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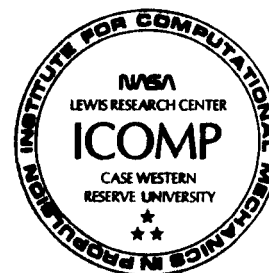
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A NEAR-WALL TURBULENCE MODEL AND ITS APPLICATION TO
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Summary

A near-wall turbulence model and its incorporation into a multiple-time-scale turbulence model are presented in this report. In the method, the conservation of mass, momentum, and the turbulent kinetic energy equations are integrated up to the wall; and the energy transfer rate and the dissipation rate inside the near-wall layer are obtained from algebraic equations. The algebraic equations for the energy transfer rate and the dissipation rate inside the near-wall layer have been obtained from a k-equation turbulence model and the near wall analysis. A fully developed turbulent channel flow and fully developed turbulent pipe flows were solved using a finite element method to test the predictive capability of the turbulence model. The computational results compared favorably with experimental data. It is also shown that the present turbulence model could resolve the over-shoot phenomena of the turbulent kinetic energy and the dissipation rate in the region very close to the wall.

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Nomenclature

$c_{p\ell}$	Turbulence model constants for ϵ_p equation, ($\ell=1,3$)
$c_{t\ell}$	Turbulence model constants for ϵ_t equation, ($\ell=1,3$)
$c_{\mu f}$	A constant coefficient ($=0.09$)
c_{μ}	A coefficient used in eddy viscosity equation
f_{μ}	Wall damping function for eddy viscosity equation
f_{ϵ}	Wall damping function for dissipation rate
k	Total turbulent kinetic energy, ($k=k_p+k_t$)
k_p	Turbulent kinetic energy of eddies in the production range
k_t	Turbulent kinetic energy of eddies in the dissipation range
k^+	Normalized turbulent kinetic energy ($=k/u_{\tau}^2$)
Pr	Production rate of turbulent kinetic energy
R_t	Turbulent Reynolds number ($=k^2/(\nu\epsilon)$)
r	Radial distance
u	Time averaged velocity
u^+	Non-dimensional velocity ($=u/u_{\tau}$)
u_{τ}	Friction velocity ($=\sqrt{(\tau_w/\rho)}$)
$\overline{u'^2}$	Normal Reynolds stress, R.M.S. value of the fluctuating axial velocity
$\overline{u'v'}$	Reynolds stress
$\overline{u'v'}^+$	Normalized Reynolds stress ($=\overline{u'v'}/u_{\tau}^2$)
v	Time averaged velocity in the y-coordinate direction
v_s	turbulence velocity scale
y	normal distance from the wall
y^+	Wall coordinate ($=u_{\tau}y/\nu$)
ϵ	Dissipation rate
ϵ_p	Transfer rate of turbulent kinetic energy from the production range to the dissipation range

ϵ_t	Dissipation rate of turbulent kinetic energy
ϵ_w	Dissipation rate inside the near-wall layer
ϵ^+	Non-dimensional dissipation rate ($=\nu\epsilon/u_\tau^4$)
κ	von Karman constant
l	turbulence length scale
l_m	mixing length
ν	kinematic viscosity of fluid
ν_t	turbulent eddy viscosity
σ_{kp}	Turbulent Prandtl number for k_p equation
σ_{kt}	Turbulent Prandtl number for k_t equations
$\sigma_{\epsilon p}$	Turbulent Prandtl number for ϵ_p equation
$\sigma_{\epsilon t}$	Turbulent Prandtl number for ϵ_t equation
τ_w	Wall shearing stress

Introduction

For wall bounded turbulent flows in the equilibrium state, the logarithmic velocity profile prevails in the near-wall region¹. The most widely used wall function methods in numerical calculations of turbulent flows have been derived from the logarithmic velocity profile based on the experimental observation that the turbulence in the near-wall region can be described in terms of the wall shearing stress. The wall function methods are not valid at or near the separation point since the turbulence in this region can not be described in terms of the wall shearing stress. For unsteady turbulent flows, the logarithmic velocity profile no longer prevails in the near-wall or in the wake region², therefore the wall function methods can not be applied. Other occasions in which the wall function methods become invalid include low turbulent Reynolds number flows in which the effect of molecular viscosity become important and flows over surfaces with mass injection and/or suction. The objective of this study is to establish a near-wall turbulence model which can be used in place of wall function methods. Further application of the present near-wall turbulence model for complex turbulent flows such as the turbulent flow over a curved hill³ and the turbulent boundary layer - shock wave interactions⁴⁻⁵ can be found in Reference 6.

Numerous efforts have been made to include the near-wall low turbulent Reynolds number region in turbulent flow computations. Various turbulence models which include the near-wall low turbulence region can be classified as two- or multi-layer turbulence models⁷⁻¹⁰, low Reynolds number turbulence models, and partially low Reynolds number turbulence models. The advantages and disadvantages of these various methods are discussed in the following.

In the two- or multi-layer turbulence models, the turbulence in the near-wall layer has been described by algebraic expressions⁷⁻¹⁰. In these turbulence models, the turbulent kinetic energy and the dissipation rate in the near-wall layer have been constructed by piecewise continuous functions. As a consequence, the computational results may depend on the location of the partition between the near-wall layer and the fully turbulent region⁸. In some of these methods, a quadratic variation of the turbulent kinetic energy has been assumed in the near-wall region and the dissipation rate has been derived from the logarithmic velocity profile equation⁴. This class of methods is advantageous in studying the near-wall turbulence structure for equilibrium turbulent flows. However, these methods become invalid if the logarithmic velocity profile does not prevail in the near wall region. The underlying assumption that the turbulent kinetic energy is proportional to square of the distance from the wall inside the near-wall layer is also questionable, since the quadratic variation of the turbulent kinetic energy is valid only inside the viscous sublayer and become invalid as the fully turbulent region is approached.

In the low Reynolds number turbulence models, the high Reynolds number turbulence models have been extended to include the near-wall low turbulence effect¹¹. In this class of methods, the near-wall low turbulence effects have been incorporated into the high Reynolds number turbulence models by using the wall damping functions. These wall damping functions have been derived mostly from numerical experiments in such a way that the low Reynolds number turbulence models could reproduce the experimentally observed turbulent flow phenomena in the near-wall region. In this class of methods, a significant number of grid points has to be assigned in the near wall region in order to resolve the stiff dissipation rate equation.

Aside from the above two classes of methods, a new approach has been used in Chen and Patel¹² to solve complex turbulent flow. In the method, only the turbulent kinetic energy equation of the $k-\epsilon$ turbulence model has been extended to include the near-wall low turbulence effect and the dissipation rate inside the near-wall layer has been prescribed algebraically. The dissipation rate equation has been obtained from a k -equation turbulence model¹³. Thus the turbulent kinetic energy and the dissipation rate varies smoothly from the wall toward the outside fully turbulent region. In this case, it would be more appropriate to classify the turbulence model as a partially low Reynolds number turbulence model to distinguish it from the other two classes of methods.

It has been shown previously that the high Reynolds number multiple-time-scale turbulence model¹⁶ yielded significantly improved computational results for a class of complex turbulent flows such as a wall jet flow¹⁷, a wake-boundary layer interaction flow¹⁸, a confined coaxial jet without swirl¹⁹, and a confined coaxial swirling jet²⁰, to name a few. In the single-time-scale turbulence models such as the $k-\epsilon$ turbulence models and the Reynolds stress turbulence models, a single-time-scale is used to express both the turbulent transport and the dissipation of the turbulent kinetic energy. However, this practice is inconsistent with physically observed turbulence in a sense that the turbulent transport is related to the time scale of energy containing large eddies and the dissipation rate of turbulent kinetic energy is related to the time scale of fine scale eddies in the dissipation range. The single time-scale turbulence models have been used most widely and yielded quite accurate computational results for many turbulent flows; however, the predictive capability degenerated significantly for complex turbulent flows with

strong inequilibrium turbulence. In the multiple-time-scale turbulence models^{16,21-24}, the turbulent transport of mass and momentum has been described using the time scale of the large eddies; and the dissipation rate has been described using the time scale of the fine scale eddies. The improved computational results obtained by using the multiple-time-scale turbulence model for complex turbulent flows can be attributed to the above discussed physically consistent nature of the turbulence models.

It has been shown that the k-equation turbulence models yielded highly accurate computational results for a class of standard turbulent boundary layer flows²⁵, turbulent flows with drag reduction²⁶, an unsteady fully developed turbulent channel flow²⁷, and fully developed unsteady turbulent pipe flows². However, the k-equation turbulence model itself is less useful for separated and/or swirling turbulent flows with complex geometry due to lack of a systematic method to evaluate the turbulence length scale.

The near-wall turbulence model presented in this report belongs to the partially low Reynolds number turbulence models. In the model, the turbulence structure in the near-wall low turbulence region has been solved by extending the turbulent kinetic energy equations to include the low turbulence effect and the energy transfer rate and the dissipation rate have been prescribed algebraically. The energy transfer rate and the dissipation rate equations in the near-wall layer have been obtained from the k-equation turbulence model¹³. The rest of the flow domain has been solved by the high Reynolds number multiple-time-scale turbulence model¹⁶. Further advantages of this approach originating from physical and numerical considerations are discussed in the following section.

Example problems considered include: a fully developed turbulent channel flow¹⁴ at Reynolds number (Re) of 30,800 and turbulent pipe flows¹⁵

for $Re = 50,000$ and $500,000$. The computational results compared favorably with experimental data globally. More importantly, significantly improved computational results for the turbulence structure in the near-wall region, including the experimentally observed over-shoot phenomena of the turbulent kinetic energy and the dissipation rate, have been obtained.

NEAR-WALL TURBULENCE MODEL

The turbulence in external flows and that in near-wall boundary layer flows have quite different length scales^{28,29}. The turbulence length scale of the external flows is related to the flow field characteristics. On the other hand, the turbulence length scale of boundary layer flows is strongly related to the normal distance from the wall. This nature of the wall bounded turbulent flows can be described quite naturally by the partially low Reynolds number turbulence models. The same purpose could be achieved by the low Reynolds number turbulence models as more experimental data become available. However, the gradient of the dissipation rate is the most stiff in the near-wall region, and a great number of grid points has to be used in the region for the low Reynolds number turbulence models to resolve the dissipation rate. Therefore, the partially low Reynolds number turbulence models seem to be more advantageous as compared with the low Reynolds number turbulence models, unless the low Reynolds number turbulence models can describe the wall bounded turbulent flows more accurately.

Eddy Viscosity Equation in the Near-Wall Region

In the Prandtl-Kolmogorov theory, the eddy viscosity is given as;

$$\nu_t = \nu_s \ell \quad (1)$$

where v_s and l are the turbulence velocity and length scales, respectively. The velocity scale has been most frequently represented by the square root of the turbulent kinetic energy. The turbulent length scale in the fully turbulent region of wall bounded turbulent flows is given as^{11,25};

$$l = c_{\mu f}^{1/4} l_m \quad (2)$$

$$l_m = \kappa y \quad (3)$$

where $c_{\mu f}$ (=0.09) is a constant, l_m is the mixing length, κ is the von Karman constant, and y is the normal distance from the wall. The fully turbulent region extends from $y^+ \approx 30$ up to $y^+ \approx 300$, where $y^+ = u_\tau y / \nu$ is the wall coordinate, $u_\tau = \sqrt{(\tau_w / \rho)}$ is the friction velocity, τ_w is the wall shearing stress, and ν is the kinematic viscosity of fluid. Thus the turbulent eddy viscosity in this fully turbulent region is given as;

$$\nu_t = k^{1/2} l \quad (4)$$

where k is the turbulent kinetic energy.

The instantaneous velocity in the viscous sublayer region can be written as¹¹;

$$\left. \begin{aligned} u' &= a_1 y + a_2 y^2 + \dots \\ v' &= b_2 y^2 + \dots \\ w' &= c_1 y + c_2 y^2 + \dots \end{aligned} \right\} \quad (5)$$

where the coefficients a_i , b_i , and c_i are functions of time such that $a_i =$

$b_i = c_i = 0$, and the over-bar denotes time average. Note that the fluctuating normal velocity component grows in proportion to the square of the distance from the wall due to the wall proximity effect. The turbulence in the very closed to the wall region, i.e., $y \approx 0$ can be written as;

$$k = \frac{1}{2} (\overline{u'^2} + \overline{v'^2} + \overline{w'^2}) = \frac{1}{2} (a_1^2 + c_1^2) y^2 + \dots \quad (6)$$

$$\epsilon = \nu \frac{\partial u_j}{\partial x_i} \frac{\partial u_j}{\partial x_i} = \frac{2\nu k}{y^2} \quad (7)$$

$$\overline{u'v'} = a_1 b_2 y^3 \quad (8)$$

where ϵ is the dissipation rate, and $\overline{u'v'}$ is a component of the Reynolds stress. Due to the difficulty in measuring the turbulence quantity in the very close to the wall region, there exist only a limited number of experimental data to support the above analysis. For example, the experimental data compiled by Cole³⁰ showed that the turbulent kinetic energy grows in proportion to the square of the distance from the wall.

In the Boussinesq eddy viscosity assumption, the Reynolds stress is given as;

$$-\overline{u_i' u_j'} = \nu_t \left(\frac{\partial u_i}{\partial x_j} + \frac{\partial u_j}{\partial x_i} \right) \quad (9)$$

Very close to the wall, the velocity gradient is a constant. Thus eqs. (8) and (9) indicate that the eddy viscosity is in proportion to the third power of the distance from the wall; whereas, eqs. (2-4) and (6) indicate

that the eddy viscosity is proportional to the square of the distance from the wall in the viscous sublayer region. This difference is attributed to the fact that the molecular viscosity dominates in the viscous sublayer region and that the eddy viscosity dominates in the fully turbulent region. The turbulent viscosity equation can be modified to include the effect of molecular viscosity in the viscous sublayer region as follows⁸⁻¹²;

$$\nu_t = f_\mu k^{1/2} \ell \quad (10)$$

Thus the damping function f_μ has to be a linear function of the distance from the wall and has to approach unity as the fully turbulent region is approached.

Note that the eddy viscosity in the Prandtl mixing length theory is proportional to the fourth power of the distance from the wall, i.e.;

$$\nu_t = \ell_m^2 \left| \frac{\partial u}{\partial y} \right| \quad (11)$$

where $\ell_m = \kappa y (1 - \exp(-y^+/A^+))$ and A^+ is the wall damping factor. There also exists a few low Reynolds number turbulence models in which the eddy viscosity varies in proportion to the fourth power of the distance from the wall, see Reference 11 for more discussion.

In the fully turbulent region of wall bounded turbulent flows, the dissipation rate is related to the mixing length or the turbulence length scale as;

$$\epsilon = c_\mu f^{3/4} \frac{k^{3/2}}{\ell_m}$$

$$= c_{\mu} f \frac{k^{3/2}}{l} \quad (12)$$

The dissipation rate given as eq. (12) vanishes in the region very close to the wall. However, the experimentally observed dissipation rate approaches a constant value in the region, see eq. (7). Two slightly different approaches have been used to approximate the dissipation rate in the near-wall region. In the k-equation turbulence model of Gibson et. al.²⁵, Hassid and Poreh²⁶, and Acharya and Reynolds²⁷, the dissipation rate in the near-wall layer has been obtained by linear combination of eqs. (7) and (12), and is given as;

$$\epsilon_w = c_{\mu} f^{3/4} f_{\epsilon h} \frac{k^{3/2}}{\kappa y} + \frac{2\nu k}{y^2} \quad (13)$$

where $f_{\epsilon h}$ is a wall damping function varying from null on the wall to unit in the fully turbulent region. On the other hand, in the k-equation turbulence model of Wolfshtein¹³, the dissipation rate in the near-wall layer was given as;

$$\epsilon_w = \frac{1}{f_{\epsilon}} \frac{c_{\mu} f^{3/4} k^{3/2}}{\kappa y} \quad (14)$$

where f_{ϵ} has been chosen so that the dissipation rate would approach to the value given in eq. (7) for $y \approx 0$ and f_{ϵ} take unit value in the fully turbulent region. The fully turbulent region with equilibrium turbulence extends from $y^+ \approx 30$ to $y^+ \approx 300$ for wall bounded flows. Eq. (14) has also been used in the partially low Reynolds number k- ϵ turbulence model of Chen and

Patel¹² for numerical computations of separated turbulent flows. Eq. (14) has been used in the present study, and partial justification is presented in the following paragraph.

Consider the turbulent kinetic energy equation given as;

$$u_j \frac{\partial k}{\partial x_j} - \frac{\partial}{\partial x_j} \left(\nu + \frac{\nu_t}{\sigma_k} \right) \frac{\partial k}{\partial x_j} = Pr - \epsilon \quad (15)$$

where σ_k is the turbulent Prandtl number for the k-equation and $Pr = \overline{u_i' u_j'} (\partial u_i / \partial x_j)$ is the production rate. Very close to the wall ($y \approx 0$), the molecular viscosity dominates over the turbulent eddy viscosity, and the convection term is found to be negligible compared with the diffusion term from an order of magnitude analysis¹. Then the analytical solution of eq. (15) for $y \approx 0$ is given as eq. (7). For $y > 0$, the turbulent eddy viscosity grows in proportion to the third power of the distance from the wall. Hence it can be argued that the dissipation rate given as eq. (7), which is the analytical solution of eq. (15) for $y \approx 0$, may valid only at very close to the wall. However, the dissipation rate given as eq. (7) retains significant magnitude even in the fully turbulent region, i.e. $y^+ \approx 100$. For this reason, the work of Wolfshtein¹³ and Chen and Patel¹² has been followed herein. In the present study, the near-wall damping function for eq. (14) is given as;

$$f_\epsilon = 1 - \text{Exp}(-A_\epsilon R_\epsilon) \quad (16)$$

where $R_\epsilon = k^2 / (\nu \epsilon)$ is the turbulent Reynolds number and $A_\epsilon = c_{\mu f}^{3/2} / (2\kappa^2)$. For $y \approx 0$, eq. (14) takes the limit value given as eq. (7).

Substituting eq. (12) into eq. (10) yields:

$$\nu_t = c_{\mu} f f_{\mu} \frac{k^2}{\epsilon} \quad (17)$$

and substituting ϵ_w , eq. (14), for ϵ in eq. (17) yields the eddy viscosity equation for the near-wall layer given as;

$$\nu_t = c_{\mu} f f_{\mu} \frac{k^2}{\epsilon_w} \quad (18)$$

where $f_{\mu} = 1 - \exp(-A_1 \sqrt{R_t} - A_2 R_t^2)$ is a linear function of the distance from the wall in the viscous sublayer region and become unity in the fully turbulent region. $A_1 = 0.025$ and $A_2 = 0.00001$ have been used for the near wall layer in the present study.

For near-wall equilibrium turbulent flows, the production rate is approximately equal to dissipation rate (ϵ_t), and hence the energy transfer rate (ϵ_p) from the low wave number production range to the high wave number dissipation range has to be approximately equal to both of them. The energy transfer rate and the dissipation rate inside the near-wall layer are given as;

$$\epsilon_p = \epsilon_t = \epsilon_w = \frac{1}{f_{\epsilon}} \frac{c_{\mu} f^{3/4} k^{3/2}}{\kappa y} \quad (19)$$

Note that the production rate vanishes on the wall and grows to full strength at $y^+ \approx 15$. Hence eq. (19) may not be a good approximation for $0 < y^+ < 15$. However, use of the vanishing boundary condition for the

turbulent kinetic energy on the wall yields the growth rate of the turbulent kinetic energy and the production rate which is in good agreement with experimental data as well as theoretical analysis.

Multiple-Time-Scale Turbulence Equations

For clarity, the partially low Reynolds number multiple-time-scale turbulence equations are summarized below. The partition between the near-wall region and the fully turbulent outer region can be located between y^+ greater than 40 and less than 300 approximately. The turbulent kinetic energy equations for the entire flow domain are given as;

$$u_j \frac{\partial k_p}{\partial x_j} - \frac{\partial}{\partial x_j} \left(\left(\nu + \frac{\nu_t}{\sigma_{kp}} \right) \frac{\partial k_p}{\partial x_j} \right) = Pr - \epsilon_p \quad (20)$$

$$u_j \frac{\partial k_t}{\partial x_j} - \frac{\partial}{\partial x_j} \left(\left(\nu + \frac{\nu_t}{\sigma_{kt}} \right) \frac{\partial k_t}{\partial x_j} \right) = \epsilon_p - \epsilon_t \quad (21)$$

where u_j is the time averaged velocity in the j -th spatial coordinate direction, ν is the kinematic viscosity of the fluid, ν_t is the turbulent eddy viscosity, and $\sigma_{kp}=0.75$ and $\sigma_{kt}=0.75$ are the turbulent Prandtl numbers for the k_p and k_t equations, respectively.

The energy transfer rate and the dissipation rate in the near-wall layer are given as eq. (19). The convection-diffusion equations for the energy transfer rate and the dissipation rate in the rest of the flow domain are given as;

$$u_j \frac{\partial \epsilon_p}{\partial x_j} - \frac{\partial}{\partial x_j} \left(\left(\nu + \frac{\nu_t}{\sigma_{\epsilon_p}} \right) \frac{\partial \epsilon_p}{\partial x_j} \right) = c_{p1} \frac{Pr^2}{k_p} + c_{p2} \frac{Pr \epsilon_p}{k_p} - c_{p3} \frac{\epsilon_p^2}{k_p} \quad (22)$$

$$u_j \frac{\partial \epsilon_t}{\partial x_j} - \frac{\partial}{\partial x_j} \left(\left(\nu + \frac{\nu_t}{\sigma_{\epsilon_t}} \right) \frac{\partial \epsilon_t}{\partial x_j} \right) = c_{t1} \frac{\epsilon_p^2}{k_t} + c_{t2} \frac{\epsilon_p \epsilon_t}{k_t} - c_{t3} \frac{\epsilon_t^2}{k_t} \quad (23)$$

where $\sigma_{\epsilon_p}=1.15$ and $\sigma_{\epsilon_t}=1.15$ are the turbulent Prandtl numbers for the ϵ_p and ϵ_t equations, respectively, and $c_{p\ell}$ ($\ell=1,3$) and $c_{t\ell}$ ($\ell=1,3$) are turbulence model constants. These model constants are given as; $c_{p1}=0.21$, $c_{p2}=1.24$, $c_{p3}=1.84$, $c_{t1}=0.29$, $c_{t2}=1.28$, and $c_{t3}=1.66$. Detailed derivation of these model constants can be found in Reference 16.

The eddy viscosity equation in the near-wall region is given as eq. (13); and the eddy viscosity in the rest of the flow domain is given as;

$$\nu_t = c_{\mu f} \frac{k^2}{\epsilon_p} \quad (24)$$

COMPUTATIONAL RESULTS

The turbulent boundary layer flows were solved by a finite element method³¹. It has been shown in Reference 31 that the finite element method could solve a wide range of laminar boundary layer flows, such as the Blasius flat plate flow, the retarded Howarth flow, flow over a wedge, plane stagnation flow, flow over a circular cylinder, flow in the wake of a flat plate, uniform suction flow over a flat plate, flow over a cone, and flow over a sphere, as accurately as any available numerical methods including the semi-analytical methods (i.e., a fourth-order Runge-Kutta method¹). Convergence study of the finite element method can be found in reference 31, and implementation of the method for turbulent flows can be

found in Reference 32. For completeness, the computational procedure relevant to the present study is described briefly below.

In each iteration, the momentum equation and the turbulence equations were solved sequentially with under-relaxation. The systems of equations have been solved iteratively until the maximum relative error of each turbulent flow variable became less than the specified convergence criterion for each flow variable. Each system of equations was solved by a penta-diagonal matrix algorithm (PDMA). Since the discrete system of equations contained five diagonal entries, the PDMA yielded exact solution for each system of equations. The convergence criterion used is given as;

$$|(a_{i,j}^{n+1} - a_{i,j}^n)/A_i^{n+1}| < e_i, \quad j=1,N, \quad (25)$$

where i ($=u, k_p, \epsilon_p, k_t, \text{ or } \epsilon_t$) denotes each flow variable; A_i denotes the maximum magnitude of the i -th flow variable; N denotes the number of degrees of freedom for each flow variable; $e=1 \times 10^{-7}$ has been used for velocity; and $e=5 \times 10^{-5}$ has been used for the rest of flow variables.

1. Fully Developed Channel Flow

The experimental data for the fully developed channel flow can be found in Laufer¹⁴. The Reynolds number based on the center line mean velocity (7.07 m/sec) and the half of the channel width (0.0635 meters) was approximately 30,800. The partition between the near-wall layer and the fully turbulent region has been located at $y^+ \approx 100$. The near-wall layer has been discretized by 20 grid points; and the rest of the flow domain, by 40 grid points. The Dirichlet boundary condition ($u = k_p = k_t = 0$) has been prescribed at the wall; and the vanishing gradient boundary condition, at

the center line of the channel. The pressure gradient estimated from the pressure measurement and the wall shearing stress measurement were $-1.41 \text{ kg-m/sec}^2\text{-m}^3$ and $-1.40 \text{ kg-m/sec}^2\text{-m}^3$, respectively. In the present computation, $dp/dx = -1.405 \text{ kg-m/sec}^2\text{-m}^3$ has been used. The converged solution has been obtained after approximately 400 iterations.

The computational results for the velocity, the turbulent kinetic energy, and the Reynolds stress are compared with the experimental data in Figure 1. The velocity profile compared less favorably with the experimental data. The under-predicted velocity profile may be due to the inaccurate pressure gradient. The magnitude and location of the maximum turbulent kinetic energy compared favorably with experimental data. It can be seen from the Reynolds stress profile that the present turbulence model yielded correct distribution of the turbulent viscosity.

The normalized velocity, the turbulent kinetic energy, and the Reynolds stress inside the near-wall layer are shown in Figure 2; and the normalized dissipation rate, the ratio of Pr/ϵ_t , and the wall damping function are shown in Figure 3. The calculated magnitude and the location of the overshoots of the turbulent kinetic energy and the dissipation rate were in good agreement with the experimental data. The rest of computational results such as the ratio of production rate to dissipation rate of the turbulent kinetic energy and the wall damping function compared favorably with the semi-empirical data.¹¹ It is shown in Reference 11 that only a few low Reynolds number turbulence models could yield the turbulent kinetic energy profile with overshoot in the near-wall region. It can be found in Reference 32 that the global computational results obtained by using various turbulence models with wall function methods compared satisfactorily with experimental data. However, the correct magnitude of

the overshoot of the turbulent kinetic energy and the dissipation rate have seldom been obtained.

2. Fully Developed Pipe Flows

The fully developed pipe flows at Reynolds numbers of 50,000 and 500,000 are considered below. The experimental data can be found in Laufer¹⁴. The Reynolds number was based on the diameter of pipe (0.24688 meters) and the center line mean velocity. The center line velocities were 3.048 m/sec and 30.48 m/sec for Re=50,000 and 500,000, respectively. In each case, the partition between the near-wall layer and the fully turbulent region has been located at $y^+ \approx 100$. For Re=50,000, the near-wall layer has been discretized by 20 grid points; and the rest of the flow domain, by 40 grid points. For Re=500,000, the near-wall layer has been discretized by 20 grid points; and the rest of the flow domain, by 60 grid points. For both cases, the Dirichlet boundary condition ($u = k_p = k_t = 0$) has been prescribed at the wall; and the vanishing gradient boundary condition, at the center line of the pipe. The pressure gradients estimated from the pressure measurements were $-0.32 \text{ kg-m/sec}^2\text{-m}^3$ and $-23.05 \text{ kg-m/sec}^2\text{-m}^3$ for Re=50,000 and 500,000, respectively. The converged solutions have been obtained after approximately 450 iterations for both cases.

The computational results for the velocity, the turbulent kinetic energy, and the Reynolds stress for Re=50,000 are compared with experimental data in Figure 4. For this case, the computational results compared favorably with the experimental data. The Reynolds stress profile was slightly under-predicted, however, the difference was negligible. The normalized velocity, the turbulent kinetic energy, and the Reynolds stress

inside the near-wall layer are shown in Figure 5; and the normalized dissipation rate, the ratio of Pr/ϵ_t , and the wall damping function are shown in Figure 6. The calculated magnitude and the location of the overshoots of the turbulent kinetic energy and the dissipation rate were in excellent agreement with the experimental data.

The computational results for the velocity, the turbulent kinetic energy, and the Reynolds stress for $Re=500,000$ are compared with experimental data in Figure 7. It was found that the mean velocity profile was severely under-predicted. Again, this may be due to the inaccurate pressure gradient as in the fully developed channel flow case. The thickness of the near-wall layer (i.e., $y^+ < 100$) for $Re=500,000$ case was approximately one order of magnitude smaller than that of $Re=50,000$ case. Both the calculated and the measured turbulent kinetic energy profiles exhibited strong peak in the region very close to the wall.

The normalized velocity, turbulent kinetic energy, and Reynolds stress inside the near-wall layer are shown in Figure 8; and the normalized dissipation rate, ratio of Pr/ϵ_t , and wall damping function are shown in Figure 10. Again, the calculated magnitude and the location of the overshoots of the turbulent kinetic energy and the dissipation rate were in excellent agreement with the experimental data.

Conclusions and Discussion

A near-wall turbulence model and numerical computations of fully developed turbulent channel flows and pipe flows using a partially low Reynolds number multiple-time-scale turbulence model have been presented.

It has been shown that the present turbulence model yielded accurate computational results for the example flows considered. The correct

magnitude and location of the overshoots of the turbulent kinetic energy and the dissipation rate have been obtained only by a few low Reynolds number turbulence models¹¹; and have seldom been obtained by the two- or multi-layer turbulence models³³. The turbulent kinetic energy and the dissipation rate overshoots obtained by using the present turbulence model were in excellent agreement with experimental data. The rest of the computational results in the near-wall region such as the normalized velocity profile, the Reynolds stress profile, the ratio of production rate to dissipation rate, and the wall damping function compared favorably with experimental data.

In the two- or multi-layer turbulence models, the turbulent kinetic energy in the near-wall layer is constructed by piecewise continuous functions; and the dissipation rate, by discontinuous functions. In the partially low Reynolds number turbulence models and in the low Reynolds number turbulence models, the turbulent kinetic energy and the dissipation rate vary smoothly from the wall toward the outside fully turbulent region. In this regard, the partially low Reynolds number turbulence models and the low Reynolds number turbulence models are more consistent with the experimentally observed distribution of the turbulent kinetic energy and the dissipation rate than the two- or multi-layer turbulence models are. A significant number of grid points has to be assigned in the near-wall layer for numerical computation of turbulent flows with the low Reynolds number turbulence models. However, with the use of partially low Reynolds number turbulence models, less number of grid points need to be assigned inside the near-wall layer and the stiff dissipation rate in the region need not be solved numerically. Therefore, many numerical codes can be made more robust and more efficient with the use of the partially low Reynolds number

turbulence models.

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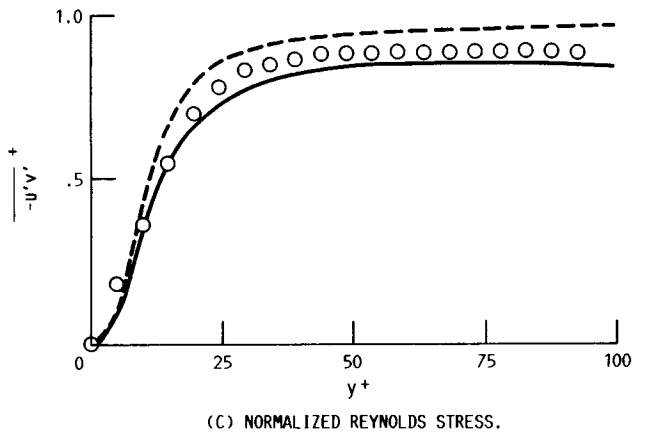
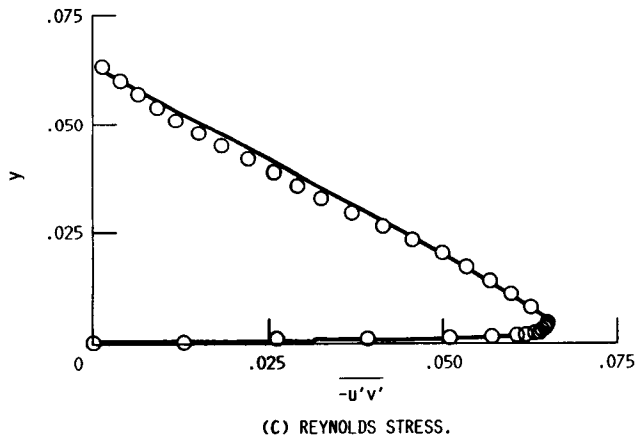
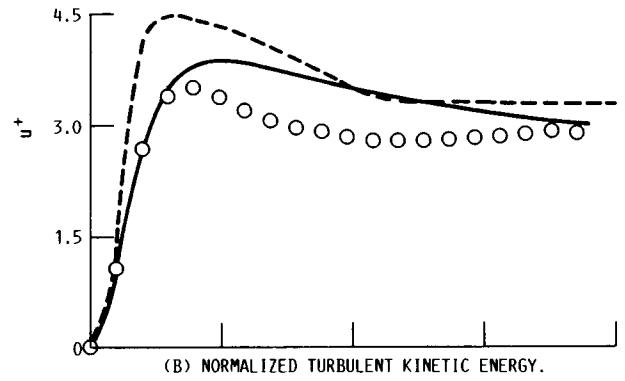
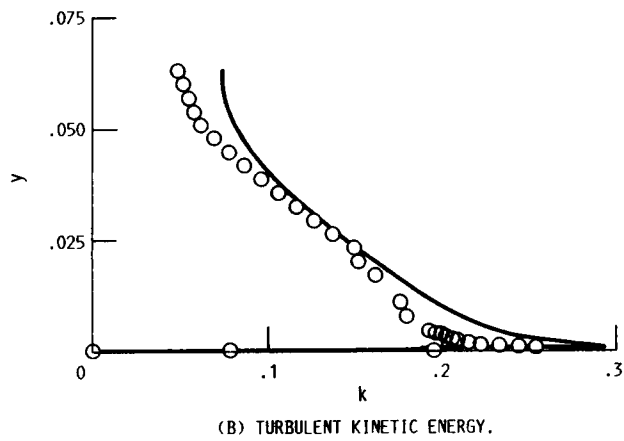
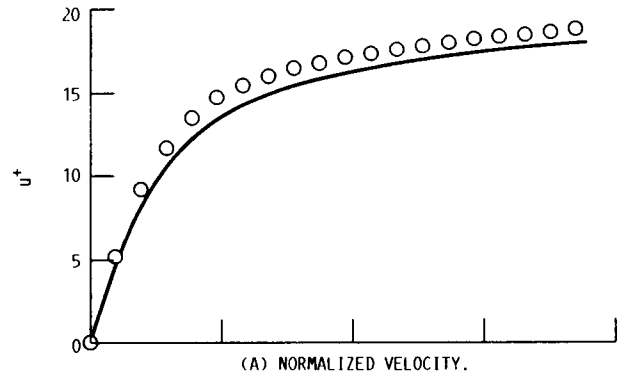
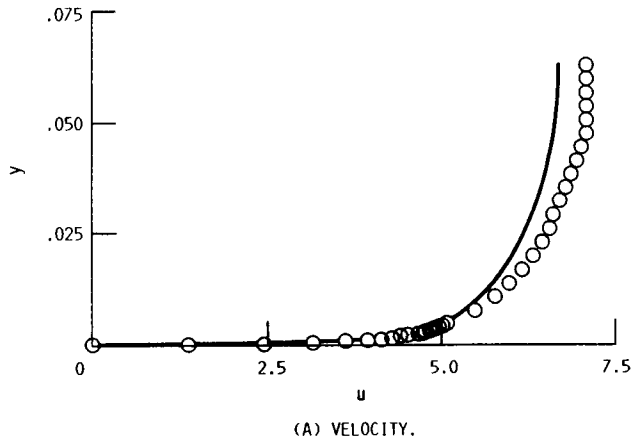


FIGURE 1. - FULLY DEVELOPED CHANNEL FLOW. O: EXPERIMENTAL DATA (REF. 10), —: COMPUTATIONAL RESULT.

FIGURE 2. - FULLY DEVELOPED CHANNEL FLOW. O: EXPERIMENTAL DATA (REF. 10), —: COMPUTATIONAL RESULT, - - -: SEMI-EMPERICAL DATA (REF. 7).

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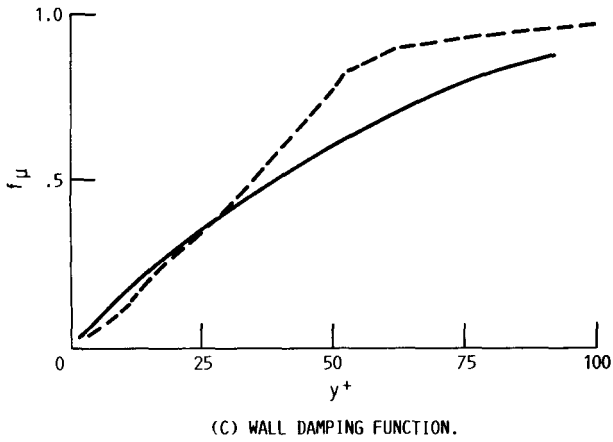
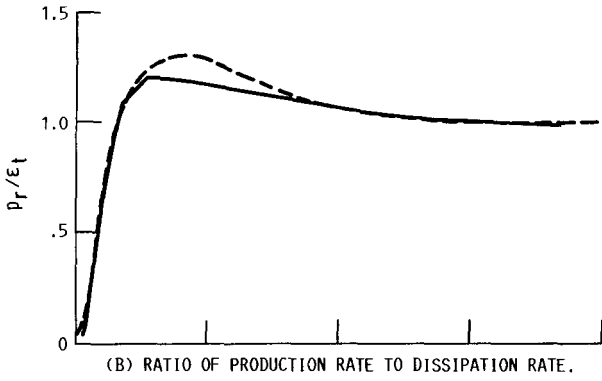
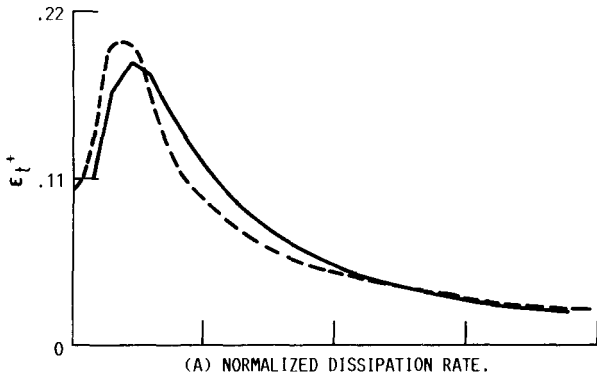


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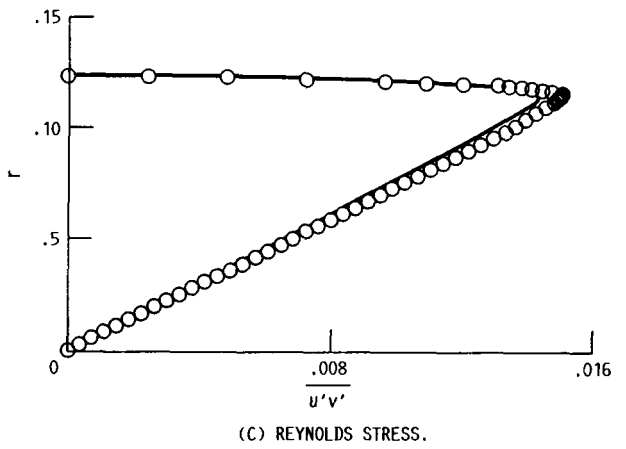
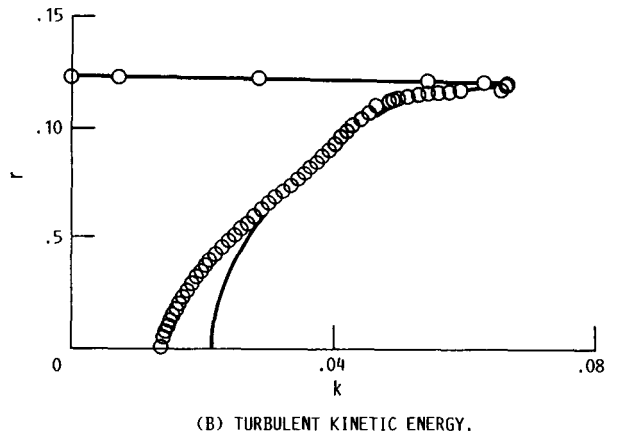
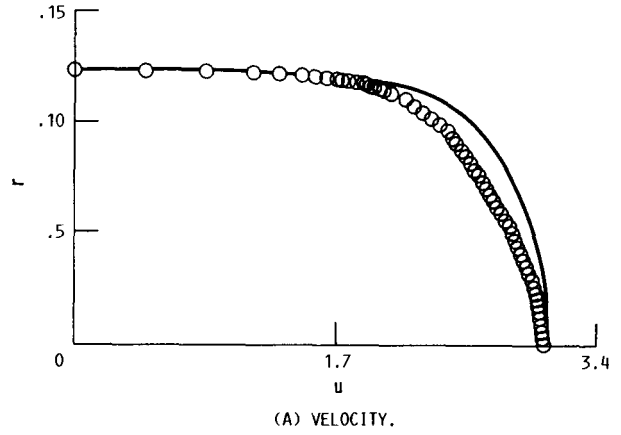


FIGURE 4. - FULLY DEVELOPED PIPE FLOW FOR $Re = 50\ 000$, O: EXPERIMENTAL DATA (REF. 11), — : COMPUTATIONAL RESULT.

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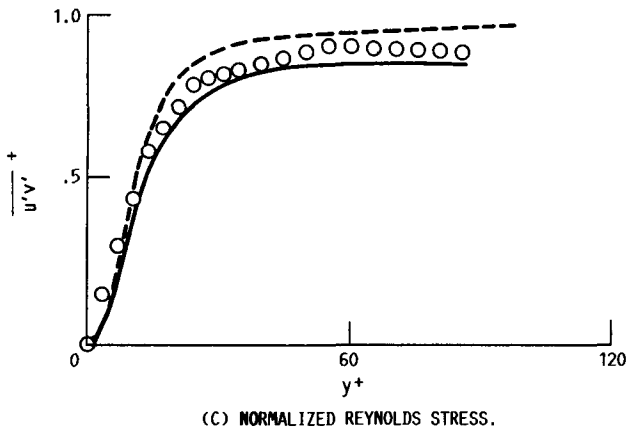
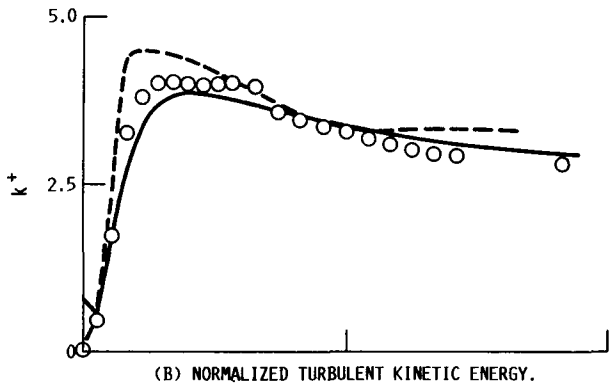
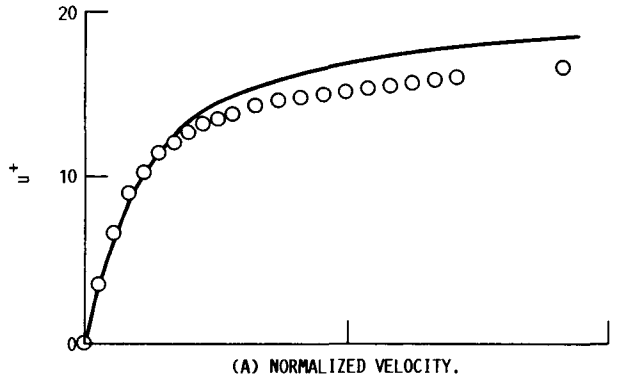


FIGURE 5. - FULLY DEVELOPED PIPE FLOW FOR $Re = 50\ 000$.
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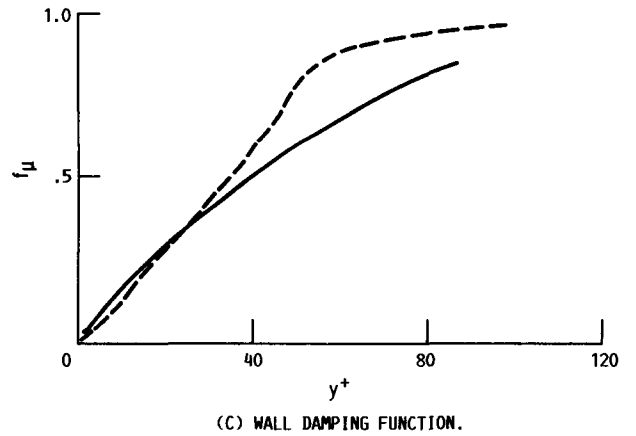
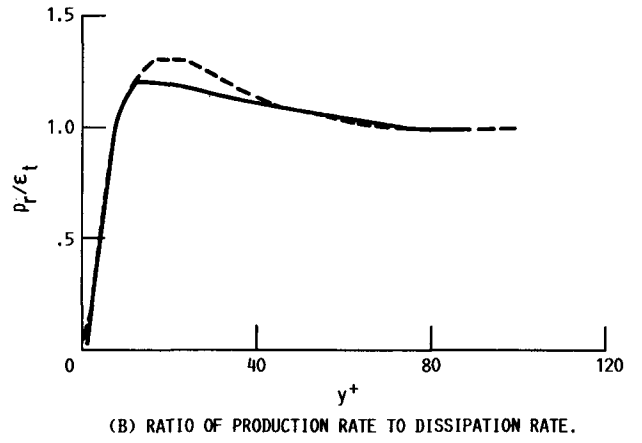
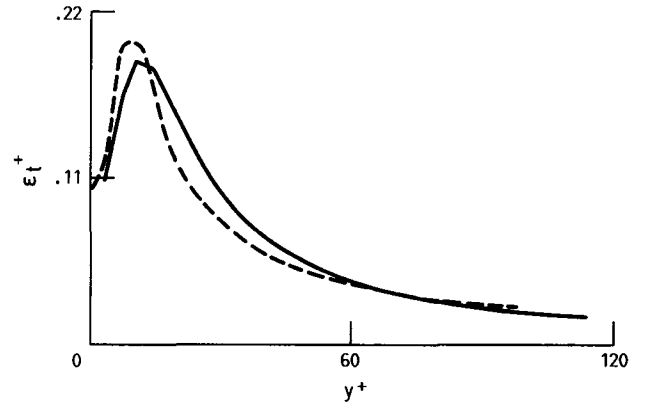


FIGURE 6. - FULLY DEVELOPED PIPE FLOW FOR $Re = 50\ 000$.
—: COMPUTATIONAL RESULT, ---: SEMI-EMPERICAL
DATA (REF. 7).

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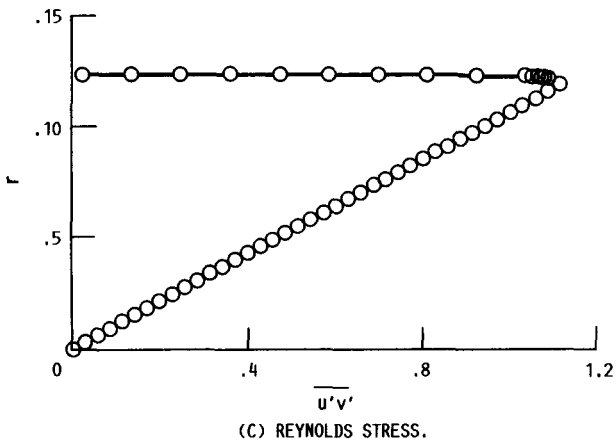
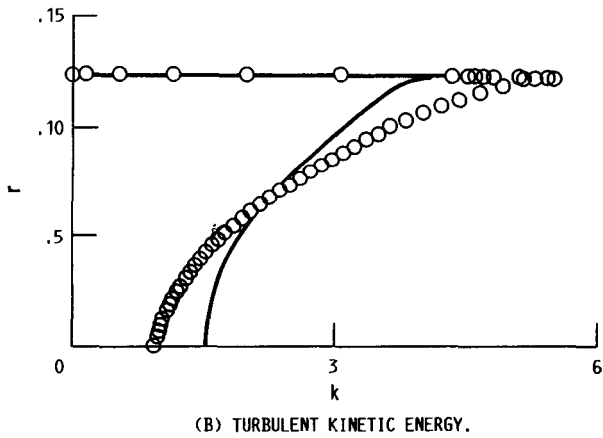
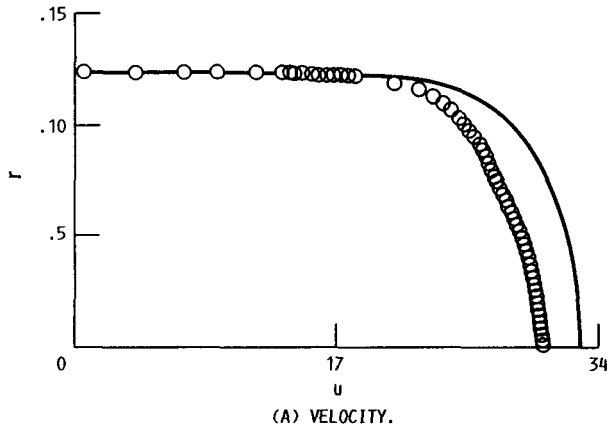


FIGURE 7. - FULLY DEVELOPE PIPE FLOW FOR $Re = 500\ 000$,
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RESULT.

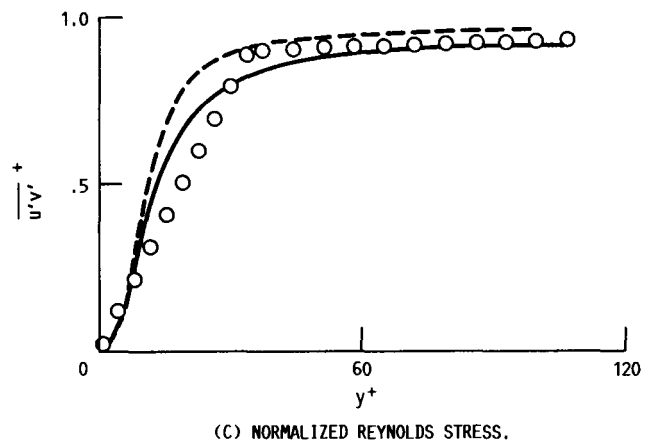
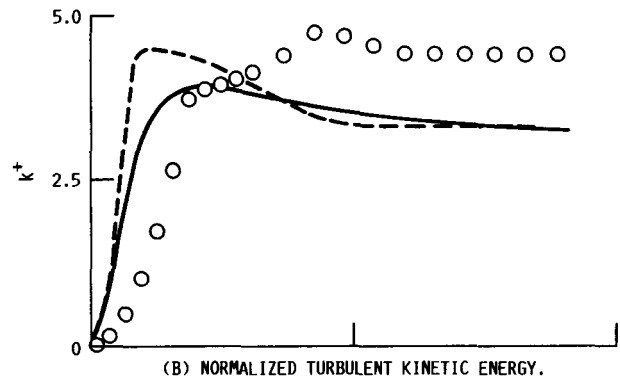
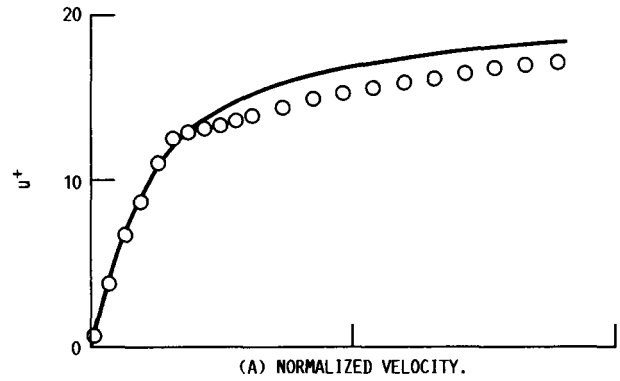


FIGURE 8. - FULLY DEVELOPED PIPE FLOW FOR $Re = 500\ 000$,
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RESULT, - - - : SEMI-EMPERICAL DATA (REF. 7).

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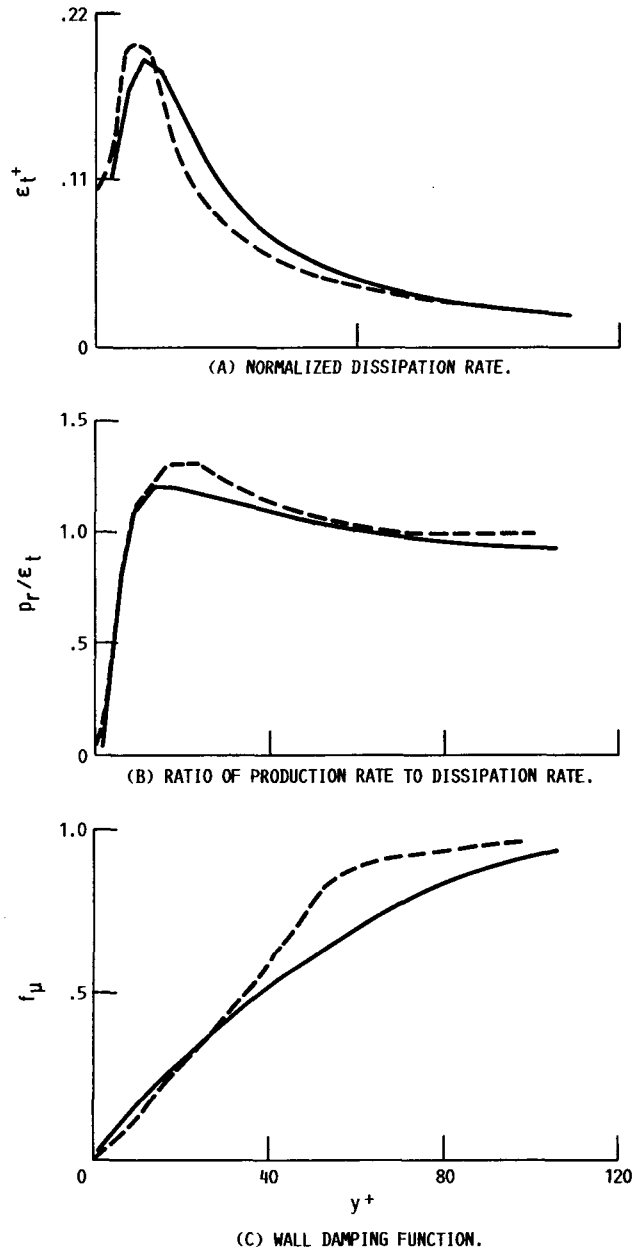


FIGURE 9. - FULLY DEVELOPED PIPE FLOW FOR $Re = 500\ 000$.
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DATA (REF. 7).

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16. Abstract A near-wall turbulence model and its incorporation into a multiple-time-scale turbulence model are presented in this report. In the method, the conservation of mass, momentum, and the turbulent kinetic energy equations are integrated up to the wall; and the energy transfer rate and the dissipation rate inside the near-wall layer are obtained from algebraic equations. The algebraic equations for the energy transfer rate and the dissipation rate inside the near-wall layer have been obtained from a k-equation turbulence model and the near wall analysis. A fully developed turbulent channel flow and fully developed turbulent pipe flows were solved using a finite element method to test the predictive capability of the turbulence model. The computational results compared favorably with experimental data. It is also shown that the present turbulence model could resolve the over-shoot phenomena of the turbulent kinetic energy and the dissipation rate in the region very close to the wall.					
<p><i>K-epsilon</i></p> <p>TURBULENCE FLOW CHANNEL PIPE TURBULENCE MODEL WALL FLOW</p> <p>FINITE ELEMENT METHOD MULTI-TIME SCALE KINETIC ENERGY ENERGY TRANSFER RATE DISSIPATION RATE</p>					
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