

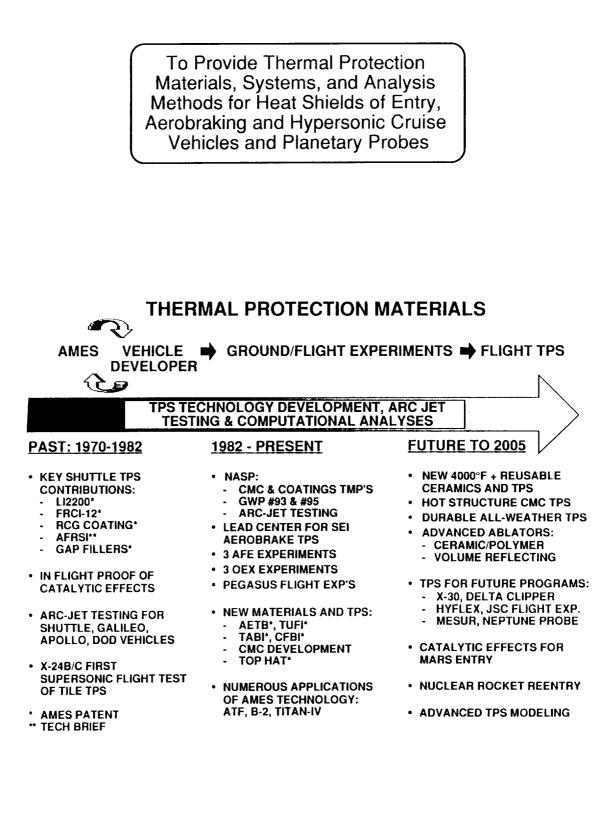
## ADVANCED CERAMIC MATRIX COMPOSITES FOR TPS

Daniel J. Rasky NASA Ames Research Center Moffett Field, CA

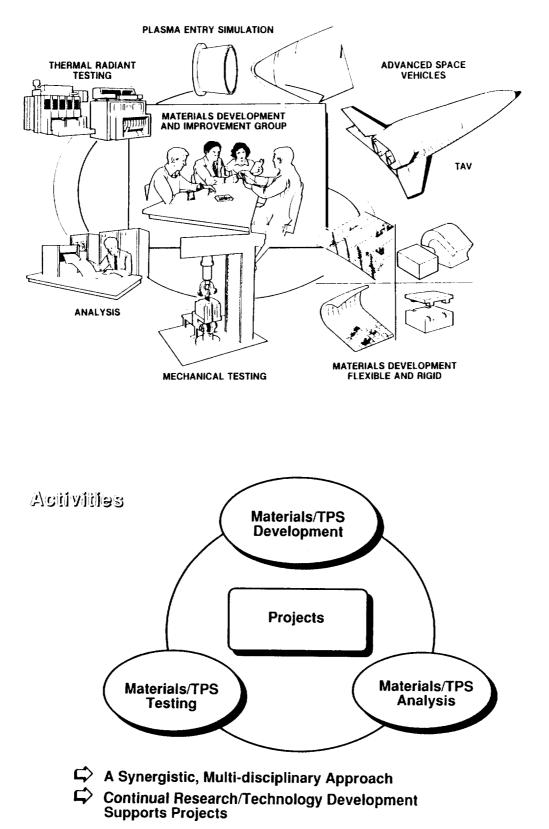
### Abstract

Recent advances in ceramic matrix composite (CMC) technology provide considerable opportunity for application to future aircraft thermal protection systems (TPS), providing materials with higher temperature capability, lower weight, and higher strength and stiffness than traditional materials. The Thermal Protection Material Branch at NASA Ames Research Center has been making significant progress in the development, characterization, and entry simulation (arc-jet) testing of new CMC's. This presentation gives a general overview of the Ames Thermal Protection Materials Branch research activities, followed by more detailed descriptions of recent advances in very-high temperature Zr and Hf based ceramics, high temperature, high strength SiC matrix composites, and some activities in polymer precursors and ceramic coating processing. The presentation closes with a brief comparison of maximum heat flux capabilities of advanced TPS materials.

## Long Range Goal of the Ames Thermal Protection Materials Branch



## THERMAL PROTECTION SYSTEM DEVELOPMENT PROCESS



Projects

## **NASA Programs**

- SEI: Recent Langley "Aerobrake Assembly with Minimum Accommodation" study performed by Lockheed baselined Ames developed "TOP HAT" CMC/rigid tile TPS.
- Shuttle: Working with KSC, JSC, NASA HQ and Rockwell to fly Ames developed TUFI TPS on the Orbiters in high erosion areas.
- MESUR: Performed initial TPS sizing and trades. Identified a light weight silicon rubber TPS (SLA-561) which allows a 50% increase in scientific payload.
- Pegasus: Teaming with Dryden and LaRC for boundary layer cross flow transition experiment (scheduled to fly in FY92). Constructing Pegasus Wing-Glove and PI for and TPS performance evaluation experiment. Wing fillet heating experiment flown on first two Pegasus launches.
- HYFLEX: Working with a multi-agency team to define vehicle. Diboride leading edges and nosetip being evaluated.
- Wave-Rider: Discussions with McDonnell Douglas regarding leading edge design.

## NASP

- Responsibility for government work packages #93 and #95 for arc-jet testing and internal TPS insulation design.
- Both have been highly praised by NPO/JPO and Industry Leads (i.e. General Dynamics, Rockwell, Pratt Whitney).

## <u>DoD</u>

- Delta Clipper: Cooperative research program being developed with McDonnell Douglas and SDIO. Cooperative efforts proposed in three areas:
  - 1) TPS design and consultation
  - 2) Arc-jet testing
  - 3) Computational studies

## Material/TPS Testing Areas

- Arc-Jet Testing
  - Aerodynamic Heating Facility (20 MW)
  - Interactive Heating Facility (60 MW)
  - Panel Test Facility (20 MW)
- Material Characterization
  - SEM, XRF, Optical Microscopes
  - XRD, Large Sample TGA
  - Dilatometer, Instron
  - Infrared & Ultraviolet Spectrometers
  - ICP Mass Spectrometer (inorganic)
- Special Testing
  - Laser Time-of-Flight Mass Spectrometer (SALI)
  - Side Arm Reactor

## Material/TPS Analysis Areas

- Computational Surface Thermochemistry
  - Surface heating and catalysis effects (NSCAND, BLIMPK, LAURA, VSL, GASP)
  - Ablation, erosion, and shape change computations (ASC, CMA, ACE)
- Computational Solid Mechanics
  - Multi-dimensional conduction/radiation analyses (SINDA, TRASYS)
  - Multi-dimensional thermal-stress analyses (COSMOS)
- Computational Materials
  - CVD/CVI Processing (GENMIX, NACHOS)
  - Reflective TPS analyses
  - Composite material properties (MATX)

## Material/TPS Development Areas

## **Advanced Material Families**

- Ceramic Matrix Composites
  - Very-High Temperature Ceramics (HfB<sub>2</sub>+SiC)
  - High Temperature, High Strength Ceramics (C/SiC)
  - Polymer Precursors (Si/C/B fibers, tape casting)
  - Ceramic coatings processing
- Light Weight Ceramic Insulations
  - Rigid Tiles (AETB, SMI, UltraLight)
  - TABI and CFBI Flexible Blankets
  - Aerogel Studies
- Light Weight Ablators
  - Rigid Ceramic Insulation with a Polymer Filler
- Surface Coatings
  - Low Catalytic Efficiency, High Emissivity
  - Reflective

## **Diboride Materials**

- Manlabs Inc. (Cambridge MA) tested and compiled a data base on a large number of refractory materials in the 60's and early 70's
- The diborides of zirconium and hafnium (ZrB2 and HfB2) were found to be the most oxidation resistant, high temperature materials in the study, e.g.

## Arc testing of ZrB2 + 20 v/o SiC surface temp. 2510 C, stagn. press. 1.0 atm, stagn. enthalpy 11.6 kJ/gm recession: 0.66 mm/2 hrs equivalent graphite recession: 30 cm ! equivalent SiC recession: 45 cm !

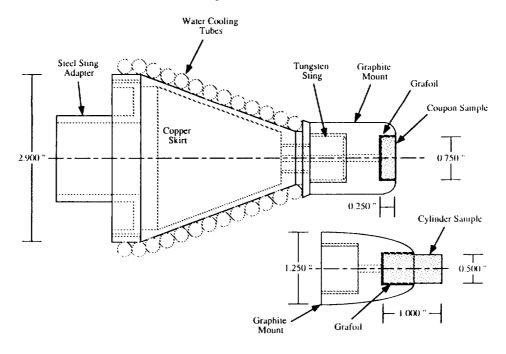
"These results illustrate the reuse capability of the boride composites... This capability is unrivaled by any other material system." - Quote from Dr. Larry Kaufman, Principal Investigator in the Manlabs Studies

## **Research Highlights for FY91**

Very-High Temperature Ceramics

- Phase I arc-jet testing completed
- 19 reinforced Zr and Hf based ceramics tested (from Manlabs, Cerac, Lanxide, SAIC)
- Arc-jet data in good agreement with earlier Manlabs results
- Over 2 times RCC maximum heat flux capability demonstrated
- 2200°C+ (4000°F+) capability demonstrated
- Successfully applied ZrB2 coatings to RCC using RF sputtering
- Phase II testing of disk samples, nosetip and leading edge components currently in progress

## Sample Model Holder



# Post-Test Photographs of RCC and ZrB2 + 20 v/o SiC Samples

Test Conditions: test time = 3 min, cold wall heat flux = 295 W/cm<sup>2</sup>, stag. press. = 0.046 atm, stag. enth. = 25 kJ/gm



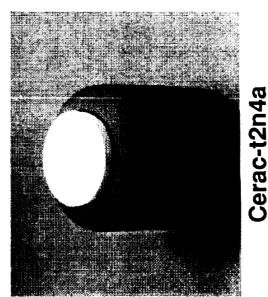
## LTV-t1n2a RCC

Recession: 2.0 mm Weight loss: 1.31 gm Peak temp.: 2040 C SiC coating lost after approximately 100 sec.

Recession: -0.03 mm Weight loss: 0.01 gm Peak temp.: 1820 C Adherent, thin, glassy coating

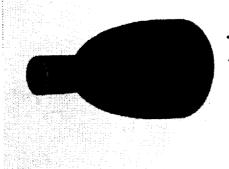
formed on sample

ZrB2 + 20v/o SiC



## Post-Test Photographs of Two HfB2 + 20 v/o SiC Samples

Test time = 5 min Cold wall heat flux = 560 W/cm<sup>2</sup> Stag. press. = 0.075 atm Stag. enth. = 27 kJ/gm

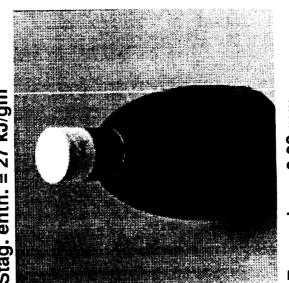


M an - (4n 1 (A-7-1) HfB2 + 20v/o SiC

Recession: -0.05 mm Weight loss: 0.00 gm Peak temp.: 1740 C

Clear glassy coating formed on sample

Test time = 3 min 2 Cold wall heat flux = 730 W/cm Stag. press. = 0.105 atm Stag. enth. = 27 kJ/gm



Recession: -0.03 mm Weight loss: 0.08 gm Peak temp.: 2460 C Adherent, thin oxide coating formed on sample

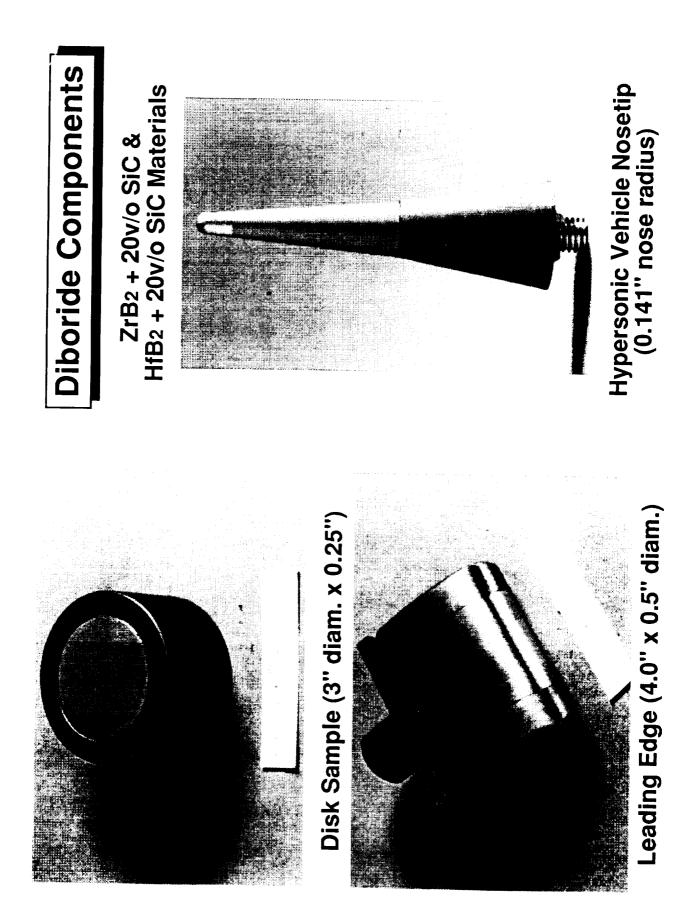


Table 1: Sample ComponentsAdvanced Refractory Composites (Testing Program Phase II)10/28/91				
Sample	Matrix/	Geometry/Dimension	Quantity	
Component	Reinforcement			
ManLabs-Cl	ZrB <sub>2</sub> /SiC <sub>p</sub>	Coupons/2.8"Dia. x 0.25"	3	
ManLabs-C2	ZrB <sub>2</sub> /SiC <sub>pl</sub>	Coupons/2.8"Dia. x 0.25"	3	
ManLabs-C3	ZrB <sub>2</sub> /SiC <sub>pl</sub> +C <sub>fch</sub>	Coupons/2.8"Dia x 0.25"	32	
ManLabs-LE	ZrB <sub>2</sub> /SiC <sub>pt</sub>	Leading Edge/0.75"Dia. x 2.75"	2	
ManLabs-H1	HfB <sub>2</sub> /SiC <sub>pl</sub>	Hemisphere/0.700"Radius	1	
ManLabs-112	HfB <sub>2</sub> /SiC <sub>pl</sub>	Hemisphere/0.500"Radius	1	
ManLabs-H3	HfB2/SiCpl	Hemisphere/0.125"Radius	1	
ManLabs-NT	HfB <sub>2</sub> /SiC <sub>pl</sub>	Nose Tip/0.141"Radius on	3	
ManLabs-S	ZrB <sub>2</sub> /SiC <sub>n</sub>	5,25 Deg. Cone Half Angle	1	
	p	Skirt		
Cerac-S	ZrB <sub>2</sub> /SiC <sub>p</sub>	5.25 Deg. Cone Half Angle Skirt	2	
Cerac-C	ZrB <sub>2</sub> /SiC <sub>n</sub>	Coupons/2.8"Dia. x 0.25"	3	
ACR-C1	$ZrB_2/SiC_p+C_{fc}$	Coupons/2.8"Dia. x 0.25"	2	
ACR-C2	ZrB2/SiCp+SiCfc	Coupons/2.8"Dia. x 0.25"	2	
ARC-C1	ZrB <sub>2</sub> Coated RCC	Coupons/2.8"Dia. x 0.25"	1	
ARC-C2	ZrB <sub>2</sub> Coated RCC	Coupons/2.8"Dia. x 0.25"	1	
GA-C1	RS-HfB <sub>2</sub> Coated	Coupons/2"Dia. x 0.25"	2	
	C/C		1	
GA-C2	HfO <sub>2</sub> Coated RS-	Coupons/2"Dia. x 0.25"	2	
	HfB2 Coated C/C		1	
SAIC-C1	ZrB2/SiC+Cfc	Coupons/2.8"Dia. x 0.25"	1	
SAIC-C2	ZrB <sub>2</sub> /SiC+C <sub>fc</sub>	Coupons/2.8"Dia. x 0.25"	1	
Total	1		35	

Subscript definitions: p = particulate, pl = platelet, fc = continuous fiber, fch = chopped fiber

## Material/TPS Development Areas

## **Advanced Material Families**

## Ceramic Matrix Composites

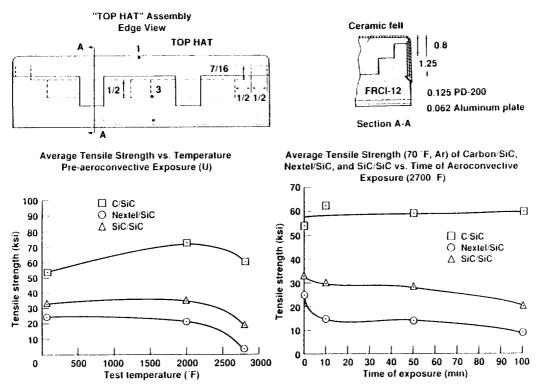
- Very-High Temperature Ceramics (HfB<sub>2</sub>+SiC)
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- Light Weight Ceramic Insulations
  - Rigid Tiles (AETB, SMI, UltraLight)
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  - Aerogel Studies
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  - Polymer Filler + Rigid Ceramic Insulation
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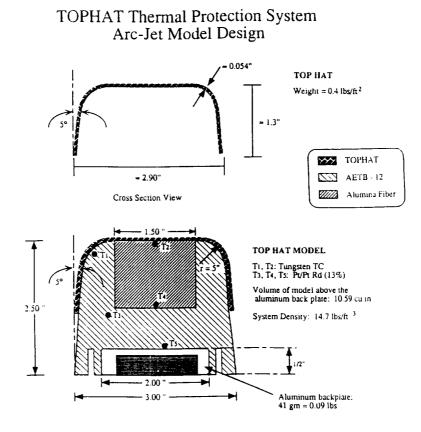
## **Research Highlights for FY91**

**Ceramic Matrix Composites** 

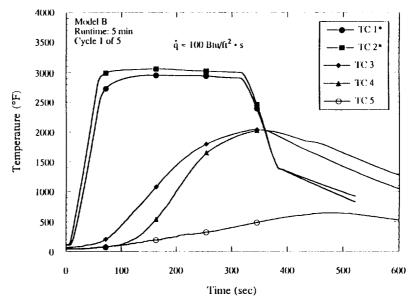
- DuPont and SEP fabricated Nicalon, Nextel, and carbon fiber reinforced SiC matrix composites evaluated for aerothermal and mechanical performance
- Pre and post-test mechanical property characterization showed that carbon fiber reinforced materials have little degradation after arc-jet exposure to 2700°F for ten cycles of ten minutes each
- DuPont material found to be equivalent or better (particularly in quasi-isotropic configuration) than SEP material.
- Mass loss and mechanical property retention results in very good agreement with radiative heating testing data recently reported by General Dynamics
- New Ames developed "TOP HAT" CMC/rigid tile TPS, using Ames CVD/CVI fabricated C/SiC CMC, shown to survive multiple arc-jet exposures to 3100°F

## **CERAMIC MATRIX COMPOSITES PROGRAM**

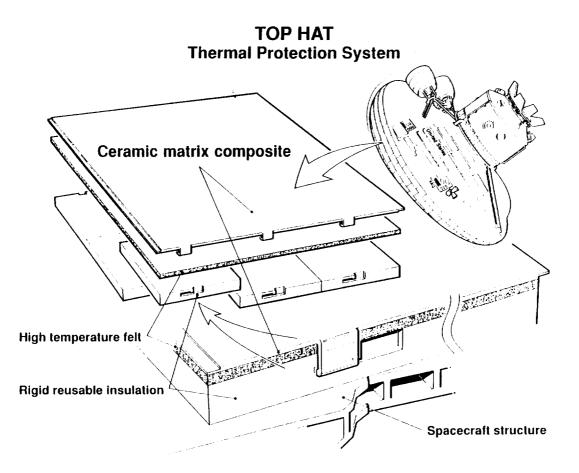




Thermal Response Of TOPHAT Model In An Aeroconvective Environment



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## Material/TPS Development Areas

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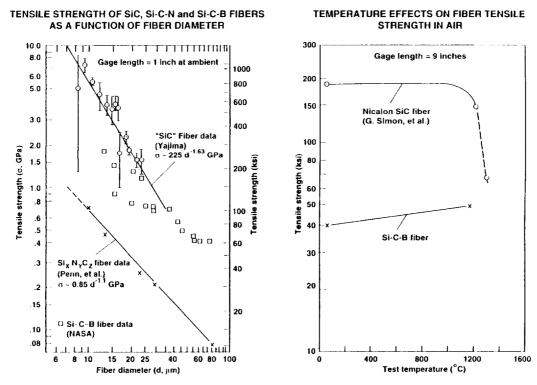
## **Research Highlights for FY91**

**Polymer Precursors** 

- Low oxygen content Si/C/B polymers synthesized
- UV air and non-oxygen cure procedure demonstrated
- Ceramic fibers show tensile strength retention to 1300°C
- Successfully synthesized Zircon/ZrB2/SiC 20 mil tapes using a combination of tape casting and sol-gel processing

**Ceramic Coating Processing** 

- Successfully applied thin (20 micron) coatings for ZrB<sub>2</sub> to a SiC substrate using RF sputtering
- Planning initial trials for plasma spraying ZrB2 and ZrB2/SiC using a constricted arc-jet



Ref. K.J. Wynne and R.W. Rice, Ann. Rev. Mater. Sci., 14, 297 - 334 (1984).

## Maximum Cold Wall Heat Flux Computations

For one-dimensional, radiative equilibrium, the maximum cold wall heat flux, Qcw, can be computed from the maximum material use temperature, Tmax, by:

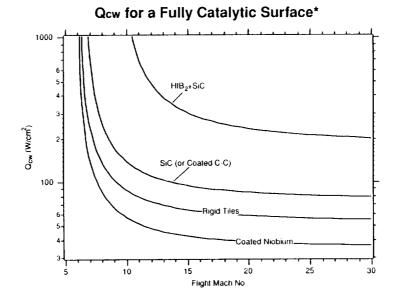
$$Q_{cw} = \varepsilon \sigma T_{max}^4 / (1 - H_w/H_r)$$

where  $\epsilon$  is the emissivity and H<sub>w</sub> is the wall gas enthalpy at T<sub>max</sub>, and H<sub>r</sub> is the local recovery enthalpy

- Surface catalytic effects all roll into the value of Hw
- With values for the material maximum use temperature and emissivity, Qcw can be easily computed

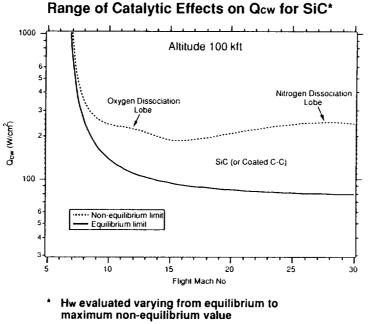
Material	Maximum Use Temp. (C)	Emissivity
HfB2+SiC	2480	0.62
SiC (or Coated C-C	i) 1760	0.76
Rigid Tiles	໌ 1540	0.85
<b>Coated Niobium</b>	1530	0.65

## Maximum Cold Wall Heat Flux Computations



\* Hw evaluated assuming chemical equilibrium

## Maximum Cold Wall Heat Flux Computations



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