N88-18951

NASDA's New Test Facilities for Satellites and Rockets

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Recently, the space development activities for the practical purposes are progressing in the world. For the development of large satellite, rocket, space station and spaceplane, new technology at the field of space simulation has been required. Based on the results of our basic study and investigation on the technology, National Space Development Agency of Japan (NASDA) has decided to construct the integrated environmental and structural test facilities for the future large satellites. Presently, these facilities are under construction. This paper presents the outline of NASDA's new test facilities and some technical considerations, especially for the unique vibration test facility.

1. Introduction

Recently, we are developing H-2 rocket, 2 ton class large geostationary earth orbit (GEO) satellite
Engineering Test Satellite ∇ , (ETS- ∇) Free-Flyer and Japanese Experimental Module (JEM) of the space station under the co-operation with NASA and ESA, for the 1990's space applications. These future spacecraft become larger in dimensions and heavier in weight. With the development of advanced spacecraft, more severe test specifications are required for the environmental and space simulation test facilities.

The environmental and space simulation tests for our satellites and rocket components are performed at Tsukuba- Space- Center (TKSC) of NASDA. Our current facilities were constructed for the satellites which are launched by N and H-1 rockets. And the requirements for the future large spacecraft are beyond the capacities of these facilities .

From this situation, we have studied environmental technologies for the future large satellites for several years. In 1983, we started to make the preliminary investigation on the future test facilities.

In 1985, we got test engineer's opinion from the space industries in our country.

Based on the groval evaluation of the results of our studies, we made a construction plan of new environmental test facilities, in 1986.

Presently,our new facilities are under construction at TKSC . And it will be initially used for the development tests of ETS- ∇ I in 1989.

In this paper, our philosophy for new test facilities, the outline of each facility and in paticular, some of the technical uniqueness of vibration test facility are discussed.

2. Philosophy of New test Facilities

Fig. 1 shows total system of our new test facilities. Our philosophy is to perform all tests of a spacecraft in one building, which we call "integrated test building".

ESA/ESTEC and IABG have a plan to improve test capabilities by adding some equipments and facilities for next generation satellites.

And CNES/INTESPACE, The Institute of Space and Astronautical Science of Japan (ISAS) have also attractive concentrated test facilities.

However, our new test systems and facilities will be one of the most advanced ones in the world. Next generation environment facilities will have this tendency.

Here, we discribe the requirements for our facilities.

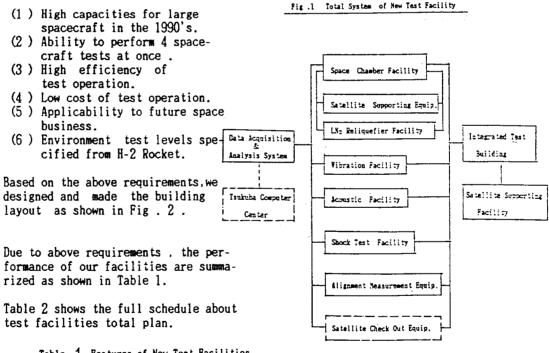


Table .1 Features of New Test Facilities

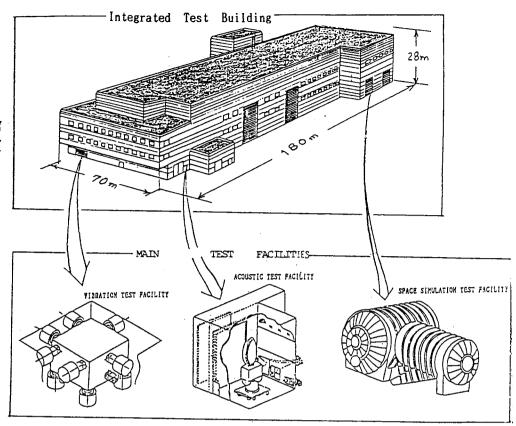
1. Target ----2 Ton class satellites (at GEO)

2. High Efficiency

3. Can Test Many Satellites at a Time

4. Low Cost

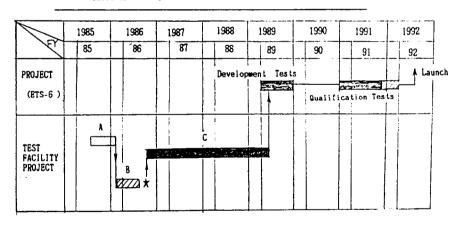
5. Open to Many World's Users



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Fig .2 New Test Facilitis and Integrated Test Building

Table .2 Project Plan of Integrated Test Facility



Total Span ---- 4 Years (7 Years including basic studies)

PHASE

- A : Preriminary Studies and Test System Plan $\,$
- $B : 1 \ \text{MASDA's detail} \quad investigation including industries opinion$
 - 2 Project Planning
 - 3 Decision of contractors
- C : Construction of facilities .

3. Vibration Test Facility

Fig. shows the bird's-eye view of the vibration test facility, which is a three dimensional vibration system. We can perform the vibration tests of three directions separately without removing the test specimen from the table.

Therefore, we can complite the test for a spacecraft shorter period than that of conventional test facility, which results in high operational efficiency.

The new vibration system consists of 4 vertical and 3 horizontal shakers for each axis, totally 10 shakers.

From the results of our trade-off studies, we decided to adopt electrodynamic shaker rather than hydrodynamic one, from the operational and control point of view.

The test table has 3mX3m size, which is made of aluminum alloy and supported through 12 hydrostatic joints. We designed the joint to move in 5 degrees of freedom. Using the table support system composed of these joints the control system becomes less complicated.

The specification of the vibration facility is shown in Table 3.

Here, we explain some technical features of the system.

(1) Principle of the Supporting System

Fig .4 shows a free body diagram of the rigid supporting table movement. To move the rigid table in one direction, two surfaces of the table in parallel with the direction of the motion have to be supported at two points in one surface and at three points in another surface. Our supporting system adopts this principle.

However, for the horizontal slidings in X and Y direction, one more points is added to the above three points for resisting the rolling moment forces due to the test specimen.

Fig .5 shows the location of the spherical pad bearings which are used at each point due to the above principle .

(2) Mechanism of Spherical Pad Bearing

The hydrostatic joint designed for our system, which we call "spherical pad bearing", restricts only one degree of freedom of the motion.

Fig.6 shows a cross section of the spherical pad bearing. As shown in Fig.7, the spherical pad bearing has five degree of freedom of the motion. In this joint, one degree of freedom of the motion, which is the motion along the connecting line between the joint base and the supporting table, is restricted.

One of the technical key points in our system is to develop the hydrostatic joint, especially to increase the rigidity of the joint. Presently, the rigidity in the axial direction of the joint is designed to be approximately 8×10^7 kg/mm.

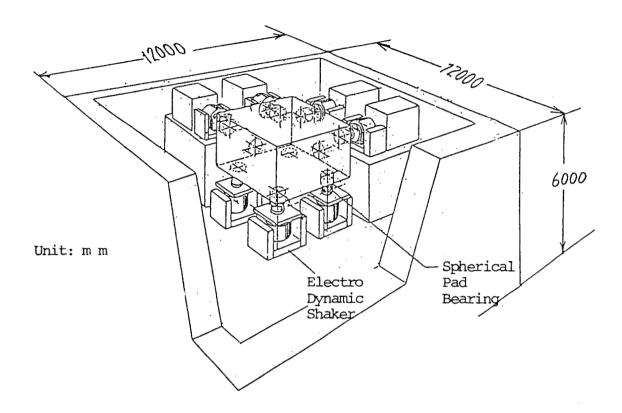


Fig. 3 Vibration Facility (Shaker and Table Assembly)

Table. 3 Vibration Test Facility Specification

TOTAL PERFONANCE	3 DIRECTIONAL SHAKER SYSTEM				
	HEIGHT CAPABILITY	:	4.5 tons (9,900 lbs.)		
	FREQUECY RANGE	:	SINE 5 - 100 llz RANDON 5 - 200 llz (Low Lorel) TRANSIENT		
	OVERTURNING MOMENT CAPABILITY	:	6 0 tos-s		
			(434,000 ft-lbs)		
SIIAKER	LDS ELECTRODYNAMIC SHAKER VERTICAL: 9.5 tonF X 4 shakers HORIZONTAL: 9.5 tonF X 3 shakers X 2 directions (21,000 (bs.)				
TEST TABLE	DIMENSION				
	3m×3m; (9.8 × 9.8 ft.)				
	Aluminum: alloy				
CONTROL	- Genrad, digtal for amplitude control				
	LDS, analog for current-phase control				

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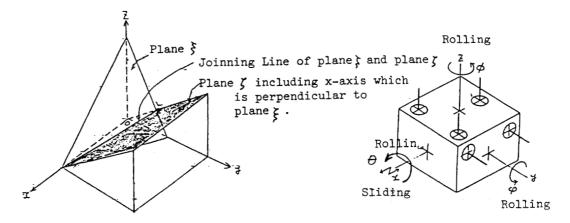


Fig. 4 Principle of Supporting in the Free Space

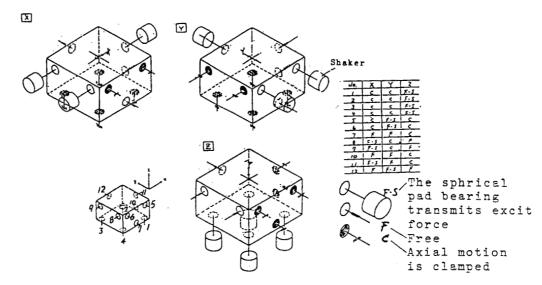


Fig. 5 Distribution of the Spherical Pad Bearings and their Function for Each Excitation Axis

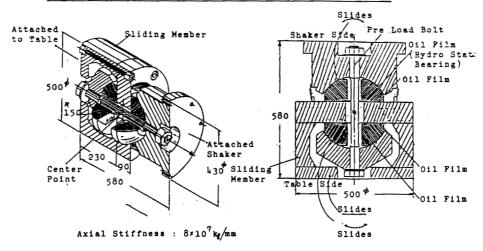


Fig .6 Spherical Pad Bearing

Fig. Cross Section of Spherical Pad Bearing

4. Space Simulation Test Facility

Fig.8 shows the space simulation test facility, which enables us to perform solar simulation test. IR simulation test, and vacuum thermal cycle test.

The vacuum chamber is a horizontal hammer type one with a full-open-door. This type of door enables us to use the chamber volume efficiently, because it is allowed to set a large specimen up to the chamber diameter. The efficient chamber volume, 13^{ϕ} m $\chi 16^{\circ}$ m, was determined from the requirements of spacecraft and precision of solar simulator design. The efficient beam diameter of the solar simulator is 6 m.

One of the most advanced technologies adopted in this facility is the collimation mirror composed of glass coated CFRP segments . This mirror is light weight . Therefore , it requires a simple mechanism for the temperature control as shown in Fig .9.

And to operate the chamber system at low cost , we reuse the vaparized N2 through the $LN_2\text{-Reliquefier facility}$.

The specification of the space simulation test facility is shown in table 4.

5. Acoustic Test Facility

Fig .10 shows the acoustic test facility. In this facility, we adopted a compressed air type system which is the same type as the current facility and is superior to the GN_2 blow - down type system in operational test efficiency.

The maximum overall sound pressure level (SPL) is 151dB, and one-third octave band spectrum shaping is performed with the degital controller, which consists of a redundant system.

The volume of the new reverberation chamber is approximately $1600~\text{m}^3~(10.5\text{m}\times9.0\text{m}\times17.0^{\text{H}}\text{m})$. And also this facility is provided with a supporting cart for large spacecraft.

The specification of the acoustic test facility is shown in Table 5 .

6. Data Acquisition and Analysis System

Fig. 11 shows the data acquisition and analysis system. This system is a kind of data processing center with the LAN, which consists of data analysis and management computers and terminals at each test area.

We can use this system not only to process the data acquired at each test and to establish the data base of spacecraft design and tests. but also to storage ourselves technical potential.

The new facility has high speed data processing, and the data memory of 40 GB .laser disk.

Table 6 shows the characteristics of the data acquisition and analysis system .

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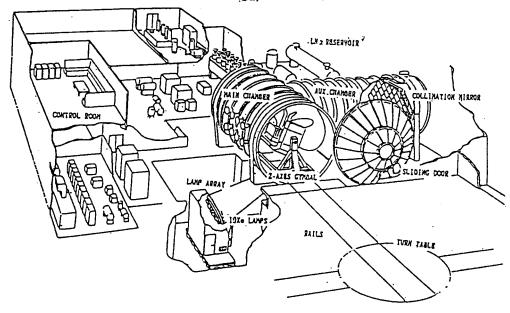
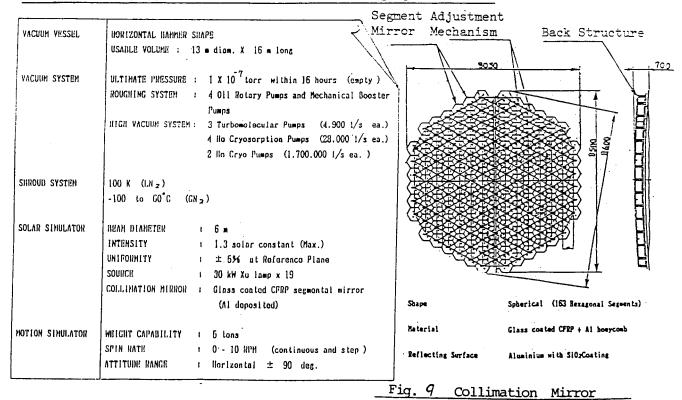


Fig. 8 Space Simulation Test Facility

Table. 4 Space Simulation Test Facility Specification



DRIGINAL PAGE IS DE POOR QUALITY TY-CAHERA ACOUSTIC CHAMBER Reserved to the second ACOUSTIC CHAMBER JET HOZZLE NI CROPHONUS TRANSDUCER LOH PROUENCY SOUND CENERATION SYSTEM STRAIN CAUCES CONTROL CONSOLE ACCELERONETERS > HIGH FREQUENCY HORN MIDIUM FREQUENCY HORK COOLING .UNIT. POWER AMP.

AIR COMPRESSOR

ATE SUPPLY SYSTEM

Fig. 10 Acoustic Test Facility

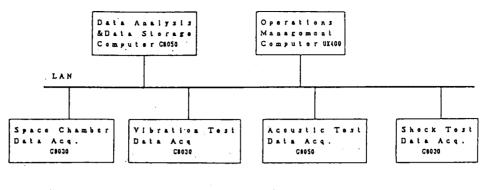
CONTROL COMPUTER

CONTROL SYSTEM

Table	5	Acoustic	Test	Facility	Specification.

		
TOTAL PERFRHANCE COMPRESSED AIR · SYSTEM		
	SOUND PRESSURE LEVEL: 151 db (o.	A.)
	SPECTRUM RANGE : 25 Hz - 10) kilz (1/3 oct, band width)
AIR COMPRESSOR	AIR FLOH RATE : 245 Nm²/mi	n.
	MOTOR : 1,440 kH	
SOUND GENERATOR	TRANSDUCER : EPT-200 (110kH) X 3
	EPT-1094 (10kH) X 4
	JET MOZZLE	(0.2kH) X 1
	HORN : 25 llz X	1
	100 Hz X	1
	200 !lz X	1
CONTROL	1/3 oct.band DIGITAL CONTROL	
ACOUSTIC CHAMBER	DIMENSION : 10.5 M X 9	.0 ° X 17.0 " (m)
·	ACCESS DOOR : 7.0 H X 13	3.0 ¹ (m) approx.
	YOLUME : 1,6 00 m	(56,500 /1;)

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米Feature
Using the LAN System
Compatible with each other
High Spred Data Processing
Large Digital Data Memory (Laser Disk 40GB)

Fig. || Data Acquisition and Handling System

Table. 6 Data handling System Characteristics

1. VIBRATION	3. ACOUSTIC	
Data Acquisition	Data Acquisition	
ChannelACC. 300ch.	ChannelACC. 200 cH.	
Strain 50ch.	Strain 30cH.	
Frequency Range5~100Hz (Sin.) 5~200Hz (Ran)	Microphone-12cH. Frequency Range	
Sampling Rate800 sam/sec	ACC. 5-2kHz	
Data Analysis	Sampling Rate ACC.&STR. Sk√sec	
	Microphone	
FFT , PSD , Trancefer Func. Ana. Wave Form Analysis	40 k/sec	
Notch Level Analysis	Bata Analysis	
Analysis and Print Out Time		
44 min. 350 cH (FFT.PSD,f-g)	1/1. 1/3 Oct Analysis PSD, AL-SPL	
	Transfer Func. Analysis	
2. SPACE CHAMBER	Abalysis and Print Out Time25 min. 200cH	
Data Association	GSD, 1/1 (AL-SPL)	
Data Acquisition		
ChannelTemp. 800 cH .	A DUOCH	
Calorimeter 300cH. Analog Sig. 50 cH .	4. SHOCK	
Digital Sig. RS232Cx2	Data Acquisition	
Scanning Speed10 msec, 100m sec/cH Measurement Interval 2 min.	ChannelACC, 200cH	
	Frequency Range	
Data Processing	20~10kHz Sampling Rate	
Scan Print, Senser vs. Time Print and Prot	50 kHz Sam./sec	
Average Print AT/t Print and Plot Equilibrium Search Print , Limit Check	Para Analysia	
Min. Max. of Sensor Defind	Data Analysis	
Calolimeters Process.	FFT SRS .	
Equilibrium Frequency Bar Graph. Prediction of Equilibrium ,	Wave Form Analysis Analysis and Print Out	
	Time25 min. 200 cH.	
·	(FFT , SRS ,)	

7. Integrated Test Building

Fig . 12 shows the integrated test building . The total-area of this building is about 1800 $\rm m^2$ and the layout is shown in Fig. 13 .

There are two test area . One is the static test area and another is the dynamic test area .

The spacecraft test rooms have the cleanness of class 100000 .

To keep the high cleanness of the building, two types of air lock loading room are adopted for the entrance of satellites and its supporting equipments. Especially, in this building, a large preparation area is provided to satisfy a variety of user's requirements.

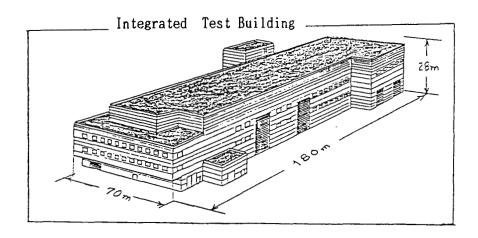


Fig . 12 Integrated Test Building

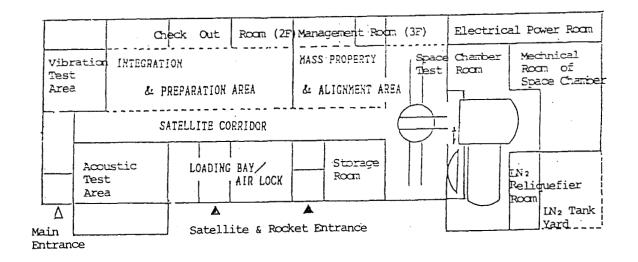


Fig .13 Layout of Integrated Test Building

8. Conclusions

We presented the outline of NASDA's new test facilities , our philosophy of NASDA's future spacecraft development and some technical key points of our vibration test system .

Our new facilities' "easy and low cost operationability" will answer to the requirements of many users in the world and open a door to the tests of their future large spacecraft.

We will be able to present some detail $\mbox{performances}$ of the facilities $\mbox{ at the next chance}$.