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RESEARCH MEMORANDUM

PRESSURE DISTRIBUTIONS ON THE BLADE SECTIONS
OF THE NACA 10-(5)(066)-03 PROPELLER
UNDER OPERATING CONDITIONS

By Albert J. Evans and Wallace Luchuk

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NATIONAL ADVISORY COMMITTEE FOR AERONAUTICS

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PRESSURE DISTRIBUTIONS ON THE BLADE SECTIONS
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SUMMARY

A broad investigation has been made in the Langley 16-foot high-speed tunnel to determine propeller section aerodynamic characteristics by measuring the surface pressure distribution on the airfoil sections of a rotating propeller. Five specially designed propellers incorporating NACA 16-series airfoil sections were tested. The design parameters of the five propellers covered a range of section thickness ratio and design camber.

This paper presents the data obtained from the tests of one of the five propellers. The present tests were conducted on the NACA 10-(5)(066)-03 propeller which had the highest cambered blades of the group. The design camber of all the sections tested was 0.5 and the thickness-chord ratio varied from 16 percent to 4 percent. The data are presented in tabular form as pressure coefficient, normal-force coefficient, chordwise-force coefficient, and moment coefficient. A geometric angle-of-attack range from -3.5° to 11° was covered in the Mach number range from 0.40 to 0.80. For higher Mach numbers, from 0.80 to 1.15, the section nominal angle of attack varied from -2.5° to 3.5° .

The results are presented as preliminary data for each propeller test made and no attempt has been made to analyze the data.

INTRODUCTION

Since propeller sections operate at speeds considerably higher than those encountered on other parts of an airplane, the propeller designer and analyst have continually been faced with a lack of airfoil data in the transonic speed range. At subsonic speeds above the critical speed of the airfoil nearly all available data are subject to wind-tunnel

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choking effects, and attempts at extrapolation to higher values of Mach number have yielded uncertain results. Even if the two-dimensional data were available for supercritical values of Mach number, the effects of velocity gradient along the blade, the three-dimensional tip effects, and the action of the centrifugal force on the boundary layer along the blade impose problems that need to be investigated on the operating propeller.

As a first step toward obtaining propeller section data, tests were made in the Langley 16-foot high-speed tunnel whereby section aerodynamic characteristics were determined by measuring the surface pressure distributions on the operating propeller blade sections of an NACA 10-(3)(08)-03 propeller. Preliminary results of these tests are presented in reference 1.

The success of the initial investigation led to the inauguration of a broad program of tests during which five propellers were tested in the two-blade configuration and to a limited extent in the one-blade configuration. The five propellers were designed especially for this investigation and the design parameters covered a range of section thickness-chord ratio and a range of section design lift coefficient. The propellers tested are designated as follows:

NACA 10-(3)(066)-03
NACA 10-(3)(049)-03
NACA 10-(3)(090)-03
NACA 10-(5)(066)-03
NACA 10-(0)(066)-03

The results of the tests of the NACA 10-(3)(066)-03, the NACA 10-(3)(049)-03, and the NACA 10-(3)(090)-03 propellers were reported in references 2, 3, and 4, respectively. It is pointed out that the propeller designations as given in references 2 and 3 are in error in that the digits after the last hyphen in the designation should read 03 instead of 033.

This paper presents the results of the NACA 10-(5)(066)-03 propeller which is the highest cambered propeller of the present program. The results are presented as pressure coefficient, normal-force coefficient, pitching-moment coefficient, and chordwise-force coefficient in tabular form. No analysis of the data is presented other than that which is considered essential for a clear understanding of the data presented.

SYMBOLS

The symbols used throughout this paper, some of which are defined in figure 3, are as follows:

B	number of blades
b	blade chord, feet
c	distance from section leading edge to any point on the chord, feet
\bar{c}	distance from section leading edge to any point about which pitching moments are taken, feet
c_c	section chordwise-force coefficient
c_l	section lift coefficient
c_{ld}	blade-section design lift coefficient
c_m	section pitching-moment coefficient about the quarter-chord point
c_n	section normal-force coefficient
D	propeller diameter, feet
F_c	section chordwise pressure force, pounds
F_n	section normal pressure force, pounds
G	Goldstein induced-velocity correction factor for a finite number of blades
h	blade-section maximum thickness, feet
J	advance ratio (V/nD)
M	Mach number of advance
M_x	helical section Mach number $\left(M \sqrt{1 + \left(\frac{\pi x}{J} \right)^2} \right)$
m	section pitching moment, pound-feet
N	propeller rotational speed, rpm.

n	propeller rotational speed, rps
P	pressure coefficient $\left(\frac{p - p_0}{q_x}\right)$
p	static pressure at a point on the airfoil surface, pounds per square foot
p_0	free-stream static pressure, pounds per square foot
q_x	resultant dynamic pressure at a radial station x, pounds per square foot $\left(\frac{1}{2}\rho W_0^2\right)$
R	propeller-tip radius, feet
r	radius to a blade element, feet
r_p	polar ordinate, feet
s	distance along surface of blade section, feet
V	velocity of advance (corrected for wind-tunnel-wall interference effects), feet per second
W_0	velocity vector $\left(V \sqrt{1 + \left(\frac{\pi x}{J}\right)^2}\right)$
W	resultant velocity at blade section, feet per second
w_1	induced velocity at blade section, feet per second
x	fraction of propeller-tip radius (r/R)
y	normal distance from chord line to upper or lower surface of airfoil, inches
α_1	induced angle of attack, degrees
α_x	angle of attack of blade element, corrected for induced flow and blade deflection, at radial station x, degrees $(\beta_x - \phi + \Delta\beta)$
α_x'	geometric angle of attack of blade element at radial station x, degrees $(\beta_x - \phi_0)$
β	blade angle, degrees

$\beta_{0.75R}$	blade angle at 0.75 tip radius, degrees
β_x	blade angle at station x, degrees
$\Delta\beta$	change in blade angle caused by operation loads, degrees
γ	ratio of specific heats for air (1.4)
θ	polar angular ordinate, radians
ρ	mass density of air in free stream, slugs per cubic foot
σ	solidity $\left(B \frac{b}{D} / \pi x \right)$
ϕ	helix angle, degrees
ϕ_0	geometric helix angle, degrees $\left(\tan^{-1} (J/\pi x) \right)$
ψ	slope angle at the surface of the section, referenced to chord, degrees
ω	propeller rotational speed, radians per second
Subscripts:	
L	lower-surface value
U	upper-surface value

APPARATUS

Basic equipment.- The tests were made with the NACA 2000-horsepower propeller dynamometer in the Langley 16-foot high-speed tunnel. A complete description of the dynamometer is contained in reference 5. The pressure-transfer device used to transfer the pressures measured at the blade surface orifices from the rotating members of the test setup to the stationary manometers is described in reference 2 together with a description of the optical deflectometer. The deflectometer was necessary for an accurate determination of the blade-section angles of attack because the blades twisted due to the air loads and centrifugal force acting on the blade when the propeller was operating. A schematic diagram of the test setup is shown in figure 1.

Propellers.- The propeller blades were of solid duralumin construction and were designated the NACA 10-(5)(066)-03 design. The digits

in the propeller designation describe the propeller diameter and the airfoil section at the design radius ($\frac{r}{R} = 0.70$) as follows: propeller diameter, 10 feet; section design lift coefficient, 0.50; section thickness-chord ratio, 0.066; and solidity per blade, 0.03. The blades had a rectangular plan form with a blade width of 8 inches and were made up of NACA 16-series sections throughout having a design lift coefficient of 0.50 along the entire radius with the exception of a small portion near the tip. Due to inaccuracies in the fabrication process the section at the $\frac{r}{R} = 0.975$ station was not precisely an NACA 16-series section.

From measurements made at the $\frac{r}{R} = 0.975$ station the actual section was determined and the ordinates are given in table 1 together with a sketch of the actual section compared with an NACA 16-series section. Blade-form characteristic curves are presented in figure 2.

Twenty-four pressure tubes were imbedded in the surface of one of the blades together with a resistance thermometer imbedded in the thrust face. Details of the blade construction, pressure tube and orifice installation, and temperature measurements are described in reference 2.

TESTS

The tests were made at a blade-angle setting of 45° at the $\frac{r}{R} = 0.75$ station. For most of the tests a constant rotational speed was used and a range of advance ratio was covered by changing the tunnel airspeed, which was varied from about 215 to 500 miles per hour. At higher speeds, however, the dynamometer could not deliver sufficient torque for operation at constant rotational speed and for this reason high-speed data were obtained by operating the tunnel at constant high values of Mach number and the advance ratio was varied by changing rotational speed. The test procedure and techniques employed are described in detail in reference 2.

Pressure-distribution data were obtained on the sections located at the following stations with the test blade operating in a two-blade propeller; $\frac{r}{R} = 0.30, 0.45, 0.60, 0.70, 0.78, 0.85, 0.90, 0.95,$ and 0.975 .

In order to extend the range of advance ratio to lower values and, consequently, to extend the range of angle of attack and normal-force coefficient to high values, pressure data were obtained on the section

at the $\frac{r}{R} = 0.95$ station with the test blade operating as a one-blade propeller. The details of the one-blade test procedure are also described in reference 2.

The range of Mach number and angle of attack covered and the operating conditions for each test are specified in tables 2 to 10. The table index provides an outline of the test schedule.

REDUCTION OF DATA

The following equations, which are explained in detail in reference 2, have been used in the reduction of the section data presented herein.

Section pressure coefficient:

$$P = \frac{p - p_o}{q_x} \quad (1)$$

Section normal force:

$$F_n = \int_0^b p \cos \psi \, ds = \int_0^{1.0} \left[(P_L - p_o) - (P_U - p_o) \right] \frac{dc}{b} \quad (2)$$

Section normal-force coefficient:

$$c_n = \frac{F_n}{q_x b} = \int_0^{1.0} (P_L - P_U) \frac{dc}{b} \quad (3)$$

Section chordwise force:

$$F_c = \int_0^b p \sin \psi \, ds = \int_0^{1.0} \left[(P_U - p_o) \tan \psi_U - (P_L - p_o) \tan \psi_L \right] \frac{dc}{b} \quad (4)$$

Section chordwise-force coefficient:

$$c_c = \frac{F_c}{q_x b} = \int_0^{1.0} \left[P_U \tan \psi_U - P_L \tan \psi_L \right] \frac{dc}{b} \quad (5)$$

or, in polar coordinates,

$$c_c = \int_0^{2\pi} (P) \left[\frac{\sin \psi}{\sin(\theta - \psi)} \right] \left(\frac{r_P}{b} \right) d\theta \quad (6)$$

Equation (5) was used to evaluate that portion of chordwise-force coefficient from $\frac{c}{b} = 0.025$ to $\frac{c}{b} = 1.0$ and equation (6) was used to evaluate the chordwise-force coefficient from $\frac{c}{b} = 0$ to $\frac{c}{b} = 0.025$.

Section pitching-moment coefficient:

$$c_m = \frac{m}{q_x b^2} = \frac{\bar{c}}{b} \int_0^{1.0} (P_L - P_U) \frac{d\bar{c}}{b} - \int_0^{1.0} (P_L - P_U) \frac{c}{b} \frac{d\bar{c}}{b} \quad (7)$$

where $\frac{\bar{c}}{b} = 0.25$.

Section angle of attack:

$$\alpha_x = \alpha_x' + \Delta\beta - \alpha_1$$

where α_1 , the induced angle of attack, was computed by use of Goldstein's correction for a finite number of blades as applied by Lock in reference 6 as described in reference 2.

The torsional deflection of the blades $\Delta\beta$ due to the combination of the air loads and centrifugal loads on the blades was measured during the tests as described in reference 2 and were verified by independent calculations. The accuracy of the measurements is believed to be within 0.1° .

For the one-blade propeller tests no torsional deflection measurements were made and values for the angle-of-blade twist for the one-blade tests were estimated by extrapolation of the two-blade data to lower values of advance ratio. The extrapolation was determined by computing the twist for the higher values of normal-force and moment coefficients obtained at the lower values of advance ratio with the one-blade propeller. A knowledge of the blade loading needed for calculating $\Delta\beta$ was obtained from wake-survey measurements made during the one-blade tests, and the moment coefficient was determined by extrapolation of the curve of moment coefficient against normal-force coefficient from the two-blade propeller tests. Some accuracy in the estimation of the value of the deflection angle was lost by the extrapolation process, but the values presented are believed to be within 0.2° . In certain cases

for which the values of the blade deflection angle were determined by extrapolations which were considered too great, or doubtful, the value of the angle has been omitted from the tables. Extrapolated values have been identified in the tables.

Values of the induced angles and the blade torsional deflection angles are presented for each test point in tables 2 to 10.

Tunnel-wall interference.- The data presented herein have been corrected to equivalent free air by the application of the Glauert tunnel-wall interference correction (reference 7).

RESULTS AND DISCUSSION

Pressure distribution.- The values of pressure coefficient obtained on the surface of the propeller sections are presented in tabular form in tables 2 to 10, and three typical pressure plots are shown in figure 4. The curves shown in figure 4 are plotted from the data presented in tables 8(a), 8(d), and 8(h). The three curves in figure 4 are plotted for a value of angle of attack close to 0° and are typical of the pressure distribution obtained in the subsonic and transonic speed ranges.

The symbols on the curves of figure 4 represent the chordwise points at which pressure orifices were located on the upper and lower surfaces of the blade section. The value of stagnation pressure on the leading edge of the section, which is recorded on the plots and appears in the data tables, was determined by computation from the equation

$$P = 1.0 + \frac{1}{4}M_x^2 + \frac{1}{4}\left(\frac{2 - \gamma}{6}\right)M_x^4$$

The value of the pressure coefficient at the trailing edge of the sections was determined from plots such as those in figure 4 by fairing the pressure-distribution curves of the upper and lower surface to a common value at the trailing edge. The notation "faired value" which appears in the data tables occurs wherever a pressure reading was either not obtained or was considered faulty.

The high negative pressure peaks near the nose on the lower surface of the section, shown in figure 4, were caused by a reverse curvature of the airfoil section. The reverse curvature of the section surface occurred because of the relatively high camber and low thickness ratio of the section at the $\frac{r}{R} = 0.90$ radius station.

Aerodynamic coefficients.- Values of normal-force coefficient, moment coefficient, and chordwise-force coefficient obtained by integration of the pressure-distribution plots are presented for each test run in tables 2 to 10. A detailed description of the method used to obtain values of chordwise-force coefficient is presented in reference 2.

A typical plot of the aerodynamic coefficients obtained is shown in figure 5 with propeller advance ratio as a common parameter. The propeller advance ratio provides a convenient parameter against which to plot the aerodynamic coefficients since both the angle of attack and section Mach number varied simultaneously during a test run. From plots such as the one illustrated in figure 5, cross plots can be made to obtain the variation of the aerodynamic coefficients with angle of attack or Mach number. The data plotted in figure 5 were obtained from table 8(d).

Induced angle.- The values of the section induced angle of attack presented herein have been computed by Goldstein's vortex theory as applied by Lock in reference 6. Goldstein's theory assumes that the blades operate with the Betz loading for minimum induced energy loss. The present blades were designed for the purpose of supplying section data on a given family of airfoil sections, and the loading was not considered in the design. As a consequence the test blades never operate with the ideal loading assumed in the theory used for calculating the induced angle of attack. The values of induced angle presented in the tables are therefore admittedly not precise, particularly for stations near the tip but are of sufficient interest to have warranted their calculation. Work is progressing on the problem of obtaining values of induced angle of attack for this propeller when operating with the arbitrary loadings obtained during the tests. An analysis of the problem of the calculation of the induced flow for propellers with arbitrary loading is beyond the scope of this paper, but some of the work that has been done on this problem has been reported in references 8, 9, and 10.

The relative magnitude of the induced angle of attack and the effect of its application on the lift-curve slope is shown for one section in figure 6. Figure 6 is a plot of normal-force coefficient against the uncorrected angle of attack $(\beta_x + \Delta\beta - \phi_0)$ compared with a plot of normal-force coefficient against angle of attack corrected for the induced angle $(\beta_x + \Delta\beta - \phi)$. Also shown in figure 6 is a plot of lift coefficient against angle of attack as determined from wind-tunnel tests on a two-dimensional model (reference 11). The application of the induced angle to the geometric angle of attack brought the lift curve for the propeller data much closer to that for the tunnel data. The lack of agreement between the propeller data and the wind-tunnel model data is due, in part, to the inexact value of induced angle used for correcting the angle of attack and may also be due to the fact that,

even though the correct value of induced angle were known, the boundary-layer flow on the blade due to centrifugal force and the presence of a Mach number gradient along the blade radius would affect the data obtained on the propeller blade so that it would not be in complete agreement with data from two-dimensional model tests.

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TABLE INDEX

Table 1.- Ordinates for the Blade Section at the 0.975 Radius of the NACA 10-(5)(066)-03 Propeller

Table 2.- Pressure Coefficients and Aerodynamic Characteristics of an NACA 16-516.25 Propeller Blade Section ($x = 0.30$; $\beta_x = 68.78^\circ$; $\beta_{0.75R} = 45^\circ$; $B = 2$)

- (a) $N = 1140$ rpm
- (b) $N = 1350$ rpm
- (c) $N = 1500$ rpm
- (d) $N = 1600$ rpm
- (e) $M = 0.56$
- (f) $M = 0.58$
- (g) $M = 0.60$
- (h) $M = 0.65$

Table 3.- Pressure Coefficients and Aerodynamic Characteristics of an NACA 16-510.00 Propeller Blade Section ($x = 0.45$; $\beta_x = 59.25^\circ$; $\beta_{0.75R} = 45^\circ$; $B = 2$)

- (a) $N = 1140$ rpm
- (b) $N = 1350$ rpm
- (c) $N = 1500$ rpm
- (d) $N = 1600$ rpm
- (e) $M = 0.56$
- (f) $M = 0.58$
- (g) $M = 0.60$
- (h) $M = 0.65$

Table 4.- Pressure Coefficients and Aerodynamic Characteristics of an NACA 16-507.50 Propeller Blade Section ($x = 0.60$; $\beta_x = 51.33^\circ$; $\beta_{0.75R} = 45^\circ$; $B = 2$)

- (a) $N = 1140$ rpm
- (b) $N = 1350$ rpm
- (c) $N = 1500$ rpm
- (d) $N = 1600$ rpm
- (e) $M = 0.56$
- (f) $M = 0.58$
- (g) $M = 0.60$
- (h) $M = 0.65$

Table 5.- Pressure Coefficients and Aerodynamic Characteristics of an
NACA 16-506.62 Propeller Blade Section ($x = 0.70$; $\beta_x = 47.00^\circ$;
 $\beta_{0.75R} = 45^\circ$; $B = 2$)

- (a) $N = 1140$ rpm
- (b) $N = 1350$ rpm
- (c) $N = 1500$ rpm
- (d) $N = 1600$ rpm
- (e) $M = 0.56$
- (f) $M = 0.58$
- (g) $M = 0.60$
- (h) $M = 0.65$

Table 6.- Pressure Coefficients and Aerodynamic Characteristics of an
NACA 16-505.85 Propeller Blade Section ($x = 0.78$; $\beta_x = 43.90^\circ$;
 $\beta_{0.75R} = 45^\circ$; $B = 2$)

- (a) $N = 1140$ rpm
- (b) $N = 1350$ rpm
- (c) $N = 1500$ rpm
- (d) $N = 1600$ rpm
- (e) $M = 0.56$
- (f) $M = 0.58$
- (g) $M = 0.60$
- (h) $M = 0.65$

Table 7.- Pressure Coefficients and Aerodynamic Characteristics of an
NACA 16-505.30 Propeller Blade Section ($x = 0.85$; $\beta_x = 41.10^\circ$;
 $\beta_{0.75R} = 45^\circ$; $B = 2$)

- (a) $N = 1140$ rpm
- (b) $N = 1350$ rpm
- (c) $N = 1500$ rpm
- (d) $N = 1600$ rpm
- (e) $M = 0.56$
- (f) $M = 0.58$
- (g) $M = 0.60$
- (h) $M = 0.65$

Table 8.- Pressure Coefficients and Aerodynamic Characteristics of an
 NACA 16-504.80 Propeller Blade Section ($x = 0.90$; $\beta_x = 39.50^\circ$;
 $\beta_{0.75R} = 45^\circ$; $B = 2$)

- (a) $N = 1140$ rpm
- (b) $N = 1350$ rpm
- (c) $N = 1500$ rpm
- (d) $N = 1600$ rpm
- (e) $M = 0.56$
- (f) $M = 0.58$
- (g) $M = 0.60$
- (h) $M = 0.65$

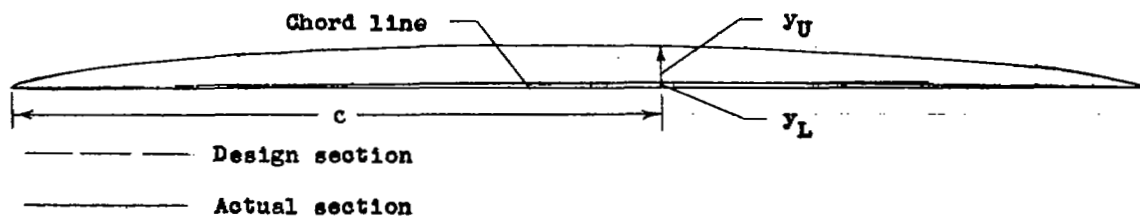
Table 9.- Pressure Coefficients and Aerodynamic Characteristics of an
 NACA 16-504.40 Propeller Blade Section ($x = 0.95$; $\beta_x = 38.35^\circ$;
 $\beta_{0.75R} = 45^\circ$)

- (a) $N = 1140$ rpm; $B = 2$
- (b) $N = 1350$ rpm; $B = 2$
- (c) $N = 1500$ rpm; $B = 2$
- (d) $N = 1600$ rpm; $B = 2$
- (e) $M = 0.56$; $B = 2$
- (f) $M = 0.58$; $B = 2$
- (g) $M = 0.60$; $B = 2$
- (h) $M = 0.65$; $B = 2$
- (i) $N = 1500$ rpm; $B = 1$
- (j) $M = 0.56$; $B = 1$
- (k) $M = 0.58$; $B = 1$
- (l) $M = 0.60$; $B = 1$
- (m) $M = 0.65$; $B = 1$

Table 10.- Pressure Coefficients and Aerodynamic Characteristics of the
 Blade Section ($x = 0.975$; $\beta_x = 37.90^\circ$; $\beta_{0.75R} = 45^\circ$; $B = 2$)

- (a) $N = 1140$ rpm
- (b) $N = 1350$ rpm
- (c) $N = 1500$ rpm
- (d) $N = 1600$ rpm
- (e) $M = 0.56$
- (f) $M = 0.58$
- (g) $M = 0.60$
- (h) $M = 0.65$

TABLE 1.- ORDINATES FOR THE BLADE SECTION AT THE 0.975 RADIUS OF
THE NACA 10-(5)(066)-03 PROPELLER



c (in.)	y_U (in.)	y_L (in.)
0	0	0
.048	.028	.006
.10	.040	.008
.20	.062	.009
.40	.102	.010
.60	.134	.006
.80	.161	.004
1.20	.203	.006
1.60	.235	.008
2.00	.263	-.005
2.40	.283	-.022
3.20	.305	-.028
4.00	.312	-.032
4.80	.296	-.028
5.60	.267	-.023
6.40	.212	-.020
7.20	.158	-.015
7.60	.097	-.008
8.00	0	0

TABLE 2.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN
 NACA 16-516.25 PROPELLER BLADE SECTION ($\alpha = 0.30$; $\beta_x = 68.78^\circ$;
 $\beta_{0.75R} = 45^\circ$; $B = 2$)

(a) $N = 1140$ rpm.

J M g ft ² c p c	1.661	1.811	1.949	2.095	2.236	2.432	2.614	2.715	2.658	2.554	2.361	2.176	2.035	1.887	1.752	
	.336	.361	.383	.403	.427	.459	.489	.508	.497	.477	.445	.416	.393	.369	.351	
$\beta_{0.75R}$	8.27	6.19	4.51	2.92	1.55	-.12	-1.47	-2.16	-1.78	-1.04	.46	2.12	3.55	5.24	6.98	
$c_{p, \text{total}}$	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
$c_{p, \text{upper}}$	1.75	1.36	1.06	.78	.50	.18	-.05	-.16	-.10	.06	.30	.63	.89	1.19	1.51	
$c_{p, \text{lower}}$.7174	.5677	.4503	.3368	.2165	.0794	-.0242	-.0723	-.0439	.0258	.1303	.2710	.3813	.5039	.6245	
$c_{p, \text{total}}$	-.0051	-.0090	-.0131	-.0170	-.0186	-.0217	-.0313	-.0338	-.0313	-.0272	-.0198	-.0172	-.0174	-.0107	-.0087	
c/b	Pressure coefficient, P															
Upper surface	$\beta_{0.000}$	1.029	1.033	1.037	1.042	1.047	1.054	1.061	1.066	1.063	1.058	1.051	1.044	1.040	1.035	1.031
	.025	-1.373	-.833	-.461	-.151	.103	.365	.549	.630	.587	.493	.292	-.002	-.257	-.611	-1.030
	.050	-1.521	-1.163	-.871	-.614	-.385	-.127	.063	.099	.099	-.002	-.212	-.490	-.720	-1.004	-1.297
	.100	-1.266	-1.042	-.840	-.667	-.499	-.306	-.162	-.098	-.136	-.206	-.368	-.572	-.741	-.934	-1.127
	.200	-1.123	-.992	-.871	-.787	-.682	-.518	-.417	-.373	-.398	-.445	-.563	-.699	-.809	-.934	-1.044
	.300	-.927	-.846	-.762	-.701	-.620	-.529	-.457	-.432	-.449	-.477	-.557	-.650	-.727	-.802	-.882
	.400	-.853	-.808	-.754	-.715	-.652	-.591	-.542	-.527	-.537	-.547	-.607	-.673	-.727	-.777	-.827
	.500	-.721	-.703	-.668	-.649	-.605	-.566	-.537	-.532	-.537	-.535	-.575	-.619	-.657	-.686	-.716
	.600	-.602	-.620	-.610	-.610	-.582	-.553	-.532	-.555	-.557	-.545	-.563	-.589	-.608	-.616	-.620
	.700	-.416	-.460	-.465	-.475	-.459	-.457	-.460	-.470	-.466	-.445	-.451	-.458	-.468	-.466	-.448
	.800	-.185	-.209	-.215	-.208	-.195	-.206	-.230	-.250	-.240	-.208	-.197	-.199	-.204	-.219	-.200
.900	-.093	-.009	.039	.051	.084	.110	.126	.123	.122	.129	.109	.072	.048	.017	-.042	
.950	-.077	0	.057	.054	.084	.119	.136	.136	.136	.139	.113	.072	.055	.037	-.024	
Lower surface	.0375	.653	.443	.261	.034	-.179	-.493	-.792	-.961	-.867	-.652	-.374	-.072	.059	.348	.530
	.075	.447	.277	.139	-.029	-.170	-.373	-.557	-.672	-.611	-.469	-.298	-.095	.044	.204	.346
	.150	.271	.139	.042	-.079	-.172	-.309	-.428	-.498	-.459	-.367	-.257	-.122	-.023	.087	.193
	.250	.158	.057	-.020	-.114	-.185	-.281	-.360	-.418	-.387	-.315	-.245	-.148	-.075	.014	.096
	.350	.074	-.013	-.075	-.149	-.201	-.273	-.337	-.380	-.361	-.299	-.247	-.169	-.116	-.049	.022
	.450	-.014	-.091	-.145	-.212	-.272	-.309	-.377	-.389	-.373	-.325	-.286	-.225	-.182	-.127	-.056
	.550	-.077	-.139	-.176	-.225	-.258	-.298	-.333	-.359	-.349	-.307	-.283	-.235	-.204	-.165	-.117
	.650	-.141	-.178	-.193	-.236	-.256	-.281	-.302	-.323	-.314	-.284	-.271	-.238	-.216	-.190	-.172
	.750	-.181	-.209	-.215	-.236	-.246	-.256	-.257	-.269	-.265	-.245	-.251	-.235	-.224	-.215	-.190
	.850	-.181	-.191	-.173	-.180	-.170	-.166	-.152	-.152	-.153	-.146	-.168	-.171	-.171	-.181	-.177
	.925	-.137	-.130	-.091	-.082	-.064	-.050	-.027	-.023	-.025	-.025	-.053	-.068	-.082	-.111	-.126
.975	-.112	-.087	-.020	-.088	.014	.035	.065	.073	.067	.063	.029	.005	-.009	-.049	-.088	
$\beta_{1.000}$	-.106	-.066	.024	.036	.056	.099	.114	.128	.118	.110	.072	.043	.036	-.012	-.063	

^aNo orifice.



TABLE 2.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN

NACA 16-516.25 PROPELLER BLADE SECTION ($x = 0.30$; $\beta_x = 68.78^\circ$; $\beta_{0.75R} = 45^\circ$; $B = 2$) - Continued(b) $N = 1350$ rpm.

J	1.801	1.925	2.061	2.188	2.372	2.522	2.657	2.576	2.431	2.271	2.125	1.986	1.852	
	M_x	.416	.439	.465	.490	.527	.556	.583	.568	.535	.503	.476	.449	.425
$\Delta \beta_x$	6.32	4.79	3.27	2.00	.37	-.81	-1.77	-1.20	-.11	1.24	2.62	4.09	5.67	
α_1	.02	.02	.01	.01	0	0	-.01	-.01	0	0	.01	.01	.02	
c_{l1}	1.42	1.13	.86	.57	.26	0	-.16	-.05	.14	.42	.72	1.02	1.29	
c_{m1}	.5935	.4768	.3690	.2477	.1155	-.0013	-.0723	-.0245	.0632	.1806	.3116	.4348	.5445	
c_c	-.0033	-.0093	-.0151	-.0172	-.0179	-.0213	-.0262	-.0275	-.0203	-.0172	-.0151	-.0134	-.0046	
c/b	Pressure coefficient, P													
Upper surface	θ_0	.000	.025	.050	.100	.200	.300	.400	.500	.600	.700	.800	.900	.950
	1.044	1.049	1.055	1.062	1.071	1.079	1.087	1.083	1.073	1.065	1.058	1.052	1.046	
	-1.057	-.621	-.262	.008	.291	.485	.605	.539	.382	.148	-.133	-.443	-.876	
	-1.227	-.942	-.674	-.445	-.191	.002	.136	.064	-.103	-.323	-.567	-.812	-1.107	
	-1.090	-.902	-.712	-.550	-.360	-.214	-.108	-.168	-.299	-.461	-.641	-.809	-1.017	
	-1.030	-.920	-.803	-.696	-.566	-.469	-.392	-.337	-.529	-.641	-.760	-.864	-.991	
	-.867	-.799	-.720	-.651	-.559	-.500	-.445	-.474	-.542	-.617	-.694	-.757	-.844	
	-.820	-.781	-.729	-.681	-.615	-.579	-.545	-.564	-.609	-.660	-.715	-.751	-.808	
	-.703	-.687	-.654	-.625	-.579	-.565	-.545	-.556	-.583	-.612	-.649	-.664	-.706	
	-.613	-.624	-.605	-.590	-.566	-.567	-.564	-.566	-.576	-.595	-.607	-.606	-.622	
	-.420	-.442	-.443	-.437	-.423	-.434	-.439	-.435	-.440	-.440	-.449	-.437	-.439	
	-.180	-.200	-.191	-.183	-.177	-.180	-.191	-.182	-.185	-.187	-.199	-.193	-.195	
	-.033	.021	.050	.070	.100	.114	.123	.082	.103	.078	.052	.042	-.012	
-.020	.039	.061	.073	.106	.122	.130	.088	.109	.081	.057	.059	.001		
Lower surface	θ_1	.0375	.075	.150	.250	.350	.450	.550	.650	.750	.850	.925	.975	1.000
	.483	.310	.170	.073	0	-.090	-.137	-.170	-.210	-.210	-.197	-.137	-.097	-.050
	.300	.167	.064	-.006	-.067	-.145	-.176	-.207	-.224	-.224	-.191	-.109	-.042	.011
	.105	.029	-.032	-.078	-.120	-.188	-.207	-.229	-.244	-.227	-.174	-.078	-.002	.051
	-.108	-.121	-.138	-.158	-.183	-.239	-.249	-.280	-.244	-.260	-.178	-.070	.010	.053
	-.394	-.307	-.262	-.249	-.253	-.293	-.339	-.316	-.278	-.280	-.173	-.057	.033	.087
	-.685	-.500	-.394	-.341	-.328	-.357	-.394	-.331	-.282	-.280	-.172	-.043	.051	.108
	-.925	-.653	-.479	-.411	-.380	-.357	-.394	-.333	-.282	-.280	-.168	-.037	.068	.120
	-.786	-.564	-.429	-.369	-.353	-.373	-.365	-.323	-.278	-.278	-.185	-.059	.060	.083
	-.548	-.408	-.334	-.302	-.299	-.334	-.351	-.308	-.278	-.263	-.187	-.072	.009	.085
	-.258	-.227	-.211	-.215	-.230	-.278	-.282	-.308	-.278	-.263	-.187	-.083	.009	.062
	-.006	-.054	-.093	-.130	-.162	-.225	-.238	-.246	-.246	-.249	-.188	-.083	-.004	.040
	.222	.109	.024	-.031	-.086	-.159	-.185	-.202	-.220	-.220	-.176	-.086	-.016	.050
.403	.242	.117	.033	-.034	-.124	-.163	-.191	-.220	-.220	-.201	-.130	-.079	-.030	

No orifice.

NACA

TABLE 2.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN
 NACA 16-516.25 PROPELLER BLADE SECTION ($\alpha = 0.30$; $\beta_x = 68.78^\circ$;
 $\beta_{0.75R} = 45^\circ$; $B = 2$) - Continued

(c) $N = 1500$ rpa.

	J	1.962	2.048	2.132	2.238	2.322	2.412	2.501	2.599	2.743	2.867	2.961	2.283	2.185	2.114	2.139	
	M_x	.495	.514	.531	.555	.575	.595	.614	.639	.623	.605	.581	.564	.543	.529	.507	
	$\Delta \delta$	4.34	3.40	2.75	1.52	.78	.03	-.66	-1.38	-.98	-.40	.45	1.12	2.02	2.72	3.76	
	α_1	1.09	.93	.75	.50	.34	.17	.02	-.14	-.05	.08	.26	.42	.62	.78	1.00	
	c_{n1}	.4645	.3974	.3226	.2181	.1497	.0761	-.0068	-.0613	-.0226	.0361	.1135	.1819	.2690	.3355	.4258	
	c_{n2}	-.0044	-.0085	-.0102	-.0133	-.0142	-.0149	-.0151	-.0221	-.0203	-.0161	-.0151	-.0138	-.0123	-.0113	-.0077	
	c_o																
	c/b	Pressure coefficient, P															
Upper surface	α 0.000	1.064	1.068	1.072	1.079	1.085	1.091	1.097	1.107	1.100	1.094	1.087	1.082	1.075	1.072	1.066	
	.025	-.502	-.282	-.097	.107	.257	.387	.498	.598	.545	.453	.321	.188	.012	-.146	-.377	
	.050	-.889	-.715	-.555	-.372	-.239	-.113	.006	.117	.059	-.040	-.177	-.296	-.456	-.596	-.788	
	.100	-.879	-.762	-.645	-.511	-.411	-.315	-.221	-.132	-.180	-.258	-.367	-.454	-.572	-.672	-.807	
	.200	-.923	-.854	-.780	-.692	-.631	-.562	-.494	-.432	-.466	-.519	-.601	-.653	-.735	-.796	-.875	
	.300	-.803	-.762	-.712	-.656	-.616	-.569	-.523	-.483	-.506	-.539	-.601	-.629	-.682	-.723	-.771	
	.400	-.788	-.764	-.732	-.694	-.672	-.641	-.611	-.591	-.740	-.619	-.664	-.675	-.714	-.738	-.767	
	.500	-.692	-.681	-.660	-.635	-.628	-.608	-.591	-.586	-.589	-.594	-.626	-.627	-.648	-.663	-.677	
	.600	-.618	-.620	-.610	-.601	-.601	-.591	-.584	-.591	-.589	-.584	-.603	-.595	-.606	-.610	-.613	
	.700	-.438	-.447	-.442	-.437	-.440	-.433	-.431	-.440	-.435	-.428	-.443	-.434	-.443	-.441	-.438	
	.800	-.187	-.187	-.175	-.168	-.161	-.144	-.132	-.135	-.134	-.135	-.158	-.159	-.174	-.175	-.183	
.900	-.017	.030	.048	.066	.077	.093	.107	.112	.112	.107	.103	.081	.075	.042	.027		
.950	.032	.046	.056	.073	.082	.099	.112	.115	.114	.108	.085	.082	.065	.053	.046		
Lower surface	α 0.000	-.0375	.258	.123	-.009	-.201	-.355	-.507	-.682	-.905	-.790	-.605	-.443	-.274	-.113	.027	.186
	.075	.135	.035	-.055	-.182	-.293	-.393	-.504	-.649	-.576	-.455	-.350	-.233	-.126	-.031	.082	
	.150	.039	-.030	-.094	-.182	-.258	-.326	-.398	-.482	-.441	-.366	-.301	-.217	-.145	-.075	.006	
	.250	-.025	-.079	-.127	-.191	-.248	-.297	-.347	-.415	-.381	-.323	-.282	-.217	-.166	-.113	-.051	
	.350	-.081	-.125	-.162	-.215	-.260	-.297	-.336	-.391	-.365	-.319	-.287	-.233	-.193	-.153	-.100	
	.450	-.158	-.197	-.225	-.270	-.308	-.335	-.368	-.407	-.389	-.351	-.329	-.284	-.253	-.217	-.176	
	.550	-.190	-.218	-.243	-.276	-.308	-.330	-.352	-.384	-.370	-.342	-.327	-.288	-.265	-.235	-.202	
	.650	-.212	-.234	-.249	-.276	-.301	-.315	-.331	-.354	-.346	-.323	-.318	-.284	-.267	-.242	-.218	
	.750	-.236	-.245	-.254	-.270	-.285	-.290	-.293	-.303	-.302	-.290	-.295	-.272	-.267	-.250	-.235	
	.850	-.199	-.194	-.193	-.197	-.198	-.194	-.185	-.182	-.186	-.187	-.204	-.204	-.195	-.198	-.192	
	.925	-.116	-.102	-.090	-.084	-.080	-.069	-.056	-.050	-.058	-.058	-.082	-.082	-.079	-.090	-.103	
.975	-.052	-.023	-.007	.001	.009	.023	.040	.054	.054	.046	.035	.011	.010	-.005	-.032		
α 1.000	.040	.035	.049	.071	.070	.087	.098	.102	.102	.115	.096	.079	.068	.035	.026	.001	

^aNo orifices.



TABLE 2.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN

NACA 16-516.25 PROPELLER BLADE SECTION ($x = c.30$; $B_x = 68.78^\circ$; $\beta_{0.75R} = 45^\circ$; $B = 2$) - Continued(a) $N = 1600$ rpm.

J	2.134	2.224	2.303	2.395	2.474	2.554	2.611	2.585	2.510	2.436	2.350	2.253	2.182	
$M_{x,1}$.553	.574	.591	.613	.632	.651	.664	.658	.639	.621	.601	.578	.562	
$\Delta\beta$	2.53	1.67	.96	.18	-.45	-1.05	-1.45	-1.27	-.72	-.15	.35	1.40	2.06	
$\alpha_{x,1}$.01	.01	.01	.01	0	0	0	0	0	0	.01	.01	.01	
$\alpha_{x,2}$.86	.68	.50	.32	.17	.01	-.10	-.05	.09	.25	.44	.61	.78	
$\alpha_{x,3}$.3710	.2948	.2206	.1416	.0742	.0058	-.0445	-.0206	.0381	.1097	.1935	.2639	.3374	
α_c	-.0077	-.0084	-.0087	-.0102	-.0108	-.0129	-.0154	-.0144	-.0126	-.0113	-.0107	-.0100	-.0090	
a/b	Pressure coefficient, P													
Upper surface	^a 0.000	1.078	1.084	1.090	1.097	1.103	1.110	1.115	1.113	1.106	1.100	1.093	1.086	1.081
	.025	-.203	-.005	-.143	.285	.407	.513	.577	.546	.461	.347	.205	-.039	-.123
	.050	-.681	-.512	-.370	-.226	-.107	.006	.079	.048	-.048	-.162	-.300	-.454	-.598
	.100	-.753	-.627	-.524	-.416	-.319	-.229	-.170	-.197	-.274	-.362	-.469	-.585	-.691
	.200	-.871	-.788	-.727	-.652	-.588	-.525	-.482	-.499	-.557	-.616	-.686	-.766	-.827
	.300	-.778	-.720	-.684	-.636	-.595	-.557	-.531	-.539	-.576	-.611	-.655	-.710	-.747
	.400	-.782	-.744	-.727	-.696	-.672	-.655	-.644	-.644	-.665	-.678	-.706	-.741	-.761
	.500	-.696	-.670	-.665	-.646	-.635	-.633	-.633	-.628	-.635	-.635	-.650	-.671	-.679
	.600	-.628	-.613	-.621	-.611	-.610	-.617	-.627	-.617	-.614	-.604	-.606	-.622	-.619
	.700	-.442	-.437	-.442	-.435	-.433	-.441	-.448	-.440	-.436	-.429	-.432	-.445	-.436
	.800	-.173	-.157	-.153	-.129	-.113	-.104	-.098	-.097	-.105	-.117	-.135	-.162	-.161
.900	.027	.043	.052	.068	.084	.090	.094	.096	.089	.081	.063	.049	.042	
.950	.042	.057	.059	.072	.085	.093	.097	.099	.093	.085	.070	.059	.056	
Lower surface	.0375	.081	-.062	-.214	-.365	-.523	-.712	-.862	-.782	-.612	-.428	-.265	-.122	.032
	.075	.007	-.087	-.201	-.303	-.408	-.536	-.630	-.579	-.468	-.344	-.234	-.132	-.026
	.150	-.053	-.118	-.199	-.270	-.341	-.423	-.479	-.450	-.382	-.293	-.220	-.153	-.075
	.250	-.096	-.145	-.207	-.257	-.307	-.368	-.413	-.388	-.335	-.274	-.220	-.170	-.113
	.350	-.144	-.180	-.233	-.271	-.312	-.363	-.401	-.382	-.337	-.281	-.238	-.201	-.153
	.450	-.214	-.244	-.290	-.321	-.354	-.396	-.423	-.407	-.375	-.328	-.293	-.262	-.221
	.550	-.236	-.262	-.298	-.321	-.347	-.381	-.402	-.389	-.363	-.326	-.300	-.276	-.241
	.650	-.251	-.266	-.299	-.314	-.336	-.360	-.377	-.367	-.349	-.317	-.298	-.280	-.251
	.750	-.265	-.272	-.294	-.300	-.309	-.321	-.327	-.323	-.315	-.296	-.287	-.280	-.259
	.850	-.214	-.207	-.216	-.213	-.209	-.210	-.206	-.207	-.211	-.202	-.207	-.211	-.201
	.925	-.117	-.103	-.103	-.090	-.080	-.075	-.067	-.068	-.077	-.079	-.089	-.101	-.101
.975	-.041	-.019	-.013	-.001	.013	.024	.032	.031	.018	.012	0	-.015	-.020	
^b 1.000	0	.030	.033	.073	.065	.075	.085	.081	.071	.060	.047	.050	.038	

^aNo orifice.

TABLE 2.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN

NACA 16-516.25 PROPELLER BLADE SECTION ($x = 0.30$; $\beta_x = 68.78^\circ$;

$\beta_{0.75R} = 45^\circ$; $B = 2$) - Continued

(e) $M = 0.56$.

	J	M_x	C_{Df}	ΔP	C_{L1}	C_{L2}	C_{D1}	C_{D2}	C_{D3}	C_{D4}	C_{D5}	C_{D6}	C_{D7}
	2.111	2.138	2.180	2.218	2.259	2.314	2.358	2.393	2.442	2.485	2.540	2.622	
	.623	.620	.614	.617	.612	.615	.614	.610	.609	.604	.606	.604	
	2.74	2.49	2.08	1.77	1.35	.86	.49	.20	-.20	-.53	-.94	-1.53	
	.04	.03	.02	.02	.02	.02	.02	.01	0	0	0	-.01	
	.70	.64	.57	.49	.43	.32	.22	.16	.08	.02	-.08	-.17	
	.3032	.2774	.2452	.2116	.1858	.1381	.0974	.0684	.0348	.0065	-.0361	-.0774	
	-.0070	-.0082	-.0084	-.0090	-.0111	-.0133	-.0147	-.0164	-.0175	-.0203	-.0249	-.0272	
c/b	Pressure coefficient, P												
Upper surface	0.000	1.100	1.099	1.097	1.098	1.096	1.098	1.097	1.096	1.095	1.094	1.095	1.094
	.025	.033	.073	.124	.187	.235	.307	.367	.409	.457	.499	.560	.614
	.050	-.510	-.469	-.414	-.350	-.300	-.224	-.160	-.111	-.055	-.009	.061	.127
	.100	-.648	-.614	-.567	-.516	-.472	-.411	-.355	-.317	-.272	-.231	-.178	-.122
	.200	-.828	-.800	-.768	-.731	-.695	-.649	-.604	-.572	-.536	-.502	-.461	-.412
	.300	-.754	-.738	-.714	-.690	-.665	-.635	-.600	-.579	-.552	-.529	-.500	-.466
	.400	-.771	-.760	-.745	-.732	-.711	-.691	-.665	-.652	-.630	-.613	-.594	-.565
	.500	-.679	-.677	-.669	-.666	-.651	-.642	-.623	-.616	-.603	-.593	-.585	-.565
	.600	-.606	-.612	-.607	-.610	-.604	-.602	-.593	-.593	-.589	-.584	-.586	-.578
	.700	-.410	-.420	-.421	-.431	-.428	-.432	-.428	-.436	-.438	-.437	-.448	-.448
	.800	-.116	-.125	-.122	-.127	-.125	-.125	-.123	-.132	-.139	-.145	-.163	-.179
.900	.040	.042	.049	.051	.061	.069	.082	.088	.096	.103	.106	.115	
.950	.049	.052	.061	.063	.070	.062	.088	.093	.101	.108	.113	.122	
Lower surface	.0375	-.022	-.075	-.126	-.207	-.256	-.352	-.426	-.503	-.587	-.661	-.802	-.924
	.075	-.065	-.102	-.138	-.195	-.228	-.294	-.340	-.393	-.447	-.493	-.583	-.656
	.150	-.102	-.130	-.155	-.199	-.218	-.265	-.293	-.329	-.361	-.392	-.447	-.490
	.250	-.137	-.153	-.169	-.204	-.218	-.252	-.272	-.295	-.320	-.342	-.384	-.414
	.350	-.168	-.186	-.201	-.228	-.237	-.265	-.277	-.297	-.317	-.331	-.368	-.385
	.450	-.240	-.253	-.264	-.286	-.293	-.315	-.325	-.338	-.352	-.364	-.391	-.403
	.550	-.256	-.269	-.278	-.296	-.300	-.317	-.321	-.333	-.343	-.349	-.369	-.376
	.650	-.268	-.279	-.285	-.300	-.300	-.312	-.312	-.320	-.324	-.328	-.343	-.345
	.750	-.276	-.283	-.285	-.293	-.290	-.294	-.291	-.294	-.294	-.294	-.298	-.291
	.850	-.218	-.220	-.216	-.220	-.211	-.210	-.200	-.198	-.192	-.186	-.187	-.174
	.925	-.113	-.115	-.106	-.105	-.097	-.090	-.077	-.074	-.066	-.057	-.052	-.039
.975	-.037	-.033	-.023	-.019	-.007	-.001	-.014	-.018	-.028	-.036	-.047	-.059	
1.000	.005	.012	.025	.027	.047	.035	.056	.067	.072	.081	.093	.106	

^aNo orifice.



TABLE 2.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN

NACA 16-516.25 PROPELLER BLADE SECTION ($\alpha = 0.30$; $\beta_x = 68.78^\circ$;

$\beta_{0.75R} = 45^\circ$; $B = 2$) - Continued

(r) $H = 0.58$.

	2.106	2.140	2.172	2.212	2.253	2.288	2.327	2.371	2.416	2.462	2.525	2.566	2.598	
J	2.106	2.140	2.172	2.212	2.253	2.288	2.327	2.371	2.416	2.462	2.525	2.566	2.598	
M_x	.646	.643	.639	.639	.638	.635	.633	.632	.630	.629	.631	.625	.621	
$\frac{\Delta B}{B}$	2.81	2.47	2.16	1.78	1.40	1.09	.75	.38	.01	-.35	-.83	-1.13	-1.36	
$\frac{\Delta \beta}{\beta}$.05	.05	.04	.04	.03	.03	.03	.02	.02	.01	.01	0	0	
$\frac{\Delta \beta}{\beta}$.70	.63	.56	.47	.39	.35	.28	.21	.13	.04	-.05	-.10	-.16	
$\frac{\Delta \beta}{\beta}$.3006	.2716	.2413	.2058	.1716	.1510	.1242	.0939	.0594	.0168	-.0206	-.0439	-.0710	
$\frac{\Delta \beta}{\beta}$.0003	-.0044	-.0041	-.0066	-.0088	-.0085	-.0088	-.0097	-.0098	-.0142	-.0162	-.0177	-.0213	
c/b	Pressure coefficient, P													
Upper surface	.000	1.108	1.107	1.106	1.106	1.105	1.104	1.104	1.103	1.102	1.102	1.103	1.101	1.100
	.025	.047	.108	.169	.218	.267	.310	.358	.395	.457	.499	.559	.588	.618
	.050	-.509	-.444	-.377	-.325	-.270	-.225	-.173	-.130	-.064	-.016	.056	.092	.128
	.100	-.662	-.604	-.549	-.502	-.455	-.418	-.375	-.339	-.280	-.241	-.180	-.152	-.125
	.200	-.864	-.814	-.770	-.733	-.694	-.665	-.632	-.602	-.554	-.519	-.467	-.439	-.421
	.300	-.782	-.750	-.720	-.697	-.666	-.652	-.626	-.605	-.569	-.546	-.504	-.487	-.473
	.400	-.800	-.776	-.756	-.741	-.717	-.709	-.692	-.677	-.650	-.632	-.598	-.586	-.579
	.500	-.701	-.686	-.677	-.669	-.652	-.654	-.643	-.635	-.618	-.608	-.585	-.577	-.578
	.600	-.619	-.614	-.613	-.611	-.601	-.608	-.606	-.603	-.596	-.593	-.578	-.577	-.586
	.700	-.414	-.416	-.420	-.421	-.417	-.428	-.432	-.433	-.432	-.436	-.430	-.434	-.447
	.800	-.117	-.114	-.113	-.114	-.106	-.115	-.118	-.118	-.117	-.124	-.131	-.148	-.169
.900	.031	.043	.048	.054	.061	.062	.071	.077	.089	.094	.112	.114	.110	
.950	.039	.051	.060	.064	.073	.070	.078	.082	.092	.099	.117	.120	.116	
Lower surface	.0375	-.029	-.080	-.154	-.213	-.268	-.345	-.413	-.480	-.575	-.661	-.765	-.843	-.943
	.075	-.077	-.116	-.164	-.203	-.238	-.293	-.338	-.381	-.441	-.497	-.561	-.608	-.670
	.150	-.116	-.141	-.176	-.201	-.225	-.265	-.294	-.324	-.363	-.397	-.430	-.460	-.500
	.250	-.142	-.160	-.186	-.205	-.222	-.252	-.274	-.295	-.321	-.346	-.372	-.395	-.425
	.350	-.184	-.198	-.219	-.231	-.243	-.267	-.284	-.300	-.321	-.341	-.355	-.373	-.399
	.450	-.254	-.265	-.281	-.291	-.298	-.318	-.333	-.346	-.360	-.375	-.382	-.395	-.415
	.550	-.274	-.278	-.291	-.299	-.303	-.322	-.331	-.342	-.351	-.361	-.366	-.375	-.390
	.650	-.290	-.291	-.300	-.304	-.305	-.318	-.326	-.332	-.336	-.343	-.342	-.347	-.360
	.750	-.297	-.293	-.296	-.297	-.293	-.305	-.306	-.309	-.306	-.307	-.298	-.300	-.306
	.850	-.235	-.227	-.225	-.221	-.214	-.218	-.215	-.213	-.204	-.200	-.185	-.182	-.186
	.925	-.192	-.116	-.110	-.104	-.094	-.097	-.090	-.087	-.075	-.068	-.050	-.046	-.046
.975	-.049	-.034	-.024	-.017	-.005	-.007	.003	.008	.018	.030	.048	.052	.054	
a1.000	.072	.028	.036	.056	.058	.051	.079	.070	.080	.094	.100	.110	.105	

No orifice.



TABLE 2.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN
 NACA 16-516.25 PROPELLER BLADE SECTION ($x = 0.30$; $R_x = 68.76^\circ$;
 $\beta_{0.75R} = 45^\circ$; $B = 2$) - Continued

(g) $M = 0.50$.

	2.108	2.142	2.180	2.224	2.262	2.296	2.344	2.380	2.426	2.473	2.520	2.578	
J	2.108	2.142	2.180	2.224	2.262	2.296	2.344	2.380	2.426	2.473	2.520	2.578	
M_x	.665	.660	.658	.660	.659	.654	.655	.651	.649	.647	.646	.644	
α_{T1}	2.79	2.45	2.08	1.67	1.32	1.02	.60	.30	-.07	-.44	-.79	-1.22	
$\Delta\delta$.06	.06	.04	.03	.02	.01	0	0	0	0	0	0	
α_1	.69	.61	.53	.45	.38	.31	.22	.16	.08	.01	-.07	-.14	
c_n	.2968	.2645	.2310	.1935	.1639	.1348	.0977	.0703	.0352	.0035	-.0290	-.0639	
c_m	-.0043	-.0066	-.0059	-.0082	-.0079	-.0113	-.0121	-.0118	-.0135	-.0132	-.0167	-.0213	
c_o													
c/b	Pressure coefficient, P												
Upper surface	β_0 .000	1.116	1.114	1.113	1.114	1.113	1.111	1.111	1.110	1.109	1.108	1.108	1.107
	.025	-.035	-.108	-.156	-.220	-.278	-.314	-.366	-.406	-.449	-.498	-.536	-.592
	.050	-.501	-.428	-.372	-.301	-.237	-.197	-.140	-.096	-.047	-.007	-.053	-.117
	.100	-.668	-.601	-.550	-.489	-.435	-.400	-.352	-.315	-.271	-.227	-.187	-.198
	.200	-.905	-.840	-.790	-.739	-.694	-.662	-.625	-.591	-.556	-.521	-.485	-.437
	.300	-.822	-.776	-.738	-.704	-.673	-.651	-.630	-.606	-.579	-.554	-.531	-.492
	.400	-.847	-.810	-.779	-.756	-.732	-.718	-.705	-.685	-.666	-.651	-.631	-.600
	.500	-.734	-.714	-.694	-.682	-.668	-.662	-.659	-.646	-.635	-.628	-.617	-.597
	.600	-.643	-.634	-.626	-.621	-.617	-.617	-.624	-.617	-.613	-.614	-.612	-.600
	.700	-.427	-.424	-.422	-.422	-.423	-.427	-.435	-.435	-.437	-.442	-.447	-.447
	.800	-.135	-.127	-.116	-.106	-.102	-.105	-.106	-.102	-.104	-.109	-.114	-.128
	.900	.014	.029	.039	.049	.056	.066	.069	.078	.085	.090	.095	.105
.950	.025	.042	.051	.059	.064	.071	.072	.083	.090	.095	.100	.110	
Lower surface	.0375	-.050	-.112	-.163	-.234	-.310	-.367	-.461	-.527	-.601	-.709	-.802	-.917
	.075	-.097	-.138	-.171	-.221	-.274	-.308	-.371	-.411	-.460	-.531	-.588	-.657
	.150	-.135	-.161	-.184	-.216	-.251	-.274	-.320	-.347	-.376	-.421	-.455	-.489
	.250	-.163	-.180	-.195	-.216	-.243	-.260	-.293	-.310	-.334	-.366	-.395	-.421
	.350	-.202	-.215	-.226	-.243	-.262	-.274	-.301	-.316	-.331	-.358	-.380	-.395
	.450	-.278	-.284	-.291	-.303	-.320	-.327	-.351	-.360	-.369	-.390	-.408	-.413
	.550	-.297	-.298	-.302	-.311	-.321	-.327	-.346	-.353	-.361	-.378	-.387	-.390
	.650	-.314	-.313	-.310	-.314	-.321	-.325	-.339	-.342	-.347	-.358	-.364	-.361
	.750	-.319	-.313	-.308	-.306	-.307	-.306	-.315	-.313	-.311	-.318	-.317	-.307
	.850	-.253	-.242	-.233	-.226	-.221	-.217	-.218	-.215	-.207	-.206	-.202	-.186
	.925	-.141	-.125	-.114	-.102	-.096	-.089	-.089	-.081	-.076	-.072	-.066	-.048
	.975	-.060	-.038	-.024	-.011	-.004	-.004	-.002	-.012	.019	.025	.032	.048
β_1 1.000	-.002	.006	.030	.034	.040	.055	.050	.062	.072	.080	.091	.096	

^aNo orifice.



TABLE 2.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN

NACA 16-516.25 PROPELLER BLADE SECTION ($\alpha = 0.30$; $\beta_x = 68.76^\circ$; $\beta = 45^\circ$; $B = 2$) - Concluded
0.75R(h) $M = 0.65$.

J	2.077	2.101	2.130	2.151	2.184	2.208	2.239	2.261	2.293	2.319	2.350	2.383	2.412	2.451	
M_x	.730	.727	.725	.722	.720	.719	.717	.715	.713	.710	.709	.707	.705	.703	
$\Delta \beta_x$	3.11	2.86	2.57	2.36	2.04	1.81	1.53	1.33	1.04	.82	.55	.28	.04	-.27	
c_{d_i}	.06	.06	.05	.05	.04	.04	.03	.02	0	0	0	-.01	-.01	-.01	
c_{d_e}	.63	.61	.54	.50	.44	.38	.33	.27	.22	.18	.12	.04	.01	-.09	
$c_{d_{total}}$.2684	.2613	.2342	.2142	.1903	.1665	.1419	.1187	.0968	.0774	.0510	.0181	.0039	-.0381	
c_{m_c}	-.0029	-.0007	-.0003	-.0015	-.0002	0	-.0033	-.0046	-.0048	-.0062	-.0046	-.0085	-.0066	-.0121	
c_{m_c}	.0041	.0041	.0042	.0041	.0052	.0057	.0063	.0072	.0085	.0079	.0080	.0098	.0100	.0137	
o/b	Pressure coefficient, P														
Upper surface	b_0 .000	1.141	1.140	1.139	1.138	1.137	1.137	1.136	1.135	1.134	1.133	1.133	1.132	1.131	1.131
	.025	.196	.216	.250	.279	.313	.339	.367	.391	.427	.4390	.4265	.4460	.4365	.4580
	.050	-.385	-.361	-.320	-.290	-.251	-.225	-.188	-.159	-.116	-.092	-.049	-.014	.012	.228
	.100	-.594	-.571	-.535	-.508	-.472	-.447	-.414	-.388	-.349	-.328	-.288	-.256	-.234	-.198
	.200	-.919	-.909	-.884	-.855	-.818	-.790	-.750	-.717	-.678	-.654	-.616	-.585	-.563	-.525
	.300	-.834	-.825	-.810	-.794	-.774	-.760	-.733	-.709	-.681	-.667	-.638	-.613	-.598	-.568
	.400	-1.065	-1.034	-1.006	-.964	-.930	-.898	-.858	-.828	-.799	-.785	-.758	-.734	-.718	-.690
	.500	-.841	-.808	-.798	-.781	-.772	-.766	-.747	-.731	-.720	-.713	-.700	-.688	-.680	-.666
	.600	-.641	-.645	-.652	-.650	-.651	-.656	-.650	-.649	-.647	-.644	-.644	-.639	-.640	-.638
	.700	-.363	-.376	-.385	-.385	-.388	-.395	-.400	-.406	-.411	-.414	-.416	-.416	-.424	-.430
	.800	-.091	-.092	-.089	-.078	-.066	-.063	-.060	-.059	-.058	-.053	-.047	-.042	-.046	-.051
.900	-.015	-.003	-.007	.020	.028	.036	.043	.048	.055	.051	.060	.072	.074	.080	
.950	-.009	.002	.014	.026	.032	.040	.050	.053	.062	.057	.066	.078	.080	.084	
Lower surface	.0375	-.076	-.107	-.160	-.194	-.247	-.285	-.328	-.378	-.440	-.494	-.564	-.616	-.679	-.770
	.075	-.121	-.143	-.178	-.204	-.241	-.270	-.297	-.333	-.374	-.410	-.456	-.488	-.525	-.583
	.150	-.158	-.172	-.196	-.213	-.240	-.260	-.277	-.301	-.328	-.352	-.382	-.398	-.421	-.454
	.250	-.186	-.193	-.217	-.223	-.242	-.257	-.269	-.287	-.304	-.324	-.344	-.357	-.375	-.400
	.350	-.234	-.240	-.252	-.262	-.279	-.291	-.297	-.311	-.325	-.339	-.354	-.362	-.375	-.394
	.450	-.317	-.322	-.330	-.336	-.349	-.357	-.360	-.371	-.381	-.392	-.392	-.402	-.414	-.426
	.550	-.341	-.340	-.346	-.350	-.359	-.364	-.365	-.372	-.378	-.388	-.395	-.394	-.401	-.408
	.650	-.369	-.366	-.369	-.369	-.374	-.377	-.373	-.375	-.378	-.385	-.387	-.385	-.389	-.391
	.750	-.379	-.370	-.367	-.363	-.366	-.364	-.356	-.354	-.354	-.357	-.352	-.345	-.344	-.343
	.850	-.307	-.296	-.285	-.279	-.277	-.273	-.259	-.255	-.248	-.249	-.241	-.232	-.229	-.222
	.925	-.190	-.172	-.160	-.150	-.146	-.137	-.122	-.117	-.109	-.108	-.099	-.089	-.087	-.078
.975	-.109	-.086	-.071	-.061	-.052	-.042	-.026	-.020	-.011	-.010	-.003	.009	.010	.019	
b_1 .000	-.009	-.001	.013	.010	.027	.026	.044	.044	.044	.048	.048	.058	.055	.067	.078

^aNo orifice.^bPaired value.

TABLE 3.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN

NACA 16-510.00 PROPELLER BLADE SECTION ($x = 0.45$; $\beta_x = 59.25^\circ$;

$\beta_{0.75R} = 45^\circ$; $B = 2$)

(a) $N = 1140$ rpm.

$\frac{r}{R}$	$\frac{C_p}{\rho V^2}$	$\frac{C_{p, \text{max}}}{\rho V^2}$	$\frac{C_{p, \text{min}}}{\rho V^2}$	$\frac{C_{p, \text{max}}}{\rho V^2}$	$\frac{C_{p, \text{min}}}{\rho V^2}$	$\frac{C_{p, \text{max}}}{\rho V^2}$	$\frac{C_{p, \text{min}}}{\rho V^2}$	$\frac{C_{p, \text{max}}}{\rho V^2}$	$\frac{C_{p, \text{min}}}{\rho V^2}$	$\frac{C_{p, \text{max}}}{\rho V^2}$	$\frac{C_{p, \text{min}}}{\rho V^2}$	$\frac{C_{p, \text{max}}}{\rho V^2}$	$\frac{C_{p, \text{min}}}{\rho V^2}$	$\frac{C_{p, \text{max}}}{\rho V^2}$	$\frac{C_{p, \text{min}}}{\rho V^2}$	$\frac{C_{p, \text{max}}}{\rho V^2}$	$\frac{C_{p, \text{min}}}{\rho V^2}$
1.589	1.778	1.965	2.152	2.285	2.400	2.522	2.659	2.794	2.469	2.338	2.190	2.049	1.872	1.679	1.541		
.369	.395	.422	.450	.468	.487	.506	.527	.546	.498	.477	.454	.434	.411	.381	.364		
10.91	7.74	4.98	2.55	.99	-.25	-1.48	-2.75	-4.24	-5.95	-7.41	-8.85	-10.35	-11.87	-13.35	-14.79		
.17	.13	.10	.06	.04	.01	-.01	-.03	-.02	0	.03	.05	.08	.11	.15	.17		
2.62	2.12	1.64	1.19	.88	.62	.35	.09	.23	.47	.78	1.07	1.43	1.87	2.37	2.78		
1.0775	.8684	.6774	.5000	.3703	.2645	.1497	.0394	.0987	.2000	.3290	.4510	.5942	.7703	.9626	1.1174		
-.0311	-.0462	-.0600	-.0728	-.0767	-.0803	-.0756	-.0668	-.0513	-.0305	-.0095	-.0191	-.0369	-.0537	-.0421	-.0223		
$\frac{r}{h}$	Pressure coefficient, C_p																
Upper surface																	
0.000	1.035	1.040	1.046	1.052	1.056	1.061	1.065	1.071	1.068	1.063	1.058	1.053	1.048	1.043	1.037	1.034	
.025	-2.885	-1.912	-1.161	-.823	-.558	-.303	-.103	.339	.924	1.43	1.96	2.49	2.91	3.32	3.71	4.08	
.050	-2.176	-1.561	-1.049	-.617	-.354	-.147	.039	.205	.531	1.04	1.55	2.06	2.57	3.08	3.59	4.10	
.100	-1.592	-1.207	-.872	-.593	-.341	-.124	.006	.091	.268	.534	.799	1.064	1.329	1.594	1.859	2.124	
.200	-1.200	-.986	-.777	-.602	-.475	-.375	-.282	-.186	-.089	.014	.111	.208	.305	.402	.499	.596	
.300	-1.008	-.872	-.731	-.605	-.517	-.441	-.373	-.300	-.231	-.165	-.100	-.035	.030	.095	.160	.225	
.400	-.866	-.751	-.638	-.562	-.506	-.457	-.410	-.371	-.338	-.306	-.274	-.242	-.210	-.178	-.146	-.114	
.500	-.741	-.709	-.652	-.591	-.541	-.502	-.471	-.429	-.389	-.350	-.311	-.272	-.233	-.194	-.155	-.116	
.600	-.612	-.625	-.603	-.573	-.541	-.515	-.497	-.467	-.434	-.406	-.377	-.348	-.319	-.290	-.261	-.232	
.700	-.441	-.488	-.501	-.508	-.490	-.472	-.440	-.445	-.456	-.472	-.485	-.497	-.509	-.521	-.533	-.545	
.800	-.211	-.260	-.314	-.353	-.387	-.416	-.440	-.458	-.470	-.476	-.477	-.473	-.464	-.451	-.434	-.416	
.900	-.086	-.024	-.019	-.083	-.085	-.087	-.088	-.088	-.087	-.084	-.079	-.073	-.066	-.058	-.049	-.040	
.950	-.078	.010	.066	.099	.097	.098	.104	.107	.106	.101	.098	.093	.097	.036	-.039	-.084	
Lower surface																	
0.000	.0375	.836	.651	.411	.129	-.085	-.279	-.516	-.757	-.943	-1.107	-1.297	-1.492	-1.687	-1.882	-2.077	
.075	.682	.515	.325	.111	-.041	-.175	-.332	-.489	-.644	-.797	-.947	-1.094	-1.238	-1.379	-1.517	-1.654	
.150	.498	.367	.220	.070	-.039	-.127	-.248	-.344	-.496	-.633	-.754	-.861	-956	-1.049	-1.130	-1.200	
.250	.369	.264	.155	.032	-.049	-.125	-.205	-.275	-.341	-.401	-.454	-.501	-.542	-.578	-.609	-.636	
.350	.285	.198	.112	.017	-.041	-.092	-.135	-.180	-.218	-.250	-.276	-.297	-.313	-.325	-.333	-.338	
.450	.219	.183	.073	-.001	-.044	-.084	-.136	-.177	-.215	-.248	-.276	-.299	-.317	-.330	-.338	-.342	
.550	.144	.094	.039	-.018	-.058	-.084	-.126	-.154	-.189	-.217	-.239	-.256	-.269	-.278	-.283	-.285	
.650	.085	.050	.014	-.027	-.055	-.074	-.104	-.125	-.144	-.159	-.169	-.174	-.176	-.176	-.176	-.176	
.750	.027	.013	-.009	-.030	-.044	-.051	-.073	-.085	-.097	-.105	-.108	-.108	-.108	-.108	-.108	-.108	
.850	.006	.013	.014	.014	.010	.015	.003	-.003	.006	.012	.002	.002	.002	.002	.002	.002	
.925	-.011	.021	.050	.070	.084	.088	.088	.078	.065	.046	.021	.003	.003	.003	.003	.003	
.975	-.077	.010	.063	.123	.135	.144	.137	.138	.141	.143	.131	.127	.127	.127	.127	.127	
1.000	-.022	0	.071	.153	.160	.172	.160	.169	.176	.172	.165	.153	.105	.033	-.048	-.119	

*No orifice.



TABLE 3.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN

NACA 16-510.00 PROPELLER BLADE SECTION ($\alpha = 0.45$; $\beta_x = 59.25^\circ$; $\beta_{0.75R} = 45^\circ$; $B = 2$) - Continued(b) $N = 1350$ rpm.

	J	M_x	$\frac{dC_p}{d\beta}$	$\frac{dC_m}{d\beta}$	$\frac{dC_n}{d\beta}$	$\frac{dC_{Dp}}{d\beta}$	$\frac{dC_{Dm}}{d\beta}$	$\frac{dC_{Dn}}{d\beta}$	$\frac{dC_{Dp}}{d\beta}$	$\frac{dC_{Dm}}{d\beta}$	$\frac{dC_{Dn}}{d\beta}$	$\frac{dC_{Dp}}{d\beta}$	$\frac{dC_{Dm}}{d\beta}$	$\frac{dC_{Dn}}{d\beta}$	$\frac{dC_{Dp}}{d\beta}$	$\frac{dC_{Dm}}{d\beta}$	$\frac{dC_{Dn}}{d\beta}$	
	2.647	2.473	2.329	2.207	2.087	1.978	1.872	1.768	1.819	1.926	2.027	2.143	2.269	2.408	2.550			
	.626	.590	.565	.543	.522	.504	.487	.468	.477	.495	.513	.532	.557	.582	.609			
	-2.64	-.99	.51	1.89	3.29	4.80	6.31	7.90	7.10	5.53	4.14	2.66	1.17	-.33	-1.75			
	-.08	-.02	.03	.08	.11	.16	.20	.23	.21	.18	.14	.09	.05	0	-.04			
	.10	.43	.75	1.05	1.39	1.65	1.94	2.25	2.10	1.80	1.55	1.23	.92	.59	.26			
	.0426	.182	.3187	.4445	.5800	.6858	.7981	.9200	.8606	.7426	.6439	.5148	.3890	.2503	.1097			
	-.0751	-.0726	-.0711	-.0706	-.0657	-.0560	-.0475	-.0408	-.0444	-.0524	-.0582	-.0688	-.0688	-.0705	-.0719			
	Pressure coefficient, P																	
o/b	1.101	1.090	1.082	1.077	1.070	1.065	1.061	1.056	1.059	1.063	1.067	1.072	1.080	1.087	1.095			
Upper surface	.000	.549	.289	-.021	-.354	-.769	-1.188	-1.669	-2.065	-1.922	-1.425	-1.007	-.554	-.190	.145	.425		
	.025	.228	-.008	-.262	-.518	-.808	-1.096	-1.434	-1.734	-1.970	-2.156	-2.277	-2.333	-2.327	-2.255	-2.09		
	.100	.015	-.172	-.362	-.544	-.737	-.922	-1.105	-1.319	-1.216	-.999	-.843	-.642	-.452	-.260	-.080		
	.200	-.195	-.329	-.466	-.593	-.714	-.828	-.948	-1.062	-1.007	-.882	-.776	-.655	-.526	-.393	-.265		
	.300	-.322	-.424	-.524	-.616	-.701	-.787	-.863	-.933	-.901	-.820	-.743	-.659	-.565	-.467	-.374		
	.400	-.412	-.483	-.558	-.627	-.683	-.743	-.794	-.832	-.816	-.761	-.712	-.655	-.586	-.513	-.447		
	.500	-.474	-.521	-.574	-.623	-.657	-.697	-.722	-.739	-.732	-.704	-.675	-.642	-.590	-.540	-.495		
	.600	-.519	-.539	-.574	-.605	-.623	-.644	-.647	-.641	-.647	-.635	-.628	-.616	-.579	-.547	-.525		
	.700	-.486	-.491	-.508	-.525	-.526	-.526	-.511	-.480	-.495	-.508	-.518	-.526	-.504	-.488	-.480		
	.800	-.351	-.342	-.346	-.350	-.339	-.313	-.277	-.228	-.253	-.283	-.317	-.344	-.333	-.334	-.340		
.900	-.041	-.027	-.029	-.033	-.025	-.008	-.007	-.029	-.015	.002	-.004	-.030	-.016	-.022	-.032			
.950	.120	.118	.103	.090	.093	.052	.024	-.010	.009	.044	.076	.095	.101	.115	.119			
Lower surface	.0375	-.789	-.470	-.196	.020	.238	.391	.544	.687	.820	.938	1.038	1.136	1.206	1.267	1.319	1.368	1.418
	.075	-.544	-.300	-.121	.033	.195	.309	.428	.548	.653	.748	.828	.896	.954	1.002	1.040	1.068	1.086
	.150	-.322	-.229	-.101	.007	.127	.207	.299	.395	.488	.578	.658	.728	.786	0.834	0.872	0.896	0.914
	.250	-.315	-.196	-.111	-.035	.059	.120	.197	.283	.368	.452	.532	.608	.682	0.746	0.800	0.844	0.878
	.350	-.243	-.149	-.081	-.023	.050	.096	.153	.220	.286	.352	.418	.484	.550	0.606	0.652	0.688	0.714
	.450	-.209	-.133	-.079	-.033	.027	.062	.112	.165	.216	.272	.328	.384	.440	0.496	0.542	0.578	0.604
	.550	-.187	-.129	-.087	-.052	-.003	.023	.060	.108	.156	.204	.252	.300	.348	0.396	0.444	0.482	0.510
	.650	-.156	-.112	-.085	-.059	-.019	.003	.024	.061	.103	.146	.188	.230	.272	0.314	0.356	0.398	0.430
	.750	-.111	-.084	-.069	-.052	-.025	-.020	-.002	.023	.069	.112	.154	.196	.238	0.280	0.322	0.364	0.406
	.850	-.022	-.010	-.011	-.008	.009	.001	.006	.015	.009	.004	.007	.019	.036	.051	.062	.070	.076
.925	.056	.057	.049	.043	.047	.018	.009	.004	.009	.019	.036	.051	.062	.070	.076	.080	.082	
.975	.108	.100	.083	.073	.072	-.014	-.012	-.034	-.023	-.004	.041	.077	.083	.096	.103	.106	.108	
1.000	.165	.170	.131	.117	.132	.044	-.036	-.064	-.050	-.014	.063	.100	.123	.160	.168			

No orifice.



TABLE 3.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN
NACA 16-510.00 PROPELLER BLADE SECTION ($\alpha = 0.45$; $\beta_x = 59.25^\circ$;

$\beta_{0.75R} = 45^\circ$; B = 2) - Continued

(a) N = 1500 rpm.

	2.584	2.511	2.431	2.345	2.284	2.201	2.139	2.068	1.983	2.021	2.084	2.158	2.227	2.318	2.395	2.480	2.547	
Σ	.690	.674	.654	.635	.621	.604	.592	.577	.560	.569	.582	.595	.612	.629	.646	.664	.678	
M_x	-2.07	-1.37	-.57	.33	1.01	1.96	2.71	3.61	4.74	4.22	3.40	2.48	1.65	.63	-.20	-1.07	-.72	
ΔP	-.07	-.03	.03	.10	.15	.20	.22	.23	.23	.23	.23	.21	.19	.12	.06	0	-.05	
ϵ_x	.11	.30	.49	.70	.86	1.14	1.30	1.51	1.70	1.61	1.45	1.23	1.06	.80	.58	.38	.23	
ϵ_m	.0477	.1271	.2103	.2948	.3800	.4806	.5458	.6303	.7071	.6703	.6065	.5174	.4458	.3368	.2484	.1616	.0974	
ϵ_m	-.0775	-.0728	-.0734	-.0728	-.0698	-.0710	-.0693	-.0665	-.0577	-.0616	-.0695	-.0708	-.0714	-.0719	-.0713	-.0735	-.0755	
ϵ_s																		
c/p	Pressure coefficient, P																	
Upper surface	^a 0.000	1.125	1.119	1.111	1.104	1.100	1.094	1.090	1.085	1.080	1.083	1.087	1.091	1.096	1.102	1.109	1.115	1.120
	.025	.523	.420	.263	.090	-.110	-.367	-.568	-.843	-1.197	-1.033	-.778	-.488	-.262	-.002	.190	.349	.475
	.050	.202	.102	-.039	-.190	-.344	-.542	-.691	-.889	-1.137	-.845	-.636	-.466	-.262	-.101	.040	.154	.257
	.100	-.008	-.091	-.204	-.319	-.431	-.572	-.676	-.810	-.962	-.893	-.780	-.639	-.521	-.370	-.252	-.143	-.047
	.200	-.227	-.292	-.372	-.460	-.529	-.628	-.697	-.783	-.871	-.831	-.766	-.676	-.596	-.491	-.407	-.330	-.297
	.300	-.361	-.411	-.473	-.537	-.581	-.655	-.702	-.762	-.824	-.796	-.749	-.687	-.633	-.573	-.497	-.440	-.385
	.400	-.460	-.496	-.538	-.584	-.610	-.664	-.697	-.739	-.780	-.760	-.734	-.691	-.653	-.594	-.556	-.515	-.478
	.500	-.522	-.545	-.570	-.603	-.612	-.650	-.673	-.700	-.723	-.712	-.697	-.671	-.646	-.603	-.562	-.527	-.532
	.600	-.567	-.578	-.584	-.604	-.600	-.626	-.637	-.653	-.660	-.657	-.653	-.639	-.626	-.599	-.591	-.583	-.570
	.700	-.513	-.514	-.512	-.522	-.509	-.525	-.531	-.539	-.529	-.534	-.539	-.536	-.532	-.514	-.514	-.513	-.514
	.800	-.337	-.337	-.331	-.336	-.317	-.325	-.324	-.327	-.296	-.308	-.328	-.332	-.333	-.323	-.329	-.331	-.338
	.900	.010	.008	.006	-.004	.011	.004	-.002	-.007	.006	.004	-.007	-.006	-.003	.012	.017	.019	.011
	.950	.126	.122	.116	.102	.105	.091	.083	.084	.055	.072	.083	.082	.088	.105	.110	.115	.125
Lower surface	.0375	-.969	-.573	-.448	-.287	-.106	.051	.154	.271	.396	.341	.246	.110	-.017	-.192	-.368	-.532	-.607
	.075	-.497	-.419	-.287	-.183	-.047	.062	.137	.223	.315	.274	.204	.102	-.013	-.111	-.237	-.345	-.459
	.150	-.382	-.312	-.220	-.146	-.047	.030	.085	.145	.213	.183	.131	.058	-.006	-.092	-.183	-.265	-.339
	.250	-.315	-.261	-.194	-.146	-.073	-.015	.026	.070	.124	.099	.060	.005	-.042	-.106	-.168	-.226	-.281
	.350	-.246	-.204	-.149	-.109	-.046	-.003	.029	.066	.104	.086	.057	.012	-.028	-.077	-.126	-.174	-.217
	.450	-.215	-.182	-.140	-.108	-.053	-.017	.009	.035	.067	.054	.030	-.008	-.037	-.077	-.118	-.157	-.191
	.550	-.197	-.171	-.138	-.114	-.066	-.039	-.017	.004	.029	.016	-.001	-.032	-.054	-.085	-.121	-.152	-.180
	.650	-.170	-.151	-.127	-.111	-.070	-.048	-.032	-.017	-.004	-.010	-.020	-.043	-.061	-.085	-.113	-.135	-.152
	.750	-.125	-.116	-.101	-.093	-.061	-.046	-.034	-.027	-.020	-.023	-.026	-.043	-.056	-.070	-.091	-.105	-.112
	.850	-.032	-.032	-.026	-.027	-.008	.001	.005	.006	-.004	0	.007	-.001	-.005	.011	.021	-.025	-.026
	.925	.050	.040	.043	.037	.049	.048	.048	.036	.021	.028	.045	.043	.045	.045	.043	.046	.054
	.975	.099	.090	.083	.077	.079	.071	.065	.052	.015	.030	.060	.067	.070	.078	.077	.082	.096
	^a 1.000	.120	.115	.101	.098	.092	.088	.074	.067	0	.033	.071	.078	.084	.090	.104	.115	.114

^aNo a.c. file.



TABLE 3.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN

NACA 16-510.00 PROPELLER BLADE SECTION ($x = 0.45$; $\beta_x = 59.25^\circ$; $\beta_{0.75R} = 45^\circ$; $B = 2$) - Continued(d) $N = 1600$ rpm.

	2.136	2.227	2.330	2.424	2.514	2.469	2.381	2.295	2.188	2.108	
J	.634	.656	.677	.701	.719	.708	.687	.667	.641	.626	
M_x	2.75	1.66	.50	-.50	-1.40	-.96	-.05	.88	2.12	3.09	
$\Delta\delta$.16	.11	.04	-.04	-.09	-.06	-.01	.06	.13	.17	
α_1	1.36	1.11	.81	.56	.24	.40	.67	.89	1.20	1.45	
α_{11}	.5716	.4671	.3432	.2368	.1013	.1703	.2892	.3781	.5032	.6052	
α_0	-.0744	-.0777	-.0805	-.0832	-.0855	-.0849	-.0826	-.0798	-.0760	-.0731	
α_0				.0162	.0209	.0204					
c/b	Pressure coefficient, P										
Upper surface	∞ .000	1.104	1.112	1.120	1.129	1.137	1.132	1.124	1.116	1.107	1.102
	.025	-.537	-.213	.081	.300	.478	.395	.210	-.014	-.342	-.648
	.050	-.701	-.452	-.205	-.016	.153	.075	-.093	-.284	-.545	-.778
	.100	-.710	-.527	-.341	-.189	-.048	-.117	-.253	-.401	-.594	-.728
	.200	-.743	-.623	-.492	-.379	-.269	-.321	-.425	-.531	-.660	-.768
	.300	-.763	-.681	-.585	-.503	-.414	-.455	-.536	-.609	-.698	-.773
	.400	-.760	-.707	-.641	-.586	-.523	-.553	-.608	-.651	-.710	-.760
	.500	-.730	-.697	-.658	-.630	-.592	-.608	-.641	-.659	-.691	-.724
	.600	-.673	-.676	-.658	-.656	-.644	-.648	-.653	-.648	-.660	-.676
	.700	-.560	-.564	-.562	-.570	-.569	-.572	-.569	-.548	-.547	-.551
	.800	-.331	-.333	-.335	-.344	-.345	-.349	-.344	-.326	-.323	-.323
	.900	-.001	.012	.022	.034	.036	.036	.033	.022	.011	-.001
	.950	.065	.076	.084	.092	.102	.101	.093	.087	.080	.070
Lower surface	.0375	.145	.030	-.245	-.468	-1.069	-.588	-.367	-.164	.057	.201
	.075	.132	0	-.192	-.308	-.438	-.377	-.237	-.096	.065	.174
	.150	.078	.014	-.111	-.225	-.351	-.288	-.174	-.078	.034	.109
	.250	.024	.043	-.122	-.203	-.295	-.245	-.171	-.089	-.004	.051
	.350	.023	.032	-.093	-.152	-.230	-.190	-.126	-.071	-.001	.044
	.450	.004	.041	-.090	-.137	-.202	-.169	-.115	-.074	-.016	.020
	.550	-.022	.059	-.099	-.133	-.188	-.160	-.117	-.085	-.039	-.008
	.650	-.036	.065	-.093	-.115	-.157	-.138	-.105	-.085	-.049	-.025
	.750	-.039	.056	-.074	-.085	-.115	-.098	-.079	-.071	-.045	-.032
	.850	.001	.003	-.007	-.007	-.024	-.013	-.006	-.008	.004	.006
	.925	.046	.056	.051	.057	.052	.058	.057	.050	.053	.047
	.975	.061	.066	.072	.077	.081	.082	.078	.070	.070	.061
	1.000	.071	.071	.084	.086	.093	.098	.085	.075	.069	.065

^aNo orifice.

NACA

TABLE 3.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN
NACA 16-510.00 PROPELLER BLADE SECTION ($x = 0.45$; $\beta_x = 59.25^\circ$;

$\beta_{0.75R} = 45^\circ$; $B = 2$) - Continued

(a) $M = 0.56$.

	2.655	2.600	2.559	2.512	2.466	2.429	2.384	2.347	2.318	2.280	2.252	2.214	2.178	2.140	2.117
J	.646	.646	.649	.652	.655	.657	.661	.659	.665	.668	.673	.675	.676	.676	.678
M_x	-2.71	-2.22	-1.83	-1.38	-.92	-.55	-.08	.31	.63	1.05	1.37	1.81	2.24	2.70	2.98
a_{x1}	-.08	-.05	-.03	0	.03	.05	.08	.10	.11	.13	.14	.15	.16	.17	.18
$\Delta\beta$.04	.13	.19	.29	.42	.47	.57	.67	.74	.87	.97	1.08	1.15	1.28	1.34
c_{L1}	.0168	.0542	.0826	.1239	.1806	.2000	.2406	.2832	.3148	.3690	.4084	.4548	.4826	.5355	.5613
c_{Dn}	-.0782	-.0778	-.0773	-.0770	-.0747	-.0760	-.0754	-.0749	-.0754	-.0746	-.0760	-.0721	-.0708	-.0710	-.0698
c_o															
a/b	Pressure coefficient, P														
Upper surface	0.000	1.108	1.109	1.110	1.111	1.112	1.113	1.114	1.113	1.116	1.116	1.119	1.120	1.120	1.120
	.025	.573	.519	.480	.413	.327	.282	.205	.129	.127	.033	-.111	-.189	-.263	-.383
	.050	.250	.198	.158	.097	.022	-.021	-.090	-.156	-.214	-.298	-.365	-.428	-.492	-.552
	.100	.040	-.009	-.041	-.093	-.154	-.190	-.244	-.294	-.341	-.405	-.460	-.511	-.562	-.639
	.200	-.176	-.215	-.244	-.287	-.332	-.362	-.401	-.445	-.485	-.534	-.579	-.621	-.661	-.721
	.300	-.305	-.341	-.365	-.400	-.436	-.462	-.501	-.532	-.564	-.603	-.645	-.679	-.715	-.762
	.400	-.399	-.429	-.451	-.480	-.506	-.531	-.564	-.588	-.614	-.646	-.682	-.710	-.739	-.778
	.500	-.464	-.488	-.505	-.527	-.546	-.564	-.590	-.607	-.627	-.648	-.674	-.695	-.713	-.737
	.600	-.510	-.528	-.544	-.558	-.567	-.583	-.599	-.609	-.622	-.634	-.653	-.665	-.675	-.686
	.700	-.477	-.489	-.497	-.503	-.503	-.512	-.522	-.522	-.527	-.528	-.536	-.538	-.541	-.537
	.800	-.343	-.344	-.343	-.340	-.338	-.328	-.328	-.323	-.319	-.309	-.308	-.302	-.293	-.280
.900	-.023	-.016	-.007	-.003	.011	.014	.016	.019	.020	.023	.018	.021	.024	.024	
.950	.131	.128	.125	.123	.120	.116	.108	.103	.100	.096	.087	.084	.079	.075	
Lower surface	.0375	-.855	-.705	-.657	-.598	-.497	-.436	-.377	-.298	-.239	-.151	-.094	-.035	.014	.096
	.075	-.542	-.499	-.464	-.405	-.316	-.289	-.244	-.187	-.145	-.079	-.039	.005	.043	.100
	.150	-.390	-.362	-.338	-.300	-.242	-.222	-.187	-.147	-.119	-.073	-.045	.014	.012	.056
	.250	-.314	-.293	-.276	-.250	-.207	-.193	-.168	-.142	-.125	-.092	-.073	-.048	-.029	.006
	.350	-.240	-.227	-.213	-.192	-.157	-.148	-.128	-.106	-.089	-.062	-.048	-.029	.014	.015
	.450	-.260	-.194	-.187	-.171	-.143	-.134	-.122	-.103	-.089	-.067	-.056	-.040	-.029	.005
	.550	-.181	-.178	-.171	-.160	-.136	-.133	-.123	-.109	-.100	-.079	-.073	-.060	-.050	.029
	.650	-.148	-.150	-.145	-.139	-.120	-.118	-.114	-.103	-.097	-.081	-.077	-.069	-.061	.044
	.750	-.101	-.107	-.105	-.103	-.091	-.093	-.090	-.084	-.081	-.070	-.068	-.063	-.058	.044
	.850	-.011	-.019	-.020	-.023	-.014	-.018	-.020	-.018	-.019	-.011	-.014	-.012	-.012	.005
	.925	.069	.062	.059	.053	.056	.049	.045	.047	.044	.045	.041	.040	.037	.038
.975	.115	.108	.103	.097	.095	.086	.081	.078	.075	.075	.067	.066	.060	.055	
1.000	.135	.125	.128	.124	.112	.102	.102	.092	.082	.093	.070	.082	.072	.065	

^aNo orifice.



TABLE 3.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN

NACA 16-510.00 PROPELLER BLADE SECTION ($x = 0.45$; $\beta_x = 59.25^\circ$; $\beta_{0.75R} = 45^\circ$; $B = 2$) - Continued $(r) M = 0.58$.

	2.138	2.164	2.196	2.216	2.247	2.271	2.299	2.327	2.357	2.384	2.419	2.447	2.482	2.510	2.544	2.583
J	2.138	2.164	2.196	2.216	2.247	2.271	2.299	2.327	2.357	2.384	2.419	2.447	2.482	2.510	2.544	2.583
M_x	.703	.700	.699	.695	.694	.691	.689	.687	.684	.683	.680	.678	.676	.674	.672	.669
$C_{L, \beta}$	2.72	2.41	2.02	1.79	1.42	1.15	.84	.53	.21	-.08	-.45	-.73	-1.08	-1.36	-1.69	-2.06
ΔP	.16	.15	.13	.13	.11	.10	.09	.07	.05	.04	.02	.01	-.01	-.03	-.04	-.06
$C_{D, \beta}$	1.28	1.19	1.12	1.06	.98	.91	.82	.74	.68	.62	.53	.44	.33	.27	.24	.16
$C_{D, \beta}$.5381	.4994	.4703	.4458	.4135	.3845	.3490	.3161	.2897	.2632	.2245	.1897	.1639	.1406	.1055	.0690
$C_{D, \beta}$	-.0793	-.0767	-.0752	-.0754	-.0744	-.0752	-.0767	-.0749	-.0755	-.0770	-.0767	-.0770	-.0773	-.0777	-.0778	-.0780
$C_{D, \beta}$	-.0060	-.0031														
o/b	Pressure coefficient, P															
Upper surface	0.000	1.131	1.129	1.129	1.127	1.127	1.126	1.125	1.124	1.123	1.122	1.121	1.120	1.119	1.118	1.117
	.025	-.306	-.223	-.157	-.114	-.075	-.066	-.053	-.108	-.173	-.217	-.290	-.337	-.386	-.464	-.521
	.050	-.538	-.471	-.414	-.374	-.324	-.281	-.232	-.108	-.127	-.088	-.022	.021	.069	.103	.141
	.100	-.615	-.556	-.511	-.477	-.434	-.401	-.361	-.324	-.277	-.247	-.192	-.158	-.119	-.088	-.057
	.200	-.720	-.670	-.634	-.602	-.570	-.541	-.510	-.479	-.440	-.415	-.371	-.342	-.311	-.286	-.259
	.300	-.794	-.745	-.716	-.685	-.656	-.630	-.602	-.577	-.542	-.521	-.483	-.458	-.429	-.409	-.387
	.400	-.833	-.789	-.762	-.730	-.705	-.680	-.657	-.636	-.607	-.588	-.554	-.533	-.508	-.491	-.473
	.500	-.844	-.793	-.762	-.739	-.716	-.697	-.682	-.666	-.651	-.631	-.617	-.591	-.576	-.556	-.542
	.600	-.829	-.786	-.762	-.736	-.716	-.697	-.682	-.666	-.651	-.631	-.617	-.591	-.576	-.556	-.542
	.700	-.751	-.747	-.732	-.716	-.705	-.688	-.675	-.659	-.649	-.629	-.617	-.609	-.597	-.584	-.573
	.800	-.286	-.288	-.296	-.299	-.303	-.306	-.317	-.320	-.322	-.338	-.337	-.339	-.340	-.348	-.352
.900	.012	.019	.020	.026	.028	.033	.032	.033	.035	.035	.025	.020	.016	.017	.008	
.950	.057	.064	.064	.070	.074	.079	.084	.087	.095	.108	.115	.119	.123	.127	.129	
Lower surface	.0375	.066	.016	-.037	-.066	-.114	-.153	-.210	-.264	-.322	-.376	-.457	-.513	-.542	-.558	-.588
	.075	.073	.036	-.002	-.024	-.058	-.085	-.126	-.165	-.206	-.244	-.293	-.327	-.364	-.395	-.445
	.150	.038	.013	-.015	-.029	-.053	-.071	-.101	-.128	-.152	-.179	-.220	-.249	-.276	-.297	-.325
	.250	-.007	-.025	-.046	-.054	-.073	-.085	-.110	-.134	-.155	-.174	-.198	-.217	-.234	-.250	-.271
	.350	-.003	-.016	-.034	-.042	-.055	-.065	-.084	-.101	-.114	-.130	-.149	-.164	-.179	-.192	-.208
	.450	-.020	-.031	-.046	-.050	-.062	-.068	-.086	-.099	-.108	-.121	-.135	-.148	-.159	-.168	-.181
	.550	-.045	-.051	-.069	-.067	-.077	-.083	-.095	-.108	-.113	-.122	-.134	-.144	-.151	-.158	-.167
	.650	-.056	-.062	-.072	-.073	-.080	-.083	-.095	-.102	-.105	-.113	-.119	-.127	-.130	-.133	-.141
	.750	-.053	-.057	-.066	-.066	-.070	-.071	-.078	-.084	-.083	-.086	-.090	-.095	-.096	-.097	-.102
	.850	-.008	-.008	-.012	-.010	-.012	-.010	-.016	-.018	-.014	-.013	-.015	-.016	-.015	-.012	-.014
	.925	.044	.046	.044	.046	.047	.048	.045	.045	.050	.053	.056	.056	.059	.063	.064
.975	.064	.065	.063	.064	.065	.067	.065	.066	.074	.082	.086	.090	.094	.102	.103	
1.000	.074	.074	.088	.072	.071	.072	.080	.076	.085	.092	.100	.107	.113	.118	.119	

*No orifice.

NACA

TABLE 3.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN
NACA 16-510.00 PROPELLER BLADE SECTION ($\alpha = 0.45^\circ$; $\beta_x = 59.25^\circ$;

$\beta_{0.75R} = 45^\circ$; $B = 2$) - Continued

(g) $M = 0.60$.

	2.169	2.192	2.217	2.238	2.266	2.293	2.319	2.346	2.378	2.911	2.430	2.468	2.492	2.525	2.561
$\frac{J}{\rho V^2 c}$.725	.723	.718	.716	.713	.711	.709	.706	.707	.705	.700	.701	.696	.693	.691
$\Delta \beta$	2.34	2.07	1.78	1.53	1.21	.90	.61	.32	.02	-.36	-.56	-.95	-1.18	-1.51	-1.85
α_1	1.14	1.09	1.01	.95	.86	.79	.72	.65	.58	.51	.45	.38	.32	.25	.17
α_m	.4768	.4606	.4265	.4000	.3626	.3323	.3045	.2735	.2452	.2187	.1933	.1619	.1368	.1065	.0729
α_o	-.0808	-.0773	-.0724	-.0752	-.0737	-.0769	-.0770	-.0793	-.0793	-.0770	-.0770	-.0788	-.0777	-.0793	-.0793
c_o	.0009	.0005	.0021	.0040	.0072	.0094	.0112	.0132	.0151	.0163	.0175	.0198			
a/b	Pressure coefficient, P														
Upper surface	α_0 .000	1.139	1.138	1.136	1.135	1.134	1.133	1.133	1.132	1.132	1.131	1.129	1.129	1.128	1.126
	.025	.032	-.102	-.060	-.010	.065	.119	.160	.217	.266	.304	.344	.399	.437	.479
	.050	-.408	-.376	-.338	-.293	-.230	-.179	-.141	-.093	-.047	.012	.025	.079	.112	.153
	.100	-.507	-.422	-.445	-.411	-.358	-.319	-.288	-.247	-.210	-.181	-.152	-.108	-.060	-.046
	.200	-.697	-.627	-.594	-.564	-.520	-.486	-.460	-.427	-.395	-.368	-.346	-.306	-.286	-.257
	.300	-.760	-.723	-.692	-.663	-.627	-.595	-.571	-.542	-.513	-.488	-.468	-.435	-.417	-.390
	.400	-.859	-.810	-.777	-.741	-.705	-.673	-.650	-.623	-.596	-.569	-.554	-.522	-.508	-.485
	.500	-.890	-.784	-.756	-.731	-.709	-.688	-.670	-.652	-.630	-.609	-.598	-.575	-.564	-.544
	.600	-.768	-.736	-.715	-.700	-.691	-.679	-.670	-.688	-.674	-.627	-.618	-.603	-.597	-.583
	.700	-.597	-.550	-.541	-.543	-.546	-.549	-.552	-.549	-.545	-.536	-.530	-.533	-.541	-.544
	.800	-.293	-.291	-.289	-.295	-.301	-.311	-.318	-.322	-.326	-.323	-.330	-.333	-.341	-.343
.900	.015	.021	.023	.023	.021	.019	.015	.014	.012	.017	.009	.008	-.002	-.006	
.950	.096	.104	.109	.111	.111	.112	.111	.115	.116	.120	.122	.125	.122	.126	
Lower surface	.0375	-.041	-.061	-.093	-.139	-.202	-.279	-.307	-.363	-.425	-.463	-.514	-.530	-.542	-.630
	.075	-.146	-.009	-.043	-.076	-.122	-.162	-.196	-.237	-.277	-.295	-.326	-.371	-.419	-.452
	.150	-.023	-.029	-.046	-.068	-.098	-.124	-.147	-.179	-.209	-.223	-.248	-.281	-.314	-.338
	.250	-.099	-.061	-.071	-.088	-.111	-.132	-.153	-.169	-.190	-.198	-.216	-.239	-.265	-.280
	.350	-.048	-.047	-.057	-.071	-.088	-.102	-.117	-.132	-.148	-.155	-.168	-.186	-.208	-.221
	.450	-.060	-.059	-.065	-.073	-.090	-.102	-.113	-.124	-.138	-.140	-.153	-.167	-.184	-.194
	.550	-.084	-.080	-.085	-.090	-.102	-.111	-.121	-.129	-.139	-.140	-.149	-.151	-.173	-.179
	.650	-.095	-.089	-.091	-.096	-.104	-.109	-.115	-.122	-.128	-.126	-.133	-.140	-.151	-.154
	.750	-.089	-.082	-.084	-.088	-.091	-.092	-.095	-.099	-.100	-.100	-.104	-.105	-.114	-.114
	.850	-.034	-.026	-.026	-.027	-.026	-.025	-.022	-.024	-.024	-.022	-.022	-.020	-.025	-.022
	.925	-.026	.035	.036	.037	.041	.043	.044	.047	.050	.054	.054	.059	.056	.061
.975	.064	.072	.075	.080	.085	.089	.090	.096	.099	.103	.107	.112	.141	.117	
1.000	.085	.099	.094	.108	.107	.095	.120	.122	.122	.132	.138	.155	.175	.140	

^aNo orifice.



TABLE 3.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN
 NACA 16-510.00 PROPELLER BLADE SECTION ($\alpha = 0.45$; $\beta_x = 59.25^\circ$;

$\beta_{0.75R} = 45^\circ$; B = 2) - Concluded.

(h) M = 0.65.

	2.123	2.139	2.172	2.179	2.206	2.218	2.253	2.273	2.299	2.303	2.333	2.356	2.380	2.417
J	2.123	2.139	2.172	2.179	2.206	2.218	2.253	2.273	2.299	2.303	2.333	2.356	2.380	2.417
$\mu_{1/2}$.808	.801	.801	.794	.791	.785	.788	.782	.780	.774	.772	.770	.765	.764
$\mu_{1/4}$	2.91	2.71	2.31	2.23	1.90	1.76	1.36	1.13	.84	.80	.47	.21	-.04	-.43
$\Delta\delta$.11	.09	.06	.05	.03	.01	-.01	-.03	-.05	-.05	-.07	-.09	-.11	-.13
α_1	1.06	1.02	.96	.91	.86	.83	.75	.71	.64	.62	.56	.46	.40	.33
b_n	.4419	.4265	.4013	.3832	.3600	.3503	.3161	.2987	.2697	.2626	.2374	.1968	.1703	.1400
c_m	-.0968	-.0983	-.0960	-.0911	-.0934	-.0921	-.0901	-.0888	-.0875	-.0888	-.0849	-.0836	-.0846	-.0846
c_D	.0240	.0248	.0234	.0230	.0232	.0222	.0220	.0191	.0197	.0201	.0199	.0203	.0205	.0210
c/b	Pressure coefficient, P													
Upper surface	0.000	1.174	1.171	1.171	1.168	1.166	1.164	1.165	1.162	1.162	1.159	1.158	1.155	1.155
	.025	.082	.081	.118	.133	.171	.185	.224	.239	.282	.291	.326	.368	.395
	.050	-.231	-.217	-.183	-.171	-.137	-.123	-.088	-.074	-.033	-.025	.007	.046	.072
	.100	-.361	-.348	-.318	-.310	-.284	-.276	-.244	-.235	-.200	-.197	-.170	-.136	-.116
	.200	-.566	-.548	-.512	-.505	-.483	-.476	-.449	-.440	-.409	-.407	-.383	-.355	-.337
	.300	-.694	-.659	-.637	-.638	-.620	-.618	-.595	-.587	-.560	-.559	-.535	-.509	-.493
	.400	-.789	-.795	-.771	-.775	-.760	-.760	-.740	-.736	-.713	-.714	-.691	-.667	-.652
	.500	-.909	-.921	-.895	-.896	-.880	-.875	-.845	-.827	-.800	-.800	-.779	-.750	-.732
	.600	-1.002	-1.006	-.976	-.975	-.960	-.960	-.939	-.919	-.878	-.863	-.831	-.799	-.750
	.700	-.499	-.473	-.464	-.507	-.534	-.613	-.636	-.668	-.665	-.713	-.700	-.685	-.669
	.800	-.368	-.370	-.327	-.310	-.294	-.270	-.246	-.230	-.228	-.246	-.248	-.263	-.285
.900	-.286	-.293	-.250	-.228	-.202	-.166	-.129	-.077	-.040	-.029	-.002	.011	.016	
.950	-.181	-.198	-.164	-.146	-.131	-.100	-.065	-.020	-.009	-.019	-.039	.058	.070	
Lower surface	.0375	-.102	-.141	-.167	-.207	-.257	-.294	-.331	-.358	-.415	-.469	-.521	-.640	-.745
	.075	-.090	-.080	-.096	-.128	-.165	-.193	-.217	-.235	-.277	-.312	-.338	-.362	-.364
	.150	-.056	-.079	-.088	-.110	-.136	-.156	-.170	-.182	-.208	-.238	-.257	-.289	-.312
	.250	-.092	-.109	-.115	-.132	-.155	-.171	-.183	-.192	-.209	-.230	-.242	-.263	-.278
	.350	-.086	-.101	-.101	-.118	-.135	-.148	-.155	-.162	-.174	-.193	-.200	-.218	-.230
	.450	-.105	-.117	-.115	-.128	-.142	-.153	-.158	-.162	-.170	-.187	-.191	-.204	-.213
	.550	-.142	-.152	-.144	-.157	-.168	-.178	-.178	-.179	-.183	-.197	-.197	-.206	-.212
	.650	-.168	-.174	-.164	-.184	-.181	-.188	-.183	-.179	-.180	-.189	-.186	-.191	-.194
	.750	-.181	-.183	-.165	-.172	-.176	-.178	-.170	-.163	-.157	-.164	-.157	-.158	-.157
	.850	-.132	-.129	-.107	-.108	-.108	-.105	-.095	-.084	-.075	-.079	-.069	-.066	-.064
	.925	-.086	-.082	-.054	-.051	-.046	-.039	-.027	-.015	0	-.003	.008	.014	.020
.975	-.084	-.092	-.058	-.046	-.037	-.022	-.010	-.013	.031	.032	.043	.053	.069	
1.000	-.080	-.099	-.064	-.047	-.036	-.021	-.010	.025	.047	.048	.062	.072	.100	

^aNo profile.



TABLE 4.-- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN

NACA 16-507.50 PROPELLER BLADE SECTION ($\alpha = 0.60$; $\beta_x = 51.33^\circ$)

$\beta_{0.75r} = 45^\circ$; $B = 2$)

(a) $N = 1140$ rpm.

	1.569	1.718	1.860	1.998	2.150	2.309	2.459	2.574	2.685	2.621	2.511	2.380	2.231	2.079	1.931	1.796	1.636
C_L	.419	.434	.454	.472	.489	.511	.532	.544	.562	.552	.535	.519	.497	.478	.461	.439	.426
C_D	11.56	8.98	6.71	4.66	2.57	.56	-1.20	-2.24	-3.60	-2.95	-1.77	-.29	1.52	3.53	5.64	7.72	10.38
$\Delta\delta$.50	.42	.35	.29	.20	.10	.01	-.06	-.14	-.10	-.03	.06	.15	.25	.32	.39	.46
α_1	2.84	2.58	2.13	1.75	1.35	.93	.56	.34	.02	.17	.41	.74	1.14	1.54	1.96	2.33	2.68
σ_{11}	1.0892	.9890	.8264	.6832	.5316	.3661	.2229	.1361	.0071	.0665	.1642	.2923	.4465	.6019	.7587	.9000	1.0245
σ_{12}	-.0562	-.0439	-.0578	-.0659	-.0767	-.0784	-.0789	-.0864	-.0900	-.0847	-.0819	-.0793	-.0787	-.0813	-.0819	-.0505	-.0442
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*No critical.



TABLE 4.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN

NACA 16-507.50 PROPELLER BLADE SECTION ($\alpha = 0.60$; $\beta_x = 51.33^\circ$; $P_{0.75R} = 45^\circ$; $B = 2$) - Continued(b) $N = 1350$ rpm.

J	1.709	1.822	1.937	2.051	2.199	2.322	2.450	2.580	2.668	2.625	2.524	2.388	2.252	2.136	2.025	1.875	1.762	
M	.517	.531	.550	.571	.587	.609	.630	.651	.666	.659	.640	.618	.600	.576	.561	.536	.520	
ΔC_p	9.13	7.30	5.26	3.50	1.93	.40	-1.10	-2.52	-3.43	-2.99	-1.92	-.38	.89	2.76	4.28	6.48	8.26	
C_p	.69	.58	.44	.32	.22	.09	-.05	-.17	-.25	-.21	-.12	.01	.13	.27	.37	.53	.64	
C_{Dp}	2.76	2.39	2.00	1.65	1.26	.93	.77	.84	.04	.14	.40	.75	1.04	1.47	1.81	2.18	2.59	
C_{Dp}	1.0626	.9252	.7781	.6471	.4935	.3674	.2271	.0977	.0161	.0574	.1603	.2965	.4097	.5768	.7071	.8432	.9994	
C_c	-.0416	-.0487	-.0708	-.0772	-.0803	-.0790	-.0858	-.0928	-1.000	-.0939	-.0882	-.0855	-.0856	-.0821	-.0742	-.0649	-.0416	
c/b	Pressure coefficient, P																	
Upper surface	$\alpha 0.000$	1.068	1.072	1.078	1.084	1.089	1.096	1.103	1.110	1.116	1.113	1.106	1.099	1.093	1.085	1.081	1.073	1.069
	.025	-2.868	-2.664	-1.411	-.867	-.359	-.009	-.309	.571	.636	.581	.446	.177	-.126	-.593	-1.107	-1.612	-2.874
	.050	-2.213	-1.626	-1.294	-.927	-.563	-.272	-.010	.199	.300	.249	.119	-.127	-.383	-.735	-1.089	-1.527	-2.228
	.100	-1.807	-1.250	-1.001	-.785	-.548	-.342	-.151	.011	.096	.052	-.054	-.237	-.420	-.661	-.880	-1.153	-1.534
	.200	-1.227	-.990	-.837	-.707	-.561	-.417	-.284	-.165	-.101	-.135	-.214	-.348	-.471	-.630	-.763	-.932	-1.097
	.300	-.937	-.871	-.772	-.685	-.582	-.477	-.378	-.285	-.235	-.261	-.324	-.427	-.516	-.630	-.722	-.835	-.945
	.400	-.795	-.800	-.741	-.685	-.614	-.532	-.460	-.391	-.354	-.373	-.419	-.499	-.561	-.646	-.708	-.783	-.858
	.500	-.672	-.695	-.661	-.621	-.572	-.513	-.462	-.413	-.388	-.402	-.433	-.490	-.532	-.593	-.632	-.680	-.738
	.600	-.561	-.585	-.579	-.564	-.534	-.489	-.458	-.426	-.413	-.420	-.438	-.480	-.504	-.546	-.566	-.590	-.628
	.700	-.426	-.448	-.468	-.472	-.461	-.433	-.419	-.405	-.405	-.405	-.411	-.432	-.440	-.464	-.466	-.466	-.490
	.800	-.310	-.294	-.341	-.364	-.376	-.367	-.370	-.378	-.390	-.381	-.374	-.374	-.365	-.369	-.351	-.319	-.352
	.900	-.149	-.077	-.074	-.088	-.096	-.097	-.109	-.125	-.142	-.130	-.118	-.107	-.093	-.090	-.080	-.072	-.154
.950	-.083	-.023	-.020	-.036	-.048	-.063	-.067	-.066	-.056	-.063	-.063	-.063	-.062	-.046	-.032	-.006	-.083	
Lower surface	.0375	.751	.684	.525	.349	.126	-.092	-.385	-.765	-1.219	-1.037	-.599	-.295	-.003	.237	.434	.618	.685
	.075	.612	.554	.422	.287	.126	-.020	-.207	-.417	-.816	-.577	-.316	-.125	.047	.212	.354	.497	.550
	.150	.446	.397	.289	.183	.061	-.045	-.167	-.279	-.377	-.308	-.238	-.125	-.003	.119	.233	.346	.389
	.250	.354	.317	.235	.157	.069	-.004	-.090	-.177	-.235	-.200	-.139	-.055	.032	.117	.194	.278	.297
	.350	.295	.270	.203	.141	.073	.016	-.050	-.120	-.161	-.138	-.089	-.025	.045	.111	.172	.239	.244
	.450	.224	.203	.148	.097	.040	-.002	-.077	-.110	-.137	-.122	-.086	-.037	.021	.074	.123	.176	.175
	.550	.139	.127	.083	.044	.001	-.031	-.071	-.110	-.126	-.117	-.091	-.057	-.012	.027	.065	.108	.097
	.650	.106	.102	.071	.042	.008	-.016	-.047	-.073	-.082	-.077	-.058	-.037	.001	.029	.057	.086	.069
	.750	.044	.006	.035	.016	-.005	-.018	-.037	-.050	-.051	-.050	-.043	-.032	-.006	.009	.027	.040	.011
	.850	.054	.068	.069	.060	.050	.049	.040	.068	.035	.036	.039	.040	.056	.062	.065	.066	.025
	.925	-.005	.019	.037	.042	.048	.058	.060	.066	.070	.070	.067	.056	.060	.060	.050	.043	.025
	.975	-.034	-.001	.035	.054	.069	.090	.101	.113	.117	.116	.112	.101	.086	.064	.047	.011	-.046
$\alpha 1.000$	-.041	-.009	.033	.062	.043	.127	.145	.160	.146	.145	.142	.125	.108	.073	.052	.010	-.040	

^aNo orifices.

TABLE 4.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN

NACA 16-507.50 PROPELLER BLADE SECTION ($\alpha = 0.60$; $\beta_x = 51.33^\circ$;

$\beta_{0.75R} = 45^\circ$; $B = 2$) - Continued

(a) $N = 1500$ rpm.

	2.027	2.103	2.193	2.306	2.417	2.520	2.589	2.599	2.483	2.383	2.254	2.171	2.069	1.981	
J	.638	.650	.663	.684	.705	.727	.740	.732	.694	.675	.674	.655	.639	.623	
M_x	4.25	3.17	2.01	.59	-.72	-1.87	-2.61	-2.29	-1.47	-.33	1.23	2.30	3.66	4.90	
$\Delta\delta$.56	.48	.37	.20	0	-.19	-.33	-.26	-.11	.06	.29	.40	.52	.60	
α_1	1.89	1.62	1.30	.92	.59	.22	-.09	.10	.42	.69	1.07	1.40	1.75	2.08	
c_n	.7361	.6342	.5119	.3645	.2316	.0865	-.0181	.0400	.1632	.2732	.4206	.5497	.6871	.8110	
c_m	-.0762	-.0793	-.0850	-.0880	-.0905	-.0973	-.1078	-.1021	-.0905	-.0880	-.0854	-.0818	-.0783	-.0723	
c_o															
a/b	Pressure coefficient, P														
Upper surface	0.000	1.106	1.110	1.115	1.123	1.131	1.140	1.145	1.142	1.135	1.127	1.119	1.112	1.106	1.100
	.025	-1.012	-.644	-.292	.100	.374	.598	.639	.599	.488	.286	-.044	-.380	-.822	-1.352
	.050	-1.166	-.862	-.575	-.243	.010	.193	.282	.238	.120	-.075	-.364	-.641	-1.000	-1.432
	.100	-.886	-.722	-.545	-.317	-.127	.021	.098	.060	-.043	-.193	-.401	-.585	-.802	-.937
	.200	-.802	-.691	-.583	-.428	-.289	-.176	-.112	-.145	-.227	-.339	-.485	-.604	-.743	-.887
	.300	-.761	-.685	-.603	-.489	-.382	-.295	-.244	-.269	-.336	-.418	-.526	-.613	-.720	-.813
	.400	-.744	-.693	-.639	-.561	-.477	-.411	-.369	-.389	-.441	-.506	-.583	-.642	-.717	-.776
	.500	-.693	-.626	-.594	-.543	-.484	-.442	-.415	-.425	-.464	-.505	-.555	-.591	-.643	-.680
	.600	-.608	-.589	-.572	-.544	-.507	-.487	-.474	-.480	-.501	-.521	-.548	-.567	-.600	-.619
	.700	-.543	-.539	-.539	-.532	-.516	-.521	-.527	-.523	-.525	-.523	-.528	-.529	-.543	-.540
	.800	-.334	-.339	-.347	-.350	-.343	-.354	-.361	-.357	-.356	-.333	-.344	-.338	-.341	-.325
.900	-.062	-.064	-.074	-.079	-.078	-.091	-.101	-.097	-.093	-.081	-.075	-.065	-.069	-.064	
.950	.030	.045	.052	.064	.080	.078	.078	.078	.076	.071	.064	.057	.035	.014	
Lower surface	.0375	.407	.280	.110	-.151	-.418	-1.238	-1.572	-1.515	-.562	-.315	-.038	.167	.342	.501
	.075	.345	.253	.131	-.044	-.210	-.387	-1.192	-.600	-.312	-.150	.030	.174	.297	.415
	.150	.247	.180	.090	-.035	-.149	-.259	-.274	-.269	-.225	-.110	.021	.124	.212	.301
	.250	.202	.149	.080	-.008	-.088	-.178	-.212	-.198	-.147	-.063	.035	.108	.172	.240
	.350	.165	.133	.079	.004	-.056	-.130	-.166	-.148	-.103	-.037	.041	.102	.143	.197
	.450	.127	.095	.049	-.010	-.058	-.117	-.147	-.131	-.096	-.043	.019	.070	.108	.154
	.550	.093	.064	.025	-.020	-.055	-.102	-.127	-.115	-.088	-.046	.004	.044	.078	.116
	.650	.060	.035	.003	-.034	-.058	-.092	-.108	-.100	-.083	-.052	-.015	.019	.046	.074
	.750	.045	.025	.003	-.020	-.035	-.056	-.064	-.060	-.051	-.031	-.007	.019	.035	.054
	.850	.062	.068	.054	.040	.038	.025	.022	.024	.028	.037	.050	.065	.065	.069
	.925	.073	.071	.066	.067	.075	.073	.076	.077	.073	.072	.071	.076	.071	.073
.975	.055	.064	.071	.084	.104	.111	.120	.118	.109	.096	.082	.076	.068	.045	
1.000	.032	.058	.072	.088	.122	.178	.183	.199	.155	.144	.127	.117	.108	.019	

^aNo orifices.



TABLE 4.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN

NACA 16-507.50 PROPELLER BLADE SECTION. ($x = 0.60$; $\beta_x = 51.33^\circ$; $\beta_{0.728} = 45^\circ$; $B = 2$) - Continued(a) $N = 1600$ rpm.

	σ	$C_{D, \text{total}}$	$C_{D, \text{tip}}$	$C_{D, \text{root}}$	$C_{D, \text{mid}}$	$C_{D, \text{mid}}$	$C_{D, \text{mid}}$	$C_{D, \text{mid}}$	$C_{D, \text{mid}}$	$C_{D, \text{mid}}$	$C_{D, \text{mid}}$	$C_{D, \text{mid}}$	$C_{D, \text{mid}}$	$C_{D, \text{mid}}$
	2.095	2.183	2.237	2.314	2.383	2.458	2.531	2.509	2.434	2.354	2.280	2.221	2.141	
	.683	.699	.712	.726	.738	.753	.774	.764	.746	.730	.716	.702	.687	
	3.31	2.14	1.45	.90	-.32	-1.19	-2.21	-1.75	-.91	.02	.92	1.65	2.69	
	.43	.30	.21	.08	-.07	-.23	-.41	-.34	-.18	0	.14	.23	.37	
	1.79	1.50	1.29	1.00	.79	.46	.14	.28	.62	.87	1.10	1.35	1.62	
	.7032	.5897	.5077	.3948	.3135	.1839	.0948	.1103	.2439	.3426	.4342	.5316	.6381	
	-.0862	-.0864	-.0942	-.0942	-.0944	-.0986	-.1047	-.1041	-.0929	-.0921	-.0921	-.0895	-.0860	
						.0215	.0264	.0239						
r/b	Pressure coefficient, C_p													
Upper surface	0.000	1.122	1.129	1.134	1.139	1.144	1.150	1.159	1.155	1.148	1.141	1.135	1.130	1.124
	.025	-.718	-.347	-.127	-.129	-.297	.483	.604	.592	.432	.229	.048	-.197	-.518
	.050	-1.010	-.635	-.438	-.208	-.074	.131	.270	.206	.055	-.129	-.293	-.507	-.795
	.100	-.841	-.628	-.493	-.323	-.197	-.053	.070	.014	-.105	-.264	-.357	-.536	-.725
	.200	-.806	-.668	-.576	-.452	-.356	-.243	-.136	-.185	-.283	-.410	-.497	-.600	-.728
	.300	-.801	-.712	-.648	-.554	-.477	-.386	-.291	-.334	-.417	-.521	-.586	-.659	-.747
	.400	-.809	-.762	-.723	-.661	-.603	-.531	-.447	-.485	-.551	-.636	-.674	-.720	-.773
	.500	-.711	-.693	-.677	-.644	-.610	-.564	-.501	-.528	-.574	-.621	-.644	-.663	-.691
	.600	-.628	-.625	-.624	-.616	-.609	-.602	-.568	-.580	-.591	-.600	-.608	-.609	-.621
	.700	-.505	-.512	-.520	-.525	-.526	-.543	-.562	-.548	-.513	-.510	-.509	-.498	-.500
	.800	-.333	-.343	-.354	-.365	-.339	-.363	-.387	-.385	-.370	-.383	-.363	-.346	-.340
.900	-.044	-.040	-.043	-.045	-.040	-.049	-.049	-.049	-.040	-.060	-.046	-.036	-.041	
.950	.033	.044	.049	.056	.067	.069	.077	.075	.075	.050	.056	.055	.041	
Lower surface	.0375	.332	.175	.043	-.143	-.311	-.486	-1.369	-1.250	-.416	-.269	-.086	.096	.250
	.075	.285	.171	.075	-.056	-.153	-.281	-1.268	-.611	-.248	-.133	-.007	.119	.226
	.150	.183	.097	.026	-.066	-.135	-.251	-.271	-.269	-.206	-.139	-.044	.055	.136
	.250	.151	.099	.048	-.020	-.067	-.157	-.207	-.191	-.116	-.067	.003	.075	.133
	.350	.154	.106	.063	-.008	-.027	-.101	-.152	-.129	-.069	-.033	.025	.082	.127
	.450	.110	.071	.035	-.010	-.038	-.100	-.147	-.122	-.070	-.047	.002	.052	.089
	.550	.052	.022	-.006	-.039	-.059	-.109	-.147	-.126	-.085	-.072	-.031	.011	.039
	.650	.055	.031	-.006	-.022	-.036	-.076	-.102	-.087	-.057	-.050	-.017	.018	.041
	.750	.028	.004	-.010	-.025	-.031	-.059	-.075	-.063	-.046	-.050	-.024	.005	.018
	.850	.075	.068	.056	.045	.045	.028	.026	.032	.038	.025	.045	.063	.069
	.925	.055	.056	.052	.051	.057	.049	.054	.053	.055	.033	.046	.058	.053
.975	.052	.060	.060	.067	.078	.077	.090	.091	.081	.053	.062	.063	.053	
1.000	.062	.079	.085	.100	.102	.110	.126	.135	.116	.089	.090	.080	.070	

*No orifice.

NACA

TABLE 4.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN
NACA 16-507.50 PROPELLER BLADE SECTION ($\alpha = 0.60$; $\beta_x = 51.33^\circ$;

$\beta_{0.75R} = 45^\circ$; $B = 2$) - Continued

(a) $M = 0.56$.

	2.621	2.563	2.527	2.492	2.447	2.403	2.379	2.338	2.302	2.269	2.246	2.212	2.188	2.168	2.135	2.117	
J	.700	.701	.709	.715	.717	.722	.727	.732	.734	.738	.744	.745	.748	.754	.756	.759	
$c_{x'}$	-2.95	-2.94	-1.95	-1.57	-1.06	-.56	-.28	.21	.64	1.05	1.34	1.77	2.07	2.33	2.77	3.01	
Δh	-.23	-.19	-.16	-.13	-.08	-.01	.03	.07	.09	.11	.12	.14	.17	.19	.25	.30	
c_1	.01	.13	.26	.38	.47	.62	.69	.81	.92	1.03	1.12	1.22	1.29	1.37	1.47	1.53	
c_2	-.0052	-.0535	-.1026	-.1487	-.1874	-.2439	-.2735	-.3203	-.3613	-.4071	-.4426	-.4794	-.5077	-.5400	-.5755	-.6006	
c_m	-.0908	-.0852	-.0857	-.0844	-.0844	-.0846	-.0850	-.0855	-.0840	-.0824	-.0828	-.0839	-.0872	-.0865	-.0885	-.0869	
c_o														-.0002	-.0031	-.0051	
q/h	Pressure coefficient, P																
Upper surface	∞	1.129	1.130	1.133	1.135	1.136	1.138	1.140	1.142	1.143	1.144	1.146	1.147	1.148	1.151	1.152	1.153
	.025	.636	.589	.551	.497	.445	.397	.309	.217	.131	.040	-.009	-.080	-.141	-.201	-.276	-.328
	.050	.294	.244	.206	.155	.104	.084	-.019	-.101	-.173	-.249	-.293	-.356	-.411	-.466	-.538	-.594
	.100	.105	.062	.029	-.012	-.053	-.115	-.150	-.213	-.270	-.329	-.362	-.407	-.447	-.481	-.528	-.557
	.200	-.095	-.132	-.161	-.196	-.232	-.286	-.313	-.368	-.415	-.462	-.491	-.527	-.560	-.586	-.622	-.649
	.300	-.224	-.258	-.282	-.315	-.347	-.394	-.419	-.469	-.511	-.553	-.581	-.613	-.642	-.669	-.721	-.754
	.400	-.338	-.370	-.393	-.422	-.453	-.494	-.520	-.568	-.609	-.652	-.688	-.725	-.761	-.791	-.819	-.829
	.500	-.376	-.404	-.422	-.446	-.470	-.501	-.521	-.560	-.592	-.620	-.646	-.671	-.707	-.765	-.823	-.864
	.600	-.435	-.456	-.470	-.487	-.508	-.528	-.542	-.571	-.592	-.612	-.631	-.644	-.659	-.669	-.683	-.680
	.700	-.414	-.429	-.437	-.443	-.455	-.464	-.469	-.484	-.493	-.497	-.500	-.499	-.498	-.491	-.487	-.479
	.800	-.370	-.372	-.368	-.360	-.360	-.352	-.347	-.344	-.341	-.329	-.324	-.313	-.305	-.289	-.281	-.270
	.900	-.120	-.111	-.098	-.085	-.078	-.065	-.058	-.053	-.051	-.044	-.040	-.034	-.034	-.030	-.031	-.030
.950	.059	.063	.071	.073	.074	.075	.074	.065	.058	.054	.049	.044	.037	.033	.023	.020	
Lower surface	.0375	-1.314	-1.161	-.889	-.551	-.414	-.311	-.238	-.198	-.121	-.025	.021	.080	.120	.165	.207	.238
	.075	-.707	-.542	-.428	-.349	-.310	-.236	-.189	-.119	-.063	-.005	.024	.063	.091	.125	.157	.184
	.150	-.369	-.312	-.275	-.238	-.208	-.155	-.129	-.087	-.053	-.013	.007	.038	.057	.083	.107	.127
	.250	-.237	-.213	-.184	-.155	-.133	-.093	-.073	-.044	-.020	.009	.025	.047	.063	.082	.100	.117
	.350	-.171	-.156	-.134	-.111	-.095	-.063	-.047	-.025	-.008	.016	.028	.047	.059	.074	.088	.102
	.450	-.147	-.137	-.121	-.102	-.089	-.065	-.052	-.036	-.023	-.005	.005	.019	.029	.042	.054	.064
	.550	-.122	-.117	-.104	-.089	-.079	-.061	-.051	-.039	-.030	-.014	-.008	.004	.012	.021	.030	.039
	.650	-.101	-.100	-.092	-.081	-.076	-.061	-.052	-.047	-.041	-.031	-.025	-.016	-.011	-.003	.002	.008
	.750	-.058	-.062	-.056	-.049	-.048	-.038	-.034	-.031	-.029	-.022	-.020	-.013	-.011	-.006	-.003	.001
	.850	.023	.018	.023	.026	.025	.031	.033	.032	.031	.032	.034	.036	.037	.041	.041	.043
	.925	.072	.068	.071	.072	.069	.069	.069	.063	.059	.058	.056	.057	.053	.053	.050	.049
	.975	.115	.109	.108	.106	.100	.094	.091	.081	.072	.066	.061	.057	.051	.048	.039	.035
∞	.130	.130	.120	.130	.113	.109	.100	.090	.075	.069	.060	.059	.050	.040	.030	.030	

^aNo critical.



TABLE 4. -- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN
NACA 16-507.50 PROPELLER BLADE SECTION ($\alpha = 0.60$; $\beta_x = 51.33^\circ$)

$R_{0.75R} = 45^\circ$; $B = 2$) - Continued

(r) $M = 0.58$.

J	2.584	2.549	2.509	2.471	2.421	2.381	2.343	2.315	2.289	2.260	2.241	2.211	2.185	2.152	2.131	
M_x	.727	.735	.739	.743	.744	.749	.753	.757	.760	.764	.772	.775	.779	.781	.788	
α_x'	-2.56	-2.18	-1.75	-1.33	-1.76	-1.30	.15	.49	.81	1.16	1.40	1.78	2.12	2.54	2.81	
α_1	-.33	-.27	-.21	-.17	-.12	-.10	-.08	-.05	0	.05	.09	.16	.22	.30	.34	
α_2	-.03	.10	.21	.37	.51	.61	.76	.83	.91	1.00	1.08	1.16	1.25	1.36	1.44	
α_n	-.0110	.0394	.0852	.1484	.2006	.2423	.3006	.3271	.3574	.3926	.4239	.4568	.4910	.5355	.5632	
α_m	-.0988	-.0964	-.0932	-.0909	-.0893	-.0879	-.0892	-.0886	-.0890	-.0882	-.0918	-.0911	-.0928	-.0973	-.1009	
α_c						.0192	.0159	.0141	.0128	.0108	.0097	.0077	.0067	.0031	.0024	
o/b	Pressure coefficient, P															
Upper surface	$R_{0.000}$	1.140	1.143	1.145	1.147	1.147	1.149	1.150	1.152	1.153	1.155	1.158	1.159	1.161	1.162	1.165
	.025	.634	.590	.556	.492	.435	.372	.304	.247	.200	.155	.089	.039	-.026	-.127	-.173
	.050	.289	.246	.204	.148	.093	.034	-.045	-.075	-.116	-.173	-.213	-.257	-.316	-.410	-.459
	.100	.102	.067	.037	-.014	-.062	-.110	-.170	-.193	-.227	-.270	-.302	-.331	-.372	-.438	-.464
	.200	-.102	-.133	-.162	-.205	-.249	-.290	-.342	-.357	-.387	-.422	-.448	-.471	-.503	-.553	-.584
	.300	-.236	-.261	-.288	-.327	-.368	-.411	-.457	-.469	-.499	-.530	-.552	-.573	-.615	-.683	-.699
	.400	-.359	-.381	-.408	-.445	-.490	-.532	-.579	-.597	-.630	-.663	-.692	-.721	-.741	-.767	-.796
	.500	-.399	-.416	-.441	-.471	-.510	-.548	-.583	-.591	-.622	-.666	-.721	-.760	-.792	-.839	-.853
	.600	-.462	-.472	-.493	-.512	-.547	-.577	-.603	-.608	-.637	-.669	-.681	-.725	-.807	-.872	-.925
	.700	-.441	-.442	-.456	-.463	-.485	-.497	-.503	-.497	-.508	-.513	-.516	-.514	-.510	-.506	-.494
	.800	-.372	-.361	-.359	-.351	-.355	-.349	-.338	-.317	-.319	-.306	-.295	-.281	-.270	-.256	-.249
.900	-.099	-.079	-.071	-.059	-.057	-.051	-.043	-.028	-.034	-.029	-.023	-.028	-.031	-.047	-.064	
.950	.073	.084	.084	.082	.076	.070	.064	.070	.058	.050	.045	.036	.023	-.003	-.027	
Lower surface	.0375	-1.562	-1.398	-1.262	-.749	-.414	-.299	-.212	-.195	-.170	-.083	.024	.023	.081	.152	.190
	.075	-.878	-.581	-.462	-.319	-.290	-.251	-.163	-.110	-.087	-.037	-.001	.028	.067	.116	.145
	.150	-.325	-.276	-.256	-.221	-.198	-.166	-.115	-.079	-.066	-.035	-.009	.014	.042	.079	.100
	.250	-.233	-.195	-.179	-.145	-.126	-.102	-.063	-.035	-.029	-.004	.014	.030	.051	.079	.095
	.350	-.176	-.143	-.129	-.103	-.089	-.072	-.040	-.016	-.013	.003	.020	.032	.050	.070	.082
	.450	-.152	-.126	-.118	-.096	-.087	-.075	-.051	-.030	-.029	-.016	-.002	.007	.021	.036	.047
	.550	-.127	-.107	-.101	-.085	-.080	-.071	-.051	-.034	-.036	-.025	-.015	-.008	.002	.014	.020
	.650	-.106	-.092	-.089	-.079	-.079	-.075	-.059	-.043	-.047	-.041	-.033	-.030	-.023	-.015	-.011
	.750	-.061	-.052	-.053	-.047	-.049	-.050	-.027	-.027	-.031	-.029	-.026	-.026	-.020	-.019	-.019
	.850	.021	.028	.027	.029	.023	.021	.025	.035	.029	.028	.031	.028	.028	.024	.023
	.925	.073	.078	.075	.074	.066	.059	.057	.067	.058	.054	.054	.050	.046	.037	.029
.975	.113	.115	.111	.106	.093	.083	.077	.062	.070	.061	.058	.048	.039	.020	.005	
$R_{1.000}$.125	.150	.150	.128	.115	.102	.098	.096	.081	.074	.060	.057	.042	.010	-.024	

^aNo orifices.



TABLE 4.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN

NACA 16-507.50 PROPELLER BLANK SECTION ($x = 0.60$; $\beta_x = 51.33^\circ$;

$\beta_{0.72R} = 45^\circ$; $B = 2$) - Continued

(e) $M = 0.60$.

J	2.112	2.148	2.192	2.229	2.275	2.307	2.348	2.387	2.431	2.477	2.533	2.567	
M_x	.814	.808	.800	.796	.794	.795	.780	.771	.766	.760	.762	.754	
α_x	3.08	2.60	2.02	1.55	.97	.58	.09	-.37	-.88	-1.40	-2.02	-2.38	
$\Delta\theta$.18	.15	.10	.05	-.02	-.07	-.14	-.19	-.25	-.30	-.37	-.42	
α_1	1.46	1.39	1.25	1.09	.95	.83	.70	.57	.45	.34	.17	.05	
c_n	.5729	.5458	.4910	.4297	.3755	.3258	.2771	.2274	.1768	.1329	.0698	.0194	
c_m	-.1259	-.1208	-.1160	-.1085	-.1059	-.1031	-.1032	-.1045	-.1065	-.1042	-.1119	-.1159	
c_c	.0182	.0162	.0154	.0159	.0165	.0177	.0191	.0200	.0219	.0232	.0254	.0265	
o/b	Pressure coefficient, P												
Upper surface	$\theta_{0.000}$	1.177	1.174	1.171	1.168	1.168	1.164	1.162	1.158	1.156	1.153	1.154	1.151
	.025	-.009	-.038	-.097	-.177	-.258	-.315	-.369	-.417	-.476	-.524	-.579	-.614
	.050	-.375	-.324	-.253	-.177	-.097	-.038	-.019	-.066	-.124	-.176	-.234	-.271
	.100	-.397	-.394	-.344	-.286	-.223	-.177	-.134	-.097	-.051	-.009	.041	.074
	.200	-.573	-.516	-.431	-.348	-.259	-.195	-.120	-.068	-.246	-.209	-.165	-.136
	.300	-.680	-.657	-.626	-.564	-.517	-.487	-.456	-.427	-.390	-.354	-.313	-.286
	.400	-.789	-.766	-.724	-.706	-.673	-.636	-.613	-.583	-.542	-.503	-.464	-.435
	.500	-.856	-.833	-.803	-.765	-.724	-.692	-.645	-.601	-.571	-.539	-.506	-.479
	.600	-.921	-.899	-.863	-.834	-.789	-.735	-.704	-.671	-.631	-.588	-.554	-.527
	.700	-.979	-.916	-.879	-.805	-.729	-.710	-.658	-.587	-.555	-.533	-.527	-.508
	.800	-.981	-.954	-.901	-.876	-.820	-.804	-.731	-.655	-.631	-.591	-.511	-.416
	.900	-.905	-.832	-.760	-.692	-.649	-.627	-.624	-.630	-.643	-.654	-.668	-.680
.950	-.849	-.771	-.700	-.642	-.601	-.630	-.647	-.666	-.666	-.674	-.676	-.680	
Lower surface	.0375	.072	.021	-.042	-.138	-.227	-.329	-.446	-.641	-1.032	-1.204	-1.360	-1.476
	.075	.103	.069	-.016	-.047	-.108	-.159	-.213	-.245	-.281	-.312	-.330	-.313
	.150	.047	.021	-.011	-.060	-.100	-.142	-.178	-.208	-.245	-.264	-.266	-.275
	.250	.077	.059	-.031	-.002	-.031	-.063	-.091	-.111	-.147	-.169	-.191	-.200
	.350	.061	.049	-.028	0	-.021	-.046	-.066	-.084	-.111	-.127	-.150	-.158
	.450	.024	.016	-.001	-.020	-.035	-.054	-.070	-.084	-.105	-.117	-.133	-.140
	.550	-.007	-.011	-.021	-.035	-.044	-.057	-.070	-.079	-.094	-.102	-.113	-.116
	.650	-.044	-.041	-.046	-.054	-.056	-.065	-.073	-.076	-.087	-.091	-.095	-.096
	.750	-.067	-.060	-.053	-.056	-.051	-.053	-.056	-.057	-.061	-.060	-.058	-.056
	.850	-.029	-.010	.001	.007	.016	.019	.019	.023	.022	.023	.028	.032
	.925	-.055	-.021	.004	.017	.033	.041	.046	.053	.056	.062	.068	.073
	.975	-.118	-.063	-.017	.007	.028	.041	.051	.064	.074	.084	.092	.098
$\theta_{1.000}$	-.160	-.099	-.032	-.012	-.012	-.043	-.053	-.076	-.082	-.101	-.106	-.109	

^aNo profiles.

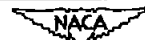


TABLE 4.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN

NACA 16-907.50 PROPELLER BLADE SECTION ($x = 0.60$; $\beta_x = 51.33^\circ$;

$\beta_{0.75R} = 45^\circ$; $B = 2$) - Concluded

(h) $M = 0.65$.

	2.448	2.403	2.388	2.350	2.313	2.299	2.264	2.235	2.202	2.183	2.162	2.125	2.116	
J	.830	.834	.841	.843	.846	.853	.856	.861	.865	.871	.877	.878	.885	
M_x	-1.07	-.96	-.98	-.06	.51	.68	1.11	1.47	1.89	2.14	2.41	2.90	3.02	
$\Delta\theta$	-.44	-.38	-.37	-.32	-.28	-.27	-.23	-.19	-.15	-.13	-.10	-.06	-.05	
α_1	.06	.19	.27	.38	.47	.52	.62	.68	.80	.86	.93	1.01	1.08	
c_n	.0232	.0748	.1058	.1484	.1852	.2045	.2419	.2658	.3155	.3374	.3645	.3929	.4219	
c_m	-1.001	-1.008	-1.016	-1.021	-1.037	-1.045	-1.021	-1.013	-1.045	-1.060	-1.083	-1.093	-1.072	
c_o	.0301	.0310	.0319	.0320	.0326	.0335	.0343	.0350	.0350	.0355	.0350	.0344	.0333	
c/b	Pressure coefficient, P													
Upper surface	0.000	1.184	1.186	1.189	1.190	1.192	1.195	1.197	1.199	1.201	1.204	1.207	1.208	1.211
	.025	.574	.540	.519	.488	.448	.432	.392	.359	.315	.296	.273	.225	.185
	.050	.239	.205	.187	.155	.115	.101	.065	.037	-.004	-.021	-.041	-.085	-.124
	.100	.074	.045	.031	.005	-.029	-.039	-.067	-.088	-.119	-.130	-.141	-.174	-.197
	.200	-.132	-.158	-.169	-.191	-.220	-.226	-.249	-.264	-.286	-.294	-.297	-.330	-.355
	.300	-.273	-.296	-.304	-.322	-.349	-.354	-.387	-.414	-.435	-.438	-.438	-.455	-.469
	.400	-.433	-.451	-.461	-.487	-.512	-.513	-.522	-.527	-.550	-.556	-.557	-.572	-.585
	.500	-.515	-.536	-.545	-.560	-.586	-.590	-.610	-.625	-.632	-.635	-.634	-.654	-.660
	.600	-.617	-.649	-.649	-.669	-.693	-.695	-.712	-.720	-.732	-.736	-.733	-.749	-.759
	.700	-.706	-.749	-.760	-.772	-.791	-.791	-.804	-.815	-.826	-.827	-.823	-.835	-.830
	.800	-.297	-.308	-.311	-.313	-.320	-.324	-.336	-.335	-.369	-.384	-.379	-.350	-.387
	.900	-.075	-.111	-.140	-.163	-.197	-.217	-.242	-.267	-.286	-.300	-.302	-.319	-.327
.950	-.016	-.054	-.089	-.116	-.163	-.197	-.233	-.267	-.291	-.307	-.309	-.327	-.335	
Lower surface	.0375	-.962	-.915	-.841	-.767	-.682	-.603	-.456	-.326	-.210	-.155	-.078	-.017	.060
	.075	-.911	-.848	-.765	-.672	-.542	-.456	-.319	-.247	-.135	-.098	-.051	-.023	.016
	.150	-.627	-.594	-.293	-.206	-.170	-.199	-.138	-.117	-.076	-.053	-.020	-.001	.033
	.250	-.183	-.171	-.162	-.150	-.136	-.120	-.099	-.082	-.048	-.028	.001	.014	.042
	.350	-.157	-.152	-.143	-.130	-.117	-.103	-.087	-.071	-.042	-.027	-.001	.009	.030
	.450	-.166	-.162	-.155	-.143	-.135	-.123	-.110	-.100	-.075	-.062	-.037	-.030	-.012
	.550	-.165	-.163	-.158	-.149	-.145	-.137	-.129	-.124	-.103	-.092	-.069	-.065	-.048
	.650	-.165	-.168	-.169	-.160	-.164	-.161	-.159	-.159	-.144	-.136	-.114	-.114	-.097
	.750	-.133	-.142	-.142	-.143	-.152	-.155	-.161	-.167	-.159	-.156	-.137	-.139	-.126
	.850	-.044	-.059	-.063	-.070	-.087	-.095	-.109	-.122	-.118	-.118	-.104	-.109	-.099
	.925	-.002	-.023	-.034	-.046	-.072	-.088	-.110	-.130	-.135	-.139	-.128	-.134	-.127
	.975	.020	-.011	-.033	-.057	-.101	-.132	-.172	-.207	-.226	-.239	-.236	-.249	-.246
1.000	.032	-.009	-.035	-.059	-.124	-.187	-.228	-.272	-.309	-.319	-.323	-.344	-.355	

^aNo orifice.



TABLE 5.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN
NACA 16-306.62 PROPELLER BLADE SECTION ($\alpha = 0.70$; $\beta_x = 47.00^\circ$;

$$\beta_{0.72R} = 45^\circ; B = 2)$$

(a) $N = 1140$ rpm.

	1.608	1.766	1.945	2.139	2.254	2.367	2.514	2.654	2.592	2.443	2.321	2.195	2.066	1.875	1.667	
J	.473	.487	.507	.532	.546	.562	.579	.598	.587	.570	.552	.538	.521	.501	.478	
M_x	10.83	8.23	5.51	2.79	1.29	-.11	-1.82	-3.35	-2.69	-1.01	.46	2.05	3.79	6.55	9.84	
α_x^1	.74	.62	.48	.33	.22	.11	-.05	-.22	-.15	.03	.16	.27	.39	.54	.69	
$\Delta\theta$	2.97	2.69	2.13	1.57	1.21	.87	.48	.06	.88	.65	1.00	1.38	1.78	2.35	2.89	
c_n	1.0445	.9568	.7639	.5645	.4400	.3158	.1752	.0213	.1032	.2371	.3613	.4968	.6387	.8374	1.0219	
c_m	-.0465	-.0634	-.0829	-.0928	-.0944	-.0955	-.0950	-.1062	-.0990	-.0925	-.0928	-.0933	-.0887	-.0757	-.0503	
c/b	Pressure coefficient, P															
Upper surface	r^0 .000	1.057	1.061	1.066	1.072	1.076	1.081	1.086	1.092	1.088	1.083	1.078	1.074	1.070	1.064	1.059
	.025	-2.456	-2.495	-1.220	-.517	-.143	1.162	.429	.593	.533	.321	-.326	-.776	-1.531	-2.639	
	.050	-2.250	-2.162	-1.268	-.714	-.427	-.180	.072	.245	.180	-.036	-.263	-.573	-.909	-1.430	-2.349
	.100	-1.824	-1.299	-.933	-.627	-.436	-.269	-.081	.063	.006	-.162	-.327	-.534	-.758	-1.096	-1.689
	.200	-1.233	-.923	-.782	-.579	-.453	-.340	-.210	-.101	-.142	-.265	-.378	-.517	-.658	-.860	-1.096
	.300	-.899	-.808	-.706	-.570	-.478	-.401	-.298	-.211	-.245	-.342	-.428	-.526	-.626	-.757	-.886
	.400	-.710	-.716	-.649	-.552	-.484	-.429	-.354	-.282	-.307	-.384	-.447	-.517	-.594	-.683	-.702
	.500	-.574	-.639	-.606	-.541	-.491	-.450	-.392	-.342	-.355	-.418	-.463	-.517	-.571	-.624	-.598
	.600	-.466	-.558	-.549	-.512	-.478	-.454	-.411	-.373	-.383	-.427	-.461	-.495	-.535	-.575	-.502
	.700	-.363	-.471	-.497	-.492	-.474	-.464	-.438	-.417	-.419	-.447	-.467	-.487	-.503	-.487	-.401
	.800	-.265	-.299	-.339	-.357	-.351	-.356	-.346	-.339	-.333	-.344	-.352	-.356	-.356	-.319	-.263
.900	-.189	-.113	-.116	-.149	-.154	-.169	-.177	-.185	-.172	-.119	-.163	-.154	-.140	-.103	-.135	
.950	-.154	-.031	.010	.015	.018	.009	.005	-.007	.007	.012	.013	.017	.011	-.005	-.087	
Lower surface	.0375	.779	.689	.522	.236	.043	-.192	-.511	-1.159	-.924	-.330	-.103	.143	.342	.607	.748
	.075	.640	.557	.413	.192	.052	-.117	-.298	-.904	-.527	-.210	-.055	.126	.271	.484	.610
	.150	.505	.434	.320	.161	.058	-.052	-.173	-.393	-.224	-.115	-.004	.113	.214	.376	.477
	.250	.407	.347	.263	.136	.067	-.015	-.104	-.189	-.133	-.059	.013	.102	.180	.307	.384
	.350	.323	.281	.203	.099	.045	-.023	-.093	-.134	-.108	-.057	0	.070	.127	.241	.307
	.450	.255	.209	.132	.052	.014	-.041	-.097	-.120	-.105	-.071	-.022	.033	.077	.172	.237
	.550	.201	.178	.137	.072	.039	-.007	-.047	-.069	-.054	-.028	.009	.054	.091	.157	.195
	.650	.136	.127	.096	.048	.024	-.011	-.041	-.052	-.041	-.028	0	.035	.059	.113	.136
	.750	.101	.112	.094	.061	.045	-.017	-.001	-.007	.002	.008	.027	.052	.068	.103	.110
	.850	.068	.102	.099	.085	.077	.060	.051	.048	.056	.055	.057	.083	.084	.101	.088
	.925	.060	.117	.129	.140	.132	.121	.114	.108	.118	.121	.125	.130	.123	.125	.088
.975	.142	.191	.203	.221	.244	.235	.237	.238	.245	.237	.236	.217	.210	.192	.179	
r^1 1.000	.235	.248	.250	.225	.228	.232	.263	.238	.238	.230	.240	.227	.271	.308	.279	

¹No orifice.

NACA

TABLE 5.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN

NACA 16-506.62 PROPELLER BLADE SECTION ($\alpha = 0.70$; $\beta_x = 47.00^\circ$;

$\beta_{0.75R} = 45^\circ$; $B = 2$) - Continued.

(b) $N = 1350$ rpm.

	1.663	1.786	1.885	1.984	2.095	2.209	2.312	2.438	2.547	2.637	2.584	2.486	2.371	2.249	2.162	2.068	1.958	1.845	1.734	
J	1.663	1.786	1.885	1.984	2.095	2.209	2.312	2.438	2.547	2.637	2.584	2.486	2.371	2.249	2.162	2.068	1.958	1.845	1.734	
M_{x_1}	.969	.580	.998	.606	.625	.642	.656	.676	.695	.708	.700	.684	.664	.644	.631	.618	.603	.587	.572	
q_{x_1}	9.90	7.92	6.40	4.94	3.39	1.87	.57	-.95	-2.19	-3.17	-2.60	-1.51	-.16	1.36	2.49	3.76	5.32	7.00	8.74	
ΔB	1.12	.93	.77	.62	.45	.27	.10	-.09	-.26	-.39	-.32	-.17	.01	.21	.34	.49	.66	.84	1.01	
α_1	3.00	2.82	2.57	2.15	1.77	1.43	1.06	.69	.34	.07	.24	.51	.89	1.26	1.61	1.96	2.31	2.73	3.02	
c_{D1}	1.0639	1.0052	.9168	.7710	.6374	.5174	.3852	.2516	.1226	.0245	.0890	.1892	.3219	.4581	.5810	.7039	.8277	.9742	1.0742	
c_c	-.0452	-.0598	-.0744	-.0847	-.0944	-.0991	-.1006	-.1031	-.1082	-.1167	-.1091	-.1032	-.0989	-.0992	-.0950	-.0860	-.0821	-.0633	-.0519	
c/b	Pressure coefficient, P																			
Upper surface	0.000	1.083	1.087	1.092	1.095	1.101	1.107	1.112	1.120	1.127	1.133	1.130	1.123	1.115	1.108	1.103	1.099	1.094	1.089	1.084
	.025	-2.235	-2.939	-2.278	-1.103	-.663	-.248	.096	.361	.538	.633	.581	.460	.235	-.094	-.412	-.823	-1.221	-1.641	-2.241
	.050	-2.169	-2.693	-1.487	-1.328	-.903	-.563	-.264	-.014	.171	.276	.219	.086	-.137	-.430	-.699	-1.028	-1.470	-2.239	-2.947
	.100	-1.979	-1.252	-1.190	-.996	-.773	-.555	-.346	-.157	-.010	.081	.089	-.081	-.253	-.466	-.642	-.854	-1.065	-1.168	-1.624
	.200	-1.350	-.980	-.929	-.815	-.687	-.555	-.415	-.282	-.175	-.102	-.143	-.226	-.351	-.499	-.608	-.728	-.847	-.963	-.978
	.300	-.888	-.868	-.829	-.749	-.667	-.574	-.477	-.375	-.289	-.232	-.265	-.330	-.429	-.535	-.610	-.688	-.774	-.846	-.876
	.400	-.700	-.765	-.741	-.689	-.632	-.568	-.501	-.428	-.364	-.320	-.344	-.395	-.467	-.543	-.593	-.646	-.707	-.749	-.770
	.500	-.592	-.684	-.678	-.649	-.613	-.571	-.523	-.468	-.425	-.394	-.413	-.446	-.498	-.555	-.584	-.620	-.658	-.679	-.679
	.600	-.484	-.589	-.601	-.587	-.571	-.545	-.515	-.479	-.453	-.437	-.446	-.464	-.498	-.535	-.550	-.577	-.586	-.596	-.581
	.700	-.376	-.491	-.525	-.532	-.533	-.529	-.517	-.498	-.492	-.490	-.493	-.495	-.508	-.528	-.530	-.526	-.535	-.509	-.475
	.800	-.256	-.395	-.334	-.351	-.368	-.373	-.374	-.367	-.372	-.380	-.376	-.368	-.371	-.378	-.370	-.375	-.349	-.316	-.286
	.900	-.162	-.086	-.096	-.107	-.125	-.139	-.146	-.150	-.164	-.177	-.169	-.157	-.148	-.146	-.132	-.114	-.106	-.089	-.097
.950	-.122	-.017	-.004	.015	.023	.028	.029	.034	.026	.015	.021	.032	.030	.024	.029	.022	.008	-.007	-.030	
Lower surface	.0375	.767	.700	.601	.468	.304	.112	-.120	-.357	-.948	-1.202	-1.082	-.584	-.242	.014	.201	.369	.511	.650	.742
	.075	.633	.569	.482	.372	.242	.104	-.066	-.229	-.548	-.936	-.749	-.323	-.148	.031	.169	.297	.406	.523	.608
	.150	.499	.447	.376	.293	.201	.095	-.014	-.121	-.236	-.474	-.306	-.178	-.068	.044	.145	.238	.319	.411	.478
	.250	.415	.366	.308	.241	.168	.095	.013	-.064	-.145	-.231	-.169	-.106	-.024	.057	.130	.200	.261	.335	.392
	.350	.323	.291	.234	.179	.120	.066	.001	-.059	-.119	-.157	-.132	-.091	-.030	.032	.091	.145	.195	.258	.313
	.450	.245	.220	.159	.118	.071	.024	-.025	-.072	-.114	-.131	-.125	-.097	-.049	-.002	.044	.091	.130	.182	.240
	.550	.205	.190	.159	.125	.084	.049	.007	-.026	-.063	-.078	-.070	-.047	-.011	.026	.068	.104	.134	.177	.207
	.650	.144	.140	.113	.088	.059	.031	.001	-.026	-.048	-.056	-.054	-.039	-.016	.011	.044	.072	.096	.129	.150
	.750	.112	.119	.104	.088	.067	.049	.026	.011	-.004	-.006	-.006	.003	.017	.034	.059	.079	.094	.116	.128
	.850	.084	.111	.104	.097	.084	.079	.068	.063	.052	.050	.050	.057	.061	.070	.084	.095	.097	.108	.112
	.925	.080	.125	.126	.129	.129	.132	.125	.127	.115	.109	.114	.115	.124	.122	.132	.133	.130	.127	.124
	.975	.132	.163	.182	.197	.203	.218	.230	.239	.241	.239	.238	.241	.234	.220	.213	.205	.192	.173	.175
1.000	.235	.191	.189	.241	.249	.263	.222	.227	.236	.275	.331	.499	.330	.300	.268	.269	.252	.215	.215	

^aNo orifice.



TABLE 5.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN

NACA 16-506.62 PROPELLER BLADE SECTION ($x = 0.70$; $\beta_x = 47.00^\circ$;

$\beta_{0.75R} = 45^\circ$; $B = 2$) - Continued

(c) $N = 1500$ rpm.

	1.962	2.051	2.130	2.212	2.315	2.388	2.475	2.595	2.528	2.436	2.341	2.267	2.173	2.096	2.013	
J	1.962	2.051	2.130	2.212	2.315	2.388	2.475	2.595	2.528	2.436	2.341	2.267	2.173	2.096	2.013	
M_x	.667	.680	.696	.709	.728	.740	.756	.777	.765	.746	.731	.715	.700	.687	.671	
α_x	5.26	4.00	2.91	1.83	.53	-.36	-1.38	-2.72	-1.98	-.93	.21	1.13	2.34	3.37	4.32	
$\Delta\beta$.95	.74	.56	.38	.12	-.05	-.25	-.59	-.39	-.15	.06	.24	.46	.63	.83	
α_1	2.51	2.17	1.80	1.46	1.14	.84	.49	-.07	.31	.69	1.00	1.27	1.59	1.92	2.26	
c_n	.9032	.7794	.6510	.5274	.4132	.3068	.1800	-.0245	.1116	.2526	.3639	.4600	.5735	.6929	.8129	
c_m	-.0705	-.0898	-.0991	-.1023	-.1042	-.1074	-.1144	-.1332	-.1183	-.1099	-.1057	-.1016	-.1012	-.0988	-.0867	
c/b	Pressure coefficient, P															
Upper surface	β_0 .000	1.116	1.121	1.128	1.133	1.140	1.145	1.152	1.160	1.155	1.148	1.141	1.135	1.129	1.124	1.118
	.025	-1.418	-.817	-.458	-.135	-.146	.334	.499	.643	.429	.226	.011	-.284	-.625	-.825	-1.041
	.050	-1.397	-1.159	-.830	-.515	-.241	-.059	.120	.287	.042	-.161	-.372	-.654	-.994	-1.277	-1.538
	.100	-1.457	-.938	-.750	-.549	-.345	-.205	-.089	.089	.014	-.125	-.288	-.443	-.644	-.832	-1.138
	.200	-1.102	-.972	-.723	-.590	-.450	-.335	-.236	-.118	-.176	-.291	-.413	-.523	-.647	-.778	-.948
	.300	-.848	-.787	-.713	-.632	-.529	-.453	-.361	-.257	-.308	-.403	-.497	-.580	-.672	-.740	-.808
	.400	-.760	-.720	-.675	-.624	-.555	-.503	-.437	-.348	-.397	-.467	-.534	-.590	-.650	-.694	-.736
	.500	-.706	-.686	-.662	-.635	-.590	-.562	-.518	-.453	-.487	-.536	-.576	-.611	-.648	-.670	-.692
	.600	-.623	-.616	-.605	-.594	-.568	-.559	-.541	-.509	-.525	-.547	-.564	-.579	-.600	-.607	-.615
	.700	-.548	-.557	-.560	-.567	-.558	-.566	-.574	-.592	-.578	-.568	-.564	-.562	-.566	-.555	-.548
	.800	-.438	-.432	-.439	-.438	-.436	-.437	-.431	-.431	-.438	-.436	-.437	-.436	-.436	-.435	-.434
	.900	-.093	-.098	-.103	-.111	-.108	-.113	-.120	-.119	-.119	-.116	-.111	-.110	-.108	-.098	-.093
.950	.004	.009	.020	.025	.040	.041	.043	.047	.048	.044	.039	.033	.021	.018	.008	
Lower surface	.0375	.513	.378	.238	.064	-.133	-.318	-1.031	-1.541	-1.447	-.424	-.216	-.031	.150	.314	.444
	.075	.413	.306	.197	.066	-.072	-.206	-.315	-1.396	-.744	-.265	-.127	0	.131	.255	.357
	.150	.327	.244	.166	.072	-.014	-.102	-.188	-.536	-.220	-.155	-.050	.031	.117	.208	.285
	.250	.246	.209	.153	.082	-.038	-.088	-.119	-.178	-.149	-.100	-.027	.036	.099	.167	.227
	.350	.205	.150	.104	.049	-.001	-.050	-.109	-.125	-.127	-.078	-.020	.025	.075	.131	.178
	.450	.126	.082	.044	0	-.032	-.074	-.120	-.139	-.138	-.097	-.054	-.016	.019	.066	.104
	.550	.140	.103	.073	.033	-.007	-.027	-.063	-.087	-.075	-.044	-.009	.021	.051	.089	.121
	.650	.099	.070	.047	.015	-.004	-.029	-.056	-.073	-.064	-.040	-.017	.007	.028	.060	.085
	.750	.096	.076	.060	.036	.026	.008	-.010	-.021	-.015	0	.016	.003	.044	.070	.086
	.850	.099	.088	.078	.066	.063	.053	.044	.038	.042	.054	.058	.064	.072	.086	.094
	.925	.127	.124	.123	.116	.121	.114	.110	.107	.111	.114	.116	.119	.118	.095	.127
	.975	.180	.186	.195	.197	.211	.219	.231	.236	.238	.231	.222	.214	.195	.194	.186
1.000	.235	.232	.240	.262	.275	.300	.320	.320	.338	.325	.298	.266	.248	.297	.250	

^aNo orifice.



TABLE 5.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN

NACA 16-506.62 PROPELLER BLADE SECTION ($x = 0.70$; $\beta_x = 47.00^\circ$;

$\beta = 45^\circ$; $B = 2$) - Continued
0.75B

(d) $N = 1600$ rpm.

	2.071	2.144	2.212	2.290	2.370	2.450	2.536	2.480	2.418	2.329	2.259	2.183	2.100	
J	2.071	2.144	2.212	2.290	2.370	2.450	2.536	2.480	2.418	2.329	2.259	2.183	2.100	
M_x	.789	.745	.756	.771	.787	.804	.821	.809	.796	.777	.763	.748	.736	
α_x'	3.72	2.73	1.83	.84	-.14	-1.09	-2.07	-1.44	-.71	.36	1.23	2.21	3.32	
$\Delta\theta$.71	.53	.35	.14	-.09	-.35	-.65	-.47	-.24	.03	.23	.43	.64	
α_1	2.09	1.76	1.52	1.22	.93	.47	0	.27	.68	1.06	1.33	1.62	1.93	
c_n	.7548	.6348	.5484	.4445	.3368	.1710	-.0013	.0968	.2484	.3845	.4839	.5839	.6961	
c_m	-.0967	-.1006	-.1067	-.1111	-.1139	-.1247	-.1308	-.1250	-.1185	-.1119	-.1080	-.1032	-.0977	
c_c						.0226	.0285	.0244						
c/b	Pressure coefficient, P													
Upper surface	$a_{0.000}$	1.141	1.147	1.152	1.158	1.165	1.172	1.180	1.174	1.168	1.160	1.154	1.148	1.143
	.025	-.584	-.278	-.044	.186	.383	.528	.625	.574	.466	.291	.092	-.138	-.435
	.050	-.948	-.705	-.454	-.218	-.013	.151	.268	.206	.081	-.110	-.311	-.549	-.855
	.100	-.990	-.693	-.517	-.337	-.173	-.030	.077	.019	-.091	-.252	-.410	-.592	-.791
	$b_{.200}$	-.957	-.742	-.622	-.490	-.349	-.221	-.128	-.189	-.278	-.405	-.543	-.672	-.820
	.300	-.878	-.767	-.693	-.584	-.473	-.366	-.275	-.325	-.410	-.524	-.629	-.727	-.835
	.400	-.765	-.729	-.674	-.607	-.532	-.449	-.370	-.416	-.484	-.568	-.637	-.701	-.759
	.500	-.742	-.737	-.715	-.671	-.613	-.552	-.487	-.527	-.580	-.643	-.694	-.729	-.749
	.600	-.630	-.649	-.703	-.766	-.745	-.687	-.613	-.657	-.712	-.756	-.730	-.673	-.643
	.700	-.549	-.566	-.580	-.599	-.688	-.760	-.719	-.749	-.720	-.619	-.590	-.579	-.563
	.800	-.320	-.332	-.341	-.341	-.341	-.338	-.351	-.344	-.338	-.342	-.344	-.340	-.332
.900	-.070	-.073	-.076	-.073	-.073	-.065	-.073	-.073	-.071	-.073	-.077	-.078	-.076	
.950	-.022	.026	.027	.034	.036	.039	.044	.040	.042	.037	.031	.024	.021	
Lower surface	$a_{0.375}$.347	.193	.046	-.142	-.315	-1.196	-1.304	-1.286	-.988	-.257	-.061	.108	.272
	.075	.286	.167	.054	-.075	-.225	-.909	-1.190	-1.159	-.256	-.153	-.023	.102	.226
	.150	.234	.147	.070	-.015	-.120	-.175	-.956	-.343	-.156	-.065	.022	.101	.191
	$b_{.250}$.183	.124	.075	-.003	-.083	-.132	-.250	-.164	-.120	-.039	.030	.080	.166
	.350	.153	.100	.052	.002	-.061	-.118	-.118	-.128	-.091	-.027	.020	.069	.124
	.450	.085	.042	.004	-.034	-.084	-.136	-.138	-.145	-.110	-.058	-.021	.015	.061
	.550	.108	.071	.037	.005	-.011	-.075	-.090	-.087	-.053	-.016	.016	.048	.087
	.650	.075	.044	.019	-.007	-.013	-.069	-.082	-.081	-.053	-.024	.001	.025	.057
	.750	.083	.060	.041	.023	0	-.021	-.029	-.029	-.008	.012	.028	.044	.068
	.850	.096	.083	.071	.062	.049	.034	.029	.028	.044	.054	.063	.070	.087
	.925	.134	.128	.121	.119	.109	.101	.100	.097	.107	.115	.116	.120	.128
.975	.189	.194	.197	.203	.205	.203	.233	.224	.215	.206	.199	.193	.189	
$a_{1.000}$.230	.240	.240	.260	.270	.340	.330	.320	.310	.265	.260	.250	.250	

^aNo orifice.
^bPaired value.



TABLE 5.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN
MACA 16-506.62 PROPELLER BLADE SECTION ($\alpha = 0.70$; $\beta_x = 47.00^\circ$;

$\beta_{0.75R} = 45^\circ$; $B = 2$) - Continued

(e) $M = 0.56$.

J	2.116	2.156	2.179	2.206	2.241	2.276	2.304	2.362	2.388	2.424	2.468	2.512	2.552	2.622	
M_x	.818	.813	.805	.796	.791	.786	.778	.779	.772	.763	.761	.755	.750	.741	
α_x'	3.10	2.57	2.26	1.91	1.46	1.01	.66	-.05	-.36	-.79	-1.30	-1.80	-2.25	-3.01	
$\Delta\delta$.30	.17	.12	.07	.04	.02	.01	-.06	-.11	-.18	-.27	-.34	-.38	-.43	
α_1	1.77	1.69	1.57	1.50	1.34	1.23	1.13	.92	.79	.67	.52	.37	.22	.03	
c_n	.6400	.6110	.5652	.5432	.4877	.4477	.4123	.3326	.2877	.2442	.1910	.1348	.0813	.0097	
c_m	-.1314	-.1278	-.1236	-.1226	-.1177	-.1145	-.1129	-.1108	-.1084	-.1091	-.1096	-.1150	-.1152	-.1173	
c_c	.0070	.0070	.0066												
c/p	Pressure coefficient, P														
Upper surface	0.000	1.179	1.176	1.173	1.169	1.166	1.164	1.161	1.161	1.158	1.155	1.154	1.151	1.149	1.146
	.025	-.039	.012	.057	.090	.160	.206	.259	.363	.415	.455	.507	.590	.593	.697
	.050	-.484	-.427	-.371	-.335	-.257	-.206	-.148	-.037	.021	.064	.125	.172	.225	.301
	.100	-.509	-.486	-.454	-.429	-.367	-.327	-.281	-.188	-.139	-.105	-.050	-.011	.035	.103
	.200	-.599	-.581	-.574	-.568	-.512	-.477	-.437	-.359	-.319	-.288	-.239	-.205	-.165	-.104
	.300	-.682	-.653	-.640	-.631	-.604	-.592	-.557	-.483	-.441	-.413	-.364	-.331	-.294	-.236
	.400	-.762	-.729	-.695	-.671	-.628	-.598	-.583	-.534	-.499	-.473	-.428	-.401	-.368	-.318
	.500	-.815	-.794	-.777	-.769	-.726	-.694	-.659	-.620	-.586	-.555	-.507	-.481	-.448	-.400
	.600	-.931	-.910	-.889	-.865	-.793	-.787	-.771	-.674	-.596	-.573	-.533	-.513	-.485	-.446
	.700	-.782	-.825	-.827	-.813	-.793	-.696	-.623	-.602	-.599	-.592	-.565	-.566	-.536	-.508
	.800	-.340	-.310	-.292	-.292	-.298	-.312	-.334	-.348	-.359	-.367	-.367	-.374	-.373	-.372
.900	-.197	-.148	-.109	-.091	-.073	-.066	-.071	-.075	-.087	-.098	-.105	-.118	-.130	-.149	
.950	-.136	-.083	-.037	-.018	.002	.019	.033	.044	.050	.048	.053	.047	.045	.034	
Lower surface	.0375	.145	.094	.036	-.003	-.082	-.139	-.210	-.302	-.352	-.360	-.975	-1.335	-1.527	-1.722
	.075	.135	.097	.054	.024	-.032	-.070	-.119	-.201	-.235	-.252	-.293	-.439	-.634	-.898
	.150	.135	.108	.077	.056	.017	-.009	-.042	-.097	-.129	-.156	-.174	-.189	-.222	-.360
	.250	.090	.080	.060	.046	.022	.006	-.017	-.056	-.079	-.102	-.119	-.142	-.153	-.191
	.350	.085	.070	.053	.037	.016	.001	-.017	-.047	-.064	-.083	-.096	-.117	-.129	-.155
	.450	.024	.013	0	-.011	-.025	-.036	-.052	-.072	-.084	-.099	-.110	-.128	-.137	-.153
	.550	.048	.041	.031	.021	.010	.001	-.009	-.024	-.033	-.045	-.051	-.066	-.073	-.083
	.650	.013	.012	.005	-.001	-.010	-.013	-.020	-.029	-.033	-.042	-.044	-.055	-.061	-.064
	.750	.024	.026	.023	.021	.017	.016	.014	.009	.005	0	.001	-.008	-.009	-.011
	.850	.038	.046	.025	.051	.052	.055	.055	.054	.055	.051	.056	.050	.049	.049
	.925	.073	.085	.094	.098	.105	.110	.111	.115	.117	.114	.119	.114	.114	.114
.975	.178	.186	.191	.192	.195	.200	.202	.209	.213	.214	.224	.224	.226	.236	
1.000	.238	.261	.260	.270	.265	.278	.272	.280	.285	.305	.305	.340	.365	.390	

*No orifice.



TABLE 5.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN

NACA 16-506.62 PROPELLER BLADE SECTION ($\alpha = 0.70$; $\beta_x = 47.00^\circ$;

$\beta_{0.75R} = 45^\circ$; B = 2) - Continued

(r) M = 0.58.

J	2.609	2.570	2.528	2.487	2.446	2.407	2.376	2.337	2.297	2.271	2.234	2.208	2.167	2.137	
M_{x_1}	.768	.775	.781	.786	.792	.798	.805	.809	.813	.819	.826	.833	.838	.844	
α_{x_1}	-2.87	-2.45	-1.98	-1.32	-1.04	-.58	-.21	.26	.75	1.08	1.55	1.88	2.42	2.82	
ΔB	-.64	-.55	-.45	-.38	-.31	-.27	-.26	-.23	-.16	-.09	.03	.12	.25	.35	
α_1	-.11	-.01	.15	.30	.46	.58	.72	.86	.99	1.10	1.22	1.35	1.48	1.52	
c_H	-.0394	-.0026	.0529	.1090	.1677	.2103	.2619	.3135	.3600	.3974	.4394	.4858	.5342	.5471	
c_H	-.1163	-.1177	-.1154	-.1124	-.1121	-.1134	-.1108	-.1082	-.1075	-.1119	-.1173	-.1214	-.1272	-.1377	
c_c							.0174	.0162	.0143	.0136	.0142	.0148	.0145	.0138	
c/b	Pressure coefficient, P														
Upper surface	^a 0.000	1.157	1.160	1.162	1.164	1.167	1.169	1.172	1.175	1.177	1.179	1.182	1.185	1.188	1.191
	.025	.654	.621	.588	.552	.507	.462	.421	.373	.321	.275	.233	.200	.125	.089
	.050	.254	.216	.175	.130	.076	.022	-.027	-.085	-.145	-.201	-.249	-.295	-.389	-.444
	.100	.116	.083	.051	.014	-.029	-.071	-.108	-.153	-.197	-.234	-.267	-.293	-.349	-.376
	.200	-.097	-.126	-.156	-.189	-.229	-.267	-.299	-.338	-.376	-.412	-.449	-.476	-.505	-.522
	.300	-.225	-.254	-.280	-.312	-.348	-.384	-.415	-.453	-.490	-.507	-.525	-.540	-.570	-.593
	.400	-.319	-.346	-.373	-.402	-.437	-.467	-.489	-.506	-.519	-.533	-.569	-.598	-.633	-.660
	.500	-.409	-.436	-.466	-.497	-.537	-.553	-.576	-.609	-.629	-.650	-.670	-.680	-.713	-.732
	.600	-.463	-.488	-.516	-.546	-.614	-.687	-.712	-.715	-.741	-.743	-.785	-.801	-.828	-.848
	.700	-.462	-.471	-.484	-.505	-.530	-.579	-.619	-.633	-.642	-.632	-.691	-.709	-.710	-.738
	.800	-.365	-.361	-.357	-.347	-.342	-.327	-.308	-.300	-.299	-.313	-.341	-.359	-.366	-.378
.900	-.136	-.122	-.111	-.097	-.089	-.077	-.072	-.076	-.085	-.110	-.154	-.203	-.247	-.289	
.950	.046	.052	.055	.058	.052	.048	.036	.015	-.006	-.038	-.089	-.143	-.201	-.262	
Lower surface	.0375	-1.582	-1.460	-1.377	-1.306	-1.213	-1.066	-.740	-.420	-.309	-.222	-.164	-.106	-.022	.019
	.075	-1.160	-1.144	-1.013	-.756	-.547	-.359	-.269	-.217	-.156	-.104	-.065	-.023	.036	.065
	.150	-.505	-.423	-.358	-.263	-.213	-.162	-.137	-.104	-.062	-.026	-.001	.030	.067	.066
	.250	-.305	-.235	-.204	-.162	-.142	-.114	-.092	-.063	-.032	-.004	.013	.035	.064	.078
	.350	-.203	-.167	-.149	-.124	-.112	-.096	-.079	-.058	-.034	-.016	-.003	.015	.038	.047
	.450	-.156	-.142	-.133	-.120	-.113	-.103	-.091	-.075	-.059	-.045	-.041	-.024	-.008	-.002
	.550	-.088	-.083	-.079	-.070	-.068	-.060	-.053	-.042	-.028	-.017	-.014	-.003	.007	.010
	.650	-.063	-.064	-.063	-.057	-.058	-.055	-.052	-.046	-.038	-.031	-.031	-.026	-.020	-.022
	.750	-.010	-.011	-.012	-.008	-.012	-.012	-.012	-.011	-.006	-.002	-.002	-.008	-.007	-.014
	.850	.048	.047	.045	.047	.042	.040	.036	.034	.033	.031	.021	.017	.006	-.009
	.925	.112	.112	.110	.112	.106	.104	.098	.092	.088	.081	.065	.054	.035	.015
.975	.210	.210	.206	.207	.199	.195	.189	.187	.185	.184	.174	.173	.160	.143	
^a 1.000	.270	.270	.250	.250	.250	.250	.240	.250	.260	.255	.250	.270	.265	.298	

^aNo orifice.
^bFaired value.



TABLE 5.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN

NACA 16-506.62 PROPELLER BLADE SECTION ($x = 0.70$; $\beta_x = 47.00^\circ$;

$\beta_{0.75R} = 45^\circ$; $B = 2$) - Continued

(a) $M = 0.60$.

α	2.553	2.528	2.489	2.460	2.419	2.377	2.338	2.311	2.281	2.246	2.220	2.197	2.164	2.128	2.106	
M_x	.796	.806	.811	.820	.826	.828	.830	.839	.849	.851	.856	.863	.870	.869	.873	
$\Delta \beta$	-2.26	-1.98	-1.54	-1.20	-.73	-.23	.58	.95	1.40	1.73	2.03	2.46	2.94	3.24	3.24	
c_f	-.14	-.03	.11	.21	.32	.49	.79	.82	.95	1.03	1.14	1.24	1.31	1.39	1.39	
$c_{f,1}$	-.0497	-.0103	.0406	.0768	.1174	.1774	.2535	.2953	.3439	.3710	.4097	.4465	.4735	.4994	.4994	
$c_{f,2}$	-.1132	-.1091	-.1118	-.1080	-.1091	-.1078	-.1096	-.1114	-.1108	-.1118	-.1137	-.1147	-.1180	-.1249	-.1249	
c_c		.0241	.0233	.0222	.0247	.0204	.0210	.0216	.0220	.0212	.0208	.0210	.0211	.0208	.0203	
c/b	Pressure coefficient, P															
Upper surface	0.000	1.169	1.173	1.175	1.180	1.182	1.183	1.184	1.188	1.193	1.194	1.196	1.200	1.203	1.203	1.205
	.025	.633	.607	.578	.554	.520	.474	.446	.417	.389	.337	.298	.261	.223	.184	.148
	.050	.211	.199	.163	.134	.092	.036	-.001	-.034	-.070	-.132	-.177	-.223	-.278	-.322	-.380
	.100	.099	.073	.044	.022	-.012	-.055	-.083	-.107	-.132	-.177	-.209	-.237	-.267	-.296	-.317
	.200	-.117	-.138	-.166	-.184	-.213	-.252	-.279	-.298	-.322	-.367	-.404	-.419	-.449	-.438	-.452
	.300	-.249	-.268	-.295	-.311	-.339	-.374	-.403	-.421	-.429	-.458	-.477	-.487	-.509	-.528	-.531
	.400	-.350	-.368	-.392	-.406	-.427	-.446	-.452	-.460	-.482	-.513	-.540	-.559	-.573	-.599	-.615
	.500	-.455	-.475	-.498	-.501	-.522	-.553	-.570	-.575	-.587	-.611	-.627	-.642	-.658	-.674	-.676
	.600	-.529	-.566	-.625	-.644	-.663	-.670	-.697	-.690	-.697	-.737	-.746	-.775	-.774	-.790	-.793
	.700	-.358	-.375	-.428	-.463	-.490	-.510	-.525	-.532	-.538	-.552	-.574	-.586	-.604	-.623	-.629
	.800	-.350	-.340	-.333	-.316	-.320	-.323	-.344	-.356	-.361	-.356	-.352	-.354	-.372	-.391	-.402
	.900	-.102	-.089	-.080	-.073	-.085	-.102	-.138	-.172	-.214	-.244	-.274	-.297	-.325	-.348	-.359
.950	.053	.053	.047	.038	0	-.028	-.074	-.119	-.176	-.214	-.255	-.286	-.322	-.346	-.359	
Lower surface	.0375	-1.404	-1.327	-1.272	-1.223	-1.163	-1.106	-1.039	-.850	-.563	-.304	-.244	-.188	-.138	-.079	-.027
	.075	-1.336	-1.256	-1.181	-1.110	-.927	-.527	-.338	-.235	-.202	-.161	-.130	-.075	-.015	.014	.057
	.150	-.828	-.684	-.539	-.368	-.239	-.173	-.156	-.127	-.095	-.058	-.040	0	.037	.060	.088
	.250	-.217	-.170	-.145	-.133	-.129	-.113	-.099	-.076	-.055	-.028	-.013	.014	.040	.050	.066
	.350	-.132	-.131	-.133	-.129	-.122	-.102	-.093	-.074	-.058	-.040	-.029	-.007	.018	.027	.046
	.450	-.147	-.143	-.145	-.140	-.135	-.120	-.114	-.098	-.083	-.072	-.066	-.048	-.024	-.022	-.010
	.550	-.098	-.094	-.096	-.091	-.089	-.076	-.074	-.063	-.056	-.047	-.046	-.034	-.018	-.015	-.003
	.650	-.082	-.081	-.085	-.083	-.084	-.076	-.080	-.073	-.070	-.067	-.067	-.062	-.053	-.053	-.043
	.750	-.028	-.027	-.032	-.032	-.038	-.035	-.042	-.041	-.043	-.045	-.054	-.050	-.048	-.050	-.042
	.850	.031	.032	.026	.024	.014	.011	-.001	-.006	-.015	-.024	-.037	-.040	-.045	-.049	-.044
	.925	.101	.101	.095	.091	.077	.069	.052	.042	.025	.010	-.008	-.016	-.024	-.030	-.027
	.975	.199	.197	.193	.192	.185	.182	.175	.172	.163	.150	.133	.114	.086	.060	.030
1.000	.280	.265	.253	.270	.270	.270	.270	.288	.280	.278	.260	.263	.172	.140	.100	

^a% orifice.



TABLE 5.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN

WACA 16-506.62 PROPELLER BLADE SECTION ($\alpha = 0.70$; $\beta_x = 47.00^\circ$;

$\beta_{0.75R} = 45^\circ$; $B = 2$) - Continued

(h) $M = 0.65$.

	2.124	2.152	2.183	2.219	2.259	2.286	2.326	2.364	2.397	2.434	2.456	2.098	
J	2.124	2.152	2.183	2.219	2.259	2.286	2.326	2.364	2.397	2.434	2.456	2.098	
M	.943	.932	.922	.917	.911	.903	.896	.889	.879	.874	.867	.948	
$\Delta \delta$	3.00	2.62	2.21	1.74	1.23	.89	.39	-.07	-.47	-.90	-1.16	3.35	
$\Delta \delta_{1/2}$	-.25	-.29	-.34	-.40	-.46	-.50	-.56	-.61	-.66	-.71	-.75	-.21	
$\delta_{1/2}$	1.18	1.08	.93	.80	.67	.57	.42	.26	.12	.01	-.05	1.27	
C_{L1}	.4232	.3897	.3348	.2890	.2419	.2069	.1503	.0929	.0452	.0026	-.0181	.4574	
C_{L2}	-.1608	-.1576	-.1522	-.1501	-.1413	-.1360	-.1295	-.1254	-.1224	-.1222	-.1222	-.1593	
C_D	.0428	.0434	.0426	.0418	.0406	.0388	.0381	.0366	.0358	.0347	.0335	.0420	
c/b	Pressure coefficient, P												
Upper surface	$a_{0.000}$	1.242	1.236	1.231	1.228	1.225	1.221	1.217	1.213	1.208	1.205	1.202	1.245
	$a_{.025}$.410	.419	.453	.470	.495	.518	.552	.572	.587	.608	.627	.363
	$a_{.050}$	-.001	.011	.053	.077	.106	.130	.173	.206	.225	.248	.270	-.037
	$a_{.100}$	-.133	-.128	-.095	-.077	-.052	-.031	.005	.034	.047	.068	.085	-.156
	$a_{.200}$	-.299	-.294	-.281	-.273	-.246	-.221	-.187	-.163	-.152	-.133	-.116	-.297
	$a_{.300}$	-.352	-.356	-.342	-.337	-.328	-.322	-.318	-.310	-.305	-.285	-.270	-.363
	$a_{.400}$	-.448	-.450	-.435	-.426	-.412	-.394	-.366	-.344	-.346	-.341	-.340	-.462
	$a_{.500}$	-.522	-.533	-.523	-.518	-.507	-.494	-.478	-.466	-.474	-.461	-.456	-.524
	$a_{.600}$	-.637	-.650	-.641	-.637	-.627	-.626	-.596	-.597	-.604	-.594	-.588	-.635
	$a_{.700}$	-.749	-.762	-.752	-.748	-.739	-.731	-.735	-.733	-.744	-.729	-.720	-.742
	$a_{.800}$	-.849	-.863	-.863	-.859	-.823	-.795	-.621	-.520	-.442	-.386	-.376	-.839
$a_{.900}$	-.473	-.466	-.416	-.378	-.337	-.301	-.279	-.255	-.233	-.199	-.176	-.467	
$a_{.950}$	-.444	-.440	-.397	-.364	-.326	-.292	-.271	-.245	-.223	-.176	-.143	-.441	
Lower surface	$a_{0.0375}$	-.157	-.235	-.455	-.568	-.653	-.737	-.829	-.890	-.969	-1.021	-1.077	-.068
	$a_{.075}$	-.066	-.121	-.231	-.371	-.520	-.622	-.720	-.786	-.863	-.910	-.963	-.008
	$a_{.150}$.013	-.027	-.075	-.093	-.130	-.248	-.361	-.475	-.560	-.608	-.662	.056
	$a_{.250}$.024	-.012	-.052	-.073	-.087	-.102	-.135	-.178	-.247	-.345	-.465	.058
	$a_{.350}$.001	-.033	-.071	-.091	-.107	-.120	-.131	-.130	-.154	-.157	-.176	.031
	$a_{.450}$	-.054	-.087	-.123	-.140	-.153	-.163	-.174	-.172	-.183	-.167	-.161	-.030
	$a_{.550}$	-.031	-.063	-.091	-.106	-.116	-.122	-.134	-.133	-.148	-.135	-.126	-.009
	$a_{.650}$	-.076	-.107	-.130	-.142	-.145	-.143	-.151	-.150	-.161	-.143	-.129	-.056
	$a_{.750}$	-.060	-.087	-.104	-.110	-.111	-.108	-.113	-.109	-.114	-.096	-.083	-.043
	$a_{.850}$	-.035	-.057	-.070	-.076	-.077	-.074	-.078	-.071	-.072	-.052	-.038	-.018
	$a_{.925}$.012	-.008	-.021	-.029	-.031	-.033	-.036	-.029	-.026	-.002	.014	.031
$a_{.975}$	-.099	-.103	-.088	-.065	-.032	.012	.044	.084	.113	.151	.168	-.095	
$a_{1.000}$	-.264	-.239	-.175	-.108	-.060	.101	.120	.195	.285	.290	.303	-.308	

^aNo orifice.
^bPaired value.



TABLE 6.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN
NACA 16-505.05 PROPELLER BLADE SECTION ($\alpha = 0.78$; $\beta_x = 43.90^\circ$;

$\beta_{0.77R} = 45^\circ$; $B = 2$)

(a) $N = 1140$ rpm.

	J	M_x	α_x	$\Delta\theta$	c_l	c_m	c_n	c_c												
	1.606	1.689	1.816	1.928	2.052	2.169	2.300	2.423	2.549	2.649	2.601	2.492	2.367	2.258	2.106	1.982	1.876	1.774	1.652	
	.503	.509	.524	.534	.551	.566	.579	.593	.608	.624	.616	.600	.586	.573	.559	.544	.528	.520	.506	
	10.66	9.32	7.36	5.70	3.96	2.39	.71	-.78	-2.23	-3.33	-2.81	-1.58	-.11	1.24	3.22	4.93	6.46	8.00	9.91	
	.94	.85	.72	.59	.46	.33	.16	-.02	-.20	-.36	-.28	-.12	.06	.22	.41	.54	.65	.76	.89	
	3.11	3.05	2.77	2.35	1.99	1.57	1.15	.72	.31	-.01	.15	.54	.92	1.29	1.77	2.20	2.52	2.88	3.09	
	.9058	.9671	.8781	.7503	.6387	.5023	.3703	.2313	.0994	-.0019	.0471	.1761	.2965	.4158	.5658	.7039	.8026	.9123	.9755	
	-.0539	-.0542	-.0718	-.0831	-.0893	-.0932	-.0918	-.0919	-.0983	-.1031	-.1009	-.0932	-.0931	-.0921	-.0910	-.0846	-.0783	-.0674	-.0518	
c/b	Pressure coefficient, P																			
Upper surface	.000	1.065	1.066	1.070	1.073	1.078	1.082	1.086	1.091	1.095	1.101	1.098	1.093	1.088	1.084	1.079	1.076	1.071	1.069	1.065
	.025	-1.841	-2.126	-2.290	-1.161	-.788	-.345	.027	.328	.507	.605	.558	.424	.198	-.093	-.367	-1.005	-1.600	-2.285	-1.989
	.050	-1.846	-2.078	-1.655	-1.085	-.765	-.462	-.187	.054	.227	.325	.275	.147	-.055	-.279	-.613	-.934	-1.201	-2.026	-1.977
	.100	-1.780	-1.788	-1.085	-.903	-.696	-.490	-.295	-.120	.017	.101	.058	-.047	-.197	-.362	-.592	-.806	-.982	-1.327	-1.841
	.200	-1.153	-1.013	-.804	-.722	-.605	-.488	-.358	-.239	-.132	.070	-.103	-.181	-.291	-.403	-.547	-.669	-.751	-.791	-1.090
	.300	-.937	-.753	-.719	-.661	-.578	-.488	-.393	-.304	-.220	-.168	-.197	-.261	-.343	-.424	-.526	-.624	-.692	-.724	-.806
	.400	-.682	-.620	-.626	-.583	-.520	-.454	-.380	-.315	-.247	-.208	-.229	-.279	-.343	-.405	-.483	-.555	-.605	-.630	-.617
	.500	-.543	-.527	-.585	-.565	-.528	-.480	-.424	-.380	-.323	-.296	-.312	-.348	-.395	-.442	-.500	-.551	-.576	-.584	-.534
	.600	-.432	-.469	-.508	-.504	-.480	-.450	-.408	-.380	-.338	-.318	-.330	-.339	-.388	-.422	-.463	-.495	-.510	-.502	-.448
	.700	-.344	-.394	-.445	-.456	-.452	-.438	-.408	-.395	-.366	-.354	-.363	-.377	-.397	-.418	-.442	-.459	-.452	-.431	-.362
	.800	-.261	-.285	-.327	-.352	-.362	-.365	-.351	-.350	-.334	-.333	-.337	-.339	-.346	-.354	-.360	-.360	-.337	-.314	-.262
.900	-.172	-.141	-.131	-.133	-.151	-.164	-.162	-.172	-.167	-.175	-.174	-.167	-.161	-.160	-.154	-.146	-.129	-.131	-.143	
.950	-.138	-.077	-.031	-.018	-.013	-.019	-.015	-.026	-.025	-.034	-.033	-.024	-.017	-.015	-.012	-.015	-.022	-.039	-.095	
Lower surface	.0375	.744	.712	.638	.527	.377	.184	-.029	-.295	-.902	-1.074	-1.076	-.544	-.159	.052	.293	.459	.585	.667	.733
	.075	.618	.585	.518	.423	.300	.154	.006	-.180	-.460	-.790	-.679	-.254	-.080	.060	.235	.366	.470	.545	.606
	.150	.492	.462	.407	.333	.245	.142	.051	-.078	-.185	-.474	-.309	-.123	-.010	.083	.200	.291	.368	.431	.482
	.250	.399	.370	.330	.248	.186	.116	.045	-.048	-.107	-.194	-.132	-.078	0	.071	.172	.239	.286	.327	.390
	.350	.334	.313	.279	.231	.176	.116	.060	-.013	-.055	-.096	-.075	-.034	.028	.079	.151	.206	.255	.296	.327
	.450	.263	.249	.222	.181	.138	.090	.045	-.013	-.041	-.064	-.057	-.027	.020	.062	.118	.161	.204	.236	.261
	.550	.227	.221	.202	.168	.132	.092	.054	.011	-.011	-.029	-.024	.022	.036	.069	.116	.148	.182	.213	.227
	.650	.152	.155	.147	.120	.092	.062	.037	-.002	-.011	-.021	-.021	-.005	.020	.048	.081	.105	.133	.156	.163
	.750	.122	.131	.132	.111	.092	.070	.054	.028	.021	.014	.014	.025	.043	.062	.085	.103	.120	.137	.134
	.850	.096	.114	.127	.117	.109	.100	.089	.070	.067	.060	.062	.071	.083	.093	.107	.114	.120	.131	.113
	.925	.064	.095	.123	.120	.124	.122	.120	.108	.108	.100	.100	.111	.119	.122	.126	.120	.120	.121	.089
.975	.040	.081	.128	.126	.150	.138	.144	.142	.140	.125	.050	.140	.146	.143	.142	.128	.125	.116	.068	
al.000	.025	.074	.130	.128	.164	.148	.148	.137	.155	.140	.130	.155	.160	.155	.150	.130	.128	.110	.057	

^aNo orifice.
^bPaired value.



TABLE 6.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN

NACA 16-505,85 PROPELLER BLADE SECTION ($x = 0.78$; $\beta_x = 43.90^\circ$; $\beta_{0.75R} = 45^\circ$; $B = 2$) - Continued.(b) $N = 1350$ rpm.

	1.793	1.890	1.988	2.130	2.272	2.420	2.567	2.634	2.606	2.490	2.367	2.223	2.087	1.945	1.837	
J	.630	.640	.652	.674	.696	.717	.740	.750	.744	.727	.705	.685	.665	.645	.632	
M_x	7.71	6.26	4.85	2.90	1.06	-.74	-2.43	-3.17	-2.86	-1.56	-.11	1.69	3.48	5.46	7.04	
α_x	1.12	.92	.71	.43	.16	-.13	-.46	-.62	-.55	-.27	-.03	.26	.51	.80	1.03	
ΔB	3.14	2.70	2.35	1.85	1.38	.80	.28	0	.07	.60	1.02	1.54	2.04	2.51	2.98	
c_d	.9961	.8619	.7523	.5939	.4439	.2594	.0903	.0013	.0219	.1932	.3287	.4942	.6535	.8013	.9497	
c_m	-.0688	-.0816	-.0906	-.0991	-.1023	-.1048	-.1150	-.1180	-.1219	-.1045	-.1031	-.0986	-.0967	-.0928	-.0777	
c_c																
c/b	Pressure coefficient, P															
Upper surface	*0.000	1.103	1.106	1.111	1.120	1.128	1.136	1.145	1.149	1.147	1.140	1.131	1.123	1.113	1.108	1.103
	.025	-2.537	-2.084	-1.227	-.488	-.041	.356	.574	.643	.609	.471	.231	-.220	-.733	-1.593	-2.374
	.050	-2.368	-1.864	-1.091	-.561	-.223	.103	.311	.380	.349	.209	-.005	-.371	-.748	-1.289	-2.181
	.100	-2.164	-1.008	-.919	-.584	-.350	-.094	.088	.153	.125	-.005	-.182	-.468	-.721	-.990	-1.803
	.200	-.687	-.728	-.712	-.556	-.421	-.245	-.103	-.048	-.073	-.307	-.303	-.503	-.631	-.736	-.720
	.300	-.746	-.748	-.689	-.547	-.460	-.332	-.221	-.174	-.194	-.274	-.376	-.529	-.618	-.719	-.756
	.400	-.656	-.654	-.615	-.508	-.451	-.361	-.275	-.238	-.254	-.316	-.392	-.511	-.567	-.635	-.660
	.500	-.622	-.624	-.599	-.522	-.494	-.433	-.371	-.346	-.357	-.400	-.452	-.546	-.571	-.610	-.625
	.600	-.536	-.541	-.531	-.475	-.470	-.435	-.398	-.384	-.392	-.414	-.446	-.514	-.518	-.537	-.537
	.700	-.465	-.480	-.485	-.452	-.466	-.453	-.447	-.447	-.446	-.445	-.455	-.502	-.485	-.484	-.478
	.800	-.328	-.340	-.358	-.340	-.370	-.373	-.382	-.388	-.385	-.372	-.372	-.403	-.371	-.354	-.332
.900	-.106	-.103	-.117	-.100	-.136	-.145	-.161	-.170	-.166	-.148	-.143	-.168	-.130	-.111	-.102	
.950	-.003	.001	.005	.040	.013	.010	0	-.009	-.006	.009	.010	-.021	.005	.005	.001	
Lower surface	.0375	.698	.605	.485	.299	.025	-.315	-1.370	-1.125	-1.722	-.657	-.190	.075	.349	.547	.697
	.075	.576	.495	.393	.254	.053	-.189	-.652	-.970	-.935	-.336	-.103	.079	.283	.443	.541
	.150	.470	.407	.329	.238	.090	-.071	-.267	-.656	-.554	-.134	-.013	.099	.251	.367	.441
	.250	.308	.238	.215	.192	.072	-.043	-.138	-.343	-.223	-.086	-.002	.067	.177	.231	.276
	.350	.323	.280	.227	.182	.084	-.003	-.073	-.137	-.096	-.039	.027	.075	.175	.252	.303
	.450	.267	.228	.184	.151	.066	-.003	-.053	-.067	-.055	-.028	.021	.052	.141	.205	.248
	.550	.239	.208	.168	.151	.075	.021	-.019	-.024	-.020	.003	.039	.058	.134	.188	.226
	.650	.183	.154	.123	.114	.048	.010	-.016	-.011	-.012	-.003	.021	.029	.093	.138	.172
	.750	.164	.141	.118	.120	.068	.039	.023	.027	.025	.031	.048	.041	.096	.130	.153
	.850	.158	.143	.129	.145	.103	.087	.075	.072	.072	.081	.091	.073	.117	.137	.151
	.925	.152	.141	.136	.164	.133	.124	.115	.107	.108	.121	.126	.099	.131	.140	.146
^b .975	.250	.246	.245	.303	.267	.252	.260	.257	.258	.257	.258	.243	.247	.272	.250	
^a 1.000	.387	.407	.430	.458	.395	.410	.417	.460	.428	.440	.414	.380	.453	.463	.445	

^aNo orifice.^bPaired value.

TABLE 6.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN
 NACA 16-505.85 PROPELLER BLADE SECTION ($\alpha = 0.78$; $\beta_x = 43.90^\circ$;
 $\beta_{0.75R} = 45^\circ$; $B = 2$) - Continued

(c) $N = 1500$ rpm.

J	2.003	2.100	2.169	2.305	2.409	2.505	2.582	2.547	2.470	2.359	2.252	2.148	2.063	
M_x	.721	.736	.747	.768	.787	.802	.815	.808	.793	.774	.757	.737	.725	
$\Delta\delta$	4.64	3.30	2.39	.65	-.61	-1.73	-2.60	-2.21	-1.33	-.01	1.32	2.66	3.81	
α_1	.96	.67	.46	.02	-.27	-.56	-.82	-.70	-.45	-.13	.20	.53	.78	
α_n	2.40	2.10	1.81	1.28	.87	.34	-.02	.13	.55	1.06	1.46	1.91	2.24	
c_m	.7671	.6742	.5819	.4126	.2803	.1084	-.0065	.0439	.1781	.3406	.4710	.6135	.7174	
c_c	-.0975	-.1037	-.1071	-.1154	-.1200	-.1324	-.1362	-.1331	-.1268	-.1147	-.1143	-.1064	-.0968	
c/b		Pressure coefficient, P												
Upper surface	$\theta_0.000$	1.137	1.143	1.148	1.157	1.165	1.171	1.177	1.173	1.167	1.159	1.152	1.144	1.139
	.025	-.948	-.903	-.866	-.825	-.789	-.750	-.707	-.662	-.623	-.586	-.550	-.519	-.488
	.050	-1.003	-.970	-.938	-.903	-.873	-.841	-.809	-.778	-.741	-.709	-.680	-.649	-.619
	.100	-1.107	-.756	-.530	-.295	-.068	.067	.152	.117	.020	-.150	-.364	-.618	-.918
	.200	-.689	-.635	-.567	-.483	-.385	-.284	-.178	-.069	-.173	-.308	-.458	-.623	-.804
	.300	-.708	-.668	-.596	-.462	-.352	-.258	-.190	-.219	-.292	-.399	-.518	-.626	-.695
	.400	-.688	-.675	-.628	-.525	-.429	-.346	-.282	-.306	-.375	-.469	-.567	-.643	-.680
	.500	-.644	-.625	-.608	-.557	-.504	-.451	-.402	-.419	-.469	-.527	-.579	-.612	-.634
	.600	-.568	-.561	-.563	-.551	-.535	-.504	-.464	-.480	-.518	-.542	-.577	-.561	-.566
	.700	-.508	-.511	-.524	-.543	-.562	-.582	-.597	-.565	-.597	-.611	-.633	-.619	-.611
	.800	-.359	-.366	-.378	-.384	-.387	-.386	-.381	-.380	-.390	-.386	-.386	-.376	-.365
.900	-.101	-.103	-.111	-.114	-.114	-.116	-.103	-.110	-.117	-.115	-.116	-.112	-.104	
.950	.013	.020	.022	.027	.030	.031	.040	.038	.030	.031	.022	.021	.016	
Lower surface	.0375	.457	.319	.168	-.098	-.468	-1.293	-1.353	-1.351	-1.237	-.243	.013	.237	.376
	.075	.374	.265	.150	-.035	-.245	-1.181	-1.274	-1.260	-.694	-.129	.037	.201	.308
	.150	.310	.232	.154	.031	-.081	-.222	-.296	-.489	-.110	-.033	.085	.188	.262
	.250	.117	.140	.117	.029	-.047	-.079	-.225	-.103	-.079	-.010	.064	.126	.149
	.350	.225	.177	.128	.055	-.006	-.046	-.051	-.042	-.037	.022	.084	.149	.195
	.450	.180	.139	.099	.042	-.005	-.038	-.031	-.036	-.031	.017	.064	.115	.155
	.550	.168	.135	.102	.057	.022	-.007	-.004	-.006	0	.038	.072	.115	.146
	.650	.121	.097	.069	.036	.009	-.012	-.008	-.010	-.007	.021	.047	.081	.105
	.750	.117	.099	.079	.057	.039	.023	.028	.025	.028	.047	.065	.087	.105
	.850	.131	.121	.109	.098	.087	.078	.082	.080	.081	.093	.101	.115	.123
	.925	.141	.138	.133	.132	.125	.118	.123	.121	.119	.128	.130	.135	.137
$\theta_{.975}$.255	.261	.245	.255	.260	.253	.270	.260	.255	.260	.242	.243	.260	
$\theta_{1.000}$.380	.360	.358	.380	.393	.420	.405	.430	.405	.425	.375	.390	.440	

^aNo orifice.
^bReared value.



TABLE 6.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN

NACA 16-505.85 PROPELLER BLADE SECTION ($x = 0.78$; $\beta_x = 43.90^\circ$; $\beta_{0.75R} = 45^\circ$; $B = 2$) - Continued(d) $N = 1600$ rpm.

J	2.165	2.267	2.349	2.444	2.528	2.483	2.406	2.315	2.235	2.130	
M_x	.796	.816	.831	.847	.864	.854	.838	.820	.804	.788	
α_x	2.44	1.13	.11	-1.02	-1.99	-1.48	-.58	.53	1.53	2.90	
$\Delta\delta$.54	.15	-.16	-.57	-.91	-.75	-.40	-.03	.28	.67	
α_1	1.79	1.44	.99	.38	-.14	.16	.66	1.19	1.54	1.98	
c_n	.5735	.4626	.3187	.1245	-.0445	.0535	.2123	.3826	.4942	.6374	
c_m	-.1150	-.1265	-.1401	-.1422	-.1468	-.1475	-.1298	-.1232	-.1200	-.1167	
c_c	.0021	.0137	.0243	.0328	.0385	.0343	.0258	.0192			
c/b	Pressure coefficient, P										
Upper surface	$\beta_{0.000}$	1.169	1.186	1.185	1.192	1.200	1.195	1.188	1.180	1.172	1.165
	.025	-.058	.220	.422	.565	.659	.608	.505	.342	.129	-.212
	.050	-.305	-.052	.137	.311	.390	.336	.224	.097	-.135	-.434
	.100	-.463	-.245	-.075	.069	.170	.116	.008	-.149	-.319	-.591
	.200	-.560	-.403	-.255	-.127	-.037	-.086	-.185	-.321	-.446	-.610
	.300	-.633	-.481	-.364	-.249	-.170	-.214	-.300	-.417	-.524	-.709
	.400	-.604	-.478	-.424	-.351	-.282	-.322	-.389	-.457	-.511	-.658
	.500	-.760	-.691	-.623	-.531	-.464	-.500	-.576	-.661	-.724	-.796
	.600	-.802	-.751	-.673	-.575	-.450	-.510	-.622	-.707	-.773	-.808
	.700	-.510	-.763	-.711	-.616	-.571	-.598	-.651	-.733	-.638	-.460
	.800	-.310	-.300	-.571	-.529	-.701	-.625	-.408	-.316	-.321	-.324
	.900	-.074	-.070	-.075	-.090	-.114	-.100	-.076	-.075	-.077	-.074
.950	.028	.024	.003	-.030	-.068	-.045	-.004	.020	.027	.032	
Lower surface	.0375	.144	-.071	-.730	-1.082	-1.147	-1.121	-1.040	-.199	-.009	.235
	.075	.136	-.013	-.132	-.922	-1.087	-1.048	-.890	-.111	.031	.205
	.150	.149	.047	-.059	-.551	-.926	-.874	-.095	-.022	.079	.196
	.250	.120	.047	-.038	-.073	-.811	-.213	-.060	-.005	.070	.121
	.350	.127	.066	-.001	-.031	-.208	-.047	-.025	.025	.082	.155
	.450	.097	.049	-.004	-.033	-.059	-.031	-.025	.015	.062	.124
	.550	.100	.062	.014	-.003	-.007	-.006	.001	.033	.070	.122
	.650	.065	.036	-.002	-.019	-.018	-.022	-.014	.011	.041	.086
	.750	.078	.054	.021	.009	.007	.008	.015	.034	.059	.092
	.850	.111	.094	.069	.056	.049	.054	.061	.078	.096	.121
	.925	.132	.122	.099	.084	.072	.080	.093	.110	.126	.141
	$\beta_{0.975}$.155	.155	.120	.115	.090	.100	.120	.139	.150	.160
$\beta_{1.000}$.165	.170	.132	.130	.105	.115	.133	.153	.162	.167	

^aNo orifice.^bPaired value.

TABLE 6.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN

NACA 16-505.85 PROPELLER BLADE SECTION ($x = 0.78$; $\beta_x = 43.90^\circ$; $\beta_{0.75R} = 45^\circ$; $B = 2$) - Continued(c) $M = 0.56$.

	J	2.114	2.146	2.192	2.229	2.278	2.326	2.371 ^a	2.417	2.469	2.542	2.578	2.620
M_x		.879	.868	.858	.847	.837	.828	.817	.805	.800	.789	.784	.778
$c_{x'}$		3.12	2.69	2.09	1.61	.99	.39	-.16	-.71	-1.55	-2.15	-2.56	-3.02
$\Delta\beta$.30	.17	.04	-.03	-.07	-.10	-.18	-.32	-.49	-.58	-.64	-.70
α_1		1.82	1.70	1.57	1.45	1.32	1.15	.93	.74	.45	.22	.12	-.05
c_n		.5826	.5445	.5045	.4665	.4239	.3690	.2987	.2400	.1471	.0710	.0374	-.0174
c_m		-.1434	-.1385	-.1350	-.1355	-.1309	-.1222	-.1257	-.1263	-.1273	-.1286	-.1286	-.1306
c_c		.0153	.0173	.0182	.0174	.0174	.0184	.0196	.0217	.0232			
c/b		Pressure coefficient, P											
Upper surface	$\beta_{0.000}$	1.208	1.203	1.198	1.192	1.187	1.183	1.178	1.172	1.170	1.166	1.163	1.161
	.025	.053	.098	.151	.207	.271	.338	.409	.482	.532	.590	.613	.650
	.050	-.138	-.105	-.062	-.018	.037	.095	.162	.201	.280	.337	.361	.396
	.100	-.319	-.289	-.253	-.216	-.169	-.116	-.054	-.018	.056	.110	.132	.167
	.200	-.444	-.430	-.381	-.374	-.338	-.290	-.235	-.206	-.138	-.090	-.070	-.040
	.300	-.553	-.521	-.511	-.468	-.434	-.404	-.352	-.326	-.264	-.193	-.202	-.173
	.400	-.583	-.554	-.510	-.491	-.452	-.407	-.402	-.400	-.344	-.257	-.281	-.252
	.500	-.708	-.697	-.679	-.663	-.628	-.627	-.606	-.548	-.453	-.406	-.389	-.361
	.600	-.756	-.743	-.736	-.722	-.706	-.666	-.584	-.542	-.511	-.464	-.447	-.416
	.700	-.848	-.838	-.827	-.798	-.788	-.735	-.642	-.640	-.524	-.470	-.459	-.433
	.800	-.336	-.310	-.304	-.298	-.307	-.307	-.337	-.371	-.284	-.389	-.393	-.391
	.900	-.295	-.256	-.218	-.167	-.104	-.065	-.076	-.096	-.109	-.123	-.133	-.143
	.950	.293	-.247	-.196	-.130	-.052	.020	.043	.039	.040	.034	.025	.019
Lower surface	.0375	.153	.093	.018	-.060	-.144	-.218	-.272	-.3075	-1.271	-1.430	-1.495	-1.591
	.075	.177	.112	.054	-.004	-.068	-.118	-.152	-.307	-.890	-1.269	-1.346	-1.440
	.150	.180	.148	.107	.066	.022	-.016	-.053	-.074	-.095	-.220	-.332	-.473
	.250	.133	.113	.084	.057	.026	-.002	-.033	-.057	-.070	-.081	-.093	-.108
	.350	.135	.116	.091	.068	.046	.027	.004	-.017	-.032	-.047	-.060	-.071
	.450	.098	.084	.066	.048	.033	.021	.004	-.013	-.024	-.037	-.049	-.057
	.550	.090	.080	.067	.054	.045	.038	.027	.014	.007	-.003	-.013	-.020
	.650	.036	.032	.025	.019	.017	.017	.013	.003	.002	-.005	-.013	-.017
	.750	.030	.032	.029	.030	.034	.042	.043	.036	.038	.034	.028	.025
	.850	.038	.044	.050	.059	.072	.085	.091	.086	.091	.088	.084	.081
	.925	.027	.038	.051	.071	.093	.118	.128	.126	.132	.130	.126	.123
	^b .975	.250	.310	.340	.340	.280	.290	.280	.350	.360	.345	.360	.348
	^a 1.000	.500	.470	.512	.495	.550	.550	.500	.510	.570	.490	.570	.470

^aNo orifice.^bFaired value.

TABLE 6.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN

NACA 16-505.85 PROPELLER BLADE SECTION ($\alpha = 0.78^\circ$; $\beta_x = 43.90^\circ$;

$\beta_{0.75R} = 45^\circ$; $B = 2$) - Continued

(r) $M = 0.58$.

	J	2.110	2.152	2.198	2.244	2.281	2.329	2.370	2.422	2.488	2.519	2.551	2.596
M_{∞}		.907	.897	.887	.878	.867	.858	.847	.838	.830	.824	.819	.810
$c_{d_{max}}$		3.16	2.60	2.00	1.41	.95	.35	-.15	-.77	-1.64	-1.90	-2.26	-2.76
$\Delta\beta$.42	.24	.05	-.13	-.27	-.37	-.40	-.44	-.56	-.64	-.73	-.86
α_1		1.63	1.51	1.38	1.24	1.09	.96	.79	.59	.33	.17	.04	-.11
c_n		.5219	.4826	.4445	.3974	.3510	.3090	.2529	.1916	.1065	.0555	.0123	-.0348
c_m		-.1417	-.1350	-.1319	-.1244	-.1226	-.1272	-.1293	-.1309	-.1345	-.1352	-.1370	-.1395
c_c		.0251	.0252	.0250	.0249	.0258	.0255	.0253	.0258	.0279	.0292	.0305	.0323
c/b		Pressure coefficient, P											
Upper surface	^a 0.000	1.223	1.217	1.212	1.207	1.203	1.197	1.192	1.188	1.184	1.181	1.179	1.175
	.025	.165	.212	.254	.310	.358	.400	.438	.500	.558	.591	.616	.650
	.050	-.038	-.003	.033	.081	.122	.158	.193	.251	.309	.342	.367	.400
	.100	-.226	-.194	-.165	-.124	-.089	-.055	-.023	.032	.084	.116	.140	.172
	.200	-.379	-.350	-.308	-.296	-.270	-.239	-.212	-.163	-.117	-.088	-.067	-.037
	.300	-.475	-.446	-.437	-.394	-.365	-.356	-.334	-.290	-.250	-.222	-.203	-.176
	.400	-.513	-.486	-.445	-.422	-.402	-.371	-.355	-.350	-.335	-.315	-.295	-.268
	.500	-.638	-.628	-.611	-.597	-.584	-.563	-.576	-.555	-.509	-.448	-.419	-.389
	.600	-.684	-.679	-.667	-.657	-.644	-.641	-.620	-.572	-.527	-.482	-.474	-.466
	.700	-.786	-.775	-.767	-.745	-.736	-.726	-.706	-.657	-.623	-.616	-.596	-.537
	.800	-.430	-.388	-.348	-.328	-.331	-.343	-.382	-.384	-.381	-.364	-.374	-.394
	.900	-.337	-.301	-.265	-.230	-.202	-.158	-.105	-.066	-.075	-.085	-.097	-.115
	.950	-.338	-.301	-.260	-.219	-.180	-.120	-.049	.025	.039	.047	.046	.040
Lower surface	.0375	.089	.017	-.039	-.119	-.344	-.659	-.888	-1.058	-1.182	-1.263	-1.326	-1.423
	.075	.112	.056	.013	-.050	-.094	-.166	-.503	-.912	-1.069	-1.161	-1.220	-1.310
	.150	.150	.111	.083	.039	-.005	-.027	-.045	-.102	-.433	-.635	-.790	-.996
	.250	.118	.090	.071	.037	.002	-.019	-.043	-.052	-.059	-.072	-.107	-.180
	.350	.115	.093	.079	.055	.028	.012	-.009	-.019	-.029	-.029	-.032	-.040
	.450	.080	.063	.054	.036	.014	.004	-.012	-.019	-.029	-.029	-.030	-.037
	.550	.074	.061	.055	.043	.027	.020	.010	-.009	-.001	.001	0	-.006
	.650	.017	.009	.008	.002	-.008	-.007	-.009	-.005	-.009	-.005	-.005	-.009
	.750	.013	.008	.011	.010	.006	.013	.016	.027	.027	.032	.032	.030
	.850	.027	.024	.029	.034	.036	.050	.061	.079	.080	.087	.089	.086
	.925	.025	.019	.025	.036	.043	.065	.086	.113	.120	.128	.130	.129
	^b .975	.031	.010	.020	.037	.050	.072	.098	.140	.150	.159	.160	.160
	^a 1.000	.020	.002	.016	.037	.050	.078	.102	.160	.168	.178	.175	.175

^aNo orifices.
^bFaired value.



TABLE 6.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN

NACA 16-505.05 PROPELLER BLADE SECTION ($\alpha = 0.78$; $\beta_x = 43.90^\circ$;

$\beta_{0.75R} = 45^\circ$; $B = 2$) - Continued

(8) $M = 0.60$.

	2.103	2.142	2.174	2.206	2.244	2.275	2.323	2.362	2.407	2.443	2.486	2.534	2.566	
J	2.103	2.142	2.174	2.206	2.244	2.275	2.323	2.362	2.407	2.443	2.486	2.534	2.566	
M_x	.940	.933	.922	.915	.908	.898	.891	.883	.875	.865	.858	.850	.845	
$q_{p,1}$	3.26	2.74	2.32	1.91	1.42	1.03	.43	-.05	-.59	-1.01	-1.51	-2.06	-2.42	
ΔP	-.06	-.11	-.14	-.17	-.23	-.31	-.45	-.55	-.66	-.73	-.81	-.89	-.94	
a_1	1.64	1.52	1.47	1.29	1.11	.96	.74	.62	.42	.30	.19	.03	-.12	
a_n	.5265	.4877	.4697	.4129	.3548	.3071	.2697	.1994	.1355	.0955	.0619	.0097	-.0374	
a_m	-.1752	-.1719	-.1689	-.1590	-.1516	-.1467	-.1444	-.1426	-.1460	-.1478	-.1509	-.1544	-.1509	
a_c	.0361	.0364	.0367	.0359	.0345	.0337	.0338	.0341	.0343	.0347	.0347	.0350	.0351	
c/b	Pressure coefficient, P													
Upper surface	^a 0.000	1.241	1.237	1.231	1.227	1.223	1.218	1.214	1.210	1.206	1.201	1.198	1.194	1.191
	.025	.251	.297	.313	.347	.393	.417	.469	.498	.535	.561	.588	.624	.653
	.050	.041	.082	.091	.121	.161	.181	.231	.258	.293	.317	.344	.379	.408
	.100	-.148	-.113	-.107	-.084	-.048	-.029	.018	.042	.075	.095	.120	.154	.181
	.200	-.308	-.277	-.261	-.241	-.227	-.213	-.170	-.149	-.120	-.103	-.083	-.052	-.029
	.300	-.404	-.373	-.382	-.370	-.334	-.309	-.285	-.275	-.248	-.232	-.216	-.190	-.169
	^b .400	-.490	-.465	-.483	-.470	-.434	-.408	-.400	-.390	-.373	-.362	-.351	-.319	-.293
	.500	-.569	-.560	-.562	-.551	-.535	-.528	-.502	-.498	-.500	-.498	-.495	-.455	-.418
	.600	-.662	-.611	-.615	-.609	-.595	-.593	-.569	-.570	-.546	-.534	-.514	-.484	-.461
	.700	-.718	-.706	-.713	-.711	-.691	-.682	-.664	-.659	-.639	-.625	-.614	-.592	-.581
	.800	-.838	-.828	-.837	-.790	-.708	-.619	-.574	-.552	-.554	-.571	-.606	-.636	-.581
	.900	-.414	-.393	-.372	-.332	-.285	-.259	-.230	-.208	-.178	-.152	-.110	-.067	-.063
	.950	-.409	-.387	-.366	-.325	-.278	-.251	-.217	-.186	-.147	-.108	-.056	.014	.041
Lower surface	.0375	.052	-.028	-.058	-.226	-.491	-.608	-.739	-.840	-.946	-1.035	-1.105	-1.194	-1.257
	.075	.086	.039	-.005	-.058	-.148	-.338	-.657	-.751	-.856	-.939	-1.012	-1.110	-1.171
	.150	.141	.109	.074	.028	-.002	-.009	-.064	-.302	-.599	-.766	-.850	-.935	-.993
	.250	.111	.088	.059	.024	.002	-.013	-.031	-.047	-.072	-.124	-.210	-.355	-.490
	.350	.113	.095	.070	.043	.028	.016	-.002	-.018	-.023	-.030	-.035	-.053	-.093
	.450	.078	.063	.041	.020	.011	.002	-.011	-.025	-.029	-.031	-.030	-.023	-.017
	.550	.073	.060	.041	.024	.020	.013	.006	-.005	-.006	-.008	-.006	.003	.008
	.650	.015	.005	-.011	-.022	-.022	-.024	-.027	-.032	-.027	-.025	-.022	-.009	-.001
	.750	.016	.007	-.009	-.017	-.013	-.013	-.011	-.011	-.011	-.004	.001	.009	.024
	.850	.041	.033	.017	.009	.013	.013	.020	.023	.023	.036	.044	.057	.085
	.925	.051	.041	.024	.013	.015	.016	.025	.033	.051	.065	.082	.107	.120
	^b .975	.056	.040	.025	0	.015	.022	.022	.038	.056	.076	.096	.112	.130
	^a 1.000	.060	.044	.025	0	.014	.023	.020	.039	.052	.080	.100	.111	.130

^aNo orifice.

^bPaired value.



TABLE 6.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN

NACA 16-505.85 PROPELLER BLADE SECTION ($\alpha = 0.78$; $\beta_x = 43.90^\circ$; $\beta_{0.75R} = 45^\circ$; $B = 2$) - Computed(h) $M = 0.65$.

	2.089	2.102	2.132	2.160	2.179	2.213	2.243	2.268	2.299	2.326	2.359	2.386	2.418	2.451	
J	2.089	2.102	2.132	2.160	2.179	2.213	2.243	2.268	2.299	2.326	2.359	2.386	2.418	2.451	
M_x	1.026	1.015	1.007	.999	.989	.983	.977	.969	.962	.956	.949	.941	.934	.923	
$\Delta \delta$	3.45	3.28	2.88	2.50	2.26	1.81	1.43	1.11	.73	.39	-.01	-.34	-.72	-1.11	
α_1	-.49	-.41	-.47	-.52	-.56	-.63	-.69	-.73	-.79	-.82	-.89	-.93	-.98	-1.03	
α_2	1.44	1.38	1.21	1.12	1.01	.87	.70	.58	.42	.27	.12	0	-.12	-.30	
$c_{p, \text{total}}$.4613	.4406	.3858	.3587	.3239	.2781	.2239	.1858	.1342	.0855	.0394	.0013	-.0381	-.0961	
$c_{p, \text{upper}}$	-.1922	-.1929	-.1875	-.1870	-.1829	-.1780	-.1696	-.1671	-.1516	-.1457	-.1383	-.1367	-.1327	-.1296	
$c_{p, \text{lower}}$.0506	.0528	.0515	.0521	.0529	.0534	.0509	.0506	.0471	.0450	.0446	.0446	.0440	.0434	
c/b	Pressure coefficient, P														
Upper surface	$a_{0.000}$	1.291	1.284	1.279	1.274	1.268	1.265	1.261	1.257	1.253	1.250	1.245	1.241	1.237	1.231
	$a_{.025}$.399	.419	.451	.463	.471	.491	.513	.524	.545	.559	.589	.602	.615	.631
	$a_{.050}$.199	.214	.240	.251	.257	.273	.292	.298	.318	.330	.361	.371	.385	.398
	$a_{.100}$.008	.021	.045	.052	.056	.071	.088	.093	.110	.120	.150	.159	.170	.182
	$a_{.200}$	-.156	-.145	-.118	-.100	-.097	-.093	-.090	-.092	-.076	-.067	-.039	-.031	-.024	-.014
	$a_{.300}$	-.255	-.243	-.220	-.223	-.230	-.220	-.195	-.197	-.175	-.171	-.158	-.157	-.152	-.143
	$a_{.400}$	-.335	-.320	-.308	-.317	-.324	-.316	-.297	-.290	-.281	-.273	-.270	-.264	-.279	-.269
	$a_{.500}$	-.415	-.410	-.404	-.404	-.407	-.402	-.394	-.401	-.391	-.390	-.375	-.373	-.381	-.392
	$a_{.600}$	-.467	-.467	-.453	-.454	-.461	-.454	-.448	-.458	-.454	-.456	-.442	-.448	-.453	-.448
	$a_{.700}$	-.554	-.554	-.550	-.545	-.559	-.555	-.561	-.556	-.578	-.586	-.573	-.579	-.595	-.578
	$a_{.800}$	-.669	-.669	-.664	-.672	-.683	-.681	-.679	-.689	-.687	-.693	-.692	-.700	-.707	-.713
$a_{.900}$	-.810	-.814	-.817	-.830	-.843	-.843	-.837	-.817	-.839	-.812	-.849	-.829	-.827	-.845	
$a_{.950}$	-.860	-.865	-.835	-.836	-.822	-.638	-.517	-.455	-.395	-.356	-.317	-.303	-.269	-.228	
Lower surface	$b_{.0375}$	-.050	-.139	-.260	-.314	-.368	-.418	-.486	-.536	-.604	-.654	-.726	-.784	-.837	-.907
	$b_{.075}$.032	-.026	-.188	-.266	-.331	-.382	-.447	-.492	-.552	-.600	-.661	-.711	-.763	-.833
	$b_{.150}$.129	.115	.090	.055	-.060	-.204	-.305	-.357	-.424	-.474	-.534	-.580	-.630	-.701
	$b_{.250}$.099	.085	.055	.036	.007	-.021	-.093	-.200	-.359	-.438	-.497	-.540	-.589	-.654
	$b_{.350}$.115	.103	.073	.055	.021	0	-.021	-.045	-.103	-.188	-.315	-.420	-.509	-.580
	$b_{.450}$.080	.068	.041	.023	-.015	-.038	-.057	-.074	-.089	-.101	-.125	-.152	-.160	-.197
	$b_{.550}$.086	.071	.050	.054	-.001	-.021	-.041	-.057	-.069	-.075	-.069	-.075	-.103	-.123
	$b_{.650}$.013	0	-.015	-.027	-.065	-.079	-.094	-.103	-.102	-.096	-.078	-.082	-.094	-.087
	$b_{.750}$.020	.008	.003	-.005	-.033	-.034	-.041	-.045	-.045	-.043	-.035	-.042	-.048	-.042
	$b_{.850}$.097	.081	.076	.064	.044	.040	.031	.022	.016	.013	.014	.004	-.001	.003
	$b_{.925}$.138	.123	.110	.098	.079	.072	.063	.049	.040	.031	.028	.017	.011	.012
$b_{.975}$.145	.138	.127	.113	.095	.093	.078	.057	.050	.041	.035	.021	.029	.029	
$b_{1.000}$.142	.140	.131	.116	.096	.100	.082	.060	.050	.045	.038	.023	.034	.032	

^aNo orifice.^bPaired value.

NACA

TABLE 7.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN
 NACA 16-505.30 PROPELLER BLADE SECTION ($\alpha = 0.85$; $\beta_x = 41.10^\circ$;
 $\beta_{0.72R} = 45^\circ$; $B = 2$)

(a) $N = 1140$ rpm.

r	2.709	2.541	2.376	2.183	2.178	2.030	1.879	1.710	1.551	1.629	1.759	1.959	2.086	2.267	2.426	2.614	
M_x	.690	.628	.612	.587	.589	.573	.554	.536	.520	.530	.548	.563	.580	.604	.620	.643	
α_x	4.31	2.48	-.56	1.83	1.90	3.86	5.97	8.46	10.95	9.72	7.13	4.84	3.11	.77	-1.16	-3.29	
$\Delta\theta$	-.63	-.32	-.04	.30	.30	.50	.72	.96	1.18	1.08	.84	.60	.43	.16	-.13	-.45	
α_1	-.21	.47	1.06	1.75	1.70	2.37	2.86	3.42	3.60	3.51	3.17	2.61	2.10	1.40	.88	.15	
α_m	-.0581	.1277	.2890	.4735	.4613	.6387	.7697	.9248	.9568	.9387	.8477	.6994	.5652	.3787	.2387	.0400	
c_m	-.1019	-.1006	-.0929	-.0950	-.0954	-.0891	-.0823	-.0600	-.0760	-.0530	-.0744	-.0887	-.0928	-.0935	-.0954	-.1049	
c_o																	
a/b		Pressure coefficient, P															
Upper surface	0.000	1.110	1.102	1.097	1.088	1.089	1.084	1.079	1.073	1.069	1.072	1.077	1.081	1.087	1.086	1.099	1.107
	0.025	.695	.501	.250	-.277	-.272	-.290	-1.318	-1.969	-1.381	-1.721	-2.167	-1.153	-.613	.011	.348	.572
	0.050	.393	.237	.001	-.408	-.399	-.810	-1.178	-1.885	-1.391	-1.680	-1.836	-1.049	-.641	-.186	.050	.309
	0.100	.179	.045	-.134	-.419	-.412	-.670	-.907	-1.625	-1.402	-1.621	-1.179	-.837	-.564	-.265	-.071	.109
	0.200	-.009	-.112	-.243	-.429	-.417	-.584	-.705	-.940	-1.052	-1.052	-.720	-.671	-.494	-.326	-.199	-.064
	0.300	-.119	-.202	-.299	-.438	-.433	-.546	-.633	-.695	-.986	-.870	-.664	-.641	-.502	-.365	-.268	-.163
	0.400	-.179	-.242	-.317	-.431	-.426	-.498	-.557	-.729	-.789	-.680	-.583	-.584	-.463	-.367	-.295	-.214
	0.500	-.249	-.311	-.354	-.434	-.429	-.484	-.517	-.486	-.547	-.482	-.527	-.527	-.457	-.389	-.337	-.276
	0.600	-.301	-.331	-.372	-.423	-.420	-.462	-.472	-.424	-.423	-.393	-.475	-.525	-.445	-.398	-.362	-.317
	0.700	-.338	-.356	-.381	-.413	-.410	-.430	-.422	-.350	-.322	-.316	-.407	-.422	-.420	-.393	-.370	-.344
	0.800	-.302	-.304	-.314	-.331	-.326	-.326	-.299	-.243	-.254	-.234	-.291	-.374	-.326	-.321	-.310	-.301
0.900	-.188	-.176	-.169	-.174	-.171	-.149	-.115	-.121	-.187	-.152	-.130	-.192	-.157	-.168	-.171	-.178	
0.950	-.080	-.005	-.002	-.005	-.001	-.001	.001	-.047	-.149	-.107	-.106	-.054	.004	-.001	0	-.008	
Lower surface	0.0375	-.767	-.837	-.180	.164	.161	.419	.607	.735	.802	.761	.667	.454	.321	.002	-.293	-.811
	0.075	-.787	-.646	-.062	.152	.152	.339	.491	.603	.671	.630	.542	.356	.266	.061	-.122	-.764
	0.150	-.727	-.186	-.018	.133	.132	.263	.381	.476	.536	.495	.422	.264	.215	.065	-.058	-.509
	0.250	-.450	-.048	.023	.129	.131	.223	.309	.336	.297	.257	.315	.187	.174	.078	-.005	-.149
	0.350	-.200	-.024	.034	.118	.117	.189	.263	.327	.365	.334	.289	.170	.164	.076	.014	-.034
	0.450	-.055	.010	.056	.129	.129	.171	.233	.280	.311	.285	.250	.144	.156	.091	.042	.009
	0.550	-.009	.014	.049	.100	.102	.151	.195	.233	.253	.232	.207	.119	.135	.076	.037	.014
	0.650	.017	.021	.045	.079	.083	.119	.161	.189	.197	.180	.169	.085	.107	.063	.037	.022
	0.750	.050	.055	.074	.100	.102	.127	.161	.178	.173	.161	.167	.089	.121	.087	.069	.056
	0.850	.077	.086	.099	.114	.115	.127	.149	.149	.122	.123	.149	.085	.125	.107	.097	.086
	0.925	.106	.117	.128	.137	.138	.139	.149	.131	.082	.093	.143	.091	.145	.135	.129	.116
0.975	.130	.140	.150	.157	.150	.145	.153	.130	.067	.070	.148	.104	.167	.160	.150	.140	
1.000	.140	.151	.160	.171	.160	.150	.160	.128	.066	.060	.150	.111	.180	.173	.163	.154	

^aNo orifice.
^bPaired value.



TABLE 7.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN

NACA 16-505.30 PROPELLER BLADE SECTION ($\alpha = 0.85^\circ$; $\beta_x = 41.10^\circ$;

$\beta_{0.7R} = 45^\circ$; $B = 2$) - Continued.

(b) $N = 1350$ rpm.

	1.762	1.887	2.053	2.186	2.344	2.464	2.610	2.700	2.694	2.538	2.413	2.276	2.126	1.972	1.856	
J	1.762	1.887	2.053	2.186	2.344	2.464	2.610	2.700	2.694	2.538	2.413	2.276	2.126	1.972	1.856	
M_{I_1}	.649	.662	.682	.697	.723	.743	.763	.776	.769	.750	.729	.707	.690	.670	.655	
α_{T_1}	7.68	5.85	3.55	1.80	-.18	-1.60	-3.25	-4.22	-3.72	-2.44	-1.00	.66	2.98	4.66	6.30	
$\Delta\beta$	1.33	1.01	.61	.31	-.05	-.33	-.79	-1.02	-.92	-.54	-.21	.10	.44	.80	1.09	
α_r	3.63	3.13	2.46	1.88	1.22	.79	.15	-.27	-.06	.42	1.03	1.50	2.10	2.74	3.30	
α_H	.9716	.8413	.6639	.5097	.3332	.2142	.0400	-.0723	-.0174	.1135	.2800	.4058	.5681	.7355	.8890	
α_M	-.0655	-.0814	-.0944	-.1029	-.1064	-.1082	-.1240	-.1209	-.1240	-.1196	-.1081	-.1048	-.1001	-.0890	-.0762	
α_0																
o/b	Pressure coefficient, P															
Upper surface	$\theta_{0.000}$	1.109	1.114	1.122	1.128	1.138	1.146	1.154	1.160	1.177	1.149	1.140	1.131	1.129	1.117	1.111
	.025	-2.374	-1.848	-.799	-.202	.249	.484	.634	.702	.668	.566	.385	.069	-.433	-1.246	-2.001
	.050	-2.244	-1.721	-.688	-.384	-.009	.207	.365	.438	.401	.292	.113	-.164	-.566	-1.369	-2.075
	.100	-2.040	-1.222	-.708	-.436	-.171	.002	.141	.209	.174	.076	-.074	-.284	-.554	-.825	-1.558
	.200	-.620	-.635	-.604	-.432	-.292	-.172	-.061	-.005	-.034	-.113	-.223	-.370	-.533	-.643	-.630
	.300	-.648	-.672	-.584	-.482	-.361	-.271	-.183	-.137	-.161	-.227	-.307	-.416	-.527	-.626	-.667
	.400	-.601	-.600	-.537	-.474	-.394	-.330	-.262	-.229	-.246	-.297	-.352	-.434	-.500	-.565	-.596
	.500	-.560	-.562	-.529	-.477	-.424	-.375	-.330	-.310	-.319	-.353	-.390	-.448	-.501	-.541	-.556
	.600	-.509	-.515	-.500	-.471	-.441	-.411	-.385	-.379	-.383	-.401	-.415	-.456	-.486	-.502	-.508
	.700	-.444	-.458	-.462	-.454	-.442	-.435	-.425	-.440	-.437	-.433	-.427	-.449	-.460	-.457	-.448
	.800	-.309	-.318	-.335	-.342	-.347	-.348	-.356	-.377	-.367	-.355	-.335	-.347	-.345	-.324	-.309
.900	-.123	-.114	-.128	-.144	-.155	-.162	-.176	-.199	-.189	-.174	-.147	-.154	-.144	-.116	-.107	
.950	-.006	-.004	.004	.015	.014	.015	.008	-.010	-.001	.008	-.027	.011	.008	0	.004	
Lower surface	.0375	.689	.588	.388	.154	-.161	-.511	-.985	-1.006	-1.005	-1.008	-.271	-.018	.297	.489	.622
	.075	.569	.481	.321	.152	-.042	-.186	-.460	-.949	-.924	-.702	-.113	.058	.225	.400	.511
	.150	.448	.376	.255	.137	-.003	-.106	-.348	-.763	-.682	-.280	-.046	.061	.185	.312	.400
	.250	.288	.242	.210	.129	.035	-.035	-.212	-.465	-.349	-.075	.013	.082	.172	.272	.322
	.350	.311	.263	.189	.127	.046	-.007	-.070	-.239	-.150	-.031	.030	.078	.151	.224	.282
	.450	.270	.231	.187	.135	.069	.030	0	-.092	-.038	.007	.059	.093	.154	.212	.251
	.550	.229	.197	.149	.109	.059	.028	.014	-.032	-.005	.012	.055	.077	.123	.174	.216
	.650	.186	.158	.119	.087	.051	.031	.029	.009	.019	.021	.052	.064	.098	.137	.170
	.750	.183	.159	.131	.109	.082	.068	.063	.047	.056	.057	.086	.090	.116	.144	.170
	.850	.165	.151	.134	.124	.107	.101	.095	.080	.094	.092	.115	.111	.126	.141	.159
	.925	.161	.153	.148	.148	.140	.135	.127	.109	.116	.124	.149	.140	.146	.149	.161
b .975	.165	.185	.160	.166	.170	.160	.150	.130	.143	.153	.174	.164	.161	.154	.189	
b 1.000	.170	.210	.165	.178	.185	.173	.159	.140	.157	.167	.187	.175	.169	.160	.210	

^aNo orifice.
^bFaired value.



TABLE 7.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN

NACA 16-505,30 PROPELLER BLADE SECTION ($\alpha = 0.85^\circ$; $\beta_x = 41.10^\circ$;

$\beta_{0.75R} = 45^\circ$; B = 2) - Continued

(c) $N = 1500$ rpm.

	2.038	2.104	2.233	2.313	2.436	2.540	2.611	2.778	2.897	2.985	2.273	2.177	2.062	1.968	
$\frac{r}{M}$.753	.763	.766	.799	.819	.837	.848	.841	.827	.806	.790	.776	.756	.744	
C_{L1}	3.75	2.86	1.20	.20	-1.27	-2.47	-3.26	-2.89	-1.96	-.67	.70	1.91	3.43	4.71	
AP	.88	.65	.20	-.10	-.53	-.96	-1.22	-1.11	-.76	-.35	.05	.40	.80	1.12	
P_1	2.60	2.33	1.79	1.38	.78	.20	-.08	.01	.54	1.11	1.61	1.97	2.48	2.93	
C_n	.7032	.6303	.4852	.3768	.2123	.0542	-.0219	.0026	.1471	.3039	.4351	.5348	.6703	.7871	
C_m	-.1000	-.1052	-.1124	-.1170	-.1308	-.1447	-.1573	-.1524	-.1383	-.1209	-.1141	-.1114	-.1029	-.0898	
C_o						.0310	.0358	.0329	.0275						
c/b	Pressure coefficient, P														
Upper surface	0.000	1.151	1.155	1.164	1.170	1.179	1.188	1.193	1.189	1.183	1.173	1.166	1.160	1.152	1.147
	.025	-.693	-.589	.035	.283	.509	.643	.775	.739	.632	.433	.182	-.116	-.577	-1.070
	.050	-.860	-.596	-.209	.013	.233	.374	.505	.464	.371	.156	-.078	-.342	-.766	-1.100
	.100	-.920	-.619	-.332	-.159	.027	.152	.275	.237	.153	-.041	-.232	-.437	-.796	-1.137
	.200	-.655	-.610	-.438	-.315	-.164	-.056	.019	-.019	-.056	-.219	-.410	-.585	-.640	-.777
	.300	-.615	-.598	-.495	-.406	-.286	-.193	-.096	-.123	-.188	-.328	-.442	-.541	-.598	-.623
	.400	-.595	-.571	-.502	-.444	-.358	-.282	-.195	-.219	-.273	-.390	-.470	-.539	-.595	-.574
	.500	-.607	-.613	-.580	-.551	-.487	-.422	-.351	-.370	-.415	-.511	-.565	-.595	-.609	-.574
	.600	-.548	-.548	-.529	-.508	-.462	-.419	-.363	-.366	-.398	-.480	-.521	-.537	-.547	-.536
	.700	-.495	-.502	-.498	-.517	-.460	-.422	-.399	-.408	-.439	-.509	-.517	-.505	-.499	-.482
	.800	-.332	-.343	-.339	-.345	-.335	-.332	-.340	-.316	-.287	-.341	-.344	-.343	-.336	-.324
.900	-.109	-.117	-.114	-.116	-.113	-.098	-.086	-.045	-.060	-.111	-.114	-.116	-.110	-.105	
.950	.021	.026	.034	.034	.034	.046	.095	.095	.092	.041	.035	.032	.026	.020	
Lower surface	.0375	.403	.282	.054	-.154	-.1054	-.1.238	-.1.281	-.1.258	-.1.196	-.626	-.056	.149	.358	.513
	.075	.340	.249	.107	-.033	-.273	-.1.125	-.1.179	-.1.152	-.1.062	-.082	.038	.154	.304	.424
	.150	.273	.207	.107	-.007	-.046	-.907	-.1.059	-.1.023	-.1.135	-.051	.052	.142	.248	.338
	.250	^b .222	.163	.117	.049	-.009	-.043	-.353	-.143	.049	.009	.079	.130	^b .194	^b .272
	.350	.204	.164	.108	.056	.008	-.021	-.057	.062	.058	.026	.080	.132	.190	.246
	.450	.193	.167	.121	.080	.041	.047	.105	.104	.090	.057	.099	.141	.185	.223
	.550	.162	.135	.099	.066	.036	.040	.108	.095	.084	.049	.081	.114	.154	.192
	.650	.127	.105	.082	.057	.036	.036	.103	.092	.081	.046	.067	.091	.122	.151
	.750	.140	.123	.105	.086	.071	.073	.132	.127	.122	.080	.095	.112	.136	.158
	.850	.142	.133	.122	.114	.105	.108	.161	.152	.158	.111	.119	.129	.141	.157
	.925	.156	.153	.152	.145	.141	.143	.193	.195	.195	.145	.147	.153	.157	.165
^b .975	.170	.172	.180	.172	.171	.175	.220	.219	.226	.166	.175	.180	.167	.178	
^a 1.000	.177	.182	.192	.188	.186	.189	.235	.230	.240	.178	.190	.193	.172	.183	

^aNo orifice.

^bPaired values.



TABLE 7.—PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN

NACA 16-505.30 PROPELLER BLADE SECTION ($\alpha = 0.85$; $\beta_x = 41.10^\circ$;

$\beta_{0.75R} = 45^\circ$; $B = 2$) — Continued

(d) $N = 1600$ rpm.

	2.545	2.493	2.438	2.360	2.302	2.240	2.151	2.080	2.115	2.191	2.269	2.337	2.396	2.469	2.529	
τ	.903	.886	.876	.861	.852	.840	.826	.815	.817	.831	.843	.858	.867	.881	.894	
$\Delta \delta H_c^2$	-2.52	-1.93	-1.30	-.37	.34	1.11	2.25	3.18	2.72	1.73	.75	-.09	-.80	-1.66	-2.34	
δF	-1.13	-.94	-.67	-.31	-.05	.22	.62	.95	.79	.44	.09	-.21	-.47	-.81	-1.08	
δF	-.38	.07	.53	.93	1.35	1.74	2.22	2.52	2.32	1.98	1.56	1.12	.77	.36	-.10	
δF	-1.019	.0194	.1445	.2523	.3665	.4723	.6013	.6800	.6277	.5361	.4245	.3045	.2103	.0981	-.0277	
δF	-1.516	-1.622	-1.472	-1.368	-1.257	-1.125	-1.226	-1.141	-1.173	-1.255	-1.259	-1.311	-1.386	-1.560	-1.598	
δF	.0425	.0393	.0327	.0253	.0193	.0121	.0017			.0069	.0155	.0226	.0280	.0363	.0411	
α/b	Pressure coefficient, P															
Upper surface	.000	1.221	1.211	1.206	1.199	1.195	1.190	1.182	1.177	1.178	1.185	1.191	1.197	1.202	1.209	1.216
	.025	.715	.699	.585	.482	.363	.187	-.084	-.292	-.162	.055	.276	.426	.514	.624	.693
	.050	.460	.398	.318	.211	.093	-.074	-.323	-.526	-.396	-.196	.007	.152	.244	.374	.434
	.100	.245	.184	.110	.009	-.096	-.236	-.427	-.636	-.499	-.330	-.167	-.043	.041	.148	.217
	.200	.032	-.026	-.096	-.184	-.274	-.379	-.536	-.748	-.544	-.464	-.331	-.227	-.159	-.061	.003
	.300	-.109	-.165	-.227	-.307	-.378	-.491	-.649	-.762	-.704	-.565	-.454	-.348	-.287	-.198	-.138
	.400	-.188	-.230	-.279	-.363	-.441	-.530	-.670	-.818	-.717	-.599	-.497	-.406	-.334	-.255	-.211
	.500	-.328	-.377	-.423	-.474	-.520	-.589	-.675	-.781	-.714	-.640	-.556	-.499	-.466	-.403	-.355
	.600	-.431	-.484	-.535	-.588	-.627	-.664	-.730	-.843	-.733	-.694	-.650	-.612	-.579	-.512	-.458
	.700	-.577	-.625	-.667	-.699	-.743	-.776	-.835	-.945	-.843	-.751	-.765	-.730	-.701	-.648	-.605
	.800	-.678	-.678	-.687	-.678	-.698	-.689	-.676	-.624	-.624	-.622	-.626	-.646	-.628	-.605	-.697
.900	-.755	-.745	-.724	-.702	-.688	-.671	-.674	-.682	-.673	-.670	-.678	-.610	-.620	-.630	-.645	
.950	-.093	-.082	-.061	-.040	-.026	-.002	.023	.040	.040	.009	-.014	-.043	-.060	-.069	-.087	
Lower surface	.0375	-1.083	-1.052	-.986	-.865	-.716	-.629	-.472	-.302	-.235	-.071	-.123	-.749	-.932	-1.026	-1.080
	.075	-.997	-.962	-.893	-.740	-.592	-.460	-.272	-.268	-.220	.113	-.006	-.186	-.827	-.935	-.993
	.150	-.903	-.864	-.776	-.615	-.419	-.265	-.155	-.224	-.192	.114	.022	-.034	-.210	-.832	-.895
	.250	-.790	-.720	-.607	-.417	-.232	-.081	-.122	-.131	-.131	.115	.055	.009	.012	-.331	-.772
	.350	-.737	-.667	-.537	-.286	-.040	.082	.157	.180	.163	.109	.061	.023	.015	-.026	-.351
	.450	-.730	-.665	-.559	-.353	.063	.096	.143	.178	.168	.117	.080	.049	.040	.069	-.002
	.550	-.629	-.664	-.642	-.539	.048	.075	.113	.149	.136	.092	.061	.034	.025	.051	.068
	.650	-.675	-.648	-.628	-.528	.035	.060	.088	.117	.108	.073	.048	.025	.014	.036	.065
	.750	-.689	-.666	-.656	-.560	.024	.085	.110	.134	.127	.095	.075	.055	.045	.060	.078
	.850	-.691	-.680	-.678	-.684	.029	.106	.124	.144	.141	.114	.097	.079	.068	.078	.086
	.925	-.693	-.692	-.696	-.706	.112	.127	.146	.166	.163	.135	.121	.101	.091	.095	.093
.975	-.699	-.710	-.710	-.725	.130	.147	.168	.180	.178	.156	.140	.120	.119	.110	.108	
1.000	.100	.118	.118	.134	.141	.155	.179	.190	.185	.166	.150	.126	.132	.118	.111	

^aNo orifice.

^bPaired value.



TABLE 7.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN
 NACA 16-505.30 PROPELLER BLADE SECTION ($\alpha = 0.85$; $\beta_x = 41.10^\circ$;
 $\beta_{0.75R} = 45^\circ$; $B = 2$) - Continued

(e) $M = 0.56$.

	2.128	2.152	2.192	2.235	2.276	2.323	2.367	2.414	2.453	2.514	2.564	2.602	2.659	2.460	
C_L	.918	.903	.894	.885	.876	.868	.859	.850	.840	.832	.823	.814	.805	.838	
C_{Dp}	2.55	2.24	1.72	1.17	.66	.08	-.45	-1.01	-1.47	-2.17	-2.74	-3.16	-3.78	-1.55	
C_{Df}	.18	.08	-.03	-.12	-.17	-.21	-.30	-.45	-.58	-.74	-.86	-.94	-1.06	-.60	
C_{Dc}	1.98	1.86	1.74	1.77	1.46	1.21	1.08	.90	.73	.39	.21	.02	-.16	.69	
C_{Dc}	.5361	.5026	.4729	.4258	.3968	.3290	.2942	.2452	.1994	.1071	.0568	.0065	-.0439	.1890	
C_{Dc}	-.1385	-.1350	-.1299	-.1247	-.1245	-.1257	-.1316	-.1342	-.1321	-.1372	-.1417	-.1419	-.1347	-.1314	
C_{Dc}	.0202	.0203	.0205	.0213	.0213	.0222	.0231	.0249	.0262	.0289					
c/b	Pressure coefficient, P														
Upper surface	$c/b = 0.000$	1.228	1.221	1.216	1.211	1.207	1.202	1.198	1.194	1.189	1.185	1.181	1.177	1.173	1.188
	0.025	.210	.219	.253	.303	.338	.425	.464	.513	.553	.610	.677	.678	.708	.537
	0.050	-.050	-.043	-.015	.031	.063	.148	.188	.238	.281	.338	.437	.409	.444	.265
	0.100	-.212	-.207	-.186	-.152	-.128	-.051	-.014	.032	.070	.122	.167	.185	.217	.095
	0.200	-.359	-.367	-.358	-.324	-.308	-.238	-.205	-.167	-.133	-.086	-.044	-.029	-.001	-.145
	0.300	-.462	-.469	-.455	-.430	-.406	-.347	-.324	-.290	-.260	-.220	-.180	-.166	-.139	-.272
	0.400	-.544	-.546	-.532	-.507	-.491	-.436	-.400	-.381	-.356	-.314	-.271	-.256	-.229	-.369
	0.500	-.610	-.617	-.607	-.588	-.586	-.526	-.498	-.471	-.439	-.427	-.374	-.354	-.327	-.454
	0.600	-.668	-.683	-.680	-.670	-.697	-.594	-.583	-.547	-.513	-.453	-.442	-.434	-.410	-.522
	0.700	-.794	-.815	-.815	-.802	-.793	-.723	-.702	-.679	-.639	-.623	-.588	-.551	-.507	-.634
	0.800	-.324	-.317	-.293	-.284	-.280	-.319	-.380	-.406	-.362	-.340	-.355	-.373	-.383	-.384
0.900	-.280	-.269	-.243	-.222	-.180	-.113	-.072	-.068	-.092	-.113	-.136	-.130	-.180	-.110	
0.950	-.274	-.261	-.233	-.206	-.155	-.070	-.001	-.036	-.049	-.047	-.043	-.031	-.010	-.029	
Lower surface	0.0375	.096	.022	-.039	-.116	-.191	-.246	-.311	-.375	-.409	-.4209	-.4322	-.4403	-.4429	-.4117
	0.075	.157	.105	-.057	-.107	-.132	-.161	-.192	-.214	-.263	-.299	-.3206	-.3283	-.3294	-.2992
	0.150	.144	.096	-.061	-.016	-.006	-.018	-.019	-.015	-.065	-.145	-.1739	-.1788	-.1661	-.110
	0.250	.152	.111	-.086	-.053	-.039	-.032	-.022	-.013	-.008	-.007	-.033	-.023	-.215	-.009
	0.350	.130	.095	-.074	-.049	-.040	-.040	-.020	-.021	-.014	-.012	-.006	-.007	-.105	-.005
	0.450	.132	.100	-.084	-.063	-.060	-.065	-.062	-.053	-.046	-.018	-.035	-.024	-.034	-.027
	0.550	.093	.063	-.052	-.036	-.036	-.047	-.048	-.042	-.038	-.011	-.032	-.021	-.008	-.019
	0.650	.055	.030	-.021	-.011	-.014	-.033	-.039	-.038	-.037	-.011	-.034	-.026	-.014	-.017
	0.750	.064	.041	-.035	-.029	-.037	-.061	-.072	-.074	-.076	-.076	-.074	-.066	-.057	-.057
	0.850	.058	.036	-.034	-.032	-.046	-.078	-.097	-.105	-.108	-.107	-.107	-.100	-.090	-.087
	0.925	.056	.034	-.034	-.036	-.055	-.095	-.123	-.137	-.145	-.147	-.146	-.140	-.126	-.125
0.975	.059	.037	-.039	-.035	-.059	-.110	-.145	-.164	-.175	-.185	-.178	-.170	-.160	-.156	
1.000	.062	.038	-.040	-.035	-.060	-.120	-.157	-.180	-.190	-.217	-.195	-.188	-.180	-.173	

^aNo airfoil.
^bPaired value.



TABLE 7.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN

NACA 16-505.30 PROPELLER BLADE SECTION ($x = 0.85$; $\beta_x = 41.10^\circ$; $\beta_{0.75R} = 45^\circ$; $B = 2$) - Continued(r) $M = 0.58$.

J	2.163	2.177	2.216	2.240	2.270	2.324	2.350	2.387	2.414	2.449	2.481	2.526	2.563	2.601	2.636	
M_x	.934	.923	.915	.906	.899	.897	.884	.881	.871	.869	.858	.854	.843	.837	.831	
α_x'	2.09	1.91	1.41	1.11	.73	.07	-.25	-.69	-1.01	-1.42	-1.80	-2.31	-2.73	-3.15	-3.53	
$\Delta\theta$.09	.02	-.16	-.26	-.38	-.50	-.53	-.56	-.59	-.65	-.73	-.86	-.99	-1.11	-1.22	
α_1	1.79	1.62	1.50	1.39	1.32	1.08	.93	.84	.72	.65	.53	.34	.09	-.04	-.21	
α_n	.4839	.4374	.4058	.3768	.3594	.2948	.2535	.2284	.1974	.1761	.1439	.0916	.0252	-.0103	-.0581	
α_m	-.1553	-.1414	-.1416	-.1354	-.1331	-.1390	-.1421	-.1434	-.1481	-.1527	-.1552	-.1596	-.1540	-.1499	-.1496	
α_c	.0283	.0269	.0262	.0262	.0262	.0290	.0295	.0296	.0308	.0319	.0319	.0338	.0343	.0343	.0356	
c/b	Pressure coefficient, P															
Upper surfaces	∞	1.237	1.231	1.227	1.222	1.218	1.217	1.210	1.209	1.204	1.203	1.197	1.195	1.190	1.187	1.184
	.025	.317	.345	.375	.394	.413	.479	.502	.530	.549	.577	.608	.645	.676	.695	.723
	.050	.055	.080	.108	.125	.143	.209	.231	.258	.278	.307	.337	.410	.430	.460	.460
	.100	-.120	-.102	-.079	-.067	-.054	.005	.024	.048	.065	.092	.118	.155	.184	.202	.230
	.200	-.270	-.265	-.244	-.241	-.233	-.184	-.169	-.149	-.135	-.112	-.089	-.057	-.032	-.016	.009
	.300	-.386	-.376	-.363	-.354	-.351	-.304	-.289	-.275	-.265	-.244	-.222	-.194	-.172	-.157	-.133
	.400	-.472	-.462	-.441	-.433	-.420	-.381	-.370	-.351	-.335	-.322	-.322	-.300	-.275	-.262	-.239
	.500	-.487	-.479	-.465	-.470	-.471	-.437	-.432	-.424	-.429	-.422	-.411	-.410	-.406	-.402	-.368
	.600	-.608	-.607	-.599	-.606	-.608	-.576	-.571	-.562	-.577	-.538	-.506	-.487	-.416	-.402	-.401
	.700	-.706	-.715	-.707	-.717	-.725	-.702	-.708	-.697	-.692	-.670	-.668	-.642	-.643	-.649	-.625
	.800	-.598	-.478	-.411	-.383	-.371	-.434	-.441	-.435	-.465	-.506	-.539	-.576	-.458	-.381	-.359
.900	-.315	-.295	-.251	-.235	-.214	-.200	-.175	-.151	-.142	-.113	-.108	-.064	-.080	-.103	-.124	
.950	-.297	-.266	-.234	-.214	-.184	-.160	-.123	-.083	-.063	-.041	-.001	.022	-.040	.041	.040	
Lower surfaces	.0375	0	-.093	-.215	-.356	-.487	-.720	-.805	-.876	-.948	-1.011	-1.083	-1.165	-1.250	-1.313	-1.380
	.075	.102	.053	.017	0	-.046	-.294	-.702	-.779	-.855	-.917	-.987	-1.068	-1.148	-1.209	-1.272
	.150	.104	.067	.040	.017	.002	-.009	-.078	-.246	-.459	-.675	-.785	-.941	-1.026	-1.081	-1.138
	.250	.117	.092	.076	.059	.048	.033	.029	.032	.027	.017	.008	-.090	-.207	-.290	-.382
	.350	.116	.092	.080	.066	.055	.040	.032	.035	.031	.036	.042	.043	.028	0	-.077
	.450	.120	.100	.091	.079	.073	.060	.056	.058	.054	.057	.061	.066	.064	.060	.077
	.550	.085	.069	.063	.054	.049	.040	.036	.041	.038	.044	.051	.052	.052	.048	.049
	.650	.048	.034	.032	.026	.025	.017	.017	.025	.024	.033	.043	.048	.047	.044	.046
	.750	.061	.049	.069	.044	.044	.041	.044	.054	.056	.065	.079	.082	.083	.079	.080
	.850	.063	.054	.076	.050	.054	.054	.054	.075	.080	.092	.108	.113	.116	.111	.111
	.925	.065	.054	.076	.054	.054	.059	.062	.074	.093	.102	.118	.138	.143	.144	.144
.975	.069	.052	.074	.057	.058	.069	.066	.086	.109	.120	.135	.161	.173	.170	.175	
1.000	.071	.051	.077	.055	.055	.070	.092	.117	.129	.145	.177	.190	.189	.182	.189	

^aNo orifice.^bFaired value.

TABLE 7.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN
 NACA 16-505.30 PROPELLER BLADE SECTION ($\alpha = 0.85^\circ$; $\beta_x = 41.10^\circ$;

$\beta_{0.75R} = 45^\circ$; $B = 2$) - Continued

(g) $M = 0.60$.

	2.135	2.158	2.173	2.220	2.240	2.265	2.290	2.314	2.346	2.370	2.392	2.429	2.464	2.496	2.522	2.560	
σ	.977	.970	.958	.939	.951	.945	.939	.933	.926	.921	.911	.908	.901	.898	.890	.883	
M_x	2.46	2.16	1.96	1.36	1.11	.80	.48	.19	-.20	-.49	-.73	-1.19	-1.60	-1.97	-2.26	-2.69	
$C_{p,x}$	-.25	-.27	-.28	-.33	-.37	-.44	-.51	-.60	-.72	-.79	-.85	-.94	-1.01	-1.07	-1.11	-1.16	
$C_{p,y}$	1.69	1.55	1.49	1.29	1.18	1.10	.98	.90	.71	.59	.49	.28	.13	.02	-.04	-.20	
$C_{p,z}$.4574	.4000	.4026	.3497	.3200	.2974	.2665	.2452	.1929	.1594	.1323	.0774	.0348	.0052	-.0123	-.0542	
$C_{p,w}$	-.1794	-.1726	-.1680	-.1639	-.1601	-.1624	-.1614	-.1650	-.1622	-.1621	-.1626	-.1590	-.1576	-.1573	-.1599	-.1588	
C_o	.0407	.0379	.0370	.0373	.0370	.0375	.0378	.0380	.0384	.0387	.0387	.0397	.0399	.0399	.0396	.0400	
c/b	Pressure coefficient, P																
Upper surface	0.000	1.261	1.257	1.250	1.251	1.247	1.244	1.240	1.237	1.233	1.230	1.225	1.223	1.220	1.218	1.214	1.210
	.025	.406	.418	.420	.465	.479	.499	.529	.555	.565	.579	.595	.619	.642	.661	.671	.705
	.050	.154	.163	.161	.206	.218	.238	.268	.291	.303	.316	.332	.359	.380	.403	.412	.447
	.100	-.015	-.010	-.014	.024	.032	.050	.075	.094	.105	.116	.130	.153	.171	.189	.196	.228
	.200	-.209	-.196	-.197	-.156	-.152	-.140	-.118	-.101	-.090	-.082	-.070	-.051	-.035	-.019	-.015	.014
	.300	-.312	-.296	-.300	-.271	-.263	-.252	-.240	-.224	-.210	-.208	-.201	-.185	-.174	-.160	-.155	-.129
	.400	-.383	-.382	-.390	-.356	-.348	-.332	-.314	-.303	-.294	-.282	-.270	-.240	-.228	-.222	-.221	-.221
	.500	-.437	-.443	-.447	-.414	-.410	-.405	-.393	-.385	-.380	-.378	-.373	-.370	-.373	-.368	-.369	-.358
	.600	-.539	-.541	-.548	-.524	-.525	-.520	-.513	-.507	-.505	-.502	-.498	-.494	-.488	-.477	-.471	-.447
	.700	-.642	-.652	-.663	-.636	-.638	-.636	-.634	-.631	-.634	-.635	-.634	-.629	-.628	-.620	-.617	-.608
	.800	-.752	-.756	-.767	-.751	-.757	-.753	-.747	-.742	-.737	-.739	-.730	-.727	-.715	-.699	-.692	-.682
	.900	-.667	-.687	-.708	-.671	-.649	-.613	-.582	-.557	-.527	-.493	-.458	-.416	-.377	-.355	-.336	-.302
	.950	-.455	-.411	-.371	-.339	-.320	-.283	-.254	-.229	-.215	-.198	-.169	-.155	-.129	-.102	-.077	-.041
Lower surface	.0375	-.154	-.252	-.318	-.446	-.511	-.569	-.629	-.672	-.731	-.807	-.894	-.921	-.982	-1.031	-1.084	-1.148
	.075	.047	-.044	-.114	-.332	-.441	-.498	-.556	-.597	-.675	-.729	-.774	-.838	-.899	-.947	-.997	-1.061
	.150	.069	.036	.020	-.012	-.094	-.228	-.379	-.472	-.578	-.634	-.678	-.745	-.804	-.851	-.898	-.960
	.250	.107	.065	.071	.054	.040	.038	.031	-.124	-.235	-.340	-.372	-.467	-.573	-.671	-.771	-.840
	.350	.100	.083	.071	.061	.051	.055	.061	.040	.035	.030	-.024	-.104	-.163	-.215	-.230	-.230
	.450	.109	.095	.083	.079	.072	.073	.077	.085	.070	.070	.073	.068	.054	.042	.033	.013
	.550	.069	.058	.049	.048	.042	.045	.050	.058	.046	.045	.051	.055	.057	.063	.062	.067
	.650	.089	.020	.013	.015	.010	.014	.019	.028	.018	.019	.026	.032	.038	.048	.051	.068
	.750	.046	.039	.031	.033	.028	.033	.038	.044	.035	.035	.043	.047	.052	.062	.066	.084
	.850	.066	.058	.047	.049	.043	.043	.047	.054	.043	.043	.052	.055	.060	.072	.080	.098
	.925	.085	.074	.061	.061	.052	.051	.052	.059	.046	.046	.056	.059	.067	.079	.091	.113
	.975	.100	.082	.070	.070	.069	.065	.076	.067	.044	.047	.057	.066	.074	.088	.106	.128
	1.000	.110	.085	.077	.077	.075	.067	.058	.070	.044	.047	.057	.066	.074	.093	.110	.132

^aNo orifices.
^bPaired values.



TABLE 7.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN

NACA 16-505.30 PROPELLER BLADE SECTION ($\alpha = 0.85$; $\beta_x = 41.10^\circ$; $\beta_{0.7R} = 45^\circ$; $B = 2$) - Concluded(h) $M = 0.65$.

	2.472	2.446	2.411	2.374	2.351	2.317	2.280	2.264	2.233	2.205	2.170	2.147	2.117	
J	.947	.956	.964	.972	.985	.989	.995	1.007	1.015	1.023	1.031	1.037	1.046	
C_{L1}	-1.69	-1.39	-.98	-.54	-.26	.15	.61	.81	1.20	1.55	2.00	2.30	2.69	
$\Delta\delta$	-1.37	-1.33	-1.28	-1.21	-1.17	-1.11	-1.03	-.91	-.93	-.87	-.79	-.74	-.66	
α_1	-.52	-.38	-.15	.06	.24	.43	.58	.73	.90	1.03	1.17	1.31	1.41	
α_n	-.1426	-.1045	-.0413	.0168	.0658	.1174	.1568	.1974	.2426	.2787	.3174	.3529	.3794	
α_m	-.1281	-.1336	-.1416	-.1580	-.1706	-.1742	-.1785	-.1898	-.1939	-.1925	-.1894	-.1917	-.1904	
α_c	.0449	.0449	.0457	.0499	.0518	.0514	.0508	.0539	.0543	.0520	.0508	.0499	.0490	
o/b	Pressure coefficient, P													
Upper surface	^a 0.000	1.244	1.249	1.254	1.258	1.266	1.268	1.272	1.279	1.284	1.285	1.294	1.301	1.304
	.025	.712	.694	.655	.644	.637	.619	.597	.586	.568	.554	.535	.513	.505
	.050	.461	.445	.414	.394	.386	.371	.348	.336	.319	.303	.286	.265	.261
	.100	.255	.243	.215	.197	.194	.181	.160	.151	.137	.123	.112	.098	.096
	.200	.050	.040	.016	0	.001	-.011	-.030	-.037	-.044	-.054	-.069	-.064	-.091
	.300	-.085	-.093	-.109	-.115	-.114	-.133	-.143	-.145	-.162	-.169	-.171	-.183	-.191
	.400	-.143	-.157	-.184	-.205	-.205	-.211	-.226	-.234	-.246	-.258	-.266	-.275	-.274
	.500	-.277	-.274	-.282	-.290	-.286	-.292	-.299	-.300	-.307	-.317	-.324	-.332	-.328
	.600	-.396	-.395	-.406	-.414	-.406	-.409	-.414	-.414	-.420	-.420	-.423	-.431	-.426
	.700	-.508	-.526	-.533	-.532	-.521	-.522	-.524	-.519	-.520	-.524	-.525	-.527	-.521
	.800	-.643	-.640	-.643	-.630	-.643	-.640	-.641	-.637	-.635	-.635	-.635	-.638	-.627
	.900	-.849	-.825	-.809	-.683	-.795	-.795	-.758	-.793	-.788	-.784	-.778	-.775	-.763
.950	-.801	-.732	-.886	-.344	-.421	-.477	-.585	-.805	-.828	-.822	-.815	-.812	-.800	
Lower surface	^a 0.0375	-.889	-.835	-.775	-.723	-.662	-.617	-.560	-.501	-.442	-.380	-.321	-.253	-.182
	.075	-.813	-.762	-.704	-.654	-.597	-.553	-.500	-.446	-.391	-.333	-.276	-.214	-.141
	.150	-.731	-.681	-.624	-.577	-.519	-.475	-.425	-.373	-.315	-.256	-.202	-.133	-.018
	.250	-.628	-.577	-.520	-.475	-.419	-.379	-.334	-.292	-.234	-.133	-.013	.051	.096
	.350	-.612	-.566	-.517	-.475	-.419	-.370	-.325	-.289	-.209	-.077	0	.034	.060
	.450	-.545	-.496	-.440	-.346	-.220	-.076	-.016	-.018	-.017	.044	.073	.091	.119
	.550	-.218	-.172	-.100	-.065	.002	.037	.037	.018	.025	.039	.052	.060	.084
	.650	.033	.045	.042	.037	.040	.045	.037	.022	.010	.005	.009	.013	.032
	.750	.085	.085	.072	.061	.063	.064	.060	.051	.043	.037	.035	.033	.047
	.850	.086	.085	.074	.068	.072	.077	.078	.081	.081	.084	.087	.090	.100
	^b .925	.073	.072	.066	.066	.077	.085	.093	.102	.109	.118	.127	.133	.148
	.975	.074	.070	.068	.070	.077	.095	.110	.120	.127	.142	.154	.165	.182
^a 1.000	.075	.071	.070	.076	.077	.100	.115	.130	.140	.160	.169	.182	.200	

^aNo crifices.^bInterpolated values.

TABLE B.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN

NACA 16-504.80 PROPELLER BLADE SECTION ($x = 0.90$; $\beta_x = 39.50^\circ$;

$\beta_{0.75R} = 45^\circ$; $B = 2$)

(a) $N = 1140$ rpm.

	1.579	1.739	1.876	1.983	2.114	2.255	2.379	2.505	2.635	2.712	2.667	2.578	2.445	2.313	2.170	2.053	1.913	1.806	1.649	
J	1.579	1.739	1.876	1.983	2.114	2.255	2.379	2.505	2.635	2.712	2.667	2.578	2.445	2.313	2.170	2.053	1.913	1.806	1.649	
M_x	.558	.571	.588	.596	.611	.627	.640	.653	.667	.679	.675	.662	.645	.628	.616	.602	.589	.579	.568	
α_x	10.32	7.90	5.93	4.45	2.71	.92	-.78	-2.04	-3.49	-4.31	-3.83	-2.86	-1.36	.21	1.99	3.51	5.41	6.93	9.24	
$\Delta\theta$	1.26	.99	.76	.56	.40	.12	-.12	-.36	-.61	-.76	-.68	-.50	-.24	.01	.29	.47	.70	.88	1.14	
α_1	3.97	3.68	3.14	2.67	2.18	1.65	1.19	.66	.12	-.19	-.05	.35	.94	1.47	1.98	2.44	2.93	3.45	3.79	
c_D	.8716	.8239	.6948	.6000	.4916	.3632	.2577	.1432	.0213	-.0510	-.0116	.0839	.2084	.3219	.4361	.5387	.6471	.7458	.8329	
c_M	-.0513	-.0629	-.0801	-.0852	-.0878	-.0902	-.0918	-.0993	-.1057	-.1042	-.1073	-.1044	-.0955	-.0916	-.0890	-.0852	-.0814	-.0711	-.0523	
c_c																				
a/b	Pressure coefficient, P																			
Upper surface	$a_0.000$	1.080	1.084	1.089	1.091	1.096	1.102	1.106	1.111	1.116	1.121	1.119	1.114	1.108	1.102	1.098	1.093	1.089	1.086	1.083
	.025	-1.770	-1.979	-1.183	-.766	-.364	.042	.311	.491	.617	.677	.649	.562	.416	.170	-.170	-.554	-.923	-1.916	-1.693
	.050	-1.715	-1.793	-.982	-.738	-.474	-.171	.044	.215	.341	.404	.374	.284	.140	-.070	-.294	-.595	-.883	-1.302	-1.652
	.100	-1.513	-1.283	-.822	-.662	-.483	-.284	-.131	.002	.109	.166	.138	.061	-.058	-.216	-.393	-.547	-.751	-.894	-1.494
	.200	-.913	-.672	-.604	-.514	-.423	-.295	-.182	-.118	-.040	.001	-.020	-.075	-.159	-.263	-.380	-.458	-.560	-.631	-.878
	.300	-.746	-.589	-.557	-.499	-.430	-.339	-.271	-.202	-.142	-.108	-.126	-.169	-.231	-.308	-.391	-.447	-.526	-.576	-.615
	.400	-.567	-.527	-.506	-.465	-.405	-.347	-.300	-.248	-.202	-.174	-.190	-.221	-.269	-.326	-.377	-.428	-.485	-.517	-.509
	.500	-.457	-.482	-.479	-.454	-.408	-.365	-.332	-.296	-.263	-.239	-.250	-.273	-.308	-.350	-.386	-.425	-.461	-.478	-.446
	.600	-.379	-.434	-.444	-.431	-.403	-.369	-.346	-.323	-.301	-.286	-.294	-.308	-.330	-.359	-.384	-.410	-.432	-.437	-.388
	.700	-.309	-.369	-.395	-.393	-.375	-.353	-.340	-.327	-.314	-.306	-.313	-.316	-.330	-.346	-.364	-.378	-.388	-.381	-.325
	.800	-.233	-.288	-.315	-.328	-.324	-.309	-.308	-.305	-.306	-.302	-.304	-.300	-.303	-.310	-.316	-.319	-.315	-.299	-.242
.900	-.153	-.138	-.149	-.165	-.172	-.169	-.176	-.179	-.190	-.194	-.192	-.179	-.172	-.173	-.170	-.164	-.151	-.143	-.136	
.950	-.109	-.037	-.026	-.027	-.027	-.023	-.031	-.036	-.047	-.055	-.051	-.037	-.028	-.024	-.023	-.021	-.029	-.067		
Lower surface	.0375	.707	.638	.525	.398	.229	.016	-.164	-.783	-.838	-.841	-.838	-.858	-.704	.113	.300	.475	.582	.660	
	.075	.580	.517	.419	.320	.198	.060	-.079	-.458	-.806	-.805	-.824	-.719	-.147	.008	.135	.258	.383	.469	
	.150	.459	.410	.333	.259	.178	.114	.012	-.072	-.509	-.645	-.610	-.276	-.026	.067	.142	.217	.307	.371	
	.250	.248	.297	.244	.187	.130	.084	.023	-.020	-.164	-.345	-.247	-.046	.003	.064	.120	.169	.221	.260	
	.350	.299	.266	.216	.172	.128	.079	.027	-.011	-.050	-.155	-.081	-.016	.011	.055	.106	.151	.202	.240	
	.450	.248	.230	.189	.153	.119	.084	.044	.011	-.005	-.048	-.017	.009	.031	.064	.102	.138	.177	.209	
	.550	.217	.203	.169	.146	.121	.090	.057	.033	.020	.007	.018	.030	.050	.074	.110	.134	.164	.185	
	.650	.162	.161	.134	.110	.090	.065	.040	.026	.022	.022	.022	.028	.038	.053	.077	.101	.126	.144	
	.750	.139	.149	.130	.113	.101	.084	.066	.056	.049	.050	.050	.056	.065	.074	.093	.110	.128	.141	
	.850	.117	.143	.130	.123	.119	.111	.098	.087	.080	.079	.078	.088	.097	.104	.115	.123	.131	.139	
	.925	.113	.161	.156	.153	.156	.149	.139	.133	.122	.116	.119	.132	.142	.143	.153	.156	.158	.158	
.975	.119	.180	.180	.184	.185	.182	.163	.185	.160	.142	.150	.170	.184	.180	.190	.185	.180	.180		
$a_{1.000}$.125	.190	.197	.200	.200	.200	.180	.215	.180	.158	.169	.190	.210	.199	.210	.200	.200	.197		

^aNo orifice.
^bPaired values.

TABLE 8.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN
NACA 16-504.80 PROPELLER BLADE SECTION ($x = 0.90$; $\beta_x = 39.50^\circ$;

$\beta_{0.75R} = 45^\circ$; $B = 2$) - Continued

(c) $N = 1500$ rpm.

	2.004	2.059	2.133	2.218	2.304	2.392	2.476	2.563	2.634	2.596	2.523	2.438	2.352	2.261	2.186	2.106	2.048	
r	.783	.793	.807	.817	.828	.842	.858	.874	.885	.877	.867	.851	.837	.821	.813	.798	.791	
C_{LH}	4.17	3.44	2.21	1.39	.32	-.73	-1.71	-2.69	-3.47	-3.03	-2.24	-1.27	-.26	.85	1.79	2.82	3.43	
$\Delta\theta$	1.02	.81	.46	.21	-.11	-.45	-.81	-1.22	-1.58	-1.39	-1.03	-.64	-.29	.05	.33	.64	.85	
C_{DH}	3.01	2.72	2.41	2.03	1.63	1.23	.78	.34	-.31	-.07	.51	.98	1.38	1.93	2.24	2.59	2.83	
C_{FH}	.6697	.6065	.5384	.4555	.3642	.2768	.1742	.0768	-.0690	-.0161	.1148	.2200	.3090	.4310	.5000	.5790	.6290	
e_0	-.1000	-.1037	-.1104	-.1112	-.1155	-.1229	-.1434	-.1619	-.1632	-.1598	-.1555	-.1298	-.1184	-.1139	-.1084	-.1077	-.1016	
c/p	Pressure coefficient, P																	
Upper surface	^a 0.000	1.163	1.167	1.173	1.178	1.183	1.189	1.197	1.205	1.211	1.207	1.202	1.194	1.187	1.180	1.176	1.169	1.166
	.025	-.505	-.317	-.045	.146	.353	.497	.604	.691	.760	.729	.650	.559	.434	.252	.043	-.192	-.375
	.050	-.743	-.547	-.301	-.130	.064	.205	.319	.413	.488	.454	.367	.271	.142	-.031	-.221	-.430	-.611
	.100	-.842	-.710	-.448	-.306	-.149	-.022	.084	.168	.239	.205	.128	.035	-.082	-.229	-.380	-.591	-.759
	.200	-.714	-.667	-.537	-.370	-.268	-.172	-.089	-.018	.045	.014	-.052	-.127	-.217	-.320	-.424	-.605	-.677
	.300	-.552	-.450	-.484	-.447	-.372	-.294	-.225	-.168	-.110	-.138	-.192	-.255	-.331	-.410	-.472	-.486	-.427
	.400	-.479	-.524	-.491	-.464	-.423	-.371	-.312	-.265	-.219	-.242	-.285	-.340	-.397	-.445	-.481	-.510	-.516
	.500	-.533	-.545	-.527	-.516	-.486	-.438	-.400	-.368	-.337	-.356	-.380	-.416	-.459	-.496	-.522	-.534	-.546
	.600	-.515	-.524	-.512	-.499	-.503	-.500	-.473	-.443	-.441	-.442	-.456	-.487	-.507	-.489	-.508	-.520	-.522
	.700	-.463	-.473	-.482	-.508	-.534	-.523	-.512	-.493	-.503	-.488	-.498	-.519	-.523	-.523	-.492	-.478	-.472
	.800	-.344	-.350	-.346	-.348	-.342	-.334	-.315	-.328	-.307	-.323	-.320	-.337	-.334	-.347	-.349	-.349	-.348
.900	-.128	-.130	-.123	-.125	-.124	-.115	-.101	-.080	-.067	-.076	-.086	-.107	-.118	-.123	-.126	-.128	-.129	
.950	.013	.012	.020	.022	.023	.032	.038	.041	.046	.044	.045	.038	.031	.025	.018	.017	.012	
Lower surface	.0375	.397	.308	.164	.033	-.098	-.883	-1.045	-1.093	-1.134	-1.164	-1.100	-1.021	-.544	-.050	.099	.237	.334
	.075	.363	.264	.164	.086	-.025	-.268	-.965	-1.026	-1.080	-1.070	-1.004	-.883	-.032	.044	.121	.223	.291
	.150	.287	.235	.194	.145	.055	.037	-.292	-.822	-.924	-.914	-.780	.026	.038	.104	.175	.207	.254
	.250	.048	.085	.159	.121	.062	.035	.067	-.213	-.814	-.631	.027	.045	.047	.095	.138	.120	.053
	.350	.200	.167	.133	.100	.056	.035	.044	.055	-.234	-.091	.070	.034	.046	.083	.116	.154	.179
	.450	.189	.158	.129	.102	.069	.051	.051	.091	-.005	.088	.068	.049	.056	.090	.114	.146	.169
	.550	.174	.151	.129	.107	.081	.068	.063	.090	.112	.109	.076	.066	.076	.098	.117	.144	.161
	.650	.131	.109	.093	.078	.057	.049	.045	.062	.103	.079	.055	.049	.055	.071	.084	.103	.118
	.750	.137	.121	.110	.102	.085	.080	.077	.085	.111	.093	.084	.080	.084	.095	.104	.119	.128
	.850	.151	.140	.134	.127	.118	.118	.114	.117	.130	.120	.121	.119	.119	.127	.129	.139	.145
	.925	.185	.177	.174	.169	.164	.116	.161	.161	.163	.162	.167	.166	.166	.169	.170	.177	.180
^b .975	.213	.206	.206	.197	.198	.207	.201	.204	.196	.207	.200	.208	.205	.204	.210	.211	.214	
1.000	.228	.223	.224	.213	.217	.230	.223	.226	.212	.228	.219	.230	.227	.223	.232	.229	.232	

^aNo orifice.

^bPaired value.



TABLE 8.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN

NACA 16-504.80 PROPELLER BLADE SECTION ($x = 0.90$; $\beta_x = 39.50^\circ$; $\beta_{0.75R} = 45^\circ$; $B = 2$) - Continued(d) $N = 1600$ rpm.

	2.103	2.170	2.240	2.295	2.352	2.410	2.457	2.509	2.561	2.554	2.499	2.439	2.389	2.337	2.275	2.224	2.161	
J	2.103	2.170	2.240	2.295	2.352	2.410	2.457	2.509	2.561	2.554	2.499	2.439	2.389	2.337	2.275	2.224	2.161	
M_x	.856	.866	.876	.885	.896	.908	.916	.924	.934	.933	.923	.908	.892	.881	.873	.860		
q_x	2.86	1.99	1.11	.43	-.26	-.94	-1.49	-2.08	-2.67	-2.99	-1.97	-1.28	-.70	-.08	.68	1.31	2.11	
$\Delta\beta$.86	.52	.17	-.11	-.40	-.70	-.93	-1.17	-1.33	-1.31	-1.13	-.84	-.59	-.33	-.01	.25	.57	
a_1	2.69	2.30	1.98	1.64	1.30	.89	.56	-.06	-.51	-.53	.09	.65	.99	1.37	1.79	1.98	2.32	
c_m	.6003	.5142	.4426	.3687	.2910	.1994	.1251	-.0148	-.1155	-.1194	.0194	.1465	.2226	.3077	.4006	.4432	.5194	
c_m	-.1209	-.1211	-.1237	-.1355	-.1481	-.1542	-.1588	-.1504	-.1393	-.1404	-.1581	-.1586	-.1547	-.1424	-.1288	-.1216	-.1180	
c_o	.0009	.0083	.0144	.0214	.0274	.0321	.0362	.0397	.0420	.0414	.0394	.0344	.0308	.0263	.0191	.0124	.0058	
c/b	Pressure coefficient, P																	
Upper surface	∞ .000	1.196	1.201	1.206	1.211	1.217	1.223	1.227	1.231	1.237	1.237	1.231	1.223	1.220	1.215	1.209	1.204	1.198
	.025	-.008	-.178	.317	.428	.516	.593	.610	.716	.761	.757	.705	.632	.566	.500	.395	.276	.121
	.050	-.261	-.098	.030	.139	.230	.311	.334	.445	.494	.491	.432	.352	.282	.215	.107	-.007	-.149
	.100	-.451	-.288	-.174	-.081	.002	.077	.099	.208	.254	.252	.194	.118	.051	-.014	-.111	-.208	-.334
	.200	-.543	-.447	-.334	-.219	-.154	-.091	-.081	.023	.065	.064	.010	-.057	-.113	-.165	-.245	-.385	-.464
	.300	-.612	-.495	-.407	-.347	-.287	-.230	-.228	-.129	-.088	-.089	-.139	-.202	-.249	-.295	-.363	-.424	-.520
	.400	-.647	-.571	-.496	-.431	-.387	-.334	-.328	-.231	-.195	-.197	-.242	-.303	-.355	-.388	-.439	-.511	-.594
	.500	-.663	-.579	-.524	-.503	-.463	-.438	-.444	-.359	-.323	-.324	-.368	-.413	-.448	-.466	-.514	-.535	-.577
	.600	-.663	-.616	-.582	-.561	-.520	-.516	-.537	-.451	-.416	-.416	-.458	-.506	-.503	-.524	-.566	-.597	-.615
	.700	-.675	-.658	-.641	-.620	-.591	-.569	-.617	-.540	-.507	-.505	-.544	-.581	-.573	-.598	-.625	-.650	-.659
	.800	-.240	-.307	-.380	-.524	-.644	-.655	-.711	-.659	-.633	-.632	-.666	-.647	-.671	-.627	-.473	-.355	-.275
.900	-.062	-.064	-.073	-.091	-.103	-.105	-.164	-.133	-.139	-.132	-.124	-.105	-.103	-.093	-.077	-.065	-.063	
.950	.026	.002	-.018	-.042	-.061	-.062	-.134	-.104	-.108	-.102	-.096	-.065	-.059	-.044	-.020	0	.021	
Lower surface	.0375	.202	.081	-.023	-.402	-.654	-.804	-.908	-.916	-.941	-.962	-.948	-.902	-.847	-.771	-.338	-.034	.103
	.075	.205	.113	.057	.006	-.613	-.765	-.862	-.864	-.888	-.893	-.870	-.823	-.767	-.618	.015	.072	.135
	.150	.226	.173	.119	.073	.051	-.535	-.713	-.727	-.754	-.765	-.739	-.689	-.448	.076	.076	.128	.189
	.250	.141	.122	.095	.062	.073	.068	-.471	-.638	-.676	-.684	-.650	-.203	.088	.042	.074	.099	.121
	.350	.153	.116	.091	.056	.054	.086	.002	-.509	-.648	-.664	-.314	.096	.066	.049	.065	.071	.124
	.450	.146	.115	.095	.065	.060	.077	.067	-.008	-.400	-.332	.061	.097	.064	.058	.074	.096	.120
	.550	.141	.116	.101	.074	.064	.075	.058	.108	-.002	-.007	.123	.088	.066	.066	.081	.101	.121
	.650	.101	.080	.067	.042	.033	.037	.011	.099	.082	.088	.089	.048	.033	.033	.051	.067	.084
	.750	.116	.098	.087	.065	.055	.057	.020	.092	.112	.115	.084	.063	.054	.060	.074	.089	.103
	.850	.138	.122	.112	.092	.082	.082	.035	.089	.107	.107	.089	.085	.081	.087	.099	.115	.127
	.925	.174	.156	.145	.122	.114	.112	.057	.099	.103	.106	.103	.110	.111	.118	.134	.150	.165
b.975	.202	.183	.173	.154	.139	.137	.077	.105	.096	.106	.120	.130	.138	.141	.167	.178	.197	
a1.000	.218	.198	.187	.169	.152	.153	.089	.110	.093	.107	.130	.140	.150	.155	.184	.192	.215	

a No orifices.

b Paired values.



TABLE 8.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN

NACA 16-504.80 PROPELLER BLADE SECTION ($\alpha = 0.90$; $\beta_x = 39.50^\circ$;

$\beta_{0.75R} = 45^\circ$; $B = 2$) - Continued

(e) $M = 0.56$.

J	2.677	2.641	2.588	2.547	2.512	2.482	2.429	2.398	2.346	2.316	2.281	2.254	2.221	2.185	2.159	2.127	
M_x	.826	.832	.837	.849	.855	.864	.872	.878	.885	.896	.900	.911	.920	.927	.938	.946	
α_r'	-3.93	-3.55	-2.97	-2.51	-2.12	-1.78	-1.16	-1.16	-1.18	.18	.61	.94	1.35	1.80	2.13	2.55	
$\Delta\beta$	-1.32	-1.26	-1.13	-1.01	-.90	-.81	-.63	-.50	-.34	-.29	-.25	-.22	-.16	-.08	0	.14	
α_1	-.29	-.08	.11	.37	.55	.70	1.00	1.12	1.37	1.45	1.57	1.76	1.82	1.98	2.08	2.28	
c_{Df}	-.0645	-.0174	.0258	.0839	.1226	.1574	.2245	.2516	.3058	.3239	.3503	.3942	.4055	.4423	.4655	.5090	
c_{Df}	-.1262	-.1427	-.1442	-.1462	-.1491	-.1542	-.1442	-.1501	-.1490	-.1436	-.1424	-.1427	-.1408	-.1431	-.1463	-.1496	
c_c				.0323	.0321	.0308	.0284	.0272	.0265	.0263	.0260	.0252	.0245	.0244	.0243	.0236	
c/b	Pressure coefficient, P																
Upper surface	^a 0.000	1.182	1.185	1.187	1.193	1.196	1.200	1.204	1.207	1.211	1.217	1.219	1.225	1.230	1.234	1.239	1.244
	.025	.752	.738	.711	.677	.653	.628	.579	.555	.512	.493	.466	.444	.419	.390	.374	.340
	.050	.481	.462	.432	.398	.372	.347	.297	.273	.228	.211	.185	.164	.142	.116	.103	.075
	.100	.227	.207	.176	.147	.124	.104	.056	.036	-.007	-.022	-.046	-.062	-.081	-.102	-.114	-.142
	.200	.028	.010	-.011	-.035	-.055	-.072	-.110	-.128	-.163	-.175	-.194	-.240	-.280	-.301	-.308	-.325
	.300	-.105	-.123	-.143	-.170	-.191	-.206	-.241	-.259	-.286	-.297	-.313	-.322	-.329	-.346	-.356	-.376
	.400	-.204	-.221	-.237	-.259	-.277	-.297	-.317	-.330	-.366	-.387	-.411	-.420	-.432	-.439	-.445	-.455
	.500	-.296	-.314	-.337	-.364	-.376	-.385	-.419	-.431	-.451	-.454	-.480	-.513	-.528	-.535	-.539	-.546
	.600	-.367	-.384	-.406	-.404	-.437	-.454	-.486	-.514	-.523	-.526	-.538	-.537	-.556	-.576	-.599	-.621
	.700	-.445	-.467	-.498	-.508	-.518	-.518	-.549	-.561	-.556	-.551	-.604	-.604	-.613	-.622	-.631	-.640
	.800	-.392	-.380	-.365	-.463	-.571	-.610	-.643	-.663	-.675	-.674	-.682	-.686	-.681	-.660	-.661	-.664
	.900	-.201	-.172	-.155	-.127	-.113	-.085	-.063	-.059	-.075	-.101	-.127	-.145	-.168	-.188	-.218	-.246
.950	-.026	.007	.019	.034	.037	.050	.049	.032	-.010	-.051	-.087	-.112	-.139	-.165	-.199	-.229	
Lower surface	.0375	-1.041	-1.348	-1.284	-1.200	-1.142	-1.063	-.973	-.915	-.819	-.717	-.633	-.503	-.362	-.158	-.061	.022
	.075	-.910	-1.218	-1.174	-1.091	-1.040	-.966	-.862	-.758	-.668	-.504	-.311	-.037	.066	.078	.094	.113
	.150	-.647	-.755	-.770	-.719	-.640	-.529	-.204	-.023	-.035	-.021	-.042	.101	.109	.137	.154	.182
	.250	-.413	-.302	-.259	-.005	.051	.083	.084	.079	.070	.079	.077	.088	.098	.121	.132	.150
	.350	-.246	.005	.056	.060	.059	.063	.059	.057	.054	.063	.063	.074	.081	.102	.109	.122
	.450	-.116	.046	.058	.060	.059	.065	.065	.064	.063	.070	.068	.079	.083	.100	.107	.117
	.550	-.028	.059	.066	.069	.068	.074	.076	.075	.072	.078	.074	.082	.084	.099	.103	.110
	.650	.020	.051	.053	.055	.051	.055	.056	.051	.045	.045	.038	.042	.044	.052	.054	.060
	.750	.062	.080	.083	.085	.083	.086	.086	.081	.072	.068	.058	.059	.057	.065	.065	.069
	.850	.098	.119	.121	.126	.124	.127	.125	.118	.105	.097	.083	.082	.077	.082	.081	.085
	.925	.135	.162	.168	.171	.170	.171	.169	.159	.142	.129	.111	.106	.098	.102	.096	.103
	^b .975	.175	.211	.220	.216	.209	.216	.195	.199	.174	.150	.120	.125	.111	.121	.108	.116
^a 1.000	.198	.245	.250	.248	.230	.240	.210	.225	.189	.162	.130	.140	.118	.134	.115	.124	

^aNo orifice.

^bPaired value.



TABLE 8.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN

HACA 16-504.80 PROPELLER BLADE SECTION ($\alpha = 0.90$; $\beta_x = 39.50^\circ$;

$\beta_{0.75R} = 45^\circ$; $B = 2$) - Continued

(r) $M = 0.58$.

	2.637	2.585	2.544	2.512	2.476	2.424	2.391	2.354	2.319	2.280	2.249	2.220	2.185	2.149	
J	.863	.870	.877	.887	.894	.905	.912	.920	.929	.935	.946	.954	.961	.972	
M_x	-3.50	-2.94	-2.48	-2.12	-1.71	-1.11	-.72	-.28	.14	.62	1.00	1.36	1.80	2.26	
$\Delta\delta$	-1.42	-1.24	-1.09	-.97	-.86	-.73	-.68	-.64	-.61	-.52	-.41	-.29	-.11	.10	
c_l	-.21	0	.16	.30	.47	.69	.85	.97	1.10	1.26	1.44	1.58	1.77	1.99	
c_{l1}	-.0465	0	.0348	.0665	.1065	.1542	.1890	.2168	.2452	.2816	.3219	.3542	.3945	.4413	
c_{m1}	-.1558	-.1552	-.1540	-.1557	-.1562	-.1540	-.1513	-.1534	-.1534	-.1526	-.1533	-.1513	-.1541	-.1560	
c_c	.0383	.0363	.0350	.0341	.0336	.0326	.0322	.0320	.0318	.0305	.0308	.0294	.0294	.0286	
c/d	Pressure coefficient, P														
Upper surface	^a 0.000	1.200	1.203	1.207	1.212	1.216	1.222	1.225	1.230	1.235	1.238	1.244	1.249	1.252	1.259
	.025	.757	.727	.703	.678	.661	.617	.594	.580	.561	.530	.518	.487	.464	.430
	.050	.485	.452	.426	.399	.380	.335	.314	.298	.282	.250	.239	.211	.193	.160
	.100	.236	.208	.186	.162	.146	.105	.084	.073	.059	.030	.022	0	-.015	-.046
	.200	.039	.015	-.006	-.025	-.038	-.071	-.085	-.092	-.101	-.122	-.148	-.204	-.223	-.247
	.300	-.113	-.137	-.155	-.172	-.186	-.214	-.223	-.228	-.235	-.251	-.255	-.265	-.278	-.304
	.400	-.220	-.241	-.260	-.279	-.286	-.313	-.329	-.336	-.342	-.360	-.361	-.373	-.380	-.397
	.500	-.335	-.352	-.363	-.390	-.407	-.424	-.434	-.446	-.454	-.467	-.468	-.476	-.481	-.492
	.600	-.387	-.425	-.437	-.461	-.487	-.508	-.518	-.524	-.529	-.543	-.547	-.560	-.566	-.574
	.700	-.490	-.481	-.493	-.509	-.534	-.562	-.573	-.576	-.583	-.584	-.585	-.589	-.595	-.603
	.800	-.598	-.603	-.621	-.630	-.626	-.646	-.647	-.648	-.655	-.664	-.664	-.667	-.674	-.683
	.900	-.104	-.085	-.067	-.060	-.067	-.092	-.114	-.133	-.154	-.179	-.210	-.231	-.267	-.303
.950	.039	.045	.046	.026	.001	-.042	-.075	-.100	-.127	-.153	-.183	-.204	-.236	-.268	
Lower surface	.0375	-1.235	-1.182	-1.116	-1.042	-.988	-.908	-.841	-.766	-.707	-.632	-.561	-.474	-.359	-.181
	.075	-1.142	-1.084	-1.021	-.951	-.902	-.827	-.764	-.694	-.635	-.548	-.479	-.312	-.076	.110
	.150	-.992	-.928	-.866	-.799	-.733	-.679	-.610	-.506	-.375	-.049	.081	.126	.136	.156
	.250	-.390	-.345	-.286	-.253	-.214	0	.060	.099	.106	.103	.105	.106	.117	.136
	.350	-.159	-.065	.019	.064	.083	.093	.090	.090	.087	.082	.083	.087	.098	.114
	.450	.042	.080	.099	.103	.102	.087	.080	.081	.080	.079	.082	.087	.097	.112
	.550	.096	.098	.100	.099	.095	.080	.075	.079	.078	.078	.083	.086	.094	.108
	.650	.057	.076	.074	.070	.062	.044	.037	.037	.034	.032	.034	.037	.044	.054
	.750	.097	.093	.093	.088	.080	.063	.054	.053	.050	.049	.049	.054	.059	.070
	.850	.124	.123	.122	.115	.107	.089	.078	.075	.069	.069	.068	.076	.082	.091
	.925	.162	.160	.160	.149	.138	.118	.104	.101	.093	.091	.090	.097	.105	.117
	^b .975	.189	.180	.188	.178	.162	.140	.124	.128	.117	.108	.108	.112	.121	.137
^a 1.000	.202	.192	.202	.191	.178	.150	.134	.138	.129	.117	.116	.120	.129	.147	

^aNo orifice.
^bPaired value.



TABLE 8.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN
NACA 16-504.80 PROPELLER BLADE SECTION ($\alpha = 0.90$; $\beta_x = 39.50^\circ$;

$\beta_{0.75R} = 45^\circ$; $B = 2$) - Continued

(g) $M = 0.60$.

	2.611	2.563	2.522	2.485	2.445	2.405	2.374	2.344	2.303	2.274	2.253	2.209	2.167	2.150	2.131	
J	.901	.905	.913	.921	.929	.939	.945	.957	.963	.971	.984	.986	.993	1.003	1.009	
C_{p1}	-3.22	-2.69	-2.23	-1.81	-1.35	-.88	-.52	-.16	.34	.73	.95	1.50	2.03	2.25	2.49	
$\Delta\theta$	-1.43	-1.35	-1.29	-1.24	-1.18	-1.07	-.97	-.86	-.69	-.58	-.52	-.41	-.38	-.37	-.37	
C_{p2}	-.38	-.21	-.08	.14	.27	.44	.54	.74	.99	1.08	1.29	1.60	1.78	1.95	2.05	
C_{p3}	-.0845	-.0477	-.0174	.0310	.0613	.0981	.1213	.1645	.2206	.2419	.2890	.3568	.3961	.4355	.4568	
C_{p4}	-.1496	-.1542	-.1531	-.1583	-.1647	-.1568	-.1563	-.1594	-.1570	-.1601	-.1668	-.1703	-.1799	-.1953	-.1981	
C_{p5}	.0400	.0393	.0393	.0387	.0385	.0377	.0377	.0379	.0362	.0366	.0375	.0377	.0403	.0424	.0423	
a/b	Pressure coefficient, P															
Upper surface	^a 0.000	1.220	1.222	1.226	1.230	1.235	1.240	1.244	1.250	1.254	1.258	1.265	1.264	1.275	1.277	1.280
	.025	.775	.748	.726	.700	.672	.661	.646	.630	.597	.582	.567	.546	.520	.506	.504
	.050	.506	.476	.454	.501	.481	.388	.371	.356	.323	.309	.296	.275	.251	.220	.219
	.100	.262	.234	.216	.259	.243	.157	.145	.131	.102	.092	.082	.062	.042	.105	.104
	.200	.063	.043	.027	.069	.059	-.015	-.023	-.032	-.051	-.061	-.102	-.141	-.165	-.107	-.103
	.300	-.091	-.112	-.124	-.082	-.090	-.155	-.161	-.167	-.184	-.190	-.192	-.204	-.225	-.170	-.169
	.400	-.202	-.228	-.231	-.187	-.195	-.263	-.271	-.276	-.295	-.297	-.300	-.311	-.325	-.271	-.266
	.500	-.320	-.344	-.356	-.316	-.315	-.378	-.385	-.391	-.404	-.404	-.404	-.413	-.425	-.370	-.366
	.600	-.423	-.434	-.448	-.408	-.412	-.464	-.470	-.474	-.489	-.490	-.492	-.504	-.515	-.461	-.454
	.700	-.521	-.532	-.533	-.499	-.499	-.549	-.549	-.550	-.561	-.560	-.558	-.570	-.583	-.535	-.530
	.800	-.640	-.653	-.657	-.618	-.621	-.667	-.663	-.659	-.664	-.658	-.652	-.666	-.661	-.613	-.600
.900	-.057	-.076	-.059	-.060	-.083	-.164	-.196	-.224	-.250	-.310	-.403	-.516	-.736	-.702	-.690	
.950	.009	-.026	-.064	-.029	-.059	-.141	-.171	-.195	-.217	-.248	-.278	-.305	-.378	-.485	-.616	
Lower surface	.0375	-1.079	-1.049	-.986	-.889	-.829	-.812	-.764	-.709	-.631	-.569	-.507	-.440	-.367	-.262	-.196
	.075	-1.020	-.969	-.909	-.817	-.758	-.747	-.699	-.643	-.568	-.513	-.450	-.380	-.306	-.189	-.077
	.150	-.875	-.829	-.773	-.679	-.626	-.622	-.573	-.518	-.430	-.365	-.291	-.213	.074	.199	.247
	.250	-.792	-.743	-.690	-.597	-.538	-.528	-.473	-.390	-.303	-.263	.111	.127	.127	.204	.226
	.350	-.320	-.322	-.360	-.130	-.017	.017	.053	.089	.118	.118	.116	.112	.106	.182	.200
	.450	-.108	-.028	.018	.146	.180	.126	.125	.125	.110	.109	.108	.107	.103	.179	.197
	.550	.051	.100	.118	.192	.192	.121	.115	.113	.100	.100	.102	.102	.099	.173	.191
	.650	.118	.112	.104	.153	.144	.069	.061	.057	.043	.044	.045	.044	.039	.108	.125
	.750	.128	.112	.099	.150	.142	.069	.063	.062	.056	.056	.056	.061	.063	.128	.145
	.850	.134	.117	.102	.155	.149	.079	.072	.076	.075	.080	.088	.095	.095	.170	.144
	.925	.149	.131	.115	.168	.161	.093	.088	.093	.099	.106	.120	.119	.132	.212	.230
.975	.154	.148	.120	.178	.182	.102	.100	.119	.118	.120	.142	.128	.168	.250	.278	
^a 1.000	.160	.158	.129	.182	.199	.110	.110	.128	.129	.130	.158	.130	.182	.270	.298	

^aNo orifice.

^bPaired values.

NACA

TABLE 8.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN

NACA 16-504.80 PROPELLER BLADE SECTION ($x = 0.90$; $\beta_x = 39.50^\circ$; $\beta_{0.75R} = 45^\circ$; $B = 2$) - Concluded(h) $M = 0.65$.

J	2.110	2.142	2.161	2.194	2.213	2.255	2.284	2.312	2.336	2.371	2.405	2.439	2.471	2.501	
M_x	1.095	1.088	1.074	1.064	1.055	1.047	1.039	1.031	1.022	1.013	1.005	.997	.985	.978	
$C_{x'}$	2.77	2.35	2.11	1.69	1.45	.93	.57	.23	-.06	-.48	-.88	-1.28	-1.65	-1.99	
ΔB	-.79	-.89	-.94	-1.03	-1.08	-1.20	-1.26	-1.33	-1.38	-1.45	-1.50	-1.55	-1.59	-1.62	
F_1	1.54	1.38	1.29	1.09	.96	.80	.68	.54	.38	.14	-.08	-.29	-.50	-.73	
c_m	.3413	.3071	.2871	.2429	.2132	.1761	.1516	.1213	.0852	.0316	-.0181	-.0639	-.1123	-.1639	
c_H	-.1803	-.1858	-.1847	-.1857	-.1817	-.1820	-.1821	-.1819	-.1799	-.1735	-.1580	-.1480	-.1368	-.1206	
c_c	.0432	.0458	.0467	.0478	.0478	.0485	.0503	.0514	.0522	.0533	.0515	.0505	.0476	.0456	
a/b	Pressure coefficient, P														
Upper surface	^a 0.000	1.336	1.331	1.322	1.315	1.310	1.304	1.300	1.294	1.288	1.283	1.276	1.273	1.266	1.262
	.025	.606	.626	.629	.631	.644	.654	.669	.684	.712	.720	.737	.749	.764	.777
	.050	.348	.367	.369	.373	.383	.394	.407	.424	.451	.458	.473	.486	.501	.515
	.100	.144	.161	.161	.164	.172	.181	.192	.206	.230	.234	.248	.258	.272	.283
	.200	-.045	-.037	-.041	-.039	-.030	-.005	.031	.050	.067	.067	.076	.082	.092	.101
	.300	-.113	-.104	-.107	-.103	-.100	-.095	-.089	-.078	-.085	-.066	-.059	-.056	-.052	-.046
	.400	-.202	-.196	-.202	-.204	-.203	-.199	-.195	-.186	-.172	-.174	-.168	-.164	-.155	-.148
	.500	-.297	-.294	-.301	-.305	-.308	-.306	-.302	-.295	-.286	-.291	-.287	-.284	-.274	-.270
	.600	-.377	-.379	-.389	-.395	-.398	-.396	-.393	-.387	-.379	-.382	-.379	-.378	-.373	-.372
	.700	-.449	-.460	-.473	-.479	-.484	-.480	-.478	-.470	-.463	-.468	-.467	-.467	-.463	-.461
	.800	-.543	-.549	-.562	-.568	-.575	-.575	-.571	-.567	-.567	-.576	-.576	-.580	-.582	-.581
.900	-.631	-.643	-.659	-.669	-.679	-.683	-.687	-.686	-.687	-.701	-.706	-.698	-.691	-.685	
.950	-.654	-.672	-.690	-.704	-.715	-.722	-.730	-.732	-.737	-.742	-.743	-.739	-.731	-.728	
Lower surface	.0375	-.179	-.217	-.264	-.326	-.371	-.419	-.471	-.534	-.577	-.630	-.670	-.711	-.768	-.807
	.075	-.130	-.190	-.237	-.298	-.341	-.387	-.440	-.497	-.537	-.589	-.628	-.668	-.721	-.756
	.150	-.007	-.068	-.120	-.178	-.223	-.266	-.315	-.368	-.407	-.461	-.511	-.558	-.606	-.635
	.250	.124	.008	-.070	-.141	-.188	-.231	-.279	-.329	-.365	-.416	-.456	-.494	-.544	-.575
	.350	.153	.102	.004	-.101	-.170	-.221	-.271	-.319	-.354	-.408	-.446	-.484	-.532	-.562
	.450	.160	.148	.120	.064	-.018	-.112	-.205	-.266	-.313	-.374	-.415	-.454	-.501	-.530
	.550	.168	.156	.139	.122	.112	.092	.047	.022	-.024	-.180	-.250	-.304	-.359	-.408
	.650	.078	.067	.054	.046	.049	.064	.080	.117	.105	.053	.034	.014	-.005	-.034
	.750	.093	.081	.070	.064	.069	.083	.098	.113	.121	.105	.109	.107	.100	.091
	.850	.128	.115	.113	.112	.117	.122	.126	.129	.131	.116	.119	.117	.112	.109
	.925	.224	.210	.199	.181	.176	.169	.163	.155	.153	.132	.127	.118	.109	.104
^b .975	.297	.308	.278	.250	.224	.203	.193	.177	.170	.149	.138	.129	.123	.108	
^a 1.000	.330	.370	.322	.290	.248	.222	.212	.189	.180	.157	.140	.142	.133	.117	

^aNo orifice.^bPaired value.

TABLE 9.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN

NACA 16-504 NO PROPELLER BLADE SECTION ($\alpha = 0.93^\circ$;

$\beta_x = 38.35^\circ$; $\beta_{0.75R} = 45^\circ$)

(a) $M = 1140$ rpm; $B = 2$.

	2.793	2.616	2.419	2.224	2.039	1.875	1.682	1.598	1.777	1.939	2.135	2.311	2.523	2.704	
C_d	.797	.683	.662	.639	.619	.603	.589	.585	.598	.611	.632	.650	.673	.697	
C_{d1}	-4.73	-2.89	-.68	1.66	4.01	6.21	8.95	10.18	7.58	5.34	2.77	.60	-1.86	-3.83	
C_{d2}	-.92	-.66	-.23	.06	.49	.78	1.14	1.29	.96	.66	.33	-.02	-.46	-.84	
C_{d3}	-.53	.33	1.26	2.05	2.86	3.65	4.64	4.83	4.19	3.30	2.41	1.72	.82	-.04	
C_{m1}	-.0852	.0542	.2039	.3316	.4597	.5658	.7445	.7755	.6697	.5323	.3890	.2787	.1329	-.0071	
C_{m2}	-.1121	-.0963	-.0885	-.0885	-.0821	-.0800	-.0775	-.0623	-.0749	-.0811	-.0864	-.0899	-.0928	-.1014	
c/b	Pressure coefficient, P														
Upper surface	^a 0.000	1.132	1.123	1.115	1.106	1.099	1.094	1.089	1.088	1.092	1.096	1.104	1.110	1.119	1.128
	^b 0.025	.680	.625	.428	-.068	-.412	-.916	-1.223	-1.665	-1.717	-1.684	-1.553	-1.252	-.941	-.680
	.050	.434	.322	.132	-.153	-.483	-.815	-1.600	-1.579	-1.087	-.675	-.308	-.015	.237	.381
	.100	.178	.081	-.072	-.267	-.443	-.646	-1.118	-1.348	-.760	-.561	-.359	-.177	.011	.131
	.200	-.020	-.088	-.187	-.267	-.406	-.513	-.604	-.755	-.559	-.458	-.352	-.249	-.134	-.054
	.300	-.106	-.173	-.223	-.299	-.364	-.438	-.505	-.532	-.487	-.406	-.333	-.263	-.187	-.130
	.400	-.193	-.226	-.274	-.324	-.391	-.442	-.486	-.471	-.478	-.418	-.354	-.301	-.246	-.210
	.500	-.291	-.215	-.252	-.292	-.343	-.389	-.425	-.419	-.416	-.368	-.318	-.277	-.230	-.204
	.600	-.298	-.273	-.300	-.327	-.362	-.394	-.421	-.405	-.416	-.379	-.345	-.319	-.282	-.266
	.700	-.263	-.273	-.290	-.314	-.341	-.367	-.381	-.363	-.381	-.354	-.328	-.308	-.275	-.267
	.800	-.265	-.264	-.269	-.285	-.299	-.314	-.318	-.298	-.325	-.306	-.294	-.281	-.261	-.264
.900	-.248	-.230	-.225	-.232	-.214	-.210	-.216	-.205	-.217	-.213	-.229	-.234	-.221	-.238	
.950	-.087	-.069	-.064	-.065	-.058	-.065	-.066	-.094	-.076	-.079	-.062	-.065	-.060	-.076	
Lower surface	^a 0.0375	-.763	-.889	-.305	.019	.261	.449	.584	.619	.730	.376	.135	-.105	-.745	-.871
	.075	-.714	-.673	-.125	.069	.215	.355	.462	.492	.416	.301	.128	-.013	-.316	-.702
	.150	-.646	-.337	-.048	.074	.168	.265	.344	.368	.310	.228	.113	.020	-.099	-.566
	.250	-.421	-.082	.006	.069	.140	.209	.261	.267	.229	.176	.103	.051	-.017	-.252
	.350	-.206	-.049	.009	.068	.119	.172	.219	.230	.197	.151	.091	.039	-.004	-.085
	.450	-.090	0	.027	.073	.107	.149	.182	.191	.167	.132	.088	.051	.017	-.017
	.550	-.033	.011	.027	.061	.088	.123	.150	.156	.138	.109	.072	.046	.022	.005
	.650	.012	.037	.051	.081	.100	.129	.146	.150	.139	.119	.089	.067	.048	.035
	.750	.029	.044	.051	.071	.079	.100	.112	.112	.108	.094	.074	.062	.053	.044
	.850	.061	.075	.079	.093	.089	.100	.104	.100	.102	.100	.089	.088	.082	.072
	^b .925	.099	.117	.127	.139	.126	.127	.123	.113	.126	.130	.134	.136	.129	.113
.975	.124	.147	.170	.177	.162	.150	.148	.132	.149	.159	.178	.182	.164	.145	
^a 1.000	.140	.161	.195	.198	.182	.169	.160	.140	.160	.170	.205	.206	.182	.160	

^aNo orifice.
^bPaired value.

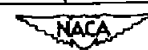


TABLE 9.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN

NACA 16-504.40 PROPELLER BLADE SECTION ($x = 0.95$;

$\beta_x = 38.35^\circ$; $\beta_{0.75R} = 45^\circ$) - Continued

(b) $N = 1350$ rpm; $B = 2$.

	2.038	2.179	2.296	2.427	2.563	2.673	2.603	2.493	2.352	2.229	2.110	
J	2.038	2.179	2.296	2.427	2.563	2.673	2.603	2.493	2.352	2.229	2.110	
M_x	.738	.756	.771	.788	.810	.823	.814	.799	.776	.760	.746	
α_x'	4.02	2.22	.78	-.77	-2.30	-3.70	-2.74	-1.52	.11	1.58	3.07	
$\Delta\delta$.67	.27	-.07	-.45	-.91	-1.29	-1.06	-.67	-.23	.12	.47	
c_d	3.03	2.32	1.73	1.09	.36	-.19	.09	.78	1.44	2.02	2.64	
c_n	.4887	.3732	.2761	.1768	.0581	-.0316	.0142	.1298	.2335	.3258	.4245	
c_m	-.0870	-.0872	-.0880	-.0930	-.1073	-.1149	-.1121	-.1016	-.0891	-.0874	-.0866	
c_c												
c/b	Pressure coefficient, P											
Upper surface	∞ .000	1.144	1.151	1.158	1.165	1.175	1.181	1.176	1.170	1.160	1.153	1.148
	.025	-.377	.031	.312	.515	.690	.732	.690	.584	.412	.174	-.163
	.050	-.526	-.226	.009	.196	.334	.423	.376	.263	.098	-.112	-.374
	.100	-.510	-.311	-.153	-.010	.104	.178	.141	.045	-.087	-.235	-.405
	.200	-.453	-.355	-.268	-.181	-.105	-.051	-.082	-.145	-.229	-.313	-.399
	.300	-.401	-.336	-.278	-.219	-.166	-.133	-.150	-.193	-.250	-.308	-.367
	.400	-.421	-.369	-.327	-.284	-.245	-.219	-.232	-.265	-.305	-.346	-.390
	.500	-.378	-.340	-.307	-.278	-.257	-.244	-.250	-.266	-.293	-.325	-.357
	.600	-.399	-.367	-.343	-.322	-.311	-.307	-.307	-.315	-.331	-.346	-.362
	.700	-.383	-.356	-.336	-.322	-.320	-.322	-.321	-.319	-.330	-.349	-.368
	.800	-.334	-.313	-.300	-.292	-.295	-.307	-.298	-.291	-.295	-.308	-.322
	.900	-.217	-.205	-.198	-.197	-.207	-.223	-.212	-.200	-.197	-.202	-.210
.950	-.051	-.036	-.026	-.022	-.025	-.032	-.028	-.021	-.024	-.032	-.044	
Lower surface	.0375	.273	.071	-.120	-.565	-1.319	-1.335	-1.371	-1.241	-.187	-.016	.178
	.075	.229	.105	-.019	-.107	-.816	-1.183	-1.126	-.276	-.074	.092	.162
	.150	.181	.102	.019	-.046	-.099	-.513	-.309	-.050	-.016	.062	.136
	.250	.149	.103	.049	.002	-.009	-.133	-.013	-.010	.026	.078	.132
	.350	.126	.079	.041	.009	-.011	-.027	-.016	-.002	.026	.062	.101
	.450	.113	.078	.048	.024	-.003	-.011	-.003	.014	.036	.062	.094
	.550	.087	.061	.036	.019	.005	-.006	-.001	.013	.029	.047	.072
	.650	.101	.079	.061	.048	.035	.025	.030	.043	.053	.068	.090
	.750	.057	.042	.032	.028	.021	.016	.019	.027	.029	.035	.048
	.850	.093	.086	.079	.078	.073	.067	.070	.078	.078	.080	.089
	.925	.122	.121	.119	.119	.114	.106	.111	.118	.117	.119	.118
	.975	.138	.142	.145	.151	.140	.137	.150	.150	.150	.150	.152
1.000	.145	.156	.160	.171	.161	.159	.170	.170	.173	.171	.165	

^aNo orifice.
^bPaired value.



TABLE 9.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN
 NACA 16-904.40 PROPELLER BLADE SECTION ($x = 0.95$)
 $\beta_x = 36.35^\circ$; $\beta_{0.75R} = 45^\circ$ - Continued

(a) $M = 1500$ rpm; $B = 2$.

	2.028	2.188	2.198	2.294	2.389	2.474	2.564	2.614	2.520	2.434	2.343	2.247	2.168	2.093	
J	2.028	2.188	2.198	2.294	2.389	2.474	2.564	2.614	2.520	2.434	2.343	2.247	2.168	2.093	
M_x	.822	.833	.845	.858	.875	.885	.904	.912	.894	.880	.863	.851	.837	.826	
β_x	4.15	2.86	1.98	.80	-.33	-1.31	-2.32	-2.86	-1.83	-.85	.22	1.37	2.36	3.31	
$\Delta\beta$.93	.53	.26	-.10	-.48	-.87	-1.34	-1.61	-1.11	-.68	-.29	.07	.38	.68	
α_1	3.31	2.84	2.35	1.91	1.38	.86	.18	-.36	.43	1.10	1.60	2.10	2.58	3.05	
α_2	.5332	.4561	.3794	.3087	.2239	.1394	.0897	-.0574	.0703	.1794	.2581	.3387	.4145	.4906	
α_m	-.0914	-.0969	-.0977	-.0984	-.1101	-.1240	-.1288	-.1367	-.1296	-.1159	-.1041	-.0973	-.0950	-.0952	
c_c							.0336	.0374							
c/b	Pressure coefficient, P														
Upper surface	0.000	1.180	1.185	1.191	1.197	1.206	1.211	1.221	1.225	1.216	1.208	1.200	1.194	1.187	1.182
	.025	-.220	.038	.221	.399	.529	.629	.721	.769	.680	.586	.482	.324	.131	-.065
	.050	-.433	-.243	-.085	.082	.210	.313	.412	.465	.366	.267	.162	.009	-.162	-.317
	.100	-.691	-.428	-.258	-.122	-.012	.081	.170	.220	.129	.040	-.053	-.182	-.320	-.570
	.200	-.975	-.690	-.465	-.283	-.211	-.146	-.081	-.037	-.109	-.172	-.237	-.317	-.400	-.522
	.300	-.107	-.375	-.347	-.297	-.254	-.209	-.182	-.149	-.129	-.127	-.129	-.138	-.161	-.192
	.400	-.448	-.428	-.405	-.368	-.336	-.299	-.274	-.260	-.260	-.317	-.349	-.383	-.413	-.444
	.500	-.413	-.390	-.378	-.352	-.331	-.305	-.285	-.260	-.268	-.314	-.335	-.359	-.380	-.405
	.600	-.445	-.428	-.422	-.415	-.410	-.387	-.362	-.337	-.332	-.398	-.408	-.411	-.418	-.440
	.700	-.441	-.426	-.422	-.417	-.417	-.408	-.396	-.386	-.399	-.413	-.420	-.424	-.423	-.436
	.800	-.370	-.352	-.345	-.338	-.338	-.328	-.317	-.306	-.313	-.411	-.344	-.340	-.347	-.363
	.900	-.204	-.188	-.180	-.168	-.159	-.141	-.124	-.119	-.133	-.153	-.166	-.175	-.184	-.197
.950	-.030	-.018	-.009	.003	.011	.021	.034	.038	.029	.016	.007	-.005	-.013	-.027	
Lower surface	.0375	.279	.138	.011	-.108	-.251	-.398	-.501	-.604	-.620	-.649	-.688	-.747	-.823	-.896
	.075	.242	.155	.080	-.006	-.128	-.238	-.338	-.438	-.513	-.582	-.611	-.623	-.619	-.583
	.150	.193	.141	.086	-.028	-.045	-.135	-.225	-.303	-.373	-.408	-.415	-.403	-.373	-.323
	.250	.153	.136	.094	-.055	-.040	-.086	-.168	-.232	-.299	-.334	-.340	-.324	-.287	-.232
	.350	.137	.105	.076	-.050	-.030	-.058	-.123	-.183	-.239	-.284	-.304	-.301	-.287	-.253
	.450	.123	.098	.076	-.055	-.038	-.046	-.098	-.143	-.190	-.234	-.254	-.254	-.243	-.213
	.550	.096	.076	.059	-.042	-.026	-.030	-.068	-.106	-.143	-.184	-.214	-.214	-.204	-.174
	.650	.110	.095	.079	-.027	-.055	-.055	-.074	-.094	-.123	-.153	-.183	-.183	-.173	-.143
	.750	.062	.055	.043	-.037	-.029	-.032	-.044	-.061	-.086	-.116	-.146	-.146	-.136	-.106
	.850	.103	.098	.092	-.090	-.084	-.088	-.095	-.104	-.124	-.154	-.184	-.184	-.174	-.144
	.925	.134	.134	.132	-.133	-.131	-.135	-.139	-.144	-.156	-.172	-.184	-.184	-.174	-.144
	.975	.156	.164	.162	-.166	-.170	-.176	-.180	-.180	-.180	-.190	-.190	-.190	-.180	-.150
1.000	.166	.180	.175	-.184	-.187	-.200	-.200	-.200	-.200	-.200	-.200	-.200	-.200	-.160	

^aNo orifice.
^bReaired value.



TABLE 9.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN

NACA 16-504 HO PROPELLER BLADE SECTION ($x = 0.95$; $\beta_x = 38.35^\circ$; $\beta_{0.75R} = 45^\circ$) - Continued(d) $N = 1600$ rpm; $B = 2$.

J	2.097	2.185	2.269	2.343	2.435	2.521	2.549	2.479	2.392	2.322	2.240	2.151	
M_x	.891	.904	.919	.928	.946	.961	.965	.951	.934	.920	.906	.893	
α_x'	3.26	2.14	1.10	.22	-.86	-1.84	-2.15	-1.36	-.36	.47	1.46	2.57	
$\Delta\beta$.90	.43	-.03	-.44	-.91	-1.32	-1.40	-1.14	-.69	-.32	.12	.61	
α_1	3.04	2.45	1.84	1.32	.53	-.19	-.53	.19	.93	1.46	2.02	2.76	
c_n	.4903	.3939	.2977	.2142	.0852	-.0303	-.0852	.0316	.1497	.2361	.3261	.4429	
c_m	-.1163	-.1110	-.1113	-.1173	-.1327	-.1290	-.1196	-.1334	-.1239	-.1145	-.1103	-.1129	
c_c		.0154	.0219	.0275	.0338	.0391	.0408	.0369	.0306	.0252	.0190		
c/b	Pressure coefficient, P												
Upper surface	β_0 .000	1.214	1.222	1.229	1.234	1.244	1.219	1.254	1.247	1.237	1.230	1.222	1.215
	.025	.139	.329	.465	.570	.670	.749	.773	.714	.620	.530	.418	.226
	.050	-.136	.020	.151	.253	.353	.451	.478	.409	.309	.214	.103	-.069
	.100	-.413	-.189	-.067	.025	.130	.215	.241	.175	.078	-.007	-.109	-.325
	.200	-.472	-.389	-.303	-.213	-.114	-.036	-.010	-.071	-.159	-.255	-.338	-.432
	.300	-.504	-.422	-.320	-.205	-.127	-.146	-.121	-.176	-.255	-.322	-.331	-.453
	.400	-.477	-.390	-.298	-.222	-.132	-.255	-.236	-.280	-.337	-.333	-.366	-.450
	.500	-.446	-.390	-.314	-.238	-.155	-.312	-.294	-.332	-.338	-.348	-.376	-.409
	.600	-.495	-.463	-.438	-.408	-.402	-.394	-.380	-.409	-.381	-.414	-.450	-.487
	.700	-.535	-.508	-.479	-.455	-.425	-.442	-.432	-.451	-.427	-.457	-.488	-.525
	.800	-.582	-.569	-.537	-.515	-.484	-.513	-.508	-.494	-.493	-.517	-.545	-.576
.900	-.107	-.111	-.126	-.163	-.194	-.196	-.213	-.192	-.168	-.133	-.110	-.105	
.950	-.028	-.035	-.043	-.050	-.051	-.084	-.092	-.056	-.040	-.037	-.026	-.019	
Lower surface	.0375	.144	-.010	-.541	-.727	-.799	-.853	-.868	-.853	-.791	-.704	-.237	.073
	.075	.168	.071	-.041	-.606	-.709	-.764	-.782	-.761	-.690	-.562	.035	.123
	.150	.151	.082	.052	-.163	-.397	-.668	-.685	-.664	-.575	.064	.046	.118
	.250	.140	.091	.058	.101	-.375	-.553	-.524	-.524	-.455	.073	.065	.118
	.350	.108	.074	.046	.061	.072	-.419	-.460	-.493	.095	.047	.053	.091
	.450	.099	.072	.048	.049	.103	-.446	-.316	-.071	.074	.044	.056	.087
	.550	.074	.050	.026	.020	.064	-.049	-.070	.079	.036	.021	.037	.064
	.650	.090	.069	.047	.040	.064	.086	.069	.082	.049	.044	.058	.082
	.750	.042	.025	.006	-.006	.010	.049	.056	.029	.004	.002	.016	.035
	.850	.088	.073	.055	.047	.054	.072	.077	.062	.053	.053	.067	.084
	.925	.119	.108	.093	.087	.088	.088	.087	.090	.091	.092	.105	.121
b.975	.142	.135	.119	.115	.100	.100	.095	.112	.125	.122	.130	.144	
a1.000	.156	.151	.135	.130	.110	.111	.102	.129	.148	.140	.145	.157	

^aNo orifices.
^bPaired values.



TABLE 9.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN

NACA 16-504 40 PROPELLER BLADE SECTION ($x = 0.95$); $\beta_x = 38.35^\circ$; $\beta_{0.75R} = 45^\circ$ - Continued(e) $M = 0.56$; $B = 2$.

J	2.122	2.162	2.195	2.236	2.270	2.314	2.363	2.416	2.465	2.517	2.549	2.612	2.653	
M_x	.982	.970	.960	.951	.938	.927	.918	.906	.895	.884	.875	.863	.850	
α_x	2.94	2.43	2.02	1.51	1.09	.56	-.02	-.64	-1.20	-1.79	-2.15	-2.84	-3.28	
$\Delta\delta$.12	-.04	-.15	-.22	-.28	-.35	-.46	-.55	-.61	-1.03	-1.13	-1.32	-1.44	
α_1	2.46	2.32	2.10	1.91	1.69	1.42	1.29	.96	.68	.48	.28	.03	-.24	
α_n	.3965	.3713	.3384	.3074	.2716	.2297	.2090	.1555	.1103	.0767	.0452	.0045	-.0397	
α_m	-.1379	-.1363	-.1240	-.1216	-.1154	-.1154	-.1170	-.1221	-.1270	-.1270	-.1263	-.1229	-.1208	
c_c	.0266	.0278	.0255	.0251	.0243	.0251	.0256	.0280	.0303	.0319	.0322	.0344	.0357	
c/b	Pressure coefficient, P													
Upper surface	θ_0 .000	1.264	1.257	1.251	1.246	1.239	1.233	1.228	1.221	1.217	1.210	1.206	1.199	1.194
	.025	.433	.421	.407	.404	.392	.384	.360	.369	.364	.372	.364	.372	.354
	.050	.143	.150	.161	.177	.193	.221	.244	.293	.330	.359	.381	.420	.447
	.100	-.125	-.080	-.056	-.042	-.027	-.001	.019	.064	.097	.124	.141	.177	.201
	.200	-.265	-.268	-.270	-.272	-.267	-.232	-.213	-.170	-.138	-.113	-.095	-.062	-.039
	.300	-.352	-.357	-.358	-.355	-.333	-.298	-.267	-.231	-.206	-.187	-.174	-.146	-.126
	.400	-.391	-.384	-.368	-.348	-.336	-.327	-.317	-.300	-.288	-.275	-.264	-.234	-.215
	.500	-.363	-.362	-.353	-.352	-.348	-.344	-.345	-.327	-.305	-.291	-.284	-.259	-.243
	.600	-.412	-.420	-.421	-.419	-.420	-.415	-.405	-.397	-.384	-.377	-.360	-.333	-.314
	.700	-.448	-.462	-.463	-.463	-.464	-.461	-.454	-.439	-.416	-.400	-.396	-.365	-.340
	.800	-.512	-.519	-.484	-.521	-.523	-.515	-.510	-.492	-.455	-.419	-.367	-.319	-.310
.900	-.616	-.562	-.404	-.290	-.188	-.139	-.110	-.101	-.124	-.151	-.117	-.189	-.204	
.950	-.254	-.212	-.167	-.130	-.082	-.040	-.004	.026	.030	.024	.010	.003	-.010	
Lower surface	.0375	-.025	-.155	-.335	-.464	-.571	-.675	-.749	-.858	-.948	-1.015	-1.095	-1.185	-1.282
	.075	.113	.104	.066	-.101	-.310	-.534	-.631	-.753	-.842	-.909	-.990	-1.082	-1.175
	.150	.115	.099	.084	.085	.090	.082	.023	-.332	-.754	-.647	-.732	-.561	-.519
	.250	.112	.098	.083	.074	.071	.078	.087	.101	.077	.030	-.045	-.178	-.299
	.350	.096	.085	.070	.061	.053	.051	.054	.068	.075	.080	.074	.059	.007
	.450	.092	.081	.069	.062	.053	.047	.047	.053	.058	.058	.052	.056	.047
	.550	.056	.049	.039	.032	.028	.023	.025	.031	.033	.037	.029	.033	.031
	.650	.071	.064	.055	.050	.047	.044	.049	.053	.059	.059	.055	.055	.050
	.750	.016	.011	.004	.001	.002	.005	.013	.025	.033	.037	.033	.033	.033
	.850	.066	.057	.049	.046	.047	.053	.067	.081	.090	.093	.088	.089	.083
	.925	.108	.097	.085	.079	.082	.093	.111	.128	.136	.140	.132	.133	.124
.975	.138	.125	.115	.110	.108	.122	.138	.156	.170	.171	.169	.172	.155	
1.000	.153	.141	.130	.127	.121	.137	.151	.170	.185	.188	.188	.192	.171	

^aNo orifice.

TABLE 9.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN

NACA 16-504 40 PROPELLER BLADE SECTION ($x = 0.95$;

$\beta_x = 38.35^\circ$; $\beta_{0.75R} = 45^\circ$) - Continued

(r) $M = 0.58$; $B = 2$.

	2.129	2.161	2.197	2.229	2.264	2.296	2.337	2.388	2.426	2.471	2.520	2.573	2.637	
J	2.129	2.161	2.197	2.229	2.264	2.296	2.337	2.388	2.426	2.471	2.520	2.573	2.637	
M_x	1.019	1.009	.999	.988	.975	.963	.952	.943	.931	.920	.910	.899	.882	
α_x'	2.85	2.44	1.99	1.60	1.17	.78	.29	-.31	-.76	-1.27	-1.83	-2.41	-3.11	
$\Delta\delta$.18	-.04	-.26	-.42	-.56	-.65	-.71	-.76	-.82	-.85	-1.12	-1.32	-1.55	
α_i	2.41	2.19	1.95	1.85	1.62	1.47	1.25	.97	.84	.60	.46	.22	-.20	
c_n	.3884	.3532	.3142	.2961	.2610	.2374	.2019	.1555	.1368	.0961	.0748	.0348	-.0329	
c_m	-.1610	-.1526	-.1439	-.1392	-.1366	-.1322	-.1281	-.1259	-.1272	-.1281	-.1322	-.1268	-.1281	
c_c	.0341	.0332	.0325	.0328	.0340	.0310	.0306	.0304	.0308	.0310	.0317			
c/b	Pressure coefficient, P													
Upper surface	$r_{0.000}$	1.286	1.280	1.274	1.268	1.260	1.253	1.248	1.242	1.236	1.230	1.224	1.219	1.210
	.025	.502	.522	.538	.552	.613	.587	.604	.636	.654	.692	.701	.728	.762
	.050	.207	.225	.238	.250	.268	.281	.296	.328	.346	.364	.393	.423	.459
	.100	-.040	-.009	.025	.036	.051	.061	.073	.100	.115	.149	.155	.178	.211
	.200	-.211	-.205	-.201	-.203	-.195	-.179	-.166	-.144	-.132	-.099	-.095	-.073	-.040
	.300	-.299	-.293	-.277	-.292	-.274	-.272	-.269	-.249	-.232	-.199	-.196	-.175	-.142
	.400	-.368	-.358	-.347	-.348	-.348	-.346	-.343	-.331	-.329	-.294	-.280	-.271	-.239
	.500	-.338	-.324	-.318	-.329	-.330	-.330	-.346	-.351	-.345	-.306	-.299	-.272	-.263
	.600	-.389	-.381	-.378	-.384	-.383	-.381	-.386	-.377	-.369	-.360	-.358	-.364	-.340
	.700	-.422	-.417	-.414	-.420	-.420	-.420	-.425	-.419	-.424	-.405	-.403	-.385	-.378
	.800	-.478	-.470	-.470	-.478	-.480	-.482	-.485	-.480	-.484	-.459	-.452	-.430	-.384
.900	-.588	-.585	-.589	-.595	-.577	-.401	-.281	-.188	-.145	-.101	-.110	-.139	-.175	
.950	-.645	-.641	-.621	-.643	-.614	-.425	-.091	-.047	-.019	.036	.035	.068	.013	
Lower surface	.0375	-.209	-.308	-.383	-.457	-.540	-.607	-.679	-.758	-.833	-.911	-.970	-1.060	-1.162
	.075	.009	-.165	-.269	-.353	-.438	-.507	-.584	-.668	-.744	-.816	-.873	-.968	-1.073
	.150	.135	.137	.121	-.002	-.178	-.318	-.459	-.574	-.632	-.707	-.761	-.845	-.929
	.250	.124	.124	.125	.127	.131	.129	.096	-.005	-.083	-.142	-.175	-.250	-.364
	.350	.098	.096	.093	.089	.094	.099	.123	.112	.106	.102	.079	.002	-.119
	.450	.098	.093	.087	.078	.077	.077	.077	.089	.092	.108	.102	.099	.073
	.550	.060	.057	.052	.043	.041	.041	.038	.049	.052	.071	.067	.068	.070
	.650	.071	.069	.065	.055	.051	.052	.047	.054	.057	.077	.074	.073	.073
	.750	.037	.036	.033	.026	.029	.022	.019	.029	.035	.061	.061	.062	.064
	.850	.079	.074	.067	.056	.049	.046	.043	.054	.063	.093	.094	.095	.095
	$r_{.925}$.150	.141	.127	.115	.102	.096	.092	.104	.114	.146	.148	.146	.144
$r_{.975}$.227	.216	.186	.171	.166	.140	.130	.150	.156	.186	.200	.189	.189	
$r_{1.000}$.280	.265	.225	.205	.205	.166	.150	.170	.177	.210	.225	.210	.210	

^aNo orifice.
^baired value.



TABLE 9.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN

NACA 16-504.40 PROPELLER BLADE SECTION ($\alpha = 0.95^\circ$;

$\beta_x = 38.35^\circ$; $\beta_{0.72R} = 45^\circ$) - Continued

(g) $M = 0.60$; $B = 2$.

	2.132	2.161	2.189	2.222	2.253	2.287	2.312	2.333	2.381	2.412	2.451	2.490	2.527	2.568	2.599	
\bar{J}	2.132	2.161	2.189	2.222	2.253	2.287	2.312	2.333	2.381	2.412	2.451	2.490	2.527	2.568	2.599	
M_x	1.050	1.040	1.031	1.083	1.014	1.005	.993	.987	.975	.967	.958	.949	.941	.932	.921	
α_x^1	2.81	2.44	2.09	1.68	1.30	.89	.59	.10	-.23	-.79	-1.04	-1.49	-1.91	-2.36	-2.70	
$\Delta\theta$	-.45	-.46	-.48	-.53	-.61	-.72	-.81	-.99	-1.10	-1.20	-1.30	-1.37	-1.42	-1.47	-1.51	
α_t	2.09	1.97	1.85	1.70	1.55	1.25	1.11	.85	.73	.53	.25	.13	-.09	-.22	-.40	
c_n	.3371	.3181	.2971	.2745	.2481	.2003	.1790	.1381	.1177	.0868	.0406	.0206	-.0155	-.0348	-.0658	
c_m	-.1565	-.1604	-.1615	-.1631	-.1592	-.1540	-.1525	-.1531	-.1490	-.1460	-.1399	-.1388	-.1355	-.1360	-.1368	
c_o	.0355	.0371	.0377	.0391	.0386	.0384	.0389	.0397	.0392	.0378	.0365	.0368	.0365	.0367	.0376	
c/b	Pressure coefficient, P															
Upper surface	^a 0.000	1.306	1.300	1.294	1.289	1.283	1.277	1.271	1.267	1.260	1.256	1.251	1.246	1.241	1.236	1.230
	.025	.564	.576	.581	.633	.610	.636	.642	.665	.677	.688	.705	.721	.740	.759	.778
	.050	.272	.280	.284	.296	.311	.336	.341	.364	.375	.386	.402	.421	.439	.458	.477
	.100	.041	.061	.070	.081	.096	.120	.122	.142	.151	.159	.172	.186	.201	.217	.233
	.200	-.154	-.154	-.156	-.153	-.147	-.125	-.117	-.099	-.094	-.088	-.077	-.064	-.051	-.038	-.023
	.300	-.241	-.245	-.248	-.244	-.229	-.213	-.217	-.204	-.203	-.198	-.185	-.174	-.164	-.153	-.142
	.400	-.331	-.334	-.328	-.315	-.311	-.299	-.302	-.289	-.290	-.290	-.285	-.279	-.272	-.261	-.250
	.500	-.315	-.331	-.331	-.335	-.335	-.327	-.336	-.332	-.337	-.338	-.334	-.333	-.331	-.329	-.324
	.600	-.359	-.371	-.374	-.378	-.382	-.389	-.402	-.402	-.406	-.409	-.408	-.411	-.413	-.412	-.404
	.700	-.385	-.395	-.398	-.400	-.401	-.402	-.414	-.417	-.428	-.432	-.438	-.450	-.449	-.444	-.423
	.800	-.444	-.449	-.451	-.453	-.454	-.455	-.465	-.467	-.474	-.477	-.481	-.491	-.484	-.471	-.453
	.900	-.550	-.559	-.563	-.564	-.566	-.567	-.577	-.571	-.511	-.375	-.231	-.172	-.120	-.099	-.096
.950	-.648	-.661	-.665	-.637	-.501	-.370	-.285	-.188	-.141	-.107	-.068	-.048	-.008	-.023	-.042	
Lower surface	^a 0.0375	-.245	-.309	-.363	-.418	-.474	-.539	-.587	-.644	-.696	-.745	-.798	-.859	-.920	-.970	-1.030
	.075	-.164	-.221	-.270	-.324	-.383	-.453	-.503	-.565	-.617	-.663	-.715	-.773	-.831	-.881	-.946
	.150	-.085	-.072	-.139	-.218	-.279	-.351	-.402	-.463	-.517	-.563	-.616	-.675	-.729	-.774	-.830
	.250	.133	.143	.134	.095	.028	-.140	-.223	-.320	-.376	-.425	-.483	-.549	-.608	-.657	-.714
	.350	.116	.116	.116	.122	.128	.121	.108	.055	.016	-.016	-.094	-.199	-.293	-.253	-.223
	.450	.112	.106	.103	.105	.110	.120	.117	.122	.115	.110	.100	.071	.050	.035	.033
	.550	.064	.096	.054	.058	.064	.074	.072	.084	.085	.086	.090	.086	.087	.087	.085
	.650	.070	.063	.061	.062	.067	.072	.068	.078	.079	.080	.085	.086	.092	.092	.100
	.750	.030	.022	.020	.018	.027	.031	.029	.039	.039	.042	.050	.053	.066	.066	.076
	.850	.078	.073	.069	.068	.065	.061	.054	.057	.054	.054	.063	.066	.083	.083	.106
	^b .925	.172	.161	.150	.141	.132	.123	.111	.107	.100	.096	.103	.106	.124	.140	.153
	.975	.259	.248	.218	.195	.188	.172	.162	.147	.153	.133	.137	.140	.161	.180	.188
^b 1.000	.305	.298	.255	.222	.218	.195	.188	.168	.183	.151	.154	.160	.180	.200	.202	

^aNo orifice.
^bPaired value.



TABLE 9.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN

NACA 16-504.40 PROPELLER BLADE SECTION ($x = 0.95$; $\beta_x = 38.35^\circ$; $\beta_{0.75R} = 45^\circ$) - Continued(h) $M = 0.65$; $B = 2$.

	2.104	2.132	2.157	2.189	2.212	2.243	2.266	2.304	2.326	2.356	2.390	2.413	2.455	2.483	
\bar{C}_m	1.136	1.127	1.117	1.108	1.095	1.087	1.076	1.069	1.060	1.045	1.037	1.028	1.020	1.009	
α_x'	3.17	2.81	2.49	2.09	1.81	1.42	1.14	.68	.42	.06	-.34	-.61	-1.09	-1.41	
$\Delta\beta$	-.90	-.98	-1.06	-1.16	-1.23	-1.31	-1.37	-1.46	-1.51	-1.57	-1.63	-1.67	-1.73	-1.76	
F_1	1.77	1.55	1.39	1.29	1.08	.89	.80	.63	.47	.27	.12	-.09	-.34	-.64	
c_n	.2839	.2481	.2235	.2077	.1748	.1432	.1297	.1019	.0768	.0432	.0187	-.0155	-.0552	-.1032	
$c_{m\alpha}$	-.1467	-.1483	-.1482	-.1526	-.1515	-.1511	-.1513	-.1480	-.1501	-.1462	-.1420	-.1406	-.1268	-.1163	
c_c	.0342	.0376	.0390	.0412	.0418	.0429	.0442	.0445	.0460	.0471	.0493	.0482	.0469	.0391	
c/b	Pressure coefficient, P														
Upper surface	$\alpha_0.000$	1.364	1.358	1.351	1.344	1.336	1.331	1.323	1.319	1.312	1.303	1.298	1.292	1.287	1.280
	.025	.659	.671	.674	.687	.696	.710	.717	.729	.738	.746	.757	.763	.780	.795
	.050	.378	.390	.389	.400	.409	.421	.428	.440	.450	.455	.466	.473	.489	.504
	.100	.121	.161	.167	.184	.193	.204	.212	.223	.232	.234	.243	.247	.262	.273
	.200	-.038	-.036	-.043	-.038	-.038	-.035	-.032	-.017	-.004	-.003	.003	.004	.016	.025
	.300	-.124	-.124	-.134	-.129	-.130	-.125	-.115	-.111	-.109	-.113	-.110	-.112	-.100	-.090
	.400	-.227	-.223	-.234	-.222	-.217	-.213	-.214	-.207	-.203	-.208	-.208	-.211	-.205	-.202
	.500	-.241	-.240	-.255	-.251	-.256	-.259	-.258	-.252	-.252	-.259	-.262	-.267	-.260	-.256
	.600	-.291	-.297	-.316	-.316	-.325	-.329	-.331	-.327	-.329	-.340	-.342	-.347	-.341	-.340
	.700	-.310	-.320	-.339	-.341	-.350	-.356	-.358	-.356	-.360	-.372	-.372	-.383	-.381	-.384
	.800	-.358	-.370	-.392	-.395	-.407	-.414	-.420	-.418	-.427	-.442	-.447	-.455	-.454	-.460
.900	-.453	-.465	-.487	-.494	-.509	-.517	-.525	-.524	-.535	-.555	-.559	-.570	-.570	-.579	
.950	-.540	-.552	-.575	-.583	-.599	-.610	-.618	-.620	-.634	-.651	-.658	-.680	-.689	-.688	
Lower surface	$\alpha_0.0375$	-.124	-.186	-.234	-.280	-.330	-.376	-.424	-.466	-.512	-.554	-.600	-.644	-.686	-.741
	.075	-.058	-.112	-.177	-.203	-.256	-.305	-.356	-.398	-.443	-.487	-.532	-.574	-.615	-.666
	.150	.023	-.035	-.086	-.129	-.181	-.228	-.276	-.318	-.362	-.405	-.450	-.491	-.533	-.583
	.250	.091	.028	-.020	-.059	-.107	-.150	-.192	-.228	-.265	-.307	-.354	-.393	-.436	-.488
	.350	.146	.067	-.001	-.036	-.077	-.113	-.147	-.175	-.203	-.240	-.282	-.313	-.344	-.387
	.450	.169	.155	.088	.031	-.033	-.067	-.096	-.116	-.139	-.171	-.205	-.230	-.254	-.288
	.550	.131	.125	.104	.087	.025	-.035	-.078	-.102	-.123	-.167	-.200	-.221	-.242	-.269
	.650	.131	.125	.109	.107	.096	.074	.049	.040	.029	-.045	-.113	-.131	-.146	-.194
	.750	.076	.068	.055	.058	.056	.061	.067	.078	.072	.044	.010	.008	.002	-.026
	.850	.063	.055	.043	.059	.076	.098	.113	.122	.113	.098	.091	.085	.084	.074
	.925	.220	.207	.194	.199	.195	.193	.187	.181	.168	.149	.138	.126	.120	.106
.975	.392	.370	.304	.352	.301	.284	.252	.230	.210	.175	.149	.148	.138	.117	
1.000	.485	.450	.446	.440	.356	.335	.288	.255	.232	.187	.157	.156	.146	.123	

*No orifice.
 †Faired value.



TABLE 9.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN

NACA 16-504 NO PROPELLER BLADE SECTION ($\alpha = 0.95^\circ$;

$\beta_x = 38.35^\circ$; $\beta_{0.75R} = 45^\circ$) - Continued

(1) $N = 1500$ rpm; $B = 1$.

r	2.592	2.512	2.399	2.288	2.185	2.092	2.009	2.033	1.990	1.965	1.930	1.897	1.849	1.812	1.785	1.751
M_x	.883	.871	.851	.833	.821	.805	.799	.798	.791	.789	.784	.781	.777	.771	.770	.765
α_1	-2.62	-1.74	-1.44	.88	2.14	3.32	3.75	4.09	4.66	4.99	5.46	5.91	6.57	7.09	7.47	7.95
α_2	-1.48	-1.06	-1.52	-.08	.30	.68	.82	.92	1.08	1.17	1.29	1.40	1.54	1.64	1.70	1.77
α_3	.25	.75	1.24	1.70	2.23	2.72	2.90	3.06	3.35	3.47	3.72	3.93	4.23	4.46	4.57	4.76
c_m	.0477	.1439	.2368	.3268	.4313	.5235	.5945	.626	.6323	.6548	.6955	.7315	.7897	.8355	.8594	.9000
c_m	-.1504	-.1386	-.1287	-.1133	-.1050	-.1045	-.1031	-.0985	-.1073	-.1021	-.0995	-.1014	-.0968	-.0968	-.0950	-.0944
c_e																
a/b	Pressure coefficient, P															
Upper surface	a _{0.000}	1.210	1.204	1.194	1.185	1.180	1.173	1.170	1.169	1.166	1.166	1.163	1.162	1.160	1.158	1.155
	a _{.025}	.698	.671	.630	.628	-.060	-.354	-.488	-.628	-.747	-.829	-.860	-.963	-1.177	-1.282	-1.366
	a _{.050}	.423	.345	.225	.064	-.148	-.340	-.420	-.519	-.659	-.754	-.835	-.905	-1.059	-1.175	-1.251
	a _{.100}	.136	.062	-.044	-.176	-.352	-.603	-.699	-.774	-.829	-.883	-.983	-1.072	-1.178	-1.232	-1.304
	b _{.200}	-.209	-.270	-.314	-.380	-.440	-.597	-.655	-.668	-.660	-.669	-.683	-.708	-.780	-.827	-.896
	b _{.300}	-.305	-.332	-.371	-.416	-.467	-.496	-.496	-.501	-.505	-.500	-.495	-.496	-.533	-.568	-.594
	b _{.400}	-.236	-.256	-.293	-.330	-.372	-.403	-.414	-.423	-.432	-.435	-.436	-.439	-.453	-.455	-.458
	b _{.500}	-.290	-.305	-.330	-.356	-.388	-.413	-.424	-.434	-.445	-.449	-.452	-.455	-.469	-.472	-.473
	b _{.600}	-.304	-.313	-.324	-.341	-.367	-.385	-.391	-.399	-.409	-.412	-.417	-.422	-.433	-.435	-.436
	b _{.700}	-.373	-.378	-.367	-.373	-.393	-.404	-.408	-.415	-.425	-.430	-.435	-.440	-.453	-.455	-.459
	b _{.800}	-.395	-.398	-.387	-.388	-.340	-.343	-.343	-.350	-.357	-.360	-.365	-.373	-.383	-.388	-.390
	b _{.900}	-.146	-.151	-.154	-.156	-.165	-.169	-.171	-.174	-.180	-.183	-.188	-.193	-.202	-.203	-.209
	b _{.950}	.088	.021	.012	.004	-.006	-.015	-.019	-.022	-.028	-.031	-.034	-.039	-.046	-.050	-.055
Lower surface	a _{0.000}	-.0375	-1.071	-1.022	-.895	-.074	.094	.224	.318	.363	.397	.436	.474	.517	.548	.569
	a _{.075}	-.967	-.916	-.801	-.020	.102	.198	.229	.262	.295	.321	.353	.380	.414	.438	.455
	a _{.150}	-.881	-.788	-.020	0	.073	.149	.169	.190	.213	.232	.254	.276	.297	.317	.333
	a _{.250}	-.205	.070	.022	.057	.107	.141	.156	.173	.189	.200	.218	.236	.254	.270	.280
	b _{.350}	.065	.021	.007	.041	.073	.114	.124	.135	.146	.157	.169	.183	.197	.209	.217
	b _{.450}	.084	.052	.049	.072	.100	.116	.123	.131	.141	.149	.162	.174	.184	.192	.199
	b _{.550}	.050	.034	.030	.051	.073	.091	.098	.104	.112	.119	.128	.139	.146	.155	.160
	b _{.650}	.055	.050	.050	.064	.080	.090	.094	.100	.106	.113	.120	.130	.134	.141	.145
	b _{.750}	.066	.062	.059	.065	.076	.079	.082	.087	.091	.095	.103	.109	.114	.119	.122
	b _{.850}	.098	.095	.090	.090	.091	.088	.088	.073	.092	.095	.101	.106	.108	.110	.111
	b _{.925}	.123	.114	.113	.120	.112	.107	.104	.062	.090	.094	.097	.092	.098	.095	.100
	b _{.975}	.144	.130	.132	.144	.129	.123	.114	.058	.090	.090	.094	.087	.094	.086	.090
	a _{1.000}	.153	.140	.142	.157	.138	.131	.120	.055	.090	.090	.092	.084	.092	.082	.086

^aNo orifice.

^bPaired value.

^cExtrapolated value.



TABLE 9.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN

NACA 16-504.40 PROPELLER BLADE SECTION ($\tau = 0.95$; $\beta_x = 38.35^\circ$; $\beta_{0.75R} = 45^\circ$) - Continued(j) $M = 0.56$; $B = 1$.

J	2.336	2.301	2.267	2.252	2.222	2.194	2.172	2.145	2.128	2.106	2.079	2.049	2.030	2.006	
M_{x1}	.933	.938	.942	.951	.959	.966	.972	.980	.989	.996	1.003	1.009	1.015	1.024	
$c_{d\beta}$.30	.72	1.13	1.31	1.68	2.03	2.30	2.64	2.86	3.14	3.49	3.88	4.13	4.44	
$c_{d\beta}$	-.39	-.33	-.28	-.25	-.20	-.14	-.08	.02	.20	.40	.61	.83	1.07	1.32	
α_1	1.28	1.43	1.53	1.55	1.72	1.85	2.00	2.10	2.21	2.37	2.51	2.66	2.78	2.82	
c_n	.2442	.2758	.2942	.2981	.3335	.3565	.3865	.4042	.4242	.4526	.4784	.5061	.5252	.5306	
c_m	-.1209	-.1192	-.1195	-.1154	-.1179	-.1233	-.1230	-.1275	-.1343	-.1391	-.1528	-.1637	-.1682	-.1682	
c_o	.0255	.0242	.0239	.0235	.0233	.0233	.0228	.0235	.0245	.0256	.0281	.0305	.0307	.0306	
o/b	Pressure coefficient, P														
Upper surface	a_0	1.238	1.240	1.242	1.247	1.251	1.255	1.259	1.263	1.268	1.272	1.276	1.280	1.284	1.290
	$a_{.025}$.490	.501	.510	.520	.533	.543	.553	.560	.574	.587	.601	.610	.621	.632
	$a_{.050}$.256	.230	.213	.208	.196	.183	.173	.159	.150	.146	.149	.129	.119	.115
	$a_{.100}$	-.021	-.047	-.063	-.067	-.079	-.098	-.117	-.133	-.147	-.154	-.160	-.165	-.168	-.167
	$b_{.200}$	-.305	-.333	-.342	-.352	-.372	-.387	-.401	-.402	-.403	-.418	-.423	-.422	-.419	-.417
	$b_{.300}$	-.390	-.417	-.439	-.448	-.454	-.462	-.464	-.466	-.469	-.470	-.470	-.473	-.476	-.475
	$b_{.400}$	-.312	-.318	-.325	-.334	-.349	-.361	-.365	-.374	-.378	-.386	-.390	-.395	-.403	-.407
	$b_{.500}$	-.367	-.378	-.378	-.378	-.382	-.393	-.398	-.402	-.407	-.410	-.413	-.414	-.415	-.414
	$b_{.600}$	-.339	-.354	-.357	-.355	-.360	-.368	-.368	-.373	-.375	-.378	-.380	-.382	-.386	-.386
	$b_{.700}$	-.431	-.438	-.444	-.441	-.443	-.449	-.451	-.454	-.456	-.456	-.455	-.455	-.459	-.459
Lower surface	$b_{.800}$	-.488	-.496	-.500	-.499	-.493	-.503	-.504	-.507	-.508	-.507	-.507	-.507	-.508	-.507
	$b_{.900}$	-.268	-.282	-.282	-.291	-.328	-.368	-.387	-.419	-.448	-.507	-.535	-.603	-.607	-.613
	$b_{.950}$	-.027	-.050	-.076	-.096	-.130	-.162	-.199	-.249	-.310	-.406	-.524	-.664	-.714	-.723
	$a_{.0375}$	-.693	-.608	-.537	-.476	-.372	-.233	-.066	.011	.038	.089	.122	.149	.178	.201
	$a_{.075}$	-.568	-.405	-.225	-.107	.035	.073	.074	.083	.107	.130	.156	.185	.211	.231
	$a_{.150}$	-.048	.052	.035	.031	.028	.032	.045	.058	.079	.096	.114	.134	.150	.165
	$a_{.250}$.079	.069	.066	.068	.075	.083	.095	.105	.119	.132	.146	.161	.175	.185
	$a_{.350}$.045	.041	.041	.046	.052	.059	.069	.074	.087	.095	.105	.117	.127	.135
	$a_{.450}$.065	.066	.068	.071	.078	.083	.092	.096	.107	.116	.124	.136	.144	.152
	$a_{.550}$.036	.037	.037	.040	.044	.048	.055	.057	.067	.074	.081	.091	.099	.106
$a_{.650}$.053	.053	.052	.054	.058	.060	.067	.068	.076	.082	.090	.097	.106	.111	
$a_{.750}$.028	.024	.022	.022	.023	.022	.027	.027	.033	.038	.044	.051	.058	.061	
$a_{.850}$.053	.047	.043	.040	.041	.043	.047	.049	.055	.062	.069	.075	.084	.089	
$b_{.925}$.092	.092	.093	.077	.077	.086	.086	.089	.102	.107	.123	.130	.141	.145	
$b_{.975}$.120	.136	.142	.112	.112	.126	.123	.131	.150	.151	.178	.183	.204	.188	
$a_{1.000}$.134	.162	.173	.133	.133	.146	.146	.157	.182	.177	.214	.218	.248	.232	

^aNo orifice.^bPaired values.^cExtrapolated value.

TABLE 9.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN

NACA 16-504.40 PROPELLER BLADE SECTION ($\alpha = 0.97^\circ$;

$\beta_x = 38.35^\circ$; $\beta_0.75R = 45^\circ$) - Continued

(k) $M = 0.58$; $B = 1.$

	2.494	2.379	2.311	2.279	2.245	2.225	2.198	2.172	2.154	2.129	2.103	2.084	2.063	2.043	2.022	2.003	1.986	1.976	1.951	
J	.930	.949	.965	.974	.980	.985	.991	.999	1.008	1.016	1.021	1.029	1.036	1.043	1.050	1.057	1.065	1.069	1.079	
α_{x1}	-1.10	-.23	.58	.96	1.38	1.63	1.96	2.28	2.51	2.83	3.16	3.40	3.68	3.94	4.21	4.46	4.69	5.09	5.16	
α_{48}	-.90	-.73	-.68	-.61	-.59	-.40	-.26	-.12	0	.15										
α_1	.67	.88	1.13	1.28	1.45	1.57	1.68	1.83	2.01	2.07	2.20	2.24	2.34	2.40	2.45	2.52	2.55	2.57	2.58	
α_n	.1897	.1684	.2161	.2468	.2803	.3016	.3235	.3589	.3868	.3992	.4197	.4432	.4581	.4687	.4687	.4687	.4687	.4687	.4835	
α_m	-.1273	-.1193	-.1213	-.1226	-.1230	-.1274	-.1330	-.1452	-.1540	-.1541	-.1595	-.1697	-.1686	-.1610	-.1635	-.1668	-.1664	-.1635	-.1649	
α_c	.0297	.0282	.0278	.0281	.0272	.0278	.0289	.0301	.0334	.0325	.0326	.0334	.0333	.0325	.0332	.0331	.0329	.0335	.0328	
a/b	Pressure coefficient, P																			
Upper surface	$b_0.000$	1.235	1.246	1.254	1.259	1.263	1.266	1.270	1.275	1.280	1.285	1.288	1.293	1.296	1.302	1.306	1.311	1.317	1.319	1.325
	$b_{.025}$.547	.571	.598	.609	.617	.627	.639	.650	.664	.674	.683	.694	.707	.716	.723	.730	.741	.751	.763
	$b_{.050}$.364	.332	.302	.289	.263	.255	.246	.238	.234	.226	.216	.213	.204	.199	.195	.190	.183	.174	.175
	$b_{.100}$.076	.048	.022	.010	-.014	-.023	-.036	-.051	-.062	-.069	-.076	-.075	-.073	-.079	-.072	-.069	-.060	-.050	-.037
	$b_{.300}$	-.228	-.247	-.284	-.287	-.317	-.317	-.324	-.326	-.334	-.328	-.332	-.326	-.335	-.353	-.328	-.339	-.320	-.278	-.278
	$b_{.400}$	-.366	-.375	-.386	-.393	-.410	-.412	-.414	-.410	-.411	-.413	-.409	-.410	-.411	-.410	-.411	-.410	-.413	-.417	-.410
	$b_{.500}$	-.312	-.319	-.320	-.327	-.333	-.337	-.334	-.336	-.335	-.341	-.349	-.349	-.354	-.358	-.361	-.364	-.366	-.375	-.369
	$b_{.600}$	-.342	-.361	-.354	-.356	-.358	-.362	-.364	-.369	-.371	-.374	-.378	-.378	-.377	-.380	-.376	-.377	-.374	-.372	-.363
	$b_{.700}$	-.301	-.311	-.320	-.323	-.329	-.333	-.333	-.337	-.336	-.343	-.343	-.343	-.344	-.344	-.347	-.344	-.344	-.353	-.346
	$b_{.800}$	-.404	-.403	-.406	-.408	-.413	-.414	-.413	-.417	-.415	-.418	-.416	-.416	-.415	-.414	-.415	-.416	-.416	-.420	-.417
	$b_{.900}$	-.463	-.461	-.462	-.464	-.468	-.469	-.467	-.469	-.468	-.466	-.469	-.468	-.464	-.465	-.464	-.466	-.466	-.469	-.465
$b_{.950}$	-.185	-.186	-.277	-.323	-.347	-.322	-.462	-.477	-.549	-.598	-.572	-.573	-.574	-.572	-.558	-.563	-.564	-.573	-.562	
$b_{.990}$.010	-.040	-.104	-.153	-.189	-.250	-.309	-.469	-.621	-.671	-.688	-.689	-.683	-.683	-.677	-.677	-.666	-.667	-.658	
Lower surface	$b_0.000$	-.0375	-.717	-.593	-.534	-.475	-.420	-.364	-.302	-.225	-.150	-.092	-.063	-.039	-.022	-.009	0	.015	.028	.043
	$b_{.075}$	-.730	-.638	-.508	-.451	-.373	-.289	-.169	-.033	-.080	-.111	-.118	-.135	-.164	-.184	-.203	-.220	-.247	-.262	-.283
	$b_{.150}$	-.685	-.584	-.353	-.197	.037	.022	.079	.073	.073	.079	.091	.106	.127	.141	.156	.167	.188	.199	.216
	$b_{.250}$	-.020	.103	.138	.131	.110	.105	.104	.107	.115	.125	.135	.146	.163	.172	.182	.192	.208	.216	.231
	$b_{.350}$.113	.101	.081	.072	.060	.059	.064	.069	.080	.089	.096	.103	.117	.125	.130	.137	.152	.153	.169
	$b_{.450}$.101	.094	.088	.086	.083	.086	.093	.095	.109	.118	.123	.132	.144	.150	.157	.162	.176	.178	.191
	$b_{.550}$.056	.045	.039	.037	.038	.041	.047	.052	.061	.069	.076	.082	.089	.094	.099	.106	.109	.122	.126
	$b_{.650}$.060	.049	.048	.046	.049	.051	.058	.062	.071	.079	.082	.089	.090	.103	.108	.112	.130	.124	.134
	$b_{.750}$.043	.032	.026	.024	.026	.027	.033	.034	.041	.049	.050	.056	.066	.067	.071	.075	.090	.087	.096
	$b_{.850}$.066	.048	.041	.040	.043	.047	.054	.058	.066	.073	.076	.081	.091	.091	.095	.097	.112	.105	.111
	$b_{.925}$.092	.063	.066	.072	.077	.081	.097	.102	.116	.128	.136	.148	.168	.167	.167	.182	.145	.132	.146
$b_{.975}$.118	.083	.090	.102	.110	.113	.138	.145	.162	.176	.190	.148	.168	.167	.167	.142	.174	.155	.174	
$b_{1.000}$.131	.092	.104	.120	.130	.133	.163	.170	.188	.151	.142	.163	.190	.188	.185	.193	.168	.168	.188	

^aNo orifice.

^bFaired value.

^cExtrapolated value.

NACA

TABLE 9.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN

NACA 16-504.40 PROPELLER BLADE SECTION ($\alpha = 0.95^\circ$; $\beta_x = 38.35^\circ$; $\beta_{0.75R} = 45^\circ$) - Continued(1) $M = 0.60$; $B = 1$.

r	2.323	2.289	2.257	2.230	2.211	2.183	2.160	2.141	2.115	2.102	2.072	2.049	2.030	2.010	1.985	1.970		
M_{x_1}	.995	1.004	1.008	1.016	1.025	1.028	1.036	1.042	1.050	1.060	1.063	1.071	1.077	1.085	1.093	1.104		
c_{d_i}	.45	.86	1.25	1.58	1.82	2.17	2.46	2.70	3.03	3.19	3.58	3.88	4.13	4.39	4.72	4.92		
c_{d_e}	-.86	-.73	-.62	-.55	-.51	-.48	-.46	-.45	-.44	-.44	-.42	-.40	-.38	-.34	-.28	-.23		
c_{l_1}	1.02	1.20	1.35	1.55	1.59	1.67	1.81	1.85	1.92	1.89	2.07	2.19	2.29	2.37	2.43	2.47		
c_{n_1}	.1939	.2306	.2619	.2994	.3088	.3216	.3468	.3538	.3592	.3584	.3890	.4100	.4287	.4451	.4541	.4632		
c_{m_1}	-.1397	-.1390	-.1435	-.1495	-.1509	-.1483	-.1493	-.1513	-.1496	-.1384	-.1436	-.1450	-.1442	-.1473	-.1481	-.1485		
c_{c_1}	.0334	.0345	.0353	.0367	.0367	.0366	.0361	.0361	.0352	.0345	.0333	.0330	.0326	.0324	.0322	.0315		
c/b	Pressure coefficient, P																	
UPPER SURFACE	$b_{0.000}$	1.272	1.277	1.280	1.285	1.290	1.293	1.297	1.301	1.306	1.313	1.315	1.320	1.324	1.329	1.334	1.342	
	$b_{.025}$.907	.905	.909	.921	.935	.952	.973	.966	.976	.987	.996	.606	.615	.628	.641	.652	
	$b_{.050}$.352	.339	.319	.310	.306	.291	.285	.283	.272	.270	.262	.251	.247	.244	.241	.230	
	$b_{.100}$	-.069	-.058	-.039	-.029	-.022	-.002	-.012	-.020	-.035	-.041	-.052	-.063	-.066	-.066	-.067	-.069	
	$b_{.200}$	-.252	-.249	-.268	-.287	-.278	-.298	-.268	-.246	-.258	-.257	-.268	-.271	-.316	-.322	-.302	-.309	
	$b_{.300}$	-.344	-.350	-.361	-.363	-.364	-.370	-.369	-.365	-.369	-.364	-.365	-.371	-.369	-.367	-.367	-.367	
	$b_{.400}$	-.296	-.301	-.311	-.317	-.321	-.327	-.326	-.325	-.327	-.322	-.326	-.335	-.332	-.329	-.330	-.331	
	$b_{.500}$	-.375	-.367	-.365	-.352	-.359	-.361	-.357	-.354	-.358	-.357	-.360	-.367	-.362	-.357	-.356	-.354	
	$b_{.600}$	-.339	-.330	-.324	-.317	-.308	-.312	-.314	-.314	-.320	-.318	-.319	-.327	-.324	-.317	-.317	-.315	
	$b_{.700}$	-.400	-.395	-.394	-.394	-.393	-.392	-.387	-.388	-.392	-.388	-.388	-.394	-.390	-.382	-.382	-.379	
	$b_{.800}$	-.448	-.445	-.445	-.442	-.444	-.440	-.442	-.438	-.439	-.438	-.438	-.442	-.438	-.430	-.427	-.424	
	$b_{.900}$	-.415	-.406	-.401	-.385	-.398	-.368	-.367	-.358	-.357	-.357	-.356	-.356	-.352	-.352	-.352	-.348	
	$b_{.950}$	-.267	-.388	-.513	-.612	-.649	-.666	-.667	-.664	-.664	-.657	-.652	-.653	-.649	-.639	-.631	-.627	
	LOWER SURFACE	$b_{0.075}$	-.551	-.509	-.465	-.415	-.370	-.322	-.272	-.229	-.164	-.070	.038	.121	.153	.187	.217	.255
		$b_{.075}$	-.471	-.435	-.391	-.343	-.295	-.243	-.185	-.114	.024	.115	.145	.164	.186	.215	.239	.273
		$b_{.150}$	-.430	-.409	-.375	-.328	-.270	-.208	.080	.103	.098	.100	.107	.124	.142	.164	.182	.207
$b_{.250}$		-.317	-.047	.138	.165	.154	.136	.130	.131	.129	.138	.147	.159	.173	.191	.206	.228	
$b_{.350}$.101	.087	.063	.065	.118	.105	.091	.088	.089	.097	.105	.113	.124	.141	.151	.172	
$b_{.450}$.082	.072	.049	.052	.071	.016	.102	.089	.072	.055	.087	.083	.102	.116	.127	.142	
$b_{.550}$.063	.057	.051	.052	.029	-.033	.067	.093	.083	.078	.084	.088	.097	.111	.119	.136	
$b_{.650}$.060	.058	.055	.061	.063	.058	.009	.061	.114	.111	.103	.101	.107	.122	.131	.146	
$b_{.750}$.055	.055	.054	.065	.072	.063	.037	.053	.111	.082	.097	.097	.103	.118	.134	.148	
$b_{.850}$.043	.047	.047	.054	.059	.060	.070	.071	.068	.012	.069	.078	.076	.092	.097	.105	
$b_{.925}$.031	.038	.040	.039	.042	.041	.047	.047	.003	-.053	.014	.035	.036	.052	.045	.042	
$b_{.975}$.023	.033	.035	.028	.027	.016	.003	-.003	-.052	-.100	-.032	-.003	.002	.013	.005	.013	
$b_{1.000}$.019	.029	.032	.022	.020	-.003	-.027	-.035	-.082	-.124	-.058	-.025	-.013	-.008	-.016	-.041	

*No ariettes.

†Paired value.

‡Extrapolated value.

NACA

TABLE 9.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN

NACA 16-204.40 PROPELLER BLADE SECTION ($x = 0.95$);

$\beta_x = 38.35^\circ$; $\beta_{0.75R} = 45^\circ$ - Concluded

(a) $M = 0.65$; $\Pi = 1.$

α	2.277	2.245	2.225	2.199	2.178	2.159	2.125	2.116	2.103	2.068	2.064	2.042	2.019	
M_{∞}	1.060	1.069	1.076	1.082	1.089	1.100	1.103	1.115	1.123	1.126	1.136	1.144	1.150	
c_{dR}	1.01	1.40	1.65	1.97	2.23	2.47	2.90	3.01	3.18	3.63	3.68	3.97	4.27	
c_{dR}^*	-1.40	-1.33	-1.27	-1.19	-1.13	-1.07	-.96	-.93	-.89	-.77	-.76	-.68	-.60	
c_{dR}^*	.95	1.06	1.20	1.20	1.30	1.35	1.47	1.57	1.64	1.80	1.84	1.91	1.95	
c_{dR}^*	.1832	.2058	.2119	.2303	.2481	.2574	.2768	.2965	.3084	.3361	.3439	.3577	.3635	
c_{dR}^*	-.1323	-.1485	-.1458	-.1454	-.1416	-.1390	-.1369	-.1364	-.1345	-.1337	-.1360	-.1363	-.1337	
c_{dR}^*	.0410	.0401	.0395	.0392	.0384	.0367	.0360	.0363	.0354	.0349	.0346	.0343	.0332	
r/b	Pressure coefficient, P													
Upper surface	$r_0/0.000$	1.313	1.319	1.324	1.327	1.331	1.339	1.342	1.349	1.355	1.377	1.364	1.370	1.374
	.025	.618	.632	.641	.652	.663	.673	.679	.698	.710	.717	.730	.740	.745
	.050	.480	.497	.493	.499	.495	.486	.472	.472	.472	.462	.461	.453	.447
	.100	.145	.130	.125	.120	.112	.099	.079	.077	.073	.068	.075	.077	.078
	.200	-.159	-.147	-.177	-.155	-.155	-.156	-.164	-.162	-.156	-.163	-.156	-.164	-.164
	.300	-.264	-.272	-.270	-.269	-.265	-.267	-.271	-.265	-.268	-.266	-.264	-.270	-.272
	.400	-.223	-.237	-.235	-.236	-.235	-.238	-.245	-.243	-.242	-.244	-.242	-.247	-.250
	.500	-.307	-.313	-.312	-.307	-.305	-.305	-.309	-.305	-.299	-.301	-.294	-.297	-.296
	.600	-.288	-.292	-.287	-.281	-.277	-.274	-.272	-.264	-.254	-.250	-.245	-.247	-.250
	.700	-.369	-.370	-.365	-.356	-.348	-.343	-.338	-.330	-.321	-.319	-.312	-.314	-.317
	.800	-.417	-.416	-.409	-.395	-.386	-.380	-.378	-.371	-.366	-.364	-.356	-.357	-.361
	.900	-.532	-.517	-.530	-.518	-.510	-.487	-.501	-.492	-.503	-.487	-.476	-.474	-.465
	.950	-.605	-.616	-.609	-.597	-.588	-.583	-.580	-.571	-.566	-.564	-.555	-.551	-.553
Lower surface	.0375	-.427	-.378	-.348	-.308	-.272	-.236	-.193	-.144	-.106	-.075	-.044	-.019	-.006
	.075	-.354	-.315	-.287	-.247	-.211	-.171	-.122	-.067	-.024	.023	.084	.154	.185
	.150	-.341	-.298	-.274	-.240	-.211	-.179	-.138	-.086	-.024	.129	.167	.174	.182
	.250	-.192	-.152	-.124	-.084	-.030	.002	.083	.161	.192	.193	.205	.214	.221
	.350	-.142	-.104	-.070	-.009	.047	.109	.126	.134	.143	.148	.157	.164	.170
	.450	.009	.075	.106	.148	.156	.163	.162	.168	.176	.179	.189	.196	.199
	.550	.095	.098	.100	.107	.106	.103	.093	.095	.104	.111	.123	.131	.133
	.650	.110	.103	.102	.105	.104	.104	.101	.107	.116	.124	.136	.144	.145
	.750	.066	.056	.055	.058	.059	.061	.059	.067	.076	.086	.099	.106	.109
	.850	.035	.063	.051	.047	.045	.041	.036	.042	.049	.059	.073	.078	.078
	.925	.108	.083	.064	.054	.051	.048	.047	.052	.043	.043	.060	.065	.063
	.975	.124	.098	.077	.061	.058	.058	.058	.062	.045	.038	.055	.057	.056
	1.000	.133	.106	.084	.065	.064	.064	.065	.068	.045	.038	.054	.054	.052

^aNo orifice.

^bPaired value.

^cExtrapolated value.

NACA

TABLE 10.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS

OF THE BLADE SECTION ($x = 0.975$; $\beta_x = 37.90^\circ$; $\beta_{0.75R} = 45^\circ$; $B = 2$)(a) $N = 1140$ rpm.

	1.679	1.794	1.898	1.974	2.080	2.201	2.317	2.445	2.563	2.744	2.846	2.511	2.391	2.275	2.147	2.032	1.939	1.830	1.749	1.600	
J	.607	.618	.627	.637	.644	.654	.668	.685	.695	.716	.704	.688	.678	.664	.642	.635	.629	.622	.615	.602	
M_x	9.17	7.54	6.12	5.10	3.72	2.20	.80	-.70	-2.02	-3.95	-2.92	-1.45	-.08	1.30	2.87	4.34	5.57	7.04	8.17	10.32	
$\Delta\delta$	1.16	.94	.74	.60	.45	.20	-.05	-.32	-.57	-.95	-.75	-.46	-.20	.05	.32	.50	.67	.87	1.02	1.31	
α_1	5.87	5.17	4.28	3.67	3.05	2.30	1.61	1.09	.55	-.47	.09	.81	1.32	1.83	2.55	3.28	3.85	4.67	5.31	6.10	
α_n	.6819	.5987	.4935	.4229	.3548	.2700	.1884	.1265	.0639	-.0548	-.0110	.0942	.1529	.2139	.2981	.3813	.4432	.5406	.6123	.7097	
α_m	-.0787	-.0785	-.0793	-.0753	-.0723	-.0702	-.0679	-.0674	-.0705	-.0767	-.0764	-.0688	-.0666	-.0678	-.0696	-.0725	-.0771	-.0785	-.0831	-.0773	
α_c	-.0394	-.0251	-.0180	-.0079	-.0034	-.0025	-.0073	-.0143	-.0174	-.0223	-.0192	-.0151	-.0105	-.0067	-.0011	-.0038	-.0083	-.0165	-.0280	-.0455	
o/b	Pressure coefficient, P																				
Upper surface	a_0 .000	1.095	1.099	1.102	1.105	1.108	1.111	1.117	1.123	1.127	1.135	1.131	1.125	1.121	1.115	1.111	1.104	1.102	1.100	1.098	1.093
	.025	-1.638	-1.587	-1.547	-1.448	-1.272	-.016	.237	.448	.535	.658	.604	.486	.336	.153	-.112	-.379	-.525	-1.396	-1.619	-1.510
	.050	-1.540	-1.072	-.569	-.442	-.324	-.164	-.002	.161	.286	.338	.287	.186	.067	-.056	-.232	-.372	-.517	-.711	-1.259	-1.523
	.100	-.860	-.542	-.483	-.409	-.325	-.244	-.147	-.031	.001	.086	.047	-.025	-.104	-.181	-.281	-.379	-.463	-.535	-.582	-1.277
	.200	-.460	-.439	-.384	-.338	-.291	-.246	-.196	-.118	-.121	-.076	-.097	-.137	-.172	-.213	-.270	-.327	-.380	-.427	-.460	-.493
	.300	-.415	-.379	-.327	-.289	-.249	-.215	-.182	-.118	-.139	-.118	-.129	-.142	-.164	-.194	-.236	-.280	-.326	-.365	-.401	-.430
	.400	-.433	-.391	-.341	-.306	-.272	-.244	-.210	-.156	-.178	-.152	-.163	-.184	-.198	-.223	-.262	-.300	-.340	-.377	-.414	-.454
	.500	-.391	-.351	-.309	-.275	-.241	-.214	-.183	-.125	-.146	-.150	-.140	-.151	-.170	-.194	-.231	-.272	-.311	-.346	-.378	-.409
	.600	-.399	-.361	-.320	-.289	-.256	-.231	-.201	-.145	-.171	-.160	-.163	-.173	-.189	-.211	-.249	-.285	-.323	-.355	-.385	-.415
	.700	-.397	-.363	-.323	-.296	-.266	-.241	-.210	-.156	-.184	-.177	-.179	-.187	-.200	-.223	-.260	-.292	-.328	-.355	-.385	-.413
	.800	-.366	-.337	-.306	-.279	-.254	-.235	-.207	-.151	-.178	-.170	-.175	-.181	-.195	-.219	-.254	-.282	-.313	-.332	-.356	-.378
.900	-.349	-.326	-.303	-.282	-.261	-.244	-.219	-.165	-.201	-.211	-.203	-.199	-.207	-.231	-.260	-.285	-.313	-.328	-.346	-.361	
.950	-.220	-.204	-.181	-.165	-.144	-.132	-.108	-.057	-.093	-.106	-.095	-.091	-.099	-.121	-.144	-.168	-.195	-.205	-.218	-.232	
Lower surface	.0375	.521	.453	.363	.281	.178	.036	-.125	-.232	-.534	-1.004	-.838	-.362	-.195	-.072	.079	.211	.294	.401	.467	.544
	.075	.385	.331	.262	.202	.130	.032	-.061	-.116	-.273	-.598	-.427	-.211	-.106	-.037	.058	.148	.206	.288	.338	.401
	.150	.278	.241	.193	.156	.110	.049	0	-.020	-.125	-.326	-.208	-.089	-.031	.010	.060	.116	.150	.208	.244	.288
	.250	.205	.181	.148	.124	.093	.049	.019	.024	-.055	-.177	-.097	-.034	.002	.028	.056	.001	.112	.153	.179	.207
	.350	.167	.149	.124	.105	.083	.058	.028	.042	-.022	-.103	-.048	-.007	.015	.034	.053	.077	.091	.125	.145	.166
	.450	.161	.145	.127	.113	.097	.065	.044	.063	.006	-.050	-.013	.017	.035	.050	.070	.089	.098	.127	.141	.159
	.550	.138	.126	.112	.100	.087	.060	.042	.066	.015	-.024	.002	.023	.035	.045	.061	.077	.085	.108	.120	.133
	.650	.111	.099	.089	.078	.067	.047	.033	.060	.015	-.013	.005	.020	.027	.034	.043	.057	.061	.083	.095	.103
	.750	.100	.094	.086	.078	.070	.050	.041	.072	.028	.010	.022	.033	.036	.041	.047	.057	.059	.076	.084	.092
	b .850	.085	.087	.085	.078	.077	.060	.058	.092	.051	.041	.052	.057	.055	.054	.053	.061	.058	.066	.070	.070
	.925	.076	.078	.082	.083	.083	.073	.074	.112	.075	.069	.074	.077	.073	.071	.066	.067	.059	.067	.066	.066
b .975	.139	.135	.120	.145	.136	.135	.145	.164	.128	.116	.143	.114	.113	.103	.091	.093	.078	.118	.118	.118	
a_1 .000	.215	.200	.153	.220	.200	.197	.212	.208	.183	.162	.197	.145	.152	.127	.108	.122	.115	.187	.200	.200	

^aNo orifice.^bPaired value.

TABLE 10.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS

OF THE BLADE SECTION ($x = 0.975$; $\beta_x = 37.90^\circ$;

$\beta_{0.75R} = 45^\circ$; $B = 2$) - Continued

(b) $N = 1350$ rpm.

	2.739	2.628	2.502	2.408	2.323	2.231	2.152	2.049	2.097	2.169	2.257	2.355	2.470	2.575	2.696	
J	2.739	2.628	2.502	2.408	2.323	2.231	2.152	2.049	2.097	2.169	2.257	2.355	2.470	2.575	2.696	
M_x	.855	.835	.817	.804	.791	.778	.769	.760	.763	.764	.782	.796	.811	.828	.845	
α_{L1}	-3.90	-2.73	-1.35	-.27	.73	1.83	2.81	4.12	3.50	2.60	1.40	.35	-.98	-2.37	-3.45	
$\Delta\delta$	-1.52	-1.19	-.72	-.43	-.18	.09	.33	.64	.50	.28	-.01	-.27	-.62	-.98	-1.40	
α_1	-.50	.12	.86	1.40	1.85	2.31	2.90	3.49	3.21	2.74	2.12	1.65	1.04	.47	-.23	
c_n	-.0594	-.0135	.0994	.1632	.2155	.2703	.3394	.4058	.3755	.3213	.2471	.1935	.1213	-.0548	-.0271	
c_m	-.0882	-.0926	-.0859	-.0783	-.0793	-.0824	-.0826	-.0839	-.0832	-.0836	-.0810	-.0777	-.0813	-.0822	-.0918	
c_o	-.0256	-.0223	-.0174	-.0130	-.0069	-.0049	-.0002	-.0049	-.0019	-.0026	-.0071	-.0104	-.0155	-.0190	-.0214	
c/b	Pressure coefficient, P															
Upper surface	$a_{0.000}$	1.195	1.186	1.178	1.172	1.167	1.161	1.157	1.153	1.155	1.155	1.162	1.168	1.175	1.183	1.191
	$a_{.025}$.708	.643	.536	.443	.303	.132	-.089	-.344	-.214	-.018	.195	.355	.498	.595	.679
	$a_{.050}$.394	.327	.227	.138	.030	-.096	-.245	-.418	-.329	-.196	-.049	.070	.193	.283	.364
	$a_{.100}$.118	.063	-.009	-.077	-.151	-.231	-.317	-.409	-.362	-.291	-.201	-.126	-.034	.030	.093
	$a_{.200}$	-.086	-.113	-.148	-.183	-.220	-.259	-.302	-.353	-.325	-.288	-.244	-.210	-.158	-.188	-.098
	$a_{.300}$	-.139	-.151	-.161	-.175	-.198	-.228	-.258	-.300	-.278	-.248	-.214	-.193	-.163	-.155	-.143
	$a_{.400}$	-.173	-.171	-.182	-.195	-.213	-.239	-.265	-.303	-.283	-.257	-.226	-.209	-.184	-.170	-.171
	$a_{.500}$	-.187	-.175	-.171	-.188	-.208	-.233	-.262	-.296	-.277	-.253	-.221	-.203	-.173	-.162	-.182
	$a_{.600}$	-.212	-.195	-.202	-.215	-.231	-.256	-.285	-.317	-.300	-.277	-.245	-.228	-.204	-.197	-.199
	$a_{.700}$	-.226	-.215	-.219	-.230	-.246	-.273	-.298	-.327	-.311	-.291	-.261	-.242	-.218	-.212	-.216
	$a_{.800}$	-.229	-.243	-.223	-.232	-.251	-.276	-.299	-.325	-.311	-.294	-.267	-.248	-.223	-.217	-.221
	$a_{.900}$	-.276	-.244	-.231	-.237	-.254	-.281	-.301	-.327	-.313	-.296	-.268	-.250	-.229	-.233	-.254
$a_{.950}$	-.107	-.086	-.085	-.097	-.113	-.138	-.156	-.181	-.166	-.152	-.126	-.110	-.087	-.081	-.093	
Lower surface	$b_{0.0375}$	-1.193	-1.178	-.981	-.198	-.158	-.034	.099	.201	.154	.059	-.070	-.193	-.775	-1.101	-1.191
	$b_{.075}$	-.965	-1.006	-.158	-.141	-.073	-.011	.075	.140	.110	.048	-.033	-.105	-.126	-.748	-1.049
	$b_{.150}$	-.306	-.119	-.071	-.075	-.014	.019	.067	.103	.089	.055	.015	-.036	-.063	-.068	-.205
	$b_{.250}$	-.212	-.096	-.027	-.010	.014	.037	.062	.082	.073	.055	.032	.001	-.014	-.041	-.130
	$b_{.350}$	-.162	-.055	0	.016	.031	.048	.062	.074	.069	.058	.045	.021	-.011	-.015	-.097
	$b_{.450}$	-.100	-.015	.021	.034	.045	.058	.079	.086	.085	.074	.055	.036	.029	.009	-.049
	$b_{.550}$	-.054	.011	.034	.041	.052	.063	.083	.086	.086	.078	.063	.044	.043	.028	-.014
	$b_{.650}$	-.032	.013	.029	.034	.040	.046	.058	.059	.061	.055	.046	.032	.034	.023	-.003
	$b_{.750}$.001	.033	.042	.041	.046	.049	.058	.058	.060	.056	.051	.040	.046	.040	.021
	$b_{.850}$.048	.063	.068	.067	.060	.060	.063	.060	.068	.067	.068	.059	.067	.049	.040
	$b_{.925}$.084	.098	.095	.088	.083	.078	.080	.070	.078	.081	.083	.081	.095	.098	.094
	$b_{.975}$.142	.152	.175	.162	.158	.162	.172	.138	.142	.140	.152	.181	.160	.183	.172
$b_{1.000}$.188	.205	.250	.258	.250	.282	.284	.220	.222	.205	.230	.300	.220	.270	.260	

^aNo orifice.

^bPaired value.



TABLE 10.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS

OF THE BLADE SECTION ($x = 0.975$; $\beta_x = 37.90^\circ$; $\beta_{0.75R} = 45^\circ$; $B = 2$) - Continued(a) $N = 1500$ rpm.

	2.067	2.145	2.254	2.378	2.475	2.561	2.551	2.434	2.336	2.235	2.119	2.040	
$\frac{r}{R}$.844	.892	.865	.884	.899	.917	.910	.890	.874	.860	.842	.833	
α_x	3.89	2.90	1.55	.08	-1.04	-2.22	-1.89	-.57	-.57	1.78	3.22	4.23	
$\Delta\beta$.78	.46	.03	-.45	-.89	-1.45	-1.29	-.70	-.28	.11	.57	.88	
α_1	3.73	3.03	2.35	1.55	.89	.16	.34	1.15	1.85	2.30	3.26	3.91	
α_n	.4381	.3552	.2748	.1797	.1045	.0187	.0400	.1342	.2168	.2700	.3226	.4977	
α_m	-.0915	-.0896	-.0885	-.0901	-.1008	-.1137	-.1055	-.0960	-.0864	-.0882	-.0882	-.0909	
α_g	-.0019	.0028	.0096	.0157	.0199	.0248	.0216	.0180	.0137	.0090	.0021	-.0045	
c/b	Pressure coefficient, P												
Upper surface	^a 0.000	1.191	1.195	1.201	1.210	1.219	1.228	1.224	1.214	1.206	1.199	1.190	1.185
	.025	-.189	.046	.274	.412	.567	.665	.642	.528	.398	.225	-.047	-.272
	.050	-.347	-.179	0	.158	.260	.356	.333	.222	.105	-.035	-.246	-.406
	.100	-.473	-.313	-.193	-.076	.002	.065	.063	-.028	-.116	-.217	-.357	-.521
	.200	-.371	-.315	-.259	-.206	-.180	-.151	-.162	-.182	-.222	-.267	-.338	-.388
	.300	-.303	-.263	-.232	-.198	-.179	-.209	-.192	-.183	-.208	-.237	-.276	-.315
	.400	-.329	-.294	-.262	-.236	-.219	-.233	-.208	-.225	-.242	-.266	-.308	-.340
	.500	-.312	-.274	-.244	-.213	-.193	-.169	-.169	-.198	-.220	-.248	-.287	-.321
	.600	-.347	-.309	-.286	-.262	-.252	-.236	-.240	-.254	-.265	-.284	-.321	-.354
	.700	-.377	-.342	-.316	-.293	-.285	-.275	-.274	-.287	-.293	-.314	-.350	-.379
	.800	-.364	-.337	-.324	-.316	-.313	-.293	-.297	-.307	-.296	-.309	-.341	-.368
.900	-.357	-.318	-.285	-.246	-.237	-.333	-.238	-.230	-.254	-.290	-.333	-.366	
.950	-.164	-.135	-.108	-.074	-.047	-.017	-.026	-.099	-.084	-.116	-.150	-.176	
Lower surface	.0375	.198	.079	-.097	-.625	-.801	-.888	-.879	-.771	-.377	-.060	.118	.229
	.075	.144	.065	-.043	-.259	-.746	-.843	-.835	-.697	-.071	-.019	.090	.166
	.150	.121	.074	-.033	.004	-.277	-.700	-.691	.036	-.008	.040	.099	.143
	.250	.092	.072	.041	.016	.054	-.317	-.021	.027	.021	.050	.086	.109
	.350	.085	.077	.044	.024	.035	.053	.065	.023	.030	.050	.077	.099
	.450	.105	.090	.062	.044	.045	.078	.068	.044	.051	.067	.088	.106
	.550	.097	.085	.062	.046	.043	.063	.056	.044	.051	.064	.082	.097
	.650	.071	.062	.046	.033	.030	.041	.043	.031	.037	.049	.059	.072
	.750	.067	.062	.049	.040	.038	.045	.037	.038	.042	.049	.056	.067
	^b .850	.079	.079	.070	.069	.070	.080	.075	.060	.065	.069	.070	.075
	.925	.087	.092	.091	.094	.103	.118	.113	.098	.092	.085	.084	.083
^b .975	.100	.106	.105	.118	.120	.152	.162	.132	.114	.102	.094	.102	
^a 1.000	.104	.114	.114	.138	.125	.170	.200	.157	.125	.110	.099	.115	

^aNo orifice.^bFaired values.

TABLE 10.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS

OF THE BLADE SECTION ($x = 0.975$; $\beta_x = 37.90^\circ$;

$\beta_{0.75R} = 45^\circ$; $B = 2$) - Continued.

(a) $N = 1600$ rpm.

J	2.177	2.278	2.370	2.460	2.553	2.581	2.507	2.423	2.323	2.232	2.119	
$C_{p, \text{max}}$.907	.925	.940	.955	.973	.973	.960	.946	.928	.912	.893	
$\Delta\delta$	2.50	1.26	.17	-.87	-1.93	-2.22	-1.40	-.44	.72	1.82	3.22	
δ	.47	-.10	-.60	-1.07	-1.45	-1.51	-1.30	-.88	-.34	.17	.78	
δ_{min}	2.92	2.21	1.37	.67	-.34	-.79	.20	1.07	1.76	2.53	3.35	
δ_{min}^*	.3419	.2590	.1619	.0781	-.0394	-.0929	.0232	.1292	.2065	.2955	.3923	
δ_c	-.1010	-.0920	-.1069	-.1116	-.1113	-.1049	-.1144	-.1090	-.1009	-.0974	-.1024	
δ_c^*	.0123	.0190	.0241	.0283	.0347	.0373	.0312	.0266	.0220	.0154	.0051	
a/b	Pressure coefficient, P											
Upper surface	^a 0.000	1.223	1.232	1.241	1.249	1.259	1.259	1.252	1.244	1.234	1.225	1.216
	.025	.214	.391	.520	.620	.710	.733	.666	.577	.462	.304	.066
	.050	-.040	.105	.218	.320	.410	.433	.366	.277	.165	.032	-.150
	.100	-.230	-.121	-.027	.063	.143	.166	.101	.023	-.071	-.174	-.333
	.200	-.347	-.289	-.248	-.176	-.098	-.077	-.137	-.209	-.253	-.313	-.384
	.300	-.266	-.213	-.200	-.213	-.174	-.163	-.195	-.233	-.211	-.237	-.301
	.400	-.220	-.233	-.201	-.274	-.237	-.224	-.259	-.228	-.224	-.249	-.328
	.500	-.269	-.244	-.214	-.245	-.248	-.239	-.269	-.203	-.232	-.263	-.312
	.600	-.318	-.303	-.268	-.255	-.302	-.298	-.294	-.252	-.285	-.323	-.358
	.700	-.383	-.340	-.305	-.281	-.336	-.351	-.302	-.292	-.318	-.360	-.416
	.800	-.422	-.384	-.347	-.316	-.334	-.362	-.316	-.333	-.365	-.404	-.445
.900	-.448	-.471	-.504	-.485	-.472	-.485	-.477	-.504	-.494	-.437	-.337	
.950	-.073	-.069	-.080	-.097	-.110	-.124	-.088	-.093	-.068	-.069	-.100	
Lower surface	.0375	.009	-.319	-.560	-.679	-.754	-.780	-.739	-.661	-.525	-.088	.110
	.075	.022	-.644	-.503	-.644	-.724	-.749	-.706	-.624	-.449	-.033	.087
	.150	.070	.022	-.221	-.506	-.610	-.642	-.587	-.481	.057	.037	.103
	.250	.065	.033	.078	-.365	-.451	-.474	-.423	-.303	.033	.044	.084
	.350	.063	.038	.056	.018	-.369	-.399	-.297	.075	.031	.048	.078
	.450	.076	.037	.038	.088	-.248	-.337	.035	.075	.046	.062	.086
	.550	.073	.052	.049	.074	-.003	-.203	.067	.056	.044	.061	.083
	.650	.051	.033	.026	.043	.040	-.006	.051	.029	.024	.040	.061
	.750	.049	.031	.022	.030	.041	.026	.040	.023	.024	.039	.057
	.850	.060	.046	.037	.043	.058	.051	.051	.040	.041	.054	.066
	.925	.076	.063	.056	.063	.071	.070	.070	.058	.061	.071	.082
.975	.088	.076	.074	.085	.089	.078	.086	.071	.076	.085	.100	
1.000	.095	.082	.082	.098	.094	.080	.091	.080	.084	.092	.108	

^aNo orifices.
^bpaired values.



TABLE 10.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS

OF THE BLADE SECTION ($\alpha = 0.975$; $\beta_x = 37.90^\circ$;

$\beta_{0.75R} = 45^\circ$; $B = 2$) - Continued

(e) $M = 0.56$.

	2.147	2.179	2.218	2.258	2.284	2.314	2.354	2.395	2.434	2.475	2.517	2.560	2.610	2.654	2.697	
J	.988	.978	.968	.960	.950	.942	.932	.922	.913	.904	.895	.886	.879	.870	.859	
α_r'	2.87	2.47	1.99	1.51	1.19	.83	-.36	-.12	-.57	-1.04	-1.51	-1.99	-2.53	-3.01	-3.46	
$\Delta\delta$	0	-.12	-.21	-.28	-.32	-.36	-.46	-.61	-.76	-.92	-1.07	-1.20	-1.36	-1.48	-1.50	
α_1	2.80	2.62	2.30	2.14	1.91	1.82	1.60	1.44	1.18	.93	.54	.15	-.09	-.36	-.53	
α_n	-.3265	-.3077	-.2684	-.2490	-.2239	-.2110	-.1877	-.1677	-.1368	-.1077	-.0626	-.0174	-.0097	-.0413	-.0619	
α_m	-.1255	-.1254	.1170	-.1080	-.1019	-.0998	-.0990	-.1013	-.1006	-.1001	-.1008	-.1024	-.0985	-.0995	-.0926	
α_c	.0295	.0294	.0271	.0249	.0238	.0227	.0203	.0210	.0201	.0193	.0197	.0204	.0214	.0221	.0238	
c/b	Pressure coefficient, P															
Upper surface	.000	1.268	1.262	1.257	1.252	1.246	1.242	1.236	1.231	1.226	1.222	1.217	1.212	1.211	1.203	1.198
	.025	.360	.361	.404	.438	.455	.466	.487	.520	.548	.570	.611	.636	.665	.685	.698
	.050	.094	.105	.121	.147	.160	.168	.186	.216	.240	.260	.297	.322	.351	.370	.382
	.100	-.120	-.109	-.098	-.078	-.071	-.066	-.054	-.031	-.012	.003	.033	.053	.080	.095	.108
	.200	-.287	-.288	-.288	-.285	-.285	-.279	-.260	-.224	-.200	-.186	-.160	-.145	-.124	-.109	-.092
	.300	-.239	-.239	-.239	-.223	-.200	-.199	-.205	-.198	-.186	-.178	-.164	-.157	-.142	-.137	-.136
	.400	-.264	-.260	-.253	-.226	-.222	-.221	-.226	-.226	-.220	-.218	-.208	-.203	-.189	-.181	-.179
	.500	-.255	-.247	-.232	-.221	-.222	-.226	-.229	-.214	-.203	-.194	-.178	-.171	-.156	-.156	-.173
	.600	-.295	-.286	-.286	-.279	-.279	-.286	-.279	-.267	-.256	-.254	-.233	-.216	-.200	-.193	-.193
	.700	-.334	-.333	-.331	-.321	-.319	-.317	-.309	-.303	-.296	-.287	-.261	-.251	-.230	-.219	-.216
	.800	-.385	-.383	-.380	-.368	-.362	-.363	-.357	-.350	-.337	-.318	-.283	-.260	-.225	-.209	-.186
.900	-.543	-.542	-.542	-.535	-.532	-.520	-.478	-.398	-.297	-.237	-.215	-.216	-.212	-.214	-.228	
.950	-.632	-.615	-.507	-.309	-.174	-.105	-.065	-.038	-.034	-.041	-.044	-.049	-.050	-.060	-.079	
Lower surface	.0375	-.059	-.156	-.268	-.343	-.422	-.504	-.573	-.652	-.716	-.783	-.878	-.958	-1.028	-1.102	-1.160
	.075	.009	-.024	-.151	-.279	-.376	-.459	-.533	-.614	-.674	-.736	-.827	-.903	-.967	-1.036	-1.069
	.150	.064	.049	.045	.068	.073	.067	.025	-.124	-.203	-.300	-.511	-.673	-.748	-.811	-.823
	.250	.064	.055	.042	.047	.045	.043	.048	.060	.063	.059	.055	.038	.017	-.016	-.108
	.350	.065	.063	.037	.047	.043	.036	.042	.070	.052	.051	.060	.053	.030	.007	-.075
	.450	.073	.066	.055	.062	.053	.045	.044	.047	.049	.046	.048	.042	.039	.027	-.038
	.550	.064	.058	.053	.052	.048	.042	.041	.044	.048	.046	.049	.044	.044	.034	-.008
	.650	.035	.032	.022	.026	.023	.019	.001	.026	.031	.031	.034	.031	.030	.024	-.001
	.750	.021	.021	.012	.018	.016	.014	.001	.029	.037	.041	.046	.043	.045	.039	.023
	.850	.027	.027	.015	.021	.015	.024	.021	.049	.070	.069	.076	.070	.074	.071	.061
	.925	.057	.048	.035	.035	.035	.044	.061	.081	.098	.103	.112	.112	.117	.112	.100
.975	.103	.075	.060	.060	.061	.072	.108	.127	.128	.140	.154	.156	.162	.164	.134	
1.000	.135	.095	.080	.077	.081	.091	.140	.156	.145	.164	.182	.185	.192	.197	.156	

^aNo orifice.
^bPaired value.



TABLE 10.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS
OF THE BLADE SECTION ($x = 0.975$; $\beta_x = 37.90^\circ$)

$\beta_{0.75R} = 45^\circ$; $B = 2$ - Continued

(r) $M = 0.58$.

J	2.148	2.181	2.214	2.251	2.285	2.318	2.354	2.394	2.434	2.473	2.519	2.555	2.593	2.647	2.693	
M_{∞}	1.024	1.014	1.004	.995	.985	.976	.967	.957	.947	.938	.930	.919	.912	.901	.892	
α_{T1}	2.86	2.45	2.04	1.99	1.18	.78	.36	-.11	-.57	-1.02	-1.53	-1.93	-2.35	-2.93	-3.42	
$\Delta\beta$.01	-.20	-.38	-.54	-.65	-.72	-.75	-.79	-.88	-.99	-1.16	-1.31	-1.45	-1.64	-1.78	
α_1	2.55	2.34	2.17	2.00	1.81	1.60	1.35	1.15	1.02	.79	.61	.40	.22	-.21	-.42	
α_n	.2987	.2729	.2542	.2339	.2103	.1871	.1590	.1355	.1200	.0935	.0716	.0465	.0298	-.0245	-.0490	
α_m	-.1218	-.1200	-.1168	-.1191	-.1213	-.1160	-.1122	-.1109	-.1075	-.1095	-.1101	-.1083	-.1055	-.1082	-.1062	
α_c	-.0315	-.0307	-.0290	-.0306	-.0322	-.0299	-.0265	-.0264	-.0263	-.0246	-.0248	-.0242	-.0235	-.0241	-.0243	
o/b	Pressure coefficient, P															
Upper surface	0.000	1.290	1.283	1.277	1.272	1.266	1.261	1.256	1.250	1.244	1.240	1.235	1.230	1.224	1.220	1.215
	.025	.430	.455	.459	.485	.508	.523	.545	.567	.590	.613	.635	.657	.680	.709	.726
	.050	.169	.185	.188	.204	.219	.229	.247	.265	.287	.308	.326	.346	.367	.394	.413
	.100	-.060	-.041	-.042	-.025	-.013	-.007	.006	.019	.033	.048	.060	.076	.094	.117	.133
	.200	-.231	-.231	-.239	-.234	-.234	-.233	-.224	-.216	-.204	-.187	-.175	-.160	-.141	-.120	-.104
	.300	-.208	-.213	-.232	-.240	-.243	-.242	-.241	-.240	-.233	-.226	-.222	-.215	-.194	-.166	-.180
	.400	-.231	-.226	-.233	-.222	-.233	-.235	-.247	-.258	-.257	-.250	-.252	-.252	-.212	-.205	-.194
	.500	-.220	-.211	-.209	-.198	-.204	-.202	-.203	-.209	-.204	-.187	-.180	-.173	-.164	-.174	-.185
	.600	-.258	-.247	-.252	-.249	-.252	-.253	-.255	-.256	-.247	-.238	-.236	-.237	-.230	-.213	-.212
	.700	-.293	-.290	-.296	-.292	-.294	-.295	-.292	-.287	-.281	-.277	-.281	-.277	-.259	-.252	-.243
	.800	-.342	-.338	-.340	-.335	-.334	-.332	-.331	-.330	-.325	-.319	-.317	-.299	-.279	-.264	-.245
.900	-.447	-.446	-.440	-.449	-.441	-.443	-.445	-.444	-.444	-.444	-.402	-.385	-.247	-.220	-.222	
.950	-.572	-.572	-.576	-.576	-.554	-.402	-.248	-.153	-.084	-.030	-.016	-.015	-.028	-.038	-.056	
Lower surface	.0375	-.125	-.196	-.250	-.321	-.400	-.457	-.527	-.593	-.657	-.728	-.795	-.859	-.938	-1.006	-1.075
	.075	-.073	-.187	-.249	-.314	-.389	-.436	-.503	-.565	-.625	-.691	-.757	-.816	-.889	-.954	-1.018
	.150	.100	.115	.056	-.094	-.231	-.296	-.368	-.429	-.488	-.556	-.623	-.679	-.746	-.807	-.870
	.250	.082	.085	.080	.092	.085	.081	.089	-.069	-.137	-.198	-.269	-.295	-.276	-.365	-.360
	.350	.071	.066	.057	.065	.073	.076	.081	.078	.077	.074	.061	.054	.043	.019	-.017
	.450	.092	.084	.071	.070	.072	.072	.077	.078	.082	.084	.080	.077	.066	.054	.026
	.550	.080	.072	.060	.058	.055	.055	.057	.058	.063	.067	.064	.065	.058	.053	.036
	.650	.050	.042	.032	.029	.023	.024	.025	.026	.033	.040	.038	.040	.039	.037	.027
	.750	.031	.026	.018	.015	.011	.012	.014	.017	.025	.036	.038	.044	.046	.047	.038
	b .850	.057	.048	.036	.028	.023	.020	.021	.030	.047	.064	.070	.076	.079	.081	.083
	b .925	.096	.083	.067	.056	.044	.038	.036	.039	.061	.089	.101	.113	.119	.123	.118
b .975	.137	.117	.098	.087	.067	.056	.073	.067	.087	.149	.138	.140	.160	.171	.122	
b ¹ 1.000	.159	.136	.115	.105	.080	.067	.112	.085	.110	.208	.165	.168	.205	.215	.300	

^aNo orifice.
^bPaired value.



TABLE 10.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS

OF THE BLADE SECTION ($x = 0.975$; $\beta_x = 37.90^\circ$; $\beta_{0.75R} = .45^\circ$; $B = 2$) - Continued(g) $M = 0.60$.

	2.143	2.172	2.205	2.243	2.275	2.308	2.330	2.375	2.411	2.447	2.477	2.525	2.555	2.600	2.642	
J	1.059	1.050	1.039	1.034	1.025	1.015	1.004	.997	.988	.979	.967	.960	.949	.939	.931	
M	2.92	2.56	2.15	1.68	1.30	.90	.64	.11	-.31	-.72	-1.06	-1.60	-1.93	-2.43	-2.88	
$\Delta \delta$	-.48	-.49	-.52	-.60	-.70	-.83	-.92	-1.11	-1.23	-1.32	-1.38	-1.45	-1.50	-1.57	-1.64	
$\Delta \delta_{1/2}$	2.20	2.07	1.79	1.60	1.44	1.23	1.03	.93	.64	.45	.31	.10	-.04	-.36	-.60	
$C_{L_{max}}$.2552	.2416	.2084	.1868	.1687	.1445	.1200	.1094	.0752	.0523	.0358	.0123	-.0045	-.0413	-.0703	
C_D	-.1220	-.1206	-.1173	-.1186	-.1214	-.1209	-.1236	-.1236	-.1204	-.1183	-.1171	-.1191	-.1209	-.1183	-.1200	
$C_{D_{min}}$.0293	.0310	.0305	.0315	.0330	.0324	.0338	.0345	.0335	.0311	.0309	.0306	.0302	.0296	.0293	
c/b	Pressure coefficient, P															
Upper surface	$a_{0.000}$	1.312	1.307	1.299	1.296	1.290	1.284	1.277	1.273	1.267	1.262	1.256	1.251	1.245	1.240	1.235
	$b_{.025}$.485	.494	.522	.541	.552	.569	.581	.600	.623	.646	.655	.678	.691	.713	.750
	$b_{.050}$.215	.217	.241	.255	.266	.279	.288	.305	.326	.345	.353	.374	.386	.405	.423
	$b_{.100}$	-.003	0	.020	.031	.038	.047	.052	.063	.076	.091	.094	.110	.118	.133	.147
	$b_{.200}$	-.193	-.197	-.191	-.188	-.187	-.186	-.184	-.175	-.163	-.150	-.147	-.133	-.127	-.111	-.096
	$b_{.300}$	-.208	-.216	-.216	-.215	-.209	-.206	-.207	-.203	-.199	-.197	-.202	-.196	-.198	-.194	-.189
	$b_{.400}$	-.227	-.236	-.247	-.246	-.245	-.253	-.259	-.257	-.255	-.250	-.258	-.258	-.260	-.253	-.245
	$b_{.500}$	-.206	-.207	-.202	-.203	-.209	-.226	-.240	-.248	-.257	-.263	-.272	-.267	-.272	-.274	-.278
	$b_{.600}$	-.237	-.235	-.229	-.230	-.232	-.240	-.251	-.261	-.273	-.280	-.289	-.295	-.293	-.289	-.275
	$b_{.700}$	-.262	-.265	-.260	-.259	-.260	-.265	-.271	-.272	-.272	-.278	-.279	-.278	-.278	-.266	-.252
	$b_{.800}$	-.315	-.314	-.307	-.304	-.304	-.306	-.306	-.308	-.307	-.305	-.311	-.307	-.303	-.286	-.262
$b_{.900}$	-.463	-.467	-.459	-.458	-.461	-.465	-.469	-.472	-.471	-.472	-.478	-.471	-.462	-.432	-.380	
$b_{.950}$	-.537	-.541	-.533	-.535	-.538	-.544	-.548	-.528	-.364	-.215	-.116	-.048	-.013	.005	-.004	
Lower surface	$b_{.0375}$	-.143	-.181	-.243	-.292	-.345	-.395	-.456	-.510	-.574	-.626	-.692	-.752	-.816	-.884	-.948
	$b_{.075}$	-.140	-.178	-.245	-.295	-.347	-.397	-.455	-.504	-.561	-.606	-.665	-.719	-.778	-.840	-.899
	$b_{.150}$	-.028	-.081	-.149	-.189	-.227	-.274	-.330	-.378	-.434	-.482	-.546	-.601	-.658	-.715	-.768
	$b_{.250}$.112	.109	.014	-.060	-.102	-.178	-.229	-.267	-.314	-.348	-.394	-.435	-.479	-.523	-.567
	$b_{.350}$.117	.107	.090	.046	.029	-.013	-.053	-.098	-.191	-.147	-.154	-.202	-.220	-.282	-.289
	$b_{.450}$.095	.093	.098	.104	.105	.105	.098	.092	.079	.066	.049	.026	.023	.011	.002
	$b_{.550}$.076	.073	.076	.081	.081	.083	.082	.081	.082	.083	.074	.071	.066	.061	.053
	$b_{.650}$.040	.037	.039	.042	.044	.045	.046	.048	.052	.057	.051	.055	.053	.054	.051
	$b_{.750}$.022	.017	.018	.020	.021	.023	.027	.029	.036	.043	.041	.050	.051	.058	.058
	$b_{.850}$.053	.051	.043	.041	.040	.028	.023	.032	.038	.048	.050	.078	.080	.080	.093
	$b_{.925}$.113	.103	.093	.084	.072	.064	.054	.049	.047	.054	.060	.089	.103	.122	.130
$b_{.975}$.169	.143	.134	.120	.100	.101	.084	.060	.056	.077	.106	.143	.160	.180	.179	
$b_{1.000}$.204	.167	.157	.140	.113	.123	.103	.069	.060	.112	.150	.212	.208	.220	.210	

^aNo orifice.^bPaired values.

TABLE 10.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS

OF THE BLADE SECTION ($\alpha = 0.975$; $\beta_x = 37.90^\circ$; $\beta_{0.75R} = 45^\circ$; $B = 2$) - Concluded(h) $M = 0.65$.

	2.110	2.136	2.150	2.164	2.199	2.222	2.235	2.273	2.293	2.324	2.354	2.383	2.413	2.450	2.483	2.520	
J	2.110	2.136	2.150	2.164	2.199	2.222	2.235	2.273	2.293	2.324	2.354	2.383	2.413	2.450	2.483	2.520	
M_x	1.162	1.152	1.144	1.135	1.127	1.121	1.113	1.101	1.090	1.080	1.072	1.060	1.052	1.042	1.034	1.025	
α_x	3.34	3.01	2.83	2.66	2.22	1.94	1.78	1.32	1.08	.71	.36	.02	-.33	-.76	-1.13	-1.54	
$\Delta\beta_x$	-.950	-1.038	-1.080	-1.130	-1.235	-1.300	-1.338	-1.432	-1.480	-1.550	-1.618	-1.670	-1.718	-1.765	-1.810	-1.840	
α_i	1.90	1.68	1.57	1.43	1.27	1.18	1.06	.82	.63	.47	.27	.02	-.28	-.36	-.59	-.87	
c_n	.2187	.1935	.1813	.1639	.1477	.1368	.1226	.0961	.0742	.0548	.0316	.0026	-.0323	-.0426	-.0697	-.1019	
c_m	-.1036	-.1070	-.1044	-.1047	-.1055	-.1047	-.1027	-.1029	-.1014	-.1000	-.0998	-.0909	-.0900	-.0891	-.0857	-.0865	
c_c	.0309	.0317	.0324	.0332	.0334	.0338	.0345	.0355	.0360	.0375	.0382	.0395	.0400	.0410	.0421	.0430	
c/b	Pressure coefficient, P																
Upper surface	$a_0.000$	1.383	1.375	1.370	1.363	1.357	1.353	1.348	1.340	1.333	1.326	1.321	1.313	1.307	1.301	1.297	1.290
	.025	.582	.611	.607	.609	.616	.623	.637	.655	.660	.678	.684	.695	.703	.712	.728	.741
	.050	.322	.344	.336	.336	.341	.346	.356	.372	.377	.392	.397	.405	.414	.419	.436	.446
	.100	.098	.126	.121	.118	.124	.128	.133	.146	.149	.160	.162	.168	.170	.172	.184	.191
	.200	-.077	-.066	-.076	-.084	-.084	-.086	-.085	-.080	-.081	-.075	-.074	-.072	-.070	-.069	-.056	-.050
	.300	-.109	-.100	-.113	-.124	-.128	-.134	-.135	-.134	-.134	-.127	-.129	-.134	-.139	-.143	-.140	-.131
	.400	-.144	-.142	-.157	-.172	-.175	-.181	-.184	-.173	-.175	-.170	-.176	-.181	-.183	-.185	-.181	-.186
	.500	-.144	-.138	-.155	-.169	-.173	-.178	-.178	-.179	-.186	-.187	-.195	-.208	-.216	-.223	-.222	-.215
	.600	-.166	-.160	-.177	-.188	-.193	-.203	-.210	-.210	-.215	-.217	-.228	-.239	-.248	-.255	-.257	-.257
	.700	-.184	-.179	-.199	-.216	-.223	-.234	-.242	-.243	-.249	-.255	-.265	-.276	-.284	-.290	-.288	-.292
	.800	-.224	-.216	-.236	-.252	-.258	-.270	-.275	-.274	-.278	-.282	-.293	-.303	-.308	-.314	-.314	-.323
	.900	-.354	-.347	-.364	-.376	-.383	-.393	-.401	-.404	-.410	-.418	-.432	-.446	-.455	-.463	-.465	-.475
.950	-.420	-.416	-.431	-.445	-.450	-.460	-.468	-.473	-.480	-.489	-.504	-.520	-.532	-.540	-.546	-.555	
Lower surface	$a_0.0375$	-.004	-.052	-.083	-.117	-.150	-.184	-.211	-.249	-.291	-.339	-.386	-.429	-.480	-.522	-.573	-.624
	.075	-.002	-.045	-.078	-.111	-.141	-.178	-.215	-.259	-.302	-.351	-.397	-.442	-.489	-.528	-.573	-.615
	.150	.040	.004	-.027	-.061	-.087	-.121	-.152	-.186	-.225	-.264	-.304	-.344	-.387	-.424	-.467	-.511
	.250	.051	.024	-.004	-.034	-.053	-.081	-.103	-.127	-.153	-.180	-.211	-.247	-.279	-.309	-.340	-.374
	$b_0.350$.109	.084	.031	-.017	-.022	-.043	-.066	-.085	-.103	-.120	-.150	-.200	-.232	-.240	-.290	-.314
	.450	.162	.133	.083	.037	.013	-.012	-.033	-.053	-.075	-.096	-.124	-.155	-.184	-.208	-.234	-.261
	.550	.147	.155	.125	.074	.041	.004	-.020	-.038	-.056	-.075	-.103	-.135	-.162	-.187	-.213	-.240
	.650	.103	.115	.096	.079	.059	.024	-.016	-.047	-.075	-.096	-.127	-.166	-.192	-.214	-.236	-.262
	.750	.083	.091	.072	.063	.059	.050	.040	.021	.009	-.009	-.037	-.119	-.146	-.156	-.175	-.178
	$b_0.850$.107	.116	.094	.069	.082	.090	.091	.086	.072	.059	.044	-.010	-.029	-.038	-.050	-.049
	.925	.139	.151	.129	.120	.122	.124	.130	.138	.133	.123	.110	.091	.082	.075	.070	.062
	$b_0.975$.167	.188	.148	.160	.154	.152	.161	.180	.175	.180	.179	.171	.171	.157	.161	.151
$a_1.000$.180	.207	.158	.180	.170	.166	.176	.201	.195	.218	.231	.215	.218	.200	.210	.197	

^aNo orifice.^bFaired value.

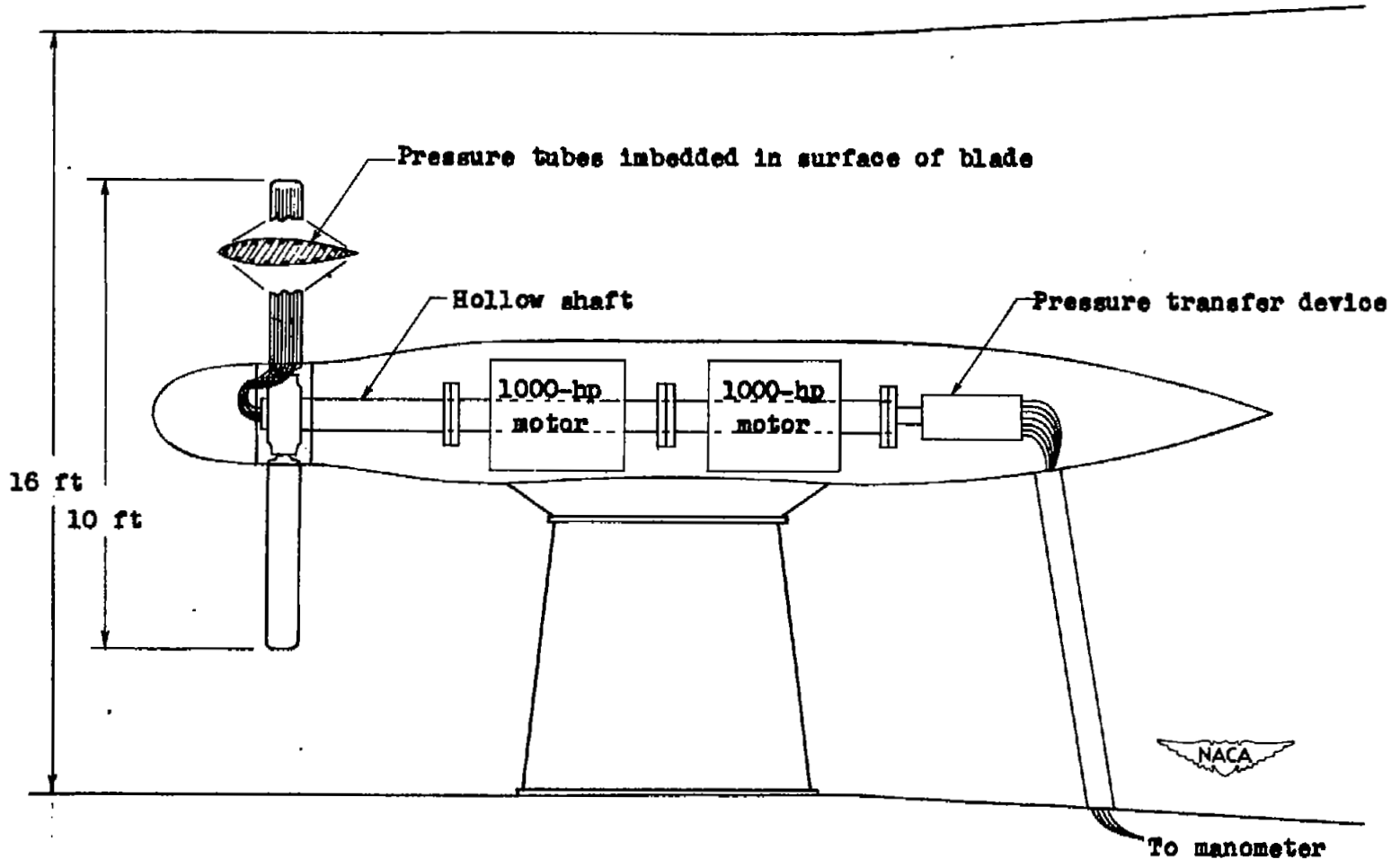


Figure 1.- Diagram of the apparatus used to obtain pressure distributions on the sections of operating propellers.

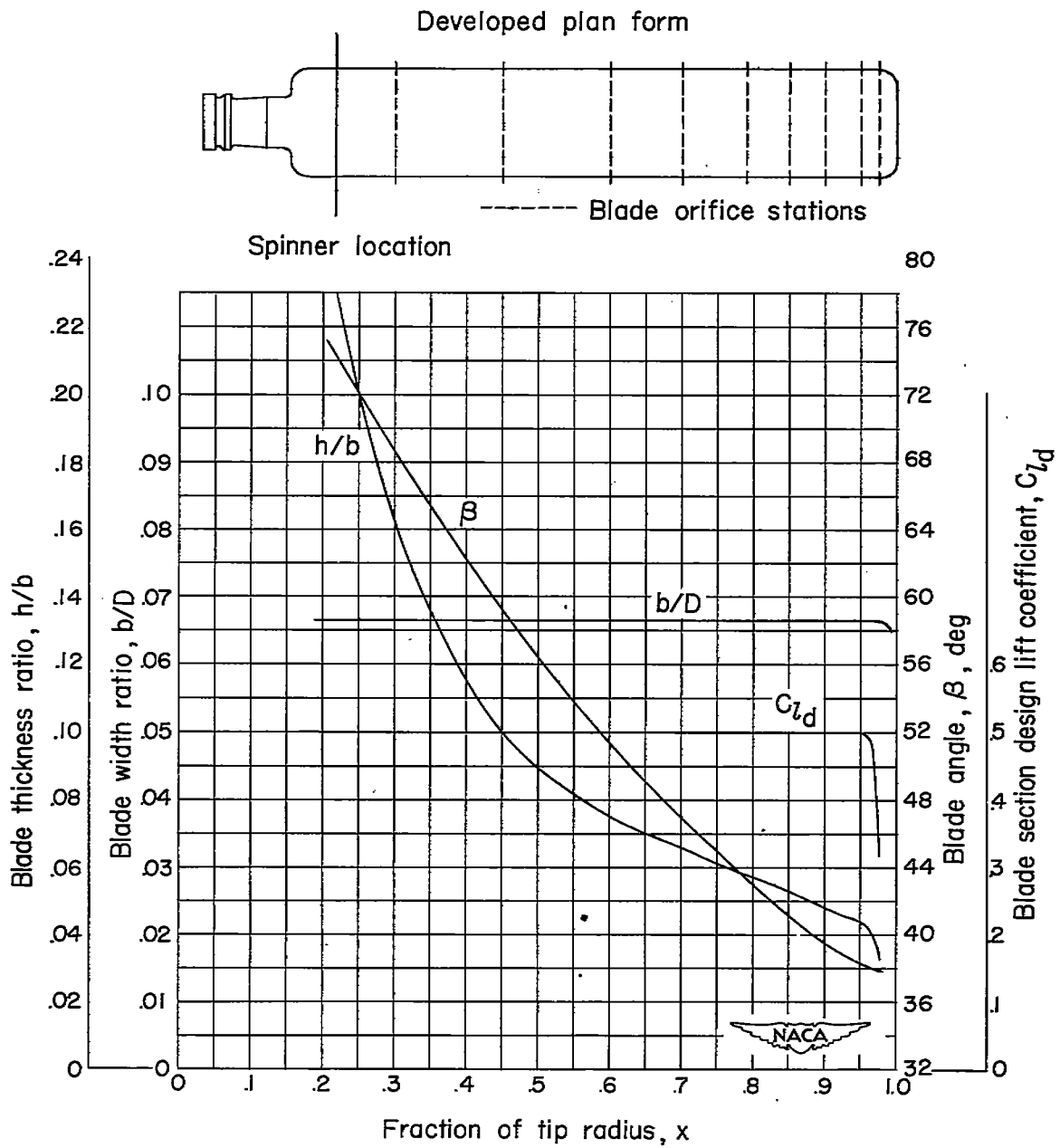


Figure 2.- Blade-form curves for NACA 10-(5)(066)-03.

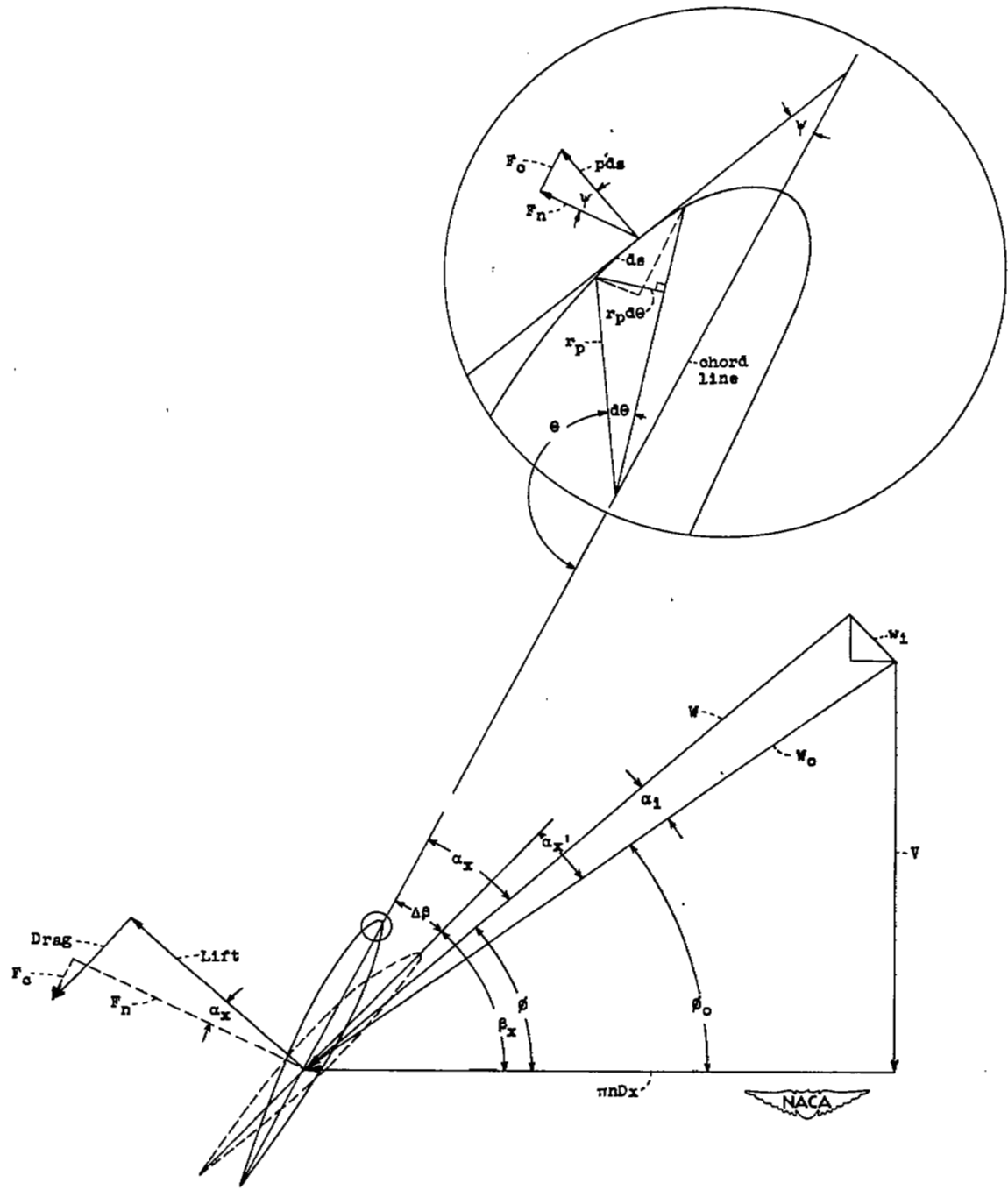


Figure 3.- Vector diagram of the velocities and forces acting on a blade section.

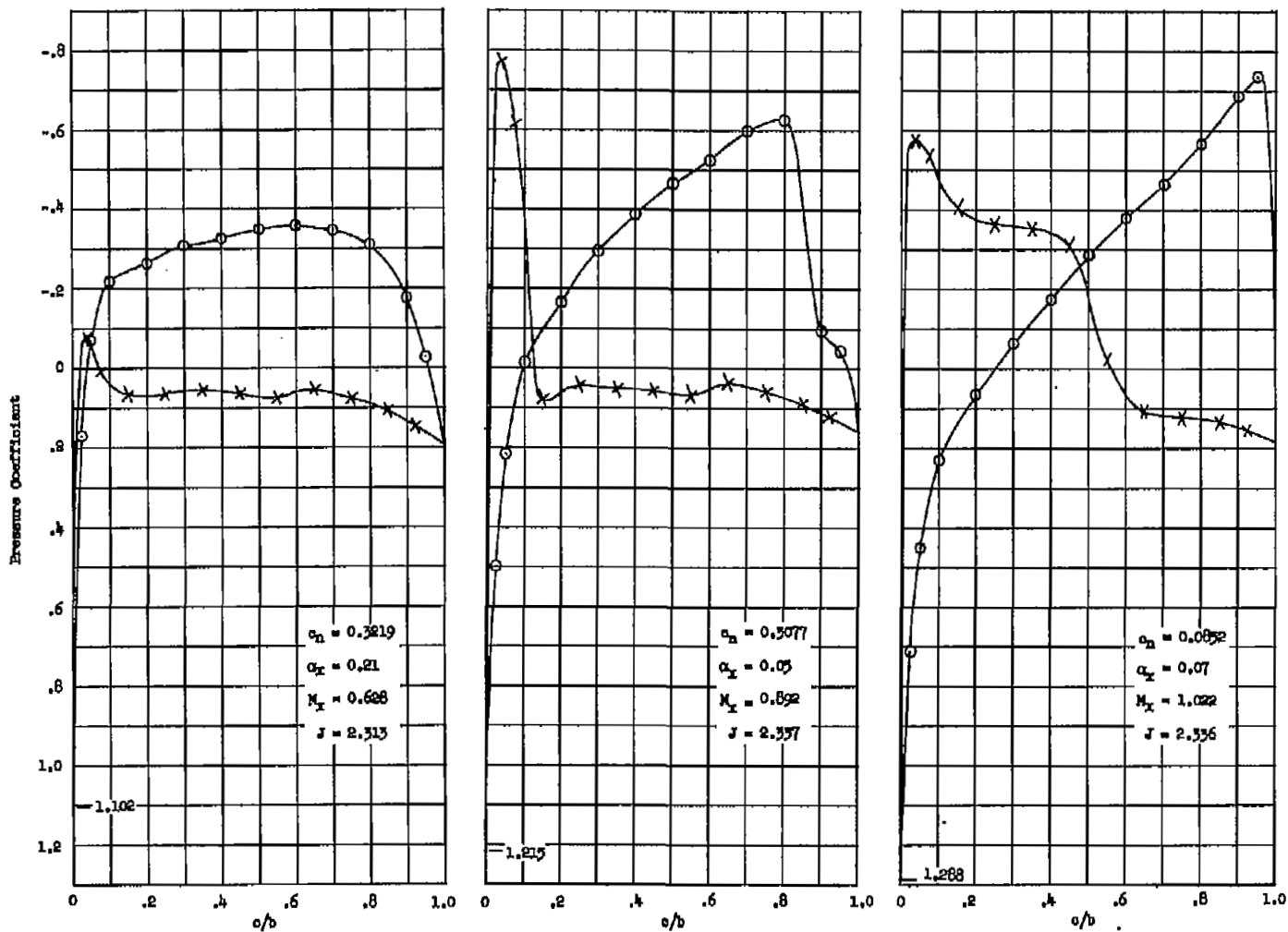


Figure 4.- Typical pressure distributions along the chord of the NACA 16-504.80 blade section located at the $x = 0.90$ radius.

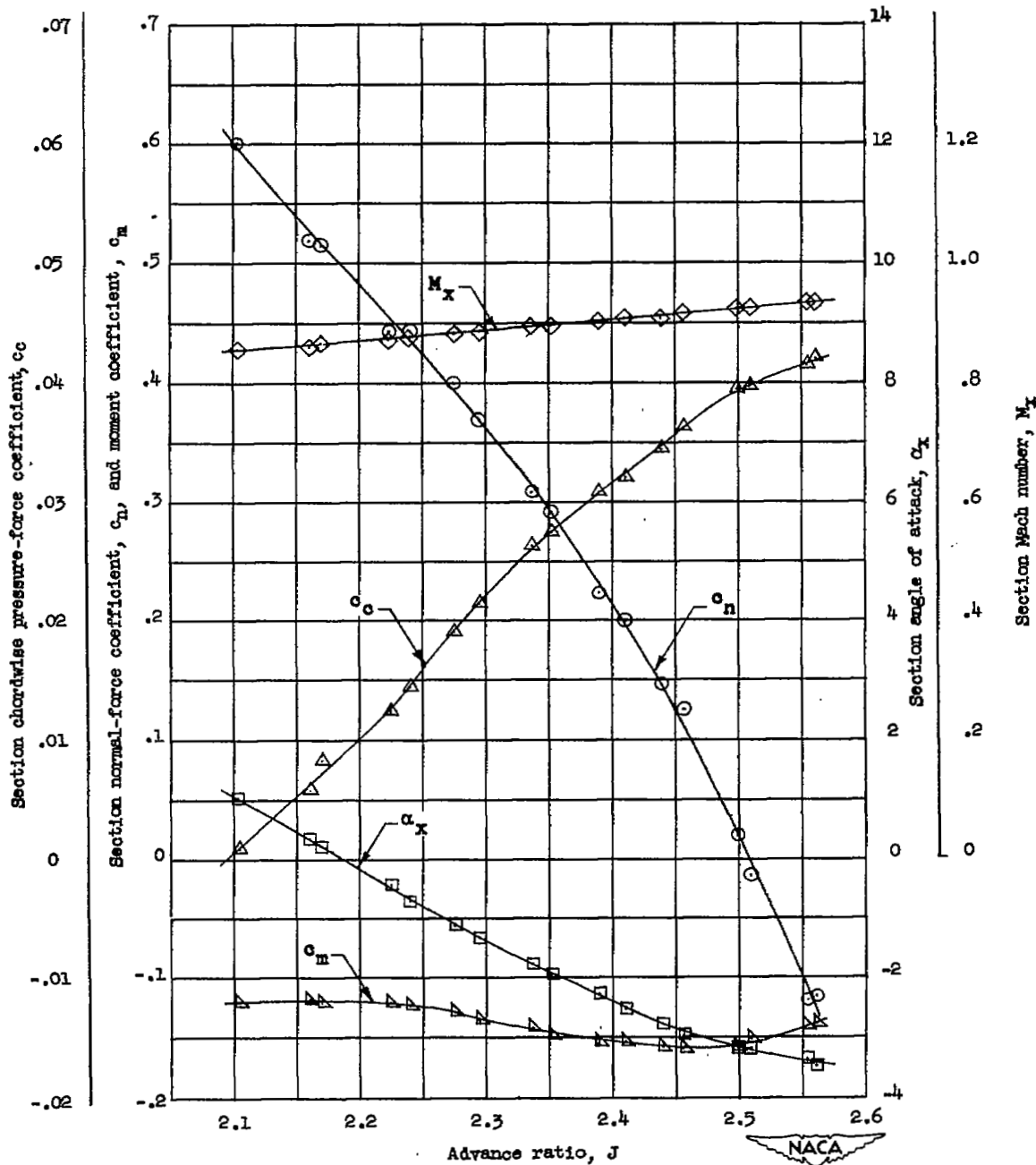


Figure 5.- Variation of section normal-force coefficient, moment coefficient, chordwise pressure-force coefficient, angle of attack, and Mach number with advance ratio for the blade section at the 0.90 radius, from table 8(d). $\beta_{0.75R} = 45^\circ$; 1600 rpm.

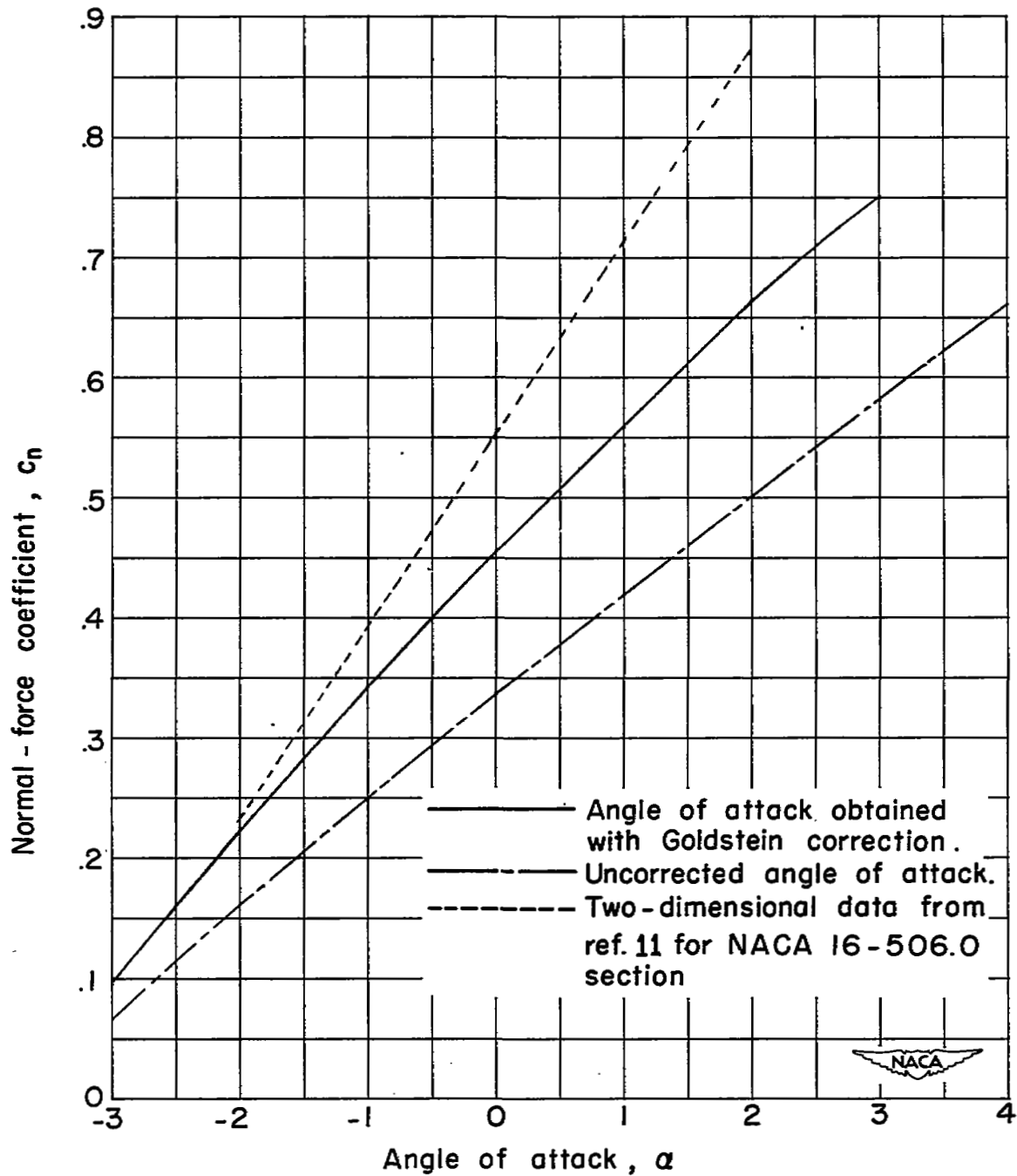


Figure 6.- Variation of normal-force coefficient with angle of attack for NACA 16-505.85 section showing effect of induced angle correction. $x = 0.78$; $M_x = 0.70$.

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