٩

brought to you by CORE provided by NASA Technical Reports Server

GRAN. 1N-36-CR 217715 148

MATHEMATICAL SCIENCES DEPARTMENT COLLEGE OF SCIENCES OLD DOMINION UNIVERSITY NORFOLK, VIRGINIA 23529

COMPARISON OF LASER MODELS

By John H. Heinbockel, Principal Investigator	N89-26220 Unclas U217715
Progress Report For the period ended May 15, 1989	G3/36
Prepared for National Aeronautics and Space Administration Langley Research Center Hampton, Virginia 23665	N OF LASER MODELS led 15 May 1539 CSCL 20E
Under Research Grant NAG-1-757 Dr. Robert C. Costen, Technical Monitor SSD-High Energy Science Branch	COMPARISO period end iv.) 14 p
Submitted by the Old Dominion University Research Foundation P.O. Box 6369 Norfolk, Virginia 23508-0369 June 1989	(NASA-CR-185390) Progress Report, (Old Dominion Uni

. .

Progress Report Research Grant NAG-1-757 ODURF 176613 Comparison of Laser Models

Notation.

In this report the following notations will be used:

$$\begin{array}{ll} x_1 = [RI] & x_4 = [I_2] \\ x_2 = [R] & x_5 = [I^*] \\ x_3 = [R_2] & x_6 = [I] \\ & x_7 = [\rho] \end{array}$$

where [] denotes concentration and R is a perflouride radical, I is iodine, I^* is an excited state of iodine, and ρ is the photon density.

Oscillatory Model.

The following is the unscaled version of the time varying chemical kinetics equations for the simulation of the iodine laser operation

$$\begin{aligned} \frac{dx_1}{dt} &= k_1 x_2 x_5 + k_2 x_2 x_6 - \psi_1 x_1 - k_4 x_1 x_2 \\ \frac{dx_2}{dt} &= -k_1 x_2 x_5 - k_2 x_2 x_6 - 2k_3 x_2^2 + \psi_1 x_1 - k_4 x_1 x_2 \\ \frac{dx_3}{dt} &= k_3 x_2^2 + k_4 x_1 x_2 \\ \frac{dx_4}{dt} &= c_1 x_1 x_5 x_6 + c_2 x_1 x_6^2 + c_3 x_4 x_5 x_6 - \psi_2 x_4 + c_4 x_4 x_6^2 \\ \frac{dx_5}{dt} &= -k_1 x_2 x_5 - c_1 x_1 x_5 x_6 - c_3 x_4 x_5 x_6 - Q_1 x_1 x_5 - Q_2 x_4 x_5 \\ - A x_5 + \psi_1 x_1 + 0.51 \psi_2 x_4 - \Gamma_{max} \\ \frac{dx_6}{dt} &= 1.49 \psi_2 x_4 + Q_1 x_1 x_5 + Q_2 x_4 x_5 + A x_5 - c_1 x_1 x_5 x_6 + \Gamma_{max} \\ + k_4 x_1 x_2 - 2 c_2 x_1 x_6^2 - c_3 x_4 x_5 x_6 - k_2 x_2 x_6 - 2 c_4 x_4 x_6^2 \\ \frac{dx_7}{dt} &= \sqrt{\frac{\pi}{2.77}} \left(\frac{L}{L_c}\right) \Gamma_{max} + \frac{\log(R_1 R_2)}{2\left(\frac{L_c}{c}\right)} x_7 + 2\left(\frac{0.18}{L_c}\right)^2 A x_5 \\ \text{where} \quad \Gamma_{max} = \frac{c x_7 (x_5 - \frac{1}{2} x_6)}{A_{00} + B_{00} x_1} \end{aligned}$$

The above equations are solved subject to the initial conditions

 $x_1(0) = P * (3.5E16)$ and $x_i(0) = 0$, i = 2, ..., 7

where P is the pressure in torr. The above system was solved using a variable step size Runge-Kutta-Fehlberg alogorithm. The figures 1.1 through 1.4 illustrated a typical set of solution curves to the above system of differential equations. Note the violent oscillations which occur during start-up of the laser. These oscillations require that small step sizes be taken during the numerical integration process in order to achieve some desired degree of accurracy. The numerical method becomes unstable and the results are meaningless if too large a step size is selected. This is not an uncommon situation in trying to numerical solve chemical kinetic systems of equations.

Nonoscillatory Model.

The inversion term $[I^*] - \frac{1}{2}[I] = x_5 - \frac{1}{2}x_6$ which occurs in the Γ_{max} term as well as the equations which define the rate of change of $[I^*] = x_5$ and $[I] = x_6$, is the term which causes the oscillations in the nonlinear system of coupled ordinary differential equations. Under quasi-steady state conditions we set the rate of change of this term equal to zero. That is we require that

$$\frac{d}{dt}\left([I^*] - \frac{1}{2}[I]\right) = 0$$

and then solve for Γ_{max} which is then relabled as $(\Gamma_{max})_{ss}$. We find that

$$(\Gamma_{max}) = -Ax_5 - Q_2 x_4 x_5 + \{2\psi_1 x_1 - 0.47\psi_2 x_4 - 2k_1 x_2 x_5 + k_2 x_2 x_6 - c_1 x_1 x_5 x_6 + 2c_2 x_1 x_6^2 - c_3 x_4 x_5 x_6 + 2c_4 x_4 x_6^2 - k_4 x_1 x_2\}/3$$

Initially the Γ_{max} term is removed from the above equations as it is assumed to be initially zero. As time increases, $[I^*]$ and [I] build up and when the threshold condition is met we have

$$[I^*] - \frac{1}{2}[I] = -\frac{1}{2} \frac{\ln(R_1 R_2)}{\sqrt{(\pi/2.77)}} (L\sigma)^{-1} = I_{th}.$$

Here it is assumed that steady state conditions have been achieved and gains balance with losses. The above steady state value is subsituted for Γ_{max} . In this way the ocillatory character of the solution is removed and the integration can be made to proceed at a much faster rate. The results from this second nonoscillatory model were generated by L.Stock and are presented in the figures 1.5, 1.6. Observe how the oscillatory character of the solutions has been removed. Also, as a check on the model, the values of the power output were compared for both models and both values were found to be in agreement. The figure 1.7 lists the values of the reaction rate coefficients used in both models.

Currently there are four models for the simulation of an iodine laser. These models can be described by:

- 1. A time dependent model which is given by the above set of coupled nonlinear differential equations which describe the chemical kinetics at a fixed point as a function of time t.
- 2. A quasi-steady state model whereby the Γ_{max} term is replaced by its steady state value. This model is also a time dependent model with much faster integration times.
- 3. A noncompressible model which solves the above system of differential equations as a function of distance z along the axis of the laser tube. This model is characterized by substituting a material derivative in place of the time derivatives in the above differential equations. For an assumed steady flow, we make the substitutions:

$$\frac{d}{dt}[] = \frac{\partial[]}{\partial t} + \frac{\partial[]}{\partial z}\frac{dz}{dt}$$

and assume that $\frac{dz}{dt} = \omega$ is a constant. The time dependence is removed by assuming steady state values. Problems of stiffness arise in the numerical integration of this system.

4. A compressible flow laser model which solves the above system of differential equations with the material derivative replacing the time derivatives. In addition to these equations there is added: (i) a continuity equation (ii) an equation of state (iii) a momentum equation and (iv) an energy equation.

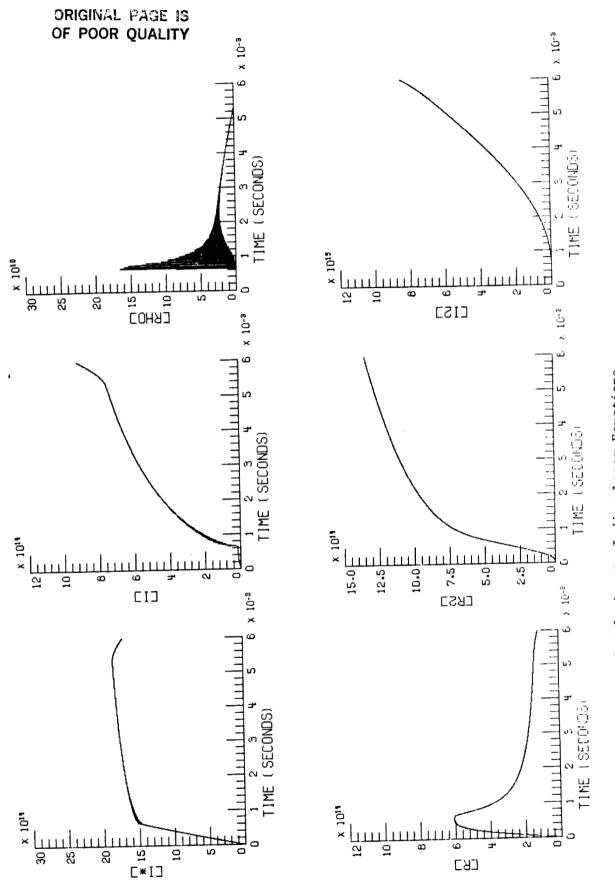
The figures 1.8 illustrates power vs beam radius which was obtained from the model 4, above assuming a parabolic velocity profile. The figure 1.9 illustrated power vs reflectivity for various pumping distances along a 45cm laser tube.

Current research is being directed toward:

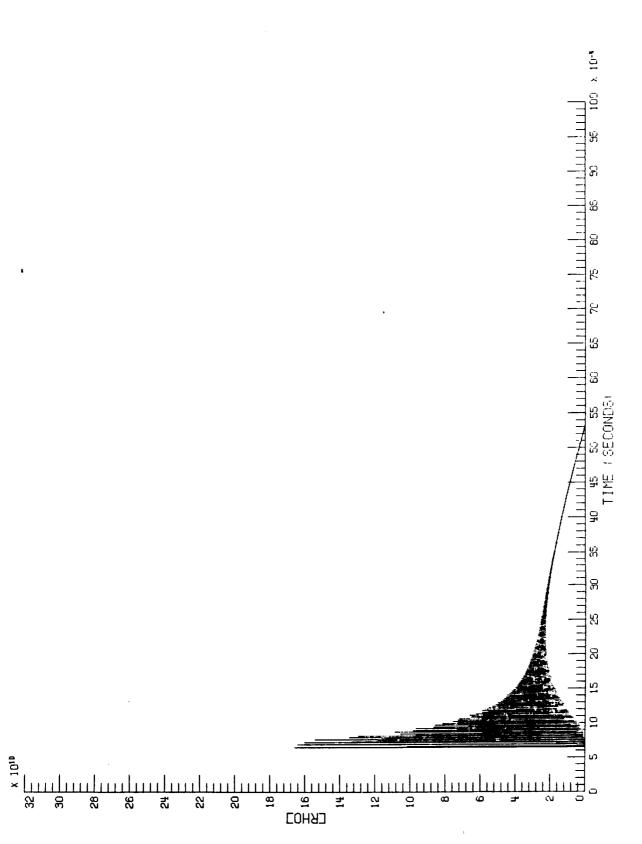
- 1. Parameter studies using the compressible flow laser model.
- 2. Development of a two pass amplifier model.
- 3. Solve system of equations describing operation of high powerhh iodine MOPA (Master Oscillator Power Amplifier). These equations are derived from the Frantz-Nodvik Amplifier theory.

REFERENCES

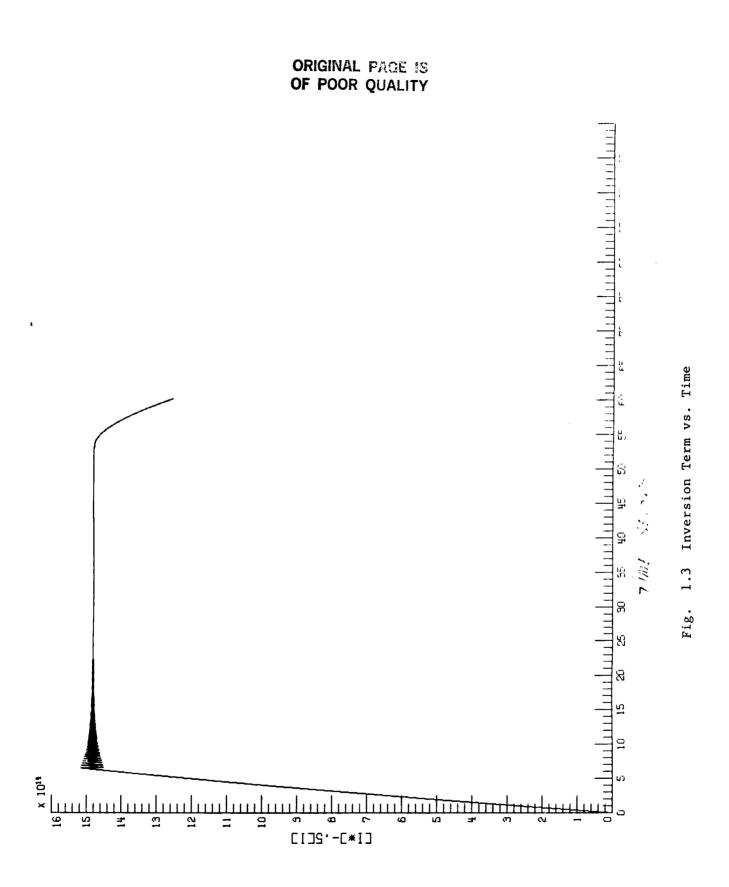
- 1. L.V. Stock, J.W.Wilson, R.J.DeYoung, A Model for the Kinetics of a Solar-pumped Long Path Laser Experiment., NASA Technical Memorandum 87668, May 1986.
- 2. J.W.Wilson, S.Raju, Y.J. Shiu, Solar-Simulator-Pumped Atomic Iodine Laser Kinetics, NASA Technical Paper 2182, August 1983.



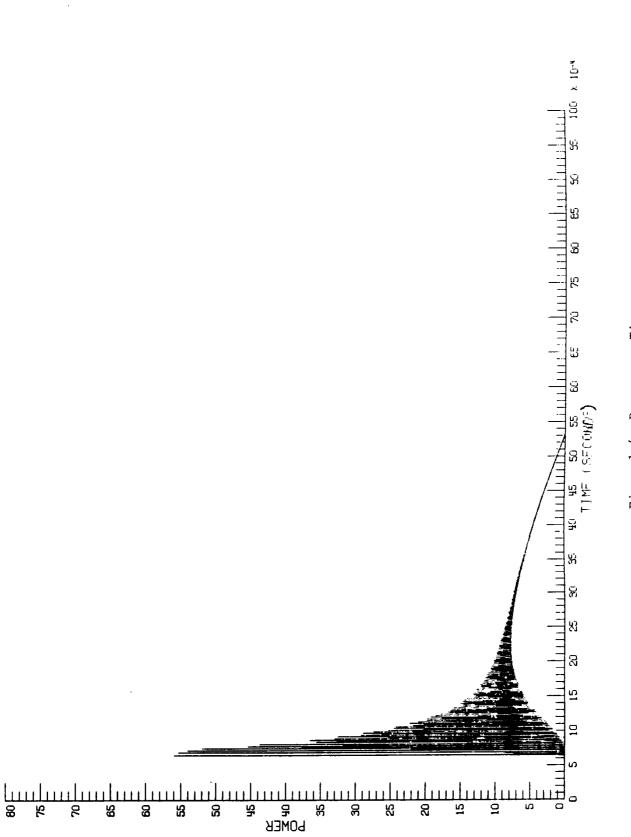








.





İ

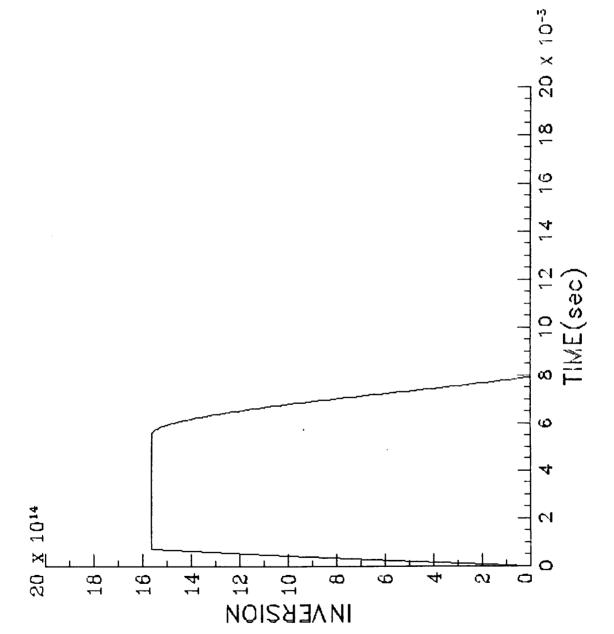
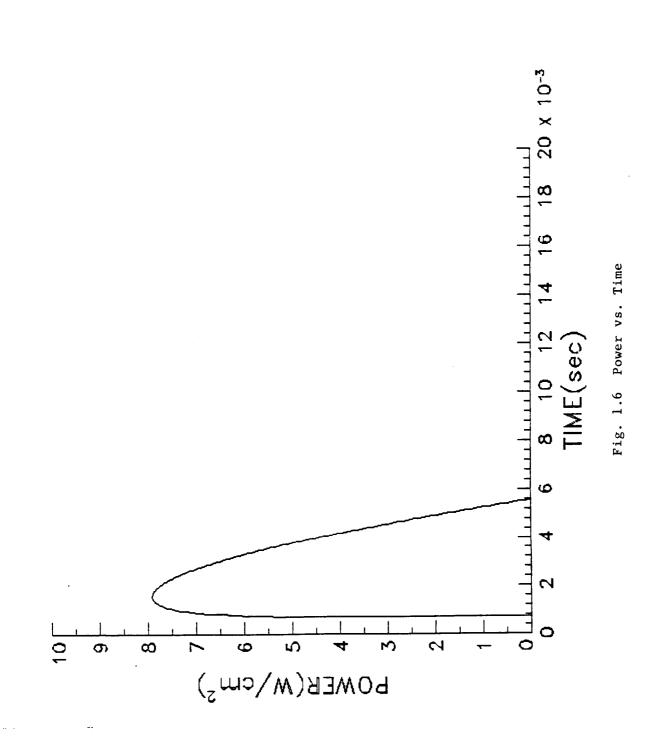


Fig. 1.5 Inversion vs. Time

ļ



Lasant	n-C ₃ F ₇ I	Reaction Rate Coefficient
Reactions	Symbol	(cm³)"/sec
R + I [*] + RI	К,	.5600 X 10 ⁻¹²
R + I + RI	K ₂	.2300 X 10 ⁻¹⁰
$R + R \rightarrow R_2$	K3	.2600 X 10 ⁻¹¹
$R + RI + R_2 + I$	K.	.3000 X 10 ⁻¹⁵
$R + I_2 + RI + I$	K,	.0000 X 10 ⁺⁰⁰
$ ^{*} + + R + I_{2} + R $	C,	.3200 X 10 ⁻³²
$ + + R + _2 + R $	Ċ,	.8500 X 10 ⁻³¹
$ ^{a} + + _{2} \rightarrow _{2} + _{2}$	C,	.8000 X 10 ⁻³¹
$ + + _2 + _2 + _2$	C,	.3800 X 10 ⁻²⁹
I [•] + RI → I + RI	Q,	.2000 X 10 ^{-1\$}
$ ^{*} + _{2} + _{1} + _{2}$	O ₂	.1900 X 10 ⁻¹⁰
	Ts	1.0000
	α	.0000

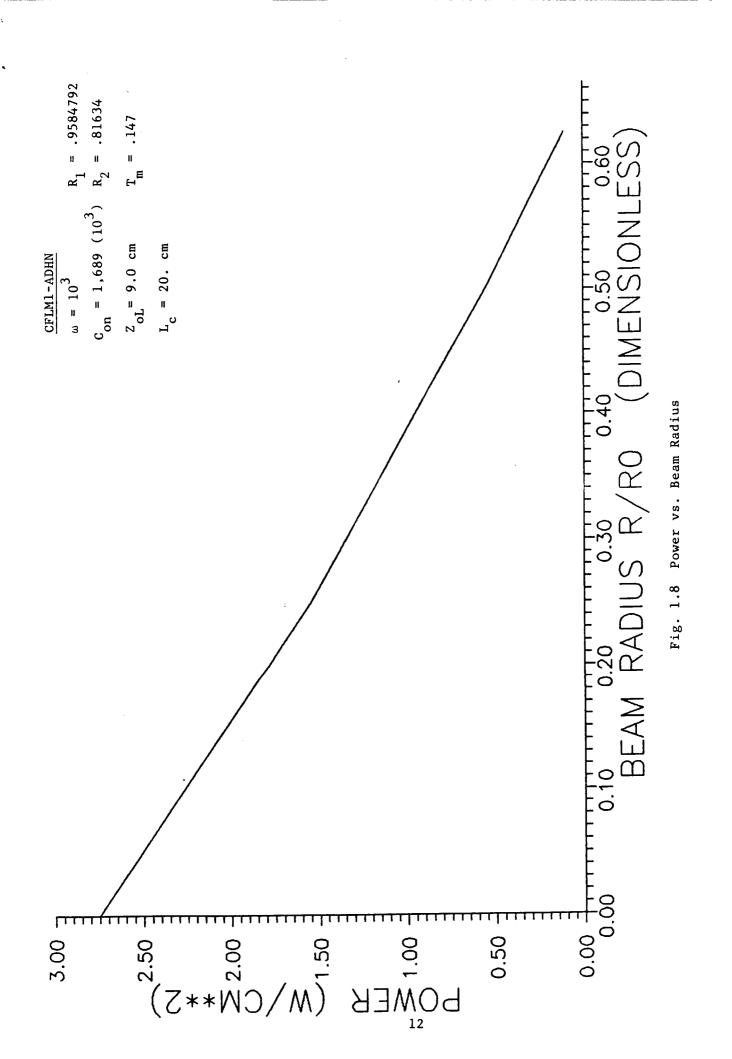
TABLE 1 – Reaction rate coefficients and their associated reactions for the lasant $n-C_3F_7I$ along with the parameters used to modify the optical time constant (ref. 2).

-

,

Fig. 1.7 Table I. Reaction Rate Coefficients

-



45 CM LASER WITH VARIABLE PUMPING DISTANCE AND VARIABLE REFLECTIVITY

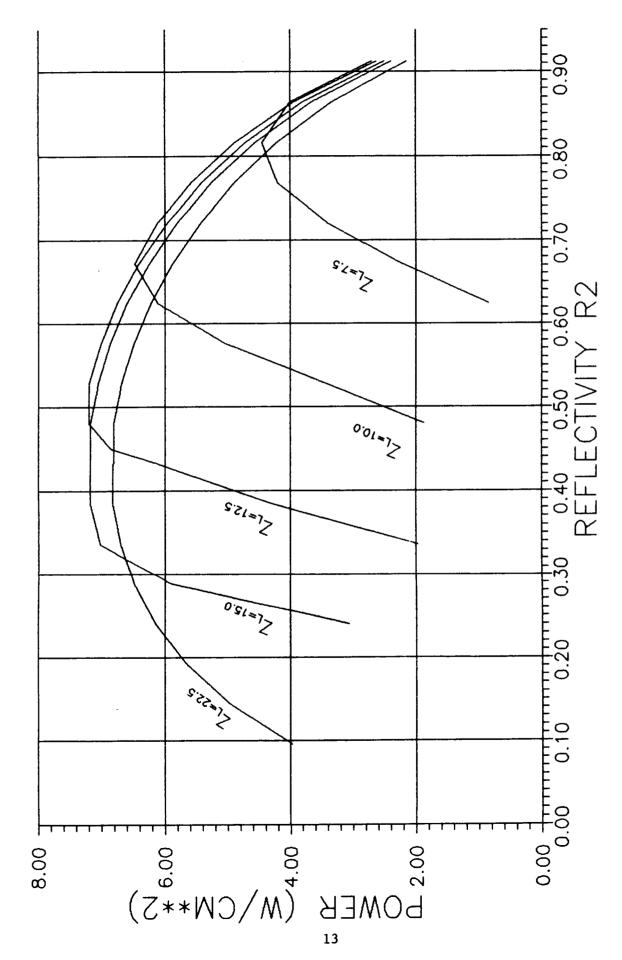


Fig. 1.9 Power vs. Reflectivity