

NASA Contractor Report 191059

LOX/Hydrocarbon Rocket Engine Analytical Design Methodology Development and Validation

Karen E. Niiya and Richard E. Walker
Aerojet Propulsion Division
Sacramento, California

May 1993

Prepared for
Lewis Research Center
Under Contract NAS3-25556

NASA
National Aeronautics and
Space Administration

LOX/HYDROCARBON ROCKET ENGINE
ANALYTICAL DESIGN METHODOLOGY
DEVELOPMENT AND VALIDATION

(Contract NAS 3-25556)

Final Report

VOLUME II
APPENDICES

Prepared
For

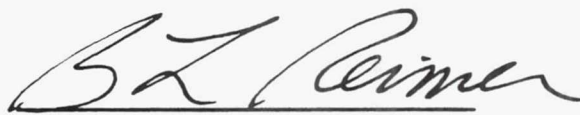
NASA/Lewis Research Center
21000 Brookpark Road
Cleveland, Ohio 44135

Prepared By:

Approved By:



J.L. Pieper
Project Engineer



Bryce L. Reimer
Program Manager



Thong V. Nguyen
Project Engineer

Aerojet Propulsion Division
P.O. Box 13222
Sacramento, California 95813-6000

Page intentionally left blank

TABLE OF CONTENTS

Appendices		<u>Page</u>
A	Measured Manifold and Chamber Mean Pressures Versus Time Plot for All Successful Tests	A-1
B	Time Series, Amplitude and Frequency Evolution, and Power Spectral Analysis of Chamber Pressure for All Unstable-Combustion Tests	B-1
C	Time Series, Amplitude and Frequency Evolution, and Power Spectral Analysis of Manifold and Chamber Pressures and Accelerations for Test 004	C-1
D	ROCCID Validation Hardware Design Drawing Package	D-1
E	Advanced Document Change Notices for the ROCCID Design Disclosure	E-1
F	Nonconformance Reports	F-1

APPENDIX A

MEASURED MANIFOLD AND CHAMBER MEAN
PRESSURES VERSUS TIME PLOT FOR
ALL SUCCESSFUL TESTS

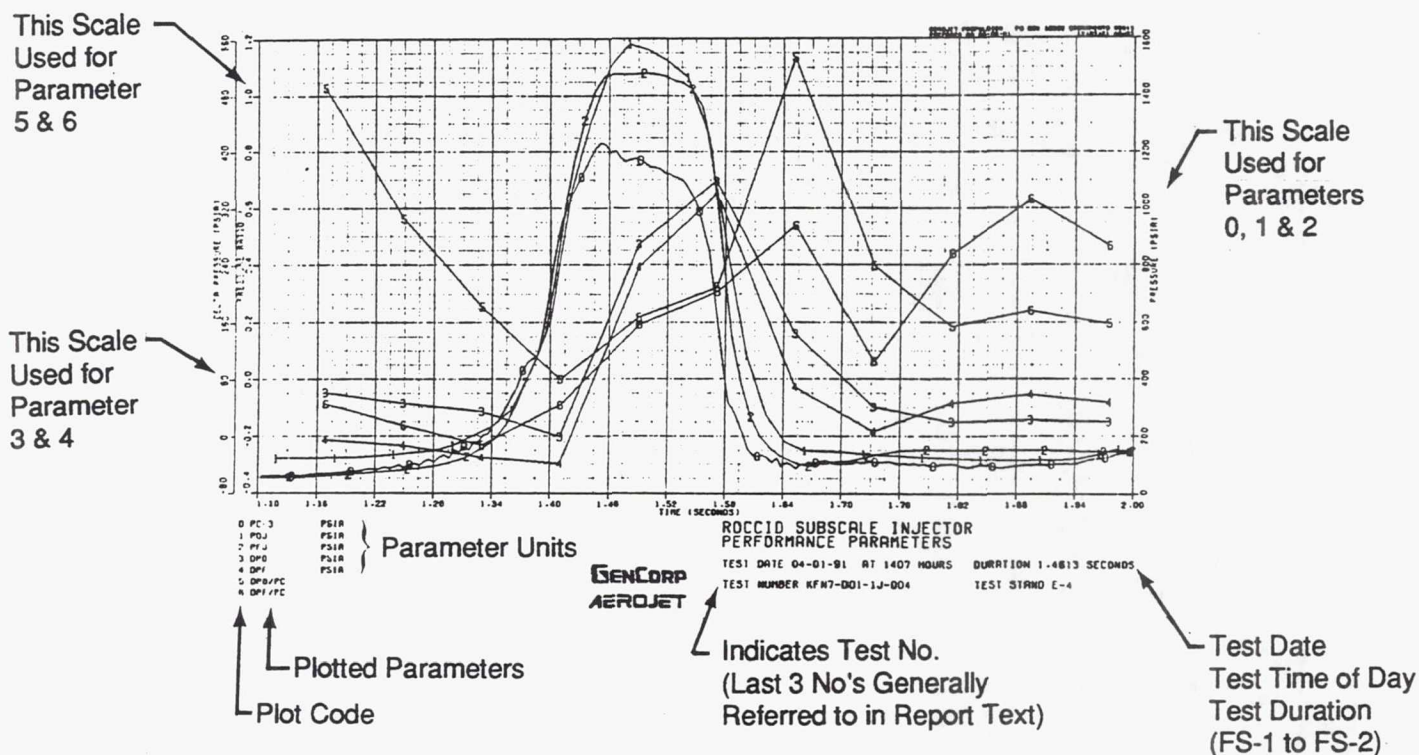
INDEX OF TEST DATA PLOTS

Page No.

A-3	Foreword
A-5	Data From Test No. KFN7-D01-1J-004
A-6	Data From Test No. KFN7-D01-1J-007
A-7	Data From Test No. KFN7-D01-1J-009
A-8	Data From Test No. KFN7-D01-1J-012
A-9	Data From Test No. KFN7-D01-1J-013
A-10	Data From Test No. KFN7-D01-1J-014
A-11	Data From Test No. KFN7-D01-1J-015
A-12	Data From Test No. KFN7-D01-1J-017
A-13	Data From Test No. KFN7-D01-1J-018
A-14	Data From Test No. KFN7-D01-1J-019
A-15	Data From Test No. KFN7-D01-1J-020
A-16	Data From Test No. KFN7-D01-1J-021
A-17	Data From Test No. KFN7-D01-1J-022
A-18	Data From Test No. KFN7-D01-1J-023
A-19	Data From Test No. KFN7-D01-1J-025
A-20	Data From Test No. KFN7-D01-1J-026
A-21	Data From Test No. KFN7-D01-1J-027
A-22	Data From Test No. KFN7-D01-1J-028
A-23	Data From Test No. KFN7-D01-1J-029
A-24	Data From Test No. KFN7-D01-1J-030
A-25	Data From Test No. KFN7-D01-1J-031
A-26	Data From Test No. KFN7-D01-1J-036
A-27	Data From Test No. KFN7-D01-1J-037
A-28	Data From Test No. KFN7-D01-1J-038
A-29	Data From Test No. KFN7-D01-1J-039
A-30	Data From Test No. KFN7-D01-1J-040

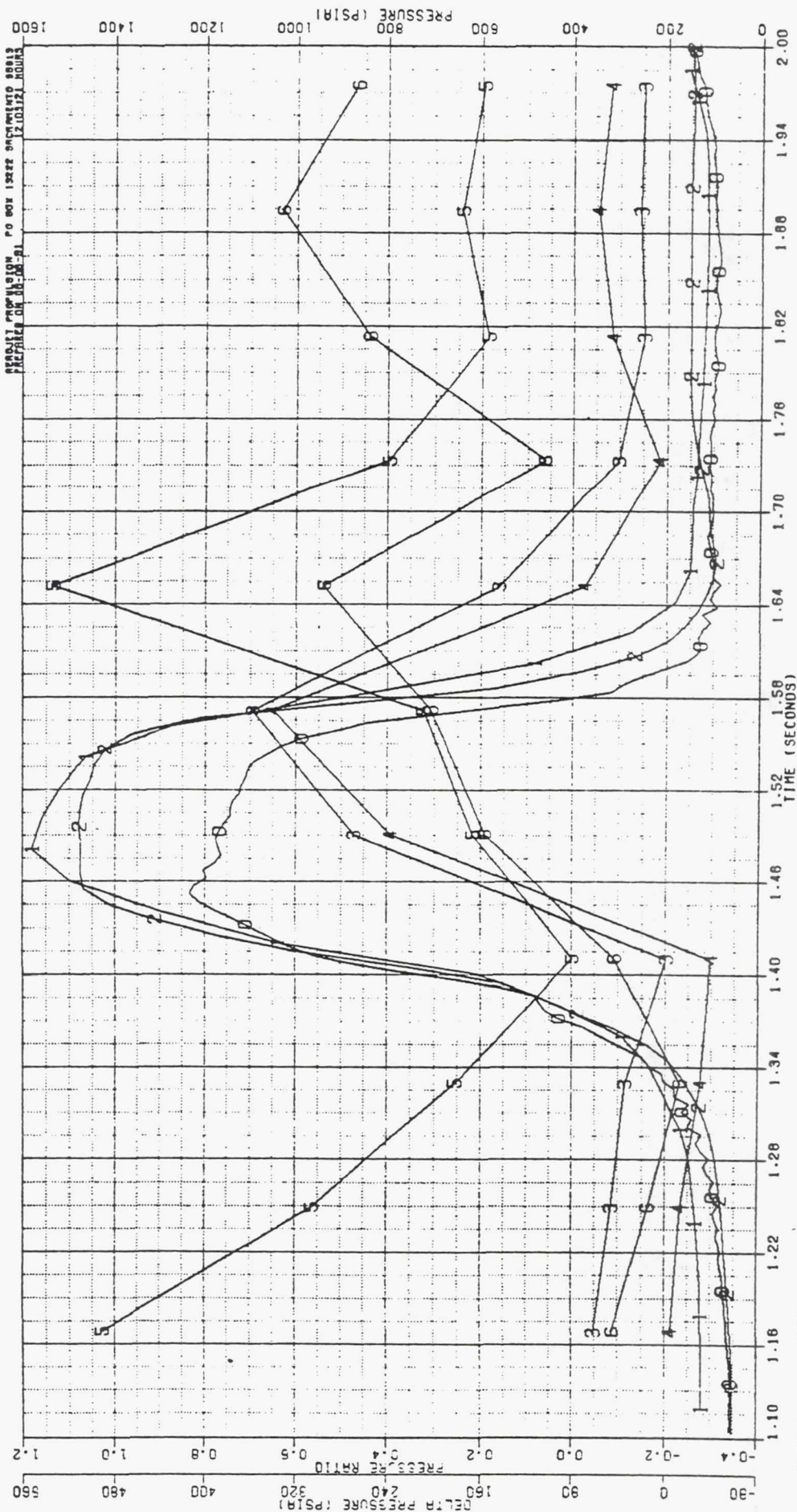
FOREWORD

This Appendix contains plots of selected pressure measurements as a function of time from the initial fireswitch (FS-1) activation. These plots were prepared from digital data obtained from the analog-to-digital converter for all 27 tests, where meaningful operation was achieved, in order to assess the combustion stability or instability characteristics of the combustor. The plots start at FS-1 + 1.10 seconds, which is the approximate time that the LOX/TEA + TEB ignition occurs. This hypergolic propellant combination is used as a combustion source to ignite the LOX/RP-1 propellants. Test data is plotted until well after the test shutdown switch (FS-2) in order to show pressure decays during the shutdown transient. Information contained in these plots are identified below:



PLOTTED PARAMETERS

PC-3	Chamber Pressure
POJ	LOX Injector Manifold Pressure
PFJ	RP-1 Injector Manifold Pressure
DPO	LOX Injector ΔP (POJ-Pc-3)
DPF	RP-1 Injector ΔP (PFJ-Pc-3)
DPO/Pc	DPO/Pc-3
DPF/Pc	DPF/Pc-3

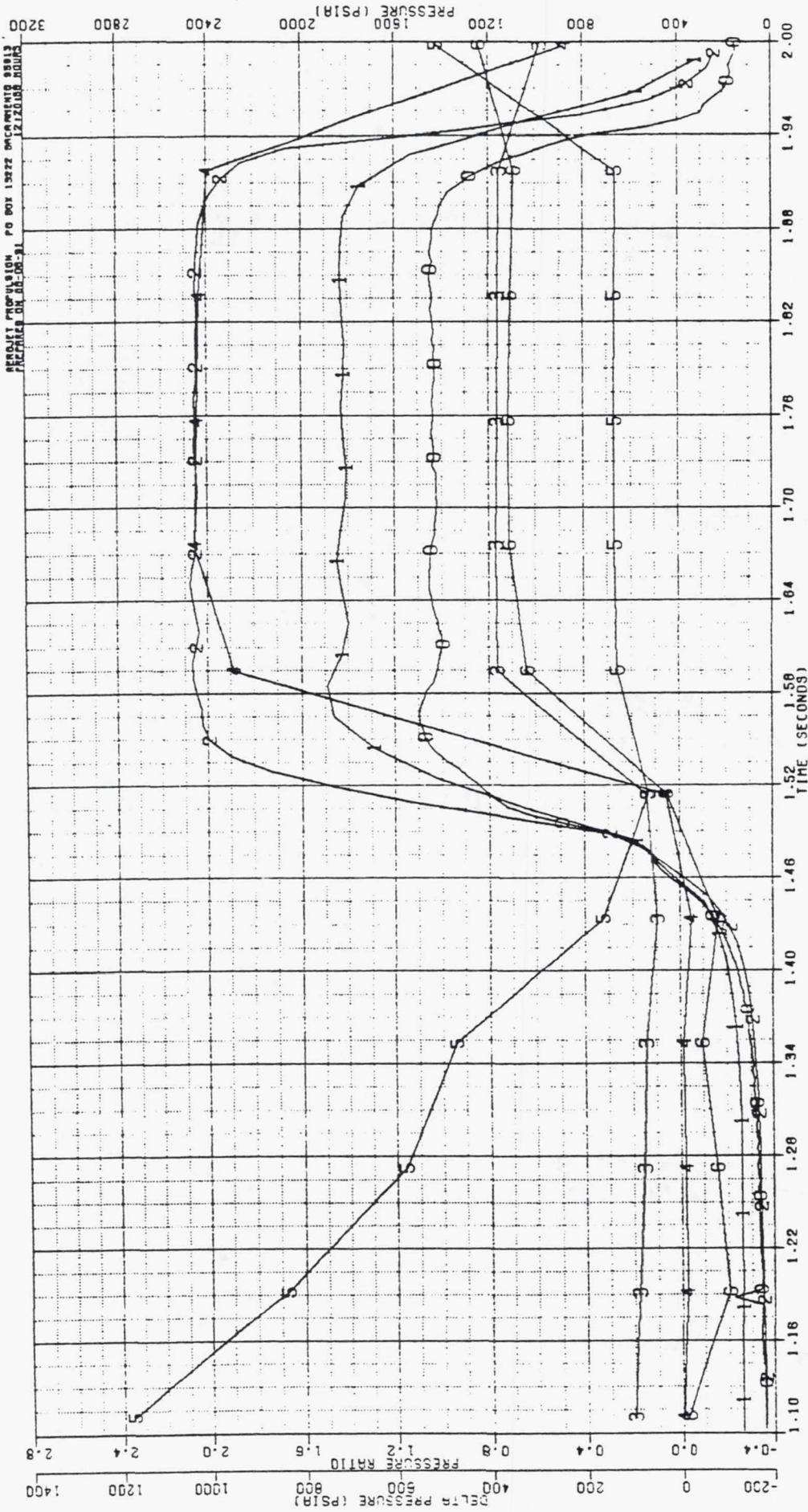


RESULTS PRESENTED FOR EACH INJECTOR CONFIGURATION
 PRESENTED ON DE-00-011

**ROCCIO SUBSCALE INJECTOR
 PERFORMANCE PARAMETERS**

TEST DATE 04-01-91 AT 1407 HOURS DURATION 1.4613 SECONDS
 TEST NUMBER KFN7-001-1J-004 TEST STAND E-4

**GENCORP
 AEROJET**

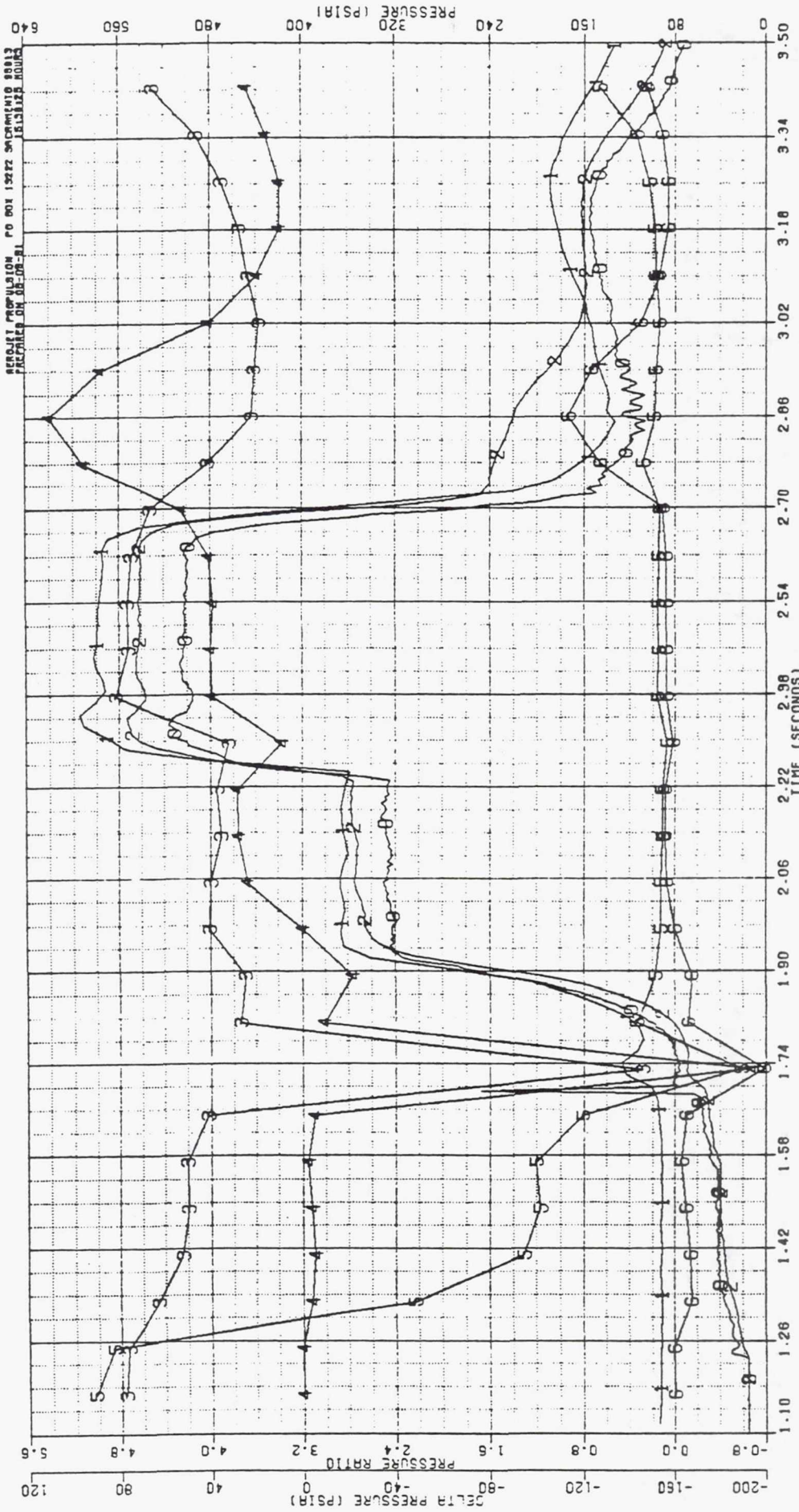


ROCCID SUBSCALE INJECTOR
 PERFORMANCE PARAMETERS

TEST DATE 04-04-91 AT 1115 HOURS DURATION 1.853 SECONDS
 TEST NUMBER KFN7-001-1J-007 TEST STAND E-4



- 0 PC-3 PSIA
- 1 FOJ PSIA
- 2 PFJ PSIA
- 3 DPO PSIA
- 4 DPF PSIA
- 5 DPO/PC
- 6 DPF/PC



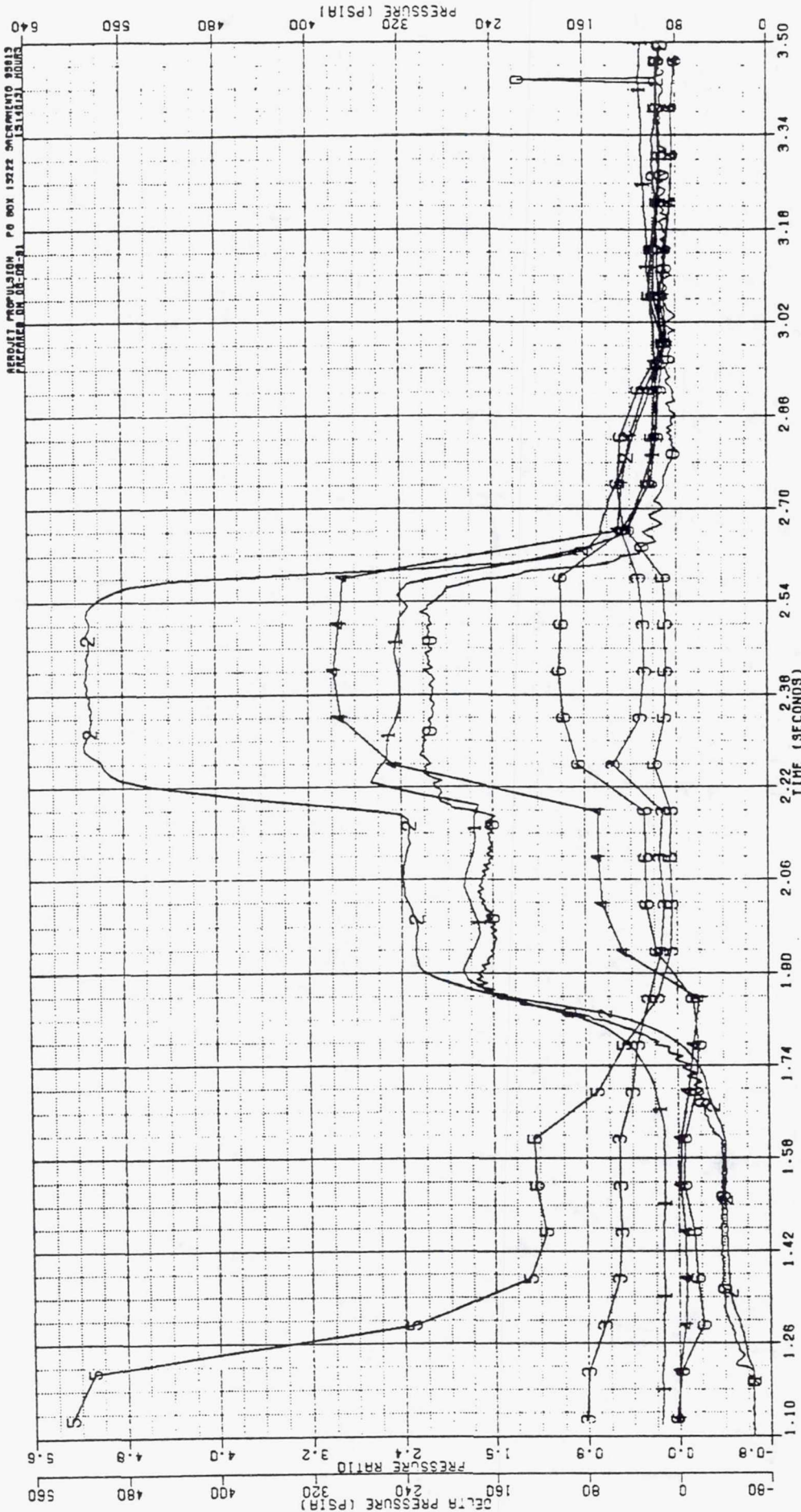
AEROJET PROPULSION PO BOX 13222 SACRAMENTO 95813
 FILED ON 08-08-91 15:33:25 HOURS

**ROCCID SUBSCALE INJECTOR
 PERFORMANCE PARAMETERS**

TEST DATE 04-04-91 AT 1522 HOURS DURATION 2.569 SECONDS
 TEST NUMBER KFN7-001-1J-009 TEST STAND E-4



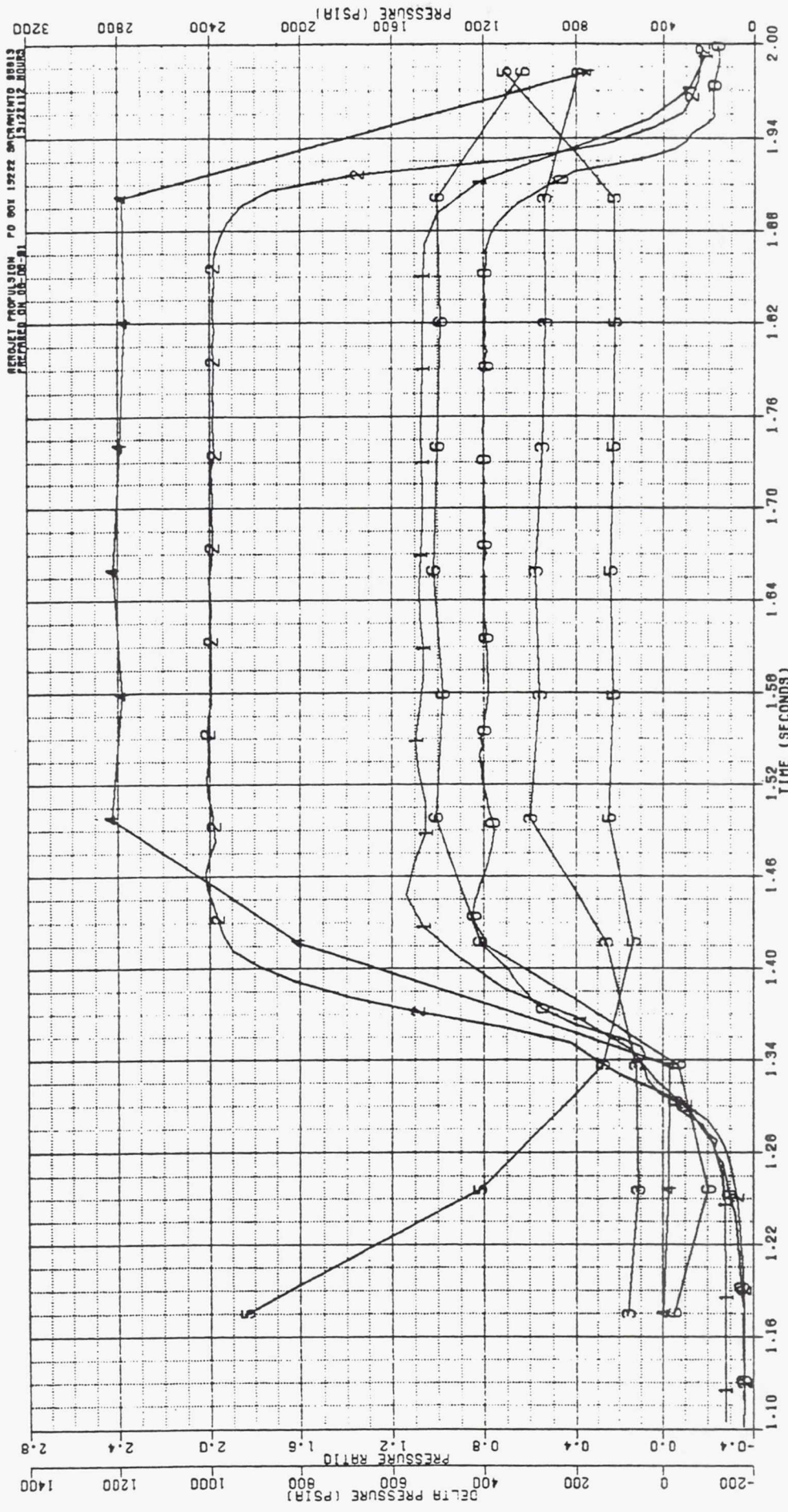
- 0 PC-3 PSIA
- 1 POJ PSIA
- 2 PFJ PSIA
- 3 DFO PSIA
- 4 DFF PSIA
- 5 DPF/PC
- 6 DPF/PC



**ROCCID SUBSCALE INJECTOR
 PERFORMANCE PARAMETERS**

TEST DATE 04-08-91 AT 1409 HOURS DURATION 2.494 SECONDS
 TEST NUMBER KFN7-D01-1J-012 TEST STAND E-4



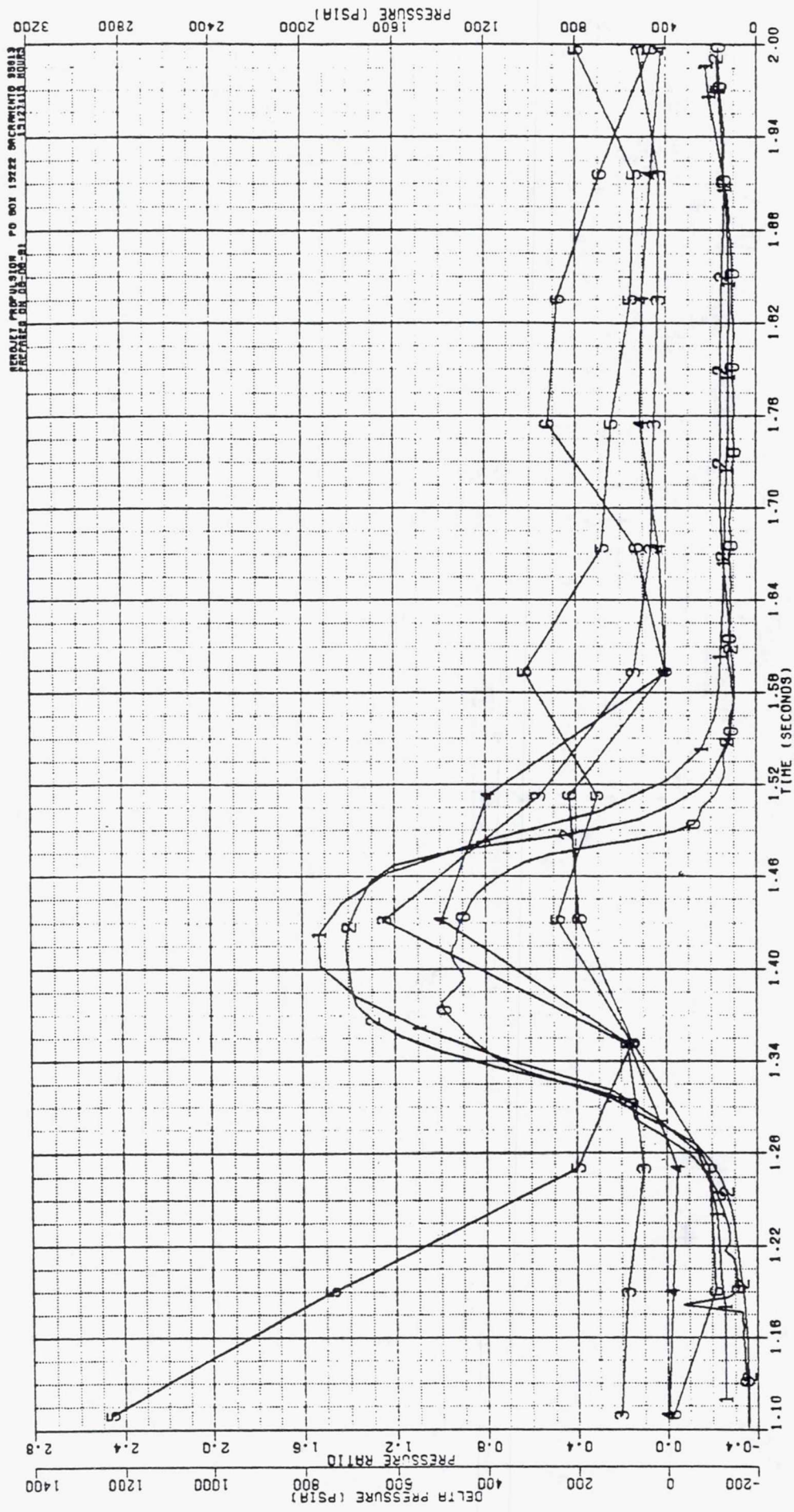


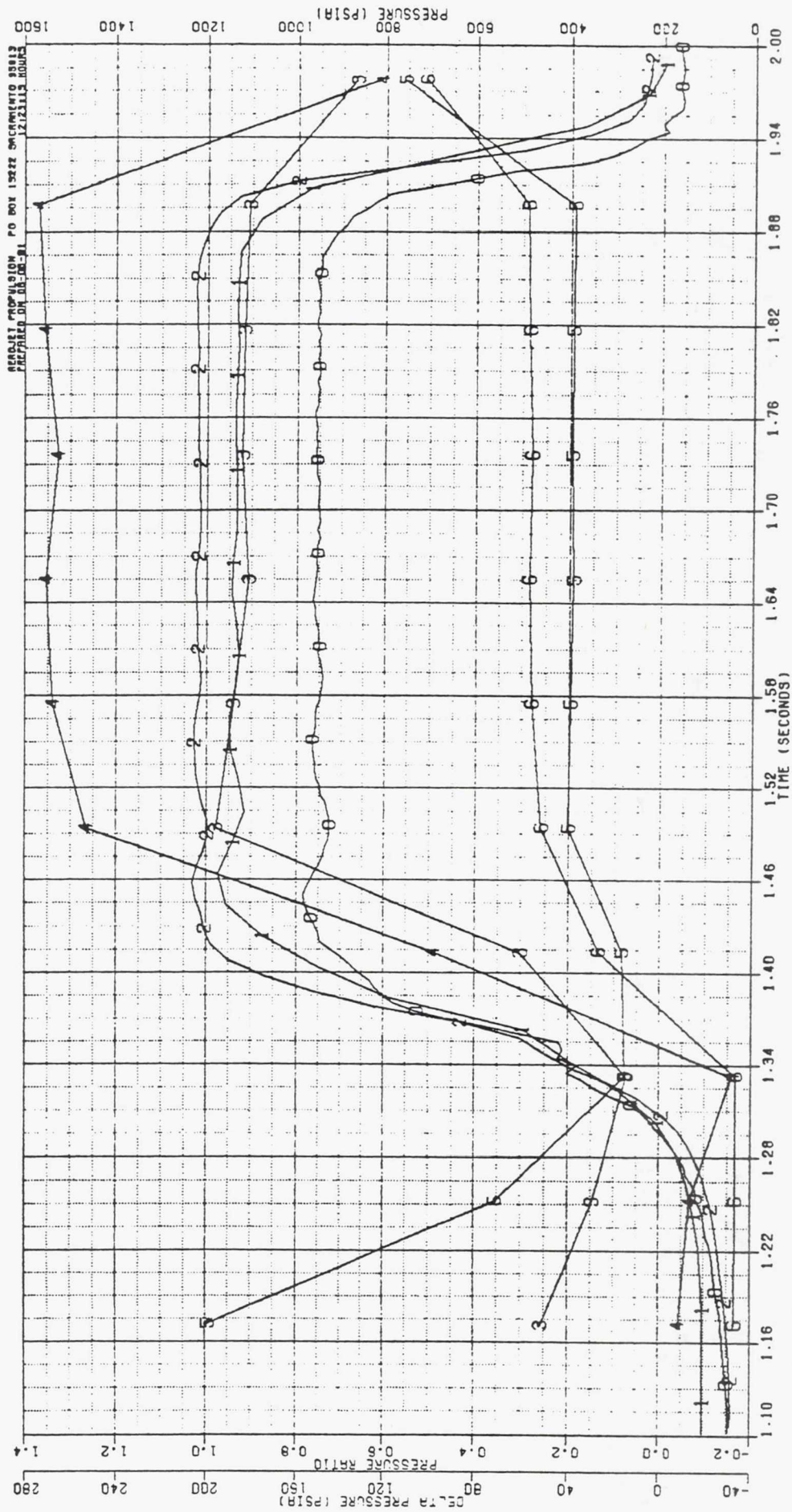
**ROCCID SUBSCALE INJECTOR
PERFORMANCE PARAMETERS**

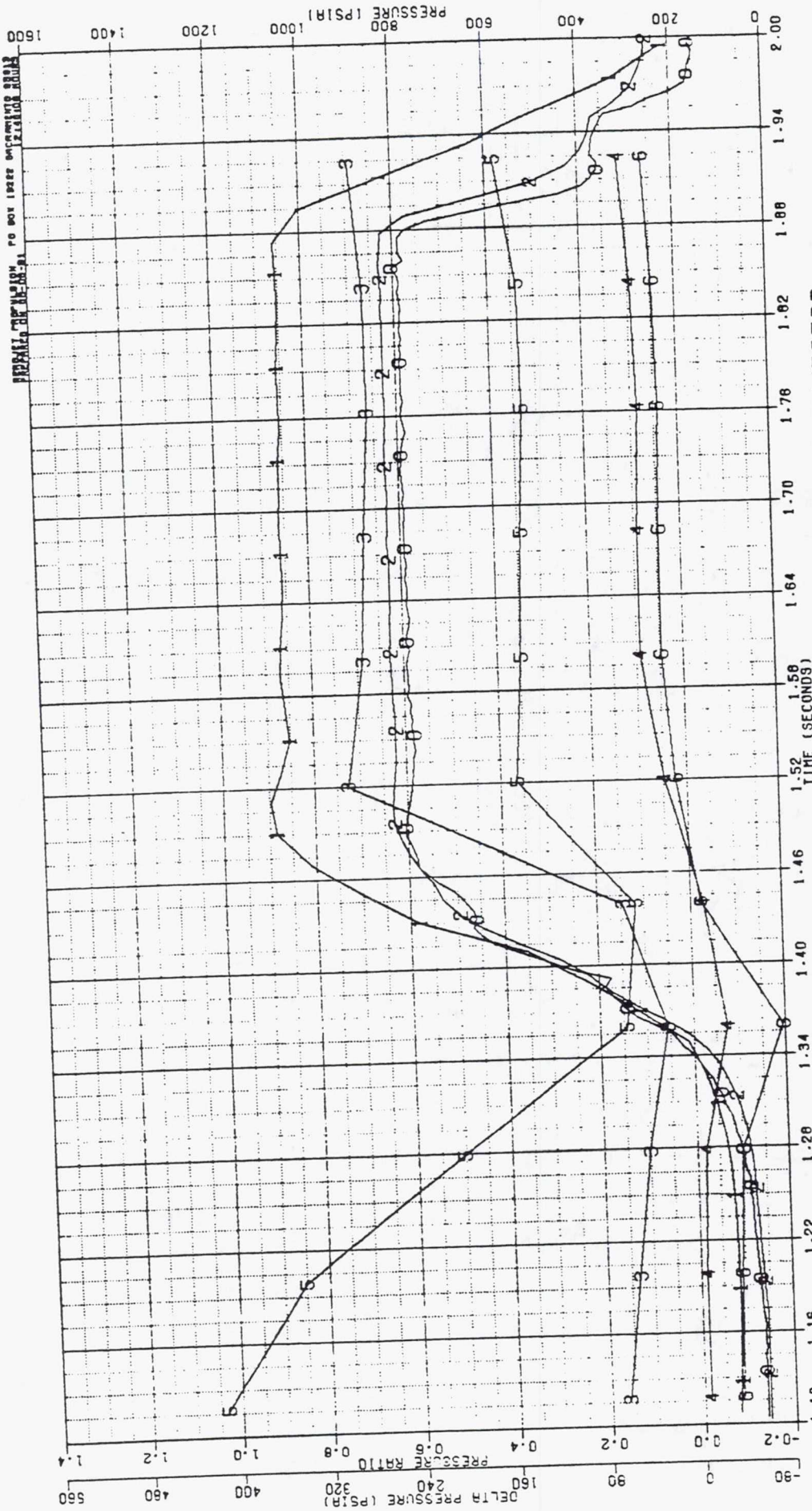
TEST DATE 04-08-91 AT 1750 HOURS DURATION 1.823 SECONDS
TEST NUMBER KFN7-001-1J-013 TEST STAND E-4



- 0 PC-3 PSIA
- 1'POJ PSIA
- 2 PFJ PSIA
- 3 DPO PSIA
- 4 DPF PSIA
- 5 DPO/PC
- 6 DPF/PC





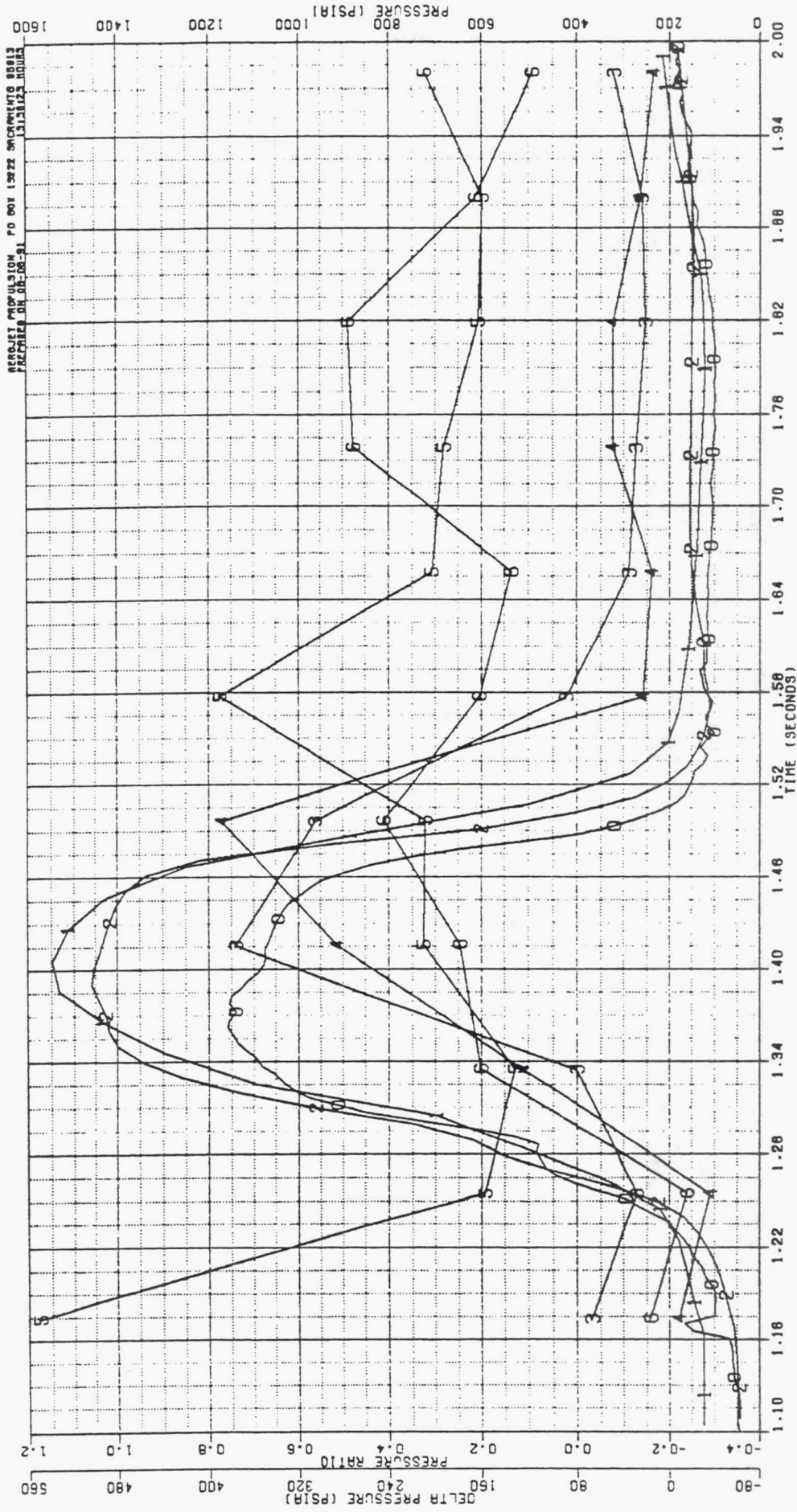


**ROCCID SUBSCALE INJECTOR
 PERFORMANCE PARAMETERS**

TEST DATE 04-09-91 AT 1553 HOURS DURATION 1.836 SECONDS
 TEST NUMBER KFN7-001-1J-017 TEST STAND E-4



- 0 PC-3 PSIA
- 1 POU PSIA
- 2 PFJ PSIA
- 3 OP0 PSIA
- 4 OPF PSIA
- 5 OP0/PC
- 6 OPF/PC

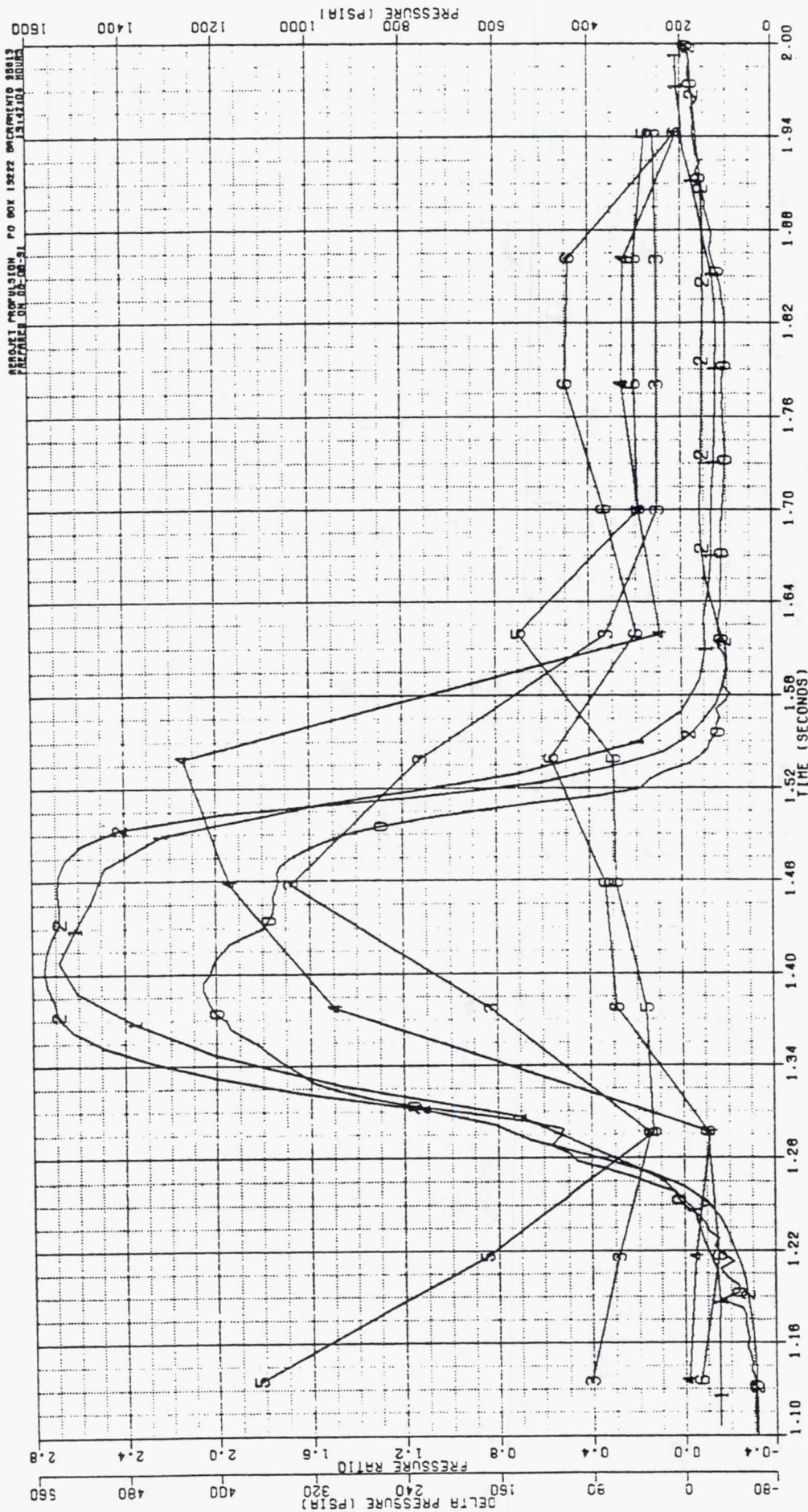


**ROCCID SUBSCALE INJECTOR
 PERFORMANCE PARAMETERS**

TEST DATE 04-10-91 AT 1105 HOURS DURATION 1.383 SECONDS
 TEST NUMBER KFN7-001-1J-010 TEST STAND E-4



- 0 PC-3 PSIA
- 1 POJ PSIA
- 2 PFJ PSIA
- 3 DPO PSIA
- 4 DPF PSIA
- 5 DPO/PC
- 6 DPF/PC

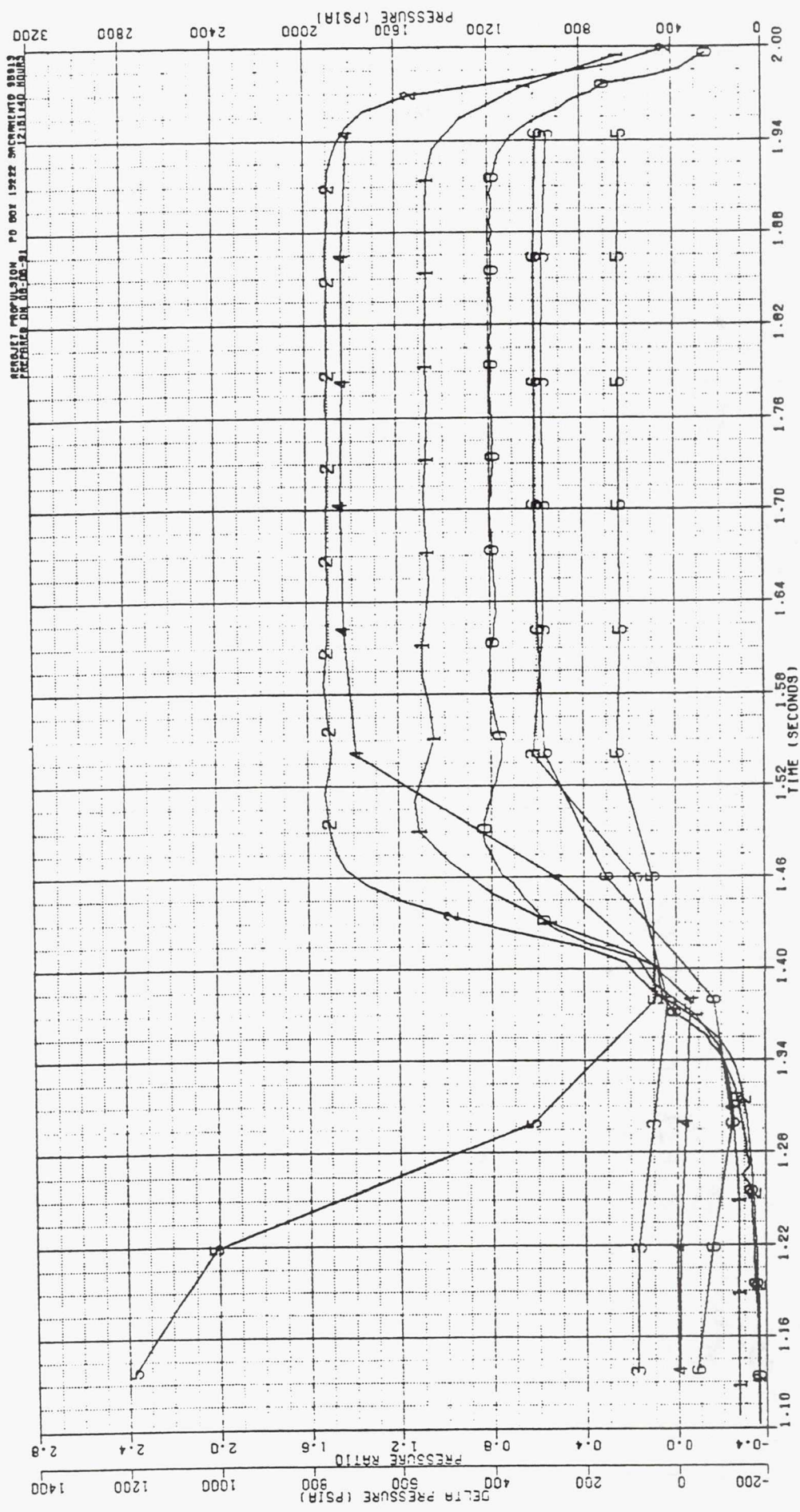


**ROCCIO SUBSCALE INJECTOR
 PERFORMANCE PARAMETERS**

TEST DATE 04-10-91 AT 1341 HOURS DURATION 1.403 SECONDS
 TEST NUMBER KFN7-001-1J-019 TEST STAND E-4



- 0 PC-3 PSIA
- 1 POJ PSIA
- 2 PFJ PSIA
- 3 DPO PSIA
- 4 OPF PSIA
- 5 OPO/PC
- 6 OPF/PC



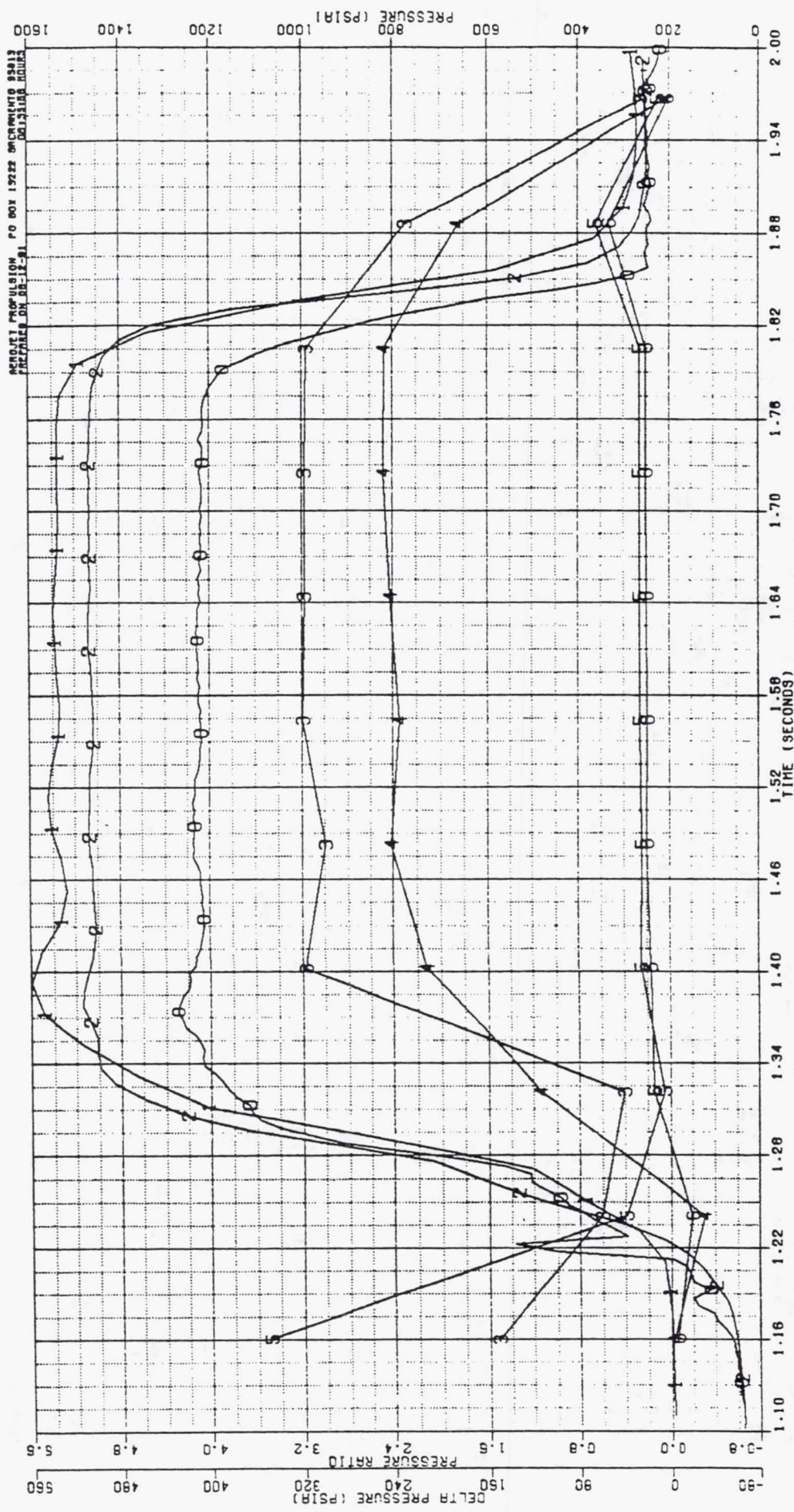
AEROJET PROPULSION PO BOX 137222 SACRAMENTO 95813
 PREPARED ON 08-06-91

**ROCCID SUBSCALE INJECTOR
 PERFORMANCE PARAMETERS**

TEST DATE 04-10-91 AT 1455 HOURS DURATION 1.865 SECONDS
 TEST NUMBER KFN7-D01-1J-020 TEST STAND E-4



- 0 PC-3 PSIA
- 1 POJ PSIA
- 2 PFJ PSIA
- 3 PO PSIA
- 4 DPF PSIA
- 5 DPO/PC
- 6 DPF/PC

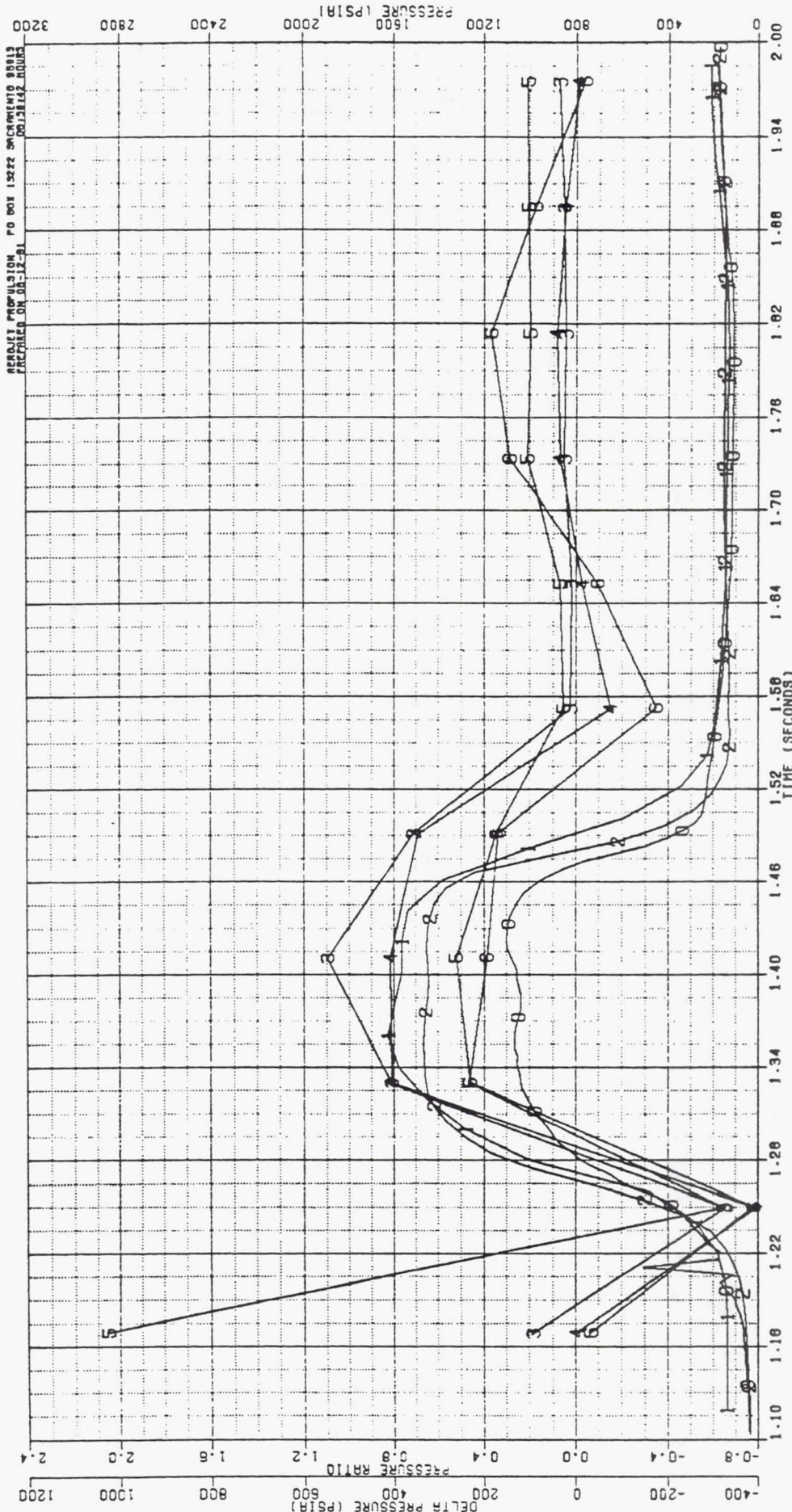


**ROCCID SUBSCALE INJECTOR
PERFORMANCE PARAMETERS**

TEST DATE 04-15-91 AT 1342 HOURS DURATION 1.744 SECONDS
TEST NUMBER KFN7-001-1J-021 TEST STAND E-4



- 0 PC-3 PSIA
- 1 POJ PSIA
- 2 PFJ PSIA
- 3 OPD PSIA
- 4 OPF PSIA
- 5 OPD/PC
- 6 OPF/PC

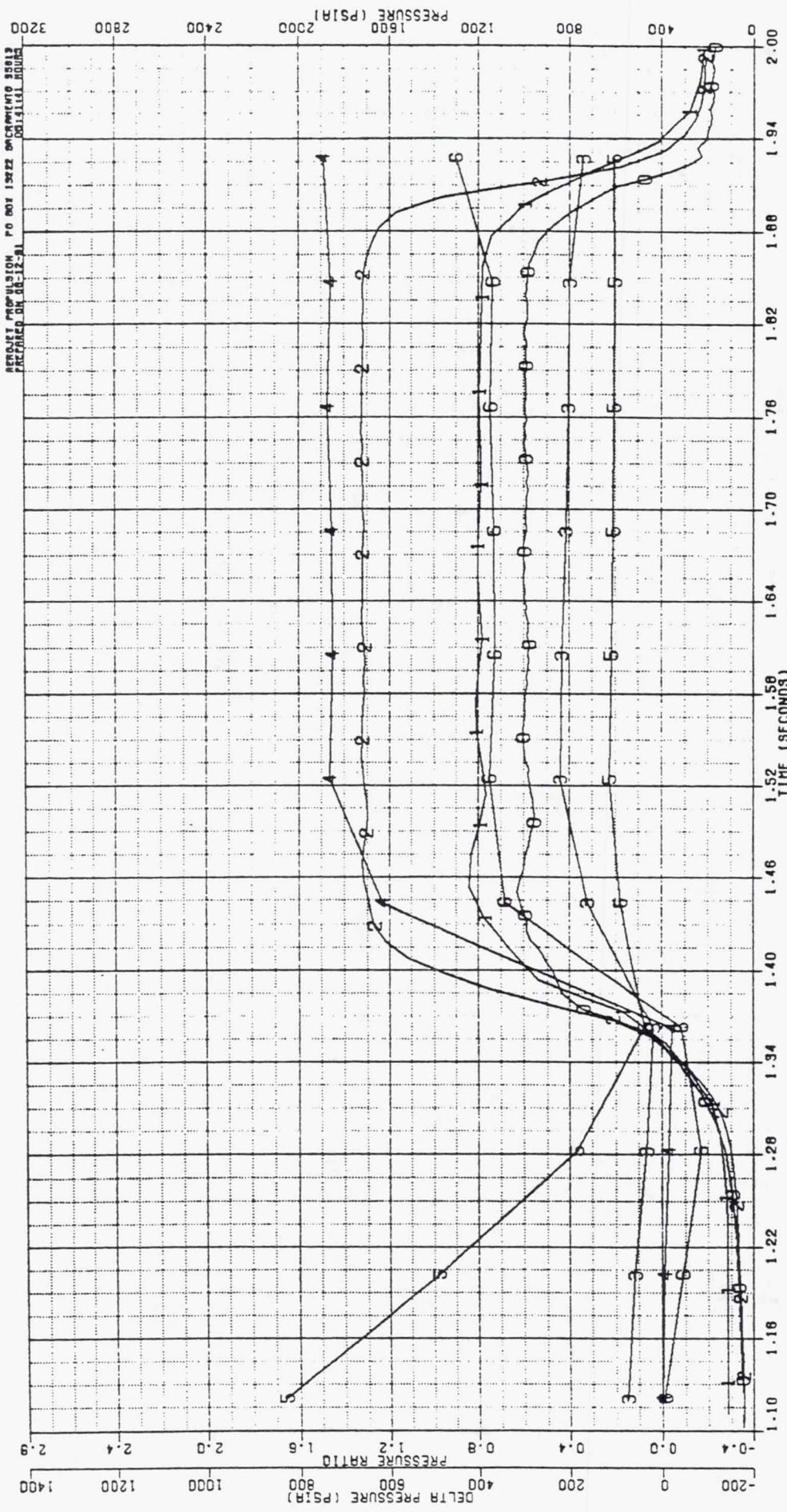


**ROCCID SUBSCALE INJECTOR
PERFORMANCE PARAMETERS**

TEST DATE 04-15-91 AT 1439 HOURS DURATION 1.366 SECONDS
TEST NUMBER KFN7-001-1J-022 TEST STAND E-4



- 0 PC-3
- 1 POU
- 2 PFJ
- 3 OPD
- 4 OPF
- 5 OPD/PC
- 6 OPF/PC
- PSIA
- PSIA
- PSIA
- PSIA
- PSIA



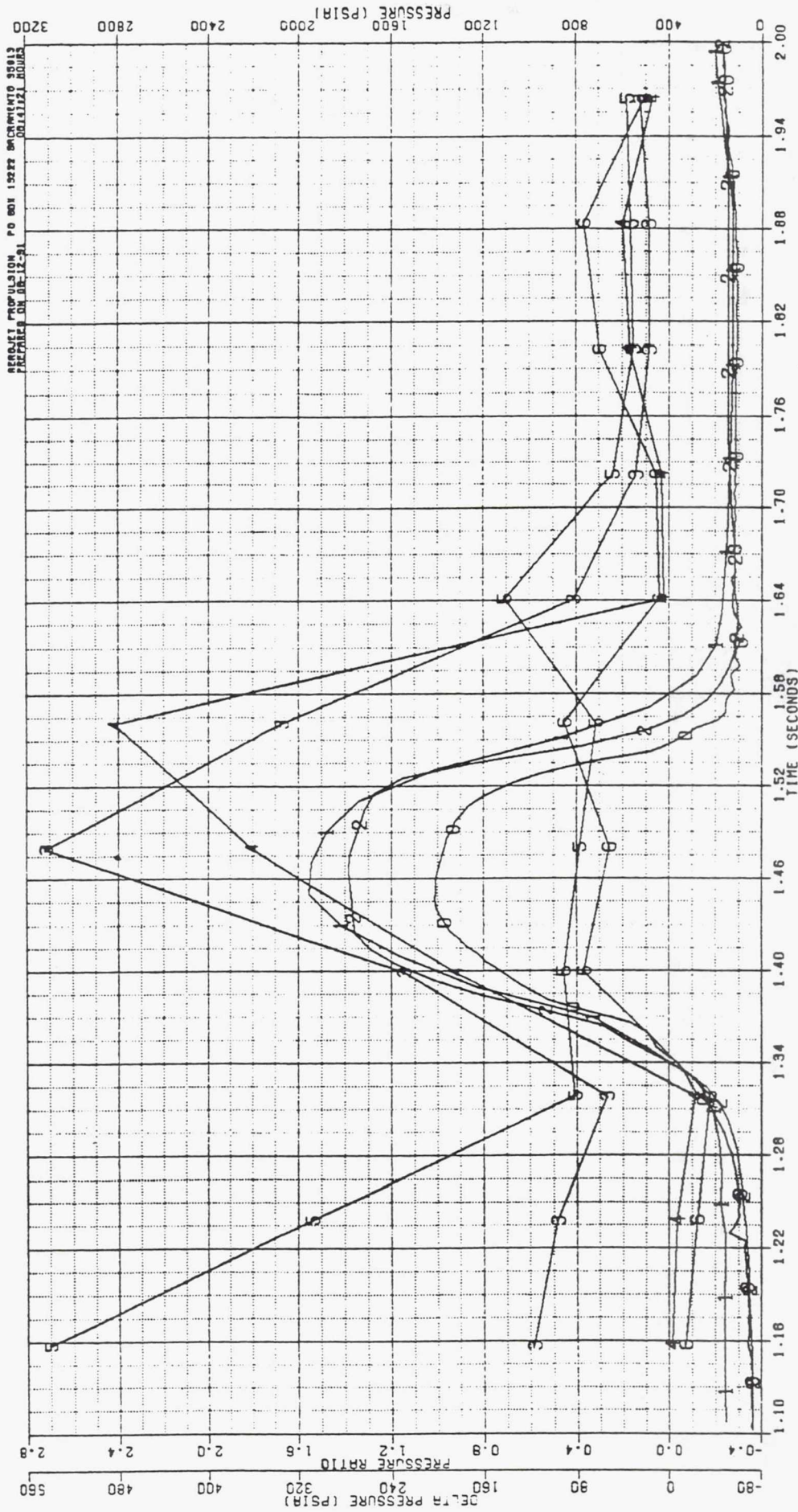
AEROJET PROPULSION PO BOX 13722 CHICAGO, ILL 60613
 PREPARED ON 08-12-91

ROCCID SUBSCALE INJECTOR PERFORMANCE PARAMETERS

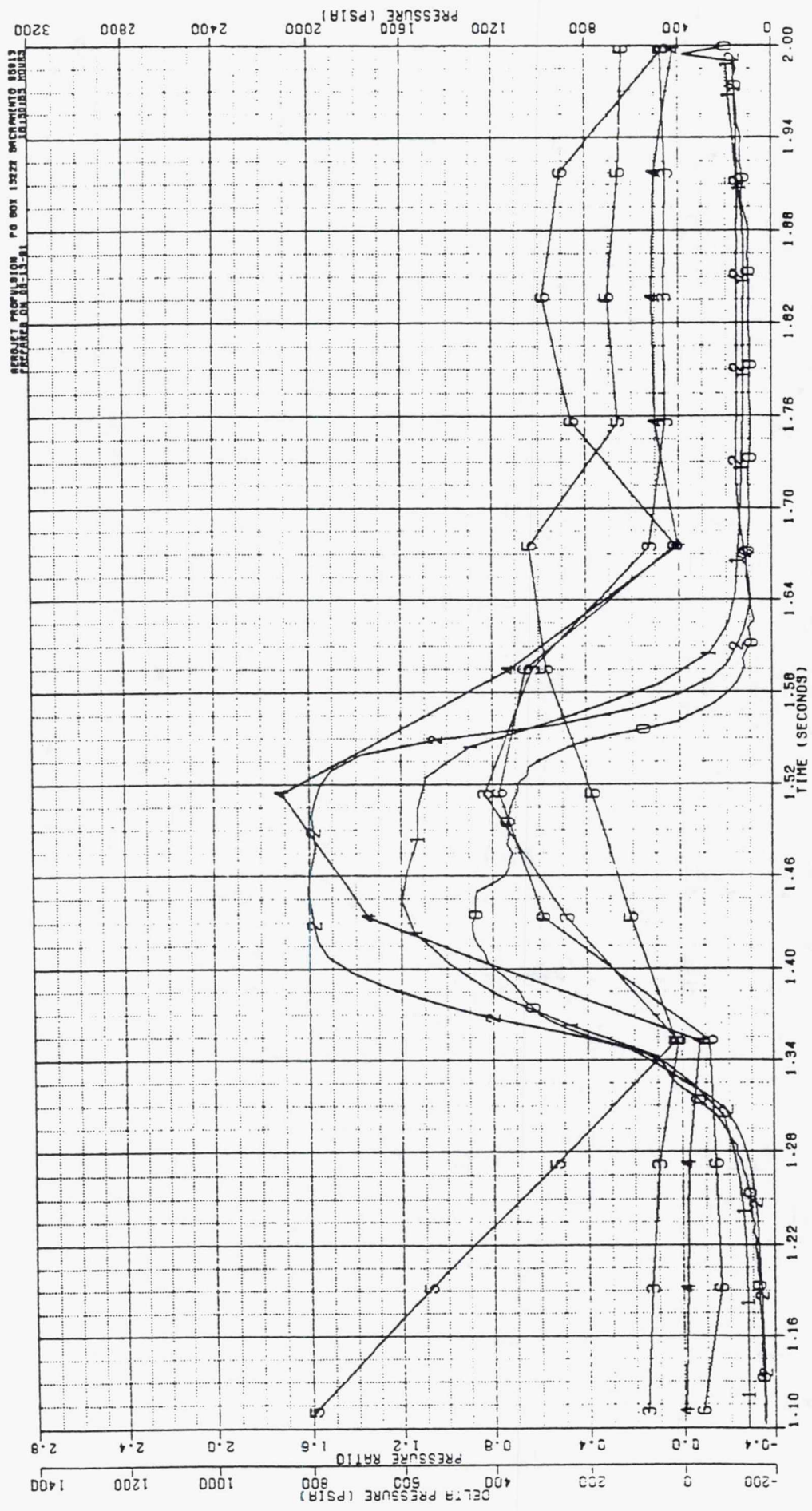
TEST DATE 04-17-91 AT 1000 HOURS DURATION 1.825 SECONDS
 TEST NUMBER KFN7-001-1J-023 TEST STAND E-4



- 0 PC-3 PSIA
- 1 PDJ PSIA
- 2 PFJ PSIA
- 3 OPD PSIA
- 4 OPF PSIA
- 5 OPD/PC
- 6 OPF/PC



GENCORP
AEROJET



PRESSURE RATIO
 PRESSURE (PSIA)

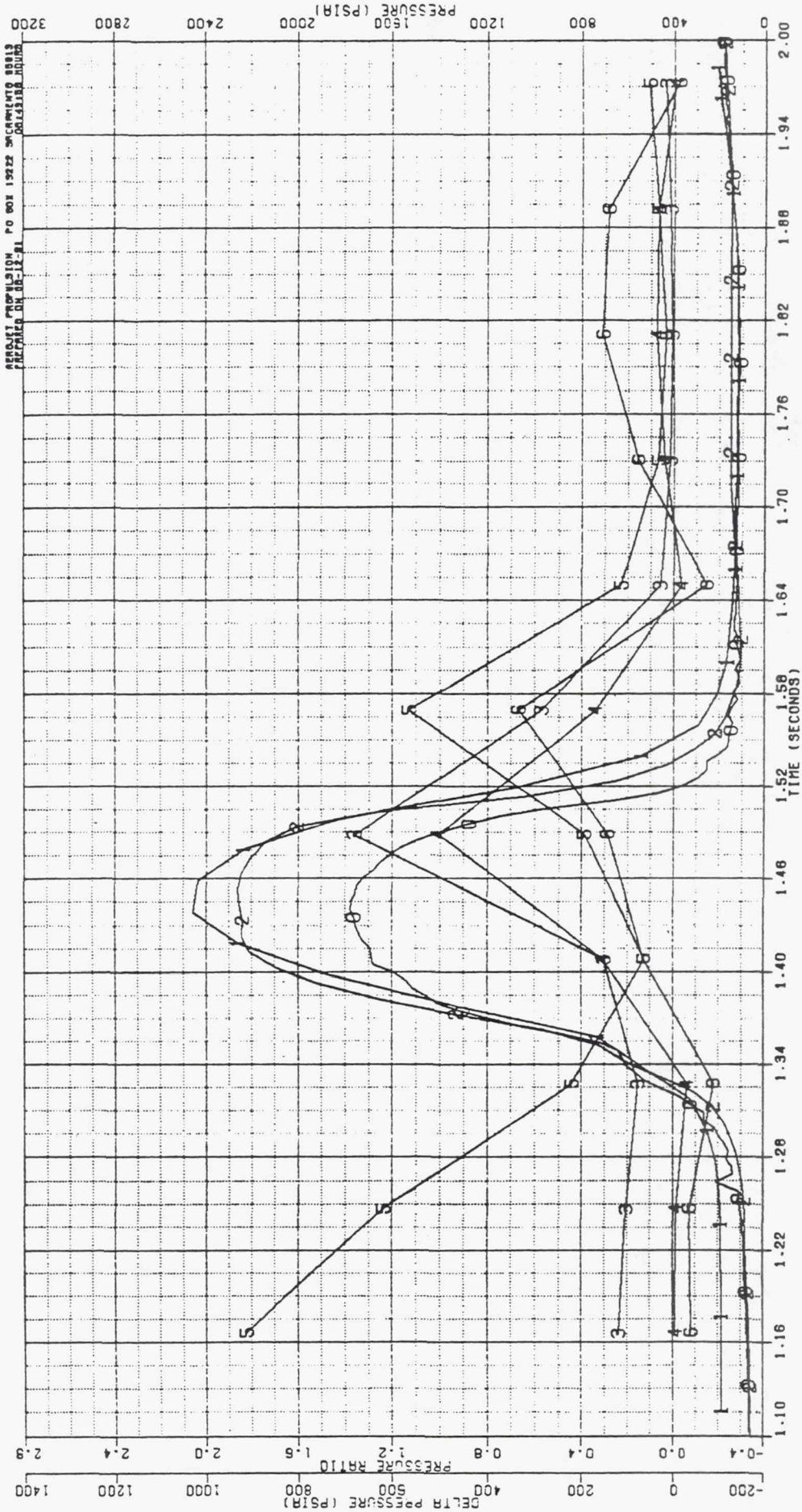
PO BOX 13222 OMAHA NE 68113
 1315 HOURS

**ROCCIO SUBSCALE INJECTOR
 PERFORMANCE PARAMETERS**

TEST DATE 04-22-91 AT 1315 HOURS DURATION 1.464 SECONDS
 TEST NUMBER KFN7-D01-1J-026 TEST STAND E-4

- 0 PC-3 PSIA
- 1 POJ PSIA
- 2 PFJ PSIA
- 3 OPD PSIA
- 4 OPF PSIA
- 5 OPD/PC
- 6 OPF/PC



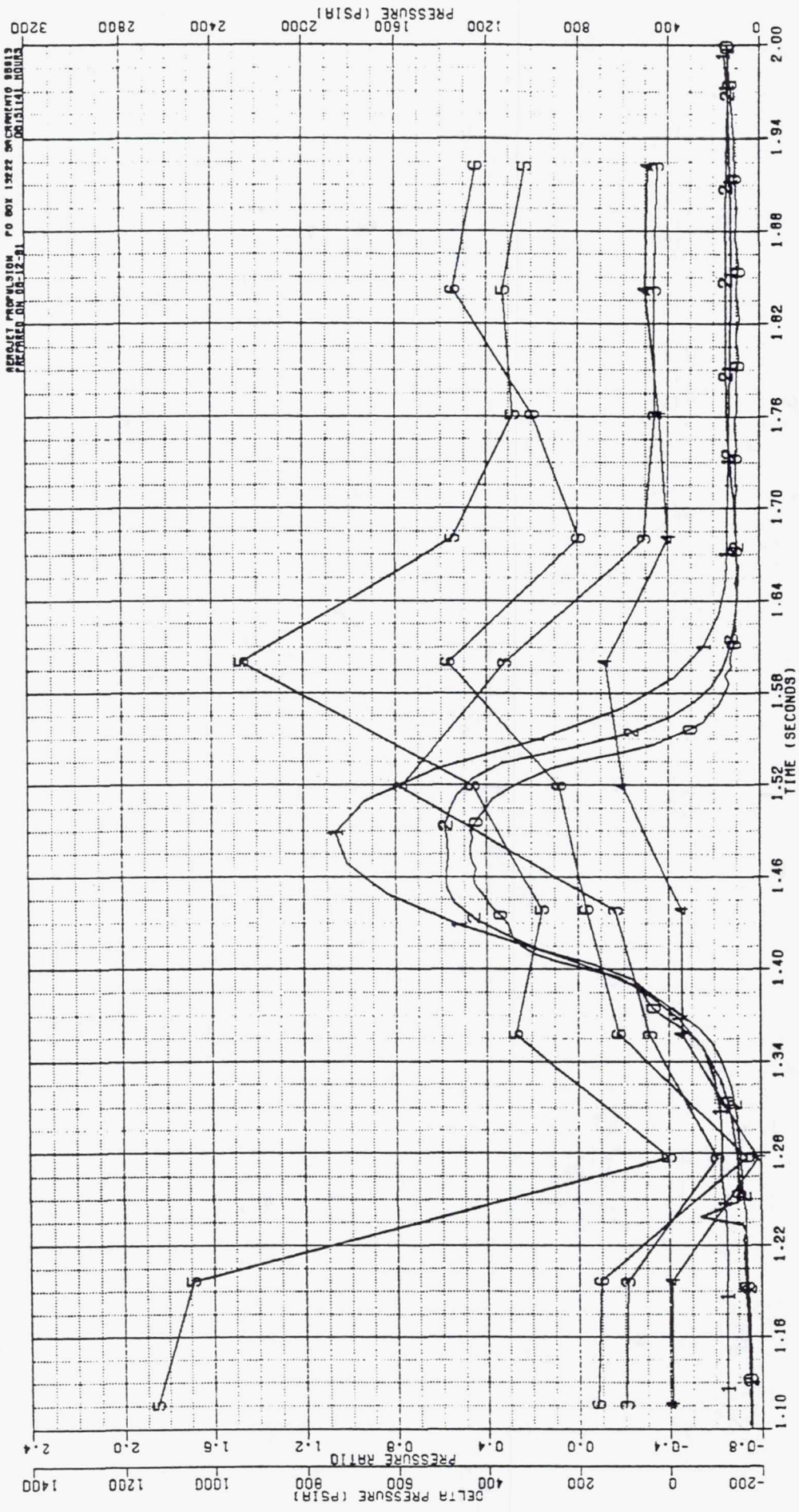


- 0 PC-3 PSIA
- 1 POJ PSIA
- 2 PFJ PSIA
- 3 OP0 PSIA
- 4 DPF PSIA
- 5 DP0/PC
- 6 DPF/PC

**ROCCID SUBSCALE INJECTOR
PERFORMANCE PARAMETERS**

TEST DATE 04-23-91 AT 1056 HOURS DURATION 1.410 SECONDS
 TEST NUMBER KFN7-D01-1J-027 TEST STAND E-4

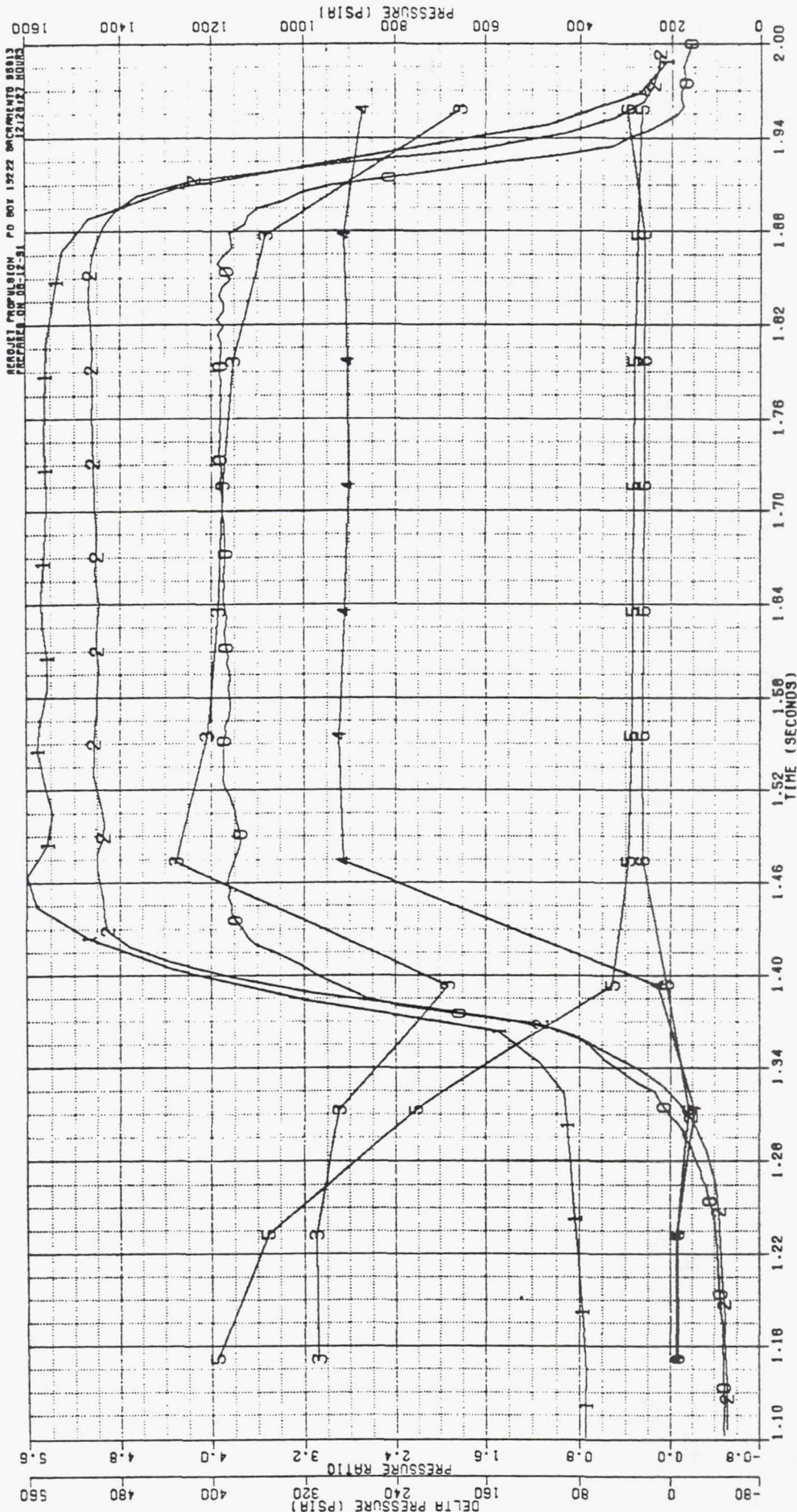
**GENCORP
AEROJET**



**ROCCID SUBSCALE INJECTOR
PERFORMANCE PARAMETERS**

TEST DATE 04-23-91 AT 1305 HOURS DURATION 1.436 SECONDS
TEST NUMBER KFN7-001-1J-028 TEST STAND E-4

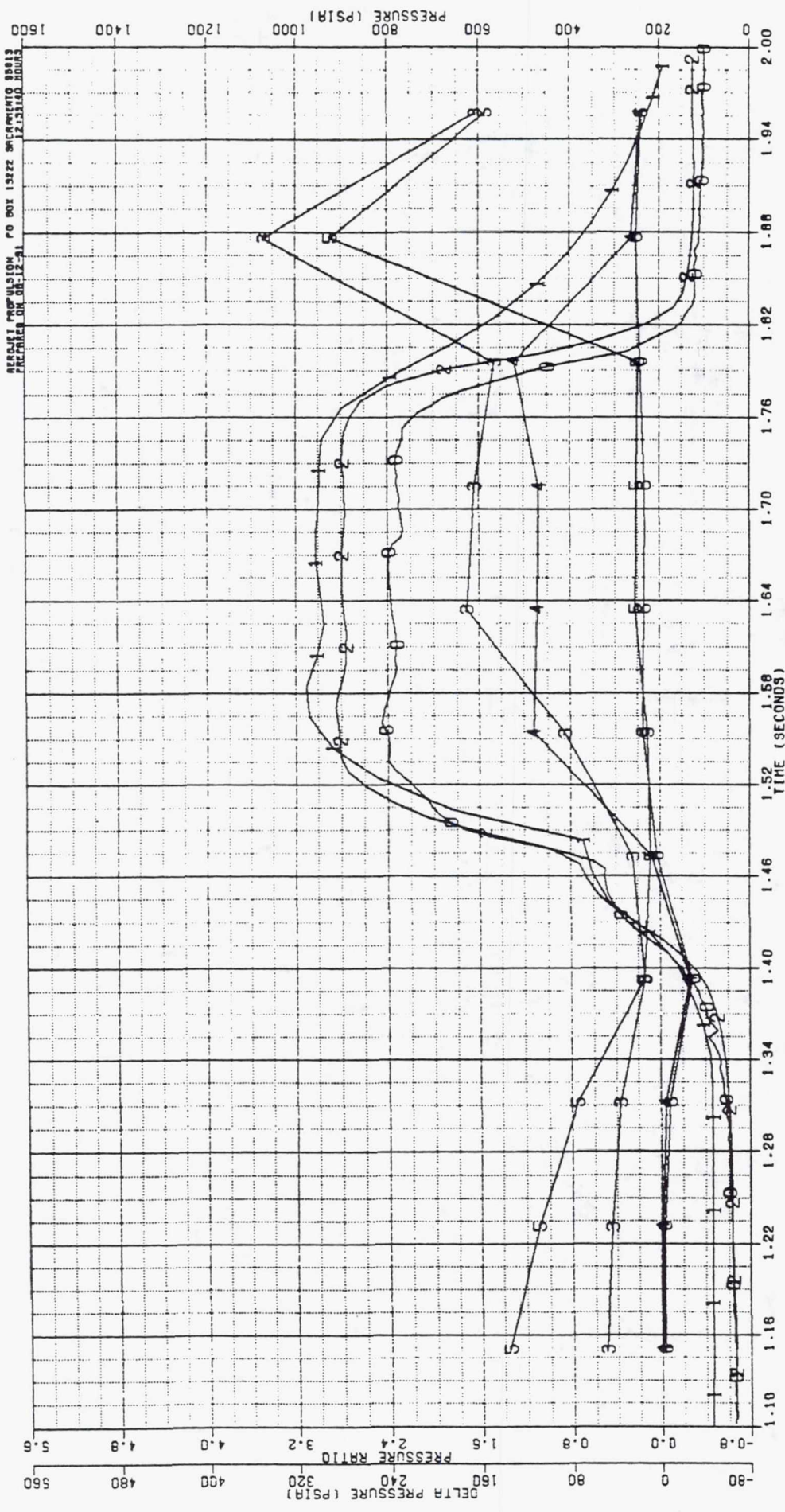




**ROCCID SUBSCALE INJECTOR
PERFORMANCE PARAMETERS**

TEST DATE 04-30-91 AT 1300 HOURS DURATION 1.835 SECONDS
TEST NUMBER KFN7-D01-1J-029 TEST STAND E-4



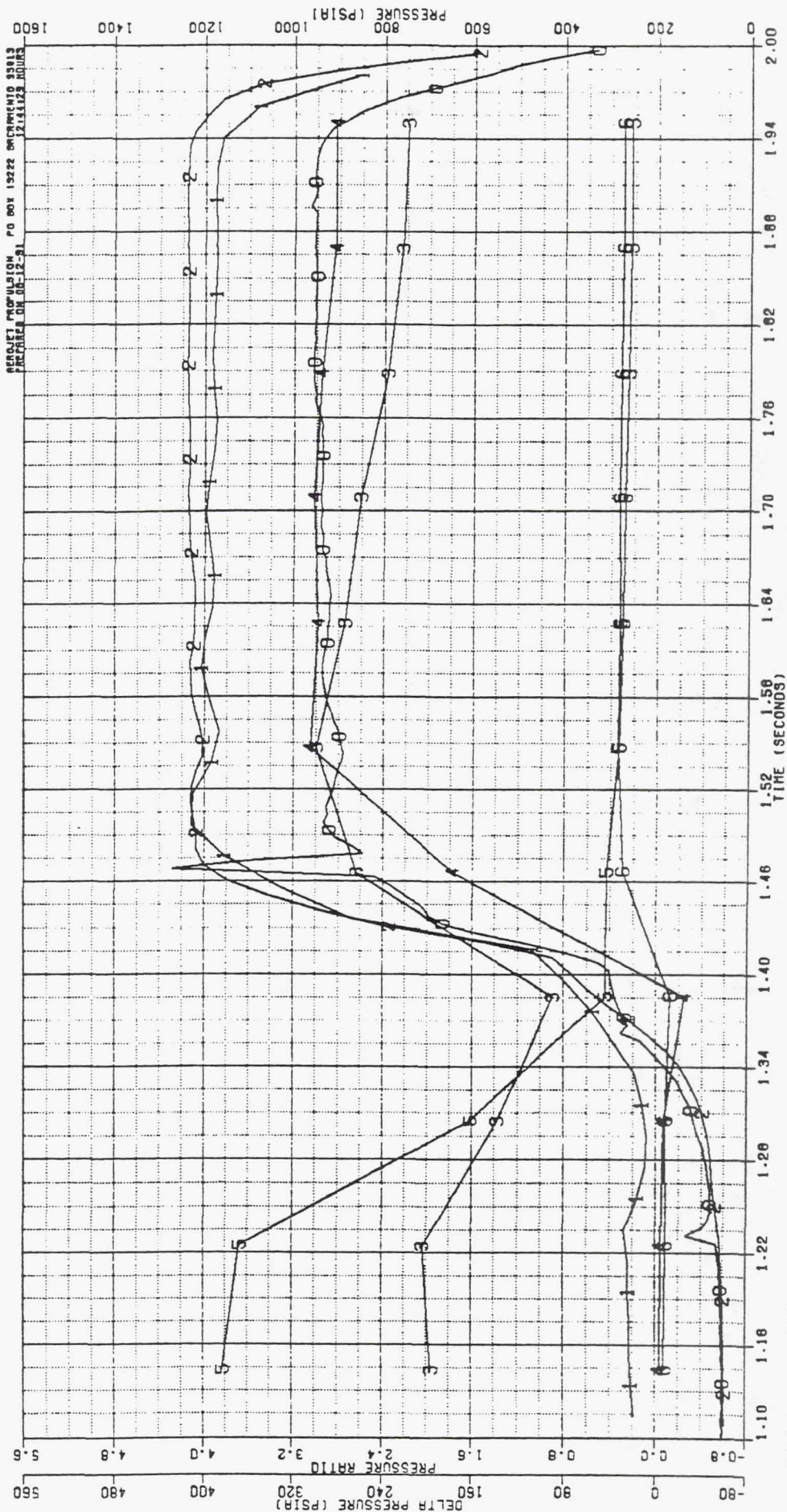


**ROCCID SUBSCALE INJECTOR
 PERFORMANCE PARAMETERS**

TEST DATE 04-30-91 AT 1441 HOURS DURATION 1.693 SECONDS
 TEST NUMBER KFN7-001-1J-030 TEST STAND E-4



- 0 PC-3 PSIA
- 1 FOJ PSIA
- 2 PFJ PSIA
- 3 DPD PSIA
- 4 DPF PSIA
- 5 DPF/PC
- 6 DPF/PC



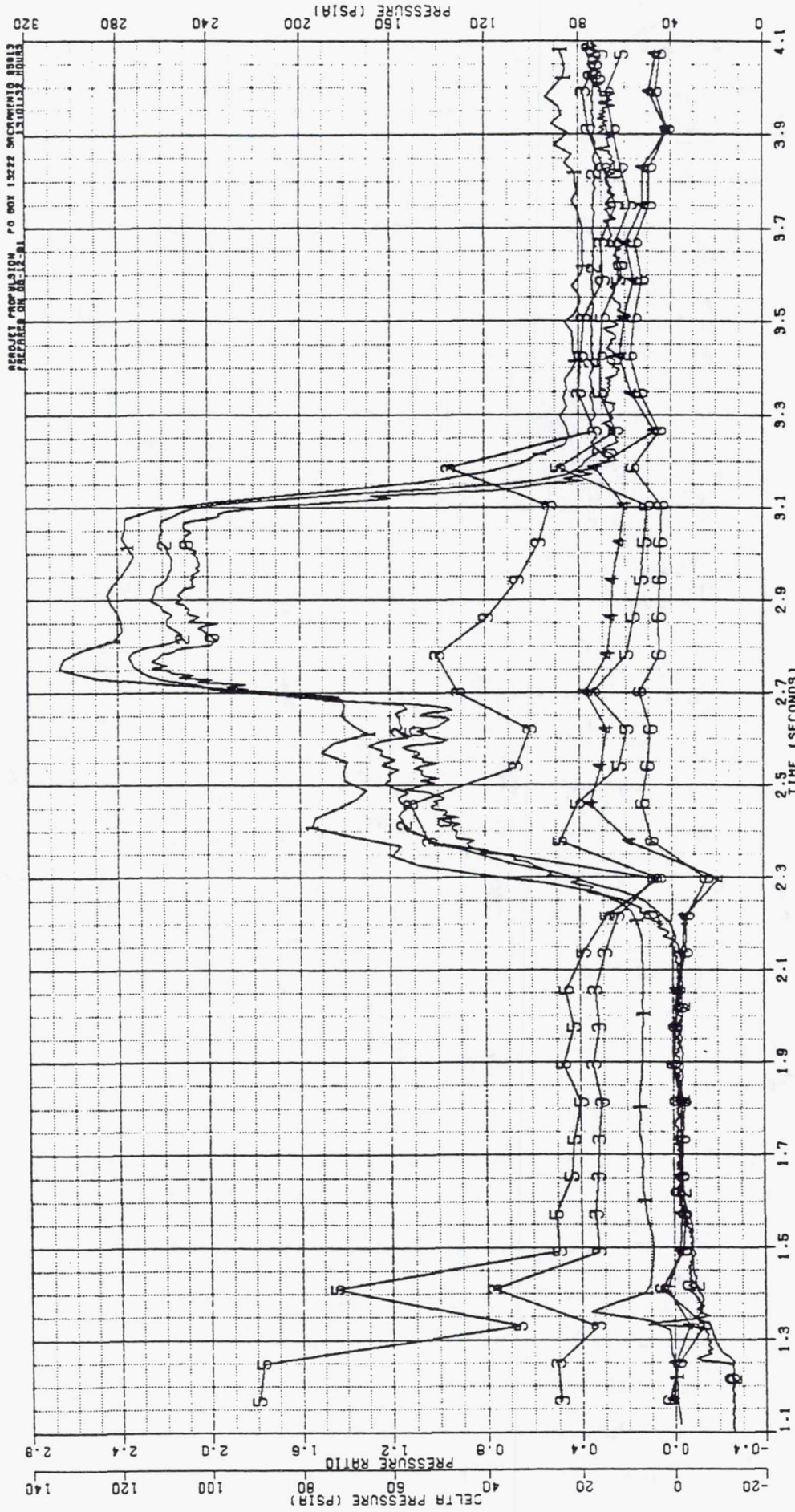
AEROJET PROPOSITION PO BOX 13222 CANTONMENT 95013
 PREPARED ON 08-12-91 12:11:25 HOURS

**ROCCID SUBSCALE INJECTOR
 PERFORMANCE PARAMETERS**

TEST DATE 05-01-91 AT 1102 HOURS DURATION 1.904 SECONDS
 TEST NUMBER KFN7-001-1J-031 TEST STAND E-4



- 0 PC-3 PSIA
- 1 POJ PSIA
- 2 PFJ PSIA
- 3 OPO PSIA
- 4 OPF PSIA
- 5 OPO/PC
- 6 OPF/PC



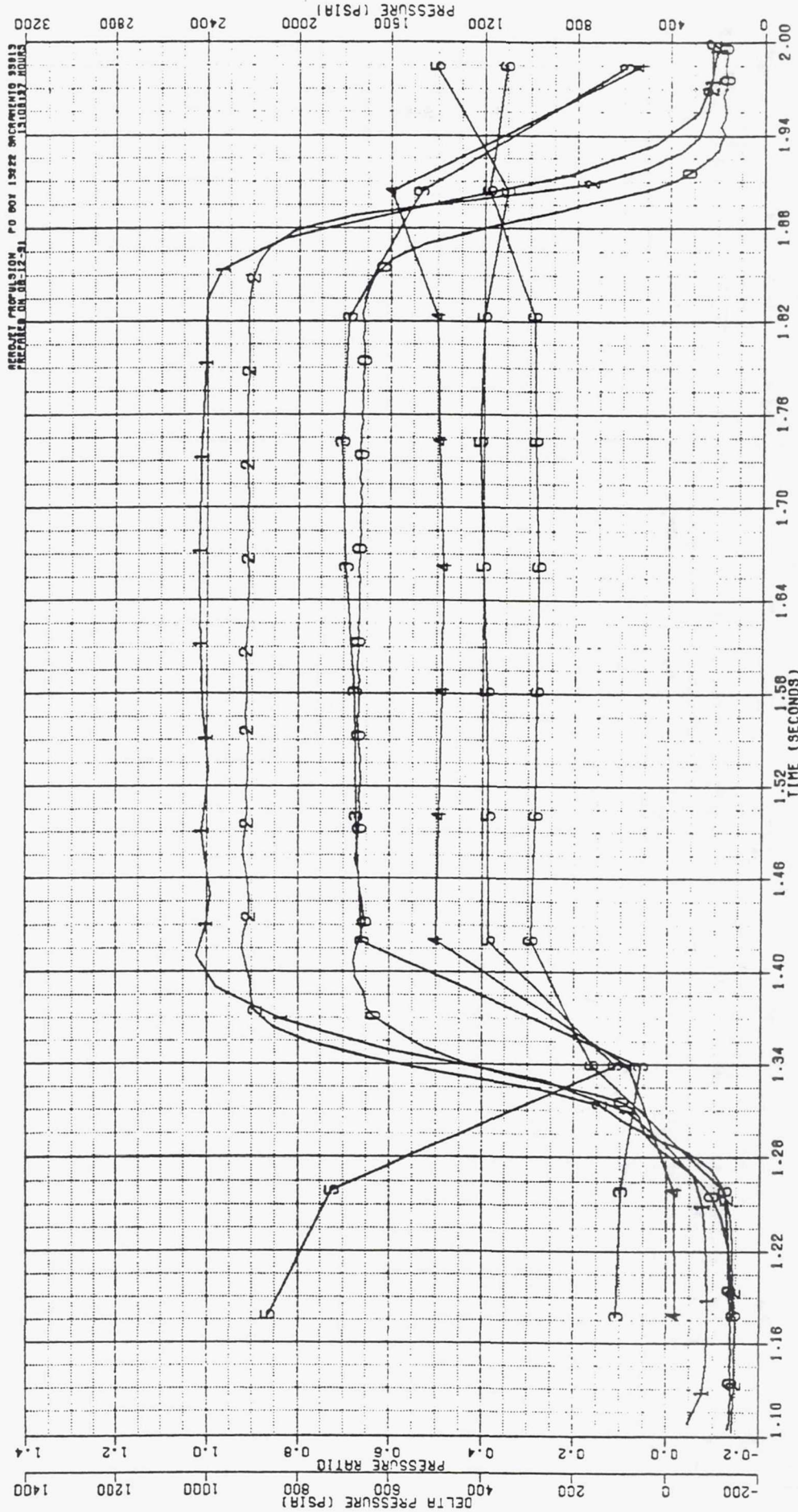
PRODUCT PROGRAM: ROCCID SUBSCALE INJECTOR
 TEST DATE: 05-01-91 AT 1618 HOURS
 TEST NUMBER: KFN7-001-1J-036
 TEST STAND: E-4

ROCCID SUBSCALE INJECTOR PERFORMANCE PARAMETERS

- 0 PC-3 PSIA
- 1 POJ PSIA
- 2 PFJ PSIA
- 3 OPD PSIA
- 4 OPF PSIA
- 5 OPD/PC
- 6 OPF/PC

TEST DATE 05-01-91 AT 1618 HOURS DURATION 3.016 SECONDS
 TEST NUMBER KFN7-001-1J-036 TEST STAND E-4



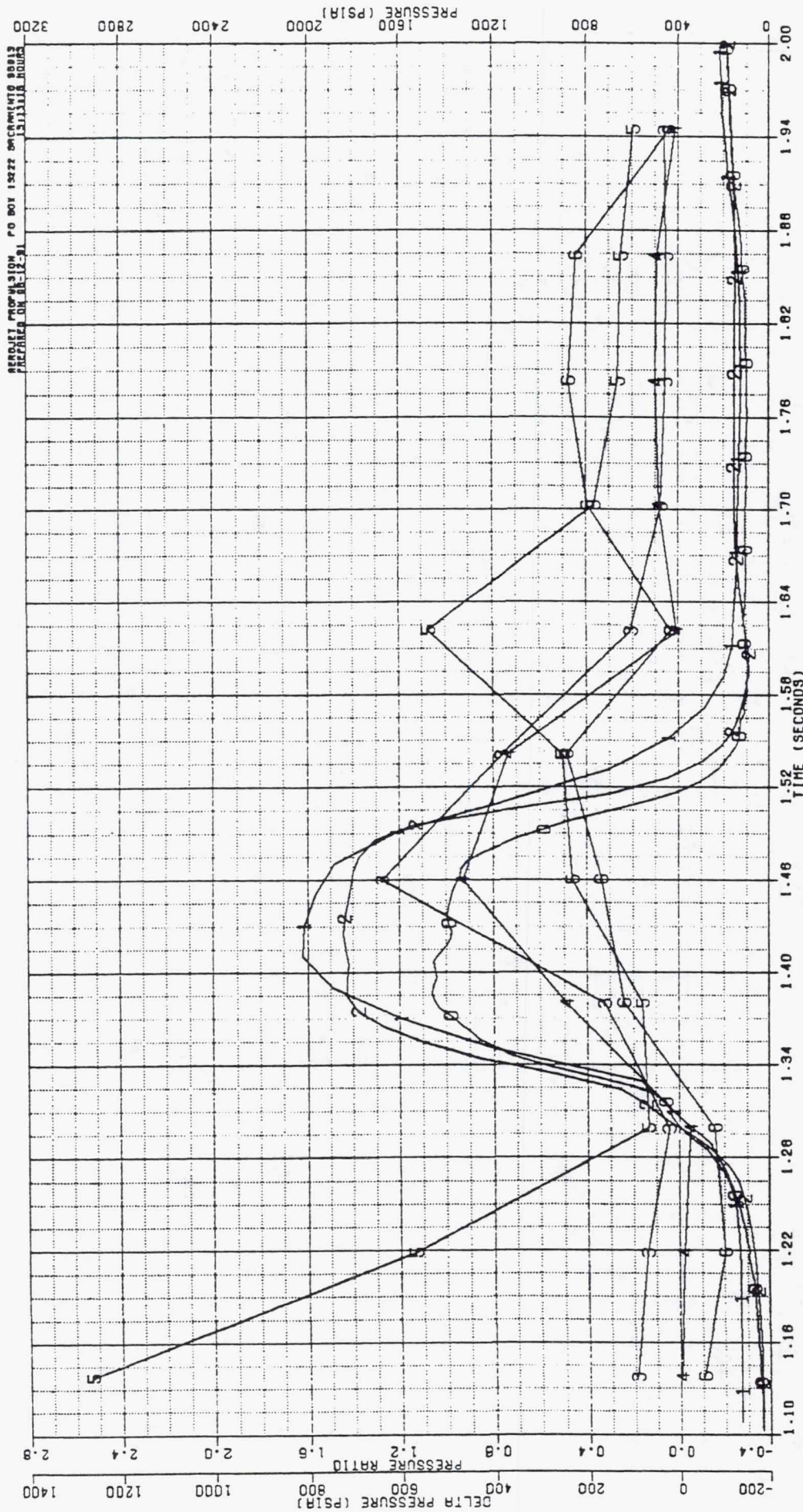


**ROCCIO SUBSCALE INJECTOR
 PERFORMANCE PARAMETERS**

TEST DATE 05-02-91 AT 1336 HOURS DURATION 1.805 SECONDS
 TEST NUMBER KFN7-001-1J-037 TEST STAND E-4

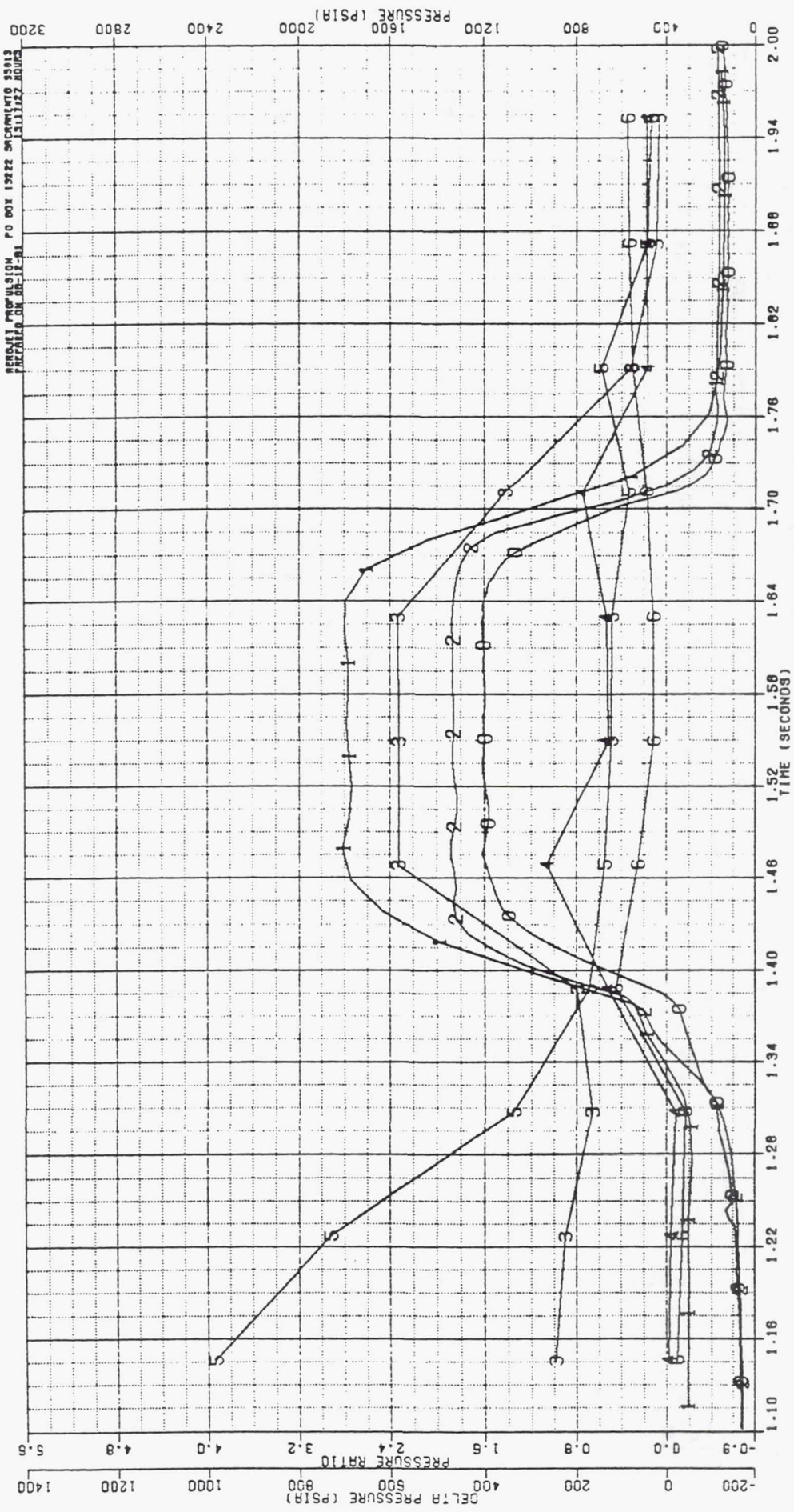


- 0 PC-3 PSIA
- 1 POJ PSIA
- 2 PFJ PSIA
- 3 DPO PSIA
- 4 DPF PSIA
- 5 DPO/PC
- 6 DPF/PC



- 0 PC-3 PSIA
- 1 OPJ PSIA
- 2 OPJ PSIA
- 3 OPF PSIA
- 4 OPF PSIA
- 5 OPF/PC PSIA
- 6 OPF/PC PSIA



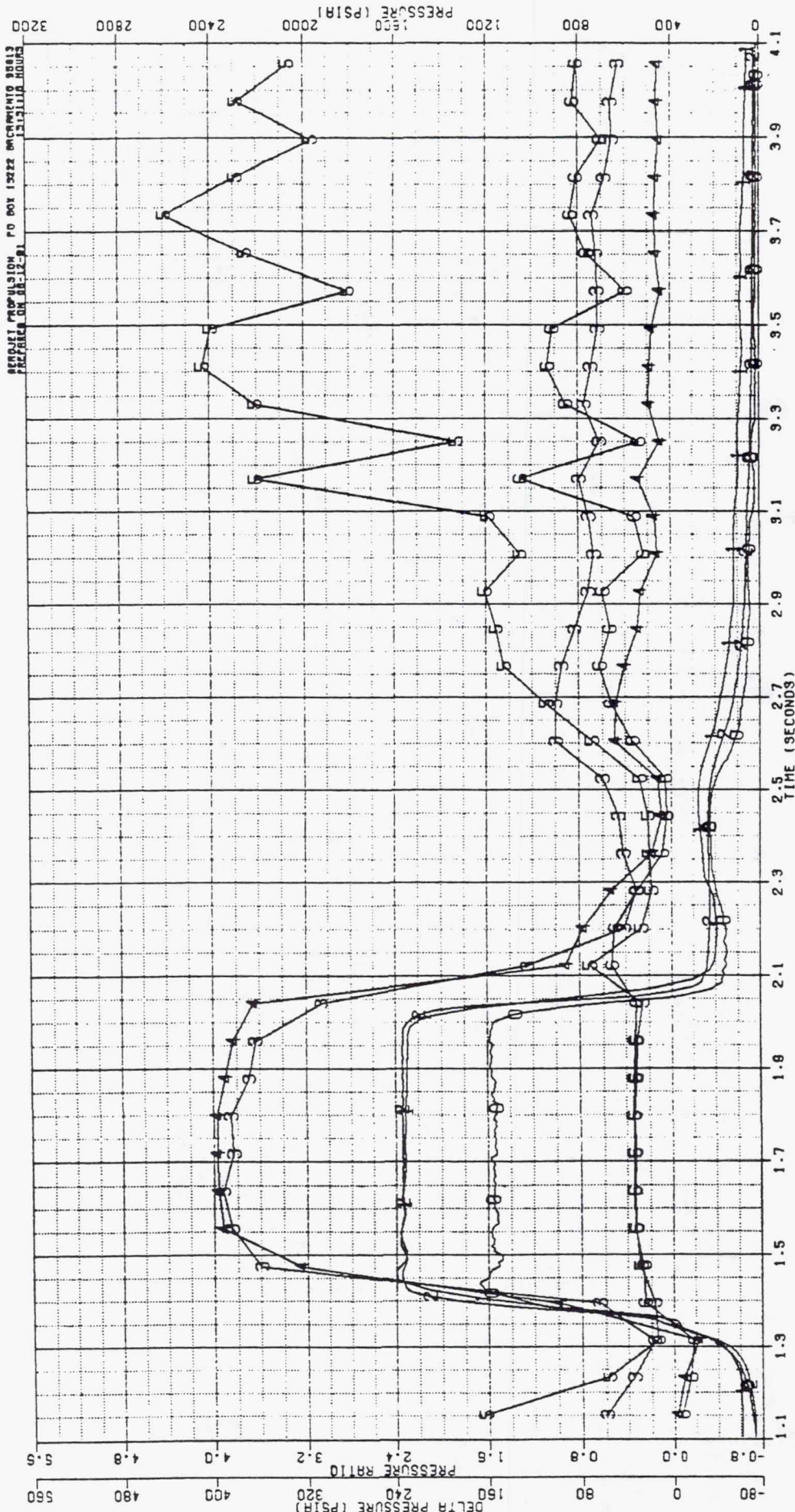


**ROCCID SUBSCALE INJECTOR
PERFORMANCE PARAMETERS**

TEST DATE 05-03-91 AT 1120 HOURS DURATION 1.594 SECONDS
 TEST NUMBER KFN7-001-1J-039 TEST STAND E-4



- 0 PC-3 PSIA
- 1 POJ PSIA
- 2 PFJ PSIA
- 3 OPO PSIA
- 4 OPF PSIA
- 5 OPO/PC
- 6 OPF/PC



**ROCCID SUBSCALE INJECTOR
PERFORMANCE PARAMETERS**

TEST DATE 05-03-91 AT 1314 HOURS DURATION 1.943 SECONDS
TEST NUMBER KFN7-001-1J-040 TEST STAND E-4

**GENCORP
AEROJET**

- 0 PC-3 PSIA
- 1 POJ PSIA
- 2 PEJ PSIA
- 3 DPF PSIA
- 4 DPF PSIA
- 5 DPF/PC
- 6 DPF/PC

APPENDIX B

TIME SERIES, AMPLITUDE AND FREQUENCY EVOLUTION, AND
POWER SPECTRAL ANALYSIS OF CHAMBER PRESSURE
FOR ALL UNSTABLE-COMBUSTION TESTS

INDEX OF TEST DATA PLOTS

Page No.

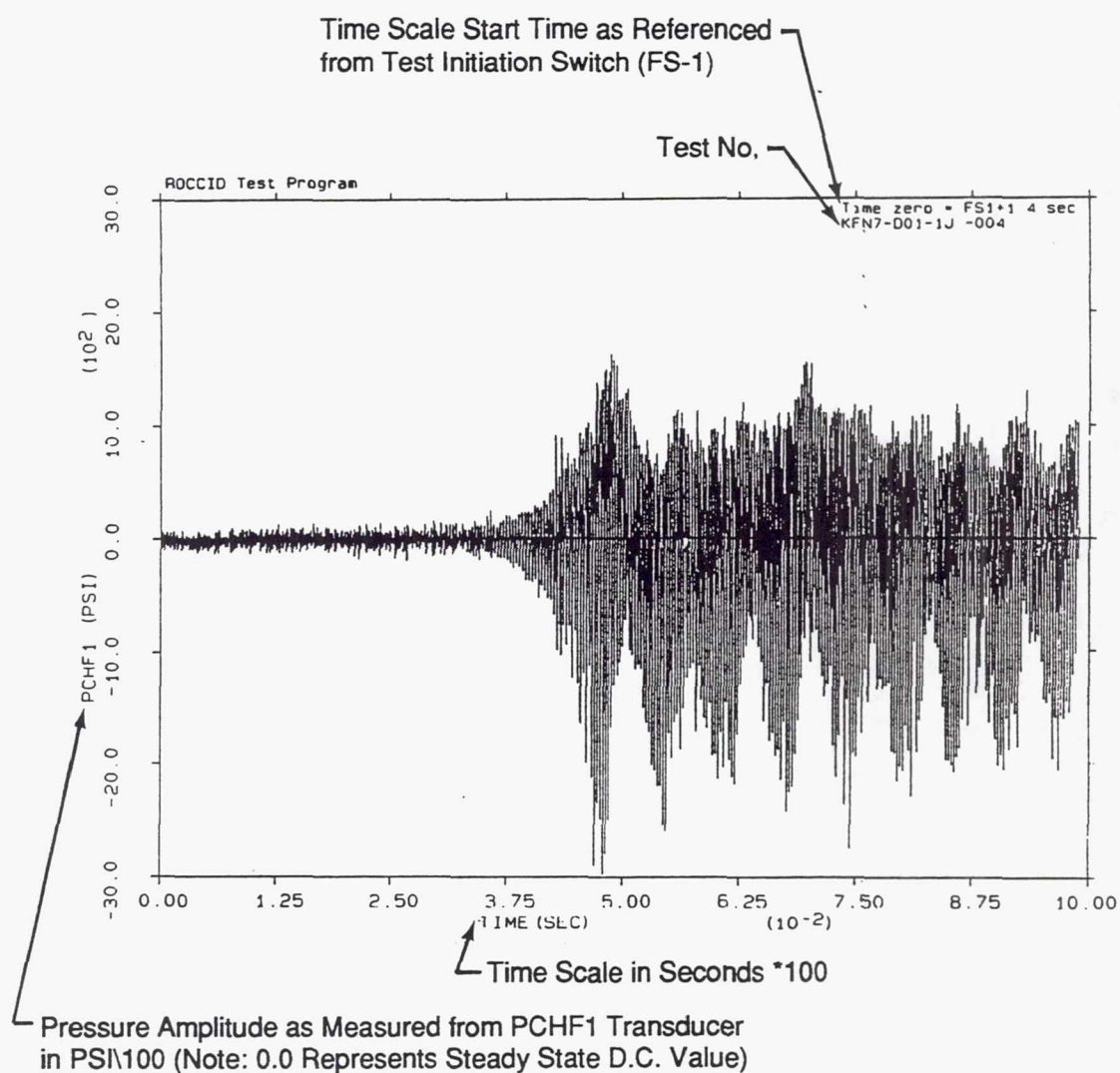
B-3 Thru B-5	Foreword
B-6 Thru B-8	Data From Test No. KFN7-D01-1J-004
B-9 Thru B-11	Data From Test No. KFN7-D01-1J-014
B-12 Thru B-14	Data From Test No. KFN7-D01-1J-018
B-15 Thru B-17	Data From Test No. KFN7-D01-1J-019
B-18 Thru B-20	Data From Test No. KFN7-D01-1J-021
B-21 Thru B-23	Data From Test No. KFN7-D01-1J-022
B-24 Thru B-26	Data From Test No. KFN7-D01-1J-025
B-27 Thru B-29	Data From Test No. KFN7-D01-1J-026
B-30 Thru B-32	Data From Test No. KFN7-D01-1J-027
B-33 Thru B-35	Data From Test No. KFN7-D01-1J-028
B-36 Thru B-38	Data From Test No. KFN7-D01-1J-029
B-39 Thru B-41	Data From Test No. KFN7-D01-1J-030
B-42 Thru B-44	Data From Test No. KFN7-D01-1J-037
B-45 Thru B-47	Data From Test No. KFN7-D01-1J-038
B-48 Thru B-50	Data From Test No. KFN7-D01-1J-039
B-51 Thru B-53	Data From Test No. KFN7-D01-1J-040

Note: See Foreword (next page) for explanation of information contained in the 3 plot set for each test.

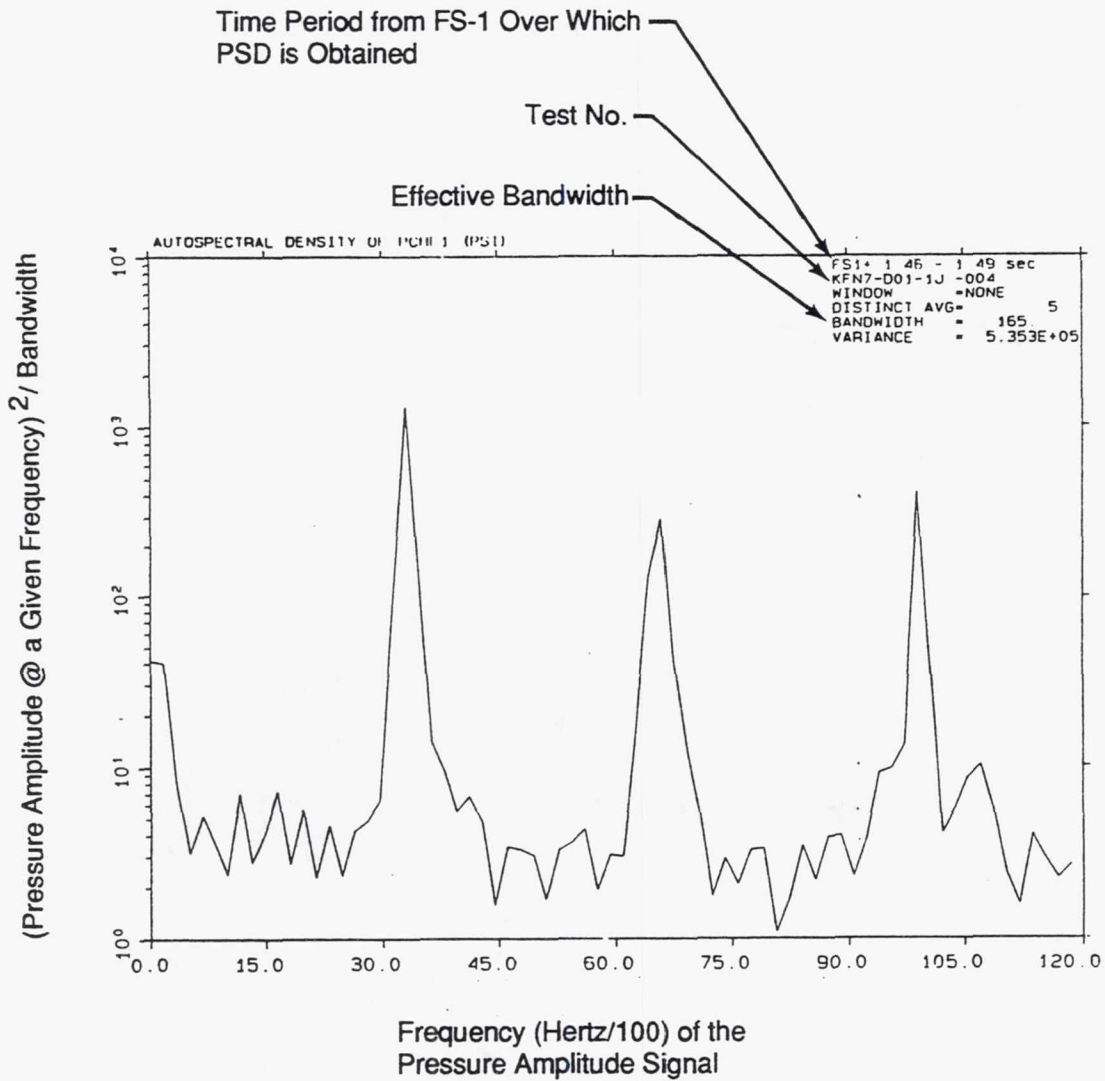
FOREWORD

Unstable operation was observed during 16 of the 27 valid tests conducted during the ROCCID validation test program. For each of these unstable tests, the following information is contained in this appendix:

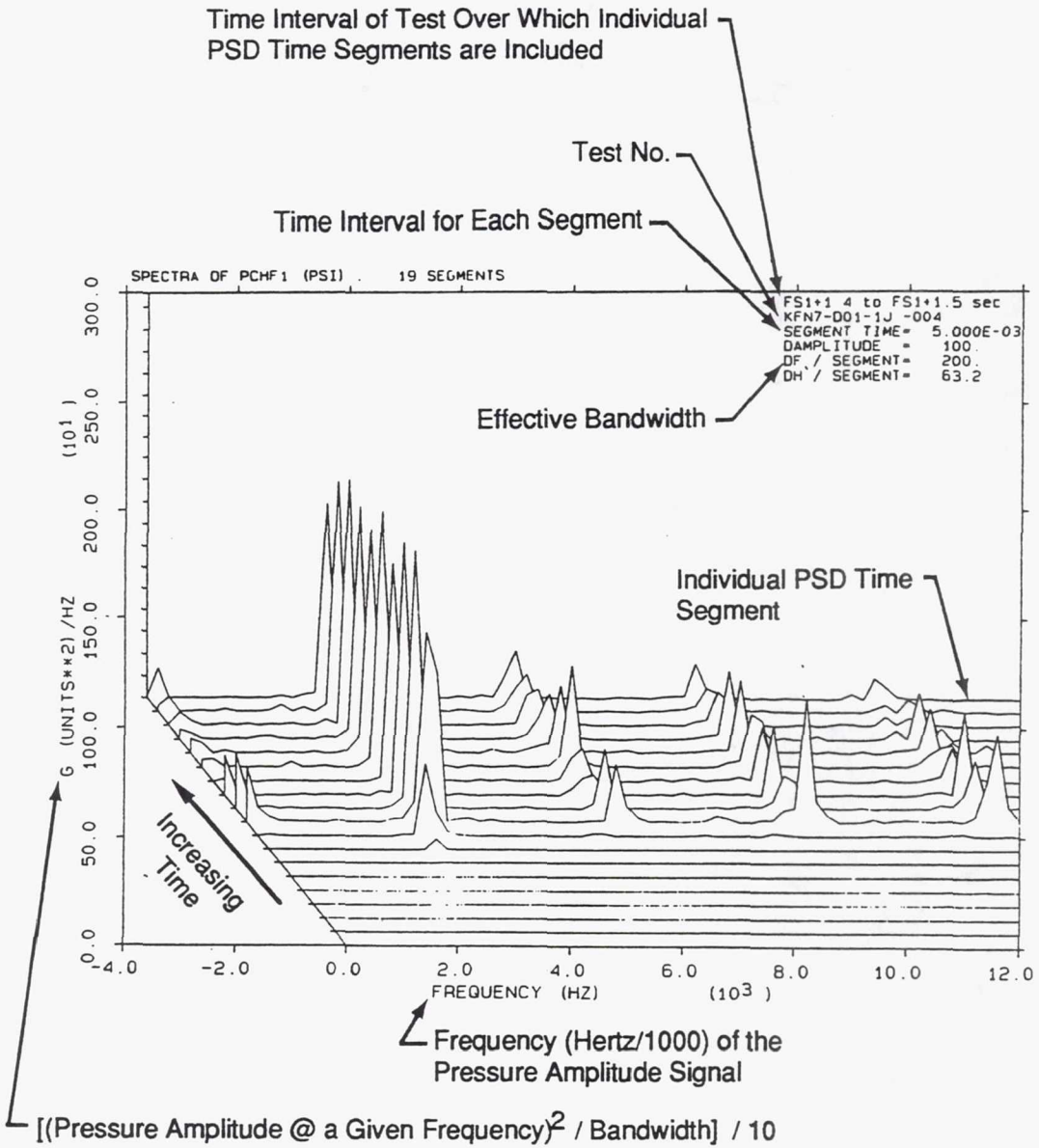
- (1) High Frequency Chamber Pressure Transducer playback of the pressure amplitude versus time prior to and during the observed unstable combustion event. Sample format for this plot is as follows:



- (2) Power Spectral Density (PSD) analysis of the high frequency pressure amplitude recorded signal. Sample format for this plot is as follows:

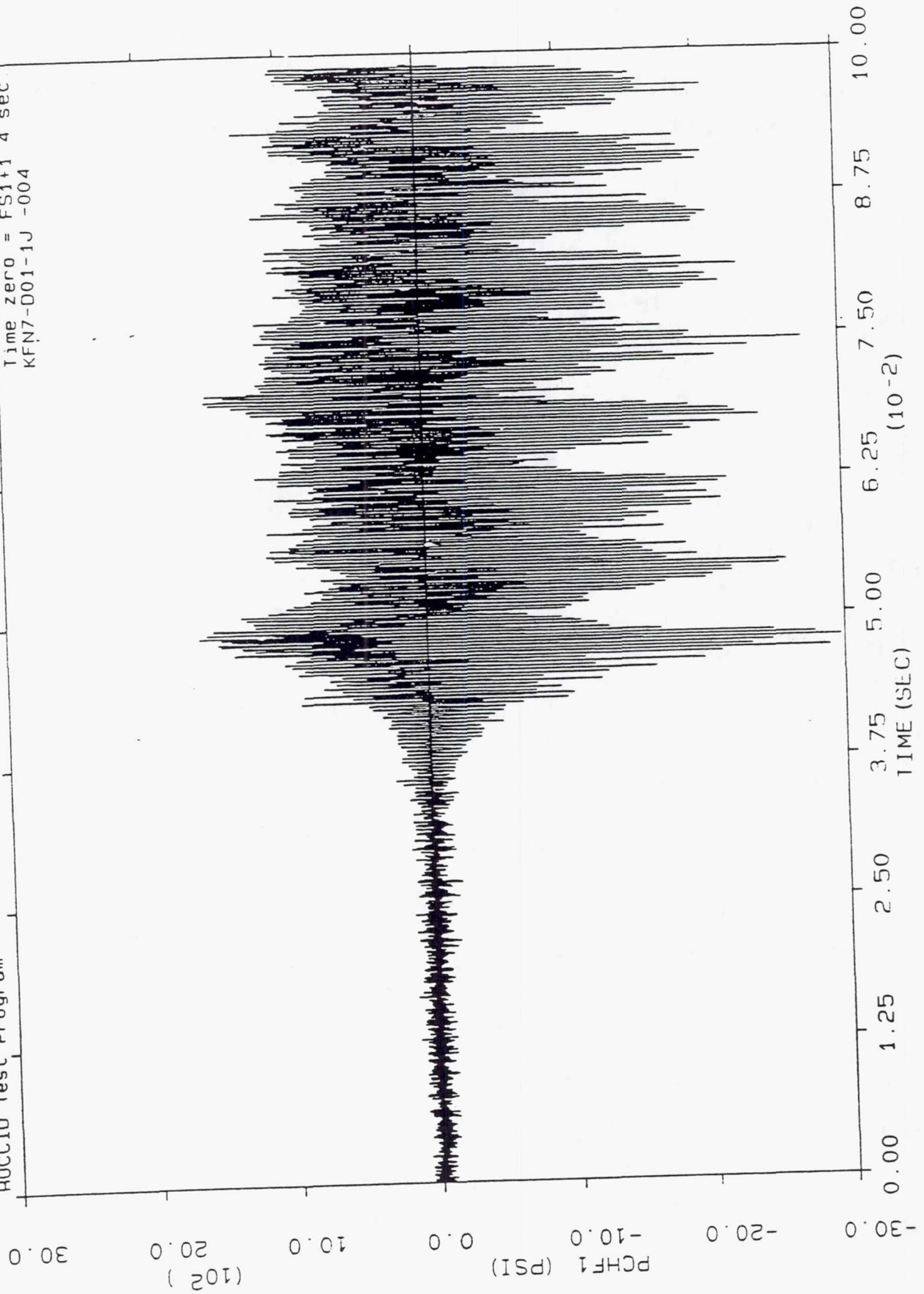


- (3) Power Spectral Analysis of the high frequency pressure amplitude signal. Sample format for this pot is as follows:



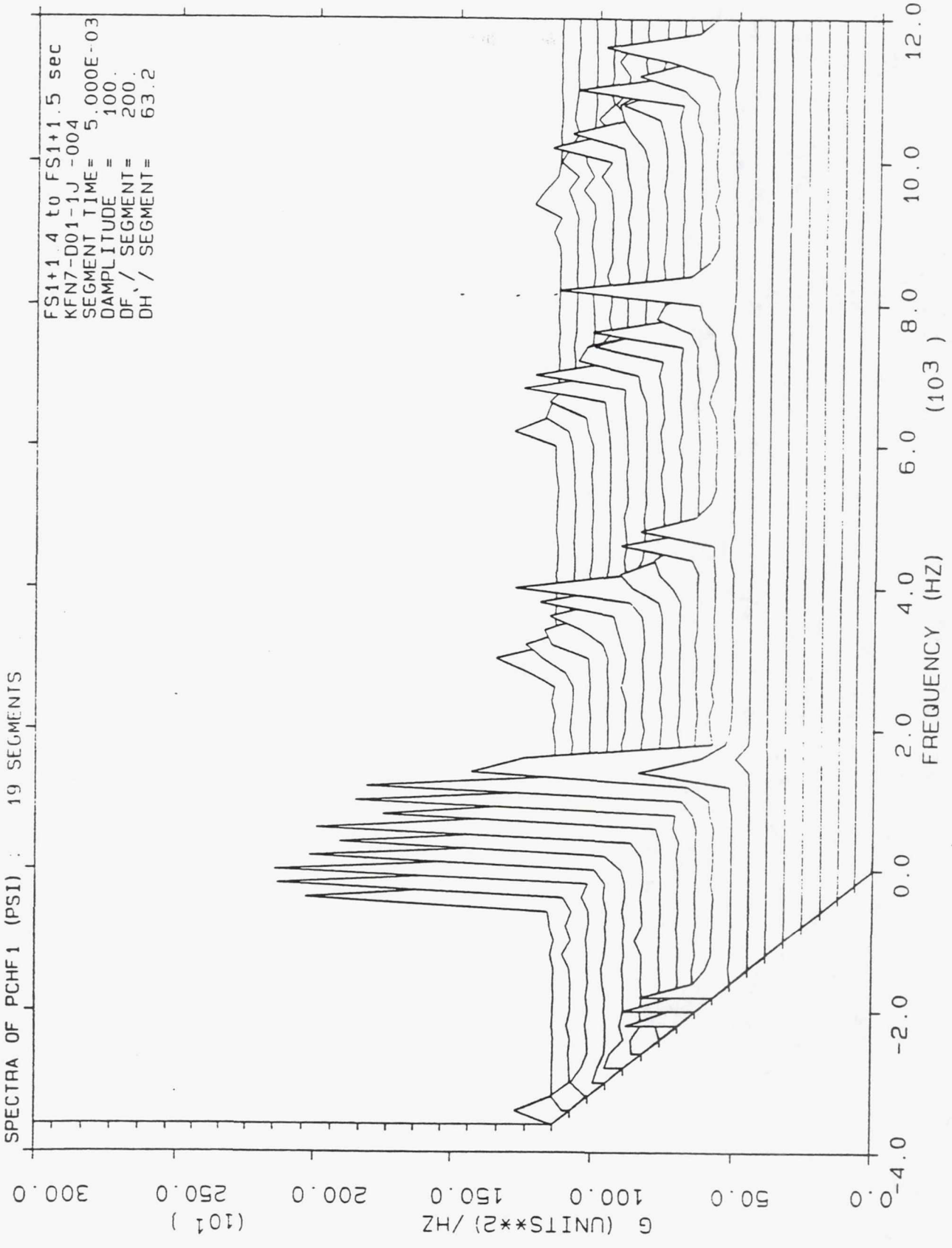
ROCCID Test Program

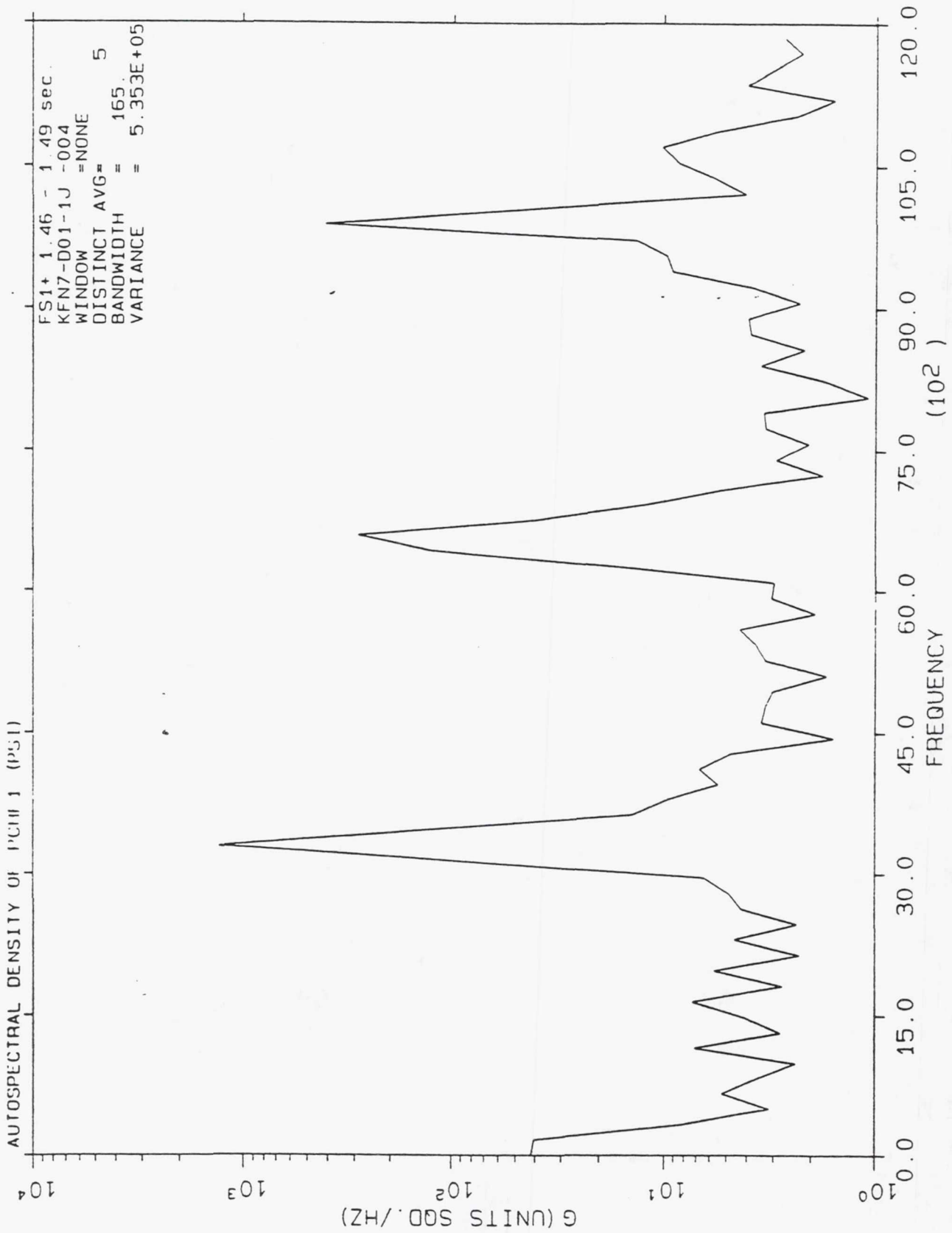
Time zero = FS1+1 4 sec
KFN7-001-1J -004



SPECTRA OF PCHF1 (PSI) : 19 SEGMENTS

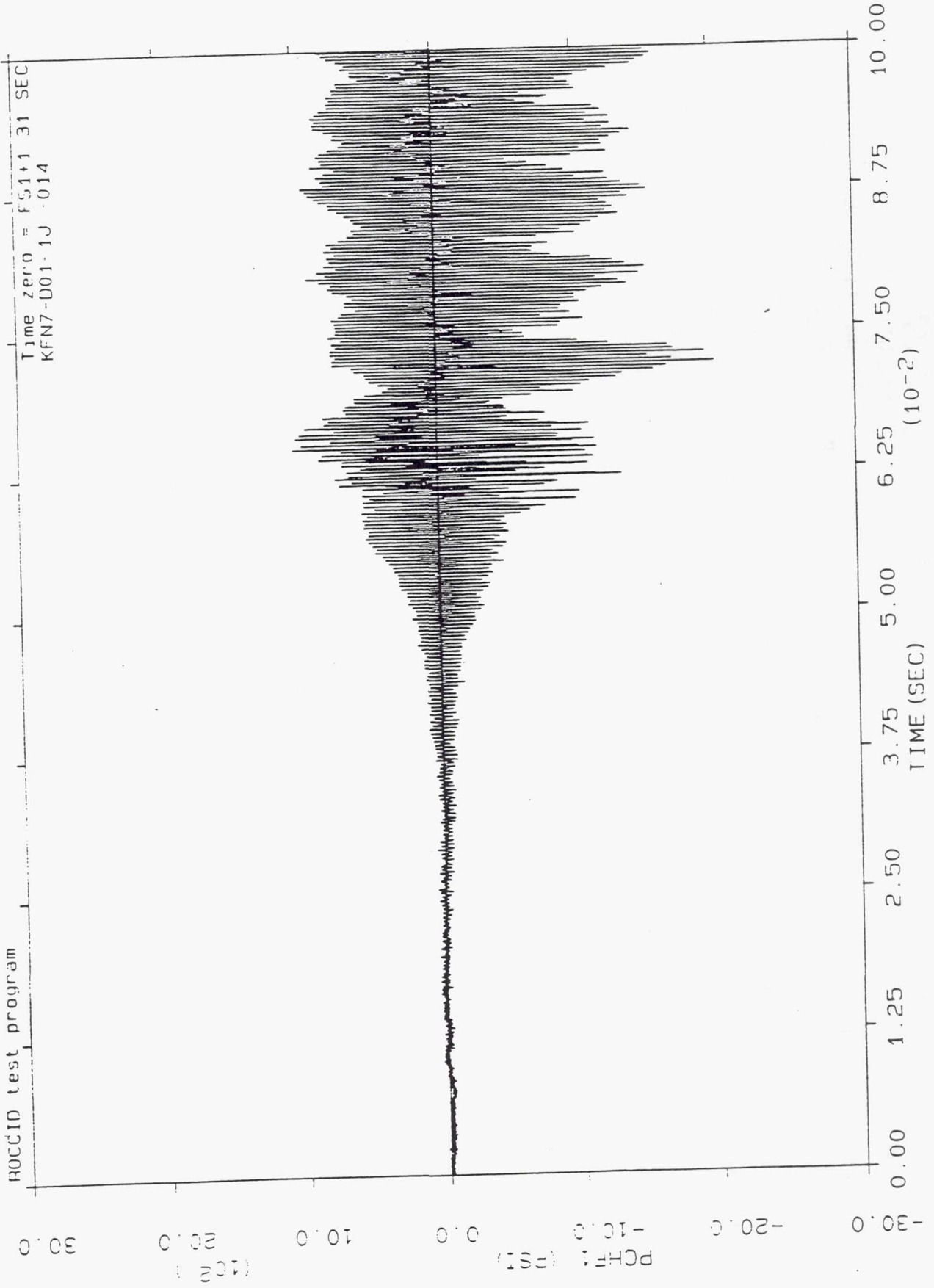
FS1+1.4 to FS1+1.5 sec
KEN7-D01-1J-004
SEGMENT TIME= 5.000E-03
DAMPLITUDE = 100.
DF / SEGMENT= 200.
DH / SEGMENT= 63.2





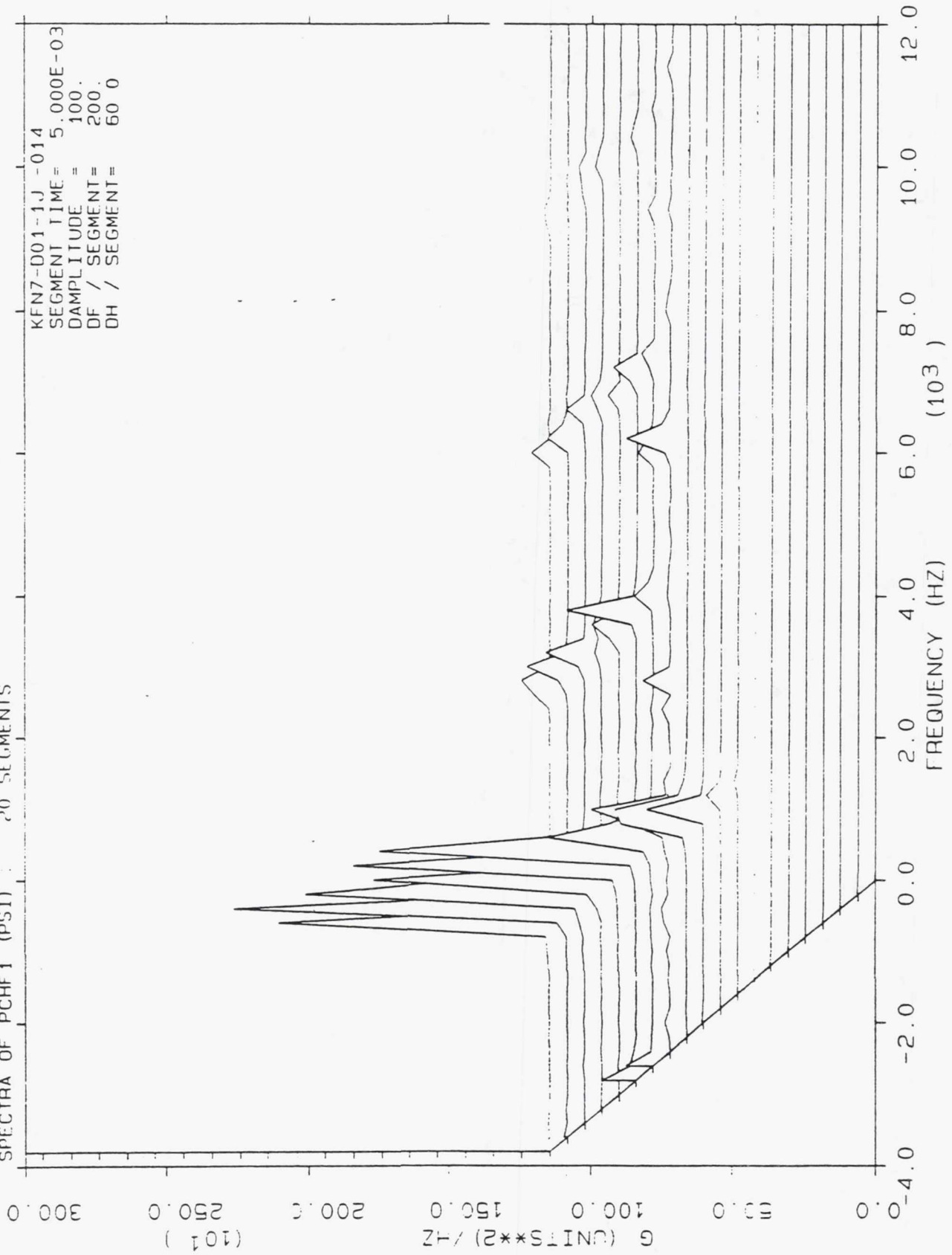
HOCCID test program

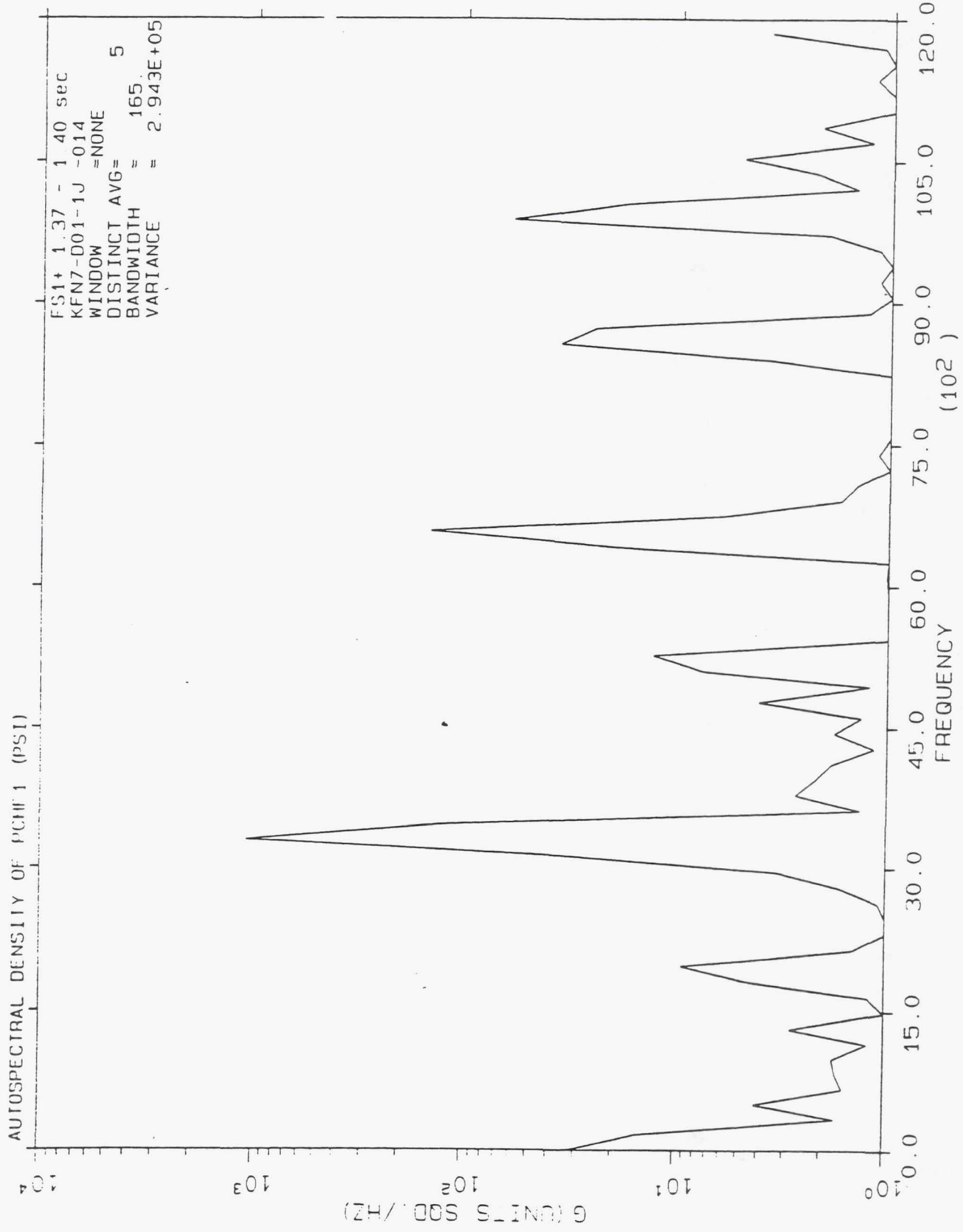
Time zero = F51+1 31 SEC
KFN7-D01-1J .014



SPECTRA OF PCHF1 (PSI) : 20 SEGMENTS

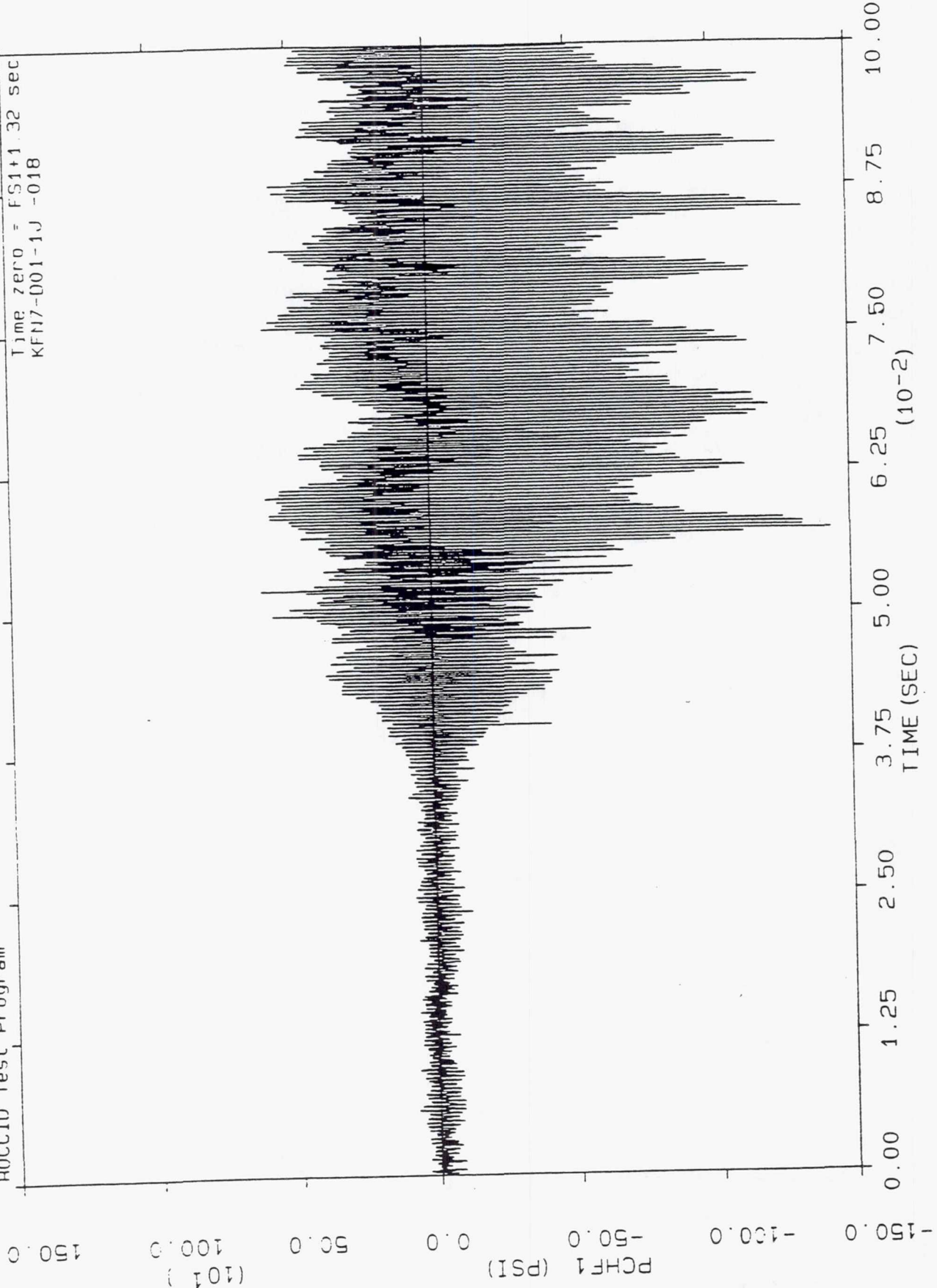
KFN7-D01-1J -014
SEGMENT TIME= 5.000E-03
DAMPLITUDE = 100.
DF / SEGMENT= 200.
DH / SEGMENT= 60 0



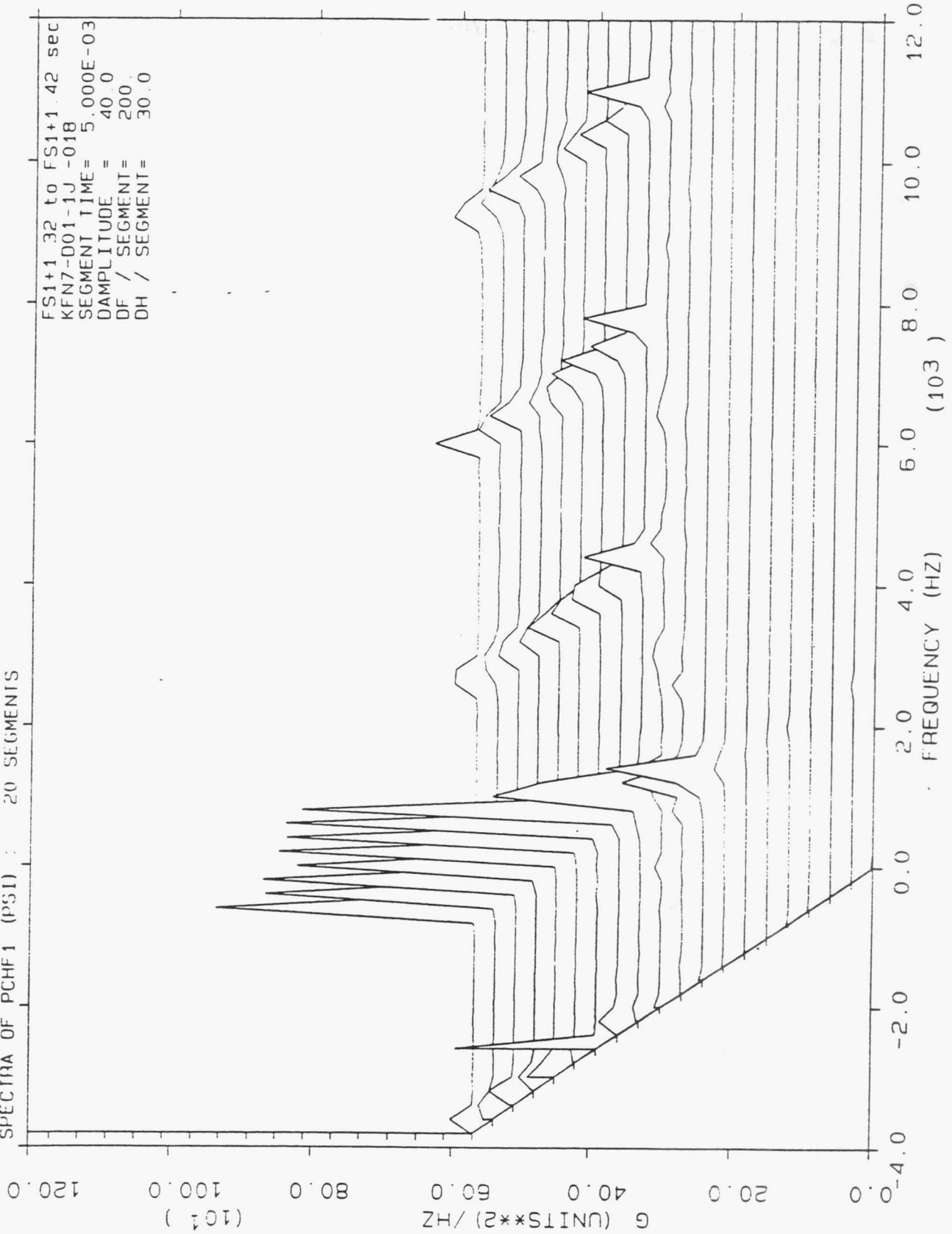


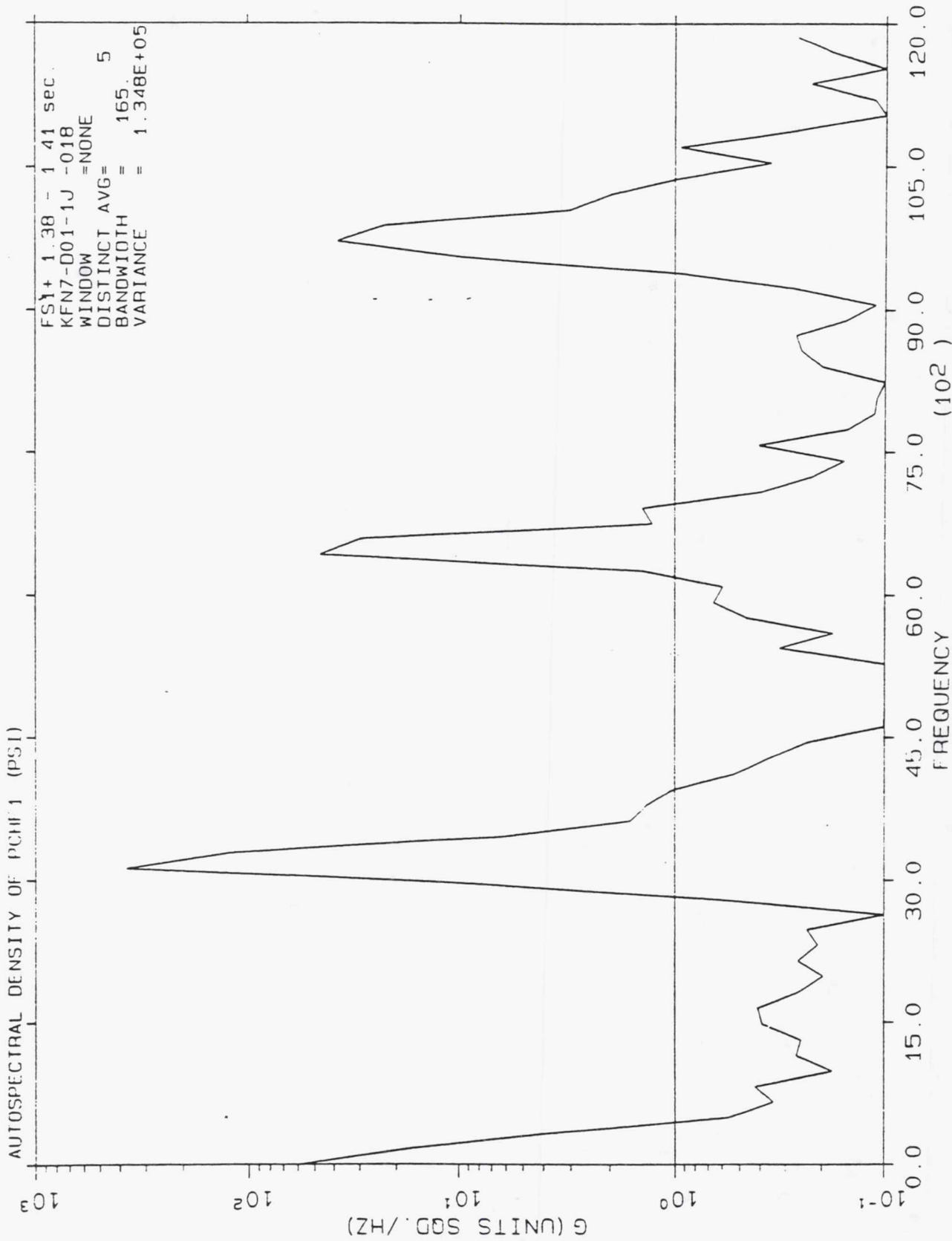
ROCCID Test Program

Time zero = FS1+1.32 sec
KFN7-D01-1J -018



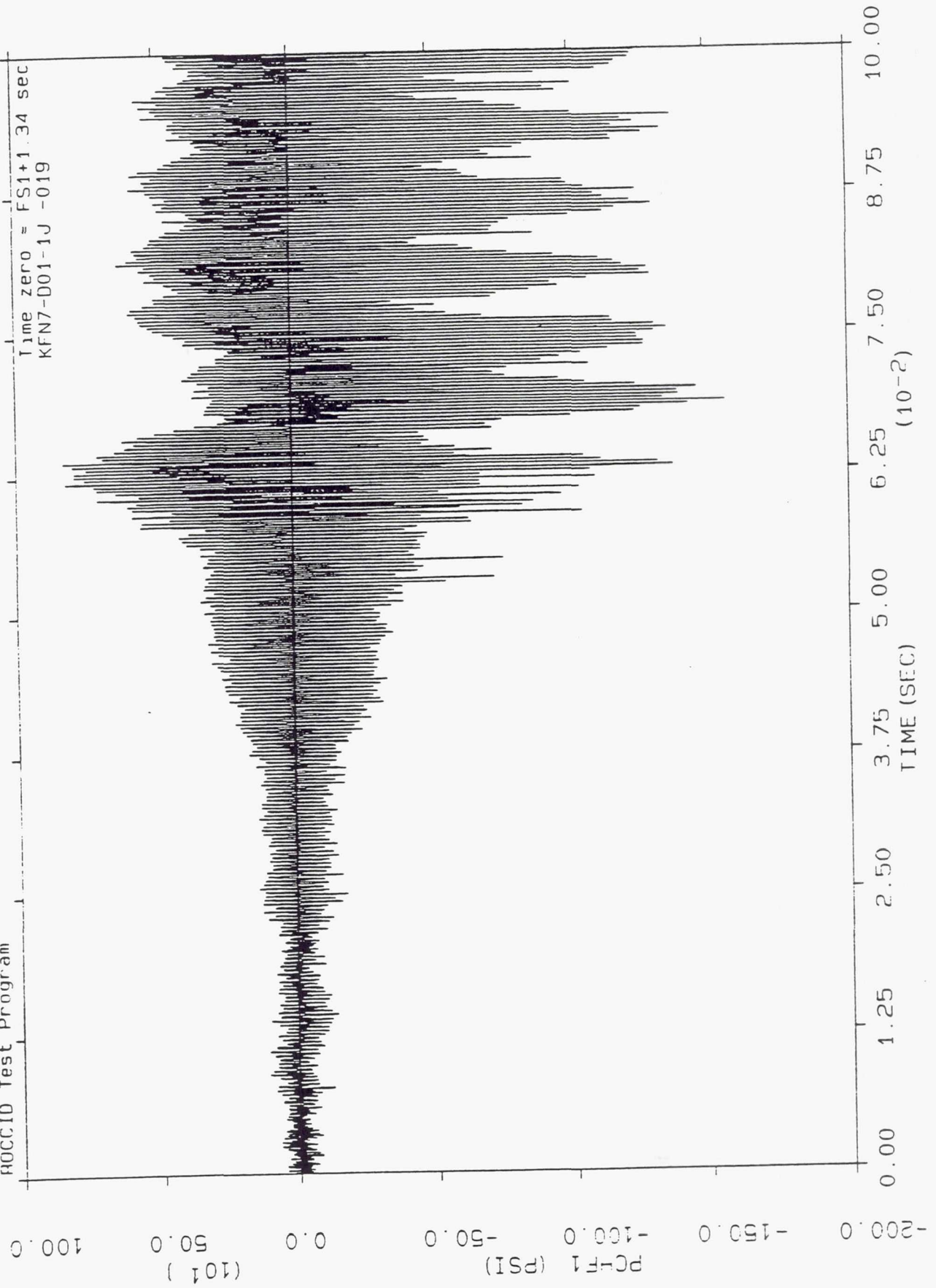
SPECTRA OF PCHF1 (PSI) : 20 SEGMENTS





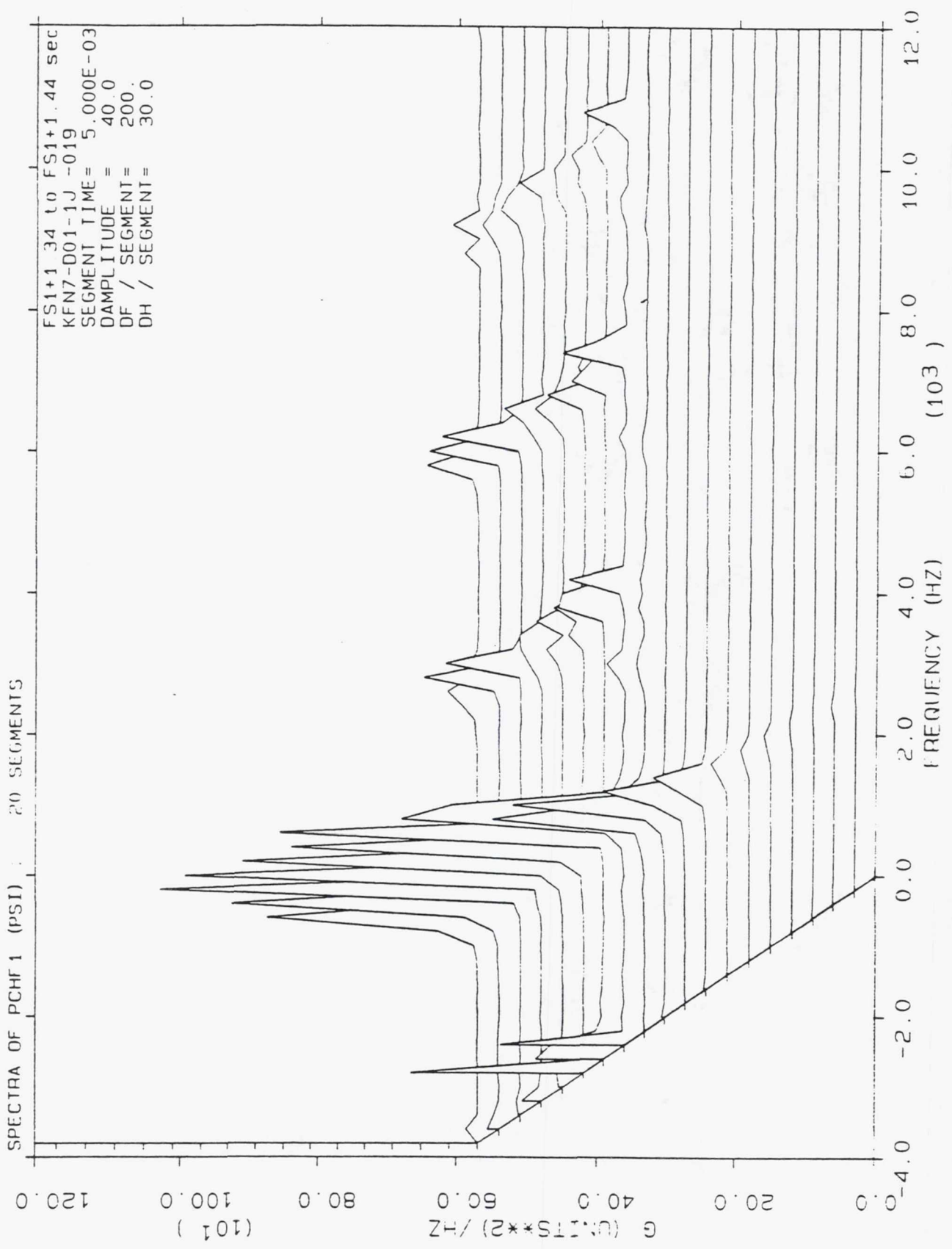
ROCCID Test Program

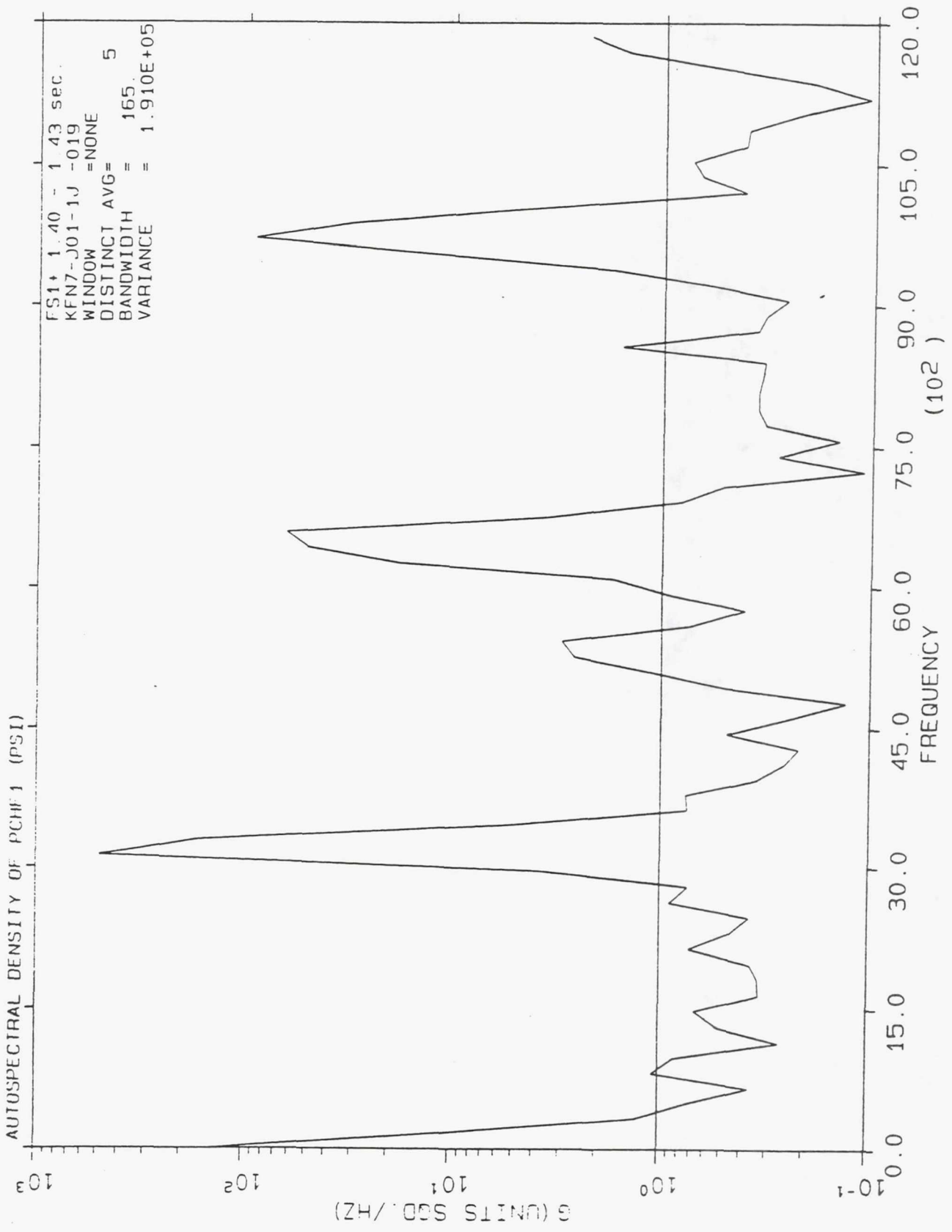
Time zero = FS1+1.34 sec
KFN7-001-1J -019



SPECTRA OF PCHF 1 (PSI) : 20 SEGMENTS

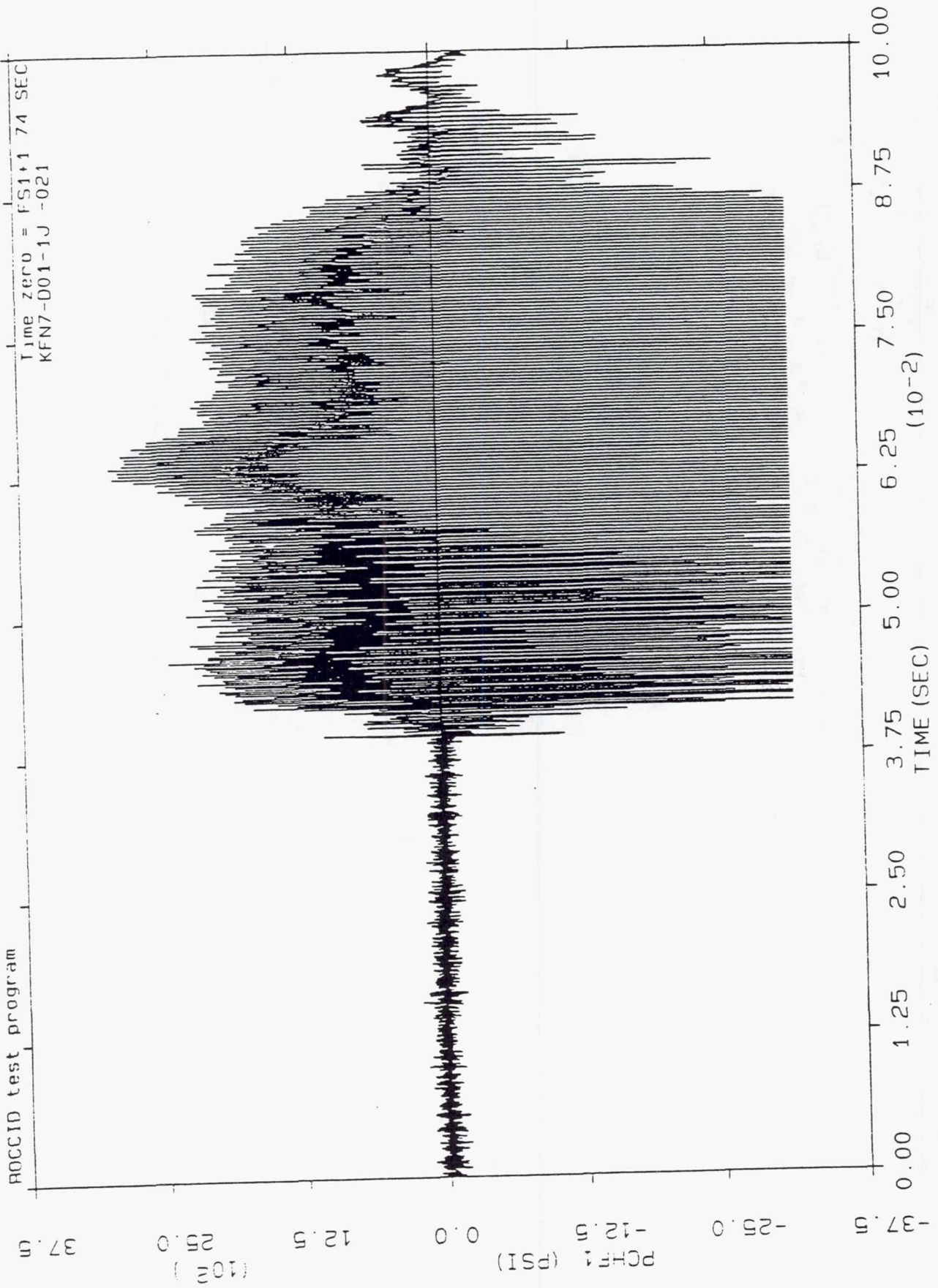
FS1+1 34 to FS1+1.44 sec
KFN7-001-1J -019
SEGMENT TIME= 5.000E-03
DAMPLITUDE = 40.0
DF / SEGMENT= 200.
DH / SEGMENT= 30.0





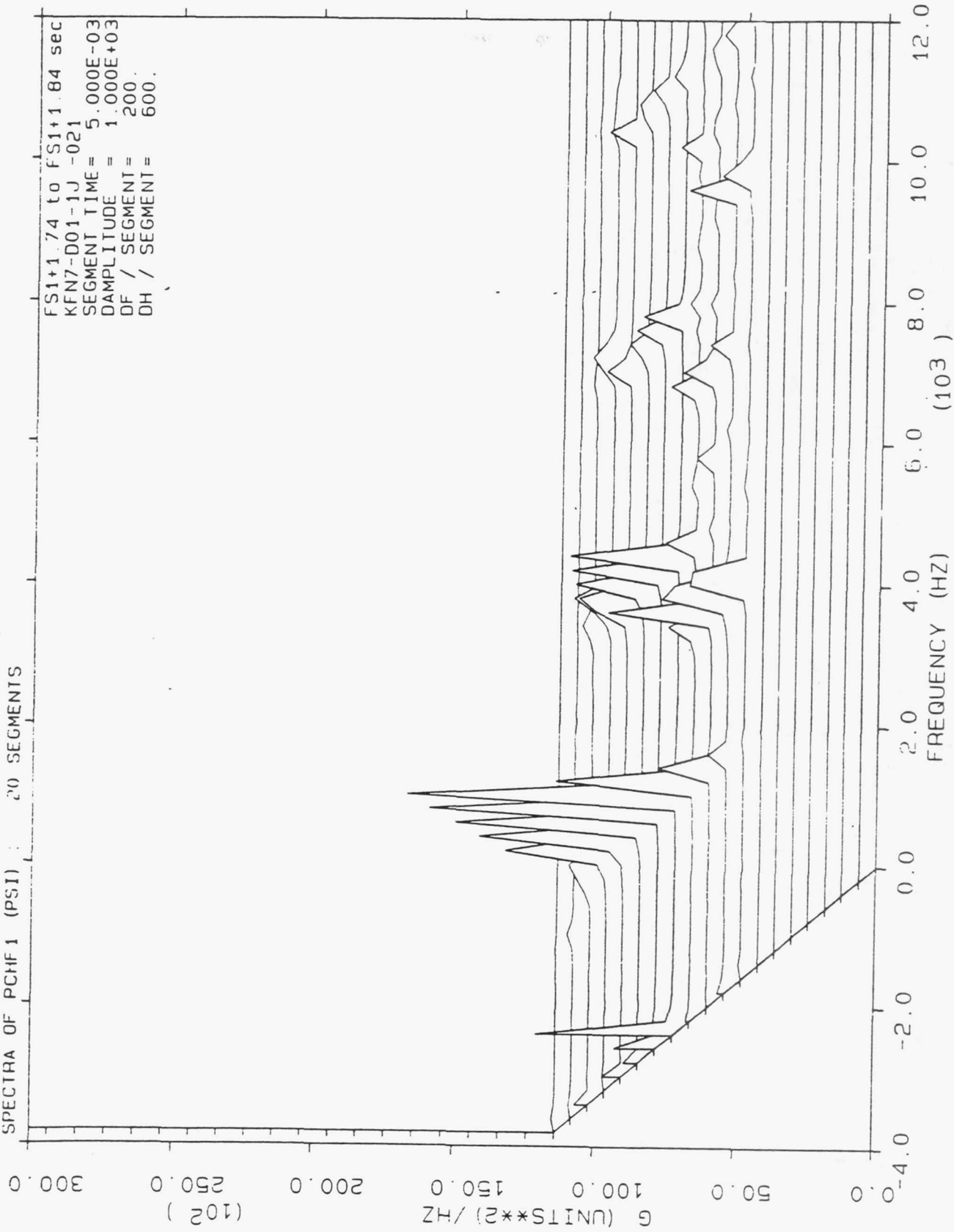
ROCCID test program

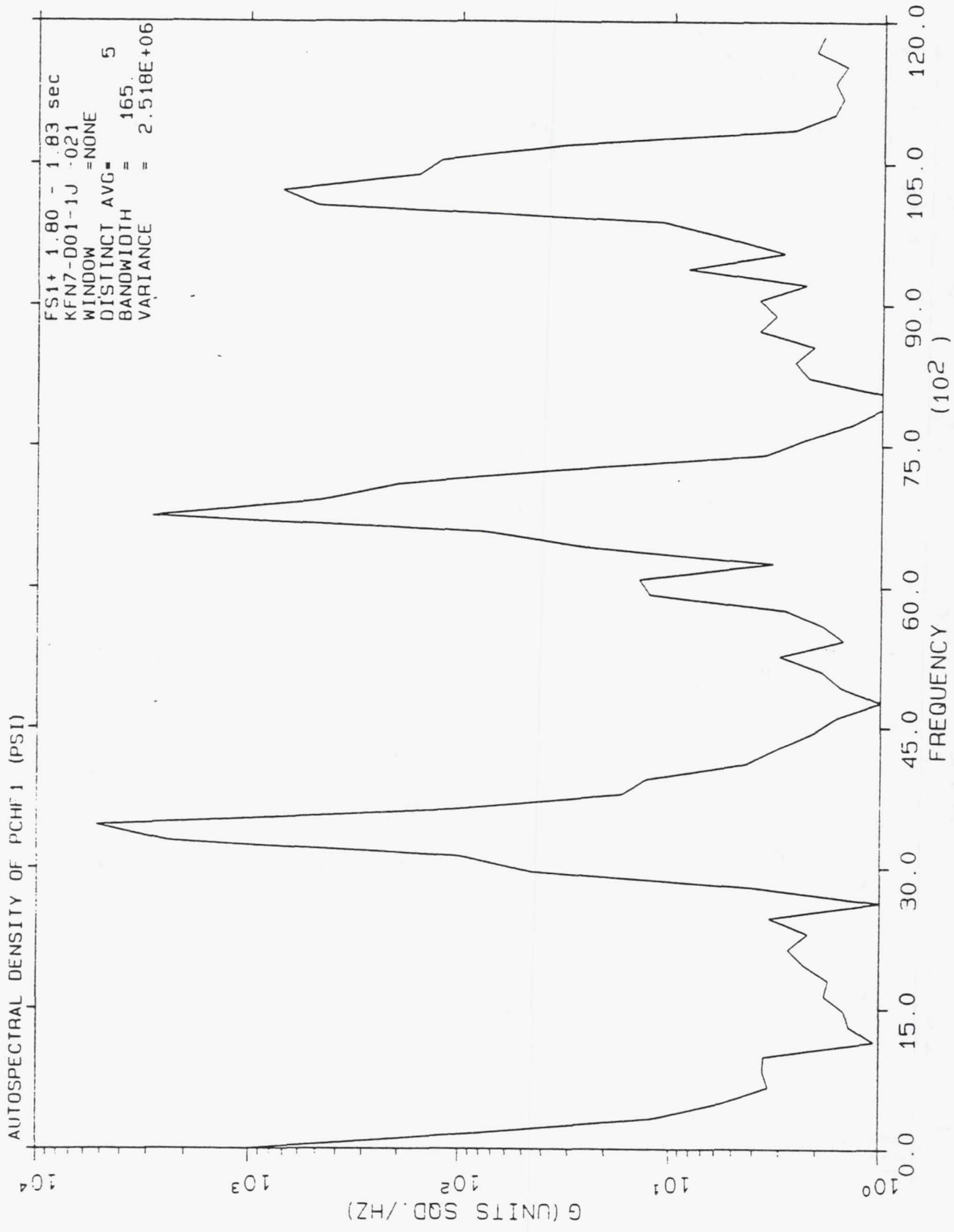
Time zero = FS1+1 74 SEC
KFN7-D01-1J -021



SPECTRA OF PCHF 1 (PSI) : 20 SEGMENTS

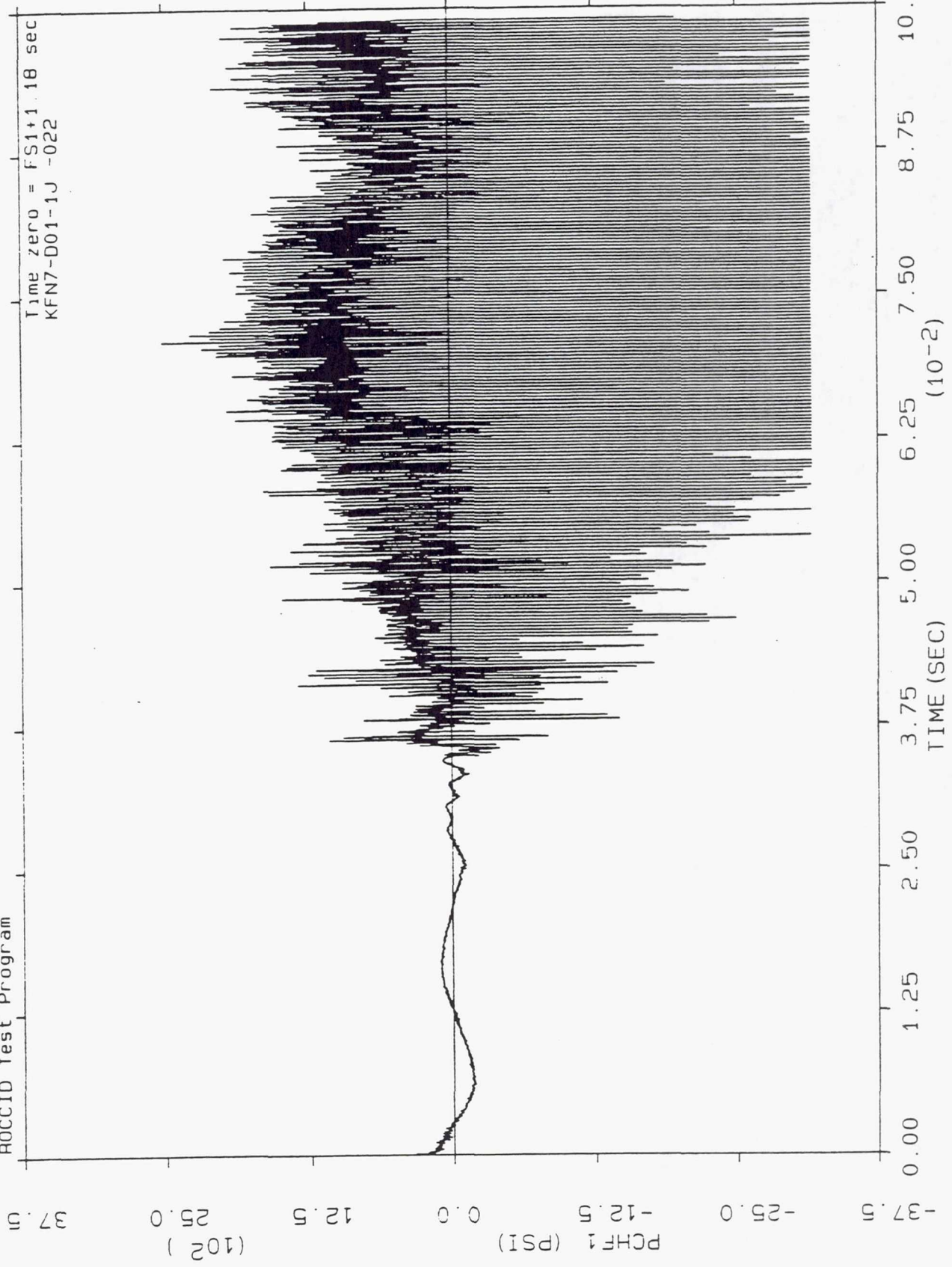
FS1+1.74 to FS1+1.84 sec
KFN7-D01-1J -021
SEGMENT TIME = 5.000E-03
DAMPLITUDE = 1.000E+03
DH / SEGMENT = 200.
DH / SEGMENT = 600.





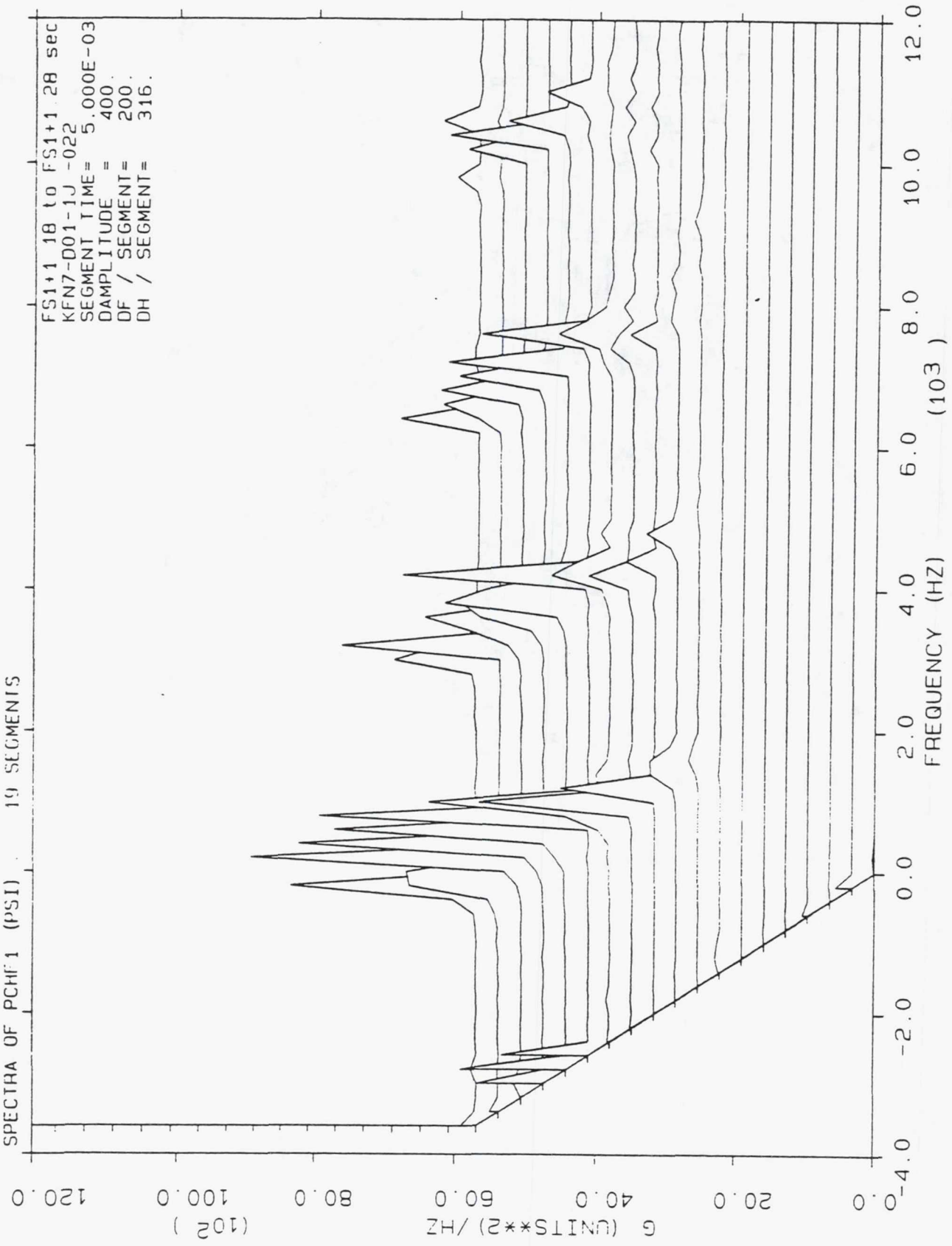
ROCCID Test Program

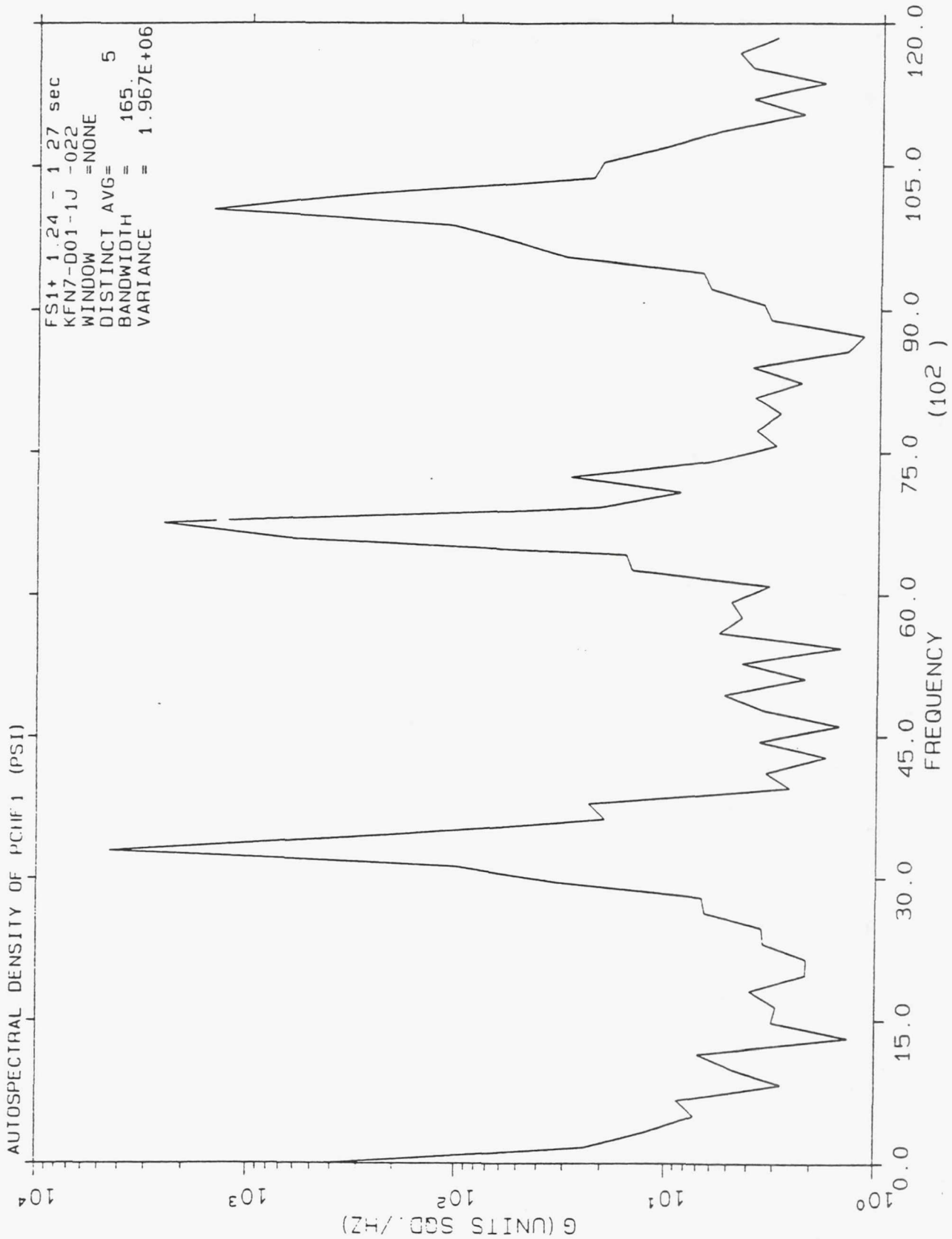
Time zero = FS1+1.18 sec
KFN7-D01-1J -022



SPECTRA OF PCH1 (PSI) 19 SEGMENTS

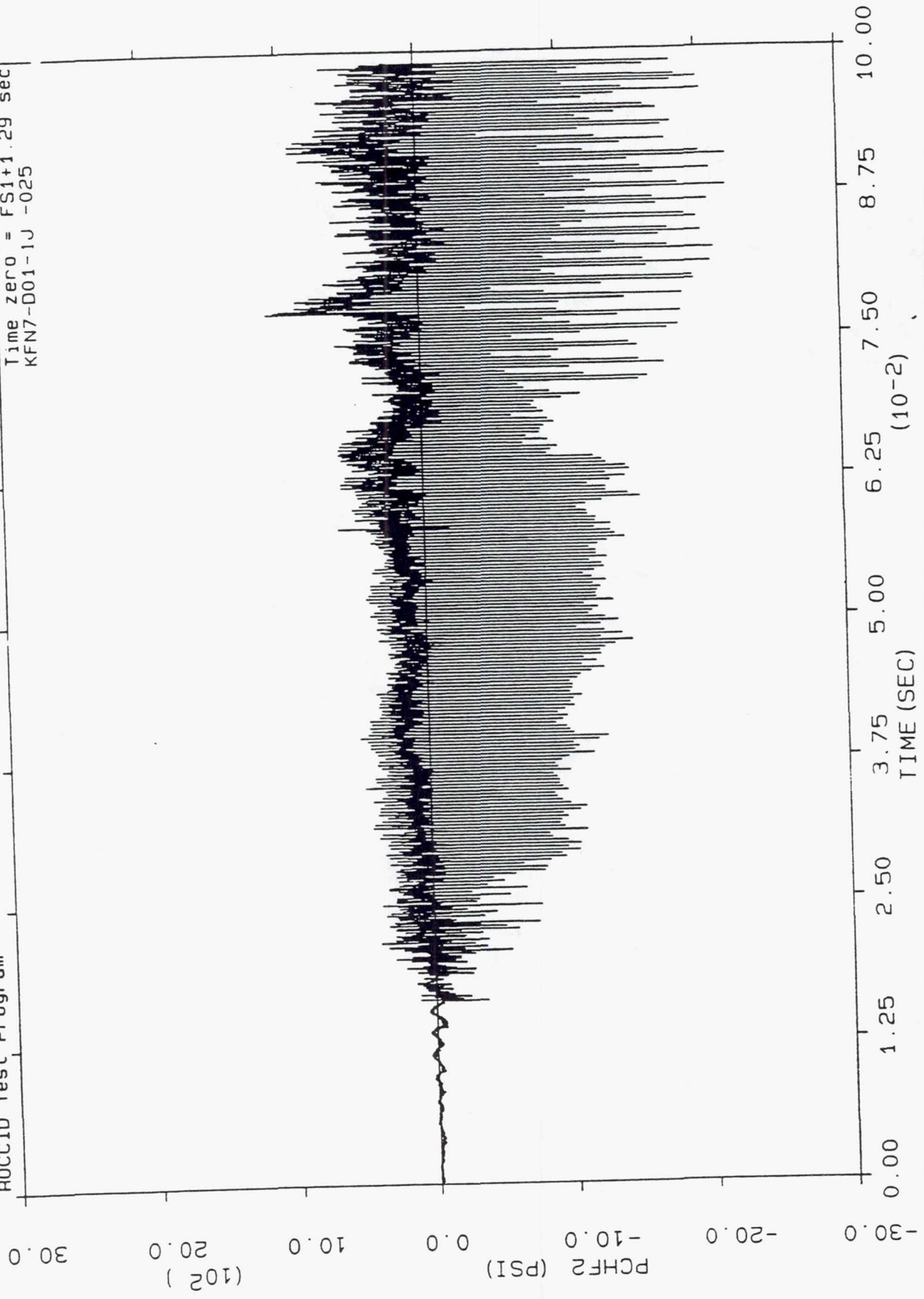
FS1+1 18 to FS1+1 28 sec
KFN7-D01-1J -022
SEGMENT TIME= 5.000E-03
DAMPLITUDE = 400.
DF / SEGMENT= 200.
DH / SEGMENT= 316.





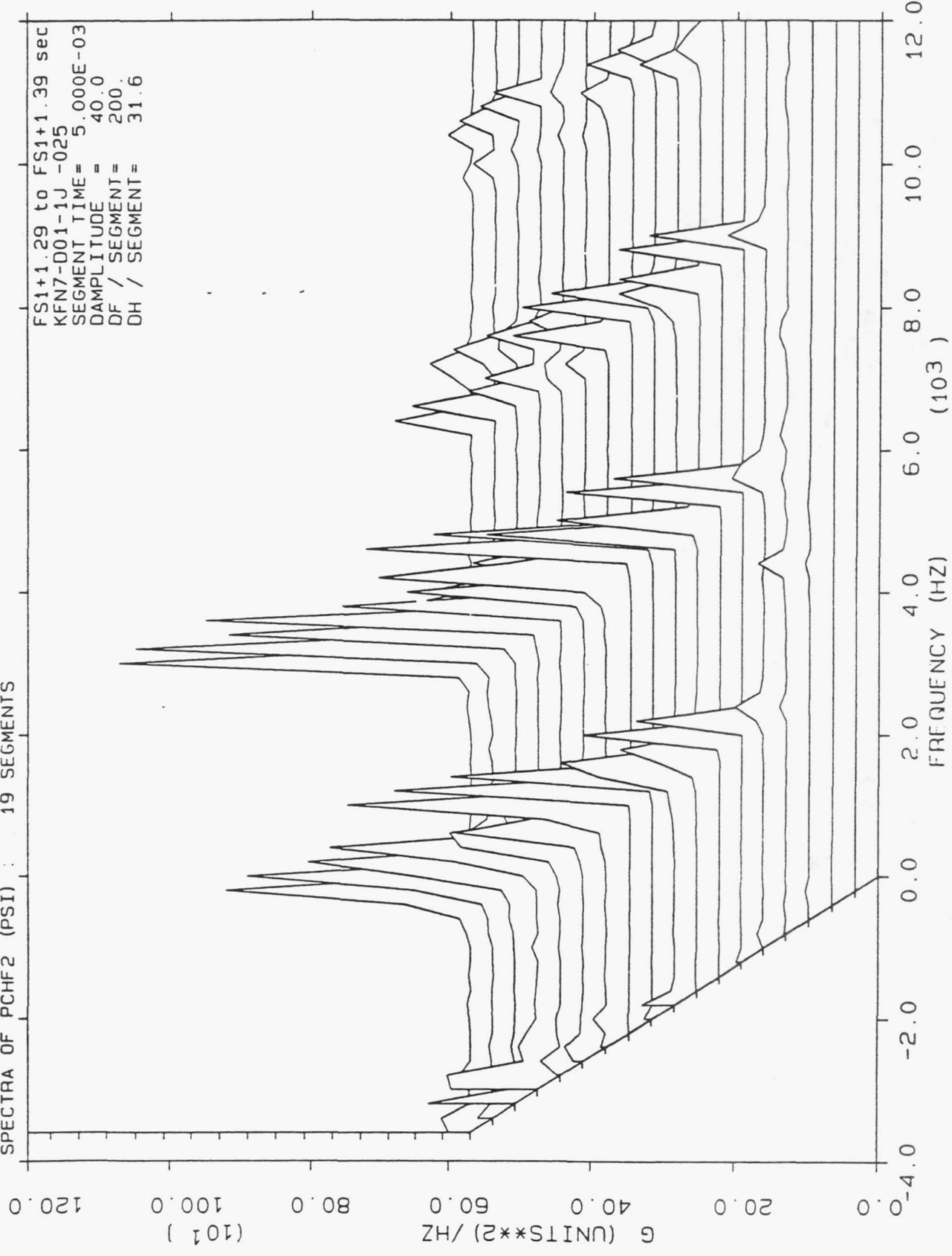
ROCCID Test Program

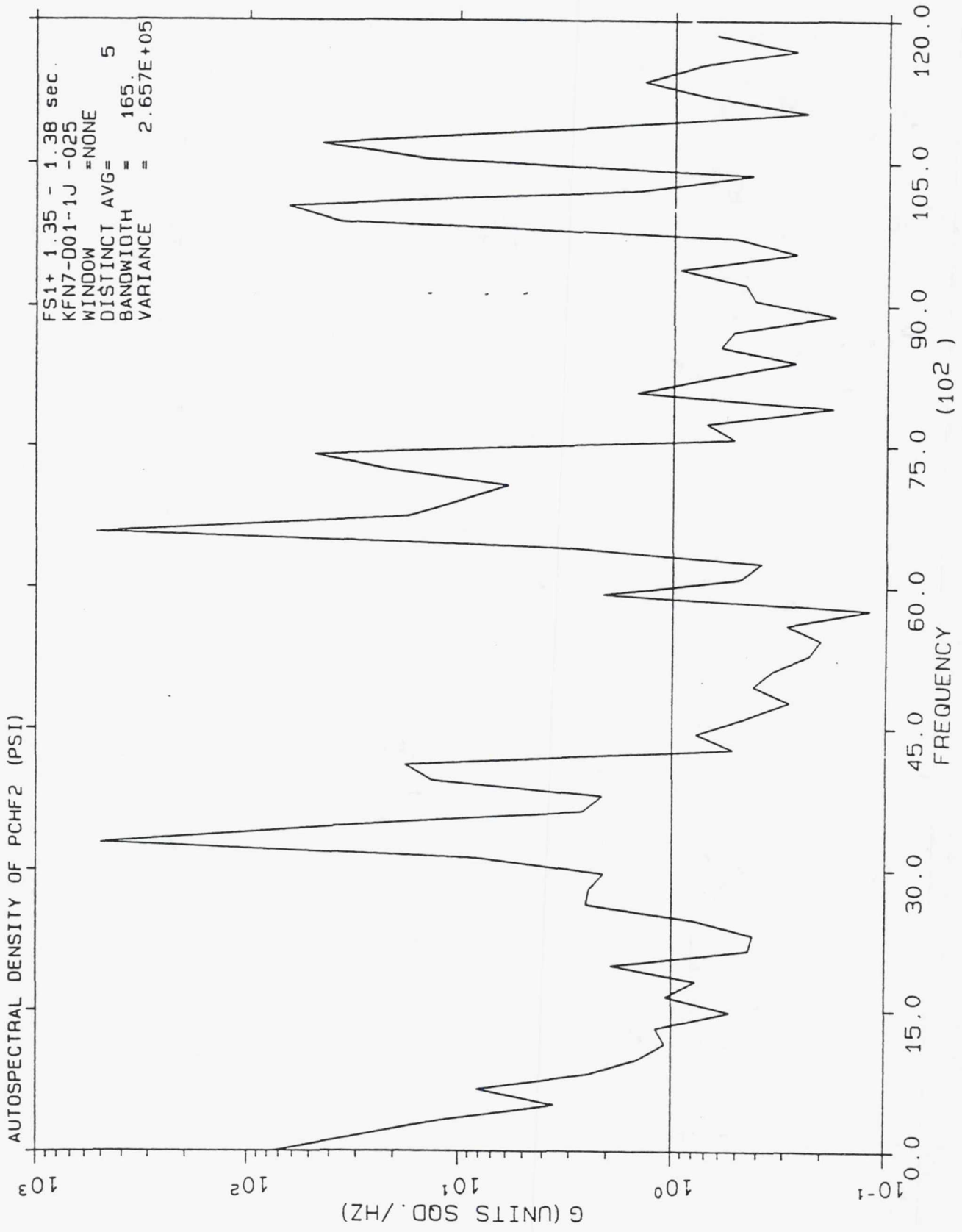
Time zero = FS1+1.29 sec
KFN7-D01-1J -025



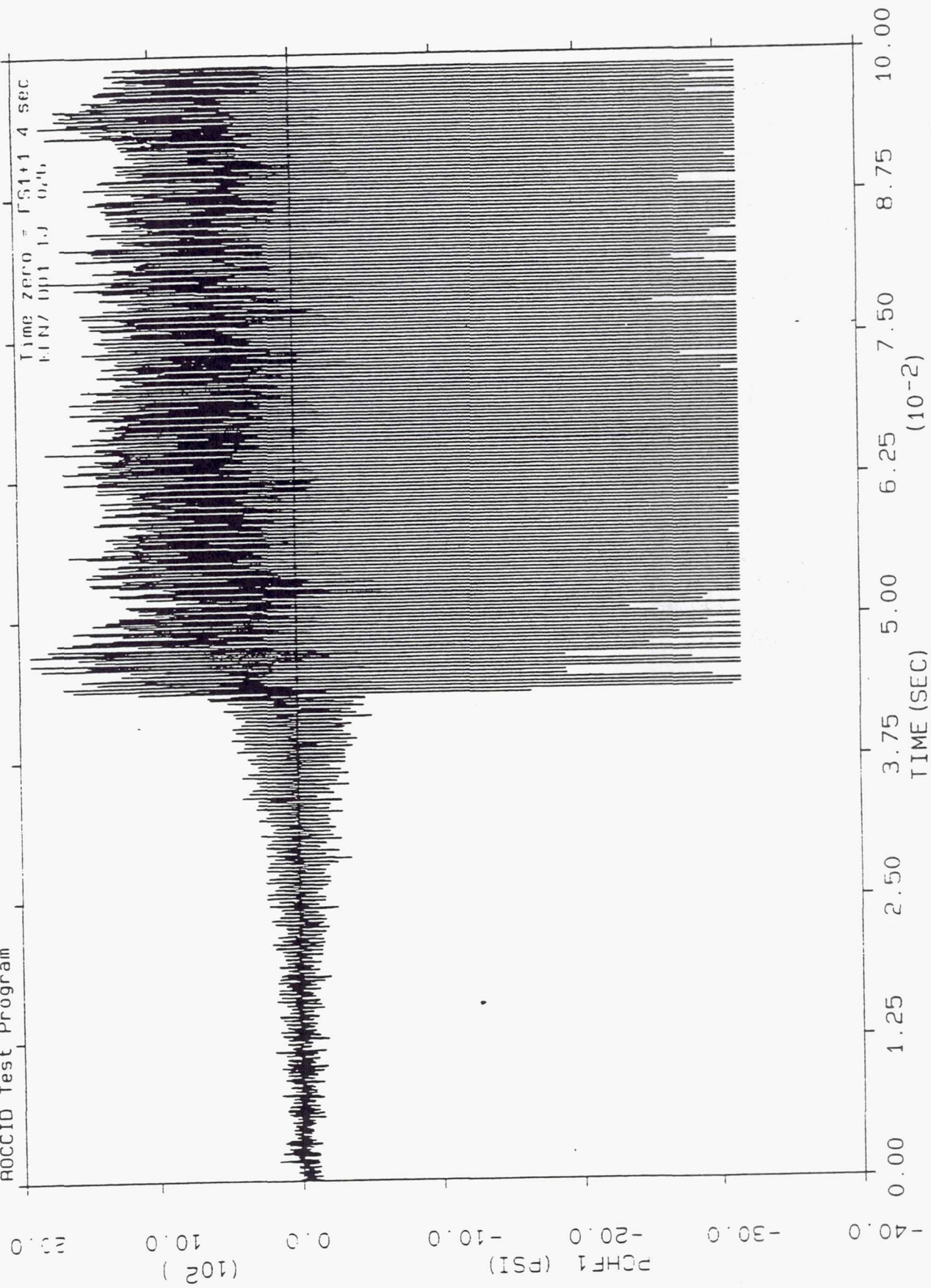
SPECTRA OF PCHF2 (PSI) : 19 SEGMENTS

FS1+1.29 to FS1+1.39 sec
KFN7-D01-1J -025
SEGMENT TIME= 5.000E-03
DAMPLITUDE = 40.0
DF / SEGMENT = 200.
DH / SEGMENT = 31.6



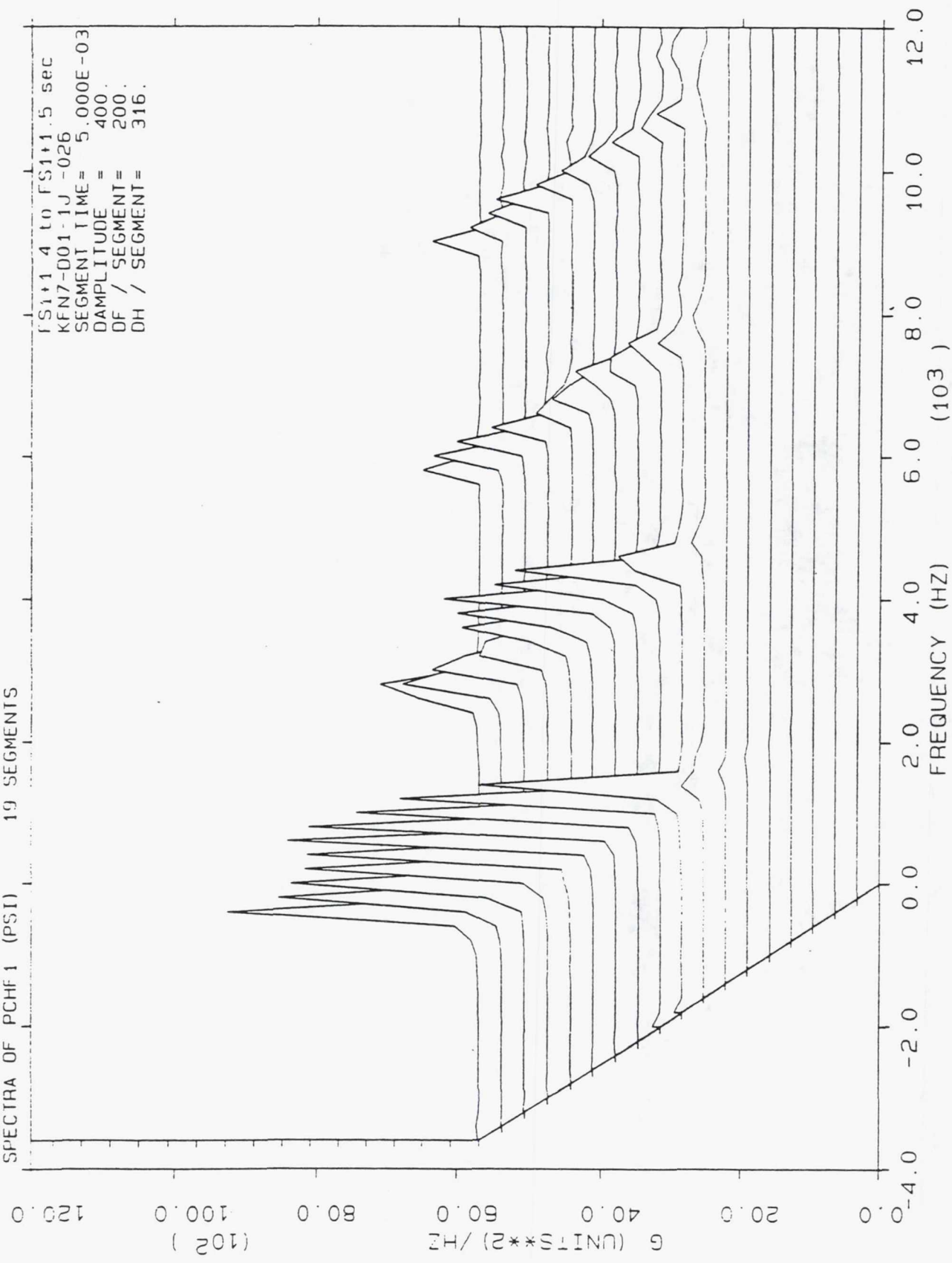


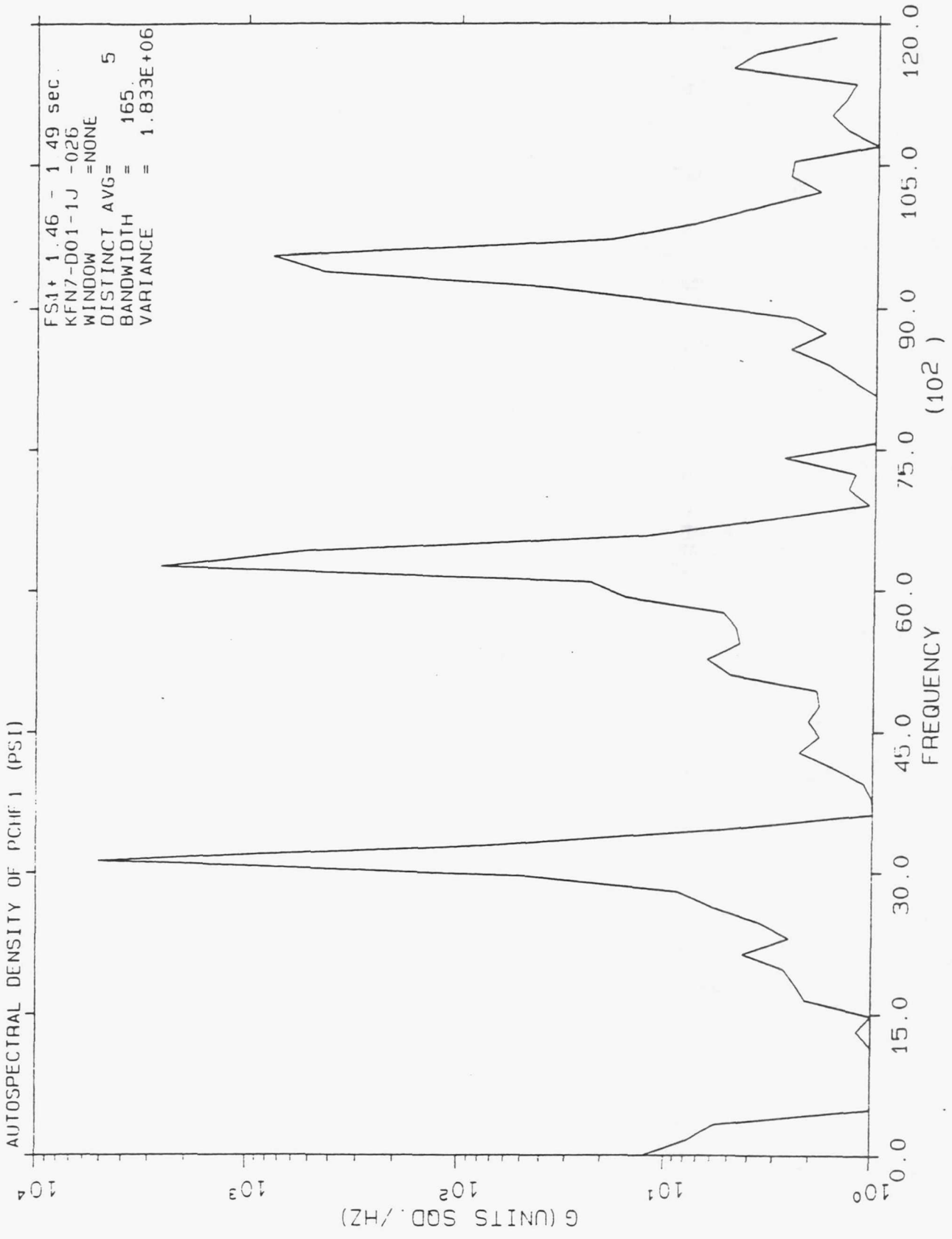
ROCCID Test Program



SPECTRA OF PCHF 1 (PSI) 19 SEGMENTS

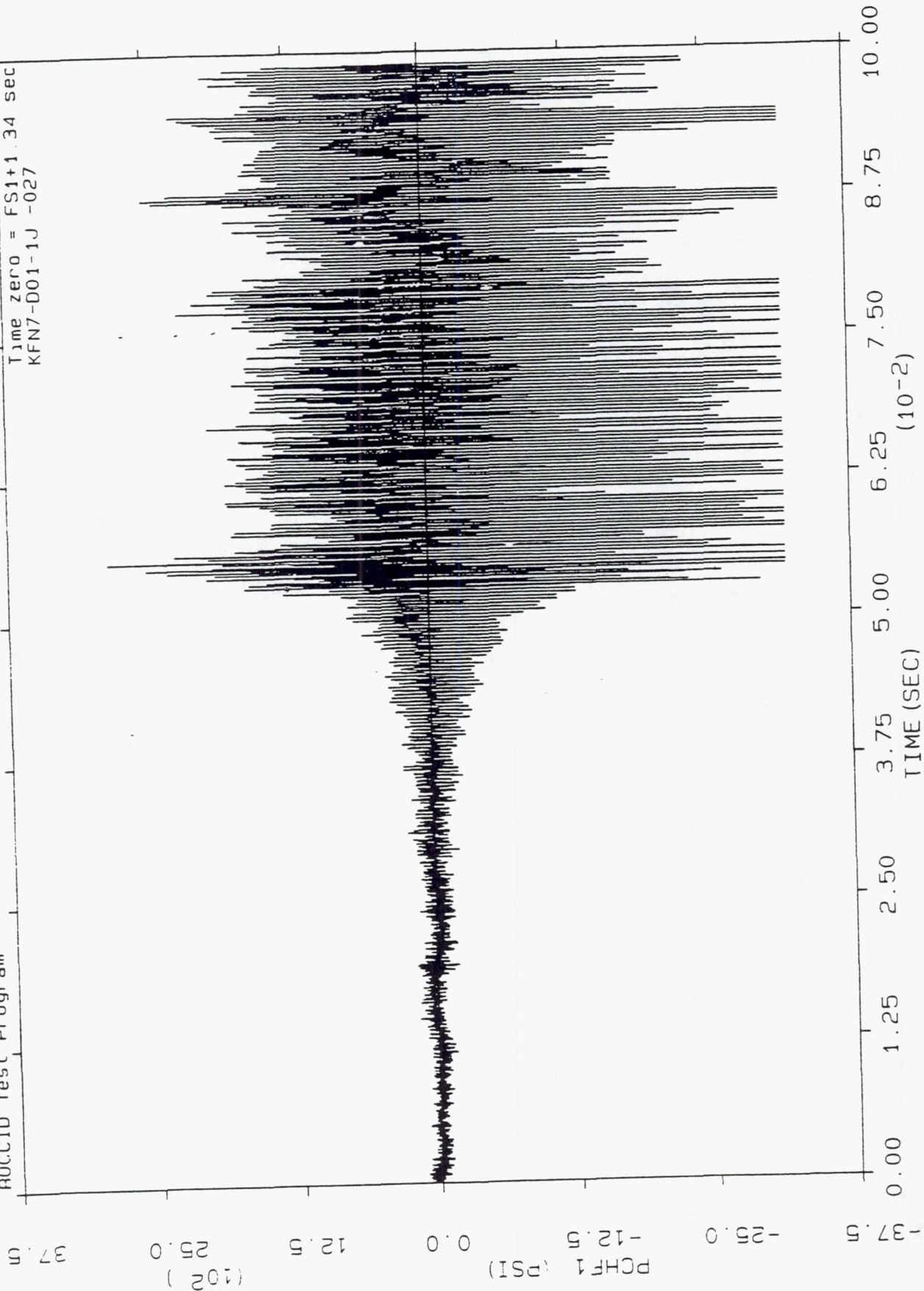
FS1+1 4 to FS1+1.5 sec
KEN7-001-1J -026
SEGMENT TIME= 5.000E-03
DAMPLITUDE = 400.
DF / SEGMENT= 200.
DH / SEGMENT= 316.





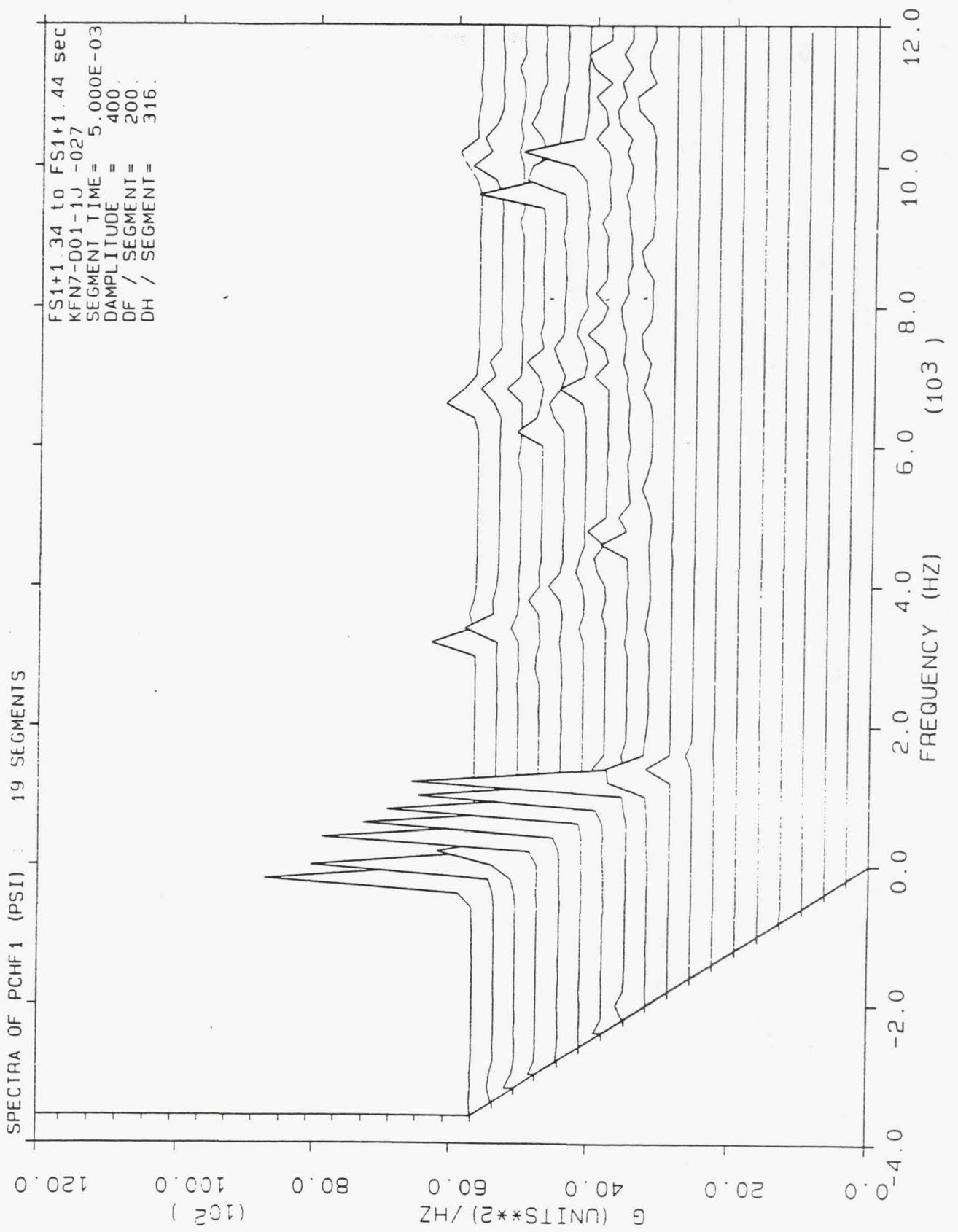
ROCCID Test Program

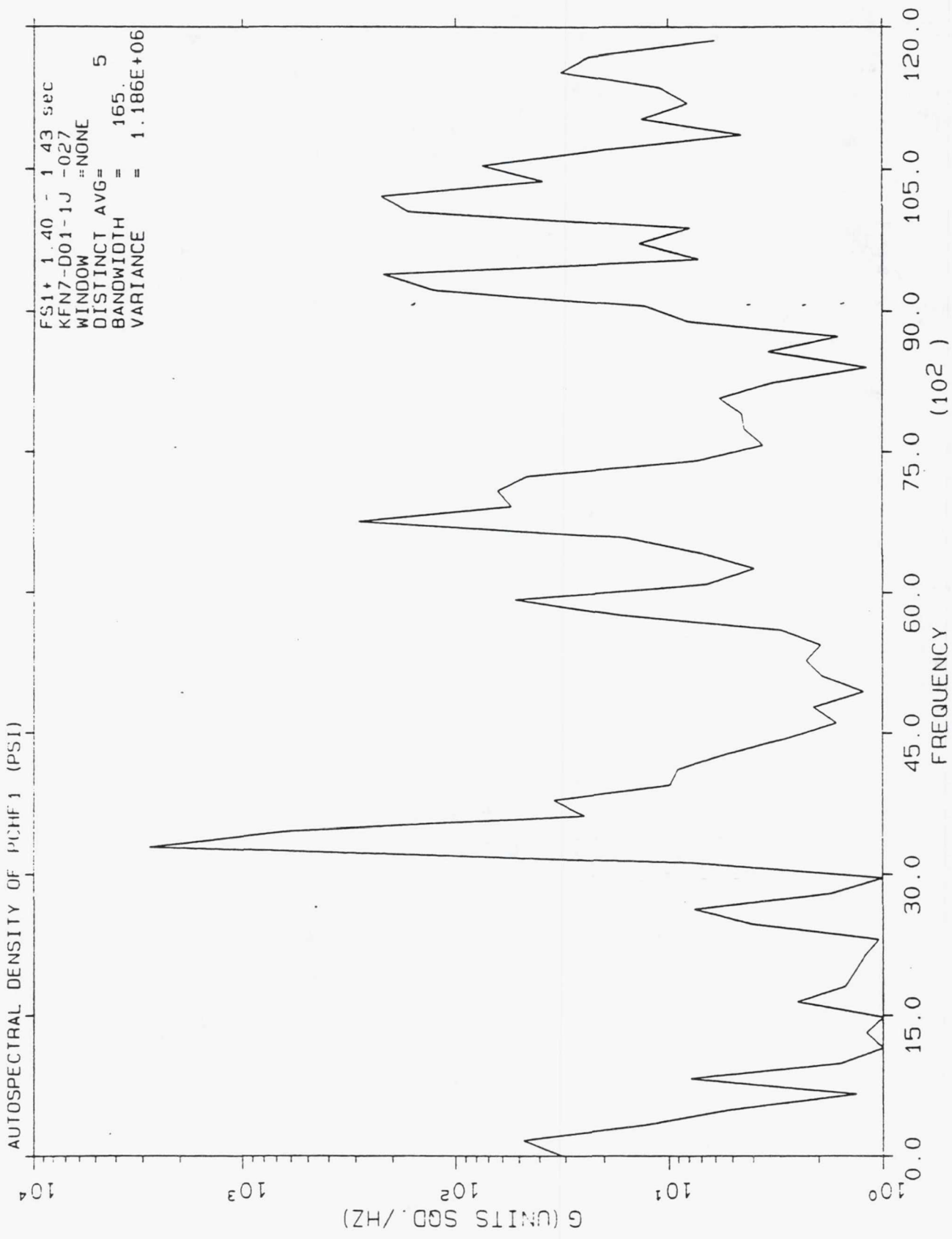
Time zero = FS1+1.34 sec
KFN7-D01-1J -027



SPECTRA OF PCHF1 (PSI) : 19 SEGMENTS

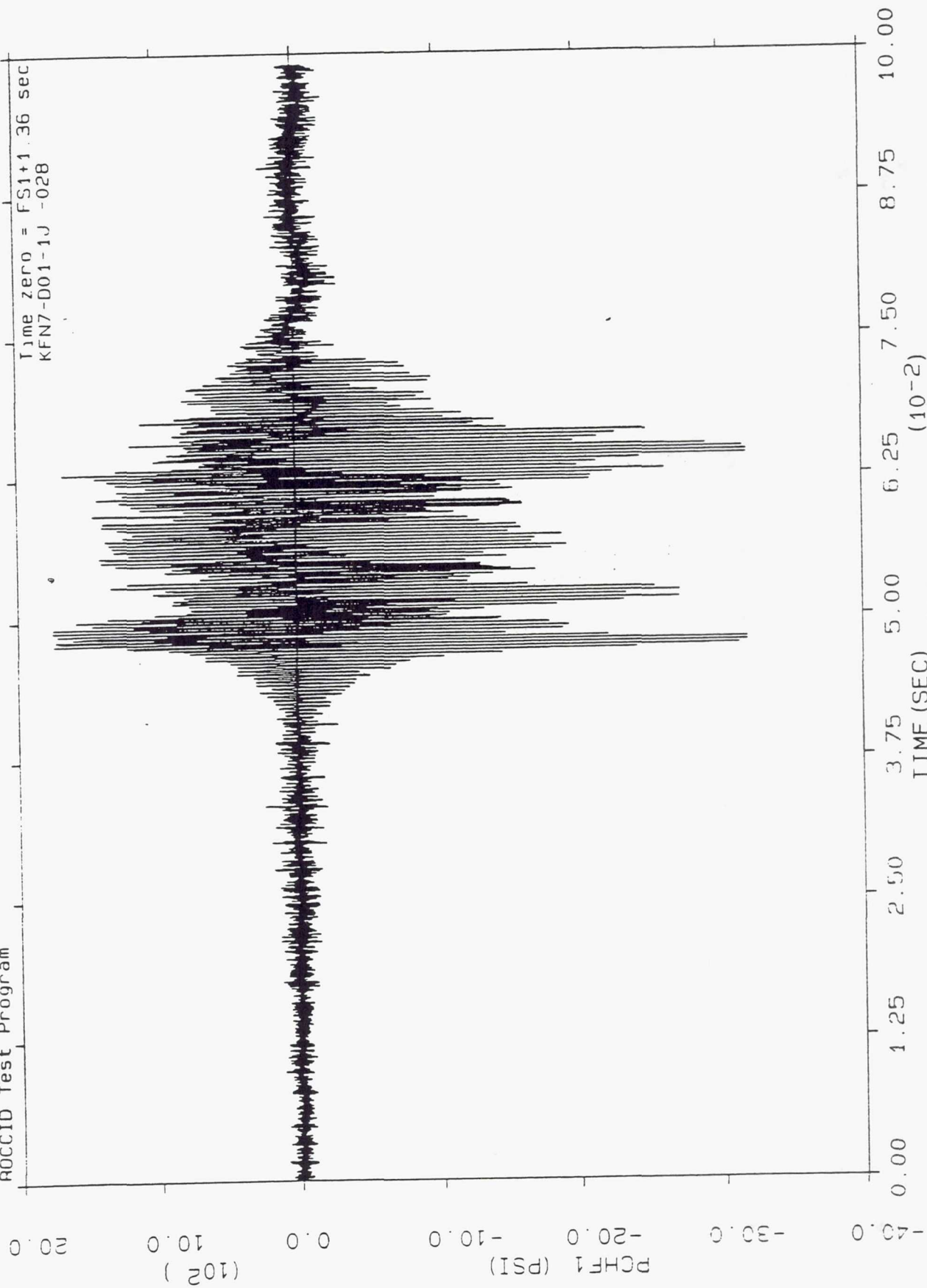
FS1+1.34 to FS1+1.44 sec
KFN7-001-1J -027
SEGMENT TIME = 5.000E-03
DAMPLITUDE = 400.
DF / SEGMENT = 200.
DH / SEGMENT = 316.



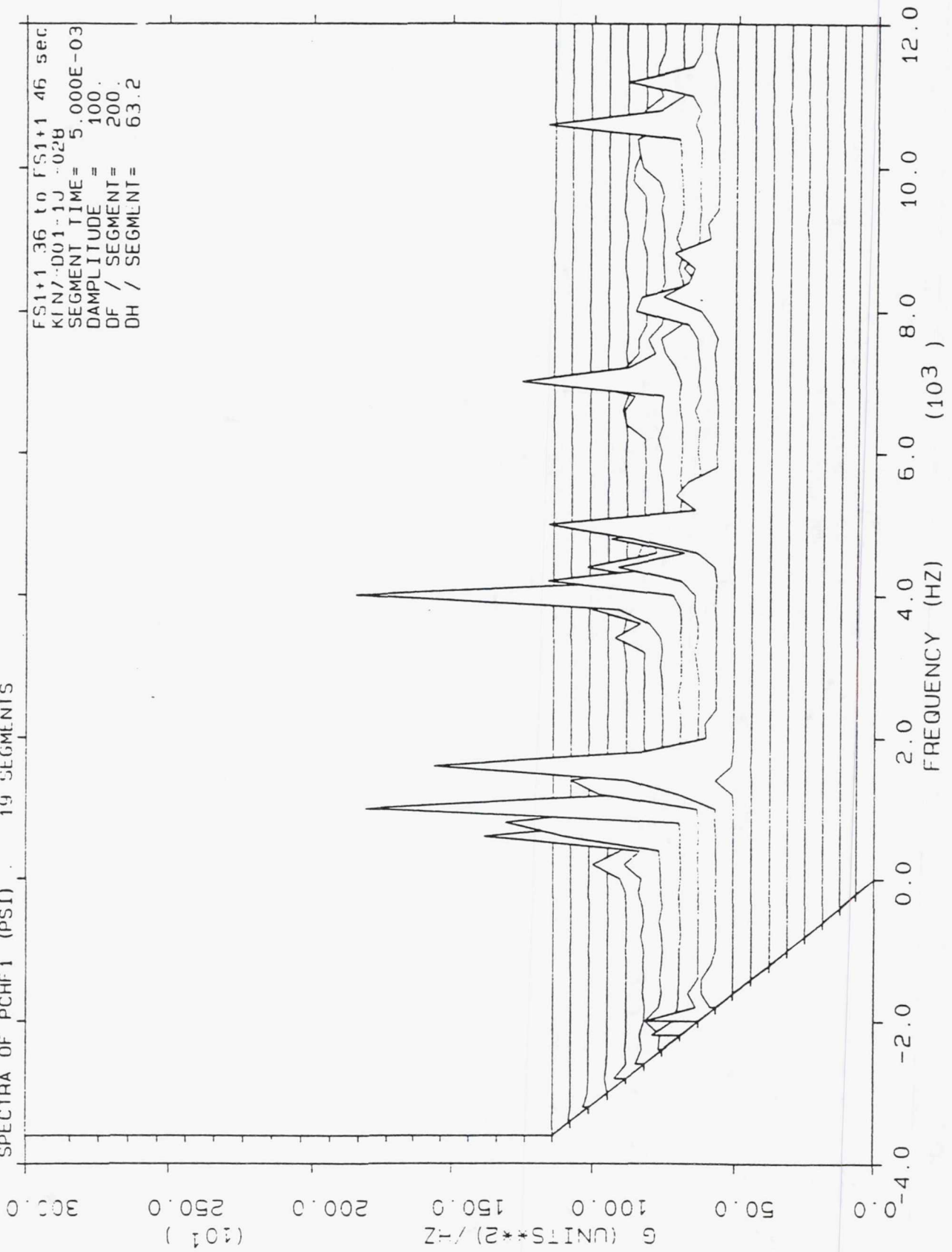


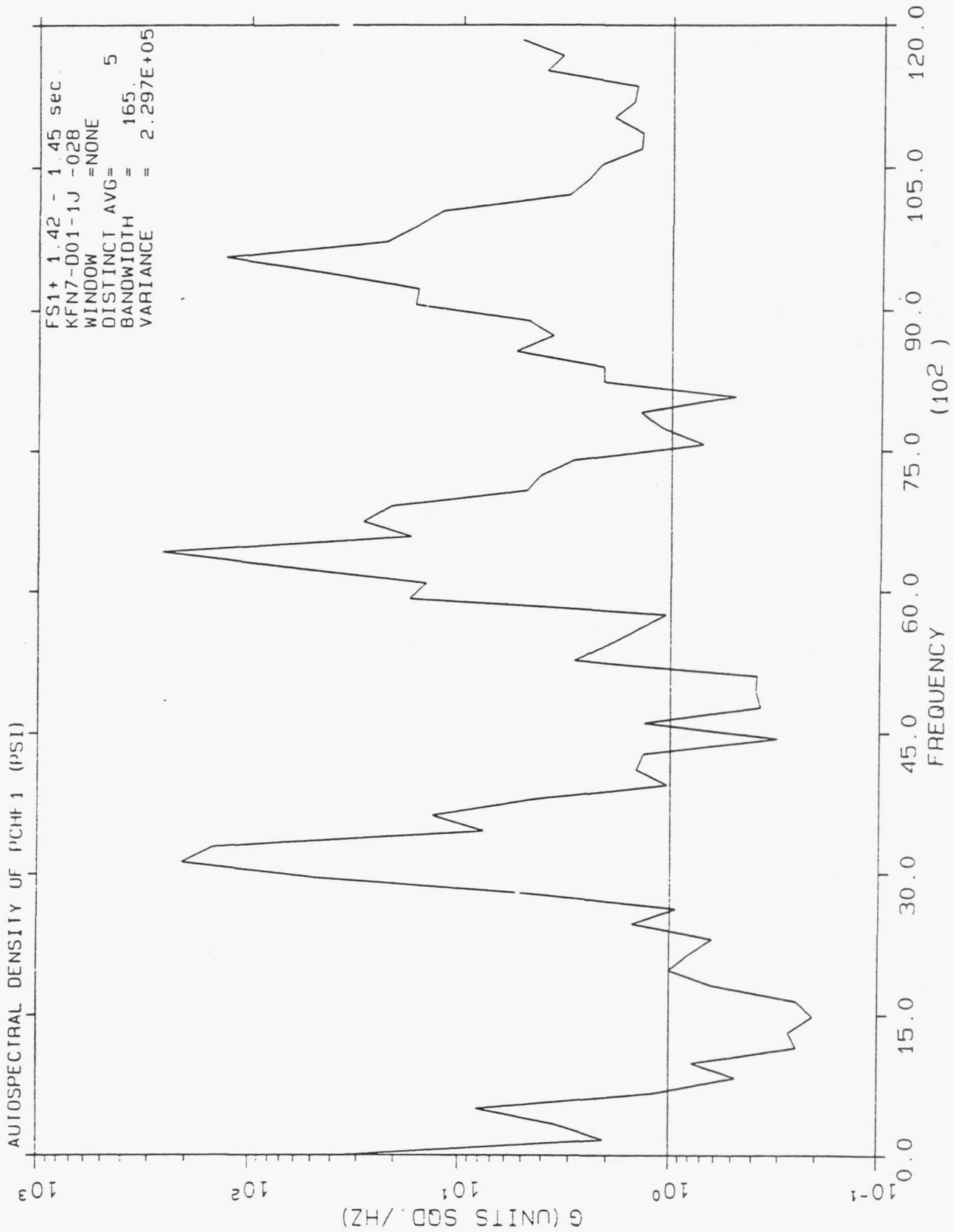
ROCCID Test Program

Time zero = FS1+1.36 sec
KFN7-D01-1J -028



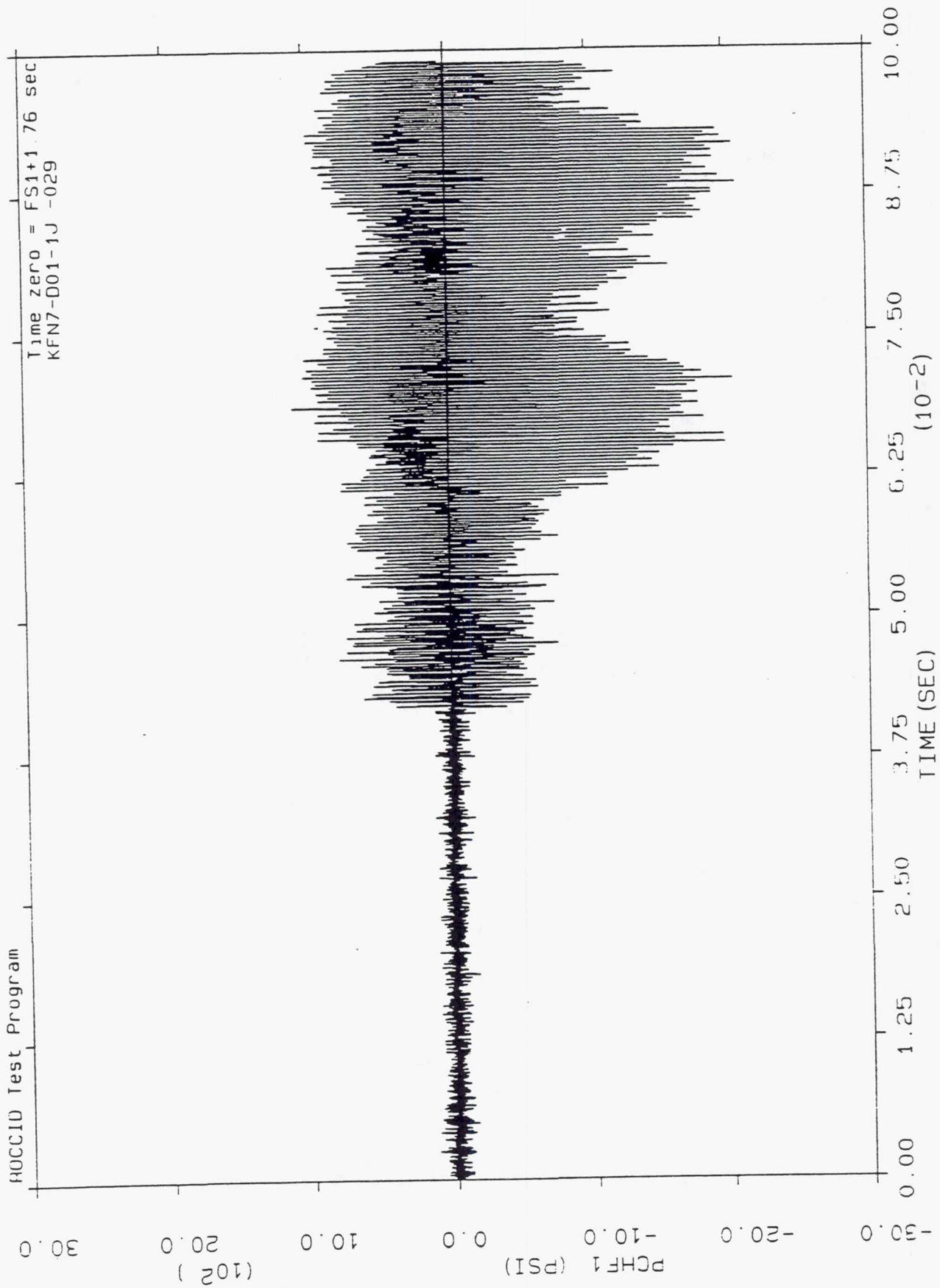
SPECTRA OF PCHF1 (PSI) 19 SEGMENTS



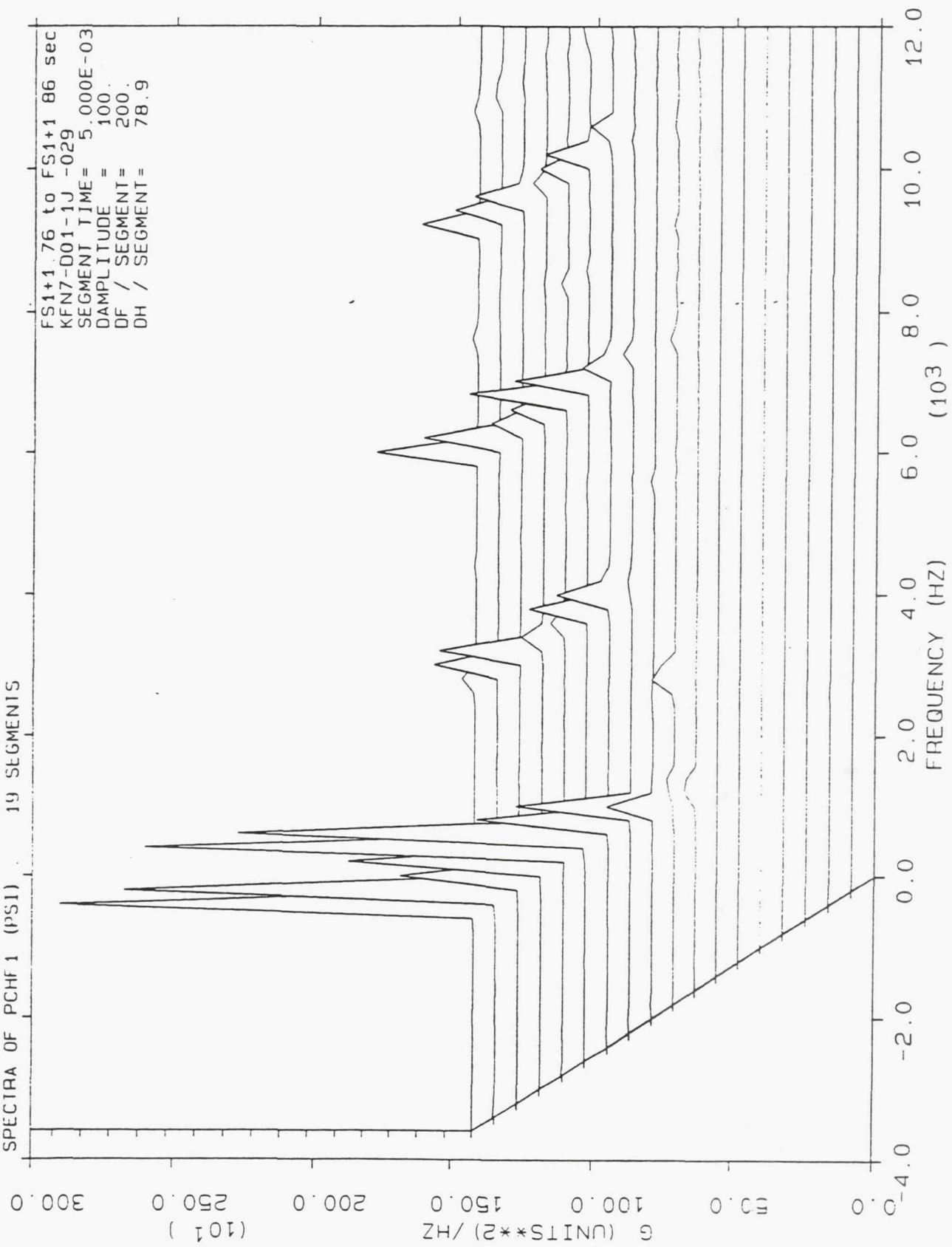


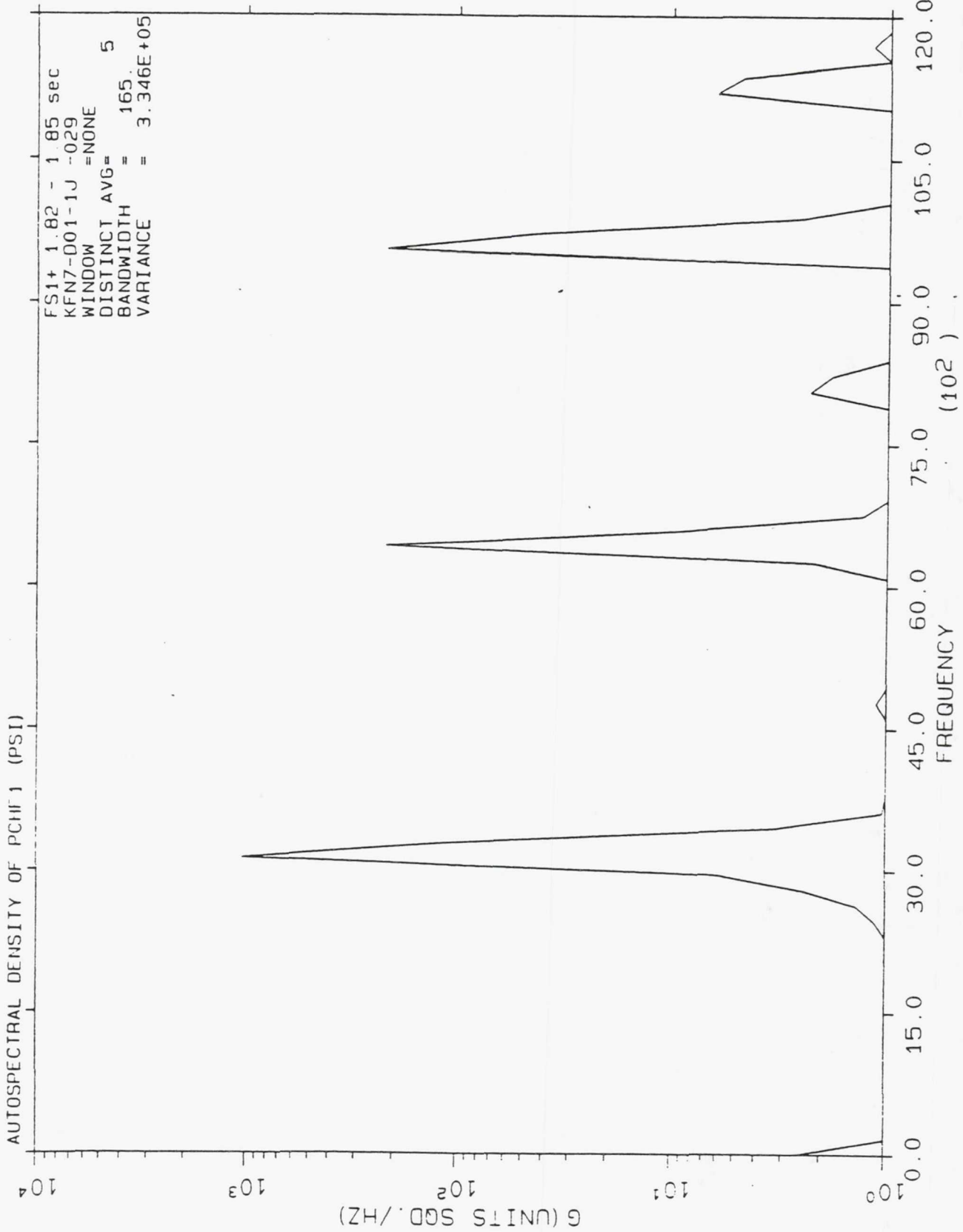
HOCC10 Test Program

Time zero = FS1+1.76 sec
KFN7-D01-1J -029



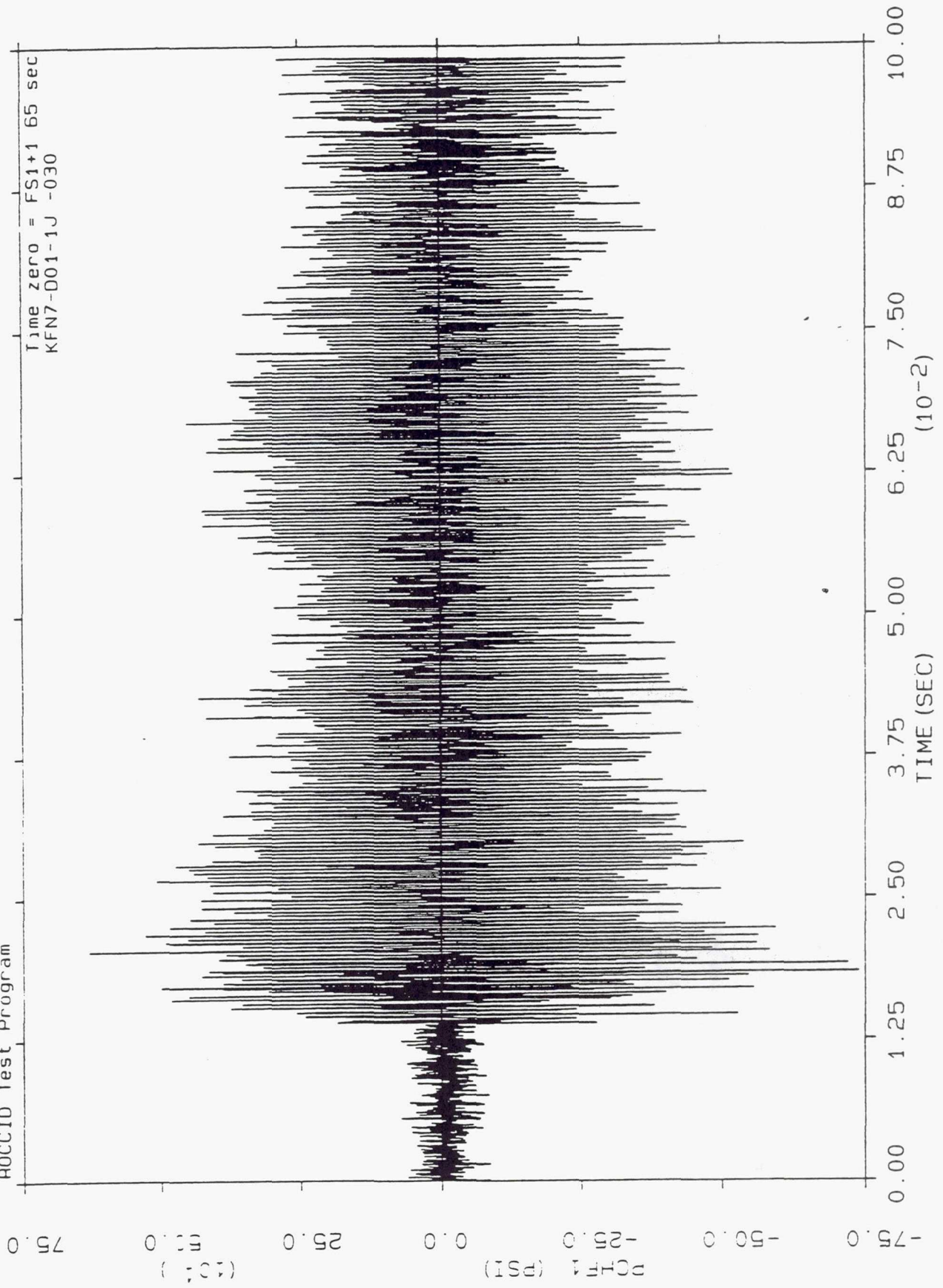
SPECTRA OF PCHF 1 (PSI) 19 SEGMENTS





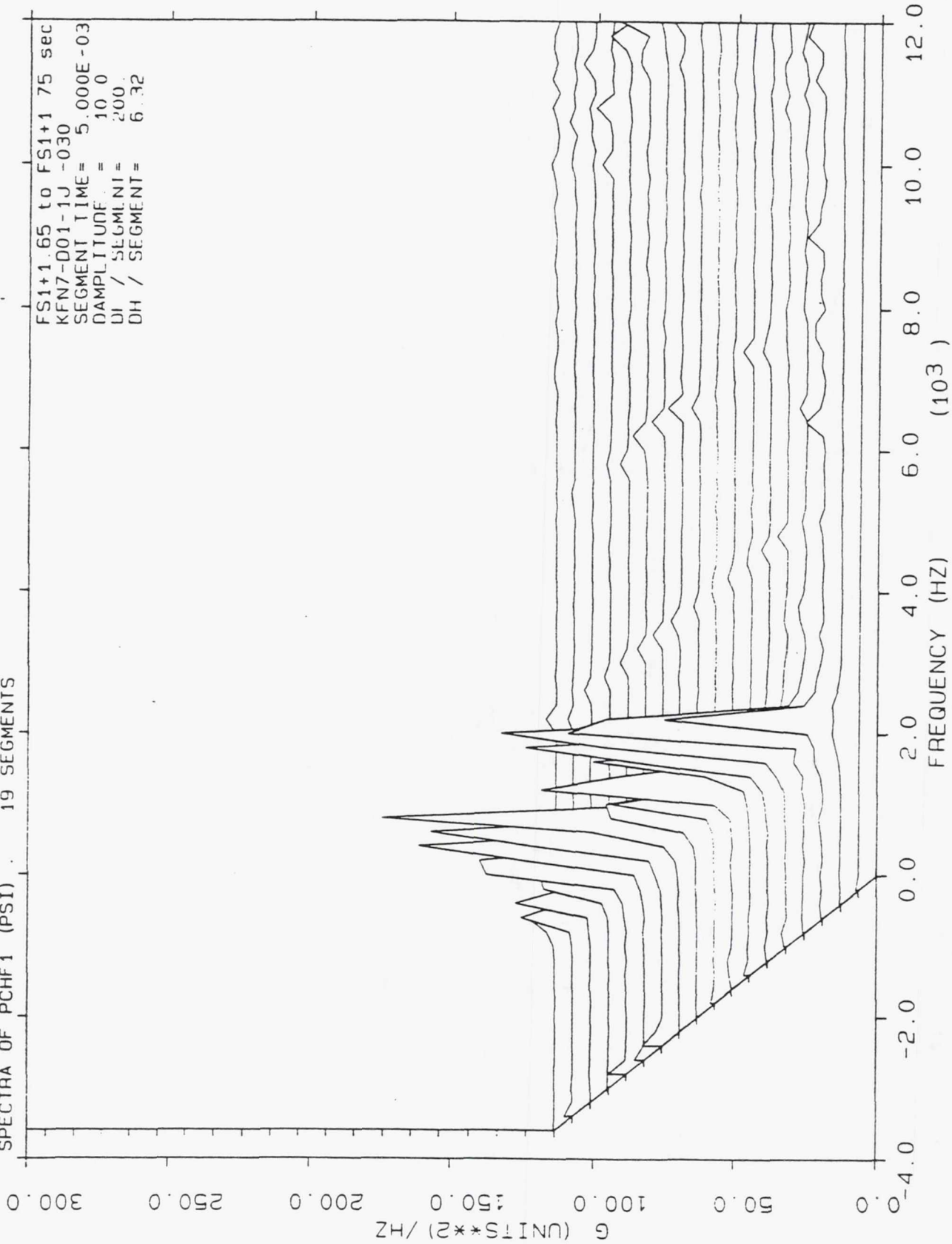
ROCCID Test Program

Time zero = FS1+1 65 sec
KFN7-D01-1J -030



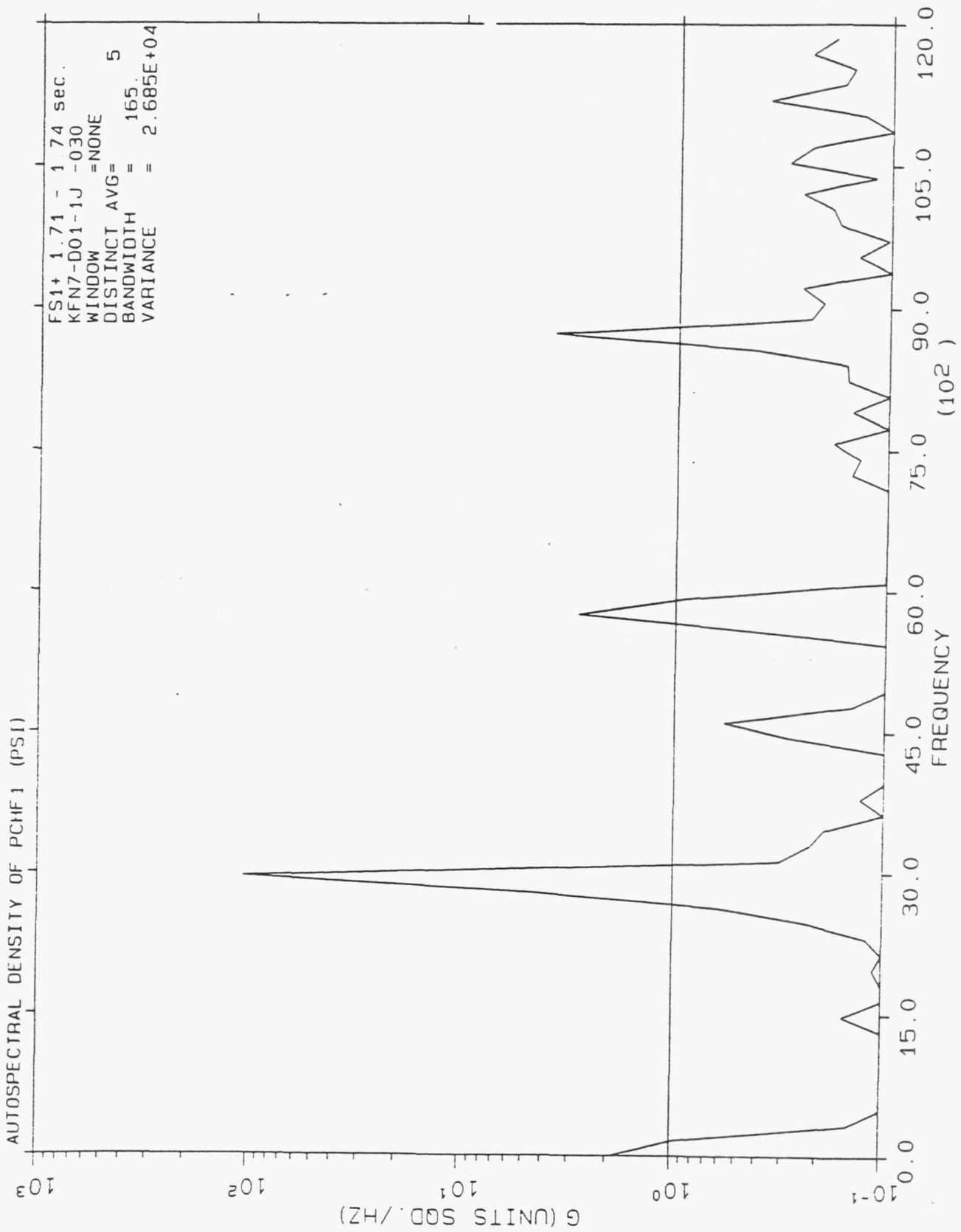
SPECTRA OF PCHF 1 (PSI) . 19 SEGMENTS

FS1+1.65 to FS1+1.75 sec
KFN7-D01-1J -030
SEGMENT TIME= 5.000E-03
DAMPLITUDE = 10 0
DI / SEGMENT= 200
DH / SEGMENT= 6.32



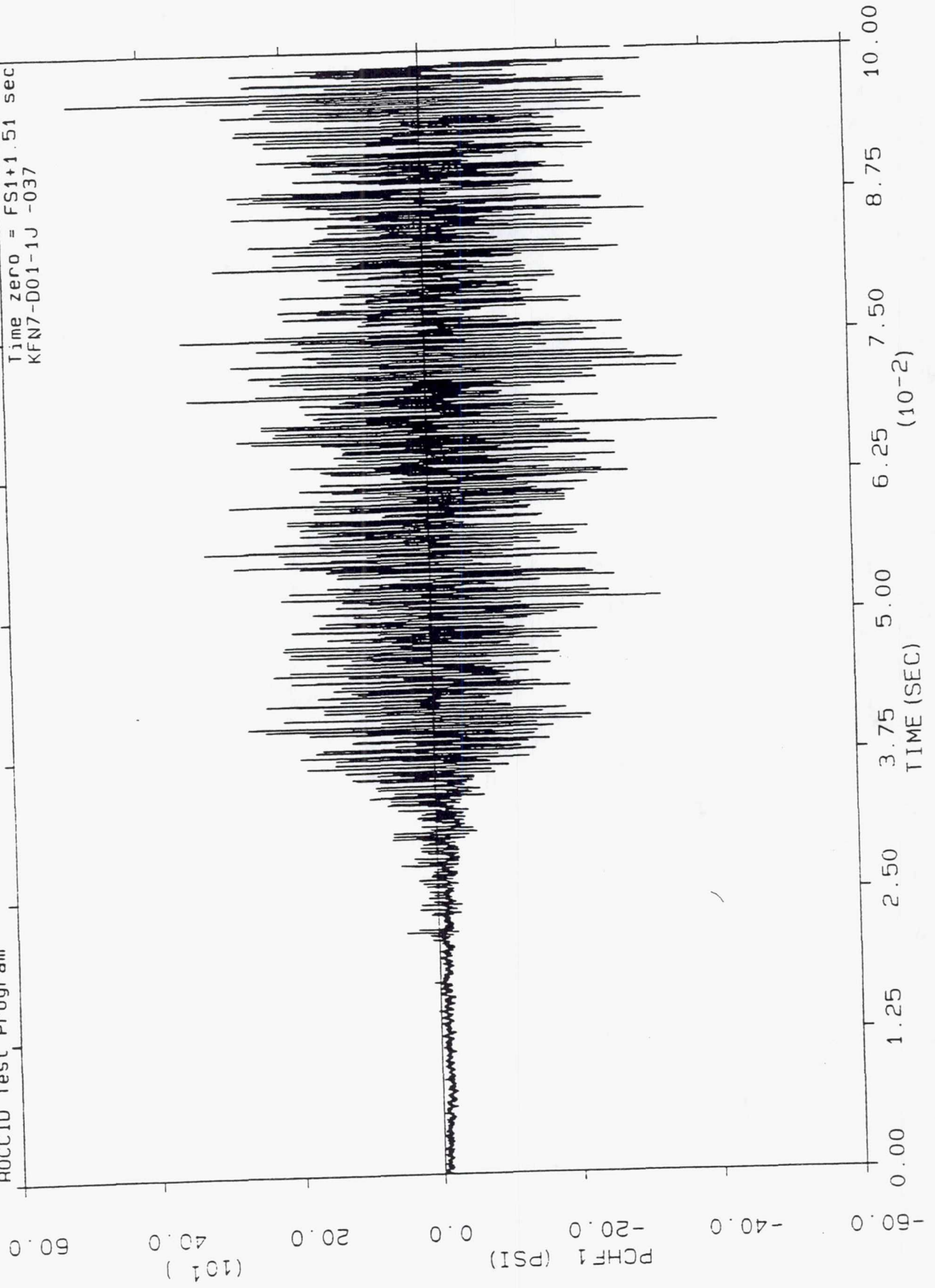
AUTOSPECTRAL DENSITY OF PCHF1 (PSI)

FS1+ 1.71 - 1.74 sec.
KFN7-D01-1J -030
WINDOW =NONE
DISTINCT AVG= 5
BANDWIDTH = 165.
VARIANCE = 2.685E+04



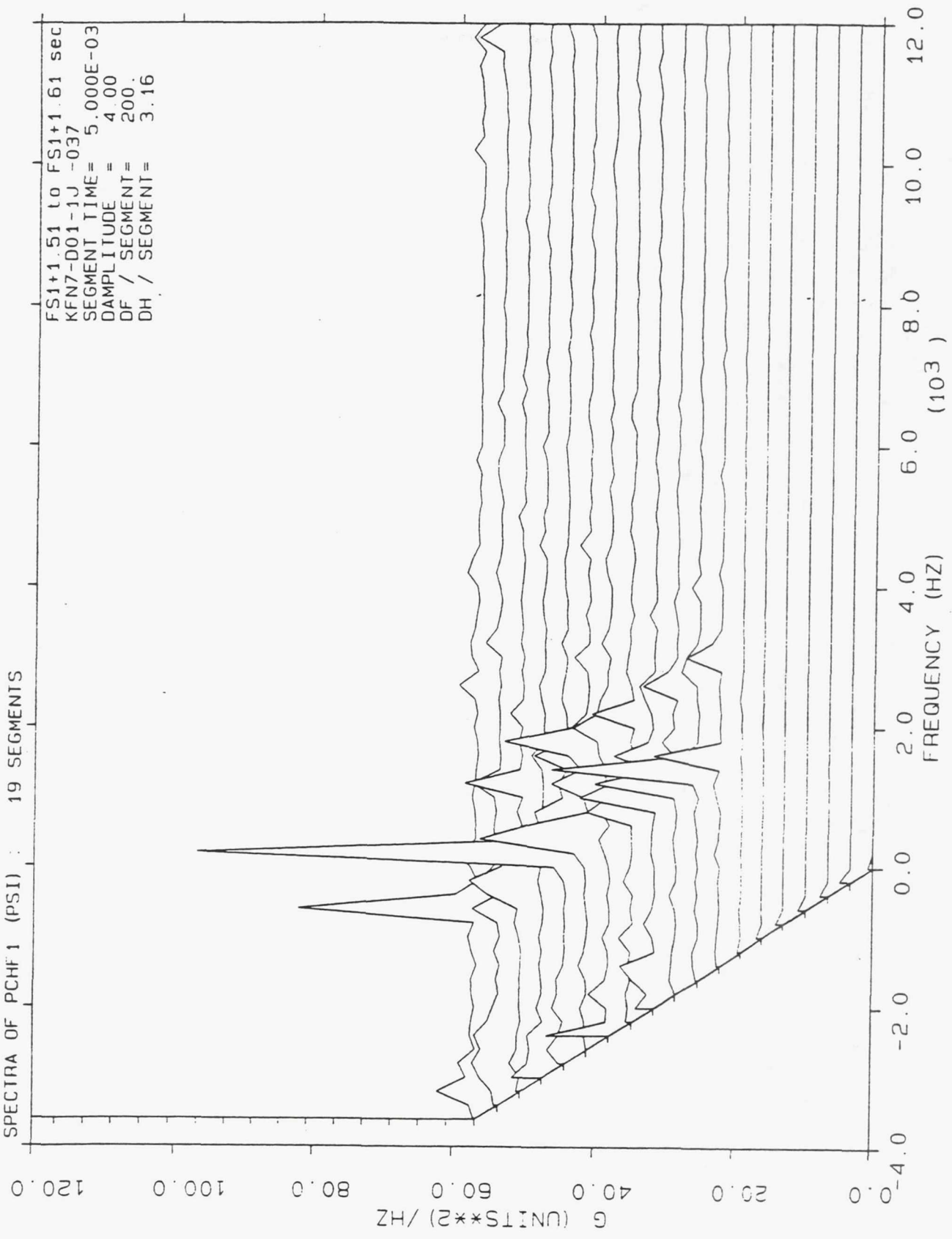
ROCCID Test Program

Time zero = FS1+1.51 sec
KFN7-D01-1J -037



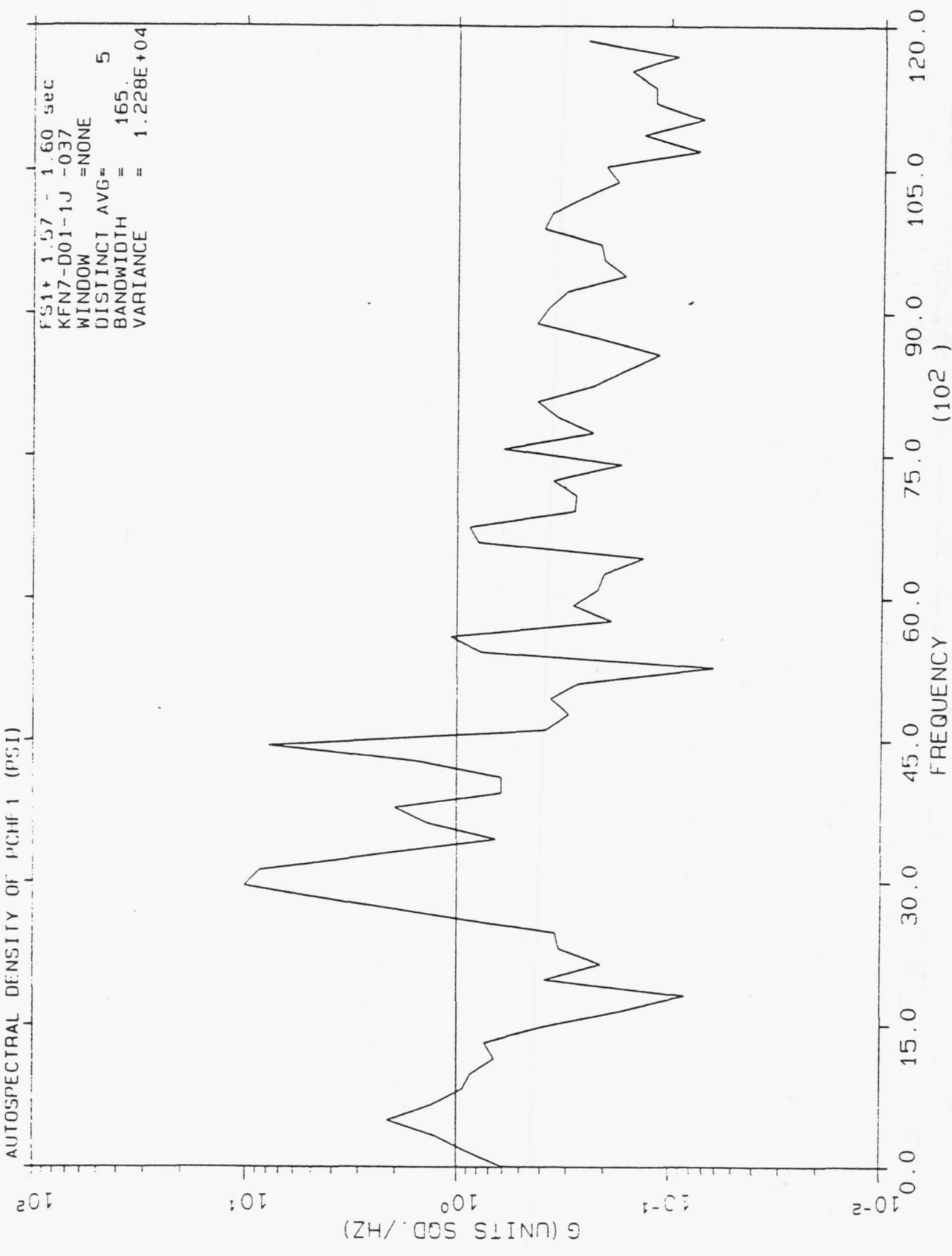
SPECTRA OF PCHF 1 (PSI) : 19 SEGMENTS

FS1+1.51 to FS1+1.61 sec
KFN7-001-1J -037
SEGMENT TIME= 5.000E-03
DAMPLITUDE = 4.00
DF / SEGMENT= 200.
DH / SEGMENT= 3.16



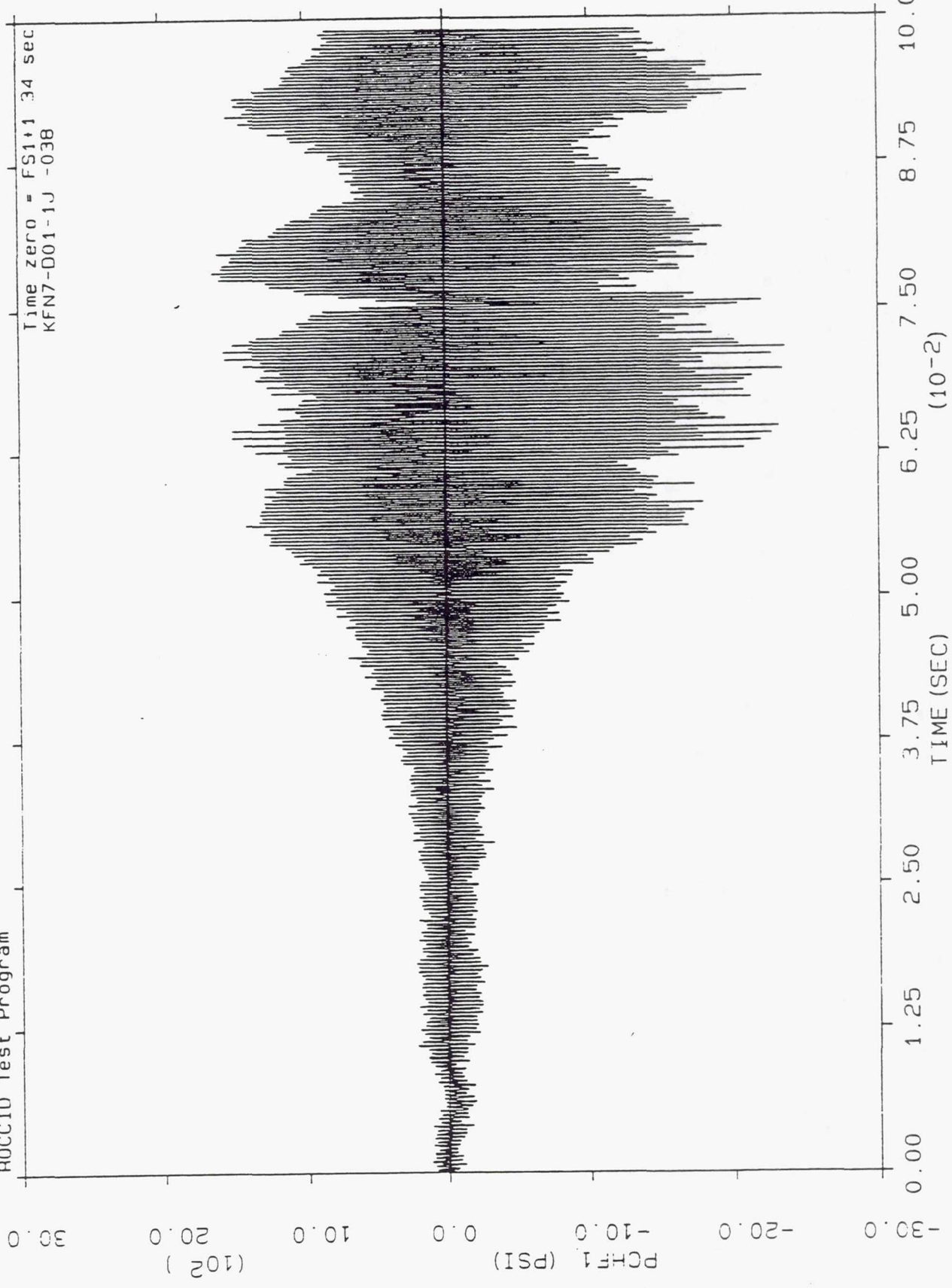
AUTOSPECTRAL DENSITY OF PCHF 1 (PSI)

FS1+ 1.57 - 1.60 sec
KFN7-D01-1J -037
WINDOW =NONE
DISTINCT AVG= 5
BANDWIDTH = 165.
VARIANCE = 1.228E+04



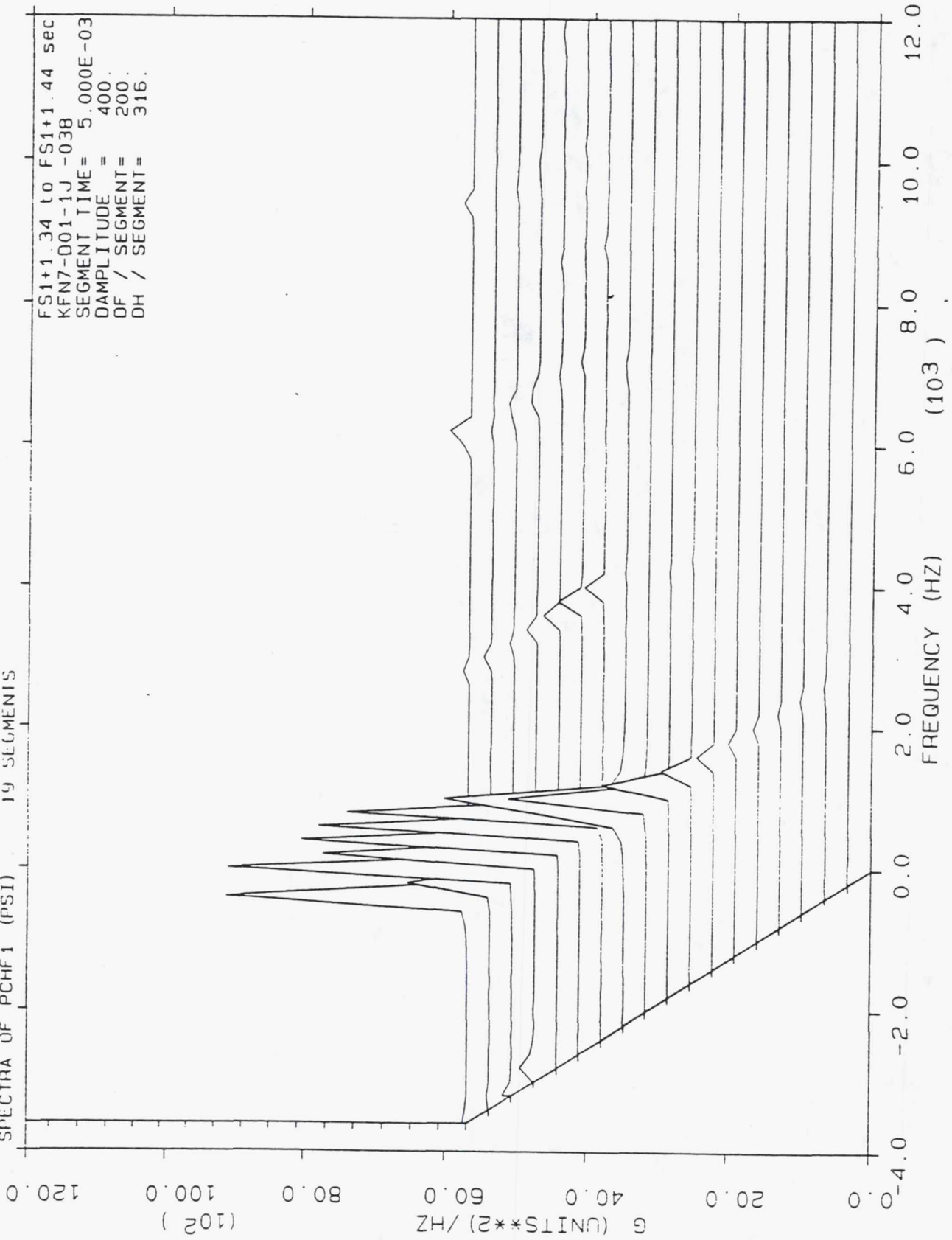
ROCCID Test Program

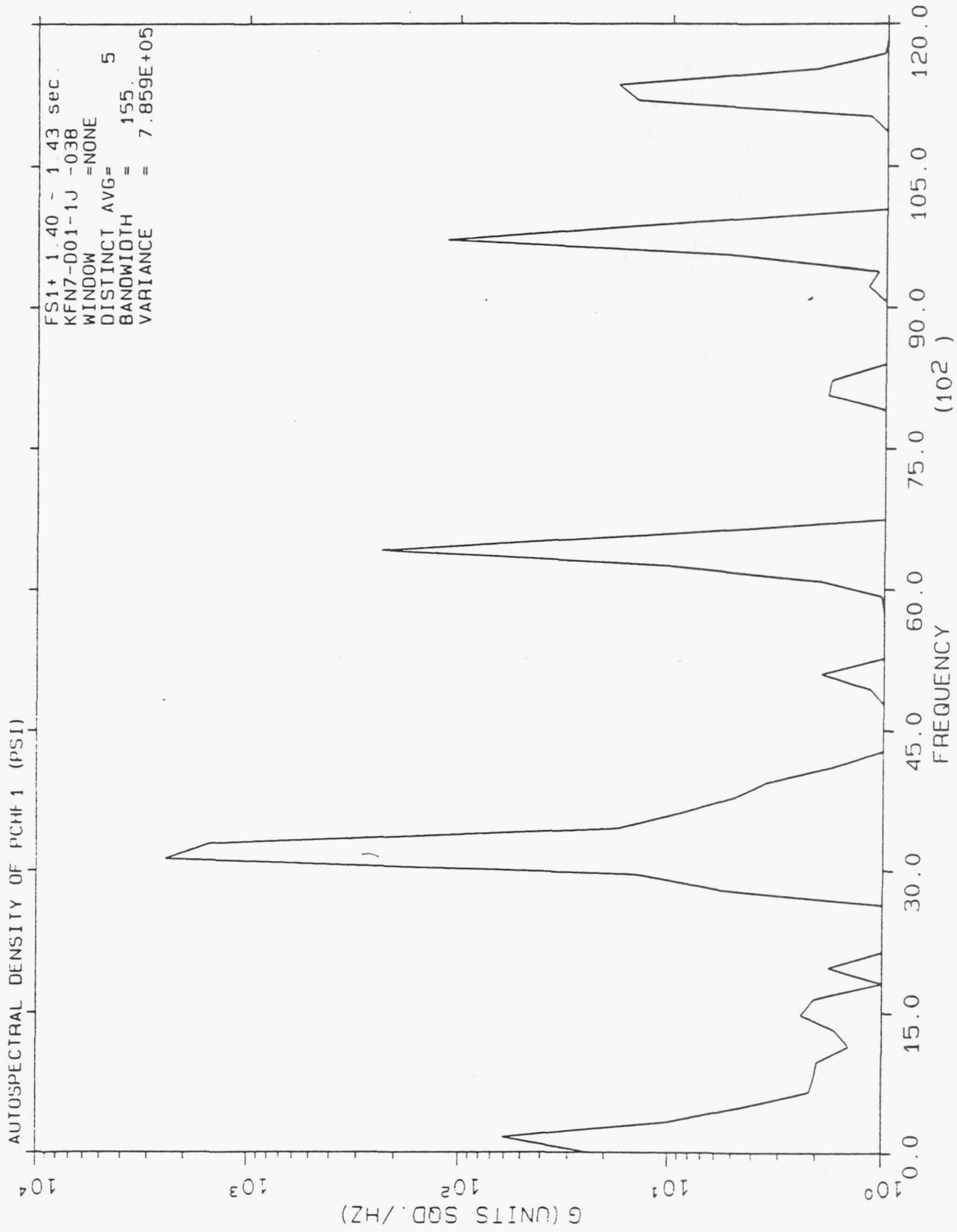
Time zero = FS1+1 34 sec
KFN7-D01-1J -038



SPECTRA OF PCHF1 (PSI) 19 SEGMENTS

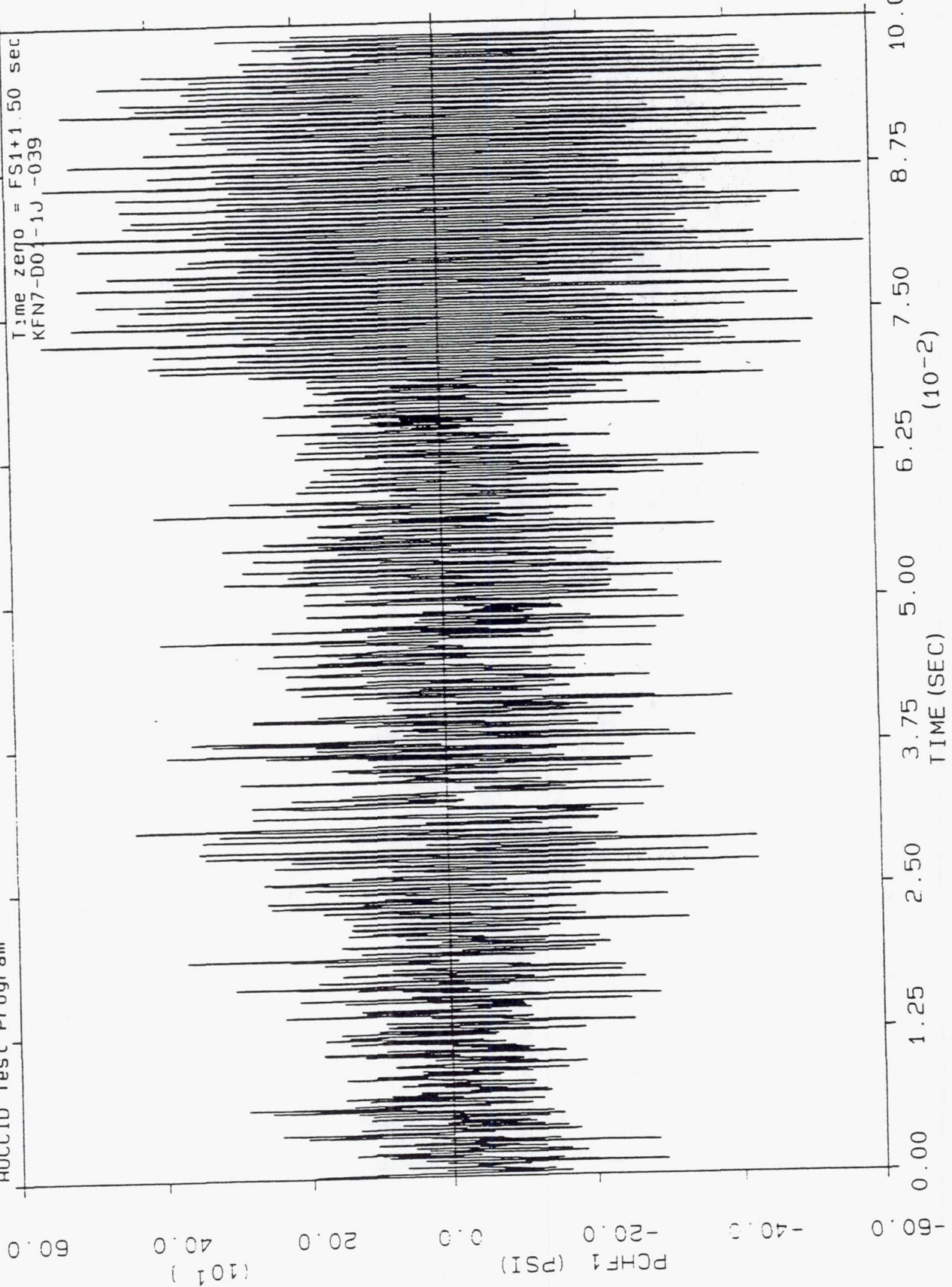
FS1+1.34 to FS1+1.44 sec
KFN7-001-1J -038
SEGMENT TIME= 5.000E-03
DAMPLITUDE = 400.
OF / SEGMENT= 200.
DH / SEGMENT= 316.





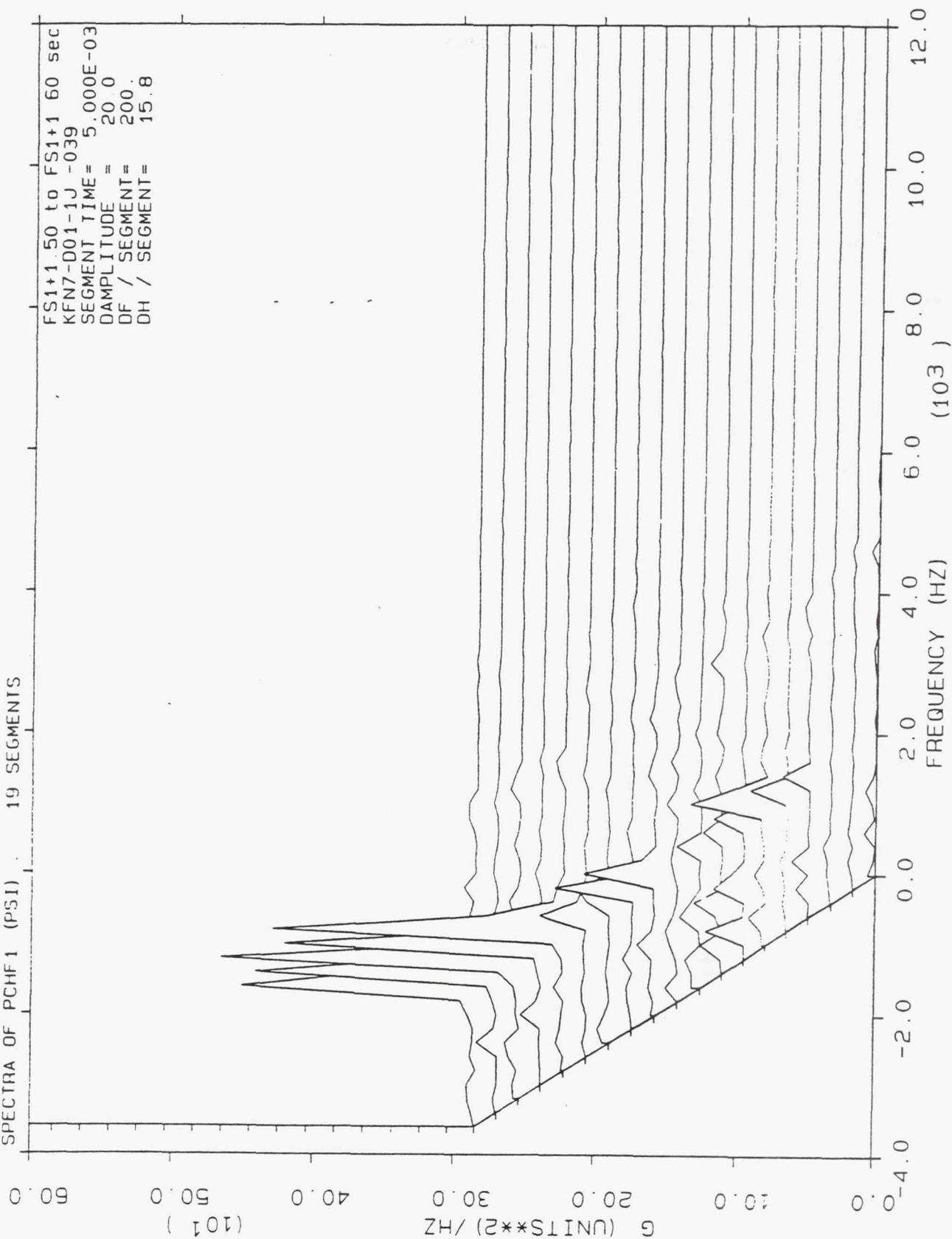
ROCCID Test Program

Time zero = FS1+1.50 sec
KFN7-D01-1J -039

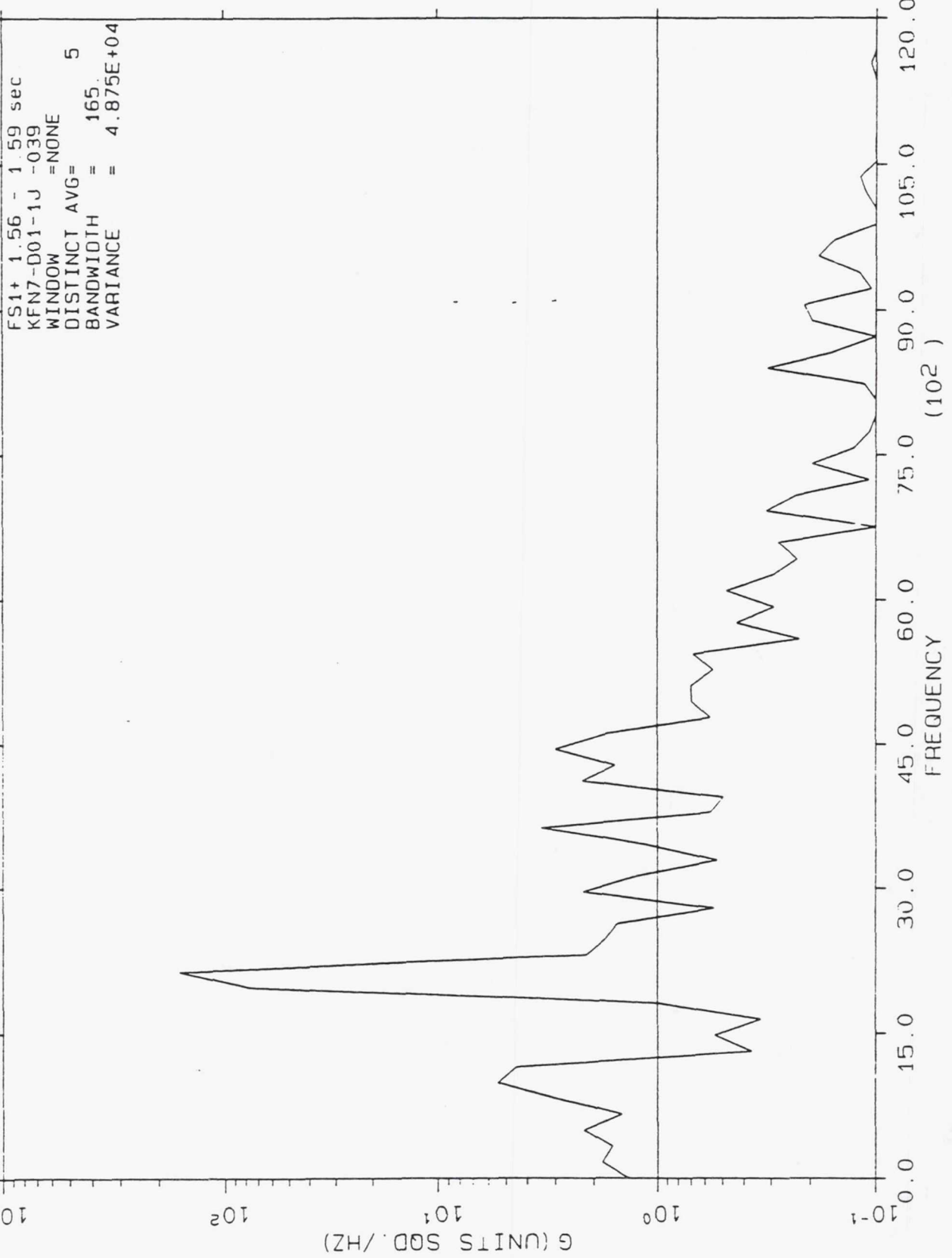


SPECTRA OF PCHF1 (PSI) 19 SEGMENTS

FS1+1 50 to FS1+1 60 sec
KFN7-001-1J -039
SEGMENT TIME= 5.000E-03
DAMPLITUDE = 20.0
DF / SEGMENT= 200.
DH / SEGMENT= 15.8

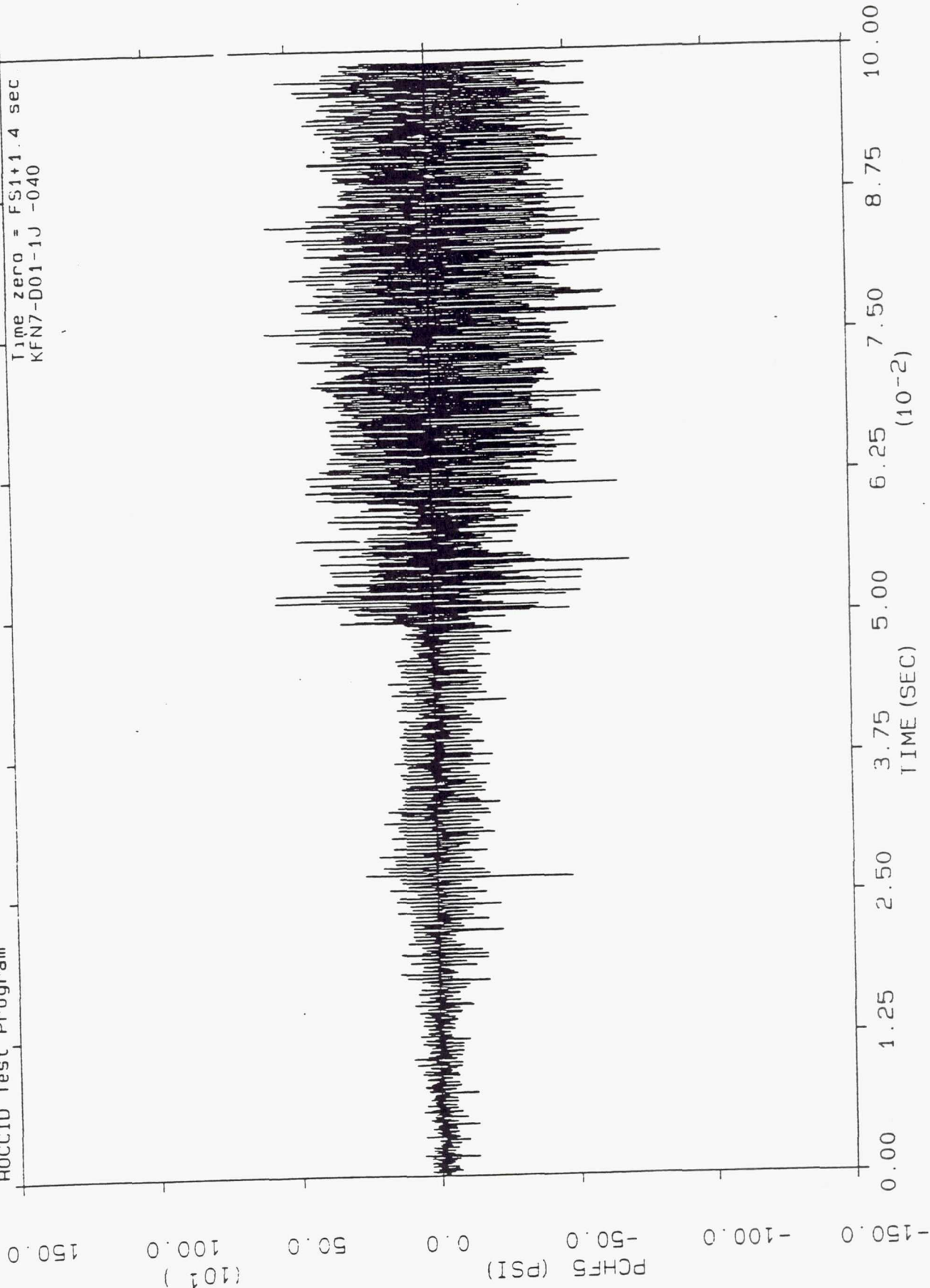


AUTOSPECTRAL DENSITY OF PCHP 1 (PSI)

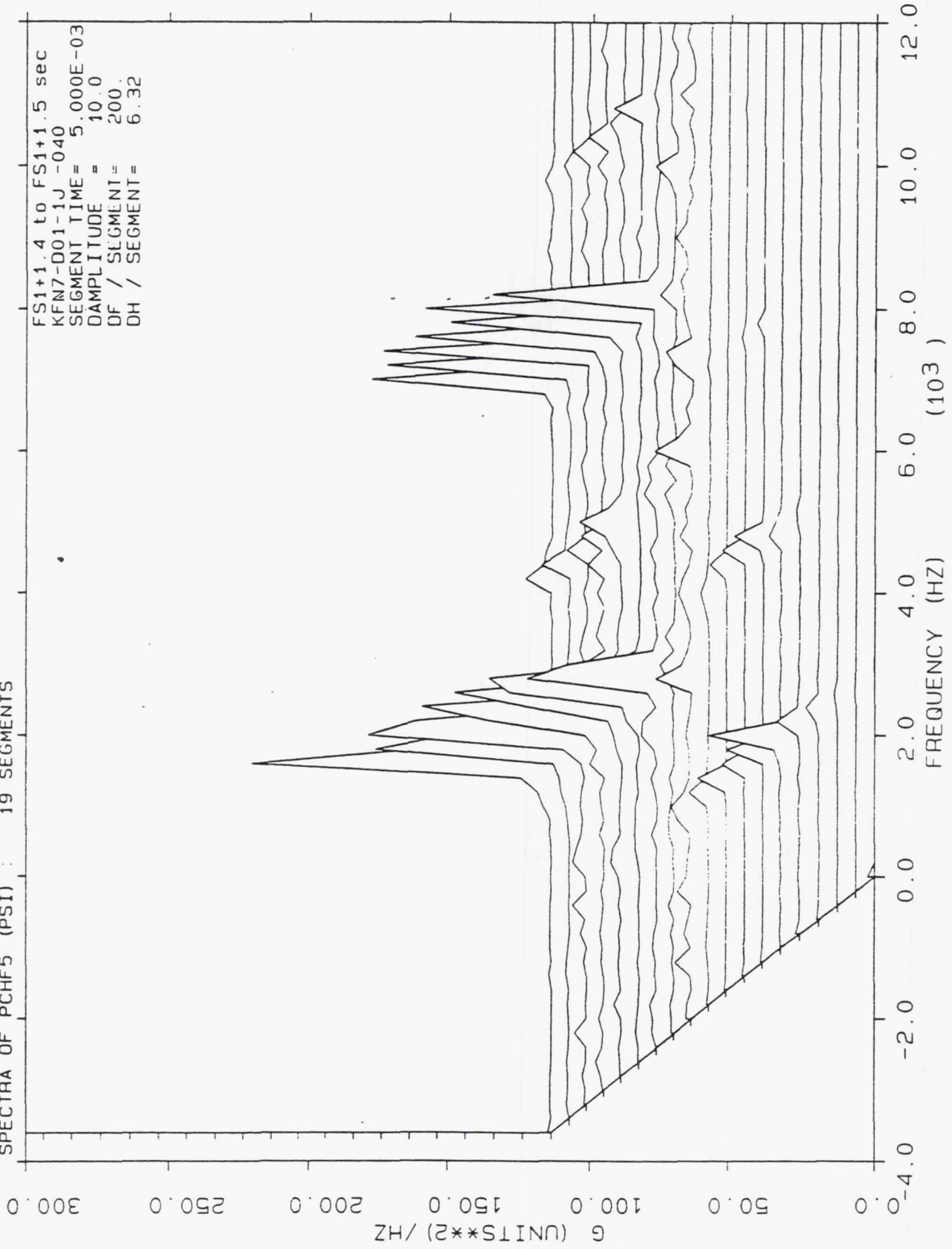


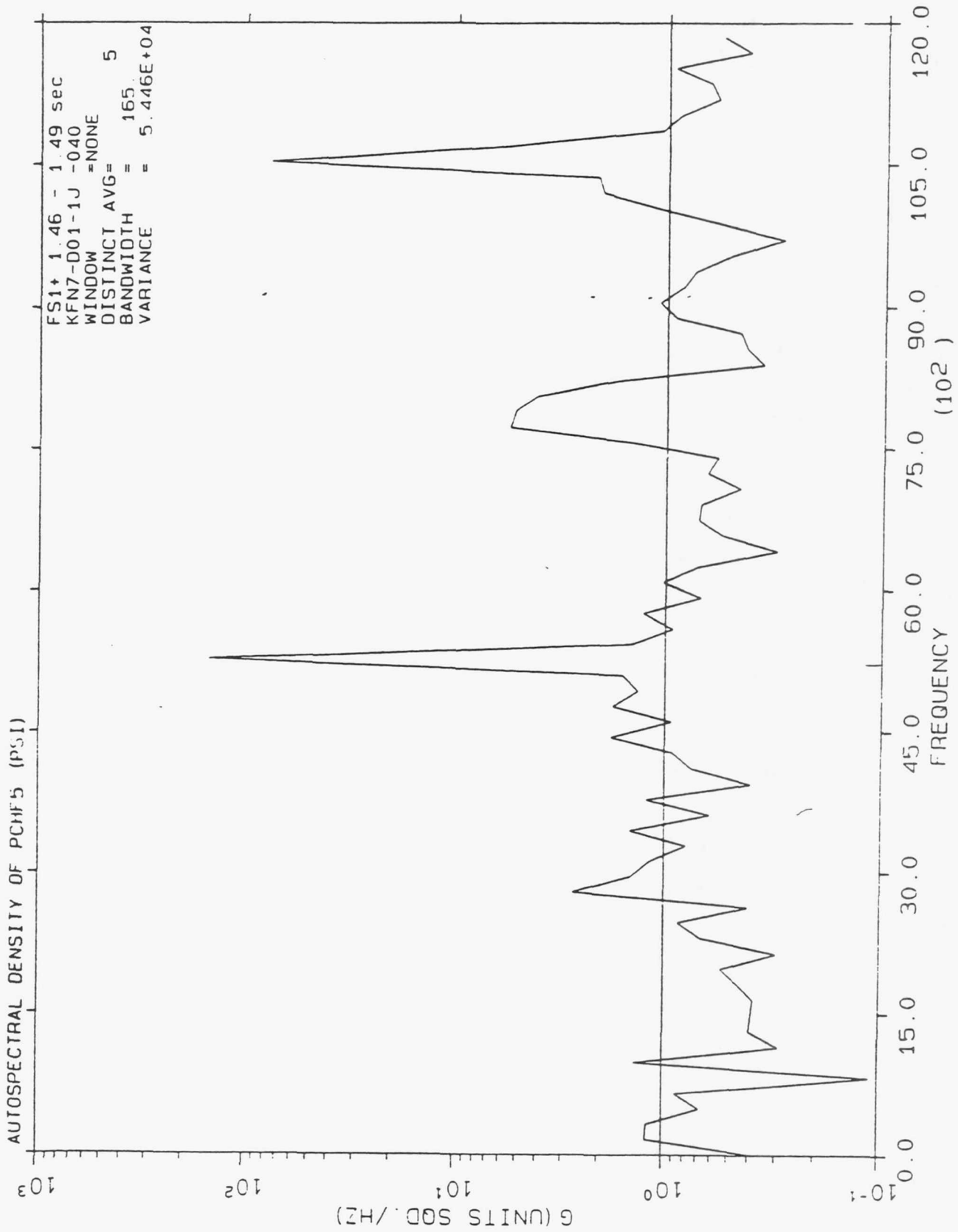
HOCCID Test Program

Time zero = FS1+1.4 sec
KFN7-D01-1J -040



SPECTRA OF PCHF5 (PSI) : 19 SEGMENTS





APPENDIX C

TIME SERIES, AMPLITUDE AND FREQUENCY EVOLUTION, AND POWER
SPECTRAL ANALYSIS OF MANIFOLD AND CHAMBER
PRESSURES AND ACCELERATIONS FOR TEST 004

INDEX OF TEST DATA PLOTS
ALL DATA OBTAINED FROM TEST NO. KFN7-D01-1J-004

High Frequency Measurement Parameter	High Frequency Amplitude Versus Time Playback	Power Spectral Analysis	Power Spectral Density
(Page Nos. for Specific Plot for Each Parameter)			
PCHF-1	C-2	C-3	C-4
PCHF-2	C-5	C-6	C-7
PCHF-3	C-8	C-9	C-10
PCHF-4	C-11	C-12	C-13
PCHF-5	C-14	C-15	C-16
POJHF	C-17	C-18	C-19
PFJHF	C-20	C-21	C-22
AX	C-23	C-24	C-25
AY	C-26	C-27	C-28
AZ	C-29	C-30	C-31

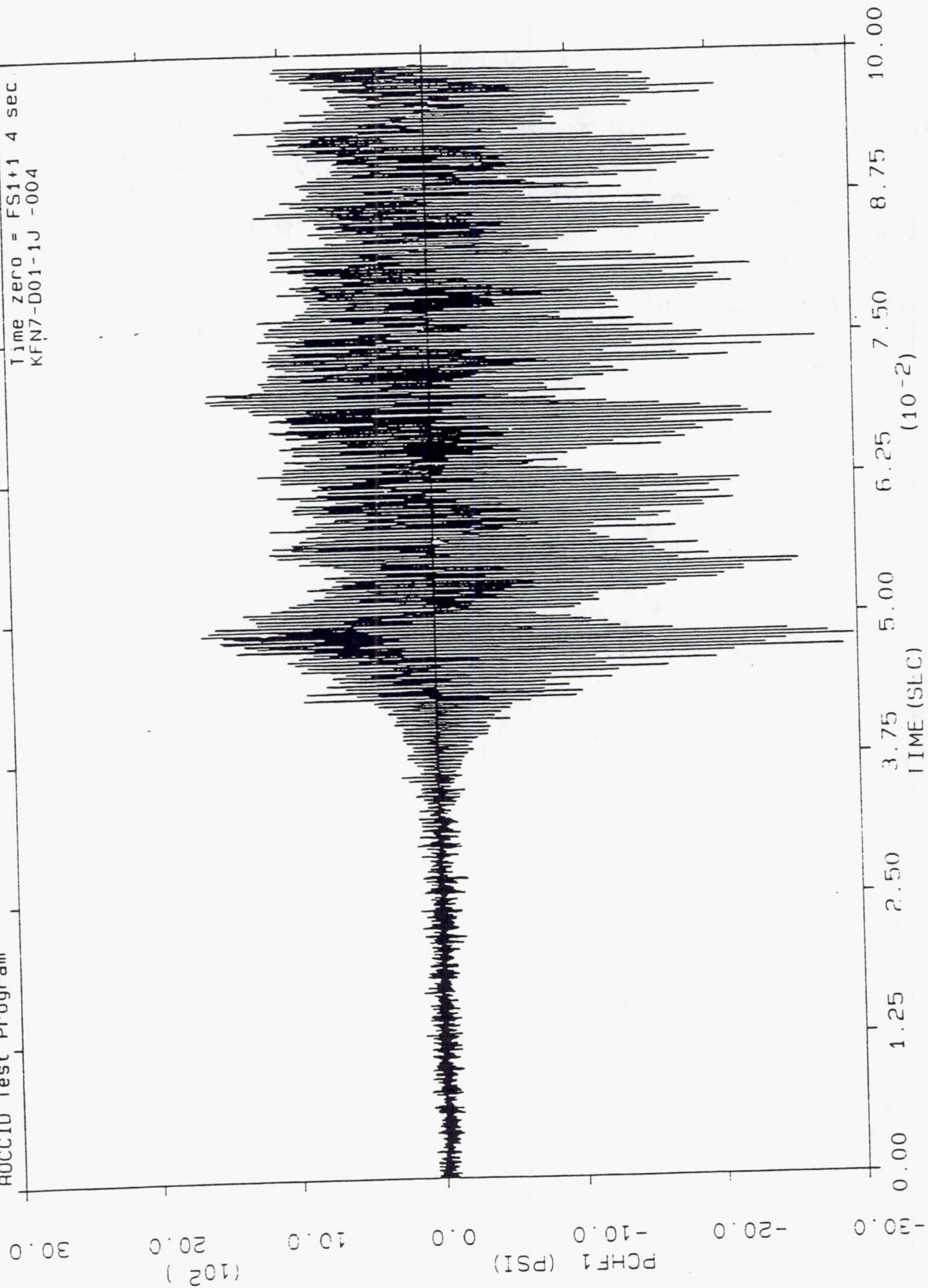
<u>Symbol</u>	<u>Parameter Definition</u>
PCHF	High Frequency Chamber Pressure (PSI)
POJHF	High Frequency LOX Injector Manifold Pressure (PSI)
PFJHF	High Frequency RP-1 Injector Manifold Pressure (PSI)
AX	Accelerometer X Axis (g's)
AY	Accelerometer Y Axis (g's)
AZ	Accelerometer Z Axis (g's)

FOREWORD

Included in this appendix is a complete display of high frequency measurements obtained during test KFN7-D01-1J-004. A total of 10 parameters are displayed including five high frequency chamber pressure measurements (see Figure 51 of Volume I for measurement locations), one each high frequency pressure measurements located in the injector manifold inlet pipes of the fuel and oxidizer circuits, and three accelerometer recordings obtained from a tri-axial accelerometer mounted on the injector assembly. High frequency amplitude versus time, power spectral analysis and power spectral density plots for each of the 10 parameters are included. The plot formats are the same as those described in Appendix B.

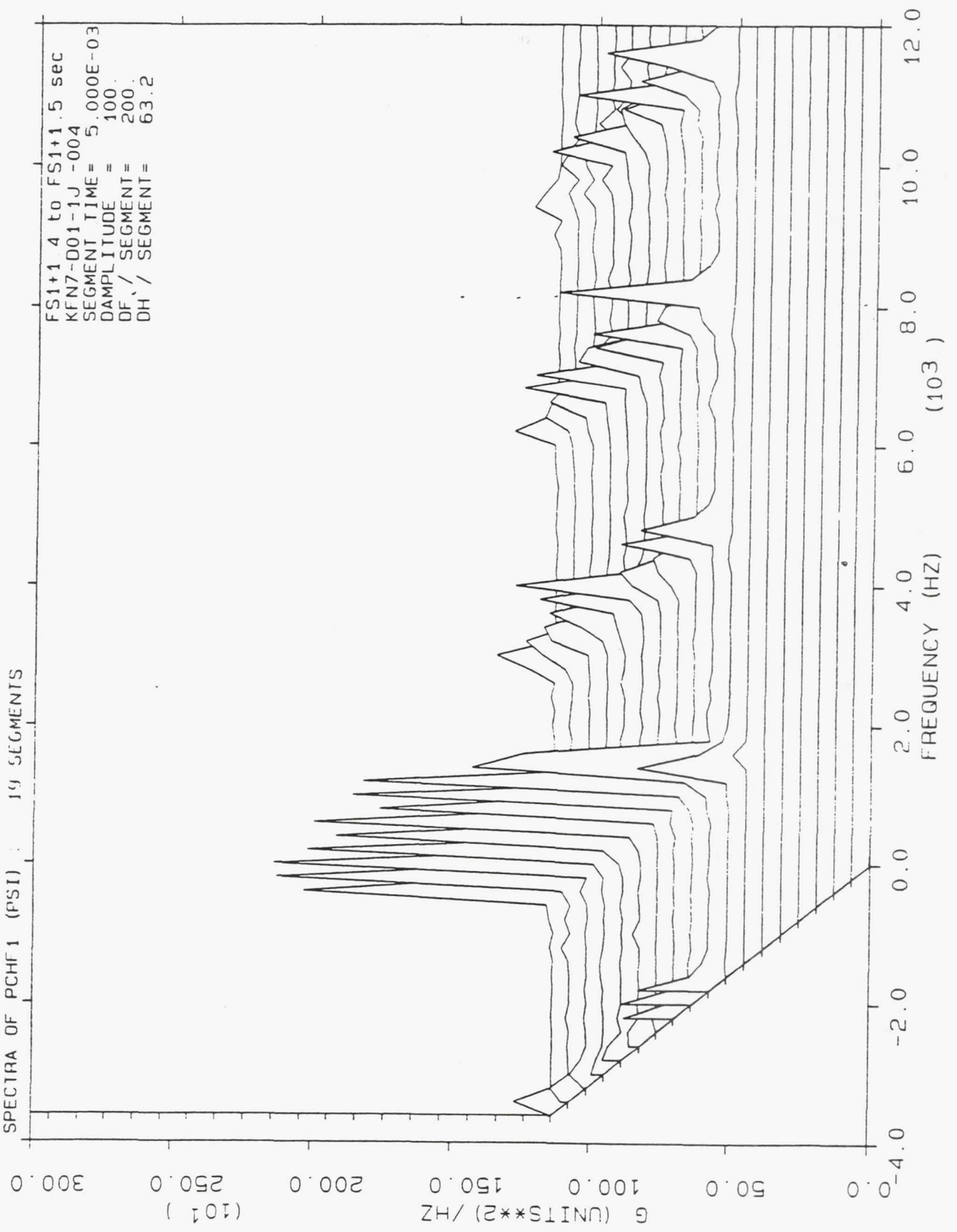
ROCCIO Test Program

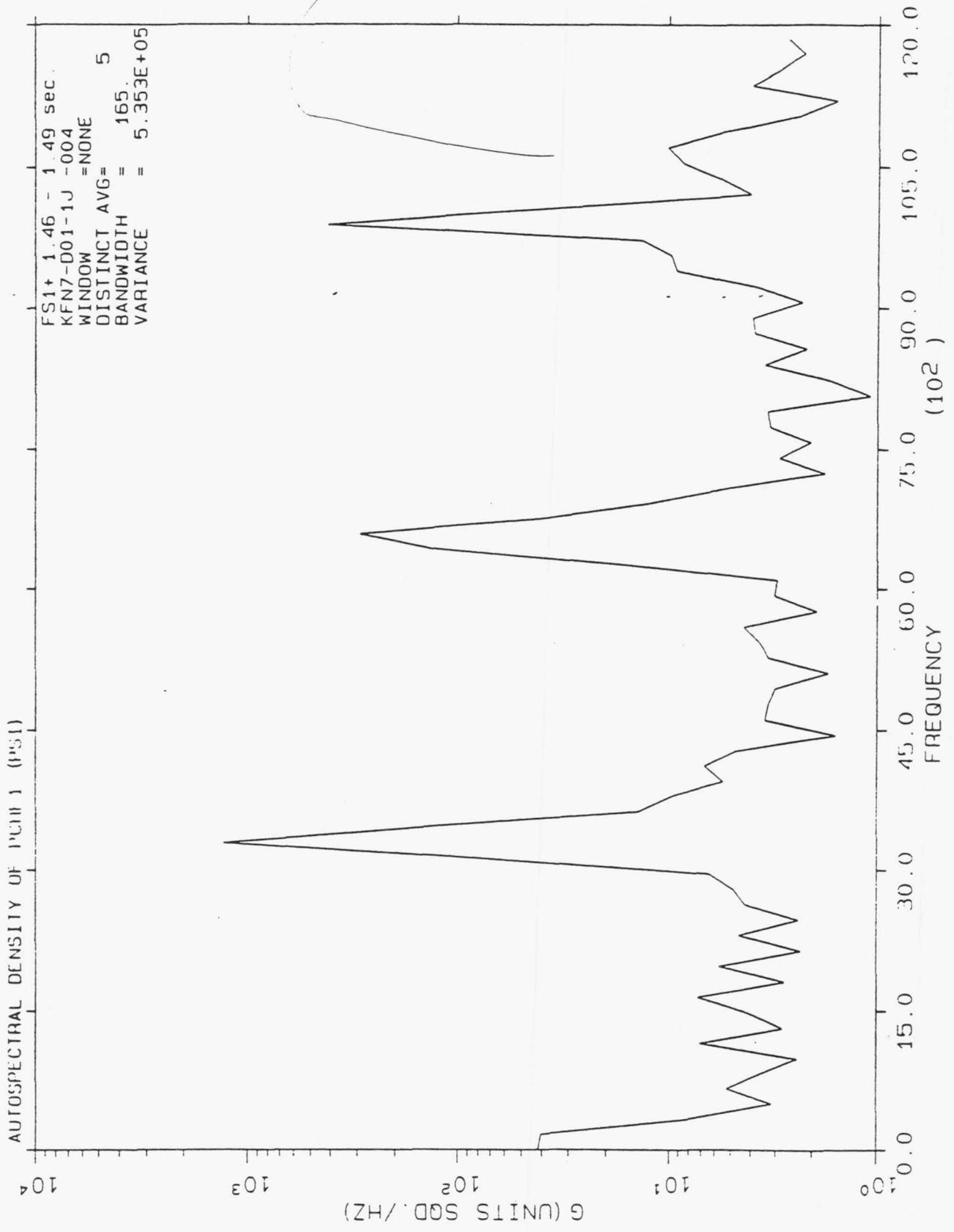
Time zero = FS1+1 4 sec
KFN7-D01-1J -004



SPECTRA OF PCHF1 (PSI) : 19 SEGMENTS

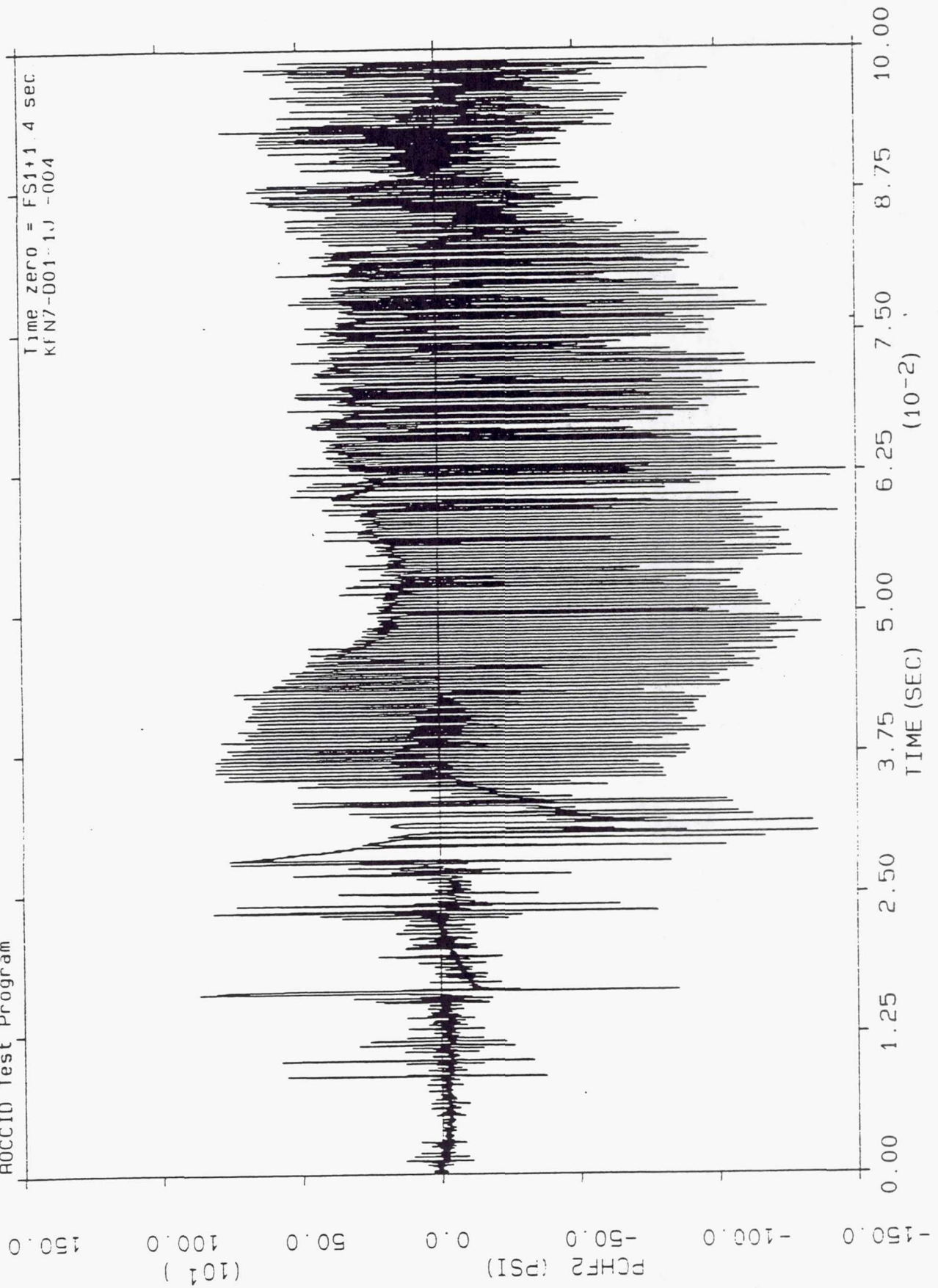
FS1+1 4 to FS1+1 5 sec
KFN7-001-1J -004
SEGMENT TIME= 5.000E-03
AMPLITUDE = 100
DF / SEGMENT= 200
DH / SEGMENT= 63.2

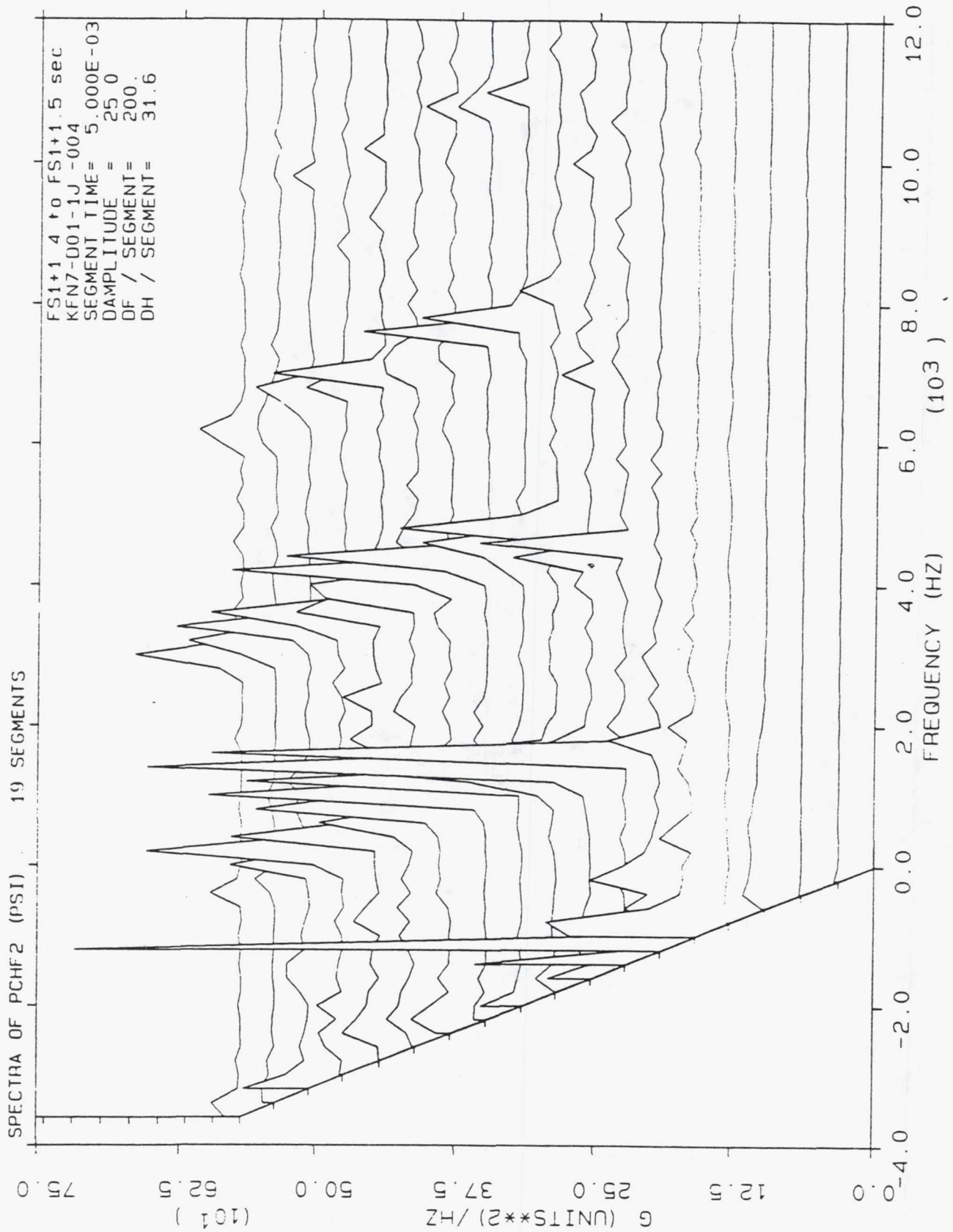


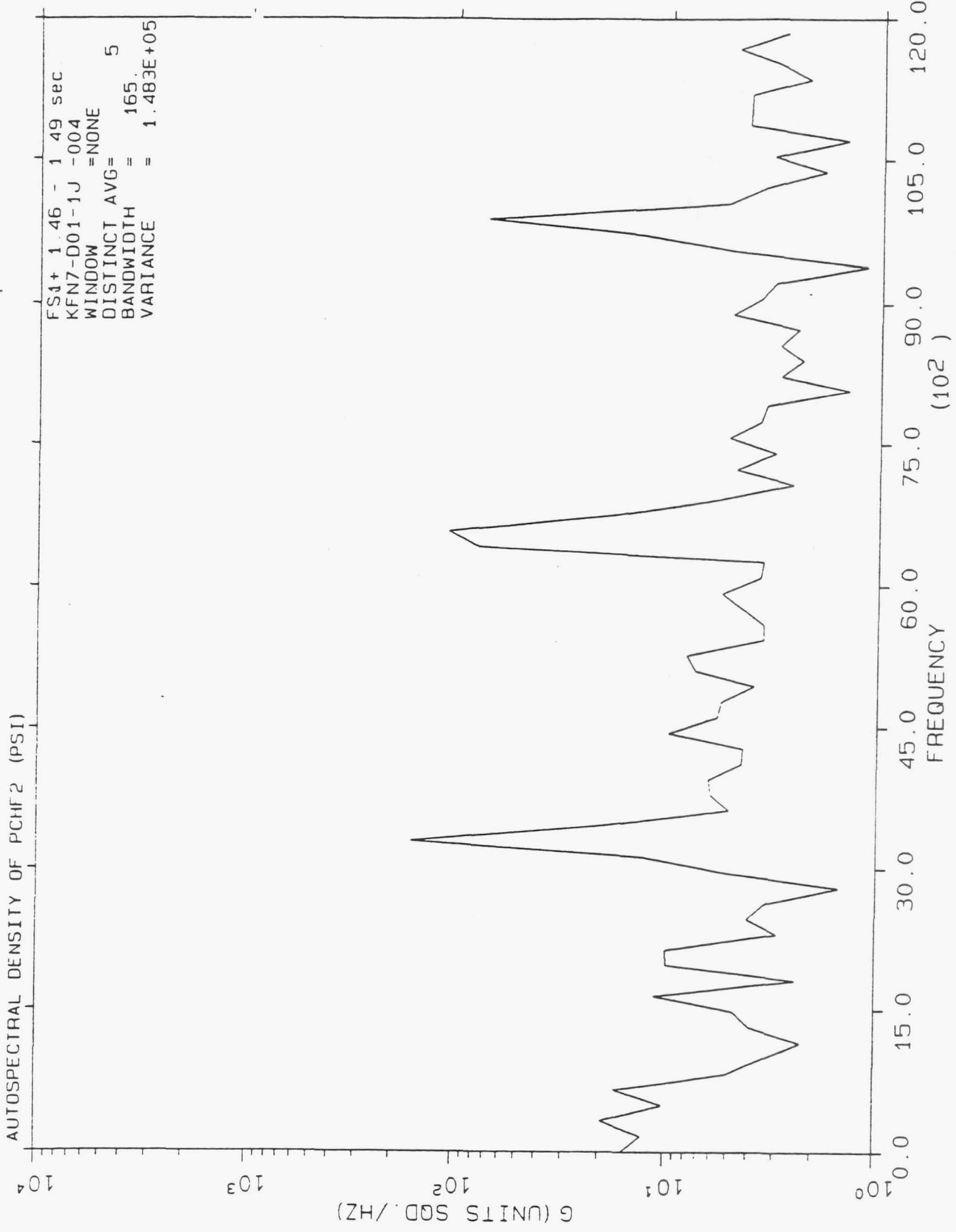


ROCCID Test Program

Time zero = FS1+1.4 sec
KFN7-D01-1J -004

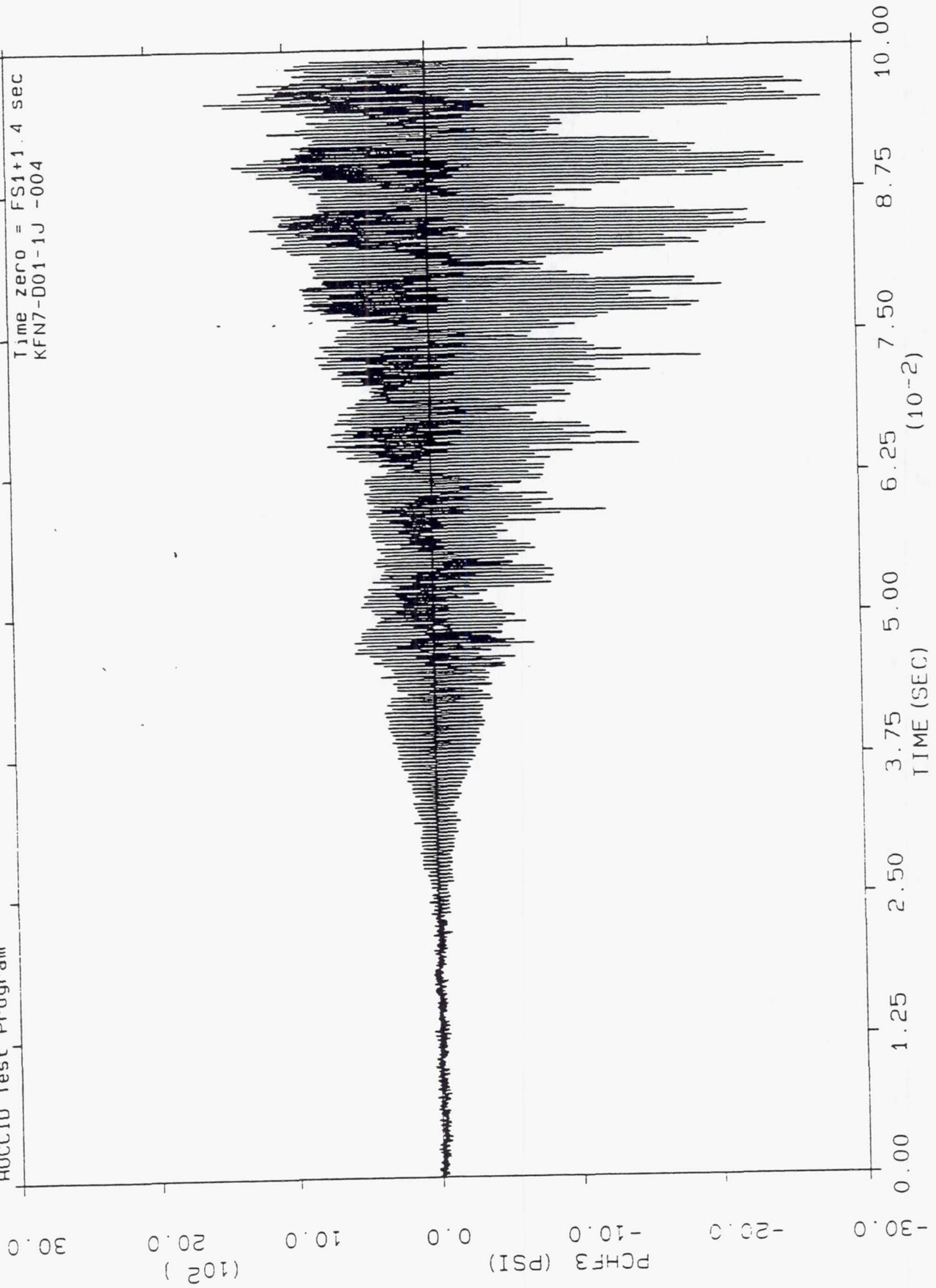




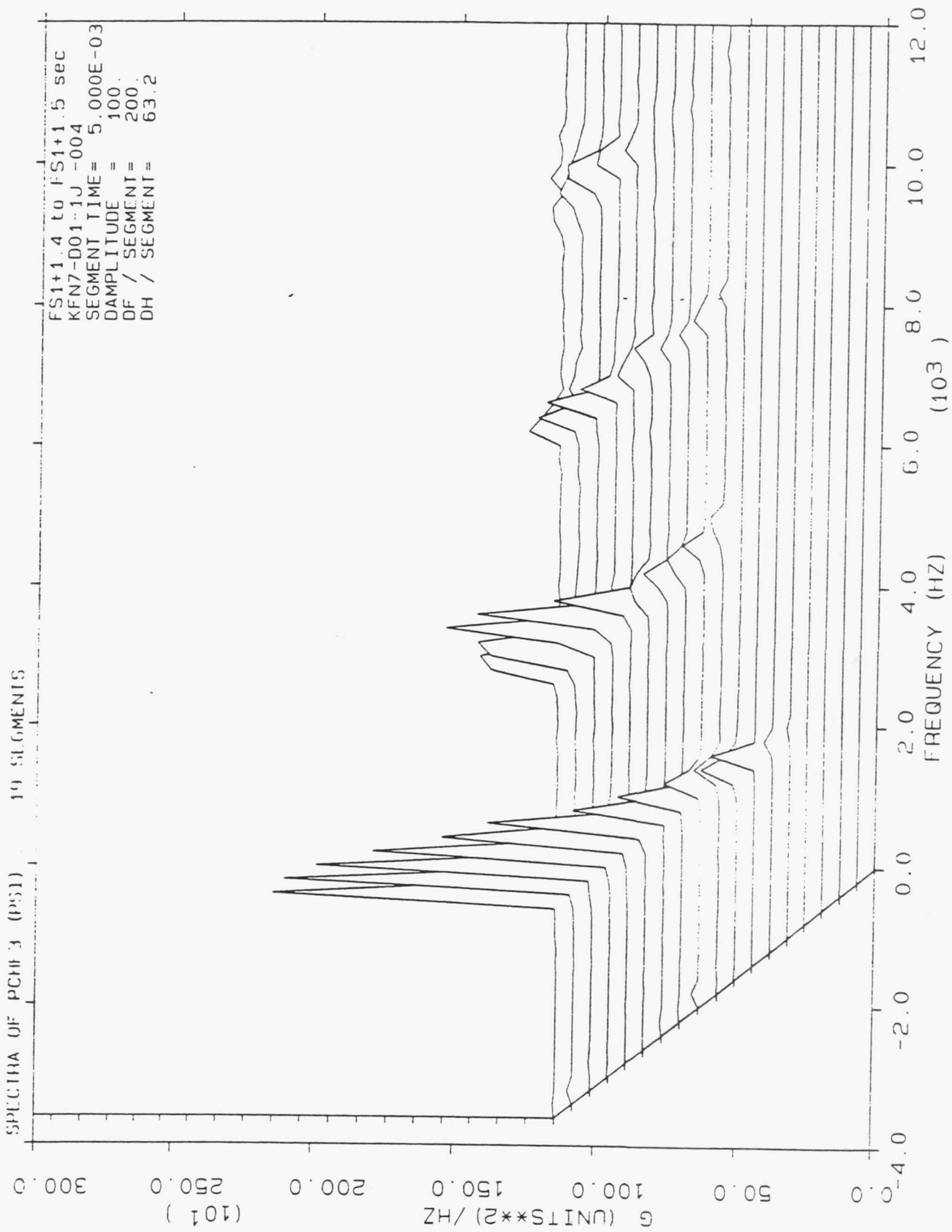


ROCCIO Test Program

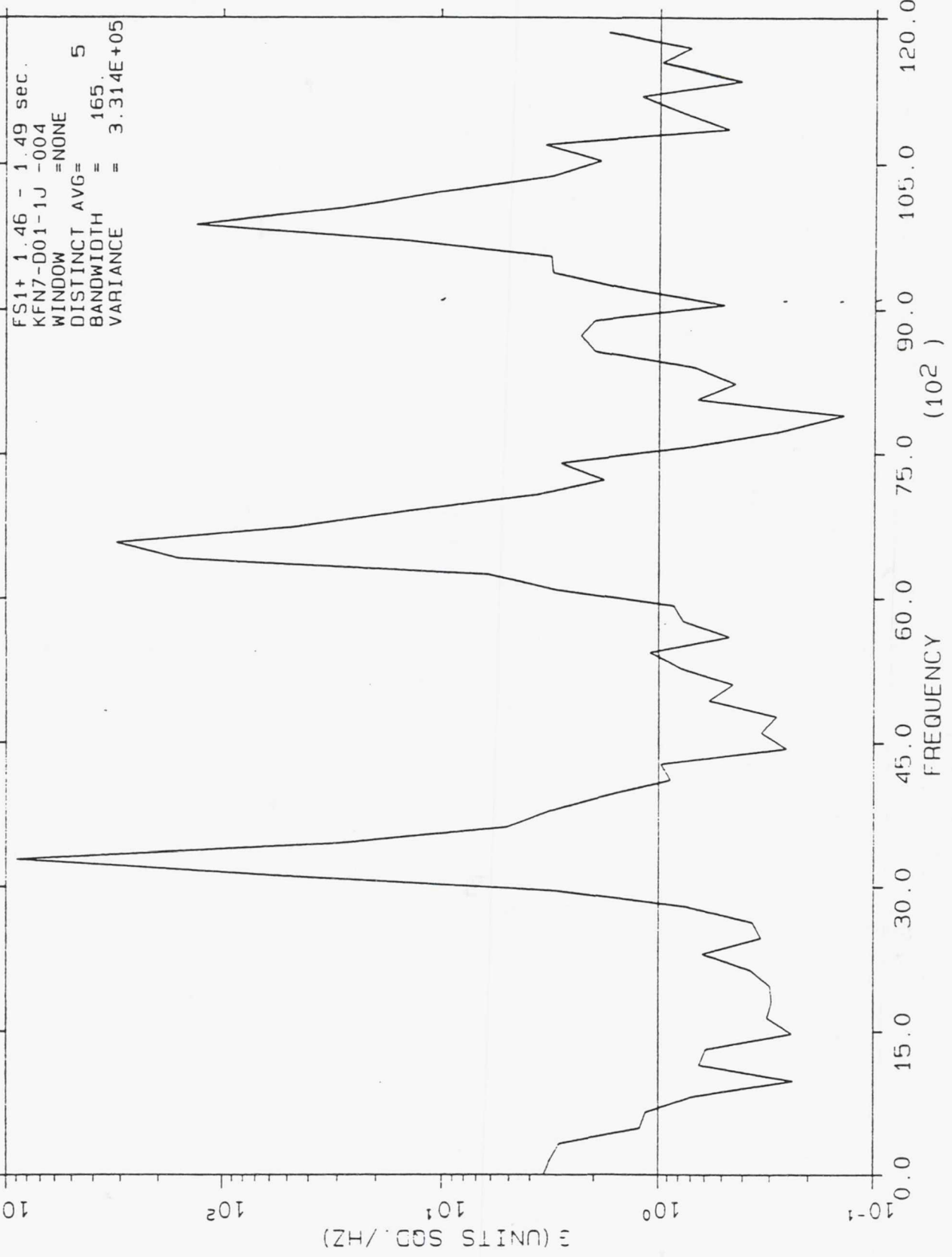
Time zero = FS1+1.4 sec
KFN7-D01-1J -004



SPECTRA OF PCH 3 (PSI) 10 SEGMENTS

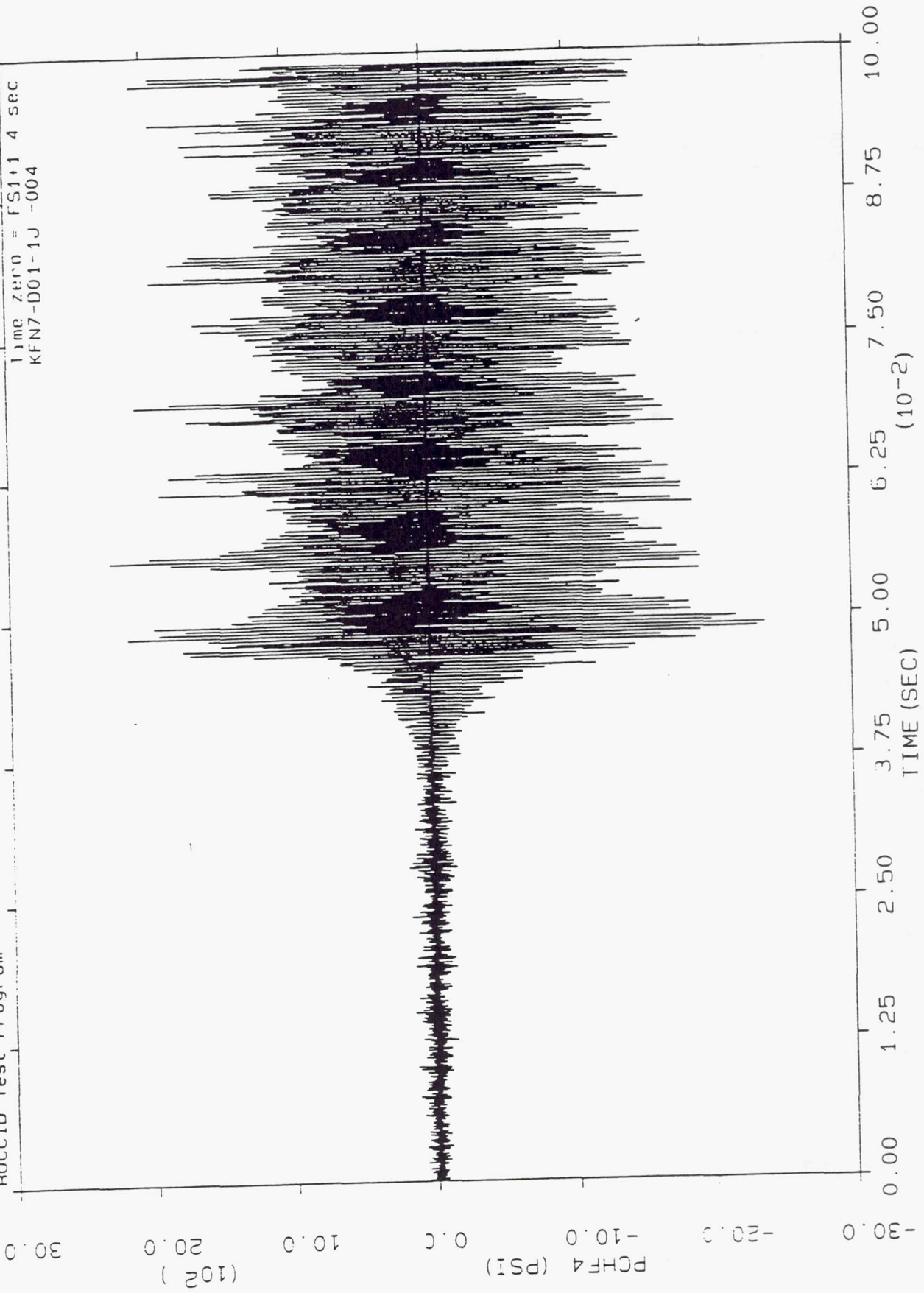


AUTOSPECTRAL DENSITY OF PCHIF3 (PSI)



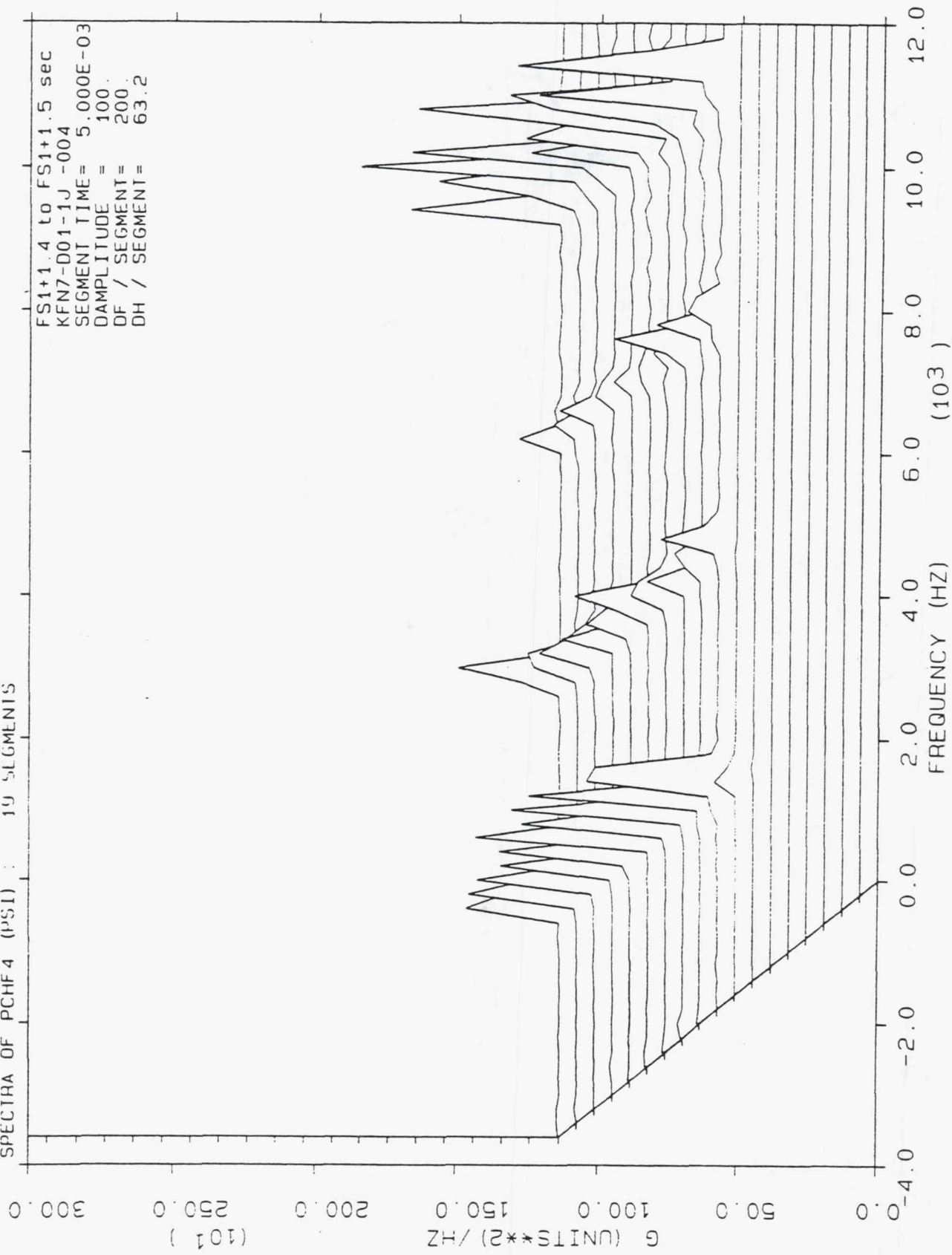
ROCCID Test Program

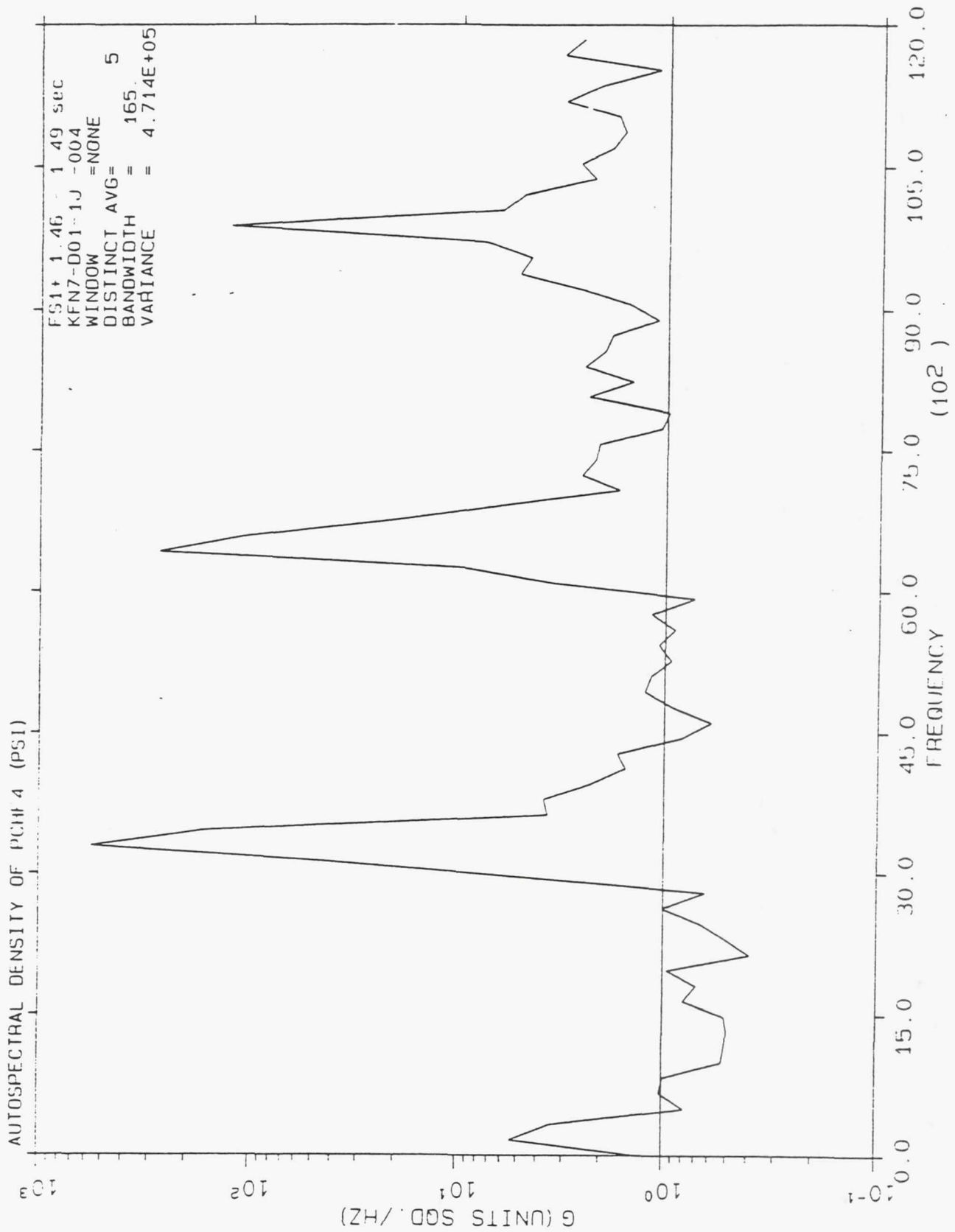
Time zero = FS111 4 sec
KFN7-D01-1J -004



SPECTRA OF PCHF4 (PSI) : 19 SEGMENTS

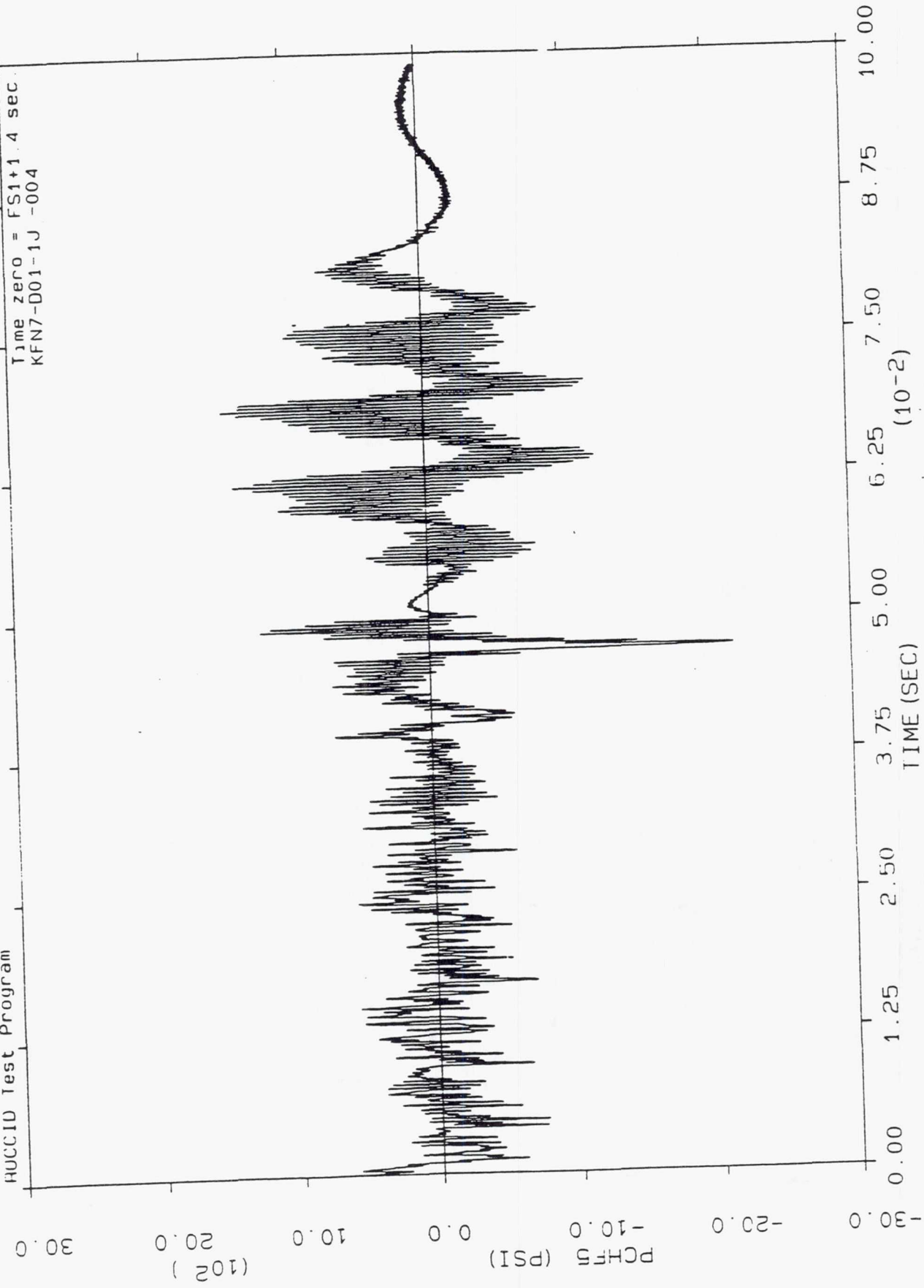
FS1+1.4 to FS1+1.5 sec
KFN7-001-1J -004
SEGMENT TIME= 5.000E-03
DAMPLITUDE = 100.
DF / SEGMENT= 200.
DH / SEGMENT= 63.2





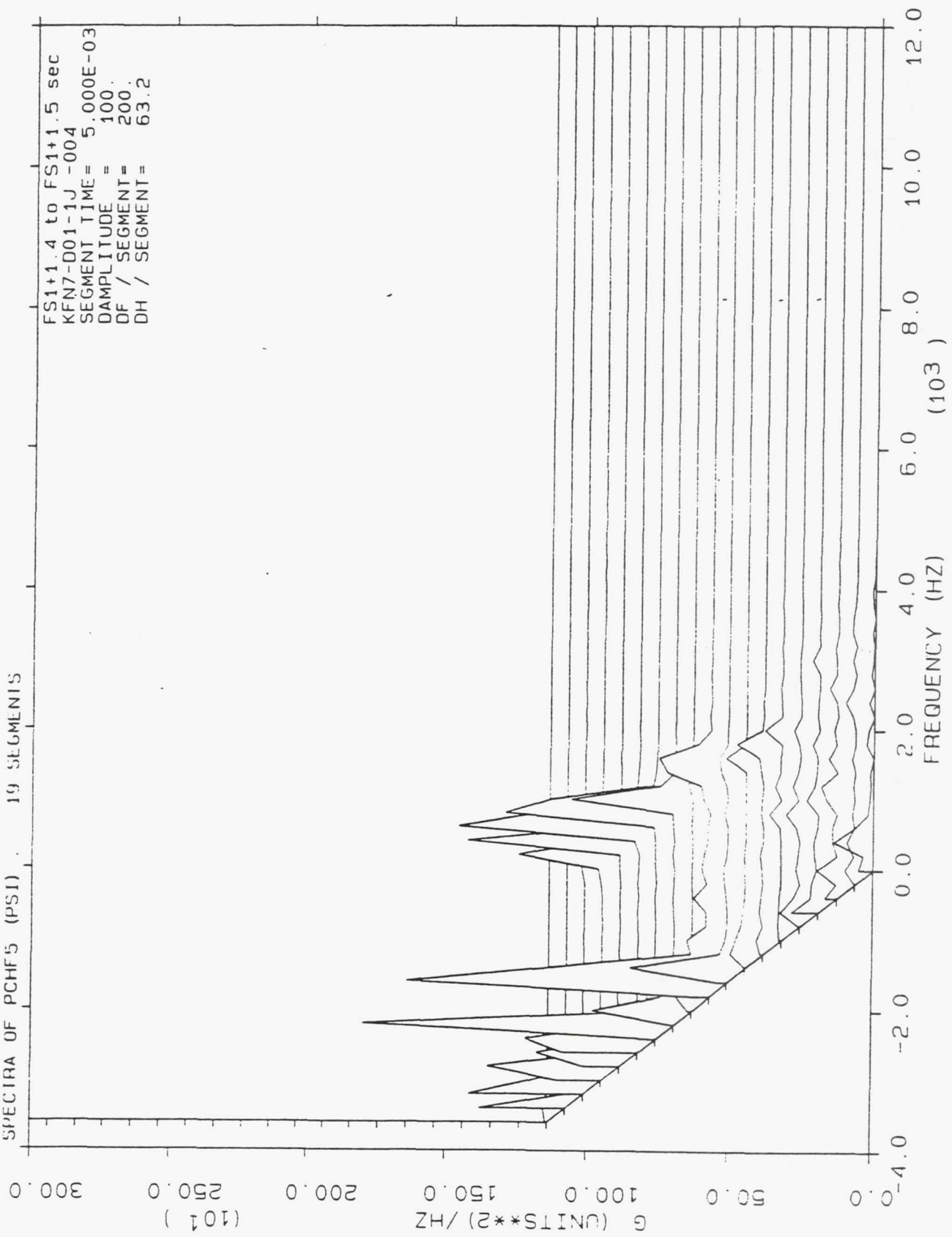
HUCCID Test Program

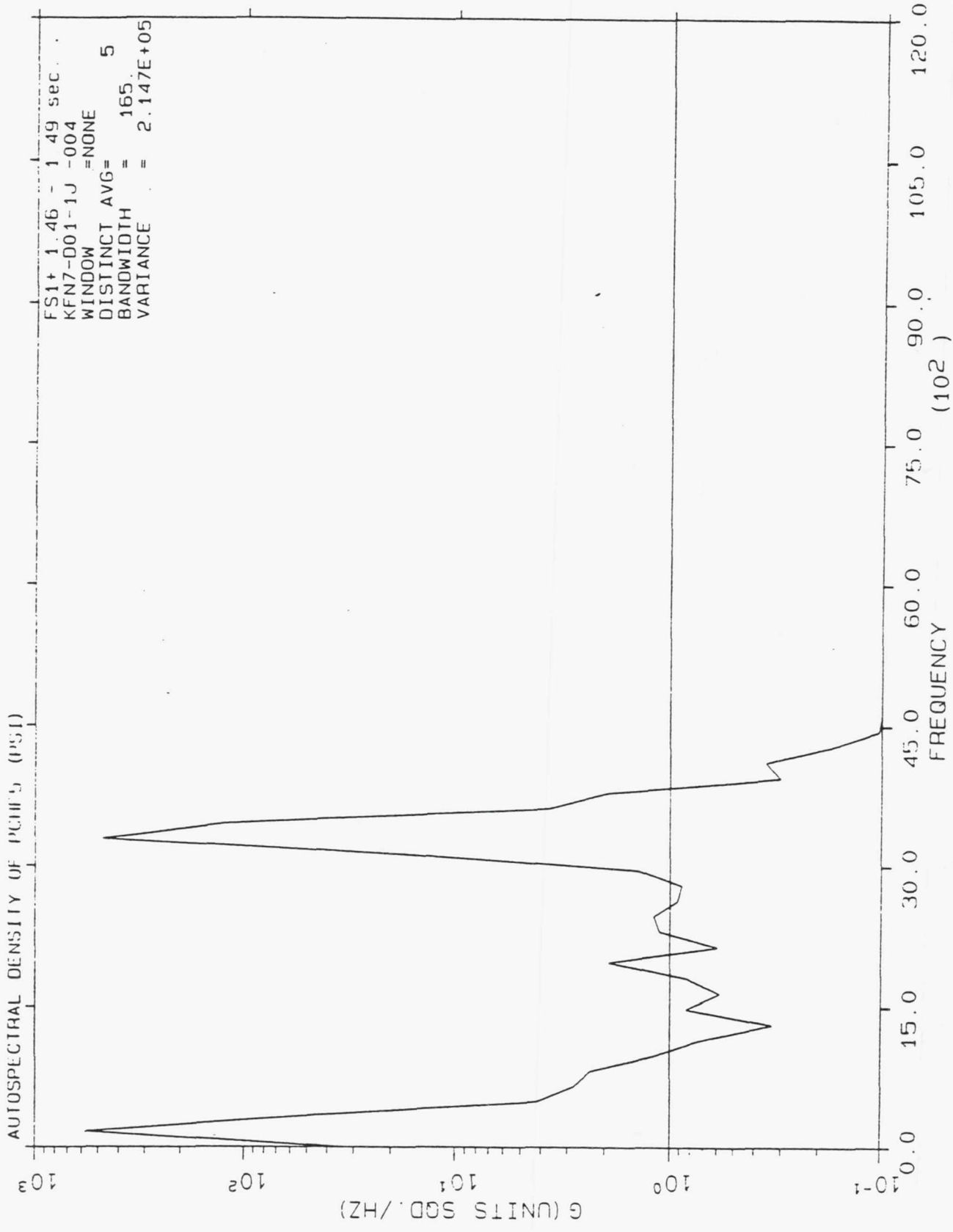
Time zero = FS1+1.4 sec
KFN7-D01-1J -004



SPECTRA OF PCHF5 (PSI) . 19 SEGMENTS

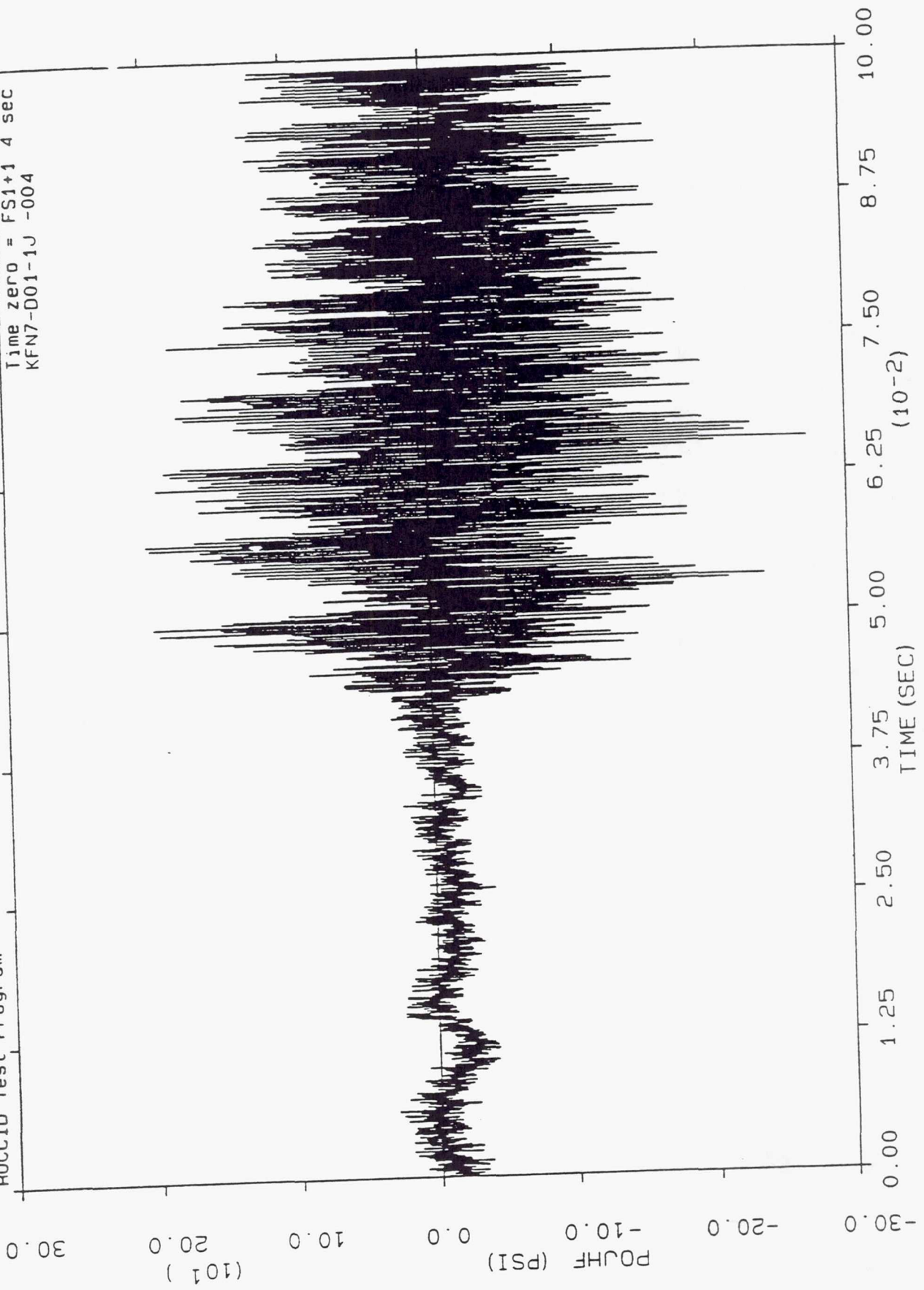
FS1+1.4 to FS1+1.5 sec
KFN7-001-1J -004
SEGMENT TIME= 5.000E-03
DAMPLITUDE = 100.
DF / SEGMENT= 200.
DH / SEGMENT= 63.2



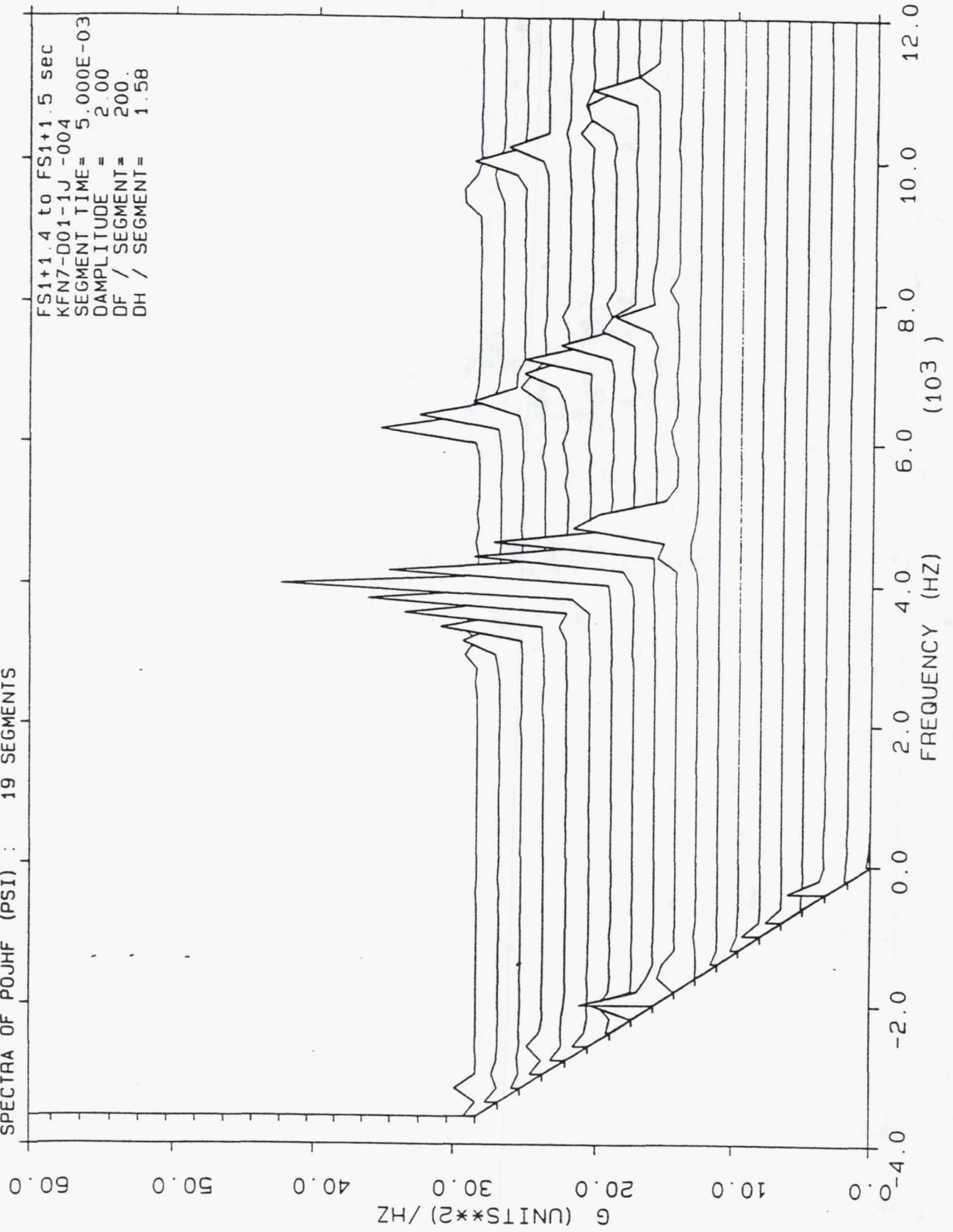


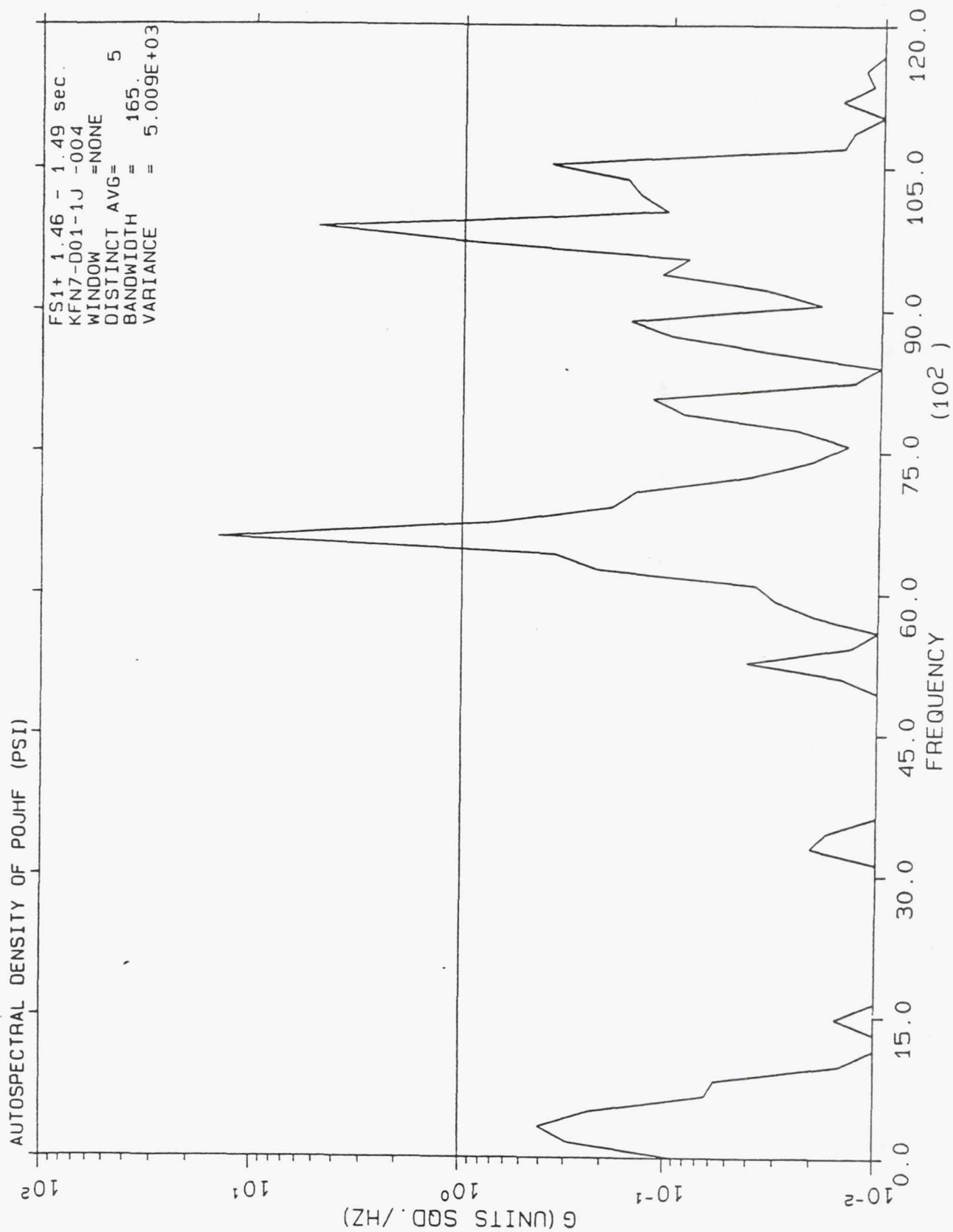
ROCCID Test Program

Time zero = FS1+1 4 sec
KFN7-D01-1J -004



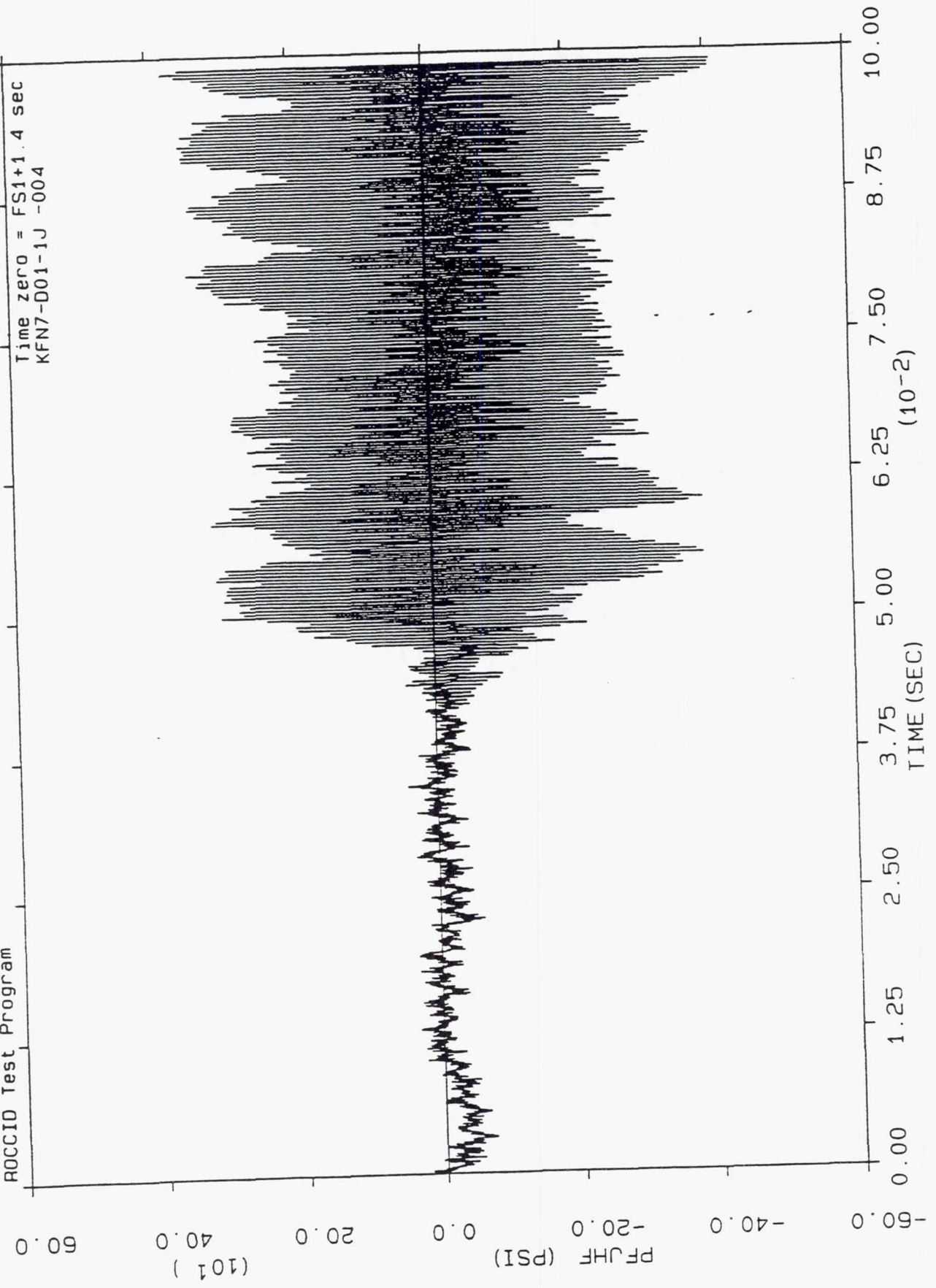
SPECTRA OF POJHF (PSI) : 19 SEGMENTS





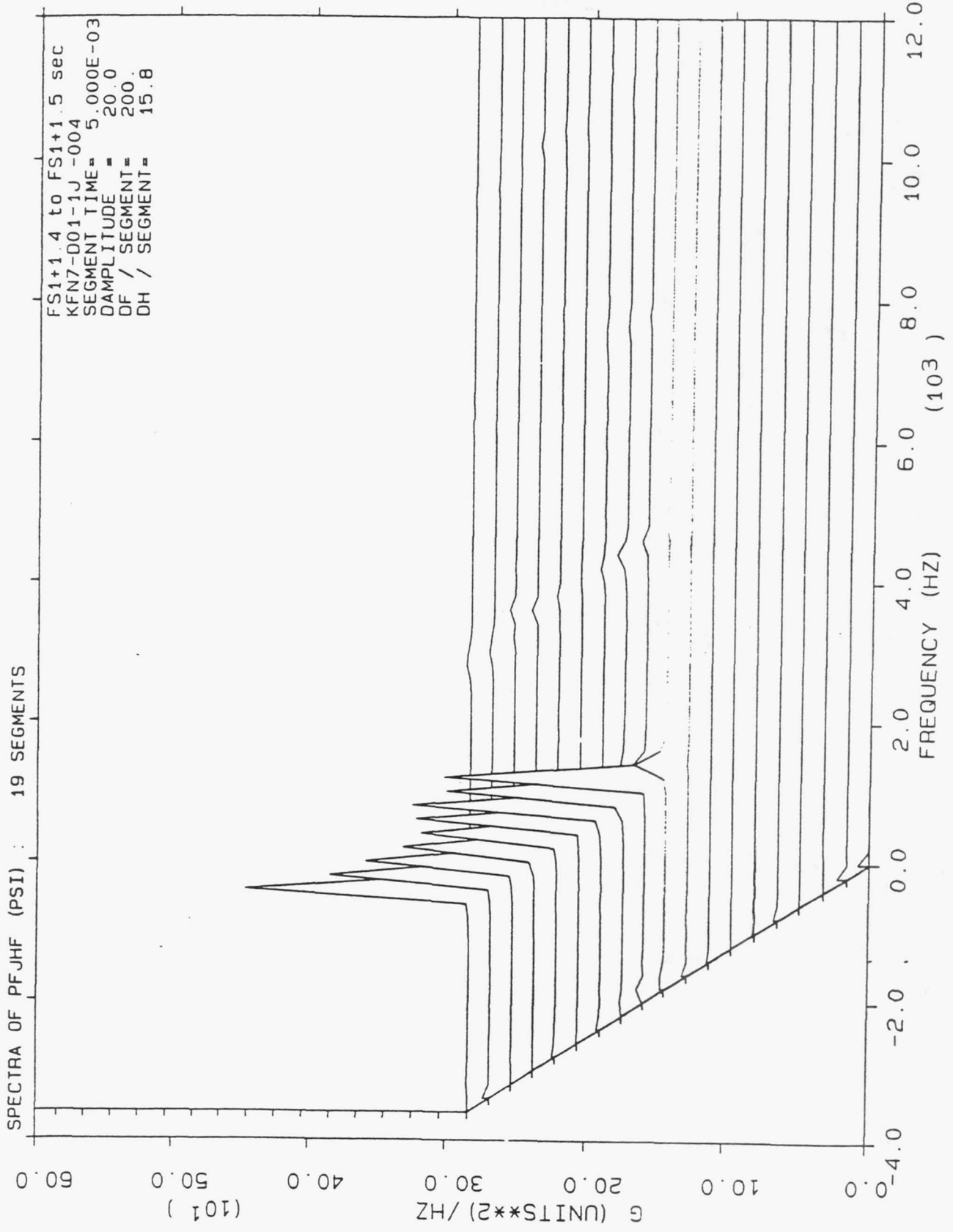
ROCCID Test Program

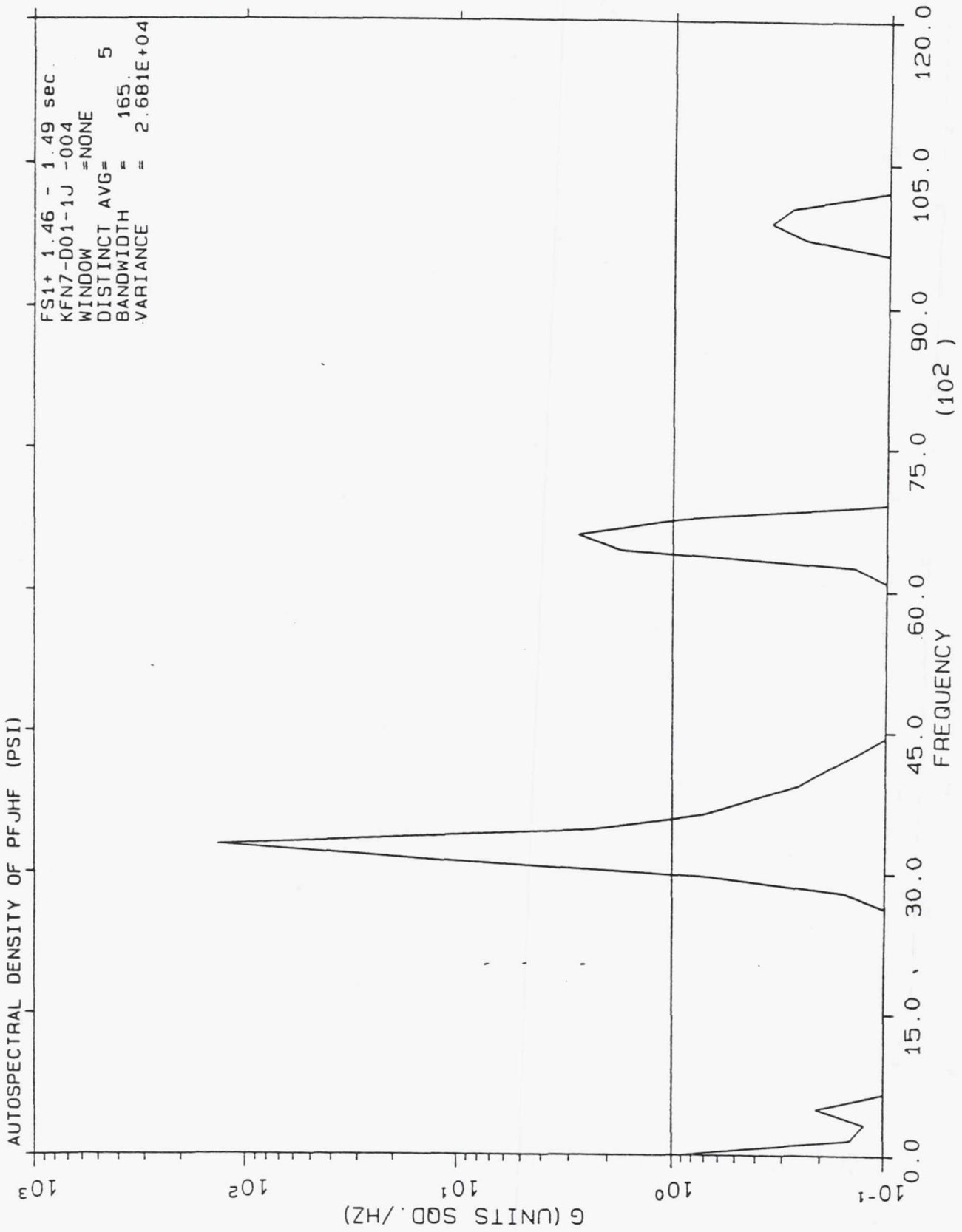
Time zero = FS1+1.4 sec
KFN7-D01-1J -004



SPECTRA OF PFJHF (PSI) : 19 SEGMENTS

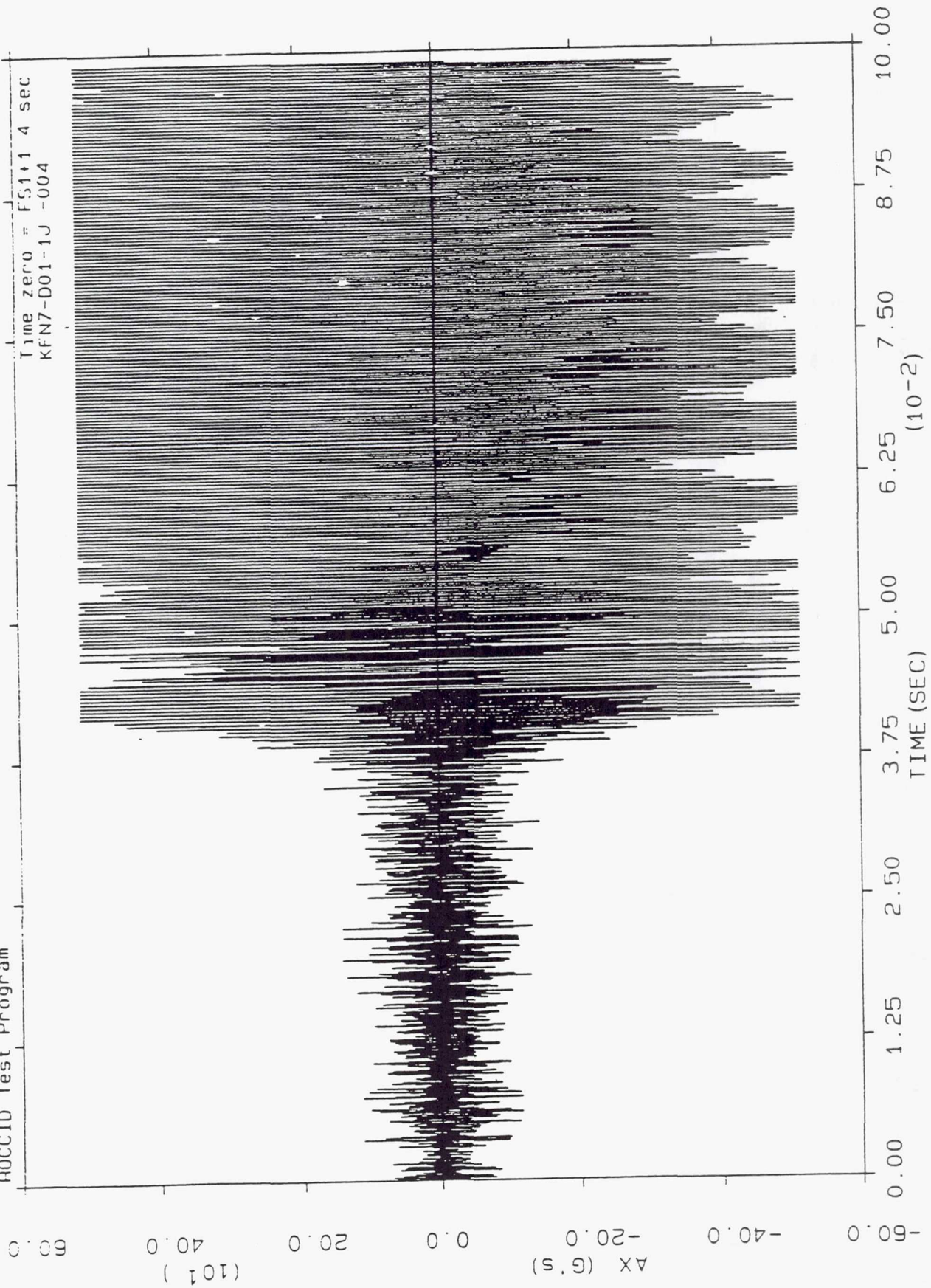
FS1+1.4 to FS1+1.5 sec
KFN7-D01-1J -004
SEGMENT TIME = 5.000E-03
DAMPLITUDE = 20.0
DF / SEGMENT = 200.
DH / SEGMENT = 15.8



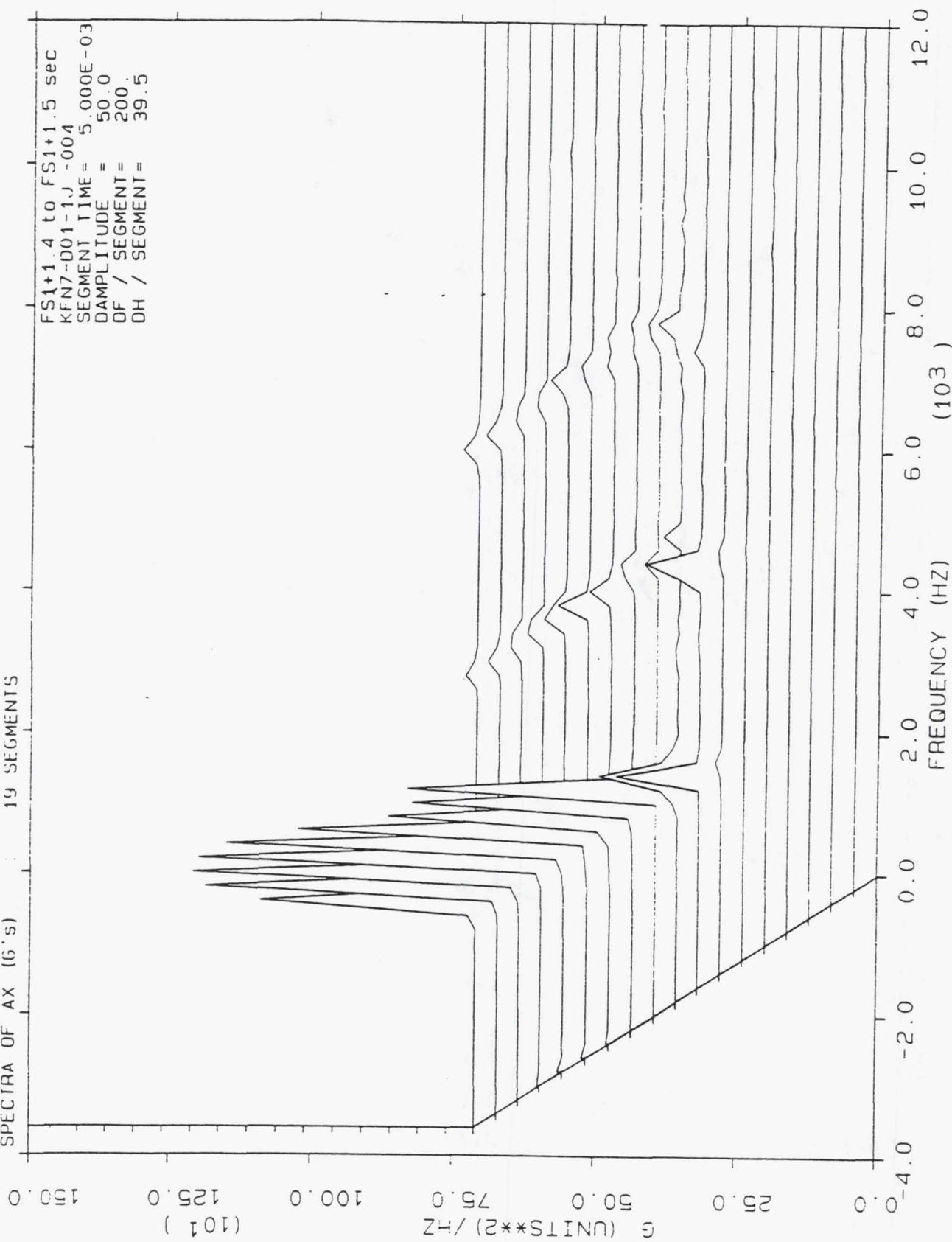


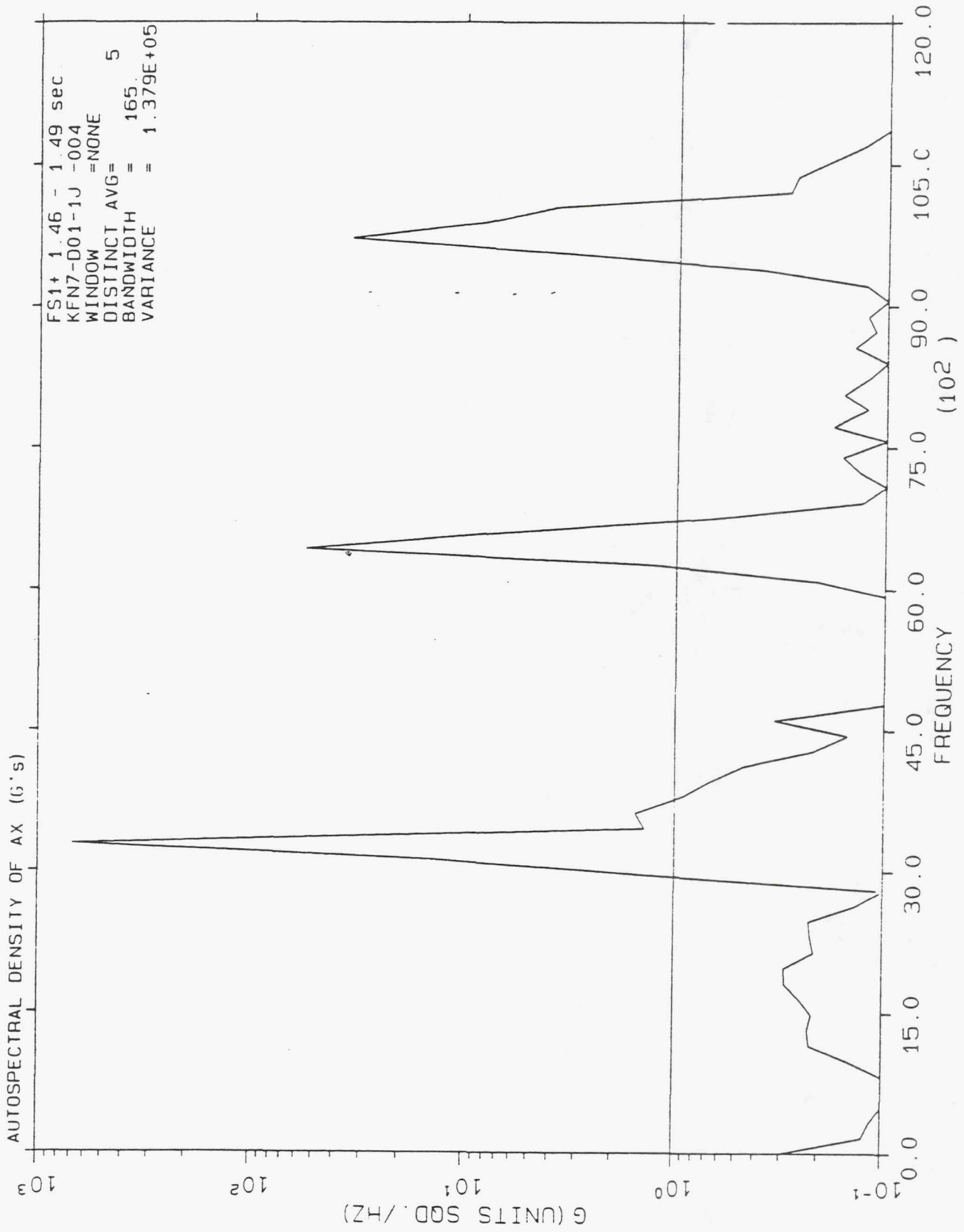
ROCCIO Test Program

Time zero = F51+1 4 sec
KFN7-D01-1J -004



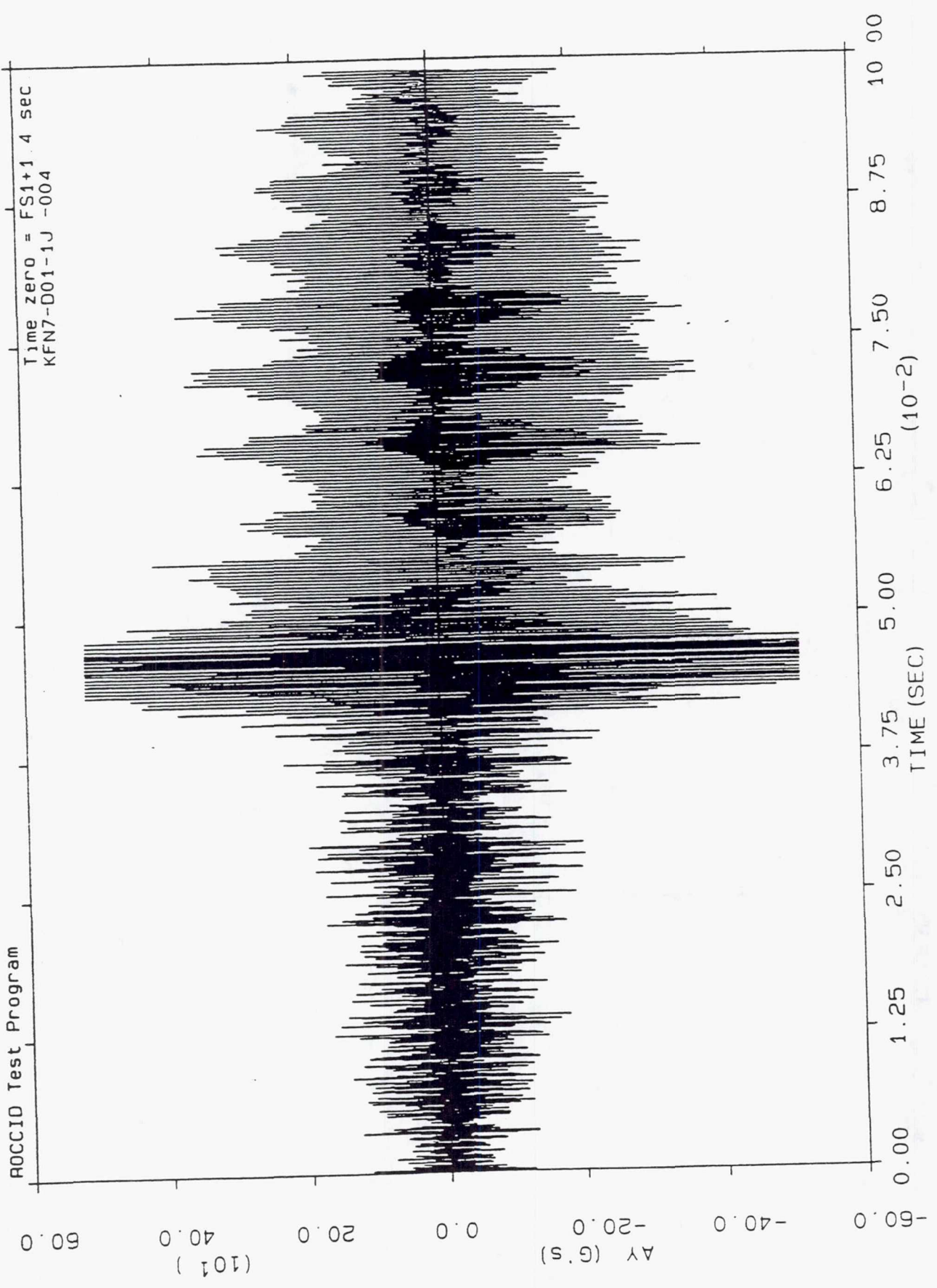
SPECTRA OF AX (G's) : 19 SEGMENTS



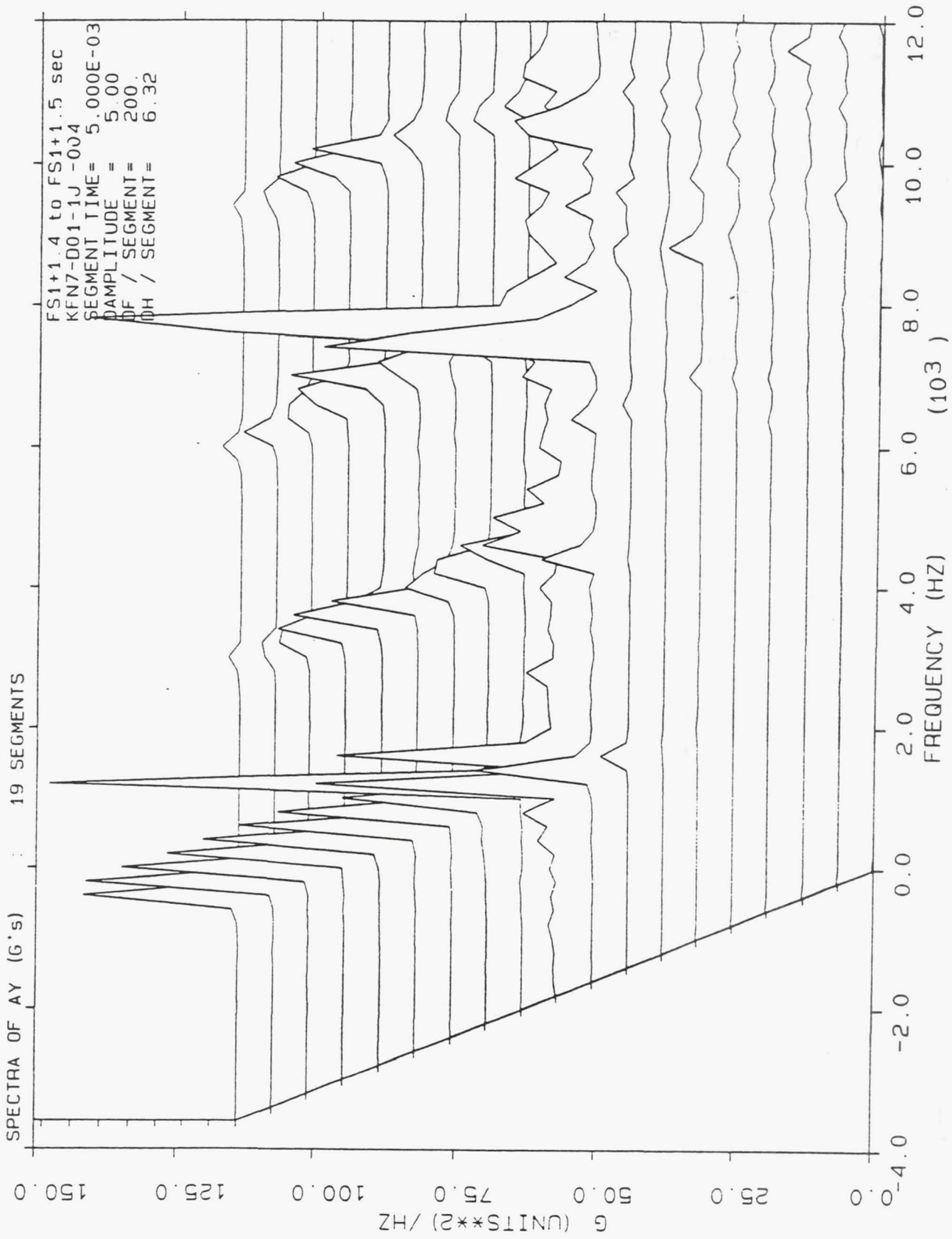


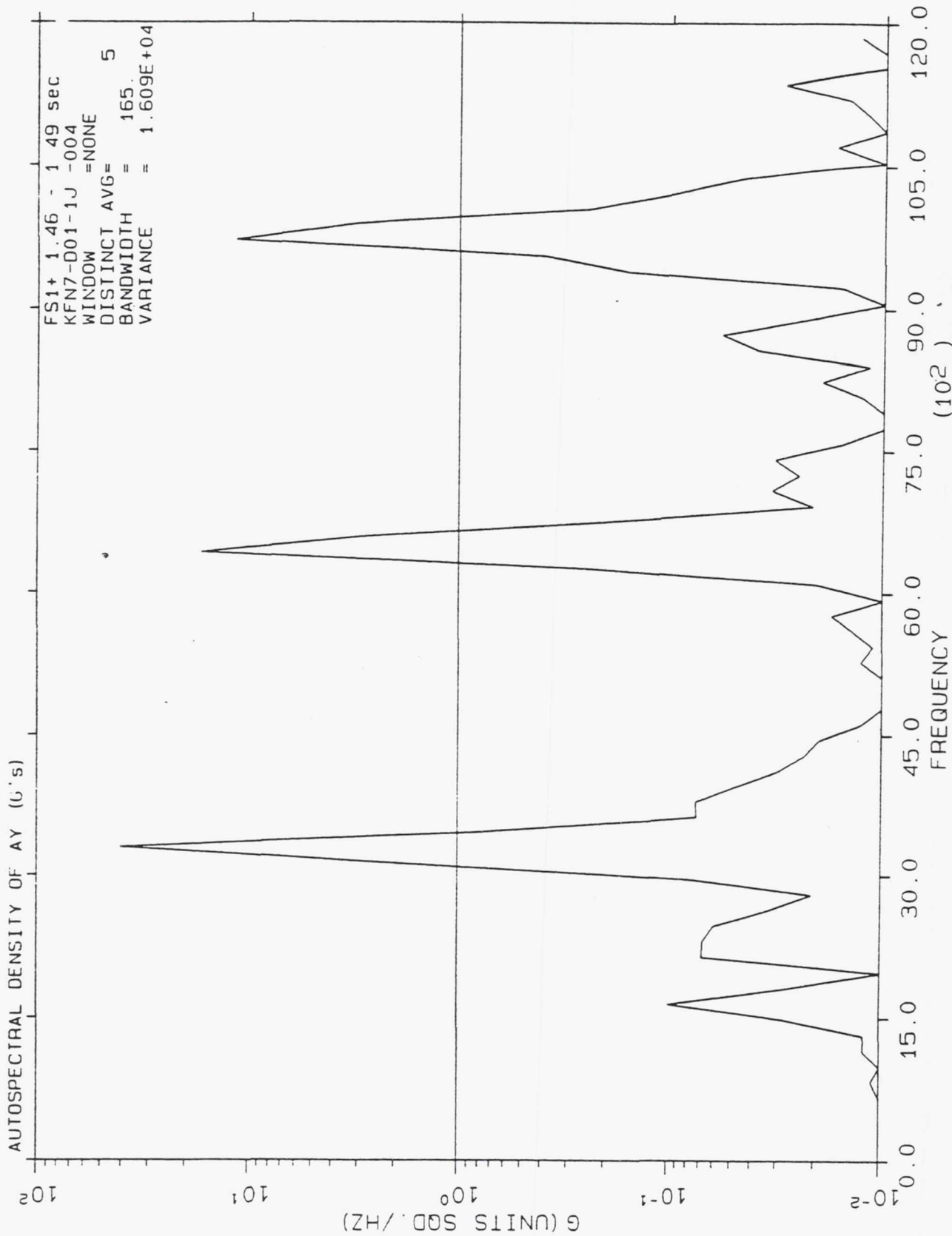
ROCCIO Test Program

Time zero = FS1+1.4 sec
KFN7-D01-1J -004



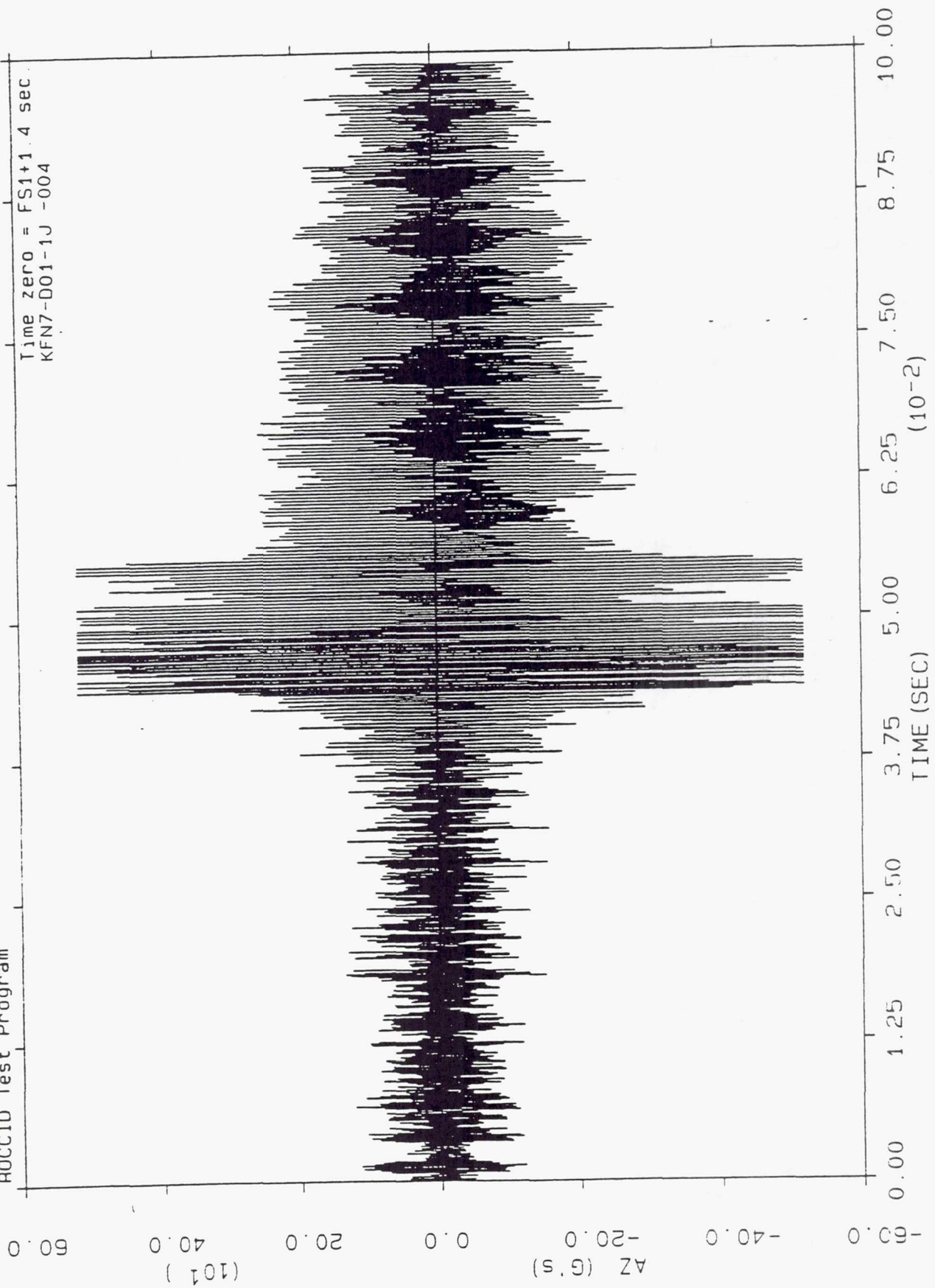
SPECTRA OF AY (G*s) : 19 SEGMENTS



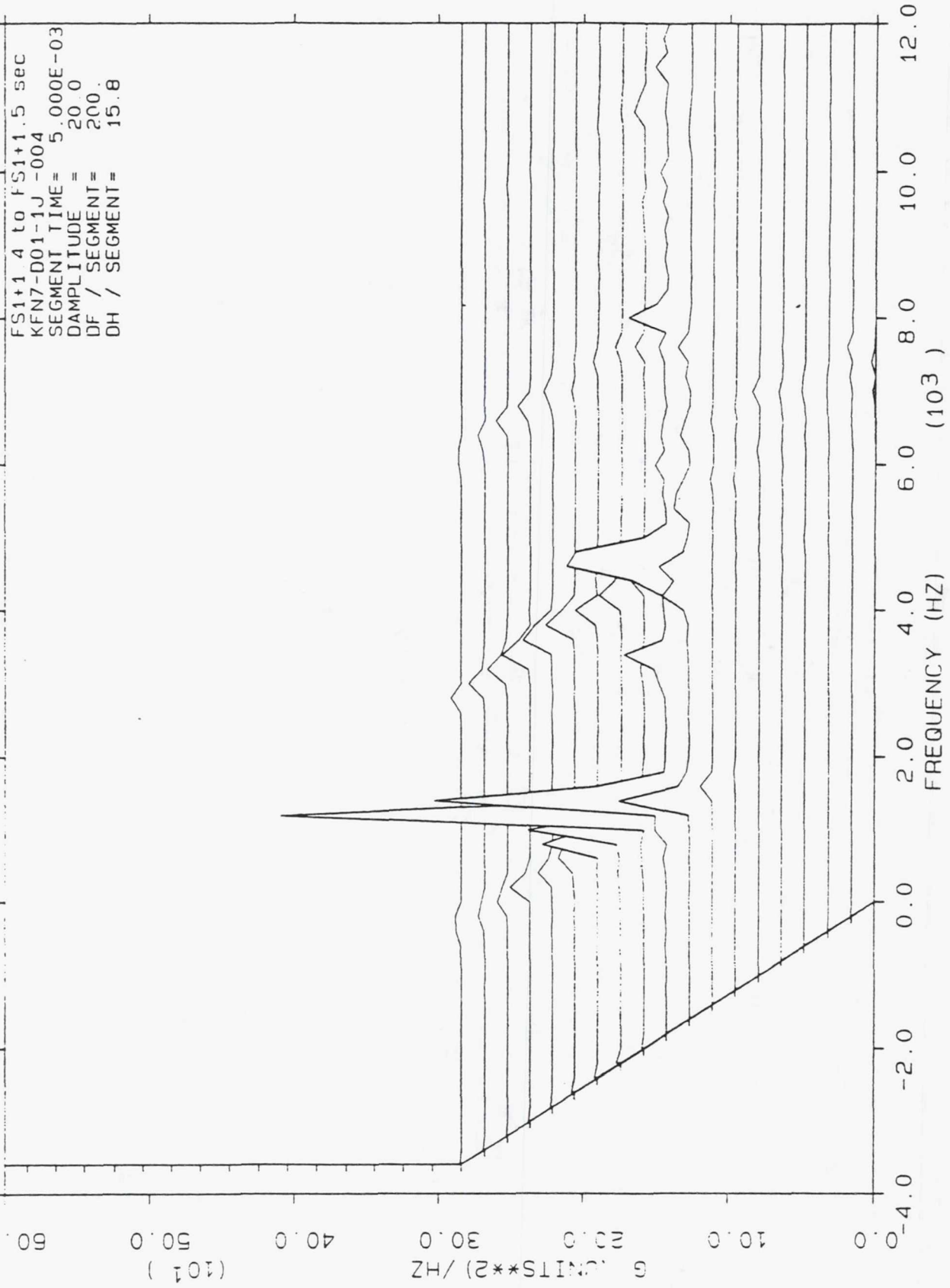


ROCCID Test Program

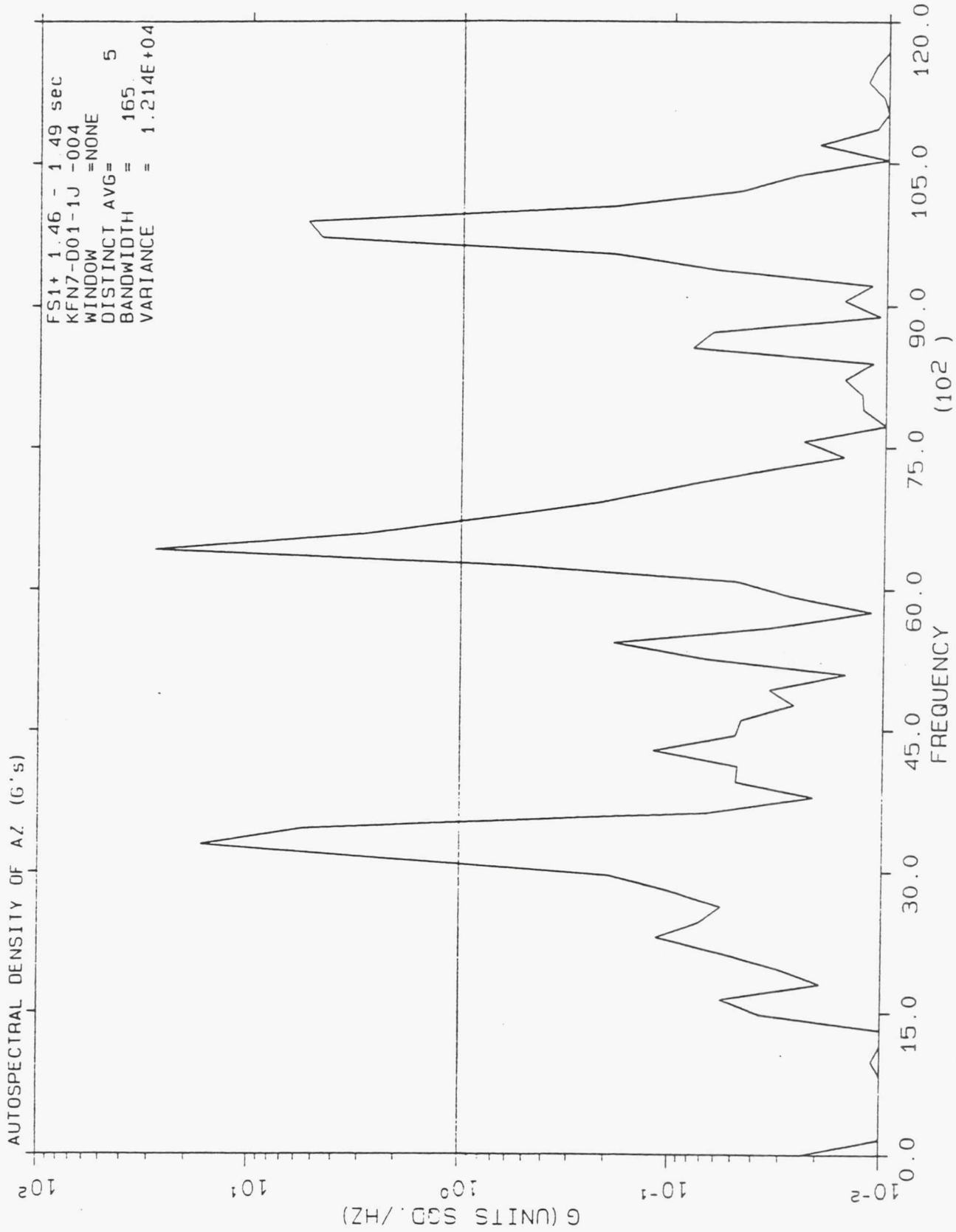
Time zero = FS1+1.4 sec
KFN7-001-1J -004



SPECTRA OF AZ (G's) : 19 SEGMENTS



FS1+1 4 to FS1+1 5 sec
KFN7-D01-1J -004
SEGMENT TIME= 5.000E-03
DAMPLITUDE = 20.0
DF / SEGMENT= 200.
DH / SEGMENT= 15.8



APPENDIX D

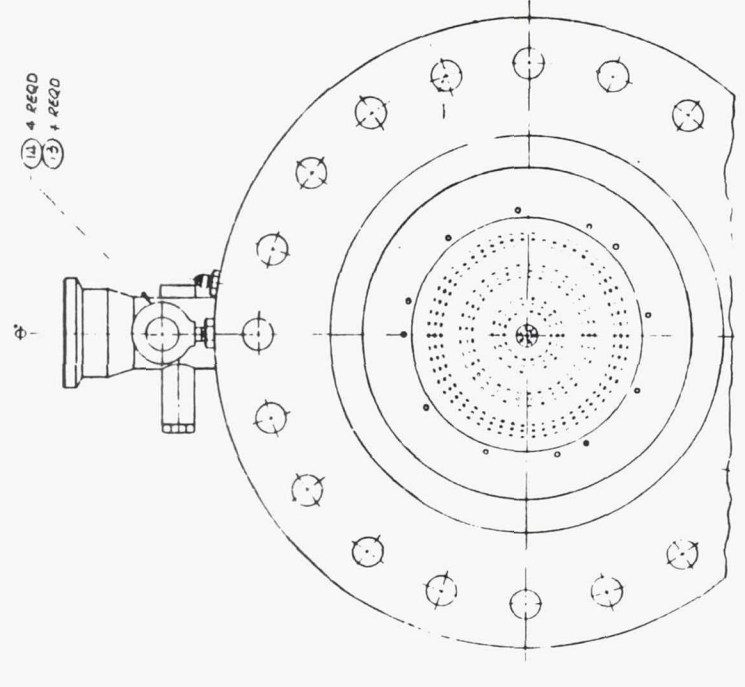
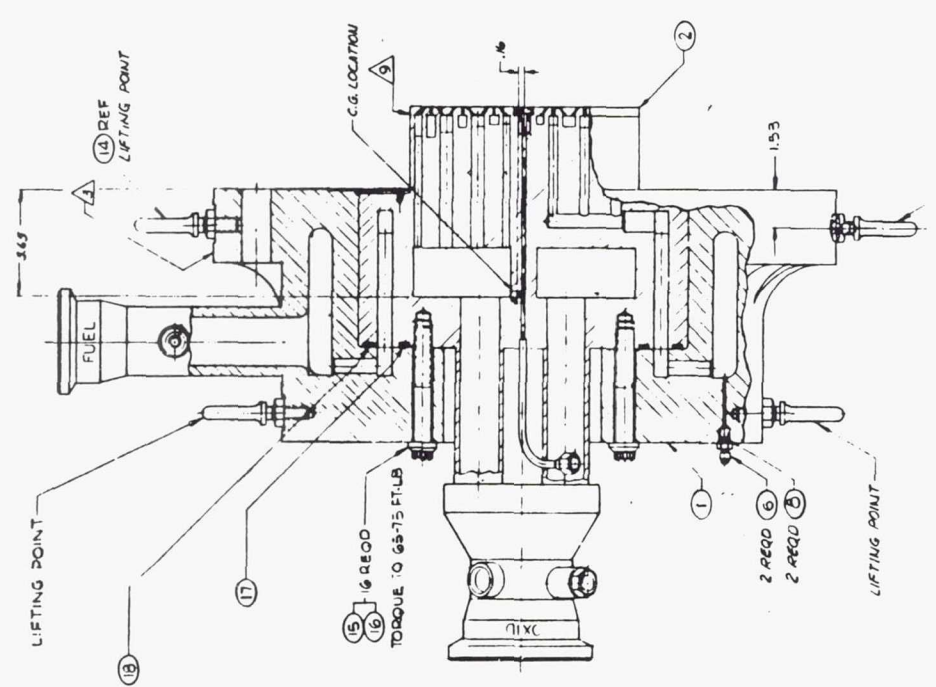
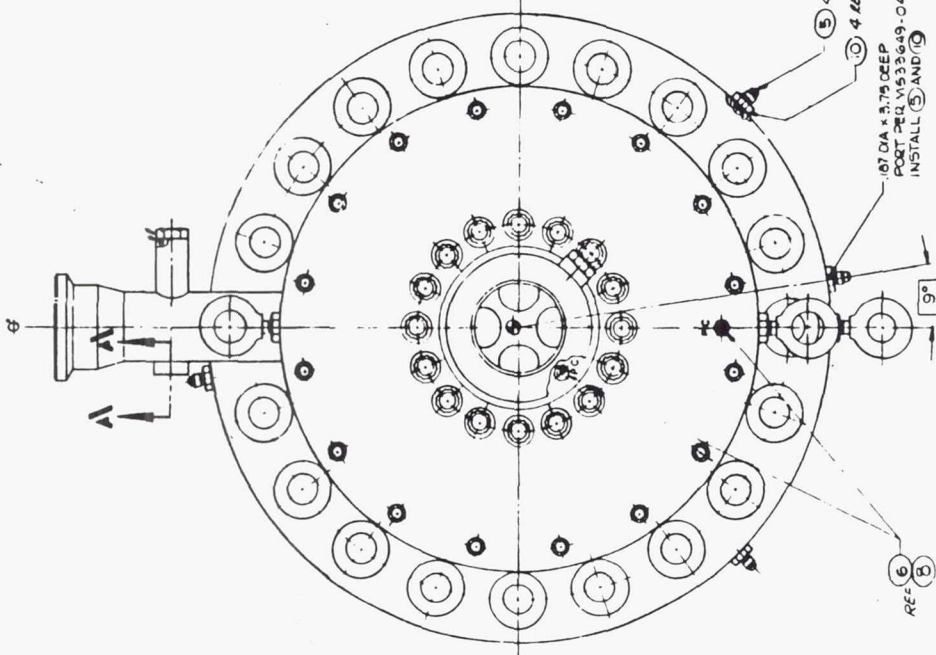
ROCCID VALIDATION HARDWARE
DESIGN DRAWING PACKAGE

LIST OF DRAWINGS

<u>Drawing Description</u>	<u>Drawing No.</u>	<u>No. of Sheets</u>	<u>Figure Nos.</u>
Engine assembly	1206430	2	D-3/D-4
Injector Assembly	1206427	1	D-5
Injector Flange	1200773A	3	D-6/D-8
Injector Core Assembly	1206423	2	D-9/D-10
Injector Core	1200729	7	D-11/D-17
Thrust Chamber Assembly	1206428	3	D-18/D-20
Chamber Body Forging	1206432	1	D-21
Chamber Liner	1206429	1	D-22
Chamber Retaining Plate	1200976A	1 + ADCN	D-23/D-24
Chamber Proof Plate	1200977A	1 + ADCN	D-25/D-26
1/4 Wave Tube Resonator	1206426	1	D-27
Resonator Cavity Blank	1206431	1	D-28
Bomb Adapters	1201080A	1	D-29

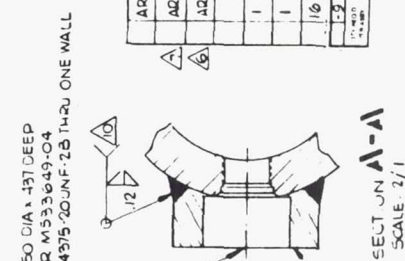
H
G
F
E
D
C
B
A

- NOTES:
1. INTERMEDIATE DRAWING PER ATC-STD-492A.
 2. LOX CIRCUIT CLEANLINESS PER WPFC-SPEC-164; ISA IS 2.75 50 FT., FUEL CIRCUIT PER ATC-STD-494G, LEVEL 1000. CODE 15A IS 3.0 50 FT. AND FLAME 15A IS 3.2 50 FT.
 3. MAKE PER 1206427 WITH 1206427, APPLICABLE PART NUMBER AND AERJET TECHNOLOGIES ASSIGNED SERIAL NUMBER.
 4. ASSEMBLED WEIGHT IS 600 LB.
 5. PROTECTIVE CLOSURES REQUIRED.
 6. APPLY ITEM 25 TO ALL THREADS PRIOR TO INSTALLATION.
 7. APPLY ITEM 27 TO ALL O-RINGS PRIOR TO INSTALLATION.
 8. STORAGE AND USE CONTROL PER ATC-STD-491 AND ATC-STD-492.



- TEST ASSEMBLY IN THE FOLLOWING ORDER:
1. ULTRASONIC INSPECT BRAZE JOINT PER ATC-STD-491, TYP 1. ACCEPTANCE PER COMBUSTION DESIGN ACTIVITY.
 2. PROOF TEST BRAZE JOINT BY FLOW & CLEAN WATER (PER ATC-STD-494G, LEVEL 1000) SIMULTANEOUSLY WITH THE OXIDIZER AND FUEL CIRCUITS TO ATMOSPHERE. HOLD FOR APPROXIMATELY FIVE MINUTES.
 - FLOW RATE: 750 ± 10 PSI; APPROX FLOW = 175 LB/SEC
 - EXCELLENCE: 710 ± 10 PSI; APPROX FLOW = 85 LB/SEC
 3. REPEAT ULTRASONIC INSPECT OF BRAZE JOINT PER ATC-STD-491, TYP 1. NOTE ANY DIFFERENCES. ACCEPTANCE PER COMBUSTION DESIGN ACTIVITY.
 4. LEAK TEST ASSEMBLY PER ATC-490G, METHOD 1E, USING CLEAN DRY NITROGEN AT 20 ± 5 PSIA. HOLD FOR 5 MINUTES MINIMUM. NO LEAKAGE ALLOWED.
 5. FLOW TEST WITH CLEAN WATER (ATC-STD-494G, LEVEL 1000) AS FOLLOWS:
 1. PERFORM VISUAL PATTERN CHECK PER COMBUSTION DESIGN ACTIVITY.
 2. THE OXIDIZER AND FUEL SHALL BE FLOWED SEPARATELY AT THE FOLLOWING FLOW RATES: OXIDIZER: 25, 35, 45, 55, 65; FUEL: 20, 25, 35, 40, 45. FOR EACH DATA POINT RECORD THE MANIFOLD P, FLOWRATE, INITIAL WATER FLOW TEMPERATURE AND ACTUAL OUTPUT FREQUENCY OF FLOWMETER. CALCULATE q_p :

$$q_p = \frac{P}{(\rho)(5)}$$
 WHERE: q_p = FLOWRATE, LB/SEC
 P = INLET-OUTLET PRESSURE, PSI
 ρ = SPECIFIC GRAVITY OF WATER AT FLOW TEMPERATURE
- NOTE: POSITION HOLD PER ATC-4935A USING 22.



LIFTING POINT (12) REF

LIFTING POINT (13) REF

AR	WELD ROD	ER 316	AWS A 5.9	22
AD	LUBRICANT		ATC-4410B-1	21
AQ	LUBRICANT	WD12		20
1	C-RING	A500J0K2		19
1	C-RING	A500J0K2		18
1	BOLT	M31700		17
2	BOLT	M1004B		16

16	M52002100	WASHER		5
4	M551937-5C	BOLT EYE		4
4	M53569F-33	NUT		3
2	A500J0K2	O-RING		2
4	A500J0K2	O-RING		11
2	A500J0K2	O-RING		10
2	A500J0K2	O-RING		9
2	AN893-3J	BUSHING		7
2	AN815-2J	UNION		6
4	AN815-4J	UNION		5
1	1100773-B	BOSS		4
1	1206427-9	INJECTOR		3
1	-3	INJECTOR		2
1	-3	INJECTOR		1

GENCORP AERJET TechSystems

INJECTOR ASSY, OX/H-C 3D SUBASSEMBLY (ROCCID TEST VALIDATION)

E 05824 1206427

DATE: 2011/11/13

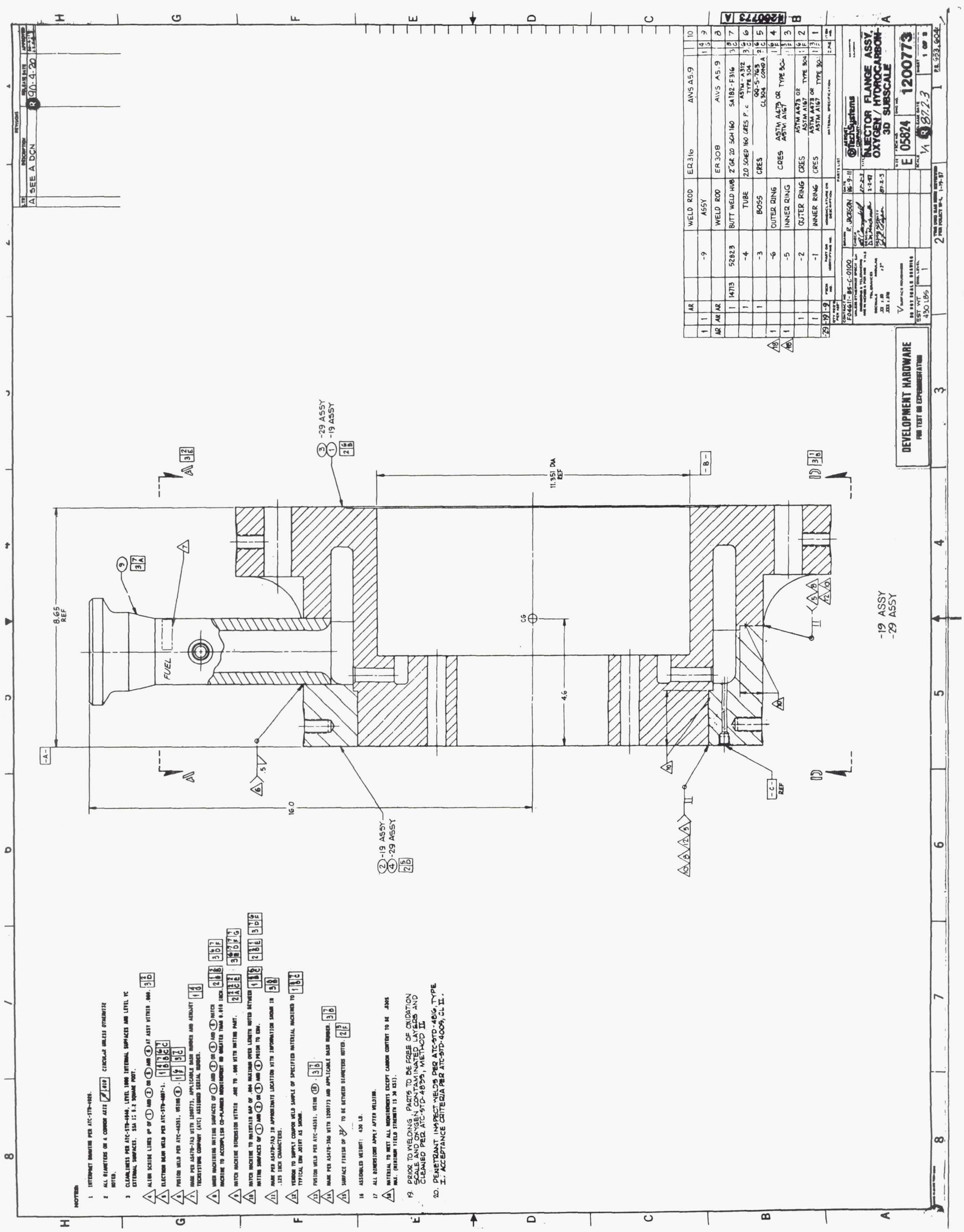
REV: 1

DO NOT SCALE DRAWING

2 THE ORIGINAL COPY IS KEPT IN THE FILE

1 OF 1

DEVELOPMENT HARDWARE FOR TEST OR EXPERIMENTATION



- NOTES:**
1. INTERMITTENT DIMENSIONS PER ATC-579-4823.
 2. ALL DIMENSIONS ON A COMMON AXIS UNLESS OTHERWISE NOTED.
 3. CLEARANCES PER ATC-579-4844, LEVEL AND INTERNAL SURFACES AND LEVEL VC EXTERNAL SURFACES, 25 ± 1.4 SQUARE FEET.
 4. ALLOW SCISSOR LINES OF ① AND ② OR ③ AND ④ AT ASST WITHIN .004. ③ ④
 5. ELECTRON BEAM WELD PER ATC-579-4897-1. ① ② ③ ④
 6. POSITION WELD PER ATC-48381, USE TIME ① ② AND ③ SWITCH MACHINE TO ACCOMPLISH CO-PLANAR ALIGNMENT TO MAXIMUM TOLERANCE 0.015 INCH. ① ② ③ ④
 7. WELD PER AS479-743 WITH 1200773, APPLICABLE WELD NUMBER AND AGENCY TECHNICAL COMPANY (ATC) ASSIGNED SERIAL NUMBER. ① ② ③ ④
 8. WELD INCLUDING INTERNAL SURFACES OF ① AND ② OR ③ AND ④ SWITCH MACHINE TO ACCOMPLISH CO-PLANAR ALIGNMENT TO MAXIMUM TOLERANCE 0.015 INCH. ① ② ③ ④
 9. SWITCH MACHINE EXTENSION WELLS ARE TO .004 WITH WITHIN PART. ① ② ③ ④
 10. SWITCH MACHINE TO MAINTAIN GAP OF .004 MAXIMUM OVER LENGTH NOTED BETWEEN INTERNAL SURFACES OF ① AND ② OR ③ AND ④ PRIOR TO ENM. ① ② ③ ④
 11. WELD PER AS479-743 IN APPROPRIATE LOCATION WITH INFORMATION SHOWN IN ⑤ ⑥
 12. .125 TIE CONNECTORS.
 13. TYPICAL END JOINT AS SHOWN.
 14. POSITION WELD PER ATC-48381, USE TIME ① ② ③
 15. WELD PER AS479-743 WITH 1200773 AND APPLICABLE WELD NUMBER. ③ ④
 16. SURFACE FINISH OF ⑤ TO BE BETWEEN DIMENSIONS NOTED. ② ③
 17. ASSEMBLED WEIGHT: 430 LB.
 18. ALL DIMENSIONS APPLY AFTER WELDING.
 19. MATERIAL TO MEET ALL REQUIREMENTS EXCEPT CARBON CONTENT TO BE .42MAX. MAX. (MINIMUM YIELD STRENGTH IS 34 031).
 20. PRIOR TO WELDING, PARTS TO BE FREE OF OXIDATION SCALE AND OXYGEN CONTAMINATED LAYERS AND CLEANED PER ATC-579-4897-1, METHOD II.
 21. PENETRANT INSPECT WELDS PER ATC-579-4896, TYPE I. ACCEPTANCE CRITERIA PER ATC-579-4896, CL II.

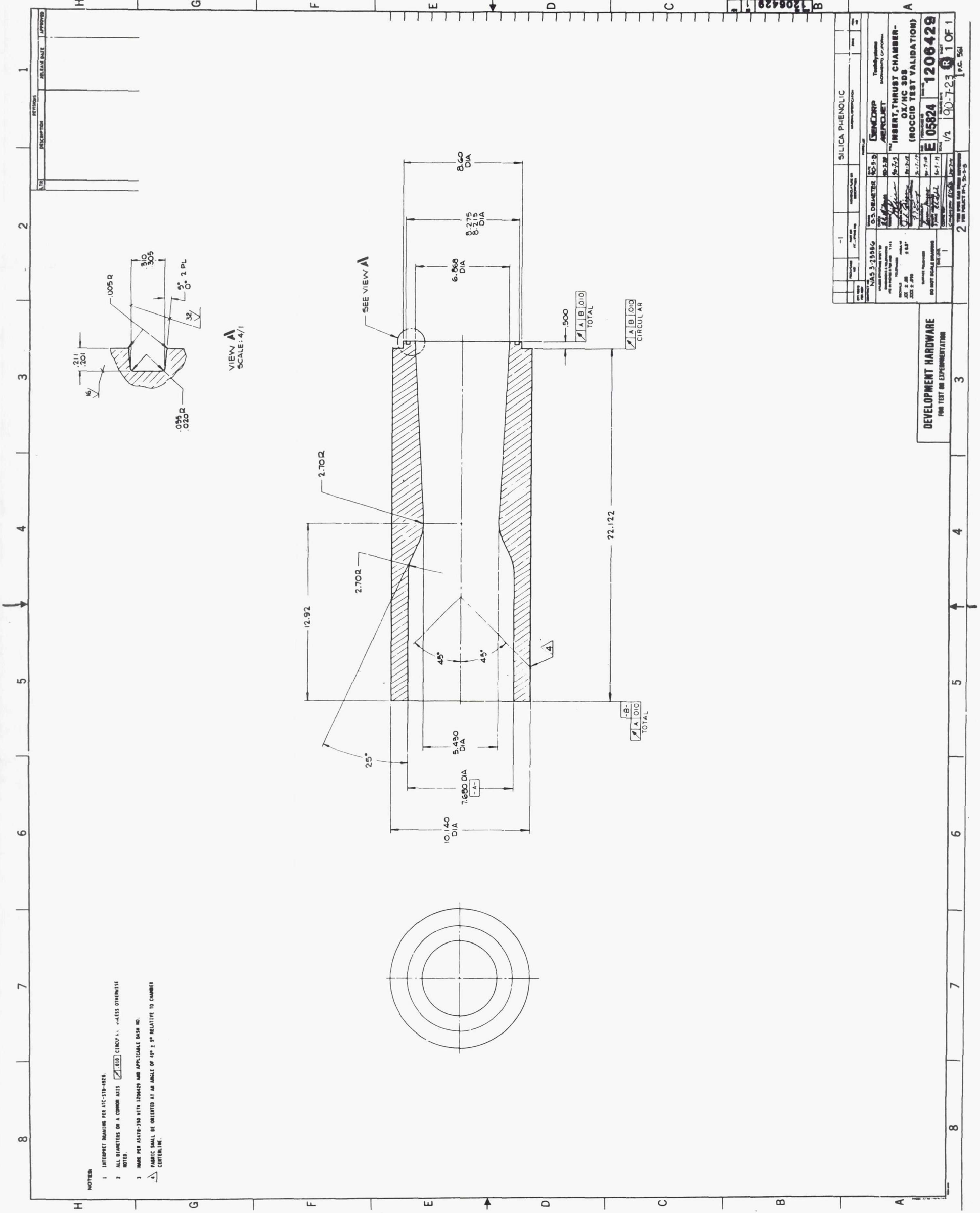
AR	WELD ROD	ER316	AN5 A5.9	10
1	ASSY			1
AR AR	WELD ROD	ER308	AIVS A5.9	1
1	14713	52823	2 GR 20 SCH 160	SA182-F316
1		-4	20 SCHED 160 GRES P. C	TYPE 304
1		-3	BOSS	CRES
1		-6	OUTER RING	CRES
1		-5	INNER RING	CRES
1		-2	OUTER RING	CRES
1		-1	INNER RING	CRES
29	9			

ITEM NO.	DESCRIPTION	QTY	UNIT
1	ASSY	1	EA
2	WELD ROD	10	EA
3	WELD ROD	1	EA
4	WELD ROD	1	EA
5	WELD ROD	1	EA
6	WELD ROD	1	EA
7	WELD ROD	1	EA
8	WELD ROD	1	EA
9	WELD ROD	1	EA
10	WELD ROD	1	EA
11	WELD ROD	1	EA
12	WELD ROD	1	EA
13	WELD ROD	1	EA
14	WELD ROD	1	EA
15	WELD ROD	1	EA
16	WELD ROD	1	EA
17	WELD ROD	1	EA
18	WELD ROD	1	EA
19	WELD ROD	1	EA
20	WELD ROD	1	EA

DEVELOPMENT HARDWARE
FOR TEST OR EXPERIMENTATION

-19 ASSY
-29 ASSY

CONTRACT NO. **FO461-85-C-0100**
 WORK ORDER NO. **1200773**
 DATE **12-2-87**
 DRAWN BY **D.M. [Signature]**
 CHECKED BY **[Signature]**
 DATE **12-2-87**
 TITLE **INJECTOR FLANGE ASSY. OXYGEN / HYDROCARBON-3D SUBSCALE**
 PART OR IDENTIFYING NO. **1200773**
 QUANTITY **1**
 UNIT **EA**
 WEIGHT **430** LBS
 EST. WT. **430** LBS
 MATERIAL SPECIFICATION **AN5 A5.9**
 PART OR IDENTIFYING NO. **1200773**
 QUANTITY **1**
 UNIT **EA**
 WEIGHT **430** LBS
 EST. WT. **430** LBS
 MATERIAL SPECIFICATION **AN5 A5.9**



NOTES

- 1 INTERPRET DIMENSIONS PER ATC-119-4926.
- 2 ALL DIMENSIONS ON A COMMON AXIS UNLESS OTHERWISE NOTED.
- 3 MAKE PER AS179-350 WITH LENGTHS AND APPLICABLE DASH NO. FABRIC SHALL BE ORIENTED AT AN ANGLE OF 45° ± 5° RELATIVE TO CHAMBER CENTERLINE.

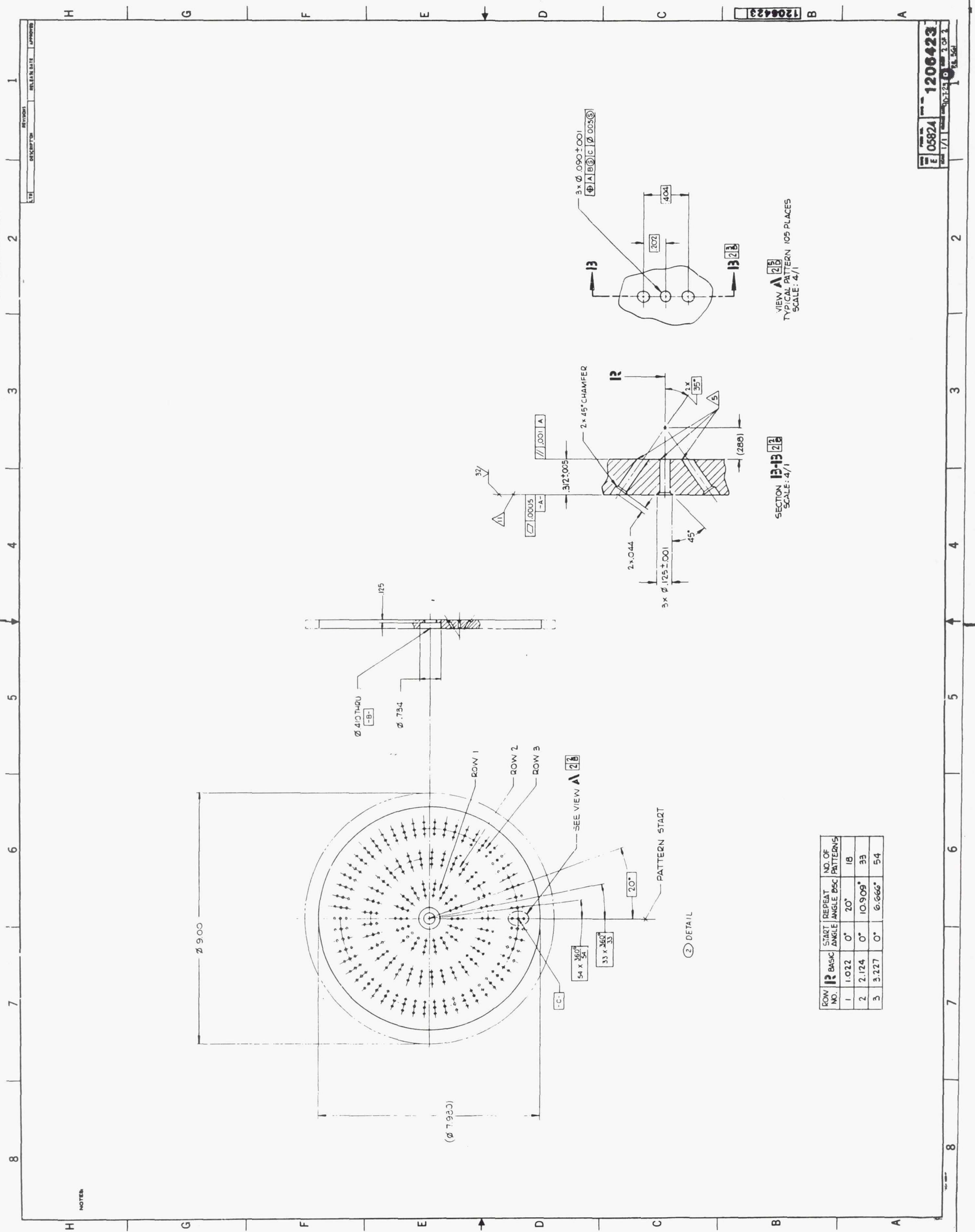
VIEW A
SCALE: A/1

REV		DATE	DESCRIPTION	APPROVED
1				

PART NAME		SILICA PHENOLIC	
MATERIAL SPECIFICATION			
DRAWING NO.		1206429	
REV		1	
DATE		90-7-23	
BY		[Signature]	
CHECKED		[Signature]	
APPROVED		[Signature]	
TITLE		INERT, THRUST CHAMBER- OX/HC 3DB (ROCCID TEST VALIDATION)	
PROJECT NO.		E 05824	
PAGE NO.		1 OF 1	
P.C. NO.		561	

DEVELOPMENT HARDWARE
FOR TEST ON EXPERIMENTATION

Figure D-7 D-9



NOTES

ROW NO.	BASIC ANGLE	START ANGLE	REPEAT ANGLE	NO. OF PDC PATTERNS
1	1.022	0°	20°	18
2	2.124	0°	10.909°	33
3	3.227	0°	6.666°	54

SECTION B-B
SCALE: 4/1

VIEW A-A
TYPICAL PATTERN 105 PLACES
SCALE: 4/1

(2) DETAIL

H G F E D C B A

1 2 3 4 5 6 7 8

Figure D-8 D-10

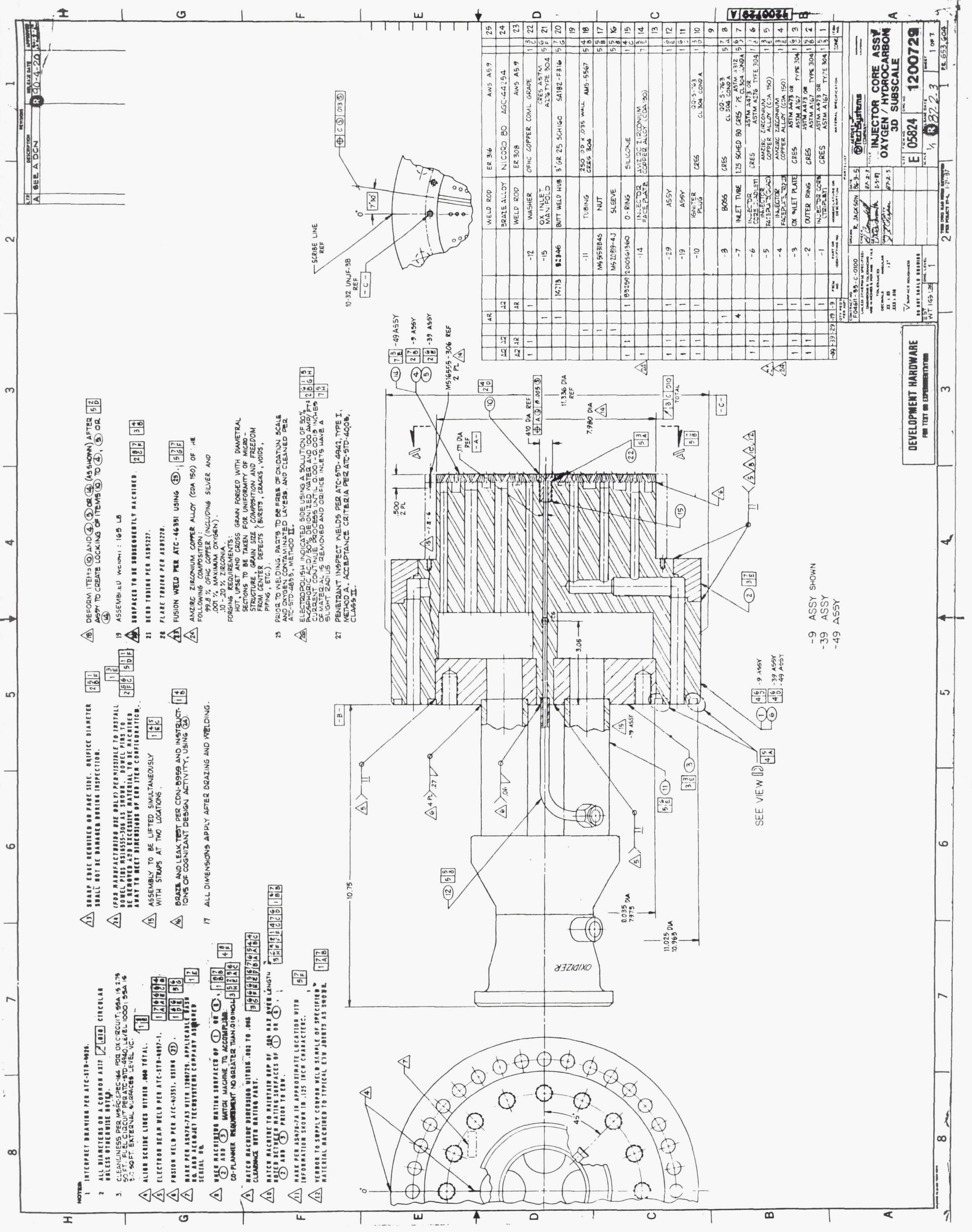
REV	DATE	BY	CHKD	APP'D
1				

DESCRIPTION: RELEASE DATE: APPROVED

1208423

05824 1208423

1/1



QTY	DESCRIPTION	REF	UNIT	MATERIAL
25	WELD ROD	ER 316	AWS A59	
24	BRAZE ALLOY	NICORO 80	AGC-44254	
23	WELD ROD	ER 308	AWS A59	
22	WASHER	OFHC COPPER COML GRADE		
21	OX INLET MANIFOLD		CRES ASTM A276 TYPE 304	
20	BUTT WELD HUB	3.68 25 SCH160	SA182-F316	
19	TUBING	250 OD X 0.035 WALL	AMS-5567	
18	NUT	M595184S		
17	SLEEVE	M52079-4J		
16	O-RING	193299	1000561960	
15	INJECTOR FEEDER PLATE		SILICONE	
14	ASSY			
13	ASSY			
12	ASSY			
11	IGNITER PLUG			
10	ROD			
9	ROD			
8	INLET TUBE	125 SCHED 80 CRES	CL 304	
7	INJECTOR CORE MANIFOLD			
6	INJECTOR CORE MANIFOLD			
5	INJECTOR CORE MANIFOLD			
4	INJECTOR CORE MANIFOLD			
3	OX INLET PLATE			
2	OUTER RING			
1	INJECTOR CORE (TRIPLET)			

DEVELOPMENT HARDWARE
FOR TEST OR DEMONSTRATION

DATE: 10/13/78
REV: 1
E 05824
1200729

INJECTOR CORE ASSY
OXYGEN / HYDROCARBON
3D SUBSCALE

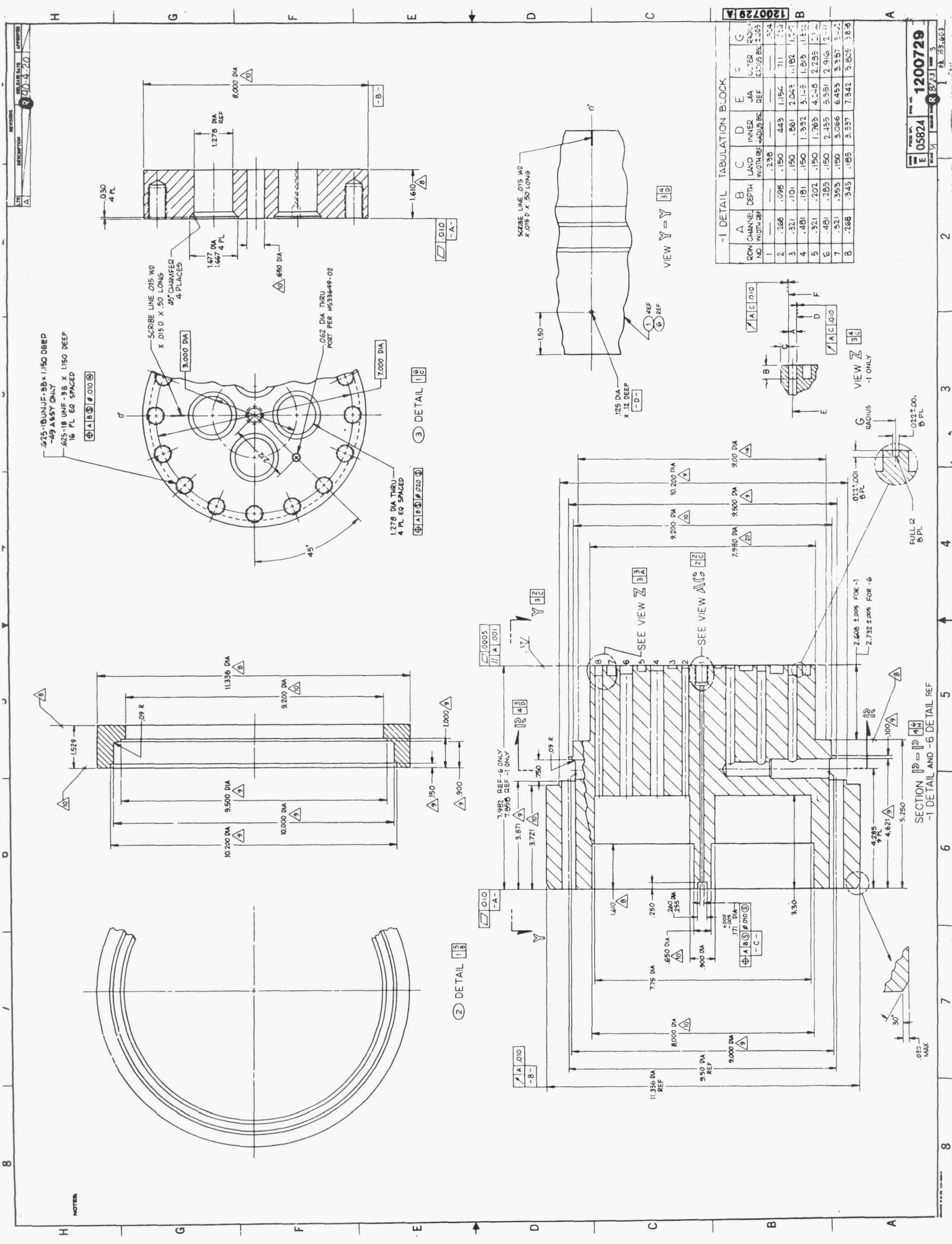
DESIGNED BY: J. JACKSON
CHECKED BY: J. JACKSON
DRAWN BY: J. JACKSON
DATE: 10/13/78

- 17 ALL DIMENSIONS APPLY AFTER BRAZING AND WELDING.
- 18 BRAZING AND LEAK TEST PER CON-8969 AND INSTRUC-TIONS OF COGNIZANT DESIGN ACTIVITY, USING ②①④⑤⑥⑦⑧⑨⑩⑪⑫⑬⑭⑮⑯⑰⑱⑲⑳㉑㉒㉓㉔㉕㉖㉗㉘㉙㉚㉛㉜㉝㉞㉟㊱㊲㊳㊴㊵㊶㊷㊸㊹㊺㊻㊼㊽㊾㊿
- 19 ASSEMBLY TO BE SUBSEQUENTLY MACHINED, ㉑㉒㉓㉔㉕㉖㉗㉘㉙㉚㉛㉜㉝㉞㉟㊱㊲㊳㊴㊵㊶㊷㊸㊹㊺㊻㊼㊽㊾㊿
- 20 FLARE TYPING PER ASS9227.
- 21 BEAD TYPING PER ASS9227.
- 22 FUSION WELD PER ATC-46381 USING ㉑㉒㉓㉔㉕㉖㉗㉘㉙㉚㉛㉜㉝㉞㉟㊱㊲㊳㊴㊵㊶㊷㊸㊹㊺㊻㊼㊽㊾㊿
- 23 ANZIRC ZIRCONIUM COPPER ALLOY (CDA 150) OF THE FOLLOWING COMPOSITION: 99.8% OFHC COPPER (INCLUDING SILVER AND .001% MAXIMUM OXYGEN), .10-20% ZIRCONIA.
- 24 FORGING REQUIREMENTS: GRAIN FORGED WITH DIAMETRAL SECTIONS TO BE TAKEN FOR UNIFORMITY OF MICRO-STRUCTURE, GRAIN SIZE, COMPOSITION AND FREEDOM FROM CENTER DEFECTS (BURSTS, CRACKS, VOIDS, PIPING, ETC.).
- 25 PRIOR TO WELDING, PARTS TO BE FREE OF OXIDATION SCALE AND OXYGEN CONTAMINATED LAYERS AND CLEANED PER ATC-57D-4895, METHOD II.
- 26 ELECTROPOLISH INDICATED SIDE USING A SOLUTION OF 50% PLAGHORIC ACID/50% DEIONIZED WATER AND 100 AMP/FT² PLATING CURRENT. POLISHING DISCS MUST BE 0.002-0.003 INCHES THICK AND MUST BE REMOVED AND DISPOSED INLET'S HAVE A SLIGHT RADIUS.
- 27 PENETRANT INSPECT WELDS PER ATC-57D-4943, TYPE I, METHOD A, ACCEPTANCE CRITERIA PER ATC-57D-6008, CLASS II.

- 1 STRAP EDGE REQUIRED ON FARE SIDE. BRIFICE DIAMETER SHALL NOT BE DAMAGED DURING INSPECTION.
- 2 FOR MANUFACTURING USE ONLY: PERMISSIBLE TO INSTALL BOWL PINS R31855-308 AS SHOWN. BOWL PINS TO BE REMOVED AS EXCESSIVE MATERIAL TO BE MACHINED AWAY TO MEET DIMENSIONS OF END ITEM CONFIGURATION.
- 3 ASSEMBLY TO BE LIFTED SIMULTANEOUSLY WITH STRAPS AT TWO LOCATIONS.
- 4 BRAZING AND LEAK TEST PER CON-8969 AND INSTRUC-TIONS OF COGNIZANT DESIGN ACTIVITY, USING ㉑㉒㉓㉔㉕㉖㉗㉘㉙㉚㉛㉜㉝㉞㉟㊱㊲㊳㊴㊵㊶㊷㊸㊹㊺㊻㊼㊽㊾㊿
- 5 ALL DIMENSIONS APPLY AFTER BRAZING AND WELDING.

- 1 INTERPRET DRAWING PER ATC-57D-0026.
- 2 ALL DIMENSIONS ON A COMMON AXIS UNLESS OTHERWISE NOTED.
- 3 CLEANLINESS PER MFSC-PRC-664, P20, OIL CLEAN, 500 IS 3.75 SOFT, FULL CIRCUIT PER ATC-57D-4940, LEVEL 0001, 50A, 16 5-750 FT. EXTERNAL SPRINGS LEVEL VC.
- 4 ALIGN SCRIBE LINES WITHIN .000 TOTAL.
- 5 ELECTROD BEAR WELD PER ATC-57D-1007-1.
- 6 FUSION WELD PER ATC-46381, USING ㉑㉒㉓㉔㉕㉖㉗㉘㉙㉚㉛㉜㉝㉞㉟㊱㊲㊳㊴㊵㊶㊷㊸㊹㊺㊻㊼㊽㊾㊿
- 7 MAKE PER ASS9227 WITH IDENTIFYING APPLICABLE SERIAL NO. AND LABELS/TECHSYSTEMS COMPANY NUMBER SERIAL NO.
- 8 WHEN MACHINING SURFACES OF ㉑㉒㉓㉔㉕㉖㉗㉘㉙㉚㉛㉜㉝㉞㉟㊱㊲㊳㊴㊵㊶㊷㊸㊹㊺㊻㊼㊽㊾㊿
- 9 ADD ㉑㉒㉓㉔㉕㉖㉗㉘㉙㉚㉛㉜㉝㉞㉟㊱㊲㊳㊴㊵㊶㊷㊸㊹㊺㊻㊼㊽㊾㊿
- 10 PLANNER REQUIREMENT NO GREATER THAN 0.001 INCHES CLEARANCE WITH MATING PART.
- 11 MATCH MACHINING DIMENSIONS WITHIN .002 TO .005 CLEARANCE WITH MATING PART.
- 12 MATCH MACHINE TO MAINTAIN GAP OF .004 MAX OVER LENGTH
- 13 HOLER BETWEEN MATING SURFACES OF ㉑㉒㉓㉔㉕㉖㉗㉘㉙㉚㉛㉜㉝㉞㉟㊱㊲㊳㊴㊵㊶㊷㊸㊹㊺㊻㊼㊽㊾㊿
- 14 ADD ㉑㉒㉓㉔㉕㉖㉗㉘㉙㉚㉛㉜㉝㉞㉟㊱㊲㊳㊴㊵㊶㊷㊸㊹㊺㊻㊼㊽㊾㊿
- 15 MAKE PER ASS9227 IN APPROPRIATE LOCATION WITH INFORMATION SHOWN IN .125 INCH CHARACTERS.
- 16 PERFORM TO SUPPLY COPPER WELD SAMPLE OF SPECIFIED MATERIAL MACHINED TO TYPICAL ETW JOINTS AS SHOWN.
- 17 ㉑㉒㉓㉔㉕㉖㉗㉘㉙㉚㉛㉜㉝㉞㉟㊱㊲㊳㊴㊵㊶㊷㊸㊹㊺㊻㊼㊽㊾㊿

-9 ASSY SHOWN
-39 ASSY
-49 ASSY



REVISIONS: 3 10-4-70

NO.	DESCRIPTION	DATE	BY	APP'D
1				

ROW NO.	A	B	C	D	E	F	G
	CHANNEL WIDTH REF	DEPTH	INNER RADIUS REF	INNER RADIUS REF	INNER RADIUS REF	INNER RADIUS REF	RADIUS REF
1	.238		.443	1.154	.711		.554
2	.268	.098	.150	.443	1.154		.711
3	.321	.101	.150	2.043	1.182		1.57
4	.481	.181	.150	1.332	3.125		1.818
5	.321	.202	.150	1.363	4.248		2.735
6	.481	.285	.150	2.435	5.351		2.916
7	.321	.365	.150	3.066	6.453		3.357
8	.268	.345	.185	3.537	7.342		3.805

PART NO. 1200729
 E 05824
 REV. 1
 DATE 10/23/73
 BY 233/603

Figure D-11 D-13

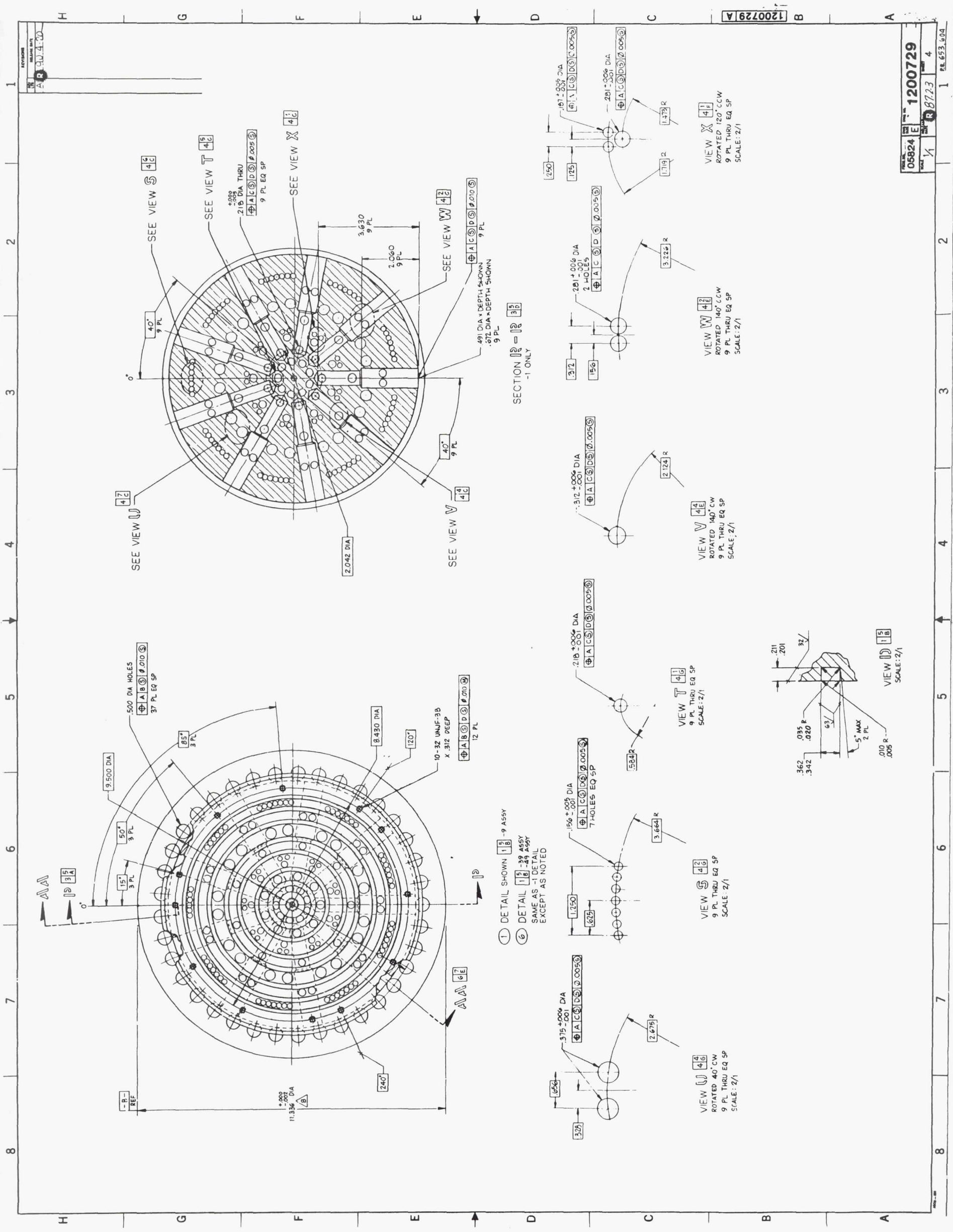
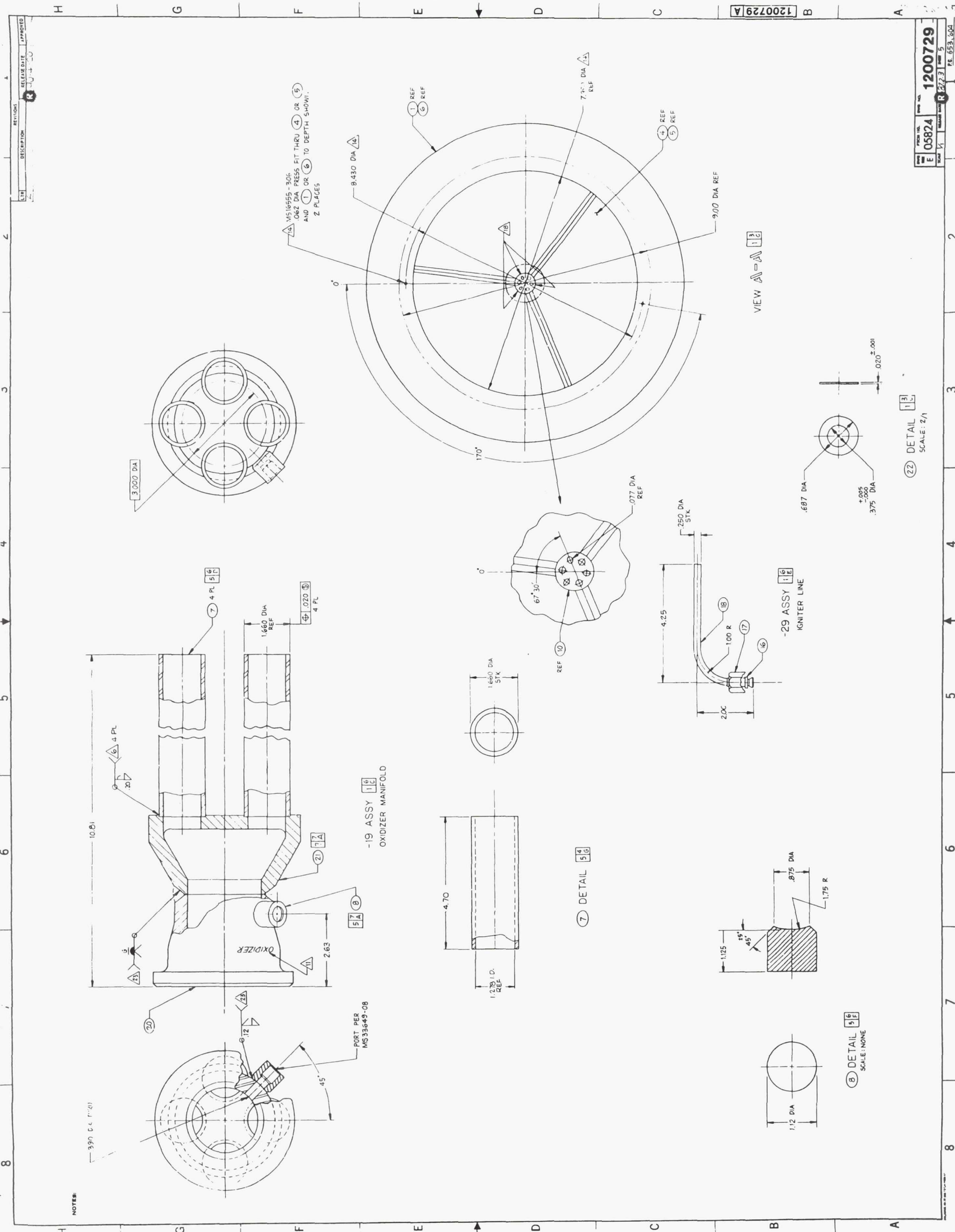


Figure D-12 D-14



NOTES:

390 C & T-01

PORT PER MS33649-08

-19 ASSY 116 OXIDIZER MANIFOLD

8 DETAIL 56 SCALE: NONE

7 DETAIL 54

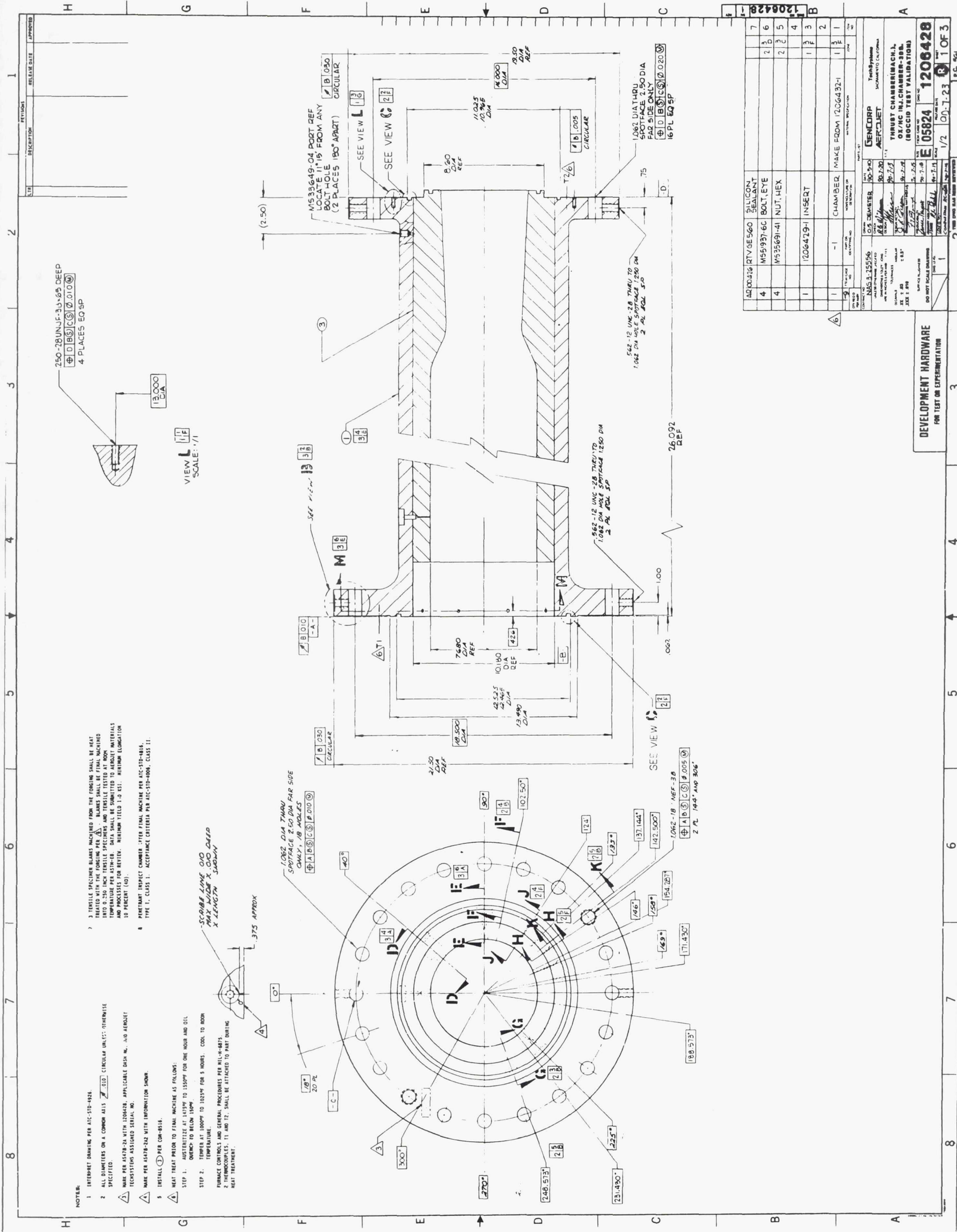
-29 ASSY 116 IGNITER LINE

22 DETAIL 13 SCALE: 2/1

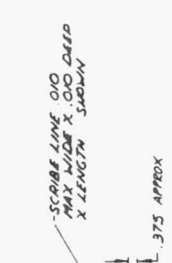
VIEW A-A 13

REV	DATE	BY	CHKD	APP'D	DESCRIPTION
1					
2					
3					
4					
5					
6					
7					
8					
9					
10					
11					
12					
13					
14					
15					
16					
17					
18					
19					
20					
21					
22					
23					
24					
25					
26					
27					
28					
29					
30					
31					
32					
33					
34					
35					
36					
37					
38					
39					
40					
41					
42					
43					
44					
45					
46					
47					
48					
49					
50					
51					
52					
53					
54					
55					
56					
57					
58					
59					
60					
61					
62					
63					
64					
65					
66					
67					
68					
69					
70					
71					
72					
73					
74					
75					
76					
77					
78					
79					
80					
81					
82					
83					
84					
85					
86					
87					
88					
89					
90					
91					
92					
93					
94					
95					
96					
97					
98					
99					
100					

Figure D-13 D-15



- NOTES:**
- 1 INTERPRET DRAWING PER AIC-STD-492B.
 - 2 ALL DIMENSIONS ON A COMMON AXIS UNLESS OTHERWISE SPECIFIED.
 - 3 TERRESTRIAL SPECIMEN BLANKS MACHINED FROM THE FORGING SHALL BE HEAT TREATED WITH THE FORGING PER AIC-STD-492B. BLANKS SHALL BE FINISH MACHINED TO THE SPECIFIED DIMENSIONS AND TENSILE TESTED AT ROOM TEMPERATURE PER AIC-STD-492B. MATERIALS AND PROCESSES FOR REVIEW. MINIMUM TILED 1.0-1.5% MINIMUM ELONGATION 10 PERCENT (40).
 - 4 PREHEAT INSPECT CHAMBER AFTER FINAL MACHINE PER AIC-STD-492B. TYPE T, CLASS 1. ACCEPTANCE CRITERIA PER AIC-STD-492B, CLASS 1.
 - 5 INSTALL (3) PER COM-8514.
 - 6 HEAT TREAT PRIOR TO FINAL MACHINE AS FOLLOWS:
 STEP 1. AUSTENITIZE AT 1425°F TO 1530°F FOR ONE HOUR AND OIL QUENCH TO BELOW 135°F.
 STEP 2. TEMPER AT 1000°F TO 1025°F FOR 5 HOURS. COOL TO ROOM TEMPERATURE.
 FURNACE CONTROLS AND GENERAL PROCEDURES PER MIL-W-8875.
 2. THERMOCOUPLES, T1 AND T2, SHALL BE ATTACHED TO PART DURING HEAT TREATMENT.



QTY	DESCRIPTION	REVISION	DATE	APPROVED
7	AD000416 RTV/GE560 SILICON SEALANT			
4	M551937-6C BOLT, EYE	2	3	6
4	M535691-41 NUT, HEX	2	2	5
1	1206429-1 INSERT	1	3	4
1	-1 CHAMBER MAKE FROM 1206432-1	1	3	1
2	PER PROJECT PL. 30-9-C			

REV	DATE	DESCRIPTION
1	00-7-23	1 OF 3

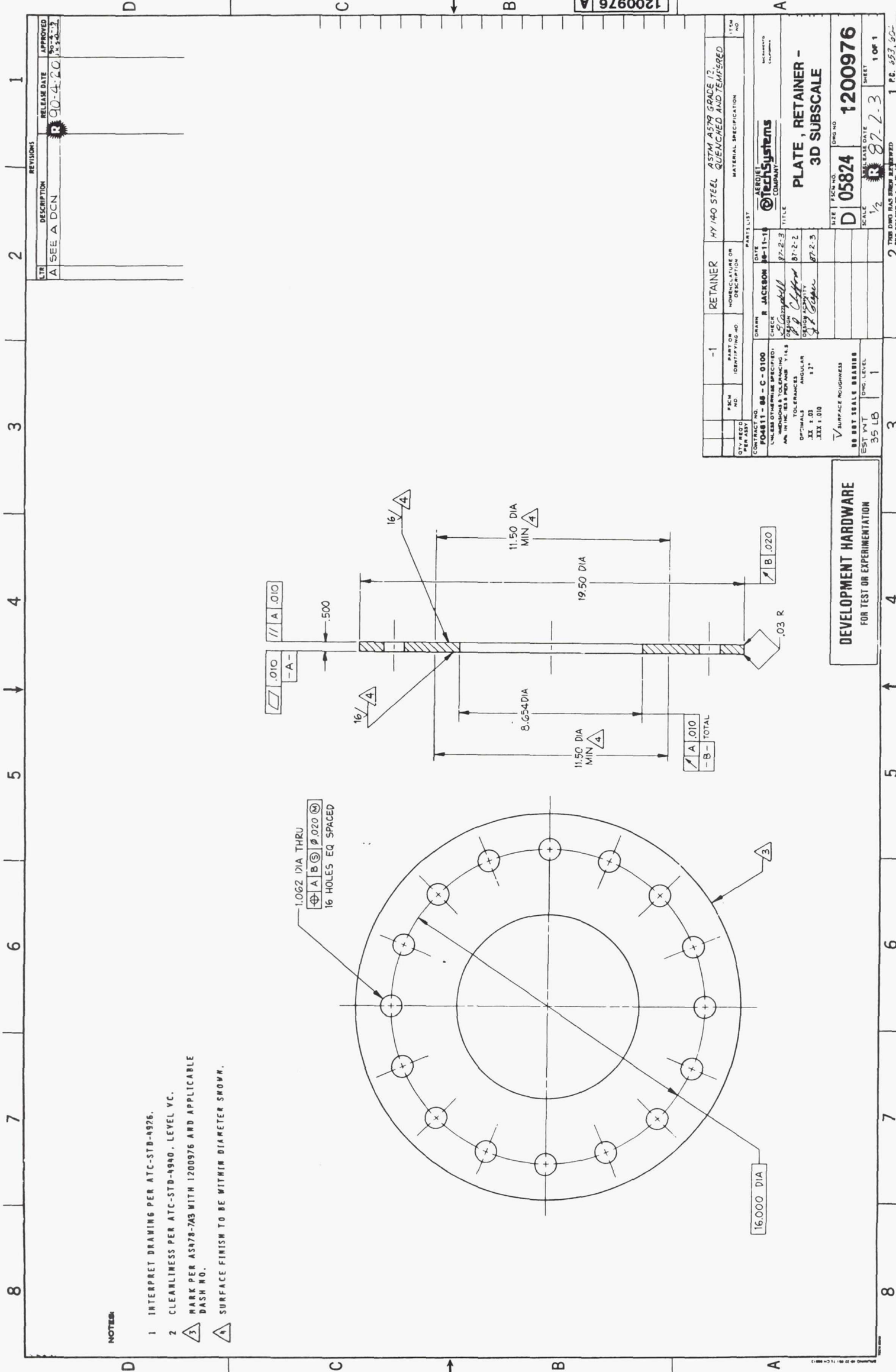
REV	DATE	DESCRIPTION
1	00-7-23	1 OF 3

REV	DATE	DESCRIPTION
1	00-7-23	1 OF 3

REV	DATE	DESCRIPTION
1	00-7-23	1 OF 3

REV	DATE	DESCRIPTION
1	00-7-23	1 OF 3

REV	DATE	DESCRIPTION
1	00-7-23	1 OF 3



- NOTES:**
- 1 INTERPRET DRAWING PER ATC-STD-4976.
 - 2 CLEANLINESS PER ATC-STD-4940, LEVEL VC.
 - 3 MARK PER AS478-7A3 WITH 1200976 AND APPLICABLE DASH NO.
 - 4 SURFACE FINISH TO BE WITHIN DIAMETER SHOWN.

REV	DESCRIPTION	DATE	APPROVED
1	A SEE A DCN	90-4-20	

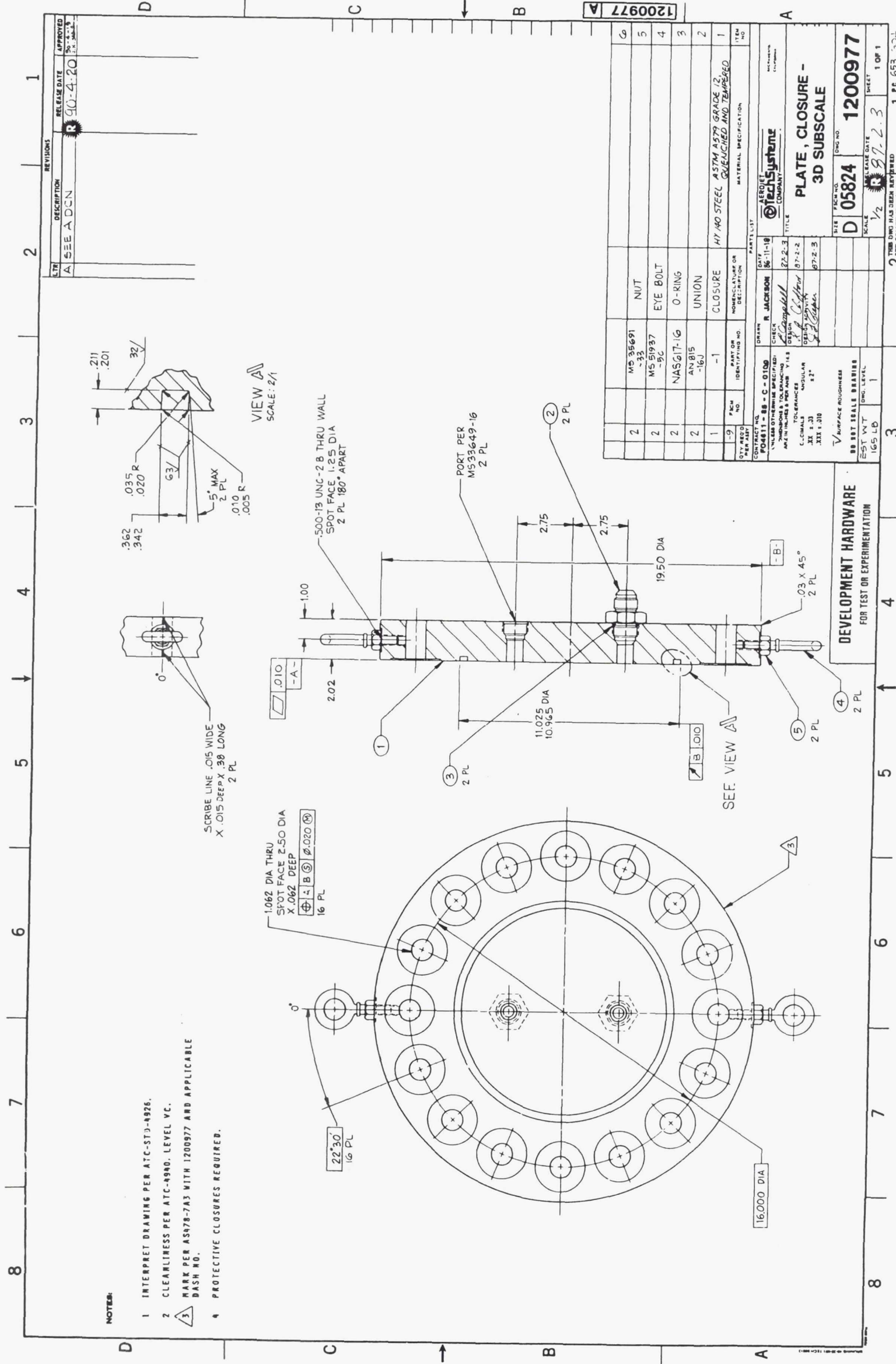
CONTRACT NO.	FO4811-88-C-0100	DATE	88-11-18
UNLESS OTHERWISE SPECIFIED:		CHECK	
UNLESS OTHERWISE SPECIFIED:		DATE	87-2-3
UNLESS OTHERWISE SPECIFIED:		DATE	87-2-3
UNLESS OTHERWISE SPECIFIED:		DATE	87-2-3
TOLERANCES			
XX ± .03			
XXX ± .08			
✓ SURFACE FINISHES			
88 887 ISALE BEARERS			
EST. WGT.	35 LB		
DRG. LEVEL	1		
SIZE	D	FIG. NO.	1200976
SCALE	1/2	RELEASE DATE	87-2-3
			1 OF 1

DEVELOPMENT HARDWARE
FOR TEST OR EXPERIMENTATION

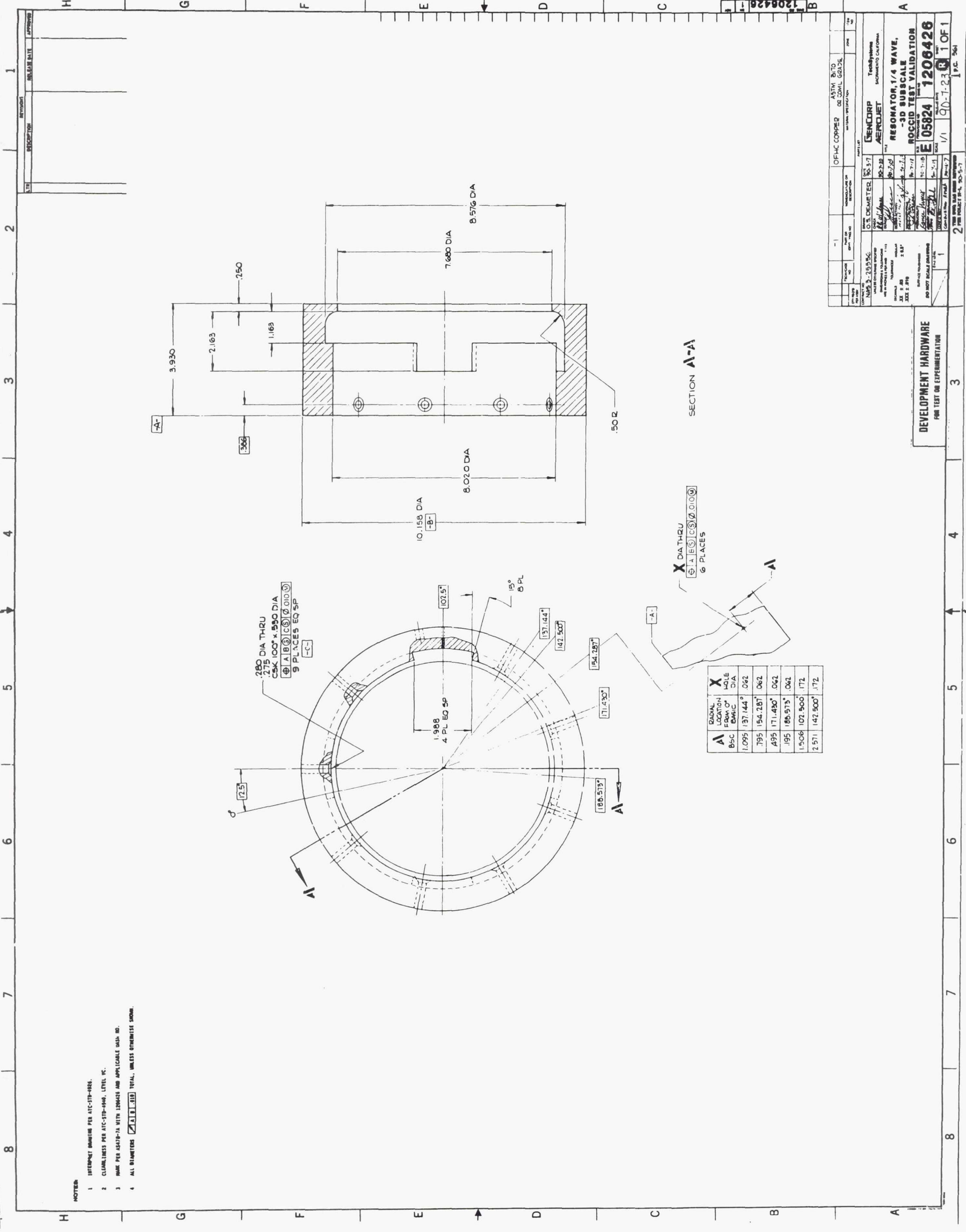
<input checked="" type="checkbox"/> AD CN		<input type="checkbox"/> DCN	DATE 90-5-15	DOCUMENT CHANGE NOTICE		1200976	A-1
PREPARED BY DEMETER		RELEASE DATE 90-7-23		GENCORP TechSystems AEROMET SACRAMENTO, CALIFORNIA		PLATE, RETAINER - 3D SUBSCALE	1 of 1
SH	ZONE	ITEM	DESIGN	APPROVALS	STRESS	WF CONSTRUCTION	
		PL 1	ADD: 5-2 RETAINER	90-7-13 R. E. BARKER 90-7-13	90-7-13 R. E. BARKER 90-7-13	90-7-13 R. E. BARKER 90-7-13	
		F/D 2	ADD CALLOUTS & DIMENSION SHOWN				
		GN 3	ADD NOTE:				

4340 STEEL VACUUM MELT PER AMS 6414E

PC 653, 604, 56



- NOTES:**
- 1 INTERPRET DRAWING PER ATC-STJ-4926.
 - 2 CLEANLINESS PER ATC-4990, LEVEL VC.
 - 3 MARK PER AS78-7A3 WITH 1200977 AND APPLICABLE DASH NO.
 - 4 PROTECTIVE CLOSURES REQUIRED.



- NOTES
1. INTERMEDIATE DIMENSIONS PER AIC-STD-488A.
 2. CLEARANCES PER AIC-STD-484, LEVEL 1C.
 3. HOLE PER AS4776-1A WITH 1206419 AND APPLICABLE GUN-DR.
 4. ALL DIMENSIONS \checkmark (1.1.11) TOTAL, UNLESS OTHERWISE SHOWN.

DIAL LOCATION FROM C	WAVE DIA
A	1.095
B-C	.795
	.495
	.195
	1.506
	2.511

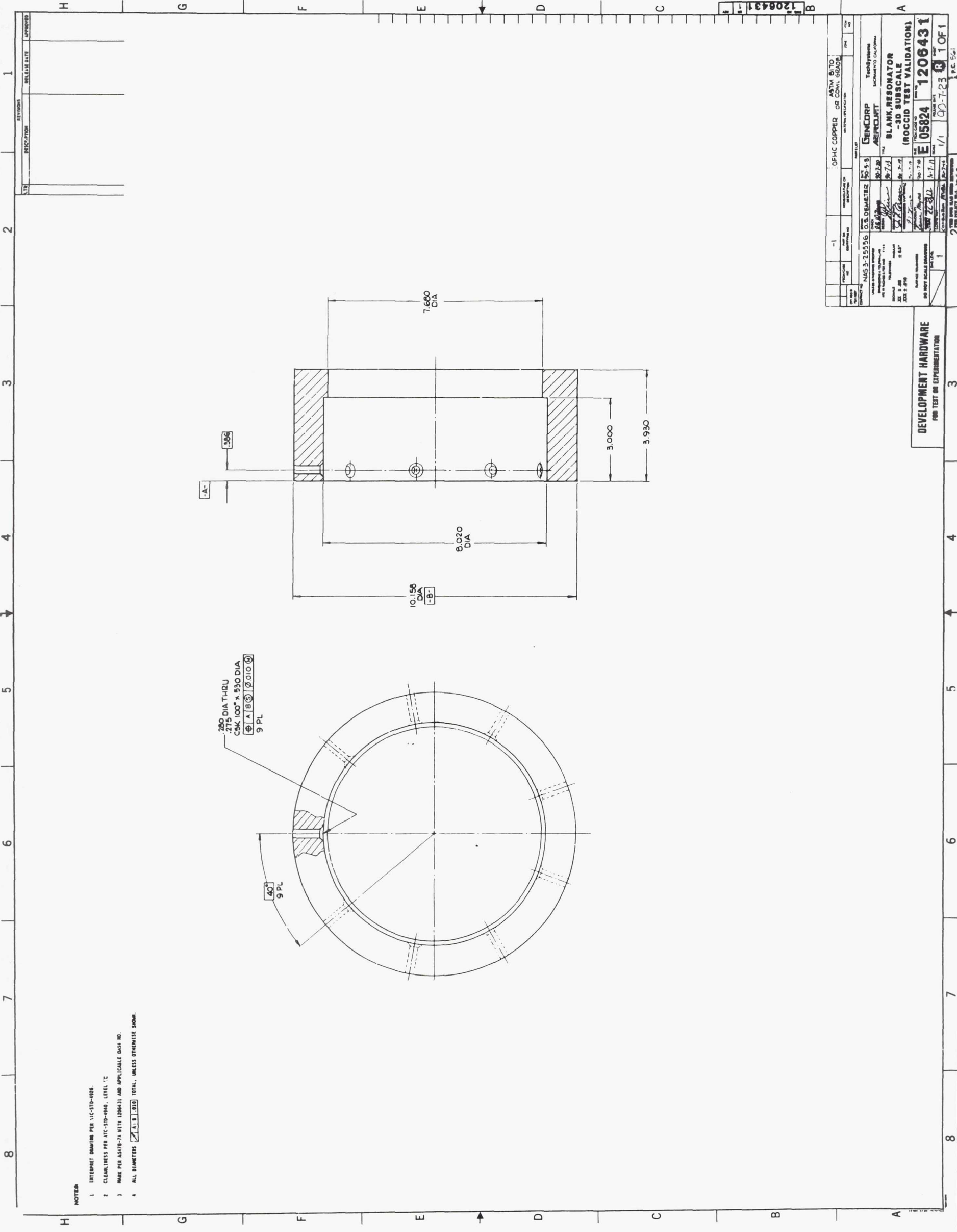
X DIA THRU
0.125 DIA
6 PLACES

SECTION A-A

DEVELOPMENT HARDWARE
FOR TEST ON EXPERIMENTATION

PROJECT NO.	1208426	REV.	1
DATE	90-1-23	BY	1
DESIGNED BY	1	CHECKED BY	1
APPROVED BY	1	DATE	90-1-23
SCALE	1 P.C. 364	TOTAL SHEETS	1 OF 1
MATERIALS			
ITEM	DESCRIPTION	QTY	UNIT
1	OFHC COPPER	1	PC
2	ASTM B170	1	PC
3	DE JONL G24.5C	1	PC
PART LIST			
QTY	DESCRIPTION	QTY	UNIT
1	O.S. DEMETER 30-3-7	1	PC
2	GENCORP AEROCORP	1	PC
3	RESONATOR, 1/4 WAVE, -3D SUBSCALE	1	PC
4	ROCCID TEST VALIDATION	1	PC
5	E 05824	1	PC
6	1208426	1	PC

Figure D-25 D-27



NOTES

- 1 INTERPRET DIMENSIONS PER 11C-17D-0104.
- 2 CLEARANCES PER 11C-17D-0104, LEVEL 'C'
- 3 MAKE PER AS478-7A WITH 12004-31 AND APPLICABLE DASH NO.
- 4 ALL DIMENSIONS $\sqrt{A \cdot B \cdot C \cdot D}$ TOTAL, UNLESS OTHERWISE SHOWN.

DEVELOPMENT HARDWARE
FOR TEST OR EXPERIMENTATION

REV	DATE	BY	CHKD	DESCRIPTION
1				INITIALS
DESIGNER		CHECKED		DATE
DRAWN		APPROVED		
MATERIAL				
OPHC COPPER OR CONV. GRADE				
PART NAME				
NAS 3-25536				
DIA				
8.020				
LENGTH				
3.930				
MATERIAL				
OPHC COPPER OR CONV. GRADE				
PART NAME				
BLANK RESONATOR				
-3D SUBSCALE				
(ROCCID TEST VALIDATION)				
E 05824		1206431		1 OF 1
1/1		90-7-23		1 PC 5G1

Figure D-26 D-28

APPENDIX E

ADVANCED DOCUMENT CHANGE
NOTICES FOR THE ROCCID
DESIGN DISCLOSURE

DOCUMENT CHANGE NOTICE

GENCORP TechSystems
SACRAMENTO, CALIFORNIA

AEROJET

DCN DCN

DATE **91-3-8**

RELEASE DATE

DWG LVL **1**

DOCUMENT NUMBER **1206427**

DOCUMENT TITLE **INJECTOR ASSY, OX/HC**

REV LTR **A-1**

SHEET **1** OF **3**

APPROVALS

DESIGN AUTHORITY *[Signature]* 15 MAR 91

CHECK

MANUF *France Myer* 91-3-15

QA

STRESS

MATE

WI

CMO

PREPARED BY **L. MYERS**

DESIGN *[Signature]* 91-03-18

ZONE

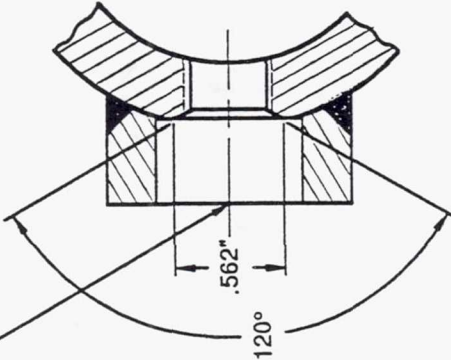
ITEM

SH

IS;

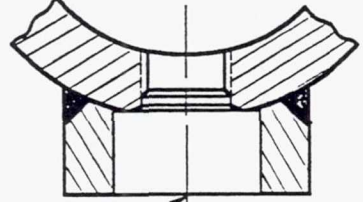
1 6 B 1

C'BORE .750 DIA X .437 DEEP
.4375-20UNF-2B THRU



WAS;

C'BORE .750 DIA X .437 DEEP
PORT PER MS33649-04
EXCEPT .4375-20UNF-2B THRU ONE WALL



DOCUMENTATION CHANGE NOTICE
CONTINUATION SHEET

<input checked="" type="checkbox"/> ADCN	<input type="checkbox"/> DCN	DATE 91-3-8	DWG LEVEL 1	DOCUMENT NUMBER 1206427	REV LTR NC-1	SHEET 2	OF 3
--	------------------------------	-----------------------	-----------------------	-----------------------------------	------------------------	-------------------	----------------

SH	ZONE	ITEM	
1	GN	2	<p>IS; NOTE 9 TEST ASSEMBLY IN THE FOLLOWING ORDER:</p> <p>A. LEAK TEST ASSEMBLY PER ATC-47063, METHOD II, USING CLEAN DRY NITROGEN AT 50 ±5 PSIA. HOLD FOR 5 MINUTES MINIMUM. NO LEAKAGE ALLOWED.</p> <p>B. FLOW TEST WITH CLEAN WATER (PER ATC-STD-4940, LEVEL 1000) AS FOLLOWS:</p> <ol style="list-style-type: none"> 1. PERFORM VISUAL PATTERN CHECK PER COGNIZANT DESIGN ACTIVITY. 2. THE OXIDIZER AND FUEL CIRCUITS SHALL BE FLOWED SEPARATELY AT SEVERAL FLOWRATES BELOW CAVITATION ONSET (~ 50 PSIG ΔP). FOR EACH DATA POINT RECORD THE MANIFOLD ΔP, FLOWRATE, NOMINAL WATER FLOW TEMPERATURE AND ACTUAL OUTPUT FREQUENCY OF FLOWMETER. CALCULATE K_{ω}: $K_{\omega} = \frac{\dot{w}}{(\Delta P) (S_g)}$ <p>WHERE: \dot{w} = FLOWRATE, LB/SEC ΔP = INLET - OUTLET PRESSURE, PSI S_g = SPECIFIC GRAVITY OF WATER AT FLOW TEMPERATURE</p>

DOCUMENTATION CHANGE NOTICE
CONTINUATION SHEET

<input checked="" type="checkbox"/> ADCN	<input type="checkbox"/> DCN	DATE 91-3-8	DWG LEVEL 1	DOCUMENT NUMBER 1206427	REV LTR NC-1	SHEET 3 OF 3
--	------------------------------	-----------------------	-----------------------	-----------------------------------	------------------------	-------------------------------

SH	ZONE	ITEM	DESCRIPTION
1	GN	2	<p>WAS; NOTE Δ9 TEST ASSEMBLY IN THE FOLLOWING ORDER:</p> <p>A. ULTRASONIC INSPECT BRAZE JOINT PER ATC-STD-4819, TYPE I. ACCEPTANCE PER COGNIZANT DESIGN ACTIVITY.</p> <p>B. PROOF TEST BRAZE JOINT BY FLOWING CLEAN WATER (PER ATC-STD-4940, LEVEL 1000) SIMULTANEOUSLY THRU THE OXIDIZER AND FUEL CIRCUITS TO ATMOSPHERE. HOLD FOR APPROXIMATELY FIVE MINUTES.</p> <p>OXIDIZER CIRCUIT: MANIFOLD P = 750 ±10 PSI; APPROX FLOW = 175 LB/SEC</p> <p>FUEL CIRCUIT: MANIFOLD P = 710 ±10 PSI; APPROX FLOW = 85 LB/SEC</p> <p>C. REPEAT ULTRASONIC INSPECT OF BRAZE JOINT PER ATC-STD-4819, TYPE I. NOTE ANY DIFFERENCES. ACCEPTANCE PER COGNIZANT DESIGN ACTIVITY.</p> <p>D. LEAK TEST ASSEMBLY PER ATC-47063, METHOD II, USING CLEAN DRY NITROGEN AT 50 ±5 PSIA. HOLD FOR 5 MINUTES MINIMUM. NO LEAKAGE ALLOWED.</p> <p>E. FLOW TEST WITH CLEAN WATER (ATC-STD-4940, LEVEL 1000) AS FOLLOWS:</p> <ol style="list-style-type: none"> PERFORM VISUAL PATTERN CHECK PER COGNIZANT DESIGN ACTIVITY. THE OXIDIZER AND FUEL SHALL BE FLOWED SEPARATELY AT THE FOLLOWING FLOW RATES: OXIDIZER: 25, 35, 45, 55, 65; FUEL: 20, 25, 35, 40, 45. FOR EACH DATA POINT RECORD THE MANIFOLD ΔP, FLOWRATE, NOMINAL WATER FLOW TEMPERATURE AND ACTUAL OUTPUT FREQUENCY OF FLOWMETER. CALCULATE K_{ω}: $K_{\omega} = \frac{\dot{w}}{(\Delta P) (Sg)}$ <p>WHERE: \dot{w} = FLOWRATE, LB/SEC ΔP = INLET - OUTLET PRESSURE, PSI Sg = SPECIFIC GRAVITY OF WATER AT FLOW TEMPERATURE</p>

DWG LVL 1	DOCUMENT NUMBER 1206428	REV LTR NC-1
DOCUMENT TITLE INJECTOR CORE ASSY, OX/HC		SHEET 1 OF 3

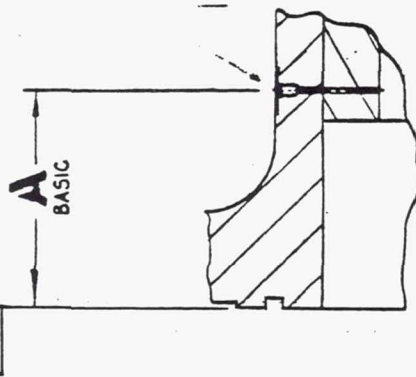
DOCUMENT CHANGE NOTICE
GENCORP TechSystems
 SACRAMENTO, CALIFORNIA
AEROJET

ADCN <input type="checkbox"/> DCN	DATE 91-2-25
TECH NO	RELEASE DATE
PREPARED BY L. MYERS	

APPROVALS	
DESIGN ACTIVITY	CHECK
<i>Steph</i> 15 MAR 91	
MANUF <i>France Myers</i> 91-2-28	
CA	
STRESS	WT
MAT'L	CMO

ADDED;

2 5F 1

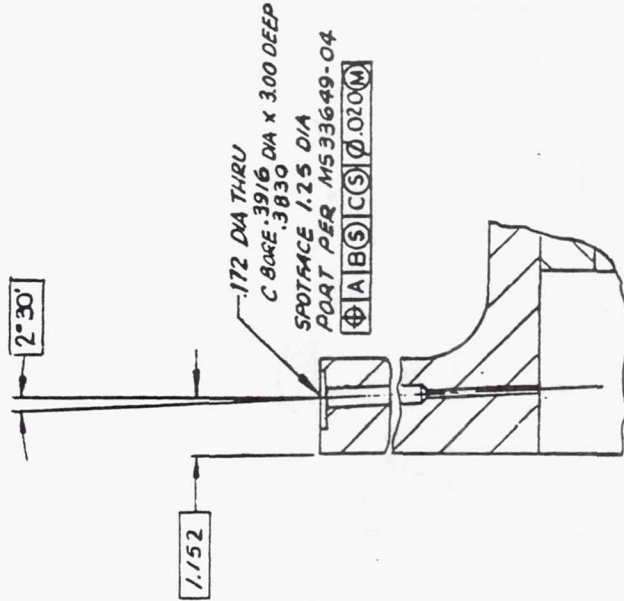


- A -

REMOVED;

2 5C 1

WAS;



SECTION K-K
LOCATED AT 142.500°

SECTION **K-K** 16
LOCATED AT 142.500°

DOCUMENTATION CHANGE NOTICE
CONTINUATION SHEET



TechSystems
SACRAMENTO, CALIFORNIA

FSCM NO. 05824

DATE	91-2-25	DWG LEVEL	1	DOCUMENT NUMBER	1206428	REV/LTR	NC-1	SHEET	3 OF 3
------	---------	-----------	---	-----------------	---------	---------	------	-------	--------

SH	ZONE	ITEM
1	2 A	6

IS;

QTY REQ'D PER ASSY	FSCM/CAGE NO.	PART OR IDENTIFYING NO.	NOMENCLATURE OR DESCRIPTION	MATERIAL SPECIFICATION	ZONE	ITEM NO.
4		NAS334CPA10	BOLT			10
1		-9	ASSY			9
1		1200976-2	RETAINER			8
	AR 00426	RTV GE 627	SILICON SEALANT			7
4		M551937-6C	BOLT, EYE		2 D	6
4		M535691-4I	NUT, HEX		2 C	5
						4
1		1206429-1	INSERT		1 F	3
						2
1		-1	CHAMBER	MAKE FROM 1206432-1	1 F	1
-19						

6

WAS;

QTY REQ'D PER ASSY	FSCM/CAGE NO.	PART OR IDENTIFYING NO.	NOMENCLATURE OR DESCRIPTION	MATERIAL SPECIFICATION	ZONE	ITEM NO.
	AR 00426	RTV GE 560	SILICON SEALANT			7
4		M551937-6C	BOLT, EYE		2 D	6
4		M535691-4I	NUT, HEX		2 C	5
						4
1		1206429-1	INSERT		1 F	3
						2
1		-1	CHAMBER	MAKE FROM 1206432-1	1 F	1
-9						

6

ADCN	<input type="checkbox"/> DCN	DATE	91-2-25	DWG LVL	1	DOCUMENT NUMBER	1200729	REV LTR	A-1
ECHANQ		RELEASE DATE		DOCUMENT TITLE	INJECTOR CORE ASSY, OX/HC				
PREPARED BY		GENCORP TechSystems SACRAMENTO, CALIFORNIA AEROJET							

SH	ZONE	ITEM	DESIGN	DESIGN ACTIVITY	CHECK	STRESS	WT
1	GN	1	<i>J. Myers</i>	<i>91-03-13</i>	<i>15 MAR 91</i>		
			CA	<i>Manuf</i>	<i>Myers</i>		<i>91-3-15</i>

IS; RADIUS THE ORIFICE INLETS USING ONE OF THE **WAS;**

FOLLOWING PROCESS:

A. ELECTROPOLISH INDICATED SIDE USING A SOLUTION OF 50% PHOSPHORIC ACID/50% DEIONIZED WATER AND 100 AMPS/FT² CURRENT. CONTINUE PROCESS UNTIL 0.001-0.0015 INCH RADIUS IS ACHIEVED ON THE ORIFICE INLETS.

B. MICRO BLAST INDICATED SIDE USING 100 MICRON SILICON CARBIDE GLASS BEADS FOR ≈10 SEC. CONTINUE PROCESS UNTIL ALL BURRS ARE REMOVES AND A 0.001-0.0015 INCH RADIUS IS ACHIEVED ON THE ORIFICE INLETS.

ELECTROPOLISH INDICATED SIDE USING A SOLUTION OF 50% PHOSPHORIC ACID/50% DEIONIZED WATER AND 100 AMP/FT² CURRENT. CONTINUE PROCESS UNTIL 0.001-0.0015 INCHES OF MATERIAL IS REMOVED AND ORFICE INLETS HAVE A SLIGHT RADIUS.

ADCN DCN

DATE 2-27-91

RELEASE DATE

PREPARED BY L. MYERS

DOCUMENT CHANGE NOTICE

GENCORP TechSystems
SACRAMENTO, CALIFORNIA

AEROJET

DWG LVL 1

DOCUMENT NUMBER 1200773

REV LTR A-2

DOCUMENT TITLE
INJECTOR FLANGE ASSY,
OXYGEN/HYDROCARBON

SHEET OF 1 2

APPROVALS

DESIGN	CHECK	STRESS	WT
<i>[Signature]</i>	MANUJ	MATL	CMO
DESIGN ACTIVITY <i>[Signature]</i>	2-27-91		
QA			

1 1A 1 IS;

REV	QTY REQD PER ASSY	PCPN NO.	PART OR IDENTIFYING NO.	DESCRIPTION	MATERIAL SPECIFICATION	ZONE	ITEM NO.
1	1		-39	ASSY			12
1	1		-8	BOSS	QQ-S-763 CL 304 COND A		11
AR	AR			WELD ROD	AWS A5.9		10
	1		-9	ASSY			9
AR	AR			WELD ROD	AWS A5.9		8
	1	14713	52823	BUTT WELD HUB	2" GR 20 SCH 160 SA182-F316		7
	1		-4	TUBE	ASTM-A312 TYPE 304		6
	1		-3	BOSS	QQ-S-763 CL304 CONDA		5
	1		-6	OUTER RING	CRES		4
	1		-5	INNER RING	CRES ASTM A473 OR ASTM A167		3
	1		-2	OUTER RING	ASTM A473 OR ASTM A167		2
	1		-1	INNER RING	ASTM A473 OR ASTM A167		1
49-39	29-19-9			NUMERATURE OR DESCRIPTION	MATERIAL SPECIFICATION	ZONE	ITEM NO.

PARTS LIST

DOCUMENTATION CHANGE NOTICE
CONTINUATION SHEET

<input checked="" type="checkbox"/> ADCN	<input type="checkbox"/> DCN	DATE	2-27-91	DWG LEVEL	1	DOCUMENT NUMBER	1200773	REV LTR	A-2	SHEET	2 OF 2
--	------------------------------	------	---------	-----------	---	-----------------	---------	---------	-----	-------	--------

SH	ZONE	ITEM										
1	1A	1	WAS;									

QTY REQD PER ASSY	PCDN NO.	PART OR IDENTIFYING NO.	NOMENCLATURE OR DESCRIPTION	MATERIAL SPECIFICATION	ZONE	ITEM NO.
1			WELD ROD	ER316	AW5 A5.9	10
1		-9	ASSY			4
AR	AR		WELD ROD	ER308	AIVS A5.9	8
	1	14713	BUTT WELD HUB	2"GR 20 SCH 160	SA182-F316	7
	1	-4	TUBE	2.0 SCHED 160 CRES PIPE	ASTM-A312 TYPE 304	6
	1	-3	BOSS	CRES	QQ-S-763 CL304 CONDA	5
	1	-6	OUTER RING	CRES	ASTM A473 OR TYPE 304	4
	1	-5	INNER RING	CRES	ASTM A473 OR TYPE 304	3
	1	-2	OUTER RING	CRES	ASTM A473 OR TYPE 304	2
	1	-1	INNER RING	CRES	ASTM A473 OR TYPE 304	1
29	19	-9	PARTS LIST			

APPENDIX F
NONCONFORMANCE REPORTS

NONCONFORMANCE REPORT

G.F.M. NO. V21175

PAGE 1 OF 1

1. PART NUMBER 1206432	2. NOMENCLATURE Forging- Chamber Body	3. SERIAL NO. N/A	4. PROGRAM	5. LOT SIZE 1	6. ACC.	7. DISC.
8. WORK ORDER KFN 600	9. SHOP ORDER N/A	10. OPER. NO. / 11. SUPPLIER NAME N/A / Viking Metallurgical	12. P.O. NUMBER L823696H	13. DISTRIBUTION NO. N/A	PREVIOUS NR NUMBER N/A	
14. NONCONFORMANCE						
(A) DWG. ZONE, SPEC. PARA., SHOP ORDER OPER., ETC AS APPLICABLE (B) STATE REQUIREMENT (C) INSPECTION RESULTS						
15. DISPOSITION/COMMENTS ITEMS <input type="checkbox"/> MRB <input type="checkbox"/> ERB (A) CAUSE C/C (B) FREQ. OCCUR. (C) DISC.						
B/P note 5 requires ultrasonic inspection to ATC- STD-4819 with acceptance to ATC-Std 4006 Class II. Forging is rejected to Class II and Class III. Forging is acceptable to Class IV.						
Accept As Is providing the forging will meet Ultrasonic Inspection per ATC-STD-4819 with acceptance to ATC-STD-4006 Class IV. Also, provide all available records substantiating the material meets MIL-S-5000E requirements.						
23. CAUSE The heat of 4340AQ used was not adequate for Class II sonic requirement.						
24. CORRECTIVE ACTION Purchase better quality steel; - Next Purchase Order.						
25. EFFECTIVITY: (DATE/SERIAL NUMBER/ETC.)						

17. REVIEWER IDENTITY <i>[Signature]</i>	18. REVIEW DATE 10-29-90	19. REVIEW BY <i>[Signature]</i>	20. REINSPECT DATE 10/11/90	21. MRB/ENB APPROVALS DATE 10-29-90 <i>[Signature]</i>	22. MRB/ENB RESUBMIT DECISIONS DATE 10-16-90 <i>[Signature]</i>	23. MRB/ENB RESUBMIT DATE 10-16-90
24. CORRECTIVE ACTION Purchase better quality steel; - Next Purchase Order.			25. EFFECTIVITY: (DATE/SERIAL NUMBER/ETC.)			

DISCR. PART MATERIAL DISPOSITION	RESPONSIBILITY: <input type="checkbox"/> GM <input type="checkbox"/> ATC <input type="checkbox"/> SUPPLIER	R/S	SHIPPER NO.	SALVAGE	PROC/MFG/ILS REPR	DATE	QA REPR	DATE
NO. V21175								

PRINT OR TYPE IN BLACK INK

NONCONFORMANCE REPORT

G.F.M.

NO. **V21264**

PAGE 1 OF

1. PART NUMBER 1206429		3. SERIAL NO. 2873-1-001		4. PROGRAM 182386SH		5. LOT SIZE 1		6. ACC. D		7. DISC. 1	
2. NOMENCLATURE INSERT THRUST CHAMBER		10. OPER. NO. AAE		11. SUPPLIER NAME AAE		12. P.O. NUMBER 182386SH		13. DISTRIBUTION NO.		16. DISPOSITION/COMMENTS ITEMS	
8. WORK ORDER		9. SHOP ORDER		14. NONCONFORMANCE		15. (A) CAUSE C/C (B) FREQ. OCCUR		17. INITIAL IDENTITY		18. REVIEWED	
AREA: Supplier		REV. M/C		19. DWG. ZONE, SPEC., PARA., SHOP ORDER OPER., ETC. AS APPLICABLE		20. MBR/ERB APPROVALS		21. MBR/ERB APPROVALS		22. MBR/ERB RESUBMIT DECISIONS	
1. RESIN CONTENT 31±4% is		2. 36.83 FWD		3. 36.61 AFT		4. 1-14-91		5. 1-14-91		6. 1-14-91	
16. DISPOSITION/COMMENTS ITEMS		17. INITIAL IDENTITY		18. REVIEWED		19. DWG. ZONE, SPEC., PARA., SHOP ORDER OPER., ETC. AS APPLICABLE		20. MBR/ERB APPROVALS		21. MBR/ERB RESUBMIT DECISIONS	
Us As Is; the higher resin content will not affect the performance of the liner in the hot fire environment.		DATE (A REPR.)		DATE (CUST REPR.)		DATE (CUST REPR.)		DATE (CUST REPR.)		DATE (CUST REPR.)	
23. CAUSE		24. CORRECTIVE ACTION		25. EFFECTIVITY: (DATE/SERIAL NUMBER/ETC.)		26. MBR/ERB RESUBMIT DECISIONS		27. MBR/ERB RESUBMIT DECISIONS		28. MBR/ERB RESUBMIT DECISIONS	
BROWN METHOD FOR SILICA PHENOLIC MATERIALS HISTORICALLY HAS BEEN HIGHER THAN THE RAW MATERIAL CERTIFICATIONS. IN THIS CASE THE FIBERITE CERT REPORT 32% ALSO THE REQ'D CURE CYCLE REDUCES RESIN FLOW DURING CURE		RAISE PART RESIN CONTENT LIMITS, OR PROCURE MX2600 WITH A LOWER RESIN CONTENT WHICH WOULD NOT BE THEIR STANDARD PRODUCT.		DATE		DATE		DATE		DATE	
DISCREPANT MATERIAL DISPOSITION		RESPONSIBILITY: <input type="checkbox"/> CFM <input type="checkbox"/> GJT <input type="checkbox"/> RTS		SHIPPER NO		SALVAGE		PHOC-M G-I-L-S III PH		DATE	
RESIN FLOW DURING CURE		DATE		DATE		DATE		DATE		DATE	



PRINT OR TYPE IN BLACK INK

NONCONFORMANCE REPORT

G.F.M.

NO. Y2204

PAGE 1 OF 1

1. PART NUMBER 1200729	DASH REV. -1 A	2. NOMENCLATURE INJECTOR CORE	3. SERIAL NO.	4. PROGRAM 3D SUBSCALE	5. LOT SIZE 1	6. ACC.	7. DISC.
8. WORK ORDER S/O 4444	9. SHOP ORDER S/O 4444	10. OPER. NO. MARTINEZ & TUREK	NUMBER	12. P.O. NUMBER L823839	13. DISTRIBUTION NO.	PREVIOUS NR NUMBER	
ITEM	14. NONCONFORMANCE (A) DWG. ZONE, SPEC., PARA., SHOP ORDER OPER., ETC AS APPLICABLE (B) STATE REQUIREMENT (C) INSPECTION RESULTS		15 (A) CAUSE (B) FREQ (C) OCCUR	<input type="checkbox"/> MPB ITEMS	16. DISPOSITION/COMMENTS <input type="checkbox"/> EFB ITEMS		
1	REF. DWG. SHEET 4/7, ZONE: F-8 SHOULD BE: $\phi 11.336 \pm .000$ IS: $\phi 11.331$ at 68° F			Us As Is; the smaller diametrical dimension will not affect the assembly nor will it jeopardize the seal of the o-ring.			
2	REF. DWG SHEET 3/7, ZONE: A-3 SHOULD BE: $.022 \pm .001$ @ 8 places, (BRAZE CHANNEL DEPTH) IS: ACCEPTABLE AT (7) LOCATIONS, (1) LOCATION ($\phi 1.888$) FOUND TO BE .024" DEEP.			Us As Is; the difference of .001" in channel depth will not change the flow characteristics to detriment the hardware performance.			
17. INITIATOR IDENTITY S. NICKERSON	DATE 18 REVIEWED BY <i>S. Nickerson 9/19/91</i>	DATE 19 <i>9/19/91</i>	DATE 20 <i>1/25/91</i>	QTY	ACC.	DISC.	INSPECTOR
DATE 18 <i>2-1-91</i>	DATE 19 <i>2-1-91</i>	DATE 20 <i>1/25/91</i>	DATE 21 <i>1/23/91</i>	DATE 22 <i>1/23/91</i>	DATE 23 <i>1/23/91</i>	DATE 24 <i>1/23/91</i>	DATE 25 <i>1/23/91</i>
23. CAUSE Items 1&2: OPERATOR ERROR							
24. CORRECTIVE ACTION OPERATOR HAD PROPER INSTRUCTIONS AND DID NOT FOLLOW. THIS OPERATOR HAS BEEN COUNSELED ON CRITICAL NATURE OF THIS ASSEMBLY. VERBAL WARNING ISSUED.							
25. EFFECTIVITY: (DATE/SERIAL NUMBER/ETC.) 1/23/91							
DISCREPANT MATERIAL DISPOSITION	RESPONSIBILITY: <input type="checkbox"/> SUPPLIER <input type="checkbox"/> GM <input type="checkbox"/> ATC	IRTS	SHIPPER NO.	SALVAGE	PROC/MFG-ILS REPR.	DATE <i>1/23/91</i>	NO.



NONCONFORMANCE REPORT

PRINT OR TYPE IN BLACK INK

G.F.M. NO. V21221

PAGE 1 OF 2

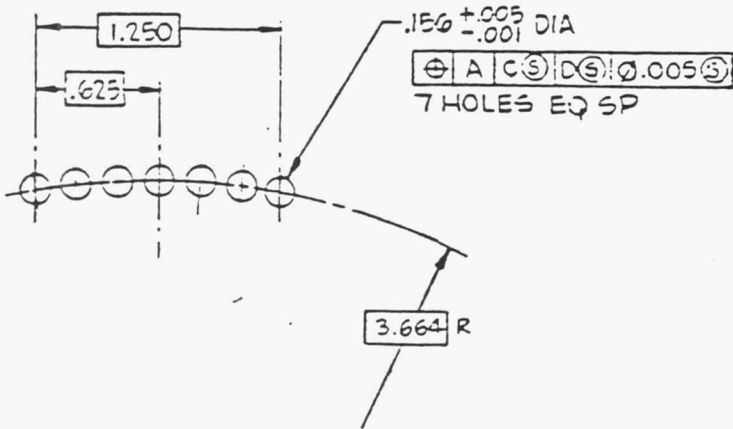
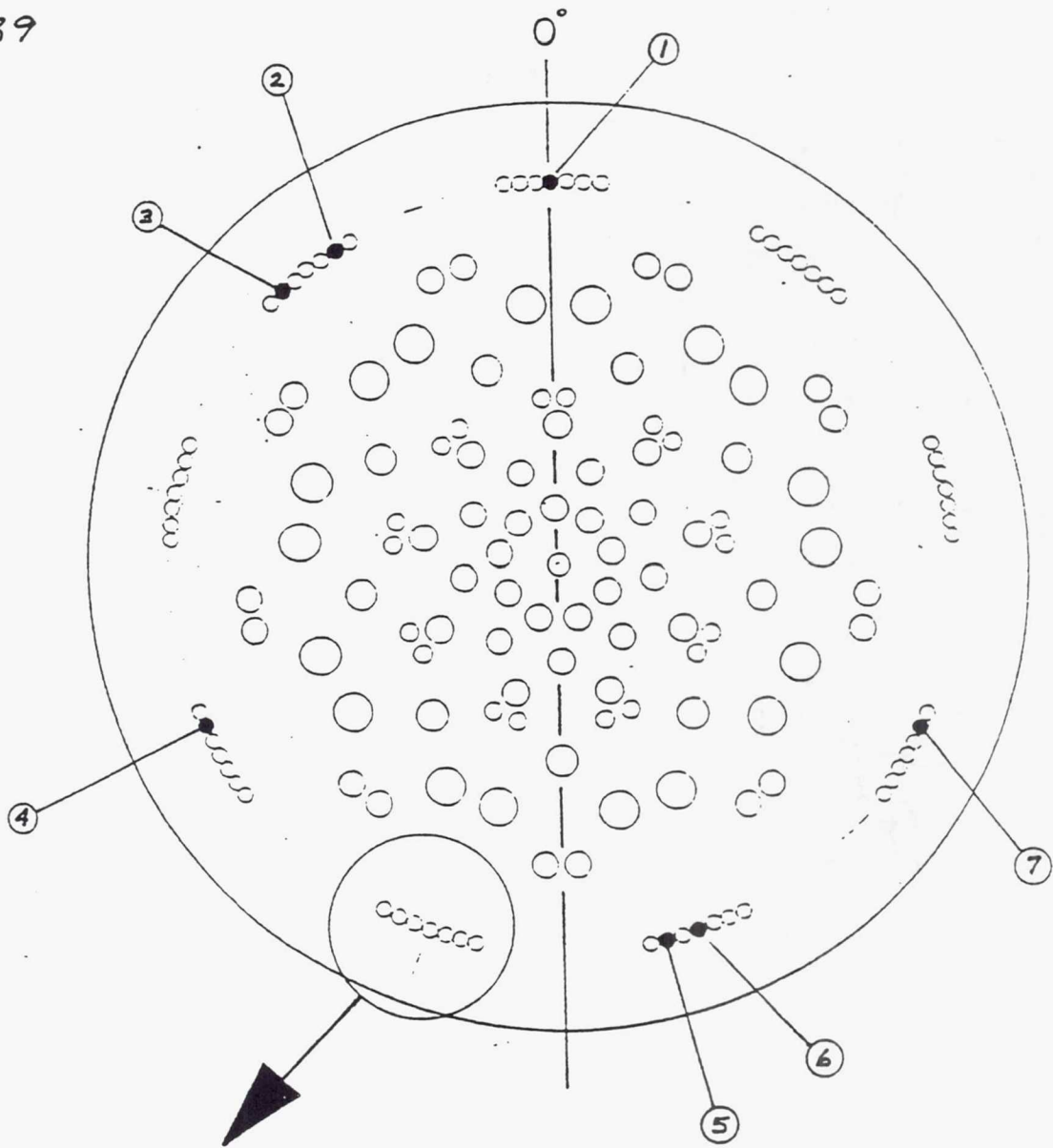
1. PART NUMBER 1200729	DASH -1	2. NOMENCLATURE INJECTOR CORE	3. SERIAL NO.	4. PROGRAM	5. LOT SIZE 1	6. ACC.	7. DISC.
8. WORK ORDER KFN 600		9. SHOP ORDER S/O 4444		10. OPER NO. MARTINEZ & TUREK		11. SUPPLIER NAME MARTINEZ & TUREK	
14. NONCONFORMANCE		15. (A) CAUSE (B) FREQ (C) OCCUR		16. DISPOSITION/COMMENTS		17. PREVIOUS NR NUMBER	
1. REF: DWG. SHEET -4, Zone: D-5		Should be: $\varnothing .156 \pm .005$		Accept as is providing all metal chips have been		deburred so there will be nothing dislodged during testing.	
IS: True position varies up to .020.		(See Attached for Discrepant locations) 7 pls.		9 Equal Spaces			
17. INITIATOR/IDENTITY		DATE 18. REVIEW		DATE 19. APPROVALS		DATE 20. RESPECT	
G.F.M.		11-12-90		11-12-90		11/8/90	
DATE 21. MRB/ERB APPROVALS		DATE 22. MRB/ERB RESUBMIT DECISIONS		DATE 23. CORRECTIVE ACTION		DATE 24. CORRECTIVE ACTION	
11/8/91		11/8/91		24. CORRECTIVE ACTION		24. CORRECTIVE ACTION	
23. CAUSE		23. CAUSE		23. CAUSE		23. CAUSE	
Due to the length of the drill is required to complete this configuration (Approx. 5" Long) Deflection occurred thus causing drilled hole to be off location.		Operator has been instructed to pilot drill holes first and then bore to size.					
DISCREPANT MATERIAL DISPOSITION		RESPONSIBILITY		EFFECTIVITY: (DATE/SERIAL NUMBER ETC.)		RESUBMIT FOR	
SUPPLIER		CITY		DATE		DATE	
SALVAGE		PHCC-MFG/US/REP		DATE		DATE	
NO.		NO.		NO.		NO.	

ATC PN# 1200729

√2/221

-1 INJECTOR CORE

P.O.# LB23839



HOLE NO. #	TRUE POSITION
1	.006
2	.020
3	.006
4	.006
5	.012
6	.007
7	.0085

VIEW S 4/2
4/6
9 PL THRU EQ SP
SCALE: 2/1

REPORT DOCUMENTATION PAGE

Form Approved
OMB No. 0704-0188

Public reporting burden for this collection of information is estimated to average 1 hour per response, including the time for reviewing instructions, searching existing data sources, gathering and maintaining the data needed, and completing and reviewing the collection of information. Send comments regarding this burden estimate or any other aspect of this collection of information, including suggestions for reducing this burden, to Washington Headquarters Services, Directorate for Information Operations and Reports, 1215 Jefferson Davis Highway, Suite 1204, Arlington, VA 22202-4302, and to the Office of Management and Budget, Paperwork Reduction Project (0704-0188), Washington, DC 20503.

1. AGENCY USE ONLY (Leave blank)	2. REPORT DATE May 1993	3. REPORT TYPE AND DATES COVERED Final Contractor Report	
4. TITLE AND SUBTITLE LOX/Hydrocarbon Rocket Engine Analytical Design Methodology Development and Validation		5. FUNDING NUMBERS WU-590-21-21 C-NAS3-25556	
6. AUTHOR(S) Karen E. Niiya and Richard E. Walker			
7. PERFORMING ORGANIZATION NAME(S) AND ADDRESS(ES) Aerojet Propulsion Division P.O. Box 13222 Sacramento, California 95813		8. PERFORMING ORGANIZATION REPORT NUMBER E-7827	
9. SPONSORING/MONITORING AGENCY NAME(S) AND ADDRESS(ES) National Aeronautics and Space Administration Lewis Research Center Cleveland, Ohio 44135-3191		10. SPONSORING/MONITORING AGENCY REPORT NUMBER NASA CR-191059	
11. SUPPLEMENTARY NOTES Project Manager, Mark D. Klem, Space Propulsion Technology Division, (216) 977-7473.			
12a. DISTRIBUTION/AVAILABILITY STATEMENT Unclassified - Unlimited Subject Category 20		12b. DISTRIBUTION CODE	
13. ABSTRACT (Maximum 200 words) <p>This final report includes a discussion of the work accomplished on contract NAS 3-25556 during the period from December 1988 through November 1991. The objective of the program was to assemble existing performance and combustion stability models into a usable design methodology capable of designing and analyzing high-performance and stable LOX/Hydrocarbon booster engines. The methodology was then used to design a validation engine. The capabilities and validity of the methodology were demonstrated using this engine in an extensive hot fire test program. The engine used LOX/RP-1 propellants and was tested over a range of mixture ratios, chamber pressures and acoustic damping device configurations. This volume contains time domain and frequency domain stability plots which indicate the pressure perturbation amplitudes and frequencies from approximately 30 tests of a 50K thrust rocket engine using LOX/RP-1 propellants over a range of chamber pressures from 240 to 1750 psia with mixture ratios of from 1.2 to 7.5. The data is from test configurations which used both bitune and monotune acoustic cavities and from tests with no acoustic cavities. The engine had a length of 14 inches and a contraction ratio of 2.0 using a 7.68 inch diameter injector. The data was taken from both stable and unstable tests. All combustion instabilities were spontaneous in the first tangential mode. Although stability bombs were used and generated over pressures of approximately 20%, no tests were driven unstable by the bombs. The stability instrumentation included six high-frequency Kistler transducers in the combustion chamber, a high-frequency Kistler transducer in each propellant manifold, and tri-axial accelerometers. Performance data is presented, both characteristic velocity efficiencies and energy release efficiencies, for those tests of sufficient duration to record steady state values.</p>			
14. SUBJECT TERMS Combustion stability; Combustion efficiency; Rocket engine design; Combustion chambers; Rocket thrust chambers; Design analysis; Injectors		15. NUMBER OF PAGES 160	
		16. PRICE CODE A08	
17. SECURITY CLASSIFICATION OF REPORT Unclassified	18. SECURITY CLASSIFICATION OF THIS PAGE Unclassified	19. SECURITY CLASSIFICATION OF ABSTRACT Unclassified	20. LIMITATION OF ABSTRACT