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# Satellite Radar Altimetry Over Ice 

Volume 1-Processing and
Corrections of Seasat Data
Over Greenland
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Anita C. Brenner,
Judith A. Major,
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and Robert A. Bindschadler

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## Satellite Radar

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Over Greenland
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The data-processing methods and ice data products derived from Seasat radar altimeter measurements over the Greenland ice sheet and surrounding sea ice are documented in this first volume of a series. The corrections derived and applied to the Seasat radar altimeter data over ice are described in detail, including the editing and retracking algorithm to correct for height crrors caused by lags in the automatic range tracking circuit. The methods for radial adjustment of the orbits and estimation of the slope-induced errors are given. The various levels of ice data sets are described in this report, but the user is referred to Volumes 2 (Grecnland) and 4 (Antarctica) for more detailed descriptions of the gridded elevation data sets and the gco-referenced data bases.

## INTRODUCTION

This volume is the first in a series documenting the data-processing methods and ice data products derived from satellite radar altimeter measurements over the ice sheets of Greenland and Antarctica and surrounding sea ice. The data-processing procedures and corrections derived and applied to the Seasat radar altimeter data are described in detail in this report. A flowchart depicting the procedures involved in obtaining the various data products is given in Figure 1. A detailed description of the editing and retracking algorithm is given in Section 2, along with descriptions of the other corrections. The methods for radial adjustment of the orbits and estimation of the slope-induced errors are described. The various levels of ice data sets produced are described in this report, but the user is referred to Volumes 2 and 4 for more detailed descriptions of the gridded elevation data set and the geo-referenced data base.

The input Seasat radar altimeter data, in the form of Geophysical Data Records (GDR's) and Sensor Data Records (SDR's) produced by NASA's Seasat project at the Jet Propulsion Laboratory, were obtained from the NOAA Environmental Satellite Data and Information Scrvice (EDIS) archive on about 1000 magnetic tapes. Development of the data processing methods, the production of higher-level geophysical data products, and analysis and cvaluation of the data have been supported at the Goddard Space Flight Center by funding for research and data analysis, provided primarily by NASA's Ocean Processes Program and by the Climate program. Computer programming and technical assistance has been provided by the EG\&G Washington Analytical Services Center, Inc. until January 1989 and by ST Systems Corporation since then. Numcrous other individuals have provided valuable assistance.

Results have been reported in refereed scientific literature (e.g., Brenner et al., 1983; Martin et al., 1983; Zwally et al., 1983; Thomas et al., 1983; and Gundestrup et al., 1986). In addition, elevation data in various forms have been provided to other scientists and placed in the National Snow and Ice Data Center (NSIDC) and the National Space Science Data Center (NSSDC). The purpose of this series of reports is to document technical details and provide guidance to users of the ice data products.

While all reasonable quality-control efforts have been made to eliminate erroncous data, some data of questionable quality is likely to have persisted, particularly in the lower-level data products. Users should apply normal standards of scientific caution in their use of the data.


Figure 1. Processes Involved in Obtaining Data Products

The current list of reports is:

Satellite Radar Altimetry over Ice, Volume 1: Processing and Corrections of Scasat Data over Greenland, July 1989. This volume.

Satellite Radar Altimetry over Ice, Volume 2: User's Guide for Grcenland Elevation Data from Seasat, July 1989. NASA Reference Publication. $\qquad$ -.

Satellite Radar Altimetry over Ice, Volume 4: User's Guide for Antarctic Elcvation Data from Seasat, July 1989. NASA Reference Publication. $\qquad$ -.

Volume 3 will be the Antarctic equivalent of Volume 1. Additional volumes will include descriptions of the data sets being produced by NASA from the radar altimeter data acquired by the U.S. Navy's GEOSAT, using methods similar to those for the Seasat data.

The Seasat spacecraft (e.g., Lame and Born, 1982 and Lame et al., 1980) was launched in late June 1978, and during its brief 110-day lifetime, collected 90 days of nearly continuous radar altimeter data from July 9 through October 10 between the latitudes of $72^{\circ} \mathrm{S}$ and $72^{\circ} \mathrm{N}$. Although designed only for measurements over water, the Seasat radar altimeter (MacArthur, 1978; Tapley et al., 1982; and Townsend, 1980), acquired more than 600,000 uscful altimeter range measurements over the continental ice sheets of Greenland and Antarctica.

Over sloping and undulating surfaces, such as ice covered land, or surfaces with highly-variable reflecting characteristics, such as in regions of sea ice, the range to the surface and the characteristics of the received radar pulse changed faster than the response capability of the altimeter electronics. Consequently, it has been necessary to correct each range value for lags of the altimeter range servo-tracking circuitry by a procedure called retracking (Martin et al., 1983). The retracking correction typically had a mean value of +1.4 m as applicd to the surface clevation, a standard deviation of 2.9 m , and maximum and minimum values of $\pm 15 \mathrm{~m}$. In addition, the pulse-limited footprint ( 1.6 km minimum diameter), which was located near the satellite nadir point over the relatively flat ocean, was in general located anywhere within the beam-limited footprint ( 22 km in diameter) over sloping surfaces. The resulting slope-induced error, which was nearly 80 m over slopes of 0.8 degree, can be partially corrected using the procedures described in Brenner et al., 1983. Corrections are also made for errors in orbit determination, atmospheric propagation path-length variations, and earth and ocean tides.

Elevation measurements were obtained at $0.1-$ second intervals, corresponding to $662-\mathrm{m}$ intervals along the subsatellite ground track. The precision of the corrected range measurements is about 1.6 m overall with a minimum of about 0.25 m in the smoothest regions of the ice shects
(Zwally et al., 1983). The 5- to $10-\mathrm{cm}$ precision over the ocean is for 1 -sec data averages.) The absolute accuracy of the elevations is primarily determined by the limitations on the correction methods for the slope-induced errors and uncertainties in the geoid reference level.

The principal ice data sets produced and/or retained are:

Level 4: Contour maps and gridded elevations with respect to earth ellipsoid and sea level (e.g., this Volume and Volume 2).

Level 3: Geo-referenced data base including all individual elevation measurements (including time, latitude/longitude positions, and slope-correction estimates) accessible by geographic cells (e.g., this Volume and Volume 2).

Level 2: Ice Data Records (IDR's). Orbital-format data records including altimeter parameters, corrected elevations, latitude/longitude positions, AGC, applied corrections, retracking beta parameters, and estimates of along-track and cross-track slope corrections. (this Volume)

Level 1: Waveform Data Records (WDR's). Orbital-format data records including waveform amplitudes by gate, ranges, AGC, and latitude/longitude positions. (this Volume)

Sensor Data Records (SDR's)
Geodetic Data Records (GDR's)

## SECTION 2.0

ICE DATA RECORDS

The Seasat altimeter data were released in two forms: the Altimeter Sensor Data Record (hereafter referred to as SDR), and the Geophysical Data Record, GDR. The SDR's were obtained from the NOAAEDIS archives and contain, among other quantities, the telemetered range measurements between the spacecraft and earth's surface, averaged radar return pulses, the altimeter status flags and the satellite latitude, longitude, and elevation. The data are output in $0.098-\mathrm{sec}$ intervals. The GDR's contain processed SDR data averaged over $1-\mathrm{sec}$ intervals, and the sensor, atmospheric, and surface dynamic corrections necessary to utilize the data in detailed geodetic work. Data over the ice sheets are not available from the GDR's.

To obtain the ice sheet elevation measurements, data from the SDR's are used and the appropriate corrections and adjustments applied. This subset of ice sheet data obtained from the SDR's is referred to as ice data records or IDR's. A detailed description of these records may be found in Table 1. The surface heights, located in bytes 73-76 of the IDR, are referenced to the IUGG 1980 Geodetic Reference Ellipsoid (Moritz, 1980), which is defined with a $6378.137-\mathrm{km}$ semi-major axis of the earth and a flattening ratio of $1 / 298.257$. Heights relative to sea level can be calculated by subtracting the geoid value from the surface height. Geoid values, linearly interpolated from a one-by-one degree GEM10-B geoid grid, are located in bytes 61-64 of the IDR.

Figure 2 is a map of Greenland which depicts the coverage obtained from the IDR's after data were edited and retracked (see Section 2.1). The gaps in the data are a result of the altimeter not being able to maintain valid height measurements over the rougher surfaces of the ice sheets. Table 2 gives a concise catalog of the available Seasat Greenland IDR data. Included in this table are the start and stop locations of each rev, the number of points in each rev, and the data base bins (see Section 4.0) through which each rev traverses. The rev numbers are ordered such that all ascending passes are listed first, ordered by increasing latitude as they cross 315 degrees East Longitude. Then the descending passes are listed using the same ordering criterion as for the ascending passes.

### 2.1 EDITING AND RETRACKING

As explained in Section 1.0, Seasat altimetry returns over non-ocean surfaces required special processing in order to calculate meaningful height measurements. To understand this processing one must first have an understanding of the return itself.


Each altimeter return, referred to as a waveform, consists of the output of a set of 63 gates that span a height window of approximately 30 m . Each gate has a level of return associated with it measured in counts. A typical occan return from Seasat is presented in Figure 3. The level of return in the first 22 gates is at the noise or pre-pulse level of 4 or 5 counts. The level quickly increases to a relative maximum and then slowly decreases over the latter portion of the window. There are three half-gates at the center that have a spacing of 23 cm instead of 46 cm . The tracking gate is the center of these. The on-board tracker attempts to kecp the center of the return leading edge positioned at the tracking gate by predicting the travel time of each pulse based on previous returns. The measurement telemetered from the altimeter is equivalent to the travel time to the tracking gate.

Altimeter returns over non-ocean surfaces vary greatly from this ocean return. Figure 4 shows representative returns over ice sheet surfaces for a Seasat pass over Antarctica (Martin et al., 1983). The Figure 3 sea ice returns are represented by one or more sharp spikes that may or may not be at the tracking gate. As the altimeter travels onto the ice shelf, acquisition is lost, represented as a flat return. On the ice shelf the returns are shaped similar to the oceans, but again are not always centered at the tracking gate. As the satellite moves over the ice sheet, acquisition is again lost temporarily. Over the ice shects the returns are noisy, have multiple leading edges, and the mid-point of the first leading edge is not always aligned with the tracking gate.

The measurement telemetered from the on-board tracker needs to be corrected for the variation of the mid-point of the leading edge from the tracking gate. This retracking correction, $\Delta H_{r e t}$ is calculated as

$$
\begin{equation*}
\Delta H_{\mathrm{ret}}=(\mathrm{Gm}-\mathrm{Gt})^{*} \mathrm{~g} 2 \mathrm{~m} \tag{2.1}
\end{equation*}
$$

where

```
Gm = gate of the mid-point of the leading edge (sce Sections 2.1.3-2.1.4),
Gt = the tracking gate (29.5 where the whole gates are numbered from 0 to 59; sce
        Figure 3), and
g2m = the conversion from gates to meters =.4684375 m/gate.
```


Figure 3. Ideal Ocean Altimetry Return Pulse

It then follows that

$$
\begin{equation*}
\mathrm{H}_{\mathrm{ret}_{\mathrm{t}}}=\mathrm{H}_{\mathrm{meas}_{\mathrm{t}}}+\Delta \mathrm{H}_{\mathrm{ret}}^{\mathrm{t}+1} \mathrm{l} \tag{2.2}
\end{equation*}
$$

where
$H_{r e t}=$ the retracked altimeter measurement at time $t$,
$\mathrm{H}_{\text {meas }}=$ the measurement calculated by the on-board tracker at time t , and
$\Delta \mathrm{H}_{\mathrm{ret}}^{\mathrm{t}+\mathrm{l}}=$theretrackingcorrectioncalculatedfromwaveformattime $\mathrm{t}+.098 \mathrm{sec}$.

Due to the return being telemetered one time step later, the retracking correction for the measurement at time $t$ is calculated from the return at time $t+.098 \mathrm{sec}$. Methods have been developed at NASA/GSFC to calculate the $\Delta H_{\text {ret }}$ for returns over the ice sheet, ice shelf, and sca ice which can yield valid height measurements. A detailed description of these procedures may be found in Sections 2.1.3 and 2.1.4. Parameters resulting from these retracking techniques may be found in bytes 109-144 of the IDR. The criteria used to automatically select and discriminate between different types of returns are described in the next two sections.

### 2.1.1 Selecting Retrackable Non-Ocean Altimetry Returns

The SDR for Scasat includes all telemetered altimeter data even when the instrument was in calibration or standby mode. Since valid measurements could be acquired when the tracker was in acquisition mode, all data that are not in acquisition or track modes are discarded.

All tracking and acquisition returns have to meet two initial tests to determine if the waveform actually represents the initial return, or if the return is outside the tracking window.

1) The counts in the first gate must be less than 100 :
2) There must be at least one gate with a count value greater than 25.

### 2.1.2 Categorizing the Returns

The remaining returns are then categorized into two groups. Group one will be referred to as specular and consists of those returns that display a sharp spike. Returns in this catcgory are usually found in regions of sea ice or over flat, desert-type surfaces. The second group, consisting of the remaining returns, is called diffuse and resembles ocean returns. These returns
are found over continental ice and the ice shelves. Different methods are used to retrack each group.

Returns are automatically categorized as either diffuse or specular depending on the existence of a significant spike in the return. To determine this the following algorithm is used. The noise level, Yn, is calculated as the average number of counts in the first five gates. The maximum, Ymax, is calculated as the maximum number of counts in any gate. The value Ymed is then calculated using the equation

$$
\begin{equation*}
\text { Ymed }=\frac{(Y \max -Y n)}{2.0}+Y n \tag{2.3}
\end{equation*}
$$

The gate number, Gmid, is then found as the first gate where the number of counts excecds Ymed. Two sums of consecutive counts from the signal are then formed, Ylow and Yhigh, where

$$
\begin{align*}
& \text { Ylow }=\sum_{i=\text { Gmid }}^{i=\text { Gmid }_{1}+9} \mathrm{Y}_{1}  \tag{2.4}\\
& \text { Yhigh }=\sum_{\mathrm{i}=\text { Gmid }+10 .} \mathrm{Y}_{\mathrm{Gmid}}+20 \tag{2.5}
\end{align*}
$$

If Gmid is so large that there are less than 20 remaining gates, then the number of gates used to form the sums is adjusted. When the ratio of Yhigh/Ylow is $\leq 0.7$, the return is considered specular.

### 2.1.3 Retracking Specular Type Returns

Specular waveforms are not found in the Seasat altimeter data over Greenland. This is probably due to the absence of sea ice near Greenland during Seasat's lifetime. As a result, all of the Greenland returns are retracked using the diffuse method. However, for the sake of completeness, the method used to retrack specularly shaped returns, which is employed in the region of the Antarctic, will be discussed.

Specular-type returns are defined for this procedure as being characterized by one or more extremely sharp spikes and are retracked by attempting to locate the mid-point or halfpower point of the first significant spike. In addition, since the shape of the return essentially records topographic characteristics, parameters are also calculated which define the shape of a single-or double-peak return. Figure 5 a shows the five-parameters required to define a singlepeak return, while Figure 5b shows the nine-parameters required for a double-peak return.

### 2.1.3.1 Half-power Point of First Significant Peak

In determining the mid-point of the first significant spike, the location of this spike must first be found. The value of Ymed, which is calulated to determine whether or not the return is specularly shaped (Equation 2.3), is used. Starting with the gate number prior to Gmid, where Gmid is define to be the gate number whose counts exceed Ymed, a gate is sought whose counts exceed or equal $25 \%$ of the difference between Ymax and Yn. Upon finding this gate, Grise, it is determined to be the first significant spike if the following conditions are met:

$$
\begin{align*}
Y_{\text {Grise+1 }} & -Y_{\text {Grise }}
\end{align*}<0.0 \text { Ymax } * .3
$$

where

$$
\begin{array}{cl}
Y_{\text {Grise }} & \text { is the counts for gate Grise, and } \\
Y_{\text {Grise }+1} & \text { is the counts for gate Grise }+1 .
\end{array}
$$

Smaller, more rounded waveforms, which might be encountered in the vicinity of an ice shelf require that the following condition be met:

$$
\begin{array}{rlr}
Y_{\text {Grise }+1} & -Y_{\text {Grise }} & <(\text { Ymax-Yn }) * .05 \\
& \text { for } Y_{\text {Grise }} & \leq Y_{m a x} * .3 . \tag{2.7}
\end{array}
$$

Grise is incremented by one, up to the maximum number of gates, until one of the above conditions is met, after which the gate of the first significant spike, Glst, and its corresponding counts, Y1st, are used to determine the half-power point of the peak. The count value at the halfpower point, Ymidl, is determined as follows:

$$
\begin{equation*}
\text { Ymid } 1=\frac{(Y 1 \text { st-Yn) }}{2.0}+Y n \tag{2.8}
\end{equation*}
$$

The exact gate location of the half-power point, Gtmid 1 , is then determined by performing a linear interpolation for the count value Ymid1 located between gates X 1 and X 2 , with corresponding count value Y1, Y2.

### 2.1.3.2 Remaining Parameters to Define Shape

In order to define the exact shape of the specular returns depicted in Figures 5a and 5b, it is necessary to calculate several other parameters in addition to the noise level, the maximum counts of the first significant peak, and the gate location of the half-power point. For the singleand double-peak return, additional quantities which define the width of the significant peak and slope at the half-power point are defined. A double-peak return has four additional quantities calculated: the maximum counts for the second significant peak, the gate location of the halfpower point for the second peak, the slope at the second half-power point, and the minimum counts found between the two significant peaks.

The slopes at the half-power point for both the first and second significant peaks, Slp 1 st and Slp2nd, are determined by the following algorithm:

$$
\begin{equation*}
\text { Slp1st }=\frac{\mathrm{Y} 2-\mathrm{Y} 1}{\mathrm{X} 2-\mathrm{X} 1} \tag{2.9}
\end{equation*}
$$

Slp2nd uses the gate locations and corresponding counts determined to surround the half-power point of the second significant peak. These values are found in a manner similar to that of the first peak.

The actual existence of a second significant peak is determined in the following manner. Starting with the gate location of the first significant peak, the difference between counts of consecutive gates is monitored. As soon as the change in successive gates becomes negative, at gate location Gentmin, it is assumed that another peak has been encountered. At this point, a sum if formed, Totup, which totals the counts in all gates following the Gentmin. When Totup equals or exceeds $9 \%$ of Y1st then the second peak is considered significant. The gate at which the second peak occurs, X2nd, is determined to occur when the difference in the counts of consecutive gates becomes positive.

The counts at the second significant peak, Y2nd, are then used in the following manner to calculate the counts at the half-power point of the second peak, Ymid2:

$$
\begin{equation*}
\text { Ymid2 }=\frac{\text { (Y2nd-Cntmin) }}{2}+\text { Cntmin } \tag{2.10}
\end{equation*}
$$

(a) Single Peak

(b) Double Peak


Figures 5a and 5b. Specularly Shaped Waveforms

Again, a linear interpolation is performed in a manner identical with the first significant peak to determine the exact gate location of the second significant peak half-power point, Gtmid2.

The final parameter to be determined is the total width of the peak or peaks at the first half-power point. The width is defined as the number of gates between Gtmidl (Section 2.1.3.1) and the location, Gtrail, where the trailing cdge passes through Ymid 1 (Equation 28). The width is computed as follows:

$$
\begin{equation*}
\text { Width }=\text { Gtrail }- \text { Gtmid } 1 \tag{2.11}
\end{equation*}
$$

In summary, the parameters for a specular return with a single significant peak are as follows:

$$
\begin{align*}
\beta_{1} & =\text { Yn } \\
\beta_{2} & =\text { Y1st } \\
\beta_{3} & =\text { Gtmid } 1  \tag{2.12}\\
\beta_{4} & =\text { Slp1st } \\
\beta_{5} & =\text { Width } .
\end{align*}
$$

The parameters for a specular return with double significant peaks are as follows:

$$
\begin{align*}
& \beta_{1}=\text { Yn } \\
& \beta_{2}=\text { Y1st } \\
& \beta_{3}=\text { Gtmidl } \\
& \beta_{4}=\text { Slp1st } \\
& \beta_{5}=\{\text { Y2nd }  \tag{2.13}\\
& \beta_{6}=\text { Gtmid2 } \\
& \beta_{7}=\text { Slp2nd } \\
& \beta_{8}= \\
& \beta_{9}=\text { Width } \\
& \text { Cntmin } .
\end{align*}
$$

### 2.1.4 Retracking Diffuse-Type Returns

The method used to retrack the diffuse return is to model the return with a function that has the retracking position (the mid-point of the leading edge) as a parameter. The Bayesian leastsquares method (Ref. 8) is used to solve for the parameters of the function that best fit the return. For this method, initial estimates of the parameters must be provided. Weights are given to these initial estimates that designate how well each parameter is known relative to the others.

Residuals are then calculated between the return value and the function value at each gate. These residuals are weighted based on their proximity to the mid-point of the leading edge position. A minimum to the sum of these squared weighted residuals is sought by an iterative method which simultaneously adjusts all of the function parameters. The process is repeated until convergence or until the maximum number of iterations is reached. Because linear methods are used to solve a non-linear problem the procedure can be numerically unstable. Checks are done to assure the reasonableness of the results. The key to making this method function correctly is in the choice of the initial estimates and weighting functions.

The theory of solving for the function parameters using Bayesian least-squares can be found in Ref. 8. The actual equations used will be presented here without justification.

Given an overdetermined set of equations $\mathrm{MX}=\mathrm{R}$ where
$M=$ the matrix of partials $\left[\begin{array}{llll}\frac{\partial c_{1}}{\partial \beta_{1}} & \cdots & \frac{\partial c_{1}}{\partial \beta_{n}} \\ \frac{\partial c_{m}}{\partial \beta_{1}} & \cdots & & \frac{\partial c_{m}}{\partial \beta_{n}}\end{array}\right] \quad m \quad m>n$
$\mathrm{x}=$ column vector $=\left[\begin{array}{cl}\beta_{\mathrm{c} 1} & -\beta_{1} \\ \vdots \\ \beta_{\mathrm{cn}} & -\beta_{\mathrm{n}}\end{array}\right]$
$R=\left[\begin{array}{ccc}m_{1} & -c_{1} \\ & \cdot & \\ & \cdot & \\ m_{m} & & -c_{m}\end{array}\right]$
and
$m_{t}=$ observed value (counts at $t=$ gate $i$ ),
$c_{1}=$ calculated values of $m_{1}$ based upon a given set of parameters $\beta$,
$\beta_{\mathrm{J}}=$ current best estimate of the model parameters $\beta$,
$\beta_{\mathrm{cj}}=$ corrected best estimate of the model parameters $\beta$,
$i=$ gate number ( $0-59$ ), and
$\mathrm{n}=$ number of parameters in the function.

We can then define a weight matrix, W
$W=\left[\begin{array}{cccc} & & & \\ & & & \\ & & & \\ & & \cdot & \\ & & & \\ & 0 & & \\ & & \\ & & & \\ m\end{array}\right]$
where $w t_{1}$ is the weight associated with each observation $i$.

If we multiply both sides of the equation by W we get
$W M X=W R$.

Multiplying through by $\mathrm{M}^{\mathrm{T}}$ gives

$$
\begin{equation*}
M^{T} W M X=M^{T} W R . \tag{2.18}
\end{equation*}
$$

The solution of X is solved for as

$$
\begin{equation*}
\mathrm{X}=\left[\mathrm{M}^{\mathrm{T}} \mathrm{WM}\right]^{-1} \mathrm{M}^{\mathrm{T}} \mathrm{WR} \tag{2.19}
\end{equation*}
$$

where $M^{T} W M$ is referred to as the normal matrix. To add information as to the validity of the current best estimate of the model parameters the a priori covariance matrix $\mathrm{V}_{\mathrm{O}}$ is included

$$
\mathrm{V}_{\mathrm{o}}=\left[\begin{array}{ccc}
\mathrm{wt}_{\beta 1} & & 0  \tag{2.20}\\
\cdot & & \\
& \cdot & \\
0 & \mathrm{wt}_{\beta \mathrm{n}}
\end{array}\right]
$$

where $\mathrm{wt}_{\beta \mathrm{j}}=$ weight associated with the a priori value of parameter j . This matrix is then added to the normal matrix before it is inverted so the equation becomes

$$
\begin{equation*}
\mathrm{X}=\left(\mathrm{M}^{\mathrm{T}} \mathrm{WM}+\mathrm{V}_{\mathrm{o}} \mathrm{o}^{-1} \mathrm{M}^{\mathrm{T}} \mathrm{WR} .\right. \tag{2.21}
\end{equation*}
$$

X then is the vector giving the new best estimate of the $\beta$ parameters.

### 2.1.4.1 The Function Representing the Altimeter Return

It has been shown (Miller and Brown, 1974) that the mean return waveform over a Gaussian surface can be mathematically described using the function

$$
\begin{equation*}
\mathrm{c}(\mathrm{t})=\beta_{1}+\beta_{2} * \mathrm{P}(\mathrm{~W}) \tag{2.22}
\end{equation*}
$$

where

$$
\begin{align*}
& \mathrm{P}(\mathrm{~W})=\int_{-\infty}^{\mathrm{W}} \mathrm{Z}(\mathrm{q}) \mathrm{dq}  \tag{2.23}\\
& \mathrm{Z}(\mathrm{q})=\frac{1}{\sqrt{2 \pi}} \exp \left(\frac{-\mathrm{q}^{2}}{2}\right)  \tag{2.24}\\
& \mathrm{W}=\frac{\mathrm{t}-\beta_{3}}{\beta_{4}} . \tag{2.25}
\end{align*}
$$

This assumes that the pointing angle errors have negligible effects on the waveform shape. This also represents the ice sheet waveforms very well if it is modified to include a slope to the trailing edge. The modified function used to represent the diffuse-type waveforms is chosen as

$$
\begin{equation*}
c(t)=\beta_{1}+\beta_{2}\left(1+\beta_{5} G(x)\right) P(W) \tag{2.26}
\end{equation*}
$$

where

$$
\begin{aligned}
\mathrm{G}(\mathrm{x}) & =0 \text { for } \mathrm{t}<\beta_{3}+0.5 \beta_{4} \\
& =\mathrm{t}-\mathrm{x} \text { for } \mathrm{t}>\beta_{3}+0.5 \beta_{4}
\end{aligned}
$$

This is plotted in Figure 6a where
(a) Single-Ramp Function

$\beta_{4}$ Is the waveform risetime parameter

$$
\begin{aligned}
& y=\beta_{1}+\beta_{2}\left(1+\beta_{5} Q\right) P \frac{\left(t-\beta_{3}\right)}{\beta_{4}} \text { where } Q=0 \text { for } X<\beta_{3}+0.5 \beta_{4} \\
&=1 \text { for } X \geq \beta_{3}+0.5 \beta_{4} \\
& X=t-\left(\beta_{3}+0.5 \beta_{4}\right) \\
& z \\
& P(z)=\int_{\infty} \frac{1}{\sqrt{2} \pi} \exp \left(-q^{2 / 2}\right) d q
\end{aligned}
$$

(b) Double-Ramp Function

$\beta_{4}$ and $\beta_{7}$ are risetime parameters for the 1 st and 2 nd ramp respectively
Where $y=\beta_{1}+\beta_{2} P \frac{\left(t-\beta_{3}\right)}{\beta_{4}}\left\{1+\beta_{9} Q\left(x_{1}\right)\right)+\left(\beta_{5} P \frac{\left(t-\beta_{6}\right)}{\beta_{7}}\left(1+\beta_{3}\left(Q\left(X_{2}\right)\right)\right.\right.$

$$
\begin{array}{rlr}
x_{1}=t-\beta_{3}-0.5 \beta_{4} \\
x_{2}=t-\beta_{6}-0.5 \beta_{7} & Q(x) & =0 \text { for } x<0 \\
& =1 \text { for } x \geq 0 & P(z)=\int_{-\infty}^{z} \frac{1}{\sqrt{2 \pi}} \exp \left(-q^{2} / 2\right) d q
\end{array}
$$

Figures 6a and 6b. Diffusely Shaped Waveforms
$\mathrm{x}=\beta_{3}+0.5 \beta_{4}$.

The partials of this function with respect to each parameter are

$$
\begin{align*}
& \frac{\partial c}{\partial \beta_{1}}=1.0  \tag{2.27}\\
& \frac{\partial c}{\partial \beta_{2}}=P[W]+\beta_{5} \Theta \mathrm{P}[\mathrm{~W}]  \tag{2.28}\\
& \frac{\partial c}{\partial \beta_{3}}=-\beta_{2}\left\{\frac{\left(1+\beta_{5} G\right)}{\beta_{4}} \frac{\partial \mathrm{P}}{\partial \mathrm{~W}}+\mathrm{P}(\mathrm{~W}) \beta_{5}\right\}  \tag{2.29}\\
& \frac{\partial c}{\partial \beta_{4}}=\beta_{2}\left\{\frac{\left(1+\beta_{5} G\right)}{\beta_{4}} \frac{\partial \mathrm{P}}{\partial \mathrm{~W}} \mathrm{~W}+\beta_{5} \frac{\mathrm{P}(\mathrm{~W})}{2}\right\}  \tag{2.30}\\
& \frac{\partial c}{\partial \beta_{5}}=\beta_{2} \mathrm{BP}[\mathrm{~W}] \tag{2.31}
\end{align*}
$$

where

$$
\frac{\partial P}{\partial W}=\frac{1}{\sqrt{2 \pi}} \exp \left(\frac{-W^{2}}{2}\right)
$$

The value of $\beta_{3}$ is the mid-point of the leading edge, Gm. As previously noted, some of the returns display multiple leading edges. A nine-parameter function is used to represent these returns, where the mid-point of the first leading edge is still $\beta_{3}$. The mid-point of the second leading edge, $\beta 6$, probably represents a return from another surface in the footprint and is being stored for future use. The nine-parameter function is

$$
\begin{equation*}
c(t)=\beta_{1}+\beta_{2} \mathrm{P}\left(\mathrm{~W}_{1}\right)\left(1+\beta_{9} \mathcal{G}\left(\mathrm{x}_{1}\right)\right)+\beta_{5} \mathrm{P}(\mathrm{~W})\left(1+\beta_{8}\left(\mathrm{G}\left(\mathrm{x}_{2}\right)\right)\right. \tag{2.32}
\end{equation*}
$$

This is plotted in Figure 6b where

$$
\begin{aligned}
& \mathrm{x}_{1}=\mathrm{t}-\beta_{3}-.5 \beta_{4} \\
& \mathrm{x}_{2}=\mathrm{t}-\beta_{6}-0.5 \beta_{7}
\end{aligned}
$$

$$
\begin{aligned}
& \mathrm{w}_{1}=\frac{\mathrm{t}-\beta_{3}}{\beta_{4}} \\
& \mathrm{w}_{2}=\frac{\mathrm{t}-\beta_{6}}{\beta_{7}}
\end{aligned}
$$

The partials of this nine-parameter function are

$$
\begin{align*}
& \frac{\partial c}{\partial \beta_{1}}=1.0  \tag{2.33}\\
& \frac{\partial c}{\partial \beta_{2}}=P\left(W_{1}\right)\left[1+\beta_{9}\right] G_{1}  \tag{2.34}\\
& \frac{\partial c}{\partial \beta_{3}}=-\beta_{2}\left[\frac{\left(1+\beta_{9} G_{1}\right)}{\beta_{4}} \frac{\partial \mathrm{P}}{\partial W_{1}}+\mathrm{P}\left(\mathrm{~W}_{1}\right) \beta_{9}\right]  \tag{2.35}\\
& \frac{\partial c}{\partial \beta_{4}}=-\beta_{2}\left[\frac{\left(P\left(W_{1}\right) \beta_{9}\right.}{2}+\frac{\left(1+\beta_{9} Q_{1}\right)}{\beta_{4}} \frac{\partial \mathrm{P}}{\partial \mathrm{~W}_{1}} \mathrm{~W}_{1}\right]  \tag{2.36}\\
& \frac{\partial c}{\partial \beta_{5}}=1+\beta_{8} G_{2} \mathrm{P}\left(\mathrm{~W}_{2}\right)  \tag{2.37}\\
& \frac{\partial c}{\partial \beta_{6}}=-\beta_{5}\left(\mathrm{P}\left(\mathrm{~W}_{2}\right) \beta_{8}+\frac{\left(1+\beta_{8} \Theta_{2}\right)}{\beta_{7}} \frac{\partial \mathrm{P}}{\partial \mathrm{~W}_{2}}\right] \tag{2.38}
\end{align*}
$$

$$
\begin{align*}
& \left.\frac{\partial c}{\partial \beta_{7}}=-\beta_{5} \quad \frac{\left(1+\beta_{8} \mathrm{G}_{21}\right.}{\beta_{7}} \mathrm{~W}_{2} \frac{\partial \mathrm{P}}{\partial \mathrm{~W}_{2}}+\frac{\mathrm{P}\left(\mathrm{~W}_{2}\right)}{2} \beta_{8}\right)  \tag{2.39}\\
& \frac{\partial \mathrm{c}}{\partial \beta_{8}}=\beta_{5} \mathcal{G}_{2} \mathrm{P}\left(\mathrm{~W}_{2}\right)  \tag{2.40}\\
& \frac{\partial \mathrm{c}}{\partial \beta_{9}}=\beta_{2} \mathrm{G}_{2} \mathrm{P}\left(\mathrm{~W}_{1}\right) . \tag{2.41}
\end{align*}
$$

### 2.1.4.2 Setting the Initial Estimates for the Parameters

Initial estimates of each parameter are calculated from each individual return. To calculate these the general shape of the waveform is mathematically described by defining a mean slope and average value (bias) for every whole gate. For gates 4 through 56 , the mean slopes and biases correspond to a straight line that is fit using least-squares minimization through the gate in question and the six surrounding gates. The biases for gates 1 through 4 are taken as the gate values and the slopes are delined as zero. For gates 57 through 60 the biases are the gate values and the slopes are defined as the slope calculated for gate 56 . This set of slopes and biases is then interrogated to determine the locations of the leading edges and how many occur in the waveform.

The conditions required for a leading edge at gate Ir are:

1) The Slope(lr) must be greater than a given valuc, Thsl. A value of Thsl $=0.5$ count/gate is used to find the first leading edge, for succeeding leading edges Thsl is set to 1.0 count/gate. These numbers were chosen by visually and mathematically evaluating many typical ice sheet waveforms to determine when a leading edge designating a valid return could be perceived.
2) The $\operatorname{Slope}($ Ir $)$ must be a relative maximum, ic:
```
Slope(Ir) > Slope (Ir-1)
Slope(Ir) > Slope (Ir +1) .
```

3) There must be a significant increase in counts after the leading edge compared with that before the leading edge, i.c.:
$\operatorname{Bias}(\mathrm{Ir}+3)-\mathrm{Bias}(\mathrm{Ir}-3)>$ Thbs
where
Thbs $=13.5$ counts for first leading edge
$=20.0$ counts for succecding leading edge.
4) If there was a leading edge already detected within 3 gates of Ir then the location is taken as that with the larger slope.

The initial estimates of the function parameters are then calculated from the position of the leading edge(s) and the Slopes and Biases. The five-parameter function (2.26) is used when only one leading edge is found, the nine-parameter function (2.32) is used when two or more lcading edges are found.

Initial estimates, $\beta_{1}^{0}$, and the corresponding standard deviations of these estimates, Sig( 1 ) through Sig(5), for the five-parameter function are defined as:

```
\beta
\beta
\beta
\beta
        Slope(Ir)}*0.5 (gate)
\beta
```

```
Sig(1)=0.01 (count)
```

Sig(1)=0.01 (count)
Sig(2)}=10.0(counts

```
Sig(2)}=10.0(counts
```




```
Sig(4)=.01 \betao(4)(gatcs)
```

Sig(4)=.01 \betao(4)(gatcs)
Sig(5)=.01(count/gatc).

```
Sig(5)=.01(count/gatc).
```

Initial estimates and the corresponding standard deviations for the nine-parameter function are defined as:

| $\beta_{1}^{\mathrm{o}}=\mathrm{Bias}(4)$ (counts) | Sig(1) $=.01$ (count) |
| :---: | :---: |
| $\beta_{2}^{\text {o }}=\operatorname{Bias}(\operatorname{Ir} 1+3)-\operatorname{Bias}(4)$ (counts) | $\operatorname{Sig}(2)=0.1$ (count) |
| $\beta_{3}^{\text {o }}=$ Ir 1 (gates) | $\operatorname{Sig}(3)=.05 \beta_{\mathrm{o}}(4)$ (gates) |
| $\beta_{4}^{o}=\begin{gathered} \{\mid \operatorname{Bias}(\operatorname{Ir} 1+3)-\operatorname{Bias}(\operatorname{Ir} 1-3) V \\ \text { Slope(Ir } 1)\} * 0.5 \text { (gates) } \end{gathered}$ | Sig(4) $=.005 \beta_{\mathrm{o}}(4)$ (gates) |
| $\beta_{5}^{0}=\operatorname{Bias}(\operatorname{Ir} 2+3)-\operatorname{Bias}(\operatorname{Ir} 1+3)$ (counts) | $\mathrm{Sig}(5)=0.1$ (count) |
| $\beta_{6}^{\mathrm{o}}=\mathrm{Ir} 2$ (gates) | Sig(6) $=.05 \beta_{0}(7)$ (gates) |
| $\beta_{7}^{\circ}=\underset{\substack{\text { Slope(Ir2) }\} \text { (gates) }}}{\{[\text { Bias(Ir2 } 2+3) \text { Bias (Ir2-3) }}$ | $\mathrm{Sig}(7)=.005 \beta_{\mathrm{o}}(7)$ (gates) |
| $\beta_{8}^{0}=0.0$ (count/gate) | $\mathrm{Sig}(8)=.01$ (count/gate) |
| $\beta_{9}^{0}=0.0$ (count/gate) | $\mathrm{Sig}(9)=.01$ (count/gate) |

where

Ir l is the predicted gate corresponding to the mid-point of the first leading edge

Ir2 is the predicted gate corresponding to the mid-point of the second leading edge.

### 2.1.4.3 Calculating the Weight Matrix, w

The weight associated with each observation, $\mathrm{wt}_{\mathrm{l}}$, is selected to optimize the fit in the vicinity of the leading edge.

$$
\begin{equation*}
\mathrm{wt}_{1}=1+\mathrm{K}_{1} *\left\lfloor\exp \left(\mathrm{~K}_{2}\right)+\mathrm{K}_{3}\right] \tag{2.44}
\end{equation*}
$$

where

$$
\begin{aligned}
\mathrm{K}_{1} & =\left(\mathrm{I}_{\text {ter }}-1\right) * 0.5 \\
\mathrm{I}_{\mathrm{ter}} & =\text { iteration number } \\
\mathrm{K}_{2} & =\mathrm{T}_{\mathrm{c}}+0.5 \\
& =\operatorname{Min}\left(\mathrm{K}_{2}, 60\right) \\
& =\operatorname{Max}\left(\mathrm{K}_{2}, 1\right) \\
\mathrm{T}_{\mathrm{c}} & =\mathrm{X}_{1}-\beta_{3}-\operatorname{Max}\left(5.0, \beta_{4}\right) \text { for 5-parameter function }
\end{aligned}
$$

$=X_{1}-\beta_{6}-\operatorname{Max}\left(5.0, \beta_{7}\right)$ for 9-parameter function
$\mathrm{X}_{1}=$ gate number of the ith observation
for the five-parameter function

$$
\begin{aligned}
\mathrm{K}_{3} & =0 \text { for }\left|\mathrm{T}_{\mathrm{c}}\right| \geq 2.0 \\
& =1 \text { for }\left|\mathrm{T}_{\mathrm{c}}\right|<2.0
\end{aligned}
$$

for the nine-parameter function

$$
\begin{aligned}
\mathrm{K}_{3} & =0 \text { for }\left|\mathrm{T}_{\mathrm{c}}\right| \geq 5.0 \\
& =1 \text { for }\left|\mathrm{T}_{\mathrm{c}}\right|<5.0 .
\end{aligned}
$$

### 2.1.4.4 Calculating the Covariance Matrix, $\mathrm{V}_{o}$

A priori values of $\mathrm{V}_{\mathrm{o}}$ are calculated from the sigmas in equations (2.42) and (2.43) as follows:

$$
\begin{align*}
w_{\mathrm{t}_{\beta_{\mathrm{j}}}} & =w \text { scale/Sig(j) })^{2}  \tag{2.45}\\
w \text { scale } & =1+.6 * \mathrm{~K} * \mathrm{H} 1 / 3 /(120 * \mathrm{~g} 2 \mathrm{~m})  \tag{2.46}\\
\mathrm{H} 1 / 3 & =1.875 * \beta_{4} \\
\mathrm{~K} & =4
\end{align*}
$$

Using the function, $w$ scale, causes the initial estimate information to have a greater effect on the solution when the rise time is large.

After each iteration, $n$, the values of $\operatorname{Sig}(3), \operatorname{Sig}(4)$ and $K$ are altered as follows:

$$
\begin{aligned}
& \operatorname{Sig}(3)=\operatorname{Sig}(3)_{n-1} * 0.1 \\
& \operatorname{Sig}(4)=\operatorname{Sig}(4)_{n-1} * 10.0
\end{aligned}
$$

$$
\mathrm{K}=\mathrm{K}_{\mathrm{n}-1}+.5
$$

This has the effect of weighting the current best estimate of the leading edge position more and the rise time of the leading edge less. This has proven to speed up convergence.

### 2.1.4.5 Method of Iteration

An interative scheme is used starting out with the initial estimate of the $\beta$ parameters. The Bayesian least-squares method is then used to solve for another set of $\beta$ parameters that better fits the data. Iterations are performed always using the current set for the best estimate until $\Delta \mathrm{H}_{\text {ret }}$, as calculated from $\beta_{3}(2.1)$, converges to within 10 cm or the number of iterations exceeds 7.

Each succeeding set of $\beta$ parameters is checked for reasonableness using these criteria:

$$
\begin{aligned}
& 0.0<\beta_{2} \\
& 0.0<\beta_{3}<60.0 \\
& 0.0<\beta_{4} \\
& \beta_{3}<\beta_{6}<60.0 \\
& 0.0<\beta_{7}
\end{aligned}
$$

If any of the criteria fail, then the fit is considered unsuccessful and the waveform is discarded.

After convergence or the maximum number of iterations is reached, tests are then made to assure that the values reasonably represent the return. The rms of the residuals between the waveform and the function for the portion of the waveform from gate zero to just past the top of the leading edge is calculated.

$$
\mathrm{RMS}_{\mathrm{E}}=\frac{\sum_{i=1}^{\text {Iedit }}\left(\mathrm{C}_{1}-\mathrm{m}_{\mathrm{i}}\right)^{2}}{\text { Iedit }}
$$

where

$$
\begin{aligned}
\text { Iedit } & =\beta_{3}+0.5 \beta_{4} \text { for the five-parameter function } \\
& =\beta_{6}+0.5 \beta_{7} \text { for the nine-parameter function. }
\end{aligned}
$$

If $\mathrm{RMS}_{\mathrm{E}}$ is greather than 20.0 counts then the fit is unacceptable. If the nine-parameter function is being fit and the process is unsuccessful, then the initial estimates are reset to
coincide with the initial estimates for the first leading edge and a five-parameter fit is tried. If problems occur during the five-parameter fit, the initial estimates are altered so that the leading edge position is taken as the gate, $\mathrm{I}_{\mathrm{r}}$, where Slope ( $\mathrm{I}_{\mathrm{r}}$ ) (as defined in Section 2.1.4.2) is a maximum for the waveform. If the fit is still unsuccessful, then the waveform is discarded.

The procedures explained here and the numerical values given yield the best results to date. Wherever possible values were chosen based on theory, but many times trial and error was necessary. At the time the Seasat Greenland data were processed, the procedures and numcrical values differed slightly. There was no $\mathrm{RMS}_{\mathrm{E}}$ check as explained in the last part of Section 2.1.4.5, nor were the initial parameter values altered if an unsuccessful fit was made. The variables that were different and their values for the Greenland processing were:

$$
\begin{aligned}
\text { Thbs } & =5.0 \text { counts for the first leading edge } \\
& =10.0 \text { counts for the second leading edge } \\
\operatorname{Sig}(3) & =\beta_{0}(4) \quad \text { (for the five-parameter function) } \\
\operatorname{Sig}(4) & =0.1 \beta_{0}(4) .
\end{aligned}
$$

A direct consequence of these differences was that the entire Greenland data sct had to be visually reviewed to assure that the fit adequately represented the data. This resulted in approximately $1 \%$ of the data being discarded which would not have been rejected using newer methods. The newer methods described here identify these problems automatically.

### 2.2 SENSOR-RELATED CORRECTIONS

After the ice altimeter data are edited and retracked, the precise orbits from NASA/GSFC (PGS-S4) are used to calculate the measured ice shect elevation above the ellipsoid (Lerch et al., 1982). Corrections are then applied to correct for sensor-related biases.

Both the time tag and center of gravity corrections are calculated using the algorithms released by JPL (Lorell, 1979). These are summarized below.

### 2.2.1 Time Tag Correction

The SDR time tag, $\mathrm{t}_{\mathrm{SDR}}$, is corrected for a track mode correction and a signal travel time correction so that the resultant data time, $t$, refers to the time of signal reflection from the ice sheet.

$$
\begin{equation*}
\mathrm{t}=\mathrm{t}_{\mathrm{SDR}}-0.0794+\mathrm{H} / \mathrm{c} \tag{2.47}
\end{equation*}
$$

where
$\mathrm{c}=2.99792458 \times 10^{8} \mathrm{~m} / \mathrm{sec}$,
$\mathrm{H}=$ spacecraft altitude in meters, and
0.0794 is the track mode correction in seconds.

### 2.2.2 Center of Gravity Correction

The correction applied to make the spacecraft center of gravity the height reference point is

$$
\begin{equation*}
\Delta H_{c g}=Z_{c g}-Z_{\mathrm{cone}} \tag{2.48}
\end{equation*}
$$

where
$Z_{\mathrm{cg}}=$ the distance from the altimeter base plate to the spacecraft center of gravity. This varied during the flight due to maneuvers. Table S-07 of Lorell (1979) is used to obtain $Z_{\mathrm{cg}}$
$Z_{\text {cone }}=-1.238 \mathrm{~m}$ which is the sum of the distance from the feed flange on the antenna to the base plate and a distance corresponding to a time bias in the electronic circuitry.

This correction is located in bytes 49-52 of the IDR.

### 2.3 ATMOSPHERIC CORRECTIONS

The measurements are corrected for ionospheric and tropospheric refraction using parameters supplied by JPL on the GDR's (Lorell et al., 1980).

### 2.3.1 Ionosphere Correction

The ionosphere correction for the ice data, $\Delta \mathrm{H}_{\mathrm{ION}}$, is calculated by linearly interpolating from the ionosphere corrections on the GDR's. Bytes 57-60 on the IDR contain the value of this correction. A detailed description of the algorithm used is given in Lorell et al., (1980).

### 2.3.2 Troposphere Correction

The wet tropospheric correction is calculated using the following equations explained in Lorell et al., (1980).

$$
\begin{equation*}
\Delta \mathrm{H}_{\mathrm{TROP}}^{\mathrm{WET}} ⿵ 冂=2.277^{*} 10^{-3 *} \mathrm{E}_{\mathrm{o}}\left(1.25503 / \mathrm{T}_{\mathrm{K}}+0.5\right) \tag{2.49}
\end{equation*}
$$

where

$$
\mathrm{E}_{\mathrm{o}}=6.11 * \mathrm{H}_{\mathrm{R}}^{*} 10^{\left(7.5^{*} \mathrm{~T}_{\mathrm{K}}-273.16\right) /\left(\mathrm{T}_{\mathrm{K}}-35.86\right)}
$$

$\mathrm{T}_{\mathrm{K}}$ is the surface temperature calculated by assuming a linear temperature profile with boundary conditions:
at sea level $\quad T_{K}=2.73 .0 \mathrm{~K}$
at 3200 m above sea level $\mathrm{T}_{\mathrm{K}}=243.0 \mathrm{~K}$, and
$H_{R} \quad$ is the relative humidity (assumed to be $100 \%$ over the ice sheet).

The dry tropospheric correction is calculated from the equation

$$
\begin{equation*}
\Delta \mathrm{H}_{\mathrm{TROP}}^{\mathrm{DRY}}, ~=2.277^{*} 10^{-3 *}\left\{\mathrm{P}^{*}\left[1.0+0.0026^{*} \cos (\phi)\right]\right\} \tag{2.50}
\end{equation*}
$$

where
$\phi=$ subsatellite latitude,
$\mathrm{P}=\mathrm{P}_{\mathrm{o}} *\left(1.0-1.1138^{*} 10^{-4} * \mathrm{Ht}\right)$,
$P_{o} \quad-\quad$ is the atmospheric pressure interpolated from the GDR's, and
$\mathrm{Ht} \quad$ - is the ice sheet elevation above sea level in meters.

The total height correction due to the troposphere is

$$
\begin{equation*}
\Delta \mathrm{H}_{\mathrm{TROP}}=\Delta \mathrm{H}_{\mathrm{TROP}}^{\mathrm{WET}}-2 \mathrm{H}_{\mathrm{TROP}}^{\mathrm{DRY}} \tag{2.51}
\end{equation*}
$$

The troposphere correction may be found in bytes 53-56 of the IDR.

### 2.4 SURFACE DYNAMIC CORRECTIONS

The solid earth tides are computed by linearly interpolating their values from the GDR's. The resultant interpolated value may be found in bytes $83-84$ of the IDR.

### 2.5. ORBITAL CORRECTIONS

The NASA/GSFC PGS-S4 orbits which are used to improve the height measurements, have rms radial errors of 1.5 m . In an effort to reduce the radial error of these orbits, a technique was devised to further improve the orbit accuracy by referencing the orbits to a common ocean surface. Previous attempts to adjust the orbits using crossover minimization techniques with the ice sheet crossovers proved unsuccessful due to extreme segmentation of the data (see Figure 2). The new technique is not dependent upon the ice data but upon ocean altimetry, and utilizes the smoothed Seasat 84306 global ocean surface (Marsh et al., 1986). Through crossover minimization techniques the radial orbit error for the 84306 ocean surface has been reduced to 11 cm in the open ocean areas.

The method involves obtaining the residuals between the Seasat ocean data for passes which traverse Greenland, and the smoothed 84306 ocean surface. Using least-squares minimization, these residuals are then fit to a linear or quadratic function depending on the proximity of the data to Greenland. The function is, in turn, interpolated or extrapolated to determine the value of the orbit adjustment over Greenland which is to be subtracted from the surface height. This function is of the following form:

$$
\begin{equation*}
\mathrm{f}(\mathrm{t})=\mathrm{C}_{0}+\mathrm{C}_{1} \Delta \mathrm{t}+\mathrm{C}_{2} \Delta \mathrm{t}^{2} \tag{2.52}
\end{equation*}
$$

where
$C_{0}, C_{1}, C_{2}$ are the coefflcients of the fit where the units are meters, meters/fractions of a day and meters/(fractions of a day) ${ }^{2}$, respectively, and
$\Delta t \quad$ is the time from the start of the pass in fractions of a day.

Since this method attempts to adjust for orbit error only, the ocean data which are used must have all sensor, atmospheric, and surface dynamic corrections applied. The ocean data used in the adjustment are obtained from the Seasat Geophysical Data Records (GDR's), as corrected by JPL (Lorell et al., 1980).

Since the orbit error is strongly periodic, with a dominant frequency of two cycles per one revolution, only data from the northern hemisphere need to be used in computing the orbit adjustment over Greenland.

The distribution of the data affects the way in which the residuals are fit. To aid in categorizing the distributions of data, the northern hemisphere is subdivided into five ocean regions: 1) the area to the east of Greenland and within 1000 km . of the coast; 2) the area to the east of Greenland from 1000 km . from the coast to the Greenwich meridian; 3) the Indian Ocean; 4) the area to the west of Greenland between Greenland and North America; and 5) the Pacific Ocean (see Figure 7). The type of fit performed depends upon particular regions containing a minimum amount of data. If the criteria are not met, then no fit is performed

Figure 7 summarizes the type of fit which is performed depending upon the region(s) in which data are found. An ' X ' in regions $1,2,3$ or 5 represents a minimum of 10 points, whilc region 4, due to its limited open ocean area, requires a minimum of 19 points. Linear fits are performed when data are found either very close to Greenland or are widely separated from Greenland. Guadratic fits are performed when the data are more evenly distributed over several regions.

After the coefficients for the fit are initially determined, outlying data which satisfy the following criterion are removed:
$|\mathrm{H}(\mathrm{t})-\mathrm{f}(\mathrm{t})| \geq \mathrm{m}$ * RMS
where
is an integer editing multiplier,

RMS is the rms between the residual heights and the function $f(t)$, and
$H(t)$ is the surface elevation of the datum point.


Figure 7. Orbit Adjustment Regions and Effects of Data Distribution on the Orbit Adjustment Fit

| REGIONS <br> (MINIMUM NUMBER OF POINTS |  |  |  |  | $\begin{gathered} \text { TYPE OF } \\ \text { FIT } \\ \mathrm{L}=\text { LINEAR } \\ \mathrm{g}=\mathrm{QUADRATIC} \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} 1 \\ (10) \end{gathered}$ | $\begin{gathered} 2 \\ (10) \end{gathered}$ | $\begin{gathered} 3 \\ (10) \end{gathered}$ | $\begin{gathered} 4 \\ (19) \end{gathered}$ | $\begin{gathered} 5 \\ (10) \end{gathered}$ |  |
| XX |  |  | X |  | L |
|  |  |  |  |  | L |
|  |  |  | X |  | L |
|  |  | X |  | X | L |
|  | X |  |  | X | L |
| X |  |  |  | X | 8 |
|  | X | X |  | X | 9 |
|  |  | X | X |  | 9 |
|  | X |  | X |  | 8 |

'X' INDICATES A REGION CONTAINING THE MINIMUM NUMBER OF POINTS

The remaining data are then used to solve for the function. This process is repeated until either the latest computed rms does not change by more than .02 m from the previous iteration, or 15 iterations are completed. In the case of the Seasat Greenland data, an editing multiplier of 4.0 is used with an initial rms of 20.0 m .

After solving for the coefficients and removing outliers, the function must satisfy a final test. For a linear function, the orbit adjustments are computed at the endpoints of the pass. If the absolute value of the orbit adjustment at either endpoint exceeds 3.0 m , then the function is not used. In the case of a quadratic function, the extremum of the function is first located. If the extremum is outside the endpoints of the data just fit, then the endpoints of the pass are checked as in the linear case. If the extremum lies between the endpoints, its value is checked. Again, a 3.0 m adjustment is deemed too large and if exceeded, an attempt is made to refit the data with a linear function. Of the 331 GDR passes for which an orbit adjustment was computed, 181 resulted in quadratic fits and 150 in linear fits. Of the 194 quadratic fits initially attempted, 12 failed the extremum test and were refit using a linear function. Of these, only one failed the endpoint test.

Two examples of results from the orbit adjustment procedure are shown in Figures 8 and 9. In the first case (Figure 8), data which are found in close proximity to Greenland are fit by a linear function. The latitude and east longitude of the points along the pass closest to the west and east coasts of Greenland are indicated. A linear function is fit to the smoothed ocean surface residuals. The orbit adjustment in the region traversing Greenland is indicated by dashes. Figure 9 shows the orbit adjustment results when a quadratic fit is necessary due to data being available just off Greenland's east coast and in the Pacific Ocean. The final rms between the data and function are 27 cm in the linear case and 14 cm the quadratic case.

Table 3 summarizes the orbit adjustments computed for each GDR rev at 310,320 , and 330 East Longitudes, representing the west coast, central region, and east coast of Greenland. Also included are the coefficients for the function (Equation 2.52) and the elapsed time in fractions of a day from the start point of the pass used to compute the adjustment for the longitude in question.

Utilizing Equation (2.52), the orbit adjustment is then computed for each Seasat IDR, and subtracted from the surface height. The orbit adjustment and its corresponding rms are located in bytes 93-96 and 97-100, respectively, of the IDR.
OBS HT - REF SURF HT (METERS) REV 519

SECONDS PAST START OF PASS

OBS HT - REF SURF HT (METERS) REV 158

Figure 9. Orbit Adjustment Computed From Widely Distributed Data

Application of the orbit adjustment to the data yields improved crossover results. When the differences in heights are computed at 1235 crossover locations for ascending and descending passes over Greenland, the resultant crossover residual mean of the data without the orbit adjustment is 33 cm with an rms of 1.15 m . After application of the orbit adjustment, the data give a crossover residual mean of 7 cm and an rms of 0.99 m .

### 2.6 SLOPE CORRECTION

The altimeter height is measured to the closest point within its footprint, which does not correspond to the subsatellite location for sloping surfaces. This effect introduces an error into the height measurement which can be corrected by adjusting either the value of the measurement or its location (Brenner et al., 1983). Upon examination of both techniques, the method which was chosen for the Seasat data is to adjust the measurement. The magnitude of the slopeinduced error may be represented by:

$$
\begin{equation*}
\Delta \mathrm{H}_{\mathrm{SLOPE}}=\mathrm{H}(1-\cos \alpha) \tag{2.54}
\end{equation*}
$$

where

H is the satellite altitude in meters
$\alpha \quad$ is the maximum regional surface slope in radians
or

$$
\begin{equation*}
\Delta \mathrm{H}_{\mathrm{SLOPE}}=\frac{\mathrm{H} \alpha^{2}}{2}, \text { for small } \alpha . \tag{2.55}
\end{equation*}
$$

The surface slope in Equation (2.55) for any one point is calculated using the following equation:

$$
\alpha=\sqrt{\alpha} \begin{align*}
& 2  \tag{2.56}\\
& \text { along-track }
\end{align*}+\alpha_{\text {cross-track }}^{2}
$$

where
$\alpha_{\text {along-track }} \quad$ is the slope of the surface in the along-track direction of the data, and
$\alpha_{\text {cross-track }} \quad$ is the slope of the surface in the cross-track direction of the data, perpendicular to the along-track direction.

The cross-track slope is obtained by using a reference surface of Greenland, generated from the Seasat data. This surface consists of a two-dimensional grid of heights. The spacing between grid points is 20 km . Bilinear interpolation between these grid values is used to determine the heights at the points where the cross-track intersects the closest grid lines. From these heights, the cross-track slope is then determined.

The along-track slope is obtained using the available along-track data. Since the height profile is initially unknown, an iterative procedure is used to attempt a reconstruction of the true height proflle. The initial along-track slope at a data point location is calculated by performing a linear fit to the five elevations of the along-track data points nearest the data point in question. A slope correction is then calculated for that point and each point in the pass using Equation (2.55), but applying only $25 \%$ of the correction to the elevations. This entire procedure is repeated using the revised elevations three more times, each time applying $25 \%$ of the current elevation correction. After the final iteration, the total along-track height correction and Equation (2.55) are used to calculate an "effective" along-track slope. This slope may then be used in Equation (2.56) along with the cross-track slope to calculate the total slope. In the case of both the along and cross-track slopes, a maximum of .8 degree is allowed. This is a limitation set by the physical characteristics of the altimeter.

If two points cannot be found on both sides of the point being adjusted, after having searched 10 km in both directions, then the reference grid which is used to calculate the crosstrack slope is also used to determine the along-track slope in a manner equivalent to the crosstrack slope calculation described above.

Slope corrections are not applied to the surface heights on the IDR's. However, the alongtrack and cross-track slopes, from which the slope correction may be computed, are stored in bytes $85-86$ and $87-88$, respectively. Bytes $89-90$ contain the size of the window required to find the five points to perform the along-track linear fit. Bytes $91-92$ give information pertaining to how the along-track and cross-track slopes were determined.

### 2.7 SUMMARY OF CORRECTIONS

In order to obtain a corrected surface elevation relative to sea level with the solid tide effects removed, the following algorithm is used.

$$
\begin{gather*}
\mathrm{H}_{\mathrm{COR}}=\mathrm{H}_{\mathrm{SC}}-\mathrm{H}_{\mathrm{ALT}}-\Delta \mathrm{H}_{\mathrm{RET}}-\Delta \mathrm{H}_{\mathrm{CG}}+\Delta \mathrm{H}_{\mathrm{ION}}+\Delta \mathrm{H}_{\mathrm{TROP}}-\Delta \mathrm{H}_{\mathrm{TIDE}} \\
-\Delta \mathrm{H}_{\mathrm{ORB}}-\Delta \mathrm{H}_{\mathrm{SLOPE}}-\mathrm{H}_{\mathrm{GEOID}} \tag{2.57}
\end{gather*}
$$

where
$\mathrm{H}_{\mathrm{SC}} \quad$ is the height of the spacecraft above the ellipsoid,
$\mathrm{H}_{\mathrm{ALT}} \quad$ is the original altimeter measurement,
$\Delta \mathrm{H}_{\mathrm{RET}} \quad$ is the retracking correction,
$\Delta \mathrm{H}_{\mathrm{CG}}$
$\Delta \mathrm{H}_{\text {ION }} \quad$ is the center of gravity correction,
$\Delta \mathrm{H}_{\mathrm{TROP}} \quad$ is the ionospheric correction,
$\Delta \mathrm{H}_{\mathrm{TIDE}} \quad$ is the value of solid tide,
$\Delta \mathrm{H}_{\mathrm{ORB}}$
$\Delta \mathrm{H}_{\mathrm{SLOPE}} \quad$ is the orbit adjustment,
$\mathrm{H}_{\mathrm{GEOID}} \quad$ is the slope correction, and

The surface elevation on the IDR is relative to the ellipsoid and is corrected for tropospheric and ionospheric effects, the center of gravity offset, the retracking correction, and the orbit adjustment when available. However, the elevation still contains solid tide effects, and the application of the slope correction or removal of the solid tides have been left to the discretion of the user. The surface elevation status word located in bytes 77-78 of the IDR should be checked to verify whether or not corrections have been applied.

Corrections which are applied to the altimeter measurement are done in the opposite sense from the surface elevation corrections and may be verified using the altimeter measurement status word in bytes 13-16 of the IDR.

An outline of the adjustments and corrections required to the Seasat data and their values or range of values is given in Table 4.

## SECTION 3.0 <br> WAVEFORM DATA RECORDS

The averaged radar return pulses contained in the SDR's are stored on a separate file called the Waveform Data Records (WDRs) to facilitate their use. Table 5 outlines in detail the format of this record.

The time, geographical position, and altimeter measurement on the WDRs are not identical to the corresponding records on the IDRs. This is due to the fact that the WDRs information is obtained directly from the SDR's without the application of any correction or adjustment of any kind. The time differs by the time tag correction described in Section 2.2.1. Positions on the WDR are from the orbits on the SDR's and not PGS-S4 orbits. The altimeter measurement represents the raw observation on the $\operatorname{SDR}$ without any of the corrections described in Section 2.7 applied.

## SECTION 4.0

Ordering the Seasat data merely by time presents certain limitations when only data in a particular locale are desired. This situation arises when data are used to generate a grid of smoothed surface heights. To circumvent this problem, a data base was developed which orders the Seasat data by geographical areas or "bins". Figure 10 shows the configuration of the 4,300 bins in the vicinity of Greenland. Bin sizes vary in order to compensate for the higher data density near Seasat's maximum latitude. Each bin is assigned a number starting with " 1 " in the southwestern-most corner. Bin numbers increment first from west to east and then from south to north. The ending bin number for each row is indicated in the right-most margin of the map in Figure 10, while the number of data points is printed within the appropriate bin. Bins which contain no data have no number entered. Table 6 summarizes the number of points and the rev numbers found in each bin, along with the geographical coordinates of the southwestern-most corner of the bin. The bin number in which a particular data point is located may be found in bytes 153-156 of the IDR.

The geo-referenced data base is a subset of the IDR's, containing only information relating to the position, rev number, surface height, slope correction and orbit adjustment for each data point. Slope correction and orbit adjustment values are flagged with a -9999, if unavailable. In addition, the data are ordered first by bin number and then by time within each bin. The surface elevations on this data set have the orbit adjustment applied where it was available. If the orbit adjustment was not available, (indicated by the orbit adjustment value for that record being set to -9999 ) then the surface elevation contains the value calculated from the unadjusted orbit. The slope correction has not been applied to any of the surface elevations.

The data base is designed to be used on a direct-access device, so that data from one or several bins may be accessed without the need to read all the records prior to the location desired. This is achieved by dividing the data base into three sections.

The first section of the data base, a header, consists of one logical record and gives a summary of its configuration: the locations of the corners of the data base, the number of latitudinal rows, the width in degrees of each of these rows, and the number of longitudinal divisions in each row. These pieces of information give the layout of the data base, as depicted in Figure 10. Information pertaining to the size of the data base, the starting record of the bin directory, and the corrections applied to the data are also contained in this header.


Figure 10. Seasat Greenland Geo-referenced Data Base Configuration

Following the header are the altimetry data ordered by bin number and, within each bin, by time. The altimetry data are subdivided into two groups for each bin which contains data. The first subgroup consists of one logical record which indicates the number of data points contained in the bin. The second subgroup consists of the actual altimetry data (position, rev number, surface height, orbit adjustment and slope correction), with each record corresponding to a data point.

The final section is a bin directory which follows the altimetry data. The bin directory starts at the logical record indicated in the data base header. The directory contains an entry for each bin, and starting with the first bin, indicates the record number in the data base (not including the header record) at which the start of the data for a particular bin may be found. Bins which contain no data have a zero entered in the directory. Table 7 summarizes the structure of the data base in greater detail.

One use of the data base is to assist the gridding program (Section 5.0) in locating and accessing all data contained within a specifled radius of a grid location. In addition, the data base may be used to locate data within any desired area. The following example demonstrates how this may be donc. The limits of a desired area are used in conjunction with the header information to determine exactly which bin numbers contain the data. Using the southernmost latitude of the desired area, along with the width of the latitude rows, establishes the southernmost row which contains the data. Longitudinal limits of the desired area are then checked in conjunction with the size and location of the longitudinal divisions in that row. When the longitude limit of the desired area for that latitudinal group is exceeded, the process starts again with the next latitude row to the north. These steps are repeated until the northernmost boundary limit of the desired area is reached.

Equipped with the bin numbers which contain the data, the directory, which gives the logical record on the direct-access disk at which each bin begins, is read. If the directory value for the bin is non-zero, this logical record is then read to determine the number of records which follow and are contained in the same bin. The subsequent data is then read for each bin.

## SECTION 5.0

GRIDS

The uneven distribution of Seasat data presents problems when attempting to create computer generated contours. An intermediate step is useful which fits the data to nodes of a regular grid. Data local to each grid point are fit with a biquadratic or bilinear surface to determine the surface height at the grid point. This procedure is referred to as gridding the data. Grids are generated using the corrected and adjusted data in the geographical data base.

### 5.1 POLAR STEREOGRAPHIC PROJECTION

Grids of the Greenland data are generated in a tangent polar stereographic projection where the plane of projection is located at the geographic North Pole (the projection latitude) and is normal to the earth's axis. This projection is conformal which results in equality of scale about a point. Figure 1la depicts the concept behind this type of projection. A straight line is drawn from the South Pole (pole of projection), through a point on the earth's surface, 9 , to the projection plane which is tangent to the North Pole. The projection plane is in turn divided into square grids from the pole to the Equator with the North Pole at the center. Three projection parameters define the size and the orientation of the plane and the grid size:

S - a conversion factor from half-inch grids at the projection latitude to the desired grid size;
$\phi_{p}$ - the minimum latitude extent of the map perimeter for the projection latitude located at the North Pole; maximum latitude extent for the projection latitude located at the South Pole;

G - the Greenwich orientation in degrees

In the case of Greenland, where 20 kilometer grid cells were decided as being optimum for the data distribution, values of $S=1.65, \phi_{\mathrm{p}}=50^{\circ}$, and $\mathrm{G}=45^{\circ}$ were chosen.

These three parameters are sufficient to define a grid of the northern hemisphere, from the North Pole to $50^{\circ}$ north latitude where the number of cells of desired size from the pole to the equator may be represented by:


Figures 1la and 1lb. Polar Stereographic Projection of Point 9 with Latitude $\phi$ and Longitude $\lambda$ onto Plane with Map Perimeter $50^{\circ}$

$$
\begin{equation*}
D=\frac{2 R}{S \times 10^{6}} \tag{5.1}
\end{equation*}
$$

where $R$ is the radius of the earth measured in one half-inch grid cells and was chosen to be consistent with polar stereographic projections described in other documentation.

The integer number of grids of desired size from the pole to the map perimeter is:

$$
\begin{equation*}
\mathrm{N}=\mathrm{D} \times \tan \frac{90-\left|\phi_{\mathrm{p}}\right|}{2} \tag{5.2}
\end{equation*}
$$

The grid, defined by I and $J$ axes, with the origin in the upper left corner (see Figure 11b), represents the coordinate of the North Pole as:

$$
\begin{align*}
& \mathrm{Ip}=\mathrm{N}+1  \tag{5.3}\\
& \mathrm{Jp}=\mathrm{N}+1
\end{align*}
$$

Any point with latitude $\phi$ and longitude $\lambda$, which is located in the northern hemisphere north of $\phi_{p}$ is positioned at the following $I, J$ coordinate:
$I=I N T[d x A \times \cos (X)+I p+0.5]$
$J=I N T[d x \sin (X)+J p+0.5]$
where
$d$ is $D \times \tan \frac{90-\left|\phi_{p}\right|}{2}$
X is $\lambda+\mathrm{G}$
$A$ is +1 if $\phi_{p} \geq 0$
$A$ is -1 if $\phi_{p}<0$.

### 5.2 GRIDDING PROCEDURE

The surface height at each grid point location is calculated by fitting the surrounding data to the following biquadratic surface modeling function:

$$
\begin{aligned}
& \mathrm{h}_{\mathrm{ij}}(\lambda, \phi)=\mathrm{C}_{1_{\mathrm{ij}}}+\mathrm{C}_{2_{\mathrm{ij}}} \frac{\left(\lambda-\lambda_{\mathrm{i}}\right)}{\text { capmin }}+\mathrm{C}_{3_{\mathrm{ij}}} \frac{\left(\phi-\phi_{j}\right)}{(\operatorname{capmin})\left(\cos \phi_{\mathrm{j}}\right)} \\
& +\mathrm{C}_{4_{\mathrm{ij}}} \frac{\left(\lambda-\lambda_{i}\right)}{(\text { capmin })} \frac{\left(\phi-\phi_{j}\right)}{(\operatorname{capmin})\left(\cos \phi_{\mathrm{j}}\right)}+\mathrm{C}_{5_{i \mathrm{l}}} \frac{\left(\lambda-\lambda_{1} 1^{2}\right.}{\text { capmin }^{2}} \\
& +\mathrm{C}_{6_{1 J}} \frac{\left(\phi-\phi_{j}\right)^{2}}{\left(\cos ^{2} \phi_{j}\right)\left(\operatorname{capmin}^{2}\right)}
\end{aligned}
$$

where
$h_{i j} \quad=$ value of the surface elevation function for the $i j g r i d$ point as evaluated at the location ( $\lambda, \phi$ );
$\mathrm{C}_{1_{1 \mathrm{j}}}-\mathrm{C}_{6_{\mathrm{ij}}}=$ numerically determined coefficients of the biquadratic function for grid point ij; and
$\lambda_{1} \phi_{\mathrm{j}} \quad=$ longitude and latitude of the ij grid point in deg.
capmin $\quad=$ minimum cap size in deg longitude.

A weighted least-squares method is used to solve for the coefficients $C_{1_{1 j}}-C_{6_{1 j}}$ at each grid point ij. The weighting is invoked to prevent the obliteration of the local surface details by the smoothing process, and to lend greater importance to the data closest to the grid point location. The form of the weighting function is

$$
\begin{equation*}
\mathrm{w}_{\mathrm{k}_{\mathrm{ij}}}=\frac{1}{\sigma_{\mathrm{O}_{\mathrm{k}} \mathrm{D}_{\mathrm{k}_{1 \mathrm{j}}}^{2}}^{\mathrm{N}}} \tag{5.6}
\end{equation*}
$$

where

$$
\begin{aligned}
& \mathrm{w}_{\mathbf{k}_{\mathrm{ij}}}=\begin{array}{l}
\text { weight of the } \mathbf{k}^{\text {th }} \text { data point used in determining the coefficlents of the surface } \\
\text { function for the } i \mathrm{j} \text { grid location; }
\end{array} \\
& \sigma_{\mathrm{o}_{\mathbf{k}}}=\text { observation standard deviation of the } \mathbf{k}^{\text {th }} \text { data point; } \\
& \mathrm{N}=\text { power of inverse distance weighting; and } \\
& \mathrm{D}_{\mathrm{k}_{\mathrm{ij}}}=\text { the distance from the } \mathbf{k}^{\text {th }} \text { data point to location } \mathrm{ij},
\end{aligned}
$$

where $\quad D_{k i j}=\left\{\left[\left(\lambda_{k}-\lambda_{i}\right) \cos \phi_{k}\right]^{2}+\left(\phi_{k}-\phi_{j}\right)^{2}\right\}^{1 / 2}$
The observation standard deviation was assigned a value of 1.0 m . The power of inverse distance weighting was assigned a value of 2.0 m . The formula used for the least-squares minimization in matrix notation is

$$
\begin{equation*}
P_{i j}^{T} W_{i j} P_{i j} C_{i j}=P_{i j}^{T} W_{i j} H_{i j} \tag{5.7}
\end{equation*}
$$

or

$$
\begin{equation*}
\mathrm{C}_{1 \mathrm{j}}=\left[\mathrm{P}_{\mathrm{ij}}^{\mathrm{T}} \mathrm{~W}_{\mathrm{ij}} \mathrm{P}_{\mathrm{ij}}\right]^{-1} \mathrm{P}_{\mathrm{ij}}^{\mathrm{T}} \mathrm{~W}_{\mathrm{ij}} \mathrm{H}_{\mathrm{ij}} \tag{5.8}
\end{equation*}
$$

where

$$
\mathrm{H}_{\mathrm{ij}}=\left[\begin{array}{l}
\mathrm{h}_{1} \\
\vdots \\
\mathrm{~h}_{\mathrm{k}} \\
\vdots \\
\mathrm{~h}_{\mathrm{m}}
\end{array}\right]
$$

is the observational data set used in determination of grid point ij ;

$$
\mathrm{P}_{\mathrm{ij}}=\left[\begin{array}{ccccc}
\partial \mathrm{h}_{1} & \frac{\partial \mathrm{~h}_{1}}{} & \cdot & \cdot \frac{\partial \mathrm{~h}_{\perp}}{\partial \mathrm{C}_{6_{\mathrm{ij}}}} \\
\partial \mathrm{C}_{1_{i j}} & \frac{\partial \mathrm{C}_{2_{\mathrm{ij}}}}{} & & & \vdots \\
\vdots & & & & \vdots \\
2 \mathrm{~h}_{\mathrm{m}} & \cdot & \cdot & \cdot & \frac{2 \mathrm{~h}_{\mathrm{m}}}{\partial \mathrm{C}_{6_{\mathrm{ij}}}}
\end{array}\right]
$$

is the matrix of observational partial derivatives;

$$
c_{1 j}=\left[\begin{array}{c}
c_{1_{1 j}} \\
\vdots \\
c_{6_{1 j}}
\end{array}\right]
$$

is the set of coefficients for grid point;

$$
\mathrm{w}_{1 \mathrm{j}}=\left[\begin{array}{lllll}
\mathrm{w}_{1_{1 j}} & & & & 0 \\
& & \cdot & & \\
& & & \cdot & \\
0 & & & \cdot & w_{\mathrm{m}_{1 j}}
\end{array}\right]
$$

is the observation weighting matrix.

A solution exists for Equation (5.8) if the determinant of the normal matrix $B_{i j}=P_{i j}^{T} W_{i j} C_{i j}$ is positive. However, poor data distribution can cause ill-conditioned matrices yielding solutions that vary considerably from the expected results. One needs to be able to recognize when numerical problems occur to assure reasonable solutions. To this end the singular value decomposition (SVD) method is used to solve the matrix equation. The results of the SVD process give an indication of the stability of the equations and therefore whether a unique stable solution exists (Forsythe, Malcolm, and Moler, 1977). When the normal matrix $\mathrm{B}_{\mathrm{l}}$ is used as input to SVD, three output matrices are calculated: $\Sigma, \mathrm{U}$, and $\mathrm{V} . \Sigma$ is a diagonal matrix, such that

$$
\Sigma=\left[\begin{array}{lllll}
\sigma_{1} & & & & 0 \\
& \cdot & & & \\
& & \cdot & & \\
0 & & & & \sigma_{6}
\end{array}\right]
$$

where the $\sigma$ 's are referred to as the singular values of $B$. The matrices $U$ and $V$ are used to transform the equations

$$
\mathrm{Bc}=\mathrm{y}
$$

into an equivalent diagonal set of equations

$$
\Sigma \bar{c}=\bar{y}
$$

In principle, if none of the $\sigma$ 's are zero the transformed equations could be solved using

$$
\overline{\mathrm{C}}_{1}=\frac{\overline{\mathrm{y}}_{1}}{\sigma_{1}}
$$

In practice, when any of the $\sigma$ 's are small, numerical instability can result, giving unreasonable answers. The key to using SVD is to set a tolerance $\tau$ which reflects the accuracy of the data and the arithmetic used. If any $\sigma$ 's are less than $\tau$ times the largest $\sigma$ then those corresponding
$\bar{c}$ 's are not uniquely defined and unreasonable results can occur. When problems occur, steps must be taken to provide more information to evaluate the surface function.

Once $\tau$ is chosen, then $\Sigma, \mathrm{U}$, and V are used in the following manner to calculate cach coefficient $\mathrm{C}_{1}$.

$$
S=\sum_{j=1}^{m} U(j, i) Y_{j}
$$

for all j where $\sigma_{\mathrm{j}}>\tau$

$$
C_{1}=\sum_{k=1}^{n} \frac{S}{\sigma_{k}} V(i, k)
$$

In this study the value of $\tau$ used was .001 m . SVD is then used to determine when there are sufficient data to provide a unique solution to the surface modeling function. When a unique solution cannot be found more data are added and the function is reevaluated. At each grid location ij , data within the circular area defined by radius R from the grid location are used in the solution. Four different values for R are used: $33 \mathrm{~km}, 55 \mathrm{~km}, 88 \mathrm{~km}$, and 132 km . Initially the smallest value of $R$ is used and if a solution cannot be found then $R$ is increased. If the biquadratic solution at the maximum value of $R$ is unsatisfactory according to the SVD criterion, then the function (Equation 5.5) is reduced to a bilinear function by setting coefficients C 4 through C 6 to zero. If a valid solution still cannot be found, then the grid value is considered undefined and set to -1000.0 .

Individual data point removal is also invoked during the gridding process. After finding a valid solution at location ij , the weighted rms of the residuals of the data with respect to the surface is calculated using

where

$$
\operatorname{Res}_{k l j}=h_{k}-h_{k l j}
$$

$h_{\mathrm{kij}}=\quad$ height at location of measurement k evaluated using the surface function for grid location ij.

The following inequality is then evaluated for each data point used in the solution.

$$
\begin{equation*}
\frac{\operatorname{Res}_{k y}}{\sigma_{\mathrm{O}_{\mathrm{k}} D^{N}}^{N}}<\mathrm{E}_{\text {mult }} * \mathrm{RMS}_{\mathrm{WT}_{\mathrm{ij}}} \tag{5.10}
\end{equation*}
$$

A value of the editing multiplier ( $\mathrm{E}_{\text {mult }}$ ) equal to 3.5 is used and all data points that do not satisfy the inequality are deleted. When any data points are deleted the surface function is reevaluated using the remaining data. A minimum of 10 data points are required to solve for the function.

The standard deviation associated with the grid height, $\sigma_{\text {Gij }}$, is then calculated to determine how well the grid represents the data.

$$
\sigma_{\mathrm{GIIf}}=\mathrm{RMS}_{\mathrm{WT}_{\mathrm{ij}}} \cdot\left(\mathrm{~V}_{11} \mathrm{ij}\right)^{1 / 2} .
$$

where

$$
\mathrm{V}_{\mathrm{ij}}=\quad \mathrm{B}_{\mathrm{ij}}^{-1} \mathrm{P}_{\mathrm{ij}} \mathrm{~W}_{\mathrm{ij}}\left[\begin{array}{cccc}
\sigma_{\mathrm{o}_{1}}^{2} & & & \\
& & & \\
& \ddots & & \\
& & \ddots & \\
& & & \\
0 & & & o_{\mathrm{o}_{\mathrm{o}}}^{2}
\end{array}\right] \quad\left[\mathrm{B}_{1 \mathrm{j}}^{-1} \mathrm{P}_{\mathrm{ij}}^{\mathrm{T}} \mathrm{~W}_{\mathrm{ij}}\right] \text {. }
$$

Grid points that have a large value of $\sigma_{\mathrm{G}}$ do not represent the data as well as those that have smaller $\sigma_{\mathrm{G}}$ 's.

The format of the grid record is described in Table 8. The location, coefficients, $\sigma_{\mathrm{G}}$, number of points used and other pertinent parameters are output for each grid point location. The user can utilize these parameters to decide the accuracy of the individual grid values.

## TABLES

Table 1. Ice Data Record Description

General Characteristics:

| Record Format | - variable |
| :--- | :--- |
| Record Size (bytes) | $-164+4$ for IBM record control word |
| Blocksize (bytes) | $-31920+4$ for IBM block control word |

The first seven records of the IDR data set are 80 bytes long and contain a brief description of the contents of the file. The remaining records follow the 164 -byte format.

HEADER RECORDS

|  | FORTRAN <br> Variable <br> Type | Description |
| :--- | :--- | :--- |
| Bytes | Al | Brief description of file contents. (Comprises first seven records <br> only) |

## DATA RECORDS

| Bytes | FORTRAN <br> Variable <br> Type | Description |
| :---: | :---: | :---: |
| 1-4 | I*4 | Satellite ID - This is the international satellite designation nnpppqq where: |
|  |  | nn - last two digits of the year of launch (e.g., 197474,1969 69). |
|  |  | ppp - order of launch. <br> Example: <br> The 25th vehicle launch in a given year is designated with $\mathrm{ppp}=025$. |
|  |  | qq - component identifier (e.g., component a $\rightarrow 01$, component $\ell \rightarrow 12$, etc.). |
| 5-6 | I*2 | Measurement type |
|  |  | 40-44 Altimeter height |
|  |  | $40=$ Long pulse (GEOS data) |
|  |  | $41=$ Short pulse (GEOS data) |
|  |  | 43 = Seasat altimetry |

Table 1. Ice Data Record Description (Cont.)


Table 1. Ice Data Record Description (Cont.)


Table 1. Ice Data Record Description (Cont.)

| Bytes | FORTRAN <br> Variable $\qquad$ <br> Type <br> Desc | ion |  |
| :---: | :---: | :---: | :---: |
| (13-16 Cont.) | Bits | Value | Description |
|  | 14 | 0 1 | Total tide indicator <br> Solid and ocean tides removed from observation if found on data record Observation includes solid and ocean tides |
|  | 15 | 0 1 | Center of gravity indicator <br> Center of gravity correction applied to observation <br> Center of gravity correction not applicd to observation |
|  | 16-20 |  | Unused |
|  | 21 | $\begin{gathered} 0 \\ 1 \end{gathered}$ | Altimeter mode (GEOS only) Global track mode Intensive track mode |
|  | 22-27 |  | Unused |
|  | 28 | $\begin{aligned} & 0 \\ & 1 \end{aligned}$ | Location indicator Over water Over land |
|  | 29 | 0 1 | Orbit adjustment indicator <br> Orbit adjustment has been applied to observation <br> Orbit adjustment has not been applied to observation |
|  | 30 | 0 1 | Slope correction indicator <br> Slope correction has been applied to observation <br> Slope correction has not been applied to observation |
|  | 31 | 0 1 | Retracking correction indicator <br> Retracking correction has been applied to observation <br> Retracking correction has not been applied to observation |

Table 1. Ice Data Record Description (Cont.)

| Bytes | FORTRAN Variable $\qquad$ | Description |
| :---: | :---: | :---: |
| 17-20 | I*4 | Modified Julian Date (MJD) of observation Julian Date $=$ MJD +2400000.5 |
| 21-28 | R*8 | Fraction of day past midnight (GMT) |
| 29-36 | R*8 | Altimeter range measurement in meters |
| 37-40 | R*4 | Satellite latitude in degrees |
| 41-44 | R*4 | Satellite east longitude in degrees |
| 45-48 | R*4 | Measurement standard deviation in meters |
| 49-52 | R*4 | Center of gravity correction in meters |
| 53-56 | R*4 | Tropospheric refraction correction in meters |
| 57-60 | R*4 | Ionospheric refraction correction in meters |
| 61-64 | R*4 | GEM10-B geoid height above reference ellipsoid in meters |
| 65-68 | R*4 | Total tide height above reference ellipsoid in cm . |
| 69-72 | I* 4 | Rev number |
| 73-76 | I* 4 | Surface height with respect to ellipsoid in cm. |
| 77-78 | $\mathrm{I}^{*} 2$ | Surface height status word |
|  |  |  |
|  |  | Bits Value Description |
|  |  | 0-8 0 Unused |
|  |  | $\begin{array}{lll} 9 & 1 & \text { Slope correction applied } \\ & 0 & \text { Slope correction not applied } \end{array}$ |
|  |  | $\begin{array}{lll} 10 & 1 & \text { Orbit adjustment applied } \\ 0 & \text { Orbit adjustment not applied } \end{array}$ |
|  |  | 1131 Solid tides removed  <br>  0 Solid tides not removed |
|  |  | 12 <br> 1 <br> Retracking correction applied Retracking correction not applied |
|  |  | $13 \begin{array}{lll}1 & \text { Center of gravity blas applied } \\ 0 & \text { Center of gravity bias not applied }\end{array}$ |

Table 1. Ice Data Record Description (Cont.)

| $\frac{\text { Bytes }}{(77-78}$ | FORTRAN <br> Variable $\qquad$ Type | Bits | Value | Description |
| :---: | :---: | :---: | :---: | :---: |
|  |  | 14 | $\begin{aligned} & 1 \\ & 0 \end{aligned}$ | Tropospheric correction applied Tropospheric correction not applied |
|  |  | 15 | $\begin{aligned} & 1 \\ & 0 \end{aligned}$ | Ionospheric correction applied Ionospheric correction not applied |
| 79-80 | I*2 |  |  |  |
| 81-82 | I*2 | Automatic Gain Control (AGC) in dB |  |  |
| 83-84 | I*2 | Solid tides in cm. |  |  |
| 85-86 | I*2 | Tangent of along-track slope ( $\times 10^{5}$ ) |  |  |
| 87-88 | I*2 | Tangent of cross-track slope ( $\times 10^{5}$ ) |  |  |
| 89-90 | I*2 | Size of window used in obtaining along-track slope in meters |  |  |
| 91-92 | I*2 | Along-track and cross-track slope correction word. If all bits are zero, then slopes for slope correction were not able to be computed. |  |  |
|  |  |  |  |  |
|  |  | Bits | Value | Description |
|  |  | 0-9 |  | Unused |
|  |  | 10 | 1 | Along-track slope set to the maximum value of .8 degree during iterative procedure. |
|  |  | 11 | 1 | Cross-track slope set to the maximum value of .8 degree. |
|  |  | 12 | 1 | Along-track slope set to .8 degree after final iteration. |
|  |  | 13 | 1 | Window was extended to 20 km with no point found; reference grid used to calculate alongtrack slope. |
|  |  | 14 | 1 | Window had to be extended in both directions to determine along-track slope, but it is less than 20 km . |
|  |  | 15 | 1 | Two adjacent points were found and used to determine along-track slope. |
| 93-96 | R*4 | Orbit adjustment to 84,306 ocean surface in meters |  |  |
| 97-100 | R*4 | RMS of | rbit adju | tment fit in meters |

Table 1. Ice Data Record Description (Cont.)


Table 1. Ice Data Record Description (Cont.)

| Bytes | FORTRAN <br> Variable <br> Type | Description |  |  |
| :---: | :---: | :---: | :---: | :---: |
| (161-162 | Cont.) | Bits | Value | Description |
|  |  | 6 | 0 1 | For double waveforms the retracking correction is not calculated from a weighted average of the two leading edges. <br> For double waveforms the retracking correction is calculated from a weighted average of the two leading edges. |
|  |  | 7 | 0 1 | No problem with leading edge definition of waveform <br> Waveform not defined well enough to filter, no leading edges or too many leading edges |
|  |  | 8 | $0$ | No problem retracking Problem retracking |
|  |  | 9 | $0$ | Timing bias was not applied to time tag Timing bias applied to time tag |
|  |  | 10 | $0$ | Waveform not retracked Waveform retracked |
|  | applies to water data | 11 | $0$ | Whole edge retracked Leading edge retracked |
|  |  | 12 | $0$ | Ht correction not applied due to $\ddot{\mathrm{h}}$ Ht correction applied due to $\ddot{\mathrm{h}}$ |
|  |  | 13 | $0$ | Attitude seastate correction not applied to $h$ Attitude seastate correction applied to $h$ |
|  |  | 14-15 | $\begin{aligned} & 0 \\ & 1 \\ & 2 \\ & 3 \end{aligned}$ | Tracking mode 1 Tracking mode 2 Tracking mode 3 Tracking mode 4 |
| 163-164 | I*2 | Version number of retracking program that converted the data from SDR to IDR format |  |  |
|  |  | $\mathrm{n}_{1} \mathrm{n}_{2} \mathrm{n}_{3} \mathrm{n}_{4} \mathrm{n}_{5}$ |  |  |
|  |  | $\mathrm{n}_{1} \mathrm{n}_{2}$ | year | version |
|  |  | $\mathrm{n}_{3} \mathrm{n}_{4}$ | mon | f version |
|  |  | $\mathrm{n}_{5}$ | poin | . of version |






| $\begin{aligned} & \text { REV } \\ & \text { NUMBER } \end{aligned}$ | APPROXIMATE <br> LATITUDE AND <br> DIRECTION AT <br> 315.0 E LONG <br> $A=A S C E N D I N G$ $D=D E S C E N D I N G$ <br> D = DESCENDING |  | $\begin{gathered} \text { STAR } \\ \text { LEAT } \end{gathered}$ | $\begin{aligned} & \text { ING } \\ & \text { LONG } \\ & \text { DEG } \end{aligned}$ | $\begin{gathered} \text { END } \\ \operatorname{DEGT} \mathrm{S}_{\mathrm{K}} \end{gathered}$ | NC <br> LONG DEG E | NUMBER <br> OF PTS |  |  |  | $\underset{R E}{\text { BINS }}$ | $\begin{aligned} & \text { THROU } \\ & \text { TRAV } \end{aligned}$ | $\begin{aligned} & \text { H WHI } \\ & \text { RSES } \end{aligned}$ |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 805 | 70.53 | A | 68.310 | 327.112 | 71.604 | 304.313 | 447 | 1295 | 1452 | 1608 | 1685 | 1684 | 1764 | 1763 | 1762 | 1853 |
|  |  |  |  |  |  |  |  | 2252 | 1851 | 1951 | 1950 | 2050 | 2049 | 2148 | 2147 2540 | 2247 2640 |
|  |  |  |  |  |  |  |  | 2646 | 2738 | 2734 | 2835 | 2934 | 3032 | 3130 | 3128 | 3228 |
|  |  |  |  |  |  |  |  | 3227 | 3226 | 3326 | 3324 | 3712 | 3811 |  |  |  |
| 604 | 70.62 | A | 69.792 | 320.366 | 70.650 | 314.611 | 103 | 1951 | 2051 | 2050 | 2445 | 2444 | 2443 | 2641 | 2740 | 2739 |
|  | 70.78 | A | 68.879 |  |  |  | 536 | 2738 1533 | 2838 | 2837 |  |  |  |  |  | 2054 |
| 848 |  |  |  | 326.476 | 71.336 | 309.603 |  | 1533 2053 | 21512 | 2152 | 1689 | 2251 | 2250 | 2350 | 2349 | 2348 |
|  |  |  |  |  |  |  |  | 2448 | 2447 | 2547 | 2546 | 2545 | 2645 | 2644 | 2643 | 2743 |
|  |  |  |  |  |  |  |  | 2742 | 2741 | 2841 | 2840 | 2939 | 2938 | 2937 | 3037 | 3036 |
|  |  |  |  |  |  |  |  | 3035 | 3135 | 3134 | 3133 | 3233 | 3231 | 3331 | 3330 | 3329 |
|  |  |  |  |  |  |  |  | 3328 | 3428 | 3427 | 3426 | 3525 |  |  |  |  |
| 647 | 70.80 | A | 69.386 | 324.062 | 71.393 | 309.039 | 574 | 1689 2153 | 1768 2152 | 1857 | 1856 | 1956 2250 | 1955 | 2055 2349 | 2054 | 2053 2448 |
|  |  |  |  |  |  |  |  | 2447 | 2547 | 2546 | 2545 | 2645 | 2644 | 2643 | 2743 | 2742 |
|  |  |  |  |  |  |  |  | 2842 | 2841 | 2840 | 2939 | 2938 | 3038 | 3036 | 3035 | 3135 |
|  |  |  |  |  |  |  |  | 3134 | 3133 | 3233 | 3231 | 3331 | 3330 | 3329 | 3328 | 3428 |
|  |  |  |  |  |  |  |  | 3427 | 3426 | 3526 1534 | 3525 1690 | 3523 1769 |  |  |  |  |
| 891 | 70.85 | A | 68.446 | 329.146 | 71.715 | 305.207 | 575 | 1379 2055 | 1535 2155 | 1534 | 21690 | 1769 | 1858 | 2358 | 2351 | 2056 <br> 2350 |
|  |  |  |  |  |  |  |  | 2450 | 2449 | 2549 | 2548 | 2547 | 2647 | 2646 | 2645 | 2745 |
|  |  |  |  |  |  |  |  | 2744 | 2743 | 2843 | 2842 | 2841 | 2941 | 2940 | 2939 | 3039 |
|  |  |  |  |  |  |  |  | 3038 | 3037 | 3137 | 3136 | 3135 | 3235 | 3234 | 3332 |  |
|  |  |  |  |  |  |  |  | 3429 | 3428 | 3427 | 3525 | 3524 | 3624 | 3914 |  |  |
| 1020 | 70.89 | A | 68.603 | 328.751 | 71.498 | 308.684 | 507 | 1458 | 1614 2155 | 1692 | 1770 2254 | 1768 2253 | 1958 2353 | 1957 | 2057 2351 | 2056 |
|  |  |  |  |  |  |  |  | 2450 | 2449 | 2549 | 2548 | 2647 | 2646 | 2746 | 2745 | 2744 |
|  |  |  |  |  |  |  |  | 2844 | 2843 | 2842 | 2942 | 2941 | 2940 | 3040 | 3038 | 3138 |
|  |  |  |  |  |  |  |  | 3136 | 3236 | 3235 | 3234 | 3233 | 3332 | 3430 | 3428 | 3528 |
|  |  |  |  |  |  |  |  | 3526 | 3625 | 3622 |  |  |  |  |  |  |
| 1493 | 70.89 | A | 68.484 | 329.376 | 68.503 | 329.293 | 12 | 1379 1380 |  |  |  |  |  |  |  |  |
| 1321 | 70.89 70.89 | A | 68.445 71.326 | 329.532 310.857 | 71.794 | 309.528 | 21 | 358 | 3526 | 3625 | 3624 |  |  |  |  |  |
| 1235 | 70.89 70.89 | A | 71.392 | 310.110 | 71.441 | 309.515 | 13 | 3526 | 3626 | 3625 | 3624 |  |  |  |  |  |
| 690 | 70.97 | ${ }_{\text {A }}$ | 68.590 | 329.348 | 71.790 | 304.691 | 527 | 1379 2354 | 1536 2353 | 1769 | 1959 | 2057 | 2157 2551 | 2156 2550 | 2255 | 2254 2649 |
|  |  |  |  |  |  |  |  | 2648 | 2647 | 2747 | 2746 | 2745 | 2845 | 2844 | 2843 | 2943 |
|  |  |  |  |  |  |  |  | 2942 | 2941 | 3041 | 3039 | 3139 | 3138 | 3137 | 3237 | 3334 |
|  |  |  |  |  |  |  |  | 3333 | 3431 | 3529 | 3528 | 3625 | 3912 |  |  |  |
| 446 | 70.98 | A | 69.127 | 326.991 | 71.388 | 310.684 | 651 | 1614 | 1771 | 1770 | 1860 | 1960 | 1959 | 2059 | 2058 | 2057 2452 |
|  |  |  |  |  |  |  |  | 2451 | 2551 | 2550 | 2549 | 2649 | 2648 | 2647 | 2747 | 2746 |
|  |  |  |  |  |  |  |  | 2846 | 2845 | 2844 | 2944 | 2943 | 2942 | 33042 | 33041 | 3040 3431 |
|  |  |  |  |  |  |  |  | 3139 3430 | 3137 3529 | 3237 3527 | 3236 | 3235 | 3335 | 3334 | 3333 | 3431 |










| $\begin{aligned} & \text { REV } \\ & \text { NUMBER } \end{aligned}$ | APPROXIMATE LATITUDE AND DIRECTION AT 315.0 E LONG $A=A S C E N D I N G$ $D=$ DESCENDING <br> D = DESCENDING |  | $\begin{gathered} \text { STARTING } \\ \text { LAT \& IONG } \\ \text { DEGN DEG E } \end{gathered}$ |  | Table 2. Seasat IDR Greenland Catalog (Cont.) |  |  |  |  | Bins through which REV TRAVERSES |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | $\begin{gathered} \text { LAT } \\ \text { ENI } \end{gathered}$ | $\begin{aligned} & \text { ING } \\ & \text { LONG } \\ & \text { DEG E } \end{aligned}$ | $\begin{aligned} & \text { NUMBER } \\ & \text { OF PTS } \end{aligned}$ |  |  |  |  |  |  |  |  |  |
| 401 | 69.95 | D |  |  | 71.680 | 330.606 | 68.899 | 309.260 |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  | 330.606 | 68.899 | 309.260 | 264 | 3877 3053 | 3772 2953 | 3670 2952 | 3565 2951 | 3462 2851 | 3360 2850 | 3155 2849 | 3055 | 3054 2748 |
|  |  |  |  |  |  |  |  | 2646 | 2645 | 2442 | 2342 | 2341 | 2239 | 2849 2138 | 1746 | 2748 1745 |
| 645 | 69.97 | D | 71.920 | 335.139 | 68.859 | 308.895 | 635 | 1664 | 1663 | 1580 | 1500 | 1499 |  |  |  |  |
|  |  |  |  |  | 68.859 | 308.895 | 635 | 4188 | 4086 3567 | 4084 | 4083 | 4082 | 3978 | 3877 | 3876 | 3874 |
|  |  |  |  |  |  |  |  | 3258 | 3257 | 3157 | 35156 | 3462 | 33154 | 3360 3054 | 3359 3053 | 3259 |
|  |  |  |  |  |  |  |  | 2952 | 2951 | 2950 | 2850 | 2849 | 2848 | 2748 | 2747 | 3052 2746 |
|  |  |  |  |  |  |  |  | 2646 | 2645 | 2545 | 2544 | 2543 | 2443 | 2442 | 2441 | 2341 |
|  |  |  |  |  |  |  |  | 2340 | 2240 | 2239 | 2238 | 2138 | 2137 | 2036 | 1934 | 1833 |
| 846 | 70.00 | D | 71.672 | 330.105 | 68.958 | 309.216 |  | 1832 | 1746 | 1745 | 1744 | 1663 | 1581 | 1580 | 1499 | 1498 |
|  |  |  |  |  | 68.958 | 309.216 | 638 | 3876 336 | 3875 3359 | 3772 | 3669 | 3667 | 3564 | 3462 | 3461 | 3361 |
|  |  |  |  |  |  |  |  | 3054 | 3053 | 3052 | 2952 | 2951 | 2950 | 2850 285 | 2859 | 3154 <br> 2848 |
|  |  |  |  |  |  |  |  | 2748 | 2747 | 2746 | 2646 | 2645 | 2644 | 2544 | 2543 | 2848 |
|  |  |  |  |  |  |  |  | 2442 | 2441 | 2341 | 2340 | 2239 | 2238 | 2137 | 2136 |  |
|  |  |  |  |  |  |  |  | 2035 | 1935 | 1933 | 1833 | 1745 | 1744 | 1743 | 1663 | 1662 |
| 803 | 70.30 | D | 71.960 | 334.170 | 69.319 | 309.108 | 474 | 1499 | 4184 | 4183 | 3975 | 3974 | 3972 |  |  |  |
|  |  |  |  |  |  |  |  | 3665 | 3662 | 3562 | 3561 | 3560 | 3559 | 3459 | 3458 | 3767 3457 |
|  |  |  |  |  |  |  |  | 3456 | 3356 | 3355 | 3354 | 3254 | 3253 | 3252 | 3151 | 3767 3150 |
|  |  |  |  |  |  |  |  | 2947 | 2946 | 2945 | 2845 | 2844 | 2843 | 2743 | 2742 | 2641 |
|  | 70.41 | D |  |  |  |  |  | 2640 2132 | 2539 1659 | 2538 | 2437 | 2436 | 2335 | 2234 | 2233 | 2133 |
| 559 | 70.41 | D | 71.929 | 332.481 | 69.499 | 309.216 | 749 | 4182 | 4181 | 4076 | 3971 | 3766 | 3764 | 3763 | 3663 | 3662 |
|  |  |  |  |  |  |  |  | 3661 3454 | 33660 | 3560 3353 | 3559 | 3558 | 3557 | 3457 | 3456 | 3455 |
|  |  |  |  |  |  |  |  | 3148 | 3147 | 3047 | 3046 | 3045 | 2945 | 2944 | 2249 | 3149 |
|  |  |  |  |  |  |  |  | 2842 | 2841 | 2741 | 2740 | 2739 | 2639 | 2638 | 2637 | 2843 |
|  |  |  |  |  |  |  |  | 2536 | 2436 | 2435 | 2434 | 2334 | 2333 | 2232 | 2231 | 2537 2131 |
| 760 | 70.58 | D | 71.895 | 330.394 | 70.041 | 311.170 | 617 | 2130 4076 | 2129 | 2029 | 2028 | 1928 | 1826 | 1739 |  |  |
|  |  |  |  |  |  | 31.170 |  | 3659 | 3658 | 3968 | 3856 | 3763 | 3762 | 3761 | 3760 | 3660 |
|  |  |  |  |  |  |  |  | 3452 | 3451 | 3351 | 3350 | 3349 | 3249 | 3248 | 3247 | 3453 3145 |
|  |  |  |  |  |  |  |  | 3144 | 3044 | 3043 | 3042 | 2942 | 2941 | 2940 | 2840 | 3145 2839 |
|  |  |  |  |  |  |  |  | 2838 | 2737 | 2635 | 2634 | 2534 | 2533 | 2432 | 2431 | 2331 |
| 272 | 70.59 | D | 72.051 | 336.279 | 69.867 | 310.053 | 810 | 2330 4291 | 2229 4290 | 4228 | 4287 |  |  |  |  |  |
|  |  |  |  |  |  |  |  | 3970 | 3969 | 3968 | 3967 | 3867 | 3866 | 3865 | 3864 | 4072 |
|  |  |  |  |  |  |  |  | 3763 | 3762 | 3761 | 3760 | 3660 | 3659 | 3658 | 3657 | 3863 |
|  |  |  |  |  |  |  |  | 3556 | 3555 | 3554 | 3454 | 3453 | 3452 | 3451 | 3351 | 3350 |
|  |  |  |  |  |  |  |  | 3349 | 3249 | 3248 | 3247 | 3246 | 3145 | 3144 | 3044 | 3043 |
|  |  |  |  |  |  |  |  | 2635 | 2634 | 2534 | 2533 | 2432 | 2839 | 2838 | 2737 | 2736 |
| 516 | 70.61 | D | 72.019 | 334.122 | 69.643 | 308571 |  | 2228 | 2127 | 2026 |  |  |  |  |  | 2229 |
|  |  |  |  |  | 69.643 | 308.571 | 731 | 4286 3863 | 4285 | 4183 | 4075 | 3968 | 3967 | 3866 | 3865 | 3864 |
|  |  |  |  |  |  |  |  | 3656 | 3556 | 3555 | 3554 | 3553 | 3453 | 3659 | 3658 | 3657 |
|  |  |  |  |  |  |  |  | 3350 | 3349 | 3348 | 3248 | 3247 | 3145 | 3144 | 3044 | 3043 |
|  |  |  |  |  |  |  |  | 3042 | 3041 | 2941 | 2940 | 2939 | 2839 | 2838 | 2737 | 3645 2635 |
|  |  |  |  |  |  |  |  | 2634 | 2534 | 2533 | 2432 | 2431 | 2228 | 2127 | 1822 |  |


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| $\frac{2}{2}$ |  |  |  |  |  |  | － |





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Table 4. Corrections To Seasat Ice Data Records

| CORRECTION ADJUSTMENT | VALUE OR RANGE | MANNER IN WHICH APPLIED |  | SECTION <br> IN WHICH DOCUMENTED |
| :---: | :---: | :---: | :---: | :---: |
|  |  | TIME | SURFACE HEIGHT |  |
| RETRACKING CORRECTION accounts for lag in tracker response | $-15 \mathrm{~m}<\Delta \mathrm{H}_{\mathrm{RET}}<15 \mathrm{~m}$ | N/A | (-) | 2.1 |
| TIME BIAS accounts for track mode correction | $-7.9451 \times 10^{-2} \mathrm{~s}$ | (+) | N/A | 2.2.1 |
| SIGNAL TRAVEL TIME CORRECTION | $-2.67 \times 10^{-3} \mathrm{~s}$ | $(+)$ | N/A | 2.2.1 |
| CENTER OF GRAVITY OFFSET adjusts measurement to $\mathrm{s} / \mathrm{c}$ center of mass | $\sim 6.04 \mathrm{~m}$ | N/A | (-) | 2.2.2 |
| IONOSPHERIC REFRACTION CORRECTION accounts for signal delay | $\sim 2-3 \mathrm{~cm}$ | N/A | ( + ) | 2.3.1 |
| TROPOSPHERIC REFRACTION CORRECTION accounts for signal delay | $\sim 1.5-2.5 \mathrm{~m}$ | N/A | ( + ) | 2.3.2 |
| SOLID TIDE removal | $\sim 2-10 \mathrm{~cm}$. | N/A | (-) | 2.4 |
| ORBIT ADJUSTMENT reduces orbit crror and references the data to a mean ocean surface | $3 \mathrm{~m} \leq \Delta \mathrm{H}_{\mathrm{ORB}} \leq 3 \mathrm{~m}$ | N/A | (-) | 2.5 |
| SLOPE CORRECTION accounts for signal being returned from closest point within satellite footprint | $\mathrm{Om} \leq \Delta \mathrm{H}_{\mathrm{SLOPE}}<80 \mathrm{~m}$ | N/A | (-) | 2.6 |

Table 5. Waveform Data Record Description

## General Characteristics:

$\begin{array}{ll}\text { Record Format } & - \text { variable } \\ \text { Record Size (bytes) } & -170+4 \text { for IBM record control word } \\ \text { Blocksize (bytes) } & -31842+4 \text { for IBM block control word }\end{array}$

FORTRAN
Variable
Bytes
$1-8$
9-16
17-20 $\mathrm{R}^{*}$
21-24 R*4
25-28

29-32 $\mathrm{R}^{*} 4$
33-36 I*4
37-38 I*2
$39-40 \quad I * 2$
41-166 I*2
167-168

Type
R*8
R*8
R*4

R*4

I*2

## Description

Fraction of day past midnight from sensor data record
Altimeter range measurement in meters from sensor data record
Satellite latitude in degrees from sensor data record
Satellite east longitude in degrees from sensor data rccord
Altitude error $\Delta \mathrm{h}$ in meters

Altitude rate error $\Delta \mathrm{h}$ in meters/sec

Modified Julian Date of observation from sensor data record
Significant wave height ( $\mathrm{H} 1 / 3$ ) in cm .
Automatic Gain Control (AGC) in dB
Waveform counts
Word indicating original data flags


Bits Value Description
0-10 Unused

| 11 | 1 | Not in track mode |
| :--- | :--- | :--- |
| 12 | 1 | Chirp/cw |
| 13 | 1 | Altimeter error status |
| 14 | 1 | Reacquisition |
| 15 | 1 | Acq/Trk |

Table 5. Waveform Data Record Description (Cont.)

| Bytes | FORTRAN <br> Variable <br> Type | Description |
| :--- | :--- | :--- |$\quad$| Retracking status word |
| :--- |

Table 5. Waveform Data Record Description



Table 6. Seasat Greenland Geographical Data Base (Cont.)






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| 1219 （ | 3） |  |  |  |  |  |  |  |  |
| 676 | 18） | 7176 | 2） | 12648 | 2） |  |  |  |  |
| 7176 | 2） | 1264 | 2） |  |  |  |  |  |  |
| 7196 | 3） |  |  |  |  |  |  |  |  |
| 4756 | 1） |  |  |  |  |  |  |  |  |
| 2726 | 13） | 516 | 12） | 7601 | 8） |  |  |  |  |
| 5168 | 5） | 518 （ | 2） | 760 （ | 11） |  |  |  |  |
| 5181 | 4） |  |  |  |  |  |  |  |  |
| 559 | 1） | 7626 | 10） |  |  |  |  |  |  |
| 8036 | 4） |  |  |  |  |  |  |  |  |
| 8036 | 22） |  |  |  |  |  |  |  |  |
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| 846 | 24） |  |  |  |  |  |  |  |  |
| 846 | 19） |  |  |  |  |  |  |  |  |
| 647 （ | 6） | 8481 | 12） | 8891 | 23） | 10186 | 8） |  |  |
| 848 （ | 25） | 889 （ | 19） | 1018 | 15） |  |  |  |  |
| 4440 | 13） | 647 （ | 13） | 688 （ | 25） | 8481 | 6） | 891 | 16） |
| 4441 | 10） | 6881 | 18） | 8916 | 22） | 10208 | 21） |  |  |
| 4441 | 5） | 4461 | 6） | 6901 | 15） | 8916 | 1） | 1020 | 20） |
| 6901 | 24） |  |  |  |  |  |  |  |  |
| 446 （ | 13） | 6901 | 4） |  |  |  |  |  |  |
| 2451 | 4） | 4891 | 14） |  |  |  |  |  |  |
| 4891 | 25） | 5301 | 9） |  |  |  |  |  |  |
| 2866 | 21） | 4896 | 3） | 5300 | 24） | 7746 | 6） |  |  |
| 5301 | 10） | 774 （ | 25） |  |  |  |  |  |  |
| 5326 | 21） | 7746 | 12） |  |  |  |  |  |  |
| 5326 | 20） | 5736 | 16） | 776 | 18） |  |  |  |  |
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| 4088 | 5 | 71.80 | 334.79 | 14050 | 1） | 14916 | 4） |  |  |  |  |  |  |  |  |
| 4090 | 10 | 71.80 | 335.59 | 4446 | 4） | 12916 | 3） | 13776 | 3） |  |  |  |  |  |  |
| 4112 | 5 | 71.90 | 304.40 | 7760 | 5） |  |  | 1377 |  |  |  |  |  |  |  |
| 4113 | 3 | 71.90 | 304.80 | 2301 | 2） | 7768 | 1） |  |  |  |  |  |  |  |  |
| 4114 | 4 | 71.90 | 305.20 | 2736 | 1） | 7766 | 3） |  |  |  |  |  |  |  |  |
| 4115 | 1 | 71.90 | 305.60 | 2731 | 1） |  |  |  |  |  |  |  |  |  |  |
| 4119 | 1 | 71.90 | 307.20 | 2738 | 1） |  |  |  |  |  |  |  |  |  |  |
| 4121 | 19 | 71.90 | 308.00 | 2738 | 8） | 4170 | 4） | 5176 | 7） |  |  |  |  |  |  |
| 4122 | 16 | 71.90 | 308．40 | 1738 | 2） | 4608 | 2） | 10346 | 2） |  |  |  |  |  |  |
| 4124 | 38 | 71.90 | 309.20 | 1738 | $7)$ | 8176 | 12） | 4601 | 3） | 5601 | 7） | 6036 | 4） | 8048 | 9） |
| 4125 | 38 |  |  | 847 （ | 5） |  |  |  |  |  |  |  |  |  |  |
|  | 38 | 71.90 | 309.60 | 158 （ | 1） | 1730 | 3） | 2591 | 1） | 5036 | 1） | 6036 | 6） | 6468 | 5） |
| 4126 | 43 | 71.90 | 310.00 | 1588 | 4） | 4600 | 1） | 5036 | 1） | 6468 | 9） | 8040 | 17） | 8476 | 2） |
| 4127 | 53 | 71.90 | 310.40 | $1034($ | 11） | 6460 | 3） |  |  |  |  |  |  |  |  |
|  |  |  |  | 11916 | 18） |  | 3） | 847 | 3） | 8900 | 6） | 10198 | 4） | 11486 | 8） |
| 4128 | 85 | 71.90 | 310.80 | 158 （ | $15)$ | 4601 | 4） | 5036 | 2） | 6469 |  | 8476 | 5） | 8906 | 4） |
| 4129 |  |  |  | 10198 | 3） | 11488 | 18） | 11919 | 6） | 12346 | 17） |  |  |  |  |
| 4130 | 66 | 71.90 | 311.20 311.60 | 4608 1586 | 6） | 6461 | 1） | 1019 | 1） | 11488 | 3） | 11916 | 1） | 12346 | 3） |
|  |  |  |  | 8478 | 20） | 8900 | 4） | 10198 | 6） | 1191 （ |  | 12346 | 2） | 6896 |  |
| 4131 | 51 | 71.90 | 312.00 | 2598 | 10） | 6466 | 21） | 8476 | 20） |  |  |  |  |  |  |
| 4132 | 170 | 71.90 | 312.40 | 1586 | 18） | 2016 | 21） | 2591 | 21） | 4451 | 20） | 4886 | 7） | 5036 |  |
|  |  |  |  | 5468 | 9） | 6461 | 10） | 6891 | 11） | 7901 |  | 8901 | 17） | 10198 | 7） |
| 4133 | 177 | 71.90 | 312.80 | 12346 | 4） |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  | 5460 | 17） | 6898 | 18） | 7901 | 18） | 8900 | 17） | 10196 | 16） | 4881 | 19） |
| 4134 | 120 | 71.90 | 313.20 | 2018 | 18） | 2446 | 21） | 4450 | 21） | 488 C | 19） | 6896 | 19） | 7908 | 21） |
| 4135 | 136 | 71.90 | 313.60 | 2016 | 21） | 2446 | 21） | 4451 | 21） | 488 （ |  | 5461 | 18） | 6891 | 11） |
| 4136 | 140 | 71.90 | 314.00 | 7901 | 21） | 83336 | 17） |  |  | 4458 |  | 488 | 18） | 586 | 9） |
|  |  |  |  | 6320 | 15） | 7906 | 17） | 8336 | 21） | 445 |  | 488 | 18） | 5461 | 9） |
| 4137 | 146 | 71.90 | 314.40 | 2018 | 4） | 2446 | 21） | 2876 | 21） | 4886 | 21） | 6320 | 21） | 7758 | 16．） |
| 4138 | 134 | 71.90 | 314.80 | 2446 | 21） | 833 287 | 21） | 488！ | 21） | 6326 | 21） | 7750 | 19） | 7906 | 10） |
| 4139 | 150 | 71.90 | 315.20 | 83338 | 21） |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  | 7756 | 21） | 8331 | 21） | 8766 | 18） | 5746 | 5） | 6320 | 21） | 6756 | 2） |
| 4140 | 182 | 71.90 | 315.60 | 1876 | 7） | 2446 | 17） | 2876 | 21） | 4316 | 18） | 4885 | 6） | 5746 | 9） |
| 4141 | 168 | 71.90 | 316.00 | 6328 | 21） | 675 287 | 21） | 7756 4316 | 21） | 833 6328 | 21） | 8768 | 21） |  | 21） |
|  |  |  | 316.00 | 8338 | 21） | 8760 | 21） | 4316 |  |  |  | 675 ${ }^{\circ}$ | 21） | 775 | 21） |
| 4142 | 169 | 71.90 | 316.40 | 1876 | 21） | 2871 | 21） | 4310 | 21） | 6320 | 22） | 6751 | 21） | 7756 | 21） |
| 4143 | 167 | 71.90 | 316.80 | 8337 | 21） | 8768 | 21） | $431($ | 21） | 4740 | 4） |  |  |  |  |
|  |  |  |  | 675 | 21） | 7186 | 4） | 7751 | 21） | 8331 | 7） | 8768 | 21） |  |  |
| 4144 | 182 | 71.90 | 317.20 | $187($ | 21） | 2301 | 16） | 287 （ | 7） | 4311 | 21） | 4746 | 21） | 6171 | 19） |
| 4145 | 164 | 71.90 | 317.60 | 675 187 | 21） | 718 2306 | 21） | 7750 | 14） | 8768 4748 | 21） | 6171 | 19） | 675 | 21） |
|  |  |  |  | $718($ | 21） | 876 | 21） |  |  |  |  |  |  |  | 21） |


| BIN NUMBER | NUMBER PTS | LAT－LON | G SW Cor |  |  |  |  | REV（NUMBER PTS） |  |  |  |  |  |  |  |
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| 4088 | 5 | 71.80 | 334.79 | 14050 | 1） | 14916 | 4） |  |  |  |  |  |  |  |  |
| 4090 | 10 | 71.80 | 335.59 | 4446 | 4） | 12916 | 3） | 13776 | 3） |  |  |  |  |  |  |
| 4112 | 5 | 71.90 | 304.40 | 7760 | 5） |  |  | 1377 |  |  |  |  |  |  |  |
| 4113 | 3 | 71.90 | 304.80 | 2301 | 2） | 7768 | 1） |  |  |  |  |  |  |  |  |
| 4114 | 4 | 71.90 | 305.20 | 2736 | 1） | 7768 | 3） |  |  |  |  |  |  |  |  |
| 4115 | 1 | 71.90 | 305.60 | 2731 | 1） |  |  |  |  |  |  |  |  |  |  |
| 4119 | 1 | 71.90 | 307.20 | 2738 | 1） |  |  |  |  |  |  |  |  |  |  |
| 4121 | 19 | 71.90 | 308.00 | 2738 | 8） | 4176 | 4） | 5176 | 7） |  |  |  |  |  |  |
| 4122 | 16 | 71.90 | 308.40 308.80 | 1738 | 2） | 4608 | 2） | 10346 | 2） |  |  |  |  |  |  |
| 4124 | 38 | 71.90 | 309.20 | 1738 | $7)$ | 8176 | 12） | 4601 | 3） | 5600 | 7） | 6036 | 4） | 8045 | 9） |
| 4125 |  |  |  | 847 （ | 5） |  |  |  |  |  |  |  |  |  |  |
| 4125 | 38 | 71.90 | 309.60 | 1588 | 1） | 1736 | 3） | 2591 | 1） | 5036 | 1） | 6036 | 6） | 6468 | 5） |
| 4126 | 43 | 71.90 | 310.00 | 1588 | 4） | 4600 | 1） | 5036 | 1） | 6468 | 9） | 8046 | 17） | 8475 | 2 |
| 4127 | 53 | 71.90 | 310.40 | $\begin{array}{r}1034 \\ 158 \\ \hline\end{array}$ | 11） | 6461 | 3） |  |  |  |  |  |  |  |  |
|  |  |  |  | 11916 | 18） |  | 3） | 847 | 3） | 8906 | $6)$ | 10198 | 4） | 11486 | ） |
| 4128 | 85 | 71.90 | 310.80 | 158 （ | 15） | 4601 | 4） | 5036 | 2） | 6469 |  | 8476 | 5） | 8901 | $4)$ |
| 4129 |  |  |  | 10198 | 3） | 11488 | 18） | 11919 | 6） | 12346 | 17） |  |  |  |  |
| 4130 | 66 | 71.90 | 311.20 311.60 | 1586 | 6） | 6461 | 1） | 1019 | 1） | 1148 | 3） | 11916 | 1） | 12346 | 3） |
|  |  |  |  | 8471 | 20） | 8906 | 4） | 10198 | 6） | $1191($ |  | 12346 | 2） | 6896 |  |
| 4131 | 51 | 71.90 | 312.00 | 2598 | 10） | 6468 | 21） | 8476 | 20） |  |  |  |  |  |  |
| 4132 | 170 | 71.90 | 312.40 | 1586 | 18） | 2016 | 21） | $259($ | 21） | 4451 | 20） | 4886 | 7） | 5036 | 8） |
|  |  |  |  | 5468 | 9） | 6468 | 10） | 6891 | 11） | 7901 |  | 8901 | 17） | 10196 | 7） |
| 4133 | 177 | 71.90 | 312.80 | 12346 | 9） | 2016 | 19） | 2441 | 17） | 2591 | 7） | 445 | 20） | 488 C | 19） |
|  |  |  |  | 5466 | 17） | 6891 | 18） | 790 （ | 18） | 8901 | 17） | 10196 | 16） | 488 | 19） |
| 4134 | 120 | 71.90 | 313.20 | 12019 | 18） | 2446 | 21） | 445 | 21） | 4886 |  | 6891 | 19） | 7901 | 21） |
| 4135 | 136 | 71.90 | 313.60 | 2016 | 21） | 2446 | 21） | 4451 | 21） | 488 （ |  | 546 （ | 18） | 689 （ | 11） |
| 4136 | 140 | 71.90 | 314.00 | 7901 | 21） | 8336 | 2） |  |  |  |  |  |  |  |  |
|  |  |  |  | 6320 | 15） | 7906 | 17） | 8336 | 21） | 4456 | 16） | 4888 | 18） | 5461 | 9） |
| 4137 | 146 | 71.90 | 314.40 | 2015 | 4） | 2440 | 21） | 2876 | 21） | 488 C | 21） | 6326 | 21） | 7756 | 16．） |
| 4138 | 134 | 71.90 | 314.80 | 2440 | 21） | 88331 | 21） | 488！ | 21） | 6326 |  |  |  |  |  |
| 4139 | 150 |  |  | 8336 | 21） |  |  |  |  |  |  |  | 19） | 906 | 10） |
|  | 150 | 71.90 | 315.20 | 2448 | 21） | 2871 | 21） | 4886 | 20） | 5746 | 5） | 6326 | 21） | 6756 | 2） |
| 4140 | 182 | 71.90 | 315.60 | 1878 | 21） | 2446 | 17） |  | $18)$ |  |  |  |  |  |  |
|  |  |  |  | 6321 | 20） | 6751 | 21） | 7756 | 21） | 83318 | 18） | 4888 | 21） | 5746 | 9） |
| 4141 | 168 | 71.90 | 316.00 | 1876 | 21） | 2876 | 21） | 4316 | 21） | $632($ | 21） | 6756 | 21） | 775 | 21） |
| 4142 | 169 | 71.90 | 316.40 | 833 187 | 21） | 8761 | 21） | 4310 | 21） | 6320 | 22） | 675 | 21） | 775 | 21） |
| 4143 |  |  |  | 8336 | 21） | 8766 | 21） |  |  |  |  |  |  |  |  |
| 4143 | 167 | 71.90 | 316.80 | 1875 | 21） | 2878 | 21） | $431($ | 21） | 4746 | 4） | 6176 | 8） | 6326 | 18） |
| 4144 | 182 | 71.90 | 317.20 | 6757 | 21） | 718 | 16） | 7750 | 21） | 8331 | 21） | $876 \%$ 4740 | 21） | 6170 |  |
| 4145 | 164 |  |  | $675($ 187 | 21） | 7180 | 21） | 7751 | 14） | 8768 | 21） |  |  |  |  |
| 4145 | 164 | 71.90 | 317.60 | 7878 | 21） | 2306 | 21） | $431($ | 21） | 4746 | 19） | 617（ | 19） | 675（ | 21） |


| BIN NUMBER | NUMBER PTS | LAT－LON | G SW Cor |  |  |  |  | REV（NUMBER PTS） |  |  |  |  |  |  |  |
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| 4088 | 5 | 71.80 | 334.79 | 14050 | 1） | 14916 | 4） |  |  |  |  |  |  |  |  |
| 4090 | 10 | 71.80 | 335.59 | 4446 | 4） | 12916 | 3） | 13776 | 3） |  |  |  |  |  |  |
| 4112 | 5 | 71.90 | 304.40 | 7760 | 5） |  |  | 1377 |  |  |  |  |  |  |  |
| 4113 | 3 | 71.90 | 304.80 | 2301 | 2） | 7768 | 1） |  |  |  |  |  |  |  |  |
| 4114 | 4 | 71.90 | 305.20 | 2736 | 1） | 7768 | 3） |  |  |  |  |  |  |  |  |
| 4115 | 1 | 71.90 | 305.60 | 2731 | 1） |  |  |  |  |  |  |  |  |  |  |
| 4119 | 1 | 71.90 | 307.20 | 2738 | 1） |  |  |  |  |  |  |  |  |  |  |
| 4121 | 19 | 71.90 | 308.00 | 2738 | 8） | 4176 | 4） | 5176 | 7） |  |  |  |  |  |  |
| 4122 | 16 | 71.90 | 308.40 308.80 | 1738 | 2） | 4608 | 2） | 10346 | 2） |  |  |  |  |  |  |
| 4124 | 38 | 71.90 | 309.20 | 1738 | $7)$ | 8176 | 12） | 4601 | 3） | 5600 | 7） | 6036 | 4） | 8045 | 9） |
| 4125 |  |  |  | 847 （ | 5） |  |  |  |  |  |  |  |  |  |  |
| 4125 | 38 | 71.90 | 309.60 | 1588 | 1） | 1736 | 3） | 2591 | 1） | 5036 | 1） | 6036 | 6） | 6468 | 5） |
| 4126 | 43 | 71.90 | 310.00 | 1588 | 4） | 4600 | 1） | 5036 | 1） | 6468 | 9） | 8046 | 17） | 8475 | 2 |
| 4127 | 53 | 71.90 | 310.40 | $\begin{array}{r}1034 \\ 158 \\ \hline\end{array}$ | 11） | 6461 | 3） |  |  |  |  |  |  |  |  |
|  |  |  |  | 11916 | 18） |  | 3） | 847 | 3） | 8906 | $6)$ | 10198 | 4） | 11486 | ） |
| 4128 | 85 | 71.90 | 310.80 | 158 （ | 15） | 4601 | 4） | 5036 | 2） | 6469 |  | 8476 | 5） | 8901 | $4)$ |
| 4129 |  |  |  | 10198 | 3） | 11488 | 18） | 11919 | 6） | 12346 | 17） |  |  |  |  |
| 4130 | 66 | 71.90 | 311.20 311.60 | 1586 | 6） | 6461 | 1） | 1019 | 1） | 1148 | 3） | 11916 | 1） | 12346 | 3） |
|  |  |  |  | 8471 | 20） | 8906 | 4） | 10198 | 6） | $1191($ |  | 12346 | 2） | 6896 |  |
| 4131 | 51 | 71.90 | 312.00 | 2598 | 10） | 6468 | 21） | 8476 | 20） |  |  |  |  |  |  |
| 4132 | 170 | 71.90 | 312.40 | 1586 | 18） | 2016 | 21） | $259($ | 21） | 4451 | 20） | 4886 | 7） | 5036 | 8） |
|  |  |  |  | 5468 | 9） | 6468 | 10） | 6891 | 11） | 7901 |  | 8901 | 17） | 10196 | 7） |
| 4133 | 177 | 71.90 | 312.80 | 12346 | 9） | 2016 | 19） | 2441 | 17） | 2591 | 7） | 445 | 20） | 488 C | 19） |
|  |  |  |  | 5466 | 17） | 6891 | 18） | 790 （ | 18） | 8901 | 17） | 10196 | 16） | 488 | 19） |
| 4134 | 120 | 71.90 | 313.20 | 12019 | 18） | 2446 | 21） | 445 | 21） | 4886 |  | 6891 | 19） | 7901 | 21） |
| 4135 | 136 | 71.90 | 313.60 | 2016 | 21） | 2446 | 21） | 4451 | 21） | 488 （ |  | 546 （ | 18） | 689 （ | 11） |
| 4136 | 140 | 71.90 | 314.00 | 7901 | 21） | 8336 | 2） |  |  |  |  |  |  |  |  |
|  |  |  |  | 6320 | 15） | 7906 | 17） | 8336 | 21） | 4456 | 16） | 4888 | 18） | 5461 | 9） |
| 4137 | 146 | 71.90 | 314.40 | 2015 | 4） | 2440 | 21） | 2876 | 21） | 488 C | 21） | 6326 | 21） | 7756 | 16．） |
| 4138 | 134 | 71.90 | 314.80 | 2440 | 21） | 88331 | 21） | 488！ | 21） | 6326 |  |  |  |  |  |
| 4139 | 150 |  |  | 8336 | 21） |  |  |  |  |  |  |  | 19） | 906 | 10） |
|  | 150 | 71.90 | 315.20 | 2448 | 21） | 2871 | 21） | 4886 | 20） | 5746 | 5） | 6326 | 21） | 6756 | 2） |
| 4140 | 182 | 71.90 | 315.60 | 1878 | 21） | 2446 | 17） |  | $18)$ |  |  |  |  |  |  |
|  |  |  |  | 6321 | 20） | 6751 | 21） | 7756 | 21） | 83318 | 18） | 4888 | 21） | 5746 | 9） |
| 4141 | 168 | 71.90 | 316.00 | 1876 | 21） | 2876 | 21） | 4316 | 21） | $632($ | 21） | 6756 | 21） | 775 | 21） |
| 4142 | 169 | 71.90 | 316.40 | 833 187 | 21） | 8761 | 21） | 4310 | 21） | 6320 | 22） | 675 | 21） | 775 | 21） |
| 4143 |  |  |  | 8336 | 21） | 8766 | 21） |  |  |  |  |  |  |  |  |
| 4143 | 167 | 71.90 | 316.80 | 1875 | 21） | 2878 | 21） | $431($ | 21） | 4746 | 4） | 6176 | 8） | 6326 | 18） |
| 4144 | 182 | 71.90 | 317.20 | 6757 | 21） | 718 | 16） | 7750 | 21） | 8331 | 21） | $876 \%$ 4740 | 21） | 6170 |  |
| 4145 | 164 |  |  | $675($ 187 | 21） | 7180 | 21） | 7751 | 14） | 8768 | 21） |  |  |  |  |
| 4145 | 164 | 71.90 | 317.60 | 7878 | 21） | 2306 | 21） | $431($ | 21） | 4746 | 19） | 617（ | 19） | 675（ | 21） |


| BIN NUMBER | NUMBER PTS | LAT－LON | G SW Cor |  |  |  |  | REV（NUMBER PTS） |  |  |  |  |  |  |  |
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| 4088 | 5 | 71.80 | 334.79 | 14050 | 1） | 14916 | 4） |  |  |  |  |  |  |  |  |
| 4090 | 10 | 71.80 | 335.59 | 4446 | 4） | 12916 | 3） | 13776 | 3） |  |  |  |  |  |  |
| 4112 | 5 | 71.90 | 304.40 | 7760 | 5） |  |  | 1377 |  |  |  |  |  |  |  |
| 4113 | 3 | 71.90 | 304.80 | 2301 | 2） | 7768 | 1） |  |  |  |  |  |  |  |  |
| 4114 | 4 | 71.90 | 305.20 | 2736 | 1） | 7768 | 3） |  |  |  |  |  |  |  |  |
| 4115 | 1 | 71.90 | 305.60 | 2731 | 1） |  |  |  |  |  |  |  |  |  |  |
| 4119 | 1 | 71.90 | 307.20 | 2738 | 1） |  |  |  |  |  |  |  |  |  |  |
| 4121 | 19 | 71.90 | 308.00 | 2738 | 8） | 4176 | 4） | 5176 | 7） |  |  |  |  |  |  |
| 4122 | 16 | 71.90 | 308.40 308.80 | 1738 | 2） | 4608 | 2） | 10346 | 2） |  |  |  |  |  |  |
| 4124 | 38 | 71.90 | 309.20 | 1738 | $7)$ | 8176 | 12） | 4601 | 3） | 5600 | 7） | 6036 | 4） | 8045 | 9） |
| 4125 |  |  |  | 847 （ | 5） |  |  |  |  |  |  |  |  |  |  |
| 4125 | 38 | 71.90 | 309.60 | 1588 | 1） | 1736 | 3） | 2591 | 1） | 5036 | 1） | 6036 | 6） | 6468 | 5） |
| 4126 | 43 | 71.90 | 310.00 | 1588 | 4） | 4600 | 1） | 5036 | 1） | 6468 | 9） | 8046 | 17） | 8475 | 2 |
| 4127 | 53 | 71.90 | 310.40 | $\begin{array}{r}1034 \\ 158 \\ \hline\end{array}$ | 11） | 6461 | 3） |  |  |  |  |  |  |  |  |
|  |  |  |  | 11916 | 18） |  | 3） | 847 | 3） | 8906 | $6)$ | 10198 | 4） | 11486 | ） |
| 4128 | 85 | 71.90 | 310.80 | 158 （ | 15） | 4601 | 4） | 5036 | 2） | 6469 |  | 8476 | 5） | 8901 | $4)$ |
| 4129 |  |  |  | 10198 | 3） | 11488 | 18） | 11919 | 6） | 12346 | 17） |  |  |  |  |
| 4130 | 66 | 71.90 | 311.20 311.60 | 1586 | 6） | 6461 | 1） | 1019 | 1） | 1148 | 3） | 11916 | 1） | 12346 | 3） |
|  |  |  |  | 8471 | 20） | 8906 | 4） | 10198 | 6） | $1191($ |  | 12346 | 2） | 6896 |  |
| 4131 | 51 | 71.90 | 312.00 | 2598 | 10） | 6468 | 21） | 8476 | 20） |  |  |  |  |  |  |
| 4132 | 170 | 71.90 | 312.40 | 1586 | 18） | 2016 | 21） | $259($ | 21） | 4451 | 20） | 4886 | 7） | 5036 | 8） |
|  |  |  |  | 5468 | 9） | 6468 | 10） | 6891 | 11） | 7901 |  | 8901 | 17） | 10196 | 7） |
| 4133 | 177 | 71.90 | 312.80 | 12346 | 9） | 2016 | 19） | 2441 | 17） | 2591 | 7） | 445 | 20） | 488 C | 19） |
|  |  |  |  | 5466 | 17） | 6891 | 18） | 790 （ | 18） | 8901 | 17） | 10196 | 16） | 488 | 19） |
| 4134 | 120 | 71.90 | 313.20 | 12019 | 18） | 2446 | 21） | 445 | 21） | 4886 |  | 6891 | 19） | 7901 | 21） |
| 4135 | 136 | 71.90 | 313.60 | 2016 | 21） | 2446 | 21） | 4451 | 21） | 488 （ |  | 546 （ | 18） | 689 （ | 11） |
| 4136 | 140 | 71.90 | 314.00 | 7901 | 21） | 8336 | 2） |  |  |  |  |  |  |  |  |
|  |  |  |  | 6320 | 15） | 7906 | 17） | 8336 | 21） | 4456 | 16） | 4888 | 18） | 5461 | 9） |
| 4137 | 146 | 71.90 | 314.40 | 2015 | 4） | 2440 | 21） | 2876 | 21） | 488 C | 21） | 6326 | 21） | 7756 | 16．） |
| 4138 | 134 | 71.90 | 314.80 | 2440 | 21） | 88331 | 21） | 488！ | 21） | 6326 |  |  |  |  |  |
| 4139 | 150 |  |  | 8336 | 21） |  |  |  |  |  |  |  | 19） | 906 | 10） |
|  | 150 | 71.90 | 315.20 | 2448 | 21） | 2871 | 21） | 4886 | 20） | 5746 | 5） | 6326 | 21） | 6756 | 2） |
| 4140 | 182 | 71.90 | 315.60 | 1878 | 21） | 2446 | 17） |  | $18)$ |  |  |  |  |  |  |
|  |  |  |  | 6321 | 20） | 6751 | 21） | 7756 | 21） | 83318 | 18） | 4888 | 21） | 5746 | 9） |
| 4141 | 168 | 71.90 | 316.00 | 1876 | 21） | 2876 | 21） | 4316 | 21） | $632($ | 21） | 6756 | 21） | 775 | 21） |
| 4142 | 169 | 71.90 | 316.40 | 833 187 | 21） | 8761 | 21） | 4310 | 21） | 6320 | 22） | 675 | 21） | 775 | 21） |
| 4143 |  |  |  | 8336 | 21） | 8766 | 21） |  |  |  |  |  |  |  |  |
| 4143 | 167 | 71.90 | 316.80 | 1875 | 21） | 2878 | 21） | $431($ | 21） | 4746 | 4） | 6176 | 8） | 6326 | 18） |
| 4144 | 182 | 71.90 | 317.20 | 6757 | 21） | 718 | 16） | 7750 | 21） | 8331 | 21） | $876 \%$ 4740 | 21） | 6170 |  |
| 4145 | 164 |  |  | $675($ 187 | 21） | 7180 | 21） | 7751 | 14） | 8768 | 21） |  |  |  |  |
| 4145 | 164 | 71.90 | 317.60 | 7878 | 21） | 2306 | 21） | $431($ | 21） | 4746 | 19） | 617（ | 19） | 675（ | 21） |




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 $\approx ニ 26$ Table 6．Seasat Greenland Geographical Data Base（Cont．）

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$\left.\begin{array}{lll}1491( & 4\end{array}\right) \quad 1377(3)$

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| BIN NUMBER | NUMBER PTS | LAT－LON | G SW Cor |  |  |  |  | REV（NUMBER PTS） |  |  |  |  |  |  |  |
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| 4088 | 5 | 71.80 | 334.79 | 14050 | 1） | 14916 | 4） |  |  |  |  |  |  |  |  |
| 4090 | 10 | 71.80 | 335.59 | 4446 | 4） | 12916 | 3） | 13776 | 3） |  |  |  |  |  |  |
| 4112 | 5 | 71.90 | 304.40 | 7760 | 5） |  |  | 1377 |  |  |  |  |  |  |  |
| 4113 | 3 | 71.90 | 304.80 | 2301 | 2） | 7768 | 1） |  |  |  |  |  |  |  |  |
| 4114 | 4 | 71.90 | 305.20 | 2736 | 1） | 7768 | 3） |  |  |  |  |  |  |  |  |
| 4115 | 1 | 71.90 | 305.60 | 2731 | 1） |  |  |  |  |  |  |  |  |  |  |
| 4119 | 1 | 71.90 | 307.20 | 2738 | 1） |  |  |  |  |  |  |  |  |  |  |
| 4121 | 19 | 71.90 | 308.00 | 2738 | 8） | 4176 | 4） | 5176 | 7） |  |  |  |  |  |  |
| 4122 | 16 | 71.90 | 308.40 308.80 | 1738 | 2） | 4608 | 2） | 10346 | 2） |  |  |  |  |  |  |
| 4124 | 38 | 71.90 | 309.20 | 1738 | $7)$ | 8176 | 12） | 4601 | 3） | 5600 | 7） | 6036 | 4） | 8045 | 9） |
| 4125 |  |  |  | 847 （ | 5） |  |  |  |  |  |  |  |  |  |  |
| 4125 | 38 | 71.90 | 309.60 | 1588 | 1） | 1736 | 3） | 2591 | 1） | 5036 | 1） | 6036 | 6） | 6468 | 5） |
| 4126 | 43 | 71.90 | 310.00 | 1588 | 4） | 4600 | 1） | 5036 | 1） | 6468 | 9） | 8046 | 17） | 8475 | 2 |
| 4127 | 53 | 71.90 | 310.40 | $\begin{array}{r}1034 \\ 158 \\ \hline\end{array}$ | 11） | 6461 | 3） |  |  |  |  |  |  |  |  |
|  |  |  |  | 11916 | 18） |  | 3） | 847 | 3） | 8906 | $6)$ | 10198 | 4） | 11486 | ） |
| 4128 | 85 | 71.90 | 310.80 | 158 （ | 15） | 4601 | 4） | 5036 | 2） | 6469 |  | 8476 | 5） | 8901 | $4)$ |
| 4129 |  |  |  | 10198 | 3） | 11488 | 18） | 11919 | 6） | 12346 | 17） |  |  |  |  |
| 4130 | 66 | 71.90 | 311.20 311.60 | 1586 | 6） | 6461 | 1） | 1019 | 1） | 1148 | 3） | 11916 | 1） | 12346 | 3） |
|  |  |  |  | 8471 | 20） | 8906 | 4） | 10198 | 6） | $1191($ |  | 12346 | 2） | 6896 |  |
| 4131 | 51 | 71.90 | 312.00 | 2598 | 10） | 6468 | 21） | 8476 | 20） |  |  |  |  |  |  |
| 4132 | 170 | 71.90 | 312.40 | 1586 | 18） | 2016 | 21） | $259($ | 21） | 4451 | 20） | 4886 | 7） | 5036 | 8） |
|  |  |  |  | 5468 | 9） | 6468 | 10） | 6891 | 11） | 7901 |  | 8901 | 17） | 10196 | 7） |
| 4133 | 177 | 71.90 | 312.80 | 12346 | 9） | 2016 | 19） | 2441 | 17） | 2591 | 7） | 445 | 20） | 488 C | 19） |
|  |  |  |  | 5466 | 17） | 6891 | 18） | 790 （ | 18） | 8901 | 17） | 10196 | 16） | 488 | 19） |
| 4134 | 120 | 71.90 | 313.20 | 12019 | 18） | 2446 | 21） | 445 | 21） | 4886 |  | 6891 | 19） | 7901 | 21） |
| 4135 | 136 | 71.90 | 313.60 | 2016 | 21） | 2446 | 21） | 4451 | 21） | 488 （ |  | 546 （ | 18） | 689 （ | 11） |
| 4136 | 140 | 71.90 | 314.00 | 7901 | 21） | 8336 | 2） |  |  |  |  |  |  |  |  |
|  |  |  |  | 6320 | 15） | 7906 | 17） | 8336 | 21） | 4456 | 16） | 4888 | 18） | 5461 | 9） |
| 4137 | 146 | 71.90 | 314.40 | 2015 | 4） | 2440 | 21） | 2876 | 21） | 488 C | 21） | 6326 | 21） | 7756 | 16．） |
| 4138 | 134 | 71.90 | 314.80 | 2440 | 21） | 88331 | 21） | 488！ | 21） | 6326 |  |  |  |  |  |
| 4139 | 150 |  |  | 8336 | 21） |  |  |  |  |  |  |  | 19） | 906 | 10） |
|  | 150 | 71.90 | 315.20 | 2448 | 21） | 2871 | 21） | 4886 | 20） | 5746 | 5） | 6326 | 21） | 6756 | 2） |
| 4140 | 182 | 71.90 | 315.60 | 1878 | 21） | 2446 | 17） |  | $18)$ |  |  |  |  |  |  |
|  |  |  |  | 6321 | 20） | 6751 | 21） | 7756 | 21） | 83318 | 18） | 4888 | 21） | 5746 | 9） |
| 4141 | 168 | 71.90 | 316.00 | 1876 | 21） | 2876 | 21） | 4316 | 21） | $632($ | 21） | 6756 | 21） | 775 | 21） |
| 4142 | 169 | 71.90 | 316.40 | 833 187 | 21） | 8761 | 21） | 4310 | 21） | 6320 | 22） | 675 | 21） | 775 | 21） |
| 4143 |  |  |  | 8336 | 21） | 8766 | 21） |  |  |  |  |  |  |  |  |
| 4143 | 167 | 71.90 | 316.80 | 1875 | 21） | 2878 | 21） | $431($ | 21） | 4746 | 4） | 6176 | 8） | 6326 | 18） |
| 4144 | 182 | 71.90 | 317.20 | 6757 | 21） | 718 | 16） | 7750 | 21） | 8331 | 21） | $876 \%$ 4740 | 21） | 6170 |  |
| 4145 | 164 |  |  | $675($ 187 | 21） | 7180 | 21） | 7751 | 14） | 8768 | 21） |  |  |  |  |
| 4145 | 164 | 71.90 | 317.60 | 7878 | 21） | 2306 | 21） | $431($ | 21） | 4746 | 19） | 617（ | 19） | 675（ | 21） |

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Table 7. Seasat Geo-referenced Data Base Header Description


Table 7. Seasat Geo-referenced Data Base Header Description (Cont.)

| (477-480 Cont.) | Bits |  | Value |  |
| :---: | :---: | :---: | :---: | :--- |
|  |  |  | Description |  |
|  | 27 |  |  | Retracking correction applied |
|  | 28 | 0 |  | Retracking correction not applied |
|  |  | 1 |  | Center of gravity bias applied |
|  | 29 | 0 |  | Center of gravity bias not applied |
|  |  | 1 |  | Tropospheric correction applied |
|  | 30 | 0 |  | Tropospheric correction not applied |
|  |  | 0 |  | Ionospheric correction applied |
| Ionospheric correction not applied |  |  |  |  |
|  | 31 | 1 |  | Time bias applied |

Table 8. Seasat Geo-referenced Data Base Description

| GILE 2: | GEO-REFERENCED DATA BASE |
| :--- | :--- |
|  | Record Format: |
|  | Blocksize: |
|  | 19040 logical records correspond to one physical record |

Subgroup 1: One logical record for each bin containing data

| Bytes | FORTRAN <br> Variable <br> Type |
| :--- | :--- |
| I*4 | Description |
| $5-32$ | Indicates the number of logical records which follow which are <br> located in the bin |
| Unused |  |

Subgroup 2: One logical record for each data point in the bin

| Bytes | FORTRAN <br> Variable <br> Type | Description |
| :---: | :---: | :---: |
| $1-4$ | I*4 | North latitude of datum point in degrees ( $\times 10^{6}$ ) |
| 5-8 | I* 4 | East longitude of datum point in degrees ( $\times 10^{6}$ ) |
| 9-12 | I* 4 | Surface height relative to the ellipsoid in cm . |
| 13-16 | I* ${ }^{\text {4 }}$ | Height sigma, arbitrary value of 1.0 m used ( $\times 10^{5}$ ) |
| 17-18 | I*2 | Rev number |
| 19-20 | I*2 | Used for temporary flags when gridding the data |
| 21-24 | I*4 | Orbit adjustment in meters ( $\times 10^{5}$ ) (-999999999 if unavailable) |
| 25-28 | I*4 | RMS of orbit adjustment in meters ( $\mathrm{X} \mathrm{10}{ }^{5}$ ) (-999999999 if unavailable) |
| 29-32 | I* 4 | Slope correction in meters ( $\times 10^{5}$ ) (-999999999 if unavailable) |

NOTE: Subgroups 1 and 2 are repeated for as many bins with data.

Table 8. Seasat Geo-referenced Data Base Description (Cont.)

Subgroup 3: Directory

| Bytes | FORTRAN <br> Variable $\qquad$ | Description |
| :---: | :---: | :---: |
| 1-4 | I*4 | Record number at which data for bin 1 starts |
| 5-8 | I*4 | Record number at which data for bin 2 starts |
| 9-12 | I*4 | Record number at which data for bin 3 starts |
| 13-16 | I*4 | Record number at which data for bin 4 starts |
| 17-20 | I*4 | Record number at which data for bin 5 starts |
| 21-24 | I* 4 | Record number at which data for bin 6 starts |
| 25-28 | I*4 | Record number at which data for bin 7 starts |
| 29-32 | I* 4 | Record number at which data for bin 8 starts |

NOTE: The directory contains as many 32-byte logical records as necessary to designate the record locations of all bins.

| FILE 4: | ELEVATION GRID HEADER RECORD |
| :--- | :--- |
|  | Record Format: One logical record corresponds to one physical record |
|  | Blocksize: |
|  | 80 Bytes |


|  | FORTRAN <br> Variable |
| :--- | :--- |
| Bytes | Type |


| $1-4$ | $I * 4$ |
| :--- | :---: |
| $5-8$ | $I * 4$ |
| $9-12$ | $I * 4$ |
| $13-16$ | $I * 4$ |
| $17-20$ | $I * 4$ |
| $21-24$ |  |

Description
Number of latitude increments in the grid for a non-polar stereographic grid (140)

Number of longitude increments in the grid for a non-polar stereographic grid (152)

Starting north latitude of grid in degrees North ( $\times 10^{6}$ ) (this will be approximate for a polar stereographic grid) (50000000)

Starting east longitude of grid in degrees East ( $\times 10^{6}$ ) (this will be approximate for a polar stereographic grid) (300000000)

Ending north latitude of grid in degrees North ( $\times 10^{6}$ ) (this will be approximate for a polar stereographic grid) (73000000)

25-28 I*4
21-24 I*4

Ending east longitude of grid in degrees East ( $\times 10^{6}$ ) (this will be approximate for a polar stereographic grid) (340000000)

Status word for data used to generate grid. A zero in any bit position indicates that the correction is not applied.


Table 9. Elevation Grid Header Description (Cont.)

| Bytes | FORTRAN <br> Variable <br> Type | Description |
| :---: | :---: | :---: |
| 29-32 | I* 4 | Polar stereographic grid size conversion and scaling factor from <br>  (1650000) |
| 33-36 | I* 4 | The number of grids of desired size from the pole to the equator based on the grid size conversion and scaling factor ( $\mathrm{x} 10^{6}$ ) (608754894) |
| 37-40 | I* 4 | Latitude of the map perimeter in degrees North ( $\times 10^{6}$ ) (500000000) |
| 41-44 | I*4 | Greenwich orientation in degrees ( $\times 10^{6}$ ) (450000000) |
| 45-48 | I*4 | ```Polar stereographic switch (1) =0,grid has constant increment in latitude and longitude =1,grid is in polar stereographic projection``` |
| 49-52 | I* 4 | Number of I -axis divisions to the extent of the map perimeter (445) |
| 53-56 | I*4 | Number of $J$-axis divisions to the extent of the map perimeter (445) |
| 57-60 | I* 4 | $J$ coordinate of the projected pole (223) |
| 61-64 | I* 4 | I coordinate of the projected pole (223) |
| 65-68 | I* 4 | Minimum $J$ index of the grid (166) |
| 69-72 | I* 4 | Maximum $J$ index of the grid (317) |
| 73-76 | I*4 | Minimum I index of the grid (305) |
| 77-80 | I* 4 | Maximum I index of the grid (444) |

Table 10. Elevation Grid Description

| FILE 5: | ELEVATION GRID DATA RECORD |  |
| :---: | :---: | :---: |
|  | Record Format: Blocksize: | 10 logical records correspond to one physical record 1800 Bytes |
|  |  |  |
|  | Variable |  |
| Bytes | Type | Description |
| 1-4 | I* 4 | Condition number of the matrix used in the least-squares solution to the function ( $\times 10^{6}$ ) |
| 5-8 | I* 4 | Capsize in degrees latitude - radius from grid location defining area from which data was used to define grid ( $\times 10^{6}$ ) |
| 9-12 | I* 4 | North latitude of grid point in degrees ( $\times 10^{6}$ ) |
| 13-16 | I* 4 | East longitude of grid point in degrees ( $\times 10^{6}$ ) |
| 17-20 | I* 4 | Height values of the grid at location relative to sea level in meters ( $\times 10^{5}$ ) |
| 21-24 | I* 4 | Number of data values that were used to calculate grid value |
| 25-28 | I* 4 | Number of parameters used to define function, NPT, (equals 0 , 3, or 6) |
| 29-52 | I* 4 | Six gridding function coefficients. If NPT is $<6$ then the rest of the coefficients are initialized to zero. ( $\times 10^{5}$ ) |
| 53-76 | I* 4 | Set of null coefficients associated with any negligible singular values (sce SVD reference). If NPT is $<6$ then rest of coefficients are initialized to zero ( $\times 10^{6}$ ) |
| 77-80 | I*4 | Distance in km from grid locations to closest data point ( $\times 10^{6}$ ) |
| 81-84 | I*4 | North latitude of closest data point to grid location in degrees ( $\times 10^{6}$ ) |
| 85-88 | I* 4 | East longitude of closest data point to grid location in degrees ( $\times 10^{6}$ ) |
| 89-92 | I*4 | Height associated with closest data point to grid location in meters ( $\mathrm{x} 10^{5}$ ) |
| 93-96 | I*4 | Standard deviation of the data with respect to the gridding function in meters ( $\times 10^{6}$ ) |
| 97-180 | 1*4 | Correlation matrix from solution. This is a symmetrical $6 \times 6$ matrix so only the upper triangular portion is stored. The order of storage is elements $1-6$ are the first row elements, $7-11$ columns $2-6$ of second row etc. ( $\times 10^{5}$ ) |

NOTE: Ten of the above-mentioned 180-byte logical records make up one block of data.

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| 16. Abstract <br> The data processing methods and ice data products derived from Seasat radar altimeter measurements over the Greenland ice sheet and surrounding sea ice are documented in this first volume of a series. The corrections derived and applied to the Seasat radar altimeter data over ice are described in detail, including the editing and retracking algorithm to correct for height errors caused by lags in the automatic range tracking circuit. The methods for radial adjustment of the orbits and estimation of the slope-induced errors are given. The various levels of ice data sets are described in this report, but the user is referred to Volumes 2 (Greenland) and 4 (Antarctica) for more detailed descriptions of the gridded elevation data sets and the geo-referenced data bases. |  |  |
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