

NASA Technical Memorandum 105630

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A Flexible CPW Package for a 30 GHz MMIC Amplifier

Rainee N. Simons
Sverdrup Technology, Inc.
Lewis Research Center Group
Brook Park, Ohio

and

Susan R. Taub
National Aeronautics and Space Administration
Lewis Research Center
Cleveland, Ohio

Prepared for the
Topical Meeting on Electrical Performance of Electronic Packaging
cosponsored by the IEEE, MTT, and CHMT
Tuscon, Arizona, April 22-24, 1992

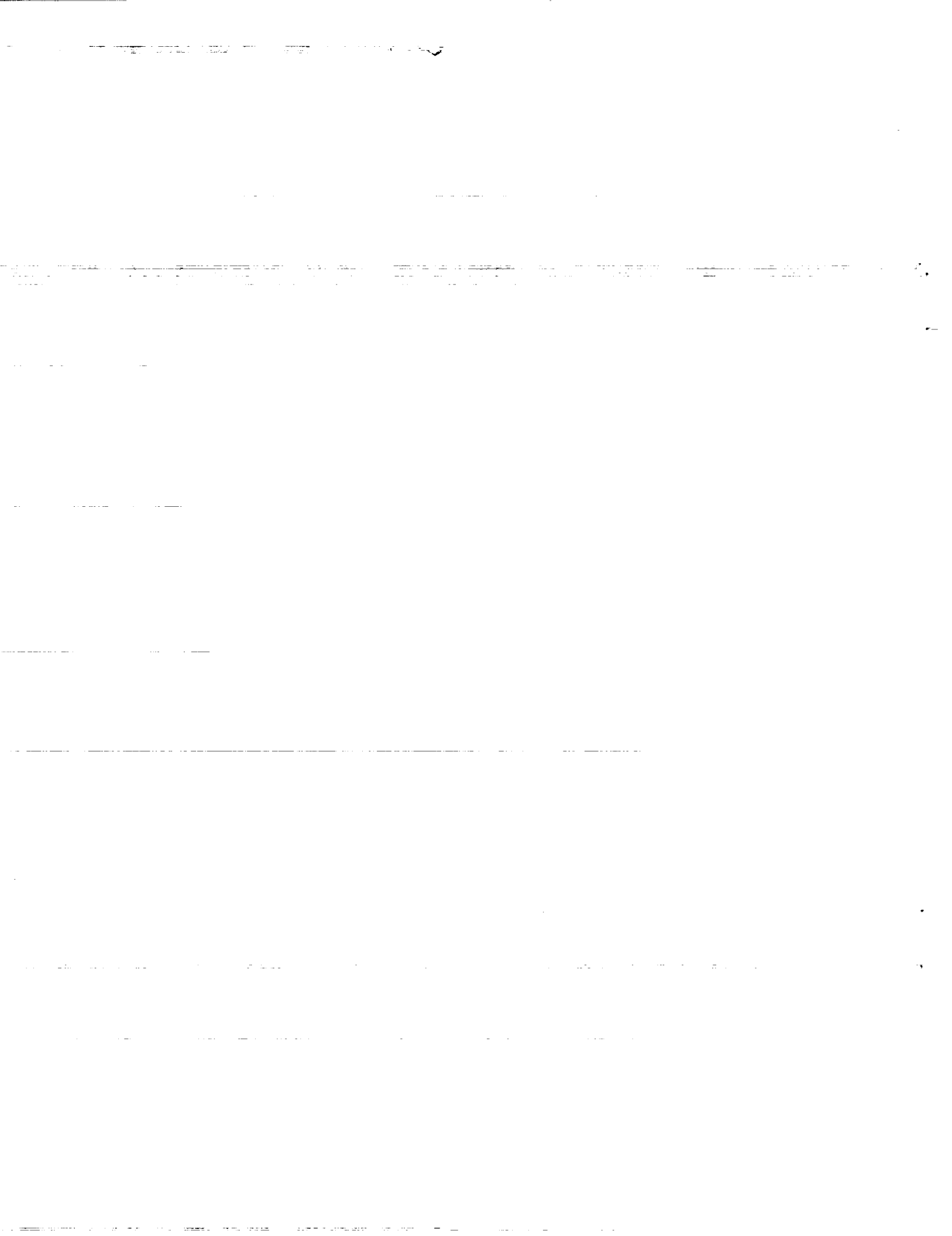


(NASA-TM-105630) A FLEXIBLE CPW PACKAGE FOR
A 30 GHz MMIC AMPLIFIER (NASA) 6 pCSCL 09A

N92-23193

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A FLEXIBLE CPW PACKAGE FOR A 30 GHz MMIC AMPLIFIER

Rainee N. Simons and Susan R. Taub
National Aeronautics and Space Administration
Lewis Research Center
Cleveland, OH 44135

SUMMARY

A novel package, which consists of a carrier and housing, has been developed for monolithic-millimeter wave Integrated Circuit amplifiers which operate at 30 GHz. The carrier has coplanar waveguide (CPW) interconnects and provides heat-sinking, tuning, and cascading capabilities. The housing provides electrical isolation, mechanical protection, and a feed-thru for biasing.

INTRODUCTION

MMICs (monolithic-millimeter integrated circuits) are currently available for satellite communication applications at millimeter wave frequencies (ref. 1). However, very little has been done in the development of carriers and housings that enable these circuits to be inserted into actual systems. In this paper we present the design and characteristics of a CPW (coplanar waveguide) carrier and a housing for MMIC amplifiers operating at 30 GHz. CPW circuits have the advantage of providing easy series as well as shunt mounting of microwave devices. Furthermore, since the ground planes are on the same side as the strip conductor, via holes and wraparounds are eliminated; therefore, parasitics are small. Radiation loss, when compared to microstrip, is low; hence CPW circuits are less prone to interaction with the package and EM interference. Another advantage is that CPW circuits lend themselves to fast and inexpensive characterization using wafer probing equipment.

CARRIER DESIGN

The carrier assembly is shown in figure 1. The carrier consists of a finite width conductor backed CPW (CBCPW) circuit on a dielectric substrate. The CBCPW circuit consists of a pair of tapered open circuits which face each other, and are separated by the surrounding ground plane. The ground plane also serves as an island for mounting MMIC devices and facilitates low inductance ground connections from any point on the perimeter of the MMIC. The length of separation between the open circuits is chosen to accommodate a particular MMIC chip. By tapering the CPW open circuit the electric field lines are concentrated at the open end and therefore are coupled efficiently to the short wire bonds between the CPW input/output lines and the MMIC. A copper post (diameter 0.031 in.) inserted in the center of the carrier serves as a heat sink for the MMIC. A brass backing plate provides heat dissipation and mechanical support. The MMIC and brass backing plate are attached to the dielectric substrate using silver conductive epoxy.

This carrier provides advantages in the following areas: Tuning, cascading and calibration. MMIC tuning is accomplished by sliding small lengths of metal strips over the CPW circuit until the desired S-parameters are obtained. The metal strips are then glued in place. Two or more of the above carriers can be cascaded, as shown in figure 1, by use of a novel plastic clip. The clip slides over and grips the two brass backing plates. This ensures excellent alignment for wire bonding. LRL calibration can be performed to the plane of the MMIC.

HOUSING

A single carrier with the housing is shown in figure 2. The housing provides mechanical protection, electrical isolation, and a coaxial feed-thru for bias lines.

EXPERIMENTAL RESULTS

A single carrier was tested by fixing a $50\ \Omega$ GaAs microstrip line, 700 mils long, in place of an MMIC, wire-bonding it to the CPW lines and measuring the S-parameters over the frequency range of 29 to 30 GHz with an HP 8510B Network Analyzer. The measured insertion loss, $S_{21} = 1.9\ \text{dB}$ and the return loss, $S_{11} < -15\ \text{dB}$, as shown in figure 3. This includes the losses of the Wiltron Universal Test Fixture and the carrier. These losses were found to be 0.9 dB by measuring the insertion loss of an identical CPW thru-line on an identical substrate. The insertion loss and return loss measured with and without the housing is shown in figure 4. The S_{21} measured, without the microstrip line, is a measure of the isolation between the input and output ports. The carrier and the housing were tested. An isolation of greater than 16 dB was measured, which is an improvement of 10 dB over the isolation of the carrier without the housing. The measured characteristics are shown in figure 5. Figure 6 shows the carrier, carrier with housing and cascaded carriers.

REFERENCE

1. Saunier, P.; and Tserng, H.Q.: AlGaAs/InGaAs Heterostructures with Doped Channels for Discrete Devices and Monolithic Amplifiers. IEEE Trans. Electron Devices, vol. 36, Oct. 1989, pp. 2231-2235.

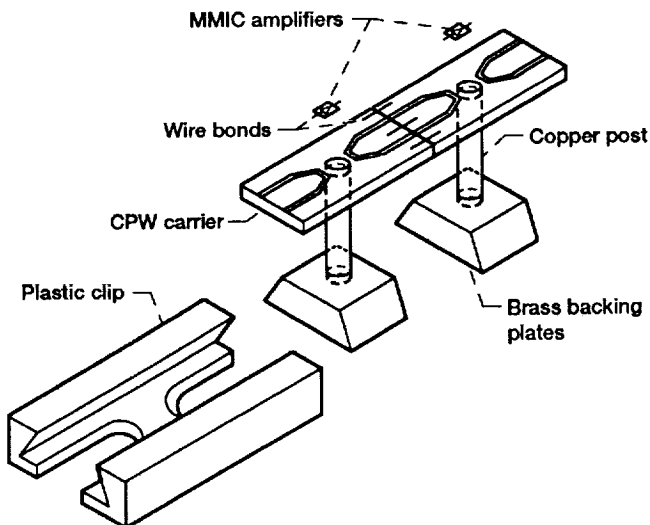


Figure 1.—Schematic for cascading CBCPW carriers using a plastic clip.

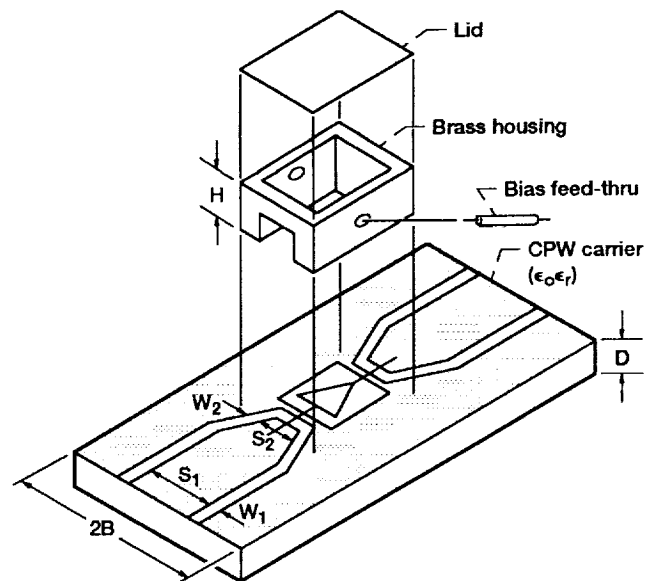
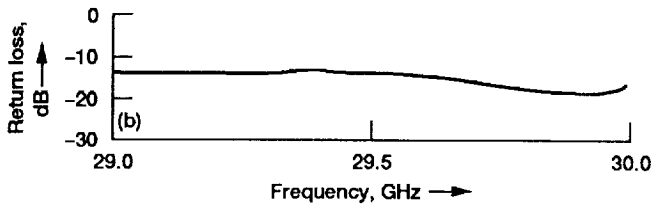
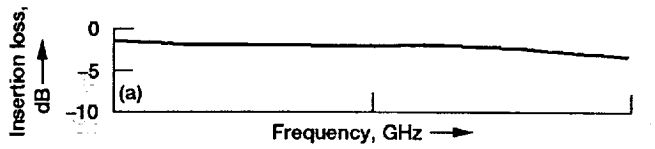
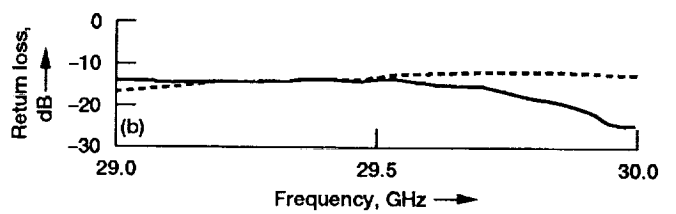
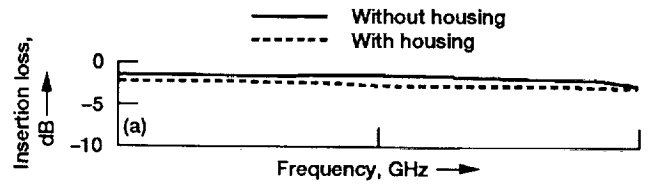


Figure 2.—Schematic of carrier with housing. Finite width conductor backed coplanar waveguide; $S_1 = 0.013\ \text{in.}$, $W_1 = 0.010\ \text{in.}$, $S_2 = 0.010\ \text{in.}$, $W_2 = 0.008\ \text{in.}$, $D = 0.025\ \text{in.}$, $\epsilon_r = 10.5$, $2B = 0.2\ \text{in.}$, $H = 0.135\ \text{in.}$



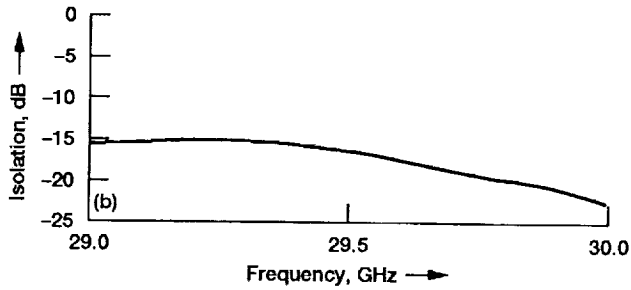
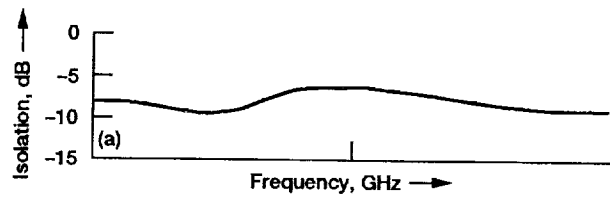
(a) Insertion loss.
(b) Return loss.

Figure 3.—Measured characteristics of the carrier.



(a) Insertion loss.
(b) Return loss.

Figure 4.—Effect of housing on the measured characteristics of the carrier.



(a) Without housing.
(b) With housing.

Figure 5.—Measured isolation.

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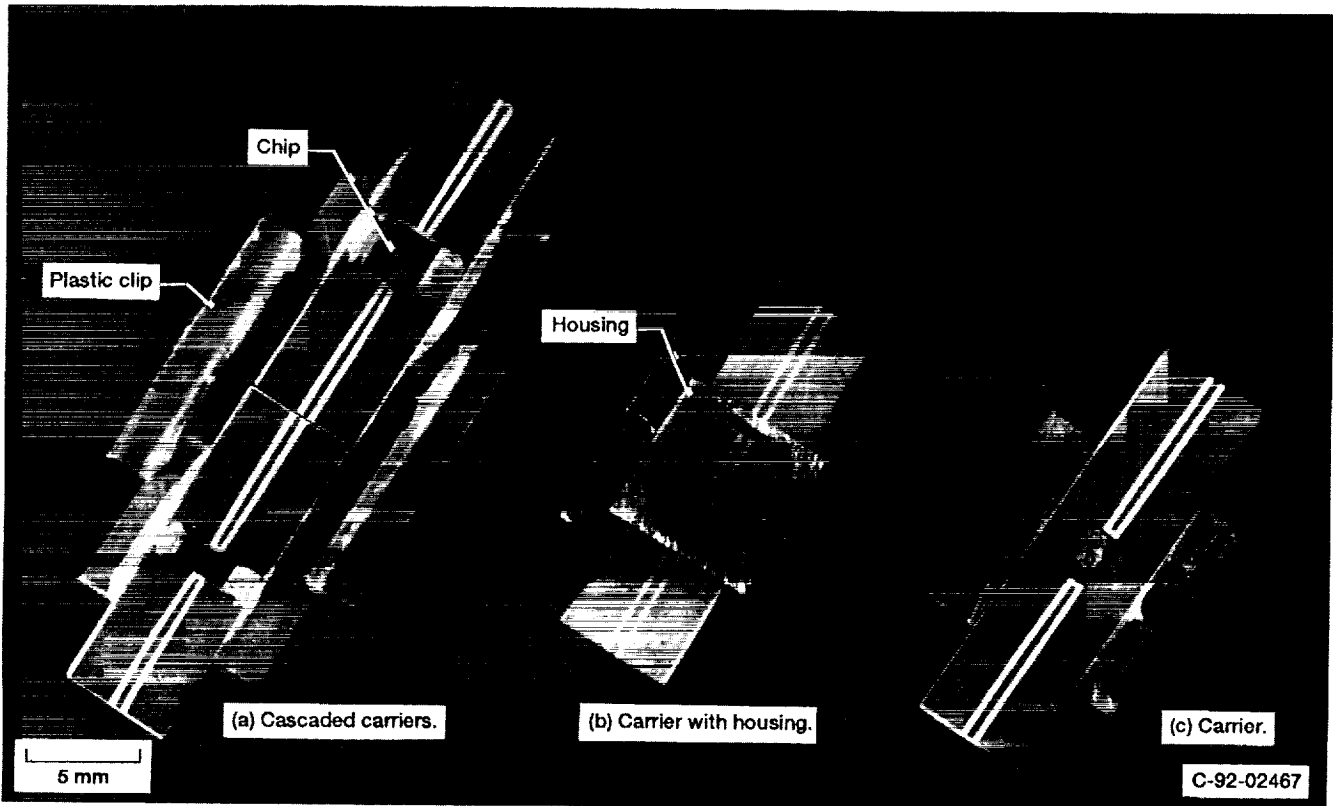
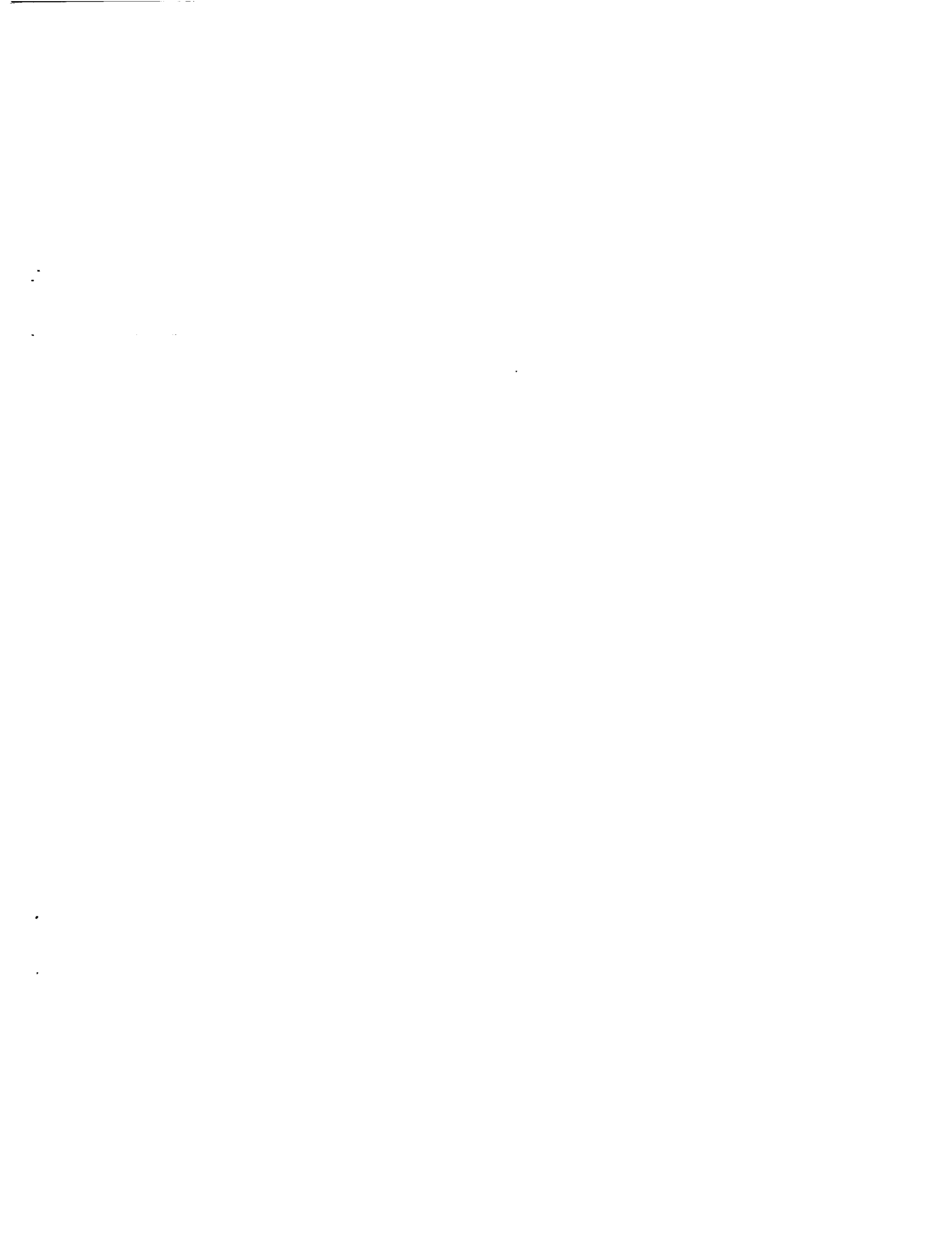


Figure 6.—CPW carriers.



REPORT DOCUMENTATION PAGE

Form Approved
OMB No. 0704-0188

Public reporting burden for this collection of information is estimated to average 1 hour per response, including the time for reviewing instructions, searching existing data sources, gathering and maintaining the data needed, and completing and reviewing the collection of information. Send comments regarding this burden estimate or any other aspect of this collection of information, including suggestions for reducing this burden, to Washington Headquarters Services, Directorate for Information Operations and Reports, 1215 Jefferson Davis Highway, Suite 1204, Arlington, VA 22202-4302, and to the Office of Management and Budget, Paperwork Reduction Project (0704-0188), Washington, DC 20503.

1. AGENCY USE ONLY (Leave blank)	2. REPORT DATE 1992	3. REPORT TYPE AND DATES COVERED Technical Memorandum	
4. TITLE AND SUBTITLE A Flexible CPW Package for a 30 GHz MMIC Amplifier		5. FUNDING NUMBERS WU-506-44-2C	
6. AUTHOR(S) Rainee N. Simons and Susan R. Taub			
7. PERFORMING ORGANIZATION NAME(S) AND ADDRESS(ES) National Aeronautics and Space Administration Lewis Research Center Cleveland, Ohio 44135-3191		8. PERFORMING ORGANIZATION REPORT NUMBER E-6973	
9. SPONSORING/MONITORING AGENCY NAMES(S) AND ADDRESS(ES) National Aeronautics and Space Administration Washington, D.C. 20546-0001		10. SPONSORING/MONITORING AGENCY REPORT NUMBER NASA TM-105630	
11. SUPPLEMENTARY NOTES Prepared for the Topical Meeting on Electrical Performance of Electronic Packaging cosponsored by the IEEE, MTT, and CHMT, Tuscon, Arizona. April 22-24, 1992. Rainee N. Simons, Sverdrup Technology, Inc., Lewis Research Center Group, 2001 Aerospace Parkway, Brook Park, Ohio 44142 (work funded by NASA Contract NAS3-25266); and Susan R. Taub, NASA Lewis Research Center. Responsible person, Susan R. Taub, (216) 433-6571.			
12a. DISTRIBUTION/AVAILABILITY STATEMENT Unclassified - Unlimited Subject Category 33		12b. DISTRIBUTION CODE	
13. ABSTRACT (Maximum 200 words) A novel package, which consists of a carrier and housing, has been developed for monolithic-millimeter wave Integrated Circuit amplifiers which operate at 30 GHz. The carrier has coplanar waveguide (CPW) interconnects and provides heat-sinking, tuning and cascading capabilities. The housing provides electrical isolation, mechanical protection and a feed-thru for biasing.			
14. SUBJECT TERMS Coplanar waveguide; Package; Amplifier		15. NUMBER OF PAGES 6	
		16. PRICE CODE A02	
17. SECURITY CLASSIFICATION OF REPORT Unclassified	18. SECURITY CLASSIFICATION OF THIS PAGE Unclassified	19. SECURITY CLASSIFICATION OF ABSTRACT Unclassified	20. LIMITATION OF ABSTRACT