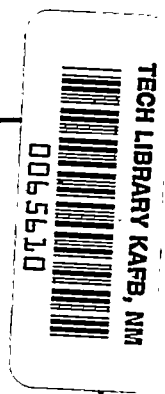


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# NATIONAL ADVISORY COMMITTEE FOR AERONAUTICS

TECHNICAL NOTE 2451

MATHEMATICAL IMPROVEMENT OF METHOD FOR COMPUTING POISSON  
INTEGRALS INVOLVED IN DETERMINATION OF VELOCITY  
DISTRIBUTION ON AIRFOILS

By I. Flügge-Lotz  
Stanford University



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## MATHEMATICAL IMPROVEMENT OF METHOD FOR COMPUTING POISSON

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## SUMMARY

The Poisson integral involved in the determination of the change in velocity distribution resulting from a change in airfoil profile in parallel incompressible flow is solved.

First, three well-developed numerical methods of evaluating this integral, all based on the division of the range of integration into small equal intervals, and the difficulties involved in each method, are discussed. Then a new method, based on the use of unequal intervals, is developed, and compared with the other methods by means of several examples. The new method is found to give good results for both the direct and inverse airfoil problems and is easily adaptable to rather complicated problems. It is particularly recommended for all those functions where steep slopes in small portions of the region to be integrated exist.

## INTRODUCTION

The ordinary thin airfoil at small angles of attack produces only slight disturbances in the flow of a parallel incompressible fluid. Hence, the influences of camber and thickness upon the velocity distribution may be computed independently and their effects superimposed. The effect of camber may be represented by vortices distributed along the chord line of the airfoil section; the effect of the thickness, by sources and sinks also along the same chord line. The velocities produced by these singularity distributions enable one to compute the pressure distribution on the airfoil rather quickly.

Allen (reference 1) has presented this singularity method in a form which has proved to be very practical for common usage. However, in special cases the unavoidable evaluation of the Poisson integral in

the course of the computations has given rise to numerical difficulties. Such integrals are usually computed by the application of finite differences using intervals of equal length. However, changes in airfoil shape, which result in marked changes in the function to be integrated in only small portions of the range of integration, require that extremely small interval sizes be employed in this range, and, consequently over the entire range of integration. This leads to a considerable amount of computational work; hence, it appears reasonable to discuss the possibility of employing intervals of varying lengths for the evaluation of the Poisson integral.

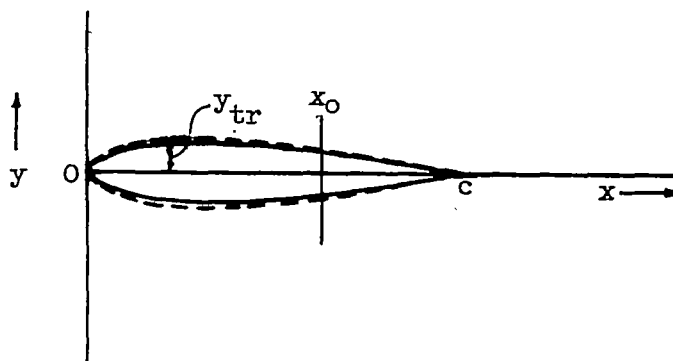
This investigation was prompted by the difficulties arising from the problem of small changes in the shape of symmetrical airfoils at the angle of zero lift. The examples included in the present report are restricted to this case, but the results obtained are in no way specialized and may be applied to all problems wherein the Poisson integral occurs.

This work was done at Stanford University under the sponsorship and with the financial assistance of the National Advisory Committee for Aeronautics.

The author wishes to express her appreciation to Mr. H. Norman Abramson for his intelligent and skillful help in the computational work and for his assistance in writing the final report. The author also wishes to extend her thanks to Mr. R. E. Dannenberg and the computing staff of the 7- by 10-foot wind-tunnel section of the Ames Aeronautical Laboratory, Moffett Field, California, for preparing the extended tables of the functions  $j_{no}$  and  $j_{no}^*$ .

#### DISCUSSION OF PROBLEM

The basic reference profile may be given by  $y_{tr} = f(x)$ , and its velocity distribution may be known from an earlier computation. The problem at hand is that of determining the change in the velocity distribution resulting from a change in the shape of the profile (indicated by the dotted line in the following fig.). The difference of these two shapes is designated as  $\Delta y_t$ .



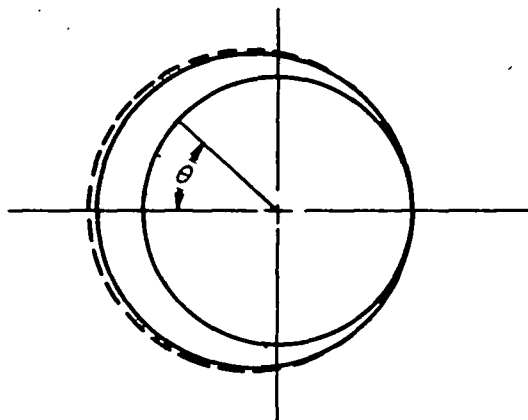
Allen (reference 1, p. 7) gives for the change of velocity the equation

$$\frac{\Delta v(x_0)}{V_0} = -\frac{1}{\pi} \int_0^c \frac{\frac{d(\Delta y_t)}{dx} dx}{x - x_0} \quad (1)$$

where  $V_0$  is the velocity of the basic parallel flow. If, by conformal mapping of the outside flow region, the center line of the profile is transformed into a circle by the relation

$$x = \frac{c}{2} (1 - \cos \theta) \quad (2)$$

then the profile is transformed into a curve approximating the circle shown below.



The change in velocity due to a change in form will then be given as

$$\frac{\Delta v}{V_0}(\theta_0) = -\frac{1}{2\pi} \int_0^{2\pi} \frac{d(\Delta y_t)}{dx} \cot \frac{\theta - \theta_0}{2} d\theta \quad (3)$$

defining

$$\left[ \frac{d(\Delta y_t)}{dx} \right]_{\pi+\theta} = - \left[ \frac{d(\Delta y_t)}{dx} \right]_{\pi-\theta}$$

This is the form most often used for computation purposes, because the inverse problem (that of computing the change in shape due to a change in velocity distribution) utilizes the analytic form

$$\left[ \frac{d(\Delta y_t)}{dx} \right]_{x_0} = \frac{1}{2\pi} \int_0^{2\pi} \frac{\Delta v}{V_0} \cot \left( \frac{\theta - \theta_0}{2} \right) d\theta \quad (4)$$

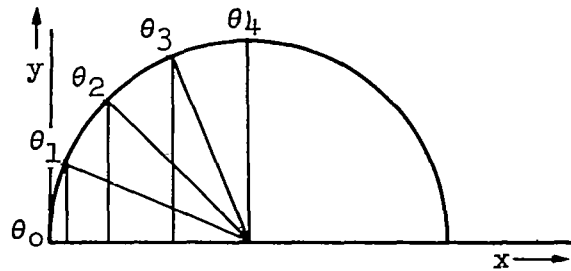
defining

$$\left( \frac{\Delta v}{V_0} \right)_{\pi+\theta} = \left( \frac{\Delta v}{V_0} \right)_{\pi-\theta}$$

which is strikingly similar. The corresponding formula in the original  $x, y$  coordinate system is given by

$$\left[ \frac{d(\Delta y_t)}{dx} \right]_{x_0} = \frac{1}{\pi} \int_0^c \frac{\frac{\Delta v}{V_0}}{x - x_0} \frac{\sqrt{x_0(c - x_0)}}{\sqrt{x(c - x)}} dx \quad (5)$$

The evaluation of equation (3) may be accomplished by any one of several different methods; however, all of these methods employ the device of replacing the integral over the range 0 to  $2\pi$  by a sum of integrals over intervals of equal length  $\Delta\theta$ . The equally distributed points  $\theta_n$  have corresponding values  $x_n$  which are not equally distributed (see following fig.).

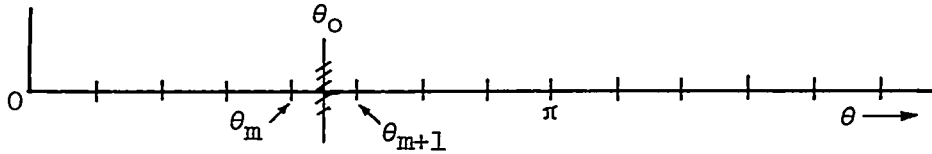
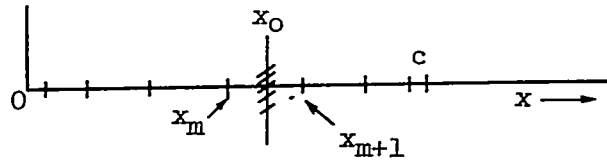


This arrangement is sometimes favorable, and sometimes not, depending upon the particular form of  $\frac{d(\Delta y_t)}{dx}$ . (See discussion following equation (43).)

The use of the angular coordinate  $\theta$  has the advantage that the functions  $\frac{d(\Delta y_t)}{dx}$  or  $\frac{\Delta v}{V_0}$  are periodic functions in  $\theta$ , and this periodicity facilitates the organization of the numerical computations. The disadvantage arises from the fact that these functions are usually given as functions of  $x$ , and, since the analytic form is not usually known, any transformations made will lead to small errors. For example, if  $\frac{d(\Delta y_t)}{dx}$  or  $\frac{\Delta v}{V_0}$  is given at special points which do not correspond to  $\theta_n = n\Delta\theta$ , then the computer must obtain the values of these functions for the values  $\theta_1$ ,  $\theta_2$ , and so forth by interpolation.

#### DISCUSSION OF SOME OF THE EXISTING NUMERICAL SOLUTIONS OF POISSON INTEGRAL

The difficulty encountered in the solution of the Poisson integral arises from the fact that the term  $\cot \frac{(\theta - \theta_0)}{2}$  or  $\frac{1}{x - x_0}$  (equations (1) and (3), e.g.) approaches infinity when  $\theta$  approaches  $\theta_0$  or when  $x$  approaches  $x_0$ . The difficulty is of much less consequence when the function  $\frac{d(\Delta y_t)}{dx}$  or  $\frac{\Delta v}{V_0}$  is given analytically than when a numerical computation is undertaken. As a consequence, any simple integration, performed by replacing the integral with a summation over smaller intervals, always requires that the interval in which  $\theta_0$  or  $x_0$  is located be given special consideration (see following fig.).



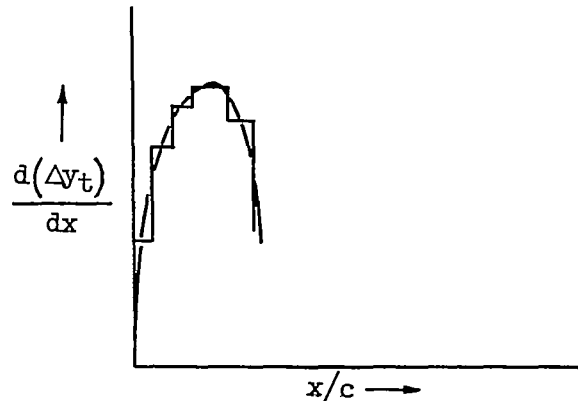
A majority of the solutions currently in use have been developed to such an extent that, for example,  $\frac{\Delta v}{V_0}(\theta_0)$  is given by a sum of products of single values of  $\left(\frac{d(\Delta y_t)}{dx}\right)_n$  and known factors  $A_n$ ; that is,

$$\begin{aligned} \frac{\Delta v}{V_0}(\theta_0) &= -\frac{1}{2\pi} \int_0^{2\pi} \frac{d(\Delta y_t)}{dx} \cot \left( \frac{\theta - \theta_0}{2} \right) d\theta \\ &= -\frac{1}{2\pi} \int_{-\theta_0}^{2\pi - \theta_0} \frac{d(\Delta y_t)}{dx} \cot \frac{\theta^*}{2} d\theta^* \\ &= -\frac{1}{2\pi} \sum_n \int_{\theta_n^*}^{\theta_{n+1}^*} \frac{d(\Delta y_t)}{dx} \cot \frac{\theta^*}{2} d\theta^* \end{aligned} \quad (6)$$

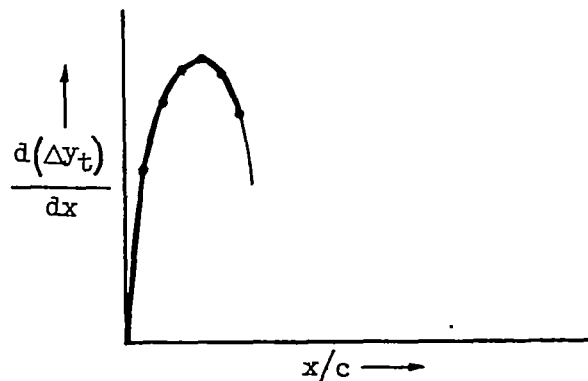
which leads to (see reference 2, e.g.)

$$\frac{\Delta v}{V_0}(\theta_0) = \sum_n A_{no} \left[ \frac{d(\Delta y_t)}{dx} \right]_n \quad (7)$$

The coefficients  $A_{no}$  depend upon the particular method of numerical integration which is employed. If, for example,  $\frac{d(\Delta y_t)}{dx}$  is replaced by a step-curve, that is, assumed constant in every interval (see fig. below), one set of values of  $A_{no}$  would be obtained.



Greater accuracy would be obtained by the assumption that  $\frac{d(\Delta y_t)}{dx}$  is replaced by straight-line segments (see fig. below), in which case a second set of values of  $A_{no}$  would be obtained.



A further refinement would be that of assuming  $\frac{d(\Delta y_t)}{dx}$  to be composed of segments of parabolas, and so forth. Since the accuracy of the resulting values of  $\frac{\Delta y}{V_0}$  depends upon both the character of the approximate curve and the size of interval taken, it is apparent that the same degree of accuracy might be achieved from many different combinations of interval sizes and approximations to the function  $\frac{d(\Delta y_t)}{dx}$ .



Naiman (reference 2) has used Simpson's rule for computing the Poisson integral, which corresponds to the replacement of the product  $\left[ \frac{d(\Delta y_t)}{dx} \cot \frac{\theta^*}{2} \right]$  by segments of parabolas. The "critical interval" (i.e., where  $\cot \frac{\theta^*}{2} \rightarrow \infty$ ) was carefully treated by using differences of higher order (including the fifth derivative of  $\frac{d(\Delta y_t)}{dx}$ ). Naiman divided the period of  $2\pi$  in 20 or 40 intervals and calculated the corresponding sets of values of  $A_{no}$ . Other workers at the NACA have extended the calculation of these values of  $A_{no}$  to 80 and 160 intervals (unpublished information).<sup>1</sup>

Obviously, the time required for computing  $\frac{\Delta v}{v_0}$  increases with the number of intervals taken because of the increased number of multiplications to be performed. In addition, greater preparations for the computing process are necessarily involved, particularly since the values of  $\frac{d(\Delta y_t)}{dx}$  needed must usually be obtained by interpolation. This interpolation has to be done rather carefully as it is often not sufficient simply to take the values of the plotted curve of  $\frac{d(\Delta y_t)}{dx}$ . This curve should be checked by difference tables if the values  $\left[ \frac{d(\Delta y_t)}{dx} \right]_n$  are to represent a smooth curve.

For those functions of  $\Delta y_t$  which may be well-represented by a Fourier series, there exists a simple method of evaluating the Poisson integral which has apparently been overlooked until the present time. This method has the advantage of leading to a computation which does not involve the derivative of  $\Delta y_t$ .

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<sup>1</sup>Naiman has also suggested a second method for computing the Poisson integral (see reference 3). In this second method he uses Fourier polynomials to represent the function  $\frac{d(\Delta y_t)}{dx}$ . The computing procedure is very simple; however, the results depend largely on the degree of approximation of  $\frac{d(\Delta y_t)}{dx}$  by such a polynomial. Thus, for large families of functions results are good; however, cases are known to the author where results were not satisfactory because regions with steep gradients may not be represented well enough by a Fourier polynomial of moderate order.

Equation (6) may be written in a different form (reference 1, equation (43)) as follows:

$$\frac{\Delta v}{V_0} = \frac{1}{\pi} \int_0^\pi \frac{d(\Delta y_t)}{dx} \frac{\sin \theta}{\cos \theta - \cos \theta_0} d\theta \quad (8)$$

and this may be rewritten as

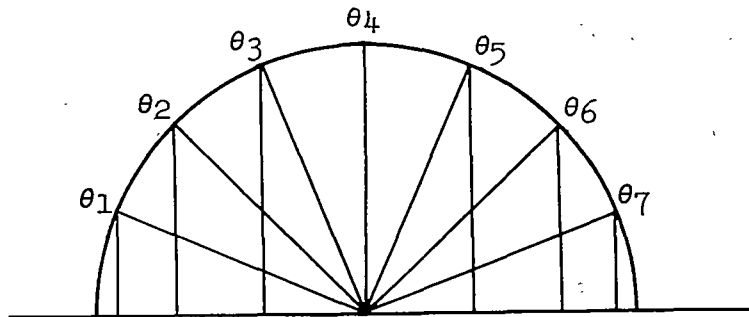
$$\frac{\Delta v}{V_0} = \frac{1}{\pi} \frac{2}{c} \int_0^\pi \frac{d(\Delta y_t)}{d\theta} \frac{d\theta}{\cos \theta - \cos \theta_0} \quad (9)$$

Equation (9) is strikingly similar to an integral occurring in the theory of the lift distribution of a finite wing in incompressible flow. There, the induced angle  $\alpha_i$  is given by

$$\alpha_i = \frac{1}{2\pi} \int_0^\pi \frac{d\gamma}{d\theta'} \frac{d\theta'}{\cos \theta' - \cos \theta} \quad (10)$$

where  $\gamma$  is the local dimensionless circulation.

Multhopp (reference 4) has given a solution for equation (10). He divides the range of integration into  $(m_1 + 1)$  intervals (see fig. below)



with

$$\left. \begin{aligned} \theta_n &= \frac{n}{m_1 + 1} \pi \\ \gamma_n &= \gamma(\theta_n) \end{aligned} \right\} \quad (11)$$

and computes  $\alpha_i$  at the points  $\theta_n$ . He assumes that  $\gamma$  may be expanded in the form

$$\gamma = \sum C_\mu \sin \mu\theta$$

or

$$\gamma = \frac{2}{m+1} \sum_{n=1}^{m_1} \gamma_n \sum_{\mu=1}^{m_1} \sin \mu\theta_n \sin \mu\theta \quad (12)$$

He then obtains the expression

$$\alpha_{iv} = b_{vv}\gamma_v - \sum_1^{m_1} b_{vn}' \gamma_n \quad (13)$$

The prime on the summation symbol indicates that  $n = v$  is to be omitted from the summation because that special term has already been considered in the first term of the right-hand side (i.e.,  $b_{vv}\gamma_v$ ). Reference 4 presents tables for the coefficients  $b_{vv}$  and  $b_{vn}$  for  $m_1 = 7, 15,$  and  $31$ . Applied to the problem at hand,  $m_1 = 31$  would appear to be rather small; therefore a table for  $m_1 = 63$  has been computed and is included in the present report (appendix A). As a comparison: For  $m_1 = 63$ ,  $\Delta\theta = 2.8125^\circ$ ; for Naiman's method with 160 points,  $\Delta\theta = 2.25^\circ$ .

Utilizing this method of integration which was developed by means of Fourier series, an expression may be obtained for the velocity distribution as follows:

$$\frac{\Delta v}{V_0}(\theta_0) = \frac{h}{c} \left( b_{vv} \Delta v_v - \sum_1^{m_1} b_{vn}' \Delta v_n \right) \quad (14)$$

The great advantage of this method is that of simplicity: (1) The actual computational procedure is very simple and (2) the derivative  $\frac{d(\Delta v_t)}{dx}$  is avoided. The simplicity of computation is reflected in the fact that the time required for computing  $\frac{\Delta v}{V_0}$  at one value of  $\theta_0$  is approximately half that required by the method of Naiman when the intervals have approximately the same size. It should be noted,

however, that the accuracy of the method of Naiman will be greater than that of Multhopp in those cases where the differentiation of  $\Delta y_t$  by Fourier expansion (equation (12)) does not give good results.

A third method of evaluating the Poisson integral became known during the course of the present investigation. In a paper by Timman (reference 5), the integral is studied in the form

$$\tau(\phi) = -\frac{1}{2\pi} \int_0^{2\pi} \bar{\sigma}(\psi) \cot \frac{\phi - \psi}{2} d\psi \quad (15)$$

Timman assumes that  $\bar{\sigma}(\psi)$  is not given analytically, but only at equidistant points. An interpolation polynomial (reference 6) for  $\bar{\sigma}(\psi)$  is employed, and these polynomials replace the function  $\bar{\sigma}(\psi)$  in a single interval by a function of third order. The polynomial function thus introduced has a continuous first derivative,<sup>2</sup> and it is evident that this continuity is essential for the attainment of good results.

Timman has divided the period  $2\pi$  into 36 intervals of equal length and established a computing scheme. The function  $\bar{\sigma}(\psi)$  is separated into its symmetrical and unsymmetrical parts so that

$$\bar{\sigma}(\psi) = s + d \quad (16)$$

Then

$$\tau(\psi_l) = \sum_{k=0}^{18} \alpha_{kl} s_k - \sum_{k=0}^{18} \beta_{kl} d_k \quad (17)$$

where the factors  $\alpha_{kl}$  and  $\beta_{kl}$  are given in tabular form. In the present particular case  $\frac{d(\Delta y_t)}{dx}$  is antisymmetrical (equation (3)) and  $\frac{\Delta v}{V_0}$  is symmetrical (equation (4)). Thus the separation indicated by equation (16) does not require any additional work.

Timman's method should give good results provided that a sufficient number of intervals are taken - the division of 36 intervals over a period of  $2\pi$  (i.e., 18 intervals over the chord of the profile) appears to be insufficient for an accurate representation of the function which occurs,  $\frac{d(\Delta y_t)}{dx}$  or  $\frac{\Delta v}{V_0}$ .

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<sup>2</sup>The polynomials used in the classical interpolation formulas are less smooth (see reference 5, pp. 7 and 10, figs. 1 and 2).

The time required for computing one point by the method of Timman is approximately the same as for Naiman's method with the same interval size.

Other methods of evaluating the Poisson integral have been suggested. They will not be discussed here as it is the intention of this section to consider only the most practical of the known methods. The three methods already discussed have their own particular advantages and have been especially developed for rapid and simple computation; however, all three of these methods, when  $\frac{d(\Delta y_t)}{dx}$  or  $\frac{\Delta v}{V_0}$ , change rapidly in magnitude, become cumbersome, and require that very small intervals be taken over the entire range of integration because the scheme of equal interval size is utilized.

## EVALUATION OF POISSON INTEGRAL BY A METHOD

### EMPLOYING UNEQUAL INTERVALS

#### Development of Method

As the change in airfoil shape, or the change in velocity distribution, is given originally as a function of  $x$  it appears logical to retain the coordinate  $x$  in selecting the size of the different intervals. Hence, the Poisson integral may be studied in the form

$$\tau(x_0) = -\frac{1}{\pi} \int_0^c \sigma(x) \frac{dx}{x - x_0} \quad (18)$$

which corresponds to equation (1). Conforming with its physical meaning  $\sigma(x) = \frac{d(\Delta y_t)}{dx}$  is assumed to be a function which is finite in every point of its range of definition.<sup>3</sup>

Define

$$\Delta x_n = x_{n+1} - x_n \quad (19a)$$

with

$$n = 0, 1, 2, 3, \dots$$

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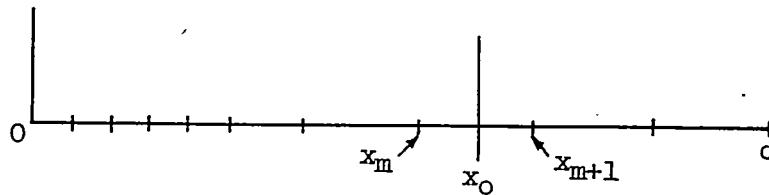
<sup>3</sup>This restriction will be dropped later; see discussion beginning with the first paragraph after equation (32).

and

$$x_m < x_0 < x_{m+1} \quad (19b)$$

For convenience, there is chosen (see following fig.)

$$x_0 = \frac{x_m + x_{m+1}}{2} \quad (19c)$$



The function  $\sigma(x)$  is approximated by straight-line segments (see third sketch in preceding section). Then, for  $x_n < x < x_{n+1}$ ,

$$\begin{aligned} \sigma(x) &= \sigma(x_n) + \frac{\sigma(x_{n+1}) - \sigma(x_n)}{\Delta x_n} (x - x_n) \\ &= \sigma_n + \frac{\sigma_{n+1} - \sigma_n}{\Delta x_n} (x - x_n) \end{aligned} \quad (20)$$

from which there is obtained

$$\begin{aligned}
\tau(x_0) &= -\frac{1}{\pi} \int_0^c \sigma(x) \frac{dx}{x-x_0} = -\frac{1}{\pi} \sum \int_{x_n}^{x_{n+1}} \frac{\sigma_n + \frac{\sigma_{n+1} - \sigma_n}{\Delta x_n} (x - x_n)}{x - x_0} dx \\
&= -\frac{1}{\pi} \left[ \sum \int_{x_n}^{x_{n+1}} \frac{\sigma_n + \frac{\sigma_{n+1} - \sigma_n}{\Delta x_n} (x - x_0 + x_0 - x_n)}{x - x_0} dx \right] \\
&= -\frac{1}{\pi} \left\{ \sum \left( \frac{\sigma_{n+1} - \sigma_n}{\Delta x_n} \right) \Delta x_n + \right. \\
&\quad \left. \sum \left[ \sigma_n + \frac{\sigma_{n+1} - \sigma_n}{\Delta x_n} (x_0 - x_n) \right] \left( \int_{x_n}^{x_{n+1}} \frac{dx}{x - x_0} \right) \right\} \quad (21)
\end{aligned}$$

Also,

$$\int_{x_n}^{x_{n+1}} \frac{dx}{x - x_0} = j_{no} \quad (22)$$

by definition. The function  $j_{no}$ , in the different regions of  $x$ , is given by different expressions as follows:

$$j_{no} = \left\{ \begin{array}{l} \log_e \frac{x_{n+1} - x_0}{x_n - x_0} \quad \text{for } x_{n+1} > x_n > x_0 \\ \log_e \frac{x_{n+1} - x_0}{x_0 - x_n} \quad \text{for } x_{n+1} > x_0 > x_n \\ \log_e \frac{x_0 - x_{n+1}}{x_0 - x_n} \quad \text{for } x_0 > x_{n+1} > x_n \end{array} \right\} \quad (23)$$

Introducing  $j_{no}$  into equation (21), there results

$$\begin{aligned} \tau(x_0) &= -\frac{1}{\pi} \left\{ \sum (\sigma_{n+1} - \sigma_n) + \sum \left[ \sigma_n + \frac{\sigma_{n+1} - \sigma_n}{\Delta x_n} (x_0 - x_n) \right] j_{no} \right\} \\ &= -\frac{1}{\pi} \left[ \sum \sigma_n j_{no} + \sum (\sigma_{n+1} - \sigma_n) \left( 1 + \frac{x_0 - x_n}{\Delta x_n} j_{no} \right) \right] \end{aligned} \quad (24)$$

Or, defining

$$1 + \frac{x_0 - x_n}{\Delta x_n} j_{no} = j_{no}^* \quad (25)$$

there results, finally,

$$\tau(x_0) = -\frac{1}{\pi} \left[ \sum \sigma_n j_{no} + \sum (\sigma_{n+1} - \sigma_n) j_{no}^* \right] \quad (26)$$

Since  $x_{n+1} = x_n + \Delta x_n$ , the functions  $j_{no}$  and  $j_{no}^*$  may be written as

$$\left. \begin{aligned} j_{no}^* &= 1 + \frac{x_0 - x_n}{\Delta x_n} j_{no} \\ j_{no} &= \log_e \left( 1 + \frac{\Delta x_n}{x_n - x_0} \right) \text{ for } x_n > x_0 \\ &= \log_e \left( -1 + \frac{\Delta x_n}{x_0 - x_n} \right) \text{ for } x_n + \Delta x_n > x_0 > x_n \\ &= \log_e \left( 1 + \frac{\Delta x_n}{x_n - x_0} \right) \text{ for } x_0 > x_n + \Delta x_n \end{aligned} \right\} \quad (27a)$$

and this form shows that  $j_{no}$  and  $j_{no}^*$  are functions of  $\frac{x_n - x_0}{\Delta x_n}$  only.



$$\left. \begin{array}{l} \text{For } \frac{x_n - x_0}{\Delta x_n} \rightarrow \pm\infty \quad j_{no} \rightarrow 0 \quad j_{no}^* \rightarrow 0 \\ \text{For } x_0 - x_n = \frac{1}{2} \Delta x_n \quad j_{no} = 0 \quad j_{no}^* = 1 \end{array} \right\} \quad (27b)$$

$$\left. \begin{array}{l} \text{For very large } \frac{x_n - x_0}{\Delta x_n} = \xi, \\ j_{no} \rightarrow \frac{1}{\xi} - \frac{1}{2\xi^2} + \dots \\ j_{no}^* \rightarrow \frac{1}{2\xi} - \frac{1}{3\xi^2} + \dots \end{array} \right\} \quad (27c)$$

$$\left. \begin{array}{l} \text{For very large negative } \frac{x_n - x_0}{\Delta x_n} \text{ with } \left| \frac{x_n - x_0}{\Delta x_n} \right| = \xi^*, \\ j_{no} \rightarrow -\frac{1}{\xi^*} - \frac{1}{2\xi^{*2}} + \dots \\ j_{no}^* \rightarrow -\frac{1}{2\xi^*} - \frac{1}{3\xi^{*2}} + \dots \end{array} \right\} \quad (27d)$$

These functions are given in figure 1 and in table I.

It is seen that high absolute values of  $j_{no}$  and  $j_{no}^*$  occur near those values of  $\frac{x_n - x_0}{\Delta x_n}$  which characterize the critical interval.<sup>4</sup>

Figure 1 gives an idea of the characteristic qualities of  $j_{no}$  and  $j_{no}^*$  as functions of  $\frac{x_n - x_0}{\Delta x_n}$ ; however, the representation is not sufficient for picking out values for a computation. Table I gives the values of  $j_{no}$  and  $j_{no}^*$  for  $-49.5 < \frac{x_n - x_0}{\Delta x} < 49.5$ . This table might

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<sup>4</sup>If  $x_0 = \frac{x_m + x_{m+1}}{2}$  (equation (19c)) the critical interval is given by  $-0.5 < \frac{x_n - x_0}{\Delta x_n} < 0.5$ .

be used for rough computation and for getting acquainted with the method. In general, it is advisable to use those tables which are given in appendix B.

It will prove of benefit to investigate the exactness of that portion of the integral which contains the singularity. Recalling that the function  $\sigma(x)$  was replaced by a straight line in every interval (equation (20)), there is obtained:

$$-\frac{1}{\pi} \int_{x_0 - \frac{\Delta x}{2}}^{x_0 + \frac{\Delta x}{2}} \frac{\sigma(x)}{x - x_0} dx = -\frac{1}{\pi} (\sigma_{m+1} - \sigma_m) \quad (28)$$

if  $x_m < x_0 < x_{m+1}$ . Now, let an expansion of the function  $\sigma(x)$  in the critical interval around  $x_0$  be assumed as follows:

$$\begin{aligned} \sigma(x) = & \sigma(x_0) + \sigma'(x_0)(x - x_0) + \frac{\sigma''(x_0)}{2!}(x - x_0)^2 + \\ & \frac{\sigma'''(x_0)}{3!}(x - x_0)^3 + \frac{\sigma^{IV}(x_0)}{4!}(x - x_0)^4 + \dots \end{aligned} \quad (29)$$

Then,

$$\begin{aligned} -\frac{1}{\pi} \int_{x_0 - \frac{\Delta x}{2}}^{x_0 + \frac{\Delta x}{2}} \frac{\sigma(x)}{x - x_0} dx &= -\frac{1}{\pi} \left[ \sigma'(x_0) \Delta x + \frac{\sigma'''(x_0)}{3!} \frac{2}{3} \left(\frac{\Delta x}{2}\right)^3 + \dots \right] \\ &= -\frac{1}{\pi} \left[ \frac{13}{12} (\sigma_{m+1} - \sigma_m) - \frac{1}{36} (\sigma_{m+2} - \sigma_{m-1}) \right] \\ &= -\frac{1}{\pi} \left\{ \frac{19}{18} (\sigma_{m+1} - \sigma_m) - \right. \\ & \quad \left. \frac{1}{36} [(\sigma_{m+2} - \sigma_{m+1}) + (\sigma_m - \sigma_{m-1})] \right\} \end{aligned} \quad (30)$$

Comparison of formulas (30) and (28) shows that the error in the critical interval is approximately given by

$$- \frac{1}{\pi} \left\{ \frac{1}{18} (\sigma_{m+1} - \sigma_m) - \frac{1}{36} \left[ (\sigma_{m+2} - \sigma_{m+1}) + (\sigma_m - \sigma_{m-1}) \right] \right\} \quad (31)$$

The error of evaluating the whole integral by finite differences may be estimated by using two different interval distributions and comparing the results for a given  $x_0$ .

However, in addition to that error of the result produced by replacing the Poisson integral by a sum there exists another error. This sum cannot be computed exactly, but has a certain error depending on the accuracy of the given data for  $\sigma_n(x)$  and the tabulated values of  $j_{no}$  and  $j_{no}^*$ . As the function  $\sigma(x) = \frac{d(\Delta y_t)}{dx}$  usually has an error of  $\epsilon_1 = 1 \times 10^{-3}$  it has proved amply satisfactory to give  $j_{no}$  and  $j_{no}^*$  to four decimal places, the error being less than  $\epsilon_2 = 5 \times 10^{-5}$ . The error of

$$\tau(x_0) = - \frac{1}{\pi} \left[ \sum \sigma_n j_{no} + \sum (\sigma_{n+1} - \sigma_n) j_{no}^* \right]$$

is smaller than its upper limit given by

$$\frac{1}{\pi} \left[ \epsilon_1 \left( \sum |j_{no}| + 2 \sum |j_{no}^*| \right) + \epsilon_2 \left( \sum |\sigma_n| + \sum |\sigma_{n+1} - \sigma_n| \right) \right] \quad (32)$$

This formula shows that the influence of  $\epsilon_1$  is stronger than the influence of  $\epsilon_2$  as long as  $\sum |\sigma_n| + \sum |\sigma_{n+1} - \sigma_n|$  is smaller than 1 - as it is in our later examples - and the sums  $\sum |j_{no}|$  and  $\sum |j_{no}^*|$  are always larger than 1. An increase of subdivisions makes the sums in the upper limit of the error (32) grow, thus requiring a higher accuracy, especially in  $\sigma_n$  and perhaps also in the values of  $j_{no}$  and  $j_{no}^*$ .

In establishing the solution of equation (18) it was assumed that  $\sigma(x)$  is finite throughout its range of definition. If it is desired to compute the change in shape due to a proposed change of velocity distribution, this restriction must be eliminated, as will be recognized immediately.

Equation (5) may be written in the form

$$\frac{d(\Delta y_t)}{dx} = \frac{1}{\pi} \sqrt{x_0(c-x_0)} \int_0^c \frac{\Delta v/V_0}{\sqrt{x(c-x)}} \frac{dx}{x-x_0} \quad (5')$$

Omitting the factor  $\sqrt{x_0(c-x_0)}$ , which does not affect the integration process, the integral may be reduced to the form of equation (18) by defining

$$\frac{\Delta v/V_0}{\sqrt{x(c-x)}} = \sigma_1(x) \quad (33)$$

However,  $\sigma_1(x)$  will be infinite at  $x=0$  and  $x=c$  if  $\left(\frac{\Delta v}{V_0}\right)_0 \neq 0$  and  $\left(\frac{\Delta v}{V_0}\right)_c \neq 0$ ; therefore, a special consideration of the neighborhood of  $x=0$  and  $x=c$  is required. This is done by splitting the integral into the following three parts:

$$\int_0^c \sigma_1(x) \frac{dx}{x-x_0} = \int_0^{\epsilon_1} \sigma_1(x) \frac{dx}{x-x_0} + \int_{\epsilon_1}^{c-\epsilon_2} \sigma_1(x) \frac{dx}{x-x_0} + \int_{c-\epsilon_2}^c \sigma_1(x) \frac{dx}{x-x_0} \quad (34)$$

with  $\epsilon_1$  and  $\epsilon_2$  being small compared with  $c$ . The integral

$$\int_{\epsilon_1}^{c-\epsilon_2} \sigma_1(x) \frac{dx}{x-x_0}$$

may be treated as was explained formerly for

$$\int_0^c \sigma(x) \frac{dx}{x-x_0}$$

(see equation (18)) because  $\sigma_1(x)$  is finite for  $\epsilon_1 < x < c - \epsilon_2$ . For the first and third integrals, however, a new integration formula must be developed. By introducing

$$\mu = c - x \quad \text{and} \quad \sigma_1(x) = \sigma_1[\mu(x)] = \sigma_1^*(\mu)$$

there is obtained

$$\int_{c-\epsilon_2}^c \sigma_1(x) \frac{dx}{x - x_0} = - \int_0^{\epsilon_2} \sigma_1^*(\mu) \frac{d\mu}{\mu - \mu_0} \quad (35)$$

Hence, the method used for the first integral will also apply to the third. In most cases  $\left(\frac{\Delta v}{V_0}\right)_c$  will be zero and there will be no need for a special evaluation in the neighborhood of  $x = c$ .

The integral

$$\int_0^{\epsilon_1} \sigma_1(x) \frac{dx}{x - x_0} = \int_0^{\epsilon_1} \frac{\Delta v/V_0}{\sqrt{x(c-x)}} \frac{dx}{x - x_0} \quad (36)$$

will have an important influence on the result of equation (34) only if  $x_0$  is near to  $\epsilon_1$ . First the general formula will be given and then a simplification will be discussed for  $x_0 \gg \epsilon_1$ .

The integral (36) will be solved assuming that

$$\frac{\Delta v}{V_0} = a_0 + a_1\left(\frac{x}{c}\right) + a_2\left(\frac{x}{c}\right)^2 \quad \text{for} \quad 0 < x < \epsilon_1 \quad (37)$$

Only the final formula of this procedure is given here; the details of the solution will be found in appendix C.

$$F_1(x_0) = \int_0^{\epsilon_1} \frac{\Delta v/V_0}{\sqrt{x(c-x)}} \frac{dx}{x-x_0} = \frac{1}{c} \left\{ M_0 \frac{1}{\sqrt{\frac{x_0}{c}}} \left[ a_0 + a_1^* \left( \frac{x_0}{c} \right) + a_2^* \left( \frac{x_0}{c} \right)^2 \right] + 2 \sqrt{\frac{\epsilon_1}{c}} \left[ a_1^* + a_2^* \left( \frac{x_0}{c} \right) \right] + \frac{2}{3} a_2^* \sqrt{\frac{\epsilon_1}{c}}^3 \right\} \quad (38)$$

with  $M_0$  given in figure 2, and

$$\left. \begin{aligned} a_0 &= \left( \frac{\Delta v}{V_0} \right)_0 \\ a_1^* &= a_1 + \frac{1}{2} a_0 \\ \text{with} \\ a_1 &= \frac{c}{2\epsilon_1} \left[ -3 \left( \frac{\Delta v}{V_0} \right)_0 + 4 \left( \frac{\Delta v}{V_0} \right)_{\epsilon_1} - \left( \frac{\Delta v}{V_0} \right)_{2\epsilon_1} \right] \\ \text{with} \\ a_2^* &= a_2 + \frac{1}{2} a_1 + \frac{3}{8} a_0 \\ a_2 &= \frac{c^2}{2\epsilon_1} \left[ \left( \frac{\Delta v}{V_0} \right)_0 - 2 \left( \frac{\Delta v}{V_0} \right)_{\epsilon_1} + \left( \frac{\Delta v}{V_0} \right)_{2\epsilon_1} \right] \end{aligned} \right\} \quad (39)$$

The coefficients  $a_0$ ,  $a_1$ , and  $a_2$  may be determined first, as they do not depend upon the particular value of  $x_0$ , and then  $F_1(x_0)$  may be computed. The term depending on  $a_1$  and  $a_2$  will exert an influence only for small values of  $x_0/c$ . After a brief training the computer should be able to decide rather accurately when the formula

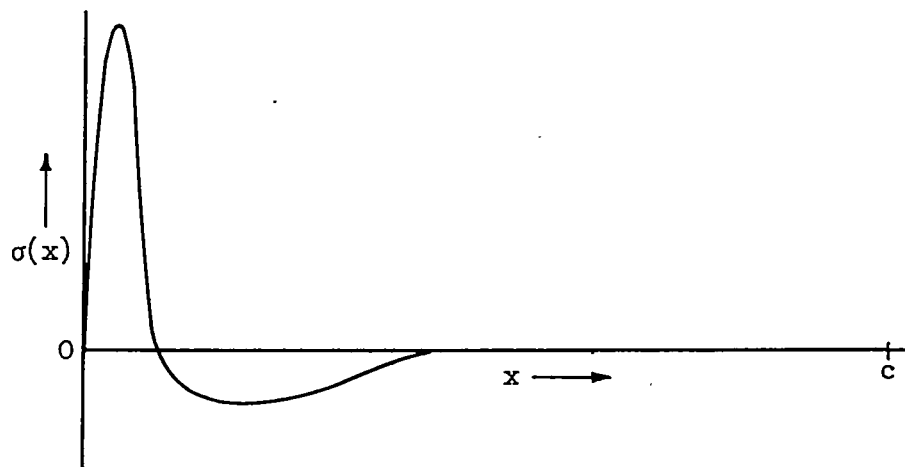
$$F_1(x_0) = \frac{1}{c} M_0 \frac{a_0}{\sqrt{\frac{x_0}{c}}} \rightarrow \frac{a_0}{x_0} \left( -2 \sqrt{\frac{\epsilon_1}{c}} \right) \quad (40)$$

is sufficient and when the more exact expression (equation (38)) is required (also see fig. 2).

Organization of Computational Procedure for Unequal Intervals;  
Transition from One Size of Interval to Another

A thorough understanding of the method is best achieved by following through a rather simple example; in addition various short cuts to the method will be demonstrated.

Assume a function  $\sigma(x)$  of the type shown in the following figure.



It appears reasonable to take rather small intervals for small values of  $x$  because of the form of the curve  $\sigma(x)$ ; therefore, the following arrangement of interval sizes is arbitrarily selected:

$$\overline{\Delta x} = 0.002 \quad \text{for } 0 < x < 0.030$$

$$\overline{\Delta x} = 0.006 \quad \text{for } 0.030 < x < 0.096$$

Compute  $\tau(0.009)$  with the help of equation (26). Note that the critical interval extends from 0.008 to 0.010. Table II(a) gives the values of  $x/c$ ,  $\sigma_n$ ,  $\sigma_{n+1} - \sigma_n$ ,  $j_{no}$ , and  $j_{no}^*$  for the range with  $\overline{\Delta x} = 0.002$ . At  $x = 0.030$  the interval changes to  $\overline{\Delta x} = 0.006$  and the same functions are given for the range with this size of interval in table II(b). Naturally the range above the broken line in table II(b) is not utilized in the computation since this portion has been considered in table II(a).

Note that  $\frac{x_n - x_0}{\Delta x}$  progresses in table II(b) in the same manner as in table II(a); this is due to the special choice of  $\overline{\Delta x}$ . If  $\overline{\Delta x} = 0.006$  were used starting with  $x = 0$  the critical interval for  $x_0 = 0.009$  would extend from 0.006 to 0.012. Hence, for  $\overline{\Delta x} = 0.006$ ,  $j_{no} = 0$  and  $j_{no}^* = 1$  is to be found at  $x/c = 0.006$ .

For rapid computation it is best to have  $j_{no}$  and  $j_{no}^*$  as functions of  $\frac{x_n - x_0}{\Delta x}$  on a paper strip and to place this strip adjacent to the columns headed by  $\sigma_n$  and  $\sigma_{n+1} - \sigma_n$ . If  $\frac{x_n - x_0}{\Delta x}$  progresses as indicated in table I, the correct location of  $j_{no} = 0$  and  $j_{no}^* = 1$  at the beginning of the critical interval fixes the placement of the strip.

In the example just treated, the transition from one size of interval to another is very easy because  $x_0$  lies at the midpoint of an interval of the size 0.006 as well as of the size 0.002, if starting with  $x = 0$ .

If  $\overline{\Delta x}$  had been chosen 0.004, such a desirable arrangement would not have resulted because  $x_0 = 0.009$  would not be located at the midpoint of an interval of this size (starting with such intervals at  $x = 0$ ).

As a second example compute the value of  $\tau$  at  $x_0 = 0.015$ . Again,  $\frac{x_n - x_0}{\overline{\Delta x}}$  and  $\frac{x_n - x_0}{\overline{\Delta x}}$  will progress as in table I. The values  $j_{no} = 0$  and  $j_{no}^* = 1$  will be placed opposite  $x/c = 0.014$  for the region with  $\overline{\Delta x} = 0.002$  and opposite  $x/c = 0.012$  for the region with  $\overline{\Delta x} = 0.006$ . As long as  $\overline{\Delta x} = 3\overline{\Delta x}$ ,  $\overline{\Delta x} = 3\overline{\Delta x}$ , and so forth and if  $x_0$  is chosen so as to be at the midpoint of the largest size of interval, the computation may be accomplished by shifting the strip with  $j_{no}$  and  $j_{no}^*$  corresponding to table I.

But suppose that the interval sizes are so arranged and it is desired to compute a point where  $x_0$  does not lie at the midpoint of the largest size of interval; for example,  $x_0 = 0.013$ . The value  $x_0 = 0.013$  lies at the midpoint of an interval with  $\overline{\Delta x} = 0.002$ ; hence,



for the range  $0 < x < 0.030$ ,  $j_{no}$  and  $j_{no}^*$  may be taken directly from table I. However, at  $x/c = 0.030$ , intervals of the size  $\overline{\Delta x} = 0.006$  commence and there is obtained

$$\frac{x_n - x_0}{\overline{\Delta x}} = \frac{0.030 - 0.013}{0.006} = 2.833$$

The value of  $\frac{x_n - x_0}{\Delta x}$  progresses by 1, that is, 2.833; 3.833, 4.833, . . . . Thus the functions  $j_{no}$  and  $j_{no}^*$  are needed for values of  $\frac{x_n - x_0}{\Delta x}$  which are not given in table I. One might think of taking them out of an enlarged diagram (see fig. 1); however, it is much more convenient to take them out of an extended table, which is conveniently arranged for "advancing by 1." Such tables are given in appendix B.

The example presented by the figure at the beginning of this section suggested starting at  $x = 0$  with the smallest intervals. However, other examples may suggest another distribution of intervals. The smallest size of intervals may lie at any part of  $0 < x < c$ . There are no restrictions in the arrangement of intervals. (See, e.g., discussion following equation (43).)

#### Accuracy of Method, Examined by Means of an Analytical Example

The accuracy of the result depends directly upon the size of the interval taken and the reliability of the data comprising the function  $\sigma(x)$ . Because the function  $\sigma(x)$  will be replaced by a broken line, a glance at the curve will quickly suggest an arrangement of intervals. In addition, the error in the critical interval may be used as a first test of the choice of intervals.

As a test of the quality of this new method, involving unequal intervals, a function  $\sigma(x) = \frac{d(\Delta y_t)}{dx}$  has been treated which allows the analytical computation of  $\tau(x) = \frac{\Delta y}{V_0}$ .

The function  $\sigma(x)$  is given analytically as

$$0 \leq x \leq 2\Delta \quad \frac{d(\Delta y_t)}{dx} = Bx(2\Delta - x)$$

$$2\Delta \leq x \leq c_1 \quad \frac{d(\Delta y_t)}{dx} = -D(c_1 - x)(x - 2\Delta)$$

$$c_1 \leq x \leq c \quad \frac{d(\Delta y_t)}{dx} = 0$$

The following arbitrary values have been selected:

$$c_1 = 0.35$$

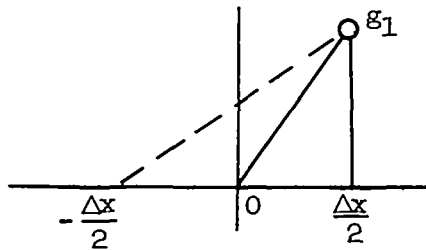
$$c = 1.0$$

D = Some multiple of B so that  $\int_0^{c_1} \frac{d(\Delta y_t)}{dx} dx = 0$

The functions  $\Delta y_t$  and  $\frac{d(\Delta y_t)}{dx}$  are given in figures 3(a) and 3(b), respectively.

The analytical computation of  $\frac{\Delta v}{v_0}$  for figure 3(b) is given in figures 4(a) and 4(b). The arrangement of the unequal division for the numerical computation of  $\frac{\Delta v}{v_0}$  is indicated in figure 4(a).<sup>5</sup>

<sup>5</sup>It was desirable to obtain the value of  $\frac{\Delta v}{v_0}$  at  $x_0 = 0$ ; hence, the first interval has been placed so that  $-0.001 < x_0 < 0.001$  and the function  $\frac{d(\Delta y_t)}{dx} = 0$  for  $-0.001 < x < 0$ . Since the function  $\frac{d(\Delta y_t)}{dx} = g$  is replaced in every interval by a straight line, the error might be expected to be large. However,  $g = 0$  at  $x_0 = 0$  will aid in preventing the error from being too large.



A more exact solution would be obtained by putting

$$g = 0 \quad -\frac{\Delta x}{2} < x < 0$$

$$g = \frac{\varepsilon_1}{\frac{\Delta x}{2}} x \quad 0 < x < \frac{\Delta x}{2}$$

$$-\frac{1}{\pi} \int_0^{\Delta x/2} \left( \frac{\varepsilon_1}{\frac{\Delta x}{2}} x \right) \frac{dx}{x - x_0} = -\frac{1}{\pi} \varepsilon_1 \times 1$$

For the interval  $-\frac{\Delta x}{2} < x < \frac{\Delta x}{2}$  equation (26) would yield

$$-\frac{1}{\pi} \int_{-\Delta x/2}^{\Delta x/2} g \frac{dx}{x - x_0} = -\frac{1}{\pi} \left[ (\varepsilon_1 - 0) j_{no}^* + 0 \times j_{no} \right] = -\frac{1}{\pi} \varepsilon_1$$

and no error is introduced. For  $x_0 \neq 0$  there is a very small error which may be avoided by respecting the change of size of the interval near  $x = 0$ .

Also given in figure 4(a) are points of the  $\frac{\Delta v}{V_0}$  curve determined by the method of unequal intervals. Figure 4(b) presents the same information plotted to a larger scale.

For comparative purposes the same problem has been treated by the three methods of computation discussed earlier, namely, those of Naiman, Multhopp, and Timman. Figures 5(a) and 5(b) show the results obtained by the method of Naiman; obviously, the 40-point solution does not use a sufficiently accurate representation of the  $\frac{d(\Delta y_t)}{dx}$  curve, while the 80- and 160-point solutions are quite good, with the exception of the maximum and minimum points of the  $\frac{\Delta v}{V_0}$  curve. In order to obtain a value at approximately  $\frac{x}{c} = 0.036$  a solution involving 320 points would be required. In this respect the method of unequal intervals is more adaptable to special conditions without involving much new work than is the method of Naiman.

The results obtained by Multhopp's method are given in figures 6(a) and 6(b). The 31-point solution (in Multhopp's somewhat odd manner of designation) corresponds to  $\Delta\theta = 5.625^\circ$ ; the 63-point solution, to  $\Delta\theta = 2.8125^\circ$ . The computation is very simple and the results of the method with 63 points are comparable with that of Naiman with 80 points, with the exception of those near the region  $0 < x < 0.01$  (this is shown most clearly in fig. 6(b)). The very steep peak of  $\frac{d(\Delta y_t)}{dx}$  at  $x/c = 0.02$  requires rather high harmonics for the representation of  $\Delta y_t$ ; consequently, good accuracy in the region near the origin may not be expected. This is substantiated by the fact that for the 63-point method the highest effective harmonic would have three waves in the region  $0 < x < 0.04$ ; obviously a sufficient degree of accuracy in the differentiation process cannot be obtained.

As mentioned earlier, Timman's method might be expected to give good results if the size of interval is properly chosen. Inasmuch as only a table for  $\Delta\theta = \frac{360}{36} = 10^\circ$  was available, the result of the computation for  $\frac{\Delta v}{V_0}$  cannot be expected to be good, as is evidenced by observing figure 7. The result obtained is comparable with that of Multhopp's 15-point and Naiman's 40-point solutions.

An excellent method of examining the accuracy of these methods still further is simply that of solving the inverse problem. From the curves of  $\frac{\Delta v}{V_0}$  just discussed, values for  $\frac{d(\Delta y_t)}{dx}$  have been computed

and are presented in figure 8. The method of unequal intervals gives good results, indicating that the arrangement of intervals chosen was as good for the inverse problem as for the direct problem. It is apparent that Naiman's method requires even smaller divisions than 160 points in order to avoid inaccuracies near the point  $x/c = 0.04$ .

The reader may wonder that the inverse problem is not given by Multhopp's method. It must be recalled that Multhopp's method of solving the direct problem does not involve the differentiation of  $\Delta y_t$ ; that is, it is particularly fit for this problem and presents, on the other hand, no analogy for the inverse problem:

$$\frac{d(\Delta y_t)}{dx} = \frac{1}{2\pi} \int_0^{2\pi} \frac{\Delta v}{V_0} \cot \frac{\theta - \theta_0}{2} d\theta = - \frac{1}{\pi} \int_0^{\pi} \frac{\Delta v}{V_0} \frac{\sin \theta_0}{\cos \theta - \cos \theta_0} d\theta$$

Because more extended tables for Timman's method are not available, and the results obtained from the 36-point method for which tables exist are very poor, no further examples of the application of this method will be given.

COMPARISONS OF METHODS OF NAIMAN AND MULTHOPP WITH METHOD EMPLOYING  
UNEQUAL INTERVALS BASED ON ACTUAL EXAMPLES OF CHANGES IN  
AIRFOIL SHAPE

The method of unequal intervals has shown good qualities when applied to a problem where the function  $\sigma(x)$  is known analytically. However, as mentioned earlier, this function is not usually known in analytic form. This section, therefore, will compare the three principle methods, those of Naiman, Multhopp, and unequal intervals, on the basis of actual design problems, solving the direct problem for  $\frac{\Delta v}{V_0}$  and using these results to solve the inverse problem (excluding Multhopp for the inverse problem).

Figure 9(a) shows the  $\Delta y_t$  relations for examples I and II and figure 9(b), the  $\frac{d(\Delta y_t)}{dx}$  relations. Note that the slope of  $\left[ \frac{d(\Delta y_t)}{dx} \right]$  for example II is more than twice that of example I near  $x/c = 0$ .

The direct problem for example I by Naiman's method is given in figure 10. The 160-point solution does not show any appreciable deviation from the 80-point solutions at the region of  $\left(\frac{\Delta v}{v_0}\right)_{\max}$ ; however, near the origin, at  $\left(\frac{\Delta v}{v_0}\right)_{\min}$ , the influence of the smaller-sized intervals ( $80:\Delta\theta = 4.5^\circ$ ;  $160:\Delta\theta = 2.25^\circ$ ) is quite pronounced.

The solution by Multhopp's method is given in figure 11;<sup>6</sup> 31 points around the half circle are not sufficient for a solution comparable with Naiman's 80-point solution, and even a solution based on 63 points does not offer much improvement. The results are poor, as might be expected, in the region very near the origin (see preceding section).

Figure 12 presents the results obtained by the method of unequal intervals, compared with results obtained by Naiman's 80- and 160-point solutions. The method of unequal intervals gives results corresponding to those established by Naiman's 160-point solution. The subdivision used is shown in the figure.

As before, the inverse problem was solved, and is given in figure 13. In each case the computed curve of  $\frac{\Delta v}{v_0}$  was the one used in obtaining the values for the  $\frac{d(\Delta y_t)}{dx}$  curve. Both methods give good results, thus proving that the chosen number of divisions was sufficient in Naiman's method and in the method employing unequal intervals.

The value of  $\frac{d(\Delta y_t)}{dx}$  computed at  $x/c = 0.171$  is of some interest.

This point was computed by the method of unequal intervals in two different ways: First, the arrangement of intervals shown in figure 13 was utilized to compute the lower point. Then a new arrangement of intervals ( $\Delta x = 0.018$  for  $0 < x < 0.36$ ) was set up and the same point computed. The idea was to determine the inaccuracies that would result. One might predict that, since the point  $x/c = 0.171$  lies at a considerable distance from the region of rapid changes in  $\frac{\Delta v}{v_0}$ , errors of only small magnitude would be introduced; this is fairly well substantiated by the results shown in the figure because the error thus introduced is approximately that of the deviation of Naiman's 160-point solution.

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<sup>6</sup>Recall that this method does not involve the differentiation of  $\Delta y_t$ .

Now, turning our attention to example II, which, it will be recalled, has a slope of  $\frac{d(\Delta y_t)}{dx}$  of approximately twice that of example I, the results given in figures 14 to 17 are obtained.

For the direct problem Naiman's method of 160 points and the method employing unequal intervals give results which are in good agreement. For the inverse problem (fig. 17) it is apparent that the method using unequal intervals is superior (see the deviation at  $\left[\frac{d(\Delta y_t)}{dx}\right]_{\max}$  given by the method of Naiman). Multhopp's method gives a rather good result (fig. 15), which may be attained when the Fourier representation of the  $\Delta y$  curve is adequate.

The two examples thus far presented are favorable for Naiman's method because the steep slopes of  $\sigma(x)$  occur near  $x = 0$  where the points Naiman uses are close together. However, going to still steeper slopes near  $x = 0$  would require a rapidly increasing number of points. The new method offers another possibility here. Assume that in that critical region  $x_k < x < x_{k+1}$  ( $x_k$  may be 0)  $\sigma(x)$  may be represented by  $\sigma(x) = \sum a_n x^n$ . Then the integral

$$\int_0^c \frac{\sigma(x)}{x - x_0} dx$$

may be split into three integrals

$$\int_0^c \frac{\sigma(x)}{x - x_0} dx = \int_0^{x_k} \frac{\sigma(x)}{x - x_0} dx + \int_{x_k}^{x_{k+1}} \frac{\sigma(x)}{x - x_0} dx + \int_{x_{k+1}}^c \frac{\sigma(x)}{x - x_0} dx \quad (41)$$

The first and third of these integrals may be solved in the usual manner using the functions  $j_{no}$  and  $j_{no}^*$ . The second integral will be solved analytically.

This simple form, due to the use of the coordinate  $x$  in the Poisson integral, allows a rapid integration, because the integral

$$k_{n,o} = \int_{x_k}^{x_{k+1}} \frac{x^n}{x - x_0} dx$$

can be solved by recurrence as follows:

$$k_{n,o} = \frac{x_{k+1}^n - x_k^n}{n} + x_0 k_{n-1,o} \quad \text{for } n \geq 1 \quad (42)$$

with

$$k_{0,o} = j_{no} \left( \frac{x_k - x_0}{x_{k+1} - x_k} \right) \quad (43)$$

Thus even very steep slopes cause no difficulties.

As already mentioned, examples I and II correspond well to the qualities demanded by Naiman's method insofar as the rather steep slopes occur in those portions where the points  $\theta_n$  are close together. If those steep slopes should occur in other portions of the chord, however, a very great number of points in the Naiman method would be needed in order to represent  $\sigma(x)$  adequately, and to get reliable results. In such a case the method using unequal intervals shows its advantage by allowing a free subdivision of the chord.

A third example will serve to illustrate this. Figure 18 shows a function  $\sigma(x) = \frac{d(\Delta y_t)}{dx}$ . The essential values of the function lie in a part of the chord where even Naiman's method with 160 points is not sufficient to represent the function accurately. This is forcibly shown by the two curves of  $\frac{\Delta v}{V_0}$ . If the function  $\sigma(x)$  is modified (dotted line) so as to eliminate the high peak, then the  $\frac{\Delta v}{V_0}$  curve by unequal intervals can be made to agree with the original  $\frac{\Delta v}{V_0}$  by Naiman's 160-point solution, thus definitely proving that, in this example, Naiman's method with 160 points is insufficient.

Table III indicates the computation for the point  $x_0 = 0.065$  by unequal intervals.



## CONCLUDING DISCUSSION

The new method of evaluating the Poisson integral developed herein is to be recommended for all those functions  $\sigma(x)$ , where steep slopes in small portions of the region to be integrated exist. In these portions a very small size of interval may be chosen without requiring that this same size of interval be used throughout the region of integration. In this manner, the work required for computation may be maintained at a reasonable level even for the most complicated problems.

The analytical treatment of special parts of the integral is possible (evaluating the remainder by the new method; see preceding section). In those problems where a transition to very small intervals in part of the integration range would require the determination of a great many values of  $\sigma_n$ , this idea might be used to advantage.

It should be noted that the smoothness of the function  $\sigma(x)$  and its accurate representation by single points is essential for good results. If, for example, single points  $\sigma_n$  are simply taken from a curve for  $x_n$  very close to one another it may be compulsory to check these values by a table of differences.

Stanford University  
Stanford, Calif., December 6, 1950

APPENDIX A  
VALUES OF  $b_{vm}$  FOR  $n_1 = 63$

$\nu$	1	3	5	7	9	11	13	15	17	19	21	23	25	27	29	31	$b_{vm}$	$n$
$\nu$	536.5974	109.0141	65.8699	47.4876	37.4851	31.1890	26.8610	23.8240	21.5948	19.9200	18.6545	17.6989	16.9936	16.4942	16.1752	16.0192	$b_{vm}$	$n$
2	117.7031	43.5039	24.4288	16.2670	12.1841	9.0810	6.8418	5.1237	3.8146	2.8098	2.0065	1.4048	1.0056	0.7027	0.5021	0.3017		62
4	9.5228	45.8468	25.5068	1.9794	.5175	.8015	.0967	.0530	.0319	.0206	.0140	.0100	.0073	.0056	.0044	.0036		60
6	2.5926	4.5825	26.6982	18.9041	1.4805	.4680	.1920	.0975	.0558	.0347	.0233	.0161	.0118	.0089	.0069	.0058		58
8	1.0858	1.4036	2.8072	19.1848	15.1443	1.3882	.4108	.1788	.0939	.0554	.0336	.0248	.0174	.0129	.0098	.0078		56
10	.8395	.6410	.9490	2.0744	15.1485	12.8185	1.1578	.3703	.1684	.0899	.0544	.0356	.0249	.0181	.0136	.0107		54
12	.3100	.5491	.4323	.7183	1.6605	12.5828	10.8609	1.0699	.3398	.1561	.0862	.0638	.0364	.0261	.0186	.0142		52
14	.1944	.8122	.2653	.5491	.8777	1.3788	10.8639	9.6947	.9643	.3183	.1490	.0831	.0581	.0332	.0235	.0169		50
16	.1300	.1688	.1898	.8011	.9850	.4885	1.1970	9.6917	8.7687	.8896	.2967	.1414	.0808	.0513	.0361	.0255		48
18	.0910	.0960	.1078	.1881	.1585	.2421	1.0680	8.7421	7.9460	.7702	.2820	.1364	.0768	.0508	.0352	.0252		46
20	.0655	.0682	.0748	.0682	.1067	.1406	.2093	.3738	.9538	7.9895	7.4840	.7828	.2686	.1313	.0768	.0601		44
22	.0496	.0814	.0854	.0624	.0736	.0922	1.251	.1998	.8438	.8913	7.5161	7.1773	.7650	.2542	.1308	.0778		42
24	.0320	.0392	.0418	.0462	.0631	.0638	.0816	.1117	.1750	.3182	.8506	7.1618	6.9070	.7392	.2594	.1897		40
26	.0298	.0306	.0324	.0332	.0394	.0464	.0569	.0735	.1029	.1605	.2986	.7948	6.8901	6.6451	.7250	.2666		38
28	.0228	.0243	.0255	.0275	.0306	.0349	.0414	.0514	.0674	.0965	.1505	.2837	.7616	6.6920	6.5771	.7161		36
30	.0190	.0198	.0204	.0218	.0240	.0269	.0313	.0376	.0472	.0628	.0898	.1431	.2722	.7394	6.5335	6.5062		34
32	.0156	.0159	.0168	.0177	.0191	.0212	.0242	.0284	.0346	.0441	.0691	.0866	.1376	.2848	.6316	6.8104		32
34	.0129	.0132	.0138	.0144	.0154	.0170	.0191	.0221	.0262	.0323	.0418	.0864	.0823	.1338	.2697	.7203		30
36	.0108	.0110	.0113	.0119	.0127	.0138	.0153	.0175	.0204	.0245	.0305	.0396	.0541	.0798	.1511	.2572		28
38	.0089	.0091	.0094	.0098	.0105	.0114	.0125	.0140	.0162	.0191	.0230	.0290	.0380	.0526	.0782	.1298		26
40	.0075	.0077	.0079	.0082	.0085	.0092	.0102	.0115	.0130	.0150	.0180	.0219	.0278	.0369	.0515	.0775		24
42	.0064	.0065	.0065	.0069	.0075	.0078	.0086	.0095	.0106	.0121	.0142	.0171	.0211	.0270	.0360	.0509		22
44	.0052	.0053	.0054	.0056	.0059	.0063	.0068	.0075	.0082	.0094	.0110	.0129	.0156	.0194	.0250	.0335		20
46	.0046	.0046	.0047	.0049	.0051	.0054	.0059	.0064	.0071	.0080	.0091	.0107	.0129	.0168	.0219	.0299		18
48	.0039	.0039	.0040	.0041	.0043	.0045	.0049	.0055	.0062	.0072	.0083	.0098	.0123	.0152	.0203	.0283		16
50	.0031	.0031	.0032	.0034	.0035	.0038	.0040	.0043	.0048	.0055	.0066	.0081	.0098	.0124	.0157	.0216		14
52	.0025	.0025	.0026	.0027	.0028	.0030	.0032	.0035	.0039	.0045	.0054	.0065	.0078	.0094	.0117	.0146		12
54	.0020	.0020	.0021	.0022	.0023	.0024	.0026	.0028	.0030	.0034	.0040	.0048	.0058	.0070	.0085	.0112		10
56	.0016	.0016	.0016	.0017	.0018	.0018	.0020	.0021	.0023	.0026	.0031	.0038	.0048	.0058	.0072	.0088		8
58	.0012	.0012	.0012	.0012	.0013	.0014	.0014	.0016	.0017	.0018	.0021	.0025	.0030	.0037	.0044	.0054		6
60	.0008	.0008	.0008	.0008	.0008	.0009	.0009	.0010	.0011	.0012	.0013	.0015	.0016	.0017	.0018	.0020		4
62	.0004	.0004	.0004	.0004	.0004	.0004	.0005	.0005	.0005	.0006	.0007	.0007	.0008	.0008	.0008	.0008		2
	63	61	59	57	55	53	51	49	47	45	43	41	39	37	35	33	$\nu$	

$\nu$	2	4	6	8	10	12	14	16	18	20	22	24	26	28	30	32	$\frac{h\nu}{n}$
$\frac{h\nu}{n}$	163.3820	82.0134	55.1021	41.8104	33.9472	28.7992	25.2183	22.6273	20.6926	19.4730	18.1414	17.3183	16.7205	16.3135	16.0773	16.0000	$\frac{h\nu}{n}$
1	58.9176	2.3635	0.4377	0.1566	0.0661	0.0274	0.0150	0.0090	0.0058	0.0039	0.0028	0.0020	0.0015	0.0012	0.0009	0.0008	63
3	63.7000	28.7600	8.2050	2.5283	1.1998	0.5922	0.491	0.288	0.182	0.122	0.086	0.062	0.047	0.036	0.029	0.023	61
5	6.0252	31.6326	22.5288	1.7821	1.4892	1.077	0.978	0.549	0.337	0.221	0.153	0.110	0.082	0.063	0.050	0.040	59
7	1.6220	5.4125	21.9364	16.9222	1.4830	1.4347	1.254	0.958	0.658	0.384	0.235	0.168	0.124	0.094	0.074	0.059	57
9	0.5050	1.1541	2.3967	17.1222	15.6528	1.2700	1.295	1.122	0.919	0.550	0.357	0.246	0.177	0.133	0.105	0.082	55
11	0.2264	0.5312	0.8178	1.6573	15.0468	11.6391	1.1170	1.356	1.610	0.979	0.552	0.352	0.249	0.183	0.159	0.109	53
13	0.2526	0.2953	0.3940	0.692	1.6011	11.6339	10.2476	1.0073	0.828	1.517	0.945	0.586	0.354	0.252	0.187	0.144	51
15	0.1623	0.1624	0.2250	0.3156	0.8875	1.2793	10.1253	9.2053	9.252	0.555	1.444	0.915	0.517	0.352	0.254	0.191	49
17	0.1106	0.1211	0.1423	0.1819	0.2680	0.4529	1.1222	9.1221	8.3291	0.8201	0.222	1.527	0.764	0.510	0.352	0.257	47
19	0.0786	0.0846	0.0968	0.1166	0.1631	0.2257	0.3990	1.0103	8.3267	7.7950	0.8112	0.2767	1.346	0.722	0.506	0.354	45
21	0.0572	0.0615	0.0693	0.0829	0.0990	0.1331	0.1999	0.3598	9.249	7.7919	7.3236	0.7760	0.877	1.317	0.774	0.507	43
23	0.0439	0.0461	0.0504	0.0573	0.0664	0.0866	0.1125	0.1807	0.3999	0.8613	7.3268	7.0274	0.7809	0.815	1.300	0.773	41
25	0.0340	0.0365	0.0393	0.0427	0.0495	0.0602	0.0774	0.1222	0.3076	0.8146	7.0328	6.7793	0.7312	0.2575	1.296	0.773	39
27	0.0268	0.0278	0.0297	0.0327	0.0371	0.0438	0.0529	0.0704	0.0922	1.561	0.922	0.2777	0.7496	0.2535	0.2507	1.296	37
29	0.0215	0.0222	0.0233	0.0256	0.0284	0.0330	0.0394	0.0492	0.0650	0.925	1.467	0.2777	0.7496	0.2535	0.2507	1.296	35
31	0.0174	0.0180	0.0189	0.0204	0.0225	0.0256	0.0298	0.0360	0.0455	0.0608	0.0875	1.402	0.2879	0.7315	0.2529	1.296	33
33	0.0145	0.0147	0.0154	0.0166	0.0180	0.0201	0.0231	0.0273	0.0324	0.0427	0.0676	0.0937	1.358	0.2619	0.2522	1.296	31
35	0.0118	0.0122	0.0127	0.0136	0.0146	0.0162	0.0183	0.0212	0.0253	0.0313	0.0404	0.0651	0.0909	1.322	0.2521	0.2522	29
37	0.0099	0.0101	0.0105	0.0111	0.0120	0.0131	0.0147	0.0168	0.0197	0.0252	0.0297	0.0527	0.0853	0.0990	1.294	0.2522	27
39	0.0083	0.0086	0.0088	0.0092	0.0099	0.0106	0.0119	0.0138	0.0166	0.0223	0.0283	0.0374	0.0520	0.0772	1.296	0.2522	25
41	0.0070	0.0071	0.0074	0.0077	0.0082	0.0089	0.0098	0.0110	0.0128	0.0146	0.0178	0.0215	0.0274	0.0344	0.0412	0.0473	23
43	0.0062	0.0060	0.0062	0.0065	0.0069	0.0074	0.0081	0.0090	0.0102	0.0117	0.0138	0.0167	0.0207	0.0266	0.0329	0.0397	21
45	0.0050	0.0050	0.0052	0.0054	0.0057	0.0062	0.0067	0.0074	0.0085	0.0095	0.0110	0.0131	0.0160	0.0201	0.0261	0.0324	19
47	0.0042	0.0042	0.0044	0.0045	0.0048	0.0051	0.0056	0.0062	0.0072	0.0082	0.0099	0.0124	0.0156	0.0196	0.0257	0.0327	17
49	0.0035	0.0035	0.0036	0.0037	0.0040	0.0042	0.0046	0.0050	0.0058	0.0068	0.0081	0.0098	0.0120	0.0149	0.0191	0.0241	15
51	0.0029	0.0029	0.0030	0.0031	0.0032	0.0035	0.0037	0.0041	0.0048	0.0056	0.0067	0.0082	0.0098	0.0120	0.0144	0.0184	13
53	0.0023	0.0024	0.0024	0.0025	0.0026	0.0028	0.0030	0.0033	0.0036	0.0040	0.0045	0.0052	0.0061	0.0072	0.0086	0.0109	11
55	0.0018	0.0019	0.0019	0.0020	0.0021	0.0022	0.0024	0.0026	0.0028	0.0031	0.0035	0.0040	0.0047	0.0056	0.0068	0.0082	9
57	0.0014	0.0014	0.0015	0.0015	0.0016	0.0017	0.0018	0.0019	0.0021	0.0023	0.0025	0.0028	0.0032	0.0038	0.0049	0.0059	7
59	0.0010	0.0010	0.0010	0.0010	0.0011	0.0012	0.0012	0.0013	0.0015	0.0016	0.0018	0.0021	0.0024	0.0028	0.0035	0.0040	5
61	0.0006	0.0006	0.0006	0.0006	0.0006	0.0007	0.0007	0.0008	0.0009	0.0010	0.0011	0.0012	0.0014	0.0016	0.0019	0.0023	3
63	0.0002	0.0002	0.0002	0.0002	0.0002	0.0002	0.0002	0.0002	0.0003	0.0003	0.0004	0.0004	0.0005	0.0006	0.0006	0.0008	1
	62	60	58	56	54	52	50	48	46	44	42	40	38	36	34	32	$\nu$

## APPENDIX B

VALUES OF  $j_{no}$  AND  $j_{no}^*$  AS FUNCTIONS OF  $\frac{x_n - x_0}{\Delta x}$ 

The values of the functions  $j_{no}$  and  $j_{no}^*$  are presented as indicated in the following table. The values are tabulated in a form selected to minimize the necessity for interpolation except for the region containing the singularities of the functions  $j_{no}$  and  $j_{no}^*$ . For ease in computation, tables B-I to B-VIII, inclusive, are arranged so that the vertical increment of  $\frac{x_n - x_0}{\Delta x}$  is unity. Table B-IX gives additional values for the region containing the singularities of the functions  $j_{no}$  and  $j_{no}^*$ .

TABLE NO.	RANGE OF $\frac{x_n - x_0}{\Delta x}$	INCREMENT OF $\frac{x_n - x_0}{\Delta x}$
B-I	-189 to -90	1.0
B-II	-89.5 to -40.0	.5
B-III	-39.9 to -20.0	.1
B-IV	-19.99 to 0	.01
B-V	0 to 19.99	.01
B-VI	20.0 to 39.9	.1
B-VII	40.0 to 89.5	.5
B-VIII	90 to 189	1.0
B-IX	-1.000 to 0.000	0.001

TABLE B-I.- VALUES OF  $j_{no}$  AND  $j_{no}^*$  USED IN EVALUATING EQUATION (26)

$$-189 \leq \frac{x_n - x_0}{\Delta x} \leq -90$$

$\frac{x_n - x_0}{\Delta x}$	-18x.0		-17x.0		-16x.0		-15x.0		-14x.0		-13x.0		-12x.0		-11x.0		-10x.0		-9x.0	
	$j_{no}$	$j_{no}^*$	$j_{no}$	$j_{no}^*$	$j_{no}$	$j_{no}^*$	$j_{no}$	$j_{no}^*$	$j_{no}$	$j_{no}^*$	$j_{no}$	$j_{no}^*$	$j_{no}$	$j_{no}^*$	$j_{no}$	$j_{no}^*$	$j_{no}$	$j_{no}^*$	$j_{no}$	$j_{no}^*$
9	-0.0053	-0.0027	-0.0056	-0.0028	-0.0059	-0.0030	-0.0063	-0.0032	-0.0067	-0.0034	-0.0072	-0.0036	-0.0078	-0.0039	-0.0084	-0.0042	-0.0092	-0.0046	-0.0102	-0.0051
8	-0.0053	-0.0027	-0.0056	-0.0028	-0.0060	-0.0030	-0.0063	-0.0032	-0.0068	-0.0034	-0.0073	-0.0036	-0.0078	-0.0039	-0.0085	-0.0043	-0.0093	-0.0047	-0.0103	-0.0051
7	-0.0054	-0.0027	-0.0057	-0.0028	-0.0060	-0.0030	-0.0064	-0.0032	-0.0068	-0.0034	-0.0073	-0.0037	-0.0079	-0.0040	-0.0086	-0.0043	-0.0094	-0.0047	-0.0104	-0.0052
6	-0.0054	-0.0027	-0.0057	-0.0029	-0.0060	-0.0030	-0.0064	-0.0032	-0.0069	-0.0034	-0.0074	-0.0037	-0.0080	-0.0040	-0.0087	-0.0043	-0.0095	-0.0047	-0.0105	-0.0053
5	-0.0054	-0.0027	-0.0057	-0.0029	-0.0061	-0.0030	-0.0065	-0.0032	-0.0069	-0.0035	-0.0074	-0.0037	-0.0080	-0.0040	-0.0087	-0.0044	-0.0096	-0.0047	-0.0106	-0.0053
4	-0.0054	-0.0027	-0.0058	-0.0029	-0.0061	-0.0031	-0.0065	-0.0033	-0.0070	-0.0035	-0.0075	-0.0037	-0.0081	-0.0041	-0.0088	-0.0044	-0.0097	-0.0048	-0.0107	-0.0053
3	-0.0055	-0.0027	-0.0058	-0.0029	-0.0062	-0.0031	-0.0066	-0.0033	-0.0070	-0.0035	-0.0075	-0.0038	-0.0082	-0.0041	-0.0089	-0.0045	-0.0098	-0.0049	-0.0108	-0.0054
2	-0.0055	-0.0028	-0.0058	-0.0029	-0.0062	-0.0031	-0.0066	-0.0033	-0.0071	-0.0035	-0.0076	-0.0038	-0.0082	-0.0041	-0.0090	-0.0045	-0.0099	-0.0049	-0.0109	-0.0055
1	-0.0055	-0.0028	-0.0059	-0.0029	-0.0062	-0.0031	-0.0066	-0.0033	-0.0071	-0.0036	-0.0077	-0.0038	-0.0083	-0.0042	-0.0090	-0.0045	-0.0100	-0.0050	-0.0110	-0.0055
0	-0.0056	-0.0028	-0.0059	-0.0030	-0.0063	-0.0031	-0.0067	-0.0033	-0.0072	-0.0036	-0.0077	-0.0039	-0.0084	-0.0042	-0.0091	-0.0046	-0.0101	-0.0050	-0.0112	-0.0056

TABLE B-II.- VALUES OF  $j_{no}$  AND  $j_{no}^*$  USED IN EVALUATING EQUATION (26)

$$-89.5 \leq \frac{x_n - x_0}{\Delta x} \leq -40.0$$

$\frac{x_n - x_0}{\Delta x}$	-8x.5		-8x.0		-7x.5		-7x.0		-6x.5		-6x.0		-5x.5		-5x.0		-4x.5		-4x.0	
	$j_{no}$	$j_{no}^*$	$j_{no}$	$j_{no}^*$	$j_{no}$	$j_{no}^*$	$j_{no}$	$j_{no}^*$	$j_{no}$	$j_{no}^*$	$j_{no}$	$j_{no}^*$	$j_{no}$	$j_{no}^*$	$j_{no}$	$j_{no}^*$	$j_{no}$	$j_{no}^*$	$j_{no}$	$j_{no}^*$
9	-0.0112	-0.0056	-0.0113	-0.0057	-0.0127	-0.0064	-0.0127	-0.0064	-0.0145	-0.0073	-0.0146	-0.0073	-0.0169	-0.0085	-0.0171	-0.0085	-0.0204	-0.0102	-0.0206	-0.0103
8	-0.0114	-0.0057	-0.0114	-0.0058	-0.0128	-0.0064	-0.0129	-0.0064	-0.0147	-0.0074	-0.0148	-0.0074	-0.0172	-0.0086	-0.0174	-0.0087	-0.0208	-0.0104	-0.0211	-0.0105
7	-0.0115	-0.0058	-0.0116	-0.0058	-0.0130	-0.0065	-0.0131	-0.0065	-0.0149	-0.0075	-0.0150	-0.0075	-0.0175	-0.0088	-0.0177	-0.0089	-0.0213	-0.0107	-0.0215	-0.0108
6	-0.0116	-0.0058	-0.0117	-0.0059	-0.0132	-0.0066	-0.0132	-0.0067	-0.0152	-0.0076	-0.0153	-0.0076	-0.0179	-0.0090	-0.0180	-0.0090	-0.0217	-0.0109	-0.0220	-0.0110
5	-0.0118	-0.0059	-0.0118	-0.0059	-0.0133	-0.0067	-0.0134	-0.0067	-0.0154	-0.0077	-0.0155	-0.0078	-0.0182	-0.0092	-0.0184	-0.0093	-0.0222	-0.0112	-0.0225	-0.0112
4	-0.0119	-0.0059	-0.0120	-0.0060	-0.0135	-0.0067	-0.0136	-0.0068	-0.0156	-0.0078	-0.0157	-0.0079	-0.0185	-0.0093	-0.0187	-0.0094	-0.0227	-0.0114	-0.0230	-0.0116
3	-0.0120	-0.0060	-0.0121	-0.0061	-0.0137	-0.0068	-0.0138	-0.0069	-0.0159	-0.0079	-0.0160	-0.0080	-0.0189	-0.0094	-0.0190	-0.0095	-0.0233	-0.0117	-0.0235	-0.0118
2	-0.0122	-0.0061	-0.0123	-0.0061	-0.0139	-0.0070	-0.0140	-0.0070	-0.0161	-0.0081	-0.0163	-0.0081	-0.0192	-0.0096	-0.0194	-0.0097	-0.0238	-0.0120	-0.0241	-0.0121
1	-0.0123	-0.0062	-0.0124	-0.0062	-0.0141	-0.0071	-0.0142	-0.0071	-0.0164	-0.0082	-0.0165	-0.0083	-0.0196	-0.0099	-0.0198	-0.0100	-0.0244	-0.0122	-0.0247	-0.0124
0	-0.0125	-0.0062	-0.0126	-0.0063	-0.0143	-0.0071	-0.0144	-0.0072	-0.0167	-0.0084	-0.0168	-0.0084	-0.0200	-0.0101	-0.0202	-0.0102	-0.0250	-0.0125	-0.0253	-0.0127



TABLE B-III.- VALUES OF  $j_{no}$  AND  $j_{no}^*$  USED IN EVALUATING EQUATION (26)

$$-39.9 \leq \frac{I_n - I_0}{\Delta x} \leq -20.0$$

I $\frac{I_n - I_0}{\Delta x}$	9		8		7		6		5		4		3		2		1		0	
	$j_{no}$	$j_{no}^*$	$j_{no}$	$j_{no}^*$	$j_{no}$	$j_{no}^*$	$j_{no}$	$j_{no}^*$	$j_{no}$	$j_{no}^*$	$j_{no}$	$j_{no}^*$	$j_{no}$	$j_{no}^*$	$j_{no}$	$j_{no}^*$	$j_{no}$	$j_{no}^*$	$j_{no}$	$j_{no}^*$
-39.I	-0.0254	-0.0127	-0.0254	-0.0128	-0.0255	-0.0128	-0.0256	-0.0128	-0.0256	-0.0129	-0.0257	-0.0129	-0.0258	-0.0130	-0.0258	-0.0130	-0.0259	-0.0130	-0.0260	-0.0131
-38.	-0.0260	-0.0131	-0.0261	-0.0131	-0.0262	-0.0132	-0.0262	-0.0132	-0.0263	-0.0132	-0.0264	-0.0133	-0.0265	-0.0133	-0.0265	-0.0133	-0.0266	-0.0134	-0.0267	-0.0134
-37.	-0.0267	-0.0134	-0.0268	-0.0135	-0.0269	-0.0135	-0.0270	-0.0135	-0.0270	-0.0136	-0.0271	-0.0137	-0.0272	-0.0137	-0.0273	-0.0137	-0.0273	-0.0137	-0.0274	-0.0138
-36.	-0.0275	-0.0138	-0.0276	-0.0138	-0.0276	-0.0139	-0.0277	-0.0139	-0.0278	-0.0139	-0.0279	-0.0140	-0.0279	-0.0140	-0.0280	-0.0141	-0.0281	-0.0141	-0.0282	-0.0141
-35.	-0.0283	-0.0142	-0.0283	-0.0142	-0.0284	-0.0142	-0.0285	-0.0143	-0.0285	-0.0143	-0.0287	-0.0144	-0.0287	-0.0145	-0.0288	-0.0145	-0.0289	-0.0145	-0.0290	-0.0146
-34.	-0.0291	-0.0146	-0.0292	-0.0146	-0.0292	-0.0147	-0.0293	-0.0147	-0.0294	-0.0148	-0.0295	-0.0148	-0.0296	-0.0149	-0.0297	-0.0149	-0.0298	-0.0150	-0.0299	-0.0150
-33.	-0.0299	-0.0150	-0.0300	-0.0151	-0.0301	-0.0151	-0.0302	-0.0152	-0.0303	-0.0153	-0.0304	-0.0153	-0.0305	-0.0154	-0.0306	-0.0154	-0.0307	-0.0154	-0.0308	-0.0155
-32.	-0.0309	-0.0156	-0.0310	-0.0156	-0.0311	-0.0156	-0.0312	-0.0157	-0.0313	-0.0157	-0.0314	-0.0158	-0.0315	-0.0158	-0.0315	-0.0158	-0.0316	-0.0159	-0.0317	-0.0160
-31.	-0.0319	-0.0160	-0.0320	-0.0161	-0.0321	-0.0161	-0.0322	-0.0162	-0.0323	-0.0162	-0.0324	-0.0163	-0.0325	-0.0163	-0.0326	-0.0164	-0.0327	-0.0164	-0.0328	-0.0165
-30.	-0.0329	-0.0165	-0.0330	-0.0166	-0.0331	-0.0166	-0.0332	-0.0167	-0.0333	-0.0167	-0.0334	-0.0168	-0.0336	-0.0169	-0.0337	-0.0169	-0.0338	-0.0170	-0.0339	-0.0171
-29.	-0.0340	-0.0171	-0.0341	-0.0172	-0.0342	-0.0172	-0.0344	-0.0173	-0.0345	-0.0173	-0.0346	-0.0174	-0.0347	-0.0175	-0.0348	-0.0175	-0.0350	-0.0176	-0.0351	-0.0176
-28.	-0.0352	-0.0177	-0.0353	-0.0178	-0.0355	-0.0178	-0.0356	-0.0179	-0.0357	-0.0180	-0.0358	-0.0180	-0.0360	-0.0181	-0.0361	-0.0182	-0.0362	-0.0182	-0.0364	-0.0183
-27.	-0.0365	-0.0184	-0.0366	-0.0184	-0.0368	-0.0185	-0.0369	-0.0186	-0.0370	-0.0186	-0.0372	-0.0187	-0.0373	-0.0188	-0.0375	-0.0188	-0.0376	-0.0189	-0.0377	-0.0190
-26.	-0.0379	-0.0191	-0.0380	-0.0191	-0.0382	-0.0192	-0.0383	-0.0193	-0.0385	-0.0193	-0.0386	-0.0194	-0.0388	-0.0195	-0.0389	-0.0196	-0.0391	-0.0196	-0.0392	-0.0197
-25.	-0.0394	-0.0198	-0.0395	-0.0199	-0.0397	-0.0200	-0.0398	-0.0200	-0.0400	-0.0201	-0.0402	-0.0202	-0.0403	-0.0203	-0.0405	-0.0204	-0.0407	-0.0205	-0.0408	-0.0206
-24.	-0.0410	-0.0206	-0.0412	-0.0207	-0.0413	-0.0208	-0.0415	-0.0209	-0.0417	-0.0210	-0.0418	-0.0211	-0.0420	-0.0211	-0.0422	-0.0212	-0.0424	-0.0213	-0.0426	-0.0214
-23.	-0.0427	-0.0215	-0.0429	-0.0216	-0.0431	-0.0217	-0.0433	-0.0218	-0.0435	-0.0219	-0.0437	-0.0219	-0.0439	-0.0221	-0.0441	-0.0222	-0.0443	-0.0223	-0.0444	-0.0223
-22.	-0.0447	-0.0225	-0.0449	-0.0226	-0.0451	-0.0227	-0.0453	-0.0228	-0.0455	-0.0229	-0.0457	-0.0230	-0.0459	-0.0231	-0.0461	-0.0232	-0.0463	-0.0233	-0.0465	-0.0235
-21.	-0.0467	-0.0236	-0.0470	-0.0237	-0.0472	-0.0238	-0.0474	-0.0239	-0.0476	-0.0240	-0.0479	-0.0241	-0.0481	-0.0242	-0.0483	-0.0243	-0.0486	-0.0244	-0.0488	-0.0246
-20.I	-0.0490	-0.0247	-0.0493	-0.0248	-0.0495	-0.0250	-0.0498	-0.0251	-0.0500	-0.0252	-0.0503	-0.0253	-0.0505	-0.0255	-0.0508	-0.0256	-0.0510	-0.0257	-0.0513	-0.0259

















TABLE B-V. - CONTINUED

(c)  $0.XX \leq \frac{X_{II} - X_0}{\Delta X} \leq 19.XX$  where  $20 \leq XX \leq 29$

II $\frac{X_{II} - X_0}{\Delta X}$	20		21		22		23		24		25		26		27		28		29	
	$\downarrow_{no}$	$\downarrow_{no}^*$	$\downarrow_{no}$	$\downarrow_{no}^*$	$\downarrow_{no}$	$\downarrow_{no}^*$	$\downarrow_{no}$	$\downarrow_{no}^*$	$\downarrow_{no}$	$\downarrow_{no}^*$	$\downarrow_{no}$	$\downarrow_{no}^*$	$\downarrow_{no}$	$\downarrow_{no}^*$	$\downarrow_{no}$	$\downarrow_{no}^*$	$\downarrow_{no}$	$\downarrow_{no}^*$	$\downarrow_{no}$	$\downarrow_{no}^*$
0.XX	1.7918	0.6416	1.7713	0.6322	1.7530	0.6231	1.7367	0.6144	1.7222	0.6059	1.7094	0.5976	1.6983	0.5897	1.6883	0.5819	1.6798	0.5744	1.6725	0.5678
1.	.6661	.4726	.6604	.4711	.6557	.4696	.6510	.4648	.6463	.4601	.6416	.4553	.6370	.4506	.6323	.4458	.6276	.4411	.6230	.4363
2.	.3747	.1797	.3732	.1791	.3719	.1784	.3705	.1778	.3691	.1772	.3678	.1765	.3664	.1758	.3650	.1751	.3637	.1744	.3623	.1737
3.	.2719	.1398	.2712	.1393	.2705	.1389	.2697	.1384	.2690	.1379	.2682	.1373	.2675	.1368	.2667	.1362	.2660	.1357	.2652	.1351
4.	.2136	.1030	.2131	.1028	.2127	.1026	.2122	.1023	.2118	.1021	.2113	.1019	.2109	.1017	.2104	.1015	.2100	.1013	.2095	.1011
5.	.1759	.0824	.1756	.0822	.1753	.0821	.1750	.0820	.1747	.0819	.1744	.0818	.1741	.0817	.1739	.0816	.1737	.0815	.1735	.0814
6.	.1499	.0729	.1493	.0728	.1491	.0727	.1489	.0726	.1486	.0725	.1484	.0724	.1482	.0723	.1480	.0722	.1478	.0721	.1477	.0720
7.	.1301	.0636	.1299	.0635	.1297	.0634	.1295	.0633	.1293	.0632	.1292	.0631	.1290	.0630	.1289	.0629	.1287	.0628	.1286	.0627
8.	.1151	.0564	.1149	.0564	.1148	.0563	.1147	.0562	.1145	.0561	.1144	.0560	.1143	.0559	.1142	.0558	.1141	.0557	.1140	.0556
9.	.1032	.0507	.1031	.0506	.1030	.0505	.1029	.0504	.1027	.0503	.1027	.0502	.1025	.0501	.1024	.0500	.1023	.0499	.1022	.0498
10.	.0935	.0460	.0934	.0460	.0933	.0459	.0932	.0458	.0931	.0457	.0930	.0456	.0929	.0455	.0928	.0454	.0927	.0453	.0926	.0452
11.	.0855	.0421	.0854	.0421	.0853	.0420	.0852	.0419	.0851	.0418	.0850	.0417	.0849	.0416	.0848	.0415	.0847	.0414	.0846	.0413
12.	.0788	.0389	.0787	.0388	.0787	.0388	.0786	.0387	.0785	.0386	.0784	.0385	.0783	.0384	.0782	.0383	.0781	.0382	.0780	.0381
13.	.0730	.0361	.0730	.0360	.0729	.0360	.0729	.0359	.0728	.0358	.0727	.0357	.0726	.0356	.0725	.0355	.0724	.0354	.0723	.0353
14.	.0681	.0336	.0680	.0335	.0680	.0334	.0679	.0333	.0678	.0332	.0677	.0331	.0676	.0330	.0675	.0329	.0674	.0328	.0673	.0327
15.	.0637	.0315	.0637	.0314	.0636	.0313	.0635	.0312	.0634	.0311	.0633	.0310	.0632	.0309	.0631	.0308	.0630	.0307	.0629	.0306
16.	.0599	.0297	.0599	.0296	.0598	.0295	.0598	.0294	.0597	.0293	.0596	.0292	.0595	.0291	.0594	.0290	.0593	.0289	.0592	.0288
17.	.0566	.0280	.0565	.0279	.0565	.0278	.0564	.0277	.0563	.0276	.0562	.0275	.0561	.0274	.0560	.0273	.0559	.0272	.0558	.0271
18.	.0538	.0263	.0537	.0262	.0537	.0261	.0536	.0260	.0535	.0259	.0534	.0258	.0533	.0257	.0532	.0256	.0531	.0255	.0530	.0254
19.XX	.0508	.0248	.0507	.0247	.0507	.0246	.0507	.0245	.0506	.0244	.0505	.0243	.0504	.0242	.0503	.0241	.0502	.0240	.0501	.0239

TABLE B-V. - CONTINUED

(d)  $0.XX \leq \frac{X_{II} - X_0}{\Delta X} \leq 19.XX$  where  $30 \leq XX \leq 39$

II $\frac{X_{II} - X_0}{\Delta X}$	30		31		32		33		34		35		36		37		38		39	
	$\downarrow_{no}$	$\downarrow_{no}^*$	$\downarrow_{no}$	$\downarrow_{no}^*$	$\downarrow_{no}$	$\downarrow_{no}^*$	$\downarrow_{no}$	$\downarrow_{no}^*$	$\downarrow_{no}$	$\downarrow_{no}^*$	$\downarrow_{no}$	$\downarrow_{no}^*$	$\downarrow_{no}$	$\downarrow_{no}^*$	$\downarrow_{no}$	$\downarrow_{no}^*$	$\downarrow_{no}$	$\downarrow_{no}^*$	$\downarrow_{no}$	$\downarrow_{no}^*$
0.XX	1.4669	0.5661	1.4412	0.5582	1.4171	0.5510	1.3938	0.5440	1.3713	0.5377	1.3498	0.5311	1.3282	0.5250	1.3074	0.5194	1.2872	0.5143	1.2683	0.5094
1.	.7905	.5993	.7872	.5969	.7839	.5946	.7807	.5923	.7774	.5900	.7742	.5877	.7710	.5854	.7678	.5831	.7646	.5808	.7614	.5785
2.	.5610	.4697	.5597	.4691	.5584	.4686	.5571	.4680	.5558	.4674	.5545	.4668	.5532	.4662	.5519	.4656	.5506	.4650	.5493	.4644
3.	.4647	.4263	.4640	.4262	.4633	.4259	.4626	.4256	.4619	.4253	.4612	.4250	.4605	.4247	.4598	.4244	.4591	.4241	.4584	.4238
4.	.4091	.4009	.4087	.4007	.4080	.4005	.4073	.4002	.4066	.4001	.4059	.4000	.4052	.3999	.4045	.3998	.4038	.3997	.4031	.3996
5.	.3728	.0839	.3725	.0838	.3722	.0837	.3719	.0836	.3716	.0835	.3713	.0834	.3710	.0833	.3707	.0832	.3704	.0831	.3701	.0830
6.	.3473	.0719	.3471	.0718	.3469	.0717	.3467	.0716	.3465	.0715	.3463	.0714	.3461	.0713	.3459	.0712	.3457	.0711	.3455	.0710
7.	.3284	.0628	.3282	.0627	.3281	.0627	.3279	.0626	.3277	.0625	.3275	.0624	.3273	.0623	.3271	.0622	.3270	.0621	.3268	.0620
8.	.3138	.0558	.3136	.0557	.3135	.0557	.3133	.0556	.3132	.0555	.3130	.0554	.3128	.0553	.3127	.0552	.3125	.0551	.3124	.0550
9.	.3021	.0502	.3020	.0501	.3019	.0501	.3018	.0500	.3017	.0500	.3016	.0499	.3015	.0498	.3014	.0498	.3013	.0497	.3012	.0496
10.	.0677	.0456	.0686	.0456	.0695	.0455	.0704	.0454	.0713	.0453	.0722	.0452	.0731	.0451	.0740	.0450	.0749	.0449	.0758	.0448
11.	.0648	.0418	.0647	.0417	.0646	.0417	.0645	.0416	.0644	.0415	.0643	.0414	.0642	.0413	.0641	.0412	.0640	.0411	.0639	.0410
12.	.0628	.0386	.0621	.0385	.0614	.0384	.0607	.0383	.0600	.0382	.0593	.0381	.0586	.0380	.0579	.0379	.0572	.0378	.0565	.0377
13.	.0615	.0358	.0614	.0358	.0613	.0357	.0612	.0356	.0611	.0355	.0610	.0354	.0609	.0353	.0608	.0352	.0607	.0351	.0606	.0350
14.	.0607	.0334	.0603	.0334	.0600	.0333	.0597	.0332	.0594	.0331	.0591	.0330	.0588	.0329	.0585	.0328	.0582	.0327	.0579	.0326
15.	.0593	.0313	.0593	.0313	.0592	.0312	.0591	.0311	.0590	.0310	.0589	.0309	.0588	.0308	.0587	.0307	.0586	.0306	.0585	.0305
16.	.0585	.0295	.0585	.0295	.0584	.0294	.0583	.0293	.0582	.0292	.0581	.0291	.0580	.0290	.0579	.0289	.0578	.0288	.0577	.0287
17.	.0582	.0280	.0581	.0279	.0581	.0278	.0580	.0277	.0579	.0276	.0578	.0275	.0577	.0274	.0576	.0273	.0575	.0272	.0574	.0271
18.	.0580	.0263	.0579	.0262	.0579	.0261	.0578	.0260	.0577	.0259	.0576	.0258	.0575	.0257	.0574	.0256	.0573	.0255	.0572	.0254
19.XX	.0565	.0248	.0565	.0247	.0565	.0246	.0564	.0245	.0563	.0244	.0562	.0243	.0561	.0242	.0560	.0241	.0559	.0240	.0558	.0239

TABLE B-V. - CONTINUED

(e)  $0.XX \leq \frac{X_n - X_0}{\Delta X} \leq 19.XX$  where  $40 \leq XX \leq 49$

XX X <sub>n</sub> -X <sub>0</sub> ΔX	40		41		42		43		44		45		46		47		48		49	
	↓ <sub>00</sub>	↓ <sub>00</sub> *	↓ <sub>00</sub>	↓ <sub>00</sub> *	↓ <sub>00</sub>	↓ <sub>00</sub> *	↓ <sub>00</sub>	↓ <sub>00</sub> *	↓ <sub>00</sub>	↓ <sub>00</sub> *	↓ <sub>00</sub>	↓ <sub>00</sub> *	↓ <sub>00</sub>	↓ <sub>00</sub> *	↓ <sub>00</sub>	↓ <sub>00</sub> *	↓ <sub>00</sub>	↓ <sub>00</sub> *	↓ <sub>00</sub>	↓ <sub>00</sub> *
0.XX	1.0928	0.4909	1.0938	0.4906	1.0948	0.4894	1.0957	0.4883	1.0966	0.4873	1.0975	0.4863	1.0984	0.4853	1.0993	0.4843	1.1002	0.4833	1.1011	0.4823
1.	.0930	.4914	.0930	.4914	.0931	.4910	.0932	.4908	.0933	.4906	.0934	.4904	.0935	.4902	.0936	.4899	.0937	.4897	.0938	.4894
2.	.0931	.4919	.0932	.4919	.0933	.4917	.0934	.4915	.0935	.4913	.0936	.4911	.0937	.4909	.0938	.4907	.0939	.4905	.0940	.4901
3.	.0932	.4924	.0933	.4924	.0934	.4922	.0935	.4920	.0936	.4918	.0937	.4916	.0938	.4914	.0939	.4913	.0940	.4910	.0941	.4906
4.	.0933	.4929	.0934	.4929	.0935	.4927	.0936	.4925	.0937	.4923	.0938	.4921	.0939	.4919	.0940	.4917	.0941	.4916	.0942	.4912
5.	.0934	.4934	.0935	.4934	.0936	.4932	.0937	.4930	.0938	.4928	.0939	.4926	.0940	.4924	.0941	.4921	.0942	.4919	.0943	.4915
6.	.0935	.4939	.0936	.4939	.0937	.4937	.0938	.4935	.0939	.4933	.0940	.4931	.0941	.4929	.0942	.4926	.0943	.4924	.0944	.4920
7.	.0936	.4944	.0937	.4944	.0938	.4942	.0939	.4940	.0940	.4938	.0941	.4936	.0942	.4934	.0943	.4931	.0944	.4929	.0945	.4924
8.	.0937	.4949	.0938	.4949	.0939	.4947	.0940	.4945	.0941	.4943	.0942	.4941	.0943	.4939	.0944	.4937	.0945	.4934	.0946	.4929
9.	.0938	.4954	.0939	.4954	.0940	.4952	.0941	.4950	.0942	.4948	.0943	.4946	.0944	.4944	.0945	.4942	.0946	.4940	.0947	.4934
10.	.0939	.4959	.0940	.4959	.0941	.4957	.0942	.4955	.0943	.4953	.0944	.4951	.0945	.4949	.0946	.4946	.0947	.4944	.0948	.4937
11.	.0940	.4964	.0941	.4964	.0942	.4962	.0943	.4960	.0944	.4958	.0945	.4956	.0946	.4954	.0947	.4951	.0948	.4949	.0949	.4940
12.	.0941	.4969	.0942	.4969	.0943	.4967	.0944	.4965	.0945	.4963	.0946	.4961	.0947	.4959	.0948	.4956	.0949	.4953	.0950	.4944
13.	.0942	.4974	.0943	.4974	.0944	.4972	.0945	.4970	.0946	.4968	.0947	.4966	.0948	.4964	.0949	.4962	.0950	.4960	.0951	.4952
14.	.0943	.4979	.0944	.4979	.0945	.4977	.0946	.4975	.0947	.4973	.0948	.4971	.0949	.4969	.0950	.4967	.0951	.4966	.0952	.4956
15.	.0944	.4984	.0945	.4984	.0946	.4982	.0947	.4980	.0948	.4978	.0949	.4976	.0950	.4974	.0951	.4972	.0952	.4971	.0953	.4964
16.	.0945	.4989	.0946	.4989	.0947	.4987	.0948	.4985	.0949	.4983	.0950	.4981	.0951	.4979	.0952	.4977	.0953	.4976	.0954	.4968
17.	.0946	.4994	.0947	.4994	.0948	.4992	.0949	.4990	.0950	.4988	.0951	.4986	.0952	.4984	.0953	.4982	.0954	.4981	.0955	.4972
18.	.0947	.4999	.0948	.4999	.0949	.4997	.0950	.4995	.0951	.4993	.0952	.4991	.0953	.4989	.0954	.4987	.0955	.4986	.0956	.4976
19.XX	.0948	.5004	.0949	.5004	.0950	.5002	.0951	.5000	.0952	.4999	.0953	.4997	.0954	.4995	.0955	.4994	.0956	.4993	.0957	.4990

TABLE B-V. - CONTINUED

(f)  $0.XX \leq \frac{X_n - X_0}{\Delta X} \leq 19.XX$  where  $50 \leq XX \leq 59$

XX X <sub>n</sub> -X <sub>0</sub> ΔX	50		51		52		53		54		55		56		57		58		59	
	↓ <sub>00</sub>	↓ <sub>00</sub> *	↓ <sub>00</sub>	↓ <sub>00</sub> *	↓ <sub>00</sub>	↓ <sub>00</sub> *	↓ <sub>00</sub>	↓ <sub>00</sub> *	↓ <sub>00</sub>	↓ <sub>00</sub> *	↓ <sub>00</sub>	↓ <sub>00</sub> *	↓ <sub>00</sub>	↓ <sub>00</sub> *	↓ <sub>00</sub>	↓ <sub>00</sub> *	↓ <sub>00</sub>	↓ <sub>00</sub> *	↓ <sub>00</sub>	↓ <sub>00</sub> *
0.XX	1.0986	0.4907	1.0995	0.4894	1.0998	0.4883	1.0999	0.4873	1.0999	0.4863	1.0999	0.4853	1.0999	0.4843	1.0999	0.4833	1.0999	0.4823	1.0999	0.4813
1.	.0988	.4912	.0989	.4901	.0990	.4890	.0991	.4880	.0992	.4870	.0993	.4860	.0994	.4850	.0995	.4840	.0996	.4830	.0997	.4820
2.	.0989	.4917	.0990	.4907	.0991	.4897	.0992	.4887	.0993	.4877	.0994	.4867	.0995	.4857	.0996	.4847	.0997	.4837	.0998	.4827
3.	.0990	.4922	.0991	.4912	.0992	.4902	.0993	.4892	.0994	.4882	.0995	.4872	.0996	.4862	.0997	.4852	.0998	.4842	.0999	.4832
4.	.0991	.4927	.0992	.4917	.0993	.4907	.0994	.4897	.0995	.4887	.0996	.4877	.0997	.4867	.0998	.4857	.0999	.4847	.1000	.4837
5.	.0992	.4932	.0993	.4922	.0994	.4912	.0995	.4902	.0996	.4892	.0997	.4882	.0998	.4872	.0999	.4862	.1000	.4852	.1001	.4842
6.	.0993	.4937	.0994	.4927	.0995	.4917	.0996	.4907	.0997	.4897	.0998	.4887	.0999	.4877	.1000	.4867	.1001	.4857	.1002	.4847
7.	.0994	.4942	.0995	.4932	.0996	.4922	.0997	.4912	.0998	.4902	.0999	.4892	.1000	.4882	.1001	.4872	.1002	.4862	.1003	.4852
8.	.0995	.4947	.0996	.4937	.0997	.4927	.0998	.4917	.0999	.4907	.1000	.4897	.1001	.4887	.1002	.4877	.1003	.4867	.1004	.4857
9.	.0996	.4952	.0997	.4942	.0998	.4932	.0999	.4922	.1000	.4912	.1001	.4902	.1002	.4892	.1003	.4882	.1004	.4872	.1005	.4862
10.	.0997	.4957	.0998	.4947	.0999	.4937	.1000	.4927	.1001	.4917	.1002	.4907	.1003	.4897	.1004	.4887	.1005	.4877	.1006	.4867
11.	.0998	.4962	.0999	.4952	.1000	.4942	.1001	.4932	.1002	.4922	.1003	.4912	.1004	.4902	.1005	.4892	.1006	.4882	.1007	.4872
12.	.0999	.4967	.1000	.4957	.1001	.4947	.1002	.4937	.1003	.4927	.1004	.4917	.1005	.4907	.1006	.4897	.1007	.4887	.1008	.4877
13.	.1000	.4972	.1001	.4962	.1002	.4952	.1003	.4942	.1004	.4932	.1005	.4922	.1006	.4912	.1007	.4902	.1008	.4892	.1009	.4882
14.	.1001	.4977	.1002	.4967	.1003	.4957	.1004	.4947	.1005	.4937	.1006	.4927	.1007	.4917	.1008	.4907	.1009	.4897	.1010	.4887
15.	.1002	.4982	.1003	.4972	.1004	.4962	.1005	.4952	.1006	.4942	.1007	.4932	.1008	.4922	.1009	.4912	.1010	.4902	.1011	.4892
16.	.1003	.4987	.1004	.4977	.1005	.4967	.1006	.4957	.1007	.4947	.1008	.4937	.1009	.4927	.1010	.4917	.1011	.4907	.1012	.4897
17.	.1004	.4992	.1005	.4982	.1006	.4972	.1007	.4962	.1008	.4952	.1009	.4942	.1010	.4932	.1011	.4922	.1012	.4912	.1013	.4902
18.	.1005	.4997	.1006	.4987	.1007	.4977	.1008	.4967	.1009	.4957	.1010	.4947	.1011	.4937	.1012	.4927	.1013	.4917	.1014	.4907
19.XX	.1006	.5002	.1007	.4992	.1008	.4982	.1009	.4972	.1010	.4962	.1011	.4952	.1012	.4942	.1013	.4932	.1014	.4922	.1015	.4912



TABLE B-V. -- CONTINUED

(i)  $0.XX \leq \frac{X_{II}-X_0}{\Delta X} \leq 19.XX$  where  $80 \leq XX \leq 89$

II X <sub>II</sub> -X <sub>0</sub> ΔX	80		81		82		83		84		85		86		87		88		89	
	+00	+00*	+00	+00*	+00	+00*	+00	+00*	+00	+00*	+00	+00*	+00	+00*	+00	+00*	+00	+00*	+00	+00*
0.XX	0.8109	0.3513	0.8081	0.3487	0.7973	0.3429	0.7906	0.3438	0.7811	0.3413	0.7777	0.3369	0.7714	0.3310	0.7629	0.3282	0.7529	0.3250	0.7433	0.3227
1.	8108	3512	8080	3486	7972	3428	7905	3437	7810	3412	7776	3368	7713	3309	7628	3281	7528	3249	7432	3226
2.	8107	3511	8079	3485	7971	3427	7904	3436	7809	3411	7775	3367	7712	3308	7627	3280	7527	3248	7431	3225
3.	8106	3510	8078	3484	7970	3426	7903	3435	7808	3410	7774	3366	7711	3307	7626	3279	7526	3247	7430	3224
4.	8105	3509	8077	3483	7969	3425	7902	3434	7807	3409	7773	3365	7710	3306	7625	3278	7525	3246	7429	3223
5.	8104	3508	8076	3482	7968	3424	7901	3433	7806	3408	7772	3364	7709	3305	7624	3277	7524	3245	7428	3222
6.	8103	3507	8075	3481	7967	3423	7900	3432	7805	3407	7771	3363	7708	3304	7623	3276	7523	3244	7427	3221
7.	8102	3506	8074	3480	7966	3422	7899	3431	7804	3406	7770	3362	7707	3303	7622	3275	7522	3243	7426	3220
8.	8101	3505	8073	3479	7965	3421	7898	3430	7803	3405	7769	3361	7706	3302	7621	3274	7521	3242	7425	3219
9.	8100	3504	8072	3478	7964	3420	7897	3429	7802	3404	7768	3360	7705	3301	7620	3273	7520	3241	7424	3218
10.	8099	3503	8071	3477	7963	3419	7896	3428	7801	3403	7767	3359	7704	3300	7619	3272	7519	3240	7423	3217
11.	8098	3502	8070	3476	7962	3418	7895	3427	7800	3402	7766	3358	7703	3299	7618	3271	7518	3239	7422	3216
12.	8097	3501	8069	3475	7961	3417	7894	3426	7799	3401	7765	3357	7702	3298	7617	3270	7517	3238	7421	3215
13.	8096	3500	8068	3474	7960	3416	7893	3425	7798	3400	7764	3356	7701	3297	7616	3269	7516	3237	7420	3214
14.	8095	3499	8067	3473	7959	3415	7892	3424	7797	3399	7763	3355	7700	3296	7615	3268	7515	3236	7419	3213
15.	8094	3498	8066	3472	7958	3414	7891	3423	7796	3398	7762	3354	7699	3295	7614	3267	7514	3235	7418	3212
16.	8093	3497	8065	3471	7957	3413	7890	3422	7795	3397	7761	3353	7698	3294	7613	3266	7513	3234	7417	3211
17.	8092	3496	8064	3470	7956	3412	7889	3421	7794	3396	7760	3352	7697	3293	7612	3265	7512	3233	7416	3210
18.	8091	3495	8063	3469	7955	3411	7888	3420	7793	3395	7759	3351	7696	3292	7611	3264	7511	3232	7415	3209
19.XX	8090	3494	8062	3468	7954	3410	7887	3419	7792	3394	7758	3350	7695	3291	7610	3263	7510	3231	7414	3208

TABLE B-V.-- CONCLUDED

(j)  $0.XX \leq \frac{X_{II}-X_0}{\Delta X} \leq 19.XX$  where  $90 \leq XX \leq 99$

II X <sub>II</sub> -X <sub>0</sub> ΔX	90		91		92		93		94		95		96		97		98		99	
	+00	+00*	+00	+00*	+00	+00*	+00	+00*	+00	+00*	+00	+00*	+00	+00*	+00	+00*	+00	+00*	+00	+00*
0.XX	0.7474	0.3273	0.7444	0.3253	0.7397	0.3231	0.7351	0.3210	0.7305	0.3189	0.7271	0.3169	0.7237	0.3149	0.7203	0.3129	0.7169	0.3109	0.7135	0.3089
1.	7473	3272	7443	3252	7396	3230	7350	3209	7304	3188	7268	3168	7234	3148	7200	3128	7166	3108	7132	3088
2.	7472	3271	7442	3251	7395	3229	7349	3208	7303	3187	7267	3167	7233	3147	7199	3127	7165	3107	7131	3087
3.	7471	3270	7441	3250	7394	3228	7348	3207	7302	3186	7266	3166	7232	3146	7198	3126	7164	3106	7130	3086
4.	7470	3269	7440	3249	7393	3227	7347	3206	7301	3185	7265	3165	7231	3145	7197	3125	7163	3105	7129	3085
5.	7469	3268	7439	3248	7392	3226	7346	3205	7300	3184	7264	3164	7230	3144	7196	3124	7162	3104	7128	3084
6.	7468	3267	7438	3247	7391	3225	7345	3204	7299	3183	7263	3163	7229	3143	7195	3123	7161	3103	7127	3083
7.	7467	3266	7437	3246	7390	3224	7344	3203	7298	3182	7262	3162	7228	3142	7194	3122	7160	3102	7126	3082
8.	7466	3265	7436	3245	7389	3223	7343	3202	7297	3181	7261	3161	7227	3141	7193	3121	7159	3101	7125	3081
9.	7465	3264	7435	3244	7388	3222	7342	3201	7296	3180	7260	3160	7226	3140	7192	3120	7158	3100	7124	3080
10.	7464	3263	7434	3243	7387	3221	7341	3200	7295	3179	7259	3159	7225	3139	7191	3119	7157	3099	7123	3079
11.	7463	3262	7433	3242	7386	3220	7340	3199	7294	3178	7258	3158	7224	3138	7190	3118	7156	3098	7122	3078
12.	7462	3261	7432	3241	7385	3219	7339	3198	7293	3177	7257	3157	7223	3137	7189	3117	7155	3097	7121	3077
13.	7461	3260	7431	3240	7384	3218	7338	3197	7292	3176	7256	3156	7222	3136	7188	3116	7154	3096	7120	3076
14.	7460	3259	7430	3239	7383	3217	7337	3196	7291	3175	7255	3155	7221	3135	7187	3115	7153	3095	7119	3075
15.	7459	3258	7429	3238	7382	3216	7336	3195	7290	3174	7254	3154	7220	3134	7186	3114	7152	3094	7118	3074
16.	7458	3257	7428	3237	7381	3215	7335	3194	7289	3173	7253	3153	7219	3133	7185	3113	7151	3093	7117	3073
17.	7457	3256	7427	3236	7380	3214	7334	3193	7288	3172	7252	3152	7218	3132	7184	3112	7150	3092	7116	3072
18.	7456	3255	7426	3235	7379	3213	7333	3192	7287	3171	7251	3151	7217	3131	7183	3111	7149	3091	7115	3071
19.XX	7455	3254	7425	3234	7378	3212	7332	3191	7286	3170	7250	3150	7216	3130	7182	3110	7148	3090	7114	3070





TABLE B-VI.- VALUES OF  $j_{no}$  AND  $j_{no}^*$  USED IN EVALUATING EQUATION (26)

$$20.0 \leq \frac{T_{in} - T_{co}}{\Delta T} \leq 39.9$$

$\frac{T_{in} - T_{co}}{\Delta T}$	0		1		2		3		4		5		6		7		8		9	
	$j_{no}$	$j_{no}^*$	$j_{no}$	$j_{no}^*$	$j_{no}$	$j_{no}^*$	$j_{no}$	$j_{no}^*$	$j_{no}$	$j_{no}^*$	$j_{no}$	$j_{no}^*$	$j_{no}$	$j_{no}^*$	$j_{no}$	$j_{no}^*$	$j_{no}$	$j_{no}^*$	$j_{no}$	$j_{no}^*$
20.X	0.0488	0.0242	0.0486	0.0241	0.0483	0.0241	0.0481	0.0239	0.0478	0.0237	0.0476	0.0236	0.0474	0.0236	0.0472	0.0234	0.0470	0.0232	0.0467	0.0231
21.	.0465	.0231	.0463	.0230	.0461	.0229	.0459	.0227	.0457	.0226	.0455	.0226	.0453	.0224	.0451	.0224	.0448	.0223	.0446	.0222
22.	.0444	.0221	.0443	.0220	.0441	.0219	.0439	.0218	.0437	.0217	.0435	.0216	.0433	.0215	.0431	.0214	.0429	.0213	.0427	.0212
23.	.0426	.0211	.0424	.0210	.0422	.0210	.0420	.0209	.0418	.0208	.0417	.0207	.0415	.0206	.0413	.0205	.0412	.0204	.0410	.0204
24.	.0408	.0203	.0407	.0202	.0405	.0201	.0403	.0200	.0402	.0199	.0400	.0199	.0398	.0198	.0397	.0197	.0395	.0196	.0394	.0195
25.	.0392	.0195	.0391	.0194	.0389	.0193	.0388	.0192	.0386	.0192	.0385	.0191	.0383	.0190	.0382	.0190	.0380	.0189	.0379	.0188
26.	.0377	.0187	.0376	.0187	.0375	.0186	.0373	.0185	.0372	.0185	.0370	.0184	.0369	.0184	.0368	.0183	.0366	.0182	.0365	.0182
27.	.0364	.0181	.0362	.0180	.0361	.0179	.0360	.0179	.0358	.0178	.0357	.0178	.0356	.0177	.0355	.0176	.0353	.0176	.0352	.0175
28.	.0351	.0175	.0350	.0174	.0348	.0173	.0347	.0173	.0346	.0172	.0345	.0172	.0344	.0171	.0342	.0171	.0341	.0170	.0340	.0169
29.	.0339	.0168	.0338	.0168	.0337	.0167	.0336	.0167	.0334	.0166	.0333	.0166	.0332	.0165	.0331	.0165	.0330	.0164	.0329	.0164
30.	.0328	.0163	.0327	.0162	.0326	.0162	.0325	.0161	.0324	.0161	.0323	.0160	.0322	.0160	.0321	.0159	.0320	.0158	.0319	.0158
31.	.0317	.0158	.0316	.0157	.0315	.0157	.0315	.0156	.0314	.0156	.0313	.0155	.0312	.0155	.0311	.0154	.0310	.0154	.0309	.0153
32.	.0306	.0153	.0307	.0152	.0306	.0152	.0305	.0151	.0304	.0151	.0303	.0151	.0302	.0150	.0301	.0150	.0300	.0150	.0299	.0149
33.	.0299	.0149	.0298	.0148	.0297	.0148	.0296	.0147	.0295	.0147	.0294	.0146	.0293	.0146	.0292	.0145	.0292	.0145	.0291	.0145
34.	.0290	.0144	.0289	.0144	.0288	.0143	.0287	.0143	.0287	.0143	.0286	.0142	.0285	.0142	.0284	.0142	.0283	.0141	.0283	.0141
35.	.0282	.0141	.0281	.0140	.0280	.0139	.0279	.0139	.0279	.0138	.0278	.0138	.0277	.0138	.0276	.0138	.0276	.0137	.0275	.0137
36.	.0274	.0136	.0273	.0136	.0273	.0136	.0272	.0135	.0271	.0135	.0270	.0134	.0269	.0134	.0269	.0134	.0268	.0133	.0267	.0133
37.	.0267	.0133	.0266	.0132	.0265	.0132	.0265	.0132	.0264	.0131	.0263	.0131	.0262	.0130	.0262	.0130	.0261	.0130	.0260	.0130
38.	.0260	.0129	.0259	.0129	.0258	.0129	.0258	.0128	.0257	.0128	.0256	.0127	.0256	.0127	.0255	.0127	.0254	.0127	.0254	.0126
39.X	.0253	.0126	.0253	.0126	.0252	.0126	.0251	.0125	.0251	.0125	.0250	.0125	.0249	.0124	.0249	.0124	.0248	.0124	.0248	.0123



TABLE B-VII.-- VALUES OF  $j_{no}$  AND  $j_{no}^*$  USED IN EVALUATING EQUATION (26)

$$40.0 \leq \frac{x_n - x_0}{\Delta x} \leq 89.5$$

$\frac{x_n - x_0}{\Delta x}$ X	4X.0		4X.5		5X.0		5X.5		6X.0		6X.5		7X.0		7X.5		8X.0		8X.5	
	$j_{no}$	$j_{no}^*$	$j_{no}$	$j_{no}^*$	$j_{no}$	$j_{no}^*$	$j_{no}$	$j_{no}^*$	$j_{no}$	$j_{no}^*$	$j_{no}$	$j_{no}^*$	$j_{no}$	$j_{no}^*$	$j_{no}$	$j_{no}^*$	$j_{no}$	$j_{no}^*$	$j_{no}$	$j_{no}^*$
0	0.0247	0.0123	0.0244	0.0122	0.0198	0.0099	0.0196	0.0097	0.0165	0.0082	0.0164	0.0082	0.0142	0.0071	0.0141	0.0071	0.0124	0.0062	0.0123	0.0061
1	.0241	.0120	.0238	.0118	.0194	.0097	.0192	.0096	.0163	.0081	.0161	.0081	.0140	.0069	.0139	.0069	.0123	.0061	.0122	.0061
2	.0235	.0117	.0233	.0116	.0190	.0095	.0189	.0094	.0160	.0080	.0159	.0079	.0138	.0068	.0137	.0068	.0121	.0061	.0120	.0060
3	.0230	.0114	.0227	.0113	.0187	.0093	.0185	.0092	.0157	.0079	.0156	.0078	.0136	.0068	.0135	.0068	.0120	.0059	.0119	.0059
4	.0225	.0112	.0222	.0110	.0184	.0091	.0182	.0090	.0155	.0077	.0154	.0077	.0134	.0066	.0133	.0066	.0118	.0059	.0118	.0059
5	.0220	.0109	.0217	.0108	.0180	.0090	.0179	.0089	.0153	.0076	.0152	.0075	.0132	.0066	.0132	.0065	.0117	.0058	.0116	.0058
6	.0215	.0107	.0213	.0106	.0177	.0089	.0175	.0088	.0150	.0075	.0149	.0074	.0131	.0065	.0130	.0065	.0116	.0058	.0115	.0058
7	.0211	.0105	.0208	.0103	.0174	.0087	.0172	.0086	.0148	.0074	.0147	.0073	.0129	.0064	.0128	.0064	.0114	.0057	.0114	.0056
8	.0206	.0103	.0204	.0101	.0171	.0085	.0169	.0085	.0146	.0073	.0145	.0072	.0127	.0063	.0127	.0063	.0113	.0056	.0112	.0056
9	.0202	.0101	.0200	.0100	.0168	.0084	.0167	.0083	.0144	.0072	.0143	.0072	.0126	.0063	.0125	.0062	.0112	.0055	.0111	.0055

TABLE B-VIII.-- VALUES OF  $j_{no}$  AND  $j_{no}^*$  USED IN EVALUATING EQUATION (26)

$$90 \leq \frac{x_n - x_0}{\Delta x} \leq 189$$

$\frac{x_n - x_0}{\Delta x}$ X	9X.0		10X.0		11X.0		12X.0		13X.0		14X.0		15X.0		16X.0		17X.0		18X.0	
	$j_{no}$	$j_{no}^*$	$j_{no}$	$j_{no}^*$	$j_{no}$	$j_{no}^*$	$j_{no}$	$j_{no}^*$	$j_{no}$	$j_{no}^*$	$j_{no}$	$j_{no}^*$	$j_{no}$	$j_{no}^*$	$j_{no}$	$j_{no}^*$	$j_{no}$	$j_{no}^*$	$j_{no}$	$j_{no}^*$
0	0.0111	0.0035	0.0100	0.0050	0.0091	0.0045	0.0083	0.0042	0.0077	0.0038	0.0071	0.0036	0.0067	0.0033	0.0063	0.0031	0.0059	0.0029	0.0056	0.0028
1	.0109	.0034	.0099	.0050	.0090	.0045	.0083	.0041	.0076	.0038	.0071	.0035	.0066	.0033	.0062	.0031	.0058	.0029	.0055	.0028
2	.0108	.0034	.0098	.0049	.0089	.0045	.0082	.0041	.0076	.0038	.0070	.0035	.0066	.0033	.0062	.0031	.0058	.0029	.0055	.0027
3	.0107	.0034	.0097	.0049	.0088	.0044	.0081	.0041	.0075	.0038	.0070	.0035	.0065	.0033	.0061	.0031	.0058	.0029	.0055	.0027
4	.0106	.0033	.0096	.0048	.0088	.0044	.0081	.0040	.0074	.0037	.0069	.0035	.0065	.0032	.0061	.0031	.0057	.0029	.0054	.0027
5	.0105	.0033	.0095	.0048	.0087	.0043	.0080	.0040	.0074	.0037	.0069	.0034	.0065	.0032	.0061	.0030	.0057	.0029	.0054	.0027
6	.0104	.0032	.0094	.0047	.0086	.0043	.0079	.0040	.0074	.0037	.0068	.0034	.0064	.0032	.0060	.0030	.0057	.0028	.0054	.0027
7	.0103	.0032	.0093	.0047	.0085	.0043	.0079	.0039	.0073	.0036	.0068	.0034	.0064	.0032	.0060	.0030	.0056	.0028	.0053	.0027
8	.0102	.0031	.0093	.0046	.0085	.0042	.0078	.0039	.0072	.0036	.0068	.0034	.0063	.0032	.0060	.0030	.0056	.0028	.0053	.0027
9	.0101	.0031	.0092	.0046	.0084	.0042	.0078	.0039	.0072	.0036	.0067	.0034	.0063	.0031	.0059	.0030	.0056	.0028	.0053	.0026



TABLE B-IX.- VALUES OF  $j_{no}$  AND  $j_{no}^*$  USED IN EVALUATING EQUATION (26)

(a)  $-0.999 \leq \frac{x_n - x_0}{\Delta x} \leq -0.750$

$\frac{x_n - x_0}{\Delta x}$	9		8		7		6		5		4		3		2		1		0	
	$j_{no}$	$j_{no}^*$	$j_{no}$	$j_{no}^*$	$j_{no}$	$j_{no}^*$	$j_{no}$	$j_{no}^*$	$j_{no}$	$j_{no}^*$	$j_{no}$	$j_{no}^*$	$j_{no}$	$j_{no}^*$	$j_{no}$	$j_{no}^*$	$j_{no}$	$j_{no}^*$	$j_{no}$	$j_{no}^*$
-0.99	-6.9068	-5.8998	-6.2126	-5.2022	-5.8061	-4.7887	-5.5175	-4.4954	-5.2933	-4.2668	-5.1100	-4.0793	-4.9548	-3.9202	-4.8203	-3.7617	-4.7015	-3.6992	-4.5951	-3.5492
-0.98	-4.4988	-3.4493	-4.4108	-3.3578	-4.3297	-3.2734	-4.2546	-3.1753	-4.1846	-3.1218	-4.1190	-3.0531	-4.0574	-3.9884	-3.9992	-3.9272	-3.8441	-3.8692	-3.8918	-3.8140
-0.97	-3.8420	-2.7613	-3.7945	-2.7110	-3.7489	-2.6627	-3.7034	-2.6165	-3.6636	-2.5720	-3.6233	-2.5291	-3.5845	-2.4878	-3.5473	-2.4480	-3.5110	-2.4092	-3.4761	-2.3718
-0.96	-3.4423	-2.3356	-3.4095	-2.3004	-3.3777	-2.2662	-3.3468	-2.2330	-3.3168	-2.2007	-3.2876	-2.1692	-3.2591	-2.1385	-3.2314	-2.1086	-3.2044	-2.0794	-3.1761	-2.0509
-0.95	-3.1523	-2.0231	-3.1272	-1.9959	-3.1026	-1.9692	-3.0786	-1.9431	-3.0550	-1.9176	-3.0340	-1.8925	-3.0095	-1.8680	-2.9873	-1.8440	-2.9657	-1.8204	-2.9444	-1.7972
-0.94	-2.9236	-1.7745	-2.9031	-1.7522	-2.8830	-1.7304	-2.8632	-1.7086	-2.8439	-1.6875	-2.8248	-1.6666	-2.8060	-1.6461	-2.7875	-1.6259	-2.7694	-1.6060	-2.7516	-1.5865
-0.93	-2.7339	-1.5671	-2.7167	-1.5482	-2.6995	-1.5295	-2.6827	-1.5110	-2.6662	-1.4929	-2.6499	-1.4750	-2.6337	-1.4572	-2.6178	-1.4398	-2.6022	-1.4226	-2.5867	-1.4056
-0.92	-2.5715	-1.3889	-2.5564	-1.3723	-2.5415	-1.3560	-2.5268	-1.3399	-2.5123	-1.3239	-2.4980	-1.3081	-2.4838	-1.2926	-2.4699	-1.2772	-2.4560	-1.2620	-2.4423	-1.2470
-0.91	-2.4289	-1.2321	-2.4155	-1.2174	-2.4022	-1.2029	-2.3892	-1.1885	-2.3763	-1.1743	-2.3635	-1.1602	-2.3508	-1.1463	-2.3383	-1.1326	-2.3259	-1.1189	-2.3136	-1.1054
-0.90	-2.3015	-1.0920	-2.2895	-1.0788	-2.2775	-1.0657	-2.2657	-1.0528	-2.2541	-1.0399	-2.2425	-1.0272	-2.2310	-1.0146	-2.2196	-1.0021	-2.2084	-0.9898	-2.1972	-0.9775
-0.89	-2.1862	-0.9694	-2.1792	-0.9533	-2.1643	-0.9414	-2.1535	-0.9296	-2.1429	-0.9179	-2.1323	-0.9063	-2.1218	-0.8947	-2.1113	-0.8833	-2.1010	-0.8720	-2.0908	-0.8608
-0.88	-2.0806	-0.8496	-2.0705	-0.8386	-2.0605	-0.8276	-2.0505	-0.8168	-2.0407	-0.8060	-2.0309	-0.7953	-2.0212	-0.7847	-2.0115	-0.7742	-2.0019	-0.7637	-1.9924	-0.7533
-0.87	-1.9830	-0.7431	-1.9736	-0.7328	-1.9643	-0.7227	-1.9551	-0.7127	-1.9459	-0.7027	-1.9368	-0.6928	-1.9277	-0.6829	-1.9188	-0.6732	-1.9098	-0.6635	-1.9010	-0.6538
-0.86	-1.8921	-0.6443	-1.8834	-0.6348	-1.8747	-0.6254	-1.8660	-0.6160	-1.8575	-0.6067	-1.8489	-0.5975	-1.8404	-0.5883	-1.8320	-0.5792	-1.8236	-0.5701	-1.8153	-0.5612
-0.85	-1.8070	-0.5522	-1.7988	-0.5434	-1.7906	-0.5345	-1.7825	-0.5258	-1.7744	-0.5171	-1.7663	-0.5084	-1.7583	-0.4999	-1.7504	-0.4913	-1.7425	-0.4828	-1.7346	-0.4744
-0.84	-1.7268	-0.4660	-1.7190	-0.4577	-1.7113	-0.4495	-1.7036	-0.4412	-1.6959	-0.4330	-1.6883	-0.4249	-1.6807	-0.4168	-1.6732	-0.4088	-1.6657	-0.4008	-1.6582	-0.3929
-0.83	-1.6508	-0.3850	-1.6434	-0.3772	-1.6361	-0.3694	-1.6288	-0.3617	-1.6215	-0.3539	-1.6142	-0.3463	-1.6070	-0.3387	-1.5999	-0.3311	-1.5927	-0.3244	-1.5856	-0.3161
-0.82	-1.5786	-0.3086	-1.5715	-0.3012	-1.5645	-0.2938	-1.5575	-0.2865	-1.5506	-0.2792	-1.5437	-0.2720	-1.5368	-0.2648	-1.5300	-0.2576	-1.5231	-0.2505	-1.5164	-0.2434
-0.81	-1.5096	-0.2304	-1.5029	-0.2293	-1.4962	-0.2224	-1.4895	-0.2154	-1.4828	-0.2085	-1.4762	-0.2016	-1.4696	-0.1948	-1.4630	-0.1880	-1.4565	-0.1812	-1.4500	-0.1745
-0.80	-1.4435	-0.1678	-1.4371	-0.1611	-1.4306	-0.1545	-1.4242	-0.1479	-1.4178	-0.1414	-1.4115	-0.1348	-1.4051	-0.1283	-1.3988	-0.1219	-1.3926	-0.1154	-1.3863	-0.1090
-0.79	-1.3801	-0.1027	-1.3738	-0.0963	-1.3676	-0.0900	-1.3615	-0.0837	-1.3553	-0.0775	-1.3492	-0.0713	-1.3431	-0.0651	-1.3370	-0.0589	-1.3310	-0.0528	-1.3249	-0.0467
-0.78	-1.3189	-0.0406	-1.3129	-0.0346	-1.3069	-0.0286	-1.3010	-0.0226	-1.2951	-0.0166	-1.2891	-0.0107	-1.2832	-0.0048	-1.2774	0.0011	-1.2715	0.0070	-1.2657	0.0128
-0.77	-1.2599	0.0186	-1.2540	0.0244	-1.2483	0.0301	-1.2425	0.0358	-1.2368	0.0415	-1.2310	0.0472	-1.2253	0.0528	-1.2196	0.0594	-1.2140	0.0640	-1.2083	0.0696
-0.76	-1.2027	0.0791	-1.1970	0.0807	-1.1914	0.0862	-1.1859	0.0916	-1.1803	0.0971	-1.1747	0.1025	-1.1692	0.1079	-1.1637	0.1133	-1.1582	0.1186	-1.1527	0.1240
-0.75	-1.1472	0.1293	-1.1417	0.1346	-1.1363	0.1398	-1.1309	0.1451	-1.1254	0.1503	-1.1200	0.1555	-1.1147	0.1606	-1.1093	0.1658	-1.1040	0.1709	-1.0986	0.1760



TABLE B-IX.- CONTINUED

$$(b) \quad -0.749 \leq \frac{x_n - x_0}{\Delta x} \leq -0.500$$

$\frac{x_n - x_0}{\Delta x}$	9		8		7		6		5		4		3		2		1		0	
	$f_{no}$	$f_{no}^*$	$f_{no}$	$f_{no}^*$	$f_{no}$	$f_{no}^*$	$f_{no}$	$f_{no}^*$	$f_{no}$	$f_{no}^*$	$f_{no}$	$f_{no}^*$	$f_{no}$	$f_{no}^*$	$f_{no}$	$f_{no}^*$	$f_{no}$	$f_{no}^*$	$f_{no}$	$f_{no}^*$
-.74	-1.0933	0.1811	-1.0880	0.1862	-1.0827	0.1912	-1.0774	0.1963	-1.0721	0.2013	-1.0669	0.2062	-1.0616	0.2112	-1.0564	0.2162	-1.0512	0.2211	-1.0460	0.2260
-.73	-1.0408	.2309	-1.0356	.2357	-1.0304	.2406	-1.0253	.2454	-1.0201	.2502	-1.0150	.2550	-1.0099	.2598	-1.0048	.2645	-1.0097	.2692	-1.0046	.2739
-.72	-.9895	.2786	-.9843	.2833	-.9793	.2879	-.9741	.2926	-.9689	.2972	-.9637	.3018	-.9584	.3064	-.9531	.3109	-.9479	.3155	-.9425	.3200
-.71	-.9395	.3245	-.9346	.3290	-.9296	.3334	-.9247	.3379	-.9198	.3423	-.9149	.3468	-.9100	.3512	-.9051	.3556	-.9002	.3599	-.8954	.3643
-.70	-.8905	.3686	-.8857	.3729	-.8809	.3772	-.8761	.3815	-.8712	.3858	-.8664	.3900	-.8616	.3943	-.8568	.3985	-.8521	.4020	-.8473	.4069
-.69	-.8426	.4111	-.8378	.4152	-.8330	.4194	-.8283	.4235	-.8236	.4276	-.8189	.4317	-.8142	.4358	-.8095	.4398	-.8048	.4439	-.8001	.4479
-.68	-.7954	.4519	-.7908	.4559	-.7861	.4599	-.7815	.4639	-.7768	.4679	-.7722	.4718	-.7676	.4757	-.7630	.4796	-.7584	.4835	-.7538	.4874
-.67	-.7492	.4913	-.7446	.4952	-.7400	.4990	-.7354	.5028	-.7309	.5067	-.7263	.5104	-.7218	.5142	-.7173	.5180	-.7127	.5218	-.7082	.5255
-.66	-.7036	.5293	-.6991	.5330	-.6946	.5367	-.6901	.5404	-.6857	.5440	-.6812	.5477	-.6767	.5513	-.6722	.5550	-.6678	.5586	-.6633	.5622
-.65	-.6589	.5658	-.6544	.5694	-.6500	.5730	-.6455	.5765	-.6411	.5801	-.6367	.5836	-.6322	.5872	-.6278	.5914	-.6234	.5952	-.6191	.5996
-.64	-.6146	.6011	-.6103	.6046	-.6059	.6080	-.6015	.6114	-.5971	.6149	-.5928	.6183	-.5884	.6217	-.5841	.6250	-.5797	.6284	-.5754	.6318
-.63	-.5710	.6351	-.5667	.6385	-.5624	.6418	-.5581	.6451	-.5537	.6484	-.5494	.6517	-.5451	.6549	-.5408	.6582	-.5365	.6615	-.5322	.6647
-.62	-.5279	.6679	-.5237	.6711	-.5194	.6743	-.5151	.6776	-.5108	.6807	-.5066	.6839	-.5023	.6871	-.4980	.6902	-.4938	.6934	-.4896	.6965
-.61	-.4853	.6996	-.4811	.7027	-.4769	.7058	-.4726	.7089	-.4684	.7119	-.4642	.7150	-.4600	.7180	-.4557	.7211	-.4515	.7241	-.4473	.7271
-.60	-.4431	.7302	-.4389	.7331	-.4347	.7361	-.4305	.7391	-.4264	.7420	-.4222	.7450	-.4180	.7480	-.4138	.7509	-.4097	.7538	-.4055	.7567
-.59	-.4013	.7596	-.3972	.7625	-.3930	.7654	-.3888	.7683	-.3847	.7711	-.3806	.7739	-.3764	.7768	-.3723	.7796	-.3680	.7824	-.3639	.7853
-.58	-.3598	.7681	-.3557	.7708	-.3516	.7736	-.3475	.7764	-.3433	.7791	-.3392	.7819	-.3351	.7846	-.3310	.7874	-.3269	.7901	-.3228	.7928
-.57	-.3187	.8155	-.3146	.8182	-.3105	.8209	-.3064	.8235	-.3023	.8262	-.2982	.8288	-.2941	.8315	-.2900	.8341	-.2859	.8367	-.2818	.8393
-.56	-.2778	.8419	-.2737	.8449	-.2696	.8471	-.2656	.8497	-.2614	.8529	-.2574	.8548	-.2533	.8574	-.2493	.8599	-.2452	.8624	-.2412	.8649
-.55	-.2371	.8675	-.2331	.8700	-.2290	.8724	-.2249	.8749	-.2209	.8774	-.2169	.8799	-.2128	.8823	-.2088	.8848	-.2047	.8873	-.2007	.8896
-.54	-.1966	.8920	-.1926	.8945	-.1886	.8969	-.1845	.8993	-.1805	.9016	-.1765	.9040	-.1724	.9064	-.1684	.9087	-.1644	.9111	-.1603	.9134
-.53	-.1563	.9177	-.1523	.9181	-.1483	.9204	-.1443	.9227	-.1402	.9250	-.1362	.9273	-.1322	.9295	-.1282	.9318	-.1242	.9341	-.1201	.9363
-.52	-.1161	.9386	-.1121	.9408	-.1081	.9430	-.1041	.9452	-.1001	.9475	-.961	.9497	-.961	.9519	-.9681	.9540	-.9640	.9562	-.9600	.9584
-.51	-.0760	.9605	-.0720	.9627	-.0680	.9648	-.0640	.9670	-.0600	.9691	-.0560	.9712	-.0520	.9733	-.0480	.9754	-.0440	.9775	-.0400	.9796
-.50	-.0360	.9817	-.0320	.9837	-.0280	.9858	-.0240	.9879	-.0200	.9899	-.0160	.9919	-.0120	.9940	-.0080	.9960	-.0040	.9980	0	1.0000



TABLE B-IX.- CONTINUED

(c) 
$$-0.499 \leq \frac{x_{II} - x_0}{\Delta x} \leq -0.250$$

I $\frac{x_{II} - x_0}{\Delta x}$	9		8		7		6		5		4		3		2		1		0	
	$\downarrow_{no}$	$\downarrow_{no}^*$	$\downarrow_{no}$	$\downarrow_{no}^*$	$\downarrow_{no}$	$\downarrow_{no}^*$	$\downarrow_{no}$	$\downarrow_{no}^*$	$\downarrow_{no}$	$\downarrow_{no}^*$	$\downarrow_{no}$	$\downarrow_{no}^*$	$\downarrow_{no}$	$\downarrow_{no}^*$	$\downarrow_{no}$	$\downarrow_{no}^*$	$\downarrow_{no}$	$\downarrow_{no}^*$	$\downarrow_{no}$	$\downarrow_{no}^*$
-.499	0.0040	1.0020	0.0080	1.0040	0.0120	1.0060	0.0160	1.0079	0.0200	1.0099	0.0240	1.0119	0.0280	1.0138	0.0320	1.0157	0.0360	1.0177	0.0400	1.0196
-.48	.0440	1.0215	.0480	1.0234	.0520	1.0253	.0560	1.0272	.0601	1.0291	.0640	1.0310	.0680	1.0329	.0720	1.0347	.0760	1.0366	.0800	1.0384
-.47	.0841	1.0403	.0881	1.0421	.0920	1.0439	.0960	1.0457	.1001	1.0476	.1041	1.0493	.1081	1.0511	.1121	1.0529	.1161	1.0547	.1202	1.0565
-.46	.1243	1.0582	.1282	1.0600	.1322	1.0617	.1362	1.0635	.1402	1.0652	.1443	1.0669	.1482	1.0686	.1523	1.0704	.1563	1.0721	.1603	1.0738
-.45	.1643	1.0734	.1684	1.0771	.1724	1.0788	.1765	1.0805	.1805	1.0821	.1845	1.0838	.1886	1.0854	.1926	1.0871	.1966	1.0887	.2007	1.0903
-.44	.2047	1.0919	.2087	1.0935	.2128	1.0951	.2169	1.0967	.2209	1.0983	.2250	1.0999	.2290	1.1014	.2330	1.1030	.2371	1.1046	.2411	1.1061
-.43	.2452	1.1077	.2493	1.1092	.2533	1.1107	.2574	1.1122	.2615	1.1138	.2655	1.1152	.2696	1.1168	.2737	1.1182	.2778	1.1197	.2819	1.1212
-.42	.2859	1.1227	.2900	1.1241	.2941	1.1256	.2982	1.1270	.3023	1.1285	.3064	1.1299	.3105	1.1313	.3146	1.1328	.3187	1.1342	.3227	1.1355
-.41	.3269	1.1370	.3310	1.1383	.3351	1.1397	.3392	1.1411	.3433	1.1425	.3475	1.1439	.3516	1.1452	.3557	1.1466	.3598	1.1479	.3639	1.1492
-.40	.3681	1.1506	.3723	1.1519	.3764	1.1532	.3806	1.1545	.3847	1.1558	.3888	1.1571	.3930	1.1584	.3972	1.1597	.4013	1.1609	.4055	1.1622
-.39	.4097	1.1635	.4138	1.1647	.4180	1.1659	.4222	1.1672	.4264	1.1684	.4305	1.1696	.4347	1.1708	.4389	1.1720	.4431	1.1732	.4473	1.1745
-.38	.4515	1.1756	.4557	1.1768	.4600	1.1780	.4642	1.1792	.4684	1.1803	.4726	1.1815	.4769	1.1826	.4811	1.1838	.4853	1.1849	.4896	1.1860
-.37	.4938	1.1871	.4980	1.1883	.5023	1.1894	.5066	1.1905	.5108	1.1916	.5151	1.1926	.5194	1.1937	.5237	1.1948	.5279	1.1959	.5322	1.1969
-.36	.5365	1.1980	.5408	1.1990	.5451	1.2001	.5494	1.2011	.5537	1.2021	.5581	1.2031	.5624	1.2041	.5667	1.2051	.5710	1.2061	.5754	1.2071
-.35	.5797	1.2081	.5841	1.2091	.5884	1.2101	.5927	1.2110	.5971	1.2120	.6015	1.2129	.6059	1.2139	.6103	1.2148	.6146	1.2157	.6191	1.2167
-.34	.6234	1.2176	.6278	1.2185	.6322	1.2194	.6367	1.2203	.6411	1.2212	.6455	1.2221	.6500	1.2229	.6544	1.2238	.6589	1.2247	.6633	1.2255
-.33	.6678	1.2264	.6722	1.2272	.6767	1.2281	.6812	1.2289	.6857	1.2297	.6901	1.2305	.6946	1.2313	.6991	1.2321	.7036	1.2329	.7082	1.2337
-.32	.7127	1.2343	.7173	1.2353	.7218	1.2360	.7263	1.2368	.7309	1.2375	.7354	1.2383	.7400	1.2390	.7446	1.2398	.7492	1.2405	.7538	1.2412
-.31	.7584	1.2419	.7630	1.2426	.7676	1.2433	.7722	1.2440	.7768	1.2447	.7815	1.2454	.7861	1.2461	.7908	1.2467	.7954	1.2474	.8001	1.2480
-.30	.8048	1.2487	.8095	1.2493	.8142	1.2500	.8189	1.2506	.8236	1.2512	.8283	1.2518	.8330	1.2524	.8378	1.2530	.8426	1.2536	.8473	1.2542
-.29	.8521	1.2548	.8568	1.2553	.8616	1.2559	.8664	1.2565	.8712	1.2570	.8761	1.2576	.8809	1.2581	.8857	1.2586	.8905	1.2591	.8954	1.2597
-.28	.9002	1.2602	.9051	1.2607	.9100	1.2612	.9149	1.2617	.9198	1.2624	.9247	1.2628	.9296	1.2631	.9346	1.2639	.9395	1.2640	.9445	1.2644
-.27	.9494	1.2649	.9544	1.2653	.9594	1.2658	.9644	1.2662	.9694	1.2666	.9744	1.2670	.9795	1.2674	.9845	1.2678	.9895	1.2682	.9946	1.2685
-.26	.9997	1.2689	1.0048	1.2693	1.0099	1.2696	1.0150	1.2700	1.0201	1.2703	1.0253	1.2707	1.0304	1.2710	1.0356	1.2713	1.0408	1.2716	1.0460	1.2720
-.25	1.0512	1.2723	1.0564	1.2726	1.0616	1.2728	1.0669	1.2731	1.0721	1.2734	1.0774	1.2737	1.0827	1.2739	1.0880	1.2742	1.0933	1.2744	1.0986	1.2747



TABLE B-IX.- CONCLUDED

(d)  $-0.249 \leq \frac{I_{II}-I_0}{\Delta x} \leq 0.000$

I $\frac{I_{II}-I_0}{\Delta x}$	9		8		7		6		5		4		3		2		1		0	
	$\downarrow_{no}$	$\downarrow_{no}^*$	$\downarrow_{no}$	$\downarrow_{no}^*$	$\downarrow_{no}$	$\downarrow_{no}^*$	$\downarrow_{no}$	$\downarrow_{no}^*$	$\downarrow_{no}$	$\downarrow_{no}^*$	$\downarrow_{no}$	$\downarrow_{no}^*$	$\downarrow_{no}$	$\downarrow_{no}^*$	$\downarrow_{no}$	$\downarrow_{no}^*$	$\downarrow_{no}$	$\downarrow_{no}^*$	$\downarrow_{no}$	$\downarrow_{no}^*$
-0.41	1.1040	1.2749	1.1093	1.2751	1.1147	1.2753	1.1200	1.2755	1.1254	1.2757	1.1309	1.2759	1.1363	1.2761	1.1417	1.2763	1.1472	1.2765	1.1527	1.2766
-0.33	1.1582	1.2768	1.1637	1.2770	1.1692	1.2771	1.1747	1.2772	1.1803	1.2774	1.1859	1.2775	1.1914	1.2776	1.1970	1.2777	1.2027	1.2778	1.2083	1.2779
-0.28	1.2140	1.2780	1.2196	1.2781	1.2253	1.2782	1.2310	1.2782	1.2368	1.2783	1.2425	1.2784	1.2483	1.2784	1.2540	1.2784	1.2599	1.2784	1.2657	1.2784
-0.21	1.2715	1.2785	1.2774	1.2785	1.2832	1.2785	1.2891	1.2785	1.2951	1.2785	1.3010	1.2784	1.3069	1.2784	1.3129	1.2783	1.3189	1.2783	1.3249	1.2782
-0.20	1.3310	1.2788	1.3370	1.2781	1.3431	1.2780	1.3492	1.2779	1.3553	1.2778	1.3615	1.2777	1.3676	1.2776	1.3738	1.2775	1.3801	1.2774	1.3863	1.2773
-0.19	1.3926	1.2771	1.3988	1.2770	1.4051	1.2768	1.4115	1.2766	1.4178	1.2765	1.4242	1.2763	1.4306	1.2761	1.4371	1.2759	1.4435	1.2757	1.4500	1.2755
-0.18	1.4565	1.2753	1.4630	1.2751	1.4696	1.2748	1.4762	1.2746	1.4828	1.2743	1.4895	1.2741	1.4962	1.2738	1.5029	1.2735	1.5096	1.2732	1.5164	1.2729
-0.17	1.5231	1.2736	1.5300	1.2723	1.5368	1.2720	1.5437	1.2717	1.5506	1.2714	1.5575	1.2710	1.5645	1.2707	1.5715	1.2703	1.5786	1.2699	1.5856	1.2696
-0.16	1.5927	1.2692	1.5999	1.2688	1.6070	1.2684	1.6142	1.2680	1.6215	1.2675	1.6288	1.2671	1.6361	1.2667	1.6434	1.2662	1.6508	1.2658	1.6582	1.2653
-0.15	1.6657	1.2648	1.6732	1.2644	1.6807	1.2639	1.6883	1.2634	1.6959	1.2629	1.7036	1.2625	1.7113	1.2621	1.7190	1.2613	1.7268	1.2607	1.7346	1.2602
-0.14	1.7425	1.2596	1.7504	1.2591	1.7583	1.2585	1.7663	1.2579	1.7744	1.2573	1.7825	1.2567	1.7906	1.2561	1.7988	1.2554	1.8070	1.2548	1.8153	1.2541
-0.13	1.8236	1.2535	1.8320	1.2528	1.8404	1.2521	1.8489	1.2515	1.8575	1.2508	1.8660	1.2501	1.8747	1.2493	1.8834	1.2486	1.8921	1.2479	1.9010	1.2471
-0.12	1.9098	1.2464	1.9188	1.2456	1.9277	1.2448	1.9368	1.2440	1.9459	1.2432	1.9551	1.2424	1.9643	1.2416	1.9736	1.2408	1.9830	1.2399	1.9924	1.2391
-0.11	2.0019	1.2382	2.0115	1.2374	2.0212	1.2365	2.0309	1.2356	2.0407	1.2347	2.0505	1.2338	2.0605	1.2328	2.0705	1.2319	2.0806	1.2309	2.0908	1.2300
-0.10	2.1010	1.2290	2.1113	1.2280	2.1218	1.2270	2.1323	1.2260	2.1429	1.2250	2.1536	1.2240	2.1643	1.2229	2.1752	1.2219	2.1862	1.2209	2.1972	1.2197
-0.09	2.2084	1.2186	2.2196	1.2175	2.2310	1.2164	2.2425	1.2153	2.2541	1.2141	2.2657	1.2130	2.2775	1.2118	2.2895	1.2106	2.3015	1.2094	2.3136	1.2082
-0.08	2.3259	1.2070	2.3383	1.2058	2.3508	1.2045	2.3635	1.2033	2.3763	1.2020	2.3892	1.2007	2.4022	1.1994	2.4155	1.1981	2.4289	1.1967	2.4423	1.1954
-0.07	2.4560	1.1940	2.4693	1.1927	2.4838	1.1913	2.4980	1.1898	2.5123	1.1884	2.5268	1.1870	2.5415	1.1855	2.5564	1.1841	2.5715	1.1826	2.5867	1.1811
-0.06	2.6022	1.1796	2.6178	1.1780	2.6337	1.1763	2.6499	1.1749	2.6662	1.1733	2.6827	1.1717	2.6995	1.1701	2.7166	1.1684	2.7339	1.1668	2.7516	1.1651
-0.05	2.7654	1.1634	2.7816	1.1617	2.8000	1.1599	2.8188	1.1582	2.8379	1.1564	2.8572	1.1546	2.8768	1.1528	2.9031	1.1510	2.9236	1.1491	2.9444	1.1472
-0.04	2.9657	1.1453	2.9873	1.1434	3.0095	1.1414	3.0320	1.1395	3.0550	1.1375	3.0786	1.1355	3.1026	1.1334	3.1272	1.1313	3.1523	1.1292	3.1781	1.1271
-0.03	3.2044	1.1290	3.2314	1.1228	3.2591	1.1206	3.2876	1.1184	3.3168	1.1161	3.3468	1.1138	3.3777	1.1115	3.4095	1.1091	3.4423	1.1067	3.4761	1.1043
-0.02	3.5110	1.1018	3.5473	1.0993	3.5845	1.0968	3.6233	1.0942	3.6636	1.0916	3.7054	1.0889	3.7489	1.0862	3.7945	1.0835	3.8420	1.0807	3.8918	1.0778
-0.01	3.9441	1.0749	3.9992	1.0720	4.0574	1.0690	4.1190	1.0659	4.1846	1.0628	4.2546	1.0596	4.3297	1.0563	4.4108	1.0529	4.4988	1.0495	4.5951	1.0460
-0.00	4.7015	1.0423	4.8203	1.0386	4.9548	1.0347	5.1100	1.0307	5.2833	1.0265	5.5175	1.0221	5.8061	1.0174	6.2126	1.0124	6.9068	1.0069	*	1.0000



## APPENDIX C

## DETAILS OF SOLUTION OF INTEGRAL (36)

$$F_1 = \int_0^{\epsilon_1} \frac{\frac{\Delta v}{V_0}}{\sqrt{x(c-x)}} \frac{dx}{x-x_0} = \frac{1}{c} \int_0^{\epsilon_1} \frac{\Delta v}{V_0} \frac{1}{\sqrt{\frac{x}{c}}} \frac{1}{\sqrt{1-\frac{x}{c}}} \frac{d(\frac{x}{c})}{\frac{x}{c} - \frac{x_0}{c}} \quad (C1)$$

Introduce  $\xi = \frac{x}{c}$  and find

$$F_1 = \frac{1}{c} \int_0^{\epsilon_1/c} \frac{\Delta v}{V_0} \frac{1}{\sqrt{\xi}} \left( 1 + \frac{1}{2} \xi + \frac{3}{8} \xi^2 + \dots \right) \frac{d\xi}{\xi - \xi_0} \quad (C2)$$

With the expansion (see equation (37))

$$\begin{aligned} \frac{\Delta v}{V_0} \left( 1 + \frac{1}{2} \xi + \frac{3}{8} \xi^2 + \dots \right) &= a_0 + \left( a_1 + \frac{1}{2} a_0 \right) \xi + \left( a_2 + \frac{1}{2} a_1 + \frac{3}{8} a_0 \right) \xi^2 \\ &= a_0 + a_1^* \xi + a_2^* \xi^2 + \dots \end{aligned} \quad (C3)$$

Hence,

$$\begin{aligned} F_1 &= \frac{1}{c} \int_0^{\epsilon_1/c} \frac{a_0 + a_1^* \xi + a_2^* \xi^2}{\sqrt{\xi} (\xi - \xi_0)} d\xi \\ &= \frac{1}{c} \left[ a_0 \int_0^{\epsilon_1/c} \frac{d\xi}{\sqrt{\xi} (\xi - \xi_0)} + \right. \\ &\quad a_1^* \int_0^{\epsilon_1/c} \frac{\xi d\xi}{\sqrt{\xi} (\xi - \xi_0)} + \\ &\quad \left. a_2^* \int_0^{\epsilon_1/c} \frac{\xi^2 d\xi}{\sqrt{\xi} (\xi - \xi_0)} \right] \end{aligned} \quad (C4)$$

As the occurring integrals are all of the same type, define

$$L_n = \int_0^{\epsilon_1/c} \frac{\xi^n d\xi}{\sqrt{\xi}(\xi - \xi_0)} \quad (C5)$$

These integrals  $L_n$  are easily solved by recurrence.

$$L_n = \xi_0 L_{n-1} + \frac{\left(\frac{\epsilon_1}{c}\right)^{n-\frac{1}{2}}}{n - \frac{1}{2}} \quad (C6)$$

with

$$L_0 = \frac{1}{\sqrt{\xi_0}} \log_e \frac{1 - \sqrt{\frac{\epsilon_1}{x_0}}}{1 + \sqrt{\frac{\epsilon_1}{x_0}}} \quad \text{for } x_0 > \epsilon_1 \quad (C7)$$

and

$$L_0 = \frac{1}{\sqrt{\xi_0}} \log_e \frac{1 - \sqrt{\frac{x_0}{\epsilon_1}}}{1 + \sqrt{\frac{x_0}{\epsilon_1}}} \quad \text{for } x_0 < \epsilon_1 \quad (C8)$$

The function

$$M_0 = \log_e \frac{1 - \sqrt{\frac{\epsilon_1}{x_0}}}{1 + \sqrt{\frac{\epsilon_1}{x_0}}} \quad \text{and} \quad \log_e \frac{1 - \sqrt{\frac{x_0}{\epsilon_1}}}{1 + \sqrt{\frac{x_0}{\epsilon_1}}}$$

is given in figure 2 in order to provide a more rapid computation in the event that  $\frac{x_0}{\epsilon_1}$  or  $\frac{\epsilon_1}{x_0}$  is not very small.



If  $\frac{\epsilon_1}{x_0} \ll 1$ ,

$$M_0 = -2 \left( \sqrt{\frac{\epsilon_1}{x_0}} + \frac{1}{3} \sqrt{\frac{\epsilon_1}{x_0}}^3 + \frac{1}{5} \sqrt{\frac{\epsilon_1}{x_0}}^5 + \dots \right) \quad (C9)$$

The integrals  $L_0$ ,  $L_1$ , and  $L_2$  are needed; these are given by

$$\left. \begin{aligned} L_0 &= \frac{1}{\sqrt{\xi_0}} M_0 \\ L_1 &= \sqrt{\xi_0} M_0 + 2 \sqrt{\frac{\epsilon_1}{c}} \\ L_2 &= \xi_0 L_1 + \frac{2}{3} \sqrt{\frac{\epsilon_1}{c}}^3 \\ &= \xi_0^{3/2} M_0 + 2 \xi_0 \sqrt{\frac{\epsilon_1}{c}} + \frac{2}{3} \sqrt{\frac{\epsilon_1}{c}}^3 \end{aligned} \right\} \quad (C10)$$

If  $\frac{\epsilon_1}{x_0} \ll 1$ ,

$$\left. \begin{aligned} L_0 &= -\frac{2}{\sqrt{\xi_0}} \left( \sqrt{\frac{\epsilon_1}{x_0}} + \frac{1}{3} \sqrt{\frac{\epsilon_1}{x_0}}^3 + \frac{1}{5} \sqrt{\frac{\epsilon_1}{x_0}}^5 + \dots \right) \\ L_1 &= -2 \sqrt{\xi_0} \left( \frac{1}{3} \sqrt{\frac{\epsilon_1}{x_0}}^3 + \frac{1}{5} \sqrt{\frac{\epsilon_1}{x_0}}^5 + \dots \right) \\ L_2 &= -2 \sqrt{\xi_0}^3 \left( \frac{1}{5} \sqrt{\frac{\epsilon_1}{x_0}}^5 + \dots \right) \end{aligned} \right\} \quad (C11)$$

With these expressions the integral  $F_1$  is as follows:

$$\begin{aligned}
 F_1 &= \frac{1}{c} (a_0 L_0 + a_1^* L_1 + a_2^* L_2) \\
 &= \frac{1}{c} \left[ \frac{a_0}{\sqrt{\xi_0}} M_0 + a_1^* \left( \sqrt{\xi_0} M_0 + 2\sqrt{\frac{\epsilon_1}{c}} \right) + a_2^* \left( \sqrt{\xi_0}^3 M_0 + \right. \right. \\
 &\quad \left. \left. 2\xi_0 \sqrt{\frac{\epsilon_1}{c}} + \frac{2}{3} \sqrt{\frac{\epsilon_1}{c}}^3 \right) \right] \\
 &= \frac{1}{c} \left[ M_0 \left( \frac{a_0}{\sqrt{\xi_0}} + a_1^* \sqrt{\xi_0} + a_2^* \sqrt{\xi_0}^3 \right) + \right. \\
 &\quad \left. 2\sqrt{\frac{\epsilon_1}{c}} (a_1^* + \xi_0 a_2^*) + \frac{2}{3} a_2^* \sqrt{\frac{\epsilon_1}{c}}^3 \right] \quad (C12)
 \end{aligned}$$

The coefficients  $a_0$ ,  $a_1$ , and  $a_2$  of the expansion of  $\frac{\Delta v}{V_0}$  are given by

$$\left. \begin{aligned}
 a_0 &= \left( \frac{\Delta v}{V_0} \right)_{x=0} \\
 a_1 &= \frac{c}{2\epsilon_1} \left[ -3 \left( \frac{\Delta v}{V_0} \right)_{x=0} + 4 \left( \frac{\Delta v}{V_0} \right)_{x=\epsilon_1} - \left( \frac{\Delta v}{V_0} \right)_{x=2\epsilon_1} \right] \\
 a_2 &= \frac{c^2}{2\epsilon_1^2} \left[ \left( \frac{\Delta v}{V_0} \right)_{x=0} - 2 \left( \frac{\Delta v}{V_0} \right)_{x=\epsilon_1} + \left( \frac{\Delta v}{V_0} \right)_{x=2\epsilon_1} \right]
 \end{aligned} \right\} \quad (C13)$$

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TABLE I.- VALUES OF  $j_{no}$  AND  $j_{no}^*$  FOR  $-49.5 < \frac{x_n - x_0}{\Delta x} < 49.5$

$\frac{x_n - x_0}{\Delta x}$	$j_{no}$	$j_{no}^*$	$\frac{x_n - x_0}{\Delta x}$	$j_{no}$	$j_{no}^*$
-49.5	-0.0204	-0.0102	0.5	1.0986	0.4507
-48.5	-.0208	-.0104	1.5	.5108	.2338
-47.5	-.0213	-.0107	2.5	.3365	.1588
-46.5	-.0217	-.0109	3.5	.2513	.1204
-45.5	-.0222	-.0112	4.5	.2007	.0970
-44.5	-.0227	-.0114	5.5	.1671	.0812
-43.5	-.0233	-.0117	6.5	.1431	.0698
-42.5	-.0238	-.0120	7.5	.1252	.0613
-41.5	-.0244	-.0122	8.5	.1112	.0546
-40.5	-.0250	-.0125	9.5	.1001	.0492
-39.5	-.0256	-.0129	10.5	.0910	.0448
-38.5	-.0263	-.0132	11.5	.0834	.0411
-37.5	-.0270	-.0136	12.5	.0770	.0380
-36.5	-.0278	-.0139	13.5	.0715	.0353
-35.5	-.0286	-.0143	14.5	.0667	.0330
-34.5	-.0294	-.0148	15.5	.0625	.0309
-33.5	-.0303	-.0153	16.5	.0588	.0291
-32.5	-.0313	-.0157	17.5	.0556	.0275
-31.5	-.0323	-.0162	18.5	.0526	.0261
-30.5	-.0333	-.0167	19.5	.0500	.0248
-29.5	-.0345	-.0173	20.5	.0476	.0236
-28.5	-.0357	-.0180	21.5	.0455	.0226
-27.5	-.0370	-.0186	22.5	.0435	.0216
-26.5	-.0385	-.0193	23.5	.0417	.0207
-25.5	-.0400	-.0201	24.5	.0400	.0199
-24.5	-.0417	-.0210	25.5	.0385	.0191
-23.5	-.0435	-.0219	26.5	.0370	.0184
-22.5	-.0455	-.0229	27.5	.0357	.0178
-21.5	-.0476	-.0240	28.5	.0345	.0172
-20.5	-.0500	-.0252	29.5	.0333	.0166
-19.5	-.0526	-.0266	30.5	.0323	.0160
-18.5	-.0556	-.0280	31.5	.0313	.0155
-17.5	-.0588	-.0297	32.5	.0303	.0151
-16.5	-.0625	-.0316	33.5	.0294	.0146
-15.5	-.0667	-.0337	34.5	.0286	.0142
-14.5	-.0715	-.0362	35.5	.0278	.0138
-13.5	-.0770	-.0390	36.5	.0270	.0134
-12.5	-.0834	-.0423	37.5	.0263	.0131
-11.5	-.0910	-.0462	38.5	.0256	.0127
-10.5	-.1001	-.0509	39.5	.0250	.0125
-9.5	-.1112	-.0567	40.5	.0244	.0122
-8.5	-.1252	-.0639	41.5	.0238	.0118
-7.5	-.1431	-.0733	42.5	.0233	.0116
-6.5	-.1671	-.0859	43.5	.0227	.0113
-5.5	-.2007	-.1037	44.5	.0222	.0111
-4.5	-.2513	-.1309	45.5	.0217	.0108
-3.5	-.3365	-.1777	46.5	.0213	.0106
-2.5	-.5108	-.2771	47.5	.0208	.0103
-1.5	-1.0986	-.6479	48.5	.0204	.0101
-.5	0	1.0	49.5	.0200	.0100



TABLE II.- COMPUTATION BY UNEQUAL INTERVALS, TRANSITION FROM  
ONE INTERVAL SIZE TO ANOTHER

(a)  $\overline{\Delta x} = 0.002$ .

$\frac{x}{c}$	$\sigma_n$	$\sigma_{n+1} - \sigma_n$	$\frac{x_n - x_0}{\Delta x}$	$j_{no}$	$j_{no}^*$
0	$\sigma_0$	$\sigma_1 - \sigma_0$	-4.5	-0.2513	-0.1309
.002	$\sigma_1$	$\sigma_2 - \sigma_1$	-3.5	-.3365	-.1777
.004	$\sigma_2$	$\sigma_3 - \sigma_2$	-2.5	-.5108	-.2771
.006	$\sigma_3$	$\sigma_4 - \sigma_3$	-1.5	-1.0986	-.6479
.008	$\sigma_4$	$\sigma_5 - \sigma_4$	-.5	0	1.0
.010	$\sigma_5$	$\sigma_6 - \sigma_5$	.5	1.0986	.4507
.012	$\sigma_6$	$\sigma_7 - \sigma_6$	1.5	.5108	.2338
.014	.	.	2.5	.3365	.1588
.016	.	.	3.5	.2513	.1204
.018	.	.	4.5	.2007	.0970
.020	.	.	5.5	.1671	.0812
.022	.	.	6.5	.1431	.0698
.024	.	.	7.5	.1252	.0613
.026	.	.	8.5	.1112	.0546
.028	$\sigma_{14}$	$\sigma_{15} - \sigma_{14}$	9.5	.1001	.0492
.030	$\sigma_{15}$		10.5		

(b)  $\overline{\Delta x} = 0.006$ .

$\frac{x}{c}$	$\sigma_n$	$\sigma_{n+1} - \sigma_n$	$\frac{x_n - x_0}{\Delta x}$	$j_{no}$	$j_{no}^*$
0	$\sigma_0$	$\sigma_3 - \sigma_0$	-1.5	-1.0986	-0.6479
.006	$\sigma_3$	$\sigma_6 - \sigma_3$	-.5	0	1.0
.012	$\sigma_6$	$\sigma_9 - \sigma_6$	.5	1.0986	.4507
.018	$\sigma_9$	$\sigma_{12} - \sigma_9$	1.5	.5108	.2338
.024	$\sigma_{12}$	$\sigma_{15} - \sigma_{12}$	2.5	.3365	.1588
-----					
.030	$\sigma_{15}$	$\sigma_{16} - \sigma_{15}$	3.5	.2513	.1204
.036	$\sigma_{16}$	$\sigma_{17} - \sigma_{16}$	4.5	.2007	.0970
.042	$\sigma_{17}$	$\sigma_{18} - \sigma_{17}$	5.5	.1671	.0812
.048	$\sigma_{18}$	$\sigma_{19} - \sigma_{18}$	6.5	.1431	.0698
.054	.	.	7.5	.1252	.0613
.060	.	.	8.5	.1112	.0546
.066	.	.	9.5	.1001	.0492
.072	.	.	10.5	.0910	.0448
.078	.	.	11.5	.0834	.0411
.084	.	.	12.5	.0770	.0380
.090	$\sigma_{25}$	$\sigma_{26} - \sigma_{25}$	13.5	.0715	.0353
.096	$\sigma_{26}$	$\sigma_{27} - \sigma_{26}$	14.5	.0667	.0330

TABLE III.- COMPUTATION FOR  $x_0 = 0.065$  BY UNEQUAL INTERVALS

[Example, fig. 18]

$\frac{x}{c}$	$\sigma_n$	$\sigma_{n+1} - \sigma_n$	$\frac{x_n - x_0}{\overline{\Delta x}_n}$	$\frac{x_n - x_0}{\overline{\overline{\Delta x}}_n}$	$\frac{x_n - x_0}{\overline{\overline{\overline{\Delta x}}}_n}$	$j_{no}$	$j_{no}^*$
0.060	0	0.005	-1.5			-1.099	-0.648
.0633	.005	.010	-.5			0	1.0
.0667	.015	.021	.5			1.099	.451
.070	.036	.0565		1.0		.693	.307
.075	.0925	.1075		2.0		.406	.189
.080	.2000	-.1000		3.0		.288	.137
.085	.1000	-.094		4.0		.223	.107
.090	.006	-.0087			2.5	.336	.159
.100	-.0027	.0011			3.5	.251	.120
.110	-.0016	.0016			4.5	.201	.097
.120	0	0			5.5	.167	.081
			$\overline{\Delta x} = 0.0033$	$\overline{\overline{\Delta x}} = 0.005$	$\overline{\overline{\overline{\Delta x}}} = 0.010$		



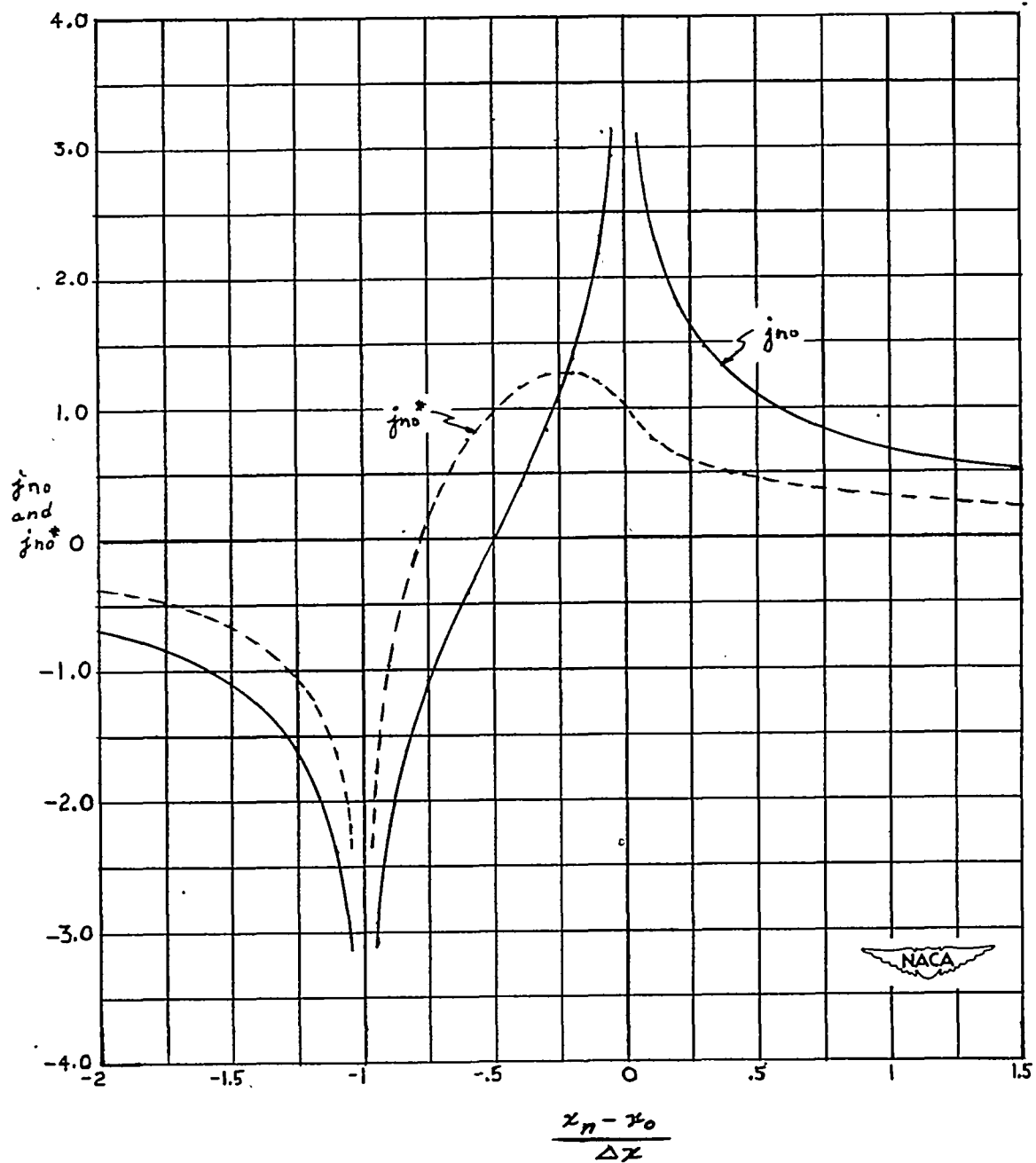


Figure 1.- Characteristic qualities of  $j_{no}$  and  $j_{no}^*$  as functions of  $\frac{x_n - x_0}{\Delta x}$ .

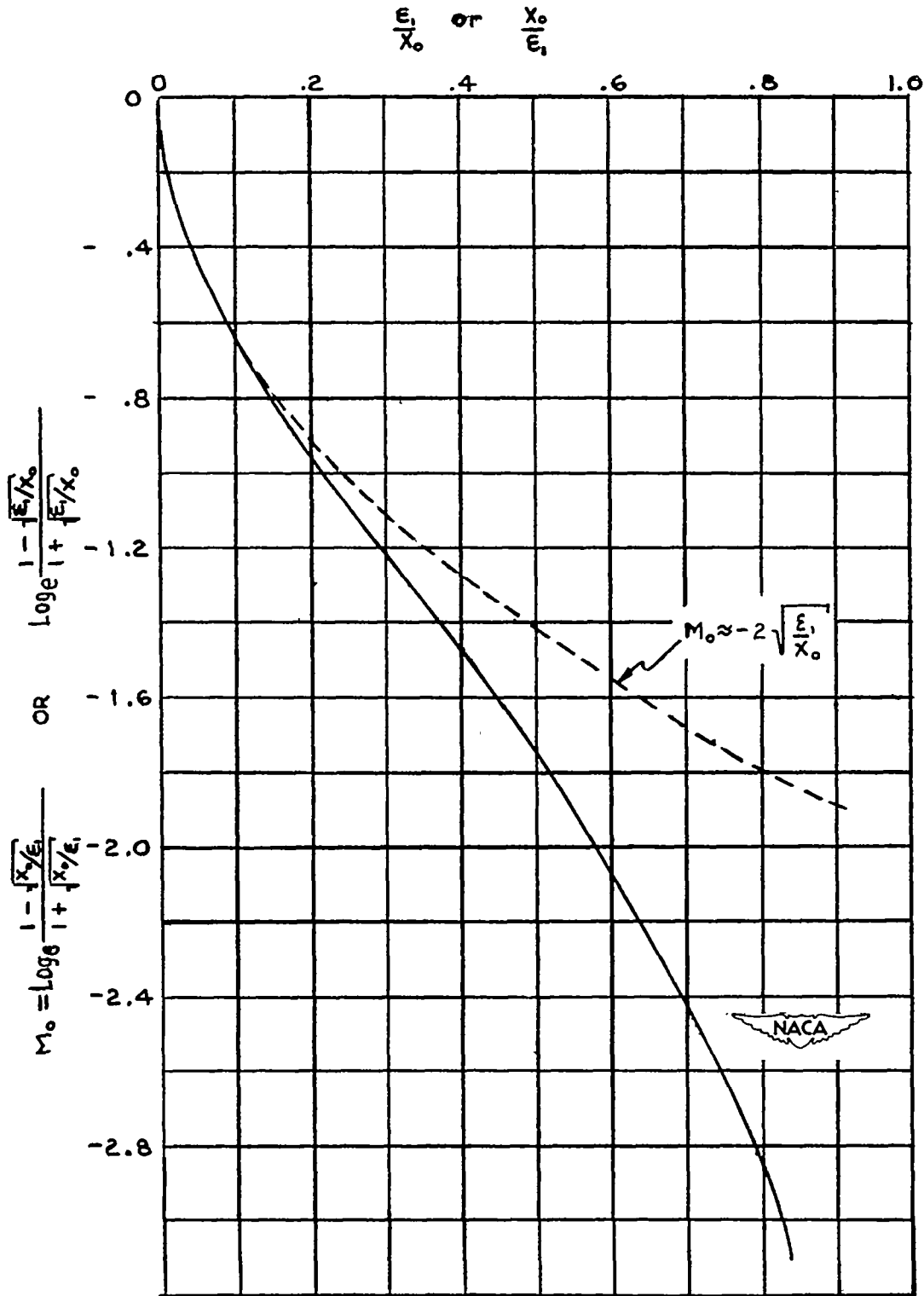
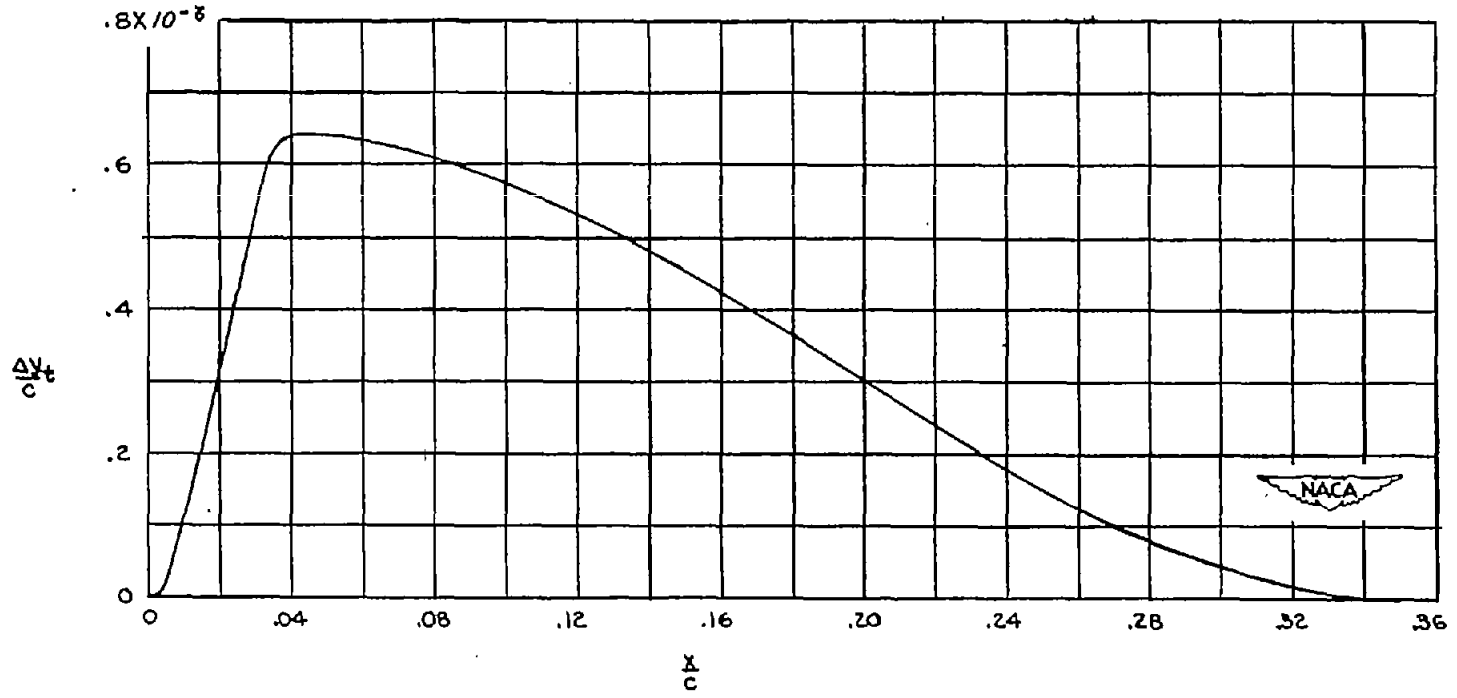


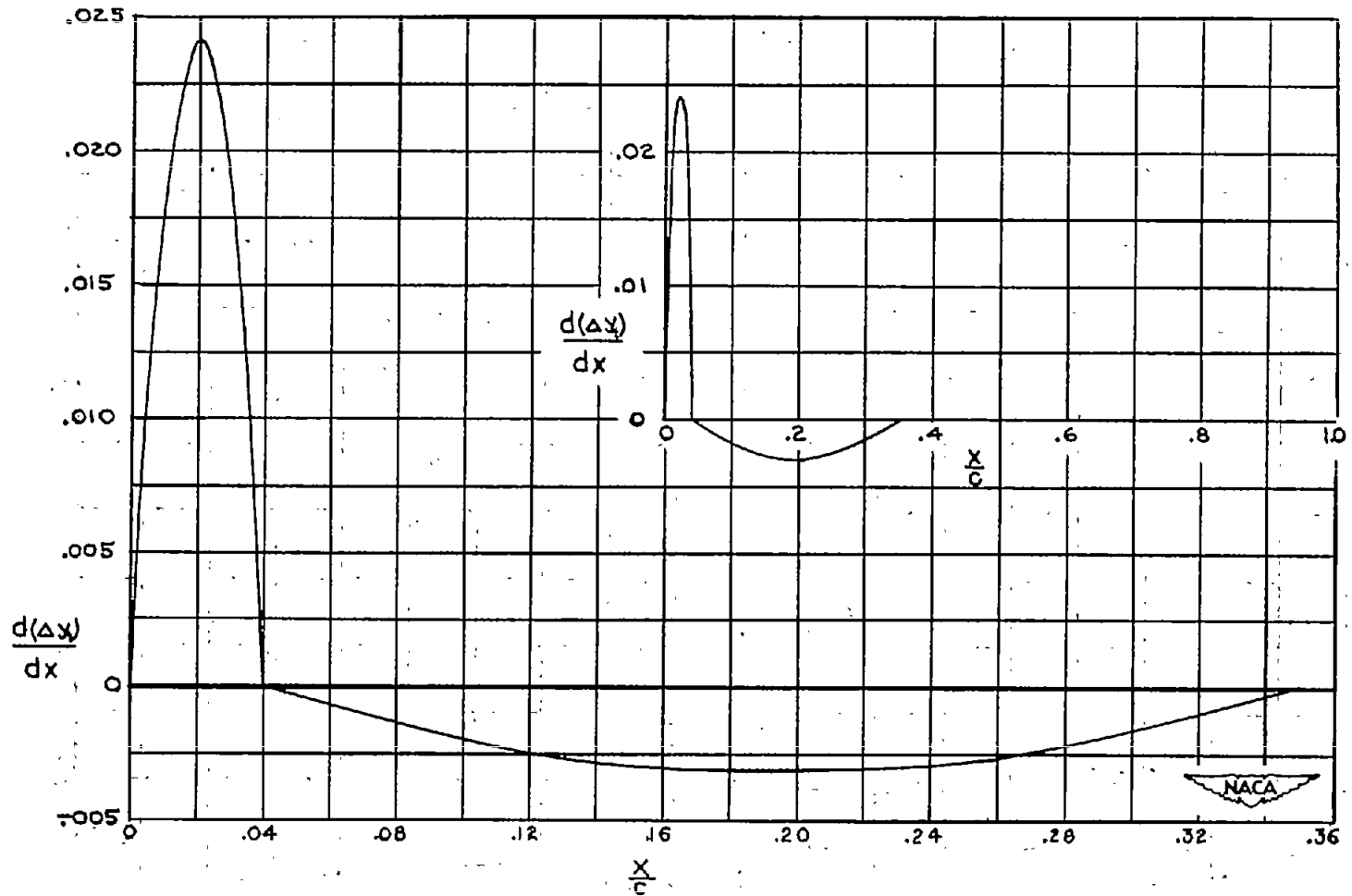
Figure 2.- Function  $M_0$  for computation when  $x_0/\epsilon_1$  or  $\epsilon_1/x_0$  is not small.



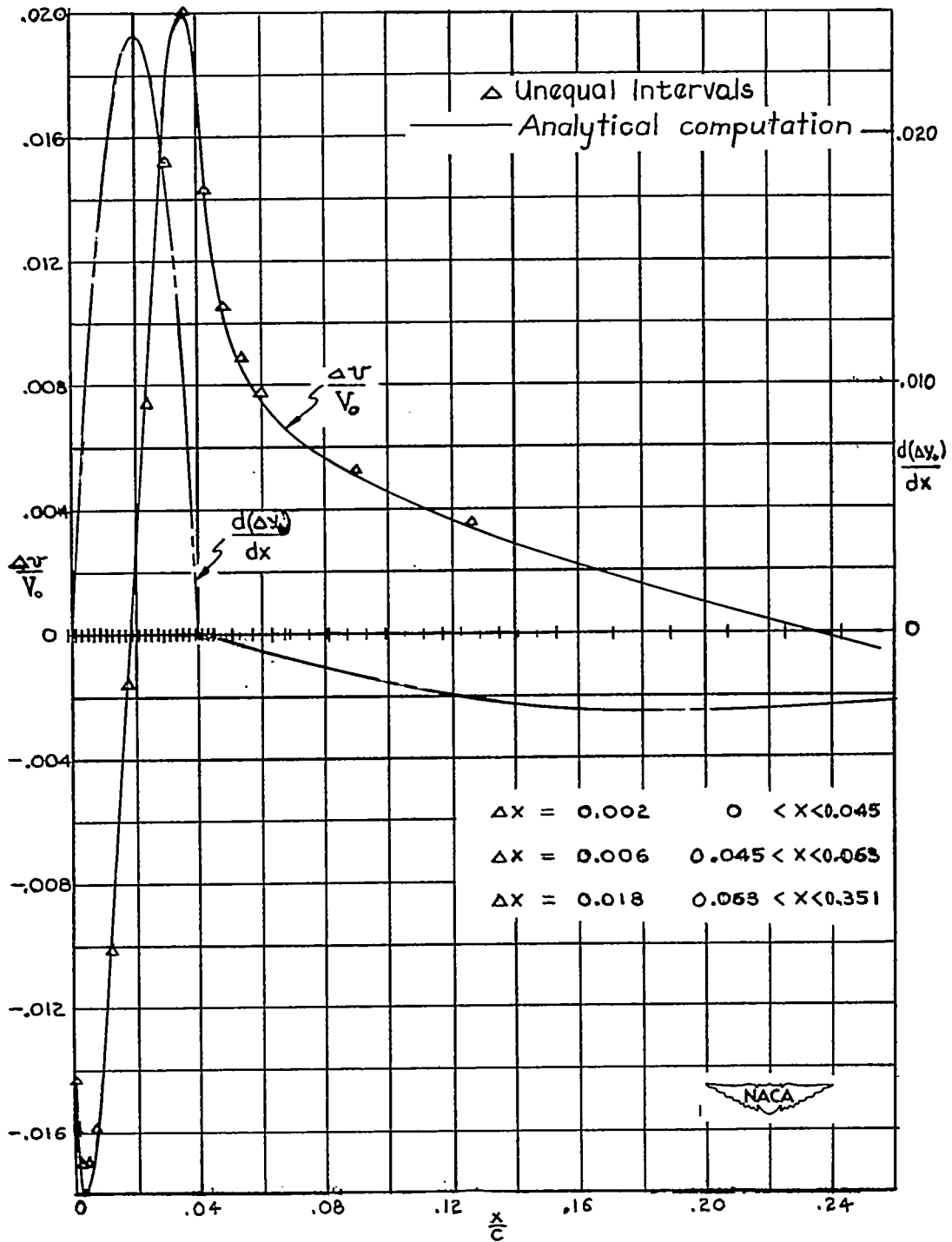


(a) Function  $\Delta y_t$ .

Figure 3.- Analytical example for testing accuracy of method.

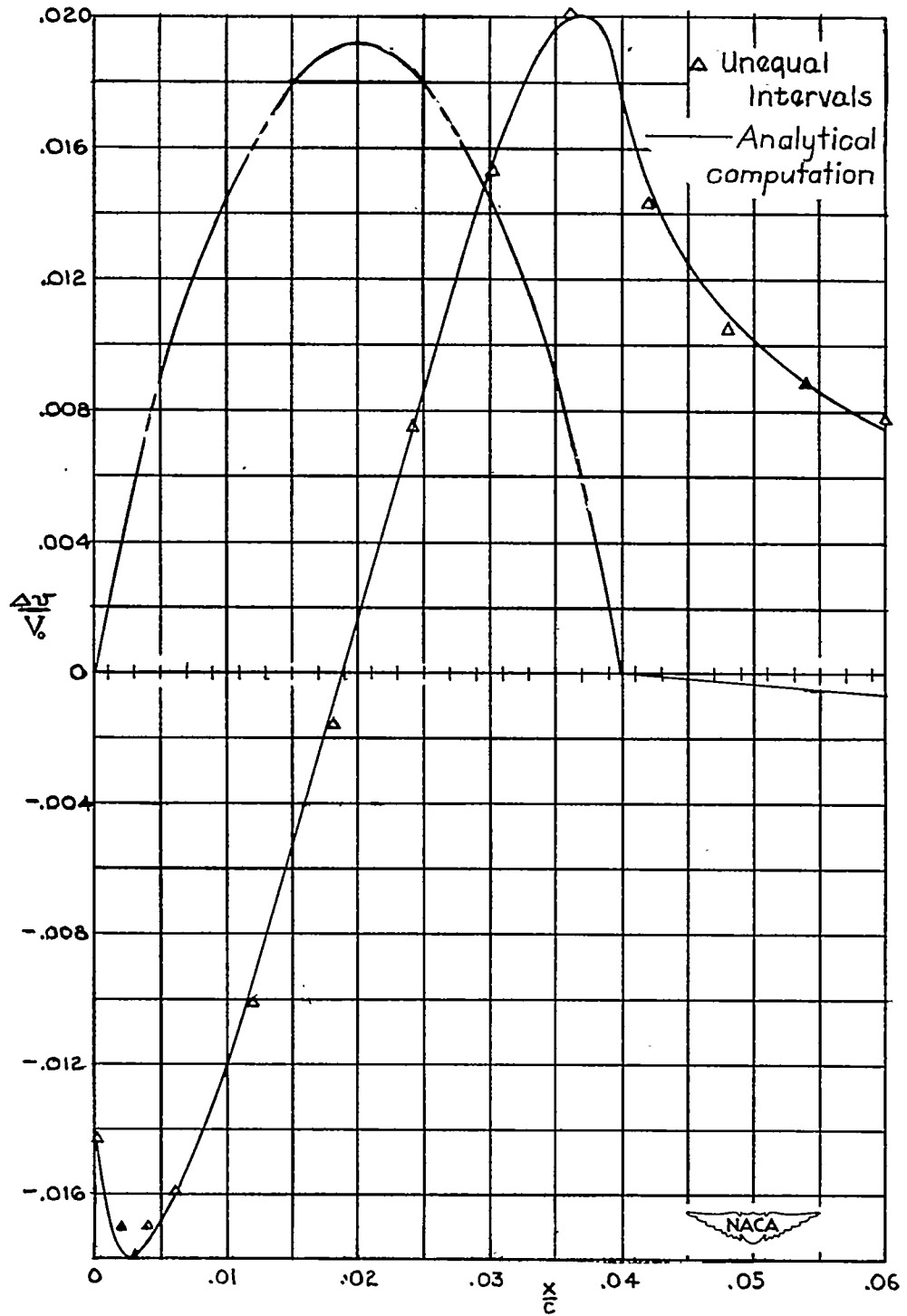


(b) Function  $\frac{d(\Delta y_t)}{dx}$ .



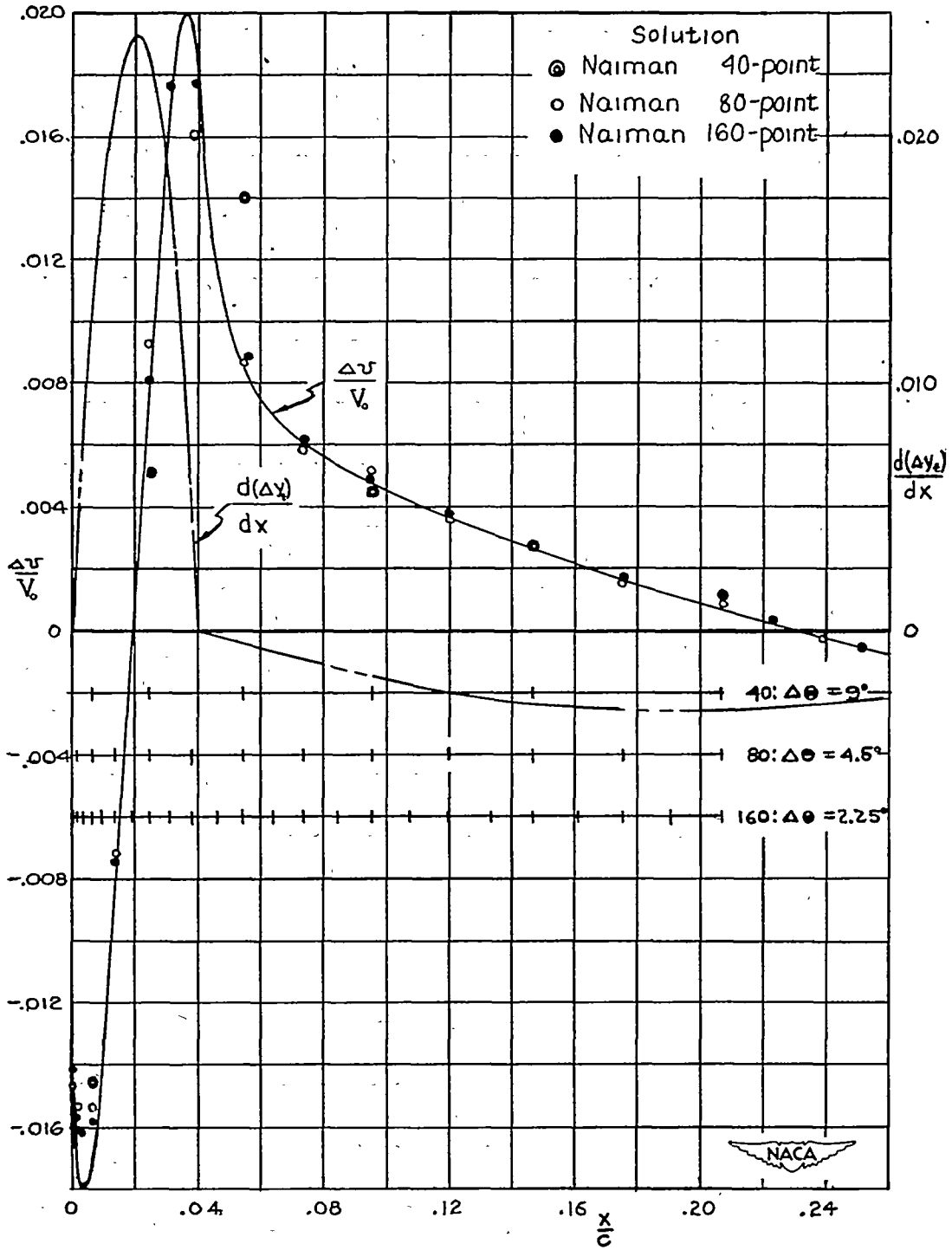
(a) Plot for  $0 < x < 0.25$ .

Figure 4.- Analytical computation of  $\frac{\Delta v}{V_0}$  for figure 3(b) and comparison with results by computation with unequal intervals.



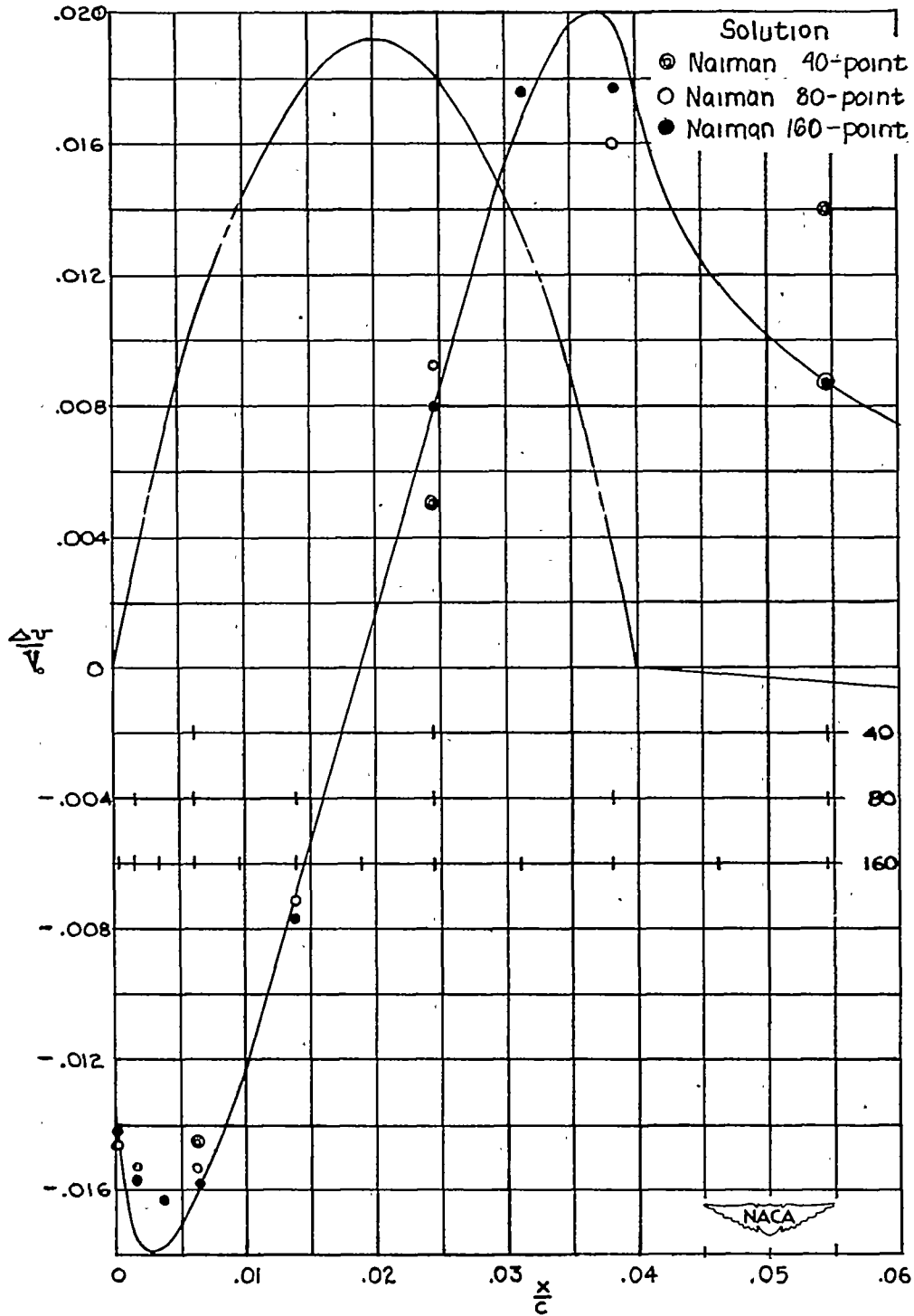
(b) Part of figure 4(a) plotted to larger scale.

Figure 4.- Concluded.



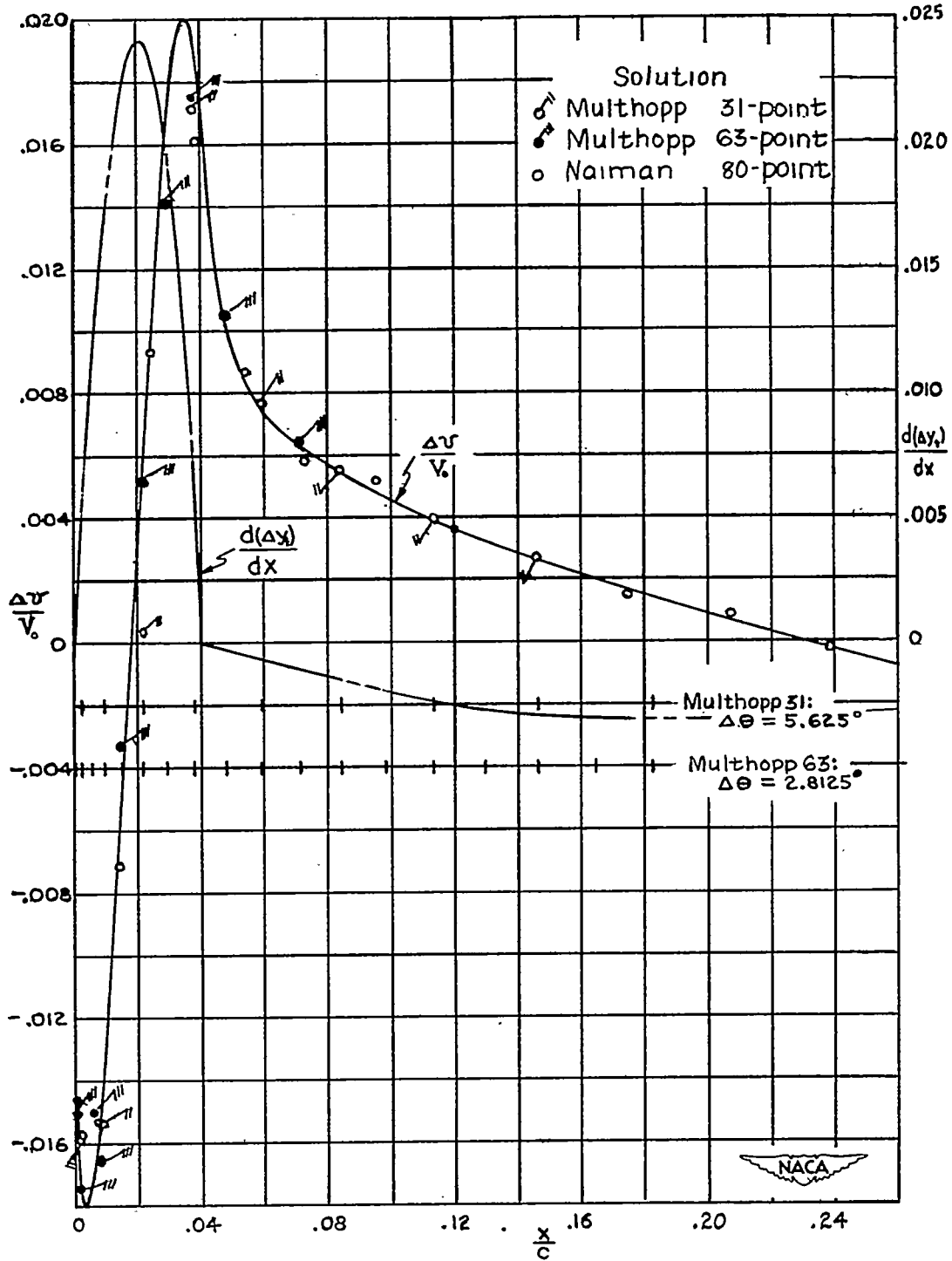
(a) Comparison with analytical results.

Figure 5.- Results obtained by Naiman's method. 40-, 80-, and 160-point solutions.



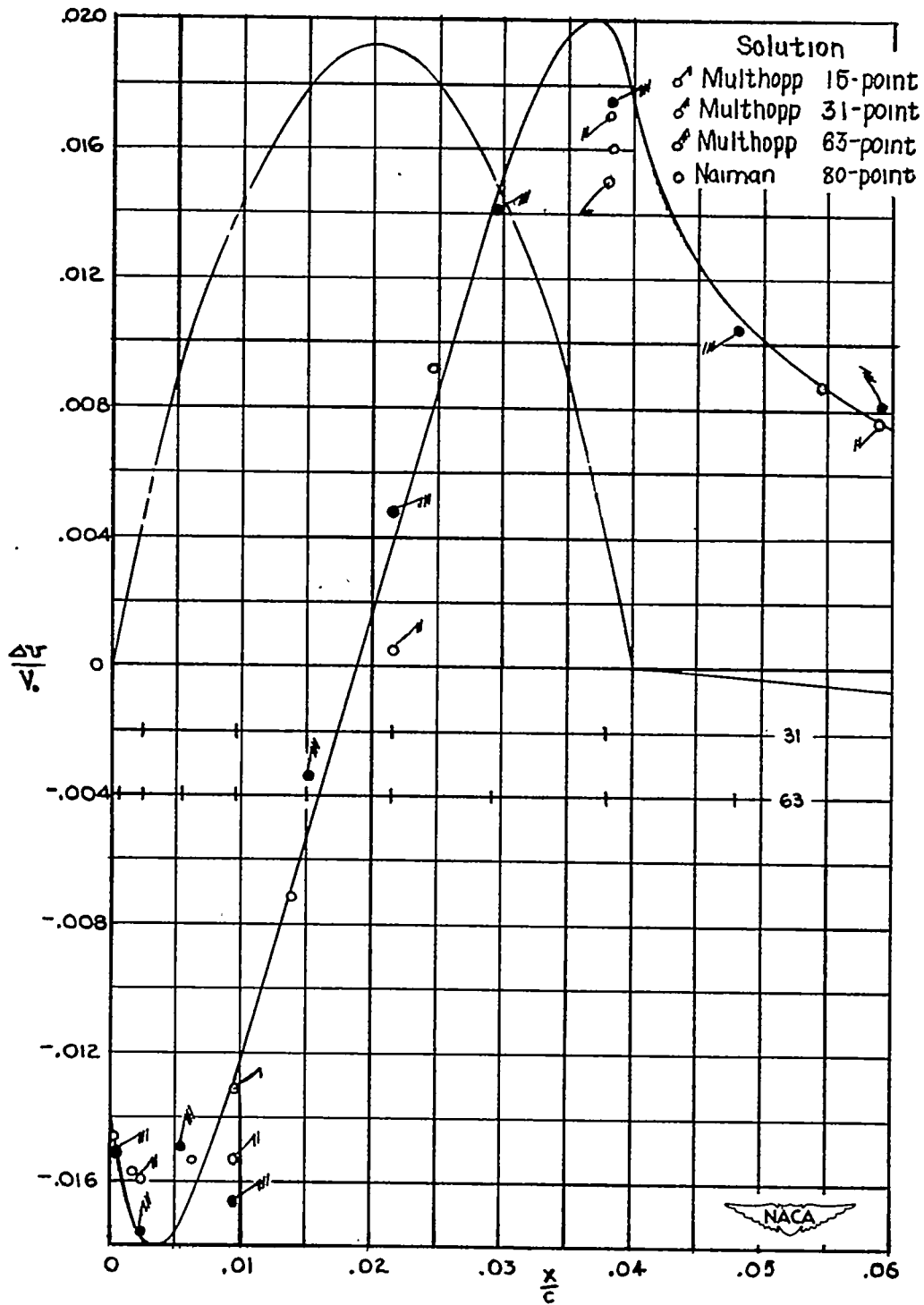
(b) Figure 5(a) plotted to a larger scale.

Figure 5.- Concluded.



(a) Comparison with analytical results and results of Naiman's method.

Figure 6.- Results obtained by Multihopp's method. 31- and 63-point solutions.



(b) Figure 6(a) plotted to larger scale.

Figure 6.- Concluded.



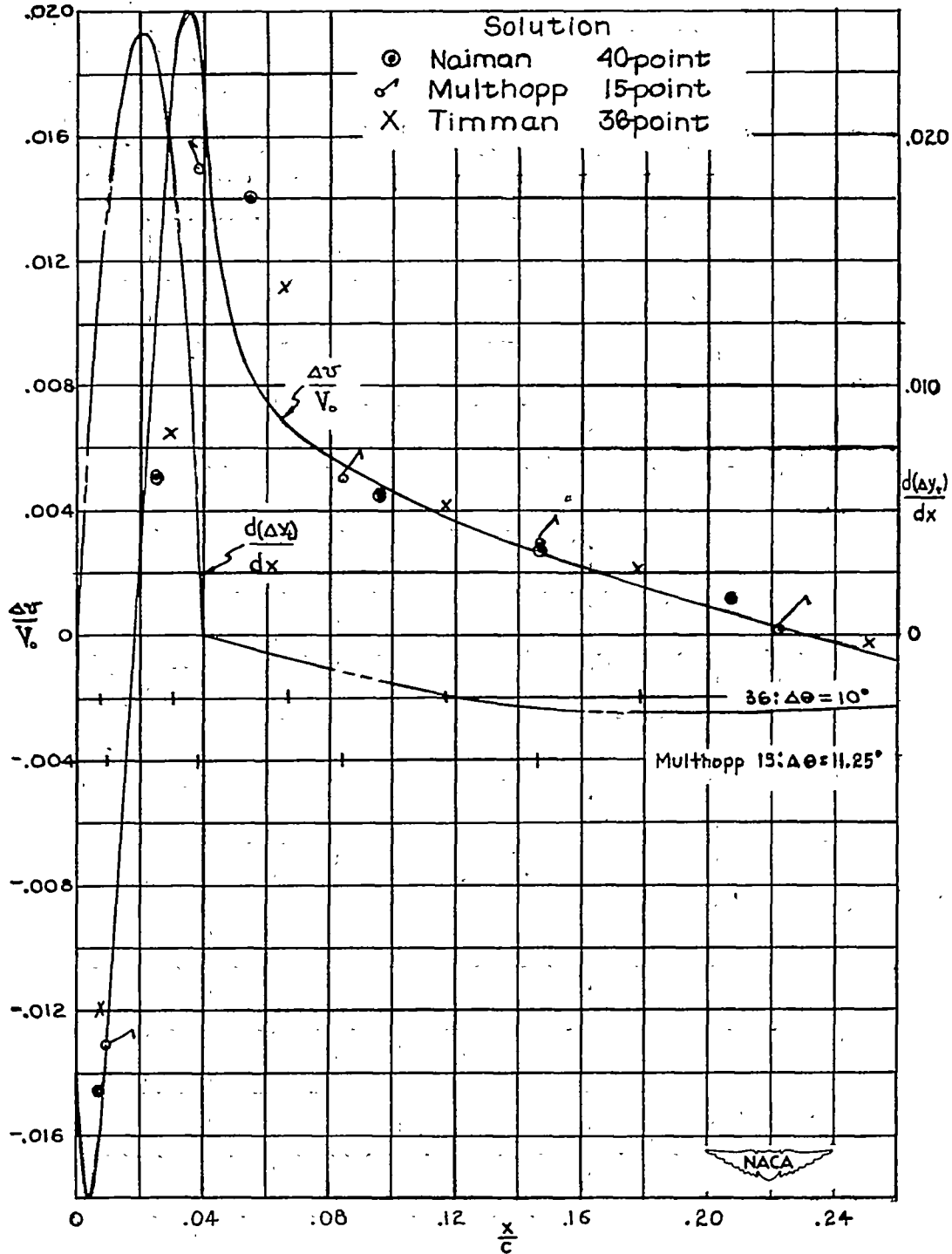


Figure 7.- Comparison of methods of Naiman, Multhopp, and Timman with analytical solution as basis.

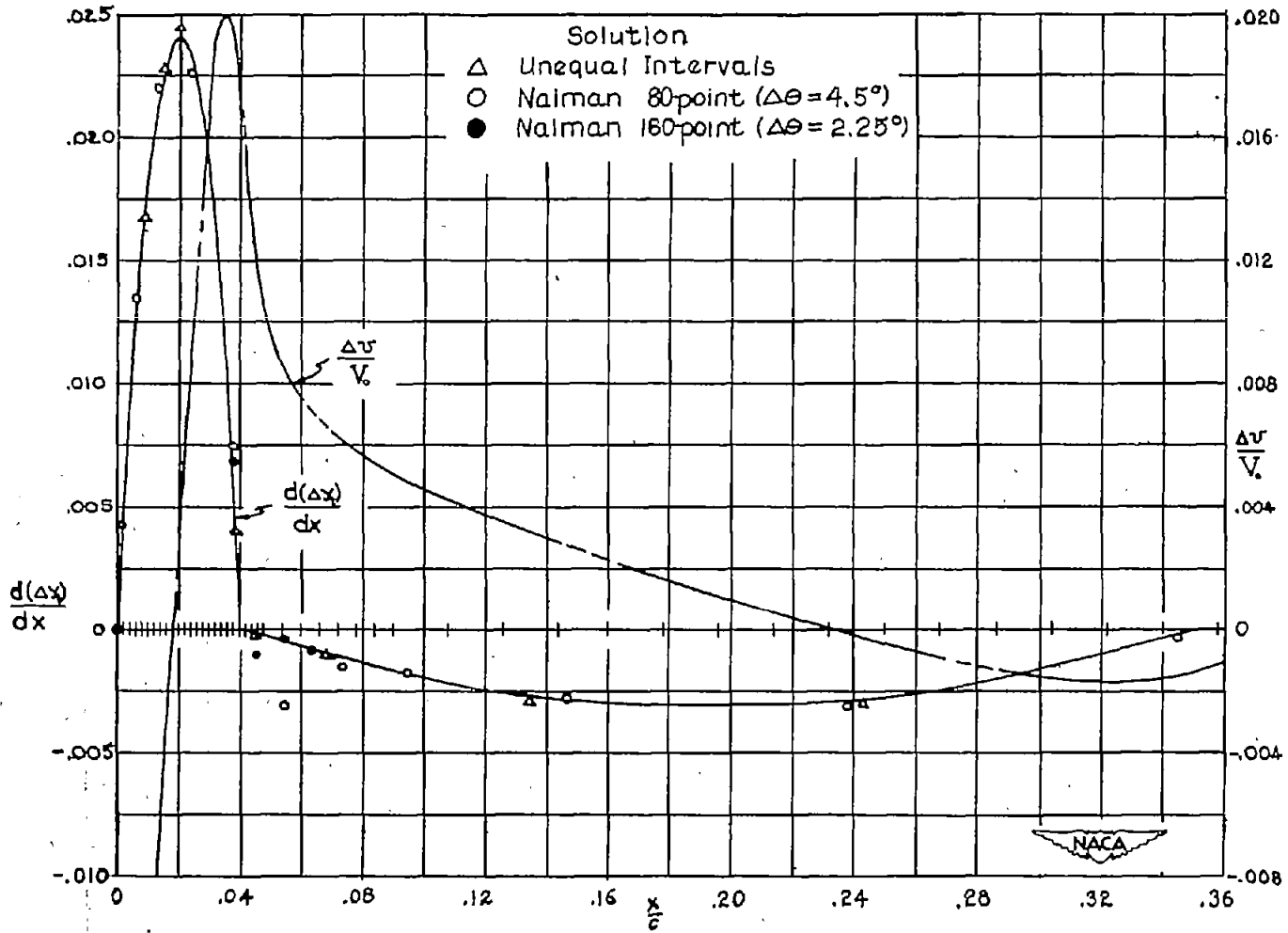
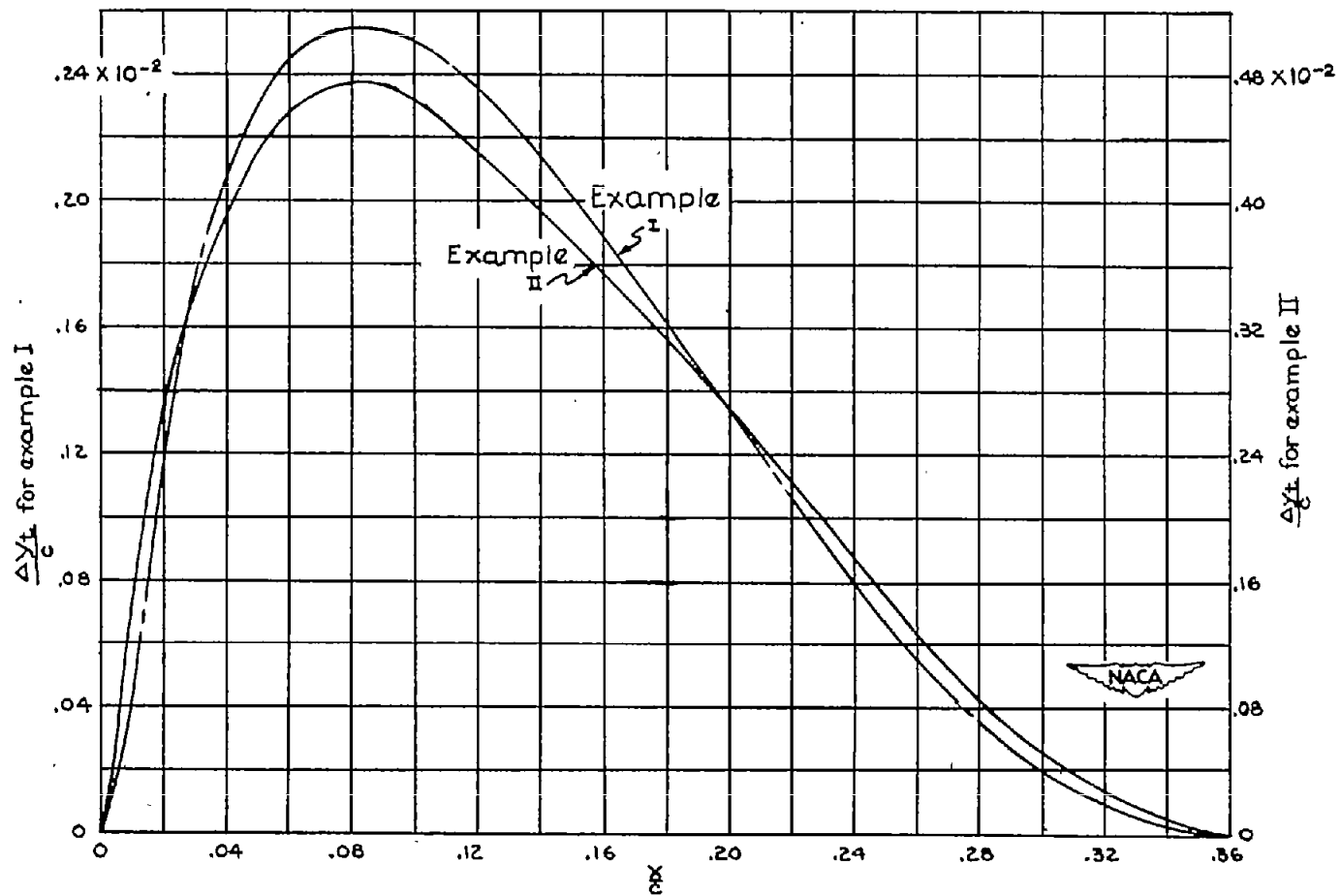
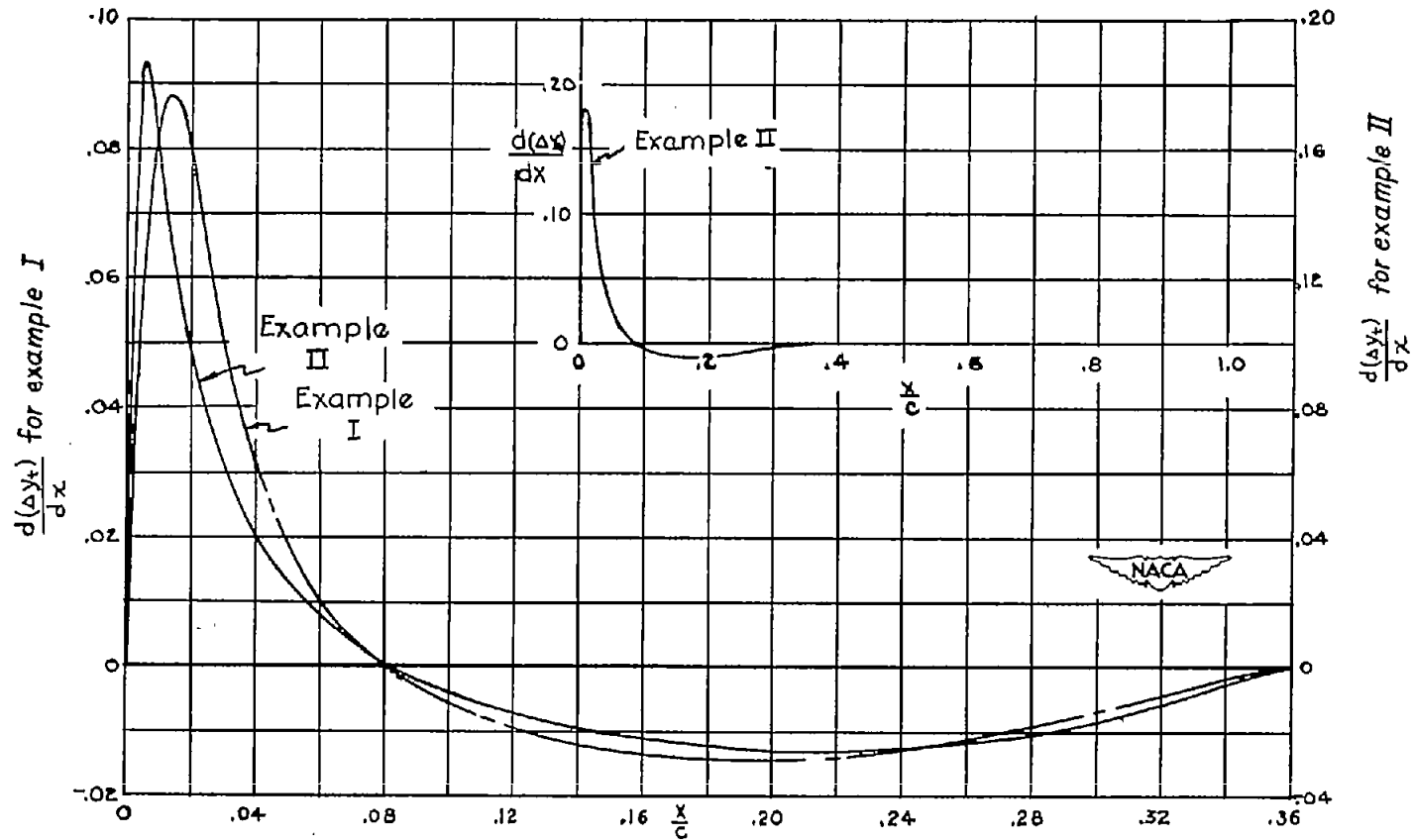


Figure 8.- Solution of inverse problem. Comparison of Naiman's 80- and 160-point solutions with that obtained by the method of unequal intervals.



(a) Functions  $\Delta y_t(x)$ .

Figure 9.- Examples I and II.



(b)  $\frac{d(\Delta y_t)}{dx}$  as function of  $x/c$ .

Figure 9.- Concluded.

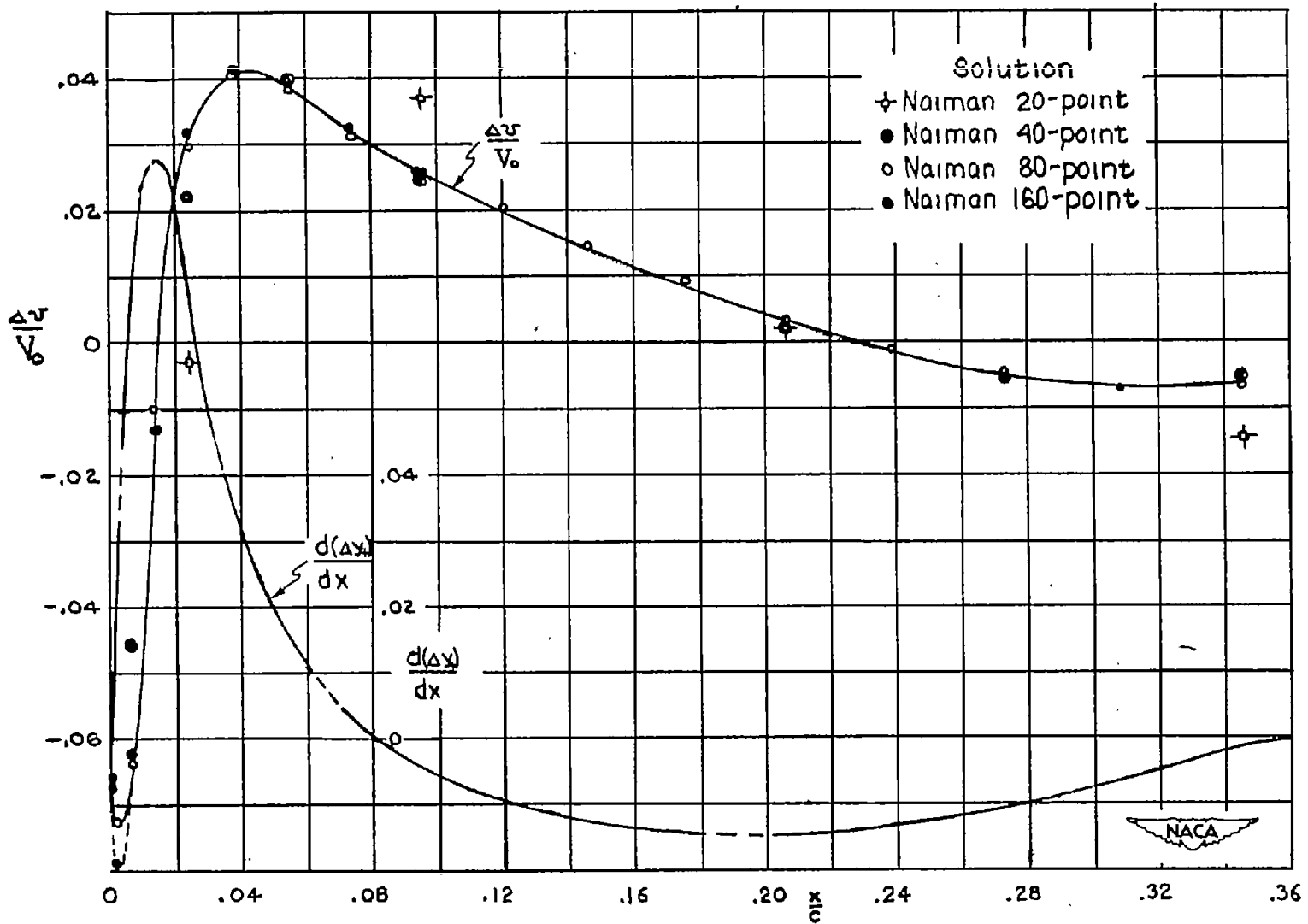


Figure 10.- Direct problem for example I by Naiman's method.

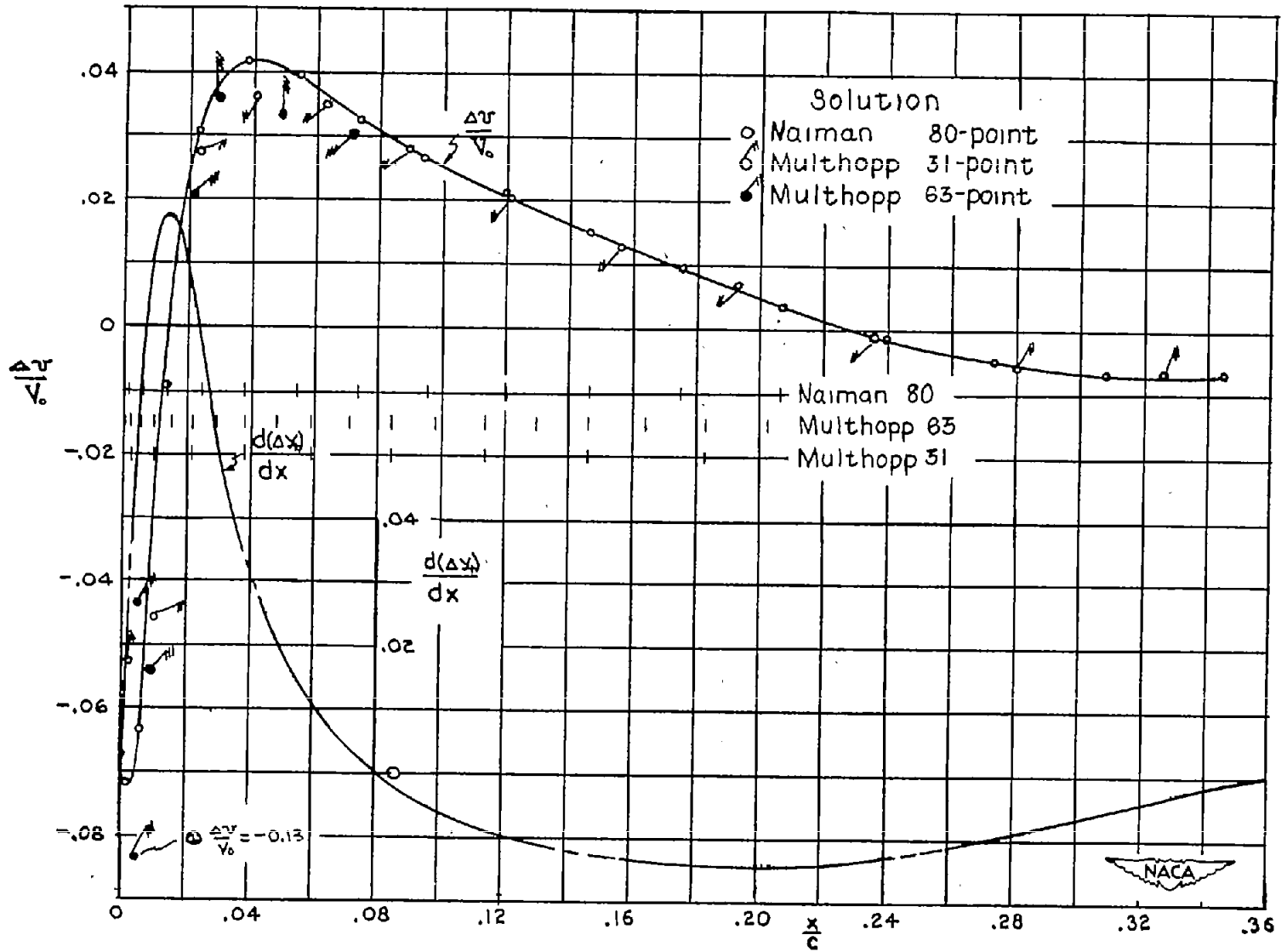


Figure 11.- Direct problem for example I by Multhopp's method.

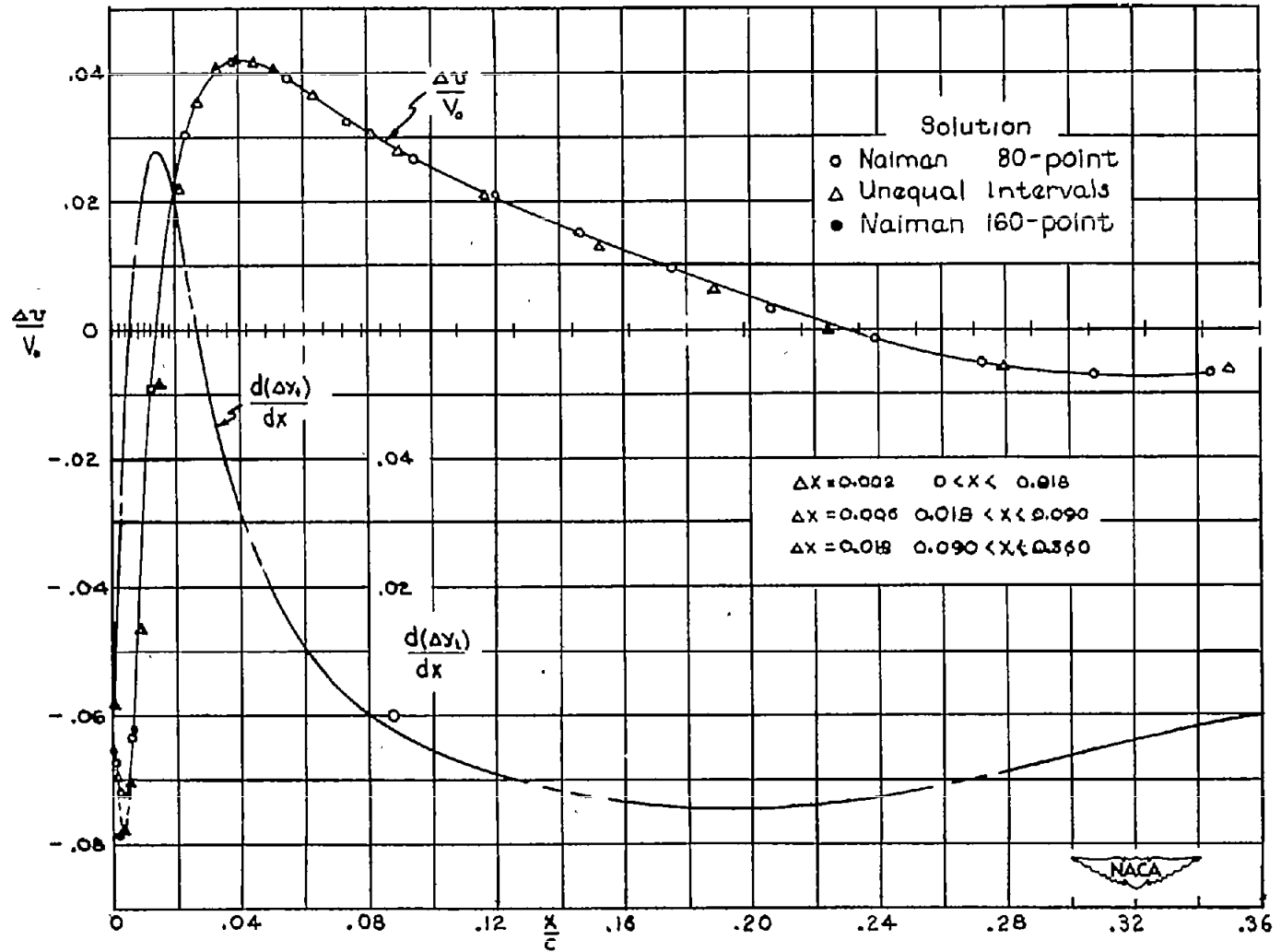


Figure 12.- Results obtained for example I by method of unequal intervals compared with results obtained by Naiman's 80- and 160-point solutions.

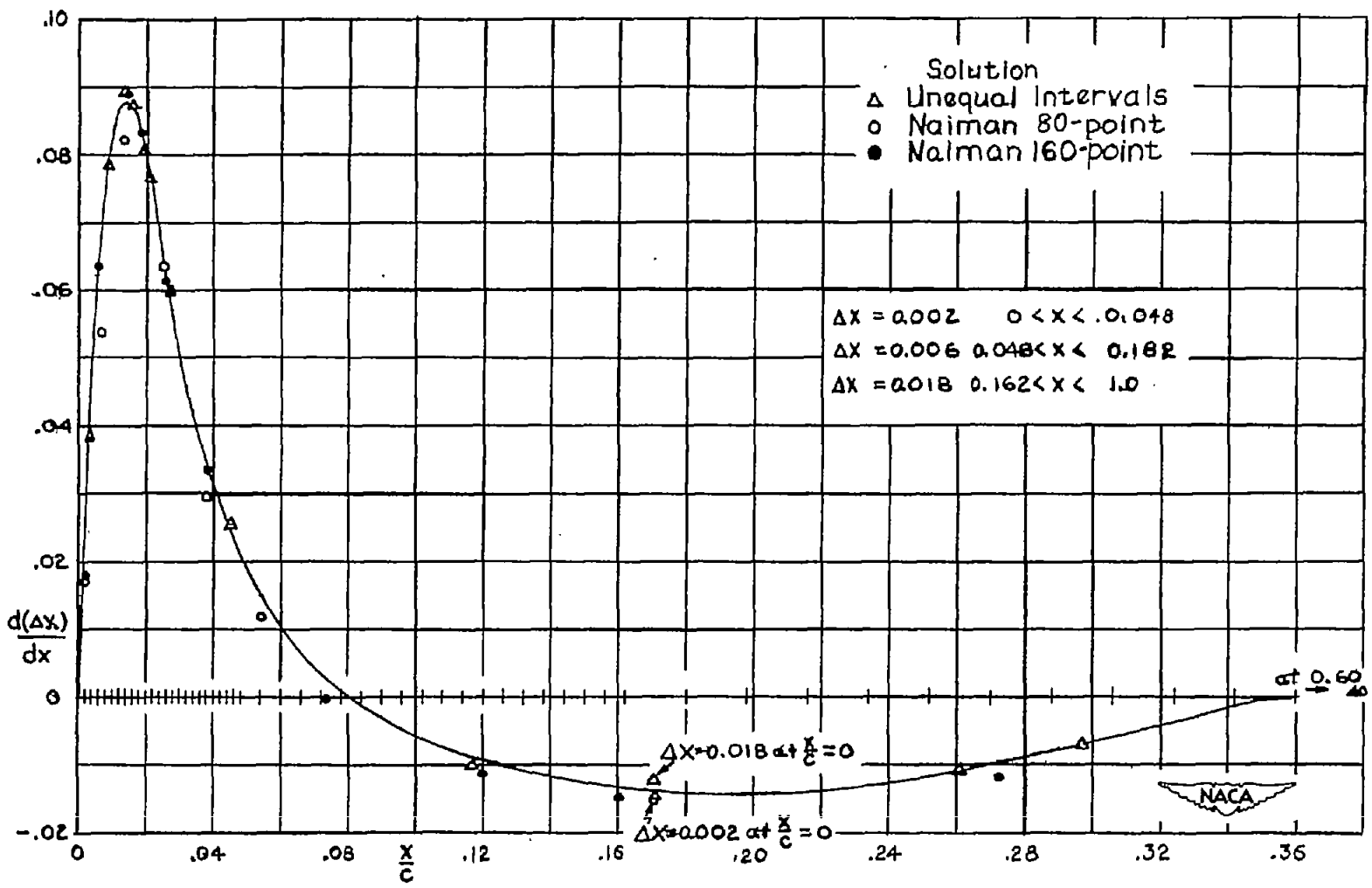


Figure 13.- Solution of inverse problem. Results obtained for example I by method of unequal intervals compared with results obtained by Naiman's 80- and 160-point solutions.



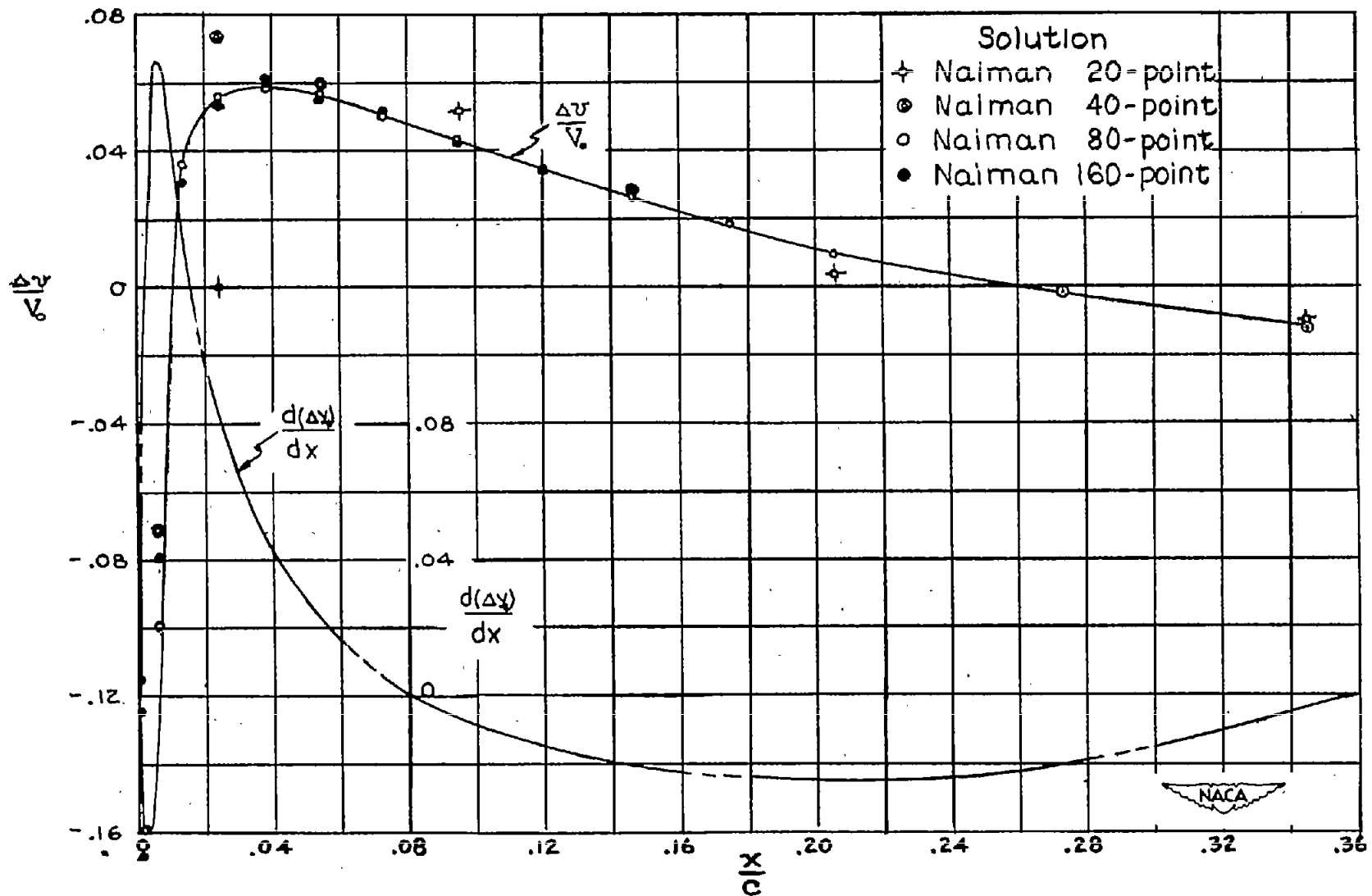


Figure 14.- Direct problem for example II by Naiman's method.

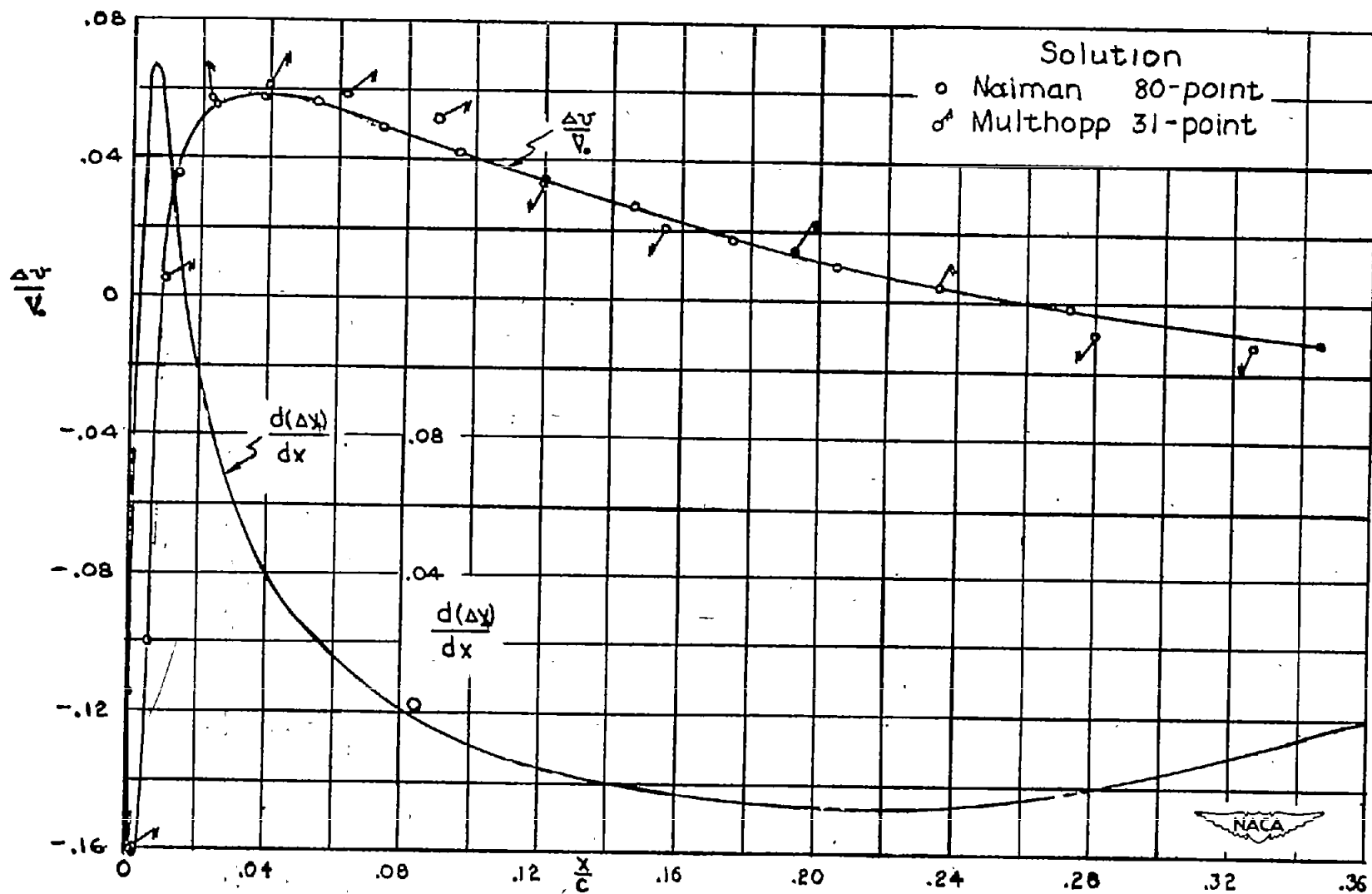


Figure 15.- Direct problem for example II by Multhopp's method.

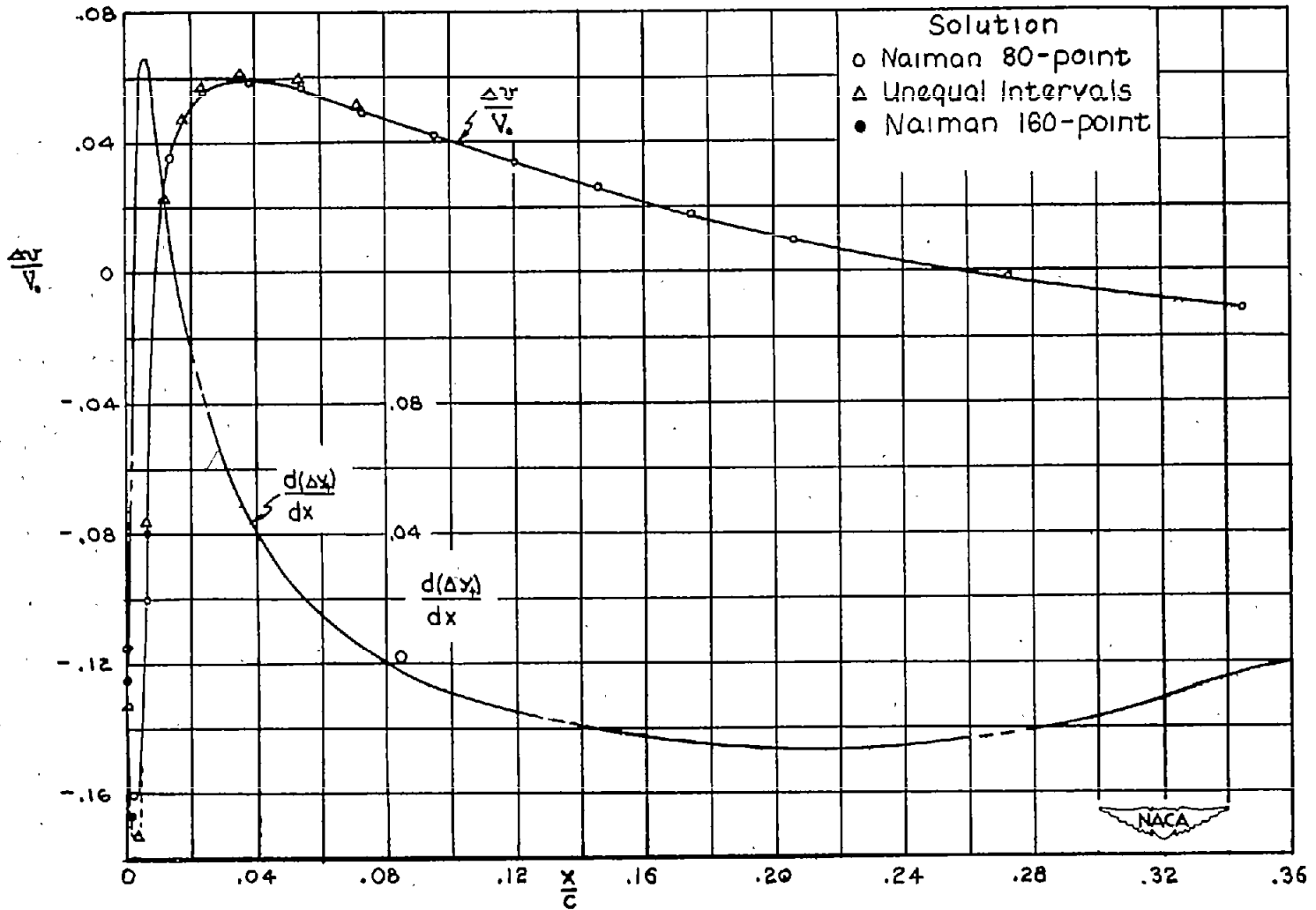


Figure 16.- Results obtained for example II by method of unequal intervals compared with results obtained by Naiman's 80- and 160-point solutions.

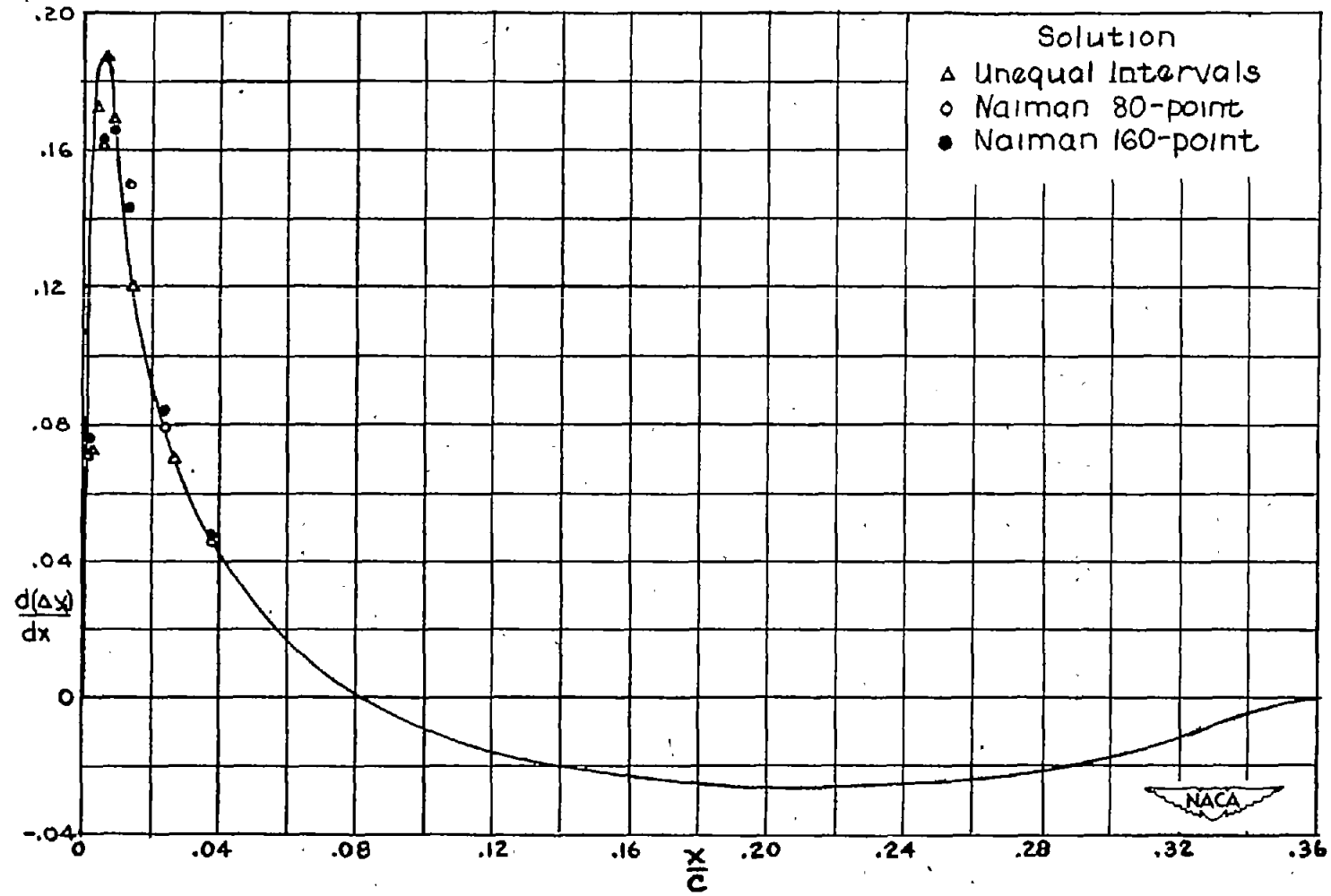


Figure 17.- Solution of inverse problem. Results obtained for example II by method of unequal intervals compared with results obtained by Naiman's 80- and 160-point solutions.

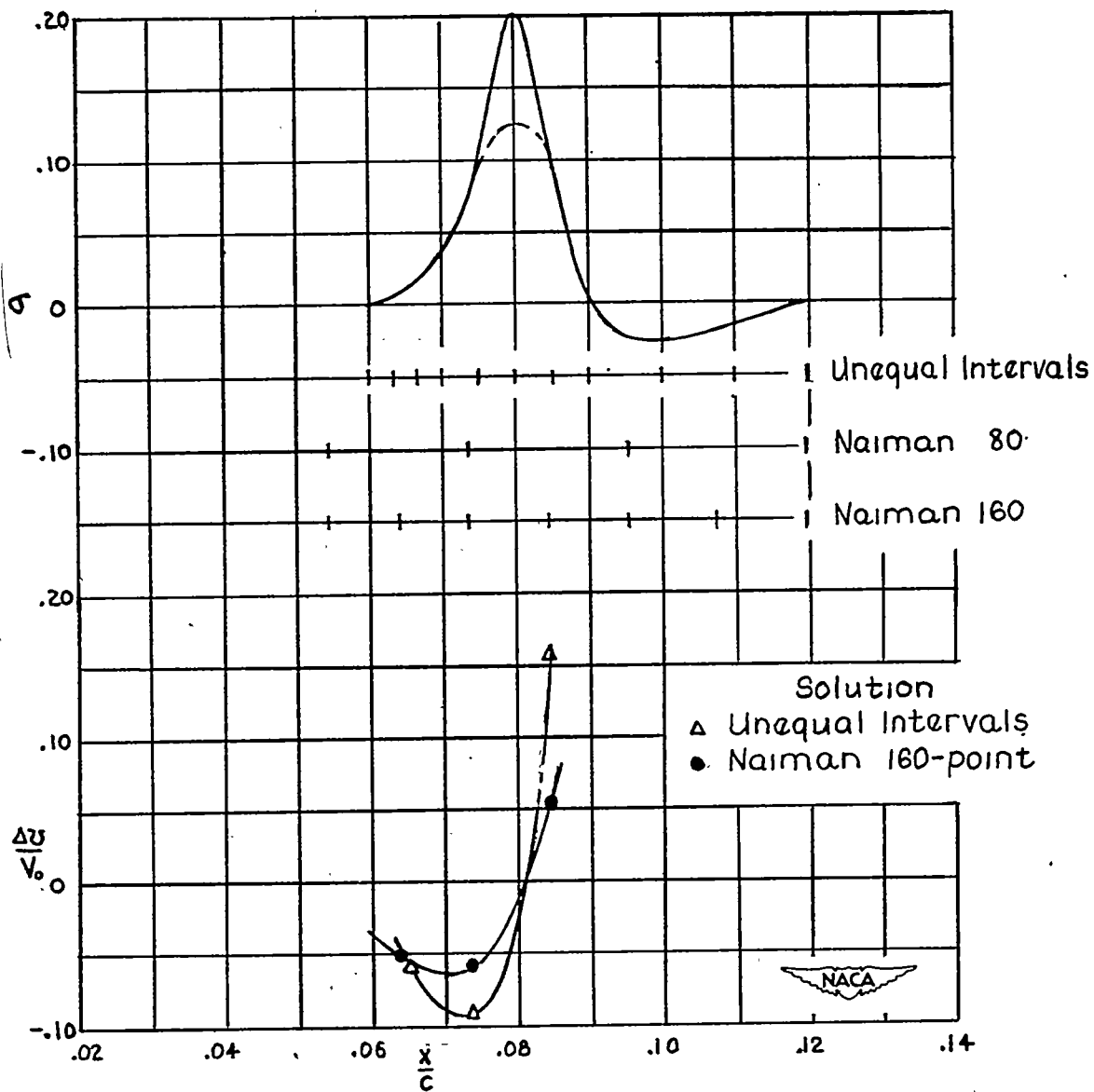


Figure 18.- Results obtained for example III by method of unequal intervals compared with results obtained by Naiman's 80- and 160-point solutions.