

Net Current Measurements and Secondary Electron Emission Characteristics of the Voyager Plasma Science Experiment and Their Impact On Data Interpretation

RALPH L. MCNUTT, JR.

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AND SECONDARY ELECTRON EMISSION
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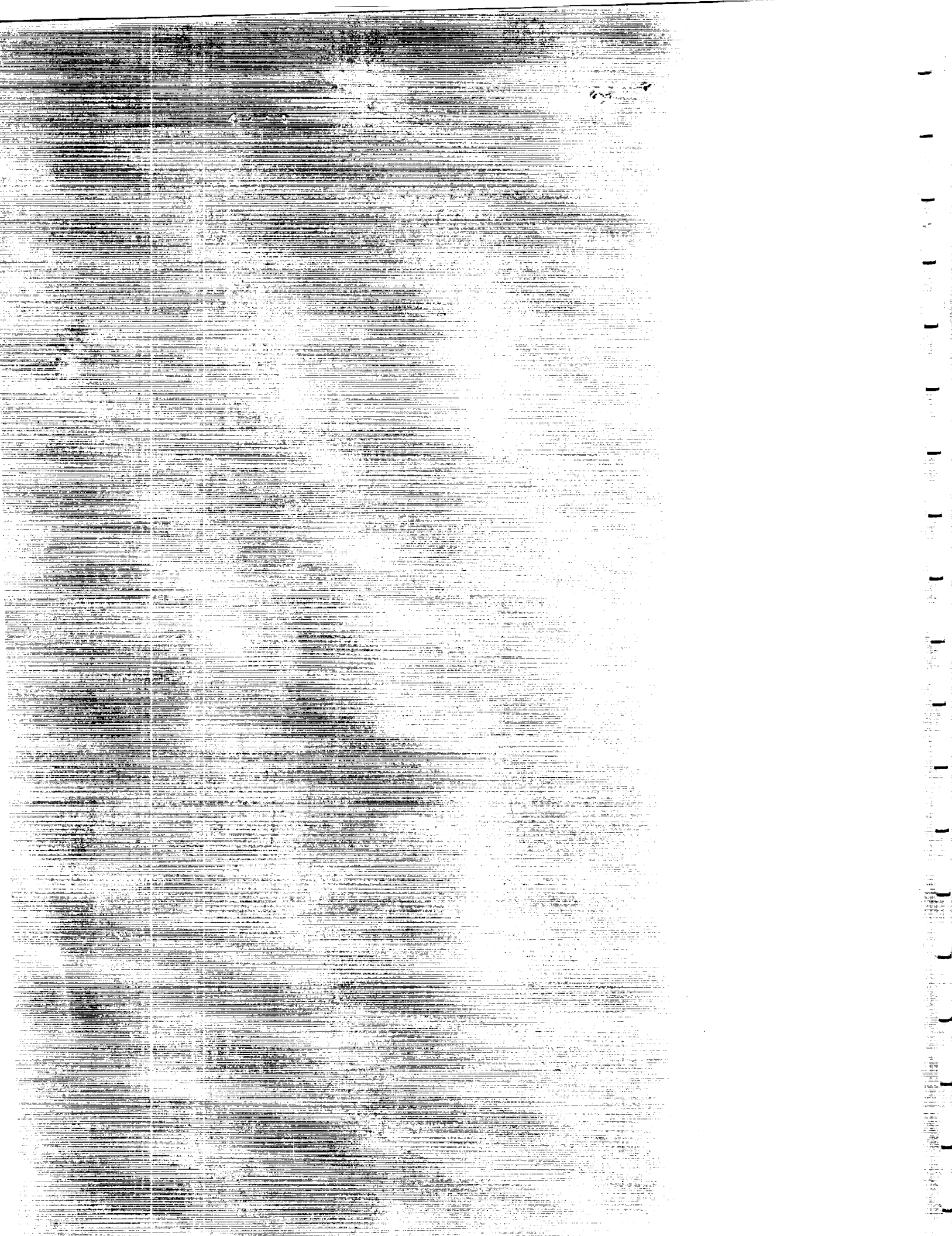
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Department of Physics and Center for Space Research
Massachusetts Institute of Technology
Cambridge, MA 02139

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The Voyager Plasma Science (PLS) instrument is capable of returning integral (DC) current measurements as well as normal plasma measurements. These measurements are similar in some respects to measurements made with a Langmuir probe or a retarding potential analyzer, although there are significant differences. The integral measurements have been made during calibration sequence in the solar wind, during Cruise Science Maneuvers, and within the magnetospheres of Jupiter and Saturn by Voyager 1. After the failure of the PLS experiment after the Saturn encounter, that instrument was placed in the DC return mode and returned possibly usable data from early 1981 through early 1985. The DC return measurements are difficult to interpret and are above threshold values only for relatively large fluxes; the determination of the measured current level is dependent on the operating temperature of the preamplifiers which further complicates the interpretation. Nevertheless, these measurements can be used to determine the efficiency of the suppressor grid at preventing the loss of secondary electrons off of the collector plate. Some DC return measurements have been invaluable in aiding in the interpretation of some electron plasma measurements which had not previously been understood. We find that the electron spectra can be significantly modified by the presence of second generation secondary electrons produced by the production of either first generation secondaries or photoelectrons on the support ring of the negative high voltage modulator grid within the instrument housing. This accounts for electron spectra obtained when the PLS side sensor is illuminated by sunlight while in one of the electron modes. The effect also explains the characteristics of electron spectra obtained by Voyager 2 in the plasma voids near Ganymede during the Jupiter encounter and in the "charging region" while that spacecraft was outbound from Uranus. As a result, we have also identified other regions in which the Voyager spacecraft was charged to -1 kV and have noted regions in which care must be taken in the analysis of the suprathermal component of the measured electron distributions.

INTRODUCTION

The Plasma Science (PLS) experiment on the two Voyager spacecraft has returned a wealth of scientific information concerning the state of the interplanetary medium [Gazis, 1984] and the plasma populations of the magnetospheres of the outer planets visited to date [Belcher, 1983 and references therein; Sittler *et al.*, 1981; Lazarus and McNutt, 1983; Sittler *et al.*, 1983; Richardson, 198 ; McNutt *et al.*, 1987; Selesnick and McNutt, 1987]. In addition to the plasma measurements made most of the time by the instrument upon which all previously reported analyses are based, there are integral (DC return) measurements. These measurements effectively bypass the action of the modulator grid in the instrument and are only taken over a limited dynamical range [Bridge *et al.*, 1977]. These measurements are also difficult to interpret as is made clear in the body of this paper. However, they have proven to be an invaluable diagnostic tool in better understanding the effects due to the production of secondary electrons within the instrument housing itself. In particular, there are electron spectra which do not "make sense" given the normal operating characteristics and environment of the PLS instrument. Using the DC return measurements and the production of photoelectrons within the instrument as guides and diagnostics, we have been able to explain semi-quantitatively data which had previously defied explanation.

DC RETURN MEASUREMENTS

DC return currents and normal plasma data are returned from the A and D cups of the PLS instrument in the DC return mode; plasma data from the B and C cups is replaced by A cup DC return and D cup DC return currents, respectively. The quantization steps for DC return currents are large to accommodate both large fluxes and currents of both positive and negative sign. The nominal sensitivity/range of the DC amplifiers (there are 2 DC measurement chains) is $\pm (10^{-10}$ to $10^{-7})$ amperes [Bridge *et al.*, 1977]. In the main PLS analysis software package (VGRANL), there is a conversion lookup table from DN to femtoamperes. This table, in the common block PLCONS, has negative currents from -1.00×10^5 fA (femtoamperes; $1 \text{ fA} = 10^{-15} \text{ A}$) for DN=0 to -1.00×10^8 fA for DN=127 and positive currents from $+7.5 \times 10^4$ fA for DN=128 to $+1.00 \times 10^8$ fA for DN=255. A listing of these currents is included as Table 1 and a graph of the absolute value of these currents versus DN is included as Figure 1. The calibration curve from which this table was constructed is not known, but it is probably based upon a laboratory calibration curve (A. Mavretic, private communication) which was made at a temperature of $+25^\circ \text{ C}$ (this is the most detailed curve which is available to me and is for SN003, the flight spare; there is also a "quick check" measurement which was made for SN002, launched on Voyager; SN001 is on Voyager 2 - the spacecraft numbers and instrument serial numbers *really are* reversed). This curve is appended as Figure 2; note that for negative

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currents there is a small difference between the conversions for the A and D cups.

From another laboratory notebook (A. Mavretic, private communication), a full set of I_{DC} calibration have been found for SN002 (also designated Flight 1 or F1). These are from the summer of 1977. Figures 3 through 5 plot DC current (positive and negative) versus DN for both A and D cups. These were made for three different temperatures: -10°C , $+27^{\circ}\text{C}$, and $+50^{\circ}\text{D}$. Figures 6 through 9 show DC current versus temperature for constant DN values. Figures 6 and 7 are for the A cup (negative and positive current) and Figures 8 and 9 are for the D cup (negative and positive current). The calibration changes as a function of temperature (the preamplifier temperature) can be significant for the DC measurements; this is (thankfully!) not the case for the AC, i.e., plasma, measurements.

DC return spectra typically show a DN value of 128 (positive threshold) in the D cup and a flat spectrum at the upper positive levels in the A cup (from DC return measurements in the L and M - positive modulator voltage - modes). At lower positive voltages in the A cup, higher positive currents indicative of the solar wind are apparent (at small enough heliographic distances). The currents at large potentials in the A cup have been ascribed to photoelectron production in the A cup, presumably off of the gold-plated collector plate. The D cup is usually in shadow so no photoelectrons should be produced. Considerable structure is found in the DC return spectra (all modes) from the Voyager 1 encounters with Jupiter and Saturn when particle fluxes into the cups were large; the PLS-A science link (the nomenclature may have been different for the Saturn encounter) included DC return measurements about every 45 minutes. No DC measurements were made routinely during the Voyager 2 encounters with Jupiter, Saturn or Uranus. The few DC return measurements made during the Voyager 2 encounter with Jupiter occurred far from the planet when particle fluxes were low and exhibit the same flat structure as found in the solar wind.

R. S. Selesnick attempted to verify the photoelectron hypothesis by plotting the DC return current from the A cup (channel 128) as a function of spacecraft distance from the sun. At these voltages, there should be no contribution from the solar wind, even if the particle flux in the wind is very large. Selesnick's plots are appended as Figures 10 (Voyager 1) and 11 (Voyager 2). Although the current tends to follow an r^{-2} line for both spacecraft, there are unexplained deviations. Two possible effects not taken into account are i) the angle at which the sunlight is incident upon the collector and ii) changes in the DN to current conversion as the spacecraft moves out from the sun and cools (the calibration curve for a temperature of $+25^{\circ}\text{C}$ is used to do all of the conversions). The last point on the Voyager 1 plot is for day 236 of 1984 (corresponding to a heliocentric distance of 20.8 AU). In spot checking the printout of currents made at JPL (O. Divers, private communication), I found that in the L mode measurements in the A cup, the DN values in channel 16 are down to 128 by this time (Selesnick was using M mode spectra). In the lower channels, DC levels apparently due to the solar wind are being measured. The DN value in channel 1 is down to 129 (1 DN above positive

threshold) on day 25 of 1985. The corresponding heliocentric distance is 22 AU. Information on the solar wind velocity and flux (hence, density) is apparently available from the DC return measurements through this time. The M mode measurements seem to be clamped to a constant value indicative of the solar wind; in other words, the M mode measurements do seem to have been effected adversely by the failure.

In Voyager Memorandum #153, I gave a rough estimate that the DC return values should be near threshold at ~ 24 AU. This distance was reached near the end of 1985, so the available numbers are roughly consistent. At 400 km s^{-1} , 10^5 fA corresponds to a charge density of $\sim 0.23 \text{ cm}^{-3}$ (see Table 3 of Voyager Memorandum #99).

PHOTOELECTRON YIELDS

The photoelectron yield can vary as $\sec\theta$ although this effect is dependent on both polarization and wavelength of the incident light in a complicated fashion (see Whipple [1981]). The energy distribution of photoelectrons can be well represented by a Maxwellian energy distribution,

$$f(E) = \frac{2}{\pi^{1/2} E_0^{3/2}} E^{1/2} e^{-E/E_0} \quad (1)$$

Here $\int_0^{\infty} f(E) dE = 1$ and E_0 is the "temperature" of the photoelectrons.

In dealing with both photoelectron and secondary electron emission, a flux "distribution function" is used [Grard, 1973; Hachenberg and Brauer, 1959]. In this case the Maxwellian energy distribution is

$$j(E) = E/E_0^2 e^{-E/E_0} \quad (2)$$

Again, the normalization is such that $\int_0^{\infty} j(E) dE = 1$. Note that the most probable energy E_{mp} - defined at the maximum of $j(E)$ - is E_0 . Hence, when a "most probable" secondary electron energy is quoted in the literature, it is *almost always* with respect to $j(E)$ and, therefore, is the same as the secondary "temperature."

Grard [1973] finds values of E_0 ("most probable energy") of 0.88 eV for gold (appropriate for the collector plate) and 1.02 eV for graphite (appropriate more or less for the black conducting paint - up to 12% carbon by weight (A. C. Whittlesey, private communication, Feb. 20, 1987) - used on the Voyager spacecraft; secondary and photoemission characteristics of the paint are not known).

PLS INSTRUMENT TEMPERATURES

Three instrument temperatures are routinely telemetered to Earth in the PLS engineering records. Knowledge of the temperature decreases during the missions of Voyagers 1 and 2 as they move away from the sun is of both general interest as well as necessary for the proper interpretation of DC return measurements: the calibration curves for translating DN (data numbers) to I_{DC} values is dependent upon the temperature of the preamplifier and measurement chain.

The temperature readouts from the PLS instruments on both

spacecraft have been indicating decreasing temperature with increasing distance from the sun. Temperatures and other readouts are returned in engineering records and are plotted to produce engineering plots. Such plots have been made for both spacecraft for a great deal of the two missions and are in a notebook in the programmers' office. Printout of the engineering records consists of 9 integer fields (IENG) and 3 real fields (TEMPS). The integer fields are data numbers, and 8 of these are plotted on engineering plots with the not terribly illuminating labels ESUP, VREF, VCOM, PSUP, TSEN, TPMC, TMOD, and MODE. The non-temperature data is part of the PLS analog multiplexer output. The latter is comprised of the PLS backup science data ("a 0 to 3 volt representation of the four decade plasma measurement to be used in the event that the PLS ADC ceases to function"), the internal reference voltage of 10 volts, the suppressor voltages, and a combination of the positive and negative 15 volt supply voltages; correspondence with the engineering plots is obvious given this information. Backup science data DNs are not routinely plotted; backup science data is also not well documented at this juncture. What documentation I have found is in JPL document 618-505, Vol. IV, Rev. B.

The temperature data are interpreted as follows

Label	Description	IENG ()	TEMP ()
TMOD	Modulator Temperature	1	1
TPMC	Preamplifier and Measurement Chain	2	2
TSEN	Sensor Temp. (A cup Housing ?)	3	3

The units of TEMP are °C; the conversion algorithm from DN to °C is not documented but buried in the subroutine MJSTEM. The DN values are first converted to resistance values. These are then converted to temperatures via interpolation from a lookup table stored with the subroutine. The sensor temperature conversion is different from the other two. Lookup tables and graphs for the conversion for the sensors on S/C 31 are included as Appendix A (from JPL document 618-301).

Engineering plots were not routinely made during the encounter periods; they have been recently run for one day periods during the encounters. Variation during these periods was minimal; typical temperatures from the encounters are listed in the following table.

S/C	Date	Planet	TSEN (°C)	TPMC (°C)	TMOD (°C)
1	1979/ 64	Jupiter	-123.58	9.07	11.18
1	1980/318	Saturn	-148.22	4.14	6.95
2	1979/189	Jupiter	-122.39	9.07	11.18
2	1981/237	Saturn	-147.17	4.84	6.95
2	1986/ 24	Uranus	-160.35	3.43	6.95

Selesnick's numbers (referred to above) have not been corrected for the temperature shift; how much this will "help" his curves is not yet known.

PHOTOCURRENT LOSS FROM DC RETURN MEASUREMENTS

At the Earth *Garrett* [1981] lists the photoelectron flux from solar spectrum photons incident on gold as $j_{ph} = 2.9 \times 10^{-9} \text{ A cm}^{-2}$ (see his Table 4). The effective area of each of the main sensor cups is $A_{eff} = 66 \text{ cm}^2$ (see p.12 of *Barnett*, [1984]), and the photoelectron flux at Jupiter is down from that at Earth by a factor of 5.2^{-2} . This should produce a photocurrent at the collector plate of

$$I_{ph} = j_{ph,Earth} A_{eff} r^{-2} \quad (3)$$

or $7.08 \times 10^6 \text{ fA}$. I have looked at the L mode DC return measurements from the Voyager 1 Jupiter encounter (DC return measurements were made every 45 minutes as part of the PLS-A science link). The following table lists DC return times and the A cup current and the D cup current in channel 16 (the D cup current was at the positive threshold of $7.5 \times 10^4 \text{ fA}$ for most of the spectra). Note that the currents listed are nominal values using the lookup table exhibited in Table 1 and Figure 1.

Time	$I_{A,16} \text{ fA}$	DN, A	$I_{D,16} \text{ fA}$
62 0601	1.71×10^6	192	7.50×10^4
63 1924	1.38×10^6	191	7.50×10^4
64 0503	8.20×10^5	184	7.50×10^4
64 0737	1.38×10^6	191	7.50×10^4
64 0921	1.38×10^6	191	7.50×10^4
64 1426	1.38×10^6	191	7.50×10^4
64 1829	-2.40×10^6	66	-2.0×10^6
64 1922	-2.40×10^6	66	-4.9×10^6
65 0629	4.14×10^5	164	-2.0×10^6

The difference between the fluxes into A and D should be representative of the current measured due to the loss of photoelectrons within the instrument (i.e. those not returned to the collector plate by the potential on the suppressor grid). If we take 1.5×10^6 as a representative photocurrent, this implies an internal loss of ~ 20 %, consistent with more detailed calculations on secondary electron losses in the side sensor. From Voyager Bulletin #37, entrance into solar occultation was 1637 and exit from solar occultation was 1849. This is consistent with the no photoelectron production and the measured negative current at 1829. The very large negative currents at 1922 of day 64 are apparently due to photoelectron production in the side sensor; due to a maneuver, the angle between the D cup normal and the sun decreased to just under a critical angle discussed elsewhere. The large negative currents on 65 are presumably from the hot electron population near the spacecraft, but this needs further investigation (and use of the proper DN to current curve). Four DC return measurements at Saturn on day 317 of 1980 (at 0736, 0738, 0828, and 0919) all gave the D cup at positive threshold and the A cup at $5.80 \times 10^5 \text{ fA}$, somewhat larger than predicted than a simple r^{-2} scaling from Jupiter would predict, but, again, this could be related to the change in the preamplifier temperature.

There are a few other things to note about the Voyager 1 encounter with Saturn. The first is that there was one 360° yaw turn at Saturn, similar to the PLOMAN and FLOMAP maneuvers by Voyager 1 at Jupiter. For the record, appropriate information about the maneuver (FSMAN-5) is as follows:

Voyager 1 Yaw Maneuver at Saturn	
Type of Rotation	Start Time of Rotation
Roll	318/2117:02
Yaw	318/2128:24
Yaw	318/2146:29
Roll	318/2210:42

My notes indicate that the first yaw went through 132° and the second completed the 360° turn.

In addition, it should be noted that the sun occultation ingress for Voyager 1 was 1980-318/0153:23 and the sun occultation egress was 1980-318/0240:01. In occultation, there is no evidence from a cursory examination of the 1800 plots that any charging of the spacecraft to high negative levels was occurring. This is probably not surprising in that the bulk of the electrons had a relatively low (< 50 eV) temperature during this time. It should also be noted that of DC return spectra were acquired around ~ 318/0200 within the occultation period. The spectra from the A cup do show that the photoelectron current from the collector plate was turned off. They also indicate large negative currents at positive potentials up to several tens of volts. If such a signature has occurred elsewhere in the DC return spectra, I have not yet run across it.

SECONDARY ELECTRON EMISSION FROM THE COLLECTOR PLATE

I am also investigating the possibility of "experimentally" obtaining the suppressor efficiency from looking at DC return measurements made early in the mission when sunlight illuminated the D cup collector plate. In addition, George and I are working on a quantitative model of secondary electron loss from the D cup. Secondary electrons can also be modeled with Maxwellian distribution functions [Whipple, 1981].

The collector plate is electroplated gold on an electrolous Ni-Cu phosphate substrate on Al. The substrate prevents the "leeching" of the magnesium structure into the gold plating. Plating details (from the instrument specifications) are as follows: 1) flash Cu to thickness of 100 ± 50 micro in., 2) underplate non-magnetic electroless Ni per Mil-C-26074 Class I to thickness of 500 ± 100 micro in., 3) overplate bright Au per Mil-G-45204 Type I Class II to thickness of 100 ± 25 micro in. (from drawing 21-8001, rev. C). Hence the gold plating has a thickness of at least 2 × 10⁻⁴ cm.

Secondary electrons are emitted from a surface layer much thinner than this, ~ 10⁻⁶cm (see p. 423 of Dekker [1957]); hence the secondary emission characteristics of gold are appropriate for determining the secondary yield and energy spectrum.

The most extensive compilation of the secondary emission characteristics of metals appears to be due to Kollath [1947, 1956]. The best "temperature" for secondaries emitted from gold is ~2 to 3 eV (from table 1 of [Kollath, 1956]) obtained from a primary electron energy of 150 eV. The secondary emission spectra are not very sensitive to the energy of the primary for primary energies above ~ 20 eV [Hachenberg and Brauer, 1959] and at least up to ~ 1.6 MeV [Schultz and Pomerantz, 1963]; these are well outside the energy range for which the total secondary electron yield is significant (see below). A temperature of ~ 3 eV is also consistent with the theoretical treatment of Chung and Everhart [1973]. For quantitative modeling of the loss of secondaries from the collector, we have assumed a temperature of 2.5 eV; as this is small compared to the instrument suppressor voltages of ~ -8 V and -95 V, small errors in the temperature have a negligible effect on our results.

The loss of secondary electrons (i.e. those produced at the collector and not returned to the collector by the suppressor grid) was considered in detail for the PLS instrument by Sittler in 1979 (E. C. Sittler, Jr., private communication). The geometrical problem is illustrated in Figure 12 (figure due to E. C. Sittler). For a given radial location r on the collector plate (of radius r_c), an impact by a primary electron will cause the emission of secondary electrons with an energy distribution as discussed above and an angular distribution which is isotropic [Whipple and Parker, 1969] (for an extended emitting surface) with respect incidence angle θ and azimuthal angle ϕ (early work, see e.g. Hachenberg and Brauer [1959] and McDaniel [1964], suggested a $\cos \theta$ emission distribution, but isotropy seems to now be accepted by most workers in the field []). Consider a secondary electron of energy E_s emitted at angle θ . The trajectory will follow a straight line in the field-free region between the collector plate and the grounded grid (Grid 1 - this is the "normal suppressor" electrical configuration). Grid 2, held at the suppressor potential V_{sup} will decelerate the electron motion perpendicular to the collector plate, resulting in the parabolic trajectory shown in the figure for $E_{se} < V_{sup}$; higher energy electrons penetrate the potential barrier and are immediately lost from the system. The parabolic trajectory will again intersect grid 1 a distance R from the position at which it first crossed the grid plane. If d_{sup} is the distance between the grounded grid and the suppressor grid (equivalent to $z_2 - z_1$ in Fig. 12), then an elementary calculation shows that

$$R = 2d_{sup} \frac{E_s}{eV_{sup}} \sin 2\theta \quad (4)$$

The electron will again move in a straight line until it crosses the plane of the collector plate. If d (z_1 in the figure) is the separation of the collector plate and the ground grid, the electron will intersect the plane of the collector plate a distance a (equal to Δx in the figure) from where it was created where

$$a = 2d \tan \theta + R \quad (5)$$

If the impact point is outside of the collector, the secondary electron is lost, giving rise to a spurious (positive) current in the data. From Figure 12, it is obvious that the electrons emitted in a cone of half angle θ map to a circle in the plane of the

collector plate. As long as $a - r < r_c$ there will be a range of azimuthal angles ϕ such that $|\phi| \leq \phi_{\max}$ for which the secondaries will be lost. For larger values of a (corresponding to smaller values of θ), all of the secondaries will be lost.

Noting again that both the angular and energy distributions of the secondary electrons is independent of the energy and angular distributions of the primary electrons, we can calculate a solid angle $\Omega_{\text{lost}}(r)$ corresponding to secondaries which are lost. Define the angular limit $\theta_1(E_s)$ as the smallest value of θ for which $a = r_c$ using equations 4 and 5 (found numerically); define $\theta_2(E_s)$ as the largest value of θ for which $a = r_c$ or $\pi/2$, whichever is smaller (N.B. θ considered as a function of R is a double-valued function). Define ϕ_0 by

$$\phi_0(\theta, E_s) \equiv \cos^{-1} \left[\frac{r_c^2 - r^2 - a^2}{2ra} \right] \quad \text{for } a < r + r_c \quad (6)$$

$$\phi_0(\theta, E_s) \equiv \pi \quad \text{for } a \geq r + r_c \quad (7)$$

The angular limits are, of course, dependent upon the energy of the secondaries due to the parabolic section of their trajectories. The solid angle for lost current (integrated over the secondary electron energy spectrum) is

$$\Omega_{\text{lost}}(r) = 2 \int_0^{eV_{\text{sup}}} f(E_s) dE_s \int_{\theta_1(E_s)}^{\theta_2(E_s)} h(\theta) \phi_0(\theta, E_s) \sin\theta \, d\theta \quad (8)$$

where $h(\theta)$ is the angular distribution of secondaries, and $j(E_s)$ is their energy distribution function with respect to current, given by equation 2. We have computed $\Omega_{\text{lost}}(r)$ both for the case of isotropically emitted secondaries, i.e., $h(\theta) = 1$ and for a cosine distribution (normalized to unity over a hemisphere), $h(\theta) = 2\cos\theta$ for the various operating modes of the instrument.

There are four relevant operating modes of the instrument for which $\Omega_{\text{lost}}(r)$ has been evaluated: the normal suppressor configuration, described above, and the "reversed suppressor" configuration, in which the grounded grid and suppressor grid are reversed; for each configuration there are two suppressor voltages, one for the low energy electron measurements (E1) and one for the high energy electron (E2) and ion (L, M) measurements (see *Bridge et al.* [1977]). Relevant parameters are listed in the table below.

Mode	Configuration	V_{sup} (V)	d (cm)	d_{sup} (cm)
E1	Normal	-8.05	0.996	0.417
E1	Reversed	-7.70	0.000	0.996
E2, L, M	Normal	-95.2	0.996	0.417
E2, L, M	Reversed	-85.9	0.000	0.996

The distances between the grids are from Figure 2.12 of *Barnett* [1984]. The cups of the main sensor only have a "normal" configuration and use a suppressor voltage of -95.2 V (these numbers are from Voyager Memorandum #69 of 1/8/80 which indicates the data source as Mavretic's notebook #4. The voltages quoted are within 50 mV for SN002 and SN003; it is

assumed that SN001 has the same values, but these are not documented).

Note that for $\phi_0 = \pi$, $\theta_1 = 0$, and $\theta_2 = \pi/2$, $\Omega_{\text{lost}}(r) = 2\pi$, i.e. the solid angle in a hemisphere. G. S. Gordon, Jr. has normalized $\Omega_{\text{lost}}(r)$ to 2π to find the fraction of secondaries lost per unit incident current as a function of radial distance r from the center of the D cup collector plate. E. C. Sittler, Jr. performed the same calculations in 1979; his results for the fraction of secondary electrons lost in the E1 and E2 modes are shown in Figures 13 and 14, respectively. Sittler normalized the losses to their maximum values and expressed radial distance as a fraction of the collector radius. The maximum loss occurs at the edge of the collector plate. In E1 Ed found a loss of 26.3% for the normal suppressor configuration and 12.5% for reversed suppressor configuration. For E2 the loss fractions at the edge are 25.3% and 3.5%, respectively.

The results of Gordon's calculation are shown in Figures 15 through 19. Again the *normalized* value of $\Omega_{\text{lost}}(r)$ is plotted. In Figure 15, results for all of the cases noted in the table above are plotted. The notations "iso" and "cos" refer to isotropic and cosine angular distributions of the emitted secondaries, respectively. The notations "std" and "rev" refer to whether the suppressor voltage is on the standard or reversed grid. The suppressor potentials are also indicated. Figures 16 through 19 show the loss fraction for cosine and isotropic secondary distributions for each of the four suppressor modes; the dotted lines indicate the isotropic results and the solid line cosine results. Note that in the standard configuration - denoted by "s" in the label on the graph - the isotropic distribution produces more losses as there are more electrons emitted at large angles of incidence which are not reflected back to the collector until they have moved relatively far from their point of emission. In the reversed configuration - denoted by an "r" - the cosine distribution gives rise to more losses as there are more "forward emitted" secondaries which simply penetrate the potential barrier in the forward direction; electrons emitted at large angles of incidence are immediately "shoved" back into the collector plate by the suppressor potential. Note that "i" refers to the case of L, M, or E2 and "e" in the label refers to the E1 potential, e.g., the label "is" identifies the normal, or standard, suppressor configuration with -95.2 volts on the suppressor grid.

Listings of the loss fraction as a function of radial distance across the collector plate are included in Appendix B. The file "out.rlme15ci" contains numerical output for the isotropic cases; the file "out.rlme15cc" contains the the corresponding numbers for the case of a cosine angular distribution. The parameters used for each table are listed at the top: "ds", "d", and "volts" correspond to d_{sup} , d , and V_{sup} respectively. The parameter "e0" refers to the assumed energy of the secondary electrons, here 2.5 eV for each case.

We have not included either elastically scattered (reflected) primaries or inelastically scattered (rediffused or "backscattered" primaries) electrons [*Hachenberg and Brauer*, 1959; *Dekker*, 1957]. Reflected primaries have the same energy as the incident electrons and display a maximum in the direction of the incident beam [*Hachenberg and Brauer*, 1959]. According to *Whipple* [1981], reflection is only significant at primary energies less than -10 eV. Backscattered electrons occupy the energy range

between ~50 eV and the energy of the primary. They obey the same angular distribution law as the true secondaries [Hachenberg and Brauer, 1959] and can contribute a net backscattered current ~ 0.3 of the incident current [Whipple, 1981]. As the true secondaries contribute most of the current at the collector, we only consider their effect here; it should be noted that a sizable fraction of the backscattered electrons will be lost in any event if the energy of the primaries substantially exceeds eV_{sup} .

SECONDARY YIELD AND LOST SECONDARY CURRENT

The loss of secondary electrons produced at the collector plate is measured as a positive current by the DC measurement chain, and, if modulated, as a positive current by the AC measurement chain (see Bridge *et al.* [1977]). This current is superimposed on the "direct" current produced by the primary flux of charged particles on the collector plate. It is convenient to consider separately the "direct" or primary current as opposed to the secondary current. This is done in terms of the secondary yield function δ where

$$j_s = \delta j_p \quad (9)$$

and the subscripts refer to the current density of the primary particles and that of the secondary particles [Hachenberg and Brauer, 1959]. In what follows we concentrate on the production of secondary electrons by primary electrons; at primary energies above several keV the production of secondary electrons by primary ions can also give rise to significant effects [Whipple, 1981].

The yield of secondary electrons from primary electrons is, in general, a function of both the primary energy E_p and angle of incidence θ_p . However, the yield curve tends to be universal, i.e., independent of the emitting material, if parameterized in terms of the maximum yield δ_m and the energy at this maximum E_m (see e.g., Dekker [1957]). The yield function is further characterized by the energies E_I and E_{II} corresponding, respectively, to the lowest and highest primary energy for which the secondary yield exceeds unity. For gold δ_m is 1.45 at E_m of 800 eV, and E_I and E_{II} are 150 eV and > 2000 eV, respectively [Kollath, 1956]. An analytic form for the yield is given by Whipple [1981] which we use here

$$\delta(E_p, \theta_p) = \frac{1.114\delta_m}{\cos\theta_p} \left[\frac{E_m}{E} \right]^{0.35} \times \left\{ 1 - \exp \left[-2.28 \cos\theta \left[\frac{E}{E_m} \right]^{1.35} \right] \right\} \quad (10)$$

Note that for small energies or angles of incidence near 90°, $\delta(E_p, \theta_p) \propto E_p$.

The response of the PLS side sensor to electrons is a convolution of the the distribution function of the electrons with the "response" function of the detector. The response function can be conveniently separated into a transparency function T and an area overlap function A ; the latter contains the effects of the refraction of particle trajectories by the various grids as well as the decrease in effective collector area due to particle

trajectories within the detector [Barnett, 1984; Barnett and Olbert, 1986].

If we define a coordinate system with the z axis along the symmetry axis of the side sensor, or D cup, then the angle of incidence of a primary electron with respect to the collector plate is the same as that with respect to the entrance aperture of the detector (both the grid at the entrance aperture and the collector plate are at the spacecraft "ground" (which is the potential of the conducting surface of Voyager; the latter can, of course, have some floating potential with respect to the surrounding plasma). Hence $\theta_p = \tan^{-1}(v_z/v_t)$ where v_z is the component of electron velocity into the sensor and v_t is the component of velocity transverse to the sensor. The energy dependence of the yield follows from $E_p = 1/2 m_e (v_z^2 + v_t^2)$.

For a given angle of incidence and given primary energy, the region of the collector plate illuminated by electrons passing through the aperture grid, will, in general, be the common overlap area of three circles whose centers are colinear [Barnett, 1984]. This is a two parameter function $A(d_{ag}, d_{gc})$ which can be described by the distance between the centers of the aperture image and the guard ring image d_{ag} and between the centers of the guard ring image and collector image d_{gc} , respectively; the function can be written in closed analytic form [Barnett, 1984]. The distances are offsets determined by the refraction effects which are, in turn, functions of v_z , v_t , V_{sup} , and V_{mod} the modulator potential. The current measured due to electrons more energetic than eV_{mod} is

$$I_{DC,m} = e \int_{v_m}^{\infty} dv_z v_z \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} d^2v_t f(v) T A \quad (11)$$

where $v_m = (2eV_{mod}/m_e)^{1/2}$. The DC return current actually measured by the instrument is $I_{DC} = 1/2 (I_{DC,m} + I_{DC,m-1})$, i.e. the average current in a given channel (when the modulator is on, which is usually the case).

To calculate the effect of secondary current loss, we have modified the area overlap function as follows. We have numerically integrated the solid angle for secondary loss $\Omega_{loss}(r)$ over the overlap area to find an effective "loss area" A_{loss}

$$A_{loss} \equiv \int_{\text{overlap area}} \Omega_{loss}(r) dA \quad (12)$$

The secondary current lost due to primary electrons more energetic than eV_{mod} is given by the current density at the collector plate multiplied by the secondary yield and the loss area, viz.

$$I_{sec} = e \int_{v_m}^{\infty} dv_z v_z \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} d^2v_t f(v) T \delta A_{loss} \quad (13)$$

(Note that the lost secondary current density per velocity space volume is simply the primary current density at the collector plate $\times \delta \times \Omega_{loss}$).

In the DC return mode, the current measured for modulator voltage V_{mod} is given by $I_{DC} - I_{sec}$. In the normal plasma mode, the measured current is the modulated part of this current.

To incorporate this effect into the simulation of electron

spectra, Gordon computed a set of eight loss tables (low and high suppressor potential; normal and reverse suppressor configuration; isotropic and cosine law for the angular distribution of the secondary electrons). The numerical integrations of eqn. 12 for these 8 cases were run on a Sun Microsystems Workstation on the weekend preceding May 18, 1987. The jobs were run in the background beginning on the preceding Friday and completed late on Sunday, May 17.

The loss tables have been incorporated into the PMODEL package via modified versions of the subroutine REDART (which reads the tables into the SUN from the disk where they are stored) and the functions ARSIDE and CPRESP. In CPRESP, the overlap area A (refer to eqn. 11 above) has been replaced by $A - \delta A_{loss}$ (refer to eqn. 12 above). The output from PMODEL then produces synthesized electron spectra which are corrected for the inefficiency of the suppressor. Listings of the relevant code are included as Appendix C. Note that the hand lettering on the listing for CPRESP is only applicable to using the code to simulate the effects of photoelectrons; the code as printed on the laser printer was implemented for the case of secondary electrons made from primary electron (rather than photon) impacts. Equation 10 with $\delta_m = 1.45$ and $E_m = 800$ eV is used to compute the yield.

Figure 20 displays a contour map of the normal area overlap function; the two axes are the relative displacement of the aperture and shield circle centers (DAS) and the relative displacement of the shield and collector circle centers (DSC) (these correspond to the coordinates X and Y, respectively, which appear in the call to ARSIDE in the function CPRESP). Figures 21 and 22 show the area (in cm²) as a function of one of these two parameters (labeled "1" and "2") for a constant value of the other. The distance from one side of the aperture to the other side of the shield is 10.8 cm, and the distance from one side of the shield to the other side of the collector plate is 11.5 cm; hence, these are the values of DAS and DSC for which the area overlap goes to zero. Parameter 1 is therefore DAS, and parameter 2 is DSC. A three-dimensional projection of the overlap area function is shown in Figure 23.

Figures 24 through 39 are plots of A_{loss} versus DAS (= "1") and DSC (= "2"), in an analogous fashion to the plots of A in Figures 21 and 22. Each plot is labeled with a four character alphanumeric label: "vcan", where "v" is "e" (E1 suppressor voltage) or "i" (L, M, and E2 suppressor voltage), "c" is "s" (normal suppressor configuration) or "r" (reversed suppressor configuration), "a" is "i" (isotropic angular distribution of secondaries) or "c" (cosine angular distribution of secondaries) and "n" is "1" or "2" depending upon whether DAS or DSC is the independent variable plotted along the abscissa. Note that in each case in which the independent parameter is DSC, the effective loss area is a minimum for DSC=0. As this parameter is increased, the losses increase (refer to Figure 15), but the overlap area decreases (Figures 21 and 22). Hence, there is a maximum loss for some nonzero value of DSC. Also note that the scale along the ordinate is different for Figures 24 through 39.

Figures 40 and 41 are contour plots for the E2, normal configuration case, for isotropic and cosine distributions of the secondaries, respectively. Corresponding three-dimensional

representations for these two cases are shown (on the same scale) in Figures 42 and 43, respectively. Figure 44 reproduces Figure 42 but on the same scale as Figure 23; from this last comparison, it is obvious that the loss of secondary electrons from the collector plate can decrease the measured electron current but cannot change its sign (a seemingly trivial point which is important in accounting for some of the PLS electron spectra).

We simulated electron spectra (E2 mode) by using PMODEL and including the loss portion for assumed isotropic and cosine distributions in the normal suppressor configuration. Figures 45, 46, and 47 show simulated currents for an isotropic Maxwellian distribution of electrons at a temperature of 400 eV assuming, respectively, no losses, isotropic emission of secondaries, and a cosine law for the emission of secondaries. The losses decrease the measured currents by ~20% or less. Note that the apparent discontinuity between channels 3 and 4 is due to the suppressor grid; the threshold of channel 4 is -92.3 volts whereas the suppressor potential is -95.2 volts. The currents in the first three channels are due entirely to modulation of the trajectories of the electrons in the input distribution with energies greater than 95 eV (this is the so-called feedthrough effect). To further investigate this effect, we also simulated a κ distribution with a most probable speed corresponding to an energy of 9.85 eV. The case for no losses is shown in Figure 48. This spectrum is qualitatively similar to those observed in the vicinity of the "voids" in the Jovian magnetosphere by Voyager 2 [McNutt et al., 1987]. The high energy cutoff is due to numerical cutoffs used in simulating the spectrum. The spectrum including losses from isotropic secondaries is shown in Figure 49 and the loss current itself in Figure 50.

EXPERIMENTAL VERIFICATION OF THE SUPPRESSOR EFFICIENCY

General Considerations

The calculation of the apparent current due to the inefficiency of the suppressor grid is complex enough that it is desirable to verify it experimentally. Efforts are currently underway at M.I.T. to do so in a vacuum chamber using the side sensor of the Flight Spare PLS experiment (as of this writing, Sept. 17, 1988, these have not yet begun). In addition to what can be done in a laboratory (which can approach but not really duplicate the environment of interplanetary space), we can look for this effect in some of the plasma measurements themselves, in which the local environment is correct but the types of measurements were not really optimized for looking for this effect. We noted previously that photoelectrons and secondary electrons have similar energy distributions for production from gold surfaces, the mean energy of the photoelectrons being smaller (0.88 eV versus ~2.5eV). These energies are small with respect to typical potentials within the PLS detectors; hence, the emitted electrons should follow similar trajectories. No experimental information on the angular distribution of emitted photoelectrons appears to be readily available; however, it is reasonable to assume that the angular distributions are also similar. We can thus use sunlight into the instrument hitting the collector plate as a probe to determine the suppressor loss as a function of the illuminated part of the collector plate.

When the instrument is in an electron measurement mode, photoelectrons are emitted by the support ring for the negative high voltage grid whenever the angle between the cup normal and the sun is less than 78.5°. If sunlight also hits the collector plate, photoelectrons will also be emitted there, but the loss current is small compared to that produced by those photoelectron coming from the negative modulator support. To eliminate this effect, the instrument must be in a positive ion detection mode. In this case, the only surfaces with negative potentials are the suppressor grid, which has a small cross sectional area, and the buckout grid. The latter has only a small negative potential which alternates with a positive potential. As the suppressor grid is between it and the collector plate, any electrons from the buckout grid cannot reach the collector plate in any case.

The loss of photoelectron current from the collector plate cannot be affected by the modulator potential and will give rise to only a DC signal as the modulator steps. This is the source of the DC current in the high channels of the A cup measured during cruise. The geometry of the A cup is complex enough that a good mathematical model for the suppressor losses, while possible to construct, will also be very complex. Fortunately, there were a series of cruise maneuvers conducted during the cruise phase of both spacecraft during which the D cup collector plate is illuminated by the sun, and the instrument is in DC return mode.

Cruise Maneuvers

Several types of changes in spacecraft attitude are made during cruise. Early in the mission Cruise Science Maneuvers (CRSMVR) were performed, consisting of 25 roll turns (counterclockwise about the +Z axis of the spacecraft, which points opposite to the high gain antenna) and 10 yaw turns (counterclockwise about the +Y axis of the spacecraft, which is aligned with the projection of the science boom perpendicular to the +Z axis - see Figure 51). Later in the mission these were changed to mini-Cruise Science Maneuvers (Mini-CRSMVR) which included fewer revolutions of the spacecraft. The original idea was to partially roll the spacecraft so as to bring the D cup directly across the sun during the yaws. As far as I can tell this was not done, probably as the result of operational constraints of which I am not aware. A listing of all maneuvers through a complete revolution for both spacecraft as well as a memo describing our original thoughts on PLS measurements (from J.D. Sullivan, dated June 14,1978) are included as Appendix D.

I have looked in some detail at the CRSMVR yaw turns on Voyager 1 on day 258 of 1978. There is one sequence of DC return measurements (normal suppressor) for one full yaw early on day 258. Other measurements during the yaws are normal plasma and current calibrations (CURCAL) with both modulator on and off, all with normal suppressor. The minimum angle between the D cup normal and the sun is 43.3°, corresponding to the angle between the D cup normal and the +X axis of the spacecraft (refer to Figure 51). Sunlight reaches the collector plate in the D cup when the sun-cup angle is less than 63.1°. Due to the fairly rapid rotation rate of the spacecraft (~32 minutes to rotate through 360°), this limits the available DC

return spectra for which the theory and observations can be compared.

The DC return measurements were removed from the sequence when the change was made to mini-CRSMVRs. From the maneuver list in Appendix D, this limits the comparison to 11 maneuvers on Voyager 1 and 6 maneuvers on Voyager 2. The comparison is further limited by the distance between the spacecraft and the sun. The suppressor in the D cup is apparently more efficient at returning photoelectrons to the collector plate than is the suppressor in the A cup. In addition, the geometry during the yaws limits the illuminated area of the collector in the D cup. These effects combined with the relatively high threshold for detectable current in the DC return mode further limits the availability of data. As the spacecraft both receded from the sun, the observed current decreased to threshold before the CRSMVRs were changed to mini-CRSMVRs and the DC return measurements were deleted from the measurement sequence. The following tables list the CRSMVRs by date, the maximum DC return DN in the D cup in channel 16 of the L mode, and whether evidence of photoelectrons in the DC returns in the electron modes is present.

Voyager 1			
SCET	Max DN (IDC)	Photoelectrons	Range (AU)
1978-048	172	Yes	2.4
1978-257/8	151	Yes	4.1
1979-034	146	Yes	5.1
1979-288/9	130	Yes	6.4
1980-031	N/A	N/A	7.1
1980-168	128	Yes	8.2
1981-041	128	??	9.9

More information concerning the DC return levels after the Voyager 1 failure can be found in Voyager Memorandum #157. No maneuver data could be found from the tape logs on day 31 of 1980.

Voyager 2			
SCET	Max DN (IDC)	Photoelectrons	Range (AU)
1977-362	177	Yes	1.9
1978-275	N/A	N/A	4.0
1979-155	136	Yes	5.2
1980-024	128	Yes	6.1
1980-136	128	Yes	6.7
1981-148	128	Yes	9.0
1982-103	128	No	10.0

Data from a maneuver on day 275 of 1978 could not be located and the mini-CRSMVR on day 155 of 1979 does have DC return data during a yaw turn. The SOEs have not been

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investigated closely to clear up these discrepancies. During the yaw turn on day 24 of 1980, the lower channels of the D cup registered 134 DN and fell off to 128 at the location of the solar wind peak in the normal plasma data for the D cup. The same behavior occurred on day 136 of 1980, with the first channel of the D cup showing a maximum of 132 DN. On day 148 of 1981, the solar wind can no longer be seen in the DC return measurements from the D cup. N.B. the "Range" is actually the heliocentric distance of the spacecraft.

In spite of the entry for 1982-103 there were photoelectrons observed in the E1 and E2 modes during the Uranus encounter during a spacecraft maneuver (day 24 of 1986). In addition, the threshold for detecting the solar wind in the DC return A cup currents is apparently lower for Voyager 2 than for Voyager 1 (refer to discussion above). As of day 160 of 1987, Voyager 2 was 23.0 AU from the sun, and the first channel of the L mode (A cup) showed a DN of 132 in DC return. Channel 16 registered a DN of 130 from photoelectrons. The "break" in the L mode spectrum occurs at the location of the solar wind peak in the A cup as indicated by the normal plasma data.

To attempt to test the numerical loss calculations, we have concentrated on the Voyager 1 Cruise Science Maneuver from day 258 of 1978. From the PLS engineering output for this time of the maneuver, the electronics temperature (TPMC) 12.6°C and the sensor temperature (TSEN) was -117.5°C. Modulation of the temperatures during the maneuver is clear from the engineering plots from this period (Figure 52). The times of the L mode spectra used, the DN value in channel 16, the corresponding current (corrected for temperature using interpolated values from Figure 9), and the angle between the D cup normal and the sun (using the nominal sensor orientation with respect to the spacecraft) are shown in the following table.

I_{DC} From CRSMVR 1978-258			
SCET	DN	I (fA)	$\theta_{D, \text{sun}}$
0132:25.276	128	$< 10^5$	75.0°
0134:01.276	128	$< 10^5$	63.3°
0135:37.276	128	$< 10^5$	53.2°
0137:13.276	144	2.50×10^5	45.9°
0138:49.276	151	3.25×10^5	43.1°
0140:25.276	151	3.25×10^5	45.6°
0142:01.276	145	2.58×10^5	52.7°
0143:37.276	128	$< 10^5$	62.8°
0145:13.276	128	$< 10^5$	74.4°

It is immediately obvious that the variation in current does not exactly track the variation in angle; whether this is related to the motion of the cup, shading of the instrument, bias in the timing information, hysteresis in the electronics or whatever is unknown. Another feature which is not understood is that when both the A and D cups are in shadow, at 0156:25.276 - angles between the sun and the normals of the A and D cups 66.6° and 136°, respectively, negative currents were measured in both cups. At other angles, DN of 128 were recorded in shadow.

To see if this behavior was peculiar to this maneuver (and to check for errors in the analysis), a cruise maneuver on Voyager

2 was also examined in some detail. The first one, from day 362 of 1977, was examined; the electronics temperature is not readily available so only the DN values from channel 16 (L mode, DC return, normal suppressor) are listed. The angles are obviously incorrect; the changes in the DN values are well-centered in the time period during which photoelectrons are observed in the E1 and E2 modes. Examination of the trajectory data indicates that the time labels are off by about the round-trip light time between the spacecraft and Earth (to within a minute). This error in the trajectory data precludes a better analysis. The trajectory data corresponding to the Voyager 2 Cruise Science Maneuver on day 155 of 1979 and the Voyager 1 maneuver on day 34 of 1979 are in Jupiter encounter format; the pointing information is supposed to be updated every 48 s, rather than every 4 m on the usual CRSMVR tapes (which is interpolated to provide the angles listed in the tables).

I_{DC} From CRSMVR 1977-362		
SCET	DN	$\theta_{D, \text{sun}}$
0606:00.350	128	97.2°
0607:36.350	128	109.0°
0609:12.350	128	121.0°
0610:48.350	170	130.0°
0612:24.350	177	136.0°
0614:00.350	175	137.0°
0615:36.350	169	132.0°
0617:12.350	140	124.0°
0618:48.350	128	113.0°
0620:24.350	128	101.0°

Examination of these maneuvers in more detail should provide better estimates on the angles through which the sunlight was entering the side sensor as a function of time.

Predicted Photocurrent at the Collector Plate

To compare the theoretical predictions of suppressor loss with the data, the quantity A_{loss} of equation 12 must be computed for the illuminated area of the D cup collector plate. As photons are not refracted by the fields between the intervening grids as electrons are, A_{loss} is a one parameter function; the parameter can be taken to be the angle from the D cup normal at which sunlight enters the cup. To perform this calculation, the subroutine CPRESP was modified as shown by the handwritten notes in Appendix C. The actual code used is appended in Appendix E along with the effective loss area for both isotropic and cosine angular distributions of the secondaries. The optical transparency of the intervening grid wires is also listed. As the measured currents are from the positive ion mode, the lookup tables used are for -95.2 volts on the suppressor grid in the normal suppressor configuration.

Comparison of Measured Currents with the Data

The saturation photoelectron current density for gold under solar irradiation is $j_{\text{photo, Au}} = 2.9 \times 10^{-9}$ amperes cm^{-2} [Grard, 1973]. For the Cruise Science Maneuver by Voyager 1 on day

258 of 1978 (the maneuver used by Barnett [1984] in testing the algorithm for the response function), this must be corrected for the heliocentric distance of the spacecraft, 4.152 AU. At Voyager, the expected photocurrent density from the illuminated part of the collector plate is $j_{photo, AU corr} = 1.7 \times 10^{-10}$ amperes cm^{-2} . Predicted currents as a function of angle, using this current density and values from the table in Appendix E are given in the following table; the loss current is in fA for both isotropic and cosine angular distributions. The illuminated area is corrected for the grid transparency.

I_{DC} Predicted for CRSMVR 1978-258			
SCET	$\theta_{D, sun}$	$I_{loss, iso}$ (10^5 fA)	$I_{loss, cos}$ (10^5 fA)
0135:37.276	53.2°	5.20	3.37
0137:13.276	46.0°	8.35	4.85
0138:49.276	43.3°	9.20	5.19
0140:25.276	45.8°	8.40	4.88
0142:01.276	52.9°	5.36	3.45
0143:37.276	63.0°	0.055	0.047

Note that the angles used are slightly different than those quoted above (pointing accuracy is no better than -0.02° in any case); the difference comes from a somewhat crude linear interpolation of the angles which are used in the table immediately above; the "better" values used in the table previously were not available when the predictive calculations were done.

All of the predicted currents are larger than those actually measured; however, there is an additional effect which lowers the calculated predicted current. Sunlight on the suppressor grid will also produce photoelectrons; some of these (one can estimate roughly half) will be accelerated toward the collector plate while the rest will be accelerated in the direction of the buckout grid and eventually lost to the sides of the cup (more details of where secondaries go after they are produced is discussed below). The grid wires are woven tungsten mesh. The expected photoelectron saturation current for tungsten at 1 AU is bracketed by [Whipple, 1981] $2.1 \times 10^{-9} A cm^{-2} < j_{photo, W} < 8.1 \times 10^{-9} A cm^{-2}$. Correcting for the distance of the spacecraft from the sun yields $1.2 \times 10^{-10} A cm^{-2} < j_{photo, W corr} < 4.7 \times 10^{-10} A cm^{-2}$. To have reached the suppressor grid, the light must pass through 6 grids, and to reach the collector plate from the suppressor grid another grid must be passed (which is at ground potential). The associated transparency can be estimated as $(1 - 1/[42 \cos 43.3])^7 \times (1 - \frac{1}{42})^7 = 0.6693$. The area of suppressor grid illuminated with sunlight is given by the overlap area of the aperture and the guard rings multiplied by $1 - (1 - 1/[42 \cos 43.3]) \times (1 - \frac{1}{42}) = 0.0558$. The overlap area is $46.0 cm^2$; hence, the area for emission is $2.56 cm^2$. Multiplying by the transparency yields an effective area of $1.72 cm^2$, which is smaller than but not negligible compared to the effective area for photoelectron loss.

If we take half of the average current density suggested for

tungsten and combine it with this effective area, we obtain a negative current of 2.5×10^5 fA.

From the table above, at 43.3° , the total predicted current is 6.5×10^5 fA using the numbers for isotropic emission and 2.5×10^5 fA assuming the emission follows a cosine law. Given the uncertainty in the photoemission properties of the grid wires as well as the uncertainty in the fraction of photoelectrons emitted by the suppressor grid that will travel toward the collector, the predicted current (especially for the cosine distribution) is in excellent agreement with the maximum measured positive current of 3.25×10^5 fA during the Cruise Science Maneuver in question.

We note that the DC return current should be negative in the reversed suppressor configuration due to the vastly increased suppressor efficiency. Unfortunately, no cruise full yaw turns were performed in the DC return mode with the suppressor position reversed; hence, this prediction cannot be verified.

OTHER SOURCES OF PHOTO- AND SECONDARY ELECTRON CURRENTS

Electrical Configuration of the Side Sensor

Figure 53 is a scaled working drawing of the D cup showing the placement and support structures for the various grids. A comparably detailed drawing of one of the main sensor cups can be found in Barnett [1984] and in Barnett and Olbert [1986]. A less detailed drawing of the side sensor, in similar format, can be found in Barnett [1984]. The original version of that drawing is included as Figure 54. There are some differences in the dimensions which should be noted; they are probably too small to have any effect on any analysis done to date or contemplated for the future using the algorithm developed by Barnett [1984].

Although the dimensions in Figure 53 are quoted to the nearest thousandth of an inch (inches because those are the units in which the original mechanical specifications were made), the quoted uncertainties on all of the machine drawings for the various pieces of the assembly are typically $\pm 0.002"$, if not larger. In labeling Figure 53, the intergrid spacings were computed from the nominal dimensions on the final machine drawings (including all of the Engineering Change Orders - ECOs) from the top surface of one grid to the top of the next (or to the top of the collector plate); the reference line is the top surface of the aperture grid. An expanded detail in the lower left corner illustrates the assembly of the 1 mil tungsten mesh (woven like nylon hose) to the grid support rings. There is a nominal 0.009" space between the top surface of the outer support ring and the top surface of the grid wires. This spacing has been included in calculating the between the grids and the top of the collector plate; it was not included in the dimensions on Figure 54. The mesh is stretched over each inner support ring and then secured with the outer ring (press fit). Excess mesh was then trimmed away at the bottom surface of both rings which were positioned to be flush. The nominal size of the openings in the mesh is $0.042" \times 0.042"$. Variations from this are small and are documented in the appropriate engineering notebooks which record details of the grid assemblies.

The thickness of the insulating spacers which electrically

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isolate the bottom four grids were not specified exactly, rather, a range was given; to compute the spacing, the relative spacing of the centers of the holes for the anchor screws was used. These values were generally consistent with those inferred from the thicknesses of the grid support rings and the insulators.

The intergrid spacings are listed in the table at the lower right in inches. The computed values are in the column labeled nominal. The column labeled Flight 1 (i.e., SN002) are values measured after assembly of the cup using a microscope. The grid wires were brought into focus and the spacings computed. Most of the dimensions are fairly close and give a better idea of the range of error involved. The measured dimension F is almost certainly in error; not only does it differ from the computed value by 0.0049" (a lot), but also the difference between F and G is 0.0120", which is smaller than the specified machine thickness of the outer support ring for the second suppressor grid.

The intergrid spacings shown on Figures 53 and 54 are consistent to better than 0.002" for five of the spacings and not as consistent on the other three. The spacing E - D on Figure 53 (based on the screw hole spacing) is 0.159" as compared to 0.164" on Figure 54. This difference of 0.005" is annoying and probably small due to an error but follows directly from the dimensions to the anchor holes as given on the machine drawing for the lower housing. The spacing F - E is probably correct on Figure 53 and too large by 0.010" on Figure 54 (from including too much thickness for the shield ring). Finally, the spacing from the second suppressor grid and the top of the collector plate is 0.015" larger on Figure 54 than on Figure 53. I have triple and quadruple checked the distance from the aperture grid to the top of the collector plate; I believe that 2.338" is correct as shown on Figure 53. The collector plate thickness is 0.020" so this does not seem to be the source of the problem. The standoffs which separate the lower housing and collector plate come in two sizes 0.250" and 0.235". There are two of each; the shorter ones also support solder lugs which come between them and the collector plate (these are used to connect the wires to the collector plate to make the electrical connection from the plate to the input amplifiers). If the shorter length were assumed for all of the standoffs, the grid to collector spacing would be larger by 0.015"; this is the likely source of the error on Figure 54.

This latter discrepancy is probably the most important, as it would lead to more secondary electrons escaping from the collector plate than were found in the calculations discussed above. In other words, the suppressor is probably slightly more efficient than the numerical calculations done to date imply. This difference is probably not great enough to justify a recalculation of the tables for A_{loss} however.

Overall, the aperture grid - to - collector plate spacing may be in error by up to 0.030" in the algorithms of *Barnett* [1984]. This maximum error is only 1.3% and certainly smaller than other uncertainties in the algorithm.

Characteristics of the Buckout Grid

The so-called "buckout" grid was included in the instrument design to fine tune the instrument to depress the electrical noise level. The effect of the buckout potential was not included in

the algorithms of *Barnett* [1984] and *Barnett and Olbert* [1986]. Given the very small potentials involved and other uncertainties, such treatment is easily justified. However, the buckout potential may be important in understanding one of the features in the "photospectrum", and is not documented elsewhere in an easily accessible way. For reference then, we discuss it here.

In the real instrument there is a certain amount of capacitive coupling between the modulator grid and collector plate, i.e., some field lines from the modulator grid "leak" through the grounded grids to the collector plate. As a result, the changing modulator voltage can produce a spurious current at the collector. The buckout grid is "tuned" to cancel this effect. The voltage applied to the buckout comes from the secondary winding of a transformer in the AC portion of the circuit for the modulator; hence, the buckout voltage is proportional to the AC part of the modulator voltage. The waveform is quasi-square and out of phase with the square wave voltage on the modulator grids. There are separate adjustments for the buckout potential for the main sensor and for the side sensor. The first failure (in 1978) of the PLS instrument on Voyager 1 occurred in the buckout transformer for the main sensor, effectively degrading the sensitivity by a large amount which varied in time (the failure was "repaired" by thermally cycling the instrument, presumably cold soldering a connection which had come loose).

After assembly, the voltage to the buckout grids was trimmed to minimize the modulator to collector feedthrough. For the 16th channel of the L mode the buckout signal was measured to be 5 volts peak-to-peak for the main sensor and 2 volts peak-to-peak for the side sensor for SN001, the PTM or "Proof Test Model" which was flown on Voyager 2 (H.S. Bridge, private communication, July 14, 1987). These values can be scaled by the modulator voltage (AC component) to the other channels of the L mode and to the other operating modes (E1, E2, and M) as well.

It should be noted somewhere that SN003 was to be flown on Voyager 2 but was replaced with SN001 shortly before launch (the substitution was made June 17, 1977 at ETR, i.e., the Eastern Test Range). Hence, SN003 was not flown on either spacecraft and is the "flight spare" in the group's possession at M.I.T.

A calculation of the capacitive coupling based upon planar grids rather than a mesh (and invoking other assumptions and approximations which are reasonable) is included as Appendix G. The solution follows the treatment presented on pp. 1235-7 of *Morse and Feshbach* [1953].

MEASURED CURRENTS IN THE PRESENCE OF SUNLIGHT

Angular Dependence

If the angle between the D cup normal and the direction to the sun decrease to less than a critical angle when a negative potential is present on the negative modulator grid (refer to Figure 53), large modulated currents are measured at the collector plate in the E1 and E2 plasma modes. The spectra have a peculiar character in that some of the channels register threshold, i.e., 0 DN, regardless of the magnitude of the currents in the other channels.

During 1977 and 1978 there were extended periods of time

during which sunlight entered the D cup at a fairly large angle, and these currents were measured in the electron modes for ~100 days at both spacecraft during each year. The effect turned on and off suddenly in 1977 due to spacecraft rolls through relatively small angles; the cutoff occurred when both Voyagers were reoriented to acquire the DSN stations with the spacecraft high gain antenna (HGA). The turn on and turn off of the effect occurred due to very gradual changes in the D cup sun angle. As the spacecraft HGA stays pointed at the Earth, the angular separation of the sun and Earth on the sky change as the Earth orbits the sun; the amplitude of this variation decreases as the spacecraft recede from the Earth. In 1978 the photoelectron signal changed between the off and on states as the angle between the side sensor normal and the sun decreased from 78.5° to 77.5°. As the angle again increased through this range the effect shut off. This behavior was seen on both spacecraft, and is consistent with the range of angles over which the photo-induced currents have been seen during the Cruise Science Maneuvers and special yaw maneuvers which have taken place as part of planetary encounter operations. It should also be noted that during 1978 while the effect was "on" the sun-D cup angle never decreased to less than 74°. In 1979, the minimum angle for the Voyager 2 spacecraft was 78.7° and no effect was seen; the minimum angle for Voyager 1 during 1979 was larger. As both spacecraft have receded from the sun and the angular separation of the Earth and sun have decreased, the corresponding minimum angles have increased; the effect has not been observed again during cruise (all angles quoted are accurate to better than 0.5° and are probably accurate to 0.2° as found from observations of the steady solar wind during cruise maneuvers, H.S. Bridge, private communication, 1987). More details and documented evidence concerning the value of the critical angle can be found in Voyager Memorandum #156.

Character of DC Return Spectra

The DC return mode of the spacecraft has been referred to previously, and must be discussed again because they provide an important clue to the production of the observed modulated current. Figures 55 and 56 show DC return spectra from the cruise phase for Voyager 1 and Voyager 2, respectively. During this phase of the mission sunlight was entering the D cup at less than the critical angle referred to previously. Both figures are a generalized version of the usual display of (the logarithm of) the current versus channel number (~logarithmic in energy per charge). The ordinate here is scaled to the logarithm of the magnitude of the measured current. As the DC return currents can be positive or negative, regardless of the operating mode (i.e., the potential on the modulator grids), the plot format has been generalized to take into account both signs of the current. The abscissa is a similar generalization of the channel number. The basic unit is one channel width in the M mode. The width of an L or E2 channel is 8 basic units and the width of an E1 channel is 2 basic units (one E2 channel is spanned by four E1 channel widths where the two overlap in coverage).

The "generalized data number" 1 through 8 corresponds to channel 16 of the E2 mode, 9 through 16 to channel 15 and so on, with decreasing magnitude of negative modulator potential.

Data numbers 121 through 128 correspond to channel 1 of the E2 mode and numbers 127 and 128 correspond to channel 1 of the E1 mode; the "lower edge" of data number 1 is (a nominal) -5950 volts and the "upper edge" of data number 128 is -10 volts. A 16 unit gap is included to represent the gap in coverage from -10 V to +10 V. Data number 145 then corresponds to channel 1 of the M mode (positive modulator potentials), and numbers 145 through 152 correspond to channel 1 of the L mode. Channel 128 of the M mode corresponds to data number 272 and channel 16 of the L mode corresponds to data numbers 265 through 272. The "upper edge" of data number 272 corresponds to +5950 volts.

The conversion between channel number and voltage is discussed in *Bridge et al.* [1977]; for the sake of completeness, we give it here. Let n be the channel number, which can take on values of 1 to 16 for the E1, E2, and L modes and 1 to 128 for the M mode. Let M be an integer with values of 8 for E2 and L modes, 32 for E1 and 64 for M. Then the potential ϕ_n at the lower edge ("bottom") of channel n , which is equal to the voltage at the upper edge ("top") of channel $n + 1$ (the upper edge potentials follow from considering "channel" 129 for the M mode and 17 for the other modes), is given by

$$\phi_n = 60 \cdot 10^{n/M} - 50 \quad (14)$$

where ϕ_n is in volts.

In Figures 55 and 56, data from the E1, E2, and L modes are plotted; the times of the spectra are indicated across the bottom (the title "NEPTUNE MAGNETOSPHERE" is, of course, erroneous, and a glitch left over from rapidly converting some software to make these plots). Data from the M mode is not shown on these particular plots. The two traces for positive modulator potential are from the A and D cups, the D cup trace being at the positive threshold value. To plot the data as current, the conversion used is that of Figure 1 and Table 1. No temperature correction was made because it is not generally available.

In the DC return mode, the PLS instrument works similarly to a Langmuir plasma probe but only in a superficial way. First because the aperture grid is grounded, the modulator potential can have no direct effect on the surrounding plasma; it can only effect plasma which drifts into the aperture. The exposed aperture grid is always at the spacecraft potential, so there is no way of using these measurements to directly infer the spacecraft potential by adjusting the modulator potential until zero current is measured. At large positive modulator potential, the positive ions should all be excluded, leaving a saturated negative current due to the electrons. At large negative potentials, all electrons should be excluded and a positive saturation current should be measured. This behavior does not usually occur in the DC return measurements although there are exceptions.

For positive modulator potentials, the current saturates at a positive current which is due to the suppressor inefficiency (discussed previously). At lower positive modulator potentials, higher currents are measured as the solar wind is excluded less and less from the collector plate. For the times considered, the solar wind is more obvious on Figure 56 than on Figure 55 even though it is present in both. From the discussion in the previous paragraph, this curve should have started at a large

negative value, increasing toward zero as the positive solar wind is included with decreasing potential. The curve is shifted up due to the suppressor potential. In the solar wind, most of the negative current reaching the spacecraft is due to electrons with energies substantially less than the 95.2 volts (negative) on the suppressor; hence, in this case the suppressor acts as a rectifier allowing no negative current to reach the collector. There are a few cases, in the magnetospheres of Jupiter and Saturn when DC return currents were measured, that the electrons carrying most of the current through the aperture had energies in excess of 95 volts; in these cases, the expected behavior does occur; the total current to the collector plate is negative at large positive modulator potentials.

For negative modulator potentials the expected behavior again does not occur. In this case, an increasing negative modulator potential should exclude more and more electrons while not affecting the ion current to the collector. At large negative potentials, all electrons should be excluded and the current measured should just be the positive saturation current due to the positive ions. In figures 55 and 56, increasing negative current is measured with increasing negative modulator voltage for the first channel of the E1 mode (data numbers 128 and 127) and the first 9 channels (data numbers 128 through 56) of the E2 mode. Due the way that currents are synchronously detected in the normal plasma mode [Bridge *et al.*, 1977], the currents in the first 9 channels of a regular plasma measurement in the E2 mode (and the first channel of E1) will not be detected because the current is out of phase with the detector; a level of 0 DN, i.e., threshold, will be entered into the telemetry stream. The modulator potential at the upper edge of channel 9 is -750 volts. This corresponds to an energy close to the maximum in the secondary emission yield curve for gold, an important clue to the origin of this effect. At higher negative potentials, the negative current is decreasing in magnitude, but is still large and negative at -5950 volts, a potential sufficiently large to easily exclude all ambient electrons.

The switch in suppressor potential between -95.2 volts in E2 and -8.05 volts in E1 introduces a subtle change. The two traces from E1 and E2 are different just below -95 volts (data number less than 103), although they are approximately continuous at the "top" of the E1 mode. Another effect is present also in that channel 3 of E2 (data numbers 111 to 104) corresponds to nominal potentials from -56.7 to -92.3 volts. However, electrons in this energy range cannot pass the -95.2 volt potential barrier of the suppressor grid, so a current with the modulator at this channel is also a mystery. These changes imply that both the modulator and suppressor potentials determine the current measured at the collector plate.

The position of the suppressor potential also affects the currents. For both Voyager 1 and Voyager 2 there are sets of DC return spectra acquired within two hours of those spectra shown in Figures 55 and 56. Figures 57 and 58 show DC return spectra for Voyagers 1 and 2, respectively, in the reversed suppressor configuration. In both cases, there are qualitative changes in the shapes of the curves and the current is larger in magnitude by roughly 50% in the reversed configuration. This behavior suggests that in the normal configuration, the suppressor excludes more current from reaching the collector

plate.

In Figures 59 through 69 are DC return scans from the Voyager 1 encounters with Jupiter and Saturn. They illustrate (sometimes) the "correct" behavior of the spectra and also some of the difficulties of interpretation. Figure 59 is from the middle magnetosphere of Jupiter. Photoelectron current dominates the A cup signal. E2 and D are continuous (both use the same suppressor voltage); note that E2 exhibits an increasing (positive) current with decreasing (negative) potential in the lowest 4 channels. This out of phase behavior is similar to that produced by photoelectrons and is, presumably, due to secondaries produced by hot energetic electrons in the ambient medium. The side sensor was not illuminated with solar UV at this time (UV reflected from Jupiter might be able to enter the cup - I haven't checked the geometry - but is probably of too low an intensity to have an effect). Note that the transition through zero net current occurs in the E1 scan. That it does not occur at zero modulator potential is not surprising; the spacecraft is not illuminated uniformly with the positive ion and electron fluxes, and this will be manifested in the zero current potential. The "crossover" is in no way related to the floating potential of the spacecraft with respect to the plasma due to the grounded aperture grid.

Figures 60 through 64 contain data from the warm Io torus. Effects of photocurrent loss in the A cup, hot electrons, and the change in the ram direction of the positive ions are all present, as well as what appears to be the effect of rapid time variations resulting in time aliasing of the A cup data in Figure 61.

Figure 65 is illustrative of (but not the best example of) data from the cold torus, and Figure 66 is from the torus outbound just prior to the encounter with the Io flux tube. Figure 67 is the from the period of solar occultation; at large positive modulator potentials the A and D cups track each other well as the shadow of the planet has cut off the photoelectron production in the A cup. With both the A and D cups looking away from the positive ion flow direction, the positive ion flux reaching the spacecraft is poorly sampled. As a result the transition through zero current occurs at a relatively large negative modulator potential (the entire trace should be shifted up) and the A and D cup spectra are relatively flat (neither cup is pointed in the correct direction to sample ions which a positive modulator potential would exclude). Figure 68 shows the first set of spectra back in sunlight; the A cup is still low, presumably due to a large electron flux.

Finally, Figure 69 is one of the more interesting ones from the Saturn encounter. It is from the outbound crossing of the Dione - Tethys plasma torus. The positive potential traces appear to have the wrong sign for the current; at least that would make more sense than the data as displayed. The effect of the suppressor voltage in excluding electrons is illustrated nicely by the E1 and E2 data in this case.

In principle, it should be possible to use plasma parameter determinations from the normal plasma data in conjunction with the DC return spectra along with the condition of zero current at zero modulator potential (equivalent to modulator off DC measurements, of which we have none in the magnetospheres) to estimate the net current to the spacecraft due to the (subsonic) electrons and ions with energies per charge above

5950 volts. In practice this would be difficult because the electron plasma and DC measurements would have to be corrected for contamination by secondaries within the housing itself. More troublesome than that is the fact that the secondary electron emission characteristics of the materials from which the spacecraft is made are not really known (discussed above in the section on photoelectron yields).

ELECTRIC FIELDS WITHIN THE SIDE SENSOR HOUSING

For the purpose of calculating the instrument response to a variety of plasma conditions, *Barnett* [1984] and *Barnett* and *Olbert* [1986] make the simplifying assumption of uniform electric fields between the various grid planes. For most purposes this is adequate. Further refinements, such as taking into account the nonuniformity of the field in the immediate vicinity of the grid wires, effectively makes the problem enormously more complicated, if not impossible due to the small differences between the sensors as designed and as actually configured once assembled. An example (the subject of grid spacing) has been mentioned above. There are two examples where the effects of the field nonuniformities may play important roles in the effects of photoelectrons and secondary electrons within the instrument housing. We can also give some quantitative estimates of these nonuniformities, if we make some approximations. The regions in question are in the vicinity of the modulator grid support ring and in the vicinity of the suppressor grids.

Fringing Electric Field Near the Negative Modulator Grid Support

In light of the evidence presented, the currents produced when the PLS side sensor is appropriately illuminated with sunlight must be due to photoelectrons produced on the inner surface of the inner support ring of the negative high voltage modulator grid. Referring to Figure 53, it does not appear possible for such electrons to reach the collector directly due to the presence of the shield ring. A more important objection to a direct collection of these electrons is the fact that all electrons produced at this location will be "born" at the modulator potential; photoelectrons are cold, with an average energy of less than -1 eV, small compared to the other potentials which are present. To assess the possibility of a direct contribution to the current, it is necessary to consider the electric field configuration in the vicinity of the ring.

The actual boundary conditions for the appropriate Dirichlet problem are rather complicated even though there is cylindrical symmetry. To simplify the problem so that it is more easily treated numerically, we can replace the true boundary value problem with a two-dimensional analogue. If the scale length of changes in the potential is small compared to the support ring radius, this approximation should be adequate for our purposes. Figure 70 shows the boundary conditions for the two-dimensional problem. The electrostatic potential is sought for the indicated surface at some potential V_{mod} ; all other surfaces are at ground potential. Equipotentials were calculated numerically and are displayed in Figure 71, and electric field

lines in the near vicinity of the support are displayed in Figure 72 (from a Laplacian problem solver available on Project Athena, C. K. Clark, private communication, June, 12, 1987). The modeling used a fairly coarse grid spacing but does indicate that the "fringing" effect around the support rings dies out after a displacement toward the center of the cup equal to about twice the width of the combined inner and outer ring supports. This is, also roughly, half of the distance from the inner surface of the inner ring to the inner edge of the shield ring.

An approximate solution to the problem is available in analytic form using conformal mapping techniques. This approximation includes only the inner wall of the support ring with their surface facing the shield ring extended to infinity. The appropriate map (inverted) is from *Kober* [1957] and is shown in Figure 73.

A detailed calculation of electron trajectories from the surface of the support to the plane of the shield ring has not been carried out; however, it appears unlikely that the fringe field can impart enough of a "kick" to the electrons to enable them to clear the shield ring. A proper calculation would need to take into account the drift space between the various ground grids and buckout grid. The intergrid spacing is small enough and the modulator frequency low enough that the problem can be treated as a static one with photoelectrons first produced at the upper potential and then at the lower potential for a given modulator step.

The problem is simplified somewhat by the low energy of the photoelectrons. As the energy the electrons gain from the modulator potential is large compared to the energy with which they are "born" and the buckout potential is a small fraction of the modulator potential, the trajectories of the photoelectrons are independent of the modulator potential. This statement is true only above the ground grid above the first suppressor grid in the normal suppressor configuration. As discussed immediately below, the suppressor potential, which is independent of the modulator potential, produces a nonuniform field in this region. The effect of this constant field will tend to deflect toward the cup wall the electrons coming from the modulator grid. The deflection will then determine where on the shield ring the electrons impact; the deflection should decrease with increasing modulator potential.

Further Work on the Fringing Problem

After the initial assessment of the "fringing field" problem discussed in the section immediately above, it became obvious that the question of whether electrons produced on the relatively large surface area of the modulator support ring can indeed reach the collector plate. As of January, 1988, an experimental answer based on the characteristics of the Flight Spare PLS instrument is still unavailable. In December, 1987 an extensive set of calculations was undertaken (by G. S. Gordon, Jr.) to find a theoretical answer to this question. Details and results of this calculation are outlined in this section (note that the figures referred to herein are out of numerical order with some of those referred to in following sections).

The problem is solved in a two-dimensional approximation using the map from *Korber* [1957] depicted in Figure 73 (this mapping function is also given in problem 10.21 on p. 1315 of

Morse and Feshbach [1953]. The appropriate Schwarz-Christoffel transformation is specified by (note that the numbering of the equations is out of sequence)

$$\frac{dz}{dw} = \frac{k\sqrt{w-1}}{\pi w\sqrt{w-c}} \quad (22)$$

with $k \equiv hc^{-1/2}$ and $c > 1$, $k > 0$. The solution is

$$z(w) = \frac{k}{\pi} \cosh^{-1} \left[\frac{2w-c-1}{c-1} \right] - \frac{k}{\pi} \frac{1}{\sqrt{c}} \cosh^{-1} \left[\frac{[c+1]w-2c}{[c-1]w} \right] \quad (23)$$

In this problem $k = 0.452$ inches, $h = 0.312$ inches, and $c = 2.0988$; the dimensions again correspond to the nominal values given in Figures 53 and 75. Details of the computer routines used to make the plots discussed immediately below and to obtain $w(z)$ from eqn. (23) can be found in Appendix F.

Contour maps of $\text{Re}[z(w)]$ are shown in Figures 78 through 81 for different regions with contour lines at 0.1 and 0.01 levels. Corresponding maps of $\text{Im}[z(w)]$ are shown in Figures 82 through 85. The inverse mapping $w(z)$ was found using a variation on the Newton-Rapson technique (see Appendix F and the appropriate source listings for further details). Contour plots of $\text{Re}[w(z)]$ and $\text{Im}[w(z)]$ are shown in Figures 86 and 87, respectively. The contour levels are powers of 2 in these two figures. In Figure 86, heavy lines indicate the contour levels of -1, 0, and +1; heavy lines in Figure 87 show the contours at 0 (along the periphery) and +1. Note that the rectangular region in the upper left hand corner indicates the modulator grid support. Dimensions are given in inches in these figures with the 0.0 along the vertical scale located at the ground grid just below the negative modulator grid (cf. Figure 53).

Given the mapping function, Laplace's equation can be solved in the w plane and the solution mapped into the z plane. From p. 1245 of Morse and Feshbach [1953], we choose the complex potential

$$F \equiv \psi + i\chi = \frac{V}{i\pi} \ln w \quad (24)$$

which gives zero potential on the positive real w axis and potential V on the negative real w axis. Hence,

$$w(F) = e^{i\pi F/V} \quad (25)$$

and contours of constant $\text{Re} F = \psi$ are lines of constant potential which can be mapped to the z plane. These are shown in Figure 88. Contours of constant $\text{Im} F = \chi$ give the electric field lines; these are shown in Figure 89.

Given the electrostatic potential of Figure 88, we assume photo- or secondary electrons are "born" on the inner edge of the modulator support ring. For a given set of initial conditions, the trajectories of these electrons can then be integrated to the plane containing the shield ring to see what fraction pass the ring and can continue to the collector plate (this, of course, assumes that the electron energy is greater than that expended in climbing the potential barrier of the suppressor grid. To make a set of representative calculations, we have assumed that the

suppressor potential is zero (representative of the reversed suppressor configuration) and that the electrons are emitted normal to the surface. Figures 90 and 91 show the resulting trajectories for -10 volts on the modulator grid and initial electron energies of 0 eV and 2 eV, respectively. Figures 92 and 93 show trajectories for modulator potentials of -6000 volts and the same two initial electron energies.

On Figures 90 through 93, the inner edge of the support ring is in the upper left corner. Small tic marks on the y axis locate the two ground grids and buckout grid located at dimensions C, D, and E on Figure 53. For the purposes of this calculation, the buckout grid was also assumed to be at ground potential. As the electrons have been accelerated through the modulator potential before reaching it, this potential should produce a negligible effect on the trajectories. The edge of the shield ring is indicated by the rectangle on the lower left. Again all dimensions are in inches. The information of the previous figures is summarized in Figure 94. The equipotential contours in the region between the negative modulator grid and the first grounded grid are shown at the top; the trajectories shown in Figures 90 through 93 are shown below with the physical region covered to the same scale.

The immediate and obvious conclusion to be drawn from the figures is that the electrons get enough of a sideways "kick" to make it past the shield ring. Therefore, such electrons will reach the collector plate and contribute a negative current. This current is a constant, i.e., has no modulated component. To attempt to determine the origin of the modulated component detected in the normal plasma mode, we must now consider the effects of the suppressor potential.

Electric Fields in the Space Above the Suppressor Grid

In both the reversed suppressor configuration and in the normal suppressor configuration, the field line configuration within the cup is somewhat complicated due to the details of the cup design. In the usual analysis algorithms, the electric field lines are all assumed to be parallel with the symmetry axis; this approximation is not necessarily as good in dealing with the effect of electrons produced on the modulator support ring. In the reversed suppressor configuration, the previously computed suppressor efficiencies will be modified by the fact that edge of the collector does not extend as far as the edge of the second suppressor grid itself (see Figure 53); there are modifications in the vicinity of the collector plate edge because, past the edge, the suppressor potential must drop across a greater distance, i.e., the distance to the bottom of the cup housing which is also at ground potential. Between the second suppressor grid and the first suppressor grid (clamped to ground in the reversed suppressor configuration) the field lines should indeed be straight (ignoring all of the incalculable second order effects present in the real cup). It is important to note that the (approximate) plane occupied by the shield ring and the first suppressor grid is at ground potential in this case.

In the normal suppressor configuration, the second suppressor grid is held at ground potential, and the field lines between the second suppressor and first suppressor grid are straight, to first order. A complication in the field structure now arises in the space between the plane occupied by the first suppressor and

shield ring on the one hand and the ground grid which separates the first suppressor and buckout grids on the other.

The space in question can be modeled as a circular cylinder whose sides and one end are at a potential of zero and whose other end is at a finite potential out to some radius a (the hole in the shield ring) and held to zero potential from radius a out to the edge of the cylinder at radius b (the space above the shield ring). The configuration exhibits sufficient symmetry that the potential can be written explicitly as a Fourier-Bessel series. Choose $z = 0$ as the plane of the ground grid just below the buckout grid, and let positive z be in the direction toward the collector plate; the boundary condition of $\Phi = 0$ at $z = 0$ is satisfied by taking the potential to be proportional to $\sinh kz$. The combination of cylindrical symmetry and finite potential at $r = 0$ imposes a radial dependence of $J_0(kr)$. The boundary condition $\Phi = 0$ at $r = b$ is satisfied by taking $k = x_{0,n}/b$ where $x_{0,n}$ is the n th zero of the Bessel function of order zero. Let the spacing between the plane of the ground grid and that of the shield ring be denoted by L . Again, we ignore the 0.024" difference between the top surface of the shield ring (gold plate on a copper-clad piece of epoxy glass) and the top surface of the first suppressor grid. Then using the expansion

$$\Phi(r, z) = \sum_{n=1}^{\infty} A_n J_0(k_n r) \sinh k_n z \quad (15)$$

where $k_n = x_{0,n}/b$ and applying the boundary condition

$$\Phi(r, L) = V \text{ for } 0 < r < a \quad (16)$$

and zero otherwise, we can find A_n . After some algebra

$$A_n = 2V \frac{a}{b} \frac{\operatorname{csch} k_n L}{x_{0,n}} \frac{J_1(k_n a)}{J_1(x_{0,n})^2} \quad (17)$$

The series does not converge very rapidly (for $n = 1$ to 4, A_n is +10.7, -0.53, -1.0, and +0.99, respectively).

The same calculation can be made for a two-dimensional geometry, i.e., eqn. (15) is now replaced by

$$\Phi(r, z) = \sum_{n_{\text{odd}}=1}^{\infty} A_n \cos(k_n r) \sinh k_n z \quad (15a)$$

with $k_n = n\pi/2b$. Applying the boundary condition eqn. (16) for this formulation yields

$$A_n = \frac{4V}{\pi} \frac{\operatorname{csch} k_n L}{n} \sin(k_n a) \quad (17a)$$

which is an equally unenlightening result.

An integral formulation can be found by letting $b \rightarrow \infty$. An analysis of this case yields

$$\Phi(r, z) = V \int_0^{\infty} J_0(kr) J_1(ka) \frac{\sinh kz}{\sinh kL} d(ka) \quad (18)$$

which is more elegant but no more illuminating. This case can also be approximated by a two-dimensional analogue. In this case we obtain

$$\Phi(r, z) = \frac{2V}{\pi} \int_0^{\infty} \frac{\cos kr \sin ka}{k} \frac{\sinh kz}{\sinh kL} dk \quad (19)$$

This integral can be evaluated in terms of simple functions by noting that $\cos kr \sin ka = 1/2(\sin k(x+a) - \sin k(x-a))$ and using 4.114.1 of *Gradshteyn and Ryzhik* [1980], viz.

$$\int_0^{\infty} \frac{\sin \alpha k}{k} \frac{\sinh kz}{\sinh kL} dk = \tan^{-1} \left[\tan \frac{\pi z}{2L} \tanh \frac{\pi \alpha}{2L} \right] \quad (20)$$

A plot of the field lines is shown in Figure 76 (note that the numbering is off, Figures 74 and 75 have not yet been introduced). The fact that the field lines are not really parallel to the symmetry axis of the cup is not included in either the algorithm of *Barnett* [1984] for the side sensor or in the numerical integration scheme PMODEL. Note that the effect on charged particles entering the cup will be to focus ions and defocus electrons. Put differently, the effect is to make the hole in the shield ring larger for ions and smaller for electrons with the effect becoming less important with increasing particle energy.

To better assess the potential configuration, eqns. (15) and (17) were numerically evaluated by G. S. Gordon, Jr. to produce a contour plot of $\Phi(r, z)$. This is shown in Figure 77; note that the figure is inverted with the suppressor grid at the top and the ground plane at the bottom. The dimensions are in inches, and the plot space (0.165 x 2.765) corresponds to the dimensions on Figure 75 (the vertical dimension used in Figure 76 does not include the 0.015 inch thickness of the shield ring). The contours are at 10% intervals, except for those nearest the boundaries, which are at 1% above/below the boundary value. The mesh used is 999 x 999 and the sum of eqn. (15) was terminated at either the 999th term or when the next term gave a further correction of less than 10^{-6} , whichever came first.

At this time, a rigorous, quantitative analysis of the difference between switching between normal and reversed configurations cannot be given. Qualitatively, one might think that the reversed configuration should lead to more electrons in the vicinity of the hole in the shield ring actually passing through the hole. This is consistent with the increased negative current observed in the DC return mode, reversed suppressor configuration, when sunlight is illuminating the negative modulator support ring.

From early in the mission of Voyager 2 on day 243 of 1977 (11 days after launch), there are DC return spectra for both the normal and reversed suppressor configurations. At this time the angle between the sun and the D cup normal was 73.3°, hence, the negative modulator support was illuminated but not the shield ring (and suppressor grid) or collector plate. A plasma measurement from 1977-238:2011, normal suppressor, modulator on, shows the "turn on" in channel 10, i.e., channel 9 is at threshold, as are channels 3, 4, 6-9, 15, and 16. This is in sharp contrast to the turn on location in the PLOMAN 2 spectra (see below). A corresponding DC return measurement on 1977-249:1340 indicates a maximum (negative) current of -7.04×10^6 fA in channels 9 and 10, i.e., a maximum at ~750 volts (negative) on the modulator grid. This is consistent with the turn on in one of the "voids" in the Jovian magnetosphere

(see below). An earlier DC measurement at 1977-243:1856, gave a broad maximum of -6.40×10^6 fA in channels 7 through 11, indicating that the maximum is flat to $\sim 10\%$ (resolution in this current range for the DC currents, cf. Table 1).

About an hour after the DC measurement in the normal configuration, at 1977-243:1954, there is a DC return measurement in the reversed suppressor configuration. Here the maximum current is -9.60×10^6 fA and extends from channel 6 through channel 10. This is an increase of 50% in the current; the fractional increase in other channels is less, ranging down to % for channel 16. The only logical explanation is that increased refraction of secondary electron trajectories in the normal configuration prevents more electrons from reaching the collector. Given that additional refraction of electrons emitted from the modulator support ring should direct them farther toward the center of the cup, this is also consistent with most of the electrons originating on the underside of the modulator grid itself, presumably due to internally reflected photons.

It is interesting to note that the next available plasma measurement in the reversed suppressor configuration, at 1977-242:2332, shows a turn on in channel 8, i.e., at a modulator voltage of 400 volts. This is consistent with the movement downward (in modulator potential) of the broad maximum in the DC return current; it is not simply consistent with the yield curve for any exposed materials in the interior of the cup. We return to this point below in considering the fractional modulation in the presence of sunlight.

A QUALITATIVE EXPLANATION OF THE EFFECT

Illuminated Area of the Support Ring for the Modulator Grid

To quantitatively evaluate the spectra due to photoelectrons, we need to know the illuminate area of the inner surface of the inner ring supporting the negative high voltage modulator grid as a function of the angle of illumination. The geometry is illustrated in Figure 74. Let the inner radius of the ring be a ($= 2.457''$ from Figure 53) and let the height of the ring be h ($= 0.140''$). Assume the ring is tilted at an angle θ with respect to the viewing direction. The illuminated area (in projection) appears as the intersection of two ellipses of semi-major axis a and semi-minor axis $a \cos \theta$ whose centers are displaced by an amount $h \sin \theta$. The geometry is illustrated in Figure 74. Note that the illuminated area is conveniently divided into Regions A and B as indicated in the figure. The point where the lower branch of the upper ellipse $y_1(x)$ coincides with the upper branch of the lower ellipse $y_2(x)$ separates the two regions; its x coordinate is given by $x_0 = \sqrt{a^2 - (h \tan \theta / 2)^2}$.

A straightforward, but tedious, integration gives the projection of the illuminated area A_{illum} . Define the parameter $\beta \equiv h \tan \theta / (2a)$. The illuminated area is then given by

$$A_{illum} = ah \sin \theta \sqrt{1 - \beta^2} + 2a^2 \cos \theta \sin^{-1} \beta \quad (21)$$

For small θ , $A_{illum} \rightarrow 2ah \sin \theta$ as expected.

We have investigated the variation with angle of the modulated part of the current in the E2 spectra acquired during the PLOMAN 2 maneuver within the Jovian magnetosphere. The following table lists the times of the spectra, the angle θ , the illuminated area of the modulator support from equation 21,

and the peak current. For the first two spectra the peak current appeared in channels 10 and 11 (i.e., from 750 to 1373 volts); the peak current was located in channel 11 for the rest of the spectra (1017 to 1373 volts).

E2 Spectra From PLOMAN 2 Maneuver 1979-062			
SCET	θ	A_{illum} cm ⁻²	I_{peak} (10 ⁴ fA)
1825:19.471	75.3°	4.28	1.59
1826:55.471	63.6°	3.97	2.63
1828:31.471	53.4°	3.56	3.15
1830:07.471	46.1°	3.19	3.26
1831:43.471	43.2°	3.04	3.15

The change in illuminated area of the support ring is obviously not the major factor in causing the current to increase as θ decreases; the illuminated area is actually decreasing due to projection effects. If we assume that the photoelectron current varies as the secant of the angle between the incident photons and the normal to the support ring surface, we still cannot account for the factor of two increase in current as the cup is rotated more into the sunlight.

Let α be the angle of incidence of the photons with respect to the normal to the inner surface of the ring. Then

$$\langle \frac{A_{illum}}{\cos \alpha} \rangle = 2ah \left(\frac{\pi}{2} - \sin^{-1} \beta \right) + 4a^2 \cot \theta (1 - \sqrt{1 - \beta^2}) \quad (26)$$

where β is defined as above and $\langle \dots \rangle$ indicates an average over the illuminated angle. In this case we obtain

E2 Spectra From PLOMAN 2 Maneuver 1979-062			
SCET	θ	$\langle \frac{A_{illum}}{\cos \alpha} \rangle$ cm ⁻²	I_{peak} (10 ⁴ fA)
1825:19.471	75.3°	6.73	1.59
1826:55.471	63.6°	6.84	2.63
1828:31.471	53.4°	6.89	3.15
1830:07.471	46.1°	6.91	3.26
1831:43.471	43.2°	6.91	3.15

The averaging over $\cos \alpha$ increases the effective illuminated area by about 50%; dividing A_{illum} by $\sin \theta$ gives a roughly constant value of 4.4 cm⁻². These variations show that even including the angular dependence of the electron yield per photon, the variation cannot be accounted for.

To produce a modulated current, electrons produced at the modulator potential must be involved. A final source for such electrons is the modulator grid itself illuminated by photons reflected from the inside of the cup (E. C. Sittler, Jr, private communication, December, 1987). Photoelectrons produced on the underside of the grid wires will be accelerated toward the collector plate while those produced by direct illumination on

the top will tend to be accelerated toward the aperture grid and leave the cup.

In the review on reflectivity in the ultraviolet by *Koller* [1965], the reflectivity of thin gold film is ~20% for photons of energies between 6 and 10 eV. Such photons form the bulk of the solar spectrum in the energy range for which photoelectron yields are appreciable for many materials [*Grard*, 1973]. Although photoelectron yield versus photon energy is not readily available for tungsten, it is reasonable to assume that ~1/5 of the photons incident on the inner surfaces of the cup will be reflected back to illuminate the negative modulator grid wires. In this case the illuminating flux goes like $\cos \theta$. At normal incidence, the grid wire area is $\pi a^2 [1 - (1 - \frac{1}{42})^2] = 5.76 \text{ cm}^2$, i.e., comparable to the directly illuminated area of the modulator support ring. At angles of incidence of 75.3° and 43.2°, respectively, the areas of the modulator grid wires illuminated by sunlight are 1.46 and 4.20 cm^2 , respectively. These values should be reduced by a factor of 0.2 (the reflectivity coefficient). Adding the values from the table apparently again give too low a modulation with angle.

One final correction is the transparency of the aperture grid, positive modulator grid (grounded), and negative modulator grid to the photons hitting the support ring. The transmission probability can be estimated as

$$T = (1 - \frac{1}{42})^3 (1 - \frac{1}{42} \sec \theta)^3 \quad (27)$$

This effect also yields too small a modulation with angle of incidence: in changing the angle of incidence from 75.3° to 43.2°, respectively, the transparency increases from 0.692 to 0.842 if estimated from eqn. (27).

It is important to note that as the PLOMAN 2 maneuver occurred within the magnetosphere of Jupiter, the positive ions were flowing about at right angles to the spacecraft-sun line [*Sands and McNutt*, 1988]. This is not an important consideration for the plasma mode measurements as such; however, it identifies the problem with attempting to determine the angular modulation of the unmodulated electron current produced by photoelectrons. This component is only available from DC return measurements during a period in which the spacecraft is rotating. Such measurements are made during the Cruise Science Maneuvers mentioned earlier. These maneuvers are made only in the solar wind, so the angular modulation of the photocurrent also includes the positive contribution of the current due to the solar wind at the smaller angles of incidence (<-63° at which the solar wind can reach the collector plate - cf. Figure 53). In addition, there is the positive current which results from photons on the collector plate and escape due to the inefficiency of the suppressor grid, an effect discussed in detail above. We can attempt to disentangle these effects by differencing DC return currents from the L and E2 modes in the same channel acquired at about the same angle (there is some difference in angle due to the finite rotational speed of the spacecraft and the non-simultaneity of the L and E2 measurements).

We again consider the Cruise Science Maneuver on Voyager 1 from day 258 of 1978. If we use the nominal DN to current conversion of Table 1, the currents are smaller than those listed

in the above table in the text. It does appear that the time delay between L and E2 acquisition is too slow compared to the angular change in spacecraft orientation to use this technique to come to a definitive conclusion about the angular variation of the DC photocurrent.

The variations are plotted as a function of angle in Figure 95. The modulated current is fairly consistent with a cosine variation, except for the turnover at angles of incidence of less than ~50°. The DC curve indicates an even larger variation at larger angles, but this could be due to not correctly incorporating the electronics temperature in the DN to current conversion. The obvious conclusion to be drawn is that the internally reflected photons illuminating the underside of the negative modulator grid must play a major role in producing the photoelectrons in the instrument. In light of the lack of information in the literature on the photoelectron yield of tungsten as a function of photon energy, as well as the geometric complexities of internal reflection within the instrument, it is likely that a quantitative model of the photoelectron response could only be derived from extensive laboratory calibrations of the flight spare (under appropriate conditions). If back illumination of the modulator grid is the major source of photoelectrons, then their utility as tracers of secondary electrons produced inside the instrument must also be considered limited.

Production of Intermediate Secondaries

Given the photoelectrons produced at the support ring and/or on the modulator grid itself, we turn to the question of how this can give rise to a modulated current at the collector plate. As the modulator potential increases, the photoelectron current produced will increase somewhat but reaches a saturation value at an applied potential of a few volts. This could explain the initial increase in current with negative modulator potential, but cannot explain the peak at ~750 volts. The location of the peak current in the DC return spectra during the Cruise Science Maneuver on day 258 of 1978 is located in channels 8 and 9. PLOMAN 2 spectra shows a "turn on" of the effect in channel 9, which is consistent with the location of the peak in the DC return spectra. The thresholds of channels 9 and 10 are 550 and 750 volts, respectively, so 750 volts is certainly past the maximum. According to *Kollath* [1956], the peak in the secondary yield curve for gold is 800 volts and for tungsten 650 volts. Hence, the location of the peak in current versus modulator potential is consistent with secondaries produced from a tungsten surface, i.e., from the grid wires, but not from a gold surface, i.e., the plating on the cup surface.

An exception to this occurs on Voyager 2 during its encounter with Jupiter in 1979 on day 190 from ~1150 to ~1155. This period is during the crossing of one of the "voids" identified in the Voyager plasma data [*McNutt et al.*, 1987; *Khurana et al.*, 1987]. During this period, the E2 current is apparently out of phase with the synch detector for all channels through channel 9, i.e., the "turn on" occurs in channel 10 above its threshold of 750 volts. This suggests that at very high electron temperatures, the secondary electrons produced off of the gold plating can produce a significant effect.

Secondary electrons capable of reaching the collector plate

must have an energy in excess of -95 volts to pass the potential barrier established by the suppressor potential (secondary electrons can also be produced on the grounded grid between the suppressor and collector in the normal suppressor mode). This implies that the electrons must originate on either the modulator grid itself (or the support ring) or on the suppressor grid. The fact that sunlight produces a modulated current means that this current must be produced on a surface whose potential varies with respect to the modulator as the modulator voltage is stepped. By elimination, this surface must be the suppressor grid itself. At the peak current, the suppressor is at a potential of $0 - 95 = -650$ volts with respect to the modulator; this, of course, corresponds to the energy of the peak in secondary yield from tungsten.

Most of the secondaries produced at the suppressor grid will be produced on the sunlit, or outward facing, side (along with photoelectrons which constitute another unmodulated component). These will be accelerated by the suppressor potential out of the cup; however, if the modulator voltage is greater than the suppressor voltage (as is the case except for the lowest 3 channels of the E2 mode), these will be reflected back into the cup by the modulator potential. Furthermore, they will have just enough energy to climb over the potential barrier between the suppressor grid wires, which is fractionally smaller than that on the wires themselves. Only those electrons initially emitted nearly parallel to the cup axis will not drift to the sides of the cup and be lost; however, those that do make it through will reach the collector plate. For a given lighting condition, the number of electrons striking the collector will be proportional to the secondary electron yield of tungsten at an energy corresponding to the difference between the modulator and suppressor voltages. Some of the possible electron trajectories and secondary production sites are illustrated qualitatively in Figure 96.

The other case of real interest concerns the production of secondary electrons within the instrument by energetic secondary electrons in the local plasma environment. Again, to produce a modulated signal (which can either add to or subtract from the modulated primary electron current) the modulator potential must be involved. As noted by *Vasyliunas* [1968], a component of secondary flux in phase with the primary flux (and therefore simply adding to it) will be produced at both the suppressor grid (proportional to the yield at energy $E_{primary} - eV_{sup}$) and the grounded grid between the suppressor grid and collector plate (proportional to the yield at energy $E_{primary}$).

More importantly, secondary electrons can be produced at the modulator grid or support ring. In fact, given the relatively large area of the modulator support ring compared to the area of the grid, most of the secondaries presumably would originate on the inner surface of the support structure. Here, of course, the underside of the grid cannot be illuminated by primary electrons as it can by reflected photons. The current so produced will be proportional to the yield at the energy $E_{primary} - eV_{mod}$. The total current so produced is actually given by (cf. eqn. 13)

$$I_{sec} = e \int_{v_m}^{\infty} dv, v, \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} d^2v, f(v) T\delta \left(\frac{1}{2} mv^2 - eV_{mod} \right) \quad (28)$$

This current will flow with an annular cross section (cf. Figure 94), intersect the suppressor with an energy of $E_{primary} - eV_{sup}$ (recall that the secondaries are "born" with energies on the order of 1 eV), and continue to the collector plate with this intermediate population of "daughter" secondaries. The current reaching the collector plate can be modulated due to i) modulation of the primary flux reaching the modulator grid and/or support ring, ii) modulation of the yield at the modulator grid and/or support ring, iii) modulation of the number of electrons getting by the shield ring, and iv) modulation of the yield at the suppressor grid. In regard to mechanism iii), some electrons may be stopped by the shield ring. An assessment of possible modulation due to the angular distribution of electrons emitted from the ring support combined with the potential distribution above the suppressor grid is beyond the scope of this study, however.

Figure 96 also shows possible trajectories of electrons produced by energetic primary electrons. Again, in this case it may be possible to produce a current on the collector plate which follows the yield curve for gold. This is apparently necessary to explain the "turn on" in the E2 plasma data observed in at least one of the "voids" observed by Voyager 2 near Ganymede.

The only source of readily available data on the relative amount of modulation in the secondary electron current for both normal and reversed suppressor configurations comes from early in the mission when both forward and reversed suppressor configurations were used in conjunction with DC return measurements. There are also a few places where both DC return and plasma data are available for the case of large secondary currents produced by energetic electrons. These cases occurred in the Jovian magnetosphere during the Voyager 1 pass. The "clean" data, i.e., those in which the fluxes are high enough to be over the DC threshold and positive ions are not flowing into the D cup, occurred outbound on day 65 of 1979.

First we consider spectra in the solar wind near the earth when the ambient electron population was relatively cold, i.e., no ambient electrons were energetic enough to produce a real signal in the E2 mode. The following table lists measured E2 currents as a function of channel number using the DN to DC return conversion of Table 1. All currents are in units of fA (10^{-15} amperes), and TH indicates a threshold current for the measurement in question. These spectra are plotted in Figures 97 through 100 along with neighboring E1 and L spectra (A and D cups). The format is the same as that used for Figures 55 through 69, with the currents from the plasma measurements plotted as positive for both ions and electrons. These figures also show the appearance of the solar wind in the A cup during the DC return measurements.

Voyager 2 1977				
Suppressor:	Normal		Reversed	
Time:	243:1856	238:2011	243:1954	242:2332
Channel	I_{DC}	I_{PLS}	I_{DC}	I_{PLS}
1	-1.00×10^5 - TH	8.475×10^2	-1.37×10^5	1.740×10^3
2	-1.00×10^5 - TH	9.787×10^2	-1.28×10^5	2.585×10^3
3	-6.20×10^5	1.353×10^2 - TH	-8.00×10^5	1.353×10^2 - TH
4	-3.20×10^6	1.353×10^2 - TH	-4.48×10^6	1.353×10^2 - TH
5	-5.44×10^6	1.082×10^3	-8.32×10^6	1.353×10^2 - TH
6	-5.92×10^6	1.353×10^2 - TH	-9.60×10^6	1.353×10^2 - TH
7	-6.40×10^6	1.353×10^2 - TH	-9.60×10^6	1.353×10^2 - TH
8	-6.40×10^6	1.353×10^2 - TH	-9.60×10^6	7.339×10^4
9	-6.40×10^6	1.353×10^2 - TH	-9.60×10^6	2.239×10^5
10	-6.40×10^6	1.172×10^3	-9.60×10^6	4.278×10^5
11	-6.40×10^6	2.494×10^3	-8.96×10^6	5.705×10^5
12	-5.92×10^6	2.160×10^3	-8.32×10^6	5.504×10^5
13	-5.92×10^6	1.305×10^3	-7.68×10^6	4.278×10^5
14	-5.92×10^6	4.597×10^4	-7.68×10^6	2.986×10^5
15	-5.92×10^6	1.353×10^2 - TH	-7.04×10^6	1.939×10^5
16	-5.44×10^6	1.353×10^2 - TH	-7.04×10^6	1.353×10^2 - TH

It is interesting to note that electrons produced at the modulator cannot reach the collector plate for the lowest 3 channels due to the suppressor potential. The currents measured in those channels could be due to feedthrough from higher energy electrons, but these are not present if "high energy" electrons are simply those photoelectrons ejected from the modulator grid. A constant current in the reversed mode would simply be due to photoelectrons produced at the suppressor grid, but here that grid is not illuminated. At face value there seems to be no way of producing a negative current in these channels; this is one mystery we return to later.

One final thought on this subject: the angle between the normal and the direction to the sun is 73.3° , as stated above. For sunlight not to be fully intercepted by the shield ring and the structure of the cup above it, an angle of less than 70.2° is required. Obviously, sunlight cannot be producing photoelectrons off of the suppressor grid, and these would not be modulated anyway. However, the solar wind is entering the cup at a large angle of incidence, and, as the modulator potential is increased, the protons are refracted more toward the center of the cup. This refraction effect may be just enough to illuminate the suppressor grid, produce secondary electrons via proton bombardment (more of this later), and produce a negative current from the secondaries. The protons themselves would have to miss the collector plate itself for the net current to be positive as the secondary yield is below unity for typical solar wind proton energies. In the corresponding positive ion mode, the DC return current in the side sensor is at positive threshold, while the measurements in the A cup suggest the solar wind current is -10^6 fA. With all of the efficiency factors involved, this mechanism appears to be ruled out, as negative current approaching this in magnitude is measured in the D cup.

The solution to a complicated problem is always the obvious one! Recall from above that the measured suppressor potentials were -95.2 V in the normal mode and -85.9 V in the reversed

mode. For channel 3, the modulator potential is oscillating between (nominal) potentials of 56.7 V and 92.3 V. Hence, we expect that a finite amount of secondary current can reach the collector in the reversed configuration. If the true modulator potential is off by as much as 3%, electrons would be just at the threshold for producing a current. Currents in the first two channels in the reversed configuration are still an embarrassment.

A source of negative current in the third channel of E2 is also present during the Cruise Science Maneuvers (normal suppressor configuration). A spot check of the DC return data shows positive currents in the first three channels of E2 when the solar wind is entering the D cup; channels 4 through 16 have negative currents due to the larger currents produced by photoelectrons. However, while the currents in the first two channels are the same, the current in channel 3 is consistently lower. For example, for Voyager 1 at 1978-258/0139: 8.237 the angle to the sun is 43.2° (the minimum reached). The previous L mode has a DN of 153 in channels 7 (solar wind + suppressor inefficiency + photoelectrons from suppressor grid). The E2 mode has DNs of 154 in channels 1 and 2, DN of 148 in channel 3, and DNs ranging between 0 and 34 (net negative current) in all the other channels. It is curious to note that the DNs in the previous E1 mode, all due to the solar wind plus photoelectrons, range from 165 to 174, i.e., much more positive current when the suppressor potential is lower. Using the nominal values of Table 1, channels 1 and 2 of E2 show currents of 2.75×10^5 fA, while channel 3 has 2.17×10^5 fA, a change of 0.21. Given the relatively large suppressor grid transparency, this cannot be simply accounted for by secondary emission. Further study is required to pin down the source of negative current. Another possibility is leakage due to the grid plane not being an equipotential (A. J. Lazarus, private communication); it is possible that this is the source of the current (from electrons produced on the modulator at 92.3 volts). This mechanism cannot, of course, be the source of the negative current measured in the first two channels in the reversed suppressor configuration.

As noted above, the normal suppressor DC currents are, at most, one third of the current measured in the reversed suppressor mode. The normal plasma measurements are, at most, $\sim 40\%$ of the reversed suppressor plasma measurements, although this percentage is a fairly strong function of channel number.

One can also consider the fractional modulation by taking the ratio of the plasma to DC return currents, keeping in mind the possible uncertainties in the DC currents due to temperature dependence and the quantization of the steps ($\sim 10\%$ as compared to less than 1% for the plasma measurements). These ratios are shown in the following table for those channels not registering only threshold current; for the latter N/A (not available) is indicated.

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Voyager 2 1977		
Suppressor:	Normal	Reversed
Time:	243:1856, 238:2011	243:1954, 242:2332
Channel	$-I_{PLS}/I_{DC}$	$-I_{PLS}/I_{DC}$
1	N/A	0.01270
2	N/A	0.0202
3	N/A	N/A
4	N/A	N/A
5	0.01934	N/A
6	N/A	N/A
7	N/A	N/A
8	N/A	0.00764
9	N/A	0.02332
10	0.01831	0.04456
11	0.03897	0.06367
12	0.03649	0.06615
13	0.02204	0.05570
14	0.00776	0.03888
15	N/A	0.02574
16	N/A	N/A

We estimate that $\Delta\delta \approx 0.1$ across one E2 channel near the peak plasma current, where $\Delta\delta$ is the variation in secondary yield (cf. eqn. (10)). If the yield variation were the only source of modulation for $\delta = 1$, we would obtain

$$I_{DC} \approx I_{inc} <\delta> \quad (29)$$

and

$$I_{PLS} \approx I_{inc} \Delta\delta \left[1 - \left(1 - \frac{1}{42} \right)^2 \right] \quad (30)$$

which yields a modulated fraction $I_{PLS}/I_{DC} \sim 5 \times 10^{-3}$, a smaller value than is actually measured in the spectra considered above. We have assumed that the conditions producing the spectra are constant and that eqn. (10) adequately represents the yield. These are probably not bad assumptions. It is also possible that the DC return currents are larger than assumed above, i.e., that the fractional modulation is smaller than indicated in the above tables. Given that table 1 is for low temperatures and the thermal dependence shown in Figure 9, this is likely to be part of the problem. More detailed calculations of secondary electron trajectories within the cup and/or actual measurements with the flight spare instrument will be required to resolve the apparent discrepancy.

As we have noted, a similar type of analysis is possible in the case that we know photoelectrons are not responsible by using data obtained during the Voyager 1 encounter with Jupiter. Currents and the modulation ratio from an example are listed in the following table (in the normal suppressor configuration).

The fractional modulation is apparently comparable to that obtained when photoelectrons are present. The variation with modulator potential is, of course, different in the two cases, and for both cases time aliasing, and the conversion of DC return DN's to current are possible sources of error. However, it

appears that the resulting E2 spectra are qualitatively consistent.

Voyager 1 1979, Day 65			
Channel Number	DC Return Current (fA) 1122:55.416	Plasma Current (fA) 1121:27.560	Fractional Modulation
1	-1.09×10^5	1.647×10^2 - TH	N/A
2	-1.12×10^5	1.647×10^2 - TH	N/A
3	-1.20×10^5	1.647×10^2 - TH	N/A
4	-1.28×10^5	1.647×10^2 - TH	N/A
5	-1.40×10^5	1.647×10^2 - TH	N/A
6	-1.40×10^5	1.647×10^2 - TH	N/A
7	-1.40×10^5	1.647×10^2 - TH	N/A
8	-1.45×10^5	3.507×10^2	0.0024
9	-1.40×10^5	8.621×10^2	0.0062
10	-1.40×10^5	1.708×10^3	0.0122
11	-1.40×10^5	2.726×10^3	0.0195
12	-1.36×10^5	3.507×10^3	0.0258
13	-1.28×10^5	3.264×10^3	0.0255
14	-1.20×10^5	3.709×10^3	0.0314
15	-1.05×10^5	5.210×10^3	0.0496
16	-1.00×10^5 - TH	5.401×10^3	N/A

We have also examined the E1 spectra at this time. The DC return spectrum at 65/1123:43.416 exhibits a broad maximum from channel 4 through channel 8; the plasma measurement at 65/1122:15.560 shows occasional currents above the 0 DN level which have no organized structure, i.e., they are consistent with noise.

Given that there were no DC return measurements in the the Voyager 2 measurement sequence at Jupiter near the so-called voids, but there is also no indication of random noise in the lower channels, i.e., the lower channels appear to be "clamped" to threshold values, we can only conclude that those spectra are produced by a very hot primary population which produces significant numbers of secondary electrons within the instrument housing.

The E1 Spectra

We have not concentrated on the E1 spectra for because the physics of secondary emission is more complicated for impacting electrons at under 50 eV. In particular, it is difficult to differentiate between secondary electron, backscattered electrons, and reflected primaries at these low energies. It is clear from Figures 55 through 58, 97, and 99 that in the E1 spectra, the current at the collector increases for increasing potential for at least the first two, and sometimes, the first three channels (typically for the reversed suppressor configuration). This behavior covers the range from 10 to ~25 volts. However, from ~25 to ~140 volts, the measured current decreases with increasing modulator potential, i.e., the collected current does not simply follow the expected yield curve as occurs in the E2 mode measurements. This behavior is clear in the PLOMAN 2 spectrum from 1979-62/1832:31.471 as well (angle to the sun 43.7°). In the cruise science maneuvers, the signature is complicated by the solar wind at such small angles: the total current in the E1 spectra are positive in all channels but with variations due to the ambient electrons and photoelectrons also

present. In addition, the secondary yield is expected to be small; it is less than unity for less than 250 eV electrons bombarding tungsten [e.g., *McDaniel*, 1964].

The other fact of interest to note is that on the figures referred to immediately above, the E1 and E2 spectra do correspond. In the normal suppressor configuration, the same current is measured in the fourth channel of E2 and the top four channels of E1. In the reversed configuration, the current measured in E1 is always somewhat larger in magnitude. This variation between the two configurations suggests part of this behavior reflects the inefficiency of the suppressor in the normal configuration.

The decrease in measured current with increasing energy above 25 volts on the modulator must, therefore be related to the suppressor potential, by elimination. One possible way of decreasing the negative current would be by increasing the energy of the electrons liberated as secondaries from the collector plate as the primary energy increases. True secondaries have a common energy distribution independent of the energy of the incident primary. At 2.5 volts, a substantial fraction of secondaries from the collector can pass the suppressor to be absorbed at other grounded surfaces in the cup. The fraction lost is about 8% for the reversed suppressor and 10% for the normal configuration (see Appendix B and Figure 15).

The energy of the secondaries is not a function of primary energy, but the energies of backscattered electrons are ([*Sternglass*, 1954] and references therein). Unfortunately, the literature on secondary and backscattered electrons at energies below 200 eV is limited and probably dated with respect to the measurement techniques employed. It is interesting to note that there are secondary maxima in the energy spectra of secondary electrons which are characteristic of the target material, although this seems to be related to the prior heating of the target [*Hachenberg and Brauer*, 1959]. *Rudberg* [1936] found such secondary maxima for a gold target at ~ 3 and ~ 24 eV. If such maxima are present in the secondaries emitted from the collector plate, then as the modulator potential (at which the photoelectrons are produced) exceeds 24 volts, electrons at this characteristic energy can be emitted; they would immediately be lost as they could not be stopped by the ~ 8 volts on the suppressor grid. If a larger fraction of the secondaries are emitted with this energy as the primary energy increases, this could account for the decrease in negative current at higher energies in the E1 mode. However, this does not appear to be easily reconciled with similar measured currents at similar accelerating potentials in the E2 mode; with a suppressor potential of -95 V, all the higher energy secondaries should be stopped. This change in suppressor efficiency should be reflected in an abrupt increase in collector current magnitude. Such a change is, of course, not present.

A comparison of the E1 and E2 spectra does suggest that whatever mechanism is responsible for electrons to leak past the suppressor to the collector plate in the E2 mode is also responsible for them leaking past the suppressor in the E1 mode. This process must become independent of the suppressor potential once the primary energy has exceeded ~ 90 volts. Again, this could be due to the details of the secondary,

reflected primary, and backscattered primary electrons at the energies where the distinction between these various populations becomes blurred.

A final consideration for interpreting E1 spectra is a problem with the amplitude in the E1 measurements (see section 3.1 of report by R. J. Butler, unpublished manuscript). The effect is present at some level in the first two channels and is due to transients from switching the suppressor potential just prior to the E1 measurements. Calibration curves exist which can be used to remove this problem in the analysis of the electron data.

Secondary Electrons Produced By Positive Ions

A subject not touched upon here, but of potential importance in the analysis of some of the magnetospheric data obtained by the Voyagers, is the production of secondary electrons by positive ions. Production of such electrons at the modulator grid was of concern in the analysis of IMP-2 and OGO 1 and 3 data obtained by M.I.T. Faraday cups in the Earth's magnetosphere [*Vasyliunas*, 1968; *Binsack*, 1967]. *Vasyliunas* [1966] noted that due to the energy dependence of the secondary yield with respect to ion energy, the current produced will be out of phase with respect to the synchronous detector (this effect has also been noted by *Sittler* [1983]). As the yield is an increasing function of proton energy, more negative modulator potentials, should lead to larger yields of electron currents. Evidence that this was indeed occurring came in the form of electron data from OGO 1 in which the telemetered signal was clamped to the instrument zero level, below the noise level [*Binsack*, 1967]. These measurements occurred in the plasmopause where all of the cold, high density protons appeared within a given energy window, exceeding the nominal electron flux in that window by some two orders of magnitude.

The behavior of the measurements, i.e., a "clamping" at the zero DN level, is exactly the phenomenon found in the E2 measurements discussed above. In that case, the electrons have to simply be "hot", i.e., mostly in an energy range over which the secondary yield coefficient exceeds unity.

The yield coefficient for O^+ incident on tungsten exceeds unity around a few keV [*Large*, 1963]. It is almost certainly the case that the 0 DN values in the upper channels of the E2 spectra in the warm Io torus (1979, day 64 for Voyager 1) are produced by this effect, i.e., the positive ions are accelerated to ~ 5 keV by the negative modulator potential, and hit the modulator grid yielding secondary electrons. This current would be out of phase with that due to the primary electron population, and, if of sufficiently large magnitude, can produce the observed effect [see also *Sittler and Strobel*, 1987]. A more complex version of this effect, including yield curve modulation of the daughter secondaries, is almost certainly responsible for the bizarre E2 spectra recorded in the cold Io torus when large fluxes of positive ions could reach the (negative) modulator support ring but not the collector plate itself (due to the geometry of the flow).

Comparison with Other Instrumentation

The problem of secondary electron contamination in plasma experiment observations in space is not limited to modulated

grid Faraday cups. Difficulties associated with secondaries in RPAs due to large positive ion fluxes [Knudsen and Harris, 1973] as well as in electrostatic analyzers due to large electron fluxes [Zwick et al., 1987] have been reported. In both cases, the problem was only recognized when trying to explain unexpected observations. This is also true of the motivation for this report; however, our investigations indicate that the effects of secondaries can be present at other times as well and not be noticeable due to the "masking" effect of expected observations. Such behavior is, in principle, possible in RPAs and electrostatic analyzers as well, especially in exotic environments for which only limited data sets are available. Hence, one is left with the caveat that significant corrections for spurious secondary electrons may be required to characterize the local plasma environment around a spacecraft, but the need to make such corrections may not be obvious in the data.

REMAINING QUESTIONS

Quantitative Modeling

The central question is whether a quantitative model of these secondary emission effects can be made which will allow us to simulate the data to a high degree of accuracy (~1% level). Such simulations are possible with the positive ion data in all four Faraday cups under conditions of negligible charging in the Jovian magnetosphere even when the ions are hot (see, e.g., [Barnett, 1986]. To accomplish this task the cascading or "feedthrough" of higher energy ions into lower energy measurement channels must be effectively taken into account. The feedthrough of electrons into the positive ion mode and of positive ions into the electron mode, both of which have been known of for some time [Vasyliunas, 1971], have been incorporated into the simulation code PMODEL (written by V. M. Vasyliunas, with documentation and corrections by J. W. Belcher). As noted above, PMODEL has been modified (with the efforts of G. S. Gordon, Jr.) to include the effect of suppressor inefficiency in simulating electron spectra. The additional current source provided by secondary electrons created at the modulator grid/support assembly and the suppressor grid have not as yet been included.

The possibility of feedthrough from higher to lower energies was also recognized by Vasyliunas [1971] but was dismissed as a "higher order correction". The latter is certainly the case for measurements of the supersonic solar wind, the task for which the PLS experiment was primarily designed [Bridge et al., 1977], but is a crucial effect to model in interpreting plasma data returned from the magnetospheres of the outer planets. Such a feedthrough effect is also present in electron data but is not modeled in the current analysis scheme (details of the analysis are given by Sittler [1983]). As more superthermal electrons are added this effect becomes more important; it accounts for ~10% corrections to the relatively well-behaved electron data acquired during the Uranus encounter of Voyager 2 (see Voyager Memorandum 136). A recent analysis of the electron data from the Io torus by Sittler and Strobel [1987] showed that ion feedthrough provides a substantial contribution to the high energy electron channels. The calculation was made with the unmodified PMODEL code, i.e., suppressor inefficiency

not taken into account, and was based upon the thermal ions; the feedthrough effect is actually larger as there are significant fluxes of non-Maxwellian ions in this region [Bagenal, 1987].

The other effects of secondaries with which we are concerned have been recognized in a qualitative way for some time as "extraneous effects" characteristic of the modulated-grid Faraday cup scheme [Vasyliunas, 1971]. These effects include the modulated signal produced when sunlight illuminates the interior of the cup, which was not well understood at the time but thought to be related to yield of secondaries produced at the suppressor by photoelectrons produced at the modulator grid; this mechanism appears to be solidly supported by the Voyager data. They also include the out of phase signal resulting from secondaries produced by ion impact on the modulator grid (in the electron mode), and the enhancement of electron current due to secondaries produced at the modulator and suppressor grids in the electron mode. That the latter effect can also produce out of phase signals was not noted or, more likely, not considered, before as a very hot primary electron population is required to produce this effect. Such a situation has been encountered in the magnetospheres of Jupiter and Uranus (see below), and the study of these bizarre plasma conditions provided the impetus for this in depth study.

The modeling problem is also complicated by having no a priori information as to the functional form of the distribution function to be used. The current state of affairs is illustrated in Figure 101. We show E1 and E2 spectra taken in the Jovian magnetosphere at the top. Note the 0 DN levels in channel 1 of E1 and channel 3 of E2. Both of these features, as well as potentially low values of current in channels 2 and 3 of E1 and 4 of E2 are due to out-of-phase signals produced by internal secondary emission due to the electrons present in the non-Maxwellian tail. The second two plots (from the top) show a best simulation from the unmodified PMODEL code. Note that there can be no direct current in the first 3 channels of E2 due to the suppressor potential; the currents there are entirely due to feedthrough from higher energy electrons. Note also that the simulated and measured currents in the first two channels of E2 show a rather good match. This simulation assumed a κ distribution (see, e.g., [Vasyliunas, 1971] and references therein), with $\kappa = 1.5$. The next two rows of plots show, respectively, a simulation with $\kappa = 5.5$ and $\kappa \rightarrow \infty$, i.e., a Maxwellian, both with only somewhat higher most probable speeds. Finally, the fourth row shows the simulated two Maxwellian fit from the NSSDC. Although, the E1 currents match fairly well, the match to the high energy tail is not good. This latter discrepancy has been alleviated to some extent by the use of four Maxwellians to fit the data (E. C. Sittler, Jr., private communication). Note that none of these simulations include effects due to secondaries or ion feedthrough. Note also that the effects in the first few channels of the E1 spectrum introduce difficulties in the determination of an electron "temperature" (or most probable speed). This problem systematically occurs when the apparent electron temperature exceeds a few tens of volts (E. C. Sittler, Jr., private communication).

Other Qualitative Problems

There is a great deal of data, especially from the Voyager encounters with Jupiter, which has not been analyzed because we have not understood how to do the analysis. The example of the "voids" near Ganymede during the Voyager 2 encounter is one, but not the only, example. The positive ion data acquired during the times in which 0 DN levels are recorded in the E2 data have been mystifying as well. The Voyager 2 encounter with Uranus may have provided the Rosetta stone with which these data may be understood, at least qualitatively.

Spacecraft Charging at Uranus. Figure 102 shows positive ion and electron data (long and short integration times) from the Uranus encounter during that time that a large (~ -400 V) potential on the spacecraft is inferred [McNutt et al., 1987]. It is important to note that the low energy tail is not "real", i.e., the ions are all accelerated to a potential consistent with the peak location in the ion spectra; the "tail" is purely a feed through effect due to these ions down to lower channels. The plot format is described in Voyager Memorandum 122 and is a modification of the "1800" plots produced during the other encounters (refer to Voyager Memorandum 79) to incorporate all of the GS-5 mode data. The charging signature is readily apparent in the D cup in all of the L and M mode spectra. Similar signatures can be seen in the A, B, and C cups. It should also be noted that the E2 spectra exhibit the "turn on" signature characteristic of secondary electron production. In other words, if the ambient electrons are hot enough to produce secondary electrons which contaminate the E2 spectra, then the ambient electron flux is large enough to charge the spacecraft to negative potentials of several hundred volts. The transition to clear signatures in E2 occur as the ion spectra show an average acceleration through ~ 250 eV. The channel corresponding to the turn on is about one channel lower than that containing the the peak in the L mode. This is the qualitative behavior expected: the spacecraft charges to a potential corresponding to the peak location in the electron flux, and, if the latter is below the maximum in the secondary yield curve, the secondaries produced will provide a large out of phase signal in lower channels. Further quantitative analysis of these features may be possible; however, such an effort is hampered by the relatively small signal-to-noise ratio and additional noise produced by the LECP stepping motor.

Inferred Charging at Jupiter. Figures 103 and 104 show ~ 45 minutes of data from the PLS experiment on Voyager 2 as it was outbound from Jupiter. The spacecraft is $\sim 21 R_J$ from the center of the planet, the D cup should show some response to corotating flow of plasma ions, and the main sensor cups none at all. The obvious question is what is the origin of the currents in the positive ion measurements? The E2 spectra suggest an answer, in light of the Uranus charging data. In all of the E2 spectra, channels 2 through 7 are clamped to 0 DN; in addition, the turn on occurs slowly with channel number suggesting the gradual reduction of an out-of-phase signal. Such electron spectra can only be produced if the ambient electrons are hot. The Uranus spectra suggest that electrons which are that hot provide fluxes sufficient to charge the spacecraft negative. Given the similarity of the ion spectra with those at Uranus, it is

probable that the spacecraft is charged to a large negative potential, and most of the ion currents are the feedthrough signatures of the positive ions (of several different plasma species) which are being accelerated into the four cups of the PLS instrument. The occurrence of a peak in the ion spectra in channels 14, 15, or 16 implies that the potential is at least -2500 volts. There is roughly a 24 hour period during which these charging levels were maintained. If this interpretation is correct, it may be possible to extract positive ion densities which can be checked against the cut off frequency observed in the Plasma Wave (PWS) data [Scarf et al., 1981].

Figures 105 and 106 show a similar set of spectra which include the last of the plasma depletions observed during the Voyager 2 inbound pass [McNutt et al., 1987]. The E2 spectra show the same qualitative behavior but are clamped to 0 DN up to a larger channel number. Most of the positive ion spectra peak in channel 16 or higher (with the two obvious exceptions). Both of the features are consistent with a hotter ambient electron population and, as a consequence, more negative spacecraft potential. Such behavior is observed in all of the depletions. In all qualitative respects, the data obtained within the depletions is consistent with that obtained for more extended periods outbound illustrated in Figures 103 and 104.

Similar data were obtained by Voyager 1 outbound from Jupiter. Figure 107 shows data obtained $\sim 22 R_J$ from Jupiter by the PLS instrument on Voyager 1. At the top of the figure and just past the center are E2 spectra similar to those of Figure 104. The corresponding L mode spectra also show the characteristic rise with channel number which would be associated with ions accelerated into the various Faraday cups. At the center of the figure are two sets of DC return spectra acquired ~ 1120 . One of these was used in the analysis of the fractional modulation due to secondaries given in tabular form above. It is readily apparent from the E2 spectra in Figure 107 that the turn on in the plasma spectrum is associated with the location of the peak in the DC return E2 spectra.

Puzzling Features in the Ion Spectra. The lower part of Figure 107 shows a feature which is not so readily understood. The E2 and E1 spectra indicate relatively cooler electron temperatures, and the lower channels in the ion spectra have apparently been filled in with direct signals. However, Channel 16 in the main sensor cups remains at a relatively low level. Figure 108 shows similar behavior a few hours earlier on day 65, along with some bizarre jumps in the data in the D cup (the glitches in the M mode spectra are from LECP 6 second stepping). Figures 109 and 110 show similar behavior from the inbound pass of Voyager 1 on day 63 of 1979. In this latter case, azimuthally flowing ions are apparent in the D cup.

Similar E2 and L spectra were also acquired for a limited region during the Voyager 1 outbound pass at Saturn. The signatures are not as clear due to the signal to noise ratio.

The ion spectra in Figure 110 are particularly puzzling in that there is a drop to the 0 DN level in high channels of the C cup for both the L and M modes, without corresponding behavior in the A or B cups. The 16th channel of E2 also seems to be adversely affected. These spectra are not easily understood. If the signals in the upper channels of the A, B, and C cups in the L mode were due entirely to the ambient plasma population, the

ions producing the signature would be hot, and the signature should be the same in all of the cups. Large anisotropies can also be ruled out if the anisotropy is gyrotropic. Similarly, if the measured currents were due to energetic electrons, a similar signature should be present in all the cups of the main sensor, which it clearly is not. In addition, the affected cup is not always C, i.e., the cup showing 0 DN in channel 16 changes, so an electronics failure can be ruled out.

The 0 DN levels certainly suggest an out-of-phase signal which must somehow be associated with the direction of positive ion flow. We come to this latter conclusion as there is no other phenomenon to distinguish between cups at the highest energies. Unfortunately, there are no DC return measurements for which the downturn is seen in the A cup plasma measurements and the fluxes are sufficiently above the photoelectron current (from suppressor leakage) for the change in net phase to be directly measurable.

An out of phase signal is not readily produced in the positive ion measurements. As the modulator has a positive potential, secondary electrons can only be produced at the negative suppressor grid. For such a current to be modulated, the rate must be varied via the refraction modulation of the particles reaching the suppressor grid [Vasyliunas, 1971]. To produce an out-of-phase current, the net (positive) current must increase with increasing (positive) modulator potential. Either, more positive ions must reach the collector plate or less electrons. Neither of these options has an obvious mechanism. The out-of-phase signal does seem to occur in the cups furthest away from the ion flow. As secondary electrons can escape only from grids charged to negative potentials, and the energies are too low to produce ions from either electron or ion impact, it would appear that the effect must be related to the collection of fewer secondary electrons with increasing modulator potential. Further study will require a full accounting of all feedthrough and secondary production corrections.

Figures 111 and 112 show a sequence from Voyager 1 inbound as the spacecraft neared the warm Io torus. Toward the end of the sequence, there is a component of convective flow into the B, C, and D cups. Up until -0135, there is a relatively high energy background signal in all cups in the positive ion modes. At this time the superthermal electrons disappear and both the electron and ion spectra change qualitatively. The signals in the high energy ion channels drop, indicating that these signals were probably feedthrough from the hot electrons (those with energies greater than 95 volts which could reach the collector in spite of the suppressor potential). After this time much of the electron currents may be due to ion feedthrough in the upper channels; the 0 DN level in channel 16 is almost certainly due to secondary electrons produced by the ions at the modulator grid. This effect must also have been present in previously but masked by the hot ambient electrons. Such a combination of effects would explain the somewhat depressed electron current in channel 16 of the E2 spectra in Figures 103 through 106 and 109 through 111. In some of these figures, the ions producing the secondaries must have been accelerated by the spacecraft potential in the first place where the latter was caused by the hot electron flux; such synergistic effects apparently result in the complexities found in attempting to

explain many of the ion and electron spectra.

Other strange features are found in spectra obtained with the Voyager 1 instrument within the Io torus itself. Figures 113 and 114 shown data from $\sim 9 R_J$ and $\sim 6 R_J$ from Jupiter, respectively. In Figure 113, out-of-phase currents contribute to the low energy channels in the A and B cups in the L mode but not the M mode. In Figure 114, intermediate channels of the L mode spectra from the B and C cup exhibit large subtracting currents never seen again in the mission. This behavior could be related to the saturation of the amplifiers in the L mode, as there is no analogous affect in the M mode spectra and the L mode measurements are highest in the B and C cups of the M mode. More thought should be given to this possibility.

The Oscillator Effect. Figures 115 and 116 show the best example of the most bizarre effect to appear in the data. For this particular period, the E2 spectra are relatively unaffected, although there are counterexamples. The E1, L, and, especially, M mode spectra exhibit oscillations with respect to channel number. In the M mode, the oscillation period is clearly resolved, with the telemetered currents reaching down to the 0 DN level between peaks. This behavior is presumably to be interpreted as indicating an out-of-phase signal in these regions; if DC return measurements were available (and none seem to be) they would apparently show a current varying sinusoidally with respect to the channel number. It is worth noting that the widths of the zero DN regions are less than half the widths of the nonzero DN regions. In other words, a the sinusoidal variation appears to be superimposed on top of an in-phase modulated current, shifting the oscillation point upward from the zero level. That this is likely the case is more evident in the bottom of Figure 116. The oscillation frequency appears to reach a minimum -192/0815, and a similar minimum occurred -192/0515. Plate 1 of Scarf *et al.* [1981] suggests that these times may be associated with rapidly changing plasma densities. During these times, the plasma frequency was rapidly swept through 2.4 kHz, which is the frequency of the square wave power supplied to the PLS experiment; the plasma frequency apparently remained above 1 kHz throughout this region. The square wave applied to the modulator grids has a frequency of 400 Hz, so it is not obvious why an effect is seen. Presumably, the oscillations in the measured current are a beat phenomenon occurring at the difference between the local plasma frequency and some reference frequency produced by the PLS experiment. The 400 Hz square wave on the modulator grid will also produce odd harmonics, so the relevant frequency provided by the instrument may be 1.2 or 2.0 kHz (3rd or 5th harmonic, J. H. Binsack, private communication). Only narrow band data from the PWS experiment is available at this time, so the error bars on the density determined from the cutoff of the continuum radiation are rather large. Further, more detailed comparisons are required to determine the exact limits which can be put on the density.

A better determination of the relevant spacecraft frequency may be obtainable from Voyager 2 data in the solar wind just prior to its encounter with Saturn. Here the solar wind is clearly visible in the M mode spectra, as are the oscillations. A fit to the solar wind proton peak at 1981-236/1300:58 (J. D. Richardson, private communication) yields a proton density of

0.0475 cm⁻³. The oscillation envelope occupies ~10 M mode channels, or ~2.4 seconds. The corresponding electron plasma (from charge neutrality, neglecting the α particles) and difference frequencies would then be 1960 Hz and 0.42 Hz. This is suspiciously close to the 5th harmonic. The 3rd harmonic corresponds to an electron density of 0.018 cm⁻³. Such low density regions have been sampled, and there is, presumably, more power in the third harmonic than the 5th. It is possible that such lower densities do not provide enough electrons to yield a signal above the noise level. It is also possible that the spectra of Figures 116 and 117 correspond to such lower densities. Again, careful comparisons are needed to further pin down this effect. We note that a plasma frequency of 400 Hz corresponds to a density of 0.00198 cm⁻³. Rather large speeds would be required to produce a measurable flux.

For the solar wind spectrum considered above, the amplitude corresponds to a flux of $\sim 2 \times 10^5$ cm⁻² s⁻¹. For the density quoted above, the speed is 4.2×10^6 cm s⁻¹. This does not seem to relate to much of anything but is based on the assumption that the oscillating charges are spread out uniformly on the collector. If the area of the collector impacted were smaller, the corresponding particle speeds would be larger.

Obviously, this phenomenon is not understood. Other complications include the exact mechanism of setting up current oscillations at the collector plate and to what extent, if any, Doppler shifts in the plasma frequency affect the exact resonance conditions. The reason for selecting a 400 Hz frequency for the modulator was a concern about resonance effects (A. J. Lazarus and J. H. Binsack, private communication). The alternating changes in the modulator potential are certainly suspect for establishing charge density oscillations, but no detailed studies of mechanisms were ever conducted. Another possible clue is the fact that the PWS experiment "sees" the PLS experiment when the modulator is on; presumably this is due to waves excited in the ambient plasma (H. S. Bridge, private communication).

IMPLICATIONS

There several implications which follow from this study, one being major. The major result is that the energetic electron spectra, i.e., those obtained in the E2 mode cannot be taken at face value. We have also noted that corrections to the E1 spectra can be important if the electron temperature is high enough. Even in those cases where there is no obvious out-of-phase current, the electron current below channel 8 will be decreased and above channel 8 increased over the fluxes present in the parent population outside the instrument housing. Obviously, the extent of the corrections are a function of the electron distribution function which cannot be simply read off of the measured currents due to the electron cascade-type of feedthrough effect. Further complications arise due to feedthrough from the ions, which can be affected by feedthrough from the electrons, and spacecraft charging. These effects, and the resulting corrections to the analysis, are certainly minimal in the solar wind or cold Io torus. In other locales they may also be unimportant to some level, e.g., 1% or 10% say, but this must be judged on a case by case basis.

These complications may (or may not) have a major effect on the electron impact ionization rates for multiply charged ions in the warm Io torus as calculated by *Sittler and Strobel* [1987]. Their rates are probably within a factor of 3 or so of the true rates, but a more detailed study is necessary to confirm or reject such a number. Given that the ionization cross sections typically peak around 100 eV and secondaries apparently cause an out-of-phase signal up to ~750 eV, the published rates are almost certainly low. Their other conclusions based upon details of variations in the hot electron component, rather than those based upon gross morphological characteristics, are also called into question by these results and should be reexamined.

Consequences for positive ion results tend to be less dramatic, as a ready source of modulated secondaries within the instrument is no longer available. The major source of "contamination" is expected to be simple electron feedthrough, which may explain currents in the main sensor in the upper channels, such as depicted in the top of Figure 111. The feedthrough contribution should be relatively flat (based on some simulations), and certain features remain unexplained, notably the downturn in the highest energy channels, present in the C cup in Figure 110. As a matter of course, we have refrained from publishing these data or any analysis based upon them because we could not duplicate them from our knowledge of the instrument response. This "policy" has, perhaps been overdone. A search for a qualitative mechanism for producing an out-of-phase signal in the ion measurements is required and, can perhaps lead to new physical insights concerning the characteristics of the ambient plasma.

A final major consequence is that many of the spectra from the various planetary encounters can be understood in terms of a very hot electron environment and a negative charging of the Voyager spacecraft. The work of *Khurana et al.* [1987] notwithstanding, the spacecraft potential never seems to have exceeded significantly a few kV. Some of the spectra shown in Figure 105 appear at first sight to be difficult to reconcile with this solution, as a turnover in channel 16 alone must be viewed with suspicion. On the other hand, for the apparent feedthrough signals to be the amplitude they are with the corresponding spectral shape, the ion energy cannot appreciably exceed 5 kV. Some preliminary work suggests 7 kV is a hard upper limit unless appreciable plasma injection (factors of 10) is occurring simultaneously with the charging process. The latter can be ruled out as it would give rise to a corresponding discharge current to the spacecraft, lowering the potential, and contradicting the observations. The charging levels found in the Voyager data should prove useful in the interpretation of plasma data returned from the Jovian magnetosphere from the Galileo orbiter, as such charging levels had not previously been inferred from Voyager and Pioneer data sets (F. L. Scarf seems to be vindicated on this point!).

Finally, we note in passing that the DC return measurements have been crucial in sorting out these various phenomena. At the same time, they are difficult to work with due to the (presumed) thermal dependence of the DN to current conversion. Examination of data during the thermal cycling of the Voyager 1 instrument seems to preclude as strong a dependence as inferred from the pre-flight calibrations, however

(see Voyager Memorandum #158). The DC return measurements are typically difficult to interpret due to the presence of the suppressor grid and the combined effects of ion, electron, and secondary electron currents. The PLS experiment is fundamentally different from an RPA (retarding potential analyzer) due to the grounded aperture grid, i.e., the instrument potentials do not, except to low order, intrude into the local plasma (this may be a bit misleading: using the formulas of *Morse and Feshbach* [1953], I estimate about a 4% "leakage" in the ion modes, or about 100 V for a modulator potential of 2500 V). As a result, the floating potential of the spacecraft cannot be determined, and, at zero modulator potential, there should be a net zero current to the collector plate. That this does not happen in the Jovian and Saturnian magnetospheres can usually be traced to i) directional effects due to supersonic ion flow, ii) photoelectron production and suppressor leakage, iii) changing electron temperature with respect to the suppressor potentials used for E1, E2, and ion measurements, and iv) secondary electron production at the skin of the spacecraft itself. Effect ii) accounts for the difference in the A and D cup currents in Figures 55 through 59. Effect i) accounts for the differences between the currents in the A and D cups in Figures 61, 64, 65, and 66. Effects iii) and iv) apparently account for the zero in the current (with respect to modulator potential) in Figures 67, 68, and 71. It may be possible to understand the some aspects of the secondary emission characteristics of the spacecraft from these data, but it will not be an easy undertaking. Note that due to effect iii) the measured DC return current is almost always positive; in the E2, L, and M modes, the suppressor potential is -95.2 volts, and current carrying electrons with energies less than this cannot reach the collector plate to cancel the positive current carried by the ions. This also explains why the D cup, L mode and E2 traces are usually continuous as the average modulator potential changes sign. The spectra in Figure 61 are the exception; in this case most of the electron current is carried by hot electrons.

SUMMARY AND CONCLUSIONS

We have completed an extensive survey of PLS data from the two Voyager spacecraft in an attempt to understand certain anomalous spectra obtained within the magnetospheres of the outer planets. The study of the plasma voids on the Voyager 2 pass and the ensuing argument over charging levels with investigators studying LECP data motivated this study. In attempting to explain these spectra we have developed a much improved understanding of how modulated-grid Faraday cups actually respond to the often bizarre plasma environments encountered in deep space. This has included an understanding of the generation of photo- and secondary electrons within the cup housing, and how these populations affect the currents actually measured by the instrument and telemetered to Earth. Some of this understanding is quantitative while much is not. Due to the various synergistic effects, such quantitative study will require the use of the flight spare in laboratory tests coupled with further numerical modeling. We have also found regions in these magnetospheres where the spacecraft was apparently charged negatively to kilovolt potentials. This may

well open up possibilities for further analysis of PLS data. Finally, we have made the first systematic study of the DC return spectra from the PLS instrument, used them in interpreting some of the strange plasma data, and identified the difficulties and potential uses of this data set.

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DC RETURN CURRENTS - FROM PLCONS

-1.000E+05	-1.000E+05	-1.000E+05	-1.120E+05	-1.150E+05	-1.120E+05	-1.200E+05	-1.240E+05	-1.280E+05	-1.320E+05	-1.350E+05
-1.400E+05	-1.450E+05	-1.500E+05	-1.550E+05	-1.600E+05	-1.600E+05	-1.650E+05	-1.700E+05	-1.750E+05	-1.800E+05	-1.850E+05
-1.900E+05	-1.970E+05	-2.040E+05	-2.110E+05	-2.180E+05	-2.250E+05	-2.320E+05	-2.360E+05	-2.470E+05	-2.580E+05	-2.690E+05
-2.800E+05	-3.120E+05	-3.400E+05	-3.400E+05	-3.400E+05	-3.600E+05	-3.800E+05	-3.800E+05	-4.000E+05	-4.200E+05	-4.400E+05
-4.600E+05	-4.840E+05	-5.080E+05	-5.320E+05	-5.560E+05	-5.800E+05	-6.000E+05	-6.000E+05	-6.200E+05	-6.400E+05	-6.600E+05
-6.800E+05	-7.040E+05	-7.280E+05	-7.520E+05	-7.760E+05	-8.000E+05	-8.200E+05	-8.200E+05	-8.400E+05	-8.600E+05	-8.800E+05
-9.400E+05	-1.150E+06	-1.360E+06	-1.580E+06	-1.800E+06	-2.000E+06	-2.200E+06	-2.400E+06	-2.600E+06	-2.800E+06	-3.000E+06
-4.000E+06	-4.480E+06	-4.960E+06	-5.440E+06	-5.920E+06	-6.400E+06	-6.880E+06	-7.360E+06	-7.840E+06	-8.320E+06	-8.800E+06
-9.600E+06	-1.050E+07	-1.140E+07	-1.220E+07	-1.310E+07	-1.400E+07	-1.490E+07	-1.580E+07	-1.670E+07	-1.760E+07	-1.840E+07
-3.200E+07	-3.340E+07	-3.480E+07	-3.620E+07	-3.760E+07	-3.900E+07	-4.040E+07	-4.180E+07	-4.320E+07	-4.460E+07	-4.600E+07
-4.000E+07	-5.120E+07	-5.340E+07	-5.560E+07	-5.780E+07	-6.000E+07	-6.220E+07	-6.440E+07	-6.660E+07	-6.880E+07	-7.100E+07
-7.400E+07	-7.760E+07	-8.120E+07	-8.480E+07	-8.840E+07	-9.200E+07	-9.560E+07	-9.920E+07	-1.028E+08	-1.064E+08	-1.100E+08
1.000E+05	1.050E+05	1.100E+05	1.150E+05	1.200E+05	1.250E+05	1.300E+05	1.310E+05	1.370E+05	1.430E+05	1.490E+05
1.550E+05	1.620E+05	1.690E+05	1.760E+05	1.830E+05	1.900E+05	1.970E+05	2.040E+05	2.110E+05	2.170E+05	2.240E+05
2.350E+05	2.450E+05	2.550E+05	2.650E+05	2.750E+05	2.850E+05	2.950E+05	3.050E+05	3.150E+05	3.250E+05	3.350E+05
3.500E+05	3.660E+05	3.820E+05	3.980E+05	4.140E+05	4.300E+05	4.460E+05	4.620E+05	4.780E+05	4.940E+05	5.100E+05
5.200E+05	5.400E+05	5.600E+05	5.800E+05	6.000E+05	6.200E+05	6.400E+05	6.600E+05	6.800E+05	7.000E+05	7.200E+05
7.400E+05	7.600E+05	7.800E+05	8.000E+05	8.200E+05	8.400E+05	8.600E+05	8.800E+05	9.000E+05	9.200E+05	9.400E+05
1.050E+06	1.300E+06	1.550E+06	1.800E+06	2.050E+06	2.300E+06	2.550E+06	2.800E+06	3.050E+06	3.300E+06	3.550E+06
5.000E+06	5.520E+06	6.040E+06	6.560E+06	7.080E+06	7.600E+06	8.120E+06	8.640E+06	9.160E+06	9.680E+06	1.020E+07
1.100E+07	1.190E+07	1.280E+07	1.370E+07	1.460E+07	1.550E+07	1.640E+07	1.730E+07	1.820E+07	1.910E+07	2.000E+07
2.100E+07	2.240E+07	2.380E+07	2.520E+07	2.660E+07	2.800E+07	2.940E+07	3.080E+07	3.220E+07	3.360E+07	3.500E+07
3.500E+07	3.650E+07	3.840E+07	4.020E+07	4.200E+07	4.380E+07	4.560E+07	4.740E+07	4.920E+07	5.100E+07	5.280E+07
5.400E+07	5.640E+07	5.880E+07	6.120E+07	6.360E+07	6.600E+07	6.840E+07	7.080E+07	7.320E+07	7.560E+07	7.800E+07
8.200E+07	8.560E+07	8.920E+07	9.280E+07	9.640E+07	1.000E+08	1.040E+08	1.080E+08	1.120E+08	1.160E+08	1.200E+08

without 1 from real number
(first entry = 0 DN!)

TABLE 1

Look like table was for
~ -10°C

DC RETURN CURRENT

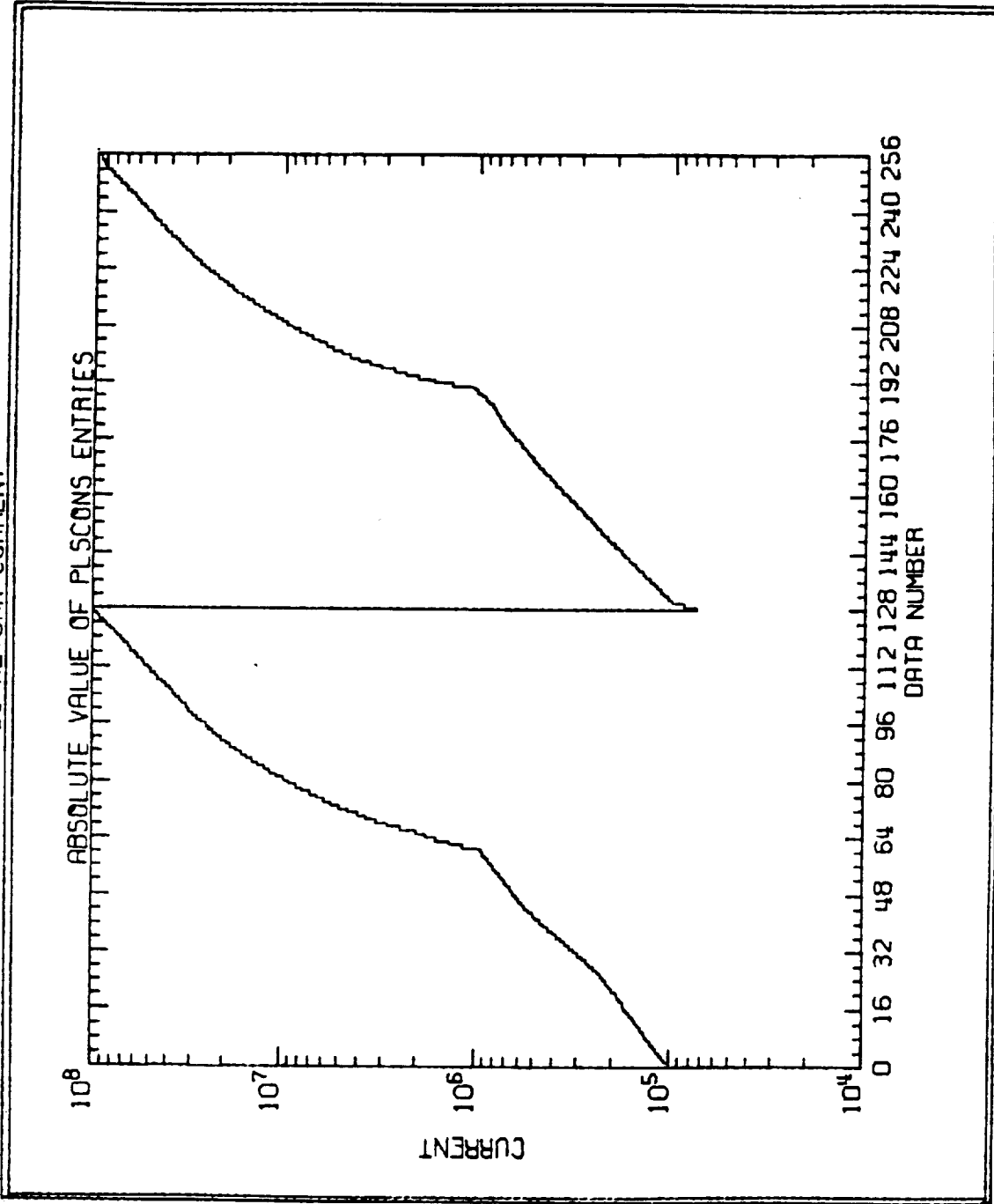


FIGURE 1

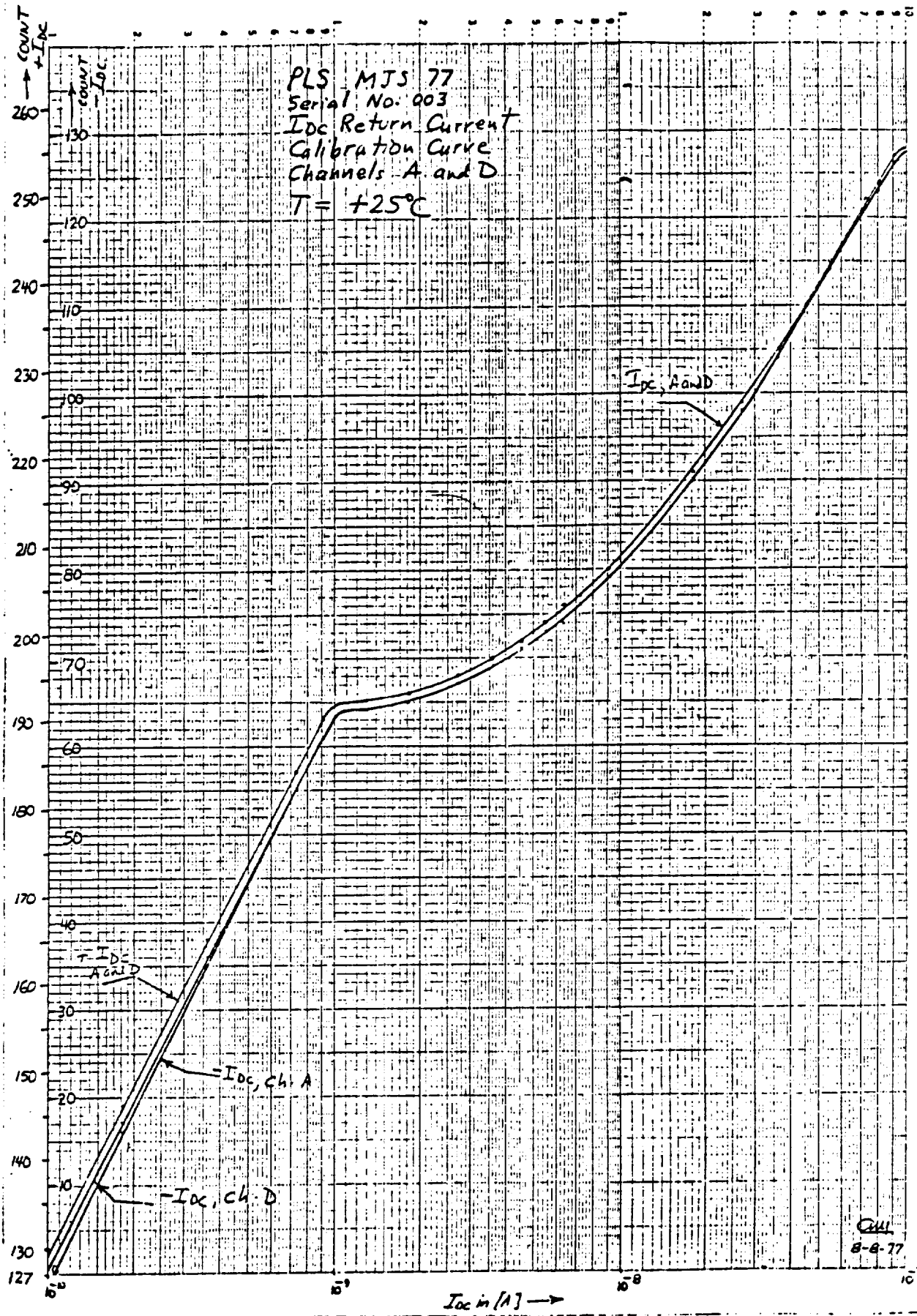


FIGURE 2

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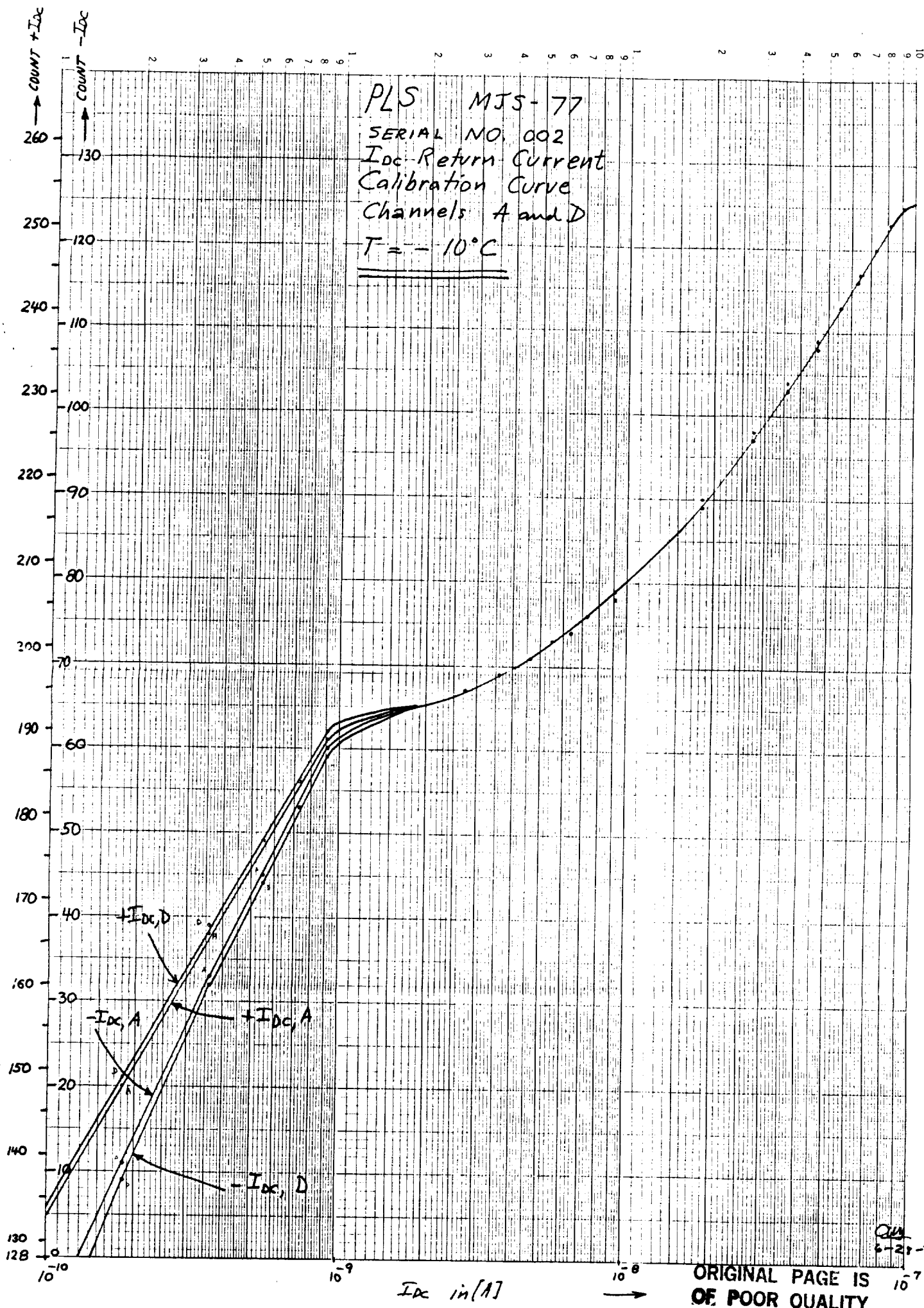


Figure 3

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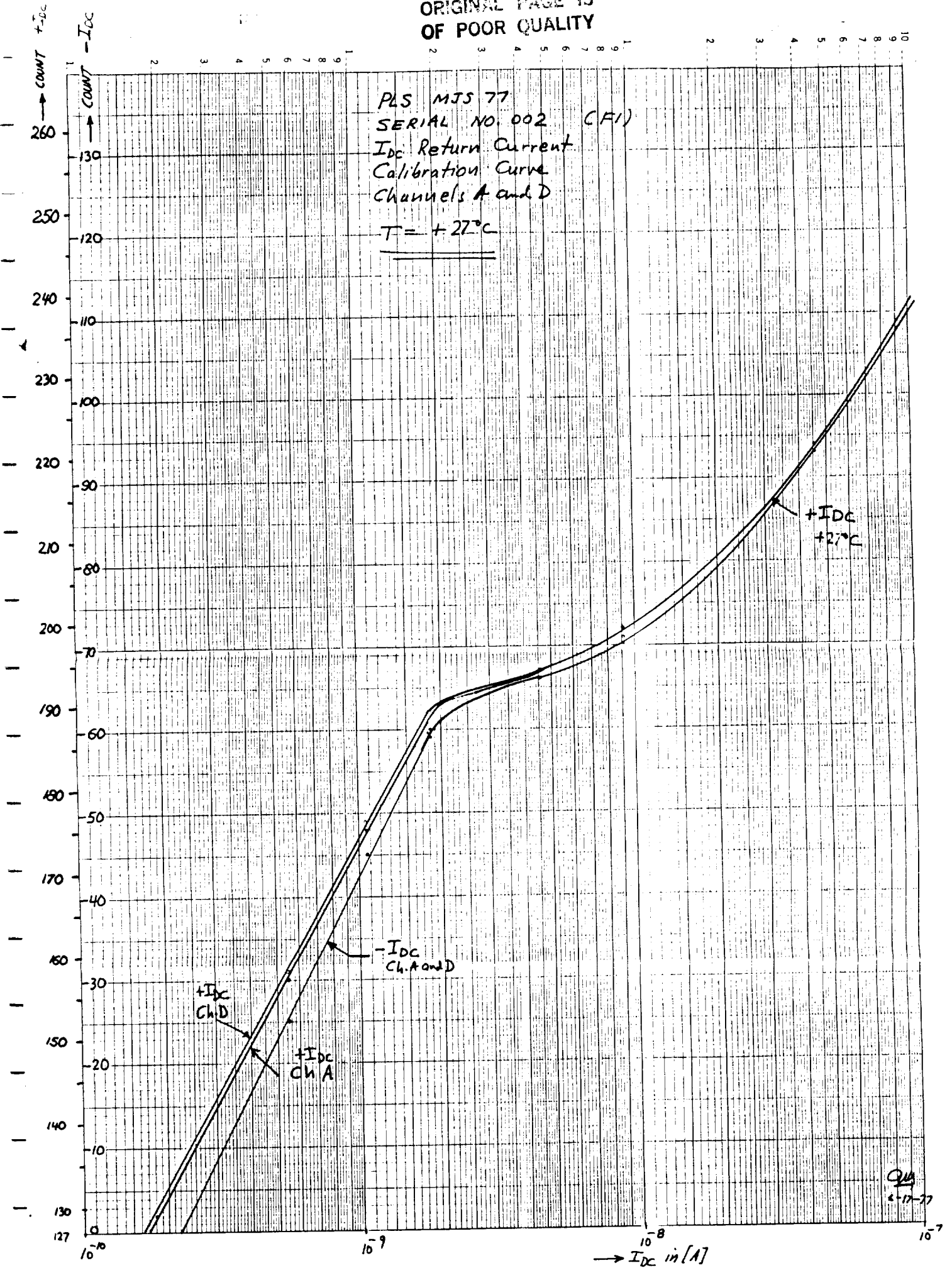


Figure 4

PL5 MJS 77
SERIAL No. 002
I_{DC} Return Current
Calibration Curve
Channels A and D
T = +50°C

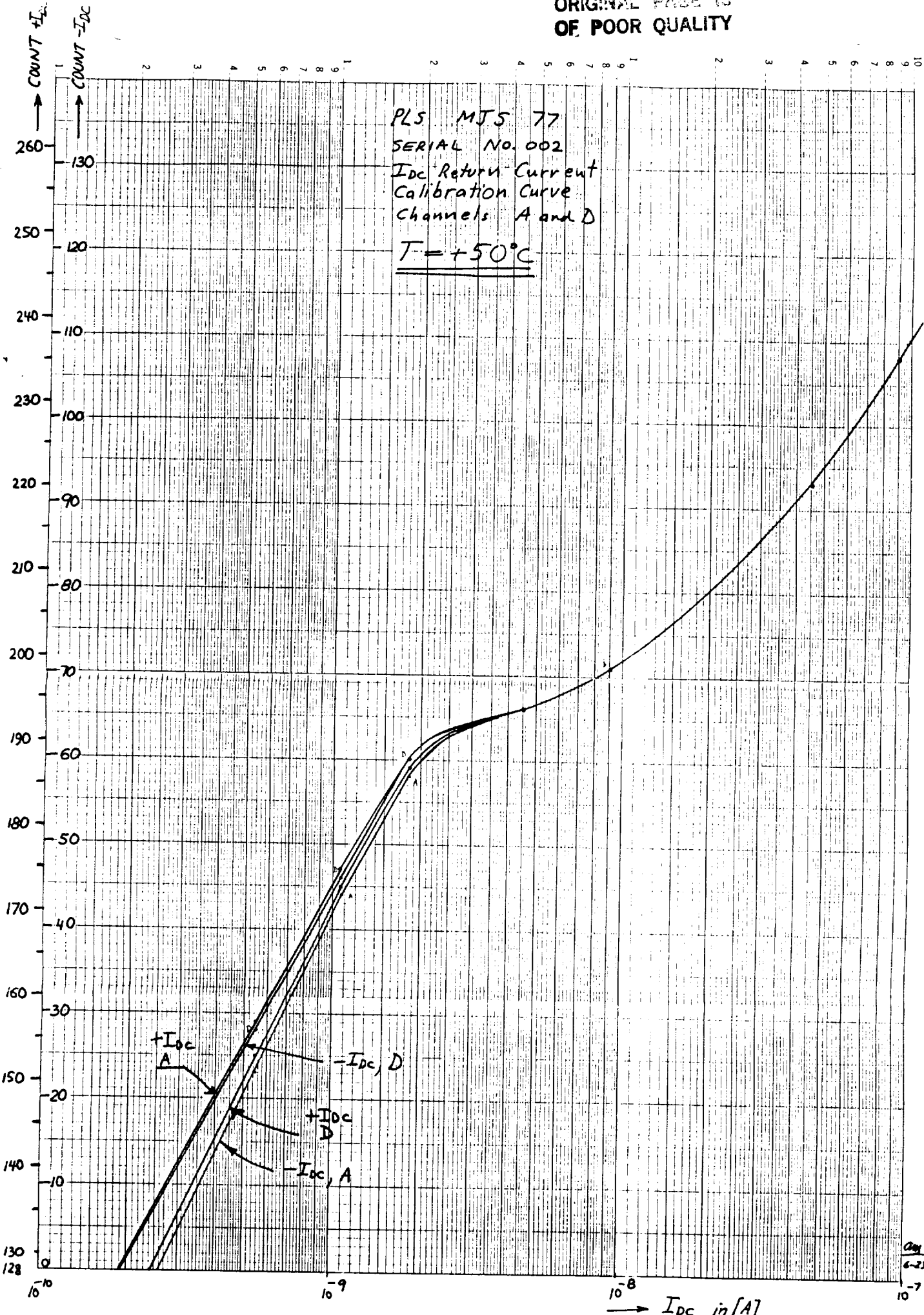


FIGURE 5

281
6-23-77

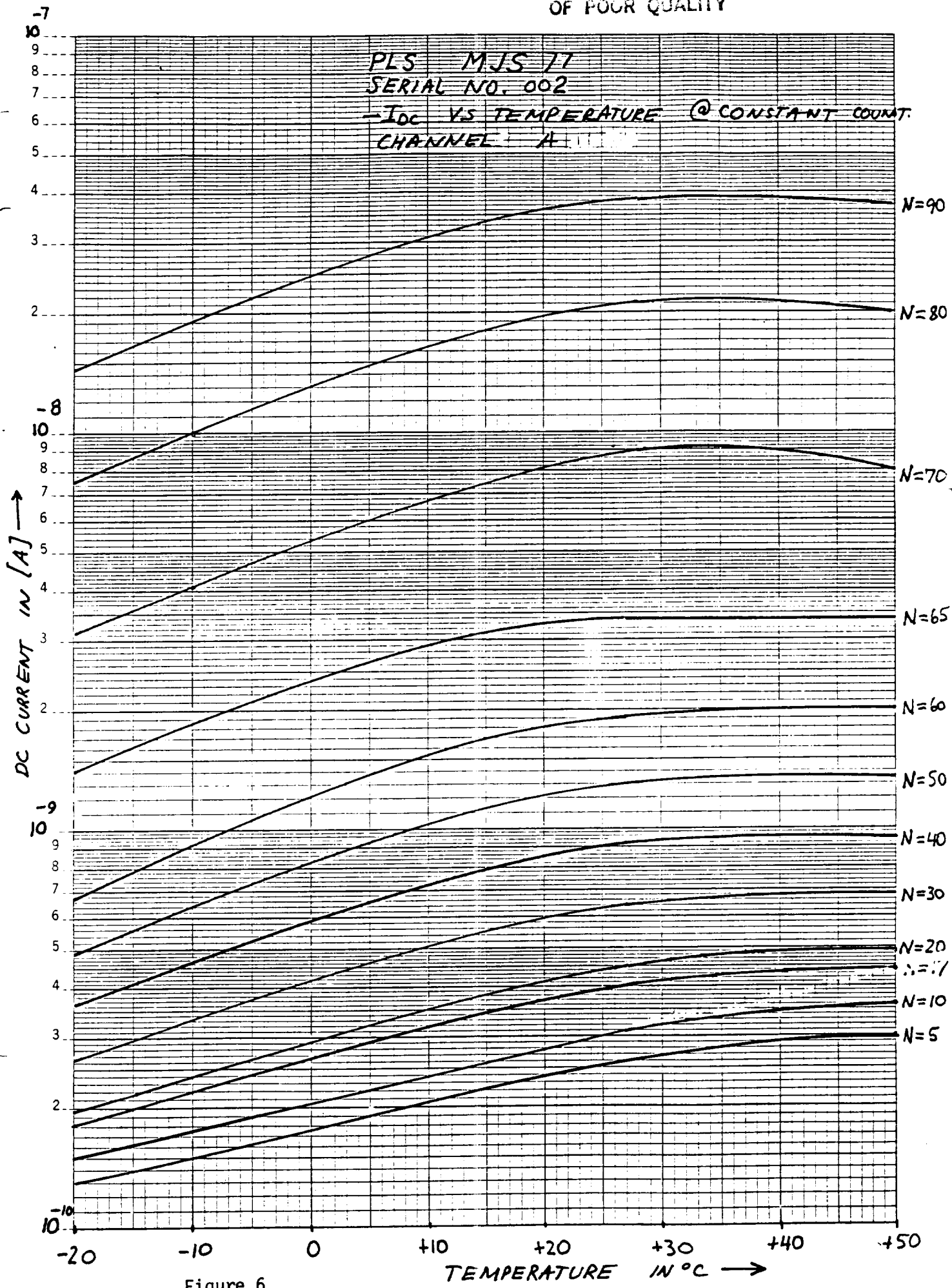


Figure 6

PLS MTS 77
Serial No. 002
 I_{DC} Return Current
Calibration Curve
Channel A

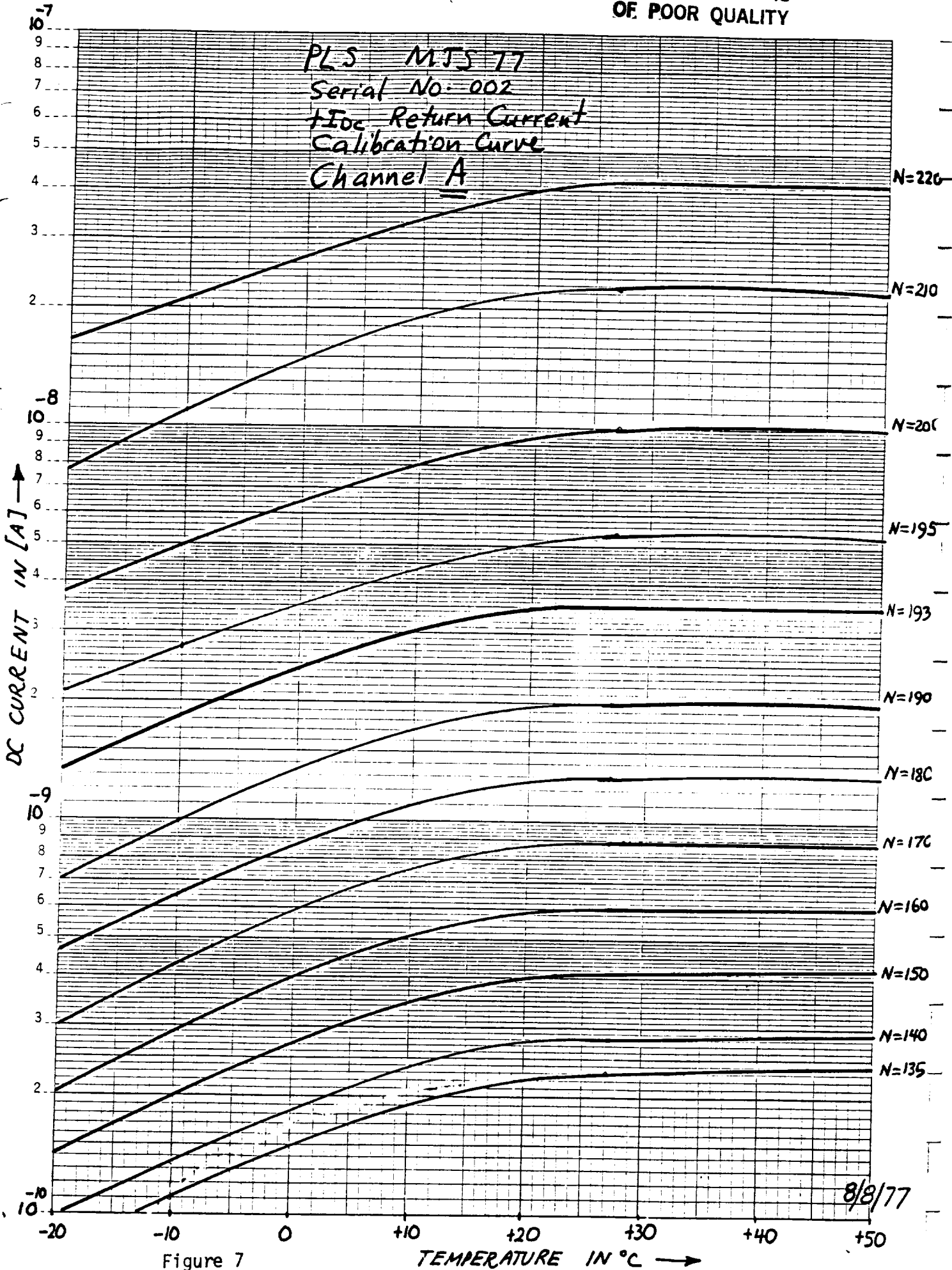


Figure 7

8/8/77

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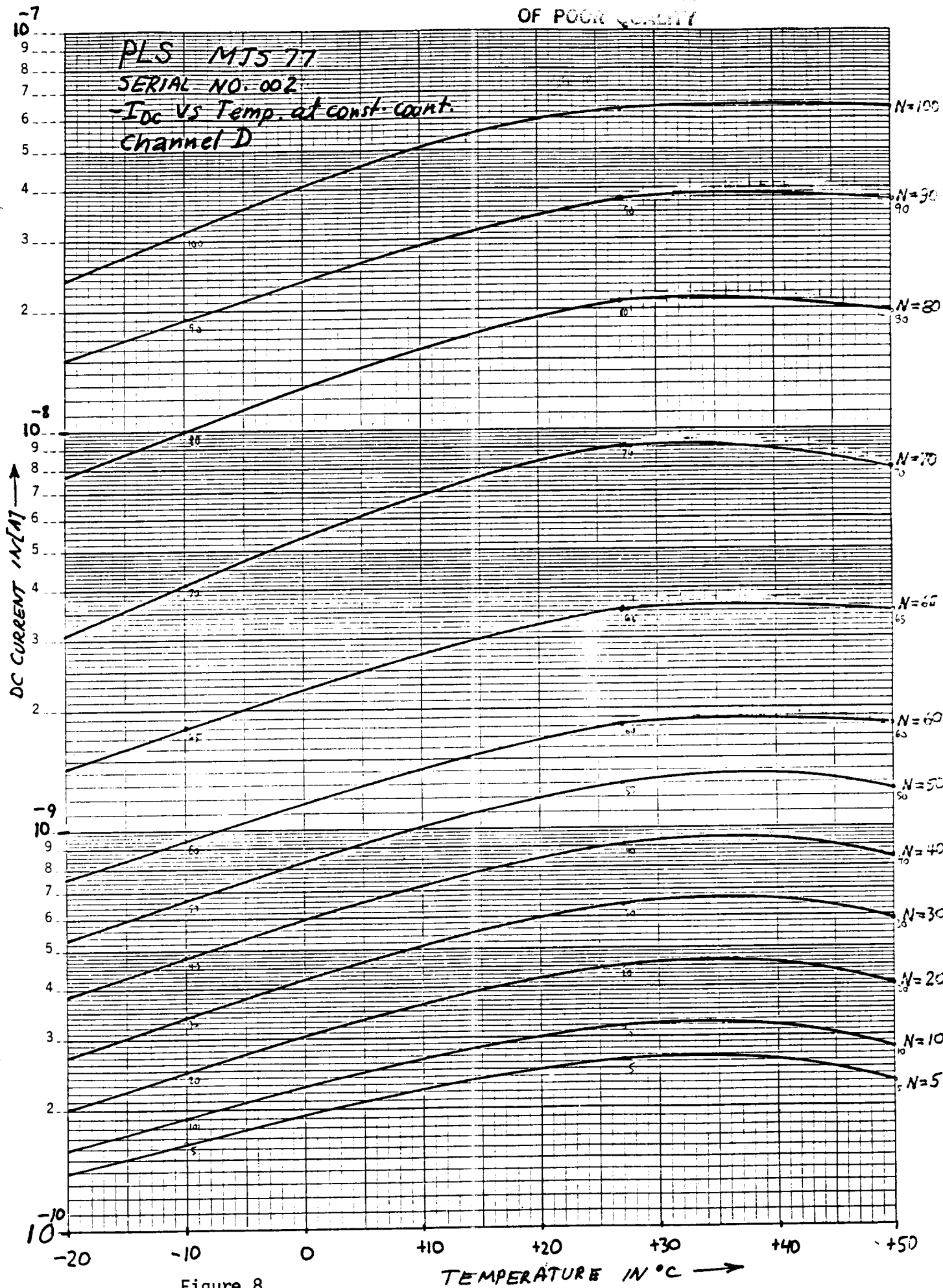


Figure 8

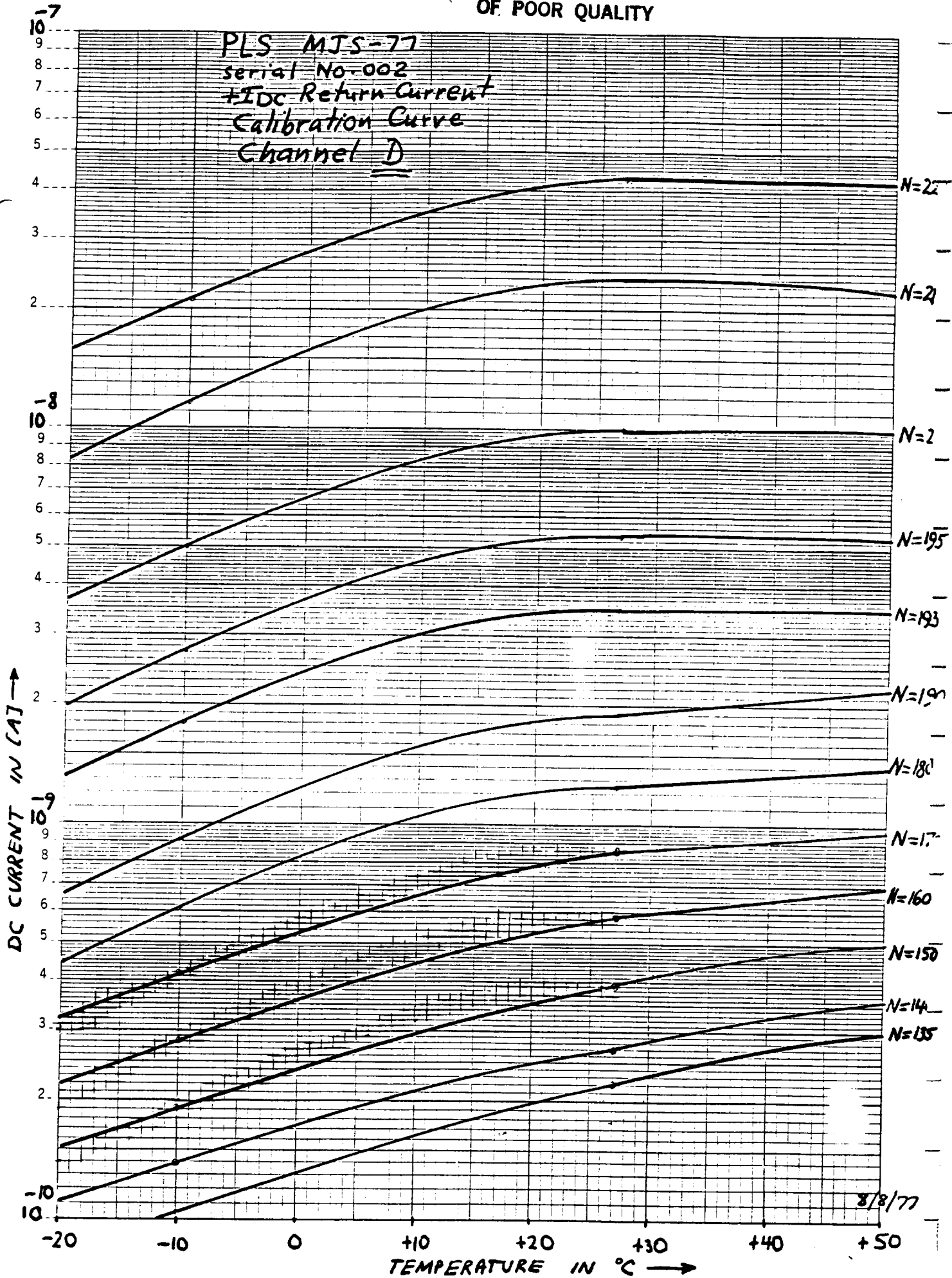


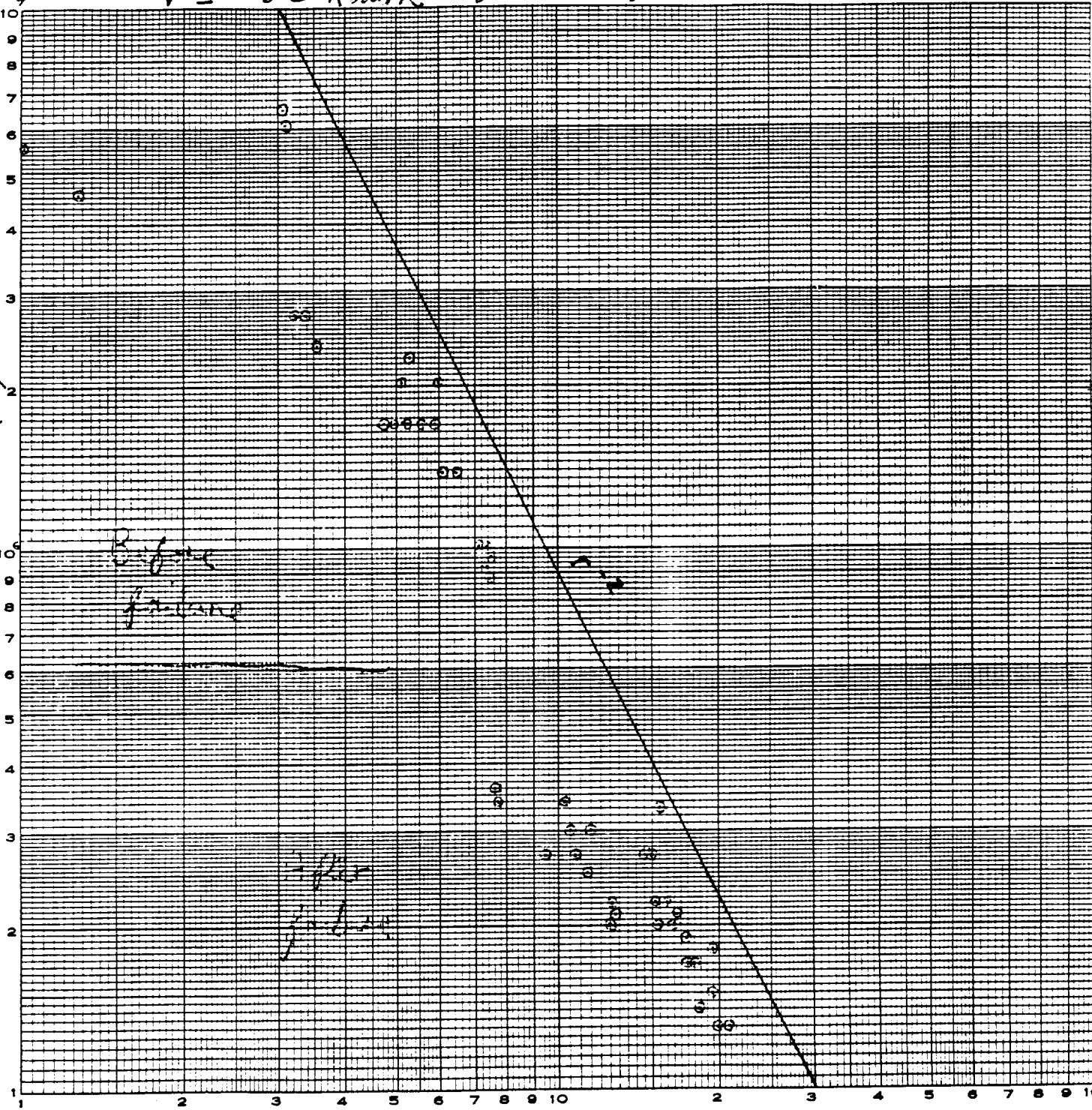
Figure 9

DC RETURN CURRENT VERSUS HELIOCENTRIC DISTANCE

V1 DC Return vs Radius

DIETZGEN CORPORATION
MADE IN U.S.A.
NO. 340-L22 DIETZGEN GRAPH PAPER
LOGARITHMIC
2 CYCLES X 2 CYCLES

D. Current (fA)

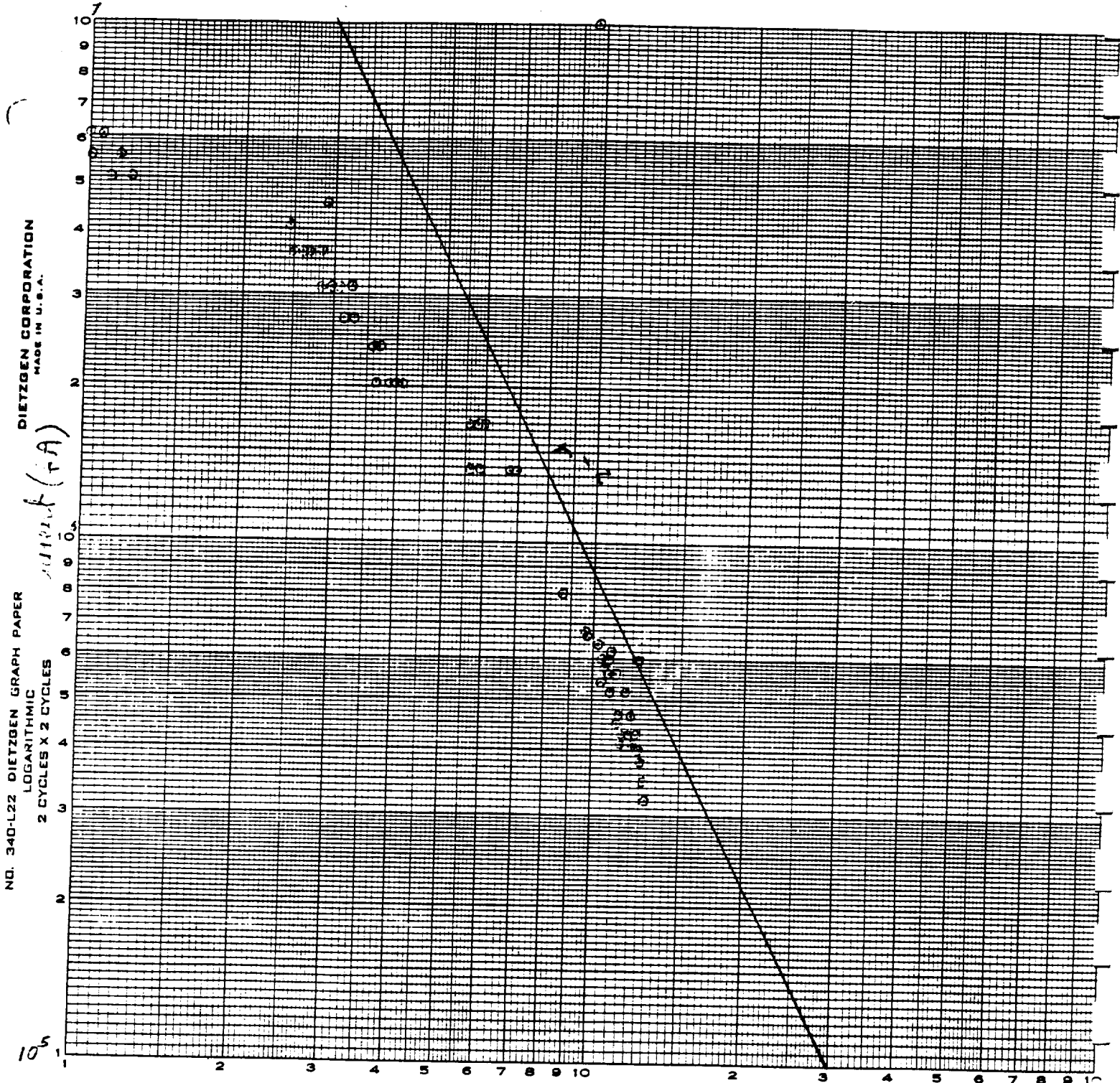


Radius (A.U.)

Figure 10

DC RETURN CURRENT VERSUS HELIOCENTRIC DISTANCE

V2 DC Return vs. Radius

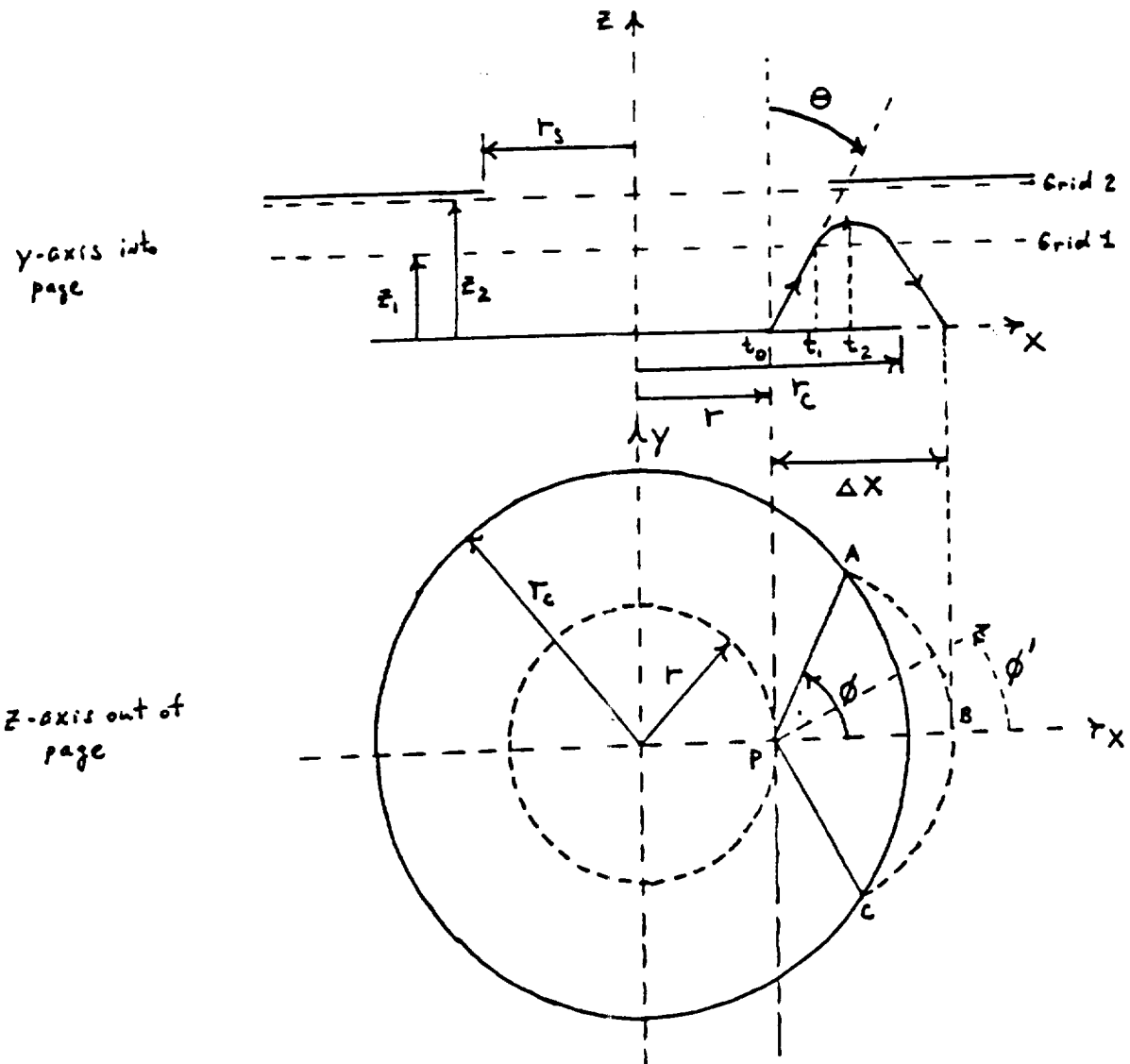


Radius (A.U) Figure 11

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Section B

Fig. 1



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Figure 12

FSLP versus

"E1 Made"

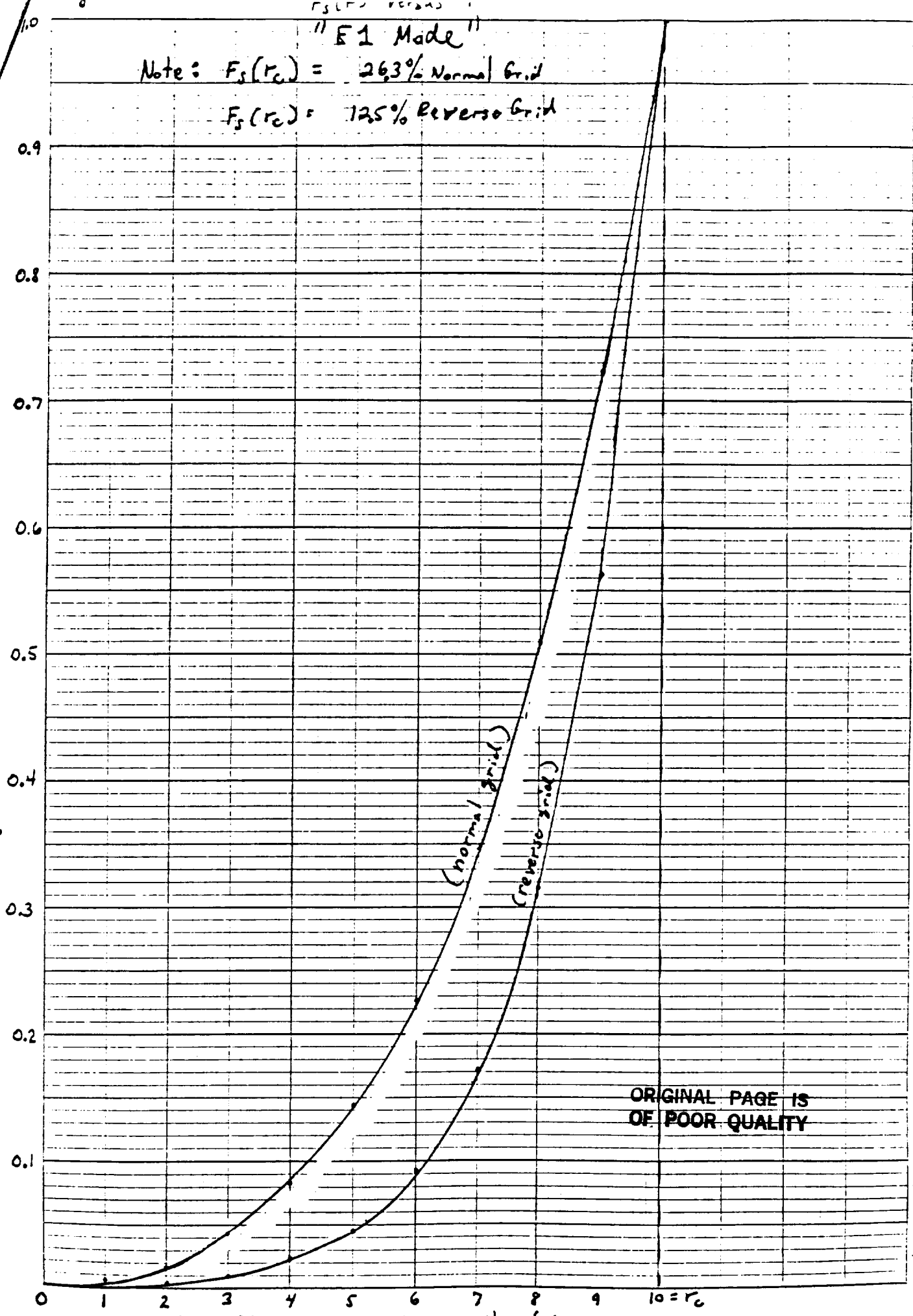
Note: $F_s(r_c) = 263\%$ Normal Grid

$F_s(r_c) = 125\%$ Reverse Grid

46 0780

SCALE 10 X TO THE INCHES X IN INCHES
MATH & ENGINEERING CO.

$$F_s(r) = F_s(r) / F_s(r_c)$$



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Figure 13

r in units of Δr

"F2 Mode"

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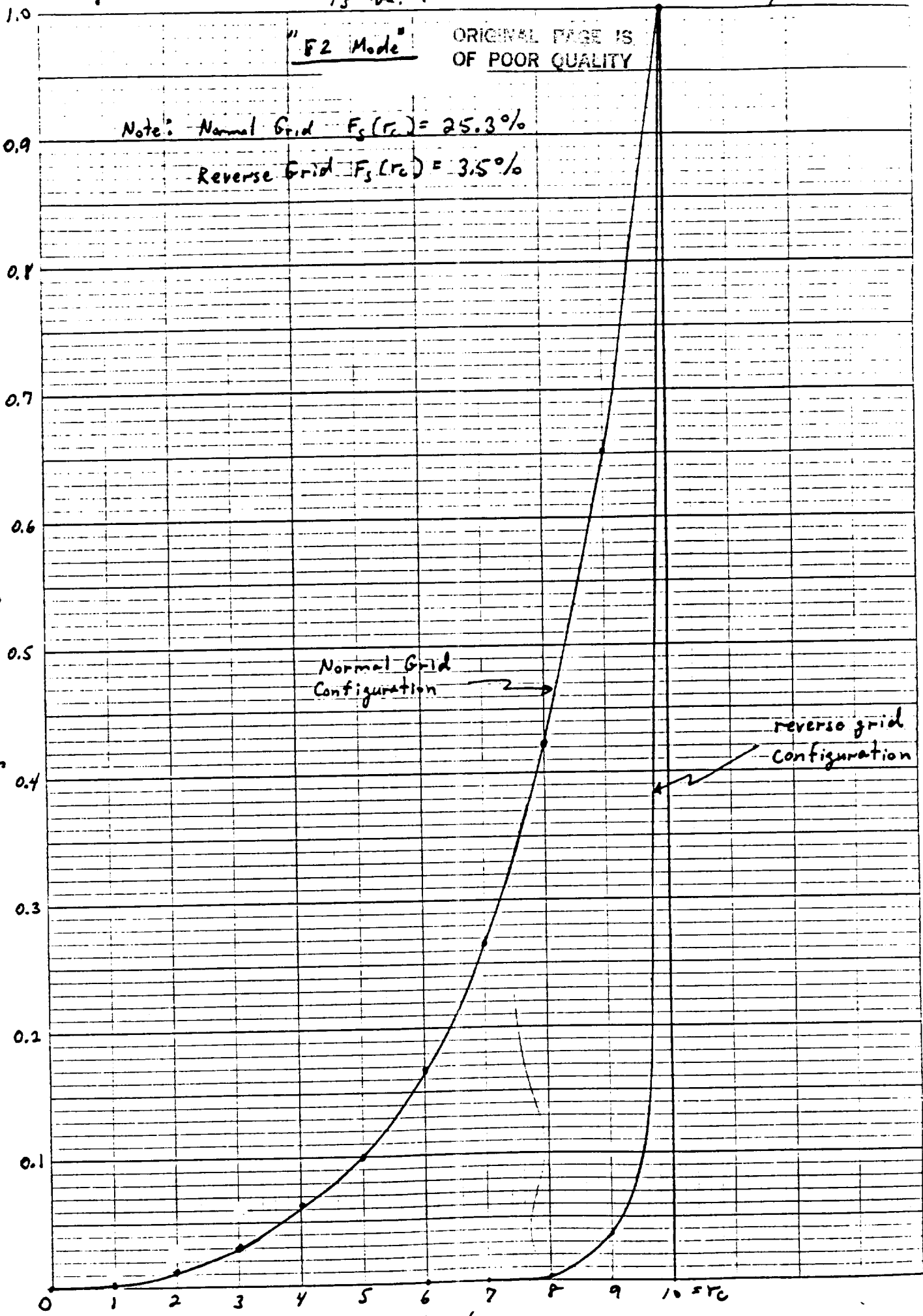
Note: Normal Grid $F_s(r_c) = 25.3\%$

Reverse Grid $F_s(r_c) = 3.5\%$

46 0780

10 X 10 TO THE INCHES / 10 INCHES
KEUFFEL & ESSER CO. MADE IN U.S.A.

$$\frac{F_s(r)}{F_s(r_c)} = F_s(r) / F_s(r_c)$$

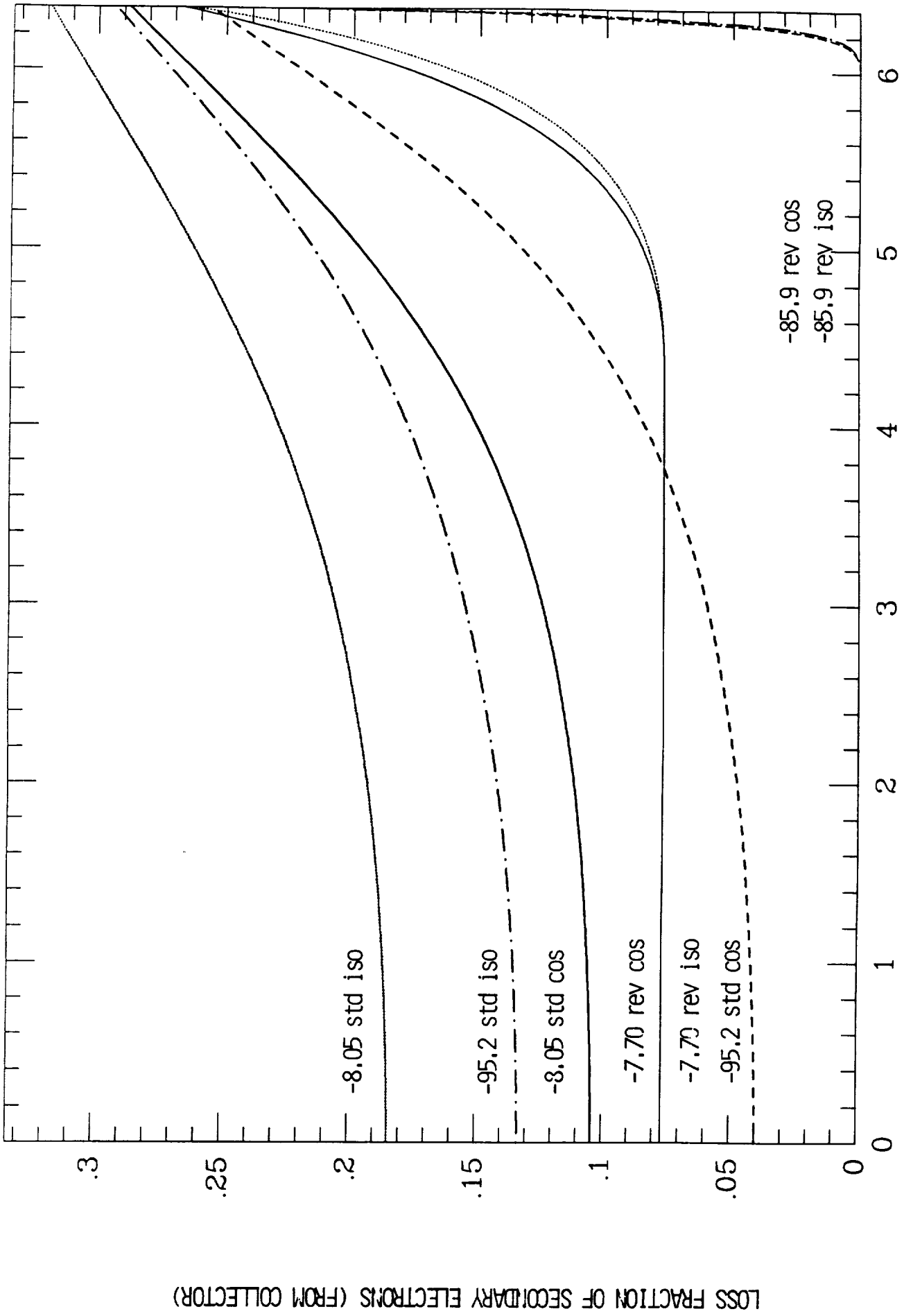


Normal Grid Configuration

reverse grid Configuration

Figure 14

r in units of Δr



RADIAL DISTANCE FROM CENTER OF COLLECTOR PLATE (SIDE SENSOR) (cm)

Figure 15

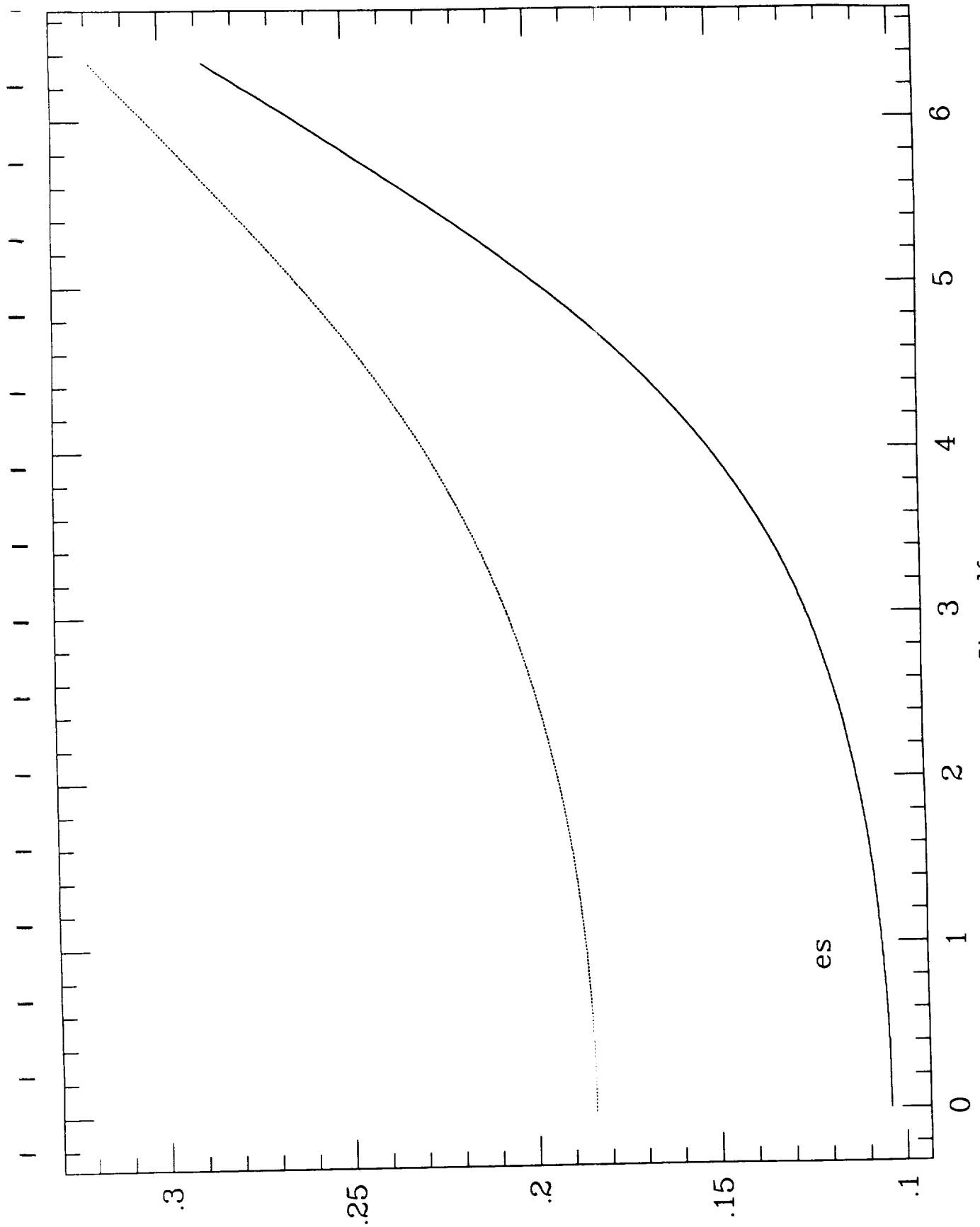


Figure 16

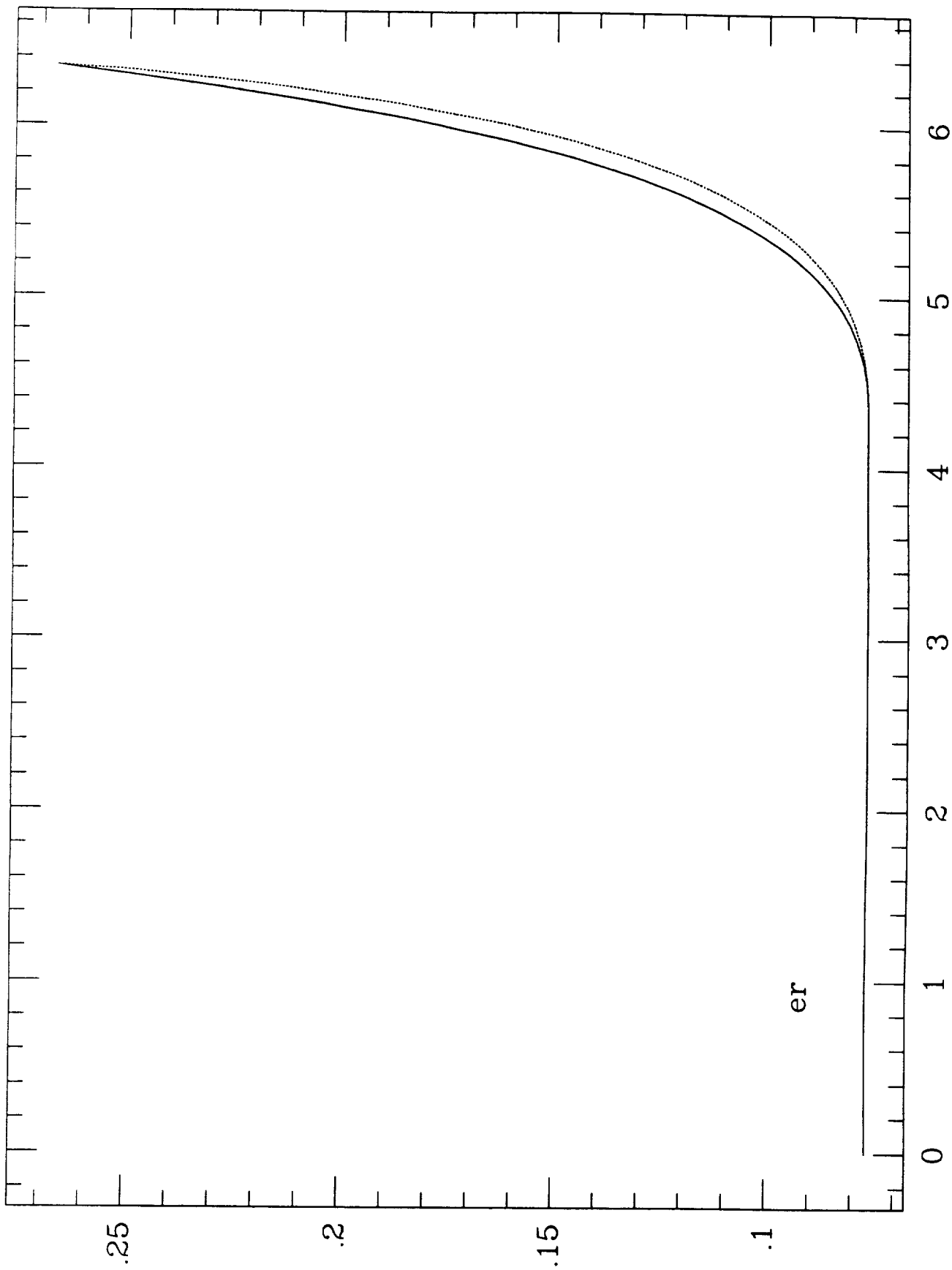


Figure 17

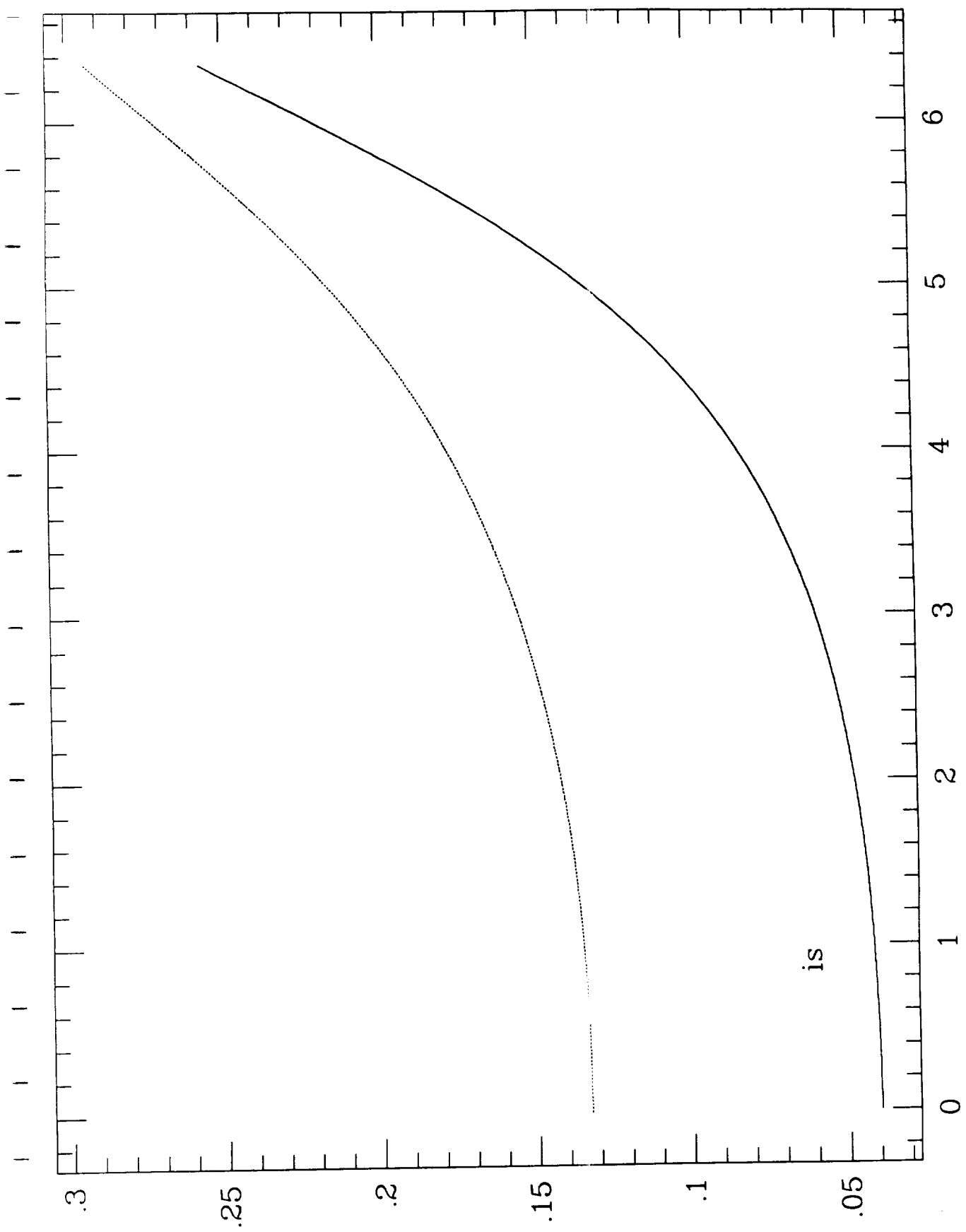


Figure 18

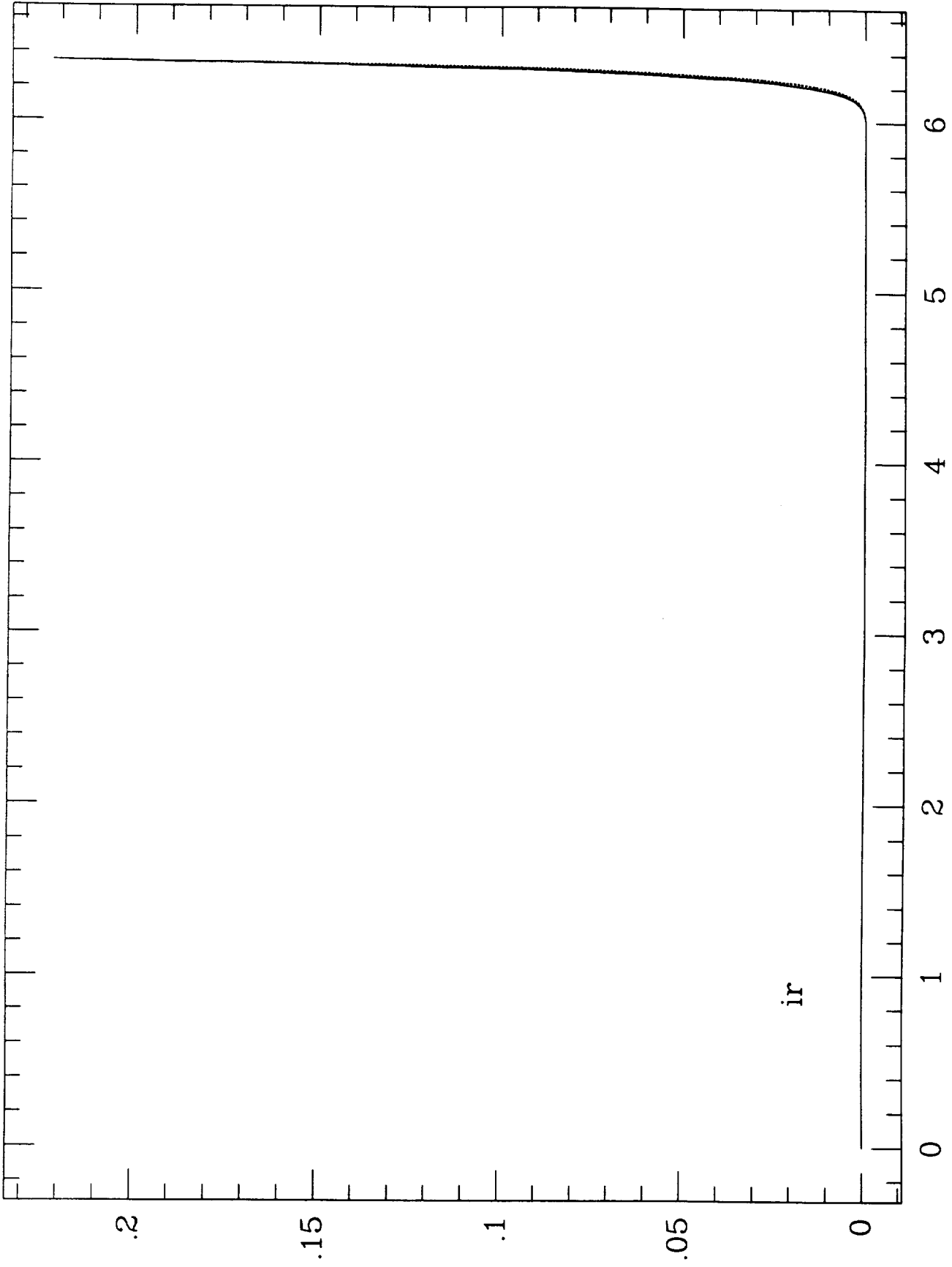


Figure 19

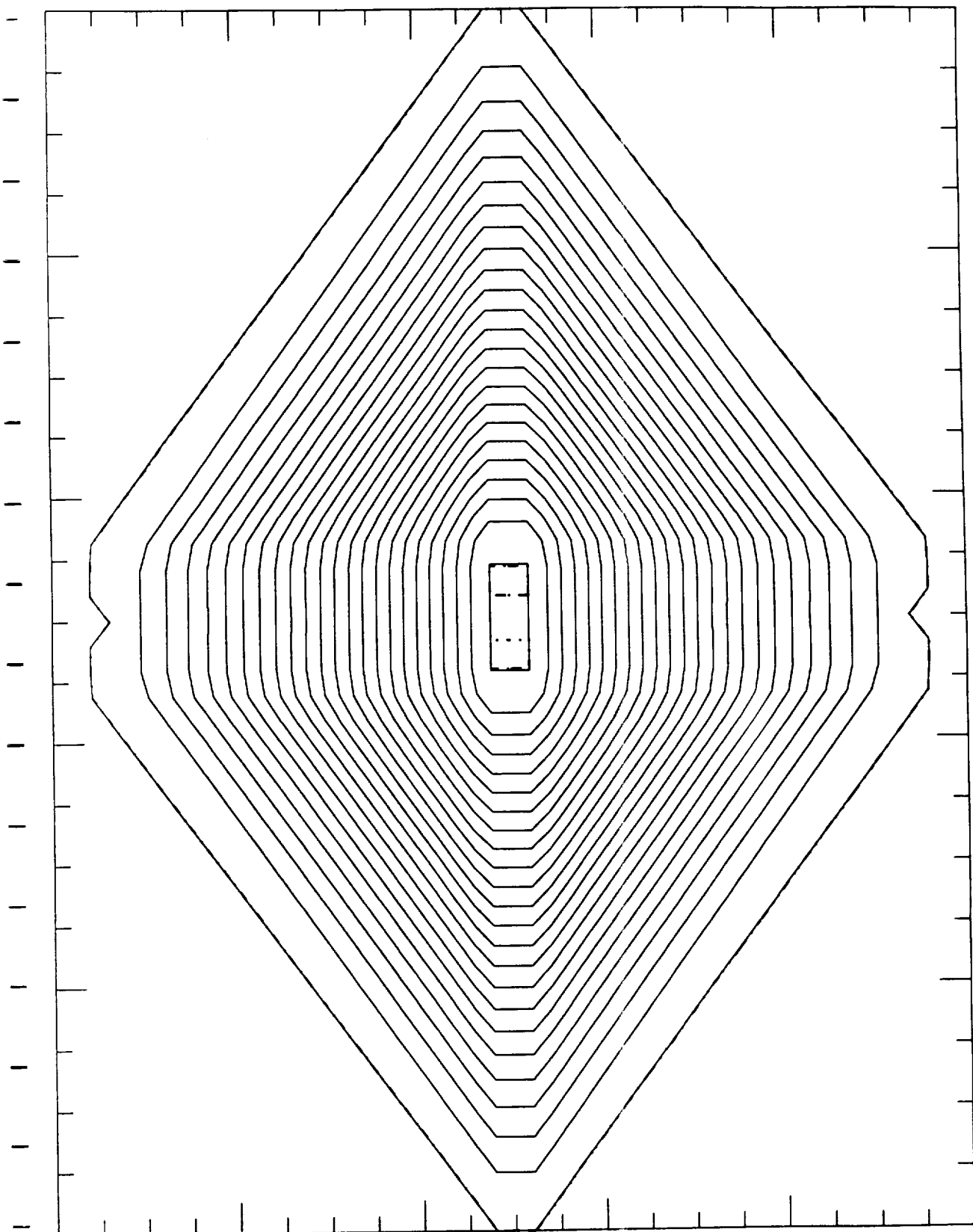
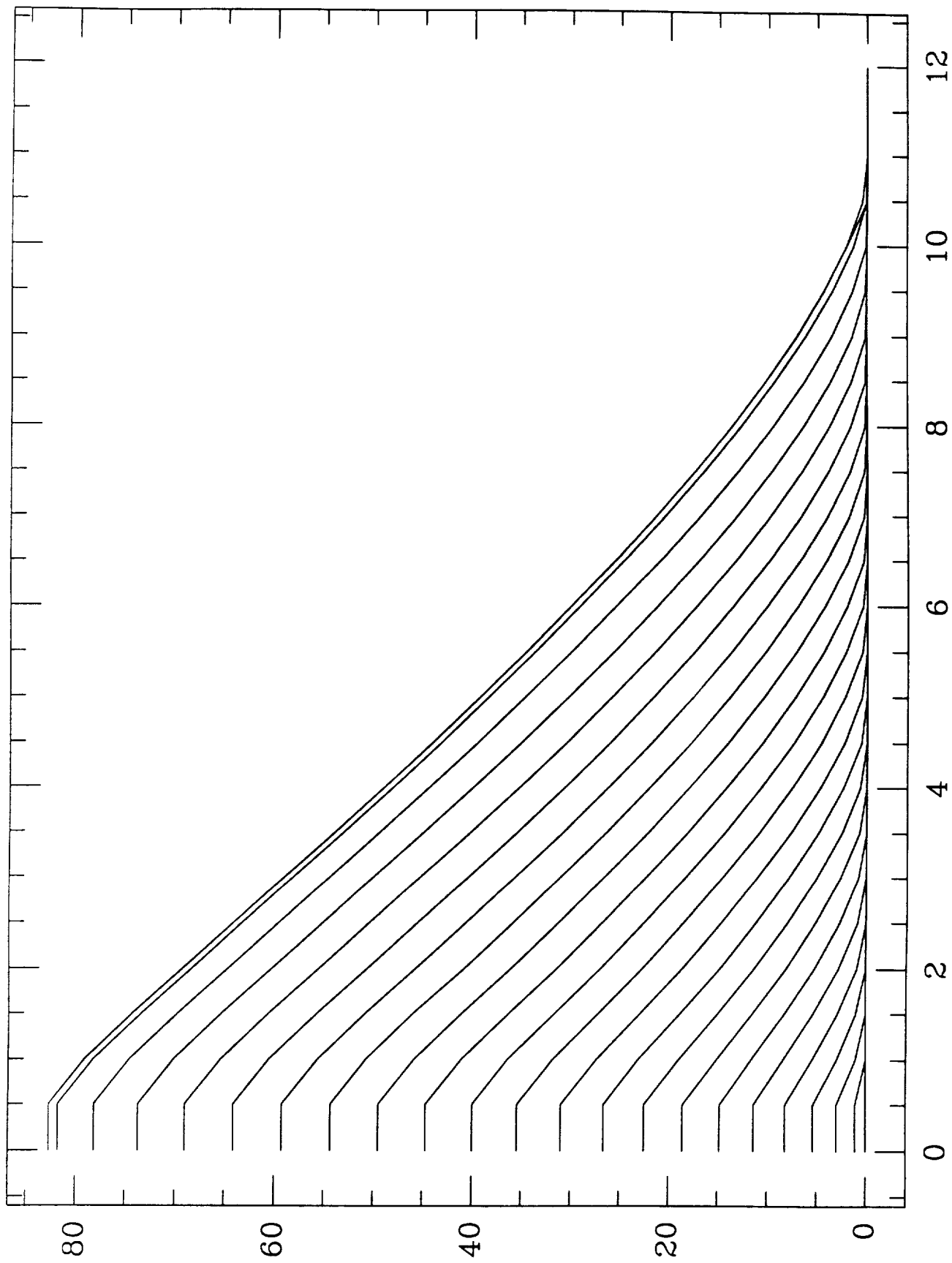


Figure 20

are



ar1

Figure 21

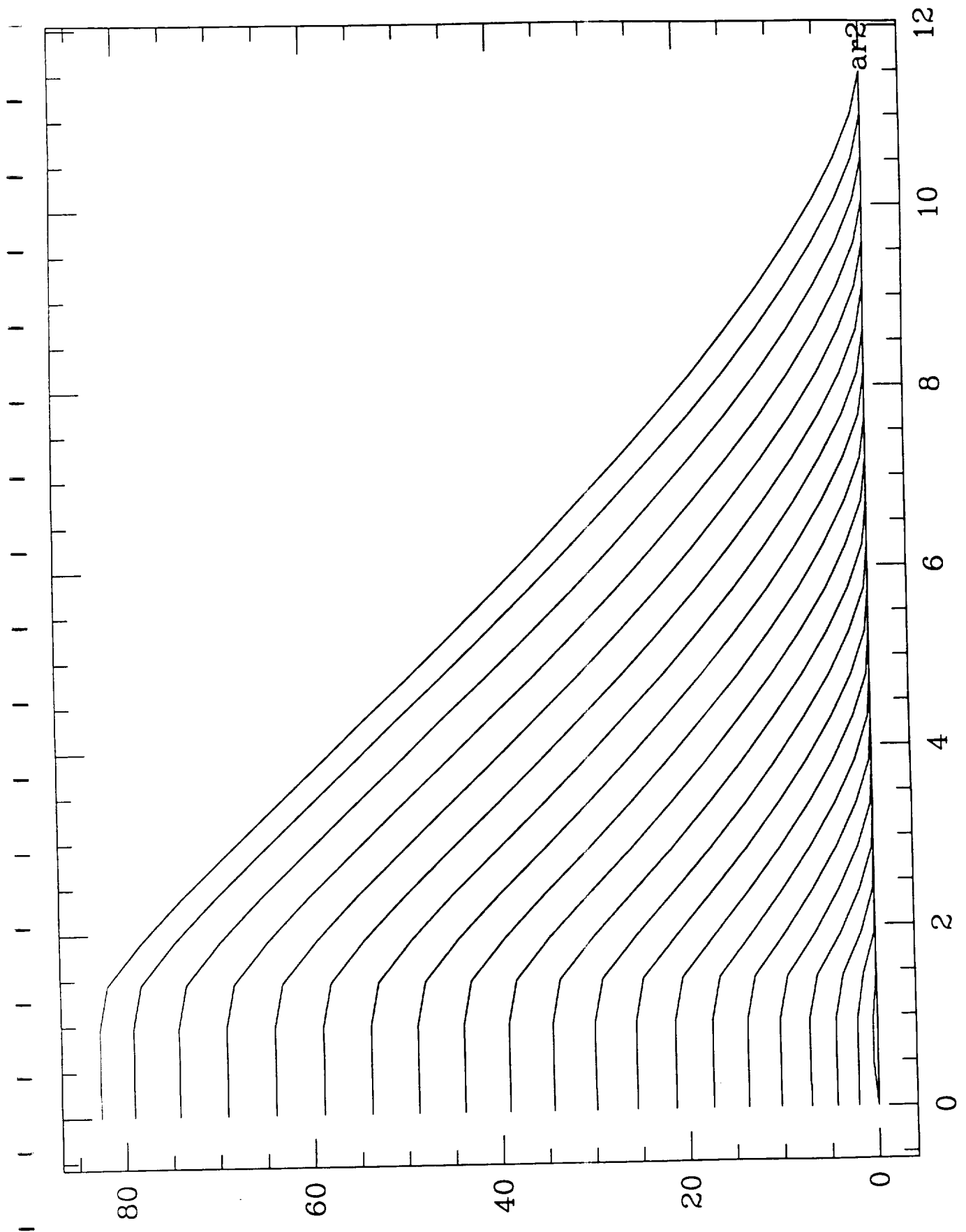
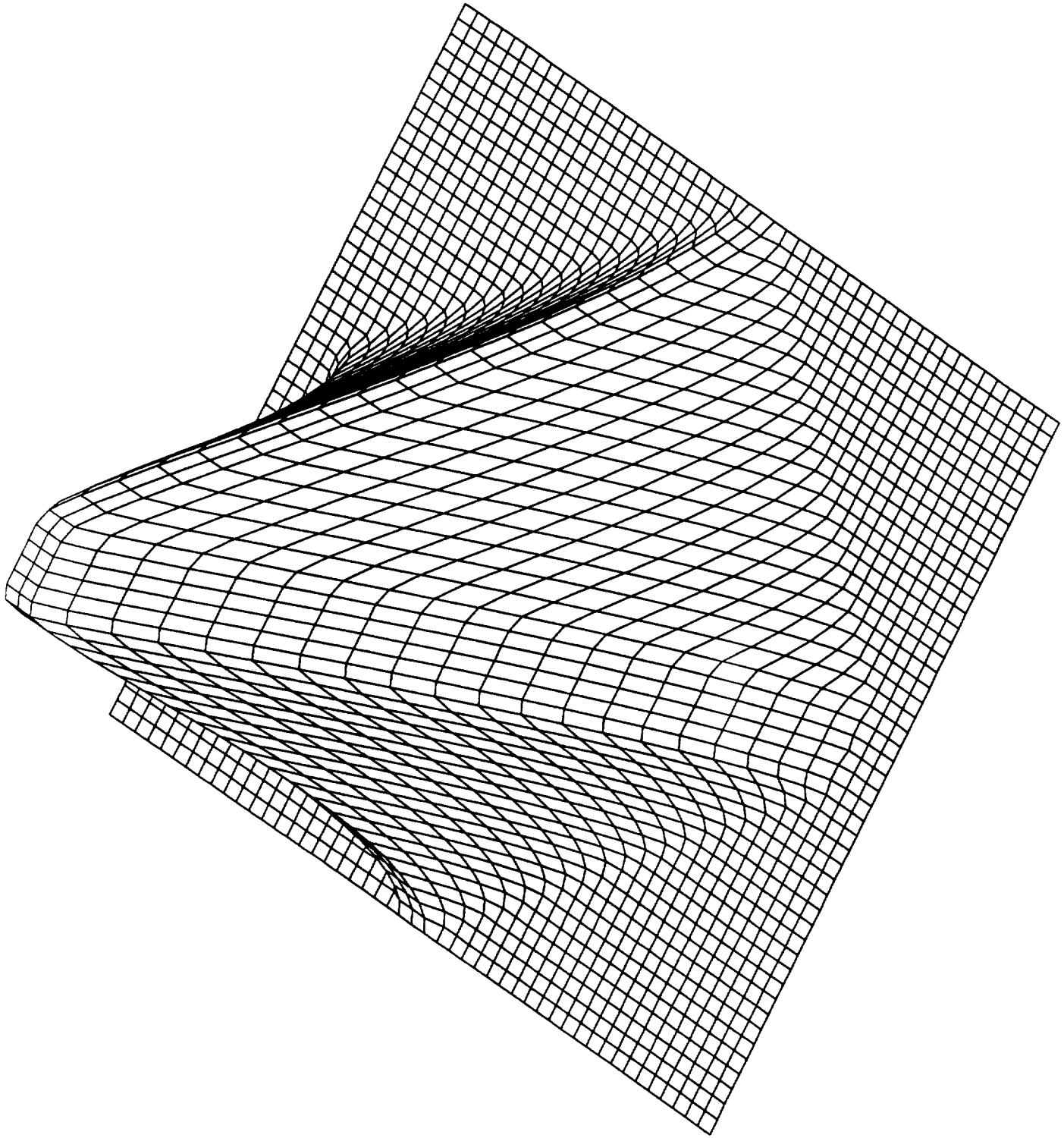
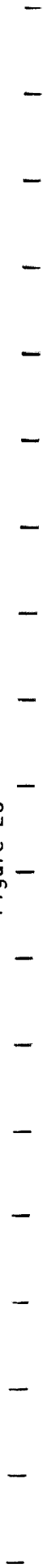


Figure 22



2140
0.05 -8 55 60

Figure 23



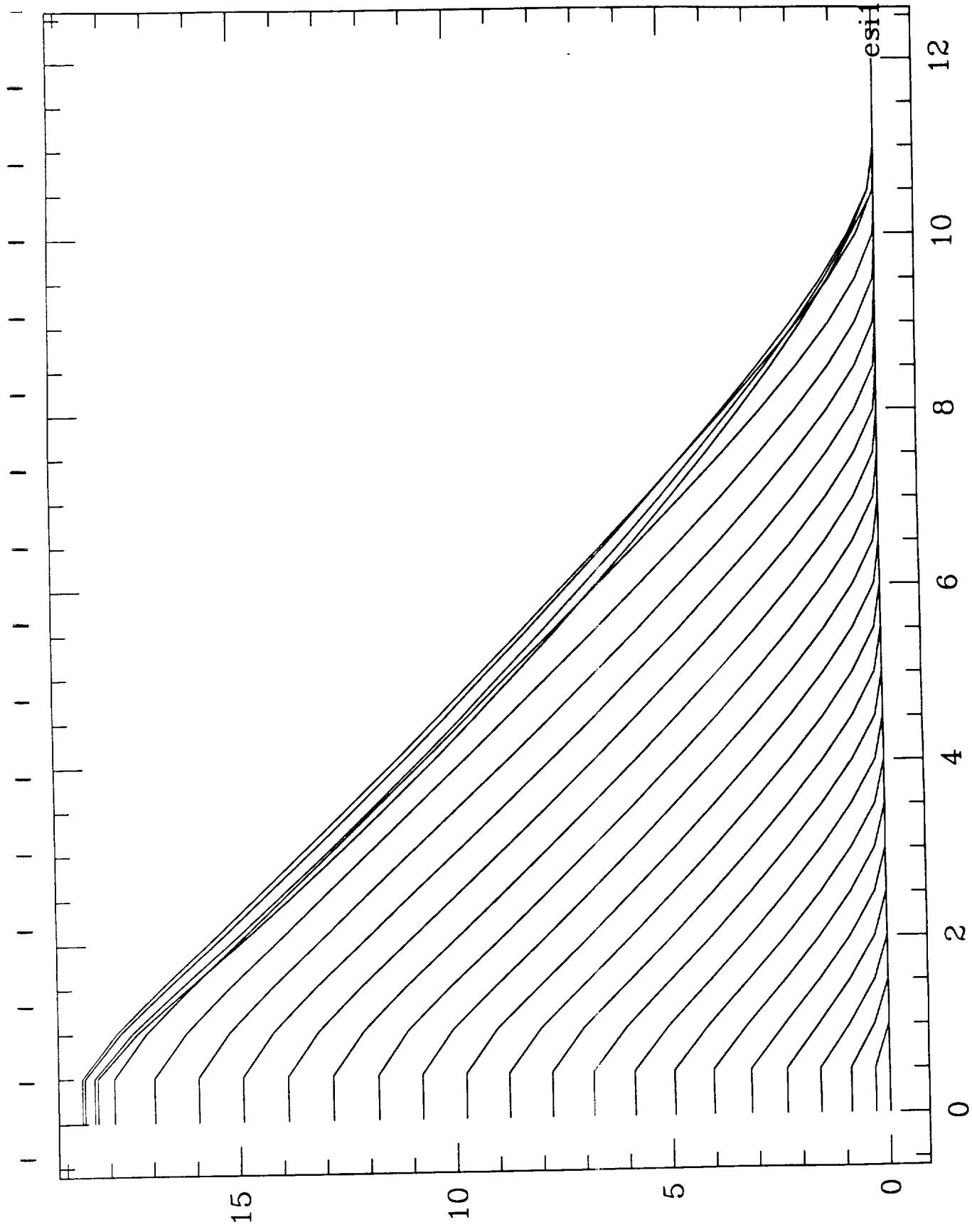


Figure 24

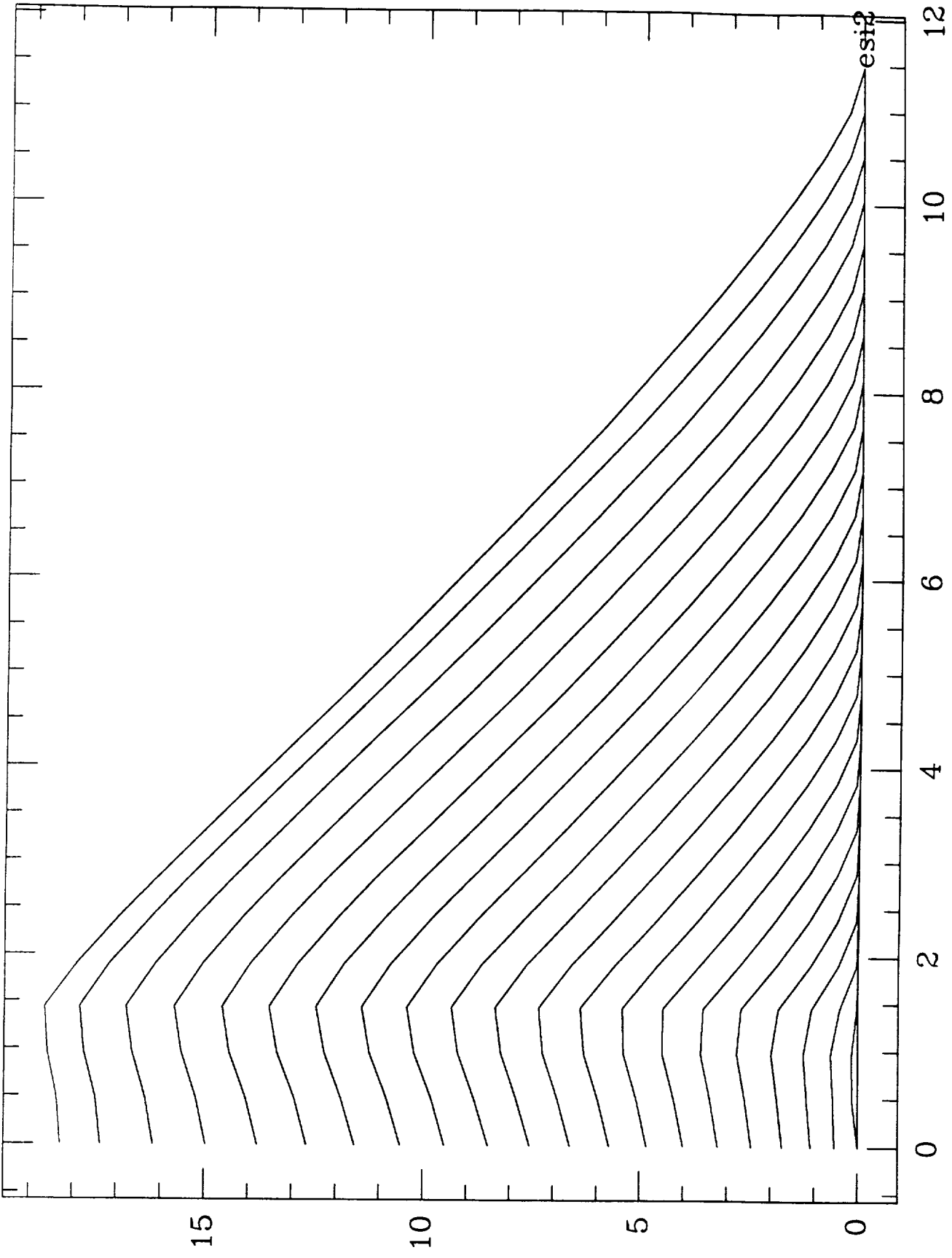


Figure 25



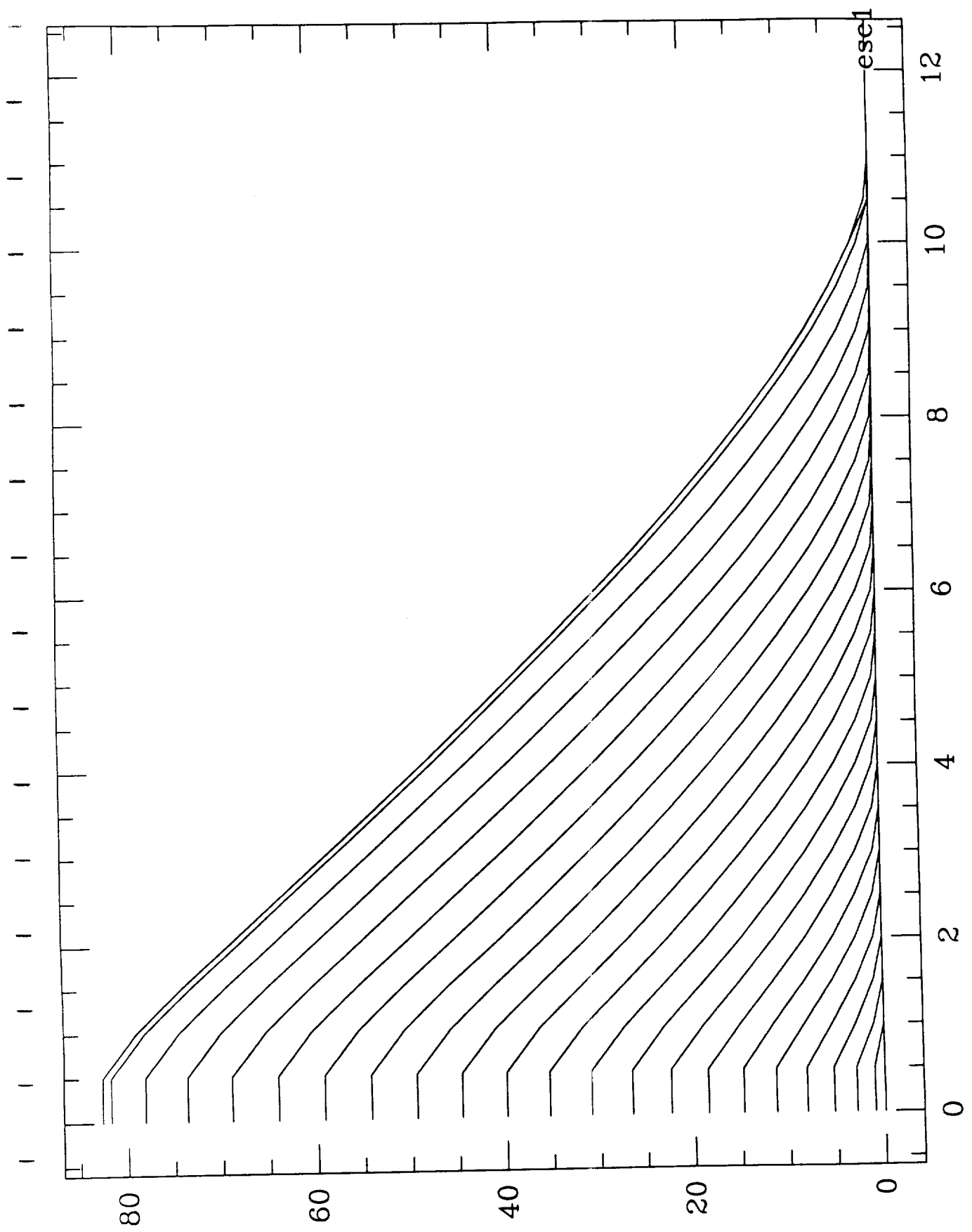


Figure 26

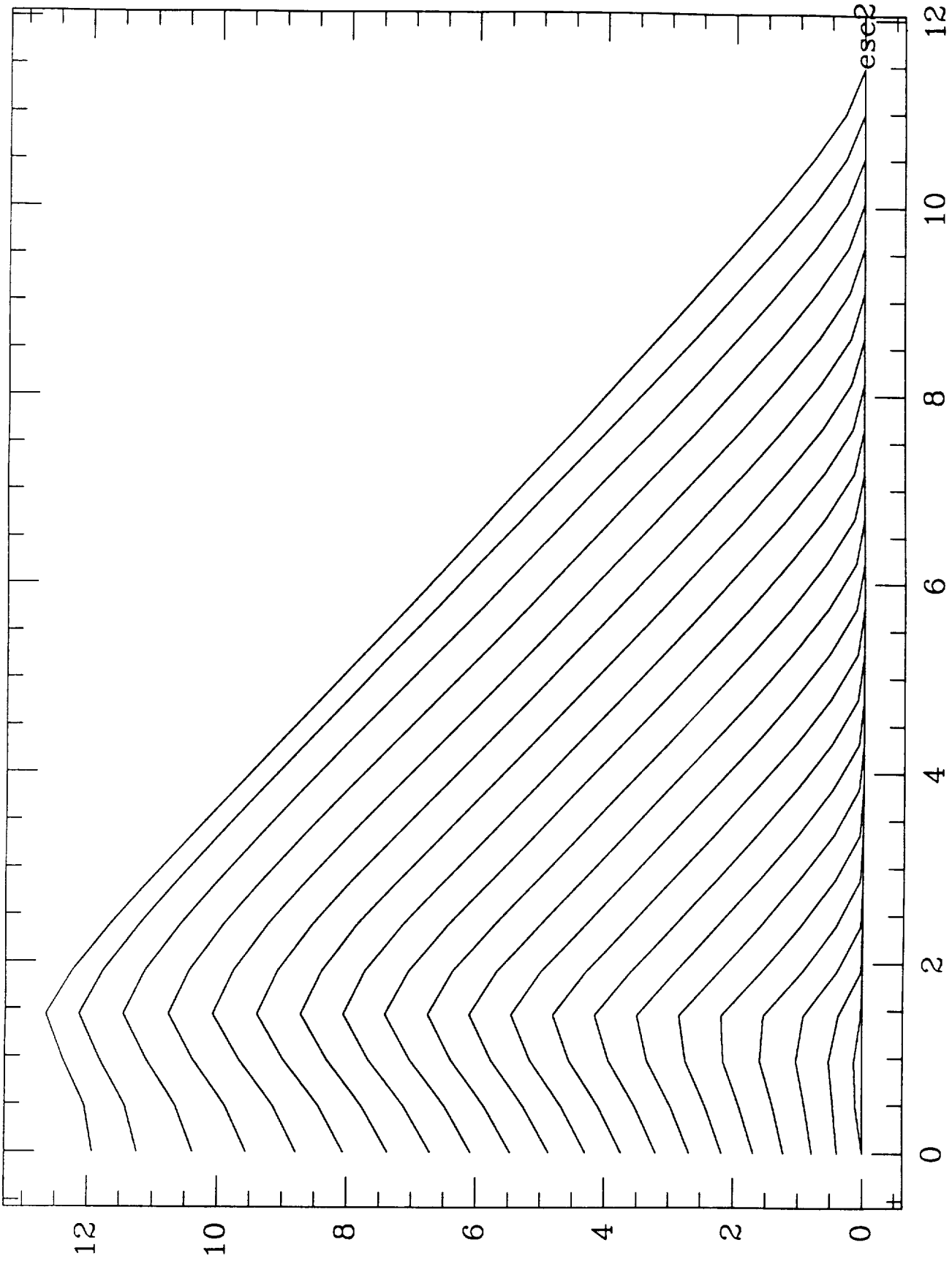
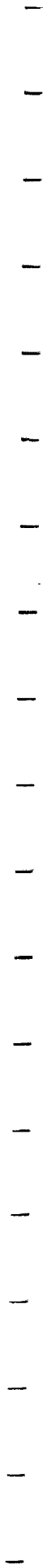


Figure 27



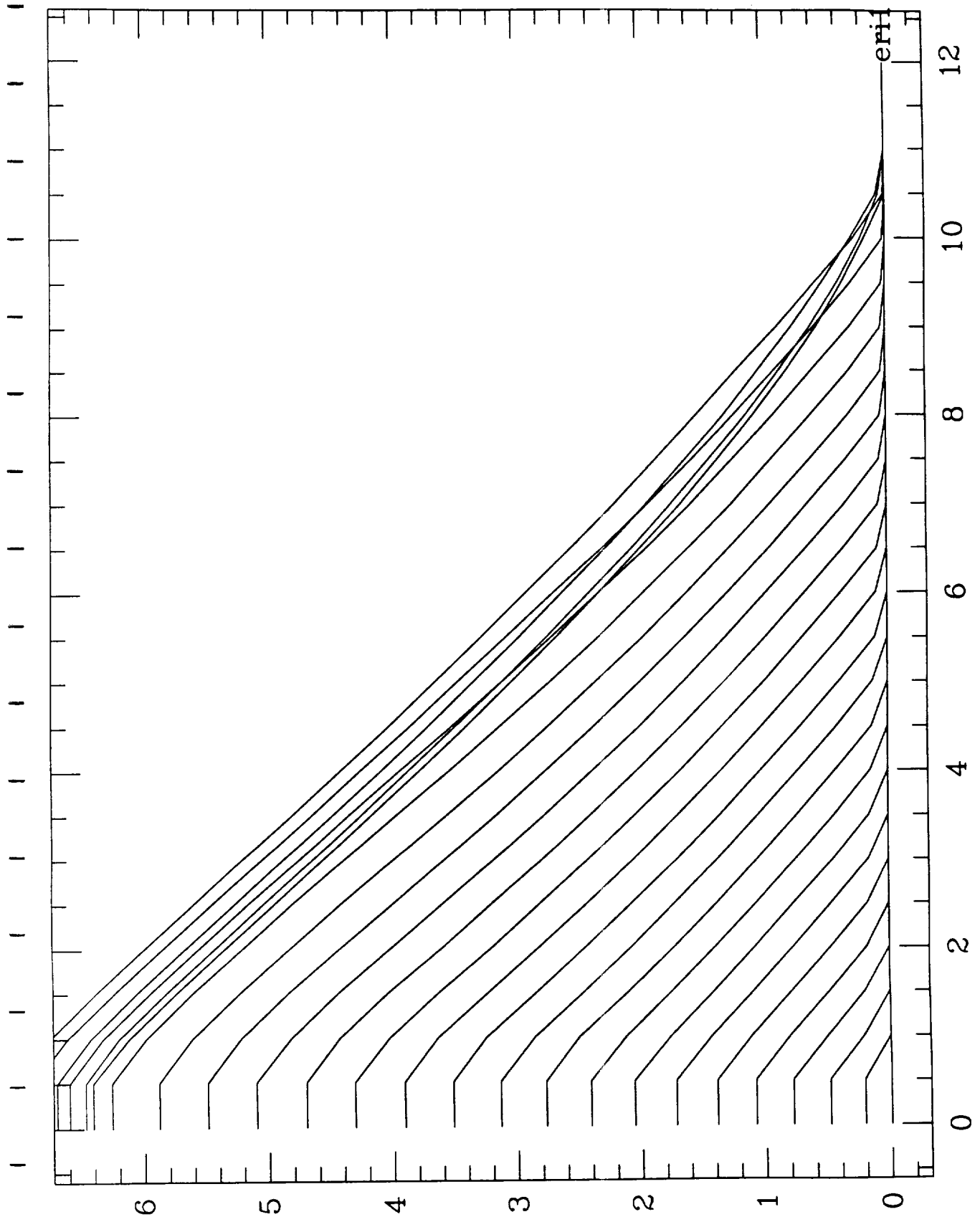


Figure 28

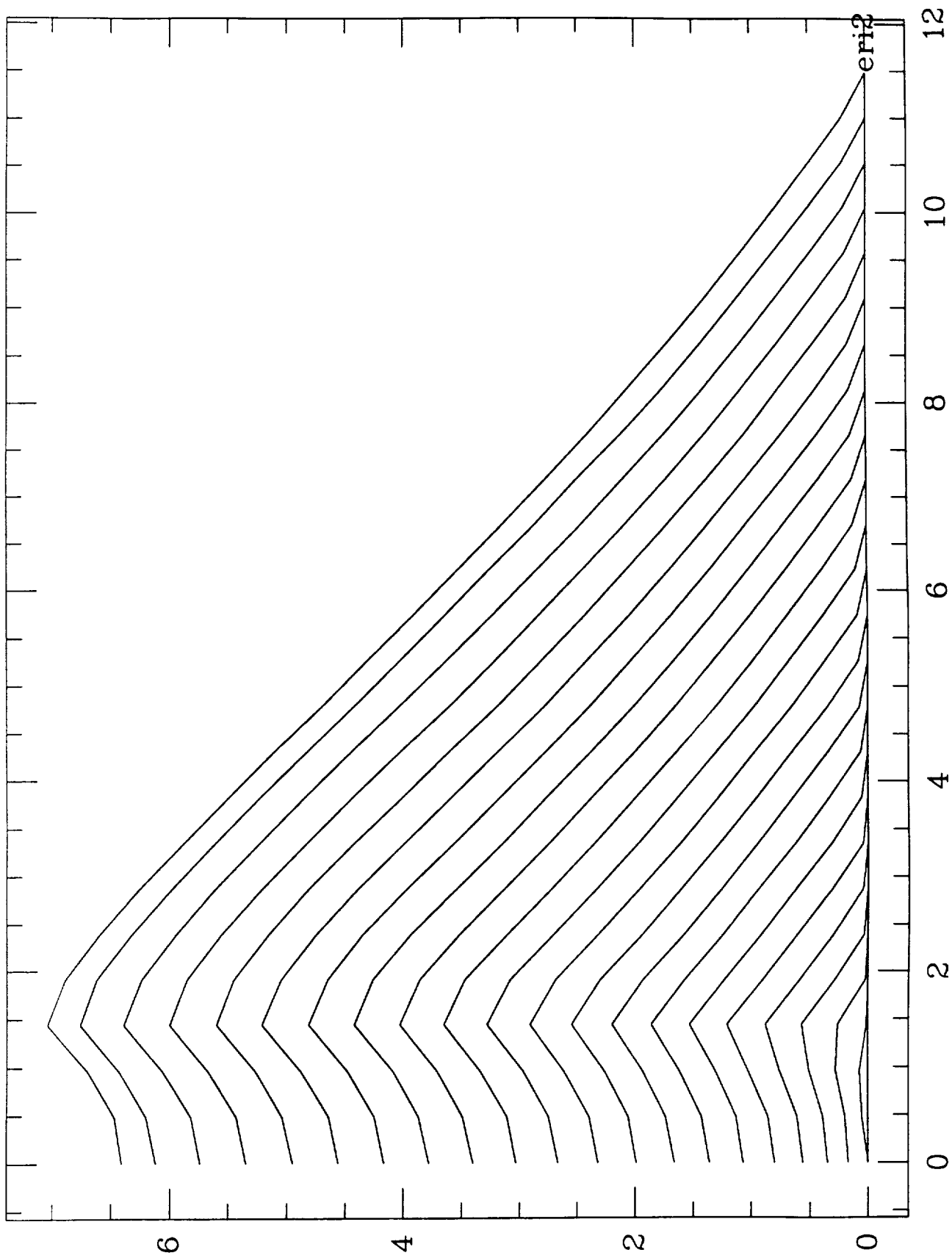


Figure 29



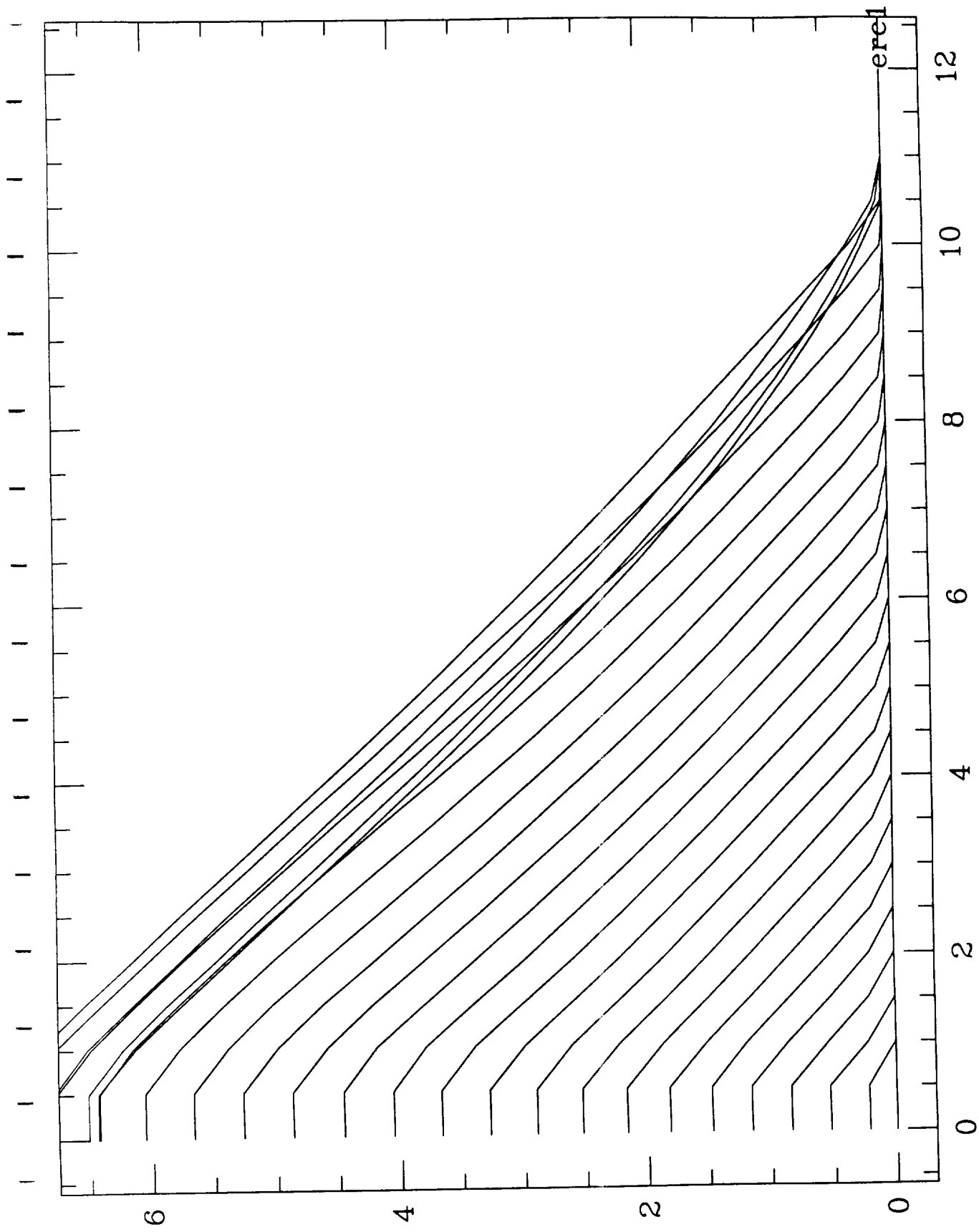


Figure 30

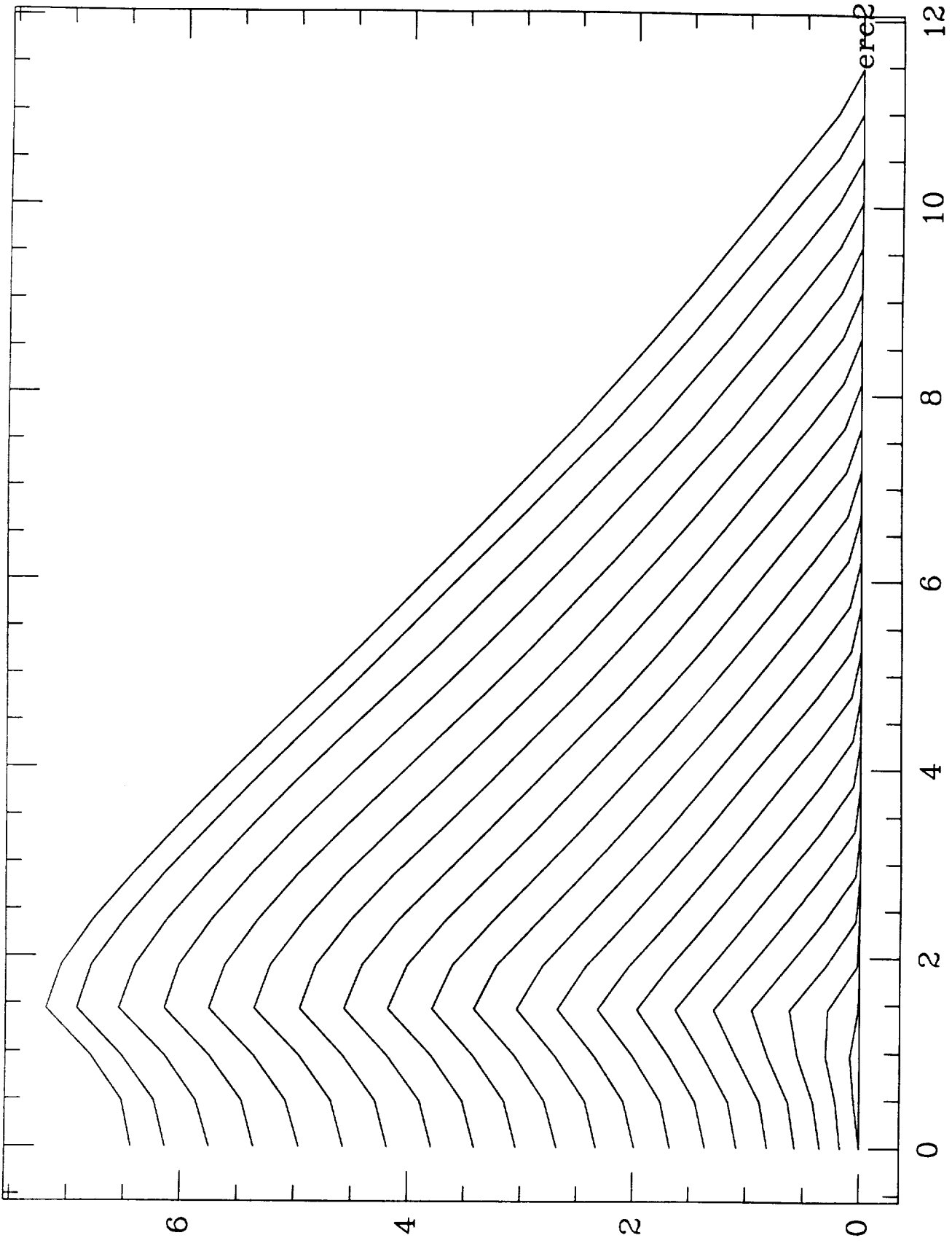


Figure 31



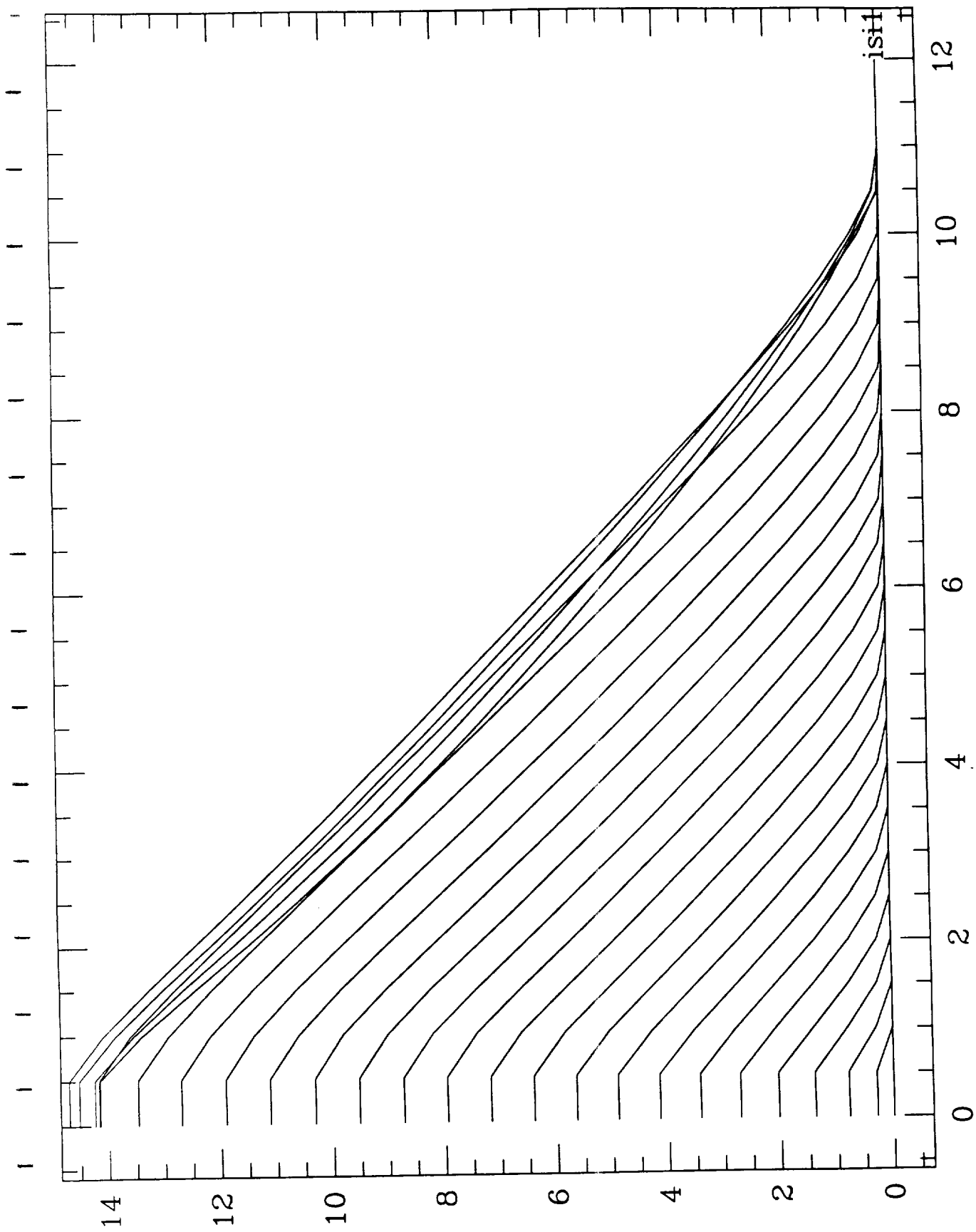


Figure 32

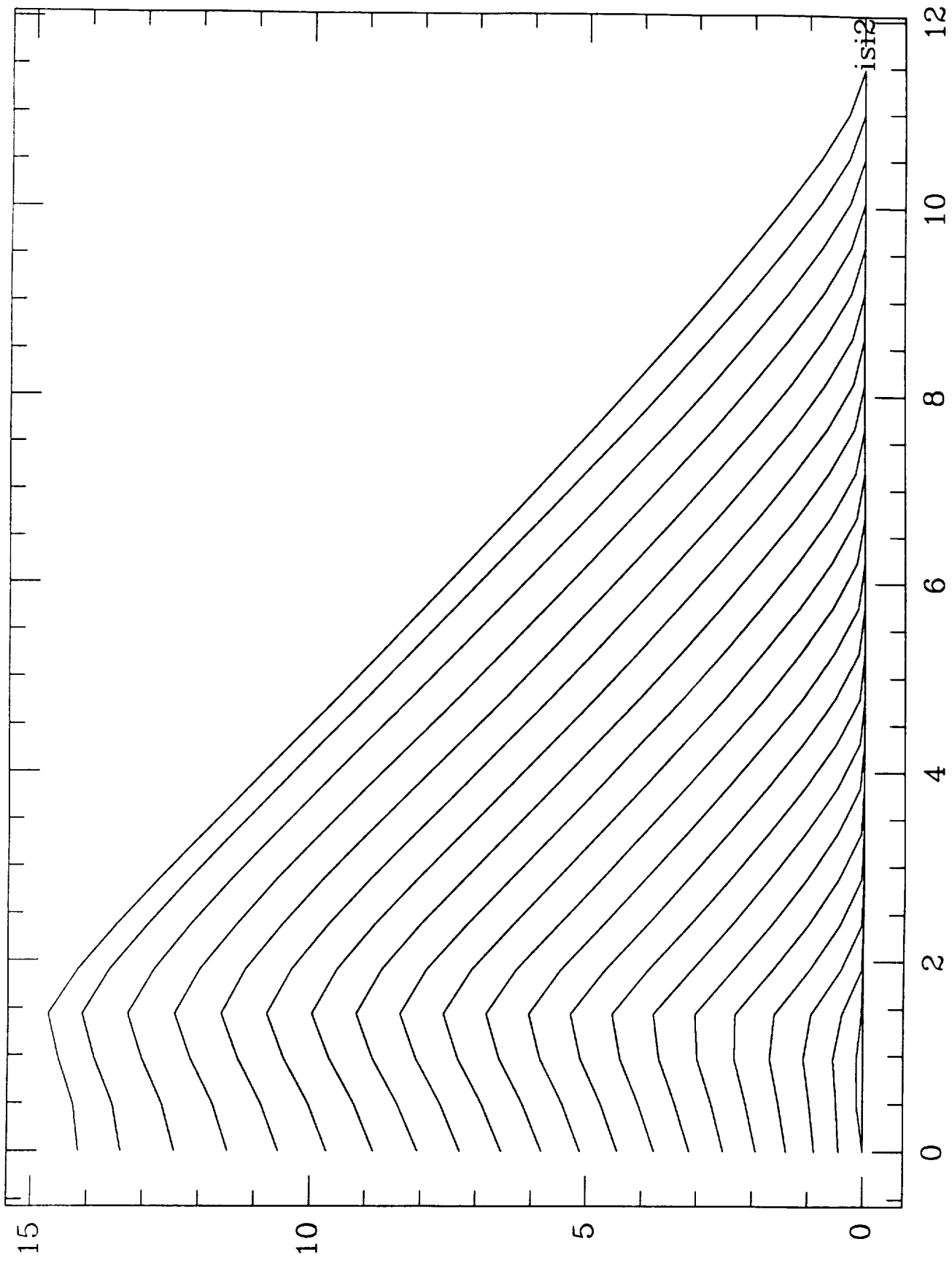


Figure 33



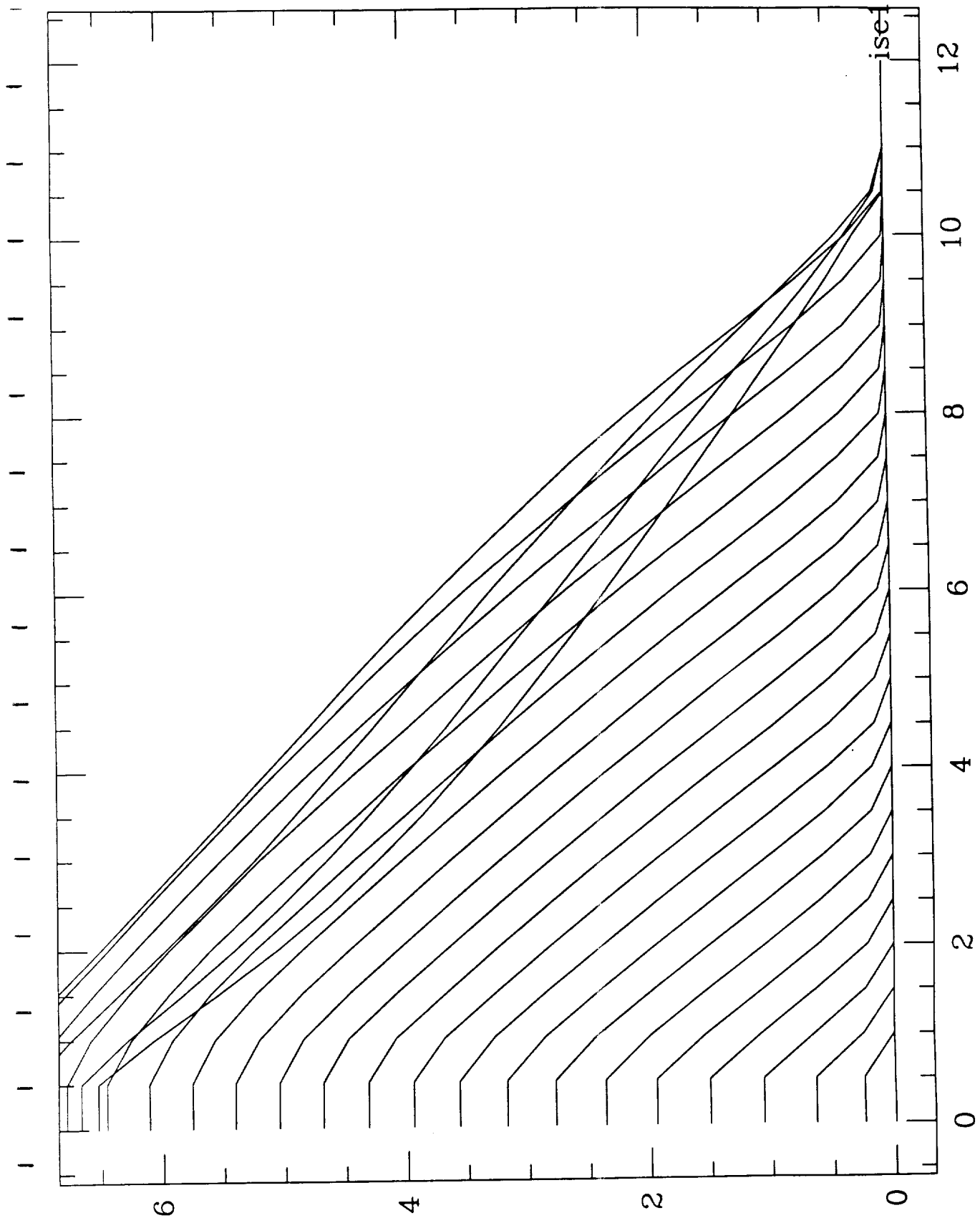


Figure 34

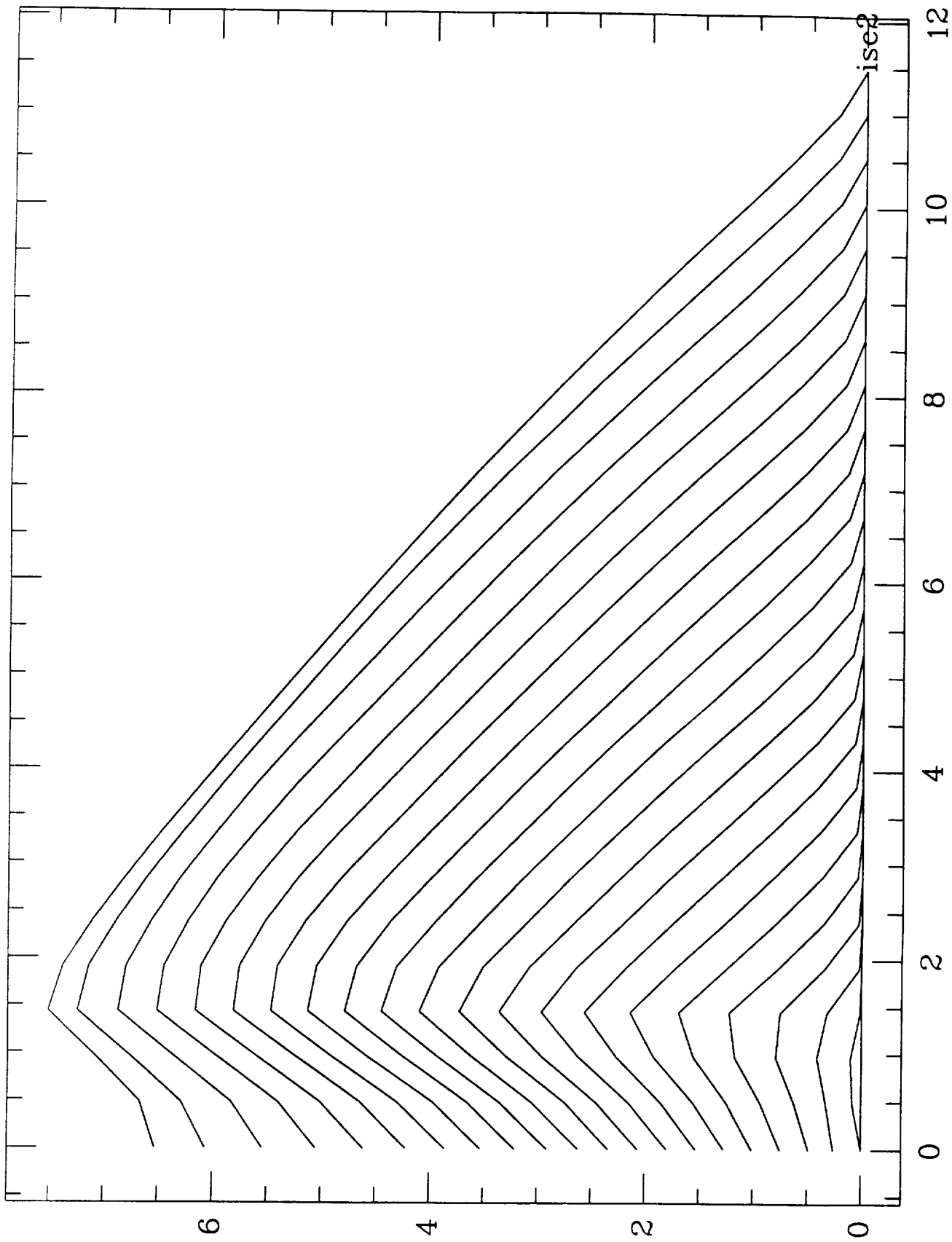


Figure 35

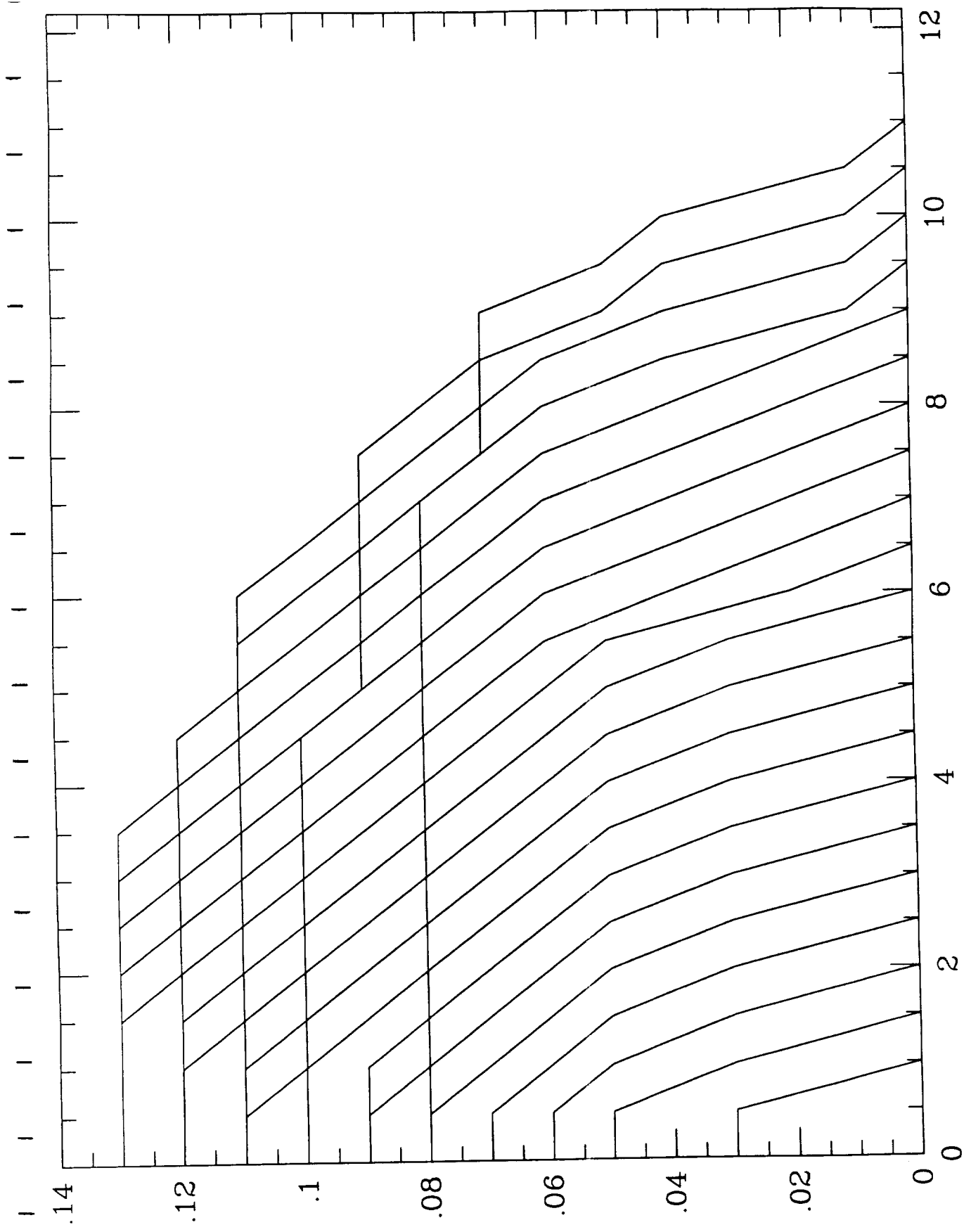


Figure 36

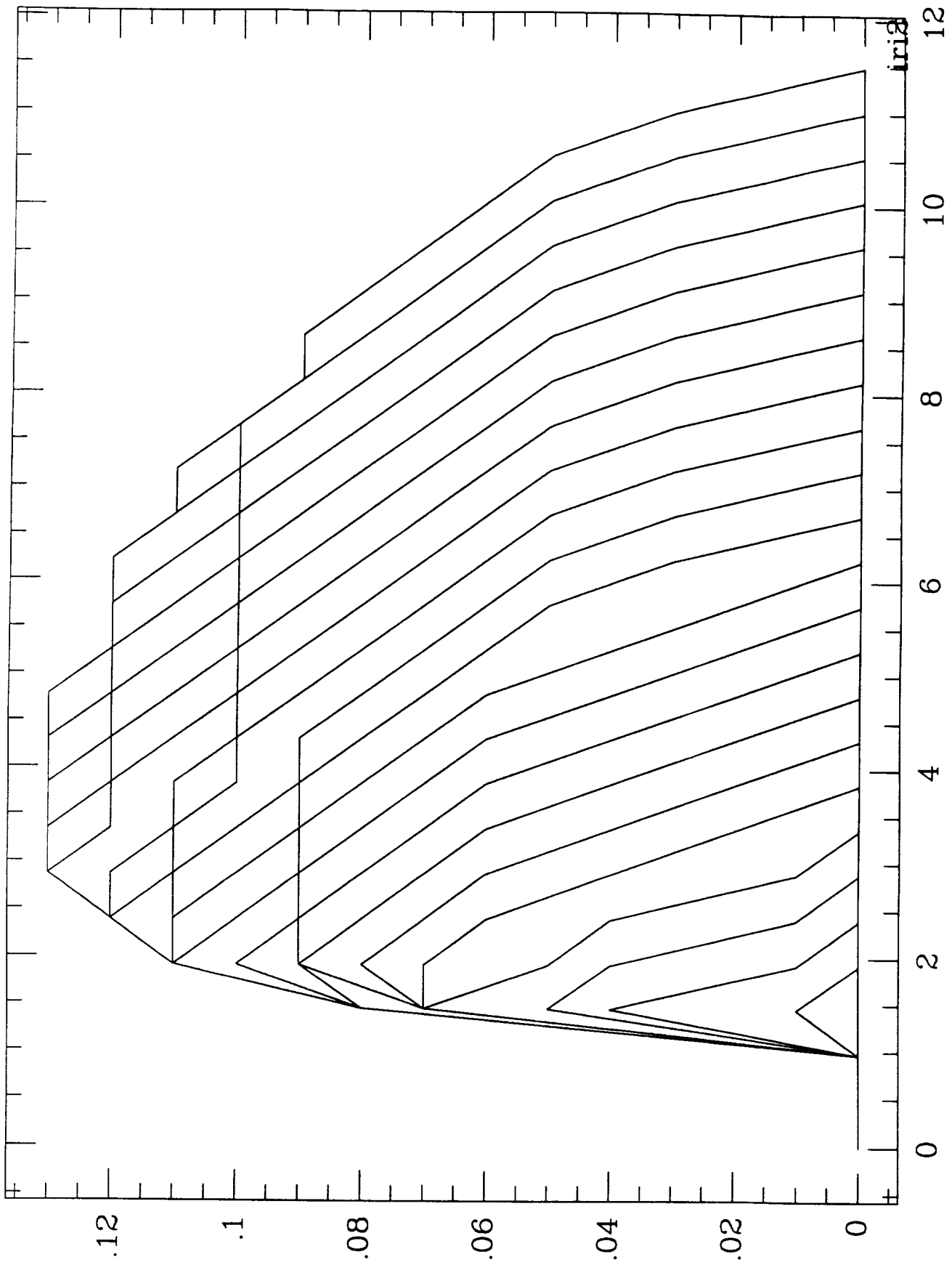


Figure 37



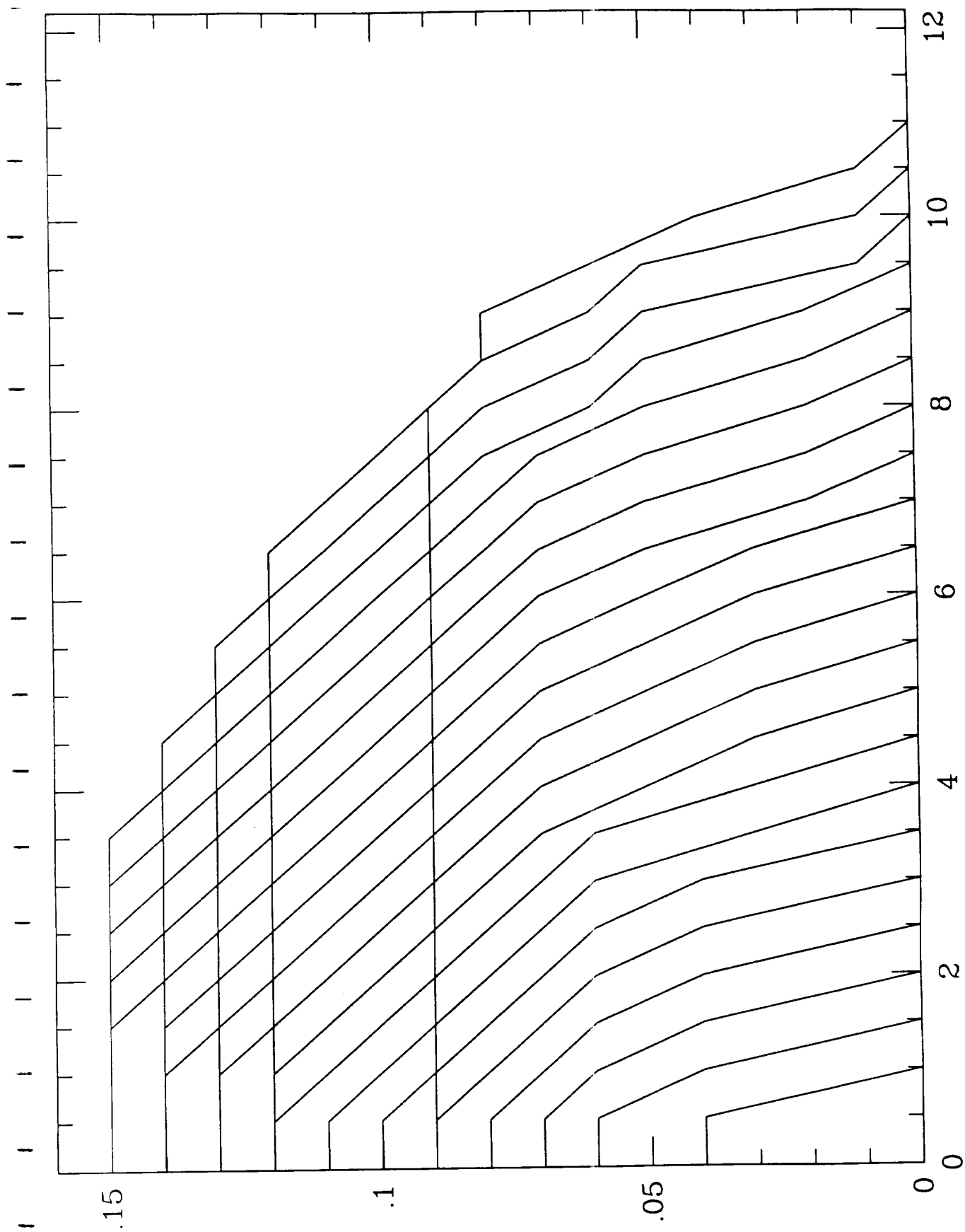


Figure 38

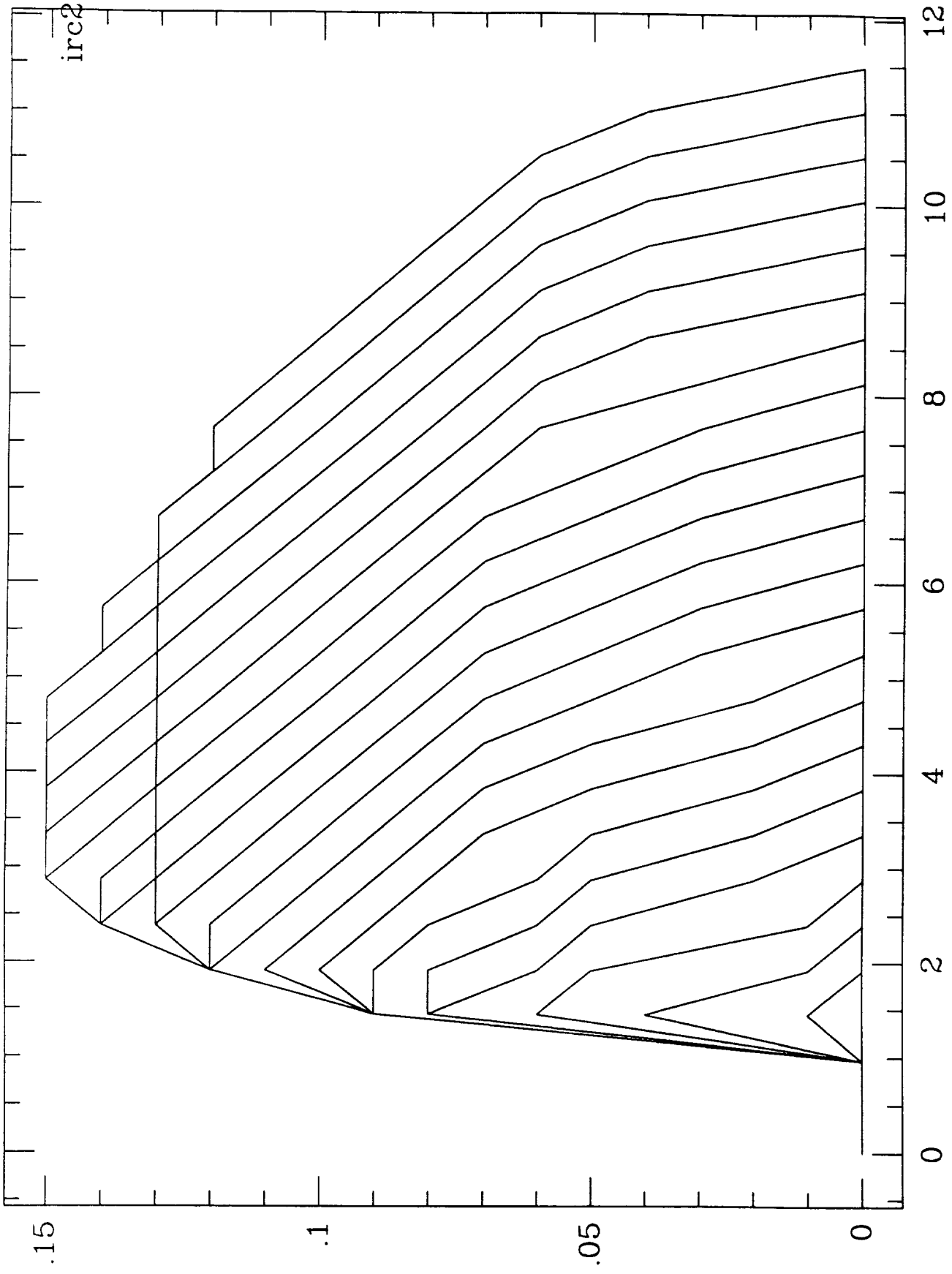


Figure 39



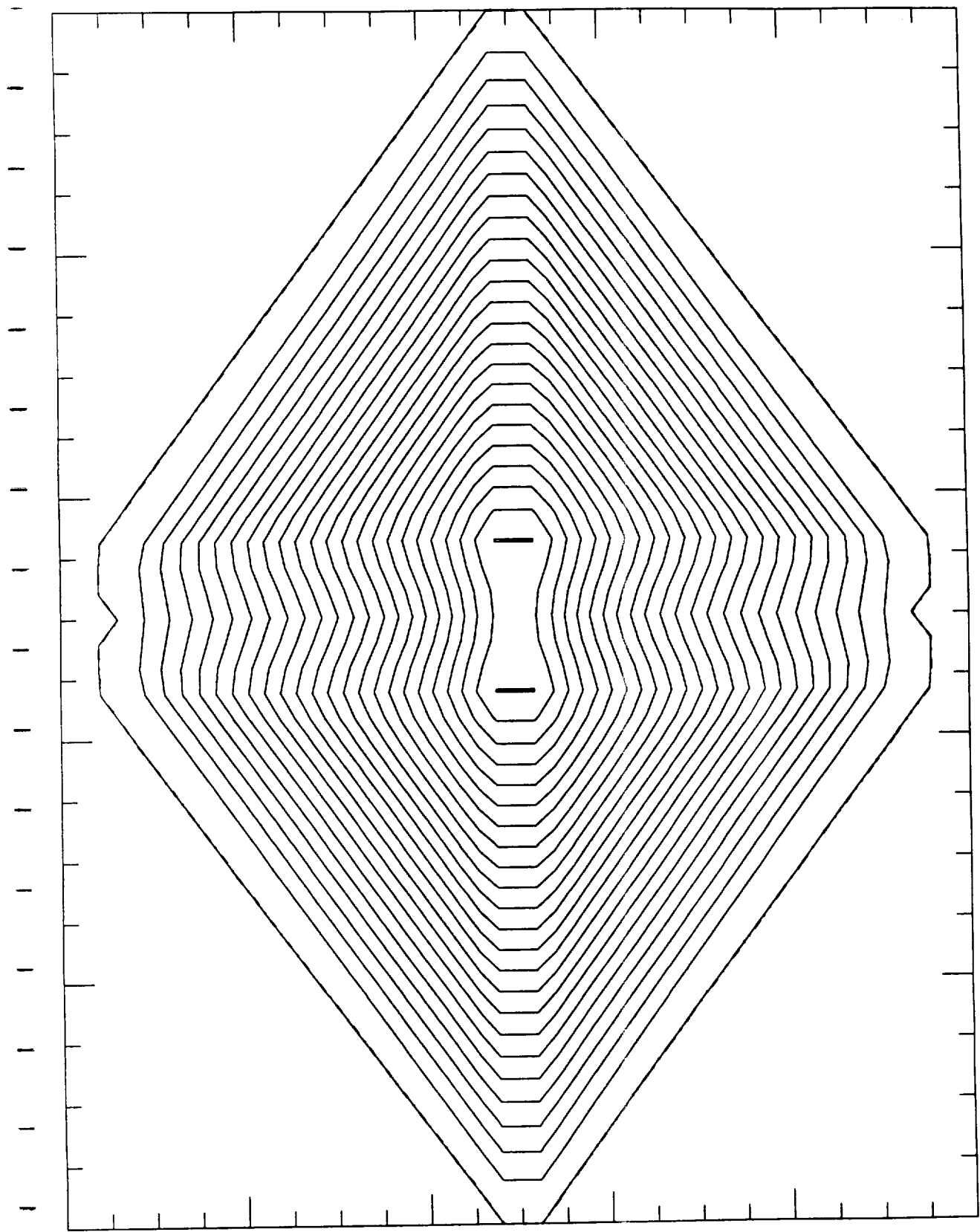


Figure 40

J S I 2
AS

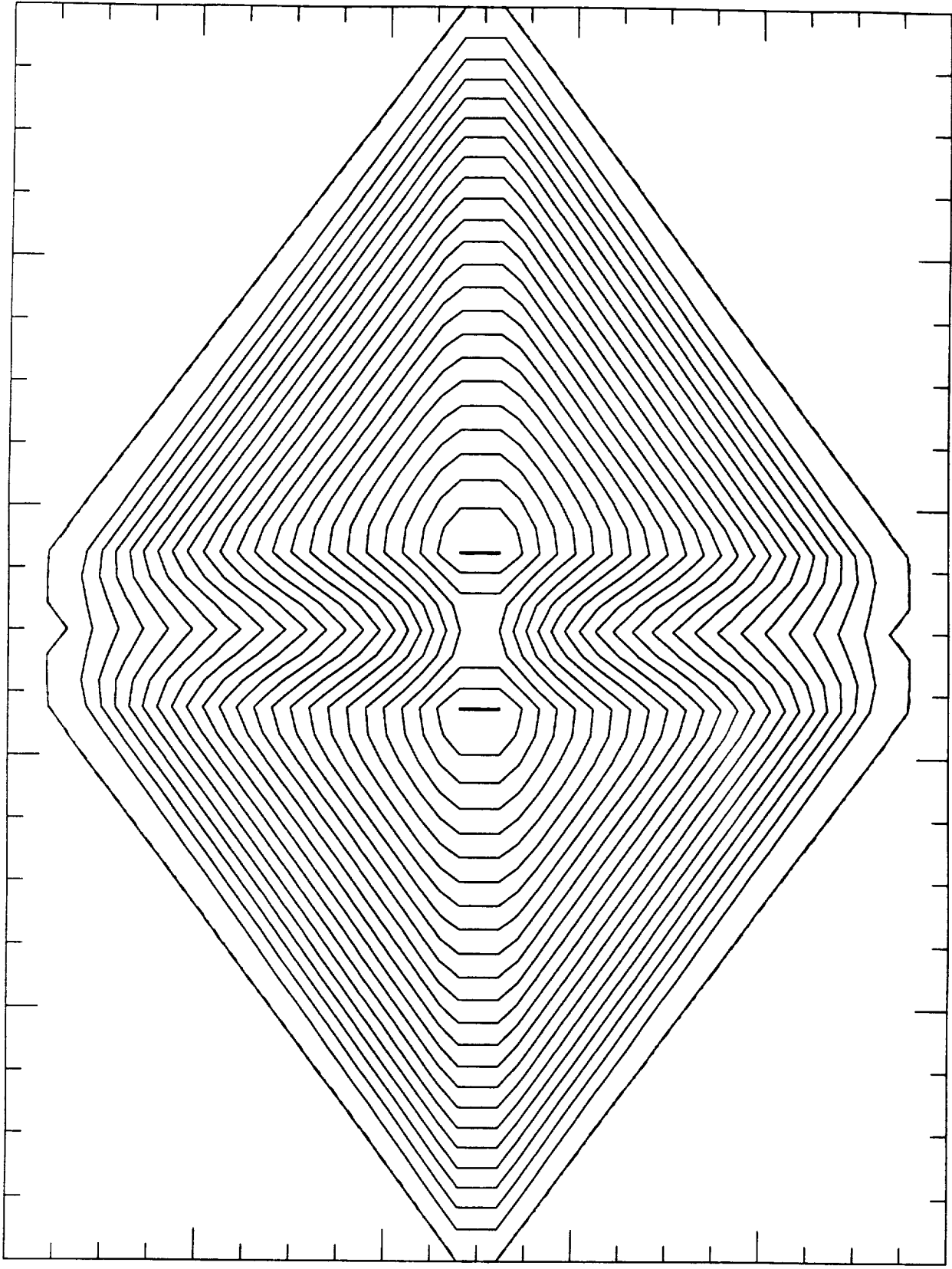


Figure 41

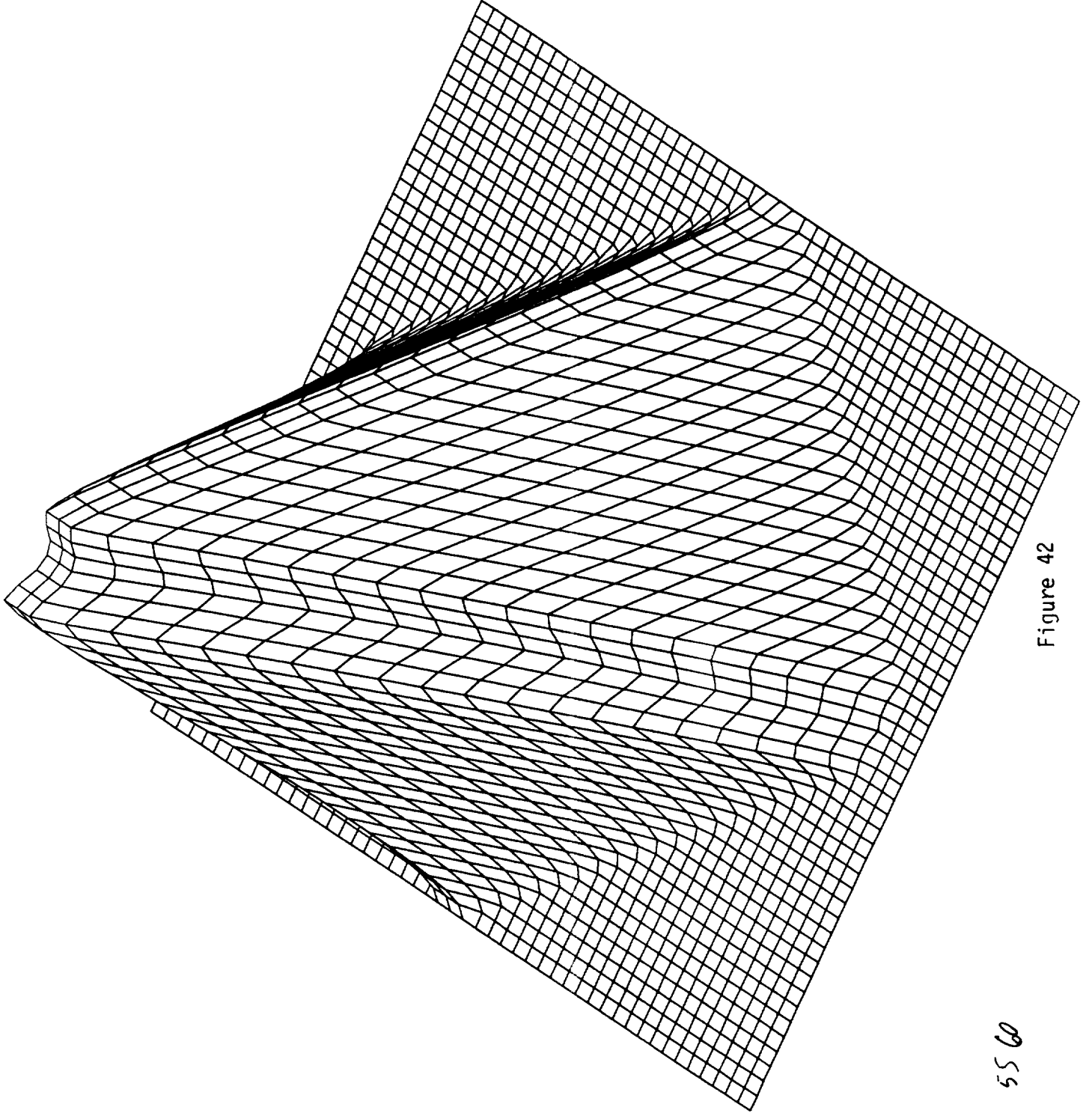


Figure 42

JSFZ 0,3 -2 55 60

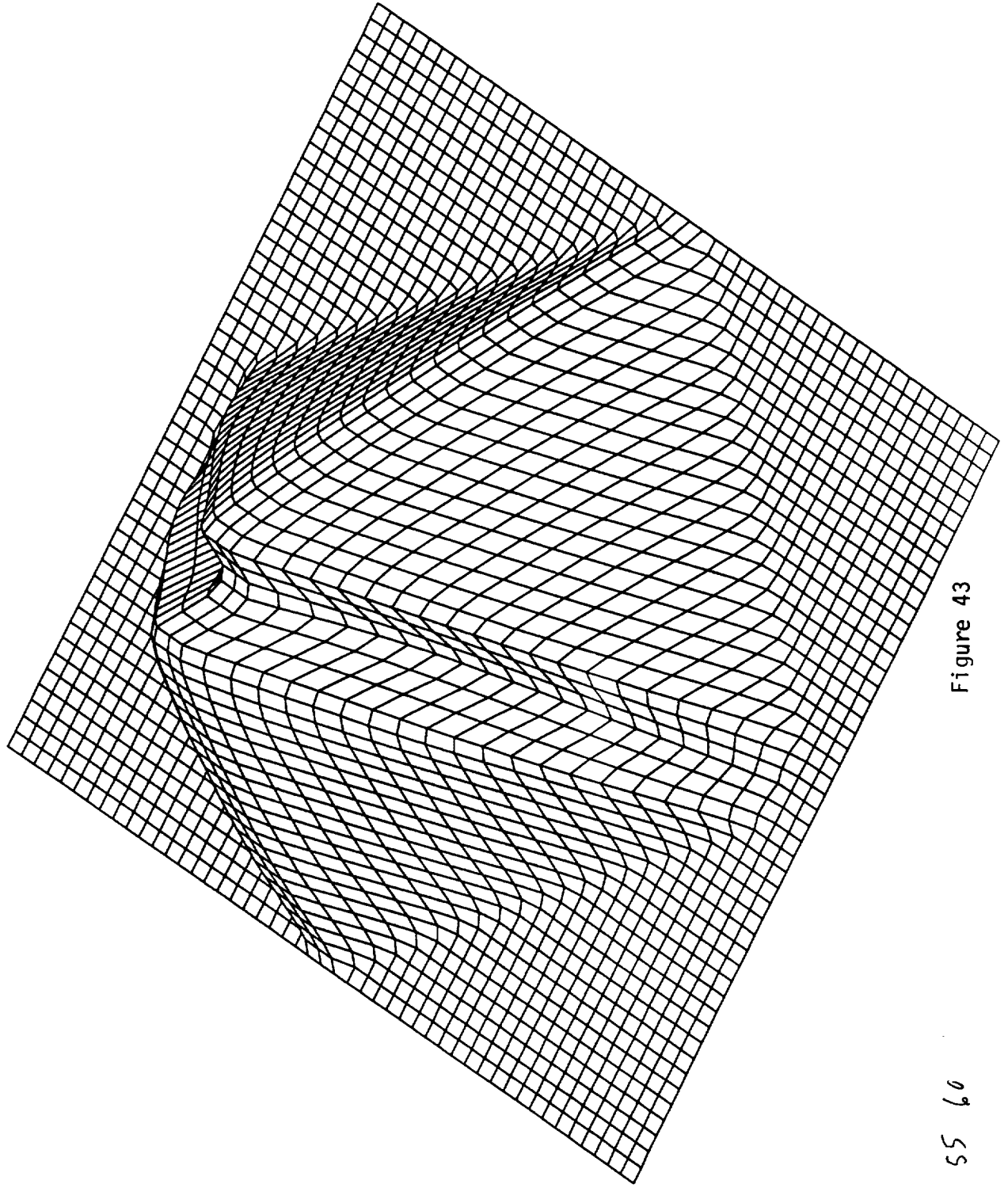
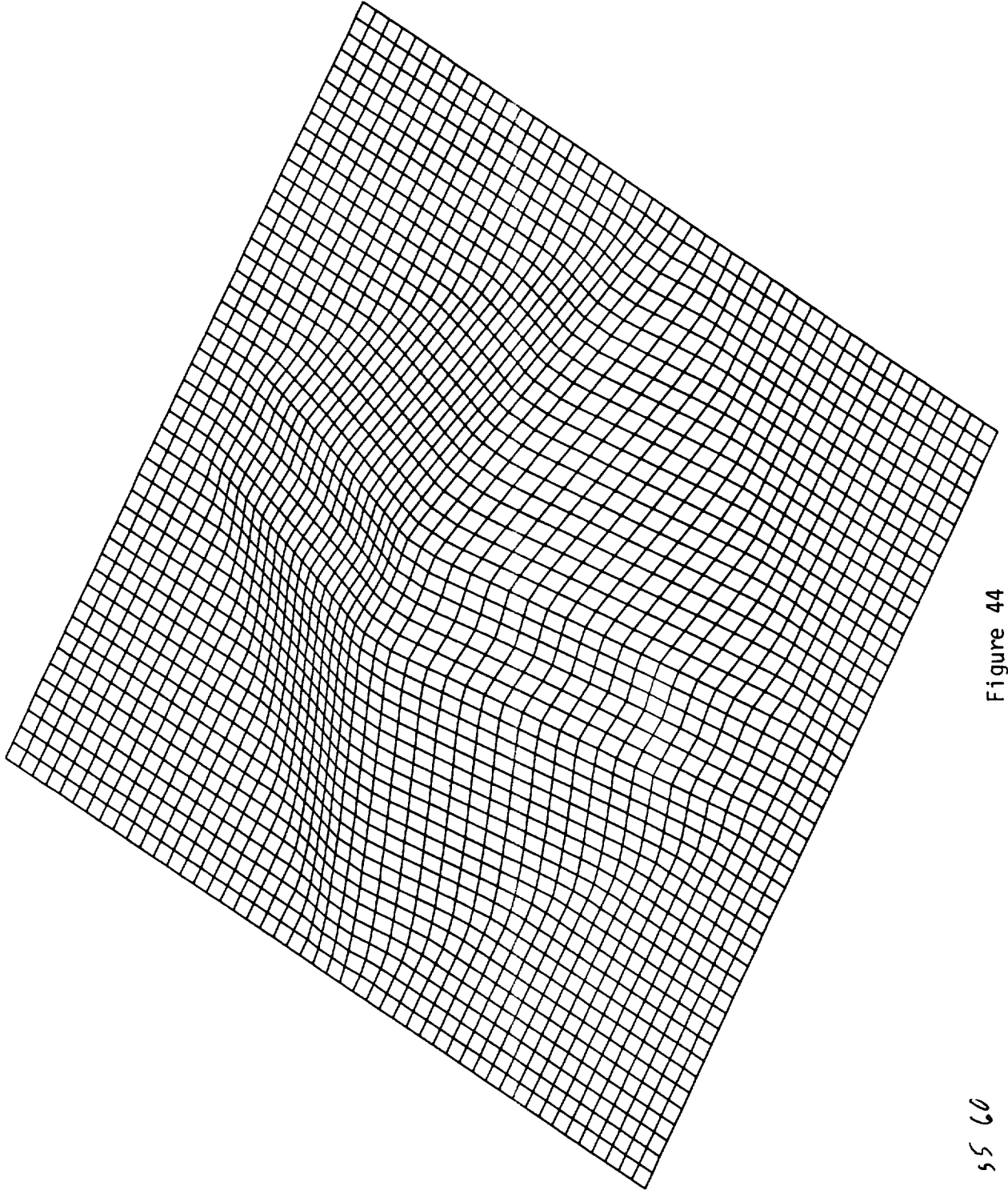


Figure 43

ISCZ 0.3 -2 55 60





5572 0.05 - 8 55 60

Figure 44

```

VOYAGER DATA - CURRENTS (FA) J= 3
0.000e+00 0.000e+00 0.000e+00 0.000e+00 0.000e+00 0.000e+00 0.000e+00 0.000e+00
0.000e+00 0.000e+00 0.000e+00 0.000e+00 0.000e+00 0.000e+00 0.000e+00 0.000e+00

VOYAGER DATA - CURRENTS (FA) J= 4
4.215e+01 6.382e+01 1.118e+02 4.570e+02 6.945e+02 8.442e+02 1.858e+03 1.178e+03
1.888e+03 8.548e+02 5.786e+02 2.718e+02 1.858e+02 2.499e+01 2.676e+00 1.882e-01

TYPE 1 TO CONTINUE

```

```

$0.78 TYPE 1 TO CONTINUE
CONNECT= 08 PLOT SIMULATED DATA? 1=YES, 0=NO
LOGOFF AT 08
VM/370 ONLINE CHANGE CURRENT SCALE FROM CURRENT VALUE? 1=YES, 0=NO
[Back at Loc C-Kermit]g
Retain log?
gsg@space[0]
gsg@space[0]
4.9u 9.5e 2:
gag logged c
Connection c
win3 gsg[9]
aab spa
dje pla
dje spa
dumpster spa
gag spa
gag sta
gag sta
gag sta
gag sta
gag sta
gag sta
gag sta
gag sta
jwb spa
jwb spa
jwb spa
jwb spa
jwb spa
jwb spa
jwb spa
jwb spa
win3 gsg[10]
USER
gsg 117
gsg 117
gsg 117
win3 gsg[11]
win3 gsg[12]
win3 gsg[13]
win3 gsg[14]
win3 gsg[15]
win3 gsg[15]
lp is ready
Rank Owner
active gsg
lst gsg
win3 gsg[16]
win3 gsg[17]

```

BIMAXWELLIAN SIMULATION

Channel Number	Current
0	10 ^{1.5}
1	10 ^{2.0}
2	10 ^{2.5}
3	10 ^{3.0}
4	10 ^{3.5}
5	10 ^{3.8}
6	10 ^{3.9}
7	10 ^{4.0}
8	10 ^{4.0}
9	10 ^{3.9}
10	10 ^{3.8}
11	10 ^{3.5}
12	10 ^{3.0}
13	10 ^{2.5}
14	10 ^{2.0}
15	10 ^{1.5}
16	10 ^{1.0}

SIMULATION :NO LOSS
V = <0.000 , 0.000 , 0.000 > KM/S B = <1.000 , 0.000 , 0.000 > GAMMA
A = 0 Z = -1
N(CM-3) = .008
WPAR = 11861.120 WPER = 11861.120 KM/S

Figure 45

ORIGINAL PAGE IS OF POOR QUALITY

```

VOYAGER DATA - CURRENTS (FA) J= 3
0.000e+00 0.000e+00 0.000e+00 0.000e+00 0.000e+00 0.000e+00 0.000e+00 0.000e+00
0.000e+00 0.000e+00 0.000e+00 0.000e+00 0.000e+00 0.000e+00 0.000e+00 0.000e+00

VOYAGER DATA - CURRENTS (FA) J= 4
3.858e+01 4.667e+01 8.244e+01 3.688e+02 5.388e+02 6.264e+02 7.687e+02 8.357e+02
7.666e+02 8.216e+02 4.338e+02 2.188e+02 8.377e+01 2.847e+01 2.239e+00 1.585e-01

TYPE 1 TO CONTINUE

```

```

CONNECT= 88 TYPE 1 TO CONTINUE
LOGOFF AT 88
PLOT SIMULATED DATA? 1=YES, 0=NO
VM/370 ONLIN 1
THE SCALE STARTS AT 1.00e+01 FEMTOAMPS AND GOES UP 3 DECADES
[Back at Location] CHANGE CURRENT SCALE FROM CURRENT VALUE? 1=YES, 0=NO
C-Kermit>q 0

Retain log?
gsg@space[8] Plot option [cefghnqw]: g
gsg@space[8]
4.9u 2.5e 2:
gsg logged c
Connection c
win3 gsg[9]
aeb spa
dje pla
dje spa
dumper spa
gsg spa
gsg sta
gsg sta
gsg sta
gsg sta
gsg sta
gsg sta
gsg sta
gsg sta
jwb spa
jwb spa
jwb spa
jwb spa
jwb spa
jwb spa
jwb spa
jwb spa
win3 gsg[10]
USER P
gsg 117
gsg 117
gsg 117
win3 gsg[11]
win3 gsg[12]
win3 gsg[13]
win3 gsg[14]
win3 gsg[15]
win3 gsg[15]
lp is ready
Rank Owner
active gsg
1st gsg
win3 gsg[16]
win3 gsg[17]
win3 gsg[18]
win3 gsg[19]

```

BI-MAXWELLIAN SIMULATION

SIMULATION : ISOTROPIC

V = <0.000 , 0.000 , 0.000 > KM/S B = <1.000 , 0.000 , 0.000 > GAMMA

A = 0 Z = -1

N<CM-3> = .008

WPAR = 11861.120 WPER = 11861.120 KM/S

Figure 46

```

VOYAGER DATA - CURRENTS (FA) J= 3
0.000e+00 0.000e+00 0.000e+00 0.000e+00 0.000e+00 0.000e+00 0.000e+00 0.000e+00
0.000e+00 0.000e+00 0.000e+00 0.000e+00 0.000e+00 0.000e+00 0.000e+00 0.000e+00

VOYAGER DATA - CURRENTS (FA) J= 4
3.598e+01 5.460e+01 9.549e+01 4.074e+02 6.059e+02 7.246e+02 8.976e+02 9.985e+02
9.193e+02 7.388e+02 5.877e+02 2.424e+02 9.497e+01 2.288e+01 2.473e+00 1.735e-01

TYPE 1 TO CONTINUE

```

```

VM/370 ONLINE
[Back at Loc 1]
C-Kermit>q
Retain log? 0
gsg@space[8]
gsg@space[8]
4.9u 0.5s 2: Plot option [cefghnqw]: g
gsg logged c
Connection c
win3 gsg[9]
aeb spa
dje pla
dje spa
dumpster spa
gsg spa
gsg sta
gsg sta
gsg sta
gsg sta
gsg sta
gsg sta
gsg sta
jwb spa
jwb spa
jwb spa
jwb spa
jwb spa
jwb spa
jwb spa
jwb spa
win3 gsg[10]
USER f
gsg 117
gsg 117
gsg 117
win3 gsg[11]
win3 gsg[12]
win3 gsg[13]
win3 gsg[14]
win3 gsg[15]
win3 gsg[15]
lp is ready
Rank Owner
active gsg
lst gsg
win3 gsg[16]
win3 gsg[17]
win3 gsg[18]
win3 gsg[19]
win3 gsg[20]
win3 gsg[21]

```

BIHAXWELLIAN SIMULATION

SIMULATION :COSINE

V = <0.000 , 0.000 , 0.000 > KM/S B = <1.000 , 0.000 , 0.000 > GAMMA

A = 0 Z = -1

N<CM-3> = .008

WPAR = 11861.120 WPER = 11861.120 KM/S

Figure 47

ORIGINAL PAGE IS
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ORIGINAL PAGE IS
OF POOR QUALITY

```
VOYAGER DATA - CURRENTS (FA) J= 3
0.000e+00 0.000e+00 0.000e+00 0.000e+00 0.000e+00 0.000e+00 0.000e+00 0.000e+00
0.000e+00 0.000e+00 0.000e+00 0.000e+00 0.000e+00 0.000e+00 0.000e+00 0.000e+00

VOYAGER DATA - CURRENTS (FA) J= 4
4.481e+02 7.197e+02 1.457e+03 1.349e+04 1.188e+04 9.847e+03 7.483e+03 6.262e+03
5.321e+03 4.462e+03 3.824e+03 3.175e+03 2.584e+03 1.918e+03 1.054e+03 1.858e+02

TYPE 1 TO CONTINUE
```

```
TYPE 1 TO CONTINUE
.sp 1
.nf 0 PLOT SIMULATED DATA? 1=YES, 0=NO
.ta 5.01 1
7 Co THE SCALE STARTS AT 1.00e+01 FEMTOAMPS AND GOES UP 4 DECADES
Lex1 CHANGE CURRENT SCALE FROM CURRENT VALUE? 1=YES, 0=NO
(617) 0

.sp
.f1
.nf Plot option [cefghnqw]: g
.ta 0.51C 1.
.vf80objective

BIMAXWELLIAN SIMULATION

E2 MODE

CURRENT
10^5
10^4
10^3
10^2
10^1
0 4 8 12 16
CHANNEL NUMBER

SIMULATION :NO LOSS
V = <0.000 , 0.000 , 0.000 > KM/S B = <1.000 , 0.000 , 0.000 > GAMMA
A = 0 Z = -1
N(CM-3) = .445
WPAR = 1861.019 WPER = 1861.019 KM/S
```

Figure 48

```
VOYAGER DATA - CURRENTS (FA) J= 3
0.000e+00 0.000e+00 0.000e+00 0.000e+00 0.000e+00 0.000e+00 0.000e+00 0.000e+00
0.000e+00 0.000e+00 0.000e+00 0.000e+00 0.000e+00 0.000e+00 0.000e+00 0.000e+00

VOYAGER DATA - CURRENTS (FA) J= 4
3.583e+02 5.673e+02 1.173e+03 1.186e+04 9.896e+03 7.838e+03 5.544e+03 4.492e+03
3.788e+03 3.217e+03 2.832e+03 2.429e+03 2.043e+03 1.555e+03 8.827e+02 1.588e+02

TYPE 1 TO CONTINUE
1
```

```
TYPE 1 TO CONTINUE
FUNCTION 1
COMMON PLOT SIMULATED DATA? 1=YES, 0=NO
REAL *E1
DATA A THE SCALE STARTS AT 1.00e+01 FEMTOAMPS AND GOES UP 4 DECADES
XMAX=0 CHANGE CURRENT SCALE FROM CURRENT VALUE? 1=YES, 0=NO
0
C FUNCTION I
C FAC AND WT
C AKAP IS KA Plot option [cefghnqw]: g
C IF(W/W
C WRITE
C 998 FORMAT
W2=W*W
ZZZ=W*W
IF (ZZ
IF ( W
C FOR E1 MOD
C IF (W
C CALCULATE
C ZZZ=W2
ARG1=A
C AG1 = GAMMA
C AG1=DG
ARG2=A
C AG2 = GAMMA
C AG2=DG
AFAC=F
XMAX=A
C WRITE
C 999 FORMAT
15 RETURN
END
C 01
C BIMAXWELL I
C
C FUNCTI
C REAL *
C
C COMMON
XMAX=0
IF(W/W
"xx.f" 02 11
win3 gsg[21]
win3 gsg[22]
```

BIMAXWELLIAN SIMULATION

Channel Number	Current (approx.)
0	10 ^{1.5}
2	10 ³
4	10 ⁴
6	10 ^{3.5}
8	10 ³
10	10 ^{2.5}
12	10 ²
14	10 ^{1.5}
16	10 ^{1.5}

SIMULATION : isotropic loss
V = <0.000 , 0.000 , 0.000 > KM/S B = <1.000 , 0.000 , 0.000 > GAMMA
A = 0 Z = -1
N(CM-3) = .445
WPRR = 1861.019 WPER = 1861.019 KM/S

Figure 49

ORIGINAL PAGE IS
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ORIGINAL PAGE IS
OF POOR QUALITY

```
VOYAGER DATA - CURRENTS (FA) J= 3
0.000e+00 0.000e+00 0.000e+00 0.000e+00 0.000e+00 0.000e+00 0.000e+00 0.000e+00
0.000e+00 0.000e+00 0.000e+00 0.000e+00 0.000e+00 0.000e+00 0.000e+00 0.000e+00

VOYAGER DATA - CURRENTS (FA) J= 4
9.778e+01 1.524e+02 2.839e+02 1.838e+03 1.988e+03 2.889e+03 1.939e+03 1.778e+03
1.542e+03 1.245e+03 9.919e+02 7.455e+02 5.414e+02 3.554e+02 1.716e+02 2.781e+01

TYPE 1 TO CONTINUE
```

```

PLOT SIMULATED DATA? 1=YES, 0=NO
1
THE SCALE STARTS AT 1.00e+01 FEMTOAMPS AND GOES UP 4 DECADES
CHANGE CURRENT SCALE FROM CURRENT VALUE? 1=YES, 0=NO
0
Plot option [cefghnqw]: g
COMMON BL
comm
floc
floc
COMMON
COMMON
* NDOCU
COMMON
COMMON BL
COMMON
EXTERN
REAL*4
REAL*4
DIMEN
REAL*4
REAL B
REAL B
charac
INTEGE
LOGICA
LOGICA
LOGICA
"psim.f" 444
win3 gsg[24]
USER P
gsg 40
gsg 43
gsg 43
win3 gsg[25]
no entries
win3 gsg[26]
USER P
gsg 43
gsg 43
win3 gsg[27]
win3 gsg[28]
```

BI-MAXWELLIAN SIMULATION

Channel Number	Current (FA)
0	10 ¹
1	10 ²
2	10 ³
3	10 ⁴
4	10 ^{4.5}
5	10 ^{4.2}
6	10 ^{3.8}
7	10 ^{3.5}
8	10 ^{3.2}
9	10 ^{2.8}
10	10 ^{2.5}
11	10 ^{2.2}
12	10 ^{1.8}
13	10 ^{1.5}
14	10 ^{1.2}
15	10 ^{1.0}
16	10 ^{1.0}

SIMULATION : loss isotropys

V = <0.000 , 0.000 , 0.000 > KM/S B = <1.000 , 0.000 , 0.000 > GAMMA
A = 0 Z = -1
N(CM-9) = .445
WPAR = 1861.019 WPER = 1861.019 KM/S

Figure 50

SPACE CRAFT SHOWN IN 0° ROLL ORIENTATION
 ROLL ANGLE IS COUNTERCLOCKWISE ABOUT SPACECRAFT -Z AXIS

NOTE THAT ROLL
 DIRECTIONS
 ARE SPACE FIX
 WHILE CLOCK
 DIRECTIONS ARE
 SPACECRAFT FIX

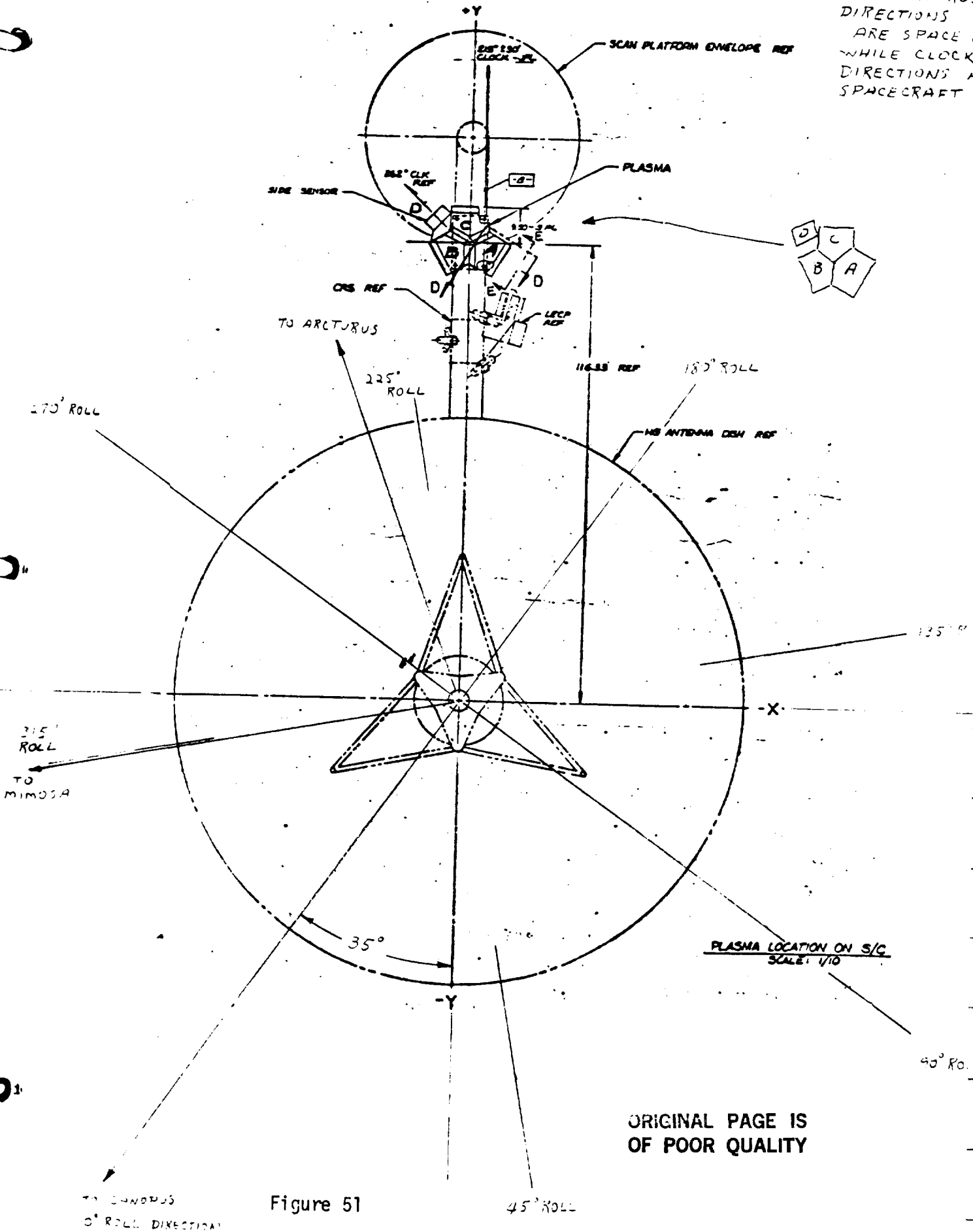
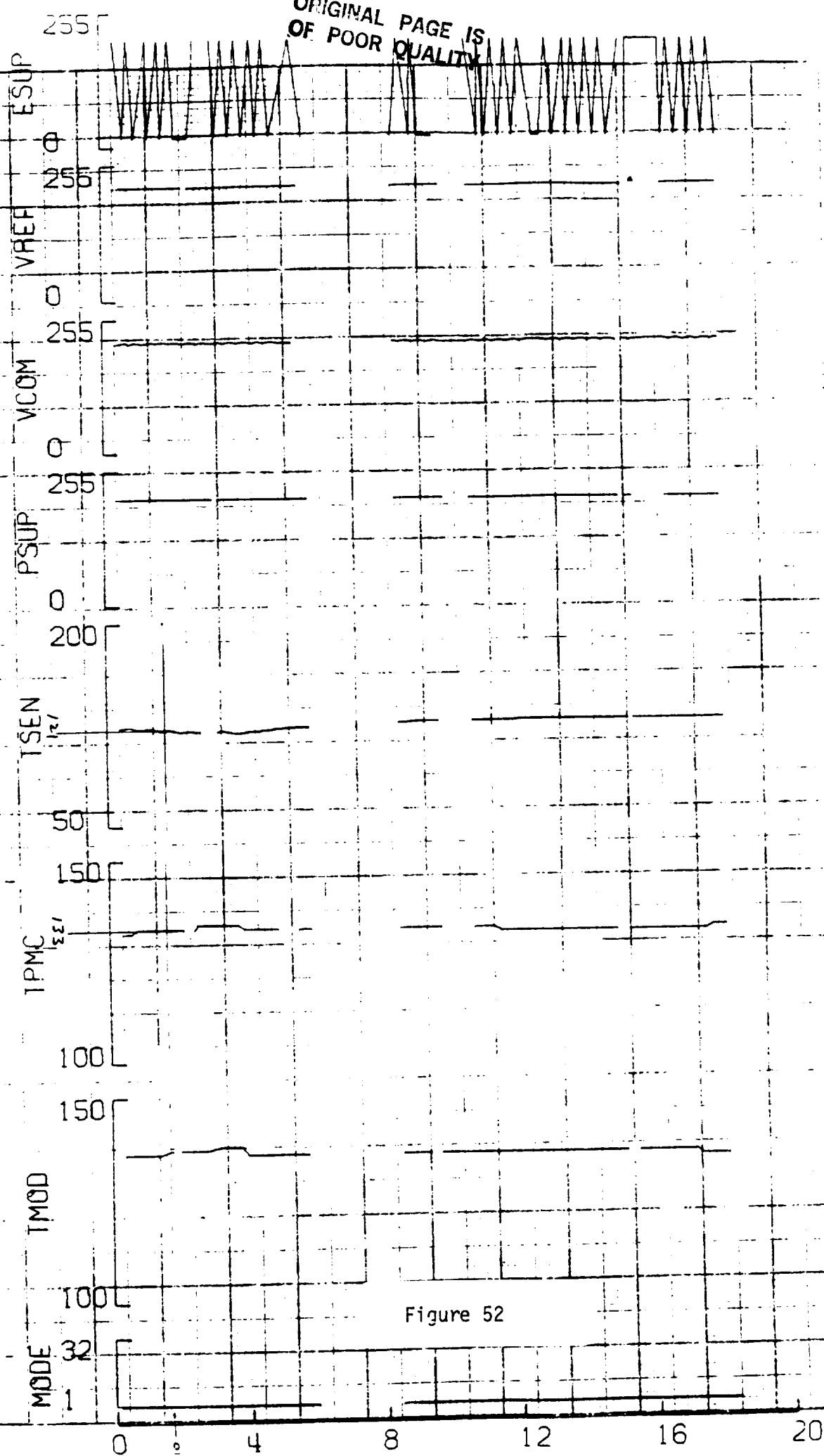


Figure 51

ORIGINAL PAGE IS
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ORIGINAL PAGE IS
OF POOR QUALITY

SR 1 ENGINEERING DATA
YEAR 1978 DAY 258
MIT 10/24/78 14:22:12.56



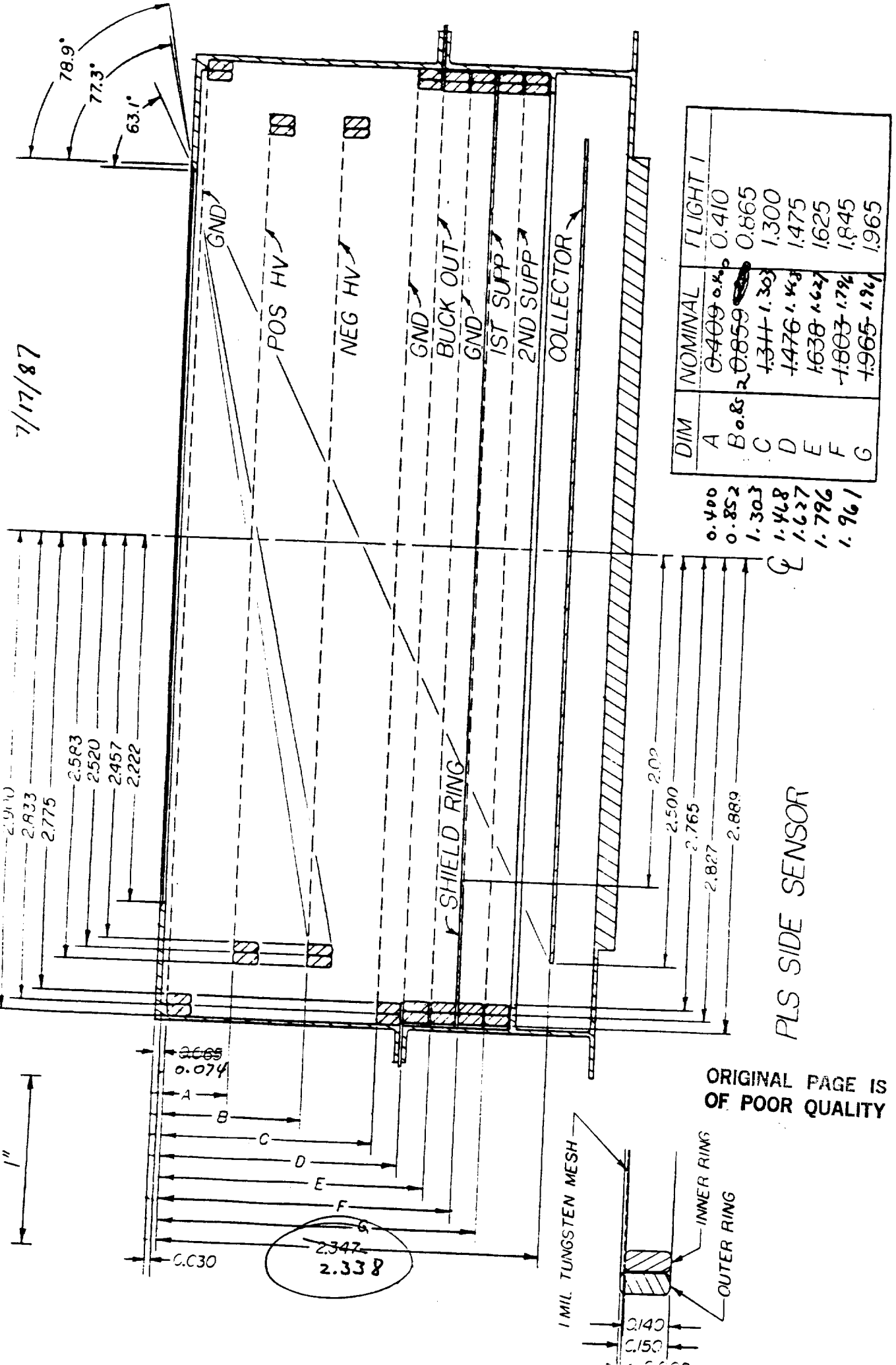
TPMC DN = 133
AT 258 0138

TSEN DN = 121

Figure 52

(T MOD = 15°C)

7/17/87



DIM	NOMINAL	FLIGHT 1
A	0.409 ± 0.006	0.410
B	0.852 ± 0.005	0.865
C	1.303 ± 0.003	1.300
D	1.476 ± 0.003	1.475
E	1.638 ± 0.002	1.625
F	1.803 ± 0.002	1.845
G	1.965 ± 0.001	1.965

PLS SIDE SENSOR

ORIGINAL PAGE IS OF POOR QUALITY

Revisions made on original
7/21/87

Figure 53

Sigs Sensor - Vertical cut

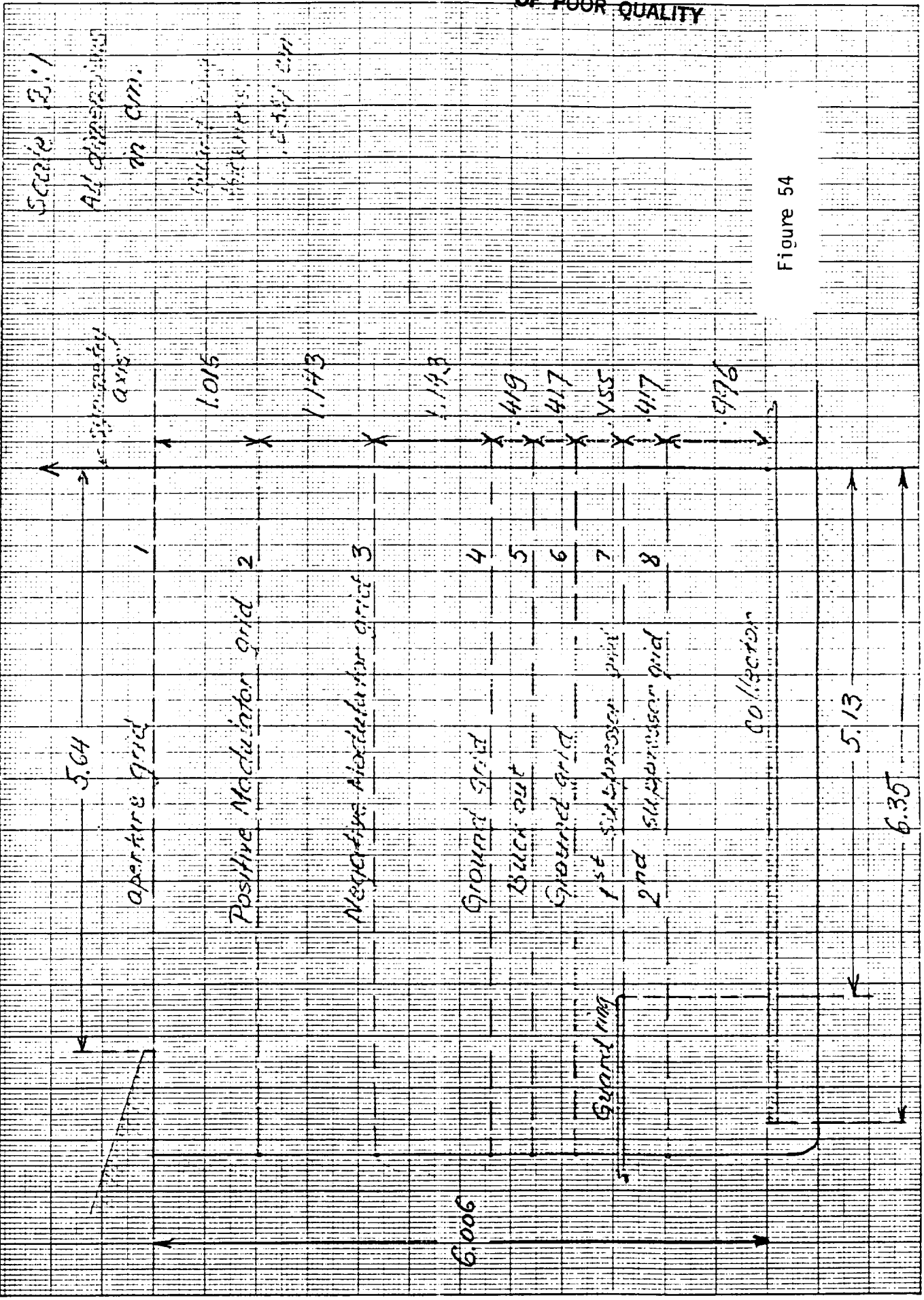
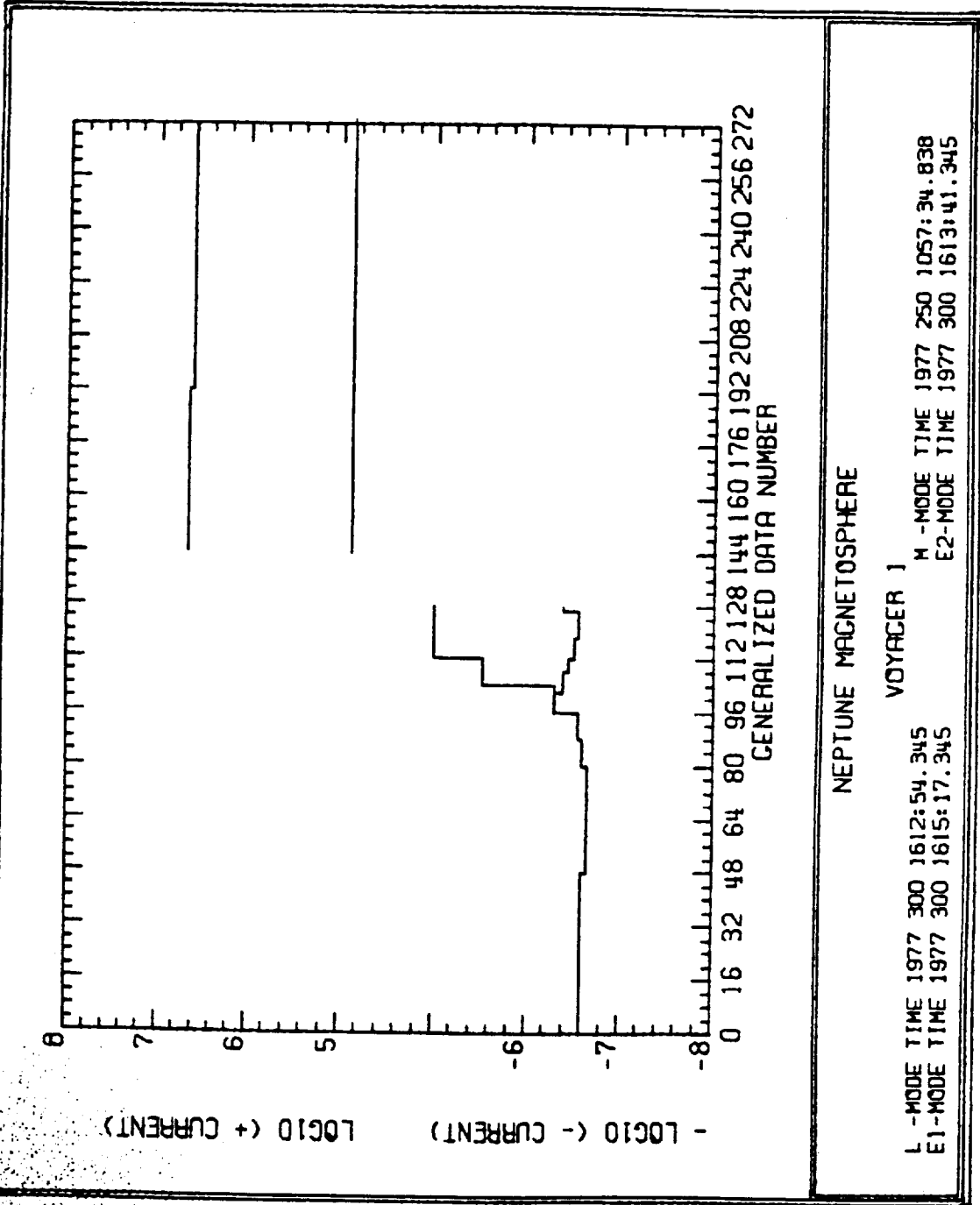


Figure 54

MOD ON NORMAL IDC

VOYAGER DC RETURN DATA

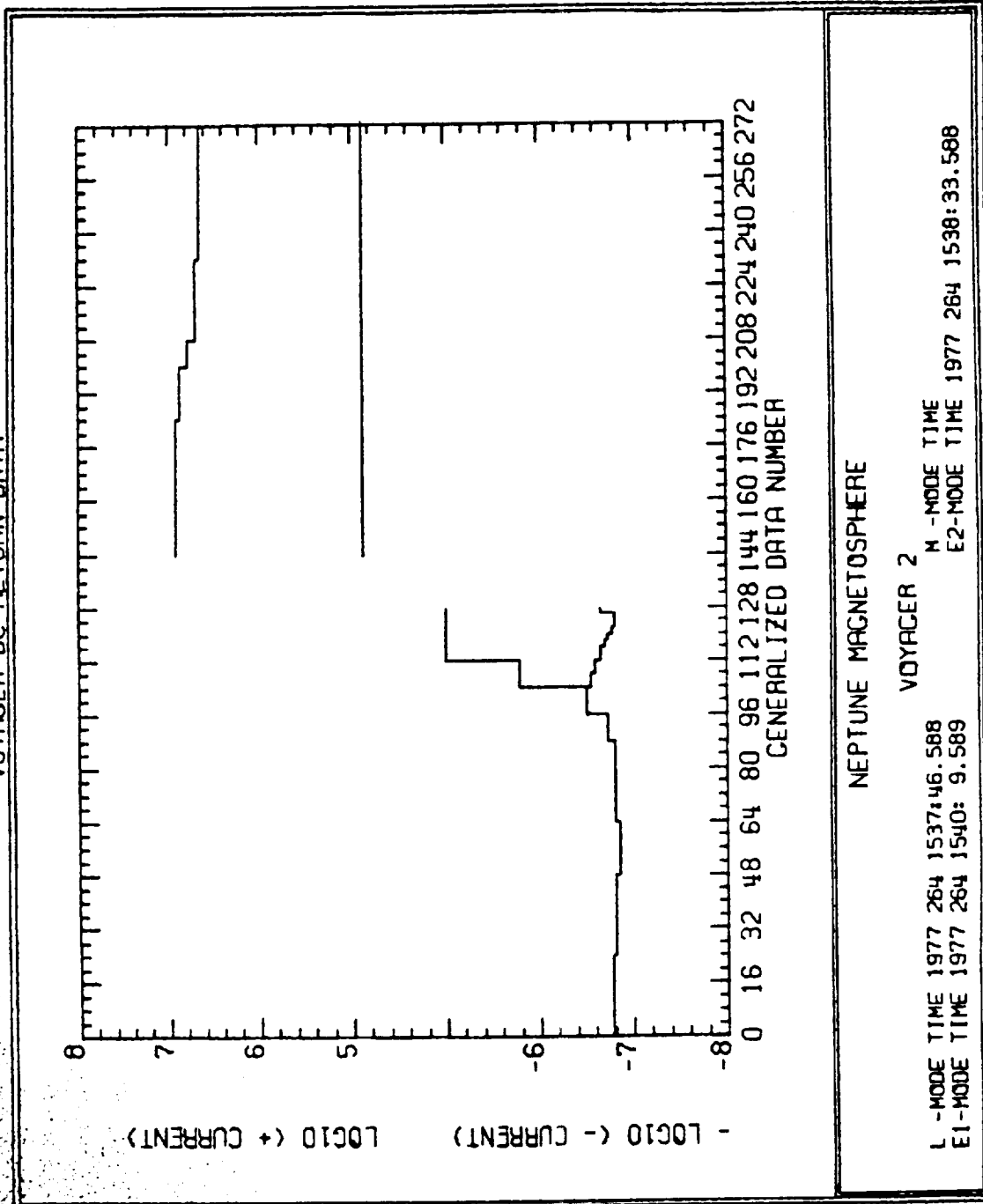


ORIGINAL PAGE IS
OF POOR QUALITY

Figure 55

DC RET MOD ON
NORMAL

VOYAGER DC RETURN DATA



NEPTUNE MAGNETOSPHERE

VOYAGER 2

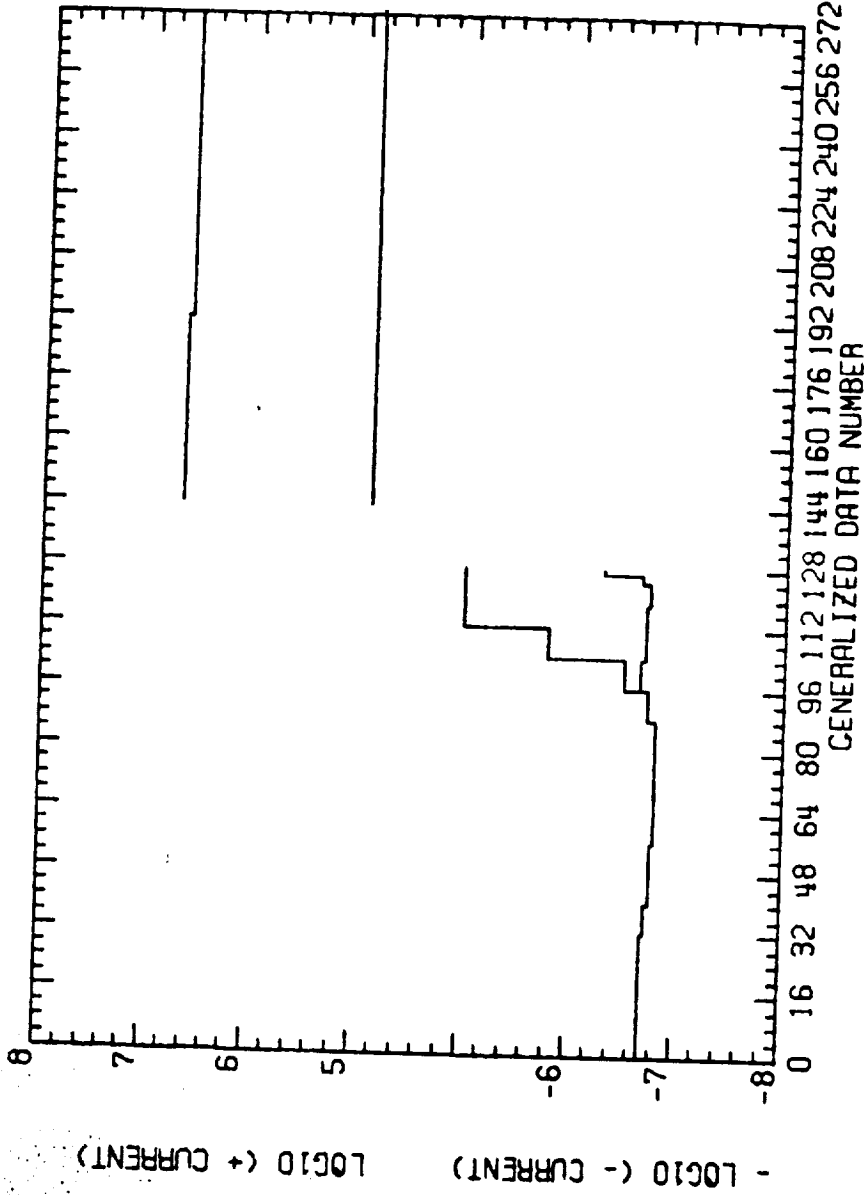
L-MODE TIME 1977 264 1537:46.588
E1-MODE TIME 1977 264 1540: 9.589

M-MODE TIME
E2-MODE TIME 1977 264 1538:33.588

Figure 56

MOD ON - REV - IDC

VOYAGER DC RETURN DATA



-NEPTUNE MAGNETOSPHERE-

VOYAGER 1

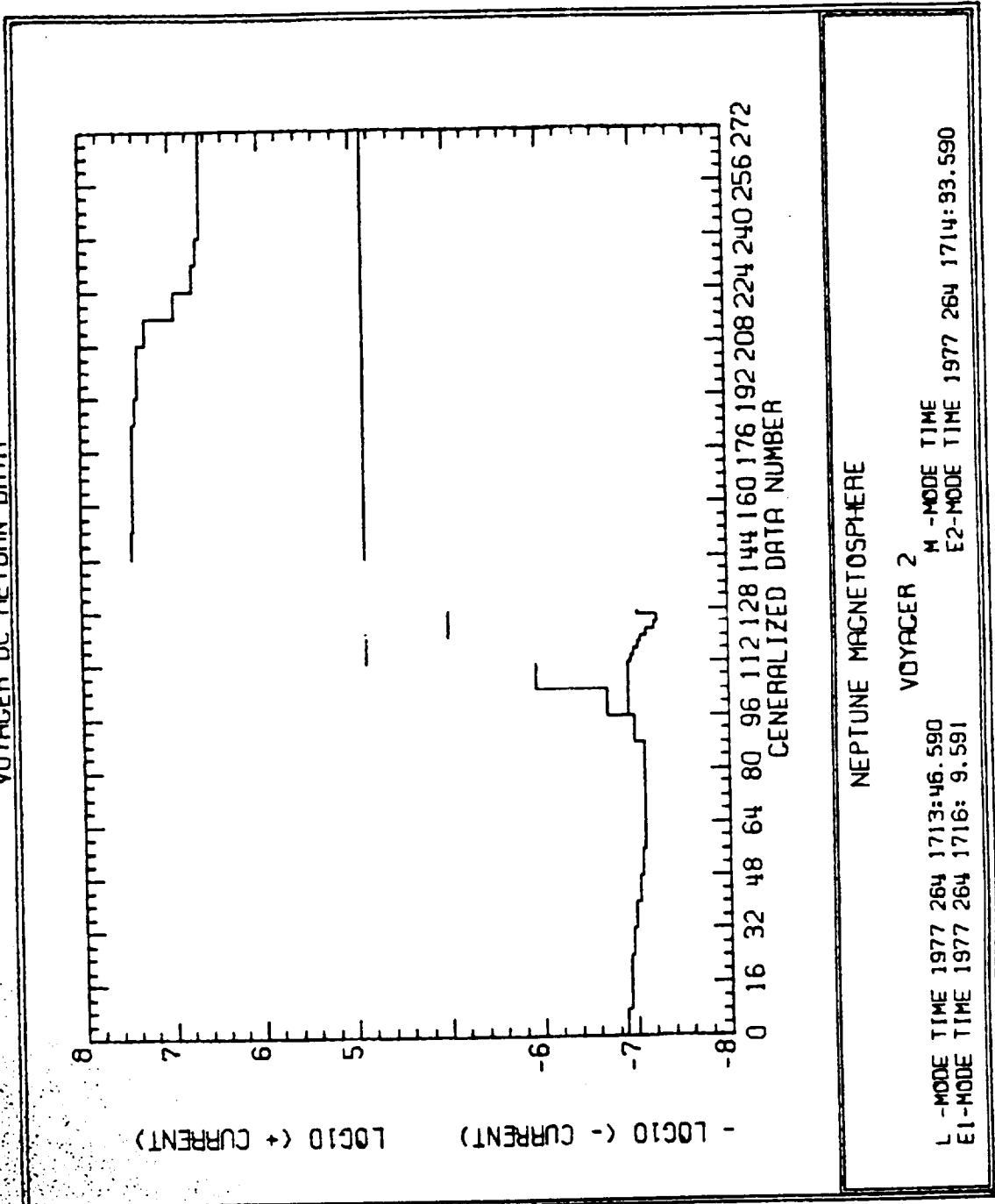
L -MODE TIME 1977 300 1436:54.340
E1 -MODE TIME 1977 300 1439:17.340
M -MODE TIME 1977 258 1857:34.838
E2 -MODE TIME 1977 300 1437:41.340

Figure 57

ORIGINAL PAGE IS
OF POOR QUALITY

DC RET
MODON REV

VOYAGER DC RETURN DATA



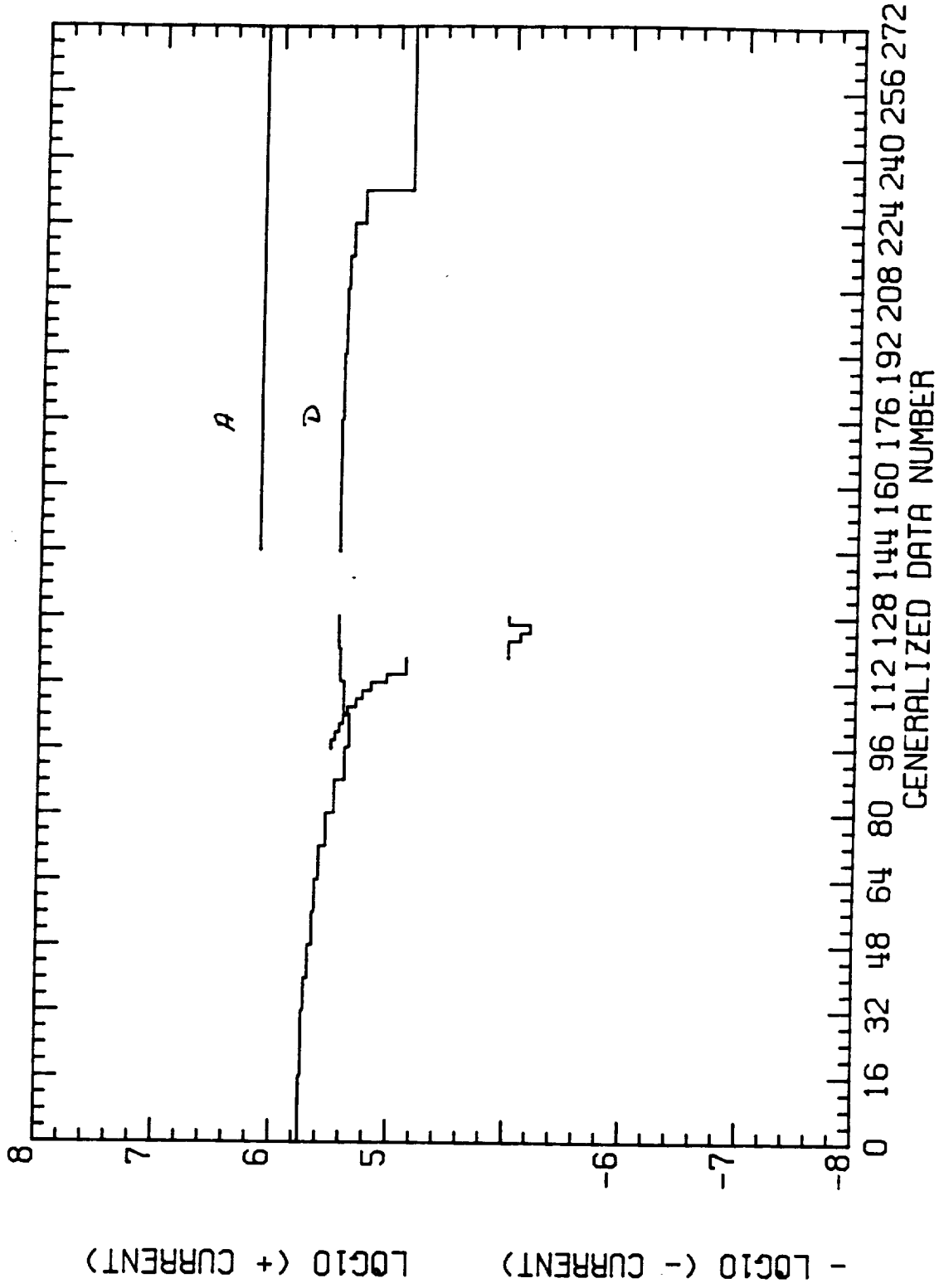
NEPTUNE MAGNETOSPHERE

VOYAGER 2

L -MODE TIME 1977 264 1713:46.590
E1 -MODE TIME 1977 264 1716: 9.591

M -MODE TIME
E2 -MODE TIME 1977 264 1714:93.590

Figure 58



JUPITER MAGNETOSPHERE

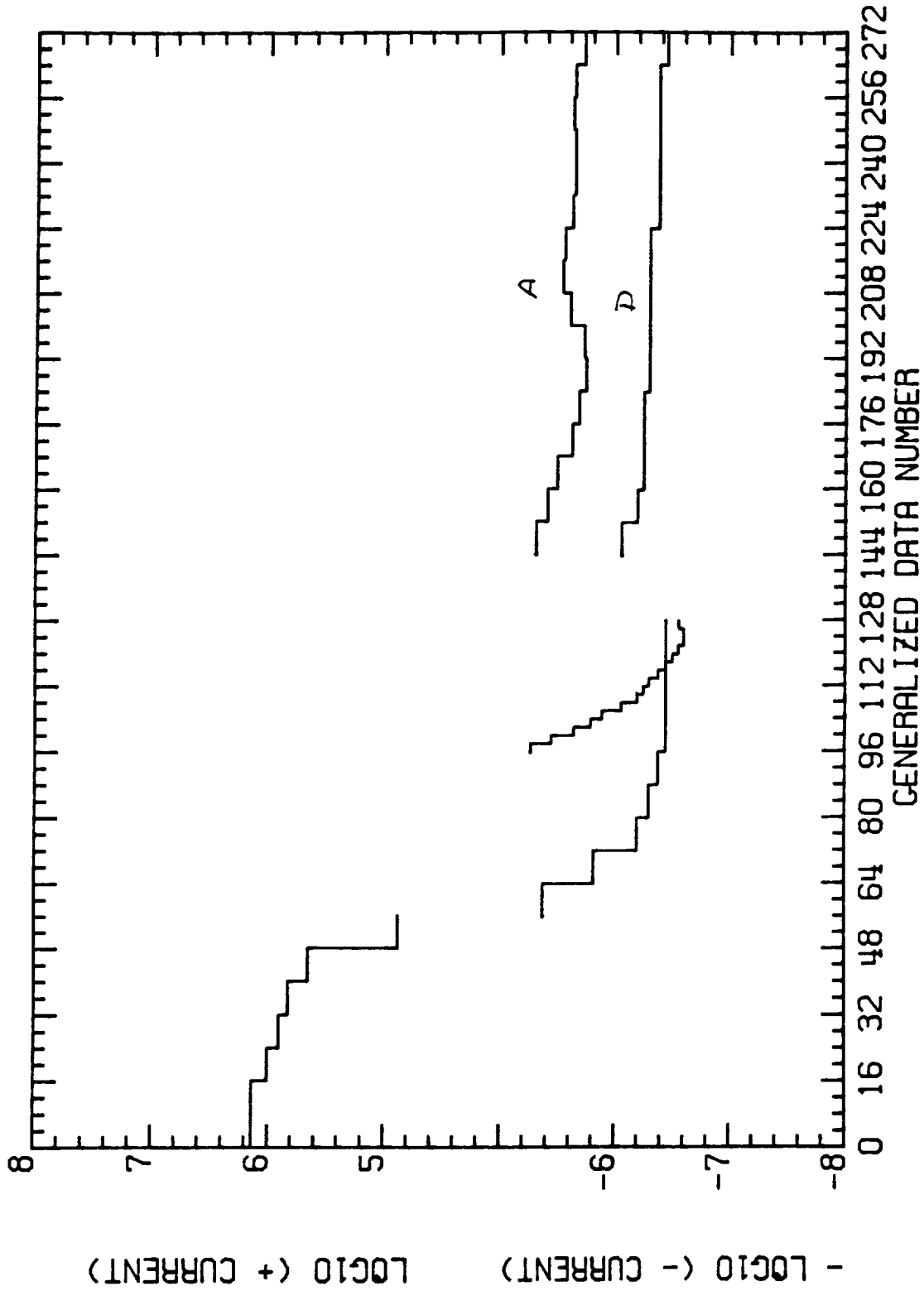
VOYAGER 1

L -MODE TIME 1979 63 1925:48.442
E1-MODE TIME 1979 63 1926:55.403

M -MODE TIME 1979 63 1926:23.003
E2-MODE TIME 1979 63 1926: 7.403

Figure 59

VOYAGER DC RETURN DATA



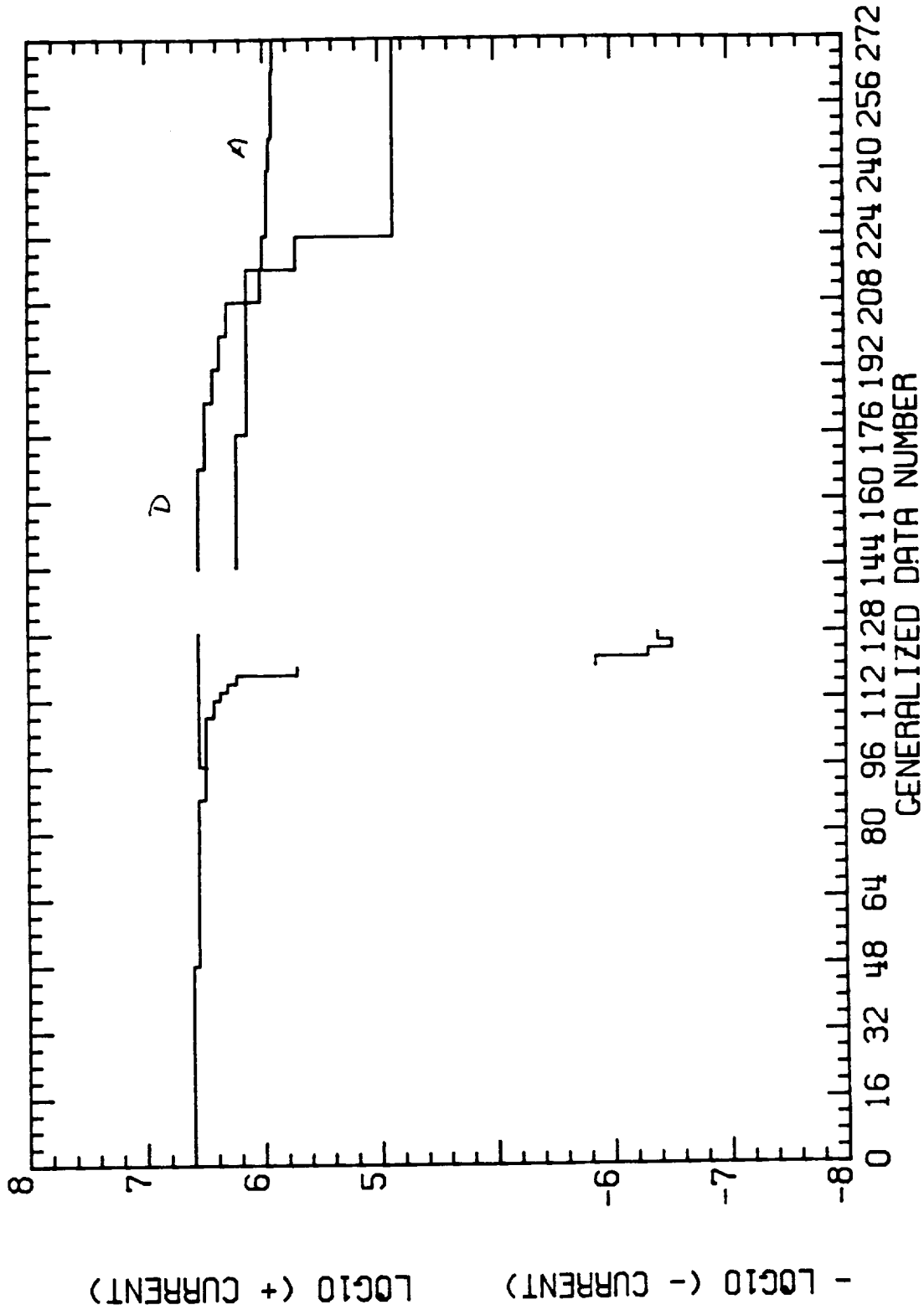
JUPITER MAGNETOSPHERE

VOYAGER 1

L -MODE TIME 1979 64 0426:36.445	M -MODE TIME 1979 64 0427:11.006
E1-MODE TIME 1979 64 0427:43.406	E2-MODE TIME 1979 64 0426:55.406

Figure 61

VOLTCEN DC CURRENT DATA



JUPITER MAGNETOSPHERE

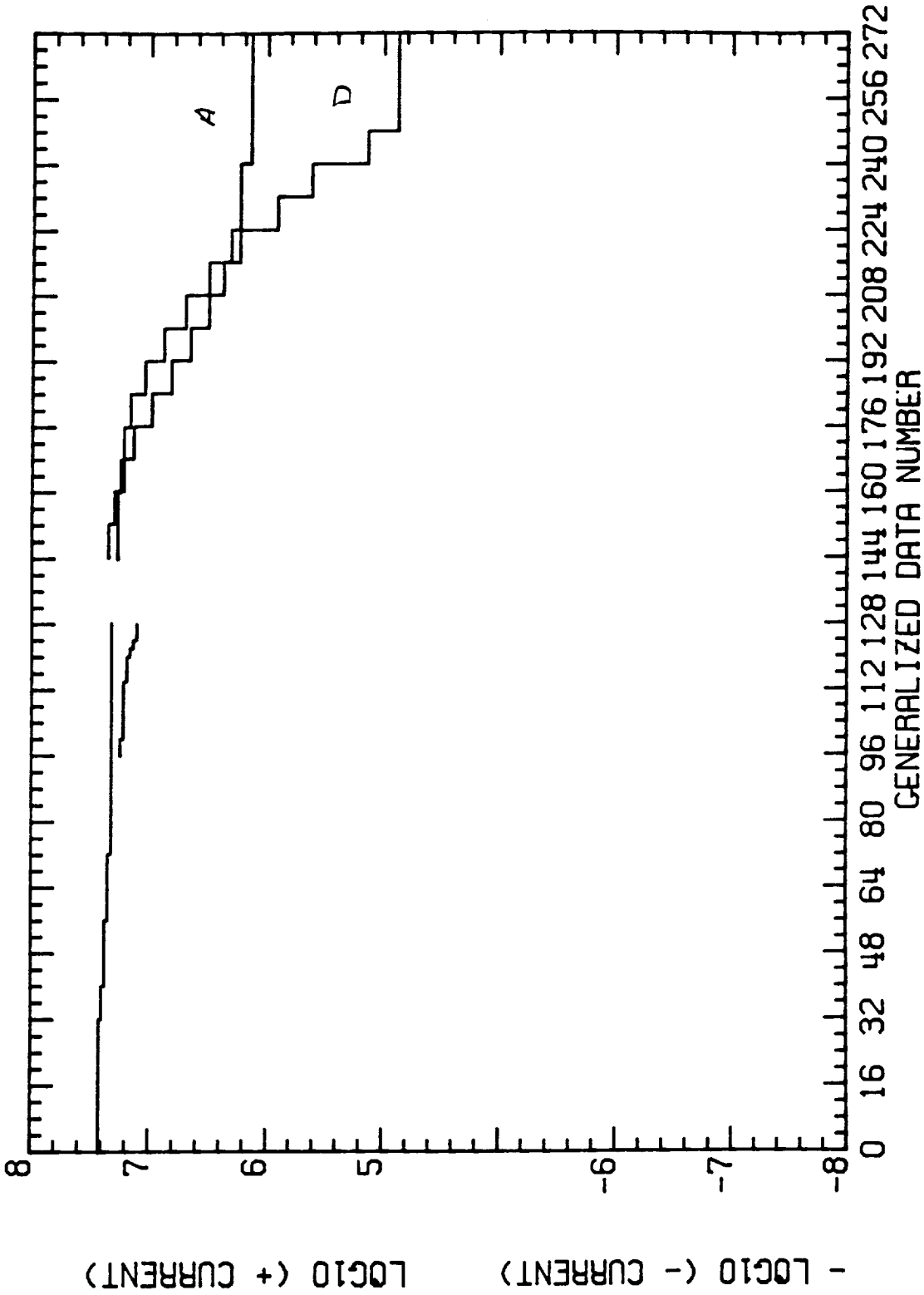
VOYAGER 1

L -MODE TIME 1979 64 0503:24.446
 E1--MODE TIME 1979 64 0504:31.407

M -MODE TIME 1979 64 0503:59.007
 E2--MODE TIME 1979 64 0503:43.407

Figure 62

VOYAGER DC RETURN DATA



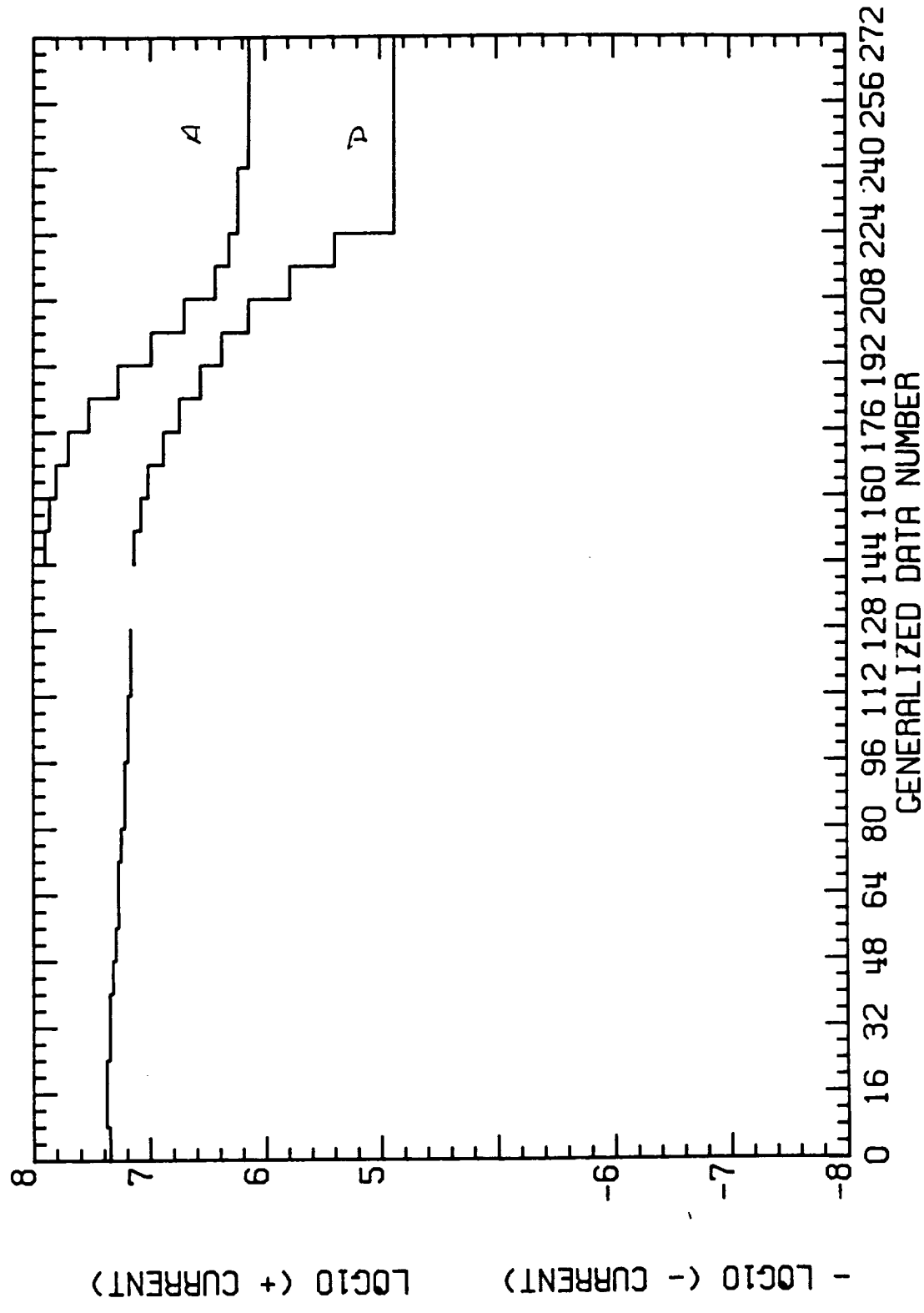
JUPITER MAGNETOSPHERE

VOYAGER 1

L -MODE TIME 1979	64 0737: 0.445
E1-MODE TIME 1979	64 0738: 7.406
M -MODE TIME 1979	64 0737: 35.006
E2-MODE TIME 1979	64 0737: 19.406

Figure 63

VOYAGER DC RETURN DATA



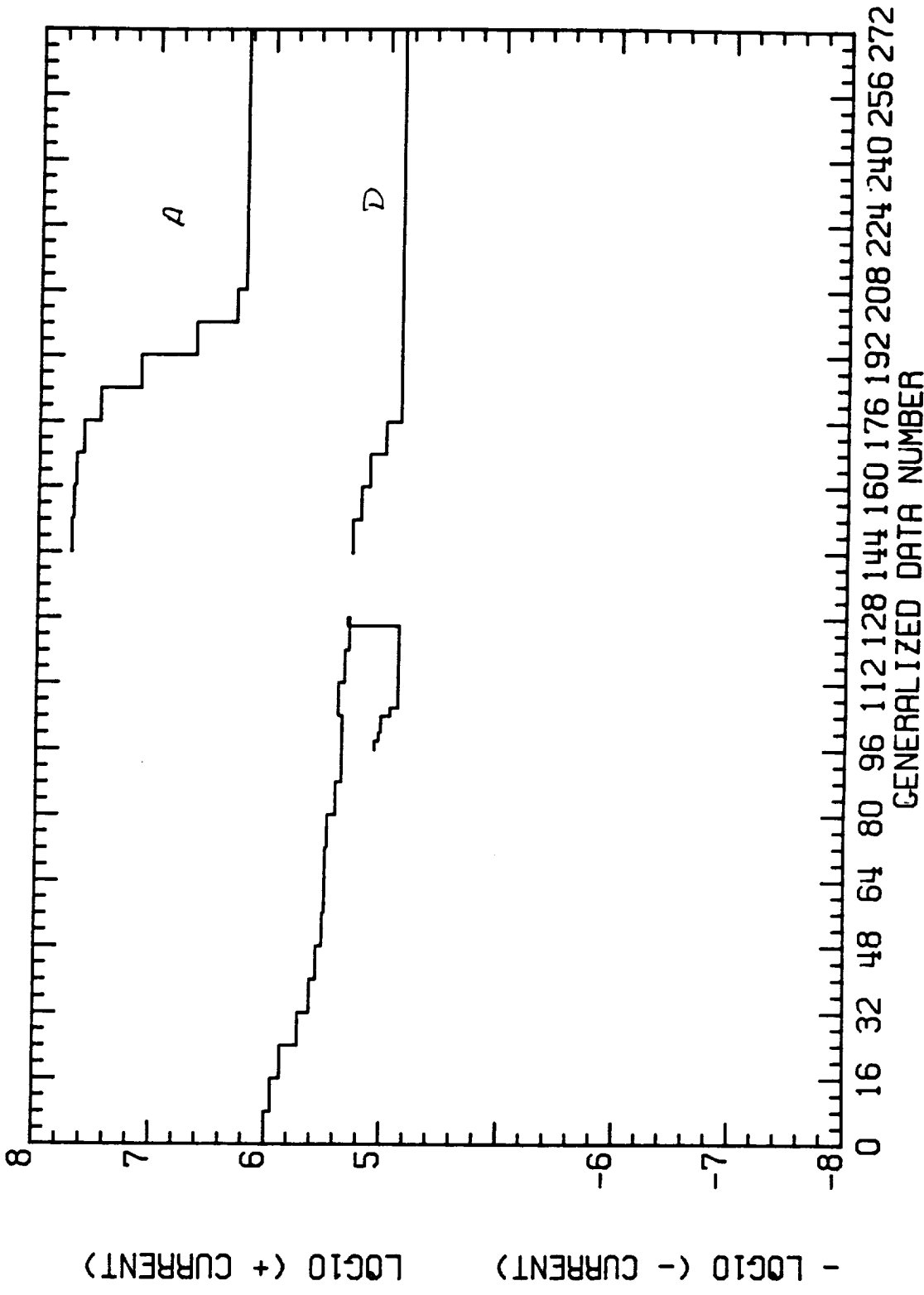
JUPITER MAGNETOSPHERE

VOYAGER 1

L -MODE TIME 1979 64 0921: 0.447
E1-MODE TIME 1979 64 0922: 7.408
M -MODE TIME 1979 64 0921:35.008
E2-MODE TIME 1979 64 0921:19.408

Figure 64

VOYAGER DC RETURN DATA



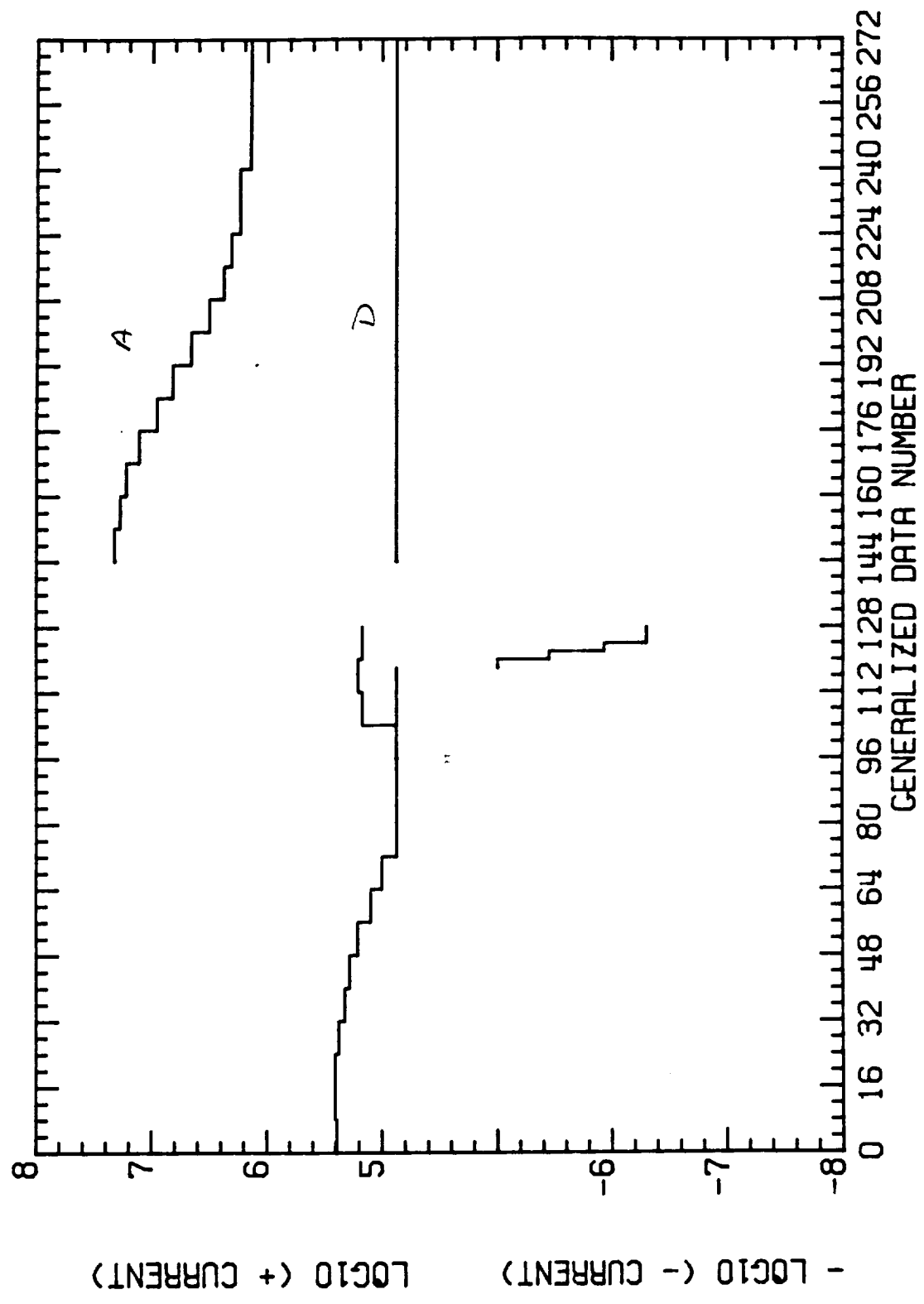
JUPITER MAGNETOSPHERE

VOYAGER 1

L -MODE TIME 1979 64 1012:12.447	M -MODE TIME 1979 64 1012:48.262
E1-MODE TIME 1979 64 1013:19.408	F2-MODE TIME 1979 64 1012:31.408

Figure 65

VOYAGER DC RETURN DATA



JUPITER MAGNETOSPHERE

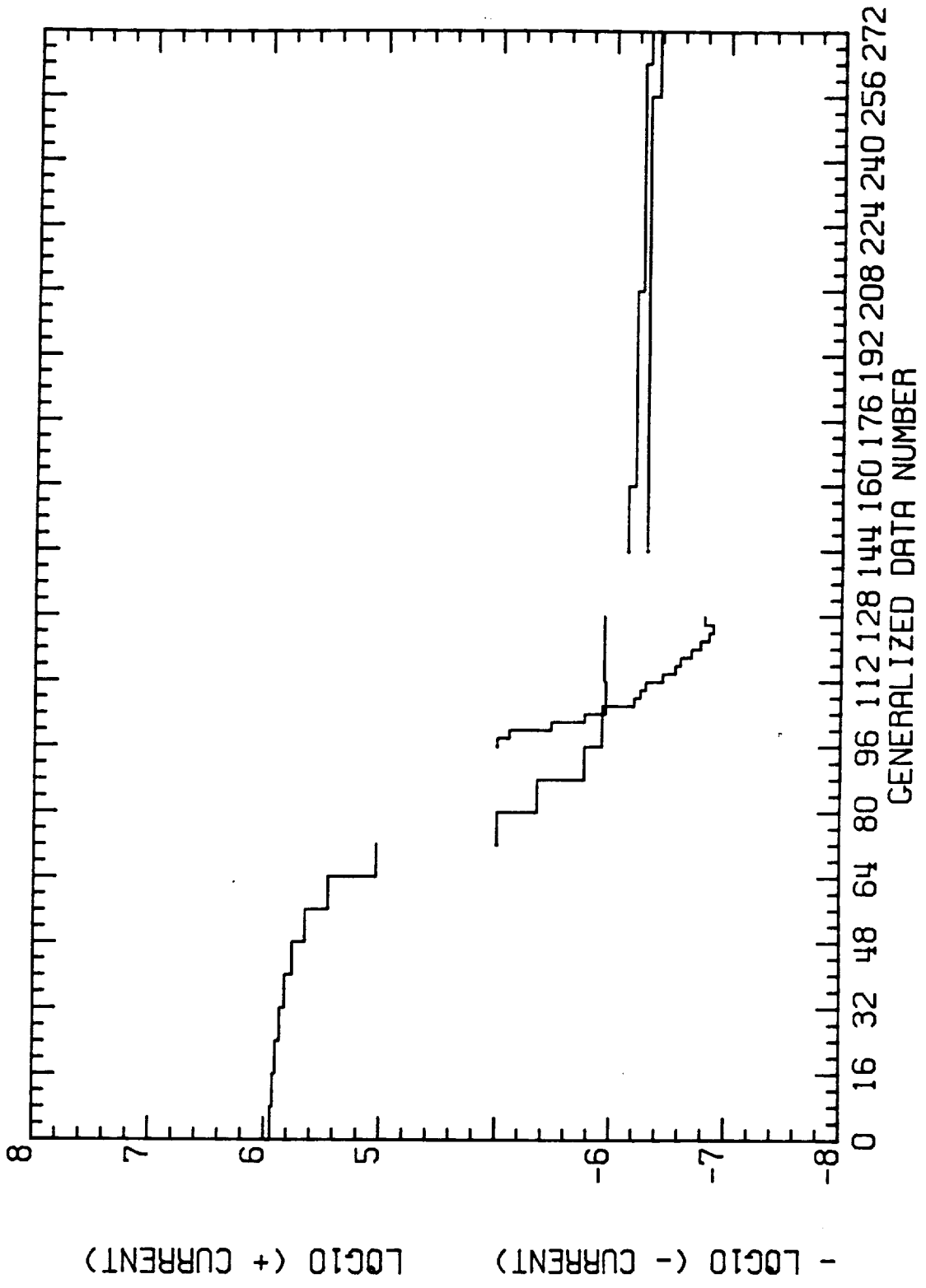
VOYAGER 1

L -MODE TIME 1979 64 1426:41.626
 E1--MODE TIME 1979 64 1427:48.597

M -MODE TIME 1979 64 1427:16.192
 JDE TIME 1979 64 1427: 0.587

Figure 66

VOYAGER DC RETURN DATA



JUPITER MAGNETOSPHERE

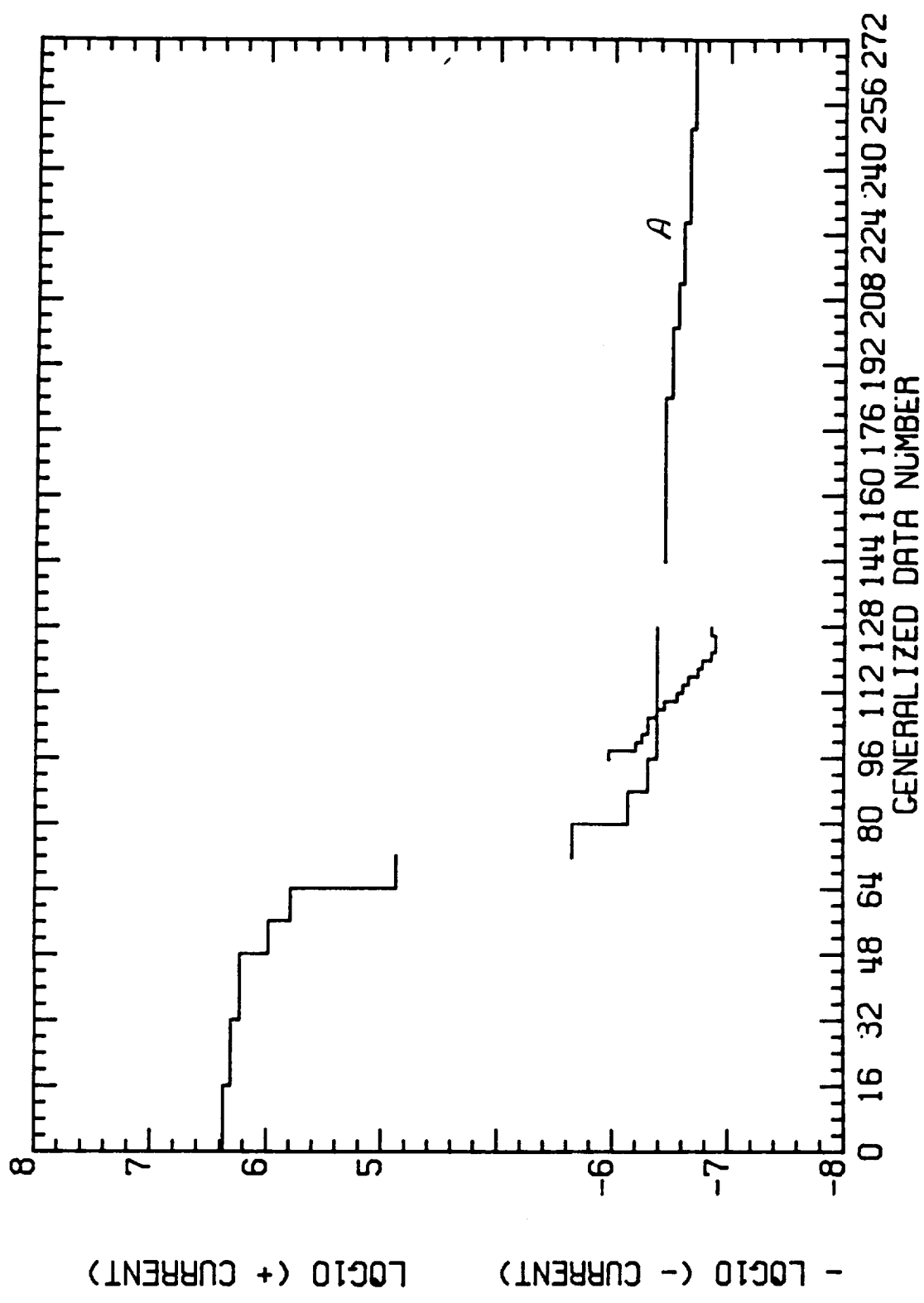
VOYAGER 1

L -MODE TIME 1979 64 1829:55.382	M -MODE TIME 1979 64 1830:29.948
E1-MODE TIME 1979 64 1831: 2.353	E2-MODE TIME 1979 64 1830:14.343

Figure 67

6-9

VOYAGER DC RETURN DATA



JUPITER MAGNETOSPHERE

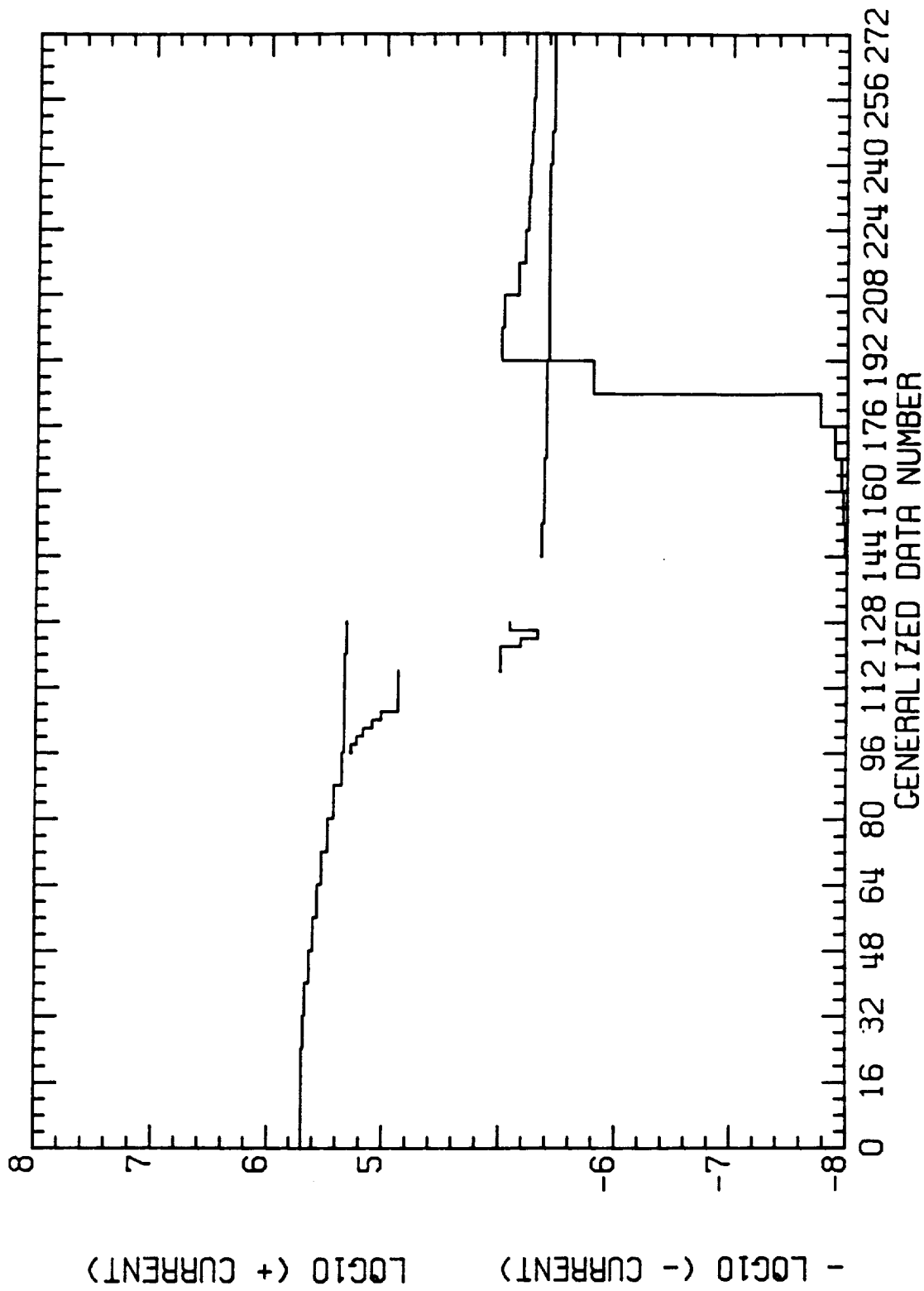
VOYAGER 1

L -MODE TIME 1979 64 1921: 7.711
 E1-MODE TIME 1979 64 1922: 14.682

M -MODE TIME 1979 64 1921: 42.277
 E2-MODE TIME 1979 64 1921: 26.672

Figure 68

VOYAGER DC RETURN DATA



SATURN MAGNETOSPHERE

Figure 69

VOYAGER 1

L -MODE TIME 1980 318 0343:23.564
E1 -MODE TIME 1980 318 0344:30.525

M -MODE TIME 1980 318 0343:58.125
E2 -MODE TIME 1980 318 0343:42.525

== X SCALE ==

from -1.00
to 9.00 1.00
tick

== Y SCALE ==

from -1.00
to 4.00
tick 0.50

Resolution: 51

Units are:

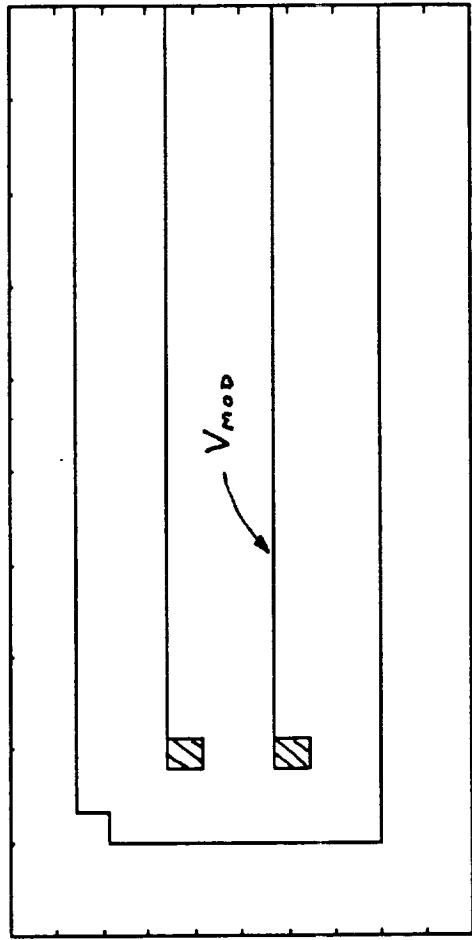
Centimeters
Volts

CURSOR AT:

X = 50.00
Y = 2.29

COMMAND -->

Type ? for list
of commands.



Total # of
boundaries = :
Total # of
segments = 58

Figure 70

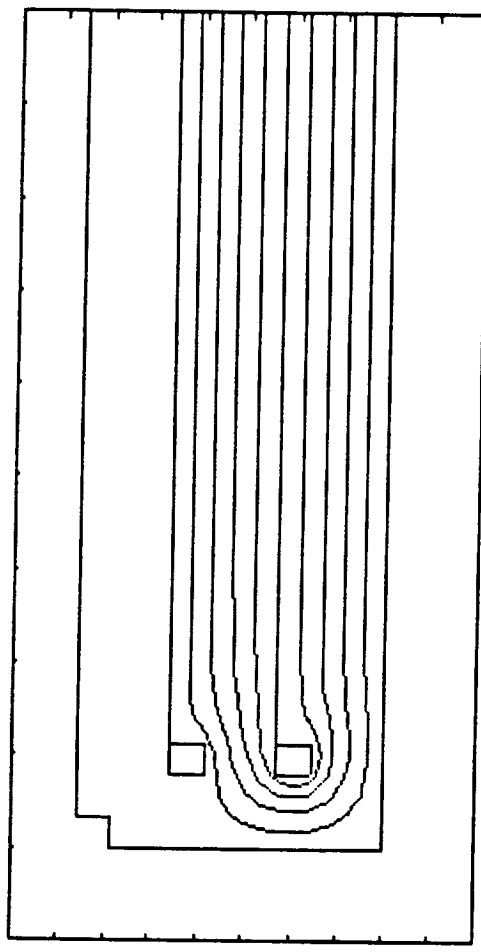
== X SCALE ==
from -1.00
to 9.00
tick 1.00

== Y SCALE ==
from -1.00
to 4.00
tick 0.50

Resolution: 51

Units are:
Centimeters
Volts

CURSOR AT:
X = 50.00
Y = 2.29



Type ? for list
of commands.

Total # of
boundaries = 18
Total # of
segments = 58

Please hit RETURN to continue. (NOTE: Screen will be cleared).

Figure 71

== X SCALE ==
from 0.70
to 1.70
tick 0.10

== Y SCALE ==
from -0.10
to 1.40
tick 0.15

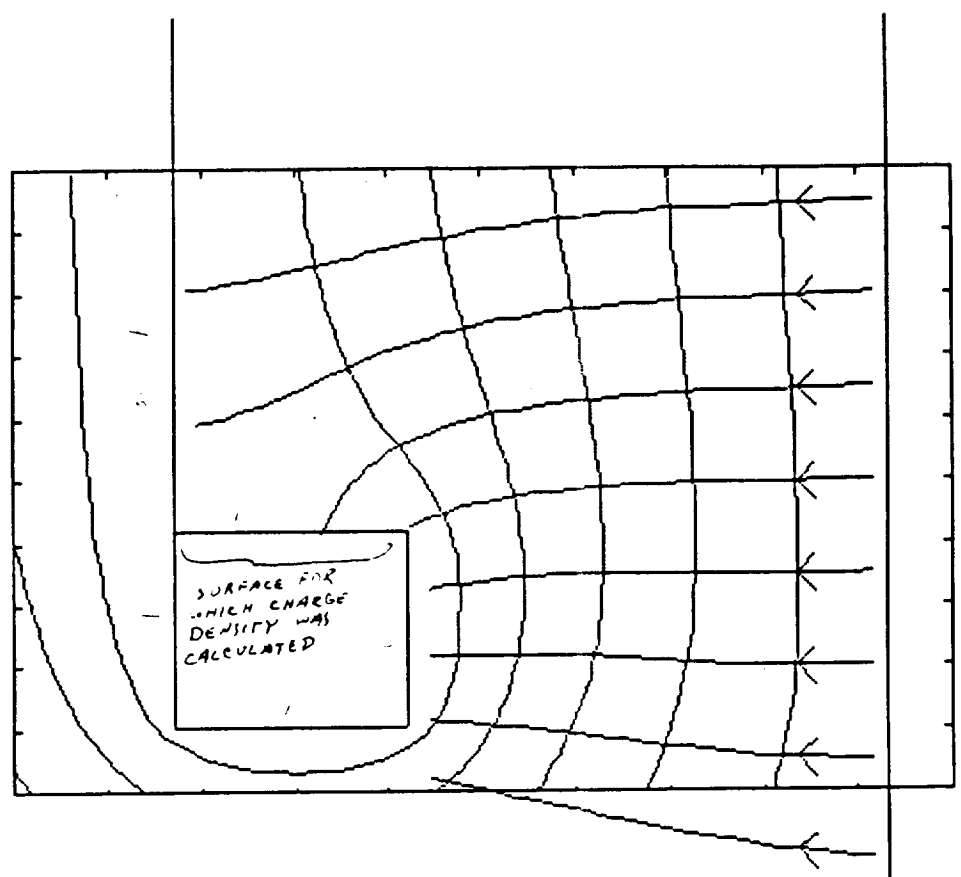
Resolution: 51

Units are:
Centimeters
Volts

CURSOR AT:
x = 50.00
y = 2.29

Type ? for list
of commands.

Total # of
boundaries = 18
Total # of
segments = 58



Electric field at (1.5,0.1): Ex = -513.356 V/m, Ey = 10006.8 V/m
Do you wish to continue drawing electric field lines (y or n)?

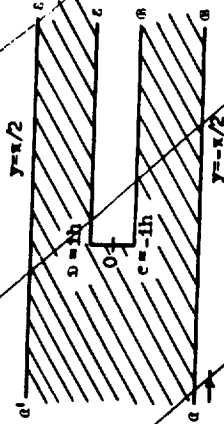
Figure 72

$$\frac{dz}{dw} = \frac{\sqrt{(w^2 - a^2)}}{w^2 - 1}, \quad 0 < a < 1.$$

$$z = \frac{1}{2} \left[\frac{w}{2} - \cosh^{-1} \frac{w}{a} + \frac{(1-a^2)^{1/2}}{2} \cosh^{-1} \frac{w^2(2-a^2)-a^2}{a^2(w^2-1)} \right].$$

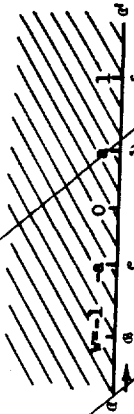
z - plane

points $z = 0; -ih; ih$



w - plane

points $w = 0; -a; a$



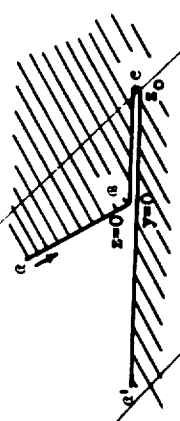
$$a = \frac{2}{\pi} \sqrt{(x-h)^2}, \quad 0 < h < \frac{1}{2}\pi - \frac{1}{2}\pi\sqrt{(1-a^2)} < \frac{1}{2}\pi$$

12.8 Further transformations.

$$\frac{dz}{dw} = -\frac{w}{(w+1)^\beta}, \quad 0 < \beta < 1; \quad z = -\frac{1}{2-\beta}(w+1)^{2-\beta} + \frac{1}{1-\beta}(w+1)^{1-\beta}.$$

z - plane

points $z = 0; \{(1-\beta)(2-\beta)\}^{-1} = z_0$



$$c = \frac{1}{1-\beta}$$

w - plane

points $w = -1; 0$

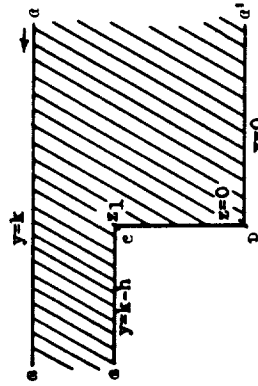


$$\frac{dz}{dw} = \frac{k(w-1)^{1/2}}{\pi w(w-c)^{1/2}}, \quad c > 1; \quad k > 0, \quad kc^{-1/2} = h$$

$$z = \frac{1}{\pi} \cosh^{-1} \left(\frac{2w-c-1}{c-1} \right) - \frac{k}{\pi\sqrt{c}} \cosh^{-1} \left(\frac{(c+1)w-2c}{(c-1)w} \right)$$

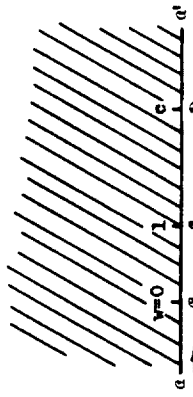
z - plane

points $1(k-h) = z_1; 0$



w - plane

points $w = 1; c$



$$\frac{dz}{dw} = \frac{(w+1)^\beta}{w-1}, \quad 0 < \beta < 1.$$

Representable in terms of elementary functions, if $\beta = p/q$ (p, q integers):

$$z = 2q \int_c^\infty t^{p+q-1}(t^q-1)^{-2} dt, \quad \text{where } \zeta = (w+1)^{1/q}(w-1)^{-1/q}.$$

z - plane

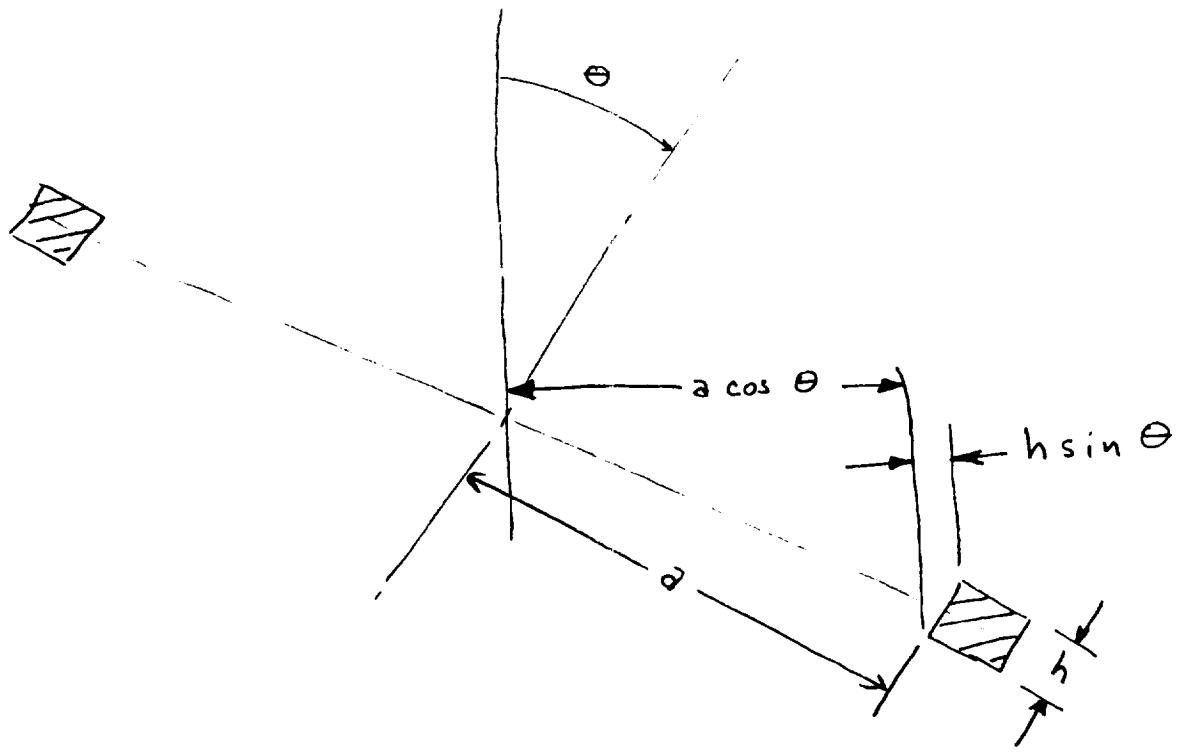
points $z = 0; \beta$



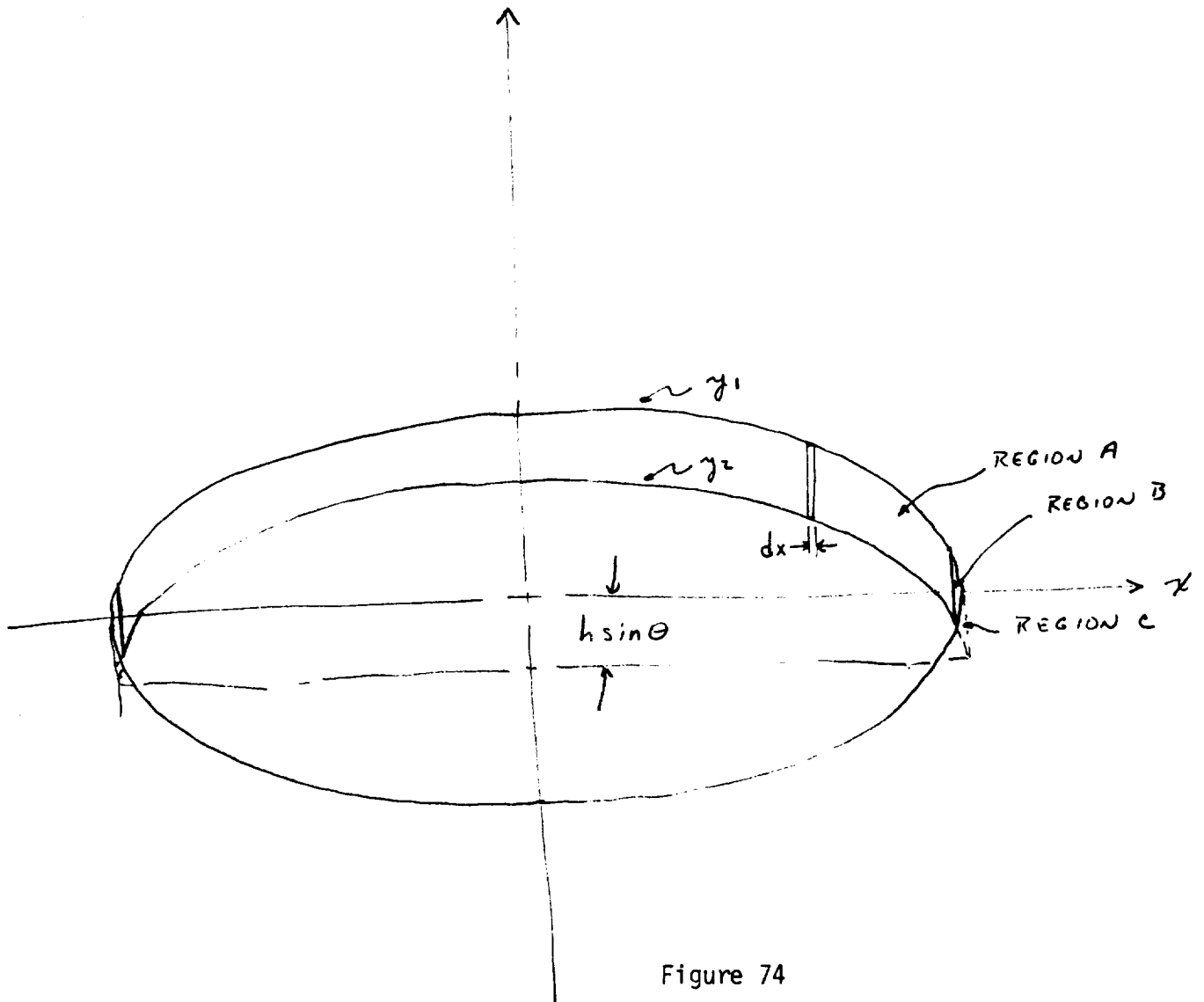
w - plane



Figure 73

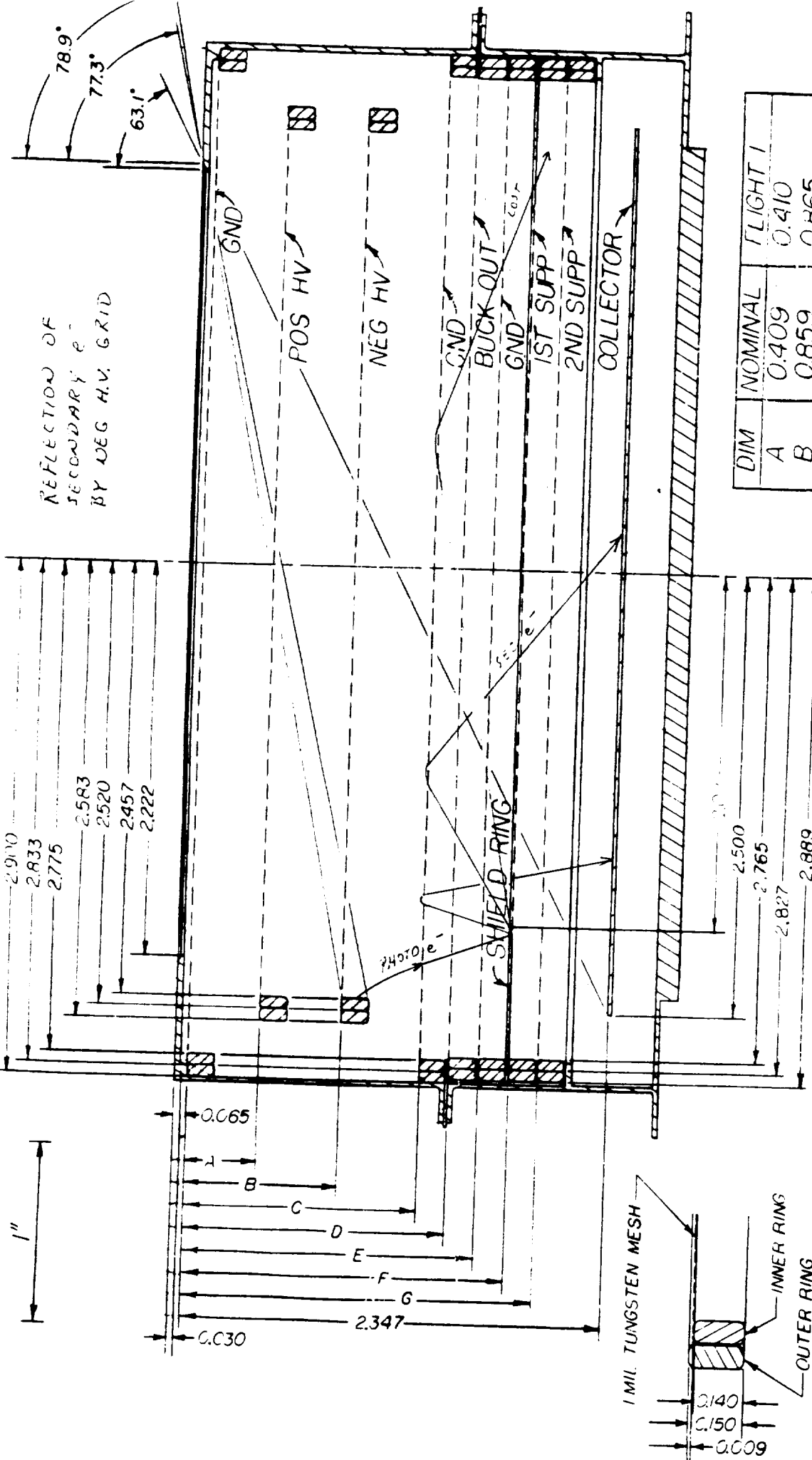


SIDE VIEW



FRONT VIEW

Figure 74

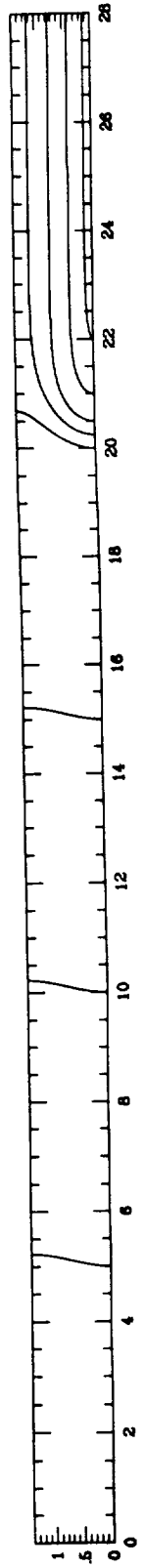


DIM	NOMINAL	FLIGHT 1
A	0.409	0.410
B	0.859	0.865
C	1.311	1.300
D	1.476	1.475
E	1.638	1.625
F	1.803	1.845
G	1.965	1.965

PLS SIDE SENSOR

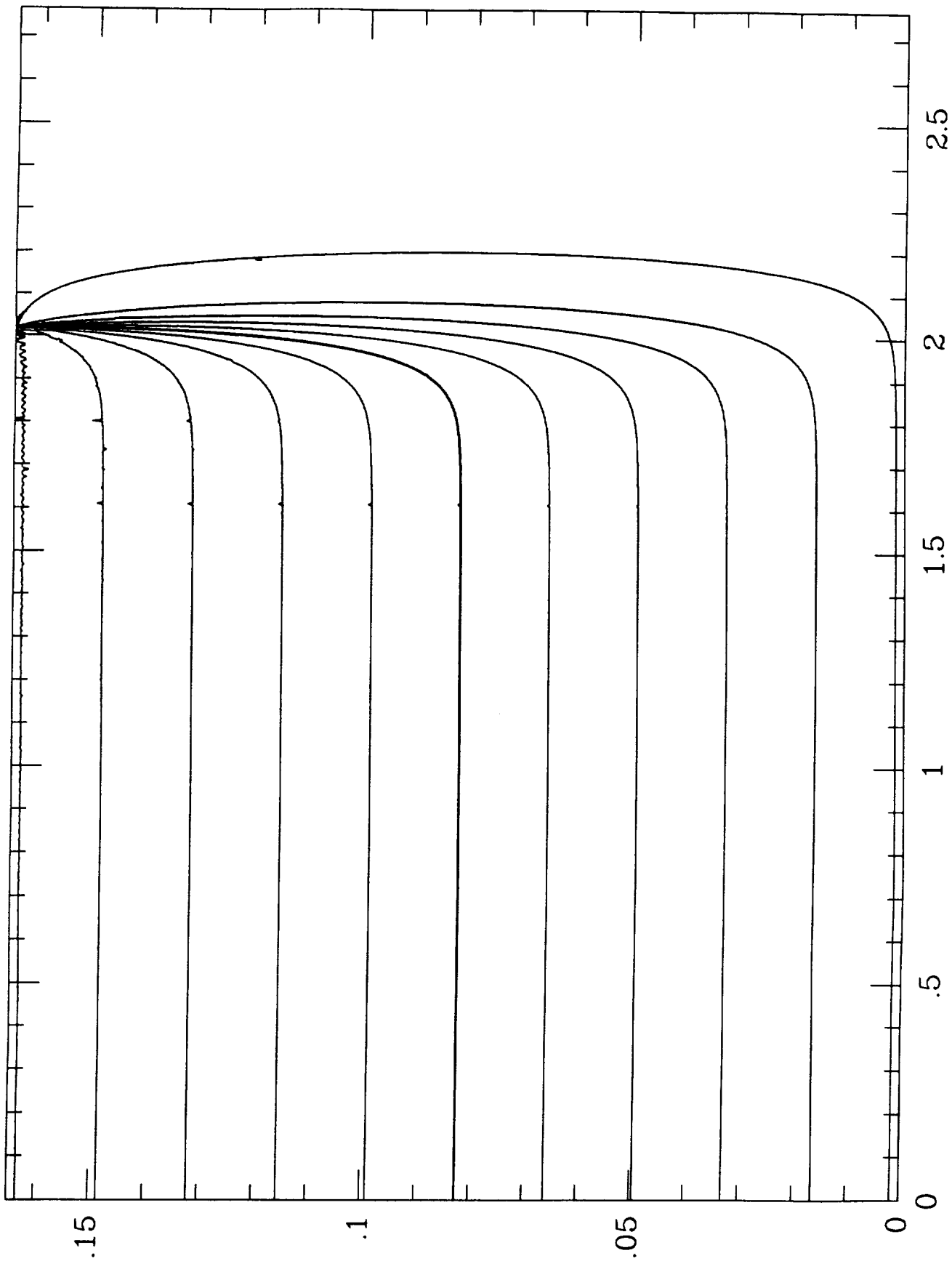
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Figure 75



R

Figure 76



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Figure 77

9-2's 1024
642 x 664

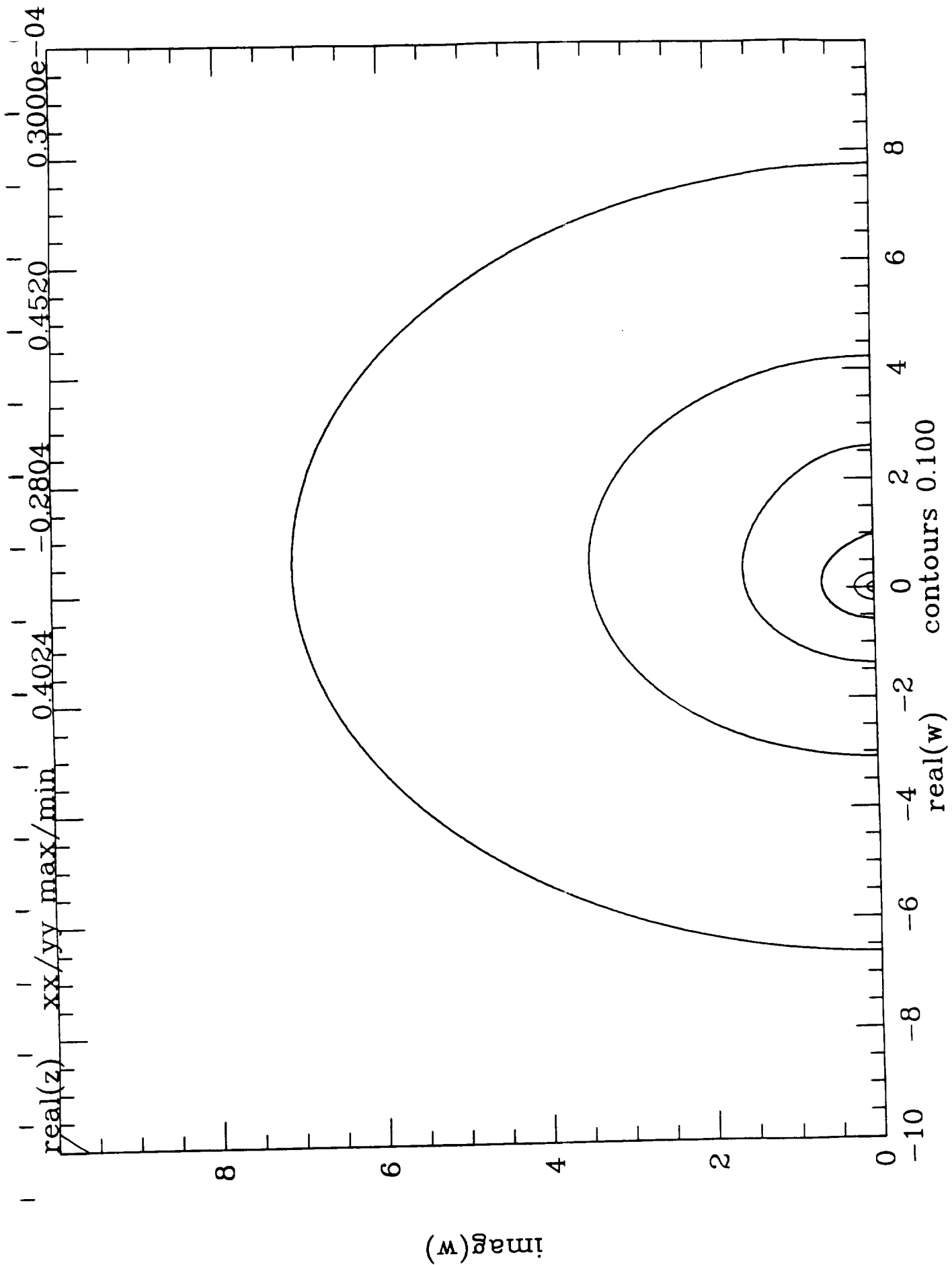
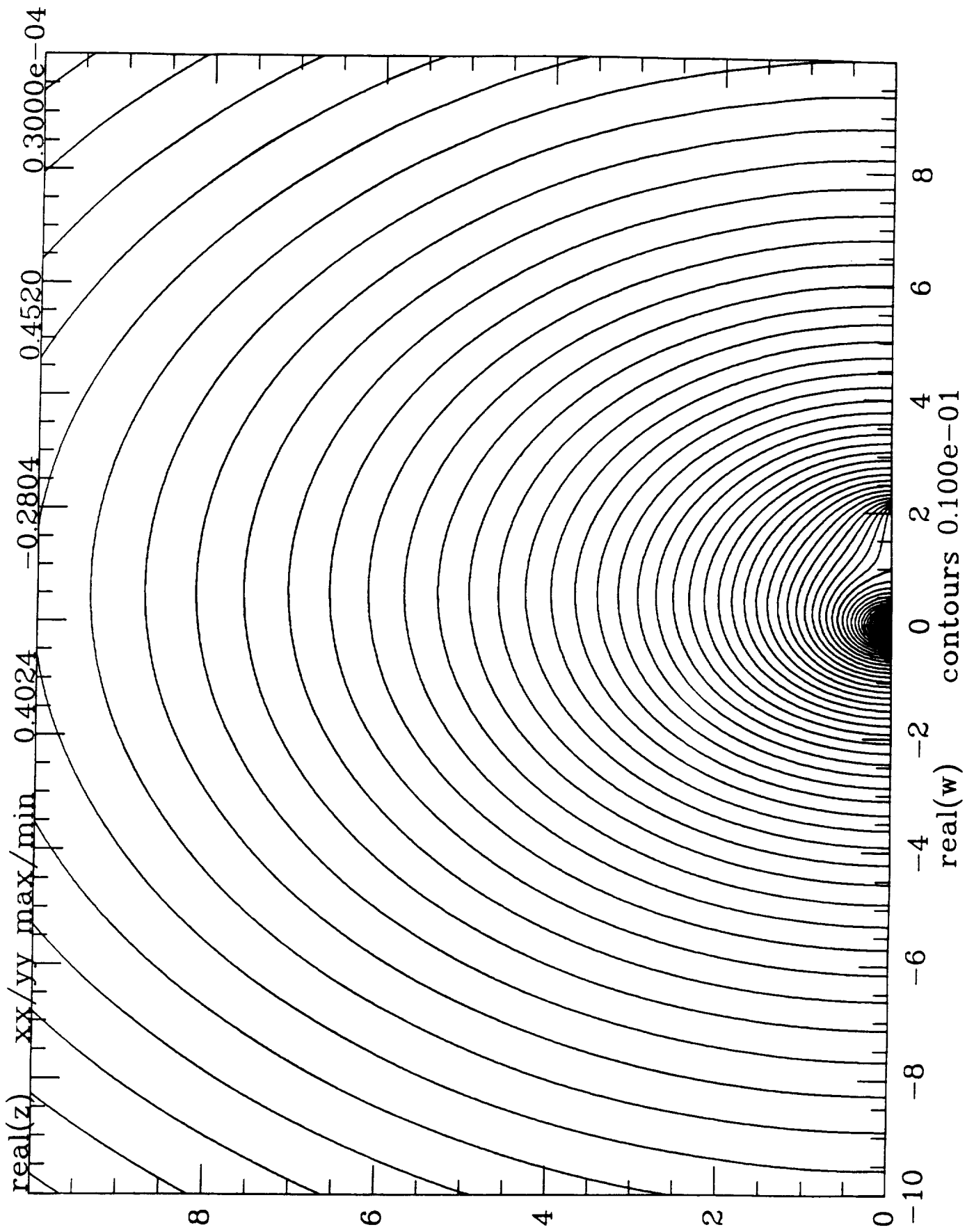


Figure 78



$\text{imag}(w)$

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Figure 79

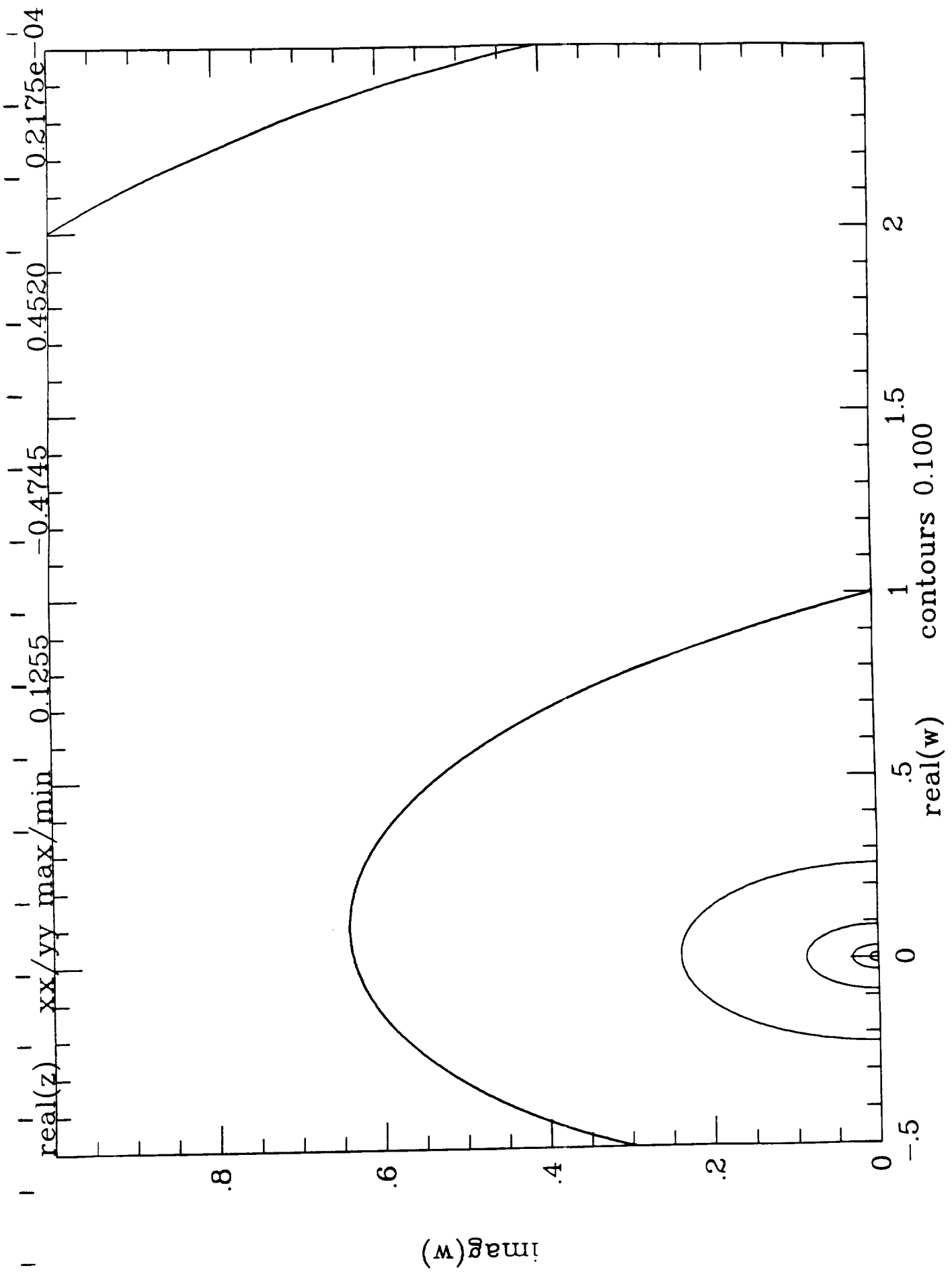


Figure 80

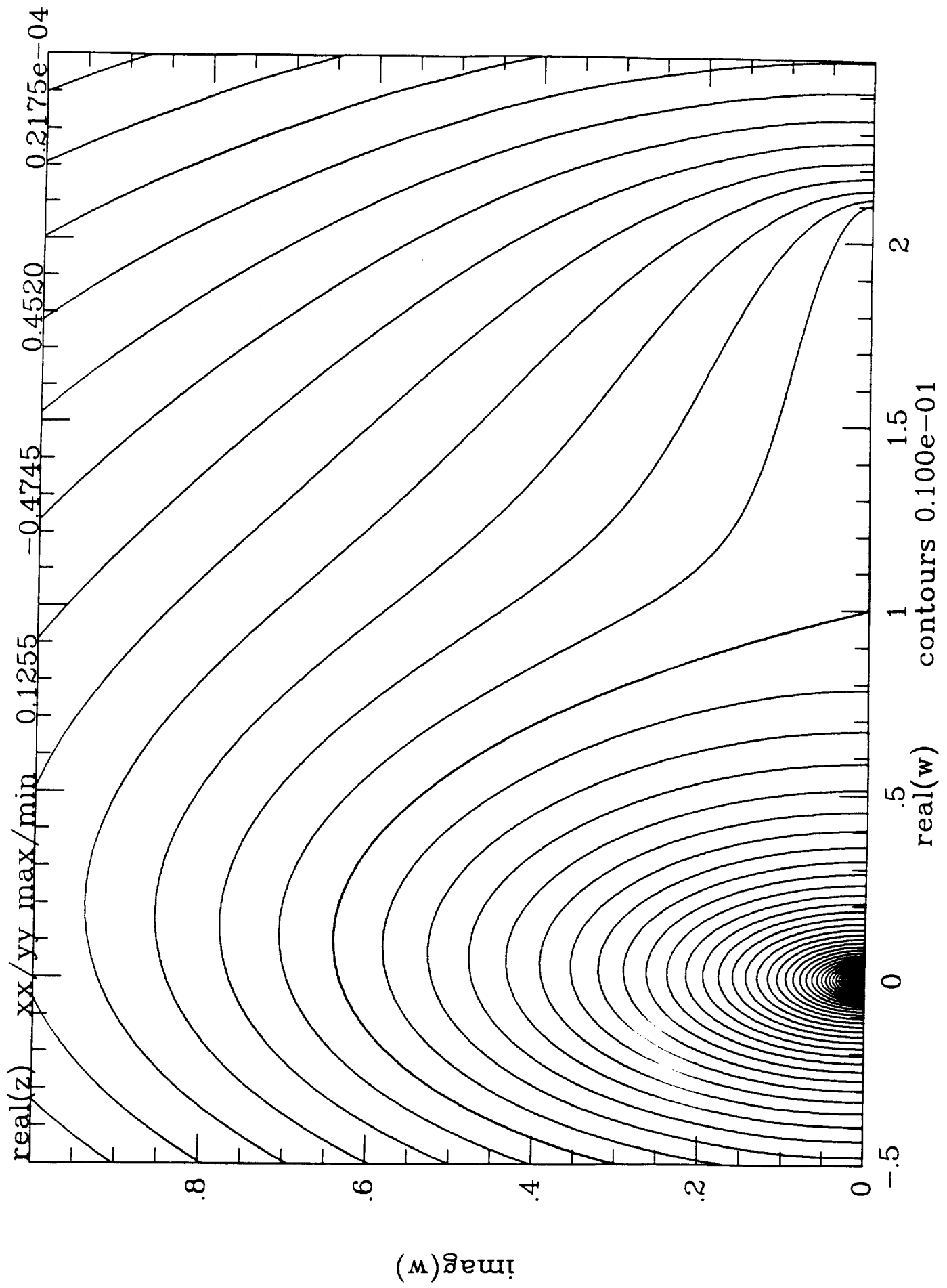


Figure 81

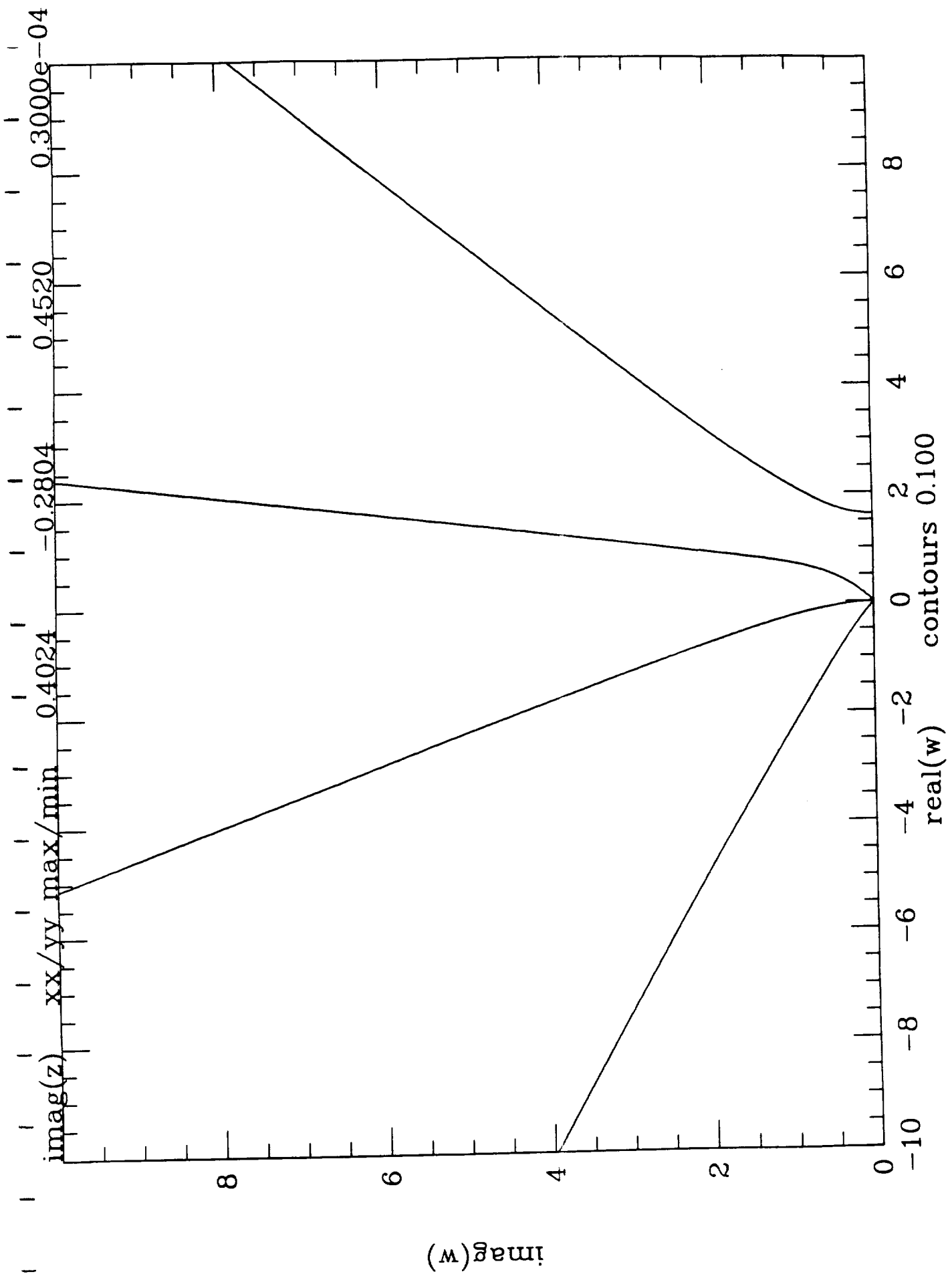


Figure 82

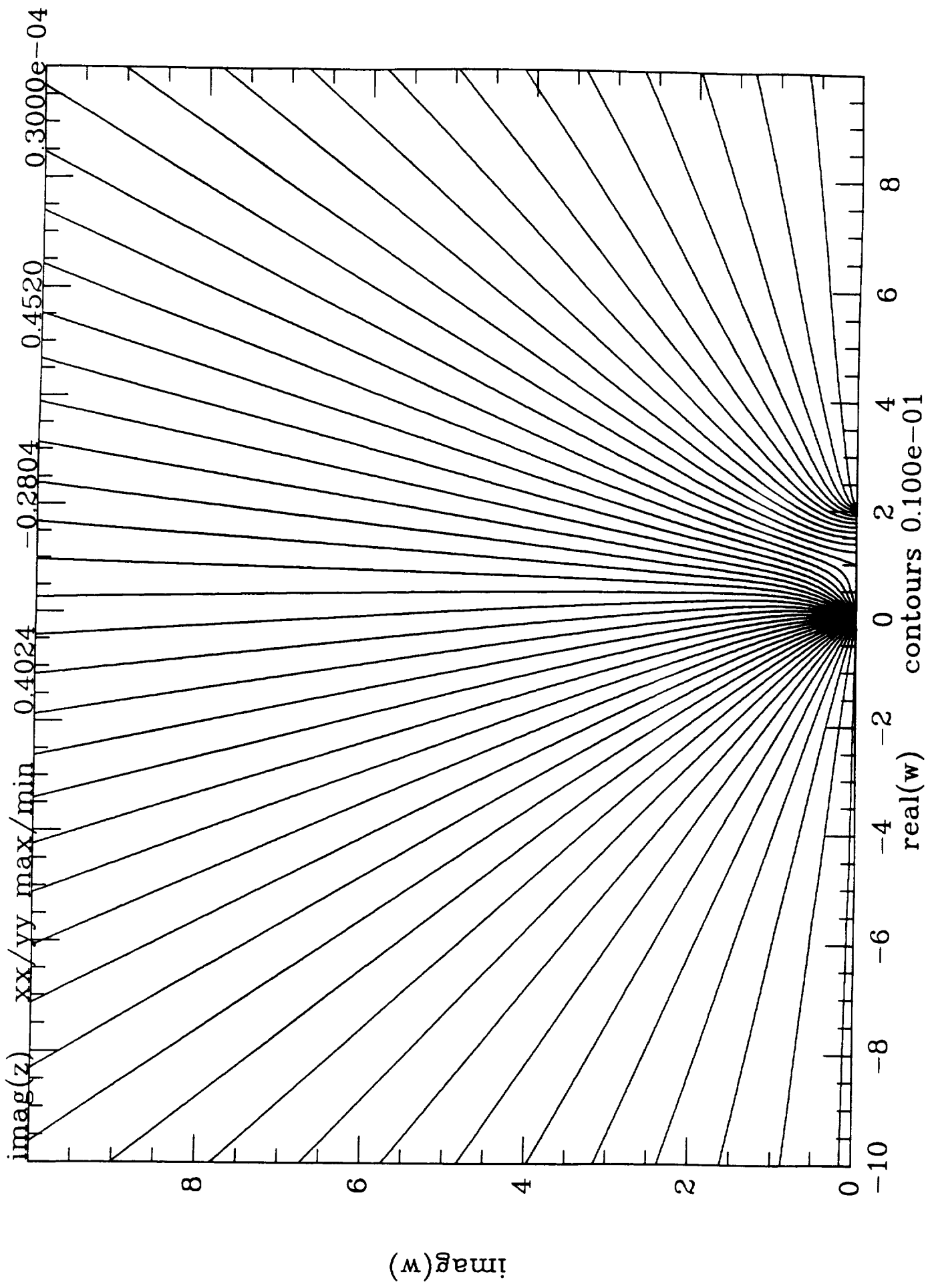


Figure 83

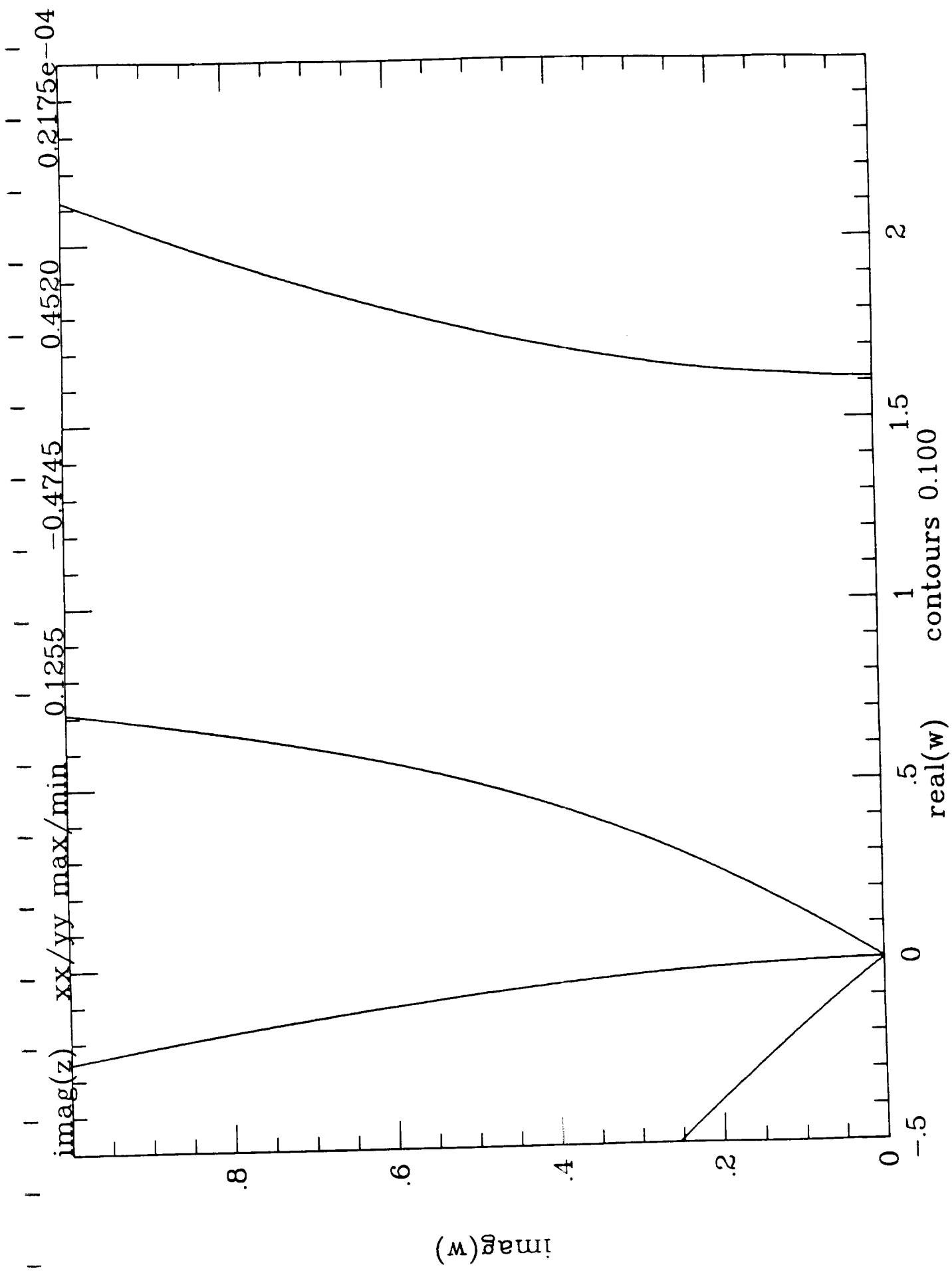


Figure 84

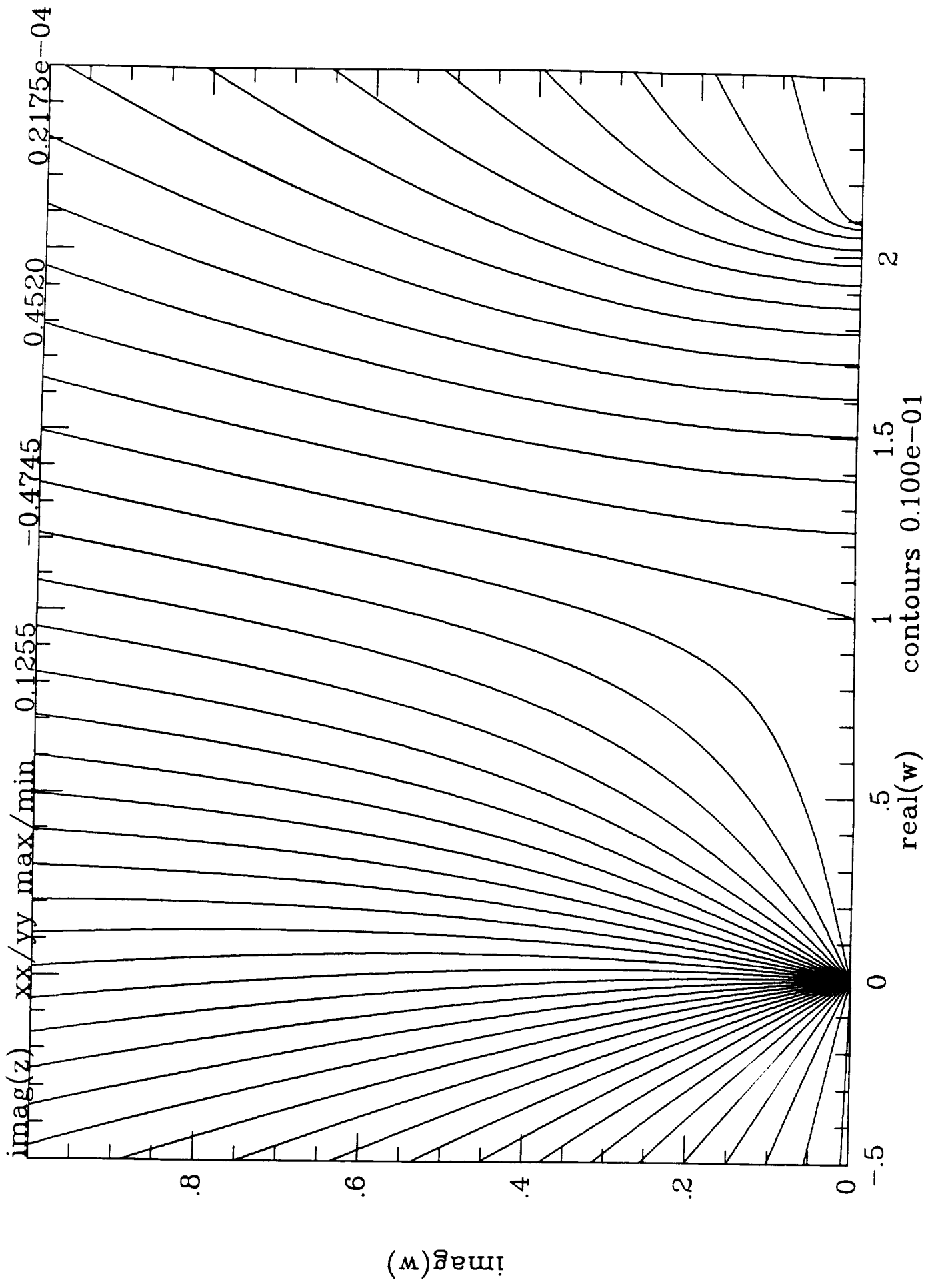


Figure 85

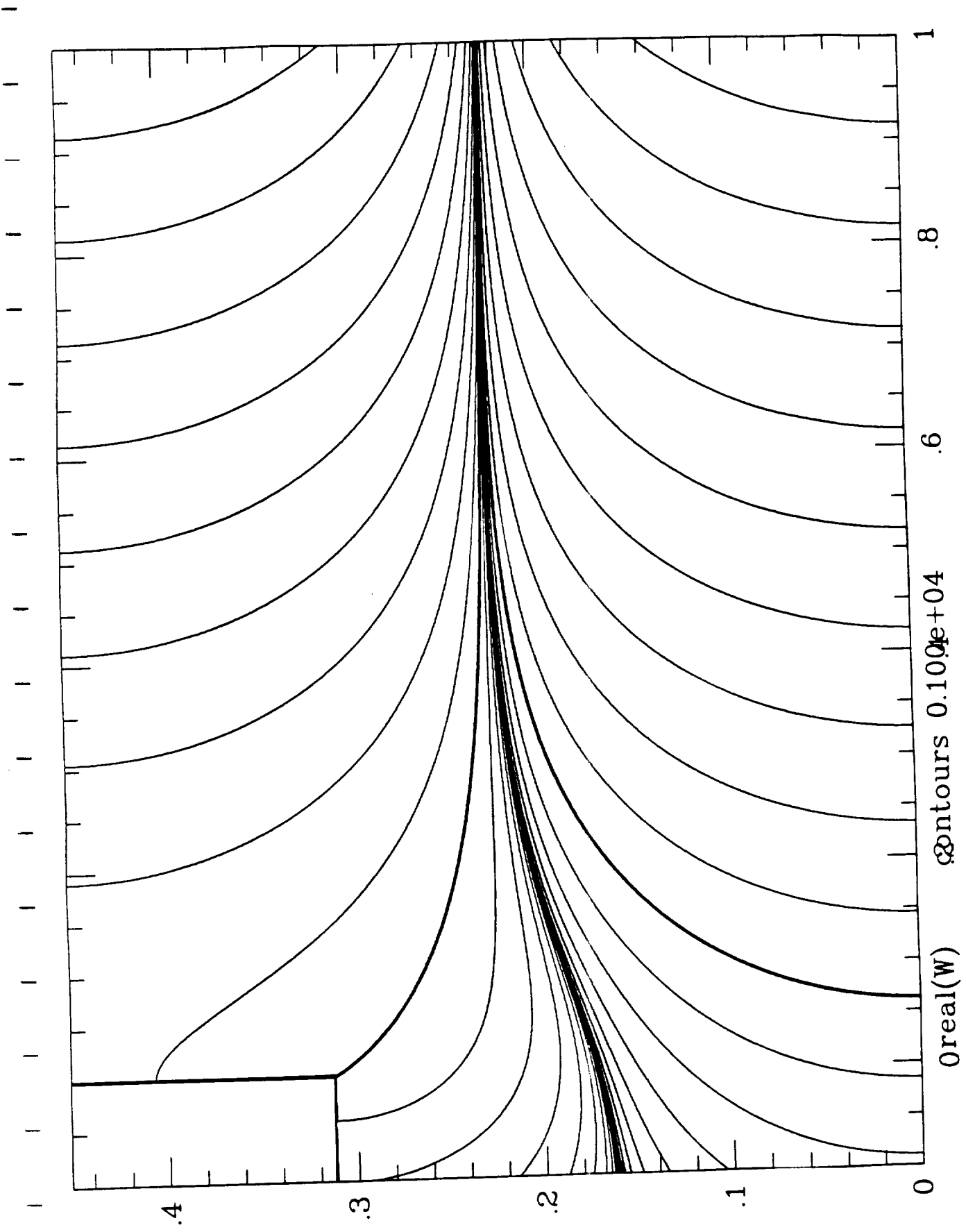


Figure 86

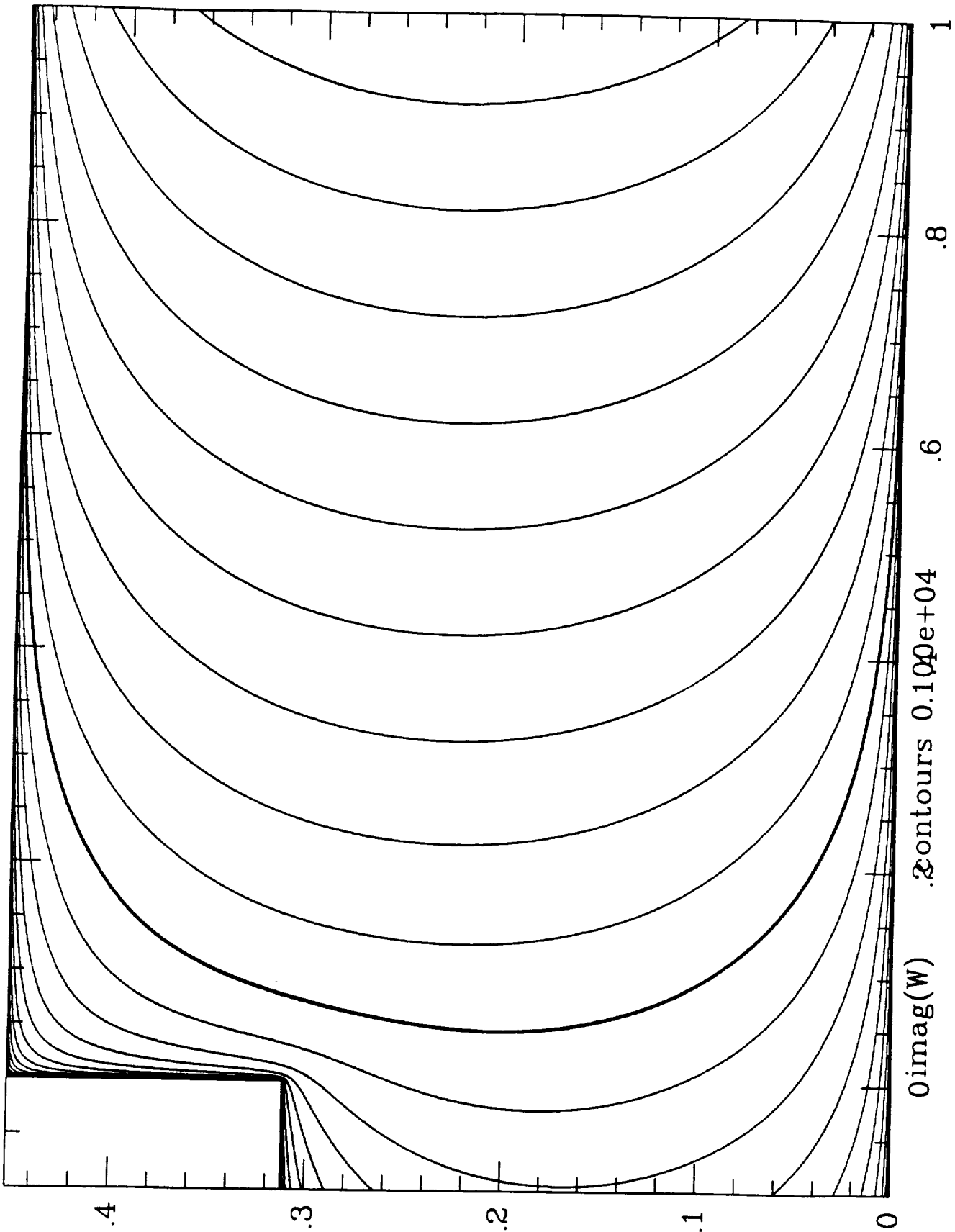


Figure 87

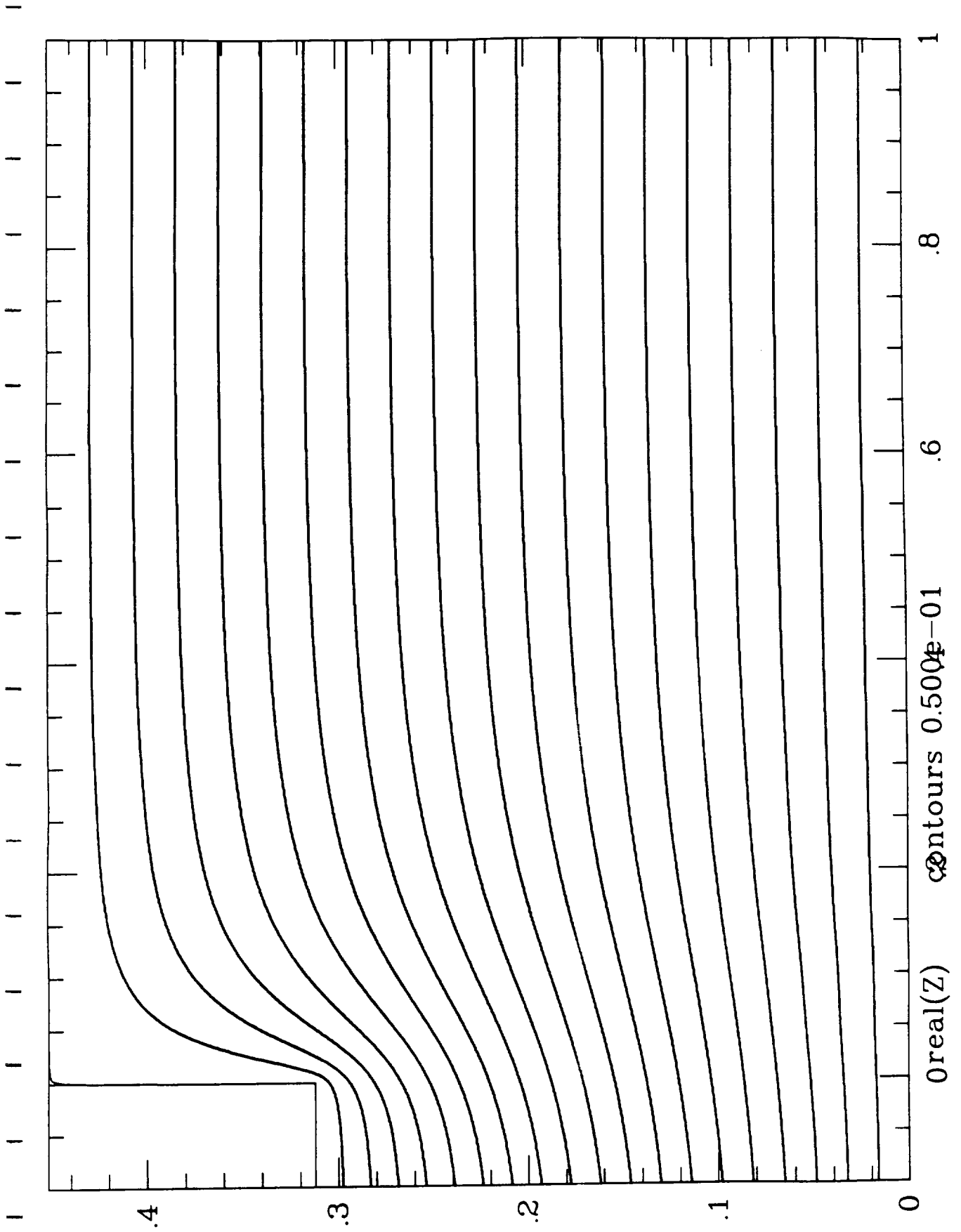


Figure 88

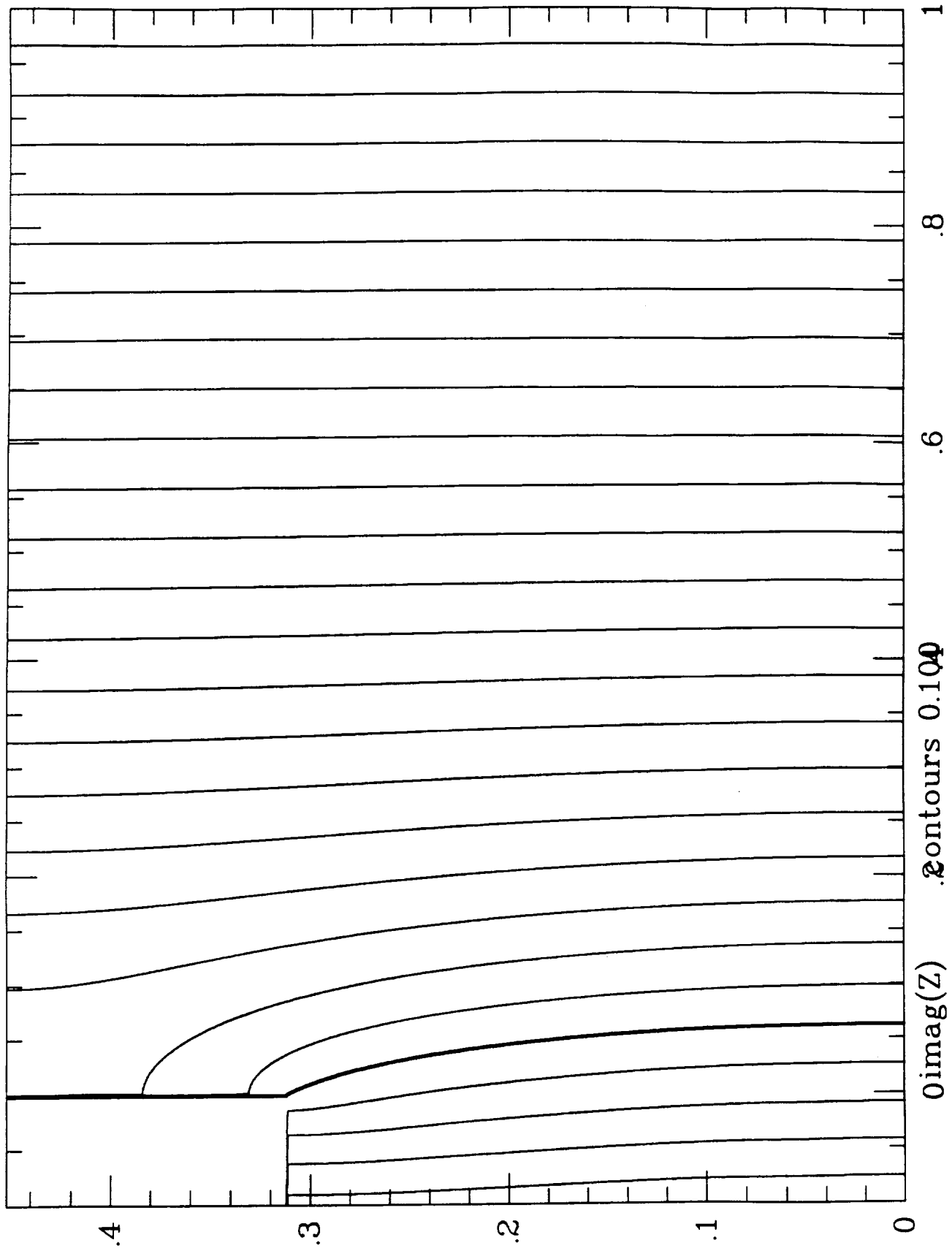


Figure 89

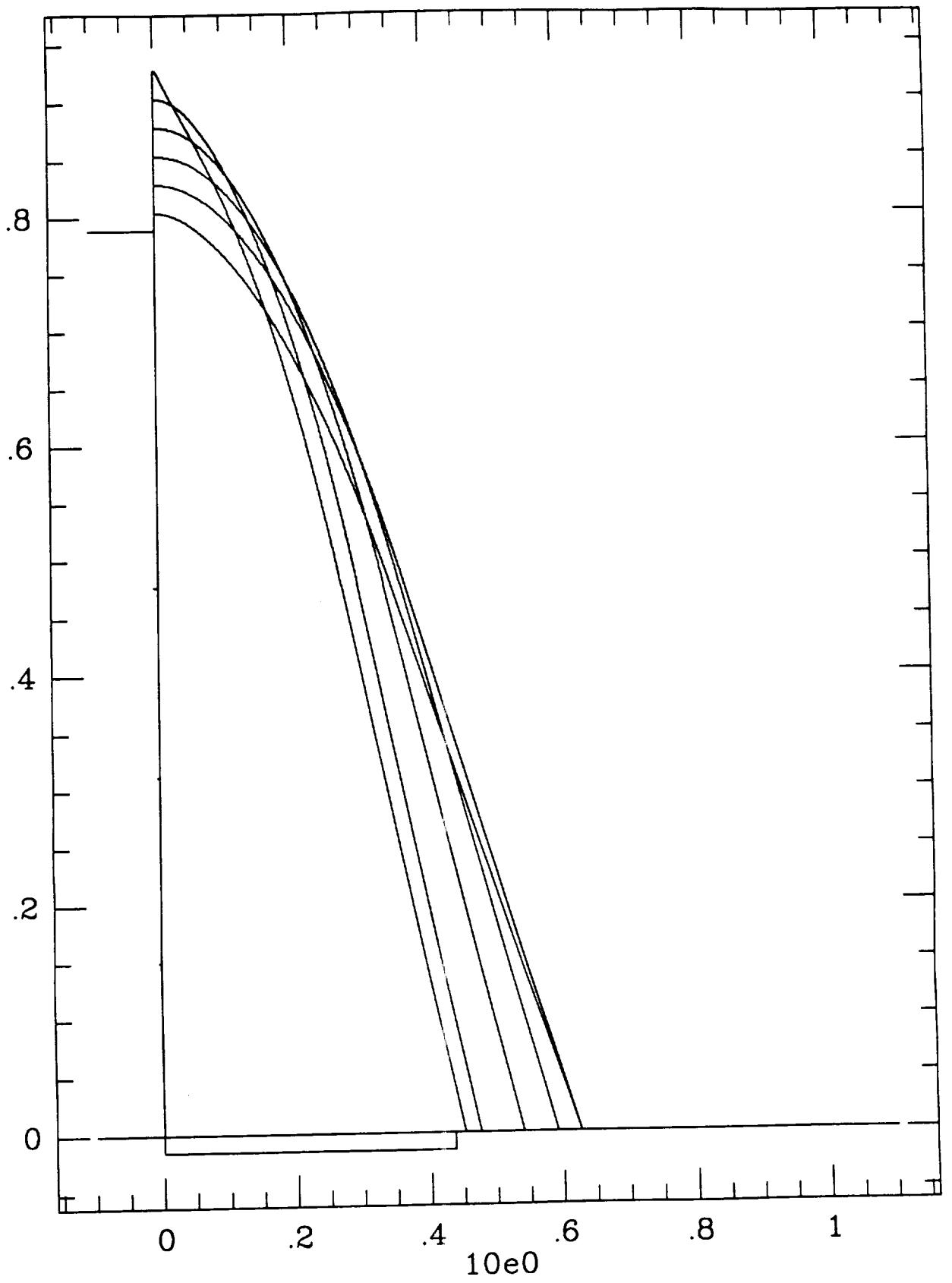


Figure 90

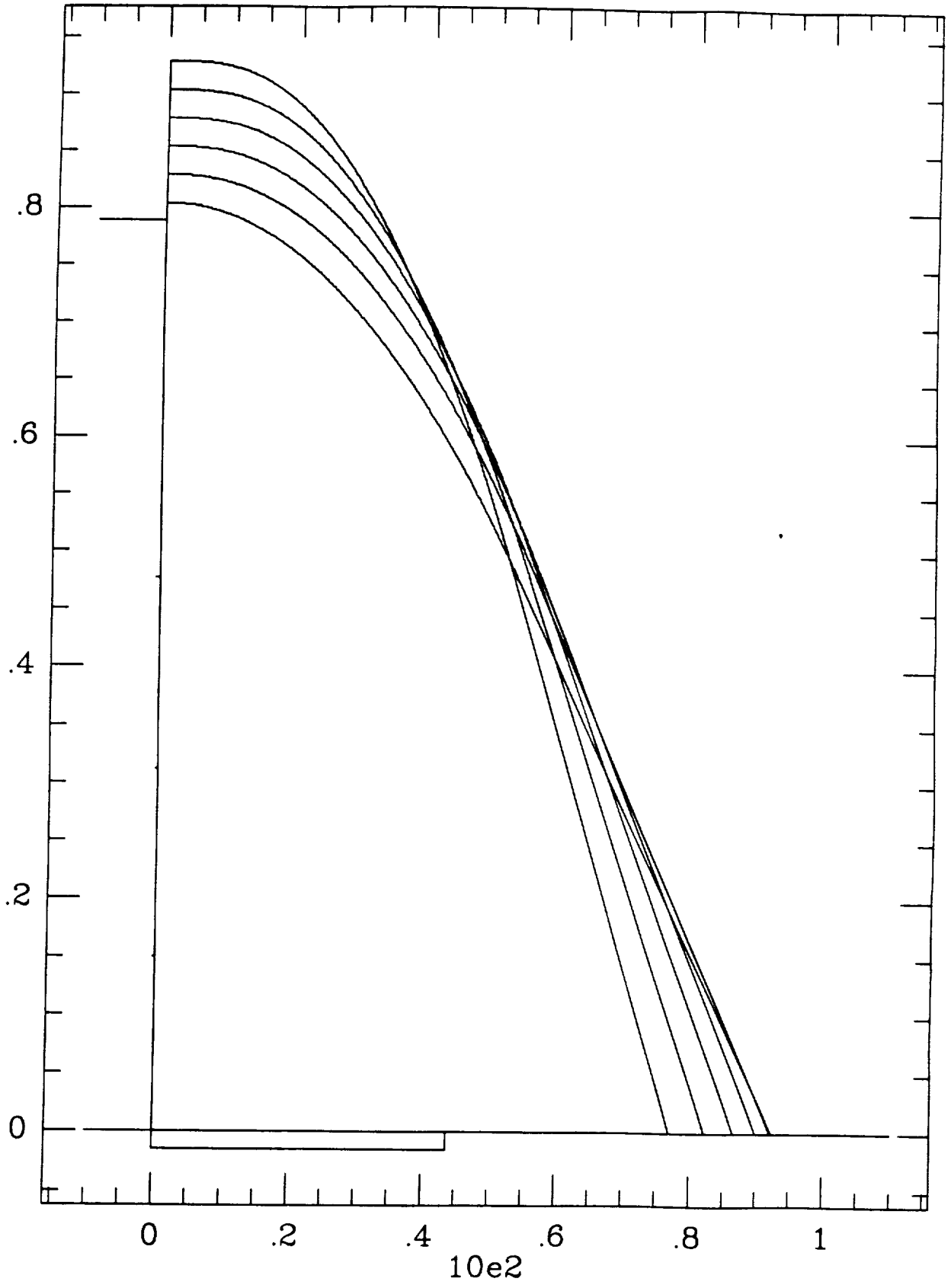


Figure 91

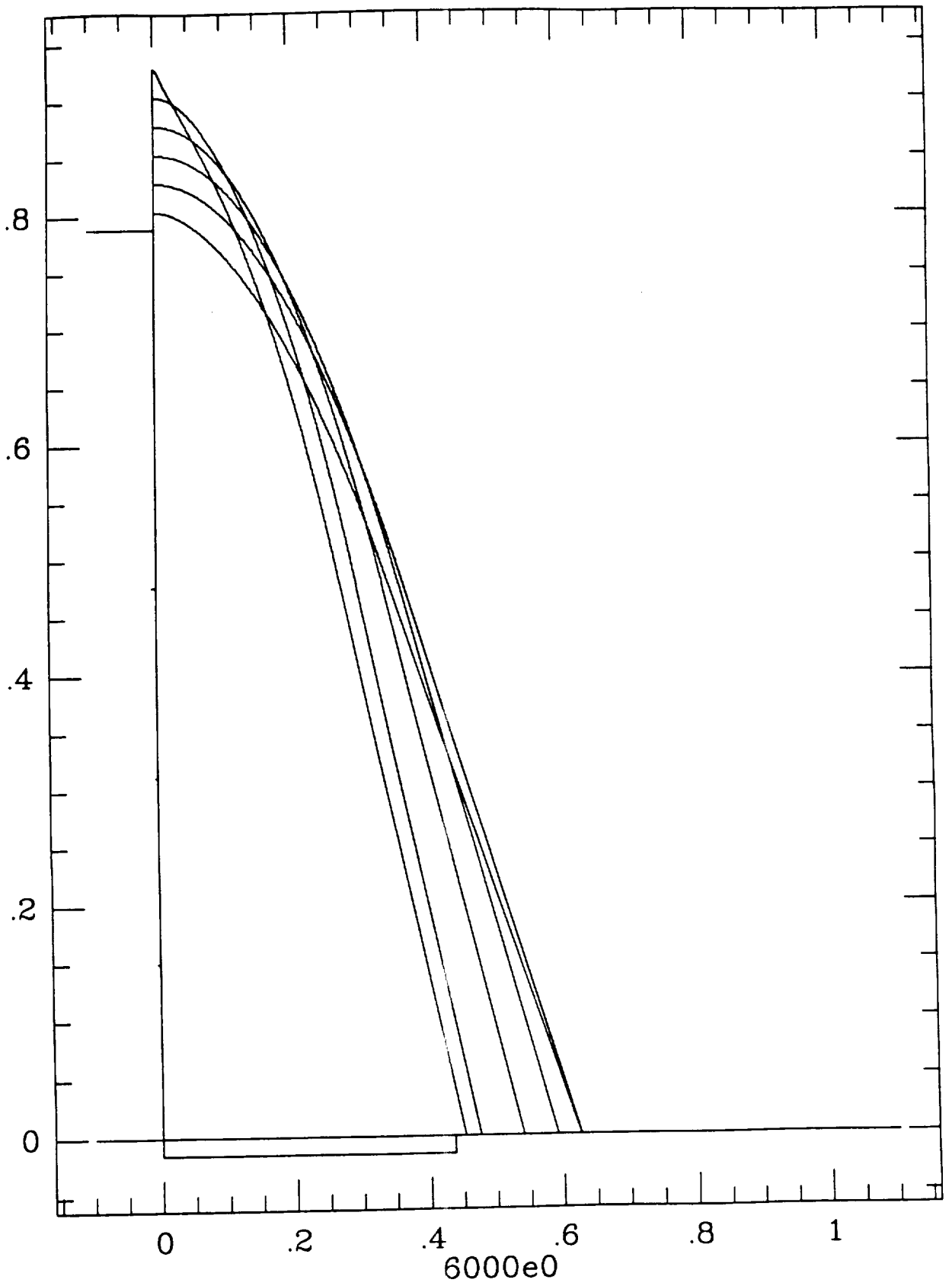


Figure 92

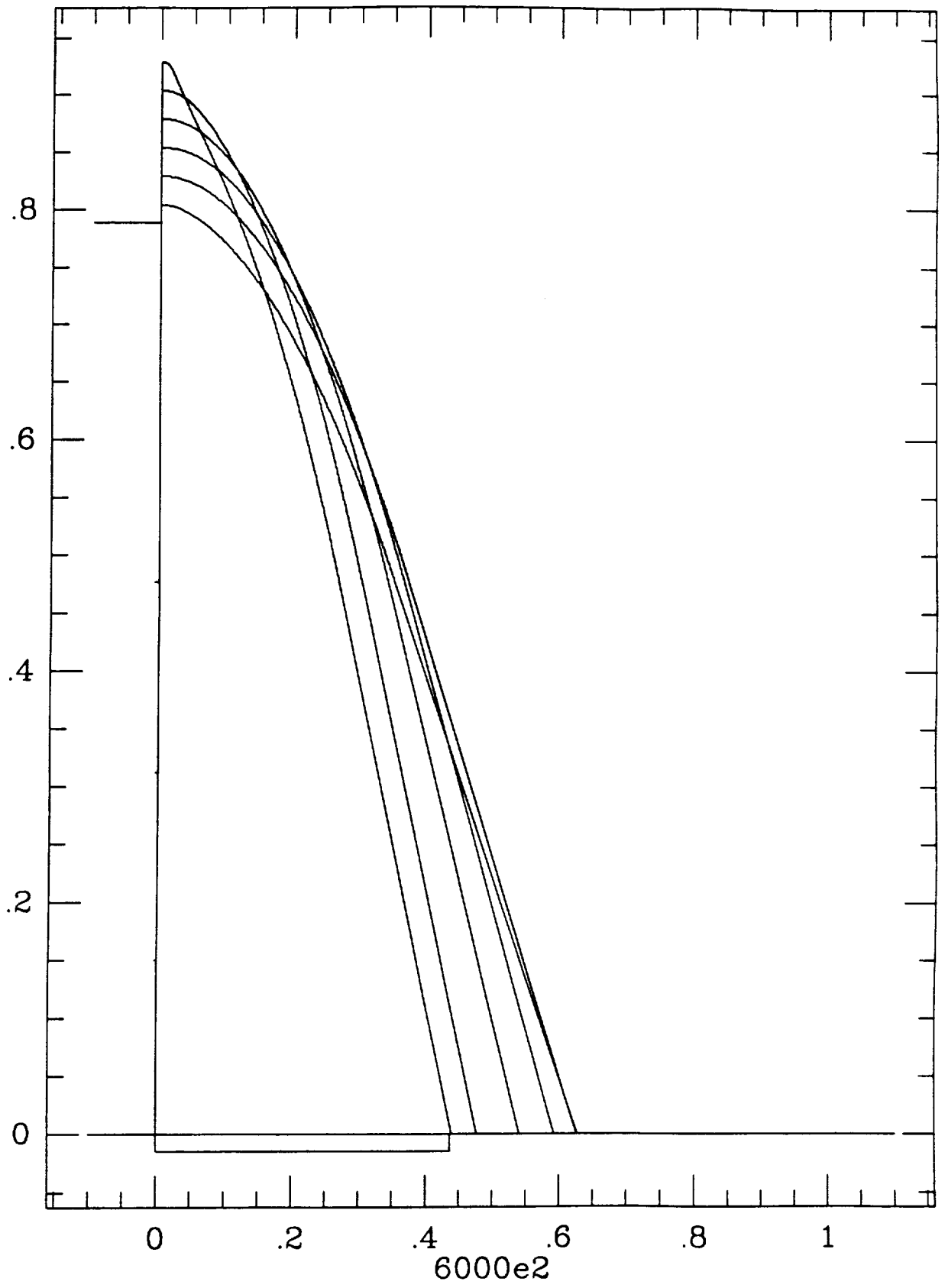


Figure 93

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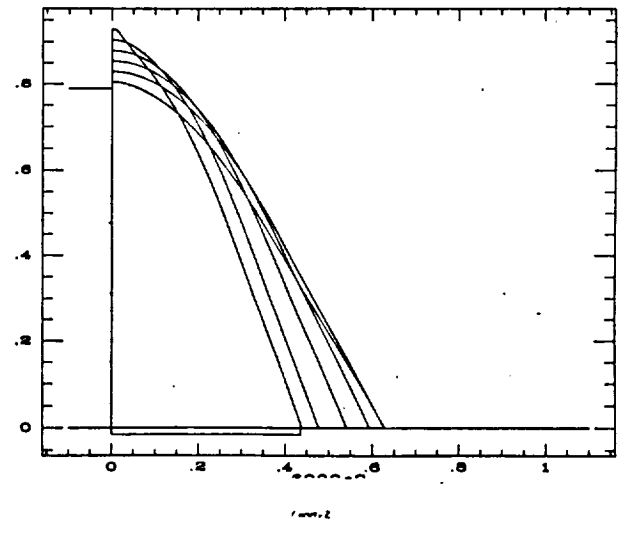
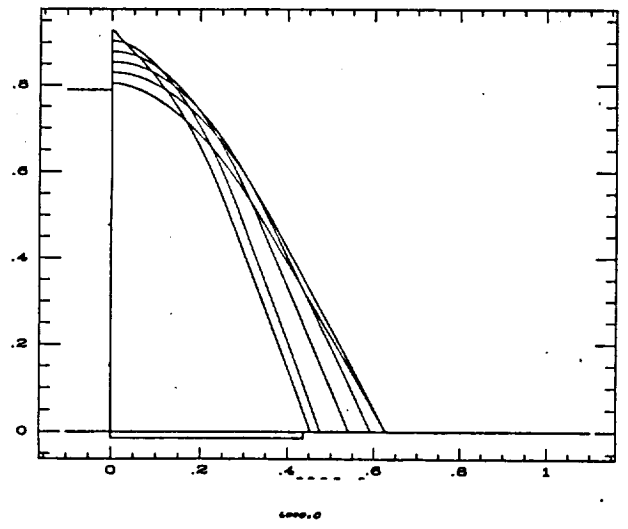
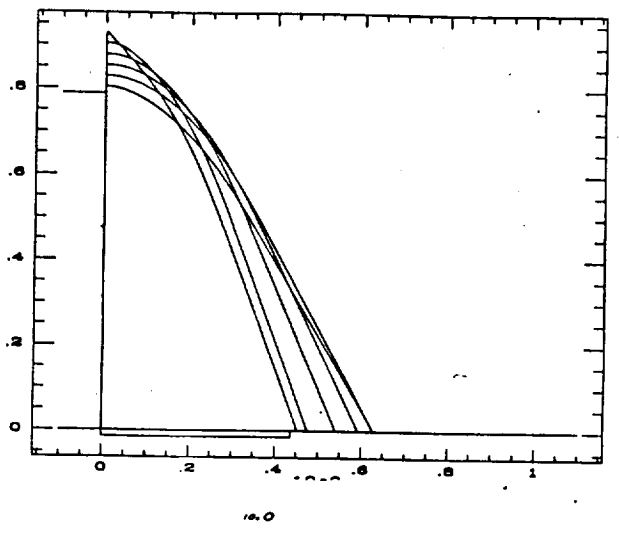
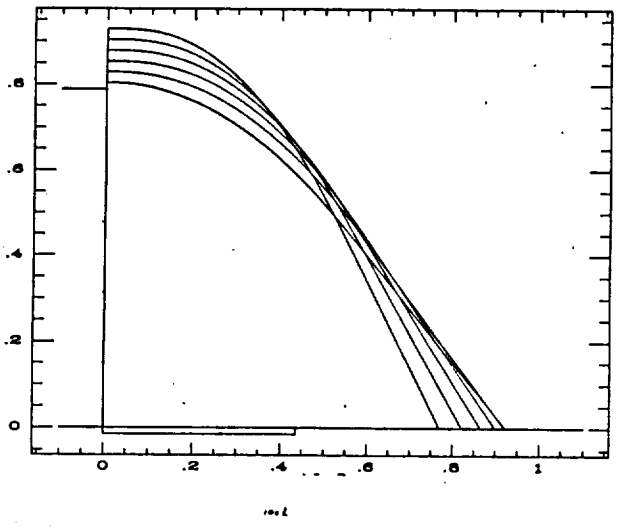
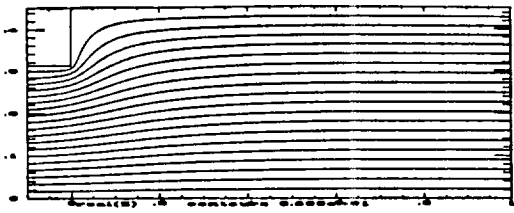


Figure 94

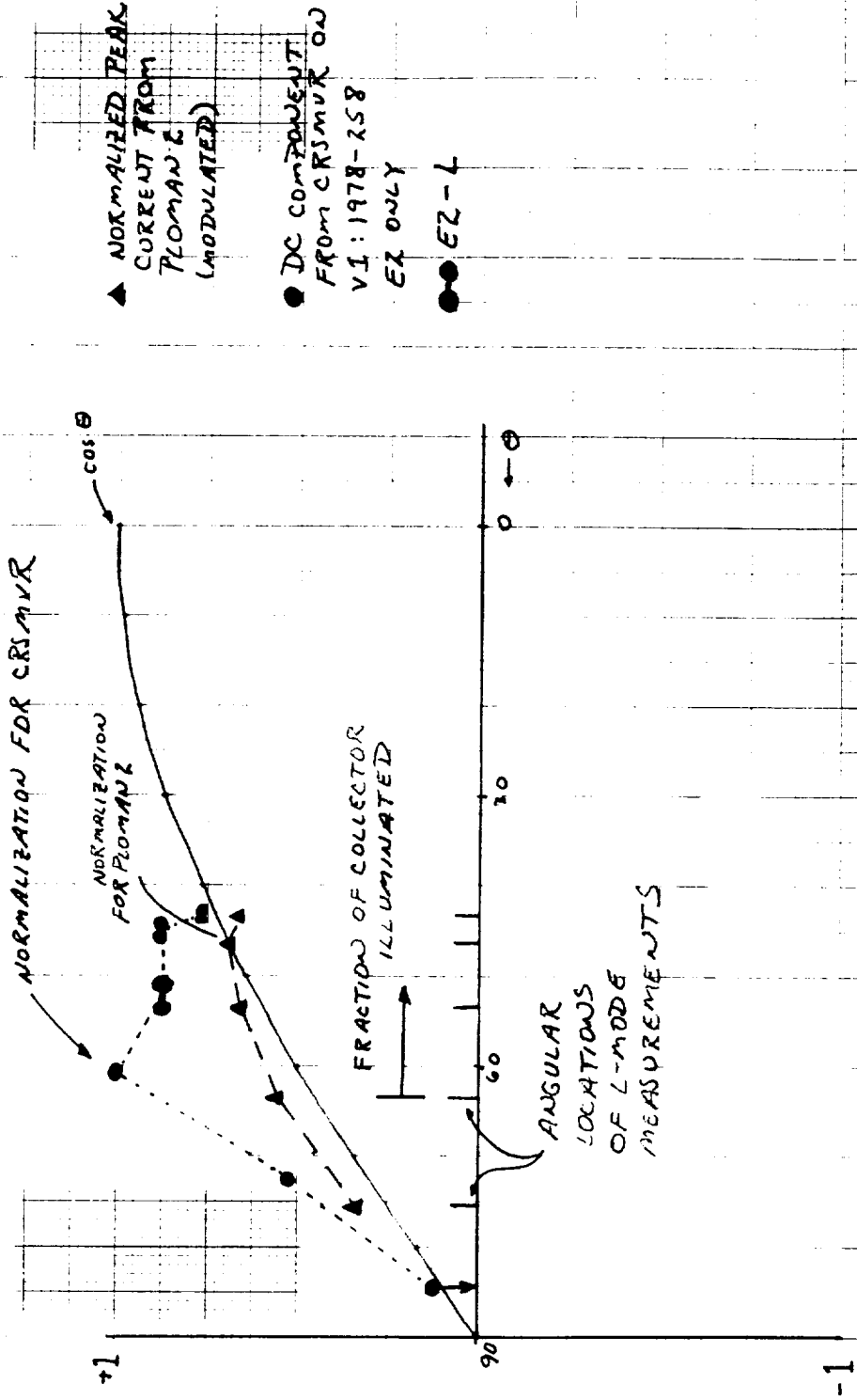
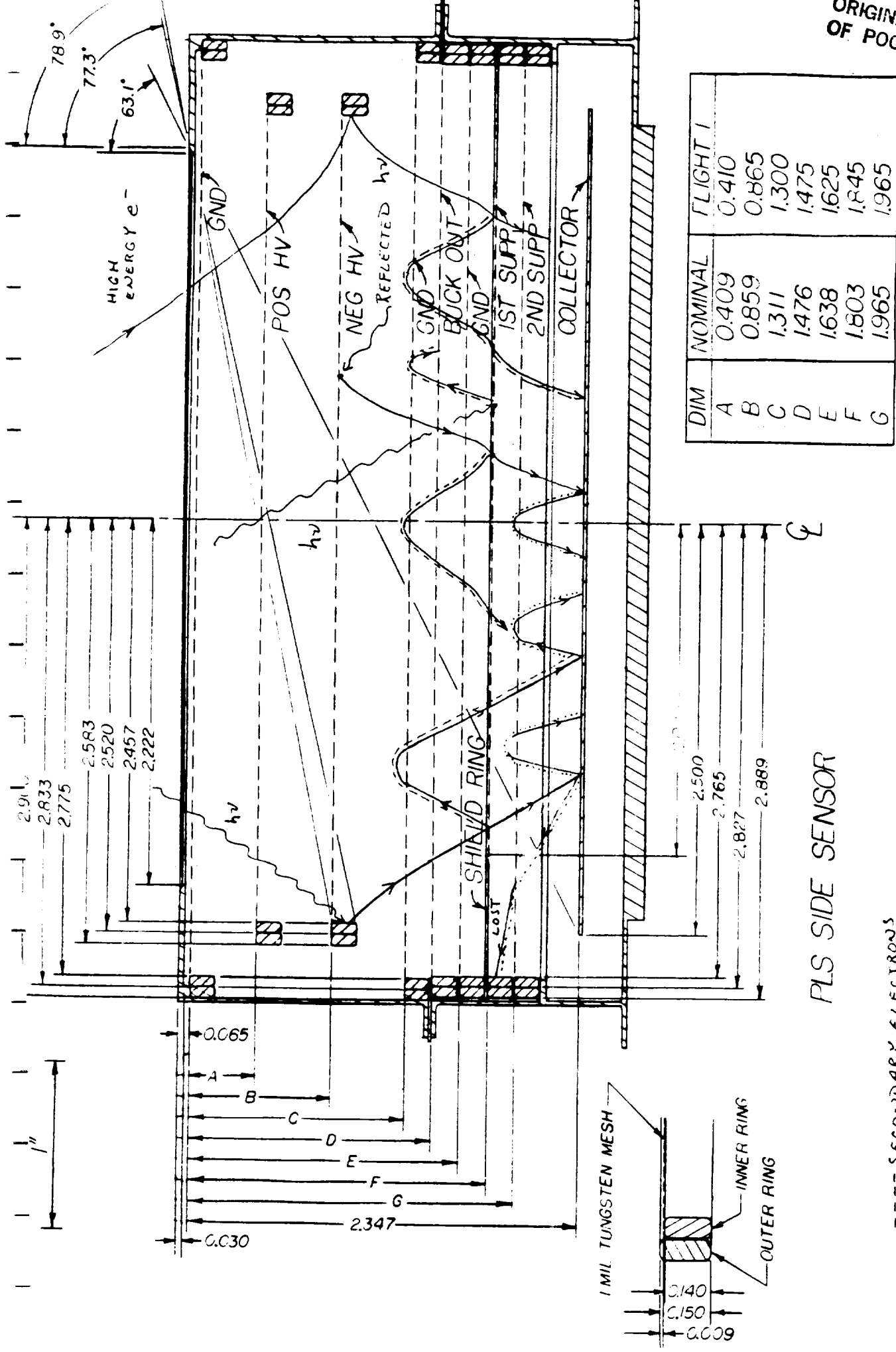


Figure 95

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PLS SIDE SENSOR

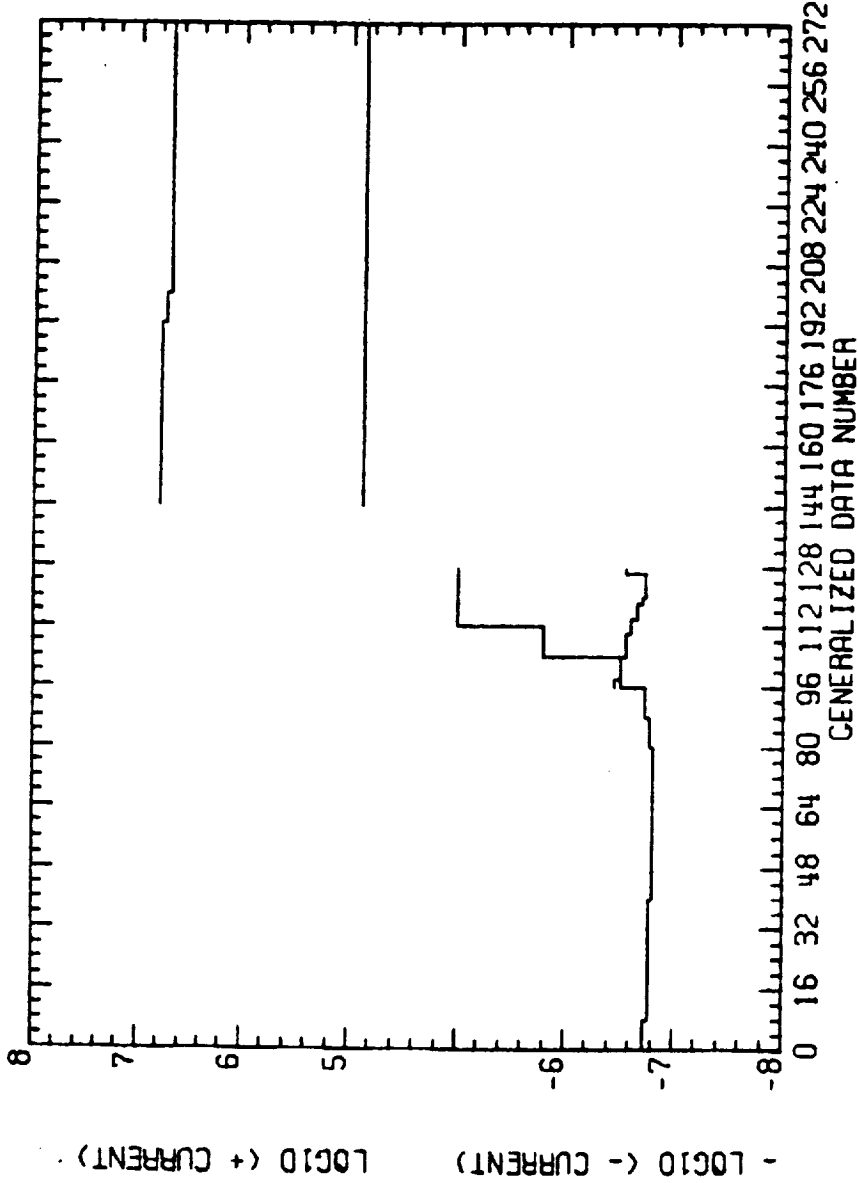
--- SECONDARY ELECTRONS
PRODUCED AT SUPPRESSOR GRID

..... SECONDARY ELECTRONS
PRODUCED AT COLLECTOR PLATE

Figure 96

DC RET MOD ON
NORMAC

VOYAGER DC RETURN DATA



NEPTUNE MAGNETOSPHERE

VOYAGER 2
L -MODE TIME 1977 243 1856: 9.627
E1 -MODE TIME 1977 243 1856: 32.627
M -MODE TIME 1977 243 1856: 56.627
E2 -MODE TIME 1977 243 1856: 56.627

Figure 97

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PLS MOD ON

VOYAGER DC RETURN DATA

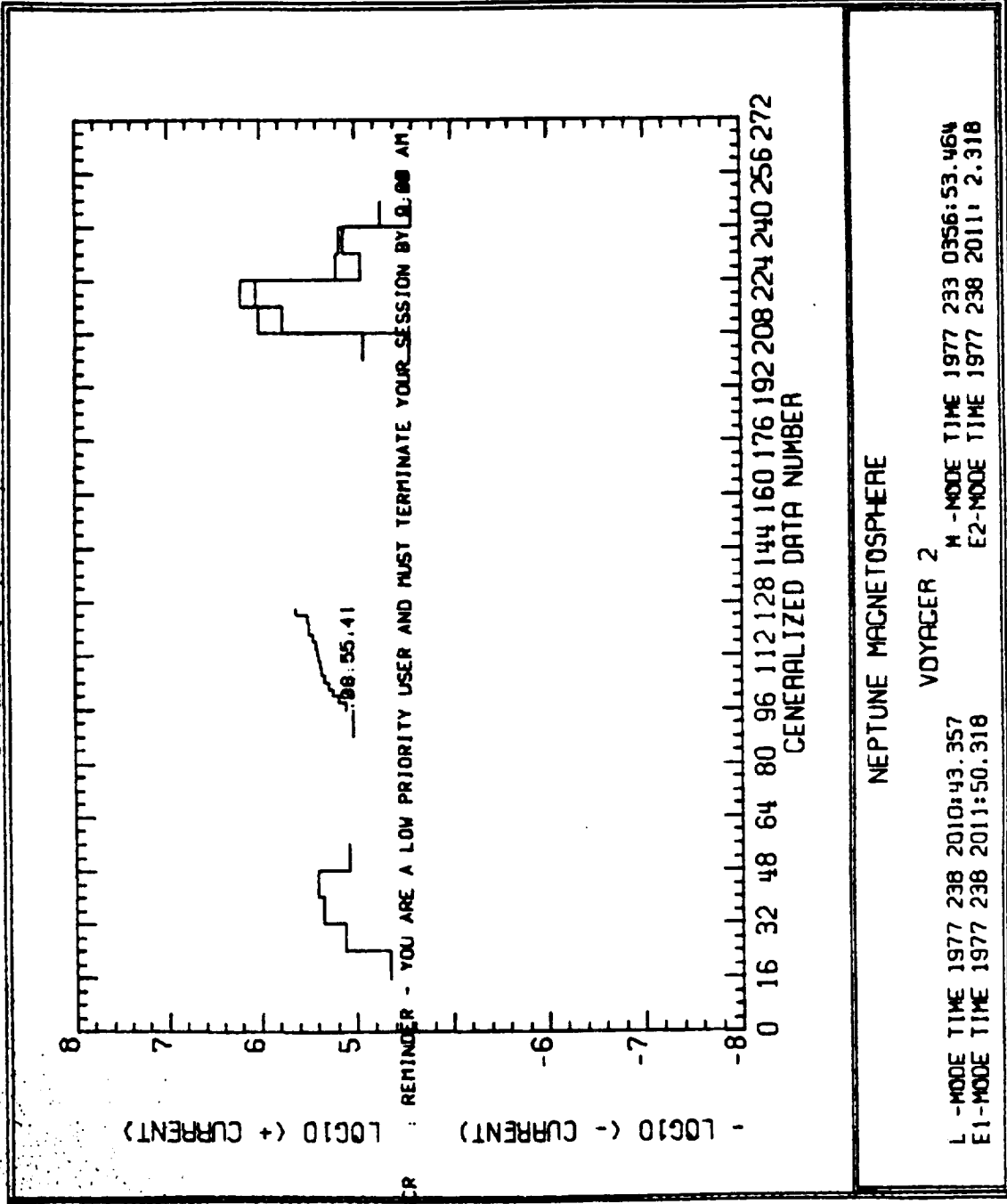


Figure 98

DC RET
~~REV~~ REV MOD ON

VOYAGER DC RETURN DATA

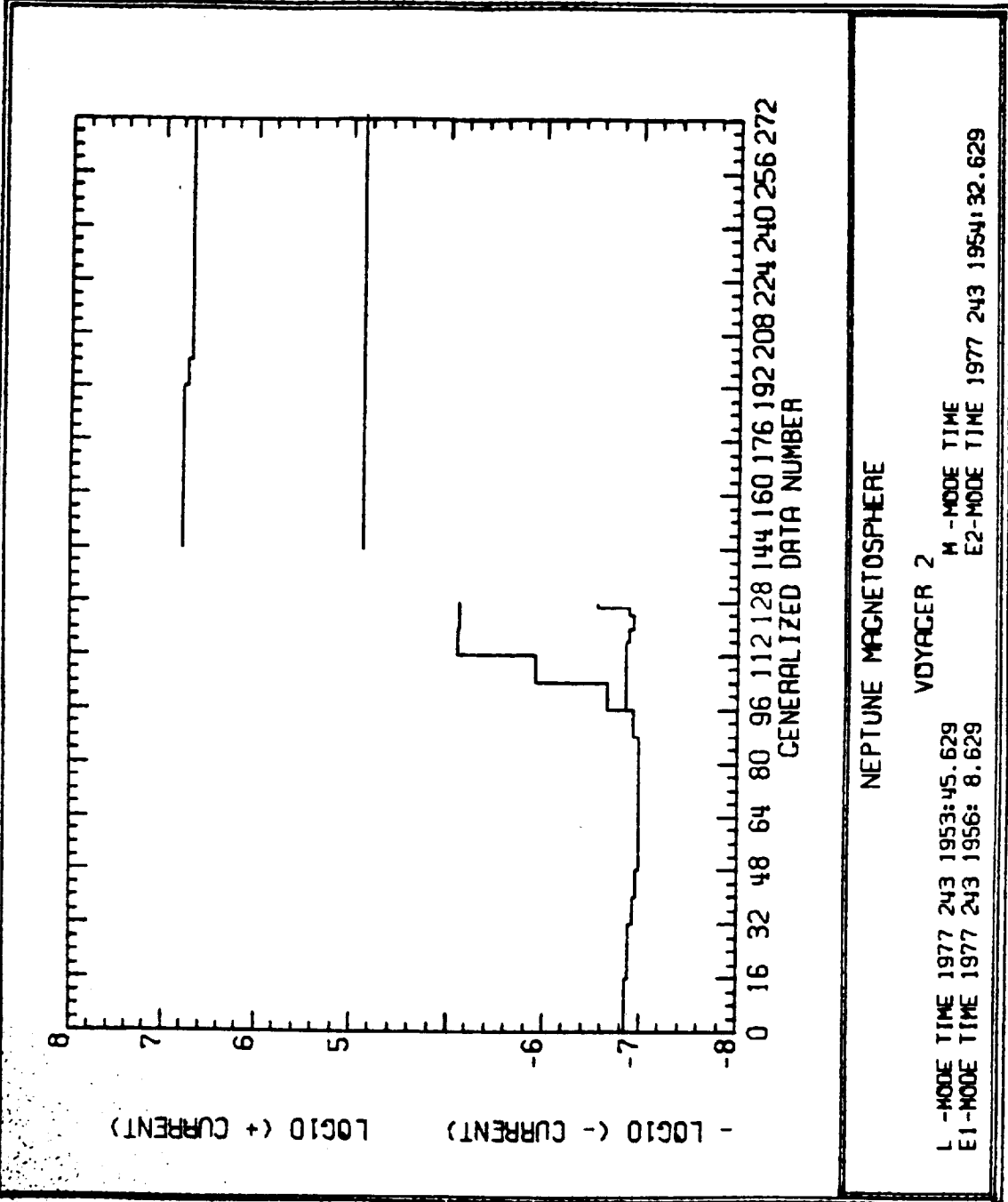


Figure 99

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PLS MODON
REV

VOYAGER DC RETURN DATA

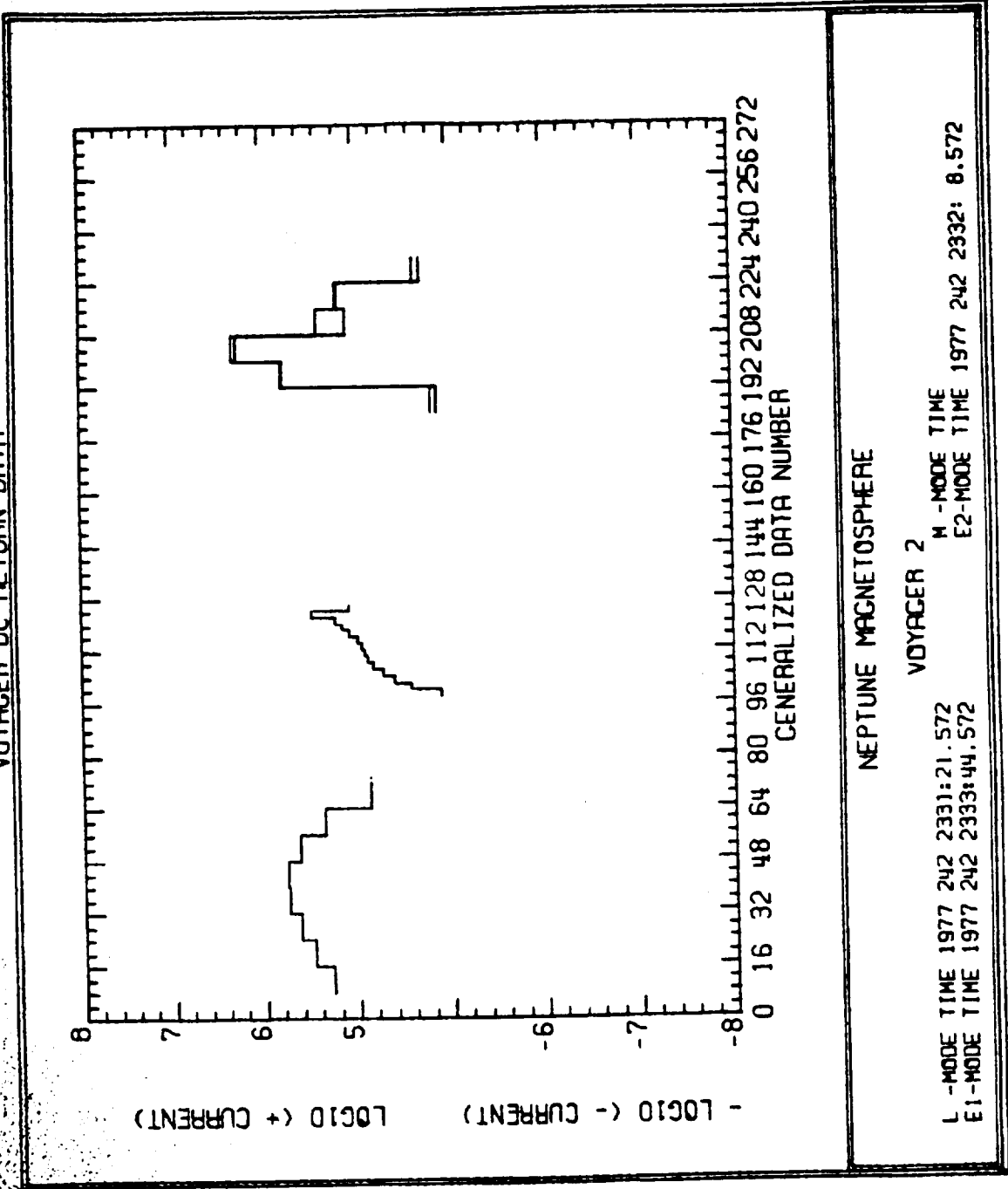


Figure 100

VOYAGER 2
1979 190 1146:18.467

VOYAGER 2
1979 190 1147: 6.467

Figure 101

DATA

PMODEL

$K = 1.5$

$W_{\text{most prob}} = 2500 \text{ km/s}$
(17.8 eV)
 $n = 7.66 \text{ cm}^{-3}$

PMODEL

$K = 5.5$

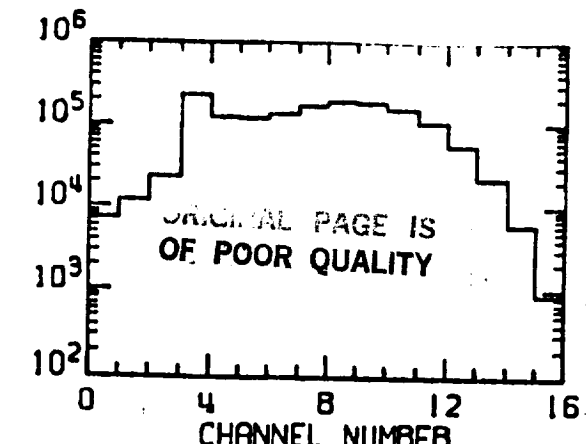
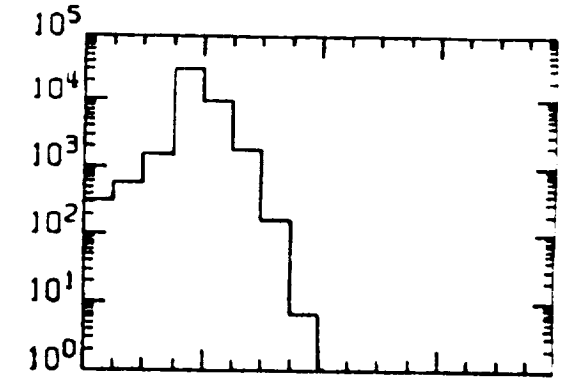
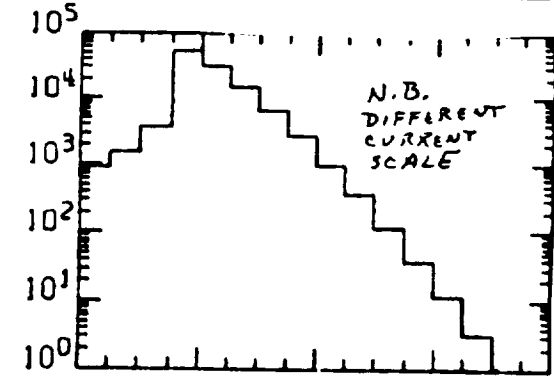
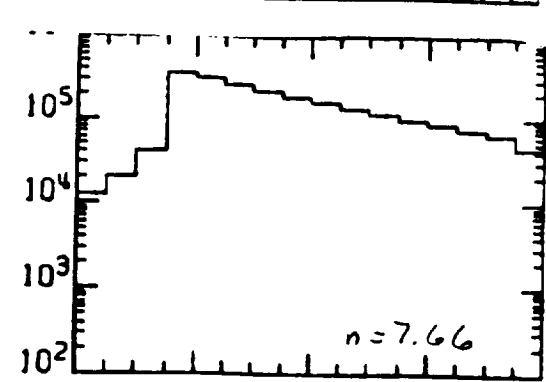
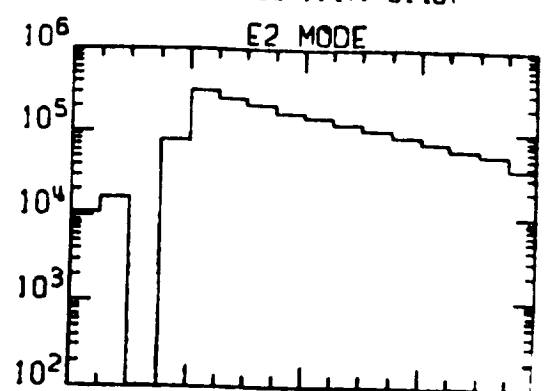
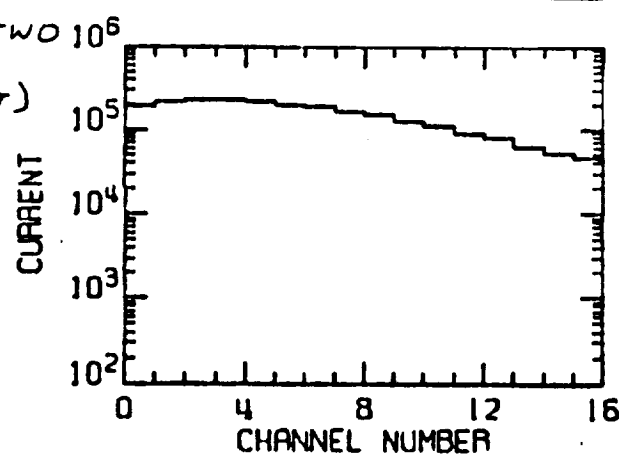
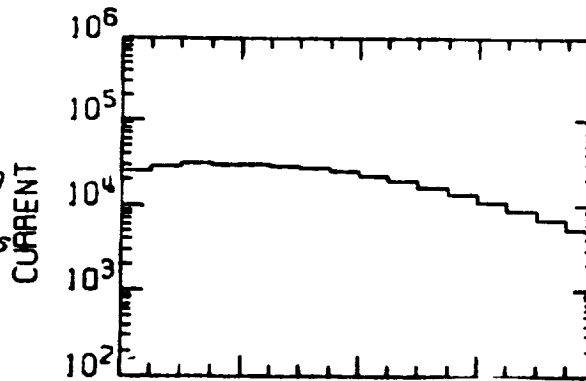
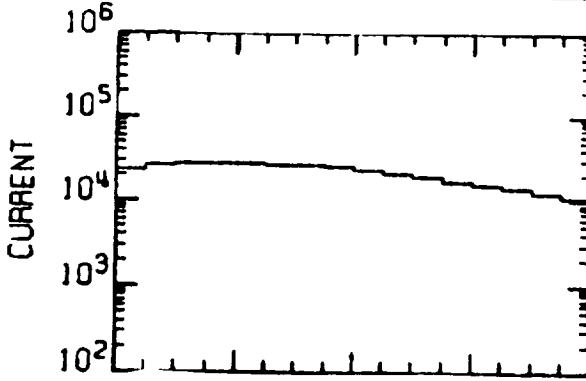
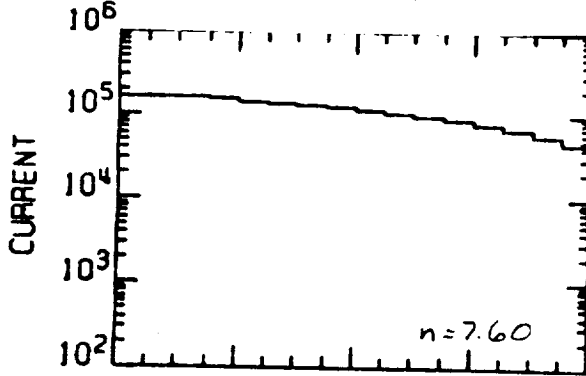
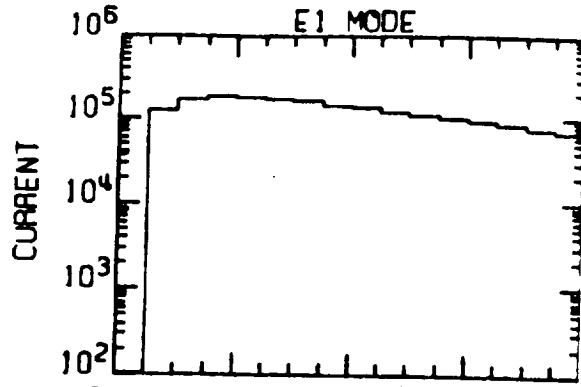
$W_{\text{most prob}} = 3500 \text{ km/s}$
(34.8 eV)
 $n = 1.0 \text{ cm}^{-3}$

PMODEL
MAXWELLIAN

$W_{th} = 300 \text{ km/s}$
(T = 34.8 eV)
 $n = 1.0 \text{ cm}^{-3}$

GSFC FIT TO TWO
MAXWELLIANS
(NSSDC DATA SET)
PMODEL

$n_L = 7.113$ | $n_H = 0.883$
 $T_L = 32.3$ | $T_H = 573$
($W_{th} = 3369.7$) | ($W_{th} = 14,146$)



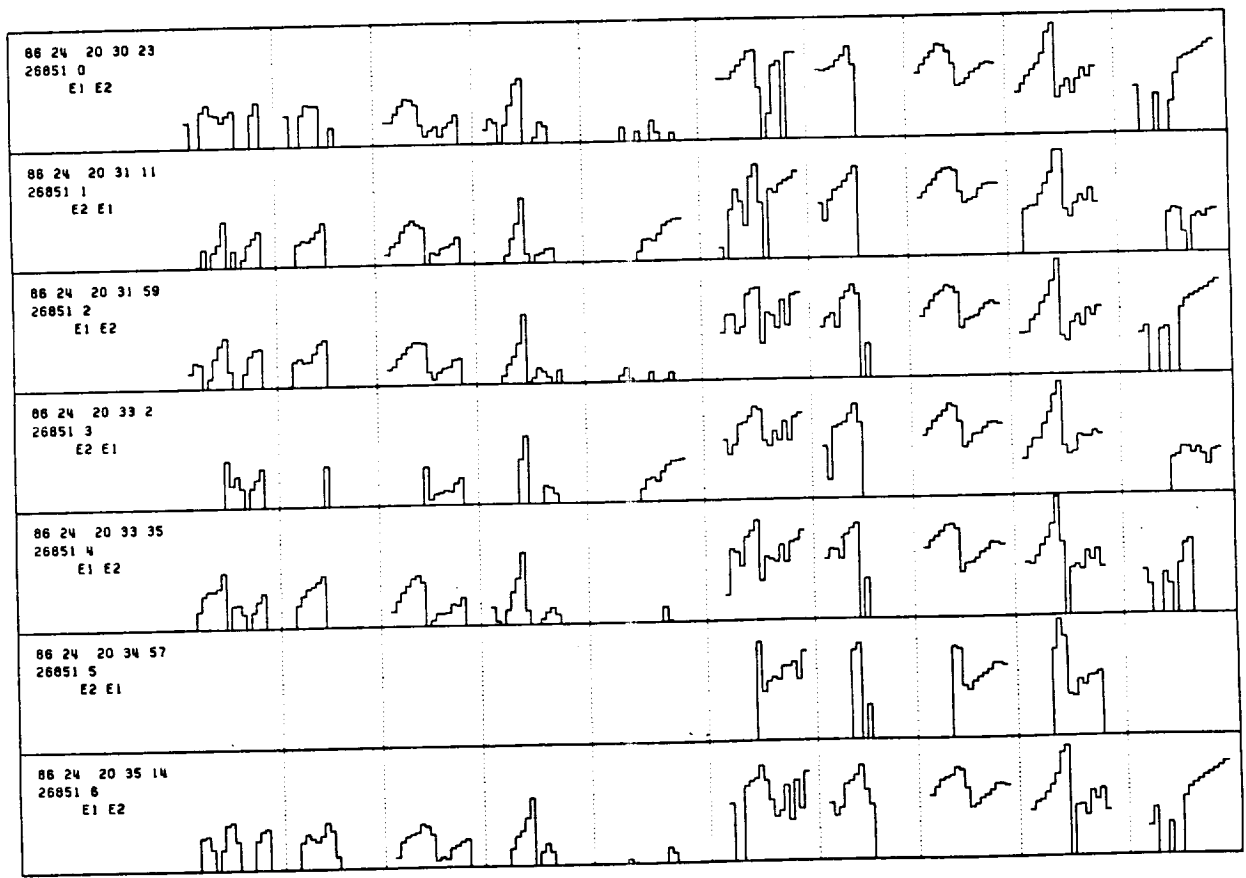
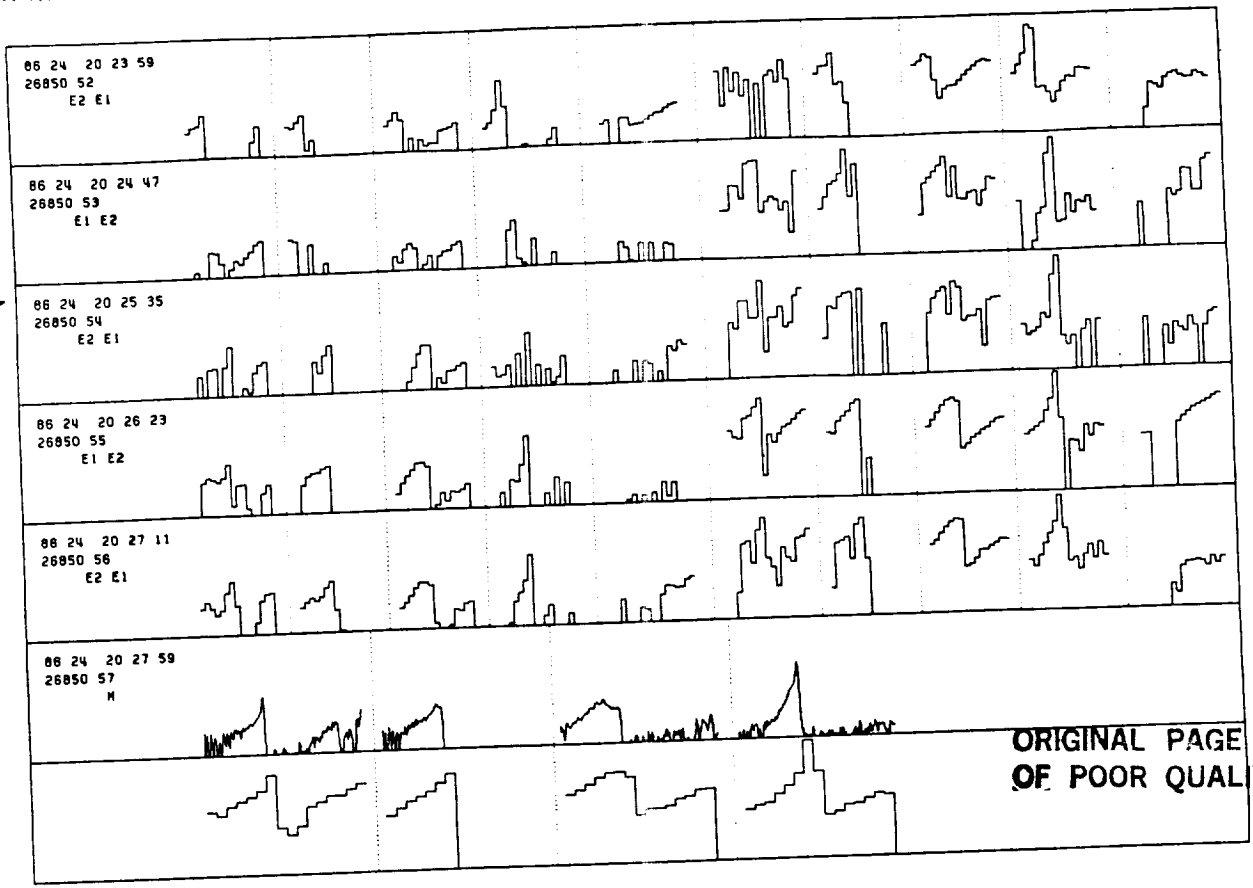
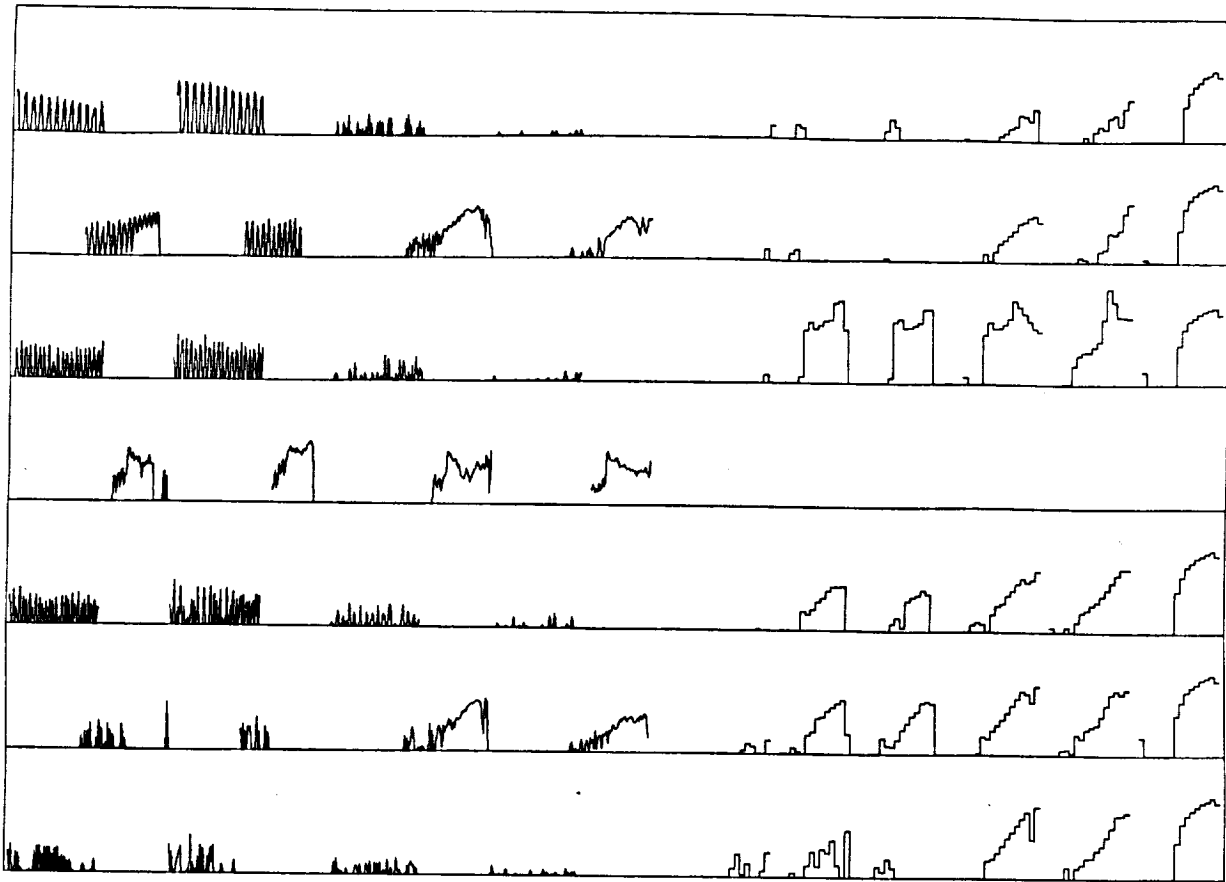


Figure 102



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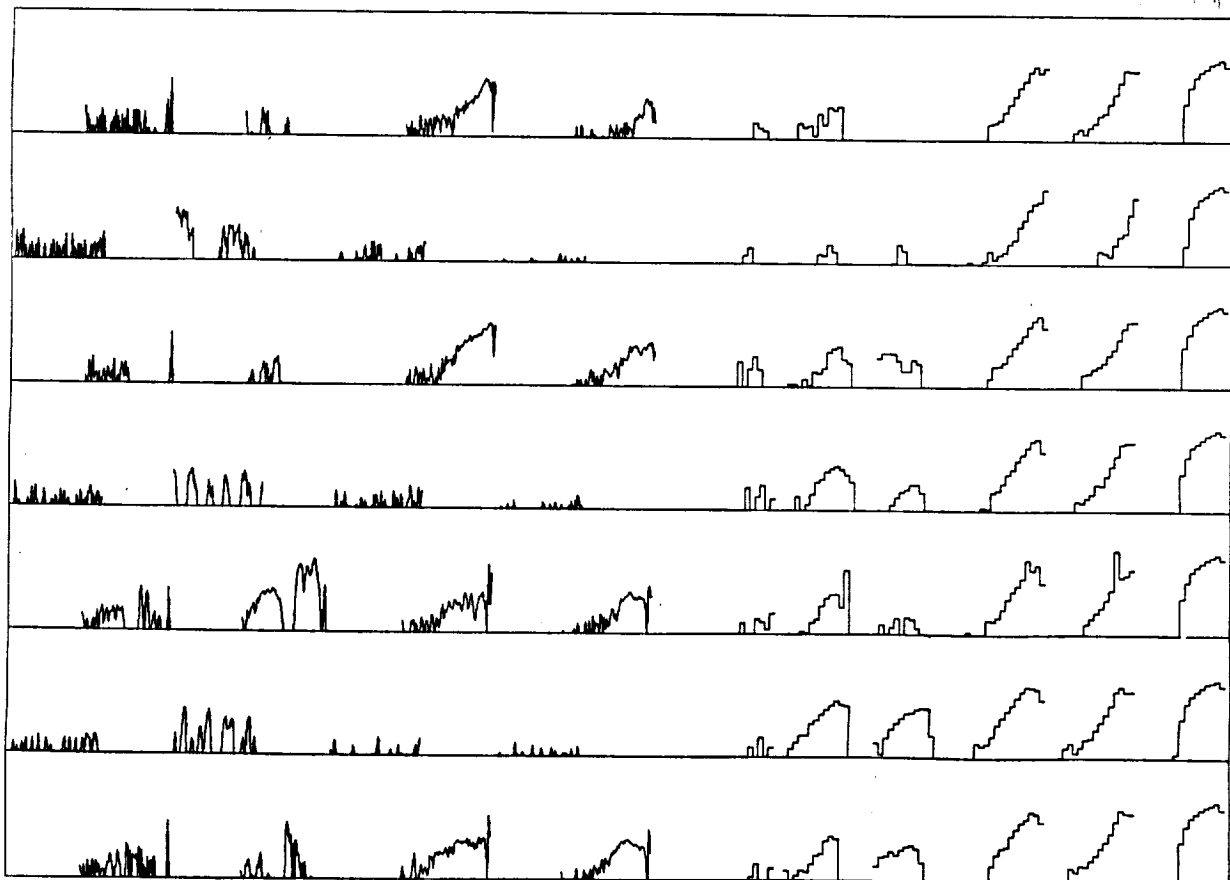


Figure 103

ORIGINAL PAGE IS
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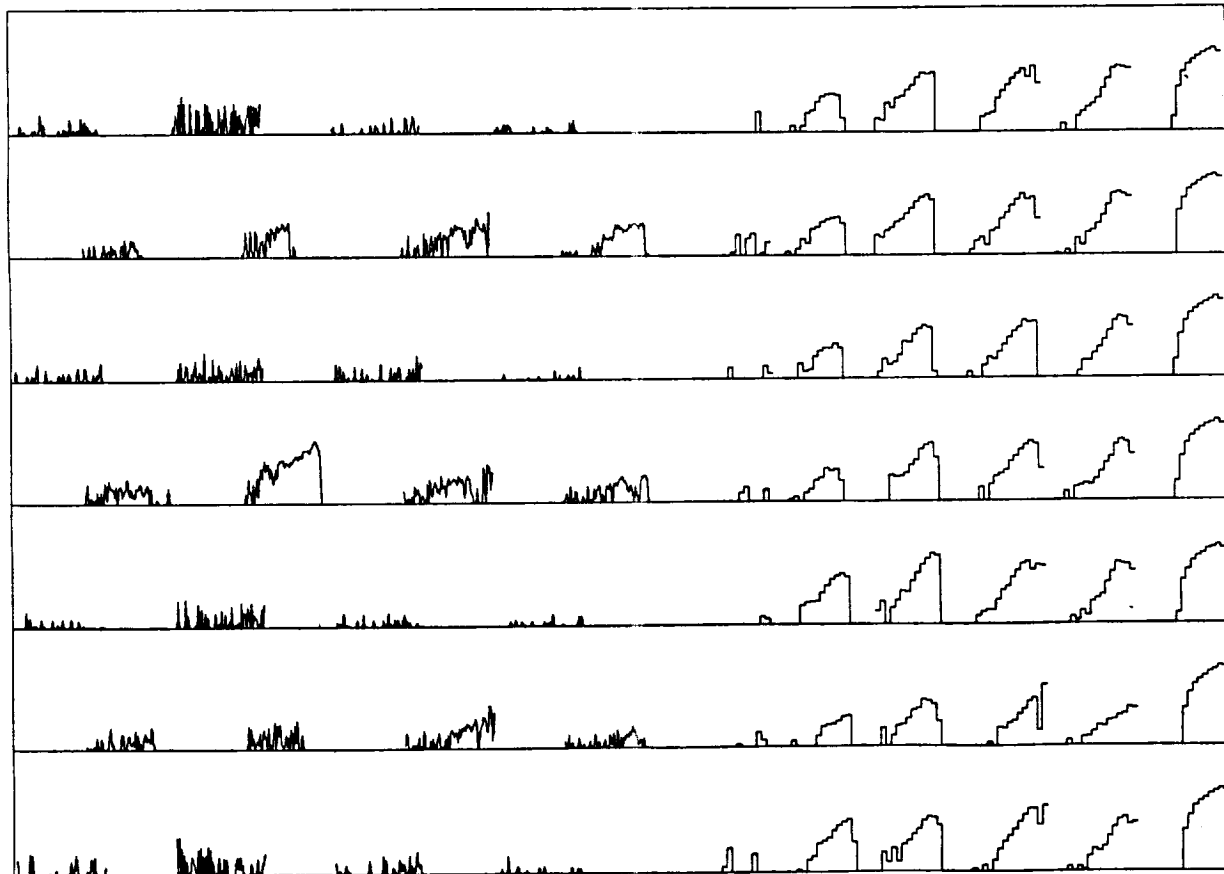
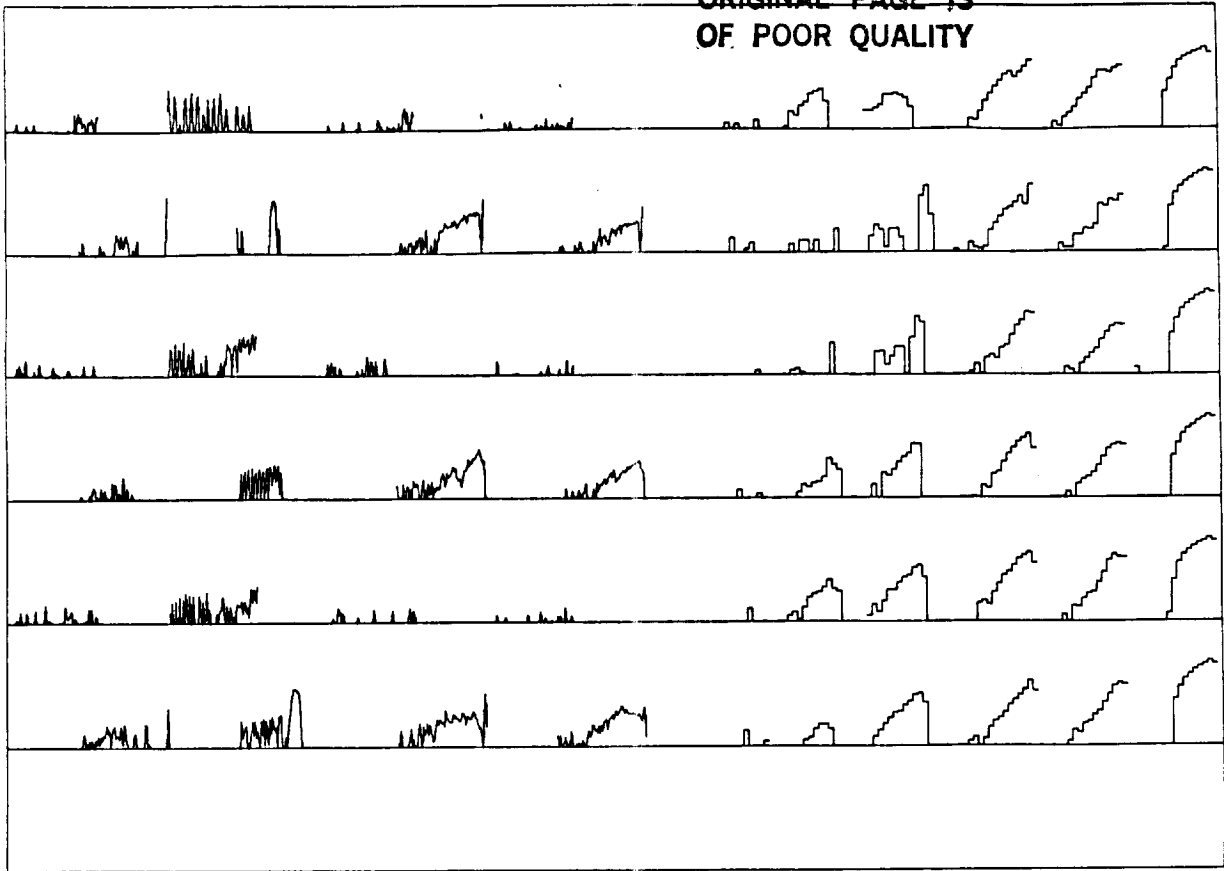
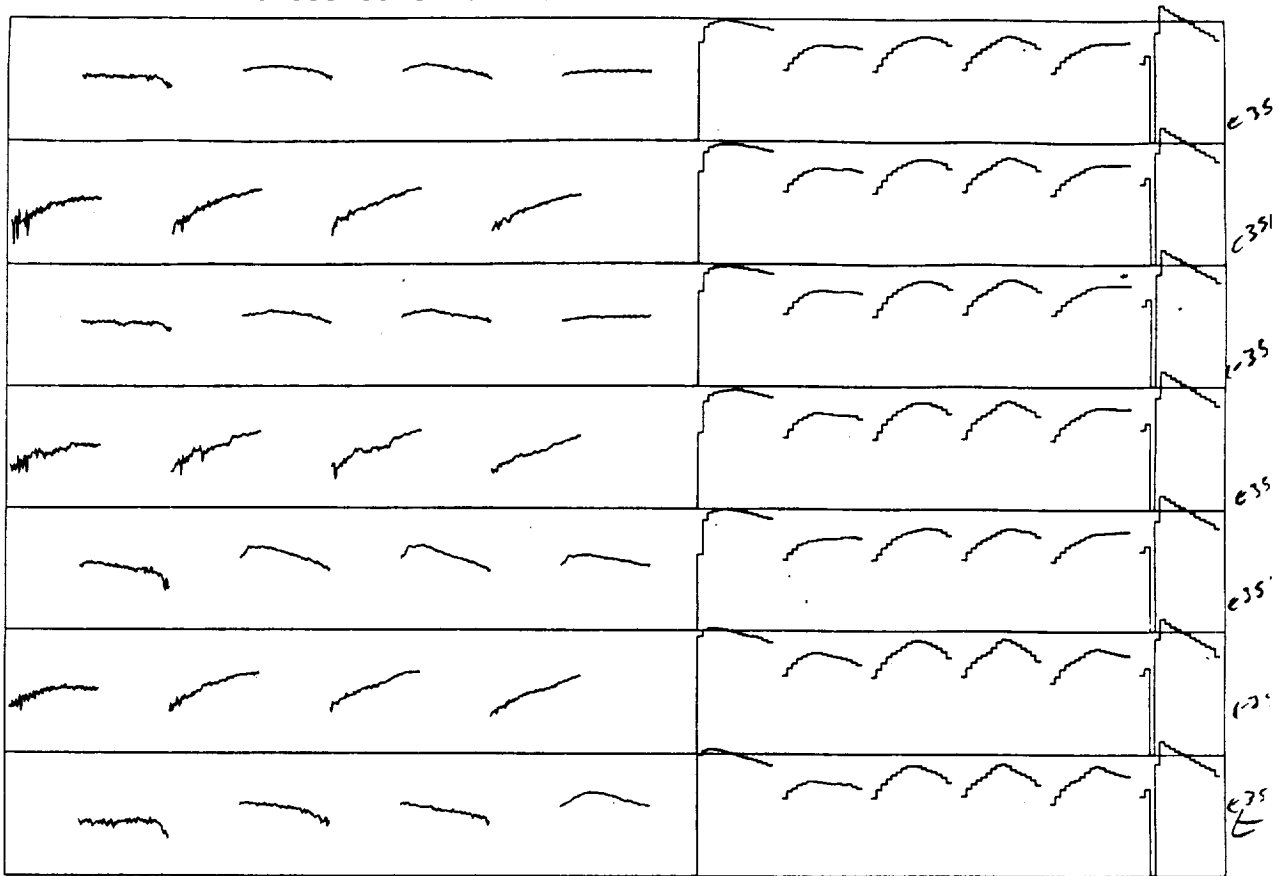


Figure 104



ORIGINAL PAGE IS
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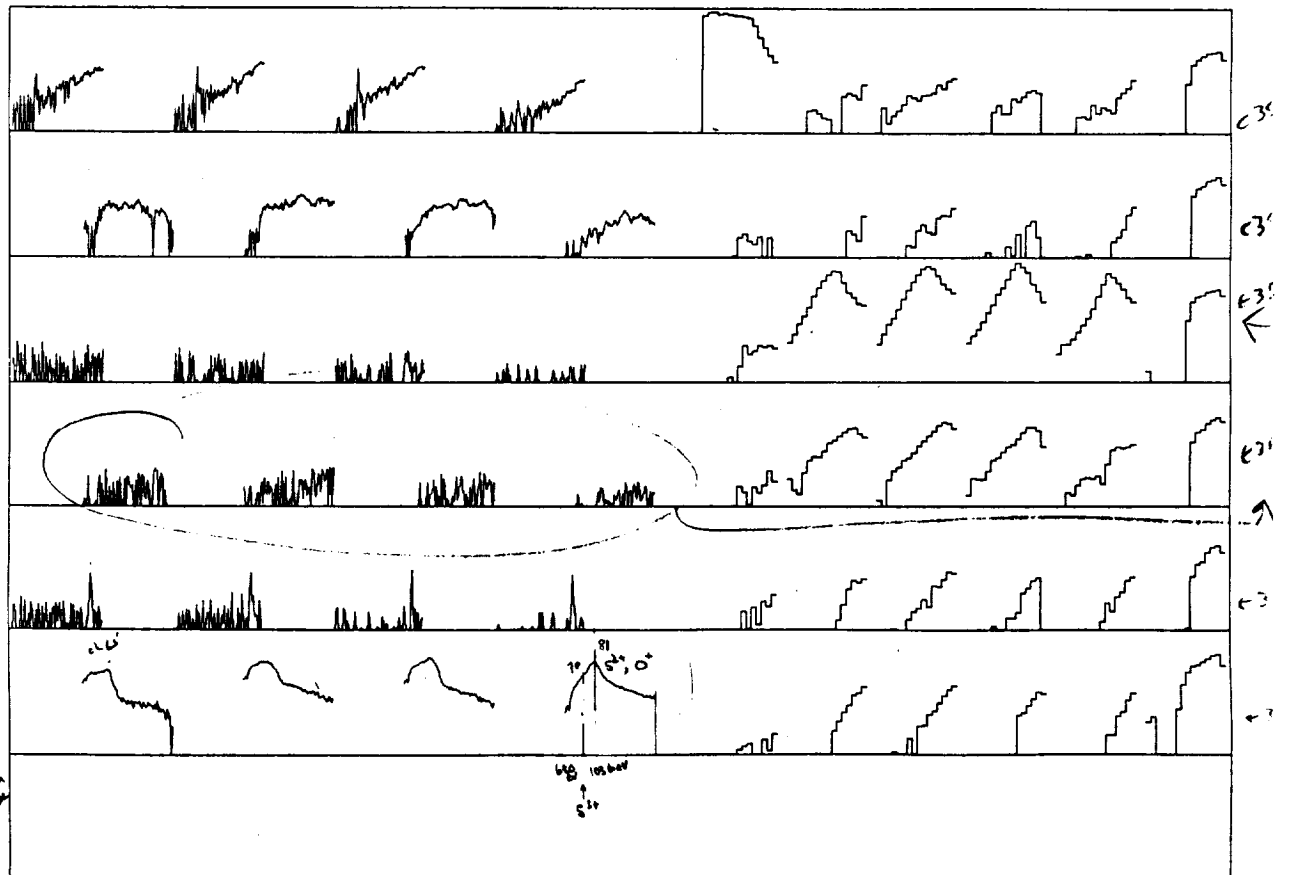
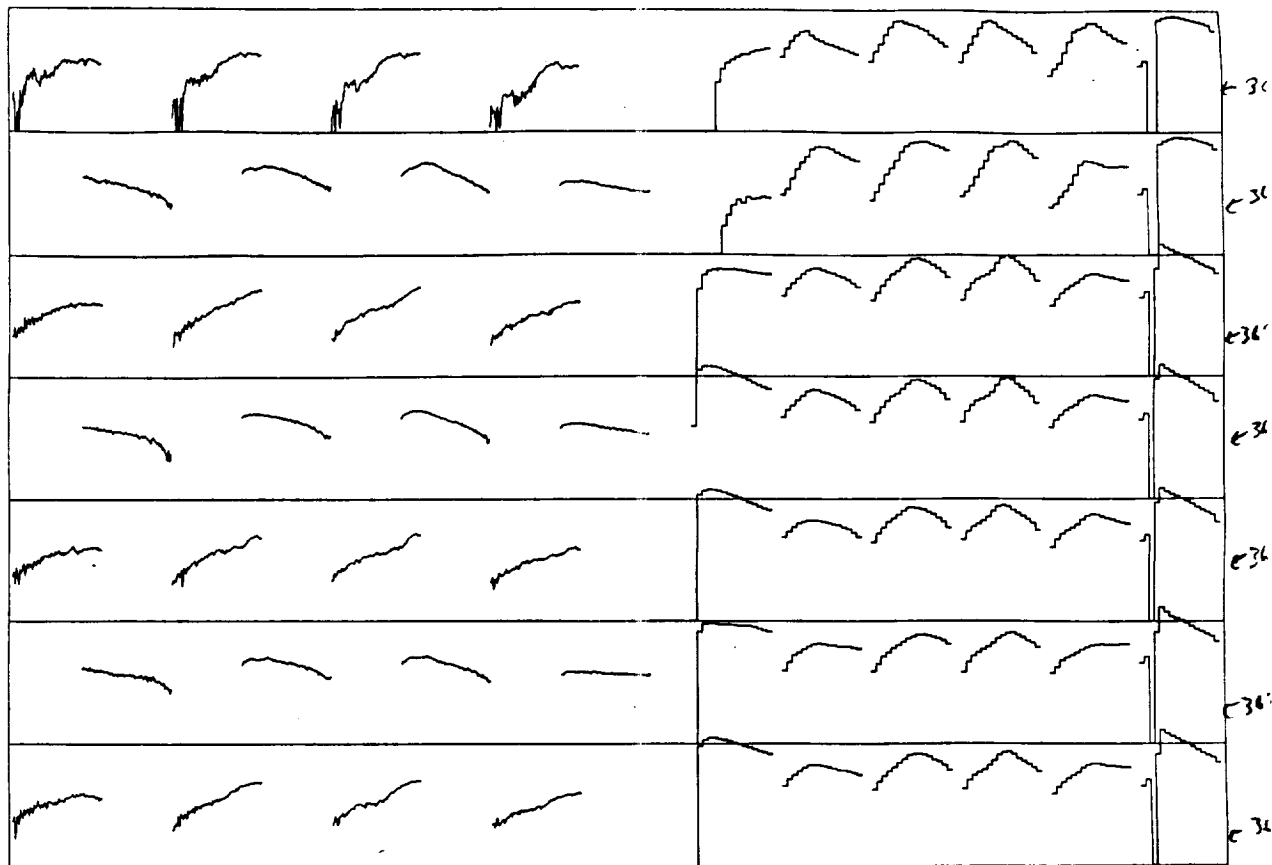


Figure 105



ORIGINAL PAGE IS
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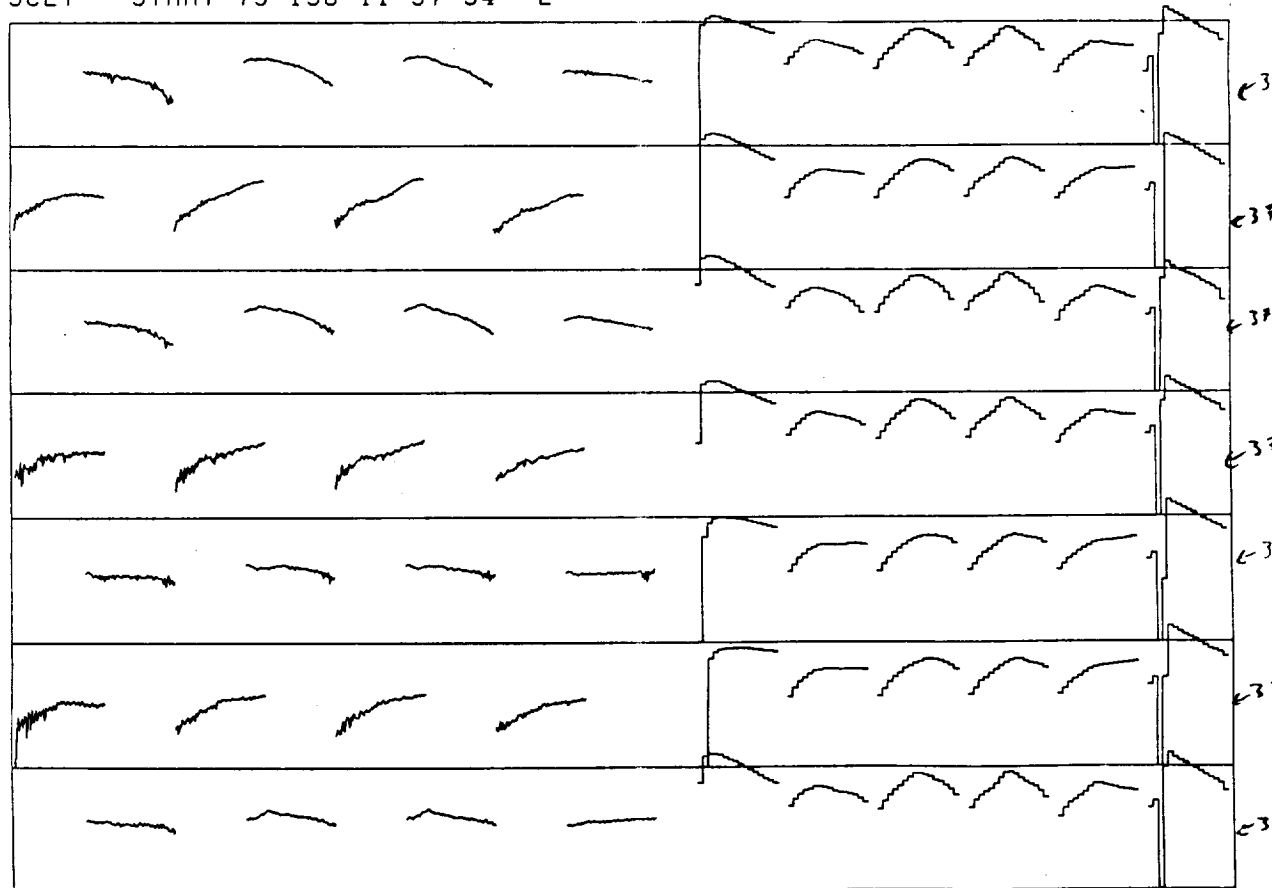
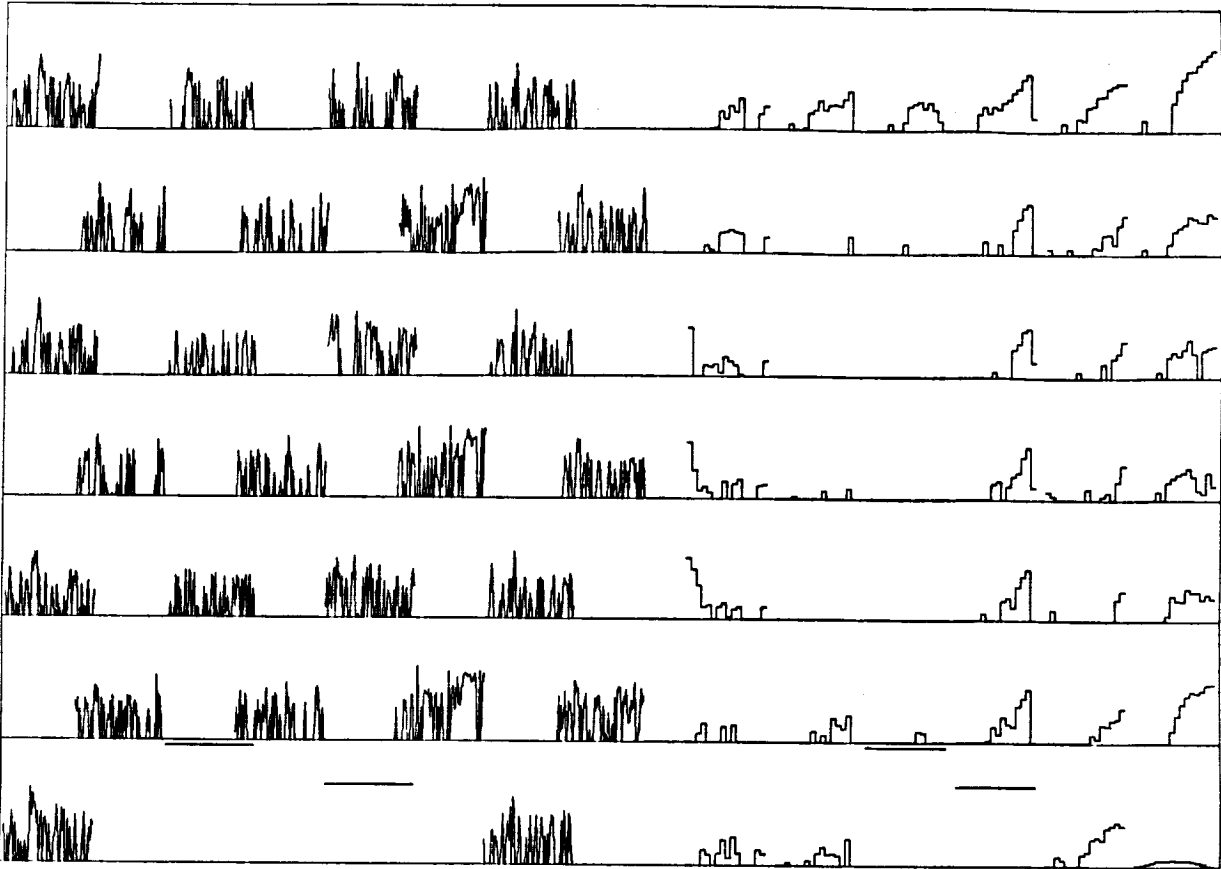


Figure 106

SCET START 79 65 11 12 41 1



SCET START 79 65 11 12 41 2

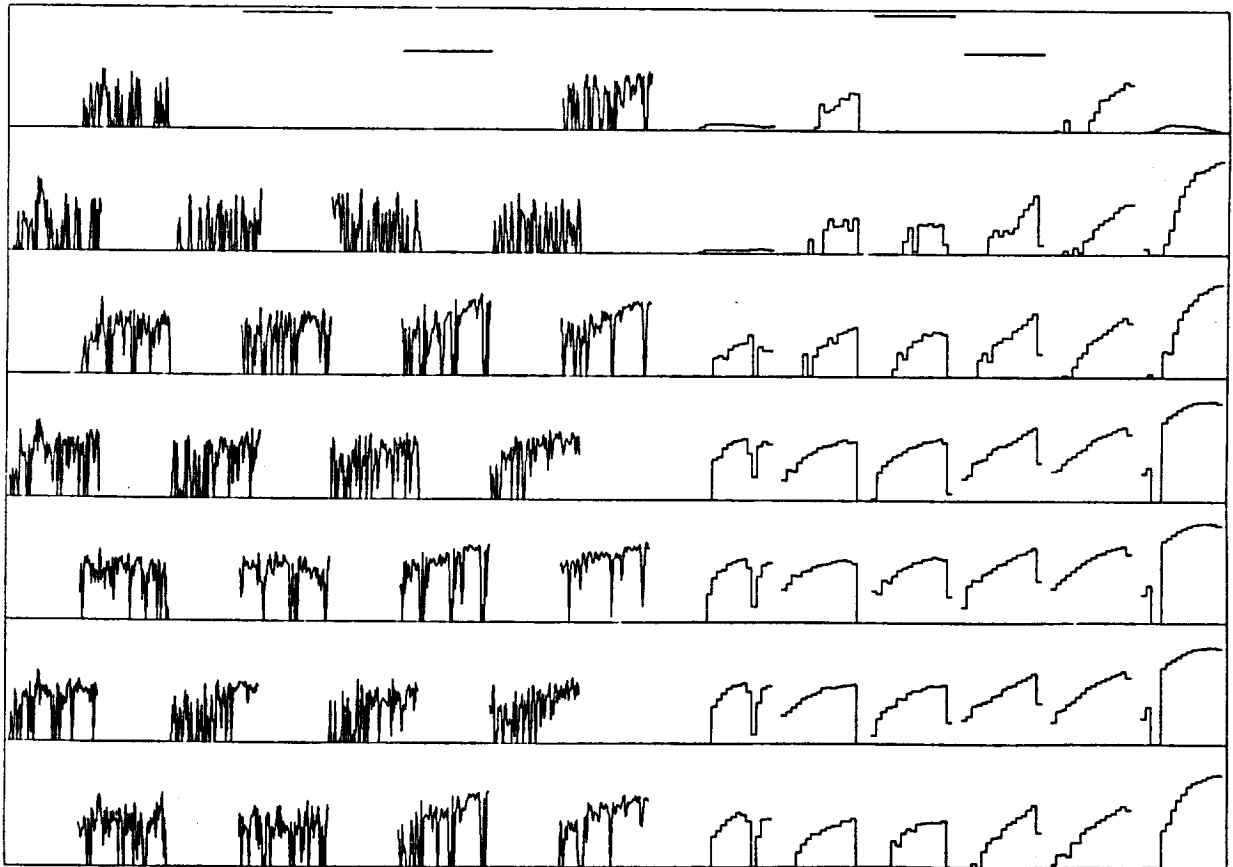


Figure 107

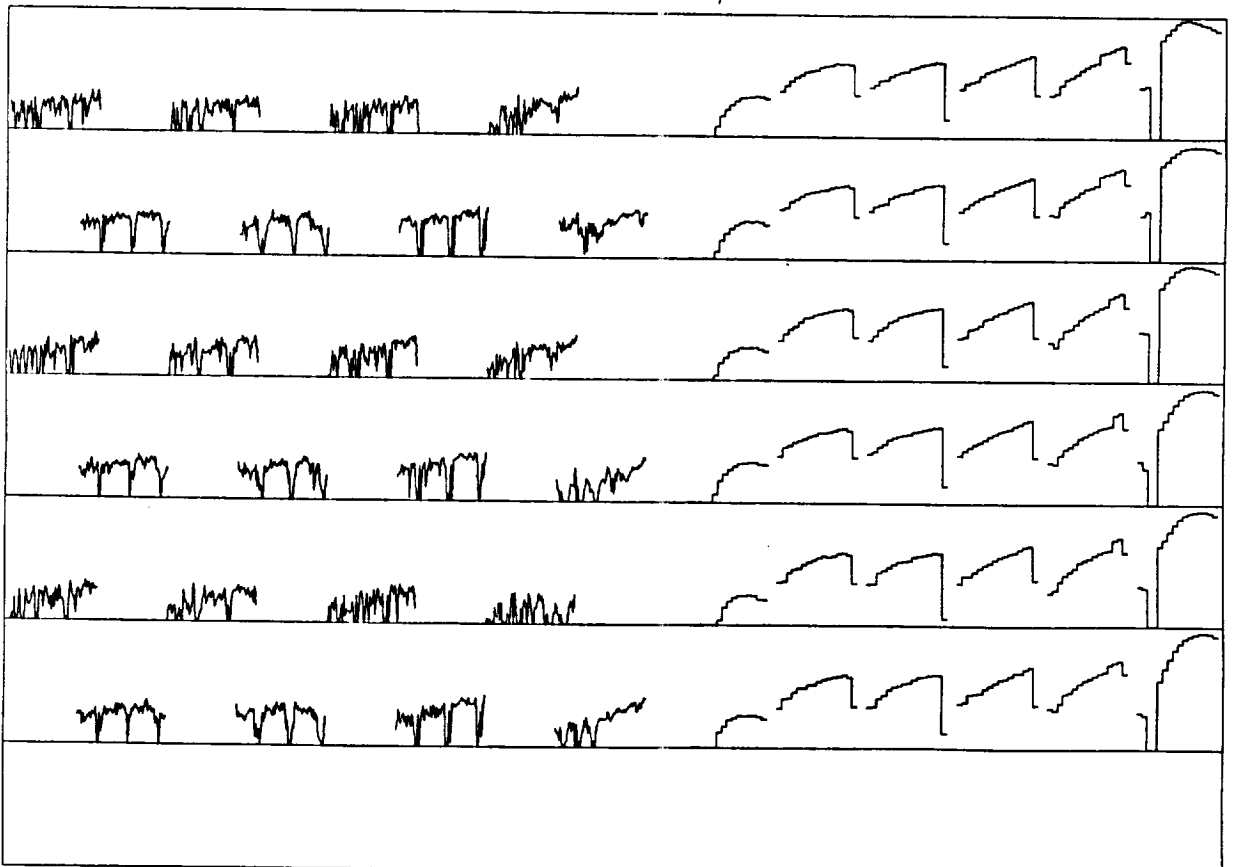
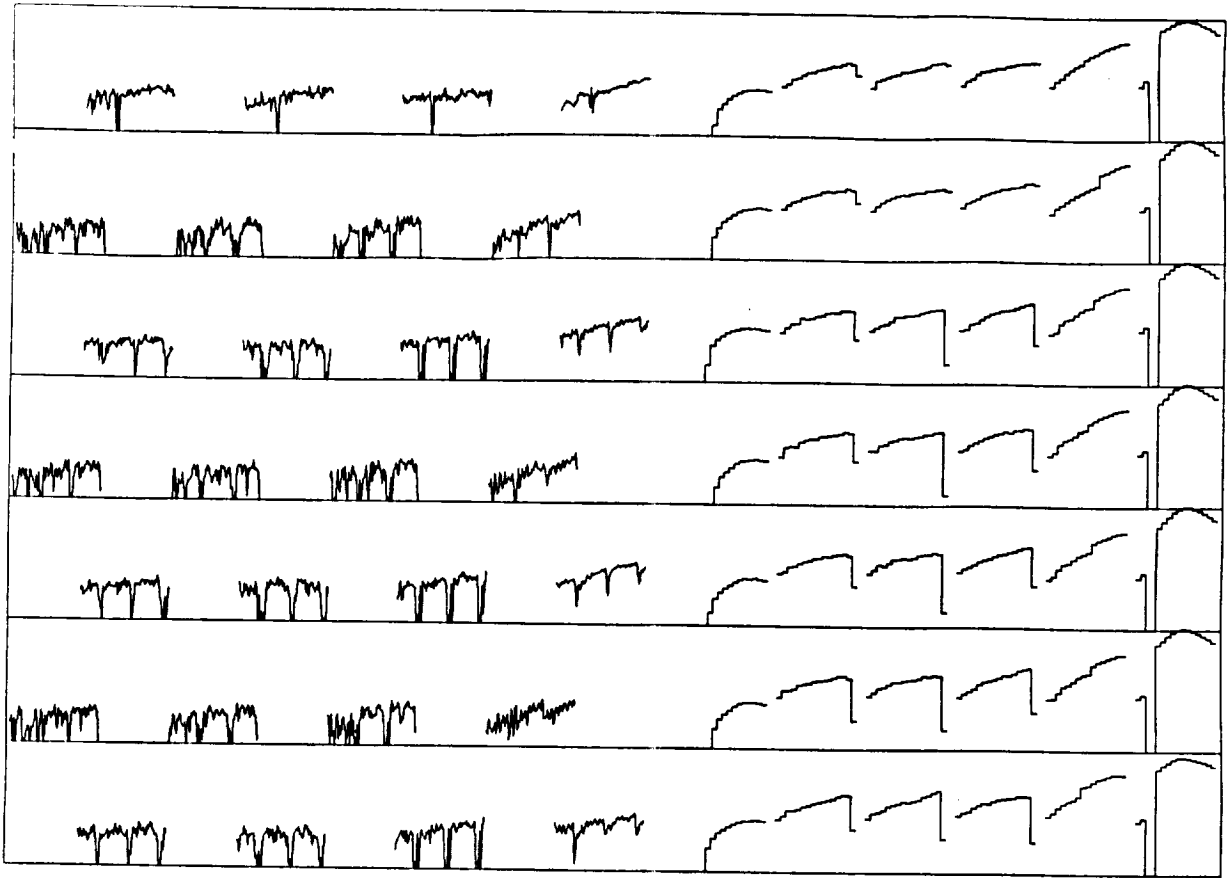
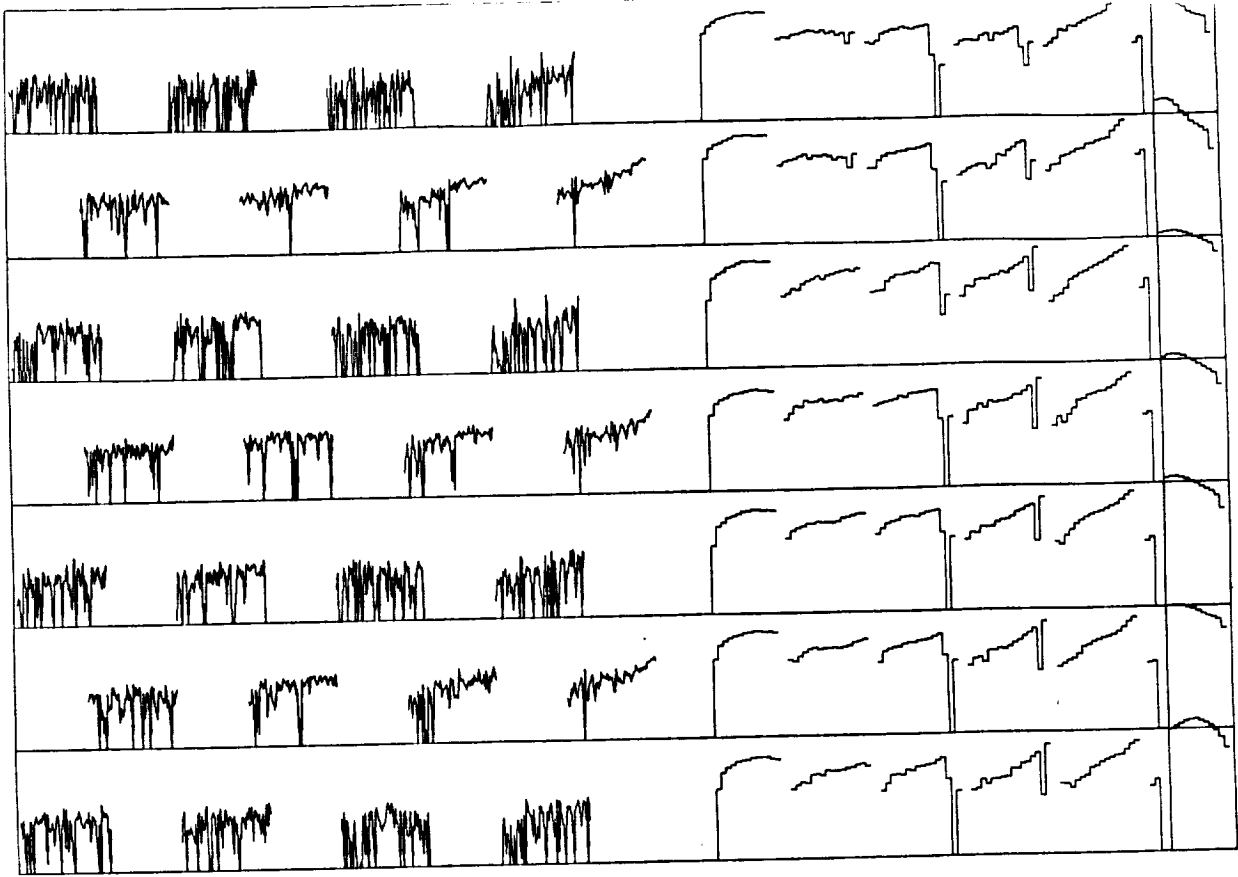


Figure 108



SCET START 79 63 0 0 31 2

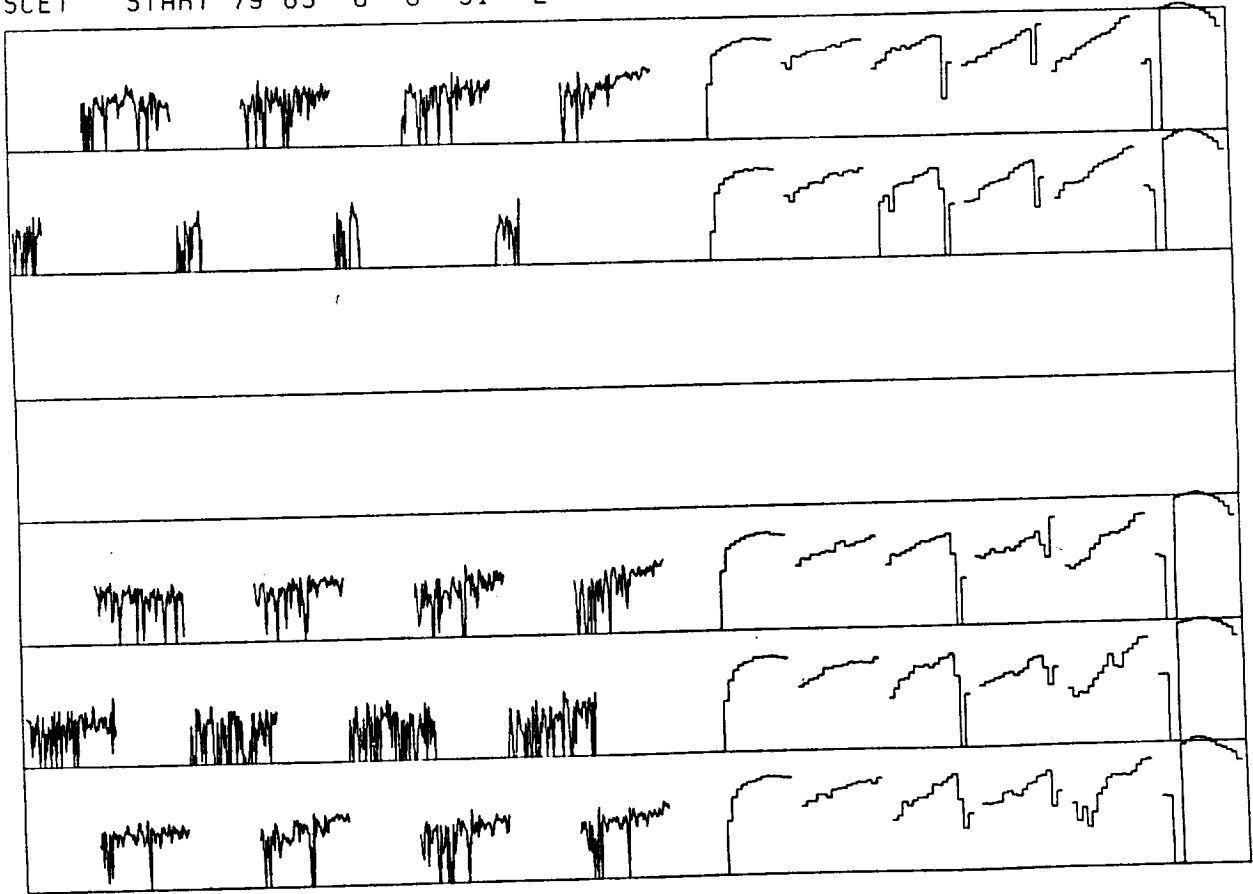
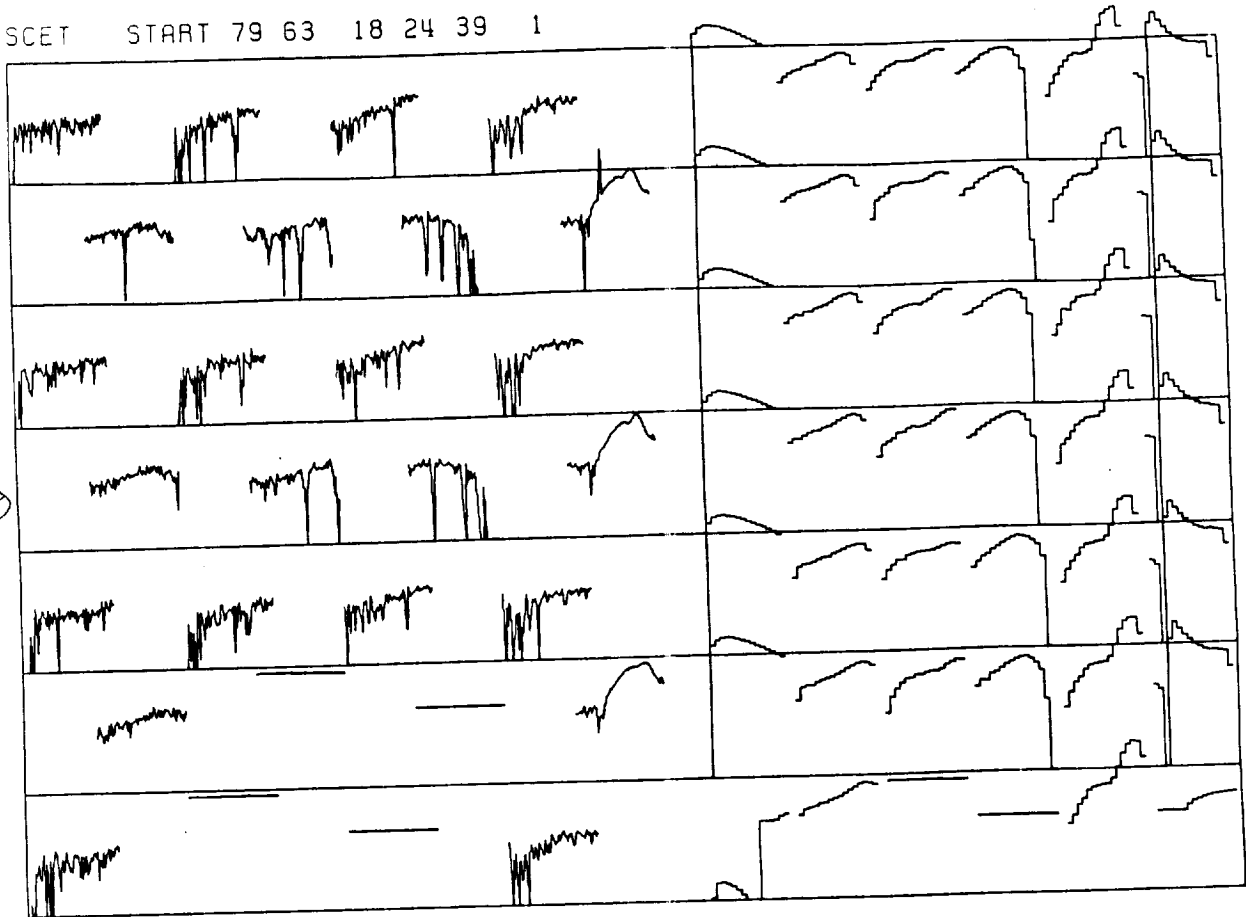


Figure 109

SCET START 79 63 18 24 39 1



SCET START 79 63 18 24 39 2

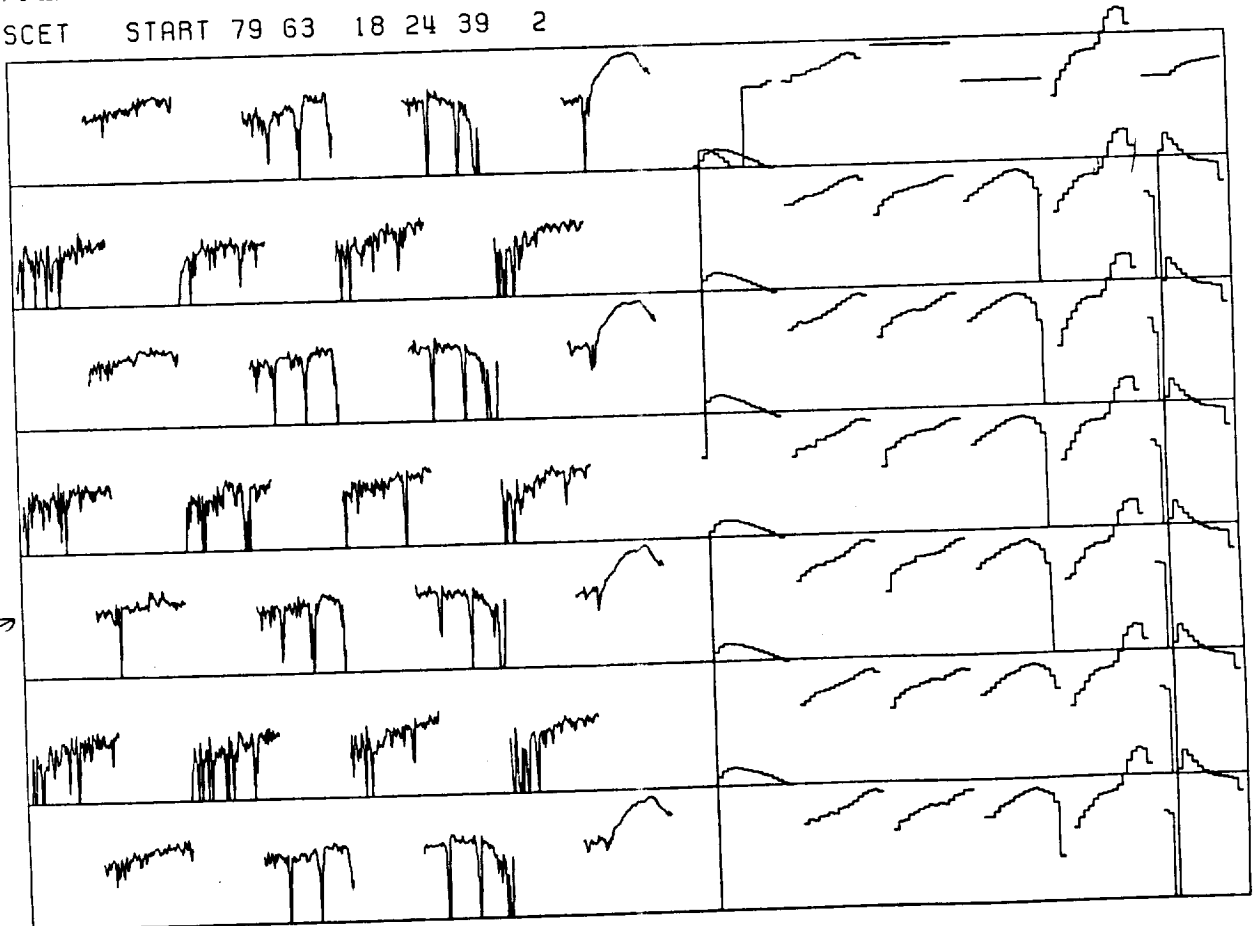
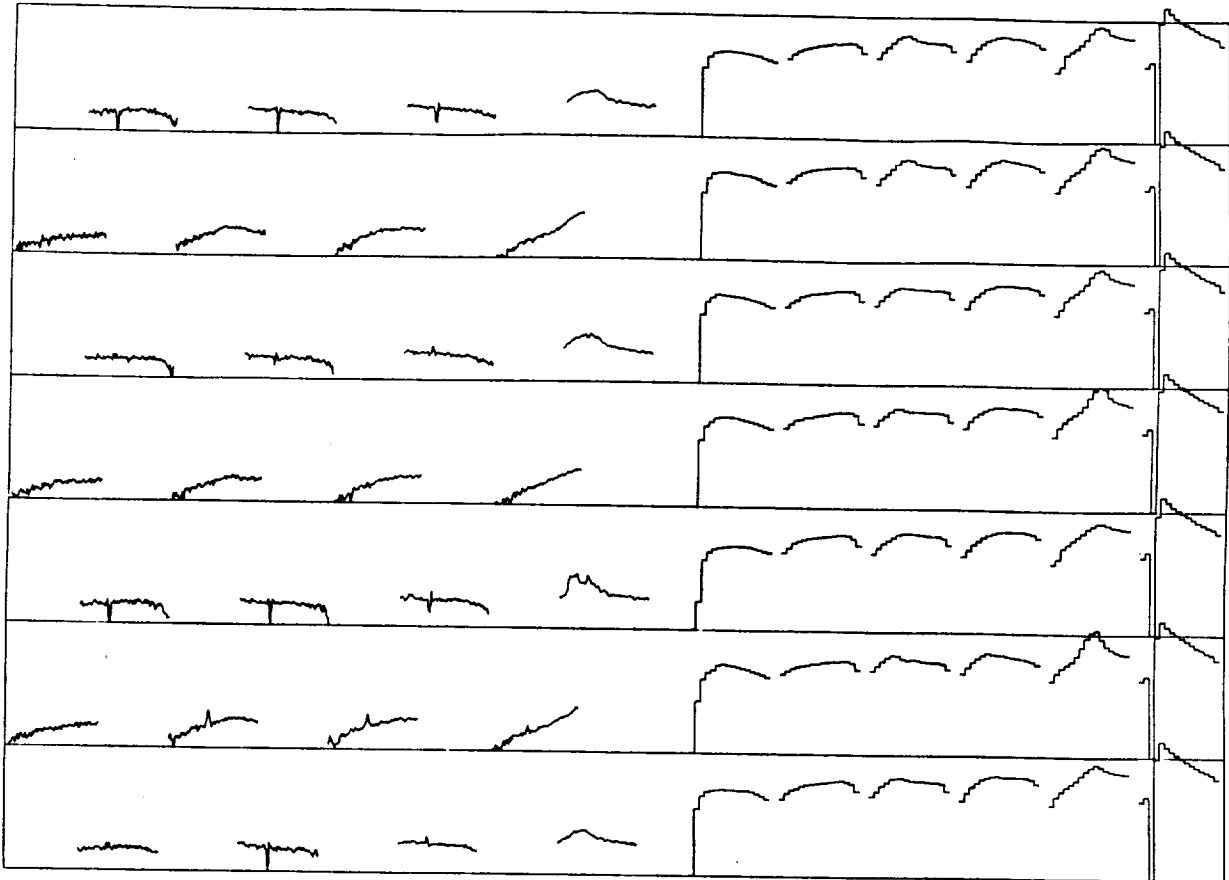


Figure 110

SCET START 79 64 1 4 42 2



SCET START 79 64 1 4 42 3

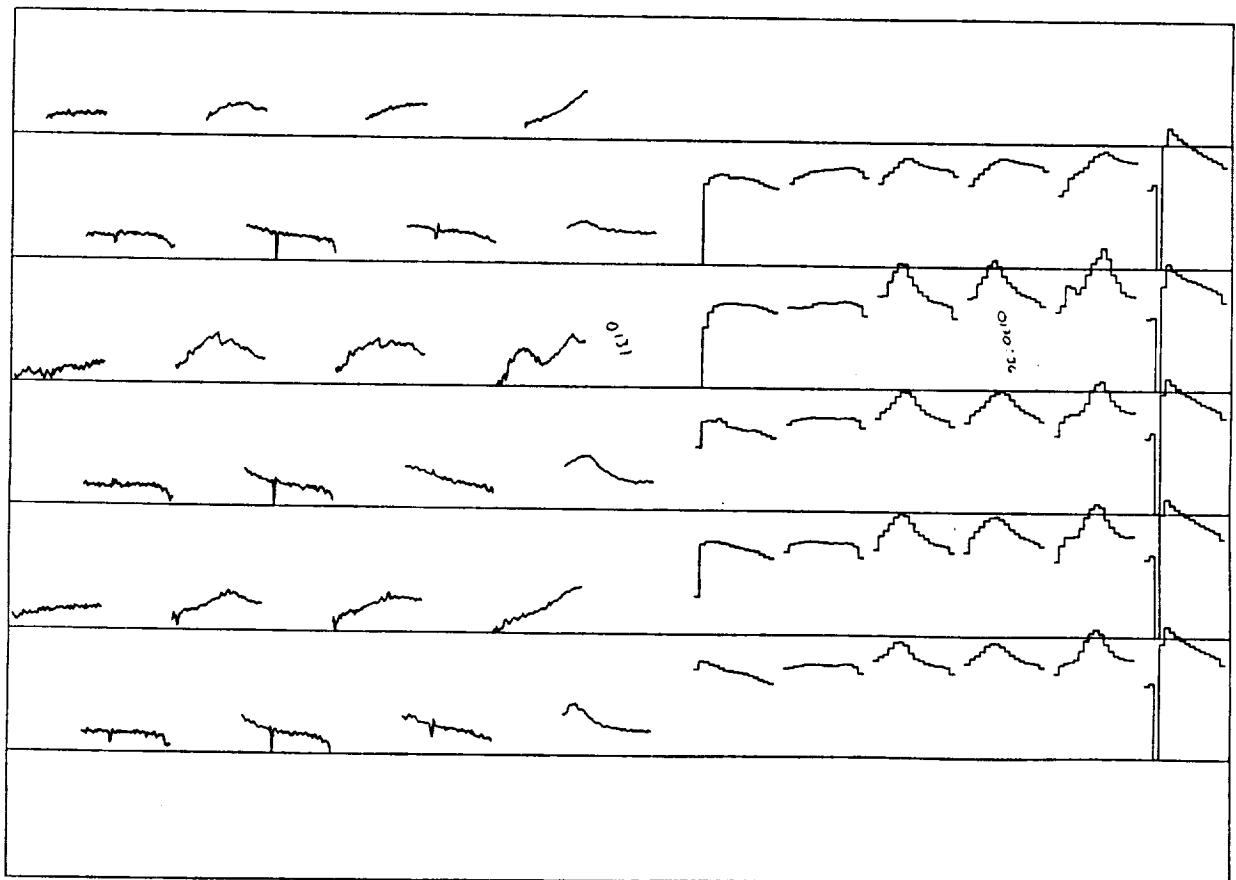
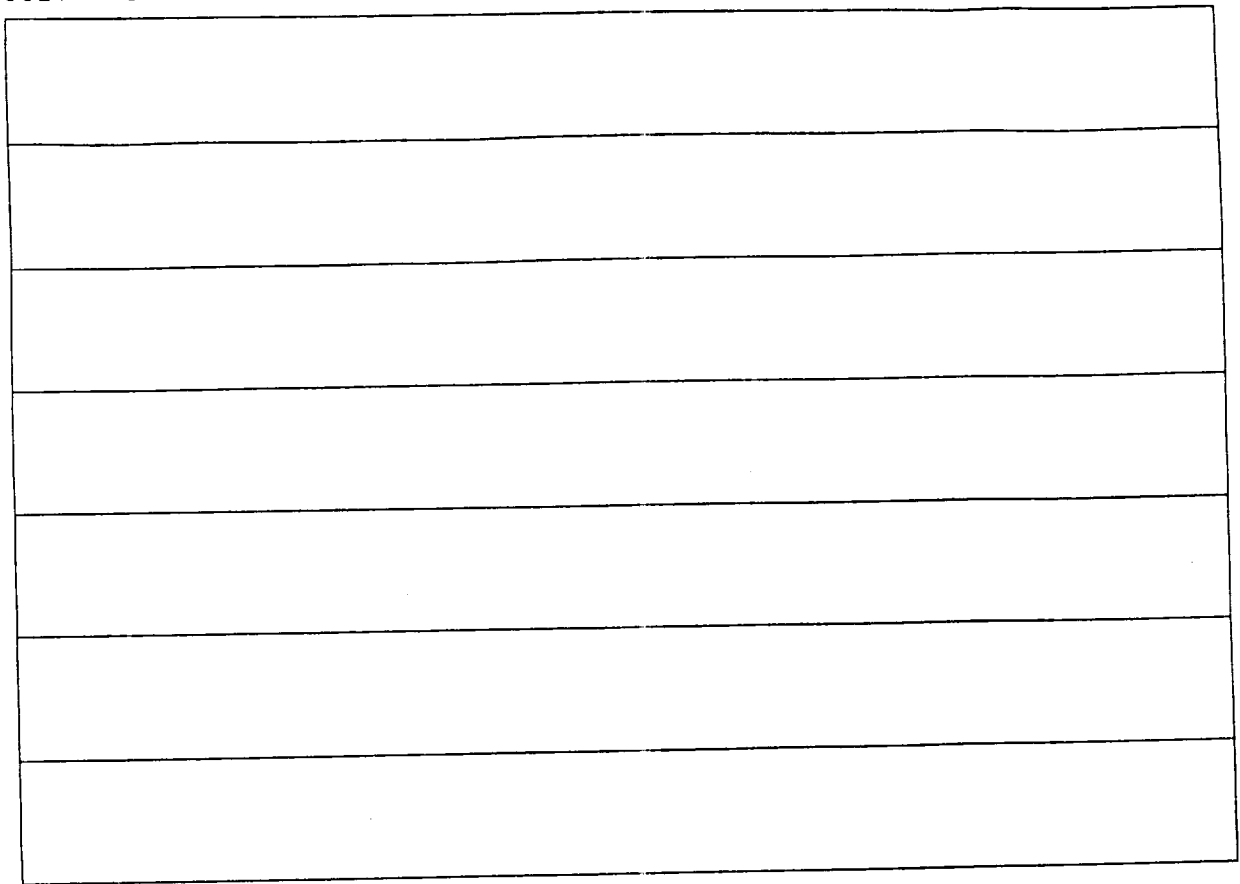


Fig. 111

SCET START 79 64 1 20 42 1



SCET START 79 64 1 20 42 2

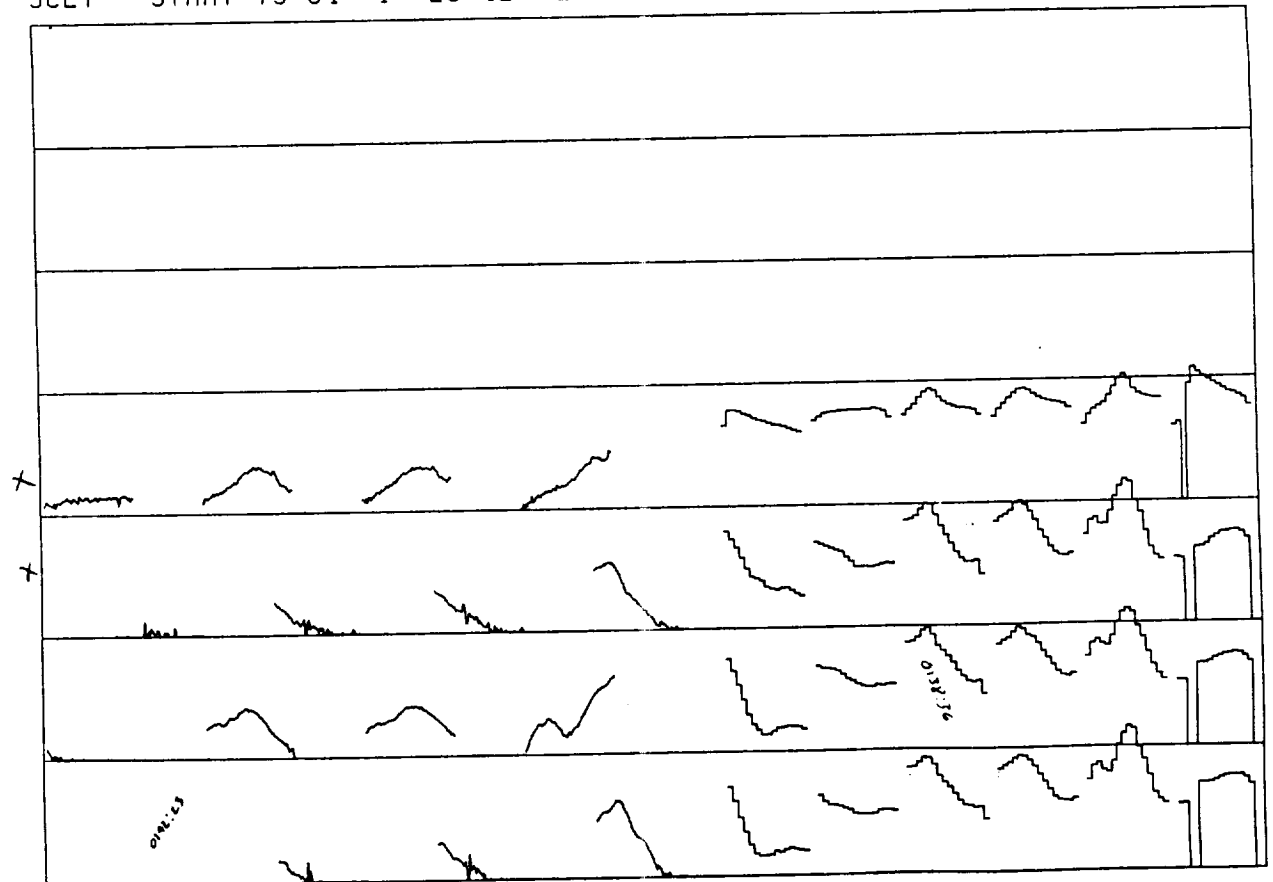
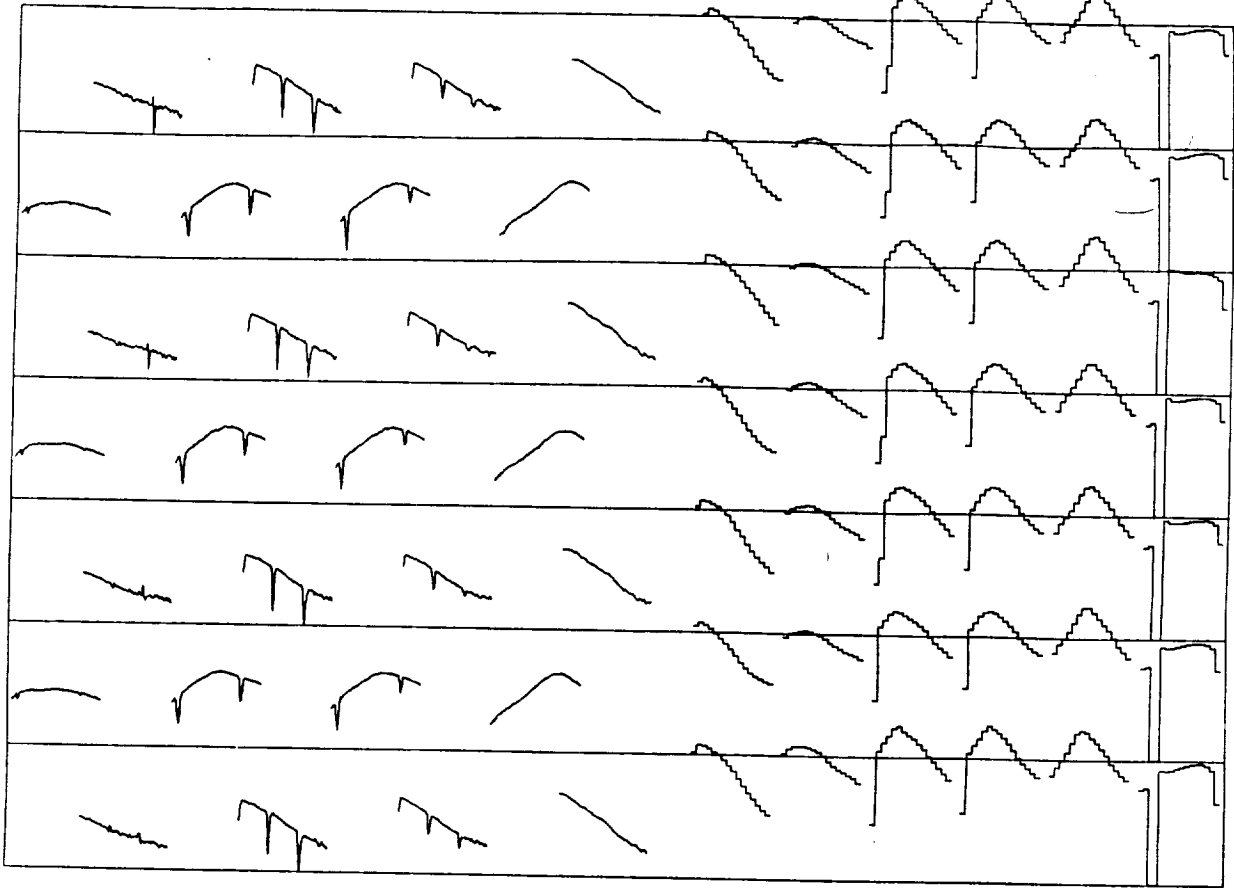


Fig. 112

SCET START 79 64 5 4 44 2



SCET START 79 64 5 4 44 3

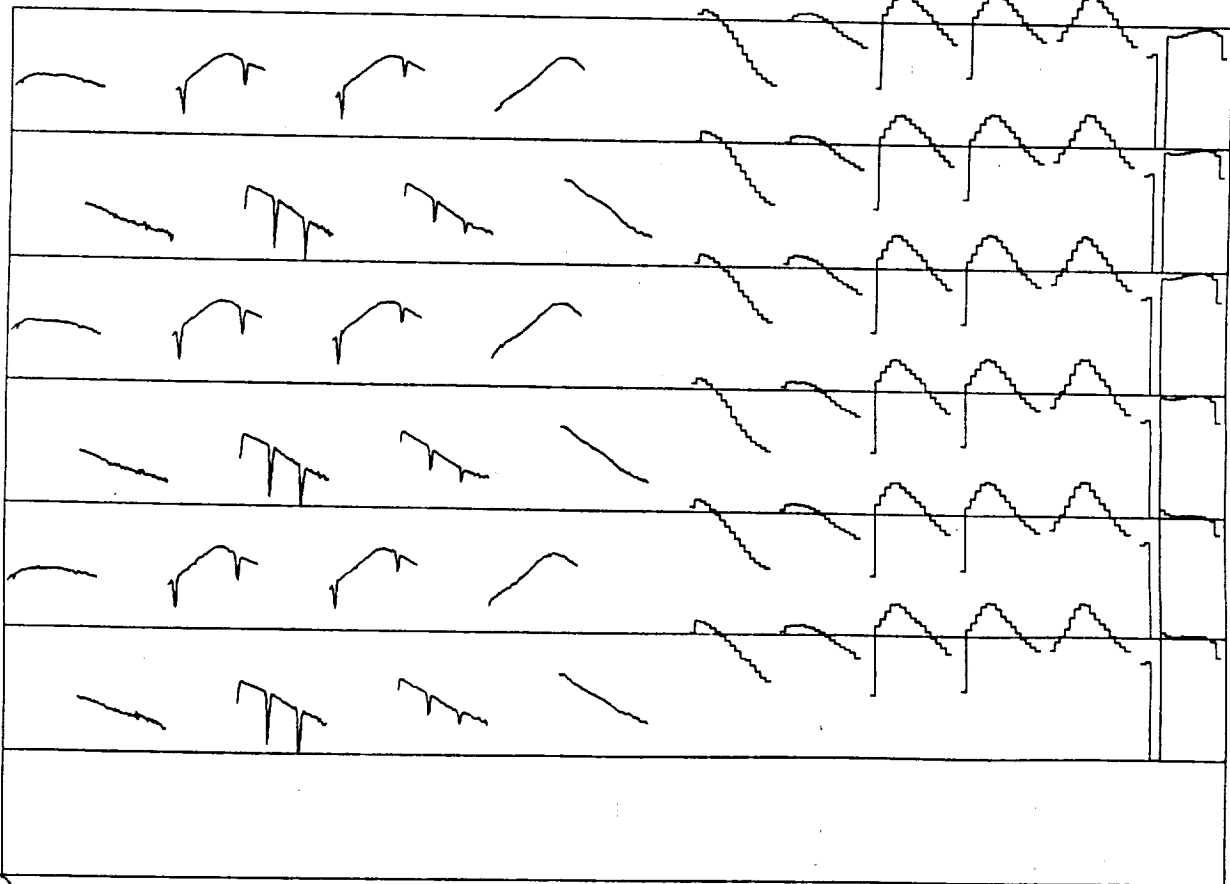
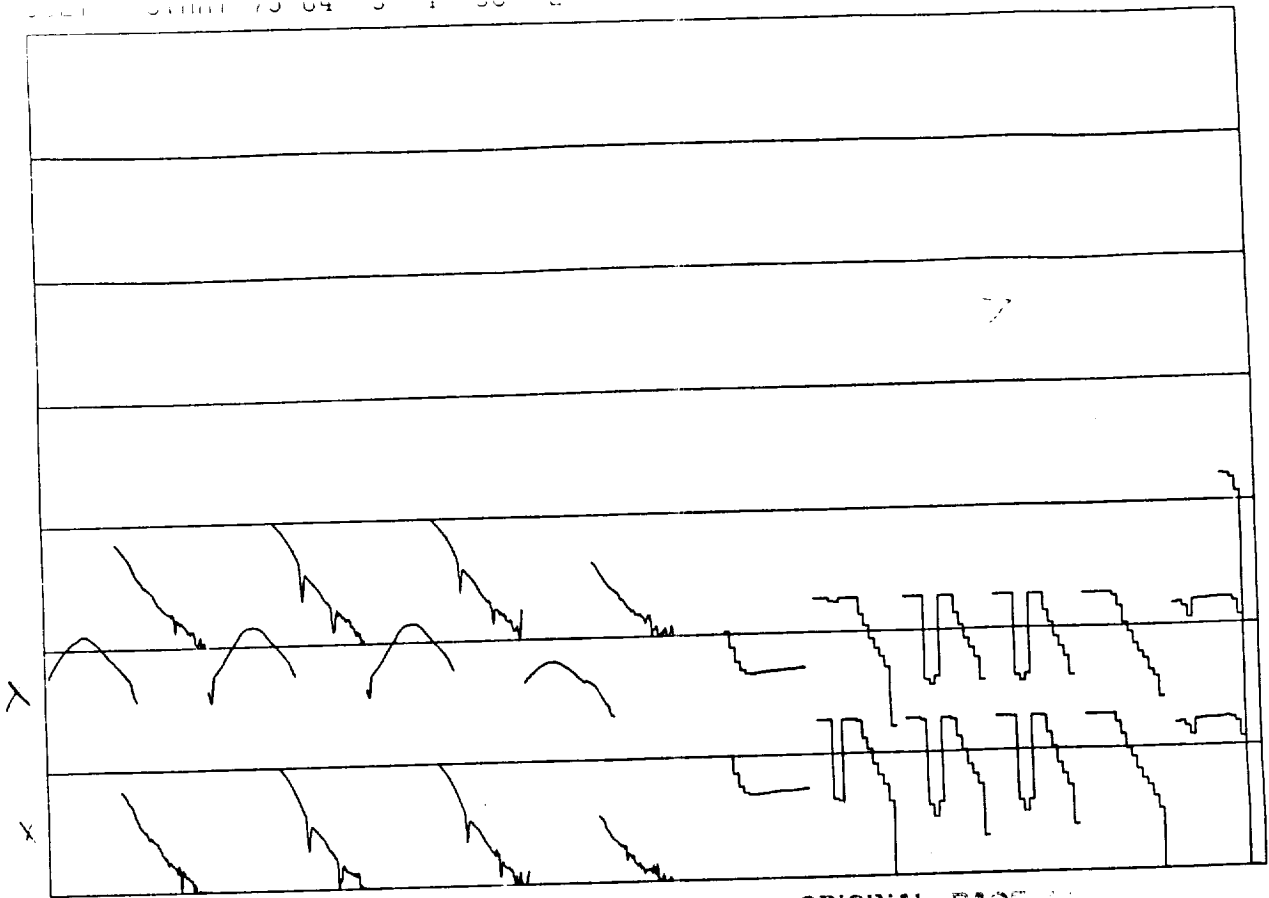


Fig. 113



ORIGINAL PAGE IS
OF POOR QUALITY

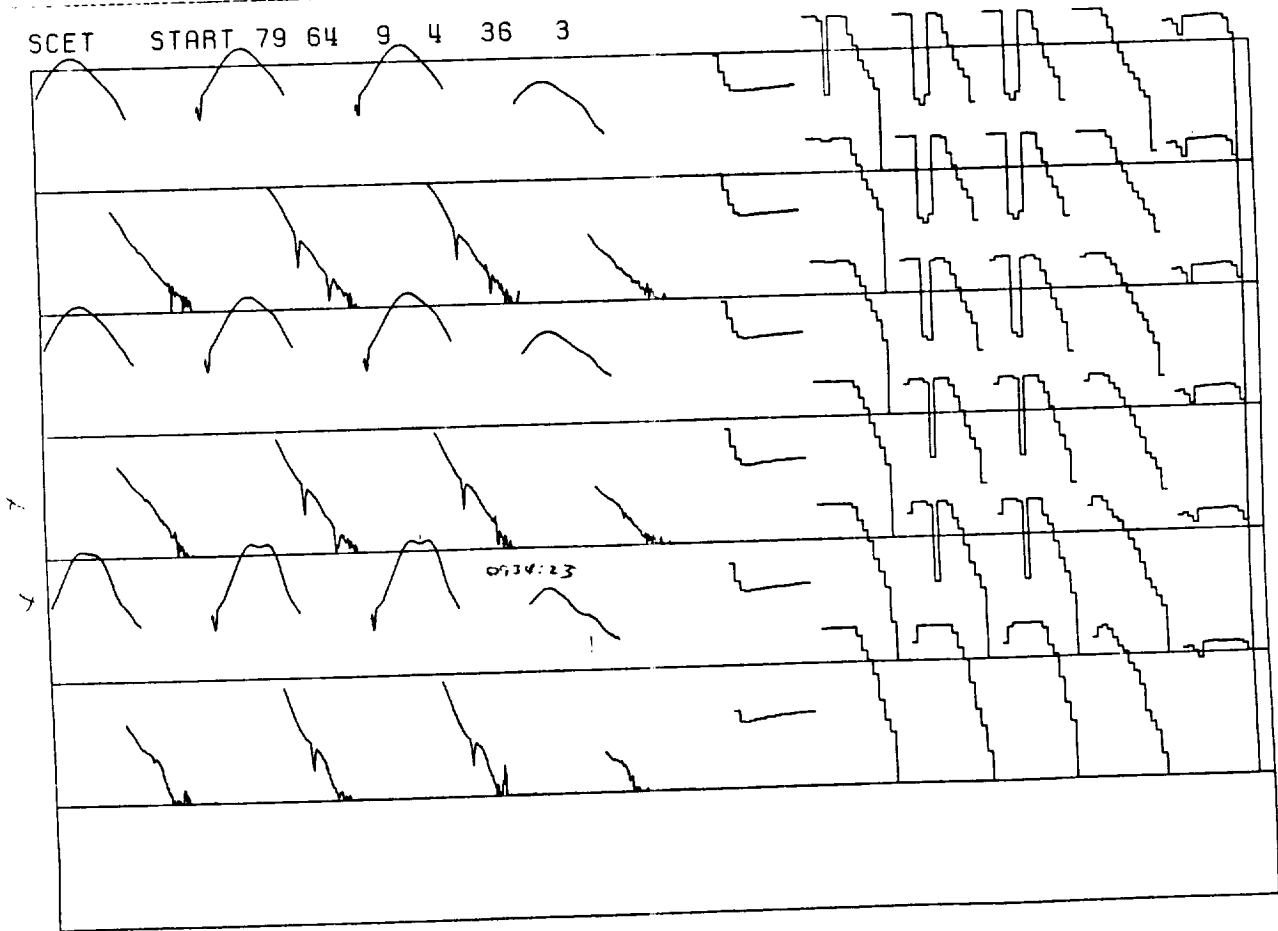
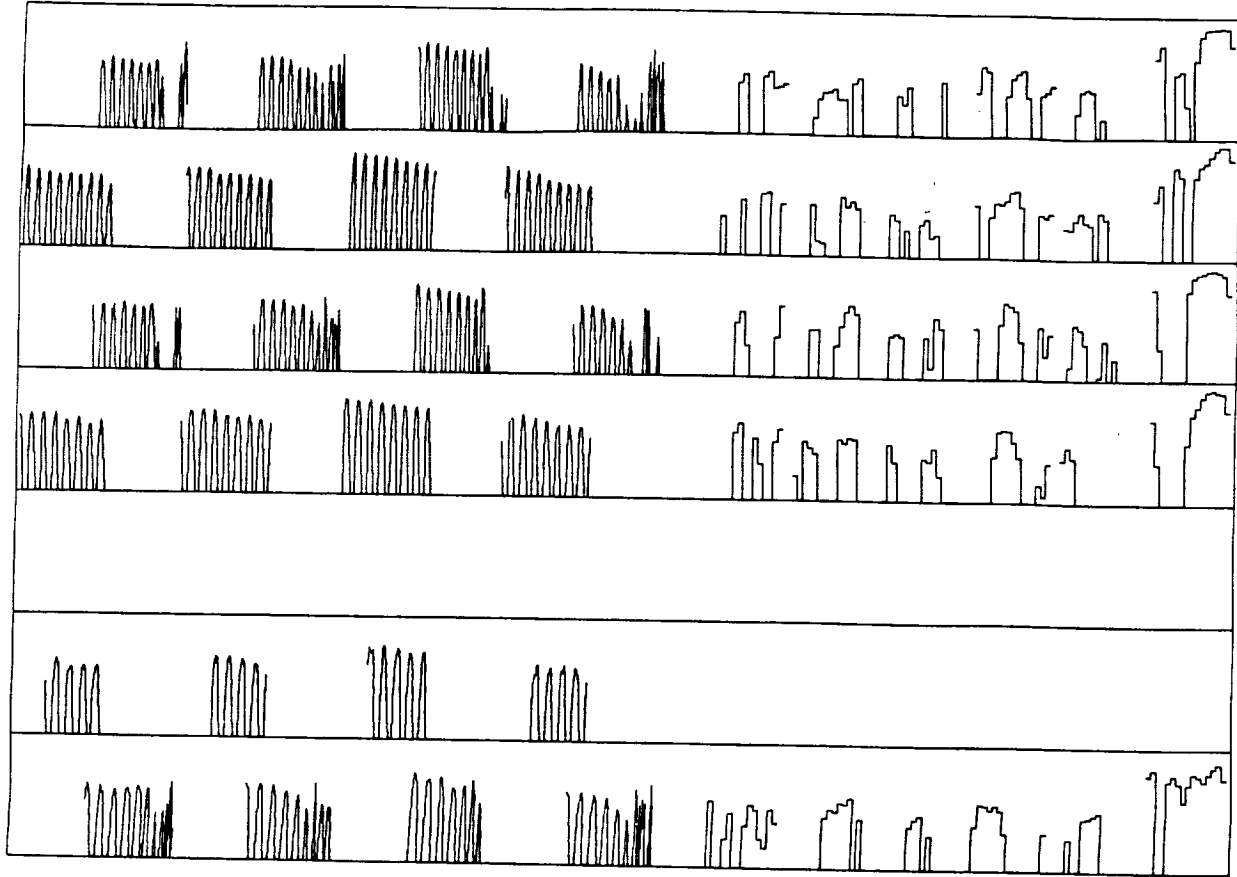


Fig. 114

SCET START 79 192 7 41 34 2



SCET START 79 192 7 41 34 3

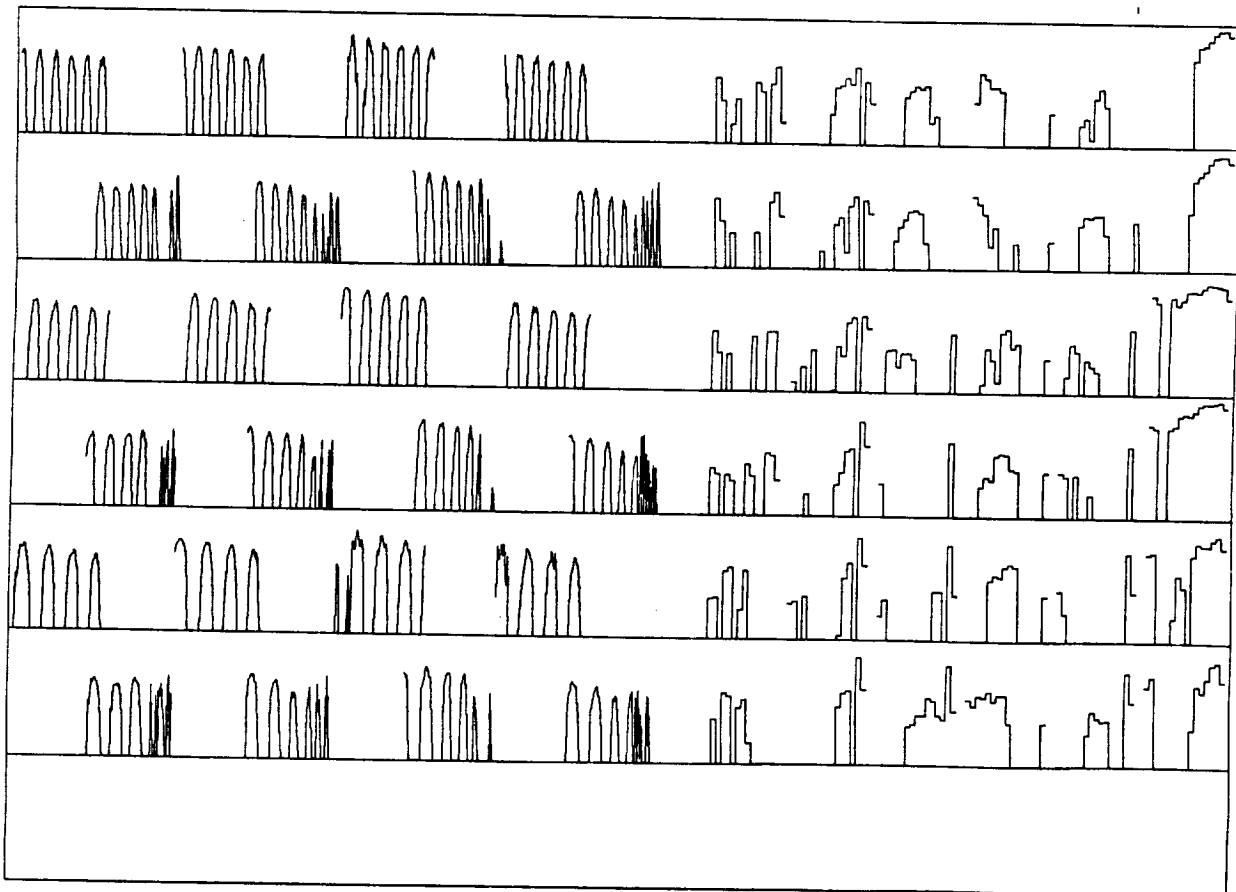
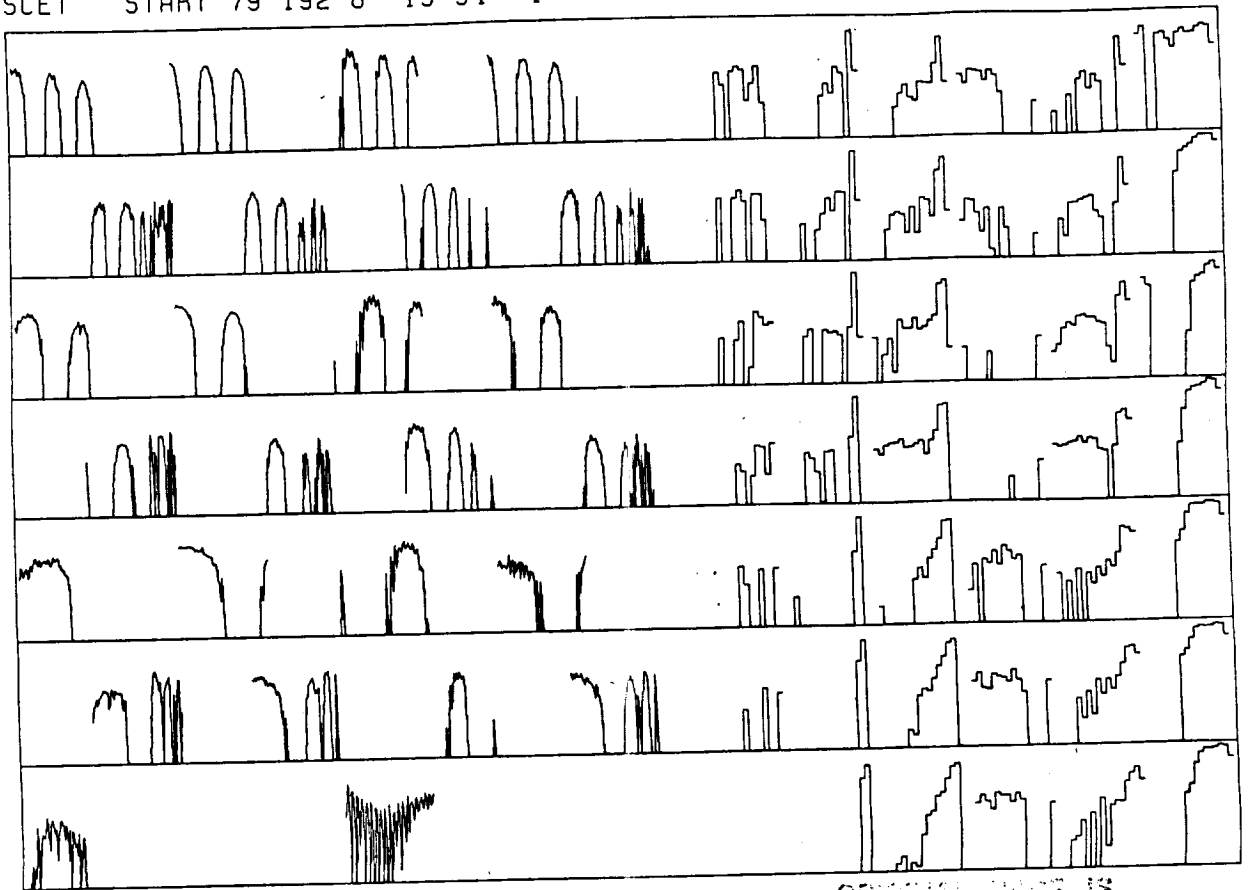


Fig. 115

SCET START 79 192 8 13 34 1



ORIGINAL IMAGE IS
OF POOR QUALITY

SCET START 79 192 8 13 34 2

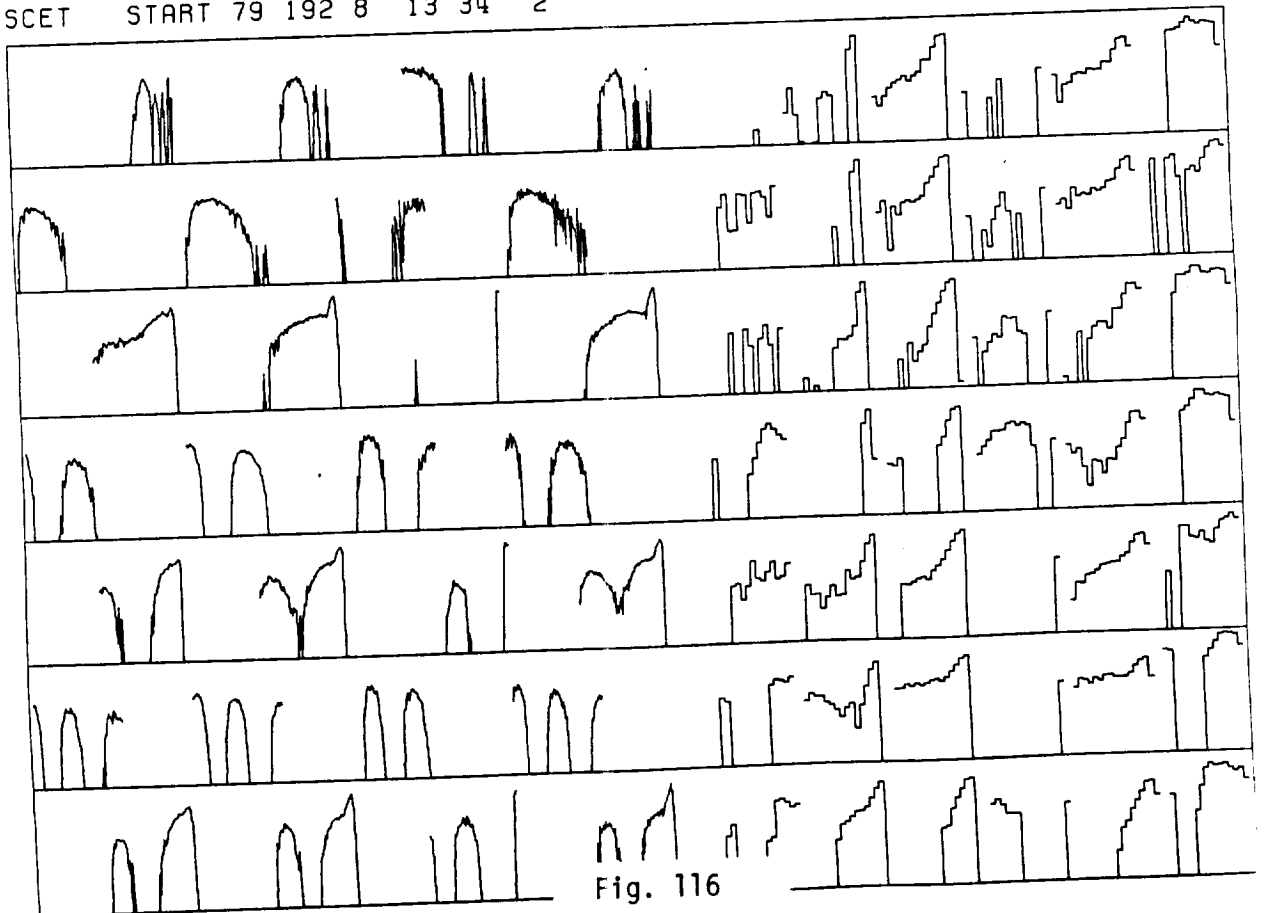


Fig. 116

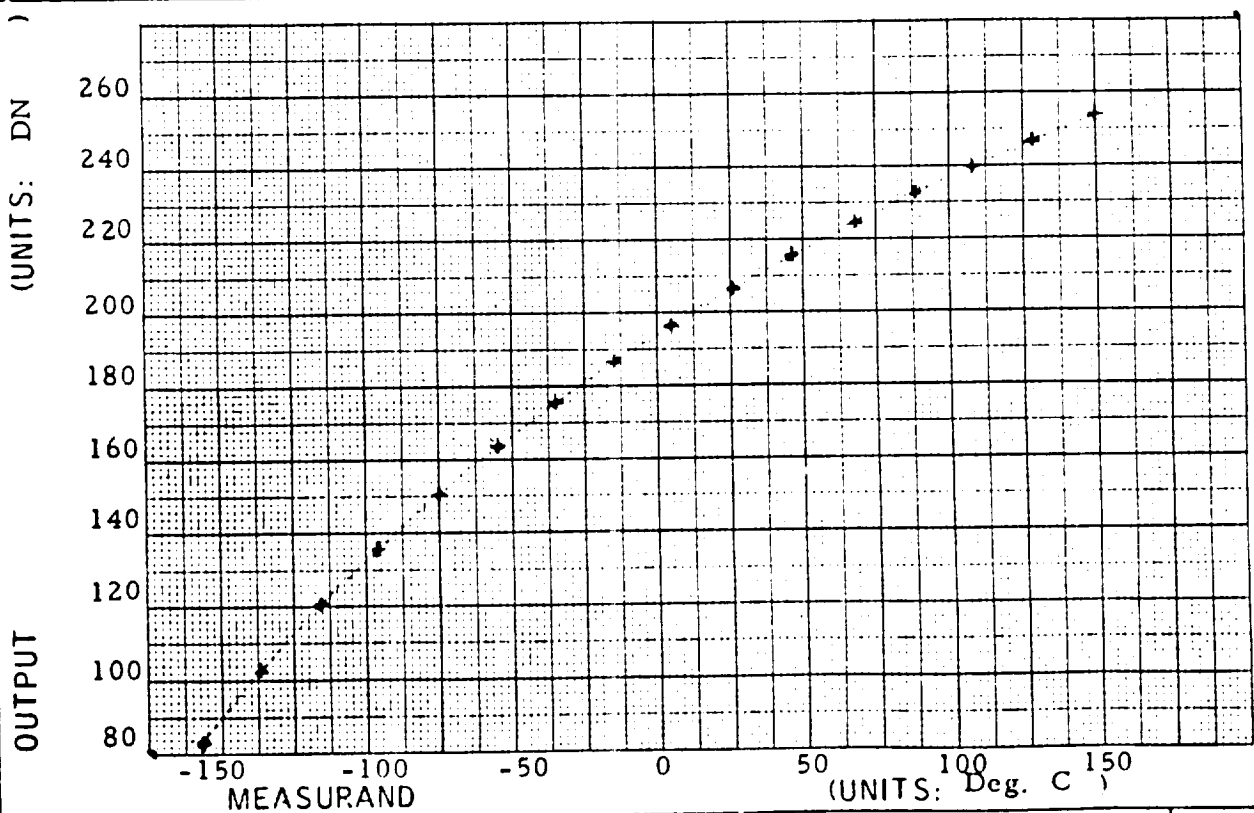
APPENDIX A



S/S ABBREV. PLS		MEASUREMENT TITLE PLS SEN T		TTS NO. E-622	
SUBASSEMBLY NAME Plasma Subsystem			SUBASSY. REF. NO. 2032	SUBASSY. SER. NO. 002	CALIBRATION TEMP. N/A
SENSING DEVICE <input checked="" type="checkbox"/> TRANSDUCER <input type="checkbox"/> OTHER		TRANSDUCER TYPE	TRANSDUCER PART NO. ST 11785-0004	TRANSDUCER SER. NO. 8676	
CALIBRATED BY C. Odd		DATE 10/21/77	APPROVED BY <i>A.R. Zieger</i>		DATE 10/25/77

CALIBRATION: LOAD IMPEDANCE USED: _____ MEGOHMS, TRANSD EXCITATION _____

MEASURAND (UNITS Deg. C)	OUTPUT (UNITS DN)	MEASURAND (UNITS Deg. C)	OUTPUT (UNITS CN)
-157.59	83	68.299	224
-137.50	102	89.00	232
-116.29	120	108.19	239
-96.699	135	128.50	246
-75.199	150	150.19	253
-55.00	163		
-34.70	175		
-14.499	186		
+5.100	196		
26.199	206		
46.500	215		



COMMENTS: Table Lookup Coefficients ORIGINAL PAGE IS OF POOR QUALITY E-622

MJS 77 NO -2
S/C-31
VGR-1

SC 31

ORIGINAL PAGE IS
OF POOR QUALITY

RUN 0697 0022PLS

FRAME 15
8

MJS77 SERIAL NO..... MJS-2
MJS77 FUNCTION PLS SENSOR TEMP

FDS TREESWITCH ID .. 70
FDS RANGE 25-800 OHMS
FDS SERIAL NO..... 2

SUBASSY REF NO..... 2032
SUBASSY SERIAL NO... 002

MEAS CALIB RANGE ... -70 TO 100 DEG C
MEAS CALIB TEMP -

XDUCER SERIAL NO.... 8676
XDUCER IMPEDANCE ... -
XDUCER CALIB DATE .. 9 OCT 74

DATA PREPARED BY ... ROSEMONT ENC CO
APPROVED BY ... -
APPROVED BY ... R. ROTTER
RUN DATE 0697 0022PLS

STANDARD DEVIATION . .56643248-01

COEFFICIENT A0 -.20276987+03
COEFFICIENT A152035174+00
COEFFICIENT A225540733-03
COEFFICIENT A312712726-04

MEASURAND EU	OUTPUT DN	F(X) PRIME	DELTA
-70.00	154.15	-69.9296	-.070376
-60.00	160.56	-60.0212	.021169
-50.00	166.69	-50.0593	.059255
-40.00	172.55	-40.0605	.060527
-30.00	178.18	-30.0336	.033602
-20.00	183.57	-20.0041	.004107
-10.00	188.75	-9.9694	-.030637
.00	193.73	.0513	-.051264
10.00	198.52	10.0619	-.061867
20.00	203.15	20.0596	-.059597
30.00	207.62	30.0397	-.039662
40.00	211.94	40.0054	-.005437
50.00	216.13	49.9684	.031590
60.00	220.20	59.9328	.067192
70.00	224.17	69.9159	.084074
80.00	228.04	79.9327	.067263
90.00	231.83	89.9904	.009581
100.00	235.55	100.1195	-.119519

DATA NUMBER

	0	2	4	6	8
0	-202.77	-201.73	-200.68	-199.64	-198.58
10	-197.53	-196.47	-195.40	-194.33	-193.25
20	-192.16	-191.06	-189.96	-188.84	-187.72
30	-186.59	-185.44	-184.28	-183.11	-181.93
40	-180.73	-179.52	-178.30	-177.06	-175.80
50	-174.52	-173.23	-171.92	-170.60	-169.25
60	-167.88	-166.50	-165.09	-163.66	-162.21
70	-160.73	-159.24	-157.71	-156.17	-154.60
80	-153.00	-151.37	-149.72	-148.04	-146.34
90	-144.60	-142.84	-141.04	-139.21	-137.36
100	-135.47	-133.55	-131.59	-129.60	-127.58
110	-125.52	-123.43	-121.30	-119.13	-116.92
120	-114.68	-112.40	-110.08	-107.72	-105.32
130	-102.88	-100.39	-97.87	-95.30	-92.69
140	-90.03	-87.33	-84.58	-81.79	-78.95
150	-76.06	-73.13	-70.15	-67.12	-64.04
160	-60.90	-57.72	-54.49	-51.20	-47.86
170	-44.47	-41.03	-37.53	-33.97	-30.36
180	-26.69	-22.97	-19.18	-15.34	-11.44
190	-7.49	-3.47	.61	4.75	8.95
200	13.22	17.55	21.94	26.39	30.91
210	35.50	40.15	44.87	49.66	54.51
220	59.43	64.43	69.49	74.62	79.82
230	85.10	90.44	95.86	101.36	106.92
240	112.57	118.28	124.08	129.95	135.89
250	141.92	148.02	154.20	160.46	

DEG C

E-622

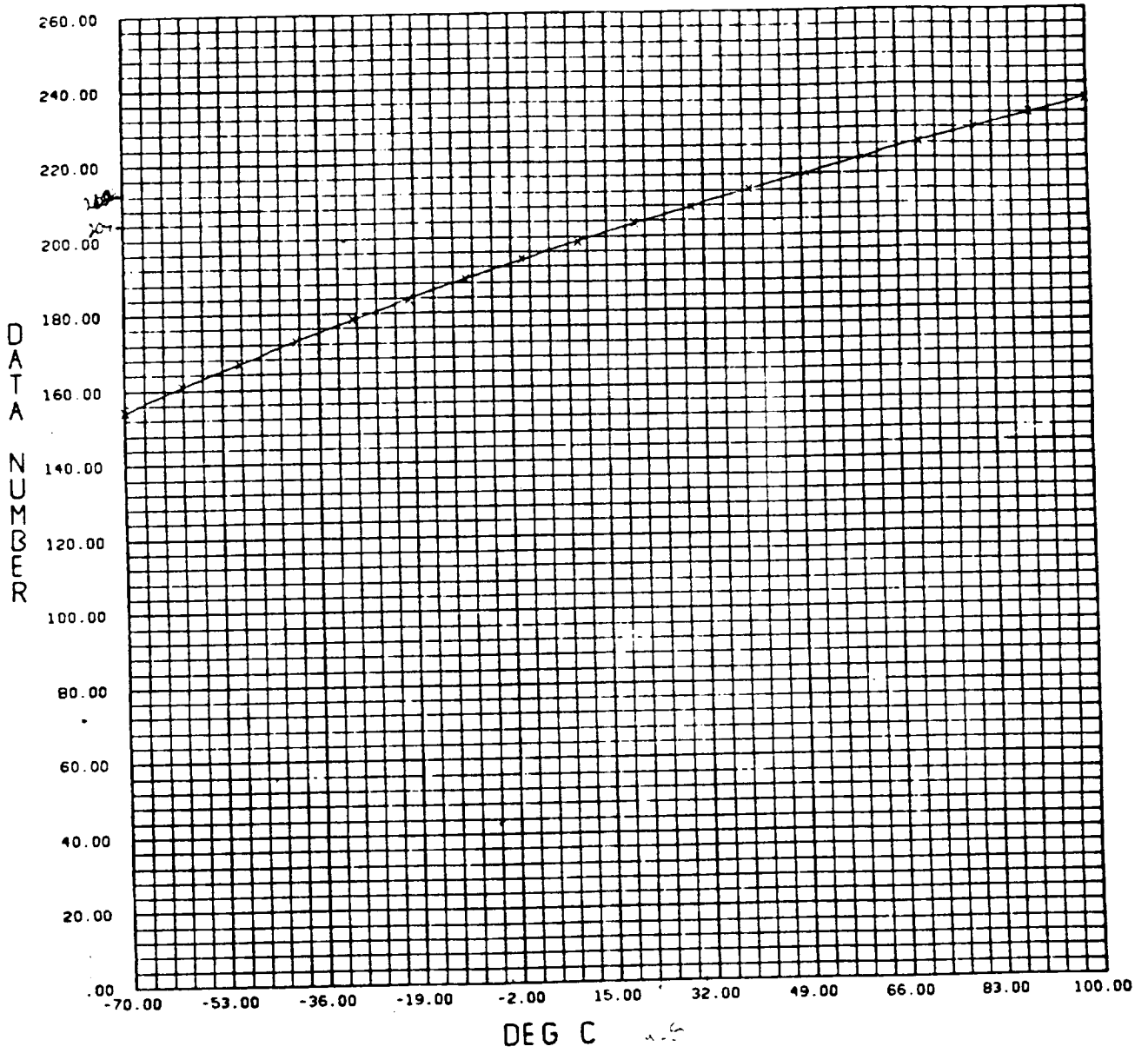
PLS SEN T

SC31

ORIGINAL PAGE IS
OF POOR QUALITY

RUN 0697 0022PLS

FRAME 16



E-622

PLS SEN T

8C31

ORIGINAL PAGE IS
OF POOR QUALITY

RUN 0397 002PPLS

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MULTI SERIAL NO.....	MJS-2			0	-79.66	-78.25	-76.84	-75.43	-74.03
MULTI FUNCTION.....	PLS MODULATOR TEMP			10	-72.62	-71.21	-69.80	-68.39	-66.99
FDS THRESHOLD ID.....	58			20	-65.58	-64.17	-62.76	-61.36	-59.95
FDS RANGE.....	350-700 OHMS			30	-58.54	-57.13	-55.72	-54.32	-52.91
FDS SERIAL NO.....	2			40	-51.50	-50.09	-48.69	-47.28	-45.87
SUBSECT REF NO.....	2032			50	-44.46	-43.05	-41.65	-40.24	-38.83
SUB-ISA SERIAL NO.....	002			60	-37.42	-36.02	-34.61	-33.20	-31.79
MEAS CALIB RANGE.....	-70 TO 100 DEG C			70	-30.38	-28.98	-27.57	-26.16	-24.75
MEAS CALIB TEMP.....	-			80	-23.34	-21.94	-20.53	-19.12	-17.71
INDICER SERIAL NO.....	LASS			90	-16.31	-14.90	-13.49	-12.08	-10.67
INDICER IMPEDANCE.....	-			100	-9.27	-7.86	-6.45	-5.04	-3.64
INDICER CALIB DATE.....	11 NOV 74			110	-2.23	-0.82	.59	2.00	3.40
DATA PREPARED BY.....	ROSEMONT ENG CO			120	4.81	6.22	7.63	9.03	10.44
APPROVED BY.....	-			130	11.85	13.26	14.67	16.07	17.48
APPROVED BY.....	R. ROTTER			140	18.89	20.30	21.70	23.11	24.52
RUN DATE.....	0397 002PPLS			150	25.93	27.34	28.74	30.15	31.56
STANDARD DEVIATION.....	.34950326-00			160	32.97	34.38	35.78	37.19	38.60
COEFFICIENT A0.....	.79657113-02			170	40.01	41.41	42.82	44.23	45.64
COEFFICIENT A1.....	.70390205-00			180	47.05	48.45	49.86	51.27	52.68
ME-LEAD	OUTPUT	F(V)	DELTA	190	54.08	55.49	56.90	58.31	59.72
EU	DN	PRIME		200	61.12	62.53	63.94	65.35	66.75
-70.00	12.74	-70.6907	.690693	210	68.16	69.57	70.98	72.39	73.79
-80.00	27.32	-60.4288	.428842	220	75.20	76.61	78.02	79.42	80.83
-50.00	41.84	-50.2076	.207632	230	82.24	83.65	85.06	86.46	87.87
-40.00	56.39	-40.0271	.027062	240	89.28	90.69	92.09	93.50	94.91
-30.00	70.71	-29.8921	-.117947	250	96.32	97.73	99.13	100.54	
-20.00	85.06	-19.7675	-.232475						
-10.00	99.40	-9.6286	-.311442						
0.00	113.69	.3599	-.359927						
10.00	127.92	10.3830	-.293015						
20.00	142.12	20.3907	-.380699						
30.00	156.28	30.3479	-.347901						
40.00	170.40	40.2897	-.289705						
50.00	184.48	50.2010	-.201028						
60.00	198.53	60.0870	.086950						
70.00	212.53	69.9424	.057609						
80.00	226.49	79.7724	.027567						
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DATA NUMBER

DEG C

E-623

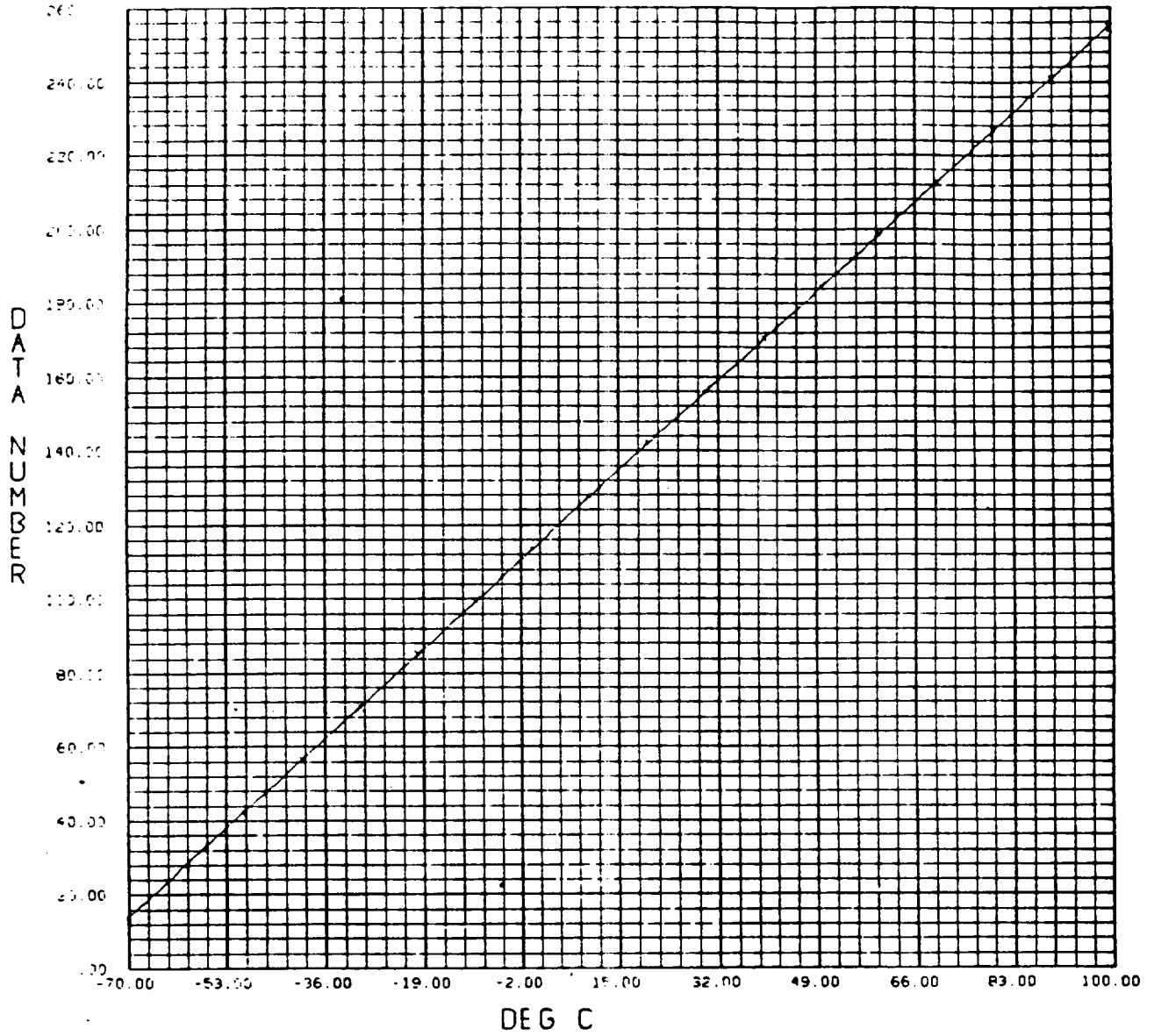
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SCJ1

ORIGINAL PAGE IS
OF POOR QUALITY

RUN 0397 0022PLS

FRAME



E-623

PLS MOD T

SC 31

ORIGINAL PAGE IS
OF POOR QUALITY

RUN 0397 0022PLS

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	FRAME					
MJS77 SERIAL NO..... MJS-2	0	-80.11	-78.70	-77.29	-75.88	-74.47
MJS77 FUNCTION PLS ELECTRONICS TEMP	10	-73.06	-71.66	-70.25	-68.84	-67.43
FDS TREESWITCH ID ... F6	20	-66.02	-64.61	-63.21	-61.80	-60.39
FDS RANGE 350-700 OHMS	30	-58.98	-57.57	-56.17	-54.76	-53.35
FDS SERIAL NO..... 2	40	-51.94	-50.53	-49.12	-47.72	-46.31
SUBASSY REF NO..... 2032	50	-44.90	-43.49	-42.08	-40.67	-39.27
SUBASSY SERIAL NO... 002	60	-37.86	-36.45	-35.04	-33.63	-32.22
MEAS CALIB RANGE ... -70 TO 100 DEG C	70	-30.82	-29.41	-28.00	-26.59	-25.18
MEAS CALIB TEMP -	80	-23.77	-22.37	-20.96	-19.55	-18.14
XDUCER SERIAL NO.... 6135	90	-16.73	-15.32	-13.92	-12.51	-11.10
XDUCER IMPEDANCE ... -	100	-9.69	-8.28	-6.87	-5.47	-4.06
XDUCER CALIB DATE .. 3 MAR 72	110	-2.65	-1.24	.17	1.57	2.98
DATA PREPARED BY ... ROSEMONT ENG CO	120	4.39	5.80	7.21	8.62	10.02
APPROVED BY ... -	130	11.43	12.84	14.25	15.66	17.07
APPROVED BY ... R. ROTTER	140	18.47	19.88	21.29	22.70	24.11
RUN DATE 0397 0022PLS	150	25.52	26.92	28.33	29.74	31.15
STANDARD DEVIATION . .34991763+00	160	32.56	33.97	35.37	36.78	38.19
Coefficient A0 -.80105934+02	170	39.60	41.01	42.42	43.82	45.23
Coefficient A170414370+00	180	46.64	48.05	49.46	50.86	52.27
MEASURAND	190	53.68	55.09	56.50	57.91	59.31
EU	200	60.72	62.13	63.54	64.95	66.36
OUTPUT	210	67.76	69.17	70.58	71.99	73.40
DN	220	74.81	76.21	77.62	79.03	80.44
F(X)	230	81.85	83.26	84.66	86.07	87.48
PRIME	240	88.89	90.30	91.71	93.11	94.52
DELTA	250	95.93	97.34	98.75	100.16	

DATA NUMBER

DEG C

E-621

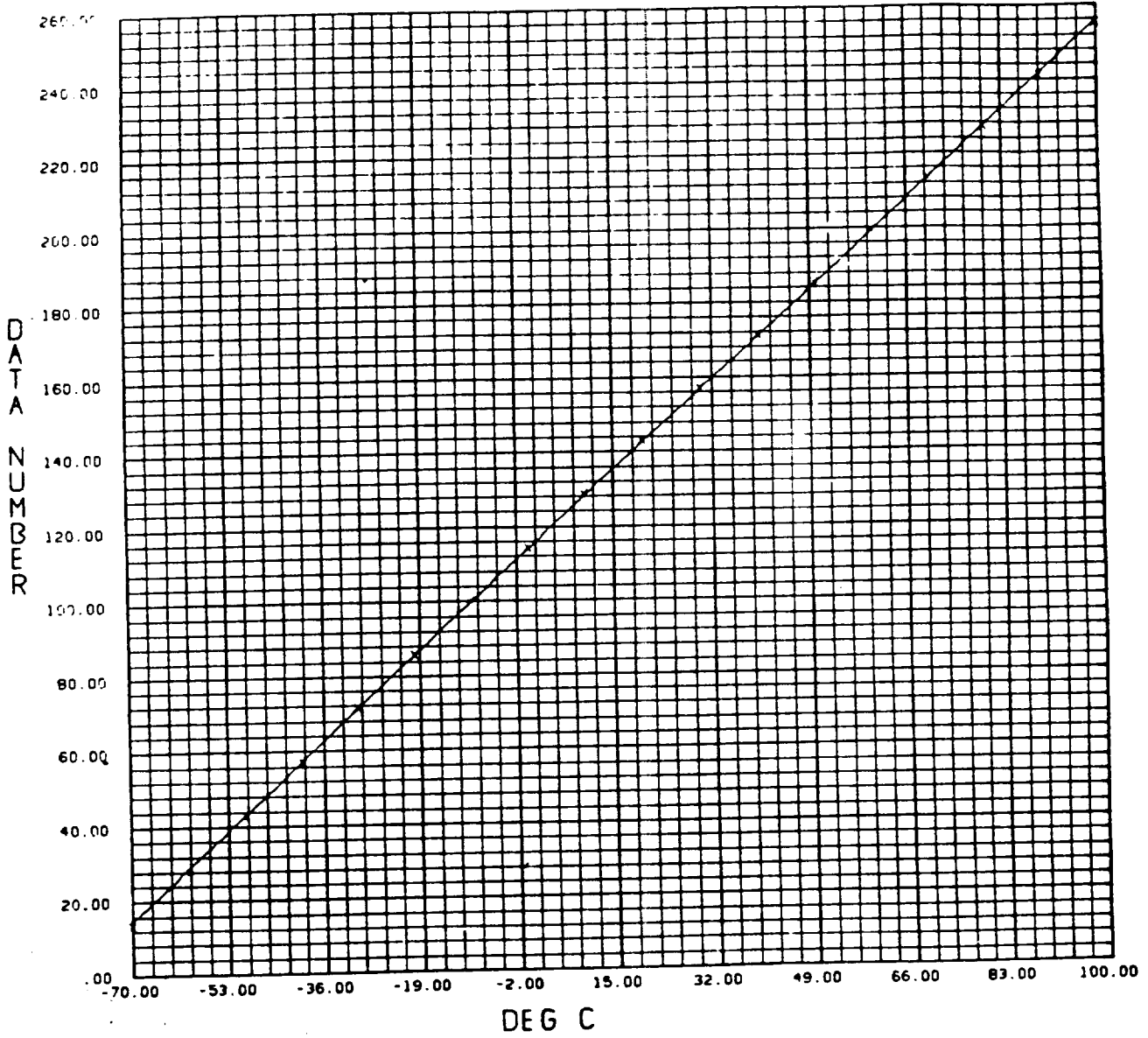
PLS EL T

SC31

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OF POOR QUALITY

RUN 0397 0022PLS

FRAME 10



E-621

PLS EL T

APPENDIX B

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Fri May 15 15:40:15 EDT 1987

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```

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ORIGINAL PAGE IS OF POOR QUALITY

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ORIGINAL SOURCE OF POWER

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r1mint( 4.19199218750000 ) = 9.1112584672439d-02
r1mint( 4.21679687500000 ) = 9.2089925341502d-02
r1mint( 4.24160156250000 ) = 9.3081841425532d-02
r1mint( 4.26640625000000 ) = 9.4096206128575d-02
r1mint( 4.29121093750000 ) = 9.5123675144164d-02
r1mint( 4.31601562500000 ) = 9.6173959007386d-02
r1mint( 4.34082031250000 ) = 9.7240555287394d-02
r1mint( 4.36562500000000 ) = 9.8321621737157d-02
r1mint( 4.39042968750000 ) = 9.9425420397581d-02
r1mint( 4.41523437500000 ) = 0.10054744224483
r1mint( 4.44003906250000 ) = 0.10169100493293
r1mint( 4.46484375000000 ) = 0.10285361313772
r1mint( 4.48964843750000 ) = 0.10403531138192
r1mint( 4.51445312500000 ) = 0.10523732026966
r1mint( 4.53925781250000 ) = 0.10646323123916
r1mint( 4.56406250000000 ) = 0.10770748168958
r1mint( 4.58886718750000 ) = 0.10897416334504
r1mint( 4.61367187500000 ) = 0.11025910242613
r1mint( 4.63847656250000 ) = 0.11156806757619
r1mint( 4.66328125000000 ) = 0.11290138106085
r1mint( 4.68808593750000 ) = 0.11425654298876
r1mint( 4.71289062500000 ) = 0.11563326317740
r1mint( 4.73769531250000 ) = 0.11703637834104
r1mint( 4.76250000000000 ) = 0.11845029893015
r1mint( 4.78730468750000 ) = 0.11990346001197
r1mint( 4.81210937500000 ) = 0.12137455794868
r1mint( 4.83691406250000 ) = 0.12286857007173
r1mint( 4.86171875000000 ) = 0.12438533607687
r1mint( 4.88652343750000 ) = 0.12592970987433
r1mint( 4.91132812500000 ) = 0.12750522563749
r1mint( 4.93613281250000 ) = 0.12909101535385
r1mint( 4.96093750000000 ) = 0.13070615935510
r1mint( 4.98574218750000 ) = 0.1323518151040
r1mint( 5.01054687500000 ) = 0.13402279864215
r1mint( 5.03535156250000 ) = 0.13571882401392
r1mint( 5.06015625000000 ) = 0.13742590346827

```

Sun May 17 07:56:07 EDT 1987

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APPENDIX C

```

C      03/21/84 16:14:04 03/21/84 14:46:26 $380300.MJS
C      FUNCTION CPRESP(V,UU,SUP,ZCU,AEVV,III)
C      11/12/78 VMV
C      REVISED 12/30/78 VMV
C      COMPUTES RESPONSE FUNCTION OF VOYAGER CUP, IN (CURRENT UNIT)CM**3/SC
C      V(3)=VELOCITY VECTOR, CM/SEC
C      UU=EFFEKTIVE MODULATOR VOLTAGE (VOLTS*Z, INCLUDING SIGN)
C      SUP= SUPPRESSOR VOLTAGE
C      ZCU= PARTICLE CHARGE
C      AEVV=PARTICLE MASS (AEVV*V**2=ENERGY IN EV)
C      III=CUP INDEX 1=A, 2=B, 3=C, 4=D PROTON MODE, 5=D ELECTRON MODE
C
C      SUBPROGRAMS CALLED - - - TRANSN,TRANSD,DIPLN,DISPLD,ARMAIN,ARSD

```

CPRESP

```

C      REAL*8 $$$DT(6) 1'$$DATE$$,'03/21/84','14:46:26',
C      1' CPRESP','FORTRAN','MJS' '1'

```

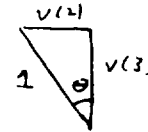
FOR AREA CORRECTION

$$I = \int \vec{F} \cdot d\vec{S}$$

$$= F S \cos \theta$$

$$= (F \cos \theta) S$$

where F is unit flux



$$v(1) = 0.0$$

$$v(2) = \sin \theta$$

$$v(3) = \cos \theta$$

```

C      DIMENSION V(3)
C      common /comellos/ ilossm,ilosd,ilossi
C      ilossm 1 for e1 voltage, 2 for e2 or ion voltages
C      ilosd 0 no losses, 1 isotropic secondaries, 2 cosine law
C      data dml /1.6153/, ame /3.553513e-19/

```

```

C      VZ=V(3)
C      IF(VZ.LE.0.)GO TO 99
C      U=AEVV*VZ**2
C      GET TRANSPARENCY AND BEAM DISPLACEMENT FACTOR
C      IF(III.GE.4)GO TO 5
C      TR=TRANSN(V,U,UU,SUP)
C      BDSPL=DISPLN(U,UU,SUP)
C      GET AREA

```

FOR INCOMING PHOTONS AT ANGLE θ

SET

$$U = 0.0$$

$$P = 0.0$$

$$ILOSS1 = 7 \text{ (norm. supp., IDN)}$$

3

```

C      X=BDSPL*V(1)/VZ
C      Y=BDSPL*V(2)/VZ
C      AR=ARMAIN(X,Y)
C      alossd = 0.0
C      GO TO 20
C      COME HERE FOR SIDE SENSOR
C      TR=TRANSD(V,U,UU,SUP)
C      CALL DISPLD(V,U,UU,SUP,X,Y)
C      AR=ARSD(X,Y,aloss,ilossi)

```

GIVES CORRECT TRANSPARENCY AND "DISPLACEMENT" TO FIND AREA OF COLLECTOR ACTUALLY ILLUMINATED

```

C      IF ( ar*aloss .eq. 0.0) then
C          alossd = 0.0
C      else
C          vt2 = v(1)**2 + v(2)**2
C          vt = sqrt(vt2)
C          vz2 = v(3)**2
C          vv2 = vt2 + vz2
C          vv = sqrt(vv2)
C          epem = ame*(vt2 + vz2)
C          costhp = vz/vv
C          del = dml /costhp*epem**0.35*
C              (1.0-exp(-2.28*costhp*epem**1.35))
C          alossd = 1.0*del*aloss
C      end if
C      IF (ilosd .lt. 0) then
C          ar = 0.0
C          alossd = -alossd
C      end if

```

EFFECTIVE LOSS AREA

including correction for angle of incidence

This quantity multiplied by the photo current density should give the measured current

YIELD PER INCIDENT ELECTRON

$$PUT \quad AEVV = 1$$

$$ZCU = 1$$

$$ILOSSD = 1, 2$$

$$ILOSSM = 2$$

$$III = 4$$

RELEVANT OUTPUT QUANTITY IS

$$(aloss)(TR)$$

```

20 CONTINUE
C      PUT IT ALL TOGETHER
C      CPRESP=ZCU*VZ*TR*(AR - alossd)
C      CHANGE SIGN OF CURRENT IN ELECTRON MODE, TO KEEP OUTPUT SIGNAL POSIT

```


C

IVE

99

```
IF(III.EQ.5)CPRESP=-CPRESP  
RETURN  
CPRESP=0.  
RETURN  
END
```

```

C          03/22/85  14:01:55    03/22/85  13:52:09    $380300.MJS
C          FUNCTION ARSIDE(DAS,DSC,aloss,ils)
C          12/30/78
C          COMPUTES AREA IN SQ.CM, OF VOYAGER SIDE SENSOR
C          DAS=RELATIVE DISPLACEMENT OF APERTURE AND SHIELD CIRCLE CENTERS, CM
C          DSC=RELATIVE DISPLACEMENT OF SHIELD AND COLLECTOR CIRCLE CENTERS, CM
C          aloss is loss function from secondary electrons on collector
C
C
C          CCC
C          CCCCCCCCC
C
C          HERR SULLIVAN SOLL DIESES PROGRAM SCHREIBEN
C          REAL*8 $$$DT(6) / '$$DATE$$', '03/22/85', '13:52:09',
C          | ' ARSIDE', ' FORTRAN', 'MJS' ' /
C          COMMON /SDTABL/TABLS(25,25),NDAS,NDSC,DDAS,DDSC
C          LOOK-UP TABLE FOR AREA OF SIDE SENSOR
C          TABLS(NDAS,NDSC) = AREA OF SIDE SENSOR AT (DAS,DSC)
C          NDAS,NDSC SIZE OF ARRAY
C          DDAS,DDSC RESPECTIVE STEP SIZE
C          common /sidloss/ tabls(25,25,8)
C          tabel of losses for secondary electrons
C          same indicies as for tablsd
C          third index is for type of configuration
C          i=0 noloss, i=odd normal supressor, even reverse supressos
C          i< 5 isotropic secondary production, i>4 cosine law secondary
C          i=1,2,5,6 e1 voltages, i=3,4,7,8 e2 or ion voltages
C
C          LOGICAL INIT
C          data INIT/.TRUE./
C          IF (INIT) CALL REDART
C          INIT = .FALSE.
C          ARSIDE = 0
C          XAS = DAS/DDAS+1.0
C          XSC = DSC/DDSC+1.0
C          NAS = XAS
C          NSC = XSC
C          IF(NAS+1.GE.NDAS.OR.NSC+1.GE.NDSC) RETURN
C          IF(NAS.GT.0.AND.NSC.GT.0) GO TO 10
C          RETURN
10         CONTINUE
C          FOUR POINT BIVARIATE INTERPOLATION
C          DXAS = XAS-NAS
C          CXAS = 1.0-DXAS
C          DXSC = XSC-NSC
C          CXSC = 1.0-DXSC
C          if ( ils .ne. 0) then
C             aloss = (TABLs(NAS,NSC,ils)*CXAS+TABLs(NAS+1,NSC,ils)*
C             |         DXAS)*CXSC+
C             1 (TABLs(NAS,NSC+1,ils)*CXAS+TABLs(NAS+1,NSC+1,ils)*DXAS)*
C             |         DXSC
C          else
C             aloss = 0.0
C          end if
C          ARSIDE = (TABLS(NDAS,NDSC)*CXAS+TABLS(NDAS+1,NDSC)*DXAS)*CXSC+
C          1 (TABLS(NDAS,NDSC+1)*CXAS+TABLS(NDAS+1,NDSC+1)*DXAS)*DXSC
C          RETURN
C          END

```

ARSIDE

```

C          01/16/85  16:04:22      01/16/85  10:11:39      $380300.MJS
C          SUBROUTINE REDART
C          CMS VERSION OF SETART FOR READING IN AREA TABLES PREVIOUSLY GENERATED
C          WITH ARGEN.
C
C          FT21F001 FOR MAIN SENSOR
C          FT22F001 FOR SIDE SENSOR
C
C          FILEDEF FT21F001 X DSN CSR $380300 ARMAIN DATA (PERM RECFM VBS
C          BLKSIZE 19069 DSORG PS
C          FILEDEF FT22F001 X DSN CSR $380300 ARSIDE DATA (PERM RECFM VBS
C          BLKSIZE 19069 DSORG PS
C
C          REAL*8 $$$DT(6) /'$$DATE$$','01/16/85','10:11:39',
C          | ' REDART',' FORTRAN','MJS      '/
C          COMMON /MNTABL/TABL MN(32,32),NSTPX,NSTPY,DSTPX,DSTPY,XMAX,YMIN,
C          * YMAX
C          LOOK-UP TABLE FOR AREA OF MAIN SENSOR
C          TABLMN(IX,IY)= AREA OF MAIN SENSOR AT X=VX/VZ8 Y=VY/VZ
C          NSTPX, NSTPY SIZE OF ARRAY IN X,Y
C          DSTPX= STEP SIZE IN X,      DSTPY= STEP SIZE IN Y
C          XMAX,YMIN,YMAX LIMITS BEYOND WHICH AREA IS ZERO
C          PRESUME XMIN=0.      AREA SAME FOR +X,-X
CCC
C          COMMON /SDTABL/TABLSD(25,25),NDAS,NDSC,DDAS,DDSC
C          LOOK-UP TABLE FOR AREA OF SIDE SENSOR
C          TABLSD(IAS,ISC) = AREA OF SIDE SENSOR AT (DAS,DSC)
C          NDAS,NDSC SIZE OF ARRAY
C          DDAS,DDSC RESPECTIVE STEP SIZEA
C
C          common /sidloss/ tablls(25,25,8)
C          real t1(25,25),t2(25,25),t3(25,25),t4(25,25)
C          real t5(25,25),t6(25,25),t7(25,25),t8(25,25)
C          equivalence (t1(1,1),tablls(1,1,1))
C          equivalence (t2(1,1),tablls(1,1,2))
C          equivalence (t3(1,1),tablls(1,1,3))
C          equivalence (t4(1,1),tablls(1,1,4))
C          equivalence (t5(1,1),tablls(1,1,5))
C          equivalence (t6(1,1),tablls(1,1,6))
C          equivalence (t7(1,1),tablls(1,1,7))
C          equivalence (t8(1,1),tablls(1,1,8))
C          tabel of losses for secondary electrons
C          same indicies as for tablsd
C          third index is for type of configuration
C          i=0 noloss, i=odd normal surpressor, even reverse supressos
C          i< 5 isotropic secondary production, i>4 cosine law secondary
C          i=1,2,5,6 el voltages, i=3,4,7,8 e2 or ion voltages
C
C          LOGICAL FIRST
C          Integer ia,ib
C          data FIRST/.FALSE./
C          IF (FIRST) RETURN
C          FIRST = .TRUE.
C          open(21 file="redart.data" form="unformatted")
C          ia = -31
C          call init( 1, ia, ib)
C
C          READ (31) TABLMN,          DSTPX,DSTPY,XMAX,YMIN,YMAX
C          1024 1 1 1 1 1 1 1
C          1024 1 2 1 2 3 4 5
C          READ (31) TABLSD,          DDAS,DDSC

```

```
c          625    1    1    1    1
c          625    1    2    1    2
      read (31)
| NDAS,NDSC
| ,          NSTPX,NSTPY
c
      call initex( 1, ia, ib)
      read (31,end=100) t1
      read (31,end=100) t2
      read (31,end=100) t3
      read (31,end=100) t4
      read (31,end=100) t5
      read (31,end=100) t6
      read (31,end=100) t7
      read (31,end=100) t8
      return
100  continue
      write (6,*) ' do loss table read'
RETURN
END
```

APPENDIX D

S/C 31 YEAR	DOY	TYPE OF MANEUVER	# 360 YAW TURNS	# 360 ROLL TURNS	Comments
1978	048	CRSMVR	10	25	ABORTED
1978	257	CRSMVR	10	25	
1979	034	CRSMVR	10	25	
1979	288/9	CRSMVR	10	25	
1980	004	MAG-ROLL		1	
1980	031	CRSMVR	10	25	
1980	121	MAG-ROLL	0	1	
1980	168	CRSMVR	10	25	
1980	189	MAG-ROLL	0	1	
1980	235	Mini-CRSMVR	4	4	
1980	334	MAG-ROLL	0	1	
1981	041	CRSMVR	10	25	
1981	117	MAG-ROLL	0	1	
1981	134	CRSMVR	10	25	
1981	195	MAG-ROLL	0	1	
1981	321	CRSMVR	10	25	
1981	351	MAG-ROLL	0	2	
1982	089	CRSMVR	10	25	
1982	218	MAG-ROLL	0	2	
1982	300	Mini-CRSMVR	4	4	
1983	117	CRSMVR	10	25	
1983	145	MAG-ROLL	0	4	
1983	306	Mini-CRSMVR	4	4	
1984	011	Mini-CRSMVR	4	4	
1984	116	Mini-CRSMVR	4	4	
1984	193	Mini-CRSMVR	4	4	
1984	312	Mini-CRSMVR	4	4	
1985	059	Mini-CRSMVR	0	0	CANCELLED
1985	213	MAG-ROLL & ABCAL	0	4	
1985	238	MAG-YAW	4	0	
1985	283	Mini-CRSMVR	4	4	
1986	093/4	Mini-CRSMVR	4	4	
1986	155/6	Mini-CRSMVR	4	4	
1986	264/7	Mini-CRSMVR	4	4	
1986	309	Mini-CRSMVR	4	4	
1987	016	Mini-CRSMVR	4	4	
1987	155/6	Mini-CRSMVR	4	4	SCHEDULED

S/C 32 YEAR	DOY	TYPE OF MANEUVER	# 360 YAW TURNS	# 360 ROLL TURNS	Comments
1977	362	CRSMVR	10	25	
1978	275	CRSMVR	10	25	
1979	155	Mini-CRSMVR	4	4	
1980	024	CRSMVR	10	25	
1980	136	CRSMVR	10	25	
1980	192	MAG-ROLL	0	4	
1980	249	MAG-ROLL	0	1	
1980	341	MAG-ROLL	0	1	
1980	351	Mini-CRSMVR	4	4	
1981	077	Mini-CRSMVR	4	4	
1981	148	CRSMVR	10	25	
1981	302	Mini-CRSMVR	4	4	
1982	103	CRSMVR	10	25	
1982	293	Mini-CRSMVR	4	4	
1983	132	Mini-CRSMVR	4	4	
1983	188	MAG-ROLL	0	4	
1983	313	Mini-CRSMVR	4	4	
1984	020	MAG-ROLL	0	4	
1984	145	Mini-CRSMVR	4	4	
1984	206	MAG-ROLL	0	4	
1984	329	Mini-CRSMVR	4	4	
1985	036	MAG-ROLL	0	0	MISSED
1985	112	MAG-ROLL	0	4	
1985	150	Mini-CRSMVR	4	4	
1985	170	MAG-ROLL & ABCAL	0	4	
1985	231	MAG-ROLL & ABCAL	0	4	
1985	330	Mini-CRSMVR	4	4	
1986	036	Mini-CRSMVR	4	4	
1986	113	Mini-CRSMVR	4	4	
1986	197	Mini-CRSMVR	4	4	
1986	273	Mini-CRSMVR	4	4	
1986	339	Mini-CRSMVR	4	4	
1987	042	Mini-CRSMVR	4	4	
1987	133	Mini-CRSMVR	4	4	

MASSACHUSETTS INSTITUTE OF TECHNOLOGY
CENTER FOR SPACE RESEARCH
CAMBRIDGE, MASSACHUSETTS 02139

June 14, 1978

MEMORANDUM

To: J. Belcher, G. Gordon, A. Lazarus
From: J. D. Sullivan
Subject: Nominal Cruise Science Maneuver (CRSMVR)

1. A science maneuver comprises 10 yaw turns and 26 roll turns; it is possible to do an initial partial roll before commencing the yaw turns. We have requested partial rolls to bring the side sensor across the sun, and to sweep the main cluster through the ecliptic on different CRSMVR.

2. The schedule for yaw turns is:

Turn 1	AJ15	normal plasma
2	AJ15	normal plasma
3	AJ03	plasma, reversed grid
4	AJ15	normal plasma
5	AJ10	current cal. mod off
6	AJ11	current cal. mod on
7	AJ13	IDC mod on normal grid
8	AJ15	normal plasma
9	AJ15	normal plasma
10	AJ15	normal plasma

The purpose of the calibrations is to determine the modulator pickup with no plasma input and to measure the net photo current. To really clean this up, we probably should do a turn with IDC mod on reversed grid.

3. The schedule for roll turns is:

Turn 1 - 25	AJ15	normal plasma
26	AJ10	current cal. mod off

The prime roll turn calibration goal is intermeasurement chain calibration.

APPENDIX E

```

C      03/21/84  16:14:04  03/21/84  14:46:26  $380300.MJS
C      FUNCTION CPRESP(V,UU,SUP,ZCU,AEVV,III)
C      modified to compute respons to sunlight
C      11/12/78  VMV
C      REVISED 12/30/78  VMV
C      COMPUTES RESPONSE FUNCTION OF VOYAGER CUP, IN (CURRENT UNIT)CM**3/SC
C      V(3)=VELOCITY VECTOR, CM/SEC
C      UU=EFFEKTIVE MODULATOR VOLTAGE (VOLTS*Z, INCLUDING SIGN)
C      SUP= SUPPRESSOR VOLTAGE
C      ZCU= PARTICLE CHARGE
C      AEVV=PARTICLE MASS (AEVV*V**2=ENERGY IN EV)
C      III=CUP INDEX 1=A, 2=B, 3=C, 4=D PROTON MODE, 5=D ELECTRON MODE
C
C      SUBPROGRAMS CALLED  - - - TRANSN,TRANSD,DIPLN,DISPLD,ARMAIN,AR SIDE
C
C      REAL*8 $$$DT(6) / '$$DATE$$','03/21/84','14:46:26',
C      | ' CPRESP',' FORTRAN','MJS' ' /
C
C      DIMENSION V(3)
C      common /comellos/ ilossm,ilossd,ilossi
C      ilossm 1 for e1 voltage, 2 for e2 or ion voltages
C      ilossd 0 no losses, 1 isotropic secondaries, 2 cosine law
C      real ara(2),alossa(2)
C      data dml /1.6153/, ame /3.553513e-19/
C      data th1 /40./, th2 /80./, dth /0.5/ degrad /1.74533e-2/
C      th = th1
1     continue
C      v(1) = 0.0
C      tt = th*degrad
C      v(2) = sin(tt)
C      v(3) = cos(tt)
C      uu = 0.0
C      sup = 0.0
C      zcu = 1.0
C      aeVV = 1.0
C      iii = 4
C      VZ=V(3)
C      IF(VZ.LE.0.)GO TO 99
C      U=AEVV*VZ**2
5     TR=TRANSD(V,U,UU,SUP)
C      CALL DISPLD(V,U,UU,SUP,X,Y)
C      ilossm=2
C      do 10 ilossd=1,2
C      if (ilossd .eq. 1 ) then
C          ilossi = 3
C      else
C          ilossi = 7
C      end if
C      AR=ARSIDE(X,Y,aloss,ilossi)
C      ara(ilossd) = ar
C      alossa(ilossd) = aloss
10     continue
C
C      write ( 6,16) th, x, y, tr, ara, alossa
16     format(f6.2,1x,2f6.2,2x,pe13.3,2x,2e13.3,2x,2e13.3)
C      if ( th .gt. th2) go to 20
C      th = th+dth
C      go to 1
20     CONTINUE
C      PUT IT ALL TOGETHER
C      call exit

```

CPRESP

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OF POOR QUALITY

```
c      CPRESP=ZCU*VZ*TR*(AR - alossd)
cC     CHANGE SIGN OF CURRENT IN ELECTRON MODE, TO KEEP OUTPUT SIGNAL POSIT
cC                                         IVE
c      IF(III.EQ.5)CPRESP=-CPRESP
c      RETURN
c99    CPRESP=0.
c      RETURN
c      END
```

ANGLE FROM D-UP NORMAL	NO. OF POINTS		TRANSPARENCY	OVERLAP AREA		EFF. LOSS AREA ISOTROPIC SECONDARIES	EFF. LOSS AREA COSINE DISTRIBUTION
	DAS	DSC					
40.00	3.87	1.22	0.639e+00	0.497e+02	0.497e+02	0.925e+01	0.497e+01
40.50	3.94	1.24	0.638e+00	0.490e+02	0.490e+02	0.915e+01	0.495e+01
41.00	4.01	1.26	0.637e+00	0.483e+02	0.483e+02	0.906e+01	0.493e+01
41.50	4.08	1.28	0.636e+00	0.475e+02	0.475e+02	0.896e+01	0.490e+01
42.00	4.15	1.31	0.634e+00	0.468e+02	0.468e+02	0.886e+01	0.488e+01
42.50	4.22	1.33	0.633e+00	0.460e+02	0.460e+02	0.876e+01	0.486e+01
43.00	4.30	1.35	0.631e+00	0.452e+02	0.452e+02	0.865e+01	0.484e+01
43.50	4.37	1.38	0.630e+00	0.444e+02	0.444e+02	0.855e+01	0.481e+01
44.00	4.45	1.40	0.628e+00	0.436e+02	0.436e+02	0.844e+01	0.479e+01
44.50	4.53	1.43	0.627e+00	0.428e+02	0.428e+02	0.833e+01	0.476e+01
45.00	4.61	1.45	0.625e+00	0.419e+02	0.419e+02	0.820e+01	0.471e+01
45.50	4.69	1.48	0.623e+00	0.410e+02	0.410e+02	0.805e+01	0.465e+01
46.00	4.77	1.50	0.622e+00	0.400e+02	0.400e+02	0.789e+01	0.459e+01
46.50	4.86	1.53	0.620e+00	0.389e+02	0.389e+02	0.773e+01	0.452e+01
47.00	4.94	1.56	0.618e+00	0.379e+02	0.379e+02	0.756e+01	0.445e+01
47.50	5.03	1.58	0.616e+00	0.369e+02	0.369e+02	0.740e+01	0.438e+01
48.00	5.12	1.61	0.615e+00	0.358e+02	0.358e+02	0.723e+01	0.431e+01
48.50	5.21	1.64	0.613e+00	0.348e+02	0.348e+02	0.705e+01	0.423e+01
49.00	5.30	1.67	0.611e+00	0.337e+02	0.337e+02	0.687e+01	0.416e+01
49.50	5.39	1.70	0.609e+00	0.326e+02	0.326e+02	0.669e+01	0.408e+01
50.00	5.49	1.73	0.607e+00	0.314e+02	0.314e+02	0.650e+01	0.399e+01
50.50	5.59	1.76	0.604e+00	0.303e+02	0.303e+02	0.631e+01	0.390e+01
51.00	5.69	1.79	0.602e+00	0.291e+02	0.291e+02	0.612e+01	0.381e+01
51.50	5.79	1.82	0.600e+00	0.280e+02	0.280e+02	0.591e+01	0.372e+01
52.00	5.90	1.86	0.598e+00	0.268e+02	0.268e+02	0.570e+01	0.362e+01
52.50	6.00	1.89	0.595e+00	0.256e+02	0.256e+02	0.549e+01	0.351e+01
53.00	6.11	1.92	0.593e+00	0.243e+02	0.243e+02	0.527e+01	0.340e+01
53.50	6.23	1.96	0.590e+00	0.230e+02	0.230e+02	0.503e+01	0.327e+01
54.00	6.34	2.00	0.588e+00	0.217e+02	0.217e+02	0.478e+01	0.314e+01
54.50	6.46	2.03	0.585e+00	0.204e+02	0.204e+02	0.454e+01	0.301e+01
55.00	6.58	2.07	0.582e+00	0.191e+02	0.191e+02	0.428e+01	0.287e+01
55.50	6.70	2.11	0.580e+00	0.177e+02	0.177e+02	0.402e+01	0.272e+01
56.00	6.83	2.15	0.577e+00	0.164e+02	0.164e+02	0.376e+01	0.257e+01
56.50	6.96	2.19	0.574e+00	0.151e+02	0.151e+02	0.350e+01	0.242e+01
57.00	7.10	2.23	0.571e+00	0.137e+02	0.137e+02	0.322e+01	0.226e+01
57.50	7.23	2.28	0.567e+00	0.124e+02	0.124e+02	0.295e+01	0.209e+01
58.00	7.37	2.32	0.564e+00	0.111e+02	0.111e+02	0.267e+01	0.192e+01
58.50	7.52	2.37	0.561e+00	0.973e+01	0.973e+01	0.238e+01	0.174e+01
59.00	7.67	2.41	0.557e+00	0.842e+01	0.842e+01	0.209e+01	0.155e+01
59.50	7.82	2.46	0.554e+00	0.718e+01	0.718e+01	0.181e+01	0.136e+01
60.00	7.98	2.51	0.550e+00	0.594e+01	0.594e+01	0.152e+01	0.116e+01
60.50	8.14	2.56	0.546e+00	0.475e+01	0.475e+01	0.124e+01	0.964e+00
61.00	8.31	2.62	0.542e+00	0.365e+01	0.365e+01	0.964e+00	0.762e+00
61.50	8.49	2.67	0.538e+00	0.255e+01	0.255e+01	0.689e+00	0.556e+00
62.00	8.67	2.73	0.534e+00	0.164e+01	0.164e+01	0.450e+00	0.368e+00
62.50	8.85	2.79	0.530e+00	0.828e+00	0.828e+00	0.230e+00	0.191e+00
63.00	9.04	2.85	0.525e+00	0.215e+00	0.215e+00	0.614e-01	0.525e-01
63.50	9.24	2.91	0.521e+00	0.679e-01	0.679e-01	0.197e-01	0.170e-01
64.00	9.45	2.97	0.516e+00	0.000e+00	0.000e+00	0.000e+00	0.000e+00
64.50	9.66	3.04	0.511e+00	0.000e+00	0.000e+00	0.000e+00	0.000e+00
65.00	9.88	3.11	0.506e+00	0.000e+00	0.000e+00	0.000e+00	0.000e+00
65.50	10.11	3.18	0.501e+00	0.000e+00	0.000e+00	0.000e+00	0.000e+00
66.00	10.35	3.26	0.495e+00	0.000e+00	0.000e+00	0.000e+00	0.000e+00
66.50	10.60	3.34	0.490e+00	0.000e+00	0.000e+00	0.000e+00	0.000e+00
67.00	10.85	3.42	0.484e+00	0.000e+00	0.000e+00	0.000e+00	0.000e+00
67.50	11.12	3.50	0.478e+00	0.000e+00	0.000e+00	0.000e+00	0.000e+00
68.00	11.40	3.59	0.471e+00	0.000e+00	0.000e+00	0.000e+00	0.000e+00
68.50	11.70	3.68	0.465e+00	0.000e+00	0.000e+00	0.000e+00	0.000e+00
69.00	12.00	3.78	0.458e+00	0.000e+00	0.000e+00	0.000e+00	0.000e+00
69.50	12.32	3.88	0.451e+00	0.000e+00	0.000e+00	0.000e+00	0.000e+00
70.00	12.66	3.98	0.444e+00	0.000e+00	0.000e+00	0.000e+00	0.000e+00
70.50	13.01	4.10	0.436e+00	0.000e+00	0.000e+00	0.000e+00	0.000e+00
71.00	13.38	4.21	0.428e+00	0.000e+00	0.000e+00	0.000e+00	0.000e+00
71.50	13.77	4.33	0.420e+00	0.000e+00	0.000e+00	0.000e+00	0.000e+00
72.00	14.18	4.46	0.412e+00	0.000e+00	0.000e+00	0.000e+00	0.000e+00
72.50	14.61	4.60	0.403e+00	0.000e+00	0.000e+00	0.000e+00	0.000e+00
73.00	15.07	4.74	0.393e+00	0.000e+00	0.000e+00	0.000e+00	0.000e+00
73.50	15.55	4.90	0.384e+00	0.000e+00	0.000e+00	0.000e+00	0.000e+00
74.00	16.07	5.06	0.374e+00	0.000e+00	0.000e+00	0.000e+00	0.000e+00
74.50	16.61	5.23	0.363e+00	0.000e+00	0.000e+00	0.000e+00	0.000e+00
75.00	17.20	5.41	0.352e+00	0.000e+00	0.000e+00	0.000e+00	0.000e+00
75.50	17.82	5.61	0.341e+00	0.000e+00	0.000e+00	0.000e+00	0.000e+00
76.00	18.48	5.82	0.329e+00	0.000e+00	0.000e+00	0.000e+00	0.000e+00
76.50	19.19	6.04	0.317e+00	0.000e+00	0.000e+00	0.000e+00	0.000e+00
77.00	19.96	6.28	0.304e+00	0.000e+00	0.000e+00	0.000e+00	0.000e+00
77.50	20.78	6.54	0.291e+00	0.000e+00	0.000e+00	0.000e+00	0.000e+00
78.00	21.68	6.82	0.277e+00	0.000e+00	0.000e+00	0.000e+00	0.000e+00
78.50	22.65	7.13	0.263e+00	0.000e+00	0.000e+00	0.000e+00	0.000e+00
79.00	23.70	7.46	0.248e+00	0.000e+00	0.000e+00	0.000e+00	0.000e+00
79.50	24.86	7.83	0.232e+00	0.000e+00	0.000e+00	0.000e+00	0.000e+00
80.00	26.13	8.23	0.216e+00	0.000e+00	0.000e+00	0.000e+00	0.000e+00
80.50	27.53	8.67	0.199e+00	0.000e+00	0.000e+00	0.000e+00	0.000e+00

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APPENDIX F

FRINGE FIELD CALCULATIONS NEAR
NEGATIVE MODULATOR GRID SUPPORT

From: G. S. Gordon Jr.

Date: January 6, 1988

The directory /usr4/r1m/fringe contains the programs for computing the fringing field in the region near the negative modulator grid for the side sensor; some more generally usefull programs are also included. All of the programs are compiled and linked using make and are run by direct invocation. The user must set up any environmental variables by hand, although some sample files (e.g., setft[123]) exist which can be run with the source command.

The most important programs are:

elec

ELEC calls initvolt to read in the potential field from unit ft10. From specified initial conditions (stdin), ELEC then integrates an electron trajectory through the electric field to the plane containing the shield ring and supressor grid (the assumed potential there is zero as in the reversed supressor configuration). If ft11 is defined, the trajectory is written out on ft11 in a format suitable for mongo. Note that the voltage is normally negative and the the external units are in inches while the internal dimensions are in meters. Note that TRAJ is a logical part of ELEC, and that the PARAMETERS must match. VOLTAGE computes the E field from the read in potential field. It should be noted the the field at the very edge is not correct as the first equipotential contour does not lie exactly on the metal conductor, i.e., at the exact boundary.

pltxy

PLTXY plots out the potential contours, E field lines, or the inverse of the conformal map(real,imaginary), depending upon the type of plot specified: 1, 2, 3, 4. PLTXY does its plotting with mongo coutours, and it will plot to several devices, s=sun, t=tek, l=landscape laser, p=portrait laser, with different contour integrval which are documented (some what) in the program.

wfromz

WFROMZ inverts the function ZFUNC using a variation on Newton Rapson method. ZFUNC is $z(w)$ which is the solution of

$$\frac{dz}{dw} = \frac{k \sqrt{w-1}}{\pi w \sqrt{w-c}} \quad (1)$$

with $k \equiv hc^{-1/2}$ and $c > 1, k > 0$. The solution is given by

$$z(w) = \frac{k}{\pi} \left[\cosh^{-1} \left(\frac{2w-c-1}{c-1} \right) - \frac{1}{\sqrt{c}} \cosh^{-1} \left(\frac{[c+1]w-2c}{[c-1]w} \right) \right] \quad (2)$$

In this problem $k = 0.452$ inches, $h = 0.312$ inches, and $c = 2.0988$. This solution is given on p.161 of H. Korber [*Dictionary of Conformal Representations*, Dover Publications, Inc., 1957] and in problem 10.21 on p.1315 of Morse and Feshbach [*Methods of Theoretical Physics*, Mc Graw-Hill Book Co., Inc., New York, 1953]. The inversion method tries using both the numerical and analytic derivatives to find the solution and accepts the closer iteration; however, if both iterations are farther from the solution than the initial guess, the method checks in the immediate vicinity of the initial guess for a better solution. WFROMZ also changes the size of the interval both for computing the derivative and for what it considers the immediate vicinity. It returns when either the max iterations have been run or the

required accuracy achieved (defined as moving less than derr on the last iteration or if the number of iterations is more than jmax/2 being within a specified error of z); both W and Z of the final point are returned.

acosh

ACOSH compute the inverse sin, cos, sinh, cosh for complex*16 arguments. It should be noted that the cutlines used may not be what are expected as they were made for this problem.

cone.f

CONE computes and stores the potential field as is used by ELEC.

con[f12]?

These programs are closely related to one another. They all compute the conformal maps much as CONE does, only where cone and conf compute the inverse map, con and con1 compute the forward map; con1 and con2 plot out the contours.

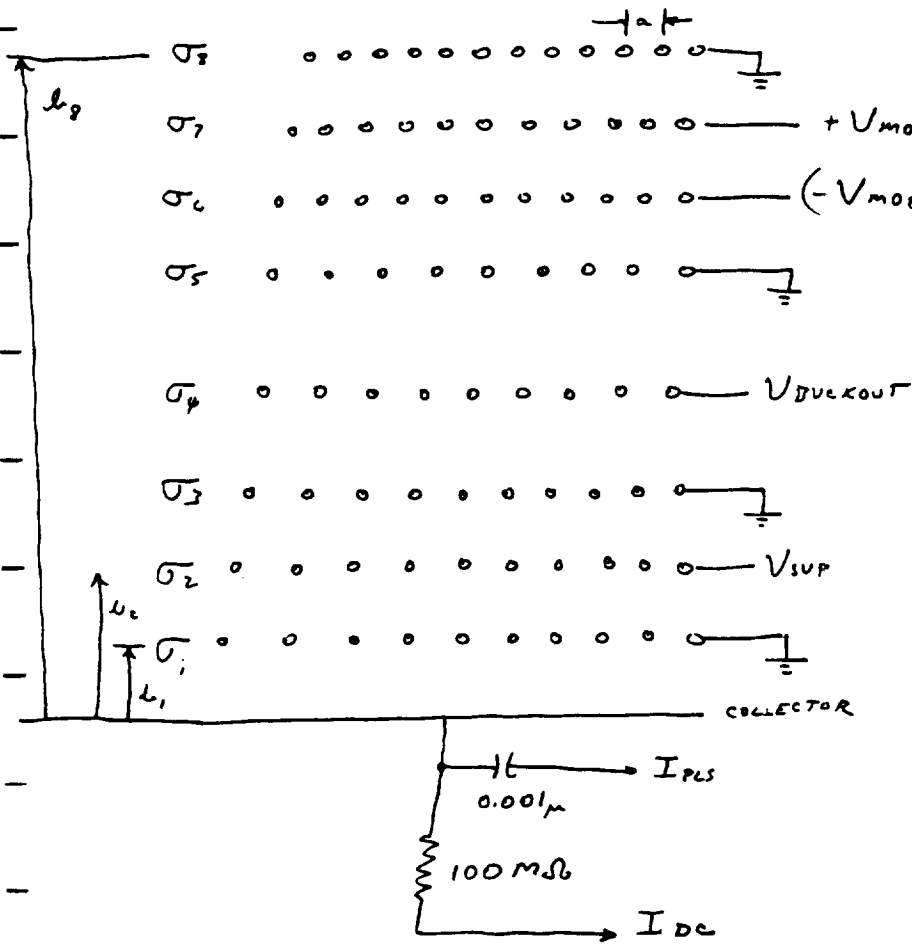
APPENDIX G

11/17/87



Modulator grid pickup (RTM)

D-caps



$\sigma_i = \text{charge per unit area on grid } i$
 $\rho = \text{grid wire radius}$

$l_i = \text{distance from collector to grid } i$

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Including the eight grids and their images, the electrostatic potential (in cgs units) is given by (see House and Freedback):

$$\psi = a \sum_{i=1}^8 \sigma_i \ln \left\{ \frac{\sin^2 \frac{\pi x}{a} + \sin^2 \left[\frac{\pi}{a} (y + b_i) \right]}{\sin^2 \frac{\pi x}{a} + \sin^2 \left[\frac{\pi}{a} (y - b_i) \right]} \right\}$$

Enforce the ordering $\rho \ll a \ll b_i \forall i$ to obtain

$$\begin{aligned} V_n &= 4\pi \sum_{i=1}^8 \sigma_i b_i + 2a \sigma_n \ln \left(\frac{a}{2\pi\rho} \right) \\ &= 4\pi \left[\sum_{i=1}^8 \sigma_i b_i + \sigma_n \left(\frac{a}{2\pi} \ln \frac{a}{2\pi\rho} \right) \right] \end{aligned}$$

where V_n is the potential of the n th grid.

In the same limit, the total charge on the collector plate is given by

$$\sigma_c = - \frac{1}{4\pi} \left. \frac{\partial \psi}{\partial y} \right|_{y=0} \approx - \sum_{i=1}^8 \sigma_i \quad (\text{where the } x \text{ dependence is suppressed}).$$

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Suppose we restrict ourselves to only the oscillatory part of the T_i 's (due to the oscillatory part of the V_i 's). Then we obtain the set of equations

$$\frac{1}{4\pi} \begin{pmatrix} 0 \\ 0 \\ 0 \\ \Delta V_{\text{DUCROUOT}} \\ 0 \\ 0 \\ \Delta V_{\text{MOD}} \\ 0 \end{pmatrix} = \begin{pmatrix} b_1 + \epsilon & b_1 & b_1 & \dots & b_1 \\ b_1 & b_2 + \epsilon & b_2 & \dots & b_2 \\ b_1 & b_2 & b_3 + \epsilon & \dots & b_3 \\ b_1 & b_2 & b_3 & \dots & b_4 \\ b_1 & b_2 & b_3 & \dots & b_5 \\ b_1 & b_2 & b_3 & \dots & b_6 \\ b_1 & b_2 & b_3 & \dots & b_7 \\ b_1 & b_2 & b_3 & \dots & b_8 + \epsilon \end{pmatrix} \begin{pmatrix} \sigma_1 \\ \sigma_2 \\ \sigma_3 \\ \sigma_4 \\ \sigma_5 \\ \sigma_6 \\ \sigma_7 \\ \sigma_8 \end{pmatrix}$$

↑
Oscillatory part

Define $a_{j+1} \equiv \frac{\epsilon a_j}{\epsilon + a_j} + b_{j+2} - b_{j+1}$
 $a_0 = b_1$

so in the limit of small ϵ , $a_j \rightarrow b_{j+1} - b_j$ which is just the intergrid spacing.

$$\epsilon \equiv \frac{a}{2\pi} \ln \frac{a}{2\pi\rho}$$

$$\approx 0.0299 \text{ cm}$$

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By manipulating the equations into a triangular form and using backsubstitution, we obtain (after simplified algebra):

$$\sum_{i=1}^8 \sigma_i = \left(\prod_{j=0}^5 \frac{\epsilon}{\epsilon + a_j} \right) \frac{1}{\epsilon + a_6} \left(1 - \frac{\epsilon}{\epsilon + a_7} \frac{a_6}{\epsilon + a_6} \right) \frac{\Delta V_{\text{MOD}}}{4\pi}$$

$$+ \left(\prod_{j=0}^2 \frac{\epsilon}{\epsilon + a_j} \right) \frac{1}{\epsilon + a_3} \left(-\frac{1}{\epsilon + a_6} \frac{a_3}{\epsilon + a_3} \left[\frac{\epsilon}{\epsilon + a_4} \right]^2 \left[\frac{\epsilon}{\epsilon + a_5} \right]^2 \right.$$

$$\times \left[1 + \frac{\epsilon}{\epsilon + a_6} \frac{\epsilon}{\epsilon + a_7} \right] + \left[1 + \frac{\epsilon}{\epsilon + a_4} \frac{a_3}{\epsilon + a_3} \right] \left. - 1 + \frac{\epsilon}{\epsilon + a_4} \frac{\epsilon}{\epsilon + a_5} \right)$$

$$\times \frac{\Delta V_{\text{BUCKOUT}}}{4\pi}$$

If we let $\epsilon \rightarrow 0$ and only keep the lowest order, non-vanishing terms, we obtain

$$\sum_{i=1}^8 \sigma_i \approx \frac{1}{a_0 a_1 a_2 a_3} \left[\frac{\Delta V_{\text{BUCKOUT}}}{4\pi} + \frac{\epsilon^3}{a_4 a_5 a_6} \frac{\Delta V_{\text{MOD}}}{4\pi} \right]$$

with the a 's equal to the intergral spacing.

For the side sensor

$$\epsilon = 0.0299 \text{ cm}$$

$$\frac{\epsilon^3}{a_0 a_1 a_2 a_3} = 3.8829 \times 10^{-4} \text{ cm}^{-1}$$

$$\frac{\epsilon^3}{a_4 a_5 a_6} = 4.8604 \times 10^{-5}$$

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⑤

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In the L-mode for channel 16 $\Delta V_{\text{mod}} = \frac{1500}{300}$
 $= 5$ statvolt peak-to-peak

$$\frac{\epsilon^3}{2.4 \times 10^6} (1500) = 0.0729 \text{ volts to compensate}$$

$$\text{at this level } i_c = \frac{d\sigma_c}{dt} A$$
$$= 2\pi \nu A \sigma_c$$

$$A = 126.68 \text{ cm}^2$$

$$\nu = 800 \pi \text{ s}^{-1}$$

$$\rightarrow i_c = 7.963 \times 10^{-13} \text{ ampere}$$

If the shielding of each grid is increased by a factor of 2
due to the 2D mesh

$$i_c = 1.24 \times 10^{-14} \text{ ampere} \text{ - below the thermal noise level } (\sim 5 \times 10^{-14} \text{ ampere})$$

[Exact solution of the equations give results within $\sim 60\%$ of these approximate results]

For the main sensor, a rough calculation gives ~ 4.6 volts at the
back out grid (1500 volt p-p on the modulator grid); hence, 5 volt p-p
back out voltage (out of phase) gives a fair noise for the compensated
pick up (at the level of approximations used).

