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# January 1990

# Satellite Radar Altimetry Over Ice

Volume 1—Processing and Corrections of Seasat Data Over Greenland

H. Jay Zwally, Anita C. Brenner, Judith A. Major, Thomas V. Martin, and Robert A. Bindschadler

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# PREFACE

The data-processing methods and ice data products derived from Seasat radar altimeter measurements over the Greenland ice sheet and surrounding sea ice are documented in this first volume of a series. The corrections derived and applied to the Seasat radar altimeter data over ice are described in detail, including the editing and retracking algorithm to correct for height errors caused by lags in the automatic range tracking circuit. The methods for radial adjustment of the orbits and estimation of the slope-induced errors are given. The various levels of ice data sets are described in this report, but the user is referred to Volumes 2 (Greenland) and 4 (Antarctica) for more detailed descriptions of the gridded elevation data sets and the geo-referenced data bases.

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# SECTION 1.0 INTRODUCTION

This volume is the first in a series documenting the data-processing methods and ice data products derived from satellite radar altimeter measurements over the ice sheets of Greenland and Antarctica and surrounding sea ice. The data-processing procedures and corrections derived and applied to the Seasat radar altimeter data are described in detail in this report. A flowchart depicting the procedures involved in obtaining the various data products is given in Figure 1. A detailed description of the editing and retracking algorithm is given in Section 2, along with descriptions of the other corrections. The methods for radial adjustment of the orbits and estimation of the slope-induced errors are described. The various levels of ice data sets produced are described in this report, but the user is referred to Volumes 2 and 4 for more detailed descriptions of the gridded elevation data set and the geo-referenced data base.

The input Seasat radar altimeter data, in the form of Geophysical Data Records (GDR's) and Sensor Data Records (SDR's) produced by NASA's Seasat project at the Jet Propulsion Laboratory, were obtained from the NOAA Environmental Satellite Data and Information Service (EDIS) archive on about 1000 magnetic tapes. Development of the data processing methods, the production of higher-level geophysical data products, and analysis and evaluation of the data have been supported at the Goddard Space Flight Center by funding for research and data analysis, provided primarily by NASA's Ocean Processes Program and by the Climate program. Computer programming and technical assistance has been provided by the EG&G Washington Analytical Services Center, Inc. until January 1989 and by ST Systems Corporation since then. Numcrous other individuals have provided valuable assistance.

Results have been reported in refereed scientific literature (e.g., Brenner et al., 1983; Martin et al., 1983; Zwally et al., 1983; Thomas et al., 1983; and Gundestrup et al., 1986). In addition, elevation data in various forms have been provided to other scientists and placed in the National Snow and Ice Data Center (NSIDC) and the National Space Science Data Center (NSSDC). The purpose of this series of reports is to document technical details and provide guidance to users of the ice data products.

While all reasonable quality-control efforts have been made to eliminate erroncous data, some data of questionable quality is likely to have persisted, particularly in the lower-level data products. Users should apply normal standards of scientific caution in their use of the data.



Figure 1. Processes Involved in Obtaining Data Products

The current list of reports is:

Satellite Radar Altimetry over Ice, Volume 1: Processing and Corrections of Seasat Data over Greenland, July 1989. This volume.

Satellite Radar Altimetry over Ice, Volume 2: User's Guide for Greenland Elevation Data from Seasat, July 1989. NASA Reference Publication.

Satellite Radar Altimetry over Ice, Volume 4: User's Guide for Antarctic Elevation Data from Seasat, July 1989. NASA Reference Publication.

Volume 3 will be the Antarctic equivalent of Volume 1. Additional volumes will include descriptions of the data sets being produced by NASA from the radar altimeter data acquired by the U.S. Navy's GEOSAT, using methods similar to those for the Seasat data.

The Seasat spacecraft (e.g., Lame and Born, 1982 and Lame et al., 1980) was launched in late June 1978, and during its brief 110-day lifetime, collected 90 days of nearly continuous radar altimeter data from July 9 through October 10 between the latitudes of 72°S and 72°N. Although designed only for measurements over water, the Seasat radar altimeter (MacArthur, 1978; Tapley et al., 1982; and Townsend, 1980), acquired more than 600,000 useful altimeter range measurements over the continental ice sheets of Greenland and Antarctica.

Over sloping and undulating surfaces, such as ice covered land, or surfaces with highly-variable reflecting characteristics, such as in regions of sea ice, the range to the surface and the characteristics of the received radar pulse changed faster than the response capability of the altimeter electronics. Consequently, it has been necessary to correct each range value for lags of the altimeter range servo-tracking circuitry by a procedure called retracking (Martin et al., 1983). The retracking correction typically had a mean value of  $\pm 1.4$  m as applied to the surface elevation, a standard deviation of 2.9 m, and maximum and minimum values of  $\pm 15$  m. In addition, the pulse-limited footprint (1.6 km minimum diameter), which was located near the satellite nadir point over the relatively flat ocean, was in general located anywhere within the beam-limited footprint (22 km in diameter) over sloping surfaces. The resulting slope-induced error, which was nearly 80 m over slopes of 0.8 degree, can be partially corrected using the procedures described in Brenner et al., 1983. Corrections are also made for errors in orbit determination, atmospheric propagation path-length variations, and earth and ocean tides.

Elevation measurements were obtained at 0.1-second intervals, corresponding to 662-m intervals along the subsatellite ground track. The precision of the corrected range measurements is about 1.6 m overall with a minimum of about 0.25 m in the smoothest regions of the ice sheets

(Zwally et al., 1983). The 5- to 10- cm precision over the ocean is for 1-sec data averages.) The absolute accuracy of the elevations is primarily determined by the limitations on the correction methods for the slope-induced errors and uncertainties in the geoid reference level.

The principal ice data sets produced and/or retained are:

Level 4: Contour maps and gridded elevations with respect to earth ellipsoid and sea level (e.g., this Volume and Volume 2).

Level 3: Geo-referenced data base including all individual elevation measurements (including time, latitude/longitude positions, and slope-correction estimates) accessible by geographic cells (e.g., this Volume and Volume 2).

Level 2: Ice Data Records (IDR's). Orbital-format data records including altimeter parameters, corrected elevations, latitude/longitude positions, AGC, applied corrections, retracking beta parameters, and estimates of along-track and cross-track slope corrections. (this Volume)

Level 1: Waveform Data Records (WDR's). Orbital-format data records including waveform amplitudes by gate, ranges, AGC, and latitude/longitude positions. (this Volume)

Sensor Data Records (SDR's) Geodetic Data Records (GDR's)

# SECTION 2.0 ICE DATA RECORDS

The Seasat altimeter data were released in two forms: the Altimeter Sensor Data Record (hereafter referred to as SDR), and the Geophysical Data Record, GDR. The SDR's were obtained from the NOAA/EDIS archives and contain, among other quantities, the telemetered range measurements between the spacecraft and earth's surface, averaged radar return pulses, the altimeter status flags and the satellite latitude, longitude, and elevation. The data are output in 0.098-sec intervals. The GDR's contain processed SDR data averaged over 1-sec intervals, and the sensor, atmospheric, and surface dynamic corrections necessary to utilize the data in detailed geodetic work. Data over the ice sheets are not available from the GDR's.

To obtain the ice sheet elevation measurements, data from the SDR's are used and the appropriate corrections and adjustments applied. This subset of ice sheet data obtained from the SDR's is referred to as ice data records or IDR's. A detailed description of these records may be found in Table 1. The surface heights, located in bytes 73-76 of the IDR, are referenced to the IUGG 1980 Geodetic Reference Ellipsoid (Moritz, 1980), which is defined with a 6378.137-km semi-major axis of the earth and a flattening ratio of 1/298.257. Heights relative to sea level can be calculated by subtracting the geoid value from the surface height. Geoid values, linearly interpolated from a one-by-one degree GEM10-B geoid grid, are located in bytes 61-64 of the IDR.

Figure 2 is a map of Greenland which depicts the coverage obtained from the IDR's after data were edited and retracked (see Section 2.1). The gaps in the data are a result of the altimeter not being able to maintain valid height measurements over the rougher surfaces of the ice sheets. Table 2 gives a concise catalog of the available Seasat Greenland IDR data. Included in this table are the start and stop locations of each rev, the number of points in each rev, and the data base bins (see Section 4.0) through which each rev traverses. The rev numbers are ordered such that all ascending passes are listed first, ordered by increasing latitude as they cross 315 degrees East Longitude. Then the descending passes are listed using the same ordering criterion as for the ascending passes.

#### 2.1 EDITING AND RETRACKING

As explained in Section 1.0, Seasat altimetry returns over non-ocean surfaces required special processing in order to calculate meaningful height measurements. To understand this processing one must first have an understanding of the return itself.



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Each altimeter return, referred to as a waveform, consists of the output of a set of 63 gates that span a height window of approximately 30 m. Each gate has a level of return associated with it measured in counts. A typical ocean return from Seasat is presented in Figure 3. The level of return in the first 22 gates is at the noise or pre-pulse level of 4 or 5 counts. The level quickly increases to a relative maximum and then slowly decreases over the latter portion of the window. There are three half-gates at the center that have a spacing of 23 cm instead of 46 cm. The tracking gate is the center of these. The on-board tracker attempts to keep the center of the return leading edge positioned at the tracking gate by predicting the travel time of each pulse based on previous returns. The measurement telemetered from the altimeter is equivalent to the travel time to the tracking gate.

Altimeter returns over non-ocean surfaces vary greatly from this ocean return. Figure 4 shows representative returns over ice sheet surfaces for a Scasat pass over Antarctica (Martin et al., 1983). The Figure 3 sea ice returns are represented by one or more sharp spikes that may or may not be at the tracking gate. As the altimeter travels onto the ice shelf, acquisition is lost, represented as a flat return. On the ice shelf the returns are shaped similar to the oceans, but again are not always centered at the tracking gate. As the satellite moves over the ice sheet, acquisition is again lost temporarily. Over the ice sheets the returns are noisy, have multiple leading edges, and the mid-point of the first leading edge is not always aligned with the tracking gate.

The measurement telemetered from the on-board tracker needs to be corrected for the variation of the mid-point of the leading edge from the tracking gate. This retracking correction,  $\Delta H_{ret}$  is calculated as

$$\Delta H_{ret} = (Gm-Gt)^* g^{2m}$$
(2.1)

where

- Gm = gate of the mid-point of the leading edge (see Sections 2.1.3-2.1.4),
- Gt = the tracking gate (29.5 where the whole gates are numbered from 0 to 59; see Figure 3), and
- $g_{2m}$  = the conversion from gates to meters = .4684375 m/gate.



Figure 3. Ideal Ocean Altimetry Return Pulse





It then follows that

$$H_{ret_t} = H_{meas_t} + \Delta H_{ret_{t+1}}$$
(2.2)

where

$$H_{ret_t}$$
 = the retracked altimeter measurement at time t,

$$H_{meas}$$
 = the measurement calculated by the on-board tracker at time t, and

$$\Delta H_{ret_{t+1}}$$
 = the retracking correction calculated from waveform at time t+.098 sec.

Due to the return being telemetered one time step later, the retracking correction for the measurement at time t is calculated from the return at time t+.098 sec. Methods have been developed at NASA/GSFC to calculate the  $\Delta H_{ret}$  for returns over the ice sheet, ice shelf, and sea ice which can yield valid height measurements. A detailed description of these procedures may be found in Sections 2.1.3 and 2.1.4. Parameters resulting from these retracking techniques may be found in bytes 109-144 of the IDR. The criteria used to automatically select and discriminate between different types of returns are described in the next two sections.

## 2.1.1 Selecting Retrackable Non-Ocean Altimetry Returns

The SDR for Seasat includes all telemetered altimeter data even when the instrument was in calibration or standby mode. Since valid measurements could be acquired when the tracker was in acquisition mode, all data that are not in acquisition or track modes are discarded.

All tracking and acquisition returns have to meet two initial tests to determine if the waveform actually represents the initial return, or if the return is outside the tracking window.

- 1) The counts in the first gate must be less than 100:
- 2) There must be at least one gate with a count value greater than 25.

#### 2.1.2 Categorizing the Returns

The remaining returns are then categorized into two groups. Group one will be referred to as specular and consists of those returns that display a sharp spike. Returns in this category are usually found in regions of sea ice or over flat, desert-type surfaces. The second group, consisting of the remaining returns, is called diffuse and resembles ocean returns. These returns are found over continental ice and the ice shelves. Different methods are used to retrack each group.

Returns are automatically categorized as either diffuse or specular depending on the existence of a significant spike in the return. To determine this the following algorithm is used. The noise level, Yn, is calculated as the average number of counts in the first five gates. The maximum, Ymax, is calculated as the maximum number of counts in any gate. The value Ymed is then calculated using the equation

$$Ymed = \frac{(Ymax-Yn)}{2.0} + Yn .$$
(2.3)

The gate number, Gmid, is then found as the first gate where the number of counts exceeds Ymed. Two sums of consecutive counts from the signal are then formed, Ylow and Yhigh, where

$$Ylow = \sum_{i=Gmid+9}^{i=Gmid+9} (2.4)$$

$$Ylow = \sum_{i=Gmid+20}^{i=Gmid+20} (2.5)$$

$$Yhigh = \sum_{i=Gmid+10}^{i=Gmid+10} (2.5)$$

If Gmid is so large that there are less than 20 remaining gates, then the number of gates used to form the sums is adjusted. When the ratio of Yhigh/Ylow is  $\leq 0.7$ , the return is considered specular.

#### 2.1.3 Retracking Specular Type Returns

Specular waveforms are not found in the Seasat altimeter data over Greenland. This is probably due to the absence of sea ice near Greenland during Seasat's lifetime. As a result, all of the Greenland returns are retracked using the diffuse method. However, for the sake of completeness, the method used to retrack specularly shaped returns, which is employed in the region of the Antarctic, will be discussed.

Specular-type returns are defined for this procedure as being characterized by one or more extremely sharp spikes and are retracked by attempting to locate the mid-point or halfpower point of the first significant spike. In addition, since the shape of the return essentially records topographic characteristics, parameters are also calculated which define the shape of a single-or double-peak return. Figure 5a shows the five-parameters required to define a singlepeak return, while Figure 5b shows the nine-parameters required for a double-peak return. 2.1.3.1 Half-power Point of First Significant Peak

In determining the mid-point of the first significant spike, the location of this spike must first be found. The value of Ymed, which is calulated to determine whether or not the return is specularly shaped (Equation 2.3), is used. Starting with the gate number prior to Gmid, where Gmid is define to be the gate number whose counts exceed Ymed, a gate is sought whose counts exceed or equal 25% of the difference between Ymax and Yn. Upon finding this gate, Grise, it is determined to be the first significant spike if the following conditions are met:

$$Y_{Grise+1} - Y_{Grise} < 0.$$
 (2.6)  
for  $Y_{Grise} > Y_{max} * .3$ 

where

$$Y_{Grise}$$
 is the counts for gate Grise, and  
 $Y_{Grise+1}$  is the counts for gate Grise+1.

Smaller, more rounded waveforms, which might be encountered in the vicinity of an ice shelf, require that the following condition be met:

$$Y_{Grise+1} - Y_{Grise} < (Ymax-Yn) * .05$$
for  $Y_{Grise} \le Ymax * .3$ .
$$(2.7)$$

Grise is incremented by one, up to the maximum number of gates, until one of the above conditions is met, after which the gate of the first significant spike, G1st, and its corresponding counts, Y1st, are used to determine the half-power point of the peak. The count value at the half-power point, Ymid1, is determined as follows:

$$Ymid1 = \frac{(Y1st-Yn)}{2.0} + Yn .$$
 (2.8)

The exact gate location of the half-power point, Gtmid1, is then determined by performing a linear interpolation for the count value Ymid1 located between gates X1 and X2, with corresponding count value Y1, Y2.

# 2.1.3.2 Remaining Parameters to Define Shape

In order to define the exact shape of the specular returns depicted in Figures 5a and 5b, it is necessary to calculate several other parameters in addition to the noise level, the maximum counts of the first significant peak, and the gate location of the half-power point. For the single-and double-peak return, additional quantities which define the width of the significant peak and slope at the half-power point are defined. A double-peak return has four additional quantities calculated: the maximum counts for the second significant peak, the gate location of the half-power point, and the minimum counts found between the two significant peaks.

The slopes at the half-power point for both the first and second significant peaks, Slp1st and Slp2nd, are determined by the following algorithm:

Slp1st = 
$$\frac{Y2 - Y1}{X2 - X1}$$
 (2.9)

Slp2nd uses the gate locations and corresponding counts determined to surround the half-power point of the second significant peak. These values are found in a manner similar to that of the first peak.

The actual existence of a second significant peak is determined in the following manner. Starting with the gate location of the first significant peak, the difference between counts of consecutive gates is monitored. As soon as the change in successive gates becomes negative, at gate location Gentmin, it is assumed that another peak has been encountered. At this point, a sum if formed, Totup, which totals the counts in all gates following the Gentmin. When Totup equals or exceeds 9% of Y1st then the second peak is considered significant. The gate at which the second peak occurs, X2nd, is determined to occur when the difference in the counts of consecutive gates becomes positive.

The counts at the second significant peak, Y2nd, are then used in the following manner to calculate the counts at the half-power point of the second peak, Ymid2:

$$Ymid2 = \frac{(Y2nd-Cntmin)}{2} + Cntmin .$$
 (2.10)



.....

Figures 5a and 5b. Specularly Shaped Waveforms

Again, a linear interpolation is performed in a manner identical with the first significant peak to determine the exact gate location of the second significant peak half-power point, Gtmid2.

The final parameter to be determined is the total width of the peak or peaks at the first half-power point. The width is defined as the number of gates between Gtmid1 (Section 2.1.3.1) and the location, Gtrail, where the trailing edge passes through Ymid1 (Equation 28). The width is computed as follows:

$$Width = Gtrail - Gtmid1 \quad . \tag{2.11}$$

In summary, the parameters for a specular return with a single significant peak arc as follows:

$$\beta_{1} = Yn$$

$$\beta_{2} = Y1st$$

$$\beta_{3} = Gtmid1 \qquad (2.12)$$

$$\beta_{4} = Slp1st$$

$$\beta_{5} = Width.$$

The parameters for a specular return with double significant peaks are as follows:

$$\beta_{1} = Yn$$

$$\beta_{2} = Y1st$$

$$\beta_{3} = Gtmid1$$

$$\beta_{4} = Slp1st$$

$$\beta_{5} = Y2nd$$

$$\beta_{6} = Gtmid2$$

$$\beta_{7} = Slp2nd$$

$$\beta_{8} = Width$$

$$\beta_{9} = Cntmin.$$
(2.13)

## 2.1.4 Retracking Diffuse-Type Returns

The method used to retrack the diffuse return is to model the return with a function that has the retracking position (the mid-point of the leading edge) as a parameter. The Bayesian leastsquares method (Ref. 8) is used to solve for the parameters of the function that best fit the return. For this method, initial estimates of the parameters must be provided. Weights are given to these initial estimates that designate how well each parameter is known relative to the others. Residuals are then calculated between the return value and the function value at each gate. These residuals are weighted based on their proximity to the mid-point of the leading edge position. A minimum to the sum of these squared weighted residuals is sought by an iterative method which simultaneously adjusts all of the function parameters. The process is repeated until convergence or until the maximum number of iterations is reached. Because linear methods are used to solve a non-linear problem the procedure can be numerically unstable. Checks are done to assure the reasonableness of the results. The key to making this method function correctly is in the choice of the initial estimates and weighting functions.

The theory of solving for the function parameters using Bayesian least-squares can be found in Ref. 8. The actual equations used will be presented here without justification.

Given an overdetermined set of equations MX=R where

$$M = \text{ the matrix of partials} \begin{bmatrix} \frac{\partial c_1}{\partial \beta_1} & \dots & \frac{\partial c_1}{\partial \beta_n} \\ \vdots & \vdots & \vdots \\ \frac{\partial c_m}{\partial \beta_1} & \dots & \frac{\partial c_m}{\partial \beta_n} \end{bmatrix}$$
(2.14)  
$$m > n$$

$$\mathbf{x} = \text{column vector} = \begin{bmatrix} \beta_{c1} & -\beta_{1} \\ & \cdot \\ & \cdot \\ & \beta_{cn} & -\beta_{n} \end{bmatrix}$$
(2.15)

$$R = \begin{bmatrix} m_{l} & -c_{l} \\ & \ddots \\ & \ddots \\ & m_{m} & -c_{m} \end{bmatrix}$$
(2.16)

and

 $m_i = observed$  value (counts at t=gate i),

 $c_1 = calculated$  values of  $m_i$  based upon a given set of parameters  $\beta$ ,

 $\beta_1$  = current best estimate of the model parameters  $\beta$ ,

 $\beta_{cj}$  = corrected best estimate of the model parameters  $\beta$ ,

- i = gate number (0 59), and
- n = number of parameters in the function.

We can then define a weight matrix, W

$$W = \begin{bmatrix} wt_{i} & 0 \\ . & . \\ . & . \\ 0 & . \\ 0 & wt_{m} \end{bmatrix}$$
(2.17)

where  $wt_i$  is the weight associated with each observation i.

If we multiply both sides of the equation by W we get

$$WMX = WR$$
.

Multiplying through by M<sup>T</sup> gives

$$\mathbf{M}^{\mathrm{T}}\mathbf{W}\mathbf{M}\mathbf{X} = \mathbf{M}^{\mathrm{T}}\mathbf{W}\mathbf{R} . \tag{2.18}$$

The solution of X is solved for as

 $\mathbf{X} = [\mathbf{M}^{\mathrm{T}}\mathbf{W}\mathbf{M}]^{-1} \quad \mathbf{M}^{\mathrm{T}}\mathbf{W}\mathbf{R}$ (2.19)

where  $M^TWM$  is referred to as the normal matrix. To add information as to the validity of the current best estimate of the model parameters the a priori covariance matrix  $V_0$  is included

$$V_{o} = \begin{bmatrix} wt_{\beta 1} & 0 \\ \vdots & \vdots \\ 0 & wt_{\beta n} \end{bmatrix}$$
(2.20)

where  $wt_{\beta j}$  = weight associated with the a priori value of parameter j. This matrix is then added to the normal matrix before it is inverted so the equation becomes

$$X = [M^{T}WM + V_{o}]^{-1} M^{T}WR.$$
 (2.21)

X then is the vector giving the new best estimate of the  $\beta$  parameters.

#### 2.1.4.1 The Function Representing the Altimeter Return

It has been shown (Miller and Brown, 1974) that the mean return waveform over a Gaussian surface can be mathematically described using the function

$$c(t) = \beta_1 + \beta_2 * P(W)$$
 (2.22)

where

W

$$P(W) = \int_{-\infty}^{-\infty} Z(q) \, dq \qquad (2.23)$$

$$Z(q) = \frac{1}{\sqrt{2\pi}} \exp\left(\frac{-q^2}{2}\right)$$
(2.24)

$$W = \frac{t-\beta_3}{\beta_4} . \tag{2.25}$$

This assumes that the pointing angle errors have negligible effects on the waveform shape. This also represents the ice sheet waveforms very well if it is modified to include a slope to the trailing edge. The modified function used to represent the diffuse-type waveforms is chosen as

$$c(t) = \beta_1 + \beta_2 (1 + \beta_5 Q(x)) P (W)$$
 (2.26)

where

$$Q(x) = 0 \text{ for } t < \beta_3 + 0.5 \beta_4$$
  
= t-x for t >  $\beta_3 + 0.5 \beta_4$ 

This is plotted in Figure 6a where

(a) Single-Ramp Function



 $\beta_4$  and  $\beta_7$  are risetime parameters for the 1st and 2nd ramp respectively

Where 
$$y = \beta_1 + \beta_2' P \frac{(t - \beta_3)}{\beta_4} (1 + \beta_9 Q(x_1)) + (\beta_5 P \frac{(t - \beta_6)}{\beta_7} (1 + \beta_3 (Q(X_2)))$$
  
 $X_1 = t - \beta_3 - 0.5 \beta_4 \qquad Q(x) = 0 \text{ for } x < 0$   
 $X_2 = t - \beta_6 - 0.5 \beta_7 \qquad = 1 \text{ for } x \ge 0$   
 $P(z) = \int_{-\infty}^{z} \frac{1}{\sqrt{2\pi}} \exp(-q^2/2) dz$ 

Figures 6a and 6b. Diffusely Shaped Waveforms

 $\mathbf{x} = \boldsymbol{\beta}_3 + 0.5 \, \boldsymbol{\beta}_4 \quad .$ 

The partials of this function with respect to each parameter are

$$\frac{\partial \mathbf{c}}{\partial \beta_1} = 1.0 \tag{2.27}$$

$$\frac{\partial c}{\partial \beta_2} = P[W] + \beta_5 Q P[W]$$
(2.28)

$$\frac{\partial c}{\partial \beta_3} = -\beta_2 \left\{ \frac{(1+\beta_5 Q)}{\beta_4} \frac{\partial P}{\partial W} + P(W) \beta_5 \right\}$$
(2.29)

$$\frac{\partial c}{\partial \beta_4} = \beta_2 \left\{ \frac{(1+\beta_5 Q)}{\beta_4} \frac{\partial P}{\partial W} W + \beta_5 \frac{P(W)}{2} \right\}$$
(2.30)

$$\frac{\partial c}{\partial \beta_5} = \beta_2 Q P[W] \tag{2.31}$$

where

$$\frac{\partial P}{\partial W} = \frac{1}{\sqrt{2\pi}} \exp \left(\frac{-W^2}{2}\right).$$

The value of  $\beta_3$  is the mid-point of the leading edge, Gm. As previously noted, some of the returns display multiple leading edges. A nine-parameter function is used to represent these returns, where the mid-point of the first leading edge is still  $\beta_3$ . The mid-point of the second leading edge,  $\beta 6$ , probably represents a return from another surface in the footprint and is being stored for future use. The nine-parameter function is

$$c(t) = \beta_1 + \beta_2 P(W_1) (1 + \beta_9 Q(x_1)) + \beta_5 P(W) (1 + \beta_8 (Q(x_2)))$$
(2.32)

This is plotted in Figure 6b where

$$x_1 = t - \beta_3 - .5 \beta_4$$
  
 $x_2 = t - \beta_6 - 0.5 \beta_7$ 

$$W_1 = \frac{t - \beta_3}{\beta_4}$$
$$W_2 = \frac{t - \beta_6}{\beta_7}$$

The partials of this nine-parameter function are

$$\frac{\partial c}{\partial \beta_1} = 1.0 \tag{2.33}$$

$$\frac{\partial c}{\partial \beta_2} = P(W_1) [1+\beta_9] Q_1$$
(2.34)

$$\frac{\partial c}{\partial \beta_3} = -\beta_2 \left[ \frac{(1+\beta_9 Q_1)}{\beta_4} \frac{\partial P}{\partial W_1} + P(W_1) \beta_9 \right]$$
(2.35)

$$\frac{\partial c}{\partial \beta_4} = -\beta_2 \left[ \frac{(P(W_1)\beta_9}{2} + \frac{(1+\beta_9Q_1)}{\beta_4} - \frac{\partial P}{\partial W_1} W_1 \right]$$
(2.36)

$$\frac{\partial c}{\partial \beta_5} = 1 + \beta_8 Q_2 P(W_2) \tag{2.37}$$

$$\frac{\partial c}{\partial \beta_6} = -\beta_5 \left[ P(W_2) \beta_8 + \frac{(1+\beta_8 Q_2)}{\beta_7} \frac{\partial P}{\partial W_2} \right]$$
(2.38)

$$\frac{\partial c}{\partial \beta_7} = -\beta_5 \left[ \frac{(1+\beta_8 Q_2)}{\beta_7} W_2 \frac{\partial P}{\partial W_2} + \frac{P(W_2)}{2} \beta_8 \right]$$
(2.39)

$$\frac{\partial c}{\partial \beta_8} = \beta_5 Q_2 P(W_2)$$
(2.40)

$$\frac{\partial c}{\partial \beta_9} = \beta_2 Q_2 P(W_1) . \qquad (2.41)$$

# 2.1.4.2 Setting the Initial Estimates for the Parameters

Initial estimates of each parameter are calculated from each individual return. To calculate these the general shape of the waveform is mathematically described by defining a mean slope and average value (bias) for every whole gate. For gates 4 through 56, the mean slopes and biases correspond to a straight line that is fit using least-squares minimization through the gate in question and the six surrounding gates. The biases for gates 1 through 4 are taken as the gate values and the slopes are defined as zero. For gates 57 through 60 the biases are the gate values and the slopes are defined as the slope calculated for gate 56. This set of slopes and biases is then interrogated to determine the locations of the leading edges and how many occur in the waveform.

The conditions required for a leading edge at gate Ir are:

- The Slope(Ir) must be greater than a given value, Thsl. A value of Thsl=0.5 count/gate is used to find the first leading edge, for succeeding leading edges Thsl is set to 1.0 count/gate. These numbers were chosen by visually and mathematically evaluating many typical ice sheet waveforms to determine when a leading edge designating a valid return could be perceived.
- 2) The Slope(Ir) must be a relative maximum, ie:

Slope(Ir) > Slope(Ir-1)Slope(Ir) > Slope(Ir+1). 3) There must be a significant increase in counts after the leading edge compared with that before the leading edge, i.e.:

Bias(Ir+3)-Bias(Ir-3) > Thbs

where

Thbs = 13.5 counts for first leading edge

- = 20.0 counts for succeeding leading edge.
- 4) If there was a leading edge already detected within 3 gates of Ir then the location is taken as that with the larger slope.

The initial estimates of the function parameters are then calculated from the position of the leading edge(s) and the Slopes and Biases. The five-parameter function (2.26) is used when only one leading edge is found, the nine-parameter function (2.32) is used when two or more leading edges are found.

Initial estimates,  $\beta_1^0$ , and the corresponding standard deviations of these estimates, Sig(1) through Sig(5), for the five-parameter function are defined as:

$\beta_1^{\rm o}$	=	Bias(4) (counts)	Sig(1)	-	0.01 (count)	
$\beta_2^{\rm o}$	=	Bias(Ir+3)–Bias(4) (counts)	Sig(2)		10.0 (counts)	
$\beta_3^{0}$	=	Ir (gate)	Sig(3)	=	.1 $\beta_0(4)$ (gates)	
$\beta_4^0$	=	${[Bias(Ir+3)-Bias(Ir-3)]/}$	Sig(4)	=	.01 $\beta_0(4)$ (gates)	
		Slope(Ir)}*0.5 (gate)				
$\beta_5^{\rm o}$		0.0 (count/gate)	Sig(5)	=	.01 (count/gate).	
Ŭ						(2.42)

Initial estimates and the corresponding standard deviations for the nine-parameter function are defined as:

$\beta_1^{\rm o}$	=	Bias(4) (counts)	Sig(1)	=	.01 (count)	
$\beta_2^{\rm o}$	=	Bias(Ir1+3)-Bias(4) (counts)	Sig(2)	=	0.1 (count)	
$\beta_3^{\rm o}$	=	Ir1 (gates)	Sig(3)	=	.05 $\beta_{\rm o}(4)$ (gates)	
$\beta_4^{\rm o}$	=	{[Bias(Ir1+3)-Bias(Ir1-3)]/ Slope(Ir1)}*0.5 (gates)	Sig(4)	=	.005 $\beta_0(4)$ (gates)	
$\beta_5^{o}$	=	Bias(Ir2+3)–Bias(Ir1+3) (counts)	Sig(5)	=	0.1 (count)	
$\beta_6^{\rm o}$	=	Ir2 (gates)	Sig(6)	=	.05 $\beta_0(7)$ (gates)	
β°7	=	{[Bias(Ir2+3)–Bias(Ir2–3)] Slope(Ir2)} (gates)	Sig(7)	=	.005 $\beta_0(7)$ (gates)	
$\beta_8^{\rm o}$	=	0.0 (count/gate)	Sig(8)	=	.01 (count/gate)	
$\beta_9^{\rm o}$	=	0.0 (count/gate)	Sig(9)	=	.01 (count/gate)	
						(2.43)

#### where

Ir1 is the predicted gate corresponding to the mid-point of the first leading edge

Ir2 is the predicted gate corresponding to the mid-point of the second leading edge.

2.1.4.3 Calculating the Weight Matrix, W

The weight associated with each observation,  $wt_{i}$ , is selected to optimize the fit in the vicinity of the leading edge.

$$wt_1 = 1 + K_1 * [exp (K_2) + K_3]$$
 (2.44)

where

 $K_1 = (I_{ter} - 1) * 0.5$ 

I<sub>ter</sub> = iteration number

$$K_2 = T_c + 0.5$$

- = Min ( $K_2$ , 60)
- = Max (K<sub>2</sub>, 1)

 $T_c = X_1 - \beta_3 - Max (5.0, \beta_4)$  for 5-parameter function

- =  $X_1 \beta_6$  Max (5.0,  $\beta_7$ ) for 9-parameter function
- $X_1$  = gate number of the ith observation

for the five-parameter function

$$K_3 = 0 \text{ for } |T_c| \ge 2.0$$
  
= 1 for  $|T_c| < 2.0$ 

for the nine-parameter function

$$K_3 = 0 \text{ for } |T_c| \ge 5.0$$
  
= 1 for  $|T_c| < 5.0$ .

2.1.4.4 Calculating the Covariance Matrix,  $V_o$ 

A priori values of  $V_0$  are calculated from the sigmas in equations (2.42) and (2.43) as follows:

$$w_{t_{\beta_{j}}} = w \text{scale/Sig(j)}^{2}$$
(2.45)  

$$w \text{scale} = 1 + .6 * \text{K} * \text{H1/3/(120*g2m)}$$
(2.46)  

$$H1/3 = 1.875 * \beta_{4}$$
  

$$K = 4$$

Using the function, w scale, causes the initial estimate information to have a greater effect on the solution when the rise time is large.

After each iteration, n, the values of Sig(3), Sig(4) and K are altered as follows:

$$Sig(3) = Sig(3)_{n-1} * 0.1$$

 $Sig(4) = Sig(4)_{n-1} * 10.0$ 

$$K = K_{n-1} + .5$$
 .

This has the effect of weighting the current best estimate of the leading edge position more and the rise time of the leading edge less. This has proven to speed up convergence.

# 2.1.4.5 Method of Iteration

An interative scheme is used starting out with the initial estimate of the  $\beta$  parameters. The Bayesian least-squares method is then used to solve for another set of  $\beta$  parameters that better fits the data. Iterations are performed always using the current set for the best estimate until  $\Delta H_{ret}$ , as calculated from  $\beta_3$  (2.1), converges to within 10 cm or the number of iterations exceeds 7.

Each succeeding set of  $\beta$  parameters is checked for reasonableness using these criteria:

$$\begin{array}{l} 0.0 < \beta_2 \\ 0.0 < \beta_3 < 60.0 \\ 0.0 < \beta_4 \\ \beta_3 < \beta_6 < 60.0 \\ 0.0 < \beta_7 \ . \end{array}$$

If any of the criteria fail, then the fit is considered unsuccessful and the waveform is discarded.

After convergence or the maximum number of iterations is reached, tests are then made to assure that the values reasonably represent the return. The rms of the residuals between the waveform and the function for the portion of the waveform from gate zero to just past the top of the leading edge is calculated.

$$RMS_{E} = \frac{\frac{Iedit}{\sum} (C_{1} - m_{1})^{2}}{\frac{i=1}{Iedit}}$$

where

Iedit =  $\beta_3$  + 0.5  $\beta_4$  for the five-parameter function =  $\beta_6$  + 0.5  $\beta_7$  for the nine-parameter function.

If  $RMS_E$  is greather than 20.0 counts then the fit is unacceptable. If the nine-parameter function is being fit and the process is unsuccessful, then the initial estimates are reset to

coincide with the initial estimates for the first leading edge and a five-parameter fit is tried. If problems occur during the five-parameter fit, the initial estimates are altered so that the leading edge position is taken as the gate,  $I_r$ , where Slope ( $I_r$ ) (as defined in Section 2.1.4.2) is a maximum for the waveform. If the fit is still unsuccessful, then the waveform is discarded.

The procedures explained here and the numerical values given yield the best results to date. Wherever possible values were chosen based on theory, but many times trial and error was necessary. At the time the Seasat Greenland data were processed, the procedures and numerical values differed slightly. There was no  $RMS_E$  check as explained in the last part of Section 2.1.4.5, nor were the initial parameter values altered if an unsuccessful fit was made. The variables that were different and their values for the Greenland processing were:

Thbs = 5.0 counts for the first leading edge = 10.0 counts for the second leading edge

Sig(3) =  $\beta_0(4)$  (for the five-parameter function)

$$Sig(4) = 0.1 \beta_0(4).$$

A direct consequence of these differences was that the entire Greenland data set had to be visually reviewed to assure that the fit adequately represented the data. This resulted in approximately 1% of the data being discarded which would not have been rejected using newer methods. The newer methods described here identify these problems automatically.

## 2.2 SENSOR-RELATED CORRECTIONS

After the ice altimeter data are edited and retracked, the precise orbits from NASA/GSFC (PGS-S4) are used to calculate the measured ice sheet elevation above the ellipsoid (Lerch et al., 1982). Corrections are then applied to correct for sensor-related biases.

Both the time tag and center of gravity corrections are calculated using the algorithms released by JPL (Lorell, 1979). These are summarized below.

#### 2.2.1 Time Tag Correction

The SDR time tag,  $t_{SDR}$ , is corrected for a track mode correction and a signal travel time correction so that the resultant data time, t, refers to the time of signal reflection from the ice sheet.

 $t = t_{SDR} - 0.0794 + H/c$ 

where

- c =  $2.99792458 \times 10^8$  m/sec, H = spacecraft altitude in meters, and
- 0.0794 is the track mode correction in seconds.

# 2.2.2 Center of Gravity Correction

The correction applied to make the spacecraft center of gravity the height reference point is

$$\Delta H_{cg} = Z_{cg} - Z_{cone}$$
(2.48)

where

- $Z_{cg}$  = the distance from the altimeter base plate to the spacecraft center of gravity. This varied during the flight due to maneuvers. Table S-07 of Lorell (1979) is used to obtain  $Z_{cgr}$
- $Z_{cone} = -1.238$  m which is the sum of the distance from the feed flange on the antenna to the base plate and a distance corresponding to a time bias in the electronic circuitry.

This correction is located in bytes 49-52 of the IDR.

# 2.3 ATMOSPHERIC CORRECTIONS

The measurements are corrected for ionospheric and tropospheric refraction using parameters supplied by JPL on the GDR's (Lorell et al., 1980).

## 2.3.1 Ionosphere Correction

The ionosphere correction for the ice data,  $\Delta H_{ION}$ , is calculated by linearly interpolating from the ionosphere corrections on the GDR's. Bytes 57-60 on the IDR contain the value of this correction. A detailed description of the algorithm used is given in Lorell et al., (1980).
#### 2.3.2 Troposphere Correction

The wet tropospheric correction is calculated using the following equations explained in Lorell et al., (1980).

$$\Delta H_{\text{TROP}_{\text{WET}}} = 2.277 * 10^{-3} * E_{0} (1.25503 / T_{\text{K}} + 0.5)$$
(2.49)

where

$$E_{o} = 6.11*H_{R}*10^{(7.5*T_{K}-273.16)/(T_{K}-35.86)}$$

T<sub>K</sub> is the surface temperature calculated by assuming a linear temperature profile with boundary conditions:

at sea level 
$$T_{K} = 2.73.0K$$

at 3200m above sea level  $T_{K} = 243.0K$ , and

 $H_R$  is the relative humidity (assumed to be 100% over the ice sheet).

The dry tropospheric correction is calculated from the equation

$$\Delta H_{\text{TROP}_{\text{DRY}}} = 2.277*10^{-3}*\{P* [1.0+0.0026*\cos(\phi)]\}$$
(2.50)

where

 $\phi$  = subsatellite latitude,

 $P = P_0 * (1.0-1.1138*10^{-4} * Ht),$ 

 $P_0$  – is the atmospheric pressure interpolated from the GDR's, and

Ht - is the ice sheet elevation above sea level in meters.

The total height correction due to the troposphere is

$$\Delta H_{\text{TROP}} = \Delta H_{\text{TROP}_{\text{WET}}} + \Delta H_{\text{TROP}_{\text{DRY}}}$$
(2.51)

The troposphere correction may be found in bytes 53-56 of the IDR.

#### 2.4 SURFACE DYNAMIC CORRECTIONS

The solid earth tides are computed by linearly interpolating their values from the GDR's. The resultant interpolated value may be found in bytes 83-84 of the IDR.

#### 2.5. ORBITAL CORRECTIONS

The NASA/GSFC PGS-S4 orbits which are used to improve the height measurements, have rms radial errors of 1.5 m. In an effort to reduce the radial error of these orbits, a technique was devised to further improve the orbit accuracy by referencing the orbits to a common ocean surface. Previous attempts to adjust the orbits using crossover minimization techniques with the ice sheet crossovers proved unsuccessful due to extreme segmentation of the data (see Figure 2). The new technique is not dependent upon the ice data but upon ocean altimetry, and utilizes the smoothed Seasat 84306 global ocean surface (Marsh et al., 1986). Through crossover minimization techniques the radial orbit error for the 84306 ocean surface has been reduced to 11 cm in the open ocean areas.

The method involves obtaining the residuals between the Seasat ocean data for passes which traverse Greenland, and the smoothed 84306 ocean surface. Using least-squares minimization, these residuals are then fit to a linear or quadratic function depending on the proximity of the data to Greenland. The function is, in turn, interpolated or extrapolated to determine the value of the orbit adjustment over Greenland which is to be subtracted from the surface height. This function is of the following form:

$$f(t) = C_0 + C_1 \Delta t + C_2 \Delta t^2$$
(2.52)

where

- $C_0, C_1, C_2$  are the coefficients of the fit where the units are meters, meters/fractions of a day and meters/(fractions of a day)<sup>2</sup>, respectively, and
- $\Delta t$  is the time from the start of the pass in fractions of a day.

Since this method attempts to adjust for orbit error only, the ocean data which are used must have all sensor, atmospheric, and surface dynamic corrections applied. The ocean data used in the adjustment are obtained from the Seasat Geophysical Data Records (GDR's), as corrected by JPL (Lorell et al., 1980).

Since the orbit error is strongly periodic, with a dominant frequency of two cycles per one revolution, only data from the northern hemisphere need to be used in computing the orbit adjustment over Greenland.

The distribution of the data affects the way in which the residuals are fit. To aid in categorizing the distributions of data, the northern hemisphere is subdivided into five ocean regions: 1) the area to the east of Greenland and within 1000 km. of the coast; 2) the area to the east of Greenland from 1000 km. from the coast to the Greenwich meridian; 3) the Indian Ocean; 4) the area to the west of Greenland between Greenland and North America; and 5) the Pacific Ocean (see Figure 7). The type of fit performed depends upon particular regions containing a minimum amount of data. If the criteria are not met, then no fit is performed.

Figure 7 summarizes the type of fit which is performed depending upon the region(s) in which data are found. An 'X' in regions 1, 2, 3 or 5 represents a minimum of 10 points, while region 4, due to its limited open ocean area, requires a minimum of 19 points. Linear fits are performed when data are found either very close to Greenland or are widely separated from Greenland. Quadratic fits are performed when the data are more evenly distributed over several regions.

After the coefficients for the fit are initially determined, outlying data which satisfy the following criterion are removed:

$$|H(t)-f(t)| \ge m * RMS$$
(2.53)

where

m is an integer editing multiplier,

RMS is the rms between the residual heights and the function f(t), and

H(t) is the surface elevation of the datum point.



Figure 7. Orbit Adjustment Regions and Effects of Data Distribution on the Orbit Adjustment Fit

(M	R I INIMUM I	TYPE OF			
1 (10)	2 (10)	3 (10)	4 (19)	5 (10)	L = LINEAR $Q = QUADRATIC$
X X X	x x x	x x x	x x x x	X X X X	L L L L Q Q Q Q Q Q

'X' INDICATES A REGION CONTAINING THE MINIMUM NUMBER OF POINTS

The remaining data are then used to solve for the function. This process is repeated until either the latest computed rms does not change by more than .02 m from the previous iteration, or 15 iterations are completed. In the case of the Seasat Greenland data, an editing multiplier of 4.0 is used with an initial rms of 20.0 m.

After solving for the coefficients and removing outliers, the function must satisfy a final test. For a linear function, the orbit adjustments are computed at the endpoints of the pass. If the absolute value of the orbit adjustment at either endpoint exceeds 3.0 m, then the function is not used. In the case of a quadratic function, the extremum of the function is first located. If the extremum is outside the endpoints of the data just fit, then the endpoints of the pass are checked as in the linear case. If the extremum lies between the endpoints, its value is checked. Again, a 3.0 m adjustment is deemed too large and if exceeded, an attempt is made to refit the data with a linear function. Of the 331 GDR passes for which an orbit adjustment was computed, 181 resulted in quadratic fits and 150 in linear fits. Of the 194 quadratic fits initially attempted, 12 failed the extremum test and were refit using a linear function. Of these, only one failed the endpoint test.

Two examples of results from the orbit adjustment procedure are shown in Figures 8 and 9. In the first case (Figure 8), data which are found in close proximity to Greenland are fit by a linear function. The latitude and east longitude of the points along the pass closest to the west and east coasts of Greenland are indicated. A linear function is fit to the smoothed ocean surface residuals. The orbit adjustment in the region traversing Greenland is indicated by dashes. Figure 9 shows the orbit adjustment results when a quadratic fit is necessary due to data being available just off Greenland's east coast and in the Pacific Ocean. The final rms between the data and function are 27 cm in the linear case and 14 cm the quadratic case.

Table 3 summarizes the orbit adjustments computed for each GDR rev at 310, 320, and 330 East Longitudes, representing the west coast, central region, and east coast of Greenland. Also included are the coefficients for the function (Equation 2.52) and the elapsed time in fractions of a day from the start point of the pass used to compute the adjustment for the longitude in question.

Utilizing Equation (2.52), the orbit adjustment is then computed for each Seasat IDR, and subtracted from the surface height. The orbit adjustment and its corresponding rms are located in bytes 93-96 and 97-100, respectively, of the IDR.



Figure 8. Orbit Adjustment Computed From Data in Close Proximity to Greenland's Coast





Application of the orbit adjustment to the data yields improved crossover results. When the differences in heights are computed at 1235 crossover locations for ascending and descending passes over Greenland, the resultant crossover residual mean of the data without the orbit adjustment is 33 cm with an rms of 1.15 m. After application of the orbit adjustment, the data give a crossover residual mean of 7 cm and an rms of 0.99 m.

### 2.6 SLOPE CORRECTION

The altimeter height is measured to the closest point within its footprint, which does not correspond to the subsatellite location for sloping surfaces. This effect introduces an error into the height measurement which can be corrected by adjusting either the value of the measurement or its location (Brenner et al., 1983). Upon examination of both techniques, the method which was chosen for the Seasat data is to adjust the measurement. The magnitude of the slope-induced error may be represented by:

$$\Delta H_{\text{SLOPE}} = H(1 - \cos \alpha) \tag{2.54}$$

where

- H is the satellite altitude in meters
- $\alpha$  is the maximum regional surface slope in radians

or

$$\Delta H_{\text{SLOPE}} = \frac{H\alpha^2}{2}, \text{ for small } \alpha. \tag{2.55}$$

The surface slope in Equation (2.55) for any one point is calculated using the following equation:

$$\alpha = \sqrt{\alpha} \frac{2}{\text{along-track}} + \frac{2}{\alpha} \frac{2}{\text{cross-track}}$$
(2.56)

where

 $\alpha_{\text{along-track}}$  is the slop

is the slope of the surface in the along-track direction of the data, and

 $\alpha_{cross-track}$  is the slope of the surface in the cross-track direction of the data, perpendicular to the along-track direction.

The cross-track slope is obtained by using a reference surface of Greenland, generated from the Seasat data. This surface consists of a two-dimensional grid of heights. The spacing between grid points is 20 km. Bilinear interpolation between these grid values is used to determine the heights at the points where the cross-track intersects the closest grid lines. From these heights, the cross-track slope is then determined.

The along-track slope is obtained using the available along-track data. Since the height profile is initially unknown, an iterative procedure is used to attempt a reconstruction of the true height profile. The initial along-track slope at a data point location is calculated by performing a linear fit to the five elevations of the along-track data points nearest the data point in question. A slope correction is then calculated for that point and each point in the pass using Equation (2.55), but applying only 25% of the correction to the elevations. This entire procedure is repeated using the revised elevations three more times, each time applying 25% of the current elevation correction. After the final iteration, the total along-track height correction and Equation (2.55) are used to calculate an "effective" along-track slope. This slope may then be used in Equation (2.56) along with the cross-track slope to calculate the total slope. In the case of both the along and cross-track slopes, a maximum of .8 degree is allowed. This is a limitation set by the physical characteristics of the altimeter.

If two points cannot be found on both sides of the point being adjusted, after having searched 10 km in both directions, then the reference grid which is used to calculate the cross-track slope is also used to determine the along-track slope in a manner equivalent to the cross-track slope calculation described above.

Slope corrections are not applied to the surface heights on the IDR's. However, the along-track and cross-track slopes, from which the slope correction may be computed, are stored in bytes 85-86 and 87-88, respectively. Bytes 89-90 contain the size of the window required to find the five points to perform the along-track linear fit. Bytes 91-92 give information pertaining to how the along-track and cross-track slopes were determined.

## 2.7 SUMMARY OF CORRECTIONS

In order to obtain a corrected surface elevation relative to sea level with the solid tide effects removed, the following algorithm is used.

$$H_{COR} = H_{SC} - H_{ALT} - \Delta H_{RET} - \Delta H_{CG} + \Delta H_{ION} + \Delta H_{TROP} - \Delta H_{TIDE}$$

$$-\Delta H_{ORB} - \Delta H_{SLOPE} - H_{GEOID}$$
(2.57)

where

H <sub>SC</sub>	is the height of the spacecraft above the ellipsoid,
H <sub>ALT</sub>	is the original altimeter measurement,
$\Delta H_{RET}$	is the retracking correction,
$\Delta H_{CG}$	is the center of gravity correction,
$\Delta H_{ION}$	is the ionospheric correction,
$\Delta H_{TROP}$	is the tropospheric correction,
$\Delta H_{TIDE}$	is the value of solid tide,
ΔH <sub>ORB</sub>	is the orbit adjustment,
$\Delta H_{SLOPE}$	is the slope correction, and
H <sub>GEOID</sub>	is the value of the geoid.

The surface elevation on the IDR is relative to the ellipsoid and is corrected for tropospheric and ionospheric effects, the center of gravity offset, the retracking correction, and the orbit adjustment when available. However, the elevation still contains solid tide effects, and the application of the slope correction or removal of the solid tides have been left to the discretion of the user. The surface elevation status word located in bytes 77-78 of the IDR should be checked to verify whether or not corrections have been applied.

Corrections which are applied to the altimeter measurement are done in the opposite sense from the surface elevation corrections and may be verified using the altimeter measurement status word in bytes 13-16 of the IDR.

An outline of the adjustments and corrections required to the Seasat data and their values or range of values is given in Table 4.

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## SECTION 3.0 WAVEFORM DATA RECORDS

The averaged radar return pulses contained in the SDR's are stored on a separate file called the Waveform Data Records (WDRs) to facilitate their use. Table 5 outlines in detail the format of this record.

The time, geographical position, and altimeter measurement on the WDRs are not identical to the corresponding records on the IDRs. This is due to the fact that the WDRs information is obtained directly from the SDR's without the application of any correction or adjustment of any kind. The time differs by the time tag correction described in Section 2.2.1. Positions on the WDR are from the orbits on the SDR's and not PGS-S4 orbits. The altimeter measurement represents the raw observation on the SDR without any of the corrections described in Section 2.7 applied.

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## SECTION 4.0 GEO-REFERENCED DATA BASE

Ordering the Seasat data merely by time presents certain limitations when only data in a particular locale are desired. This situation arises when data are used to generate a grid of smoothed surface heights. To circumvent this problem, a data base was developed which orders the Seasat data by geographical areas or "bins". Figure 10 shows the configuration of the 4,300 bins in the vicinity of Greenland. Bin sizes vary in order to compensate for the higher data density near Seasat's maximum latitude. Each bin is assigned a number starting with "1" in the southwestern-most corner. Bin numbers increment first from west to east and then from south to north. The ending bin number for each row is indicated in the right-most margin of the map in Figure 10, while the number of data points is printed within the appropriate bin. Bins which contain no data have no number entered. Table 6 summarizes the number of points and the rev numbers found in each bin, along with the geographical coordinates of the southwestern-most corner of the bin. The bin number in which a particular data point is located may be found in bytes 153-156 of the IDR.

The geo-referenced data base is a subset of the IDR's, containing only information relating to the position, rev number, surface height, slope correction and orbit adjustment for each data point. Slope correction and orbit adjustment values are flagged with a -9999, if unavailable. In addition, the data are ordered first by bin number and then by time within each bin. The surface elevations on this data set have the orbit adjustment applied where it was available. If the orbit adjustment was not available, (indicated by the orbit adjustment value for that record being set to -9999) then the surface elevation contains the value calculated from the unadjusted orbit. The slope correction has not been applied to any of the surface elevations.

The data base is designed to be used on a direct-access device, so that data from one or several bins may be accessed without the need to read all the records prior to the location desired. This is achieved by dividing the data base into three sections.

The first section of the data base, a header, consists of one logical record and gives a summary of its configuration: the locations of the corners of the data base, the number of latitudinal rows, the width in degrees of each of these rows, and the number of longitudinal divisions in each row. These pieces of information give the layout of the data base, as depicted in Figure 10. Information pertaining to the size of the data base, the starting record of the bin directory, and the corrections applied to the data are also contained in this header.

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BIN #4300-6 1.1 <u>ر ۲</u> 100 210  $i \sim i$ 1.18 .э. :43 219 94 1et :19 26 1, 8 22 :14  $| \infty$ : •c . 1 E 91 ..i -.L. 3.31 335. . Eb 1... и. 328. 144 54Ľ 333. 3.14. ÷Ψ 330 -98 329. 326 327. 2. 324 316 317. 3:8-319. 320. 321. 322. 323 315 3(4)

EAST LONGITUDE (DEGREES)

ORIGINAL PAGE IS OF POOR QUALITY **BIN NUMBER** 

Following the header are the altimetry data ordered by bin number and, within each bin, by time. The altimetry data are subdivided into two groups for each bin which contains data. The first subgroup consists of one logical record which indicates the number of data points contained in the bin. The second subgroup consists of the actual altimetry data (position, rev number, surface height, orbit adjustment and slope correction), with each record corresponding to a data point.

The final section is a bin directory which follows the altimetry data. The bin directory starts at the logical record indicated in the data base header. The directory contains an entry for each bin, and starting with the first bin, indicates the record number in the data base (not including the header record) at which the start of the data for a particular bin may be found. Bins which contain no data have a zero entered in the directory. Table 7 summarizes the structure of the data base in greater detail.

One use of the data base is to assist the gridding program (Section 5.0) in locating and accessing all data contained within a specified radius of a grid location. In addition, the data base may be used to locate data within any desired area. The following example demonstrates how this may be done. The limits of a desired area are used in conjunction with the header information to determine exactly which bin numbers contain the data. Using the southernmost latitude of the desired area, along with the width of the latitude rows, establishes the southernmost row which contains the data. Longitudinal limits of the desired area are then checked in conjunction with the size and location of the longitudinal divisions in that row. When the longitude limit of the desired area for that latitudinal group is exceeded, the process starts again with the next latitude row to the north. These steps are repeated until the northernmost boundary limit of the desired area is reached.

Equipped with the bin numbers which contain the data, the directory, which gives the logical record on the direct-access disk at which each bin begins, is read. If the directory value for the bin is non-zero, this logical record is then read to determine the number of records which follow and are contained in the same bin. The subsequent data is then read for each bin.

The uneven distribution of Seasat data presents problems when attempting to create computer generated contours. An intermediate step is useful which fits the data to nodes of a regular grid. Data local to each grid point are fit with a biquadratic or bilinear surface to determine the surface height at the grid point. This procedure is referred to as gridding the data. Grids are generated using the corrected and adjusted data in the geographical data base.

#### 5.1 POLAR STEREOGRAPHIC PROJECTION

Grids of the Greenland data are generated in a tangent polar stereographic projection where the plane of projection is located at the geographic North Pole (the projection latitude) and is normal to the earth's axis. This projection is conformal which results in equality of scale about a point. Figure 11a depicts the concept behind this type of projection. A straight line is drawn from the South Pole (pole of projection), through a point on the earth's surface, Q, to the projection plane which is tangent to the North Pole. The projection plane is in turn divided into square grids from the pole to the Equator with the North Pole at the center. Three projection parameters define the size and the orientation of the plane and the grid size:

- S a conversion factor from half-inch grids at the projection latitude to the desired grid size;
- $\phi_p$  the minimum latitude extent of the map perimeter for the projection latitude located at the North Pole; maximum latitude extent for the projection latitude located at the South Pole;
- G the Greenwich orientation in degrees

In the case of Greenland, where 20 kilometer grid cells were decided as being optimum for the data distribution, values of S=1.65,  $\phi_{\rm p} = 50^{\circ}$ , and G=45° were chosen.

These three parameters are sufficient to define a grid of the northern hemisphere, from the North Pole to 50° north latitude where the number of cells of desired size from the pole to the equator may be represented by:



Figures 11a and 11b. Polar Stereographic Projection of Point Q with Latitude  $\phi$  and Longitude  $\lambda$  onto Plane with Map Perimeter 50°

$$D = \frac{2R}{S \times 10^6}$$
(5.1)

where R is the radius of the earth measured in one half-inch grid cells and was chosen to be consistent with polar stereographic projections described in other documentation.

The integer number of grids of desired size from the pole to the map perimeter is:

$$N = D x \tan \frac{90 - |\phi_p|}{2} .$$
 (5.2)

The grid, defined by I and J axes, with the origin in the upper left corner (see Figure 11b), represents the coordinate of the North Pole as:

$$Ip = N + 1$$

$$Jp = N + 1.$$
(5.3)

Any point with latitude  $\phi$  and longitude  $\lambda$ , which is located in the northern hemisphere north of  $\phi_p$  is positioned at the following I, J coordinate:

$$I = INT [d x A x cos(X) + Ip + 0.5]$$

$$J = INT [d x sin(X) + Jp + 0.5]$$
(5.4)

where

d is  $D x \tan \frac{90 - |\phi_p|}{2}$ X is  $\lambda + G$ A is +1 if  $\phi_p \ge 0$ A is -1 if  $\phi_p < 0$ .

## 5.2 GRIDDING PROCEDURE

The surface height at each grid point location is calculated by fitting the surrounding data to the following biquadratic surface modeling function:

$$h_{ij}(\lambda,\phi) = C_{1_{ij}} + C_{2_{ij}} \left(\frac{\lambda - \lambda_i}{\text{capmin}}\right) + C_{3_{ij}} \frac{(\phi - \phi_j)}{(\text{capmin})(\cos\phi_j)}$$

$$+ C_{4_{ij}} \left(\frac{\lambda - \lambda_i}{(\text{capmin})}\right) \frac{(\phi - \phi_j)}{(\text{capmin})(\cos\phi_j)} + C_{5_{ij}} \frac{(\lambda - \lambda_i)^2}{(\text{capmin}^2)}$$

$$+ C_{6_{ij}} \frac{(\phi - \phi_j)^2}{(\cos^2\phi_j)(\text{capmin}^2)}$$
(5.5)

where

h<sub>ij</sub>

= value of the surface elevation function for the ij grid point as evaluated at the location  $(\lambda, \phi)$ ;

- $C_{1_{ij}} C_{6_{ij}} =$  numerically determined coefficients of the biquadratic function for grid point ij; and
- $\lambda_i \phi_j$  = longitude and latitude of the ij grid point in deg.

capmin = minimum cap size in deg longitude.

A weighted least-squares method is used to solve for the coefficients  $C_{1_{ij}} - C_{6_{ij}}$  at each grid point ij. The weighting is invoked to prevent the obliteration of the local surface details by the smoothing process, and to lend greater importance to the data closest to the grid point location. The form of the weighting function is

$$W_{k_{ij}} = \frac{1}{\sigma_{O_k D_{k_{ij}}}^2}$$
(5.6)

where

 $W_{k_{ij}} =$  weight of the k<sup>th</sup> data point used in determining the coefficients of the surface function for the ij grid location;

$$\sigma_{o_{\rm br}}$$
 = observation standard deviation of the k<sup>th</sup> data point;

N = power of inverse distance weighting; and

$$D_{k_{ij}}$$
 = the distance from the k<sup>th</sup> data point to location ij,

where 
$$D_{kij} = \{[(\lambda_k - \lambda_i) \cos \phi_k]^2 + (\phi_k - \phi_j)^2\}^{1/2}$$

The observation standard deviation was assigned a value of 1.0 m. The power of inverse distance weighting was assigned a value of 2.0 m. The formula used for the least-squares minimization in matrix notation is

$$P_{ij}^{T} W_{ij} P_{lj} C_{ij} = P_{ij}^{T} W_{ij} H_{lj}$$

$$(5.7)$$

or

$$C_{ij} = [P_{ij}^{T} W_{ij} P_{ij}]^{-1} P_{ij}^{T} W_{ij} H_{ij}$$
(5.8)

where

$$H_{ij} = \begin{bmatrix} h_{1} \\ \vdots \\ h_{k} \\ \vdots \\ h_{m} \end{bmatrix}$$

is the observational data set used in determination of grid point ij;

$$P_{ij} = \begin{bmatrix} \frac{\partial h_1}{\partial C_{1_{ij}}} & \frac{\partial h_1}{\partial C_{2_{ij}}} & \cdots & \frac{\partial h_1}{\partial C_{6_{ij}}} \\ \vdots & & \vdots \\ \frac{2h_m}{\partial C_{1_{ij}}} & \cdots & \cdots & \frac{2h_m}{\partial C_{6_{ij}}} \end{bmatrix}$$

is the matrix of observational partial derivatives;

$$\mathbf{C}_{ij} = \begin{bmatrix} \mathbf{C}_{1_{ij}} \\ \vdots \\ \mathbf{C}_{6_{ij}} \end{bmatrix}$$

is the set of coefficients for grid point;

$$W_{ij} = \begin{bmatrix} W_{1_{ij}} & 0 \\ & \ddots & \\ 0 & & W_{m_{ij}} \end{bmatrix}$$

is the observation weighting matrix.

A solution exists for Equation (5.8) if the determinant of the normal matrix  $B_{ij} = P_{ij}^T W_{ij}C_{ij}$  is positive. However, poor data distribution can cause ill-conditioned matrices yielding solutions that vary considerably from the expected results. One needs to be able to recognize when numerical problems occur to assure reasonable solutions. To this end the singular value decomposition (SVD) method is used to solve the matrix equation. The results of the SVD process give an indication of the stability of the equations and therefore whether a unique stable solution exists (Forsythe, Malcolm, and Moler, 1977). When the normal matrix  $B_{ij}$  is used as input to SVD, three output matrices are calculated:  $\Sigma$ , U, and V.  $\Sigma$  is a diagonal matrix, such that

$$\Sigma = \begin{bmatrix} \sigma_1 & & 0 \\ & & \\ 0 & & \sigma_6 \end{bmatrix}$$

where the  $\sigma$ 's are referred to as the singular values of B. The matrices U and V are used to transform the equations

$$Bc=y$$

into an equivalent diagonal set of equations

$$\Sigma \overline{c} = \overline{y}$$
.

In principle, if none of the  $\sigma$ 's are zero the transformed equations could be solved using

$$\overline{C}_{i} = \frac{\overline{y}_{i}}{\sigma_{i}}$$

In practice, when any of the  $\sigma$ 's are small, numerical instability can result, giving unreasonable answers. The key to using SVD is to set a tolerance  $\tau$  which reflects the accuracy of the data and the arithmetic used. If any  $\sigma$ 's are less than  $\tau$  times the largest  $\sigma$  then those corresponding

 $\overline{c}$ 's are not uniquely defined and unreasonable results can occur. When problems occur, steps must be taken to provide more information to evaluate the surface function.

Once  $\tau$  is chosen, then  $\Sigma$ , U, and V are used in the following manner to calculate each coefficient C<sub>1</sub>.

$$S = \sum_{\substack{j=1}}^{m} U(j,i) Y_{j}$$

for all j where  $\sigma_1 > \tau$ 

$$C_{l} = \sum_{k=1}^{n} \frac{S}{\sigma_{k}} V(i,k)$$

In this study the value of  $\tau$  used was .001 m. SVD is then used to determine when there are sufficient data to provide a unique solution to the surface modeling function. When a unique solution cannot be found more data are added and the function is reevaluated. At each grid location ij, data within the circular area defined by radius R from the grid location are used in the solution. Four different values for R are used: 33 km, 55 km, 88 km, and 132 km. Initially the smallest value of R is used and if a solution cannot be found then R is increased. If the biquadratic solution at the maximum value of R is unsatisfactory according to the SVD criterion, then the function (Equation 5.5) is reduced to a bilinear function by setting coefficients C4 through C6 to zero. If a valid solution still cannot be found, then the grid value is considered undefined and set to -1000.0.

Individual data point removal is also invoked during the gridding process. After finding a valid solution at location ij, the weighted rms of the residuals of the data with respect to the surface is calculated using



where

$$\operatorname{Res}_{kij} = h_k - h_{kij}$$

 $h_{kij}$  = height at location of measurement k evaluated using the surface function for grid location ij.

The following inequality is then evaluated for each data point used in the solution.

A value of the editing multiplier ( $E_{mult}$ ) equal to 3.5 is used and all data points that do not satisfy the inequality are deleted. When any data points are deleted the surface function is reevaluated using the remaining data. A minimum of 10 data points are required to solve for the function.

The standard deviation associated with the grid height,  $\sigma_{Gij}$ , is then calculated to determine how well the grid represents the data.

$$\sigma_{\rm Gij} = \rm RMS_{\rm WT_{ij}} \bullet (V_{11}ij)^{1/2}$$

where

$$V_{ij} = \begin{array}{cccc} B^{-1}P_{ij} W_{ij} \\ ij \end{array} \begin{bmatrix} \sigma_{o_1}^2 & 0 \\ & \ddots & \\ & \ddots & \\ & & \ddots & \\ & & \ddots & \\ & & & \sigma_{o_m}^2 \\ 0 \end{array} \end{bmatrix} \begin{bmatrix} B_{1j}^{-1} P_{1j}^T W_{ij} \end{bmatrix}.$$

Grid points that have a large value of  $\sigma_G$  do not represent the data as well as those that have smaller  $\sigma_G$ 's.

The format of the grid record is described in Table 8. The location, coefficients,  $\sigma_G$ , number of points used and other pertinent parameters are output for each grid point location. The user can utilize these parameters to decide the accuracy of the individual grid values.

TABLES

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## Table 1. Ice Data Record Description

General Characteristics:

Record Format	-	variable
Record Size (bytes)	-	164 + 4 for IBM record control word
Blocksize (bytes)	-	31920 + 4 for IBM block control word

The first seven records of the IDR data set are 80 bytes long and contain a brief description of the contents of the file. The remaining records follow the 164-byte format.

### HEADER RECORDS

<u>Bytes</u>	FORTRAN Variable <u>Type</u>	Description	
1-80	A1	Brief description of file contents. only)	(Comprises first seven records

#### DATA RECORDS

Bytes	FORTRAN Variable <u>Type</u>	Description
1-4	I*4	Satellite ID - This is the international satellite designation nnpppqq where:
		nn - last two digits of the year of launch (e.g., 1974 74, 1969 69).
		ppp - order of launch. Example: The 25th vehicle launch in a given year is designated with ppp = 025.
		qq - component identifier (e.g., component $a \rightarrow 01$ , component $\ell \rightarrow 12$ , etc.).
5-6	I*2	Measurement type 40-44 Altimeter height 40 = Long pulse (GEOS data) 41 = Short pulse (GEOS data) 43 = Seasat altimetry

<u>Bytes</u>	FORTRAN Variable <u>Type</u>	Description
7-8 I*2	I*2	Time system indicator (nm)
		n-valueDescription Tracking data times0Ground received time1Satellite transponder/reflector time2Ground transmitted time
		Altimeter data times1Transmitter time2Ground bounce time3Receiver time
		m-value         Description           0         UT-0           1         UT-1           2         UT-2           3         UTC           4         A.1           5         A.3 (A.T. B.I.H.)           6         A-S (Smithsonian)
9-12	I*4	Station Number (0 indicates altimeter)
13-16	I*4	Altimeter measurement status word
		The status word consists of bit switches packed into a single 32 bit word. The rightmost bit (bit 31) is of lowest order and the leftmost bit (bit 0) is of highest order.
		 031
		The status bits are configured as follows:
		BitsValueDescription0Unused
		1-2Format indicator for measurement types 40-41120 obs/frame232 obs/frame3320 obs/frame

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	FORTRAN Variable			
<u>Bytes</u>	<u>Type</u>	Descript	tion	
(13-16 Cont.)		<u>Bits</u>	<u>Value</u>	Description
		3	0 1	Net instrument corrections indicator Instrument corrections applied to observation Instrument corrections not applied
		4		Unused
		5-6	0 3	Speed of light indicator 2.997925x10 <sup>8</sup> meters/sec 2.99792458x10 <sup>8</sup> meters/sec
		7		Unused
		8	0 1	Solid tide indicator Solid tide not on data record Solid tide on data record
		9	0 1	Ocean tide indicator Ocean tides not included in total tides Ocean tides included in total tides
		10-11	0 1	Tropospheric correction indicator Total tropospheric correction not on data record Total tropospheric correction on data record
		12	0 1	Ionospheric correction indicator Ionospheric correction not on data record Ionospheric correction on data record
		13	0 1	Atmospheric corrections indicator Ionospheric and tropospheric corrections applied to observation if found on data record Ionospheric and tropospheric corrections not applied to observation if found on data record

	FORTRAN Variable			
<u>Bytes</u>	<u>Type</u>	Descript	tion	
(13-16 Cont.)		<u>Bits</u>	<u>Value</u>	Description
		14	0	Total tide indicator Solid and ocean tides removed from observation if found on data record
			1	Observation includes solid and ocean tides
		15	0	Center of gravity indicator Center of gravity correction applied to observation
			1	Center of gravity correction not applied to observation
		16-20		Unused
		21	0 1	Altimeter mode (GEOS only) Global track mode Intensive track mode
		22-27		Unused
		28	0 1	Location indicator Over water Over land
		29	0 1	Orbit adjustment indicator Orbit adjustment has been applied to observation Orbit adjustment has not been applied to observation
		30	0 1	Slope correction indicator Slope correction has been applied to observation Slope correction has not been applied to observation
		31	0 1	Retracking correction indicator Retracking correction has been applied to observation Retracking correction has not been applied to observation

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<u>Bytes</u>	FORTRAN Variable <u>Type</u>	Description
17-20	I*4	Modified Julian Date (MJD) of observation Julian Date = MJD + $2400000.5$
21-28	R*8	Fraction of day past midnight (GMT)
29-36	R*8	Altimeter range measurement in meters
37-40	R*4	Satellite latitude in degrees
41-44	R*4	Satellite east longitude in degrees
45-48	R*4	Measurement standard deviation in meters
49-52	R*4	Center of gravity correction in meters
53-56	R*4	Tropospheric refraction correction in meters
57-60	R*4	Ionospheric refraction correction in meters
61-64	R*4	GEM10-B geoid height above reference ellipsoid in meters
65-68	R*4	Total tide height above reference ellipsoid in cm.
69-72	I*4	Rev number
73-76	I*4	Surface height with respect to ellipsoid in cm.
77-78	1*2	Surface height status word

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<u>Bits</u>	<u>Value</u>	Description
0-8	0	Unused
9	1 0	Slope correction applied Slope correction not applied
10	1 0	Orbit adjustment applied Orbit adjustment not applied
11	1 0	Solid tides removed Solid tides not removed
12	1 0	Retracking correction applied Retracking correction not applied
13	1 0	Center of gravity bias applied Center of gravity bias not applied
	0	Center of gravity bias not applied

Bytes	FORTRAN Variable <u>Type</u>	<u>Bits</u>	<u>Value</u>	Description	
(77-78 COIII	., )	14	1 0	Tropospheric correction applied Tropospheric correction not applied	
		15	1 0	Ionospheric correction applied Ionospheric correction not applied	
79-80	I*2	Signifi	cant wave	height (H 1/3) in cm.	
81-82	I*2	Autom	Automatic Gain Control (AGC) in dB		
83-84	I*2	Solid t	ides in cm	1.	
85-86	I*2	Tangen	it of along	-track slope (x 10 <sup>5</sup> )	
87-88	I*2	Tangen	it of cross-	-track slope (x 10 <sup>5</sup> )	
89-90	I*2	Size of	Size of window used in obtaining along-track slope in meters		
91-92 I*2		Along-t zero, t comput	rack and c hen slope ted.	cross-track slope correction word. If all bits are so for slope correction were not able to be	
		 0		-  15	
		<u>Bits</u>	Value	Description	
		0-9		Unused	
		10	1	Along-track slope set to the maximum value of .8 degree during iterative procedure.	
		11	1	Cross-track slope set to the maximum value of .8 degree.	
		12	1	Along-track slope set to .8 degree after final iteration.	
		13	1	Window was extended to 20 km with no point found; reference grid used to calculate along-track slope.	
		14	1	Window had to be extended in both directions to determine along-track slope, but it is less than 20 km.	
		15	1	Two adjacent points were found and used to determine along-track slope.	
93-96	R*4	Orbit ad	ljustment (	to 84,306 ocean surface in meters	
97-100	R*4	RMS of orbit adjustment fit in meters			

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Bytes	FORTRAN Variable Type						
101-104	R*4	RMS of filtered fit in counts					
105-108	R*4	Timing bias in seconds					
109-144	R*4	Retracking parameters $\beta(1) - \beta(9)$					
145-148	R*4	Attitude information from SDR					
149-152	R*4	Correction to surface height if using leading edge of leading edge in meters					
153-156	I*4	Geographical data base bin number					
157-158	I*2	Standard deviation of 1st leading edge position in gates					
159-160	I*2	Standard deviation of 2nd leading edge position in gates					
161-162	I*2	Retracking status word					
		 0 15					
		<u>Bits</u>	<u>Value</u>	Description			
		0		Unused			
		1	0	Gains and offsets were not applied to waveform counts in plots and in determining $\beta$			
			1	Gains and offsets were applied to waveform counts in plots and in determining $\beta$ parameters			
		2	0	Specular test not performed or waveform not specularly shaped			
			1	Waveform determined to be specularly shaped			
		3	0	Status flag from SDR less than or equal to one			
			1	Status flag from SDR greater than one			
		4	0 1	Waveform not specularly retracked Waveform specularly retracked			
		5	0	Gains and offsets not applied to waveform count values on WDR's			
			1	Gains and offsets applied to waveform count values on WDR's			

<u>Bytes</u>	FORTRAN Variable <u>Type</u>	<u>Descript</u>	ion		
(161-162 Con	t.)	<u>Bits</u>	Value	Description	
		6	0 1	For double waveforms the retracking correction is not calculated from a weighted average of the two leading edges. For double waveforms the retracking correction is calculated from a weighted average of the two leading edges.	
		7	0 1	No problem with leading edge definition of waveform Waveform not defined well enough to filter, no leading edges or too many leading edges	
		8	0 1	No problem retracking Problem retracking	
		9	0 1	Timing bias was not applied to time tag Timing bias applied to time tag	
		10	0 1	Waveform not retracked Waveform retracked	
		11	0 1	Whole edge retracked Leading edge retracked	
	applies to water data	12	0 1	Ht correction not applied due to $\ddot{h}$ Ht correction applied due to $\ddot{h}$	
		13	0 1	Attitude seastate correction not applied to h Attitude seastate correction applied to h	
		14-15	0 1 2 3	Tracking mode 1 Tracking mode 2 Tracking mode 3 Tracking mode 4	
163-164	I*2	Version number of retracking program that converted the data from SDR to IDR format			
		$n_1 n_2 n_3 n_4 n_5$			
		$n_1 n_2 = \text{year of version}$			
		$n_3n_4 = \text{month of version}$			

 $n_5 = point no. of version$
		251	331	409 331	331	331	252	531	40 <del>0</del>	<b>531</b> 292	332	332	533	412	534	573	505	555	556	90	58	07	56
		52	16	70	52	52	53	. 19	20	225	33	33	56	73	50	54	20	10		22	- ·	24	07
		N N	8	ю н м	N M	8	2	Ñ N	M N	NN N <del>J</del>	м м	8	Ñ Ŧ	M t	10	0 M 	110	~~~	5				
	ICH	21:	29	52	25	25	21:	293	293	522	293	293	296	374	29	000		456	503	558	200	2020	
	ERSES	290 213	252	252 214	213	213	214	252	252	253 214	294	294	254	334	296	0.22 0.22 0.20	1410	1221	457	508	0.00	508	558 936
	TRAVI	330 291 173	253	253 174	174	214	174	253	253	213 175	254	800 800	255	294 294	256	562	3740	140	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	605	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	0.00	559 937
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		171 172 212 134	174	175	136	4 n 4 9 6	135	214	214	175	215	215	216	2255	217	526		275	375		417	0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	\$03 \$03
		92 133 173 173 96	135	135	96	0/c	136	174	174	135	176	176	176	256 256	771		336	376	376	416		416 416	460
d Catalog		888888 888888	202 202	202 202 202	257	222	26	136	136	136	137	137	137	178	7 40 V	7 00 F	5962	925	337	277	5 K K K	214	417 706
<b>JR</b> Greenland	NUMBER OF PTS	849966 849966	159	99 162	102	130	123	129	164	71 100	214	59	172	180	207	307	428	408	321	309	403	330	230
easat II	B G E	1.908 0.127 9.222 9.850 8.216	8.803	8.155 8.071	8.905	9.251	8.792	7.891	7.858	0.555	7.586	0.310	8.516	6.861	6.908	6.907	6.775	7.582	7.126	5.986	5.971	6.793	7.507
N. N.	ADING ACLO		30	2000	30	3 30	30	20.	.02	30.2	0 20	4 31	30	30	30	30	30	30	30	306	300	306	201
Table	DEG N	61.32 62.62 63.621 64.29	64.318	64.74 64.77	64.43	64.298	64.48	64.847	64.86	63.75 64.85	65.541	64.530	65.296	66.307	66.349	66.39(	66.789	66.818	67.11	67.53]	67.562	67.708	67.652
	LONG DEG E DEG E	312.420 312.420 314.881 314.481 315.238	315.428	315.859 316.552	316.523	316.576	316.260	315.209	315.059	315.305 316.033	316.316	316.698	316.621	317.010	317.299	317.040	315.969	315.911	316.457	316.968	317.624	316.488	316.824
	STAR LAT & DEG N	61.039 61.334 60.759 61.109 60.894	61.149	61.131 60.738	60.754	60.726	60.909	61.490	61.572	61.449 61.250	61.729	61.567	61.706	62.157	62.1Q2	62.294	63.352	63.779	63.778	64.133	63.899	64.524	64.589
	MATE AND A AT N AT L ONG NDING ENDING	ৰৰৰৰ	A	44	A	A	A	A	A	44	A	A	A	A	A	A	A	A	A	A	A	4	A
	APPROXI LATITUDE DIRECTIO 315.0 E A = ASCE DESCI	59.56 60.74 60.74 61.04	61.38	61.58 61.58	61.58	61.58	61.58	61.58	61.58	61.72 61.83	62.43	62.51	62.56	63.21	63.25	63.31	63.86	64.20	64.46	64.96	65.04	65.12	65.28
	REV NUMBER	792 591 635 146	878	1437 1394	1351	1308	1265	1222	1179	677 189	720	476	232	519	275	763	562	806	605	849	648	160	1021

		608	607	607 1015	559 802	657	608 858	609	757	758	759	809 1104	950	871 1185	953 1267 1816	874 1189 1502	953 1266	1032 1423	1033	953
		558	608	1094 608 936	509 803	607	558 802	559	708	759	710	810 1025	870	872 1186	873 1187 1734	875 1109 1423	954 1267	1033	953 1916	956
	T	559	558	936 558 858	510 705	608	559 803	510	658 658	200	9116 1451	1415 760 1026	871	810 1106	874 1188 1735	812 1110 1344	874 1268	953 1345	954	874
	H WHIC	509	559	937 559 803	460 706	558	509 754	511	659	210 710	946	1416 761 946	810	811 1107	875 1109 1579	813 1111 1345	875 1189	954 1267	874 1818	875
	TRAVE	510	209	938 509 753	461 656	559	510 705	461 706	609	4061 661 740	8662	1258 711 947	1261 811 7263	1027	812 1110 1500	763 1031 1346	812 1110	874 1268	875	876 1110
	BINS .	417 802	510	858 510 705	417 657	509	7060	1034 462	610	612	613	1259	192 192	763 1028	813 1030 1501	764 1032 1266	813 1111	875 875 1188	876 1110	813
		418 656	461	461 706	507 578 607	510	6561 6561		195	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	563 807	1180 662 868	599 7971	713	1419 763 1031 1422	715 952 1267	764	1189 1189	813	765 1031
nt.)		379	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	656173	+6.09 7.74	1001	657	8404 378	295	0 4 1 0 4 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	808 808	1181 663 869	1185 614 7071	714	1421 764 1032 1424	2014 716 953 1187	765 1032		764	716
og (Co		339	418 418	8418 8788 1288	255 255 255 255 255 255 255 255 255 255	461 461	879 879	-645 279	512	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	514	808 808 808 808	615 615	870	1342 715 952 1266	1914 956 1188		618 618 1111	765	1033
l Catal					-								•							
Greenland	NUMBER OF PTS	293	239	54 342	314	334	325	195	218	357	388	310	130	293	383	313	386	213	210	199
asat IDR	L DNG DEG E	307.023	312.752	306.593 306.455	308.475	309.482	306.749	310.655	308.209	309.560	307.033	310.201	311.211	309.407	305.255	309.041	306.135	309.620	305.889	314.775
ole 2. Sea	LAT & DEG N	67.806	66.108	67.913 67.950	67.415	67.130	67.877	66.927	68.035	68.103	68.765	68.257	68.278	68.769	69.844	69.179	69.756	69.118	69.824	67.962
Tał	NG ONG EG E	18.426	17.304	17.268 17.968	18.521	16.285	18.026	18.365	17.558	18.532	19.184	<b>518</b> . 666	519.381	519.004	519.559	\$20.720	519.893	522.115	519.493	520.552
	STARTI Lat & L Deg N D	63.966 3	64.428 3	64.443 3 64.156 3	63.924 3	64.839 3	64.137 3	64.197 3	65.153 3	65.394 3	65.273 3	65.798 3	65.930 3	66.173 3	66.462	66.138 3	66.471 3	65.752	66.637	66.298
	ATE AND ATE AND ATE OING OING	A	A	44	A	A	٨	A	A	A	A	٩	A	A	A	A	A	¥	A	A
	APPROXIM LATITUDE DIRECTION 315.0 E LU A = ASCEN D = DESCEN	65.30	65.31	65.31 65.31	65.31	65.31	65.31	65.57	66.11	66.62	66.71	67.02	67.31	67.44	67.83	67.86	67.88	67.88	67.89	67.89
	REV NUMBER	1494	1365	1322 1279	1236	1193	1150	691	490	289	777	576	820	619	662	418	174	1035	1465	1422

+ IDP Creanland Catalog (Cont.) Ű c Table 2. Seasat IDR Greenland Catalog (Cont.)

	874 1818	1031	1032	953 1267	1110	1033 1346	1114 1348	1194 1663	1117 1351 1663	1118 1433 1744	1278 1511 1829 2519	1201 1435 1930	1280 1594 2031	1359 1673 2032	1362 1674 2231
	875 1735	1032	1033	954 1268	1111	-953 1266	1034	1195 1584	1037 1352 1664	1119 1353 1745	1198 1512 1830 2419	1043 1436 1832	1281 1514 2032	1360 1594 2033	1283 1675 2232
ж	876 1110	1033 2015	953	874 1188	1032	1267 1267	1035	1115 1585	1038 1272 1585	1039 1354 1666	1120 1432 1745 2420	1044 1356 1748	1202 1515 1835	1281 1595 1933	1204 1595 2134
SH WHIGERSES	813 1111	953 2016	954	875 1189	1033	874	955	1116 1508	959 1273 1586	1040 1274 1667	1041 1433 1746 2321	964 1357 1669	1203 1516 1748	1124 1515 1934	1205 1596 2034
THROUC	814 1031	954 1916	874	876 1110	953	875	956 1190	1037 1350	960 1274 1507	962 1275 1588	963 1434 1668 2322	965 1277 1591	1124 1437 1749	1125 1516 1835	1206 1597 1935
BINS REV	764 1032	\$74 1917	875	813 1111	954	813	957 1191	1038	880 1194	1276 1276 1589	964 1355 1588 2224	886 1278 1512	1045 1438 1750	1045 1517 1836	1126 1518 1936
	765 1033	875 1817	876	765 1031	876 1268	1111	877 877 1192	958 1352	11195 1428 1428	883 883 1196 1510	884 1356 1589 2027	887 1279 1513	1046 1358 1672	1437	1127 1519 1837 2526
	715 953	764	813	1032	813 813 1 813	715	878 878 1112	959 1272	11115629	11978 11978 1431	1276 1590 1927	819 1199 1514	1359 1592 1592	1671	2429 1752 2429 2429
	716 954	715	765	716	765	1032	815 815 1113	816 816 1193	11116 1350	111980	1277 1510 1928	1200	968 1593 1593	967 1439 1672	2121 823 1440 1673 2329
NUMBER OF PTS	290	174	207	286	148	298	294	217	430	403	340	404	322	330	233
NG Long Deg e	305.291	305.678	314.754	310.856	309.501	306.043	306.813	308,832	309.271	310.884	306.589	309.000	310.825	310.456	310.200
LAT & LAT & DEG N	69.921	69.857	67.968	68.876	69.156	69.797	69.852	69.756	69.710	69.651	70.440	70.198	70.105	70.196	70.388
ING LONG DEG E	320.531	319.694	319.510	320.033	319.585	320.600	319.283	320.465	321.170	323.708	323.910	324.872	323.523	323.492	325.822
START Lat & Deg N	66.303	66.57 <b>1</b>	66.630	66.467	66.610	66.286	67.038	67.116	66.962	66.575	66.728	66.663	67.415	67.486	67.126
TE ND NG DING DING	٩	A	A	A	A	¥	A	A	A	4	· <b>A</b>	٨	4	٨	4
APPROXIMA LATITUDE A DIRECTION 315.0 E LO A = ASCEND D = DESCEN	67.89	67.89	67.89	67.89	67.89	67.89	68.22	68.56	68.59	68.88	69.01	69.18	69.40	69.46	69.62
REV NUMBER	1379	1336	1293	1250	1207	1164	461	504	260	547	167	590	834	633	877

	1754	1361 1561 1674 2331	1440 1674 2135	1442 1676 2037 2529	1522 1756 2138 2629	1523 1843 2237	1365 1679 1941 2533	1524 1847 2241 2634	1603 1946 2340 2733	1682 1945 2438	1685 1969 2341 3225 3225
	1674 2134	2823 1362 2233	1441 1675 2035	1363 1596 1937 2429	1523 1757 2039 2630	1444 1755 2138	2727 1366 1599 1942 2434	1525 1758 2141 2534	1604 1846 2240 2633	1602 1946 2339	1605 1849 2342 2736 3126
CH	1675 2135	2724 1284 1597 2134	1361 1676 2036	2528 1284 1597 1838 2430	1444 1677 2040 2531	1365 1756 2139	2728 1367 1600 1843 2435	1526 1759 2142 2535	1524 1847 2241 2634	3026 1603 1846 2241	1606 1850 2343 2637 3128
JGH WHI	1284 2035	2725 1285 1598 2135	1362 1596 1936	2429 1585 1585 2339 2331 2339 2331 2339 2331 2339 2331 2339 2331 2331	2823 1365 1678 1940 2433	1366 1757 2039	2729 1287 1601 1844 2335	1446 1680 2536 2536	1525 1759 2141 2635	2927 1604 1847 2242	1607 1851 2243 2638 3029
S THROU	1285	2626 1518 2036	1363 1597 1937	2430 1518 2322 2322 2322 2322 2322 2322 2322 23	2724 1366 1679 1941 2434	1286 1677 2040	2630 1288 1521 1755 2336	2728 1447 1681 2643 2436	3026 1368 1760 2142 2535	2928 1524 1848 2142	1527 1761 2244 2538 3030
BINS	1206 1838	2528 1206 1519 1937	1598 1598	23350 1219 1519 22333 22333	2725 1286 1599 1942 2335	1287 1678 1940	2532 1208 1522 1756 2236	2729 1289 1682 2437 2437	2927 1369 1680 2143 2437	2929 1525 1759 2143	1449 1762 2145 2539 2930
	1127 1839	2529 1048 1520 1839	1205 1518 1838	2331 12207 15207 1754	2626 1287 1600 2236 236	2827 1288 1599 1941	2433 1209 1523 1757 2237	2630 1290 1602 1944 2338	2829 1370 1681 2643 2438	2829 1447 1760 2043	1371 1763 2047 2540 2931
	1049 1752	2429 970 1440 1753	1206 1519 1752	2233 1440 1674 2135	2627 1208 1601 1843 2237	2727 1208 1600 1942	2434 1131 1443 1677 2238	2631 1133 1603 1945 2339	2731 1290 1682 2044 2338	2831 1369 1680 2044	2831 1372 1683 2048 2440 2833
	892 1753	2331 892 1441 1754	1126	2134 1441 20355	2528 1209 1521 21355	2728 1209 1522 1842	23355 1053 1444 1678 2040	2532 1134 1604 1846 2240	2633 1134 1602 1945 2339	2731 1213 1681 2045	2536 1292 1684 1684 2641 3224 3224
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NUMBEI OF PT:	172	269	449	437	532	335	560	529	482	328	561
L DNG DEG E	309.083	309.222	310.924	308.907	310.514	310.746	310.836	310.046	310.086	312.344	309.298
LAT & DEG N	70.600	70.582	70.340	70.637	70.608	70.586	70.598	70.854	70.870	70.607	71.097
LING Long Deg e	325.925	325.869	322.998	325.913	324.057	324.121	326.124	326.512	326.804	326.103	325.978
STAR LAT & DEG N	67.216	67.233	67.995	67.260	68.113	68.116	67.650	67.880	67.850	68.057	68.36 <b>8</b>
ATE AND AT DING DING VDING	A	A	۷	٨	×	¥	A	A	A	¥	•
APPROXIM LATITUDE ) DIRECTION 315.0 E L( A = ASCEN D = DESCEN	69.68	69.68	69.72	69.74	69.96	69.99	70.00	70.21	70.23	70.25	70.43
REV NUMBER	1264	1221	676	432	719	475	231	518	274	762	561

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Table 2. Seasat IDR Greenland Catalog (Cont.)

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	2062 2356 3045 3529 3529	2259 2553	2360 2755 3249 32242 3535	2828 2825 28559 28559 2967 28559 2967 2967 2967 2967 2967 2967 2967 296	5728 1777 25559 3147 5731 5731 4018	2462 2954 3247 3540 3733	22669 22669 32256 3737 3737 3737 3737 3737 3737 3737 37	3929 28666 3154 33474 38347 38347
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	. 495	.785	.516	.165	.707	.847	.261	.852
DEG DEG	307	320	310	310	304	308	310	310
DEG N	71.722	70.450	71.623	71.658	71.946	71.809	71.793	71.779
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ING LONG DEG E	330.14	328.9	328.49	329.2	332.31	327.81	331.43	328.7(
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Table 2. Seasat IDR Greenland Catalog (Cont.)

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920	740	868	677	340	867	817	12 12 19 13 13 13 13 13	145	125
309 . 008	308,969	304.995	308.170	304.291	308.893	309.128	316.127 315.619 315.619 314.975 313.572 313.572 313.056	313.043	313.046
72.046	72.042	71.936	71.997	71.849	72.011	71.985	59.901 60.206 60.096 60.943 60.943 60.967	60.965	60.970
334.161	330.993	329.468	332.832	317.604	330.727	331.708	316.127 315.859 315.436 317.068 316.880 316.882 318.874	317.584	318.903
70.789	71.147	71.310	71.108	72.026	71.338	71.353	59.901 60.247 61.280 62.073 62.754 53.862	63.272	63.861
NDING ENDING A	A	A	A	٨	A	٩	0000000	A	A
A = ASCEI D = DESCI 72.04	72.05	72.05	72.06	72.06	72.06	72.07	59.09 59.09 59.94 60.094 61.16 021	62.02	62.02
718	474	230	517	273	761	560	572 773 5285 6453 1189 1189	1232	1275
	A = ASCENDING D = DESCENDING 718 72.04 A 70.789 334.161 72.046 309.008 920 2986 3086 3085 3378 3571 3671 3670 3 5768 3765 3765 3764 3865 366 43863 3 5768 3765 3765 3764 3865 4056 4056 4056 4056 4056 4056 4056 40	A = ASCENDING     D = DESCENDING     718   72.04   A   70.789   334.161   72.046   309.008   920   2986   3086   3085   3571   3671   3670   3     718   72.04   A   70.789   334.161   72.046   309.008   920   2986   3086   3085   3571   3671   3670   3     718   72.04   A   70.789   334.161   72.046   309.008   920   2986   3086   3085   3571   3671   3670   3   3   3   3   3   3   3   3   3   3   3   3   3   3   3   3   3   3   3   3   3   3   3   3   3   3   3   3   3   3   3   3   3   4   3   4   4   4   4   4   4   4   4   4   4   4   4   4   4   4   4   4   4   4   4   4   4   4   4<	A = ASCENDING     718   72.04   A   70.789   334.161   72.046   309.008   920   2986   3085   3085   3576   3564   3867   3564   3863   3863   3863   3863   3863   3865   3865   3865   3865   3865   3865   3865   3865   3865   3865   3865   3865   3865   3865   3865   3865   3865   3865   3865   3865   3865   3865   3865   3865   3865   3865   3865   3865   3865   4195   4145   4145   4145   4145   4145   4145   4145   4145   4145   4145   4145   4145   4145   4145   4145   4145   4145   4145   4145   4145   4145   4145   4145   4145   4241   4241   4241   4241   4241   4241   4241   4241   4241   4241   4242   4242   4242   4242   4242   4242   4242   4242   4242   4242   4242   4242   4242   4242   4	A = ASCENDING     718   72.04   70.789   534.161   72.046   309.008   920   2986   5085   5767   5765   5765   5764   5664   5664   5664   5664   5664   5664   5664   5664   5664   5664   5664   5664   5664   5664   5664   5664   5664   5664   5664   5664   5664   5664   5664   5664   5664   5664   5664   5664   5664   5664   5664   5664   5664   5664   5664   5664   5664   5664   5664   5664   5664   5664   5664   5664   5664   5664   5664   5664   5664   5664   5664   5664   5664   5664   5664   5676   5664   5676   5664   5676   5676   5664   5676   5664   5664   5664   5676   5664   5676   5664   5676   5664   5676   5664   5676   5664   5676   5664   5676   5664   5676   5664   5676   5664   5676 <t< td=""><td>D = DESCENDING     718   72.04   A   70.789   534.161   72.046   309.008   920   2986   5065   3565   3564   3671   3671   3671   3671   3671   3671   3671   3671   3671   3673   3564   9566   9566   9566   9566   9566   9566   9566   9566   9566   9566   9566   9566   9566   9566   9566   9566   9566   9566   9566   9566   9566   9566   9566   9566   9566   9566   9566   9566   9566   9566   9566   9566   9566   9566   9566   9566   9566   9566   9566   9566   9566   9566   9566   9566   9566   9566   9566   9566   9566   9566   9566   9566   9566   9566   9566   9566   9566   9566   9566   9566   9566   9566   9566   9566   9566   9566   9566   9566   9566   9566   9566   9566   9566   9566   9566</td><td>D = DESCENDING       718     72.04     A     70.789     534.161     72.046     509.105     956.105     957.105     557.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1</td><td>D = ESCENDING       71.01     72.04     309.101     72.04     309.101     301.101     301.101     301.101     301.101     301.101     301.101     301.101     301.101     301.101     301.101     301.101     301.101     301.101     301.101     301.101     301.101     301.101     301.101     301.101     301.101     301.101     301.101     301.101     301.101     301.101     301.101     301.101     301.101     301.101     301.101     301.101     301.101     301.101     301.101     301.101     301.101     301.101     301.101     301.101     301.101     301.101     301.101     301.101     301.101     301.101     301.101     301.101     301.101     301.101     301.101     301.101     301.101     301.101     301.101     301.101     301.101     301.101     301.101     301.101     301.101     301.101     301.101     301.101     301.101     301.101     301.101     301.101     301.101     301.101     301.101     301.101     301.101     301.101     301.101     301.</td><td>D = Accelentive     C = 0     C = 0     C = 0     C = 0     C = 0     C = 0     C = 0     C = 0     C = 0     C = 0     C = 0     C = 0     C = 0     C = 0     C = 0     C 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9765     9765     9765     9765     9765     9765     9765     9765     9765     9765     9765     9765     9765     9765     9765     9765     9765     9765     9765     9765     9765     9765     9765     9765     9765     9765     9765     9765     9765     9765     9765     9765     9765     9765     9765     9765     9765     9765     9765     9765     9765     9765     9765     9765     9765     9765     9765     9765     9765     9765     9765     9765     9765     9765     9765     9765     9765     9765     9765     9765     9765     9765     9765     9765     9765     <th< td=""></th<></td></t<>	D = DESCENDING     718   72.04   A   70.789   534.161   72.046   309.008   920   2986   5065   3565   3564   3671   3671   3671   3671   3671   3671   3671   3671   3671   3673   3564   9566   9566   9566   9566   9566   9566   9566   9566   9566   9566   9566   9566   9566   9566   9566   9566   9566   9566   9566   9566   9566   9566   9566   9566   9566   9566   9566   9566   9566   9566   9566   9566   9566   9566   9566   9566   9566   9566   9566   9566   9566   9566   9566   9566   9566   9566   9566   9566   9566   9566   9566   9566   9566   9566   9566   9566   9566   9566   9566   9566   9566   9566   9566   9566   9566   9566   9566   9566   9566   9566   9566   9566   9566   9566   9566	D = DESCENDING       718     72.04     A     70.789     534.161     72.046     509.105     956.105     957.105     557.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1     567.1	D = ESCENDING       71.01     72.04     309.101     72.04     309.101     301.101     301.101     301.101     301.101     301.101     301.101     301.101     301.101     301.101     301.101     301.101     301.101     301.101     301.101     301.101     301.101     301.101     301.101     301.101     301.101     301.101     301.101     301.101     301.101     301.101     301.101     301.101     301.101     301.101     301.101     301.101     301.101     301.101     301.101     301.101     301.101     301.101     301.101     301.101     301.101     301.101     301.101     301.101     301.101     301.101     301.101     301.101     301.101     301.101     301.101     301.101     301.101     301.101     301.101     301.101     301.101     301.101     301.101     301.101     301.101     301.101     301.101     301.101     301.101     301.101     301.101     301.101     301.101     301.101     301.101     301.101     301.101     301.101     301.101     301.	D = Accelentive     C = 0     C = 0     C = 0     C = 0     C = 0     C = 0     C = 0     C = 0     C = 0     C = 0     C = 0     C = 0     C = 0     C = 0     C = 0     C = 0     C = 0     C = 0     C = 0     C = 0     C = 0     C = 0     C = 0     C = 0     C = 0     C = 0     C = 0     C = 0     C = 0     C = 0     C = 0     C = 0     C = 0     C = 0     C = 0     C = 0     C = 0     C = 0     C = 0     C = 0     C = 0     C = 0     C = 0     C = 0     C = 0     C = 0     C = 0     C = 0     C = 0     C = 0     C = 0     C = 0     C = 0     C = 0     C = 0     C = 0     C = 0     C = 0     C = 0     C = 0     C = 0     C = 0     C = 0     C = 0     C = 0     C = 0     C = 0     C = 0     C = 0     C = 0     C = 0     C = 0     C = 0     C = 0     C = 0     C = 0     C = 0     C = 0     C = 0     C = 0     C = 0     C = 0     C = 0     C = 0 <thc 0<="" =="" th="">     C = 0     C = 0</thc>	N = 4 SCRENING     T2.04     T0.769     134.161     T2.046     300.1016     9765     9765     9765     9765     9765     9765     9765     9765     9765     9765     9765     9765     9765     9765     9765     9765     9765     9765     9765     9765     9765     9765     9765     9765     9765     9765     9765     9765     9765     9765     9765     9765     9765     9765     9765     9765     9765     9765     9765     9765     9765     9765     9765     9765     9765     9765     9765     9765     9765     9765     9765     9765     9765     9765     9765     9765     9765     9765     9765     9765     9765     9765     9765     9765     9765     9765     9765     9765     9765     9765     9765     9765     9765     9765     9765     9765     9765     9765     9765     9765     9765     9765     9765     9765     9765 <th< td=""></th<>

				175 255	566 214	666 376 172	665 335	1132 335	665 293	1537 715 414	1047 714 415	1291 816 561 333	1617 963 662 457
		175 53 176 175	56	215 133 295	719 254	821 377 212	716 375	1213 375	666 334	1538 765 415	1210 715 459	1292 817 611 373	1697 1044 712 458
	сн	176 94 176 176	45 96 96	216 134 296	770	971 417 213	717 376	1214 1214 415	716 375	1619 766 459	1291	1373 1373 884 374 374	1780 1045 713 2508
	GH WHI ERSES	217 217 217 216	11366	256 174 336	822 295	1134 462 253	767 416	1458 416	818 615	1620 816 511	1292 816 510	1456 885 414 414	1781 1125 763 509 290
	THROU V TRAV	257	1355	297 175 337	132 1463 296	1135 463 254	768	1541 614	887 887 416	1701 817 561	1707 817 560	1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	1877 1126 764 291
	BINS	52222 52222 52225 52525 5255 5255 5255	175	298 215 619	173 1708 336	1379 513 294	819 512	1885	1132 562	1702 884 562	1982 884 561	1700 966 714	221 1878 815 560 331
		20088 50088 50088 50088 50088 50088 50088 5008 5008 5008 5008 5008 5008 5008 5008 5008 5008 5008 5008 5008 5008 5008 5008 500 500	256 256 216	338 133 216 216	174 1890 418	172 1625 514 295	513	293 2089 666	1212 563	1703 885 612	2084 8854 612	2083 2083 715 459	291 1979 881 610 372
ont.)		2399 2399 2999	2227 2216 257 257	339 134 256	214 1891 419	1707 1707 335	1132	2189 2189 819	1459 614 614	2002 2002 2002 2002 2002 2002 2002 200	2085 2085 2085 2085 2085 2085 2085 2085	2084 1128 765 510	2182 2182 882 611 412
atalog (C		66666 55555 55555 55555 55555 55555 55555 5555	298 257 298	379 379 379 822	215 1992 463	213 616 336	1624 1624 614	2190 2190	1556	2288 2288 1047	2186 1046	2186 2186 1210 566	2352 1370 962 661 413
Greenland C	NUMBER OF PTS	888 89 89 80 90	46 89 152	166 120	242	448	381	313	315	363	507	468	817
asat IDR	NG LONG DEG E	314.837 312.793 315.272 314.846	314.283 312.837 313.600 312.213	312.904 312.749 311.473	311.703	310.546	310.996	311.259	311.347	310.251	309.793	309.727	309.013
2. Se	CAT &	. 938 . 830 . 940	. 689 . 641 . 641	. 465 461 474	. 918	.751	.591	.745	.874	.949	.821	.840	.133
Table	DE	600 600 600 600 600	01-19 09 09	61 61 61	19	61	62	62	62	62	62	62	63
	LNG DEG E DEG E	518.557 518.553 518.489 518.489	518.201 516.886 517.551 516.870	518.249 518.926 574.845	336.460	334.653	331.511	335.841	329.819	335.038	334.310	334.099	333.759
	START LAT & L DEG N D	63.712 63.682 63.682 63.685	63.589 63.112 63.563 63.344	64.026 64.370 64.907	69.738	69.565	69.198	69.984	68.898	70.084	66.99	69.983	70.139
	IATE AND I AT ONG IDING	6666	9999		а <u>а</u>	Q	Q	Ω	Q	A	A	Q	A
	APPROXIV LATITUDE DIRECTION 315.0 E L A = ASCEN	62.02 62.02 62.02	62.20 62.35 62.35	62.57 62.57 63.15	63.47	63.80	64.35	64.37	64.42	64.95	64.99	65.06	65.53
	NUMBER	1318 1361 1447 1442	1017 888 156 400	644 845 601	802	558	759	271	515	228	472	716	429

		1289 962 662 457		1287 880 610 412	1448 1042 813 608	526 1448 1041 761 556	1693 1282 709 504	2477 1692 1282 1036 1036 559	1443 1118 810 605	1524 1278 952 706
		1371 963 712 507		1452 881 660 413	1449 814 609	1530 1122 762 557	1774 1283 1037 505	2578 1772 1362 809 555	1444 872 872 855 872	1605 10328 201 501
	Н	1533 1043 713 508		1532 962 456	1450 1123 877 659	1531 1123 812 607	1775 1284 1038 760 555	2782 1773 1363 1117 810 605	1526 1199 873 656	1770 1359 1033 757 551
	GH WHI ERSES	1534 1044 763 558		1533 1043 711 457	1531 1204 873 660	1532 1532 813 608	1869 1364 1039 810 556	2883 1774 1364 1118 811 811 606	1771 1279 953 706	11362 807 5527
	V TRAU	1616 1045 559 259	290	1534 1124 712 507	1615 879 710	1612 1612 877 658	1365 11365 811 811 606	2985 1867 1444 1119 873 656	1772 1280 954 707	111 801 801 80 80 80 80 80 80 80 80 80 80 80 80 80
	BINS Re	1697 1125 814 609	100 121	1615 1125 762 508	1696 1285 959 711	1284	2175 2175 1446 1120 812 607	3292 1526 1199 874 657	1867 1281 1035 757	2066 11441 8699 6049
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Ë	LONG LONG DEG E	331.124	311.256 311.790 312.288	328.245	337.172	327.958	337.118	337.569	332.999	335.768
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NUMBER OF PTS	745	723	695	748	728	718	636	38 59	9740 37	18 640
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DEG	309	310	306	310	305	310	309	309 308	2005 2005 2005	200 200 200
END N N S	638	678	.560	.823	.563	848	.807	.860 .800	.591	213 619 764
DEG	71.	71.	71.	11	71	71	71	17	222	
ш	084	967	944	.139	.175	. 884	.754	.573	489 741 897	161.
DEG	335.	327 .	336.	327	335	331	330	337 311	337 336 304	336 3276 3276
STAR AT & N	069	166	428	968	455	.677	.737	.176 .956	185 256	8692 8653 8653
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	SH WHIG	4068 4260 42551 42551	4163 4251 4251 4233	4257 4257 4257 4257 4253 4239 4131	44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 444419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 44419 444194419	4124 33390 4063 4155 4247 4238	4125 42250 42241 42241 42241 42241 42241 42241 42241 42241 42241 42241 42241 42241 42241 42241 42241 42241 42241 42241 42241 42241 42241 42241 42241 42241 42241 42241 42241 42241 42241 42241 42241 42241 42241 42241 42241 42241 42241 42241 42241 42241 42241 42241 42241 42241 42241 42241 42241 42241 42241 42241 42241 42241 42241 42241 42241 42241 42241 42241 42241 42241 42241 42241 42241 4225 4225
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nd Cata							
reenlar	NUMBER OF PTS	690	561	662	643	743	634
IDR (	, ш	651	835	224	340	836	182
seasat	DING BECONC	309.	309.	304.	304.	304.	304.
ble 2. S	LAT & DEG N	71.877	71.894	71.606	71.625	71.737	71.735
Ta	ш	720	607	207	964	82	0 2 2
	DEG	331.	335.	337	336.9	337.6	330.7
	STAF Lat 8 Deg n	71.627	71.286	71.074	71.119	70.896	71.504
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	IMATE E ANI ON AT LONG CENDIN	A	Q	<b>A</b>	9	Ð	A
	APPROX LATITUD DIRECTI 315.0 E A = ASC DES	72.04	72.04	72.04	72.05	72.06	72.06
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Table 3. Summary of Seasat Greenland Orbit Adjustment

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ST/ LAT	60.89 63.56 64.52 64.52 69.81 66.81	72.07 70.71 61.25 71.76 71.45 70.08	71.86 71.31 67.65 71.23 71.23 69.07	71.13 72.06 69.86 69.98 72.05 72.05	62.16 62.15 60.25 71.99 69.28 65.39 65.39	71.68 69.75 69.75 60.14 60.14 60.20 62.05 62.25 88 71.88 71.88 71.88 71.88 71.88 71.88 71.88 71.68	722.06 722.06 722.06 722.06 722.06 722.06 722.06 722.06 722.06 722.06 722.06 722.06 722.06 722.06 722.06 722.06 722.06 722.06 722.06 722.06 722.06 722.06 722.06 722.06 722.06 722.06 722.06 722.06 722.06 722.06 722.06 722.06 722.06 722.06 722.06 722.06 722.06 722.06 722.06 722.06 722.06 722.06 722.06 722.06 722.06 722.06 722.06 722.06 722.06 722.06 722.06 722.06 722.06 722.06 722.06 722.06 722.06 722.06 722.06 722.06 722.06 722.06 722.06 722.06 722.06 722.06 722.06 722.06 722.06 722.06 722.06 722.06 722.06 722.06 722.06 722.06 722.06 722.06 722.06 722.06 722.06 722.06 722.06 722.06 722.06 722.06 722.06 722.06 722.06 722.06 722.06 722.06 722.06 722.06 722.06 722.06 722.06 722.06 722.06 722.06 722.06 722.06 722.06 722.06 722.06 722.06 722.06 722.06 722.06 722.06 722.06 722.06 722.06 722.06 722.06 722.06 722.06 722.06 722.06 722.06 722.06 722.06 722.06 722.07 722.06 722.07 722.07 722.07 722.07 722.07 722.07 722.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 727.07 72
AT 330.E	0.243 -0.966 -0.149 -0.077 -0.808	-0.087 -0.488 -1.413 -0.920 -1.742		-2.750 1.463 -0.109 -0.370 -0.370	-0.729 -0.152 -0.152 -0.372 -0.372 -0.372 -0.163	-0.469 263 401 768 101 768 101 784 101 784 101 784 101 784 101 784 101 784 101 784 101 784 101 784 101 784 101 784 101 784 101 784 101 784 101 784 101 784 101 784 101 784 101 784 101 784 101 784 101 784 101 784 101 784 101 784 101 784 101 784 101 784 101 784 101 784 101 784 101 784 101 784 101 784 101 784 101 784 101 784 101 784 101 784 101 784 101 784 101 784 101 784 101 784 101 784 101 784 101 784 101 784 101 784 101 784 101 784 101 784 101 784 101 784 101 784 101 784 101 784 101 784 101 784 101 784 101 784 101 784 101 784 101 784 101 784 101 784 101 784 101 784 101 784 101 784 101 784 101 784 101 784 101 784 101 784 101 784 101 784 101 784 101 784 101 784 101 784 101 784 101 784 101 784 101 784 101 784 101 784 101 784 101 784 101 784 101 784 101 784 101 784 101 784 101 784 101 784 101 784 101 784 101 784 101 784 101 784 101 784 101 784 101 784 101 784 101 784 101 784 101 784 101 784 101 784 101 784 101 784 101 784 101 784 101 784 101 784 101 784 101 784 101 784 101 784 101 784 101 784 101 784 101 784 100 784 101 784 101 784 101 784 101 784 101 784 101 784 101 784 101 784 101 784 101 784 101 784 101 784 101 784 100 784 100 784 100 784 100 784 100 784 100 784 100 784 100 784 100 784 100 784 100 784 100 784 100 784 100 784 100 784 100 784 100 784 100 784 100 784 100 784 100 784 100 784 100 784 100 784 100 784 100 784 100 784 100 784 100 784 100 784 100 784 100 784 100 784 100 784 100 784 100 784 100 784 100 784 100 784 100 784 100 784 100 784 100 784 100 784 100 784 100 784 100 784 100 784 100 784 100 784 1000 784 100 784 100 784 100 784 100 784 100 784 100 784 100 784 100 784 100 784 100 784 100 784 100 784 100 784 100 784 100 784 100 784 100 784 100 784 100 784 100 785 100 100 100 100 100 100 100 100 100 10	
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0RB 310.E	0.744 0.297 0.286 0.986 0.986 0.982 0.982	-0.626 -0.626 -0.881 -0.881 -1.901	-1.254 -1.125 -1.125 -1.289 -1.289				
Y) AT 330.e	.0101568 .0187124 .0030267 .0119976 .0173161 .0090887	.0178369 .0165213 .0105042 .0183764 .0183764 .0168784	.0179181 .0164095 .0068522 .0108522 .0108522 .0184626 .0169545	.001994563 .001748242 .0094563 .00619563 .018768282 .018768282 .018768282	.0069762 .0111462 .02045467 .0185551 .01855510 .01853510 .01853510 .01853510 .01853510 .0185050	01248 011960548 0119605656 0119605656 0117826656 0117826656 0117826656 01288265656 01288265656 01288575 01288575 01288575 01288575 01288575 01288575 01288575 01288575 01288575 01288575 01288575 01288575 01288575 01288575 01288575 01288575 01288575 01288575 01288575 01288575 01288575 01288575 01288575 01288575 01288575 01288575 01288575 01288575 01288575 01288575 01288575 01288575 01288575 01288575 01288575 01288575 01288575 01288575 01288575 01288575 01288575 01288575 01288575 01288575 01288575 01288575 01288575 01288575 01288575 01288575 01288575 01288575 01288575 01288575 01288575 01288575 01288575 01288575 01288575 01288575 01288575 01288575 01288575 01288575 01288575 01288575 01288575 01288575 01288575 01288575 01288575 01288575 01288575 01288575 01288575 01288575 01288575 01288575 01288575 01288575 01288575 01288575 01288575 01288575 000 000 00000000000000000000000000	
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Table 3. Summary of Seasat Greenland Orbit Adjustment (Cont.)

Table 3. Summary of Seasat Greenland Orbit Adjustment (Cont.)

LON	313.33 309.09 304.69 310.66	309.73 309.21 309.01	510.51 307.59 311.00	311.17 308.89 312.34	306.91 315.62 308.28	309.63 304.71	310.11	306.59	311.70	304.18	310.26 310.26	309.73	308.88 310.83 300.22	312.75	304.34 309.60 306.60	309.33	310.20 310.20 308.80	312.84 309.46 309.65	305.21	311.72	308.68 307.51 308.07
LAT	60.90 68.58 71.81 71.79 66.93	62.84 70.01	70.61 65.54 62.59	70.04 72.01 70.61	66.39 60.21 67.51	71.64	65.20	70.44	61.92 69.32	71.74	66.82 71.79 28 28	64.27 70.69	70.11	61.46 68.96	71.63	63.50	70.39	61.05 68.84 71 88	71.71	69.25 71.76	71.50 67.65 66.13
LON	316.88 328.54 330.75 329.35 318.36	334.10 333.94 334.16	324.06 316.32 331.51	330.39 330.73 326.10	317.04 315.86 336.40	335.08 332.31	337.57	323.91	336.46 334.17	330.77	515.91 531.43 210 28	327.96 333.94	329.55	518.93 330.10	336.96 326.48 314.97	328.25	551.01 325.82 315.43	316.89 330.69 331.72	329.15	320.04	328.75 316.82 332.64
LAT	62.75 71.45 68.59 66.59	69.98 72.04 70.79	68.11 61.73 69.20	71.89 71.34 68.06	62.29 60.35 71.75	71.69 68.72	71.12	66.73 66.73 61.04	69.74 71.96	71.50	63.78 69.32 65.03	69.48 72.07	70.95	64.37 64.37 71.67	71.12	69.26 72.06	70.94 67.13 61.15	63.11 71.66	63.59	71.60	68.60 64.59 71.09
4T 330.E	-0.386 -0.571 -1.155 -1.048	-0.985 0.111 -0.135	-0.021 -1.123 -0.503	0.036 0.244 0.416	-0.519 -1.145 -1.607	-0.196	-1.092	-0.839	-0.097 -0.406	0.157	-0.273	-0.250	-0.349	-0.720 0.113 -0.763	-0.072	-1.205	-0.264	-1.506	-0.100	-1.814 0.708	0.277 0.543 -0.332
ADJ (M) / 320.E	-0.134 -0.492 -0.078 -1.147	-0.870 0.152 -0.213	-0.101	-0.030 0.213 0.306	0.021 -1.108 -1.417	-0.119	-0.920	-0.904	-0.399	-0.028	-0.247	-0.263	-0.325	-0.126	-0.205	-1.312	-0.344 -0.374	-1.409	-0.292	5 -1.562	1.007 1.007 1.007
0RB / 310.E	0.204 -0.403 0.169 -1.136 -0.001	-0.702 0.196 -0.287	-0.169 -0.239 -0.408	-0.107 0.177	-1.058	-0.053	-0.859	-0.954	-0.392	-0.101	0.623	-0.279	-0.351	0.561	-0.386	-1.447	-0.42			-1.24	-0.02
Y) AT 330.E	.0199557 .0170194 .0163892 .0083960 .0121906	.0194669 .0179056	.006824L .0107710 .0184938	0180078	0111521	.0153938	.0127429	0063832	0171857	.0166370	.0115654	0254210. 0156780	0161822	.00999976 .0052317 .0182469	0167565	.0158937	.0162738 .0066174	.0177768	.0085934	0140588	0086153
RAC 0F DA 320.e	.0209689 .0176703 .0169846 .0091571 .0136167	.0203219	.0076998 .0126249 .0193820	.0186280	.0128839	.0176553	.0140146	.0103263 .0073706 .017471	0181158	.0172406	.0131728	.0156501 .0164804 .0187157	0168150	.0120979 .0062059	.0173551	.0167180 .0184008	0168998	0187710.	.0093656 .0093656	0189405	0093837
TIME (F 310.E	.0223233 .0184121 .0175776 .0098189	.0214093 .0191887 .0176033	0139312	.0193131	.0141185	.0182548	.0149790	.0109272 .0081660 .0127055	.0193296	0178309	.0143346	.0145491	.0131745	.0135493 .0074941	0179464	.01905737	0082827	0200931	.0100338 .0100338	.0152676	0100498
	44	554	4 0 0 0	444		222	45	002	20	500	05		0 4 0 0 5	5 02	500	03	40	05	04	05	04
(3)	0.0 0.0 -0.92901D 0.44393D	0.10743D	-0.12410D 0.0	-0.526640	0.0	-0.15515D 0.24897D	-0.61157D 0.18465D	-0.18149D 0.17145D	0.0 1.05731	-0.12490D	0.0 -0.11223D	000	-0.72448D	-0.32334D 0.0	-0.15323D 0.67876D	0.0 0.0 -0.57408D	-0.647960	0.0 0.0 0.16286D	0.0 0.62137D	0.30819D	0.15080D 0.0 0.51847D
ITS	00000				1000	200	<b>5</b> 00	222	120	200	033	200 200	2000	502	200	0000	000		585	200	2000
COEFFICIEN (2)	0.24916D 0.12075D 0.47423D -0.67295D	-0.293470 0.473680 -0.160380	-0.730050	0.251290	0.328150	0.66800D -0.19174D	0.14213D	0.48584D -0.89363D	0.266950	0.51190D -0.18267D	0.323660	0.43143D -0.15942D	-0.14868J 0.20281D 0.24702D	-0.572910	-0.28852D	0.36532D -0.12967D -0.34944D	0.869090	-0.251590 -0.251590 -0.396450	- 0.53450D -0.36084D	-0.75891D	-0.236250 0.318720
	55585	1882		5866	5555	366	100	282	322	585	555	100	855	283	322			288	853	388	
(1)	-0.53585D -0.26259D -0.52961D -0.52961D	-0.619150 -0.89886D -0.89886D	-0.413490	0.18052D -0.14566D	-0.176590	-0.70769D -0.70769D 0.16223D	-0.16154D 0.73024D	-0.33120D -0.33810D	-0.468500	-0.49028D	-0.401670	-0.742290	-0.45924L -0.16865L -0.18338D	-0.870461	-0./20231 -0.562851 0.185341	-0.438211 0.855541 0.332451	0.380341	-0.907001 -0.204361 0.607741	0.415351	-0.175621	0.220071 0.220071 -0.328821
PTS	5269 5269 5276	400	2142	617 867 867	2070	610 745 745	388	816 340	242	634 634	808 829	130	564 323 322	120	9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	309 739 739	283	159 89 640	575	240	507 571 571
REV	683 683 683 683 683	217 217 217	720	761	762	775	727	791	802	200 200 200	806	820	80 80 80 80 80 80 80 80 80 80 80 80 80 80 80 80 80 80 80 80 80 80 80 80 80 80 80 80 8	2000 2007 2007	8 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	8 8 7 7 7 7 7 7 7 7	826	8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	890 891	1018	1020

	L ON	08.66 09.62 09.25	09.57	19.60	10.47	06.04	05.71	13.06	10.28 08.31	60.48	07.60	05.91	09.50 28	09.04	05.51	07.89	13.04	99.52	08.47	11.29	10.86	80.60	13.05	10.57	06.45	35.91 14.75	22.73	05.78 26.78	14.84	56.08 25.25	265.90 90	8.90	6.50	18.91 270	122	5.94
	LT END	96 12 71 23 33 34 34 34 34 34 34 34 34 34 34 34 34	000	525	200	5 0 80 80 80	67 8 7 7 8	67	80 80 80 80 80	13	26 26 36	50	16 57 57	22		2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	96 96 80	24 24 24	61 25 31	199	20 20 20 20 20 20 20 20 20 20 20 20 20 2	60 30	26 27	60 66 31	95 30	88 97 71	07	02 30	94 31	32 33	61 30	39	03 30	44 30 84 31		201 00
	LA	71. 69. 68.	12			63. 63.	. 6 9 4		68. 71.	67.	20. 71.	72.	69. 74.		72.	6.6	60.		67.		6.9 6.3.	70.	. 0.9	69.	67.		72.			17	9	90	22	9 4 9 9 4	99	21.
	ART LON	332.32 322.12 309.39	337.57	336.67	311.51	320.60 311.26	309.04	318.87	311.99	316.28	311.24	311.87	319.59	311.47	312.21	315.21	317.58	310.11	318.52	312.53	312.29	325.93	318.90	312.98	317.97	335.98	335.82	309.20	318.56	336.74	317.27	309.58	309.53	316.52 318.35	317.30	335.98
	ST/ LAT	69.58 65.75 68.75	71.18 64.14	71.46	71.85	66.29 64.16	70.22	63.84	69.29 71.96	64.84	6/.US	71.83	66.61 64.39	70.56	12.06	61.49	63.27	71.39	63.92 71.53	71.80	64.59	67.22 60.01	63.86	69.48 71.33	64.16	71.88 66.63	72.07	72.07	63.71	71.26	64.44	66.60	72.07	60.75 63.62	64.43	71.88
	ш	544	<b>0</b>		n	4 M	~~		<b>0</b> ~ €0	,	707	0.1	~ ~	~~~	~ ~		mo	<b>m</b>	0 10	.0	<u>, 1</u>	<b>۲</b> ۳	2		0	5	. M			00	5.47	0.	210		Ман	0. <b>+</b>
Jont.)	AT 330.	-0.90 -0.18 -0.24	-0.11	0.40		-0.73	0.69	-0.22	0.88	0.61	0.40	02.0	-0.52	0.36		-0.69	-0.63	-0.06	-0.25	60.0	-1.12	0-08	-1.01	-0.29	0.01	-0.11	60.0-		00	162.0-	-0.10	-0.56	-0-	-0.69		0.21
nent (C	0J (M) 320.E	0.979 0.191 0.252	$0.677 \\ 0.421$	-0.399	0.734	-0.366	0.619	-0.218	0.919	0.948	0.505	0.714	-0.114	0.358	-0.269	-0.472	-0.409 0.475	0.233	0.251	0.247	1.192	0.267	0.914	1.0/5	0.526	0.155	0.059	0.174	0.198	0.892	0.541	0.382	0.636	0.358	0.609	0.172
Adjustn	ORB A1 310.E	1.025 0.484 -0.268	0.749 0.818	-0.322	0.785	-0.0/8 -	0.527	-0.211	-0.143	1.196	0.519	0.707	- 220.0	0.364	0.336	-0.315 -	-0.110 - 0.601	-0.370 -	0.367	0.371	-1.276 -	-0.416	-0.783 -	- 0.538 -	0.905	- 195	0.025 -	- 123 -	0.459	0.994	1.017	0.155 -	0.678 -	0.122 -	0.916	0.129
nd Orbit	AT 530.E	090848 060303 182032	168249 121075	187639	091512	193647	178236 104080	201458	1823314 165314	121046 22012	73285	90634	1426/1 94151 -	78150	.02992 164845	04072	68274	05824 -	.20947	191024	94533	03955 -	01443 -	86132	20937	42300 -	78142 -	- 50059 13983	01388	68249 85300 -	21021	88574 -	62970 -	03940 - 01406 -	21005	73228
enlar	DAY	2014 200	6 6	0.0		56.	6.6. 7.0	6	- - - - - - - - - - - - - - - - - - -	4r 62		20	79. 20.	500		6	20.22	4	8. 20. 20.	84	20.	200	20.	-00 - 9	100		10	50	.03 0	25 25	55	20.02	363	10.20.		; []
ısat Gre	RAC 0F 320.E	.009763 .007151 .018851	.017421	.019482	.009829	.020195	.018431	021149	.012127	.0135555	616210.	.009741	.020245	.018422	.007390	.012376	.017423	001349	C16210.	009780	.020284	.007587	.021147	.0093800.	.013545	.005349	018421	012368	021142	017421	.0135536	019576	016921	021143	013552	017913
ary of Sea	TIME (F 310.e	.0103806 .0080260 .0195886	.0180136 .0146276	0203419	.0104461	.0212425	.0190905	0224876	0177201	.0146253	.0185328	.0103584	0212926	0190818	00812/10	0137512	0180161	0020146	0185311	0103975	0213306	0137402	0224852	0950010	0146153	0062230	0190810	0137437	0224794	0180136	0146240	0204348	0175147	015/596	0146226	0185271
gmmu		05 04		04	05		04	5	2	96	*	05		44	n M 0 0			50		02		5		1.4 2.0	•	•••	4.0	<u>.</u>	•••			04	. 40	• •	90	· ·
ble 3. S <sup>1</sup>	(3)	.22040D 0 .25156D	<u>.</u> .	.19309D	.15221D	.0	.92352D .0	.0	0. 	.0 562830	0.00	.145400		519560	.63032D	0,0	20	.11576D		.22336D	00	.30894D	0	390420	0.0	00	275630	000000		U 27568D	0	99328D 0	46636D		0 38766D	0
Tal	S	000 000 000	00 MM	00 00	101 101	20 20	90 90	-	201	0 C M M	50	о Ми	200		201	ю с мн	- 	00		рс ММ	201	- - -	0	 		- - -	0 0 0	- - - -		 		 		 	00	
	DEFFICIENT (2)	0.51875D 0 0.33454D 0 0.75421D 0	0.12170D 0 0.37032D 0	0.12293D 0 0.61332D 0	0.391840 0	0.57560D 0	0.20645D 0 0.83758D 0	0.51668D 0	0.53161D 0	0.23217D 0	0.224100 0	0.28115D 0	0.61006D 0	0.173090 0	0.800860 0	0.114450 0	0.21193D 0	0.244210 0	0.152840 0	0.65229D 0	0.806090	0.19451D 0 0.56911D 0	0.979890 0	0.241320 0	0.35410D 0	0.33297D 0	0.155820 0	0.233090 0	0.19557D 0	0.1/210D 0.0.14361D 0.	0.44448D 0	0.13343D 0.0.44092D 0.	0.898780 0	0.362300-0	0.28650D 0.0.10668D 0.0	0.70541D 0
	0	1100		10	102	38	58	88	20,	33	200	85	55	12	38	55	10	- 22	33	10	:2:		10	32	22	56	50	50	10	10	13	-	0;	100	100	1
	(1)	0.19847D 0.22015D 0.78021D	0.14433D 0.45994D	0.13713D 0.50784D	0.164740	0.143640	0.48657D 0.60069D	0.327080	0.884750	0.219990	0.103280	0.64518D	0.142100	0.106750	0.35746D	0.18889D	0.321720	0.75488D	0.246570	0.39966D	0.443260	0.75420D	0.29864D	0.149250	0.42703D	0.21656D	1.19944D	0.33106D	0.39372D	0.95465D	.548350	1.15761D	0.82139D	1.60358D	1.32736D	1.14361D
	MSL	500		1 I 9 9		201	9.2 1 1	<u>ي</u> ا	10.	1 50	141	ا ا م	202 1	1 ī 200	20	і ї 6. <u>4</u>	י ד אַרָ	n N	1 T 12	īī 82	20	NM	្រះ	5.7	T T	- - -	T T V P			7 N		74 77	77 75	1 1 1 1	0.4 1 1	m.
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	REI	1035	1150	1162	1163	1175	1176	1185		1204	1205	1206	1218	1219	1221	1222	1234	1235	1248	1250	1261	1265	1275	1278	1279	1293	1305	1308	1318	1321	1322	1336	1349	1361	L365 L376	1377

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Table 3. Summary of Seasat Greenland Orbit Adjustment (Cont.)

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4D LON	33395555555555555555555555555555555555
LAT	000145000000000000000000000000000000000
LON LON	2304,95 2304,95 2320,55 2320,55 2320,55 2320,55 2320,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,55 2321,5
LAT	665 665 665 665 665 665 665 665 665 665
AT 330.E	0.530 0.517 0.817 0.817 0.816 0.816 0.816 0.816 0.826 0.025 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.0550 0.0550 0.0550 0.0550 0.0550 0.0550 0.0550 0.0550 0.05
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(3)	0.16952D 05 0.05734D 05 0.25734D 04 0.25130D 04 0.25240D 04 0.25240D 04 0.25240D 04 0.25240D 04 0.17976D 05 0.17976D 05 0.020 0.020 0.12195D 05 0.12195D 05 0.123850D 05 0.22277D 04 0.22859D 05 0.22859D 05 0.13840D 04
COEFFICIENTS (2)	0.34356D 03 0.21410D 03 0.94408D 03 0.19202D 03 0.19202D 03 0.20202D 03 0.20202D 03 0.20202D 03 0.20204D 03 00004D 00004D 0000000000000000000000000
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		MANNER IN V	WHICH APPLIED	SECTION
ADJUSTMENT	VALUE OR RANGE	TIME	SURFACE HEIGHT	IN WHICH DOCUMENTED
RETRACKING CORRECTION accounts for lag in tracker response	–15m<∆H <sub>RET</sub> <15m	N/A	()	2.1
TIME BIAS accounts for track mode correction	-7.9451 x 10 <sup>-2</sup> s	(+)	N/A	2.2.1
SIGNAL TRAVEL TIME CORRECTION	–2.67 x 10 <sup>–3</sup> s	(+)	N/A	2.2.1
CENTER OF GRAVITY OFFSET adjusts measurement to s/c center of mass	~ 6.04 m	N/A	()	2.2.2
IONOSPHERIC REFRACTION CORRECTION accounts for signal delay	~ 2–3 cm	N/A	(+)	2.3.1
TROPOSPHERIC REFRAC- TION CORRECTION accounts for signal delay	~ 1.5–2.5 m	N/A	(+)	2.3.2
SOLID TIDE removal	~ 2–10 cm.	N/A	(-)	2.4
ORBIT ADJUSTMENT reduces orbit error and references the data to a mean ocean surface	3m≤∆H <sub>ORB</sub> ≤3m	N/A	(–)	2.5
SLOPE CORRECTION accounts for signal being returned from closest point within satellite footprint	Om≤∆H <sub>SLOPE</sub> <80m	N/A	()	2.6

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## Table 5. Waveform Data Record Description

General Characteristics:

Record Format	-	variable
Record Size (bytes)	-	170 + 4 for IBM record control word
Blocksize (bytes)	-	31842 + 4 for IBM block control word

<u>Bytes</u>	FORTRAN Variable Type	Descriț	otion												
1-8	R*8	Fractio	n of day p	ast midnight from sensor data record											
9-16	R*8	Altimet	er range m	easurement in meters from sensor data record											
17-20	R*4	Satellit	e latitude	in degrees from sensor data record											
21-24	R*4	Satellit	e east long	gitude in degrees from sensor data record											
25-28	R*4	Altitud	e error ∆h	in meters											
29-32	R*4	Altitud	e rate erro	$r \Delta h$ in meters/sec											
33-36	I*4	Modifie	ed Julian I	Date of observation from sensor data record											
37-38	I*2	Signific	Significant wave height (H 1/3) in cm.												
39-40	I*2	Autom	Automatic Gain Control (AGC) in dB												
41-166	I*2	Wavefo	rm counts												
167-168	I*2	Word i	ndicating o	original data flags											
		 0		-  15											
		<u>Bits</u>	Value	Description											
		0-10		Unused											
		11	1	Not in track mode											
		12	1	Chirp/cw											
		13	1	Altimeter error status											
		14	1	Reacquisition											
		15	1	Acq/Trk											

Table 5.	Waveform	Data	Record	Descrip	ption	(Cont.)
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<u>Bytes</u>	FORTRAN Variable <u>Type</u>	Descript	tion	
169-170	I*2	Retrack	ing status v	word
		 0	 1!	5
		<u>Bits</u>	Value	Description
		0		Unused
		1	0	Gains and offsets were not applied to waveform counts in plots and in determining $\beta$
			1	parameters Gains and offsets were applied to waveform counts in plots and in determining $\beta$ parameters
		2	0 1	Specular test not performed or waveform not specularly shaped Waveform determined to be specularly shaped
		3	0 1	Status flag from SDR less than or equal to one Status flag from SDR greater than one
		4	0 1	Waveform not specularly retracked Waveform specularly retracked
		5	0	Gains and offsets not applied to waveform
			1	Gains and offsets applied to waveform count values on WDR's
		6	0	For double waveforms the retracking correction is not calculated from a weighted average of
			1	For double waveforms the retracking correction is calculated from a weighted average of the two leading edges

## Table 5. Waveform Data Record Description

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Detes	FORTRAN Variable	Descrip	tion	
Byles	<u> </u>	Deserip		
169-170		<u>Bits</u>	Value	Description
(cont.)		7	0 1	No problem with leading edge definition of m Waveform not defined well enough to filter, no leading edges or too many leading edges
		8	0 1	No problem retracking Problem retracking
		9	0 1	Timing bias was not applied to time tag Timing bias applied to time tag
		10	0 1	Waveform not retracked Waveform retracked
		11	0 1	Whole edge retracked Leading edge retracked
	applies to	12	0 1	Ht correction not applied due to $\dot{h}$ Ht correction applied due to $\dot{h}$
	water data	13	0 1	Attitude seastate correction not applied to $h$ Attitude seastate correction applied to $h$
		14-15	0 1 2 3	Tracking mode 1 Tracking mode 2 Tracking mode 3 Tracking mode 4

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1 AT-1 01		71.60	71.60	71.60	71.60	71.60	71.60	71.60	71.60	71.60	71.60	71.60	71.60	71.60	71.60	71.60	71.60	71.60	71.60	71.60	71.60	71.60	71.60	71.60	71.60	71.60	71.60	no.1/	71.60	71.60	71.60	71.60	71.60	71.60 71.60
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Table 6. Seasa	3 SW CORNER	329.19 329.59 329.99	330.39 330.79	331.59	555.59 334.79 335.59	335.99	304.00 304.40	304.80	307.20	307.60 308.00	508.40 308 80	309.60	310.40	510.80 311.20	311.60 312.00	312.40	313.20	314.00	314.40 314.80	315.20	316.00	316.40 316.80	317.20	318.00	318.40 318.80	319.20	320.00	320.40 320.79	321.19 321.59
	LAT-LON(	71.60 71.60 71.60	71.60	71.60	71.60 71.60 71.60	71.60	71.70	11.70	71.70	71.70		71.70	71.70	71.70	71.70	71.70	21.70	71.70	71.70	71.70	71.70	71.70	71.70	71.70	71.70	71.70	71.70	71.70	71.70
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	BIN NUMBER	3874 3875 3876	3877 3878	3880	3885 3888 3880	3891	3911 3912	3913	5914 3919	3920 3921	3922	3925	5926 3927	3928 3929	3930 3931	3932	3934	5955 3936	3937 3938	3939	3941	3942	3946	3946	3947 2048	3949	3951 3951	3952 3953	3954 3955

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3957	143	71.70	322.39	187(21)	230(	15.	4310	13)	474(	22)	631(	22)	6750	()
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3978	1	71.70	330.79	445( 4)	6450	3)								
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4028	55	71.80	310.80	1191( 1) 173( 21)	201(	3)	244(	5)	417(	10)	445(	()	488(	2
4029	85	71.80	311.20	173( 12)	244(	14)	417(	3)	460(	13)	488(	13)	1034(	5
4030	24	71.80	311.60	1163( 10) 244( 10)	1249(	15) 7)	12065	(,						
4031	68	71.80	312.00	173( 8)	244(	16)	287(	200	460(	1)	488(	21)	775(	5)
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R PTS)	60( 22) 5 03( 20) 7	46( 8) 7		247 CT7	90(21) 90(17) 8	33( 21)	33(21) 8 32(21) 6	59( 22) 6	59( 21) 6	159(21) 6	(12)18	131( 4)			761( 21)		804( 2) 832( 3)	804( 17) 875( 2)	(7)2(2)	890(22)	847(2) 546(4)						
REV (NUMBE	287(22) 4 460(13) 5		546(22) 6 546(22) 6		617(19) 7 632(3) 7	833(21) 632(21) 8	632( 21) 8 459( 21) 6	431(21) 4	431(21) 4	431(21) 4 258(21) 4	876( 22) 258( 21) 4	258( 22)	4/4( ZZ) 474( 14)		588( 12) 588( 12)	761( 6)	631( 3) 804( 10) 3	631( 1) 804( 9)		847(2)	689( 8) 473( 1)	019( 2)	COT JC44	760( 2)			
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IG SM CORNER	312.80 313.20	313.60 314.00	314.40 314.80	315.60 315.60	010.010 316.40 316.80	317.20	518.00 318.00		319.20	319.60 320.00	320.40	320.79	321.19 321.59	321.99 322.39	522.79 323.19	323.99 323.99	324.39	325.19	325.99	326.39	327.19	10.120	327.99 328.39	329.19	329.99	332.79 333.19	333.99
S LAT-LON	71.80 71.80	71.80	71.80	71.80	08.17 71.80 80	71.80	71.80	00.17	71 80	71.80	71.80	71.80	71.80	71.80	71.80	71.80	71.80	71.80	71.80	71.80	71.80	no.1/	71.80	71.80	71.80	71.80	71.80
NUMBER PTS	103 92	80 77	68 72	60	8 6 9 8 8 6 9 8	N (0) V D VO V	91 91	5 J F	711 711	126	146 146	104	90 81	63 67	50 53 53 53 53 53 53 53 53 53 53 55 55 55	46 25	20	194	2	22	233	7	6 28 6	ы. К	N 00 №	0~~	. 4
<b>BIN NUMBER</b>	4033 4034	4035 4036	4037 4038	4039 4040	4041 4042	4040	10/0 70/0 70/0	404	8404	4050	1CU4	4053	4054 4055	4056 4057	4058 4059	4060 4061	4062		4066 4066	4067 4068	4069	4070	4071 4072	4074	4076 4076	4002 4083 4084	4086

				(6	5)	2)	8)	<b>( )</b>	6.3		8) (2	(61	21)	(11)	(6	16.)	10)	2)	(6	21)	21)	18)	(61	(12
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5	3.6	31	<del>3</del> 95	32	3)	1	3)		ຊຸລລະ	21) 21)	21)	19)	21)	21)	2 <u>5</u> ;		55	21)					16)	556
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5	193 193	2222	2883	356	222	<u> </u>		150		20) 10)	<b>8</b> 66	<b>.</b>				<u>]</u> @;								
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SW CORNER	54.79 55.59	00.80 00.80 00.80	07.20 8.40 8.40	19.20	19.60	0.00	0.40	0.80	1.20	2.00	2.40	2.80	3.20	3.60	4.00	4.40	4.80	5.20	5.60	6.00	6.40	6.80	7.20	7.60
ONG S	000	, , , , , , , , , , , , , , , , , , ,		20 20 20	0 30	0 31	0 31	0 31	121	0 31	31	0 31	31	31	31	31	1 31	1 31	1 31	1 31	31	1 31	31	31
LAT-L	71.8	66.6	6.12 1/2	71.9	71.9	71.9	71.9	71.9	71.91	71.90	71.90	71.9(	71.90	71.9(	71.9(	71.90	71.90	71.90	71.90	71.90	71.90	71.90	71.90	71.90
NUMBER PTS	μÖκ	)M4H1	161 161	38	38	43	53	85	15 66	51	170	177	120	136	140	146	134	150	182	168	169	167	182	164
BIN NUMBER	4088 4090 4112		4119 4121 4122 4123	4124	4125	4126	4127	4128	4129 4130	4131	4132	4133	4134	4135	4136	4137	4138	4139	4140	1414	4142	4143	4144	4145

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		<u> </u>		660	10)	12)	122	18)	13.0	12 12	)CC	95	51)	190	30	<b>~~</b>	<u>5</u> 6	21)	<b>1</b> 60		; A A	21)	ନିତ୍	20) 19)	6	5120
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	SW CORNER	305.20 305.60 306.00	306.40	308.00 308.40	308.80		309.20	309.60	310.00		310.40 310.80		311.20		N9.11c	312.00		312.40	512.80		513.20		513.60		00 91	0 0 1
		72.00 72.00 72.00	72.00	72.00	72.00		72.00	72.00	72.00		72.00		72.00		12.00	72.00		00.27	72.00		72.00		72.00		10 22	, , , ,
ALLMBED DTC	NUMBER 113	242 10	σM	32 34	155		101	195	139		32 137		290	14.0	001	129		167	343		299		300		384	-
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	431(21) 646(20) 847(20)	431(21) 646(21) 847(21)	431(21) 646(21) 847(21)	273( 21) 560( 21) 804( 21)	445(20) 646(20) 890(20)	445(21) 646(21) 890(21)	445(21) 646(21) 890(21)	287(14) 646(21) 890(21)	445(20) 689(21) 1019(21) 488(21)	761( 18) 488( 21)	488( 21) 488( 21) 775( 18)	488( 20) 804( 20)	488( 21) 775( 20)	488( 21) 775( 21)
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		rable 7	. Seasat C	seo-referenced Data Base Header Description
FILE 1:	GEO-REFEI Record Forr Blocksize:	RENCED I nat: Or 48	DATA BAS le logical i 0 Bytes	E HEADER RECORD record corresponds to one physical record
	FORTRAN Variable			
Bytes	Туре	Descri	ption	
1–4	I*4	Numb	er of latitu	ide rows in the data base (56)
5–8	<b>]*4</b>	North (72100	vestern-me )00)	ost latitude of data base in degrees North (x $10^5$ )
9-12	I*4	Northy (30000	vestern-me )000)	ost longitude of data base in degrees East (x 10 <sup>5</sup> )
13–16	I*4	Southe (59900	eastern-mo )00)	ost latitude of data base in degrees North (x $10^5$ )
17–20	I*4	Southe (34000	eastern-mo )000)	ost longitude of data base in degrees East (x $10^5$ )
21–244	I*4	Width southe rows i	of each la rnmost ro n the data	titude row in degrees (x 10 <sup>5</sup> ), starting with the w. This is dimensioned by the number of latitude base.
245-468	I*4	The nu with th of latit	umber of le le souther ude rows	ongitude divisions in each latitude row, starting nmost row. This is dimensioned by the number in the data base.
469-472	I*4	Logical	l record ir	n data base at which directory starts.
473-476	I*4	Size of	the data	base, including the directory, in blocks.
477-480	I*4	Status	word for	altimetry data.
		 0		 
		<u>Bits</u>	value	Description
		0-23	0	Unused
		24	1	Slope correction applied
		25	1	Orbit adjustment applied
		00	0	Orbit adjustment not applied
		26	0	Solid tides removed Solid tides not removed

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Table 7. Seasat Geo-referenced Data Base Header Description (Cont.)

(477-480 (	Cont.)	)
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<u>Bits</u>	<u>Value</u>	Description
27	1	Retracking correction applied
	0	Retracking correction not applied
28	1	Center of gravity bias applied
	0	Center of gravity bias not applied
29	1	Tropospheric correction applied
	0	Tropospheric correction not applied
30	1	Ionospheric correction applied
	0	Ionospheric correction not applied
31	1	Time bias applied
-	0	Time bias not applied

Table 8. Seasat Geo-referenced Data Base Description

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FILE 2: GEO-REFERENCED DATA BASE Record Format: 595 logical records correspond to one physical record Blocksize: 19040 Bytes

Subgroup 1: One logical record for each bin containing data

<u>Bytes</u>	FORTRAN Variable Type	Description
1-4	I*4	Indicates the number of logical records which follow which are located in the bin
5–32		Unused

Subgroup 2: One logical record for each data point in the bin

	FORTRAN Variable	
<u>Bytes</u>	Туре	Description
1-4	I*4	North latitude of datum point in degrees (x $10^6$ )
5–8	I*4	East longitude of datum point in degrees (x $10^6$ )
9–12	I*4	Surface height relative to the ellipsoid in cm.
13–16	I*4	Height sigma, arbitrary value of 1.0 m used (x $10^5$ )
17–18	I*2	Rev number
19–20	I*2	Used for temporary flags when gridding the data
21–24	I*4	Orbit adjustment in meters (x $10^5$ ) (-9999999999 if unavailable)
25–28	I*4	RMS of orbit adjustment in meters (x $10^5$ ) (-9999999999 if unavailable)
29–32	I*4	Slope correction in meters (x $10^5$ ) (-9999999999 if unavailable)

NOTE: Subgroups 1 and 2 are repeated for as many bins with data.

Table 8. Seasat Geo-referenced Data Base Description (Cont.)

Subgroup 3: Directory

	FORTRAN Variable	
<u>Bytes</u>	Туре	Description
1-4	I*4	Record number at which data for bin 1 starts
5–8	I*4	Record number at which data for bin 2 starts
9-12	I*4	Record number at which data for bin 3 starts
13–16	I*4	Record number at which data for bin 4 starts
17-20	I*4	Record number at which data for bin 5 starts
21-24	I*4	Record number at which data for bin 6 starts
25–28	I*4	Record number at which data for bin 7 starts
29–32	I*4	Record number at which data for bin 8 starts

NOTE: The directory contains as many 32-byte logical records as necessary to designate the record locations of all bins.

Table 9. Elevation Grid Header Description

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FILE 4: ELEVATION GRID HEADER RECORD Record Format: One logical record corresponds to one physical record Blocksize: 80 Bytes

	FORTRAN Variable			
<b>Bytes</b>	Type	Desc	ription	
1-4	I*4	Num stere	ber of lat ographic g	itude increments in the grid for a non-polar rid (140)
5–8	I*4	Num stere	ber of lon ographic g	gitude increments in the grid for a non-polar rid (152)
9–12	I*4	Start be ap	ing north l	atitude of grid in degrees North (x 10 <sup>6</sup> ) (this will for a polar stereographic grid) (50000000)
13-16	I*4	Start be ap	ing east lo proximate	ngitude of grid in degrees East (x 10 <sup>6</sup> ) (this will for a polar stereographic grid) (300000000)
17–20	I*4	Endir be ap	ng north la proximate	titude of grid in degrees North (x $10^6$ ) (this will for a polar stereographic grid) (73000000)
21-24	I*4	Endir appro	ng east long ximate for	gitude of grid in degrees East (x $10^6$ ) (this will be a polar stereographic grid) (340000000)
25–28	I*4	Statu: positi	s word for on indicate	data used to generate grid. A zero in any bit es that the correction is not applied.
		 0		 31
		Bits	<u>Value</u>	Description
		0-23		Unused
		24	1	Slope correction applied
			0	Slope correction not applied
		25	1	Orbit adjustment applied
			0	Orbit adjustment not applied
		26	1	Solid tides removed
		07	0	Solid tides not removed
		21	1	Retracking correction applied
		28	1	Center of growity biog on the
		20	0	Center of gravity bias applied
		29	1	Tropospheric correction applied
			Ō	Tropospheric correction not applied
		30	1	Ionospheric correction applied
			0	Ionospheric correction not applied
		31	1	Time bias applied
			0	Time bias not applied

## Table 9. Elevation Grid Header Description (Cont.)

Distan	FORTRAN Variable	Description
Bytes	<u> </u>	Description
29–32	I*4	Polar stereographic grid size conversion and scaling factor from half-inch grids on projection plane to the desired grid size (x $10^6$ ) (1650000)
33–36	I*4	The number of grids of desired size from the pole to the equator based on the grid size conversion and scaling factor $(x \ 10^6)$ (608754894)
37-40	I*4	Latitude of the map perimeter in degrees North (x 10 <sup>6</sup> ) (500000000)
41-44	I*4	Greenwich orientation in degrees (x $10^6$ ) (45000000)
4548	I*4	Polar stereographic switch (1) =0, grid has constant increment in latitude and longitude =1, grid is in polar stereographic projection
49–52	I*4	Number of I-axis divisions to the extent of the map perimeter (445)
53–56	I*4	Number of J-axis divisions to the extent of the map perimeter (445)
57-60	I*4	J coordinate of the projected pole (223)
61-64	I*4	I coordinate of the projected pole (223)
65–68	I*4	Minimum J index of the grid (166)
69–72	I*4	Maximum J index of the grid (317)
73–76	I*4	Minimum I index of the grid (305)
7780	I*4	Maximum I index of the grid (444)

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## Table 10. Elevation Grid Description

FILE 5:	ELEVATION GF Record Format: Blocksize:	RID DATA RECORD 10 logical records correspond to one physical record 1800 Bytes		
<u>Bytes</u>	FORTRAN Variable <u>Type</u>	<u>Description</u>		
1-4	I*4	Condition number of the matrix used in the least-squares solution to the function $(x \ 10^6)$		
5-8	I*4	Capsize in degrees latitude - radius from grid location defining area from which data was used to define grid (x $10^6$ )		
9-12	I*4	North latitude of grid point in degrees (x $10^6$ )		
13-16	I*4	East longitude of grid point in degrees (x $10^6$ )		
17-20	I*4	Height values of the grid at location relative to sea level in meters $(x \ 10^5)$		
21-24	I*4	Number of data values that were used to calculate grid value		
25-28	I*4	Number of parameters used to define function, NPT, (equals 0, 3, or 6)		
29-52	I*4	Six gridding function coefficients. If NPT is $< 6$ then the rest of the coefficients are initialized to zero. (x $10^5$ )		
53-76	I*4	Set of null coefficients associated with any negligible singular values (see SVD reference). If NPT is < 6 then rest of coefficients are initialized to zero (x $10^6$ )		
77-80	I*4	Distance in km from grid locations to closest data point (x $10^6$ )		
81-84	I*4	North latitude of closest data point to grid location in degrees $(x \ 10^6)$		
85-88	I*4	East longitude of closest data point to grid location in degrees $(x \ 10^6)$		
89-92	I*4	Height associated with closest data point to grid location in meters (x $10^5$ )		
93-96	I*4	Standard deviation of the data with respect to the gridding function in meters (x $10^6$ )		
97-180	I*4	Correlation matrix from solution. This is a symmetrical 6 X 6 matrix so only the upper triangular portion is stored. The order of storage is elements $1-6$ are the first row elements, $7-11$ columns $2-6$ of second row etc. (x $10^5$ )		

NOTE: Ten of the above-mentioned 180-byte logical records make up one block of data.

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16. Abstract The data processing metho altimeter measurements ov are documented in this fi and applied to the Seasat detail, including the edi height errors caused by 1 methods for radial adjusts errors are given. The va report, but the user is r for more detailed descrip geo-referenced data bases	ds and ice data er the Greenland rst volume of a radar altimeter ting and retrack ags in the autom ment of the orbi rious levels of eferred to Volum tions of the grid	products deriv ice sheet and series. The c data over ice ing algorithm atic range tra- ts and estimat ice data sets es 2 (Greenland ded elevation	ed from Seasat surrounding s orrections der are described to correct for cking circuit. ion of the slo are described d) and 4 (Anta data sets and	radar ea ice ived in The pe-induced in this rctica) the
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