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Solar Radiation on Mars-Update 1990

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SOLAR RADIATION ON MARS

UPDATE 1990

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SUMMARY

Detailed information on solar radiation characteristics on Mars are necessary for effective design of future planned solar energy systems operating on the surface of Mars. In this paper we present a procedure and solar radiation related data from which the diurnally and daily variation of the global, direct beam and diffuse insolation on Mars are calculated. The radiation data are based on measured optical depth of the Martian atmosphere derived from images taken of the sun with a special diode on the Viking Lander cameras; and computation based on multiple wavelength and multiple scattering of the solar radiation. This work is an update to NASA TM-102299 and includes a refinement of the solar radiation model.

INTRODUCTION

Missions to the Martian surface will require electric power. Of the several possibilities, photovoltaic power systems can offer many advantages, including high power to weight, modularity, scalability, and a long history of successful application in space. To design a photovoltaic system, detailed information on solar radiation data on the Martian surface is necessary to allow more accurate estimates of photovoltaic power system size and mass in system analysis and trade-off studies of relevant technology options.

This report is an update to NASA TM-102299 (ref. 1) and to the paper (ref. 2) on "Solar Radiation on Mars." We present a procedure and solar radiation data from which the diurnally and daily variation of the global, direct beam and diffuse insolation are calculated. The calculation of these quantities became possible with the introduction of the "normalized net solar flux function" based on multiple wavelength and multiple scattering of the solar radiation. The solar radiation data presented in this report pertain again to the two Viking Lander locations VL1 (22.3° N, 47.9° W) and VL2 (47.7° N, 225.7° W). This update report include a refinement of the solar radiation model. The opacities at the two Viking Landers were updated, the net solar flux function was extended for albedo 0.4, and an analytical expression for the net solar flux function was formulated. In addition, the solar radiation calculations were extended to include the daylight hours and the daily insolation on a horizontal surface for a Martian year calculated for each 5° of areocentric longitudes.

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OPTICAL DEPTH

The most direct and probably most reliable estimates of opacity are those derived from Viking Lander imaging of the Sun. Figures 1 and 2 show the seasonal variation of the normal-incidence of the optical depth at the Viking Lander locations VL1 and VL2, respectively. The season is indicated by the value of L_s areocentric longitude of the Sun, measured in the orbital plane of the planet from its vernal equinox, $L_s = 0^\circ$. Figures 1 and 2 were derived from (ref. 3) and were discretized for each 5° (see measured and discretized). The optical depth is assumed to remain constant throughout the day. Opacities are minimum during the northern spring ($L_s = 0^\circ$ to 90°) and summer ($L_s = 90^\circ$ to 180°), and maximum during southern spring ($L_s = 180^\circ$ to 270°) and summer ($L_s = 270^\circ$ to 360°), the seasons during which most local and major dust storms occur. When dust storms are not present, the optical depth is typically about 0.5. Two global dust storms occurred during the periods of each observation as indicated by the high values of the optical depth of figures 1 and 2 in greater detail.

DUST STORMS

Observation from Earth, from orbit around Mars, and from the surface of the planet itself have shown that airborne dust is a highly variable and thermodynamically significant component of the Martian atmosphere. Martian dust plays a key role in determining the current climate of Mars, and is suspected of having a major influence on the evolution of the surface and the history of climatic conditions on the planet. Airborne dust may be transported over short or long distance depending upon regional meteorological conditions. Dust is raised from the surface into the atmosphere, and when certain conditions are met, it may be translated into local or global dust storms. The spacial distribution of dust storms and of changes in surface albedo suggest that dust can be removed from the surface almost anywhere on the planet. There may be long periods when little dust moves at all at some locations, while there appear to be other regions where dust is raised more frequently. Many of the parameters controlling the location, severity, and frequency of dust-raising activity are not well understood. The classical view is that dust storm activity is correlated with a general intensification of winds around the time of maximum insolation, near southern summer solstice and perihelion. Dust storms are distinguished as minor or major storms, the former being localized clouds that remain locally and dissipate in a few days or so. Major dust storms are also called "global" or "great" storms and are classified as regional or planet-encircling storms. Local storms appear to play an important role in initiating the global storms. The thermodynamics of local storm generation and the mechanisms by which local storms become planet-recircling storms remain obscure. During the planet-encircling dust storms, dust is raised and spread over much of the planet for many Martian days (sols), and eventually falls to the sur-The direction of the dust transport of these storms is that dust is face. moved about within the southern hemisphere or from the south to the north over several weeks. The atmospheric dust decreases the amount of insolation reaching the surface, increases the infrared atmosphere heat flux, and absorb radiation emitted by the surface. The intensity of the dust storms are defined in terms of the optical depth of the Martian atmosphere. From a photovoltaic system design point of view, the intensity, frequency, and duration of these

storms may be viewed as "partially cloudy" and "cloudy" days for which additional energy storage must be taken into account. The characteristics of the global and local dust storms are discussed in the following subsections.

Global Dust Storms

(Regional and Planet-Encircling Dust Storms)

The regional and planet-encircling dust storms are defined as:

Regional: regional in area, with the long axis of the affected area >2000 km, but did not encircle the planet.

Planet-encircling: area affected encircled the planet, usually in the east-west direction. Storm cover much of one or both hemisphere

Their characteristics are:

• One or more dust storms of regional or larger size can occur in any given Mars year. When they do occur, there is significant variation in their duration, areal extent and general opacity.

• There are many Mars years in which no planet-encircling dust storm has occurred; less frequently, there may be years in which not even regional storms occur.

• The relatively rare planet-encircling storms may have occurred more frequently during the last two decades (the period of spacecraft exploration of Mars!) than earlier in the century; these storms all occurred within 90° L_s of perihelion.

• The duration of these dust storms may vary from 35 to 70 days or more.

• The storms begin near perihelion, when solar radiation is maximum (southern spring and summer) in the southern mid-latitude.

• The first global dust storm observed by the Viking Landers (1977) spread from a latitude of 40° S to a latitude 48° N in about 5 to 6 days.

• The opacity of the atmosphere during the global dust storms is greater than 1.

Local Dust Storms

• Local dust storms occur at almost all latitudes and throughout the year. However, they have observed to occur most frequently in the approximate latitude belt 10° to 20° N and 20° to 40° S, with more dust clouds seen in the south than in the north, the majority of which occurred during southern spring.

• Based on Viking orbiter observations, it is estimated that approximately 100 local storms occur in a given Martian year.

• Local dust storms last a few days.

SURFACE ALBEDO

The albedo of a surface is a measure of the incident solar radiation reflected by the surface. The albedo behavior of Mars was measured by the Viking infrared thermal mapper (IRTM) instruments in the range of 0.3 to 3.0 µm (ref. 4). Global dust storms on Mars plays an important role in the deposition and removal of fine dust materials. The major variation in albedo were associated with the two global dust storms of 1977. During the seasons that are free of global dust storms, the observed albedo was reasonably uniform. Between the two storms, the atmosphere cleared substantially with many southern hemisphere regions returning to their prestorm albedos. The northern hemisphere atmosphere retained dust longer during the decay phase of the storms than the southern hemisphere. Southern hemisphere dark regions were not measurably brighter following the global storm suggesting little net deposition of dust (rate less than $0.15 \sim 1.5 \,\mu\text{m/year}$). In contrast, the northern hemisphere dark regions of Syrtis Major and Acidalia Planitia were measurably brighter following the storms, indicating a deposition of dust. These surfaces subsequently darkened over the following months returning to prestorm albedo values. Dust is also deposited in bright, low-inertia regions (at a rate a few to ~45 µm/year), where it remains. Remote sensing observations indicate that major dust deposits are currently located in three northern equatorial regions: Tharsis, Arabia and Elysium. They are covered by fine (~2 to 40 µm) bright (albedo >0.27) particles.

Considering solar collectors operation on the Martian surface in the context of dust deposition on the collectors and the change in the nearby surface albedo, we may take into account the following: the amount of solar radiation at perihelion and maximum wind velocities occur in the south causing storm initiation, whereas regional dust deposition occur in the north suggesting net transport of dust from south to north. In the south, very small amounts of dust are deposited, whereas in the north there are regional dust deposits remaining on the surface for a length of time (few months), and there are regions where the dust accumulate and remain.

SOLAR RADIATION AT THE TOP OF MARS ATMOSPHERE

The variation of the solar radiation at the top of the Mars atmosphere is governed by the location of Mars in its orbit and by the solar zenith angle. The solar radiation is direct beam radiation. The beam irradiance, in W/m^2 , is given by:

$$G_{ob} = \frac{S}{r^2}$$
(1)

55

where S is the solar constant at the mean Sun-Earth distance of 1 AU, i.e., $S = 1371 \text{ W/m}^2$; r is the instantaneous Sun-Mars distance in AU (heliocentric distance) given by (ref. 5):

$$r = \frac{a(1 - e^2)}{1 + e \cos \theta}$$
(2)

where a is the Mars semi-major axis in AU, and e is the Mars eccentricity, i.e., e = 0.093377; and θ is the true anomaly given by:

$$\Theta = L_{s} - 248^{\circ} \tag{3}$$

where L_s is the areocentric longitude and 248° is the areocentric longitude of Mars perihelion. The Sun-Mars mean distance in astronomical units (AU) is 1.5236915; therefore, the mean beam irradiance at the top of the Martian atmosphere is: $1371/1.5236915^2 = 590 \text{ W/m}^2$. The instantaneous beam irradiance is given by equations (1) to (3).

$$G_{ob} = 590 \frac{\left[1 + e \cos(L_s - 248)\right]^2}{(1 - e^2)^2}$$
(4)

and is shown in figure 5.

SOLAR RADIATION ON THE SURFACE OF MARS

The variation of the solar radiation on the Martian surface is governed by three factors: (1) the Mars-Sun distance, (2) solar zenith angle, and (3) the opacity of the Martian atmosphere. The global solar irradiance G is the sum of the direct beam irradiance G_b , the diffuse irradiance G_d , and the albedo G_{al} :

$$G = G_b + G_d + G_{al}$$
(5)

The direct beam irradiance on the Martian surface normal to the solar rays is related by Beer's law to the optical depth, τ , of the intervening atmospheric haze:

$$G_{h} = G_{oh} \exp[-\tau m(z)]$$
(6)

where m(z) is the air mass determined by the zenith angle z, and can be approximated, for zenith angles up to about 80°, by:

$$m(z) \cong \frac{1}{\cos z} \tag{7}$$

The zenith angle of the incident solar radiation is given by:

$$\cos z = \sin \phi \sin \delta + \cos \phi \cos \delta \cos \omega$$
 (8)

where

∮ latitude

δ declination angle

 ω hour angle measured from the true noon westward

The solar declination angle is given by:

where $\delta_0 = 24.936^\circ$ is the Mars obliquity of rotation axis. The variation of the solar declination angle is shown in figure 6. The four seasons pertain here to the northern hemisphere, the reverse is true in the southern hemisphere. The ratio of Mars to Earth length of day is 24.65/24. It is convenient, for calculation purposes, to define a Mars hour, H, by dividing the Martian day (sol) into 24 hr. Using the same relationship between the Mars solar time T and the hour angle as for the Earth, we write:

$$\omega = 15T - 180$$
 (10)

(9)

This is shown in figure 7. The final solar radiation results can then be adjusted by the above ratio to correspond to actual (terrestrial) time. The sunset hour angle is given by (ref. 6):

 $\omega_{ss} = \cos^{-1}(-\tan\phi\,\tan\,\delta) \tag{11}$

$$|\phi| < \pi/2 - |\delta|$$
 (12)

polar night: the Sun will neither rise nor set for the day

for $\phi < -\pi/2 + \delta$ or $\phi > \pi/2 + \delta$ (13)

polar day: the Sun will remain above the horizon all the day

for
$$\phi > \pi/2 - \delta$$
 or $\phi < \pi/2 - \delta$ (14)

The number of Mars daylight hours is given by:

$$T_{d} = \frac{2}{15} \cos^{-1}(-\tan \phi \tan \delta)$$
 (15)

The solar irradiance on a horizontal Martian surface $(G_{a1} = 0)$ is given by:

$$G_{h} = G_{bh} + G_{dh} \tag{16}$$

where:

 G_h global irradiance on a horizontal surface G_{bh} direct beam irradiance on a horizontal surface G_{dh} diffuse irradiance on a horizontal surface

The diffuse irradiance of the Martian atmosphere may be a result of a different mechanism than that for the Earth atmosphere, nevertheless, to a first approximation, we will apply equation (16) as for Earth-terrestrial calculations.

The global irradiance G_h on a horizontal surface is given by:

$$G_{h} = G_{ob} \cos z \frac{f(z,\tau,al)}{(1-al)}$$
(17)

where "al" is the albedo, and $f(z,\tau,al)$ is called the normalized net flux function. The net solar flux integrated over the solar spectrum on the Martian surface was calculated by Pollack (ref. 7) based on multiple wavelength and multiple scattering of the solar radiation. Derived data from this calculation are shown in tables I(a) and (b) for albedo = 0.1; and tables II(a) and (b) for albedo = 0.4. The parameters are the zenith angle z and the optical depth τ . For albedos between 0.1 and 0.4 a linear interpolation can be used. Figures 8 and 9 describe the variation of the normalized net flux function with optical depth and Sun zenith angle for 0.1 and 0.4 albedo, respectively, for some data in tables I and II. The normalized net flux function can be approximated by a polynomial expression given by:

$$f(z,\tau,al) = \left[\sum_{i=0}^{5} \sum_{j=0}^{5} \sum_{k=0}^{1} p(i,j,k) \cdot \tau^{i} \cdot \tilde{z}^{j} \cdot (al)^{k}\right] (1-al), \quad \tilde{z} = z/100$$

(18)

where p(i,j,k) are the coefficients of the polynomial given in table III. These coefficients were obtained from fitting equation (18) to the data in tables I and II based on the criteria of least square error. The mean error is about 0.7 percent for the full range. For zenith angles up to 40° the error is much smaller. The largest error is for zenith angle of 80° and 85° and for τ greater than 5. The maximum error is about 7 percent. At these large angles and opacities, the error has a minor effect on the calculated daily insolation.

Using equations (6) and (7), the beam irradiance G_{bh} on a horizontal surface is given by:

$$G_{bh} = G_{ob} \cos z \exp\left(\frac{-\tau}{\cos z}\right)$$
 (19)

and the diffuse irradiance is obtained by subtracting the beam from the global irradiances (eqs. (17) and (19)). Figures 10 to 12 describe the variation of the global, beam and diffuse irradiances, respectively, on a horizontal Martian surface; and are given in pairs as functions of the optical depth τ and zenith angle z. The irradiances were calculated based on table I data and the mean irradiance of 590 W/m². The variation of the global irradiance G_h, equation (17) is shown in figures 10(a) and (b). The beam irradiance G_{bh} is obtained using equation (19) and is shown in figures 11(a) and (b). The beam irradiance decrease with increasing of the optical depth, and a relative moderate decrease with increasing of the zenith angle. The diffuse irradiance shows a sliding maximum with the variation of the zenith angle.

The actual (terrestrial) number of daylight hours, hr, is obtained by multiplying equation (15) by the ratio 24.65/24. These are given in table IV for different latitudes ϕ and areocentric longitudes L_s , and are also shown in figures 13(a) and (b).

The solar radiation (global, beam and diffuse) variation (diurnally and daily) can be calculated based on the preceding equations and the $f(z,\tau,al)$ table data. For a given L_s and ϕ , one can calculate the variation of the zenith angle z as function of the Mars solar time T using equations (8) to (10). Referring to figures 3 and 4 for the given L_s , the optical depth τ is determined. With tables I and II and equations (16), (17) and (19) one can calculate the solar radiation variation for the given day. The diurnal variation of the solar irradiances for $L_s = 141^\circ$ and $L_s = 295^\circ$ for albedo = 0.1 and for Viking Lander location VL1 are shown in figures 14(a) and (b), respectively. Areocentric longitude $L_s = 141^\circ$ corresponds to the lowest opacity of 0.35, and $L_s = 291^\circ$ to the highest opacity of 3.6 (fig. 3). The figures show clearly that at high opacity, the diffuse component dominates the solar radiation. The daily global insolation H_h, beam isolation (global, beam and diffuse) isolation H_d can be calculated by integrating the irradiances over the period from sunrise to sunset. Table V gives the daily isolation (global, beam and diffuse) on a horizontal surface, in Whr/m²-day at VL1 and VL2 for albedo = 0.1 for 72 areocentric longitudes covering a Martian year. The variation of the daily global isolation of table V is shown in figure 15.

CONCLUSIONS

Effective design and utilization of solar energy depend to a large extent on adequate knowledge of solar radiation characteristics in the region of solar energy system operation. In this paper we presented a procedure and solar radiation related data from which the diurnally and daily variation of insolation on Mars were calculated. This includes the global, beam and diffuse insolation on a horizontal surface, from which any desired solar radiation quantity can be derived for an engineering design. The global insolation on the surface of Mars was derived based on the normalized net solar flux function $f(z,\tau,al)$; the beam insolation was determined by Beer's law relating the isolation to the optical depth of the Martian atmosphere; and the diffuse insolation. The optilated as the difference between the global and the beam insolation. The optical depths were measured at the two Viking lander locations, but can also be used, to the first approximation, for other locations.

Of major concern are the dust storms, which have been observed to occur on local as well as on global scales, and their effect on solar array output. In general, the assumption has been that global storms would reduce solar array output essentially to zero, because the opacity of the atmosphere may rise to values ranging from 3 to 9, depending on the severity of the storm. The two global dust storms that were observed in 1977 and the opacities measured by the two Viking Lander cameras, as seen in figures 3 and 4, may be considered as one of the worst years of dust activities on Mars. Even though, the opacities are relatively low during the northern spring and summer for more than a half Martian year or more than a terrestrial year (ref. 1) for which the insolation is relatively high varying from about 2 to 4 kWhr/m²-day. It should also be noted

that there are many Mars years in which no planet-encircling dust storm has occurred; less frequently, there may be years in which not even regional storms occur. One of the most important results of this study is that there is a large diffuse component of the solar insolation, even at high opacity, so that solar energy system operation is still possible.

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This report is an update to report NASA TM-102299 and includes a refinement of the solar radiation model. In particularly, the refinement pertains to the extension of the net solar flux function to albedo 0.4; the extension of this function to intermediate values of opacities; and the possibility of using the net solar flux function of albedo varying from 0.1 to 0.4.

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REFERENCES

- 1. Appelbaum, J.; and Flood, D.J.: Solar Radiation on Mars. NASA TM-102299, 1989.
- 2. Appelbaum, J.; and Flood, D.J.: Solar Radiation on Mars. Sol. Energy, vol. 45, no. 6, Nov. 9, 1990, pp. 353-363.
- 3. Colburn, D.S.; Pollack, J.B.; and Haberle, R.M.: Diurnal Variation in Optical Depth at Mars. ICARUS, vol. 79, May 1989, pp. 159-189.
- Christensen, P.R.: Global Albedo Variation on Mars: Implications for Active Aelion Transport, Deposition, and Erosion. J. Geophys. Res., vol. 93, no. B7, July 10, 1988, pp. 7611-7624.
- 5. Smith, E.V.P.; and Jacob, K.C.: Introductory Astronomy and Astrophysics. W.B. Saunders Co., 1973.
- 6. Duffie, J.A.; and Beckman, W.A.: Solar Engineering of Thermal Processes. Wiley, 1980.
- 7. Pollack, J.B., et al.: Simulation of the General Circulation of Martian Atmosphere I: Polar Processes. J. Geophys. Res., vol. 95, no. B2, Feb. 1990, pp. 1447-1473.

			ALBEI	0	0.1				
Optical			ZENT	PH ANGLE	5 7 (DEC	2)			
depth,			DDINT.			31			
τ	0.	5.	10.	15.	20.	25.	30.	35.	40.
.10	.883	.883	.883	.882	.881	.880	.879	.877	.875
.15	.875	.875	.874	.873	.872	.870	.868	.866	.862
.20	.866	.866	.865	.864	.862	.860	.857	.854	.850
.25	.857	.857	.856	.854	.852	.849	.846	.842	.838
.30	.848	.848	.847	.845	.842	.839	.835	.831	.826
.35	.839	.839	.838	.836	.833	.829	.824	.819	.813
.40	.830	.830	.829	.826	.823	.819	.814	.808	.801
.45	.822	.821	.820	.817	.814	.809	.804	.797	.790
.50	.813	.813	.811	.808	.804	.799	.793	.786	.778
.55	.005	.004	.002	.799	./95	. 789	. /83	.//5	./6/
. 00	. 190	. 795	.193	.790	./00	.//9	.112	./64	./55
70	778	- 700	. 704	.700	.115	./09	./02	./34	./4.3
75	770	768	766	762	.700	.759	- 752	./43	./32
.80	761	.760	757	753	748	741	732	.733	. / 2.1
.85	.752	.751	.748	.744	.739	.731	.722	.712	701
.90	.744	.743	.740	.736	.730	.722	.713	.703	. 690
.95	.736	.735	.732	.727	.721	.713	.703	. 693	. 680
1.00	.728	.727	.724	.719	.712	.704	.694	.683	.669
1.05	.720	.719	.716	.711	.704	.695	.685	.673	.659
1.10	.712	.711	.708	.703	.696	.687	.676	.664	.649
1.15	.704	.703	.700	.695	.688	.678	.667	.655	.640
1.20	.695	.694	.691	.686	.679	.669	.658	.645	.630
1.25	.687	.686	.683	.678	.670	.660	.649	.636	.621
1.30	.679	.678	.675	.670	.662	.652	.640	.627	.611
1.35	.672	.671	.668	.662	.654	.644	.632	.619	.602
1.40	.664	.663	.660	.654	.646	.636	.624	.611	.594
1 50	. 637	. 635	.652	.646	.638	.627	.615	.602	.585
1.50	649	. 648	.044	. 638	.630	.619	.607	.593	.576
1 60	631	.040	.03/	.031	.022	.612	.599	.585	.568
1 65	627	.035	.029	.025	.015	.004	.591	.5//	. 339
1.70	619	618	614	608	599	588	.505	.560	.551
1.75	.612	.611	.607	.601	592	581	568	.500	. 534
1.80	.605	.604	. 600	.594	.585	.574	.561	.546	.527
1.85	.598	597	.593	.587	.578	.567	.553	.538	.520
1.90	.591	.590	.586	.580	.571	.559	.546	.531	.513
1.95	.584	.583	.579	.573	.564	.552	.539	.524	.506
2.00	.578	.576	.572	.566	.557	.546	.532	.517	.498
2.10	.564	.563	.558	.552	.543	.532	.518	.502	.483
2.20	.551	.549	.545	.539	.530	.518	.504	.489	.469
2.30	.538	.537	.533	.526	.517	.505	.492	.476	.457
2.40	.526	.524	.520	.514	.505	.493	.479	.464	.444
2.50	.514	.512	.508	.502	.493	.481	.467	.451	.432
2.00	.501	.499	.496	.489	.480	.468	.454	.438	.420
2.70	.409	.40/	.483	.4//	.408	.456	.441	.426	.40/
2 90	467	.4//	.4/3	.400	.430	.445	.431	.415	.390
3.00	.457	456	452	445	.440	.435	.421	.405	.300
3.20	.436	.435	.431	.425	.416	405	.391	375	. 370 357
3.40	.415	.414	.410	404	.395	.384	.371	.356	. 33/
3.60	.395	.393	.389	.384	.376	.365	.352	.337	.319
3.80	.378	.376	.372	.367	.359	.349	.336	.321	.304
4.00	.363	.361	.357	.352	.344	.334	.321	.307	.290
4.50	.325	.323	.320	.315	.307	.297	.286	.272	.257
5.00	.289	.288	.285	.280	.273	.264	.253	.241	.227
5.50	.257	.256	.253	.249	.242	.234	.225	.213	.201
6.00	.229	.227	.224	.220	.215	.209	.200	.189	.178

TABLE I(a). - NORMALIZED NET FLUX FUNCTION $f(z,\tau,al)$ AT THE MARTIAN SURFACE.

			ALBEI	00	0.3	1			
Optical depth.			ZENI	TH ANGLI	EZ(DE	G)			
τ.	45.	50.	55.	60.	65.	70.	75.	80.	85.
.10	.872	.868	.862	.855	.844	.830	.804	.757	.640
.15	.858	.852	.844	.834	.819	.798	.762	.700	.566
.20	.844	.836	.826	.813	.794	.768	.724	.651	.508
.25	.831	.821	.808	.793	.770	.739	.688	.608	.466
.30	804	.000	.791	754	. /4/	687	.030	.571	433
.40	.790	.776	.758	.736	.706	. 663	.599	.510	.385
.45	.778	.762	.742	.718	.686	.641	.575	.485	.367
.50	.765	.748	.727	.701	.667	.619	.551	.462	.351
.55	.753	.734	.712	.684	.648	.598	.528	.440	.337
.60	.741	.721	.697	.668	.631	.579	.508	.422	.325
.65	.728	.708	.683	.653	.615	.562	.491	.407	.315
.70	705	.093	.009	.030	.000	.540	.4/4	. 393	.300
80	693	670	.055	.023	.505	514	437	366	288
.85	.682	.658	.630	.596	.556	.500	. 429	.356	.281
.90	.671	.646	.617	.583	.543	.486	.416	.345	.274
.95	.660	.634	.605	.570	.528	.472	.403	.335	.267
1.00	.649	.623	.593	.557	.514	.459	.392	.324	.261
1.05	.638	.613	.582	.546	.503	.448	.382	.316	.255
1.10	.628	.602	.5/1	.535	.492	.438	.3/4	309	.250
1 20	608	581	550	513	460	416	355	295	240
1.25	.598	.570	.539	.502	.457	.405	.346	.287	.235
1.30	.588	.560	.528	.491	.446	.395	.337	.280	.230
1.35	.579	.551	.519	.482	.437	.387	.331	.275	.226
1.40	.571	.542	.510	.473	.429	.379	.324	.270	.222
1.45	.562	.533	.501	.464	.420	.372	.318	.265	.219
1.50	.553	.524	.492	.455	.412	.364	.312	.260	.215
1.55	. 344	506	.483	.440	.403	348	298	.255	207
1.65	.527	. 497	.465	.428	.385	.340	.292	.244	.203
1.70	.518	.489	.457	.420	.378	.333	.286	.240	.200
1.75	.511	.482	.450	.413	.371	.327	.281	.236	.197
1.80	.504	.475	.443	.406	.364	.321	.276	.232	.194
1.85	.496	.468	.436	.399	.358	.316	.272	.228	.191
1.90	.489	.460	.428	. 392	.352	. 310	.267	.225	.188
2 00	.402 171	455	413	.305	. 343	298	.202	217	182
2.10	.459	.431	.399	.364	.325	.287	.248	.210	.176
2.20	.446	.417	.386	.352	.314	.276	.239	.203	.170
2.30	.433	.405	.374	.341	.304	.268	.232	.197	.166
2.40	.421	.393	.362	.330	.295	.260	.226	.192	.161
2.50	.409	.381	.351	.319	.285	.252	.219	.187	.157
2.60	.396	.369	.339	.308	.276	.243	.212	.181	.153
2.70	.384	.35/	.328	.298	.200	.235	.205	.170	140
2 90	363	. 347	310	281	.250	.220	193	.166	.140
3.00	.354	.329	.301	.273	.244	.216	.188	.162	.137
3.20	.336	.311	.285	.258	.231	.205	.179	.154	.131
3.40	.317	.294	.268	.243	.218	.193	.169	.146	.124
3.60	.299	.277	.253	.230	.206	.182	.160	.138	.117
3.80	.284	.263	.241	.218	.196	.174	.153	.132	.112
4.00	240	.251	.229	.208	.187	.100 170	.140	.12/	.101
5.00	·270	1:06	170	162	146	131	.116	.101	086
5.50	.187	.173	.158	.143	.130	.116	.103	.090	.077

TABLE I(b). - NORMALIZED NET FLUX FUNCTION $f(z,\tau,al)$ AT THE MARTIAN SURFACE.

		····.	ALBED	0	0.4				
Optical									·····
depth,			ZENIT	H ANGLE	Z (DEG	i)			
τ	0.	5.	10.	15.	20.	25.	30.	35.	40.
.10	.596	.595	. 594	.593	.592	.591	.590	.589	.588
.15	.592	.590	.590	.589	.588	.586	.585	.583	.582
.20	597	.586	.585	.584	.583	.581	.579	.577	.575
.30	.578	. 502	576	575	.573	.570	.574	565	562
.35	.574	.573	.572	.570	.568	.565	.563	.559	.556
.40	.569	.568	.567	.565	.563	.560	.557	.553	.549
.45	.565	.564	.563	.560	.558	.555	.552	.547	.542
.50	.560	.559	.558	.556	.553	. 550	.546	.541	.535
.55	.555	.555	.553	.551	.548	.544	.540	.535	.529
.00	545	549	. 540	.540	. 343	. 539	.534	.529	. 322
.70	.540	.540	.538	.536	.532	.535	.522	.51.6	.509
.75	.535	.535	.533	.531	.527	.522	.516	.510	.503
.80	.531	.530	.528	.526	.522	.517	.511	.504	.496
.85	1.526	.525	.523	.520	.517	.511	.505	.498	.490
.90	.521	.520	.518	.515	.511	.505	.499	.492	.483
.95	511	.515	. 314 500	506	.306 501	.500	.494 199	.486 190	.4/6
1.05	.506	.506	.503	.500	.496	.495	. 482	.400	.464
1.10	.501	.501	.499	.495	.490	.483	.476	.468	.458
1.15	. 497	.496	.494	.490	.485	.478	.471	.462	.452
1.20	.492	.491	.489	.485	.480	.473	.465	.456	.446
1.25	.487	.486	.484	.480	.475	.467	.460	.450	.439
1 35	482	.481	.4/9	.4/5	.469	.462	.454	.445	.433
1.40	.472	.471	.469	.465	.459	.452	.449	.434	. 422
1.45	.467	.467	.465	.460	.455	.447	.438	.429	.417
1.50	.463	.462	.460	.456	.450	.442	.433	.423	.411
1.55	.458	.457	.455	.451	.445	.437	.428	.418	.406
1.60	.453	.452	.450	.446	.440	.432	.423	.413	.400
1 70	.449	.448	.445	.441	.435	.427	.418	.407	.395
1.75	.440	.438	.435	.430	425	418	408	397	384
1.80	.435	.434	.431	.427	.421	.413	.403	.392	.379
1.85	.431	.429	.427	.422	.416	.408	.398	.388	.375
1.90	.426	.425	.422	.417	.411	.403	.394	.383	.370
1.95	.422	.420	.418	.413	.406	.398	.389	.378	.365
2.00	417	.410	.413	.408	.402	.394	.384	.373	.360
2.20	.399	.398	.395	.391	.384	.376	.366	.355	.341
2.30	.391	.390	.387	.382	.376	.368	.358	.346	.332
2.40	.383	.382	.379	.374	.368	.359	.349	.338	.324
2.50	.375	.374	.371	.367	.360	.351	.341	.330	.316
2.60	.367	.365	.363	.358	.352	.343	.333	.321	.308
2.70	358	.35/	354	.350	.343	.334	. 324	.313	.299
2.90	.343	342	. 340	. 342 334	328	.320	310	298	284
3.00	.336	.335	.332	.327	.321	.313	.303	.291	.277
3.20	. 322	.321	.318	.314	.307	.299	.289	.277	.264
3.40	.308	.307	.304	.300	.293	.285	.275	.264	.251
3.60	.294	.293	.290	.286	.280	.271	.262	.251	.238
3.80	202	.281	.278	.2/4	.268	.260	.251	.239	.227
4.50	.244	.243	.207	.203	.237	. 2.249	.240	.229	.217
5.00	.219	.218	.216	.212	.207	.200	.192	.183	.173
5.50	.196	.196	.194	.190	.185	.179	.172	.163	.154
6.00	1.176	.175	.173	.170	.166	.161	.154	.146	.137

TABLE II(a). - NORMALIZED NET FLUX FUNCTION $f(z,\tau,al)$ AT THE MARTIAN SURFACE.

<u> </u>			ALBED	0	0.4	4			
Optical			ZENIT	H ANGLE	Z (DEC	G)			
τ	45	50	55	60	65	70	75	80	85
.10	.586	.583	.579	.575	.568	. 558	.540	.509	430
.15	.579	.575	.569	.563	.553	.539	.514	.473	.382
.20	.571	.566	.559	.551	.538	.520	.490	.441	.344
.25	.564	.558	.549	.539	. 524	.502	.467	.413	.316
.30	.557	.549	.539	.527	.509	.485	.447	.389	.295
.35	.549	.541	.529	.515	.496	.469	.428	.368	.278
.40	.542	.532	.519	.504	.483	.454	.411	.350	.264
.45	.534	.524	.510	.494	.471	.440	.394	.333	.252
	510	.515	. 501	.403	.439	.420	.3/9	304	233
.55	512	498	482	462	.440	401	.303	292	225
. 65	.505	. 490	.402	452	427	390	340	282	219
.70	.498	.483	.465	.443	.417	.379	.329	.273	.213
.75	.491	.475	.456	.434	.407	.368	.318	.264	.207
.80	.483	.467	.448	.425	.397	.358	.308	.256	.202
.85	.476	.459	.440	.416	.389	.349	.300	.249	.198
.90	.470	.452	.432	.408	.380	.341	.292	.242	.193
.95	.463	.445	.424	.400	.371	.332	.283	.235	.189
1.00	.456	.438	.417	.392	.362	.323	.276	.228	.184
1.05	.450	.431	.410	. 384	.354	.316	.270	.223	.180
1.10 1 15	.443	.424	.402	.3//	.34/	.309	.204	.219	174
1 20	431	411	389	363	. 3 3 3	295	.250	209	171
1.25	.424	. 404	.382	.356	.324	.288	.232	.204	167
1.30	.417	.398	.376	.349	.317	.281	.240	.200	.164
1.35	.412	. 392	.370	.343	.311	.276	.236	.197	.162
1.40	.406	.386	.363	.337	.306	.271	.232	.193	.159
1.45	.400	.380	.357	.331	.300	.265	.227	.190	.157
1.50	.395	.374	.351	.325	.294	.260	.223	.186	.154
1.55	.389	.368	.346	.319	.288	.255	.219	.183	.152
1.60	.384	.363	.340	.313	.283	.250	.215	.180	.149
1.05	.3/8	.35/	.334	.307	.211	.245	.211	.170	.14/
1.70	.312	.332	.329	. 302	.212	.240	.200	171	144
1.80	363	342	319	292	263	232	200	168	140
1.85	.358	.337	.314	.287	.258	.228	.197	.166	.138
1.90	.353	.332	.309	.283	.254	.224	.193	.163	.136
1.95	.348	.327	.304	.278	.250	.220	.190	.161	.134
2.00	.343	.322	.299	.273	.245	.217	.187	.158	.133
2.10	.333	.312	.289	.264	.237	.209	.181	.153	.129
2.20	.323	.303	.281	.256	.229	.202	.175	.149	.126
2.30	.315	.295	.273	.248	.222	.196	.170	.145	.122
2.40	.307	.28/	.265	.241	.216	.191	.166	.142	.119
2.50	.299	.279	.257	.434	.209	.100	156	124	.110
2 70	283	263	249	220	197	174	151	130	110
2.80	275	255	234	213	101	169	147	127	107
2.90	.268	.249	.228	.207	.186	.165	.144	.124	.104
3.00	.261	.243	.223	.202	.182	.161	.141	.121	.102
3.20	.249	.231	.211	.192	.172	.153	.134	.115	.097
3.40	.235	.218	.200	.181	.163	.145	.127	.110	.093
3.60	.223	.207	.189	.171	.154	.137	.121	.104	.089
3.80	.213	.197	.181	.164	.147	.131	.115	.100	.086
4.00	.204	.189	.173	.157	.141	.125	.110	.096	.082
4.50	161	.168	.154	.140	.126	.112	.099	.087	.0/4
5.00	.101 117	.149 132	.130 191	.124	100	. 101	.090	.070	.000 050
6,00	.128	.110	100		.100	.091 001	.000	.010	054
					.090	.001	.012	.005	.034

		•									
TABLE	II(b).	-	NORMALIZED	NET	FLUX	FUNCTION	$f(z,\tau,al)$	AT	THE	MARTIAN	SURFACE.

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			k =	= 0		94 1
j	0	1	2	3	4	5
0 1 2 3 4 5	1.002800 450073 5.566705 -22.471579 36.334497 -20.420490	228681 1.335955 -16.912405 64.909973 -101.800319 53.207148	.019613 -1.131691 13.739701 -52.509470 79.895539 -39.949537	.000231 .402126 -4.756079 17.997548 -26.762885 12.977108	000130 063967 .743740 -2.786548 4.074117 -1.931169	.000003 .003758 043159 .160340 231476 .107837
	•		k :	= 1		
j	0	1	2	3	4	5
0 1 2 3 4 5	.009814 156701 1.361122 -4.365924 5.991693 -2.915099	.226139 .396821 -3.758111 12.539251 -17.498138 8.275686	117733 313648 3.007907 -10.394165 14.291370 -6.593125	.030579 .099227 987457 3.486452 -4.765323 2.173999	004090 013508 .141693 513123 .703675 320308	.000218 .000651 007320 .027401 037960 .017335

TABLE III. - NORMALIZED NET FLUX FUNCTION COEFFICIENTS, $f(z,\tau,al)$

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			Latitu	ıde .Ø	, DEG.				Ls
0	10	20	30	40	50	60	70	80	
12.32	12.32	12.32	12.32	12.32	12.32	12.32	12.32	12.32	0
12.32	12.38	12.43	12.49	12.57	12.67	12.83	13.12	13.97 15.69	10
12.32	12.48	12.64	12.82	13.05	13.35	13.83	14.73	17.60	15
12.32	12.53	12.74	12.99	13.29	13.69	14.33	15.56	19.96	20
12.32	12.58	12.04	13.30	13.52	14.03	14.83	17.30	24.65	30
12.32	12.67	13.04	13.46	13.98	14.69	15.83	18.24	24.65	35
12.32	12.71	13.13	13.61	14.20	15.01	16.32	19.26	24.65	40
12.32	12.80	13.30	13.88	14.60	15.61	17.29	21.86	24.65	50
12.32	12.83	13.38	14.00	14.79	15.89	17.75	24.65	24.65	55
12.32	12.87	13.45	14.12	14.96	16.14	18.18	24.65	24.65	60
12.32	12.92	13.56	14.30	15.23	16.56	18.95	24.65	24.65	70
12.32	12.94	13.60	14.37	15.33	16.72	19.25	24.65	24.65	75
12.32	12.98	13.65	14.42	15.41	16.84	19.48	24.65	24.65	80
12.32	12.97	13.66	14.46	15.47	16.93	19.67	24.65	24.65	90
12.32	12.97	13.65	14.45	15.45	16.91	19.62	24.65	24.65	95
12.32	12.96	13.63	14.42	15.41	16.72	19.48	24.65	24.65	100
12.32	12.92	13.56	14.30	15.23	16.56	18.95	24.65	24.65	110
12.32	12.90	13.51	14.22	15.11	16.37	18.59	24.65	24.65	115
12.32	12.83	13.38	14.12	14.90	15.89	17.75	24.65	24.65	120
12.32	12.80	13.30	13.88	14.60	15.61	17.29	21.86	24.65	130
12.32	12.76	13.22	13.75	14.41 14.20	15.32	16.81	20.42	24.65	135
12.32	12.67	13.04	13.46	13.98	14.69	15.83	18.24	24.65	140
12.32	12.62	12.94	13.30	13.75	14.36	15.33	17.30	24.65	150
12.32	12.58	12.84	13.15	13.52	14.03	14.83	16.41	24.65	155
12.32	12.48	12.64	12.82	13.05	13.35	13.83	14.73	17.60	165
12.32	12.43	12.53	12.66	12.81	13.01	13.33	13.92	15.69	170
12.32 12.32	12.38	12.43	12.49	12.57	12.67	12.83	13.12	13.97	175
12.32	12.27	12.22	12.16	12.08	11.98	11.82	11.53	10.68	185
12.32	12.22	12.12	11.99	11.84	11.64	11.32	10.73	8.96	190
12.32	12.12	11.91	11.66	11.36	10.96	10.82	9.92	4.69	200
12.32	12.07	11.81	11.50	i1.13	10.62	9.82	8.24	0.00	205
12.32	12.03	11.71	11.35	10.90	10.29	9.32	7.35	0.00	210
12.32	11.94	11.52	11.04	10.45	9.64	8.33	5.39	0.00	215
12.32	11.89	11.43	10.90	10.24	9.33	7.84	4.23	0.00	225
12.32	11.85	11.35	10.77	10.05	9.04	7.36	2.79	0.00	230
12.32	11.78	11.20	10.65	9.60	8.51	6.47	0.00	0.00	235
12.32	11.75	11.14	10.43	9.54	8.28	6.06	0.00	0.00	245
12.32	11.73	11.09	10.35	9.42	8.09	5.70	0.00	0.00	250
12.32	11.69	11.05	10.28	9.24	7.93	5.40	0.00	0.00	255
12.32	11.68	11.00	10.20	9.20	7.74	5.03	0.00	0.00	265
12.32	11.68	10.99	10.19	9.18	7.72	4.98	0.00	0.00	270
12.32	11.69	11.00	10.23	9.24	7.81	5.03	0.00	0.00	275
12.32	11.71	11.05	10.28	9.32	7.93	5.40	0.00	0.00	285
12.32	11.73	11.09	10.35	9.42	8.09	5.70	0.00	0.00	290
12.32	11.78	11.20	10.53	9.69	8.51	6.47	0.00	0.00	300
12.32	11.82	11.27	10.65	9.86	8.76	6.90	0.00	0.00	305
12.32	11.85	11.35	10.77	10.05	9.04	7.36	2.79	0.00	310
12.32	11.94	11.52	11.04	10.45	9.64	8.33	5.39	0.00	320
12.32	11.98	11.61	11.19	10.67	9.96	8.82	6.41	0.00	325
12.32	12.03	11.81	11.35	11.13	10.29	9.32	7.35	0.00	330
12.32	12.12	11.91	11.66	11.36	10.96	10.32	9.09	4.69	340
12.32	12.17	12.01	11.83	11.60	11.30	10.82	9.92	7.05	345
12.32	12.27	12.22	12.16	12.08	11.98	11.82	10.73 11.53	10.68	350

TABLE IV. - DAYLIGHT HOURS (TERRESTRIAL), hr

VL1VL2L3HbhHbhHbhHbhHbhHbhHbh1175,181829,133004,311003,721313,66,362217,4151452,331731,733184,061286,081244,762250,84101786,251581,393356,64195,051502,532417,58151695,961641,463337,441244,441442,632296,77201712,241586,633456,15191,201551,343182,24351895,921186,633456,15191,201354,643454,441751,511649,75340,261973,321403,803377,12451650,851776,0683356,632192,211355,64255551292,14187,24316,582096,701451,563548,26551292,14160,8903357,432199,931494,513694,444651292,12160,8903351,632192,311415,46392,166752032,76156,3782405,3911416,461599,16599901715,04156,223518,632255,491465,16399,165991715,041562,733465,722202,521657,333885,681002243,761529,543465,722203,261657,333885,68100243,77173,563773,422212,301673,383885,68100244,751529,543465,72239,17 <th>TABLE</th> <th>V.</th> <th>- DAILY</th> <th>INSOLATION</th> <th>ON</th> <th>A HORIZO</th> <th>NTAL SURF</th> <th>ACE • Whr/m²</th> <th>-day</th>	TABLE	V.	- DAILY	INSOLATION	ON	A HORIZO	NTAL SURF	ACE • Whr/m ²	-day
Hoh Hoh <th></th> <th></th> <th>VL1</th> <th></th> <th></th> <th></th> <th>VL2</th> <th></th> <th>Ls</th>			VL1				VL2		Ls
	Hbh		Hdh	Hh ZOZE de		Hbh	Hdh	Hh 2012 80	0
	1175.18		1829.13	3004.31		1003.72	1313.69	2317.41	5
$\begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	1452.33		1731.73	3184.06		1286.08	1264.76	2550.84	10
	1788.25		1581.39	3369.64		915.05	1502.53	2417.58	15
	1695.98		1641.46	3337.44		1244.84	1442.63	2687.47	20
	1050 02		151916	3355.04 3479.08		1292.28	1565.45	2857 73	30
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1849:52		1586.63	3436.15		1831.20	1351.34	3182.54	35
$\begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	2110.70		1445.85	3556.55		2053.60	1292.21	3345.81	40
	1751.51		1649.75	3401.26		1973.32	1403.80	3377.12	45
	1205 14		1871.24	3350.93		2096 70	1451 56	3548.26	55
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	1659.76		1713.43	3373.19		2150.92	1473.70	3624.62	60
$\begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	1771.34		1664.09	3435,43		2199.93	1494.51	3694.44	65
2023.40 1547.00 3502.50 2449.40 1622.50 3502.10 152 2043.77 1563.78 3507.55 2505.26 1455.29 3960.35 85 1812.62 1705.22 3518.84 2525.49 1466.16 3991.65 90 1715.04 1774.32 3489.36 2538.91 1474.84 4013.75 95 2263.29 1542.23 3605.72 2202.52 1684.39 3885.68 100 2264.39 1542.23 3605.72 2202.52 1684.70 1388.22 110 2562.36 1337.54 4303.09 2851.03 1239.17 4090.20 125 2662.26 1399.10 4061.36 2406.42 1238.12 3807.12 130 2662.26 1339.12 3807.55 4001.66 2462.68 1338.12 3807.12 143 271.10 153.55 1867.02 327.72 373.39 1307.72 3454.51 155 1958.75 1867.03 3227.90 2243.	1892.12		1608.90	3501.02		2409.39	1416.41	3825.80	70 75
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	2023.40		1547.06	3587.63		2154.31	1629.51	3783.82	80
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	2043.77		1563.78	3607.55		2505.26	1455.29	3960.55	85
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	1812.62		1706.22	3518.84		2525.49	1466.16	3991.65	90
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	1715.04		1774.32	3489.36		2538.91	14/4.84	4013.75	95
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	2243.87		1529.54	3773 41		2212.30	1684.39	3896.77	105
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	2263.49		1542.23	3805.72		2202.52	1685.70	3888.22	110
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	2599.01		1363.67	3962.68		2709.67	1375.86	4085.53	115
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	2621.38		1375.47	3996.85		3113.77	1096.27	4210.04	120
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	2642.75		1399.10	4050.09		2804.24	1232.88	4037.12	130
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	2679.02		1410.56	4089.58		2968.84	1081.02	4049.86	135
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	2875.66		1305.02	4180.68		2482.68	1338.12	3820.80	140
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	2371.10		1630.56	4001.66		2606.58	1200.54	3807.12	145
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	1956.75		1874.57	3827.90		2243.35	1288.70	3532.05	155
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	1822.25		1939.20	3761.45		2329.90	1151.06	3480.96	160
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1805.09		1941.22	3746.31		1867.13	1338.66	3205.79	165
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	1670.50		1991.87	3662.37		972 12	1306.78	2554.85	175
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	1610.08		1991.49	3601.57		524.38	1604.87	2129.25	180
835.21 2173.37 3008.58 487.57 1431.94 1919.51 190 913.36 2124.48 3037.84 515.82 1338.23 1854.05 195 1000.00 2063.58 3063.58 362.79 1257.98 1620.77 200 278.97 1954.24 2233.21 85.85 1048.88 1134.73 205 114.93 1691.47 1806.40 25.11 843.00 868.11 210 157.26 1744.39 1901.65 28.81 809.25 838.06 215 164.98 1722.49 1877.79 22.11 684.84 706.95 225 213.94 1709.19 1923.13 83.61 745.44 829.05 230 229.59 1686.40 1915.99 27.31 612.73 640.04 235 248.87 1665.24 1914.11 13.03 527.30 540.33 240 295.53 1657.91 1953.44 41.38 568.09 609.47 245 356.65 1648.39 2005.04 24.01 505.49 529.50 250 423.73 1608.84 2032.57 8.45 417.06 425.51 260 250.87 1539.96 1790.83 15.67 37.45 453.12 265 139.08 1431.42 1570.50 2.49 355.30 357.79 270 44.89 1205.98 1220.87 0.89 325.24 326.13 275 24.33 <td>1055.67</td> <td></td> <td>2162.85</td> <td>3218.52</td> <td></td> <td>324.34</td> <td>1503.63</td> <td>1827.97</td> <td>185</td>	1055.67		2162.85	3218.52		324.34	1503.63	1827.97	185
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	835.21		2173.37	3008.58		487.57	1431.94	1919.51	190
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1000.00		2063.58	3063.58		362.79	1257.98	1620.77	200
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	278.97		1954.24	2233.21		85.85	1048.88	1134.73	205
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	114.93		1691.47	1806.40		25.11	843.00	868.11	210
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	157.20		1722 49	1901.00		28.01	809.25 739.15	762.85	220
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	173.87		1699.92	1873.79		22.11	684.84	706.95	225
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	213.94		1709.19	1923.13		83.61	745.44	829.05	230
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	229.59		1686.40	1915.99		27.31	612.73 527.30	640.04 540.33	235
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	246.67		1657.91	1914.11		41.38	568.09	609.47	245
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	356.65		1648.39	2005.04		24.01	505.49	529.50	250
423.73 1608.84 2032.57 8.45 417.06 425.51 260 250.87 1539.96 1790.83 15.67 437.45 453.12 265 139.08 1431.42 1570.50 2.49 355.30 357.79 270 44.89 1205.98 1250.87 0.89 325.24 326.13 275 24.33 1088.60 1112.93 0.50 314.51 315.01 280 40.81 1188.80 1229.61 0.88 336.35 337.23 285 9.23 925.69 934.92 0.84 346.25 347.09 290 18.57 1049.20 1067.77 0.64 350.81 351.45 295 27.61 1131.48 1159.09 1.28 391.88 393.16 300 55.15 1284.71 1339.86 3.40 454.83 458.23 305 126.11 1480.25 1606.36 8.53 531.71 540.24 310 283.80 1657.91 1941.71 74.10 726.94 801.04 315 405.84 1728.95 2134.79 200.10 842.29 1042.39 320 463.43 1767.11 2230.54 189.27 899.60 1088.87 325 565.04 1802.06 2367.10 227.97 963.33 1191.30 330 683.86 1823.83 2507.69 218.84 1025.85 1244.69 335 625.66 1856.4	437.60		1634.12	2071.72		7.04	420.64	427.68	255
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	423.73		1508.84	2032.57		8.45	417.06	425.51	265
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	139.08		1431.42	1570.50		2.49	355.30	357.79	270
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	44.89		1205.98	1250.87		0.89	325.24	326.13	275
40.81 1188.80 1229.81 0.86 336.33 337.23 203 9.23 925.69 934.92 0.84 346.25 347.09 290 18.57 1049.20 1067.77 0.64 350.81 351.45 295 27.61 1131.48 1159.09 1.28 391.88 393.16 300 55.15 1284.71 1339.86 3.40 454.83 458.23 305 126.11 1480.25 1606.36 8.53 531.71 540.24 310 283.80 1657.91 1941.71 74.10 726.94 801.04 315 405.84 1728.95 2134.79 200.10 842.29 1042.39 320 463.43 1767.11 2230.54 189.27 899.60 1088.87 325 565.04 1802.06 2367.10 227.97 963.33 1191.30 330 683.86 1823.83 2507.69 218.84 1025.85 1244.69 335 625.66 1856.45 2482.11 86.00 995.97 1081.97 340 1123.67 1769.25 2892.92 336.17 1178.71 1514.88 345 949.68 1851.76 2801.44 425.65 1250.10 1675.75 350 1279.31 1761.39 3040.70 696.57 1273.39 196.96 355	24.33		1088.60	1112.93		0.50	314.51	315.01	280
18.57 1049.20 1067.77 0.64 350.81 351.45 295 27.61 1131.48 1159.09 1.28 391.88 393.16 300 55.15 1284.71 1339.86 3.40 454.83 458.23 305 126.11 1480.25 1606.36 8.53 531.71 540.24 310 283.80 1657.91 1941.71 74.10 726.94 801.04 315 405.84 1728.95 2134.79 200.10 842.29 1042.39 320 463.43 1767.11 2230.54 189.27 899.60 1088.87 325 565.04 1802.06 2367.10 227.97 963.33 1191.30 330 683.86 1823.83 2507.69 218.84 1025.85 1244.69 335 625.66 1856.45 2482.11 86.00 995.97 1081.97 340 1123.67 1769.25 2892.92 336.17 1178.71 1514.88 345 949.68 1851.76 2801.44 425.65 1250.10 1675.75	40.81		925.69	934 92		0.88	346.25	347.09	290
27.611131.481159.091.28391.88393.1630055.151284.711339.863.40454.83458.23305126.111480.251606.368.53531.71540.24310283.801657.911941.7174.10726.94801.04315405.841728.952134.79200.10842.291042.39320463.431767.112230.54189.27899.601088.87325565.041802.062367.10227.97963.331191.30330683.861823.832507.69218.841025.851244.69335625.661856.452482.1186.00995.971081.973401123.671769.252892.92336.171178.711514.88345949.681851.762801.44425.651250.101675.753501279.311761.393040.70696.571273.391969.96355	18.57	•	1049.20	1067.77		0.64	350.81	351.45	295
55.15 1284.71 1339.86 3.40 454.83 456.23 303 126.11 1480.25 1606.36 8.53 531.71 540.24 310 283.80 1657.91 1941.71 74.10 726.94 801.04 315 405.84 1728.95 2134.79 200.10 842.29 1042.39 320 463.43 1767.11 2230.54 189.27 899.60 1088.87 325 565.04 1802.06 2367.10 227.97 963.33 1191.30 330 683.86 1823.83 2507.69 218.84 1025.85 1244.69 335 625.66 1856.45 2482.11 86.00 995.97 1081.97 340 1123.67 1769.25 2892.92 336.17 1178.71 1514.88 345 949.68 1851.76 2801.44 425.65 1250.10 1675.75 350 1279.71 1761.39 3040.70 696.57 1273.39 1969.96 355	27.61		1131.48	1159.09		1.28	391.88	393.16	300
283.80 1657.91 1941.71 74.10 726.94 801.04 315 405.84 1728.95 2134.79 200.10 842.29 1042.39 320 463.43 1767.11 2230.54 189.27 899.60 1088.87 325 565.04 1802.06 2367.10 227.97 963.33 1191.30 330 683.86 1823.83 2507.69 218.84 1025.85 1244.69 335 625.66 1856.45 2482.11 86.00 995.97 1081.97 340 1123.67 1769.25 2892.92 336.17 1178.71 1514.88 345 949.68 1851.76 2801.44 425.65 1250.10 1675.75 350 127.93 196.94 70 696.57 1273.39 196.96 355	55.15	•	1284.71	1339.86		3.40 853	454.83 531.71	540.23	310
405.841728.952134.79200.10842.291042.39320463.431767.112230.54189.27899.601088.87325565.041802.062367.10227.97963.331191.30330683.861823.832507.69218.841025.851244.69335625.661856.452482.1186.00995.971081.973401123.671769.252892.92336.171178.711514.88345949.681851.762801.44425.651250.101675.753501279.311761.393040.70696.571273.391969.96355	283.80)	1657.91	1941.71		74.10	726.94	801.04	315
463.43 1767.11 2230.54 189.27 899.60 1088.87 325 565.04 1802.06 2367.10 227.97 963.33 1191.30 330 683.86 1823.83 2507.69 218.84 1025.85 1244.69 335 625.66 1856.45 2482.11 86.00 995.97 1081.97 340 1123.67 1769.25 2892.92 336.17 1178.71 1514.88 345 949.68 1851.76 2801.44 425.65 1250.10 1675.75 350 1279.31 1761.39 3040.70 696.57 1273.39 1969.96 355	405.84	1 .	1728.95	2134.79		200.10	842.29	1042.39	320
505.04 1802.06 2367.10 227.97 903.33 1191.30 330 683.86 1823.83 2507.69 218.84 1025.85 1244.69 335 625.66 1856.45 2482.11 86.00 995.97 1081.97 340 1123.67 1769.25 2892.92 336.17 1178.71 1514.88 345 949.68 1851.76 2801.44 425.65 1250.10 1675.75 350 1279.31 1761.39 3040.70 696.57 1273.39 1969.96 355	463.43	i	1767.11	2230.54		189.27	899.60	1088.87	325
625.66 1856.45 2482.11 86.00 995.97 1081.97 340 1123.67 1769.25 2892.92 336.17 1178.71 1514.88 345 949.68 1851.76 2801.44 425.65 1250.10 1675.75 350 1279.31 1761.39 3040.70 696.57 1273.39 1969.96 355	565.04 683.86	ł	1802.00	2507.10		218.84	1025.85	1244.69	335
1123.67 1769.25 2892.92 336.17 1178.71 1514.88 345 949.68 1851.76 2801.44 425.65 1250.10 1675.75 350 1279.31 1761.39 3040.70 696.57 1273.39 1969.96 355	625.66	, ,	1856.45	2482.11		86.00	995.97	1081.97	340
949.68 1851.76 2801.44 425.65 1250.10 1675.75 350 1279.31 1761.39 3040.70 696.57 1273.39 1969.96 355	1123.67	7	1769.25	2892.92		336.17	1178.71	1514.88	345
	949.68 1270 1	\$	1851.76 1761 30	2801.44		425.65 696.57	1250.10	1969.96	355













Fig. 3 - Optical depth at Viking Lander VL1 - in detail





Fig. 5 - Beam irradiance at the top of Mars atmosphere as function of areocentric longitude









(a) Effect of optical depth with Sun zenith angle as a parameter







Fig. 8 - Concluded



(a) Effect of optical depth with Sun zenith angle as a parameter

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Fig. 9 -

Variation of the normalized net flux function at the Martian surface with optical depth and Sun zenith angle, for albedo = 0.4





Fig. 9 - Concluded





GLOBAL IRRADIANCE, Gdh, W/m²

SUN ZENITH ANGLE, Z, deg

(b) Effect of Sun zenith angle with optical depth as a parameter

Fig. 10 - Variation of the global irradiance with optical depth and Sun zenith angle on a horizontal surface, at mean irradiance of 590 W/m^2





(b) Effect of Sun zenith angle with optical depth as a parameter

Fig. 11 - Variation of beam irradiance with optical depth and Sun zenith angle, on a horizontal surface, at mean irradiance of 590 W/m^2



(b) Effect of Sun zenith angle with optical depth as a parameter

Fig. 12 - Variation of diffuse irradiance with optical depth and sun zenith angle, on a horizontal surface, at mean irradiance of 590 W/m^2



Fig. 13 - Daylight hours (terrestrial), hr



Fig. 14 - Diurnal variation of global ${\rm G}_{\rm h},$ beam ${\rm G}_{\rm bh}$ and diffuse ${\rm G}_{\rm dh}$ irradiance on a horizontal Mars surface at Viking Lander VL1



Areocentric Longitude, L_S, Deg.

Fig. 15 - Daily global insolation on a horizontal surface on Mars for seventy two areocentric longitudes covering a Martian year, at VL1 and VL2

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FIGURE 16b. - MARS MAP. 1:15,000,000, DEPARTMENT OF THE INTERTOR. U.S. GLODOGICAL SURVEY.

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6. Abstract Detailed information on solar radiation solar energy systems operating on the related data from which the diurnally are calculated. The radiation data and images taken of the sun with a spection wavelength and multiple scattering of include a refinement of the solar radional solar radional solar solar radional solar solar radional solar sol	on characteristics on Mars are necess the surface of Mars. In this paper we y and daily variation of the global, d e based on measured optical depth of ial diode on the Viking Lander cam- of the solar radiation. This work is a liation model.	sary for effective design of future planned e present a procedure and solar radiation lirect beam and diffuse insolation on Mars of the Martian atmosphere derived from eras; and computation based on multiple an update to NASA TM 102299 and			

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