# NASA Technical Memorandum 100545 

AVSCOM
Technical Memorandum TM-88-B-008
INFLOW MEASUREMENT MADE WITH A LASER VELOCIMETER ON A
HELICOPTER MODEL IN FORWARD FLIGHT
Volume V TAPERED PLANFORM BLADES AT AN ADVANCE
RATIO OF 0.23
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(NASA-TM-100545) IMFION MEASOEREEMT MADE ..... N88-23755
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National Aeronautics and Space Administration

## SUMMARY

An experimental investigation was conducted in the 14- by 22-Foot Subsonic Tunnel at NASA Langley Research Center to measure the inflow into a scale model helicopter rotor in forward flight ( $\mu_{\infty}=0.23$ ). The measurements were made with a two-component Laser Velocimeter (LV) one chord above the plane formed by the path of the rotor tips (tip path plane). A conditional sampling technique was employed to determine the position of the rotor at the time that each velocity measurement was made so that the azimuthal fluctuations in velocity could be determined. Measurements were made at a total of 168 separate locations in order to clearly define the inflow character. This data is presented herein without analysis. In order to increase the availability of the resulting data, both the mean and azimuthally dependent values are included as part of this report on two 5.25 inch floppy disks in Microsoft Corporation MS-DOS format.

## INTRODUCTION

One of the problems confronting the helicopter industry is the lack of detailed information about the velocity fluctuations around and through rotating blades. This information is needed for two reasons: to ensure a more complete understanding of the flowfield environment associated with a thrusting rotor and to provide data for the validation of rapidly emerging computational codes. One explanation for the lack of available data is the absence, until recent years, of a suitable device for making such measurements. Making measurements of the velocity around a system of rotating blades requires an accurate, nonintrusive measurement capability that presents a minimum risk to the systems involved. The Laser Velocimeter (LV), which uses high energy light beams to measure velocities, is ideally suited to this task.

The Laser Velocimeter has been successfully used to measure specific areas and localized phenomena within the rotor disk (refs. 1 through 3). In addition, the hotwire anemometer and pressure probes, both having directional measuring limitations, have been employed in similar programs (refs. 4 and 5). This is, however, the first time that a comprehensive program has been undertaken to map the flow into the complete rotor disk. This investigation has been conducted to measure the flow into a representative rotor system as a function of azimuth using a two-component (streamwise and vertical direction) $L V$ system.

## NOTATION

$A_{0} \quad$ constant term in Fourier series of blade feathering (collective) at $r / R=0.75$, deg
$A_{1} \quad$ coefficient of cosine term in Fourier series of blade feathering, deg
$B_{1} \quad$ coefficient of sine term in Fourier series of blade feathering, deg
$C_{D} \quad$ rotor drag coefficient, $D / \rho \pi R^{2} v_{\text {tip }}^{2}$
$C_{Q} \quad$ rotor torque coefficient, $Q / \rho \pi R^{3} v_{\text {tip }}^{2}$
$C_{T} \quad$ rotor thrust coefficient, $T / \rho \pi R^{2} V_{\text {tip }}^{2}$

## Greak

rotor drac, positive to the rear, lbf dynamic pressure, $1 \mathrm{bf} / \mathrm{ft}^{2}$
rotor torque, in-lhf
local radius of the rotor system, ft
rotor radius, ft
thrust produced by the rotor, lhf
tunnel freestream velocity, positive downstream ft/sec
free-stream component of velocity, positive downstream, ft/sec
induced component of velocity parallel to the tip path plane (positive flow downstream), ft/sec
vertical component of velocity, positive up, ft/sec
induced component of velocity normal to the tip path plane (positive flow up), ft/sec
rotor blade tip velocity ( $\Omega R$ ), ft/sec
anqle between rotor disk and free-stream velocity (positive nose up), deq inflow ratio normal to tip path plane (positive up), ( $\left.u_{\infty} \sin (\alpha)+v_{i}\right) / V_{t i p}$ induced inflow ratio normal to tip path plane (positive up), $v_{i} / V_{t i p}$ rotor advance ratio, $\mathrm{U}_{\infty} \cos (\alpha) / \mathrm{V}_{\text {tip }}$
inflow ratio parallel to tip path plane (positive downstream). $\left(J_{\infty} \cos (\alpha)+u_{i}\right) / V_{t i p}$
induced inflow ratio parallel to tip path plane (positive downstream) $u_{i} / V_{t i p}$
rotor rotational speed, radians/sec
rotor azimuth measured from downstream position, positive counterclockwise, as viewed from above, deq
air density, slugs/ft ${ }^{3}$
blade pitch anqle at a specific azimuth (positive nose up), deq, $\theta=A_{0}-A_{1} \cos \psi-B_{1} \sin \psi$
mein value

The experimental apparatus used in this investigation included the NASA Lanqley Research Center 14- hy 22-Foot Subsonic Tunnel, the 2-Meter Rotor Test System (2MRTS), and a two-component laser velocimeter system.

The 14- by 22-Foot Suhsonic Tunnel is an atmospheric, closed-circuit wind tunnel of conventional desiqn with enhancements for the testing of powered and high-lift confiqurations (ref. 6). The tunnel is shown in fiqure 1. When the tunnel is operated in the open confiquration, the walls and ceiling of the test section are lifted out of the flow, leaving only a solid floor and a flow collector. In this confiquration, the tunnel can be driven to ahout 170 knots. This investigation was conducted with the tunnel in the open confiquration to allow complete optical access to the rotor flowfield.

The 2 MRTS is a qeneral purpose rotorcraft model testing system which was mounted on a strut in the forward part of the test section (see fig. 2). The system consists of a 29 -horsepower electric drive motor and $90^{\circ}$ speed-reducing transmission, a blade pitch remote control system, and two six-component strain qage halances used for measuring forces and moments on the rotor system and fuselage shell. The four-blader rotor hub is fully articulated with viscous dampers for lead-lag motion and coincident flap and laq hinges. A more detailed description of the 2MRTS can be found in reference 7. The fuselaqe which was used for this test was a generic hiqh-speed helicopter confiquration. The characteristics of the tapered rotor blades used during this investiqation can be found in table 1. The rotor hlade planform is shown in fiqure 3. No attempt was made to dynamically scale the rotor blades; rather, they were very riqid to provide a qeneral research capability.

The LV system used in this investigation was desiqned to measure the instantaneous components of velocity in the longitudinal (free stream) and vertical directions. The LV system is described in reference 8. The system is comprised of four subsystems: optics, traverse, data acquisition, and seeding. The optics subsystem, which is shown in fiqure 4, operates in backscatter mode and at hiqh power (4 watts in all lines) in order to accommodate the long focal lengths needed to scan the wide test section. The transmitting and receiving optics packaqes are auqmented by a zoom lens system consisting of a 3-in. clear aperture negative lens and a 12-in. clear aperture positive lens. Braqq cells in each of the optical paths provide a directional measurement capahility. The velocity measurements are made at a point in space where the four beams cross, called the sample volume. The length of the sample volume (transverse to the flow direction) increases as the sample volume is moved away from the optics assembly. The sample volume length, over the $10-$ to 20 -foot focal lenqth of the system, is less than 1 cm and has a constant diameter of 0.2 mm .

The traverse sinsystem provides five deqrees of freedom in mositioning the sample volume and is controlled by the same computer that is used for data acquisition. Translation of the sample volume in the horizontal and vertical direction is accomplished by displacing the entire optics platform. Translation alonq the lateral axes is accomplished by displacing the negative lens located in the zoom lens assembly, thus refocusing the sample volume along the axes of optical transmission. The other two degrees of freedom, pan and tilt, are implemented by rotating the final mirror about its vertical and horizontal axes in order to change the direction of optical transmission. The total range of the traversing system is 7 ft vertically, 6 ft streamwise, 16.5 ft laterally, and $10^{\circ}$ in both pan and tilt. Measurements can be made outside of this envelope by repositioning the optics platform, which is mounted on wheels to facilitate such relocations. For this study the traversing system was
positioned to the left of the test section when looking downstream as shown in fiqure 5.

The data acquisition subsystem is shown schematically in figure 6 and interfaces with the optical siqnal processing equipment to receive two channels of raw LV data and up to five channels of auxiliary data. In this investigation, four of the auxiliary channels were used for the acquisition of data relative to blade position. Two of the channels (one each for the $U$ and $V$ components) measured the azimuthal position of the rotor shaft and the other two measured the lead/lag and flapping motion. The system converts the raw LV data to engineering units and determines the statistical characteristics of the acquired data so that the test results can be evaluated during the acquisition process. The raw data, the data which have been converted to engineering units, and 64 parameters from the tunnel static data acquisition system are written to maqnetic tape for later analysis. The final function performed by the data system is to control the five dearee-of-freedom scan system.

The seeding subsystem, shown schematically in figure 7, is a solid particle, liquid dispensinq system (ref. 9). Polystyrene latex microspheres are suspended in a mixture containing, by volume, 50 percent water and 50 percent ethyl alcohol. The advantages of the polystyrene particles are their low density, high reflectivity, and precise particle sife. The particles used in this investigation were 1.7 microns in diameter with a standard deviation of 0.0239 microns. The particle mixture is pumped to an array of 32 nozzles where compressed air is used to atomize the mixture. These nozzles are mounted on a frame 8 feet wide by 6 feet high which is suspended on cahles in the settling chamber of the tunnel. The low vapor pressure of water/alcohol mixture allows it to evaporate as it travels the 85 feet from the setting chamber to the test section. This process provides isolated single particles in the flowfield whose velocities are measured as they pass through the sample volume. The local fluid velocity is inferred from the seed particle velocity.

## ERROR ANALYSIS

The overall LV system error is ohtained by summing the error of all of the components that contribute to an error in the velocity measurement. The error sources are summarized in the tahle below, and are defined in references 10 and 11 . The resulting total hias error of -0.81 to 1.82 percent is obtained by adding the percents contributed by each error source. The total random error of 1.12 percent is obtained by taking the square root of the sum of the squared percents of the random sources. Traking the square ront of the sum of the squares of the random and hias errors qives A total system error of 1.38 percent to 2.14 percent.

| Frror source | Bias error | Random error |
| :---: | :---: | :---: |
| Cross beam angle measurement | $\pm 0.81$ | N/A |
| Diverqing fringes | A | A |
| Time jitter | N/A | N/A |
| Clock synchronization | 0.51 | $\pm 0.51$ |
| Ouantization | A | $\pm 1.00$ |
| Velocity bias | B | B |
| Braqg bias | B | B |
| Velocity gradient | B | R |
| Particle laq | $\pm 0.50$ | R |
| Total error | -0.81 to 1.82 | 1.12 |
| $\begin{array}{ll}\text { A } & \text { Not measured } \\ \text { B } & \text { Negliqible } \\ \text { N/A } & \text { Not applicable }\end{array}$ |  |  |

## TEST PROCEDURES

In all cases, measurements were made at azimuthal increments of $30^{\circ}$ from $\psi=0$, at 3.0 in. (approximately one chord) above the plane formed by the tips of the blades. Measurements were made from a radial location of $r / R=0.2$ to $r / R=1.12$, with the majority of the measurement locations concentrated toward the outhoard portion of the disk. Fiqure 8 shows the measurement locations superimposed on the rotor disk. During the test, the rotor tip path plane was maintained at $-3^{\circ}$ relative to the free stream by zeroing the blade flapping relative to the shaft and setting the shaft angle to $-3^{\circ}$. The operating tip speed for the test was held at 624 ft/sec ( 2200 rpm ), the nominal tunnel speed was $144 \mathrm{ft} / \mathrm{sec}\left(\mu_{\infty}=0.23\right)$, and the nominal rotor thrust coefficient was 0.0065 . Table 2 lists the nominal test conditions and selected test parameters. The LV data acquisition process consisted of placing the sample volume at the measurement location and acquiring data for a period of 1 minute or until 4096 velocity measurements were made in either the lonaitudinal or the vertical component. During this process, conditional sampling techniques were employed to permanently assoriate each measured velocity with the location of the rotor blades at the time when the measurement was made. At the conclusion of the nrocess, the measurement location was changer and the acquisition process was repeater.

## DATA REDIICTION

Independent velocity measurements in the free stream and vertical direction were made at each measurement location. At the same instant in time that a velocity measurement was made, the location of the blades was recorded for that velocity component. The maximum time required to acquire these data was 1 minute ( 2200 rotor
revolutions for this test) and the minimum approximately 20 sec . These data, collected over many revolutions, were sorted into 128 equally spaced azimuth seqments ( $2.81^{\circ}$ wide) that are representative of blade position and include corrections for blade lead/laq motion. The velocity value assigned to each interval at a measurement location is the arithmetic mean of all the measurements that were taken in the respective $2.81^{\circ}$ wide azimuthal range. The results of this sorting process provide the: nimuthally dependent velocity data. The "mean velocity" value refers to the velocity calculated from the arithmetic mean of all the measurements made at a single measurement location.

## FXPFRIMENTAL RFSSULTS

Table 3 lists the measurement locations, the mean and standard deviation of the two components of induced inflow velocity, and the number of measurements in each of the measured components (II and $V$ ). In fiqure 9 the mean lonqitudinal induced commonent of velocity, $\mu_{i}$, with a hand of $\pm$ one standard deviation is plotted vs. blade radius for each radial scan. The standard deviation represents the fluctuation in velocity at a qiven measurement location; it is not an indication of the error in the mean measurements. The size of the symbols used for plotting the mean velocity values is an approximation of the calculated error in the measurements. Fiqure 10 presents in the same format the mean normal induced component of velocity, $\lambda_{i}$. The same data without the $\pm$ one standard deviation is presented in a contour plot format in fiqures 11 and 12 in order to show more clearly the interactions over the whole aisk (viewed from above). The format of each of the figures ( 13 through 180) is the induced velocity vs. azimuth at the top of the figure, the number of measurements that went into determining the velocity value for each azimuth seqment in the center, and an order ratio analysis of the azimuthal variation at the hottom of the figure. The fiqure numbers for the azimuthal and radial measurement locations are indicated helow.


The mean and standard deviation of the induced inflow velocities (table 3) and the azimuthally dependent induced inflow velocities (figs. 13 through 180 ) are included on 5.25 flexible disk in the pocket on the inside of the rear cover of this report. The details of the data format and the file structure are located in the file "README.DOC". The disk format is 360 kbyte double-sided, written using the Microsoft Corporation MS-DOS operating system.

## CONCLODING REMARKS

The Laser Velocimeter provides an effective system for making measurements in the dynamic environment associated with rotor blades. It has heen used on numerous occasions to measure the localized flow phenomena encountered in such flows. This investigation demonstrates the use of a matured LV system to map the flow into a representative rotor in forward flight by making velocity measurements at 168 locations above the rotor disk. These measurements provide both the mean and azimuthally dependent velocity values, and they provide a detailed look at the nature of this flow.

ORIGINAL PAGE IS
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## TARLE 1.- 2MRTS ROTOR AND BLADE CHARACTERISTICS

Hub type .................................. Fully articulated
Number of blaies . . . . . . . . . . . . . . . . . . . . . . . . . .......... . 4
Airfoil section ................................... NACA 0012
Hinge offset, in., r/R ........................ 2.00,0.06
Root cutort, in., $r / R$........................... $9.25,0.24$
Pitch-flan coupling anqle, deq ................................
Twist linear, deq ......................................... -13.0
Radius, R, in. ............................................ 32.50
Rotor solidity, bc/iR ............................ 0.0977
Blade stiffness
Flapwise, $1 b-i n^{2} . . . . . . . . . . . . . . . . . . . . . . . . . . . .$.
Torsional, lb-in? ................................... 12750
Blade weight, qrams .................................. 222.0
Lead/lag damping, in-lb/deq/sec .................... 182.4

## TABLE 2.- NOMINAL ROTOR CONTROL AND PERFORMANCE PARAMETERS



TARLF 3.- INFLOW VFLOCITY SUMMARY

| $\psi$ | $r / R$ | Mean | Standard deviation | measurements | Mean | Standard deviation | $\begin{gathered} \# \\ \text { measurements } \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0 | .20 | . 0143 | . 0175 | 157 | -. 0138 | . 0129 | 547 |
| 0 | . 40 | .0107 | . 0172 | 168 | -. 0252 | . 0102 | 623 |
| 0 | . 50 | . 0108 | . 0163 | 171 | -. 0273 | . 0104 | 536 |
| 0 | . 60 | . 0074 | . 0190 | 121 | -. 0310 | .0107 | 499 |
| 0 | . 70 | . 0067 | . 0165 | 114 | -. 0321 | . 0117 | 388 |
| 0 | . 98 | -- | -- | 0 | -. 0491 | .0246 | 379 |
| 0 | 1.02 | -- | -- | 0 | -. 0519 | . 9188 | 416 |
| 0 | 1.04 | -- | -- | 0 | -. 0531 | . 0236 | 570 |
| 0 | 1.10 | .0067 | . 0242 | 789 | -. 0548 | . 0189 | 843 |
| 0 | . 20 | . 0249 | . 0213 | 1352 | -. 0083 | .0127 | 3901 |
| 0 | . 40 | . 0210 | . 0232 | 1202 | -. 0282 | . 0076 | 2596 |
| 30 | . 50 | .0190 | . 0212 | 543 | -. 0316 | . 0086 | 1085 |
| 30 | . 60 | . 0151 | . 0182 | 422 | -. 0355 | . 0092 | 660 |
| 30 | . 70 | . 0089 | . 0168 | 284 | -. 0383 | . 0088 | 388 |
| 30 | . 74 | . 0091 | . 0197 | 178 | -. 0403 | . 0084 | 294 |
| 30 | . 78 | . 0056 | . 0203 | 1064 | -. 0444 | .0086 | 1670 |
| 30 | . 82 | . 0057 | . 0210 | 755 | -. 0438 | . 0081 | 1095 |
| 30 | . 86 | . 0035 | . 0220 | 600 | -. 0425 | . 0073 | 383 |
| 30 | . 90 | . 0035 | . 0220 | 544 | -. 0420 | . 0066 | 748 |
| 30 | .94 | . 0028 | . 0220 | 381 | -. 0409 | . 0054 | 535 |
| 30 | .98 | 0.0000 | . 0211 | 288 | -. 0403 | . 0044 | 427 |
| 30 | 1.02 | -. 00025 | . 0231 | 324 | -. 0377 | . 0036 | 464 |
| 30 | 1.04 | -. 00023 | . 0243 | 306 | -. 0370 | . 0035 | 463 |
| 30 | 1.10 | -. 0013 | . 0216 | 316 | -. 0345 | . 0036 | 553 |
| 60 | .20 | -. 0245 | . 02.22 | 204 | -. 0059 | . 0064 | 457 |
| 60 | . 50 | .0148 | . 0232 | 330 | -. 0292 | . 0084 | 559 |
| 50 | .50 | . 0119 | . 0223 | 253 | -. 0294 | . 0093 | 362 |
| 60 | . 70 | .0095 | . 0165 | 140 | -. 0269 | .0084 | 224 |
| 60 | . 74 | . 0085 | . 0158 | 174 | -. 0255 | . 0084 | 276 |
| 60 | . 78 | .0081 | . 0278 | 282 | -. 0246 | . 0079 | 367 |
| 60 | . 82 | . 0071 | . 0234 | 156 | -. 0254 | . 0077 | 325 |
| 60 | . 86 | .0054 | . 0218 | 280 | -. 0223 | .0065 | 483 |
| 60 | . 90 | . 0038 | . 0201 | 348 | -. 0179 | .0058 | 686 |
| 60 | .94 | .0n6? | . 0208 | 407 | -. 0133 | .0047 | 690 |
| 50 | . 98 | . 0050 | . 0261 | 483 | -. 0070 | . 0045 | 598 |
| 60 | 1.02 | .0048 | . 0288 | 1232 | -. 0037 | .0057 | 2337 |
| 90 | 1.04 | . 0054 | . 0301 | 1252 | -. 0035 | . 0055 | 1951 |
| 90 | 1.10 | .0067 | .0302 | 1977 | -. 0256 | . 0051 | 1696 |
| 90 | . 20 | .0154 | . 0162 | 756 | -. 0051 | . 0058 | 1506 |
| 90 | . 40 | . 0142 | . 0162 | 1186 | -. 0250 | .0073 | 3312 |
| 90 | . 50 | .0159 | . 0207 | 933 | -. 0236 | . 0086 | 2104 |
| 90 | . 70 | .0138 | . 0208 | 1259 | -. 0134 | . 0095 | 1361 |
| 90 | . 74 | . 0121 | . 0228 | 1090 | -. 0096 | . 0098 | 1231 |
| 90 | . 78 | .0102 | . 0211 | 947 | -. 0038 | . 0090 | 941 |
| 90 | . 82 | . 0075 | . 0190 | 788 | . 0009 | . 0090 | 660 |


| $\psi$ | $r / R$ | Mran | standard <br> Aeviation | measurements | Mean | Standard deviation | measurements |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 90 | . 86 | . 0055 | . 0194 | 489 | . 0074 | . 0080 | 436 |
| 90 | . 90 | . 0035 | .0184 | 303 | . 0134 | .0n48 | 292 |
| 90 | . 94 | -. 001 ? | . 0182 | 161 | . 0167 | . 0050 | 126 |
| 90 | . 98 | -. 0007 | .0216 | 173 | .0192 | . 0034 | 120 |
| 120 | . 20 | .004? | . 0197 | 35 ? | . 0008 | . 0065 | 1261 |
| 120 | . 40 | . 0047 | .0190 | 550 | -. 0144 | . 0077 | 3054 |
| 120 | . 50 | . 0070 | . 0179 | 442 | -. 0131 | . 0083 | 2619 |
| 120 | . 50 | . 0037 | . 0190 | 597 | . 0079 | . 0098 | 3504 |
| 120 | . 70 | . 0014 | . 0185 | 543 | -. 00008 | . 0113 | 2852 |
| 120 | . 74 | . 0008 | . 0189 | 585 | . 0035 | .0105 | 2362 |
| 120 | . 78 | . 00072 | . 0176 | 458 | . 0074 | . 0090 | 1666 |
| 120 | . 82 | -. 0017 | . 0179 | 287 | . 0098 | . 0074 | 1138 |
| 120 | . 86 | -. 0024 | . 0178 | $17 ?$ | .0105 | . 0069 | 859 |
| 120 | .90 | -.0039 | .0155 | 104 | . 0198 | . 0053 | 673 |
| 120 | .94 | -- | -- | 0 | . 0119 | .0051 | 580 |
| 120 | . 98 | -- | -- | 0 | . 0108 | .0039 | 379 |
| 120 | 1.02 | -- | -- | 0 | .0090 | .0053 | 917 |
| 120 | 1.04 | -- | -- | 0 | . 0089 | . 0049 | 825 |
| 120 | 1.12 | -- | -- | 0 | . 0070 | . 0044 | 460 |
| 150 | . 20 | -. 0053 | . 0148 | 1156 | . 0019 | . 0074 | 925 |
| 150 | . 40 | . 0061 | . 0144 | 1202 | -. 0093 | . 0099 | 1260 |
| 150 | . 50 | . 0075 | . 0143 | 1186 | -. 0057 | . 0116 | 1199 |
| 150 | . 60 | . 0074 | . 0143 | 948 | -. 0017 | . 0131 | 977 |
| 150 | . 70 | . 0043 | . 0136 | 1185 | . 0051 | . 0114 | 1049 |
| 150 | . 74 | .0030 | . 0146 | 1321 | . 0094 | .0091 | 892 |
| 150 | . 78 | . 0020 | . 0141 | 1308 | . 0105 | . 0088 | 961 |
| 150 | . 82 | -. 0011 | . 0151 | 1497 | . 0116 | . 0074 | 1021 |
| 150 | . 86 | -. 0011 | . 0163 | 495 | . 0131 | . Onf\% | 2347 |
| 150 | . 90 | -. 0028 | . 0156 | 424 | . 0128 | .0056 | 2337 |
| 150 | . 94 | -. 00044 | .0211 | 325 | .0121 | . 0146 | 2343 |
| 150 | . 98 | -.006? | . 0197 | 277 | . 0110 | . 0044 | 2058 |
| 150 | 1.02 | -.0ก80 | . 0194 | 268 | .0098 | . 0041 | 1978 |
| 150 | 1.04 | -.008? | .0175 | 105 | . 0090 | .0039 | 486 |
| 150 | 1.12 | -.0086 | . 0181 | 152 | .0068 | . 01043 | 527 |
| 180 | . 20 | -. 0018 | . 0192 | 480 | -. 00001 | . 0049 | 2089 |
| 180 | . 40 | . 0018 | . 0192 | 418 | -. 0076 | . 0097 | 2244 |
| 180 | . 50 | . 0035 | . 0198 | 403 | -. 0057 | . 0115 | 1896 |
| 180 | . 50 | . 0065 | . 0210 | 353 | .0009 | .0103 | 1670 |
| 180 | . 70 | . 0047 | . 0210 | 321 | . 0049 | . 0131 | 1532 |
| 180 | . 74 | . 0016 | . 0200 | 308 | . 0076 | . 0130 | 1439 |
| 180 | . 78 | -. $001 ?$ | . 0194 | 304 | . 0096 | . 0122 | 1308 |
| 180 | . 82 | -. 00001 | . 0192 | 260 | . 0109 | .0100 | 1311 |
| 180 | . 86 | -. 00020 | . 0174 | 312 | . 0118 | . 0090 | 1177 |
| 180 | . 90 | -.0048 | . 0203 | 283 | . 0129 | . 0058 | 1125 |
| 180 | . 94 | -.005? | . 0181 | 246 | . 0122 | . 0057 | 1191 |


| $\psi$ | $r / R$ | Mran | standard deviation | measurements | Mean | Standard devjation | measurements |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 180 | . 98 | -. 0040 | .0181 | 259 | .0119 | . 0045 | 1184 |
| 180 | 1.02 | -. 0052 | . 0177 | 246 | .0110 | . 0045 | 1194 |
| 180 | 1.04 | -. 00045 | . 0192 | 246 | . 0102 | . 0046 | 1076 |
| 180 | 1.1? | -. 0065 | . 0172 | 223 | . 0075 | . 0049 | 1051 |
| 210 | . 20 | -. 0011 | . 0145 | 1290 | . 0008 | . 0067 | 2803 |
| 210 | . 40 | . 0025 | .0156 | 1150 | -. 0072 | . 0085 | 3403 |
| 210 | . 50 | . 0034 | . 0159 | 1164 | -. 0074 | . 0097 | 3471 |
| 210 | . 60 | .004? | . 0157 | 1128 | -. 0035 | . 0102 | 3365 |
| 210 | . 70 | . 0015 | . 0185 | 1305 | . 0015 | . 0122 | 2898 |
| 2.10 | . 74 | . 0037 | . 0150 | 555 | . 0025 | .0125 | 1036 |
| 2.10 | . 78 | . 0008 | . 0159 | 788 | . 0040 | . 0123 | 1520 |
| 210 | . 82 | .0009 | . 0162 | 1711 | . 0052 | .0115 | 3058 |
| 210 | . 86 | -. 0011 | . 0164 | 1625 | . 0074 | . 0096 | 3044 |
| 2.10 | .90 | -. 0017 | . 0157 | 1713 | . 0097 | . 0076 | 2824 |
| 210 | . 94 | -. 0048 | .0161 | 1787 | . 0096 | . 0073 | 2793 |
| 210 | . 98 | -. 0045 | . 0153 | 1846 | . 0089 | . 0064 | 2657 |
| 210 | 1.02 | -. 00046 | . 0155 | 1932 | .0083 | . 0083 | 2677 |
| 210 | 1.04 | -. 00049 | . 0161 | 1732 | .0080 | .0063 | 2610 |
| 210 | 1.12 | -. 00057 | . 0160 | 1840 | .0065 | . 0053 | 2633 |
| 240 | . 20 | .00? 0 | . 0154 | 3104 | 0.0000 | . 0065 | 2509 |
| 240 | . 40 | . 0009 | . 0170 | 3010 | -. 0072 | . 0079 | 3022 |
| 240 | . 50 | .0030 | . 0170 | 2909 | -.0084 | . 0090 | 3164 |
| 240 | . 60 | . 0053 | . 0179 | 2846 | -. 0212 | . 0096 | 2826 |
| 240 | . 70 | . 0039 | . 0178 | 2348 | -. 0035 | . 0106 | 2364 |
| 240 | .74 | . 004 ? | . 0171 | 2516 | -. 0028 | . 0106 | 2535 |
| 240 | . 78 | . 0035 | . 0183 | 2638 | -. 00018 | .0135 | 2501 |
| 240 | . 82 | .0ก28 | . 0183 | 2501 | . 0001 | . 0117 | 2303 |
| 240 | . 86 | .OO30 | .7181 | 2747 | . 0010 | . 0115 | 2348 |
| 240 | . 90 | . 0015 | . 0177 | 2790 | . 0057 | . 0106 | 2230 |
| 2.40 | . 94 | .000¢ | .0169 | 2784 | . 0072 | . 0074 | 1789 |
| 240 | . 98 | .000? | .0171 | 2865 | . 0080 | . 0071 | 1968 |
| 240 | 1.02 | -. 00007 | .0169 | 2831 | . 0085 | .0067 | 1834 |
| 240 | 1.04 | -. 002.1 | . 0169 | 2849 | . 0081 | . 0065 | 1911 |
| 270 | . 20 | . 005.1 | . 0173 | 2048 | -. 0019 | . 0062 | 2815 |
| 270 | . 40 | .004? | . 0179 | 2041 | -. 00094 | . 00778 | 3050 |
| 270 | . 50 | .0045 | . 0188 | 1867 | -. 0126 | . 0078 | 2814 |
| 270 | . 60 | .0045 | . 0191 | 1795 | -. 0135 | . 0089 | 2349 |
| 270 | . 70 | .0036 | . 0210 | 1755 | -. 0151 | . 0108 | 2330 |
| 270 | . 74 | .0036 | . 0194 | 174) | -. 0149 | .0108 | 2236 |
| 270 | . 78 | .004: | .0207 | 1945 | -. 0149 | . 0106 | 2406 |
| 270 | . 82 | . 0024 | . 0208 | 1908 | -. 0136 | . 0109 | 2355 |
| 270 | . 86 | -001? | . 1241 | 2105 | -. 0105 | . 0112 | 2368 |
| 270 | . 90 | -.000? | . 0240 | 2054 | -. 007 ? | .0111 | 2014 |
| 2.70 | . 94 | -.000? | . 02.37 | 2137 | -.0014 | . 0120 | 1938 |
| 270 | . 98 | -.0008 | . 0233 | 2124 | . 0050 | . 0114 | 1824 |


|  | TARI, $3 .-$ Conclurier |  |  |  |  | $0 \because \cdots+\cdots \rightarrow \pi x$ <br> OF $\angle Q Q$ QUALITY $\lambda_{1}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\psi$ | $r / R$ | Mean | Standard <br> deviation | measurements | Mean | standard deviation | measurements |
| 270 | 1.02 | -. 0024 | . 0231 | 1888 | -. 0128 | . 0076 | 1125 |
| 270 | 1.04 | -. 00050 | . 0234 | 1072 | -. 0160 | . 0066 | 644 |
| 270 | 1.12 | -. 0045 | . 0239 | 311 | -. 0154 | . 0066 | 174 |
| 300 | . 20 | . 0055 | . 0213 | 124 | -. 0026 | . 0061 | 359 |
| 300 | . 40 | . 0063 | . 0201 | 104 | -. 0081 | . 0064 | 349 |
| 300 | . 50 | .0038 | . 0202 | 519 | -. 0135 | .0070 | 2879 |
| 300 | . 50 | . 0034 | . 0220 | 311 | -. 0173 | . 0084 | 1678 |
| 300 | . 70 | . 0074 | . 0223 | 145 | -. 0214 | . 0094 | 739 |
| 300 | . 74 | . 0037 | . 0230 | 104 | -. 0232 | . 0098 | 521 |
| 300 | . 78 | -- | -- | 0 | -. 02.67 | . 0095 | 225 |
| 300 | . 82 | -- | -- | 0 | -. 0249 | . 0095 | 221 |
| 300 | . 86 | -- | -- | 0 | -. 0254 | . 0085 | 199 |
| 300 | . 90 | -. 0005 | . 0236 | 2213 | -. 0255 | . 0097 | 3342 |
| 300 | . 94 | -. 0025 | . 0227 | 2205 | -. 0258 | . 0089 | 3525 |
| 300 | . 98 | -. 0024 | . 0219 | 1484 | -. 0247 | .0080 | 2317 |
| 300 | 1.02 | -. 0030 | . 0221 | 1052 | -. 0230 | .0076 | 1613 |
| 300 | 1.04 | -. 0049 | . 0207 | 854 | -. 0219 | . 0063 | 1253 |
| 300 | 1.10 | -.0067 | . 0212 | 422 | -. 0123 | . 0056 | 546 |
| 330 | . 20 | . 0072 | . 0209 | 221 | -. 0057 | . 0076 | 502 |
| 330 | . 40 | . 0059 | . 0208 | 262 | -. 00088 | . $0 \cap 70$ | 557 |
| 330 | . 50 | . 0038 | . 0177 | 215 | -. 0123 | . 0089 | 590 |
| 330 | . 50 | . 0071 | . 0191 | 189 | -. 0161 | . 0106 | 598 |
| 330 | . 70 | . 0049 | . 0185 | 198 | -. 0193 | . 0113 | 484 |
| 330 | . 74 | .0030 | . 0210 | 182 | -. 0203 | . 0111 | 452 |
| 330 | . 78 | . 0020 | . 0225 | 175 | -. 0223 | .0106 | 413 |
| 330 | . 82 | . 0018 | . 0203 | 138 | -. 0250 | .0107 | 313 |
| 330 | . 86 | . 0018 | . 0201 | 111 | -. 0261 | . 0092 | 233 |
| 330 | . 90 | -.0003 | .0176 | 105 | -. 0270 | . 0111 | 227 |
| 330 | . 94 | 0.0000 | . 0171 | 973 | -. 0293 | . 0079 | 3010 |
| 330 | . 98 | -. 0057 | . 0215 | 863 | -. 0295 | . 0068 | 2253 |
| 330 | 1.02 | -. 0057 | . 0208 | 703 | -.0287 | . 0063 | 2055 |


(a) Aerial view

(b) Schematic

Figure 1.- $14 \times 22$ Foot Suhsonic Tunnel.


Figure 2.- 2MRTS mounted in forward bay of the test section

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Figure 3.- Rotor blade planform. $R=32.5$ inches.

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Figure 4.- Schematic diagram of Laser Velocimeter Optics Subsystem.


Figure 5.- Laser Velorimeter positioned in test chamber.


Fiqure 6.- Schematic view of data aquisition
and control subsystem.


Figure 7.- Schematic of Seeding system.


## MEASUREMENTS

- U and V
- V only
- None

Figure 8.- Locations of velocity measurements, 3.0 inches above rotor tip path plane.

(a) $\boldsymbol{\psi}=0$ degrees

(b) $\boldsymbol{\psi}=30$ degrees

(c) $\psi=60$ degrees

Figure 9.- Radial distribution of mean induced inflow ratio $\left(\mu_{L}\right)$.

(d) $\psi=90$ degrees

(e) $\psi=120$ degrees


Figure 9.- Continued.

(g) $\psi=180$ degroos

(h) $\psi=210$ degrees


Figure 9.- Continued.

(k) $\psi=300$ degrees


Figure 9.- Concluded.

(b) $\psi=30$ degrees


Figure 10.- Radial distribution of mean induced inflow ratio $\left(\boldsymbol{\lambda}_{\boldsymbol{l}}\right)$.

(e) $\psi=120$ degrees


Flgure 10.- Continued.

(g) $\psi=180$ degrees

(h) $\psi=210$ degrees


Figure 10.- Continued.

(j) $\psi=270$ degrees

(k) $\psi=300$ degrees


Figure 10.- Concluded.

## ORIGINAL RAC COLOR PHOTOGRAPH

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$>^{8}$


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COLOR PHOTOGRAPH






Figure 13.- Induced inflow velocity measured at 0 degrees and $\mathrm{r} / \mathrm{R}$ of $\mathbf{0 . 2 0}$.




Figure 13.- Concluded.




Figure 14.- Induced inflow velocity meosured at 0 degrees and $\mathrm{r} / \mathrm{R}$ of 0.40 .




Figure 14.- Concluded.




Figure 15.- Induced inflow velocity meosured at 0 degrees and $r / R$ of 0.50 .



Figure 15.- Concluded.




Figure 16.- Induced inflow velocity measured at 0 degrees and $\mathrm{r} / \mathrm{R}$ of 0.60 .




Figure 16.- Concluded.




Figure 17.- Induced inflow velocity measured at 0 degrees and $r / R$ of 0.70 .


Figure 17.- Concluded.


Figure 18.- Induced inflow velocity measured at 0 degrees and $r / R$ of 0.98 .



Figure 19.- Induced inflow velocity measured at 0 degrees and $\mathrm{r} / \mathbb{R}$ of 1.02 .

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\lambda_{\iota}-\overline{\lambda_{\iota}}
$$




Figure 20.- Induced inflow velocity measured at 0 degrees and $\mathrm{r} / \mathrm{R}$ of 1.04.


Figure 21.- Induced inflow velocity measured at 0 degrees and $r / R$ of 1.10.


Figure 21.- Concluded.




Figure 22.- Induced inflow velocity measured at 30 degrees and $r / R$ of 0.20 .


Number of Occurrences


Amplitude spectrum,


Figure 22.- Concluded.




Figure 23.- Induced inflow velocity measured at 30 degrees and $\mathrm{r} / \mathrm{R}$ of 0.40 .




Figure 23.- Concluded.




Figure 24.- Induced inflow velocity measured at 30 degrees and $\mathrm{r} / \mathrm{R}$ of 0.50 .




Figure 24.- Concluded.


Figure 25.- Induced inflow velocity measured at 30 degrees and $r / R$ of 0.60 .




Figure 25.- Concluded.


Figure 26.- Induced inflow velocity measured at 30 degrees and $r / R$ of 0.70 .




Figure 26.- Concluded.


Figure 27.- Induced inflow velocity measured at 30 degrees and $r / R$ of 0.74 .




Figure 27.- Concluded.




Figure 28.- Induced inflow velocity meosured at 30 degrees and $r / R$ of 0.78 .


Number of Occurrences



Figure 28.- Concluded.



Figure 29.- Induced inflow velocity measured ot 30 degrees and $r / \mathbb{R}$ of 0.82 .




Figure 29.- Concluded.




Figure 30.- Induced inflow velocity measured at 30 degrees and $r / \mathbb{R}$ of 0.86 .


Number of
Occurrences


Figure 30.- Concluded.




Figure 31.- Induced inflow velocity measured at 30 degrees and $\mathrm{r} / \mathrm{R}$ of 0.90 .



Figure 31.- Concluded.




Figure 32.- Induced inflow velocity measured at 30 degrees and $r / R$ of 0.94 .




Figure 32.- Concluded.




Figure 33.- Induced inflow velocity measured at 30 degrees and $r / R$ of 0.98 .




Figure 33.- Concluded.




Figure 34.- Induced inflow velocity measured at 30 degrees and $r / R$ of 1.02 .



Figure 34.- Concluded.




Figure 35.- Induced inflow velocity measured at 30 degrees and $r / R$ of 1.04 .


Figure 35.- Concluded.



Figure 36.- Induced inflow velocity measured at 30 degrees and $r / R$ of 1.10 .




Figure 36.- Concluded.




Figure 37.- Induced inflow velocity measured at 60 degrees and $r / R$ of 0.20 .




Figure 37.- Concluded.




Figure 38.- Induced inflow velocity measured at 60 degrees and $r / R$ of 0.50 .




Figure 38.- Concluded.




Figure 39.- Induced inflow velocity measured at 60 degrees and $\mathrm{r} / \mathrm{R}$ of 0.60 .


Number of Occurrences



Figure 39.- Concluded.




Figure 40.- Induced inflow velocity measured at 60 degrees and $\mathrm{r} / \mathbb{R}$ of 0.70 .




Figure 40.- Concluded.


Figure 41.- Induced inflow velocity measured at 60 degrees and $r / R$ of 0.74 .




Figure 41.- Concluded.


Figure 42.- Induced inflow velocity measured at 60 degrees and $r / R$ of 0.78 .


Number of
Occurrences


Figure 42.- Concluded.




Figure 43.- Induced inflow velocity measured at 60 degrees and $r / R$ of 0.82 .



Figure 43.- Concluded.




Figure 44.- Induced inflow velocity measured at 60 degrees and $r / R$ of 0.86 .


Figure 44.- Concluded.


Figure 45.- Induced inflow velocity measured at 60 degrees and $r / R$ of 0.90 .


Number of
Occurrences


Figure 45.- Concluded.


Number of



Figure 46.- Induced inflow velocity measured at 60 degrees and $r / R$ of 0.94 .




Figure 46.- Concluded.


Figure 47.- Induced inflow velocity measured at 60 degrees and $\mathrm{r} / \mathbb{R}$ of 0.98 .

## ( $\bar{\lambda}_{\iota}=-0.007$




Figure 47.- Concluded.


Number of



Figure 48.- Induced inflow velocity measured at 60 degrees and $r / R$ of 1.02 .




Figure 48.- Concluded.




Figure 49.- Induced inflow velocity meosured at 60 degrees and $r / R$ of 1.04 .




Figure 49.- Concluded.


Number of Occurrences



Figure 50.- Induced inflow velocity measured at 60 degrees and $r / \mathbb{R}$ of 1.10 .



Figure 50.- Concluded.




Figure 51.- Induced inflow velocity measured at 90 degrees and $r / R$ of 0.20 .


Number of Occurrences



Figure 51.- Concluded.




Figure 52.- Induced inflow velocity measured at 90 degrees and $r / R$ of 0.40 .


Number of
Occurrences


Figure 52.- Concluded.


Figure 53.- Induced inflow velocity measured at 90 degrees and $r / R$ of 0.50 .


Number of Occurrences



Figure 53.- Concluded.




Figure 54.- Induced inflow velocity measured at 90 degrees and $r / R$ of 0.70 .


Number of Occurrences



Figure 54.- Concluded.


Figure 55.- Induced inflow velocity measured at 90 degrees and $r / R$ of 0.74 .


Number of Occurrences



Figure 55.- Concluded.




Figure 56.- Induced inflow velocity measured at 90 degrees and $r / R$ of 0.78 .




Figure 56.- Concluded.




Figure 57.- Induced inflow velocity measured at 90 degrees and $r / \mathbb{R}$ of 0.82 .




Figure 57.- Concluded.




Figure 58.- Induced inflow velocity measured at 90 degrees and $r / \mathbb{R}$ of 0.86 .




Figure 58.- Concluded.




Figure 59.- Induced inflow velocity measured at 90 degrees and $\mathrm{r} / \mathrm{R}$ of 0.90 .




Figure 59.- Concluded.




Figure 60.- Induced inflow velocity measured at 90 degrees and $r / R$ of 0.94 .




Figure 60.- Concluded.




Figure 61.- Induced inflow velocity measured ot 90 degrees and $r / R$ of 0.98 .




Figure 61.- Concluded.




Figure 62.- Induced inflow velocity measured at 120 degrees and $r / R$ of 0.20 .



Figure 62.- Concluded.


Number of Occurrences



Figure 63.- Induced inflow velocity measured at 120 degrees and $r / R$ of 0.40 .


Number of Occurrences



Figure 63.- Concluded.




Figure 64.- Induced inflow velocity measured at 120 degrees and $\mathrm{r} / \mathrm{R}$ of 0.50 .




Figure 64.- Concluded.




Figure 65.- Induced inflow velocity measured at 120 degrees and $r / R$ of 0.60 .


Number of Occurrences



Figure 65.- Concluded.




Figure 66.- Induced inflow velocity measured at 120 degrees and $r / R$ of 0.70 .




Figure 66.- Concluded.


Figure 67.- Induced inflow velocity measured at 120 degrees and $\mathrm{r} / \mathrm{R}$ of 0.74 .




Figure 67.- Concluded.


Figure 68.- Induced inflow velocity measured at 120 degrees and $r / R$ of 0.78 .


Figure 68.- Concluded.




Figure 69.- Induced inflow velocity measured at 120 degrees and $\mathrm{r} / \mathrm{R}$ of 0.82 .
(



Figure 69.- Concluded.




Figure 70.- Induced inflow velocity measured at
120 degrees and $\mathrm{r} / \mathrm{R}$ of 0.86 .




Figure 70.- Concluded.


Figure 71.- Induced inflow velocity measured at 120 degrees and $\mathrm{r} / \mathrm{R}$ of 0.90 .




Figure 71.- Concluded.




Figure 72.- Induced inflow velocity measured at 120 degrees and $\mathrm{r} / \mathrm{R}$ of 0.94 .


Number of Occurrences



Figure 73.- Induced inflow velocity measured at 120 degrees and $\mathrm{r} / \mathrm{R}$ of 0.98 .




Figure 74.- Induced inflow velocity measured at 120 degrees and $r / R$ of 1.02 .


Figure 75.- Induced inflow velocity measured at 120 degrees and $r / R$ of 1.04 .




Figure 76.- Induced inflow velocity measured at 120 degrees and $\mathrm{r} / \mathbb{R}$ of 1.12 .




Figure 77.- Induced inflow velocity measured at 150 degrees and $\mathrm{r} / \mathrm{R}$ of 0.20 .




Figure 77.- Concluded.




Figure 78.- Induced inflow velocity measured at 150 degrees and $r / R$ of 0.40 .




Figure 78.- Concluded.




Figure 79.- Induced inflow velocity measured at 150 degrees and $r / R$ of 0.50 .



Figure 79.- Concluded.



Figure 80.- Induced inflow velocity measured at 150 degrees and $r / R$ of 0.60 .


Number of



Figure 80.- Concluded.




Figure 81.- Induced inflow velocity measured at 150 degrees and $r / R$ of 0.70 .




Figure 81.- Concluded.


Number of Occurrences



Figure 82.- Induced inflow velocity measured at 150 degrees and $\mathrm{r} / \mathrm{R}$ of 0.74 .




Figure 82.- Concluded.




Figure 83.- Induced inflow velocity measured at 150 degrees and $\mathrm{r} / \mathrm{R}$ of 0.78 .



Figure 83.- Concluded.




Figure 84.- Induced inflow velocity measured at 150 degrees and $r / R$ of 0.82 .



Figure 84.- Concluded.




Figure 85.- Induced inflow velocity measured at 150 degrees and $r / R$ of 0.86 .




Figure 85.- Concluded.


Figure 86.- Induced inflow velocity measured at 150 degrees and $\mathrm{r} / \mathrm{R}$ of 0.90 .




Figure 86.- Concluded.




Figure 87.- Induced inflow velocity measured at 150 degrees and $r / R$ of 0.94 .



Figure 87.- Concluded.




Figure 88.- Induced inflow velocity measured at 150 degrees and $\mathrm{r} / \mathrm{R}$ of 0.98 .


Figure 88.- Concluded.



Figure 89.- Induced inflow velocity measured at 150 degrees and $r / R$ of 1.02 .




Figure 89.- Concluded.




Figure 90.- Induced inflow velocity measured at 150 degrees and $\mathrm{r} / \mathbb{R}$ of 1.04 .




Figure 90.- Concluded.



Figure 91.- Induced inflow velocity measured at 150 degrees and $\mathrm{r} / \mathrm{R}$ of 1.12 .




Figure 91.- Concluded.


Figure 92.- Induced inflow velocity measured at 180 degrees and $\mathrm{r} / \mathrm{R}$ of 0.20 .




Figure 92.- Concluded.




Figure 93.- Induced Inflow velocity measured at 180 degrees and $\mathrm{r} / \mathrm{R}$ of 0.40 .




Figure 93.- Concluded.


Flgure 94.- Induced inflow velocity meosured at 180 degrees and $r / R$ of 0.50 .




Figure 94.- Concluded.


Number of
Occurrences



Figure 95.- Induced inflow velocity measured at 180 degrees and $r / R$ of 0.60 .


Number of



Figure 95.- Concluded.





Flgure 96. - Induced inflow velocity measured at 180 degrees and $\mathrm{r} / \mathrm{R}$ of 0.70 .




Figure 96.- Concluded.




Figure 97.- Induced inflow velocity measured at 180 degrees and $\mathrm{r} / \mathrm{R}$ of 0.74 .


Number of Occurrences



Figure 97.- Concluded.



Figure 98.- Induced inflow velocity measured at 180 degrees and $\mathrm{r} / \mathrm{R}$ of 0.78 .




Figure 98.- Concluded.



Flgure 99.- Induced inflow velocity measured at 180 degrees and $\mathrm{r} / \mathrm{R}$ of 0.82 .




Figure 99.- Concluded.
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Figure 100.- Induced inflow velocity measured ot 180 degrees and $r / R$ of 0.86 .


Number of



Figure 100.- Concluded.




Figure 101.- Induced inflow velocity measured at 180 degrees and $r / R$ of 0.90 .


Figure 101.- Conciuded.




Figure 102.- Induced inflow velocity measured at 180 degrees and $\mathrm{r} / \mathrm{R}$ of 0.94 .




Figure 102.- Concluded.




Figure 103.- Induced inflow velocity measured at 180 degrees and $r / R$ of 0.98 .


Number of Occurrences


Amplitude spectrum, rms


Figure 103.- Concluded.



Figure 104.- Induced inflow velocity measured at 180 degrees and $\mathrm{r} / \mathrm{R}$ of 1.02 .



Figure 104.- Concluded.




Figure 105.- Induced inflow velocity measured ot 180 degrees and $r / R$ of 1.04 .




Figure 105.- Concluded.




Figure 106.- Induced inflow velocity measured at 180 degrees and $\mathrm{r} / \mathrm{R}$ of 1.12 .




Figure 106.- Concluded.

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$$




Figure 107.- Induced inflow velocity measured at 210 degrees and $\mathrm{r} / \mathrm{R}$ of 0.20 .




Figure 107.- Concluded.




Figure 108.- Induced inflow velocity measured at 210 degrees and $r / R$ of 0.40 .




Figure 108.- Concluded.




Figure 109.- Induced inflow velocity measured at 210 degrees and $\mathrm{r} / \mathrm{R}$ of 0.50 .


Number of Occurrences



Figure 109.- Concluded.




Figure 110.- Induced inflow velocity measured at 210 degrees and $\mathrm{r} / \mathrm{R}$ of 0.60 .


Number of Occurrences



Figure 110.- Concluded.




Figure 111.- Induced inflow velocity measured at 210 degrees and $r / R$ of 0.70 .


Number of Rotor position, degrees


Figure 111.- Concluded.




Figure 112.- Induced inflow velocity measured at 210 degrees and $r / R$ of 0.74 .




Figure 112.- Concluded.


Figure 113.- Induced inflow velocity measured at 210 degrees and $r / R$ of 0.78 .




Flgure 113.- Concluded.




Figure 114.- Induced inflow velocity measured at 210 degrees and $r / R$ of 0.82 .


Number of Occurrences



Figure 114.- Concluded.


Number of Occurrences



Figure 115.- Induced inflow velocity measured at 210 degrees and $r / R$ of 0.86 .




Figure 115.- Concluded.




Figure 116.- Induced inflow velocity measured at 210 degrees and $r / R$ of 0.90 .


Number of
Occurrences



Figure 116.- Concluded.




Figure 117.- Induced inflow velocity measured at 210 degrees and $r / R$ of 0.94 .


Number of Occurrences



Figure 117.- Concluded.
位


Figure 118.- Induced inflow velocity measured at 210 degrees and $r / R$ of 0.98 .




Figure 118.- Concluded.




Figure 119.- Induced inflow velocity measured at 210 degrees and $\mathrm{r} / \mathrm{R}$ of 1.02 .



Number of Occurrences



Figure 119.- Concluded.




Figure 120.- Induced inflow velocity measured at 210 degrees and $r / R$ of 1.04 .





Figure 120.- Concluded.
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Figure 121.- Induced inflow velocity measured at 210 degrees and $\mathrm{r} / \mathrm{R}$ of 1.12.


Number of Occurrences



Figure 121.- Concluded.




Figure 122.- Induced inflow velocity measured at 240 degrees and $r / R$ of 0.20 .




Figure 122.- Concluded.




Figure 123.- Induced inflow velocity measured at 240 degrees and $\mathrm{r} / \mathrm{R}$ of 0.40 .


Number of Occurrences



Figure 123.- Concluded.


Number of



Figure 124.- Induced inflow velocity measured at 240 degrees and $r / \mathbb{R}$ of 0.50 .


Number of Occurrences


Amplitude spectrum, rms


Figure 124.- Concluded.


Number of Occurrences



Figure 125.- Induced inflow velocity measured at 240 degrees and $r / R$ of 0.60 .


Number of Occurrences



Figure 125.- Concluded.


Number of Occurrences



Figure 126.- Induced inflow velocity measured at 240 degrees and $\mathrm{r} / \mathrm{R}$ of 0.70 .


Number of Occurrences



Figure 126.- Concluded.



Figure 127.- Induced inflow velocity measured at 240 degrees and $r / R$ of 0.74 .




Figure 127.- Concluded.




Figure 128.- Induced inflow velocity measured at 240 degrees and $r / R$ of 0.78 .


Number of Occurrences



Figure 128.- Concluded.




Figure 129.- Induced inflow velocity measured ot 240 degrees and $r / R$ of 0.82 .


Number of Occurrences



Figure 129.- Concluded.




Figure 130.- Induced inflow velocity measured at 240 degrees and $r / R$ of 0.86 .




Figure 130.- Concluded.




Figure 131.- Induced inflow velocity measured at 240 degrees and $r / R$ of 0.90 .




Figure 131.- Concluded.




Figure 132.- Induced inflow velocity measured at 240 degrees and $\mathrm{r} / \mathrm{R}$ of 0.94 .


Number of Occurrences



Figure 132.- Concluded.




Figure 133.- Induced inflow velocity measured at 240 degrees and $\mathrm{r} / \mathrm{R}$ of 0.98 .




Figure 133.- Concluded.



Figure 134.- Induced inflow velocity measured at 240 degrees and $\mathrm{r} / \mathrm{R}$ of 1.02 .


Number of Occurrences



Figure 134.- Concluded.




Figure 135.- Induced inflow velocity measured at 240 degrees and $r / R$ of 1.04 .




Figure 135.- Concluded.




Figure 136. - Induced inflow velocity measured at 270 degrees and $r / R$ of 0.20 .


Number of



Figure 136.- Concluded.


Figure 137.- Induced inflow velocity measured at 270 degrees and $r / R$ of 0.40 .


Number of Occurrences



Figure 137.- Concluded.



Figure 138.- Induced inflow velocity measured at 270 degrees and $\mathrm{r} / \mathrm{R}$ of 0.50 .


Number of



Figure 138.- Concluded.




Figure 139.- Induced inflow velocity measured at 270 degrees and $r / R$ of 0.60 .


Number of Occurrences



Figure 139.- Concluded.




Figure 140.- Induced inflow velocity measured at 270 degrees and $\mathrm{r} / \mathrm{R}$ of 0.70 .


Number of Occurrences



Figure 140.- Concluded.




Figure 141.- Induced inflow velocity measured at 270 degrees and $r / R$ of 0.74 .




Figure 141.- Concluded.




Figure 142.- Induced inflow velocity measured at 270 degrees and $\mathrm{r} / \mathrm{R}$ of 0.78 .



Figure 142.- Concluded.




Figure 143.- Induced inflow velocity measured at 270 degrees and $\mathrm{r} / \mathrm{R}$ of 0.82 .




Figure 143.- Concluded.


Figure 144.- Induced inflow velocity measured at 270 degrees and $r / R$ of 0.86 .


Number of Occurrences



Figure 144.- Concluded.




Figure 145.- Induced inflow velocity measured at 270 degrees and $r / R$ of 0.90 .


Number of Occurrences


Amplitude spectrum, rms


Figure 145.- Concluded.




Figure 146.- Induced inflow velocity measured ot 270 degrees and $\mathrm{r} / \mathrm{R}$ of 0.94 .


Number of



Figure 146.- Concluded.


Figure 147.- Induced inflow velocity measured at 270 degrees and $r / R$ of 0.98 .




Figure 147.- Concluded.




Figure 148.- Induced inflow velocity measured at 270 degrees and $\mathrm{r} / \mathrm{R}$ of 1.02 .

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Figure 148.- Concluded.




Figure 149.- Induced inflow velocity measured at 270 degrees and $\mathrm{r} / \mathrm{R}$ of 1.04 .




Figure 149.- Concluded.




Figure 150.- Induced inflow velocity measured at 270 degrees and $r / R$ of 1.12 .




Flgure 150.- Concluded.


Figure 151.- Induced inflow velocity measured at 300 degrees and $r / R$ of 0.20 .




Figure 151.- Concluded.




Figure 152.- Induced inflow velocity measured at 300 degrees and $\mathrm{r} / \mathrm{R}$ of 0.40 .




Figure 152.- Concluded.



Figure 153.- Induced inflow velocity measured at 300 degrees and $\mathrm{r} / \mathrm{R}$ of 0.50 .


Number of Occurrences



Figure 153.- Concluded.




Figure 154.- Induced inflow velocity measured at 300 degrees and $\mathrm{r} / \mathrm{R}$ of 0.60 .




Figure 154.- Concluded.




Figure 155.- Induced inflow velocity measured at 300 degrees and $r / R$ of 0.70 .


Number of Occurrences



Figure 155.- Concluded.




Figure 156.- Induced Inflow velocity measured ot 300 degrees and $r / R$ of 0.74 .




Figure 156.- Concluded.




Figure 157.- Induced inflow velocity measured at 300 degrees and $r / R$ of 0.78 .



Figure 158.- Induced inflow velocity measured at 300 degrees and $r / R$ of 0.82 .


Number of Occurtences



Figure 159.- Induced inflow velocity measured at 300 degrees and $r / R$ of 0.86 .




Figure 160.- Induced inflow velocity measured at 300 degrees and $r / R$ of 0.90 .




Figure 160.- Concluded.




Figure 161.- Induced inflow velocity measured at 300 degrees and $r / R$ of 0.94 .



Figure 161.- Concluded.


Number of
Occurrences


Amplitude spectrum,


Figure 162.- Induced inflow velocity measured at 300 degrees and $r / R$ of 0.98 .




Figure 162.- Concluded.




Figure 163.- Induced inflow velocity measured ot 300 degrees and $r / R$ of 1.02 .


Number of Occurrences



Flgure 163.- Concluded.




Figure 164.- Induced inflow velocity measured at 300 degrees and $r / R$ of 1.04 .




Figure 164.- Concluded.


Figure 165.- Induced inflow velocity measured at 300 degrees and $r / R$ of 1.10 .




Figure 165.- Concluded.




Figure 166.- Induced inflow velocity measured at 330 degrees and $r / R$ of 0.20 .


Figure 166.- Concluded.




Flgure 167.- Induced inflow velocity measured at 330 degrees and $\mathrm{r} / \mathrm{R}$ of 0.40 .




Figure 167.- Concluded.




Figure 168.- Induced inflow velocity measured at 330 degrees and $r / R$ of 0.50 .



Figure 168.- Concluded.



Flgure 169.- Induced inflow velocity measured at 330 degrees and $r / R$ of 0.60 .




Figure 169.- Concluded.



Figure 170.- Induced inflow velocity measured at 330 degrees and $\mathrm{r} / \mathrm{R}$ of 0.70 .




Figure 170.- Concluded.


Figure 171.- Induced inflow velocity measured at 330 degrees and $r / R$ of 0.74 .




Figure 171.- Concluded.




Figure 172.- Induced inflow velocity measured at 330 degrees and $\mathrm{r} / \mathrm{R}$ of 0.78 .




Figure 172.- Concluded.


Figure 173.- Induced inflow velocity measured at 330 degrees and $\mathrm{r} / \mathrm{R}$ of 0.82 .




Figure 173.- Concluded.




Figure 174.- Induced inflow velocity measured at 330 degrees and $r / R$ of 0.86 .




Figure 174.- Concluded.




Figure 175.- Induced inflow velocity measured at 330 degrees and $\mathrm{r} / \mathrm{R}$ of 0.90 .


Number of Occurrences



Figure 175.- Concluded.




Figure 176.- Induced inflow velocity measured at 330 degrees and $r / R$ of 0.94 .


Number of



Figure 176.- Concluded.




Figure 177.- Induced inflow velocity measured at 330 degrees and $\mathrm{r} / \mathrm{R}$ of 0.98 .


Number of Occurrences



Figure 177.- Concluded.



Figure 178.- Induced inflow velocity measured at 330 degrees and $\mathrm{r} / \mathrm{R}$ of 1.02 .



Figure 178.- Concluded.


Number of Occurrences



Figure 179.- Induced inflow velocity measured at 330 degrees and $r / R$ of 1.04 .




Figure 179.- Concluded.




Figure 180.- Induced inflow velocity measured at 330 degrees and $r / R$ of 1.10 .




Figure 180.- Concluded.
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## Report Documentation Page

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Inflow Mensurements Made with A raser Velocimeter On
A Helicopter Model In Forward Flight, Volume $V$ rapered Planform Rlades at an Advance Ratio of 0.23
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16. Abstract

An experimental investigation was conducted in the 14 - by 22 -Foot Subsonic Timnel at NASA Langley Research Center to measure the inflow into a scale model helicopter rotor in forward flight ( $\mu_{\infty}=0.23$ ). The measurements were made with a two-component Laser Velocimeter (LV) one chord above the plane formed by the path of the hlade tips. A conditional sampling technique was employed to determine the position of the rotor at the time that each velocity measurement was made so that the arimuthal fluctuations in velocity could be determined. Medsurements were made at a total of 168 separate locations in order to clearly define the inflow character. This data is presented herein without analysis. In order to increase the availability of the resulting data, both the mean and azimuthally dependent values are included as part of this report on two 5.25 inch floppy disks in Microsoft Corporation MS-DOS format.


