

1N-02

160234

P.198

NASA Technical Memorandum 4434

Experimental Effects of Wing Location on Wing-Body Pressures at Supersonic Speeds

Jerry M. Allen and Carolyn B. Watson

APRIL 1993

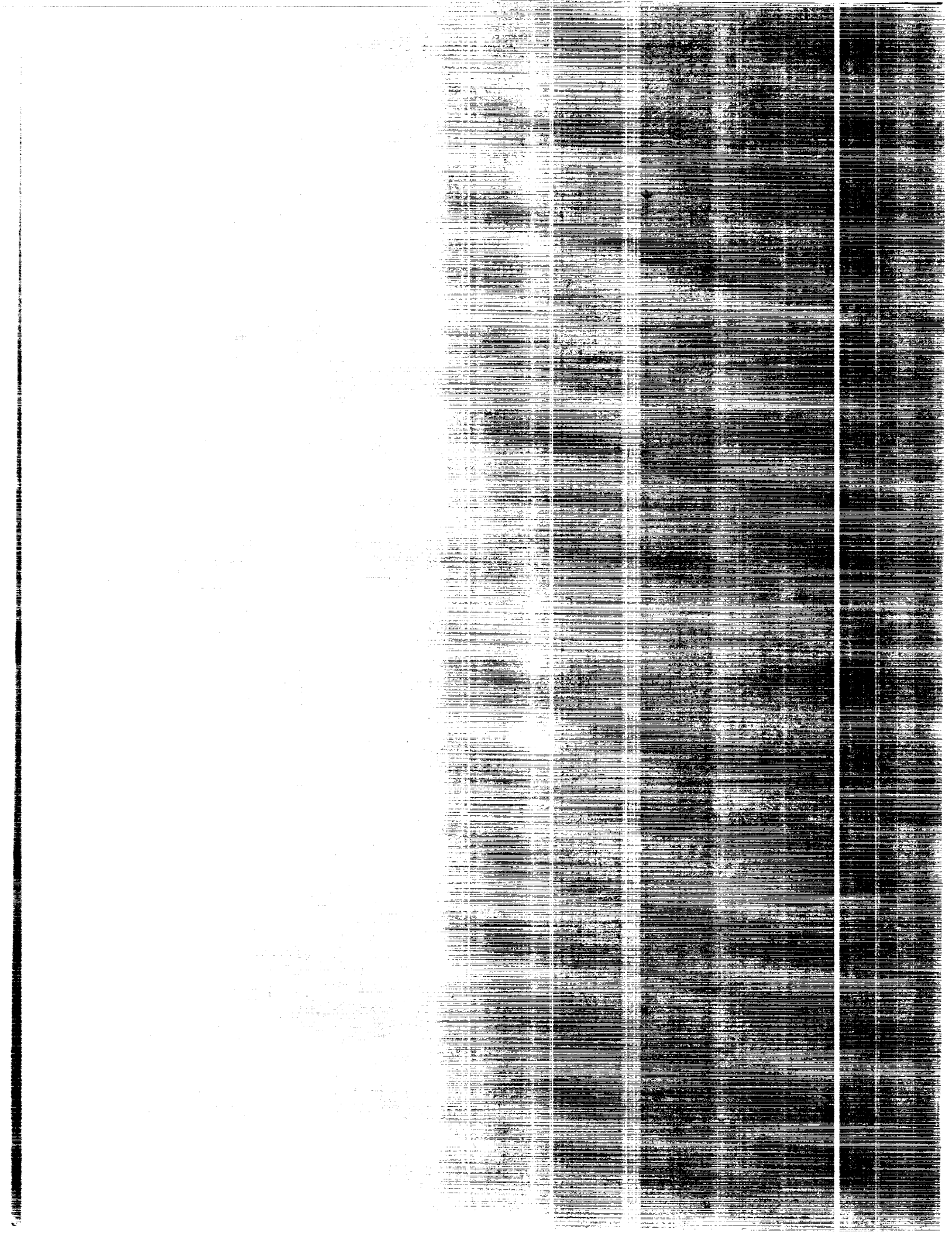
(NASA-TM-4434) EXPERIMENTAL EFFECTS OF WING LOCATION ON WING-BODY PRESSURES AT SUPERSONIC SPEEDS (NASA) 198 p

N93-26085

Unclass

H1/02 0160234

NASA



NASA Technical Memorandum 4434

Experimental Effects of Wing Location on Wing-Body Pressures at Supersonic Speeds

Jerry M. Allen and Carolyn B. Watson
Langley Research Center
Hampton, Virginia



National Aeronautics and
Space Administration

Office of Management

Scientific and Technical
Information Program

1993

Abstract

An experimental study has been performed at supersonic speeds to measure wing and body spanwise pressure distributions on an axisymmetric-body delta wing model on which the wing vertical location on the body was systematically varied from low- to high-mounted positions. In addition, for two of these positions both horizontal and radial wing angular orientations relative to the body were tested, and roll angle effects were investigated for one of the positions. Seven different wing-body configurations and a body-alone configuration were studied. The test was conducted at Mach numbers from 1.70 to 2.86 at angles of attack from about -4° to 24° . Pressure orifices were located at three longitudinal stations on each wing-body model, and at each station the orifices were located completely around the body, along the lower surface of the right wing (looking upstream), and along the upper surface of the left wing. All pressure coefficient data are tabulated, and selected samples are shown graphically to illustrate the effects of the test variables. The effects of angle of attack, roll angle, Mach number, longitudinal station, wing vertical location, wing angular orientation, and wing-body juncture are analyzed. The vertical location of the wing on the body had a very strong effect on the body pressures. For a given angle of attack at a roll angle of 0° , the pressures were virtually constant in the spanwise direction across the windward surfaces of the wing-body combination. Pressure-relieving, channeling, and vortex effects were noted in the data.

Introduction

The airframe of tactical missiles has traditionally been composed of an axisymmetric body and one or more sets of fins mounted radially on the body; that is, the plane of the fins passes through the body axis of symmetry. However, advanced carriage and fin-folding considerations can result in missile designs that have planar fins mounted either high or low on the body. In either case, these fins do not extend through the body symmetry axis and thus are termed "off-axis" fins.

Little experimental data exist on this off-axis-fin class of configurations, although a recent computational study (ref. 1) was performed using an Euler code to estimate wing-body interference effects. The primary purpose of the present experimental study was to provide a systematic set of pressure data for a generic off-axis configuration. To facilitate comparisons with other developing computational methods, the surface pressure orifices on the model were located so that a set of data could be generated completely around the wing-body configuration at constant longitudinal stations. The model was designed to have a planform similar to the wing-body portion of the force-and-moment model of reference 2 so

that pressure and loads data would be available for comparison purposes.

Symbols

The capitalized expression in parentheses next to the symbol is the computer printout equivalent of that symbol that is used in the aerodynamic data presented in tables 3-10.

C_p	(CP)	pressure coefficient, $(p - p_\infty)/q_\infty$
M_∞		free-stream Mach number
p		static pressure on body or wing surface, psi
p_∞		free-stream static pressure, psi
q_∞		free-stream dynamic pressure, psi
S	(S)	distance from body centerline to wing trailing-edge tip, 4.82 in.
y	(Y)	spanwise wing coordinate (measured from body center- line), in.

α	(ALPHA)	model angle of attack, deg
θ	(THETA)	circumferential body coordinate (measured clockwise from windward meridian at roll angle of 0° , looking upstream), deg
ϕ	(PHI)	model roll angle (measured clockwise, looking upstream, from windward meridian), deg

Apparatus and Test

Wind Tunnel

The test was conducted in the low Mach number test section of the Langley Unitary Plan Wind Tunnel. This tunnel is a variable-pressure continuous-flow facility with two test sections ranging in Mach number from 1.47 to 4.63. The Mach number is controlled by asymmetric sliding blocks, and the low-speed test section has a Mach number variation from 1.47 to 2.90. The test section is formed by the downstream section of the nozzle and is approximately 4 ft wide by 4 ft high by 7 ft long. A more detailed description of this wind tunnel can be found in reference 3.

Model

The model is composed of an axisymmetric body with a three-caliber tangent-ogive nose and delta wings with a leading-edge sweep of 77° . Interchangeable wings were designed to be mounted at various vertical and angular positions on the body at the same streamwise location. This arrangement resulted in seven different wing-body configurations in addition to a body-alone (body without wings) configuration. The model with planar wings (zero dihedral) located along the body axis of symmetry was considered the baseline configuration. Pressure orifices were located at three longitudinal stations on each configuration, and figure 1 shows sketches of the baseline configuration and the longitudinal location of the pressure orifices. The eight test configurations are identified in figure 2, and photographs of all eight sting-mounted models are shown in figure 3.

A planform sketch of the baseline model is presented in figure 4 to show the important dimensions. As seen in this figure, the model semispan measured from the body centerline was 4.82 in., which was held constant for all the winged configurations. Thus, the exposed wing area increased as the wing was moved to high or low locations from the baseline configuration. Also shown in figure 4 are the three longitudinal

stations at which pressure orifices were located on the wings and body. These locations were chosen to be at about 50, 75, and 95 percent of the theoretical wing root chord when extended to the body centerline, and they are identified as stations 1, 2, and 3, respectively.

At each station the pressure orifices were located completely around the body, along the upper surface of the left wing (looking upstream), and along the lower surface of the right wing. Body pressure orifices were located in 15° increments around the body, which resulted in a maximum of 24 body orifices at each station for the body-alone configuration. The winged configurations had up to five fewer body orifices because of the intersection of the wings with the body. Figure 5, which is a cross-sectional sketch showing the location of the body orifices, indicates the orifices that were eliminated because of the various wing locations. This sketch is applicable to all three longitudinal stations.

The wing pressure orifices were located as shown in figure 6, which is representative of either the upper surface of the left wing or the lower surface of the right wing. As many as 10 orifices were located on each wing surface at each station. These orifices were positioned to lie along constant rays originating from the theoretical wing apex. Table 1 lists the locations of these orifices and the rays on which they are found. Note that the spanwise distance coordinate y is measured along the wing surface and, thus, does not lie in a horizontal plane for the radially mounted wings. Up to five inboard wing orifices were located inside the body for some of the wing positions, thereby reducing the number of usable wing orifices for those configurations.

The body-alone configuration contained a total of 72 pressure orifices, whereas the wing-body configurations contained between 106 and 114 usable orifices. All pressure orifices were 0.026 in. in diameter and were mounted flush with and normal to the body or wing surface.

The pressure orifices were located on a flat wing surface. A sharp 10° bevel perpendicular to the edge was provided on both the leading and trailing edges of the opposite surface of that wing to provide a structural thickness and to accommodate the internal pressure tubing. As stated previously, the right and left wings of each configuration were instrumented on opposite surfaces; therefore, the flat surface of each wing was located on opposite sides. For all configurations in this study, the pressure orifices were located on the lower surface of the right wing (looking upstream) and on the upper surface of the

left wing. Thus, the lower surface of the right wing and the upper surface of the left wing were always flat. Because of this difference between the right and left wing surfaces, none of the configurations, except for the body alone, had true symmetry about the vertical plane. All wings had a maximum thickness of 0.188 in.

Instrumentation

The model pressures were measured by three 48-channel, electronically scanned pressure (ESP) modules located inside the body. The operational range of these modules was ± 5 psid over a temperature range from 0°F to 175°F . The rated accuracy of the modules was ± 0.15 percent of the full-scale value. For the test conditions of this investigation, this accuracy corresponded to an agreement in pressure coefficient of about 0.004 to 0.008.

Flexible tubing was used to connect the pressure orifices to the ESP modules inside the body. Because of the limited space available inside the body to house the three ESP modules and the associated pressure tubing, a few tubes for some of the configurations became too constricted to allow an accurate pressure measurement when the model was assembled. The pressures measured from these orifices were eliminated from the results of this study.

The model angle of attack, which was measured using an accelerometer mounted inside the nose of the model, was corrected for wind tunnel flow angularity. Model roll angle was set using the tunnel roll mechanism.

To induce boundary-layer transition to turbulent flow, transition strips were applied to the model using the technique established in reference 4. This technique was also used in the force and moment test of reference 2. These transition strips consisted of No. 50 sand grains (0.0128 in.) sprinkled in acrylic plastic. The strips were 0.062 in. wide and were located 1.20 in. aft of the nose and 0.40 in. aft of the leading edges (measured streamwise) on both the upper and lower surfaces of the wings.

Tests

Tests on all configurations were conducted at Mach numbers of 1.70, 2.16, 2.40, and 2.86 at a Reynolds number of 2×10^6 per foot. The model angle of attack ranged from about -4° to 24° in increments of 4° . The effects of roll angle ϕ were studied on the baseline configuration only (configuration 1), and for this configuration the roll angle varied from -90° to 90° in 30° increments.

Presentation of Data

Table 2 shows the arrangement of the pressure coefficient data listed in tables 3-10. Body pressure data are tabulated as a function of angular location around the body (θ), whereas the wing pressure data are tabulated as a function of the nondimensional distance along the wing from the body centerline (y/S). Note that the y/S parameter is measured along the wing surface which does not lie in a horizontal plane for the radially mounted wings. Selected data from tables 3-10 have been plotted and are analyzed in the following sections of this paper to illustrate the effects of the test variables. More extensive plots of the pressure data along with selected vapor-screen photographs of the vortex patterns on the model can be found in reference 5.

Analysis of Selected Data

The primary test variables in this investigation are the model angle of attack and roll angle, the free-stream Mach number, and the wing vertical location and angular orientation on the body. The effects of longitudinal station and wing-body juncture can also be examined because data were obtained at three streamwise locations on both the wings and body.

The effects of the resulting seven variables are examined sequentially in this section. All pressure coefficient data have been plotted to the same scale to facilitate comparisons. Body pressure data are plotted as a function of angular location around the body (θ). For $\phi = 0^\circ$, the windward meridian on the body is located at $\theta = 0^\circ$ and 360° , whereas the leeward meridian is located at $\theta = 180^\circ$. Wing pressures are plotted as a function of the nondimensional spanwise distance y/S along the wing from the body centerline.

For all wing pressure plots at $\phi = 0^\circ$ discussed in the following sections of this paper, windward and leeward pressures are shown together as if they were measured on windward and leeward surfaces of the same wing, even though they were, in fact, measured on opposite wings. For these cases, the plots are presented in this manner to facilitate comparisons between windward and leeward pressures and to emphasize that a set of pressure data encompassing the wing-body combination can be generated from these data. Data for nonzero roll angles need to be presented in a different manner, as will be discussed later when examining roll angle effects.

Effect of Angle of Attack

The effect of angle of attack on body and wing pressures is examined in this section for the body

alone (configuration 8) and for the baseline wing-body model (configuration 1). Data obtained at some of the intermediate angles of attack are not included on the plots for clarity.

The effect of angle of attack on the body-alone pressures is shown in figure 7 for station 3 at $M_\infty = 1.70$. As would be expected, the pressures on the windward side of the body increase with angle of attack and decrease on the leeward side of the body. At the higher angles of attack, the windward pressures decrease rapidly around the body and reach a minimum at about $\theta = 75^\circ$, or at 285° on the opposite side of the body, before recovering and remaining almost constant over the leeward surface. These minimums are probably due to vortices separating from the body at these locations.

Pressures on the baseline configuration (configuration 1) are shown in figure 8, where the test conditions are the same as those in figure 7. Comparing the body pressures on configuration 1 (fig. 8(a)) with the body-alone pressures of figure 7 shows a very large angle-of-attack effect because of the presence of the wings. At similar angles of attack, the wings cause much higher pressures on the windward side of the body and much lower pressures on the leeward side. Also, the wings cause the windward pressures to be relatively constant compared with the body-alone pressures. Notice that a sharp increase in pressure develops on the body at the higher angles of attack near the leeward meridian for configuration 1. This trend was not seen in the body-alone data.

The pressures on the wing for configuration 1 are shown in figure 8(b). The windward surface pressures increase systematically with angle of attack and are nearly constant in the spanwise direction. On the leeward wing surface, pressure decreases with angle of attack except at 7.17° and 15.19° when an increase occurs on the inboard part of the wing as compared with the outboard part. This pattern is typical of a classic leading-edge vortex on delta wings that was discussed in reference 6.

Effect of Roll Angle

Figure 9 shows the effect of roll angle on the pressures on configuration 1 at station 3 for $M_\infty = 1.70$ and $\alpha \approx 20^\circ$. Note that the body angular coordinate θ is fixed to the body and thus rotates with roll angle ϕ relative to the free-stream cross flow direction. For this reason the body pressures in this figure have been plotted as a function of $\theta + \phi$ so that the data can be compared at the same location on the body relative to the free-stream cross flow direction. (See the sketch in fig. 9(a).)

Figure 9(a) shows that roll angle has a strong effect on the body pressures, but for clarity, only positive roll angles are shown. For the nonsymmetrical roll angles, the maximum body pressures occur near the wing on the windward side, and the minimum pressures occur near the leeward side of that same wing.

Figure 9(b) shows roll angle effects on the wing pressures. Because of the location of the wing pressure orifices, the nonzero roll angle data in this figure are no longer representative of windward and leeward pressures on the same wing. Rather, these data are from the windward side of the lower wing and from the leeward side of the upper wing. Because vertical flow symmetry no longer applies, these data can no longer be used at a given roll angle to generate a complete data plane around the configuration.

This data plane can still be extracted from the test data in this study, however, by combining the results from positive and negative roll angles. A sample of such a combination is shown in figure 9(c) in which data from positive and negative roll angles of 30° have been combined to give a data plane over the complete wing-body combination. These data are from configuration 1 at station 3 for $\alpha \approx 20^\circ$. Note that the body pressures have been included in this figure at their corresponding values of y/S to show how a complete wing-body data plane can be constructed.

Effect of Mach Number

The effect of Mach number is discussed with the aid of figure 10 which contains data from configuration 1 at station 3 for $\alpha \approx 20^\circ$ and $\phi = 0^\circ$. Figure 10(a) shows the effect of body pressures. Even though Mach number has very little effect on the windward side of the body, a large systematic increase in body pressure occurs on the leeward side. At all Mach numbers the pressures increase sharply near the leeward meridian, which in previous discussions was attributed to the presence of the wing.

Figure 10(b) shows a similar trend in the wing pressures; that is, they are almost constant on the windward surface and systematically increase with Mach number on the leeward surface. Notice that the effect of the wing leading-edge vortex decreases with Mach number, as seen by the increase in pressures near the leeward meridian at $y/S = 0.4$ and 0.5 .

Effect of Longitudinal Station

Figure 11 shows the pressures at the three longitudinal stations for configuration 1 at $M_\infty = 1.70$, $\alpha = 19.23^\circ$, and $\phi = 0^\circ$. Figure 11(a) shows that the

pressures on the windward side of the body are nearly constant between stations 2 and 3 but are significantly lower at station 1. On the leeward surface of the body as noted earlier, the increase in pressures near the leeward meridian is seen to continually increase down the length of the body.

Figure 11(b) shows that the pressures on both surfaces of the wing are nearly constant with longitudinal station. The leeward pressures show the progression of the wing leading-edge vortex as it moves downstream over the configuration.

Effect of Wing Vertical Location

Figure 12 shows the effect of the wing vertical location. In this figure the effects of moving the horizontal wing from low to high on the body are examined by comparing data from configurations 1 5 at $M_\infty = 1.70$, $\alpha \approx 20^\circ$, and $\phi = 0^\circ$.

Figure 12(a) shows that the wing vertical location on the body has a very large effect on the body pressures. The wing location essentially acts as a dividing line between the windward and leeward pressure levels for all wing locations. For example, all body pressures for the highest mounted wing (configuration 2) are at the level of the windward pressures, whereas all body pressures for the lowest mounted wing (configuration 5) appear as leeward pressures.

In contrast, figure 12(b) shows that the wing vertical location has a much smaller effect on the wing pressures. On the low-mounted configurations, the pressures on the windward surface are almost constant over the wing span, and some effects of the body can be seen on the inboard part of the windward surfaces for the high-mounted configurations. On the leeward surface of the wing, the largest effect of the wing vertical location is also seen on the inboard part of the wing.

Effect of Wing Angular Orientation

Configurations 6 and 7 are the only wing-body configurations in this study in which the wings are not located in a horizontal plane but extend radially from the body in high- and low-mounted positions. Configurations 3 and 5 have horizontal wings mounted at the same locations as those of configurations 6 and 7, respectively. Therefore, comparisons between the data from configurations 3 and 6 and configurations 5 and 7 show the effect of angular orientation of the wings. These comparisons are made in figures 13 and 14 for $M_\infty = 1.70$ at station 3 for $\alpha \approx 20^\circ$.

Figure 13 shows the effect of wing angular orientation for the high-mounted wings (configurations 3 and 6). The effect on the body (fig. 13(a)) is confined primarily to the windward side where the horizontal wings are seen to produce the higher pressures. Therefore, rotating the wings from the horizontal to the radial position for these high-mounted wings acts to relieve the pressures on the windward side of the body but has little effect on the leeward pressures. A similar relieving effect is seen on the windward surface of the wings (fig. 13(b)). The closer proximity of the leading-edge vortex to the wing surface for the horizontal wing results in significantly lower pressures on the leeward surface of that wing.

Figure 14 shows the effect of wing angular orientation for the low-mounted wings (configurations 4 and 7). In contrast to the high-mounted case, figure 14(a) shows a large effect on the body pressures on the leeward surface, with the horizontal wings creating the lower pressures. The pressures for both wing orientations are nearly constant on the windward body surface, with the radially mounted wing producing the higher pressures. In fact, for the same angle of attack, the channeling effect of the wings on configuration 7 produced the highest body pressures measured on any configuration in this study.

Figure 14(b) shows that the pressures on the windward surface of the wings of both configurations are almost constant in the spanwise direction, again with the radially mounted wing producing the higher pressures. The pressures on the outboard part of the leeward wing surface are similar for the two configurations, but they diverge on the inboard part because of the closer proximity of the leading-edge vortex to the radially mounted wing surface.

Effect of Wing-Body Juncture

All body pressures presented thus far, except for those illustrating roll angle effects in figure 9(c), have been plotted as a function of angular location on the body (θ), whereas the wing pressures have been plotted as a function of the spanwise dimension parameter (y/S). In order to compare wing and body pressures directly in the vicinity of the wing-body juncture, figure 15 was prepared in which the location of the body pressure data was transformed from the angular location (θ) to the corresponding value of the spanwise parameter (y/S). Data are presented in figure 15 for all wing-body configurations investigated in this study at $M_\infty = 1.70$, station 3, $\alpha \approx 20^\circ$, and $\phi = 0^\circ$.

Figure 15(a) presents data from the baseline model (configuration 1). The pressures over the

windward surface are seen to be virtually constant over the span of the entire wing-body combination. The pressures on the leeward side, however, are much higher on the body than on the wing except in the vicinity of the wing-body juncture where a smooth transition takes place.

The "looping" effect in the data from the other configurations, seen in figures 15(b)–15(g), is the result of the double values of the y/S parameter when the wing is not located on the body centerline. The pressures over the entire windward wing-body combination were virtually constant in the spanwise direction for all configurations except configuration 6 (fig. 15(b)) because of the pressure-relieving effect noted earlier for that configuration. Note that no leeward body pressures exist for the highest mounted configuration (fig. 15(b)) and, conversely, no windward body pressures exist for the lowest mounted configuration (fig. 15(e)).

Concluding Remarks

An experimental study has been performed at supersonic speeds to obtain spanwise pressure distributions on an axisymmetric-body delta wing configuration in which the wing vertical and angular locations on the body were systematically varied. Pressure coefficient data for the entire investigation are listed in tabular form. Selected samples from these data are presented graphically to illustrate the effects of angle of attack, roll angle, Mach number, longitudinal station, wing vertical location, wing angular orientation, and wing-body juncture.

The vertical location of the wing on the body was found to have a very strong effect on the body

pressures. For a given angle of attack at a roll angle of 0° , the pressures were virtually constant in the spanwise direction across the windward surfaces of the wing-body combination. Pressure-relieving, channeling, and vortex effects were noted in the data.

NASA Langley Research Center
Hampton, VA 23681-0001
February 23, 1993

References

1. Jenn, A. A.; and Nelson, H. F.: Wing Vertical Position Effects on Lift for Supersonic Delta Wing Missiles. *J. Spacecr. & Rockets*, vol. 26, no. 4, July–Aug. 1989, pp. 210–216.
2. Blair, A. B., Jr.: *Effect of Wing Location and Strakes on Stability and Control Characteristics of a Monoplanar Circular Missile With Low-Profile Tail Fins at Supersonic Speeds*. NASA TM-81878, 1980.
3. Jackson, Charlie M., Jr.; Corlett, William A.; and Monta, William J.: *Description and Calibration of the Langley Unitary Plan Wind Tunnel*. NASA TP-1905, 1981.
4. Stallings, Robert L., Jr.; and Lamb, Milton: *Effects of Roughness Size on the Position of Boundary-Layer Transition and on the Aerodynamic Characteristics of a 55° Swept Delta Wing at Supersonic Speeds*. NASA TP-1027, 1977.
5. Fulton, Patsy S.: *Wind Tunnel Pressure Study and Euler Code Validation of a Missile Configuration With 77° Swept Delta Wings at Supersonic Speeds*. NASA TM-101531, 1988.
6. Miller, David S.; and Wood, Richard M.: *Lee-Side Flow Over Delta Wings at Supersonic Speeds*. NASA TP-2430, 1985.

Table 1. Spanwise Locations of Wing Orifices

Station	y , in.	y/S	Ray
1	0.241	0.050	1
	.482	.100	2
	.723	.150	3
	.964	.200	4
	1.205	.250	5
	1.446	.300	6
	1.687	.350	7
	1.929	.400	8
	2.049	.425	9
	2.170	.450	10
2	0.361	0.075	1
	.722	.150	2
	1.083	.225	3
	1.444	.300	4
	1.806	.375	5
	2.167	.450	6
	2.528	.524	7
	2.889	.599	8
	3.070	.637	9
	3.250	.674	10
3	0.914	0.190	2
	1.321	.274	3
	1.829	.379	4
	2.281	.473	5
	2.743	.569	6
	3.200	.664	7
	3.657	.759	8
	3.886	.806	9
	4.114	.854	10

Table 2. Arrangement of Tables 3-10

(a) Configuration 1 (table 3)

Mach number	Part of table 3 for roll angle, ϕ , of—						
	0°	30°	60°	90°	-30°	-60°	-90°
1.70	(a)	(e)	(i)	(m)	(q)	(u)	(y)
2.16	(b)	(f)	(j)	(n)	(r)	(v)	(z)
2.40	(c)	(g)	(k)	(o)	(s)	(w)	(aa)
2.86	(d)	(h)	(l)	(p)	(t)	(x)	(bb)

(b) Configurations 2-8 (tables 4-10) with $\phi = 0^\circ$

Mach number	Part found in table—						
	4	5	6	7	8	9	10
1.70	(a)	(a)	(a)	(a)	(a)	(a)	(a)
2.16	(b)	(b)	(b)	(b)	(b)	(b)	(b)
2.40	(c)	(c)	(c)	(c)	(c)	(c)	(c)
2.86	(d)	(d)	(d)	(d)	(d)	(d)	(d)

Table 3. Configuration 1

(a) $M_\infty = 1.70$; $\phi = 0^\circ$; station 1

THETA, DEG	CP FOR ALPHA, DEG =							
	-4.83	-.84	3.16	7.17	11.20	15.19	19.23	23.21
0								
15	-.021	-.004	.018	.050	.082	.108	.166	.232
30	-.029	-.008	.017	.051	.085	.121	.176	.237
45	-.031	-.006	.024	.062	.101	.151	.203	.274
60	-.036	-.008	.025	.067	.110	.161	.218	.296
75	-.033	-.004	.029	.062	.078	.140	.193	.265
90								
105	.037	.005	-.029	-.076	-.164	-.237	-.290	-.355
120	.034	.003	-.027	-.068	-.131	-.251	-.279	-.356
135	.036	.009	-.016	-.052	-.104	-.234	-.229	-.265
BODY 150	.034	.006	-.017	-.051	-.134	-.242	-.242	-.248
165	.034	.007	-.015	-.039	-.074	-.088	-.186	-.215
180	.032	.006	-.014	-.029	-.045	-.050	-.137	-.175
195	.035	.009	-.013	-.035	-.061	-.072	-.169	-.191
210	.040	.012	-.013	-.045	-.128	-.210	-.220	-.229
225	.045	.012	-.016	-.050	-.108	-.252	-.213	-.258
240	.049	.013	-.020	-.055	-.104	-.221	-.245	-.325
255	.047	.011	-.025	-.061	-.130	-.195	-.280	-.344
270								
285	-.047	-.012	.020	.054	.072	.115	.170	.238
300	-.045	-.011	.017	.055	.099	.152	.211	.288
315	-.038	-.009	.015	.050	.088	.139	.195	.269
330	-.032	-.007	.015	.045	.078	.114	.174	.239
345	-.026	-.006	.016	.045	.077	.104	.160	.237
Y/S	CP FOR ALPHA, DEG =							
	-4.83	-.84	3.16	7.17	11.20	15.19	19.23	23.21
.050								
.100								
.150								
.200								
WINDWARD .250								
WING .300	-.049	-.016	.021	.064	.119	.165	.208	.274
.350	-.056	-.017	.024	.072	.134	.205	.273	.356
.400	-.231	-.021	.025	.074	.138	.215	.292	.388
.425								
.450	-.197	-.055	.036	.084	.138	.203	.267	.349
.450	.066	.011	-.135	-.229	-.296	-.299	-.349	-.360
.425	.058	.008	-.152	-.233	-.298	-.315	-.361	-.370
.400	.055	.007	-.093	-.259	-.311	-.335	-.374	-.367
.350	.050	.006	-.024	-.119	-.244	-.233	-.282	-.301
LEEWARD .300	.041	.003	-.032	-.075	-.138	-.207	-.260	-.358
WING .250								
.200								
.150								
.100								
.050								

Table 3. Continued

(a) Continued; station 2

	THETA, DEG	CP FOR ALPHA, DEG =							
		-4.83	-.84	3.16	7.17	11.20	15.19	19.23	23.21
BODY	0	-.038	-.007	.024	.070	.133	.195	.276	.365
	15	-.039	-.007	.025	.071	.136	.196	.275	.366
	30	-.043	-.007	.026	.074	.136	.198	.276	.364
	45	-.044	-.007	.028	.078	.137	.204	.279	.369
	60	-.045	-.007	.030	.079	.140	.207	.279	.371
	75	-.045	-.007	.032	.080	.130	.180	.243	.336
	90								
	105	.050	.014	-.016	-.056	-.118	-.237	-.297	-.390
	120	.046	.009	-.022	-.065	-.157	-.279	-.334	-.393
	135	.047	.010	-.020	-.062	-.151	-.255	-.362	-.400
	150	.047	.011	-.018	-.061	-.111	-.162	-.307	-.341
	165	.045	.008	-.018	-.049	-.061	-.071	-.166	-.219
	180	.044	.010	-.017	-.041	-.053	-.055	-.088	-.136
	195	.043	.008	-.020	-.048	-.058	-.066	-.144	-.183
	210	.045	.008	-.020	-.062	-.107	-.141	-.277	-.304
	225	.049	.010	-.018	-.057	-.146	-.240	-.336	-.387
	240	.045	.007	-.022	-.058	-.126	-.258	-.287	-.371
	255	.044	.007	-.024	-.058	-.113	-.206	-.265	-.375
	270								
	285	-.047	-.010	.028	.071	.116	.176	.245	.330
300	-.047	-.008	.028	.074	.129	.198	.274	.360	
315	-.046	-.007	.027	.072	.128	.196	.273	.355	
330	-.045	-.008	.025	.069	.127	.190	.274	.347	
345	-.039	-.005	.026	.071	.132	.194	.280	.357	
	Y/S	CP FOR ALPHA, DEG =							
		-4.83	-.84	3.16	7.17	11.20	15.19	19.23	23.21
WINDWARD WING	.075								
	.150								
	.225								
	.300	-.045	-.008	.031	.079	.129	.196	.268	.349
	.375	-.041	-.005	.036	.088	.144	.215	.288	.371
	.450								
	.524	-.137	-.004	.037	.092	.154	.228	.302	.387
	.599								
	.637								
	.674	-.167	-.052	.047	.095	.155	.215	.276	.345
LEEWARD WING	.674	.071	.019	-.103	-.197	-.267	-.304	-.311	-.346
	.637	.068	.020	-.121	-.202	-.264	-.298	-.319	-.353
	.599	.065	.018	-.142	-.205	-.268	-.304	-.334	-.361
	.524	.059	.014	-.006	-.265	-.324	-.358	-.355	-.368
	.450	.056	.013	-.013	-.094	-.254	-.307	-.309	-.336
	.375	.054	.012	-.017	-.057	-.153	-.194	-.267	-.316
	.300	.051	.010	-.020	-.057	-.116	-.249	-.295	-.386
	.225								
	.150								
	.075								

Table 3. Continued

(a) Concluded; station 3

THETA, DEG	CP FOR ALPHA, DEG =							
	-4.83	-.84	3.16	7.17	11.20	15.19	19.23	23.21
0	-.034	-.004	.031	.076	.131	.202	.287	.385
15	-.034	-.002	.032	.078	.133	.205	.290	.386
30	-.041	-.005	.030	.077	.132	.205	.287	.376
45	-.043	-.007	.029	.076	.132	.207	.286	.368
60	-.046	-.009	.027	.075	.131	.205	.281	.356
75	-.048	-.010	.029	.076	.127	.191	.262	.328
90								
105	.057	.017	-.017	-.053	-.098	-.182	-.349	-.404
120	.054	.014	-.019	-.056	-.126	-.222	-.335	-.402
135	.057	.016	-.017	-.058	-.110	-.217	-.339	-.401
BODY 150	.058	.017	-.018	-.054	-.083	-.157	-.274	-.356
165	.053	.017	-.018	-.047	-.080	-.131	-.124	-.209
180	.053	.018	-.016	-.044	-.077	-.122	-.055	-.105
195	.054	.018	-.015	-.045	-.072	-.127	-.102	-.165
210	.053	.016	-.018	-.057	-.075	-.150	-.253	-.315
225	.052	.014	-.019	-.059	-.107	-.200	-.324	-.386
240	.049	.011	-.022	-.059	-.127	-.211	-.316	-.381
255	.047	.007	-.027	-.065	-.113	-.172	-.341	-.389
270								
285	-.043	-.007	.028	.077	.136	.194	.270	.364
300	-.046	-.009	.026	.074	.136	.201	.281	.375
315	-.040	-.004	.031	.081	.141	.207	.288	.382
330	-.040	-.005	.028	.077	.133	.202	.282	.375
345	-.036	-.004	.029	.076	.131	.202	.284	.380
Y/S	CP FOR ALPHA, DEG =							
	-4.83	-.84	3.16	7.17	11.20	15.19	19.23	23.21
.190								
.274	-.043	-.007	.028	.078	.139	.202	.277	.370
.379	-.042	-.006	.030	.081	.143	.207	.282	.378
.473	-.040	-.008	.029	.080	.143	.217	.300	.398
WINDWARD .569								
WING .664	-.179	-.006	.033	.088	.144	.213	.295	.384
.759	-.172	-.024	.037	.089	.147	.211	.286	.372
.806	-.158	-.035	.042	.091	.148	.209	.281	.364
.854	-.154	-.043	.047	.093	.148	.204	.272	.349
.854	.075	.024	-.096	-.194	-.264	-.317	-.319	-.342
.806	.073	.025	-.110	-.198	-.264	-.315	-.315	-.341
.759	.068	.022	-.142	-.197	-.260	-.318	-.321	-.350
LEEWARD .664	.065	.021	-.013	-.282	-.291	-.333	-.341	-.361
WING .569	.059	.017	-.013	-.122	-.302	-.361	-.336	-.352
.473	.058	.015	-.020	-.059	-.194	-.264	-.280	-.371
.379	.056	.014	-.022	-.055	-.117	-.153	-.351	-.421
.274	.056	.015	-.020	-.054	-.099	-.186	-.356	-.413
.190								

Table 3. Continued

(b) $M_\infty = 2.16; \phi = 0^\circ$; station 1

	THETA, DEG	CP FOR ALPHA, DEG =								
		-3.11	.93	4.96	8.97	12.92	16.92	20.97	24.02	
BODY	0									
	15	-.014	.001	.016	.026	.051	.099	.168	.224	
	30	-.015	.004	.025	.049	.066	.093	.145	.192	
	45	-.018	.006	.033	.068	.099	.145	.203	.260	
	60	-.023	.006	.039	.076	.112	.167	.233	.294	
	75	-.026	.007	.040	.050	.095	.150	.210	.263	
	90									
	105	.023	-.006	-.040	-.100	-.172	-.208	-.232	-.240	
	120	.018	-.007	-.036	-.079	-.145	-.193	-.226	-.237	
	135	.018	-.002	-.025	-.060	-.137	-.149	-.173	-.184	
	150	.011	-.005	-.026	-.070	-.165	-.166	-.176	-.189	
	165	.007	-.006	-.023	-.050	-.061	-.136	-.149	-.158	
	180	.007	-.004	-.019	-.024	-.034	-.097	-.114	-.122	
	195	.011	-.002	-.018	-.038	-.047	-.120	-.128	-.142	
	210	.017	-.001	-.022	-.068	-.147	-.160	-.155	-.187	
	225	.025	.001	-.024	-.063	-.152	-.153	-.172	-.189	
	240	.026	-.001	-.031	-.066	-.137	-.179	-.208	-.220	
	255	.032	.001	-.030	-.072	-.146	-.198	-.225	-.234	
	270									
	285	-.034	-.001	.030	.047	.073	.126	.189	.245	
300	-.030	-.002	.027	.063	.101	.156	.227	.291		
315	-.024	-.001	.024	.055	.092	.140	.210	.270		
330	-.020	-.001	.017	.038	.064	.091	.156	.205		
345	-.016	-.001	.014	.025	.051	.096	.165	.220		
WINDWARD WING	Y/S									
		-3.11	.93	4.96	8.97	12.92	16.92	20.97	24.02	
	.050									
	.100									
	.150									
	.200									
	.250									
	.300	-.033	.000	.037	.083	.122	.171	.234	.290	
	.350	-.029	.000	.041	.092	.148	.221	.304	.373	
	.400	-.143	.000	.045	.096	.152	.232	.320	.400	
	.425									
	.450	-.124	.006	.055	.104	.150	.221	.299	.372	
	LEEWARD WING	.450	.039	-.029	-.147	-.206	-.213	-.221	-.232	-.240
		.425	.038	-.006	-.152	-.204	-.214	-.220	-.232	-.239
		.400	.032	-.010	-.164	-.208	-.224	-.230	-.237	-.243
		.350	.029	-.008	-.053	-.171	-.174	-.186	-.201	-.211
		.300	.024	-.009	-.041	-.090	-.155	-.215	-.240	-.247
		.250								
		.200								
		.150								
.100										
.050										

Table 3. Continued

(b) Continued; station 2

THETA, DEG	CP FOR ALPHA, DEG =							
	-3.11	.93	4.96	8.97	12.92	16.92	20.97	24.02
0	-.023	.004	.035	.076	.127	.200	.297	.383
15	-.024	.005	.037	.078	.128	.202	.299	.383
30	-.027	.002	.035	.080	.127	.198	.295	.378
45	-.030	.002	.036	.081	.128	.201	.302	.386
60	-.034	-.001	.035	.079	.127	.200	.303	.387
75	-.034	.001	.041	.083	.112	.173	.268	.347
90								
105	.022	-.009	-.037	-.077	-.163	-.210	-.226	-.223
120	.025	-.005	-.033	-.082	-.175	-.217	-.219	-.214
135	.024	-.004	-.034	-.083	-.167	-.226	-.228	-.222
150	.024	-.003	-.035	-.079	-.121	-.206	-.203	-.188
165	.025	-.001	-.028	-.043	-.049	-.106	-.128	-.108
180	.022	-.004	-.027	-.038	-.041	-.053	-.081	-.065
195	.024	-.002	-.027	-.041	-.044	-.095	-.101	-.097
210	.022	-.005	-.034	-.077	-.106	-.190	-.174	-.173
225	.020	-.008	-.038	-.086	-.167	-.226	-.227	-.221
240	.020	-.009	-.037	-.075	-.168	-.211	-.216	-.214
255	.020	-.011	-.037	-.069	-.143	-.196	-.217	-.216
270								
285	-.027	.007	.040	.078	.110	.169	.266	.347
300	-.028	.005	.037	.078	.124	.193	.295	.381
315	-.026	.006	.037	.079	.128	.198	.298	.384
330	-.025	.004	.036	.075	.127	.195	.291	.376
345	-.023	.003	.035	.073	.126	.196	.292	.378
Y/S	CP FOR ALPHA, DEG =							
	-3.11	.93	4.96	8.97	12.92	16.92	20.97	24.02
.075								
.150								
.225								
.300	-.029	.005	.041	.087	.127	.189	.287	.371
.375	-.027	.007	.045	.092	.140	.209	.310	.394
.450								
.524	-.061	.010	.050	.095	.148	.221	.328	.419
.599								
.637								
.674	-.103	.007	.056	.100	.150	.208	.304	.389
.674	.040	-.022	-.121	-.169	-.211	-.216	-.210	-.198
.637	.038	-.011	-.132	-.186	-.212	-.218	-.210	-.197
.599	.035	-.008	-.137	-.182	-.211	-.224	-.213	-.200
.524	.034	-.003	-.148	-.195	-.221	-.224	-.208	-.193
.450	.028	-.006	-.037	-.167	-.208	-.197	-.197	-.189
.375	.025	-.005	-.034	-.094	-.139	-.175	-.193	-.194
.300	.026	-.005	-.032	-.066	-.157	-.202	-.219	-.217
.225								
.150								
.075								

Table 3. Continued

(b) Concluded; station 3

THETA, DEG	CP FOR ALPHA, DEG =							
	-3.11	.93	4.96	8.97	12.92	16.92	20.97	24.02
0	-.026	.000	.037	.081	.140	.205	.294	.373
15	-.026	.000	.037	.084	.142	.208	.297	.378
30	-.031	-.004	.033	.081	.138	.205	.292	.369
45	-.031	-.002	.036	.083	.141	.211	.299	.374
60	-.033	-.003	.035	.080	.138	.212	.301	.373
75	-.032	-.001	.037	.083	.133	.201	.284	.349
90								
105	.027	-.008	-.035	-.069	-.138	-.228	-.251	-.250
120	.025	-.007	-.036	-.081	-.159	-.227	-.250	-.251
135	.025	-.007	-.036	-.079	-.139	-.226	-.249	-.251
BODY 150	.025	-.008	-.035	-.063	-.084	-.194	-.225	-.226
165	.025	-.008	-.032	-.049	-.067	-.085	-.136	-.146
180	.025	-.009	-.031	-.048	-.065	-.029	-.061	-.088
195	.025	-.007	-.031	-.047	-.065	-.070	-.100	-.129
210	.026	-.006	-.034	-.054	-.074	-.176	-.195	-.214
225	.023	-.008	-.036	-.076	-.129	-.213	-.243	-.254
240	.021	-.011	-.038	-.077	-.152	-.214	-.239	-.250
255	.022	-.011	-.039	-.071	-.127	-.220	-.241	-.251
270								
285	-.028	.002	.039	.083	.134	.199	.284	.353
300	-.029	.001	.037	.083	.142	.210	.298	.370
315	-.028	.002	.037	.085	.145	.210	.297	.370
330	-.027	.002	.037	.083	.144	.207	.293	.368
345	-.024	.003	.039	.083	.142	.206	.294	.371
Y/S	CP FOR ALPHA, DEG =							
	-3.11	.93	4.96	8.97	12.92	16.92	20.97	24.02
.190								
.274	-.028	.003	.039	.087	.145	.212	.296	.365
.379	-.029	.001	.037	.087	.145	.211	.296	.362
.473	-.026	.005	.043	.094	.157	.231	.323	.394
WINDWARD .569								
WING .664	-.099	.004	.048	.097	.158	.229	.315	.387
.759	-.121	.002	.049	.098	.155	.228	.308	.377
.806	-.104	.005	.053	.102	.157	.228	.305	.373
.854	-.099	.005	.056	.104	.157	.222	.296	.366
.854	.040	-.021	-.118	-.159	-.199	-.206	-.220	-.227
.806	.036	-.018	-.129	-.183	-.216	-.212	-.227	-.235
.759	.036	-.013	-.129	-.179	-.208	-.210	-.227	-.233
.664	.032	-.009	-.166	-.190	-.216	-.230	-.238	-.238
LEEWARD .569	.028	-.011	-.044	-.200	-.238	-.216	-.230	-.232
WING .473	.028	-.009	-.031	-.114	-.185	-.186	-.220	-.241
.379	.026	-.010	-.036	-.077	-.113	-.233	-.257	-.260
.274	.026	-.007	-.035	-.067	-.135	-.234	-.254	-.250
.190								

Table 3. Continued

(c) $M_\infty = 2.40$; $\phi = 0^\circ$; station 1

THETA, DEG	CP FOR ALPHA, DEG =							
	-3.99	.02	4.04	8.01	12.03	16.01	20.02	24.04
0								
15	-.007	.008	.019	.028	.061	.109	.173	.254
30	-.012	.006	.024	.041	.061	.087	.136	.198
45	-.015	.008	.032	.062	.097	.133	.187	.252
60	-.021	.008	.037	.072	.113	.157	.221	.297
75	-.022	.011	.042	.056	.101	.146	.206	.276
90								
105	.036	.004	-.028	-.081	-.147	-.176	-.192	-.204
120	.029	-.001	-.028	-.065	-.124	-.162	-.181	-.194
135	.029	.004	-.017	-.047	-.114	-.132	-.144	-.153
BODY 150	.021	.002	-.014	-.049	-.130	-.137	-.144	-.157
165	.010	-.002	-.013	-.040	-.062	-.119	-.131	-.144
180	.007	.000	-.010	-.019	-.030	-.085	-.102	-.119
195	.012	.003	-.008	-.027	-.041	-.103	-.117	-.138
210	.025	.007	-.007	-.044	-.119	-.136	-.142	-.159
225	.035	.010	-.010	-.045	-.122	-.130	-.142	-.155
240	.039	.009	-.016	-.050	-.112	-.145	-.165	-.180
255	.044	.014	-.014	-.052	-.125	-.165	-.183	-.199
270								
285	-.031	.000	.031	.050	.076	.121	.177	.253
300	-.026	.002	.028	.062	.098	.147	.212	.296
315	-.022	.001	.022	.050	.081	.125	.185	.262
330	-.014	.004	.019	.036	.050	.082	.128	.196
345	-.010	.005	.014	.024	.053	.101	.163	.249
Y/S	CP FOR ALPHA, DEG =							
	-3.99	.02	4.04	8.01	12.03	16.01	20.02	24.04
.050								
.100								
.150								
.200								
WINDWARD .250								
WING .300	-.030	.000	.035	.080	.118	.161	.220	.294
.350	-.039	.000	.039	.089	.147	.210	.289	.384
.400	-.131	-.001	.042	.093	.152	.218	.304	.409
.425								
.450	-.116	-.019	.049	.099	.149	.210	.283	.380
.450	.055	.000	-.112	-.167	-.176	-.185	-.197	-.208
.425	.055	.007	-.116	-.169	-.175	-.183	-.195	-.207
.400	.052	.009	-.123	-.169	-.179	-.186	-.197	-.204
.350	.046	.005	-.030	-.142	-.152	-.158	-.173	-.189
LEEWARD .300	.040	.002	-.029	-.072	-.138	-.180	-.194	-.207
WING .250								
.200								
.150								
.100								
.050								

Table 3. Continued

(c) Continued; station 2

THETA, DEG	CP FOR ALPHA, DEG =							
	-3.99	.02	4.04	8.01	12.03	16.01	20.02	24.04
0	-.013	.010	.037	.077	.130	.188	.265	.373
15	-.014	.011	.039	.080	.133	.189	.268	.372
30	-.014	.013	.043	.084	.137	.192	.272	.373
45	-.016	.012	.042	.084	.136	.194	.277	.379
60	-.017	.012	.044	.083	.136	.195	.277	.379
75	-.019	.010	.044	.084	.120	.166	.239	.333
90								
105	.043	.012	-.013	-.052	-.128	-.165	-.187	-.197
120	.036	.007	-.019	-.062	-.145	-.177	-.192	-.203
135	.041	.012	-.014	-.055	-.137	-.180	-.193	-.202
BODY 150	.043	.014	-.011	-.053	-.108	-.163	-.175	-.181
165	.040	.013	-.010	-.033	-.044	-.094	-.125	-.131
180	.043	.015	-.007	-.021	-.027	-.046	-.088	-.093
195	.039	.011	-.012	-.028	-.035	-.083	-.111	-.126
210	.042	.014	-.011	-.050	-.082	-.152	-.157	-.172
225	.041	.012	-.013	-.054	-.131	-.176	-.189	-.198
240	.042	.014	-.013	-.047	-.125	-.166	-.178	-.191
255	.042	.012	-.015	-.046	-.111	-.153	-.180	-.193
270								
285	-.023	.006	.038	.072	.109	.157	.234	.330
300	-.019	.010	.040	.078	.126	.184	.270	.372
315	-.020	.009	.038	.077	.127	.186	.270	.372
330	-.019	.008	.036	.075	.124	.182	.262	.362
345	-.011	.013	.040	.079	.130	.189	.266	.371
Y/S								
	-3.99	.02	4.04	8.01	12.03	16.01	20.02	24.04
.075								
.150								
.225								
WINDWARD .300	-.016	.012	.045	.088	.135	.193	.275	.374
WING .375	-.014	.013	.047	.091	.145	.206	.289	.393
.450								
.524	-.105	.009	.046	.092	.148	.217	.300	.411
.599								
.637								
.674	-.092	-.003	.056	.103	.153	.216	.289	.385
.674	.064	.012	-.088	-.128	-.161	-.170	-.183	-.189
.637	.059	.013	-.093	-.144	-.165	-.172	-.183	-.190
.599	.056	.013	-.099	-.145	-.164	-.175	-.184	-.191
.524	.046	.009	-.102	-.159	-.177	-.184	-.192	-.197
LEEWARD .450	.049	.015	-.006	-.129	-.158	-.153	-.172	-.179
WING .375	.048	.015	-.009	-.063	-.108	-.138	-.163	-.175
.300	.041	.008	-.016	-.051	-.131	-.167	-.191	-.201
.225								
.150								
.075								

Table 3. Continued

(c) Concluded; station 3

THETA, DEG	CP FOR ALPHA, DEG =							
	-3.99	.02	4.04	8.01	12.03	16.01	20.02	24.04
0	-.019	.004	.034	.076	.127	.195	.281	.389
15	-.018	.007	.037	.079	.134	.198	.287	.392
30	-.023	.004	.034	.077	.133	.196	.285	.387
45	-.024	.003	.034	.077	.135	.199	.287	.389
60	-.025	.002	.034	.074	.133	.200	.287	.390
75	-.021	.006	.040	.086	.137	.193	.274	.371
90								
105	.045	.012	-.016	-.048	-.121	-.185	-.199	-.202
120	.039	.007	-.020	-.059	-.139	-.188	-.202	-.207
135	.039	.007	-.020	-.061	-.128	-.186	-.202	-.207
BODY 150	.040	.009	-.017	-.051	-.076	-.165	-.183	-.191
165	.037	.007	-.018	-.040	-.052	-.084	-.122	-.140
180	.040	.009	-.014	-.033	-.047	-.029	-.070	-.099
195	.040	.008	-.015	-.034	-.049	-.062	-.099	-.130
210	.037	.006	-.019	-.048	-.065	-.153	-.168	-.189
225	.037	.006	-.020	-.060	-.109	-.180	-.200	-.209
240	.038	.007	-.019	-.055	-.123	-.175	-.193	-.203
255	.040	.005	-.023	-.054	-.109	-.181	-.197	-.206
270								
285	-.021	.005	.037	.076	.125	.185	.266	.367
300	-.025	.002	.033	.073	.128	.195	.279	.384
315	-.016	.012	.042	.084	.137	.205	.289	.394
330	-.022	.005	.035	.076	.127	.196	.279	.383
345	-.022	.002	.032	.073	.123	.193	.277	.383
Y/S	CP FOR ALPHA, DEG =							
	-3.99	.02	4.04	8.01	12.03	16.01	20.02	24.04
.190								
.274	-.023	.003	.034	.076	.132	.196	.277	.380
.379	-.020	.006	.039	.084	.140	.203	.283	.386
.473	-.021	.002	.037	.085	.146	.214	.302	.412
WINDWARD 569								
WING 664	-.122	.005	.044	.091	.147	.216	.297	.403
.759	-.101	.004	.047	.095	.150	.215	.294	.397
.806	-.097	.001	.049	.097	.150	.213	.290	.391
.854	-.093	-.005	.051	.099	.150	.211	.283	.382
.854	.059	.006	-.087	-.128	-.163	-.177	-.191	-.198
.806	.061	.013	-.086	-.135	-.170	-.172	-.187	-.194
.759	.055	.011	-.096	-.146	-.171	-.176	-.190	-.197
LEEWARD 664	.054	.013	-.109	-.149	-.175	-.187	-.195	-.200
WING 569	.050	.013	-.010	-.158	-.186	-.174	-.186	-.193
.473	.042	.006	-.016	-.090	-.159	-.158	-.183	-.196
.379	.040	.006	-.020	-.056	-.109	-.179	-.203	-.212
.274	.040	.007	-.020	-.049	-.126	-.192	-.207	-.210
.190								

Table 3. Continued

(d) $M_{\infty} = 2.86; \phi = 0^{\circ}$; station 1

THETA, DEG	CP FOR ALPHA, DEG =							
	-3.96	.03	4.05	7.98	12.00	15.98	20.02	23.99
0								
15	-.001	.008	.015	.028	.063	.110	.170	.243
30	-.002	.012	.026	.035	.053	.089	.137	.197
45	-.007	.012	.034	.054	.079	.112	.152	.206
60	-.014	.010	.037	.064	.098	.141	.198	.266
75	-.017	.011	.039	.052	.089	.132	.187	.254
90								
105	.039	.011	-.019	-.063	-.105	-.125	-.136	-.146
120	.036	.010	-.016	-.044	-.083	-.105	-.118	-.133
135	.035	.014	-.006	-.030	-.079	-.086	-.092	-.098
BODY 150	.022	.007	-.007	-.033	-.089	-.093	-.099	-.104
165	.014	.004	-.005	-.024	-.047	-.087	-.094	-.105
180	.013	.006	-.002	-.008	-.023	-.062	-.078	-.085
195	.017	.009	-.001	-.015	-.034	-.076	-.089	-.095
210	.024	.009	-.005	-.032	-.091	-.095	-.102	-.105
225	.036	.013	-.008	-.033	-.085	-.091	-.098	-.105
240	.040	.012	-.014	-.041	-.077	-.099	-.111	-.123
255	.041	.015	-.016	-.045	-.097	-.124	-.135	-.144
270								
285	-.025	.003	.031	.047	.075	.113	.167	.226
300	-.022	.003	.027	.053	.087	.129	.189	.257
315	-.011	.008	.027	.047	.075	.108	.158	.222
330	-.008	.006	.018	.028	.045	.075	.123	.179
345	-.002	.007	.014	.027	.061	.106	.166	.237
Y/S	CP FOR ALPHA, DEG =							
	-3.96	.03	4.05	7.98	12.00	15.98	20.02	23.99
.050								
.100								
.150								
.200								
WINDWARD .250								
WING .300	-.023	.004	.037	.073	.109	.146	.201	.263
.350	-.052	.004	.040	.082	.136	.193	.270	.354
.400	-.098	.000	.042	.085	.141	.203	.285	.378
.425								
.450	-.083	-.010	.051	.095	.146	.202	.275	.360
.450	.058	.007	-.084	-.122	-.130	-.140	-.145	-.150
.425	.056	.010	-.084	-.125	-.127	-.136	-.142	-.148
.400	.049	.005	-.094	-.131	-.134	-.144	-.150	-.153
.350	.045	.007	-.036	-.121	-.119	-.127	-.134	-.145
LEEWARD .300	.043	.008	-.021	-.057	-.101	-.128	-.140	-.148
WING .250								
.200								
.150								
.100								
.050								

Table 3. Continued

(d) Continued; station 2

	THETA, DEG	CP FOR ALPHA, DEG =							
		-3.96	.03	4.05	7.98	12.00	15.98	20.02	23.99
BODY	0	-.001	.014	.038	.069	.115	.169	.242	.328
	15	-.002	.016	.039	.071	.118	.172	.243	.328
	30	-.008	.012	.037	.070	.117	.173	.244	.328
	45	-.008	.012	.038	.072	.120	.178	.251	.339
	60	-.011	.008	.035	.068	.116	.176	.250	.339
	75	-.007	.011	.041	.074	.108	.156	.219	.298
	90								
	105	.035	.008	-.017	-.049	-.108	-.127	-.140	-.150
	120	.040	.014	-.012	-.045	-.105	-.123	-.134	-.143
	135	.039	.013	-.012	-.043	-.111	-.129	-.137	-.143
	150	.038	.012	-.012	-.045	-.098	-.124	-.128	-.136
	165	.041	.014	-.008	-.024	-.041	-.077	-.091	-.104
	180	.038	.010	-.009	-.018	-.030	-.054	-.077	-.083
	195	.041	.013	-.008	-.020	-.036	-.068	-.088	-.098
	210	.039	.011	-.012	-.042	-.087	-.114	-.122	-.129
	225	.035	.006	-.017	-.046	-.109	-.129	-.140	-.145
	240	.035	.008	-.016	-.041	-.102	-.121	-.134	-.143
	255	.038	.008	-.017	-.041	-.097	-.117	-.132	-.141
	270								
	285	-.007	.013	.040	.069	.105	.152	.217	.299
	300	-.010	.011	.036	.067	.114	.170	.243	.333
	315	-.008	.014	.038	.070	.117	.173	.246	.335
	330	-.007	.013	.036	.068	.113	.167	.239	.323
345	-.004	.013	.036	.067	.112	.166	.238	.323	
	Y/S	CP FOR ALPHA, DEG =							
		-3.96	.03	4.05	7.98	12.00	15.98	20.02	23.99
WINDWARD WING	.075								
	.150								
	.225								
	.300	-.008	.011	.040	.077	.124	.179	.252	.339
	.375	-.005	.011	.042	.081	.133	.193	.269	.360
	.450								
	.524	-.093	.012	.046	.088	.144	.207	.289	.387
	.599								
	.637								
	.674	-.078	-.014	.055	.098	.149	.205	.280	.367
LEEWARD WING	.674	.060	.005	-.080	-.105	-.124	-.137	-.144	-.147
	.637	.056	.010	-.078	-.107	-.126	-.135	-.142	-.147
	.599	.053	.011	-.082	-.116	-.126	-.136	-.143	-.147
	.524	.051	.014	-.085	-.113	-.124	-.134	-.141	-.143
	.450	.043	.010	-.016	-.112	-.121	-.127	-.136	-.142
	.375	.042	.011	-.013	-.061	-.087	-.111	-.127	-.137
	.300	.042	.013	-.012	-.040	-.098	-.121	-.135	-.145
	.225								
	.150								
	.075								

Table 3. Continued

(d) Concluded; station 3

	THETA, DEG	CP FOR ALPHA, DEG =							
		-3.96	.03	4.05	7.98	12.00	15.98	20.02	23.99
BODY	0	-.005	.019	.049	.085	.133	.196	.276	.371
	15	-.005	.019	.051	.087	.136	.199	.279	.373
	30	-.010	.015	.046	.082	.132	.196	.277	.369
	45	-.007	.018	.049	.085	.136	.202	.282	.376
	60	-.009	.018	.046	.079	.133	.199	.278	.375
	75	-.008	.019	.047	.086	.131	.191	.261	.351
	90								
	105	.046	.014	-.012	-.036	-.100	-.132	-.136	-.141
	120	.043	.013	-.013	-.043	-.105	-.133	-.137	-.142
	135	.042	.013	-.013	-.045	-.105	-.129	-.138	-.143
	150	.041	.012	-.012	-.041	-.076	-.125	-.130	-.139
	165	.041	.012	-.010	-.026	-.035	-.075	-.092	-.107
	180	.039	.011	-.011	-.023	-.029	-.042	-.068	-.084
	195	.041	.012	-.010	-.023	-.033	-.060	-.083	-.097
	210	.044	.015	-.008	-.032	-.064	-.110	-.121	-.128
	225	.041	.012	-.012	-.043	-.101	-.127	-.136	-.142
	240	.038	.009	-.012	-.040	-.097	-.127	-.135	-.140
	255	.044	.013	-.010	-.036	-.093	-.126	-.135	-.139
	270								
	285	-.002	.022	.048	.083	.128	.184	.258	.347
	300	-.007	.020	.046	.081	.132	.195	.273	.368
315	-.008	.020	.049	.083	.134	.196	.275	.371	
330	-.006	.021	.050	.084	.134	.195	.273	.368	
345	.000	.022	.052	.086	.135	.197	.275	.371	
	Y/S	CP FOR ALPHA, DEG =							
		-3.96	.03	4.05	7.98	12.00	15.98	20.02	23.99
WINDWARD WING	.190								
	.274	-.001	.025	.051	.087	.139	.198	.277	.368
	.379	-.007	.017	.045	.084	.138	.198	.275	.367
	.473	.005	.021	.050	.091	.149	.217	.298	.402
	.569								
	.664	-.085	.018	.051	.093	.151	.217	.294	.394
	.759	-.072	.015	.053	.094	.150	.214	.296	.390
	.806	-.065	.015	.056	.100	.153	.214	.297	.387
	.854	-.062	-.002	.061	.106	.157	.213	.294	.381
LEEWARD WING	.854	.064	.012	-.068	-.095	-.116	-.130	-.136	-.138
	.806	.055	.013	-.075	-.103	-.126	-.135	-.141	-.143
	.759	.055	.016	-.073	-.106	-.122	-.131	-.137	-.139
	.664	.050	.013	-.086	-.115	-.128	-.138	-.143	-.145
	.569	.045	.011	-.027	-.124	-.133	-.135	-.141	-.144
	.473	.049	.015	-.005	-.074	-.105	-.116	-.125	-.131
	.379	.046	.013	-.012	-.043	-.094	-.111	-.127	-.141
	.274	.050	.018	-.007	-.033	-.100	-.126	-.136	-.139
.190									

Table 3. Continued

(e) $M_\infty = 1.70$; $\phi = 30^\circ$; station 1

THETA, DEG	CP FOR ALPHA, DEG =							
	-4.69	-.60	3.39	7.42	11.33	15.43	19.38	23.42
0								
15	-.024	-.002	.015	.032	.021	-.034	.006	.047
30	-.030	-.005	.014	.034	.040	.000	-.103	-.087
45	-.031	-.003	.019	.045	.071	.069	.044	.020
60	-.036	-.005	.022	.052	.077	.063	.053	.058
75	-.037	-.003	.026	.041	.021	-.050	-.019	-.030
90								
105	.039	.005	-.023	-.066	-.123	-.215	-.226	-.260
120	.033	.001	-.025	-.068	-.165	-.271	-.267	-.278
135	.036	.009	-.012	-.040	-.077	-.107	-.202	-.234
150	.027	.005	-.014	-.027	-.042	-.065	-.140	-.163
165	.020	.003	-.016	-.036	-.054	-.084	-.159	-.154
180	.019	.004	-.017	-.048	-.128	-.187	-.159	-.165
195	.022	.005	-.018	-.047	-.090	-.139	-.136	-.160
210	.030	.009	-.016	-.046	-.072	-.137	-.128	-.159
225	.037	.010	-.020	-.052	-.073	-.107	-.134	-.182
240	.040	.009	-.024	-.061	-.087	-.122	-.194	-.245
255	.038	.009	-.025	-.063	-.116	-.229	-.343	-.407
270								
285	-.038	-.007	.020	.062	.105	.164	.239	.334
300	-.036	-.007	.017	.057	.105	.174	.255	.350
315	-.028	-.007	.014	.047	.093	.158	.237	.332
330	-.018	-.004	.015	.040	.076	.136	.214	.305
345	-.020	-.005	.013	.032	.048	.097	.169	.249
Y/S	CP FOR ALPHA, DEG =							
	-4.69	-.60	3.39	7.42	11.33	15.43	19.38	23.42
.050								
.100								
.150								
.200								
.250								
.300	-.037	-.010	.020	.066	.121	.194	.277	.370
.350	-.039	-.010	.022	.070	.127	.202	.288	.387
.400	-.143	-.013	.025	.075	.135	.208	.295	.392
.425								
.450	-.161	-.025	.036	.090	.151	.221	.304	.403
.450	.065	.008	-.122	-.181	-.232	-.234	-.242	-.279
.425	.056	.008	-.140	-.218	-.252	-.245	-.240	-.275
.400	.052	.009	-.047	-.223	-.272	-.233	-.241	-.270
.350	.045	.006	-.020	-.087	-.181	-.181	-.253	-.277
.300	.040	.003	-.025	-.060	-.093	-.231	-.236	-.269
.250								
.200								
.150								
.100								
.050								

Table 3. Continued

(e) Continued; station 2

	THETA, DEG	CP FOR ALPHA, DEG =							
		-4.69	-.60	3.39	7.42	11.33	15.43	19.38	23.42
BODY	0	-.041	-.006	.020	.054	.100	.120	.148	.171
	15	-.041	-.006	.021	.052	.089	.111	.128	.146
	30	-.040	-.004	.025	.059	.091	.128	.163	.198
	45	-.041	-.005	.027	.066	.105	.150	.192	.241
	60	-.041	-.005	.028	.069	.110	.152	.188	.235
	75	-.040	-.006	.027	.059	.089	.125	.138	.182
	90								
	105	.048	.010	-.019	-.052	-.070	-.120	-.202	-.262
	120	.038	.002	-.027	-.068	-.105	-.153	-.256	-.289
	135	.039	.005	-.023	-.055	-.096	-.149	-.218	-.279
	150	.040	.007	-.020	-.049	-.081	-.122	-.140	-.183
	165	.033	.003	-.024	-.060	-.093	-.120	-.139	-.169
	180	.032	.004	-.022	-.067	-.115	-.115	-.142	-.185
	195	.028	.000	-.027	-.063	-.096	-.108	-.143	-.196
	210	.031	.003	-.024	-.058	-.093	-.108	-.143	-.209
	225	.034	.005	-.023	-.055	-.091	-.125	-.205	-.271
	240	.033	.003	-.026	-.054	-.099	-.193	-.322	-.385
	255	.030	.002	-.029	-.054	-.106	-.195	-.292	-.370
	270								
	285	-.043	-.012	.023	.069	.122	.188	.257	.350
	300	-.042	-.007	.026	.069	.118	.174	.235	.326
	315	-.040	-.007	.024	.067	.118	.171	.233	.313
	330	-.038	-.006	.022	.063	.114	.158	.216	.274
345	-.037	-.003	.024	.062	.109	.143	.189	.221	
	Y/S	CP FOR ALPHA, DEG =							
		-4.69	-.60	3.39	7.42	11.33	15.43	19.38	23.42
WINDWARD WING	.075								
	.150								
	.225								
	.300	-.037	-.007	.028	.075	.126	.192	.262	.357
	.375	-.037	-.005	.032	.080	.132	.195	.266	.359
	.450								
	.524	-.052	-.003	.038	.086	.142	.202	.283	.375
	.599								
	.637								
	.674	-.142	-.023	.052	.104	.161	.229	.310	.403
LEEWARD WING	.674	.069	.013	-.097	-.172	-.220	-.284	-.320	-.346
	.637	.065	.014	-.122	-.181	-.232	-.313	-.329	-.352
	.599	.060	.013	-.122	-.231	-.271	-.329	-.334	-.355
	.524	.051	.009	-.012	-.161	-.290	-.347	-.326	-.344
	.450	.052	.012	-.017	-.065	-.160	-.214	-.259	-.290
	.375	.048	.010	-.020	-.056	-.093	-.102	-.194	-.236
	.300	.043	.004	-.025	-.052	-.059	-.128	-.208	-.267
	.225								
	.150								
	.075								

Table 3. Continued

(e) Concluded; station 3

THETA, DEG	CP FOR ALPHA, DEG =							
	-4.69	-.60	3.39	7.42	11.33	15.43	19.38	23.42
0	-.036	-.003	.025	.058	.095	.134	.186	.232
15	-.035	-.002	.028	.060	.094	.127	.177	.216
30	-.037	-.004	.025	.059	.097	.144	.194	.237
45	-.038	-.006	.023	.060	.105	.156	.208	.250
60	-.039	-.006	.022	.060	.108	.154	.199	.230
75	-.036	-.006	.024	.057	.099	.136	.169	.193
90								
105	.058	.014	-.019	-.043	-.068	-.108	-.130	-.156
120	.053	.012	-.021	-.051	-.074	-.116	-.141	-.167
135	.050	.012	-.021	-.052	-.078	-.123	-.157	-.210
BODY 150	.048	.013	-.019	-.049	-.075	-.118	-.150	-.189
165	.042	.010	-.023	-.063	-.085	-.125	-.172	-.229
180	.042	.011	-.021	-.061	-.083	-.121	-.177	-.258
195	.043	.010	-.022	-.058	-.083	-.120	-.178	-.257
210	.039	.005	-.026	-.060	-.089	-.126	-.194	-.279
225	.040	.006	-.024	-.057	-.086	-.148	-.260	-.345
240	.038	.005	-.024	-.056	-.090	-.203	-.325	-.374
255	.032	-.001	-.027	-.056	-.094	-.179	-.306	-.374
270								
285	-.033	-.004	.027	.077	.137	.201	.275	.365
300	-.037	-.007	.022	.070	.125	.190	.265	.353
315	-.026	.001	.031	.076	.128	.187	.251	.327
330	-.030	-.004	.027	.066	.115	.175	.238	.306
345	-.035	-.004	.026	.062	.104	.158	.212	.272
Y/S	CP FOR ALPHA, DEG =							
	-4.69	-.60	3.39	7.42	11.33	15.43	19.38	23.42
.190								
.274	-.034	-.005	.025	.074	.134	.198	.270	.360
.379	-.031	-.003	.029	.078	.137	.203	.275	.365
.473	-.035	-.007	.027	.077	.135	.203	.279	.367
WINDWARD 569								
WING 664	-.067	-.008	.031	.085	.147	.215	.298	.387
.759	-.191	-.012	.035	.094	.157	.226	.307	.402
.806	-.137	-.017	.038	.098	.160	.230	.312	.408
.854	-.133	-.023	.044	.103	.166	.236	.318	.413
.854	.075	.013	-.098	-.171	-.226	-.275	-.317	-.348
.806	.076	.018	-.116	-.170	-.222	-.269	-.331	-.356
.759	.068	.015	-.129	-.223	-.253	-.286	-.369	-.373
LEEWARD 664	.064	.015	-.005	-.166	-.267	-.319	-.359	-.354
WING 569	.060	.013	-.017	-.058	-.138	-.208	-.270	-.283
.473	.053	.007	-.023	-.054	-.082	-.133	-.172	-.193
.379	.052	.007	-.024	-.052	-.066	-.100	-.100	-.124
.274	.053	.010	-.022	-.046	-.070	-.114	-.131	-.161
.190								

Table 3. Continued

(f) $M_\infty = 2.16$; $\phi = 30^\circ$; station 1

THETA, DEG	CP FOR ALPHA, DEG =							
	-3.97	-.01	4.01	7.98	12.03	15.98	19.99	24.02
0								
15	-.017	.001	.010	-.008	-.015	.007	.050	.100
30	-.020	.002	.015	.016	-.039	-.060	-.035	-.003
45	-.024	.003	.023	.039	.028	-.011	-.024	-.011
60	-.029	.002	.027	.046	.032	.017	.021	.047
75	-.028	.004	.031	.024	-.003	-.022	-.009	.018
90								
105	.030	.001	-.026	-.068	-.121	-.152	-.168	-.180
120	.023	-.002	-.026	-.069	-.158	-.177	-.183	-.199
135	.023	.003	-.015	-.040	-.061	-.118	-.136	-.145
BODY 150	.013	.000	-.014	-.021	-.025	-.082	-.106	-.115
165	.005	-.002	-.015	-.031	-.037	-.103	-.116	-.140
180	.003	.000	-.015	-.046	-.129	-.135	-.131	-.153
195	.007	.002	-.015	-.042	-.106	-.105	-.116	-.121
210	.016	.004	-.018	-.043	-.078	-.091	-.103	-.108
225	.026	.007	-.020	-.047	-.063	-.085	-.101	-.117
240	.028	.006	-.026	-.057	-.075	-.100	-.130	-.142
255	.031	.008	-.022	-.056	-.137	-.191	-.231	-.255
270								
285	-.030	-.006	.025	.062	.111	.172	.248	.347
300	-.028	-.005	.021	.058	.114	.181	.267	.368
315	-.020	-.002	.017	.051	.105	.168	.255	.352
330	-.015	-.002	.013	.040	.089	.147	.230	.321
345	-.014	-.001	.009	.025	.067	.117	.191	.272
Y/S	CP FOR ALPHA, DEG =							
	-3.97	-.01	4.01	7.98	12.03	15.98	19.99	24.02
.050								
.100								
.150								
.200								
WINDWARD .250								
WING .300	-.027	-.006	.028	.071	.132	.205	.292	.397
.350	-.028	-.007	.030	.075	.137	.210	.300	.409
.400	-.120	-.009	.032	.080	.143	.218	.309	.417
.425								
.450	-.116	-.021	.042	.094	.156	.233	.323	.427
.450	.048	-.002	-.112	-.148	-.168	-.158	-.180	-.196
.425	.044	.003	-.123	-.158	-.172	-.155	-.174	-.192
.400	.038	.000	-.103	-.174	-.183	-.158	-.173	-.193
.350	.034	-.001	-.024	-.101	-.130	-.163	-.178	-.189
LEEWARD .300	.030	-.002	-.027	-.058	-.096	-.151	-.174	-.181
WING .250								
.200								
.150								
.100								
.050								

Table 3. Continued
(f) Continued; station 2

THETA, DEG	CP FOR ALPHA, DEG =							
	-3.97	-.01	4.01	7.98	12.03	15.98	19.99	24.02
0	-.028	-.001	.023	.046	.069	.065	.107	.167
15	-.029	.000	.022	.046	.069	.063	.042	.074
30	-.031	-.002	.021	.053	.080	.089	.106	.141
45	-.033	-.003	.023	.056	.088	.115	.147	.192
60	-.036	-.006	.022	.054	.084	.116	.143	.187
75	-.033	-.004	.022	.047	.062	.078	.103	.146
90								
105	.030	.000	-.026	-.048	-.069	-.132	-.171	-.180
120	.030	.002	-.023	-.057	-.095	-.157	-.181	-.189
135	.030	.003	-.020	-.049	-.088	-.115	-.160	-.174
BODY 150	.029	.003	-.018	-.043	-.069	-.078	-.105	-.123
165	.028	.003	-.019	-.048	-.064	-.090	-.100	-.115
180	.025	.002	-.023	-.064	-.101	-.090	-.106	-.122
195	.025	.002	-.024	-.052	-.074	-.084	-.103	-.121
210	.024	.001	-.025	-.048	-.080	-.084	-.105	-.133
225	.023	-.003	-.028	-.050	-.083	-.107	-.134	-.150
240	.024	-.002	-.028	-.047	-.093	-.151	-.191	-.220
255	.022	-.004	-.029	-.047	-.103	-.164	-.216	-.242
270								
285	-.026	.001	.030	.067	.119	.187	.272	.370
300	-.028	.000	.028	.061	.103	.165	.244	.343
315	-.024	.000	.028	.059	.099	.165	.241	.336
330	-.025	.000	.026	.057	.086	.143	.214	.303
345	-.026	.000	.025	.052	.078	.109	.172	.248
Y/S								
	-3.97	-.01	4.01	7.98	12.03	15.98	19.99	24.02
.075								
.150								
.225								
WINDWARD .300	-.025	.001	.029	.067	.119	.186	.272	.372
WING .375	-.026	.001	.031	.069	.125	.193	.275	.376
.450								
.524	-.032	.000	.035	.077	.138	.212	.294	.398
.599								
.637								
.674	-.105	-.007	.045	.095	.161	.235	.322	.427
.674	.049	.002	-.097	-.142	-.187	-.202	-.221	-.230
.637	.045	.003	-.103	-.144	-.186	-.205	-.223	-.231
.599	.041	.003	-.127	-.159	-.190	-.208	-.225	-.229
.524	.037	.004	-.027	-.160	-.214	-.204	-.215	-.215
LEEWARD .450	.032	.000	-.021	-.079	-.156	-.167	-.189	-.189
WING .375	.031	.001	-.026	-.055	-.083	-.126	-.152	-.162
.300	.032	.001	-.024	-.040	-.048	-.128	-.170	-.181
.225								
.150								
.075								

Table 3. Continued

(f) Concluded; station 3

THETA, DEG	CP FOR ALPHA, DEG =							
	-3.97	-.01	4.01	7.98	12.03	15.98	19.99	24.02
BODY								
0	-.030	-.002	.024	.054	.084	.109	.139	.191
15	-.029	-.001	.026	.056	.086	.107	.132	.178
30	-.033	-.005	.023	.056	.092	.125	.166	.230
45	-.031	-.003	.025	.059	.101	.139	.187	.250
60	-.031	-.003	.025	.058	.099	.137	.183	.243
75	-.028	-.002	.028	.055	.086	.119	.157	.213
90								
105	.036	.002	-.023	-.036	-.060	-.089	-.119	-.125
120	.033	.001	-.024	-.044	-.063	-.092	-.131	-.128
135	.032	.002	-.022	-.044	-.068	-.103	-.143	-.142
150	.031	.003	-.021	-.042	-.066	-.100	-.110	-.137
165	.029	.003	-.023	-.053	-.072	-.107	-.119	-.159
180	.027	.002	-.025	-.056	-.077	-.104	-.124	-.160
195	.029	.003	-.026	-.050	-.073	-.102	-.123	-.156
210	.029	.002	-.025	-.047	-.075	-.099	-.124	-.156
225	.028	.001	-.026	-.048	-.080	-.126	-.157	-.194
240	.026	.000	-.027	-.047	-.095	-.175	-.220	-.249
255	.027	.001	-.025	-.043	-.095	-.160	-.214	-.244
270								
285	-.027	-.001	.030	.071	.122	.181	.267	.361
300	-.029	-.002	.027	.065	.117	.173	.255	.348
315	-.025	.000	.029	.065	.109	.154	.218	.301
330	-.025	-.001	.029	.061	.103	.145	.203	.281
345	-.027	-.001	.027	.058	.093	.126	.173	.231
Y/S								
	-3.97	-.01	4.01	7.98	12.03	15.98	19.99	24.02
WINDWARD WING								
.190								
.274	-.027	-.001	.029	.070	.120	.179	.265	.360
.379	-.030	-.004	.028	.067	.119	.177	.264	.358
.473	-.027	-.001	.031	.072	.124	.184	.273	.368
.569								
.664	-.051	-.002	.035	.079	.129	.204	.291	.392
.759	-.131	-.003	.038	.083	.136	.215	.302	.407
.806	-.102	-.003	.042	.089	.145	.224	.312	.417
.854	-.098	-.007	.047	.095	.155	.234	.322	.427
LEEWARD WING								
.854	.052	.004	-.091	-.139	-.182	-.198	-.222	-.231
.806	.046	.003	-.097	-.141	-.177	-.220	-.230	-.242
.759	.044	.004	-.123	-.149	-.176	-.228	-.235	-.244
.664	.040	.005	-.039	-.173	-.208	-.240	-.236	-.234
.569	.038	.002	-.018	-.077	-.139	-.190	-.201	-.200
.473	.038	.003	-.023	-.045	-.071	-.113	-.140	-.143
.379	.034	.000	-.025	-.042	-.050	-.062	-.092	-.105
.274	.035	.002	-.023	-.035	-.059	-.086	-.116	-.125
.190								

Table 3. Continued

(g) $M_\infty = 2.40$; $\phi = 30^\circ$; station 1

	THETA, DEG	CP FOR ALPHA, DEG =							
		-4.04	-.01	3.95	8.00	11.99	16.09	20.11	23.96
	0								
	15	-.012	.006	.010	-.008	.000	.031	.073	.120
	30	-.015	.007	.018	.002	-.037	-.030	-.005	.024
	45	-.019	.009	.027	.037	.016	-.019	-.018	-.004
	60	-.024	.008	.030	.044	.027	.018	.030	.048
	75	-.024	.011	.033	.017	.012	.005	.013	.027
	90								
	105	.035	.002	-.021	-.062	-.118	-.130	-.148	-.163
	120	.028	.000	-.020	-.062	-.133	-.148	-.162	-.177
	135	.026	.004	-.010	-.035	-.054	-.112	-.123	-.135
BODY	150	.017	.002	-.008	-.015	-.023	-.080	-.095	-.108
	165	.009	.001	-.008	-.023	-.036	-.098	-.110	-.127
	180	.002	.001	-.009	-.039	-.114	-.119	-.124	-.131
	195	.006	.004	-.009	-.036	-.098	-.102	-.108	-.114
	210	.016	.006	-.011	-.037	-.070	-.087	-.093	-.105
	225	.027	.008	-.015	-.040	-.057	-.077	-.098	-.111
	240	.030	.007	-.021	-.051	-.069	-.098	-.110	-.117
	255	.033	.011	-.018	-.052	-.112	-.153	-.184	-.202
	270								
	285	-.024	.003	.030	.069	.119	.186	.263	.356
	300	-.022	.003	.027	.066	.121	.198	.283	.379
	315	-.014	.004	.023	.058	.110	.185	.268	.362
	330	-.010	.004	.018	.046	.092	.161	.241	.331
	345	-.009	.005	.013	.031	.070	.131	.203	.285
	Y/S	CP FOR ALPHA, DEG =							
		-4.04	-.01	3.95	8.00	11.99	16.09	20.11	23.96
	.050								
	.100								
	.150								
	.200								
WINDWARD	.250								
WING	.300	-.022	.002	.033	.079	.140	.220	.310	.409
	.350	-.024	.002	.036	.083	.146	.227	.318	.420
	.400	-.113	.001	.039	.089	.152	.235	.326	.430
	.425								
	.450	-.100	-.009	.048	.104	.166	.249	.337	.441
	.450	.052	-.008	-.102	-.130	-.142	-.142	-.161	-.175
	.425	.048	.003	-.107	-.133	-.143	-.136	-.155	-.171
	.400	.043	.001	-.111	-.146	-.150	-.135	-.156	-.172
	.350	.038	.001	-.022	-.098	-.107	-.137	-.155	-.166
LEEWARD	.300	.035	-.001	-.022	-.052	-.103	-.132	-.154	-.165
WING	.250								
	.200								
	.150								
	.100								
	.050								

Table 3. Continued

(g) Continued; station 2

	THETA, DEG	CP FOR ALPHA, DEG =							
		-4.04	-.01	3.95	8.00	11.99	16.09	20.11	23.96
BODY	0	-.019	.006	.031	.053	.062	.082	.136	.197
	15	-.019	.008	.032	.053	.061	.042	.065	.106
	30	-.021	.006	.031	.058	.073	.076	.096	.112
	45	-.022	.006	.033	.062	.085	.109	.147	.190
	60	-.024	.004	.032	.060	.082	.110	.145	.188
	75	-.020	.006	.035	.054	.057	.080	.111	.152
	90								
	105	.032	.006	-.017	-.040	-.071	-.133	-.155	-.164
	120	.032	.007	-.017	-.051	-.093	-.142	-.159	-.166
	135	.032	.007	-.015	-.040	-.079	-.107	-.143	-.152
	150	.032	.007	-.013	-.033	-.062	-.066	-.104	-.115
	165	.033	.009	-.010	-.036	-.060	-.072	-.090	-.110
	180	.029	.006	-.015	-.056	-.083	-.078	-.091	-.110
	195	.029	.007	-.015	-.045	-.066	-.076	-.090	-.110
	210	.028	.006	-.017	-.041	-.069	-.078	-.100	-.107
	225	.028	.004	-.019	-.042	-.072	-.088	-.106	-.106
	240	.028	.003	-.020	-.041	-.081	-.116	-.142	-.183
	255	.028	.003	-.021	-.041	-.095	-.152	-.185	-.203
	270								
	285	-.018	.006	.035	.073	.129	.210	.302	.402
300	-.020	.005	.032	.065	.111	.185	.272	.366	
315	-.017	.006	.032	.063	.106	.181	.266	.357	
330	-.016	.006	.031	.060	.092	.161	.238	.325	
345	-.017	.007	.031	.057	.075	.129	.199	.274	
	Y/S	CP FOR ALPHA, DEG =							
		-4.04	-.01	3.95	8.00	11.99	16.09	20.11	23.96
WINDWARD WING	.075								
	.150								
	.225								
	.300	-.018	.005	.035	.075	.130	.212	.304	.405
	.375	-.018	.006	.037	.077	.132	.212	.302	.403
	.450								
	.524	-.037	.006	.040	.084	.143	.228	.319	.419
	.599								
	.637								
	.674	-.089	-.002	.050	.103	.165	.254	.348	.447
LEEWARD WING	.674	.050	.000	-.088	-.126	-.164	-.173	-.186	-.192
	.637	.046	.006	-.093	-.127	-.166	-.173	-.186	-.193
	.599	.043	.006	-.104	-.132	-.167	-.173	-.187	-.192
	.524	.039	.007	-.046	-.148	-.178	-.169	-.180	-.182
	.450	.034	.005	-.014	-.082	-.145	-.149	-.162	-.161
	.375	.033	.006	-.016	-.049	-.065	-.127	-.141	-.147
	.300	.033	.007	-.015	-.033	-.055	-.129	-.156	-.165
	.225								
	.150								
	.075								

Table 3. Continued

(g) Concluded; station 3

THETA, DEG	CP FOR ALPHA, DEG =							
	-4.04	-.01	3.95	8.00	11.99	16.09	20.11	23.96
0	-.022	.005	.031	.058	.078	.106	.137	.174
15	-.022	.006	.032	.058	.085	.106	.135	.169
30	-.024	.004	.030	.059	.095	.130	.172	.223
45	-.024	.004	.032	.063	.102	.143	.194	.249
60	-.024	.004	.030	.063	.101	.140	.190	.241
75	-.021	.005	.033	.060	.088	.121	.165	.212
90								
105	.039	.009	-.016	-.034	-.060	-.092	-.128	-.125
120	.036	.007	-.017	-.041	-.063	-.098	-.136	-.135
135	.035	.008	-.016	-.041	-.067	-.107	-.138	-.145
BODY 150	.033	.007	-.015	-.039	-.064	-.090	-.106	-.146
165	.031	.006	-.015	-.048	-.068	-.089	-.106	-.146
180	.029	.005	-.018	-.054	-.067	-.086	-.108	-.144
195	.029	.005	-.018	-.048	-.064	-.084	-.107	-.136
210	.033	.008	-.017	-.044	-.065	-.084	-.110	-.129
225	.031	.004	-.021	-.045	-.071	-.100	-.122	-.137
240	.028	.003	-.022	-.043	-.086	-.141	-.180	-.207
255	.030	.003	-.021	-.040	-.086	-.145	-.185	-.204
270								
285	-.017	.007	.036	.074	.121	.194	.287	.379
300	-.019	.007	.034	.069	.114	.184	.274	.366
315	-.017	.008	.034	.068	.105	.162	.241	.325
330	-.018	.007	.033	.065	.099	.149	.223	.303
345	-.020	.007	.032	.062	.087	.128	.178	.249
Y/S	CP FOR ALPHA, DEG =							
	-4.04	-.01	3.95	8.00	11.99	16.09	20.11	23.96
.190								
.274	-.017	.008	.035	.073	.119	.194	.285	.377
.379	-.019	.005	.034	.071	.118	.193	.285	.377
.473	-.018	.007	.036	.075	.124	.200	.292	.386
WINDWARD 569								
WING 664	-.055	.006	.041	.082	.137	.220	.311	.413
.759	-.103	.005	.043	.089	.148	.233	.327	.428
.806	-.086	.006	.047	.096	.157	.243	.337	.439
.854	-.080	.004	.052	.103	.166	.252	.347	.449
.854	.055	.006	-.078	-.122	-.161	-.177	-.191	-.193
.806	.049	.007	-.087	-.127	-.161	-.184	-.196	-.199
.759	.047	.008	-.099	-.127	-.155	-.188	-.197	-.200
LEEWARD 664	.043	.008	-.059	-.156	-.171	-.198	-.195	-.191
WING 569	.038	.006	-.012	-.085	-.133	-.169	-.170	-.162
.473	.039	.008	-.015	-.045	-.070	-.109	-.130	-.115
.379	.038	.007	-.017	-.038	-.047	-.057	-.108	-.099
.274	.038	.009	-.015	-.032	-.057	-.085	-.126	-.122
.190								

Table 3. Continued

(h) $M_\infty = 2.86$; $\phi = 30^\circ$; station 1

THETA, DEG	CP FOR ALPHA, DEG =							
	-4.03	.02	4.00	7.98	12.00	16.03	20.01	23.97
0								
15	-.003	.008	.009	.002	.016	.042	.083	.124
30	-.004	.012	.018	-.005	-.014	-.002	.022	.048
45	-.010	.012	.027	.027	.001	-.012	-.003	.013
60	-.016	.010	.030	.036	.023	.018	.031	.046
75	-.017	.012	.033	.017	.018	.011	.020	.028
90								
105	.040	.009	-.014	-.049	-.090	-.101	-.112	-.122
120	.036	.008	-.011	-.045	-.096	-.105	-.117	-.125
135	.035	.012	-.002	-.022	-.042	-.079	-.089	-.100
BODY 150	.023	.005	-.003	-.010	-.021	-.062	-.075	-.080
165	.014	.004	-.003	-.016	-.032	-.076	-.085	-.094
180	.008	.005	-.003	-.027	-.081	-.085	-.091	-.092
195	.008	.009	-.003	-.026	-.072	-.080	-.084	-.085
210	.016	.010	-.007	-.030	-.055	-.068	-.075	-.082
225	.029	.013	-.010	-.034	-.053	-.066	-.074	-.081
240	.032	.012	-.016	-.047	-.059	-.073	-.079	-.079
255	.033	.015	-.016	-.050	-.074	-.094	-.111	-.129
270								
285	-.016	.005	.033	.071	.116	.176	.251	.331
300	-.014	.004	.029	.066	.117	.184	.268	.355
315	-.003	.010	.029	.062	.109	.174	.255	.341
330	.000	.007	.020	.048	.090	.150	.226	.308
345	.002	.008	.016	.036	.072	.123	.192	.266
Y/S	CP FOR ALPHA, DEG =							
	-4.03	.02	4.00	7.98	12.00	16.03	20.01	23.97
.050								
.100								
.150								
.200								
WINDWARD .250								
WING .300	-.013	.007	.038	.081	.137	.211	.298	.389
.350	-.017	.006	.039	.085	.142	.217	.308	.399
.400	-.084	.002	.042	.090	.149	.225	.316	.409
.425								
.450	-.068	-.004	.052	.105	.166	.242	.333	.427
.450	.059	.004	-.074	-.099	-.104	-.110	-.122	-.130
.425	.054	.008	-.074	-.097	-.102	-.104	-.116	-.125
.400	.047	.004	-.084	-.107	-.109	-.105	-.119	-.129
.350	.042	.006	-.016	-.083	-.079	-.101	-.115	-.123
LEEWARD .300	.041	.006	-.015	-.042	-.092	-.101	-.115	-.122
WING .250								
.200								
.150								
.100								
.050								

Table 3. Continued

(h) Continued; station 2

	THETA, DEG	CP FOR ALPHA, DEG =							
		-4.03	.02	4.00	7.98	12.00	16.03	20.01	23.97
BODY	0	-.002	.015	.033	.048	.056	.094	.152	.207
	15	-.003	.015	.034	.048	.045	.047	.088	.127
	30	-.006	.012	.033	.051	.059	.051	.056	.075
	45	-.007	.012	.034	.056	.072	.091	.125	.160
	60	-.011	.008	.032	.052	.069	.094	.130	.163
	75	-.009	.011	.035	.047	.053	.075	.106	.135
	90								
	105	.033	.007	-.014	-.036	-.073	-.112	-.125	-.132
	120	.036	.012	-.009	-.039	-.078	-.109	-.120	-.126
	135	.034	.011	-.009	-.029	-.057	-.086	-.110	-.116
	150	.034	.011	-.008	-.022	-.046	-.056	-.083	-.092
	165	.035	.013	-.006	-.025	-.047	-.053	-.069	-.084
	180	.031	.011	-.010	-.043	-.057	-.057	-.072	-.085
	195	.034	.014	-.009	-.034	-.048	-.057	-.070	-.077
	210	.033	.012	-.011	-.032	-.049	-.062	-.073	-.078
	225	.031	.007	-.016	-.035	-.053	-.066	-.077	-.082
	240	.031	.008	-.014	-.033	-.058	-.073	-.107	-.122
	255	.033	.008	-.015	-.036	-.084	-.121	-.135	-.142
	270								
	285	.000	.015	.041	.081	.135	.210	.300	.399
	300	-.003	.013	.035	.070	.117	.183	.269	.358
	315	.001	.015	.036	.067	.115	.182	.266	.352
	330	.000	.014	.034	.058	.101	.163	.241	.321
345	-.002	.014	.033	.051	.082	.135	.206	.274	
	Y/S	CP FOR ALPHA, DEG =							
		-4.03	.02	4.00	7.98	12.00	16.03	20.01	23.97
WINDWARD WING	.075								
	.150								
	.225								
	.300	-.001	.013	.039	.081	.136	.210	.301	.399
	.375	.000	.014	.041	.083	.138	.211	.300	.398
	.450								
	.524	-.042	.014	.046	.093	.151	.228	.319	.418
	.599								
	.637								
	.674	-.060	-.007	.058	.111	.176	.255	.349	.452
LEEWARD WING	.674	.057	.000	-.071	-.097	-.122	-.130	-.137	-.140
	.637	.053	.009	-.071	-.100	-.123	-.129	-.136	-.140
	.599	.051	.010	-.079	-.102	-.125	-.130	-.137	-.140
	.524	.047	.012	-.050	-.108	-.126	-.123	-.127	-.130
	.450	.038	.008	-.010	-.075	-.115	-.116	-.122	-.124
	.375	.037	.009	-.011	-.041	-.063	-.104	-.113	-.121
	.300	.038	.012	-.009	-.025	-.063	-.108	-.121	-.128
	.225								
	.150								
	.075								

Table 3. Continued

(h) Concluded; station 3

THETA, DEG	CP FOR ALPHA, DEG =							
	-4.03	.02	4.00	7.98	12.00	16.03	20.01	23.97
0	-.005	.020	.044	.064	.078	.092	.140	.195
15	-.004	.020	.044	.064	.078	.089	.102	.124
30	-.008	.015	.038	.064	.089	.114	.159	.200
45	-.005	.018	.041	.069	.100	.133	.182	.230
60	-.006	.016	.040	.067	.098	.131	.176	.223
75	-.004	.016	.040	.062	.086	.115	.155	.197
90								
105	.042	.013	-.009	-.024	-.047	-.084	-.103	-.112
120	.039	.012	-.011	-.030	-.051	-.090	-.109	-.117
135	.037	.012	-.010	-.030	-.054	-.083	-.101	-.118
BODY 150	.036	.012	-.009	-.028	-.054	-.069	-.080	-.113
165	.036	.012	-.009	-.036	-.053	-.065	-.081	-.109
180	.034	.011	-.011	-.041	-.052	-.063	-.082	-.107
195	.036	.012	-.010	-.033	-.047	-.058	-.075	-.101
210	.040	.015	-.007	-.029	-.047	-.057	-.072	-.094
225	.037	.012	-.010	-.030	-.050	-.060	-.071	-.104
240	.034	.009	-.011	-.027	-.061	-.085	-.126	-.130
255	.038	.013	-.007	-.023	-.071	-.112	-.130	-.135
270								
285	.001	.025	.051	.083	.136	.211	.298	.394
300	-.003	.022	.048	.078	.126	.199	.282	.377
315	-.002	.022	.047	.076	.113	.175	.254	.334
330	-.001	.022	.046	.074	.106	.162	.239	.319
345	.001	.022	.047	.071	.093	.132	.198	.268
Y/S	CP FOR ALPHA, DEG =							
	-4.03	.02	4.00	7.98	12.00	16.03	20.01	23.97
.190								
.274	.002	.028	.053	.083	.136	.212	.298	.394
.379	-.004	.021	.045	.078	.133	.208	.293	.391
.473	.002	.028	.051	.086	.141	.217	.305	.402
WINDWARD 569								
WING .664	-.054	.025	.056	.102	.155	.234	.328	.428
.759	-.068	.022	.059	.109	.167	.246	.342	.446
.806	-.057	.022	.064	.117	.178	.257	.353	.461
.854	-.053	.011	.070	.126	.190	.268	.364	.474
.854	.060	.007	-.060	-.088	-.118	-.129	-.136	-.137
.806	.052	.012	-.069	-.100	-.129	-.136	-.142	-.143
.759	.051	.015	-.073	-.094	-.122	-.133	-.138	-.140
LEEWARD .664	.045	.012	-.063	-.112	-.128	-.140	-.142	-.139
WING .569	.040	.010	-.005	-.080	-.121	-.125	-.128	-.124
.473	.044	.014	-.006	-.033	-.063	-.086	-.102	-.097
.379	.041	.011	-.010	-.027	-.035	-.059	-.095	-.094
.274	.046	.016	-.005	-.018	-.044	-.080	-.101	-.108
.190								

Table 3. Continued

(i) $M_\infty = 1.70$; $\phi = 60^\circ$; station 1

THETA, DEG	CP FOR ALPHA, DEG =							
	-4.44	-.40	3.63	7.57	11.61	15.57	19.60	23.55
0								
15	-.020	.000	.006	-.013	-.085	-.208	-.228	-.221
30	-.026	-.003	.006	-.003	-.040	-.135	-.293	-.287
45	-.030	-.001	.014	.017	.004	-.061	-.208	-.263
60	-.028	-.002	.016	.021	.008	-.042	-.140	-.200
75	-.018	.001	.021	.015	-.013	-.032	-.115	-.168
90								
105	.025	.001	-.014	-.031	-.057	-.056	-.093	-.122
120	.015	-.003	-.017	-.028	-.053	-.059	-.107	-.129
135	.015	.006	-.006	-.023	-.044	-.058	-.141	-.147
BODY 150	.004	.002	-.010	-.038	-.121	-.169	-.139	-.167
165	-.005	-.004	-.017	-.042	-.079	-.117	-.116	-.155
180	-.003	-.002	-.017	-.040	-.062	-.121	-.106	-.145
195	.002	.000	-.019	-.047	-.062	-.092	-.098	-.141
210	.013	.005	-.017	-.056	-.077	-.069	-.109	-.153
225	.020	.006	-.019	-.062	-.100	-.088	-.174	-.199
240	.019	.005	-.019	-.054	-.083	-.081	-.110	-.069
255	.020	.005	-.017	-.036	-.058	-.078	-.078	-.092
270								
285	-.015	-.003	.014	.042	.084	.146	.230	.315
300	-.012	-.004	.011	.035	.068	.127	.210	.290
315	-.014	-.005	.006	.021	.041	.087	.162	.233
330	-.014	-.003	.005	.008	.008	.034	.089	.146
345	-.018	-.003	.003	-.007	-.034	-.044	-.012	.028
Y/S	CP FOR ALPHA, DEG =							
	-4.44	-.40	3.63	7.57	11.61	15.57	19.60	23.55
.050								
.100								
.150								
.200								
WINDWARD .250								
WING .300	-.017	-.006	.013	.044	.089	.151	.236	.324
.350	-.018	-.007	.015	.046	.093	.156	.241	.329
.400	-.019	-.010	.017	.050	.100	.162	.246	.335
.425								
.450	-.108	-.008	.025	.068	.125	.193	.282	.374
.450	.044	.003	-.090	-.133	-.151	-.167	-.165	-.189
.425	.039	.004	-.061	-.149	-.163	-.179	-.138	-.161
.400	.039	.006	-.010	-.070	-.151	-.173	-.097	-.128
.350	.029	.001	-.013	-.036	-.105	-.089	-.083	-.112
LEEWARD .300	.025	-.002	-.016	-.028	-.043	-.049	-.090	-.122
WING .250								
.200								
.150								
.100								
.050								

Table 3. Continued

(i) Continued; station 2

	THETA, DEG	CP FOR ALPHA, DEG =							
		-4.44	-.40	3.63	7.57	11.61	15.57	19.60	23.55
BODY	0	-.034	-.004	.010	.009	-.014	-.097	-.158	-.139
	15	-.036	-.004	.011	.014	-.009	-.033	-.143	-.238
	30	-.033	.000	.017	.028	.026	.016	-.075	-.149
	45	-.033	-.001	.018	.034	.036	.018	-.079	-.132
	60	-.028	.000	.020	.035	.038	.007	-.107	-.140
	75	-.025	-.002	.018	.022	.003	-.012	-.131	-.149
	90								
	105	.029	.004	-.014	-.029	-.047	-.079	-.109	-.124
	120	.016	-.004	-.023	-.042	-.063	-.094	-.113	-.135
	135	.015	.000	-.019	-.049	-.079	-.098	-.096	-.122
	150	.016	.003	-.017	-.050	-.075	-.085	-.085	-.105
	165	.006	-.003	-.023	-.052	-.077	-.082	-.090	-.108
	180	.006	.000	-.019	-.049	-.075	-.075	-.080	-.088
	195	.000	-.005	-.024	-.056	-.088	-.082	-.081	-.087
	210	.006	-.003	-.021	-.054	-.093	-.091	-.087	-.090
	225	.010	-.002	-.021	-.049	-.076	-.071	-.055	-.060
	240	.011	-.002	-.020	-.039	-.048	-.039	-.027	-.056
	255	.009	-.004	-.023	-.032	-.038	-.058	-.171	-.240
	270								
	285	-.027	-.012	.010	.043	.079	.126	.212	.290
	300	-.024	-.005	.016	.042	.073	.109	.186	.259
315	-.028	-.005	.015	.035	.056	.065	.131	.195	
330	-.031	-.005	.012	.025	.037	.008	.047	.104	
345	-.028	-.001	.014	.019	.013	-.051	-.049	-.011	
	Y/S	CP FOR ALPHA, DEG =							
		-4.44	-.40	3.63	7.57	11.61	15.57	19.60	23.55
WINDWARD WING	.075								
	.150								
	.225								
	.300	-.020	-.006	.015	.049	.085	.134	.220	.303
	.375	-.020	-.004	.019	.053	.088	.137	.221	.303
	.450								
	.524	-.018	-.006	.020	.055	.096	.152	.231	.320
	.599								
	.637								
	.674	-.100	-.008	.035	.075	.126	.196	.281	.378
LEEWARD WING	.674	.044	.006	-.076	-.123	-.163	-.221	-.291	-.326
	.637	.042	.009	-.095	-.174	-.213	-.268	-.309	-.314
	.599	.038	.008	-.042	-.119	-.202	-.275	-.295	-.282
	.524	.031	.001	-.016	-.034	-.064	-.134	-.203	-.211
	.450	.034	.004	-.014	-.031	-.034	-.069	-.131	-.142
	.375	.029	.002	-.016	-.031	-.037	-.072	-.114	-.122
	.300	.021	-.003	-.021	-.033	-.049	-.085	-.116	-.129
	.225								
	.150								
	.075								

Table 3. Continued

(j) $M_\infty = 2.16; \phi = 60^\circ$; station 1

THETA, DEG	CP FOR ALPHA, DEG =							
	-4.03	.01	4.02	8.05	11.98	16.02	19.98	23.97
0								
15	-.020	.000	.001	-.037	-.114	-.127	-.120	-.106
30	-.022	.002	.008	-.010	-.064	-.159	-.182	-.181
45	-.022	.003	.014	.009	-.037	-.136	-.162	-.167
60	-.021	.003	.016	.012	-.036	-.102	-.139	-.152
75	-.017	.005	.018	.003	-.065	-.088	-.126	-.143
90								
105	.019	.000	-.013	-.030	-.039	-.055	-.083	-.093
120	.013	-.002	-.013	-.023	-.034	-.062	-.086	-.097
135	.011	.002	-.006	-.023	-.032	-.091	-.097	-.117
BODY 150	.000	.000	-.009	-.037	-.129	-.111	-.122	-.141
165	-.009	-.003	-.014	-.035	-.098	-.092	-.109	-.120
180	-.010	-.001	-.015	-.035	-.069	-.082	-.105	-.111
195	-.003	.001	-.017	-.041	-.059	-.084	-.099	-.108
210	.006	.003	-.019	-.054	-.064	-.090	-.112	-.124
225	.014	.005	-.019	-.062	-.112	-.134	-.136	-.119
240	.014	.003	-.019	-.055	-.083	-.067	-.036	.003
255	.017	.007	-.012	-.038	-.039	-.015	.018	.050
270								
285	-.015	-.003	.013	.046	.095	.162	.243	.339
300	-.013	-.003	.010	.038	.085	.145	.222	.311
315	-.011	-.002	.007	.026	.064	.116	.185	.263
330	-.012	-.002	.002	.007	.029	.066	.123	.187
345	-.014	-.001	-.001	-.015	-.015	.003	.045	.090
Y/S	CP FOR ALPHA, DEG =							
	-4.03	.01	4.02	8.05	11.98	16.02	19.98	23.97
.050								
.100								
.150								
.200								
WINDWARD .250								
WING .300	-.014	-.003	.014	.049	.099	.167	.249	.345
.350	-.016	-.004	.015	.051	.102	.171	.254	.349
.400	-.027	-.006	.017	.056	.110	.180	.263	.360
.425								
.450	-.080	-.014	.024	.070	.130	.205	.293	.398
.450	.031	-.005	-.077	-.100	-.107	-.122	-.141	-.156
.425	.031	.001	-.062	-.111	-.112	-.115	-.126	-.144
.400	.025	-.002	-.022	-.084	-.112	-.088	-.105	-.123
.350	.021	-.002	-.014	-.041	-.084	-.049	-.079	-.093
LEEWARD .300	.018	-.003	-.015	-.026	-.027	-.052	-.083	-.093
WING .250								
.200								
.150								
.100								
.050								

Table 3. Continued

(j) Continued; station 2

THETA, DEG	CP FOR ALPHA, DEG =							
	-4.03	.01	4.02	8.05	11.98	16.02	19.98	23.97
0	-.023	.001	.009	.004	-.042	-.080	-.063	-.041
15	-.026	.000	.010	.010	-.008	-.099	-.136	-.128
30	-.029	-.002	.011	.018	.006	-.050	-.103	-.125
45	-.025	-.001	.013	.022	.006	-.046	-.091	-.117
60	-.021	-.003	.011	.019	.006	-.063	-.098	-.115
75	-.014	-.001	.011	.010	-.014	-.065	-.103	-.116
90								
105	.020	.001	-.012	-.024	-.038	-.079	-.088	-.097
120	.020	.003	-.010	-.025	-.042	-.080	-.087	-.090
135	.017	.003	-.011	-.042	-.061	-.083	-.087	-.092
BODY 150	.014	.003	-.014	-.045	-.077	-.068	-.074	-.082
165	.011	.003	-.015	-.039	-.060	-.065	-.072	-.077
180	.007	.002	-.018	-.040	-.069	-.055	-.061	-.072
195	.008	.002	-.018	-.043	-.065	-.048	-.063	-.069
210	.010	.001	-.019	-.048	-.068	-.055	-.079	-.075
225	.009	-.002	-.023	-.048	-.059	-.062	-.072	-.042
240	.012	-.002	-.020	-.035	-.034	-.029	-.006	.025
255	.011	-.002	-.019	-.026	-.030	-.065	-.102	-.108
270								
285	-.012	.002	.021	.043	.085	.156	.225	.321
300	-.014	.001	.018	.037	.069	.135	.202	.288
315	-.016	.002	.017	.027	.048	.099	.161	.232
330	-.019	.001	.014	.014	.012	.048	.095	.151
345	-.021	.002	.011	.004	-.032	-.014	.017	.056
Y/S	CP FOR ALPHA, DEG =							
	-4.03	.01	4.02	8.05	11.98	16.02	19.98	23.97
.075								
.150								
.225								
WINDWARD .300	-.011	.002	.020	.044	.087	.159	.229	.326
WING .375	-.012	.003	.022	.046	.089	.160	.233	.326
.450								
.524	-.005	.003	.022	.053	.101	.169	.249	.340
.599								
.637								
.674	-.072	-.005	.027	.071	.128	.205	.292	.388
.674	.031	-.001	-.069	-.097	-.125	-.175	-.221	-.214
.637	.028	.000	-.087	-.124	-.146	-.187	-.225	-.208
.599	.025	.000	-.052	-.115	-.160	-.190	-.210	-.199
.524	.024	.004	-.007	-.020	-.074	-.124	-.151	-.179
LEEWARD .450	.020	.003	-.012	-.023	-.025	-.077	-.100	-.147
WING .375	.021	.004	-.012	-.024	-.027	-.072	-.083	-.107
.300	.021	.003	-.010	-.019	-.033	-.075	-.085	-.096
.225								
.150								
.075								

Table 3. Continued

(j) Concluded; station 3

	THETA, DEG	CP FOR ALPHA, DEG =							
		-4.03	.01	4.02	8.05	11.98	16.02	19.98	23.97
BODY	0	-.025	-.003	.009	.006	-.017	-.100	-.086	-.059
	15	-.026	.000	.012	.014	.012	-.034	-.097	-.113
	30	-.029	-.005	.010	.019	.025	-.015	-.066	-.082
	45	-.024	-.003	.013	.025	.031	-.012	-.061	-.077
	60	-.020	-.003	.014	.024	.024	-.027	-.083	-.089
	75	-.015	-.001	.016	.020	.014	-.018	-.066	-.085
	90								
	105	.023	.000	-.013	-.024	-.049	-.062	-.068	-.069
	120	.020	.000	-.015	-.029	-.054	-.067	-.070	-.074
	135	.017	.000	-.017	-.046	-.063	-.066	-.067	-.079
	150	.013	.001	-.018	-.039	-.054	-.064	-.066	-.079
	165	.010	.000	-.020	-.037	-.053	-.068	-.072	-.082
	180	.007	-.001	-.021	-.039	-.056	-.068	-.074	-.081
	195	.009	.000	-.021	-.043	-.066	-.075	-.085	-.088
	210	.013	.001	-.020	-.046	-.074	-.074	-.087	-.083
	225	.013	.000	-.020	-.041	-.056	-.044	-.027	.003
	240	.012	.000	-.019	-.030	-.031	-.025	-.052	-.071
	255	.013	.001	-.015	-.021	-.023	-.083	-.126	-.128
	270								
	285	-.017	-.004	.016	.045	.076	.142	.217	.311
300	-.019	-.004	.015	.038	.059	.116	.185	.272	
315	-.020	-.002	.014	.030	.037	.079	.137	.212	
330	-.021	-.003	.011	.019	.015	.027	.070	.128	
345	-.022	-.002	.009	.010	-.008	-.037	-.007	.034	
	Y/S	CP FOR ALPHA, DEG =							
		-4.03	.01	4.02	8.05	11.98	16.02	19.98	23.97
WINDWARD WING	.190								
	.274	-.017	-.004	.014	.044	.078	.143	.218	.314
	.379	-.021	-.007	.010	.042	.073	.137	.211	.305
	.473	-.020	-.004	.015	.041	.078	.141	.215	.306
	.569								
	.664	-.014	-.002	.020	.042	.091	.155	.232	.324
	.759	-.061	-.004	.021	.047	.099	.168	.248	.342
	.806	-.090	-.003	.024	.055	.108	.180	.263	.358
	.854	-.067	-.005	.028	.064	.120	.195	.282	.381
LEEWARD WING	.854	.034	.003	-.061	-.092	-.128	-.176	-.211	-.219
	.860	.028	.001	-.083	-.124	-.163	-.198	-.217	-.218
	.759	.028	.003	-.059	-.111	-.150	-.201	-.204	-.201
	.664	.024	.001	-.010	-.020	-.039	-.133	-.169	-.171
	.569	.020	-.001	-.017	-.022	-.030	-.050	-.097	-.136
	.473	.020	.000	-.015	-.022	-.034	-.048	-.060	-.096
	.379	.019	-.002	-.016	-.024	-.043	-.057	-.066	-.071
	.274	.022	.000	-.013	-.023	-.046	-.060	-.067	-.066
.190									

Table 3. Continued

(k) $M_\infty = 2.40$; $\phi = 60^\circ$; station 1

THETA, DEG	CP FOR ALPHA, DEG =							
	-3.98	-.03	3.99	7.99	12.02	16.00	19.96	23.97
BODY								
0								
15	-.012	.007	.000	-.049	-.085	-.090	-.082	-.066
30	-.014	.009	.009	-.015	-.081	-.132	-.141	-.136
45	-.012	.010	.017	.007	-.049	-.112	-.130	-.137
60	-.012	.010	.021	.009	-.048	-.113	-.123	-.135
75	-.006	.012	.023	-.001	-.057	-.087	-.113	-.124
90								
105	.020	.001	-.009	-.025	-.035	-.052	-.082	-.098
120	.013	-.001	-.010	-.018	-.031	-.062	-.083	-.098
135	.013	.005	-.002	-.017	-.028	-.086	-.096	-.113
150	.002	.001	-.005	-.031	-.110	-.104	-.110	-.127
165	-.006	.000	-.009	-.029	-.096	-.092	-.103	-.117
180	-.008	.001	-.011	-.030	-.067	-.085	-.101	-.111
195	-.002	.004	-.013	-.035	-.056	-.082	-.097	-.110
210	.008	.006	-.015	-.049	-.062	-.092	-.105	-.119
225	.016	.008	-.017	-.063	-.099	-.112	-.101	-.085
240	.017	.008	-.018	-.050	-.060	-.043	-.013	.022
255	.022	.011	-.011	-.025	-.018	.008	.045	.078
270								
285	-.007	.006	.025	.056	.111	.176	.257	.358
300	-.006	.005	.021	.047	.099	.159	.236	.331
315	-.004	.006	.018	.036	.080	.131	.201	.285
330	-.005	.005	.011	.017	.049	.087	.143	.210
345	-.007	.006	.005	-.007	.009	.031	.070	.118
Y/S								
	-3.98	-.03	3.99	7.99	12.02	16.00	19.96	23.97
WINDWARD WING								
.050								
.100								
.150								
.200								
.250								
.300	-.005	.006	.027	.059	.117	.183	.265	.366
.350	-.007	.005	.028	.061	.120	.187	.268	.371
.400	-.016	.004	.031	.066	.128	.195	.279	.383
.425								
.450	-.057	-.002	.039	.079	.146	.219	.307	.418
LEEWARD WING								
.450	.029	-.020	-.073	-.084	-.097	-.114	-.133	-.151
.425	.029	.001	-.076	-.089	-.098	-.102	-.119	-.141
.400	.024	.000	-.038	-.079	-.101	-.082	-.104	-.132
.350	.021	-.001	-.010	-.039	-.073	-.048	-.081	-.104
.300	.019	-.001	-.011	-.021	-.025	-.051	-.083	-.099
.250								
.200								
.150								
.100								
.050								

Table 3. Continued

(k) Continued; station 2

THETA, DEG	CP FOR ALPHA, DEG =							
	-3.98	-.03	3.99	7.99	12.02	16.00	19.96	23.97
BODY								
0	-.014	.006	.016	.001	-.054	-.052	-.031	-.002
15	-.016	.008	.018	.010	-.035	-.099	-.099	-.084
30	-.017	.007	.021	.020	-.005	-.065	-.093	-.097
45	-.015	.007	.022	.024	-.003	-.052	-.085	-.092
60	-.013	.005	.021	.020	-.007	-.058	-.088	-.091
75	-.008	.007	.022	.011	-.020	-.062	-.090	-.093
90								
105	.016	.002	-.011	-.019	-.042	-.076	-.094	-.103
120	.015	.004	-.011	-.022	-.046	-.079	-.091	-.092
135	.014	.005	-.010	-.039	-.063	-.085	-.087	-.096
150	.012	.005	-.012	-.042	-.070	-.074	-.079	-.092
165	.012	.007	-.011	-.035	-.060	-.071	-.075	-.087
180	.007	.004	-.015	-.039	-.064	-.057	-.067	-.085
195	.008	.004	-.016	-.041	-.060	-.051	-.069	-.082
210	.010	.003	-.018	-.046	-.063	-.061	-.091	-.094
225	.009	.000	-.020	-.044	-.058	-.073	-.055	-.021
240	.010	.000	-.018	-.031	-.037	-.028	.019	.056
255	.011	-.001	-.016	-.025	-.038	-.048	-.056	-.067
270								
285	-.004	.006	.024	.050	.105	.169	.250	.348
300	-.006	.005	.021	.040	.090	.147	.222	.315
315	-.008	.006	.021	.027	.067	.113	.178	.260
330	-.010	.005	.018	.010	.033	.064	.116	.181
345	-.011	.007	.017	.002	-.009	.008	.044	.090
Y/S								
	-3.98	-.03	3.99	7.99	12.02	16.00	19.96	23.97
WINDWARD WING								
.075								
.150								
.225								
.300	-.005	.005	.023	.052	.106	.171	.255	.354
.375	-.005	.006	.025	.053	.107	.171	.252	.351
.450								
.524	-.002	.005	.027	.058	.114	.179	.263	.361
.599								
.637								
.674	-.056	.001	.036	.076	.142	.213	.307	.412
LEEWARD WING								
.674	.028	-.012	-.068	-.088	-.120	-.157	-.181	-.183
.637	.025	.000	-.081	-.106	-.132	-.163	-.178	-.181
.599	.022	.001	-.072	-.106	-.142	-.166	-.168	-.174
.524	.020	.003	-.005	-.025	-.089	-.120	-.138	-.161
.450	.017	.002	-.010	-.018	-.029	-.077	-.110	-.147
.375	.017	.003	-.011	-.018	-.030	-.068	-.088	-.119
.300	.017	.004	-.009	-.014	-.036	-.073	-.091	-.101
.225								
.150								
.075								

Table 3. Continued

(k) Concluded; station 3

THETA, DEG	CP FOR ALPHA, DEG =							
	-3.98	-.03	3.99	7.99	12.02	16.00	19.96	23.97
BODY								
0	-.013	.007	.018	.008	-.034	-.065	-.045	-.019
15	-.014	.008	.020	.016	.007	-.043	-.089	-.093
30	-.017	.005	.020	.023	.022	-.019	-.062	-.068
45	-.012	.007	.022	.028	.027	-.017	-.055	-.061
60	-.010	.007	.022	.025	.020	-.035	-.066	-.069
75	-.005	.009	.025	.021	.017	-.022	-.059	-.065
90								
105	.025	.007	-.008	-.021	-.049	-.056	-.070	-.075
120	.020	.005	-.010	-.026	-.056	-.060	-.073	-.085
135	.016	.005	-.012	-.044	-.062	-.058	-.072	-.093
150	.013	.005	-.014	-.038	-.052	-.057	-.073	-.093
165	.010	.004	-.015	-.036	-.050	-.062	-.076	-.094
180	.009	.003	-.017	-.037	-.053	-.063	-.079	-.096
195	.012	.004	-.018	-.042	-.060	-.069	-.092	-.101
210	.016	.006	-.015	-.043	-.067	-.072	-.092	-.075
225	.014	.003	-.018	-.039	-.050	-.037	-.018	.019
240	.012	.002	-.016	-.026	-.025	-.010	-.018	-.038
255	.014	.003	-.012	-.018	-.035	-.074	-.085	-.088
270								
285	-.003	.010	.029	.050	.094	.155	.237	.336
300	-.006	.008	.026	.042	.078	.133	.207	.300
315	-.007	.009	.025	.035	.053	.101	.164	.242
330	-.009	.008	.021	.023	.017	.052	.101	.163
345	-.010	.008	.019	.013	-.023	-.005	.028	.072
Y/S								
	-3.98	-.03	3.99	7.99	12.02	16.00	19.96	23.97
WINDWARD WING								
.190								
.274	-.002	.010	.028	.050	.096	.156	.239	.338
.379	-.005	.007	.026	.046	.093	.152	.234	.331
.473	-.004	.009	.028	.049	.097	.155	.237	.334
.569								
.664	.000	.009	.031	.057	.111	.171	.256	.353
.759	-.036	.007	.032	.063	.122	.186	.272	.374
.806	-.056	.008	.036	.070	.132	.198	.285	.390
.854	-.045	.007	.040	.079	.143	.214	.304	.413
LEEWARD WING								
.854	.033	-.003	-.062	-.080	-.120	-.154	-.180	-.178
.806	.028	.001	-.078	-.105	-.142	-.168	-.183	-.176
.759	.028	.005	-.074	-.100	-.143	-.168	-.171	-.162
.664	.026	.006	-.003	-.020	-.048	-.130	-.140	-.140
.569	.023	.005	-.010	-.019	-.032	-.058	-.101	-.118
.473	.024	.006	-.009	-.019	-.035	-.047	-.071	-.095
.379	.023	.004	-.011	-.020	-.043	-.054	-.068	-.079
.274	.024	.006	-.008	-.020	-.044	-.052	-.066	-.070
.190								

Table 3. Continued

(1) $M_\infty = 2.86; \phi = 60^\circ$; station 1

THETA, DEG	CP FOR ALPHA, DEG =							
	-4.00	.01	4.02	7.99	12.01	16.02	20.01	24.02
0								
15	-.007	.008	.001	-.040	-.054	-.052	-.043	-.028
30	-.009	.011	.010	-.022	-.060	-.089	-.088	-.083
45	-.010	.012	.017	.001	-.043	-.079	-.092	-.094
60	-.010	.011	.019	.004	-.044	-.082	-.091	-.095
75	-.005	.013	.022	-.003	-.048	-.074	-.084	-.090
90								
105	.029	.006	-.002	-.020	-.026	-.041	-.066	-.076
120	.024	.005	-.002	-.012	-.021	-.049	-.065	-.072
135	.022	.009	.003	-.011	-.023	-.064	-.072	-.081
BODY 150	.010	.005	-.001	-.023	-.070	-.076	-.084	-.091
165	.000	.004	-.004	-.023	-.068	-.075	-.084	-.091
180	-.005	.006	-.005	-.025	-.050	-.072	-.080	-.087
195	-.001	.009	-.006	-.030	-.049	-.070	-.077	-.084
210	.009	.010	-.010	-.048	-.061	-.075	-.085	-.095
225	.018	.013	-.009	-.054	-.071	-.070	-.058	-.045
240	.019	.012	-.008	-.033	-.031	-.017	.008	.038
255	.022	.014	-.002	-.013	-.002	.023	.058	.095
270								
285	-.001	.006	.024	.061	.111	.176	.254	.342
300	-.001	.006	.020	.052	.098	.160	.233	.318
315	.003	.010	.019	.044	.083	.138	.202	.280
330	.001	.008	.012	.027	.054	.097	.149	.212
345	-.001	.009	.006	.006	.020	.050	.086	.132
Y/S	CP FOR ALPHA, DEG =							
	-4.00	.01	4.02	7.99	12.01	16.02	20.01	24.02
.050								
.100								
.150								
.200								
WINDWARD .250								
WING .300	.001	.008	.027	.064	.116	.182	.262	.351
.350	.000	.008	.027	.067	.118	.185	.267	.356
.400	-.016	.005	.029	.070	.124	.194	.278	.371
.425								
.450	-.038	.002	.038	.083	.142	.217	.306	.406
.450	.038	.000	-.048	-.063	-.073	-.096	-.108	-.116
.425	.036	.005	-.046	-.062	-.071	-.087	-.098	-.108
.400	.031	.002	-.016	-.065	-.077	-.074	-.092	-.105
.350	.030	.004	-.005	-.033	-.055	-.041	-.069	-.087
LEEWARD .300	.027	.004	-.004	-.018	-.020	-.042	-.068	-.081
WING .250								
.200								
.150								
.100								
.050								

Table 3. Continued

(1) Continued; station 2

	THETA, DEG	CP FOR ALPHA, DEG =							
		-4.00	.01	4.02	7.99	12.01	16.02	20.01	24.02
BODY	0	.001	.013	.016	-.006	-.027	-.013	.008	.034
	15	-.001	.015	.019	.009	-.039	-.059	-.051	-.037
	30	-.006	.012	.020	.017	-.013	-.053	-.064	-.065
	45	-.007	.012	.021	.021	-.007	-.045	-.060	-.058
	60	-.007	.009	.020	.013	-.010	-.047	-.061	-.060
	75	-.002	.011	.023	.012	-.013	-.048	-.060	-.059
	90								
	105	.024	.006	-.003	-.010	-.033	-.061	-.075	-.088
	120	.023	.011	.000	-.011	-.033	-.060	-.073	-.079
	135	.020	.011	-.001	-.028	-.049	-.070	-.075	-.082
	150	.017	.010	-.002	-.033	-.052	-.063	-.070	-.080
	165	.017	.012	-.002	-.025	-.045	-.057	-.063	-.072
	180	.013	.010	-.006	-.030	-.046	-.048	-.063	-.073
	195	.019	.013	-.006	-.030	-.043	-.045	-.063	-.071
	210	.020	.011	-.009	-.035	-.052	-.057	-.076	-.068
	225	.020	.008	-.011	-.037	-.055	-.052	-.029	.001
	240	.021	.009	-.007	-.027	-.024	-.001	.036	.078
	255	.023	.009	-.006	-.020	-.011	-.007	-.011	-.014
	270								
	285	.009	.015	.030	.063	.112	.181	.261	.351
	300	.006	.014	.025	.052	.095	.159	.232	.317
	315	.006	.016	.023	.040	.076	.130	.193	.266
	330	.003	.014	.018	.021	.046	.087	.136	.196
	345	.002	.013	.017	.001	.011	.038	.072	.114
	Y/S	CP FOR ALPHA, DEG =							
		-4.00	.01	4.02	7.99	12.01	16.02	20.01	24.02
WINDWARD WING	.075								
	.150								
	.225								
	.300	.007	.015	.028	.063	.112	.182	.262	.354
	.375	.007	.017	.030	.065	.113	.181	.260	.352
	.450								
	.524	.011	.020	.033	.072	.122	.192	.272	.366
	.599								
	.637								
	.674	-.037	.005	.044	.089	.148	.227	.317	.421
LEEWARD WING	.674	.039	-.007	-.047	-.067	-.090	-.117	-.129	-.132
	.637	.037	.006	-.046	-.075	-.094	-.119	-.126	-.130
	.599	.035	.009	-.034	-.081	-.100	-.122	-.122	-.126
	.524	.031	.010	.005	-.028	-.084	-.100	-.106	-.113
	.450	.025	.007	-.002	-.010	-.023	-.063	-.095	-.109
	.375	.026	.008	-.002	-.008	-.021	-.053	-.073	-.095
	.300	.026	.010	.001	-.004	-.026	-.055	-.070	-.083
	.225								
	.150								
	.075								

Table 3. Continued

(1) Concluded; station 3

	THETA, DEG	CP FOR ALPHA, DEG =							
		-4.00	.01	4.02	7.99	12.01	16.02	20.01	24.02
BODY	0	.000	.020	.024	.011	-.032	-.022	-.004	.023
	15	.000	.020	.025	.021	-.003	-.041	-.054	-.043
	30	-.004	.015	.022	.026	.013	-.026	-.039	-.037
	45	-.001	.016	.025	.031	.019	-.017	-.035	-.034
	60	.000	.013	.024	.028	.010	-.028	-.039	-.038
	75	.003	.013	.025	.026	.012	-.025	-.038	-.039
	90								
	105	.029	.011	.001	-.011	-.034	-.049	-.060	-.072
	120	.025	.010	-.001	-.017	-.044	-.056	-.068	-.082
	135	.024	.011	-.002	-.033	-.049	-.054	-.065	-.084
	150	.020	.010	-.004	-.029	-.042	-.052	-.068	-.086
	165	.019	.011	-.004	-.025	-.042	-.052	-.067	-.085
	180	.018	.010	-.006	-.027	-.044	-.053	-.069	-.087
	195	.022	.012	-.007	-.030	-.047	-.055	-.071	-.091
	210	.027	.016	-.004	-.030	-.055	-.064	-.060	-.039
	225	.025	.013	-.005	-.025	-.037	-.028	.004	.041
	240	.021	.011	-.004	-.012	-.011	.009	.022	.016
	255	.025	.013	.003	-.007	-.018	-.037	-.037	-.034
	270								
	285	.008	.023	.043	.070	.112	.180	.258	.352
300	.004	.021	.038	.057	.095	.159	.229	.315	
315	.003	.022	.036	.044	.073	.127	.186	.262	
330	.002	.022	.032	.028	.042	.082	.128	.189	
345	.004	.023	.029	.019	.008	.032	.063	.106	
	Y/S	CP FOR ALPHA, DEG =							
		-4.00	.01	4.02	7.99	12.01	16.02	20.01	24.02
WINDWARD WING	.190								
	.274	.009	.027	.045	.070	.113	.182	.262	.355
	.379	.003	.020	.039	.065	.111	.177	.254	.347
	.473	.008	.025	.040	.070	.117	.183	.259	.349
	.569								
	.664	.011	.021	.041	.078	.131	.197	.278	.368
	.759	-.030	.019	.042	.083	.140	.216	.294	.389
	.806	-.033	.020	.046	.089	.150	.229	.308	.407
	.854	-.029	.011	.051	.097	.162	.245	.329	.431
LEEWARD WING	.854	.043	.002	-.037	-.061	-.088	-.113	-.130	-.128
	.806	.037	.012	-.042	-.078	-.101	-.122	-.133	-.130
	.759	.035	.013	-.031	-.081	-.105	-.120	-.123	-.118
	.664	.029	.011	-.005	-.014	-.052	-.109	-.106	-.106
	.569	.025	.009	-.001	-.008	-.020	-.060	-.086	-.090
	.473	.029	.012	.002	-.007	-.023	-.038	-.066	-.076
	.379	.028	.010	.000	-.010	-.031	-.046	-.057	-.075
	.274	.032	.016	.004	-.007	-.031	-.045	-.056	-.069
.190									

Table 3. Continued

(m) $M_\infty = 1.70$; $\phi = 90^\circ$; station 1

	THETA, DEG	CP FOR ALPHA, DEG =							
		-4.24	-.22	3.74	7.73	11.70	15.72	19.77	23.71
BODY	0								
	15	-.016	.002	-.002	-.022	-.035	-.050	-.110	-.159
	30	-.014	.001	.000	-.012	-.030	-.066	-.105	-.159
	45	-.006	.004	.005	-.007	-.038	-.086	-.097	-.141
	60	.001	.005	.006	-.013	-.077	-.161	-.096	-.136
	75	.011	.009	.010	.000	-.036	-.066	-.124	-.146
	90								
	105	-.001	-.002	.003	-.002	-.022	-.061	-.127	-.133
	120	-.008	-.005	-.004	-.022	-.096	-.174	-.112	-.154
	135	-.004	.005	.004	-.009	-.039	-.086	-.099	-.152
	150	-.014	.000	-.002	-.015	-.034	-.087	-.109	-.167
	165	-.022	-.007	-.013	-.032	-.047	-.078	-.123	-.178
	180	-.013	-.003	-.013	-.046	-.078	-.069	-.142	-.190
	195	-.006	.000	-.013	-.053	-.105	-.099	-.238	-.256
	210	.003	.005	-.009	-.044	-.091	-.159	-.161	-.142
	225	.006	.006	-.006	-.027	-.062	-.087	-.065	-.032
	240	.005	.003	-.003	-.009	-.021	-.001	.043	.100
	255	.008	.003	.002	.005	.010	.051	.117	.186
	270								
	285	.007	-.001	-.001	.006	.015	.058	.122	.201
	300	.003	-.002	-.004	-.003	-.012	.012	.064	.129
	315	-.002	-.003	-.008	-.021	-.052	-.063	-.029	.015
	330	-.003	-.001	-.008	-.037	-.081	-.142	-.133	-.109
345	-.008	-.002	-.011	-.046	-.096	-.089	-.234	-.233	
	Y/S	CP FOR ALPHA, DEG =							
		-4.24	-.22	3.74	7.73	11.70	15.72	19.77	23.71
WINDWARD WING	.050								
	.100								
	.150								
	.200								
	.250								
	.300	.009	-.002	-.002	.005	.015	.059	.125	.201
	.350	.010	-.003	-.003	.002	.011	.054	.121	.195
	.400	.007	-.005	-.005	-.003	.003	.043	.107	.177
	.425								
	.450	.007	-.001	-.002	-.002	.004	.043	.105	.171
LEEWARD WING	.450	-.003	-.004	.004	.013	.010	-.006	-.170	-.244
	.425	-.002	-.001	.005	.013	.008	-.011	-.175	-.240
	.400	.001	.002	.007	.015	.007	-.020	-.170	-.237
	.350	-.002	-.003	.003	.009	-.007	-.042	-.149	-.241
	.300	-.005	-.005	.001	.004	-.013	-.047	-.138	-.140
	.250								
	.200								
	.150								
	.100								
	.050								

Table 3. Continued

(m) Continued; station 2

	THETA, DEG	CP FOR ALPHA, DEG =							
		-4.24	-.22	3.74	7.73	11.70	15.72	19.77	23.71
BODY	0	-.020	-.001	-.005	-.026	-.066	-.094	-.097	-.113
	15	-.020	.000	-.003	-.012	-.035	-.051	-.079	-.103
	30	-.013	.003	.001	-.003	-.025	-.040	-.078	-.104
	45	-.008	.002	.001	-.005	-.024	-.037	-.088	-.111
	60	-.003	.005	.004	-.014	-.026	-.039	-.092	-.114
	75	.000	.002	.003	-.006	-.034	-.052	-.091	-.127
	90								
	105	.001	.001	.000	-.012	-.042	-.064	-.115	-.218
	120	-.009	-.006	-.009	-.035	-.049	-.060	-.110	-.166
	135	-.009	-.003	-.006	-.019	-.037	-.049	-.105	-.143
	150	-.009	.001	-.004	-.016	-.035	-.053	-.094	-.136
	165	-.018	-.005	-.011	-.027	-.045	-.063	-.092	-.134
	180	-.017	-.002	-.009	-.035	-.069	-.089	-.096	-.136
	195	-.018	-.006	-.013	-.043	-.089	-.152	-.189	-.224
	210	-.013	-.004	-.010	-.034	-.073	-.116	-.172	-.155
	225	-.013	-.006	-.010	-.024	-.044	-.052	-.065	-.031
	240	-.009	-.004	-.005	-.007	-.001	.015	.043	.093
	255	-.009	-.007	-.006	.003	.026	.058	.111	.169
	270								
	285	-.006	-.006	-.002	.013	.042	.066	.109	.186
	300	-.006	-.002	.000	.007	.020	.037	.063	.127
315	-.009	-.002	-.002	-.009	-.022	-.027	-.035	.011	
330	-.012	-.002	-.005	-.020	-.058	-.097	-.148	-.121	
345	-.013	.003	-.002	-.025	-.074	-.136	-.201	-.204	
	Y/S	CP FOR ALPHA, DEG =							
		-4.24	-.22	3.74	7.73	11.70	15.72	19.77	23.71
WINDWARD WING	.075								
	.150								
	.225								
	.300	.000	-.002	.000	.015	.041	.063	.106	.182
	.375	.004	.001	.005	.017	.042	.066	.108	.182
	.450								
	.524	-.001	.000	.003	.012	.028	.036	.088	.157
	.599								
	.637								
	.674	-.002	-.002	-.002	.004	.012	.024	.071	.129
LEEWARD WING	.674	-.005	-.005	-.003	.003	.011	.011	-.062	-.241
	.637	.001	-.001	.001	.006	.012	.006	-.102	-.263
	.599	-.001	-.002	.000	.005	.010	-.009	-.151	-.275
	.524	-.006	-.004	-.003	-.001	.002	-.057	-.211	-.231
	.450	.000	.002	.002	.003	-.011	-.089	-.149	-.206
	.375	-.001	.002	.002	-.002	-.040	-.084	-.133	-.213
	.300	-.006	-.004	-.004	-.013	-.043	-.075	-.134	-.219
	.225								
.150									
.075									

Table 3. Continued

(m) Concluded; station 3

THETA, DEG	CP FOR ALPHA, DEG =							
	-4.24	-.22	3.74	7.73	11.70	15.72	19.77	23.71
0	-.014	.002	-.004	-.027	-.050	-.083	-.086	-.100
15	-.009	.007	.003	-.011	-.023	-.042	-.056	-.089
30	-.008	.001	-.001	-.011	-.023	-.042	-.060	-.095
45	.001	.002	.000	-.009	-.020	-.040	-.070	-.100
60	.007	.006	.001	-.013	-.019	-.038	-.074	-.102
75	.007	.009	.002	-.009	-.025	-.038	-.073	-.105
90								
105	.010	.007	.001	-.011	-.018	-.048	-.110	-.152
120	.003	.002	-.004	-.023	-.025	-.048	-.081	-.162
135	-.001	.000	-.005	-.017	-.025	-.048	-.072	-.118
BODY 150	-.008	-.001	-.005	-.016	-.025	-.045	-.068	-.114
165	-.015	-.005	-.011	-.022	-.032	-.050	-.074	-.116
180	-.012	-.001	-.009	-.029	-.049	-.073	-.090	-.116
195	-.010	-.001	-.010	-.035	-.065	-.126	-.190	-.197
210	-.013	-.005	-.013	-.034	-.057	-.107	-.142	-.150
225	-.010	-.002	-.007	-.019	-.027	-.043	-.046	-.011
240	-.008	-.003	-.004	-.003	.007	.018	.046	.109
255	-.012	-.011	-.010	-.002	.021	.043	.080	.149
270								
285	.003	.006	.012	.017	.033	.059	.104	.173
300	-.006	.000	.003	.003	.012	.029	.064	.128
315	.003	.008	.008	.000	-.015	-.018	-.019	.019
330	-.006	.001	-.002	-.020	-.052	-.086	-.120	-.123
345	-.011	.000	-.006	-.032	-.064	-.119	-.170	-.198
Y/S								
	-4.24	-.22	3.74	7.73	11.70	15.72	19.77	23.71
.190								
.274	.002	.006	.011	.014	.029	.054	.099	.167
.379	.010	.006	.014	.016	.031	.055	.098	.166
.473	.006	.002	.011	.012	.026	.048	.085	.152
WINDWARD WING .569								
.664	.004	.004	.011	.010	.020	.039	.062	.125
.759	.004	.005	.012	.009	.019	.036	.056	.114
.806	.002	.004	.010	.007	.016	.033	.056	.112
.854	.000	.001	.007	.006	.014	.034	.059	.113
.854	-.004	-.004	.001	.002	.015	.017	.012	-.128
.806	.007	.005	.009	.009	.023	.021	-.008	-.164
.759	.003	.001	.005	.004	.020	.011	-.053	-.205
.664	.005	.002	.006	.005	.020	-.023	-.155	-.254
LEEWARD WING .569	.006	.003	.005	.007	.013	-.087	-.181	-.194
.473	.001	-.002	-.002	-.001	-.026	-.108	-.128	-.166
.379	.001	-.001	-.004	-.012	-.043	-.066	-.125	-.156
.274	.003	.002	-.004	-.014	-.025	-.056	-.107	-.150
.190								

Table 3. Continued

(n) $M_\infty = 2.16$; $\phi = 90^\circ$; station 1

THETA, DEG	CP FOR ALPHA, DEG =							
	-4.02	.06	4.06	8.01	12.01	16.03	19.97	24.00
0								
15	-.016	.001	-.005	-.025	-.045	-.081	-.101	-.114
30	-.011	.004	.000	-.014	-.048	-.076	-.105	-.112
45	-.006	.005	.004	-.012	-.075	-.079	-.100	-.113
60	-.002	.005	.004	-.020	-.127	-.081	-.105	-.121
75	.005	.007	.007	-.005	-.029	-.099	-.118	-.133
90								
105	-.001	-.001	.001	-.006	-.020	-.089	-.102	-.114
120	-.008	-.004	-.002	-.026	-.124	-.102	-.111	-.120
135	-.010	.001	.000	-.015	-.081	-.085	-.106	-.111
BODY 150	-.018	-.001	-.005	-.019	-.052	-.083	-.110	-.117
165	-.021	-.004	-.011	-.031	-.051	-.088	-.111	-.124
180	-.016	-.002	-.013	-.049	-.066	-.101	-.123	-.131
195	-.008	.000	-.013	-.057	-.121	-.138	-.134	-.123
210	-.001	.002	-.011	-.049	-.083	-.081	-.060	-.034
225	.003	.004	-.006	-.032	-.038	-.024	.014	.053
240	.001	.003	-.003	-.008	.008	.042	.098	.158
255	.006	.006	.004	.012	.041	.090	.158	.228
270								
285	.000	.000	-.003	.006	.038	.084	.150	.225
300	-.002	-.001	-.006	-.007	.012	.045	.100	.163
315	-.003	.001	-.008	-.024	-.028	-.006	.029	.075
330	-.007	.000	-.012	-.043	-.076	-.071	-.052	-.022
345	-.011	.001	-.012	-.052	-.115	-.133	-.129	-.115
Y/S								
	-4.02	.06	4.06	8.01	12.01	16.03	19.97	24.00
.050								
.100								
.150								
.200								
WINDWARD .250								
WING .300	.003	.000	-.003	.008	.041	.087	.153	.225
.350	.003	-.001	-.004	.006	.038	.082	.147	.220
.400	.000	-.003	-.005	.003	.035	.075	.137	.208
.425								
.450	.003	.000	-.020	-.025	-.007	.017	.079	.158
.450	-.021	-.012	-.002	.005	.009	-.062	-.175	-.174
.425	.002	-.001	.003	.009	.009	-.076	-.165	-.170
.400	-.004	-.004	.001	.007	.002	-.089	-.165	-.173
.350	-.003	-.004	.001	.005	-.006	-.092	-.168	-.179
LEEWARD .300	-.004	-.004	.000	.001	-.010	-.086	-.140	-.130
WING .250								
.200								
.150								
.100								
.050								

Table 3. Continued

(n) Continued; station 2

	THETA, DEG	CP FOR ALPHA, DEG =							
		-4.02	.06	4.06	8.01	12.01	16.03	19.97	24.00
BODY	0	-.014	.001	-.005	-.024	-.045	-.057	-.077	-.100
	15	-.013	.002	-.003	-.012	-.037	-.050	-.069	-.086
	30	-.010	.002	-.003	-.011	-.039	-.054	-.067	-.084
	45	-.005	.002	-.003	-.014	-.027	-.062	-.077	-.089
	60	.000	.001	-.003	-.029	-.047	-.063	-.082	-.091
	75	.006	.003	.002	-.009	-.038	-.061	-.091	-.098
	90								
	105	.001	-.002	.000	-.014	-.039	-.078	-.161	-.164
	120	.001	.001	.000	-.029	-.048	-.070	-.110	-.109
	135	-.004	.002	-.002	-.014	-.031	-.067	-.095	-.103
	150	-.008	.002	-.004	-.014	-.041	-.065	-.092	-.102
	165	-.010	.002	-.005	-.017	-.039	-.064	-.089	-.099
	180	-.012	.000	-.009	-.032	-.049	-.074	-.103	-.113
	195	-.008	.001	-.009	-.039	-.063	-.125	-.139	-.128
	210	-.007	.000	-.009	-.034	-.073	-.087	-.070	-.042
	225	-.009	-.004	-.009	-.027	-.048	-.026	.007	.052
	240	-.006	-.003	-.005	-.009	-.003	.037	.085	.147
	255	-.003	-.004	-.003	.003	.025	.076	.135	.208
	270								
	285	.003	.005	.007	.012	.037	.082	.142	.211
	300	-.001	.004	.004	.001	.010	.048	.102	.163
	315	-.001	.005	.000	-.012	-.031	-.009	.028	.071
	330	-.005	.003	-.005	-.023	-.049	-.078	-.057	-.031
345	-.009	.001	-.007	-.029	-.055	-.111	-.126	-.122	
	Y/S	CP FOR ALPHA, DEG =							
		-4.02	.06	4.06	8.01	12.01	16.03	19.97	24.00
WINDWARD WING	.075								
	.150								
	.225								
	.300	.003	.004	.004	.010	.034	.078	.136	.204
	.375	.006	.006	.007	.010	.032	.080	.138	.204
	.450								
	.524	.008	.005	.004	.004	.024	.067	.120	.185
	.599								
	.637								
	.674	.004	.003	.000	-.041	-.043	-.017	.053	.122
LEEWARD WING	.674	-.016	-.003	.000	.003	.012	.012	-.102	-.179
	.637	-.003	-.002	.003	.005	.013	.001	-.132	-.182
	.599	-.004	-.002	.004	.005	.013	-.022	-.159	-.180
	.524	.000	.002	.006	.007	.008	-.086	-.151	-.165
	.450	-.001	-.001	.004	.003	-.012	-.137	-.143	-.155
	.375	.002	-.001	.004	-.003	-.033	-.095	-.134	-.156
	.300	.003	.000	.004	-.006	-.030	-.085	-.142	-.158
	.225								
	.150								
	.075								

Table 3. Continued

(n) Concluded; station 3

	THETA, DEG	CP FOR ALPHA, DEG =							
		-4.02	.06	4.06	8.01	12.01	16.03	19.97	24.00
BODY	0	-.011	.001	-.006	-.025	-.046	-.052	-.067	-.082
	15	-.012	.002	-.003	-.014	-.028	-.043	-.061	-.066
	30	-.013	-.003	-.005	-.014	-.027	-.047	-.063	-.076
	45	-.005	.000	-.001	-.011	-.024	-.050	-.066	-.073
	60	.001	.001	.000	-.018	-.028	-.053	-.069	-.064
	75	.007	.003	.002	-.011	-.031	-.063	-.089	-.088
	90								
	105	.007	.002	.002	-.010	-.033	-.078	-.119	-.149
	120	.002	.002	-.002	-.021	-.032	-.063	-.129	-.126
	135	-.002	.001	-.004	-.013	-.026	-.060	-.091	-.107
	150	-.008	.000	-.005	-.012	-.026	-.056	-.084	-.102
	165	-.012	-.001	-.007	-.015	-.029	-.056	-.085	-.101
	180	-.013	-.001	-.011	-.026	-.041	-.064	-.093	-.113
	195	-.008	-.001	-.011	-.035	-.070	-.109	-.136	-.133
	210	-.005	.001	-.008	-.030	-.055	-.090	-.070	-.039
	225	-.005	-.001	-.005	-.018	-.023	-.024	.011	.063
	240	-.006	-.001	-.003	-.003	.010	.035	.085	.152
	255	-.002	-.001	.001	.010	.025	.068	.123	.195
	270								
	285	.000	.002	.006	.014	.033	.068	.124	.195
	300	-.004	.001	.001	.005	.017	.042	.094	.165
315	-.004	.001	-.002	-.008	-.015	-.019	.020	.072	
330	-.005	.001	-.005	-.022	-.053	-.086	-.063	-.032	
345	-.007	.003	-.005	-.029	-.071	-.097	-.116	-.121	
	Y/S	CP FOR ALPHA, DEG =							
		-4.02	.06	4.06	8.01	12.01	16.03	19.97	24.00
WINDWARD WING	.190								
	.274	.000	.002	.005	.012	.030	.066	.121	.191
	.379	.001	-.001	.002	.008	.023	.060	.115	.185
	.473	.005	.005	.005	.009	.019	.059	.115	.182
	.569								
	.664	.004	.003	.003	.004	.012	.046	.095	.154
	.759	.003	.002	.001	.000	.011	.044	.089	.139
	.806	.004	.004	.003	.002	.009	.046	.089	.142
	.854	.005	.004	.002	-.008	-.020	.049	.088	.125
LEEWARD WING	.854	-.006	-.002	.006	.011	.019	.029	.001	-.169
	.806	-.007	-.004	.005	.009	.016	.022	-.047	-.176
	.759	-.003	-.002	.007	.012	.017	.014	-.093	-.169
	.664	-.002	-.002	.006	.012	.012	-.035	-.161	-.173
	.569	-.002	-.004	.005	.009	-.005	-.111	-.173	-.174
	.473	.003	.000	.007	.007	-.037	-.121	-.123	-.150
	.379	.003	-.002	.004	-.007	-.048	-.089	-.113	-.144
	.274	.007	.002	.003	-.007	-.035	-.081	-.113	-.140
	.190								

Table 3. Continued

(o) $M_\infty = 2.40$; $\phi = 90^\circ$; station 1

	THETA, DEG	CP FOR ALPHA, DEG =								
		-3.96	.01	4.00	8.04	12.04	16.04	20.01	23.97	
BODY	0									
	15	-.008	.006	-.004	-.024	-.044	-.076	-.094	-.107	
	30	-.003	.009	.003	-.014	-.044	-.078	-.094	-.106	
	45	.002	.010	.007	-.012	-.081	-.085	-.096	-.109	
	60	.007	.009	.009	-.020	-.104	-.088	-.101	-.119	
	75	.013	.012	.013	-.005	-.033	-.101	-.108	-.127	
	90									
	105	.002	.002	.007	-.003	-.020	-.087	-.103	-.117	
	120	-.004	.000	.003	-.022	-.104	-.095	-.106	-.120	
	135	-.004	.005	.006	-.011	-.084	-.087	-.101	-.113	
	150	-.012	.002	.000	-.016	-.053	-.087	-.103	-.115	
	165	-.015	.000	-.007	-.026	-.052	-.090	-.106	-.118	
	180	-.011	.001	-.010	-.045	-.065	-.100	-.112	-.127	
	195	-.003	.005	-.010	-.058	-.100	-.107	-.097	-.086	
	210	.003	.006	-.008	-.045	-.060	-.051	-.028	-.004	
	225	.007	.009	-.003	-.024	-.020	.002	.037	.077	
	240	.007	.007	.001	.000	.023	.066	.121	.180	
	255	.013	.012	.012	.025	.056	.110	.176	.254	
	270									
	285	.006	.006	.006	.019	.055	.108	.175	.249	
	300	.004	.005	.002	.005	.032	.073	.127	.188	
	315	.003	.006	-.001	-.015	-.003	.022	.060	.103	
	330	-.001	.005	-.007	-.040	-.047	-.037	-.017	.009	
	345	-.005	.005	-.008	-.058	-.090	-.096	-.089	-.076	
	WINDWARD WING	Y/S								
		-3.96	.01	4.00	8.04	12.04	16.04	20.01	23.97	
.050										
.100										
.150										
.200										
.250										
.300		.008	.006	.006	.021	.058	.112	.177	.251	
.350		.009	.006	.006	.020	.056	.107	.171	.243	
.400		.007	.005	.004	.019	.054	.104	.163	.231	
.425										
.450		.008	.001	-.005	.003	.028	.067	.106	.162	
LEEWARD WING		.450	-.025	-.017	.000	.009	.006	-.075	-.157	-.160
		.425	-.010	.001	.008	.013	.007	-.093	-.149	-.154
		.400	-.001	.001	.007	.011	.000	-.106	-.152	-.156
		.350	.000	.000	.007	.008	-.009	-.101	-.155	-.145
		.300	-.001	-.001	.006	.004	-.013	-.097	-.136	-.134
		.250								
		.200								
		.150								
		.100								
		.050								

Table 3. Continued

(o) Continued; station 2

THETA, DEG	CP FOR ALPHA, DEG =							
	-3.96	.01	4.00	8.04	12.04	16.04	20.01	23.97
0	-.004	.010	.002	-.020	-.044	-.064	-.081	-.095
15	-.004	.011	.005	-.009	-.036	-.054	-.072	-.088
30	-.003	.010	.006	-.008	-.038	-.054	-.070	-.088
45	.001	.010	.007	-.011	-.033	-.065	-.077	-.092
60	.004	.007	.006	-.026	-.040	-.066	-.077	-.093
75	.009	.010	.009	-.006	-.037	-.073	-.093	-.096
90								
105	.003	.004	.004	-.009	-.044	-.090	-.146	-.132
120	.002	.007	.005	-.027	-.049	-.079	-.096	-.112
135	-.001	.007	.004	-.013	-.037	-.075	-.094	-.106
BODY 150	-.004	.007	.002	-.012	-.041	-.072	-.095	-.105
165	-.002	.009	.002	-.012	-.039	-.070	-.091	-.104
180	-.006	.005	-.004	-.028	-.050	-.082	-.102	-.112
195	-.003	.006	-.004	-.036	-.080	-.110	-.102	-.088
210	-.002	.005	-.005	-.034	-.072	-.063	-.038	-.009
225	-.004	.000	-.006	-.025	-.031	-.006	.034	.083
240	-.001	.001	-.002	-.006	.011	.054	.106	.175
255	.001	.000	.001	.007	.039	.091	.151	.234
270								
285	.010	.010	.011	.018	.055	.105	.170	.245
300	.006	.010	.007	.005	.029	.069	.126	.191
315	.006	.010	.004	-.010	-.010	.015	.057	.105
330	.003	.009	.001	-.024	-.056	-.047	-.022	.008
345	.000	.010	.000	-.027	-.071	-.097	-.094	-.078
Y/S	CP FOR ALPHA, DEG =							
	-3.96	.01	4.00	8.04	12.04	16.04	20.01	23.97
.075								
.150								
.225								
WINDWARD .300	.010	.009	.008	.017	.053	.103	.165	.237
.375	.013	.010	.011	.018	.052	.101	.162	.234
WING .450								
.524	.012	.011	.009	.015	.044	.086	.143	.208
.599								
.637								
.674	.009	.007	-.005	-.016	.008	.043	.084	.133
.674	-.038	-.009	.004	.008	.011	.007	-.116	-.141
.637	-.004	.000	.007	.012	.012	-.009	-.137	-.148
.599	.000	.002	.007	.011	.009	-.035	-.148	-.153
.524	.003	.005	.009	.013	.000	-.093	-.138	-.152
LEEWARD .450	.001	.004	.007	.010	-.022	-.129	-.132	-.145
WING .375	.003	.005	.007	.003	-.042	-.096	-.131	-.133
.300	.004	.006	.008	.000	-.037	-.092	-.133	-.131
.225								
.150								
.075								

Table 3. Continued

(o) Concluded; station 3

THETA, DEG	CP FOR ALPHA, DEG =							
	-3.96	.01	4.00	8.04	12.04	16.04	20.01	23.97
0	-.002	.009	.000	-.022	-.046	-.062	-.073	-.091
15	-.002	.010	.003	-.010	-.028	-.051	-.061	-.083
30	-.004	.007	.002	-.011	-.028	-.050	-.065	-.086
45	.003	.009	.005	-.009	-.023	-.053	-.066	-.085
60	.008	.009	.006	-.018	-.026	-.055	-.064	-.083
75	.013	.011	.009	-.010	-.030	-.078	-.073	-.084
90								
105	.009	.006	.005	-.010	-.040	-.081	-.123	-.118
120	.005	.005	.002	-.023	-.038	-.066	-.109	-.110
135	-.001	.005	.001	-.014	-.033	-.062	-.092	-.105
BODY 150	-.005	.004	.000	-.014	-.032	-.059	-.088	-.099
165	-.006	.004	-.002	-.015	-.033	-.058	-.088	-.099
180	-.006	.003	-.006	-.025	-.042	-.064	-.095	-.104
195	-.003	.004	-.007	-.034	-.073	-.096	-.107	-.092
210	.000	.006	-.003	-.028	-.069	-.061	-.037	-.006
225	-.002	.003	-.003	-.015	-.033	-.002	.038	.088
240	-.003	.001	.000	.002	.008	.054	.109	.179
255	.000	.002	.004	.013	.033	.084	.146	.223
270								
285	.008	.011	.013	.019	.042	.093	.155	.224
300	.005	.010	.009	.009	.021	.067	.126	.192
315	.005	.010	.006	-.006	-.015	.013	.056	.104
330	.004	.010	.002	-.022	-.050	-.049	-.024	.006
345	.002	.010	.000	-.029	-.067	-.096	-.092	-.078
Y/S	CP FOR ALPHA, DEG =							
	-3.96	.01	4.00	8.04	12.04	16.04	20.01	23.97
.190								
.274	.009	.012	.013	.018	.040	.092	.152	.220
.379	.009	.009	.011	.014	.037	.088	.148	.214
.473	.013	.012	.012	.014	.037	.085	.145	.211
WINDWARD 569								
WING 664	.013	.013	.011	.010	.034	.076	.127	.186
.759	.011	.011	.010	.009	.034	.073	.121	.172
.806	.011	.013	.012	.008	.033	.073	.119	.169
.854	.012	.013	.010	-.015	.021	.058	.098	.136
.854	-.023	-.002	.005	.009	.015	.027	-.051	-.140
.806	-.002	.001	.005	.010	.015	.020	-.087	-.143
.759	.003	.005	.008	.012	.016	.009	-.106	-.138
LEEWARD 664	.003	.007	.008	.011	.009	-.048	-.135	-.145
WING 569	.003	.005	.006	.009	-.013	-.113	-.141	-.151
.473	.006	.006	.007	.007	-.046	-.117	-.121	-.136
.379	.005	.005	.006	-.006	-.051	-.091	-.117	-.126
.274	.008	.007	.006	-.006	-.038	-.080	-.119	-.116
.190								

Table 3. Continued

(p) $M_\infty = 2.86; \phi = 90^\circ$; station 1

THETA, DEG	CP FOR ALPHA, DEG =							
	-4.00	.06	3.96	7.99	12.03	15.97	20.01	23.99
0								
15	-.006	.008	.000	-.023	-.042	-.063	-.072	-.080
30	-.001	.010	.006	-.013	-.040	-.062	-.071	-.079
45	.005	.011	.010	-.010	-.061	-.067	-.074	-.082
60	.009	.010	.010	-.015	-.068	-.074	-.085	-.091
75	.017	.013	.013	-.002	-.030	-.078	-.087	-.094
90								
105	.011	.005	.008	-.002	-.023	-.070	-.077	-.087
120	.004	.003	.005	-.017	-.065	-.071	-.082	-.090
135	.002	.008	.007	-.011	-.058	-.067	-.076	-.083
BODY 150	-.007	.005	.001	-.017	-.045	-.070	-.077	-.085
165	-.011	.004	-.003	-.027	-.049	-.071	-.079	-.089
180	-.009	.005	-.006	-.049	-.061	-.077	-.089	-.093
195	.000	.009	-.004	-.047	-.064	-.063	-.053	-.041
210	.007	.010	.000	-.027	-.030	-.018	.003	.026
225	.011	.012	.005	-.005	.003	.025	.058	.094
240	.013	.011	.010	.016	.039	.077	.130	.186
255	.017	.013	.016	.033	.066	.114	.174	.243
270								
285	.013	.009	.009	.027	.062	.109	.171	.243
300	.009	.008	.006	.015	.042	.079	.131	.192
315	.007	.009	.004	-.001	.014	.039	.075	.120
330	.003	.009	-.001	-.024	-.022	-.011	.010	.038
345	-.001	.008	-.003	-.045	-.058	-.057	-.048	-.034
Y/S	CP FOR ALPHA, DEG =							
	-4.00	.06	3.96	7.99	12.03	15.97	20.01	23.99
.050								
.100								
.150								
.200								
WINDWARD .250								
WING .300	.015	.009	.010	.029	.065	.113	.175	.248
.350	.016	.009	.011	.031	.064	.109	.170	.239
.400	.014	.006	.006	.019	.051	.098	.168	.236
.425								
.450	.015	.005	.000	.012	.039	.073	.116	.167
.450	-.004	-.005	.003	.010	.004	-.060	-.117	-.117
.425	.001	.000	.007	.012	.004	-.075	-.109	-.112
.400	.003	.001	.007	.010	-.003	-.091	-.112	-.113
.350	.009	.003	.008	.009	-.013	-.088	-.112	-.108
LEEWARD .300	.008	.002	.006	.004	-.017	-.087	-.105	-.105
WING .250								
.200								
.150								
.100								
.050								

Table 3. Continued

(p) Continued; station 2

THETA, DEG	CP FOR ALPHA, DEG =							
	-4.00	.06	3.96	7.99	12.03	15.97	20.01	23.99
	.006	.014	.005	-.016	-.040	-.050	-.061	-.077
0	.003	.015	.008	-.007	-.029	-.043	-.057	-.066
15	.002	.013	.009	-.006	-.031	-.045	-.057	-.067
30	.004	.013	.010	-.010	-.031	-.052	-.061	-.071
45	.006	.009	.009	-.023	-.035	-.055	-.065	-.072
60	.013	.012	.012	-.002	-.030	-.065	-.076	-.076
75								
90								
105	.009	.007	.008	-.004	-.037	-.079	-.105	-.100
120	.008	.009	.009	-.022	-.040	-.063	-.077	-.089
135	.005	.010	.008	-.010	-.035	-.059	-.076	-.086
150	.003	.010	.006	-.009	-.038	-.059	-.075	-.085
165	.004	.012	.004	-.012	-.035	-.056	-.072	-.082
180	.006	.010	.000	-.023	-.049	-.065	-.082	-.095
195	.010	.012	.001	-.037	-.066	-.068	-.058	-.044
210	.011	.012	.002	-.033	-.038	-.025	-.004	.022
225	.010	.010	.002	-.013	-.003	.023	.059	.101
240	.011	.011	.007	.009	.031	.070	.121	.180
255	.014	.011	.010	.022	.053	.101	.163	.233
270								
285	.016	.018	.015	.029	.065	.114	.177	.247
300	.013	.016	.010	.015	.042	.082	.136	.197
315	.013	.016	.009	-.004	.011	.038	.076	.121
330	.011	.014	.006	-.027	-.028	-.015	.009	.037
345	.009	.014	.005	-.029	-.059	-.060	-.051	-.036
Y/S	CP FOR ALPHA, DEG =							
	-4.00	.06	3.96	7.99	12.03	15.97	20.01	23.99
.075								
.150								
.225								
.300	.017	.018	.014	.028	.064	.112	.173	.241
.375	.020	.019	.016	.029	.062	.109	.168	.237
.450								
.524	.019	.019	.019	.028	.057	.100	.152	.214
.599								
.637								
.674	.011	.007	-.004	.003	.026	.059	.095	.138
.674	-.012	-.013	.001	.012	.013	.005	-.090	-.103
.637	-.003	.006	.011	.015	.013	-.008	-.103	-.109
.599	.006	.009	.012	.015	.012	-.027	-.108	-.111
.524	.010	.008	.012	.016	.003	-.074	-.103	-.108
.450	.007	.006	.009	.012	-.021	-.093	-.102	-.109
.375	.009	.007	.010	.008	-.038	-.076	-.099	-.102
.300	.010	.008	.011	.004	-.032	-.077	-.099	-.100
.225								
.150								
.075								

Table 3. Continued

(p) Concluded; station 3

	THETA, DEG	CP FOR ALPHA, DEG =							
		-4.00	.06	3.96	7.99	12.03	15.97	20.01	23.99
BODY	0	.009	.019	.009	-.012	-.037	-.050	-.057	-.076
	15	.008	.018	.011	-.004	-.023	-.038	-.048	-.063
	30	.006	.015	.009	-.005	-.025	-.039	-.051	-.067
	45	.010	.015	.012	-.004	-.023	-.042	-.054	-.067
	60	.011	.013	.010	-.013	-.025	-.042	-.050	-.065
	75	.015	.014	.013	-.003	-.028	-.062	-.056	-.062
	90								
	105	.015	.012	.012	-.004	-.033	-.068	-.091	-.091
	120	.011	.010	.010	-.018	-.037	-.061	-.082	-.089
	135	.010	.012	.010	-.007	-.032	-.054	-.071	-.084
	150	.007	.012	.009	-.006	-.031	-.050	-.071	-.085
	165	.006	.013	.006	-.007	-.031	-.050	-.070	-.084
	180	.007	.012	.004	-.015	-.037	-.056	-.075	-.093
	195	.009	.014	.004	-.024	-.057	-.068	-.058	-.043
	210	.012	.017	.009	-.019	-.035	-.022	.002	.030
	225	.009	.015	.010	-.006	.002	.027	.064	.112
	240	.007	.013	.013	.014	.037	.074	.128	.191
	255	.013	.015	.019	.029	.060	.103	.164	.234
	270								
	285	.019	.021	.026	.037	.068	.113	.172	.242
	300	.012	.020	.021	.022	.046	.087	.143	.206
315	.014	.021	.018	.006	.011	.041	.080	.129	
330	.013	.020	.013	-.010	-.027	-.013	.012	.042	
345	.014	.020	.013	-.015	-.057	-.057	-.046	-.030	
	Y/S	CP FOR ALPHA, DEG =							
		-4.00	.06	3.96	7.99	12.03	15.97	20.01	23.99
WINDWARD WING	.190								
	.274	.021	.025	.028	.039	.068	.112	.170	.238
	.379	.018	.020	.022	.031	.064	.107	.165	.232
	.473	.022	.024	.025	.032	.063	.106	.161	.226
	.569								
	.664	.021	.021	.020	.030	.057	.097	.143	.203
	.759	.021	.019	.020	.028	.051	.091	.134	.188
	.806	.023	.021	.016	.017	.045	.081	.119	.165
	.854	.022	.012	-.005	.008	.031	.066	.096	.132
LEEWARD WING	.854	-.009	-.004	.014	.017	.020	.026	-.051	-.089
	.806	-.001	.010	.012	.014	.017	.018	-.071	-.092
	.759	.010	.012	.013	.016	.019	.008	-.078	-.089
	.664	.010	.011	.013	.016	.014	-.044	-.093	-.101
	.569	.009	.009	.012	.015	-.005	-.090	-.103	-.109
	.473	.013	.012	.014	.014	-.038	-.092	-.094	-.102
	.379	.013	.010	.013	.001	-.043	-.076	-.090	-.097
	.274	.018	.014	.015	.003	-.031	-.066	-.087	-.090
.190									

Table 3. Continued

(q) $M_\infty = 1.70$; $\phi = -30^\circ$; station 1

THETA, DEG	CP FOR ALPHA, DEG =							
	-3.99	-.01	3.99	8.02	12.04	15.99	20.06	24.04
0								
15	-.008	.008	.026	.045	.058	.107	.182	.259
30	-.008	.006	.028	.055	.089	.151	.231	.321
45	-.008	.006	.031	.068	.113	.180	.264	.357
60	-.013	.005	.034	.076	.128	.197	.281	.376
75	-.013	.008	.041	.080	.120	.181	.264	.367
90								
105	.030	.003	-.031	-.086	-.193	-.277	-.368	-.412
120	.023	-.001	-.031	-.068	-.101	-.179	-.268	-.314
135	.025	.006	-.020	-.052	-.070	-.107	-.159	-.212
BODY 150	.022	.004	-.020	-.049	-.073	-.117	-.130	-.175
165	.019	.001	-.020	-.051	-.090	-.125	-.135	-.166
180	.023	.004	-.015	-.054	-.137	-.197	-.145	-.169
195	.026	.006	-.011	-.037	-.062	-.087	-.168	-.168
210	.034	.012	-.006	-.018	-.036	-.062	-.143	-.164
225	.039	.013	-.008	-.034	-.061	-.101	-.200	-.227
240	.042	.011	-.013	-.060	-.150	-.238	-.242	-.256
255	.048	.012	-.015	-.055	-.107	-.188	-.205	-.237
270								
285	-.032	-.003	.027	.040	.016	-.041	-.051	-.034
300	-.028	-.001	.025	.050	.073	.049	.059	.081
315	-.026	-.001	.019	.041	.066	.070	.062	.064
330	-.019	.003	.019	.033	.041	.027	-.086	-.090
345	-.016	.005	.019	.034	.024	-.036	.000	.041
Y/S	CP FOR ALPHA, DEG =							
	-3.99	-.01	3.99	8.02	12.04	15.99	20.06	24.04
.050								
.100								
.150								
.200								
WINDWARD .250								
WING .300	-.033	-.005	.030	.063	.098	.102	.072	.058
.350	-.030	-.006	.033	.076	.126	.156	.159	.103
.400	-.187	-.007	.035	.078	.129	.189	.261	.332
.425								
.450	-.155	-.005	.043	.078	.117	.172	.218	.282
.450	.051	.005	-.143	-.235	-.324	-.355	-.398	-.422
.425	.046	.006	-.152	-.252	-.343	-.352	-.395	-.419
.400	.046	.007	-.155	-.255	-.336	-.354	-.398	-.421
.350	.040	.004	-.022	-.194	-.327	-.326	-.369	-.390
LEEWARD .300	.033	.001	-.033	-.085	-.151	-.218	-.341	-.413
WING .250								
.200								
.150								
.100								
.050								

Table 3. Continued

(q) Continued; station 2

THETA, DEG	CP FOR ALPHA, DEG =							
	-3.99	-.01	3.99	8.02	12.04	15.99	20.06	24.04
0	-.029	.001	.026	.057	.092	.117	.150	.183
15	-.026	.001	.029	.066	.106	.141	.185	.242
30	-.023	.004	.034	.077	.123	.169	.225	.293
45	-.025	.004	.036	.083	.132	.186	.248	.335
60	-.026	.005	.039	.087	.132	.180	.245	.344
75	-.030	.002	.040	.093	.150	.214	.284	.385
90								
105	.037	.009	-.018	-.042	-.120	-.236	-.330	-.384
120	.028	.001	-.027	-.053	-.132	-.268	-.360	-.396
135	.032	.005	-.024	-.050	-.098	-.137	-.247	-.309
BODY 150	.032	.008	-.021	-.048	-.089	-.102	-.161	-.223
165	.027	.004	-.024	-.054	-.090	-.101	-.149	-.210
180	.031	.007	-.020	-.063	-.102	-.105	-.142	-.201
195	.028	.004	-.022	-.055	-.093	-.118	-.137	-.175
210	.033	.007	-.018	-.042	-.077	-.114	-.123	-.160
225	.036	.007	-.019	-.046	-.086	-.129	-.186	-.230
240	.037	.007	-.022	-.058	-.089	-.125	-.228	-.250
255	.038	.006	-.024	-.055	-.064	-.107	-.184	-.221
270								
285	-.031	-.003	.030	.057	.083	.129	.157	.194
300	-.027	.002	.033	.071	.104	.149	.191	.241
315	-.029	.001	.031	.067	.101	.147	.193	.244
330	-.030	.001	.026	.057	.085	.125	.167	.203
345	-.026	.006	.029	.058	.084	.110	.153	.153
Y/S	CP FOR ALPHA, DEG =							
	-3.99	-.01	3.99	8.02	12.04	15.99	20.06	24.04
.075								
.150								
.225								
WINDWARD .300	-.025	.003	.037	.074	.093	.129	.167	.217
.375	-.021	.005	.041	.089	.111	.108	.129	.166
WING .450								
.524	-.093	.002	.040	.085	.134	.221	.286	.365
.599								
.637								
.674	-.129	-.004	.052	.083	.116	.163	.212	.271
.674	.053	.008	-.115	-.186	-.248	-.307	-.343	-.368
.637	.050	.010	-.127	-.207	-.275	-.336	-.365	-.379
.599	.046	.009	-.165	-.217	-.303	-.338	-.361	-.376
.524	.039	.005	-.063	-.254	-.300	-.352	-.375	-.396
LEEWARD .450	.044	.011	-.005	-.176	-.332	-.376	-.374	-.373
WING .375	.043	.010	-.016	-.050	-.187	-.268	-.286	-.325
.300	.034	.004	-.024	-.045	-.116	-.230	-.343	-.396
.225								
.150								
.075								

Table 3. Continued

(q) Concluded; station 3

THETA, DEG	CP FOR ALPHA, DEG =							
	-3.99	-.01	3.99	8.02	12.04	15.99	20.06	24.04
0	-.030	-.001	.026	.061	.095	.128	.179	.228
15	-.024	.003	.033	.069	.109	.157	.215	.274
30	-.025	.000	.032	.069	.118	.178	.234	.299
45	-.027	-.001	.032	.073	.124	.191	.255	.340
60	-.033	-.002	.032	.079	.139	.210	.288	.371
75	-.043	-.003	.033	.084	.141	.207	.284	.367
90								
BODY								
105	.040	.009	-.018	-.049	-.105	-.195	-.325	-.366
120	.037	.006	-.022	-.054	-.116	-.251	-.336	-.372
135	.037	.007	-.023	-.056	-.100	-.162	-.295	-.374
150	.039	.009	-.022	-.056	-.092	-.119	-.223	-.303
165	.036	.006	-.025	-.060	-.091	-.118	-.203	-.289
180	.040	.010	-.021	-.063	-.084	-.116	-.197	-.291
195	.039	.012	-.020	-.058	-.086	-.118	-.188	-.263
210	.036	.008	-.023	-.050	-.076	-.113	-.151	-.200
225	.039	.010	-.022	-.049	-.072	-.111	-.142	-.176
240	.041	.008	-.026	-.050	-.070	-.108	-.131	-.148
255	.038	.002	-.040	-.055	-.069	-.109	-.128	-.144
270								
285	-.029	-.001	.031	.065	.112	.151	.197	.257
300	-.033	-.006	.026	.066	.115	.156	.212	.274
315	-.025	.005	.035	.075	.125	.167	.224	.288
330	-.031	-.001	.028	.063	.110	.144	.195	.256
345	-.032	-.003	.025	.057	.093	.125	.165	.220
Y/S	CP FOR ALPHA, DEG =							
	-3.99	-.01	3.99	8.02	12.04	15.99	20.06	24.04
.190								
.274	-.031	-.002	.029	.066	.107	.144	.195	.254
.379	-.026	.001	.035	.075	.100	.114	.155	.205
.473	-.025	-.002	.033	.079	.137	.193	.254	.316
WINDWARD								
WING								
.569								
.664	-.135	-.002	.036	.085	.127	.185	.254	.328
.759	-.160	-.001	.040	.080	.121	.168	.226	.295
.806	-.133	-.003	.043	.076	.116	.156	.208	.272
.854	-.127	-.007	.049	.074	.108	.141	.187	.242
.854	.048	.005	-.113	-.191	-.249	-.301	-.339	-.364
.806	.052	.013	-.116	-.194	-.249	-.317	-.353	-.376
.759	.046	.010	-.161	-.215	-.293	-.354	-.359	-.378
LEEWARD								
WING								
.664	.046	.012	-.082	-.218	-.283	-.342	-.360	-.383
.569	.044	.011	-.005	-.244	-.318	-.359	-.389	-.407
.473	.037	.004	-.024	-.083	-.270	-.350	-.345	-.364
.379	.037	.004	-.025	-.052	-.140	-.218	-.276	-.352
.274	.035	.005	-.024	-.054	-.106	-.202	-.329	-.367
.190								

Table 3. Continued

(r) $M_\infty = 2.16$; $\phi = -30^\circ$; station 1

THETA, DEG	CP FOR ALPHA, DEG =							
	-4.01	.02	3.99	8.02	12.01	15.99	20.02	24.02
0								
15	-.015	-.001	.008	.022	.059	.109	.182	.263
30	-.012	.003	.017	.042	.089	.149	.229	.320
45	-.015	.003	.023	.059	.111	.177	.258	.357
60	-.021	.002	.028	.067	.122	.192	.275	.376
75	-.024	.002	.032	.069	.110	.170	.249	.352
90								
105	.027	.004	-.025	-.085	-.198	-.233	-.258	-.267
120	.024	.002	-.026	-.063	-.093	-.134	-.160	-.168
135	.024	.008	-.016	-.050	-.066	-.091	-.116	-.134
BODY 150	.013	.001	-.019	-.047	-.078	-.095	-.114	-.124
165	.005	-.001	-.019	-.045	-.105	-.110	-.122	-.127
180	.008	.002	-.014	-.048	-.141	-.130	-.134	-.146
195	.014	.004	-.011	-.034	-.049	-.111	-.125	-.144
210	.022	.005	-.011	-.020	-.026	-.081	-.110	-.117
225	.032	.008	-.011	-.036	-.050	-.115	-.142	-.152
240	.036	.006	-.017	-.061	-.149	-.171	-.180	-.205
255	.044	.010	-.016	-.056	-.108	-.144	-.159	-.179
270								
285	-.041	-.006	.017	.019	-.016	-.026	-.009	.002
300	-.036	-.007	.015	.031	.023	.010	.029	.058
315	-.029	-.004	.013	.025	.020	-.005	.007	.029
330	-.025	-.004	.007	.004	-.039	-.073	-.047	-.019
345	-.021	-.002	.006	-.015	-.028	-.005	.040	.087
Y/S	CP FOR ALPHA, DEG =							
	-4.01	.02	3.99	8.02	12.01	15.99	20.02	24.02
.050								
.100								
.150								
.200								
WINDWARD .250								
WING .300	-.038	-.006	.024	.053	.058	.022	.020	.040
.350	-.047	-.007	.026	.066	.093	.095	.082	.082
.400	-.159	-.009	.027	.068	.113	.163	.227	.306
.425								
.450	-.135	-.022	.037	.072	.106	.146	.198	.268
.450	.046	.002	-.117	-.188	-.242	-.257	-.268	-.273
.425	.046	.007	-.125	-.205	-.249	-.260	-.268	-.272
.400	.039	.002	-.138	-.209	-.253	-.263	-.270	-.275
.350	.037	.001	-.025	-.203	-.256	-.263	-.270	-.270
LEEWARD .300	.031	.001	-.029	-.088	-.174	-.194	-.240	-.265
WING .250								
.200								
.150								
.100								
.050								

Table 3. Continued

(r) Continued; station 2

THETA, DEG	CP FOR ALPHA, DEG =							
	-4.01	.02	3.99	8.02	12.01	15.99	20.02	24.02
0	.009	.034	.055	.039	.054	.057	.089	.147
15	.012	.035	.058	.047	.068	.103	.159	.232
30	.009	.031	.055	.051	.081	.138	.205	.288
45	.006	.031	.057	.055	.096	.162	.237	.328
60	.001	.029	.056	.056	.094	.154	.232	.330
75	.005	.034	.062	.068	.122	.196	.277	.372
90								
105	.059	.031	.008	-.051	-.122	-.188	-.236	-.259
120	.068	.041	.017	-.051	-.123	-.186	-.230	-.257
135	.064	.039	.014	-.049	-.086	-.129	-.165	-.176
150	.062	.038	.011	-.049	-.086	-.092	-.131	-.149
165	.065	.042	.014	-.052	-.083	-.086	-.124	-.138
180	.062	.039	.011	-.064	-.117	-.094	-.131	-.145
195	.067	.041	.017	-.051	-.071	-.100	-.123	-.131
210	.066	.038	.017	-.041	-.065	-.081	-.108	-.123
225	.061	.032	.010	-.049	-.080	-.107	-.153	-.177
240	.064	.034	.009	-.060	-.085	-.153	-.184	-.195
255	.066	.034	.008	-.053	-.058	-.120	-.163	-.180
270								
285	.010	.037	.061	.041	.061	.077	.103	.145
300	.005	.033	.057	.048	.082	.109	.137	.187
315	.009	.036	.059	.049	.083	.115	.144	.196
330	.008	.034	.055	.041	.073	.095	.114	.167
345	.007	.033	.053	.035	.056	.062	.039	.060
Y/S	CP FOR ALPHA, DEG =							
	-4.01	.02	3.99	8.02	12.01	15.99	20.02	24.02
.075								
.150								
.225								
.300	.005	.033	.058	.054	.079	.097	.122	.168
.375	.011	.034	.063	.067	.086	.095	.105	.133
.450								
.524	-.105	.037	.068	.070	.126	.189	.249	.336
.599								
.637								
.674	-.076	.023	.073	.068	.106	.146	.185	.248
.674	.079	.036	-.070	-.164	-.192	-.220	-.245	-.257
.637	.080	.040	-.071	-.156	-.197	-.227	-.252	-.263
.599	.078	.041	-.088	-.179	-.223	-.240	-.260	-.266
.524	.079	.045	-.062	-.185	-.221	-.239	-.258	-.266
.450	.066	.036	.022	-.192	-.238	-.251	-.267	-.273
.375	.067	.034	.017	-.072	-.169	-.199	-.220	-.232
.300	.070	.039	.016	-.048	-.106	-.183	-.237	-.260
.225								
.150								
.075								

Table 3. Continued

(r) Concluded; station 3

	THETA, DEG	CP FOR ALPHA, DEG =							
		-4.01	.02	3.99	8.02	12.01	15.99	20.02	24.02
BODY	0	-.028	-.001	.023	.046	.075	.102	.132	.190
	15	-.024	-.001	.026	.052	.084	.121	.170	.239
	30	-.028	-.007	.020	.055	.091	.133	.192	.266
	45	-.027	-.004	.023	.058	.102	.152	.215	.295
	60	-.031	-.006	.023	.062	.114	.170	.254	.348
	75	-.036	-.007	.027	.066	.115	.177	.264	.359
	90								
	105	.033	.005	-.021	-.047	-.111	-.178	-.222	-.242
	120	.033	.004	-.021	-.051	-.121	-.196	-.231	-.245
	135	.031	.002	-.023	-.051	-.092	-.144	-.174	-.216
	150	.031	.003	-.023	-.054	-.084	-.112	-.141	-.165
	165	.029	.003	-.022	-.054	-.079	-.112	-.141	-.164
	180	.029	.002	-.023	-.059	-.085	-.112	-.148	-.172
	195	.033	.003	-.022	-.055	-.077	-.115	-.141	-.168
	210	.035	.005	-.018	-.038	-.061	-.096	-.109	-.133
	225	.032	.003	-.020	-.042	-.064	-.095	-.132	-.139
	240	.031	.001	-.025	-.045	-.062	-.091	-.127	-.133
	255	.035	.001	-.029	-.042	-.059	-.088	-.114	-.127
	270								
	285	-.023	.001	.027	.053	.086	.114	.160	.219
	300	-.025	.000	.026	.056	.096	.131	.181	.245
	315	-.027	.000	.026	.057	.098	.136	.185	.250
	330	-.026	.001	.025	.053	.092	.123	.166	.227
	345	-.025	.001	.025	.047	.078	.098	.127	.176
	Y/S	CP FOR ALPHA, DEG =							
		-4.01	.02	3.99	8.02	12.01	15.99	20.02	24.02
WINDWARD WING	.190								
	.274	-.023	.001	.028	.058	.090	.120	.166	.223
	.379	-.026	-.004	.027	.061	.074	.088	.122	.160
	.473	-.016	.002	.034	.074	.123	.173	.230	.295
	.569								
	.664	-.145	.003	.039	.071	.118	.172	.239	.315
	.759	-.113	.001	.039	.069	.109	.157	.213	.279
	.806	-.105	.001	.041	.071	.106	.149	.201	.262
	.854	-.102	-.004	.043	.072	.102	.139	.184	.239
LEEWARD WING	.854	.051	.006	-.093	-.151	-.191	-.210	-.231	-.234
	.806	.044	.003	-.100	-.153	-.191	-.215	-.236	-.237
	.759	.043	.005	-.112	-.160	-.199	-.227	-.244	-.235
	.664	.039	.004	-.108	-.172	-.215	-.235	-.247	-.237
	.569	.036	.003	-.009	-.204	-.224	-.242	-.252	-.244
	.473	.040	.006	-.016	-.107	-.221	-.238	-.246	-.250
	.379	.036	.003	-.022	-.049	-.147	-.176	-.196	-.223
	.274	.036	.007	-.019	-.047	-.108	-.177	-.224	-.242
	.190								

Table 3. Continued

(s) $M_\infty = 2.40; \phi = -30^\circ$; station 1

THETA, DEG	CP FOR ALPHA, DEG =							
	-3.97	.03	4.01	8.03	12.03	16.03	20.08	24.03
0								
15	-.005	.008	.014	.031	.068	.125	.196	.283
30	-.007	.007	.019	.050	.095	.161	.241	.336
45	-.010	.008	.028	.068	.119	.189	.275	.374
60	-.016	.007	.033	.078	.133	.205	.293	.394
75	-.016	.011	.041	.080	.126	.185	.267	.369
90								
105	.030	.004	-.025	-.088	-.157	-.193	-.211	-.217
120	.024	-.001	-.028	-.060	-.081	-.113	-.130	-.132
135	.023	.005	-.019	-.043	-.057	-.083	-.101	-.118
150	.014	.002	-.017	-.039	-.066	-.084	-.097	-.110
165	.004	-.001	-.015	-.041	-.103	-.105	-.112	-.119
180	.004	-.001	-.012	-.044	-.124	-.117	-.122	-.130
195	.012	.003	-.008	-.034	-.051	-.108	-.118	-.134
210	.025	.007	-.003	-.012	-.022	-.077	-.096	-.112
225	.034	.009	-.004	-.025	-.044	-.106	-.122	-.140
240	.039	.008	-.009	-.052	-.126	-.142	-.162	-.177
255	.047	.013	-.007	-.046	-.103	-.127	-.144	-.166
270								
285	-.032	.001	.023	.017	-.004	-.009	-.003	.016
300	-.029	.001	.021	.033	.020	.015	.031	.058
315	-.025	.001	.015	.024	.008	-.010	-.001	.019
330	-.017	.004	.011	-.004	-.046	-.043	-.022	.010
345	-.013	.005	.007	-.017	-.011	.017	.057	.109
Y/S	CP FOR ALPHA, DEG =							
	-3.97	.03	4.01	8.03	12.03	16.03	20.08	24.03
.050								
.100								
.150								
.200								
WINDWARD								
WING								
.250								
.300	-.032	.001	.029	.058	.043	.016	.020	.042
.350	-.051	.001	.032	.073	.089	.083	.080	.089
.400	-.130	.000	.035	.076	.118	.164	.231	.296
.425								
.450	-.116	-.013	.041	.076	.110	.146	.199	.258
.450	.047	.000	-.102	-.167	-.194	-.206	-.214	-.219
.425	.049	.006	-.103	-.167	-.198	-.208	-.214	-.217
.400	.048	.008	-.109	-.172	-.197	-.207	-.213	-.215
.350	.044	.005	-.024	-.180	-.204	-.213	-.217	-.219
LEEWARD	.035	.001	-.027	-.099	-.155	-.182	-.199	-.214
WING								
.250								
.200								
.150								
.100								
.050								

Table 3. Continued

(s) Continued; station 2

THETA, DEG	CP FOR ALPHA, DEG =							
	-3.97	.03	4.01	8.03	12.03	16.03	20.08	24.03
0	-.013	.011	.030	.048	.049	.071	.119	.190
15	-.009	.012	.033	.055	.071	.120	.185	.272
30	-.006	.015	.037	.063	.098	.157	.234	.331
45	-.010	.013	.037	.069	.114	.180	.265	.368
60	-.012	.013	.039	.075	.120	.177	.261	.367
75	-.014	.011	.040	.085	.141	.213	.305	.411
90								
105	.042	.014	-.005	-.035	-.103	-.155	-.186	-.204
120	.036	.009	-.011	-.040	-.097	-.138	-.163	-.190
135	.039	.013	-.008	-.033	-.070	-.094	-.116	-.122
BODY 150	.040	.016	-.005	-.031	-.064	-.076	-.106	-.124
165	.038	.015	-.005	-.034	-.064	-.073	-.096	-.118
180	.039	.016	-.004	-.043	-.073	-.073	-.095	-.113
195	.037	.012	-.006	-.042	-.065	-.081	-.099	-.120
210	.042	.016	-.003	-.022	-.050	-.058	-.096	-.110
225	.041	.015	-.004	-.026	-.063	-.089	-.130	-.146
240	.043	.015	-.005	-.034	-.071	-.133	-.149	-.159
255	.043	.014	-.007	-.029	-.047	-.118	-.140	-.158
270								
285	-.016	.010	.034	.049	.059	.075	.110	.151
300	-.013	.013	.037	.062	.084	.105	.147	.195
315	-.015	.012	.035	.061	.084	.105	.147	.200
330	-.015	.011	.032	.054	.071	.079	.109	.151
345	-.011	.014	.034	.051	.055	.035	.049	.100
Y/S	CP FOR ALPHA, DEG =							
	-3.97	.03	4.01	8.03	12.03	16.03	20.08	24.03
.075								
.150								
.225								
.300	-.012	.015	.042	.069	.085	.101	.140	.187
WINDWARD WING .375	-.006	.017	.046	.081	.093	.095	.116	.148
.450								
.524	-.114	.013	.044	.083	.130	.190	.265	.356
.599								
.637								
.674	-.090	.007	.051	.083	.112	.157	.206	.275
.674	.062	.013	-.082	-.130	-.155	-.180	-.193	-.203
.637	.059	.015	-.084	-.129	-.156	-.182	-.195	-.205
.599	.056	.015	-.087	-.137	-.170	-.190	-.202	-.208
.524	.048	.011	-.088	-.156	-.184	-.199	-.209	-.216
LEEWARD WING .450	.052	.017	.003	-.166	-.184	-.197	-.206	-.212
.375	.050	.017	-.001	-.074	-.145	-.173	-.186	-.194
.300	.042	.010	-.009	-.034	-.095	-.151	-.190	-.208
.225								
.150								
.075								

Table 3. Continued

(s) Concluded; station 3

THETA, DEG	CP FOR ALPHA, DEG =							
	-3.97	.03	4.01	8.03	12.03	16.03	20.08	24.03
0	-.022	.004	.024	.045	.064	.087	.122	.167
15	-.017	.006	.028	.052	.078	.110	.167	.247
30	-.019	.003	.026	.055	.085	.127	.202	.294
45	-.022	.002	.026	.059	.100	.152	.233	.326
60	-.025	.001	.027	.065	.114	.182	.271	.379
75	-.025	.006	.032	.073	.123	.194	.286	.396
90								
105	.038	.008	-.013	-.034	-.100	-.152	-.184	-.197
120	.034	.004	-.018	-.040	-.107	-.160	-.193	-.207
135	.034	.004	-.019	-.042	-.081	-.115	-.136	-.149
BODY 150	.034	.006	-.017	-.044	-.071	-.094	-.119	-.139
165	.030	.004	-.019	-.047	-.069	-.095	-.117	-.148
180	.032	.007	-.015	-.047	-.065	-.093	-.115	-.151
195	.034	.007	-.014	-.054	-.067	-.097	-.114	-.150
210	.033	.005	-.015	-.039	-.061	-.093	-.104	-.148
225	.033	.004	-.016	-.037	-.063	-.097	-.127	-.144
240	.036	.005	-.016	-.036	-.058	-.083	-.126	-.133
255	.037	.003	-.021	-.034	-.058	-.081	-.121	-.127
270								
285	-.019	.005	.029	.051	.081	.114	.156	.218
300	-.023	.002	.025	.054	.088	.130	.176	.241
315	-.015	.011	.034	.063	.097	.142	.191	.256
330	-.022	.004	.026	.053	.084	.127	.170	.229
345	-.024	.001	.023	.045	.064	.095	.125	.170
Y/S	CP FOR ALPHA, DEG =							
	-3.97	.03	4.01	8.03	12.03	16.03	20.08	24.03
.190								
.274	-.021	.003	.027	.053	.084	.120	.164	.222
.379	-.016	.005	.033	.060	.074	.096	.123	.163
.473	-.014	.002	.031	.071	.123	.180	.238	.302
WINDWARD .569								
WING .664	-.125	.003	.035	.075	.120	.176	.241	.327
.759	-.099	.006	.040	.076	.116	.165	.219	.296
.806	-.094	.005	.041	.076	.112	.156	.206	.277
.854	-.092	.001	.043	.075	.106	.143	.189	.255
.854	.049	.005	-.083	-.131	-.163	-.185	-.195	-.187
.806	.052	.011	-.080	-.126	-.158	-.180	-.191	-.184
.759	.048	.008	-.090	-.130	-.160	-.184	-.195	-.188
LEEWARD .664	.048	.011	-.089	-.145	-.177	-.194	-.197	-.191
WING .569	.044	.010	-.008	-.162	-.181	-.196	-.198	-.188
.473	.035	.003	-.010	-.128	-.194	-.205	-.205	-.197
.379	.035	.002	-.015	-.043	-.136	-.162	-.181	-.193
.274	.035	.004	-.017	-.037	-.097	-.156	-.189	-.202
.190								

Table 3. Continued

(t) $M_\infty = 2.86$; $\phi = -30^\circ$; station 1

THETA, DEG	CP FOR ALPHA, DEG =							
	-3.95	-.03	3.96	8.00	12.01	16.01	20.02	24.01
0								
15	.002	.007	.013	.030	.068	.113	.180	.261
30	.006	.012	.024	.050	.097	.151	.228	.319
45	.003	.013	.031	.064	.119	.179	.261	.357
60	-.005	.011	.035	.072	.132	.193	.280	.379
75	-.007	.013	.039	.073	.122	.173	.251	.347
90								
105	.031	.012	-.014	-.057	-.100	-.122	-.139	-.145
120	.028	.011	-.013	-.043	-.056	-.072	-.081	-.085
135	.028	.015	-.005	-.028	-.045	-.062	-.070	-.077
BODY 150	.013	.007	-.008	-.029	-.057	-.066	-.072	-.082
165	.005	.005	-.006	-.027	-.079	-.083	-.084	-.086
180	.008	.007	-.002	-.024	-.081	-.084	-.089	-.093
195	.017	.010	.002	-.016	-.040	-.078	-.087	-.094
210	.025	.009	.000	-.008	-.022	-.061	-.079	-.084
225	.035	.012	-.001	-.018	-.042	-.082	-.095	-.106
240	.039	.010	-.007	-.038	-.096	-.108	-.121	-.126
255	.044	.014	-.007	-.036	-.085	-.103	-.114	-.122
270								
285	-.026	.003	.022	.015	.003	.001	.007	.029
300	-.023	.003	.018	.025	.013	.016	.032	.058
315	-.012	.009	.018	.021	.000	-.001	.011	.035
330	-.009	.006	.010	-.011	-.027	-.015	.006	.036
345	-.004	.007	.007	-.003	.009	.035	.072	.119
Y/S	CP FOR ALPHA, DEG =							
	-3.95	-.03	3.96	8.00	12.01	16.01	20.02	24.01
.050								
.100								
.150								
.200								
WINDWARD .250								
WING .300	-.023	.004	.028	.048	.028	.022	.029	.051
.350	-.059	.003	.031	.063	.075	.081	.088	.104
.400	-.091	-.001	.031	.066	.107	.148	.202	.278
.425								
.450	-.079	-.010	.039	.073	.106	.140	.185	.247
.450	.048	.009	-.074	-.118	-.135	-.142	-.145	-.147
.425	.047	.012	-.071	-.113	-.131	-.138	-.143	-.146
.400	.040	.006	-.080	-.123	-.142	-.147	-.150	-.151
.350	.037	.007	-.027	-.126	-.142	-.147	-.150	-.152
LEeward .300	.035	.010	-.016	-.071	-.111	-.126	-.136	-.141
WING .250								
.200								
.150								
.100								
.050								

Table 3. Continued

(t) Continued; station 2

	THETA, DEG	CP FOR ALPHA, DEG =							
		-3.95	-.03	3.96	8.00	12.01	16.01	20.02	24.01
BODY	0	-.002	.013	.028	.039	.047	.084	.139	.201
	15	.002	.016	.031	.046	.080	.128	.196	.274
	30	.000	.013	.029	.053	.100	.155	.234	.321
	45	-.001	.014	.032	.062	.117	.178	.264	.357
	60	-.007	.010	.030	.063	.113	.168	.254	.350
	75	-.004	.013	.037	.079	.143	.209	.303	.403
	90								
	105	.031	.008	-.013	-.037	-.093	-.126	-.144	-.153
	120	.037	.014	-.006	-.029	-.066	-.082	-.095	-.134
	135	.035	.013	-.007	-.028	-.053	-.068	-.079	-.080
	150	.032	.013	-.008	-.028	-.052	-.065	-.080	-.082
	165	.033	.015	-.005	-.026	-.046	-.054	-.070	-.082
	180	.030	.011	-.008	-.037	-.053	-.058	-.074	-.089
	195	.034	.014	-.004	-.029	-.053	-.055	-.071	-.088
	210	.033	.011	-.005	-.018	-.044	-.050	-.077	-.090
	225	.029	.006	-.011	-.027	-.057	-.082	-.108	-.116
	240	.032	.009	-.009	-.036	-.071	-.109	-.119	-.126
	255	.034	.008	-.011	-.032	-.062	-.106	-.118	-.125
	270								
	285	-.005	.012	.031	.042	.052	.074	.104	.145
	300	-.007	.010	.028	.048	.066	.091	.125	.172
	315	-.004	.013	.030	.052	.069	.091	.124	.172
	330	-.005	.012	.027	.046	.053	.056	.068	.100
345	-.004	.012	.027	.038	.028	.036	.071	.116	
	Y/S	CP FOR ALPHA, DEG =							
		-3.95	-.03	3.96	8.00	12.01	16.01	20.02	24.01
WINDWARD WING	.075								
	.150								
	.225								
	.300	-.008	.010	.031	.055	.068	.085	.114	.164
	.375	-.003	.011	.034	.065	.077	.084	.100	.141
	.450								
	.524	-.081	.011	.037	.071	.116	.169	.234	.324
	.599								
	.637								
	.674	-.075	-.016	.043	.071	.101	.137	.185	.251
LEEWARD WING	.674	.053	.007	-.072	-.108	-.130	-.140	-.146	-.150
	.637	.051	.012	-.071	-.108	-.128	-.138	-.144	-.149
	.599	.049	.013	-.072	-.108	-.129	-.139	-.145	-.149
	.524	.048	.015	-.064	-.107	-.126	-.137	-.142	-.146
	.450	.041	.011	-.013	-.121	-.138	-.145	-.150	-.153
	.375	.040	.012	-.007	-.081	-.128	-.139	-.144	-.150
	.300	.040	.014	-.007	-.030	-.077	-.111	-.135	-.145
	.225								
	.150								
	.075								

Table 3. Continued

(t) Concluded; station 3

THETA, DEG	CP FOR ALPHA, DEG =							
	-3.95	-.03	3.96	8.00	12.01	16.01	20.02	24.01
0	-.005	.018	.037	.055	.065	.079	.125	.184
15	-.003	.020	.039	.062	.082	.120	.187	.262
30	-.007	.016	.037	.063	.093	.146	.223	.311
45	-.005	.020	.043	.071	.110	.165	.240	.328
60	-.008	.018	.045	.076	.130	.197	.287	.389
75	-.009	.019	.049	.080	.137	.207	.299	.406
90								
105	.042	.016	-.005	-.023	-.077	-.110	-.130	-.138
120	.039	.013	-.008	-.026	-.072	-.094	-.120	-.134
135	.039	.013	-.008	-.028	-.054	-.066	-.076	-.085
BODY 150	.037	.013	-.008	-.029	-.052	-.065	-.080	-.094
165	.036	.013	-.008	-.031	-.050	-.062	-.082	-.101
180	.033	.011	-.008	-.034	-.050	-.064	-.085	-.105
195	.034	.012	-.006	-.033	-.050	-.064	-.079	-.107
210	.038	.015	-.002	-.020	-.047	-.063	-.072	-.110
225	.035	.012	-.006	-.023	-.051	-.078	-.096	-.114
240	.035	.009	-.009	-.026	-.046	-.082	-.105	-.113
255	.040	.013	-.006	-.021	-.043	-.077	-.101	-.109
270								
285	.002	.020	.039	.059	.083	.111	.148	.199
300	-.004	.017	.037	.063	.093	.124	.165	.223
315	-.004	.019	.039	.065	.094	.127	.172	.232
330	-.004	.019	.038	.062	.086	.114	.157	.212
345	.000	.021	.039	.059	.069	.081	.093	.125
Y/S	CP FOR ALPHA, DEG =							
	-3.95	-.03	3.96	8.00	12.01	16.01	20.02	24.01
.190								
.274	.002	.020	.042	.065	.089	.116	.156	.211
.379	-.003	.013	.038	.065	.074	.089	.116	.156
.473	.008	.018	.042	.080	.129	.175	.231	.301
WINDWARD 569								
WING .664	-.074	.016	.044	.079	.123	.172	.234	.320
.759	-.072	.014	.044	.077	.116	.158	.211	.288
.806	-.068	.013	.046	.078	.114	.152	.203	.275
.854	-.067	-.005	.050	.080	.112	.144	.193	.258
.854	.056	.013	-.063	-.094	-.118	-.128	-.129	-.125
.806	.049	.017	-.071	-.101	-.124	-.134	-.134	-.129
.759	.051	.019	-.066	-.094	-.119	-.130	-.130	-.126
LEEWARD 664	.047	.016	-.059	-.104	-.126	-.137	-.138	-.131
WING 569	.044	.015	-.034	-.115	-.131	-.140	-.140	-.132
.473	.047	.019	.002	-.106	-.131	-.137	-.135	-.128
.379	.043	.015	-.005	-.034	-.109	-.126	-.136	-.133
.274	.047	.019	-.002	-.019	-.071	-.107	-.129	-.134
.190								

Table 3. Continued

(u) $M_\infty = 1.70; \phi = -60^\circ$; station 1

THETA, DEG	CP FOR ALPHA, DEG =							
	-3.98	.00	4.00	7.97	12.03	16.02	20.04	23.98
0								
15	-.006	.008	.010	-.001	-.035	-.040	-.012	.027
30	-.005	.006	.013	.014	.008	.037	.088	.147
45	-.002	.008	.019	.032	.051	.099	.170	.243
60	-.002	.006	.022	.045	.079	.139	.223	.304
75	.000	.008	.028	.058	.100	.164	.249	.338
90								
105	.021	.000	-.017	-.039	-.089	-.189	-.238	-.257
120	.014	-.003	-.023	-.050	-.070	-.058	-.077	-.062
135	.016	.004	-.017	-.052	-.081	-.061	-.148	-.158
BODY 150	.007	.002	-.018	-.055	-.079	-.060	-.133	-.146
165	.000	-.001	-.017	-.044	-.061	-.077	-.096	-.154
180	.002	.001	-.012	-.035	-.059	-.102	-.096	-.139
195	.007	.004	-.008	-.033	-.072	-.097	-.099	-.144
210	.017	.008	-.001	-.033	-.118	-.166	-.110	-.151
225	.023	.010	.001	-.023	-.050	-.063	-.145	-.153
240	.026	.008	-.002	-.012	-.034	-.036	-.104	-.122
255	.033	.010	-.002	-.017	-.035	-.036	-.081	-.108
270								
285	-.019	-.001	.016	.013	-.018	-.040	-.104	-.162
300	-.022	-.001	.014	.018	.005	-.046	-.126	-.187
315	-.023	-.001	.010	.013	-.001	-.066	-.202	-.232
330	-.017	.002	.008	-.003	-.037	-.125	-.258	-.245
345	-.014	.003	.005	-.017	-.088	-.209	-.230	-.224
Y/S	CP FOR ALPHA, DEG =							
	-3.98	.00	4.00	7.97	12.03	16.02	20.04	23.98
.050								
.100								
.150								
.200								
WINDWARD .250								
WING .300	-.020	-.003	.019	.030	.021	-.034	-.104	-.161
.350	-.015	-.004	.021	.045	.050	-.062	-.122	-.168
.400	-.099	-.005	.021	.048	.093	.012	-.098	-.145
.425								
.450	-.118	-.003	.028	.050	.082	.135	.030	-.049
.450	.035	.002	-.106	-.168	-.231	-.276	-.283	-.283
.425	.031	.003	-.092	-.187	-.246	-.277	-.290	-.299
.400	.031	.003	-.058	-.196	-.257	-.305	-.312	-.315
.350	.029	.000	-.012	-.082	-.297	-.318	-.328	-.336
LEEWARD .300	.023	-.002	-.020	-.041	-.107	-.193	-.204	-.200
WING .250								
.200								
.150								
.100								
.050								

Table 3. Continued

(u) Continued; station 2

	THETA, DEG	CP FOR ALPHA, DEG =							
		-3.98	.00	4.00	7.97	12.03	16.02	20.04	23.98
BODY	0	-.023	-.001	.008	.001	-.022	-.116	-.164	-.153
	15	-.022	-.001	.010	.009	-.003	-.068	-.053	-.028
	30	-.019	.001	.016	.025	.029	.001	.052	.096
	45	-.018	.000	.019	.037	.054	.068	.130	.198
	60	-.017	.000	.021	.047	.082	.116	.192	.272
	75	-.019	-.002	.021	.053	.096	.141	.224	.310
	90								
	105	.019	.004	-.007	-.010	-.037	-.097	-.188	-.258
	120	.011	-.003	-.016	-.025	-.040	-.065	-.091	-.084
	135	.013	.001	-.014	-.029	-.052	-.056	-.059	-.068
	150	.010	.003	-.012	-.035	-.071	-.080	-.079	-.086
	165	.005	.000	-.017	-.039	-.072	-.078	-.078	-.082
	180	.007	.002	-.014	-.035	-.059	-.066	-.075	-.085
	195	.007	.000	-.016	-.038	-.061	-.071	-.079	-.108
	210	.014	.003	-.014	-.040	-.060	-.072	-.078	-.108
	225	.019	.004	-.010	-.038	-.067	-.085	-.082	-.116
	240	.020	.003	-.011	-.024	-.045	-.078	-.096	-.118
	255	.021	.001	-.012	-.026	-.043	-.074	-.103	-.113
	270								
	285	-.017	-.005	.015	.014	-.003	-.023	-.112	-.140
300	-.018	-.001	.018	.028	.028	-.010	-.102	-.141	
315	-.023	.000	.016	.027	.030	.010	-.075	-.121	
330	-.026	-.001	.013	.018	.023	.013	-.061	-.133	
345	-.021	.002	.014	.009	-.005	-.016	-.102	-.198	
	Y/S	CP FOR ALPHA, DEG =							
		-3.98	.00	4.00	7.97	12.03	16.02	20.04	23.98
WINDWARD WING	.075								
	.150								
	.225								
	.300	-.013	.000	.022	.033	.027	.006	-.069	-.124
	.375	-.010	.002	.026	.047	.037	-.028	-.153	-.197
	.450								
	.524	-.029	.001	.026	.053	.085	.147	.132	.099
	.599								
	.637								
	.674	-.101	-.005	.031	.051	.068	.096	.096	.110
LEEWARD WING	.674	.029	-.001	-.092	-.136	-.183	-.231	-.280	-.303
	.637	.028	.002	-.102	-.142	-.188	-.234	-.284	-.306
	.599	.027	.002	-.098	-.153	-.183	-.227	-.282	-.307
	.524	.022	.000	-.014	-.210	-.219	-.281	-.315	-.324
	.450	.026	.005	-.003	-.068	-.278	-.303	-.329	-.332
	.375	.026	.004	-.008	-.005	-.120	-.260	-.341	-.361
	.300	.017	-.001	-.013	-.014	-.041	-.085	-.172	-.239
	.225								
	.150								
	.075								

Table 3. Continued

(u) Concluded; station 3

THETA, DEG	CP FOR ALPHA, DEG =							
	-3.98	.00	4.00	7.97	12.03	16.02	20.04	23.98
0	-.021	.002	.012	.010	.001	-.044	-.144	-.170
15	-.017	.005	.015	.018	.007	-.017	-.084	-.053
30	-.018	.002	.014	.026	.030	.031	.016	.066
45	-.016	.001	.018	.037	.057	.073	.104	.170
60	-.016	-.002	.020	.045	.078	.112	.166	.245
75	-.025	-.003	.020	.046	.083	.126	.192	.274
90								
105	.028	.011	-.005	-.015	-.025	-.083	-.156	-.250
120	.024	.009	-.011	-.027	-.031	-.068	-.110	-.158
135	.024	.010	-.011	-.037	-.044	-.045	-.051	-.044
BODY 150	.022	.011	-.011	-.044	-.065	-.073	-.079	-.099
165	.016	.008	-.013	-.047	-.073	-.091	-.098	-.115
180	.019	.010	-.010	-.036	-.056	-.072	-.084	-.091
195	.025	.010	-.009	-.033	-.052	-.068	-.081	-.089
210	.022	.008	-.013	-.037	-.055	-.070	-.086	-.094
225	.026	.011	-.010	-.041	-.057	-.068	-.080	-.092
240	.030	.010	-.010	-.026	-.057	-.077	-.079	-.095
255	.024	.004	-.024	-.028	-.053	-.079	-.079	-.088
270								
285	-.007	.005	.020	.024	.028	.017	-.013	-.081
300	-.014	.002	.015	.026	.039	.029	-.019	-.113
315	-.011	.010	.022	.035	.051	.046	.006	-.055
330	-.020	.004	.015	.025	.041	.035	.008	-.049
345	-.023	.002	.012	.013	.019	-.002	-.013	-.064
Y/S	CP FOR ALPHA, DEG =							
	-3.98	.00	4.00	7.97	12.03	16.02	20.04	23.98
.190								
.274	-.009	.004	.019	.028	.035	.027	-.030	-.079
.379	-.006	.006	.025	.034	.012	-.033	-.105	-.146
.473	-.009	.004	.023	.048	.079	.062	-.052	-.123
WINDWARD 569								
WING 664	-.062	.004	.025	.046	.077	.118	.175	.199
.759	-.105	.005	.028	.049	.071	.096	.138	.186
.806	-.101	.004	.028	.051	.064	.082	.115	.153
.854	-.093	.000	.030	.054	.057	.066	.091	.116
.854	.031	.007	-.079	-.134	-.185	-.227	-.264	-.295
.806	.035	.013	-.077	-.132	-.181	-.224	-.260	-.289
.759	.031	.009	-.096	-.142	-.185	-.233	-.265	-.297
LEEWARD 664	.031	.011	-.008	-.182	-.192	-.241	-.279	-.305
WING 569	.029	.009	.000	-.130	-.215	-.249	-.293	-.326
.473	.025	.006	-.011	-.007	-.246	-.315	-.356	-.367
.379	.026	.006	-.011	-.016	-.060	-.196	-.273	-.324
.274	.024	.008	-.011	-.019	-.029	-.080	-.166	-.262
.190								

Table 3. Continued

(v) $M_\infty = 2.16$; $\phi = -60^\circ$; station 1

THETA, DEG	CP FOR ALPHA, DEG =							
	-3.96	.05	3.97	7.97	12.02	16.02	20.06	24.01
0								
15	-.012	-.001	-.001	-.020	-.021	.000	.043	.086
30	-.009	.003	.005	.007	.027	.067	.125	.185
45	-.007	.003	.011	.028	.065	.118	.188	.265
60	-.008	.002	.015	.042	.089	.150	.227	.317
75	-.009	.003	.021	.053	.105	.172	.254	.350
90								
105	.014	.002	-.017	-.038	-.062	-.077	-.094	-.101
120	.010	.001	-.019	-.048	-.071	-.054	-.021	.018
135	.010	.004	-.015	-.051	-.102	-.110	-.100	-.078
BODY 150	.000	.000	-.019	-.055	-.065	-.045	-.119	-.123
165	-.007	-.002	-.017	-.043	-.060	-.079	-.101	-.118
180	-.008	.000	-.012	-.034	-.069	-.083	-.105	-.112
195	-.003	.002	-.008	-.030	-.094	-.093	-.110	-.114
210	.005	.003	-.006	-.033	-.134	-.116	-.120	-.138
225	.015	.006	-.004	-.024	-.042	-.103	-.111	-.130
240	.020	.005	-.006	-.013	-.026	-.061	-.082	-.095
255	.029	.009	-.004	-.018	-.021	-.042	-.074	-.085
270								
285	-.026	-.005	.009	-.002	-.064	-.087	-.115	-.129
300	-.028	-.005	.006	.002	-.048	-.105	-.129	-.145
315	-.027	-.003	.004	.000	-.042	-.130	-.148	-.155
330	-.025	-.004	-.002	-.018	-.064	-.150	-.164	-.177
345	-.020	-.003	-.004	-.039	-.117	-.134	-.123	-.110
Y/S								
	-3.96	.05	3.97	7.97	12.02	16.02	20.06	24.01
.050								
.100								
.150								
.200								
WINDWARD WING .250								
.300	-.025	-.006	.012	.021	-.011	-.086	-.115	-.129
.350	-.020	-.006	.014	.036	-.002	-.109	-.125	-.131
.400	-.105	-.008	.015	.040	.066	-.056	-.106	-.120
.425								
.450	-.103	-.020	.020	.044	.069	.067	-.012	-.063
.450	.026	-.001	-.090	-.139	-.160	-.166	-.160	-.151
.425	.028	.003	-.085	-.139	-.157	-.163	-.157	-.148
.400	.024	.000	-.064	-.150	-.173	-.179	-.176	-.170
.350	.022	.000	-.019	-.116	-.188	-.189	-.185	-.180
LEEWARD WING .300	.016	.000	-.020	-.041	-.087	-.109	-.104	-.089
.250								
.200								
.150								
.100								
.050								

Table 3. Continued
(v) Continued; station 2

THETA, DEG	CP FOR ALPHA, DEG =							
	-3.96	.05	3.97	7.97	12.02	16.02	20.06	24.01
0	-.026	-.007	-.002	-.014	-.067	-.094	-.079	-.059
15	-.024	-.006	.001	-.010	-.050	-.027	.002	.038
30	-.024	-.008	.003	.001	-.005	.034	.080	.134
45	-.022	-.007	.006	.014	.034	.088	.149	.216
60	-.023	-.010	.006	.025	.061	.125	.197	.275
75	-.022	-.009	.011	.036	.081	.150	.228	.313
90								
105	.006	-.005	-.023	-.025	-.051	-.108	-.129	-.145
120	.008	-.003	-.022	-.031	-.034	-.038	-.025	-.003
135	.006	-.004	-.022	-.042	-.050	-.057	-.056	-.045
150	.002	-.005	-.019	-.046	-.069	-.071	-.076	-.084
165	.000	-.004	-.020	-.044	-.071	-.062	-.071	-.077
180	-.001	-.005	-.022	-.042	-.076	-.064	-.075	-.076
195	.004	-.003	-.021	-.041	-.065	-.067	-.087	-.093
210	.006	-.004	-.021	-.049	-.078	-.067	-.089	-.098
225	.006	-.007	-.022	-.050	-.075	-.083	-.102	-.112
240	.009	-.007	-.019	-.031	-.048	-.083	-.095	-.106
255	.012	-.006	-.019	-.031	-.042	-.079	-.092	-.107
270								
285	-.020	-.006	.007	.001	-.017	-.063	-.100	-.109
300	-.023	-.007	.006	.009	-.003	-.074	-.098	-.108
315	-.026	-.006	.006	.012	.000	-.044	-.085	-.101
330	-.029	-.007	.002	.006	-.001	-.044	-.095	-.111
345	-.029	-.007	-.001	-.008	-.015	-.086	-.139	-.144
Y/S	CP FOR ALPHA, DEG =							
	-3.96	.05	3.97	7.97	12.02	16.02	20.06	24.01
.075								
.150								
.225								
.300	-.020	-.007	.008	.016	.012	-.044	-.101	-.114
.375	-.016	-.006	.011	.030	.001	-.096	-.137	-.144
.450								
.524	-.072	-.008	.011	.040	.077	.106	.091	.027
.599								
.637								
.674	-.101	-.018	.015	.038	.059	.078	.080	.101
.674	.014	-.012	-.089	-.133	-.165	-.175	-.175	-.175
.637	.013	-.010	-.084	-.133	-.166	-.176	-.175	-.175
.599	.013	-.007	-.074	-.134	-.164	-.176	-.175	-.176
.524	.015	-.004	-.047	-.154	-.152	-.166	-.170	-.174
.450	.013	-.006	-.023	-.133	-.182	-.185	-.189	-.190
.375	.014	-.004	-.022	-.018	-.169	-.211	-.215	-.217
.300	.012	-.003	-.021	-.021	-.045	-.091	-.108	-.125
.225								
.150								
.075								

Table 3. Continued

(v) Concluded; station 3

THETA, DEG	CP FOR ALPHA, DEG =							
	-3.96	.05	3.97	7.97	12.02	16.02	20.06	24.01
0	-.023	-.002	.005	-.001	-.013	-.099	-.094	-.072
15	-.021	-.001	.006	.003	-.011	-.042	-.015	.025
30	-.023	-.005	.006	.011	-.004	.021	.061	.117
45	-.020	-.004	.010	.026	.028	.076	.133	.204
60	-.019	-.007	.011	.034	.057	.114	.186	.267
75	-.021	-.007	.012	.038	.075	.137	.213	.299
90								
105	.015	.002	-.012	-.016	-.029	-.088	-.127	-.147
120	.013	.001	-.014	-.024	-.032	-.043	-.034	-.075
135	.012	.001	-.017	-.036	-.050	-.043	-.030	-.006
BODY 150	.010	.000	-.018	-.044	-.071	-.071	-.075	-.088
165	.006	-.001	-.019	-.043	-.066	-.075	-.076	-.101
180	.003	-.002	-.019	-.039	-.053	-.067	-.069	-.085
195	.006	.000	-.017	-.036	-.048	-.064	-.069	-.081
210	.013	.001	-.016	-.036	-.047	-.057	-.067	-.073
225	.016	.000	-.016	-.044	-.060	-.059	-.072	-.073
240	.015	-.002	-.017	-.028	-.054	-.064	-.078	-.077
255	.017	-.002	-.020	-.024	-.047	-.059	-.072	-.069
270								
285	-.009	.003	.016	.020	.013	-.010	-.051	-.065
300	-.015	.000	.013	.023	.021	-.016	-.074	-.080
315	-.019	.000	.013	.024	.027	-.005	-.051	-.058
330	-.023	-.001	.011	.022	.027	-.006	-.051	-.058
345	-.022	-.001	.008	.011	.016	-.025	-.079	-.089
Y/S	CP FOR ALPHA, DEG =							
	-3.96	.05	3.97	7.97	12.02	16.02	20.06	24.01
.190								
.274	-.009	.004	.017	.027	.015	-.018	-.047	-.061
.379	-.012	.001	.017	.025	-.021	-.080	-.100	-.103
.473	-.007	.002	.021	.046	.053	-.009	-.072	-.080
WINDWARD .569								
WING .664	-.077	.001	.023	.046	.073	.109	.152	.142
.759	-.089	-.001	.023	.045	.062	.090	.119	.160
.806	-.084	-.001	.025	.046	.058	.081	.102	.131
.854	-.083	-.004	.027	.045	.054	.070	.083	.105
.854	.029	.002	-.074	-.116	-.141	-.166	-.170	-.173
.806	.022	.000	-.075	-.119	-.145	-.173	-.175	-.178
.759	.022	.002	-.070	-.121	-.146	-.168	-.171	-.172
LEEWARD .664	.020	.001	-.037	-.142	-.152	-.164	-.168	-.170
WING .569	.019	.000	-.015	-.142	-.173	-.167	-.172	-.174
.473	.021	.002	-.010	-.017	-.179	-.191	-.193	-.196
.379	.017	-.001	-.013	-.014	-.097	-.186	-.198	-.198
.274	.016	.002	-.012	-.015	-.026	-.086	-.128	-.140
.190								

Table 3. Continued

(w) $M_\infty = 2.40$; $\phi = -60^\circ$; station 1

THETA, DEG	CP FOR ALPHA, DEG =							
	-4.00	.03	4.02	7.98	11.98	15.99	19.97	23.98
0								
15	-.005	.007	.003	-.009	.000	.025	.067	.113
30	-.005	.005	.007	.015	.040	.081	.141	.206
45	-.002	.007	.016	.038	.075	.130	.204	.285
60	-.003	.006	.021	.052	.097	.162	.244	.335
75	-.002	.010	.029	.065	.115	.186	.272	.370
90								
105	.016	.007	-.013	-.033	-.036	-.035	-.046	-.051
120	.010	.002	-.019	-.049	-.053	-.034	-.002	.040
135	.010	.006	-.016	-.058	-.086	-.086	-.076	-.053
BODY 150	.002	.004	-.019	-.053	-.068	-.095	-.110	-.121
165	-.006	.001	-.018	-.041	-.056	-.082	-.100	-.114
180	-.008	.000	-.014	-.033	-.063	-.084	-.103	-.111
195	-.001	.003	-.008	-.031	-.093	-.094	-.108	-.118
210	.010	.007	-.002	-.032	-.114	-.106	-.109	-.127
225	.019	.009	.001	-.022	-.042	-.098	-.100	-.122
240	.025	.009	.001	-.011	-.023	-.059	-.080	-.097
255	.036	.015	.004	-.013	-.019	-.041	-.074	-.089
270								
285	-.020	.000	.015	-.002	-.059	-.086	-.106	-.117
300	-.022	.000	.012	.003	-.051	-.109	-.116	-.130
315	-.023	.000	.007	-.002	-.047	-.108	-.123	-.133
330	-.019	.003	.003	-.019	-.070	-.119	-.138	-.142
345	-.015	.003	-.001	-.049	-.092	-.098	-.086	-.073
Y/S	CP FOR ALPHA, DEG =							
	-4.00	.03	4.02	7.98	11.98	15.99	19.97	23.98
.050								
.100								
.150								
.200								
WINDWARD .250								
WING .300	-.020	-.001	.018	.024	-.017	-.083	-.106	-.114
.350	-.017	-.001	.022	.041	-.015	-.099	-.110	-.117
.400	-.087	-.001	.023	.047	.061	-.043	-.093	-.097
.425								
.450	-.088	-.018	.026	.047	.071	.058	-.021	-.033
.450	.029	.006	-.077	-.115	-.126	-.121	-.117	-.107
.425	.030	.009	-.077	-.112	-.121	-.118	-.113	-.104
.400	.030	.010	-.056	-.117	-.129	-.125	-.124	-.118
.350	.027	.007	-.011	-.106	-.142	-.139	-.137	-.131
LEEWARD .300	.020	.004	-.016	-.036	-.058	-.069	-.067	-.056
WING .250								
.200								
.150								
.100								
.050								

Table 3. Continued

(w) Continued; station 2

	THETA, DEG	CP FOR ALPHA, DEG =							
		-4.00	.03	4.02	7.98	11.98	15.99	19.97	23.98
BODY	0	-.008	.010	.015	.000	-.057	-.055	-.033	-.006
	15	-.006	.011	.016	.002	-.014	.006	.041	.087
	30	-.002	.012	.020	.015	.029	.066	.116	.181
	45	-.002	.011	.023	.033	.063	.114	.179	.261
	60	-.001	.010	.025	.048	.090	.151	.228	.320
	75	-.003	.009	.028	.058	.105	.171	.254	.352
	90								
	105	.027	.017	.002	-.007	-.032	-.062	-.076	-.076
	120	.021	.011	-.006	-.019	-.023	-.014	.010	.049
	135	.023	.015	-.003	-.025	-.037	-.044	-.031	-.001
	150	.022	.016	-.002	-.029	-.050	-.057	-.069	-.076
	165	.018	.016	-.002	-.026	-.051	-.049	-.065	-.071
	180	.018	.016	.000	-.024	-.052	-.046	-.065	-.071
	195	.016	.013	-.003	-.028	-.052	-.059	-.075	-.082
	210	.022	.017	.001	-.031	-.051	-.054	-.074	-.085
	225	.025	.016	.003	-.027	-.054	-.066	-.079	-.093
	240	.028	.016	.004	-.009	-.031	-.064	-.082	-.086
	255	.030	.015	.003	-.006	-.024	-.058	-.082	-.087
	270								
	285	-.007	.009	.022	.015	-.008	-.054	-.075	-.078
300	-.006	.012	.024	.025	.003	-.052	-.071	-.075	
315	-.009	.011	.023	.028	.003	-.038	-.065	-.074	
330	-.011	.010	.020	.022	.001	-.048	-.074	-.078	
345	-.006	.014	.020	.013	-.018	-.079	-.095	-.083	
	Y/S	CP FOR ALPHA, DEG =							
		-4.00	.03	4.02	7.98	11.98	15.99	19.97	23.98
WINDWARD WING	.075								
	.150								
	.225								
	.300	-.002	.015	.030	.038	.019	-.041	-.069	-.072
	.375	.003	.016	.034	.051	.002	-.081	-.095	-.092
	.450								
	.524	-.048	.013	.032	.056	.085	.115	.083	.043
	.599								
	.637								
	.674	-.075	.001	.037	.055	.070	.090	.098	.130
LEEWARD WING	.674	.041	.019	-.065	-.102	-.116	-.115	-.114	-.106
	.637	.039	.019	-.061	-.104	-.118	-.116	-.116	-.107
	.599	.039	.019	-.047	-.100	-.116	-.114	-.113	-.105
	.524	.032	.013	-.027	-.105	-.111	-.109	-.111	-.106
	.450	.036	.018	.001	-.105	-.126	-.118	-.121	-.116
	.375	.035	.018	.004	-.020	-.123	-.140	-.145	-.141
	.300	.027	.012	-.004	-.011	-.040	-.057	-.065	-.062
	.225								
	.150								
	.075								

Table 3. Continued

(w) Concluded; station 3

THETA, DEG	CP FOR ALPHA, DEG =							
	-4.00	.03	4.02	7.98	11.98	15.99	19.97	23.98
0	-.016	.002	.007	.000	-.034	-.075	-.057	-.033
15	-.013	.005	.010	.005	-.035	-.019	.018	.059
30	-.014	.002	.010	.013	.003	.036	.089	.148
45	-.014	.001	.013	.024	.038	.084	.153	.231
60	-.013	.000	.015	.034	.066	.122	.202	.294
75	-.012	.003	.021	.044	.085	.150	.235	.333
90								
105	.022	.010	-.004	-.012	-.026	-.073	-.094	-.098
120	.017	.005	-.012	-.022	-.023	-.019	-.016	-.032
135	.017	.005	-.015	-.031	-.042	-.035	-.021	.013
BODY 150	.016	.006	-.016	-.038	-.064	-.071	-.080	-.076
165	.011	.004	-.017	-.040	-.063	-.075	-.086	-.114
180	.010	.006	-.013	-.034	-.048	-.064	-.080	-.100
195	.012	.006	-.011	-.032	-.045	-.061	-.075	-.092
210	.014	.005	-.012	-.036	-.047	-.058	-.079	-.092
225	.017	.005	-.011	-.043	-.056	-.058	-.079	-.092
240	.022	.006	-.007	-.026	-.051	-.058	-.081	-.087
255	.022	.005	-.011	-.023	-.047	-.055	-.077	-.078
270								
285	-.007	.004	.017	.016	.009	-.018	-.047	-.054
300	-.013	.001	.012	.017	.008	-.038	-.062	-.063
315	-.008	.010	.020	.028	.024	-.012	-.039	-.041
330	-.016	.003	.013	.019	.017	-.016	-.047	-.050
345	-.018	.000	.008	.007	.002	-.034	-.073	-.076
Y/S	CP FOR ALPHA, DEG =							
	-4.00	.03	4.02	7.98	11.98	15.99	19.97	23.98
.190								
.274	-.010	.003	.017	.021	.007	-.027	-.045	-.053
.379	-.006	.006	.023	.024	-.022	-.070	-.080	-.084
.473	-.006	.003	.021	.042	.045	-.027	-.062	-.063
WINDWARD .569								
WING .664	-.061	.003	.022	.041	.074	.107	.143	.138
.759	-.075	.003	.023	.043	.067	.091	.114	.159
.806	-.079	.001	.023	.044	.062	.080	.094	.136
.854	-.080	-.003	.024	.044	.056	.068	.074	.108
.854	.024	.005	-.076	-.106	-.123	-.131	-.132	-.128
.806	.029	.010	-.061	-.103	-.121	-.128	-.129	-.123
.759	.025	.006	-.055	-.103	-.121	-.128	-.128	-.124
LEEWARD .664	.028	.008	-.032	-.101	-.112	-.121	-.123	-.118
WING .569	.027	.008	-.014	-.106	-.116	-.114	-.119	-.116
.473	.022	.003	-.010	-.077	-.136	-.138	-.143	-.142
.379	.022	.004	-.009	-.011	-.105	-.148	-.152	-.147
.274	.019	.006	-.009	-.015	-.027	-.072	-.098	-.096
.190								

Table 3. Continued

(x) $M_\infty = 2.86; \phi = -60^\circ$; station 1

THETA, DEG	CP FOR ALPHA, DEG =							
	-4.04	.04	4.04	8.01	12.04	15.97	20.00	24.00
0								
15	-.002	.007	.003	-.001	.015	.041	.078	.125
30	.005	.012	.016	.026	.057	.096	.149	.214
45	.007	.012	.022	.045	.087	.137	.204	.285
60	.005	.011	.026	.056	.107	.165	.241	.332
75	.004	.012	.032	.066	.121	.183	.265	.362
90								
105	.021	.012	-.004	-.011	-.005	.005	.012	.013
120	.019	.012	-.007	-.024	-.022	-.005	.024	.061
135	.019	.016	-.003	-.037	-.049	-.046	-.034	-.016
BODY 150	.005	.008	-.012	-.053	-.062	-.075	-.083	-.086
165	-.005	.005	-.011	-.036	-.052	-.071	-.078	-.087
180	-.002	.007	-.005	-.024	-.051	-.069	-.077	-.085
195	.007	.010	.000	-.019	-.067	-.073	-.080	-.088
210	.015	.009	.001	-.022	-.073	-.079	-.086	-.094
225	.025	.011	.004	-.017	-.036	-.074	-.080	-.090
240	.030	.010	.001	-.009	-.021	-.051	-.067	-.075
255	.038	.012	.002	-.012	-.017	-.039	-.063	-.075
270								
285	-.015	.002	.013	-.004	-.052	-.074	-.080	-.082
300	-.019	.001	.010	-.005	-.054	-.082	-.089	-.090
315	-.014	.007	.011	-.004	-.046	-.075	-.083	-.085
330	-.015	.005	.001	-.025	-.063	-.090	-.095	-.089
345	-.009	.006	-.002	-.043	-.059	-.058	-.047	-.032
Y/S	CP FOR ALPHA, DEG =							
	-4.04	.04	4.04	8.01	12.04	15.97	20.00	24.00
.050								
.100								
.150								
.200								
WINDWARD .250								
WING .300	-.012	.004	.018	.019	-.026	-.068	-.075	-.076
.350	-.023	.003	.020	.033	-.027	-.075	-.081	-.081
.400	-.068	-.002	.020	.038	.044	-.039	-.063	-.053
.425								
.450	-.061	-.008	.027	.045	.066	.042	.008	.025
.450	.039	.007	-.051	-.074	-.079	-.075	-.067	-.059
.425	.036	.010	-.049	-.069	-.075	-.071	-.063	-.054
.400	.029	.004	-.053	-.078	-.082	-.079	-.073	-.068
.350	.026	.007	-.007	-.075	-.092	-.088	-.084	-.078
LEEWARD .300	.024	.009	-.007	-.013	-.022	-.028	-.024	-.014
WING .250								
.200								
.150								
.100								
.050								

Table 3. Continued

(x) Continued; station 2

THETA, DEG	CP FOR ALPHA, DEG =							
	-4.04	.04	4.04	8.01	12.04	15.97	20.00	24.00
0	.001	.012	.013	-.016	-.033	-.022	-.002	.025
15	.003	.013	.015	-.006	.006	.030	.064	.107
30	.002	.011	.015	.013	.040	.076	.126	.186
45	.004	.013	.020	.033	.073	.121	.185	.259
60	.001	.009	.021	.046	.095	.150	.226	.311
75	.003	.014	.028	.059	.112	.174	.257	.346
90								
105	.023	.008	-.005	-.015	-.016	-.029	-.037	-.038
120	.028	.015	.000	-.015	-.009	.013	.041	.073
135	.027	.014	-.004	-.026	-.039	-.029	-.007	.017
BODY 150	.022	.013	-.006	-.030	-.052	-.060	-.064	-.053
165	.020	.015	-.003	-.023	-.039	-.047	-.056	-.066
180	.014	.012	-.005	-.026	-.044	-.047	-.063	-.071
195	.017	.014	-.001	-.023	-.042	-.052	-.063	-.072
210	.018	.012	-.002	-.030	-.045	-.056	-.068	-.081
225	.016	.006	-.006	-.034	-.055	-.072	-.077	-.089
240	.023	.008	-.002	-.012	-.037	-.064	-.075	-.080
255	.026	.008	-.003	-.009	-.032	-.057	-.074	-.085
270								
285	-.002	.011	.022	.012	-.010	-.045	-.052	-.048
300	-.006	.009	.018	.010	-.011	-.048	-.056	-.051
315	-.004	.012	.020	.019	-.009	-.040	-.052	-.047
330	-.004	.010	.016	.014	-.016	-.047	-.056	-.052
345	-.002	.011	.013	.000	-.043	-.067	-.060	-.045
Y/S	CP FOR ALPHA, DEG =							
	-4.04	.04	4.04	8.01	12.04	15.97	20.00	24.00
.075								
.150								
.225								
WINDWARD .300	-.005	.009	.021	.026	-.007	-.044	-.054	-.049
.375	-.001	.010	.025	.037	-.026	-.064	-.067	-.062
WING .450								
.524	-.047	.010	.026	.046	.076	.090	.058	.061
.599								
.637								
.674	-.063	-.015	.029	.043	.059	.068	.079	.114
.674	.037	.004	-.053	-.075	-.079	-.077	-.073	-.066
.637	.037	.015	-.052	-.074	-.079	-.076	-.071	-.064
.599	.036	.016	-.052	-.074	-.078	-.076	-.071	-.064
.524	.037	.018	-.022	-.065	-.066	-.063	-.057	-.053
LEEWARD .450	.032	.012	-.007	-.069	-.078	-.072	-.069	-.066
.375	.032	.012	-.001	-.028	-.085	-.090	-.090	-.088
.300	.032	.015	.000	-.009	-.016	-.022	-.019	-.017
.225								
.150								
.075								

Table 3. Continued

(x) Concluded; station 3

THETA, DEG	CP FOR ALPHA, DEG =							
	-4.04	.04	4.04	8.01	12.04	15.97	20.00	24.00
BODY								
0	-.002	.017	.018	.005	-.037	-.033	-.014	.014
15	-.001	.019	.022	.005	-.002	.020	.053	.095
30	-.005	.014	.022	.011	.032	.067	.114	.173
45	.000	.018	.031	.035	.069	.116	.178	.252
60	.000	.017	.035	.051	.093	.150	.224	.310
75	-.001	.017	.038	.062	.109	.173	.254	.346
90								
105	.031	.019	.006	-.001	-.018	-.035	-.040	-.039
120	.027	.018	.002	-.008	-.006	.012	.028	.031
135	.027	.016	-.002	-.020	-.028	-.016	.008	.040
150	.026	.015	-.006	-.029	-.053	-.058	-.053	-.036
165	.024	.015	-.005	-.027	-.048	-.059	-.070	-.091
180	.020	.013	-.005	-.023	-.040	-.055	-.068	-.088
195	.020	.013	-.002	-.021	-.035	-.049	-.063	-.083
210	.025	.016	.002	-.020	-.034	-.045	-.063	-.080
225	.025	.013	.000	-.030	-.040	-.047	-.064	-.080
240	.025	.010	-.002	-.014	-.038	-.050	-.065	-.080
255	.029	.014	.001	-.007	-.031	-.043	-.059	-.071
270								
285	.007	.017	.027	.023	.008	-.018	-.028	-.022
300	.001	.013	.025	.024	.002	-.025	-.035	-.027
315	.000	.015	.025	.028	.011	-.018	-.029	-.020
330	-.001	.016	.024	.026	.012	-.021	-.027	-.021
345	.003	.019	.022	.020	.002	-.031	-.041	-.038
Y/S								
	-4.04	.04	4.04	8.01	12.04	15.97	20.00	24.00
WINDWARD WING								
.190								
.274	.006	.018	.031	.034	.009	-.022	-.030	-.026
.379	.001	.010	.026	.027	-.028	-.057	-.058	-.054
.473	.004	.017	.033	.052	.043	-.022	-.030	-.024
.569								
.664	-.043	.015	.033	.050	.077	.105	.126	.149
.759	-.061	.013	.031	.047	.067	.085	.109	.143
.806	-.058	.013	.033	.047	.063	.078	.094	.128
.854	-.058	-.006	.035	.048	.060	.069	.079	.109
LEEWARD WING								
.854	.042	.012	-.050	-.071	-.074	-.072	-.070	-.065
.806	.036	.016	-.057	-.077	-.080	-.078	-.077	-.072
.759	.039	.020	-.043	-.072	-.075	-.072	-.071	-.066
.664	.036	.017	-.017	-.061	-.070	-.070	-.067	-.062
.569	.034	.016	-.008	-.055	-.060	-.060	-.058	-.056
.473	.038	.021	.005	-.052	-.069	-.065	-.063	-.064
.379	.034	.018	.005	-.007	-.076	-.086	-.084	-.081
.274	.036	.023	.011	.003	-.012	-.030	-.037	-.034
.190								

Table 3. Continued

(y) $M_\infty = 1.70; \phi = -90^\circ$; station 1

THETA, DEG	CP FOR ALPHA, DEG =							
	-4.04	.02	4.03	8.01	11.99	16.03	19.97	23.99
0								
15	.000	.005	-.006	-.045	-.098	-.099	-.237	-.236
30	.003	.006	-.006	-.038	-.085	-.144	-.138	-.119
45	.007	.008	-.003	-.019	-.053	-.060	-.030	.008
60	.008	.006	.000	-.001	-.015	.013	.060	.120
75	.013	.009	.009	.016	.021	.068	.129	.205
90								
105	.009	.002	.003	.007	.020	.059	.124	.199
120	.004	-.001	-.003	-.007	-.015	.009	.058	.119
135	.005	.005	-.002	-.020	-.047	-.057	-.028	.016
BODY 150	.001	.002	-.009	-.044	-.088	-.149	-.149	-.129
165	-.005	.001	-.011	-.049	-.098	-.080	-.218	-.235
180	-.013	.001	-.008	-.039	-.066	-.052	-.118	-.160
195	-.014	.003	-.001	-.019	-.032	-.061	-.103	-.146
210	-.009	.006	.006	-.008	-.025	-.064	-.090	-.146
225	-.002	.007	.008	-.007	-.036	-.061	-.096	-.139
240	.003	.006	.007	-.016	-.087	-.142	-.106	-.143
255	.011	.008	.010	.000	-.029	-.066	-.133	-.149
270								
285	.000	.000	.005	-.001	-.026	-.062	-.118	-.140
300	-.003	-.001	.003	-.015	-.085	-.162	-.097	-.138
315	-.006	.000	.000	-.012	-.046	-.091	-.104	-.150
330	-.008	.002	-.001	-.013	-.034	-.085	-.118	-.167
345	-.009	.003	-.004	-.024	-.040	-.065	-.129	-.178
Y/S	CP FOR ALPHA, DEG =							
	-4.04	.02	4.03	8.01	11.99	16.03	19.97	23.99
.050								
.100								
.150								
.200								
WINDWARD .250								
WING .300	-.003	-.002	.005	.007	-.010	-.043	-.142	-.171
.350	-.004	-.003	.005	.011	-.006	-.039	-.154	-.275
.400	-.007	-.006	.003	.011	.004	-.020	-.193	-.259
.425								
.450	-.004	-.002	.008	.017	.016	.006	-.171	-.249
.450	.011	.002	.001	-.003	.006	.036	.083	.141
.425	.012	.004	.001	.000	.008	.045	.100	.161
.400	.013	.004	.002	.003	.013	.054	.111	.179
.350	.014	.003	.002	.004	.016	.055	.113	.186
LEEWARD .300	.011	.001	-.001	.004	.018	.059	.119	.193
WING .250								
.200								
.150								
.100								
.050								

Table 3. Continued

(y) Continued; station 2

	THETA, DEG	CP FOR ALPHA, DEG =							
		-4.04	.02	4.03	8.01	11.99	16.03	19.97	23.99
BODY	0	-.015	-.002	-.010	-.036	-.072	-.096	-.106	-.146
	15	-.012	-.002	-.011	-.041	-.089	-.171	-.201	-.228
	30	-.009	-.002	-.009	-.032	-.074	-.115	-.158	-.136
	45	-.007	-.002	-.007	-.020	-.038	-.040	-.047	-.007
	60	-.008	-.004	-.004	-.002	.004	.026	.058	.112
	75	-.006	-.004	.000	.012	.035	.071	.128	.192
	90								
	105	-.001	.001	.006	.018	.044	.068	.107	.178
	120	-.008	-.004	-.003	.000	.012	.031	.053	.120
	135	-.007	-.002	-.003	-.011	-.022	-.032	-.046	.000
	150	-.009	.000	-.003	-.021	-.055	-.094	-.155	-.128
	165	-.014	-.001	-.006	-.031	-.078	-.128	-.160	-.199
	180	-.016	-.001	-.006	-.025	-.065	-.087	-.079	-.105
	195	-.017	-.002	-.007	-.017	-.038	-.055	-.066	-.100
	210	-.012	.000	-.004	-.011	-.030	-.048	-.066	-.098
	225	-.006	.001	-.001	-.009	-.026	-.042	-.085	-.102
	240	-.005	.000	-.002	-.023	-.032	-.048	-.090	-.103
	255	-.003	-.002	-.001	-.012	-.038	-.063	-.101	-.125
	270								
	285	.000	-.004	-.004	-.017	-.046	-.071	-.136	-.229
	300	-.003	-.002	-.003	-.026	-.042	-.054	-.111	-.166
	315	-.006	-.001	-.004	-.014	-.034	-.045	-.119	-.156
	330	-.010	-.002	-.005	-.015	-.035	-.054	-.122	-.146
	345	-.012	.000	-.005	-.018	-.037	-.056	-.101	-.136
	Y/S	CP FOR ALPHA, DEG =							
		-4.04	.02	4.03	8.01	11.99	16.03	19.97	23.99
WINDWARD WING	.075								
	.150								
	.225								
	.300	.001	-.001	.000	-.007	-.038	-.077	-.143	-.211
	.375	.002	.001	.003	.002	-.040	-.080	-.140	-.222
	.450								
	.524	-.002	.000	.003	.009	.011	-.050	-.198	-.202
	.599								
	.637								
	.674	-.005	-.007	.001	.010	.017	.028	-.056	-.264
LEEWARD WING	.674	-.003	-.005	-.006	-.011	-.001	.007	.054	.102
	.637	.000	-.001	.000	.000	.013	.015	.061	.118
	.599	.000	-.001	.000	.002	.013	.017	.067	.130
	.524	.000	-.002	.000	.005	.018	.022	.073	.139
	.450	.002	.000	.003	.012	.031	.047	.090	.158
	.375	.002	.000	.003	.013	.037	.059	.097	.164
	.300	-.003	-.002	.000	.010	.035	.058	.097	.163
	.225								
	.150								
	.075								

Table 3. Continued

(y) Concluded; station 3

THETA, DEG	CP FOR ALPHA, DEG =							
	-4.04	.02	4.03	8.01	11.99	16.03	19.97	23.99
0	-.009	.003	-.005	-.026	-.050	-.072	-.081	-.128
15	-.005	.005	-.004	-.028	-.062	-.117	-.158	-.208
30	-.005	.003	-.005	-.024	-.048	-.098	-.147	-.131
45	-.005	.002	-.002	-.011	-.021	-.044	-.041	.001
60	-.006	.001	.000	.005	.014	.025	.055	.122
75	-.004	-.001	.000	.012	.033	.060	.099	.172
90								
105	.007	.012	.016	.020	.038	.061	.101	.160
120	.000	.006	.008	.008	.017	.039	.075	.127
135	.000	.006	.004	-.006	-.017	-.019	-.007	.013
BODY 150	-.002	.005	.001	-.022	-.047	-.085	-.108	-.126
165	-.007	.005	-.003	-.032	-.065	-.124	-.172	-.186
180	-.009	.006	.000	-.026	-.050	-.079	-.083	-.092
195	-.008	.008	.004	-.012	-.025	-.041	-.055	-.085
210	-.003	.007	.003	-.010	-.022	-.038	-.054	-.089
225	.004	.007	.004	-.007	-.018	-.033	-.053	-.089
240	.008	.008	.003	-.013	-.018	-.034	-.059	-.092
255	.002	.006	-.001	-.013	-.025	-.040	-.065	-.098
270								
285	.009	.010	.005	-.008	-.017	-.047	-.133	-.168
300	.006	.006	.001	-.016	-.025	-.048	-.097	-.166
315	.007	.009	.006	-.004	-.017	-.042	-.074	-.124
330	-.004	.005	.001	-.009	-.021	-.041	-.071	-.124
345	-.009	.003	-.003	-.013	-.025	-.043	-.068	-.121
Y/S	CP FOR ALPHA, DEG =							
	-4.04	.02	4.03	8.01	11.99	16.03	19.97	23.99
.190								
.274	.007	.010	.005	-.005	-.020	-.050	-.125	-.157
.379	.007	.009	.007	.000	-.037	-.056	-.129	-.163
.473	.006	.007	.006	.011	-.024	-.100	-.134	-.173
WINDWARD .569								
WING .664	.005	.005	.010	.013	.024	-.022	-.154	-.260
.759	.003	.005	.009	.014	.023	.018	-.048	-.205
.806	.002	.005	.008	.015	.021	.025	-.006	-.157
.854	.000	.004	.008	.015	.019	.029	.026	-.108
.854	.005	.009	.009	.002	.011	.016	.046	.088
.806	.008	.013	.016	.011	.022	.032	.048	.097
.759	.007	.011	.015	.010	.021	.031	.051	.104
LEEWARD .664	.010	.012	.016	.013	.024	.038	.058	.115
WING .569	.009	.008	.015	.013	.025	.043	.067	.129
.473	.008	.005	.011	.012	.027	.046	.078	.140
.379	.010	.008	.011	.013	.029	.052	.089	.149
.274	.005	.011	.012	.015	.032	.054	.094	.153
.190								

Table 3. Continued

(z) $M_\infty = 2.16; \phi = -90^\circ$; station 1

THETA, DEG	CP FOR ALPHA, DEG =							
	-3.97	-.01	4.05	8.04	12.02	15.98	20.06	24.05
0								
15	-.010	-.001	-.012	-.055	-.121	-.137	-.130	-.117
30	-.004	.001	-.010	-.046	-.077	-.076	-.051	-.025
45	.000	.003	-.006	-.027	-.030	-.013	.030	.075
60	.000	.002	-.003	-.007	.009	.044	.103	.165
75	.004	.004	.002	.012	.042	.089	.161	.233
90								
105	.001	.001	-.001	.007	.038	.083	.151	.225
120	-.003	-.002	-.007	-.008	.010	.043	.098	.160
135	-.002	.001	-.006	-.024	-.027	-.005	.032	.078
BODY 150	-.007	-.001	-.013	-.049	-.083	-.080	-.063	-.037
165	-.013	-.002	-.014	-.056	-.116	-.134	-.134	-.122
180	-.019	-.002	-.012	-.044	-.057	-.086	-.107	-.119
195	-.018	-.001	-.005	-.024	-.044	-.075	-.093	-.108
210	-.014	.001	.001	-.015	-.051	-.072	-.098	-.107
225	-.009	.004	.004	-.012	-.076	-.087	-.102	-.109
240	-.003	.003	.002	-.022	-.124	-.099	-.114	-.121
255	.006	.007	.007	-.002	-.024	-.099	-.117	-.126
270								
285	-.008	-.005	-.001	-.010	-.024	-.091	-.115	-.125
300	-.012	-.005	-.003	-.026	-.126	-.087	-.107	-.125
315	-.015	-.003	-.004	-.019	-.081	-.081	-.110	-.124
330	-.019	-.004	-.007	-.021	-.051	-.090	-.118	-.124
345	-.020	-.003	-.010	-.031	-.050	-.092	-.119	-.128
Y/S	CP FOR ALPHA, DEG =							
	-3.97	-.01	4.05	8.04	12.02	15.98	20.06	24.05
.050								
.100								
.150								
.200								
WINDWARD .250								
WING .300	-.008	-.006	-.001	.000	-.008	-.081	-.165	-.148
.350	-.008	-.006	-.001	.003	-.007	-.088	-.169	-.197
.400	-.008	-.008	-.003	.003	.001	-.079	-.173	-.193
.425								
.450	-.038	-.019	.000	.007	.010	-.045	-.184	-.187
.450	.002	-.002	-.011	-.026	-.018	.008	.062	.129
.425	.004	.002	.000	.002	.025	.064	.131	.199
.400	.002	-.001	-.004	.003	.035	.074	.138	.209
.350	.003	.000	-.003	.005	.038	.080	.145	.216
LEEWARD .300	.001	-.002	-.005	.005	.038	.082	.149	.221
WING .250								
.200								
.150								
.100								
.050								

Table 3. Continued

(z) Continued; station 2

	THETA, DEG	CP FOR ALPHA, DEG =							
		-3.97	-.01	4.05	8.04	12.02	15.98	20.06	24.05
BODY	0	-.014	-.002	-.011	-.035	-.052	-.074	-.110	-.126
	15	-.010	-.001	-.011	-.042	-.068	-.125	-.142	-.129
	30	-.009	-.002	-.011	-.037	-.083	-.086	-.069	-.040
	45	-.008	-.003	-.007	-.025	-.043	-.020	.014	.059
	60	-.009	-.005	-.005	-.009	-.002	.039	.090	.153
	75	-.004	-.003	.001	.007	.030	.084	.145	.219
	90								
	105	-.002	-.001	.002	.006	.030	.075	.134	.201
	120	-.005	.001	-.001	-.005	.005	.041	.095	.157
	135	-.006	.001	-.004	-.014	-.037	-.018	.019	.062
	150	-.008	-.001	-.008	-.024	-.045	-.083	-.063	-.039
	165	-.012	-.001	-.008	-.030	-.052	-.108	-.124	-.121
	180	-.017	-.003	-.007	-.027	-.044	-.059	-.078	-.094
	195	-.016	-.001	-.005	-.016	-.038	-.051	-.067	-.080
	210	-.012	-.002	-.006	-.016	-.040	-.053	-.064	-.078
	225	-.010	-.003	-.008	-.020	-.035	-.063	-.081	-.087
	240	-.005	-.003	-.006	-.032	-.058	-.060	-.077	-.084
	255	-.002	-.004	-.004	-.015	-.046	-.067	-.094	-.100
	270								
	285	.001	-.001	.001	-.014	-.038	-.077	-.166	-.182
300	-.003	-.001	-.002	-.031	-.049	-.073	-.107	-.123	
315	-.008	.000	-.003	-.016	-.032	-.071	-.102	-.121	
330	-.013	-.001	-.005	-.016	-.044	-.072	-.101	-.118	
345	-.015	-.001	-.008	-.019	-.042	-.070	-.099	-.117	
	Y/S	CP FOR ALPHA, DEG =							
		-3.97	-.01	4.05	8.04	12.02	15.98	20.06	24.05
WINDWARD WING	.075								
	.150								
	.225								
	.300	-.001	-.001	.002	-.008	-.031	-.086	-.148	-.171
	.375	.000	.000	.004	-.001	-.030	-.086	-.138	-.168
	.450								
	.524	-.003	.000	.005	.006	.009	-.086	-.129	-.163
	.599								
	.637								
	.674	-.023	-.005	.000	.003	.014	.014	-.099	-.185
LEEWARD WING	.674	.001	-.003	-.003	-.035	-.018	-.003	.038	.104
	.637	.001	-.001	-.003	-.003	.022	.059	.107	.145
	.599	.002	-.001	-.003	-.005	.015	.055	.107	.163
	.524	.003	.001	-.001	-.003	.017	.059	.113	.175
	.450	.002	.000	-.001	-.003	.018	.063	.120	.185
	.375	.001	.000	.002	.003	.025	.070	.128	.193
	.300	-.001	.001	.002	.006	.029	.073	.132	.197
	.225								
	.150								
	.075								

Table 3. Continued

(z) Concluded; station 3

THETA, DEG	CP FOR ALPHA, DEG =							
	-3.97	-.01	4.05	8.04	12.02	15.98	20.06	24.05
0	-.013	-.001	-.010	-.026	-.040	-.058	-.088	-.125
15	-.009	.000	-.009	-.034	-.068	-.101	-.132	-.129
30	-.009	-.003	-.011	-.033	-.060	-.094	-.073	-.040
45	-.008	-.001	-.007	-.019	-.023	-.025	.011	.063
60	-.008	-.002	-.003	-.003	.010	.036	.088	.155
75	-.003	-.001	.001	.011	.025	.072	.129	.204
90								
105	-.003	-.002	.002	.011	.032	.062	.119	.189
120	-.009	-.004	-.002	.001	.015	.034	.090	.160
135	-.008	-.004	-.006	-.012	-.018	-.024	.017	.069
BODY 150	-.009	-.003	-.009	-.026	-.057	-.091	-.067	-.035
165	-.012	-.003	-.010	-.035	-.076	-.111	-.120	-.119
180	-.016	-.004	-.011	-.030	-.052	-.063	-.073	-.074
195	-.017	-.003	-.007	-.018	-.033	-.048	-.065	-.062
210	-.013	-.002	-.004	-.015	-.027	-.043	-.059	-.063
225	-.009	-.003	-.004	-.014	-.026	-.044	-.066	-.064
240	-.003	-.004	-.005	-.023	-.032	-.048	-.070	-.061
255	.002	-.003	-.003	-.016	-.036	-.067	-.085	-.074
270								
285	.005	.001	.002	-.010	-.033	-.077	-.134	-.153
300	.001	.001	-.002	-.021	-.033	-.068	-.130	-.133
315	-.003	.002	-.002	-.010	-.025	-.061	-.092	-.120
330	-.009	.000	-.004	-.011	-.025	-.055	-.083	-.116
345	-.013	-.001	-.007	-.014	-.026	-.052	-.080	-.116
Y/S	CP FOR ALPHA, DEG =							
	-3.97	-.01	4.05	8.04	12.02	15.98	20.06	24.05
.190								
.274	.004	.001	.003	-.006	-.035	-.079	-.125	-.144
.379	.000	-.002	.004	-.007	-.048	-.088	-.122	-.147
.473	.000	-.001	.008	.008	-.036	-.132	-.137	-.151
WINDWARD WING .569								
.664	-.003	-.002	.007	.013	.015	-.031	-.156	-.181
.759	-.006	-.004	.005	.010	.016	.012	-.099	-.162
.806	-.007	-.003	.006	.011	.018	.024	-.055	-.155
.854	-.013	-.005	.005	.010	.019	.029	-.003	-.155
.854	.001	-.001	.000	-.013	-.037	-.023	.044	.082
.806	.000	.000	-.001	-.003	.006	.035	.080	.136
.759	.001	-.001	-.002	-.005	.011	.039	.077	.134
LEEWARD WING .664	.000	-.001	.000	-.001	.005	.037	.086	.144
.569	-.002	-.003	-.002	.000	.006	.040	.095	.158
.473	-.001	-.001	.001	.005	.015	.049	.107	.175
.379	-.002	-.003	-.001	.007	.023	.055	.112	.181
.274	-.004	-.002	.000	.010	.029	.059	.116	.185
.190								

Table 3. Continued

(aa) $M_\infty = 2.40$; $\phi = -90^\circ$; station 1

THETA, DEG	CP FOR ALPHA, DEG =							
	-4.00	.00	4.02	7.97	12.00	16.01	19.97	24.05
0								
15	-.005	.005	-.008	-.058	-.095	-.101	-.090	-.079
30	-.001	.004	-.008	-.046	-.057	-.045	-.021	.004
45	.004	.006	-.003	-.020	-.013	.015	.054	.099
60	.005	.005	.001	.001	.025	.066	.121	.187
75	.010	.008	.008	.022	.057	.110	.176	.258
90								
105	.007	.008	.007	.022	.055	.104	.166	.248
120	.002	.003	-.001	.004	.027	.066	.116	.183
135	.003	.007	-.001	-.014	-.005	.019	.052	.102
BODY 150	-.002	.004	-.009	-.044	-.055	-.048	-.033	-.004
165	-.009	.002	-.013	-.064	-.095	-.103	-.099	-.084
180	-.015	.001	-.013	-.049	-.063	-.090	-.101	-.115
195	-.013	.004	-.005	-.023	-.045	-.075	-.092	-.106
210	-.008	.008	.003	-.012	-.047	-.074	-.090	-.103
225	-.001	.011	.008	-.010	-.081	-.087	-.096	-.106
240	.005	.010	.009	-.021	-.106	-.093	-.106	-.120
255	.017	.016	.015	.000	-.028	-.100	-.105	-.126
270								
285	-.001	.000	.005	-.004	-.023	-.086	-.109	-.122
300	-.005	.000	.003	-.024	-.104	-.088	-.106	-.124
315	-.010	.000	.000	-.018	-.086	-.088	-.106	-.122
330	-.013	.001	-.001	-.018	-.050	-.088	-.104	-.117
345	-.014	.002	-.005	-.025	-.049	-.090	-.105	-.118
Y/S	CP FOR ALPHA, DEG =							
	-4.00	.00	4.02	7.97	12.00	16.01	19.97	24.05
.050								
.100								
.150								
.200								
WINDWARD .250								
WING .300	-.002	-.001	.005	.004	-.010	-.093	-.143	-.140
.350	-.001	-.001	.006	.008	-.008	-.100	-.157	-.156
.400	-.002	-.002	.004	.009	.000	-.105	-.156	-.163
.425								
.450	-.031	-.026	-.001	.009	.008	-.074	-.158	-.164
.450	.010	.008	-.002	.005	.028	.053	.083	.145
.425	.012	.011	.004	.013	.039	.074	.126	.213
.400	.012	.011	.007	.021	.054	.100	.155	.233
.350	.010	.008	.006	.022	.056	.104	.163	.241
LEEWARD .300	.007	.006	.004	.020	.054	.105	.165	.245
WING .250								
.200								
.150								
.100								
.050								

Table 3. Continued

(aa) Continued; station 2

	THETA, DEG	CP FOR ALPHA, DEG =							
		-4.00	.00	4.02	7.97	12.00	16.01	19.97	24.05
BODY	0	-.004	.006	-.005	-.029	-.051	-.083	-.105	-.115
	15	-.001	.006	-.005	-.039	-.084	-.111	-.101	-.081
	30	.002	.006	-.003	-.034	-.069	-.059	-.030	.005
	45	.002	.005	-.001	-.021	-.024	.001	.045	.101
	60	.003	.004	.002	-.004	.017	.057	.114	.191
	75	.005	.004	.005	.011	.044	.096	.161	.254
	90								
	105	.011	.012	.009	.018	.049	.093	.153	.240
	120	.005	.008	.003	.000	.019	.054	.108	.188
	135	.006	.010	.003	-.012	-.018	.004	.042	.101
	150	.005	.011	.003	-.021	-.058	-.053	-.032	.007
	165	.002	.012	.003	-.026	-.064	-.098	-.097	-.073
	180	-.003	.011	.002	-.019	-.044	-.063	-.076	-.085
	195	-.004	.009	.002	-.012	-.039	-.057	-.069	-.081
	210	.000	.011	.006	-.007	-.038	-.055	-.064	-.076
	225	.003	.012	.008	-.009	-.034	-.065	-.074	-.081
	240	.006	.011	.007	-.024	-.044	-.062	-.073	-.079
	255	.008	.009	.009	-.007	-.041	-.074	-.091	-.088
	270								
	285	.008	.006	.005	-.010	-.044	-.090	-.146	-.137
	300	.006	.007	.005	-.028	-.048	-.081	-.098	-.111
	315	.000	.007	.004	-.015	-.039	-.079	-.098	-.107
	330	-.004	.006	.002	-.013	-.043	-.076	-.099	-.104
	345	-.004	.008	.002	-.013	-.039	-.073	-.095	-.103
	Y/S	CP FOR ALPHA, DEG =							
		-4.00	.00	4.02	7.97	12.00	16.01	19.97	24.05
WINDWARD WING	.075								
	.150								
	.225								
	.300	.009	.008	.009	.001	-.033	-.092	-.135	-.133
	.375	.011	.009	.012	.008	-.034	-.090	-.128	-.127
	.450								
	.524	.007	.007	.010	.014	.003	-.093	-.128	-.143
	.599								
	.637								
	.674	-.036	-.012	.007	.013	.015	.011	-.116	-.144
LEEWARD WING	.674	.015	.013	-.005	-.003	.010	.030	.055	.129
	.637	.016	.012	.010	.013	.031	.059	.098	.178
	.599	.016	.013	.008	.014	.039	.076	.127	.199
	.524	.014	.010	.004	.010	.035	.075	.129	.207
	.450	.016	.012	.008	.013	.042	.084	.142	.222
	.375	.016	.012	.009	.016	.046	.089	.146	.231
	.300	.010	.009	.005	.013	.044	.087	.144	.230
	.225								
	.150								
	.075								

Table 3. Continued

(aa) Concluded; station 3

THETA, DEG	CP FOR ALPHA, DEG =							
	-4.00	.00	4.02	7.97	12.00	16.01	19.97	24.05
0	-.006	.002	-.005	-.026	-.041	-.064	-.099	-.119
15	-.002	.004	-.005	-.034	-.068	-.098	-.104	-.090
30	-.002	.002	-.006	-.032	-.070	-.062	-.036	-.007
45	-.002	.002	-.003	-.018	-.032	-.002	.040	.088
60	-.004	.000	-.001	-.002	.009	.052	.110	.179
75	.002	.002	.005	.012	.037	.085	.153	.231
90								
105	.007	.010	.011	.020	.036	.084	.139	.215
120	.002	.007	.005	.006	.014	.056	.110	.182
135	.002	.007	.001	-.010	-.019	.004	.042	.096
BODY 150	.001	.006	-.002	-.025	-.051	-.058	-.036	-.001
165	-.002	.005	-.006	-.032	-.074	-.103	-.101	-.088
180	-.005	.005	-.004	-.023	-.051	-.064	-.070	-.084
195	-.005	.006	-.001	-.012	-.033	-.053	-.061	-.076
210	-.004	.007	.001	-.010	-.030	-.051	-.062	-.078
225	-.001	.006	.001	-.011	-.027	-.052	-.066	-.079
240	.004	.006	.001	-.019	-.029	-.055	-.064	-.073
255	.008	.006	.004	-.014	-.035	-.080	-.077	-.079
270								
285	.010	.006	.005	-.012	-.040	-.080	-.125	-.129
300	.003	.003	.000	-.027	-.042	-.072	-.111	-.124
315	.003	.008	.005	-.011	-.028	-.060	-.091	-.112
330	-.004	.004	-.001	-.015	-.032	-.059	-.092	-.112
345	-.007	.003	-.003	-.018	-.033	-.059	-.091	-.112
Y/S	CP FOR ALPHA, DEG =							
	-4.00	.00	4.02	7.97	12.00	16.01	19.97	24.05
.190								
.274	.008	.005	.005	-.009	-.041	-.081	-.121	-.129
.379	.008	.006	.008	-.005	-.049	-.088	-.116	-.131
.473	.007	.005	.007	.006	-.046	-.124	-.126	-.143
WINDWARD .569								
WING .664	.003	.005	.007	.011	.011	-.046	-.137	-.152
.759	.002	.002	.007	.010	.016	.012	-.106	-.139
.806	.000	-.001	.006	.010	.016	.024	-.081	-.138
.854	-.020	-.007	.003	.008	.015	.028	-.040	-.139
.854	.009	.011	.004	-.004	-.005	.033	.046	.097
.806	.012	.013	.009	.010	.030	.063	.100	.155
.759	.012	.011	.007	.007	.026	.062	.105	.163
LEEWARD .664	.012	.012	.008	.007	.025	.065	.110	.173
WING .569	.011	.010	.007	.008	.026	.068	.118	.186
.473	.009	.007	.006	.009	.026	.071	.122	.195
.379	.007	.006	.007	.014	.029	.077	.129	.204
.274	.006	.008	.008	.016	.031	.079	.133	.208
.190								

Table 3. Continued

(bb) $M_\infty = 2.86; \phi = -90^\circ$; station 1

THETA, DEG	CP FOR ALPHA, DEG =							
	-3.97	.00	3.97	8.01	11.97	15.98	19.99	24.03
0								
15	-.002	.007	-.007	-.047	-.063	-.061	-.052	-.038
30	.004	.009	-.004	-.027	-.028	-.014	.005	.033
45	.007	.010	.002	-.005	.008	.035	.069	.113
60	.009	.009	.005	.012	.038	.079	.128	.187
75	.015	.012	.012	.029	.065	.115	.174	.250
90								
105	.012	.009	.011	.029	.061	.109	.169	.240
120	.007	.006	.005	.015	.038	.076	.126	.184
135	.007	.009	.003	.001	.013	.037	.073	.115
BODY 150	.001	.006	-.005	-.025	-.028	-.020	.000	.023
165	-.005	.004	-.009	-.046	-.062	-.063	-.055	-.043
180	-.012	.003	-.010	-.049	-.058	-.071	-.081	-.093
195	-.010	.005	-.003	-.024	-.043	-.064	-.072	-.080
210	-.006	.007	.003	-.013	-.042	-.064	-.072	-.080
225	.000	.009	.007	-.010	-.063	-.071	-.076	-.083
240	.007	.008	.009	-.015	-.071	-.078	-.087	-.093
255	.015	.011	.012	-.004	-.031	-.078	-.087	-.096
270								
285	.005	.000	.003	-.005	-.028	-.072	-.087	-.095
300	-.001	.000	.000	-.018	-.069	-.077	-.087	-.096
315	-.004	.002	.000	-.015	-.064	-.074	-.084	-.092
330	-.010	.002	-.003	-.018	-.048	-.072	-.082	-.091
345	-.012	.004	-.006	-.026	-.050	-.072	-.080	-.090
Y/S	CP FOR ALPHA, DEG =							
	-3.97	.00	3.97	8.01	11.97	15.98	19.99	24.03
.050								
.100								
.150								
.200								
WINDWARD .250								
WING .300	.005	-.001	.004	.002	-.017	-.088	-.111	-.108
.350	.007	.000	.004	.005	-.013	-.089	-.118	-.114
.400	-.005	-.004	.001	.005	-.005	-.096	-.118	-.120
.425								
.450	-.012	-.012	-.004	.004	.005	-.061	-.118	-.119
.450	.015	.005	.004	.017	.040	.068	.111	.152
.425	.016	.007	.008	.022	.046	.075	.119	.168
.400	.015	.006	.008	.023	.051	.089	.147	.218
.350	.014	.008	.009	.028	.060	.108	.166	.234
LEEWARD .300	.012	.006	.008	.026	.060	.108	.168	.239
WING .250								
.200								
.150								
.100								
.050								

Table 3. Continued

(bb) Continued; station 2

THETA, DEG	CP FOR ALPHA, DEG =								
	-3.97	.00	3.97	8.01	11.97	15.98	19.99	24.03	
0	.004	.009	-.003	-.024	-.050	-.066	-.086	-.096	
15	.008	.010	-.003	-.038	-.068	-.068	-.059	-.044	
30	.009	.010	-.002	-.035	-.039	-.023	-.003	.027	
45	.009	.010	.001	-.014	-.001	.028	.062	.109	
60	.009	.009	.003	.006	.030	.073	.122	.187	
75	.013	.012	.009	.022	.055	.108	.169	.244	
90									
105	.013	.014	.011	.024	.057	.104	.167	.233	
120	.012	.013	.009	.012	.037	.076	.130	.188	
135	.011	.012	.006	-.007	.005	.031	.069	.111	
BODY 150	.009	.011	.003	-.026	-.030	-.020	.003	.028	
165	.008	.012	.003	-.026	-.057	-.061	-.050	-.037	
180	.002	.011	.002	-.019	-.044	-.051	-.061	-.077	
195	.000	.011	.004	-.009	-.033	-.043	-.056	-.067	
210	-.001	.010	.005	-.008	-.034	-.045	-.055	-.068	
225	-.001	.008	.005	-.011	-.034	-.057	-.063	-.072	
240	.004	.007	.006	-.022	-.036	-.054	-.063	-.071	
255	.008	.005	.007	-.006	-.035	-.066	-.079	-.078	
270									
285	.008	.006	.007	-.004	-.038	-.076	-.104	-.103	
300	.004	.006	.005	-.023	-.044	-.067	-.081	-.095	
315	.001	.007	.004	-.012	-.038	-.063	-.080	-.092	
330	-.002	.007	.002	-.011	-.041	-.062	-.081	-.092	
345	.000	.009	.000	-.014	-.041	-.062	-.079	-.090	
Y/S	CP FOR ALPHA, DEG =								
	-3.97	.00	3.97	8.01	11.97	15.98	19.99	24.03	
.075									
.150									
.225									
WINDWARD .300	.007	.007	.008	.002	-.034	-.077	-.102	-.105	
.375	.008	.007	.009	.008	-.037	-.079	-.100	-.105	
WING .450									
.524	.008	.006	.009	.013	.003	-.072	-.100	-.110	
.599									
.637									
.674	-.023	-.018	-.004	.008	.013	.013	-.097	-.109	
.674	.012	.007	.005	.013	.027	.051	.089	.124	
.637	.015	.015	.011	.017	.034	.065	.112	.151	
.599	.017	.016	.015	.022	.045	.077	.129	.185	
.524	.017	.016	.016	.024	.051	.094	.145	.207	
LEEWARD .450	.016	.015	.012	.023	.051	.096	.152	.217	
.375	.017	.015	.012	.025	.056	.102	.161	.226	
.300	.015	.015	.011	.025	.057	.104	.165	.229	
.225									
.150									
.075									

Table 3. Concluded

(bb) Concluded; station 3

THETA, DEG	CP FOR ALPHA, DEG =							
	-3.97	.00	3.97	8.01	11.97	15.98	19.99	24.03
0	.005	.012	.001	-.014	-.036	-.058	-.080	-.095
15	.008	.014	.002	-.023	-.056	-.066	-.057	-.038
30	.007	.013	.003	-.023	-.037	-.024	-.003	.030
45	.007	.014	.008	-.007	.000	.030	.066	.115
60	.005	.013	.012	.012	.035	.077	.129	.195
75	.010	.015	.018	.028	.059	.108	.168	.240
90								
105	.015	.018	.024	.032	.062	.106	.165	.232
120	.009	.016	.019	.018	.039	.079	.133	.200
135	.010	.017	.015	.001	.005	.033	.074	.121
BODY 150	.009	.016	.010	-.014	-.034	-.020	.006	.034
165	.008	.016	.007	-.021	-.063	-.066	-.054	-.040
180	.005	.014	.004	-.015	-.043	-.053	-.056	-.074
195	.004	.014	.006	-.007	-.030	-.043	-.048	-.064
210	.007	.015	.009	-.003	-.024	-.041	-.049	-.063
225	.005	.010	.007	-.006	-.025	-.044	-.054	-.068
240	.008	.008	.006	-.013	-.026	-.043	-.051	-.063
255	.011	.010	.010	-.004	-.027	-.063	-.055	-.061
270								
285	.016	.012	.012	-.001	-.032	-.066	-.094	-.096
300	.010	.009	.007	-.018	-.037	-.060	-.081	-.092
315	.008	.011	.008	-.007	-.033	-.056	-.076	-.089
330	.005	.011	.006	-.005	-.029	-.049	-.072	-.088
345	.008	.012	.007	-.005	-.027	-.049	-.072	-.087

Y/S	CP FOR ALPHA, DEG =							
	-3.97	.00	3.97	8.01	11.97	15.98	19.99	24.03
.190								
.274	.015	.013	.013	.003	-.032	-.067	-.091	-.095
.379	.011	.008	.011	.003	-.045	-.075	-.091	-.098
WINDWARD .473	.012	.012	.015	.015	-.036	-.094	-.097	-.103
WING .569								
.664	.009	.010	.011	.015	.015	-.040	-.093	-.104
.759	.007	.009	.009	.012	.017	.010	-.081	-.094
.806	-.018	.008	.010	.013	.018	.023	-.068	-.088
.854	-.022	-.012	.007	.012	.018	.028	-.046	-.087
.854	.020	.011	.006	.007	.027	.053	.091	.124
.806	.019	.016	.014	.018	.036	.061	.099	.137
.759	.019	.016	.016	.022	.048	.080	.120	.167
LEEWARD .664	.018	.016	.016	.024	.050	.089	.133	.190
WING .569	.016	.015	.015	.021	.049	.089	.139	.199
.473	.016	.018	.018	.024	.054	.096	.151	.214
.379	.015	.017	.021	.027	.058	.099	.157	.222
.274	.016	.020	.025	.033	.060	.103	.162	.228
.190								

Table 4. Configuration 2

(a) $M_\infty = 1.70$; station 1

THETA, DEG	CP FOR ALPHA, DEG =							
	-4.02	.02	3.96	8.02	12.04	16.00	20.05	24.07
0	.000	.008	.021	.039	.041	.080	.158	.229
15	.003	.012	.026	.046	.058	.071	.139	.209
30	-.004	.008	.023	.045	.059	.036	.067	.128
45	-.008	.008	.025	.046	.065	.051	-.023	.018
60	-.015	.005	.026	.051	.079	.090	.028	.019
75	-.018	.008	.033	.065	.093	.116	.110	.137
90	-.032	.001	.031	.063	.085	.103	.112	.134
105	-.038	.001	.033	.053	.082	.085	.066	.079
120	-.050	-.007	.071	.057	.103	.110	.070	.089
135	-.054	-.011	.033	.087	.136	.176	.270	.284
BODY								
150								
165								
180								
195								
210								
225	-.049	-.004	.033	.086	.148	.201	.242	.330
240	-.044	.000	.035	.069	.140	.167	.085	.113
255	-.038	.007	.036	.054	.050	.037	.028	.062
270	.010	.162	.178	.243	.376	.353	.375	.379
285	-.020	.007	.030	.062	.094	.104	.114	.133
300	-.015	.007	.023	.044	.078	.089	.063	.033
315	-.011	.008	.019	.036	.052	.025	-.030	.008
330	-.004	.011	.022	.038	.045	.017	.066	.124
345	-.001	.011	.022	.039	.036	.065	.135	.202
Y/S	CP FOR ALPHA, DEG =							
	-4.02	.02	3.96	8.02	12.04	16.00	20.05	24.07
.050								
.100								
.150								
.200								
WINDWARD								
WING								
.250	-.040	.005	.045	.098	.162	.213	.234	.270
.300	-.040	.002	.042	.091	.148	.175	.130	.131
.350	-.058	.003	.046	.098	.156	.171	.162	.145
.400	-.186	.002	.049	.107	.177	.241	.302	.342
.425	-.157	.001	.050	.111	.184	.263	.340	.412
.450	-.156	-.007	.050	.113	.186	.272	.353	.442
.450	.061	.008	-.125	-.193	-.240	-.264	-.273	-.310
.425	.055	.005	-.139	-.203	-.248	-.266	-.275	-.310
.400	.056	.010	-.143	-.204	-.244	-.265	-.277	-.309
.350	.051	.010	-.031	-.252	-.277	-.292	-.301	-.324
.300	.048	.008	-.010	-.097	-.259	-.336	-.331	-.336
.250	.046	.007	-.017	-.054	-.148	-.254	-.304	-.317
.200	.048	.011	-.013	-.045	-.097	-.161	-.252	-.274
.150	.048	.012	-.012	-.043	-.081	-.104	-.202	-.231
.100	.042	.007	-.017	-.046	-.074	-.088	-.175	-.204
.050	.045	.012	-.012	-.037	-.065	-.079	-.150	-.176
LEEWARD								
WING								

Table 4. Continued

(a) Continued; station 2

THETA, DEG	CP FOR ALPHA, DEG =							
	-4.02	.02	3.96	8.02	12.04	16.00	20.05	24.07
0	-.011	.013	.039	.081	.142	.187	.259	.326
15	-.012	.013	.039	.082	.137	.184	.250	.318
30	-.013	.015	.042	.084	.132	.180	.243	.300
45	-.014	.016	.045	.089	.133	.184	.242	.303
60	-.017	.015	.046	.092	.137	.194	.253	.322
75	-.020	.014	.046	.093	.136	.195	.250	.318
90	-.023	.013	.047	.095	.135	.193	.245	.307
105	-.023	.015	.047	.080	.109	.142	.142	.214
120	-.023	.012	.052	.109	.153	.232	.300	.353
135	-.027	.008	.047	.100	.144	.206	.274	.345
BODY								
150								
165								
180								
195								
210								
225								
240	-.020	.017	.054	.107	.153	.225	.305	.382
255	-.021	.017	.048	.071	.109	.148	.156	.203
270	.010	.163	.178	.243	.376	.354	.376	.379
285	-.025	.012	.042	.085	.132	.187	.236	.309
300	-.020	.014	.043	.084	.134	.192	.246	.318
315	-.019	.012	.038	.076	.124	.179	.232	.297
330	-.018	.011	.037	.075	.124	.175	.235	.293
345	-.012	.015	.040	.081	.138	.185	.259	.317
Y/S								
	-4.02	.02	3.96	8.02	12.04	16.00	20.05	24.07
.075								
.150								
.225	-.020	.016	.052	.104	.150	.210	.272	.342
.300	-.019	.017	.053	.105	.150	.212	.281	.353
WINDWARD								
WING								
.375	-.016	.017	.054	.106	.145	.185	.233	.275
.450	-.017	.014	.053	.105	.160	.213	.273	.343
.524	-.107	.014	.057	.110	.176	.253	.335	.437
.599	-.154	.013	.061	.114	.184	.263	.349	.458
.637	-.128	.010	.062	.116	.185	.261	.345	.449
.674	-.122	.011	.069	.121	.186	.258	.336	.434
.674	.076	.022	-.102	-.187	-.244	-.293	-.298	-.328
.637	.068	.019	-.109	-.194	-.249	-.297	-.304	-.330
.599	.064	.020	-.122	-.195	-.244	-.287	-.307	-.332
.524	.055	.014	-.090	-.272	-.276	-.297	-.328	-.347
LEEWARD								
WING								
.450	.056	.018	.000	-.140	-.283	-.339	-.363	-.369
.375	.054	.018	-.008	-.053	-.169	-.266	-.337	-.361
.300	.047	.011	-.018	-.049	-.113	-.195	-.278	-.325
.225	.051	.016	-.014	-.045	-.085	-.146	-.212	-.268
.150	.049	.014	-.015	-.047	-.079	-.128	-.173	-.220
.075	.049	.015	-.013	-.046	-.077	-.121	-.153	-.186

Table 4. Continued

(a) Concluded; station 3

THETA, DEG	CP FOR ALPHA, DEG =							
	-4.02	.02	3.96	8.02	12.04	16.00	20.05	24.07
0	-.013	.013	.042	.085	.139	.204	.291	.380
15	-.013	.014	.044	.086	.141	.207	.290	.372
30	-.018	.012	.043	.084	.139	.207	.282	.352
45	-.021	.009	.041	.083	.140	.206	.279	.342
60	-.025	.006	.038	.082	.140	.205	.277	.343
75	-.024	.008	.040	.084	.141	.206	.275	.337
90	-.028	.004	.036	.078	.135	.195	.260	.316
105	-.029	.004	.037	.072	.116	.164	.215	.251
120	-.039	-.008	.031	.075	.130	.200	.274	.327
135								
BODY								
150								
165								
180								
195								
210								
225								
240	-.026	.007	.046	.095	.153	.225	.301	.394
255								
270	-.027	.007	.041	.087	.142	.204	.272	.351
285	-.025	.011	.043	.092	.148	.210	.284	.364
300	-.026	.008	.040	.087	.145	.206	.283	.363
315	-.019	.015	.047	.092	.153	.211	.289	.369
330	-.018	.012	.041	.085	.144	.203	.281	.359
345	-.015	.012	.041	.085	.140	.203	.286	.370
Y/S	CP FOR ALPHA, DEG =							
	-4.02	.02	3.96	8.02	12.04	16.00	20.05	24.07
.190								
.274	-.025	.008	.045	.093	.150	.213	.286	.368
.379	-.021	.012	.050	.099	.149	.196	.266	.338
.473								
WINDWARD								
WING								
.569	-.015	.013	.053	.112	.180	.251	.335	.430
.664	-.137	.011	.055	.109	.179	.256	.344	.442
.759	-.140	.011	.060	.111	.181	.255	.340	.434
.806	-.123	.010	.063	.112	.179	.252	.331	.422
.854	-.120	.009	.065	.114	.177	.247	.319	.405
.854	.072	.012	-.109	-.192	-.255	-.299	-.327	-.346
.806	.070	.015	-.110	-.195	-.258	-.300	-.340	-.350
.759	.069	.017	-.136	-.191	-.246	-.289	-.341	-.352
LEEWARD								
WING								
.664	.066	.018	-.103	-.268	-.265	-.294	-.338	-.370
.569	.063	.018	-.001	-.162	-.298	-.349	-.373	-.401
.473	.058	.014	-.012	-.062	-.193	-.285	-.352	-.377
.379	.058	.015	-.014	-.046	-.120	-.208	-.286	-.322
.274	.059	.016	-.014	-.047	-.095	-.161	-.224	-.267
.190	.055	.015	-.017	-.050	-.088	-.141	-.185	-.225

C-2

Table 4. Continued

(b) $M_\infty = 2.16$; station 1

	THETA, DEG	CP FOR ALPHA, DEG =							
		-3.95	.04	4.02	8.01	12.95	16.01	19.99	
BODY	0	-.002	.005	.008	.016	.053	.104	.175	
	15	-.005	.004	.010	.014	.043	.091	.156	
	30	-.006	.007	.017	.022	.023	.056	.109	
	45	-.010	.007	.022	.038	.029	-.001	.036	
	60	-.018	.004	.024	.050	.048	-.009	-.030	
	75	-.025	.003	.030	.057	.051	.060	.071	
	90	-.029	.004	.035	.060	.052	.064	.083	
	105	-.034	.003	.032	.028	.065	.041	.061	
	120	-.040	-.002	.032	.071	.085	.060	.049	
	135	-.045	-.004	.041	.096	.114	.158	.164	
	150								
	165								
	180								
	195								
	210								
	225	-.051	-.004	.037	.092	.128	.163	.185	
	240	-.050	-.002	.031	.071	.113	.082	.075	
	255	-.044	.000	.031	.024	.040	.002	.040	
	270	.043	.045	.074	.112	.111	.346	.467	
	285	-.028	-.001	.022	.049	.046	.054	.076	
	300	-.021	-.002	.015	.033	.034	-.020	-.028	
315	-.013	.002	.013	.012	-.013	-.008	.034		
330	-.010	.002	.007	.001	.010	.047	.105		
345	-.005	.004	.007	.010	.040	.088	.156		
WINDWARD WING	Y/S								
		-3.95	.04	4.02	8.01	12.95	16.01	19.99	
	.050								
	.100								
	.150								
	.200								
	.250	-.049	-.003	.039	.094	.132	.166	.176	
	.300	-.045	-.001	.042	.092	.121	.110	.111	
	.350	-.075	-.003	.043	.094	.119	.136	.149	
	.400	-.147	-.005	.048	.104	.157	.224	.301	
	.425	-.138	-.003	.054	.113	.175	.252	.338	
	.450	-.132	-.010	.055	.114	.183	.263	.349	
	LEEWARD WING	.450	.052	.007	-.105	-.149	-.171	-.182	-.199
		.425	.048	.007	-.115	-.162	-.177	-.180	-.197
		.400	.043	.006	-.122	-.166	-.186	-.188	-.201
		.350	.039	.007	-.079	-.181	-.187	-.200	-.210
		.300	.036	.006	-.010	-.112	-.203	-.214	-.216
		.250	.038	.010	-.013	-.045	-.146	-.203	-.199
		.200	.033	.006	-.018	-.043	-.089	-.162	-.179
		.150	.029	.003	-.020	-.043	-.068	-.115	-.155
		.100	.029	.004	-.019	-.040	-.051	-.087	-.132
.050	.028	.002	-.020	-.038	-.050	-.080	-.118		

Table 4. Continued

(b) Continued; station 2

THETA, DEG	CP FOR ALPHA, DEG =						
	-3.95	.04	4.02	8.01	12.95	16.01	19.99
BODY							
0	-.019	.002	.027	.058	.085	.120	.173
15	-.020	.002	.027	.057	.087	.121	.170
30	-.025	-.001	.025	.056	.089	.121	.162
45	-.026	.000	.027	.064	.099	.138	.180
60	-.030	-.003	.024	.062	.102	.147	.200
75	-.030	-.002	.027	.064	.105	.148	.204
90	-.037	-.008	.020	.055	.088	.135	.192
105	-.037	-.008	.015	.041	.057	.078	.112
120	-.029	.001	.034	.086	.139	.219	.274
135	-.032	-.002	.032	.079	.125	.183	.241
150							
165							
180							
195							
210							
225							
240	-.032	-.003	.030	.078	.126	.194	.278
255	-.033	-.002	.024	.046	.067	.084	.123
270	.038	.041	.070	.108	.107	.343	.468
285	-.027	.003	.031	.067	.109	.154	.209
300	-.028	.000	.027	.063	.107	.153	.205
315	-.024	.002	.028	.061	.103	.140	.177
330	-.023	.001	.027	.056	.089	.119	.158
345	-.022	.000	.024	.054	.082	.114	.166
Y/S							
	-3.95	.04	4.02	8.01	12.95	16.01	19.99
WINDWARD WING							
.075							
.150							
.225	-.031	-.001	.032	.079	.126	.180	.245
.300	-.032	-.002	.031	.076	.123	.183	.250
.375	-.028	.000	.034	.078	.111	.158	.198
.450	-.025	.002	.037	.084	.135	.196	.256
.524	-.131	.002	.042	.092	.159	.233	.317
.599	-.127	.001	.046	.098	.168	.244	.332
.637	-.117	.001	.050	.103	.173	.247	.333
.674	-.112	-.007	.049	.102	.168	.239	.320
LEEWARD WING							
.674	.052	.003	-.104	-.151	-.183	-.201	-.222
.637	.049	.003	-.114	-.166	-.197	-.214	-.220
.599	.045	.002	-.119	-.167	-.197	-.218	-.222
.524	.046	.007	-.113	-.175	-.193	-.211	-.223
.450	.035	.001	-.018	-.163	-.222	-.230	-.237
.375	.034	.001	-.021	-.069	-.173	-.217	-.240
.300	.036	.003	-.021	-.047	-.106	-.169	-.208
.225	.034	.002	-.025	-.049	-.081	-.130	-.173
.150	.033	.001	-.026	-.049	-.073	-.107	-.136
.075	.034	.003	-.022	-.047	-.069	-.095	-.108

Table 4. Continued

(b) Concluded; station 3

THETA, DEG	CP FOR ALPHA, DEG =						
	-3.95	.04	4.02	8.01	12.95	16.01	19.99
0	-.017	.003	.031	.070	.117	.176	.241
15	-.020	.003	.031	.072	.117	.173	.237
30	-.026	-.002	.026	.068	.113	.166	.231
45	-.024	.001	.031	.071	.117	.172	.242
60	-.026	.000	.031	.070	.116	.173	.243
75	-.027	.000	.031	.068	.114	.170	.238
90	-.027	.001	.030	.065	.111	.165	.232
105	-.032	-.004	.027	.062	.085	.130	.175
120	-.034	-.005	.033	.076	.132	.197	.279
135							
BODY							
150							
165							
180							
195							
210							
225							
240	-.025	.004	.040	.084	.138	.200	.275
255							
270	-.022	.007	.037	.072	.117	.169	.237
285	-.024	.005	.035	.076	.120	.172	.241
300	-.024	.005	.034	.075	.122	.172	.246
315	-.025	.003	.030	.071	.120	.169	.241
330	-.021	.005	.032	.070	.120	.167	.237
345	-.016	.007	.035	.072	.120	.173	.241
Y/S	CP FOR ALPHA, DEG =						
	-3.95	.04	4.02	8.01	12.95	16.01	19.99
.190							
.274	-.022	.006	.042	.086	.135	.192	.263
.379	-.024	.004	.040	.084	.121	.171	.233
.473							
WINDWARD							
WING							
.569	-.024	.006	.045	.092	.149	.220	.304
.664	-.140	.008	.050	.100	.159	.235	.321
.759	-.114	.004	.050	.102	.159	.234	.317
.806	-.107	.004	.053	.105	.162	.236	.314
.854	-.099	.002	.057	.108	.163	.232	.307
.854	.058	.008	-.097	-.142	-.176	-.197	-.215
.806	.055	.008	-.103	-.161	-.194	-.215	-.221
.759	.050	.005	-.114	-.166	-.198	-.219	-.231
LEEWARD							
WING							
.664	.049	.007	-.121	-.173	-.197	-.212	-.236
.569	.045	.005	-.014	-.178	-.221	-.226	-.246
.473	.048	.010	-.010	-.072	-.171	-.217	-.237
.379	.044	.008	-.017	-.046	-.113	-.175	-.205
.274	.045	.010	-.017	-.042	-.081	-.129	-.165
.190	.041	.006	-.020	-.044	-.075	-.111	-.137

Table 4. Continued

(c) $M_\infty = 2.40$; station 1

THETA, DEG	CP FOR ALPHA, DEG =							
	-1.53	-.03	4.02	7.90	12.02	15.98	20.03	23.98
0	.050	.007	.007	.021	.063	.114	.189	.269
15	.047	.008	.012	.018	.056	.104	.176	.248
30	.036	.010	.018	.014	.033	.071	.130	.190
45	.019	.010	.026	.029	.005	.020	.061	.104
60	.001	.008	.031	.047	.027	-.025	-.014	.010
75	.014	.009	.037	.056	.051	.050	.067	.095
90	.011	.009	.039	.055	.049	.055	.079	.110
105	.003	.007	.035	.025	.067	.051	.056	.090
120	-.005	.004	.040	.070	.078	.059	.043	.068
135	.012	.001	.048	.093	.108	.133	.167	.204
BODY								
150								
165								
180								
195								
210								
225	.014	.000	.042	.093	.121	.146	.175	.200
240	-.007	.001	.035	.072	.099	.073	.080	.131
255	-.007	.004	.034	.022	.053	.028	.043	.080
270	.150	.073	.062	.070	.122	.071	.083	.098
285	.013	.004	.025	.046	.037	.038	.057	.092
300	-.001	.003	.015	.028	-.005	-.033	-.023	.004
315	.017	.005	.009	.001	-.010	.013	.051	.096
330	.033	.005	.005	.002	.026	.064	.119	.182
345	.046	.006	.006	.016	.054	.101	.169	.245
Y/S	CP FOR ALPHA, DEG =							
	-1.53	-.03	4.02	7.90	12.02	15.98	20.03	23.98
.050								
.100								
.150								
.200								
WINDWARD								
WING								
.250	.014	.002	.044	.095	.125	.149	.166	.191
.300	.002	.003	.044	.090	.102	.097	.103	.136
.350	-.019	.003	.048	.094	.109	.133	.158	.177
.400	-.030	.001	.051	.103	.165	.228	.303	.377
.425	-.020	.002	.057	.111	.186	.254	.337	.423
.450	-.013	-.012	.060	.114	.195	.263	.347	.437
.450	.022	-.013	-.101	-.131	-.151	-.159	-.176	-.187
.425	.021	.000	-.104	-.140	-.154	-.156	-.172	-.184
.400	.017	.003	-.114	-.146	-.163	-.162	-.176	-.186
.350	.013	.004	-.105	-.153	-.162	-.170	-.180	-.191
.300	.008	.004	-.014	-.117	-.169	-.178	-.187	-.196
.250	.011	.006	-.012	-.044	-.142	-.176	-.179	-.191
.200	.013	.005	-.015	-.036	-.092	-.150	-.166	-.179
.150	.016	.005	-.015	-.035	-.065	-.114	-.144	-.160
.100	.017	.002	-.016	-.036	-.048	-.088	-.126	-.142
.050	.021	.004	-.015	-.031	-.045	-.078	-.115	-.132
LEEWARD								
WING								

Table 4. Continued

(c) Continued; station 2

THETA, DEG	CP FOR ALPHA, DEG =							
	-1.53	-.03	4.02	7.90	12.02	15.98	20.03	23.98
0	.038	.004	.026	.052	.075	.107	.177	.259
15	.036	.005	.027	.053	.078	.103	.164	.240
30	.032	.004	.028	.054	.081	.101	.141	.196
45	.034	.004	.031	.060	.093	.119	.168	.221
60	.035	.002	.031	.061	.101	.135	.195	.263
75	.035	.003	.034	.064	.104	.137	.197	.266
90	.030	.001	.029	.060	.090	.126	.185	.252
105	.014	.000	.028	.046	.052	.074	.112	.167
120	.043	.004	.044	.087	.144	.210	.271	.338
135	.038	.003	.043	.084	.128	.182	.237	.315
BODY 150								
165								
180								
195								
210								
225								
240	.044	.003	.037	.082	.133	.188	.266	.348
255	.015	.002	.028	.047	.052	.070	.108	.162
270	.145	.067	.057	.064	.116	.066	.078	.092
285	.034	.004	.032	.062	.101	.137	.194	.263
300	.035	.002	.029	.059	.100	.136	.194	.262
315	.032	.003	.028	.057	.092	.118	.165	.219
330	.031	.003	.025	.052	.077	.094	.128	.194
345	.035	.003	.025	.052	.073	.096	.157	.235
Y/S	CP FOR ALPHA, DEG =							
	-1.53	-.03	4.02	7.90	12.02	15.98	20.03	23.98
.075								
.150								
.225	.039	.003	.038	.080	.128	.172	.238	.309
.300	.039	.002	.038	.080	.127	.175	.243	.318
WINDWARD WING .375	.033	.004	.039	.081	.111	.144	.185	.237
.450	.041	.003	.040	.085	.136	.192	.265	.335
.524	-.027	.004	.044	.093	.160	.233	.330	.423
.599	-.016	.001	.047	.098	.169	.245	.341	.438
.637	-.009	.002	.052	.103	.175	.248	.342	.438
.674	-.008	-.004	.052	.103	.173	.243	.331	.424
.674	.019	-.005	-.099	-.133	-.161	-.174	-.195	-.198
.637	.016	.000	-.104	-.144	-.171	-.180	-.195	-.199
.599	.012	.000	-.112	-.151	-.174	-.185	-.194	-.199
.524	.010	.003	-.118	-.152	-.171	-.185	-.196	-.200
LEEWARD WING .450	.004	.001	-.033	-.157	-.186	-.195	-.205	-.209
.375	.004	.002	-.016	-.074	-.161	-.191	-.204	-.204
.300	.008	.003	-.019	-.046	-.111	-.160	-.185	-.189
.225	.013	.002	-.020	-.045	-.083	-.126	-.161	-.173
.150	.018	.002	-.022	-.045	-.072	-.104	-.139	-.159
.075	.023	.003	-.020	-.043	-.068	-.093	-.120	-.149

Table 4. Continued

(c) Concluded; station 3

THETA, DEG	CP FOR ALPHA, DEG =							
	-1.53	-.03	4.02	7.90	12.02	15.98	20.03	23.98
0	.049	.007	.032	.067	.111	.161	.234	.319
15	.047	.007	.034	.069	.112	.161	.235	.315
30	.043	.004	.031	.066	.111	.159	.230	.304
45	.045	.005	.033	.067	.117	.168	.242	.314
60	.043	.004	.032	.067	.118	.169	.245	.322
75	.042	.004	.033	.067	.118	.167	.241	.318
90	.041	.004	.028	.060	.112	.158	.231	.307
105	.028	.001	.032	.061	.093	.129	.181	.236
120	.045	.000	.035	.075	.144	.208	.292	.374
135								
BODY								
150								
165								
180								
195								
210								
225								
240	.050	.004	.040	.077	.142	.205	.283	.371
255								
270	.043	.009	.034	.061	.111	.161	.228	.310
285	.044	.008	.036	.069	.116	.167	.236	.321
300	.045	.007	.034	.069	.118	.169	.242	.325
315	.045	.007	.034	.069	.116	.168	.238	.319
330	.046	.008	.033	.068	.111	.161	.227	.308
345	.050	.008	.034	.068	.111	.161	.231	.316
Y/S	CP FOR ALPHA, DEG =							
	-1.53	-.03	4.02	7.90	12.02	15.98	20.03	23.98
.190								
.274	.049	.006	.040	.078	.137	.196	.266	.351
.379	.044	.005	.039	.078	.124	.174	.236	.312
.473								
WINDWARD								
WING								
.569	.052	.006	.044	.089	.151	.224	.312	.413
.664	-.025	.008	.049	.096	.162	.236	.326	.431
.759	-.007	.006	.051	.097	.164	.235	.323	.426
.806	-.002	.006	.054	.101	.167	.235	.320	.420
.854	.002	.005	.058	.106	.170	.233	.314	.409
.854	.025	.002	-.089	-.127	-.154	-.170	-.188	-.197
.806	.022	.005	-.093	-.134	-.166	-.180	-.190	-.197
.759	.017	.004	-.101	-.147	-.175	-.190	-.197	-.202
LEEWARD								
WING								
.664	.014	.006	-.119	-.148	-.172	-.186	-.200	-.204
.569	.009	.006	-.038	-.163	-.183	-.192	-.204	-.209
.473	.011	.009	-.007	-.081	-.163	-.192	-.202	-.202
.379	.014	.007	-.014	-.045	-.114	-.162	-.183	-.185
.274	.021	.008	-.016	-.041	-.080	-.125	-.154	-.165
.190	.023	.008	-.017	-.042	-.073	-.107	-.135	-.156

Table 4. Continued

(d) $M_\infty = 2.86$; station 1

	THETA, DEG	CP FOR ALPHA, DEG =							
		-4.04	.04	4.03	8.03	11.96	16.05	19.96	24.03
BODY	0	.007	.009	.011	.032	.071	.122	.186	.265
	15	.006	.011	.014	.029	.065	.114	.174	.248
	30	.003	.012	.016	.019	.045	.084	.133	.195
	45	-.001	.012	.022	.015	.015	.041	.075	.120
	60	-.009	.011	.028	.035	-.002	-.008	.010	.037
	75	-.014	.012	.034	.048	.042	.035	.046	.069
	90	-.021	.010	.036	.048	.046	.046	.061	.090
	105	-.025	.010	.034	.030	.047	.042	.051	.078
	120	-.033	.005	.037	.060	.058	.041	.047	.071
	135	-.035	.004	.046	.084	.101	.113	.126	.155
	150								
	165								
	180								
	195								
	210								
	225	-.040	.004	.042	.087	.108	.122	.143	.181
	240	-.041	.003	.033	.059	.073	.074	.096	.126
	255	-.033	.007	.032	.024	.040	.037	.052	.078
	270	.102	.104	.084	.068	.134	.079	.101	.123
	285	-.016	.008	.024	.036	.022	.018	.038	.067
	300	-.010	.006	.014	.012	-.020	-.015	.005	.032
315	-.003	.008	.010	.000	.008	.034	.070	.114	
330	.001	.008	.008	.015	.039	.077	.128	.189	
345	.005	.009	.010	.028	.063	.110	.171	.245	
WINDWARD WING	Y/S								
		-4.04	.04	4.03	8.03	11.96	16.05	19.96	24.03
	.050								
	.100								
	.150								
	.200								
	.250	-.039	.005	.043	.087	.108	.121	.138	.171
	.300	-.036	.005	.042	.081	.082	.079	.091	.118
	.350	-.081	.005	.045	.086	.102	.131	.162	.203
	.400	-.097	.000	.047	.096	.152	.220	.285	.365
	.425	-.094	-.010	.053	.106	.169	.244	.314	.403
	.450	-.088	-.015	.053	.110	.177	.252	.323	.414
	.450	.052	-.005	-.077	-.101	-.110	-.119	-.126	-.134
	.425	.049	.003	-.074	-.101	-.110	-.116	-.123	-.130
	.400	.045	.010	-.080	-.108	-.118	-.119	-.126	-.133
	.350	.041	.010	-.071	-.111	-.117	-.124	-.127	-.134
	.300	.038	.009	-.008	-.110	-.120	-.127	-.130	-.136
	.250	.038	.010	-.008	-.039	-.113	-.128	-.129	-.135
	.200	.037	.009	-.010	-.028	-.078	-.118	-.121	-.131
	.150	.036	.009	-.010	-.027	-.052	-.098	-.108	-.119
	.100	.033	.008	-.011	-.027	-.039	-.080	-.098	-.107
.050	.035	.008	-.009	-.023	-.034	-.069	-.090	-.098	
LEEWARD WING									

Table 4. Continued

(d) Continued; station 2

THETA, DEG	CP FOR ALPHA, DEG =							
	-4.04	.04	4.03	8.03	11.96	16.05	19.96	24.03
0	.009	.023	.039	.056	.080	.131	.196	.273
15	.007	.024	.041	.059	.080	.122	.184	.256
30	.003	.023	.042	.061	.078	.095	.142	.202
45	.001	.023	.044	.068	.090	.102	.126	.164
60	-.003	.020	.044	.072	.102	.133	.177	.234
75	-.004	.020	.046	.074	.106	.139	.181	.239
90	-.010	.018	.043	.073	.098	.133	.171	.228
105	-.014	.017	.042	.058	.070	.096	.126	.168
120	-.016	.017	.054	.096	.151	.205	.249	.305
135	-.015	.018	.056	.097	.139	.184	.224	.290
BODY								
150								
165								
180								
195								
210								
225								
240	-.013	.020	.052	.096	.141	.195	.256	.328
255	-.013	.020	.044	.058	.062	.091	.124	.174
270	.106	.111	.090	.073	.140	.085	.106	.129
285	-.008	.020	.044	.071	.099	.132	.182	.245
300	-.005	.020	.042	.068	.098	.129	.177	.239
315	-.001	.022	.041	.064	.085	.100	.126	.164
330	.002	.022	.039	.057	.067	.090	.137	.198
345	.008	.024	.039	.056	.073	.120	.180	.253
Y/S	CP FOR ALPHA, DEG =							
	-4.04	.04	4.03	8.03	11.96	16.05	19.96	24.03
.075								
.150								
.225	-.012	.021	.053	.095	.138	.183	.235	.299
.300	-.013	.020	.052	.094	.135	.182	.235	.303
.375	-.009	.021	.054	.096	.122	.147	.179	.223
WINDWARD								
WING								
.450	-.029	.019	.054	.100	.147	.203	.263	.345
.524	-.091	.020	.059	.108	.167	.242	.322	.426
.599	-.082	.019	.062	.114	.176	.253	.334	.438
.637	-.079	.015	.065	.119	.180	.255	.336	.439
.674	-.079	-.001	.070	.121	.181	.253	.332	.430
.674	.063	.011	-.065	-.092	-.105	-.120	-.127	-.130
.637	.060	.023	-.065	-.092	-.109	-.119	-.126	-.129
.599	.057	.022	-.070	-.098	-.114	-.120	-.126	-.129
.524	.052	.020	-.069	-.102	-.113	-.123	-.128	-.131
.450	.048	.019	-.015	-.112	-.118	-.127	-.132	-.135
.375	.047	.019	.001	-.055	-.112	-.127	-.131	-.132
.300	.044	.017	-.003	-.026	-.083	-.113	-.123	-.126
.225	.045	.019	-.003	-.022	-.056	-.087	-.106	-.115
.150	.044	.018	-.004	-.022	-.046	-.070	-.095	-.110
.075	.045	.019	-.002	-.019	-.040	-.060	-.084	-.104
LEEWARD								
WING								

Table 4. Concluded

(d) Concluded; station 3

THETA, DEG	CP FOR ALPHA, DEG =							
	-4.04	.04	4.03	8.03	11.96	16.05	19.96	24.03
0	-.003	.019	.044	.075	.106	.148	.207	.288
15	-.004	.021	.046	.077	.109	.151	.207	.285
30	-.008	.017	.044	.074	.108	.149	.201	.272
45	-.007	.018	.045	.076	.114	.162	.218	.287
60	-.008	.017	.043	.074	.116	.168	.228	.302
75	-.008	.018	.044	.074	.117	.168	.226	.302
90	-.007	.017	.041	.067	.109	.158	.213	.288
105	-.009	.014	.042	.068	.090	.125	.160	.215
120	-.013	.010	.044	.086	.147	.210	.286	.379
135								
BODY								
150								
165								
180								
195								
210								
225								
240	-.007	.015	.046	.087	.142	.202	.273	.361
255								
270	-.007	.020	.042	.071	.108	.154	.215	.291
285	-.007	.019	.044	.076	.111	.162	.225	.302
300	-.011	.017	.042	.074	.112	.163	.224	.304
315	-.009	.021	.045	.077	.113	.161	.219	.295
330	-.007	.019	.044	.074	.107	.148	.201	.276
345	-.002	.020	.045	.074	.106	.147	.204	.283
Y/S	CP FOR ALPHA, DEG =							
	-4.04	.04	4.03	8.03	11.96	16.05	19.96	24.03
.190								
.274	-.004	.018	.049	.087	.136	.192	.258	.340
.379	-.005	.015	.047	.086	.126	.172	.226	.296
.473								
WINDWARD								
WING								
.569	-.032	.015	.050	.096	.155	.228	.310	.416
.664	-.093	.014	.053	.102	.163	.237	.323	.431
.759	-.080	.013	.056	.106	.168	.238	.325	.429
.806	-.075	.013	.059	.108	.169	.236	.322	.423
.854	-.073	.005	.063	.113	.171	.236	.318	.415
.854	.059	.013	-.070	-.098	-.114	-.126	-.136	-.140
.806	.056	.015	-.068	-.097	-.115	-.127	-.135	-.138
.759	.052	.013	-.076	-.108	-.125	-.133	-.138	-.140
LEEWARD								
WING								
.664	.049	.013	-.083	-.111	-.125	-.135	-.138	-.142
.569	.046	.012	-.033	-.121	-.128	-.136	-.139	-.142
.473	.046	.014	-.002	-.078	-.125	-.139	-.142	-.144
.379	.044	.013	-.008	-.035	-.097	-.124	-.132	-.138
.274	.046	.016	-.007	-.028	-.064	-.099	-.116	-.125
.190	.041	.011	-.011	-.030	-.056	-.084	-.106	-.116

Table 5. Configuration 3

(a) $M_\infty = 1.70$; station 1

THETA, DEG	CP FOR ALPHA, DEG =							
	-4.23	-.12	3.82	7.86	11.81	15.85	19.79	23.92
BODY								
0	-.034	-.027	-.011	.004	.004	.051	.134	.214
15	-.030	-.020	-.005	.014	.020	.042	.116	.193
30	-.037	-.024	-.007	.017	.034	.007	.049	.114
45	-.039	-.022	-.001	.024	.050	.048	-.018	.003
60	-.045	-.023	.002	.033	.070	.089	.104	.124
75	-.046	-.019	.012	.047	.079	.096	.131	.163
90	-.061	-.025	.009	.042	.062	.078	.105	.140
105	-.064	-.024	.009	.009	.004	.001	-.053	-.008
120	-.076	-.033	.014	.070	.127	.194	.272	.333
135								
150	.019	-.019	-.047	-.080	-.123	-.186	-.262	-.296
165	.014	-.023	-.050	-.077	-.101	-.140	-.229	-.264
180	.013	-.021	-.047	-.067	-.095	-.117	-.178	-.208
195	.014	-.022	-.049	-.077	-.097	-.136	-.218	-.243
210	.018	-.022	-.051	-.088	-.145	-.193	-.258	-.266
225								
240	-.075	-.032	.016	.075	.143	.199	.276	.305
255	-.073	-.031	.008	.022	.039	.009	-.043	-.019
270	-.065	-.025	.010	.044	.053	.063	.096	.147
285	-.054	-.024	.005	.041	.076	.083	.131	.175
300	-.049	-.024	-.002	.026	.067	.089	.118	.148
315	-.044	-.024	-.008	.014	.038	.044	-.016	-.005
330	-.038	-.021	-.007	.011	.021	-.005	.044	.107
345	-.033	-.022	-.007	.008	.004	.036	.113	.186
Y/S								
	-4.23	-.12	3.82	7.86	11.81	15.85	19.79	23.92
WINDWARD WING								
.050								
.100								
.150								
.200	-.069	-.027	.021	.078	.145	.204	.271	.314
.250	-.070	-.027	.019	.075	.141	.188	.229	.254
.300	-.073	-.030	.017	.069	.136	.186	.208	.246
.350	-.079	-.030	.019	.074	.139	.176	.181	.185
.400	-.234	-.031	.023	.083	.156	.226	.299	.379
.425	-.206	-.034	.024	.086	.160	.244	.325	.427
.450	-.201	-.040	.023	.087	.159	.250	.328	.436
LEEWARD WING								
.450	.049	-.002	-.152	-.222	-.263	-.279	-.300	-.333
.425	.028	-.022	-.171	-.231	-.267	-.286	-.302	-.337
.400	.028	-.019	-.189	-.242	-.269	-.290	-.304	-.335
.350	.025	-.018	-.050	-.274	-.313	-.326	-.328	-.347
.300	.020	-.021	-.045	-.122	-.316	-.377	-.351	-.351
.250	.018	-.022	-.049	-.090	-.204	-.313	-.311	-.326
.200	.021	-.019	-.048	-.081	-.128	-.180	-.249	-.279
.150								
.100								
.050								

Table 5. Continued

(a) Continued; station 2

THETA, DEG	CP FOR ALPHA, DEG =							
	-4.23	-.12	3.82	7.86	11.81	15.85	19.79	23.92
0	-.051	-.028	.004	.049	.113	.168	.246	.330
15	-.053	-.028	.004	.049	.109	.165	.238	.322
30	-.054	-.025	.009	.051	.107	.162	.237	.312
45	-.056	-.025	.011	.058	.108	.166	.237	.318
60	-.058	-.026	.014	.062	.113	.173	.248	.333
75	-.061	-.027	.013	.064	.109	.168	.240	.324
90	-.062	-.026	.013	.061	.104	.157	.225	.301
105	-.060	-.025	.017	.071	.106	.157	.232	.296
120	-.069	-.033	.014	.072	.123	.176	.245	.339
135								
BODY								
150	.017	-.023	-.052	-.085	-.119	-.171	-.215	-.286
165	.013	-.026	-.055	-.087	-.122	-.165	-.205	-.263
180	.014	-.024	-.051	-.083	-.116	-.153	-.173	-.206
195	.012	-.027	-.055	-.088	-.117	-.158	-.207	-.249
210	.015	-.026	-.055	-.096	-.113	-.162	-.235	-.286
225								
240	-.060	-.024	.022	.074	.123	.185	.251	.335
255	-.061	-.024	.015	.063	.104	.157	.226	.298
270	-.061	-.025	.013	.054	.100	.158	.226	.294
285	-.067	-.031	.008	.054	.103	.161	.234	.314
300	-.061	-.027	.009	.054	.108	.168	.242	.325
315	-.061	-.029	.004	.047	.099	.160	.232	.312
330	-.059	-.029	.003	.044	.099	.156	.234	.305
345	-.052	-.025	.006	.050	.112	.167	.251	.323
Y/S	CP FOR ALPHA, DEG =							
	-4.23	-.12	3.82	7.86	11.81	15.85	19.79	23.92
.075								
.150								
.225	-.061	-.024	.019	.072	.120	.184	.253	.339
.300	-.061	-.025	.019	.072	.119	.183	.249	.331
WINDWARD								
WING								
.375	-.058	-.024	.019	.074	.118	.159	.209	.268
.450								
.524	-.134	-.029	.020	.076	.145	.230	.315	.413
.599								
.637	-.179	-.033	.027	.080	.149	.227	.317	.417
.674	-.176	-.037	.031	.084	.150	.223	.309	.404
.674	.044	-.016	-.145	-.232	-.288	-.336	-.342	-.372
.637	.036	-.020	-.152	-.238	-.292	-.349	-.345	-.374
.599	.033	-.018	-.185	-.240	-.288	-.337	-.345	-.375
.524	.024	-.023	-.123	-.320	-.324	-.343	-.364	-.388
LEEWARD								
WING								
.450	.025	-.019	-.036	-.191	-.347	-.391	-.401	-.401
.375	.023	-.019	-.046	-.096	-.231	-.330	-.381	-.402
.300	.018	-.024	-.054	-.090	-.155	-.247	-.314	-.358
.225	.021	-.021	-.050	-.084	-.122	-.183	-.227	-.286
.150								
.075								

Table 5. Continued

(a) Concluded; station 3

THETA, DEG	CP FOR ALPHA, DEG =							
	-4.23	-.12	3.82	7.86	11.81	15.85	19.79	23.92
			.011	.055	.112	.179	.274	.374
0	-.049	-.023	.015	.058	.116	.186	.277	.371
15	-.049	-.020	.012	-.334	.114	.187	.269	.350
30	-.055	-.024	.010	.057	.117	.190	.270	.346
45	-.058	-.027	.011	.058	.120	.192	.271	.347
60	-.059	-.027	.013	.062	.120	.191	.266	.338
75	-.057	-.023	.008	.049	.105	.162	.231	.293
90	-.062	-.027	.014	.059	.107	.179	.248	.309
105	-.062	-.028	-.017	.026	.077	.148	.217	.281
120	-.085	-.055						
135								
BODY			-.046	-.080	-.112	-.166	-.202	-.243
150	.030	-.013	-.049	-.083	-.116	-.162	-.182	-.223
165	.028	-.014	-.047	-.081	-.114	-.164	-.195	-.237
180	.029	-.012	-.046	-.079	-.107	-.160	-.190	-.246
195	.029	-.012	-.056	-.087	-.109	-.167	-.201	-.257
210	.021	-.020						
225			.015	.065	.125	.192	.272	.364
240	-.059	-.026	.051	.103	.169	.221	.289	.357
255	-.047	.014	.007	.049	.107	.168	.244	.323
270	-.063	-.029	.012	.061	.120	.185	.267	.357
285	-.060	-.025	.008	.056	.118	.183	.266	.356
300	-.062	-.029	.016	.063	.127	.191	.272	.363
315	-.054	-.020	.009	.056	.115	.182	.264	.354
330	-.056	-.023	.009	.055	.111	.179	.269	.365
345	-.051	-.023						
Y/S	CP FOR ALPHA, DEG =							
	-4.23	-.12	3.82	7.86	11.81	15.85	19.79	23.92
			.015	.065	.119	.167	.236	.318
.190			.014	.069	.132	.191	.268	.359
.274	-.056	-.025	.016	.076	.141	.220	.312	.414
.379	-.056	-.026	.020	.076	.141	.224	.315	.419
.473	-.050	-.025	.026	.076	.143	.220	.310	.407
.569	-.167	-.027	.030	.078	.142	.215	.301	.395
.664	-.189	-.026	.033	.081	.141	.211	.289	.379
.759	-.168	-.030						
.806	-.164							
.854								
			-.147	-.233	-.295	-.340	-.355	-.376
.854	.044	-.019	-.189	-.233	-.289	-.334	-.382	-.383
.806	.040	-.016	-.145	-.232	-.295	-.344	-.361	-.374
.759	.045	-.013	-.126	-.315	-.305	-.334	-.385	-.414
.664	.035	-.015	-.035	-.206	-.353	-.387	-.415	-.441
.569	.033	-.016	-.049	-.102	-.241	-.337	-.399	-.412
.473	.027	-.020	-.051	-.086	-.157	-.253	-.329	-.355
.379	.027	-.019	-.050	-.085	-.126	-.193	-.256	-.292
.274	.026	-.018	-.050	-.083	-.113	-.166	-.199	-.233
.190	.025	-.017						

Table 5. Continued

(b) $M_\infty = 2.16$; station 1

THETA, DEG	CP FOR ALPHA, DEG =							
	-4.17	-.11	3.88	7.89	11.88	15.88	19.85	23.82
0	-.017	-.008	-.004	.006	.044	.095	.164	.244
15	-.017	-.007	.000	.006	.037	.085	.149	.224
30	-.020	-.006	.005	.009	.012	.047	.099	.162
45	-.025	-.005	.012	.030	.011	-.009	.027	.074
60	-.032	-.007	.017	.048	.047	.027	.018	.036
75	-.036	-.004	.027	.059	.059	.072	.097	.142
90	-.040	-.003	.030	.053	.067	.069	.091	.140
105	-.045	-.005	.030	.024	.044	.025	.019	.053
120	-.053	-.010	.040	.099	.119	.169	.211	.249
135								
BODY								
150	.025	-.002	-.026	-.051	-.099	-.162	-.181	-.188
165	.023	-.004	-.027	-.047	-.056	-.123	-.153	-.165
180	.023	-.004	-.025	-.039	-.048	-.092	-.124	-.134
195	.024	-.003	-.025	-.048	-.052	-.119	-.152	-.156
210	.024	-.004	-.028	-.058	-.110	-.157	-.170	-.185
225								
240	-.061	-.013	.034	.096	.134	.173	.206	.259
255	-.061	-.011	.026	.035	.037	.016	.041	.063
270	-.051	-.009	.023	.046	.054	.056	.092	.145
285	-.042	-.011	.018	.048	.049	.060	.094	.150
300	-.035	-.011	.010	.034	.037	.015	.027	.054
315	-.027	-.009	.005	.010	-.017	-.017	.024	.070
330	-.023	-.008	-.001	-.007	.002	.040	.095	.159
345	-.018	-.007	-.003	.001	.033	.081	.146	.222
Y/S	CP FOR ALPHA, DEG =							
	-4.17	-.11	3.88	7.89	11.88	15.88	19.85	23.82
.050								
.100								
.150								
.200	-.057	-.008	.037	.097	.136	.176	.211	.261
WINDWARD								
WING	.250	-.059	-.012	.035	.092	.127	.157	.188
.300	-.057	-.012	.034	.088	.123	.145	.170	.204
.350	-.075	-.012	.035	.090	.122	.132	.141	.168
.400	-.168	-.013	.037	.096	.158	.221	.296	.379
.425	-.156	-.012	.041	.104	.172	.248	.335	.430
.450	-.149	-.027	.043	.105	.175	.255	.342	.437
.450	.053	.004	-.112	-.154	-.174	-.183	-.202	-.219
.425	.035	-.003	-.120	-.162	-.185	-.183	-.204	-.217
.400	.031	-.004	-.138	-.170	-.192	-.189	-.211	-.219
.350	.028	-.004	-.060	-.197	-.196	-.203	-.214	-.224
LEEWARD	.300	.025	-.004	-.023	-.131	-.207	-.220	-.215
WING	.250	.027	-.002	-.025	-.059	-.175	-.190	-.194
.200	.026	-.003	-.026	-.051	-.101	-.152	-.170	-.180
.150								
.100								
.050								

Table 5. Continued

(b) Continued; station 2

THETA, DEG	CP FOR ALPHA, DEG =							
	-4.17	-.11	3.88	7.89	11.88	15.88	19.85	23.82
0	-.029	-.007	.021	.057	.093	.135	.190	.262
15	-.032	-.008	.021	.055	.092	.133	.184	.252
30	-.036	-.008	.020	.055	.093	.133	.178	.239
45	-.038	-.008	.020	.061	.100	.145	.196	.255
60	-.041	-.012	.018	.058	.101	.149	.209	.277
75	-.044	-.013	.019	.058	.098	.146	.206	.276
90	-.048	-.016	.013	.038	.084	.130	.185	.251
105	-.047	-.013	.020	.069	.096	.149	.195	.246
120	-.046	-.012	.026	.077	.125	.173	.235	.321
135								
BODY 150	.027	-.006	-.032	-.056	-.082	-.118	-.179	-.198
165	.027	-.005	-.030	-.051	-.077	-.110	-.146	-.184
180	.025	-.007	-.030	-.055	-.076	-.103	-.111	-.163
195	.026	-.006	-.029	-.055	-.074	-.112	-.141	-.183
210	.025	-.007	-.033	-.064	-.075	-.123	-.172	-.196
225								
240	-.042	-.009	.027	.073	.126	.187	.251	.332
255	-.043	-.010	.022	.068	.097	.143	.192	.264
270	-.044	-.010	.021	.037	.086	.132	.192	.260
285	-.042	-.010	.022	.058	.100	.147	.208	.285
300	-.040	-.010	.020	.058	.104	.152	.209	.289
315	-.037	-.009	.021	.057	.103	.149	.198	.270
330	-.036	-.009	.020	.052	.094	.136	.181	.249
345	-.032	-.008	.021	.055	.091	.134	.185	.257
Y/S	CP FOR ALPHA, DEG =							
	-4.17	-.11	3.88	7.89	11.88	15.88	19.85	23.82
.075								
.150								
.225	-.041	-.008	.028	.074	.126	.190	.256	.342
.300	-.042	-.010	.025	.072	.123	.183	.246	.326
WINDWARD WING .375	-.040	-.009	.027	.074	.113	.156	.196	.261
.450								
.524	-.138	-.008	.032	.081	.149	.226	.311	.409
.599								
.637	-.135	-.011	.038	.089	.157	.230	.310	.407
.674	-.126	-.015	.041	.094	.160	.229	.305	.396
.674	.046	-.004	-.112	-.158	-.189	-.209	-.232	-.236
.637	.045	-.003	-.116	-.171	-.203	-.211	-.231	-.236
.599	.042	-.003	-.132	-.170	-.202	-.215	-.230	-.235
.524	.038	-.003	-.117	-.187	-.201	-.224	-.232	-.236
LEEWARD WING .450	.031	-.005	-.024	-.176	-.223	-.237	-.243	-.244
.375	.029	-.005	-.029	-.082	-.187	-.229	-.246	-.241
.300	.028	-.006	-.031	-.059	-.121	-.178	-.218	-.218
.225	.029	-.006	-.032	-.056	-.087	-.125	-.174	-.189
.150								
.075								

Table 5. Continued

(b) Concluded; station 3

THETA, DEG	CP FOR ALPHA, DEG =							
	-4.17	-.11	3.88	7.89	11.88	15.88	19.85	23.82
0	-.032	-.009	.021	.061	.113	.173	.240	.331
15	-.034	-.008	.022	.065	.114	.174	.242	.334
30	-.040	-.013	.020	.063	.112	.168	.237	.331
45	-.040	-.012	.022	.065	.115	.173	.246	.334
60	-.041	-.013	.022	.064	.115	.175	.248	.335
75	-.040	-.011	.023	.063	.113	.173	.245	.330
90	-.041	-.012	-.142	.051	.089	.142	.209	.288
105	-.041	-.012	.029	.074	.121	.180	.250	.327
120	-.052	-.024	.016	.059	.110	.175	.246	.325
135								
BODY								
150	.031	-.004	-.031	-.051	-.080	-.116	-.139	-.169
165	.032	-.004	-.030	-.051	-.079	-.105	-.131	-.161
180	.031	-.005	-.030	-.052	-.080	-.114	-.139	-.168
195	.031	-.003	-.028	-.049	-.076	-.108	-.147	-.171
210	.029	-.003	-.030	-.051	-.074	-.110	-.152	-.180
225								
240	-.037	-.008	.029	.075	.130	.190	.260	.344
255	-.015	.009	.044	.086	.164	.240	.291	.371
270	-.036	-.006	.024	.054	.092	.144	.209	.295
285	-.038	-.007	.025	.067	.114	.172	.243	.329
300	-.039	-.009	.022	.065	.116	.171	.245	.331
315	-.037	-.006	.024	.066	.119	.174	.246	.334
330	-.036	-.007	.023	.062	.116	.168	.237	.328
345	-.031	-.006	.024	.063	.115	.170	.240	.330
Y/S								
	-4.17	-.11	3.88	7.89	11.88	15.88	19.85	23.82
.190								
.274								
.379	-.036	-.008	.030	.075	.119	.169	.232	.307
.473	-.032	-.007	.034	.080	.131	.191	.265	.345
WINDWARD	-.039	-.008	.035	.082	.140	.213	.297	.392
WING	-.159	-.007	.037	.086	.144	.218	.299	.397
.664	-.131	-.010	.037	.088	.145	.216	.294	.389
.759	-.128	-.012	.039	.090	.145	.217	.290	.384
.806	-.118	-.014	.044	.094	.146	.213	.283	.377
.854								
.854	.049	-.004	-.105	-.152	-.186	-.206	-.223	-.235
.806	.046	-.002	-.127	-.167	-.201	-.230	-.228	-.236
.759	.047	-.003	-.111	-.169	-.205	-.221	-.227	-.236
LEEWARD	.040	-.003	-.127	-.183	-.204	-.227	-.247	-.246
WING	.035	-.005	-.021	-.192	-.227	-.236	-.256	-.256
.569	.034	-.005	-.027	-.089	-.195	-.235	-.246	-.244
.473	.031	-.006	-.031	-.058	-.131	-.194	-.212	-.217
.379	.031	-.005	-.031	-.053	-.091	-.144	-.168	-.188
.274	.030	-.006	-.032	-.052	-.078	-.111	-.131	-.161
.190								

Table 5. Continued

(c) $M_\infty = 2.40$; station 1

THETA, DEG	CP FOR ALPHA, DEG =							
	-4.20	-.23	3.92	7.84	11.92	15.91	19.85	23.78
0	-.014	-.007	-.003	.011	.053	.108	.178	.256
15	-.015	-.005	.001	.009	.047	.099	.166	.237
30	-.018	-.005	.006	.002	.024	.065	.121	.178
45	-.022	-.005	.015	.017	-.007	.013	.054	.094
60	-.030	-.006	.022	.042	.030	.000	.007	.030
75	-.034	-.004	.033	.054	.062	.070	.099	.136
90	-.039	-.003	.036	.044	.064	.071	.103	.132
105	-.043	-.003	.030	.017	.051	.037	.055	.059
120	-.052	-.008	.046	.094	.119	.156	.188	.226
135								
BODY 150	.024	-.002	-.025	-.049	-.103	-.156	-.162	-.179
165	.022	-.004	-.025	-.045	-.056	-.122	-.145	-.162
180	.021	-.004	-.023	-.036	-.047	-.092	-.119	-.132
195	.023	-.002	-.022	-.043	-.052	-.115	-.140	-.149
210	.023	-.003	-.026	-.053	-.113	-.143	-.161	-.171
225								
240	-.058	-.014	.039	.095	.128	.157	.193	.238
255	-.057	-.011	.027	.028	.032	.030	.043	.051
270	-.050	-.011	.025	.039	.052	.063	.092	.126
285	-.039	-.010	.020	.043	.044	.057	.087	.128
300	-.033	-.011	.010	.027	.007	-.014	-.001	.027
315	-.025	-.009	.002	-.005	-.020	.004	.040	.083
330	-.020	-.008	-.004	-.008	.016	.057	.109	.170
345	-.016	-.007	-.004	.005	.043	.095	.158	.232
Y/S	CP FOR ALPHA, DEG =							
	-4.20	-.23	3.92	7.84	11.92	15.91	19.85	23.78
.050								
.100								
.150								
.200	-.055	-.008	.041	.097	.128	.156	.196	.243
WINDWARD .250	-.056	-.011	.040	.092	.120	.143	.173	.211
WING .300	-.056	-.013	.039	.088	.110	.122	.149	.172
.350	-.080	-.013	.041	.089	.109	.121	.139	.177
.400	-.147	-.014	.043	.097	.160	.223	.293	.379
.425	-.139	-.021	.048	.104	.178	.249	.330	.419
.450	-.130	-.038	.052	.107	.184	.256	.335	.422
.450	.047	-.006	-.113	-.138	-.154	-.166	-.183	-.197
.425	.033	-.004	-.115	-.142	-.158	-.164	-.182	-.195
.400	.030	-.003	-.128	-.149	-.170	-.168	-.184	-.197
.350	.026	-.004	-.116	-.164	-.174	-.174	-.187	-.200
LEEWARD .300	.023	-.006	-.023	-.144	-.180	-.182	-.188	-.201
WING .250	.025	-.004	-.023	-.068	-.168	-.164	-.173	-.189
.200	.025	-.004	-.025	-.050	-.098	-.146	-.154	-.177
.150								
.100								
.050								

Table 5. Continued

(c) Continued; station 2

THETA, DEG	CP FOR ALPHA, DEG =							
	-4.20	-.23	3.92	7.84	11.92	15.91	19.85	23.78
0	-.024	-.005	.023	.052	.083	.116	.174	.254
15	-.025	-.004	.026	.053	.084	.118	.176	.245
30	-.029	-.005	.026	.056	.086	.117	.175	.234
45	-.030	-.005	.028	.059	.096	.133	.194	.256
60	-.034	-.008	.026	.059	.099	.144	.211	.283
75	-.035	-.008	.029	.061	.099	.146	.211	.283
90	-.039	-.011	.021	.043	.087	.134	.193	.259
105	-.038	-.010	.035	.073	.103	.147	.195	.253
120	-.037	-.009	.041	.082	.131	.181	.256	.327
135								
BODY								
150	.027	-.001	-.027	-.050	-.081	-.123	-.170	-.184
165	.028	.002	-.023	-.044	-.074	-.111	-.149	-.172
180	.026	-.002	-.027	-.047	-.074	-.098	-.126	-.158
195	.027	-.001	-.026	-.048	-.073	-.114	-.144	-.169
210	.026	-.002	-.029	-.056	-.076	-.135	-.161	-.176
225								
240	-.038	-.007	.037	.078	.132	.188	.261	.336
255	-.039	-.007	.030	.071	.098	.140	.196	.267
270	-.040	-.008	.025	.035	.083	.131	.188	.262
285	-.038	-.007	.028	.057	.096	.141	.206	.282
300	-.037	-.008	.026	.057	.098	.143	.210	.285
315	-.034	-.007	.025	.057	.095	.134	.194	.262
330	-.031	-.007	.023	.053	.084	.118	.167	.238
345	-.026	-.006	.023	.052	.082	.116	.165	.245
Y/S	CP FOR ALPHA, DEG =							
	-4.20	-.23	3.92	7.84	11.92	15.91	19.85	23.78
.075								
.150								
.225	-.036	-.005	.038	.079	.133	.190	.267	.344
.300	-.038	-.008	.034	.076	.128	.183	.254	.330
WINDWARD								
WING								
.375	-.036	-.007	.036	.077	.115	.153	.204	.264
.450								
.524	-.136	-.008	.040	.087	.152	.231	.322	.419
.599								
.637	-.124	-.014	.045	.093	.160	.237	.321	.414
.674	-.116	-.026	.049	.098	.164	.236	.316	.407
.674	.044	.000	-.108	-.140	-.165	-.186	-.200	-.206
.637	.042	.002	-.110	-.148	-.176	-.185	-.199	-.205
.599	.039	.003	-.114	-.152	-.181	-.185	-.198	-.204
.524	.036	.003	-.132	-.159	-.177	-.191	-.198	-.205
LEEWARD								
WING								
.450	.032	.000	-.040	-.172	-.188	-.201	-.204	-.210
.375	.031	.001	-.022	-.090	-.175	-.196	-.206	-.208
.300	.030	.000	-.025	-.056	-.125	-.159	-.189	-.194
.225	.029	.000	-.026	-.051	-.088	-.115	-.163	-.179
.150								
.075								

Table 5. Continued

(d) $M_\infty = 2.86$; station 1

THETA, DEG	CP FOR ALPHA, DEG =							
	-4.12	-.19	3.88	7.89	11.87	15.88	19.87	23.79
0	-.002	-.003	.001	.021	.058	.108	.174	.247
15	-.003	.000	.003	.019	.053	.100	.163	.232
30	-.007	.000	.004	.008	.033	.071	.122	.180
45	-.011	.001	.010	.001	.003	.028	.065	.107
60	-.020	-.002	.016	.026	.000	-.006	.008	.030
75	-.024	.000	.026	.042	.046	.053	.076	.106
90	-.030	.000	.028	.038	.048	.059	.081	.114
105	-.033	.001	.028	.016	.034	.033	.045	.075
120	-.037	-.005	.039	.079	.102	.127	.155	.198
135								
BODY								
150	.026	.001	-.019	-.041	-.094	-.120	-.125	-.135
165	.024	-.001	-.020	-.038	-.047	-.099	-.113	-.123
180	.024	-.001	-.019	-.031	-.040	-.076	-.098	-.102
195	.026	.001	-.018	-.036	-.046	-.093	-.108	-.115
210	.026	.000	-.022	-.043	-.099	-.117	-.125	-.133
225								
240	-.048	-.010	.031	.081	.109	.138	.170	.215
255	-.044	-.006	.024	.017	.022	.026	.045	.067
270	-.036	-.006	.022	.031	.041	.053	.079	.114
285	-.028	-.005	.016	.031	.032	.042	.068	.107
300	-.022	-.006	.006	.010	-.015	-.014	.002	.028
315	-.014	-.003	.002	-.010	-.003	.022	.057	.098
330	-.009	-.003	-.002	.004	.028	.065	.115	.173
345	-.004	-.002	.000	.017	.049	.096	.158	.227
Y/S	CP FOR ALPHA, DEG =							
	-4.12	-.19	3.88	7.89	11.87	15.88	19.87	23.79
.050								
.100								
.150								
WINDWARD								
WING								
.200	-.047	-.005	.034	.082	.108	.138	.170	.219
.250	-.045	-.007	.033	.079	.103	.126	.153	.196
.300	-.043	-.008	.032	.075	.088	.100	.125	.154
.350	-.075	-.007	.034	.078	.098	.122	.151	.193
.400	-.107	-.018	.034	.088	.141	.206	.273	.358
.425	-.100	-.028	.040	.097	.156	.228	.302	.392
.450	-.096	-.029	.042	.102	.161	.233	.306	.395
.450	.044	-.003	-.084	-.107	-.117	-.127	-.137	-.146
.425	.036	-.002	-.083	-.108	-.116	-.125	-.135	-.142
.400	.031	-.003	-.090	-.113	-.122	-.127	-.137	-.144
.350	.026	-.002	-.077	-.118	-.128	-.130	-.139	-.146
LEEWARD								
WING								
.300	.024	-.001	-.018	-.120	-.133	-.132	-.138	-.144
.250	.025	.001	-.018	-.064	-.126	-.122	-.129	-.136
.200	.026	.001	-.018	-.042	-.091	-.119	-.121	-.134
.150								
.100								
.050								

Table 5. Continued

(d) Continued; station 2

THETA, DEG	CP FOR ALPHA, DEG =								
	-4.12	-.19	3.88	7.89	11.87	15.88	19.87	23.79	
	0	-.009	.003	.018	.039	.062	.108	.175	.246
	15	-.011	.004	.020	.042	.066	.101	.162	.227
	30	-.014	.003	.022	.045	.070	.093	.132	.183
	45	-.016	.003	.024	.051	.080	.109	.155	.206
	60	-.021	-.002	.023	.053	.086	.127	.181	.242
	75	-.023	-.001	.024	.055	.088	.130	.184	.245
	90	-.027	-.005	.020	.045	.080	.119	.170	.229
	105	-.029	-.005	.029	.065	.095	.131	.172	.221
	120	-.029	-.004	.034	.076	.120	.160	.212	.289
	135								
BODY	150	.026	-.001	-.024	-.044	-.067	-.111	-.131	-.142
	165	.029	.001	-.021	-.039	-.064	-.090	-.118	-.133
	180	.024	-.002	-.024	-.040	-.066	-.078	-.106	-.125
	195	.025	-.002	-.025	-.043	-.065	-.094	-.119	-.135
	210	.025	-.001	-.025	-.047	-.065	-.114	-.129	-.139
	225								
	240	-.025	-.002	.032	.075	.123	.175	.233	.305
	255	-.026	-.003	.027	.066	.091	.129	.174	.236
	270	-.029	-.006	.021	.040	.074	.117	.167	.236
	285	-.026	-.005	.021	.051	.084	.125	.180	.247
	300	-.024	-.003	.021	.051	.085	.125	.182	.248
	315	-.020	-.002	.020	.047	.076	.109	.157	.211
	330	-.017	-.001	.018	.041	.062	.089	.129	.182
	345	-.012	.003	.019	.039	.058	.099	.159	.226
Y/S	CP FOR ALPHA, DEG =								
	-4.12	-.19	3.88	7.89	11.87	15.88	19.87	23.79	
	.075								
	.150								
	.225	-.024	-.001	.033	.077	.124	.177	.238	.311
	.300	-.025	-.003	.030	.074	.119	.170	.227	.299
	.375	-.022	-.002	.032	.075	.109	.142	.181	.232
WINDWARD WING	.450								
	.524	-.105	-.004	.035	.085	.143	.216	.298	.398
	.599								
	.637	-.095	-.019	.040	.091	.150	.219	.301	.397
	.674	-.092	-.023	.046	.098	.156	.222	.301	.393
	.674	.046	-.002	-.086	-.112	-.127	-.143	-.149	-.153
	.637	.044	.002	-.085	-.112	-.128	-.141	-.148	-.152
	.599	.042	.004	-.086	-.117	-.137	-.140	-.147	-.151
	.524	.036	.003	-.092	-.123	-.139	-.142	-.149	-.153
LEEWARD WING	.450	.033	.002	-.029	-.132	-.141	-.146	-.152	-.156
	.375	.031	.002	-.019	-.084	-.139	-.145	-.150	-.153
	.300	.027	.000	-.025	-.051	-.108	-.130	-.143	-.148
	.225	.029	.002	-.023	-.044	-.071	-.100	-.127	-.137
	.150								
	.075								

Table 5. Concluded

(d) Concluded; station 3

THETA, DEG	CP FOR ALPHA, DEG =							
	-4.12	-.19	3.88	7.89	11.87	15.88	19.87	23.79
0	-.014	.007	.035	.070	.104	.152	.219	.298
15	-.013	.009	.037	.073	.108	.154	.221	.297
30	-.018	.006	.035	.070	.107	.153	.217	.289
45	-.016	.008	.037	.071	.113	.165	.233	.307
60	-.018	.005	.035	.068	.111	.166	.237	.314
75	-.017	.006	.034	.066	.110	.164	.232	.310
90	-.016	.007	.033	.054	.086	.139	.200	.270
105	-.016	.005	.039	.078	.128	.181	.246	.321
120	-.022	-.003	.031	.072	.125	.185	.257	.333
135								
BODY								
150	.032	.003	-.021	-.040	-.067	-.095	-.116	-.131
165	.030	.002	-.021	-.039	-.064	-.084	-.110	-.121
180	.032	.004	-.020	-.039	-.065	-.092	-.115	-.124
195	.033	.004	-.019	-.038	-.060	-.087	-.113	-.123
210	.034	.005	-.018	-.040	-.062	-.094	-.120	-.130
225								
240	-.016	.004	.035	.075	.124	.182	.251	.331
255	.022	.037	.049	.067	.115	.137	.195	.263
270	-.013	.009	.033	.055	.086	.134	.198	.269
285	-.014	.010	.034	.067	.105	.159	.228	.304
300	-.020	.005	.033	.067	.107	.162	.231	.310
315	-.017	.009	.037	.071	.112	.165	.231	.310
330	-.016	.008	.035	.070	.106	.155	.216	.293
345	-.011	.010	.037	.071	.105	.154	.218	.296
Y/S	CP FOR ALPHA, DEG =							
	-4.12	-.19	3.88	7.89	11.87	15.88	19.87	23.79
.190								
.274								
.379	-.016	.003	.034	.075	.117	.166	.224	.293
.473	-.008	.006	.036	.080	.131	.193	.263	.348
WINDWARD								
WING	.569	-.019	.002	.038	.084	.143	.217	.298
.664	-.099	.000	.040	.089	.148	.221	.304	.403
.759	-.087	-.001	.043	.093	.152	.222	.306	.400
.806	-.082	-.004	.044	.094	.153	.222	.303	.394
.854	-.080	-.022	.049	.099	.153	.219	.297	.384
.854	.052	.007	-.077	-.105	-.121	-.136	-.147	-.150
.806	.046	.010	-.081	-.113	-.133	-.136	-.145	-.149
.759	.048	.009	-.080	-.109	-.124	-.138	-.147	-.151
LEEWARD								
WING	.664	.040	.006	-.090	-.120	-.136	-.148	-.153
.569	.037	.005	-.040	-.131	-.139	-.149	-.151	-.153
.473	.036	.005	-.014	-.098	-.140	-.151	-.153	-.156
.379	.033	.004	-.020	-.048	-.113	-.132	-.141	-.149
.274	.036	.007	-.017	-.039	-.077	-.104	-.120	-.134
.190	.031	.003	-.021	-.039	-.064	-.090	-.111	-.128

Table 6. Configuration 4

(a) $M_\infty = 1.70$; station 1

THETA, DEG	CP FOR ALPHA, DEG =							
	-3.62	.39	4.46	8.44	12.44	16.43	20.34	24.39
0	-.029	-.004	.031	.075	.129	.206	.297	.407
15	-.029	-.004	.031	.077	.131	.206	.296	.405
30	-.029	-.004	.034	.080	.133	.209	.300	.412
45								
60	.037	-.009	-.052	-.116	-.224	-.301	-.375	-.421
75	.030	-.008	-.050	-.128	-.245	-.307	-.383	-.427
90	.032	-.002	-.043	-.095	-.151	-.251	-.333	-.389
105	.024	-.003	-.035	-.069	-.095	-.150	-.218	-.250
120	.019	-.003	-.027	-.057	-.083	-.139	-.166	-.189
135	.014	-.005	-.024	-.056	-.099	-.134	-.138	-.175
150	.015	-.002	-.017	-.057	-.149	-.204	-.131	-.168
165	.014	-.002	-.014	-.039	-.066	-.093	-.153	-.160
180	.009	-.004	-.015	-.020	-.036	-.061	-.138	-.135
195	.016	.001	-.011	-.031	-.057	-.085	-.154	-.152
210	.016	.000	-.016	-.055	-.148	-.215	-.131	-.157
225	.020	.000	-.019	-.050	-.094	-.144	-.132	-.158
240	.025	.000	-.024	-.053	-.079	-.165	-.146	-.170
255	.035	.003	-.026	-.057	-.082	-.133	-.174	-.211
270	.032	-.001	-.038	-.078	-.121	-.195	-.270	-.333
285	.033	.000	-.038	-.097	-.206	-.291	-.373	-.420
300	.037	-.010	-.053	-.106	-.180	-.274	-.370	-.419
315								
330	-.026	.001	.035	.080	.134	.209	.300	.405
345	-.035	-.009	.025	.069	.121	.197	.288	.395

Y/S	CP FOR ALPHA, DEG =							
	-3.62	.39	4.46	8.44	12.44	16.43	20.34	24.39
.050								
.100								
.150								
.200	-.027	.001	.037	.081	.136	.212	.302	.408
.250	-.029	.000	.036	.079	.136	.210	.299	.405
.300	-.027	.001	.037	.080	.138	.209	.295	.400
.350	-.029	.003	.043	.085	.142	.211	.294	.397
.400	-.168	.007	.050	.093	.145	.210	.288	.388
.425	-.151	.005	.049	.090	.138	.199	.273	.371
.450	-.134	.022	.068	.107	.147	.206	.274	.372
.450	.045	-.017	-.180	-.287	-.386	-.394	-.428	-.446
.425	.045	-.013	-.184	-.289	-.386	-.398	-.433	-.452
.400	.044	-.009	-.211	-.300	-.386	-.411	-.436	-.447
.350	.039	-.008	-.054	-.209	-.304	-.292	-.345	-.373
.300	.039	-.007	-.050	-.112	-.155	-.223	-.330	-.400
.250	.040	-.005	-.049	-.108	-.208	-.289	-.374	-.422
.200	.041	-.003	-.048	-.109	-.191	-.274	-.367	-.413
.150								
.100								
.050								

Table 6. Continued

(a) Continued; station 2

	THETA, DEG	CP FOR ALPHA, DEG =							
		-3.62	.39	4.46	8.44	12.44	16.43	20.34	24.39
BODY	0	-.036	-.002	.040	.090	.159	.226	.321	.428
	15	-.039	-.005	.037	.089	.154	.223	.316	.424
	30	-.039	-.004	.039	.092	.155	.225	.313	.425
	45								
	60	.040	.001	-.029	-.064	-.139	-.228	-.341	-.373
	75	.033	-.002	-.031	-.069	-.142	-.238	-.354	-.392
	90	.033	-.001	-.032	-.080	-.171	-.275	-.351	-.386
	105	.029	-.006	-.038	-.079	-.152	-.233	-.351	-.404
	120	.031	-.002	-.032	-.064	-.108	-.159	-.235	-.331
	135	.027	-.002	-.032	-.069	-.109	-.144	-.189	-.283
	150	.025	-.003	-.031	-.080	-.141	-.161	-.176	-.255
	165	.028	.002	-.023	-.045	-.075	-.124	-.146	-.187
	180	.024	-.002	-.024	-.040	-.057	-.103	-.124	-.149
	195	.024	-.002	-.026	-.051	-.079	-.121	-.139	-.183
	210	.029	.001	-.025	-.077	-.122	-.142	-.154	-.224
	225	.030	-.001	-.028	-.064	-.090	-.126	-.165	-.251
	240	.033	.000	-.029	-.059	-.092	-.136	-.201	-.296
	255	.029	-.005	-.034	-.068	-.130	-.198	-.314	-.382
	270	.029	-.006	-.036	-.073	-.156	-.274	-.336	-.382
	285	.032	-.006	-.034	-.070	-.135	-.216	-.332	-.384
300	.030	-.013	-.043	-.077	-.140	-.219	-.326	-.376	
315									
330	-.037	-.002	.041	.092	.156	.228	.317	.427	
345	-.041	-.006	.036	.086	.153	.222	.314	.422	
	Y/S	CP FOR ALPHA, DEG =							
		-3.62	.39	4.46	8.44	12.44	16.43	20.34	24.39
WINDWARD WING	.075								
	.150								
	.225	-.037	-.001	.042	.093	.156	.230	.317	.428
	.300	-.040	-.005	.039	.093	.154	.227	.314	.423
	.375	-.031	.002	.047	.101	.161	.233	.321	.426
	.450	-.024	.003	.051	.103	.164	.236	.320	.422
	.524	-.099	-.001	.051	.100	.161	.233	.312	.414
	.599	-.183	.003	.061	.108	.165	.233	.309	.406
	.637	-.144	.001	.064	.113	.167	.230	.304	.398
	.674	-.136	.003	.067	.118	.164	.219	.289	.378
	LEEWARD WING	.674	.053	-.011	-.144	-.237	-.319	-.379	-.394
.637		.048	-.007	-.147	-.240	-.314	-.375	-.398	-.405
.599									
.524		.039	-.004	-.092	-.302	-.360	-.401	-.400	-.376
.450									
.375		.038	-.001	-.026	-.066	-.144	-.195	-.286	-.335
.300		.037	-.002	-.030	-.062	-.135	-.237	-.366	-.395
.225		.037	-.001	-.031	-.067	-.141	-.232	-.346	-.379
.150									
.075									

Table 6. Continued
(a) Concluded; station 3

THETA, DEG	CP FOR ALPHA, DEG =							
	-3.62	.39	4.46	8.44	12.44	16.43	20.34	24.39
0	-.033	.000	.042	.095	.158	.233	.324	.432
15	-.033	.000	.042	.092	.157	.232	.323	.429
30	-.045	-.010	.032	.079	.141	.218	.305	.407
45								
60	.039	.000	-.032	-.067	-.112	-.187	-.270	-.341
75								
90	.029	-.005	-.038	-.084	-.145	-.222	-.295	-.366
105	.034	-.001	-.033	-.079	-.158	-.250	-.313	-.365
120	.030	-.005	-.037	-.082	-.161	-.250	-.332	-.376
135	.040	.005	-.026	-.080	-.163	-.222	-.267	-.377
BODY 150	.034	-.002	-.032	-.080	-.148	-.201	-.233	-.324
165	.031	-.001	-.031	-.052	-.078	-.135	-.164	-.189
180	.030	.000	-.028	-.046	-.060	-.098	-.100	-.106
195	.036	.004	-.024	-.047	-.075	-.121	-.133	-.159
210	.032	-.003	-.032	-.084	-.134	-.182	-.206	-.291
225	.030	-.006	-.034	-.078	-.129	-.205	-.246	-.360
240	.031	-.004	-.033	-.070	-.128	-.218	-.297	-.385
255	.034	.000	-.031	-.069	-.134	-.232	-.331	-.364
270	.026	-.008	-.039	-.078	-.142	-.207	-.310	-.362
285	.031	-.008	-.038	-.075	-.124	-.199	-.308	-.361
300	.002	-.035	-.062	-.094	-.136	-.196	-.294	-.344
315								
330	-.035	-.001	.041	.095	.162	.235	.323	.432
345	-.036	-.003	.039	.090	.154	.228	.322	.430
Y/S	CP FOR ALPHA, DEG =							
	-3.62	.39	4.46	8.44	12.44	16.43	20.34	24.39
.190	-.041	-.006	.036	.089	.158	.228	.315	.425
.274	-.042	-.006	.038	-.380	.159	.231	.318	.429
.379	-.042	-.007	.037	.093	.157	.230	.317	.426
.473	-.039	-.006	.038	.095	.157	.231	.319	.426
WINDWARD .569	-.023	.000	.046	.106	.165	.238	.326	.427
WING .664	-.109	-.001	.048	.105	.164	.237	.321	.421
.759	-.136	.003	.063	.111	.172	.237	.312	.409
.806	-.182	-.002	.054	.105	.167	.236	.314	.414
.854	-.138	-.005	.057	.106	.162	.221	.293	.385
.854	.052	-.007	-.136	-.225	-.299	-.351	-.363	-.367
.806	.048	-.003	-.138	-.232	-.293	-.337	-.365	-.369
.759	.046	-.002	-.168	-.227	-.290	-.338	-.377	-.384
LEEWARD .664	.042	-.001	-.128	-.296	-.340	-.388	-.390	-.382
WING .569	.040	-.001	-.026	-.181	-.276	-.297	-.313	-.329
.473	.040	-.002	-.032	-.088	-.168	-.201	-.251	-.305
.379	.040	.000	-.032	-.067	-.114	-.171	-.279	-.367
.274								
.190								

Table 6. Continued

(b) $M_\infty = 2.16$; station 1

	THETA, DEG	CP FOR ALPHA, DEG =							
		-3.64	.38	4.46	8.42	12.36	16.44	20.46	24.44
BODY	0	-.023	.004	.035	.077	.138	.210	.304	.405
	15	-.023	.005	.036	.079	.139	.212	.304	.404
	30	-.028	.004	.037	.080	.139	.213	.303	.405
	45								
	60	.041	-.001	-.042	-.104	-.190	-.224	-.243	-.250
	75	.030	.002	-.041	-.119	-.204	-.229	-.243	-.248
	90	.028	.003	-.033	-.074	-.107	-.152	-.183	-.212
	105	.024	.002	-.025	-.051	-.070	-.098	-.120	-.137
	120	.014	.001	-.019	-.043	-.072	-.091	-.097	-.107
	135	.008	.003	-.012	-.037	-.101	-.096	-.101	-.094
	150	.002	.001	-.009	-.041	-.142	-.105	-.109	-.098
	165	.000	.002	-.005	-.024	-.033	-.105	-.108	-.118
	180	-.002	.001	-.003	-.004	-.005	-.069	-.084	-.091
	195	.001	.003	-.003	-.021	-.026	-.101	-.102	-.116
	210	.006	.004	-.005	-.041	-.134	-.102	-.100	-.097
	225	.013	.005	-.009	-.036	-.104	-.091	-.095	-.091
	240	.020	.004	-.017	-.041	-.073	-.086	-.086	-.091
	255	.029	.007	-.021	-.047	-.061	-.088	-.095	-.111
	270	.033	.009	-.025	-.061	-.081	-.115	-.142	-.160
	285	.030	.007	-.031	-.086	-.164	-.213	-.235	-.239
300	.043	.003	-.038	-.092	-.167	-.209	-.229	-.237	
315									
330	-.024	.005	.037	.077	.138	.209	.303	.407	
345	-.024	.003	.033	.073	.134	.204	.299	.401	
	Y/S	CP FOR ALPHA, DEG =							
		-3.64	.38	4.46	8.42	12.36	16.44	20.46	24.44
WINDWARD WING	.050								
	.100								
	.150								
	.200	-.025	.003	.038	.077	.138	.210	.304	.409
	.250	-.023	.004	.040	.080	.140	.214	.306	.411
	.300	-.023	.001	.038	.077	.134	.210	.300	.404
	.350	-.066	.001	.041	.081	.135	.210	.299	.404
	.400	-.139	.001	.044	.083	.135	.209	.292	.395
	.425	-.122	.001	.047	.085	.133	.205	.287	.387
	.450	-.114	.008	.064	.099	.141	.210	.290	.387
LEEWARD WING	.450	.054	-.005	-.125	-.211	-.246	-.253	-.255	-.254
	.425	.052	.005	-.131	-.215	-.247	-.254	-.257	-.256
	.400	.047	.001	-.147	-.219	-.250	-.258	-.261	-.260
	.350	.042	.002	-.049	-.197	-.234	-.235	-.241	-.240
	.300	.040	.001	-.038	-.104	-.167	-.197	-.226	-.239
	.250	.041	.001	-.040	-.099	-.184	-.221	-.244	-.251
	.200	.044	.004	-.037	-.098	-.180	-.217	-.238	-.245
	.150								
.100									
.050									

Table 6. Continued

(b) Continued; station 2

THETA, DEG	CP FOR ALPHA, DEG =							
	-3.64	.38	4.46	8.42	12.36	16.44	20.46	24.44
0	-.036	.000	.036	.079	.143	.222	.310	.409
15	-.035	.002	.039	.082	.147	.226	.314	.412
30	-.040	-.001	.037	.082	.145	.223	.313	.409
45								
60	.028	-.001	-.026	-.056	-.119	-.184	-.219	-.236
75	.021	-.001	-.025	-.059	-.122	-.192	-.224	-.238
90	.019	-.001	-.025	-.069	-.141	-.195	-.222	-.237
105	.022	.001	-.023	-.060	-.108	-.169	-.199	-.223
120	.020	.001	-.025	-.053	-.100	-.112	-.147	-.166
135	.022	.003	-.023	-.056	-.096	-.097	-.127	-.138
BODY 150	.021	.003	-.021	-.068	-.115	-.102	-.128	-.134
165	.021	.003	-.017	-.038	-.045	-.090	-.109	-.109
180	.022	.004	-.012	-.027	-.026	-.061	-.079	-.076
195	.022	.004	-.015	-.035	-.040	-.077	-.094	-.103
210	.021	.003	-.020	-.067	-.102	-.083	-.110	-.121
225	.022	.003	-.021	-.053	-.079	-.082	-.112	-.126
240	.019	-.001	-.025	-.049	-.086	-.101	-.132	-.157
255	.021	.000	-.025	-.052	-.094	-.151	-.185	-.214
270	.015	-.004	-.029	-.061	-.126	-.192	-.219	-.240
285	.024	-.003	-.028	-.057	-.106	-.180	-.218	-.241
300	.030	-.001	-.026	-.052	-.098	-.170	-.208	-.232
315								
330	-.035	.001	.039	.081	.145	.223	.311	.412
345	-.033	.004	.040	.081	.146	.223	.313	.412
Y/S	CP FOR ALPHA, DEG =							
	-3.64	.38	4.46	8.42	12.36	16.44	20.46	24.44
.075								
.150								
.225	-.035	.002	.041	.085	.147	.224	.314	.415
.300	-.035	.002	.042	.089	.149	.226	.316	.417
WINDWARD .375	-.034	.002	.042	.090	.150	.225	.314	.413
WING .450	-.029	.002	.044	.092	.151	.226	.312	.411
.524	-.128	.007	.051	.098	.159	.231	.315	.413
.599	-.133	.006	.053	.100	.160	.228	.310	.404
.637	-.122	.005	.056	.102	.161	.227	.306	.399
.674	-.118	.002	.056	.103	.159	.220	.294	.386
.674	.044	.001	-.110	-.168	-.220	-.238	-.247	-.253
.637	.041	.003	-.116	-.190	-.219	-.234	-.244	-.249
.599								
.524	.035	.004	-.114	-.198	-.230	-.243	-.248	-.248
LEEWARD .450								
WING .375	.027	.002	-.022	-.060	-.110	-.151	-.183	-.221
.300	.025	-.002	-.025	-.053	-.119	-.195	-.228	-.239
.225	.028	.001	-.024	-.054	-.117	-.183	-.219	-.235
.150								
.075								

Table 6. Continued

(b) Concluded; station 3

	THETA, DEG	CP FOR ALPHA, DEG =							
		-3.64	.38	4.46	8.42	12.36	16.44	20.46	24.44
BODY	0	-.032	.002	.040	.085	.149	.223	.315	.426
	15	-.031	.001	.040	.087	.150	.226	.319	.428
	30	-.032	.002	.041	.086	.148	.224	.316	.423
	45								
	60	.034	.005	-.021	-.050	-.090	-.150	-.180	-.200
	75								
	90	.030	.007	-.019	-.054	-.108	-.167	-.171	-.199
	105	.031	.005	-.021	-.054	-.128	-.181	-.176	-.202
	120	.029	.004	-.022	-.055	-.131	-.164	-.194	-.210
	135	.030	.005	-.020	-.062	-.151	-.149	-.185	-.212
	150	.029	.005	-.019	-.061	-.098	-.143	-.168	-.178
	165	.032	.006	-.015	-.026	-.039	-.092	-.103	-.095
	180	.031	.004	-.014	-.024	-.032	-.058	-.057	-.052
	195	.032	.007	-.015	-.027	-.042	-.075	-.088	-.105
	210	.027	.003	-.023	-.062	-.097	-.114	-.149	-.179
	225	.029	.004	-.022	-.053	-.106	-.119	-.163	-.186
	240	.029	.002	-.023	-.048	-.096	-.133	-.181	-.205
	255	.029	.002	-.023	-.050	-.102	-.173	-.207	-.199
	270	.027	.004	-.021	-.050	-.100	-.166	-.197	-.198
	285	.035	.002	-.024	-.050	-.089	-.163	-.198	-.201
	300	.022	-.010	-.034	-.056	-.094	-.160	-.191	-.203
315									
330	-.033	.002	.040	.086	.151	.226	.318	.426	
345	-.030	.001	.041	.086	.149	.224	.318	.430	
	Y/S	CP FOR ALPHA, DEG =							
		-3.64	.38	4.46	8.42	12.36	16.44	20.46	24.44
WINDWARD WING	.190	-.034	.000	.037	.085	.150	.225	.317	.423
	.274	-.033	.002	.041	.090	.153	.227	.320	.426
	.379	-.035	.000	.041	.090	.151	.225	.319	.422
	.473	-.030	.002	.045	.093	.154	.228	.324	.425
	.569	-.027	-.001	.044	.092	.151	.224	.321	.419
	.664	-.140	.000	.047	.094	.154	.226	.318	.419
	.759	-.116	-.001	.054	.103	.161	.230	.314	.409
	.806	-.126	.001	.052	.102	.161	.231	.319	.419
	.854	-.109	-.002	.058	.107	.162	.229	.310	.404
LEEWARD WING	.854	.047	.001	-.101	-.148	-.199	-.223	-.228	-.209
	.806	.042	.000	-.108	-.173	-.210	-.222	-.228	-.211
	.759	.040	.001	-.117	-.173	-.207	-.223	-.232	-.219
	.664	.040	.006	-.129	-.180	-.215	-.232	-.239	-.224
	.569	.036	.005	-.016	-.154	-.193	-.211	-.207	-.197
	.473	.037	.006	-.016	-.068	-.116	-.148	-.150	-.191
	.379	.033	.004	-.021	-.051	-.083	-.134	-.179	-.202
	.274								
.190									

Table 6. Continued

(c) $M_\infty = 2.40$; station 1

THETA, DEG	CP FOR ALPHA, DEG =							
	-3.66	.41	4.36	8.47	12.28	16.42	20.43	24.39
0	-.021	.002	.026	.069	.126	.196	.292	.394
15	-.021	.004	.029	.072	.129	.198	.293	.392
30	-.025	.002	.030	.073	.132	.203	.298	.396
45								
60	.044	-.007	-.050	-.126	-.181	-.205	-.217	-.226
75	.031	-.005	-.047	-.126	-.183	-.205	-.217	-.224
90	.031	-.004	-.041	-.078	-.104	-.140	-.167	-.201
105	.025	-.005	-.033	-.058	-.079	-.099	-.123	-.141
120	.016	-.005	-.026	-.050	-.079	-.092	-.105	-.127
135	.008	-.004	-.019	-.047	-.115	-.107	-.111	-.117
150	.001	-.004	-.014	-.052	-.128	-.115	-.116	-.123
165	-.001	-.003	-.010	-.035	-.058	-.117	-.125	-.133
180	-.002	-.004	-.007	-.011	-.032	-.090	-.109	-.117
195	.000	-.002	-.007	-.027	-.049	-.109	-.123	-.132
210	.004	-.001	-.010	-.050	-.129	-.116	-.119	-.124
225	.013	-.001	-.015	-.045	-.113	-.108	-.112	-.117
240	.021	-.003	-.022	-.048	-.082	-.096	-.104	-.117
255	.030	.000	-.026	-.053	-.074	-.096	-.112	-.127
270	.033	.000	-.033	-.069	-.088	-.119	-.137	-.154
285	.029	.000	-.037	-.095	-.152	-.192	-.209	-.215
300	.045	-.005	-.046	-.109	-.163	-.192	-.208	-.216
315								
330	-.021	.004	.028	.071	.130	.198	.293	.394
345	-.023	.002	.025	.067	.125	.193	.288	.390
Y/S	CP FOR ALPHA, DEG =							
	-3.66	.41	4.36	8.47	12.28	16.42	20.43	24.39
.050								
.100								
.150								
.200	-.022	.003	.029	.072	.131	.200	.296	.398
.250	-.021	.003	.029	.072	.131	.199	.294	.397
.300	-.021	.000	.027	.070	.128	.195	.288	.391
.350	-.090	.002	.029	.072	.130	.196	.288	.391
.400	-.122	.003	.033	.077	.132	.196	.283	.384
.425	-.109	.002	.036	.078	.131	.192	.274	.372
.450	-.105	-.002	.049	.091	.139	.197	.277	.373
.450	.057	-.027	-.119	-.189	-.212	-.220	-.225	-.227
.425	.052	-.014	-.129	-.195	-.215	-.221	-.225	-.228
.400	.048	-.009	-.135	-.197	-.216	-.223	-.228	-.230
.350	.045	-.005	-.066	-.193	-.210	-.214	-.216	-.219
.300	.044	-.006	-.047	-.131	-.167	-.189	-.206	-.219
.250	.046	-.005	-.047	-.121	-.173	-.200	-.215	-.224
.200	.046	-.001	-.044	-.117	-.171	-.199	-.215	-.223
.150								
.100								
.050								

Table 6. Continued

(c) Continued; station 2

THETA, DEG	CP FOR ALPHA, DEG =							
	-3.66	.41	4.36	8.47	12.28	16.42	20.43	24.39
0	-.026	.001	.030	.078	.137	.205	.305	.413
15	-.027	.002	.031	.079	.138	.207	.307	.415
30	-.028	.002	.032	.080	.139	.207	.308	.417
45								
60	.039	.000	-.027	-.060	-.135	-.177	-.207	-.219
75	.033	-.001	-.028	-.065	-.140	-.183	-.210	-.222
90	.027	-.001	-.029	-.079	-.151	-.185	-.211	-.221
105	.030	.000	-.027	-.070	-.117	-.154	-.188	-.212
120	.028	.000	-.026	-.059	-.091	-.113	-.145	-.165
135	.029	.000	-.024	-.062	-.082	-.103	-.120	-.136
BODY 150	.028	.001	-.022	-.075	-.094	-.104	-.118	-.131
165	.028	.002	-.018	-.045	-.069	-.097	-.111	-.120
180	.028	.002	-.015	-.027	-.049	-.072	-.098	-.091
195	.029	.003	-.016	-.036	-.062	-.088	-.107	-.112
210	.029	.002	-.020	-.071	-.087	-.099	-.110	-.124
225	.030	.002	-.021	-.060	-.073	-.098	-.114	-.131
240	.028	-.001	-.025	-.055	-.082	-.109	-.139	-.155
255	.029	-.001	-.027	-.060	-.107	-.144	-.175	-.200
270	.021	-.004	-.030	-.070	-.142	-.185	-.211	-.224
285	.033	-.004	-.031	-.063	-.130	-.178	-.208	-.223
300	.038	-.004	-.029	-.058	-.125	-.170	-.200	-.217
315								
330	-.026	.002	.032	.080	.139	.207	.309	.415
345	-.023	.004	.032	.079	.138	.206	.306	.413
Y/S								
	-3.66	.41	4.36	8.47	12.28	16.42	20.43	24.39
.075								
.150								
.225	-.026	.003	.034	.083	.141	.210	.312	.419
.300	-.027	.001	.034	.083	.141	.211	.310	.418
WINDWARD .375	-.023	.003	.035	.084	.143	.213	.310	.418
WING .450	-.028	.003	.037	.086	.144	.214	.309	.416
.524	-.120	.004	.040	.090	.147	.216	.308	.415
.599	-.112	.006	.045	.094	.151	.218	.308	.409
.637	-.107	.006	.048	.096	.151	.217	.304	.402
.674	-.103	.004	.049	.096	.149	.211	.294	.387
.674	.052	-.018	-.106	-.163	-.199	-.215	-.224	-.228
.637	.047	-.009	-.113	-.185	-.205	-.216	-.224	-.227
.599								
.524	.042	-.003	-.123	-.186	-.208	-.220	-.227	-.228
LEEWARD .450								
WING .375	.038	.000	-.024	-.066	-.128	-.154	-.185	-.214
.300	.037	-.001	-.026	-.055	-.135	-.183	-.212	-.223
.225	.040	.002	-.025	-.058	-.135	-.176	-.207	-.219
.150								
.075								

Table 6. Continued

(c) Concluded; station 3

	THETA, DEG	CP FOR ALPHA, DEG =							
		-3.66	.41	4.36	8.47	12.28	16.42	20.43	24.39
	0	-.027	.001	.031	.078	.133	.208	.311	.417
	15	-.026	.002	.031	.078	.136	.207	.312	.419
	30	-.027	.002	.031	.077	.134	.203	.309	.413
	45								
	60	.032	-.002	-.028	-.058	-.112	-.155	-.184	-.206
	75								
	90	.029	.000	-.026	-.063	-.132	-.166	-.183	-.205
	105	.032	.000	-.027	-.061	-.127	-.170	-.184	-.205
	120	.029	-.002	-.029	-.065	-.106	-.144	-.179	-.202
	135	.033	.002	-.024	-.070	-.100	-.129	-.157	-.182
BODY	150	.031	.000	-.025	-.077	-.101	-.130	-.148	-.171
	165	.030	.000	-.022	-.044	-.074	-.099	-.111	-.126
	180	.030	-.001	-.021	-.034	-.061	-.070	-.088	-.097
	195	.032	.001	-.020	-.037	-.069	-.085	-.108	-.124
	210	.029	-.002	-.025	-.072	-.093	-.119	-.139	-.164
	225	.031	-.001	-.026	-.071	-.087	-.122	-.148	-.171
	240	.030	-.003	-.027	-.063	-.091	-.131	-.164	-.188
	255	.031	-.002	-.027	-.061	-.111	-.162	-.191	-.195
	270	.027	-.001	-.028	-.062	-.128	-.167	-.186	-.199
	285	.038	-.003	-.029	-.060	-.111	-.164	-.184	-.198
	300	.027	-.012	-.037	-.064	-.115	-.164	-.186	-.202
	315								
	330	-.027	.001	.031	.078	.135	.209	.311	.417
	345	-.027	.000	.030	.077	.133	.207	.311	.418
	Y/S	CP FOR ALPHA, DEG =							
		-3.66	.41	4.36	8.47	12.28	16.42	20.43	24.39
	.190	-.029	.000	.030	.077	.133	.206	.308	.414
	.274	-.026	.001	.032	.080	.139	.210	.311	.417
	.379	-.029	-.001	.031	.080	.140	.209	.311	.415
	.473	-.025	.000	.032	.083	.142	.211	.311	.415
WINDWARD	.569	-.036	.001	.036	.087	.144	.213	.309	.413
WING	.664	-.128	.002	.039	.089	.147	.216	.308	.412
	.759	-.102	.005	.048	.098	.154	.218	.305	.403
	.806	-.107	.005	.045	.095	.153	.218	.308	.409
	.854	-.097	.003	.050	.100	.153	.214	.296	.392
	.854	.049	-.011	-.098	-.146	-.184	-.206	-.207	-.201
	.806	.044	-.007	-.104	-.162	-.198	-.209	-.208	-.204
	.759	.042	-.005	-.112	-.168	-.197	-.209	-.209	-.207
LEEWARD	.664	.038	-.001	-.129	-.168	-.199	-.212	-.213	-.212
WING	.569	.036	-.001	-.023	-.159	-.197	-.204	-.199	-.208
	.473	.034	-.002	-.021	-.081	-.150	-.163	-.180	-.203
	.379	.032	-.003	-.026	-.057	-.107	-.140	-.185	-.206
	.274								
	.190								

Table 6. Continued

(d) $M_\infty = 2.86$; station 1

	THETA, DEG	CP FOR ALPHA, DEG =						
		-3.64	.32	4.40	8.44	12.35	16.48	19.50
BODY	0	.021	.002	.026	.060	.112	.176	.262
	15	.022	.004	.028	.063	.115	.179	.264
	30	.023	.002	.028	.062	.116	.180	.266
	45							
	60	-.048	-.006	-.047	-.099	-.131	-.147	-.137
	75	-.044	-.003	-.044	-.092	-.124	-.144	-.133
	90	-.038	-.003	-.037	-.069	-.085	-.098	-.101
	105	-.034	-.004	-.030	-.053	-.073	-.086	-.087
	120	-.029	-.006	-.025	-.046	-.075	-.084	-.082
	135	-.022	-.004	-.017	-.041	-.088	-.090	-.085
	150	-.020	-.005	-.014	-.041	-.091	-.096	-.090
	165	-.016	-.005	-.010	-.030	-.060	-.095	-.093
	180	-.014	-.005	-.008	-.013	-.037	-.077	-.083
	195	-.015	-.004	-.008	-.024	-.052	-.091	-.091
	210	-.016	-.003	-.011	-.039	-.089	-.096	-.090
	225	-.020	-.002	-.015	-.040	-.086	-.094	-.087
	240	-.026	-.003	-.023	-.045	-.074	-.084	-.081
	255	-.030	.000	-.027	-.050	-.071	-.083	-.080
	270	-.031	.002	-.031	-.061	-.078	-.087	-.087
	285	-.035	.003	-.035	-.074	-.100	-.125	-.129
	300	-.042	-.002	-.040	-.086	-.115	-.133	-.129
	315							
	330	.022	.004	.027	.061	.113	.177	.263
345	.020	.002	.026	.060	.111	.174	.260	
	Y/S	CP FOR ALPHA, DEG =						
		-3.64	.32	4.40	8.44	12.35	16.48	19.50
WINDWARD WING	.050							
	.100							
	.150							
	.200	.022	.002	.027	.061	.114	.177	.265
	.250	.023	.003	.027	.061	.114	.177	.264
	.300	.020	.000	.025	.060	.111	.173	.259
	.350	.024	.000	.027	.063	.114	.175	.259
	.400	.026	-.003	.032	.068	.118	.178	.260
	.425	.029	-.003	.036	.070	.118	.176	.255
	.450	.033	-.006	.044	.081	.129	.184	.261
LEEWARD WING	.450	-.091	-.014	-.096	-.135	-.150	-.156	-.130
	.425	-.094	-.011	-.099	-.140	-.153	-.157	-.132
	.400	-.100	-.007	-.106	-.144	-.155	-.160	-.138
	.350	-.070	-.004	-.072	-.143	-.154	-.156	-.130
	.300	-.042	-.004	-.043	-.101	-.128	-.138	-.124
	.250	-.046	-.004	-.044	-.093	-.125	-.142	-.127
	.200	-.051	.001	-.042	-.096	-.126	-.145	-.142
	.150							
.100								
.050								

Table 6. Continued

(d) Continued; station 2

	THETA, DEG	CP FOR ALPHA, DEG =						
		-3.64	.32	4.40	8.44	12.35	16.48	19.50
BODY	0	.013	.004	.030	.068	.124	.193	.278
	15	.015	.006	.032	.070	.127	.195	.281
	30	.013	.004	.032	.071	.128	.196	.282
	45							
	60	-.042	-.002	-.031	-.061	-.114	-.141	-.138
	75	-.043	-.002	-.031	-.067	-.118	-.144	-.139
	90	-.040	-.003	-.032	-.072	-.121	-.145	-.141
	105	-.039	-.002	-.029	-.059	-.094	-.116	-.121
	120	-.038	-.003	-.028	-.052	-.076	-.096	-.104
	135	-.035	-.001	-.024	-.053	-.072	-.079	-.088
	150	-.034	-.001	-.022	-.061	-.075	-.082	-.085
	165	-.032	-.001	-.019	-.039	-.068	-.079	-.079
	180	-.029	-.001	-.016	-.023	-.050	-.068	-.070
	195	-.028	.000	-.017	-.033	-.061	-.075	-.076
	210	-.033	-.001	-.021	-.059	-.071	-.078	-.080
	225	-.034	-.001	-.023	-.053	-.067	-.079	-.084
	240	-.038	-.004	-.028	-.052	-.074	-.092	-.099
	255	-.038	-.003	-.028	-.055	-.085	-.106	-.114
	270	-.044	-.007	-.033	-.067	-.111	-.137	-.143
	285	-.045	-.007	-.034	-.066	-.114	-.142	-.142
	300	-.038	-.004	-.032	-.059	-.105	-.137	-.138
315								
330	.014	.005	.032	.071	.124	.194	.279	
345	.018	.009	.036	.071	.126	.194	.279	
	Y/S	CP FOR ALPHA, DEG =						
		-3.64	.32	4.40	8.44	12.35	16.48	19.50
WINDWARD WING	.075							
	.150							
	.225	.015	.005	.034	.074	.129	.198	.284
	.300	.017	.005	.035	.074	.128	.197	.284
	.375	.016	.005	.035	.076	.131	.199	.285
	.450	.018	.004	.036	.078	.132	.198	.286
	.524	.024	.007	.042	.083	.136	.202	.288
	.599	.025	.006	.045	.089	.141	.206	.291
	.637	.027	.003	.048	.091	.143	.207	.289
	.674	.028	-.005	.049	.092	.143	.203	.282
LEEWARD WING	.674	-.099	-.024	-.096	-.134	-.152	-.160	-.138
	.637	-.099	-.006	-.096	-.136	-.156	-.161	-.139
	.599							
	.524	-.109	-.001	-.104	-.142	-.156	-.162	-.138
	.450							
	.375	-.040	-.002	-.028	-.076	-.116	-.134	-.127
	.300	-.042	-.003	-.031	-.058	-.104	-.135	-.137
	.225	-.040	.000	-.029	-.059	-.111	-.138	-.134
	.150							
	.075							

Table 6. Concluded

(d) Concluded; station 3

	THETA, DEG	CP FOR ALPHA, DEG =						
		-3.64	.32	4.40	8.44	12.35	16.48	19.50
BODY	0	.026	.011	.044	.082	.138	.206	.297
	15	.027	.012	.045	.083	.139	.210	.301
	30	.030	.015	.048	.084	.139	.209	.300
	45							
	60	-.025	.000	-.022	-.045	-.099	-.123	-.130
	75							
	90	-.023	.005	-.020	-.051	-.106	-.125	-.127
	105	-.024	.005	-.020	-.050	-.096	-.124	-.127
	120	-.024	.001	-.025	-.051	-.074	-.099	-.114
	135	-.026	.002	-.022	-.057	-.070	-.084	-.092
	150	-.023	.002	-.022	-.060	-.073	-.085	-.088
	165	-.021	.005	-.016	-.034	-.062	-.077	-.072
	180	-.022	.000	-.019	-.029	-.053	-.066	-.067
	195	-.020	.001	-.019	-.031	-.059	-.072	-.075
	210	-.025	-.002	-.023	-.059	-.070	-.082	-.087
	225	-.026	.000	-.023	-.058	-.066	-.084	-.093
	240	-.024	-.002	-.025	-.050	-.070	-.096	-.105
	255	-.025	-.002	-.025	-.050	-.089	-.120	-.126
	270	-.023	.000	-.023	-.050	-.103	-.132	-.133
	285	-.026	-.003	-.025	-.046	-.095	-.130	-.132
300	-.032	-.009	-.031	-.052	-.099	-.131	-.134	
315								
330	.026	.011	.044	.082	.138	.207	.299	
345	.027	.012	.044	.082	.137	.207	.297	
	Y/S	CP FOR ALPHA, DEG =						
		-3.64	.32	4.40	8.44	12.35	16.48	19.50
WINDWARD WING	.190	.026	.011	.044	.081	.138	.206	.298
	.274	.031	.015	.049	.084	.141	.211	.300
	.379	.027	.012	.044	.082	.140	.211	.297
	.473	.030	.015	.046	.084	.141	.213	.299
	.569	.027	.013	.046	.084	.141	.215	.301
	.664	.030	.014	.050	.090	.146	.216	.306
	.759	.034	.015	.057	.100	.154	.217	.313
	.806	.035	.017	.057	.098	.153	.217	.313
	.854	.042	.015	.062	.103	.155	.215	.308
LEEWARD WING	.854	-.080	-.023	-.088	-.117	-.141	-.153	-.121
	.806	-.085	.002	-.088	-.123	-.147	-.154	-.126
	.759	-.090	.001	-.094	-.135	-.150	-.154	-.127
	.664	-.099	.001	-.103	-.135	-.149	-.155	-.125
	.569	-.054	.001	-.042	-.139	-.154	-.158	-.125
	.473	-.020	.004	-.016	-.078	-.127	-.139	-.112
	.379	-.026	-.001	-.024	-.048	-.096	-.116	-.118
	.274							
.190								

Table 7. Configuration 5

(a) $M_\infty = 1.70$; station 1

THETA, DEG	CP FOR ALPHA, DEG =							
	-3.99	-.03	4.02	8.03	11.03	16.01	20.03	24.03
0								
15								
30								
45	.039	-.001	-.047	-.102	-.197	-.276	-.351	-.410
60	.039	.004	-.041	-.107	-.206	-.307	-.370	-.416
75	.040	.010	-.036	-.102	-.207	-.299	-.375	-.421
90								
105	.032	.008	-.021	-.051	-.072	-.117	-.153	-.191
120	.025	.007	-.015	-.042	-.066	-.133	-.141	-.156
135	.021	.005	-.013	-.041	-.080	-.126	-.124	-.152
BODY 150	.026	.010	-.004	-.038	-.124	-.193	-.116	-.145
165	.025	.010	-.002	-.024	-.054	-.078	-.139	-.144
180	.022	.008	-.004	-.009	-.025	-.047	-.122	-.123
195	.030	.015	.001	-.017	-.045	-.070	-.124	-.134
210	.026	.010	-.006	-.039	-.125	-.182	-.110	-.140
225	.029	.010	-.009	-.036	-.076	-.114	-.113	-.143
240	.030	.007	-.016	-.041	-.067	-.131	-.136	-.148
255	.040	.010	-.018	-.045	-.067	-.115	-.141	-.159
270	.035	.002	-.032	-.068	-.098	-.132	-.182	-.234
285	.037	.004	-.034	-.078	-.151	-.228	-.319	-.413
300	.032	-.004	-.047	-.097	-.188	-.282	-.359	-.410
315	.039	-.006	-.052	-.099	-.158	-.243	-.342	-.399
330								
345								
Y/S	CP FOR ALPHA, DEG =							
	-3.99	-.03	4.02	8.03	11.03	16.01	20.03	24.03
.050	-.013	.009	.039	.078	.132	.204	.298	.396
.100	-.021	.003	.032	.071	.125	.197	.289	.387
.150	-.014	.011	.041	.081	.136	.206	.297	.395
.200	-.017	.009	.039	.079	.135	.205	.294	.391
WINDWARD .250	-.022	.003	.034	.073	.130	.199	.284	.382
WING .300	-.015	.007	.039	.078	.135	.203	.286	.384
.350	-.047	.011	.046	.084	.140	.205	.286	.382
.400	-.148	.014	.054	.093	.145	.206	.285	.377
.425	-.147	.007	.052	.091	.140	.198	.274	.364
.450	-.133	.006	.058	.096	.139	.193	.265	.353
.450	.056	.002	-.148	-.253	-.363	-.393	-.416	-.432
.425	.055	.005	-.150	-.251	-.360	-.397	-.418	-.434
.400	.055	.007	-.175	-.263	-.360	-.399	-.422	-.437
.350	.051	.007	-.044	-.218	-.336	-.351	-.370	-.388
LEEWARD .300	.046	.006	-.037	-.105	-.187	-.207	-.285	-.370
WING .250	.051	.010	-.036	-.088	-.155	-.250	-.359	-.410
.200								
.150								
.100								
.050								

Table 7. Continued

(a) Continued; station 2

	THETA, DEG	CP FOR ALPHA, DEG =							
		-3.99	-.03	4.02	8.03	11.03	16.01	20.03	24.03
	0								
	15								
	30								
	45	.053	.017	-.012	-.048	-.113	-.208	-.302	-.347
	60	.055	.020	-.010	-.049	-.119	-.219	-.331	-.368
	75	.047	.019	-.011	-.055	-.128	-.226	-.321	-.364
	90								
	105	.041	.011	-.018	-.053	-.117	-.171	-.272	-.337
	120	.044	.016	-.012	-.041	-.079	-.112	-.171	-.247
	135	.040	.015	-.013	-.045	-.076	-.099	-.139	-.209
BODY	150	.038	.015	-.011	-.056	-.105	-.110	-.132	-.191
	165	.042	.020	-.003	-.030	-.060	-.093	-.117	-.156
	180	.039	.017	-.005	-.022	-.042	-.077	-.100	-.132
	195	.039	.016	-.006	-.031	-.060	-.088	-.106	-.145
	210	.044	.019	-.006	-.050	-.088	-.092	-.112	-.162
	225	.045	.018	-.008	-.040	-.063	-.086	-.117	-.181
	240	.045	.017	-.009	-.038	-.072	-.100	-.144	-.220
	255	.042	.013	-.014	-.044	-.097	-.147	-.217	-.304
	270	.043	.013	-.016	-.049	-.123	-.218	-.327	-.380
	285	.044	.014	-.017	-.051	-.120	-.207	-.306	-.368
	300	.048	.008	-.021	-.055	-.113	-.187	-.319	-.384
	315	.045	.006	-.024	-.055	-.106	-.185	-.289	-.355
	330								
	345								
	Y/S	CP FOR ALPHA, DEG =							
		-3.99	-.03	4.02	8.03	11.03	16.01	20.03	24.03
	.075	-.024	.010	.047	.092	.158	.225	.317	.415
	.150	-.025	.008	.046	.091	.154	.224	.313	.412
	.225	-.025	.008	.046	.092	.153	.224	.311	.410
	.300	-.030	.002	.040	.087	.147	.217	.302	.401
WINDWARD	.375	-.019	.013	.052	.099	.158	.227	.312	.408
WING	.450	-.012	.014	.057	.103	.162	.228	.314	.406
	.524	-.112	.007	.053	.097	.156	.223	.303	.393
	.599	-.149	.016	.066	.109	.166	.234	.306	.393
	.637	-.130	.014	.070	.112	.166	.230	.300	.385
	.674	-.121	.013	.075	.117	.167	.223	.291	.372
	.674	.073	.019	-.109	-.201	-.289	-.351	-.374	-.390
	.637	.064	.014	-.116	-.207	-.290	-.353	-.382	-.397
	.599	.061	.017	-.154	-.204	-.292	-.360	-.391	-.405
	.524	.057	.018	-.074	-.272	-.333	-.377	-.379	-.379
LEEWARD	.450	.053	.016	-.005	-.119	-.223	-.278	-.296	-.306
WING	.375	.056	.020	-.006	-.048	-.111	-.183	-.243	-.305
	.300	.055	.019	-.010	-.044	-.102	-.200	-.328	-.370
	.225	.053	.017	-.012	-.049	-.117	-.213	-.310	-.355
	.150								
	.075								

Table 7. Continued

(a) Concluded; station 3

THETA, DEG	CP FOR ALPHA, DEG =							
	-3.99	-.03	4.02	8.03	11.03	16.01	20.03	24.03
0								
15								
30								
45	.048	.009	-.023	-.058	-.092	-.155	-.266	-.316
60	.052	.013	-.020	-.057	-.105	-.183	-.266	-.316
75								
90	.043	.009	-.024	-.069	-.145	-.212	-.245	-.315
105	.048	.014	-.018	-.062	-.127	-.226	-.258	-.328
120	.043	.009	-.021	-.061	-.110	-.176	-.257	-.351
135	.054	.020	-.010	-.055	-.095	-.148	-.199	-.307
BODY 150	.048	.014	-.016	-.066	-.116	-.144	-.181	-.279
165	.044	.013	-.017	-.042	-.071	-.115	-.142	-.186
180	.045	.015	-.013	-.033	-.051	-.091	-.100	-.111
195	.048	.017	-.011	-.034	-.061	-.100	-.114	-.149
210	.047	.014	-.014	-.060	-.091	-.127	-.150	-.234
225	.043	.010	-.018	-.057	-.083	-.136	-.181	-.278
240	.040	.007	-.021	-.055	-.086	-.150	-.230	-.329
255	.042	.010	-.019	-.055	-.106	-.197	-.303	-.328
270	.034	.002	-.028	-.065	-.132	-.225	-.295	-.320
285	.037	.005	-.025	-.062	-.112	-.179	-.272	-.318
300	.031	-.008	-.037	-.075	-.114	-.191	-.286	-.321
315	-.009	-.042	-.069	-.102	-.131	-.182	-.255	-.319
330								
345								
Y/S	CP FOR ALPHA, DEG =							
	-3.99	-.03	4.02	8.03	11.03	16.01	20.03	24.03
.190	-.027	.002	.039	.088	.150	.219	.307	.409
.274	-.027	.003	.041	.089	.156	.221	.309	.409
.379	-.027	.003	.041	.091	.155	.220	.308	.409
.473	-.027	.001	.041	.090	.151	.219	.305	.405
WINDWARD 569	-.013	.009	.051	.102	.162	.230	.316	.411
WING 664	-.122	.008	.052	.104	.164	.231	.314	.406
.759	-.156	.009	.060	.107	.168	.231	.309	.399
.806	-.129	.004	.059	.103	.165	.223	.298	.386
.854	-.128	-.001	.059	.101	.159	.212	.283	.366
.854	.066	.014	-.108	-.199	-.279	-.345	-.338	-.346
.806	.063	.015	-.111	-.209	-.282	-.337	-.338	-.353
.759	.063	.017	-.142	-.199	-.274	-.333	-.351	-.371
LEEWARD 664	.058	.015	-.104	-.266	-.315	-.373	-.366	-.355
WING 569	.060	.019	-.004	-.156	-.261	-.301	-.271	-.309
.473								
.379	.059	.019	-.014	-.050	-.092	-.134	-.281	-.314
.274	.049	.011	-.022	-.056	-.105	-.172	-.267	-.316
.190								

Table 7. Continued

(b) $M_\infty = 2.16$; station 1

THETA, DEG	CP FOR ALPHA, DEG =								
	-3.99	.01	4.01	8.00	11.99	16.03	20.04	23.99	
0									
15									
30									
45	.042	.000	-.044	-.105	-.187	-.223	-.240	-.251	
60	.034	.002	-.042	-.113	-.193	-.227	-.244	-.255	
75	.034	.004	-.037	-.093	-.144	-.199	-.235	-.255	
90									
105	.025	.002	-.024	-.048	-.065	-.096	-.108	-.126	
120	.016	.002	-.018	-.040	-.071	-.094	-.103	-.108	
135	.012	.004	-.012	-.033	-.093	-.097	-.110	-.108	
BODY	150	.007	.003	-.009	-.036	-.137	-.105	-.113	-.115
	165	.007	.004	-.004	-.024	-.043	-.106	-.117	-.131
	180	.007	.004	-.002	-.005	-.009	-.071	-.097	-.106
	195	.009	.005	-.003	-.019	-.033	-.099	-.102	-.124
	210	.014	.007	-.004	-.035	-.129	-.095	-.100	-.114
	225	.019	.008	-.008	-.034	-.093	-.089	-.103	-.109
	240	.023	.005	-.016	-.039	-.071	-.097	-.097	-.102
	255	.030	.006	-.021	-.046	-.065	-.096	-.097	-.108
	270	.033	.006	-.027	-.061	-.074	-.103	-.114	-.125
	285	.030	.006	-.032	-.075	-.111	-.150	-.192	-.231
	300	.030	.000	-.039	-.097	-.168	-.211	-.225	-.235
	315	.041	-.001	-.044	-.101	-.165	-.198	-.216	-.230
	330								
	345								
Y/S	CP FOR ALPHA, DEG =								
	-3.99	.01	4.01	8.00	11.99	16.03	20.04	23.99	
	.050	-.023	-.002	.024	.064	.119	.189	.276	.374
	.100	-.024	-.002	.024	.064	.118	.189	.277	.376
	.150	-.024	-.001	.025	.065	.118	.189	.277	.378
	.200	-.022	.000	.028	.068	.120	.190	.278	.379
WINDWARD	.250	-.020	.002	.031	.072	.124	.193	.280	.381
WING	.300	-.018	-.001	.030	.072	.124	.194	.279	.378
	.350	-.098	-.001	.034	.076	.127	.196	.279	.377
	.400	-.128	-.002	.037	.079	.129	.196	.277	.373
	.425	-.126	-.003	.041	.083	.131	.197	.276	.370
	.450	-.115	-.009	.044	.084	.129	.194	.268	.360
	.450	.063	.003	-.121	-.199	-.242	-.253	-.257	-.259
	.425	.061	.005	-.128	-.204	-.242	-.253	-.258	-.260
	.400	.055	.002	-.137	-.209	-.246	-.255	-.261	-.263
	.350	.049	.004	-.051	-.203	-.246	-.249	-.250	-.249
LEEWARD	.300	.047	.003	-.037	-.120	-.199	-.209	-.225	-.239
WING	.250	.046	.002	-.041	-.103	-.181	-.218	-.245	-.256
	.200								
	.150								
	.100								
	.050								

Table 7. Continued

(b) Continued; station 2

THETA, DEG	CP FOR ALPHA, DEG =							
	-3.99	.01	4.01	8.00	11.99	16.03	20.04	23.99
0								
15								
30								
45	.034	-.001	-.033	-.061	-.121	-.192	-.230	-.252
60	.037	.001	-.030	-.062	-.133	-.208	-.242	-.258
75	.026	.001	-.028	-.069	-.138	-.207	-.237	-.257
90								
105	.032	.005	-.022	-.055	-.098	-.141	-.180	-.209
120	.030	.003	-.025	-.052	-.086	-.104	-.137	-.162
135	.031	.005	-.023	-.053	-.081	-.086	-.116	-.130
150	.030	.004	-.021	-.064	-.111	-.087	-.116	-.125
165	.028	.003	-.018	-.042	-.056	-.090	-.111	-.113
180	.030	.004	-.014	-.030	-.037	-.073	-.087	-.087
195	.030	.004	-.014	-.038	-.050	-.079	-.094	-.102
210	.028	.002	-.019	-.065	-.104	-.081	-.102	-.113
225	.030	.003	-.021	-.054	-.073	-.081	-.105	-.117
240	.029	.001	-.025	-.050	-.079	-.097	-.123	-.148
255	.030	.002	-.024	-.051	-.093	-.115	-.156	-.186
270	.025	-.003	-.031	-.058	-.126	-.172	-.220	-.254
285	.021	-.004	-.032	-.060	-.131	-.203	-.237	-.257
300	.043	.003	-.027	-.054	-.106	-.189	-.231	-.249
315	.040	.000	-.030	-.054	-.097	-.183	-.221	-.245
330								
345								
Y/S	CP FOR ALPHA, DEG =							
	-3.99	.01	4.01	8.00	11.99	16.03	20.04	23.99
.075	-.032	-.004	.028	.067	.123	.200	.283	.382
.150	-.033	-.006	.027	.067	.122	.197	.281	.380
.225	-.032	-.006	.028	.070	.125	.198	.282	.381
.300	-.031	-.005	.031	.074	.129	.201	.284	.385
.375	-.030	-.006	.030	.075	.129	.201	.282	.382
.450	-.029	-.006	.031	.077	.130	.203	.282	.379
.524	-.133	-.001	.039	.084	.138	.209	.286	.383
.599	-.128	-.004	.040	.084	.137	.206	.280	.375
.637	-.123	-.004	.044	.087	.140	.205	.278	.370
.674	-.114	-.007	.046	.090	.140	.201	.270	.357
.674	.057	.004	-.104	-.166	-.228	-.255	-.265	-.270
.637	.057	.008	-.107	-.189	-.235	-.254	-.264	-.269
.599	.052	.006	-.122	-.188	-.234	-.255	-.265	-.270
.524	.048	.007	-.109	-.198	-.241	-.260	-.269	-.271
.450	.043	.006	-.016	-.141	-.205	-.227	-.237	-.241
.375	.038	.004	-.022	-.065	-.118	-.168	-.197	-.222
.300	.036	.001	-.028	-.056	-.105	-.186	-.234	-.257
.225	.037	.002	-.029	-.057	-.122	-.196	-.232	-.251
.150								
.075								

Table 7. Continued

(b) Concluded; station 3

THETA, DEG	CP FOR ALPHA, DEG =							
	-3.99	.01	4.01	8.00	11.99	16.03	20.04	23.99
0								
15								
30								
45	.042	.006	-.022	-.049	-.093	-.152	-.189	-.216
60	.044	.007	-.022	-.053	-.106	-.169	-.189	-.216
75								
90	.038	.008	-.019	-.056	-.122	-.177	-.175	-.211
105	.038	.006	-.021	-.055	-.109	-.171	-.181	-.213
120	.037	.006	-.021	-.052	-.095	-.128	-.178	-.207
135	.035	.006	-.018	-.056	-.092	-.113	-.160	-.190
BODY 150	.036	.007	-.018	-.062	-.101	-.109	-.149	-.180
165	.038	.008	-.015	-.033	-.054	-.091	-.114	-.119
180	.039	.007	-.014	-.027	-.043	-.072	-.076	-.072
195	.038	.008	-.014	-.030	-.053	-.082	-.091	-.111
210	.035	.006	-.020	-.059	-.091	-.099	-.125	-.156
225	.037	.007	-.020	-.049	-.076	-.102	-.135	-.165
240	.036	.005	-.022	-.045	-.080	-.116	-.155	-.188
255	.037	.005	-.023	-.047	-.091	-.156	-.197	-.219
270	.034	.005	-.023	-.051	-.105	-.177	-.210	-.211
285	.033	.002	-.026	-.054	-.096	-.167	-.207	-.212
300	.039	.000	-.029	-.057	-.095	-.177	-.209	-.206
315	.015	-.020	-.046	-.072	-.099	-.161	-.193	-.208
330								
345								
Y/S	CP FOR ALPHA, DEG =							
	-3.99	.01	4.01	8.00	11.99	16.03	20.04	23.99
.190	-.031	-.003	.028	.073	.131	.200	.287	.391
.274	-.030	-.001	.033	.079	.136	.206	.294	.394
.379	-.030	-.002	.032	.078	.136	.204	.294	.393
.473	-.024	-.001	.035	.080	.138	.206	.296	.393
WINDWARD .569	-.032	-.004	.034	.080	.135	.204	.294	.388
WING .664	-.143	-.003	.037	.082	.138	.207	.293	.389
.759	-.124	-.007	.038	.085	.139	.207	.288	.383
.806	-.116	-.007	.042	.090	.143	.209	.288	.380
.854	-.111	-.009	.045	.093	.143	.207	.281	.369
.854	.058	.007	-.092	-.145	-.207	-.238	-.246	-.234
.806	.053	.006	-.098	-.171	-.224	-.241	-.247	-.239
.759	.050	.005	-.111	-.172	-.221	-.242	-.247	-.244
LEEWARD .664	.050	.008	-.120	-.180	-.221	-.246	-.252	-.243
WING .569	.047	.008	-.013	-.156	-.214	-.229	-.217	-.219
.473								
.379	.043	.007	-.021	-.049	-.092	-.142	-.199	-.217
.274	.044	.008	-.021	-.048	-.107	-.156	-.189	-.215
.190								

Table 7. Continued

(c) $M_\infty = 2.40$; station 1

	THETA, DEG	CP FOR ALPHA, DEG =								
		-3.97	.04	3.98	8.06	12.02	15.95	20.00	24.03	
BODY	0									
	15									
	30									
	45	.051	.005	-.040	-.106	-.153	-.177	-.189	-.197	
	60	.042	.005	-.040	-.110	-.159	-.181	-.194	-.204	
	75	.039	.009	-.033	-.086	-.121	-.153	-.182	-.201	
	90									
	105	.031	.006	-.022	-.044	-.061	-.084	-.096	-.109	
	120	.021	.004	-.016	-.038	-.066	-.084	-.094	-.104	
	135	.015	.005	-.008	-.033	-.101	-.095	-.101	-.108	
	150	.009	.004	-.004	-.036	-.118	-.100	-.105	-.113	
	165	.008	.005	.000	-.023	-.045	-.103	-.112	-.120	
	180	.007	.005	.002	-.002	-.016	-.075	-.095	-.108	
	195	.008	.007	.003	-.017	-.034	-.093	-.104	-.121	
	210	.013	.008	.001	-.033	-.115	-.091	-.106	-.121	
	225	.019	.009	-.003	-.032	-.097	-.091	-.102	-.115	
	240	.026	.008	-.011	-.035	-.068	-.087	-.091	-.106	
	255	.033	.009	-.016	-.043	-.061	-.085	-.091	-.107	
	270	.035	.008	-.023	-.057	-.071	-.096	-.099	-.112	
	285	.031	.006	-.030	-.074	-.100	-.120	-.145	-.182	
300	.037	.003	-.038	-.092	-.140	-.168	-.180	-.188		
315	.047	.001	-.041	-.097	-.136	-.157	-.169	-.183		
330										
345										
WINDWARD WING	Y/S									
		-3.97	.04	3.98	8.06	12.02	15.95	20.00	24.03	
	.050	-.017	.005	.030	.071	.127	.194	.281	.394	
	.100	-.018	.004	.029	.070	.125	.192	.279	.392	
	.150	-.017	.006	.032	.073	.128	.196	.282	.395	
	.200	-.016	.007	.033	.074	.130	.198	.283	.394	
	.250	-.014	.008	.036	.077	.133	.200	.284	.394	
	.300	-.013	.006	.035	.077	.133	.199	.283	.391	
	.350	-.089	.005	.037	.080	.135	.201	.282	.389	
	.400	-.113	.003	.041	.085	.138	.203	.282	.386	
	.425	-.105	.000	.045	.089	.140	.204	.281	.382	
	.450	-.101	-.012	.047	.090	.139	.200	.273	.370	
	LEEWARD WING	.450	.070	-.002	-.105	-.168	-.194	-.202	-.205	-.205
		.425	.066	.008	-.114	-.173	-.196	-.202	-.205	-.206
		.400	.060	.006	-.121	-.178	-.198	-.204	-.207	-.209
		.350	.056	.008	-.056	-.177	-.198	-.202	-.200	-.198
		.300	.053	.008	-.035	-.120	-.164	-.172	-.178	-.188
		.250	.053	.007	-.038	-.105	-.147	-.171	-.190	-.199
		.200								
	.150									
.100										
.050										

Table 7. Continued

(c) Continued; station 2

	THETA, DEG	CP FOR ALPHA, DEG =							
		-3.97	.04	3.98	8.06	12.02	15.95	20.00	24.03
	0								
	15								
	30								
	45	.041	.004	-.026	-.059	-.127	-.174	-.203	-.216
	60	.044	.006	-.023	-.061	-.136	-.181	-.205	-.215
	75	.031	.006	-.024	-.073	-.140	-.182	-.205	-.216
	90								
	105	.037	.008	-.019	-.055	-.093	-.120	-.150	-.174
	120	.034	.007	-.019	-.048	-.076	-.096	-.125	-.139
	135	.034	.008	-.016	-.049	-.066	-.083	-.101	-.119
BODY	150	.032	.008	-.015	-.060	-.077	-.083	-.097	-.110
	165	.031	.008	-.012	-.038	-.061	-.085	-.094	-.101
	180	.031	.008	-.009	-.021	-.043	-.066	-.085	-.080
	195	.030	.008	-.010	-.032	-.055	-.074	-.090	-.096
	210	.029	.007	-.014	-.059	-.077	-.080	-.092	-.104
	225	.031	.007	-.015	-.050	-.061	-.081	-.095	-.112
	240	.029	.005	-.019	-.047	-.072	-.091	-.109	-.129
	255	.032	.006	-.019	-.050	-.088	-.106	-.129	-.161
	270	.027	.002	-.024	-.058	-.113	-.148	-.182	-.220
	285	.023	.001	-.026	-.061	-.139	-.179	-.201	-.218
	300	.043	.005	-.023	-.055	-.119	-.172	-.196	-.213
	315	.042	.005	-.024	-.055	-.107	-.165	-.193	-.212
	330								
	345								
	Y/S								
		-3.97	.04	3.98	8.06	12.02	15.95	20.00	24.03
	.075	-.023	.001	.032	.076	.135	.202	.288	.404
	.150	-.024	.000	.031	.076	.133	.201	.288	.402
	.225	-.024	.000	.032	.077	.134	.201	.289	.402
WINDWARD	.300	-.023	.001	.033	.079	.135	.202	.291	.402
WING	.375	-.022	.000	.033	.079	.136	.203	.291	.401
	.450	-.028	-.001	.034	.080	.136	.204	.291	.400
	.524	-.115	.001	.039	.085	.141	.208	.294	.400
	.599	-.112	-.002	.041	.087	.141	.209	.291	.394
	.637	-.107	-.003	.045	.089	.143	.209	.290	.388
	.674	-.100	-.007	.048	.092	.144	.207	.285	.376
	.674	.061	.002	-.100	-.158	-.194	-.211	-.219	-.222
	.637	.060	.006	-.103	-.171	-.199	-.212	-.218	-.221
	.599	.055	.004	-.114	-.174	-.201	-.212	-.218	-.222
	.524	.051	.007	-.115	-.177	-.204	-.213	-.219	-.222
LEEWARD	.450	.047	.007	-.019	-.152	-.190	-.202	-.207	-.210
WING	.375	.045	.008	-.020	-.072	-.131	-.162	-.182	-.200
	.300	.043	.006	-.024	-.054	-.109	-.158	-.196	-.214
	.225	.044	.007	-.023	-.056	-.126	-.173	-.199	-.211
	.150								
	.075								

Table 7. Continued

(c) Concluded; station 3

THETA, DEG	CP FOR ALPHA, DEG =							
	-3.97	.04	3.98	8.06	12.02	15.95	20.00	24.03
0								
15								
30								
45	.043	.007	-.018	-.045	-.096	-.139	-.167	-.191
60	.045	.007	-.019	-.050	-.109	-.155	-.166	-.191
75								
90	.037	.011	-.016	-.053	-.129	-.161	-.170	-.186
105	.041	.010	-.018	-.052	-.098	-.142	-.174	-.189
120	.040	.009	-.019	-.051	-.076	-.110	-.141	-.166
135	.040	.011	-.016	-.056	-.066	-.096	-.124	-.151
BODY								
150	.040	.010	-.014	-.062	-.071	-.094	-.117	-.143
165	.040	.011	-.012	-.036	-.061	-.081	-.097	-.112
180	.039	.010	-.010	-.026	-.050	-.061	-.076	-.081
195	.040	.011	-.010	-.030	-.058	-.071	-.087	-.108
210	.036	.008	-.015	-.058	-.072	-.088	-.106	-.135
225	.038	.009	-.015	-.054	-.064	-.088	-.109	-.140
240	.037	.008	-.016	-.048	-.070	-.098	-.127	-.156
255	.038	.009	-.018	-.046	-.089	-.128	-.161	-.191
270	.034	.008	-.018	-.048	-.110	-.160	-.185	-.189
285	.036	.006	-.021	-.050	-.102	-.151	-.182	-.192
300	.040	.003	-.024	-.052	-.099	-.156	-.185	-.192
315	.021	-.012	-.037	-.062	-.100	-.144	-.170	-.190
330								
345								
Y/S	CP FOR ALPHA, DEG =							
	-3.97	.04	3.98	8.06	12.02	15.95	20.00	24.03
.190	-.020	.005	.035	.079	.135	.207	.297	.405
.274	-.020	.006	.038	.083	.141	.210	.300	.410
.379	-.021	.004	.037	.082	.142	.209	.299	.407
.473	-.017	.005	.039	.086	.145	.211	.301	.408
WINDWARD								
.569	-.032	.003	.039	.087	.144	.211	.297	.403
WING								
.664	-.121	.004	.043	.090	.146	.214	.298	.401
.759	-.104	.002	.045	.092	.148	.214	.295	.395
.806	-.098	.001	.049	.097	.151	.215	.295	.392
.854	-.092	-.002	.052	.099	.151	.212	.289	.381
.854	.063	.009	-.084	-.133	-.179	-.199	-.207	-.194
.806	.058	.010	-.090	-.153	-.194	-.205	-.208	-.198
.759	.054	.009	-.100	-.163	-.195	-.206	-.209	-.202
LEEWARD								
.664	.051	.012	-.115	-.159	-.192	-.205	-.209	-.201
WING								
.569	.047	.010	-.011	-.155	-.194	-.203	-.207	-.197
.473								
.379	.043	.008	-.016	-.044	-.101	-.135	-.167	-.191
.274	.044	.009	-.017	-.043	-.107	-.147	-.166	-.190
.190								

Table 7. Continued

(d) $M_\infty = 2.86$; station 1

	THETA, DEG	CP FOR ALPHA, DEG =					
		-4.03	.02	4.04	8.01	11.99	16.01
	0						
	15						
	30						
	45	.048	.010	-.029	-.073	-.095	-.109
	60	.037	.009	-.031	-.076	-.102	-.116
	75	.035	.011	-.024	-.063	-.077	-.088
	90						
	105	.027	.009	-.014	-.037	-.052	-.069
	120	.016	.007	-.010	-.031	-.054	-.067
	135	.010	.008	-.003	-.025	-.074	-.075
BODY	150	.008	.007	.000	-.026	-.077	-.080
	165	.010	.007	.004	-.016	-.041	-.080
	180	.011	.006	.005	.000	-.017	-.060
	195	.011	.008	.005	-.011	-.031	-.073
	210	.013	.010	.003	-.023	-.072	-.076
	225	.020	.012	.000	-.024	-.069	-.077
	240	.026	.011	-.007	-.029	-.052	-.068
	255	.034	.014	-.011	-.035	-.053	-.069
	270	.036	.014	-.014	-.048	-.059	-.073
	285	.030	.013	-.018	-.057	-.069	-.074
	300	.037	.011	-.026	-.065	-.087	-.103
	315	.047	.008	-.029	-.066	-.087	-.098
	330						
	345						
	Y/S	CP FOR ALPHA, DEG =					
		-4.03	.02	4.04	8.01	11.99	16.01
	.050	-.006	.009	.033	.071	.122	.188
	.100	-.007	.009	.034	.069	.120	.186
	.150	-.008	.010	.033	.073	.123	.189
	.200	-.008	.010	.035	.073	.124	.190
	.250	-.006	.011	.037	.075	.127	.193
WINDWARD	.300	-.008	.010	.037	.075	.127	.192
WING	.350	-.078	.011	.039	.078	.129	.194
	.400	-.083	.010	.042	.083	.133	.197
	.425	-.076	.000	.045	.086	.136	.199
	.450	-.078	-.013	.049	.088	.136	.197
	.450	.061	.003	-.079	-.114	-.128	-.133
	.425	.060	.008	-.081	-.118	-.130	-.134
	.400	.053	.009	-.088	-.121	-.132	-.136
LEEWARD	.350	.049	.012	-.056	-.122	-.133	-.135
WING	.300	.047	.011	-.024	-.084	-.109	-.114
	.250	.048	.010	-.029	-.071	-.095	-.106
	.200						
	.150						
	.100						
	.050						

Table 7. Continued

(d) Continued; station 2

	THETA, DEG	CP FOR ALPHA, DEG =					
		-4.03	.02	4.04	8.01	11.99	16.01
	0						
	15						
	30						
	45	.047	.011	-.019	-.057	-.097	-.129
	60	.049	.013	-.017	-.057	-.102	-.128
	75	.035	.014	-.017	-.064	-.109	-.131
	90						
	105	.038	.015	-.012	-.037	-.061	-.078
	120	.035	.013	-.011	-.033	-.056	-.070
	135	.034	.014	-.007	-.034	-.047	-.060
BODY	150	.031	.013	-.005	-.042	-.050	-.059
	165	.030	.013	-.003	-.025	-.048	-.060
	180	.029	.013	-.001	-.007	-.034	-.052
	195	.032	.014	-.001	-.018	-.041	-.058
	210	.031	.012	-.005	-.043	-.051	-.062
	225	.034	.013	-.006	-.036	-.045	-.061
	240	.033	.010	-.011	-.034	-.054	-.066
	255	.037	.012	-.012	-.036	-.057	-.071
	270	.032	.009	-.018	-.047	-.073	-.094
	285	.033	.009	-.019	-.055	-.097	-.128
	300	.050	.011	-.020	-.053	-.093	-.122
	315	.050	.011	-.019	-.052	-.087	-.117
	330						
	345						
	Y/S	CP FOR ALPHA, DEG =					
		-4.03	.02	4.04	8.01	11.99	16.01
	.075	-.004	.013	.040	.081	.134	.205
	.150	-.005	.012	.039	.080	.133	.204
	.225	-.004	.012	.040	.082	.135	.205
	.300	-.004	.012	.041	.082	.136	.206
WINDWARD	.375	-.001	.012	.042	.083	.137	.206
WING	.450	-.013	.011	.042	.085	.138	.208
	.524	-.079	.014	.048	.092	.144	.213
	.599	-.074	.012	.050	.094	.147	.213
	.637	-.071	.012	.053	.098	.150	.214
	.674	-.069	-.006	.056	.101	.150	.213
	.674	.067	.005	-.078	-.119	-.135	-.142
	.637	.064	.015	-.076	-.117	-.134	-.143
	.599	.060	.015	-.079	-.120	-.136	-.143
	.524	.056	.015	-.085	-.122	-.136	-.143
LEEWARD	.450	.052	.014	-.017	-.123	-.139	-.144
WING	.375	.050	.014	-.014	-.072	-.110	-.126
	.300	.048	.013	-.017	-.055	-.092	-.123
	.225	.049	.014	-.015	-.053	-.093	-.123
	.150						
	.075						

Table 7. Concluded

(d) Concluded; station 3

	THETA, DEG	CP FOR ALPHA, DEG =					
		-4.03	.02	4.04	8.01	11.99	16.01
	0						
	15						
	30						
	45	.049	.015	-.010	-.031	-.077	-.110
	60	.050	.015	-.010	-.033	-.084	-.117
	75						
	90	.041	.018	-.008	-.042	-.092	-.121
	105	.043	.016	-.007	-.038	-.070	-.098
	120	.041	.015	-.010	-.035	-.055	-.079
	135	.043	.016	-.008	-.039	-.046	-.066
BODY	150	.040	.015	-.007	-.046	-.046	-.061
	165	.039	.015	-.003	-.022	-.044	-.056
	180	.038	.014	-.005	-.014	-.038	-.049
	195	.040	.015	-.004	-.019	-.041	-.054
	210	.038	.012	-.009	-.045	-.049	-.063
	225	.040	.013	-.009	-.042	-.048	-.065
	240	.039	.012	-.010	-.036	-.051	-.070
	255	.039	.013	-.010	-.035	-.064	-.087
	270	.034	.014	-.010	-.036	-.082	-.115
	285	.041	.011	-.013	-.038	-.083	-.115
	300	.042	.008	-.018	-.039	-.081	-.119
	315	.031	-.002	-.026	-.046	-.076	-.109
	330						
	345						
	Y/S						
		-4.03	.02	4.04	8.01	11.99	16.01
	.190	-.007	.021	.052	.088	.143	.215
	.274	-.004	.025	.054	.092	.146	.219
	.379	-.006	.023	.052	.091	.146	.220
	.473	-.001	.024	.055	.092	.147	.223
WINDWARD	.569	-.026	.022	.055	.093	.146	.222
WING	.664	-.085	.022	.058	.098	.150	.223
	.759	-.072	.019	.060	.102	.153	.222
	.806	-.063	.021	.064	.106	.157	.223
	.854	-.065	.015	.067	.109	.158	.222
	.854	.067	.013	-.071	-.109	-.130	-.141
	.806	.062	.019	-.072	-.110	-.131	-.142
	.759	.058	.017	-.077	-.118	-.135	-.141
LEEWARD	.664	.055	.018	-.083	-.120	-.135	-.141
WING	.569	.051	.017	-.018	-.127	-.140	-.145
	.473						
	.379	.049	.016	-.009	-.036	-.080	-.106
	.274	.050	.019	-.006	-.029	-.076	-.111
	.190						

Table 8. Configuration 6

(a) $M_\infty = 1.70$; station 1

THETA, DEG	CP FOR ALPHA, DEG =							
	-3.22	.74	4.77	8.74	12.74	16.68	20.76	24.74
0								
15	-.002	.001	.005	.010	.025	.072	.139	.218
30	-.005	-.001	.002	-.003	-.012	.019	.074	.140
45	-.006	.001	.003	-.015	-.059	-.053	-.017	.029
60	-.012	.000	.004	-.016	-.079	-.140	-.129	-.103
75	-.016	.004	.013	.004	-.020	-.145	-.224	-.225
90	-.022	.001	.019	.025	.023	-.038	-.119	-.165
105	-.020	.004	.027	.036	.035	-.016	-.093	-.125
120	-.026	-.002	.020	.006	-.032	-.015	-.062	-.111
135								
BODY 150	.046	.002	-.033	-.082	-.125	-.108	-.131	-.162
165	.048	.005	-.029	-.070	-.105	-.111	-.150	-.156
180	.047	.005	-.026	-.052	-.078	-.087	-.131	-.123
195	.048	.006	-.026	-.058	-.083	-.096	-.138	-.137
210	.043	.002	-.030	-.072	-.109	-.085	-.117	-.150
225								
240	-.026	-.003	.015	.008	-.033	-.037	-.065	-.114
255	-.023	-.001	.017	.027	.020	-.025	-.092	-.116
270	-.019	.001	.013	.021	.021	-.031	-.101	-.141
285	-.015	.002	.008	.002	-.016	-.113	-.199	-.228
300	-.012	.000	.001	-.017	-.074	-.156	-.147	-.128
315	-.009	-.001	-.002	-.019	-.070	-.068	-.039	-.002
330	-.005	.000	.001	-.005	-.020	.012	.061	.119
345	-.004	.000	.003	.008	.018	.067	.130	.205
Y/S	CP FOR ALPHA, DEG =							
	-3.22	.74	4.77	8.74	12.74	16.68	20.76	24.74
.050								
.100								
.150								
.200								
.250								
WINDWARD WING .300	-.023	.000	.024	.043	.044	-.006	-.055	-.106
.350	-.017	.001	.029	.063	.103	-.003	-.061	-.113
.400	-.098	-.002	.029	.062	.110	.102	.022	-.017
.425	-.138	.000	.032	.061	.103	.141	.080	.055
.450	-.133	-.001	.035	.061	.098	.146	.117	.124
.450	.058	-.002	-.127	-.178	-.210	-.233	-.220	-.261
.425	.050	-.004	-.150	-.199	-.221	-.252	-.205	-.242
.400	.051	.003	-.071	-.202	-.228	-.234	-.178	-.215
LEEWARD WING .350	.050	.003	-.029	-.108	-.190	-.138	-.131	-.173
.300	.048	.002	-.032	-.066	-.097	-.092	-.136	-.167
.250								
.200								
.150								
.100								
.050								

Table 8. Continued

(a) Continued; station 2

THETA, DEG	CP FOR ALPHA, DEG =							
	-3.22	.74	4.77	8.74	12.74	16.68	20.76	24.74
0	-.009	.003	.020	.048	.087	.082	.155	.226
15	-.009	.003	.020	.046	.078	.076	.135	.204
30	-.009	.005	.021	.043	.061	.063	.070	.132
45	-.010	.006	.021	.039	.043	.031	-.027	.020
60	-.012	.005	.020	.034	.035	.016	-.049	-.108
75	-.014	.005	.020	.041	.047	.050	.030	.001
90	-.020	.002	.020	.044	.058	.065	.056	.036
105	-.017	.005	.024	.047	.058	.062	.053	.031
120	-.021	-.002	.013	.022	.019	.008	-.016	-.019
135								
BODY								
150	.043	.001	-.038	-.075	-.102	-.138	-.174	-.199
165	.042	.000	-.040	-.081	-.110	-.149	-.181	-.207
180	.043	.002	-.037	-.078	-.108	-.145	-.171	-.200
195	.036	-.004	-.045	-.086	-.114	-.151	-.178	-.211
210	.043	.001	-.040	-.078	-.101	-.134	-.166	-.201
225								
240	-.014	.005	.019	.023	.020	.012	-.011	-.011
255	.174	.179	.184	.186	.190	.192	.196	.200
270	.155	.159	.164	.165	.169	.172	.174	.179
285	-.017	.002	.013	.026	.035	.050	.031	.016
300	-.014	.005	.013	.022	.023	.014	-.039	-.125
315	-.013	.002	.012	.022	.028	.017	-.052	-.015
330	-.013	.001	.013	.030	.049	.048	.047	.103
345	-.009	.004	.021	.045	.078	.077	.127	.195
Y/S								
	-3.22	.74	4.77	8.74	12.74	16.68	20.76	24.74
.075								
.150								
.225								
WINDWARD								
WING								
.300	-.012	.006	.025	.044	.042	.065	.039	.018
.375	-.010	.006	.029	.058	.055	.041	-.021	-.058
.450	-.009	.003	.026	.055	.094	.145	.139	.067
.524	-.004	.004	.027	.052	.092	.144	.195	.248
.599	-.146	.003	.028	.048	.081	.119	.161	.226
.637	-.135	.004	.031	.048	.076	.110	.142	.196
.674	-.110	.004	.035	.049	.073	.104	.125	.170
.674	.065	.006	-.108	-.181	-.228	-.274	-.317	-.348
.637	.060	.007	-.132	-.214	-.253	-.290	-.339	-.361
.599	.056	.007	-.139	-.255	-.298	-.317	-.348	-.359
.524	.050	.003	-.027	-.132	-.267	-.293	-.296	-.318
LEEWARD								
WING								
.450	.052	.009	-.029	-.070	-.118	-.187	-.218	-.244
.375	.050	.007	-.033	-.069	-.085	-.133	-.176	-.201
.300	.044	.002	-.039	-.072	-.096	-.136	-.177	-.199
.225								
.150								
.075								

Table 8. Continued

(a) Concluded; station 3

THETA, DEG	CP FOR ALPHA, DEG =							
	-3.22	.74	4.77	8.74	12.74	16.68	20.76	24.74
0	-.008	.005	.022	.047	.085	.124	.169	.221
15	-.006	.008	.026	.049	.084	.122	.161	.201
30	-.009	.007	.023	.042	.072	.101	.119	.125
45	-.012	.005	.020	.033	.060	.075	.071	.059
60	-.015	.003	.018	.028	.048	.064	.055	.023
75	-.014	.006	.020	.036	.052	.087	.101	.094
90	-.022	-.003	.013	.033	.052	.089	.103	.102
105	-.019	-.002	.016	.035	.055	.088	.099	.091
120	-.019	-.009	.010	.020	.034	.057	.065	.052
135								
BODY 150	.044	-.002	-.043	-.079	-.115	-.148	-.170	-.195
165	.044	-.002	-.043	-.080	-.116	-.152	-.176	-.205
180	.043	-.003	-.042	-.081	-.116	-.153	-.173	-.201
195	.044	-.003	-.042	-.080	-.113	-.151	-.172	-.198
210	.040	-.009	-.055	-.085	-.116	-.156	-.177	-.202
225								
240								
255	-.014	.002	.017	.038	.061	.086	.100	.106
270	-.015	.001	.015	.036	.058	.087	.102	.115
285	-.014	.004	.016	.034	.053	.081	.095	.108
300	-.016	.001	.012	.024	.040	.051	.037	.028
315	-.011	.006	.018	.033	.058	.066	.054	.061
330	-.010	.003	.016	.037	.069	.087	.099	.114
345	-.009	.004	.019	.044	.078	.112	.147	.186
Y/S	CP FOR ALPHA, DEG =							
	-3.22	.74	4.77	8.74	12.74	16.68	20.76	24.74
.190								
.274	-.014	.002	.021	.035	.047	.059	.075	.081
.379	-.012	.004	.026	.042	.027	.012	.004	.010
.473	-.015	.003	.023	.054	.092	.109	.107	.088
WINDWARD .569	-.008	.004	.023	.058	.096	.141	.197	.227
WING .664	-.036	.003	.023	.055	.084	.121	.179	.241
.759	-.143	.003	.026	.047	.075	.101	.148	.193
.806	-.125	.004	.028	.044	.068	.090	.129	.165
.854	-.109	.003	.031	.041	.059	.077	.105	.133
.854	.063	-.002	-.120	-.185	-.245	-.297	-.343	-.379
.806	.059	.001	-.135	-.203	-.256	-.308	-.357	-.393
.759	.057	.004	-.152	-.256	-.309	-.344	-.381	-.397
LEEWARD .664	.054	.004	-.025	-.132	-.254	-.309	-.346	-.358
WING .569	.051	.002	-.032	-.068	-.137	-.200	-.267	-.290
.473	.050	.000	-.040	-.075	-.112	-.153	-.202	-.233
.379	.049	.000	-.042	-.077	-.109	-.143	-.170	-.198
.274	.047	.001	-.042	-.076	-.110	-.146	-.168	-.194
.190								

Table 8. Continued

(b) $M_\infty = 2.16$; station 1

THETA, DEG	CP FOR ALPHA, DEG =							
	-2.64	1.36	5.33	9.35	13.39	17.33	21.37	25.38
0								
15	-.006	-.007	-.005	.012	.050	.100	.171	.253
30	-.004	-.001	-.005	.000	.026	.067	.125	.195
45	-.008	.000	-.009	-.028	-.020	.007	.048	.100
60	-.013	.000	-.005	-.056	-.075	-.064	-.040	-.009
75	-.016	.001	.005	-.018	-.111	-.133	-.126	-.110
90	-.015	.007	.020	.019	-.035	-.083	-.106	-.103
105	-.015	.009	.027	.025	-.024	-.060	-.083	-.085
120	-.019	.007	.023	-.009	-.062	-.056	-.072	-.078
135								
BODY								
150	.030	-.005	-.036	-.078	-.093	-.094	-.117	-.130
165	.028	-.006	-.035	-.070	-.096	-.105	-.109	-.132
180	.032	-.001	-.026	-.042	-.063	-.083	-.087	-.103
195	.035	.001	-.025	-.050	-.073	-.091	-.102	-.120
210	.031	-.005	-.032	-.067	-.073	-.086	-.111	-.126
225								
240	-.027	-.002	.012	-.010	-.082	-.071	-.090	-.096
255	-.024	.000	.013	.009	-.049	-.070	-.083	-.079
270	-.021	.000	.008	.007	-.039	-.075	-.094	-.086
285	-.019	-.004	-.003	-.021	-.095	-.133	-.135	-.121
300	-.016	-.005	-.012	-.065	-.091	-.080	-.057	-.026
315	-.011	-.004	-.012	-.039	-.032	-.007	.033	.082
330	-.010	-.007	-.011	-.014	.013	.049	.109	.176
345	-.006	-.007	-.003	.009	.048	.095	.169	.250
Y/S								
	-2.64	1.36	5.33	9.35	13.39	17.33	21.37	25.38
.050								
.100								
.150								
.200								
.250								
WINDWARD								
WING								
.300	-.023	.002	.025	.041	-.018	-.055	-.078	-.083
.350	-.022	.001	.030	.062	.024	-.061	-.075	-.080
.400	-.082	.000	.031	.065	.100	.048	.036	.073
.425	-.106	.003	.035	.066	.100	.104	.107	.160
.450	-.102	.005	.038	.066	.096	.125	.147	.202
.450	.032	-.035	-.114	-.144	-.153	-.167	-.182	-.198
.425	.031	-.014	-.128	-.146	-.160	-.159	-.168	-.187
.400	.028	-.012	-.113	-.159	-.171	-.145	-.158	-.177
LEEWARD								
WING								
.350	.028	-.010	-.036	-.118	-.130	-.098	-.127	-.145
.300	.030	-.007	-.035	-.061	-.069	-.099	-.119	-.131
.250								
.200								
.150								
.100								
.050								

Table 8. Continued

(b) Continued; station 2

THETA, DEG	CP FOR ALPHA, DEG =							
	-2.64	1.36	5.33	9.35	13.39	17.33	21.37	25.38
BODY								
0	-.010	.001	.014	.025	.053	.111	.180	.265
15	-.011	.002	.015	.024	.046	.099	.165	.244
30	-.016	-.001	.011	.021	.014	.055	.111	.176
45	-.016	-.001	.010	.021	-.006	-.003	.038	.086
60	-.021	-.005	.007	.017	-.002	-.070	-.052	-.021
75	-.021	-.002	.015	.027	.026	-.001	-.040	-.035
90	-.029	-.011	.008	.023	.024	.010	.000	.014
105	-.026	-.008	.008	.025	.021	.004	-.001	.011
120	-.018	-.001	.014	.017	.002	-.014	-.014	.000
135								
150	.031	-.007	-.043	-.066	-.088	-.111	-.135	-.152
165	.033	-.005	-.040	-.068	-.088	-.112	-.139	-.155
180	.030	-.009	-.042	-.073	-.093	-.111	-.139	-.154
195	.030	-.008	-.043	-.073	-.090	-.110	-.134	-.149
210	.029	-.011	-.047	-.072	-.090	-.110	-.132	-.148
225								
240	-.021	-.005	.005	.008	.001	-.023	-.022	-.003
255	.236	.235	.233	.232	.230	.230	.231	.232
270	.232	.231	.229	.227	.226	.226	.227	.228
285	-.014	.002	.013	.025	.026	.009	-.006	.000
300	-.016	-.002	.006	.010	-.004	-.069	-.064	-.034
315	-.012	.001	.008	.010	-.016	-.015	.023	.073
330	-.012	-.001	.009	.013	.007	.047	.099	.167
345	-.013	-.002	.010	.018	.036	.090	.154	.235
Y/S								
	-2.64	1.36	5.33	9.35	13.39	17.33	21.37	25.38
WINDWARD WING								
.075								
.150								
.225								
.300	-.019	-.002	.013	.032	.027	.005	-.002	.012
.375	-.017	-.002	.018	.044	.014	-.043	-.056	-.041
.450	-.012	-.001	.023	.057	.095	.107	.072	.070
.524	-.037	.001	.025	.056	.103	.144	.199	.250
.599	-.096	.001	.028	.054	.093	.122	.167	.243
.637	-.095	.004	.033	.057	.090	.112	.149	.213
.674	-.095	.001	.033	.053	.082	.097	.126	.179
LEEWARD WING								
.674	.044	-.031	-.115	-.155	-.186	-.211	-.231	-.237
.637	.039	-.022	-.122	-.159	-.189	-.220	-.237	-.241
.599	.036	-.015	-.147	-.178	-.204	-.232	-.240	-.245
.524	.039	-.006	-.032	-.160	-.210	-.205	-.209	-.225
.450	.032	-.010	-.039	-.078	-.141	-.158	-.174	-.199
.375	.033	-.007	-.042	-.066	-.082	-.117	-.140	-.160
.300	.036	-.002	-.038	-.055	-.079	-.104	-.127	-.145
.225								
.150								
.075								

Table 8. Continued

(b) Concluded; station 3

THETA, DEG	CP FOR ALPHA, DEG =							
	-2.64	1.36	5.33	9.35	13.39	17.33	21.37	25.38
0	-.014	-.005	.014	.038	.062	.094	.166	.257
15	-.014	-.004	.014	.040	.060	.085	.154	.240
30	-.021	-.010	.007	.029	.039	.040	.096	.167
45	-.018	-.005	.010	.028	.031	.007	.026	.078
60	-.019	-.003	.011	.027	.035	.013	-.026	-.019
75	-.020	-.002	.012	.030	.045	.050	.058	.075
90	-.022	-.004	.012	.030	.046	.056	.067	.091
105	-.025	-.007	.008	.024	.040	.046	.052	.074
120	-.025	-.007	.009	.016	.024	.026	.029	.051
135								
BODY								
150	.024	-.017	-.049	-.075	-.101	-.113	-.134	-.151
165	.027	-.016	-.047	-.075	-.100	-.115	-.138	-.158
180	.025	-.018	-.048	-.077	-.103	-.119	-.138	-.161
195	.027	-.017	-.048	-.076	-.101	-.116	-.137	-.156
210	.028	-.017	-.049	-.071	-.099	-.112	-.134	-.148
225								
240								
255	-.014	.001	.013	.030	.040	.047	.056	.081
270	-.015	.001	.014	.033	.045	.054	.067	.095
285	-.016	-.001	.012	.030	.043	.046	.059	.084
300	-.017	-.003	.008	.023	.033	.010	-.010	-.021
315	-.017	-.004	.007	.020	.028	.003	.009	.058
330	-.015	-.002	.011	.027	.041	.036	.088	.157
345	-.012	-.001	.016	.036	.058	.080	.146	.232
Y/S	CP FOR ALPHA, DEG =							
	-2.64	1.36	5.33	9.35	13.39	17.33	21.37	25.38
.190								
.274	-.014	.001	.016	.029	.027	.031	.039	.065
.379	-.018	-.004	.015	.026	-.010	-.033	-.032	.000
.473	-.015	.000	.023	.052	.075	.084	.072	.080
WINDWARD								
WING								
.569	-.014	-.003	.020	.047	.088	.138	.189	.219
.664	-.056	.002	.025	.047	.083	.125	.176	.247
.759	-.094	.001	.026	.043	.071	.102	.142	.199
.806	-.089	.003	.029	.045	.067	.095	.127	.180
.854	-.087	.004	.029	.043	.060	.084	.108	.159
.854	.041	-.029	-.113	-.159	-.193	-.224	-.239	-.249
.806	.037	-.020	-.117	-.163	-.199	-.225	-.247	-.253
.759	.032	-.021	-.148	-.187	-.216	-.237	-.259	-.260
LEEWARD								
WING								
.664	.029	-.017	-.058	-.177	-.222	-.243	-.239	-.249
.569	.027	-.016	-.043	-.084	-.140	-.197	-.200	-.228
.473	.030	-.010	-.043	-.067	-.092	-.131	-.156	-.188
.379	.027	-.014	-.048	-.072	-.093	-.110	-.135	-.154
.274	.029	-.014	-.046	-.070	-.095	-.109	-.129	-.145
.190								

Table 8. Continued

(c) $M_\infty = 2.40$; station 1

THETA, DEG	CP FOR ALPHA, DEG =							
	-3.99	-.02	4.03	7.96	12.00	15.97	20.11	24.03
0								
15	-.001	.003	.002	.017	.056	.108	.174	.249
30	-.003	.003	.000	.006	.034	.076	.130	.192
45	-.007	.003	-.001	-.013	-.002	.025	.063	.108
60	-.014	.002	.001	-.035	-.049	-.038	-.015	.012
75	-.018	.005	.009	-.011	-.079	-.095	-.088	-.074
90	-.021	.007	.018	.022	-.022	-.070	-.080	-.077
105	-.020	.009	.023	.029	-.011	-.049	-.064	-.065
120	-.022	.006	.020	.003	-.054	-.057	-.071	-.075
135								
BODY 150	.041	.005	-.018	-.058	-.086	-.088	-.115	-.130
165	.042	.007	-.017	-.051	-.076	-.094	-.107	-.128
180	.045	.009	-.013	-.030	-.049	-.073	-.086	-.103
195	.049	.012	-.012	-.034	-.058	-.085	-.099	-.119
210	.047	.010	-.016	-.046	-.067	-.085	-.108	-.125
225								
240	-.031	-.004	.015	.004	-.068	-.081	-.089	-.092
255	-.028	.000	.016	.016	-.039	-.060	-.069	-.069
270	-.024	.000	.013	.011	-.028	-.066	-.074	-.073
285	-.020	-.001	.005	-.013	-.075	-.103	-.100	-.091
300	-.017	-.002	-.003	-.043	-.064	-.055	-.034	-.010
315	-.009	.001	-.004	-.025	-.018	.007	.043	.085
330	-.006	.001	-.003	-.004	.020	.060	.113	.172
345	-.002	.002	.001	.012	.049	.101	.166	.240
Y/S	CP FOR ALPHA, DEG =							
	-3.99	-.02	4.03	7.96	12.00	15.97	20.11	24.03
.050								
.100								
.150								
.200								
.250								
WINDWARD 300	-.027	-.001	.023	.040	-.008	-.054	-.071	-.075
WING 350	-.036	-.001	.026	.056	.040	-.040	-.059	-.064
.400	-.121	-.002	.026	.058	.096	.079	.073	.089
.425	-.114	-.001	.029	.059	.096	.113	.128	.169
.450	-.108	-.020	.033	.061	.092	.118	.143	.187
.450	.042	-.019	-.083	-.115	-.127	-.141	-.161	-.175
.425	.040	.002	-.088	-.118	-.132	-.136	-.150	-.166
.400	.037	.002	-.067	-.126	-.138	-.125	-.143	-.161
LEEWARD 350	.039	.003	-.018	-.090	-.108	-.092	-.123	-.141
WING 300	.040	.003	-.019	-.049	-.069	-.092	-.119	-.134
.250								
.200								
.150								
.100								
.050								

Table 8. Continued

(c) Continued; station 2

THETA, DEG	CP FOR ALPHA, DEG =							
	-3.99	-.02	4.03	7.96	12.00	15.97	20.11	24.03
0	-.005	.003	.013	.021	.056	.109	.176	.260
15	-.008	.004	.014	.024	.051	.099	.165	.243
30	-.010	.004	.014	.025	.028	.064	.121	.187
45	-.010	.005	.015	.025	-.003	.014	.057	.107
60	-.014	.002	.013	.024	.000	-.047	-.022	.010
75	-.015	.003	.017	.031	.029	-.010	-.031	-.022
90	-.020	-.001	.013	.030	.032	.012	.009	.025
105	-.018	.000	.015	.031	.029	.010	.008	.023
120	-.016	.001	.017	.023	.009	-.008	-.010	.001
135								
BODY								
150	.051	.009	-.022	-.047	-.073	-.093	-.128	-.142
165	.052	.011	-.020	-.050	-.075	-.095	-.130	-.143
180	.051	.008	-.022	-.052	-.077	-.094	-.130	-.143
195	.048	.007	-.024	-.053	-.078	-.093	-.127	-.141
210	.050	.008	-.024	-.052	-.074	-.091	-.122	-.136
225								
240	-.018	.001	.016	.015	.009	-.014	-.015	-.001
255	.277	.275	.274	.272	.270	.269	.267	.265
270	.268	.267	.265	.263	.262	.260	.258	.257
285	-.015	.001	.013	.023	.017	-.008	-.012	-.008
300	-.014	.001	.011	.015	-.014	-.059	-.038	-.012
315	-.012	.002	.010	.012	-.021	-.003	.037	.081
330	-.012	.002	.010	.013	.013	.051	.104	.168
345	-.007	.003	.012	.017	.043	.092	.155	.234
Y/S	CP FOR ALPHA, DEG =							
	-3.99	-.02	4.03	7.96	12.00	15.97	20.11	24.03
.075								
.150								
.225								
.300	-.016	.002	.019	.035	.025	-.001	-.002	.009
WINDWARD	-.014	.003	.022	.044	.015	-.041	-.042	-.032
WING	-.008	.003	.024	.050	.083	.099	.078	.077
.450	-.101	.003	.025	.051	.091	.134	.190	.234
.524	-.109	.001	.026	.050	.081	.117	.158	.217
.599	-.100	.000	.029	.051	.077	.108	.141	.190
.637	-.100	.000	.029	.051	.077	.108	.141	.190
.674	-.098	-.007	.032	.053	.075	.099	.124	.166
.674	.064	.007	-.074	-.121	-.151	-.174	-.191	-.196
.637	.061	.011	-.083	-.125	-.156	-.180	-.193	-.198
.599	.059	.012	-.086	-.139	-.164	-.187	-.197	-.200
.524	.056	.013	-.012	-.131	-.176	-.176	-.180	-.191
LEEWARD	.054	.012	-.016	-.057	-.118	-.137	-.153	-.173
WING	.054	.012	-.018	-.047	-.064	-.097	-.127	-.144
.300	.053	.012	-.019	-.042	-.067	-.090	-.123	-.138
.225								
.150								
.075								

Table 8. Continued

(d) $M_\infty = 2.86$; station 1

THETA, DEG	CP FOR ALPHA, DEG =							
	-3.98	.01	4.02	8.02	11.99	16.02	20.04	23.95
0								
15	.005	.005	.008	.026	.061	.106	.168	.237
30	.002	.007	.006	.017	.043	.080	.131	.190
45	-.001	.007	.002	-.001	.012	.038	.074	.119
60	-.008	.005	.001	-.023	-.025	-.011	.010	.038
75	-.012	.007	.009	-.022	-.055	-.057	-.049	-.034
90	-.016	.008	.018	.011	-.028	-.050	-.050	-.047
105	-.016	.010	.024	.019	-.011	-.036	-.043	-.040
120	-.018	.007	.022	-.002	-.038	-.051	-.050	-.048
135								
BODY								
150	.039	.007	-.017	-.048	-.070	-.078	-.090	-.101
165	.040	.007	-.015	-.042	-.060	-.080	-.088	-.100
180	.044	.009	-.011	-.025	-.037	-.061	-.072	-.079
195	.048	.012	-.010	-.029	-.047	-.072	-.083	-.095
210	.046	.009	-.013	-.038	-.061	-.076	-.091	-.101
225								
240	-.024	.000	.014	-.002	-.051	-.067	-.066	-.061
255	-.020	.004	.015	.006	-.025	-.043	-.045	-.040
270	-.018	.004	.011	.003	-.025	-.048	-.049	-.043
285	-.014	.003	.004	-.024	-.054	-.066	-.059	-.048
300	-.009	.003	-.002	-.032	-.034	-.023	-.003	.019
315	-.003	.004	-.001	-.010	.004	.025	.060	.097
330	.001	.004	.002	.008	.033	.068	.118	.170
345	.005	.005	.007	.023	.058	.102	.163	.228
Y/S	CP FOR ALPHA, DEG =							
	-3.98	.01	4.02	8.02	11.99	16.02	20.04	23.95
.050								
.100								
.150								
.200								
.250								
WINDWARD								
WING								
.300	-.019	.003	.022	.032	-.008	-.045	-.049	-.046
.350	-.049	.002	.024	.047	.039	-.014	-.029	-.029
.400	-.083	.000	.025	.050	.082	.095	.091	.100
.425	-.079	-.007	.028	.052	.082	.106	.134	.166
.450	-.076	-.012	.032	.055	.080	.096	.128	.171
.450	.042	-.006	-.066	-.088	-.095	-.106	-.121	-.129
.425	.042	.000	-.064	-.085	-.094	-.098	-.113	-.122
.400	.037	.002	-.063	-.091	-.099	-.095	-.110	-.121
LEEWARD								
WING								
.350	.035	.005	-.014	-.073	-.080	-.083	-.097	-.107
.300	.037	.005	-.017	-.042	-.058	-.082	-.096	-.105
.250								
.200								
.150								
.100								
.050								

Table 8. Continued

(d) Continued; station 2

THETA, DEG	CP FOR ALPHA, DEG =							
	-3.98	.01	4.02	8.02	11.99	16.02	20.04	23.95
	.007	.011	.015	.028	.066	.114	.182	.252
0	.007	.011	.015	.028	.066	.114	.182	.252
15	.006	.012	.017	.027	.061	.107	.170	.238
30	.001	.010	.016	.018	.038	.077	.129	.187
45	.001	.011	.017	.017	.008	.036	.073	.117
60	-.004	.007	.015	.017	-.018	-.016	.006	.034
75	-.003	.009	.020	.027	.015	-.016	-.019	-.012
90	-.012	.002	.016	.024	.019	.008	.007	.018
105	-.013	.004	.018	.027	.020	.011	.011	.025
120	-.008	.008	.024	.025	.011	.003	.002	.015
135								
BODY 150	.052	.012	-.017	-.038	-.056	-.079	-.100	-.114
165	.053	.013	-.013	-.036	-.055	-.076	-.099	-.110
180	.050	.011	-.018	-.041	-.062	-.077	-.104	-.113
195	.049	.011	-.017	-.041	-.058	-.073	-.098	-.109
210	.048	.009	-.020	-.043	-.057	-.074	-.097	-.110
225								
240	-.009	.004	.016	.014	.008	-.008	-.005	.008
255	.359	.357	.356	.354	.354	.353	.351	.349
270	.351	.348	.347	.346	.346	.344	.343	.341
285	-.001	.009	.017	.023	.014	-.010	-.008	.003
300	-.002	.007	.012	.011	-.024	-.027	-.006	.019
315	.002	.009	.013	.006	.001	.023	.060	.100
330	.002	.009	.012	.010	.032	.067	.119	.172
345	.004	.009	.013	.020	.054	.099	.161	.227
Y/S	CP FOR ALPHA, DEG =							
	-3.98	.01	4.02	8.02	11.99	16.02	20.04	23.95
.075								
.150								
.225								
WINDWARD .300	-.009	.005	.020	.032	.019	-.004	-.002	.012
.375	-.006	.006	.023	.043	.015	-.020	-.022	-.010
WING .450	-.024	.005	.026	.050	.079	.091	.082	.090
.524	-.071	.008	.027	.051	.085	.117	.169	.215
.599	-.076	.007	.028	.050	.078	.102	.139	.186
.637	-.073	.003	.031	.052	.077	.096	.127	.168
.674	-.075	-.017	.032	.052	.073	.087	.112	.148
.674	.063	-.003	-.064	-.095	-.116	-.134	-.141	-.144
.637	.059	.012	-.066	-.096	-.117	-.135	-.141	-.144
.599	.057	.015	-.070	-.101	-.120	-.136	-.141	-.143
.524	.059	.017	-.017	-.100	-.121	-.129	-.131	-.135
LEEWARD .450	.054	.012	-.014	-.054	-.108	-.112	-.120	-.132
WING .375	.055	.013	-.016	-.038	-.050	-.080	-.099	-.112
.300	.056	.015	-.013	-.032	-.047	-.073	-.093	-.109
.225								
.150								
.075								

Table 8. Concluded

(d) Concluded; station 3

THETA, DEG	CP FOR ALPHA, DEG =							
	-3.98	.01	4.02	8.02	11.99	16.02	20.04	23.95
0	.001	.014	.026	.041	.065	.114	.181	.254
15	.001	.015	.028	.042	.060	.108	.171	.243
30	-.005	.011	.024	.035	.037	.074	.126	.188
45	-.002	.014	.026	.032	.021	.034	.072	.119
60	-.003	.013	.024	.032	.025	-.003	.008	.038
75	-.002	.013	.024	.037	.041	.039	.038	.045
90	-.001	.013	.025	.040	.046	.050	.059	.076
105	-.004	.009	.021	.033	.039	.041	.050	.070
120	-.004	.007	.020	.028	.028	.029	.037	.054
135								
BODY								
150	.050	.008	-.020	-.044	-.065	-.077	-.102	-.116
165	.050	.009	-.019	-.045	-.065	-.079	-.101	-.115
180	.050	.008	-.020	-.046	-.066	-.081	-.102	-.115
195	.051	.010	-.019	-.043	-.064	-.077	-.099	-.112
210	.055	.012	-.019	-.043	-.063	-.075	-.098	-.112
225								
240								
255	.001	.011	.021	.030	.036	.033	.047	.066
270	.001	.014	.024	.036	.043	.041	.053	.075
285	.000	.014	.020	.030	.038	.031	.037	.052
300	-.003	.012	.019	.024	.022	-.010	-.006	.019
315	-.003	.013	.021	.022	.013	.018	.056	.097
330	-.002	.014	.023	.028	.032	.066	.118	.174
345	.004	.015	.027	.038	.056	.101	.164	.233
Y/S	CP FOR ALPHA, DEG =							
	-3.98	.01	4.02	8.02	11.99	16.02	20.04	23.95
.190								
.274	.001	.011	.025	.034	.032	.025	.037	.057
.379	-.004	.004	.021	.032	.005	-.017	-.006	.014
.473	.005	.010	.028	.049	.075	.076	.072	.087
WINDWARD								
WING								
.569	-.045	.005	.023	.046	.084	.122	.168	.200
.664	-.067	.007	.026	.048	.079	.110	.154	.210
.759	-.074	.005	.026	.046	.071	.096	.127	.174
.806	-.072	.005	.029	.047	.069	.090	.117	.160
.854	-.071	-.011	.031	.048	.066	.081	.106	.144
.854	.067	.010	-.059	-.095	-.121	-.137	-.145	-.147
.806	.063	.015	-.061	-.097	-.121	-.138	-.145	-.148
.759	.057	.012	-.070	-.108	-.128	-.144	-.151	-.153
LEEWARD								
WING								
.664	.055	.011	-.037	-.116	-.134	-.146	-.150	-.149
.569	.052	.009	-.016	-.058	-.111	-.134	-.138	-.142
.473	.055	.012	-.016	-.039	-.059	-.097	-.113	-.126
.379	.052	.009	-.020	-.043	-.058	-.075	-.101	-.115
.274	.056	.014	-.016	-.039	-.059	-.071	-.097	-.111
.190								

Table 9. Configuration 7

(a) $M_\infty = 1.70$; station 1

	THETA, DEG	CP FOR ALPHA, DEG =							
		-3.52	.54	4.57	8.55	12.53	16.59	20.57	24.53
BODY	0	-.023	.011	.054	.112	.179	.267	.369	.476
	15	-.020	.012	.055	.113	.181	.269	.371	.480
	30	-.020	.011	.054	.112	.177	.262	.364	.471
	45								
	60	.016	-.007	-.033	-.071	-.162	-.260	-.355	-.394
	75	.018	-.001	-.027	-.057	-.075	-.082	-.140	-.166
	90	.013	.000	-.023	-.057	-.075	-.074	-.138	-.171
	105	.008	.000	-.019	-.046	-.059	-.088	-.116	-.137
	120	.007	.001	-.014	-.037	-.059	-.103	-.111	-.126
	135	.002	-.005	-.015	-.040	-.081	-.102	-.124	-.150
	150	.009	.002	-.006	-.040	-.114	-.144	-.117	-.150
	165	.007	.001	-.004	-.030	-.063	-.101	-.146	-.166
	180	.026	.026	.023	.020	.014	-.001	-.039	-.073
	195	.010	.006	.002	-.016	-.043	-.085	-.146	-.161
	210	.005	.001	-.007	-.044	-.130	-.199	-.125	-.165
	225	.008	.002	-.010	-.035	-.077	-.125	-.120	-.153
	240	.009	.000	-.016	-.038	-.064	-.136	-.124	-.130
	255	.017	.004	-.016	-.041	-.058	-.096	-.110	-.137
	270	.015	-.004	-.028	-.063	-.082	-.089	-.141	-.179
	285	.024	.003	-.026	-.060	-.082	-.077	-.125	-.156
	300	.017	-.007	-.037	-.066	-.110	-.193	-.287	-.348
315									
330	-.025	.010	.054	.113	.181	.269	.369	.478	
345	-.026	.008	.051	.109	.176	.266	.368	.476	
	Y/S	CP FOR ALPHA, DEG =							
		-3.52	.54	4.57	8.55	12.53	16.59	20.57	24.53
WINDWARD WING	.050								
	.100								
	.150								
	.200								
	.250								
	.300	-.024	.010	.057	.118	.189	.281	.385	.494
	.350	-.020	.013	.060	.121	.194	.285	.391	.500
	.400	-.029	.018	.069	.132	.207	.299	.406	.514
	.425	-.112	.010	.063	.126	.203	.293	.401	.510
	.450	-.110	.015	.072	.138	.215	.305	.412	.519
LEEWARD WING	.450	.030	-.009	-.155	-.227	-.292	-.347	-.379	-.397
	.425	.026	-.006	-.176	-.254	-.346	-.386	-.409	-.415
	.400	.025	-.007	-.153	-.258	-.341	-.382	-.409	-.416
	.350	.026	-.004	-.021	-.188	-.361	-.398	-.421	-.428
	.300	.024	-.003	-.028	-.070	-.156	-.203	-.300	-.351
	.250								
	.200								
	.150								
	.100								
	.050								

Table 9. Continued

(a) Continued; station 2

	THETA, DEG	CP FOR ALPHA, DEG =							
		-3.52	.54	4.57	8.55	12.53	16.59	20.57	24.53
BODY	0	-.038	.006	.055	.118	.196	.285	.387	.499
	15	-.048	-.005	.043	.108	.185	.272	.376	.487
	30	-.040	.005	.052	.117	.193	.283	.387	.497
	45								
	60	.011	-.002	-.016	-.025	-.088	-.207	-.309	-.378
	75								
	90								
	105	.000	-.010	-.029	-.042	-.065	-.071	-.112	-.145
	120	.006	-.002	-.021	-.035	-.054	-.061	-.097	-.129
	135	.003	-.004	-.023	-.040	-.056	-.066	-.094	-.121
	150	.004	-.005	-.023	-.054	-.059	-.072	-.092	-.117
	165	.012	.003	-.013	-.039	-.066	-.080	-.091	-.109
	180	.008	-.002	-.015	-.027	-.055	-.081	-.096	-.106
	195	.008	-.003	-.017	-.041	-.073	-.087	-.092	-.108
	210	.013	.002	-.014	-.055	-.062	-.068	-.078	-.103
	225	.011	.000	-.018	-.039	-.051	-.061	-.080	-.107
	240	.011	.001	-.017	-.034	-.051	-.059	-.087	-.109
	255	.006	-.005	-.024	-.040	-.059	-.070	-.098	-.121
	270	.004	-.009	-.029	-.048	-.066	-.079	-.117	-.136
	285	.008	-.006	-.026	-.039	-.063	-.119	-.202	-.289
	300	-.005	-.020	-.038	-.046	-.085	-.195	-.314	-.397
315									
330	-.041	.004	.053	.116	.194	.285	.386	.498	
345	-.045	.000	.049	.111	.190	.280	.382	.495	
	Y/S	CP FOR ALPHA, DEG =							
		-3.52	.54	4.57	8.55	12.53	16.59	20.57	24.53
WINDWARD WING	.075								
	.150								
	.225								
	.300	-.046	.000	.049	.113	.193	.286	.388	.501
	.375	-.035	.011	.060	.125	.204	.298	.400	.515
	.450	-.032	.013	.062	.129	.208	.302	.405	.520
	.524	-.034	.002	.051	.120	.198	.293	.397	.513
	.599	-.100	.012	.065	.135	.214	.309	.413	.530
	.637	-.131	.015	.071	.141	.220	.316	.420	.536
	.674	-.097	.018	.081	.149	.228	.326	.426	.541
LEEWARD WING	.674	.022	-.019	-.132	-.188	-.243	-.317	-.367	-.401
	.637	.016	-.015	-.153	-.209	-.252	-.318	-.372	-.411
	.599	.012	-.014	-.189	-.216	-.303	-.345	-.398	-.425
	.524	.012	-.009	-.058	-.268	-.298	-.347	-.402	-.429
	.450	.010	-.009	-.014	-.179	-.347	-.370	-.416	-.440
	.375	.017	-.001	-.013	-.027	-.192	-.299	-.356	-.395
	.300	.014	-.002	-.016	-.023	-.077	-.178	-.303	-.368
	.225								
.150									
.075									

Table 9. Continued

(a) Concluded; station 3

	THETA, DEG	CP FOR ALPHA, DEG =							
		-3.52	.54	4.57	8.55	12.53	16.59	20.57	24.53
BODY	0	-.042	-.002	.050	.116	.192	.281	.382	.490
	15	-.042	-.003	.050	.115	.191	.280	.380	.486
	30	-.059	-.013	.039	.103	.177	.264	.359	.459
	45								
	60								
	75	.013	-.001	-.020	-.031	-.070	-.190	-.291	-.338
	90	.008	-.004	-.023	-.039	-.058	-.086	-.166	-.177
	105	.013	.001	-.015	-.035	-.049	-.056	-.111	-.136
	120	.008	-.004	-.020	-.039	-.051	-.059	-.099	-.137
	135	.023	.008	-.007	-.025	-.034	-.044	-.074	-.115
	150	.016	-.001	-.017	-.038	-.044	-.053	-.076	-.120
	165	.011	-.003	-.020	-.042	-.051	-.056	-.075	-.109
	180	.014	.001	-.013	-.026	-.040	-.051	-.066	-.083
	195	.019	.005	-.009	-.030	-.039	-.048	-.058	-.088
	210	.016	.001	-.014	-.040	-.041	-.052	-.063	-.098
	225	.013	-.004	-.017	-.035	-.042	-.056	-.072	-.103
	240	.011	-.004	-.018	-.035	-.043	-.060	-.080	-.107
	255	.014	.000	-.016	-.033	-.045	-.061	-.091	-.111
	270	.001	-.014	-.033	-.050	-.063	-.093	-.153	-.155
	285	.009	-.007	-.026	-.037	-.060	-.166	-.277	-.328
	300	.001	-.016	-.028	-.037	-.071	-.162	-.280	-.360
	315								
	330	-.044	-.003	.049	.117	.192	.280	.383	.494
	345	-.046	-.006	.047	.114	.189	.278	.380	.491
	Y/S	CP FOR ALPHA, DEG =							
		-3.52	.54	4.57	8.55	12.53	16.59	20.57	24.53
WINDWARD WING	.190								
	.274	-.044	-.002	.050	.118	.195	.284	.387	.498
	.379	-.043	-.002	.051	.120	.196	.287	.391	.504
	.473	-.043	-.002	.050	.121	.197	.288	.392	.508
	.569	-.031	.008	.061	.133	.211	.302	.406	.523
	.664	-.020	.008	.063	.133	.212	.303	.408	.527
	.759	-.115	.011	.070	.141	.222	.313	.421	.537
	.806	-.126	.005	.067	.141	.221	.312	.422	.536
	.854	-.109	.001	.068	.145	.224	.314	.422	.535
LEEWARD WING	.854	.019	-.020	-.128	-.179	-.240	-.296	-.347	-.309
	.806	.018	-.014	-.138	-.189	-.233	-.296	-.348	-.324
	.759	.019	-.007	-.173	-.198	-.256	-.322	-.369	-.331
	.664	.015	-.008	-.107	-.232	-.278	-.336	-.384	-.341
	.569	.018	-.002	-.002	-.246	-.290	-.356	-.390	-.334
	.473	.015	-.004	-.017	-.065	-.288	-.378	-.410	-.350
	.379	.021	.002	-.012	-.023	-.110	-.219	-.280	-.312
	.274	.012	-.003	-.020	-.030	-.061	-.151	-.277	-.341
	.190								

Table 9. Continued

(b) $M_\infty = 2.16$; station 1

	THETA, DEG	CP FOR ALPHA, DEG =							
		-3.97	.00	4.03	8.04	11.99	16.05	20.03	24.03
BODY	0	-.026	.000	.035	.086	.152	.235	.335	.453
	15	-.025	.002	.038	.090	.155	.239	.338	.456
	30	-.031	-.002	.036	.087	.150	.230	.323	.436
	45								
	60	.009	-.008	-.034	-.067	-.127	-.172	-.201	-.221
	75	.010	-.005	-.030	-.061	-.092	-.095	-.090	-.075
	90	.005	-.005	-.027	-.059	-.071	-.107	-.125	-.128
	105	-.002	-.006	-.024	-.048	-.062	-.089	-.103	-.113
	120	-.008	-.008	-.021	-.041	-.072	-.097	-.103	-.105
	135	-.011	-.007	-.017	-.036	-.097	-.102	-.121	-.119
	150	-.011	-.008	-.014	-.039	-.144	-.105	-.125	-.133
	165	-.008	-.008	-.011	-.029	-.054	-.115	-.122	-.141
	180	.049	.035	.025	.021	.016	-.002	-.037	-.063
	195	-.009	-.007	-.009	-.023	-.036	-.107	-.117	-.139
	210	-.010	-.006	-.010	-.039	-.138	-.117	-.125	-.146
	225	-.011	-.005	-.014	-.035	-.104	-.104	-.123	-.128
	240	-.008	-.005	-.019	-.039	-.080	-.101	-.106	-.110
	255	.001	-.003	-.023	-.046	-.065	-.092	-.098	-.115
	270	.012	.000	-.025	-.059	-.068	-.098	-.118	-.128
	285	.017	.001	-.027	-.064	-.095	-.107	-.096	-.073
	300	.013	-.003	-.031	-.065	-.095	-.117	-.131	-.153
315									
330	-.031	-.002	.035	.086	.150	.233	.330	.445	
345	-.030	-.002	.032	.084	.149	.234	.333	.450	
	Y/S	CP FOR ALPHA, DEG =							
		-3.97	.00	4.03	8.04	11.99	16.05	20.03	24.03
WINDWARD WING	.050								
	.100								
	.150								
	.200								
	.250								
	.300	-.032	-.003	.035	.089	.156	.244	.345	.463
	.350	-.029	-.004	.035	.089	.157	.246	.347	.466
	.400	-.078	-.005	.036	.092	.162	.253	.354	.473
	.425	-.119	-.004	.037	.095	.164	.258	.359	.477
	.450	-.105	-.011	.039	.099	.171	.265	.368	.487
LEEWARD WING	.450	.031	-.003	-.116	-.173	-.204	-.217	-.222	-.225
	.425	.028	-.005	-.125	-.186	-.214	-.232	-.238	-.238
	.400	.024	-.007	-.119	-.194	-.232	-.246	-.248	-.246
	.350	.022	-.005	-.024	-.194	-.233	-.249	-.254	-.255
	.300	.018	-.005	-.030	-.068	-.155	-.179	-.189	-.190
	.250								
	.200								
	.150								
.100									
.050									

Table 9. Continued

(b) Continued; station 2

THETA, DEG	CP FOR ALPHA, DEG =							
	-3.97	.00	4.03	8.04	11.99	16.05	20.03	24.03
0	-.041	-.006	.039	.097	.166	.258	.356	.469
15	-.044	-.007	.038	.095	.165	.255	.351	.464
30	-.045	-.008	.038	.095	.166	.259	.356	.470
45								
60	.003	-.009	-.027	-.033	-.083	-.166	-.211	-.233
75								
90								
105	.004	-.005	-.019	-.032	-.061	-.067	-.090	-.103
120	.002	-.006	-.022	-.034	-.065	-.066	-.084	-.095
135	.005	-.004	-.020	-.036	-.050	-.060	-.078	-.086
150	.005	-.005	-.020	-.051	-.065	-.060	-.077	-.081
165	.007	-.005	-.017	-.041	-.062	-.069	-.080	-.082
180	.009	-.004	-.013	-.024	-.037	-.065	-.073	-.073
195	.009	-.004	-.014	-.035	-.053	-.069	-.075	-.081
210	.007	-.005	-.018	-.058	-.085	-.063	-.074	-.080
225	.006	-.004	-.020	-.041	-.053	-.064	-.076	-.081
240	.003	-.007	-.023	-.037	-.067	-.068	-.083	-.087
255	.006	-.005	-.022	-.036	-.061	-.068	-.089	-.104
270	.002	-.012	-.030	-.045	-.062	-.075	-.096	-.100
285	.004	-.011	-.029	-.041	-.054	-.077	-.086	-.168
300	.005	-.009	-.026	-.035	-.067	-.163	-.204	-.222
315								
330	-.040	-.005	.041	.096	.165	.258	.353	.471
345	-.040	-.004	.041	.098	.167	.260	.357	.472
Y/S	CP FOR ALPHA, DEG =							
	-3.97	.00	4.03	8.04	11.99	16.05	20.03	24.03
.075								
.150								
.225								
.300	-.038	-.003	.045	.101	.170	.264	.361	.481
.375	-.038	-.005	.044	.100	.169	.264	.361	.482
.450	-.036	-.005	.044	.103	.172	.266	.363	.485
.524	-.027	-.002	.048	.110	.179	.274	.373	.494
.599	-.121	-.003	.049	.114	.183	.278	.378	.498
.637	-.117	-.003	.052	.119	.189	.286	.386	.505
.674	-.101	-.004	.056	.124	.196	.293	.393	.511
.674	.025	-.005	-.106	-.153	-.192	-.224	-.238	-.246
.637	.024	-.002	-.110	-.152	-.193	-.223	-.236	-.243
.599	.020	-.003	-.120	-.162	-.197	-.225	-.238	-.246
.524	.015	-.006	-.072	-.188	-.207	-.232	-.244	-.251
.450	.010	-.009	-.010	-.177	-.223	-.242	-.250	-.255
.375	.011	-.008	-.023	-.040	-.185	-.241	-.254	-.260
.300	.009	-.008	-.026	-.030	-.070	-.148	-.197	-.217
.225								
.150								
.075								

Table 9. Continued
 (b) Concluded; station 3

THETA, DEG	CP FOR ALPHA, DEG =							
	-3.97	.00	4.03	8.04	11.99	16.05	20.03	24.03
0	-.045	-.013	.034	.092	.163	.255	.353	.471
15	-.045	-.012	.035	.093	.164	.254	.353	.471
30	-.048	-.012	.034	.094	.165	.252	.355	.469
45								
60								
75	.010	-.002	-.017	-.026	-.059	-.108	-.131	-.217
90	.011	-.002	-.018	-.029	-.043	-.066	-.072	-.046
105	.009	-.003	-.017	-.031	-.042	-.063	-.072	-.085
120	.006	-.005	-.018	-.031	-.038	-.060	-.071	-.071
135	.008	-.003	-.016	-.030	-.035	-.056	-.070	-.073
BODY 150	.010	-.003	-.016	-.035	-.038	-.051	-.066	-.075
165	.014	-.003	-.014	-.034	-.045	-.050	-.060	-.072
180	.014	-.004	-.013	-.022	-.041	-.051	-.053	-.053
195	.014	-.001	-.013	-.027	-.044	-.049	-.055	-.059
210	.009	-.004	-.018	-.043	-.044	-.052	-.061	-.064
225	.011	-.003	-.017	-.029	-.036	-.051	-.059	-.063
240	.010	-.004	-.018	-.028	-.039	-.055	-.062	-.067
255	.012	-.003	-.019	-.028	-.042	-.059	-.072	-.088
270	.010	-.005	-.023	-.034	-.049	-.065	-.071	-.095
285	.008	-.006	-.024	-.032	-.051	-.097	-.150	-.216
300	.007	-.008	-.024	-.029	-.054	-.143	-.209	-.235
315								
330	-.047	-.012	.033	.093	.164	.252	.352	.472
345	-.046	-.011	.035	.094	.164	.255	.354	.473
Y/S	CP FOR ALPHA, DEG =							
	-3.97	.00	4.03	8.04	11.99	16.05	20.03	24.03
.190								
.274	-.044	-.008	.036	.097	.169	.257	.359	.479
.379	-.045	-.010	.036	.095	.168	.261	.359	.483
.473	-.042	-.008	.040	.098	.171	.265	.364	.489
WINDWARD 569	-.040	-.009	.039	.097	.171	.265	.363	.486
WING 664	-.036	-.009	.042	.100	.175	.269	.371	.491
.759	-.130	-.009	.045	.106	.181	.276	.379	.498
.806	-.113	-.007	.049	.111	.188	.283	.387	.505
.854	-.102	-.006	.052	.118	.194	.291	.395	.513
.854	.022	-.005	-.099	-.142	-.173	-.216	-.236	-.238
.806	.020	-.005	-.101	-.142	-.176	-.217	-.236	-.242
.759	.016	-.007	-.111	-.151	-.185	-.220	-.238	-.246
LEEWARD 664	.015	-.005	-.095	-.174	-.196	-.222	-.237	-.247
WING 569	.014	-.006	-.005	-.197	-.226	-.238	-.249	-.257
.473	.016	-.004	-.014	-.065	-.224	-.255	-.259	-.261
.379	.014	-.005	-.018	-.023	-.119	-.203	-.233	-.251
.274	.013	-.002	-.017	-.023	-.058	-.136	-.200	-.222
.190								

Table 9. Continued

(c) $M_\infty = 2.40$; station 1

	THETA, DEG	CP FOR ALPHA, DEG =							
		-3.92	.04	3.97	8.04	12.00	16.09	20.06	24.04
BODY	0	-.017	.008	.039	.087	.153	.243	.336	.457
	15	-.017	.009	.042	.090	.157	.247	.340	.460
	30	-.021	.006	.041	.088	.154	.239	.330	.445
	45								
	60	.017	.000	-.026	-.060	-.086	-.122	-.136	-.158
	75	.019	.003	-.023	-.057	-.075	-.070	-.056	-.040
	90	.015	.002	-.021	-.053	-.072	-.101	-.108	-.101
	105	.005	.001	-.020	-.042	-.057	-.085	-.097	-.110
	120	-.003	-.002	-.017	-.035	-.064	-.084	-.093	-.106
	135	-.004	-.002	-.010	-.032	-.099	-.100	-.110	-.116
	150	-.003	-.002	-.006	-.032	-.113	-.103	-.115	-.124
	165	.000	-.002	-.002	-.024	-.054	-.106	-.114	-.131
	180	.010	.007	.005	.004	-.002	-.046	-.075	-.084
	195	.000	.000	.001	-.014	-.029	-.099	-.110	-.126
	210	-.005	.000	-.004	-.032	-.118	-.110	-.124	-.136
	225	-.006	.000	-.006	-.029	-.102	-.104	-.115	-.124
	240	-.005	-.001	-.012	-.034	-.076	-.095	-.101	-.114
	255	.006	.002	-.015	-.038	-.058	-.086	-.094	-.112
	270	.015	.002	-.021	-.056	-.067	-.102	-.111	-.129
	285	.021	.005	-.021	-.062	-.088	-.088	-.069	-.050
	300	.017	.000	-.026	-.059	-.074	-.080	-.087	-.105
	315								
	330	-.022	.007	.038	.086	.153	.240	.332	.451
345	-.021	.005	.036	.085	.151	.240	.336	.456	
	Y/S	CP FOR ALPHA, DEG =							
		-3.92	.04	3.97	8.04	12.00	16.09	20.06	24.04
WINDWARD WING	.050								
	.100								
	.150								
	.200								
	.250								
	.300	-.022	.006	.038	.088	.159	.252	.349	.474
	.350	-.022	.004	.036	.087	.159	.254	.351	.477
	.400	-.066	.006	.038	.089	.161	.259	.359	.488
	.425	-.091	.006	.038	.090	.162	.260	.360	.489
	.450	-.084	-.004	.042	.097	.168	.267	.370	.501
LEEWARD WING	.450	.039	-.002	-.096	-.142	-.158	-.168	-.170	-.170
	.425	.034	.003	-.103	-.149	-.164	-.177	-.181	-.183
	.400	.031	.002	-.096	-.157	-.179	-.190	-.190	-.189
	.350	.031	.004	-.025	-.162	-.180	-.193	-.194	-.196
	.300	.027	.003	-.022	-.063	-.117	-.137	-.138	-.142
	.250								
	.200								
	.150								
	.100								
	.050								

Table 9. Continued

(c) Continued; station 2

	THETA, DEG	CP FOR ALPHA, DEG =							
		-3.92	.04	3.97	8.04	12.00	16.09	20.06	24.04
BODY	0	-.027	.005	.045	.103	.176	.270	.363	.492
	15	-.030	.003	.043	.100	.171	.262	.354	.481
	30	-.030	.004	.045	.103	.175	.270	.364	.494
	45								
	60	.018	.004	-.012	-.025	-.081	-.143	-.162	-.171
	75								
	90								
	105	.015	.004	-.012	-.027	-.056	-.072	-.091	-.108
	120	.013	.003	-.010	-.026	-.054	-.066	-.082	-.093
	135	.013	.004	-.009	-.029	-.047	-.062	-.077	-.088
	150	.013	.003	-.009	-.042	-.048	-.060	-.076	-.086
	165	.015	.005	-.006	-.032	-.056	-.063	-.074	-.083
	180	.015	.005	-.004	-.013	-.038	-.059	-.073	-.069
	195	.015	.005	-.004	-.024	-.049	-.066	-.074	-.082
	210	.013	.005	-.007	-.045	-.066	-.064	-.072	-.081
	225	.013	.006	-.008	-.032	-.046	-.066	-.075	-.085
	240	.011	.003	-.012	-.029	-.057	-.068	-.080	-.096
	255	.014	.003	-.013	-.028	-.055	-.070	-.089	-.108
	270	.010	-.002	-.020	-.035	-.056	-.076	-.086	-.081
	285	.012	-.002	-.019	-.033	-.048	-.063	-.068	-.113
300	.013	-.002	-.017	-.032	-.082	-.148	-.161	-.171	
315									
330	-.026	.005	.047	.105	.175	.270	.363	.491	
345	-.025	.007	.047	.104	.177	.271	.364	.493	
	Y/S	CP FOR ALPHA, DEG =							
		-3.92	.04	3.97	8.04	12.00	16.09	20.06	24.04
WINDWARD WING	.075								
	.150								
	.225								
	.300	-.025	.007	.048	.108	.179	.275	.368	.499
	.375	-.024	.008	.050	.110	.182	.279	.372	.504
	.450	-.022	.008	.051	.112	.185	.282	.377	.507
	.524	-.016	.009	.053	.113	.187	.286	.382	.511
	.599	-.092	.009	.056	.118	.192	.293	.392	.519
	.637	-.089	.010	.058	.122	.197	.299	.400	.526
	.674	-.079	.009	.062	.127	.204	.306	.408	.534
LEEWARD WING	.674	.039	.006	-.089	-.130	-.160	-.177	-.181	-.185
	.637	.035	.006	-.091	-.131	-.162	-.179	-.183	-.186
	.599	.033	.005	-.090	-.133	-.163	-.180	-.183	-.187
	.524	.031	.007	-.065	-.146	-.158	-.179	-.185	-.190
	.450	.027	.006	-.005	-.152	-.170	-.184	-.191	-.195
	.375	.027	.007	-.009	-.055	-.169	-.193	-.197	-.199
	.300	.023	.005	-.011	-.022	-.071	-.130	-.147	-.155
	.225								
	.150								
	.075								

Table 9. Continued

(c) Concluded; station 3

	THETA, DEG	CP FOR ALPHA, DEG =							
		-3.92	.04	3.97	8.04	12.00	16.09	20.06	24.04
	0	-.030	.003	.044	.100	.170	.268	.366	.492
	15	-.030	.004	.045	.101	.171	.268	.366	.492
	30	-.031	.004	.043	.099	.171	.266	.366	.490
	45								
	60								
	75	.019	.005	-.010	-.019	-.047	-.071	-.123	-.152
	90	.022	.007	-.008	-.019	-.036	-.053	-.058	-.055
	105	.019	.006	-.010	-.023	-.038	-.058	-.077	-.100
	120	.016	.004	-.011	-.026	-.035	-.055	-.067	-.086
	135	.020	.007	-.007	-.024	-.029	-.049	-.061	-.069
BODY	150	.019	.006	-.008	-.032	-.033	-.047	-.061	-.071
	165	.020	.006	-.006	-.032	-.041	-.045	-.060	-.078
	180	.019	.004	-.005	-.018	-.041	-.043	-.056	-.061
	195	.020	.006	-.005	-.023	-.043	-.043	-.053	-.065
	210	.015	.002	-.010	-.040	-.043	-.046	-.058	-.070
	225	.016	.004	-.009	-.028	-.035	-.047	-.060	-.066
	240	.015	.003	-.011	-.027	-.036	-.050	-.065	-.067
	255	.018	.005	-.010	-.025	-.037	-.057	-.079	-.090
	270	.015	.001	-.014	-.029	-.042	-.054	-.054	-.091
	285	.015	.001	-.014	-.026	-.047	-.073	-.134	-.155
	300	.013	-.001	-.014	-.026	-.064	-.143	-.168	-.182
	315								
	330	-.030	.003	.044	.101	.171	.269	.365	.490
	345	-.030	.003	.044	.101	.171	.268	.366	.492
	Y/S	CP FOR ALPHA, DEG =							
		-3.92	.04	3.97	8.04	12.00	16.09	20.06	24.04
	.190								
	.274	-.027	.006	.047	.104	.175	.274	.369	.496
	.379	-.029	.004	.046	.104	.176	.275	.371	.499
	.473	-.026	.007	.048	.107	.180	.277	.375	.503
WINDWARD	.569	-.024	.005	.049	.108	.183	.279	.378	.507
WING	.664	-.025	.005	.050	.111	.187	.282	.384	.515
	.759	-.096	.006	.053	.117	.194	.292	.392	.522
	.806	-.086	.007	.057	.121	.198	.298	.398	.527
	.854	-.076	.006	.060	.127	.204	.304	.404	.533
	.854	.033	.004	-.083	-.119	-.151	-.178	-.185	-.181
	.806	.031	.005	-.084	-.119	-.152	-.178	-.188	-.185
	.759	.028	.004	-.085	-.123	-.154	-.179	-.188	-.187
LEEWARD	.664	.024	.004	-.070	-.139	-.154	-.175	-.185	-.189
WING	.569	.020	.002	-.014	-.150	-.164	-.180	-.189	-.194
	.473	.022	.002	-.007	-.089	-.175	-.188	-.195	-.199
	.379	.021	.002	-.010	-.017	-.134	-.180	-.190	-.196
	.274	.021	.004	-.009	-.018	-.051	-.132	-.160	-.169
	.190								

Table 9. Continued

(d) $M_\infty = 2.86$; station 1

THETA, DEG	CP FOR ALPHA, DEG =							
	-3.97	.02	4.05	8.04	11.99	16.03	19.99	23.98
0	-.009	.010	.040	.087	.149	.222	.315	.420
15	-.008	.012	.043	.090	.151	.225	.319	.427
30	-.012	.010	.041	.086	.144	.215	.307	.413
45								
60	.016	.003	-.019	-.042	-.050	-.060	-.071	-.079
75	.016	.005	-.017	-.047	-.051	-.043	-.027	-.011
90	.012	.005	-.016	-.056	-.068	-.079	-.078	-.068
105	.003	.003	-.015	-.041	-.055	-.072	-.078	-.090
120	-.005	.001	-.012	-.033	-.058	-.070	-.077	-.089
135	-.003	.002	-.007	-.028	-.074	-.080	-.086	-.091
BODY 150	.002	.002	-.003	-.027	-.076	-.085	-.091	-.097
165	.006	.001	.000	-.020	-.047	-.082	-.090	-.098
180	.065	.028	.021	.014	.008	-.010	-.036	-.049
195	.005	.001	.001	-.012	-.034	-.076	-.088	-.097
210	.001	.002	-.001	-.025	-.079	-.086	-.095	-.099
225	-.003	.003	-.004	-.025	-.073	-.084	-.091	-.094
240	-.005	.003	-.009	-.030	-.059	-.075	-.083	-.091
255	.005	.006	-.012	-.035	-.054	-.071	-.080	-.089
270	.015	.007	-.016	-.052	-.063	-.077	-.088	-.087
285	.022	.011	-.015	-.055	-.064	-.057	-.041	-.020
300	.019	.008	-.019	-.043	-.042	-.034	-.027	-.024
315								
330	-.016	.007	.037	.082	.141	.211	.304	.406
345	-.012	.008	.038	.085	.145	.217	.310	.414
Y/S	CP FOR ALPHA, DEG =							
	-3.97	.02	4.05	8.04	11.99	16.03	19.99	23.98
.050								
.100								
.150								
.200								
WINDWARD .250								
WING .300	-.016	.006	.035	.082	.142	.216	.315	.421
.350	-.014	.006	.035	.081	.142	.215	.315	.423
.400	-.065	.003	.036	.084	.145	.218	.316	.426
.425	-.064	-.001	.041	.089	.152	.225	.321	.430
.450	-.065	-.007	.041	.094	.159	.235	.330	.440
.450	.038	.002	-.068	-.097	-.107	-.111	-.111	-.111
.425	.035	.005	-.070	-.100	-.111	-.115	-.116	-.116
.400	.031	.004	-.074	-.105	-.116	-.121	-.124	-.123
.350	.029	.005	-.021	-.111	-.122	-.126	-.126	-.127
LEEWARD .300	.025	.006	-.015	-.046	-.081	-.091	-.090	-.088
.250								
.200								
.150								
.100								
.050								

Table 9. Continued

(d) Continued: station 2

THETA, DEG	CP FOR ALPHA, DEG =							
	-3.97	.02	4.05	8.04	11.99	16.03	19.99	23.98
0	-.011	.013	.049	.104	.172	.254	.359	.472
15	-.014	.012	.047	.102	.168	.247	.350	.460
30	-.016	.010	.046	.102	.170	.252	.360	.473
45								
60	.023	.007	-.009	-.028	-.062	-.089	-.102	-.107
75								
90								
105	.019	.010	-.007	-.022	-.042	-.057	-.073	-.082
120	.014	.007	-.007	-.023	-.042	-.055	-.065	-.079
135	.013	.008	-.004	-.025	-.039	-.051	-.061	-.072
150	.011	.007	-.004	-.036	-.040	-.053	-.063	-.074
165	.012	.007	-.003	-.028	-.048	-.055	-.064	-.074
180	.013	.007	.000	-.005	-.037	-.053	-.063	-.064
195	.014	.008	.000	-.016	-.045	-.056	-.067	-.072
210	.014	.007	-.003	-.039	-.047	-.057	-.068	-.074
225	.015	.008	-.004	-.028	-.043	-.057	-.067	-.076
240	.014	.005	-.008	-.026	-.045	-.056	-.072	-.083
255	.018	.007	-.009	-.024	-.043	-.057	-.077	-.087
270	.016	.002	-.015	-.024	-.043	-.057	-.077	-.087
285	.018	.004	-.015	-.031	-.049	-.064	-.067	-.051
300	.022	.005	-.012	-.031	-.039	-.036	-.027	-.038
315								
330	-.010	.013	.051	.107	.173	.256	.360	.473
345	-.007	.015	.052	.107	.174	.257	.362	.474
Y/S	CP FOR ALPHA, DEG =							
	-3.97	.02	4.05	8.04	11.99	16.03	19.99	23.98
.075								
.150								
.225								
.300	-.007	.015	.054	.111	.179	.263	.367	.482
.375	-.007	.015	.054	.110	.179	.263	.368	.483
.450	-.006	.017	.054	.111	.181	.265	.372	.488
.524	-.014	.023	.059	.116	.187	.273	.378	.497
.599	-.064	.022	.059	.119	.190	.278	.384	.505
.637	-.060	.020	.060	.122	.195	.284	.392	.515
.674	-.057	.005	.064	.127	.202	.292	.401	.526
.674	.042	.004	-.068	-.098	-.110	-.117	-.120	-.120
.637	.039	.014	-.067	-.098	-.109	-.116	-.119	-.120
.599	.036	.013	-.071	-.098	-.109	-.117	-.121	-.121
.524	.035	.013	-.053	-.096	-.105	-.112	-.118	-.121
.450	.032	.011	-.013	-.100	-.110	-.116	-.121	-.123
.375	.031	.009	-.006	-.078	-.120	-.127	-.130	-.132
.300	.027	.007	-.009	-.029	-.064	-.083	-.090	-.095
.225								
.150								
.075								

Table 9. Concluded

(d) Concluded; station 3

THETA, DEG	CP FOR ALPHA, DEG =							
	-3.97	.02	4.05	8.04	11.99	16.03	19.99	23.98
0	-.019	.017	.057	.110	.178	.264	.371	.490
15	-.019	.018	.060	.112	.178	.265	.370	.490
30	-.019	.018	.063	.114	.179	.266	.373	.492
45								
60								
75	.021	.011	-.004	-.013	-.030	-.034	-.067	-.081
90	.025	.012	-.004	-.016	-.031	-.041	-.036	-.015
105	.022	.011	-.005	-.017	-.033	-.051	-.071	-.077
120	.019	.007	-.007	-.022	-.030	-.049	-.062	-.079
135	.019	.007	-.006	-.022	-.030	-.047	-.055	-.074
BODY 150	.018	.007	-.005	-.027	-.029	-.041	-.051	-.065
165	.019	.009	-.002	-.024	-.030	-.038	-.048	-.067
180	.018	.005	-.003	-.013	-.033	-.040	-.049	-.063
195	.019	.007	-.003	-.019	-.034	-.039	-.052	-.064
210	.016	.004	-.008	-.035	-.033	-.042	-.057	-.067
225	.018	.006	-.006	-.025	-.033	-.045	-.060	-.066
240	.018	.005	-.008	-.022	-.035	-.048	-.062	-.067
255	.020	.006	-.007	-.020	-.036	-.053	-.070	-.075
270	.021	.007	-.007	-.019	-.035	-.044	-.039	-.038
285	.015	.005	-.010	-.019	-.034	-.052	-.076	-.079
300	.018	.004	-.011	-.020	-.069	-.100	-.110	-.111
315								
330	-.020	.017	.060	.108	.179	.264	.370	.489
345	-.020	.018	.059	.110	.179	.266	.372	.492

Y/S	CP FOR ALPHA, DEG =							
	-3.97	.02	4.05	8.04	11.99	16.03	19.99	23.98
.190								
.274	-.016	.023	.063	.111	.183	.268	.375	.496
.379	-.019	.018	.061	.114	.183	.269	.378	.498
.473	-.016	.020	.061	.120	.185	.273	.384	.502
WINDWARD 569	-.014	.016	.059	.121	.188	.272	.384	.501
.664	-.035	.016	.062	.126	.198	.277	.391	.505
.759	-.069	.015	.064	.129	.205	.285	.399	.514
.806	-.061	.018	.068	.134	.212	.294	.406	.524
.854	-.059	.015	.071	.139	.220	.307	.414	.535
.854	.036	.002	-.070	-.097	-.110	-.118	-.121	-.117
.806	.033	.011	-.071	-.097	-.113	-.121	-.124	-.121
.759	.030	.010	-.073	-.100	-.113	-.123	-.125	-.123
.664	.029	.010	-.053	-.093	-.104	-.116	-.121	-.123
LEEWARD 569	.027	.008	-.026	-.092	-.105	-.114	-.120	-.125
.473	.030	.012	.001	-.093	-.111	-.119	-.124	-.127
.379	.026	.008	-.006	-.037	-.112	-.126	-.129	-.130
.274	.028	.013	-.003	-.013	-.050	-.089	-.100	-.103
.190								

Table 10. Configuration 8

(a) $M_\infty = 1.70$; station 1

THETA, DEG	CP FOR ALPHA, DEG =							
	-4.00	-.01	4.02	8.01	12.01	16.04	19.99	23.96
0	.030	.018	.016	.020	.033	.072	.126	.203
15	-.005	-.011	-.011	-.003	.008	.052	.116	.192
30	-.010	-.013	-.016	-.014	-.024	.002	.055	.117
45	-.012	-.013	-.019	-.034	-.063	-.070	-.037	.006
60	-.018	-.015	-.026	-.057	-.099	-.153	-.145	-.122
75	-.021	-.014	-.028	-.067	-.119	-.119	-.248	-.245
90	-.029	-.016	-.030	-.067	-.105	-.082	-.196	-.226
105	-.028	-.014	-.024	-.049	-.067	-.084	-.144	-.193
120	-.027	-.017	-.024	-.039	-.060	-.103	-.134	-.194
135	-.016	-.014	-.017	-.031	-.062	-.100	-.122	-.174
150	-.011	-.013	-.014	-.034	-.088	-.153	-.117	-.164
165	-.009	-.013	-.014	-.030	-.068	-.098	-.145	-.166
180	-.010	-.013	-.012	-.010	-.026	-.058	-.132	-.141
195	-.011	-.013	-.012	-.023	-.050	-.086	-.146	-.157
210	-.012	-.012	-.013	-.033	-.104	-.175	-.119	-.162
225	-.017	-.013	-.016	-.030	-.063	-.095	-.120	-.169
240	-.024	-.015	-.022	-.035	-.057	-.107	-.132	-.178
255	-.022	-.012	-.021	-.043	-.059	-.089	-.134	-.175
270	-.021	-.011	-.023	-.058	-.094	-.085	-.162	-.193
285	-.017	-.012	-.026	-.064	-.116	-.119	-.257	-.260
300	-.015	-.012	-.024	-.057	-.102	-.163	-.163	-.144
315	-.012	-.012	-.022	-.040	-.071	-.082	-.057	-.020
330	-.009	-.010	-.015	-.018	-.031	-.005	.041	.097
345	-.007	-.010	-.010	-.005	.002	.047	.109	.181

Table 10. Continued

(a) Continued; station 2

THETA, DEG	CP FOR ALPHA, DEG =							
	-4.00	-.01	4.02	8.01	12.01	16.04	19.99	23.96
0	-.012	-.010	-.005	.009	.040	.078	.137	.206
15	-.012	-.008	-.005	.007	.031	.066	.115	.184
30	-.013	-.007	-.006	-.002	.004	.025	.052	.112
45	-.014	-.007	-.009	-.017	-.033	-.038	-.044	.000
60	-.017	-.007	-.012	-.032	-.072	-.112	-.154	-.127
75	-.020	-.006	-.015	-.044	-.098	-.172	-.219	-.238
90	-.021	-.004	-.014	-.039	-.086	-.115	-.113	-.145
105	-.019	-.003	-.012	-.025	-.050	-.070	-.103	-.136
120	-.021	-.009	-.016	-.024	-.047	-.072	-.115	-.148
135	-.015	-.007	-.012	-.020	-.043	-.059	-.120	-.154
150	-.010	-.006	-.011	-.026	-.044	-.061	-.124	-.163
165	-.007	-.007	-.010	-.029	-.059	-.078	-.126	-.168
180	-.008	-.008	-.008	-.013	-.043	-.074	-.112	-.143
195	-.009	-.009	-.011	-.026	-.056	-.079	-.122	-.155
210	-.010	-.008	-.011	-.035	-.051	-.064	-.120	-.152
225	-.013	-.007	-.012	-.023	-.042	-.056	-.118	-.143
240	-.019	-.007	-.012	-.023	-.043	-.064	-.111	-.137
255	-.023	-.008	-.015	-.031	-.048	-.066	-.099	-.136
270	-.024	-.008	-.017	-.044	-.077	-.093	-.102	-.138
285	-.024	-.010	-.020	-.051	-.099	-.171	-.199	-.222
300	-.019	-.008	-.017	-.042	-.081	-.126	-.175	-.154
315	-.018	-.010	-.016	-.029	-.049	-.056	-.068	-.030
330	-.017	-.011	-.012	-.013	-.008	.009	.033	.086
345	-.013	-.008	-.005	.005	.028	.060	.110	.174

Table 10. Continued

(a) Concluded; station 3

THETA, DEG	CP FOR ALPHA, DEG =							
	-4.00	-.01	4.02	8.01	12.01	16.04	19.99	23.96
0	-.007	-.008	-.002	.010	.033	.067	.122	.198
15	-.008	-.004	.000	.007	.028	.056	.107	.179
30	-.012	-.007	-.007	-.007	.000	.013	.043	.102
45	-.013	-.009	-.012	-.022	-.034	-.051	-.049	-.011
60	-.016	-.009	-.017	-.039	-.062	-.099	-.149	-.138
75	-.017	-.006	-.016	-.046	-.077	-.128	-.170	-.234
90	-.019	-.006	-.019	-.047	-.077	-.103	-.120	-.156
105	-.016	-.005	-.014	-.033	-.049	-.060	-.081	-.135
120	-.013	-.008	-.014	-.028	-.046	-.060	-.084	-.134
135	-.004	-.005	-.012	-.024	-.042	-.063	-.087	-.132
150	-.001	-.004	-.011	-.026	-.039	-.063	-.093	-.134
165	-.001	-.004	-.012	-.033	-.042	-.062	-.105	-.144
180	.001	-.002	-.007	-.015	-.027	-.054	-.092	-.112
195	.001	-.001	-.007	-.024	-.034	-.054	-.091	-.110
210	-.001	-.004	-.009	-.028	-.038	-.061	-.089	-.118
225	-.008	-.007	-.011	-.024	-.039	-.062	-.085	-.115
240	-.016	-.009	-.013	-.025	-.040	-.056	-.079	-.111
255	-.019	-.009	-.017	-.028	-.041	-.060	-.081	-.115
270								
285	-.017	-.009	-.017	-.042	-.077	-.129	-.181	-.209
300	-.018	-.012	-.020	-.041	-.064	-.110	-.166	-.161
315	-.012	-.006	-.010	-.021	-.031	-.053	-.061	-.027
330	-.013	-.009	-.011	-.009	-.005	.004	.029	.085
345	-.011	-.009	-.006	.003	.020	.048	.094	.166

Table 10. Continued

(b) $M_N = 2.16$; station 1

THETA, DEG	CP FOR ALPHA, DEG =							
	-3.97	.01	3.99	8.20	12.02	16.00	20.04	23.98
0	.000	.004	.006	.016	.043	.077	.141	.211
15	-.006	-.006	-.005	-.007	.040	.087	.157	.231
30	-.005	-.003	-.003	-.001	.019	.057	.112	.176
45	-.008	-.003	-.007	-.001	-.022	.003	.040	.087
60	-.014	-.005	-.013	-.002	-.072	-.063	-.044	-.012
75	-.020	-.007	-.018	-.006	-.121	-.130	-.125	-.108
90	-.018	-.003	-.012	-.049	-.076	-.114	-.125	-.130
105	-.018	-.003	-.010	-.036	-.052	-.087	-.109	-.119
120	-.017	-.004	-.008	-.024	-.052	-.086	-.110	-.116
135	-.008	.000	-.002	-.016	-.076	-.082	-.106	-.112
150	-.007	-.003	-.004	-.021	-.123	-.083	-.109	-.118
165	-.005	-.005	-.004	-.019	-.047	-.103	-.112	-.125
180	-.004	-.004	-.002	-.002	-.006	-.070	-.091	-.103
195	-.005	-.003	-.001	-.009	-.024	-.092	-.101	-.116
210	-.008	-.003	-.003	-.025	-.123	-.090	-.103	-.118
225	-.012	-.003	-.005	-.020	-.084	-.082	-.105	-.114
240	-.019	-.006	-.011	-.025	-.061	-.084	-.108	-.114
255	-.020	-.004	-.013	-.033	-.051	-.085	-.104	-.116
270	-.018	-.004	-.014	-.048	-.062	-.100	-.117	-.123
285	-.018	-.006	-.018	-.058	-.121	-.140	-.135	-.124
300	-.013	-.007	-.016	-.051	-.085	-.081	-.057	-.032
315	-.008	-.004	-.010	-.030	-.033	-.016	.028	.068
330	-.007	-.005	-.008	-.011	.007	.041	.099	.158
345	-.004	-.004	-.007	.007	.040	.085	.157	.228

Table 10. Continued

(b) Continued: station 2

THETA, DEG	CP FOR ALPHA, DEG =							
	-3.97	.01	3.99	8.00	12.02	16.00	20.04	23.98
0	-.006	-.004	.002	.013	.043	.096	.163	.236
15	-.006	-.002	.003	.012	.038	.086	.148	.218
30	-.010	-.004	-.003	-.004	.009	.045	.097	.154
45	-.011	-.003	-.006	-.015	-.031	-.007	.029	.070
60	-.016	-.007	-.015	-.031	-.079	-.077	-.057	-.032
75	-.018	-.006	-.014	-.042	-.074	-.133	-.134	-.122
90	-.023	-.009	-.016	-.042	-.073	-.086	-.113	-.129
105	-.020	-.006	-.012	-.028	-.054	-.073	-.101	-.117
120	-.012	-.001	-.006	-.015	-.046	-.068	-.092	-.105
135	-.007	-.002	-.006	-.016	-.035	-.071	-.096	-.108
150	-.004	-.004	-.008	-.027	-.040	-.073	-.102	-.115
165	.002	-.001	-.002	-.023	-.043	-.075	-.103	-.114
180	.000	-.004	-.002	-.007	-.027	-.067	-.086	-.090
195	.001	-.001	.000	-.013	-.038	-.070	-.090	-.104
210	-.005	-.004	-.005	-.033	-.045	-.072	-.099	-.118
225	-.014	-.008	-.012	-.025	-.035	-.076	-.099	-.115
240	-.016	-.005	-.009	-.020	-.048	-.071	-.092	-.107
255	-.021	-.006	-.011	-.024	-.048	-.069	-.094	-.110
270	-.018	-.004	-.010	-.034	-.057	-.074	-.099	-.114
285	-.012	.000	-.009	-.039	-.066	-.119	-.136	-.130
300	-.012	-.004	-.011	-.036	-.075	-.089	-.070	-.045
315	-.008	-.002	-.005	-.021	-.041	-.020	.015	.056
330	-.008	-.003	-.003	-.006	.000	.038	.089	.143
345	-.008	-.004	-.001	.007	.029	.078	.139	.207

Table 10. Continued

(b) Concluded: station 3

THETA, DEG	CP FOR ALPHA, DEG =							
	-3.97	.01	3.99	8.00	12.02	16.00	20.04	23.98
0	-.007	-.007	.001	.014	.034	.085	.150	.229
15	-.008	-.007	-.002	.010	.028	.076	.139	.214
30	-.015	-.011	-.010	-.005	.006	.031	.085	.154
45	-.012	-.008	-.009	-.016	-.023	-.023	.017	.068
60	-.014	-.007	-.012	-.030	-.062	-.088	-.063	-.032
75	-.016	-.006	-.014	-.040	-.084	-.122	-.138	-.125
90	-.017	-.005	-.013	-.037	-.058	-.068	-.109	-.131
105	-.019	-.007	-.014	-.027	-.041	-.059	-.089	-.094
120	-.016	-.007	-.011	-.022	-.038	-.060	-.088	-.092
135	-.011	-.007	-.009	-.019	-.035	-.068	-.091	-.096
150	-.006	-.007	-.008	-.021	-.037	-.069	-.092	-.098
165	.002	-.005	-.005	-.026	-.043	-.071	-.092	-.107
180	.001	-.006	-.004	-.010	-.038	-.059	-.069	-.070
195	.000	-.003	-.003	-.016	-.038	-.063	-.078	-.098
210	-.002	-.001	-.004	-.020	-.031	-.062	-.083	-.101
225	-.007	-.004	-.006	-.016	-.031	-.061	-.080	-.096
240	-.013	-.006	-.010	-.018	-.033	-.059	-.082	-.100
255	-.015	-.004	-.011	-.020	-.034	-.055	-.083	-.099
270								
285	-.015	-.005	-.013	-.037	-.076	-.108	-.136	-.135
300	-.013	-.006	-.013	-.033	-.064	-.099	-.078	-.048
315	-.013	-.006	-.010	-.021	-.028	-.034	.002	.051
330	-.011	-.005	-.005	-.004	.006	.026	.078	.141
345	-.007	-.004	.002	.010	.027	.072	.133	.205

Table 10. Continued

(c) $M_{\infty} = 2.40$; station 1

THETA, DEG	CP FOR ALPHA, DEG =							
	-4.00	.01	3.97	8.01	11.99	15.99	19.99	24.01
0	-.001	-.001	.000	.010	.040	.077	.116	.190
15	-.004	-.004	-.003	.015	.051	.103	.170	.247
30	-.006	-.003	-.004	.002	.030	.073	.128	.192
45	-.009	-.004	-.008	-.019	-.007	.022	.059	.105
60	-.015	-.006	-.015	-.047	-.053	-.041	-.020	.008
75	-.019	-.006	-.018	-.067	-.098	-.100	-.094	-.080
90	-.022	-.006	-.018	-.060	-.088	-.111	-.121	-.137
105	-.021	-.005	-.016	-.040	-.058	-.093	-.109	-.122
120	-.019	-.007	-.014	-.030	-.058	-.092	-.111	-.123
135	-.009	-.004	-.007	-.024	-.093	-.091	-.109	-.121
150	-.007	-.006	-.007	-.029	-.109	-.095	-.113	-.128
165	-.006	-.008	-.005	-.025	-.055	-.107	-.116	-.131
180	-.005	-.007	-.004	-.004	-.017	-.081	-.098	-.110
195	-.006	-.006	-.003	-.014	-.032	-.097	-.108	-.125
210	-.009	-.006	-.004	-.030	-.114	-.098	-.112	-.129
225	-.015	-.006	-.007	-.025	-.093	-.095	-.110	-.124
240	-.022	-.008	-.013	-.030	-.066	-.094	-.109	-.123
255	-.021	-.006	-.013	-.035	-.055	-.091	-.106	-.120
270	-.020	-.005	-.016	-.054	-.070	-.103	-.113	-.128
285	-.018	-.006	-.018	-.067	-.107	-.115	-.106	-.094
300	-.014	-.007	-.018	-.055	-.068	-.060	-.036	-.011
315	-.009	-.005	-.014	-.029	-.022	.003	.043	.085
330	-.007	-.005	-.009	-.007	.016	.057	.113	.171
345	-.004	-.004	-.005	.011	.046	.098	.165	.241

Table 10. Continued

(c) Continued; station 2

THETA, DEG	CP FOR ALPHA, DEG =							
	-4.00	.01	3.97	8.01	11.99	15.99	19.99	24.01
0	-.006	-.007	-.004	.010	.046	.100	.170	.256
15	-.008	-.006	-.003	.007	.043	.093	.160	.239
30	-.011	-.006	-.007	-.005	.018	.057	.113	.179
45	-.011	-.006	-.009	-.021	-.018	.007	.049	.099
60	-.015	-.008	-.014	-.040	-.067	-.056	-.032	.001
75	-.017	-.006	-.014	-.048	-.104	-.112	-.104	-.086
90	-.021	-.008	-.018	-.045	-.080	-.099	-.119	-.132
105	-.020	-.006	-.015	-.030	-.060	-.083	-.110	-.120
120	-.016	-.004	-.010	-.023	-.054	-.079	-.104	-.116
135	-.011	-.004	-.009	-.023	-.050	-.082	-.105	-.117
150	-.006	-.006	-.009	-.033	-.050	-.084	-.107	-.122
165	-.002	-.005	-.006	-.031	-.054	-.088	-.108	-.123
180	-.003	-.007	-.007	-.011	-.044	-.074	-.096	-.094
195	-.004	-.005	-.006	-.021	-.051	-.083	-.102	-.112
210	-.009	-.006	-.008	-.039	-.053	-.088	-.105	-.122
225	-.016	-.008	-.012	-.029	-.049	-.087	-.107	-.120
240	-.019	-.007	-.011	-.025	-.055	-.082	-.103	-.114
255	-.022	-.007	-.013	-.027	-.054	-.081	-.103	-.115
270	-.020	-.007	-.015	-.040	-.065	-.090	-.109	-.120
285	-.016	-.006	-.016	-.048	-.095	-.118	-.114	-.100
300	-.014	-.008	-.016	-.046	-.082	-.073	-.045	-.018
315	-.011	-.007	-.013	-.030	-.035	-.010	.032	.077
330	-.011	-.008	-.010	-.013	.005	.044	.100	.165
345	-.008	-.008	-.007	.002	.035	.084	.151	.228

Table 10. Continued
(c) Concluded; station 3

THETA, DEG	CP FOR ALPHA, DEG =							
	-4.00	.01	3.97	8.01	11.99	15.99	19.99	24.01
0	-.005	-.005	-.002	.010	.036	.091	.165	.248
15	-.006	-.004	-.002	.008	.031	.082	.153	.234
30	-.011	-.007	-.007	-.006	.005	.045	.104	.171
45	-.010	-.005	-.008	-.019	-.029	-.002	.040	.090
60	-.011	-.005	-.012	-.037	-.072	-.062	-.036	-.003
75	-.013	-.005	-.014	-.046	-.089	-.116	-.107	-.089
90	-.014	-.004	-.014	-.042	-.067	-.087	-.111	-.120
105	-.014	-.004	-.013	-.030	-.048	-.074	-.098	-.111
120	-.012	-.005	-.011	-.027	-.047	-.074	-.096	-.110
135	-.008	-.004	-.009	-.025	-.045	-.077	-.099	-.115
150	-.003	-.003	-.007	-.028	-.046	-.078	-.102	-.120
165	.000	-.003	-.006	-.033	-.051	-.080	-.104	-.121
180	.001	-.003	-.005	-.017	-.048	-.066	-.084	-.089
195	.000	-.003	-.004	-.022	-.050	-.070	-.097	-.107
210	-.002	-.002	-.005	-.031	-.045	-.074	-.099	-.115
225	-.008	-.003	-.007	-.024	-.042	-.072	-.097	-.109
240	-.014	-.005	-.010	-.026	-.044	-.070	-.097	-.107
255	-.014	-.003	-.009	-.026	-.043	-.067	-.096	-.107
270								
285	-.011	-.004	-.014	-.044	-.083	-.110	-.118	-.104
300	-.010	-.005	-.014	-.041	-.084	-.077	-.051	-.023
315	-.008	-.004	-.009	-.025	-.044	-.016	.025	.071
330	-.008	-.004	-.006	-.009	-.004	.039	.094	.159
345	-.005	-.003	-.002	.006	.027	.079	.146	.225

Table 10. Continued

(d) $M_\infty = 2.86$; station 1

THETA, DEG	CP FOR ALPHA, DEG =							
	-4.00	-.06	4.00	7.99	11.98	16.02	20.01	23.98
0	.003	-.009	.006	.020	.049	.090	.147	.211
15	.004	.001	.007	.026	.063	.113	.169	.241
30	.002	.001	.005	.018	.046	.086	.135	.197
45	-.001	.000	.000	-.001	.014	.042	.078	.122
60	-.007	-.003	-.008	-.025	-.024	-.010	.012	.038
75	-.011	-.002	-.012	-.046	-.060	-.059	-.047	-.036
90	-.013	-.002	-.012	-.053	-.068	-.083	-.089	-.086
105	-.013	-.001	-.010	-.035	-.053	-.071	-.079	-.089
120	-.013	-.004	-.009	-.024	-.052	-.072	-.080	-.089
135	-.001	.000	-.001	-.015	-.064	-.068	-.077	-.086
150	.000	-.004	-.003	-.020	-.070	-.078	-.086	-.095
165	.001	-.007	-.004	-.019	-.046	-.081	-.090	-.097
180	.003	-.006	-.001	-.003	-.018	-.062	-.077	-.080
195	.004	-.005	.000	-.009	-.031	-.074	-.082	-.090
210	.001	-.005	-.002	-.020	-.072	-.079	-.086	-.094
225	-.004	-.003	-.003	-.018	-.066	-.075	-.082	-.089
240	-.013	-.005	-.010	-.025	-.054	-.074	-.082	-.091
255	-.013	-.002	-.009	-.030	-.051	-.071	-.078	-.087
270	-.013	.000	-.012	-.049	-.063	-.076	-.085	-.095
285	-.011	-.002	-.014	-.052	-.068	-.068	-.060	-.046
300	-.008	-.003	-.012	-.033	-.035	-.023	-.005	.023
315	-.002	.000	-.004	-.009	.005	.029	.062	.106
330	.000	-.001	.000	.009	.036	.074	.119	.179
345	.003	.000	.005	.023	.061	.108	.165	.238

Table 10. Continued

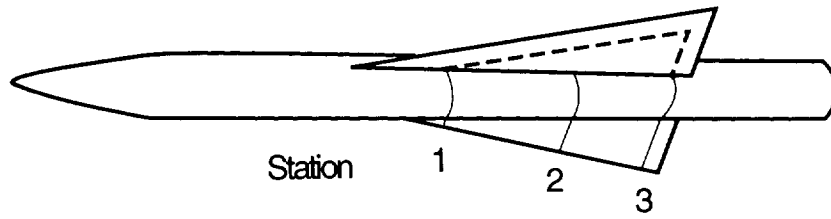
(d) Continued; station 2

THETA, DEG	CP FOR ALPHA, DEG =							
	-4.00	-.06	4.00	7.99	11.98	16.02	20.01	23.98
0	.007	.003	.007	.025	.066	.119	.179	.258
15	.006	.004	.007	.023	.061	.110	.170	.244
30	.002	.001	.002	.009	.037	.078	.128	.189
45	.001	.001	-.001	-.008	.006	.035	.073	.117
60	-.003	-.002	-.009	-.034	-.036	-.020	.004	.032
75	-.003	.000	-.010	-.046	-.070	-.067	-.053	-.040
90	-.011	-.004	-.016	-.043	-.072	-.081	-.098	-.101
105	-.013	-.004	-.013	-.029	-.056	-.073	-.087	-.096
120	-.007	-.001	-.004	-.017	-.045	-.063	-.076	-.086
135	-.005	-.001	-.003	-.018	-.045	-.067	-.080	-.089
150	-.002	-.003	-.004	-.026	-.047	-.071	-.084	-.094
165	.005	-.001	.000	-.021	-.047	-.069	-.082	-.091
180	.002	-.004	-.002	-.004	-.040	-.060	-.073	-.079
195	.003	-.002	.001	-.013	-.045	-.066	-.076	-.089
210	-.002	-.003	-.003	-.029	-.050	-.072	-.083	-.095
225	-.011	-.007	-.010	-.026	-.052	-.076	-.088	-.098
240	-.011	-.003	-.007	-.021	-.049	-.068	-.081	-.091
255	-.011	-.002	-.008	-.022	-.050	-.068	-.081	-.089
270	-.009	-.003	-.012	-.033	-.060	-.072	-.085	-.100
285	-.001	.000	-.009	-.042	-.072	-.073	-.063	-.046
300	-.001	-.001	-.010	-.040	-.043	-.030	-.009	.021
315	.002	.000	-.004	-.016	-.002	.023	.057	.104
330	.003	.000	.001	.003	.031	.070	.117	.179
345	.004	.001	.004	.017	.054	.102	.160	.234

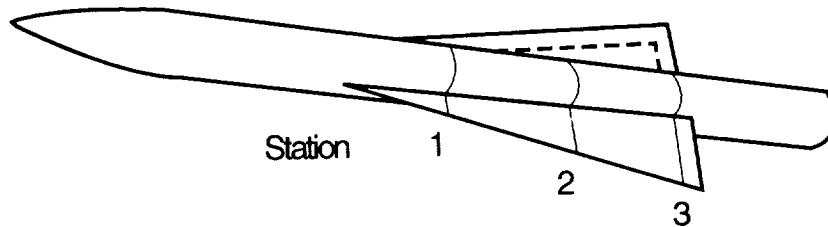
Table 10. Concluded

(d) Concluded; station 3

THETA, DEG	CP FOR ALPHA, DEG =							
	-4.00	-.06	4.00	7.99	11.98	16.02	20.01	23.98
0	.007	.009	.017	.034	.065	.119	.182	.264
15	.006	.010	.017	.032	.059	.111	.171	.249
30	-.001	.004	.008	.013	.029	.074	.124	.189
45	.004	.008	.009	-.002	.002	.034	.072	.119
60	.003	.008	.003	-.021	-.037	-.019	.007	.037
75	.002	.008	-.002	-.031	-.072	-.069	-.056	-.040
90	.004	.010	-.002	-.025	-.052	-.068	-.083	-.089
105	.001	.006	-.003	-.017	-.043	-.064	-.077	-.087
120	.001	.004	-.002	-.015	-.044	-.063	-.076	-.087
135	.001	.001	-.002	-.015	-.046	-.066	-.079	-.090
150	.003	.001	.000	-.018	-.046	-.067	-.080	-.092
165	.006	.005	.002	-.020	-.046	-.066	-.081	-.092
180	.006	.001	.003	-.004	-.039	-.057	-.067	-.080
195	.007	.003	.004	-.010	-.043	-.061	-.073	-.089
210	.008	.005	.005	-.018	-.042	-.062	-.075	-.088
225	.005	.005	.004	-.011	-.041	-.061	-.073	-.085
240	-.001	.002	.000	-.013	-.043	-.063	-.076	-.087
255	.001	.006	.001	-.011	-.039	-.061	-.073	-.084
270								
285	.002	.008	-.003	-.027	-.068	-.077	-.066	-.048
300	.002	.007	-.001	-.027	-.046	-.032	-.010	.022
315	.001	.008	.004	-.012	-.007	.019	.053	.104
330	.004	.010	.011	.011	.030	.070	.118	.184
345	.008	.012	.018	.030	.058	.108	.167	.245



(a) Bottom oblique view.

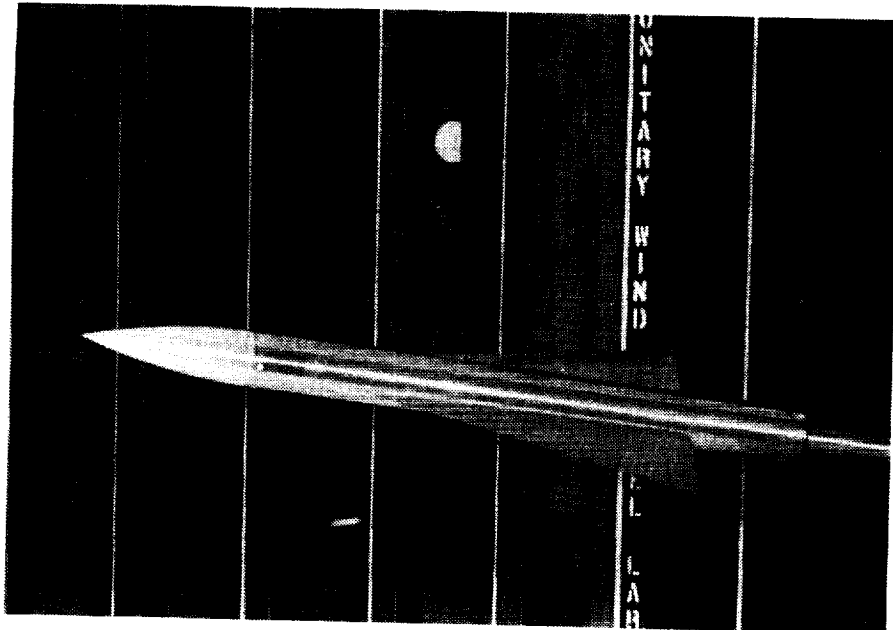


(b) Top oblique view.

Figure 1. Baseline model showing pressure orifice locations.

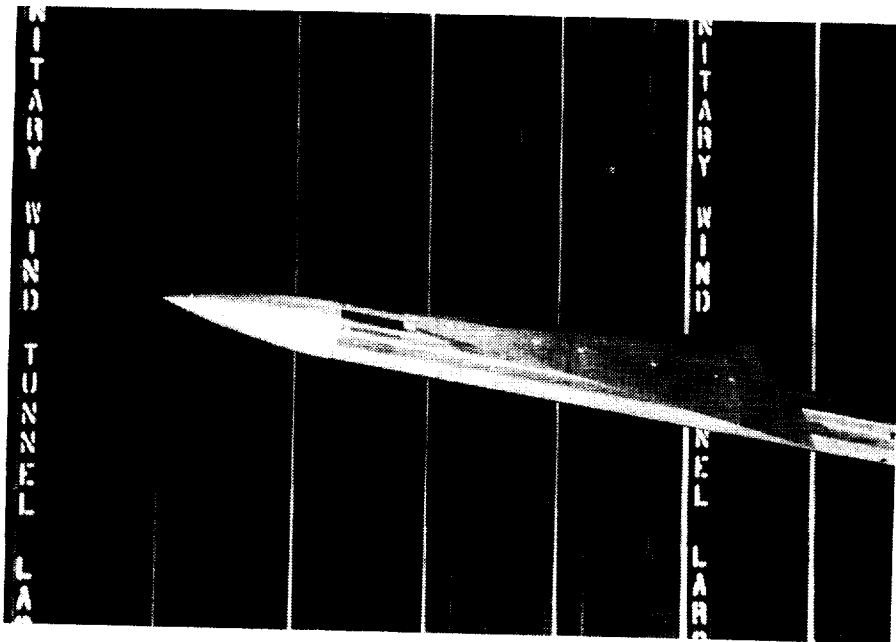
Configuration	Configuration description	Identification symbol
1	Horizontal wings mounted at body centerline (baseline configuration)	
2	Horizontal wings mounted on top of body	
3	Horizontal wings mounted midway between body centerline and top of body	
4	Configuration 3 rolled 180°	
5	Configuration 2 rolled 180°	
6	Radially mounted wings at same location as on configuration 3	
7	Configuration 6 rolled 180°	
8	Body alone (without wings)	

Figure 2. Description of test configurations shown in figures 7-15.



L-87-9272

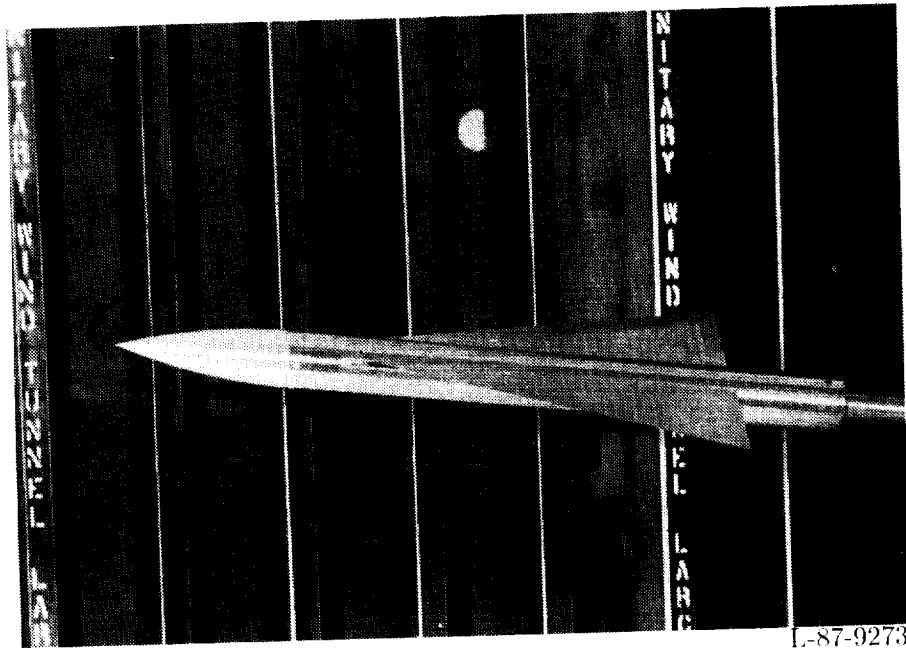
(a) Configuration 1 (baseline model).



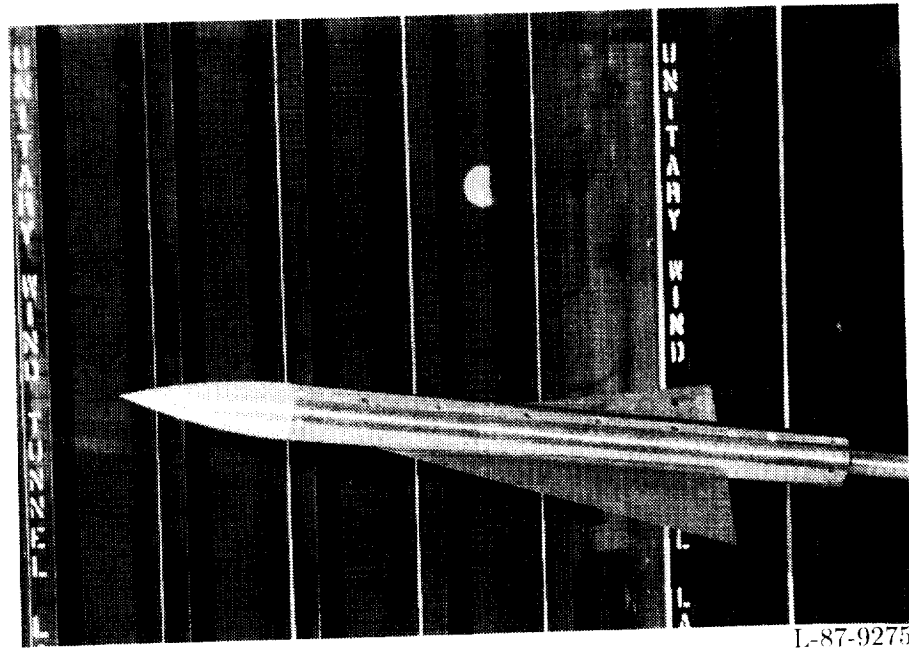
L-87-8451

(b) Configuration 2.

Figure 3. Photographs of configurations.

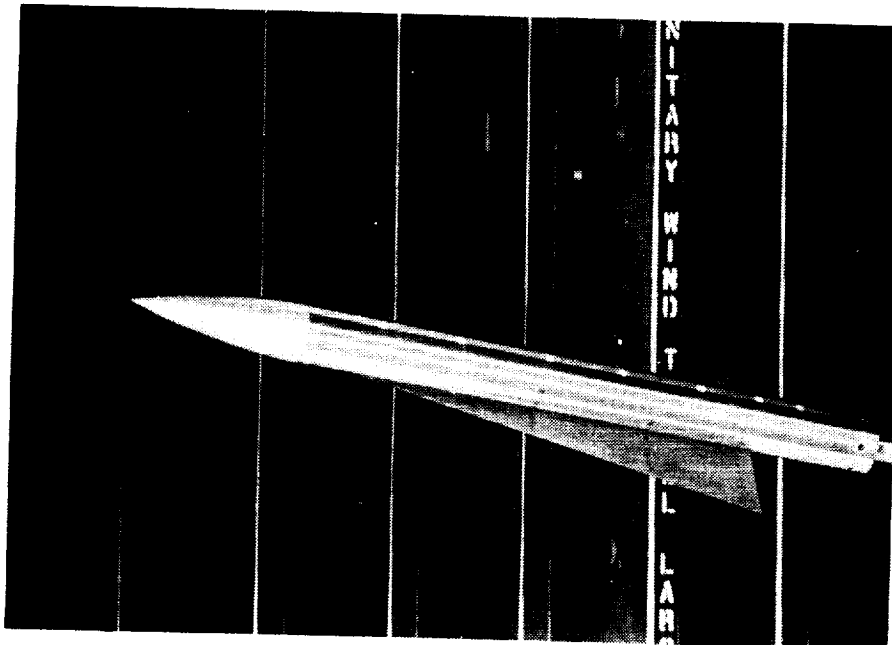


(c) Configuration 3.



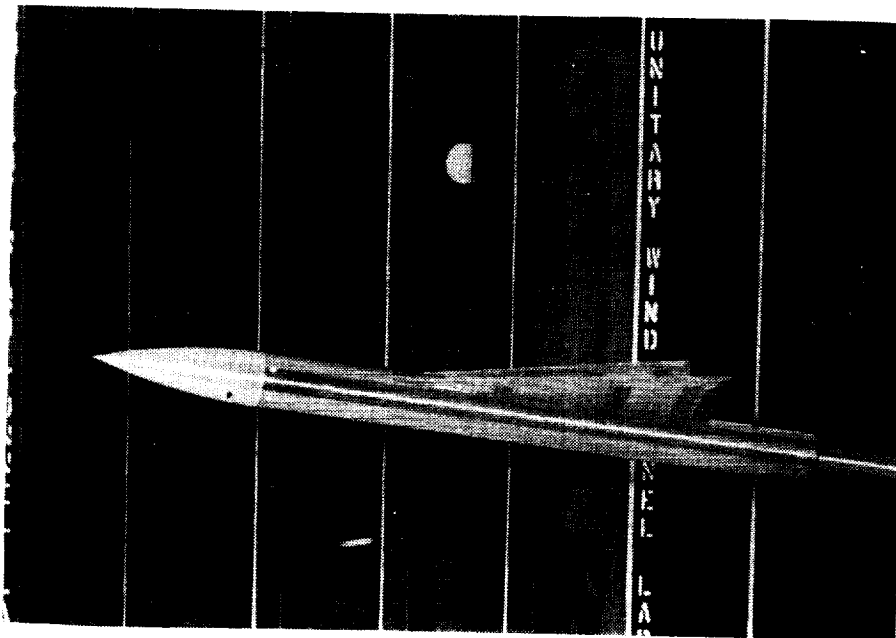
(d) Configuration 4.

Figure 3. Continued.



L-87-8450

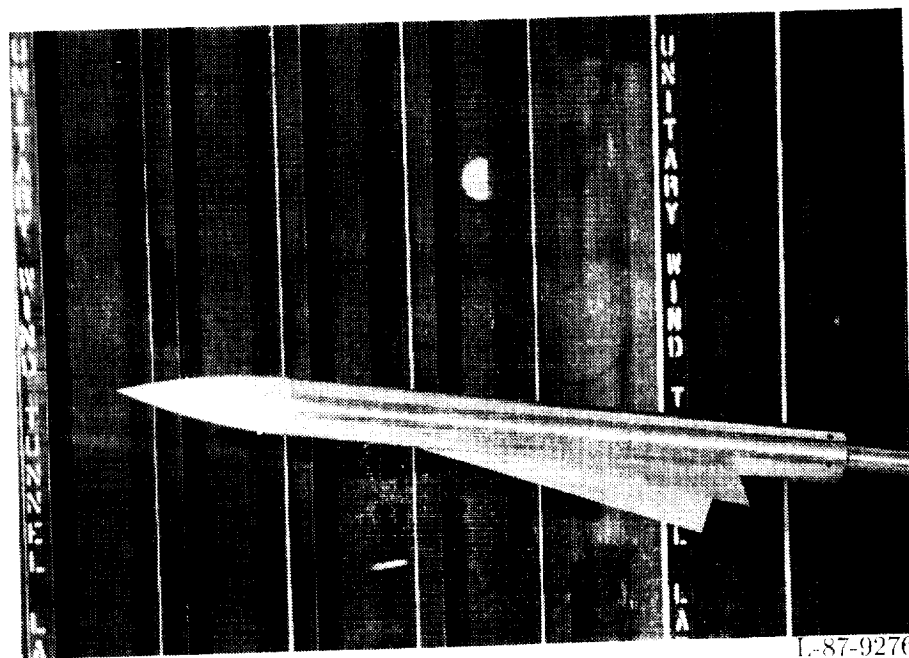
(e) Configuration 5.



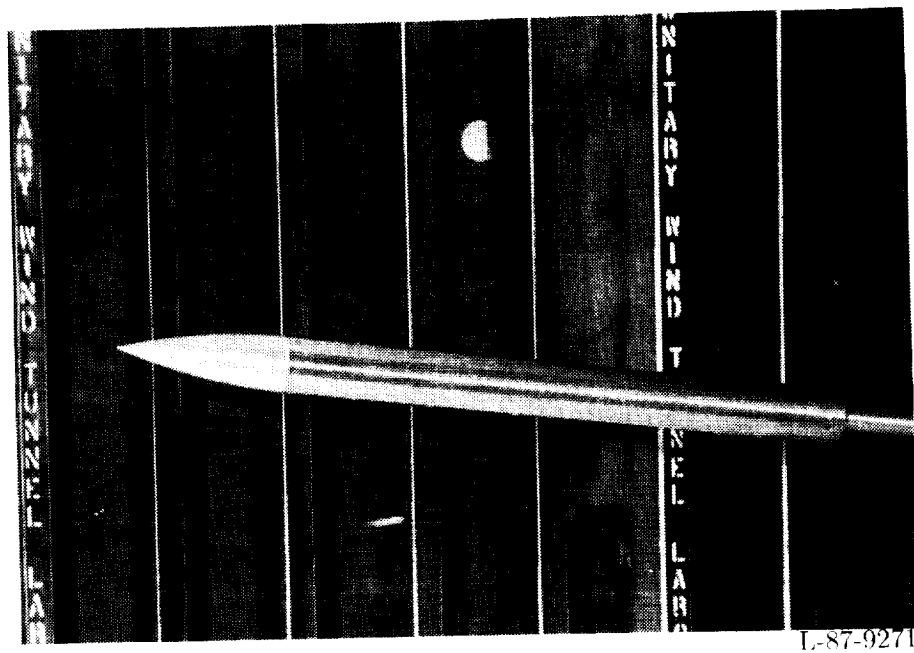
L-87-9274

(f) Configuration 6.

Figure 3. Continued.



(g) Configuration 7.



(h) Configuration 8 (body alone).

Figure 3. Concluded.

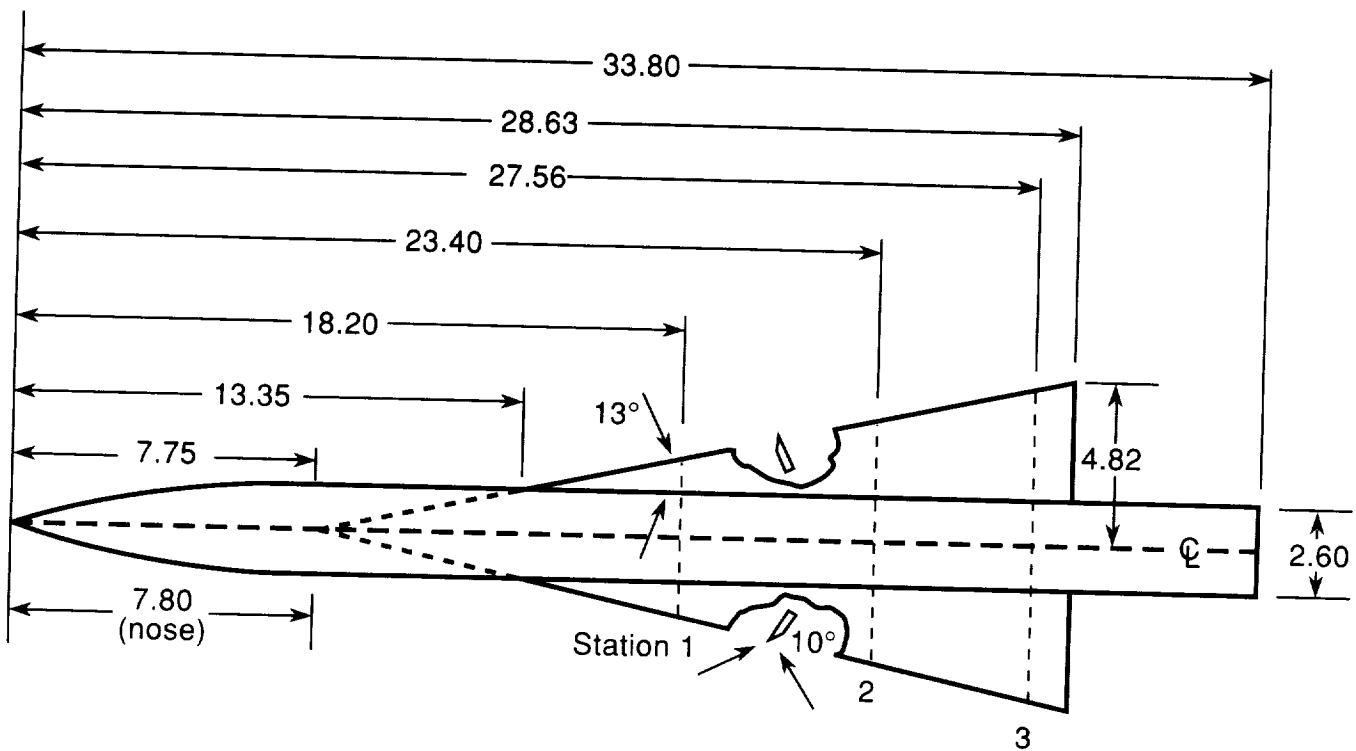


Figure 4. Dimensions of configuration 1. Linear dimensions are given in inches.

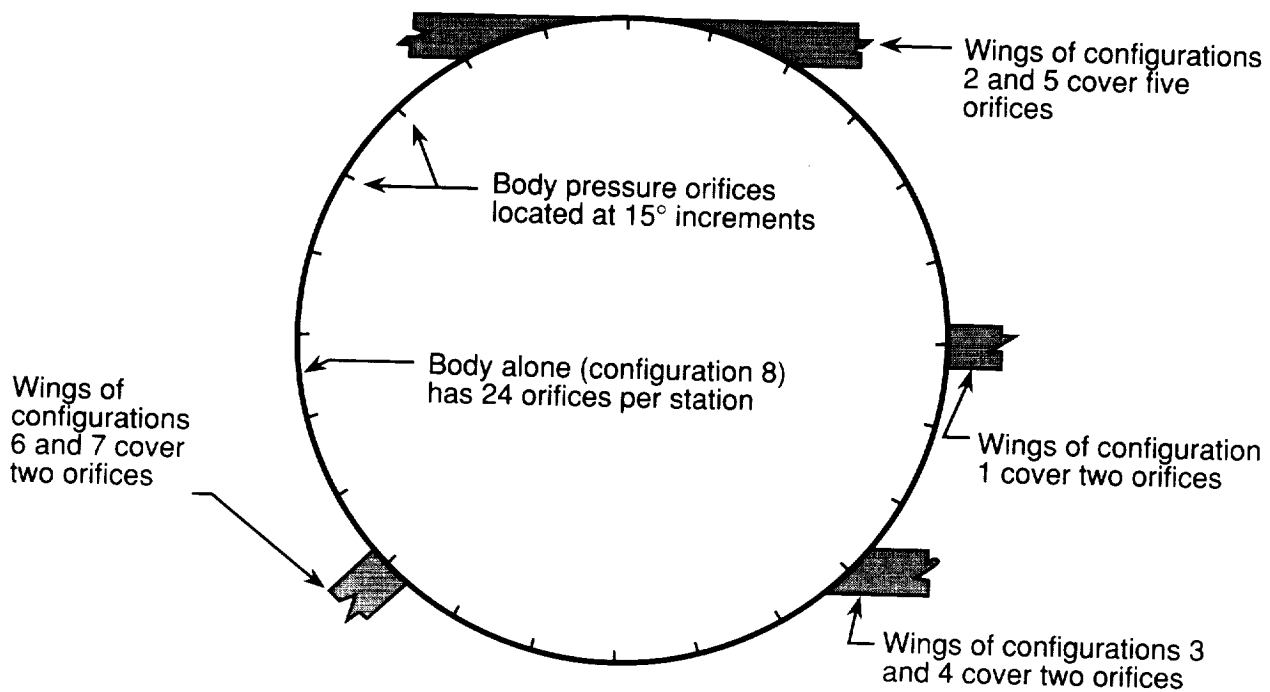


Figure 5. Locations of body pressure orifices.

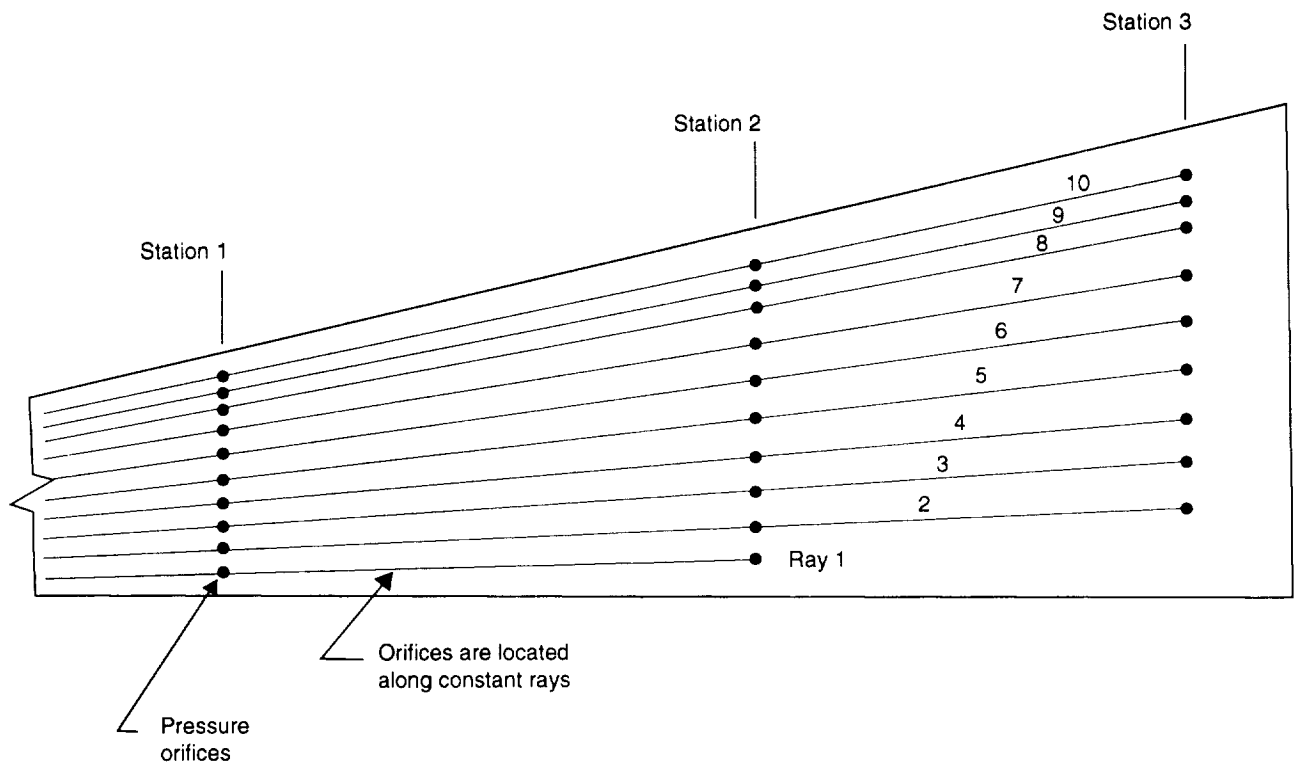


Figure 6. Locations of wing pressure orifices.

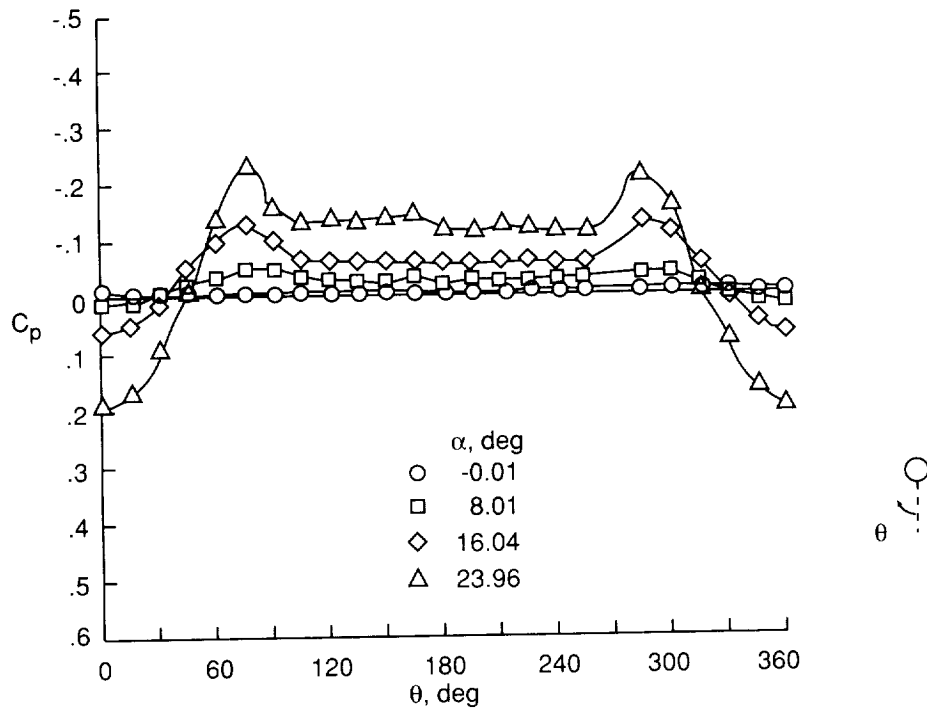
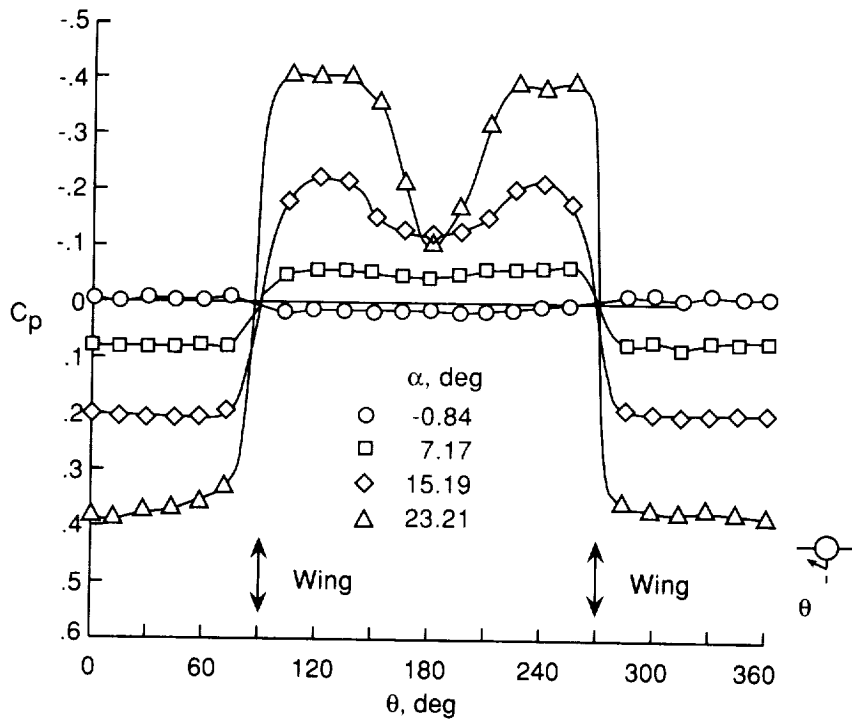
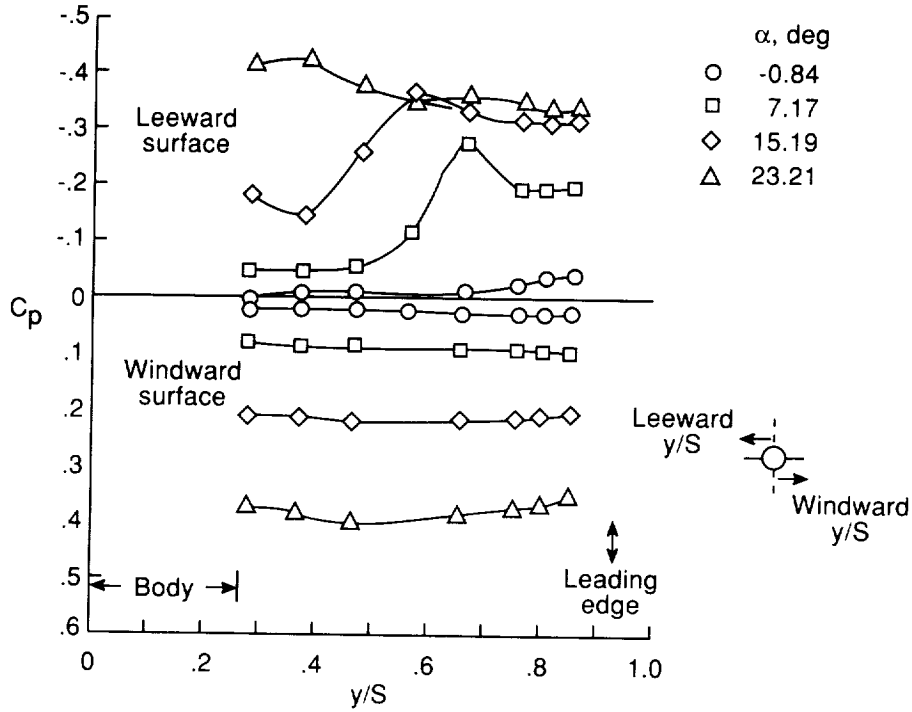


Figure 7. Pressure distributions around station 3 of configuration 8 (body alone) at $M_\infty = 1.70$ and $\phi = 0^\circ$.

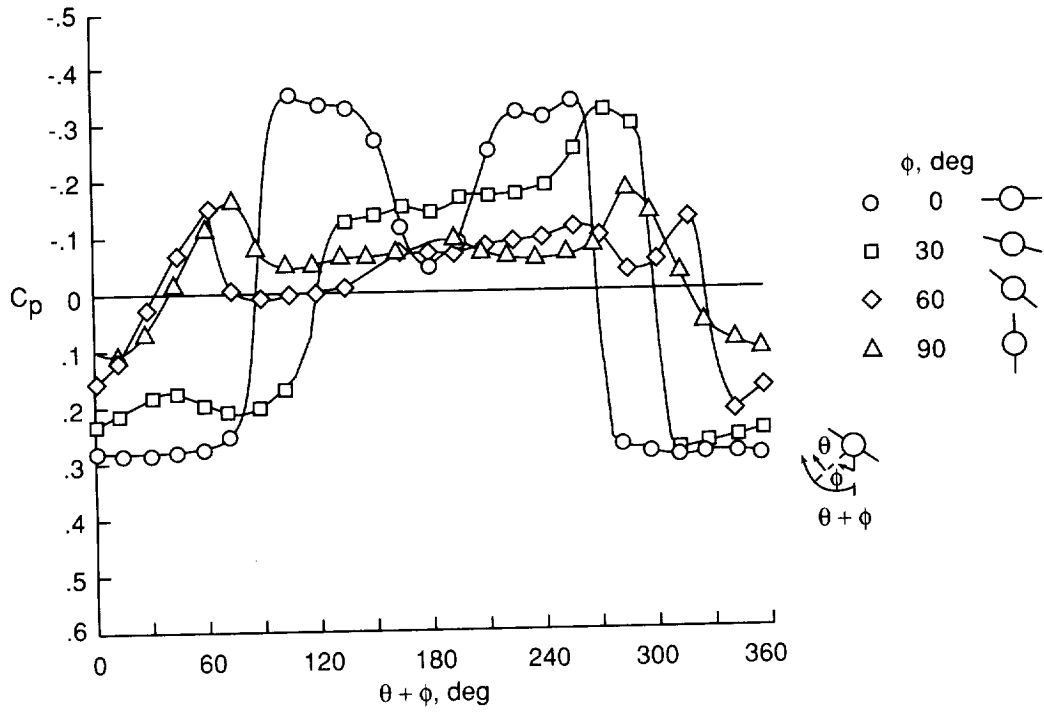


(a) Body.

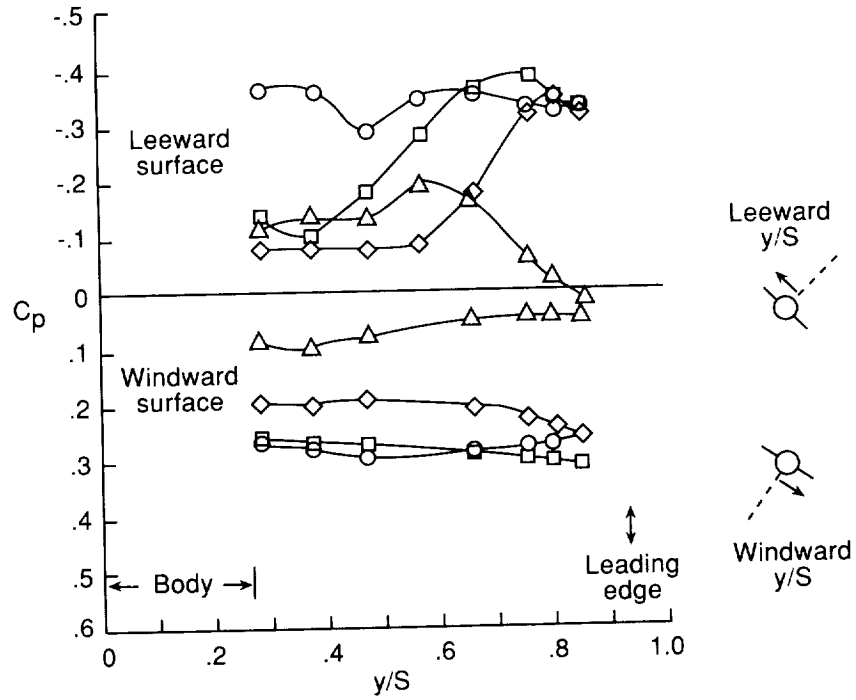


(b) Wing.

Figure 8. Effect of angle of attack on station 3 of configuration 1 at $M_\infty = 1.70$ and $\phi = 0^\circ$.

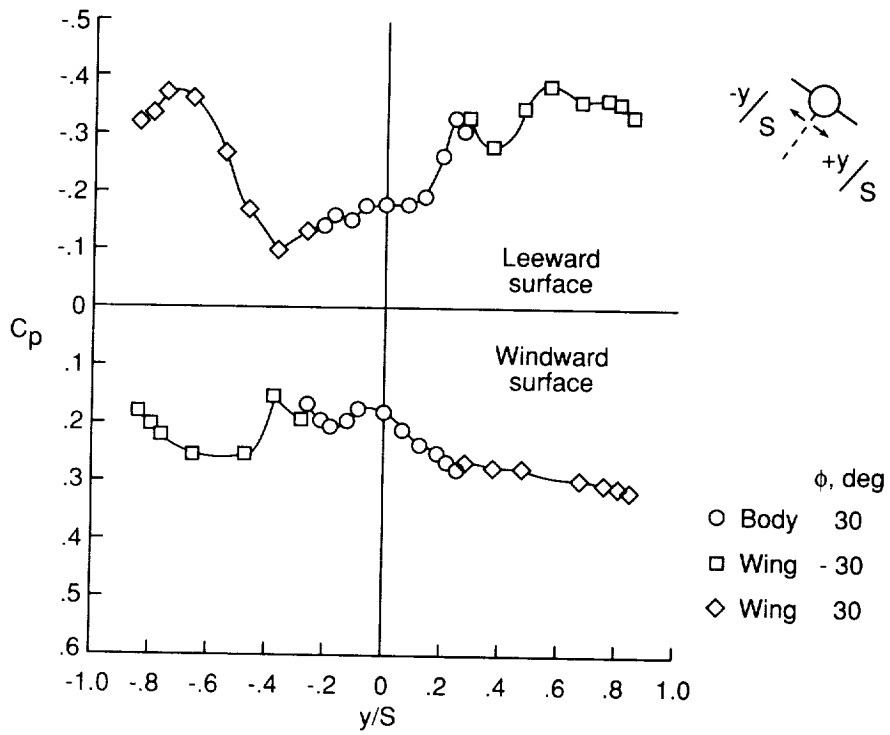


(a) Body.



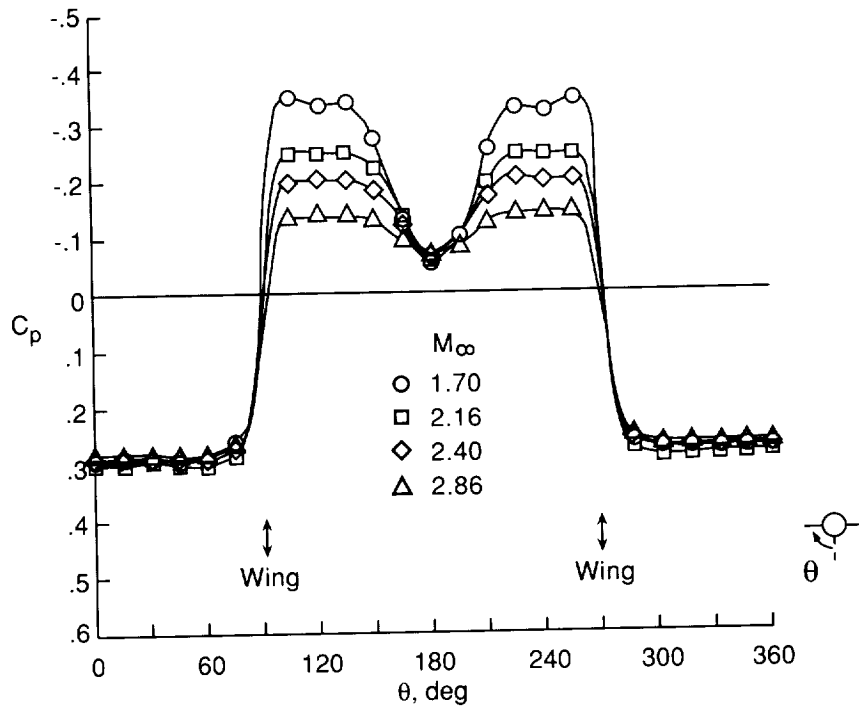
(b) Wing.

Figure 9. Effect of roll angle on station 3 of configuration 1 at $M_\infty = 1.70$ and $\alpha \approx 20^\circ$.

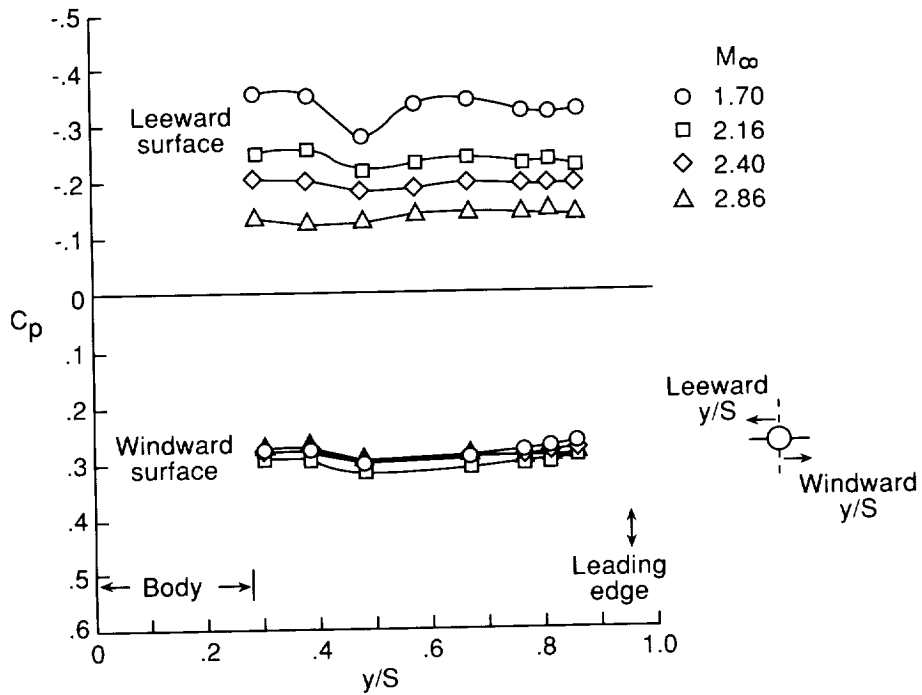


(c) Wing-body combination.

Figure 9. Concluded.

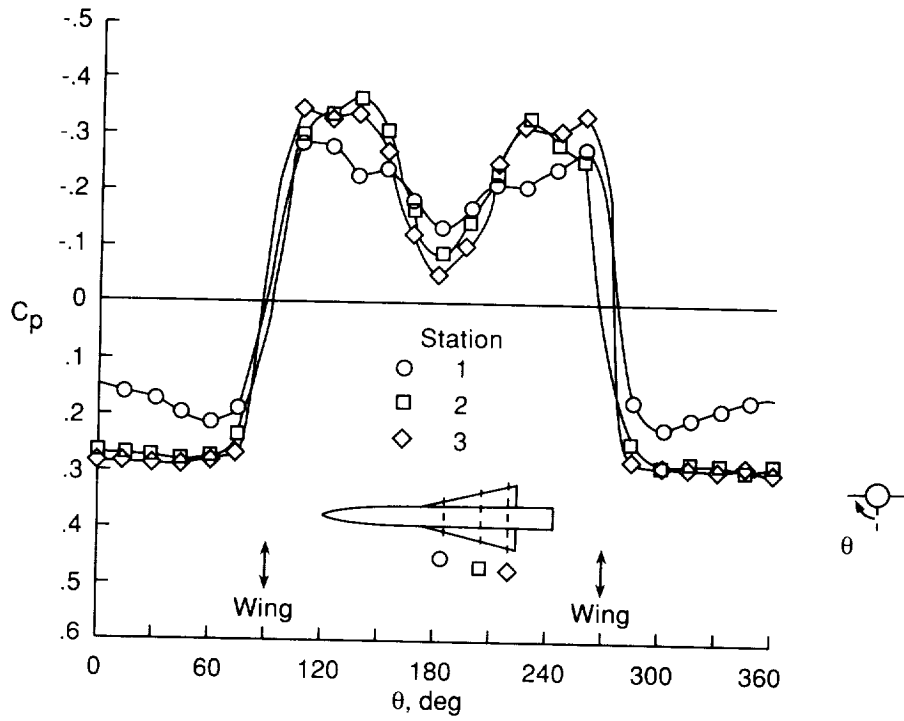


(a) Body.

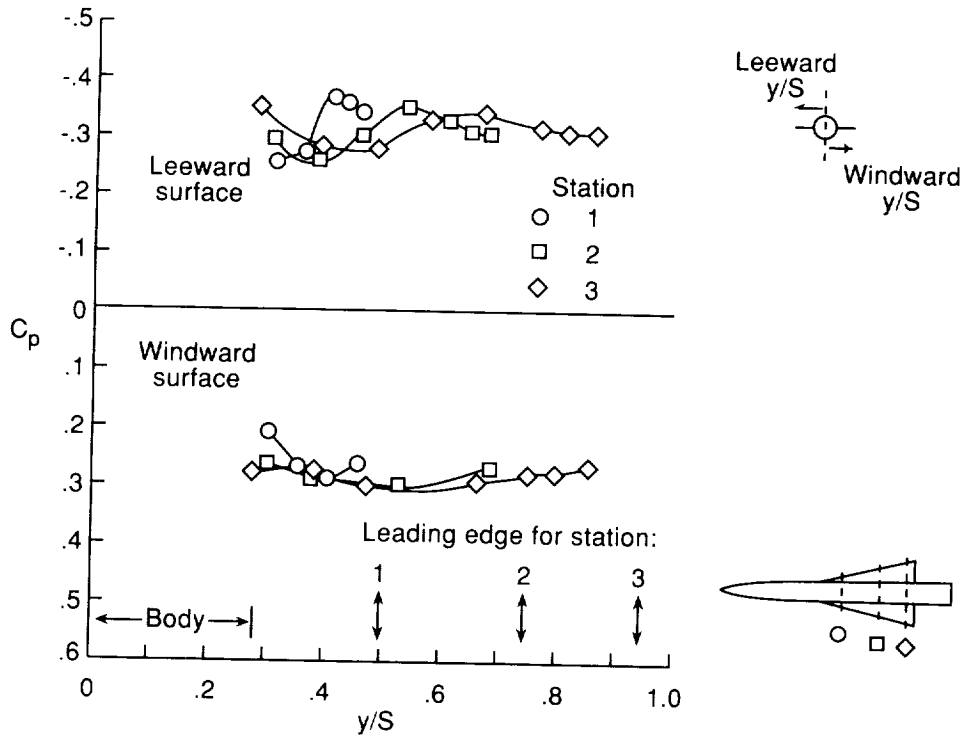


(b) Wing.

Figure 10. Effect of Mach number on station 3 of configuration 1 at $\alpha \approx 20^\circ$ and $\phi = 0^\circ$.

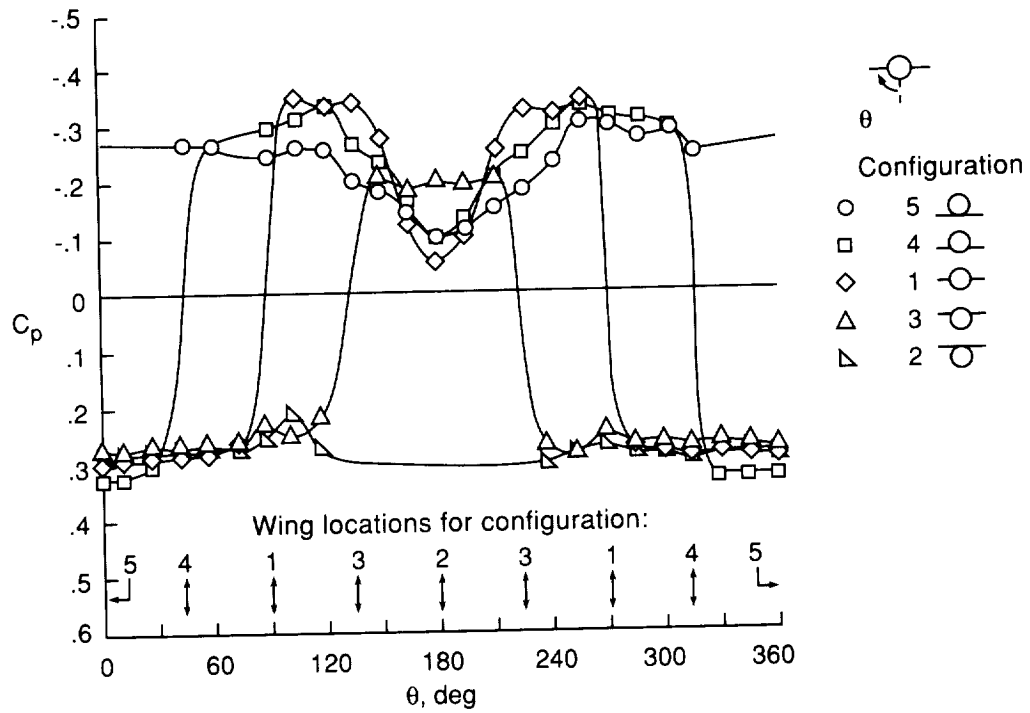


(a) Body.

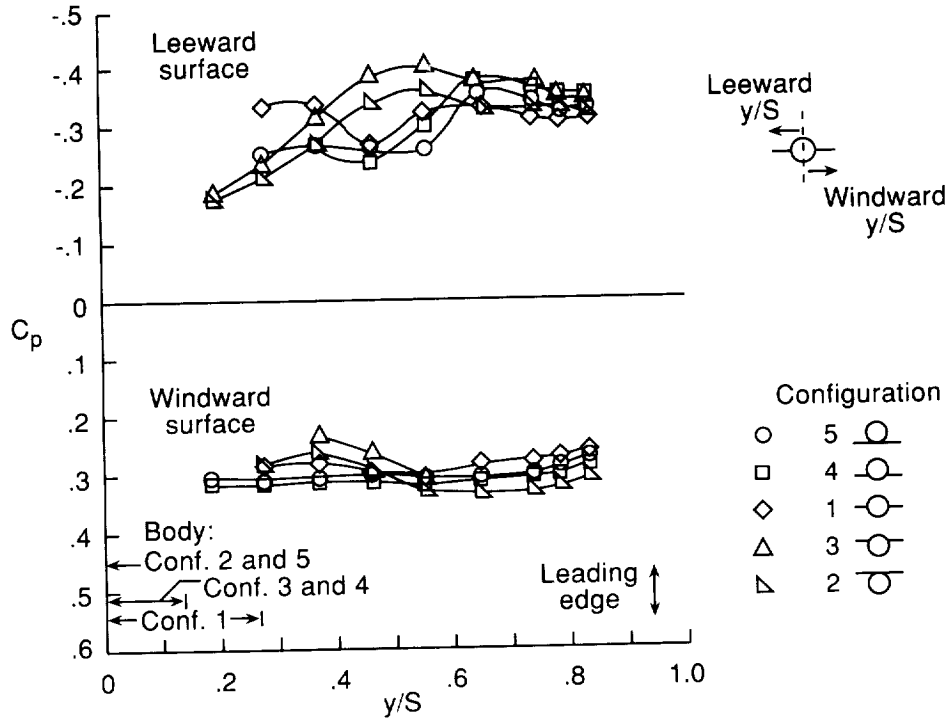


(b) Wing.

Figure 11. Effect of longitudinal station on configuration 1 at $M_\infty = 1.70$, $\alpha \approx 19.23^\circ$, and $\phi = 0^\circ$.

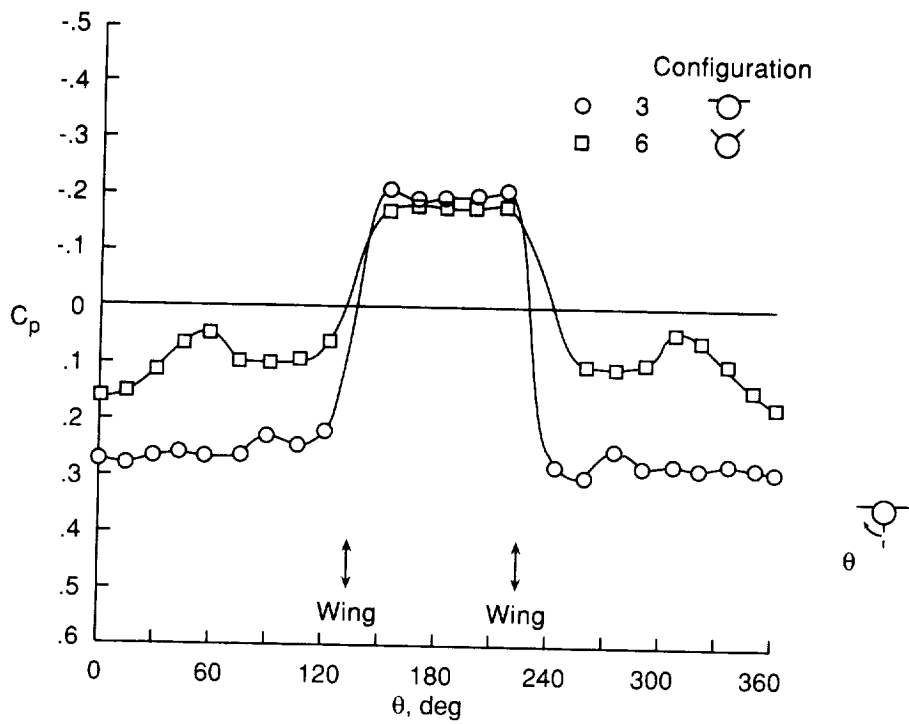


(a) Body.

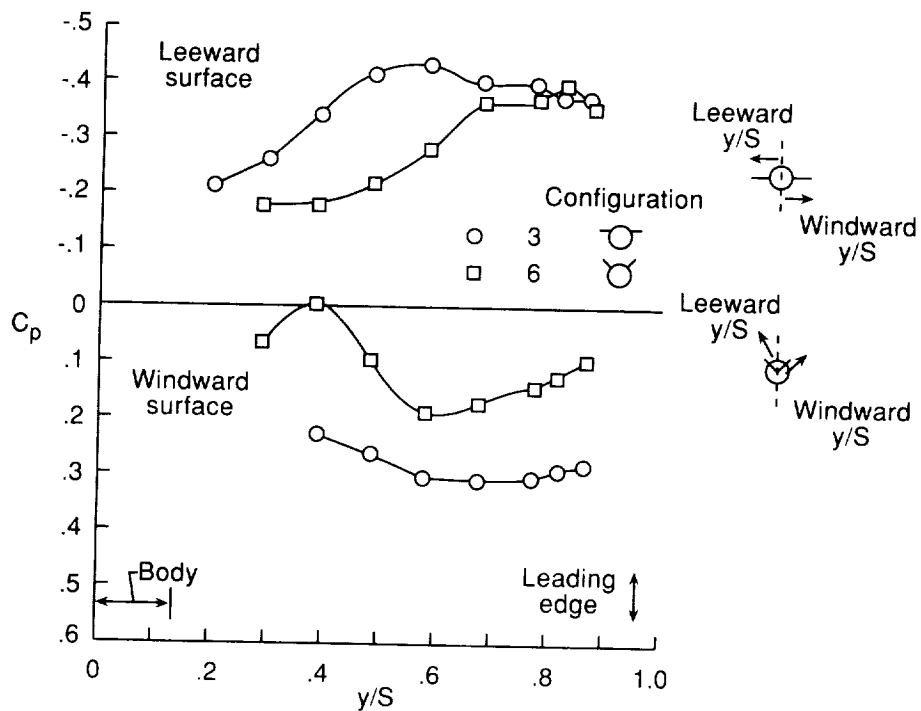


(b) Wing.

Figure 12. Effect of wing vertical location on station 3 at $M_\infty = 1.70$, $\alpha \approx 20^\circ$, and $\phi = 0^\circ$.

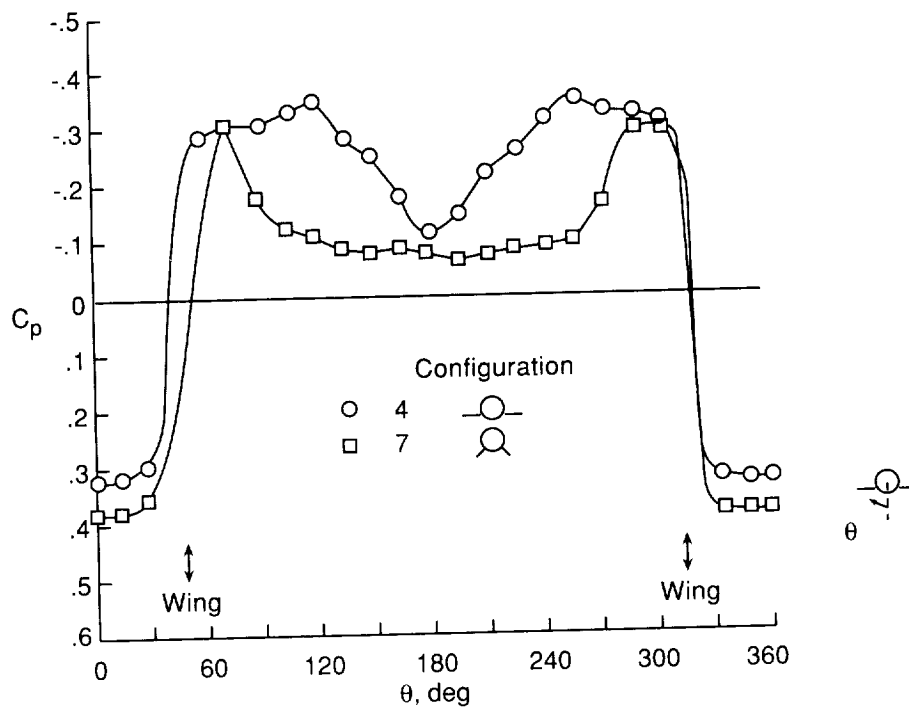


(a) Body.

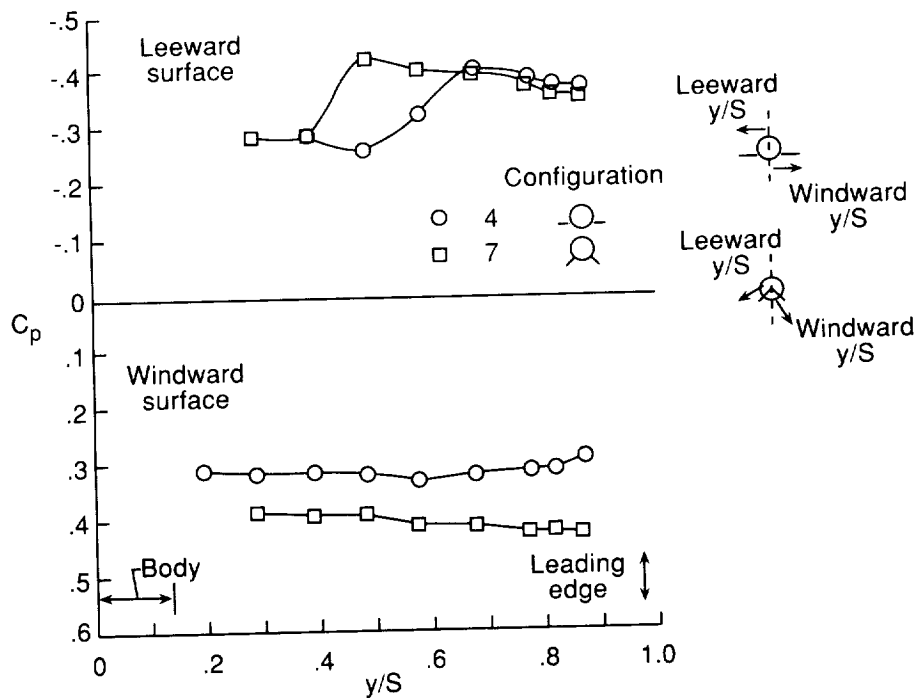


(b) Wing.

Figure 13. Wing angular orientation effect on station 3 for high-mounted wings at $M_\infty = 1.70$, $\alpha \approx 20^\circ$, and $\phi = 0^\circ$.

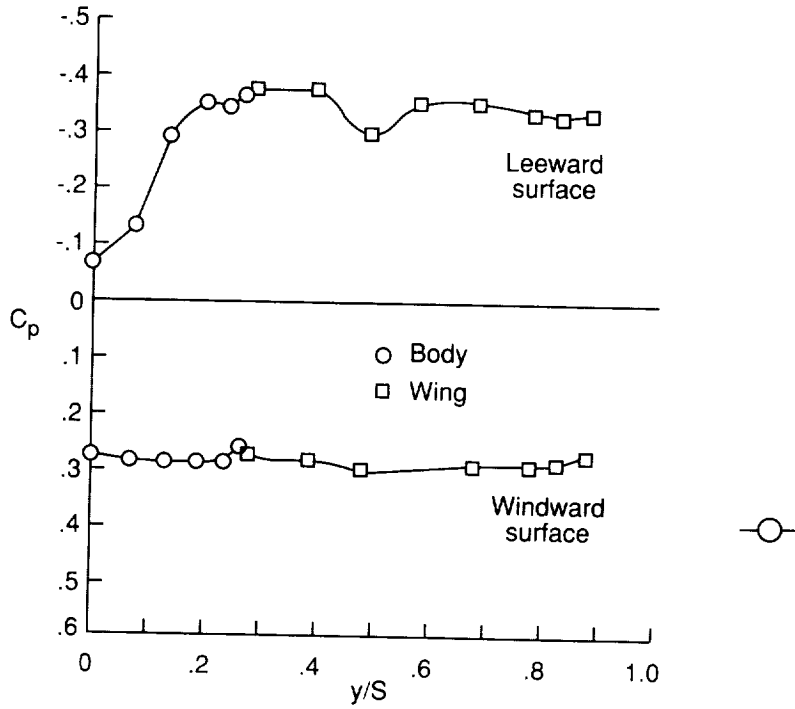


(a) Body.

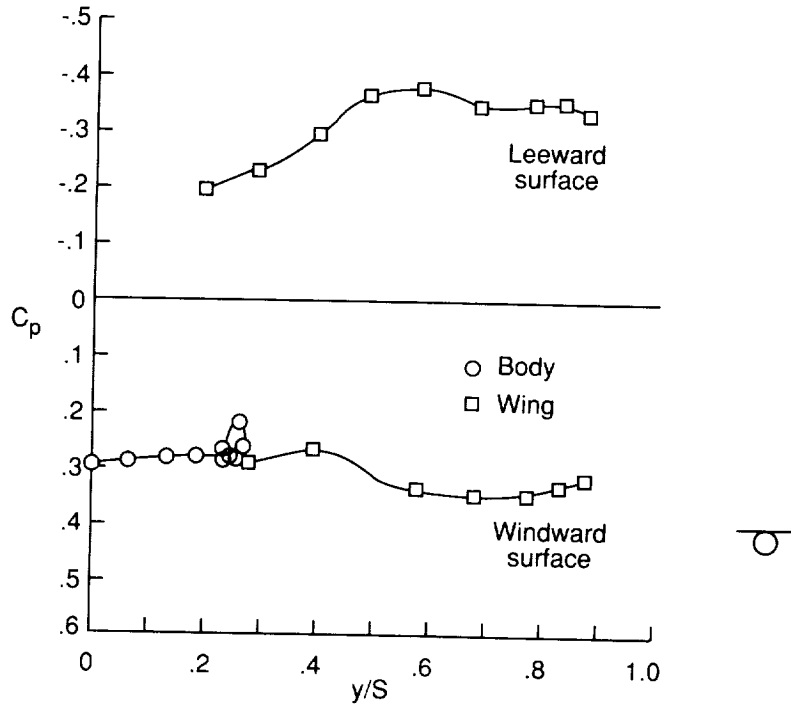


(b) Wing.

Figure 14. Wing angular orientation effect on station 3 for low-mounted wings at $M_\infty = 1.70$, $\alpha \approx 20^\circ$, and $\phi = 0^\circ$.

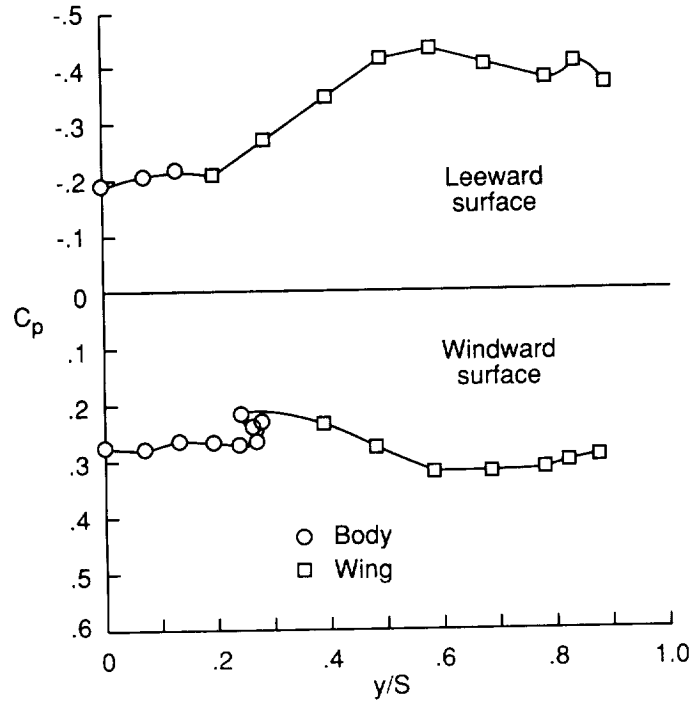


(a) Configuration 1 (baseline model).

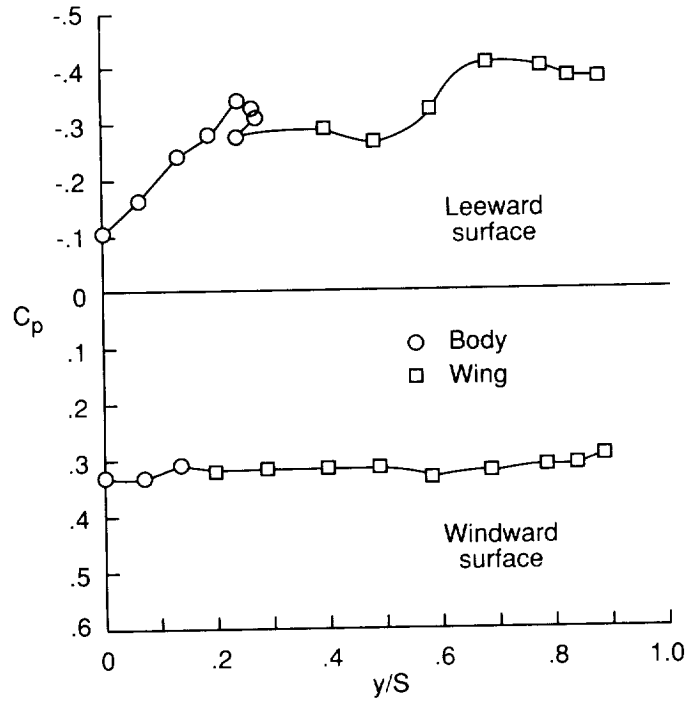


(b) Configuration 2.

Figure 15. Effect of wing-body juncture on station 3 at $M_\infty = 1.70$, $\alpha \approx 20^\circ$, and $\phi = 0^\circ$.

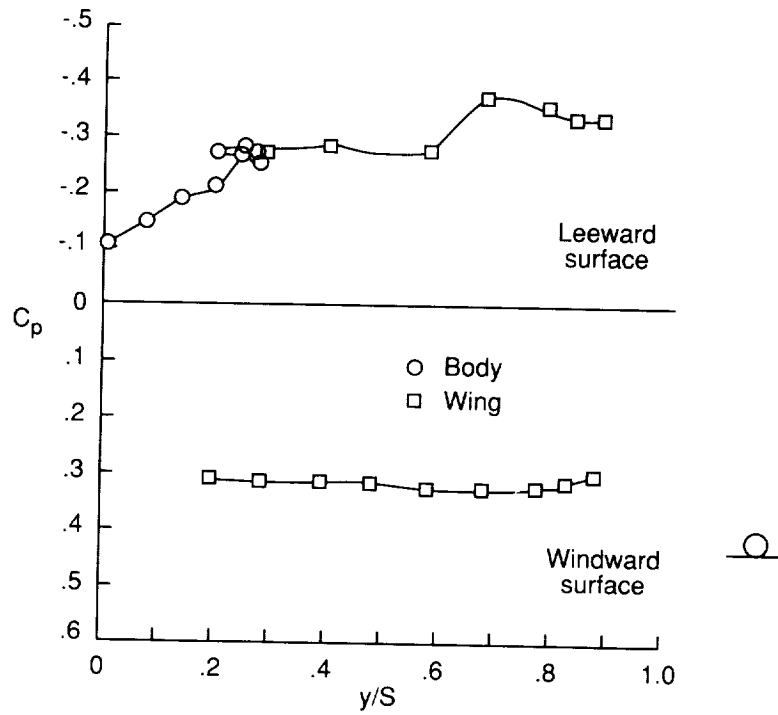


(c) Configuration 3.

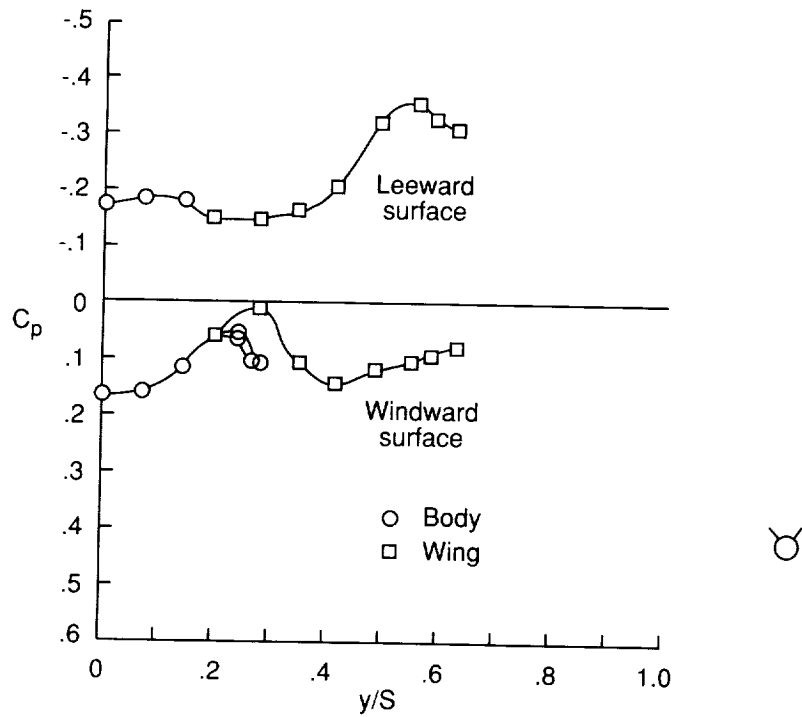


(d) Configuration 4.

Figure 15. Continued.

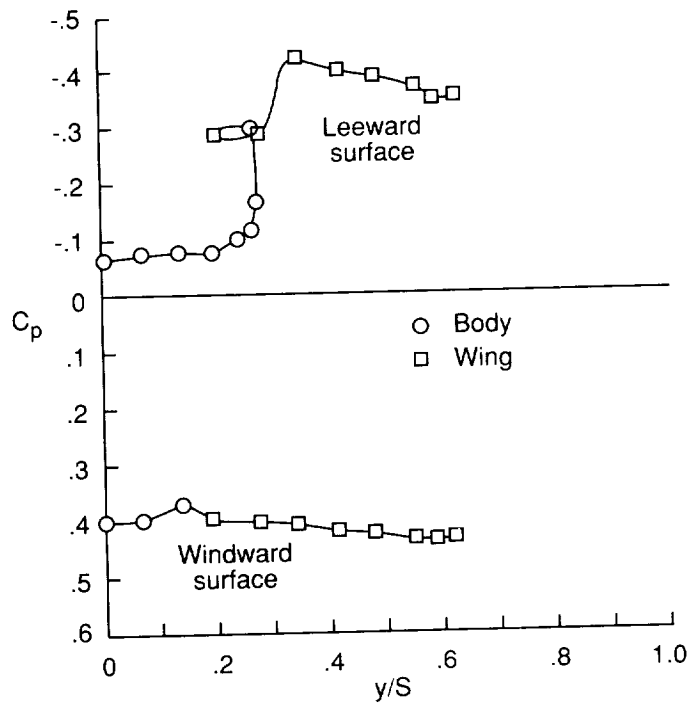


(e) Configuration 5.



(f) Configuration 6.

Figure 15. Continued.



(g) Configuration 7.

Figure 15. Concluded.

REPORT DOCUMENTATION PAGE

Form Approved
OMB No. 0704-0188

Public reporting burden for this collection of information is estimated to average 1 hour per response, including the time for reviewing instructions, searching existing data sources, gathering and maintaining the data needed, and completing and reviewing the collection of information. Send comments regarding this burden estimate or any other aspect of this collection of information, including suggestions for reducing this burden, to Washington Headquarters Services, Directorate for Information Operations and Reports, 1215 Jefferson Davis Highway, Suite 1204, Arlington, VA 22202-4302, and to the Office of Management and Budget, Paperwork Reduction Project (0704-0188), Washington, DC 20503.

1. AGENCY USE ONLY (Leave blank)	2. REPORT DATE April 1993	3. REPORT TYPE AND DATES COVERED Technical Memorandum
----------------------------------	------------------------------	--

4. TITLE AND SUBTITLE Experimental Effects of Wing Location on Wing-Body Pressures at Supersonic Speeds	5. FUNDING NUMBERS WU 505-59-30-01
--	---------------------------------------

6. AUTHOR(S) Jerry M. Allen and Carolyn B. Watson
--

7. PERFORMING ORGANIZATION NAME(S) AND ADDRESS(ES) NASA Langley Research Center Hampton, VA 23681-0001	8. PERFORMING ORGANIZATION REPORT NUMBER L-17148
--	---

9. SPONSORING/MONITORING AGENCY NAME(S) AND ADDRESS(ES) National Aeronautics and Space Administration Washington, DC 20546-0001	10. SPONSORING/MONITORING AGENCY REPORT NUMBER NASA TM-4434
---	--

11. SUPPLEMENTARY NOTES

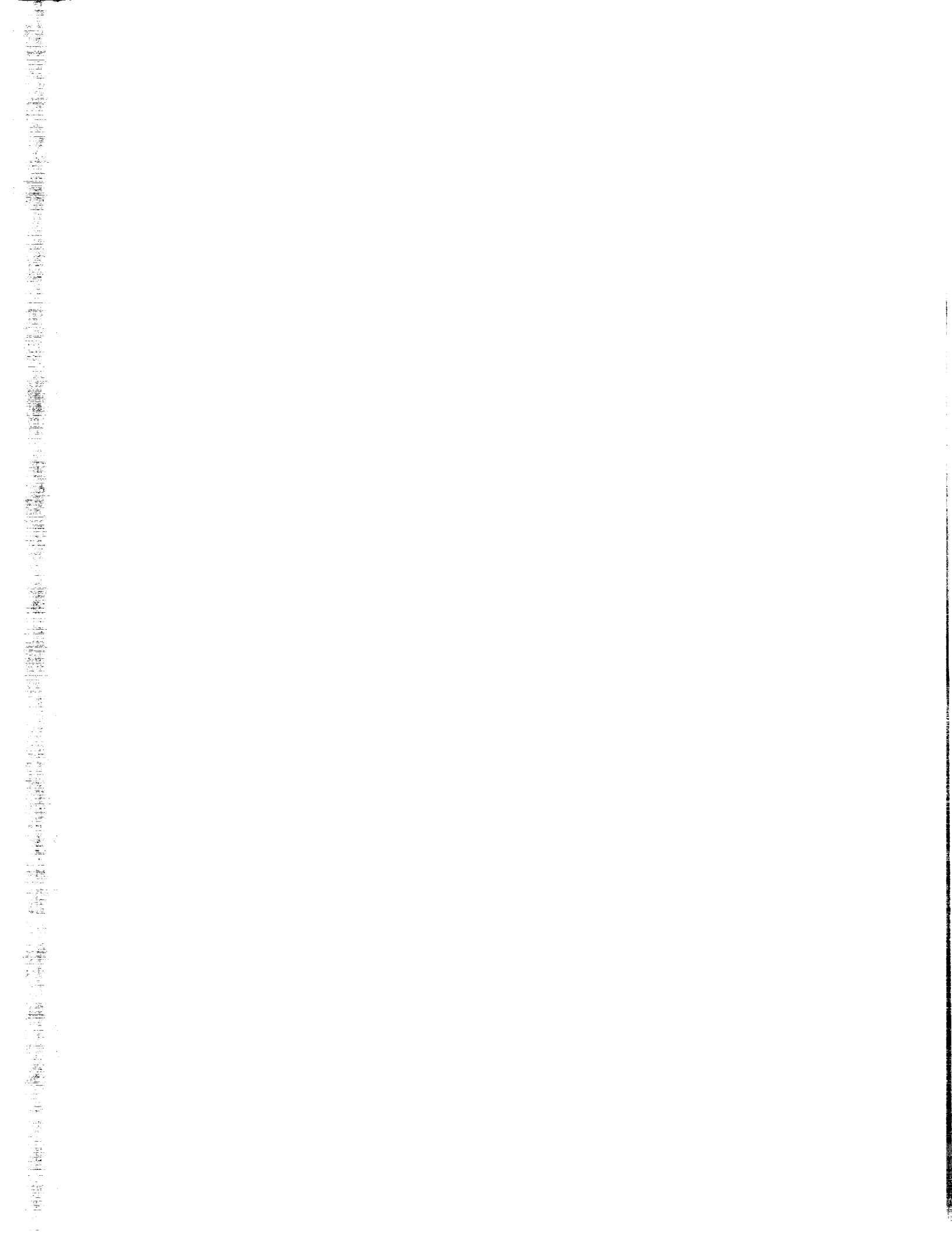
12a. DISTRIBUTION/AVAILABILITY STATEMENT Unclassified Unlimited Subject Category 02	12b. DISTRIBUTION CODE
---	------------------------

13. ABSTRACT (Maximum 200 words)
An experimental study has been performed at supersonic speeds to measure wing and body spanwise pressure distributions on an axisymmetric-body delta wing model on which the wing vertical location on the body was systematically varied from low- to high-mounted positions. In addition, for two of these positions both horizontal and radial wing angular orientations relative to the body were tested, and roll angle effects were investigated for one of the positions. Seven different wing-body configurations and a body-alone configuration were studied. The test was conducted at Mach numbers from 1.70 to 2.86 at angles of attack from about -4° to 24° . Pressure orifices were located at three longitudinal stations on each wing-body model, and at each station the orifices were located completely around the body, along the lower surface of the right wing (looking upstream), and along the upper surface of the left wing. All pressure coefficient data are tabulated, and selected samples are shown graphically to illustrate the effects of the test variables. The effects of angle of attack, roll angle, Mach number, longitudinal station, wing vertical location, wing angular orientation, and wing-body juncture are analyzed. The vertical location of the wing on the body had a very strong effect on the body pressures. For a given angle of attack at a roll angle of 0° , the pressures were virtually constant in the spanwise direction across the windward surfaces of the wing-body combination. Pressure-relieving, channeling, and vortex effects were noted in the data.

14. SUBJECT TERMS Wing-body aerodynamics; Experimental pressure distributions; Supersonic flow	15. NUMBER OF PAGES 196
	16. PRICE CODE A09

17. SECURITY CLASSIFICATION OF REPORT Unclassified	18. SECURITY CLASSIFICATION OF THIS PAGE Unclassified	19. SECURITY CLASSIFICATION OF ABSTRACT	20. LIMITATION OF ABSTRACT
---	--	---	----------------------------

NSN 7540-01-280-5500



National Aeronautics and
Space Administration
Code JTT
Washington, D.C.
20546-0001
Official Business
Penalty for Private Use, \$300

SPECIAL FOURTH-CLASS RATE
POSTAGE & FEES PAID
NASA
PERMIT No. G27



**POSTMASTER: If Undeliverable (Section 158
Postal Manual) Do Not Return**
