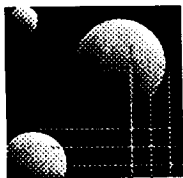


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INHIBITING MULTIPLE MODE VIBRATION IN CONTROLLED FLEXIBLE SYSTEMS

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Kenneth W. Chang
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July 1, 1991

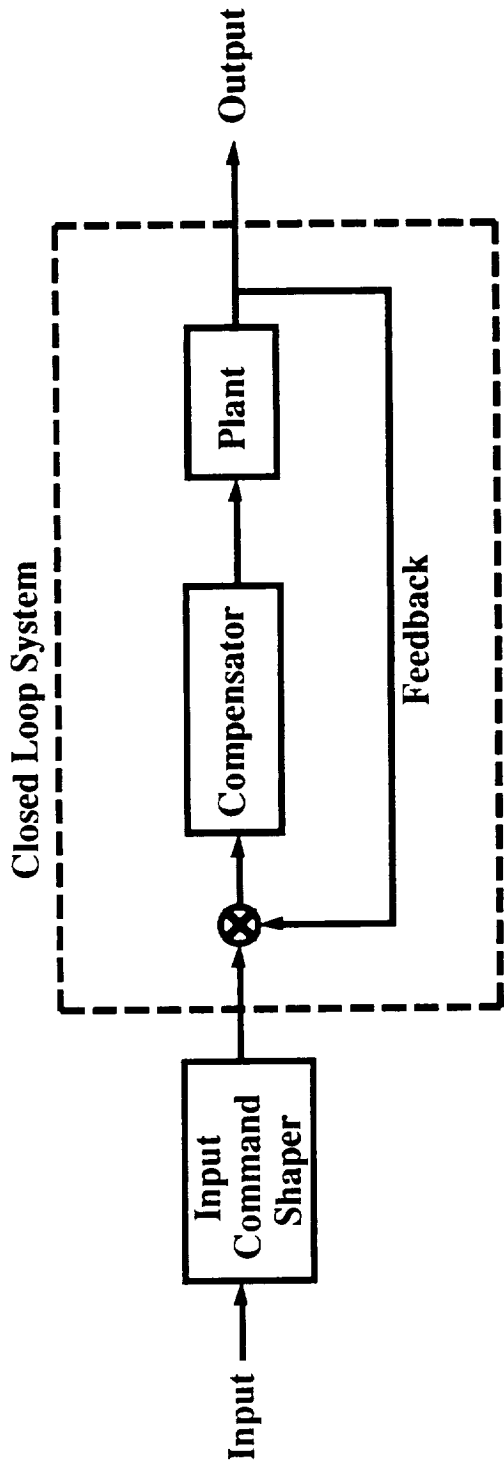
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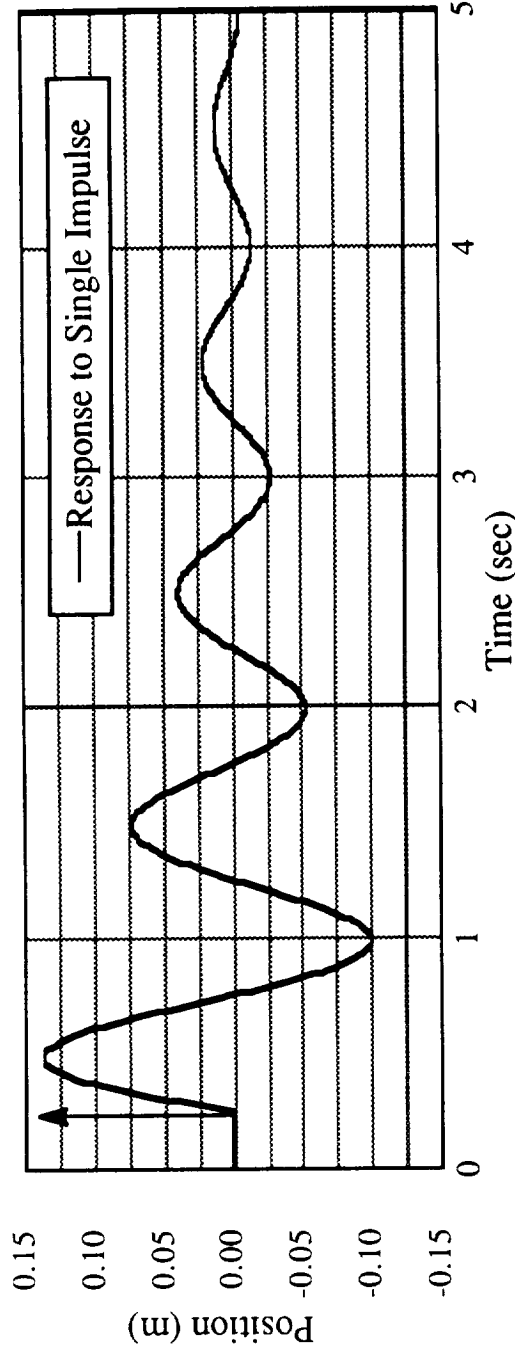
OUTLINE

- Input Pre-Shaping Background
- Developing Multiple-Mode Shapers
- The MACE Test Article
- Tests and Results

SHAPER POSITION IN CONTROL SYSTEM



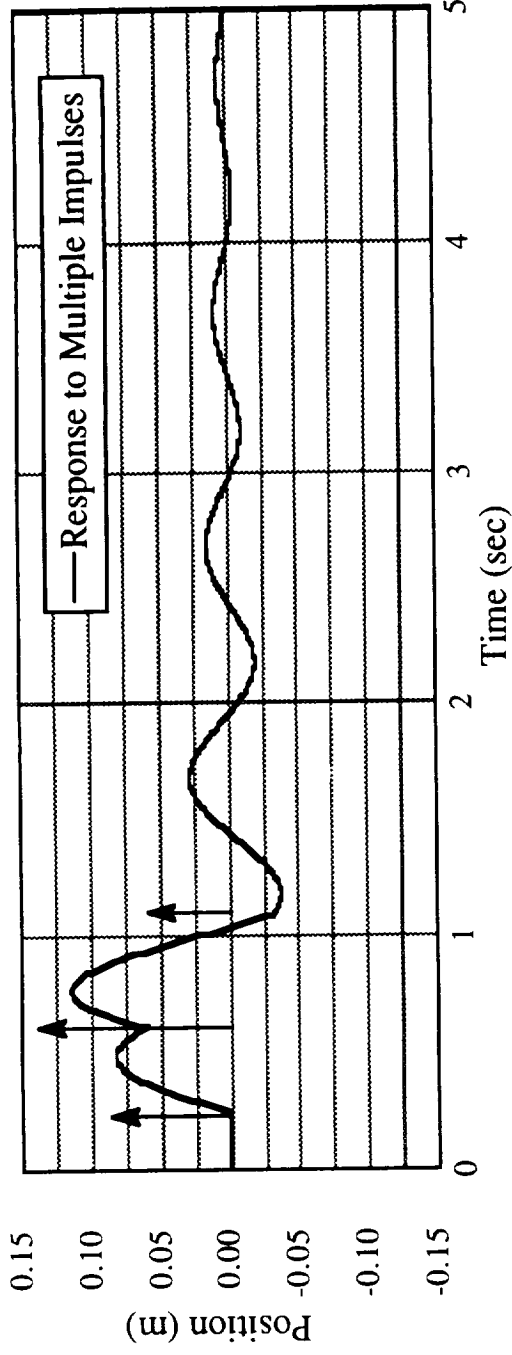
LINEAR SYSTEM IMPULSE RESPONSE



$$y_i(t) = A_i e^{-\zeta \omega (t - t_i)} \sin(\omega \sqrt{1 - \zeta^2} (t - t_i))$$

y_i	Response to Impulse i
A_i	Magnitude of Impulse i
t_i	Time of Impulse i
ω	System Natural Frequency
ζ	System Damping Ratio

RESPONSE TO "N" IMPULSES



$$y_i(t) = \sum_{i=1}^N A_i e^{-\zeta \omega (t - t_i)} \sin((t - t_i) \omega \sqrt{1 - \zeta^2})$$

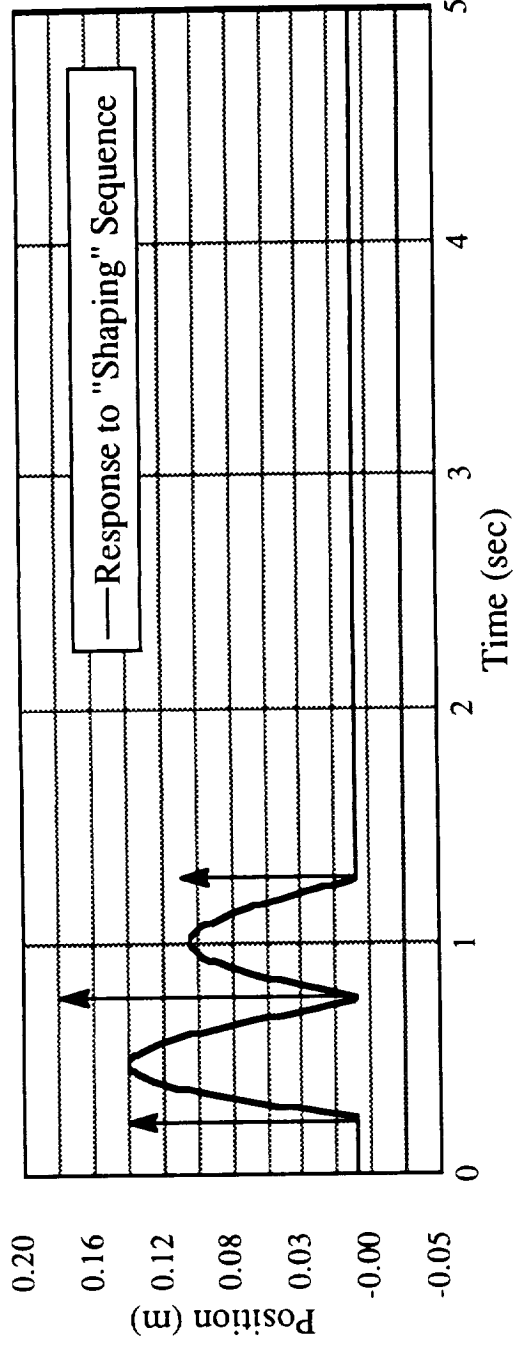
i Impulse Counter
 N Number of Impulses

AMPLITUDE OF THE MULTIPLE-IMPULSE RESPONSE ENVELOPE

$$\text{Amp} = \left[\left(\sum_{i=1}^N A_i e^{-\zeta \omega (t_N - t_i)} \sin(t_i \omega \sqrt{1 - \zeta^2}) \right)^2 + \left(\sum_{i=1}^N A_i e^{-\zeta \omega (t_N - t_i)} \cos(t_i \omega \sqrt{1 - \zeta^2}) \right)^2 \right]^{1/2}$$

Expression for envelope amplitude at t_N ,
the time of the final impulse.

ELIMINATING RESIDUAL VIBRATION



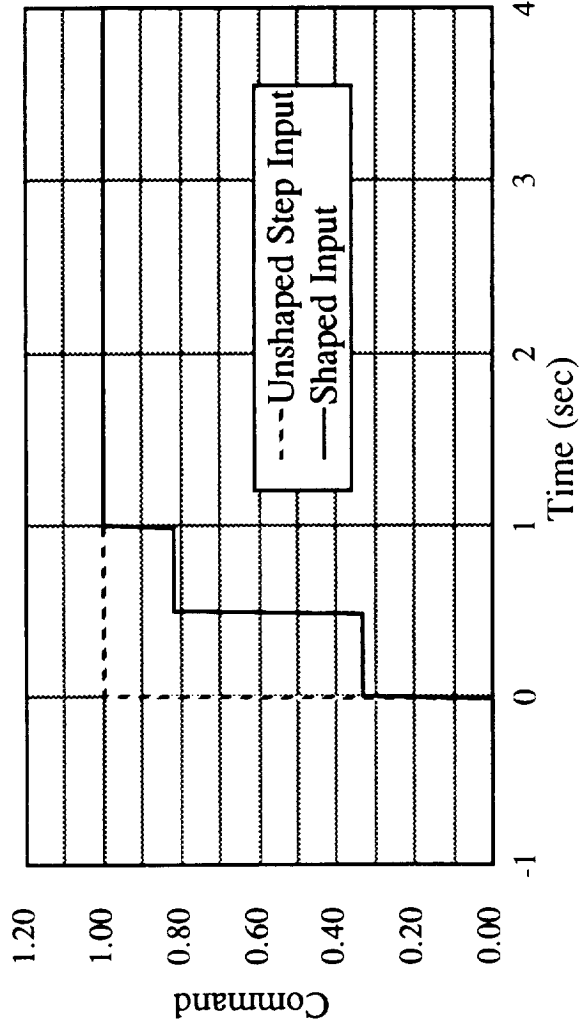
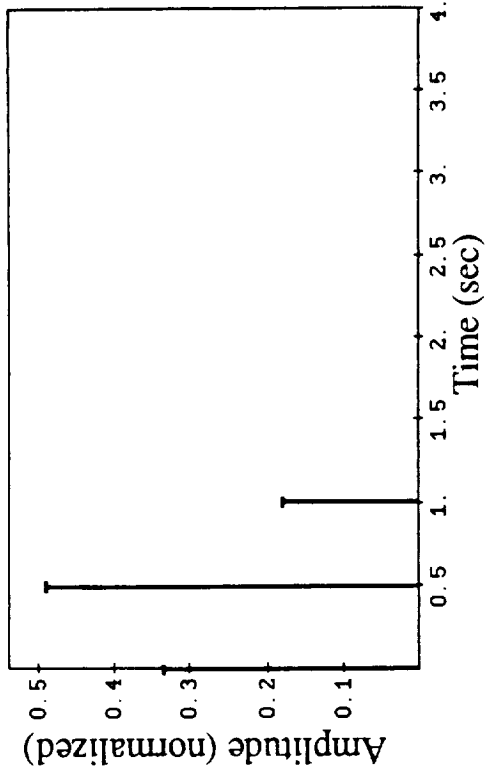
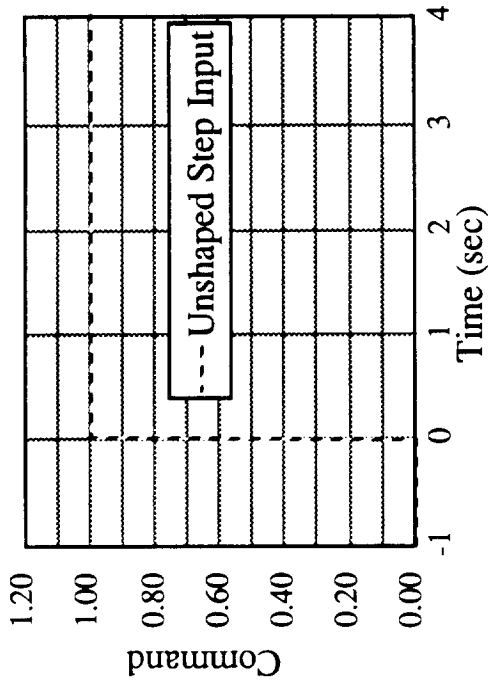
$$\sum_{i=1}^N A_i e^{-\zeta \omega t_i} \sin(t_i \omega \sqrt{1 - \zeta^2}) = 0$$

$$\sum_{i=1}^N A_i t_i e^{-\zeta \omega t_i} \sin(t_i \omega \sqrt{1 - \zeta^2}) = 0$$

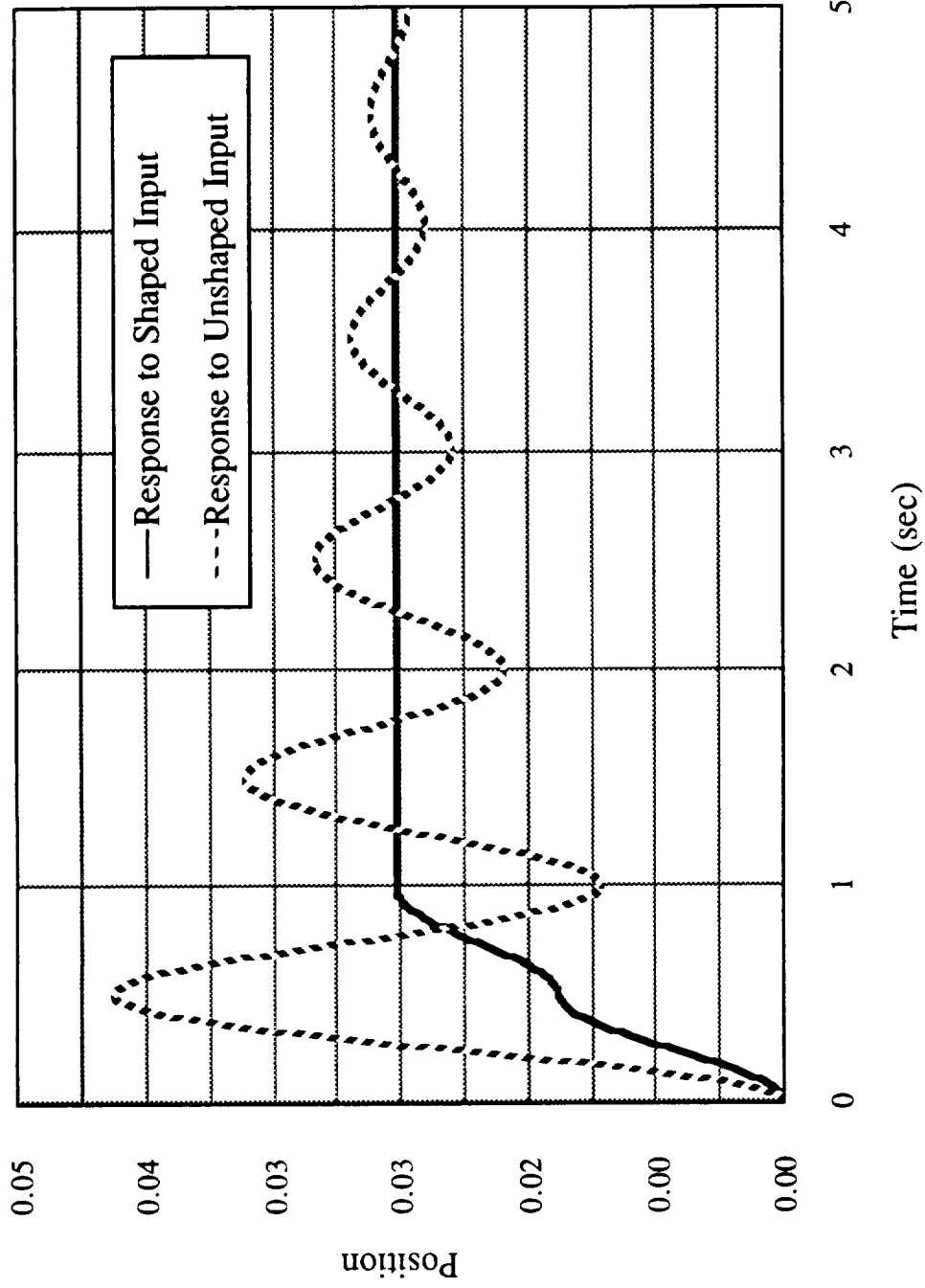
$$\sum_{i=1}^N A_i e^{-\zeta \omega t_i} \cos(t_i \omega \sqrt{1 - \zeta^2}) = 0$$

$$\sum_{i=1}^N A_i t_i e^{-\zeta \omega t_i} \cos(t_i \omega \sqrt{1 - \zeta^2}) = 0$$

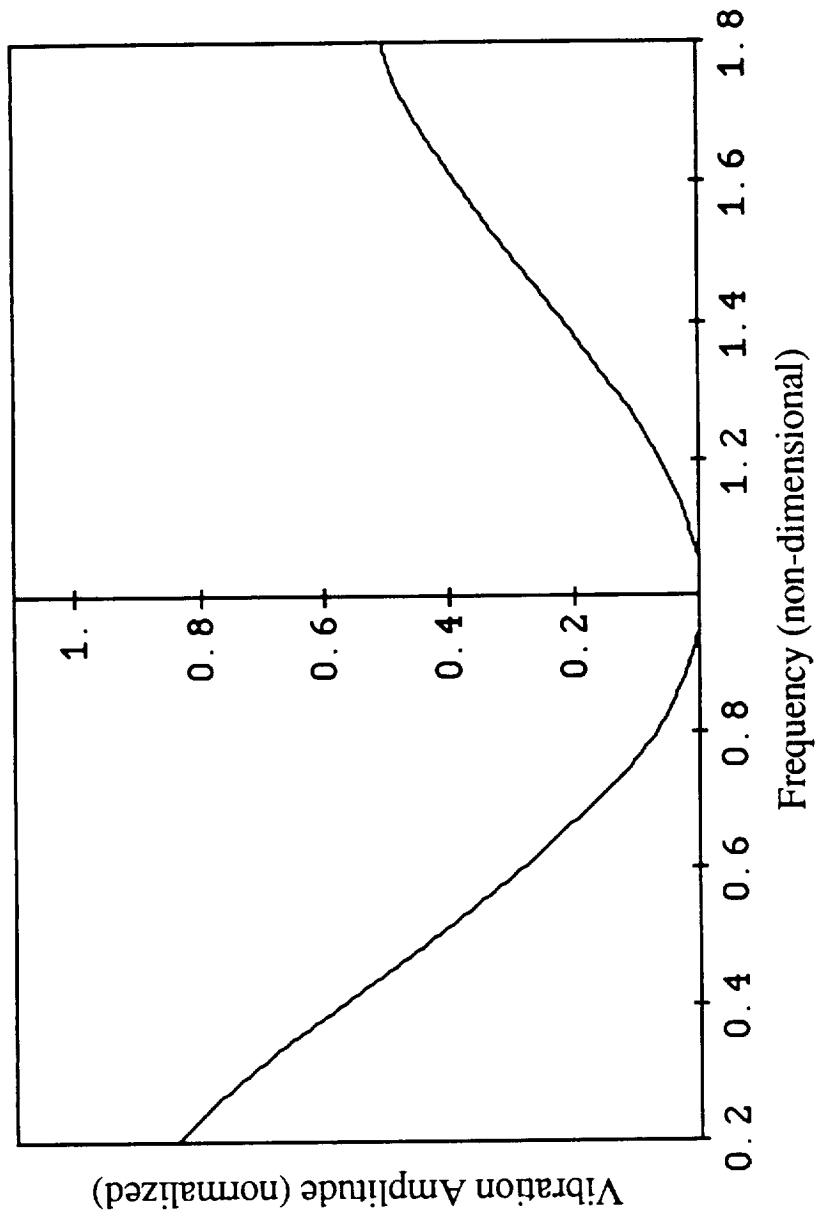
USING THE IMPULSE SEQUENCE



RESPONSE TO INPUTS

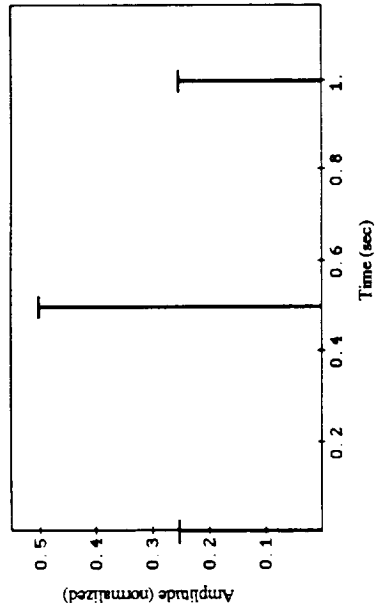


INSENSITIVITY OF THREE-IMPULSE SEQUENCE

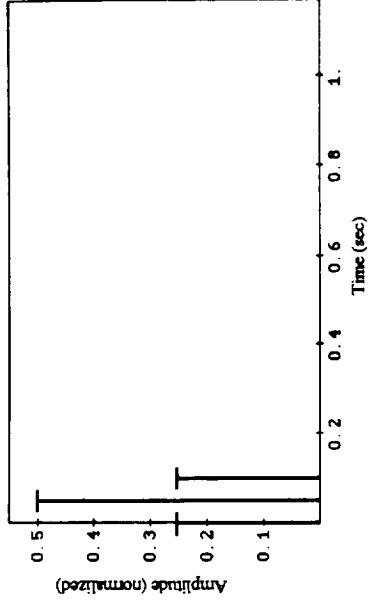


EXTENDING TO MULTIPLE MODE PROBLEMS

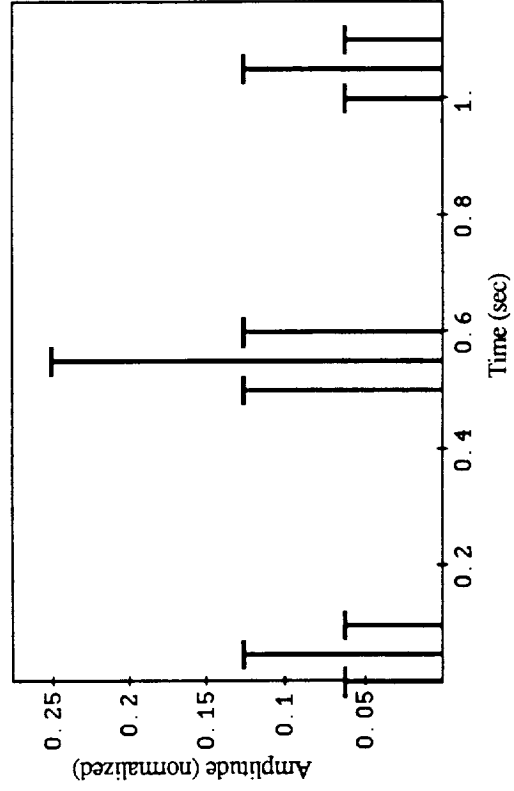
CONVOLUTION



1 Hz Shaper

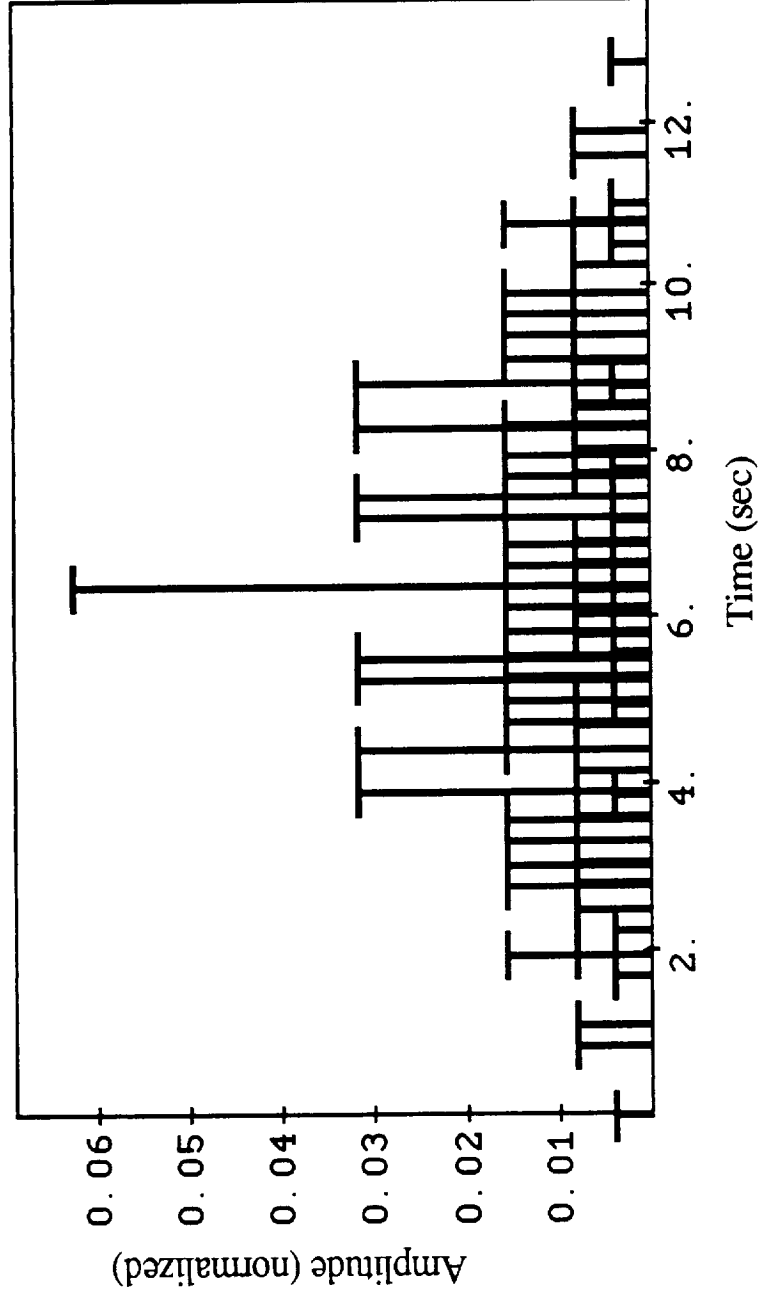


10 Hz Shaper



Convolved Shaper

CONVOLUTION SEQUENCE PROBLEMS



$$\omega_1 = 0.20 \text{ Hz} \quad \omega_2 = 0.26 \text{ Hz}$$

$$\omega_3 = 0.45 \text{ Hz} \quad \omega_4 = 0.59 \text{ Hz}$$

DIRECT SOLUTION CONSTRAINT EQUATIONS

$$\sum_{i=1}^N A_i e^{-\zeta_j \omega_j t_i} \sin(t_i \omega_j \sqrt{1 - \zeta_j^2}) = 0$$

$$\sum_{i=1}^N A_i e^{-\zeta_j \omega_j t_i} \cos(t_i \omega_j \sqrt{1 - \zeta_j^2}) = 0$$

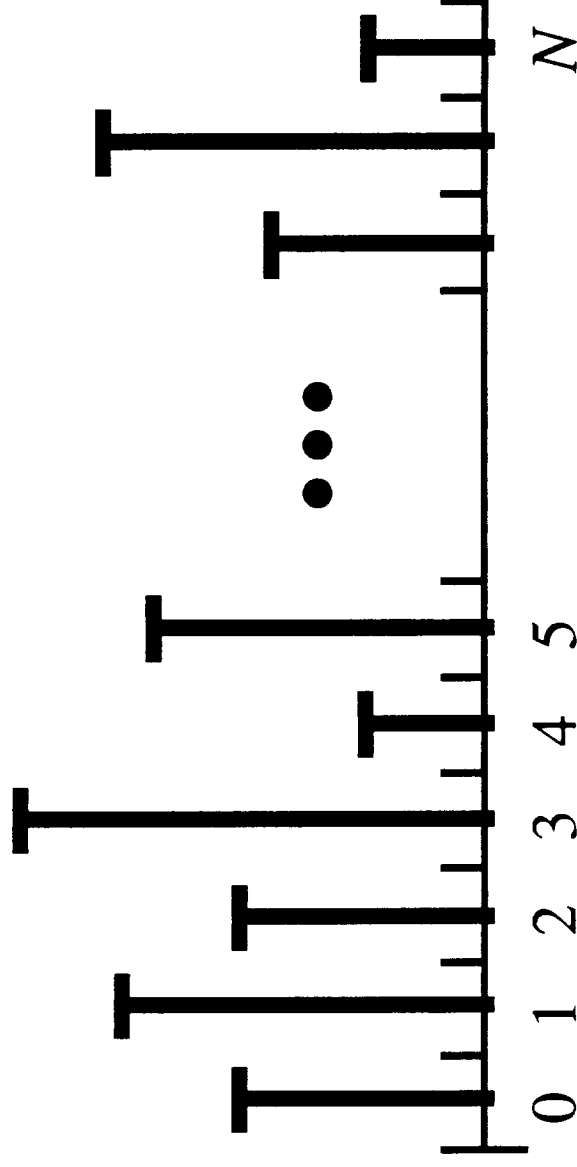
$$\sum_{i=1}^N A_i t_i e^{-\zeta_j \omega_j t_i} \sin(t_i \omega_j \sqrt{1 - \zeta_j^2}) = 0$$

$$\sum_{i=1}^N A_i t_i e^{-\zeta_j \omega_j t_i} \cos(t_i \omega_j \sqrt{1 - \zeta_j^2}) = 0$$

These four equations are repeated for each mode "j"

LINEARIZING THE EQUATIONS

Define time mesh with N slots



Impulse times (t_i): Known

Impulse amplitudes (A_i): Unknown

COST FUNCTION

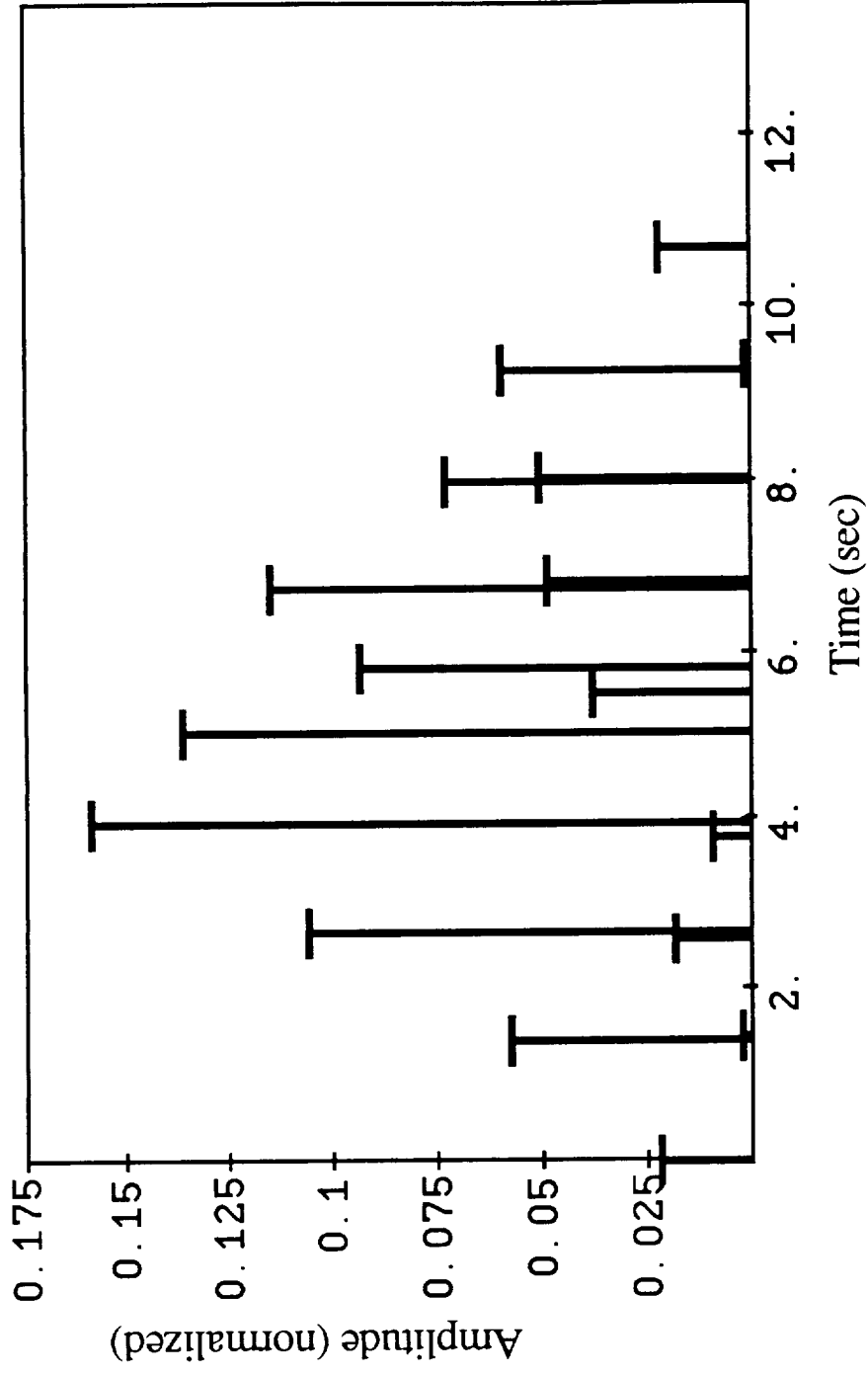
$$Cost = \sum_{j=1}^M \left[\left(\sum_{i=1}^N A_i t_i^2 e^{-\zeta_j \omega_j t_i} \sin(t_i \omega_j \sqrt{1 - \zeta_j^2}) \right)^2 + \right.$$

$$\left. \left(\sum_{i=1}^N A_i t_i^2 e^{-\zeta_j \omega_j t_i} \cos(t_i \omega_j \sqrt{1 - \zeta_j^2}) \right)^2 \right]$$

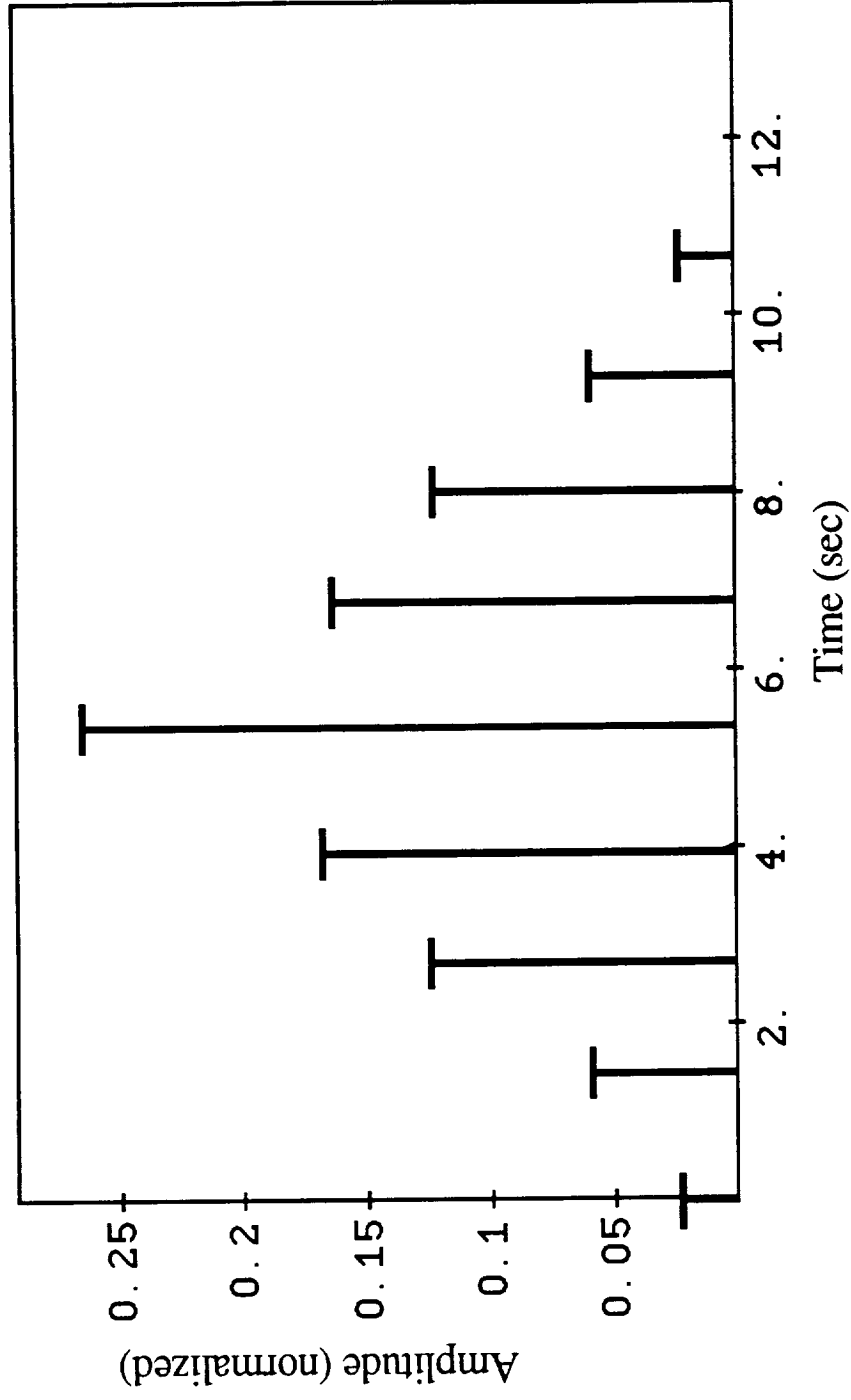
M Number of modes

j Modal index

LINEAR APPROXIMATION SEQUENCE



INTERPRETED LINEAR SEQUENCE



EXACT DIRECT SOLUTION SEQUENCE

