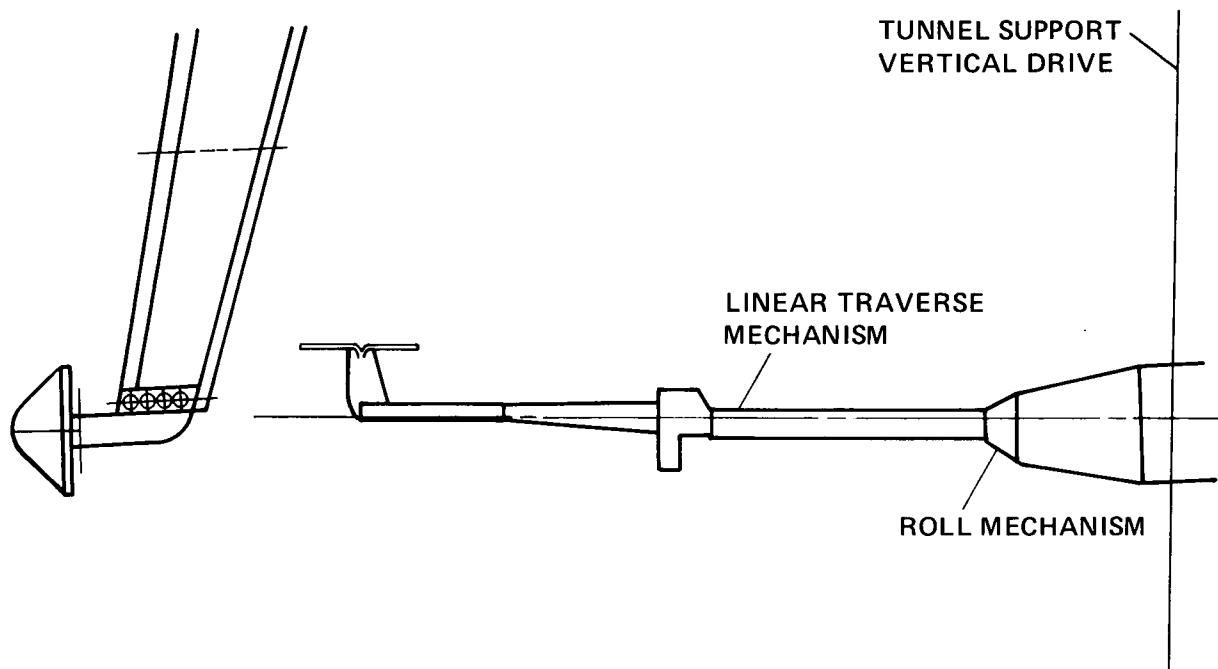


Figure 4.— Test setup.

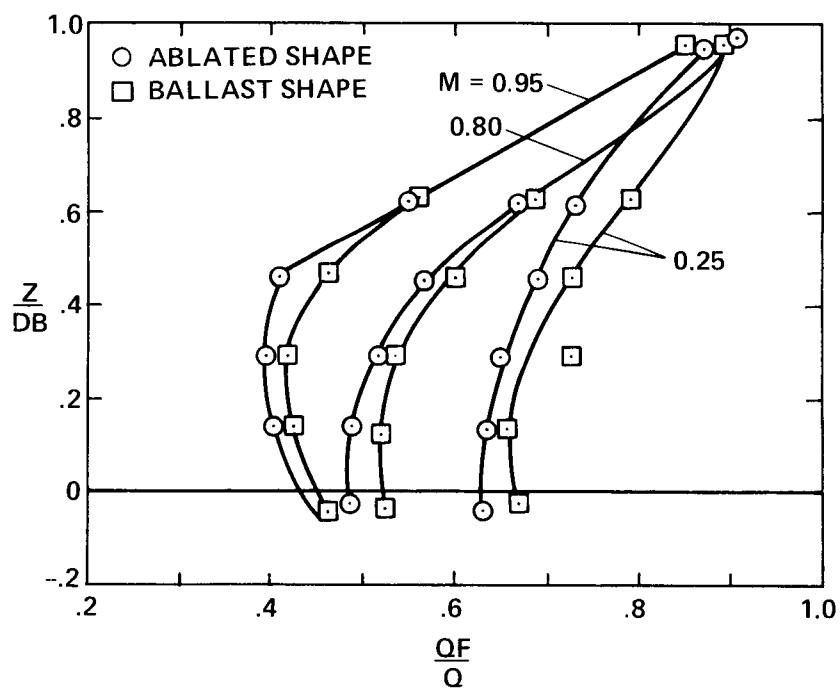
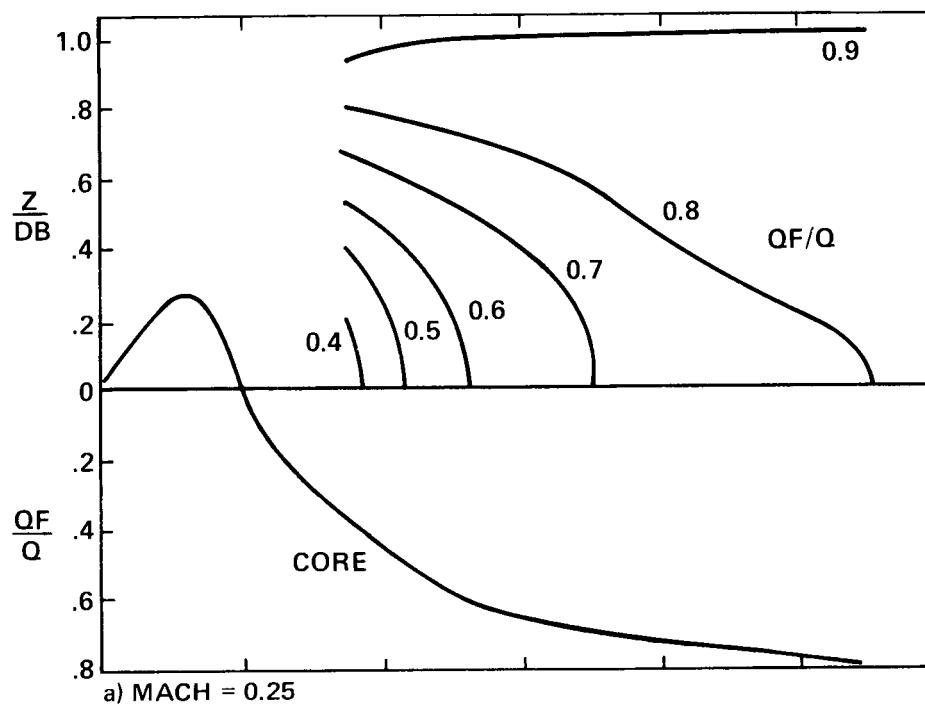


Figure 5.— Radial profiles of dynamic pressure.  $X/D_B = 5.5$ ,  $Y/D_B = 0$ ,  $R = 0.75$  million,  $\alpha = 0^\circ$ .



a) MACH = 0.25

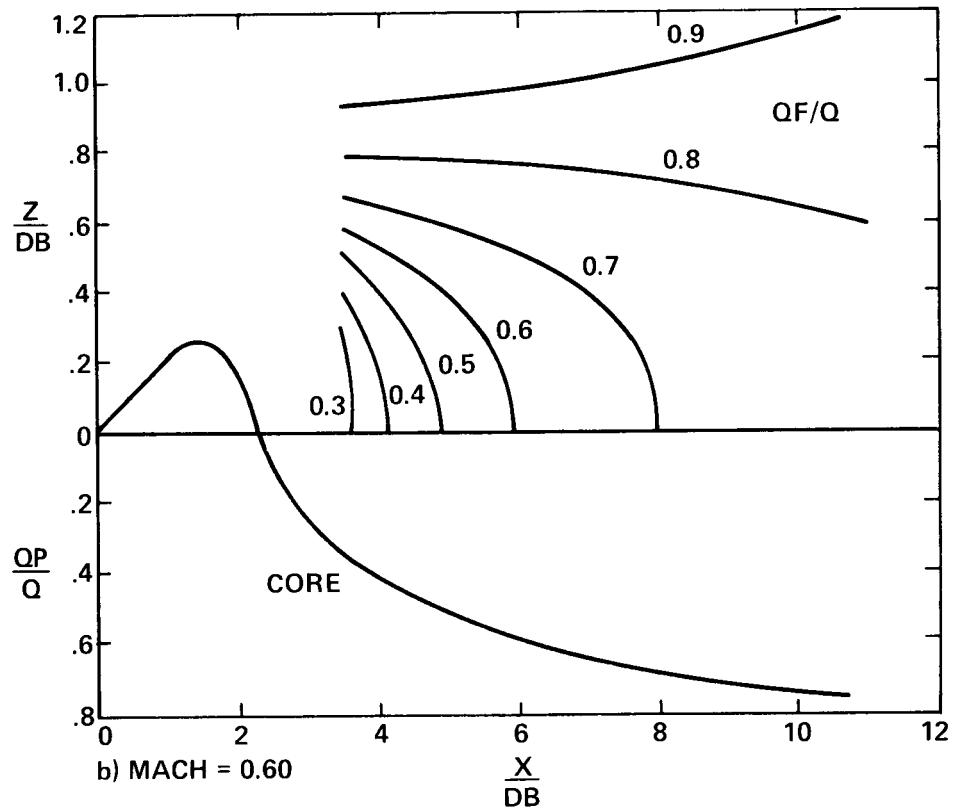


Figure 6.— Axial profile and spatial contours of dynamic pressure in wake of ablated Galileo probe.  $\alpha = 0.0^\circ$ ,  $R_D = 0.75$  Million.

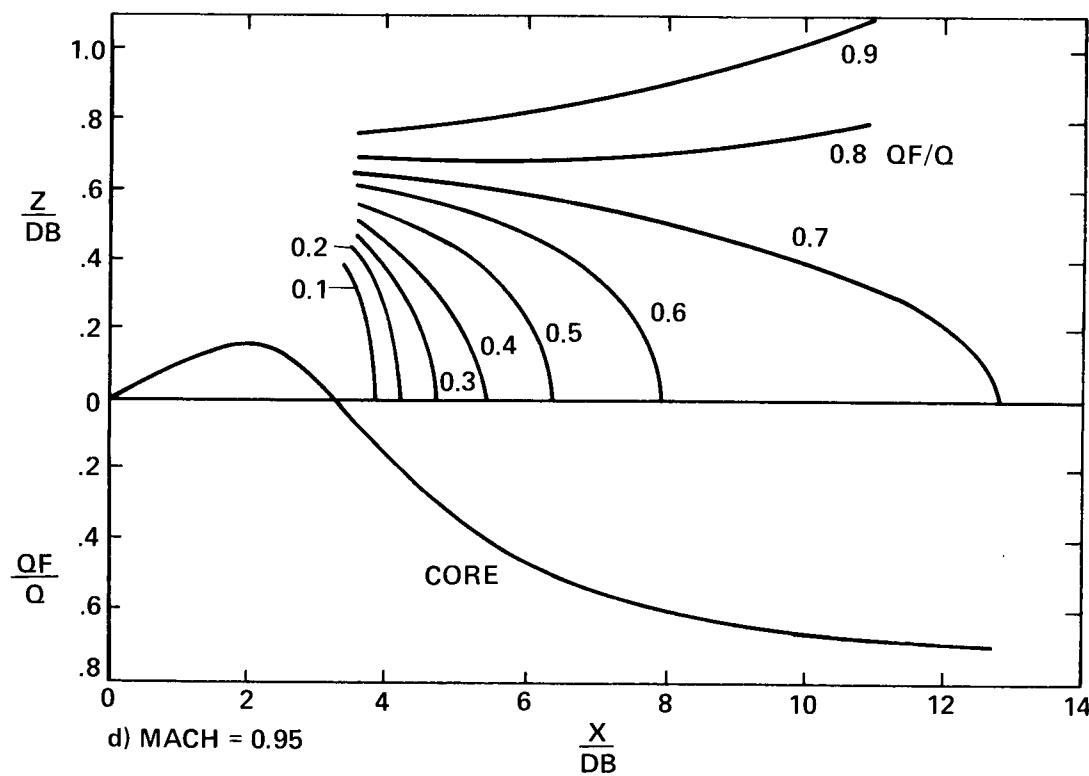
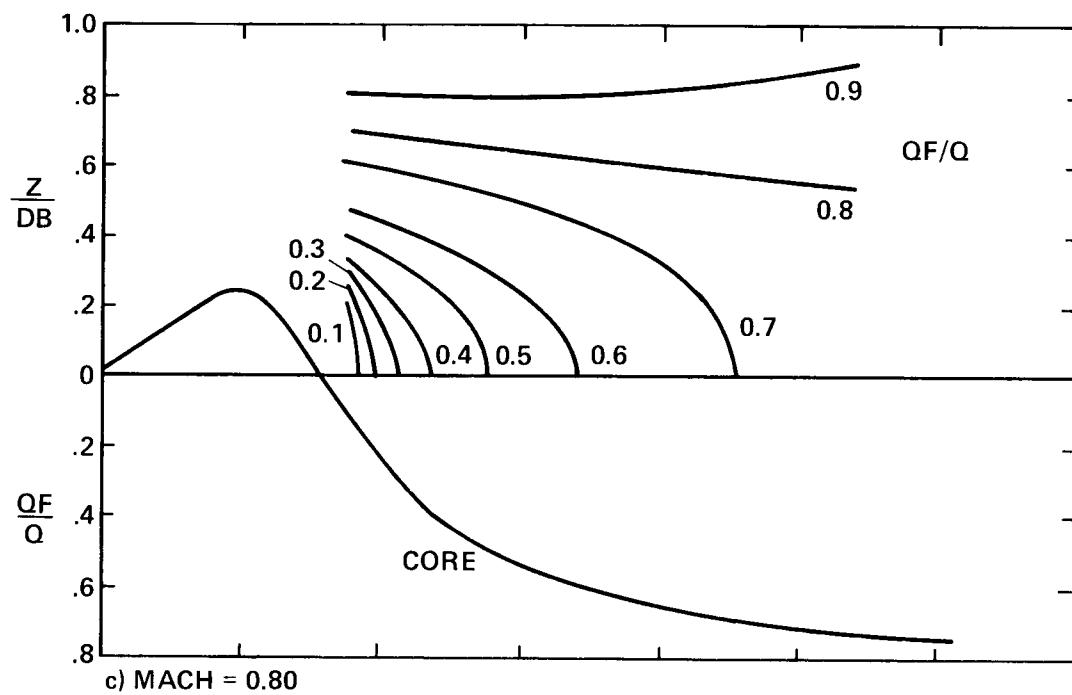


Figure 6.— Concluded.

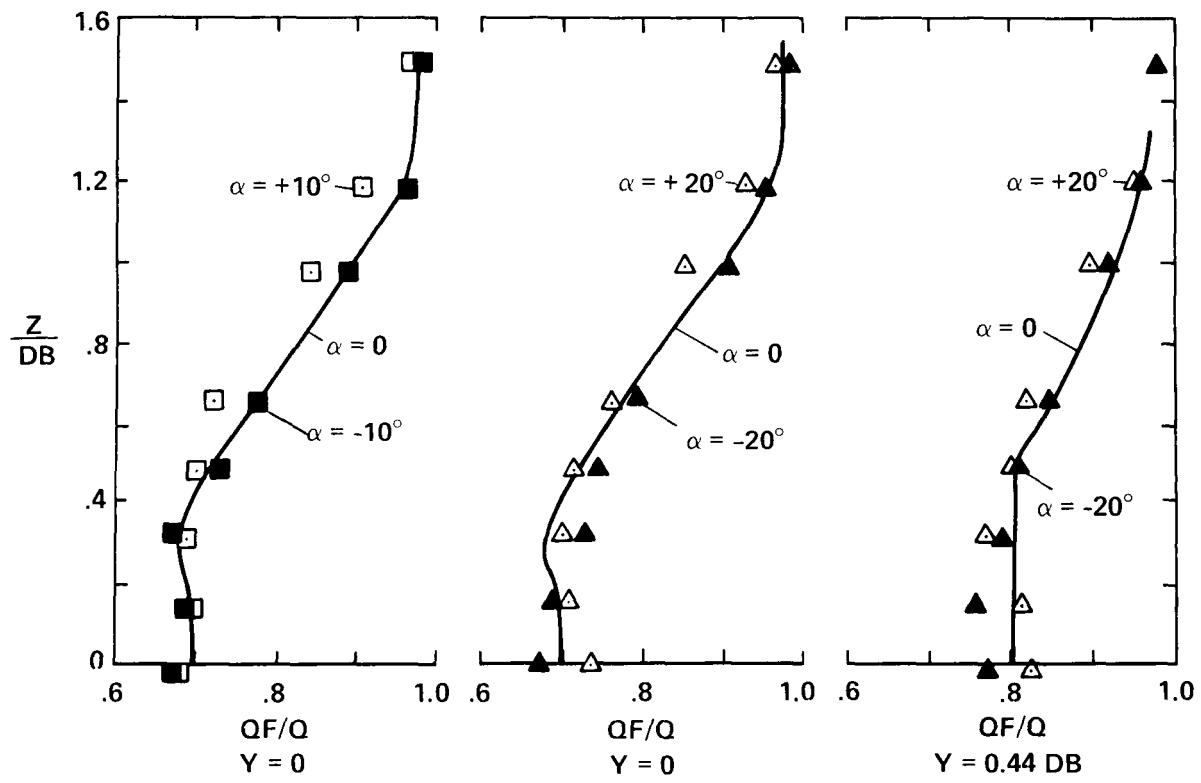
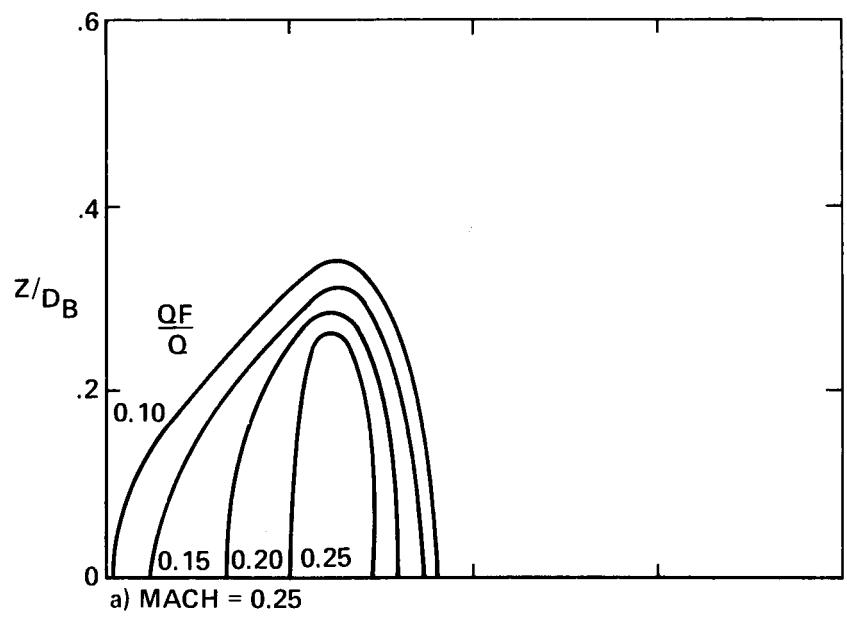
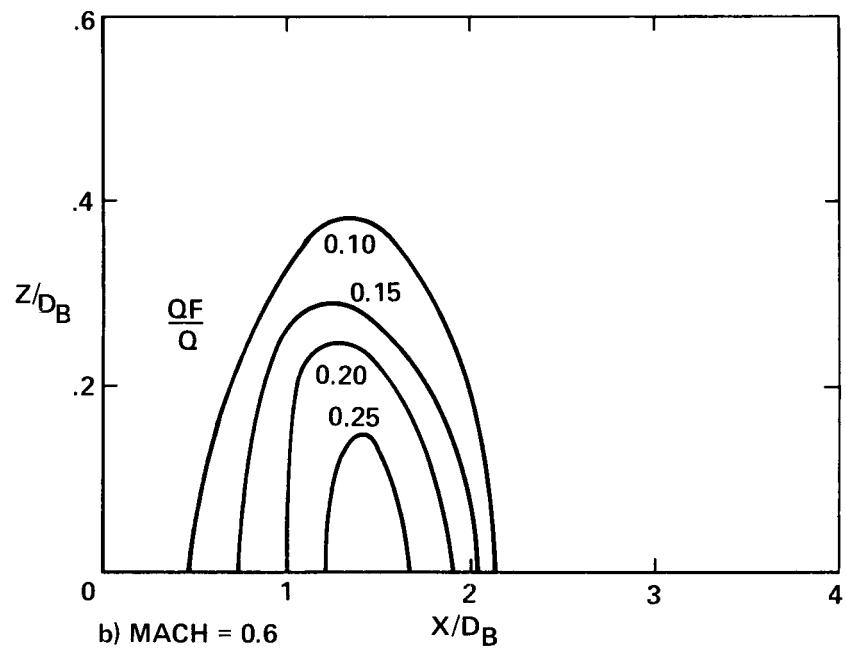


Figure 7.— Effect of angle of attack on dynamic-pressure profiles,  $X/D_B = 8.5$ ,  $M = 0.80$ ,  $R_D = 0.75$  million.



a)  $MACH = 0.25$



b)  $MACH = 0.6$

Figure 8.— Contours of constant reverse dynamic pressure in near wake of ablated model,  $\alpha = 0$ ,  $R_D = 0.75$  million,  $Y/D_B = 0$ .

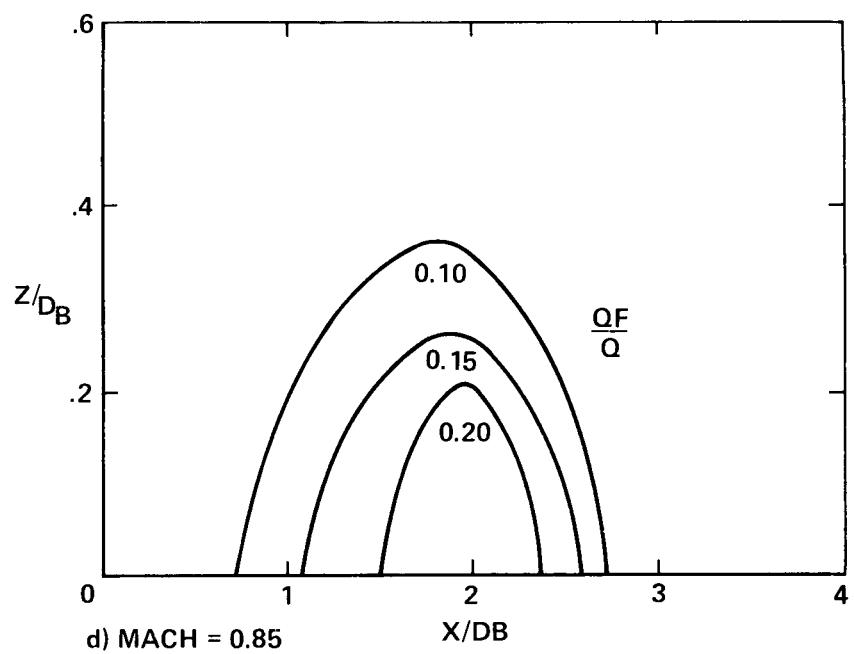
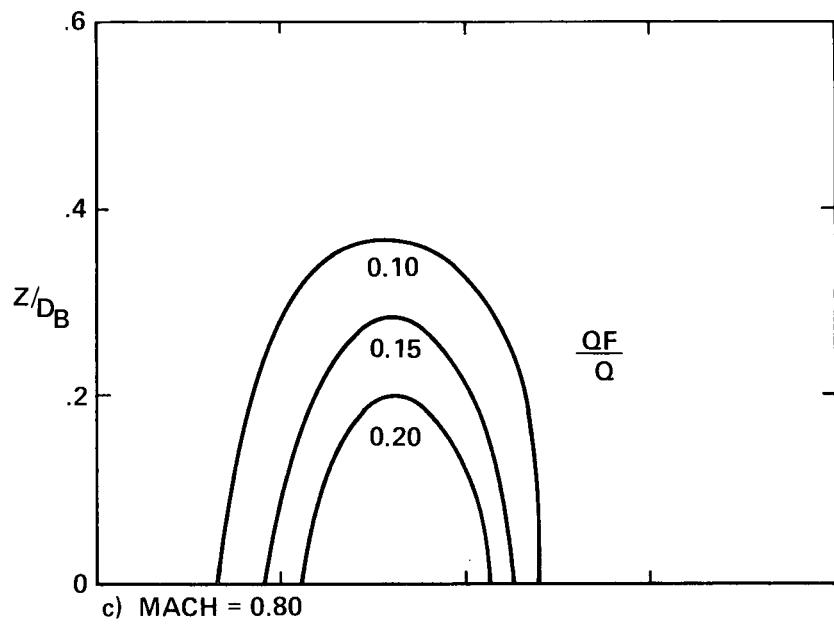


Figure 8.— Continued.

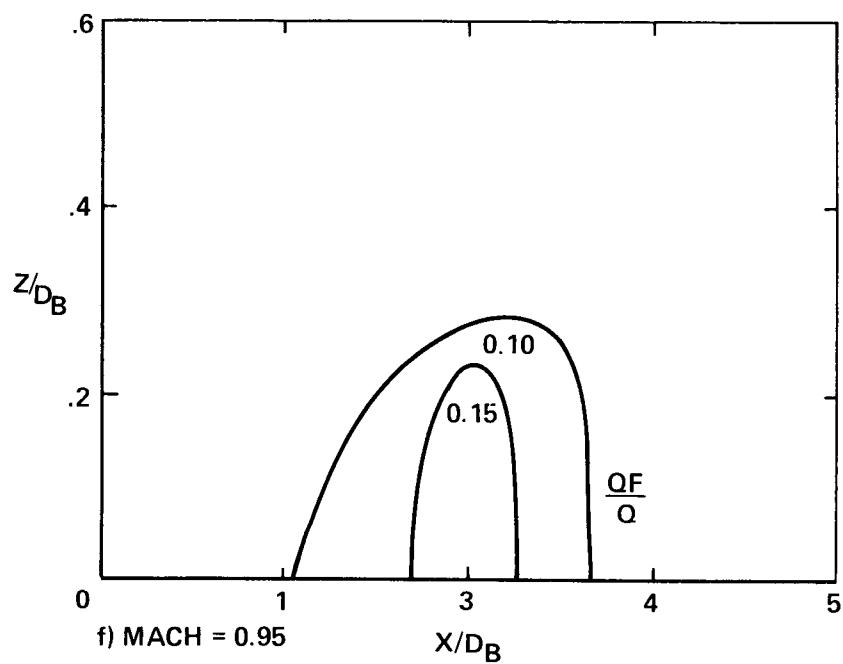
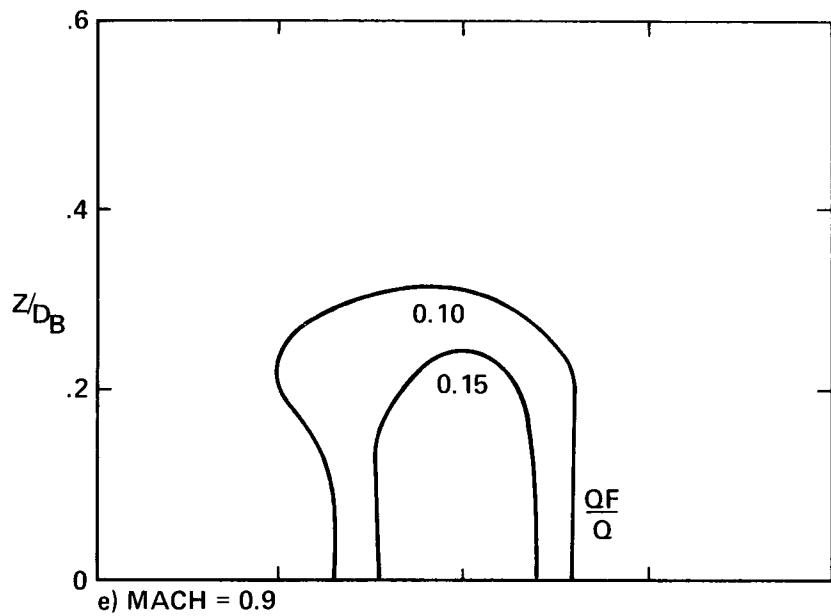


Figure 8.— Concluded.



## Report Documentation Page

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