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RESEARCH MEMORANDUM

THE FORCES AND PRESSURE DISTRIBUTION AT SUBSONIC SPEEDS ON A PLANE WING HAVING 45° OF SWEEPBACK, AN ASPECT RATIO OF 3, AND A TAPER RATIO OF 0.5

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NATIONAL ADVISORY COMMITTEE
FOR AERONAUTICS

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SUMMARY

An investigation was conducted to determine the effects of scale and compressibility on the forces, moments, and pressure distribution on a wing having an aspect ratio of 3 and a taper ratio of 0.5. The line joining the quarter-chord points of the airfoil sections was swept back 45° and the airfoil sections perpendicular to this line were the NACA 64A010.

Lift, drag, and pitching-moment data and the chordwise distribution of static pressure at seven spanwise stations are presented for Reynolds numbers up to 18,000,000 at a constant Mach number of 0.25; for Mach numbers ranging from 0.08 to 0.96 at a constant Reynolds number of 4,000,000; and for Mach numbers of 0.08, 0.25, and 0.60 at a constant Reynolds number of 8,000,000.

It was indicated from the force and moment data that, for all Mach numbers and Reynolds numbers in the test range, no apparant flow separation existed near the leading edge of the wing for lift coefficients less than 0.3. At higher lift coefficients, the initiation of flow separation and reattachment near the leading edge of the outer sections of the wing was generally accompanied by an increase in the lift-curve slope, a rearward movement of the aerodynamic center, and an increase in the rate of drag rise.

The effect of increasing the Reynolds number was to delay to higher lift coefficients the onset of leading-edge flow separation and the concomitant effects on the lift, drag, and pitching moment.

Increasing the Mach number to approximately that for drag divergence at a Reynolds number of 4,000,000 resulted in a rearward movement of

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the wing aerodynamic center of about 6 percent at the mean aerodynamic chord at zero lift.

The effects of compressibility on the force and moment characteristics up to a Mach number of 0.60 were influenced by an increase in Reynolds number from 4,000,000 to 8,000,000. At the lower Reynolds number, the angle-of-attack range for which the lift and pitching-moment curves were nearly linear was reduced by the increase in Mach number, whereas this angle-of-attack range was increased at the higher Reynolds number.

An investigation of several types of juncture arrangements between the model and the turntable indicated that varying the type of seal caused but little change in the forces, moments, and pressure distribution on the model.

INTRODUCTION

Wings having moderately high degrees of sweepback offer the possibility of flight at transonic speeds without serious compressibility effects. Studies of the pressure distributions on such wings have shown that simple sweep theory does not offer an adequate method of predicting the chordwise distribution of pressure near the roots or the tips of the wings. For swept-back wings of low aspect ratio, a substantial part of the wing surface is subjected to flow characteristics which result from the so-called root and tip effects. Experimental determination of the pressure distribution on such wings will provide not only detailed information concerning the aerodynamic characteristics, but also will furnish data for evaluating and extending the theoretical methods for computing surface pressures.

An investigation has been conducted in the Ames 12-foot pressure wind tunnel throughout a wide range of Reynolds numbers and subsonic Mach numbers to obtain experimentally the pressure distribution and the total lift, drag, and pitching moment on a wing having 45° of sweepback and an aspect ratio of 3. To determine the effects of both Mach number and Reynolds number, the wing was tested at constant Reynolds numbers over a range of Mach numbers and at a constant Mach number over a range of Reynolds numbers. The force data and a representative portion of the pressure data are presented in graphic form along with a limited analysis of the data. The complete pressure data for the wing are presented in tabular form.

NOTATION

a_o speed of sound in free stream, feet per second

$\frac{b}{2}$ semispan, measured perpendicular to plane of symmetry, feet

C_D drag coefficient $\left(\frac{\text{drag}}{q_o S}\right)$

C_{D_t} tare drag coefficient $\left(\frac{\text{tare drag}}{q_o S}\right)$

C_L lift coefficient $\left(\frac{\text{lift}}{q_o S}\right)$

C_m pitching-moment coefficient about the quarter point of the wing mean aerodynamic chord $\left(\frac{\text{pitching moment}}{q_o S \bar{c}}\right)$

C_N normal-force coefficient $\left(\frac{1}{S}\int_o^{b/2} c_n c \, dy\right)$

c local wing chord parallel to plane of symmetry, feet

c_{av} average wing chord parallel to plane of symmetry, feet

c_n section normal-force coefficient $\left(\frac{\text{section normal force}}{q_o c}\right)$

$\bar{c}$ mean aerodynamic wing chord $\left(\frac{\int_o^{b/2} c^2 dy}{\int_o^{b/2} c \, dy}\right)$, feet (using theoretical tip chord)

$\frac{L}{D}$ ratio of lift to drag

$\left(\frac{L}{D}\right)_{max}$ maximum lift-to-drag ratio

M_D drag-divergence Mach number (free-stream Mach number at which $\left(\frac{\partial C_D}{\partial M_o}\right)_{C_L} = 0.10$)

M_o free-stream Mach number $\left(\frac{V_o}{a_o}\right)$

P local pressure coefficient $\left(\frac{p - p_o}{q_o}\right)$

p local static pressure, pounds per square foot

p_o free-stream static pressure, pounds per square foot

q_o free-stream dynamic pressure $\left(\frac{1}{2}\rho_o V_o^2\right)$, pounds per square foot

R Reynolds number $\left(\frac{\rho_o V_o \bar{c}}{\mu_o}\right)$

S semispan wing area, square feet (using theoretical tip chord)

V_o free-stream velocity, feet per second

y lateral distance perpendicular to the plane of symmetry, feet

α angle of attack, degrees

α_u angle of attack uncorrected for tunnel-wall interference and angle-of-attack counter correction, degrees

η fraction of semispan $\left(\frac{y}{b/2}\right)$

μ_o coefficient of viscosity of air, slugs per foot-second

ρ_o free-stream mass density of air, slugs per cubic foot

MODEL AND APPARATUS

The model wing used in this investigation had the leading edge swept back 48.54°, an aspect ratio of 3.0, and a taper ratio of 0.5. The wing had no twist and the sections were the NACA 64A010 in planes inclined 45° to the plane of symmetry. The locus of the quarter-chord points of these sections was swept back 45°. This line was at 29.63 percent of the chord parallel to the plane of symmetry. The tip of the wing was formed by a half body having a radius equal to the corresponding half thickness of the tip section. Coordinates of the NACA 64A010 section and of the sections parallel to the plane of symmetry are presented in tables I and II, respectively.

The model, which had a semispan of 46.67 inches, was constructed of a tin-bismuth alloy bonded to a laminated steel spar. Pressure orifices were installed in seven rows in planes parallel to the plane of symmetry. The orifices were distributed along the chord on both the upper and lower surfaces from the leading edge to the 91-percent-chord point and were staggered 1/4 inch on either side of the station planes. A sketch of the plan form of the wing showing the locations of the seven orifice rows and the manner in which the orifices were staggered is given in figure 1. The locations of the orifices along the chord at each station are given with the tabulated pressure-coefficient data (tables III through XXII).

Figure 2 shows the model mounted in the wind-tunnel test section. The test-section floor served as a reflection plane. The forces and moments were transmitted directly to the balance system through the turntable upon which the model was mounted. Pressures were measured by means of multiple-tube manometers and were recorded photographically.

Twenty-six flush orifices were installed in the wind-tunnel test section for the purpose of investigating the onset and the extent of supersonic flow along the tunnel wall opposite the upper surface of the model. The location of these orifices with respect to the model is illustrated in figure 3.

Cross-sectional views of the juncture arrangements between the model and the turntable that were used in the investigation of various seals are shown in figure 4. It is to be noted that the configurations shown in figure 4 extended completely around the root section of the model.

TESTS

The chordwise distributions of pressure at seven spanwise stations on the wing were measured simultaneously with the total lift, drag, and

pitching moment at Reynolds numbers of 4,000,000, 6,000,000, 8,000,000, 12,000,000, and 18,000,000 for a Mach number of 0.25. Similar measurements were made at a Reynolds number of 4,000,000 for Mach numbers ranging from 0.08 to 0.96 and at a Reynolds number of 8,000,000 for Mach numbers of 0.08 and 0.60. The angle of attack was varied from -2° to 30° during the low-speed tests, but this range was reduced at the higher Mach numbers where wind-tunnel power limitations prevented testing at the higher angles of attack. At Reynolds numbers of 12,000,000 and 18,000,000, the capacity of the wind-tunnel balance system limited the force measurements to angles of attack of 28° and 16°, respectively.

Surface pressures on the tunnel wall were measured in the vicinity of the model to ascertain the test conditions at which the data may have been affected by wind-tunnel choking.

As an adjunct to the basic tests, an investigation was made to determine the effect of various seals at the model-turntable juncture on the measured forces, moments, and pressures on the model. For each of the six arrangements shown in figure 4, measurements of the lift, drag, pitching moment, and static pressures on the wing were obtained for Mach numbers of 0.25 and 0.80 at a constant Reynolds number of 4,000,000. The seal arrangement denoted as "original" was used throughout the general investigation of the wing aerodynamic characteristics.

CORRECTIONS TO DATA

Corrections to the data for tunnel-wall interference resulting from lift on the model were evaluated by the method of reference 1 using the theoretical span loading derived from the charts of reference 2. The following increments were added to the angle of attack and drag coefficient:

$$\Delta\alpha = 0.769\ C_L, \text{ degrees}$$

$$\Delta C_D = 0.0109\ C_L^2$$

No corrections were applied to the pitching-moment data.

The pressure data and the coefficients derived therefrom are presented in this report for values of uncorrected angle of attack α_u. The relation between the corrected and uncorrected angles of attack is as follows:

$$\alpha = 0.99\ \alpha_u + \Delta\alpha$$

Corrections for the effects of constriction were evaluated by the method of reference 3. This method, while not accounting for sweepback and being strictly applicable only to full-span models centrally located in the tunnel, has been used as the best available estimate of the constriction effects. The magnitude of the corrections applied to the free-stream Mach number and to the dynamic pressure is illustrated in the following table:

Corrected Mach number	Uncorrected Mach number	$\frac{\text{Corrected } q_o}{\text{Uncorrected } q_o}$
0.08	0.080	1.001
.25	.250	1.003
.60	.599	1.004
.80	.795	1.008
.90	.888	1.014
.92	.905	1.018
.94	.920	1.022
.96	.934	1.054

The following corrections were subtracted from the drag coefficients to compensate for the forces on the exposed surface of the turntable:

$R \times 10^{-6}$	M_o	C_{D_t}
4.0	0.08	0.0027
↓	.25	.0028
↓	.60	.0030
↓	.80	.0033
↓	.90	.0036
↓	.92	.0037
↓	.94	.0038
↓	.96	.0040
6.0	.25	.0026
8.0	.08	.0023
↓	.25	.0024
↓	.60	.0025
12.0	.25	.0023
18.0	.25	.0022

No attempt was made to evaluate the tares due to possible interference between the model and the turntable or to compensate for the tunnel-floor boundary layer which, at the model, had a displacement thickness of 1/2 inch. The magnitude of these effects is believed to be small.

Through consideration of the results of the static loading tests on a model of moderate aspect ratio presented in reference 4 and the greater

structural rigidity of the subject model, it was assumed that the effects of aeroelasticity on the aerodynamic characteristics of the model were negligible.

RESULTS AND DISCUSSION

The surface pressures on the model, measured for the complete range of Mach numbers and Reynolds numbers at selected angles of attack, are presented as pressure coefficients in tabular form immediately following the figures. Table III is an index to these data which are presented in tables IV through XXII. A representative portion of the pressure-distribution data has been presented graphically in the figures of this report to facilitate the analysis of the force and moment characteristics of the model. Due to the staggering of the orifices (as explained in the section "Model and Apparatus"), a slight "saw-tooth" variation is present in the plotted values of the chordwise pressure distributions, particularly in regions where the spanwise pressure gradients were large. A mean fairing through the plotted values of pressure coefficient was therefore used to represent the pressure distribution at the spanwise stations indicated in figure 1.

The results of an investigation that was made to ascertain the effect of model-turntable juncture seals are presented in the appendix. These data indicate that the various alterations to the seal, in the model-turntable juncture, produced no significant changes in the aerodynamic characteristics of the wing.

Effects of Reynolds Number at a Mach Number of 0.25

The lift, drag, and pitching-moment characteristics of the model are presented in figure 5 for Reynolds numbers of 4,000,000, 8,000,000, 12,000,000, and 18,000,000. Figure 6 presents the chordwise distributions of pressure coefficient at the seven spanwise stations for several angles of attack at Reynolds numbers of 4,000,000, 8,000,000, and 18,000,000. Inspection of figure 5(a) reveals that at low to moderate values of lift coefficient the variation of lift coefficient with angle of attack was linear and the lift-curve slope was little affected by the increase in Reynolds number. At a Reynolds number of 4,000,000 the lift-curve slope increased beyond a lift coefficient of about 0.4 and decreased at lift coefficients greater than about 0.75. A comparison of these data with the pressure data in figure 6 indicates that the increase in lift-curve slope was due to separation and reattachment of the flow near the leading edge of the outer sections (indicated by a reduction in the peak pressure coefficients). Further comparison of the data shows that the reduction in the lift-curve slope occurred when the.

separated flow failed to reattach over the outer sections (indicated by a chordwise distribution of nearly constant pressure). Increasing the Reynolds number above 4,000,000 resulted in an increase in the lift coefficient at which the lift-curve slope increased and an increase in the lift coefficient at which complete flow separation over the outer sections resulted in a decrease in the lift-curve slope. The maximum lift coefficient increased only slightly as the Reynolds number was increased from 4,000,000 to 12,000,000.

The increase in lift-curve slope at moderate angles of attack was accompanied by a rearward movement of the wing center of pressure (fig. 5(b)) which was followed by a forward movement as the lift-curve slope decreased. Beyond maximum lift the wing center of pressure moved rearward. With increasing Reynolds number the initiation of flow separation over the outer sections had a more pronounced effect on the rearward movement of the wing center of pressure.

Inspection of the drag data in figure 5(c) in conjunction with the lift and moment data in figures 5(a) and 5(b) shows that an additional increase in the rate of change of drag coefficient with lift coefficient occurred simultaneously with the increase in lift-curve slope and longitudinal stability.

In figure 7 the section normal-force coefficients, derived from integration of the pressure data, are presented as functions of the uncorrected angle of attack. With increasing Reynolds number there was an increase in the maximum section normal-force coefficients at the outer sections. A comparison of the data of figure 7 with that presented in figure 5 indicates that the increase in the lift-curve slope, the increase in longitudinal stability, and the more rapid rate of drag rise of the wing coincided with the increase in the section normal-force-curve slope of the tip sections. Attendant upon this increase in the section normal-force-curve slope at the higher Reynolds number was a rapid expansion of the chordwise extent of the region of flow separation starting from just behind the leading edge. The resultant redistribution of pressure caused a rearward movement of the centers of pressure of the outer sections as shown in figure 8.

Effects of Reynolds Number at a Mach Number of 0.60

The lift, drag, and pitching-moment characteristics of the wing are compared in figure 9 for Reynolds numbers of 4,000,000 and 8,000,000. The corresponding chordwise distributions of static pressure coefficient at the seven spanwise stations are presented in figure 10 for several angles of attack. From figure 9 it is evident that increasing the Reynolds number from 4,000,000 to 8,000,000 extended the linear portion of the lift curve, caused a more nearly linear variation of the pitching-moment coefficient with the lift coefficient, and resulted in a reduction

in the drag coefficients for lift coefficients greater than about 0.2. The pressure data in figure 10 reveal that at the higher Reynolds number there was an increase in the angle of attack at which the reduction in the peak pressure coefficients began at the outer sections. These data also show that at the higher Reynolds number there was a more gradual reduction in the peak pressure coefficients near the leading edge of the wing with increasing angle of attack, probably the result of a more gradual growth of the chordwise extent of the region of separation.

In figure 11 the section normal-force coefficients at the two Reynolds numbers are presented as functions of the uncorrected angle of attack. The effect of increasing the Reynolds number was to delay to higher angles of attack the rapid increase in section normal-force coefficient and also to increase the maximum values of section normal-force coefficient at the outer sections. A comparison of figures 10 and 11 reveals that at a Reynolds number of 4,000,000 the large increase in slope of the section normal-force curves was the result of the region of separation extending a considerable distance rearward from the leading edge. At a Reynolds number of 8,000,000 the onset of separation and reattachment of the flow near the leading edge was, for most sections, at first accompanied by a decrease in the slope of the section normal-force curves followed by an increase in the slope as the region of separation extended rearward from the leading edge.

In addition to the changes in the section normal-force coefficients with the increase in Reynolds number, the positions of the section centers of pressure were also changed. The variations of the locations of the section centers of pressure and of the pitching-moment coefficient of the wing with angle of attack at Reynolds numbers of 4,000,000 and 8,000,000 are shown in figure 12. It is to be noted that the rearward movement of the section centers of pressure was considerably more abrupt and of greater magnitude at a Reynolds number of 4,000,000 than at a Reynolds number of 8,000,000. Thus, it appears that changes in the section centers of pressure as well as changes in the spanwise distribution of the section normal-force coefficient were responsible for the differences noted in the pitching-moment characteristics at these two Reynolds numbers.

Effects of Mach Number at a Reynolds Number of 4,000,000

Limitations of the data due to wind-tunnel choking.- Before the effects of Mach number on the aerodynamic characteristics are discussed, it is necessary to explain the possible limitations of portions of the data obtained at Mach numbers near those at which choking occurred in the wind tunnel. In order to ascertain the degree of wind-tunnel choking, static pressures were measured along the wind-tunnel wall

opposite the upper surface of the model. From these pressure surveys the approximate extent of supersonic flow on the tunnel wall was determined.

As an illustration of the results of the surveys, figure 13 is presented. This figure shows the development of a region of supersonic flow on the upper surface of the model and on the tunnel wall with increasing angle of attack at a Mach number of 0.92. It is apparent that, at angles of attack of 4° or less, the extent of supersonic flow on the tunnel wall was small and, consequently, any alteration to the supersonic flow field about the model due to the presence of the tunnel walls was probably slight. However, as the angle of attack was increased to 6° and beyond, the region of supersonic flow on the tunnel wall increased, resulting in a "partially choked" condition. The data obtained under these conditions are represented by the dotted portions of the curves in the figures.

Force and moment characteristics.- In figure 14 the aerodynamic characteristics of the wing at Mach numbers ranging from 0.08 to 0.96 are presented for a constant Reynolds number of 4,000,000. Included in this figure are the data obtained at Mach numbers of 0.08, 0.25, and 0.60 for a constant Reynolds number of 8,000,000. These data will be discussed under the heading "Influence of Reynolds Number on the Effects of Compressibility." The effects of Mach number on the lift, drag, and pitching-moment coefficients at a Reynolds number of 4,000,000 are summarized in figures 15 and 16 wherein the coefficients are plotted as functions of Mach number. The variation with Mach number of the lift-curve slope and the locations of the aerodynamic center for several angles of attack are shown in figures 17 and 18, respectively. The maximum lift-drag ratio and the lift coefficient for maximum lift-drag ratio are presented in figure 19.

With reference to figure 14(a), it may be seen that the lift-curve slope increased at lift coefficients of 0.6 and 0.4 for Mach numbers of 0.08 and 0.25, respectively, whereas the increase in lift-curve slope began at a lift coefficient of about 0.3 for Mach numbers from 0.40 to 0.90. In figure 17 the theoretical value of lift-curve slope computed by the method of reference 2 is shown in comparison with the experimental values for lift coefficients of 0, 0.2, and 0.4. The agreement between the experimental and theoretical values is good for lift coefficients of 0 and 0.2. The marked increase in the experimental values at a lift coefficient of 0.4 is believed to have resulted from separation and reattachment of the flow near the leading edge of the tip of the wing.

In figure 15, the pitching-moment coefficients for constant values of lift coefficient at a Reynolds number of 4;000,000, obtained from figure 14(b), are shown to have gradually become more negative with increasing Mach number. At Mach numbers slightly below those where the

tunnel became partially choked the pitching-moment coefficients increased rapidly in absolute value.

The effect of Mach number on the location of the aerodynamic center at angles of attack of 0°, 2°, 4°, and 6°, is shown in figure 18. The aerodynamic center at an angle of attack of 0° moved rearward approximately 6 percent of the mean aerodynamic chord as the Mach number was increased from 0.08 to 0.92 and then moved rapidly rearward as the Mach number was further increased. At angles of attack of 2° and 4°, the position of the aerodynamic center varied only slightly up to Mach numbers of 0.91 and 0.90, respectively, beyond which it moved rapidly rearward. At an angle of attack of 6°, the aerodynamic center moved aft approximately 9 percent of the mean aerodynamic chord as the Mach number was increased from 0.08 to 0.85 and then continued rearward more rapidly with increasing Mach number.

In figure 14(c), the familiar low-drag range is discernible at low lift coefficients at Mach numbers up to 0.83. The loss of this low-drag region is reflected in the lower two curves shown in figure 16 wherein the drag coefficient is presented as a function of Mach number for constant values of lift coefficient. At a Mach number of 0.83 the drag coefficient may be seen to have increased only slightly over its low-speed value for lift coefficients of 0 and 0.1. Between a Mach number of 0.83 and that for drag divergence the drag increased roughly 50 percent. A similar variation of the drag coefficient with Mach number may be noted for a lift coefficient of 0.2 although this was outside the low-drag range. At higher lift coefficients the gradual drag rise commenced at considerably lower Mach numbers. The Mach number for drag divergence, defined as the point at which $(\partial C_D/\partial M_o)_{C_L} = 0.10$, decreased from about 0.94 at a lift coefficient of 0 to 0.875 at a lift coefficient of 0.5. The sudden reduction in drag coefficient just prior to drag divergence for lift coefficients of 0.4 and 0.5 may be due to a reduction in the region of separated flow over the forward part of the airfoil as explained in reference 5.

In figure 19 the maximum lift-drag ratio is shown to have been about 19 between Mach numbers of 0.08 and 0.45, thereafter decreasing gradually to about 16 at a Mach number of 0.92. Further increase in Mach number up to 0.96 resulted in a decrease in the maximum lift-drag ratio to about 9. The lift coefficient for maximum lift-drag ratio deviated only slightly from 0.2 throughout the Mach number range.

Pressure-distribution characteristics.- The chordwise distribution of pressure coefficient at the seven spanwise stations is presented in figure 20 for angles of attack of 2°, 4°, and 6° at several selected Mach numbers. The pressure distributions for an angle of attack of 2° were used in locating the isobars, or lines of constant pressure coefficient, on the upper and lower surfaces of the model as shown in figure 21. It can be seen that, in general, the isobars curve rearward near the root of the wing so as to approach the plane of symmetry

perpendicularly. Conversely, the isobars at the tip of the wing tend to curve forward. From the isobar plots it may be seen that the points of minimum pressure, exclusive of those at or near the leading edge, were displaced rearward at sections near the root and forward at sections near the tip. The crest lines (lines defining the locus of points at which the surface of the wing is tangent to the undisturbed free stream) are indicated in figure 21 to provide a reference from which to gage the variance in the isobars. A discussion of an interpretation of isobars is given in reference 4.

The spanwise distributions of section normal-force coefficient at several Mach numbers are presented in figure 22 for angles of attack of 2°, 4°, and 6°. As previously noted, the dotted curves represent data obtained with the supersonic flow field of the model extending to the tunnel wall. It may be observed that the maximum value of section normal-force coefficient occurred at about 70 percent of the semispan. As the Mach number was increased from 0.60 to 0.90 at an angle of attack of 6°, the section normal-force coefficient showed a greater increase at the tip stations than at stations nearer the root. This greater increase in the section normal-force coefficient of the tip sections was accompanied by an increase in the lift-curve slope, an increase in stability, and an increase in the rate of drag rise. (See fig. 14.)

In figure 23 the spanwise distribution of loading coefficient $c_n c/C_N c_{av}$ at several Mach numbers is presented in comparison with the theoretical distribution. The theoretical distribution is practically invariant throughout the range of Mach numbers for which experimental data are presented. Similarly, the experimental values of loading coefficient show only small variations with Mach number and are in good agreement with the theoretical values. The experimental loading coefficients are based upon the slopes of the section normal-force curves measured through an angle of attack of 0°.

The effects of compressibility on the locations of the section centers of pressure at the seven spanwise stations for angles of attack of 2°, 4°, and 6° are shown in figure 24. The effect of increasing Mach number was, generally, to cause a rearward movement of the section centers of pressure near the root and a forward movement near the tip up to approximately the Mach number for drag divergence. An exception to this variation with Mach number is shown for an angle of attack of 6° at 0.924 semispan where the center of pressure moved rearward with increasing Mach number. The over-all effect of the movements of the section centers of pressure, together with the changes in the spanwise distribution of load (fig. 22), on the location of the wing aerodynamic center at angles of attack of 2°, 4°, and 6° may be seen by reference to figure 18.

Influence of Reynolds Number on the Effects of Compressibility

In figure 14, the data obtained at several Mach numbers for a Reynolds number of 8,000,000 have been included with the data for a Reynolds number of 4,000,000 to show, insofar as is possible, the influence of Reynolds number on the compressibility effects encountered up to a Mach number of 0.60.

With an increase in Mach number to 0.60, the linear portion of the lift curve (fig. 14(a)) was extended to higher lift coefficients at a Reynolds number of 8,000,000, whereas at a Reynolds number of 4,000,000 it was reduced. This same trend may be seen in the pitching-moment characteristics (fig. 14(b)) where changes in stability with an increase in Mach number to 0.60 were delayed to higher lift coefficients at a Reynolds number of 8,000,000, whereas at a Reynolds number of 4,000,000 increasing the Mach number to 0.60 reduced the lift coefficient at which changes in stability occurred. Thus, the effect of increasing Mach number on the lift coefficient at which tip stalling occurred was apparently reversed by increasing the Reynolds number from 4,000,000 to 8,000,000. The drag data (fig. 14(c)) indicate, however, that an increase in the rate of change of drag coefficient with lift coefficient occurred at about the same lift coefficient for Reynolds numbers of 4,000,000 and 8,000,000 at a Mach number of 0.60. The explanation of this effect of Reynolds number is provided in the pressure data of figure 10. These data show that at a Reynolds number of 8,000,000, leading-edge flow separation with reattachment near the tip of the wing actually began at an angle of attack between 6° and 8° although the flow did not separate completely over the outer sections until the angle of attack was increased beyond 12°. At a Reynolds number of 4,000,000 the flow had separated completely over the outer sections at an angle of attack of 8°. Thus, due to the more gradual spreading of the stall near the tip at a Reynolds number of 8,000,000, there was no sudden change in the slope of either the lift curve or the pitching-moment curve although the drag rise was similar to that at a Reynolds number of 4,000,000.

It is important to note that the favorable effects of increasing the Reynolds number may persist at still higher Mach numbers. In this event, the effect of increasing Mach number at higher Reynolds numbers would differ from that shown at a Reynolds number of 4,000,000.

CONCLUSIONS

An investigation has been made of the effects of scale and compressibility on the aerodynamic characteristics of a wing having the quarter-chord line swept back 45° and an aspect ratio of 3.0. Force, moment, and surface pressures were measured for Reynolds numbers up

to 18,000,000 at a constant Mach number of 0.25; for Mach numbers up to 0.96 at a constant Reynolds number of 4,000,000; and for Mach numbers up to 0.60 at a constant Reynolds number of 8,000,000. The results of the tests indicate the following conclusions:

1. For all Mach numbers and Reynolds numbers in the test range, no flow separation appeared to exist near the leading edge of the wing for lift coefficients less than 0.3. At higher lift coefficients the initiation of leading-edge flow separation with reattachment, over the outer portions of the wing, was accompanied in nearly every case by an increase in the lift-curve slope, an increase in static longitudinal stability, and an increase in the rate of drag rise.

2. The effect of increasing the Reynolds number at Mach numbers of 0.25 and 0.60 was to delay to higher lift coefficients the onset of flow separation near the leading edge and the concomitant effects on the lift, drag, and pitching moment.

3. Increasing the Mach number to approximately that for drag divergence at a Reynolds number of 4,000,000 resulted in a rearward movement of the wing aerodynamic center of about 6 percent of the mean aerodynamic chord at zero lift. (The Mach number for drag divergence was found to vary from about 0.94 at a lift coefficient of 0 to about 0.875 at a lift coefficient of 0.5.) Further increase in Mach number resulted in a rapid rearward movement of the aerodynamic center.

4. The spanwise distribution of loading coefficient at low lift coefficients showed good agreement with theory, being practically unaffected by compressibility. The increase in lift-curve slope with Mach number also was in good agreement with that predicted by theory.

5. The effects of compressibility on the force and moment characteristics up to a Mach number of 0.60 were influenced by an increase in Reynolds number from 4,000,000 to 8,000,000. At the lower Reynolds number the angle-of-attack range for which the lift and pitching-moment curves were nearly linear was reduced by the increase in Mach number, whereas this angle-of-attack range was increased at the higher Reynolds number.

6. Various alterations to the seal at the model-turntable juncture produced no significant changes in the aerodynamic characteristics of the wing.

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APPENDIX

MODEL–TURNTABLE SEAL INVESTIGATION

In wind–tunnel testing with semispan models it would be desirable to isolate the reflection–plane turntable from the force–measuring apparatus. Such an arrangement poses the problem of minimizing air flow through the model–turntable juncture in such a manner that the flow over the model is not disturbed and the turntable acts as a true reflection plane. To ascertain the effects of various model–turntable–juncture seal arrangements on the measured forces, moments, and pressures, six seals were tested. These seal arrangements are illustrated in figure 4.

In figure 25 the lift, drag, and pitching–moment data for each of the five modified seal arrangements have been superimposed on the corresponding data for the original seal arrangement. Data are shown for Mach numbers of 0.25 and 0.80 at a constant Reynolds number of 4,000,000.

From the nature of the different configurations, it might be expected that the greatest difference in the force characteristics of the model would appear in changing from seal A to seal B. (See fig. 4). However, the data presented in figure 25 indicate that only small changes in the forces and moments resulted in changing from any one arrangement to any other. The slight differences which do exist in the force and moment data could be attributable to experimental scatter rather than to changes in the flow at the root of the wing.

Further evidence of the negligible effect of the various seal modifications is indicated in figure 26 wherein is shown a comparison of the chordwise distribution of pressure coefficient for an angle of attack of 16° at 0.086 semispan for seals A and B. The data for a rerun with seal A are included to indicate the variation in pressures which might be expected from the experimental variations. From the data in figure 26, it was found that in changing from seal A to seal B the section normal–force coefficient at 0.086 semispan decreased about 1 percent at a Mach number of 0.25 and about 3 percent at a Mach number of 0.80. The decrease in section normal–force coefficient was smaller at the remaining semispan stations so that the over–all effect was considered negligible.

REFERENCES

1. Sivells, James C., and Deters, Owen J.: Jet-Boundary and Plan-Form Corrections for Partial-Span Models with Reflection Plane, End Plate, or No End Plate in a Closed Circular Wind Tunnel. NACA Rep. 843, 1946. (Formerly NACA TN 1077)

2. DeYoung, John, and Harper, Charles W.: Theoretical Symmetric Span Loading at Subsonic Speeds for Wings Having Arbitrary Plan Form. NACA Rep. 921, 1948. (Formerly TN's 1476, 1491, and 1772)

3. Herriot, John G.: Blockage Corrections for Three-Dimensional-Flow Closed-Throat Wind Tunnels, with Consideration of the Effect of Compressibility. NACA Rep. 995, 1950. (Formerly NACA RM A7B28)

4. Edwards, George G., and Boltz, Frederick W.: An Analysis of the Forces and Pressure Distribution on a Wing with the Leading Edge Swept Back 37.25°. NACA RM A9K01, 1950.

5. Lindsey, W. F., Daley, Bernard N., and Humphreys, Milton D.: The Flow and Force Characteristics of Supersonic Airfoils at High Subsonic Speeds. NACA TN 1211, 1947.

TABLE I.- COORDINATES FOR THE NACA 64A010 AIRFOIL SECTION

[All dimensions in percent of chord]

Upper and Lower Surfaces	
Station	Ordinate
0	0
.50	.804
.75	.969
1.25	1.225
2.50	1.688
5	2.327
7.50	2.805
10	3.199
15	3.813
20	4.272
25	4.606
30	4.837
35	4.968
40	4.995
45	4.894
50	4.684
55	4.388
60	4.021
65	3.597
70	3.127
75	2.623
80	2.103
85	1.582
90	1.062
95	.541
100	.021
L. E. radius, 0.687 T. E. radius, 0.023	

TABLE II.- COORDINATES FOR SECTIONS PARALLEL TO THE PLANE OF SYMMETRY

[All dimensions in percent of chord]

Upper and Lower Surfaces	
Station	Ordinate
0	0
.63	.673
.95	.811
1.57	1.023
3.14	1.406
6.23	1.925
9.29	2.306
12.31	2.612
18.23	3.074
24.00	3.401
29.63	3.622
35.13	3.757
40.49	3.813
45.72	3.788
50.83	3.667
55.82	3.469
60.69	3.212
65.46	2.910
70.12	2.574
74.67	2.213
79.12	1.836
83.48	1.456
87.74	1.083
91.92	.720
96.00	.363
100.00	.014
L. E. radius, 0.485 T. E. radius, 0.016	

TABLE III.- INDEX OF TABULATED PRESSURE COEFFICIENTS

Table No.	$R \times 10^{-6}$	M_o	α_u Range
IV	4.0	0.25	0° to 24°
V	↓	.40	↓
VI		.60	
VII		.80	0° to 16°
VIII		.83	0° to 14°
IX		.86	0° to 12°
X		.88	0° to 12°
XI		.90	[a]0° to 12° (10° & 12°)
XII		.92	0° to 10° (6°, 8°, & 10°)
XIII		.93	0° to 8° (4°, 6°, & 8°)
XIV		.94	0° to 6° (3°, 4°, & 6°)
XV		.95	0° to 6° (2°, 3°, 4°, & 6°)
XVI	↓	.96	0° to 4° (1°, 2°, 3°, & 4°)
XVII	6.0	.25	0° to 24°
XVIII	8.0	.08	↓
XIX	↓	.25	
XX		.60	0° to 14°
XXI	12.0	.25	0° to 24°
XXII	18.0	.25	0° to 20°

[a]Parentheses indicate angles of attack for which the pressure data may have been affected by wind-tunnel choking.

TABLE IV.- PRESSURE COEFFICIENTS AT SEVEN SEMISPAN STATIONS OF THE WING. M_o, 0.25; R, 4,000,000.

(a) α_u, 0°, 1°, 2°, 3°.

Semi-span sta.	Percent chord	UPPER SURFACE Angle of attack 0°	1°	2°	3°	LOWER SURFACE Angle of attack 0°	1°	2°	3°
0.086 b/2	0	0.479	0.476	0.444	0.407	- -	- -	- -	- -
	1.5	.026	-.065	-.190	-.313	0.004	0.079	0.170	0.225
	5.5	-.035	-.082	-.140	-.198	-.037	.006	.063	.103
	6.5	-.054	-.101	-.152	-.213	-.060	-.016	.038	.074
	11.0	-.060	-.102	-.148	-.189	-.067	-.036	.007	.039
	14.5	-.077	-.113	-.150	-.191	-.079	-.049	-.014	.017
	21.0	-.090	-.119	-.150	-.184	-.092	-.068	-.035	-.009
	24.5	-.096	-.124	-.157	-.189	-.109	-.084	-.048	-.024
	31.0	-.098	-.123	-.152	-.180	-.115	-.091	-.060	-.042
	34.5	-.117	-.141	-.169	-.198	-.134	-.106	-.077	-.060
	41.0	-.140	-.161	-.188	-.215	-.136	-.119	-.092	-.075
	44.5	-.150	-.178	-.190	-.221	- -	- -	- -	- -
	51.0	-.150	-.173	-.188	-.217	-.152	-.130	-.111	-.092
	59.5	-.132	-.147	-.159	-.182	-.132	-.123	-.096	-.088
	71.0	-.098	-.115	-.125	-.143	-.102	-.095	-.073	-.070
	79.5	-.056	-.068	-.073	-.088	-.056	-.051	-.037	-.033
	91.0	0	-.011	-.016	-.024	-.002	-.001	.006	.004
0.195 b/2	0	0.427	0.417	0.347	0.247	- -	- -	- -	- -
	1.5	-.008	-.123	-.256	-.434	0.025	0.136	0.249	0.319
	5.5	-.071	-.128	-.209	-.279	-.065	-.011	.059	.114
	6.5	-.068	-.143	-.211	-.279	-.088	-.014	.023	.078
	11.0	-.098	-.141	-.196	-.248	-.102	-.062	-.014	.030
	14.5	-.111	-.150	-.192	-.233	-.111	-.080	-.035	.004
	21.0	-.115	-.154	-.190	-.222	-.125	-.095	-.056	-.029
	24.5	-.127	-.159	-.190	-.217	-.129	-.101	-.073	-.033
	31.0	-.130	-.156	-.186	-.215	-.142	-.121	-.094	-.066
	34.5	-.138	-.178	-.194	-.219	-.150	-.128	-.098	-.075
	41.0	-.153	-.178	-.205	-.230	-.153	-.137	-.113	-.084
	44.5	-.157	-.185	-.209	-.232	-.150	-.136	-.113	-.086
	51.0	-.140	-.170	-.180	-.205	-.152	-.141	-.113	-.088
	59.5	-.127	-.150	-.152	-.178	-.132	-.104	-.098	-.086
	71.0	-.083	-.095	-.113	-.123	-.083	-.069	-.065	-.059
	79.5	-.035	-.049	-.056	-.068	-.035	-.031	-.019	-.020
	91.0	.023	.015	.011	.006	.013	.015	.019	.024
0.382 b/2	0	0.408	0.390	0.295	0.135	- -	- -	- -	- -
	1.5	-.033	-.187	-.362	-.565	-0.056	0.050	0.153	0.236
	5.5	-.098	-.178	-.266	-.353	-.104	-.031	.040	.100
	6.5	-.113	-.191	-.266	-.353	-.117	-.049	.017	.076
	11.0	-.121	-.178	-.228	-.290	-.129	-.079	-.019	.024
	14.5	-.129	-.178	-.226	-.270	-.134	-.091	-.040	-.003
	21.0	-.136	-.178	-.213	-.261	-.140	-.106	-.073	-.031
	24.5	-.140	-.178	-.209	-.254	-.140	-.113	-.077	-.039
	31.0	-.140	-.178	-.205	-.237	-.161	-.132	-.100	-.068
	34.5	-.140	-.176	-.196	-.233	-.165	-.139	-.111	-.077
	41.0	-.163	-.192	-.209	-.239	-.155	-.137	-.113	-.084
	44.5	-.165	-.191	-.209	-.233	-.153	-.137	-.113	-.086
	51.0	-.148	-.176	-.186	-.211	-.150	-.141	-.115	-.090
	59.5	-.130	-.141	-.155	-.178	-.129	-.119	-.094	-.083
	71.0	-.073	-.086	-.098	-.106	-.073	-.064	-.056	-.049
	79.5	-.033	-.038	-.044	-.059	-.033	-.027	-.017	-.013
	91.0	.025	.024	.019	.015	.023	.026	.029	.035
0.555 b/2	0	0.425	0.408	0.325	0.144	- -	- -	- -	- -
	1.5	-.023	-.207	-.395	-.629	-0.065	0.059	0.165	0.260
	5.5	-.098	-.198	-.286	-.388	-.098	-.025	.048	.120
	6.5	-.111	-.203	-.286	-.386	-.109	-.035	.032	.118
	11.0	-.115	-.185	-.244	-.307	-.129	-.069	-.012	.041
	14.5	-.121	-.181	-.232	-.289	-.129	-.079	-.033	.017
	21.0	-.134	-.180	-.224	-.270	-.136	-.099	-.058	-.018
	24.5	-.129	-.178	-.211	-.252	-.144	-.106	-.069	-.027
	31.0	-.139	-.178	-.201	-.243	-.148	-.121	-.090	-.051
	34.5	-.142	-.178	-.205	-.239	-.153	-.134	-.096	-.066
	41.0	-.153	-.189	-.205	-.239	-.150	-.130	-.096	-.075
	44.5	-.155	-.185	-.198	-.232	-.148	-.134	-.102	-.081
	51.0	-.144	-.172	-.176	-.208	-.144	-.130	-.106	-.084
	59.5	-.117	-.126	-.134	-.160	-.129	-.117	-.090	-.079
	71.0	-.060	-.084	-.092	-.099	-.064	-.047	-.040	-.033
	79.5	-.019	-.031	-.039	-.046	-.014	-.014	-.008	-.002
	91.0	.038	.032	.029	-.024	.036	.041	.044	.043

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TABLE IV.- CONTINUED.

(a) α_u, 0°, 1°, 2°, 3° - Concluded.

Semi-span sta.	Percent chord	UPPER SURFACE Angle of attack 0°	1°	2°	3°	LOWER SURFACE Angle of attack 0°	1°	2°	3°
0.707 b/2	0	0.421	0.381	0.268	0.024	- -	- -	- -	- -
	1.5	-.031	-.233	-.429	-.692	-0.058	0.096	0.211	0.309
	5.5	-.107	-.214	-.307	-.425	-.109	-.023	.057	.133
	6.5	-.115	-.216	-.307	-.417	-.115	-.033	.032	.111
	11.0	-.115	-.187	-.249	-.318	-.134	-.071	-.012	.044
	14.5	-.125	-.192	-.249	-.307	-.134	-.079	-.031	.024
	21.0	-.134	-.187	-.230	-.276	-.138	-.097	-.058	-.013
	24.5	-.134	-.181	-.221	-.265	-.142	-.104	-.067	-.029
	31.0	-.148	-.180	-.211	-.250	-.148	-.115	-.086	-.049
	34.5	-.150	-.180	-.211	-.246	-.148	-.119	-.090	-.053
	41.0	-.153	-.181	-.205	-.235	-.146	-.124	-.096	-.070
	44.5	-.153	-.180	-.194	-.228	-.146	-.124	-.104	-.077
	51.0	-.142	-.169	-.173	-.197	-.144	-.126	-.109	-.086
	59.5	-.115	-.132	-.142	-.160	-.115	-.106	-.086	-.077
	71.0	-.058	-.077	-.083	-.094	-.019	-.049	-.039	-.031
	79.5	-.027	-.022	-.029	-.038	-.010	-.005	0	0
	91.0	.040	.039	.038	.033	.048	.046	.048	.044
0.831 b/2	0	0.389	0.414	0.362	0.188	- -	- -	- -	- -
	1.5	-.046	-.235	-.429	-.681	-0.060	0.098	0.203	0.300
	5.5	-.117	-.216	-.314	-.432	-.117	-.031	.036	.116
	6.5	-.117	-.214	-.305	-.417	-.123	-.046	.027	.100
	11.0	-.117	-.194	-.249	-.316	-.132	-.069	-.021	.033
	14.5	-.127	-.194	-.247	-.307	- -	- -	- -	- -
	21.0	-.136	-.180	-.219	-.270	-.146	-.104	-.071	-.031
	24.5	-.138	-.178	-.217	-.252	-.146	-.106	-.077	-.040
	31.0	-.138	-.174	-.198	-.233	-.152	-.121	-.096	-.068
	34.5	-.140	-.174	-.194	-.230	-.152	-.123	-.106	-.070
	41.0	-.144	-.180	-.194	-.232	-.150	-.126	-.109	-.083
	44.5	-.150	-.178	-.190	-.213	-.146	-.126	-.111	-.088
	51.0	-.146	-.161	-.171	-.195	-.132	-.137	-.109	-.086
	59.5	-.113	-.123	-.123	-.141	-.117	-.104	-.096	-.084
	71.0	-.056	-.068	-.075	-.083	-.046	-.058	-.042	-.042
	79.5	-.012	-.012	-.023	-.029	-.002	-.003	-.002	-.009
	91.0	.040	.043	.040	.043	.048	.046	.046	.043
0.924 b/2	0	0.410	0.322	0.165	-0.141	- -	- -	- -	- -
	1.5	-.002	-.196	-.403	-.675	-0.075	0.074	0.178	0.278
	5.5	-.032	-.227	-.316	-.421	-.123	-.038	.030	.107
	6.5	-.136	-.226	-.309	-.408	-.123	-.049	.021	.089
	11.0	-.132	-.194	-.247	-.298	-.138	-.082	-.037	.016
	14.5	-.138	-.191	-.232	-.270	-.142	-.101	-.060	-.014
	21.0	-.140	-.178	-.209	-.243	-.150	-.119	-.094	-.059
	24.5	-.136	-.163	-.192	-.222	-.144	-.121	-.098	-.070
	31.0	-.134	-.159	-.173	-.197	-.142	-.123	-.106	-.086
	34.5	-.129	-.152	-.165	-.187	-.136	-.123	-.107	-.088
	41.0	-.142	-.159	-.170	-.193	-.134	-.123	-.113	-.103
	44.5	-.138	-.158	-.157	-.178	-.127	-.121	-.111	-.105
	51.0	-.119	-.130	-.140	-.158	-.127	-.113	-.111	-.105
	59.5	-.085	-.086	-.098	-.105	-.094	-.086	-.081	-.077
	71.0	-.037	-.040	-.044	-.049	-.029	-.024	-.033	-.046
	79.5	.004	.006	.002	-.011	.011	.004	.002	0
	91.0	.052	.054	.052	.043	.059	.058	.046	.043

TABLE IV.- CONTINUED.

(b) α_u, 4°, 6°, 8°, 10°.

Semi-span sta.	Percent chord	UPPER SURFACE Angle of attack 4°	6°	8°	10°	LOWER SURFACE Angle of attack 4°	6°	8°	10°
0.086 b/2	0	0.328	0.073	-0.295	-0.784	- -	- -	- -	- -
	1.5	-.453	-.766	-1.157	-1.494	0.293	0.400	0.465	0.500
	5.5	-.246	-.376	-.503	-.648	.156	.246	.329	.394
	6.5	-.256	-.372	-.492	-.615	.121	.205	.287	.350
	11.0	-.227	-.312	-.396	-.493	.081	.151	.230	.289
	14.5	-.225	-.302	-.377	-.458	.058	.128	.194	.256
	21.0	-.212	-.276	-.339	-.401	.035	.092	.154	.210
	24.5	-.215	-.276	-.335	-.397	.012	.071	.133	.184
	31.0	-.206	-.258	-.303	-.362	-.011	.040	.100	.153
	34.5	-.221	-.272	-.310	-.364	-.034	.019	.079	.132
	41.0	-.227	-.274	-.309	-.360	-.045	.001	.059	.103
	44.5	-.231	-.274	-.312	-.353	- -	- -	- -	- -
	51.0	-.225	-.262	-.291	-.326	-.064	-.024	-.024	.071
	59.5	-.189	-.218	-.244	-.270	-.064	-.031	-.020	.057
	71.0	-.148	-.172	-.186	-.209	-.045	-.022	-.022	.051
	79.5	-.093	-.102	-.119	-.132	-.016	.009	-.039	.059
	91.0	-.022	-.035	-.034	-.040	.020	.032	.047	.067
0.195 b/2	0	0.083	-0.370	-1.017	-1.851	- -	- -	- -	- -
	1.5	-.608	-1.037	-1.710	-2.186	0.385	0.442	0.425	0.345
	5.5	-.342	-.512	-.692	-.880	.175	.269	.348	.425
	6.5	-.332	-.487	-.645	-.803	.133	.228	.305	.383
	11.0	-.286	-.404	-.435	-.629	.077	.157	.234	.308
	14.5	-.268	-.368	-.461	-.554	.041	.117	.192	.266
	21.0	-.256	-.329	-.404	-.477	.012	.078	.146	.212
	24.5	-.246	-.314	-.385	-.445	.003	.065	.127	.189
	31.0	-.233	-.295	-.352	-.401	-.032	.026	.081	.143
	34.5	-.244	-.295	-.349	-.399	-.045	.007	.062	.120
	41.0	-.242	-.291	-.330	-.376	-.057	-.006	.041	.097
	44.5	-.242	-.291	-.328	-.362	-.057	-.012	.035	.088
	51.0	-.213	-.252	-.291	-.324	-.074	-.025	.014	.063
	59.5	-.177	-.214	-.236	-.263	-.070	-.033	.007	.051
	71.0	-.131	-.151	-.167	-.180	-.037	-.014	.014	.053
	79.5	-.064	-.079	-.091	-.096	-.001	.015	.037	.063
	91.0	.003	0	-.005	-.002	.026	.040	.051	.074
0.382 b/2	0	-0.074	-0.756	-1.720	-2.968	- -	- -	- -	- -
	1.5	-.759	-1.349	-2.010	-2.240	0.303	0.400	0.438	0.438
	5.5	-.434	-.641	-.864	-1.096	.156	.261	.341	.410
	6.5	-.420	-.616	-.809	-1.016	.133	.228	.306	.383
	11.0	-.344	-.479	-.618	-.763	.075	.161	.238	.310
	14.5	-.323	-.439	-.555	-.673	.041	.126	.200	.272
	21.0	-.292	-.385	-.471	-.558	.007	.078	.150	.214
	24.5	-.284	-.366	-.444	-.519	.001	.069	.129	.193
	31.0	-.263	-.329	-.393	-.458	-.036	.021	.079	.151
	34.5	-.250	-.314	-.372	-.424	-.045	.013	.066	.128
	41.0	-.259	-.310	-.352	-.401	-.055	-.004	.049	.097
	44.5	-.248	-.295	-.339	-.376	-.062	-.018	.037	.084
	51.0	-.219	-.256	-.295	-.324	-.074	-.025	.012	.061
	59.5	-.187	-.214	-.236	-.257	-.057	-.024	.009	.051
	71.0	-.114	-.135	-.144	-.153	-.034	-.006	.014	.053
	79.5	-.055	-.054	-.079	-.081	.001	.017	.033	.059
	91.0	.018	.013	-.016	.006	.061	.051	.056	.089
0.555 b/2	0	-0.089	-0.885	-1.970	-3.433	- -	- -	- -	- -
	1.5	-.832	-1.605	-3.514	-2.638	0.345	0.421	0.440	0.396
	5.5	-.476	-.706	-.954	-1.230	.175	.286	.366	.425
	6.5	-.458	-.670	-.889	-1.134	.154	.267	.345	.408
	11.0	-.363	-.533	-.668	-.849	.087	.190	.268	.341
	14.5	-.342	-.472	-.601	-.742	.064	.151	.230	.302
	21.0	-.305	-.401	-.477	-.608	.022	.096	.173	.235
	24.5	-.280	-.368	-.456	-.550	.012	.084	.146	.212
	31.0	-.267	-.333	-.402	-.483	-.018	.046	.106	.157
	34.5	-.257	-.324	-.381	-.454	-.036	.028	.081	.138
	41.0	-.254	-.308	-.352	-.406	-.045	.005	.058	.109
	44.5	-.240	-.291	-.331	-.378	-.051	-.002	.049	.092
	51.0	-.217	-.252	-.286	-.330	-.058	-.018	.028	.071
	59.5	-.162	-.189	-.209	-.240	-.057	-.024	.012	.046
	71.0	-.102	-.118	-.133	-.150	-.018	.007	.030	.051
	79.5	-.047	-.060	-.056	-.073	.010	.026	.039	.053
	91.0	.030	.028	.026	.009	.031	.055	.058	.065

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TABLE IV.- CONTINUED.

(b) α_u, 4°, 6°, 8°, 10° - Concluded.

Semi-span sta.	Percent chord	UPPER SURFACE Angle of attack 4°	6°	8°	10°	LOWER SURFACE Angle of attack 4°	6°	8°	10°
0.707 b/2	0	-0.248	-1.195	-2.539	-4.186	- -	- -	- -	- -
	1.5	-.906	-1.762	-2.813	-2.801	0.370	0.428	0.391	0.264
	5.5	-.514	-.764	-1.040	-1.335	.192	.305	.383	.431
	6.5	-.497	-.733	-.981	-1.251	.169	.276	.360	.417
	11.0	-.372	-.529	-.692	-.895	.095	.190	.274	.341
	14.5	-.351	-.489	-.629	-.797	.070	.157	.240	.312
	21.0	-.311	-.410	-.509	-.646	.030	.103	.173	.237
	24.5	-.294	-.383	-.473	-.590	.010	.084	.152	.210
	31.0	-.275	-.343	-.414	-.506	-.018	.046	.104	.159
	34.5	-.265	-.329	-.391	-.473	-.020	.032	.083	.140
	41.0	-.250	-.301	-.352	-.408	-.047	.005	.052	.099
	44.5	-.242	-.283	-.324	-.383	-.051	-.004	.039	.080
	51.0	-.210	-.241	-.276	-.320	-.064	-.024	.020	.053
	59.5	-.162	-.185	-.205	-.238	-.057	-.024	.007	.032
	71.0	-.093	-.108	-.114	-.138	-.018	-.002	.020	.034
	79.5	-.037	-.041	-.049	-.071	.009	.026	.030	.038
	91.0	.037	.036	.030	.004	.053	.055	.058	.053
0.831 b/2	0	-0.041	-0.906	-1.852	-2.148	- -	- -	- -	- -
	1.5	-.889	-1.714	-1.942	-1.929	0.364	0.417	0.379	0.308
	5.5	-.510	-.762	-1.107	-1.502	.177	.276	.352	.412
	6.5	-.479	-.716	-.962	-1.240	.160	.263	.341	.402
	11.0	-.365	-.526	-.713	-1.000	.083	.173	.251	.316
	14.5	-.347	-.483	-.633	-.843	- -	- -	- -	- -
	21.0	-.300	-.416	-.498	-.642	.010	.078	.144	.207
	24.5	-.282	-.368	-.456	-.588	-.003	.057	.119	.178
	31.0	-.250	-.320	-.383	-.400	-.034	.021	.072	.124
	34.5	-.242	-.301	-.354	-.443	-.045	.003	.051	.097
	41.0	-.236	-.285	-.322	-.378	-.060	-.025	.018	.063
	44.5	-.210	-.262	-.297	-.347	-.068	-.037	.001	.038
	51.0	-.192	-.229	-.249	-.288	-.068	-.043	-.012	.025
	59.5	-.137	-.160	-.179	-.217	-.068	-.050	-.035	-.004
	71.0	-.078	-.093	-.102	-.132	-.032	-.025	-.016	.002
	79.5	-.020	-.031	-.043	-.081	.005	-.002	.003	.011
	91.0	.045	.034	.028	-.010	.045	.036	.031	.025
0.924 b/2	0	-0.455	-1.526	-2.721	-1.820	- -	- -	- -	- -
	1.5	-.902	-1.658	-2.664	-2.111	0.332	0.400	0.375	0.331
	5.5	-.501	-.737	-.994	-1.192	.160	.261	.327	.373
	6.5	-.464	-.695	-.794	-1.044	.152	.246	.314	.360
	11.0	-.347	-.487	-.633	-.924	.064	.140	.209	.264
	14.5	-.315	-.429	-.542	-.780	.024	.090	.152	.203
	21.0	-.269	-.349	-.425	-.608	-.028	.023	.073	.119
	24.5	-.242	-.310	-.373	-.550	-.047	-.006	.031	.076
	31.0	-.213	-.272	-.322	-.429	-.064	-.031	.003	.040
	34.5	-.200	-.251	-.297	-.412	-.074	-.050	-.024	.006
	41.0	-.198	-.239	-.274	-.347	-.087	-.064	-.041	-.014
	44.5	-.185	-.224	-.259	-.347	-.089	-.077	-.056	-.029
	51.0	-.154	-.193	-.217	-.314	-.091	-.079	-.060	-.037
	59.5	-.108	-.135	-.169	-.282	-.070	-.068	-.060	-.050
	71.0	-.051	-.077	-.106	-.211	-.032	-.041	-.041	-.033
	79.5	-.009	-.035	-.074	-.232	-.005	-.024	-.035	-.023
	91.0	.041	.015	-.030	-.148	.039	.017	.003	-.012

NACA

TABLE IV.- CONTINUED.

(c) α_u, 12°, 16°, 20°, 24°.

Semi-span sta.	Percent chord	UPPER SURFACE Angle of attack 12°	16°	20°	24°	LOWER SURFACE Angle of attack 12°	16°	20°	24°
0.086 b/2	0	-1.398	-3.085	-5.189	-5.935	- -	- -	- -	- -
	1.5	-2.050	-2.993	-4.448	-4.694	0.505	0.413	0.240	0.175
	5.5	-.799	-1.154	-1.611	-2.546	.449	.545	.615	.678
	6.5	-.761	-1.089	-1.519	-2.578	.413	.520	.610	.686
	11.0	-.587	-.830	-1.116	-1.441	.352	.465	.562	.642
	14.5	-.549	-.769	-.994	-1.356	.319	.442	.539	.615
	21.0	-.480	-.651	-.845	-1.243	.262	.381	.472	.543
	24.5	-.465	-.632	-.794	-1.133	.237	.356	.448	.518
	31.0	-.417	-.569	-.718	-.918	.203	.312	.398	.463
	34.5	-.423	-.565	-.720	-.912	.178	.292	.371	.451
	41.0	-.402	-.541	-.678	-.891	.155	.255	.331	.389
	44.5	-.398	-.527	-.657	-.870	- -	- -	- -	- -
	51.0	-.373	-.487	-.617	-.834	.109	.200	.272	.320
	59.5	-.312	-.409	-.533	-.760	.094	.173	.227	.269
	71.0	-.241	-.314	-.430	-.655	.084	.145	.187	.213
	79.5	-.155	-.215	-.316	-.533	.084	.139	.160	.130
	91.0	-.052	-.089	-.171	-.350	.084	.114	.116	.086
0.195 b/2	0	-2.912	-5.579	-3.881	-2.169	- -	- -	- -	- -
	1.5	-2.438	-3.755	-3.806	-2.013	0.166	-0.375	-0.567	-0.375
	5.5	-1.096	-1.794	-3.075	-1.976	.472	.539	.592	.634
	6.5	-1.000	-1.548	-2.856	-1.879	.434	.551	.610	.653
	11.0	-.769	-1.184	-2.529	-1.917	.369	.491	.590	.644
	14.5	-.675	-1.030	-1.923	-1.784	.319	.451	.545	.596
	21.0	-.572	-.811	-.986	-1.651	.262	.394	.486	.558
	24.5	-.532	-.765	-.912	-1.559	.243	.358	.457	.514
	31.0	-.484	-.668	-.704	-1.403	.195	.303	.402	.463
	34.5	-.465	-.634	-.699	-1.308	.168	.282	.366	.425
	41.0	-.442	-.575	-.643	-1.196	.145	.242	.324	.371
	44.5	-.426	-.556	-.628	-1.156	.128	.225	.292	.349
	51.0	-.371	-.480	-.571	-1.022	.107	.187	.255	.301
	59.5	-.308	-.402	-.491	-.908	.084	.152	.213	.238
	71.0	-.216	-.285	-.388	-.737	.073	.132	.172	.177
	79.5	-.126	-.175	-.284	-.623	.082	.128	.141	.130
	91.0	-.025	-.048	-.146	-.432	.078	.101	.097	.044
0.382 b/2	0	-4.554	-2.365	-1.672	-1.269	- -	- -	- -	- -
	1.5	-3.004	-2.218	-1.605	-1.251	0.361	0.324	0.314	0.292
	5.5	-1.367	-2.081	-1.634	-1.255	.453	.528	.566	.577
	6.5	-1.266	-2.007	-1.569	-1.213	.434	.510	.552	.573
	11.0	-.950	-2.254	-1.571	-1.213	.375	.470	.535	.573
	14.5	-.845	-2.155	-1.502	-1.175	.336	.434	.499	.539
	21.0	-.698	-1.579	-1.523	-1.179	.277	.375	.444	.491
	24.5	-.646	-1.639	-1.445	-1.156	.245	.341	.408	.463
	31.0	-.564	-1.089	-1.388	-1.158	.201	.292	.352	.406
	34.5	-.524	-1.049	-1.319	-1.118	.174	.263	.328	.368
	41.0	-.480	-.670	-1.255	-1.118	.147	.225	.280	.320
	44.5	-.447	-.611	-1.177	-1.080	.128	.206	.253	.292
	51.0	-.388	-.413	-1.081	-1.060	.099	.168	.213	.244
	59.5	-.310	-.305	-.945	-.998	.076	.139	.160	.177
	71.0	-.197	-.190	-.739	-.927	.071	.111	.118	.097
	79.5	-.121	-.106	-.624	-.851	.071	.097	.172	.025
	91.0	-.021	-.007	-.415	-.756	.071	.086	.002	-.127
0.555 b/2	0	-2.566	-2.254	-1.125	-1.047	- -	- -	- -	- -
	1.5	-2.556	-2.041	-1.066	-.998	0.340	0.282	0.324	0.257
	5.5	-1.686	-2.070	-1.072	-1.000	.455	.503	.524	.524
	6.5	-1.428	-1.851	-1.038	-.980	.453	.507	.524	.530
	11.0	-1.231	-1.693	-1.038	-.975	.398	.472	.505	.526
	14.5	-1.027	-1.557	-.998	-.952	.359	.442	.472	.505
	21.0	-.807	-1.308	-.998	-.942	.291	.371	.411	.453
	24.5	-.730	-1.260	-.963	-.921	.260	.339	.381	.419
	31.0	-.616	-1.146	-.975	-.920	.212	.288	.324	.362
	34.5	-.577	-1.108	-.952	-.899	.182	.253	.290	.324
	41.0	-.491	-1.013	-.954	-.897	.145	.215	.240	.271
	44.5	-.459	-.975	-.923	-.878	.128	.187	.217	.238
	51.0	-.386	-.880	-.920	-.878	.101	.154	.168	.183
	59.5	-.302	-.746	-.857	-.838	.071	.111	.105	.103
	71.0	-.176	-.588	-.803	-.807	.065	.086	.046	.029
	79.5	-.103	-.487	-.735	-.762	.061	.061	-.019	-.038
	91.0	-.021	-.303	-.674	-.720	.053	.025	-.152	-.209

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TABLE IV.- CONCLUDED.

(c) α_u, 12°, 16°, 20°, 24° - Concluded.

Semi-span sta.	Percent chord	UPPER SURFACE Angle of attack 12°	16°	20°	24°	LOWER SURFACE Angle of attack 12°	16°	20°	24°
0.707 b/2	0	-1.679	-1.089	-0.851	-0.847	- -	- -	- -	- -
	1.5	-1.455	-1.020	-.826	-.813	0.264	0.267	0.240	0.152
	5.5	-1.285	-1.036	-.826	-.809	.447	.491	.495	.493
	6.5	-1.208	-.994	-.786	-.792	.436	.490	.493	.499
	11.0	-1.170	-1.003	-.786	-.788	.378	.440	.463	.488
	14.5	-1.038	-.946	-.762	-.760	.340	.408	.431	.463
	21.0	-.922	-.933	-.756	-.752	.275	.339	.371	.408
	24.5	-.788	-.880	-.731	-.733	.245	.309	.337	.370
	31.0	-.681	-.880	-.731	-.733	.195	.250	.276	.312
	34.5	-.604	-.830	-.714	-.706	.174	.225	.248	.282
	41.0	-.512	-.822	-.714	-.706	.130	.170	.191	.219
	44.5	-.470	-.777	-.695	-.695	.111	.147	.160	.183
	51.0	-.394	-.750	-.701	-.704	.076	.101	.107	.124
	59.5	-.310	-.678	-.668	-.676	.048	.053	.038	.050
	71.0	-.207	-.615	-.661	-.662	.040	.017	-.019	-.019
	79.5	-.151	-.550	-.621	-.617	.036	-.023	-.076	-.076
	91.0	-.071	-.495	-.592	-.584	.034	-.112	-.190	-.194
0.831 b/2	0	-1.851	-0.948	-0.714	-0.662	- -	- -	- -	- -
	1.5	-1.373	-.754	-.642	-.634	0.262	0.322	0.276	0.206
	5.5	-1.325	-.725	-.638	-.628	.424	.459	.463	.467
	6.5	-1.111	-.697	-.619	-.609	.415	.446	.457	.461
	11.0	-1.128	-.685	-.619	-.609	.348	.383	.410	.436
	14.5	-.933	-.653	-.600	-.590	- -	- -	- -	- -
	21.0	-.881	-.638	-.586	-.586	.243	.274	.305	.337
	24.5	-.723	-.605	-.567	-.567	.214	.246	.272	.305
	31.0	-.627	-.592	-.565	-.567	.157	.185	.210	.250
	34.5	-.535	-.563	-.543	-.552	.128	.154	.175	.202
	41.0	-.459	-.565	-.554	-.565	.090	.105	.122	.149
	44.5	-.411	-.535	-.535	-.556	.065	.078	.090	.114
	51.0	-.346	-.533	-.543	-.562	.042	.042	.048	.067
	59.5	-.283	-.495	-.512	-.543	.004	-.015	-.019	.105
	71.0	-.212	-.462	-.510	-.529	.002	-.051	-.066	.128
	79.5	-.170	-.449	-.476	-.491	.002	-.087	-.105	.086
	91.0	-.115	-.432	-.455	-.466	-.012	-.158	-.181	-.186
0.924 b/2	0	-1.688	-.583	-.546	-.533	- -	- -	- -	- -
	1.5	-1.749	-.554	-.523	-.514	0.321	0.335	0.286	0.229
	5.5	-1.723	-.544	-.520	-.510	.403	.402	.406	.408
	6.5	-1.522	-.525	-.504	-.499	.386	.383	.387	.391
	11.0	-1.545	-.516	-.504	-.501	.302	.312	.333	.354
	14.5	-1.296	-.493	-.485	-.485	.233	.253	.276	.295
	21.0	-.862	-.464	-.482	-.485	.153	.177	.200	.231
	24.5	-.818	-.449	-.459	-.470	.103	.126	.152	.175
	31.0	-.512	-.438	-.449	-.470	.071	.084	.107	.126
	34.5	-.537	-.411	-.428	-.461	.032	.046	.063	.080
	41.0	-.398	-.405	-.428	-.466	.009	.019	.029	.042
	44.5	-.436	-.379	-.409	-.453	-.012	-.007	.004	.010
	51.0	-.354	-.377	-.409	-.457	-.017	-.027	-.019	-.013
	59.5	-.369	-.339	-.371	-.438	-.035	-.057	-.038	-.063
	71.0	-.293	-.339	-.371	-.428	-.035	-.076	-.086	-.095
	79.5	-.283	-.310	-.339	-.400	-.035	-.095	-.105	-.124
	91.0	-.207	-.316	-.335	-.381	-.040	-.139	-.148	-.167

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TABLE V.- PRESSURE COEFFICIENTS AT SEVEN SEMISPAN STATIONS OF THE WING. M_0, 0.40; R, 4,000,000.

(a) α_u, 0°, 1°, 2°, 3°.

Semi-span sta.	Percent chord	UPPER SURFACE				LOWER SURFACE			
		Angle of attack				Angle of attack			
		0°	1°	2°	3°	0°	1°	2°	3°
0.086 b/2	0	0.473	0.478	0.454	0.409	- -	- -	- -	- -
	1.5	.030	-.066	-.187	-.312	-0.003	0.085	0.163	0.232
	5.5	-.039	-.087	-.141	-.200	-.045	.010	.062	.109
	6.5	-.060	-.103	-.156	-.212	-.069	-.014	.031	.079
	11.0	-.075	-.111	-.151	-.189	-.082	-.037	.005	.042
	14.5	-.092	-.123	-.158	-.194	-.093	-.051	-.014	.019
	21.0	-.104	-.125	-.157	-.189	-.103	-.065	-.034	-.004
	24.5	-.114	-.138	-.165	-.193	-.120	-.085	-.056	-.023
	31.0	-.117	-.136	-.163	-.188	-.130	-.095	-.068	-.042
	34.5	-.136	-.152	-.180	-.206	-.150	-.115	-.090	-.061
	41.0	-.156	-.172	-.193	-.218	-.160	-.129	-.104	-.078
	44.5	-.161	-.176	-.198	-.221	- -	- -	- -	- -
	51.0	-.166	-.178	-.198	-.217	-.170	-.143	-.121	-.100
	59.5	-.148	-.156	-.170	-.188	-.151	-.125	-.106	-.090
	71.0	-.118	-.124	-.134	-.149	-.119	-.099	-.083	-.066
	79.5	-.069	-.075	-.081	-.090	-.070	-.054	-.044	-.032
	91.0	-.016	-.014	-.019	-.025	-.016	-.003	.003	-.007
0.195 b/2	0	0.426	0.414	0.352	0.251	- -	- -	- -	- -
	1.5	-.015	-.139	-.281	-.443	0.020	0.143	0.243	0.324
	5.5	-.079	-.140	-.214	-.285	-.080	-.013	.054	.117
	6.5	-.096	-.155	-.215	-.285	-.100	-.039	.027	.080
	11.0	-.111	-.155	-.203	-.249	-.114	-.066	-.017	.031
	14.5	-.120	-.162	-.203	-.236	-.128	-.085	-.041	.002
	21.0	-.132	-.165	-.201	-.228	-.139	-.103	-.063	-.028
	24.5	-.138	-.168	-.201	-.224	-.144	-.112	-.072	-.039
	31.0	-.143	-.172	-.201	-.224	-.162	-.129	-.096	-.066
	34.5	-.157	-.183	-.212	-.229	-.172	-.140	-.106	-.078
	41.0	-.173	-.196	-.214	-.236	-.175	-.149	-.115	-.090
	44.5	-.178	-.202	-.216	-.238	-.172	-.147	-.117	-.092
	51.0	-.165	-.180	-.191	-.212	-.175	-.152	-.124	-.101
	59.5	-.143	-.156	-.159	-.178	-.152	-.130	-.106	-.090
	71.0	-.104	-.113	-.117	-.128	-.092	-.081	-.070	-.060
	79.5	-.049	-.055	-.057	-.066	-.047	-.040	-.030	-.018
	91.0	.011	.008	.005	.006	.008	.011	.017	.021
0.382 b/2	0	0.407	0.389	0.300	0.152	- -	- -	- -	- -
	1.5	-.042	-.191	-.370	-.566	-0.072	0.042	0.148	0.229
	5.5	-.109	-.189	-.275	-.358	-.117	-.043	.029	.092
	6.5	-.128	-.198	-.275	-.357	-.130	-.060	.008	.069
	11.0	-.138	-.189	-.240	-.297	-.141	-.086	-.031	.022
	14.5	-.141	-.189	-.238	-.274	-.151	-.103	-.060	-.005
	21.0	-.154	-.189	-.227	-.266	-.162	-.118	-.074	-.033
	24.5	-.161	-.192	-.226	-.261	-.165	-.124	-.083	-.042
	31.0	-.164	-.189	-.216	-.249	-.176	-.140	-.106	-.067
	34.5	-.164	-.188	-.213	-.238	-.181	-.150	-.115	-.081
	41.0	-.183	-.203	-.225	-.247	-.175	-.147	-.115	-.089
	44.5	-.182	-.203	-.216	-.243	-.175	-.152	-.117	-.092
	51.0	-.170	-.187	-.199	-.217	-.173	-.152	-.121	-.102
	59.5	-.152	-.162	-.169	-.182	-.144	-.127	-.098	-.078
	71.0	-.086	-.101	-.104	-.115	-.085	-.066	-.061	-.053
	79.5	-.040	-.047	-.056	-.055	-.040	-.029	-.019	-.016
	91.0	.019	.019	.017	.017	.019	.021	.029	.031
0.555 b/2	0	0.419	0.413	0.330	0.163	- -	- -	- -	- -
	1.5	-.043	-.210	-.410	-.629	-0.079	0.052	0.163	0.256
	5.5	-.113	-.203	-.296	-.396	-.114	-.032	.045	.115
	6.5	-.130	-.212	-.296	-.385	-.124	-.047	.027	.094
	11.0	-.132	-.192	-.254	-.311	-.143	-.081	-.022	.035
	14.5	-.141	-.192	-.249	-.299	-.146	-.092	-.036	.013
	21.0	-.154	-.193	-.241	-.275	-.155	-.111	-.069	-.025
	24.5	-.149	-.189	-.229	-.262	-.160	-.118	-.076	-.032
	31.0	-.155	-.189	-.216	-.250	-.167	-.134	-.095	-.055
	34.5	-.161	-.191	-.216	-.247	-.171	-.141	-.106	-.070
	41.0	-.175	-.199	-.216	-.246	-.167	-.141	-.107	-.079
	44.5	-.173	-.197	-.215	-.238	-.167	-.141	-.108	-.084
	51.0	-.160	-.182	-.191	-.211	-.160	-.140	-.109	-.090
	59.5	-.134	-.144	-.149	-.165	-.143	-.124	-.096	-.081
	71.0	-.079	-.090	-.095	-.105	-.069	-.056	-.047	-.040
	79.5	-.033	-.027	-.046	-.044	-.029	-.019	-.011	-.006
	91.0	.026	.027	.027	.028	.032	.036	.039	.042

NACA

TABLE V.- CONTINUED.

(a) α_u, 0°, 1°, 2°, 3° - Concluded.

Semi-span sta.	Percent chord	UPPER SURFACE Angle of attack 0°	1°	2°	3°	LOWER SURFACE Angle of attack 0°	1°	2°	3°
0.707 b/2	0	0.416	0.388	0.269	0.055	- -	- -	- -	- -
	1.5	-.048	-.228	-.448	-.688	-0.065	0.084	0.210	0.304
	5.5	-.127	-.221	-.324	-.433	-.120	-.032	.051	.040
	6.5	-.133	-.225	-.320	-.422	-.130	-.045	.033	.103
	11.0	-.130	-.193	-.259	-.322	-.148	-.082	-.022	.039
	14.5	-.144	-.203	-.258	-.311	-.149	-.092	-.034	.018
	21.0	-.155	-.197	-.241	-.284	-.155	-.108	-.062	-.018
	24.5	-.155	-.194	-.231	-.273	-.160	-.117	-.073	-.033
	31.0	-.161	-.193	-.218	-.256	-.166	-.129	-.092	-.055
	34.5	-.164	-.192	-.216	-.250	-.166	-.133	-.095	-.061
	41.0	-.173	-.197	-.216	-.246	-.164	-.135	-.107	-.076
	44.5	-.172	-.194	-.210	-.236	-.161	-.140	-.107	-.081
	51.0	-.159	-.178	-.186	-.204	-.159	-.141	-.113	-.092
	59.5	-.135	-.151	-.154	-.165	-.134	-.119	-.095	-.079
	71.0	-.089	-.080	-.089	-.092	-.059	-.055	-.046	-.039
	79.5	-.027	-.030	-.034	-.037	-.019	-.013	-.009	-.006
	91.0	.034	.031	.033	.033	.042	.043	.042	.042
0.831 b/2	0	0.394	0.424	0.358	0.202	- -	- -	- -	- -
	1.5	-.048	-.229	-.447	-.687	-0.059	0.091	0.201	0.299
	5.5	-.122	-.218	-.327	-.433	-.127	-.039	.157	.106
	6.5	-.125	-.217	-.322	-.419	-.132	-.047	.028	.095
	11.0	-.128	-.191	-.263	-.322	-.143	-.080	-.025	.030
	14.5	-.138	-.192	-.259	-.310	- -	- -	- -	- -
	21.0	-.146	-.182	-.236	-.274	-.154	-.107	-.074	-.032
	24.5	-.148	-.181	-.227	-.261	-.155	-.113	-.081	-.045
	31.0	-.148	-.177	-.208	-.239	-.157	-.129	-.103	-.074
	34.5	-.151	-.177	-.206	-.235	-.157	-.130	-.107	-.078
	41.0	-.168	-.189	-.213	-.235	-.156	-.136	-.115	-.090
	44.5	-.159	-.178	-.199	-.217	-.155	-.138	-.117	-.096
	51.0	-.150	-.167	-.178	-.190	-.143	-.128	-.111	-.093
	59.5	-.113	-.124	-.129	-.139	-.119	-.107	-.098	-.090
	71.0	-.054	-.061	-.060	-.078	-.044	-.043	-.048	-.044
	79.5	-.008	-.011	-.019	-.022	.003	.004	-.006	-.005
	91.0	.052	.050	.042	.044	.054	.054	.044	.044
0.924 b/2	0	0.412	0.343	0.159	-0.115	- -	- -	- -	- -
	1.5	-.007	-.186	-.421	-.676	-0.079	0.067	0.176	0.270
	5.5	-.139	-.226	-.330	-.433	-.132	-.045	.028	.101
	6.5	-.145	-.228	-.324	-.419	-.133	-.056	.017	.086
	11.0	-.139	-.192	-.262	-.306	-.145	-.088	-.044	.008
	14.5	-.146	-.192	-.248	-.274	-.151	-.106	-.067	-.022
	21.0	-.150	-.180	-.218	-.250	-.156	-.122	-.096	-.066
	24.5	-.144	-.167	-.202	-.225	-.154	-.128	-.104	-.078
	31.0	-.144	-.161	-.180	-.206	-.149	-.130	-.111	-.092
	34.5	-.136	-.154	-.176	-.194	-.144	-.125	-.114	-.098
	41.0	-.152	-.166	-.178	-.200	-.144	-.130	-.117	-.105
	44.5	-.144	-.156	-.167	-.180	-.133	-.123	-.117	-.106
	51.0	-.125	-.143	-.146	-.157	-.130	-.119	-.117	-.106
	59.5	-.085	-.081	-.100	-.104	-.095	-.087	-.084	-.081
	71.0	-.033	-.033	-.045	-.050	-.145	-.019	-.031	-.042
	79.0	.008	.008	.003	-.005	.016	.014	.004	-.005
	91.0	.054	.058	.053	.046	.066	.064	.049	.044

NACA

TABLE V.- CONTINUED.

(b) α_u, 4°, 6°, 8°, 10°.

Semi-span sta.	Percent chord	UPPER SURFACE Angle of attack 4°	6°	8°	10°	LOWER SURFACE Angle of attack 4°	6°	8°	10°
0.086 b/2	0		0.104	-0.234	-0.677		- -	- -	- -
	1.5		-.759	-1.163	-1.734		0.390	0.461	0.506
	5.5		-.383	-.518	-.694		.237	.317	.392
	6.5		-.382	-.506	-.630		.201	.279	.355
	11.0		-.322	-.413	-.509		.147	.220	.291
	14.5		-.318	-.395	-.476		.116	.190	.257
	21.0		-.296	-.361	-.425		.081	.146	.212
	24.5		-.297	-.316	-.416		.061	.124	.185
	31.0		-.274	-.331	-.385		.032	.092	.152
	34.5		-.291	-.342	-.390		.013	.072	.140
	41.0		-.296	-.344	-.385		-.006	.048	.114
	44.5		-.291	-.335	-.376		- -	- -	- -
	51.0		-.281	-.320	-.358		-.035	.014	.067
	59.5		-.238	-.269	-.303		-.034	.009	.054
	71.0		-.187	-.210	-.232		-.029	.011	.046
	79.5		-.119	-.136	-.151		-.004	.026	.056
	91.0		-.041	-.048	-.055		.023	.039	.062
0.195 b/2	0	0.100	-0.322	-0.933	-1.694	- -	- -	- -	- -
	1.5	-.618	-1.039	-1.750	-2.473	0.382	0.441	0.432	0.367
	5.5	-.361	-.526	-1.931	-.905	.169	.263	.347	.427
	6.5	-.343	-.502	-1.875	-.833	.128	.220	.300	.380
	11.0	-.303	-.416	-1.743	-.653	.072	.153	.228	.308
	14.5	-.285	-.382	-.480	-.582	.041	.117	.190	.267
	21.0	-.269	-.346	-.446	-.509	.006	.075	.141	.212
	24.5	-.263	-.333	-.405	-.479	-.005	.056	.116	.188
	31.0	-.253	-.310	-.379	-.438	-.033	.019	.080	.146
	34.5	-.262	-.314	-.375	-.426	-.053	-.001	.056	.122
	41.0	-.264	-.309	-.364	-.411	-.068	-.018	.034	.092
	44.5	-.263	-.308	-.355	-.397	-.070	-.026	.026	.080
	51.0	-.234	-.273	-.312	-.352	-.083	-.041	.008	.061
	59.5	-.197	-.225	-.259	-.286	-.075	-.040	-.001	.044
	71.0	-.143	-.163	-.187	-.208	-.049	-.018	.021	.044
	79.5	-.074	-.090	-.104	-.121	-.011	.007	.032	.058
	91.0	-.003	-.005	-.076	-.016	.026	.034	.050	.068
0.382 b/2	0	-0.068	-0.710	-1.594	-1.734	- -	- -	- -	- -
	1.5	-.784	-1.387	-2.370	-1.712	0.299	0.393	0.438	0.448
	5.5	-.453	-.664	-.900	-1.292	.164	.250	.336	.404
	6.5	-.440	-.633	-.843	-1.097	.125	.225	.308	.380
	11.0	-.362	-.496	-.648	-.929	.069	.153	.237	.308
	14.5	-.341	-.456	-.587	-.788	.037	.118	.199	.272
	21.0	-.312	-.404	-.502	-.653	.005	.078	.151	.217
	24.5	-.301	-.383	-.474	-.605	-.006	.056	.128	.188
	31.0	-.280	-.347	-.422	-.521	-.041	.018	.080	.141
	34.5	-.271	-.333	-.403	-.483	-.057	.005	.063	.126
	41.0	-.275	-.324	-.381	-.437	-.065	-.015	.042	.098
	44.5	-.269	-.311	-.364	-.409	-.072	-.027	.029	.080
	51.0	-.241	-.274	-.319	-.352	-.081	-.040	.006	.057
	59.5	-.201	-.226	-.258	-.280	-.069	-.029	.003	.044
	71.0	-.125	-.144	-.162	-.182	-.041	-.017	.010	.043
	79.5	-.063	-.076	-.090	-.103	-.006	.013	.031	.054
	91.0	.013	.007	-.002	-.006	.035	.044	.050	.058
0.555 b/2	0	-0.088	-0.831	-1.429	-1.921	- -	- -	- -	- -
	1.5	-.872	-1.659	-2.062	-2.352	0.326	0.413	0.441	0.424
	5.5	-.495	-.735	-1.204	-1.392	.173	.277	.357	.410
	6.5	-.486	-.697	-.965	-1.188	.155	.260	.339	.398
	11.5	-.389	-.540	-.771	-1.074	.088	.179	.261	.329
	14.5	-.364	-.491	-.662	-.887	.058	.143	.224	.290
	21.0	-.326	-.422	-.549	-.672	.014	.091	.163	.223
	24.5	-.303	-.393	-.504	-.606	.002	.077	.139	.195
	31.0	-.285	-.358	-.444	-.507	-.026	.034	.091	.146
	34.5	-.279	-.343	-.419	-.479	-.042	.019	.069	.123
	41.0	-.271	-.322	-.383	-.423	-.055	-.003	.045	.094
	44.5	-.260	-.309	-.362	-.399	-.060	-.012	.033	.078
	51.0	-.230	-.268	-.310	-.343	-.070	-.028	.012	.051
	59.5	-.180	-.206	-.237	-.256	-.067	-.031	-.003	.027
	71.0	-.115	-.128	-.151	-.166	-.030	-.005	.015	.037
	79.5	-.054	-.063	-.080	-.095	.001	.015	.027	.038
	91.0	.024	.019	.006	-.016	.044	.050	.049	.049

NACA

TABLE V.- CONTINUED.

(b) α_u, 4°, 6°, 8°, 10° - Concluded.

Semi-span sta.	Percent chord	UPPER SURFACE Angle of attack 4°	6°	8°	10°	LOWER SURFACE Angle of attack 4°	6°	8°	10°
0.707 b/2	0	-0.249	-1.148	-1.402	-1.626	- -	- -	- -	- -
	1.5	-.955	-1.832	-1.595	-1.601	0.368	0.062	0.418	0.380
	5.5	-.541	-.797	-1.234	-1.257	.191	.299	.367	.420
	6.5	-.525	-.761	-1.138	-1.163	.167	.274	.342	.398
	11.0	-.398	-.556	-1.032	-1.139	.089	.184	.256	.320
	14.5	-.376	-.516	-.814	-.983	.063	.153	.224	.284
	21.0	-.332	-.432	-.632	-.912	.022	.094	.160	.218
	24.5	-.315	-.406	-.538	-.755	.002	.078	.137	.191
	31.0	-.291	-.363	-.451	-.635	-.026	.038	.090	.142
	34.5	-.284	-.346	-.419	-.551	-.035	.025	.073	.122
	41.0	-.273	-.321	-.367	-.444	-.054	-.005	.039	.084
	44.5	-.260	-.302	-.347	-.406	-.061	-.017	.146	.062
	51.0	-.223	-.260	-.292	-.322	-.072	-.029	-.001	.038
	59.5	-.177	-.200	-.228	-.252	-.067	-.040	-.013	.012
	71.0	-.100	-.114	-.140	-.148	-.031	-.015	.002	.014
	79.5	-.041	-.046	-.080	-.094	.001	.007	.017	.026
	91.0	.033	.032	.004	-.010	.045	.044	.042	.038
0.831 b/2	0	-0.050	-0.903	-1.069	-1.387	- -	- -	- -	- -
	1.5	-.943	-1.810	-1.349	-1.377	0.362	0.411	0.416	0.141
	5.5	-.542	-.796	-1.230	-1.247	.174	.275	.340	.395
	6.5	-.511	-.747	-1.179	-1.149	.163	.261	.313	.380
	11.0	-.396	-.552	-1.116	-1.145	.081	.167	.239	.296
	14.5	-.371	-.509	-.974	-.999	- -	- -	- -	- -
	21.0	-.323	-.419	-.745	-.953	.007	.072	.137	.188
	24.5	-.299	-.386	-.615	-.821	-.008	.051	.107	.163
	31.0	-.270	-.336	-.439	-.689	-.041	.013	.060	.108
	34.5	-.259	-.320	-.269	-.606	-.052	-.005	.034	.080
	41.0	-.251	-.297	-.313	-.473	-.067	-.029	.009	.044
	44.5	-.236	-.273	-.293	-.438	-.078	-.044	-.012	.022
	51.0	-.203	-.236	-.245	-.328	-.078	-.056	-.026	.008
	59.5	-.147	-.167	-.195	-.270	-.078	-.063	-.042	-.017
	71.0	-.080	-.094	-.117	-.172	-.041	-.033	-.020	-.010
	79.5	-.024	-.034	-.073	-.130	-.005	-.005	-.002	-.002
	91.0	.044	.034	-.002	-.064	.044	.032	.023	- -
0.924 b/2	0	-0.483	-1.533	-1.201	-1.169	- -	- -	- -	- -
	1.5	-.960	-1.756	-1.061	-1.164	0.337	0.395	0.399	0.378
	5.5	-.533	-.772	-.963	-.969	.163	.257	.313	.356
	6.5	-.495	-.723	-.945	-.913	.150	.238	.290	.335
	11.0	-.371	-.515	-.880	-.875	.058	.137	.192	.245
	14.5	-.336	-.454	-.779	-.764	.018	.080	.131	.182
	21.0	-.286	-.364	-.674	-.692	-.032	.017	.069	.105
	24.5	-.254	-.321	-.571	-.599	-.054	-.017	.022	.058
	31.0	-.225	-.285	-.472	-.529	-.072	-.041	-.007	.030
	34.5	-.213	-.260	-.415	-.474	-.081	-.060	-.032	-.004
	41.0	-.212	-.249	-.343	-.416	-.093	-.076	-.051	-.022
	44.5	-.194	-.238	-.332	-.400	-.097	-.088	-.063	-.040
	51.0	-.165	-.202	-.281	-.352	-.099	-.089	-.066	-.046
	59.5	-.114	-.141	-.257	-.337	-.078	-.078	-.064	-.053
	71.0	-.054	-.078	-.195	-.280	-.041	-.051	-.040	-.039
	79.5	-.008	-.038	-.077	-.274	-.010	-.031	-.026	-.034
	91.0	.041	.008	-.184	-.208	.039	.002	-.003	-.032

NACA

TABLE V.- CONTINUED.

(c) α_u, 12°, 16°, 20°, 24°.

Semi-span sta.	Percent chord	UPPER SURFACE Angle of attack 12°	16°	20°	24°	LOWER SURFACE Angle of attack 12°	16°	20°	24°
0.086 b/2	0	-1.256	-2.628	-3.345	-3.083	- -	- -	- -	- -
	1.5	-2.384	-3.543	-3.350	-2.551	0.518	0.483	0.423	0.420
	5.5	-.828	-1.214	-3.117	-2.690	.454	.560	.638	.698
	6.5	-.789	-1.093	-3.037	-2.469	.416	.533	.621	.692
	11.0	-.627	-.886	-.801	-2.125	.353	.469	.567	.639
	14.5	-.321	-.799	-.735	-1.823	.318	.437	.534	.608
	21.0	-.521	-.714	-.765	-1.176	.263	.376	.467	.538
	24.5	-.505	-.679	-.746	-1.158	.239	.347	.441	.509
	31.0	-.463	-.621	-.705	-.920	.202	.306	.392	.455
	34.5	-.467	-.606	-.703	-.875	.178	.278	.363	.424
	41.0	-.454	-.578	-.692	-.872	.149	.240	.321	.376
	44.5	-.439	-.547	-.677	-.862	- -	- -	- -	- -
	51.0	-.416	-.511	-.647	-.838	.104	.189	.259	.304
	59.5	-.350	-.426	-.568	-.785	.086	.159	.216	.252
	71.0	-.275	-.333	-.470	-.709	.077	.135	.178	.196
	79.5	-.181	-.231	-.358	-.607	.078	.120	.145	.143
	91.0	-.076	-.111	-.215	-.428	.073	.094	.094	.048
0.195 b/2	0	-2.247	-2.776	-2.522	-1.677	- -	- -	- -	- -
	1.5	-2.666	-2.751	-2.435	-1.603	0.250	0.015	-0.169	-0.139
	5.5	-1.317	-2.440	-2.463	-1.595	.483	.555	.607	.644
	6.5	-2.269	-2.307	-2.441	-1.539	.443	.537	.604	.646
	11.0	-.849	-2.250	-2.672	-1.569	.376	.487	.573	.631
	14.5	-.735	-1.663	-2.392	-1.505	.329	.442	.535	.590
	21.0	-.610	-.641	-1.700	-1.464	.269	.382	.472	.536
	24.5	-.578	-.557	-1.527	-1.386	.244	.351	.437	.499
	31.0	-.522	-.514	-.963	-1.304	.194	.300	.380	.441
	34.5	-.513	-.497	-.924	-1.244	.172	.269	.344	.405
	41.0	-.478	-.503	-.710	-1.161	.138	.230	.305	.358
	44.5	-.465	-.482	-.721	-1.125	.125	.216	.282	.326
	51.0	-.406	-.443	-.627	-1.165	.099	.180	.237	.277
	59.5	-.332	-.361	-.625	-.966	.078	.146	.188	.217
	71.0	-.238	-.274	-.458	-.843	.071	.121	.148	.149
	79.5	-.149	-.167	-.350	-.756	.077	.110	.116	.093
	91.0	-.054	-.046	-.196	-.572	.075	.086	.066	-.015
0.382 b/2	0	-1.701	-1.965	-1.384	-1.149	- -	- -	- -	- -
	1.5	-1.325	-1.817	-1.342	-1.126	0.417	0.384	0.375	0.339
	5.5	-1.294	-1.778	-1.384	-1.125	.447	.519	.558	.573
	6.5	-1.187	-1.720	-1.345	-1.106	.423	.507	.551	.573
	11.0	-1.178	-1.740	-1.354	-1.105	.363	.459	.521	.557
	14.5	-1.021	-1.694	-1.300	-1.076	.323	.423	.487	.526
	21.0	-.947	-1.765	-1.327	-1.076	.268	.363	.431	.478
	24.5	-.800	-1.674	-1.282	-1.053	.240	.336	.400	.442
	31.0	-.704	-1.526	-1.281	-1.053	.191	.278	.342	.386
	34.5	-.633	-1.382	-1.232	-1.033	.168	.254	.312	.354
	41.0	-.546	-1.022	-1.193	-1.029	.137	.217	.269	.306
	44.5	-.503	-.913	-1.140	-1.009	.121	.192	.237	.271
	51.0	-.416	-.600	-1.097	-.998	.090	.157	.196	.219
	59.5	-.335	-.419	-.973	-.958	.071	.120	.143	.155
	71.0	-.224	-.242	-.831	-.910	.063	.096	.091	.073
	79.5	-.152	-.193	-.733	-.852	.063	.081	.044	-.006
	91.0	-.044	-.094	-.551	-.786	.063	.062	-.040	-.163
0.555 b/2	0	-2.330	-1.500	-1.052	-0.960	- -	- -	- -	- -
	1.5	-2.229	-1.386	-1.022	-.945	0.399	0.388	0.352	0.299
	5.5	-1.814	-1.373	-1.027	-.946	.451	.509	.524	.525
	6.5	-1.509	-1.293	-.988	-.933	.442	.502	.523	.529
	11.0	-1.472	-1.343	-.988	-.932	.381	.459	.491	.520
	14.5	-1.177	-1.256	-.957	-.912	.345	.419	.462	.492
	21.0	-.829	-1.236	-.933	-.908	.279	.352	.400	.435
	24.5	-.732	-1.158	-.914	-.888	.249	.319	.380	.406
	31.0	-.587	-1.135	-.918	-.887	.198	.265	.309	.346
	34.5	-.533	-1.071	-1.915	-.869	.173	.235	.276	.312
	41.0	-.473	-1.028	-1.917	-.864	.134	.192	.227	.256
	44.5	-.432	-.968	-1.877	-.850	.120	.165	.198	.224
	51.0	-.383	-.912	-1.875	-.845	.086	.131	.148	.169
	59.5	-.295	-.793	-1.826	-.813	.056	.079	.081	.086
	71.0	-.214	-.690	-1.789	-.792	.050	.051	.018	.005
	79.5	-.152	-.610	-1.735	-.757	.058	.011	-.049	-.068
	91.0	-.082	-.484	-1.695	-.705	.029	-.057	-.125	-.222

NACA

TABLE V.- CONCLUDED.

(c) α_u, 12°, 16°, 20°, 24° - Concluded.

Semi-span sta.	Percent chord	UPPER SURFACE Angle of attack 12°	16°	20°	24°	LOWER SURFACE Angle of attack 12°	16°	20°	24°
0.707 b/2	0	-1.647	-0.850	-0.809	-0.827	- -	- -	- -	- -
	1.5	-1.453	-.796	-.788	-.802	0.330	0.340	0.262	0.181
	5.5	-1.376	-.800	-.789	-.800	.448	.484	.488	.490
	6.5	-1.302	-.778	-.768	-.781	.435	.472	.467	.495
	11.0	-1.297	-.784	-.766	-.780	.371	.419	.453	.478
	14.5	-1.177	-.755	-.741	-.756	.338	.382	.423	.453
	21.0	-1.141	-.749	-.736	-.750	.267	.316	.359	.395
	24.5	-1.023	-.719	-.716	-.726	.238	.282	.322	.359
	31.0	-.911	-.714	-.711	-.724	.184	.227	.264	.300
	34.5	-.822	-.687	-.695	-.709	.164	.197	.234	.270
	41.0	-.632	-.685	-.695	-.710	.116	.146	.177	.205
	44.5	-.588	-.663	-.678	-.693	.097	.117	.142	.172
	51.0	-.423	-.664	-.678	-.697	.062	.075	.090	.111
	59.5	-.323	-.625	-.655	-.667	.029	.015	.018	.033
	71.0	-.202	-.597	-.647	-.651	.019	-.027	-.044	-.036
	79.5	-.154	-.553	-.614	-.611	.014	-.075	-.099	-.100
	91.0	-.082	-.519	-.580	-.579	.004	-.167	-.208	-.210
0.831 b/2	0	-1.346	-0.796	-0.690	-0.662	- -	- -	- -	- -
	1.5	-1.136	-.628	-.627	-.634	0.365	0.349	0.290	0.220
	5.5	-1.145	-.618	-.625	-.630	.428	.441	.457	.461
	6.5	-1.082	-.604	-.609	-.619	.415	.422	.448	.459
	11.0	-1.112	-.606	-.606	-.619	.335	.360	.400	.428
	14.5	-1.040	-.583	-.591	-.596	- -	- -	- -	- -
	21.0	-1.000	-.579	-.579	-.595	.223	.251	.299	.332
	24.5	-.919	-.556	-.565	-.577	.193	.216	.264	.299
	31.0	-.811	-.550	-.556	-.577	.138	.159	.198	.236
	34.5	-.751	-.532	-.544	-.564	.104	.121	.161	.195
	41.0	-.644	-.532	-.548	-.577	.067	.076	.170	.140
	44.5	-.607	-.515	-.531	-.564	.043	.044	.074	.102
	51.0	-.516	-.511	-.532	-.571	.019	.008	.030	.053
	59.5	-.438	-.483	-.508	-.547	-.018	-.052	-.026	-.025
	71.0	-.332	-.472	-.505	-.534	-.020	-.087	-.081	-.075
	79.5	-.293	-.442	-.471	-.500	-.027	-.116	-.117	-.120
	91.0	-.210	-.425	-.449	-.476	.018	-.185	-.196	-.203
0.924 b/2	0	-0.537	-0.544	-.534	-0.541	- -	- -	- -	- -
	1.5	-.775	-.523	-.519	-.525	0.379	0.340	0.293	0.226
	5.5	-.776	-.520	-.517	-.524	.379	.381	.400	.402
	6.5	-.739	-.508	-.501	-.513	.356	.359	.383	.385
	11.0	-.740	-.507	-.501	-.517	.271	.292	.328	.352
	14.5	-.685	-.489	-.483	-.501	.209	.227	.269	.295
	21.0	-.661	-.484	-.482	-.506	.128	.150	.194	.223
	24.5	-.601	-.465	-.463	-.494	.081	.099	.137	.164
	31.0	-.582	-.459	-.459	-.500	.045	.056	.092	.117
	34.5	-.522	-.436	-.437	-.488	.012	.011	.048	.064
	41.0	-.520	-.428	-.436	-.492	-.009	-.015	.014	.028
	44.5	-.474	-.407	-.413	-.483	-.030	-.040	-.018	-.010
	51.0	-.463	-.400	-.412	-.486	-.042	-.064	-.042	-.036
	59.5	-.402	-.364	-.382	-.464	-.059	-.088	-.079	-.085
	71.0	-.372	-.352	-.376	-.447	-.053	-.108	-.103	-.113
	79.0	-.320	-.316	-.348	-.418	-.063	-.122	-.125	-.144
	91.0	-.291	-.310	-.340	-.398	-.083	-.151	-.162	-.191

NACA

TABLE VI.- PRESSURE COEFFICIENTS AT SEVEN SEMISPAN STATIONS OF THE WING. M_0, 0.60; R, 4,000,000.

(a) α_u, 0°, 1°, 2°, 3°.

Semi-span sta.	Percent chord	UPPER SURFACE				LOWER SURFACE			
		Angle of attack				Angle of attack			
		0°	1°	2°	3°	0°	1°	2°	3°
0.086 b/2	0	0.500	0.505	0.486	0.446	- -	- -	- -	- -
	1.5	.059	-.040	-.152	-.283	0.013	0.099	0.174	0.240
	5.5	-.019	-.068	-.124	-.187	-.035	.023	.070	.115
	6.5	-.041	-.088	-.143	-.200	-.059	-.004	.040	.082
	11.0	-.060	-.097	-.140	-.183	-.071	-.026	.013	.048
	14.5	-.081	-.113	-.154	-.195	-.086	-.044	-.008	.027
	21.0	-.092	-.121	-.158	-.190	-.097	-.057	-.027	.002
	24.5	-.107	-.133	-.167	-.200	-.112	-.073	-.045	-.016
	31.0	-.113	-.139	-.169	-.197	-.125	-.088	-.060	-.038
	34.5	-.138	-.160	-.190	-.218	-.143	-.109	-.082	-.058
	41.0	-.158	-.178	-.206	-.232	-.155	-.123	-.099	-.072
	44.5	-.170	-.189	-.216	-.241	- -	- -	- -	- -
	51.0	-.173	-.189	-.212	-.235	-.177	-.145	-.126	-.104
	59.5	-.150	-.164	-.180	-.205	-.159	-.131	-.115	-.100
	71.0	-.120	-.128	-.141	-.160	-.127	-.098	-.088	-.077
	79.5	-.066	-.070	-.082	-.096	-.070	-.052	-.044	-.036
	91.0	-.010	-.010	-.020	-.027	-.012	.005	.004	.006
0.195 b/2	0	0.445	0.436	0.386	0.294	- -	- -	- -	- -
	1.5	.010	-.112	-.254	-.420	0.027	0.152	0.247	0.324
	5.5	-.064	-.129	-.201	-.280	-.072	-.001	.061	.116
	6.5	-.086	-.144	-.209	-.283	-.090	-.026	.031	.081
	11.0	-.102	-.146	-.200	-.257	-.107	-.054	.008	.034
	14.5	-.116	-.153	-.200	-.249	-.124	-.074	-.031	.006
	21.0	-.132	-.164	-.202	-.234	-.138	-.093	-.055	-.024
	24.5	-.140	-.170	-.207	-.234	-.145	-.104	-.068	-.034
	31.0	-.151	-.175	-.208	-.234	-.162	-.126	-.095	-.063
	34.5	-.162	-.188	-.219	-.249	-.176	-.141	-.110	-.082
	41.0	-.182	-.204	-.230	-.257	-.182	-.150	-.118	-.094
	44.5	-.188	-.208	-.231	-.257	-.182	-.151	-.120	-.100
	51.0	-.176	-.190	-.215	-.237	-.185	-.160	-.133	-.115
	59.5	-.155	-.170	-.171	-.197	-.160	-.137	-.112	-.098
	71.0	-.101	-.111	-.127	-.145	-.098	-.079	-.075	-.064
	79.5	-.049	-.054	-.063	-.078	-.049	-.037	-.029	-.026
	91.0	.013	.017	.008	.003	.011	.022	.024	.026
0.382 b/2	0	0.422	0.404	0.321	0.183	- -	- -	- -	- -
	1.5	-.037	-.185	-.365	-.577	-0.061	0.057	0.155	0.235
	5.5	-.107	-.186	-.276	-.373	-.111	-.033	.038	.099
	6.5	-.126	-.198	-.282	-.370	-.125	-.048	.015	.072
	11.0	-.137	-.190	-.247	-.309	-.140	-.078	-.023	.026
	14.5	-.143	-.190	-.245	-.294	-.149	-.094	-.045	-.004
	21.0	-.158	-.197	-.238	-.287	-.160	-.114	-.074	-.033
	24.5	-.164	-.198	-.237	-.280	-.167	-.123	-.082	-.042
	31.0	-.170	-.198	-.231	-.271	-.181	-.141	-.104	-.072
	34.5	-.170	-.197	-.226	-.264	-.186	-.149	-.113	-.086
	41.0	-.190	-.212	-.239	-.272	-.181	-.147	-.113	-.093
	44.5	-.190	-.210	-.234	-.264	-.182	-.153	-.122	-.100
	51.0	-.174	-.191	-.210	-.234	-.182	-.156	-.127	-.108
	59.5	-.156	-.167	-.178	-.205	-.152	-.116	-.103	-.087
	71.0	-.078	-.094	-.111	-.123	-.086	-.071	-.060	-.052
	79.5	-.037	-.041	-.052	-.057	-.031	-.021	-.014	-.011
	91.0	.029	.028	.023	.019	.030	.038	.038	.040
0.555 b/2	0	0.428	0.423	0.341	0.183	- -	- -	- -	- -
	1.5	-.041	-.214	-.428	-.666	-0.067	0.065	0.172	0.261
	5.5	-.116	-.214	-.312	-.412	-.113	-.024	.051	.124
	6.5	-.131	-.214	-.313	-.412	-.124	-.039	.030	.098
	11.0	-.143	-.198	-.274	-.338	-.146	-.071	-.020	.035
	14.5	-.150	-.200	-.267	-.324	-.150	-.091	-.037	.020
	21.0	-.161	-.203	-.253	-.301	-.161	-.110	-.067	-.025
	24.5	-.158	-.196	-.245	-.285	-.165	-.120	-.081	-.038
	31.0	-.165	-.196	-.230	-.271	-.176	-.136	-.102	-.063
	34.5	-.169	-.196	-.230	-.265	-.180	-.141	-.104	-.077
	41.0	-.184	-.209	-.237	-.266	-.176	-.141	-.112	-.085
	44.5	-.184	-.204	-.223	-.257	-.173	-.142	-.113	-.092
	51.0	-.169	-.189	-.212	-.219	-.169	-.139	-.117	-.096
	59.5	-.143	-.151	-.159	-.175	-.150	-.123	-.104	-.091
	71.0	-.076	-.086	-.104	-.112	-.057	-.055	-.052	-.041
	79.5	-.026	-.032	-.044	-.047	-.022	-.013	-.011	-.005
	91.0	.038	.039	.030	.029	.038	.046	.045	.043

NACA

TABLE VI.- CONTINUED.

(a) α_u, 0°, 1°, 2°, 3° - Concluded.

Semi-span sta.	Percent chord	UPPER SURFACE Angle of attack 0°	1°	2°	3°	LOWER SURFACE Angle of attack 0°	1°	2°	3°
0.707 b/2	0	0.424	0.400	0.282	0.079	- -	- -	- -	- -
	1.5	-.049	-.235	-.471	-.732	-0.056	0.100	0.222	0.310
	5.5	-.131	-.228	-.342	-.442	-.120	-.024	.060	.131
	6.5	-.139	-.233	-.341	-.449	-.128	-.039	.038	.109
	11.0	-.131	-.197	-.276	-.345	-.150	-.077	-.017	.041
	14.5	-.150	-.207	-.274	-.338	-.154	-.088	-.034	.020
	21.0	-.158	-.203	-.253	-.308	-.158	-.106	-.065	-.021
	24.5	-.161	-.201	-.251	-.294	-.161	-.116	-.075	-.036
	31.0	-.169	-.200	-.237	-.277	-.169	-.129	-.096	-.056
	34.5	-.173	-.200	-.237	-.271	-.173	-.133	-.097	-.067
	41.0	-.184	-.204	-.237	-.264	-.169	-.136	-.104	-.083
	44.5	-.180	-.199	-.230	-.260	-.169	-.137	-.112	-.092
	51.0	-.161	-.182	-.200	-.219	-.165	-.138	-.118	-.100
	59.5	-.139	-.151	-.163	-.175	-.139	-.118	-.104	-.091
	71.0	-.064	-.074	-.089	-.099	-.056	-.047	-.051	-.042
	79.5	-.019	-.021	-.030	-.034	-.011	-.002	-.007	-.004
	91.0	.045	.049	.044	.042	.053	.058	.052	.049
0.831 b/2	0	0.399	0.436	0.373	0.222	- -	- -	- -	- -
	1.5	-.058	-.242	-.475	-.740	-0.060	0.096	0.216	0.304
	5.5	-.138	-.233	-.349	-.438	-.133	.037	.043	.112
	6.5	-.139	-.232	-.337	-.442	-.137	-.045	.033	.101
	11.0	-.140	-.203	-.280	-.350	-.150	-.077	-.020	.033
	14.5	-.150	-.206	-.274	-.337	- -	- -	- -	- -
	21.0	-.162	-.203	-.248	-.301	-.164	-.112	-.072	-.024
	24.5	-.164	-.197	-.244	-.271	-.165	-.119	-.081	-.047
	31.0	-.166	-.193	-.222	-.262	-.173	-.135	-.104	-.076
	34.5	-.170	-.191	-.214	-.251	-.173	-.136	-.110	-.084
	41.0	-.182	-.197	-.219	-.248	-.170	-.142	-.118	-.096
	44.5	-.175	-.186	-.207	-.232	-.169	-.143	-.122	-.108
	51.0	-.164	-.173	-.185	-.203	-.155	-.132	-.115	-.106
	59.5	-.125	-.128	-.132	-.143	-.132	-.113	-.101	-.094
	71.0	-.057	-.059	-.073	-.078	-.045	-.031	-.045	-.046
	79.5	-.008	-.007	-.015	-.018	.001	.011	0	-.004
	91.0	.056	.060	.055	.052	.060	.066	.057	.050
0.924 b/2	0	0.418	0.343	0.165	-0.108	- -	- -	- -	- -
	1.5	-.013	-.203	-.452	-.746	-0.080	0.073	0.191	0.280
	5.5	-.151	-.244	-.355	-.460	-.140	-.045	.036	.104
	6.5	-.162	-.247	-.348	-.458	-.143	-.059	.025	.091
	11.0	-.155	-.210	-.280	-.336	-.158	-.092	-.037	.013
	14.5	-.166	-.209	-.262	-.307	-.166	-.111	-.067	-.025
	21.0	-.169	-.196	-.230	-.271	-.170	-.130	-.098	-.071
	24.5	-.162	-.181	-.214	-.242	-.166	-.132	-.110	-.088
	31.0	-.157	-.173	-.193	-.223	-.162	-.135	-.118	-.100
	34.5	-.151	-.164	-.176	-.207	-.155	-.130	-.118	-.107
	41.0	-.166	-.173	-.189	-.210	-.155	-.134	-.122	-.114
	44.5	-.156	-.165	-.175	-.193	-.147	-.128	-.121	-.117
	51.0	-.135	-.137	-.152	-.164	-.140	-.122	-.118	-.114
	59.5	-.080	-.077	-.096	-.107	-.091	-.085	-.084	-.084
	71.0	-.025	-.031	-.038	-.046	-.024	-.015	-.016	-.033
	79.5	.011	.020	.012	.003	.019	.021	.009	-.002
	91.0	.062	.071	.064	.055	.071	.073	.061	.049

NACA

TABLE VI.- CONTINUED.

(b) α_u, 4°, 6°, 8°, 10°.

Semi-span sta.	Percent chord	UPPER SURFACE Angle of attack 4°	6°	8°	10°	LOWER SURFACE Angle of attack 4°	6°	8°	10°
0.086 b/2	0	0.390	0.203	-0.061	-0.403	- -	- -	- -	- -
	1.5	-.412	-.716	-1.095	-1.768	0.302	0.401	0.482	0.531
	5.5	-.235	-.365	-.499	-.660	.163	.245	.331	.403
	6.5	-.250	-.368	-.490	-.643	.132	.210	.294	.365
	11.0	-.222	-.320	-.412	-.533	.090	.157	.233	.300
	14.5	-.221	-.317	-.400	-.510	.066	.130	.203	.268
	21.0	-.220	-.297	-.370	-.465	.039	.093	.162	.220
	24.5	-.229	-.300	-.369	-.458	.020	.070	.140	.195
	31.0	-.223	-.299	-.350	-.432	-.007	.045	.107	.159
	34.5	-.245	-.299	-.366	-.442	-.026	.025	.082	.133
	41.0	-.256	-.312	-.366	-.433	-.045	.003	.059	.107
	44.5	-.262	-.315	-.366	-.430	- -	- -	- -	- -
	51.0	-.254	-.303	-.348	-.405	-.078	-.035	.020	.060
	59.5	-.218	-.260	-.295	-.343	-.077	-.040	.012	.050
	71.0	-.169	-.200	-.227	-.267	-.057	-.027	.018	.046
	79.5	-.102	-.126	-.145	-.174	-.020	-.001	.033	.054
	91.0	-.029	-.043	-.050	-.070	.017	.024	.049	.059
0.195 b/2	0	0.172	-0.189	-0.615	-0.991	- -	- -	- -	- -
	1.5	-.587	-1.017	-1.549	-1.717	0.386	0.452	0.468	0.445
	5.5	-.378	-.524	-.702	-1.403	.174	.263	.355	.427
	6.5	-.337	-.507	-.666	-1.177	.135	.223	.312	.384
	11.0	-.300	-.425	-.543	-.667	.082	.157	.239	.311
	14.5	-.286	-.397	-.500	-.579	.052	.119	.200	.269
	21.0	-.278	-.367	-.448	-.525	.015	.076	.150	.212
	24.5	-.273	-.356	-.433	-.505	.001	.060	.128	.185
	31.0	-.267	-.339	-.406	-.471	-.028	.022	.086	.143
	34.5	-.277	-.343	-.403	-.466	-.049	.001	.067	.117
	41.0	-.278	-.343	-.392	-.451	-.066	-.021	.042	.089
	44.5	-.278	-.337	-.383	-.445	-.072	-.027	.031	.076
	51.0	-.254	-.302	-.345	-.396	-.087	-.049	.007	.051
	59.5	-.226	-.250	-.283	-.321	-.078	-.043	.004	.038
	71.0	-.153	-.182	-.215	-.232	-.049	-.026	.012	.040
	79.5	-.080	-.101	-.119	-.135	-.013	.002	.033	.053
	91.0	.002	-.009	-.015	-.027	.032	.038	.055	.062
0.382 b/2	0	-0.005	-0.538	-0.915	-1.192	- -	- -	- -	- -
	1.5	-.798	-1.453	-1.574	-1.510	0.304	0.394	0.448	0.470
	5.5	-.462	-.699	-1.073	-1.141	.158	.254	.340	.393
	6.5	-.452	-.657	-.895	-1.061	.134	.224	.313	.372
	11.0	-.375	-.526	-.774	-1.028	.075	.158	.243	.305
	14.5	-.353	-.485	-.652	-.851	.046	.124	.214	.268
	21.0	-.330	-.434	-.558	-.813	.011	.078	.155	.219
	24.5	-.319	-.413	-.522	-.706	-.005	.059	.136	.185
	31.0	-.301	-.382	-.469	-.629	-.041	.017	.087	.140
	34.5	-.292	-.364	-.442	-.558	-.051	.002	.069	.118
	41.0	-.293	-.354	-.411	-.491	-.064	-.015	.045	.091
	44.5	-.284	-.339	-.387	-.453	-.072	-.027	.029	.073
	51.0	-.250	-.301	-.339	-.389	-.084	-.043	.006	.047
	59.5	-.208	-.243	-.268	-.306	-.068	-.038	.005	.038
	71.0	-.130	-.154	-.151	-.203	-.035	-.020	.014	.044
	79.5	-.061	-.079	-.091	-.127	.001	-.010	.034	.048
	91.0	.022	.010	.002	-.027	.046	.044	.055	.061
0.555 b/2	0	-0.034	-0.595	-0.960	-1.368	- -	- -	- -	- -
	1.5	-.919	-1.470	-1.317	-1.526	0.334	0.417	0.459	0.469
	5.5	-.521	-.831	-1.346	-1.406	.181	.277	.358	.415
	6.5	-.514	-.736	-1.319	-1.389	.158	.257	.339	.398
	11.0	-.412	-.572	-1.290	-1.389	.091	.180	.263	.327
	14.5	-.388	-.527	-1.207	-1.321	.062	.144	.225	.288
	21.0	-.350	-.456	-.765	-1.227	.018	.093	.164	.219
	24.5	-.327	-.425	-.619	-1.088	.003	.070	.140	.195
	31.0	-.307	-.388	-.355	-.807	-.029	.029	.094	.145
	34.5	-.299	-.369	-.327	-.694	-.042	.011	.075	.123
	41.0	-.292	-.351	-.527	-.412	-.057	-.009	.048	.091
	44.5	-.278	-.332	-.506	-.375	-.063	-.018	.035	.074
	51.0	-.249	-.292	-.283	-.260	-.071	-.033	.016	.051
	59.5	-.190	-.218	-.203	-.188	-.071	-.040	-.001	.026
	71.0	-.117	-.137	-.131	-.117	-.029	-.012	.016	.030
	79.5	-.050	-.063	-.057	-.066	.003	.011	.032	.038
	91.0	.032	.019	.028	.008	.048	.045	.058	.049

NACA

TABLE VI.- CONTINUED.

(b) α_u, 4°, 6°, 8°, 10° - Concluded.

Semi-span sta.	Percent chord	UPPER SURFACE				LOWER SURFACE			
		Angle of attack				Angle of attack			
		4°	6°	8°	10°	4°	6°	8°	10°
0.707 b/2	0	-0.188	-0.773	-0.979	-1.256	- -	- -	- -	- -
	1.5	-1.024	-1.430	-1.091	-1.163	0.379	0.432	0.454	0.436
	5.5	-.572	-1.084	-1.089	-1.140	.201	.297	.369	.420
	6.5	-.557	-.923	-1.074	-1.117	.172	.270	.345	.398
	11.0	-.425	-.619	-1.089	-1.124	.097	.183	.259	.319
	14.5	-.403	-.542	-1.077	-1.091	.069	.152	.227	.283
	21.0	-.353	-.462	-1.055	-1.101	.024	.095	.164	.215
	24.5	-.337	-.432	-1.016	-1.056	.004	.076	.141	.188
	31.0	-.311	-.388	-.856	-1.027	-.021	.033	.093	.138
	34.5	-.299	-.367	-.793	-.977	-.034	.019	.076	.117
	41.0	-.286	-.336	-.511	-.888	-.055	-.011	.043	.079
	44.5	-.272	-.316	-.467	-.839	-.063	-.025	.025	.059
	51.0	-.234	-.270	-.246	-.686	-.078	-.041	.001	.030
	59.5	-.181	-.218	-.158	-.528	-.071	-.049	-.012	.004
	71.0	-.100	-.114	-.084	-.260	-.034	-.022	-.004	.012
	79.5	-.034	-.048	-.030	-.173	.003	.003	.025	.019
	91.0	.045	.024	.034	-.030	.052	.042	.061	.037
0.831 b/2	0	0.004	-0.496	-0.587	-0.816	- -	- -	- -	- -
	1.5	-1.024	-1.310	-.858	-.844	0.375	0.423	0.443	0.433
	5.5	-.576	-1.086	-.857	-.842	.182	.274	.340	.384
	6.5	-.547	-.979	-.826	-.809	.171	.262	.325	.371
	11.0	-.422	-.719	-.826	-.804	.092	.171	.238	.290
	14.5	-.399	-.578	-.789	-.765	- -	- -	- -	- -
	21.0	-.340	-.444	-.799	-.747	.013	.077	.139	.180
	24.5	-.319	-.401	-.761	-.705	-.002	.057	.113	.149
	31.0	-.286	-.349	-.760	-.697	-.034	.011	.062	.096
	34.5	-.272	-.326	-.710	-.655	-.051	-.009	.038	.068
	41.0	-.261	-.298	-.672	-.654	-.068	-.038	.006	.031
	44.5	-.241	-.275	-.621	-.611	-.080	-.053	-.013	.010
	51.0	-.207	-.239	-.540	-.592	-.081	-.063	-.025	-.010
	59.5	-.145	-.167	-.440	-.523	-.078	-.069	-.045	-.040
	71.0	-.075	-.092	-.293	-.461	-.034	-.034	-.018	-.031
	79.5	-.013	-.038	-.222	-.403	.003	-.002	.002	-.032
	91.0	.057	.030	-.096	-.313	.053	.036	.026	-.053
0.924 b/2	0	-0.459	-1.012	-0.762	-0.792	- -	- -	- -	- -
	1.5	-1.055	-1.167	-.649	-.651	0.350	0.402	0.415	0.411
	5.5	-.577	-1.024	-.632	-.636	.173	.257	.307	.345
	6.5	-.546	-.959	-.608	-.613	.161	.242	.289	.327
	11.0	-.400	-.726	-.596	-.605	.069	.137	.193	.234
	14.5	-.361	-.593	-.561	-.567	.021	.081	.130	.170
	21.0	-.301	-.408	-.535	-.541	-.031	.013	.059	.093
	24.5	-.267	-.350	-.491	-.497	-.057	-.017	.018	.046
	31.0	-.238	-.292	-.466	-.471	-.075	-.049	-.011	.011
	34.5	-.221	-.274	-.422	-.429	-.084	-.069	-.035	-.020
	41.0	-.220	-.239	-.410	-.411	-.094	-.078	-.052	-.042
	44.5	-.200	-.239	-.370	-.377	-.098	-.090	-.064	-.058
	51.0	-.170	-.204	-.370	-.373	-.097	-.091	-.070	-.067
	59.5	-.111	-.161	-.315	-.325	-.070	-.077	-.064	-.077
	71.0	-.046	-.097	-.309	-.329	-.031	-.040	-.043	-.069
	79.5	-.001	-.072	-.278	-.293	-.002	-.019	-.038	-.077
	91.0	.050	.012	-.257	-.304	.049	.022	-.047	-.115

NACA

TABLE VI.- CONTINUED.

(c) α_u, 12°, 16°, 20°, 24°.

Semi-span sta.	Percent chord	UPPER SURFACE Angle of attack 12°	16°	20°	24°	LOWER SURFACE Angle of attack 12°	16°	20°	24°
0.086 b/2	0	-0.742	-1.311	-1.790	-1.973	- -	- -	- -	- -
	1.5	-1.997	-2.198	-2.364	-1.771	0.566	0.590	0.585	0.596
	5.5	-.812	-2.157	-2.665	-1.840	.473	.580	.665	.733
	6.5	-.818	-2.167	-2.694	-1.726	.435	.547	.641	.715
	11.0	-.652	-.660	-1.355	-1.680	.368	.478	.575	.651
	14.5	-.627	-.640	-.639	-1.503	.333	.440	.538	.619
	21.0	-.560	-.681	-.745	-1.250	.282	.379	.475	.558
	24.5	-.550	-.648	-.765	-1.178	.254	.354	.443	.517
	31.0	-.512	-.615	-.706	-.960	.215	.309	.394	.460
	34.5	-.520	-.607	-.708	-.962	.190	.280	.358	.430
	41.0	-.505	-.590	-.723	-.857	.158	.245	.318	.380
	44.5	-.496	-.572	-.721	-.855	- -	- -	- -	- -
	51.0	-.462	-.548	-.696	-.810	.110	.185	.249	.305
	59.5	-.388	-.475	-.639	-.780	.094	.157	.208	.250
	71.0	-.300	-.384	-.555	-.740	.081	.130	.165	.192
	79.5	-.200	-.270	-.443	-.690	.080	.114	.126	.128
	91.0	-.083	-.147	-.286	-.556	.074	.080	.061	.013
0.195 b/2	0-	-1.363	-1.977	-1.846	-1.341	- -	- -	- -	- -
	1.5	-1.848	-2.028	-1.740	-1.280	0.395	0.266	0.171	0.127
	5.5	-1.849	-2.121	-1.799	-1.266	.485	.567	.628	.673
	6.5	-1.876	-2.142	-1.787	-1.231	.444	.538	.609	.662
	11.0	-1.422	-2.307	-1.843	-1.233	.370	.481	.568	.636
	14.5	-.752	-2.299	-1.722	-1.199	.329	.437	.522	.595
	21.0	-.511	-1.066	-1.611	-1.192	.269	.373	.463	.535
	24.5	-.499	-.530	-1.504	-1.151	.241	.344	.427	.499
	31.0	-.512	-.415	-1.335	-1.113	.196	.293	.371	.440
	34.5	-.503	-.426	-1.241	-1.076	.168	.263	.336	.404
	41.0	-.497	-.514	-1.042	-1.031	.138	.222	.292	.353
	44.5	-.482	-.540	-1.020	-1.002	.124	.202	.267	.324
	51.0	-.438	-.534	-.842	-.961	.093	.166	.220	.271
	59.5	-.353	-.453	-.742	-.919	.077	.132	.171	.203
	71.0	-.252	-.349	-.600	-.876	.102	.105	.122	.132
	79.5	-.146	-.240	-.519	-.838	.106	.092	.082	.061
	91.0	-.029	-.103	-.355	-.731	.106	.067	.016	-.071
0.382 b/2	0	-1.590	-1.560	-1.190	-0.996	- -	- -	- -	- -
	1.5	-1.617	-1.415	-1.154	-.981	0.478	0.466	0.446	0.418
	5.5	-1.442	-1.402	-1.153	-.980	.453	.526	.564	.589
	6.5	-1.433	-1.367	-1.128	-.968	.427	.506	.552	.583
	11.0	-1.443	-1.422	-1.127	-.967	.363	.454	.514	.560
	14.5	-1.400	-1.446	-1.097	-.949	.325	.418	.478	.530
	21.0	-1.443	-1.513	-1.096	-.946	.267	.357	.420	.475
	24.5	-1.327	-1.448	-1.067	-.931	.231	.324	.387	.442
	31.0	-1.129	-1.402	-1.071	-.927	.189	.271	.329	.377
	34.5	-.974	-1.317	-1.045	-.915	.165	.243	.298	.350
	41.0	-.613	-1.210	-1.038	-.914	.133	.204	.251	.298
	44.5	-.525	-1.134	-1.000	-.902	.115	.178	.220	.261
	51.0	-.300	-1.016	-.978	-.899	.085	.138	.174	.206
	59.5	-.229	-.872	-.919	-.879	.068	.104	.115	.132
	71.0	-.154	-.603	-.859	-.860	.058	.073	.057	.045
	79.5	-.086	-.468	-.799	-.836	.066	.056	0	-.034
	91.0	-.002	-.240	-.707	-.804	.074	.025	-.121	-.197
0.555 b/2	0	-1.402	-1.131	-0.945	-0.894	- -	- -	- -	- -
	1.5	-1.311	-1.026	-.910	-.866	0.466	0.444	0.402	0.354
	5.5	-1.210	-1.014	-.910	-.867	.455	.503	.522	.532
	6.5	-1.222	-.992	-.888	-.859	.441	.491	.516	.531
	11.0	-1.204	-1.001	-.891	-.866	.376	.442	.481	.516
	14.5	-1.192	-.971	-.871	-.859	.335	.403	.446	.500
	21.0	-1.189	-.963	-.862	-.853	.269	.337	.384	.430
	24.5	-1.153	-.935	-.845	-.845	.241	.303	.351	.396
	31.0	-1.139	-.944	-.840	-.840	.189	.250	.294	.337
	34.5	-1.095	-.920	-.824	-.831	.165	.221	.256	.301
	41.0	-1.044	-.927	-.819	-.826	.130	.176	.208	.245
	44.5	-.992	-.898	-.805	-.816	.111	.151	.174	.212
	51.0	-.906	-.891	-.804	-.811	.082	.110	.124	.151
	59.5	-.736	-.826	-.774	-.788	.051	.058	.052	.066
	71.0	-.468	-.768	-.755	-.769	.049	.020	-.017	-.015
	79.5	-.340	-.699	-.721	-.740	.046	-.027	-.092	-.094
	91.0	-.127	-.617	-.690	-.711	.046	-.126	-.226	-.242

NACA

TABLE VI.- CONCLUDED.

(c) α_u, 12°, 16°, 20°, 24° - Concluded.

Semi-span sta.	Percent chord	UPPER SURFACE Angle of attack 12°	16°	20°	24°	LOWER SURFACE Angle of attack 12°	16°	20°	24°
0.707 b/2	0	-1.095	-0.864	-0.789	-0.752	- -	- -	- -	- -
	1.5	-.914	-.794	-.761	-.775	0.426	0.367	0.302	0.224
	5.5	-.909	-.798	-.763	-.776	.450	.476	.487	.490
	6.5	-.884	-.771	-.753	-.774	.430	.467	.482	.495
	11.0	-.885	-.770	-.752	- -	.357	.409	.443	.474
	14.5	-.849	-.739	-.733	-.760	.321	.373	.409	.446
	21.0	-.837	-.728	-.727	-.754	.254	.304	.345	.383
	24.5	-.803	-.703	-.710	-.739	.224	.273	.309	.351
	31.0	-.792	-.697	-.705	-.737	.173	.214	.248	.290
	34.5	-.756	-.676	-.690	-.725	.147	.185	.216	.255
	41.0	-.756	-.676	-.689	-.721	.103	.130	.157	.192
	44.5	-.716	-.658	-.675	-.710	.082	.101	.122	.157
	51.0	-.705	-.661	-.673	-.707	.046	.052	.066	.093
	59.5	-.636	-.635	-.647	-.683	.007	-.012	-.012	.009
	71.0	-.582	-.625	-.635	-.668	-.007	-.059	-.076	-.068
	79.5	-.518	-.591	-.598	-.635	-.034	-.110	-.133	-.132
	91.0	-.445	-.560	-.566	-.608	-.092	-.206	-.233	-.247
0.831 b/2	0	-0.803	-0.765	-0.705	-0.697	- -	- -	- -	- -
	1.5	-.701	-.615	-.636	-.670	0.419	0.406	0.308	0.229
	5.5	-.696	-.617	-.639	-.673	.410	.435	.449	.489
	6.5	-.678	-.606	-.626	-.661	.398	.422	.448	.483
	11.0	-.671	-.604	-.623	-.661	.320	.358	.392	.421
	14.5	-.636	-.585	-.607	-.645	- -	- -	- -	- -
	21.0	-.621	-.577	-.600	-.643	.209	.248	.285	.322
	24.5	-.582	-.560	-.584	-.630	.179	.212	.251	.288
	31.0	-.566	-.555	-.581	-.631	.121	.148	.181	.220
	34.5	-.535	-.536	-.563	-.620	.089	.110	.142	.178
	41.0	-.528	-.535	-.565	-.626	.046	.057	.082	.116
	44.5	-.499	-.519	-.551	-.615	.015	.020	.043	.073
	51.0	-.492	-.518	-.551	-.617	-.013	-.018	-.002	.020
	59.5	-.451	-.489	-.526	-.597	-.059	-.080	-.073	-.062
	71.0	-.438	-.488	-.514	-.579	-.081	-.117	-.122	-.123
	79.5	-.411	-.461	-.474	-.548	-.102	-.144	-.156	-.168
	91.0	-.395	-.443	-.457	-.520	-.211	-.205	-.225	-.252
0.924 b/2	0	-0.600	-0.537	-0.550	-0.603	- -	- -	- -	- -
	1.5	-.527	-.520	-.536	-.591	0.403	0.351	0.299	0.222
	5.5	-.520	-.518	-.535	-.591	.365	.383	.394	.394
	6.5	-.498	-.504	-.529	-.582	.345	.393	.378	.377
	11.0	-.491	-.503	-.530	-.582	.259	.297	.323	.342
	14.5	-.459	-.484	-.504	-.570	.195	.227	.261	.286
	21.0	-.445	-.479	-.505	-.573	.114	.143	.178	.206
	24.5	-.411	-.461	-.490	-.566	.066	.089	.118	.141
	31.0	-.394	-.453	-.489	-.574	.028	.040	.068	.088
	34.5	-.361	-.432	-.477	-.569	-.010	-.007	.012	.024
	41.0	-.355	-.422	-.472	-.570	-.037	-.039	-.025	-.016
	44.5	-.326	-.402	-.457	-.563	-.059	-.068	-.059	-.060
	51.0	-.330	-.398	-.458	-.562	-.077	-.092	-.087	-.089
	59.5	-.296	-.363	-.429	-.541	-.097	-.119	-.129	-.146
	71.0	-.303	-.361	-.419	-.518	-.105	-.133	-.149	-.169
	79.5	-.279	-.335	-.390	-.485	-.113	-.148	-.171	-.201
	91.0	-.295	-.339	-.372	-.455	-.146	-.183	-.206	-.240

NACA

TABLE VII.- PRESSURE COEFFICIENTS AT SEVEN SEMISPAN STATIONS OF THE WING. M_o, 0.80; R, 4,000,000.

(a) α_u, 0°, 1°, 2°, 3°.

Semi-span sta.	Percent chord	UPPER SURFACE				LOWER SURFACE			
		Angle of attack				Angle of attack			
		0°	1°	2°	3°	0°	1°	2°	3°
0.086 b/2	0	0.530	0.539	0.524	0.496	- -	- -	- -	- -
	1.5	.088	0	-.101	-.220	0.050	0.129	0.192	0.259
	5.5	.003	-.040	-.095	-.152	-.010	.045	.089	.133
	8.5	-.024	-.065	-.120	-.173	-.036	.019	.060	.100
	11.0	-.056	-.080	-.129	-.170	-.054	-.010	.027	.061
	14.5	-.075	-.109	-.150	-.191	-.072	-.030	.004	.040
	21.0	-.091	-.120	-.160	-.194	-.089	-.050	-.020	.013
	24.5	-.106	-.135	-.171	-.209	-.110	-.070	-.040	-.010
	31.0	-.118	-.141	-.179	-.210	-.130	-.090	-.064	-.032
	34.5	-.150	-.174	-.210	-.241	-.153	-.118	-.090	-.060
	41.0	-.175	-.200	-.232	-.265	-.184	-.140	-.111	-.081
	44.5	-.195	-.219	-.251	-.280	- -	- -	- -	- -
	51.0	-.206	-.229	-.260	-.289	-.205	-.171	-.150	-.120
	59.5	-.190	-.204	-.230	-.250	-.191	-.163	-.142	-.120
	71.0	-.155	-.168	-.189	-.202	-.160	-.132	-.115	-.097
	79.5	-.090	-.095	-.111	-.126	-.095	-.071	-.062	-.050
	91.0	-.022	-.020	-.031	-.040	-.022	-.010	-.008	0
0.195 b/2	0	0.467	0.453	0.416	0.351	- -	- -	- -	- -
	1.5	.025	-.089	-.223	-.373	0.055	0.160	0.253	0.330
	5.5	-.055	-.120	-.190	-.263	-.060	.003	.065	.123
	8.5	-.080	-.141	-.206	-.275	-.083	-.023	.035	.089
	11.0	-.100	-.150	-.200	-.250	-.100	-.052	-.005	.042
	14.5	-.115	-.162	-.210	-.255	-.121	-.080	-.035	.010
	21.0	-.140	-.180	-.220	-.259	-.141	-.103	-.062	-.020
	24.5	-.152	-.193	-.230	-.263	-.157	-.120	-.080	-.039
	31.0	-.168	-.203	-.240	-.262	-.180	-.150	-.110	-.070
	34.5	-.188	-.224	-.258	-.280	-.200	-.170	-.137	-.093
	41.0	-.212	-.249	-.278	-.300	-.210	-.185	-.144	-.110
	44.5	-.220	-.256	-.285	-.310	-.213	-.190	-.150	-.119
	51.0	-.203	-.238	-.265	-.283	-.223	-.200	-.167	-.137
	59.5	-.184	-.210	-.237	-.241	-.193	-.170	-.140	-.119
	71.0	-.148	-.152	-.154	-.180	-.150	-.117	-.100	-.080
	79.5	-.060	-.072	-.085	-.095	-.062	-.057	-.045	-.030
	91.0	.012	.007	.001	0	.010	.012	.020	.027
0.382 b/2	0	0.425	0.410	0.350	0.241	- -	- -	- -	- -
	1.5	-.033	-.186	-.365	-.573	-0.060	0.050	0.145	0.230
	5.5	-.117	-.203	-.295	-.393	-.121	-.048	.025	.095
	8.5	-.135	-.219	-.306	-.393	-.135	-.063	.005	.069
	11.0	-.153	-.218	-.280	-.336	-.153	-.095	-.038	.019
	14.5	-.162	-.220	-.278	-.322	-.170	-.115	-.062	-.010
	21.0	-.182	-.232	-.278	-.320	-.185	-.140	-.092	-.046
	24.5	-.194	-.241	-.284	-.322	-.192	-.152	-.105	-.057
	31.0	-.200	-.244	-.278	-.315	-.211	-.175	-.130	-.089
	34.5	-.203	-.240	-.273	-.309	-.220	-.187	-.145	-.103
	41.0	-.227	-.262	-.291	-.322	-.217	-.183	-.145	-.110
	44.5	-.230	-.261	-.289	-.314	-.220	-.189	-.155	-.120
	51.0	-.210	-.240	-.258	-.280	-.220	-.193	-.164	-.135
	59.5	-.183	-.210	-.215	-.231	-.180	-.150	-.127	-.106
	71.0	-.093	-.112	-.132	-.143	-.094	-.091	-.075	-.063
	79.5	-.041	-.052	-.060	-.065	-.037	-.030	-.020	-.017
	91.0	.032	.028	.021	.025	.035	.040	.042	.042
0.555 b/2	0	0.432	0.430	0.361	0.240	- -	- -	- -	- -
	1.5	-.050	-.225	-.450	-.708	-0.080	0.057	0.169	0.258
	5.5	-.136	-.231	-.349	-.462	-.130	-.041	.040	.110
	8.5	-.154	-.249	-.354	-.460	-.143	-.060	.020	.089
	11.0	-.161	-.233	-.311	-.379	-.170	-.101	-.033	.027
	14.5	-.171	-.237	-.309	-.371	-.177	-.113	-.053	0
	21.0	-.191	-.241	-.301	-.350	-.190	-.139	-.088	-.040
	24.5	-.190	-.236	-.290	-.330	-.200	-.150	-.102	-.051
	31.0	-.198	-.235	-.280	-.320	-.210	-.169	-.122	-.081
	34.5	-.201	-.239	-.280	-.311	-.214	-.175	-.129	-.090
	41.0	-.220	-.251	-.286	-.316	-.211	-.173	-.136	-.103
	44.5	-.219	-.248	-.271	-.300	-.207	-.175	-.138	-.110
	51.0	-.200	-.225	-.246	-.270	-.199	-.171	-.140	-.115
	59.5	-.168	-.190	-.185	-.201	-.171	-.149	-.122	-.108
	71.0	-.082	-.099	-.116	-.120	-.075	-.071	-.060	-.050
	79.5	-.031	-.035	-.042	-.044	-.024	-.017	-.010	-.010
	91.0	.048	.046	.040	.042	.050	.051	.053	.050

NACA

TABLE VII.- CONTINUED.

(a) α_u, 0°, 1°, 2°, 3° - Concluded.

Semi-span eta.	Percent chord	UPPER SURFACE Angle of attack 0°	1°	2°	3°	LOWER SURFACE Angle of attack 0°	1°	2°	3°
	0	0.429	0.408	0.306	0.141	- -	- -	- -	- -
	1.5	-.059	-.259	-.516	-.801	-0.067	0.091	0.219	0.309
	5.5	-.152	-.264	-.390	-.486	-.141	-.041	.051	.128
	6.5	-.160	-.270	-.389	-.510	-.151	-.059	.030	.103
	11.0	-.159	-.231	-.319	-.390	-.180	-.102	-.030	.030
	14.5	-.178	-.243	-.320	-.388	-.181	-.113	-.049	.010
	21.0	-.190	-.243	-.300	-.356	-.190	-.136	-.080	-.031
	24.5	-.191	-.242	-.292	-.342	-.199	-.148	-.094	-.050
0.707 b/2	31.0	-.200	-.241	-.280	-.321	-.206	-.161	-.114	-.072
	34.5	-.202	-.241	-.271	-.315	-.208	-.168	-.119	-.082
	41.0	-.213	-.248	-.279	-.307	-.201	-.170	-.129	-.100
	44.5	-.212	-.240	-.267	-.290	-.201	-.171	-.138	-.110
	51.0	-.192	-.219	-.231	-.250	-.198	-.171	-.141	-.120
	59.5	-.164	-.182	-.187	-.191	-.167	-.149	-.120	-.106
	71.0	-.070	-.082	-.095	-.095	-.060	-.061	-.058	-.050
	79.5	-.018	-.020	-.028	-.022	-.011	-.008	-.003	-.009
	91.0	.058	.059	.059	.059	.061	.063	.060	.057
	0	0.409	0.448	0.390	0.266	- -	- -	- -	- -
	1.5	-.064	-.268	-.530	-.816	-.072	.092	.220	.310
	5.5	-.159	-.272	-.403	-.484	-.154	-.053	.040	.114
	6.5	-.161	-.268	-.394	-.500	-.156	-.058	.030	.104
	11.0	-.164	-.237	-.331	-.400	-.185	-.095	-.030	.031
	14.5	-.180	-.243	-.325	-.390	- -	- -	- -	- -
	21.0	-.190	-.241	-.297	-.350	-.192	-.139	-.086	-.037
	24.5	-.199	-.240	-.290	-.330	-.195	-.149	-.100	-.050
0.831 b/2	31.0	-.200	-.233	-.265	-.300	-.205	-.168	-.128	-.090
	34.5	-.202	-.230	-.253	-.280	-.207	-.173	-.140	-.101
	41.0	-.209	-.230	-.256	-.270	-.200	-.177	-.148	-.120
	44.5	-.202	-.218	-.236	-.246	-.197	-.177	-.153	-.132
	51.0	-.182	-.200	-.208	-.215	-.178	-.159	-.140	-.127
	59.5	-.141	-.145	-.139	-.139	-.147	-.134	-.115	-.106
	71.0	-.050	-.055	-.067	-.063	-.038	-.041	-.047	-.045
	79.5	.004	.007	0	.003	.015	.015	.008	.006
	91.0	.075	.075	.075	.077	.080	.080	.071	.068
	0	0.426	0.352	0.182	-0.059	- -	- -	- -	- -
	1.5	-.012	-.230	-.508	-.856	-0.090	0.070	0.200	0.289
	5.5	-.175	-.287	-.419	-.582	-.164	-.060	.030	.108
	6.5	-.189	-.294	-.413	-.550	-.170	-.068	.020	.097
	11.0	-.189	-.258	-.340	-.400	-.190	-.117	-.050	.010
	14.5	-.204	-.260	-.324	-.361	-.205	-.145	-.089	-.039
	21.0	-.204	-.241	-.273	-.303	-.212	-.170	-.132	-.096
	24.5	-.190	-.220	-.240	-.270	-.200	-.174	-.145	-.118
0.924 b/2	31.0	-.185	-.203	-.219	-.247	-.191	-.169	-.148	-.127
	34.5	-.172	-.190	-.206	-.227	-.180	-.160	-.146	-.130
	41.0	-.185	-.200	-.215	-.227	-.172	-.159	-.149	-.135
	44.5	-.170	-.187	-.194	-.203	-.162	-.152	-.145	-.135
	51.0	-.150	-.160	-.162	-.170	-.155	-.142	-.136	-.130
	59.5	-.080	-.078	-.098	-.100	-.097	-.098	-.090	-.089
	71.0	-.022	-.025	-.030	-.030	-.012	-.017	-.008	-.028
	79.0	.025	.031	.027	.021	.034	.030	.021	.011
	91.0	.080	.085	.081	.075	.092	.089	.079	.068

TABLE VII.- CONTINUED.

(b) α_u, 4°, 6°, 8°, 10°.

Semi-span sta.	Percent chord	UPPER SURFACE Angle of attack 4°	6°	8°	10°	LOWER SURFACE Angle of attack 4°	6°	8°	10°
0.086 b/2	0	0.459	0.339	0.179	0.010	- -	- -	- -	- -
	1.5	-.240	-.609	-.946	-1.320	0.317	0.410	0.491	0.557
	5.5	-.210	-.319	-.445	-.580	.180	.259	.340	.411
	6.5	-.226	-.330	-.449	-.544	.141	.220	.301	.371
	11.0	-.210	-.300	-.396	-.497	.100	.170	.244	.310
	14.5	-.230	-.318	-.411	-.510	.069	.141	.211	.278
	21.0	-.229	-.309	-.390	-.480	.046	.107	.170	.230
	24.5	-.239	-.320	-.408	-.497	.025	.082	.146	.201
	31.0	-.241	-.319	-.399	-.485	-.001	.051	.110	.167
	34.5	-.278	-.351	-.439	-.530	-.030	.029	.085	.140
	41.0	-.299	-.370	-.452	-.552	-.054	0	.058	.109
	44.5	-.315	-.386	-.470	-.560	- -	- -	- -	- -
	51.0	-.320	-.386	-.461	-.555	-.095	-.041	.011	.060
	59.5	-.280	-.337	-.400	-.470	-.100	-.051	0	.043
	71.0	-.220	-.260	-.302	-.344	-.080	-.040	.001	.039
	79.5	-.140	-.167	-.191	-.220	-.039	-.010	.020	.048
	91.0	-.048	-.061	-.080	-.099	.005	.020	.038	.049
0.195 b/2	0	0.259	0.038	-0.201	0.397	- -	- -	- -	- -
	1.5	-.545	-.927	-1.247	-1.345	0.383	0.462	0.497	0.509
	5.5	-.349	-.478	-.820	-1.230	.173	.269	.343	.417
	6.5	-.350	-.491	-.682	-1.150	.140	.226	.308	.374
	11.0	-.300	-.423	-.567	-.900	.080	.163	.237	.295
	14.5	-.300	-.409	-.543	-.752	.043	.125	.191	.261
	21.0	-.303	-.395	-.509	-.587	.007	.083	.146	.210
	24.5	-.310	-.398	-.513	-.618	-.010	.062	.121	.182
	31.0	-.311	-.389	-.491	-.577	-.044	.021	.077	.150
	34.5	-.329	-.403	-.502	-.597	-.070	-.002	.051	.109
	41.0	-.345	-.417	-.513	-.608	-.088	-.028	.025	.080
	44.5	-.350	-.418	-.509	-.610	-.097	-.039	.012	.067
	51.0	-.319	-.379	-.453	-.518	-.120	-.062	-.012	.036
	59.5	-.268	-.310	-.369	-.403	-.103	-.052	-.014	.028
	71.0	-.198	-.223	-.265	-.278	-.070	-.033	-.007	.022
	79.5	-.106	-.123	-.157	-.163	-.030	-.001	.016	.038
	91.0	-.007	-.013	-.033	-.037	.020	.034	.041	.049
0.382 b/2	0	0.099	-0.201	-0.466	-0.713	- -	- -	- -	- -
	1.5	-.816	-1.317	-1.360	-1.390	0.289	0.388	0.441	0.479
	5.5	-.479	-.813	-1.120	-1.288	.142	.245	.320	.385
	6.5	-.479	-.630	-1.077	-1.363	.120	.219	.290	.358
	11.0	-.418	-.597	-.933	-1.257	.060	.153	.223	.290
	14.5	-.402	-.539	-.792	-1.224	.030	.118	.187	.252
	21.0	-.388	-.504	-.695	-1.156	-.009	.075	.140	.200
	24.5	-.380	-.485	-.638	-1.061	-.023	.049	.111	.174
	31.0	-.365	-.458	-.588	-.886	-.063	.008	.069	.125
	34.5	-.354	-.435	-.550	-.750	-.080	-.010	.044	.102
	41.0	-.361	-.429	-.517	-.580	-.090	-.025	.022	.075
	44.5	-.350	-.410	-.482	-.502	-.102	-.041	.004	.057
	51.0	-.309	-.355	-.420	-.399	-.116	-.060	-.020	.027
	59.5	-.256	-.281	-.323	-.305	-.091	-.050	-.019	.019
	71.0	-.157	-.170	-.207	-.192	-.059	-.027	-.004	.020
	79.5	-.075	-.070	-.112	-.120	-.012	.010	.019	.035
	91.0	.020	.014	-.010	-.010	.039	.047	.043	.052
0.555 b/2	0	0.080	-0.229	-0.309	-0.747	- -	- -	- -	- -
	1.5	-.999	-1.294	-1.321	-1.291	0.320	0.409	0.454	0.480
	5.5	-.545	-1.102	-1.340	-1.297	.169	.269	.340	.400
	6.5	-.579	-1.022	-1.318	-1.270	.150	.246	.320	.381
	11.0	-.471	-.785	-1.269	-1.285	.079	.171	.246	.311
	14.5	-.451	-.661	-1.230	-1.256	.050	.138	.210	.281
	21.0	-.413	-.542	-1.091	-1.261	.001	.082	.150	.210
	24.5	-.387	-.502	-1.016	-1.223	-.016	.060	.125	.181
	31.0	-.364	-.454	-.740	-1.193	-.050	.019	.078	.132
	34.5	-.356	-.433	-.621	-1.150	-.062	.001	.060	.112
	41.0	-.350	-.409	-.390	-1.024	-.080	-.020	.031	.080
	44.5	-.331	-.380	-.345	-.960	-.083	-.030	-.020	.061
	51.0	-.291	-.331	-.300	-.710	-.093	-.046	-.003	.035
	59.5	-.216	-.240	-.220	-.470	-.090	-.051	-.020	.018
	71.0	-.129	-.141	-.139	-.208	-.041	-.020	0	.020
	79.5	-.050	-.060	-.062	-.146	-.002	.010	.019	.036
	91.0	.040	.031	.028	-.040	.049	.050	.049	.055

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TABLE VII.- CONTINUED.

(b) α_u, 4°, 6°, 8°, 10° - Concluded.

Semi-span sta.	Percent chord	UPPER SURFACE Angle of attack 4°	6°	8°	10°	LOWER SURFACE Angle of attack 4°	6°	8°	10°
0.707 b/2	0	-0.049	-0.375	-0.653	-0.851	- -	- -	- -	- -
	1.5	-1.164	-1.230	-1.100	-.937	0.369	0.434	0.458	0.466
	5.5	-.656	-1.172	-1.109	-.937	.189	.289	.354	.410
	6.5	-.631	-1.166	-1.080	-.910	.161	.261	.331	.389
	11.0	-.490	-.960	-1.093	-.900	.082	.180	.248	.309
	14.5	-.460	-.840	-1.058	-.861	.060	.157	.214	.272
	21.0	-.420	-.630	-1.060	-.844	.009	.090	.150	.209
	24.5	-.398	-.554	-1.027	-.809	-.009	.070	.129	.180
	31.0	-.369	-.449	-.988	-.794	-.040	.026	.079	.129
	34.5	-.354	-.411	-.942	-.764	-.052	.010	.060	.109
	41.0	-.338	-.369	-.841	-.752	-.076	-.020	.025	.065
	44.5	-.312	-.340	-.800	-.712	-.089	-.037	.006	.041
	51.0	-.268	-.289	-.630	-.700	-.100	-.059	-.020	.009
	59.5	-.200	-.210	-.462	-.640	-.092	-.065	-.040	-.027
	71.0	-.100	-.110	-.169	-.581	-.047	-.030	-.020	-.027
	79.5	-.028	-.039	-.091	-.510	-.008	0	.001	-.036
	91.0	.059	.041	.019	-.400	.050	.047	.041	-.060
0.831 b/2	0	0.098	-0.193	-0.376	-0.516	- -	- -	- -	- -
	1.5	-1.174	-1.099	-.814	-.689	0.368	0.425	0.449	0.453
	5.5	-.706	-1.089	-.813	-.690	.176	.270	.333	.381
	6.5	-.610	-1.060	-.789	-.661	.167	.257	.322	.370
	11.0	-.502	-.990	-.771	-.659	.085	.170	.235	.287
	14.5	-.467	-.917	-.740	-.622	- -	- -	- -	- -
	21.0	-.408	-.754	-.720	-.609	0	.073	.134	.180
	24.5	-.375	-.672	-.681	-.575	-.017	.049	.104	.150
	31.0	-.332	-.500	-.674	-.565	-.057	0	.050	.088
	34.5	-.308	-.435	-.634	-.540	-.078	-.030	.020	.052
	41.0	-.289	-.321	-.630	-.537	-.098	-.059	-.018	.011
	44.5	-.261	-.289	-.589	-.510	-.114	-.080	-.041	-.021
	51.0	-.221	-.230	-.569	-.505	-.114	-.089	-.059	-.049
	59.5	-.145	-.160	-.502	-.469	-.100	-.090	-.074	-.089
	71.0	-.063	-.083	-.440	-.455	-.047	-.042	-.044	-.090
	79.5	0	-.025	-.379	-.422	0	-.003	-.028	-.103
	91.0	.074	.046	-.270	-.400	.058	.045	-.023	-.157
0.924 b/2	0	-0.317	-0.642	-0.700	-0.650	- -	- -	- -	- -
	1.5	-1.221	-.885	-.643	-.530	0.346	0.400	0.422	0.427
	5.5	-.679	-.873	-.647	-.537	.170	.253	.310	.347
	6.5	-.559	-.827	-.621	-.512	.155	.240	.296	.330
	11.0	-.481	-.808	-.610	-.509	.060	.135	.193	.235
	14.5	-.410	-.740	-.575	-.484	.006	.073	.130	.174
	21.0	-.330	-.703	-.553	-.476	-.060	-.008	.045	.081
	24.5	-.294	-.628	-.514	-.451	-.091	-.055	-.009	-.027
	31.0	-.264	-.540	-.488	-.439	-.110	-.083	-.041	-.018
	34.5	-.245	-.476	-.448	-.416	-.120	-.103	-.070	-.058
	41.0	-.240	-.379	-.430	-.400	-.127	-.113	-.089	-.083
	44.5	-.218	-.350	-.395	-.372	-.129	-.120	-.101	-.106
	51.0	-.179	-.270	-.388	-.361	-.124	-.115	-.105	-.119
	59.5	-.110	-.227	-.340	-.322	-.082	-.085	-.091	-.128
	71.0	-.038	-.140	-.332	-.319	-.033	-.042	-.070	-.121
	79.5	.010	-.131	-.300	-.291	0	-.013	-.070	-.123
	91.0	.060	-.057	-.309	-.310	.057	.031	-.093	-.150

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TABLE VII.- CONTINUED.

(c) α_u, 12°, 16°, 20°, 24°.

Semi-span sta.	Percent chord	UPPER SURFACE Angle of attack 12°	16°	20°	24°	LOWER SURFACE Angle of attack 12°	16°	20°	24°
0.086 b/2	0	-0.151	-0.439			- -	- -		
	1.5	-1.400	-1.545			0.601	0.670		
	5.5	-.880	-1.520			.480	.596		
	6.5	-.819	-1.530			.440	.559		
	11.0	-.569	-.892			.372	.490		
	14.5	-.601	-.561			.339	.450		
	21.0	-.571	-.690			.288	.391		
	24.5	-.571	-.690			.259	.361		
	31.0	-.562	-.671			.220	.317		
	34.5	-.619	-.689			.190	.286		
	41.0	-.648	-.569			.155	.247		
	44.5	-.660	-.476			- -	- -		
	51.0	-.649	-.541			.101	.180		
	59.5	-.492	-.723			.089	.147		
	71.0	-.362	-.548			.069	.111		
	79.5	-.250	-.433			.065	.089		
	91.0	-.131	-.286			.050	.033		
0.195 b/2	0	-0.585	-0.905			- -	- -		
	1.5	-1.435	-1.584			0.506	0.471		
	5.5	-1.408	-1.596			.480	.578		
	6.5	-1.430	-1.630			.439	.541		
	11.0	-1.303	-1.620			.370	.480		
	14.5	-1.220	-1.642			.326	.436		
	21.0	-.685	-1.579			.268	.374		
	24.5	-.590	-1.492			.238	.341		
	31.0	-.620	-.211			.191	.292		
	34.5	-.642	-.210			.162	.259		
	41.0	-.687	-.542			.130	.219		
	44.5	-.671	-.747			.112	.196		
	51.0	-.492	-.787			.078	.152		
	59.5	-.399	-.625			.060	.116		
	71.0	-.307	-.571			.050	.080		
	79.5	-.206	-.451			.050	.050		
	91.0	-.071	-.285			.043	0		
0.382 b/2	0	-0.913	-1.149			- -	- -		
	1.5	-1.470	-1.032			0.504	0.528		
	5.5	-1.392	-1.038			.437	.522		
	6.5	-1.437	-1.014			.413	.501		
	11.0	-1.394	-1.050			.350	.443		
	14.5	-1.385	-1.030			.310	.404		
	21.0	-1.350	-1.018			.254	.344		
	24.5	-1.280	-.962			.226	.312		
	31.0	-1.186	-.970			.172	.257		
	34.5	-1.101	-.955			.158	.227		
	41.0	-.925	-.971			.118	.180		
	44.5	-.797	-.943			.094	.156		
	51.0	-.528	-.915			.060	.112		
	59.5	-.442	-.859			.042	.070		
	71.0	-.300	-.797			.030	.025		
	79.5	-.217	-.738			.034	-.012		
	91.0	-.090	-.620			.033	-.096		
0.555 b/2	0	-0.939	-0.999			- -	- -		
	1.5	-1.078	-.859			0.497	0.485		
	5.5	-1.070	-.870			.442	.491		
	6.5	-1.040	-.877			.425	.479		
	11.0	-1.036	-.890			.359	.422		
	14.5	-1.001	-.880			.320	.381		
	21.0	-.988	-.871			.251	.318		
	24.5	-.955	-.850			.220	.281		
	31.0	-.947	-.843			.163	.226		
	34.5	-.914	-.829			.149	.198		
	41.0	-.901	-.819			.109	.150		
	44.5	-.862	-.800			.089	.120		
	51.0	-.838	-.791			.054	.077		
	59.5	-.760	-.759			.017	.011		
	71.0	-.680	-.732			.005	-.039		
	79.5	-.601	-.696			-.010	-.094		
	91.0	-.468	-.649			-.053	-.210		

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TABLE VII.- CONCLUDED.

(c) α_u, 12°, 16°, 20°, 24° - Concluded.

Semi-span sta.	Percent chord	UPPER SURFACE Angle of attack 12°	16°	20°	24°	LOWER SURFACE Angle of attack 12°	16°	20°	24°
0.707 b/2	0	-0.930	-0.871			- -	- -		
	1.5	-.820	-.761			0.452	0.407		
	5.5	-.818	-.759			.438	.464		
	6.5	-.800	-.745			.418	.450		
	11.0	-.799	-.750			.341	.388		
	14.5	-.780	-.732			.308	.350		
	21.0	-.772	-.730			.239	.281		
	24.5	-.751	-.711			.206	.249		
	31.0	-.740	-.708			.151	.183		
	34.5	-.717	-.690			.128	.159		
	41.0	-.700	-.687			.079	.100		
	44.5	-.678	-.668			.051	.068		
	51.0	-.659	-.665			.011	.013		
	59.5	-.612	-.640			-.040	-.061		
	71.0	-.580	-.629			-.070	-.119		
	79.5	-.538	-.599			-.110	-.173		
	91.0	-.496	-.559			-.181	-.260		
0.831 b/2	0	-0.641	-0.761			- -	- -		
	1.5	-.665	-.630			0.435	0.386		
	5.5	-.660	-.631			.399	.422		
	6.5	-.641	-.620			.388	.411		
	11.0	-.639	-.622			.310	.343		
	14.5	-.615	-.606			- -	- -		
	21.0	-.605	-.600			.195	.230		
	24.5	-.576	-.580			.170	.188		
	31.0	-.570	-.578			.099	.126		
	34.5	-.548	-.560			.060	.081		
	41.0	-.544	-.560			.010	.021		
	44.5	-.521	-.545			-.030	-.021		
	51.0	-.519	-.549			-.065	-.071		
	59.5	-.483	-.530			-.121	-.149		
	71.0	-.470	-.526			-.142	-.189		
	79.5	-.449	-.500			-.159	-.216		
	91.0	-.423	-.480			-.210	-.274		
0.924 b/2	0	-0.612	-0.557			- -	- -		
	1.5	-.528	-.536			0.407	0.360		
	5.5	-.525	-.537			.357	.373		
	6.5	-.510	-.523			.340	.359		
	11.0	-.507	-.521			.250	.282		
	14.5	-.482	-.507			.184	.219		
	21.0	-.476	-.502			.091	.122		
	24.5	-.455	-.488			.030	.058		
	31.0	-.445	-.486			-.020	-.001		
	34.5	-.421	-.470			-.067	-.062		
	41.0	-.415	-.469			-.100	-.104		
	44.5	-.391	-.451			-.129	-.145		
	51.0	-.390	-.455			-.146	-.170		
	59.5	-.350	-.431			-.159	-.204		
	71.0	-.355	-.431			-.160	-.219		
	79.5	-.331	-.410			-.164	-.231		
	91.0	-.341	-.400			-.193	-.260		

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TABLE VIII.- PRESSURE COEFFICIENTS AT SEVEN SEMISPAN STATIONS OF THE WING. M_o, 0.83; R, 4,000,000.

(a) α_u, 0°, 1°, 2°, 3°.

Semi-span sta.	Percent chord	UPPER SURFACE				LOWER SURFACE			
		Angle of attack				Angle of attack			
		0°	1°	2°	3°	0°	1°	2°	3°
0.086 b/2	0	0.535		0.530	0.505	- -		- -	- -
	1.5	.087		-.098	-.206	0.052		0.198	0.260
	5.5	.004		-.091	-.145	-.007		.091	.137
	6.5	-.026		-.118	-.169	-.033		.062	.106
	11.0	-.048		-.125	-.162	-.053		.030	.067
	14.5	-.075		-.146	-.187	-.073		.007	.041
	21.0	-.092		-.153	-.190	-.090		-.015	.015
	24.5	-.111		-.171	-.205	-.110		-.037	-.007
	31.0	-.122		-.178	-.213	-.131		-.063	-.033
	34.5	-.157		-.216	-.248	-.156		-.088	-.057
	41.0	-.185		-.240	-.275	-.179		-.110	-.082
	44.5	-.210		-.265	-.297	- -		- -	- -
	51.0	-.220		-.272	-.303	-.209		-.149	-.121
	59.5	-.204		-.246	-.270	-.218		-.158	-.136
	71.0	-.169		-.197	-.216	-.181		-.128	-.110
	79.5	-.101		-.123	-.136	-.109		-.069	-.058
	91.0	-.030		-.038	-.049	-.030		-.012	-.007
0.195 b/2	0	0.467		0.427	0.361	- -		- -	- -
	1.5	.025		-.216	-.364	0.067		0.256	0.330
	5.5	-.060		-.211	-.260	-.066		.070	.127
	6.5	-.082		-.203	-.272	-.089		.035	.091
	11.0	-.105		-.198	-.250	-.109		-.002	.041
	14.5	-.127		-.211	-.260	-.131		-.035	.010
	21.0	-.150		-.225	-.265	-.150		-.065	-.024
	24.5	-.166		-.238	-.274	-.167		-.083	-.040
	31.0	-.181		-.245	-.280	-.193		-.111	-.074
	34.5	-.203		-.256	-.297	-.213		-.135	-.097
	41.0	-.230		-.293	-.320	-.231		-.152	-.115
	44.5	-.242		-.303	-.331	-.237		-.161	-.125
	51.0	-.230		-.282	-.302	-.248		-.180	-.150
	59.5	-.207		-.251	-.259	-.218		-.153	-.130
	71.0	-.165		-.165	-.190	-.173		-.109	-.090
	79.5	-.074		-.090	-.100	-.073		-.052	-.040
	91.0	-.002		.001	-.004	0		.015	.020
0.382 b/2	0	0.421		0.351	0.250	- -		- -	- -
	1.5	-.043		-.369	-.575	-0.072		0.140	0.227
	5.5	-.129		-.300	-.400	-.133		.020	.089
	6.5	-.150		-.310	-.400	-.148		0	.063
	11.0	-.169		-.290	-.352	-.169		-.041	.010
	14.5	-.180		-.290	-.352	-.186		-.070	-.018
	21.0	-.202		-.291	-.330	-.203		-.100	-.053
	24.5	-.213		-.298	-.340	-.213		-.112	-.065
	31.0	-.225		-.295	-.335	-.234		-.141	-.099
	34.5	-.227		-.292	-.330	-.246		-.151	-.120
	41.0	-.251		-.312	-.345	-.239		-.150	-.127
	44.5	-.253		-.310	-.338	-.240		-.162	-.135
	51.0	-.230		-.279	-.300	-.242		-.173	-.150
	59.5	-.201		-.230	-.249	-.200		-.139	-.117
	71.0	-.106		-.140	-.151	-.104		-.084	-.070
	79.5	-.053		-.064	-.070	-.047		-.023	-.019
	91.0	.027		.023	.024	.029		.042	.041
0.555 b/2	0	0.429		0.361	0.246	- -		- -	- -
	1.5	-.059		-.459	-.720	-0.089		0.160	0.249
	5.5	-.147		-.355	-.480	-.140		.037	.103
	6.5	-.165		-.364	-.480	-.155		.017	.065
	11.0	-.172		-.324	-.395	-.182		-.040	.020
	14.5	-.186		-.322	-.395	-.190		-.056	-.008
	21.0	-.204		-.315	-.370	-.205		-.093	-.049
	24.5	-.204		-.305	-.350	-.213		-.110	-.060
	31.0	-.210		-.295	-.338	-.225		-.131	-.091
	34.5	-.218		-.293	-.332	-.230		-.139	-.103
	41.0	-.235		-.303	-.335	-.223		-.142	-.112
	44.5	-.231		-.291	-.321	-.220		-.144	-.119
	51.0	-.215		-.257	-.282	-.210		-.148	-.124
	59.5	-.179		-.190	-.211	-.184		-.130	-.114
	71.0	-.090		-.120	-.125	-.081		-.064	-.059
	79.5	-.031		-.047	-.049	-.022		-.013	-.010
	91.0	.046		.040	.041	.050		.055	.049

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TABLE VIII.- CONTINUED.

(a) α_u, 0°, 1°, 2°, 3° - Concluded.

Semi-span sta.	Percent chord	UPPER SURFACE Angle of attack 0°	1°	2°	3°	LOWER SURFACE Angle of attack 0°	1°	2°	3°
0.707 b/2	0	0.427		0.301	0.150	- -		- -	- -
	1.5	-.062		-.530	-.828	-0.072		0.214	0.301
	5.5	-.161		-.408	-.530	-.151		.049	.121
	6.5	-.171		-.409	-.531	-.161		.028	.097
	11.0	-.165		-.330	-.409	-.190		-.036	.027
	14.5	-.189		-.337	-.411	-.193		-.051	.001
	21.0	-.202		-.318	-.378	-.200		-.085	-.040
	24.5	-.204		-.309	-.361	-.209		-.100	-.059
	31.0	-.212		-.290	-.345	-.218		-.120	-.081
	34.5	-.215		-.288	-.321	-.218		-.123	-.091
	41.0	-.229		-.291	-.324	-.211		-.132	-.110
	44.5	-.222		-.278	-.308	-.211		-.141	-.120
	51.0	-.201		-.241	-.260	-.208		-.149	-.129
	59.5	-.171		-.190	-.200	-.173		-.124	-.115
	71.0	-.071		-.098	-.098	-.060		-.059	-.057
	79.5	-.015		-.026	-.022	-.010		-.005	-.010
	91.0	.060		.057	.060	.067		.063	.057
0.831 b/2	0	0.406		0.386	0.270	- -		- -	- -
	1.5	-.068		-.549	-.844	-0.077		0.218	0.307
	5.5	-.163		-.420	-.571	-.165		.037	.213
	6.5	-.166		-.406	-.525	-.167		.029	.102
	11.0	-.170		-.345	-.429	-.181		-.032	.030
	14.5	-.186		-.338	-.412	-.193		- -	- -
	21.0	-.199		-.310	-.373	-.200		-.090	-.043
	24.5	-.207		-.307	-.352	-.207		-.102	-.057
	31.0	-.209		-.276	-.317	-.217		-.131	-.097
	34.5	-.215		-.265	-.295	-.219		-.142	-.112
	41.0	-.223		-.258	-.280	-.211		-.150	-.131
	44.5	-.212		-.240	-.256	-.203		-.158	-.142
	51.0	-.192		-.211	-.219	-.183		-.145	-.132
	59.5	-.149		-.140	-.143	-.151		-.119	-.112
	71.0	-.050		-.064	-.064	-.038		-.048	-.047
	79.5	.008		.003	.003	.015		.010	.005
	91.0	.078		.079	.084	.082		.076	.067
0.924 b/2	0	0.425		0.179	-0.056	- -		- -	- -
	1.5	-.018		-.525	-.891	-0.100		0.199	0.287
	5.5	-.183		-.438	-.617	-.172		.032	.107
	6.5	-.197		-.433	-.584	-.178		.022	.096
	11.0	-.199		-.360	-.433	-.200		-.051	.006
	14.5	-.220		-.344	-.383	-.221		-.093	-.036
	21.0	-.219		-.282	-.310	-.225		-.140	-.103
	24.5	-.207		-.239	-.278	-.214		-.153	-.130
	31.0	-.193		-.227	-.252	-.201		-.158	-.137
	34.5	-.180		-.212	-.232	-.187		-.150	-.139
	41.0	-.191		-.220	-.233	-.180		-.153	-.147
	44.5	-.180		-.198	-.209	-.170		-.148	-.144
	51.0	-.155		-.162	-.170	-.160		-.138	-.137
	59.5	-.080		-.099	-.101	-.097		-.092	-.090
	71.0	-.022		-.026	-.030	-.012		-.003	-.029
	79.5	.030		.030	.027	.034		.025	.012
	91.0	.083		.089	.079	.095		.081	.070

TABLE VIII.- CONTINUED.

(b) α_u, 4°, 6°, 8°, 10°.

Semi-span sta.	Percent chord	UPPER SURFACE Angle of attack 6°	8°	10°	12°	LOWER SURFACE Angle of attack 6°	8°	10°	12°
0.086 b/2	0	0.360	0.213	0.067	-0.081	- -	- -	- -	- -
	1.5	-.591	-.912	-1.269	-1.342	0.414	0.494	0.559	0.608
	5.5	-.308	-.434	-.540	-.816	.264	.342	.414	.476
	6.5	-.322	-.480	-.521	-.734	.225	.303	.373	.439
	11.0	-.290	-.387	-.482	-.560	.173	.247	.312	.372
	14.5	-.306	-.397	-.489	-.575	.147	.217	.279	.337
	21.0	-.298	-.375	-.460	-.550	.110	.172	.231	.283
	24.5	-.316	-.397	-.460	-.544	.088	.145	.205	.257
	31.0	-.318	-.390	-.471	-.540	.055	.110	.167	.215
	34.5	-.363	-.446	-.534	-.603	.031	.086	.140	.187
	41.0	-.387	-.473	-.568	-.647	.006	.056	.110	.152
	44.5	-.410	-.498	-.593	-.678	- -	- -	- -	- -
	51.0	-.417	-.512	-.600	-.687	-.042	-.008	.055	.096
	59.5	-.365	-.452	-.584	-.675	-.060	-.007	.042	.075
	71.0	-.279	-.326	-.380	-.400	-.045	0	.037	.059
	79.5	-.178	-.206	-.227	-.253	-.010	.018	.043	.057
	91.0	-.066	-.080	-.100	-.143	.018	.031	.043	.041
0.195 b/2	0	0.070	-0.139	-0.317	-0.494	- -	- -	- -	- -
	1.5	-.900	-1.180	-1.290	-1.381	0.465	0.506	0.523	0.522
	5.5	-.455	-.603	-1.152	-1.356	.271	.350	.418	.483
	6.5	-.485	-.702	-1.088	-1.350	.230	.310	.380	.440
	11.0	-.413	-.515	-.857	-1.241	.172	.239	.308	.372
	14.5	-.405	-.532	-.721	-1.160	.130	.198	.265	.327
	21.0	-.393	-.500	-.580	-.693	.088	.153	.211	.270
	24.5	-.404	-.507	-.617	-.585	.066	.125	.183	.240
	31.0	-.398	-.500	-.580	-.620	.034	.085	.140	.191
	34.5	-.420	-.527	-.614	-.657	-.002	.057	.111	.160
	41.0	-.450	-.555	-.639	-.720	-.025	.026	.080	.129
	44.5	-.458	-.570	-.670	-.750	-.039	.018	.068	.110
	51.0	-.403	-.510	-.648	-.740	-.065	-.011	.035	.075
	59.5	-.327	-.384	-.445	-.414	-.057	-.013	.025	.057
	71.0	-.233	-.265	-.265	-.295	-.035	-.002	.022	.045
	79.5	-.126	-.152	-.164	-.219	0	.020	.037	.043
	91.0	-.013	-.030	-.039	-.082	.039	.041	.050	.038
0.382 b/2	0	-0.150	-0.390	-0.613	-0.806	- -	- -	- -	- -
	1.5	-1.273	-1.350	-1.370	-1.419	0.389	0.445	0.484	0.510
	5.5	-.835	-1.089	-1.240	-1.334	.248	.322	.365	.438
	6.5	-.840	-1.093	-1.332	-1.390	.220	.297	.359	.413
	11.0	-.575	-.901	-1.180	-1.334	.167	.229	.291	.349
	14.5	-.562	-.767	-1.127	-1.325	.120	.188	.251	.310
	21.0	-.531	-.701	-1.090	-1.309	.077	.140	.200	.250
	24.5	-.520	-.663	-1.002	-1.270	.050	.115	.170	.221
	31.0	-.485	-.644	-.935	-1.220	.008	.070	.126	.170
	34.5	-.459	-.610	-.853	-1.140	-.011	.050	.101	.148
	41.0	-.449	-.550	-.750	-.999	-.030	.030	.074	.113
	44.5	-.439	-.499	-.583	-.890	-.045	.010	.053	.090
	51.0	-.372	-.428	-.440	-.709	-.062	-.015	.025	.056
	59.5	-.289	-.320	-.330	-.563	-.051	-.015	.013	.038
	71.0	-.170	-.200	-.222	-.324	-.025	-.002	.017	.023
	79.5	-.080	-.105	-.145	-.233	.010	.023	.030	.028
	91.0	.021	0	-.030	-.101	.046	.046	.043	.023
0.555 b/2	0	-0.178	-0.435	-0.657	-0.849	- -	- -	- -	- -
	1.5	-1.411	-1.393	-1.373	-1.156	0.405	0.450	0.474	0.486
	5.5	-1.186	-1.397	-1.383	-1.145	.265	.336	.390	.430
	6.5	-1.069	-1.386	-1.356	-1.112	.242	.315	.369	.412
	11.0	-.740	-1.288	-1.380	-1.110	.164	.242	.299	.347
	14.5	-.634	-1.235	-1.309	-1.072	.133	.204	.260	.307
	21.0	-.569	-1.080	-1.280	-1.048	.082	.150	.200	.240
	24.5	-.535	-1.001	-1.209	-1.016	.060	.121	.170	.210
	31.0	-.491	-.752	-1.149	-.980	.019	.078	.121	.158
	34.5	-.456	-.640	-1.077	-.935	0	.057	.101	.132
	41.0	-.429	-.470	-.962	-.899	-.021	.030	.069	.099
	44.5	-.398	-.382	-.892	-.860	-.030	.015	.051	.075
	51.0	-.340	-.320	-.727	-.830	-.049	-.007	.023	.040
	59.5	-.239	-.230	-.537	-.762	-.056	-.024	-.003	0
	71.0	-.140	-.147	-.242	-.690	-.020	-.002	.002	-.013
	79.5	-.052	-.069	-.175	-.621	.010	.012	.007	-.032
	91.0	.033	.023	-.065	-.503	.049	.040	.012	-.080

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TABLE VIII.- CONCLUDED.

(b) α_u, 4°, 6°, 8°, 10° - Concluded.

Semi-span sta.	Percent chord	UPPER SURFACE				LOWER SURFACE			
		Angle of attack				Angle of attack			
		6°	8°	10°	12°	6°	8°	10°	12°
0.707 b/2	0	-0.334	-0.601	-0.818	-0.907	- -	- -	- -	- -
	1.5	-1.249	-1.150	-.983	-.825	0.431	0.455	0.458	0.448
	5.5	-1.205	-1.163	-.990	-.820	.285	.352	.398	.424
	6.5	-1.200	-1.120	-.952	-.798	.260	.328	.376	.403
	11.0	-1.003	-1.128	-.947	-.797	.177	.243	.297	.330
	14.5	-.901	-1.077	-.891	-.773	.144	.213	.260	.293
	21.0	-.700	-1.064	-.880	-.765	.090	.150	.198	.223
	24.5	-.611	-1.021	-.832	-.749	.070	.122	.160	.192
	31.0	-.481	-.963	-.820	-.739	.023	.078	.119	.140
	34.5	-.439	-.918	-.781	-.717	.010	.058	.094	.112
	41.0	-.377	-.807	-.766	-.704	-.021	.021	.052	.067
	44.5	-.346	-.771	-.731	-.681	-.040	.001	.028	.038
	51.0	-.289	-.621	-.711	-.670	-.060	-.027	-.007	-.007
	59.5	-.211	-.490	-.655	-.630	-.070	-.051	-.045	-.063
	71.0	-.110	-.249	-.597	-.607	-.035	-.028	-.048	-.192
	79.5	-.038	-.167	-.532	-.567	-.001	-.007	-.058	-.136
	91.0	.046	-.011	-.425	-.524	.050	.032	-.083	-.208
0.831 b/2	0	-0.159	-0.345	-0.485	-0.614	- -	- -	- -	- -
	1.5	-1.110	-.810	-.675	-.653	0.424	0.446	0.447	0.430
	5.5	-1.117	-.810	-.680	-.650	.267	.325	.370	.390
	6.5	-1.087	-.785	-.660	-.634	.257	.315	.360	.380
	11.0	-1.013	-.776	-.659	-.634	.169	.230	.278	.301
	14.5	-.960	-.743	-.635	-.609	- -	- -	- -	- -
	21.0	-.815	-.722	-.622	-.600	.072	.125	.170	.189
	24.5	-.743	-.689	-.594	-.580	.051	.093	.140	.154
	31.0	-.570	-.670	-.581	-.569	-.002	.040	.080	.090
	34.5	-.506	-.630	-.557	-.548	-.029	.008	.043	.050
	41.0	-.357	-.615	-.550	-.545	-.062	-.027	-.003	-.004
	44.5	-.324	-.579	-.527	-.525	-.081	-.060	-.037	-.044
	51.0	-.240	-.559	-.520	-.521	-.092	-.074	-.064	-.083
	59.5	-.165	-.492	-.487	-.495	-.095	-.090	-.108	-.146
	71.0	-.079	-.430	-.475	-.488	-.042	-.110	-.110	-.170
	79.5	-.021	-.368	-.445	-.467	0	-.040	-.125	-.187
	91.0	.049	-.277	-.418	-.446	.049	-.048	-.172	-.235
0.924 b/2	0	-0.601	-0.693	-0.670	-0.616	- -	- -	- -	- -
	1.5	-.854	-.639	-.549	-.528	0.402	0.419	.420	.402
	5.5	-.843	-.645	-.550	-.523	.255	.310	.339	.348
	6.5	-.801	-.625	-.530	-.511	.240	.295	.322	.332
	11.0	-.778	-.613	-.527	-.506	.136	.192	.228	.243
	14.5	-.720	-.580	-.503	-.487	.072	.128	.162	.175
	21.0	-.695	-.564	-.495	-.481	-.013	.040	.073	.085
	24.5	-.628	-.530	-.474	-.462	-.063	-.018	.013	.017
	31.0	-.571	-.505	-.460	-.459	-.090	-.055	-.033	-.039
	34.5	-.504	-.472	-.440	-.435	-.107	-.085	-.077	-.086
	41.0	-.425	-.453	-.430	-.430	-.120	-.105	-.104	-.125
	44.5	-.380	-.418	-.404	-.410	-.128	-.121	-.131	-.154
	51.0	-.308	-.406	-.400	-.410	-.122	-.125	-.143	-.171
	59.5	-.250	-.355	-.355	-.379	-.085	-.110	-.152	-.190
	71.0	-.158	-.338	-.348	-.382	-.040	-.084	-.141	-.191
	79.5	-.150	-.305	-.317	-.362	-.007	-.080	-.144	-.198
	91.0	-.077	-.303	-.330	-.365	.030	.099	-.168	-.221

NACA

TABLE IX.- PRESSURE COEFFICIENTS AT SEVEN SEMISPAN STATIONS OF THE WING. M_0, 0.86; R, 4,000,000.

(a) α_u, 0°, 1°, 2°, 3°.

Semi-span sta.	Percent chord	UPPER SURFACE				LOWER SURFACE			
		Angle of attack				Angle of attack			
		0°	1°	2°	3°	0°	1°	2°	3°
0.086 b/2	0	0.549	0.550	0.541	0.516	- -	- -	- -	- -
	1.5	.102	.016	-.061	-.191	0.069	0.140	0.206	0.261
	5.5	.016	-.032	-.083	-.135	.007	.055	.101	.141
	6.5	-.011	-.060	-.108	-.160	-.020	.022	.070	.109
	11.0	-.032	-.075	-.116	-.160	-.039	-.005	.035	.070
	14.5	-.061	-.100	-.139	-.181	-.061	-.027	.011	.045
	21.0	-.080	-.118	-.150	-.188	-.078	-.046	-.011	.019
	24.5	-.098	-.135	-.169	-.206	-.099	-.070	-.035	-.004
	31.0	-.110	-.145	-.177	-.211	-.122	-.094	-.060	-.031
	34.5	-.149	-.182	-.218	-.254	-.150	-.120	-.089	-.059
	41.0	-.177	-.214	-.244	-.282	-.173	-.145	-.112	-.081
	44.5	-.202	-.240	-.275	-.311	- -	- -	- -	- -
	51.0	-.216	-.254	-.289	-.322	-.208	-.180	-.154	-.126
	59.5	-.206	-.240	-.265	-.299	-.220	-.198	-.170	-.146
	71.0	-.171	-.197	-.219	-.239	-.185	-.166	-.139	-.120
	79.5	-.100	-.117	-.130	-.147	-.109	-.093	-.078	-.067
	91.0	-.029	-.036	-.042	-.052	-.029	-.023	-.016	-.011
0.195 b/2	0	0.477	0.464	0.433	0.373	- -	- -	- -	- -
	1.5	.040	-.072	-.200	-.347	0.074	0.174	0.259	0.330
	5.5	-.042	-.106	-.175	-.250	-.048	.015	.075	.126
	6.5	-.069	-.129	-.193	-.264	-.070	-.013	.042	.092
	11.0	-.090	-.136	-.187	-.240	-.090	-.045	.004	.044
	14.5	-.110	-.152	-.203	-.253	-.111	-.072	-.029	.011
	21.0	-.135	-.173	-.217	-.262	-.132	-.094	-.059	-.021
	24.5	-.151	-.192	-.234	-.279	-.152	-.116	-.080	-.040
	31.0	-.170	-.203	-.246	-.285	-.181	-.148	-.110	-.074
	34.5	-.194	-.228	-.270	-.310	-.206	-.170	-.132	-.100
	41.0	-.228	-.262	-.301	-.340	-.220	-.190	-.151	-.122
	44.5	-.240	-.276	-.314	-.351	-.224	-.198	-.162	-.131
	51.0	-.225	-.261	-.296	-.330	-.242	-.217	-.185	-.159
	59.5	-.202	-.235	-.266	-.289	-.214	-.189	-.159	-.139
	71.0	-.169	-.179	-.179	-.199	-.170	-.130	-.110	-.089
	79.5	-.063	-.081	-.090	-.112	-.068	-.063	-.052	-.045
	91.0	.012	.001	.001	-.008	.012	.013	.018	.017
0.382 b/2	0	0.437	0.418	0.361	0.266	- -	- -	- -	- -
	1.5	-.029	-.177	-.350	-.561	-0.056	0.054	0.145	0.224
	5.5	-.110	-.199	-.293	-.395	-.120	-.044	.026	.087
	6.5	-.137	-.214	-.302	-.398	-.132	-.062	.003	.06
	11.0	-.155	-.219	-.288	-.359	-.155	-.096	-.041	.014
	14.5	-.170	-.228	-.291	-.358	-.172	-.119	-.067	-.018
	21.0	-.190	-.241	-.297	-.346	-.191	-.144	-.098	-.054
	24.5	-.203	-.253	-.307	-.349	-.202	-.159	-.113	-.067
	31.0	-.214	-.260	-.309	-.355	-.230	-.186	-.145	-.102
	34.5	-.220	-.260	-.307	-.350	-.241	-.200	-.157	-.120
	41.0	-.247	-.282	-.327	-.370	-.236	-.199	-.156	-.127
	44.5	-.250	-.285	-.327	-.367	-.239	-.201	-.167	-.138
	51.0	-.229	-.259	-.298	-.320	-.240	-.210	-.180	-.153
	59.5	-.198	-.230	-.249	-.263	-.196	-.162	-.139	-.119
	71.0	-.097	-.117	-.127	-.160	-.092	-.098	-.082	-.071
	79.5	-.039	-.052	-.062	-.075	-.034	-.033	-.020	-.015
	91.0	.041	.031	.028	.023	.043	.042	.050	.044
0.555 b/2	0	0.435	0.428	0.368	0.260	- -	- -	- -	- -
	1.5	-.050	-.238	-.458	-.673	-0.077	0.050	0.159	0.248
	5.5	-.143	-.251	-.363	-.494	-.133	-.052	.032	.101
	6.5	-.160	-.267	-.372	-.493	-.150	-.070	.012	.079
	11.0	-.170	-.249	-.332	-.406	-.175	-.114	-.042	.017
	14.5	-.180	-.260	-.335	-.405	-.185	-.129	-.061	-.010
	21.0	-.202	-.270	-.331	-.389	-.200	-.153	-.095	-.050
	24.5	-.202	-.262	-.323	-.378	-.210	-.167	-.115	-.067
	31.0	-.209	-.261	-.311	-.358	-.222	-.188	-.136	-.097
	34.5	-.213	-.263	-.305	-.352	-.230	-.192	-.143	-.110
	41.0	-.231	-.281	-.320	-.358	-.220	-.193	-.148	-.120
	44.5	-.229	-.272	-.309	-.339	-.215	-.191	-.150	-.124
	51.0	-.211	-.260	-.274	-.301	-.203	-.184	-.152	-.130
	59.5	-.174	-.209	-.190	-.220	-.179	-.159	-.132	-.116
	71.0	-.079	-.104	-.121	-.128	-.070	-.080	-.081	-.058
	79.5	-.019	-.032	-.043	-.041	-.012	-.020	-.010	-.011
	91.0	.060	.049	.047	.049	.066	.060	.061	.053

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TABLE IX.- CONTINUED.

(a) α_u, 0°, 1°, 2°, 3° - Concluded.

Semi-span sta.	Percent chord	UPPER SURFACE Angle of attack 0°	1°	2°	3°	LOWER SURFACE Angle of attack 0°	1°	2°	3°
0.707 b/2	0	0.432	0.406	0.310	0.161	- -	- -	- -	- -
	1.5	-.055	-.271	-.540	-.853	-0.065	0.090	0.213	0.300
	5.5	-.156	-.286	-.419	-.574	-.144	-.050	.045	.120
	6.5	-.168	-.290	-.421	-.554	-.156	-.065	.027	.097
	11.0	-.160	-.251	-.345	-.434	-.185	-.115	-.038	.021
	14.5	-.180	-.270	-.349	-.423	-.190	-.125	-.053	0
	21.0	-.197	-.270	-.330	-.394	-.195	-.150	-.090	-.041
	24.5	-.200	-.268	-.321	-.383	-.203	-.161	-.103	-.060
	31.0	-.209	-.268	-.310	-.368	-.209	-.174	-.125	-.085
	34.5	-.212	-.267	-.303	-.353	-.209	-.179	-.128	-.091
	41.0	-.225	-.270	-.300	-.340	-.205	-.181	-.137	-.112
	44.5	-.220	-.268	-.286	-.320	-.205	-.189	-.149	-.124
	51.0	-.195	-.239	-.250	-.269	-.200	-.187	-.152	-.135
	59.5	-.170	-.200	-.193	-.199	-.178	-.159	-.130	-.122
	71.0	-.060	-.060	-.092	-.092	-.053	-.069	-.060	-.058
	79.5	0	-.018	-.018	-.020	.007	-.002	-.001	-.005
	91.0	.077	.067	.067	.068	.060	.071	.070	.060
0.831 b/2	0	0.413	0.447	0.390	0.279	- -	- -	- -	- -
	1.5	-.060	-.279	-.561	-.872	-0.070	0.094	0.221	0.307
	5.5	-.162	-.287	-.437	-.616	-.162	-.051	.037	.110
	6.5	-.164	-.280	-.422	-.570	-.162	-.059	.030	.101
	11.0	-.170	-.255	-.360	-.441	-.181	-.101	-.030	.030
	14.5	-.182	-.261	-.350	-.433	- -	- -	- -	- -
	21.0	-.201	-.262	-.329	-.385	-.200	-.148	-.093	-.045
	24.5	-.210	-.260	-.320	-.378	-.205	-.151	-.103	-.060
	31.0	-.212	-.251	-.293	-.337	-.218	-.175	-.139	-.103
	34.5	-.217	-.250	-.284	-.314	-.220	-.185	-.150	-.123
	41.0	-.222	-.248	-.265	-.280	-.211	-.187	-.160	-.140
	44.5	-.209	-.229	-.245	-.255	-.200	-.185	-.165	-.153
	51.0	-.189	-.210	-.214	-.220	-.180	-.164	-.150	-.141
	59.5	-.140	-.132	-.137	-.140	-.143	-.130	-.115	-.104
	71.0	-.038	-.048	-.060	-.058	-.022	-.032	-.040	-.055
	79.5	.020	.016	.010	.012	.030	.030	.020	.010
	91.0	.090	.090	.090	.087	.098	.092	.085	.075
0.924 b/2	0	0.434	0.352	0.183	-0.037	- -	- -	- -	- -
	1.5	-.066	-.236	-.543	-.927	0.097	0.077	0.203	0.290
	5.5	-.179	-.303	-.460	-.658	.171	-.058	.035	.107
	6.5	-.192	-.312	-.454	-.635	.179	-.068	.024	.097
	11.0	-.197	-.279	-.383	-.460	-.200	-.120	-.010	.009
	14.5	-.223	-.295	-.380	-.453	-.225	-.157	-.095	-.048
	21.0	-.223	-.260	-.303	-.297	-.230	-.189	-.150	-.113
	24.5	-.204	-.230	-.236	-.278	-.214	-.189	-.167	-.138
	31.0	-.191	-.214	-.230	-.256	-.198	-.178	-.165	-.146
	34.5	-.178	-.195	-.217	-.236	-.182	-.165	-.160	-.146
	41.0	-.187	-.201	-.224	-.237	-.176	-.161	-.160	-.149
	44.5	-.173	-.186	-.200	-.212	-.165	-.152	-.155	-.148
	51.0	-.147	-.149	-.160	-.172	-.151	-.140	-.142	-.140
	59.5	-.061	-.077	-.090	-.100	-.072	-.095	-.097	-.090
	71.0	-.009	-.013	-.018	-.025	.003	.001	-.005	-.025
	79.5	.043	.046	.042	.031	.049	.042	.030	.020
	91.0	.099	.102	.098	.085	.111	.101	.090	.076

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TABLE IX.- CONTINUED.

(b) α_u, 4°, 6°, 8°, 10°.

Semi-span sta.	Percent chord	UPPER SURFACE Angle of attack 4°	6°	8°	10°	LOWER SURFACE Angle of attack 4°	6°	8°	10°
0.086 b/2	0	0.482	0.365		0.120	- -	- -		- -
	1.5	-.309	-.560		-1.220	0.318	0.416		0.560
	5.5	-.190	-.291		-.493	.180	.266		.417
	6.5	-.210	-.309		-.505	.150	.230		.374
	11.0	-.197	-.278		-.460	.109	.180		.311
	14.5	-.220	-.296		-.472	.080	.150		.280
	21.0	-.221	-.289		-.443	.051	.112		.230
	24.5	-.237	-.310		-.453	.028	.089		.201
	31.0	-.239	-.309		-.442	-.002	.059		.162
	34.5	-.288	-.361		-.510	-.030	.031		.136
	41.0	-.318	-.398		-.550	-.054	.003		.101
	44.5	-.350	-.423		-.584	- -	- -		.051
	51.0	-.365	-.450		-.601	-.101	-.046		.049
	59.5	-.332	-.425		-.617	-.120	-.069		.033
	71.0	-.282	-.321		-.602	-.100	-.052		.026
	79.5	-.163	-.195		-.295	-.050	-.019		.031
	91.0	-.062	-.078		-.123	-.007	.009		.030
0.195 b/2	0	0.295	0.106	-0.083	-0.245	- -	- -	- -	- -
	1.5	-.510	-.872	-1.167	-1.296	0.387	0.465	0.511	0.535
	5.5	-.328	-.455	-.746	-1.078	.175	.270	.351	.420
	6.5	-.339	-.470	-.660	-.975	.139	.225	.307	.380
	11.0	-.293	-.418	-.520	-.780	.084	.165	.240	.310
	14.5	-.286	-.397	-.497	-.660	.049	.125	.197	.265
	21.0	-.305	-.410	-.490	-.550	.012	.080	.150	.211
	24.5	-.321	-.393	-.509	-.588	-.006	.060	.125	.186
	31.0	-.319	-.418	-.512	-.573	-.043	.017	.080	.140
	34.5	-.353	-.450	-.527	-.607	-.069	-.012	.050	.110
	41.0	-.384	-.470	-.570	-.639	-.093	-.039	.025	.080
	44.5	-.398	-.503	-.600	-.675	-.105	-.050	.009	.060
	51.0	-.370	-.484	-.606	-.673	-.129	-.078	-.022	.028
	59.5	-.306	-.390	-.573	-.700	-.113	-.069	-.022	.020
	71.0	-.223	-.254	-.291	-.362	-.080	-.047	-.010	.014
	79.5	-.122	-.139	-.160	-.166	-.037	-.012	.010	.028
	91.0	-.012	-.020	-.030	-.050	.017	.027	.040	.040
0.382 b/2	0	0.145	-0.100	-0.320	-0.524	- -	- -	- -	- -
	1.5	-.793	-1.204	-1.387	-1.322	0.287	0.382	0.443	0.485
	5.5	-.470	-.825	-1.100	-1.180	.142	.240	.315	.378
	6.5	-.482	-.670	-1.050	-1.300	.117	.210	.290	.355
	11.0	-.438	-.600	-.856	-1.093	.060	.148	.220	.287
	14.5	-.436	-.572	-.740	-1.050	.029	.110	.182	.248
	21.0	-.395	-.532	-.700	-1.020	-.010	.069	.132	.192
	24.5	-.428	-.548	-.670	-.950	-.030	.043	.105	.165
	31.0	-.428	-.555	-.673	-.915	-.070	-.002	.060	.117
	34.5	-.397	-.550	-.670	-.861	-.087	-.020	.040	.094
	41.0	-.412	-.577	-.705	-.845	-.099	-.040	.015	.065
	44.5	-.406	-.522	-.715	-.820	-.110	-.055	-.002	.044
	51.0	-.350	-.410	-.610	-.770	-.128	-.073	-.030	.014
	59.5	-.277	-.300	-.311	-.365	-.100	-.062	-.030	.003
	71.0	-.166	-.175	-.190	-.237	-.063	-.033	-.011	.003
	79.5	-.074	-.080	-.105	-.170	-.012	.006	.012	.020
	91.0	.027	.022	-.010	-.050	.039	.042	.039	.033
0.555 b/2	0	0.130	-0.122	-0.351	-0.554	- -	- -	- -	- -
	1.5	-1.021	-1.452	-1.610	-1.395	0.310	0.396	0.449	0.479
	5.5	-.588	-1.283	-1.550	-1.400	.160	.252	.329	.386
	6.5	-.574	-1.258	-1.510	-1.380	.139	.230	.307	.366
	11.0	-.519	-.713	-1.435	-1.380	.070	.158	.232	.294
	14.5	-.496	-.637	-1.295	-1.320	.039	.122	.197	.256
	21.0	-.460	-.647	-.820	-1.277	-.007	.070	.140	.198
	24.5	-.441	-.623	-.801	-1.219	-.026	.049	.111	.168
	31.0	-.418	-.586	-.738	-1.158	-.061	.005	.067	.119
	34.5	-.391	-.514	-.718	-1.080	-.072	-.010	.047	.096
	41.0	-.388	-.437	-.548	-.967	-.089	-.034	.019	.063
	44.5	-.370	-.397	-.550	-.908	-.094	-.043	.005	.045
	51.0	-.321	-.340	-.311	-.787	-.104	-.060	-.018	.019
	59.5	-.229	-.232	-.252	-.624	-.099	-.068	-.034	-.010
	71.0	-.128	-.133	-.160	-.350	-.050	-.030	-.012	-.004
	79.5	-.043	-.050	-.080	-.239	-.007	0	.008	0
	91.0	.048	.034	.006	-.074	.049	.043	.030	.004

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TABLE IX.- CONTINUED.

(b) α_u, 4°, 6°, 8°, 10° - Concluded.

Semi-span sta.	Percent chord	UPPER SURFACE Angle of attack 4°	6°	8°	10°	LOWER SURFACE Angle of attack 4°	6°	8°	10°
0.707 b/2	0	0.007	-0.270	-0.524	-0.740	- -	- -	- -	- -
	1.5	-1.175	-1.517	-1.631	-1.100	0.360	0.422	0.449	0.458
	5.5	-.880	-1.413	-1.570	-1.104	.181	.270	.340	.390
	6.5	-.850	-1.417	-1.570	-1.069	.157	.247	.316	.369
	11.0	-.530	-1.304	-1.500	-1.052	.078	.163	.231	.292
	14.5	-.504	-1.133	-1.323	-.995	.051	.133	.200	.254
	21.0	-.463	-.582	-1.151	-.968	0	.081	.142	.191
	24.5	-.452	-.490	-1.115	-.918	-.017	.056	.113	.162
	31.0	-.408	-.429	-.950	-.878	-.050	.013	.069	.113
	34.5	-.390	-.390	-.884	-.834	-.061	0	.050	.090
	41.0	-.366	-.362	-.842	-.793	-.082	-.031	.013	.049
	44.5	-.343	-.340	-.816	-.760	-.099	-.050	-.008	.023
	51.0	-.279	-.291	-.393	-.718	-.112	-.070	-.036	-.012
	59.5	-.200	-.215	-.297	-.660	-.109	-.080	-.060	-.050
	71.0	-.091	-.106	-.149	-.590	-.052	-.040	-.039	-.053
	79.5	-.019	-.028	-.082	-.529	-.010	-.010	-.018	-.065
	91.0	.067	.053	.010	-.425	.052	.044	.022	-.093
0.831 b/2	0	0.142	-0.125	-0.360	-0.501	- -	- -	- -	- -
	1.5	-1.211	-1.492	-1.069	-.749	0.363	0.416	0.432	0.439
	5.5	-.995	-1.403	-1.066	-.750	.173	.260	.318	.362
	6.5	-.945	-1.394	-1.036	-.725	.162	.250	.309	.352
	11.0	-.536	-1.261	-1.010	-.719	.080	.160	.221	.270
	14.5	-.495	-1.067	-.920	-.680	- -	- -	- -	- -
	21.0	-.451	-.740	-.884	-.672	-.004	.070	.121	.163
	24.5	-.430	-.646	-.822	-.632	-.023	.046	.097	.132
	31.0	-.363	-.371	-.776	-.627	-.063	-.007	.035	.071
	34.5	-.322	-.346	-.736	-.598	-.090	-.038	.004	.036
	41.0	-.282	-.305	-.695	-.596	-.114	-.070	-.037	-.012
	44.5	-.259	-.280	-.657	-.570	-.130	-.096	-.067	-.048
	51.0	-.220	-.235	-.609	-.569	-.127	-.105	-.085	-.079
	59.5	-.143	-.147	-.527	-.530	-.106	-.105	-.104	-.124
	71.0	-.058	-.069	-.415	-.517	-.050	-.047	-.067	-.128
	79.5	.010	-.003	-.333	-.478	.002	0	-.031	-.140
	91.0	.080	.065	-.194	-.443	.063	.055	-.009	-.187
0.924 b/2	0	-0.247	-0.610	-0.790	-0.694	- -	- -	- -	- -
	1.5	-1.173	-1.083	-.730	-.567	0.343	0.395	0.411	0.417
	5.5	-.936	-1.060	-.735	-.570	.165	.250	.302	.334
	6.5	-.968	-.989	-.712	-.552	.155	.240	.270	.320
	11.0	-.576	-.905	-.703	-.548	.055	.133	.190	.225
	14.5	-.490	-.828	-.670	-.517	-.003	.070	.103	.160
	21.0	-.343	-.750	-.657	-.512	-.085	-.017	.030	.068
	24.5	-.280	-.680	-.620	-.488	-.125	-.078	-.030	.002
	31.0	-.263	-.590	-.597	-.478	-.135	-.107	-.070	-.043
	34.5	-.247	-.520	-.560	-.458	-.140	-.129	-.106	-.090
	41.0	-.244	-.415	-.540	-.450	-.146	-.132	-.125	-.120
	44.5	-.223	-.374	-.500	-.423	-.146	-.139	-.140	-.146
	51.0	-.181	-.282	-.484	-.421	-.136	-.130	-.140	-.160
	59.5	-.112	-.230	-.429	-.380	-.087	-.089	-.114	-.165
	71.0	-.037	-.135	-.406	-.383	-.035	-.040	-.076	-.156
	79.5	.010	-.140	-.373	-.358	.007	-.002	-.067	-.160
	91.0	.060	-.056	-.342	-.371	.064	.044	-.079	-.190

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TABLE IX.- CONTINUED.

(c) α_u, 12°, 16°, 20°, 24°.

Semi-span sta.	Percent chord	UPPER SURFACE Angle of attack 12°	16°	20°	24°	LOWER SURFACE Angle of attack 12°	16°	20°	24°
0.086 b/2	0	-0.014				- -			
	1.5	-1.333				0.615			
	5.5	-.734				.484			
	6.5	-.601				.446			
	11.0	-.530				.378			
	14.5	-.555				.340			
	21.0	-.533				.290			
	24.5	-.530				.260			
	31.0	-.521				.218			
	34.5	-.575				.190			
	41.0	-.620				.151			
	44.5	-.657				- -			
	51.0	-.675				.094			
	59.5	-.685				.072			
	71.0	-.660				.051			
	79.5	-.341				.045			
	91.0	-.177				.025			
0.195 b/2	0	-0.408				- -			
	1.5	-1.308				0.536			
	5.5	-1.265				.480			
	6.5	-1.260				.437			
	11.0	-1.169				.370			
	14.5	-1.082				.324			
	21.0	-.715				.272			
	24.5	-.620				.235			
	31.0	-.580				.185			
	34.5	-.619				.155			
	41.0	-.696				.122			
	44.5	-.725				.102			
	51.0	-.725				.067			
	59.5	-.700				.043			
	71.0	-.410				.028			
	79.5	-.227				.025			
	91.0	-.116				.011			
0.382 b/2	0	-0.707				- -			
	1.5	-1.324				0.508			
	5.5	-1.277				.428			
	6.5	-1.330				.403			
	11.0	-1.277				.337			
	14.5	-1.282				.299			
	21.0	-1.245				.240			
	24.5	-1.253				.210			
	31.0	-1.201				.160			
	34.5	-1.180				.131			
	41.0	-1.076				.100			
	44.5	-1.013				.078			
	51.0	-.868				.040			
	59.5	-.747				.015			
	71.0	-.510				0			
	79.5	-.380				-.002			
	91.0	-.178				-.009			
0.555 b/2	0	-0.736				- -			
	1.5	-1.114				0.489			
	5.5	-1.106				.421			
	6.5	-1.080				.405			
	11.0	-1.061				.339			
	14.5	-1.051				.297			
	21.0	-1.040				.231			
	24.5	-1.010				.200			
	31.0	-.990				.149			
	34.5	-.949				.122			
	41.0	-.906				.084			
	44.5	-.864				.064			
	51.0	-.833				.029			
	59.5	-.782				-.015			
	71.0	-.719				-.030			
	79.5	-.660				-.053			
	91.0	-.561				-.118			

NACA

TABLE IX.- CONCLUDED.

(c) α_u, 12°, 16°, 20°, 24° - Concluded.

Semi-span sta.	Percent chord	UPPER SURFACE Angle of attack 12°	16°	20°	24°	LOWER SURFACE Angle of attack 12°	16°	20°	24°
0.707 b/2	0	-0.862				- -			
	1.5	-.847				0.447			
	5.5	-.837				.415			
	6.5	-.812				.395			
	11.0	-.810				.318			
	14.5	-.785				.281			
	21.0	-.780				.212			
	24.5	-.761				.181			
	31.0	-.754				.129			
	34.5	-.739				.101			
	41.0	-.729				.051			
	44.5	-.709				.024			
	51.0	-.699				-.020			
	59.5	-.657				-.080			
	71.0	-.630				-.114			
	79.5	-.593				-.160			
	91.0	-.538				-.231			
0.831 b/2	0	-0.610				- -			
	1.5	-.677				0.424			
	5.5	-.673				.378			
	6.5	-.658				.368			
	11.0	-.658				.296			
	14.5	-.638				- -			
	21.0	-.630				.172			
	24.5	-.608				.141			
	31.0	-.601				.075			
	34.5	-.580				.032			
	41.0	-.578				-.020			
	44.5	-.557				-.066			
	51.0	-.552				-.106			
	59.5	-.525				-.177			
	71.0	-.522				-.200			
	79.5	-.501				-.217			
	91.0	-.479				-.263			
0.924 b/2	0	-0.641				- -			
	1.5	-.552				0.395			
	5.5	-.547				.338			
	6.5	-.533				.324			
	11.0	-.535				.230			
	14.5	-.512				.168			
	21.0	-.505				.069			
	24.5	-.483				0			
	31.0	-.480				-.059			
	34.5	-.460				-.110			
	41.0	-.456				-.151			
	44.5	-.436				-.183			
	51.0	-.438				-.202			
	59.5	-.410				-.218			
	71.0	-.426				-.221			
	79.5	-.405				-.230			
	91.0	-.402				-.258			

TABLE X.- PRESSURE COEFFICIENTS AT SEVEN SEMISPAN STATIONS OF THE WING. M_0, 0.88; R, 4,000,000.

(a) α_u, 0°, 1°, 2°, 3°.

Semi-span sta.	Percent chord	UPPER SURFACE				LOWER SURFACE			
		Angle of attack				Angle of attack			
		0°	1°	2°	3°	0°	1°	2°	3°
0.086 b/2	0	0.557	0.561	0.540	0.528	- -	- -	- -	- -
	1.5	.111	.029	-.072	-.172	0.078	0.150	0.206	0.273
	5.5	.026	-.021	-.079	-.122	.018	.063	.102	.150
	6.5	-.002	-.048	-.101	-.147	-.012	.032	.071	.118
	11.0	-.028	-.062	-.110	-.149	-.030	.005	.040	.079
	14.5	-.055	-.090	-.134	-.171	-.052	-.018	.015	.052
	21.0	-.073	-.106	-.145	-.178	-.069	-.037	-.006	.027
	24.5	-.091	-.125	-.163	-.196	-.092	-.060	-.032	.001
	31.0	-.105	-.137	-.172	-.202	-.118	-.087	-.058	-.024
	34.5	-.145	-.178	-.213	-.249	-.147	-.113	-.085	-.052
	41.0	-.176	-.209	-.247	-.280	-.172	-.140	-.111	-.080
	44.5	-.205	-.238	-.278	-.312	- -	- -	- -	- -
	51.0	-.224	-.255	-.294	-.330	-.210	-.180	-.154	-.126
	59.5	-.217	-.243	-.282	-.318	-.231	-.202	-.177	-.148
	71.0	-.180	-.200	-.228	-.252	-.197	-.169	-.145	-.126
	79.5	-.105	-.119	-.141	-.151	-.116	-.093	-.082	-.066
	91.0	-.029	-.034	-.049	-.053	-.030	-.021	-.020	-.010
0.195 b/2	0	0.483	0.472	0.440	0.383	- -	- -	- -	- -
	1.5	.044	-.062	-.191	-.334	0.080	0.179	0.261	0.330
	5.5	-.037	-.102	-.170	-.243	-.041	.020	.075	.130
	6.5	-.067	-.127	-.190	-.258	-.068	-.010	.043	.098
	11.0	-.089	-.136	-.186	-.235	-.090	-.040	.003	.047
	14.5	-.110	-.153	-.202	-.250	-.115	-.070	-.030	-.013
	21.0	-.137	-.177	-.220	-.261	-.135	-.096	-.059	-.021
	24.5	-.156	-.194	-.238	-.280	-.156	-.115	-.080	-.040
	31.0	-.173	-.209	-.250	-.285	-.185	-.150	-.114	-.079
	34.5	-.200	-.238	-.279	-.320	-.210	-.175	-.139	-.105
	41.0	-.238	-.272	-.316	-.360	-.230	-.198	-.160	-.125
	44.5	-.252	-.290	-.334	-.381	-.240	-.206	-.170	-.141
	51.0	-.242	-.278	-.319	-.363	-.261	-.230	-.199	-.169
	59.5	-.220	-.250	-.285	-.326	-.230	-.200	-.170	-.148
	71.0	-.179	-.153	-.207	-.201	-.185	-.140	-.120	-.106
	79.5	-.074	-.085	-.100	-.120	-.071	-.069	-.060	-.051
	91.0	.011	.005	-.003	-.010	.009	.012	.012	.016
0.382 b/2	0	0.437	0.421	0.368	0.278	- -	- -	- -	- -
	1.5	-.028	-.170	-.347	-.550	-0.056	0.052	0.146	0.220
	5.5	-.116	-.200	-.291	-.392	-.120	-.048	.022	.087
	6.5	-.140	-.217	-.302	-.390	-.136	-.066	.001	.061
	11.0	-.160	-.221	-.291	-.360	-.159	-.100	-.042	.009
	14.5	-.174	-.232	-.300	-.375	-.179	-.122	-.070	-.021
	21.0	-.200	-.250	-.304	-.351	-.200	-.150	-.101	-.060
	24.5	-.216	-.264	-.323	-.375	-.211	-.166	-.120	-.077
	31.0	-.229	-.271	-.327	-.363	-.240	-.197	-.151	-.109
	34.5	-.231	-.271	-.321	-.371	-.255	-.211	-.169	-.130
	41.0	-.260	-.300	-.345	-.399	-.250	-.210	-.164	-.139
	44.5	-.265	-.301	-.350	-.394	-.251	-.213	-.178	-.150
	51.0	-.241	-.274	-.320	-.354	-.254	-.223	-.189	-.161
	59.5	-.212	-.240	-.276	-.275	-.210	-.173	-.150	-.130
	71.0	-.103	-.118	-.140	-.165	-.100	-.100	-.090	-.075
	79.5	-.045	-.052	-.066	-.077	-.035	-.031	-.026	-.021
	91.0	.040	.035	.028	.026	.044	.046	.050	.047
0.555 b/2	0	0.434	0.431	0.371	0.269	- -	- -	- -	- -
	1.5	-.054	-.222	-.452	-.709	-0.083	0.048	0.155	0.239
	5.5	-.146	-.245	-.361	-.501	-.140	-.050	.027	.093
	6.5	-.167	-.261	-.378	-.498	-.155	-.069	.006	.077
	11.0	-.174	-.247	-.340	-.427	-.169	-.113	-.049	.012
	14.5	-.190	-.260	-.343	-.399	-.197	-.130	-.070	-.017
	21.0	-.214	-.270	-.340	-.401	-.213	-.156	-.104	-.057
	24.5	-.214	-.268	-.337	-.392	-.225	-.170	-.120	-.070
	31.0	-.220	-.266	-.328	-.401	-.235	-.184	-.143	-.101
	34.5	-.227	-.267	-.324	-.369	-.245	-.193	-.149	-.113
	41.0	-.247	-.283	-.331	-.362	-.237	-.194	-.153	-.126
	44.5	-.240	-.273	-.324	-.349	-.230	-.192	-.153	-.129
	51.0	-.220	-.251	-.292	-.314	-.220	-.183	-.158	-.134
	59.5	-.185	-.205	-.180	-.221	-.186	-.150	-.137	-.119
	71.0	-.085	-.099	-.125	-.129	-.077	-.071	-.118	-.059
	79.5	-.020	-.029	-.041	-.042	-.020	-.013	-.011	-.010
	91.0	.057	.058	.047	.051	.063	.064	.061	.052

NACA

TABLE X.- CONTINUED.

(a) α_u, 0°, 1°, 2°, 3° - Concluded.

Semi-span sta.	Percent chord	UPPER SURFACE Angle of attack 0°	1°	2°	3°	LOWER SURFACE Angle of attack 0°	1°	2°	3°
0.707 b/2	0	0.427	0.407	0.313	0.171	- -	- -	- -	- -
	1.5	-.060	-.263	-.541	-.866	-0.072	0.090	0.210	0.296
	5.5	-.120	-.285	-.430	-.607	-.160	-.049	.037	.113
	6.5	-.179	-.291	-.436	-.563	-.170	-.067	.017	.090
	11.0	-.173	-.250	-.354	-.450	-.200	-.113	-.041	.019
	14.5	-.195	-.269	-.360	-.452	-.203	-.126	-.060	-.004
	21.0	-.212	-.270	-.346	-.387	-.214	-.148	-.093	-.047
	24.5	-.215	-.268	-.340	-.398	-.220	-.158	-.106	-.062
	31.0	-.223	-.269	-.327	-.386	-.225	-.173	-.126	-.087
	34.5	-.225	-.268	-.317	-.376	-.225	-.176	-.128	-.096
	41.0	-.239	-.273	-.306	-.350	-.222	-.180	-.140	-.115
	44.5	-.235	-.265	-.293	-.325	-.222	-.186	-.152	-.128
	51.0	-.209	-.238	-.253	-.272	-.214	-.187	-.157	-.139
	59.5	-.180	-.193	-.195	-.195	-.180	-.157	-.133	-.126
	71.0	-.067	-.072	-.090	-.088	-.056	-.061	-.060	-.058
	79.5	-.002	-.006	-.020	-.012	0	.001	-.001	-.008
	91.0	.075	.075	.069	.070	.080	.079	.073	.060
0.831 b/2	0	0.411	0.448	0.389	0.282	- -	- -	- -	- -
	1.5	-.070	-.280	-.577	-.909	-0.078	0.091	0.221	0.307
	5.5	-.171	-.299	-.450	-.690	-.170	-.061	.039	.110
	6.5	-.173	-.290	-.435	-.611	-.171	-.064	.030	.102
	11.0	-.179	-.266	-.371	-.454	-.191	-.109	-.032	.029
	14.5	-.190	-.270	-.368	-.469	- -	- -	- -	- -
	21.0	-.213	-.271	-.338	-.412	-.212	-.151	-.091	-.047
	24.5	-.220	-.275	-.330	-.393	-.217	-.161	-.109	-.058
	31.0	-.224	-.266	-.300	-.350	-.230	-.186	-.140	-.101
	34.5	-.233	-.269	-.299	-.333	-.238	-.199	-.157	-.125
	41.0	-.237	-.260	-.269	-.277	-.229	-.200	-.165	-.145
	44.5	-.221	-.240	-.240	-.250	-.214	-.194	-.170	-.156
	51.0	-.198	-.217	-.210	-.214	-.190	-.170	-.151	-.141
	59.5	-.144	-.122	-.133	-.132	-.150	-.135	-.120	-.118
	71.0	-.040	-.043	-.055	-.053	-.029	-.032	-.040	-.044
	79.5	.020	.020	.015	.017	.032	.030	.025	.012
	91.0	.096	.095	.094	.092	.101	.099	.090	.081
0.924 b/2	0	0.436	0.358	0.185	-0.028	- -	- -	- -	- -
	1.5	-.011	-.232	-.550	-.959	-0.099	0.071	0.207	0.292
	5.5	-.166	-.311	-.474	-.719	-.177	-.063	.038	.110
	6.5	-.201	-.319	-.465	-.697	-.182	-.071	.029	.099
	11.0	-.210	-.288	-.398	-.470	-.210	-.129	-.051	.009
	14.5	-.243	-.314	-.396	-.474	-.240	-.169	-.101	-.050
	21.0	-.244	-.281	-.339	-.363	-.254	-.205	-.160	-.122
	24.5	-.222	-.248	-.222	-.246	-.230	-.200	-.175	-.155
	31.0	-.201	-.220	-.232	-.250	-.210	-.187	-.167	-.155
	34.5	-.188	-.199	-.212	-.230	-.190	-.174	-.160	-.150
	41.0	-.194	-.205	-.225	-.234	-.184	-.169	-.159	-.152
	44.5	-.182	-.189	-.196	-.209	-.170	-.159	-.150	-.149
	51.0	-.155	-.147	-.160	-.168	-.159	-.145	-.137	-.139
	59.5	-.060	-.079	-.087	-.093	-.065	-.092	-.091	-.086
	71.0	-.011	-.010	-.012	-.019	.001	.008	0	-.019
	79.5	.042	.049	.047	.039	.053	.049	.039	.022
	91.0	.105	.108	.101	.091	.116	.110	.096	.082

NACA

TABLE X.- CONTINUED.

(b) α_u, 4°, 6°, 8°, 10°.

Semi-span sta.	Percent chord	UPPER SURFACE				LOWER SURFACE			
		Angle of attack				Angle of attack			
		4°	6°	8°	10°	4°	6°	8°	10°
0.086 b/2	0	0.496	0.405	0.283	0.159	- -	- -	- -	- -
	1.5	-.287	-.531	-.817	-1.172	0.324	0.422	0.500	0.563
	5.5	-.172	-.269	-.367	-.469	.190	.271	.346	.417
	6.5	-.195	-.285	-.390	-.469	.157	.234	.307	.377
	11.0	-.181	-.257	-.345	-.430	.113	.184	.249	.312
	14.5	-.207	-.279	-.367	-.455	.087	.156	.218	.279
	21.0	-.210	-.272	-.351	-.429	.057	.119	.180	.230
	24.5	-.228	-.292	-.351	-.434	.033	.093	.149	.201
	31.0	-.222	-.288	-.357	-.425	.003	.061	.112	.162
	34.5	-.277	-.355	-.417	-.482	-.021	.037	.088	.135
	41.0	-.313	-.380	-.460	-.522	-.050	.008	.056	.100
	44.5	-.343	-.413	-.495	-.560	- -	- -	- -	- -
	51.0	-.366	-.439	-.512	-.581	-.099	-.045	.001	.042
	59.5	-.357	-.456	-.531	-.596	-.121	-.069	-.018	.027
	71.0	-.283	-.393	-.549	-.649	-.101	-.054	-.017	.015
	79.5	-.170	-.220	-.320	-.472	-.050	-.019	.005	.020
	91.0	-.064	-.085	-.130	-.191	-.005	.010	.012	.009
0.195 b/2	0	0.313	0.138	-0.039	-0.190	- -	- -	- -	- -
	1.5	-.486	-.815	-1.117	-1.264	0.394	0.470	0.520	0.539
	5.5	-.314	-.420	-.705	-.995	.185	.273	.355	.416
	6.5	-.325	-.437	-.520	-.920	.147	.230	.313	.377
	11.0	-.283	-.390	-.509	-.711	.090	.180	.245	.306
	14.5	-.278	-.380	-.475	-.610	.055	.130	.200	.261
	21.0	-.290	-.378	-.463	-.542	.020	.095	.156	.211
	24.5	-.319	-.388	-.486	-.559	0	.063	.125	.176
	31.0	-.314	-.399	-.496	-.559	-.041	.020	.080	.130
	34.5	-.342	-.428	-.514	-.586	-.070	-.009	.053	.102
	41.0	-.401	-.480	-.560	-.625	-.092	-.035	.020	.070
	44.5	-.424	-.503	-.594	-.657	-.110	-.052	.004	.054
	51.0	-.403	-.514	-.600	-.661	-.136	-.080	-.025	.017
	59.5	-.345	-.503	-.620	-.687	-.120	-.071	-.030	.005
	71.0	-.232	-.287	-.453	-.670	-.087	-.050	-.018	.002
	79.5	-.123	-.150	-.192	-.252	-.040	-.020	0	.005
	91.0	-.011	-.021	-.046	-.078	.016	.020	.023	.012
0.382 b/2	0	0.170	-0.060	-0.265	-0.458	- -	- -	- -	- -
	1.5	-.770	-1.143	-1.312	-1.277	0.287	0.380	0.444	0.480
	5.5	-.493	-.803	-1.067	-1.150	.143	.237	.316	.375
	6.5	-.455	-.651	-1.023	-1.277	.119	.210	.288	.348
	11.0	-.411	-.590	-.830	-1.035	.061	.145	.220	.279
	14.5	-.427	-.552	-.720	-1.007	.025	.110	.180	.239
	21.0	-.415	-.530	-.687	-.962	-.014	.061	.132	.187
	24.5	-.427	-.535	-.656	-.897	-.030	.040	.105	.157
	31.0	-.443	-.548	-.661	-.870	-.074	-.007	.054	.106
	34.5	-.450	-.556	-.663	-.820	-.090	-.027	.032	.080
	41.0	-.461	-.602	-.700	-.823	-.103	-.044	.011	.051
	44.5	-.447	-.620	-.717	-.805	-.116	-.060	-.010	.030
	51.0	-.377	-.585	-.727	-.800	-.135	-.080	-.035	-.021
	59.5	-.280	-.315	-.496	-.640	-.111	-.069	-.035	-.015
	71.0	-.165	-.167	-.193	-.290	-.068	-.040	-.020	-.018
	79.5	-.070	-.071	-.101	-.205	-.018	-.002	.017	-.002
	91.0	.030	.028	-.015	-.096	.041	.042	.030	.006
0.555 b/2	0	0.150	-0.076	-0.287	-0.452	- -	- -	- -	- -
	1.5	-1.007	-1.365	-1.493	-1.373	0.303	0.392	0.443	0.470
	5.5	-.560	-1.265	-1.420	-1.368	.152	.250	.320	.372
	6.5	-.552	-1.201	-1.402	-1.354	.131	.227	.300	.352
	11.0	-.515	-.648	-1.389	-1.285	.082	.154	.226	.280
	14.5	-.521	-.584	-1.329	-1.235	.072	.122	.190	.240
	21.0	-.513	-.623	-.783	-1.166	-.012	.070	.131	.180
	24.5	-.489	-.624	-.750	-1.124	-.030	.050	.105	.151
	31.0	-.465	-.630	-.714	-1.085	-.068	.006	.060	.104
	34.5	-.428	-.639	-.701	-1.037	-.078	-.011	.040	.078
	41.0	-.390	-.681	-.739	-.970	-.095	-.033	.012	.043
	44.5	-.367	-.567	-.712	-.918	-.100	-.042	-.002	.026
	51.0	-.330	-.320	-.470	-.634	-.111	-.060	-.026	-.001
	59.5	-.230	-.201	-.250	-.720	-.103	-.066	-.047	-.032
	71.0	-.126	-.108	-.170	-.442	-.055	-.030	-.024	-.030
	79.5	-.040	-.032	-.087	-.429	-.007	.002	-.003	-.029
	91.0	.052	.050	-.005	-.221	.049	.044	.022	-.033

NACA

TABLE X.- CONTINUED.

(b) α_u, 4°, 6°, 8°, 10° - Concluded.

Semi-span sta.	Percent chord	UPPER SURFACE Angle of attack 4°	6°	8°	10°	LOWER SURFACE Angle of attack 4°	6°	8°	10°
0.707 b/2	0	0.029	-0.215	-0.450	-0.660	- -	- -	- -	- -
	1.5	-1.187	-1.414	-1.445	-1.013	0.352	0.421	0.446	0.450
	5.5	-1.001	-1.309	-1.444	-1.015	.173	.273	.330	.372
	6.5	-.939	-1.317	-1.384	-1.003	.150	.242	.305	.350
	11.0	-.563	-1.280	-1.246	-1.010	.071	.161	.223	.271
	14.5	-.549	-1.213	-1.186	-.991	.045	.132	.192	.236
	21.0	-.473	-.645	-1.134	-.973	-.003	.073	.133	.170
	24.5	-.440	-.634	-1.065	-.930	-.020	.053	.107	.144
	31.0	-.412	-.669	-.978	-.894	-.052	.013	.062	.095
	34.5	-.414	-.583	-.908	-.847	-.064	-.002	.044	.072
	41.0	-.381	-.305	-.818	-.805	-.088	-.034	.006	.029
	44.5	-.355	-.261	-.751	-.761	-.101	-.052	-.016	.002
	51.0	-.286	-.229	-.656	-.720	-.118	-.072	-.044	-.035
	59.5	-.194	-.188	-.533	-.653	-.112	-.083	-.068	-.078
	71.0	-.087	-.090	-.293	-.560	-.060	-.045	-.050	-.084
	79.5	-.014	-.020	-.198	-.520	-.012	-.009	-.028	-.100
	91.0	.068	.058	-.020	-.433	.053	.047	.013	-.135
0.831 b/2	0	0.155	-0.081	-0.294	-0.461	- -	- -	- -	- -
	1.5	-1.217	-1.420	-.938	-.787	0.359	0.411	0.431	0.431
	5.5	-1.062	-1.374	-.940	-.790	.169	.253	.312	.349
	6.5	-1.060	-1.371	-.961	-.788	.158	.244	.302	.338
	11.0	-.532	-1.281	-.958	-.789	.079	.158	.218	.253
	14.5	-.460	-1.260	-.928	-.762	- -	- -	- -	- -
	21.0	-.465	-1.118	-.887	-.745	-.003	.065	.116	.148
	24.5	-.447	-.769	-.821	-.707	-.027	.046	.090	.120
	31.0	-.393	-.203	-.770	-.693	-.069	-.010	.032	.051
	34.5	-.342	-.230	-.705	-.665	-.096	-.041	-.001	.017
	41.0	-.276	-.262	-.660	-.657	-.123	-.077	-.043	-.031
	44.5	-.246	-.240	-.617	-.630	-.141	-.102	-.076	-.071
	51.0	-.212	-.218	-.571	-.616	-.132	-.109	-.094	-.103
	59.5	-.139	-.133	-.496	-.571	-.113	-.105	-.115	-.157
	71.0	-.063	-.052	-.404	-.531	-.048	-.049	-.075	-.127
	79.5	.011	.010	-.335	-.491	.009	0	-.049	-.160
	91.0	.083	.074	-.239	-.440	.070	.060	-.043	-.195
0.924 b/2	0	-0.227	-0.550	-0.761	-0.752	- -	- -	- -	- -
	1.5	-1.151	-1.311	-.743	-.622	0.341	0.390	0.408	0.405
	5.5	-1.011	-1.234	-.750	-.632	.166	.247	.297	.322
	6.5	-1.020	-1.199	-.739	-.612	.155	.232	.283	.310
	11.0	-.650	-1.020	-.730	-.602	.057	.131	.181	.212
	14.5	-.533	-.924	-.689	-.569	-.004	.068	.119	.149
	21.0	-.390	-.795	-.671	-.561	-.090	-.023	.025	.050
	24.5	-.260	-.710	-.627	-.533	-.140	-.088	-.040	-.018
	31.0	-.247	-.593	-.607	-.531	-.148	-.120	-.073	-.069
	34.5	-.232	-.533	-.571	-.508	-.144	-.139	-.120	-.118
	41.0	-.240	-.402	-.544	-.508	-.149	-.140	-.139	-.150
	44.5	-.220	-.362	-.510	-.480	-.147	-.142	-.152	-.174
	51.0	-.179	-.250	-.483	-.481	-.136	-.131	-.149	-.187
	59.5	-.110	-.203	-.429	-.428	-.082	-.085	-.122	-.161
	71.0	-.036	-.100	-.387	-.425	-.028	-.032	-.090	-.178
	79.5	.009	-.114	-.352	-.390	.012	.004	-.070	-.178
	91.0	.061	-.036	-.322	-.391	.070	.055	-.092	-.199

NACA

TABLE X.- CONTINUED.

(o) α_u, 12°, 16°, 20°, 24°.

Semi-span sta.	Percent chord	UPPER SURFACE Angle of attack 12°	16°	20°	24°	LOWER SURFACE Angle of attack 12°	16°	20°	24°
0.086 b/2	0	0.032				- -			
	1.5	-1.306				0.619			
	5.5	-.668				.481			
	6.5	-.540				.445			
	11.0	-.499				.377			
	14.5	-.523				.340			
	21.0	-.508				.288			
	24.5	-.506				.258			
	31.0	-.500				.215			
	34.5	-.551				.185			
	41.0	-.591				.148			
	44.5	-.630				- -			
	51.0	-.648				.090			
	59.5	-.670				.063			
	71.0	-.718				.040			
	79.5	-.553				.032			
	91.0	-.249				.005			
0.195 b/2	0	-0.345				- -			
	1.5	-1.237				0.547			
	5.5	-1.223				.479			
	6.5	-1.191				.437			
	11.0	-1.100				.370			
	14.5	-1.020				.320			
	21.0	-.674				.266			
	24.5	-.610				.232			
	31.0	-.557				.185			
	34.5	-.594				.155			
	41.0	-.668				.117			
	44.5	-.704				.097			
	51.0	-.720				.080			
	59.5	-.709				.035			
	71.0	-.723				.020			
	79.5	-.288				.009			
	91.0	-.130				-.009			
0.382 b/2	0	-0.628				- -			
	1.5	-1.268				0.511			
	5.5	-1.209				.429			
	6.5	-1.281				.403			
	11.0	-1.203				.337			
	14.5	-1.220				.298			
	21.0	-1.170				.239			
	24.5	-1.165				.209			
	31.0	-1.121				.154			
	34.5	-1.093				.128			
	41.0	-1.025				.094			
	44.5	-.990				.069			
	51.0	-.890				.030			
	59.5	-.765				.005			
	71.0	-.530				-.014			
	79.5	-.470				-.017			
	91.0	-.242				-.032			
0.555 b/2	0	-0.660				- -			
	1.5	-1.118				0.481			
	5.5	-1.117				.412			
	6.5	-1.090				.393			
	11.0	-1.097				.325			
	14.5	-1.078				.288			
	21.0	-1.060				.220			
	24.5	-1.034				.190			
	31.0	-1.010				.134			
	34.5	-.980				.110			
	41.0	-.935				.071			
	44.5	-.898				.049			
	51.0	-.853				.010			
	59.5	-.790				-.031			
	71.0	-.732				-.050			
	79.5	-.680				-.074			
	91.0	-.586				-.141			

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TABLE X.- CONCLUDED.

(c) α_u, 12°, 16°, 20°, 24° - Concluded.

Semi-span sta.	Percent chord	UPPER SURFACE Angle of attack 12°	16°	20°	24°	LOWER SURFACE Angle of attack 12°	16°	20°	24°
0.707 b/2	0	-0.810				- -			
	1.5	-.923				0.440			
	5.5	-.910				.400			
	6.5	-.887				.380			
	11.0	-.882				.304			
	14.5	-.855				.269			
	21.0	-.845				.200			
	24.5	-.819				.169			
	31.0	-.808				.115			
	34.5	-.789				.090			
	41.0	-.778				.040			
	44.5	-.757				.010			
	51.0	-.745				-.038			
	59.5	-.707				-.099			
	71.0	-.672				-.135			
	79.5	-.630				-.183			
	91.0	-.565				-.259			
0.831 b/2	0	-0.610				- -			
	1.5	-.730				0.411			
	5.5	-.728				.362			
	6.5	-.716				.353			
	11.0	-.716				.280			
	14.5	-.696				- -			
	21.0	-.690				.160			
	24.5	-.675				.128			
	31.0	-.670				.059			
	34.5	-.648				.016			
	41.0	-.645				-.042			
	44.5	-.625				-.082			
	51.0	-.622				-.135			
	59.5	-.593				-.217			
	71.0	-.575				-.244			
	79.5	-.546				-.260			
	91.0	-.520				-.305			
0.924 b/2	0	-0.715				- -			
	1.5	-.613				0.380			
	5.5	-.610				.328			
	6.5	-.593				.312			
	11.0	-.599				.220			
	14.5	-.580				.155			
	21.0	-.575				.053			
	24.5	-.555				-.021			
	31.0	-.552				-.085			
	34.5	-.532				-.146			
	41.0	-.530				-.190			
	44.5	-.508				-.231			
	51.0	-.508				-.252			
	59.5	-.475				-.268			
	71.0	-.478				-.262			
	79.5	-.458				-.270			
	91.0	-.447				-.298			

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TABLE XI.- PRESSURE COEFFICIENTS AT SEVEN SEMISPAN STATIONS OF THE WING. M_o, 0.90; R, 4,000,000.

(a) α_u, 0°, 1°, 2°, 3°.

Semi-span sta.	Percent chord	UPPER SURFACE				LOWER SURFACE			
		Angle of attack				Angle of attack			
		0°	1°	2°	3°	0°	1°	2°	3°
0.086 b/2	0	0.565	0.565	0.559	0.537	- -	- -	- -	- -
	1.5	.120	.036	-.050	-.156	0.082	0.150	0.222	0.278
	5.5	.034	-.017	-.060	-.111	.028	.069	.118	.158
	6.5	.007	-.041	-.081	-.134	-.004	.036	.086	.122
	11.0	-.019	-.060	-.094	-.139	-.022	.010	.052	.086
	14.5	-.050	-.089	-.121	-.163	-.049	-.011	.030	.059
	21.0	-.069	-.100	-.130	-.169	-.064	-.037	.006	.032
	24.5	-.087	-.124	-.150	-.189	-.089	-.060	-.021	.007
	31.0	-.101	-.136	-.160	-.193	-.113	-.089	-.050	-.021
	34.5	-.140	-.176	-.202	-.240	-.144	-.118	-.077	-.050
	41.0	-.179	-.212	-.237	-.279	-.172	-.146	-.105	-.080
	44.5	-.209	-.249	-.269	-.309	- -	- -	- -	- -
	51.0	-.219	-.269	-.292	-.334	-.215	-.189	-.150	-.125
	59.5	-.220	-.271	-.297	-.341	-.240	-.221	-.179	-.157
	71.0	-.195	-.229	-.249	-.294	-.210	-.190	-.150	-.132
	79.5	-.111	-.140	-.151	-.171	-.121	-.109	-.080	-.070
	91.0	-.030	-.045	-.049	-.060	-.030	-.030	-.019	-.016
0.195 b/2	0	0.488	0.477	0.450	0.394	- -	- -	- -	- -
	1.5	.055	-.056	-.173	-.315	0.090	0.185	0.270	0.337
	5.5	-.031	-.095	-.154	-.230	-.032	.023	.084	.136
	6.5	-.055	-.118	-.176	-.245	-.056	-.007	.051	.100
	11.0	-.077	-.127	-.173	-.223	-.077	-.037	.010	.051
	14.5	-.101	-.150	-.190	-.240	-.104	-.069	-.019	.017
	21.0	-.126	-.170	-.207	-.251	-.124	-.092	-.051	-.018
	24.5	-.147	-.190	-.225	-.273	-.147	-.117	-.075	-.039
	31.0	-.167	-.205	-.239	-.282	-.180	-.150	-.108	-.075
	34.5	-.194	-.240	-.270	-.308	-.204	-.176	-.134	-.103
	41.0	-.234	-.280	-.311	-.362	-.227	-.203	-.155	-.128
	44.5	-.253	-.302	-.337	-.390	-.240	-.213	-.170	-.140
	51.0	-.245	-.296	-.330	-.391	-.241	-.240	-.198	-.172
	59.5	-.224	-.267	-.303	-.361	-.240	-.214	-.173	-.152
	71.0	-.180	-.215	-.227	-.246	-.185	-.151	-.124	-.111
	79.5	-.070	-.090	-.097	-.111	-.070	-.073	-.062	-.053
	91.0	.010	0	0	-.009	.011	.006	.012	.013
0.382 b/2	0	0.440	0.422	0.375	0.289	- -	- -	- -	- -
	1.5	-.016	-.153	-.323	-.525	-0.052	0.054	0.147	0.220
	5.5	-.109	-.195	-.275	-.381	-.119	-.043	.029	.075
	6.5	-.131	-.215	-.287	-.379	-.132	-.065	.006	.060
	11.0	-.153	-.221	-.280	-.349	-.155	-.098	-.037	.008
	14.5	-.170	-.234	-.295	-.362	-.176	-.124	-.067	-.022
	21.0	-.197	-.253	-.291	-.357	-.200	-.153	-.101	-.062
	24.5	-.212	-.275	-.322	-.377	-.210	-.170	-.119	-.079
	31.0	-.229	-.287	-.337	-.393	-.243	-.203	-.150	-.111
	34.5	-.232	-.287	-.337	-.398	-.263	-.220	-.170	-.134
	41.0	-.262	-.317	-.360	-.441	-.257	-.220	-.167	-.141
	44.5	-.270	-.318	-.357	-.441	-.256	-.223	-.179	-.153
	51.0	-.245	-.292	-.330	-.400	-.262	-.234	-.189	-.168
	59.5	-.215	-.253	-.287	-.270	-.215	-.180	-.149	-.135
	71.0	-.103	-.118	-.130	-.166	-.097	-.103	-.088	-.080
	79.5	-.040	-.053	-.058	-.074	-.033	-.032	-.020	-.020
	91.0	.043	.035	.033	.025	-.047	.047	.055	.049
0.555 b/2	0	0.433	0.425	0.375	0.279	- -	- -	- -	- -
	1.5	-.053	-.330	-.537	-.687	-0.084	0.041	0.153	0.240
	5.5	-.145	-.256	-.362	-.495	-.140	-.058	.036	.095
	6.5	-.168	-.275	-.375	-.500	-.160	-.080	.005	.070
	11.0	-.178	-.260	-.346	-.456	-.194	-.122	-.050	.005
	14.5	-.195	-.275	-.346	-.417	-.203	-.140	-.070	-.020
	21.0	-.220	-.289	-.354	-.435	-.220	-.167	-.107	-.060
	24.5	-.222	-.291	-.351	-.430	-.231	-.180	-.123	-.076
	31.0	-.228	-.289	-.348	-.440	-.246	-.202	-.145	-.109
	34.5	-.232	-.285	-.337	-.425	-.253	-.210	-.152	-.120
	41.0	-.253	-.304	-.343	-.415	-.246	-.210	-.157	-.132
	44.5	-.247	-.295	-.335	-.354	-.237	-.203	-.158	-.135
	51.0	-.227	-.270	-.307	-.307	-.222	-.195	-.158	-.137
	59.5	-.188	-.218	-.186	-.224	-.193	-.159	-.137	-.124
	71.0	-.084	-.102	-.118	-.125	-.075	-.082	-.067	-.061
	79.5	-.020	-.033	-.035	-.037	-.015	-.017	-.005	-.010
	91.0	.064	.056	.067	.056	.065	.060	.070	.056

TABLE XI.- CONTINUED.

(a) α_u, 0°, 1°, 2°, 3° - Concluded.

Semi-span sta.	Percent chord	UPPER SURFACE Angle of attack 0°	1°	2°	3°	LOWER SURFACE Angle of attack 0°	1°	2°	3°
0.707 b/2	0	0.429	0.402	0.315	0.180	- -	- -	- -	- -
	1.5	-.060	-.274	-.534	-.880	-0.075	0.080	0.205	0.290
	5.5	-.170	-.300	-.436	-.611	-.163	-.060	.038	.109
	6.5	-.180	-.309	-.447	-.603	-.170	-.077	.020	.086
	11.0	-.174	-.267	-.367	-.481	-.202	-.125	-.042	.012
	14.5	-.199	-.286	-.370	-.481	-.206	-.137	-.062	-.010
	21.0	-.213	-.289	-.352	-.470	-.217	-.157	-.095	-.048
	24.5	-.216	-.289	-.350	-.437	-.225	-.170	-.110	-.068
	31.0	-.225	-.286	-.341	-.379	-.230	-.184	-.126	-.092
	34.5	-.227	-.284	-.333	-.363	-.227	-.189	-.130	-.102
	41.0	-.240	-.284	-.320	-.363	-.223	-.192	-.143	-.120
	44.5	-.238	-.280	-.297	-.348	-.225	-.199	-.153	-.131
	51.0	-.213	-.253	-.254	-.285	-.215	-.194	-.160	-.142
	59.5	-.183	-.209	-.195	-.195	-.183	-.160	-.135	-.130
	71.0	-.061	-.072	-.084	-.080	-.050	-.066	-.056	-.063
	79.5	.002	-.007	-.007	-.007	.005	-.002	.003	-.008
	91.0	.080	.078	.077	.077	.086	.080	.080	-.067
0.831 b/2	0	0.410	0.443	0.391	0.284	- -	- -	- -	- -
	1.5	-.058	-.290	-.565	-.952	-0.081	0.088	0.220	0.305
	5.5	-.161	-.310	-.457	-.748	-.171	-.063	.035	.105
	6.5	-.163	-.302	-.446	-.690	-.173	-.068	.030	.099
	11.0	-.174	-.274	-.379	-.499	-.191	-.110	-.030	.024
	14.5	-.188	-.281	-.373	-.471	- -	- -	- -	- -
	21.0	-.207	-.279	-.348	-.405	-.211	-.154	-.090	-.050
	24.5	-.216	-.285	-.342	-.406	-.216	-.164	-.102	-.062
	31.0	-.220	-.274	-.309	-.372	-.229	-.169	-.131	-.106
	34.5	-.233	-.284	-.310	-.368	-.239	-.204	-.157	-.130
	41.0	-.238	-.275	-.287	-.302	-.230	-.209	-.168	-.153
	44.5	-.218	-.250	-.223	-.226	-.210	-.201	-.173	-.168
	51.0	-.193	-.221	-.201	-.202	-.187	-.175	-.150	-.148
	59.5	-.132	-.107	-.126	-.129	-.140	-.134	-.112	-.118
	71.0	-.030	-.047	-.047	-.046	-.017	-.032	-.032	-.043
	79.5	.031	.022	.027	.022	.041	.034	.030	.016
	91.0	.103	.099	.101	.097	.111	.002	.100	.082
0.924 b/2	0	0.434	0.352	0.191	-0.022	- -	- -	- -	- -
	1.5	.001	-.240	-.537	-.931	-0.109	0.073	0.208	0.290
	5.5	-.171	-.320	-.475	-.764	-.185	-.063	.040	.110
	6.5	-.186	-.328	-.470	-.740	-.188	-.071	.031	.100
	11.0	-.195	-.375	-.394	-.443	-.212	-.127	-.046	.010
	14.5	-.238	-.328	-.410	-.472	-.245	-.170	-.099	-.050
	21.0	-.253	-.322	-.380	-.469	-.271	-.222	-.163	-.132
	24.5	-.219	-.269	-.230	-.223	-.233	-.213	-.180	-.177
	31.0	-.197	-.218	-.205	-.217	-.206	-.193	-.167	-.166
	34.5	-.179	-.192	-.207	-.220	-.184	-.176	-.156	-.151
	41.0	-.184	-.202	-.218	-.232	-.175	-.168	-.155	-.152
	44.5	-.172	-.180	-.190	-.206	-.163	-.158	-.145	-.150
	51.0	-.140	-.139	-.149	-.162	-.146	-.143	-.131	-.139
	59.5	-.050	-.076	-.078	-.088	-.053	-.076	-.084	-.079
	71.0	.001	-.006	-.002	-.012	.010	.007	.006	-.016
	79.5	.058	.054	.052	.040	.063	.051	.046	.027
	91.0	.113	.110	.109	.093	.126	.112	.104	.087

TABLE XI.- CONTINUED.

(b) α_u, 4°, 6°, 8°, 10°.

Semi-span sta.	Percent chord	UPPER SURFACE Angle of attack 4°	6°	8°	10°	LOWER SURFACE Angle of attack 4°	6°	8°	10°
0.086 b/2	0	0.507	0.418	0.307	0.200	- -	- -	- -	- -
	1.5	-.267	-.516	-.780	-1.130	0.332	0.422	0.501	0.570
	5.5	-.165	-.262	-.355	-.442	.200	.278	.354	.428
	6.5	-.181	-.281	-.370	-.434	.161	.231	.315	.385
	11.0	-.172	-.251	-.323	-.400	.120	.190	.269	.321
	14.5	-.199	-.270	-.350	-.430	.092	.148	.223	.286
	21.0	-.201	-.270	-.332	-.409	.061	.121	.182	.240
	24.5	-.220	-.285	-.340	-.411	.040	.098	.154	.210
	31.0	-.216	-.288	-.337	-.404	.008	.061	.118	.170
	34.5	-.264	-.343	-.397	-.458	-.020	.034	.090	.140
	41.0	-.310	-.382	-.440	-.498	-.050	.006	.060	.104
	44.5	-.340	-.411	-.479	-.538	- -	- -	- -	- -
	51.0	-.365	-.439	-.499	-.555	-.097	-.050	.002	.044
	59.5	-.383	-.457	-.514	-.575	-.130	-.075	-.021	.021
	71.0	-.340	-.465	-.560	-.630	-.110	-.064	-.023	.009
	79.5	-.194	-.290	-.422	-.553	-.056	-.027	-.002	.011
	91.0	-.073	-.114	-.176	-.255	-.012	-.001	.001	-.007
0.195 b/2	0	0.327	0.159	-0.003	-0.150	- -	- -	- -	- -
	1.5	-.463	-.795	-1.076	-1.208	0.393	0.476	0.520	0.546
	5.5	-.298	-.410	-.651	-.941	.185	.278	.356	.421
	6.5	-.309	-.449	-.579	-.882	.149	.237	.307	.379
	11.0	-.273	-.374	-.489	-.678	.094	.173	.243	.310
	14.5	-.274	-.375	-.457	-.584	.056	.134	.202	.262
	21.0	-.259	-.367	-.438	-.537	.021	.092	.153	.212
	24.5	-.295	-.360	-.457	-.536	0	.070	.126	.181
	31.0	-.317	-.398	-.472	-.538	-.038	.024	.081	.132
	34.5	-.339	-.421	-.493	-.560	-.067	-.005	.050	.102
	41.0	-.383	-.467	-.538	-.601	-.092	-.033	.020	.070
	44.5	-.420	-.499	-.569	-.635	-.108	-.049	.004	.051
	51.0	-.428	-.505	-.575	-.640	-.139	-.082	-.030	.017
	59.5	-.424	-.528	-.597	-.661	-.125	-.075	-.033	0
	71.0	-.260	-.402	-.581	-.687	-.091	-.055	-.027	-.010
	79.5	-.131	-.180	-.267	-.400	-.045	-.023	-.010	-.013
	91.0	-.011	-.033	-.075	-.132	.012	.015	.009	-.013
0.382 b/2	0	0.189	-0.030	-0.217	-0.403	- -	- -	- -	- -
	1.5	-.727	-1.150	-1.328	-1.252	0.283	0.380	0.442	0.486
	5.5	-.485	-.780	-1.068	-1.134	.141	.238	.313	.373
	6.5	-.462	-.638	-1.117	-1.230	.117	.210	.284	.348
	11.0	-.402	-.556	-.765	-.982	.059	.145	.217	.279
	14.5	-.425	-.546	-.648	-.962	.025	.111	.179	.240
	21.0	-.401	-.516	-.631	-.896	-.013	.062	.129	.185
	24.5	-.428	-.529	-.618	-.830	-.032	.035	.100	.155
	31.0	-.437	-.534	-.626	-.815	-.078	-.010	.052	.102
	34.5	-.449	-.542	-.631	-.767	-.096	-.028	.030	.078
	41.0	-.502	-.595	-.671	-.788	-.108	-.047	.005	.049
	44.0	-.512	-.626	-.690	-.764	-.120	-.063	-.014	.025
	51.0	-.498	-.613	-.703	-.767	-.138	-.087	-.040	-.010
	59.5	-.291	-.532	-.714	-.745	-.113	-.073	-.043	-.028
	71.0	-.159	-.186	-.254	-.422	-.070	-.047	-.032	-.035
	79.5	-.067	-.069	-.097	-.238	-.016	-.008	-.005	-.021
	91.0	.031	.029	-.011	-.137	.042	.038	.021	-.019
0.555 b/2	0	0.174	-0.043	-0.235	-0.420	- -	- -	- -	- -
	1.5	-.981	-1.315	-1.445	-1.340	0.303	0.392	0.442	0.470
	5.5	-.542	-1.217	-1.366	-1.332	.153	.251	.317	.370
	6.5	-.507	-1.156	-1.340	-1.314	.133	.230	.297	.348
	11.0	-.509	-.655	-1.325	-1.217	.085	.156	.223	.276
	14.5	-.507	-.577	-1.270	-1.159	.035	.123	.185	.240
	21.0	-.510	-.602	-.740	-1.081	-.012	.074	.130	.185
	24.5	-.504	-.601	-.723	-1.044	-.033	.047	.102	.146
	31.0	-.511	-.612	-.683	-.998	-.070	.003	.054	.090
	34.5	-.525	-.620	-.688	-.995	-.082	-.014	.031	.070
	41.0	-.547	-.684	-.744	-.916	-.097	-.036	.003	.032
	44.5	-.457	-.715	-.720	-.867	-.100	-.047	-.010	.013
	51.0	-.298	-.635	-.713	-.829	-.112	-.063	-.035	-.016
	59.5	-.210	-.197	-.273	-.729	-.103	-.069	-.052	-.051
	71.0	-.113	-.080	-.158	-.613	-.060	-.030	-.030	-.052
	79.5	-.027	-.012	-.108	-.520	-.006	.005	-.013	-.056
	91.0	.060	.062	-.022	-.345	.054	.048	.013	-.074

NACA

TABLE XI.- CONTINUED.

(b) α_u, 4°, 6°, 8°, 10° - Concluded.

Semi-span sta.	Percent chord	UPPER SURFACE Angle of attack 4°	6°	8°	10°	LOWER SURFACE Angle of attack 4°	6°	8°	10°
0.707 b/2	0	0.060	-0.177	-0.384	-0.585	- -	- -	- -	- -
	1.5	-1.137	-1.355	-1.454	-.930	0.348	0.420	0.446	0.450
	5.5	-.963	-1.280	-1.402	-.945	.170	.266	.323	.366
	6.5	-.918	-1.275	-1.387	-.930	.146	.240	.298	.342
	11.0	-.550	-1.225	-1.250	-.932	.070	.158	.218	.261
	14.5	-.578	-1.185	-1.163	-.934	.041	.130	.185	.226
	21.0	-.565	-.634	-1.091	-.922	-.004	.070	.126	.160
	24.5	-.560	-.629	-1.020	-.903	-.020	.050	.096	.131
	31.0	-.530	-.665	-.923	-.870	-.054	.010	.050	.080
	34.5	-.444	-.685	-.851	-.837	-.065	-.005	.031	.055
	41.0	-.330	-.727	-.770	-.796	-.090	-.035	-.005	.012
	44.5	-.312	-.464	-.718	-.762	-.102	-.053	-.026	-.016
	51.0	-.263	-.176	-.640	-.717	-.117	-.075	-.055	-.054
	59.5	-.177	-.144	-.543	-.659	-.114	-.089	-.083	-.100
	71.0	-.070	-.074	-.380	-.582	-.055	-.046	-.065	-.117
	79.5	0	-.007	-.270	-.525	-.003	-.009	-.045	-.140
	91.0	.080	.075	-.090	-.443	.061	.049	-.005	-.179
0.831 b/2	0	0.170	-0.050	-0.244	-0.408	- -	- -	- -	- -
	1.5	-1.167	-1.358	-.922	-.788	0.350	0.407	0.426	0.427
	5.5	-1.032	-1.330	-.927	-.790	.161	.245	.300	.335
	6.5	-1.043	-1.337	-.937	-.795	.151	.237	.292	.324
	11.0	-.701	-1.261	-.934	-.796	.071	.149	.205	.239
	14.5	-.520	-1.236	-.923	-.787	- -	- -	- -	- -
	21.0	-.548	-1.172	-.890	-.766	-.013	.058	.103	.132
	24.5	-.449	-1.029	-.818	-.727	-.030	.034	.081	.102
	31.0	-.330	-.570	-.770	-.714	-.072	-.018	.020	.038
	34.5	-.315	-.495	-.710	-.684	-.101	-.051	-.018	-.001
	41.0	-.269	-.280	-.651	-.673	-.131	-.090	-.059	-.056
	44.5	-.230	-.310	-.615	-.649	-.154	-.121	-.092	-.098
	51.0	-.200	-.223	-.570	-.633	-.143	-.128	-.117	-.134
	59.5	-.128	-.125	-.507	-.589	-.118	-.121	-.140	-.199
	71.0	-.048	-.040	-.412	-.548	-.048	-.057	-.098	-.199
	79.5	.018	.022	-.339	-.507	.009	-.002	-.069	-.195
	91.0	.090	.083	-.246	-.446	.073	.058	-.065	-.223
0.924 b/2	0	-0.200	-0.510	-0.720	-0.775	- -	- -	- -	- -
	1.5	-1.133	-1.232	-.753	-.652	0.335	0.381	0.401	0.402
	5.5	-1.066	-1.182	-.759	-.660	.161	.235	.282	.308
	6.5	-1.066	-1.141	-.755	-.641	.151	.223	.270	.291
	11.0	-1.011	-1.021	-.751	-.636	.050	.121	.170	.198
	14.5	-.781	-.932	-.719	-.603	-.010	.058	.108	.130
	21.0	-.331	-.851	-.698	-.595	-.100	-.040	.010	.030
	24.5	-.235	-.750	-.651	-.570	-.160	-.109	-.061	-.043
	31.0	-.215	-.669	-.627	-.568	-.170	-.145	-.110	-.100
	34.5	-.191	-.589	-.587	-.547	-.156	-.170	-.149	-.156
	41.0	-.220	-.490	-.560	-.549	-.153	-.169	-.170	-.195
	44.5	-.203	-.428	-.530	-.522	-.150	-.164	-.180	-.225
	51.0	-.170	-.312	-.508	-.522	-.139	-.144	-.173	-.239
	59.5	-.109	-.230	-.450	-.475	-.088	-.098	-.148	-.227
	71.0	-.039	-.116	-.404	-.463	-.030	-.040	-.110	-.203
	79.5	.001	-.131	-.367	-.420	.011	.0	-.095	-.196
	91.0	.058	-.051	-.329	-.407	.073	.050	-.101	-.220

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TABLE XI.- CONTINUED.

(c) α_u, 12°, 16°, 20°, 24°.

Semi-span sta.	Percent chord	UPPER SURFACE Angle of attack 12°	16°	20°	24°	LOWER SURFACE Angle of attack 12°	16°	20°	24°
0.086 b/2	0	0.076				- -			
	1.5	-1.285				0.121			
	5.5	-.619				.484			
	6.5	-.504				.446			
	11.0	-.471				.380			
	14.5	-.498				.340			
	21.0	-.461				.290			
	24.5	-.451				.261			
	31.0	-.476				.210			
	34.5	-.523				.184			
	41.0	-.568				.147			
	44.5	-.605				- -			
	51.0	-.630				.080			
	59.5	-.648				.055			
	71.0	-.698				.029			
	79.5	-.667				.016			
	91.0	-.392				-.024			
0.195 b/2	0	-0.287				- -			
	1.5	-1.193				0.557			
	5.5	-1.173				.480			
	6.5	-1.140				.439			
	11.0	-1.053				.369			
	14.5	-.988				.323			
	21.0	-.840				.262			
	24.5	-.580				.233			
	31.0	-.537				.180			
	34.5	-.576				.149			
	41.0	-.645				.111			
	44.5	-.680				.090			
	51.0	-.694				.050			
	59.5	-.705				.023			
	71.0	-.750				0			
	79.5	-.609				-.017			
	91.0	-.243				-.055			
0.382 b/2	0	-0.563				- -			
	1.5	-1.257				0.511			
	5.5	-1.173				.425			
	6.5	-1.272				.397			
	11.0	-1.140				.330			
	14.5	-1.139				.290			
	21.0	-1.117				.233			
	24.5	-1.100				.200			
	31.0	-1.088				.145			
	34.5	-1.054				.115			
	41.0	-1.013				.080			
	44.5	-.980				.050			
	51.0	-.915				.012			
	59.5	-.857				-.020			
	71.0	-.731				-.044			
	79.5	-.453				-.050			
	91.0	-.253				-.062			
0.555 b/2	0	-0.590				- -			
	1.5	-1.264				0.480			
	5.5	-1.256				.406			
	6.5	-1.226				.384			
	11.0	-1.226				.315			
	14.5	-1.200				.274			
	21.0	-1.181				.210			
	24.5	-1.157				.175			
	31.0	-1.140				.119			
	34.5	-1.115				.092			
	41.0	-1.090				.051			
	44.5	-1.058				.027			
	51.0	-1.022				-.015			
	59.5	-.923				-.060			
	71.0	-.830				-.077			
	79.5	-.767				-.098			
	91.0	-.645				-.158			

TABLE XI.- CONCLUDED.

(c) α_u, 12°, 16°, 20°, 24° - Concluded.

Semi-span sta.	Percent chord	UPPER SURFACE Angle of attack 12°	16°	20°	24°	LOWER SURFACE Angle of attack 12°	16°	20°	24°
0.707 b/2	0	-0.749				- -			
	1.5	-1.075				0.436			
	5.5	-1.077				.386			
	6.5	-1.056				.366			
	11.0	-1.056				.288			
	14.5	-1.035				.250			
	21.0	-1.023				.183			
	24.5	-.999				.149			
	31.0	-.980				.095			
	34.5	-.953				.068			
	41.0	-.927				.018			
	44.5	-.893				-.014			
	51.0	-.860				-.058			
	59.5	-.812				-.120			
	71.0	-.765				-.160			
	79.5	-.721				-.213			
	91.0	-.664				-.293			
0.831 b/2	0	-0.593				- -			
	1.5	-.902				0.409			
	5.5	-.900				.357			
	6.5	-.901				.342			
	11.0	-.899				.262			
	14.5	-.881				- -			
	21.0	-.875				.148			
	24.5	-.853				.113			
	31.0	-.849				.044			
	34.5	-.820				.003			
	41.0	-.812				-.057			
	44.5	-.790				-.107			
	51.0	-.777				-.152			
	59.5	-.739				-.250			
	71.0	-.705				-.292			
	79.5	-.667				-.325			
	91.0	-.630				-.381			
0.924 b/2	0	-0.902				- -			
	1.5	-.783				0.375			
	5.5	-.780				.320			
	6.5	-.762				.306			
	11.0	-.762				.212			
	14.5	-.742				.148			
	21.0	-.742				.040			
	24.5	-.720				-.040			
	31.0	-.718				-.108			
	34.5	-.697				-.180			
	41.0	-.695				-.232			
	44.5	-.670				-.286			
	51.0	-.665				-.318			
	59.5	-.622				-.358			
	71.0	-.610				-.360			
	79.5	-.578				-.367			
	91.0	-.562				-.390			

TABLE XII.- PRESSURE COEFFICIENTS AT SEVEN SEMISPAN STATIONS OF THE WING. M_0, 0.92; R, 4,000,000.

(a) α_u, 0°, 1°, 2°, 3°.

Semi-span sta.	Percent chord	UPPER SURFACE, Angle of attack 0°	1°	2°	3°	LOWER SURFACE, Angle of attack 0°	1°	2°	3°
0.086 b/2	0	0.576	0.577	0.568	0.549	- -	- -	- -	- -
	1.5	.137	.052	-.036	-.133	0.102	0.169	0.231	0.287
	5.5	.051	.002	-.043	-.093	.041	.085	.127	.167
	6.5	.021	-.025	-.070	-.119	.012	.050	.093	.131
	11.0	-.003	-.043	-.081	-.122	-.010	.024	.060	.093
	14.5	-.034	-.071	-.109	-.149	-.031	-.001	.036	.067
	21.0	-.052	-.088	-.120	-.152	-.050	-.021	.009	.040
	24.5	-.072	-.109	-.141	-.172	-.075	-.049	-.015	.013
	31.0	-.088	-.120	-.149	-.177	-.101	-.075	-.044	-.018
	34.5	-.132	-.167	-.198	-.231	-.133	-.107	-.075	-.046
	41.0	-.167	-.200	-.233	-.269	-.162	-.135	-.105	-.077
	44.5	-.202	-.238	-.266	-.299	- -	- -	- -	- -
	51.0	-.228	-.263	-.293	-.335	-.207	-.182	-.153	-.128
	59.5	-.237	-.280	-.319	-.356	-.246	-.223	-.192	-.166
	71.0	-.205	-.251	-.299	-.351	-.229	-.204	-.170	-.144
	79.5	-.119	-.149	-.180	-.230	-.130	-.113	-.094	-.082
	91.0	-.033	-.047	-.059	-.080	-.034	-.031	-.028	-.026
0.195 b/2	0	0.497	0.488	0.459	0.410	- -	- -	- -	- -
	1.5	.070	-.038	-.155	-.289	0.103	0.197	0.274	0.342
	5.5	-.015	-.080	-.142	-.211	-.021	.038	.090	.142
	6.5	-.045	-.102	-.164	-.228	-.043	.009	.057	.106
	11.0	-.063	-.113	-.160	-.208	-.066	-.023	.018	.060
	14.5	-.089	-.135	-.180	-.223	-.093	-.054	-.017	.025
	21.0	-.116	-.156	-.198	-.232	-.116	-.081	-.047	-.009
	24.5	-.139	-.180	-.219	-.260	-.138	-.104	-.070	-.030
	31.0	-.160	-.196	-.235	-.271	-.171	-.141	-.108	-.070
	34.5	-.192	-.230	-.262	-.298	-.201	-.170	-.137	-.100
	41.0	-.238	-.279	-.319	-.343	-.227	-.196	-.161	-.127
	44.5	-.260	-.304	-.348	-.380	-.238	-.210	-.178	-.142
	51.0	-.260	-.308	-.357	-.395	-.271	-.243	-.215	-.180
	59.5	-.241	-.293	-.359	-.410	-.262	-.231	-.190	-.162
	71.0	-.190	-.230	-.289	-.350	-.200	-.157	-.138	-.118
	79.5	-.070	-.086	-.100	-.116	-.068	-.072	-.070	-.060
	91.0	.012	.006	0	-.008	.009	.009	.008	.009
0.382 b/2	0	0.445	0.431	0.383	0.308	- -	- -	- -	- -
	1.5	-.010	-.151	-.310	-.492	-0.039	0.060	0.142	0.221
	5.5	-.100	-.184	-.270	-.368	-.106	-.038	.025	.089
	6.5	-.124	-.202	-.277	-.361	-.122	-.058	.001	.065
	11.0	-.148	-.212	-.277	-.333	-.147	-.092	-.042	.011
	14.5	-.167	-.232	-.294	-.349	-.169	-.120	-.071	-.020
	21.0	-.192	-.243	-.295	-.345	-.193	-.150	-.107	-.061
	24.5	-.217	-.275	-.322	-.362	-.210	-.171	-.130	-.080
	31.0	-.238	-.298	-.350	-.383	-.242	-.208	-.164	-.120
	34.5	-.242	-.305	-.360	-.393	-.270	-.235	-.190	-.140
	41.0	-.279	-.345	-.412	-.451	-.283	-.240	-.187	-.150
	44.5	-.284	-.350	-.420	-.476	-.275	-.231	-.192	-.152
	51.0	-.261	-.319	-.400	-.471	-.270	-.248	-.210	-.176
	59.5	-.224	-.274	-.350	-.446	-.225	-.192	-.169	-.142
	71.0	-.106	-.113	-.110	-.154	-.101	-.103	-.099	-.083
	79.5	-.033	-.049	-.051	-.059	-.029	-.031	-.028	-.019
	91.0	.049	.041	.034	.038	.050	.051	.053	.055
0.555 b/2	0	0.433	0.427	0.382	0.298	- -	- -	- -	- -
	1.5	-.054	-.229	-.420	-.654	-0.079	0.040	0.142	0.227
	5.5	-.153	-.259	-.361	-.475	-.139	-.060	.018	.085
	6.5	-.174	-.280	-.379	-.481	-.160	-.080	-.004	.061
	11.0	-.184	-.271	-.354	-.440	-.196	-.130	-.061	-.001
	14.5	-.206	-.288	-.359	-.446	-.210	-.149	-.082	-.029
	21.0	-.232	-.308	-.380	-.432	-.235	-.177	-.120	-.070
	24.5	-.239	-.312	-.385	-.426	-.240	-.190	-.136	-.087
	31.0	-.243	-.326	-.402	-.450	-.254	-.210	-.160	-.118
	34.5	-.240	-.313	-.407	-.471	-.262	-.220	-.170	-.131
	41.0	-.269	-.320	-.420	-.528	-.260	-.221	-.172	-.143
	44.5	-.262	-.310	-.391	-.542	-.250	-.214	-.167	-.145
	51.0	-.240	-.284	-.359	-.480	-.229	-.200	-.167	-.145
	59.5	-.197	-.224	-.162	-.191	-.194	-.160	-.144	-.130
	71.0	-.088	-.101	-.111	-.104	-.078	-.081	-.070	-.062
	79.5	-.020	-.029	-.033	-.024	-.011	-.015	-.010	-.010
	91.0	.070	.065	.061	.066	.072	.070	.070	.060

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TABLE XII.- CONTINUED.

(a) α_u, 0°, 1°, 2°, 3° - Concluded.

Semi-span sta.	Percent chord	UPPER SURFACE Angle of attack 0°	1°	2°	3°	LOWER SURFACE Angle of attack 0°	1°	2°	3°
0.707 b/2	0	0.428	0.400	0.320	0.204	- -	- -	- -	- -
	1.5	-.067	-.283	-.539	-.870	-0.072	0.077	0.191	0.277
	5.5	-.176	-.315	-.460	-.615	-.164	-.066	.022	.099
	6.5	-.189	-.330	-.479	-.639	-.174	-.081	.004	.073
	11.0	-.180	-.289	-.402	-.481	-.208	-.130	-.059	.002
	14.5	-.204	-.305	-.413	-.486	-.216	-.143	-.074	-.020
	21.0	-.222	-.301	-.418	-.494	-.224	-.167	-.108	-.058
	24.5	-.227	-.299	-.413	-.500	-.230	-.178	-.120	-.077
	31.0	-.233	-.299	-.391	-.512	-.237	-.189	-.140	-.096
	34.5	-.234	-.299	-.374	-.524	-.230	-.190	-.141	-.108
	41.0	-.243	-.298	-.343	-.512	-.228	-.193	-.150	-.125
	44.5	-.240	-.291	-.308	-.379	-.230	-.201	-.162	-.139
	51.0	-.219	-.262	-.234	-.230	-.220	-.201	-.165	-.146
	59.5	-.190	-.213	-.211	-.168	-.189	-.173	-.148	-.140
	71.0	-.057	-.068	-.079	-.067	-.042	-.061	-.060	-.065
	79.5	.012	.003	-.004	.003	.019	.008	.005	-.001
	91.0	.092	.086	.081	.086	.097	.089	.087	.072
0.831 b/2	0	0.412	0.443	0.388	0.297	- -	- -	- -	- -
	1.5	-.065	-.300	-.604	-.950	-0.077	0.091	0.213	0.291
	5.5	-.174	-.320	-.509	-.740	-.172	-.062	.030	.099
	6.5	-.174	-.313	-.503	-.719	-.172	-.065	.023	.091
	11.0	-.183	-.283	-.434	-.513	-.190	-.110	-.037	.018
	14.5	-.196	-.292	-.420	-.541	- -	- -	- -	- -
	21.0	-.213	-.290	-.386	-.545	-.213	-.151	-.098	-.054
	24.5	-.223	-.294	-.368	-.546	-.219	-.162	-.111	-.068
	31.0	-.227	-.282	-.316	-.474	-.234	-.190	-.143	-.108
	34.5	-.245	-.294	-.303	-.363	-.244	-.210	-.169	-.140
	41.0	-.260	-.300	-.322	-.257	-.253	-.229	-.190	-.170
	44.5	-.232	-.267	-.270	-.184	-.230	-.218	-.203	-.200
	51.0	-.202	-.232	-.178	-.168	-.193	-.176	-.160	-.170
	59.5	-.114	-.084	-.118	-.115	-.126	-.121	-.113	-.115
	71.0	-.024	-.035	-.040	-.039	-.016	-.023	-.030	-.038
	79.5	.037	.035	.032	.030	.046	.042	.034	.024
	91.0	.111	.110	.109	.107	.117	.112	.103	.090
0.924 b/2	0	0.439	0.355	0.180	-0.007	- -	- -	- -	- -
	1.5	-.002	-.249	-.585	-.918	-0.093	0.081	0.212	0.287
	5.5	-.161	-.330	-.527	-.800	-.177	-.059	.040	.109
	6.5	-.192	-.336	-.518	-.799	-.180	-.064	.032	.100
	11.0	-.201	-.302	-.438	-.614	-.206	-.122	-.048	.009
	14.5	-.245	-.332	-.430	-.531	-.240	-.168	-.098	-.049
	21.0	-.290	-.359	-.413	-.572	-.291	-.239	-.182	-.141
	24.5	-.250	-.308	-.332	-.325	-.274	-.260	-.232	-.212
	31.0	-.213	-.250	-.185	-.115	-.223	-.208	-.199	-.228
	34.5	-.176	-.166	-.182	-.144	-.185	-.178	-.164	-.185
	41.0	-.182	-.160	-.213	-.200	-.170	-.165	-.157	-.151
	44.5	-.170	-.174	-.198	-.197	-.160	-.153	-.148	-.138
	51.0	-.131	-.131	-.144	-.152	-.140	-.140	-.133	-.128
	59.5	-.054	-.066	-.074	-.081	-.054	-.060	-.072	-.071
	71.0	.005	.003	0	-.010	.015	.010	.007	-.010
	79.5	.060	.061	.058	.046	.069	.060	.050	.036
	91.0	.120	.122	.117	.097	.131	.121	.110	.093

NACA

TABLE XII.- CONTINUED.

(b) α_u, 4°, 6°, 8°, 10°.

Semi-span sta.	Percent chord	UPPER SURFACE Angle of attack 4°	6°	8°	10°	LOWER SURFACE Angle of attack 4°	6°	8°	10°
0.086 b/2	0	0.521	0.442	0.338	0.231	- -	- -	- -	- -
	1.5	-.238	-.472	-.734	-1.047	0.340	0.430	0.510	0.572
	5.5	-.141	-.237	-.335	-.407	.209	.282	.359	.426
	6.5	-.162	-.252	-.347	-.404	.171	.246	.319	.365
	11.0	-.154	-.230	-.300	-.369	.129	.196	.261	.322
	14.5	-.178	-.238	-.322	-.398	.101	.163	.224	.287
	21.0	-.183	-.244	-.317	-.381	.070	.127	.188	.240
	24.5	-.200	-.263	-.328	-.389	.043	.101	.159	.209
	31.0	-.201	-.260	-.314	-.380	.012	.068	.120	.165
	34.5	-.260	-.320	-.373	-.435	-.014	.040	.090	.133
	41.0	-.289	-.360	-.410	-.470	-.046	.008	.056	.098
	44.5	-.325	-.390	-.450	-.508	- -	- -	- -	- -
	51.0	-.353	-.416	-.475	-.529	-.101	-.050	-.002	.030
	59.5	-.380	-.440	-.492	-.550	-.140	-.088	-.033	.003
	71.0	-.404	-.475	-.541	-.600	-.122	-.080	-.038	-.015
	79.5	-.291	-.395	-.494	-.579	-.071	-.045	-.024	-.022
	91.0	-.115	-.175	-.255	-.488	-.030	-.028	-.031	-.053
0.195 b/2	0	0.350	0.197	0.045	-0.090	- -	- -	- -	- -
	1.5	-.450	-.730	-1.021	-1.100	0.397	0.478	0.530	0.556
	5.5	-.277	-.373	-.607	-.880	.191	.286	.360	.423
	6.5	-.289	-.417	-.535	-.819	.152	.238	.315	.378
	11.0	-.255	-.348	-.460	-.640	.100	.177	.247	.309
	14.5	-.269	-.343	-.430	-.550	.062	.135	.203	.261
	21.0	-.263	-.337	-.417	-.511	.024	.094	.157	.210
	24.5	-.275	-.359	-.420	-.505	.002	.067	.137	.177
	31.0	-.289	-.367	-.443	-.507	-.039	.025	.080	.127
	34.5	-.325	-.397	-.468	-.529	-.067	-.007	.049	.093
	41.0	-.373	-.450	-.513	-.572	-.096	-.039	.017	.057
	44.5	-.410	-.480	-.548	-.605	-.115	-.056	-.001	.037
	51.0	-.425	-.485	-.550	-.613	-.151	-.092	-.038	-.002
	59.5	-.457	-.516	-.573	-.627	-.140	-.090	-.049	-.025
	71.0	-.404	-.509	-.594	-.660	-.108	-.075	-.050	-.042
	79.5	-.195	-.287	-.434	-.604	-.060	-.047	-.040	-.057
	91.0	-.036	-.096	-.184	-.307	-.004	-.018	-.039	-.097
0.382 b/2	0	0.213	0.020	-0.161	-0.323	- -	- -	- -	- -
	1.5	-.700	-1.070	-1.283	-1.325	0.281	0.377	0.441	0.480
	5.5	-.454	-.740	-1.107	-1.226	.141	.235	.313	.367
	6.5	-.440	-.590	-1.163	-1.268	.113	.207	.282	.340
	11.0	-.380	-.522	-.697	-.954	.057	.143	.216	.270
	14.5	-.407	-.510	-.596	-.885	.020	.103	.175	.226
	21.0	-.390	-.501	-.589	-.707	-.020	.057	.126	.173
	24.5	-.414	-.500	-.574	-.675	-.040	.032	.097	.140
	31.0	-.432	-.511	-.590	-.680	-.066	-.019	.045	.086
	34.5	-.441	-.520	-.598	-.668	-.109	-.040	.020	.057
	41.0	-.500	-.568	-.650	-.714	-.120	-.059	-.007	.036
	44.5	-.525	-.601	-.670	-.725	-.137	-.079	-.030	0
	51.0	-.520	-.603	-.670	-.734	-.155	-.103	-.060	-.040
	59.5	-.555	-.642	-.707	-.770	-.133	-.097	-.072	-.070
	71.0	-.211	-.353	-.577	-.750	-.086	-.071	-.067	-.092
	79.5	-.071	-.136	-.210	-.510	-.029	-.030	-.042	-.097
	91.0	.034	-.003	-.047	-.280	.034	.016	-.016	-.116
0.555 b/2	0	0.202	0.012	-0.172	-0.335	- -	- -	- -	- -
	1.5	-.936	-1.224	-1.362	-1.417	0.287	0.380	0.434	0.459
	5.5	-.600	-1.127	-1.270	-1.355	.140	.237	.306	.350
	6.5	-.518	-1.078	-1.248	-1.335	.118	.213	.282	.326
	11.0	-.490	-.737	-1.271	-1.350	.049	.140	.208	.252
	14.5	-.502	-.568	-1.229	-1.317	.018	.105	.169	.211
	21.0	-.508	-.586	-.760	-1.239	-.030	.048	.110	.146
	24.5	-.507	-.592	-.695	-1.180	-.050	.029	.081	.113
	31.0	-.518	-.598	-.660	-.855	-.090	-.020	.031	.058
	34.5	-.530	-.602	-.661	-.902	-.102	-.038	.008	.030
	41.0	-.590	-.662	-.728	-.768	-.120	-.061	-.024	-.010
	44.5	-.619	-.702	-.763	-.780	-.125	-.072	-.040	-.032
	51.0	-.606	-.700	-.767	-.818	-.131	-.090	-.068	-.071
	59.5	-.270	-.568	-.707	-.849	-.125	-.100	-.090	-.116
	71.0	-.099	-.148	-.207	-.800	-.067	-.060	-.070	-.125
	79.5	-.011	-.038	-.143	-.458	-.020	-.024	-.052	-.132
	91.0	.070	.040	-.085	-.241	.047	.022	-.034	-.148

NACA

TABLE XII.- CONCLUDED.

(b) α_u, 4°, 6°, 8°, 10° - Concluded.

Semi-span sta.	Percent chord	UPPER SURFACE Angle of attack 4°	6°	8°	10°	LOWER SURFACE Angle of attack 4°	6°	8°	10°
0.707 b/2	0	0.095	-0.114	-0.311	-0.487	- -	- -	- -	- -
	1.5	-1.070	-1.263	-1.390	-1.379	0.331	0.401	0.434	0.437
	5.5	-.898	-1.180	-1.358	-1.360	.150	.242	.305	.335
	6.5	-.880	-1.189	-1.360	-1.357	.128	.215	.279	.309
	11.0	-.550	-1.139	-1.295	-1.325	.049	.132	.193	.225
	14.5	-.566	-1.102	-1.273	-1.315	.023	.102	.160	.188
	21.0	-.580	-.670	-1.208	-1.289	-.022	.046	.100	.120
	24.5	-.582	-.630	-1.068	-1.276	-.040	.022	.071	.088
	31.0	-.584	-.650	-.823	-1.247	-.073	-.017	.025	.035
	34.5	-.600	-.667	-.761	-1.221	-.088	-.032	.002	.010
	41.0	-.654	-.720	-.693	-1.165	-.110	-.064	-.036	-.040
	44.5	-.683	-.773	-.716	-1.162	-.124	-.082	-.059	-.070
	51.0	-.323	-.721	-.685	-1.030	-.137	-.106	-.090	-.113
	59.5	-.130	-.182	-.618	-.981	-.140	-.122	-.128	-.169
	71.0	-.040	-.074	-.487	-.675	-.079	-.087	-.120	-.189
	79.5	.019	-.033	-.390	-.368	-.016	-.045	-.115	-.214
	91.0	.086	.043	-.222	-.259	.060	.020	-.085	-.191
0.831 b/2	0	0.203	0.014	-0.169	-0.327	- -	- -	- -	- -
	1.5	-1.095	-1.280	-.904	-1.240	0.335	0.393	0.416	0.409
	5.5	-.978	-1.250	-.917	-1.251	.149	.228	.280	.301
	6.5	-.983	-1.257	-.921	-1.257	.138	.218	.271	.290
	11.0	-.817	-1.188	-.918	-1.247	.059	.131	.185	.204
	14.5	-.722	-1.160	-.909	-1.222	- -	- -	- -	- -
	21.0	-.618	-1.099	-.877	-1.183	-.025	.035	.080	.092
	24.5	-.625	-1.018	-.848	-1.210	-.041	.018	.057	.060
	31.0	-.630	-.729	-.804	-1.184	-.083	-.039	-.003	-.004
	34.5	-.637	-.629	-.745	-1.136	-.120	-.074	-.042	-.047
	41.0	-.370	-.610	-.706	-1.134	-.156	-.119	-.091	-.103
	44.5	-.151	-.530	-.689	-1.118	-.193	-.159	-.137	-.157
	51.0	-.100	-.358	-.652	-1.099	-.187	-.169	-.164	-.198
	59.5	-.070	-.269	-.585	-.980	-.131	-.172	-.220	-.298
	71.0	-.021	-.088	-.491	-.825	-.044	-.081	-.175	-.310
	79.5	.031	.010	-.412	-.796	.013	-.020	-.129	-.287
	91.0	.097	.082	-.312	-.626	.075	.041	-.120	-.240
0.924 b/2	0	-0.150	-0.413	-0.625	-0.776	- -	- -	- -	- -
	1.5	-1.062	-1.165	-.766	-1.150	0.326	.372	.391	.379
	5.5	-1.050	-1.118	-.771	-1.157	.150	.222	.270	.279
	6.5	-1.039	-1.082	-.772	-1.147	.140	.210	.258	.268
	11.0	-1.003	-.983	-.760	-1.130	.044	.110	.147	.168
	14.5	-.876	-.994	-.750	-1.145	-.016	.050	.092	.101
	21.0	-.630	-.836	-.726	-1.115	-.111	-.054	-.010	-.004
	24.5	-.612	-.783	-.688	-1.079	-.190	-.133	-.090	-.090
	31.0	-.200	-.730	-.659	-1.058	-.233	-.185	-.149	-.164
	34.5	-.070	-.684	-.630	-1.048	-.250	-.226	-.201	-.234
	41.0	-.099	-.607	-.608	-1.024	-.222	-.240	-.235	-.287
	44.5	-.119	-.551	-.582	-1.021	-.167	-.245	-.270	-.344
	51.0	-.123	-.447	-.559	-1.011	-.121	-.197	-.272	-.373
	59.5	-.090	-.324	-.499	-1.030	-.079	-.110	-.206	-.411
	71.0	-.026	-.161	-.442	-.993	-.020	-.046	-.154	-.374
	79.5	.008	-.159	-.390	-.959	.021	-.001	-.131	-.362
	91.0	.064	-.064	-.345	-.885	.061	.048	-.130	-.352

NACA

TABLE XIII.- PRESSURE COEFFICIENTS AT SEVEN SEMISPAN STATIONS OF THE WING. M_o, 0.93; R, 4,000,000.

(a) α_u, 0°, 1°, 2°, 3°.

Semi-span sta.	Percent chord	UPPER SURFACE				LOWER SURFACE			
		Angle of attack				Angle of attack			
		0°	1°	2°	3°	0°	1°	2°	3°
0.086 b/2	0	0.578	0.580	0.572	0.555	- -	- -	- -	- -
	1.5	.140	.057	-.030	-.125	0.107	0.169	0.232	0.288
	5.5	.051	.005	-.040	-.085	.045	.072	.130	.170
	6.5	.034	-.022	-.064	-.110	.013	.050	.095	.133
	11.0	-.002	-.040	-.076	-.118	-.007	.020	.062	.096
	14.5	-.034	-.070	-.103	-.142	-.030	-.001	.035	.070
	21.0	-.052	-.078	-.113	-.149	-.050	-.023	.010	.040
	24.5	-.073	-.106	-.125	-.168	-.075	-.039	-.015	.015
	31.0	-.088	-.120	-.143	-.171	-.103	-.080	-.046	-.016
	34.5	-.134	-.167	-.193	-.226	-.126	-.112	-.075	-.048
	41.0	-.168	-.203	-.230	-.263	-.170	-.146	-.108	-.080
	44.5	-.202	-.235	-.260	-.292	- -	- -	- -	- -
	51.0	-.230	-.267	-.287	-.320	-.230	-.204	-.176	-.138
	59.5	-.250	-.288	-.314	-.350	-.240	-.220	-.184	-.159
	71.0	-.234	-.285	-.310	-.363	-.250	-.223	-.170	-.147
	79.5	-.156	-.172	-.200	-.252	-.149	-.127	-.097	-.088
	91.0	-.042	-.059	-.070	-.099	-.042	-.040	-.030	-.030
0.195 b/2	0	0.499	0.487	0.462	0.416	- -	- -	- -	- -
	1.5	.070	-.040	-.151	-.280	0.105	0.193	0.278	0.344
	5.5	-.015	-.082	-.139	-.201	-.019	.034	.096	.146
	6.5	-.042	-.108	-.160	-.220	-.042	.007	.062	.110
	11.0	-.062	-.116	-.158	-.200	-.066	-.029	.020	.064
	14.5	-.090	-.140	-.175	-.217	-.095	-.059	-.013	.030
	21.0	-.119	-.162	-.195	-.225	-.118	-.087	-.044	-.009
	24.5	-.140	-.184	-.217	-.254	-.142	-.110	-.070	-.030
	31.0	-.160	-.200	-.233	-.268	-.179	-.151	-.110	-.070
	34.5	-.197	-.237	-.259	-.296	-.211	-.184	-.139	-.102
	41.0	-.240	-.289	-.310	-.333	-.243	-.215	-.169	-.130
	44.5	-.270	-.317	-.346	-.371	-.257	-.228	-.179	-.141
	51.0	-.275	-.324	-.359	-.390	-.270	-.250	-.208	-.176
	59.5	-.271	-.334	-.371	-.411	-.287	-.267	-.195	-.166
	71.0	-.212	-.270	-.310	-.369	-.223	-.180	-.141	-.124
	79.5	-.079	-.099	-.114	-.166	-.068	-.085	-.074	-.066
	91.0	.007	-.002	-.001	-.010	.007	-.002	.008	.007
0.382 b/2	0	0.442	0.429	0.386	0.316	- -	- -	- -	- -
	1.5	-.012	-.151	-.303	-.479	-0.036	0.054	0.146	0.221
	5.5	-.102	-.189	-.268	-.361	-.110	-.043	.030	.089
	6.5	-.128	-.204	-.273	-.357	-.128	-.065	.005	.063
	11.0	-.151	-.219	-.273	-.330	-.152	-.101	-.040	.011
	14.5	-.170	-.239	-.288	-.343	-.176	-.129	-.070	-.020
	21.0	-.197	-.248	-.293	-.340	-.202	-.161	-.109	-.060
	24.5	-.227	-.282	-.317	-.357	-.223	-.180	-.130	-.080
	31.0	-.250	-.309	-.345	-.378	-.250	-.215	-.163	-.120
	34.5	-.260	-.320	-.357	-.390	-.274	-.244	-.190	-.141
	41.0	-.301	-.367	-.411	-.450	-.295	-.267	-.193	-.151
	44.5	-.315	-.380	-.426	-.472	-.312	-.267	-.192	-.168
	51.0	-.290	-.369	-.420	-.469	-.306	-.268	-.217	-.182
	59.5	-.248	-.317	-.375	-.488	-.252	-.207	-.172	-.149
	71.0	-.110	-.106	-.113	-.181	-.108	-.116	-.099	-.087
	79.5	-.036	-.049	-.039	-.055	-.032	-.036	-.021	-.018
	91.0	.048	.039	.040	.042	.049	.047	.060	.059
0.555 b/2	0	0.429	0.423	0.384	0.315	- -	- -	- -	- -
	1.5	-.057	-.221	-.413	-.635	-0.086	0.030	0.140	0.225
	5.5	-.154	-.256	-.358	-.463	-.143	-.068	.017	.085
	6.5	-.184	-.281	-.378	-.475	-.167	-.089	-.009	.062
	11.0	-.192	-.274	-.350	-.431	-.200	-.140	-.065	-.001
	14.5	-.215	-.291	-.359	-.433	-.215	-.160	-.089	-.030
	21.0	-.241	-.320	-.380	-.451	-.249	-.193	-.125	-.071
	24.5	-.255	-.330	-.387	-.425	-.264	-.210	-.144	-.091
	31.0	-.270	-.350	-.409	-.441	-.282	-.227	-.170	-.121
	34.5	-.264	-.354	-.418	-.465	-.287	-.238	-.178	-.137
	41.0	-.280	-.373	-.455	-.525	-.278	-.240	-.181	-.148
	44.5	-.275	-.345	-.440	-.543	-.269	-.231	-.174	-.147
	51.0	-.252	-.312	-.401	-.539	-.243	-.212	-.173	-.150
	59.5	-.201	-.191	-.189	-.227	-.198	-.166	-.149	-.131
	71.0	-.088	-.109	-.091	-.093	-.080	-.088	-.070	-.063
	79.5	-.021	-.031	-.025	-.011	-.019	-.020	-.009	-.010
	91.0	.070	.061	.063	.073	.075	.068	.073	.063

NACA

TABLE XIII.- CONTINUED.

(a) α_u, 0°, 1°, 2°, 3° - Concluded.

Semi-span sta.	Percent chord	UPPER SURFACE Angle of attack 0°	1°	2°	3°	LOWER SURFACE Angle of attack 0°	1°	2°	3°
0.707 b/2	0	0.418	0.394	0.322	0.215	- -	- -	- -	- -
	1.5	-.079	-.288	-.530	-.838	-0.085	0.062	0.187	0.272
	5.5	-.191	-.327	-.459	-.595	-.181	-.080	.020	.093
	6.5	-.207	-.342	-.477	-.622	-.190	-.097	0	.070
	11.0	-.199	-.304	-.404	-.487	-.223	-.149	-.063	-.002
	14.5	-.221	-.330	-.419	-.479	-.232	-.160	-.081	-.024
	21.0	-.235	-.341	-.428	-.485	-.240	-.180	-.112	-.060
	24.5	-.240	-.336	-.431	-.494	-.247	-.190	-.129	-.080
	31.0	-.249	-.323	-.433	-.510	-.250	-.201	-.143	-.101
	34.5	-.250	-.312	-.432	-.527	-.241	-.200	-.144	-.111
	41.0	-.255	-.301	-.392	-.574	-.231	-.202	-.153	-.130
	44.5	-.251	-.290	-.345	-.552	-.234	-.210	-.168	-.142
	51.0	-.229	-.260	-.220	-.262	-.228	-.206	-.170	-.151
	59.5	-.200	-.220	-.192	-.141	-.200	-.181	-.153	-.145
	71.0	-.063	-.070	-.070	-.049	-.050	-.070	-.060	-.068
	79.5	.017	.005	.002	.016	.022	.006	.010	0
	91.0	.092	.086	.088	.091	.099	.089	.091	.079
0.831 b/2	0	0.408	0.433	0.387	0.302	- -	- -	- -	- -
	1.5	-.079	-.322	-.603	-.921	-0.088	0.080	0.207	0.285
	5.5	-.191	-.349	-.512	-.720	-.189	-.074	.022	.092
	6.5	-.189	-.342	-.514	-.705	-.187	-.077	.018	.087
	11.0	-.198	-.308	-.454	-.499	-.208	-.120	-.042	.015
	14.5	-.213	-.312	-.458	-.524	- -	- -	- -	- -
	21.0	-.228	-.302	-.436	-.540	-.221	-.160	-.101	-.057
	24.5	-.235	-.302	-.420	-.551	-.229	-.170	-.116	-.069
	31.0	-.240	-.290	-.365	-.542	-.248	-.196	-.145	-.110
	34.5	-.258	-.301	-.317	-.505	-.254	-.217	-.169	-.143
	41.0	-.284	-.321	-.282	-.303	-.274	-.249	-.200	-.173
	44.5	-.264	-.302	-.248	-.163	-.264	-.253	-.222	-.210
	51.0	-.223	-.258	-.168	-.128	-.218	-.196	-.172	-.190
	59.5	-.080	-.067	-.117	-.094	-.096	-.108	-.110	-.111
	71.0	-.028	-.036	-.040	-.028	-.019	-.024	-.029	-.032
	79.5	.035	.033	.033	.038	.046	.041	.038	.030
	91.0	.110	.110	.109	.109	.118	.111	.107	.093
0.924 b/2	0	0.437	0.348	0.175	0.007	- -	- -	- -	- -
	1.5	-.013	-.266	-.599	-.890	-0.091	0.081	0.210	0.281
	5.5	-.193	-.350	-.564	-.788	-.178	-.060	.038	.103
	6.5	-.206	-.351	-.560	-.788	-.181	-.065	.031	.097
	11.0	-.211	-.311	-.474	-.630	-.209	-.123	-.049	.008
	14.5	-.250	-.339	-.468	-.553	-.240	-.166	-.098	-.049
	21.0	-.306	-.371	-.441	-.608	-.293	-.242	-.186	-.141
	24.5	-.301	-.349	-.362	-.550	-.324	-.298	-.250	-.219
	31.0	-.248	-.291	-.160	-.147	-.260	-.250	-.232	-.250
	34.5	-.194	-.199	-.157	-.087	-.210	-.195	-.173	-.228
	41.0	-.175	-.159	-.205	-.150	-.162	-.165	-.156	-.168
	44.5	-.168	-.168	-.201	-.169	-.148	-.147	-.141	-.130
	51.0	-.121	-.128	-.143	-.140	-.131	-.135	-.130	-.112
	59.5	-.056	-.069	-.075	-.079	-.057	-.060	-.068	-.070
	71.0	.008	.004	.001	-.003	.019	.010	.003	-.009
	79.5	.064	.064	.060	.045	.071	.061	.050	.038
	91.0	.122	.120	.114	.098	.132	.121	.112	.098

NACA

TABLE XIII.- CONTINUED.

(b) α_u, 4°, 6°, 8°, 10°.

Semi-span sta.	Percent chord	UPPER SURFACE Angle of attack 4°	6°	8°	10°	LOWER SURFACE Angle of attack 4°	6°	8°	10°
0.086 b/2	0	0.528	0.452	0.348		- -	- -	- -	
	1.5	-.227	-.556	-.614		0.340	0.431	0.511	
	5.5	-.137	-.225	-.328		.208	.288	.360	
	6.5	-.158	-.240	-.335		.170	.247	.319	
	11.0	-.150	-.220	-.294		.128	.198	.264	
	14.5	-.174	-.233	-.315		.100	.167	.229	
	21.0	-.179	-.242	-.303		.070	.130	.185	
	24.5	-.193	-.251	-.318		.044	.102	.154	
	31.0	-.196	-.255	-.305		.010	.067	.118	
	34.5	-.258	-.307	-.367		-.020	.039	.087	
	41.0	-.286	-.351	-.401		-.051	.006	.057	
	44.5	-.318	-.379	-.442		- -	- -	- -	
	51.0	-.344	-.403	-.465		-.110	-.056	-.008	
	59.5	-.372	-.430	-.484		-.137	-.085	-.040	
	71.0	-.404	-.474	-.534		-.124	-.087	-.050	
	79.5	-.312	-.415	-.499		-.079	-.058	-.040	
	91.0	-.132	-.205	-.290		-.035	-.045	-.051	
0.195 b/2	0	0.355	0.210	0.057		- -	- -	- -	
	1.5	-.422	-.713	-1.000		0.400	0.479	0.530	
	5.5	-.273	-.370	-.600		.191	.280	.358	
	6.5	-.284	-.402	-.520		.151	.238	.320	
	11.0	-.253	-.341	-.458		.100	.176	.248	
	14.5	-.284	-.335	-.419		.063	.135	.201	
	21.0	-.263	-.330	-.410		.022	.090	.151	
	24.5	-.274	-.350	-.411		-.001	.066	.128	
	31.0	-.291	-.363	-.434		-.041	.021	.078	
	34.5	-.320	-.395	-.457		-.072	-.012	.043	
	41.0	-.370	-.440	-.503		-.100	-.043	.010	
	44.5	-.403	-.472	-.540		-.119	-.060	-.010	
	51.0	-.421	-.480	-.543		-.150	-.096	-.046	
	59.5	-.450	-.507	-.560		-.141	-.101	-.060	
	71.0	-.427	-.516	-.588		-.113	-.089	-.064	
	79.5	-.222	-.350	-.487		-.076	-.068	-.062	
	91.0	-.052	-.147	-.235		-.010	-.041	-.073	
0.382 b/2	0	0.223	0.039	-0.140		- -	- -	- -	
	1.5	-.682	-1.020	-1.259		0.282	0.376	0.440	
	5.5	-.452	-.720	-1.129		.140	.233	.309	
	6.5	-.440	-.588	-1.143		.113	.203	.280	
	11.0	-.370	-.509	-.650		.058	.140	.210	
	14.5	-.398	-.496	-.559		.020	.100	.170	
	21.0	-.380	-.490	-.570		-.020	.057	.120	
	24.5	-.404	-.492	-.569		-.040	.030	.090	
	31.0	-.424	-.506	-.580		-.089	-.023	.035	
	34.5	-.431	-.511	-.584		-.112	-.048	.010	
	41.0	-.494	-.560	-.640		-.125	-.070	-.020	
	44.5	-.520	-.590	-.667		-.141	-.090	-.041	
	51.0	-.512	-.598	-.659		-.161	-.116	-.076	
	59.5	-.584	-.637	-.704		-.140	-.113	-.091	
	71.0	-.261	-.490	-.663		-.092	-.092	-.096	
	79.5	-.086	-.201	-.330		-.031	-.050	-.077	
	91.0	.033	-.044	-.120		.031	-.006	-.058	
0.555 b/2	0	0.216	0.031	-0.147		- -	- -	- -	
	1.5	-.896	-1.169	-1.325		0.289	0.373	0.430	
	5.5	-.579	-1.069	-1.252		.139	.230	.303	
	6.5	-.518	-1.033	-1.215		.118	.206	.277	
	11.0	-.470	-.715	-1.213		.049	.130	.203	
	14.5	-.488	-.545	-1.210		.016	.093	.161	
	21.0	-.494	-.580	-.770		-.030	.035	.102	
	24.5	-.494	-.588	-.711		-.051	.013	.070	
	31.0	-.504	-.592	-.657		-.090	-.037	.027	
	34.5	-.519	-.598	-.665		-.110	-.055	-.009	
	41.0	-.577	-.653	-.715		-.125	-.080	-.041	
	44.5	-.609	-.647	-.752		-.130	-.094	-.060	
	51.0	-.595	-.646	-.784		-.138	-.114	-.090	
	59.5	-.382	-.716	-.784		-.130	-.124	-.118	
	71.0	-.105	-.230	-.376		-.067	-.082	-.100	
	79.5	-.011	-.097	-.182		-.020	-.047	-.082	
	91.0	.075	.005	-.099		.048	.002	-.061	

NACA

TABLE XIII.- CONCLUDED.

(b) α_u, 4°, 6°, 8°, 10° - Concluded.

Semi-span sta.	Percent chord	UPPER SURFACE Angle of attack 4°	6°	8°	10°	LOWER SURFACE Angle of attack 4°	6°	8°	10°
0.707 b/2	0	0.111	-0.088	-0.277		- -	- -	- -	
	1.5	-1.024	-1.206	-1.352		0.325	0.395	0.430	
	5.5	-.857	-1.120	-1.314		.147	.233	.295	
	6.5	-.838	-1.132	-1.311		.123	.207	.270	
	11.0	-.532	-1.077	-1.258		.046	.123	.183	
	14.5	-.553	-1.043	-1.245		.020	.093	.147	
	21.0	-.566	-.632	-1.208		-.027	.033	.086	
	24.5	-.568	-.613	-1.163		-.046	.008	.057	
	31.0	-.570	-.640	-.965		-.078	-.030	.007	
	34.5	-.589	-.657	-.891		-.090	-.047	-.015	
	41.0	-.642	-.705	-.836		-.113	-.080	-.065	
	44.5	-.690	-.757	-.698		-.127	-.100	-.081	
	51.0	-.488	-.780	-.715		-.142	-.124	-.117	
	59.5	-.141	-.326	-.639		-.147	-.144	-.152	
	71.0	-.033	-.133	-.423		-.084	-.111	-.148	
	79.5	.031	-.035	-.382		-.017	-.067	-.153	
	91.0	.093	.058	-.248		.063	.014	-.130	
0.831 b/2	0	0.217	0.043	-0.133		- -	- -	- -	
	1.5	-1.050	-1.201	-1.148		0.330	0.385	0.406	
	5.5	-.930	-1.169	-1.140		.141	.217	.265	
	6.5	-.937	-1.172	-1.138		.132	.208	.254	
	11.0	-.873	-1.105	-1.113		.055	.121	.166	
	14.5	-.706	-1.078	-1.054		- -	- -	- -	
	21.0	-.604	-1.010	-.985		-.028	.028	.060	
	24.5	-.616	-1.023	-.955		-.043	.008	.037	
	31.0	-.622	-.833	-.908		-.085	-.048	-.024	
	34.5	-.635	-.719	-.815		-.121	-.085	-.063	
	41.0	-.594	-.708	-.760		-.159	-.128	-.115	
	44.5	-.265	-.710	-.740		-.198	-.172	-.163	
	51.0	-.098	-.253	-.708		-.200	-.192	-.196	
	59.5	-.040	-.111	-.640		-.144	-.224	-.270	
	71.0	-.001	-.020	-.551		-.040	-.112	-.245	
	79.5	.043	.039	-.478		.020	-.020	-.200	
	91.0	.102	.086	-.365		.081	.041	-.166	
0.924 b/2	0	-0.127	-0.361	-0.588		- -	- -	- -	
	1.5	-1.015	-1.162	-.902		0.326	0.365	0.380	
	5.5	-1.001	-1.176	-.903		.148	.211	.251	
	6.5	-.991	-1.169	-.900		.139	.201	.241	
	11.0	-.935	-1.101	-.873		.042	.101	.140	
	14.5	-.920	-1.098	-.850		-.016	.040	.077	
	21.0	-.613	-1.040	-.819		-.113	-.062	-.029	
	24.5	-.640	-1.006	-.761		-.192	-.148	-.113	
	31.0	-.441	-.883	-.732		-.240	-.206	-.177	
	34.5	-.131	-.743	-.712		-.269	-.253	-.236	
	41.0	-.065	-.559	-.697		-.253	-.278	-.273	
	44.5	-.080	-.540	-.673		-.207	-.310	-.321	
	51.0	-.089	-.368	-.652		-.122	-.289	-.340	
	59.5	-.071	-.170	-.583		-.070	-.128	-.311	
	71.0	-.013	-.008	-.523		-.013	-.044	-.229	
	79.5	.017	-.020	-.459		.027	.002	-.192	
	91.0	.070	.018	-.390		.085	.058	-.170	

NACA

TABLE XIV.- PRESSURE COEFFICIENTS AT SEVEN SEMISPAN STATIONS OF THE WING. M_0, 0.94; R, 4,000,000.

(a) α_u, 0°, 1°, 2°, 3°.

Semi-span sta.	Percent chord	UPPER SURFACE Angle of attack 0°	1°	2°	3°	LOWER SURFACE Angle of attack 0°	1°	2°	3°
0.086 b/2	0	0.584	0.589	0.578	0.562	- -	- -	- -	- -
	1.5	.146	.069	-.021	-.111	0.111	0.179	0.213	0.296
	5.5	.060	.017	-.032	-.076	.050	.095	.136	.177
	6.5	.031	-.010	-.057	-.099	.021	.064	.101	.142
	11.0	.005	-.030	-.069	-.106	-.002	.036	.068	.105
	14.5	-.027	-.059	-.097	-.131	-.025	.011	.042	.076
	21.0	-.046	-.075	-.108	-.136	-.044	-.011	.018	.050
	24.5	-.066	-.095	-.128	-.154	-.070	-.037	-.009	.023
	31.0	-.081	-.106	-.135	-.159	-.099	-.066	-.039	-.009
	34.5	-.125	-.151	-.186	-.213	-.132	-.099	-.090	-.039
	41.0	-.163	-.190	-.224	-.251	-.166	-.134	-.105	-.073
	44.5	-.197	-.222	-.253	-.285	- -	- -	- -	- -
	51.0	-.229	-.255	-.283	-.311	-.233	-.196	-.164	-.133
	59.5	-.251	-.280	-.317	-.340	-.236	-.202	-.182	-.155
	71.0	-.253	-.282	-.325	-.367	-.262	-.218	-.185	-.152
	79.5	-.149	-.175	-.238	-.287	-.164	-.121	-.157	-.094
	91.0	-.049	-.057	-.092	-.121	-.051	-.034	-.038	-.038
0.195 b/2	0	0.505	0.498	0.469	0.426	- -	- -	- -	- -
	1.5	.076	-.022	-.140	-.262	0.111	0.205	0.282	0.349
	5.5	-.008	-.066	-.130	-.192	-.011	.049	.099	.152
	6.5	-.035	-.089	-.150	-.208	-.036	.018	.067	.115
	11.0	-.057	-.100	-.147	-.189	-.059	-.014	.026	.069
	14.5	-.082	-.122	-.166	-.199	-.088	-.046	-.008	.033
	21.0	-.111	-.146	-.183	-.208	-.111	-.073	-.040	-.003
	24.5	-.134	-.168	-.207	-.242	-.137	-.099	-.066	-.026
	31.0	-.154	-.184	-.223	-.256	-.175	-.138	-.105	-.065
	34.5	-.190	-.219	-.249	-.283	-.208	-.171	-.134	-.099
	41.0	-.238	-.270	-.299	-.327	-.244	-.203	-.165	-.128
	44.5	-.270	-.301	-.335	-.360	-.259	-.217	-.175	-.141
	51.0	-.280	-.315	-.355	-.381	-.277	-.234	-.204	-.177
	59.5	-.287	-.327	-.374	-.406	-.293	-.259	-.219	-.172
	71.0	-.227	-.268	-.333	-.383	-.240	-.169	-.147	-.132
	79.5	-.084	-.097	-.167	-.239	-.083	-.076	-.083	-.077
	91.0	.005	.007	-.010	-.033	.007	.008	.001	-.004
0.382 b/2	0	0.449	0.439	0.394	0.326	- -	- -	- -	- -
	1.5	-.005	-.134	-.290	-.456	-0.034	0.066	0.149	0.224
	5.5	-.095	-.170	-.256	-.338	-.104	-.031	.032	.093
	6.5	-.119	-.188	-.263	-.346	-.121	-.052	.008	.067
	11.0	-.145	-.200	-.266	-.324	-.147	-.089	-.037	.014
	14.5	-.165	-.223	-.274	-.332	-.173	-.117	-.068	-.018
	21.0	-.192	-.231	-.285	-.329	-.201	-.150	-.105	-.059
	24.5	-.224	-.266	-.304	-.347	-.224	-.169	-.126	-.079
	31.0	-.247	-.293	-.335	-.367	-.253	-.201	-.162	-.121
	34.5	-.266	-.305	-.350	-.380	-.278	-.230	-.193	-.147
	41.0	-.308	-.359	-.407	-.442	-.289	-.255	-.207	-.157
	44.5	-.328	-.370	-.429	-.468	-.313	-.266	-.200	-.171
	51.0	-.319	-.369	-.427	-.464	-.340	-.272	-.216	-.193
	59.5	-.266	-.316	-.391	-.501	-.102	-.193	-.165	-.164
	71.0	-.104	-.100	-.265	-.312	-.099	-.106	-.102	-.096
	79.5	-.033	-.031	-.025	-.074	-.023	-.027	-.025	-.024
	91.0	.050	.051	.050	.043	.053	.058	.059	.054
0.555 b/2	0	0.429	0.432	0.391	0.316	- -	- -	- -	- -
	1.5	-.052	-.208	-.393	-.612	-0.086	0.039	0.139	0.221
	5.5	-.153	-.244	-.347	-.448	-.145	-.058	.013	.082
	6.5	-.182	-.268	-.365	-.459	-.166	-.080	-.009	.059
	11.0	-.192	-.263	-.343	-.420	-.203	-.128	-.067	-.006
	14.5	-.216	-.279	-.350	-.421	-.218	-.151	-.092	-.033
	21.0	-.249	-.310	-.375	-.429	-.249	-.189	-.130	-.076
	24.5	-.260	-.321	-.380	-.422	-.267	-.205	-.148	-.097
	31.0	-.286	-.341	-.404	-.434	-.295	-.226	-.173	-.127
	34.5	-.292	-.347	-.422	-.453	-.316	-.253	-.185	-.143
	41.0	-.310	-.384	-.464	-.522	-.315	-.232	-.192	-.161
	44.5	-.292	-.361	-.377	-.547	-.297	-.224	-.186	-.157
	51.0	-.265	-.226	-.441	-.541	-.264	-.202	-.177	-.157
	59.5	-.184	-.173	-.358	-.446	-.176	-.156	-.150	-.168
	71.0	-.090	-.091	-.049	-.101	-.083	-.078	-.072	-.068
	79.5	-.022	-.023	-.006	-.006	-.018	-.011	-.009	-.013
	91.0	.070	.072	.073	.062	.073	.076	.075	.063

NACA

TABLE XIV.- CONTINUED.

(a) α_u, 0°, 1°, 2°, 3° - Concluded.

Semi-span sta.	Percent chord	UPPER SURFACE Angle of attack 0°	1°	2°	3°	LOWER SURFACE Angle of attack 0°	1°	2°	3°
0.707 b/2	0	0.415	0.401	0.330	0.230	- -	- -	- -	- -
	1.5	-.082	-.273	-.506	-.803	-0.088	0.066	0.178	0.264
	5.5	-.197	-.315	-.449	-.576	-.187	-.074	.013	.087
	6.5	-.214	-.334	-.467	-.601	-.196	-.088	-.007	.064
	11.0	-.211	-.298	-.401	-.498	-.231	-.138	-.069	-.008
	14.5	-.241	-.321	-.414	-.481	-.249	-.152	-.088	-.031
	21.0	-.254	-.337	-.427	-.479	-.267	-.173	-.120	-.068
	24.5	-.252	-.341	-.436	-.486	-.269	-.181	-.133	-.085
	31.0	-.255	-.339	-.447	-.504	-.267	-.191	-.148	-.106
	34.5	-.254	-.322	-.461	-.519	-.249	-.189	-.150	-.117
	41.0	-.256	-.299	-.462	-.579	-.231	-.191	-.154	-.134
	44.5	-.251	-.280	-.433	-.618	-.227	-.199	-.171	-.175
	51.0	-.226	-.232	-.355	-.509	-.222	-.197	-.171	-.152
	59.5	-.200	-.206	-.119	-.147	-.205	-.174	-.160	-.152
	71.0	-.072	-.061	-.044	-.029	-.062	-.059	-.065	-.080
	79.5	.021	.018	.014	.034	.026	.018	.013	0
	91.0	.097	.098	.093	.103	.103	.100	.096	-.083
0.631 b/2	0	0.402	0.437	0.391	0.315	- -	- -	- -	- -
	1.5	-.085	-.314	-.586	-.885	-0.098	0.083	0.199	0.275
	5.5	-.196	-.346	-.505	-.688	-.199	-.070	.017	.084
	6.5	-.199	-.345	-.508	-.686	-.197	-.072	.013	.079
	11.0	-.200	-.314	-.451	-.525	-.217	-.115	-.046	.008
	14.5	-.212	-.319	-.459	-.509	- -	- -	- -	- -
	21.0	-.224	-.307	-.457	-.530	-.221	-.155	-.098	-.062
	24.5	-.231	-.297	-.459	-.543	-.223	-.162	-.114	-.072
	31.0	-.231	-.279	-.439	-.553	-.238	-.187	-.144	-.110
	34.5	-.248	-.282	-.405	-.560	-.247	-.205	-.166	-.143
	41.0	-.284	-.304	-.339	-.568	-.275	-.239	-.202	-.178
	44.5	-.286	-.302	-.255	-.354	-.287	-.260	-.233	-.218
	51.0	-.238	-.254	-.113	-.116	-.234	-.199	-.206	-.219
	59.5	-.053	-.055	-.089	-.047	-.068	-.089	-.095	-.120
	71.0	-.019	-.026	-.027	-.003	-.011	-.017	-.019	-.025
	79.5	.042	.042	.040	.049	.052	.049	.044	.035
	91.0	.118	.119	.114	.139	.124	.120	.114	.101
0.924 b/2	0	0.439	0.352	0.187	0.030	- -	- -	- -	- -
	1.5	-.006	-.265	-.585	-.857	-0.097	0.091	0.210	0.275
	5.5	-.187	-.351	-.571	-.769	-.181	-.052	.037	.100
	6.5	-.199	-.351	-.573	-.771	-.182	-.056	.031	.094
	11.0	-.205	-.308	-.490	-.659	-.206	-.114	-.045	.006
	14.5	-.241	-.329	-.493	-.616	-.236	-.155	-.092	-.047
	21.0	-.297	-.355	-.494	-.601	-.292	-.229	-.178	-.140
	24.5	-.327	-.349	-.430	-.631	-.340	-.294	-.253	-.220
	31.0	-.278	-.292	-.245	-.463	-.294	-.263	-.267	-.261
	34.5	-.223	-.206	-.127	-.203	-.236	-.200	-.215	-.282
	41.0	-.184	-.150	-.138	-.081	-.181	-.162	-.169	-.238
	44.5	-.149	-.151	-.159	-.091	-.122	-.124	-.122	-.173
	51.0	-.099	-.114	-.124	-.091	-.108	-.116	-.098	-.091
	59.5	-.053	-.058	-.064	-.057	-.052	-.053	-.057	-.057
	71.0	.012	.019	.009	.007	.022	.018	.010	.003
	79.5	.069	.073	.064	.052	.076	.069	.057	.044
	91.0	.129	.130	.118	.103	.139	.132	.119	.104

NACA

TABLE XIV.- CONTINUED.

(b) α_u, 4°, 6°, 8°, 10°.

Semi-span sta.	Percent chord	UPPER SURFACE Angle of attack 4°	6°	8°	10°	LOWER SURFACE Angle of attack 4°	6°	8°	10°
0.086 b/2	0	0.536	0.462			- -	- -		
	1.5	-.214	-.437			0.347	0.436		
	5.5	-.124	-.212			.217	.290		
	6.5	-.143	-.225			.180	.252		
	11.0	-.141	-.201			.137	.201		
	14.5	-.164	-.245			.108	.171		
	21.0	-.171	-.246			.078	.133		
	24.5	-.184	-.247			.051	.105		
	31.0	-.186	-.248			.019	.070		
	34.5	-.242	-.299			-.011	.041		
	41.0	-.269	-.341			-.045	.006		
	44.5	-.306	-.373			- -	- -		
	51.0	-.335	-.393			-.105	-.058		
	59.5	-.366	-.425			- 132	-.090		
	71.0	-.401	-.468			-.129	-.095		
	79.5	-.341	-.425			-.082	-.069		
	91.0	-.149	-.230			-.042	-.059		
0.195 b/2	0	0.364	0.222			- -	- -		
	1.5	-.406	-.698			0.404	0.481		
	5.5	-.262	-.357			.199	.283		
	6.5	-.271	-.388			.159	.240		
	11.0	-.241	-.338			.107	.178		
	14.5	-.251	-.326			.069	.137		
	21.0	-.250	-.323			.031	.092		
	24.5	-.262	-.343			.006	.068		
	31.0	-.279	-.358			-.035	.022		
	34.5	-.306	-.382			-.066	-.013		
	41.0	-.355	-.426			-.096	-.046		
	44.5	-.393	-.461			-.113	-.063		
	51.0	-.411	-.472			-.151	-.102		
	59.5	-.435	-.496			-.146	-.108		
	71.0	-.432	-.510			-.119	-.099		
	79.5	-.265	-.401			-.076	-.083		
	91.0	-.083	-.183			-.023	-.070		
0.382 b/2	0	0.236	0.055			- -	- -		
	1.5	-.667	-1.032			0.285	0.376		
	5.5	-.438	-.711			.145	.233		
	6.5	-.429	-.571			.118	.204		
	11.0	-.360	-.496			.061	.138		
	14.5	-.385	-.488			.025	.099		
	21.0	-.369	-.482			-.018	.078		
	24.5	-.390	-.482			-.036	.023		
	31.0	-.412	-.493			-.087	-.028		
	34.5	-.419	-.503			-.112	-.053		
	41.0	-.480	-.551			-.126	-.076		
	44.5	-.510	-.579			-.144	-.098		
	51.0	-.507	-.589			-.166	-.128		
	59.5	-.558	-.624			-.150	-.132		
	71.0	-.361	-.568			-.101	-.116		
	79.5	-.116	-.273			-.041	-.078		
	91.0	.019	-.090			.023	-.038		
0.555 b/2	0	0.227	0.052			- -	- -		
	1.5	-.882	-1.161			0.285	0.369		
	5.5	-.565	-1.055			.138	.224		
	6.5	-.521	-1.025			.115	.201		
	11.0	-.458	-.720			.046	.126		
	14.5	-.475	-.531			.015	.090		
	21.0	-.483	-.566			-.034	.035		
	24.5	-.486	-.573			-.055	.007		
	31.0	-.493	-.579			-.098	-.043		
	34.5	-.510	-.588			-.114	-.066		
	41.0	-.568	-.641			-.133	-.094		
	44.5	-.603	-.684			-.136	-.108		
	51.0	-.593	-.684			-.146	-.131		
	59.5	-.591	-.722			-.137	-.142		
	71.0	-.143	-.347			-.078	-.105		
	79.5	-.031	-.166			-.029	-.074		
	91.0	.067	-.047			.042	-.029		

NACA

TABLE XIV.- CONCLUDED.

(b) α_u, 4°, 6°, 8°, 10° - Concluded.

Semi-span sta.	Percent chord	UPPER SURFACE Angle of attack 4°	6°	8°	10°	LOWER SURFACE Angle of attack 4°	6°	8°	10°
0.707 b/2	0	0.124	-0.062			- -	- -		
	1.5	-1.006	-1.192			0.321	0.388		
	5.5	-.833	-1.110			.144	.225		
	6.5	-.814	-1.120			.119	.198		
	11.0	-.522	-1.077			.042	.114		
	14.5	-.549	-1.037			.015	.082		
	21.0	-.560	-.604			-.032	.022		
	24.5	-.559	-.597			-.051	-.004		
	31.0	-.561	-.629			-.083	-.045		
	34.5	-.578	-.650			-.094	-.063		
	41.0	-.632	-.693			-.117	-.097		
	44.5	-.683	-.740			-.132	-.117		
	51.0	-.668	-.775			-.146	-.142		
	59.5	-.200	-.603			-.204	-.167		
	71.0	-.054	-.226			-.097	-.142		
	79.5	.028	-.121			-.028	-.109		
	91.0	.099	.013			.064	-.019		
0.831 b/2	0	0.232	0.069			- -	- -		
	1.5	-1.030	-1.199			0.322	0.374		
	5.5	-.917	-1.177			.134	.202		
	6.5	-.923	-1.181			.127	.192		
	11.0	-.762	-1.119			.048	.105		
	14.5	-.697	-1.099			.090	.083		
	21.0	-.597	-1.041			-.032	.013		
	24.5	-.602	-1.037			-.046	-.051		
	31.0	-.611	-.843			-.090	-.065		
	34.5	-.631	-.705			-.126	-.103		
	41.0	-.689	-.711			-.164	-.147		
	44.5	-.592	-.739			-.206	-.196		
	51.0	-.169	-.659			-.219	-.224		
	59.5	-.037	-.184			-.191	-.279		
	71.0	.017	-.081			-.043	-.180		
	79.5	.057	-.016			.024	-.064		
	91.0	.108	.042			.084	.022		
0.924 b/2	0	-0.102	-0.329			- -	- -		
	1.5	-.998	-1.169			0.316	0.377		
	5.5	-1.003	-1.199			.142	.199		
	6.5	-.999	-1.201			.135	.189		
	11.0	-.937	-1.129			.040	.088		
	14.5	-.923	-1.126			-.017	.028		
	21.0	-.593	-1.115			-.113	-.074		
	24.5	-.637	-1.103			-.195	-.159		
	31.0	-.623	-1.074			-.246	-.224		
	34.5	-.475	-.952			-.286	-.279		
	41.0	-.100	-.587			-.293	-.307		
	44.5	-.052	-.567			-.296	-.351		
	51.0	-.046	-.382			-.189	-.363		
	59.5	-.039	-.230			-.054	-.249		
	71.0	.006	-.052			-.007	-.072		
	79.5	.028	-.025			.031	-.009		
	91.0	.090	-.007			.086	.044		

NACA

TABLE XV.- PRESSURE COEFFICIENTS AT SEVEN SEMISPAN STATIONS OF THE WING. M_0, 0.95; R, 4,000,000.

(a) α_u, 0°, 1°, 2°, 3°.

Semi-span sta.	Percent chord	UPPER SURFACE				LOWER SURFACE			
		Angle of attack				Angle of attack			
		0°	1°	2°	3°	0°	1°	2°	3°
0.086 b/2	0	0.594	0.596	0.590	0.574	- -	- -	- -	- -
	1.5	.154	.080	0	-.089	0.122	0.187	0.257	0.306
	5.5	.068	.025	-.015	-.055	.060	.104	.149	.190
	6.5	.039	0	-.040	-.085	.031	.070	.115	.153
	11.0	.014	-.017	-.054	-.096	.007	.043	.082	.115
	14.5	-.016	-.049	-.080	-.118	-.016	.017	.055	.087
	21.0	-.036	-.063	-.090	-.120	-.031	-.003	.030	.057
	24.5	-.058	-.085	-.110	-.137	-.061	-.030	.003	.030
	31.0	-.073	-.098	-.119	-.144	-.090	-.060	-.027	-.002
	34.5	-.120	-.145	-.170	-.200	-.125	-.095	-.060	-.034
	41.0	-.158	-.190	-.214	-.237	-.160	-.132	-.098	-.070
	44.5	-.189	-.218	-.245	-.272	- -	- -	- -	- -
	51.0	-.224	-.246	-.270	-.296	-.234	-.200	-.163	-.134
	59.5	-.250	-.277	-.301	-.323	-.260	-.207	-.176	-.153
	71.0	-.274	-.297	-.329	-.361	-.270	-.253	-.204	-.174
	79.5	-.182	-.215	-.260	-.303	-.190	-.160	-.118	-.107
	91.0	-.077	-.087	-.112	-.147	-.077	-.057	-.049	-.057
0.195 b/2	0	0.512	0.506	0.481	0.438	- -	- -	- -	- -
	1.5	.086	-.011	-.123	-.247	0.120	0.211	0.290	0.354
	5.5	0	-.054	-.115	-.180	-.002	.055	.110	.157
	6.5	-.028	-.080	-.138	-.196	-.029	.037	.078	.120
	11.0	-.049	-.090	-.132	-.178	-.050	-.009	.036	.074
	14.5	-.074	-.113	-.153	-.194	-.080	-.040	.001	.037
	21.0	-.103	-.139	-.170	-.201	-.103	-.070	-.032	0
	24.5	-.129	-.162	-.199	-.230	-.130	-.095	-.060	-.023
	31.0	-.149	-.183	-.213	-.249	-.170	-.135	-.100	-.064
	34.5	-.182	-.210	-.244	-.279	-.206	-.170	-.133	-.100
	41.0	-.235	-.261	-.289	-.320	-.243	-.207	-.168	-.132
	44.5	-.267	-.299	-.323	-.352	-.261	-.220	-.179	-.148
	51.0	-.279	-.313	-.348	-.375	-.292	-.240	-.200	-.179
	59.5	-.309	-.340	-.370	-.397	-.313	-.272	-.241	-.204
	71.0	-.262	-.301	-.348	-.392	-.261	-.222	-.161	-.151
	79.5	-.150	-.184	-.252	-.319	-.149	-.110	-.098	-.103
	91.0	-.003	-.010	-.048	-.102	-.007	0	-.012	-.032
0.382 b/2	0	0.452	0.444	0.404	0.339	- -	- -	- -	- -
	1.5	.001	-.122	-.271	-.430	-0.027	0.068	0.154	0.221
	5.5	-.090	-.162	-.243	-.332	-.098	-.029	.036	.090
	6.5	-.112	-.180	-.250	-.336	-.116	-.050	.011	.065
	11.0	-.140	-.196	-.253	-.307	-.141	-.089	-.035	.012
	14.5	-.161	-.217	-.268	-.319	-.169	-.118	-.068	-.021
	21.0	-.188	-.228	-.279	-.320	-.200	-.152	-.104	-.062
	24.5	-.220	-.259	-.296	-.340	-.225	-.174	-.128	-.089
	31.0	-.250	-.290	-.321	-.359	-.259	-.209	-.159	-.127
	34.5	-.265	-.302	-.340	-.369	-.285	-.235	-.192	-.158
	41.0	-.319	-.362	-.400	-.434	-.309	-.257	-.220	-.184
	44.5	-.338	-.380	-.425	-.458	-.328	-.278	-.240	-.192
	51.0	-.351	-.390	-.428	-.455	-.361	-.327	-.260	-.209
	59.5	-.320	-.371	-.432	-.508	-.321	-.263	-.200	-.193
	71.0	-.210	-.301	-.395	-.438	-.213	-.106	-.113	-.124
	79.5	-.014	-.011	-.042	-.165	-.009	-.020	-.029	-.042
	91.0	.060	.061	.055	.020	.067	.060	.060	.040
0.924 b/2	0	0.429	0.433	0.400	0.330	- -	- -	- -	- -
	1.5	-.050	-.194	-.369	-.579	-0.088	0.034	0.138	0.219
	5.5	-.151	-.236	-.331	-.429	-.146	-.063	.017	.079
	6.5	-.180	-.260	-.351	-.440	-.170	-.085	-.009	.053
	11.0	-.192	-.259	-.329	-.401	-.207	-.133	-.068	-.012
	14.5	-.218	-.273	-.340	-.403	-.222	-.154	-.095	-.043
	21.0	-.258	-.309	-.364	-.417	-.260	-.196	-.142	-.088
	24.5	-.270	-.320	-.370	-.419	-.281	-.220	-.163	-.111
	31.0	-.298	-.350	-.392	-.427	-.306	-.253	-.193	-.142
	34.5	-.312	-.361	-.414	-.442	-.330	-.280	-.207	-.160
	41.0	-.369	-.413	-.466	-.508	-.352	-.302	-.211	-.189
	44.5	-.373	-.436	-.486	-.543	-.364	-.298	-.211	-.200
	51.0	-.338	-.405	-.482	-.528	-.336	-.257	-.189	-.180
	59.5	-.237	-.341	-.444	-.581	-.250	-.138	-.153	-.152
	71.0	-.056	-.030	-.097	-.213	-.044	-.076	-.072	-.080
	79.5	-.017	-.006	.032	-.032	-.005	-.014	-.010	-.023
	91.0	.073	.081	.093	.081	.079	.078	.080	.060

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TABLE XV.- CONTINUED.

(a) α_u, 0°, 1°, 2°, 3° - Concluded.

Semi-span sta.	Percent chord	UPPER SURFACE Angle of attack 0°	1°	2°	3°	LOWER SURFACE Angle of attack 0°	1°	2°	3°
0.707 b/2	0	0.408	0.396	0.341	0.250	- -	- -	- -	- -
	1.5	-.088	-.262	-.470	-.742	-0.097	0.046	0.163	0.248
	5.5	-.206	-.311	-.430	-.550	-.200	-.097	-.002	.070
	6.5	-.225	-.338	-.450	-.575	-.210	-.112	-.022	.048
	11.0	-.223	-.303	-.389	-.484	-.250	-.168	-.088	-.027
	14.5	-.257	-.330	-.403	-.490	-.264	-.189	-.105	-.051
	21.0	-.289	-.355	-.418	-.466	-.290	-.221	-.140	-.094
	24.5	-.300	-.364	-.429	-.471	-.310	-.232	-.151	-.113
	31.0	-.322	-.387	-.446	-.490	-.337	-.241	-.166	-.130
	34.5	-.322	-.409	-.464	-.512	-.330	-.219	-.161	-.139
	41.0	-.308	-.416	-.510	-.571	-.299	-.195	-.161	-.150
	44.5	-.278	-.384	-.515	-.618	-.268	-.184	-.175	-.165
	51.0	-.223	-.334	-.470	-.601	-.215	-.195	-.184	-.171
	59.5	-.167	-.123	-.270	-.379	-.166	-.188	-.171	-.172
	71.0	-.081	-.049	.010	-.068	-.071	-.080	-.081	-.106
	79.5	.021	.026	.054	.036	.027	.022	.018	-.019
	91.0	.102	.103	.112	.120	.107	.106	.108	.088
0.831 b/2	0	0.386	0.421	0.398	0.342	- -	- -	- -	- -
	1.5	-.109	-.299	-.541	-.819	-0.119	0.044	0.178	0.253
	5.5	-.229	-.352	-.490	-.643	-.229	-.109	-.001	.062
	6.5	-.231	-.359	-.492	-.642	-.227	-.110	-.007	.058
	11.0	-.240	-.340	-.442	-.561	-.259	-.150	-.065	-.012
	14.5	-.260	-.358	-.456	-.549	- -	- -	- -	- -
	21.0	-.270	-.372	-.463	-.512	-.274	-.170	-.118	-.081
	24.5	-.263	-.381	-.477	-.528	-.260	-.170	-.127	-.092
	31.0	-.246	-.369	-.486	-.542	-.254	-.189	-.153	-.123
	34.5	-.241	-.346	-.493	-.556	-.241	-.201	-.169	-.150
	41.0	-.260	-.313	-.467	-.620	-.245	-.238	-.208	-.191
	44.5	-.278	-.296	-.436	-.650	-.276	-.278	-.250	-.235
	51.0	-.260	-.206	-.284	-.392	-.249	-.267	-.254	-.249
	59.5	-.072	-.050	-.005	-.077	-.087	-.080	-.100	-.215
	71.0	-.007	-.014	.019	.025	0	0	-.001	-.021
	79.5	.050	.051	.062	.077	.060	.059	.059	.050
	91.0	.126	.127	.128	.131	.131	.126	.124	.112
0.924 b/2	0	0.422	0.349	-0.210	0.069	- -	- -	- -	- -
	1.5	-.029	-.269	-.535	-.793	-0.121	0.068	0.188	0.256
	5.5	-.218	-.381	-.559	-.727	-.211	-.071	.020	.080
	6.5	-.222	-.390	-.563	-.729	-.208	-.071	.017	.076
	11.0	-.222	-.358	-.489	-.647	-.229	-.123	-.058	-.010
	14.5	-.250	-.380	-.500	-.630	-.242	-.159	-.099	-.056
	21.0	-.291	-.406	-.527	-.577	-.284	-.227	-.180	-.149
	24.5	-.324	-.396	-.549	-.611	-.332	-.299	-.262	-.230
	31.0	-.295	-.337	-.485	-.581	-.307	-.314	-.299	-.279
	34.5	-.246	-.220	-.353	-.553	-.253	-.270	-.302	-.313
	41.0	-.200	-.119	-.135	-.410	-.200	-.226	-.257	-.320
	44.5	-.158	-.119	-.052	-.171	-.141	-.145	-.203	-.304
	51.0	-.078	-.092	-.045	-.043	-.084	-.067	-.083	-.232
	59.5	-.042	-.050	-.031	-.026	-.041	-.046	-.037	-.012
	71.0	.021	.021	.027	.039	.030	.022	.021	.020
	79.5	.078	.078	.074	.070	.084	.073	.064	.056
	91.0	.135	.135	.126	.112	.147	.136	.127	.110

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TABLE XV.- CONTINUED.

(b) α_u, 4°, 6°, 8°, 10°.

Semi-span sta.	Percent chord	UPPER SURFACE Angle of attack 4°	6°	8°	10°	LOWER SURFACE Angle of attack 4°	6°	8°	10°
0.086 b/2	0	0.548	0.477			- -	- -		
	1.5	-.194	-.414			0.357	0.447		
	5.5	-.109	-.194			.225	.301		
	6.5	-.129	-.210			.190	.263		
	11.0	-.125	-.185			.147	.213		
	14.5	-.150	-.211			.117	.181		
	21.0	-.157	-.220			.088	.143		
	24.5	-.170	-.225			.060	.117		
	31.0	-.171	-.225			.026	.080		
	34.5	-.230	-.276			-.005	.050		
	41.0	-.260	-.319			-.042	.016		
	44.5	-.292	-.354			- -	- -		
	51.0	-.322	-.373			-.104	-.050		
	59.5	-.345	-.401			-.130	-.084		
	71.0	-.390	-.450			-.137	-.093		
	79.5	-.345	-.414			-.094	-.070		
	91.0	-.171	-.244			-.059	-.066		
0.195 b/2	0	0.380	0.241			- -	- -		
	1.5	-.385	-.667			0.413	0.491		
	5.5	-.247	-.332			.209	.294		
	6.5	-.255	-.360			.170	.250		
	11.0	-.228	-.322			.119	.189		
	14.5	-.231	-.305			.079	.147		
	21.0	-.235	-.303			.040	.101		
	24.5	-.247	-.320			.011	.076		
	31.0	-.269	-.340			-.030	.030		
	34.5	-.292	-.360			-.061	-.007		
	41.0	-.342	-.408			-.091	-.040		
	44.5	-.377	-.441			-.110	-.060		
	51.0	-.394	-.451			-.148	-.098		
	59.5	-.420	-.479			-.151	-.109		
	71.0	-.430	-.497			-.130	-.102		
	79.5	-.313	-.419			-.091	-.094		
	91.0	-.131	-.208			-.044	-.100		
0.382 b/2	0	0.252	0.079			- -	- -		
	1.5	-.640	-.993			0.290	0.380		
	5.5	-.423	-.692			.150	.239		
	6.5	-.425	-.567			.123	.209		
	11.0	-.334	-.478			.067	.143		
	14.5	-.361	-.462			.030	.103		
	21.0	-.352	-.461			-.014	.059		
	24.5	-.371	-.461			-.032	.030		
	31.0	-.393	-.472			-.087	-.026		
	34.5	-.403	-.482			-.118	-.050		
	41.0	-.461	-.530			-.130	-.073		
	44.5	-.498	-.561			-.150	-.100		
	51.0	-.498	-.570			-.179	-.132		
	59.5	-.544	-.605			-.170	-.147		
	71.0	-.465	-.580			-.120	-.142		
	79.5	-.189	-.345			-.059	-.110		
	91.0	-.013	-.151			.010	-.077		
0.555 b/2	0	0.245	0.079			- -	- -		
	1.5	-.845	-1.114			0.287	0.372		
	5.5	-.548	-1.008			.139	.226		
	6.5	-.511	-.979			.113	.202		
	11.0	-.447	-.684			.045	.127		
	14.5	-.451	-.502			.012	.090		
	21.0	-.462	-.547			-.038	.027		
	24.5	-.470	-.552			-.059	.002		
	31.0	-.476	-.556			-.105	-.047		
	34.5	-.490	-.564			-.125	-.071		
	41.0	-.552	-.618			-.152	-.105		
	44.5	-.585	-.658			-.157	-.122		
	51.0	-.581	-.661			-.164	-.149		
	59.5	-.622	-.702			-.154	-.170		
	71.0	-.230	-.588			-.092	-.139		
	79.5	-.080	-.238			-.046	-.112		
	91.0	.038	-.128			.023	-.087		

TABLE XV.- CONCLUDED.

(b) α_u, 4°, 6°, 8°, 10° - Concluded.

Semi-span sta.	Percent chord	UPPER SURFACE Angle of attack 4°	6°	8°	10°	LOWER SURFACE Angle of attack 4°	6°	8°	10°
0.707 b/2	0	0.149	-0.030			- -	- -		
	1.5	-.957	-1.142			0.313	0.386		
	5.5	-.781	-1.060			.135	.219		
	6.5	-.770	-1.070			.108	.191		
	11.0	-.491	-1.032			.030	.106		
	14.5	-.528	-.991			0	.072		
	21.0	-.542	-.557			-.049	.010		
	24.5	-.541	-.567			-.068	-.016		
	31.0	-.543	-.605			-.099	-.060		
	34.5	-.562	-.629			-.111	-.081		
	41.0	-.612	-.670			-.132	-.118		
	44.5	-.660	-.713			-.150	-.140		
	51.0	-.673	-.742			-.164	-.172		
	59.5	-.362	-.791			-.175	-.201		
	71.0	-.125	-.364			-.125	-.182		
	79.5	-.029	-.238			-.060	-.182		
	91.0	.077	-.057			.052	-.107		
0.831 b/2	0	0.254	0.101			- -	- -		
	1.5	-.970	-1.149			0.312	0.367		
	5.5	-.864	-1.131			.121	.190		
	6.5	-.869	-1.137			.113	.180		
	11.0	-.725	-1.076			.035	.091		
	14.5	-.670	-1.058			- -	- -		
	21.0	-.585	-1.000			-.047	-.010		
	24.5	-.590	-.993			-.060	-.027		
	31.0	-.595	-.800			-.100	-.080		
	34.5	-.610	-.659			-.136	-.120		
	41.0	-.670	-.690			-.180	-.168		
	44.5	-.698	-.719			-.220	-.217		
	51.0	-.340	-.810			-.240	-.250		
	59.5	-.122	-.440			-.270	-.330		
	71.0	-.030	-.202			-.079	-.297		
	79.0	.033	-.149			.028	-.191		
	91.0	.095	-.079			.088	-.060		
0.924 b/2	0	-0.059	-0.272			- -	- -		
	1.5	-.931	-1.116			0.304	0.347		
	5.5	-.940	-1.151			.131	.187		
	6.5	-.936	-1.155			.124	.180		
	11.0	-.874	-1.090			.030	.079		
	14.5	-.868	-1.080			-.021	.020		
	21.0	-.582	-1.070			-.120	-.082		
	24.5	-.627	-1.072			-.201	-.170		
	31.0	-.629	-1.060			-.259	-.239		
	34.5	-.580	-.978			-.304	-.300		
	41.0	-.495	-.680			-.322	-.330		
	44.5	-.220	-.657			-.352	-.376		
	51.0	-.076	-.551			-.351	-.410		
	59.5	-.011	-.259			-.042	-.411		
	71.0	.030	-.160			.010	-.261		
	79.5	.050	-.110			.042	-.099		
	91.0	.085	-.063			.085	-.009		

NACA

TABLE XVI.- PRESSURE COEFFICIENTS AT SEVEN SEMISPAN STATIONS OF THE WING. M_o, 0.96; R, 4,000,000.

(a) α_u, 0°, 1°, 2°, 3°.

Semi-span sta.	Percent chord	UPPER SURFACE Angle of attack 0°	1°	2°	3°	LOWER SURFACE Angle of attack 0°	1°	2°	3°
0.086 b/2	0	0.606	0.606	0.603	0.587	- -	- -	- -	- -
	1.5	.172	.091	.014	-.074	0.137	0.200	0.264	0.316
	5.5	.087	.039	.003	-.043	.076	.117	.163	.200
	6.5	.059	.013	-.023	-.064	.046	.085	.128	.165
	11.0	.033	-.003	-.033	-.070	.024	.057	.096	.126
	14.5	.003	-.034	-.063	-.097	.001	.031	.069	.104
	21.0	-.018	-.050	-.077	-.106	-.018	.010	.044	.070
	24.5	-.040	-.071	-.095	-.123	-.044	-.017	.019	.044
	31.0	-.051	-.081	-.100	-.126	-.071	-.046	-.012	.013
	34.5	-.098	-.133	-.156	-.187	-.105	-.078	-.043	-.019
	41.0	-.138	-.169	-.195	-.221	-.136	-.111	-.078	-.052
	44.5	-.170	-.202	-.226	-.256	- -	- -	- -	- -
	51.0	-.201	-.232	-.253	-.282	-.186	-.160	-.131	-.108
	59.5	-.235	-.268	-.293	-.305	-.238	-.219	-.192	-.166
	71.0	-.269	-.295	-.333	-.351	-.301	-.273	-.234	-.197
	79.5	-.197	-.241	-.281	-.306	-.212	-.185	-.151	-.124
	91.0	-.096	-.117	-.149	-.164	-.101	-.091	-.082	-.076
0.195 b/2	0	0.523	0.490	0.534	0.452	- -	- -	- -	- -
	1.5	.098	.001	-.103	-.220	0.160	0.224	0.302	0.365
	5.5	-.016	-.041	-.097	-.159	.014	.068	.123	.146
	6.5	-.012	-.066	-.118	-.175	-.012	.038	.091	.135
	11.0	-.031	-.074	-.114	-.158	-.034	.006	.051	.088
	14.5	-.058	-.099	-.135	-.175	-.064	-.025	.015	.052
	21.0	-.086	-.122	-.148	-.185	-.086	-.052	-.016	.015
	24.5	-.110	-.145	-.180	-.206	-.111	-.078	-.042	-.006
	31.0	-.128	-.165	-.195	-.230	-.148	-.115	-.080	-.047
	34.5	-.163	-.191	-.221	-.253	-.180	-.146	-.113	-.082
	41.0	-.217	-.242	-.267	-.299	-.210	-.177	-.145	-.113
	44.5	-.248	-.279	-.302	-.333	-.223	-.194	-.161	-.134
	51.0	-.263	-.301	-.322	-.350	-.259	-.234	-.202	-.176
	59.5	-.301	-.332	-.354	-.379	-.314	-.289	-.254	-.221
	71.0	-.274	-.316	-.351	-.384	-.283	-.250	-.204	-.161
	79.5	-.201	-.251	-.299	-.333	-.206	-.156	-.134	-.119
	91.0	-.054	-.083	-.126	-.149	-.060	-.052	-.075	-.083
0.382 b/2	0	0.461	0.453	0.417	0.355	- -	- -	- -	- -
	1.5	.020	-.106	-.248	-.402	-0.017	0.080	0.164	0.234
	5.5	-.070	-.146	-.224	-.309	-.082	-.015	.050	.104
	6.5	-.092	-.162	-.228	-.311	-.102	-.037	.024	.077
	11.0	-.122	-.178	-.231	-.288	-.126	-.073	-.019	-.026
	14.5	-.149	-.201	-.248	-.302	-.150	-.101	-.052	-.006
	21.0	-.164	-.212	-.257	-.300	-.175	-.135	-.090	-.051
	24.5	-.201	-.240	-.273	-.319	-.201	-.156	-.114	-.077
	31.0	-.233	-.272	-.306	-.340	-.231	-.192	-.148	-.119
	34.5	-.248	-.287	-.319	-.349	-.259	-.226	-.187	-.152
	41.0	-.305	-.346	-.377	-.410	-.289	-.258	-.221	-.186
	44.5	-.323	-.368	-.403	-.442	-.316	-.285	-.246	-.209
	51.0	-.345	-.380	-.412	-.438	-.371	-.335	-.290	-.243
	59.5	-.352	-.398	-.443	-.492	-.355	-.308	-.245	-.200
	71.0	-.295	-.350	-.397	-.447	-.310	-.203	-.187	-.181
	79.5	-.048	-.094	-.233	-.268	-.044	-.043	-.068	-.083
	91.0	.067	.057	.004	-.038	.071	.063	.041	.018
0.555 b/2	0	0.439	0.441	0.410	0.345	- -	- -	- -	- -
	1.5	-.036	-.181	-.341	-.550	-0.069	0.044	0.143	0.219
	5.5	-.135	-.222	-.310	-.406	-.127	-.052	.019	.081
	6.5	-.163	-.245	-.331	-.414	-.148	-.075	.005	.057
	11.0	-.177	-.246	-.310	-.381	-.186	-.125	-.063	-.009
	14.5	-.201	-.260	-.321	-.387	-.205	-.149	-.094	-.043
	21.0	-.240	-.296	-.345	-.398	-.240	-.195	-.146	-.092
	24.5	-.256	-.306	-.348	-.405	-.263	-.219	-.170	-.121
	31.0	-.290	-.339	-.373	-.412	-.296	-.251	-.211	-.160
	34.5	-.301	-.357	-.395	-.429	-.326	-.285	-.241	-.176
	41.0	-.363	-.406	-.451	-.469	-.356	-.317	-.264	-.190
	44.5	-.389	-.436	-.475	-.521	-.384	-.341	-.285	-.211
	51.0	-.388	-.443	-.485	-.509	-.404	-.351	-.258	-.227
	59.5	-.341	-.412	-.468	-.567	-.356	-.247	-.225	-.225
	71.0	-.064	-.205	-.449	-.476	-.071	-.052	-.087	-.099
	79.5	.021	.034	-.022	-.129	.031	.001	-.021	-.041
	91.0	.097	.102	.087	.036	.102	.084	.066	.036

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TABLE XVI.- CONTINUED.

(a) α_u, 0°, 1°, 2°, 3° - Concluded.

Semi-span sta.	Percent chord	UPPER SURFACE Angle of attack 0°	1°	2°	3°	LOWER SURFACE Angle of attack 0°	1°	2°	3°
0.707 b/2	0	0.413	0.400	0.351	0.271	- -	- -	- -	- -
	1.5	-.079	-.247	-.434	-.683	-0.083	0.046	0.152	0.240
	5.5	-.195	-.301	-.409	-.524	-.186	-.096	-.012	.062
	6.5	-.216	-.327	-.429	-.550	-.200	-.115	-.037	.033
	11.0	-.216	-.294	-.372	-.462	-.237	-.167	-.103	-.040
	14.5	-.249	-.318	-.389	-.467	-.258	-.193	-.133	-.066
	21.0	-.283	-.349	-.407	-.463	-.288	-.234	-.175	-.110
	24.5	-.299	-.364	-.413	-.459	-.311	-.258	-.198	-.132
	31.0	-.335	-.384	-.434	-.468	-.352	-.298	-.234	-.179
	34.5	-.357	-.408	-.455	-.488	-.373	-.307	-.233	-.184
	41.0	-.394	-.462	-.506	-.548	-.388	-.302	-.217	-.208
	44.5	-.386	-.475	-.542	-.597	-.384	-.272	-.215	-.219
	51.0	-.338	-.434	-.530	-.587	-.347	-.217	-.218	-.226
	59.5	-.165	-.313	-.500	-.637	-.174	-.151	-.176	-.190
	71.0	-.035	-.006	-.206	-.204	-.022	-.068	-.115	-.142
	79.5	.045	.068	.058	-.047	.050	.026	-.015	-.081
	91.0	.120	.128	.143	.098	.125	.120	.109	.058
0.831 b/2	0	0.380	0.414	0.397	0.347	- -	- -	- -	- -
	1.5	-.103	-.281	-.485	-.744	0.125	0.023	0.135	0.229
	5.5	-.224	-.345	-.464	-.604	-.239	-.134	-.046	.035
	6.5	-.232	-.352	-.467	-.601	-.238	-.138	-.052	.028
	11.0	-.244	-.338	-.423	-.529	-.274	-.190	-.114	-.057
	14.5	-.271	-.357	-.437	-.525	- -	- -	- -	- -
	21.0	-.301	-.374	-.447	-.503	-.324	-.238	-.165	-.131
	24.5	-.323	-.393	-.463	-.502	-.335	-.232	-.165	-.140
	31.0	-.328	-.414	-.473	-.522	-.369	-.242	-.185	-.173
	34.5	-.323	-.423	-.488	-.538	-.355	-.221	-.186	-.191
	41.0	-.318	-.428	-.541	-.613	-.332	-.225	-.219	-.229
	44.5	-.303	-.401	-.521	-.640	-.314	-.253	-.254	-.265
	51.0	-.270	-.344	-.495	-.694	-.247	-.258	-.270	-.287
	59.5	-.028	-.026	-.294	-.260	-.044	-.107	-.258	-.329
	71.0	.015	.040	.022	-.099	.024	.018	-.010	-.117
	79.5	.071	.084	.110	.006	.081	.076	.076	.039
	91.0	.141	.144	.162	.122	.146	.143	.143	.121
0.924 b/2	0	0.405	0.351	0.246	0.112	- -	- -	- -	- -
	1.5	-.037	-.237	-.455	-.718	-0.165	0.018	0.138	0.224
	5.5	-.235	-.372	-.519	-.688	-.261	-.122	-.022	.049
	6.5	-.245	-.380	-.524	-.693	-.261	-.120	-.022	.046
	11.0	-.255	-.356	-.463	-.611	-.292	-.168	-.089	-.057
	14.5	-.284	-.380	-.475	-.606	-.307	-.189	-.120	-.098
	21.0	-.333	-.429	-.506	-.593	-.355	-.242	-.191	-.184
	24.5	-.370	-.467	-.542	-.620	-.409	-.310	-.270	-.246
	31.0	-.339	-.424	-.526	-.586	-.380	-.315	-.310	-.296
	34.5	-.299	-.378	-.499	-.560	-.327	-.305	-.325	-.330
	41.0	-.213	-.248	-.462	-.590	-.213	-.267	-.329	-.345
	44.5	-.128	-.122	-.391	-.616	-.115	-.216	-.317	-.361
	51.0	-.051	-.038	-.228	-.290	-.057	-.101	-.283	-.365
	59.5	-.013	.002	.001	-.081	-.013	-.008	.020	-.104
	71.0	.046	.052	.008	.020	.049	.044	.052	.032
	79.5	.092	.098	.112	.071	.101	.091	.090	.073
	91.0	.148	.151	.148	.113	.159	.149	.143	.117

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TABLE XVI.- CONTINUED.

(b) α_u, 4°, 6°, 8°, 10°.

Semi-span sta.	Percent chord	UPPER SURFACE Angle of attack 4°	6°	8°	10°	LOWER SURFACE Angle of attack 4°	6°	8°	10°
0.086 b/2	0	0.554				- -			
	1.5	-.182				0.360			
	5.5	-.097				.231			
	6.5	-.118				.195			
	11.0	-.116				.151			
	14.5	-.137				.122			
	21.0	-.143				.089			
	24.5	-.158				.063			
	31.0	-.182				.031			
	34.5	-.220				0			
	41.0	-.259				-.034			
	44.5	-.285				- -			
	51.0	-.314				-.095			
	59.5	-.337				-.153			
	71.0	-.385				-.174			
	79.5	-.352				-.118			
	91.0	-.213				-.096			
0.195 b/2	0	0.388				- -			
	1.5	-.365				0.413			
	5.5	-.234				.209			
	6.5	-.248				.172			
	11.0	-.217				.118			
	14.5	-.221				.080			
	21.0	-.230				.040			
	24.5	-.239				.013			
	31.0	-.263				-.027			
	34.5	-.288				-.059			
	41.0	-.336				-.093			
	44.5	-.367				-.115			
	51.0	-.377				-.161			
	59.5	-.412				-.197			
	71.0	-.430				-.149			
	79.5	-.357				-.138			
	91.0	-.202				-.145			
0.382 b/2	0	0.266				- -			
	1.5	-.603				0.286			
	5.5	-.404				.148			
	6.5	-.406				.121			
	11.0	-.337				.064			
	14.5	-.342				.025			
	21.0	-.345				-.019			
	24.5	-.362				-.041			
	31.0	-.381				-.098			
	34.5	-.393				-.135			
	41.0	-.450				-.161			
	44.5	-.484				-.175			
	51.0	-.483				-.186			
	59.5	-.535				-.212			
	71.0	-.503				-.209			
	79.5	-.334				-.195			
	91.0	-.156				-.094			
0.555 b/2	0	0.259				- -			
	1.5	-.806				0.274			
	5.5	-.536				.127			
	6.5	-.489				.103			
	11.0	-.442				.031			
	14.5	-.439				-.005			
	21.0	-.448				-.057			
	24.5	-.454				-.070			
	31.0	-.464				-.123			
	34.5	-.505				-.149			
	41.0	-.539				-.186			
	44.5	-.574				-.217			
	51.0	-.568				-.233			
	59.5	-.615				-.264			
	71.0	-.574				-.238			
	79.5	-.295				-.141			
	91.0	-.139				-.102			

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TABLE XVI.- CONCLUDED.

(b) α_u, 4°, 6°, 8°, 10° - Concluded.

Semi-span sta.	Percent chord	UPPER SURFACE Angle of attack 4°	6°	8°	10°	LOWER SURFACE Angle of attack 4°	6°	8°	10°
0.707 b/2	0	0.172				- -			
	1.5	-.898				0.295			
	5.5	-.724				.115			
	6.5	-.722				.088			
	11.0	-.483				.008			
	14.5	-.514				-.027			
	21.0	-.530				-.085			
	24.5	-.534				-.115			
	31.0	-.533				-.157			
	34.5	-.547				-.166			
	41.0	-.600				-.207			
	44.5	-.647				-.237			
	51.0	-.662				-.281			
	59.5	-.688				-.310			
	71.0	-.545				-.205			
	79.5	-.294				-.227			
	91.0	-.160				-.192			
0.831 b/2	0	0.273				- -			
	1.5	-.900				0.274			
	5.5	-.795				.076			
	6.5	-.797				.068			
	11.0	-.655				-.013			
	14.5	-.617				- -			
	21.0	-.571				-.105			
	24.5	-.581				-.120			
	31.0	-.580				-.172			
	34.5	-.594				-.197			
	41.0	-.653				-.262			
	44.5	-.679				-.306			
	51.0	-.746				-.352			
	59.5	-.732				-.361			
	71.0	-.331				-.351			
	79.5	-.258				-.303			
	91.0	-.149				-.154			
0.924 b/2	0	-0.003				- -			
	1.5	-.848				0.258			
	5.5	-.853				.079			
	6.5	-.853				.074			
	11.0	-.790				-.022			
	14.5	-.781				-.070			
	21.0	-.576				-.165			
	24.5	-.624				-.254			
	31.0	-.624				-.325			
	34.5	-.581				-.376			
	41.0	-.617				-.416			
	44.5	-.662				-.451			
	51.0	-.674				-.450			
	59.5	-.661				-.427			
	71.0	-.261				-.375			
	79.5	-.200				-.252			
	91.0	-.122				-.117			

TABLE XVII.- PRESSURE COEFFICIENTS AT SEVEN SEMISPAN STATIONS OF THE WING. M_0, 0.25; R, 6,000,000.

(a) α_u, 0°, 1°, 2°, 3°.

Semi-span sta.	Percent chord	UPPER SURFACE				LOWER SURFACE			
		Angle of attack				Angle of attack			
		0°	1°	2°	3°	0°	1°	2°	3°
0.086 b/2	0	0.491	0.462	0.457	0.408	- -	- -	- -	- -
	1.5	.050	-.059	-.161	-.117	0.033	0.103	0.170	0.237
	5.5	-.041	-.099	-.155	-.191	-.016	.030	.073	.116
	6.5	-.047	-.104	-.150	-.191	-.057	.004	.043	.085
	11.0	-.069	-.104	-.150	-.185	-.085	-.014	.019	.054
	14.5	-.086	-.110	-.150	-.180	-.068	-.039	-.006	.024
	21.0	-.098	-.127	-.161	-.188	-.078	-.047	-.026	.004
	24.5	-.103	-.116	-.161	-.188	-.096	-.069	-.041	-.014
	31.0	-.109	-.150	-.161	-.188	-.107	-.081	-.056	-.028
	34.5	-.109	-.155	-.167	-.191	-.125	-.099	-.072	-.047
	41.0	-.160	-.161	-.189	-.211	-.138	-.116	-.090	-.061
	44.5	-.154	-.179	-.201	-.222	- -	- -	- -	- -
	51.0	-.155	-.176	-.199	-.217	-.148	-.131	-.110	-.085
	59.5	-.133	-.148	-.166	-.182	-.127	-.111	-.099	-.077
	71.0	-.103	-.116	-.130	-.141	-.104	-.091	-.083	-.065
	79.5	-.058	-.067	-.079	-.085	-.069	-.058	-.054	-.040
	91.0	-.014	-.017	-.023	-.026	-.016	-.010	-.008	0
0.195 b/2	0	0.423	0.406	0.349	0.246	- -	- -	- -	- -
	1.5	-.013	-.155	-.286	-.443	0.039	0.150	0.245	0.321
	5.5	-.064	-.155	-.218	-.269	-.063	-.003	.055	.115
	6.5	-.098	-.161	-.218	-.260	-.082	-.027	.026	.078
	11.0	-.103	-.161	-.218	-.241	-.096	-.052	-.010	.035
	14.5	-.109	-.161	-.189	-.241	-.111	-.070	-.033	.009
	21.0	-.132	-.167	-.206	-.219	-.123	-.088	-.049	-.014
	24.5	-.103	-.161	-.178	-.230	-.131	-.099	-.062	-.028
	31.0	-.120	-.167	-.212	-.219	-.144	-.116	-.087	-.056
	34.5	-.160	-.184	-.218	-.202	-.154	-.126	-.102	-.074
	41.0	-.182	-.201	-.223	-.230	-.160	-.131	-.110	-.085
	44.5	-.162	-.186	-.211	-.233	-.154	-.129	-.113	-.087
	51.0	-.151	-.173	-.194	-.212	-.160	-.138	-.122	-.099
	59.5	-.129	-.148	-.162	-.175	-.131	-.117	-.104	-.086
	71.0	-.098	-.107	-.122	-.129	-.091	-.082	-.073	-.060
	79.5	-.045	-.053	-.062	-.068	-.043	-.039	-.032	-.023
	91.0	.014	.009	.003	0	.010	.015	.015	.021
0.382 b/2	0	0.355	0.349	0.292	0.134	- -	- -	- -	- -
	1.5	-.047	-.218	-.393	-.557	-0.063	0.047	0.140	0.227
	5.5	-.098	-.206	-.274	-.353	-.104	-.038	.029	.094
	6.5	-.143	-.218	-.286	-.370	-.115	-.051	.012	.072
	11.0	-.115	-.189	-.235	-.286	-.127	-.076	-.029	.022
	14.5	-.154	-.184	-.257	-.286	-.135	-.087	-.044	.008
	21.0	-.154	-.206	-.218	-.258	-.141	-.104	-.068	-.024
	24.5	-.160	-.184	-.235	-.258	-.148	-.113	-.070	-.038
	31.0	-.160	-.201	-.218	-.230	-.160	-.127	-.096	-.064
	34.5	-.166	-.206	-.229	-.241	-.162	-.129	-.104	-.074
	41.0	-.182	-.218	-.223	-.241	-.160	-.128	-.107	-.081
	44.5	-.162	-.187	-.212	-.234	-.155	-.134	-.114	-.087
	51.0	-.146	-.179	-.191	-.207	-.152	-.137	-.120	-.099
	59.5	-.127	-.145	-.162	-.176	-.123	-.110	-.096	-.088
	71.0	-.079	-.090	-.106	-.112	-.080	-.069	-.060	-.049
	79.5	-.031	-.039	-.051	-.055	-.031	-.022	-.017	-.008
	91.0	.026	.021	.017	.015	.025	.031	.031	.029
0.555 b/2	0	0.406	0.400	0.304	0.134	- -	- -	- -	- -
	1.5	-.052	-.246	-.445	-.650	-0.068	0.056	0.161	0.252
	5.5	-.137	-.218	-.331	-.409	-.104	-.028	.043	.109
	6.5	-.143	-.223	-.320	-.398	-.111	- -	.025	.092
	11.0	-.154	-.218	-.274	-.325	-.128	- -	-.021	.036
	14.5	-.149	-.212	-.257	-.297	-.129	- -	-.038	.012
	21.0	-.154	-.206	-.257	-.275	-.141	- -	-.058	-.023
	24.5	-.154	-.218	-.229	-.252	-.141	- -	-.066	-.027
	31.0	-.160	-.206	-.235	-.275	-.149	- -	-.089	-.057
	34.5	-.166	-.218	-.229	-.258	-.160	-.133	-.099	-.067
	41.0	-.199	-.218	-.263	-.258	-.156	-.133	-.104	-.075
	44.5	-.160	-.184	-.211	-.232	-.155	-.127	-.106	-.079
	51.0	-.141	-.163	-.189	-.206	-.152	-.126	-.110	-.085
	59.5	-.107	-.123	-.142	-.157	-.129	-.113	-.099	-.079
	71.0	-.075	-.085	-.099	-.104	-.074	-.062	-.055	-.041
	79.5	-.027	-.039	-.044	-.049	-.027	-.016	-.015	-.002
	91.0	.030	.021	.018	.019	.031	.036	.037	.043

NACA

TABLE XVII.- CONTINUED.

(a) α_u, 0°, 1°, 2°, 3° - Concluded.

Semi-span sta.	Percent chord	UPPER SURFACE Angle of attack 0°	1°	2°	3°	LOWER SURFACE Angle of attack 0°	1°	2°	3°
0.707 b/2	0	0.355	0.349	0.236	0.022	- -	- -	- -	- -
	1.5	-.064	-.252	-.484	-.706	-0.062	0.085	0.203	0.301
	5.5	-.149	-.240	-.342	-.437	-.113	-.024	.054	.130
	6.5	-.154	-.229	-.348	-.426	-.121	-.039	.033	.104
	11.0	-.143	-.212	-.263	-.325	-.138	-.076	-.019	.042
	14.5	-.154	-.212	-.274	-.314	-.138	-.084	-.033	.022
	21.0	-.166	-.218	-.257	-.303	-.146	-.100	-.058	-.009
	24.5	-.171	-.223	-.269	-.303	-.151	-.109	-.066	-.024
	31.0	-.182	-.218	-.229	-.275	-.158	-.122	-.087	-.052
	34.5	-.199	-.218	-.240	-.275	-.160	-.125	-.092	-.061
	41.0	-.205	-.223	-.257	-.275	-.158	-.126	-.103	-.074
	44.5	-.164	-.178	-.206	-.225	-.158	-.126	-.104	-.079
	51.0	-.148	-.161	-.184	-.199	-.148	-.125	-.112	-.089
	59.5	-.119	-.132	-.150	-.159	-.120	-.105	-.097	-.077
	71.0	-.073	-.078	-.091	-.094	-.064	-.053	-.050	-.035
	79.5	-.027	-.028	-.039	-.037	-.017	-.012	-.009	0
	91.0	.033	.033	.027	.031	.043	.048	.046	.051
0.831 b/2	0	0.355	0.394	0.343	0.179	- -	- -	- -	- -
	1.5	-.086	-.274	-.496	-.689	-0.061	0.085	0.082	0.299
	5.5	-.154	-.263	-.348	-.426	-.123	-.038	.037	.110
	6.5	-.154	-.246	-.291	-.426	-.121	-.040	.032	.104
	11.0	-.154	-.218	-.274	-.321	-.131	-.073	-.017	.041
	14.5	-.166	-.229	-.274	-.321	- -	- -	- -	- -
	21.0	-.188	-.223	-.274	-.308	-.143	-.107	-.066	-.024
	24.5	-.194	-.229	-.269	-.286	-.141	-.109	-.066	-.030
	31.0	-.205	-.229	-.263	-.264	-.150	-.123	-.090	-.058
	34.5	-.199	-.218	-.229	-.264	-.149	-.127	-.102	-.069
	41.0	-.211	-.223	-.263	-.264	-.148	-.129	-.106	-.080
	44.5	-.160	-.169	-.190	-.207	-.146	-.132	-.109	-.087
	51.0	-.151	-.157	-.173	-.185	-.135	-.120	-.104	-.088
	59.5	-.099	-.111	-.125	-.130	-.108	-.093	-.090	-.076
	71.0	-.063	-.169	-.078	-.079	-.051	-.044	-.041	-.033
	79.5	-.015	-.014	-.023	-.021	-.005	-.002	-.003	.003
	91.0	.042	.044	.039	.044	.049	.050	.047	.051
0.924 b/2	0	0.355	0.298	0.122	-0.146	- -	- -	- -	- -
	1.5	-.041	-.229	-.456	-.706	-0.075	0.067	0.178	0.273
	5.5	-.166	-.269	-.348	-.734	-.123	-.039	.033	.104
	6.5	-.166	-.269	-.342	-.711	-.126	-.049	.021	.090
	11.0	-.171	-.246	-.291	-.342	-.139	-.085	-.035	.018
	14.5	-.205	-.229	-.286	-.320	-.146	-.100	-.061	-.016
	21.0	-.205	-.218	-.246	-.286	-.150	-.115	-.087	-.055
	24.5	-.177	-.218	-.240	-.264	-.146	-.117	-.095	-.067
	31.0	-.199	-.212	-.218	-.258	-.146	-.122	-.104	-.081
	34.5	-.166	-.206	-.212	-.224	-.138	-.121	-.107	-.081
	41.0	-.199	-.218	-.218	-.224	-.140	-.123	-.113	-.091
	44.5	-.139	-.145	-.162	-.173	-.135	-.121	-.112	-.093
	51.0	-.120	-.127	-.143	-.152	-.132	-.119	-.112	-.093
	59.5	-.079	-.085	-.093	-.098	-.075	-.069	-.070	-.067
	71.0	-.039	-.038	-.044	-.047	-.031	-.028	-.031	-.029
	79.5	.003	.008	.001	-.003	.009	.008	.001	0
	91.0	.051	.056	.049	.048	.062	.060	.054	.051

NACA

TABLE XVII.- CONTINUED.

(b) α_u, 4°, 6°, 8°, 10°.

Semi-span sta.	Percent chord	UPPER SURFACE Angle of attack 4°	6°	8°	10°	LOWER SURFACE Angle of attack 4°	6°	8°	10°
0.086 b/2	0	0.342	0.099	-0.236	-0.689	- -	- -	- -	- -
	1.5	-.436	-.713	-1.087	-1.556	0.295	0.396	0.466	0.506
	5.5	-.239	-.461	-.487	-.822	.163	.247	.325	.391
	6.5	-.239	-.349	-.459	-.594	.128	.209	.287	.354
	11.0	-.233	-.293	-.381	-.454	.089	.157	.230	.292
	14.5	-.216	-.287	-.359	-.437	.060	.126	.194	.255
	21.0	-.222	-.276	-.336	-.409	.033	.091	.152	.209
	24.5	-.216	-.265	-.320	-.361	.017	.070	.127	.185
	31.0	-.216	-.254	-.292	-.353	-.004	.046	.097	.150
	34.5	-.216	-.265	-.292	-.342	-.020	.025	.079	.131
	41.0	-.233	-.271	-.314	-.364	-.037	.007	.055	.104
	44.5	-.242	-.281	-.319	-.357	- -	- -	- -	- -
	51.0	-.234	-.269	-.302	-.334	-.057	-.019	.024	.067
	59.5	-.195	-.223	-.250	-.276	-.055	-.016	.022	.061
	71.0	-.149	-.171	-.189	-.205	-.049	-.010	.026	.060
	79.5	-.091	-.106	-.115	-.125	-.026	.004	.037	.065
	91.0	-.028	-.037	-.038	-.044	.011	.029	.053	.071
0.195 b/2	0	0.105	-0.338	-0.991	-1.805	- -	- -	- -	- -
	1.5	-.611	-1.032	-1.663	-1.814	0.382	0.445	0.435	0.354
	5.5	-.351	-.500	-.667	-.862	.169	.265	.351	.415
	6.5	-.351	-.478	-.627	-.790	.131	.221	.302	.375
	11.0	-.312	-.405	-.499	-.616	.077	.157	.236	.303
	14.5	-.284	-.360	-.448	-.543	.054	.126	.195	.262
	21.0	-.267	-.332	-.392	-.474	.019	.081	.144	.205
	24.5	-.250	-.310	-.376	-.454	.001	.061	.123	.183
	31.0	-.250	-.293	-.345	-.395	-.027	.027	.085	.138
	34.5	-.259	-.282	-.346	-.398	-.045	.009	.062	.119
	41.0	-.278	-.321	-.336	-.387	-.057	-.009	.044	.092
	44.5	-.251	-.290	-.329	-.369	-.062	-.014	.034	.083
	51.0	-.230	-.265	-.295	-.327	-.063	-.033	.014	.057
	59.5	-.189	-.214	-.241	-.262	-.065	-.028	.012	.050
	71.0	-.135	-.156	-.170	-.187	-.045	-.012	.020	.050
	79.5	-.073	-.085	-.092	-.104	-.012	.012	.037	.062
	91.0	0	-.002	-.003	-.008	.029	.042	.057	.074
0.382 b/2	0	-0.098	-0.769	-1.719	-2.956	- -	- -	- -	- -
	1.5	-.797	-1.369	-1.730	-2.373	0.298	0.396	0.442	0.427
	5.5	-.464	-.657	-.868	-1.120	.153	.253	.339	.399
	6.5	-.442	-.618	-.823	-1.061	.129	.229	.313	.378
	11.0	-.357	-.489	-.616	-.750	.072	.160	.241	.307
	14.5	-.346	-.444	-.560	-.672	.048	.131	.206	.270
	21.0	-.306	-.388	-.471	-.560	.013	.084	.153	.215
	24.5	-.306	-.383	-.448	-.510	-.003	.064	.130	.191
	31.0	-.295	-.349	-.392	-.465	-.033	.027	.089	.146
	34.5	-.295	-.338	-.387	-.443	-.043	.013	.073	.125
	41.0	-.295	-.321	-.364	-.420	-.053	-.002	.050	.101
	44.5	-.254	-.298	-.337	-.377	-.062	-.012	.037	.086
	51.0	-.225	-.261	-.293	-.323	-.075	-.033	.013	.057
	59.5	-.185	-.214	-.233	-.257	-.061	-.025	.013	.050
	71.0	-.121	-.133	-.145	-.159	-.037	-.008	.021	.050
	79.5	-.057	-.067	-.073	-.080	0	.020	.044	.063
	91.0	.017	.013	.015	.014	.043	.052	.062	.074
0.555 b/2	0	-0.154	-0.338	-2.066	-3.526	- -	- -	- -	- -
	1.5	-.904	-1.660	-2.021	-2.631	0.324	0.410	0.444	0.399
	5.5	-.520	-.724	-.981	-1.249	.173	.276	.359	.414
	6.5	-.504	-.702	-.907	-1.165	.153	.256	.340	.399
	11.0	-.396	-.545	-.683	-.846	.088	.181	.266	.331
	14.5	-.363	-.495	-.616	-.745	.060	.154	.228	.293
	21.0	-.329	-.433	-.510	-.605	.020	.094	.161	.225
	24.5	-.295	-.394	-.465	-.571	.011	.078	.144	.204
	31.0	-.306	-.366	-.431	-.499	-.024	.038	.101	.155
	34.5	-.295	-.355	-.404	-.465	-.035	.021	.079	.136
	41.0	-.306	-.338	-.381	-.443	-.051	.002	.051	.103
	44.5	-.254	-.299	-.342	-.381	-.056	-.008	.042	.089
	51.0	-.224	-.260	-.293	-.325	-.065	-.011	.019	.062
	59.5	-.170	-.197	-.221	-.242	-.063	-.016	.005	.042
	71.0	-.109	-.126	-.138	-.148	-.027	-.003	.021	.047
	79.5	-.052	-.061	-.066	-.074	.004	.021	.038	.059
	91.0	.019	.019	.018	.015	.047	.053	.061	.071

NACA

TABLE XVII.- CONTINUED.

(b) α_u, 4°, 6°, 8°, 10° - Concluded.

Semi-span sta.	Percent chord	UPPER SURFACE Angle of attack 4°	6°	8°	10°	LOWER SURFACE Angle of attack 4°	6°	8°	10°
0.707 b/2	0	-0.306	-1.273	-2.664	-4.422	- -	- -	- -	- -
	1.5	-.988	-1.839	-2.150	-2.905	0.369	0.426	0.386	0.260
	5.5	-.558	-.797	-1.075	-1.349	.194	.294	.380	.427
	6.5	-.549	-.769	-.997	-1.277	.169	.275	.357	.413
	11.0	-.419	-.545	-.695	-.885	.091	.186	.269	.334
	14.5	-.385	-.500	-.655	-.784	.070	.160	.236	.302
	21.0	-.351	-.450	-.528	-.639	.027	.103	.170	.233
	24.5	-.334	-.433	-.493	-.605	.013	.081	.144	.204
	31.0	-.312	-.360	-.448	-.510	-.021	.041	.098	.154
	34.5	-.312	-.371	-.420	-.493	-.033	.026	.080	.133
	41.0	-.284	-.349	-.392	-.437	-.051	.001	.048	.094
	44.5	-.249	-.293	-.337	-.375	-.056	-.009	.036	.079
	51.0	-.218	-.250	-.285	-.312	-.068	-.028	.010	.051
	59.5	-.172	-.194	-.219	-.234	-.062	-.033	-.004	.030
	71.0	-.103	-.115	-.126	-.135	-.024	-.005	.013	.033
	79.5	-.055	-.049	-.058	-.059	.004	.019	.030	.043
	91.0	.030	.030	.026	.025	.052	.056	.060	.062
0.831 b/2	0	-0.103	-1.004	-2.228	-3.907	- -	- -	- -	- -
	1.5	-.954	-1.776	-2.060	-2.872	0.365	0.420	0.381	0.255
	5.5	-.560	-.786	-1.058	-1.349	.172	.281	.360	.409
	6.5	-.537	-.758	-.980	-1.305	.165	.271	.349	.404
	11.0	-.413	-.571	-.700	-.885	.088	.180	.259	.322
	14.5	-.385	-.517	-.627	-.790	- -	- -	- -	- -
	21.0	-.363	-.439	-.532	-.622	.018	.085	.147	.207
	24.5	-.340	-.383	-.487	-.577	-.009	.065	.124	.177
	31.0	-.323	-.366	-.415	-.493	-.032	.024	.074	.124
	34.5	-.278	-.343	-.404	-.465	-.044	.004	.050	.095
	41.0	-.284	-.321	-.364	-.392	-.059	-.020	.022	.061
	44.5	-.226	-.263	-.302	-.336	-.069	-.032	.003	.039
	51.0	-.199	-.229	-.259	-.282	-.072	-.040	-.013	.019
	59.5	-.141	-.161	-.184	-.204	-.068	-.045	-.026	-.005
	71.0	-.084	-.095	-.109	-.120	-.027	-.019	-.008	.006
	79.5	-.024	-.033	-.048	-.059	.003	.007	.010	.015
	91.0	.039	.037	.026	.010	.049	.048	.040	.035
0.924 b/2	0	-0.520	-1.598	-3.107	-4.998	- -	- -	- -	- -
	1.5	-.994	-1.744	-2.754	-3.067	0.339	0.404	0.376	0.272
	5.5	-.492	-.769	-1.008	-1.293	.166	.266	.341	.385
	6.5	-.464	-.719	-.952	-1.176	.150	.251	.323	.368
	11.0	-.391	-.545	-.655	-.829	.064	.146	.218	.273
	14.5	-.380	-.478	-.583	-.700	.025	.094	.156	.205
	21.0	-.340	-.377	-.465	-.566	-.024	.036	.080	.124
	24.5	-.295	-.360	-.426	-.504	-.043	.006	.042	.075
	31.0	-.267	-.321	-.359	-.437	-.057	-.023	.008	.038
	34.5	-.256	-.293	-.342	-.398	-.069	-.043	-.021	.001
	41.0	-.233	-.287	-.331	-.381	-.081	-.057	-.037	-.018
	44.5	-.186	-.224	-.270	-.318	-.084	-.069	-.056	-.043
	51.0	-.162	-.190	-.231	-.270	-.085	-.072	-.058	-.045
	59.5	-.108	-.133	-.179	-.225	-.065	-.063	-.061	-.062
	71.0	-.053	-.075	-.116	-.163	-.030	-.033	-.037	-.041
	79.5	-.009	-.038	-.095	-.160	-.006	-.019	-.028	-.041
	91.0	.038	.008	-.042	-.100	.043	.027	.009	-.006

NACA

TABLE XVII.- CONTINUED.

(c) α_u, 12°, 16°, 20°, 24°.

Semi-span sta.	Percent chord	UPPER SURFACE				LOWER SURFACE			
		Angle of attack				Angle of attack			
		12°	16°	20°	24°	12°	16°	20°	24°
0.086 b/2	0	-1.301	-2.917	-4.977	-7.010	--	--	--	--
	1.5	-1.806	-2.748	-3.862	-5.206	0.517	0.444	0.264	0.089
	5.5	-.730	-1.071	-1.464	-1.957	.449	.545	.613	.671
	6.5	-.724	-1.014	-1.402	-1.906	.414	.528	.612	.668
	11.0	-.534	-.738	-1.016	-1.341	.353	.472	.570	.653
	14.5	-.517	-.699	-.948	-1.229	.313	.434	.537	.623
	21.0	-.461	-.586	-.792	-1.060	.263	.380	.478	.555
	24.5	-.444	-.575	-.780	-1.004	.238	.352	.453	.527
	31.0	-.416	-.513	-.702	-.920	.201	.312	.401	.471
	34.5	-.394	-.513	-.680	-.898	.180	.289	.377	.444
	41.0	-.394	-.508	-.668	-.887	.149	.254	.334	.396
	44.5	-.398	-.514	-.648	-.869	--	--	--	--
	51.0	-.370	-.478	-.605	-.826	.108	.202	.270	.323
	59.5	-.303	-.394	-.512	-.725	.098	.180	.238	.277
	71.0	-.227	-.300	-.404	-.601	.091	.159	.203	.230
	79.5	-.141	-.201	-.291	-.469	.090	.143	.170	.178
	91.0	-.050	-.093	-.165	-.301	.088	.118	.121	.096
0.195 b/2	0	-2.808	-5.613	-5.380	-2.795	--	--	--	--
	1.5	-2.450	-3.857	-4.764	-2.461	0.196	-0.332	-0.793	-0.513
	5.5	-1.066	-1.572	-2.786	-2.405	.462	.526	.570	.621
	6.5	-.988	-1.403	-2.315	-2.293	.429	.521	.594	.646
	11.0	-.730	-1.071	-1.682	-2.248	.365	.485	.582	.644
	14.5	-.668	-.924	-1.341	-2.058	.324	.449	.546	.609
	21.0	-.556	-.761	-1.016	-1.800	.263	.389	.485	.549
	24.5	-.528	-.699	-.926	-1.677	.238	.357	.461	.515
	31.0	-.455	-.631	-.780	-1.425	.192	.309	.398	.459
	34.5	-.455	-.615	-.747	-1.357	.167	.280	.362	.421
	41.0	-.444	-.594	-.674	-1.161	.139	.244	.322	.376
	44.5	-.411	-.541	-.648	-1.114	.126	.225	.295	.348
	51.0	-.364	-.478	-.580	-.959	.100	.189	.255	.298
	59.5	-.291	-.382	-.488	-.833	.085	.160	.209	.242
	71.0	-.204	-.277	-.375	-.666	.079	.136	.169	.182
	79.5	-.117	-.177	-.273	-.562	.085	.124	.137	.130
	91.0	-.013	-.052	-.140	-.379	.088	.108	.097	.048
0.382 b/2	0	-4.366	-3.542	-2.125	-1.565	--	--	--	--
	1.5	-3.111	-2.833	-1.901	-1.397	0.365	0.238	0.279	0.261
	5.5	-1.374	-2.416	-1.957	-1.408	.444	.509	.556	.564
	6.5	-1.245	-2.078	-1.817	-1.341	.425	.510	.558	.573
	11.0	-.920	-1.853	-1.901	-1.369	.365	.478	.533	.568
	14.5	-.808	-1.532	-1.789	-1.313	.329	.446	.507	.543
	21.0	-.651	-1.239	-1.783	-1.341	.271	.385	.449	.495
	24.5	-.612	-1.082	-1.649	-1.273	.244	.354	.417	.461
	31.0	-.528	-.840	-1.537	-1.296	.197	.301	.363	.407
	34.5	-.506	-.778	-1.453	-1.229	.179	.277	.336	.378
	41.0	-.472	-.620	-1.285	-1.229	.148	.238	.289	.326
	44.5	-.421	-.562	-1.176	-1.141	.130	.215	.261	.290
	51.0	-.362	-.454	-1.014	-1.114	.098	.173	.216	.242
	59.5	-.283	-.358	-.854	-1.026	.084	.143	.167	.178
	71.0	-.178	-.228	-.633	-.931	.075	.113	.120	.106
	79.5	-.093	-.141	-.529	-.844	.051	.106	.085	.036
	91.0	.003	-.033	-.332	-.721	.083	.084	.024	-.096
0.555 b/2	0	-5.318	-2.821	-1.290	-1.229	--	--	--	--
	1.5	-3.451	-2.613	-1.217	-1.116	0.289	0.250	0.315	0.248
	5.5	-1.537	-2.022	-1.173	-1.060	.447	.508	.527	.520
	6.5	-1.397	-1.853	-1.173	-1.072	.437	.509	.525	.527
	11.0	-1.060	-1.825	-1.133	-1.049	.386	.479	.508	.527
	14.5	-.915	-1.684	-1.116	-1.027	.347	.443	.473	.505
	21.0	-.730	-1.510	-1.083	-.999	.280	.374	.412	.448
	24.5	-.668	-1.391	-1.094	-1.004	.257	.344	.386	.421
	31.0	-.567	-1.211	-1.067	-.982	.208	.291	.329	.362
	34.5	-.528	-1.132	-1.060	-.993	.187	.259	.296	.332
	41.0	-.500	-.969	-1.038	-.954	.150	.218	.247	.281
	44.5	-.427	-.891	-.971	-.909	.135	.195	.220	.248
	51.0	-.364	-.751	-.949	-.907	.103	.150	.173	.188
	59.5	-.264	-.624	-.873	-.859	.077	.109	.105	.125
	71.0	-.166	-.456	-.803	-.831	.071	.084	.058	.031
	79.5	-.084	-.380	-.729	-.785	.074	.063	-.005	-.041
	91.0	.001	-.236	-.645	-.747	.074	.026	-.125	-.207

NACA

TABLE XVII.- CONCLUDED.

(c) α_u, 12°, 16°, 20°, 24° - Concluded.

Semi-span eta.	Percent chord	UPPER SURFACE Angle of attack 12°	16°	20°	24°	LOWER SURFACE Angle of attack 12°	16°	20°	24°
0.707 b/2	0	-6.568	-1.386	-1.027	-0.971	- -	- -	- -	- -
	1.5	-3.772	-1.183	-.892	-.887	0.053	0.268	0.226	0.139
	5.5	-1.649	-1.234	-.943	-.892	.447	.499	.498	.497
	6.5	-1.553	-1.132	-.892	-.836	.441	.495	.498	.500
	11.0	-1.088	-1.149	-.892	-.842	.389	.447	.466	.498
	14.5	-.999	-1.054	-.836	-.792	.357	.413	.434	.474
	21.0	-.752	-1.071	-.881	-.808	.291	.342	.375	.415
	24.5	-.708	-1.009	-.792	-.780	.258	.307	.338	.380
	31.0	-.584	-1.009	-.836	-.808	.204	.254	.283	.319
	34.5	-.556	-.941	-.780	-.769	.180	.221	.249	.284
	41.0	-.472	-.958	-.836	-.786	.139	.173	.190	.224
	44.5	-.415	-.818	-.723	-.716	.120	.149	.165	.194
	51.0	-.340	-.785	-.723	-.721	.088	.107	.111	.139
	59.5	-.256	-.704	-.692	-.691	.056	.054	.044	.055
	71.0	-.146	-.622	-.677	-.678	.053	.019	-.017	-.017
	79.5	-.075	-.550	-.631	-.633	.053	-.019	-.076	-.077
	91.0	.005	-.466	-.602	-.596	.058	-.092	-.186	-.196
0.831 b/2	0	-5.839	-1.194	-0.904	-0.780	- -	- -	- -	- -
	1.5	-3.582	-.952	-.741	-.724	0.058	0.294	0.447	0.198
	5.5	-1.570	-.851	-.696	-.696	.431	.459	.464	.464
	6.5	-1.441	-.840	-.724	-.680	.430	.452	.464	.464
	11.0	-1.173	-.761	-.674	-.668	.371	.395	.419	.450
	14.5	-1.060	-.783	-.696	-.668	- -	- -	- -	- -
	21.0	-.786	-.727	-.668	-.640	.258	.283	.309	.356
	24.5	-.702	-.738	-.668	-.651	.227	.251	.281	.319
	31.0	-.556	-.688	-.640	-.629	.167	.188	.213	.260
	34.5	-.511	-.693	-.663	-.635	.137	.156	.178	.212
	41.0	-.444	-.671	-.618	-.618	.098	.112	.127	.164
	44.5	-.370	-.590	-.561	-.565	.072	.080	.091	.121
	51.0	-.310	-.586	-.569	-.571	.047	.047	.054	.079
	59.5	-.226	-.539	-.536	-.547	.014	-.008	-.016	.006
	71.0	-.142	-.515	-.535	-.544	.016	-.044	-.063	-.053
	79.5	-.082	-.477	-.498	-.504	.017	-.078	-.100	-.090
	91.0	-.016	-.446	-.476	-.474	.026	-.152	-.181	-.186
0.924 b/2	0	-7.038	-0.783	-0.668	-0.629	- -	- -	- -	- -
	1.5	-3.806	-.676	-.618	-.612	0.107	0.330	0.284	0.221
	5.5	-1.419	-.682	-.612	-.590	.405	.405	.415	.416
	6.5	-1.296	-.620	-.556	-.556	.386	.382	.392	.392
	11.0	-1.128	-.643	-.601	-.573	.315	.317	.343	.367
	14.5	-1.027	-.615	-.556	-.556	.245	.256	.285	.308
	21.0	-.797	-.626	-.556	-.573	.160	.183	.212	.238
	24.5	-.713	-.558	-.539	-.528	.104	.136	.154	.188
	31.0	-.523	-.569	-.545	-.556	.065	.089	.115	.139
	34.5	-.506	-.502	-.500	-.506	.020	.051	.067	.091
	41.0	-.444	-.530	-.511	-.523	0	.022	.034	.055
	44.5	-.406	-.427	-.424	-.450	-.028	-.006	.007	.019
	51.0	-.341	-.424	-.424	-.453	-.030	-.021	-.017	-.005
	59.5	-.327	-.370	-.388	-.426	-.054	-.056	-.056	-.041
	71.0	-.255	-.369	-.390	-.425	-.040	-.068	-.077	-.077
	79.5	-.296	-.323	-.354	-.391	-.042	-.090	-.101	-.115
	91.0	-.197	-.323	-.352	-.378	-.022	-.128	-.149	-.160

NACA

TABLE XVIII.- PRESSURE COEFFICIENTS AT SEVEN SEMISPAN STATIONS OF THE WING. M_o, 0.85; R, 8,000,000.

(a) α_u, 0°, 1°, 2°, 3°.

Semi-span sta.	Percent chord	UPPER SURFACE Angle of attack 0°	1°	2°	3°	LOWER SURFACE Angle of attack 0°	1°	2°	3°
0.086 b/2	0	0.455	0.455	0.435	0.395	- -	- -	- -	- -
	1.5	.030	-.069	-.183	-.303	-0.019	0.061	0.151	0.206
	5.5	-.033	-.083	-.131	-.188	-.045	0	.059	.099
	6.5	-.056	-.106	-.151	-.203	-.068	-.029	.027	.064
	11.0	-.068	-.109	-.145	-.186	-.082	-.049	-.002	.027
	14.5	-.076	-.121	-.148	-.185	-.091	-.057	-.013	.013
	21.0	-.096	-.129	-.151	-.185	-.102	-.077	-.039	-.016
	24.5	-.105	-.138	-.157	-.191	-.119	-.092	-.053	-.030
	31.0	-.099	-.132	-.151	-.180	-.128	-.100	-.068	-.045
	34.5	-.119	-.152	-.168	-.200	-.142	-.121	-.088	-.068
	41.0	-.148	-.169	-.188	-.206	-.148	-.129	-.096	-.073
	44.5	- -	- -	- -	- -	- -	- -	- -	- -
	51.0	-.165	-.187	-.197	-.220	-.160	-.135	-.108	-.093
	59.5	-.142	-.164	-.168	-.188	-.151	-.123	-.102	-.088
	71.0	-.111	-.121	-.125	-.142	-.114	-.103	-.079	-.068
	79.5	-.062	-.075	-.076	-.088	-.065	-.063	-.042	-.033
	91.0	-.013	-.020	-.016	-.027	-.019	-.014	-.002	-.004
0.195 b/2	0	0.427	0.406	0.352	0.257	- -	- -	- -	- -
	1.5	-.004	-.132	-.269	-.424	0.005	0.127	0.228	0.306
	5.5	-.070	-.132	-.203	-.263	-.085	-.017	.053	.105
	6.5	-.090	-.144	-.203	-.263	-.096	-.040	.021	.070
	11.0	-.099	-.144	-.188	-.234	-.113	-.075	-.025	.019
	14.5	-.107	-.146	-.177	-.231	-.119	-.089	-.033	-.002
	21.0	-.119	-.155	-.188	-.231	-.128	-.096	-.059	-.030
	24.5	-.119	-.155	-.177	-.214	-.133	-.098	-.068	-.039
	31.0	-.125	-.155	-.174	-.208	-.151	-.121	-.091	-.068
	34.5	-.142	-.164	-.185	-.214	-.156	-.132	-.102	-.082
	41.0	-.148	-.172	-.191	-.217	-.159	-.138	-.111	-.091
	44.5	-.159	-.181	-.203	-.231	-.153	-.132	-.105	-.088
	51.0	-.148	-.167	-.183	-.203	-.153	-.135	-.111	-.093
	59.5	-.128	-.146	-.154	-.174	-.135	-.118	-.094	-.088
	71.0	-.090	-.103	-.111	-.122	-.099	-.086	-.073	-.059
	79.5	-.041	-.054	-.059	-.059	-.047	-.040	-.030	-.025
	91.0	.010	-.020	.004	-.002	.002	.006	.013	.016
0.382 b/2	0	0.398	0.377	0.300	0.148	- -	- -	- -	- -
	1.5	-.033	-.175	-.352	-.542	-0.110	0.032	0.142	0.222
	5.5	-.096	-.175	-.252	-.341	-.119	-.040	.027	.085
	6.5	-.119	-.184	-.266	-.329	-.128	-.060	.007	.062
	11.0	-.122	-.184	-.223	-.283	-.142	-.089	-.033	.021
	14.5	-.125	-.167	-.208	-.266	-.151	-.100	-.045	-.007
	21.0	-.142	-.175	-.211	-.257	-.153	-.109	-.068	-.036
	24.5	-.148	-.175	-.206	-.251	-.153	-.118	-.073	-.045
	31.0	-.148	-.169	-.194	-.231	-.171	-.132	-.099	-.073
	34.5	-.148	-.169	-.188	-.226	-.176	-.136	-.108	-.088
	41.0	-.162	-.181	-.203	-.231	-.168	-.138	-.111	-.088
	44.5	-.156	-.181	-.203	-.231	-.159	-.144	-.111	-.093
	51.0	-.148	-.167	-.177	-.203	-.153	-.134	-.114	-.093
	59.5	-.133	-.146	-.160	-.174	-.128	-.145	-.094	-.088
	71.0	-.107	-.089	-.102	-.082	-.090	-.103	-.059	-.059
	79.5	-.041	-.046	-.053	-.059	-.041	-.031	-.025	-.022
	91.0	.019	.012	.013	.004	.016	.026	.028	.027
0.555 b/2	0	0.424	0.426	0.329	0.162	- -	- -	- -	- -
	1.5	-.016	-.187	-.381	-.590	-0.073	0.052	0.165	0.251
	5.5	-.096	-.190	-.266	-.361	-.105	-.031	.047	.119
	6.5	-.116	-.198	-.266	-.361	-.105	-.040	.036	.099
	11.0	-.111	-.164	-.229	-.292	-.119	-.072	-.013	.044
	14.5	-.114	-.161	-.220	-.277	-.119	-.075	-.019	.030
	21.0	-.131	-.164	-.217	-.257	-.128	-.095	-.045	-.010
	24.5	-.125	-.155	-.191	-.234	-.131	-.103	-.062	-.022
	31.0	-.131	-.158	-.191	-.229	-.139	-.112	-.073	-.045
	34.5	-.134	-.161	-.191	-.220	-.148	-.121	-.091	-.062
	41.0	-.151	-.167	-.197	-.217	-.145	-.123	-.093	-.068
	44.5	-.148	-.164	-.191	-.214	-.142	-.126	-.099	-.073
	51.0	-.131	-.149	-.180	-.197	-.134	-.121	-.105	-.076
	59.5	-.102	-.121	-.134	-.148	-.119	-.109	-.098	-.073
	71.0	-.065	-.075	-.094	-.093	-.065	-.046	-.036	-.033
	79.5	-.019	-.037	-.036	-.039	-.016	-.011	-.007	-.002
	91.0	.036	.026	.024	.024	.042	.041	.042	.044

NACA

TABLE XVIII.- CONTINUED.

(a) α_u, 0°, 1°, 2°, 3° - Concluded.

Semi-span sta.	Percent chord	UPPER SURFACE Angle of attack 0°	1°	2°	3°	LOWER SURFACE Angle of attack 0°	1°	2°	3°
0.707 b/2	0	0.421	0.391	0.268	0.047	- -	- -	- -	- -
	1.5	-.036	-.213	-.421	-.654	-0.062	0.075	0.211	0.300
	5.5	-.102	-.210	-.297	-.389	-.114	-.023	.056	.131
	6.5	-.114	-.213	-.303	-.384	-.119	-.034	.039	.105
	11.0	-.108	-.172	-.231	-.295	-.131	-.072	-.007	.044
	14.5	-.119	-.178	-.229	-.292	-.134	-.077	-.022	.027
	21.0	-.128	-.181	-.220	-.263	-.137	-.092	-.048	-.010
	24.5	-.131	-.175	-.211	-.246	-.142	-.103	-.056	-.019
	31.0	-.139	-.178	-.206	-.234	-.148	-.118	-.076	-.045
	34.5	-.145	-.178	-.206	-.234	-.151	-.106	-.079	-.048
	41.0	-.148	-.167	-.200	-.220	-.148	-.121	-.094	-.071
	44.5	-.148	-.164	-.191	-.217	-.145	-.115	-.096	-.076
	51.0	-.137	-.149	-.165	-.188	-.134	-.123	-.102	-.099
	59.5	-.131	-.121	-.137	-.148	-.108	-.075	-.079	-.071
	71.0	-.062	-.075	-.079	-.085	-.050	-.046	-.036	-.033
	79.5	-.016	-.020	-.033	-.033	-.007	-.006	.001	.007
	91.0	.042	.038	.039	.036	.044	.052	.050	.053
0.831 b/2	0	0.389	0.420	0.360	0.211	- -	- -	- -	- -
	1.5	-.033	-.215	-.415	-.645	-0.062	0.087	0.214	0.300
	5.5	-.108	-.210	-.306	-.392	-.114	-.029	.044	.116
	6.5	-.102	-.192	-.289	-.364	-.119	-.043	.042	.113
	11.0	-.105	-.178	-.220	-.292	-.125	-.069	-.013	.039
	14.5	-.116	-.172	-.220	-.280	- -	- -	- -	- -
	21.0	-.122	-.161	-.197	-.246	-.131	-.100	-.053	-.027
	24.5	-.125	-.161	-.188	-.237	-.128	-.100	-.065	-.036
	31.0	-.125	-.158	-.177	-.214	-.131	-.103	-.073	-.053
	34.5	-.128	-.158	-.168	-.208	-.128	-.106	-.082	-.062
	41.0	-.151	-.161	-.185	-.214	-.128	-.121	-.091	-.071
	44.5	-.142	-.155	-.174	-.194	-.125	-.115	-.094	-.073
	51.0	-.131	-.152	-.160	-.171	-.116	-.100	-.082	-.073
	59.5	-.088	-.103	-.114	-.125	-.099	-.098	-.076	-.073
	71.0	-.050	-.060	-.068	-.073	-.042	-.043	-.036	-.039
	79.5	-.007	-.014	-.016	-.019	-.002	-.003	-.010	-.004
	91.0	.047	.046	.053	.044	.056	.055	.053	.053
0.924 b/2	0	0.415	0.334	0.162	0.108	- -	- -	- -	- -
	1.5	.007	-.175	-.389	-.636	-0.071	0.072	0.300	0.271
	5.5	-.116	-.213	-.303	-.392	-.116	-.040	.042	.102
	6.5	-.125	-.215	-.292	-.389	-.119	-.043	.030	.090
	11.0	-.119	-.175	-.220	-.277	-.128	-.077	-.025	.016
	14.5	-.128	-.178	-.220	-.266	-.131	-.089	-.045	-.013
	21.0	-.128	-.161	-.188	-.220	-.139	-.103	-.073	-.045
	24.5	-.125	-.155	-.162	-.206	-.137	-.106	-.091	-.065
	31.0	-.122	-.146	-.157	-.185	-.131	-.109	-.102	-.073
	34.5	-.116	-.129	-.151	-.165	-.128	-.109	-.096	-.076
	41.0	-.131	-.129	-.157	-.168	-.128	-.112	-.099	-.088
	44.5	-.131	-.132	-.154	-.162	-.116	-.109	-.099	-.088
	51.0	-.108	-.118	-.128	-.139	-.108	-.100	-.102	-.091
	59.5	-.073	-.080	-.096	-.099	-.071	-.069	-.068	-.062
	71.0	-.030	-.031	-.042	-.045	-.033	-.037	-.036	-.030
	79.5	.007	.003	.001	-.010	.013	.015	.010	.004
	91.0	.056	.049	.044	.044	.067	.061	.047	.044

TABLE XVIII.- CONTINUED.

(b) α_u, 4°, 6°, 8°, 10°.

Semi-span sta.	Percent chord	UPPER SURFACE Angle of attack 4°	6°	8°	10°	LOWER SURFACE Angle of attack 4°	6°	8°	10°
0.086 b/2	0	0.306	0.064	-0.325	-0.808	- -	- -	- -	- -
	1.5	-.461	-.763	-1.167	-1.501	0.280	0.378	0.449	0.486
	5.5	-.252	-.366	-.506	-.635	.151	.234	.319	.386
	6.5	-.260	-.366	-.492	-.612	.113	.200	.275	.342
	11.0	-.231	-.318	-.399	-.483	.070	.139	.207	.273
	14.5	-.251	-.300	-.376	-.448	.050	.113	.184	.245
	21.0	-.217	-.283	-.342	-.399	.021	.079	.135	.199
	24.5	-.226	-.286	-.342	-.388	.004	.056	.112	.170
	31.0	-.203	-.260	-.310	-.356	-.016	.033	.089	.141
	34.5	-.223	-.274	-.319	-.359	-.039	.013	.064	.115
	41.0	-.231	-.274	-.319	-.356	-.053	-.002	.046	.098
	44.5	- -	- -	- -	- -	- -	- -	- -	- -
	51.0	-.240	-.274	-.313	-.336	-.068	-.030	.017	.064
	59.5	-.203	-.231	-.261	-.282	-.068	-.033	.006	.049
	71.0	-.154	-.174	-.195	-.213	-.056	-.030	.012	.043
	79.5	-.096	-.116	-.126	-.138	-.027	-.002	.026	.055
	91.0	-.025	-.033	-.040	-.046	.007	-.025	.040	.061
0.195 b/2	0	0.055	-0.375	-1.058	-1.872	- -	- -	- -	- -
	1.5	-.613	-1.030	-1.498	-1.952	0.372	0.429	0.420	0.325
	5.5	-.346	-.507	-.693	-.865	.168	.277	.357	.426
	6.5	-.346	-.490	-.650	-.793	.128	.220	.305	.371
	11.0	-.294	-.395	-.509	-.612	.073	.148	.227	.296
	14.5	-.271	-.366	-.460	-.543	.042	.113	.190	.256
	21.0	-.260	-.335	-.408	-.469	.005	.070	.138	.199
	24.5	-.251	-.315	-.379	-.440	-.004	.053	.121	.179
	31.0	-.234	-.289	-.348	-.397	-.039	.021	.075	.138
	34.5	-.240	-.292	-.345	-.385	-.054	-.002	.058	.121
	41.0	-.240	-.286	-.334	-.371	-.064	-.016	.035	.092
	44.5	-.242	-.286	-.328	-.362	-.062	-.019	.032	.084
	51.0	-.225	-.260	-.290	-.319	-.079	-.033	.017	.064
	59.5	-.182	-.211	-.238	-.256	-.070	-.033	.006	.052
	71.0	-.130	-.148	-.167	-.175	-.050	-.025	.012	.049
	79.5	-.096	-.082	-.092	-.098	-.010	.010	.035	.064
	91.0	-.002	-.002	-.006	-.003	.019	.030	.046	.069
0.382 b/2	0	-0.090	-0.760	-1.760	-2.993	- -	- -	- -	- -
	1.5	-.759	-1.309	-1.742	-2.384	0.292	0.395	0.434	0.429
	5.5	-.432	-.636	-.865	-1.087	.148	.257	.340	.400
	6.5	-.423	-.605	-.808	-1.009	.119	.222	.305	.371
	11.0	-.349	-.476	-.609	-.742	.062	.151	.233	.299
	14.5	-.317	-.432	-.549	-.664	.033	.113	.196	.262
	21.0	-.291	-.381	-.466	-.549	-.001	.070	.141	.204
	24.5	-.288	-.361	-.437	-.509	-.004	.056	.127	.193
	31.0	-.263	-.323	-.391	-.443	-.044	.016	.078	.141
	34.5	-.257	-.318	-.376	-.411	-.059	.004	.061	.118
	41.0	-.260	-.303	-.356	-.385	-.064	-.010	.046	.089
	44.5	-.257	-.295	-.348	-.376	-.070	-.022	.026	.081
	51.0	-.222	-.260	-.290	-.319	-.079	-.036	.015	.058
	59.5	-.188	-.217	-.241	-.261	-.067	-.030	.015	.052
	71.0	-.116	-.139	-.149	-.155	-.039	-.016	.017	.049
	79.5	-.064	-.073	-.083	-.089	-.004	.007	.026	.055
	91.0	.007	.010	-.023	.012	.027	.042	.055	.069
0.555 b/2	0	-0.076	-0.909	-2.108	-3.594	- -	- -	- -	- -
	1.5	-.838	-1.510	-1.921	-2.703	0.329	0.426	0.440	0.383
	5.5	-.473	-.703	-.966	-1.222	.179	.260	.354	.409
	6.5	-.461	-.674	-.903	-1.136	.162	.271	.351	.403
	11.0	-.358	-.504	-.670	-.822	.102	.191	.268	.325
	14.5	-.332	-.450	-.598	-.722	.073	.159	.236	.294
	21.0	-.303	-.392	-.500	-.589	.019	.102	.184	.233
	24.5	-.277	-.361	-.454	-.532	.013	.073	.150	.207
	31.0	-.263	-.332	-.399	-.480	-.016	.053	.112	.179
	34.5	-.249	-.312	-.385	-.437	-.036	.021	.072	.138
	41.0	-.246	-.297	-.362	-.399	-.042	.013	.052	.112
	44.5	-.234	-.280	-.336	-.371	-.045	-.007	.038	-.054
	51.0	-.214	-.249	-.296	-.316	-.065	-.013	.026	-.080
	59.5	-.162	-.188	-.224	-.236	-.068	-.019	.009	.043
	71.0	-.105	-.119	-.138	-.144	-.016	.013	.035	.055
	79.5	-.045	-.053	-.069	-.072	.013	.019	.048	.061
	91.0	.019	.024	.017	.012	.053	.056	.064	.064

NACA

TABLE XVIII.- CONTINUED.

(b) α_u, 4°, 6°, 8°, 10° - Concluded.

Semi-span sta.	Percent chord	UPPER SURFACE Angle of attack 4°	6°	8°	10°	LOWER SURFACE Angle of attack 4°	6°	8°	10°
0.707 b/2	0	-0.274	-1.268	-2.726	-4.529	- -	- -	- -	- -
	1.5	-.932	-1.679	-2.139	-2.976	0.369	0.421	0.380	0.233
	5.5	-.504	-.763	-1.044	-1.325	.188	.300	.377	.420
	6.5	-.493	-.723	-.992	-1.256	.168	.283	.363	.409
	11.0	-.369	-.522	-.693	-.860	.099	.197	.268	.331
	14.5	-.349	-.476	-.627	-.762	.082	.165	.236	.302
	21.0	-.303	-.407	-.512	-.612	.030	.105	.179	.233
	24.5	-.289	-.378	-.471	-.561	.016	.085	.147	.207
	31.0	-.272	-.338	-.414	-.483	-.016	.044	.104	.158
	34.5	-.263	-.329	-.397	-.454	-.019	.036	.092	.144
	41.0	-.249	-.303	-.359	-.402	-.045	.004	.055	.095
	44.9	-.234	-.283	-.336	-.374	-.045	-.007	.040	.084
	51.0	-.206	-.246	-.282	-.313	-.068	-.019	.009	.058
	59.5	-.016	-.188	-.215	-.236	-.053	-.019	.003	.035
	71.0	-.091	-.108	-.126	-.138	-.019	.004	.020	.043
	79.5	-.033	.045	-.054	-.054	.010	.016	.035	.049
	91.0	.036	.010	.032	.029	.050	.056	.061	.064
0.831 b/2	0	-0.068	-0.949	-2.286	-3.974	- -	- -	- -	- -
	1.5	-.892	-1.510	-2.090	-2.873	0.363	0.429	0.386	0.242
	5.5	-.501	-.746	-1.024	-1.314	.188	.294	.360	.417
	6.5	-.473	-.691	-.955	-1.196	.165	.274	.351	.409
	11.0	-.358	-.504	-.667	-.839	.102	.188	.268	.328
	14.5	-.343	-.470	-.609	-.739	- -	- -	- -	- -
	21.0	-.289	-.375	-.480	-.566	.016	.085	.156	.213
	24.5	-.272	-.355	-.437	-.512	.007	.073	.130	.196
	31.0	-.240	-.303	-.368	-.431	-.025	.030	.081	.138
	34.5	-.231	-.289	-.351	-.420	-.030	.016	.058	.110
	41.0	-.226	-.272	-.330	-.359	-.050	-.013	.029	.072
	44.5	-.214	-.251	-.293	-.330	-.059	-.016	.015	.049
	51.0	-.188	-.217	-.250	-.276	-.062	-.030	.003	.040
	59.5	-.131	-.157	-.178	-.204	-.068	-.045	-.020	.006
	71.0	-.073	-.088	-.103	-.115	-.027	-.013	-.006	.015
	79.5	-.016	-.027	-.043	-.052	.007	.010	.012	.023
	91.0	.044	.042	.035	.023	.056	.050	.052	.052
0.924 b/2	0	-0.478	-1.584	-3.074	-4.949	- -	- -	- -	- -
	1.5	-.904	-1.656	-2.246	-3.094	0.343	0.415	0.386	0.268
	5.5	-.490	-.720	-.980	-1.242	.171	.277	.340	.388
	6.5	-.461	-.677	-.908	-1.139	.156	.260	.328	.377
	11.0	-.343	-.473	-.621	-.762	.067	.159	.225	.282
	14.5	-.309	-.415	-.535	-.650	.036	.102	.167	.219
	21.0	-.260	-.335	-.417	-.494	-.016	.039	.081	.127
	24.5	-.231	-.297	-.368	-.437	-.030	.004	.046	.078
	31.0	-.203	-.257	-.310	-.365	-.050	-.016	.012	.043
	34.5	-.185	-.237	-.302	-.351	-.059	-.033	-.017	.009
	41.0	-.185	-.231	-.276	-.322	-.073	-.048	-.034	-.014
	44.5	-.174	-.214	-.267	-.307	-.073	-.059	-.046	-.020
	51.0	-.145	-.185	-.224	-.270	-.076	-.068	-.052	-.043
	59.5	-.102	-.128	-.178	-.221	-.062	-.059	-.049	-.049
	71.0	-.045	-.073	-.112	-.158	-.030	-.039	-.034	-.034
	79.5	-.013	-.042	-.092	-.149	-.004	-.013	-.020	-.031
	91.0	.042	.004	-.040	-.092	.044	.033	.012	.006

NACA

TABLE XVIII.- CONTINUED.

(c) α_u, 12°, 16°, 20°, 24°.

Semi-span sta.	Percent chord	UPPER SURFACE Angle of attack 12°	16°	20°	24°	LOWER SURFACE Angle of attack 12°	16°	20°	24°
0.086 b/2	0	-1.418	-3.022	-5.147	-7.566	- -	- -	- -	- -
	1.5	-1.886	-2.878	-4.026	-5.277	0.495	0.406	0.177	-0.129
	5.5	-.785	-1.095	-1.435	-1.797	.437	.529	.584	.617
	6.5	-.745	-1.021	-1.329	-1.670	.406	.506	.584	.646
	11.0	-.549	-.765	-.961	-1.207	.337	.443	.541	.331
	14.5	-.529	-.693	-.869	-1.141	.308	.414	.516	.617
	21.0	-.492	-.586	-.723	-1.016	.253	.357	.464	.547
	24.5	-.448	-.563	-.694	-1.034	.227	.334	.435	.521
	31.0	-.399	-.497	-.616	-.930	.196	.299	.395	.472
	34.5	-.405	-.492	-.613	-.933	.170	.265	.369	.440
	41.0	-.391	-.469	-.588	-.881	.144	.233	.335	.400
	44.5	- -	- -	- -	- -	- -	- -	- -	- -
	51.0	-.368	-.428	-.536	-.823	.110	.199	.283	.333
	59.5	-.305	-.351	-.467	-.733	.084	.170	.240	.284
	71.0	-.227	-.261	-.364	-.606	.081	.147	.205	.229
	79.5	-.146	-.169	-.266	-.476	.084	.141	.182	.189
	91.0	-.046	-.054	-.125	-.314	.084	.121	.139	.119
0.195 b/2	0	-2.924	-5.584	-9.097	-8.797	- -	- -	- -	- -
	1.5	-2.545	-3.873	-5.428	-3.132	0.156	0.437	-1.340	-1.369
	5.5	-1.064	-1.507	-2.044	-2.944	.469	.518	.504	.582
	6.5	-.975	-1.348	-1.814	-2.641	.426	.509	.541	.625
	11.0	-.733	-.986	-1.297	-2.525	.354	.466	.550	.646
	14.5	-.644	-.851	-1.110	-2.242	.314	.426	.527	.619
	21.0	-.546	-.704	-.909	-1.774	.259	.377	.484	.567
	24.5	-.509	-.647	-.846	-1.658	.239	.348	.455	.530
	31.0	-.448	-.561	-.743	-1.311	.190	.299	.398	.475
	34.5	-.437	-.535	-.726	-1.253	.167	.276	.375	.437
	41.0	-.408	-.494	-.674	-1.028	.138	.245	.332	.394
	44.5	-.402	-.474	-.665	-1.022	.133	.230	.317	.365
	51.0	-.351	-.411	-.588	-.869	.110	.199	.277	.322
	59.5	-.279	-.325	-.493	-.762	.081	.173	.231	.264
	71.0	-.192	-.221	-.364	-.603	.078	.147	.186	.200
	79.5	-.106	-.123	-.249	-.487	.081	.147	.168	.163
	91.0	-.006	-.008	-.099	-.300	.081	.130	.122	.076
0.382 b/2	0	-4.538	-8.532	-12.334	- -	- -	- -	- -	- -
	1.5	-3.117	-4.765	-5.305	-1.499	0.354	0.043	-0.280	0.119
	5.5	-1.343	-1.924	-3.179	-1.499	.446	.478	.498	.562
	6.5	-1.228	-1.717	-2.958	-1.456	.420	.478	.533	.567
	11.0	-.897	-1.242	-2.188	-1.461	.357	.455	.547	.576
	14.5	-.782	-1.070	-2.162	-1.412	.317	.426	.524	.553
	21.0	-.638	-.834	-1.630	-1.427	.268	.368	.470	.510
	24.5	-.589	-.759	-1.507	-1.375	.245	.354	.441	.475
	31.0	-.509	-.638	-1.110	-1.355	.193	.302	.383	.420
	34.5	-.474	-.589	-1.053	-1.311	.173	.279	.355	.385
	41.0	-.437	-.529	-.832	-1.282	.144	.245	.306	.336
	44.5	-.411	-.494	-.806	-1.227	.130	.225	.283	.307
	51.0	-.353	-.417	-.665	-1.181	.104	.196	.245	.273
	59.5	-.279	-.322	-.550	-1.080	.052	.167	.197	.206
	71.0	-.169	-.195	-.392	-.938	.052	.138	.154	.134
	79.5	-.092	-.112	-.297	-.834	.052	.130	.122	.082
	91.0	.009	-.008	-.171	-.670	.052	.110	.067	-.054
0.555 b/2	0	-5.464	-10.306	-4.285	-2.034	- -	- -	- -	- -
	1.5	-3.554	-5.464	-1.613	-1.144	0.262	-0.192	0.110	0.154
	5.5	-1.512	-2.159	-1.570	-1.109	.449	.440	.524	.527
	6.5	-1.380	-1.961	-1.518	-1.092	.446	.455	.541	.539
	11.0	-.995	-1.415	-1.498	-1.083	.394	.463	.524	.547
	14.5	-.857	-1.231	-1.426	-1.037	.351	.449	.507	.527
	21.0	-.690	-.911	-1.435	-1.034	.291	.397	.449	.472
	24.5	-.616	-.822	-1.355	-1.002	.265	.371	.406	.443
	31.0	-.535	-.681	-1.340	-1.011	.210	.317	.363	.385
	34.5	-.508	-.635	-1.383	-.999	.184	.294	.326	.354
	41.0	-.443	-.549	-1.237	-.993	.153	.253	.277	.302
	44.5	-.420	-.512	-1.179	-.973	.138	.227	.257	.267
	51.0	-.351	-.523	-1.116	-.973	.115	.199	.202	.212
	59.5	-.256	-.307	-.967	-.912	.084	.150	.145	.125
	71.0	-.155	-.184	-.803	-.860	.087	.133	.145	.065
	79.5	-.072	-.106	-.662	-.803	.089	.115	.056	-.022
	91.0	.012	-.020	.490	-.742	.089	.087	-.027	-.172

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TABLE XVIII.- CONCLUDED.

(c) α_u, 12°, 16°, 20°, 24° - Concluded.

Semi-span sta.	Percent chord	UPPER SURFACE				LOWER SURFACE			
		Angle of attack				Angle of attack			
		12°	16°	20°	24°	12°	16°	20°	24°
0.707 b/2	0	-6.810	-12.544	-1.696	-1.323	- -	- -	- -	- -
	1.5	-3.908	-5.872	-1.208	-.886	-0.011	-0.785	0.062	0.065
	5.5	-1.662	-2.427	-1.064	-.860	.443	.397	.490	.498
	6.5	-1.541	-2.329	-1.030	-.849	.446	.440	.493	.501
	11.0	-1.041	-1.469	-1.024	-.831	.391	.463	.487	.501
	14.5	-.917	-1.277	-.978	-.803	.360	.446	.458	.481
	21.0	-.716	-.934	-.975	-.797	.291	.397	.403	.429
	24.5	-.658	-.851	-.938	-.771	.265	.368	.372	.403
	31.0	-.549	-.710	-.950	-.774	.210	.314	.312	.333
	34.5	-.514	-.664	-.921	-.748	.190	.291	.286	.307
	41.0	-.446	-.569	-.941	-.768	.147	.236	.228	.241
	44.5	-.423	-.520	-.912	-.745	.130	.213	.197	.212
	51.0	-.342	-.428	-.901	-.768	.092	.167	.142	.154
	59.5	-.256	-.307	-.832	-.733	.064	.138	.085	.076
	71.0	-.141	-.187	-.771	-.716	.061	.107	.027	.004
	79.5	-.063	-.106	-.978	-.667	.061	.081	.033	-.063
	91.0	.023	-.049	-.912	-.626	.064	.055	.148	-.187
0.831 b/2	0	-6.142	-11.083	-1.369	-1.025	- -	- -	- -	- -
	1.5	-3.733	-4.336	-.792	-.667	0	-0.655	0.197	0.310
	5.5	-1.604	-2.998	-.777	-.664	.443	.443	.475	.475
	6.5	-1.481	-2.976	-.746	-.638	.432	.449	.472	.472
	11.0	-1.015	-1.967	-.737	-.626	.383	.466	.444	.455
	14.5	-.900	-1.765	-.677	-.609	- -	- -	- -	- -
	21.0	-.678	-.975	-.691	-.600	.265	.354	.340	.356
	24.5	-.615	-1.003	-.674	-.586	.239	.337	.306	.330
	31.0	-.497	-.730	-.677	-.592	.184	.268	.248	.270
	34.5	-.454	-.670	-.651	-.566	.153	.236	.217	.235
	41.0	-.399	-.520	-.680	-.592	.107	.190	.168	.180
	44.5	-.365	-.437	-.662	-.586	.089	.161	.128	.137
	51.0	-.307	-.339	-.674	-.597	.066	.124	.093	.099
	59.5	-.224	-.221	-.645	-.586	.023	.066	.013	.013
	71.0	-.123	-.126	-.628	-.568	.029	.052	-.039	-.045
	79.5	-.075	-.080	-.588	-.528	.032	.038	-.056	-.089
	91.0	.009	-.049	-.536	-.499	.040	.017	-.177	-.187
0.924 b/2	0	-7.212	-2.398	-0.789	-0.655	- -	- -	- -	- -
	1.5	-4.100	-2.062	-.662	-.566	0.055	0.066	0.254	0.212
	5.5	-1.527	-2.021	-.608	-.534	.411	.449	.426	.417
	6.5	-1.397	-1.872	-.588	-.511	.386	.423	.406	.394
	11.0	-.929	-1.895	-.576	-.508	.322	.383	.358	.362
	14.5	-.765	-1.719	-.550	-.490	.256	.319	.329	.310
	21.0	-.595	-1.659	-.539	-.487	.161	.236	.225	.244
	24.5	-.532	-1.561	-.513	-.479	.110	.176	.182	.195
	31.0	-.440	-1.317	-.504	-.470	.078	.127	.133	.151
	34.5	-.411	-1.320	-.490	-.456	.026	.084	.090	.108
	41.0	-.374	-.940	-.501	-.470	.009	.061	.053	.067
	44.5	-.368	-1.044	-.476	-.456	-.020	.032	.027	.036
	51.0	-.316	-.713	-.499	-.473	-.023	.026	.001	.013
	59.5	-.284	-.808	-.473	-.453	-.052	-.017	-.045	-.045
	71.0	-.218	-.538	-.493	-.453	-.037	-.011	-.076	-.080
	79.5	-.244	-.589	-.455	-.412	-.046	-.026	-.102	-.106
	91.0	-.152	-.371	-.435	-.395	-.020	-.043	-.160	-.164

NACA

TABLE XIX.- PRESSURE COEFFICIENTS AT SEVEN SEMISPAN STATIONS OF THE WING. M_0, 0.25; R, 5,000,000.

(a) α_u, 0°, 1°, 2°, 3°.

Semi-span sta.	Percent chord	UPPER SURFACE Angle of attack 0°	1°	2°	3°	LOWER SURFACE Angle of attack 0°	1°	2°	3°
0.086 b/2	0	0.484	0.475	0.454	0.402	- -	- -	- -	- -
	1.5	.038	-.067	-.156	-.284	0.021	0.106	0.173	0.239
	5.5	-.027	-.071	-.117	-.160	-.045	.033	.078	.123
	6.5	-.031	-.079	-.121	-.164	-.038	.008	.047	.090
	11.0	-.057	-.088	-.121	-.156	-.047	-.008	.021	.059
	14.5	-.070	-.110	-.138	-.160	-.068	-.032	-.004	.030
	21.0	-.074	-.110	-.147	-.168	-.076	-.044	-.019	.009
	24.5	-.108	-.118	-.151	-.173	-.094	-.062	-.037	-.009
	31.0	-.104	-.116	-.147	-.151	-.109	-.076	-.051	-.025
	34.5	-.113	-.148	-.156	-.161	-.123	-.086	-.069	-.041
	41.0	-.130	-.170	-.194	-.194	-.130	-.111	-.084	-.059
	44.5	-.155	-.181	-.201	-.220	- -	- -	- -	- -
	51.0	-.146	-.179	-.196	-.215	-.150	-.127	-.108	-.085
	59.5	-.132	-.153	-.166	-.181	-.129	-.112	-.093	-.075
	71.0	-.104	-.117	-.128	-.142	-.107	-.090	-.079	-.067
	79.5	-.062	-.067	-.074	-.084	-.070	-.057	-.049	-.037
	91.0	-.010	-.015	-.022	-.022	-.015	-.011	-.005	.003
0.195 b/2	0	0.411	0.402	0.355	0.261	- -	- -	- -	- -
	1.5	-.010	-.165	-.280	-.430	0.032	0.155	0.240	0.053
	5.5	-.074	-.153	-.198	-.250	-.087	.001	.057	.115
	6.5	-.078	-.157	-.211	-.267	-.088	-.024	.025	.080
	11.0	-.108	-.153	-.194	-.229	-.098	-.051	-.010	.038
	14.5	-.108	-.153	-.160	-.216	-.110	-.065	-.019	.015
	21.0	-.117	-.157	-.190	-.207	-.123	-.090	-.045	-.014
	24.5	-.113	-.157	-.177	-.198	-.134	-.086	-.061	-.031
	31.0	-.121	-.157	-.168	-.203	-.147	-.108	-.087	-.058
	34.5	-.147	-.187	-.194	-.224	-.155	-.126	-.097	-.069
	41.0	-.160	-.195	-.203	-.233	-.155	-.127	-.107	-.082
	44.5	-.164	-.191	-.208	-.228	-.153	-.127	-.110	-.084
	51.0	-.154	-.173	-.192	-.209	-.155	-.136	-.120	-.097
	59.5	-.129	-.145	-.159	-.173	-.133	-.117	-.104	-.086
	71.0	-.094	-.108	-.119	-.127	-.094	-.080	-.069	-.060
	79.5	-.043	-.052	-.061	-.065	-.045	-.038	-.028	-.019
	91.0	.014	.005	.006	.003	.011	.017	.019	.024
0.382 b/2	0	0.368	0.354	0.282	0.145	- -	- -	- -	- -
	1.5	-.044	-.230	-.370	-.550	-0.065	0.107	0.144	0.227
	5.5	-.108	-.213	-.276	-.327	-.109	-.028	.032	.092
	6.5	-.121	-.200	-.280	-.323	-.113	-.041	.013	.072
	11.0	-.121	-.191	-.229	-.276	-.126	-.067	-.022	.033
	14.5	-.130	-.183	-.229	-.267	-.132	-.080	-.035	.009
	21.0	-.143	-.195	-.211	-.241	-.143	-.090	-.060	-.020
	24.5	-.151	-.185	-.203	-.241	-.150	-.102	-.071	-.037
	31.0	-.151	-.195	-.198	-.233	-.160	-.117	-.093	-.064
	34.5	-.147	-.187	-.198	-.237	-.158	-.123	-.100	-.069
	41.0	-.160	-.200	-.203	-.237	-.150	-.125	-.105	-.078
	44.5	-.160	-.188	-.209	-.252	-.151	-.128	-.109	-.087
	51.0	-.148	-.170	-.187	-.205	-.155	-.132	-.116	-.097
	59.5	-.129	-.145	-.160	-.172	-.125	-.108	-.093	-.075
	71.0	-.080	-.089	-.130	-.112	-.080	-.067	-.058	-.044
	79.5	-.034	-.039	-.047	-.051	-.030	-.020	-.014	-.006
	91.0	.024	.019	.015	.015	.024	.031	.033	.035
0.555 b/2	0	0.407	0.393	0.316	0.149	- -	- -	- -	- -
	1.5	-.053	-.277	-.417	-.628	-0.062	0.070	0.162	0.251
	5.5	-.115	-.217	-.280	-.374	-.107	-.015	.043	.109
	6.5	-.130	-.238	-.284	-.366	-.109	-.033	.025	.091
	11.0	-.130	-.195	-.241	-.297	-.123	-.064	-.018	.034
	14.5	-.143	-.195	-.233	-.280	-.126	-.076	-.033	.020
	21.0	-.151	-.191	-.224	-.259	-.140	-.097	-.060	-.020
	24.5	-.151	-.195	-.203	-.241	-.137	-.100	-.066	-.031
	31.0	-.151	-.195	-.224	-.241	-.149	-.108	-.087	-.055
	34.5	-.151	-.195	-.207	-.237	-.153	-.118	-.098	-.067
	41.0	-.160	-.200	-.229	-.241	.149	-.123	-.106	-.085
	44.5	-.155	-.184	-.206	-.229	-.148	-.124	-.107	-.078
	51.0	-.141	-.167	-.184	-.202	-.145	-.125	-.109	-.087
	59.5	-.108	-.127	-.140	-.155	-.122	-.110	-.098	-.078
	71.0	-.073	-.084	-.103	-.103	-.066	-.060	-.051	-.040
	79.5	-.028	-.035	-.041	-.047	-.020	-.016	-.013	-.004
	91.0	.030	.023	.020	.019	.037	.035	.036	.041

NACA

TABLE XIX.- CONTINUED.

(a) α_u, 0°, 1°, 2°, 3° - Concluded.

Semi-span sta.	Percent chord	UPPER SURFACE Angle of attack 0°	1°	2°	3°	LOWER SURFACE Angle of attack 0°	1°	2°	3°
0.707 b/2	0	0.359	0.324	0.261	0.029	- -	- -	- -	- -
	1.5	-.061	-.264	-.452	-.675	-0.057	0.107	0.201	0.297
	5.5	-.126	-.251	-.301	-.409	-.108	-.010	.051	.127
	6.5	-.126	-.238	-.319	-.392	-.118	-.025	.033	.110
	11.0	-.113	-.204	-.250	-.310	-.134	-.067	-.019	.040
	14.5	-.130	-.200	-.241	-.293	-.134	-.072	-.031	.026
	21.0	-.156	-.230	-.233	-.280	-.140	-.091	-.053	-.012
	24.5	-.156	-.204	-.237	-.271	-.146	-.101	-.068	-.026
	31.0	-.160	-.208	-.224	-.250	-.151	-.114	-.088	-.052
	34.5	-.164	-.200	-.237	-.246	-.153	-.112	-.092	-.060
	41.0	-.173	-.204	-.229	-.241	-.143	-.118	-.102	-.073
	44.5	-.149	-.184	-.206	-.225	-.140	-.117	-.104	-.077
	51.0	-.132	-.165	-.182	-.198	-.140	-.124	-.109	-.088
	59.5	-.113	-.135	-.150	-.161	-.114	-.105	-.094	-.077
	71.0	-.065	-.080	-.089	-.094	-.057	-.052	-.047	-.034
	79.5	-.019	-.030	-.038	-.039	-.011	-.011	-.010	-.002
	91.0	.040	.032	.028	.031	.047	.046	.044	.050
0.831 b/2	0	0.355	0.364	0.347	0.192	- -	- -	- -	- -
	1.5	-.065	-.299	-.452	-.696	-0.057	0.104	0.201	0.295
	5.5	-.147	-.247	-.323	-.413	-.120	-.024	.036	.109
	6.5	-.143	-.247	-.323	-.383	-.111	-.027	.031	.100
	11.0	-.138	-.200	-.241	-.319	-.128	-.061	-.021	.037
	14.5	-.151	-.230	-.237	-.314	- -	- -	- -	- -
	21.0	-.156	-.221	-.241	-.280	-.136	-.096	-.061	-.020
	24.5	-.164	-.221	-.233	-.271	-.133	-.098	-.069	-.032
	31.0	-.164	-.195	-.237	-.246	-.141	-.089	-.089	-.060
	34.5	-.181	-.204	-.216	-.237	-.140	-.113	-.097	-.069
	41.0	-.194	-.208	-.229	-.237	-.140	-.118	-.105	-.079
	44.5	-.146	-.173	-.190	-.207	-.138	-.118	-.108	-.087
	51.0	-.132	-.158	-.173	-.183	-.129	-.113	-.106	-.088
	59.5	-.094	-.114	-.126	-.132	-.103	-.096	-.089	-.077
	71.0	-.065	-.077	-.077	-.078	-.047	-.043	-.042	-.036
	79.5	-.009	-.017	-.022	-.022	.046	-.001	-.005	.002
	91.0	.047	.042	.037	.041	.056	.051	.047	.050
0.924 b/2	0	0.359	0.256	0.149	-0.138	- -	- -	- -	- -
	1.5	-.031	-.251	-.422	-.671	-0.066	0.090	0.174	0.270
	5.5	-.151	-.273	-.327	-.443	-.120	-.024	.030	.101
	6.5	-.151	-.247	-.323	-.409	-.123	-.033	.020	.090
	11.0	-.156	-.238	-.246	-.314	-.135	-.072	-.037	.015
	14.5	-.160	-.234	-.250	-.284	-.137	-.089	-.058	-.016
	21.0	-.173	-.230	-.229	-.259	-.143	-.109	-.086	-.048
	24.5	-.160	-.195	-.203	-.241	-.140	-.109	-.086	-.060
	31.0	-.160	-.195	-.194	-.220	-.139	-.114	-.096	-.077
	34.5	-.156	-.170	-.190	-.203	-.132	-.115	-.099	-.080
	41.0	-.151	-.187	-.186	-.203	-.124	-.118	-.108	-.091
	44.5	-.123	-.146	-.160	-.171	-.114	-.116	-.107	-.092
	51.0	-.113	-.134	-.142	-.151	-.113	-.104	-.106	-.094
	59.5	-.073	-.087	-.093	-.097	-.118	-.071	-.073	-.069
	71.0	-.033	-.040	-.045	-.046	-.023	-.026	-.030	-.030
	79.5	.012	.006	.002	-.002	.018	.007	.005	.001
	91.0	.056	.052	.048	.045	.069	.060	.052	.051

NACA

TABLE XIX.- CONTINUED.

(b) α_u, 4°, 6°, 8°, 10°.

Semi-span sta.	Percent chord	UPPER SURFACE Angle of attack 4°	6°	8°	10°	LOWER SURFACE Angle of attack 4°	6°	8°	10°
0.086 b/2	0	0.338	0.319	-0.276	-0.713	- -	- -	- -	- -
	1.5	-.413	-.711	-1.104	-1.489	0.296	0.396	0.465	0.503
	2.5	-.229	-.339	-.533	-.635	.163	.250	.326	.391
	6.5	-.229	-.331	-.465	-.585	.128	.210	.286	.356
	11.0	-.198	-.284	-.413	-.484	.088	.159	.227	.290
	14.5	-.203	-.284	-.370	-.428	.060	.126	.190	.253
	21.0	-.194	-.262	-.370	-.415	.033	.092	.152	.209
	24.5	-.198	-.258	-.327	-.372	.012	.070	.125	.184
	31.0	-.194	-.245	-.336	-.376	-.005	.047	.097	.149
	34.5	-.198	-.245	-.323	-.342	-.021	.029	.080	.128
	41.0	-.233	-.254	-.327	-.355	-.036	.010	.058	.101
	44.5	-.245	-.279	-.316	-.359	- -	- -	- -	- -
	51.0	-.236	-.269	-.302	-.334	-.060	-.017	.024	.067
	59.5	-.198	-.223	-.256	-.276	-.059	-.014	.024	.062
	71.0	-.153	-.168	-.189	-.207	-.049	-.008	.027	.060
	79.5	-.092	-.102	-.117	-.127	-.030	.005	.038	.063
	91.0	-.031	-.031	-.036	-.041	.008	.029	.050	.071
0.195 b/2	0	0.106	-0.321	-0.984	-1.769	- -	- -	- -	- -
	1.5	-.602	-1.019	-1.529	-1.842	0.378	0.445	0.433	0.353
	2.5	-.323	-.497	-.675	-.846	.165	.266	.350	.418
	6.5	-.327	-.463	-.641	-.799	.127	.224	.307	.372
	11.0	-.280	-.378	-.516	-.622	.077	.160	.235	.306
	14.5	-.271	-.339	-.460	-.549	.050	.126	.198	.263
	21.0	-.246	-.322	-.409	-.458	.016	.080	.146	.208
	24.5	-.241	-.292	-.396	-.441	.001	.063	.123	.184
	31.0	-.237	-.288	-.366	-.398	-.027	.029	.085	.141
	34.5	-.246	-.292	-.374	-.411	-.036	.010	.066	.118
	41.0	-.250	-.288	-.366	-.372	-.050	-.008	.043	.094
	44.5	-.251	-.289	-.326	-.366	-.064	-.015	.034	.081
	51.0	-.234	-.261	-.293	-.328	-.078	-.031	.012	.059
	59.5	-.190	-.213	-.237	-.265	-.068	-.028	.010	.050
	71.0	-.139	-.152	-.168	-.187	-.046	-.014	.021	.051
	79.5	-.074	-.083	-.091	-.103	-.012	.014	.038	.062
	91.0	.001	0	-.004	-.006	.029	.042	.062	.075
0.382 b/2	0	-0.091	-0.754	-1.701	-2.911	- -	- -	- -	- -
	1.5	-.765	-1.343	-1.726	-2.381	0.294	0.396	0.440	0.434
	2.5	-.443	-.626	-.868	-1.105	.147	.255	.336	.400
	6.5	-.422	-.591	-.808	-1.014	.122	.229	.312	.378
	11.0	-.344	-.459	-.628	-.760	.076	.163	.239	.310
	14.5	-.323	-.446	-.555	-.674	.045	.131	.203	.270
	21.0	-.293	-.369	-.495	-.570	.010	.083	.151	.216
	24.5	-.284	-.344	-.456	-.523	-.006	.065	.127	.190
	31.0	-.271	-.327	-.413	-.463	-.036	.029	.087	.146
	34.5	-.250	-.322	-.387	-.432	-.046	.013	.069	.127
	41.0	-.276	-.292	-.370	-.398	-.057	-.002	.049	.099
	44.5	-.255	-.293	-.336	-.375	-.065	-.010	.034	.082
	51.0	-.227	-.260	-.289	-.325	-.078	-.030	.015	.058
	59.5	-.190	-.212	-.238	-.257	-.061	-.024	.015	.050
	71.0	-.121	-.135	-.147	-.160	-.036	-.004	.021	.050
	79.5	-.060	-.066	-.073	-.079	.001	.022	.043	.063
	91.0	.014	.014	.015	.015	.037	.051	.066	.074
0.555 b/2	0	-0.113	-0.690	-2.040	-3.460	- -	- -	- -	- -
	1.5	-.881	-1.605	-1.898	-2.696	0.319	0.421	0.440	0.400
	2.5	-.495	-.711	-.980	-1.234	.166	.280	.357	.416
	6.5	-.486	-.677	-.928	-1.152	.147	.261	.337	.400
	11.0	-.370	-.510	-.683	-.842	.090	.185	.262	.333
	14.5	-.357	-.463	-.628	-.760	.063	.150	.225	.294
	21.0	-.297	-.408	-.520	-.609	.014	.093	.160	.222
	24.5	-.293	-.369	-.499	-.570	.006	.076	.141	.203
	31.0	-.280	-.339	-.426	-.497	-.027	.039	.099	.156
	34.5	-.280	-.327	-.413	-.467	-.041	.022	.078	.134
	41.0	-.263	-.322	-.383	-.415	-.052	.002	.052	.100
	44.5	-.255	-.298	-.339	-.385	-.059	-.006	.041	.088
	51.0	-.227	-.260	-.295	-.327	-.069	-.019	.020	.062
	59.5	-.173	-.195	-.222	-.244	-.066	-.027	.009	.041
	71.0	-.115	-.127	-.139	-.153	-.031	-.002	.021	.047
	79.5	-.055	-.062	-.066	-.072	.003	.023	.036	.059
	91.0	.015	.019	.019	.015	.042	.056	.063	.069

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TABLE XIX.- CONTINUED.

(b) α_u, 4°, 6°, 8°, 10° - Concluded.

Semi-span sta.	Percent chord	UPPER SURFACE Angle of attack 4°	6°	8°	10°	LOWER SURFACE Angle of attack 4°	6°	8°	10°
0.707 b/2	0	-0.280	-1.232	-2.606	-4.390	- -	- -	- -	- -
	1.5	-.937	-1.762	-2.100	-2.959	0.361	0.430	0.392	0.260
	5.5	-.538	-.767	-1.061	-1.359	.185	.307	.375	.426
	6.5	-.503	-.745	-1.010	-1.256	.163	.279	.353	.409
	11.0	-.379	-.536	-.713	-.872	.090	.168	.267	.333
	14.5	-.362	-.489	-.653	-.769	.071	.161	.233	.302
	21.0	-.323	-.416	-.542	-.631	.023	.103	.167	.229
	24.5	-.314	-.408	-.512	-.588	.006	.081	.141	.201
	31.0	-.297	-.361	-.452	-.501	-.024	.040	.095	.153
	34.5	-.280	-.344	-.421	-.467	-.034	.028	.082	.133
	41.0	-.264	-.327	-.408	-.428	-.052	.001	.047	.095
	44.5	-.251	-.291	-.335	-.381	-.059	-.008	.037	.079
	51.0	-.219	-.250	-.281	-.317	-.070	-.027	.010	.050
	59.5	-.174	-.195	-.220	-.240	-.062	-.030	0	.031
	71.0	-.105	-.113	-.128	-.138	-.030	-.004	.017	.034
	79.5	-.045	-.047	-.055	-.062	.003	.020	.031	.042
	91.0	.025	.029	.028	.023	.047	.057	.059	.061
0.831 b/2	0	-0.065	-0.937	-2.215	-3.903	- -	- -	- -	- -
	1.5	-.932	-1.651	-2.104	-2.911	0.359	0.423	0.384	0.254
	5.5	-.538	-.784	-1.065	-1.333	.166	.285	.356	.407
	6.5	-.507	-.720	-.964	-1.239	.157	.273	.346	.400
	11.0	-.374	-.540	-.713	-.864	.084	.185	.255	.322
	14.5	-.374	-.502	-.662	-.786	- -	- -	- -	- -
	21.0	-.323	-.416	-.538	-.622	.012	.085	.147	.206
	24.5	-.319	-.378	-.499	-.575	-.004	.066	.122	.178
	31.0	-.280	-.339	-.426	-.471	-.034	.024	.075	.124
	34.5	-.276	-.327	-.396	-.441	-.046	.009	.049	.096
	41.0	-.271	-.305	-.370	-.398	-.062	-.017	.020	.060
	44.5	-.228	-.261	-.299	-.343	-.071	-.028	.004	.039
	51.0	-.203	-.228	-.257	-.288	-.074	-.038	-.010	.021
	59.5	-.146	-.162	-.185	-.210	-.069	-.045	-.026	-.005
	71.0	-.088	-.095	-.111	-.127	-.032	-.017	-.007	.005
	79.5	-.030	-.036	-.045	-.062	-.001	.010	.011	.013
	91.0	-.035	.037	.027	-.011	.044	.048	.046	.038
0.924 b/2	0	-0.495	-1.574	-3.014	-4.933	- -	- -	- -	- -
	1.5	-.958	-1.732	-2.404	-3.088	0.332	0.407	0.383	0.276
	5.5	-.538	-.754	-1.027	-1.277	.157	.271	.336	.384
	6.5	-.495	-.711	-.949	-1.183	.144	.254	.318	.367
	11.0	-.379	-.506	-.671	-.807	.057	.150	.215	.272
	14.5	-.340	-.455	-.585	-.695	.015	.101	.152	.207
	21.0	-.306	-.369	-.477	-.549	-.022	.037	.079	.125
	24.5	-.276	-.331	-.413	-.488	-.042	.009	.038	.076
	31.0	-.254	-.288	-.370	-.415	-.061	-.019	.010	.038
	34.5	-.237	-.280	-.340	-.389	-.072	-.039	-.018	.002
	41.0	-.237	-.254	-.327	-.372	-.085	-.055	-.037	-.017
	44.5	-.191	-.223	-.266	-.320	-.088	-.064	-.054	-.042
	51.0	-.167	-.195	-.231	-.278	-.090	-.068	-.057	-.046
	59.5	-.115	-.139	-.178	-.232	-.071	-.064	-.063	-.062
	71.0	-.059	-.081	-.117	-.167	-.033	-.033	-.036	-.041
	79.5	-.014	-.045	-.092	-.160	-.010	-.016	-.027	-.041
	91.0	.033	.003	-.039	-.101	.040	.029	.011	-.006

TABLE XIX.- CONTINUED.

(c) α_u, 12°, 16°, 20°, 24°.

Semi-span sta.	Percent chord	UPPER SURFACE Angle of attack 12°	16°	20°	24°	LOWER SURFACE Angle of attack 12°	16°	20°	24°
0.086 b/2	0	-1.269	-2.829	-4.807	-7.002	- -	- -	- -	- -
	1.5	-1.783	-2.730	-3.760	-4.739	0.517	0.447	0.252	0.048
	5.5	-.793	-1.027	-1.381	-1.795	.453	.543	.608	.661
	6.5	-.712	-.959	-1.359	-1.756	.419	.523	.607	.683
	11.0	-.570	-.713	-.932	-1.221	.353	.468	.558	.655
	14.5	-.502	-.682	-.885	-1.191	.315	.429	.536	.623
	21.0	-.467	-.579	-.723	-1.010	.268	.376	.483	.563
	24.5	-.424	-.557	-.723	-.976	.238	.349	.454	.532
	31.0	-.420	-.484	-.637	-.896	.206	.310	.407	.481
	34.5	-.390	-.501	-.663	-.859	.184	.287	.383	.453
	41.0	-.377	-.488	-.646	-.859	.156	.251	.338	.406
	44.5	-.390	-.489	-.674	-.863	- -	- -	- -	- -
	51.0	-.362	-.453	-.601	-.812	.115	.203	.277	.333
	59.5	-.295	-.374	-.509	-.714	.103	.179	.239	.288
	71.0	-.221	-.285	-.400	-.584	.098	.158	.207	.238
	79.5	-.133	-.187	-.292	-.449	.096	.145	.174	.190
	91.0	-.043	-.079	-.164	-.284	.094	.123	.129	.114
0.382 b/2	0	-2.778	-5.527	-8.686	-4.204	- -	- -	- -	- -
	1.5	-2.388	-3.778	-4.931	-2.915	0.200	-0.322	-1.039	-0.729
	5.5	-1.055	-1.506	-2.338	-2.721	.467	.522	.548	.609
	6.5	-.965	-1.359	-2.291	-2.493	.432	.514	.586	.643
	11.0	-.725	-1.053	-1.338	-2.355	.388	.479	.582	.650
	14.5	-.634	-.876	-1.193	-2.066	.322	.439	.549	.616
	21.0	-.544	-.713	-.962	-1.752	.268	.382	.489	.560
	24.5	-.502	-.674	-.881	-1.622	.239	.357	.454	.523
	31.0	-.454	-.583	-.783	-1.351	.199	.307	.402	.467
	34.5	-.459	-.586	-.788	-1.312	.175	.279	.368	.430
	41.0	-.416	-.532	-.689	-1.088	.147	.245	.327	.387
	44.5	-.399	-.512	-.662	-1.070	.133	.226	.304	.359
	51.0	-.352	-.453	-.604	-.909	.106	.194	.258	.311
	59.5	-.281	-.368	-.505	-.794	.089	.166	.218	.254
	71.0	-.196	-.266	-.399	-.656	.084	.142	.176	.193
	79.5	-.108	-.170	-.284	-.523	.091	.132	.148	.144
	91.0	-.004	-.046	-.139	-.344	.095	.113	.105	.067
0.382 b/2	0	-4.398	-6.347	-3.538	-2.049	- -	- -	- -	- -
	1.5	-3.091	-4.498	-2.222	-1.454	0.373	0.118	0.195	0.226
	5.5	-1.342	-2.101	-2.000	-1.407	.445	.490	.548	.565
	6.5	-1.230	-1.967	-1.915	-1.359	.429	.499	.561	.576
	11.0	-.913	-1.428	-1.918	-1.364	.371	.476	.543	.575
	14.5	-.789	-1.208	-1.872	-1.320	.334	.447	.514	.551
	21.0	-.652	-.855	-1.787	-1.325	.277	.391	.458	.501
	24.5	-.600	-.803	-1.654	-1.260	.248	.363	.426	.471
	31.0	-.510	-.704	-1.513	-1.260	.203	.310	.370	.420
	34.5	-.497	-.648	-1.402	-1.213	.184	.283	.340	.388
	41.0	-.443	-.575	-1.223	-1.195	.152	.245	.295	.338
	49.5	-.408	-.538	-1.167	-1.144	.133	.221	.266	.306
	51.0	-.348	-.465	-.992	-1.106	.096	.181	.223	.255
	59.5	-.273	-.365	-.823	-1.025	.091	.148	.176	.144
	71.0	-.169	-.252	-.575	-.918	.081	.123	.129	.121
	79.5	-.081	-.161	-.466	-.872	.087	.110	.098	.058
	91.0	.008	-.065	-.274	-.692	.091	.084	.038	-.070
0.555 b/2	0	-5.260	-3.937	-1.697	-1.471	- -	- -	- -	- -
	1.5	-3.498	-3.105	-1.257	-1.118	0.297	0.191	0.283	0.227
	5.5	-1.513	-2.355	-1.218	-1.062	.446	.513	.526	.525
	6.5	-1.398	-2.260	-1.210	-1.049	.441	.517	.526	.531
	11.0	-1.016	-1.950	-1.171	-1.032	.389	.487	.511	.537
	14.5	-.887	-1.764	-1.150	-1.014	.352	.449	.480	.514
	21.0	-.716	-1.700	-1.103	-.989	.283	.382	.421	.459
	24.5	-.669	-1.536	-1.103	-.967	.260	.354	.389	.478
	31.0	-.553	-1.178	-1.095	-.967	.209	.297	.332	.374
	34.5	-.536	-1.096	-1.060	-.950	.189	.268	.301	.341
	41.0	-.459	-.773	-1.052	-.945	.151	.227	.253	.286
	44.5	-.418	-.745	-1.020	-.914	.136	.201	.226	.256
	51.0	-.352	-.529	-.994	-.911	.105	.163	.179	.200
	59.5	-.259	-.420	-.904	-.866	.079	.117	.116	.124
	71.0	-.157	-.270	-.822	-.827	.077	.094	.065	.042
	79.5	-.072	-.154	-.734	-.778	.078	.079	.010	-.034
	91.0	.016	-.081	-.627	-.733	.082	.051	-.104	-.194

NACA

TABLE XIX.- CONCLUDED.

(c) α_u, 12°, 16°, 20°, 24° - Concluded.

Semi-span eta.	Percent chord	UPPER SURFACE Angle of attack 12°	16°	20°	24°	LOWER SURFACE Angle of attack 12°	16°	20°	24°
0.707 b/2	0	-6.499	-1.717	-1.206	-1.105	- -	- -	- -	- -
	1.5	-3.811	-1.674	-.979	-.889	0.058	0.173	0.188	0.118
	5.5	-1.642	-1.351	-.924	-.859	.449	.501	.498	.495
	6.5	-1.530	-1.264	-.877	-.829	.444	.501	.499	.506
	11.0	-1.059	-1.256	-.885	-.833	.388	.454	.470	.499
	14.5	-.939	-1.187	-.825	-.799	.358	.424	.442	.472
	21.0	-.755	-1.148	-.842	-.795	.289	.352	.378	.417
	24.5	-.682	-1.114	-.804	-.773	.261	.322	.346	.387
	31.0	-.583	-1.070	-.804	-.795	.206	.264	.286	.324
	34.5	-.544	-1.032	-.787	-.756	.184	.236	.255	.294
	41.0	-.480	-.984	-.804	-.773	.142	.188	.199	.231
	44.5	-.408	-.935	-.762	-.718	.123	.162	.180	.200
	51.0	-.335	-.880	-.768	-.724	.091	.123	.119	.142
	59.5	-.250	-.784	-.725	-.701	.060	.077	.050	.067
	71.0	-.138	-.663	-.700	-.683	.057	.047	-.009	-.008
	79.5	-.063	-.566	-.655	-.645	.058	.014	-.068	-.072
	91.0	.021	-.403	-.609	-.598	.067	-.034	-.183	-.189
0.831 b/2	0	-5.822	-1.527	-1.060	-0.881	- -	- -	- -	- -
	1.5	-3.674	-.989	-.761	-.726	0.058	0.256	0.246	0.188
	5.5	-1.612	-.907	-.710	-.687	.432	.462	.463	.472
	6.5	-1.470	-.898	-.697	-.676	.431	.461	.461	.472
	11.0	-1.059	-.833	-.672	-.652	.368	.406	.422	.452
	14.5	-.956	-.842	-.676	-.644	- -	- -	- -	- -
	21.0	-.716	-.807	-.650	-.635	.259	.294	.318	.356
	24.5	-.656	-.807	-.633	-.622	.228	.264	.283	.323
	31.0	-.544	-.777	-.633	-.609	.170	.201	.220	.257
	34.5	-.502	-.760	-.607	-.601	.140	.170	.182	.219
	41.0	-.433	-.747	-.612	-.605	.101	.126	.132	.164
	44.5	-.371	-.693	-.580	-.562	.077	.095	.098	.131
	51.0	-.306	-.685	-.585	-.572	.050	.060	.055	.083
	59.5	-.223	-.644	-.560	-.551	.018	.008	-.008	.012
	71.0	-.138	-.603	-.562	-.543	.020	-.025	-.057	-.044
	79.5	-.077	-.551	-.525	-.504	.021	-.062	-.099	-.089
	91.0	-.006	-.513	-.496	-.476	.034	-.146	-.186	-.176
0.924 b/2	0	-7.104	-0.898	-0.687	-0.648	- -	- -	- -	- -
	1.5	-3.995	-.764	-.612	-.588	0.105	0.304	0.270	0.219
	5.5	-1.509	-.764	-.582	-.579	.403	.408	.415	.417
	6.5	-1.393	-.747	-.573	-.545	.386	.388	.391	.397
	11.0	-.977	-.717	-.562	-.557	.316	.324	.342	.369
	14.5	-.845	-.682	-.535	-.562	.247	.260	.284	.313
	21.0	-.656	-.682	-.539	-.545	.161	.189	.213	.247
	24.5	-.557	-.631	-.505	-.501	.105	.135	.161	.191
	31.0	-.493	-.631	-.505	-.514	.067	.097	.118	.146
	34.5	-.459	-.583	-.462	-.480	.021	.052	.074	.097
	41.0	-.377	-.596	-.479	-.493	.002	.030	.039	.067
	44.5	-.372	-.504	-.426	-.446	-.026	.003	.009	.031
	51.0	-.317	-.504	-.433	-.451	-.032	.032	-.017	.005
	59.5	-.292	-.447	-.396	-.423	-.055	-.052	-.055	-.046
	71.0	-.225	-.447	-.411	-.424	-.036	-.066	-.083	-.073
	79.5	-.259	-.394	-.378	-.392	-.042	-.090	-.107	-.104
	91.0	-.162	-.402	-.375	-.377	-.017	-.146	-.158	-.155

NACA

TABLE XX.- PRESSURE COEFFICIENTS AT SEVEN SEMISPAN STATIONS OF THE WING. M_0, 0.60; R, 8,000,000.

(a) α_u, 0°, 1°, 2°, 3°.

Semi-span sta.	Percent chord	UPPER SURFACE				LOWER SURFACE			
		Angle of attack				Angle of attack			
		0°	1°	2°	3°	0°	1°	2°	3°
0.086 b/2	0	0.502	0.493	0.470	0.436	- -	- -	- -	- -
	1.5	.064	-.043	-.148	-.262	0.036	0.114	0.183	0.245
	5.5	-.010	-.064	-.121	-.169	-.007	.040	.086	.129
	6.5	-.027	-.080	-.132	-.180	-.034	.008	.051	.093
	11.0	-.043	-.091	-.132	-.167	-.042	-.008	.026	.059
	14.5	-.061	-.109	-.146	-.182	-.064	-.031	.001	.032
	21.0	-.081	-.118	-.155	-.191	-.075	-.047	-.019	.009
	24.5	-.095	-.133	-.162	-.196	-.098	-.070	-.040	-.012
	31.0	-.103	-.138	-.179	-.196	-.114	-.086	-.056	-.028
	34.5	-.132	-.163	-.191	-.218	-.137	-.109	-.079	-.049
	41.0	-.151	-.187	-.216	-.237	-.155	-.129	-.100	-.068
	44.5	-.180	-.211	-.234	-.258	- -	- -	- -	- -
	51.0	-.183	-.212	-.233	-.255	-.172	-.153	-.129	-.101
	59.5	-.158	-.181	-.199	-.216	-.153	-.137	-.118	-.097
	71.0	-.126	-.145	-.157	-.170	-.130	-.116	-.102	-.086
	79.5	-.077	-.090	-.099	-.107	-.088	-.078	-.067	-.054
	91.0	-.024	-.033	-.037	-.041	-.029	-.025	-.017	-.009
0.195 b/2	0	0.444	0.424	0.371	0.285	- -	- -	- -	- -
	1.5	-.005	-.133	-.274	-.425	0.040	0.155	0.247	0.321
	5.5	-.061	-.136	-.207	-.271	-.067	-.003	.057	.113
	6.5	-.088	-.149	-.220	-.282	-.081	-.027	.028	.080
	11.0	-.101	-.149	-.198	-.244	-.099	-.054	-.001	.040
	14.5	-.112	-.158	-.198	-.243	-.112	-.067	-.027	.011
	21.0	-.128	-.171	-.207	-.243	-.125	-.088	-.055	-.020
	24.5	-.139	-.180	-.213	-.244	-.137	-.104	-.072	-.037
	31.0	-.146	-.183	-.213	-.241	-.157	-.128	-.098	-.066
	34.5	-.173	-.205	-.231	-.260	-.172	-.145	-.116	-.085
	41.0	-.184	-.217	-.243	-.264	-.177	-.153	-.127	-.138
	44.5	-.188	-.220	-.244	-.267	-.178	-.156	-.131	-.105
	51.0	-.176	-.204	-.225	-.245	-.185	-.166	-.142	-.119
	59.5	-.152	-.174	-.191	-.207	-.158	-.142	-.124	-.104
	71.0	-.116	-.133	-.144	-.154	-.114	-.103	-.090	-.074
	79.5	-.060	-.072	-.080	-.085	-.059	-.053	-.043	-.032
	91.0	.005	-.002	-.004	-.006	.005	.007	.012	.018
0.382 b/2	0	0.408	0.390	0.308	0.176	- -	- -	- -	- -
	1.5	-.039	-.205	-.382	-.576	-0.071	0.044	0.141	0.222
	5.5	-.117	-.205	-.286	-.371	-.117	-.043	.025	.089
	6.5	-.128	-.208	-.290	-.360	-.123	-.058	.006	.066
	11.0	-.142	-.198	-.252	-.318	-.139	-.086	-.030	.026
	14.5	-.137	-.194	-.245	-.303	-.145	-.094	-.047	-.002
	21.0	-.162	-.208	-.249	-.287	-.155	-.111	-.074	-.035
	24.5	-.157	-.207	-.240	-.282	-.162	-.125	-.088	-.051
	31.0	-.175	-.210	-.249	-.276	-.178	-.146	-.113	-.079
	34.5	-.168	-.205	-.236	-.268	-.183	-.155	-.123	-.092
	41.0	-.200	-.223	-.252	-.275	-.177	-.153	-.126	-.097
	44.5	-.187	-.220	-.245	-.268	-.180	-.158	-.132	-.105
	51.0	-.172	-.200	-.220	-.240	-.181	-.162	-.139	-.117
	59.5	-.150	-.172	-.189	-.203	-.145	-.131	-.112	-.094
	71.0	-.095	-.111	-.122	-.131	-.093	-.083	-.071	-.058
	79.5	-.042	-.054	-.060	-.066	-.037	-.031	-.023	-.014
	91.0	.024	.016	.013	.013	-.001	.028	.031	.035
0.555 b/2	0	0.427	0.413	0.337	0.188	- -	- -	- -	- -
	1.5	-.056	-.241	-.446	-.675	-0.072	0.053	0.161	0.249
	5.5	-.117	-.225	-.313	-.412	-.120	-.037	.039	.107
	6.5	-.151	-.241	-.333	-.418	-.125	-.052	.020	.088
	11.0	-.137	-.208	-.270	-.341	-.144	-.090	-.023	.032
	14.5	-.155	-.212	-.267	-.332	-.147	-.099	-.037	.010
	21.0	-.162	-.210	-.252	-.303	-.161	-.113	-.074	-.032
	24.5	-.173	-.205	-.243	-.289	-.163	-.122	-.084	-.045
	31.0	-.164	-.208	-.242	-.276	-.174	-.142	-.107	-.072
	34.5	-.173	-.214	-.250	-.280	-.180	-.148	-.115	-.083
	41.0	-.186	-.225	-.252	-.273	-.176	-.149	-.121	-.092
	44.5	-.181	-.214	-.240	-.264	-.174	-.151	-.123	-.097
	51.0	-.166	-.193	-.216	-.235	-.169	-.150	-.127	-.103
	59.5	-.127	-.150	-.167	-.181	-.145	-.132	-.113	-.095
	71.0	-.086	-.102	-.111	-.119	-.081	-.074	-.062	-.051
	79.5	-.033	-.044	-.051	-.055	-.029	-.026	-.018	-.010
	91.0	.032	.024	.023	.024	.036	.035	.038	.040

TABLE XX.- CONTINUED.

(a) α_u, 0°, 1°, 2°, 3° - Concluded.

Semi-span sta.	Percent chord	UPPER SURFACE Angle of attack 0°	1°	2°	3°	LOWER SURFACE Angle of attack 0°	1°	2°	3°
0.707 b/2	0	0.399	0.379	0.267	0.074	- -	- -	- -	- -
	1.5	-.046	-.257	-.452	-.736	-0.072	0.085	0.206	0.298
	5.5	-.141	-.250	-.360	-.460	-.130	-.036	.048	.122
	6.5	-.137	-.246	-.347	-.435	-.139	-.052	.027	.097
	11.0	-.142	-.216	-.276	-.350	-.159	-.091	-.022	.032
	14.5	-.151	-.223	-.263	-.337	-.161	-.099	-.036	.016
	21.0	-.173	-.221	-.270	-.318	-.167	-.113	-.070	-.027
	24.5	-.168	-.219	-.258	-.300	-.173	-.123	-.083	-.042
	31.0	-.177	-.219	-.250	-.287	-.178	-.138	-.102	-.068
	34.5	-.171	-.217	-.247	-.276	-.172	-.141	-.108	-.075
	41.0	-.198	-.228	-.254	-.282	-.169	-.146	-.119	-.092
	44.5	-.178	-.210	-.236	-.258	-.169	-.148	-.123	-.098
	51.0	-.162	-.189	-.209	-.226	-.166	-.149	-.128	-.107
	59.5	-.135	-.155	-.170	-.180	-.137	-.127	-.131	-.095
	71.0	-.077	-.092	-.098	-.104	-.071	-.067	-.057	-.048
	79.5	-.026	-.037	-.039	-.041	-.021	-.020	-.015	-.009
	91.0	.041	.033	.034	.035	.046	.044	.044	.046
0.831 b/2	0	0.386	0.440	0.367	0.229	- -	- -	- -	- -
	1.5	-.068	-.270	-.495	-.745	-0.076	0.082	0.205	0.295
	5.5	-.146	-.255	-.364	-.466	-.143	-.051	.031	.104
	6.5	-.150	-.248	-.355	-.444	-.138	-.056	.028	.096
	11.0	-.146	-.219	-.277	-.353	-.155	-.089	-.029	.027
	14.5	-.169	-.223	-.285	-.346	- -	- -	- -	- -
	21.0	-.171	-.221	-.263	-.309	-.163	-.121	-.076	-.036
	24.5	-.182	-.221	-.263	-.301	-.162	-.123	-.084	-.047
	31.0	-.173	-.208	-.240	-.271	-.170	-.139	-.108	-.077
	34.5	-.186	-.216	-.243	-.268	-.170	-.144	-.116	-.089
	41.0	-.188	-.219	-.238	-.257	-.169	-.148	-.126	-.103
	44.5	-.171	-.197	-.217	-.234	-.165	-.148	-.129	-.110
	51.0	-.158	-.180	-.194	-.204	-.152	-.140	-.125	-.109
	59.5	-.114	-.130	-.139	-.146	-.121	-.116	-.107	-.096
	71.0	-.067	-.078	-.080	-.084	-.057	-.056	-.052	-.047
	79.5	-.013	-.021	-.021	-.021	-.004	-.006	-.006	-.004
	91.0	.050	.046	.047	.047	.059	.054	.053	.051
0.924 b/2	0	0.404	0.278	0.155	-0.101	- -	- -	- -	- -
	1.5	-.018	-.226	-.466	-.739	-0.094	0.062	0.179	0.271
	5.5	-.168	-.271	-.374	-.475	-.150	-.057	.023	.097
	6.5	-.164	-.261	-.360	-.453	-.153	-.064	.014	.085
	11.0	-.164	-.241	-.290	-.351	-.165	-.103	-.047	.007
	14.5	-.173	-.235	-.270	-.323	-.172	-.123	-.075	-.027
	21.0	-.184	-.219	-.250	-.284	-.174	-.141	-.099	-.068
	24.5	-.173	-.205	-.229	-.255	-.171	-.138	-.111	-.086
	31.0	-.177	-.199	-.216	-.239	-.168	-.143	-.120	-.100
	34.5	-.153	-.180	-.200	-.219	-.154	-.137	-.123	-.107
	41.0	-.177	-.190	-.213	-.223	-.150	-.140	-.128	-.116
	44.5	-.150	-.167	-.181	-.194	-.142	-.136	-.123	-.117
	51.0	-.133	-.149	-.158	-.168	-.138	-.133	-.122	-.117
	59.5	-.087	-.098	-.103	-.110	-.086	-.086	-.084	-.082
	71.0	-.039	-.045	-.046	-.051	-.029	-.034	-.034	-.037
	79.5	.008	.005	.004	-.001	.016	.008	.002	.003
	91.0	.059	.056	.055	.049	.072	.063	.057	.050

NACA

TABLE XX.- CONTINUED.

(b) α_u, 4°, 6°, 8°, 10°.

Semi-span sta.	Percent chord	UPPER SURFACE Angle of attack 4°	6°	8°	10°	LOWER SURFACE Angle of attack 4°	6°	8°	10°
0.086 b/2	0	0.383	0.224	-0.040	-0.356	- -	- -	- -	- -
	1.5	-.393	-.670	-1.058	-1.631	0.302	0.398	0.473	0.531
	5.5	-.226	-.341	-.486	-.614	.172	.255	.329	.400
	6.5	-.231	-.337	-.461	-.593	.134	.214	.288	.361
	11.0	-.212	-.293	-.389	-.491	.093	.162	.228	.296
	14.5	-.222	-.299	-.384	-.479	.064	.131	.195	.261
	21.0	-.228	-.288	-.359	-.438	.037	.096	.154	.216
	24.5	-.233	-.290	-.359	-.433	.016	.073	.129	.189
	31.0	-.257	-.293	-.343	-.410	-.003	.049	.100	.156
	34.5	-.249	-.299	-.357	-.421	-.022	.028	.077	.132
	41.0	-.263	-.309	-.362	-.421	-.041	.006	.051	.101
	44.5	-.281	-.298	-.381	-.434	- -	- -	- -	- -
	51.0	-.276	-.315	-.363	-.413	-.070	-.024	.014	.059
	59.5	-.232	-.262	-.302	-.342	-.074	-.023	.011	.049
	71.0	-.182	-.203	-.232	-.263	-.070	-.021	.014	.047
	79.5	-.114	-.127	-.149	-.170	-.041	-.008	.026	.054
	91.0	-.043	-.048	-.061	-.074	0	.020	.041	.059
0.195 b/2	0	0.160	-0.168	-0.444	-1.020	- -	- -	- -	- -
	1.5	-.598	-1.019	-1.763	-2.135	0.379	0.453	0.466	0.446
	5.5	-.344	-.507	-.691	-1.001	.165	.264	.347	.419
	6.5	-.342	-.492	-.659	-.825	.131	.223	.303	.376
	11.0	-.304	-.407	-.528	-.683	.085	.162	.234	.306
	14.5	-.290	-.384	-.491	-.609	.049	.124	.193	.262
	21.0	-.285	-.353	-.442	-.532	.014	.081	.143	.206
	24.5	-.281	-.348	-.430	-.509	-.004	.060	.119	.179
	31.0	-.272	-.332	-.398	-.468	-.035	.025	.079	.136
	34.5	-.292	-.345	-.408	-.474	-.054	.004	.057	.110
	41.0	-.295	-.336	-.394	-.454	-.070	-.015	.033	.083
	44.5	-.289	-.334	-.389	-.443	-.077	-.024	.022	.070
	51.0	-.264	-.301	-.348	-.397	-.094	-.043	0	.044
	59.5	-.221	-.248	-.285	-.321	-.084	-.040	-.002	.035
	71.0	-.164	-.181	-.207	-.234	-.060	-.024	.006	.036
	79.5	-.091	-.101	-.120	-.142	-.021	.005	.027	.049
	91.0	-.007	-.008	-.019	-.038	.025	.039	.050	.061
0.382 b/2	0	-0.018	-0.523	-1.038	-1.173	- -	- -	- -	- -
	1.5	-.805	-1.471	-2.037	-1.356	0.291	0.394	0.446	0.465
	5.5	-.475	-.681	-1.019	-1.098	.147	.251	.331	.386
	6.5	-.461	-.644	-.860	-1.001	.123	.225	.305	.364
	11.0	-.384	-.511	-.705	-.940	.072	.160	.235	.297
	14.5	-.361	-.476	-.613	-.802	.042	.126	.198	.261
	21.0	-.338	-.422	-.539	-.748	.004	.079	.144	.204
	24.5	-.324	-.403	-.502	-.667	-.013	.058	.121	.178
	31.0	-.315	-.380	-.461	-.607	-.046	.020	.077	.132
	34.5	-.303	-.357	-.430	-.549	-.060	.004	.059	.111
	41.0	-.306	-.348	-.414	-.497	-.069	-.013	.037	.085
	44.5	-.291	-.336	-.390	-.460	-.078	-.024	.022	.068
	51.0	-.259	-.294	-.341	-.401	-.092	-.043	-.001	.040
	59.5	-.217	-.244	-.273	-.320	-.074	-.035	-.001	.032
	71.0	-.137	-.152	-.176	-.215	-.044	-.014	.009	.033
	79.5	-.069	-.076	-.095	-.136	-.004	.018	.031	.047
	91.0	.014	.015	.002	-.034	.041	.053	.053	.059
0.555 b/2	0	-0.044	-0.612	-1.052	-1.293	- -	- -	- -	- -
	1.5	-.940	-1.882	-2.035	-1.968	0.321	0.422	0.456	0.458
	5.5	-.532	-.770	-1.162	-1.182	.169	.278	.350	.398
	6.5	-.525	-.738	-.950	-1.112	.148	.257	.331	.383
	11.0	-.422	-.568	-.857	-1.001	.088	.181	.254	.313
	14.5	-.397	-.523	-.731	-.846	.058	.146	.216	.275
	21.0	-.354	-.451	-.595	-.725	.009	.088	.151	.208
	24.5	-.336	-.422	-.551	-.667	-.006	.068	.129	.185
	31.0	-.317	-.384	-.475	-.576	-.039	.029	.084	.136
	34.5	-.315	-.378	-.456	-.553	-.050	.013	.066	.114
	41.0	-.306	-.353	-.414	-.486	-.064	-.007	.039	.083
	44.5	-.288	-.333	-.389	-.457	-.070	-.017	.026	.068
	51.0	-.254	-.289	-.334	-.391	-.080	-.033	.005	.041
	59.5	-.195	-.218	-.249	-.296	-.077	-.038	-.011	.017
	71.0	-.125	-.137	-.156	-.196	-.037	-.010	.006	.023
	79.5	-.057	-.063	-.079	-.123	-.003	.017	.024	.029
	91.0	.024	.025	.005	-.042	.044	.052	.047	.036

NACA

TABLE XX.- CONTINUED.

(b) α_u, 4°, 6°, 8°, 10° - Concluded.

Semi-span sta.	Percent chord	UPPER SURFACE Angle of attack 4°	6°	8°	10°	LOWER SURFACE Angle of attack 4°	6°	8°	10°
0.707 b/2	0	-0.203	-0.881	-1.097	-1.344	- -	- -	- -	- -
	1.5	-1.038	-2.090	-1.550	-1.323	0.365	0.434	0.430	0.409
	5.5	-.589	-.849	-1.040	-1.054	.188	.300	.360	.405
	6.5	-.564	-.794	-.936	-.948	.160	.273	.336	.385
	11.0	-.431	-.592	-.872	-.978	.091	.185	.251	.307
	14.5	-.408	-.541	-.742	-.885	.065	.154	.218	.273
	21.0	-.372	-.469	-.668	-.860	.016	.094	.151	.206
	24.5	-.347	-.433	-.599	-.722	-.003	.071	.128	.179
	31.0	-.324	-.396	-.532	-.642	-.034	.032	.082	.129
	34.5	-.317	-.371	-.490	-.553	-.045	.017	.065	.109
	41.0	-.310	-.352	-.431	-.488	-.065	-.010	.029	.069
	44.5	-.282	-.322	-.396	-.438	-.072	-.022	.014	.051
	51.0	-.244	-.273	-.330	-.366	-.085	-.041	-.011	.021
	59.5	-.193	-.209	-.251	-.278	-.080	-.047	-.025	-.004
	71.0	-.108	-.115	-.153	-.174	-.037	-.017	-.007	.002
	79.5	-.044	-.046	-.085	-.115	-.003	.008	.009	.006
	91.0	.036	.037	-.007	-.042	.048	.049	.039	.018
0.831 b/2	0	-0.018	-0.619	-0.860	-1.251	- -	- -	- -	- -
	1.5	-1.048	-2.069	-1.303	-1.265	0.361	0.425	0.417	0.393
	5.5	-.591	-.835	-1.031	-1.154	.169	.280	.336	.382
	6.5	-.568	-.787	-.917	-.984	.160	.268	.325	.372
	11.0	-.431	-.589	-.857	-1.003	.087	.175	.235	.287
	14.5	-.413	-.546	-.745	-.860	- -	- -	- -	- -
	21.0	-.361	-.451	-.678	-.882	.005	.078	.131	.179
	24.5	-.342	-.419	-.585	-.727	-.011	.057	.105	.152
	31.0	-.306	-.362	-.495	-.614	-.046	.012	.054	.096
	34.5	-.299	-.343	-.452	-.519	-.061	-.009	.029	.068
	41.0	-.281	-.313	-.373	-.423	-.080	-.035	-.003	.029
	44.5	-.251	-.280	-.338	-.370	-.089	-.050	-.018	.007
	51.0	-.220	-.239	-.276	-.301	-.092	-.060	-.038	-.014
	59.5	-.154	-.166	-.213	-.237	-.085	-.065	-.053	-.040
	71.0	-.087	-.092	-.129	-.167	-.041	-.032	-.030	-.029
	79.5	-.024	-.029	-.077	-.128	-.003	-.002	-.009	-.017
	91.0	.048	.041	-.013	-.074	.050	.043	.020	-.006
0.924 b/2	0	-0.450	-1.299	-1.437	-1.613	- -	- -	- -	- -
	1.5	-1.066	-2.087	-1.642	-1.720	0.337	0.401	0.395	0.374
	5.5	-.598	-.830	-1.035	-1.251	.160	.264	.313	.355
	6.5	-.561	-.766	-.846	-1.026	.147	.250	.297	.339
	11.0	-.424	-.550	-.853	-1.107	.056	.146	.196	.244
	14.5	-.377	-.476	-.698	-.860	.022	.089	.135	.181
	21.0	-.324	-.391	-.564	-.778	-.039	.018	.060	.098
	24.5	-.288	-.339	-.479	-.625	-.062	-.017	.012	.048
	31.0	-.265	-.307	-.389	-.497	-.081	-.044	-.019	.012
	34.5	-.244	-.281	-.354	-.458	-.092	-.065	-.047	-.022
	41.0	-.240	-.274	-.322	-.377	-.103	-.079	-.064	-.042
	44.5	-.209	-.240	-.293	-.376	-.107	-.091	-.079	-.060
	51.0	-.181	-.203	-.255	-.309	-.110	-.094	-.084	-.068
	59.5	-.119	-.144	-.216	-.312	-.081	-.079	-.076	-.068
	71.0	-.058	-.079	-.161	-.243	-.039	-.043	-.046	-.048
	79.5	-.011	-.045	-.160	-.244	-.009	-.021	-.030	-.039
	91.0	.038	.005	-.092	-.170	.044	.024	-.001	-.029

TABLE XX.- CONTINUED.

(c) α_n, 12°, 14°, 16°, 20°.

Semi-span sta.	Percent chord	UPPER SURFACE Angle of attack 12°	14°	16°	20°	LOWER SURFACE Angle of attack 12°	14°	16°	20°
0.086 b/2	0	-0.700	-0.993			- -	- -		
	1.5	-2.226	-2.153			0.563	0.582		
	5.5	-.772	-.975			.465	.522		
	6.5	-.744	-.972			.427	.486		
	11.0	-.601	-.700			.360	.418		
	14.5	-.580	-.697			.322	.379		
	21.0	-.533	-.636			.272	.327		
	24.5	-.526	-.639			.243	.298		
	31.0	-.487	-.577			.207	.258		
	34.5	-.494	-.570			.182	.232		
	41.0	-.485	-.554			.149	.196		
	44.5	-.499	-.562			- -	- -		
	51.0	-.474	-.534			.100	.143		
	59.5	-.396	-.443			.086	.124		
	71.0	-.303	-.338			.078	.108		
	79.5	-.202	-.230			.077	.100		
	91.0	-.096	-.117			.070	.081		
0.195 b/2	0	-1.278	-1.553			- -	- -		
	1.5	-2.048	-2.124			0.401	0.340		
	5.5	-1.297	-1.448			.471	.516		
	6.5	-1.102	-1.313			.433	.483		
	11.0	-.971	-1.287			.367	.422		
	14.5	-.810	-.975			.321	.377		
	21.0	-.655	-.845			.263	.318		
	24.5	-.622	-.752			.234	.289		
	31.0	-.555	-.650			.186	.240		
	34.5	-.568	-.664			.161	.211		
	41.0	-.534	-.605			.130	.177		
	44.5	-.531	-.600			.114	.160		
	51.0	-.466	-.516			.085	.126		
	59.5	-.374	-.411			.070	.105		
	71.0	-.267	-.296			.062	.088		
	79.5	-.169	-.194			.066	.084		
	91.0	-.049	-.072			.066	.073		
0.382 b/2	0	-1.400	-1.574			- -	- -		
	1.5	-1.193	-1.243			0.469	0.459		
	5.5	-1.126	-1.325			.435	.476		
	6.5	-1.027	-1.243			.414	.459		
	11.0	-1.053	-1.309			.352	.403		
	14.5	-.966	-1.198			.315	.368		
	21.0	-.960	-1.203			.258	.310		
	24.5	-.810	-1.019			.230	.281		
	31.0	-.761	-.958			.181	.231		
	34.5	-.656	-.831			.156	.206		
	41.0	-.599	-.751			.128	.171		
	44.5	-.547	-.674			.108	.150		
	51.0	-.482	-.575			.077	.115		
	59.5	-.379	-.444			.060	.090		
	71.0	-.255	-.288			.051	.071		
	79.5	-.172	-.199			.056	.068		
	91.0	-.063	-.082			.055	.053		
0.555 b/2	0	-1.547	-1.838			- -	- -		
	1.5	-1.678	-1.694			0.448	0.426		
	5.5	-1.210	-1.488			.440	.476		
	6.5	-1.093	-1.374			.426	.466		
	11.0	-1.091	-1.434			.364	.412		
	14.5	-.985	-1.327			.326	.376		
	21.0	-.967	-1.361			.258	.308		
	24.5	-.835	-1.240			.233	.279		
	31.0	-.767	-1.153			.181	.226		
	34.5	-.667	-1.053			.158	.201		
	41.0	-.590	-.876			.123	.160		
	44.5	-.528	-.811			.104	.139		
	51.0	-.461	-.633			.073	.103		
	59.5	-.350	-.493			.041	.063		
	71.0	-.242	-.323			.033	.046		
	79.5	-.174	-.246			.029	.032		
	91.0	-.099	-.138			.016	.006		

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TABLE XX.- CONCLUDED.

(c) α_u, 12°, 14°, 16°, 20° - Concluded.

Semi-span sta.	Percent chord	UPPER SURFACE Angle of attack 12°	14°	16°	20°	LOWER SURFACE Angle of attack 12°	14°	16°	20°
0.707 b/2	0	-1.526	-1.382			- -	- -		
	1.5	-1.128	-1.201			0.371	0.356		
	5.5	-1.247	-1.189			.443	.474		
	6.5	-1.079	-1.130			.425	.462		
	11.0	-1.177	-1.128			.356	.397		
	14.5	-1.056	-1.055			.322	.362		
	21.0	-1.112	-1.071			.252	.292		
	24.5	-.946	-1.076			.223	.261		
	31.0	-.843	-.998			.170	.206		
	34.5	-.714	-.937			.148	.179		
	41.0	-.616	-.909			.103	.130		
	44.5	-.544	-.854			.083	.107		
	51.0	-.446	-.802			.046	.065		
	59.5	-.355	-.708			.010	.020		
	71.0	-.250	-.591			.002	0		
	79.5	-.200	-.504			-.007	-.026		
	91.0	-.127	-.372			-.017	-.066		
0.831 b/2	0	-1.427	-1.048			- -	- -		
	1.5	-1.163	-.822			0.367	0.362		
	5.5	-1.275	-.796			.417	.437		
	6.5	-1.121	-.772			.410	.429		
	11.0	-1.198	-.751			.334	.359		
	14.5	-1.053	-.714			- -	- -		
	21.0	-1.037	-.690			.221	.247		
	24.5	-.908	-.664			.192	.215		
	31.0	-.779	-.639			.131	.153		
	34.5	-.709	-.615			.099	.118		
	41.0	-.587	-.606			.056	.071		
	44.5	-.546	-.568			.029	.042		
	51.0	-.454	-.567			.002	.008		
	59.5	-.393	-.517			-.036	-.041		
	71.0	-.302	-.494			-.040	-.064		
	79.5	-.268	-.453			-.043	-.087		
	91.0	-.207	-.419			-.060	-.148		
0.924 b/2	0	-1.098	-0.681			- -	- -		
	1.5	-.997	-.598			0.381	0.380		
	5.5	-1.004	-.601			.387	.393		
	6.5	-.906	-.566			.370	.375		
	11.0	-.945	-.577			.280	.294		
	14.5	-.819	-.530			.215	.230		
	21.0	-.775	-.526			.130	.148		
	24.5	-.676	-.477			.078	.094		
	31.0	-.630	-.472			.037	.052		
	34.5	-.569	-.427			-.001	.009		
	41.0	-.534	-.424			-.026	-.018		
	44.5	-.493	-.379			-.047	-.044		
	51.0	-.464	-.376			-.062	-.064		
	59.5	-.406	-.327			-.070	-.085		
	71.0	-.361	-.336			-.064	-.094		
	79.5	-.311	-.300			-.068	-.107		
	91.0	-.274	-.310			-.085	-.143		

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TABLE XXI.- PRESSURE COEFFICIENTS AT SEVEN SEMISPAN STATIONS OF THE WING. M_0, 0.25; R, 12,000,000.

(a) α_u, 0°, 1°, 2°, 3°.

Semi-span sta.	Percent chord	UPPER SURFACE				LOWER SURFACE			
		Angle of attack				Angle of attack			
		0°	1°	2°	3°	0°	1°	2°	3°
0.086 b/2	0	0.465	0.477	0.461	0.415	- -	- -	- -	- -
	1.5	.039	-.061	-.167	-.285	0.013	0.088	0.160	0.229
	5.5	-.006	-.061	-.103	-.179	-.012	.034	.077	.123
	6.5	-.036	-.089	-.131	-.179	-.040	0	.040	.086
	11.0	-.039	-.080	-.112	-.165	-.048	-.015	.016	.051
	14.5	-.070	-.111	-.140	-.174	-.067	-.037	-.008	.025
	21.0	-.076	-.117	-.131	-.174	-.076	-.051	-.027	.004
	24.5	-.098	-.125	-.145	-.174	-.099	-.073	-.045	-.016
	31.0	-.104	-.131	-.154	-.179	-.110	-.084	-.058	-.030
	34.5	-.123	-.147	-.167	-.193	-.127	-.102	-.077	-.047
	41.0	-.146	-.172	-.176	-.210	-.140	-.119	-.094	-.069
	44.5	-.158	-.181	-.204	-.223	- -	- -	- -	- -
	51.0	-.158	-.179	-.199	-.218	-.152	-.133	-.114	-.089
	59.5	-.134	-.155	-.168	-.182	-.130	-.118	-.102	-.081
	71.0	-.105	-.120	-.132	-.141	-.109	-.099	-.053	-.069
	79.5	-.073	-.071	-.111	-.086	-.073	-.073	-.087	-.041
	91.0	-.013	-.022	-.027	-.027	-.018	-.014	-.008	0
0.195 b/2	0	0.420	0.410	0.361	0.253	- -	- -	- -	- -
	1.5	-.008	-.142	-.268	-.419	0.026	0.137	0.229	0.316
	5.5	-.070	-.142	-.195	-.263	-.070	-.010	.046	.113
	6.5	-.081	-.142	-.195	-.268	-.084	-.026	.027	.080
	11.0	-.101	-.145	-.187	-.241	-.093	-.047	-.009	.036
	14.5	-.109	-.145	-.181	-.221	-.108	-.076	-.032	.010
	21.0	-.123	-.153	-.187	-.224	-.118	-.088	-.057	-.026
	24.5	-.129	-.158	-.187	-.221	-.127	-.114	-.077	-.034
	31.0	-.140	-.170	-.184	-.221	-.141	-.119	-.091	-.060
	34.5	-.160	-.181	-.204	-.229	-.154	-.130	-.106	-.069
	41.0	-.174	-.195	-.215	-.235	-.157	-.136	-.114	-.086
	44.5	-.163	-.186	-.211	-.231	-.157	-.136	-.118	-.091
	51.0	-.155	-.175	-.196	-.212	-.162	-.143	-.126	-.103
	59.5	-.130	-.149	-.162	-.175	-.141	-.122	-.107	-.089
	71.0	-.097	-.111	-.122	-.129	-.096	-.088	-.077	-.060
	79.5	-.047	-.057	-.074	-.069	-.048	-.041	-.033	-.022
	91.0	.012	.005	.002	0	.011	.013	.016	.024
0.382 b/2	0	0.378	0.379	0.302	0.141	- -	- -	- -	- -
	1.5	-.045	-.197	-.363	-.553	-0.073	0.037	0.131	0.223
	5.5	-.109	-.189	-.251	-.341	-.114	-.044	.020	.091
	6.5	-.118	-.189	-.274	-.338	-.115	-.050	.013	.071
	11.0	-.118	-.181	-.223	-.285	-.122	-.071	-.026	.027
	14.5	-.132	-.178	-.223	-.277	-.131	-.087	-.044	.001
	21.0	-.146	-.172	-.221	-.263	-.137	-.101	-.074	-.027
	24.5	-.149	-.178	-.212	-.255	-.145	-.112	-.080	-.041
	31.0	-.160	-.186	-.215	-.249	-.158	-.129	-.101	-.069
	34.5	-.154	-.186	-.204	-.232	-.162	-.134	-.108	-.078
	41.0	-.174	-.200	-.223	-.246	-.155	-.132	-.109	-.083
	44.5	-.163	-.186	-.211	-.231	-.157	-.136	-.114	-.090
	51.0	-.149	-.170	-.191	-.207	-.158	-.141	-.122	-.100
	59.5	-.129	-.146	-.162	-.175	-.126	-.113	-.098	-.080
	71.0	-.076	-.095	-.106	-.112	-.080	-.070	-.071	-.047
	79.5	-.035	-.045	-.052	-.057	-.030	-.046	-.016	-.007
	91.0	.024	.017	.013	.014	.026	.027	.032	.037
0.555 b/2	0	0.409	0.399	0.333	0.161	- -	- -	- -	- -
	1.5	-.053	-.223	-.411	-.625	-0.060	0.046	0.154	0.249
	5.5	-.125	-.206	-.279	-.380	-.111	-.034	.044	.113
	6.5	-.140	-.217	-.294	-.383	-.109	-.050	.020	.094
	11.0	-.137	-.189	-.243	-.307	-.128	-.082	-.016	.037
	14.5	-.137	-.186	-.237	-.296	-.129	-.076	-.032	.016
	21.0	-.151	-.186	-.223	-.274	-.141	-.101	-.067	-.024
	24.5	-.152	-.181	-.218	-.263	-.142	-.107	-.067	-.035
	31.0	-.151	-.192	-.218	-.252	-.152	-.120	-.091	-.069
	34.5	-.160	-.197	-.221	-.249	-.157	-.126	-.101	-.069
	41.0	-.177	-.203	-.226	-.252	-.153	-.127	-.105	-.078
	44.5	-.158	-.183	-.209	-.231	-.152	-.129	-.108	-.082
	51.0	-.144	-.166	-.187	-.206	-.149	-.129	-.111	-.088
	59.5	-.110	-.130	-.144	-.157	-.129	-.114	-.100	-.082
	71.0	-.076	-.088	-.098	-.106	-.065	-.054	-.060	-.041
	79.5	-.031	-.040	-.046	-.051	-.026	-.019	-.015	-.006
	91.0	.029	-.022	.020	.019	.031	.035	.036	.042

TABLE XXI.- CONTINUED.

(a) α_u, 0°, 1°, 2°, 3° - Concluded.

Semi-span sta.	Percent chord	UPPER SURFACE Angle of attack 0°	1°	2°	3°	LOWER SURFACE Angle of attack 0°	1°	2°	3°
0.707 b/2	0	0.378	0.365	0.263	0.241	- -	- -	- -	- -
	1.5	-.059	-.236	-.444	-.681	-0.068	0.079	0.195	0.291
	5.5	-.137	-.228	-.313	-.416	-.118	-.029	.046	.122
	6.5	-.137	-.228	-.307	-.402	-.112	-.045	.027	.097
	11.0	-.137	-.184	-.251	-.310	-.129	-.079	-.016	.042
	14.5	-.146	-.200	-.237	-.305	-.131	-.075	-.028	.023
	21.0	-.174	-.200	-.243	-.291	-.142	-.097	-.060	-.017
	24.5	-.165	-.192	-.226	-.277	-.145	-.105	-.062	-.031
	31.0	-.160	-.181	-.226	-.263	-.151	-.118	-.089	-.058
	34.5	-.160	-.197	-.223	-.257	-.150	-.119	-.094	-.058
	41.0	-.188	-.192	-.229	-.263	-.152	-.126	-.105	-.078
	44.5	-.155	-.179	-.207	-.227	-.149	-.124	-.106	-.081
	51.0	-.143	-.161	-.182	-.201	-.148	-.127	-.111	-.090
	59.5	-.120	-.134	-.149	-.161	-.123	-.107	-.096	-.080
	71.0	-.071	-.079	-.090	-.097	-.068	-.062	-.048	-.038
	79.5	-.043	-.030	-.039	-.056	-.026	-.014	-.011	-.004
	91.0	.040	.062	.028	.030	.041	.044	.043	.047
0.831 b/2	0	0.353	0.385	0.358	0.200	- -	- -	- -	- -
	1.5	-.070	-.248	-.447	-.681	-0.069	0.077	0.195	0.290
	5.5	-.046	-.236	-.332	-.422	-.127	-.044	.032	.103
	6.5	-.046	-.214	-.313	-.402	-.116	-.047	.026	.094
	11.0	-.046	-.192	-.249	-.310	-.126	-.071	-.015	.039
	14.5	-.160	-.186	-.251	-.313	- -	- -	- -	- -
	21.0	-.174	-.200	-.232	-.280	-.142	-.101	-.060	-.025
	24.5	-.177	-.186	-.237	-.268	-.141	-.103	-.072	-.035
	31.0	-.165	-.192	-.221	-.252	-.148	-.118	-.094	-.063
	34.5	-.160	-.192	-.221	-.241	-.147	-.119	-.099	-.072
	41.0	-.177	-.200	-.221	-.238	-.147	-.125	-.108	-.084
	44.5	-.150	-.168	-.191	-.209	-.144	-.124	-.109	-.090
	51.0	-.142	-.156	-.174	-.188	-.129	-.118	-.106	-.089
	59.5	-.104	-.115	-.126	-.134	-.109	-.099	-.092	-.081
	71.0	-.071	-.065	-.078	-.080	-.054	-.048	-.054	-.037
	79.5	-.016	-.019	-.023	-.024	-.007	-.005	-.005	-.001
	91.0	.041	.041	.038	.039	.049	.051	.048	.049
0.924 b/2	0	0.373	0.312	0.162	-0.115	- -	- -	- -	- -
	1.5	-.034	-.211	-.419	-.673	-0.082	0.058	0.171	0.265
	5.5	-.160	-.245	-.324	-.416	-.130	-.048	.026	.095
	6.5	-.154	-.239	-.316	-.391	-.132	-.054	.016	.085
	11.0	-.154	-.200	-.260	-.319	-.143	-.087	-.024	.024
	14.5	-.160	-.206	-.232	-.296	-.130	-.088	-.046	-.010
	21.0	-.146	-.186	-.223	-.263	-.141	-.113	-.083	-.051
	24.5	-.160	-.181	-.215	-.235	-.138	-.111	-.089	-.064
	31.0	-.151	-.186	-.181	-.207	-.138	-.115	-.100	-.080
	34.5	-.151	-.172	-.181	-.202	-.133	-.115	-.103	-.086
	41.0	-.146	-.172	-.181	-.188	-.135	-.119	-.111	-.096
	44.5	-.135	-.144	-.160	-.173	-.127	-.115	-.108	-.097
	51.0	-.123	-.131	-.145	-.154	-.125	-.113	-.109	-.099
	59.5	-.082	-.087	-.095	-.103	-.081	-.076	-.077	-.072
	71.0	-.038	-.040	-.042	-.043	-.031	-.030	-.033	-.032
	79.5	.004	.004	-.002	-.006	.010	.008	0	-.004
	91.0	.049	.051	.046	.042	.061	.058	.051	.048

NACA

TABLE XXI.- CONTINUED.

(b) α_a, 4°, 6°, 8°, 10°.

Semi-span sta.	Percent chord	UPPER SURFACE Angle of attack 4°	6°	8°	10°	LOWER SURFACE Angle of attack 4°	6°	8°	10°
0.086 b/2	0	0.336	0.113	-0.213	-0.646	- -	- -	- -	- -
	1.5	-.414	-.722	-1.049	-1.423	0.286	0.390	0.459	0.506
	5.5	-.256	-.377	-.491	-.601	.163	.248	.320	.392
	6.5	-.242	-.346	-.452	-.568	.123	.206	.280	.352
	11.0	-.231	-.307	-.375	-.441	.084	.154	.224	.289
	14.5	-.220	-.285	-.363	-.427	.056	.123	.185	.253
	21.0	-.237	-.290	-.352	-.383	.030	.094	.146	.208
	24.5	-.217	-.274	-.316	-.375	.009	.067	.121	.182
	31.0	-.223	-.276	-.319	-.341	-.006	.043	.094	.152
	34.5	-.220	-.276	-.308	-.350	-.024	.025	.075	.129
	41.0	-.231	-.276	-.311	-.350	-.040	.005	.050	.102
	44.5	-.246	-.286	-.324	-.356	- -	- -	- -	- -
	51.0	-.236	-.273	-.305	-.335	-.068	-.022	.017	.065
	59.5	-.200	-.228	-.253	-.275	-.068	-.019	.017	.058
	71.0	-.154	-.174	-.191	-.207	-.068	-.014	.019	.056
	79.5	-.095	-.108	-.119	-.131	-.030	.001	.033	.063
	91.0	-.031	-.036	-.041	-.043	.008	.027	.049	.072
0.195 b/2	0	0.113	-0.343	-0.941	-1.727	- -	- -	- -	- -
	1.5	-.584	-.976	-1.408	-1.902	0.376	0.444	0.434	0.358
	5.5	-.339	-.416	-.669	-.845	.165	.264	.342	.413
	6.5	-.334	-.480	-.627	-.779	.127	.220	.298	.371
	11.0	-.292	-.399	-.502	-.607	.075	.157	.229	.302
	14.5	-.278	-.360	-.449	-.535	.045	.121	.189	.259
	21.0	-.273	-.332	-.411	-.458	.011	.077	.139	.205
	24.5	-.264	-.321	-.391	-.438	-.004	.059	.118	.175
	31.0	-.248	-.302	-.355	-.402	-.031	.025	.080	.139
	34.5	-.259	-.307	-.363	-.397	-.049	.006	.055	.117
	41.0	-.267	-.304	-.344	-.377	-.068	-.012	.044	.091
	44.5	-.253	-.294	-.332	-.366	-.068	-.019	.028	.080
	51.0	-.232	-.270	-.299	-.325	-.083	-.036	.007	.055
	59.5	-.190	-.216	-.239	-.260	-.068	-.032	.007	.048
	71.0	-.140	-.157	-.172	-.184	-.048	-.017	.015	.049
	79.5	-.077	-.087	-.096	-.101	-.013	.010	.035	.062
	91.0	.010	-.005	-.007	-.005	.027	.041	.056	.075
0.382 b/2	0	0.055	-0.725	-1.647	-2.851	- -	- -	- -	- -
	1.5	-.782	-1.246	-1.777	-2.408	0.294	0.392	0.437	0.433
	5.5	-.445	-.641	-.858	-1.083	.148	.250	.330	.396
	6.5	-.428	-.611	-.786	-.997	.125	.224	.305	.375
	11.0	-.359	-.471	-.599	-.734	.071	.159	.234	.307
	14.5	-.331	-.438	-.547	-.657	.044	.126	.198	.269
	21.0	-.306	-.388	-.472	-.549	.006	.080	.146	.213
	24.5	-.301	-.363	-.433	-.513	-.009	.060	.122	.188
	31.0	-.278	-.341	-.400	-.452	-.038	.024	.082	.143
	34.0	-.276	-.324	-.375	-.430	-.050	.008	.065	.124
	41.0	-.276	-.310	-.363	-.397	-.068	-.005	.045	.099
	44.5	-.256	-.298	-.340	-.375	-.068	-.017	.031	.083
	51.0	-.228	-.250	-.298	-.324	-.079	-.035	.009	.056
	59.5	-.250	-.216	-.238	-.258	-.068	-.027	.009	.050
	71.0	-.123	-.139	-.153	-.161	-.035	-.010	.019	.050
	79.5	-.068	-.068	-.081	-.082	.001	.020	.041	.067
	91.0	.010	.008	.009	.013	.040	.050	.064	.079
0.555 b/2	0	-0.109	-0.313	-1.977	-3.412	- -	- -	- -	- -
	1.5	-.875	-1.421	-2.027	-2.734	0.328	0.420	0.442	0.403
	5.5	-.498	-.583	-.961	-1.221	.174	.278	.355	.415
	6.5	-.492	-.683	-.899	-1.130	.153	.256	.335	.400
	11.0	-.387	-.527	-.674	-.823	.086	.180	.257	.330
	14.5	-.362	-.474	-.611	-.723	.060	.146	.219	.292
	21.0	-.326	-.413	-.502	-.596	.013	.087	.155	.223
	24.5	-.306	-.388	-.472	-.549	.001	.077	.142	.201
	31.0	-.284	-.357	-.419	-.482	-.028	.035	.093	.153
	34.5	-.292	-.343	-.408	-.449	-.041	.018	.074	.132
	41.0	-.276	-.327	-.369	-.422	-.054	-.001	.050	.102
	44.5	-.256	-.301	-.345	-.384	-.061	-.010	.037	.088
	51.0	-.226	-.262	-.298	-.327	-.070	-.024	.017	.062
	59.5	-.174	-.200	-.226	-.245	-.067	-.030	.004	.043
	71.0	-.117	-.132	-.145	-.153	-.030	-.006	.020	.049
	79.5	-.062	-.068	-.074	-.076	.002	.020	.038	.060
	91.0	.016	.016	.015	.019	.044	.054	.062	.074

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TABLE XXI.- CONTINUED.

(b) α_u, 4°, 6°, 8°, 10° - Concluded.

Semi-span sta.	Percent chord	UPPER SURFACE Angle of attack 4°	6°	8°	10°	LOWER SURFACE Angle of attack 4°	6°	8°	10°
0.707 b/2	0	-0.281	-1.224	-2.585	-4.325	- -	- -	- -	- -
	1.5	-.970	-1.563	-2.194	-2.989	0.367	0.427	0.388	0.266
	5.5	-.542	-.778	-1.058	-1.332	.193	.300	.376	.425
	6.5	-.523	-.731	-.980	-1.246	.167	.272	.350	.410
	11.0	-.395	-.536	-.697	-.864	.091	.183	.263	.332
	14.5	-.370	-.499	-.633	-.772	.067	.156	.229	.298
	21.0	-.334	-.430	-.530	-.626	.020	.097	.162	.229
	24.5	-.317	-.399	-.480	-.582	.003	.074	.138	.202
	31.0	-.303	-.363	-.433	-.494	-.025	.037	.094	.153
	34.5	-.287	-.343	-.416	-.466	-.035	.024	.078	.134
	41.0	-.292	-.332	-.388	-.411	-.057	-.005	.045	.090
	44.5	-.253	-.297	-.344	-.386	-.057	-.012	.032	.080
	51.0	-.221	-.256	-.291	-.320	-.073	-.031	.006	.051
	59.5	-.176	-.200	-.224	-.243	-.057	-.035	-.004	.029
	71.0	-.106	-.119	-.132	-.139	-.029	-.007	.012	.037
	79.5	-.047	-.055	-.055	-.065	.001	.017	.029	.045
	91.0	.027	.026	.023	.025	.047	.054	.059	.066
0.831 b/2	0	-0.081	-0.923	-2.183	-3.786	- -	- -	- -	- -
	1.5	-.959	-1.491	-2.152	-2.920	0.362	0.420	-0.104	0.256
	5.5	-.548	-.778	-1.035	-1.324	.175	.280	-.129	.407
	6.5	-.792	-.725	-.977	-1.227	.164	.268	-.140	.401
	11.0	-.398	-.538	-.697	-1.141	.086	.176	.251	.317
	14.5	-.384	-.502	-.505	-.765	- -	- -	- -	- -
	21.0	-.331	-.416	-.508	-.610	.009	.080	.147	.205
	24.5	-.328	-.402	-.474	-.549	-.004	.062	.119	.178
	31.0	-.281	-.346	-.405	-.477	-.036	.019	.070	.122
	34.5	-.278	-.332	-.391	-.438	-.048	.002	.048	.097
	41.0	-.273	-.304	-.347	-.388	-.066	-.023	.017	.060
	44.5	-.230	-.267	-.308	-.341	-.073	-.035	-.001	.039
	51.0	-.205	-.233	-.266	-.291	-.076	-.044	-.014	.020
	59.5	-.146	-.167	-.191	-.210	-.071	-.050	-.030	-.005
	71.0	-.089	-.101	-.116	-.130	-.033	-.021	-.010	.006
	79.5	.009	-.039	-.053	-.067	-.001	.005	.009	.018
	91.0	.035	.030	.020	.013	.046	.047	.072	.043
0.924 b/2	0	-0.500	-1.547	-3.019	-4.909	- -	- -	- -	- -
	1.5	-.967	-1.705	-2.255	-3.161	0.338	0.403	0.376	0.274
	5.5	-.542	-.761	-1.002	-1.268	.163	.263	.334	.384
	6.5	-.500	-.697	-.927	-1.171	.152	.250	.318	.368
	11.0	-.384	-.513	-.661	-.790	.063	.146	.213	.272
	14.5	-.356	-.455	-.563	-.676	.025	.095	.151	.206
	21.0	-.303	-.377	-.447	-.527	-.024	.031	.077	.123
	24.5	-.276	-.332	-.405	-.466	-.042	.001	.066	.074
	31.0	-.253	-.302	-.361	-.408	-.064	-.026	.004	.038
	34.5	-.228	-.276	-.313	-.380	-.075	-.049	-.025	0
	41.0	-.231	-.268	-.308	-.333	-.085	-.061	-.041	-.017
	44.5	-.192	-.228	-.275	-.323	-.090	-.072	-.058	-.044
	51.0	-.168	-.199	-.240	-.281	-.092	-.076	-.064	-.147
	59.5	-.115	-.144	-.188	-.235	-.073	-.067	-.067	-.158
	71.0	-.061	-.085	-.124	-.170	-.035	-.036	-.040	-.039
	79.5	-.017	-.044	-.102	-.160	-.009	-.019	-.031	-.039
	91.0	.030	-.003	-.043	-.100	.039	.026	.009	-.003

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TABLE XXI.- CONTINUED.

(c) α_u, 12°, 16°, 20°, 24°.

Semi-span sta.	Percent chord	UPPER SURFACE Angle of attack 12°	16°	20°	24°	LOWER SURFACE Angle of attack 12°	16°	20°	24°
0.086 b/2	0	-1.232	-2.750	-4.785	-6.975	- -	- -	- -	- -
	1.5	-1.822	-2.780	-3.892	-4.900	0.518	0.450	0.266	0.084
	5.5	-.745	-1.053	-1.405	-1.748	.452	.543	.608	.655
	6.5	-.707	-.987	-1.306	-1.628	.416	.521	.602	.674
	11.0	-.532	-.739	-.952	-1.190	.351	.462	.561	.646
	14.5	-.513	-.681	-.872	-1.165	.313	.425	.531	.623
	21.0	-.444	-.585	-.740	-1.151	.265	.373	.475	.561
	24.5	-.430	-.552	-.710	-1.138	.238	.345	.450	.531
	31.0	-.399	-.505	-.666	-.905	.204	.307	.403	.485
	34.5	-.405	-.500	-.650	-.891	.181	.283	.379	.452
	41.0	-.394	-.475	-.628	-.864	.151	.248	.336	.405
	44.5	-.395	-.472	-.618	-.845	- -	- -	- -	- -
	51.0	-.364	-.435	-.576	-.800	.109	.199	.277	.334
	59.5	-.298	-.357	-.490	-.701	.100	.179	.219	.290
	71.0	-.204	-.267	-.385	-.572	.093	.159	.209	.248
	79.5	-.136	-.169	-.274	-.440	.094	.147	.180	.194
	91.0	-.051	-.065	-.145	-.273	.093	.129	.136	.120
0.195 b/2	0	-2.759	-5.349	-8.697	-6.384	- -	- -	- -	- -
	1.5	-2.463	-3.765	-5.128	-2.983	0.207	-0.306	-1.038	-0.935
	5.5	-1.047	-1.487	-2.055	-2.780	.464	.517	.528	.591
	6.5	-.956	-1.341	-1.940	-2.537	.430	.511	.562	.632
	11.0	-.726	-.992	-1.273	-2.425	.366	.473	.568	.645
	14.5	-.637	-.854	-1.125	-2.175	.322	.434	.541	.614
	21.0	-.541	-.711	-.930	-1.817	.264	.376	.487	.559
	24.5	-.510	-.656	-.894	-1.685	.238	.349	.455	.524
	31.0	-.458	-.579	-.792	-1.346	.194	.301	.402	.470
	34.5	-.462	-.566	-.781	-1.302	.195	.275	.369	.434
	41.0	-.427	-.519	-.713	-1.056	.142	.241	.328	.387
	44.5	-.403	-.491	-.676	-1.048	.127	.224	.304	.359
	51.0	-.356	-.433	-.605	-.877	.136	.192	.261	.312
	59.5	-.282	-.345	-.499	-.757	.088	.166	.219	.257
	71.0	-.198	-.243	-.380	-.602	.082	.146	.182	.200
	79.5	-.110	-.140	-.268	-.493	.089	.139	.156	.154
	91.0	-.006	-.027	-.119	-.316	.094	.123	.111	.079
0.382 b/2	0	-4.347	-6.276	-5.677	-3.640	- -	- -	- -	- -
	1.5	-3.122	-4.653	-2.487	-1.458	0.374	0.115	0.112	0.147
	5.5	-1.343	-1.974	-2.434	-1.436	.442	.478	.541	.553
	6.5	-1.213	-1.757	-2.261	-1.390	.427	.483	.553	.568
	11.0	-.889	-1.253	-2.314	-1.395	.367	.460	.545	.575
	14.5	-.784	-1.088	-2.130	-1.343	.331	.435	.518	.554
	21.0	-.643	-.843	-1.992	-1.557	.272	.381	.463	.507
	24.5	-.596	-.772	-1.830	-1.318	.246	.355	.429	.475
	31.0	-.521	-.670	-1.575	-1.310	.198	.306	.375	.422
	34.5	-.485	-.623	-1.465	-1.270	.178	.283	.347	.391
	41.0	-.444	-.557	-1.171	-1.242	.148	.245	.303	.343
	44.5	-.415	-.513	-1.092	-1.186	.131	.224	.273	.310
	51.0	-.355	-.440	-.835	-1.146	.101	.188	.230	.261
	59.5	-.277	-.345	-.680	-1.056	.088	.159	.183	.198
	71.0	-.170	-.222	-.449	-.941	.079	.133	.140	.130
	79.5	-.086	-.129	-.355	-.839	.089	.125	.110	.088
	91.0	.013	-.026	-.195	-.682	.091	.103	.057	-.057
0.555 b/2	0	-5.224	-9.847	-3.651	-2.942	- -	- -	- -	- -
	1.5	-3.548	-10.559	-1.336	-1.080	0.300	-0.068	0.182	0.145
	5.5	-1.512	-2.255	-1.311	-1.064	.449	.459	.519	.515
	6.5	-1.393	-2.220	-1.281	-1.064	.438	.471	.524	.525
	11.0	-1.005	-1.484	-1.265	-1.050	.385	.473	.517	.536
	14.5	-.864	-1.264	-1.213	-1.034	.350	.452	.489	.517
	21.0	-.704	-.907	-1.199	-1.015	.282	.393	.429	.464
	24.5	-.632	-.857	-1.210	-1.001	.258	.369	.399	.436
	31.0	-.546	-.733	-1.191	-.998	.208	.311	.345	.378
	34.5	-.524	-.698	-1.163	-.984	.185	.286	.315	.345
	41.0	-.482	-.610	-1.144	-.976	.149	.243	.264	.291
	44.5	-.424	-.560	-1.089	-.941	.132	.221	.236	.259
	51.0	-.357	-.472	-1.058	-.935	.106	.183	.192	.205
	59.5	-.264	-.357	-.955	-.947	.077	.138	.130	.125
	71.0	-.161	-.231	-.843	-.852	.074	.114	.079	.047
	79.5	-.078	-.142	-.741	-.793	.077	.099	.031	-.039
	91.0	.018	-.057	-.596	-.744	.083	.070	-.072	-.191

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TABLE XXI.- CONCLUDED.

(c) α_u, 12°, 16°, 20°, 24° - Concluded.

Semi-span sta.	Percent chord	UPPER SURFACE Angle of attack 12°	16°	20°	24°	LOWER SURFACE Angle of attack 12°	16°	20°	24°
0.707 b/2	0	-6.516	-7.305	-2.330	-1.798	- -	- -	- -	- -
	1.5	-3.891	-2.830	-.957	-.837	0.056	-0.206	0.115	0.044
	5.5	-1.658	-2.931	-.952	-.861	.443	.483	.498	.488
	6.5	-1.534	-2.574	-.921	-.828	.440	.497	.501	.503
	11.0	-1.050	-2.458	-.927	-.837	.383	.479	.480	.500
	14.5	-.928	-2.222	-.891	-.801	.353	.451	.450	.476
	21.0	-.734	-1.820	-.900	-.820	.283	.380	.387	.419
	24.5	-.673	-1.724	-.867	-.779	.254	.353	.357	.387
	31.0	-.568	-1.218	-.861	-.795	.203	.293	.297	.330
	34.5	-.532	-1.204	-.834	-.760	.182	.266	.267	.294
	41.0	-.471	-.766	-.847	-.787	.137	.215	.210	.232
	44.5	-.415	-.780	-.805	-.739	.120	.192	.183	.202
	51.0	-.347	-.499	-.810	-.745	.089	.150	.130	.142
	59.5	-.259	-.408	-.765	-.721	.059	.106	.064	.065
	71.0	-.145	-.229	-.729	-.704	.058	.082	.001	-.007
	79.5	-.068	-.146	-.675	-.656	.058	.064	-.065	-.075
	91.0	.022	-.042	-.624	-.018	.068	.047	-.176	-.194
0.831 b/2	0	-5.041	-3.765	-2.168	-1.548	- -	- -	- -	- -
	1.5	-3.755	-1.424	-.748	-.686	0.051	0.071	0.180	0.136
	5.5	-1.628	-1.377	-.732	-.672	.430	.479	.471	.470
	6.5	-1.501	-1.308	-.729	-.664	.426	.478	.492	.467
	11.0	-1.041	-1.295	-.713	-.645	.365	.438	.432	.452
	14.5	-.928	-1.220	-.699	-.645	- -	- -	- -	- -
	21.0	-.712	-1.237	-.680	-.637	.254	.329	.327	.357
	24.5	-.648	-1.174	-.666	-.626	.226	.297	.293	.324
	31.0	-.532	-1.176	-.658	-.618	.167	.233	.228	.259
	34.5	-.496	-1.116	-.644	-.615	.137	.200	.192	.223
	41.0	-.433	-1.091	-.652	-.618	.096	.156	.142	.166
	44.5	-.379	-1.020	-.606	-.576	.071	.125	.106	.127
	51.0	-.319	-.960	-.615	-.587	.048	.094	.063	.082
	59.5	-.235	-.848	-.588	-.567	.016	.046	-.004	.008
	71.0	-.145	-.649	-.588	-.561	.017	.028	-.056	-.048
	79.5	-.085	-.552	-.553	-.519	.022	.007	-.098	-.090
	91.0	-.005	-.344	-.520	-.492	.035	-.027	-.188	-.182
0.924 b/2	0	-7.263	-1.817	-1.026	-0.782	- -	- -	- -	- -
	1.5	-4.129	-1.044	-.625	-.571	0.089	0.229	0.246	0.199
	5.5	-1.550	-1.011	-.600	-.563	.399	.431	.417	.413
	6.5	-1.418	-.965	-.586	-.535	.383	.407	.397	.396
	11.0	-.969	-.959	-.586	-.552	.312	.353	.351	.372
	14.5	-.812	-.907	-.562	-.527	.245	.287	.293	.315
	21.0	-.629	-.896	-.562	-.511	.160	.213	.219	.247
	24.5	-.560	-.841	-.529	-.505	.101	.157	.171	.190
	31.0	-.477	-.849	-.529	-.522	.064	.118	.122	.148
	34.5	-.447	-.786	-.488	-.481	.017	.072	.076	.095
	41.0	-.275	-.813	-.512	-.508	-.001	.049	.043	.062
	44.5	-.382	-.733	-.448	-.453	-.031	.020	.010	.026
	51.0	-.331	-.770	-.459	-.462	-.037	.007	-.014	-.001
	59.5	-.298	-.704	-.427	-.439	-.061	-.027	-.059	-.051
	71.0	-.229	-.726	-.439	-.439	-.043	-.045	-.083	-.078
	79.5	-.253	-.648	-.409	-.409	-.031	-.068	-.110	-.111
	91.0	-.164	-.616	-.401	-.394	-.019	-.135	-.161	-.158

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TABLE XXII.- PRESSURE COEFFICIENTS AT SEVEN SEMISPAN STATIONS OF THE WING. M_0, 0.25; R, 18,000,000.

(a) α_u, 0°, 1°, 2°, 3°.

Semi-span sta.	Percent chord	UPPER SURFACE				LOWER SURFACE			
		Angle of attack				Angle of attack			
		0°	1°	2°	3°	0°	1°	2°	3°
0.086 b/2	0	0.485	0.487	0.464	0.419	--	--	--	--
	1.5	.050	-.043	-.148	-.273	0.003	0.081	0.154	0.223
	2.5	-.015	-.081	-.139	-.178	-.012	.055	.077	.123
	6.5	-.034	-.083	-.131	-.183	-.044	-.001	.039	.083
	11.0	-.051	-.089	-.131	-.174	-.051	-.020	.014	.048
	14.5	-.069	-.104	-.144	-.180	-.071	-.039	-.008	.023
	21.0	-.086	-.118	-.150	-.180	-.082	-.052	-.027	.001
	24.5	-.094	-.123	-.160	-.182	-.102	-.074	-.046	-.018
	31.0	-.105	-.125	-.161	-.183	-.113	-.082	-.059	-.032
	34.5	-.126	-.146	-.177	-.199	-.129	-.106	-.077	-.051
	41.0	-.143	-.165	-.186	-.212	-.144	-.123	-.094	-.066
	44.5	-.161	-.185	-.206	-.226	--	--	--	--
	51.0	-.160	-.182	-.201	-.219	-.154	-.115	-.115	-.091
	59.5	-.137	-.155	-.170	-.178	-.134	-.119	-.103	-.084
	71.0	-.107	-.162	-.134	-.142	-.112	-.100	-.087	-.072
	79.5	-.062	-.072	-.081	-.087	-.073	-.064	-.053	-.042
	91.0	-.015	-.020	-.026	-.029	-.019	-.013	-.007	0
0.195 b/2	0	0.445	0.428	0.367	0.269	--	--	--	--
	1.5	.006	-.120	-.257	-.404	0.031	0.144	0.239	0.319
	2.5	-.055	-.123	-.188	-.259	-.069	-.007	.053	.110
	6.5	-.080	-.139	-.200	-.261	-.086	-.029	.023	.077
	11.0	-.092	-.140	-.186	-.237	-.097	-.053	-.010	.033
	14.5	-.105	-.142	-.184	-.225	-.111	-.072	-.034	.007
	21.0	-.124	-.154	-.188	-.221	-.121	-.089	-.056	-.022
	24.5	-.126	-.160	-.186	-.216	-.129	-.098	-.068	-.036
	31.0	-.132	-.163	-.188	-.218	-.146	-.119	-.092	-.062
	34.5	-.149	-.179	-.207	-.229	-.157	-.132	-.106	-.077
	41.0	-.166	-.182	-.213	-.237	-.160	-.139	-.114	-.088
	44.5	-.165	-.189	-.213	-.231	-.159	-.140	-.117	-.093
	51.0	-.156	-.177	-.197	-.215	-.164	-.146	-.126	-.105
	59.5	-.132	-.148	-.163	-.177	-.138	-.123	-.107	-.089
	71.0	-.098	-.111	-.121	-.131	-.098	-.087	-.075	-.062
	79.5	-.048	-.057	-.064	-.070	-.045	-.042	-.034	-.022
	91.0	.009	.005	.002	0	.009	.011	.016	.023
0.312 b/2	0	0.397	0.382	0.294	0.147	--	--	--	--
	1.5	-.015	-.163	-.337	-.523	-0.059	0.046	0.139	0.223
	2.5	-.090	-.175	-.267	-.347	-.106	-.037	.027	.090
	6.5	-.109	-.181	-.261	-.335	-.118	-.053	.008	.068
	11.0	-.124	-.177	-.224	-.286	-.126	-.076	-.026	.023
	14.5	-.128	-.177	-.222	-.275	-.135	-.090	-.046	-.001
	21.0	-.143	-.179	-.219	-.256	-.140	-.103	-.067	-.028
	24.5	-.145	-.181	-.219	-.254	-.148	-.114	-.080	-.044
	31.0	-.157	-.182	-.215	-.250	-.161	-.132	-.102	-.070
	34.5	-.151	-.181	-.207	-.237	-.165	-.137	-.109	-.078
	41.0	-.166	-.194	-.221	-.237	-.158	-.134	-.110	-.084
	44.5	-.172	-.188	-.211	-.232	-.159	-.137	-.115	-.089
	51.0	-.149	-.170	-.192	-.208	-.161	-.142	-.122	-.100
	59.5	-.130	-.147	-.163	-.175	-.129	-.113	-.098	-.080
	71.0	-.079	-.094	-.104	-.113	-.081	-.068	-.060	-.048
	79.5	-.037	-.045	-.052	-.058	-.031	-.025	-.017	-.009
	91.0	.021	.016	.014	.012	.024	.026	.031	.036
0.555 b/2	0	0.425	0.425	0.348	0.181	--	--	--	--
	1.5	-.030	-.186	-.381	-.592	-0.071	0.054	0.163	0.251
	2.5	-.095	-.182	-.282	-.379	-.106	-.028	.044	.110
	6.5	-.124	-.198	-.291	-.375	-.115	-.037	.027	.092
	11.0	-.122	-.181	-.243	-.311	-.134	-.076	-.020	.034
	14.5	-.126	-.181	-.240	-.294	-.135	-.085	-.036	.013
	21.0	-.136	-.181	-.224	-.275	-.147	-.107	-.065	-.026
	24.5	-.141	-.177	-.219	-.254	-.146	-.110	-.073	-.036
	31.0	-.147	-.181	-.219	-.250	-.156	-.125	-.093	-.060
	34.5	-.163	-.182	-.219	-.248	-.160	-.133	-.105	-.073
	41.0	-.168	-.198	-.222	-.244	-.154	-.133	-.108	-.080
	44.5	-.159	-.184	-.209	-.231	-.153	-.133	-.111	-.085
	51.0	-.145	-.167	-.188	-.204	-.149	-.133	-.112	-.090
	59.5	-.116	-.132	-.147	-.159	-.130	-.118	-.103	-.085
	71.0	-.077	-.089	-.098	-.108	-.074	-.066	-.057	-.044
	79.5	-.032	-.039	-.046	-.051	-.027	-.023	-.017	-.007
	91.0	.026	.022	.019	.019	.031	.030	.033	.038

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TABLE XXII.- CONTINUED.

(a) α_u, 0°, 1°, 2°, 3° - Concluded.

Semi-span sta.	Percent chord	UPPER SURFACE Angle of attack 0°	1°	2°	3°	LOWER SURFACE Angle of attack 0°	1°	2°	3°
0.707 b/2	0	0.405	0.376	0.254	0.050	- -	- -	- -	- -
	1.5	-.034	-.211	-.415	-.639	-0.057	0.079	0.203	0.297
	5.5	-.113	-.205	-.312	-.408	-.106	-.024	.054	.126
	5.6	-.115	-.202	-.301	-.398	-.115	-.038	.034	.102
	11.0	-.118	-.179	-.249	-.311	-.136	-.078	-.021	.035
	14.5	-.128	-.161	-.243	-.295	-.136	-.084	-.034	.017
	21.0	-.145	-.190	-.234	-.286	-.144	-.105	-.065	-.023
	24.5	-.147	-.182	-.224	-.273	-.149	-.112	-.074	-.035
	31.0	-.157	-.184	-.221	-.256	-.153	-.124	-.091	-.059
	34.5	-.161	-.182	-.222	-.254	-.153	-.125	-.096	-.065
	41.0	-.172	-.198	-.226	-.252	-.154	-.133	-.108	-.081
	44.5	-.156	-.184	-.209	-.230	-.152	-.132	-.109	-.085
	51.0	-.141	-.166	-.186	-.202	-.149	-.133	-.113	-.093
	59.5	-.119	-.135	-.153	-.163	-.124	-.113	-.100	-.083
	71.0	-.069	-.083	-.091	-.098	-.066	-.059	-.053	-.040
	79.5	-.024	-.034	-.040	-.044	-.022	-.020	-.015	-.007
	91.0	.035	.029	.026	.027	.039	.037	.038	.043
0.831 b/2	0	0.368	0.411	0.351	0.206	- -	- -	- -	- -
	1.5	-.048	-.224	-.447	-.651	-0.079	0.074	0.193	0.291
	5.5	-.128	-.222	-.318	-.415	-.128	-.034	.041	.109
	6.5	-.122	-.209	-.303	-.398	-.120	-.041	.030	.100
	11.0	-.113	-.181	-.247	-.313	-.131	-.075	-.021	.032
	14.5	-.141	-.196	-.259	-.311	- -	- -	- -	- -
	21.0	-.149	-.190	-.240	-.278	-.186	-.107	-.070	-.029
	24.5	-.161	-.194	-.234	-.271	-.183	-.109	-.075	-.039
	31.0	-.157	-.182	-.219	-.246	-.190	-.124	-.095	-.065
	34.5	-.164	-.186	-.217	-.239	-.190	-.125	-.102	-.074
	41.0	-.189	-.184	-.215	-.237	-.190	-.132	-.112	-.088
	44.5	-.152	-.174	-.194	-.210	-.186	-.131	-.112	-.093
	51.0	-.141	-.161	-.178	-.189	-.177	-.125	-.110	-.092
	59.5	-.104	-.118	-.129	-.138	-.152	-.104	-.095	-.084
	71.0	-.063	-.071	-.079	-.082	-.096	-.053	-.049	-.041
	79.5	-.016	-.021	-.025	-.027	-.007	-.009	-.008	-.003
	91.0	.042	.038	.036	.037	.050	.046	.045	.047
0.924 b/2	0	0.393	0.319	0.157	-0.102	- -	- -	- -	- -
	1.5	-.011	-.200	-.425	-.656	-0.087	0.051	0.166	0.270
	5.5	-.149	-.234	-.325	-.421	-.135	-.056	.034	.100
	6.5	-.140	-.221	-.318	-.392	-.119	-.045	.027	.091
	11.0	-.138	-.198	-.257	-.313	-.145	-.078	-.031	.016
	14.5	-.149	-.196	-.242	-.292	-.136	-.095	-.055	-.013
	21.0	-.151	-.186	-.221	-.256	-.141	-.114	-.085	-.053
	24.5	-.149	-.179	-.205	-.235	-.139	-.117	-.094	-.067
	31.0	-.147	-.175	-.200	-.218	-.139	-.122	-.104	-.082
	34.5	-.145	-.163	-.184	-.199	-.134	-.121	-.107	-.089
	41.0	-.153	-.165	-.184	-.195	-.135	-.125	-.113	-.098
	44.5	-.132	-.149	-.163	-.174	-.128	-.121	-.112	-.100
	51.0	-.121	-.134	-.147	-.156	-.125	-.120	-.112	-.101
	59.5	-.081	-.091	-.098	-.104	-.081	-.080	-.079	-.074
	71.0	-.039	-.043	-.049	-.052	-.031	-.034	-.036	-.034
	79.5	.003	0	-.004	-.008	.010	.003	-.002	-.004
	91.0	.051	.047	.043	.039	.062	.054	.049	.046

TABLE XXII.- CONTINUED.

(b) α_u, 4°, 6°, 8°, 10°.

Semi-span sta.	Percent chord	UPPER SURFACE Angle of attack 4°	6°	8°	10°	LOWER SURFACE Angle of attack 4°	6°	8°	10°
0.086 b/2	0	0.354	0.141	-0.208	-0.678	- -	- -	- -	- -
	1.5	-.399	-.676	-1.035	-1.424	0.285	0.381	0.458	0.501
	5.5	-.244	-.356	-.481	-.616	.165	.242	.321	.385
	6.5	-.234	-.343	-.462	-.584	.124	.200	.282	.349
	11.0	-.217	-.294	-.376	-.469	.083	.148	.220	.289
	14.5	-.215	-.284	-.361	-.435	.056	.118	.186	.249
	21.0	-.217	-.277	-.330	-.398	.030	.085	.146	.204
	24.5	-.211	-.269	-.323	-.381	.009	.061	.122	.178
	31.0	-.200	-.267	-.313	-.358	-.007	.040	.096	.147
	34.5	-.215	-.269	-.319	-.360	-.023	.022	.074	.126
	41.0	-.234	-.273	-.319	-.356	-.040	.001	.049	.098
	44.5	-.247	-.287	-.324	-.361	- -	- -	- -	- -
	51.0	-.238	-.273	-.305	-.337	-.063	-.025	.019	.062
	59.5	-.200	-.228	-.253	-.277	-.062	-.022	.016	.056
	71.0	-.153	-.174	-.191	-.208	-.056	-.017	.020	.053
	79.5	-.095	-.108	-.119	-.128	-.029	-.001	.033	.061
	91.0	-.030	-.037	-.041	-.044	.010	.027	.051	.070
0.195 b/2	0	0.122	-0.296	-0.939	-1.741	- -	- -	- -	- -
	1.5	-.573	-.948	-1.412	-1.914	0.380	0.441	0.437	0.359
	5.5	-.333	-.490	-.675	-.854	.166	.258	.344	.409
	6.5	-.327	-.471	-.634	-.789	.127	.214	.299	.367
	11.0	-.287	-.384	-.504	-.608	.075	.152	.229	.297
	14.5	-.270	-.352	-.451	-.542	.046	.115	.189	.254
	21.0	-.255	-.328	-.402	-.473	.013	.073	.139	.200
	24.5	-.249	-.307	-.379	-.447	-.003	.056	.118	.176
	31.0	-.242	-.294	-.355	-.411	-.032	.021	.079	.134
	34.5	-.253	-.299	-.359	-.407	-.049	.007	.059	.111
	41.0	-.253	-.296	-.342	-.381	-.062	-.014	.037	.086
	44.5	-.253	-.294	-.332	-.369	-.069	-.018	.028	.075
	51.0	-.232	-.267	-.297	-.328	-.082	-.038	.007	.052
	59.5	-.189	-.216	-.239	-.262	-.070	-.034	.007	.045
	71.0	-.140	-.157	-.172	-.186	-.048	-.018	.015	.046
	79.5	-.076	-.087	-.095	-.103	-.012	.010	.036	.060
	91.0	-.001	-.006	-.006	-.008	.029	.041	.059	.074
0.312 b/2	0	-0.073	-0.693	-1.625	-2.797	- -	- -	- -	- -
	1.5	-.731	-1.210	-1.789	-2.420	0.293	0.390	0.439	0.433
	5.5	-.439	-.630	-.854	-1.087	.149	.245	.330	.388
	6.5	-.422	-.584	-.792	-.997	.124	.219	.304	.371
	11.0	-.346	-.466	-.602	-.744	.070	.150	.235	.302
	14.5	-.327	-.426	-.545	-.661	.043	.122	.198	.265
	21.0	-.295	-.377	-.466	-.559	.009	.077	.147	.209
	24.5	-.289	-.360	-.434	-.512	-.008	.056	.122	.183
	31.0	-.272	-.339	-.402	-.464	-.038	.020	.082	.138
	34.5	-.266	-.311	-.376	-.434	-.049	.007	.065	.120
	41.0	-.268	-.307	-.361	-.409	-.057	-.005	.046	.094
	44.5	-.254	-.297	-.338	-.377	-.065	-.016	.032	.080
	51.0	-.226	-.262	-.295	-.326	-.078	-.035	.011	.054
	59.5	-.189	-.215	-.226	-.259	-.062	-.029	.010	.047
	71.0	-.122	-.138	-.152	-.164	-.034	-.010	.020	.048
	79.5	-.062	-.073	-.079	-.084	.002	.020	.043	.064
	91.0	.011	.008	.010	.011	.042	.052	.065	.077
0.555 b/2	0	-0.081	-0.848	-1.942	-3.363	- -	- -	- -	- -
	1.5	-.837	-1.382	-2.034	-2.760	0.325	0.416	0.442	0.401
	5.5	-.481	-.704	-.958	-1.219	.173	.278	.356	.412
	6.5	-.471	-.670	-.901	-1.129	.152	.252	.335	.394
	11.0	-.373	-.513	-.673	-.826	.085	.175	.258	.325
	14.5	-.348	-.473	-.602	-.734	.059	.142	.220	.285
	21.0	-.310	-.403	-.504	-.597	.013	.084	.155	.217
	24.5	-.291	-.377	-.464	-.542	0	.068	.134	.196
	31.0	-.274	-.345	-.415	-.480	-.029	.032	.093	.149
	34.5	-.272	-.328	-.394	-.454	-.042	.013	.074	.127
	41.0	-.270	-.313	-.374	-.417	-.054	-.004	.049	.097
	44.5	-.255	-.301	-.344	-.385	-.059	-.013	.038	.083
	51.0	-.244	-.282	-.296	-.329	-.069	-.028	.019	.059
	59.5	-.174	-.203	-.226	-.248	-.066	-.033	.005	.039
	71.0	-.115	-.132	-.145	-.156	-.031	-.008	.021	.046
	79.5	-.056	-.066	-.072	-.076	.003	.017	.040	.057
	91.0	.013	.015	-.016	.017	.045	.050	.065	.072

TABLE XXII.- CONTINUED.

(b) α_u, 4°, 6°, 8°, 10° - Concluded.

Semi-span sta.	Percent chord	UPPER SURFACE Angle of attack 4°	6°	8°	10°	LOWER SURFACE Angle of attack 4°	6°	8°	10°
0.707 b/2	0	-0.266	-1.176	-2.532	-4.270	- -	- -	- -	- -
	1.5	-.903	-1.503	-2.228	-3.041	0.366	0.424	0.393	0.268
	5.5	-.524	-.766	-1.048	-1.335	.191	.293	.374	.421
	6.5	-.500	-.725	-.979	-1.243	.165	.265	.351	.403
	11.0	-.382	-.528	-.692	-.854	.087	.178	.262	.325
	14.5	-.361	-.485	-.624	-.768	.065	.148	.228	.292
	21.0	-.327	-.417	-.525	-.620	.017	.089	.162	.222
	24.5	-.310	-.390	-.487	-.571	.003	.070	.139	.195
	31.0	-.289	-.358	-.428	-.492	-.026	.032	.094	.148
	34.5	-.274	-.345	-.411	-.469	-.035	.019	.078	.129
	41.0	-.272	-.326	-.378	-.430	-.055	-.008	.044	.089
	44.5	-.252	-.300	-.342	-.386	-.061	-.016	.032	.075
	51.0	-.219	-.258	-.290	-.324	-.071	-.033	.010	.047
	59.5	-.177	-.204	-.224	-.247	-.066	-.040	-.004	.026
	71.0	-.104	-.122	-.132	-.142	-.029	-.012	.014	.033
	79.5	-.046	-.057	-.061	-.068	0	.012	.028	.042
	91.0	.027	.022	.024	.023	.047	.050	.061	.064
0.831 b/2	0	-0.046	-0.887	-2.147	-3.797	- -	- -	- -	- -
	1.5	-.892	-1.481	-2.170	-2.929	0.359	0.417	0.384	0.258
	5.5	-.524	-.764	-1.035	-1.320	.173	.282	.354	.402
	6.5	-.500	-.723	-.967	-1.219	.161	.261	.344	.394
	11.0	-.384	-.524	-.688	-.851	.082	.170	.250	.311
	14.5	-.367	-.496	-.638	-.764	- -	- -	- -	- -
	21.0	-.319	- -	-.508	-.603	.009	.075	.143	.199
	24.5	-.306	- -	-.468	-.558	-.005	.057	.119	.173
	31.0	-.272	- -	-.406	-.471	-.037	.015	.070	.117
	34.5	-.268	- -	-.379	-.434	-.048	-.002	.048	.091
	41.0	-.253	- -	-.351	-.394	-.066	-.032	.017	.055
	44.5	-.229	-.270	-.306	-.348	-.074	-.040	0	.035
	51.0	-.204	-.237	-.265	-.297	-.075	-.048	-.013	.016
	59.5	-.146	-.171	-.190	-.216	-.073	-.053	-.029	-.010
	71.0	-.087	-.103	-.116	-.133	-.034	-.025	-.008	.002
	79.5	-.030	-.044	-.054	-.071	0	.001	.011	.015
	91.0	.035	.026	.021	.009	.047	.043	.045	.042
0.924 b/2	0	-0.467	- -	-2.984	-4.868	- -	- -	- -	- -
	1.5	-.930	- -	-2.326	-3.190	0.337	0.400	0.380	0.273
	5.5	-.520	- -	-1.005	-1.275	.161	.258	.334	.378
	6.5	-.488	- -	-.926	-1.166	.149	.243	.318	.362
	11.0	-.367	- -	-.643	-.789	.063	.141	.213	.267
	14.5	-.333	- -	-.560	-.678	.025	.091	.153	.202
	21.0	-.289	- -	-.449	-.531	-.025	.026	.077	.118
	24.5	-.259	- -	-.396	-.471	-.044	-.004	.037	.070
	31.0	-.232	- -	-.353	-.411	-.062	-.030	.006	.033
	34.5	-.217	- -	-.321	-.379	-.074	-.051	-.023	-.003
	41.0	-.213	- -	-.300	-.358	-.085	-.065	-.041	-.023
	44.5	-.190	-.230	-.272	-.326	-.090	-.075	-.058	-.045
	51.0	-.168	-.202	-.239	-.285	-.092	-.081	-.063	-.052
	59.5	-.114	-.147	-.185	-.241	-.071	-.070	-.064	-.064
	71.0	-.061	-.089	-.123	-.175	-.034	-.040	-.038	-.041
	79.5	-.017	-.053	-.100	-.165	-.008	-.021	-.028	-.039
	91.0	.030	-.006	-.048	-.102	.040	.023	.013	-.003

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TABLE XXII.- CONTINUED.

(c) α_u, 12°, 14°, 16°, 20°.

Semi-span sta.	Percent chord	UPPER SURFACE Angle of attack 12°	14°	16°	20°	LOWER SURFACE Angle of attack 12°	14°	16°	20°
0.086 b/2	0	-1.175	-1.867	-2.731	-4.728	- -	- -	- -	- -
	1.5	-1.813	-2.289	-2.813	-3.954	0.515	0.500	0.450	0.272
	5.5	-.742	-.888	-1.054	-1.393	.445	.500	.545	.610
	8.5	-.694	-.827	-.971	-1.281	.409	.469	.521	.603
	11.0	-.544	-.635	-.730	-.949	.344	.406	.462	.562
	14.5	-.505	-.581	-.668	-.854	.308	.373	.427	.531
	21.0	-.447	-.509	-.566	-.742	.258	.317	.373	.475
	24.5	-.430	-.486	-.548	-.696	.231	.289	.344	.448
	31.0	-.396	-.447	-.509	-.639	.198	.253	.306	.403
	34.5	-.396	-.444	-.489	-.636	.176	.230	.283	.379
	41.0	-.390	-.429	-.471	-.607	.145	.197	.248	.338
	44.5	-.394	-.424	-.464	-.604	- -	- -	- -	- -
	51.0	-.366	-.390	-.426	-.565	.105	.152	.200	.277
	59.5	-.299	-.315	-.349	-.480	.094	.137	.181	.245
	71.0	-.223	-.233	-.256	-.377	.087	.125	.163	.211
	79.5	-.137	-.148	-.159	-.265	.088	.122	.152	.183
	91.0	-.046	-.046	-.056	-.137	.089	.115	.134	.141
0.195 b/2	0	-2.659	-3.856	-5.326	-8.649	- -	- -	- -	- -
	1.5	-2.449	-3.071	-3.779	-5.204	0.216	0.001	-0.382	-1.027
	5.5	-1.040	-1.247	-1.487	-1.979	.458	.496	.518	.525
	8.5	-.948	-1.121	-1.327	-1.777	.423	.472	.509	.557
	11.0	-.713	-.834	-.969	-1.266	.357	.419	.471	.561
	14.5	-.626	-.725	-.841	-1.114	.313	.376	.432	.536
	21.0	-.535	-.609	-.698	-.918	.257	.317	.375	.485
	24.5	-.501	-.566	-.644	-.878	.231	.291	.348	.454
	31.0	-.450	-.505	-.568	-.784	.187	.245	.301	.402
	34.5	-.447	-.494	-.548	-.771	.165	.223	.275	.370
	41.0	-.413	-.451	-.509	-.711	.136	.188	.242	.328
	44.5	-.404	-.434	-.481	-.686	.122	.175	.224	.306
	51.0	-.358	-.383	-.425	-.607	.096	.144	.192	.263
	59.5	-.283	-.300	-.333	-.500	.084	.127	.169	.225
	71.0	-.200	-.209	-.236	-.373	.077	.115	.150	.186
	79.5	-.112	-.116	-.137	-.258	.085	.115	.143	.159
	91.0	-.009	-.007	-.018	-.109	.091	.113	.130	.122
0.312 b/2	0	-4.244	-6.022	-8.258	-5.790	- -	- -	- -	- -
	1.5	-3.099	-3.865	-4.741	-3.124	0.378	0.276	0.115	0.086
	5.5	-1.323	-1.584	-1.905	-2.701	.537	.566	.476	.544
	8.5	-1.199	-1.426	-1.690	-2.516	.420	.459	.481	.557
	11.0	-.873	-1.024	-1.315	-2.485	.360	.414	.458	.549
	14.5	-.769	-.896	-1.048	-2.259	.324	.381	.427	.520
	21.0	-.632	-.725	-.843	-1.981	.266	.324	.379	.464
	24.5	-.581	-.663	-.766	-1.816	.239	.291	.353	.431
	31.0	-.510	-.578	-.662	-1.448	.191	.288	.304	.376
	34.5	-.483	-.533	-.610	-1.356	.172	.227	.282	.347
	41.0	-.445	-.485	-.546	-1.010	.142	.195	.247	.300
	44.5	-.415	-.447	-.504	-.967	.125	.178	.225	.275
	51.0	-.356	-.384	-.430	-.727	.097	.144	.191	.234
	59.5	-.279	-.297	-.333	-.591	.083	.123	.164	.188
	71.0	-.173	-.178	-.211	-.434	.076	.109	.140	.146
	79.5	-.088	-.088	-.119	-.309	.080	.111	.133	.113
	91.0	.012	.014	-.012	-.170	.089	.105	.119	.089
0.555 b/2	0	-5.090	-7.222	-9.967	-3.705	- -	- -	- -	- -
	1.5	-3.555	-4.413	-5.406	-1.406	0.301	0.146	-0.087	0.178
	5.5	-1.489	-1.785	-2.170	-1.371	.443	.457	.449	.518
	8.5	-1.369	-1.621	-1.959	-1.317	.424	.456	.461	.527
	11.0	-.974	-1.153	-1.375	-1.303	.379	.426	.465	.515
	14.5	-.860	-1.006	-1.206	-1.257	.342	.394	.444	.489
	21.0	-.684	-.784	-.927	-1.264	.275	.332	.387	.429
	24.5	-.628	-.710	-.845	-1.228	.251	.306	.365	.399
	31.0	-.542	-.600	-.716	-1.248	.202	.257	.313	.366
	34.5	-.505	-.565	-.662	-1.208	.179	.229	.287	.311
	41.0	-.462	-.503	-.590	-1.191	.145	.193	.245	.266
	44.5	-.425	-.456	-.543	-1.143	.129	.174	.225	.239
	51.0	-.358	-.381	-.454	-1.103	.100	.142	.188	.194
	59.5	-.267	-.278	-.340	-.991	.075	.105	.147	.134
	71.0	-.163	-.165	-.211	-.841	.071	.098	.127	.088
	79.5	-.079	-.078	-.123	-.723	.076	.095	.109	.040
	91.0	.019	.017	-.033	-.553	.081	.087	.083	-.051

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TABLE XXII.- CONCLUDED.

(c) α_u, 12°, 14°, 16°, 20° - Concluded.

Semi-span sta.	Percent chord	UPPER SURFACE Angle of attack 12°	14°	16°	20°	LOWER SURFACE Angle of attack 12°	14°	16°	20°
0.707 b/2	0	-6.400	-8.897	-10.748	-2.710	- -	- -	- -	- -
	1.5	-3.911	-4.816	-4.520	-.971	0.068	-0.208	-0.491	0.080
	5.5	-1.631	-1.973	-3.558	-.971	.442	.436	.441	.469
	6.5	-1.515	-1.811	-3.377	-.936	.438	.447	.473	.497
	11.0	-1.027	-1.210	-1.654	-.935	.380	.419	.476	.475
	14.5	-.901	-1.056	-1.530	-.900	.348	.392	.454	.449
	21.0	-.718	-.820	-.929	-.896	.278	.327	.391	.388
	24.5	-.656	-.747	-.869	-.865	.251	.301	.361	.355
	31.0	-.557	-.628	-.730	-.878	.198	.248	.304	.300
	34.5	-.523	-.579	-.686	-.847	.178	.245	.276	.270
	41.0	-.465	-.503	-.606	-.878	.133	.177	.223	.211
	44.5	-.424	-.458	-.544	-.842	.117	.157	.201	.183
	51.0	-.352	-.374	-.438	-.847	.085	.123	.161	.134
	59.5	-.263	-.274	-.306	-.798	.055	.087	.117	.067
	71.0	-.150	-.152	-.162	-.755	.055	.075	.094	.010
	79.5	-.071	-.073	-.074	-.695	.055	.067	.076	-.053
	91.0	.022	.014	-.005	-.632	.068	.068	.057	-.168
0.831 b/2	0	-5.764	-8.097	-4.705	-2.217	- -	- -	- -	- -
	1.5	-3.750	-4.558	-1.929	-.748	0.058	-0.210	-0.043	0.158
	5.5	-1.618	-1.938	-1.851	-.729	.428	.427	.478	.464
	6.5	-1.489	-1.778	-1.714	-.715	.425	.428	.476	.460
	11.0	-1.023	-1.197	-1.747	-.709	.361	.399	.446	.429
	14.5	-.913	-1.063	-1.630	-.691	- -	- -	- -	- -
	21.0	-.694	-.788	-1.666	-.678	.250	.291	.340	.327
	24.5	-.634	-.717	-1.568	-.660	.226	.265	.309	.294
	31.0	-.523	-.581	-1.494	-.656	.164	.205	.248	.231
	34.5	-.486	-.540	-1.409	-.641	.133	.173	.213	.194
	41.0	-.430	-.468	-1.246	-.647	.093	.130	.169	.142
	44.5	-.385	-.418	-1.172	-.625	.070	.102	.139	.108
	51.0	-.325	-.349	-.897	-.652	.046	.074	.108	.065
	59.5	-.240	-.261	-.685	-.616	.012	.033	.039	-.003
	71.0	-.149	-.162	-.287	-.616	.015	.027	.046	-.058
	79.5	-.086	-.103	-.214	-.576	.022	.024	.035	-.097
	91.0	-.004	-.026	-.064	-.537	.038	.029	.029	-.188
0.924 b/2	0	-7.164	-9.809	-3.799	-1.715	- -	- -	- -	- -
	1.5	-4.128	-5.064	-1.289	-.588	0.096	-0.144	0.095	0.208
	5.5	-1.549	-1.845	-1.230	-.583	.397	.390	.427	.413
	6.5	-1.418	-1.679	-1.176	-.568	.383	.379	.410	.398
	11.0	-.939	-1.110	-1.168	-.568	.310	.339	.367	.354
	14.5	-.800	-.935	-1.088	-.535	.242	.272	.304	.296
	21.0	-.615	-.708	-1.084	-.533	.156	.188	.226	.223
	24.5	-.542	-.630	-1.005	-.513	.099	.123	.169	.168
	31.0	-.465	-.535	-1.044	-.513	.060	.084	.130	.123
	34.5	-.443	-.507	-.967	-.491	.015	.031	.082	.076
	41.0	-.409	-.464	-1.052	-.497	-.004	.013	.060	.043
	44.5	-.385	-.447	-.992	-.464	-.034	-.022	.029	.011
	51.0	-.337	-.387	-1.076	-.480	-.039	-.026	.020	-.016
	59.5	-.303	-.366	-1.007	-.451	-.062	-.058	-.014	-.059
	71.0	-.232	-.297	-.900	-.469	-.042	-.041	-.011	-.085
	79.5	-.248	-.360	-.809	-.435	-.047	-.051	-.035	-.113
	91.0	-.165	-.241	-.617	-.423	-.018	-.034	-.068	-.167

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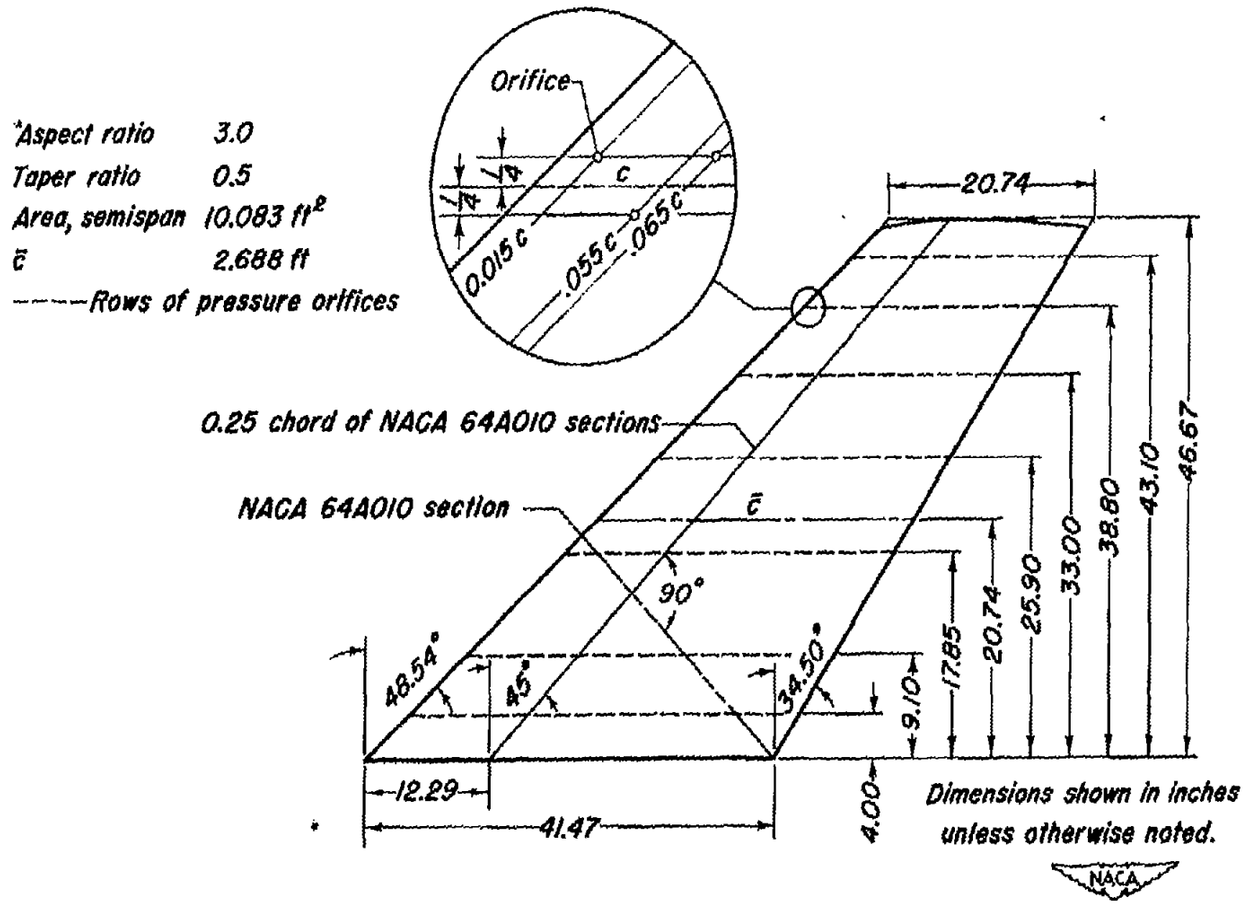


Figure 1.- Plan form of the wing.

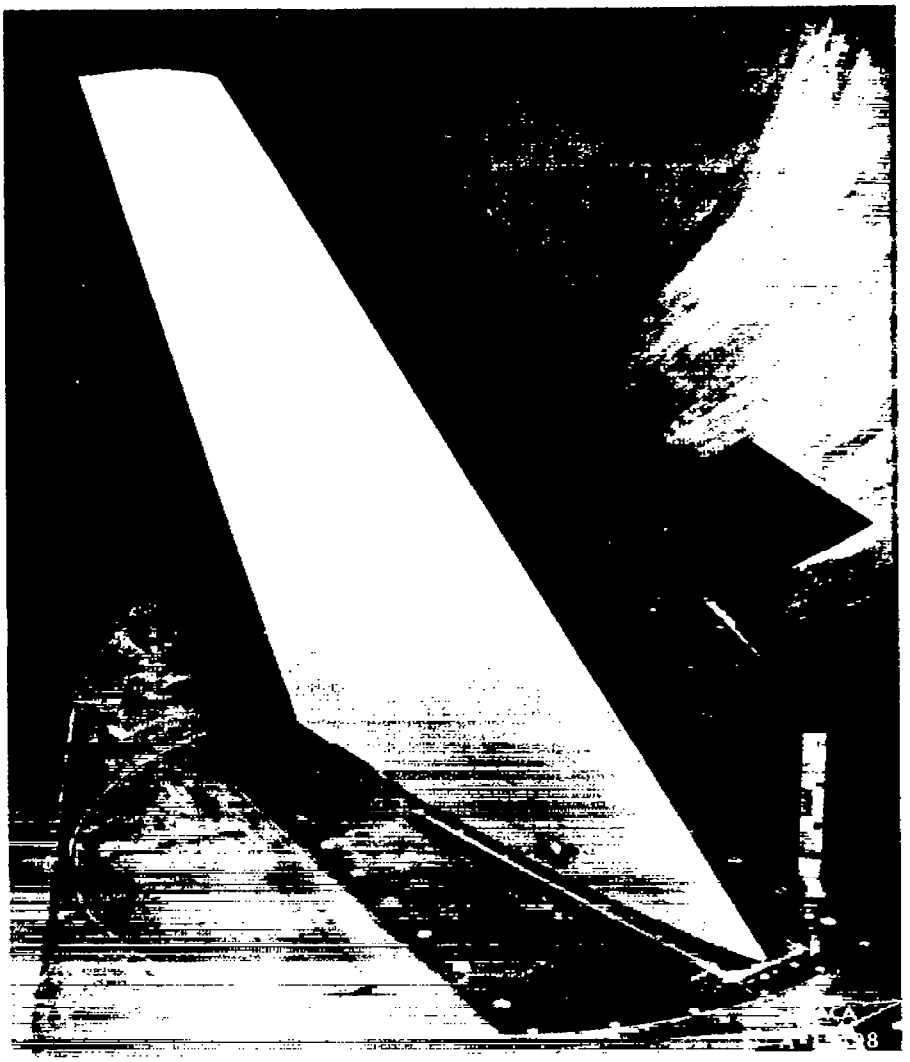


Figure 2.- The model mounted in the Ames 12-foot pressure wind tunnel.

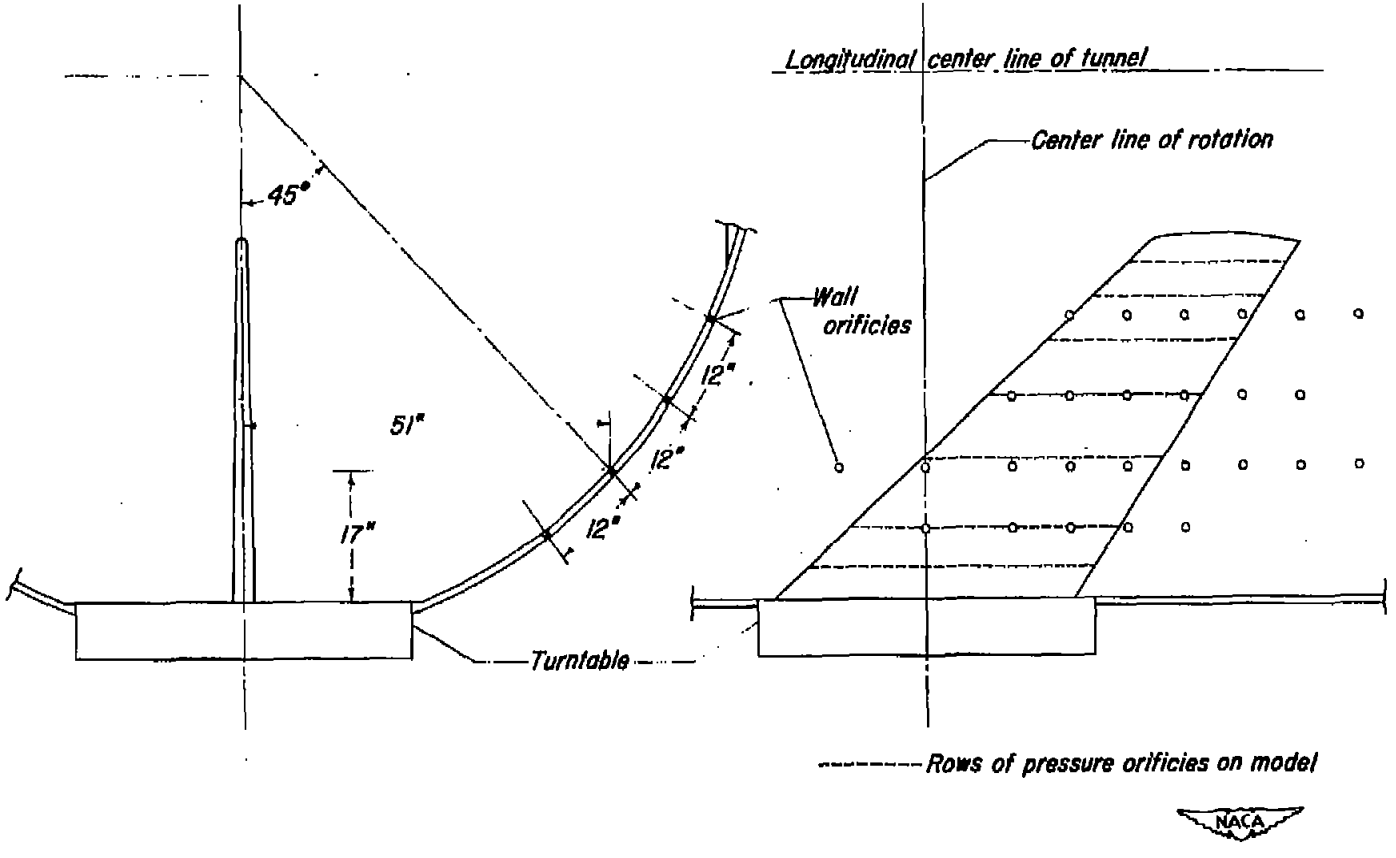


Figure 3.–The location of the wall orificies in the Ames 12-foot pressure wind-tunnel test section.

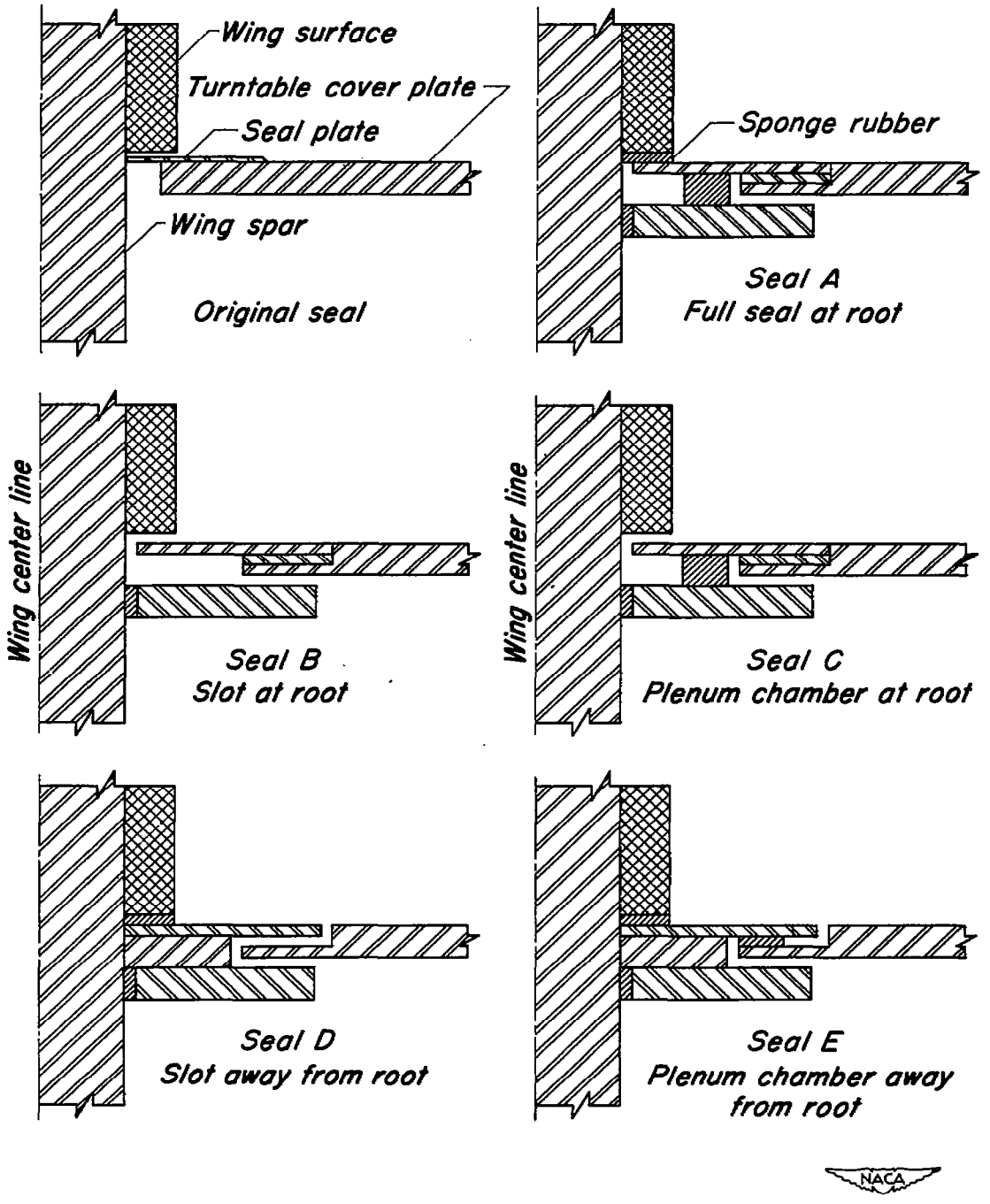
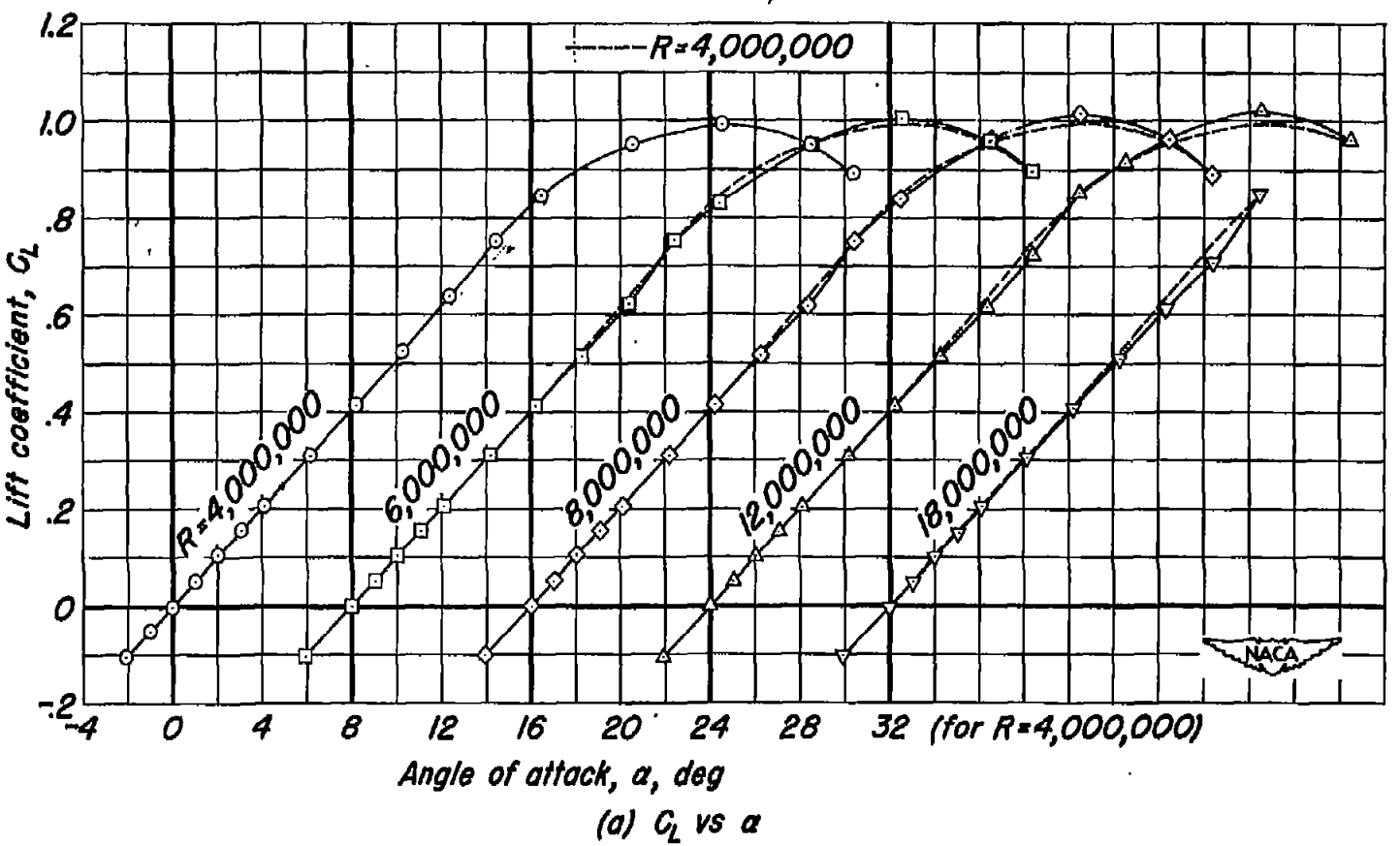
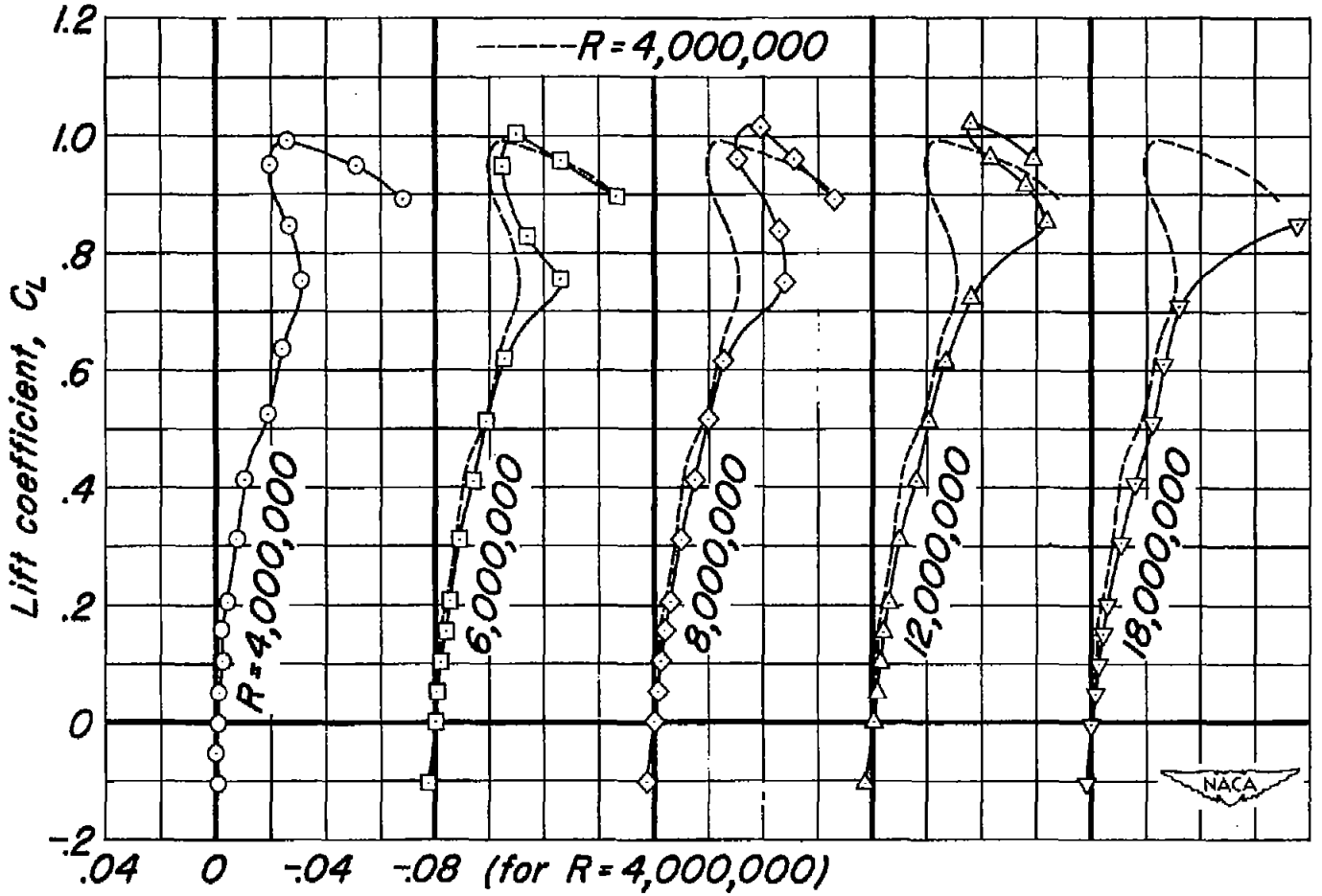


Figure 4.–Cross sections of several seals at the base of the model.



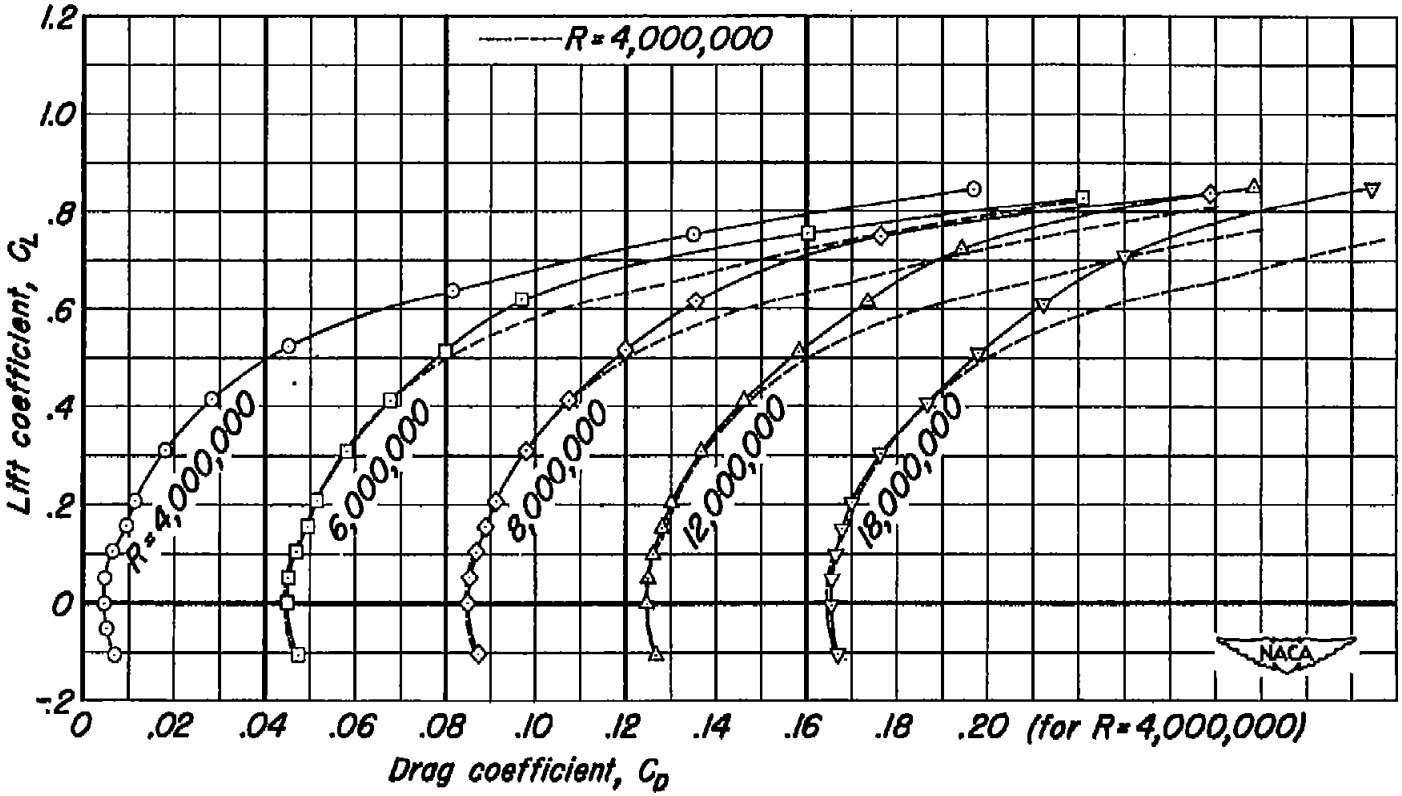
(a) C_L vs α

Figure 5.–The effect of Reynolds number on the low-speed aerodynamic characteristics. M_o, 0.25.



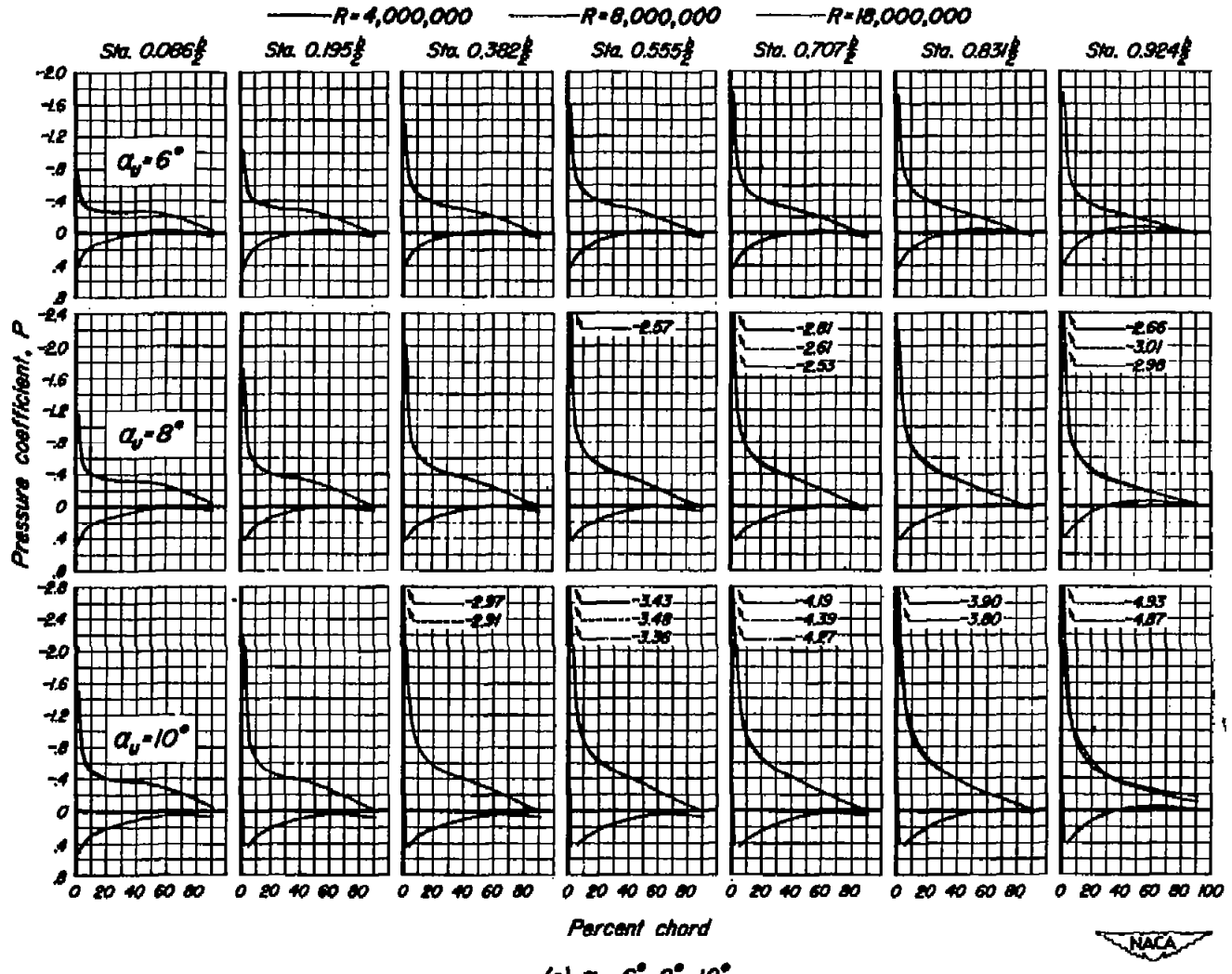
(b) C_L vs C_m

Figure 5.—Continued.



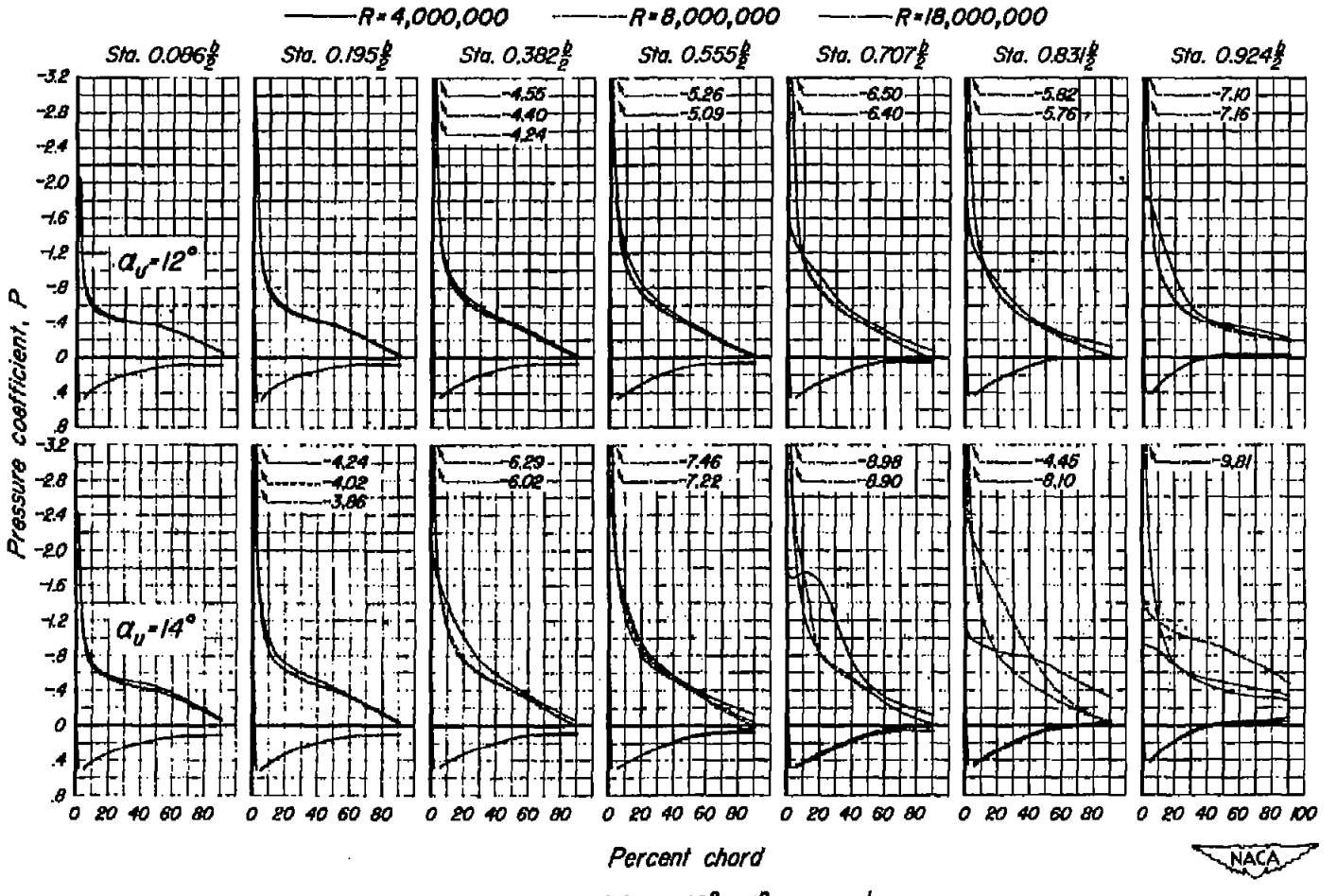
(c) C_L vs C_D

Figure 5.–Concluded.



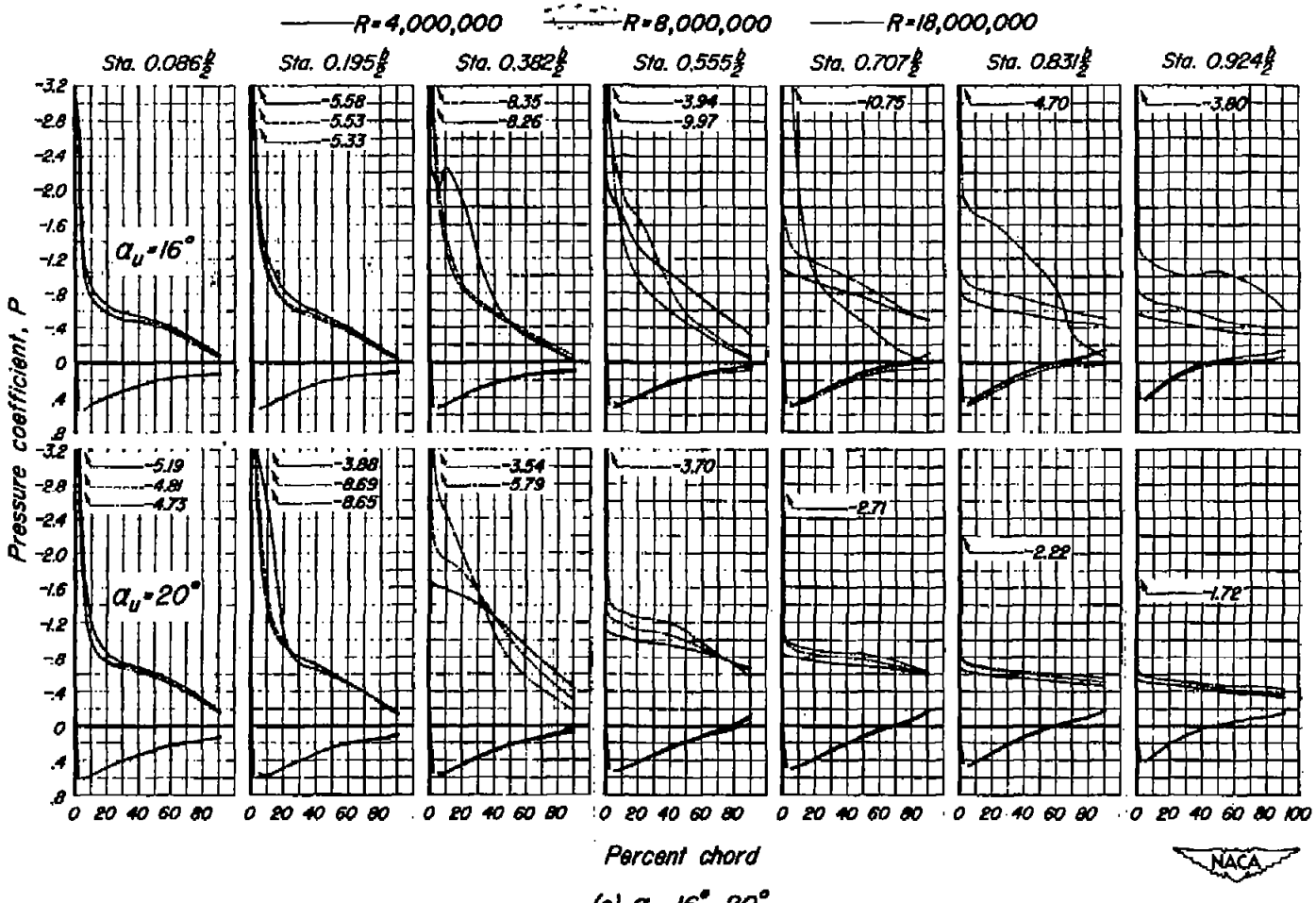
(a) α_u, 6°, 8°, 10°

Figure 6.–The chordwise distribution of pressure coefficient at seven semispan stations for several angles of attack and Reynolds numbers of 4,000,000, 8,000,000, and 18,000,000. M_∞, 0.25.



(b) α_u, 12°, 14°

Figure 6.– Continued.



(c) α_u, 16°, 20°

Figure 6.- Concluded.

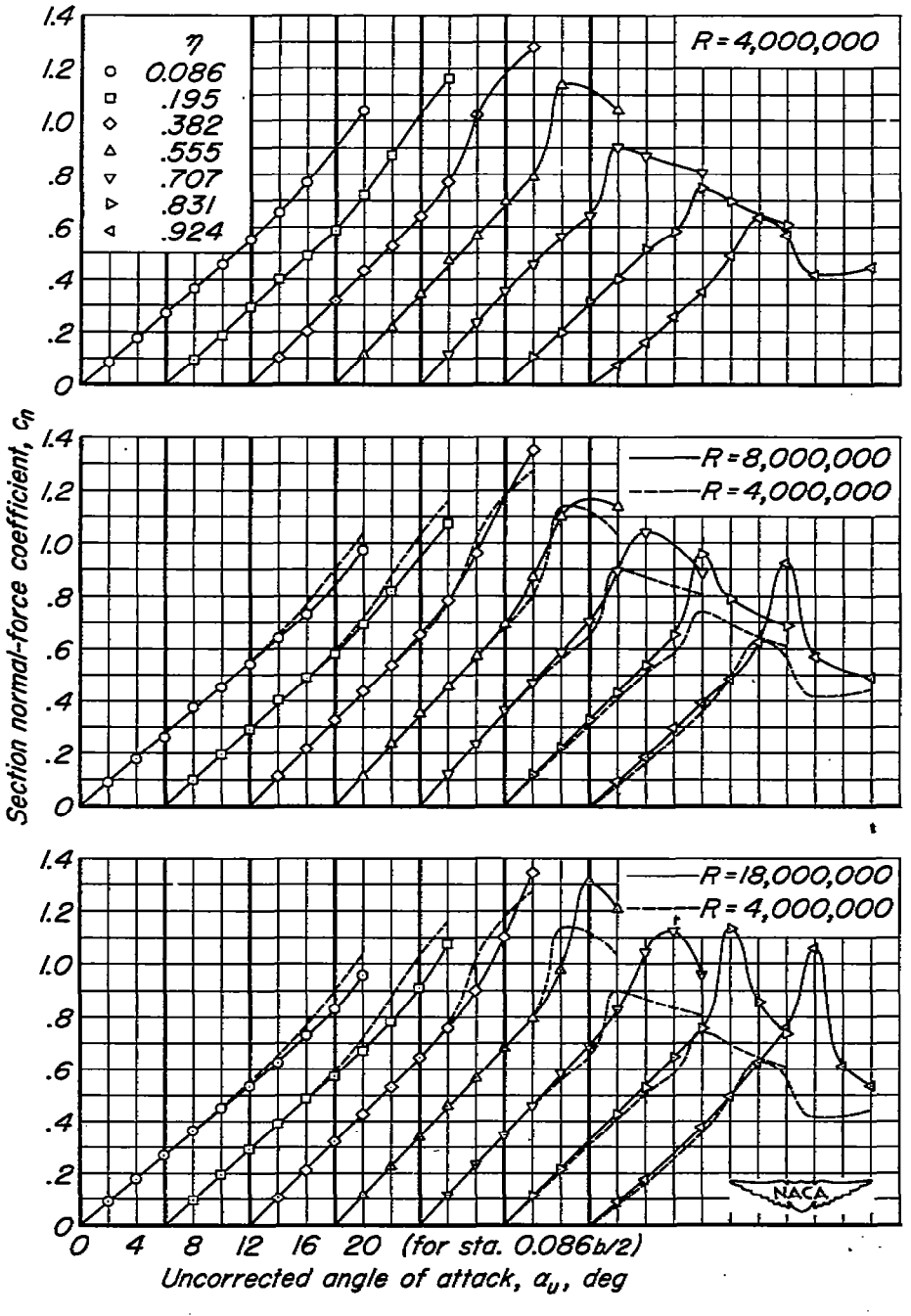


Figure 7.–The effect of Reynolds number on the section normal-force coefficients at seven semispan stations. M_o, 0.25.

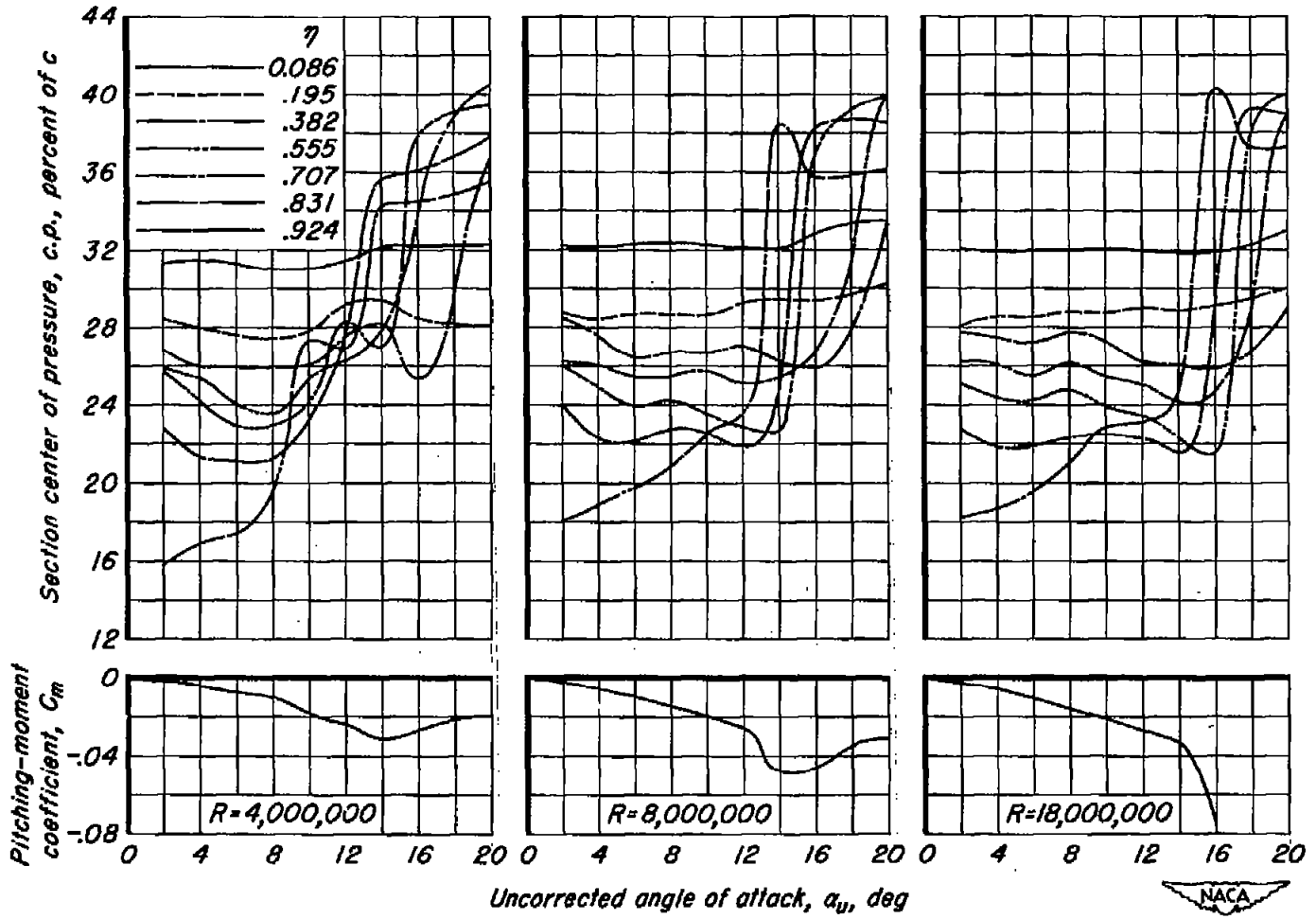


Figure 8.–The variation of the section centers of pressure and the pitching-moment coefficient with angle of attack for Reynolds numbers of 4,000,000, 8,000,000, and 18,000,000. M_o, 0.25.

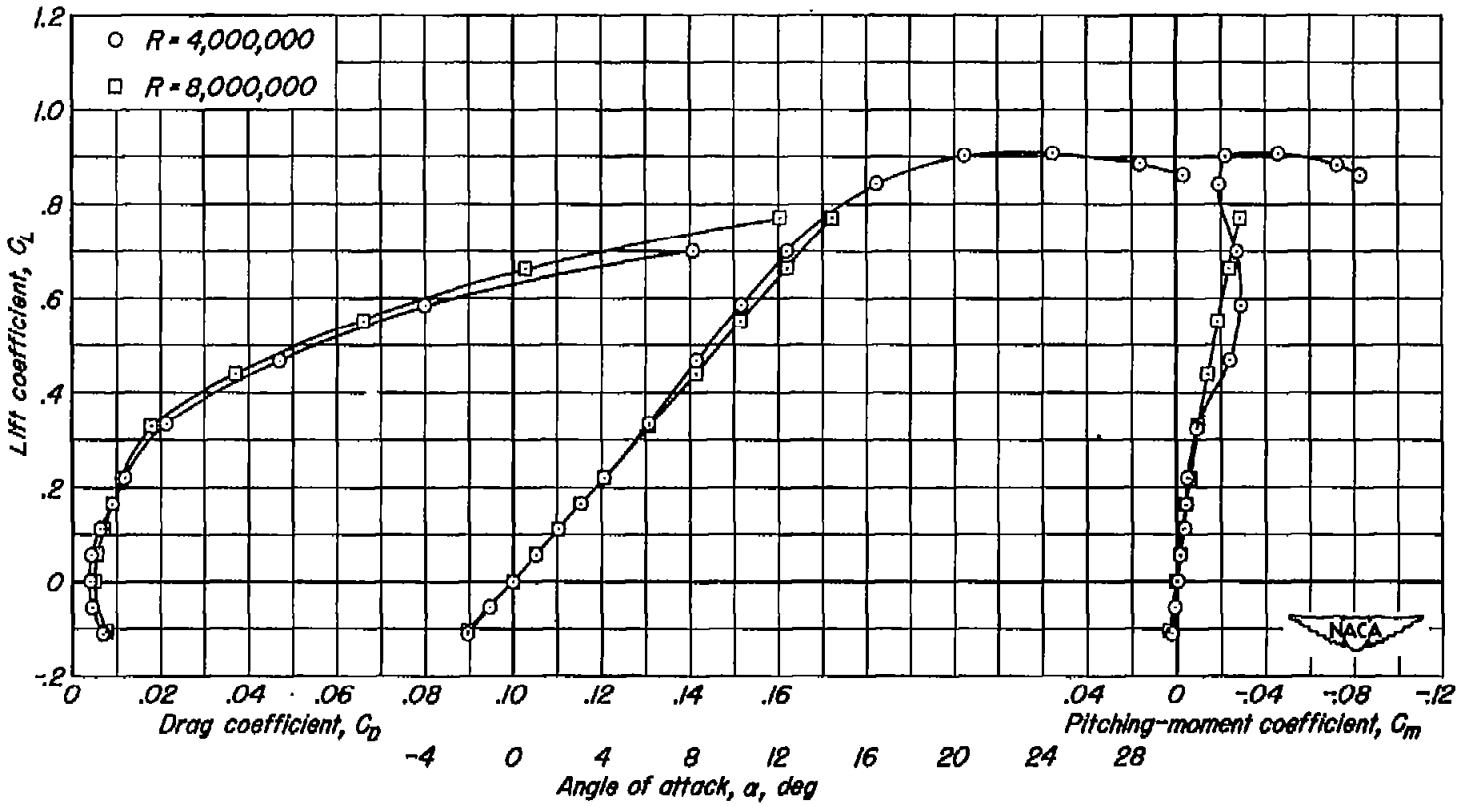
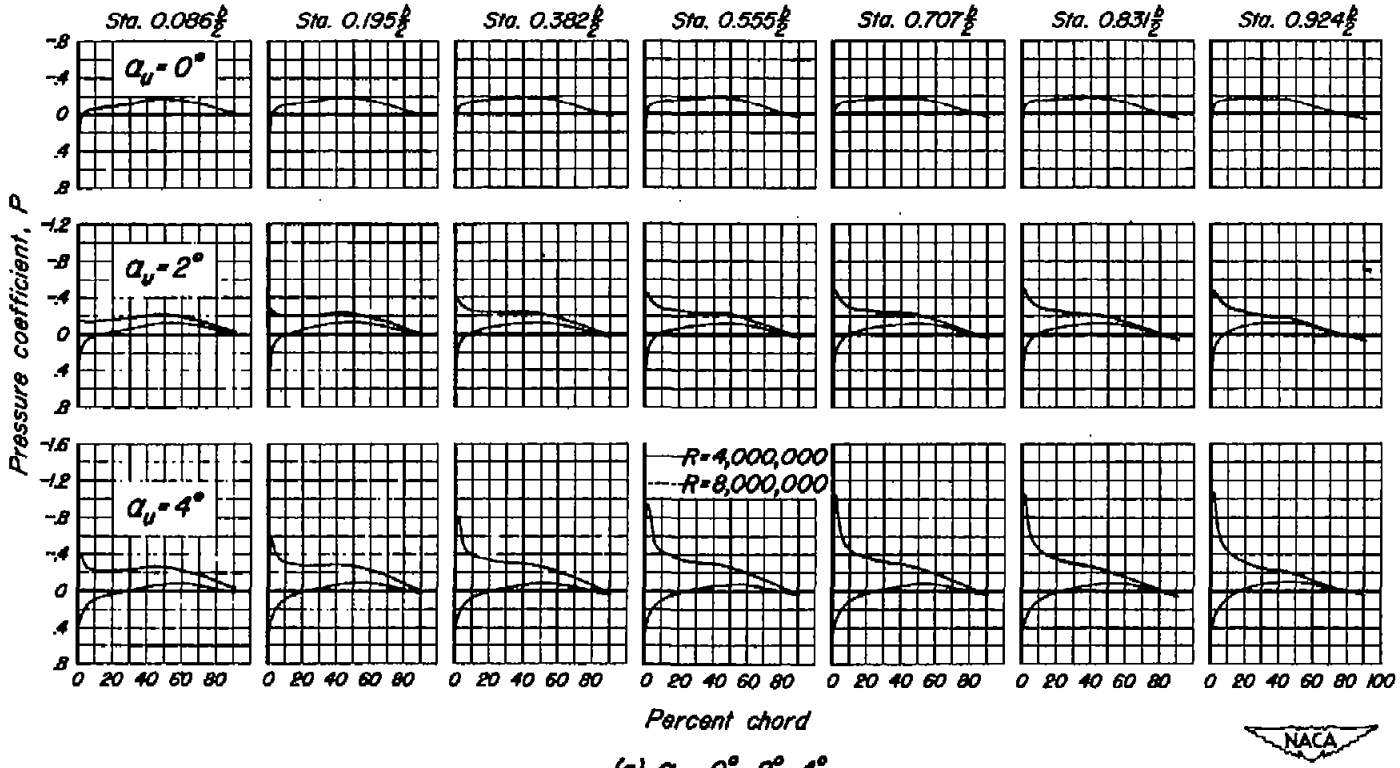
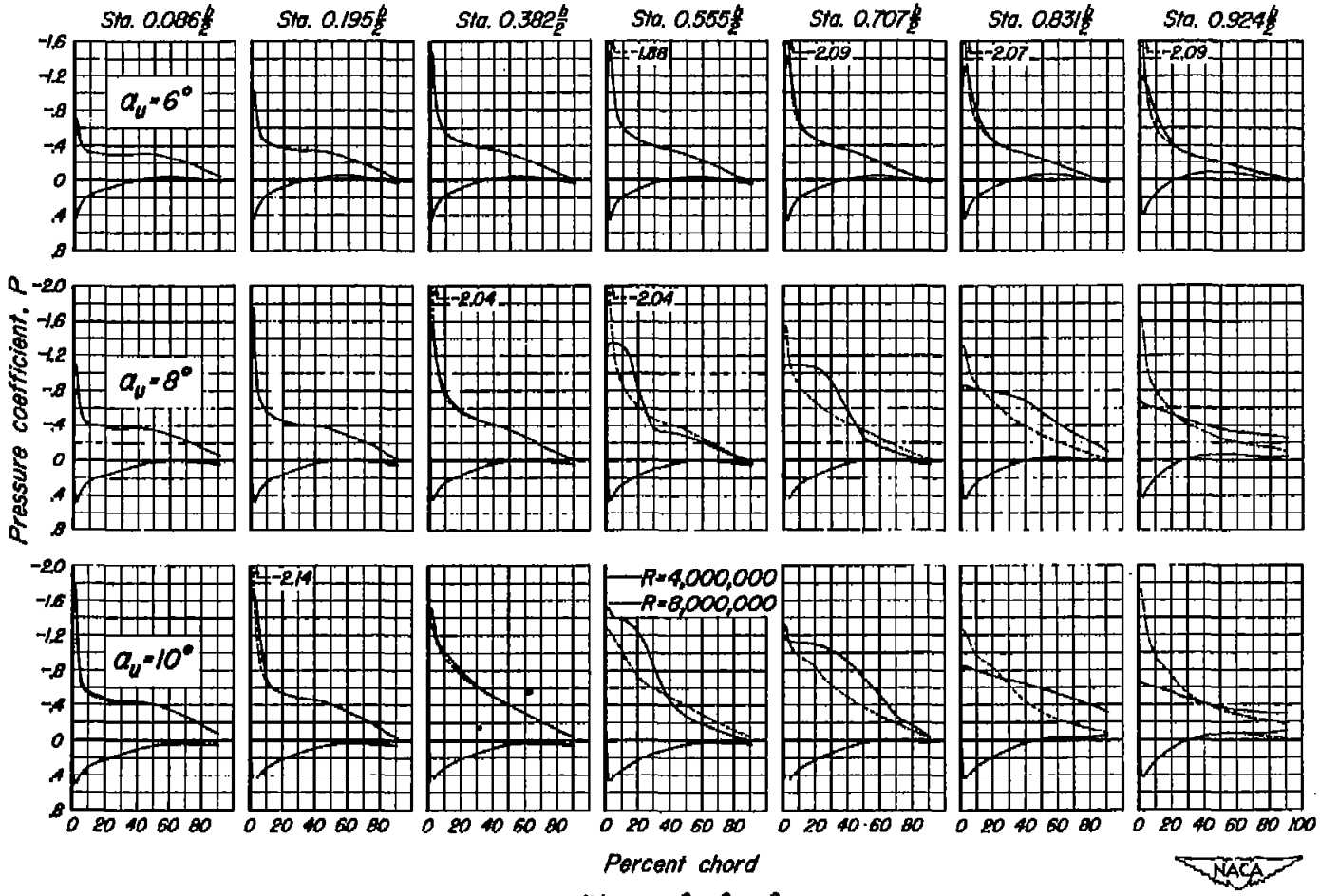


Figure 9.–The aerodynamic characteristics at Reynolds numbers of 4,000,000 and 8,000,000. M_∞, 0.60.



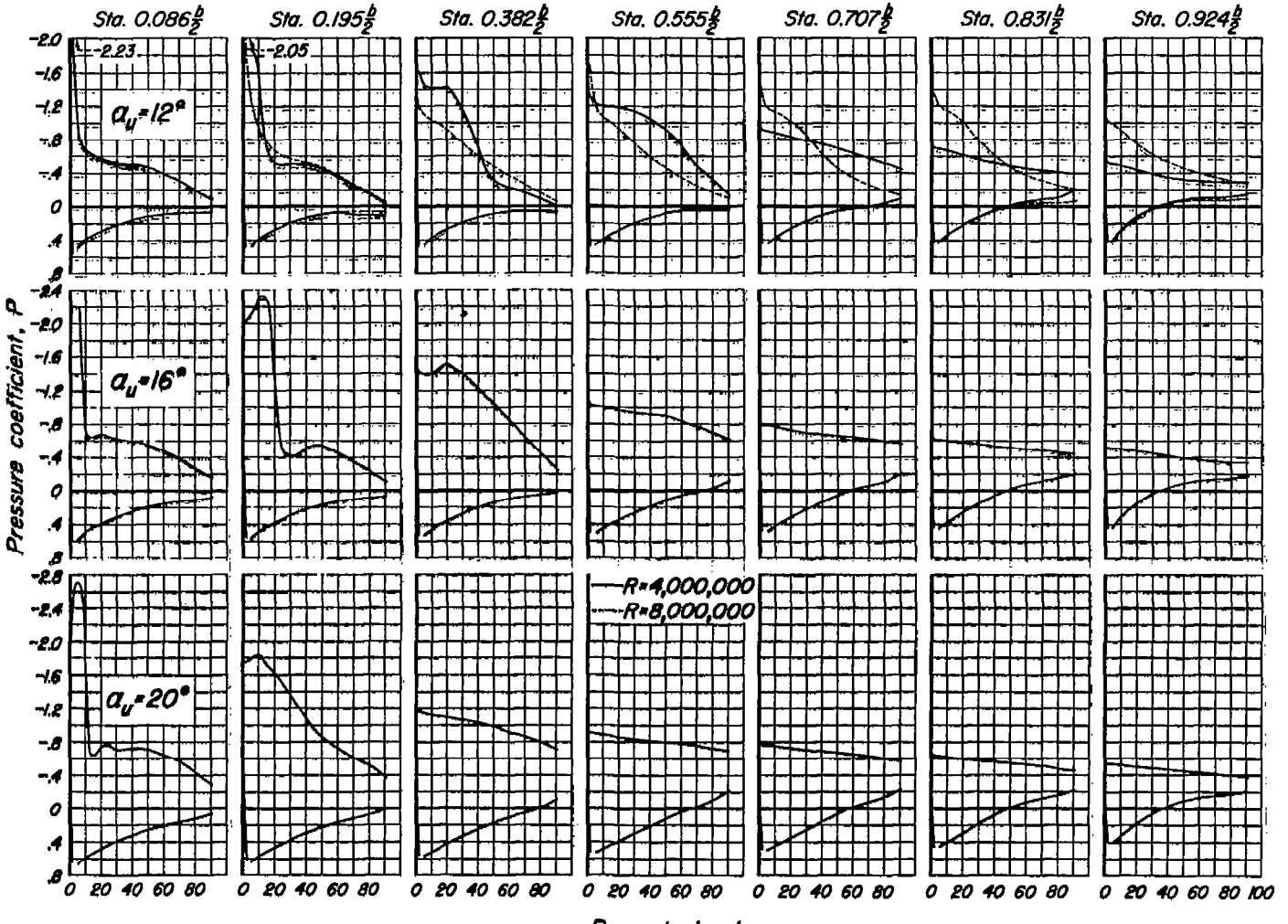
(a) α_u, 0°, 2°, 4°

Figure 10.– The chordwise distribution of pressure coefficient at seven semispan stations for several angles of attack and Reynolds numbers of 4,000,000 and 8,000,000. M_∞, 0.60.



(b) α_u, 6°, 8°, 10°

Figure 10.– Continued.



(c) α_u, 12°, 16°, 20°

Figure 10.- Concluded.

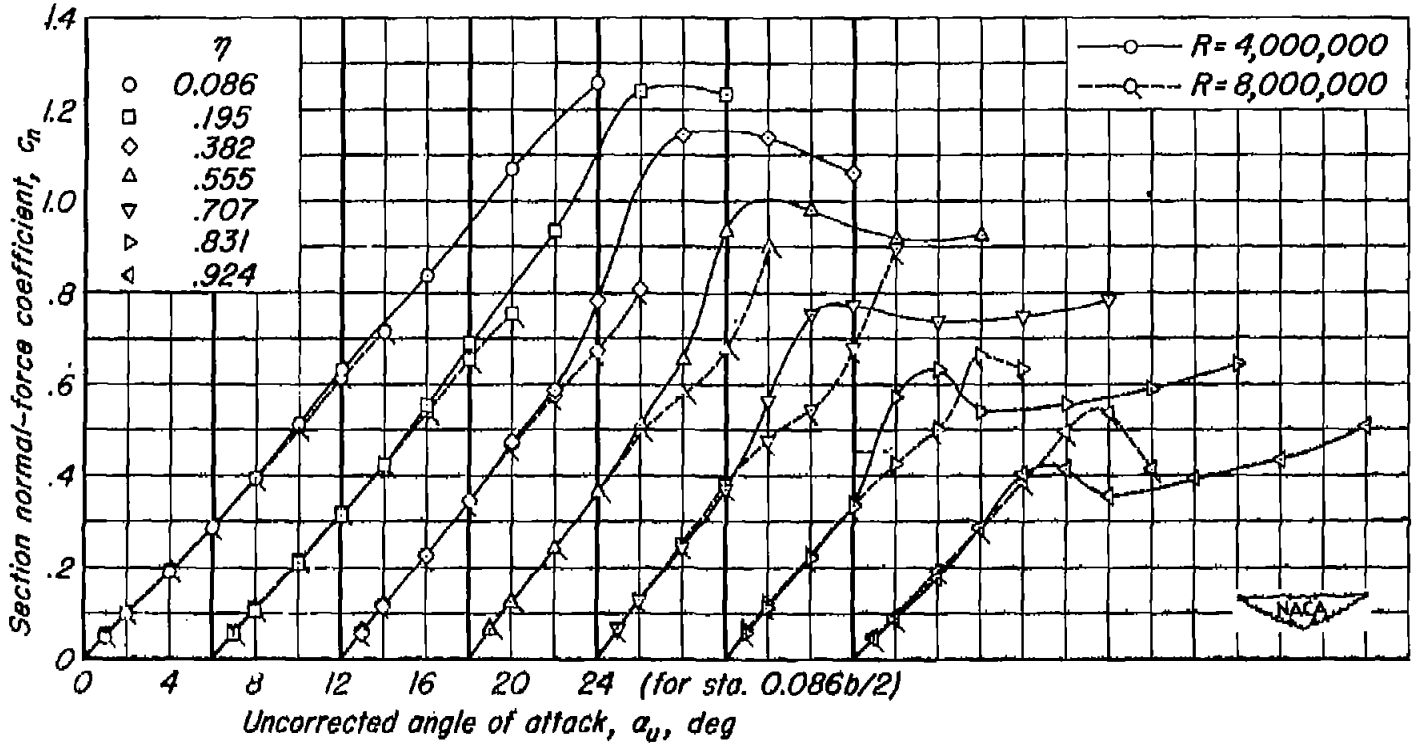


Figure 11.–The effect of Reynolds number on the section normal-force coefficients at seven semispan stations. M_o, 0.60.

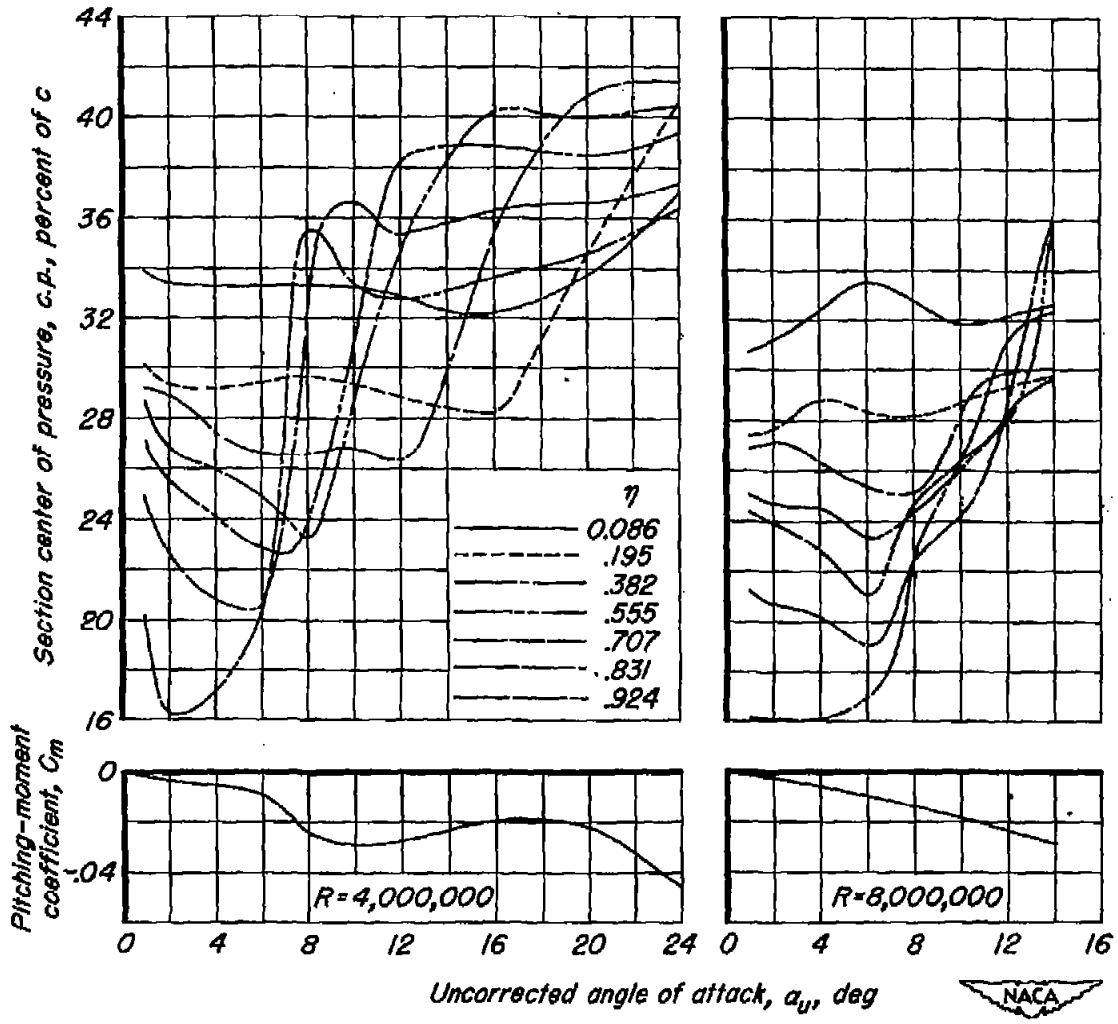


Figure 12.–The variation of the section centers of pressure and the pitching-moment coefficient with angle of attack for Reynolds numbers of 4,000,000 and 8,000,000. M_o, 0.60.

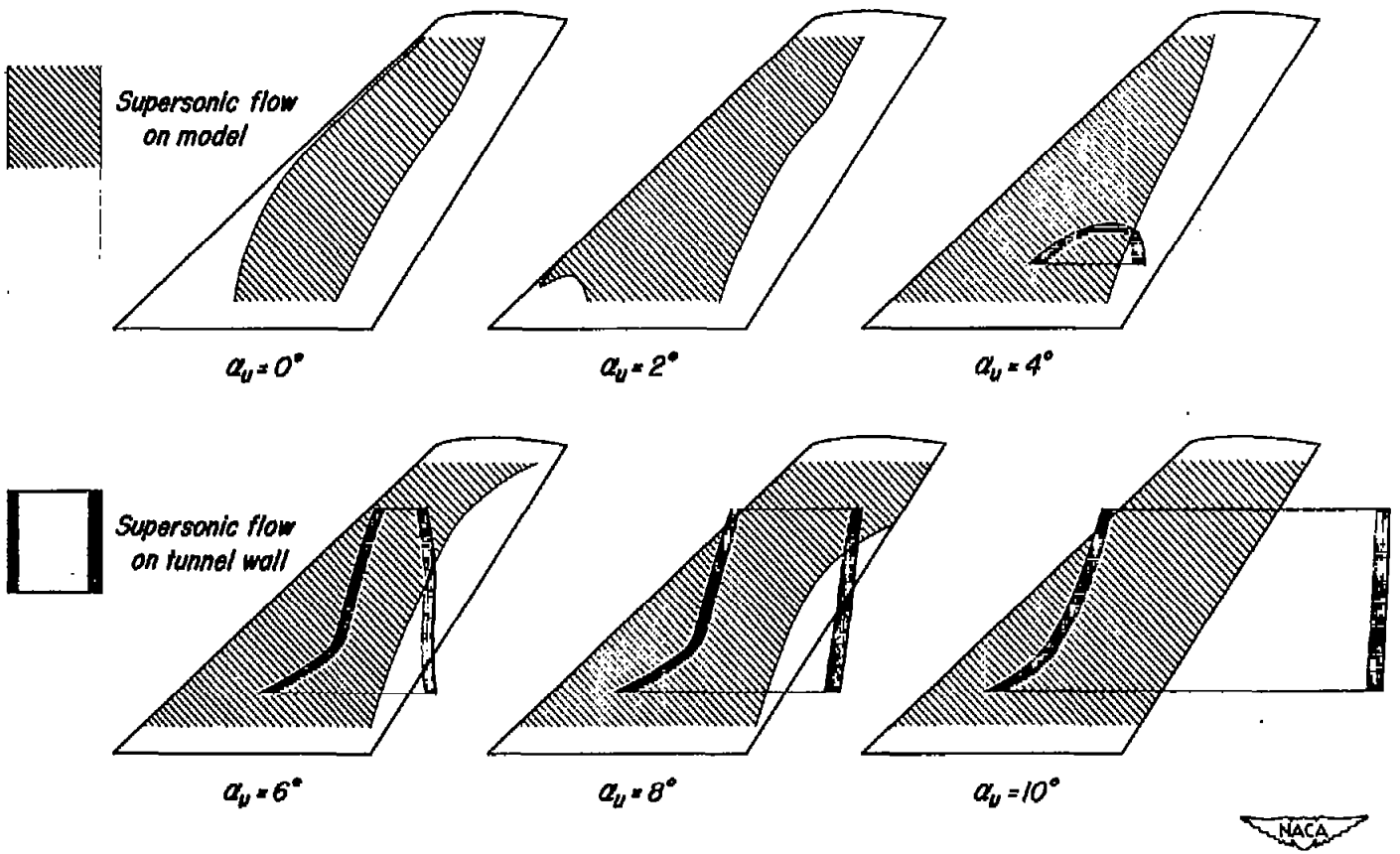
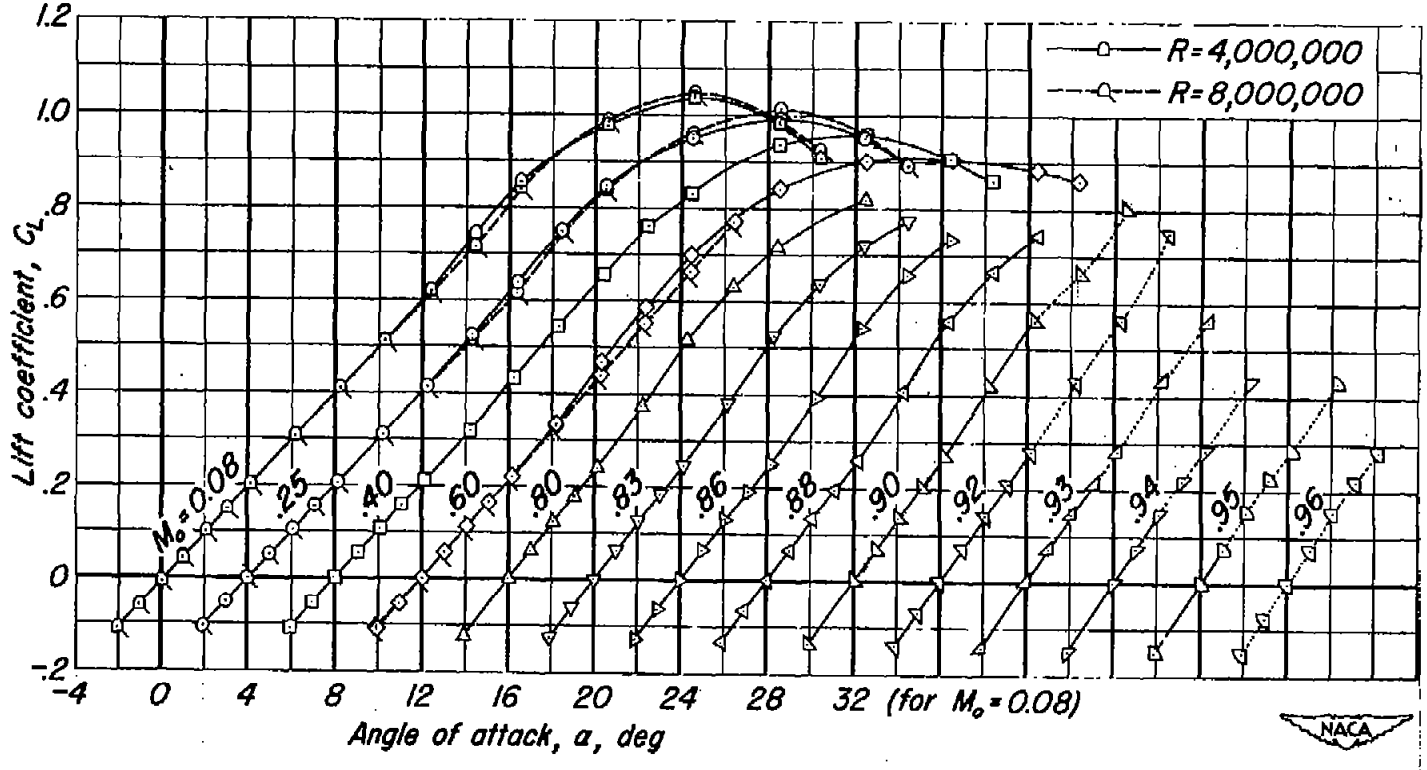
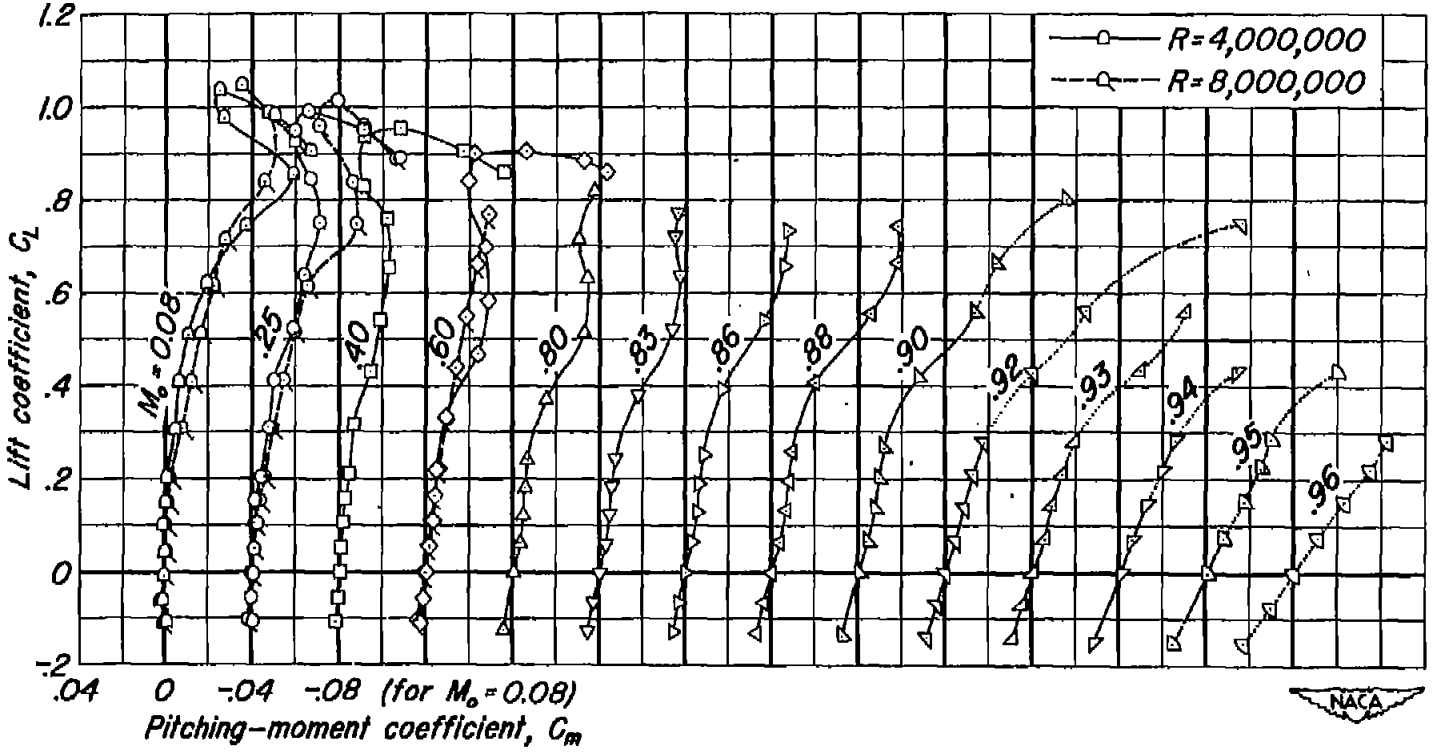


Figure 13.–The development of supersonic flow on the upper surface of the model and on the tunnel wall with increasing angle of attack. M_o, 0.92; R, 4,000,000.



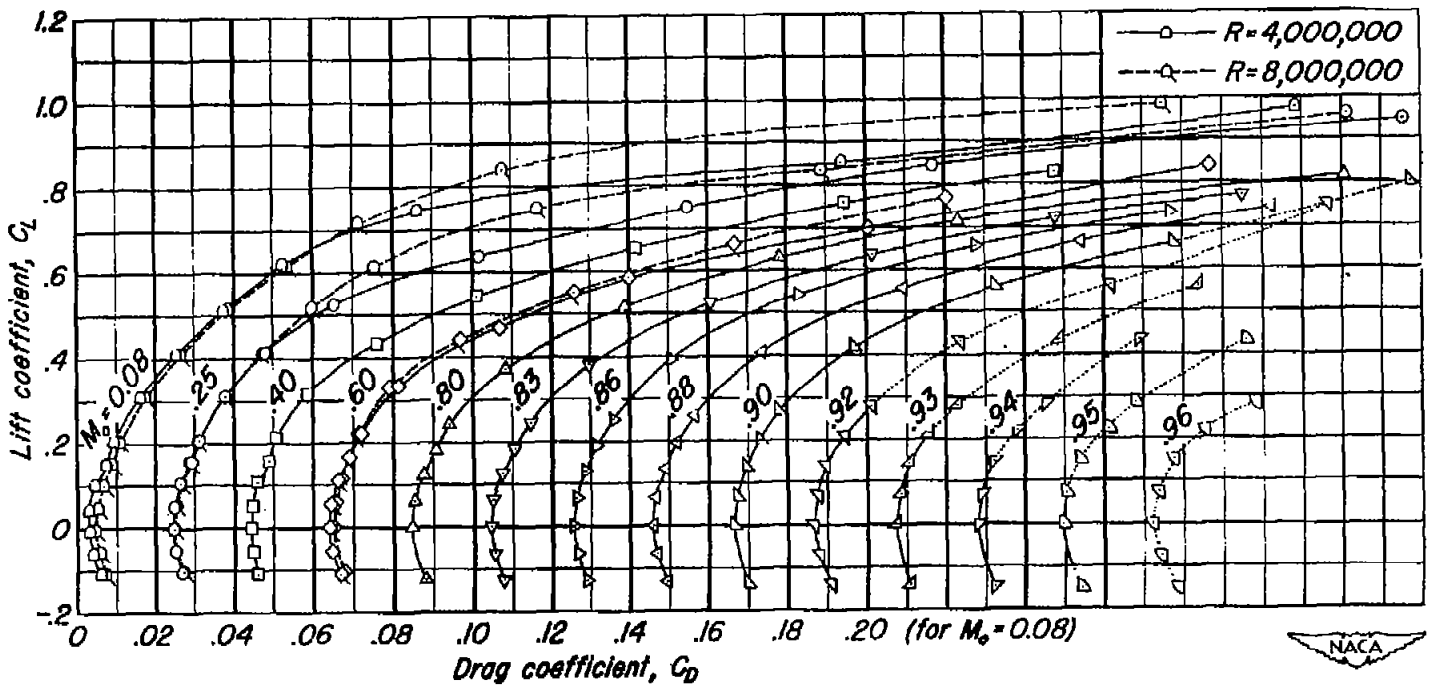
(a) C_L vs α

Figure 14.- The effect of Mach number on the aerodynamic characteristics.



(b) C_L vs C_m

Figure 14.- Continued.



(c) C_L vs C_D

Figure 14.-Concluded.

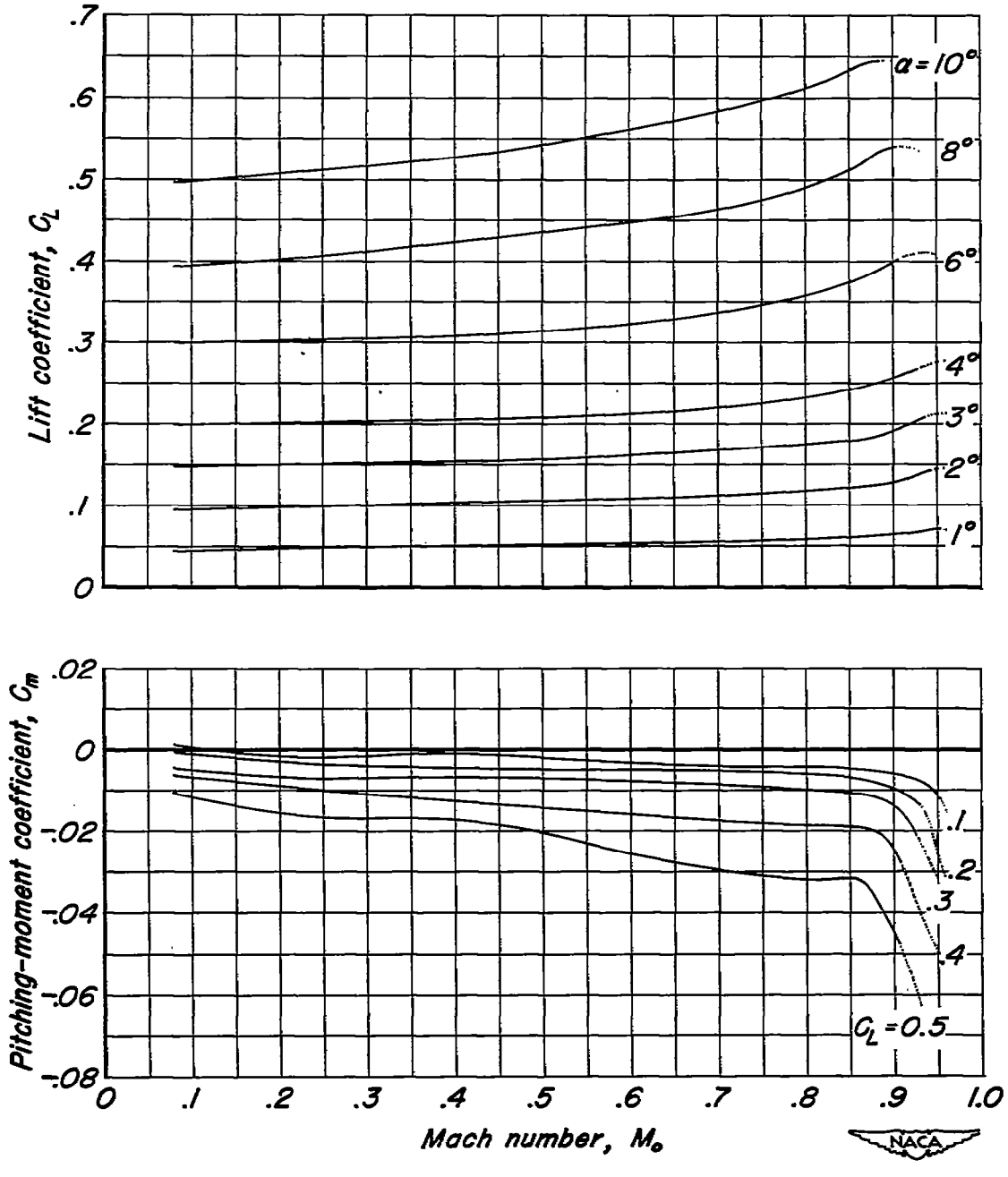


Figure 15.—The variation of the lift and pitching-moment coefficients with Mach number. R, 4,000,000.

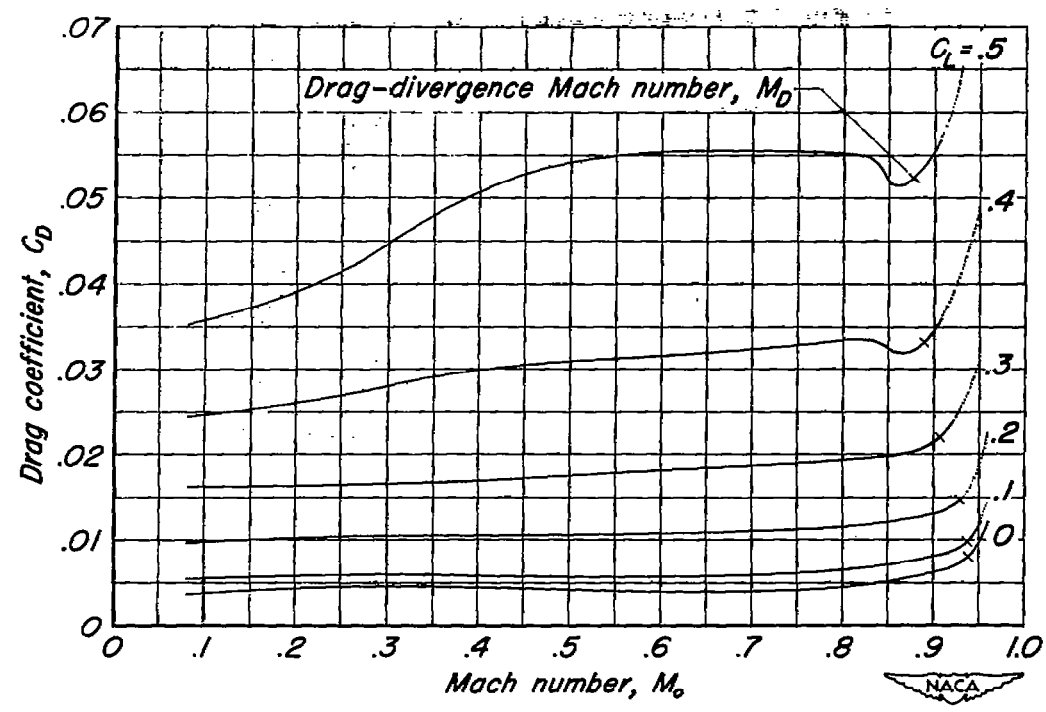


Figure 16.—The variation of the drag coefficient with Mach number. R, 4,000,000.

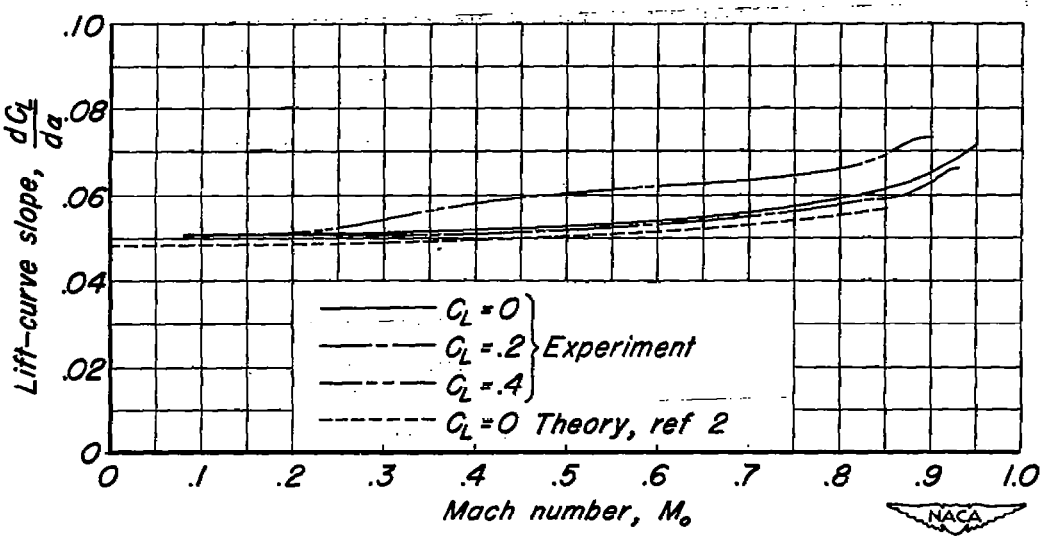


Figure 17.—The variation of the lift-curve slope with Mach number. R, 4,000,000.

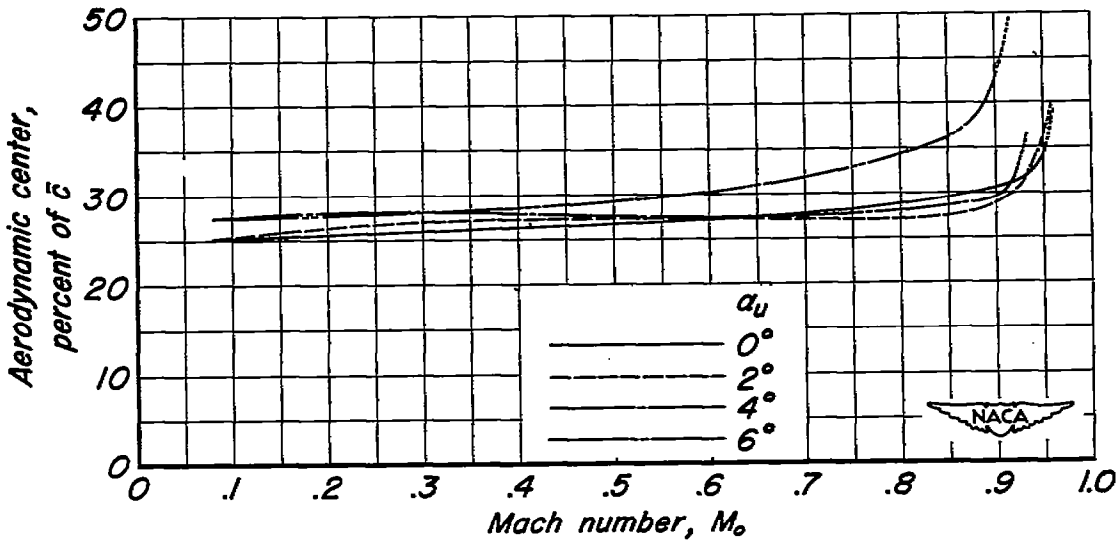


Figure 18.—The variation of the location of the aerodynamic center with Mach number. R, 4,000,000.

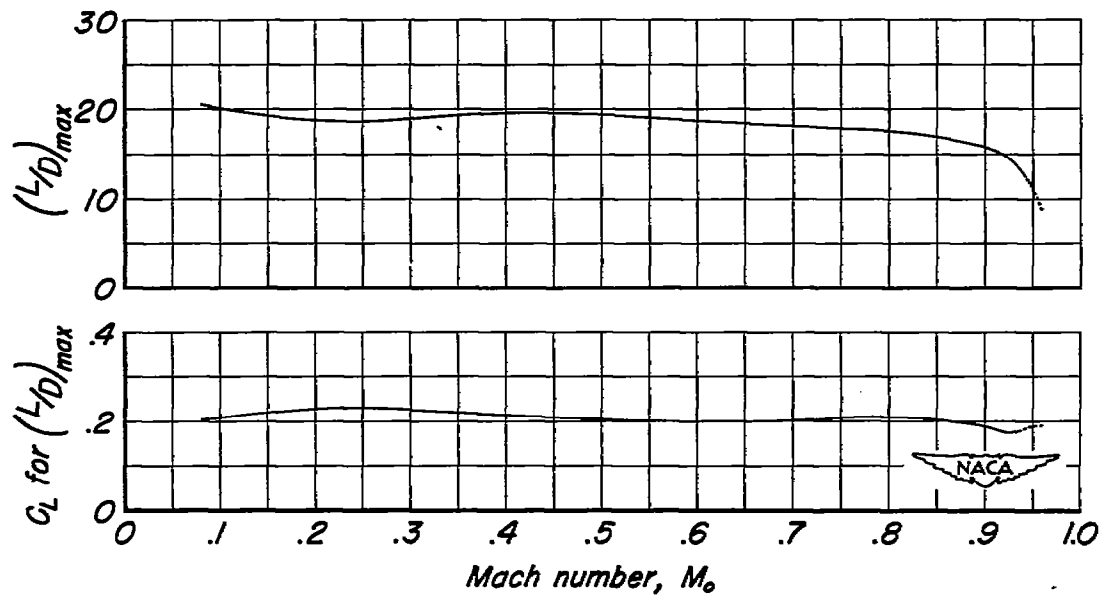
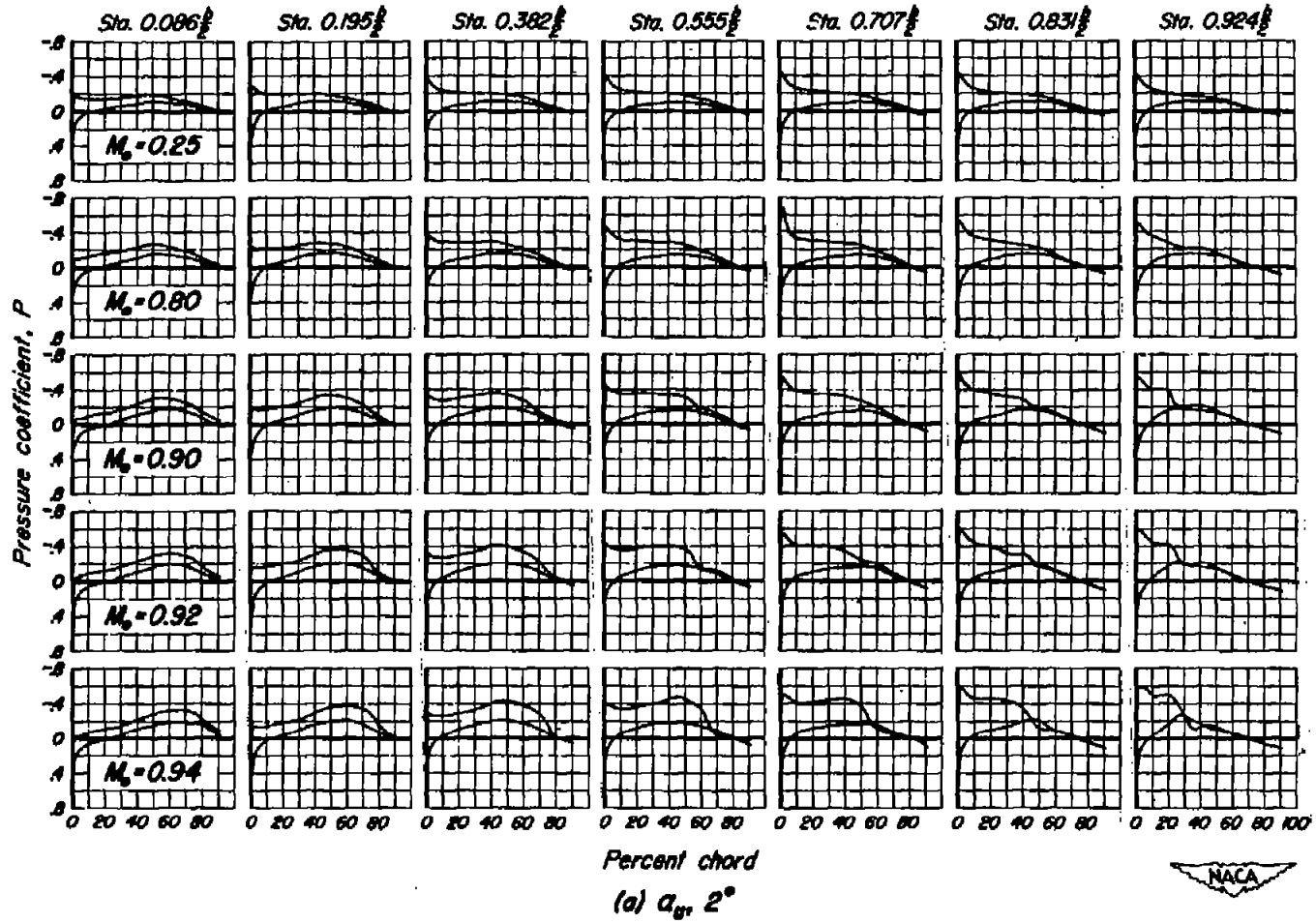
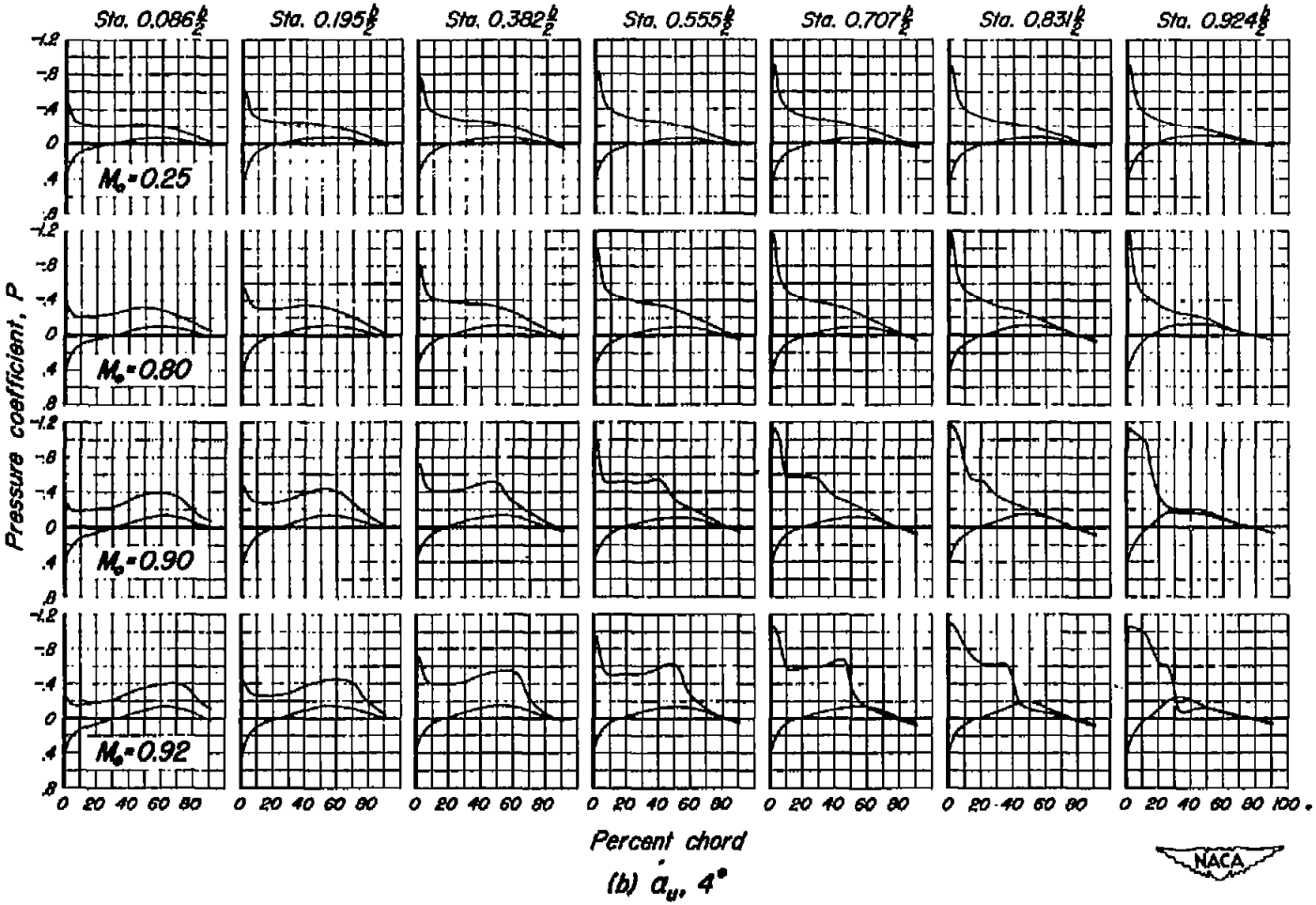


Figure 19.—The variation of the maximum lift-to-drag ratio and the lift coefficient for the maximum lift-to-drag ratio with Mach number. R, 4,000,000.



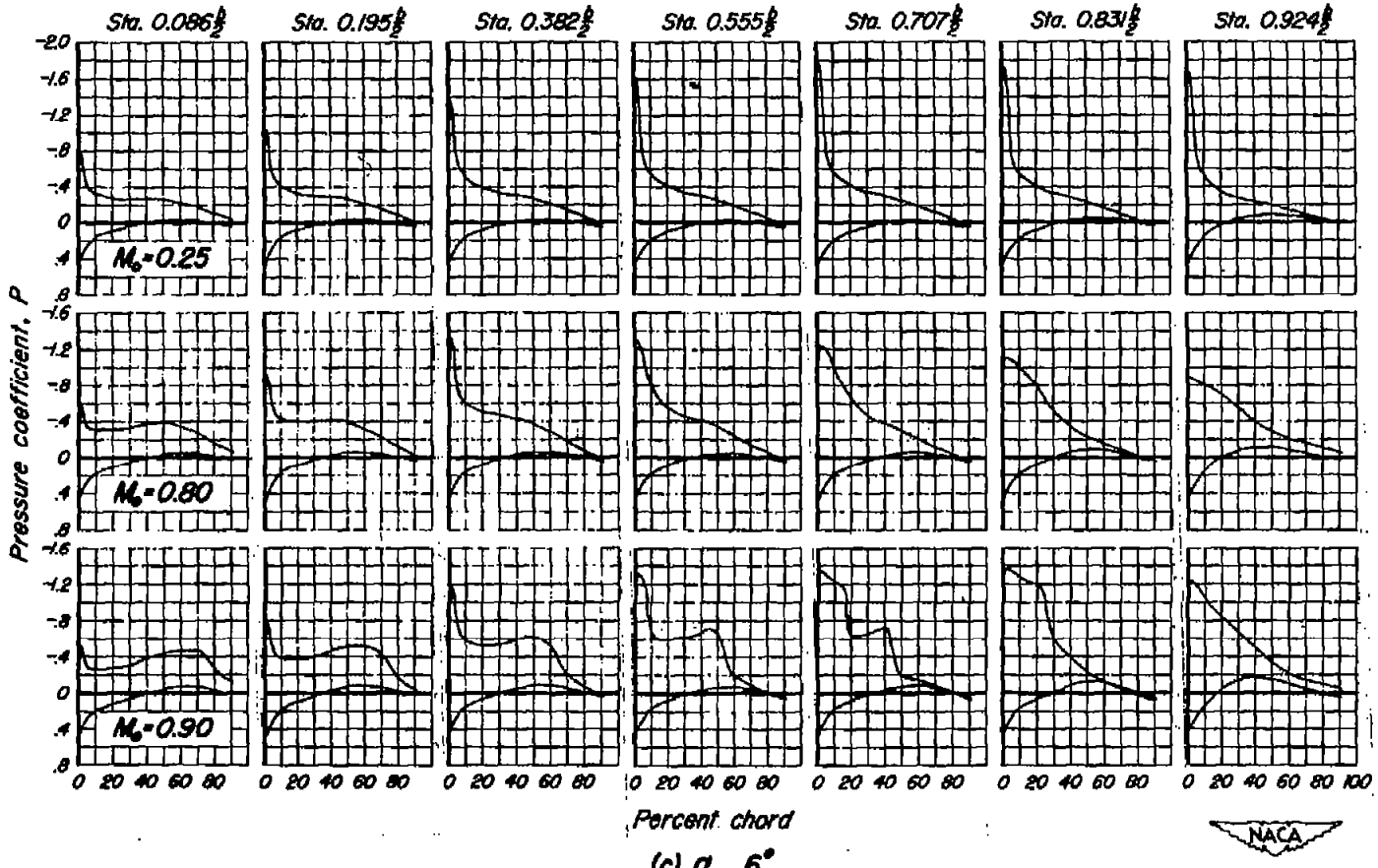
(a) α_g, 2°

Figure 20.– The chordwise distribution of pressure coefficient at seven semispan stations for several Mach numbers. R, 4,000,000.



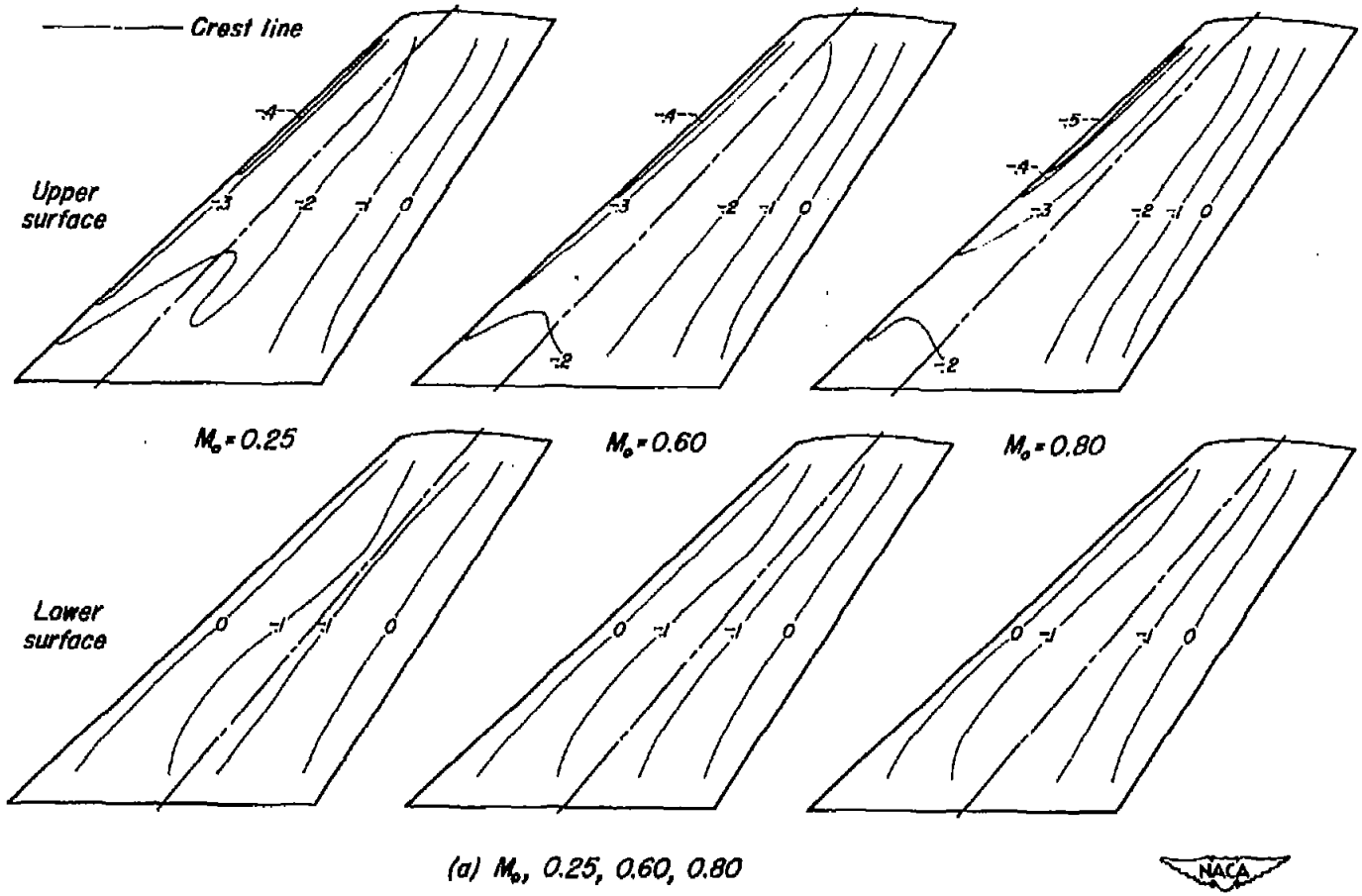
(b) α_u, 4°

Figure 20.- Continued.



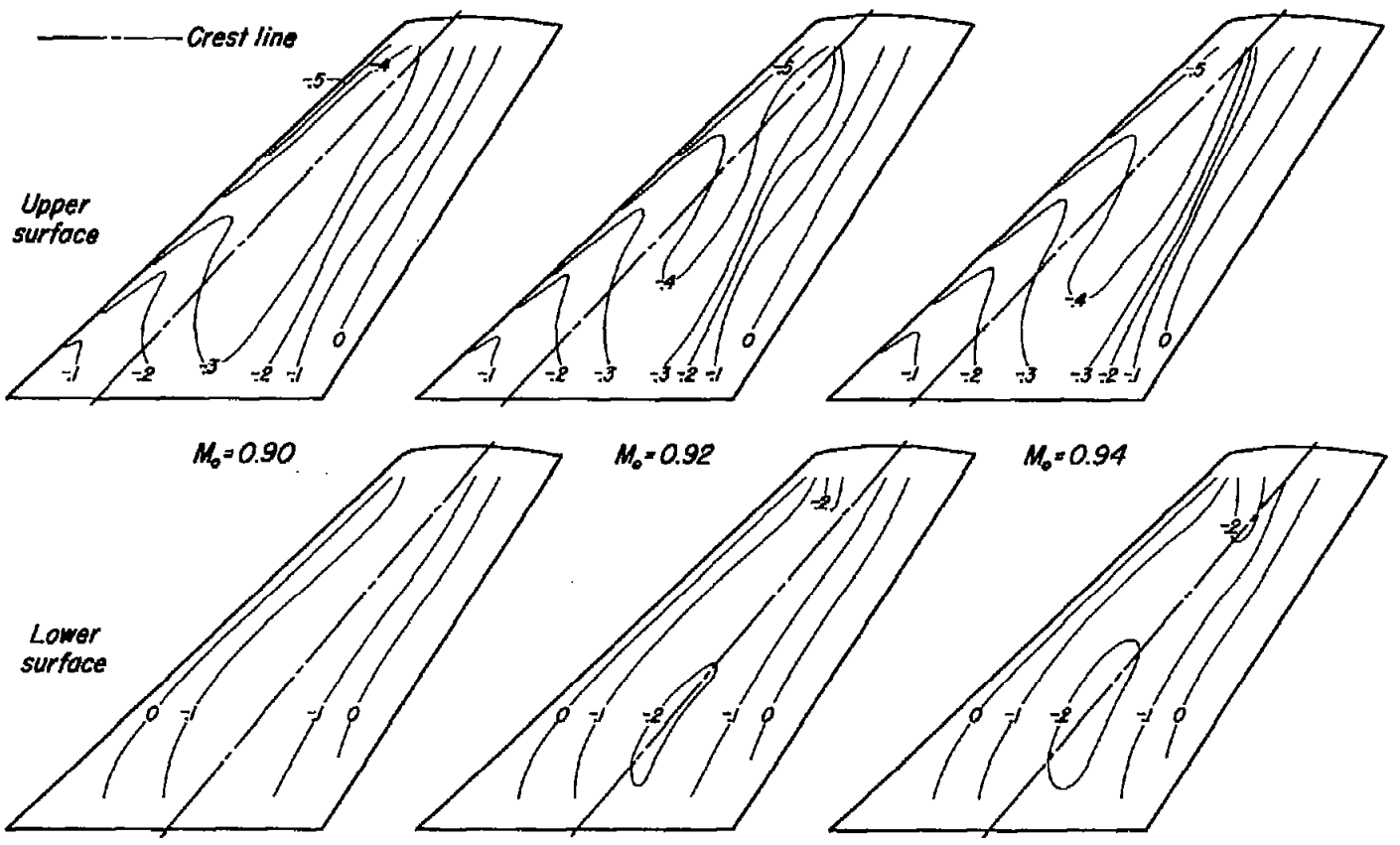
(c) α_u, 6°

Figure 20.- Concluded.



(a) M_o, 0.25, 0.60, 0.80

Figure 21.- The lines of constant pressure coefficient on the upper and lower surfaces for several Mach numbers. a_u, 2°; R, 4,000,000.



(b) M_o, 0.90, 0.92, 0.94

Figure 21.–Concluded.

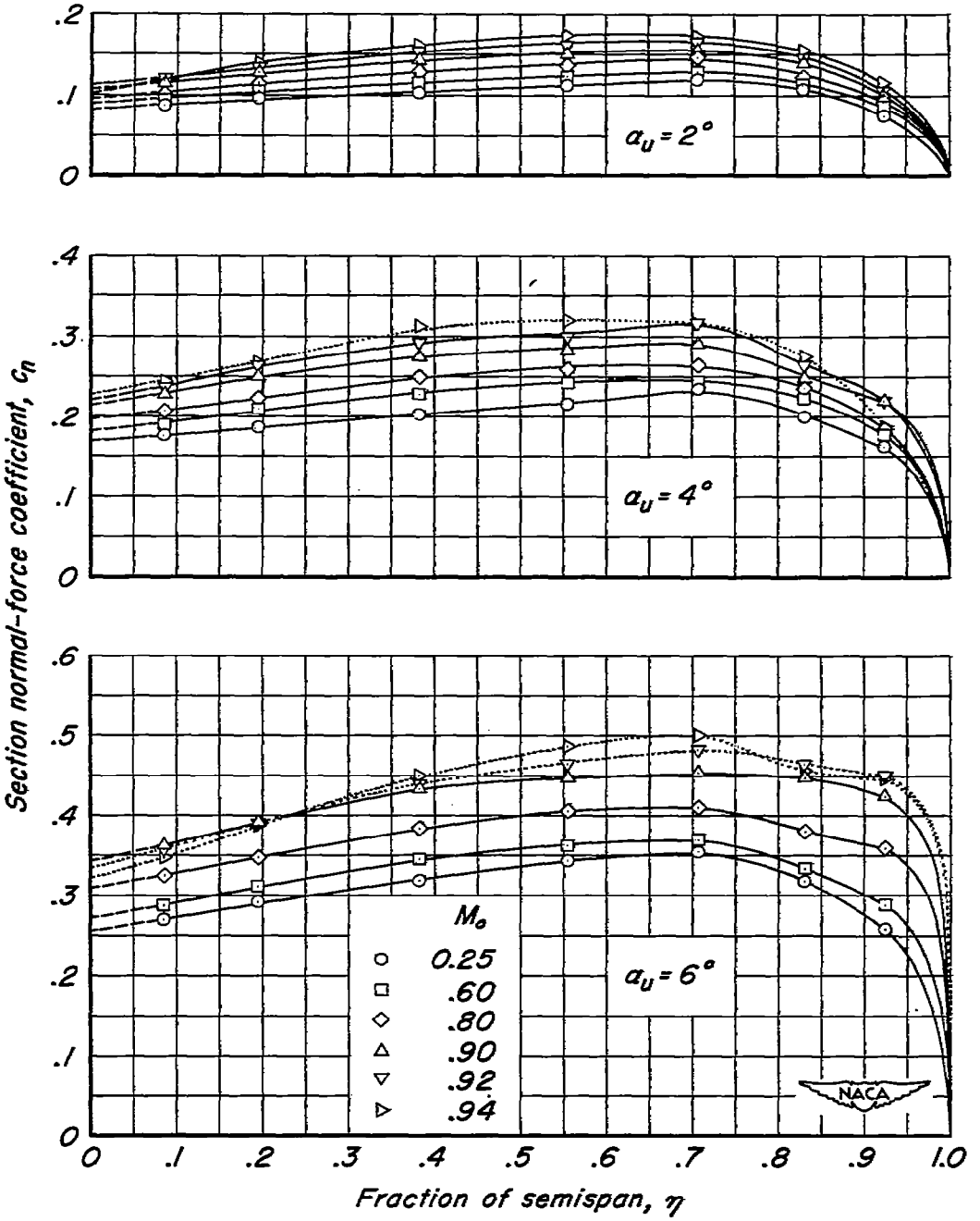


Figure 22.–The spanwise distribution of section normal-force coefficient at several Mach numbers for three angles of attack. R, 4,000,000.

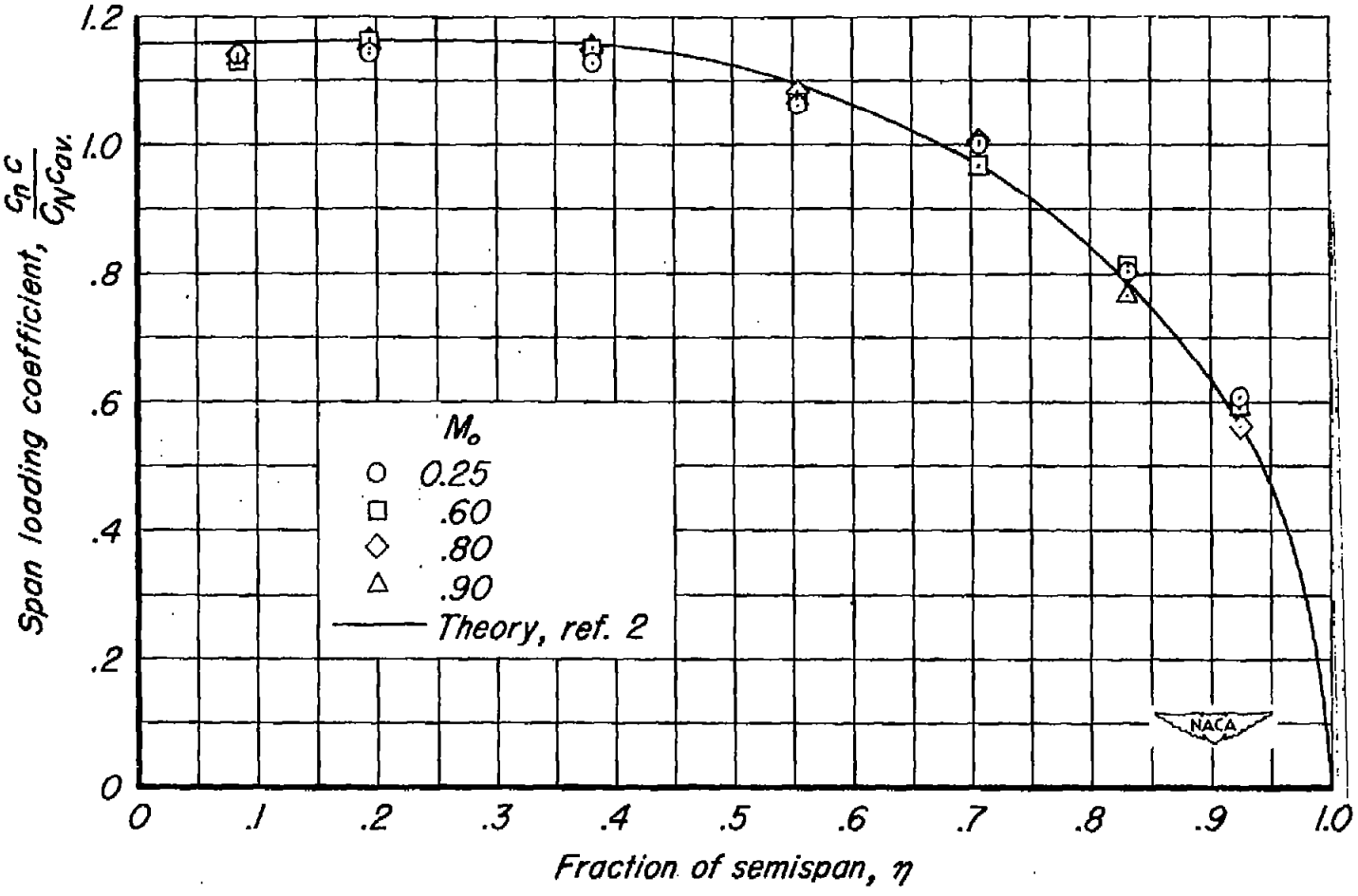


Figure 23.-The spanwise distribution of loading coefficient at several Mach numbers. R, 4,000,000.

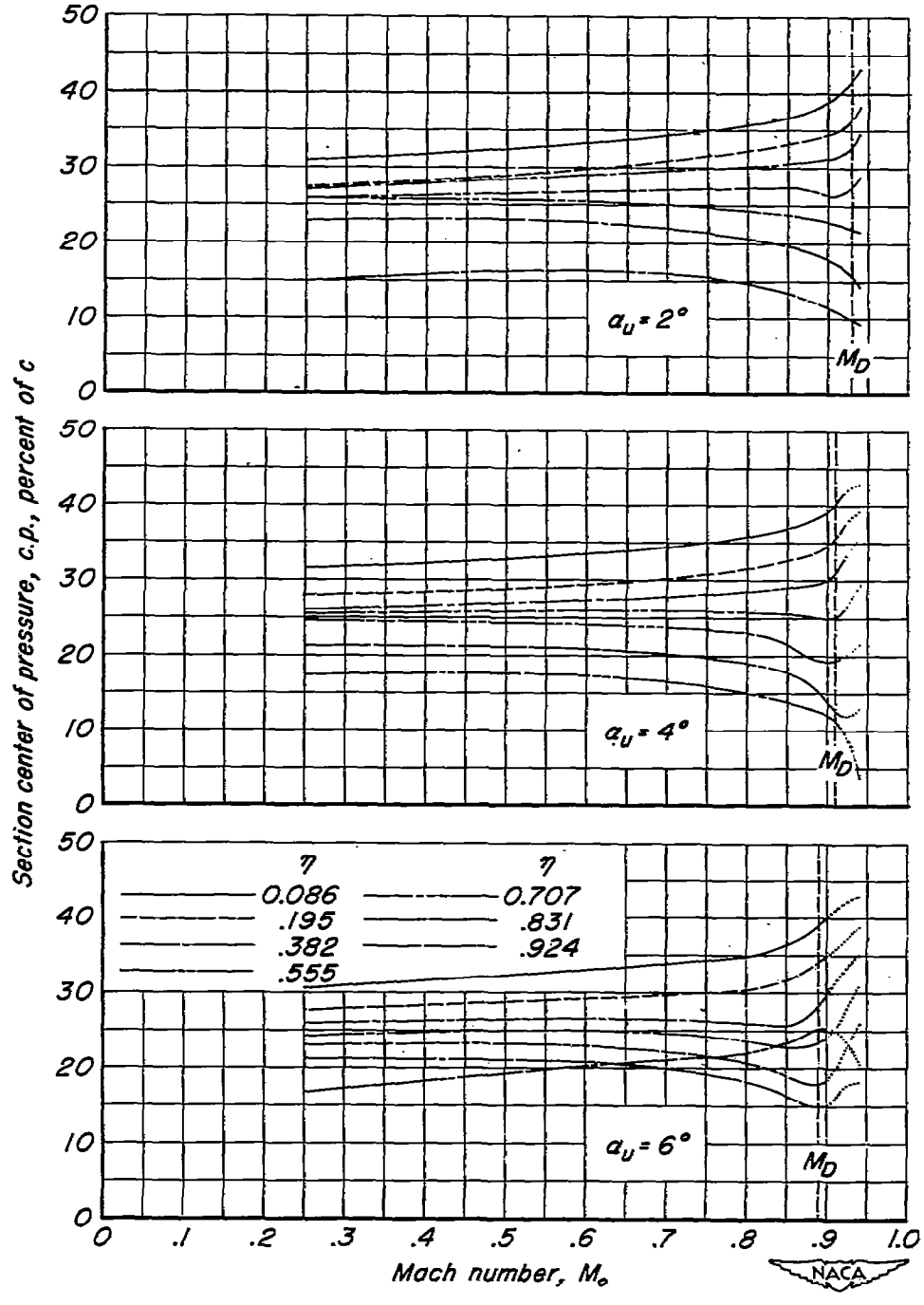
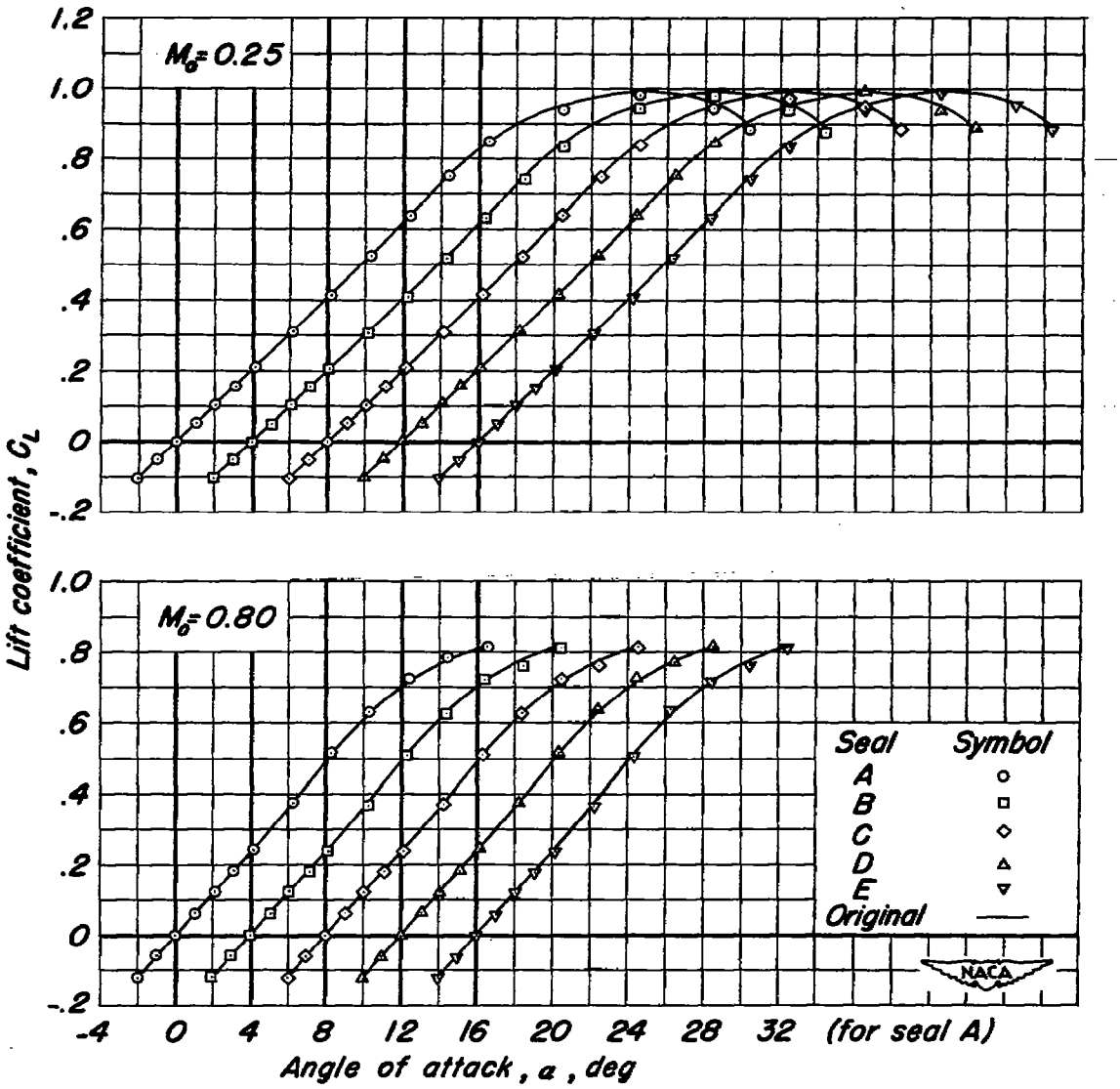
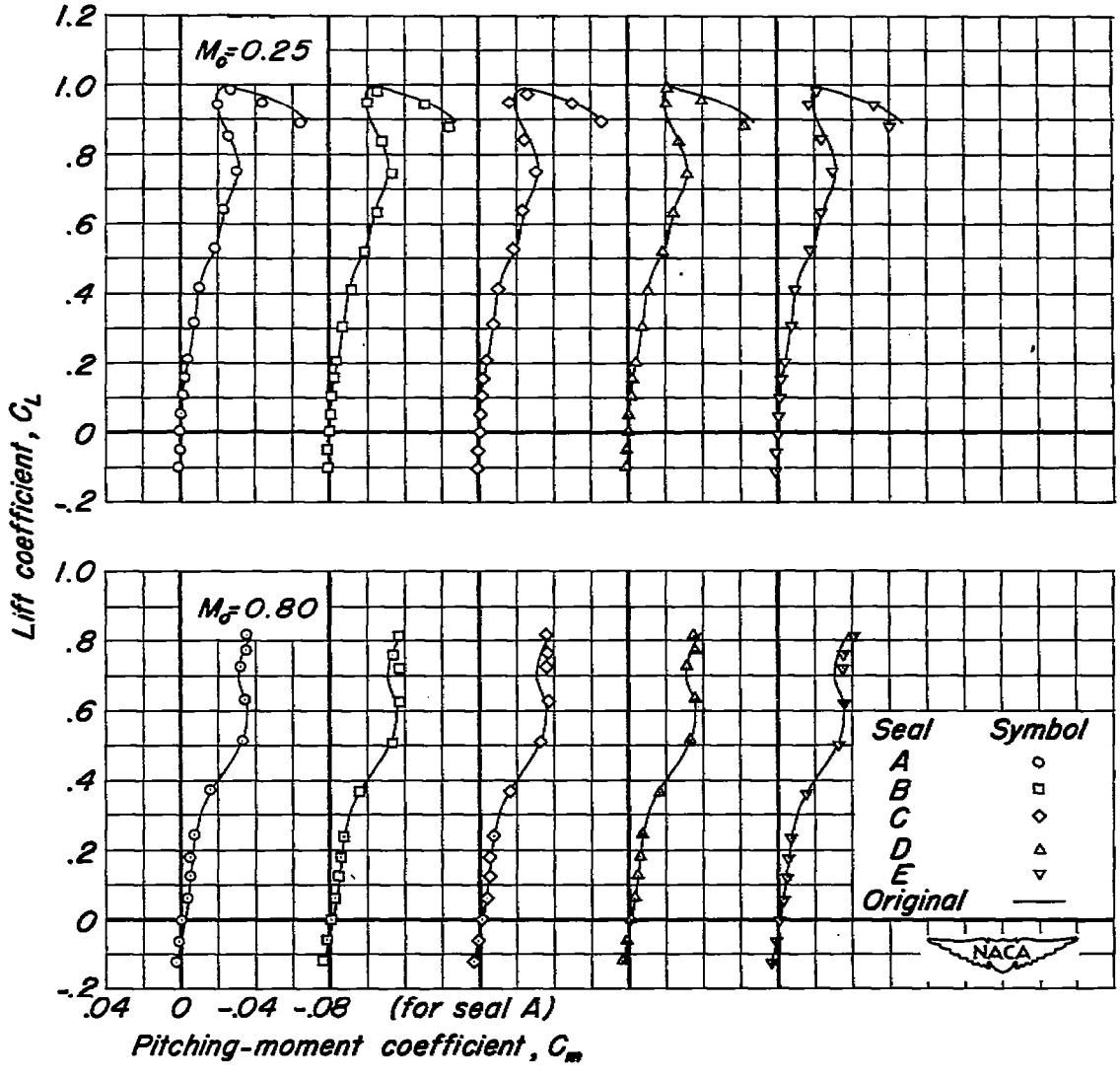


Figure 24.—The variation of the section centers of pressure with Mach number for three angles of attack. R, 4,000,000.



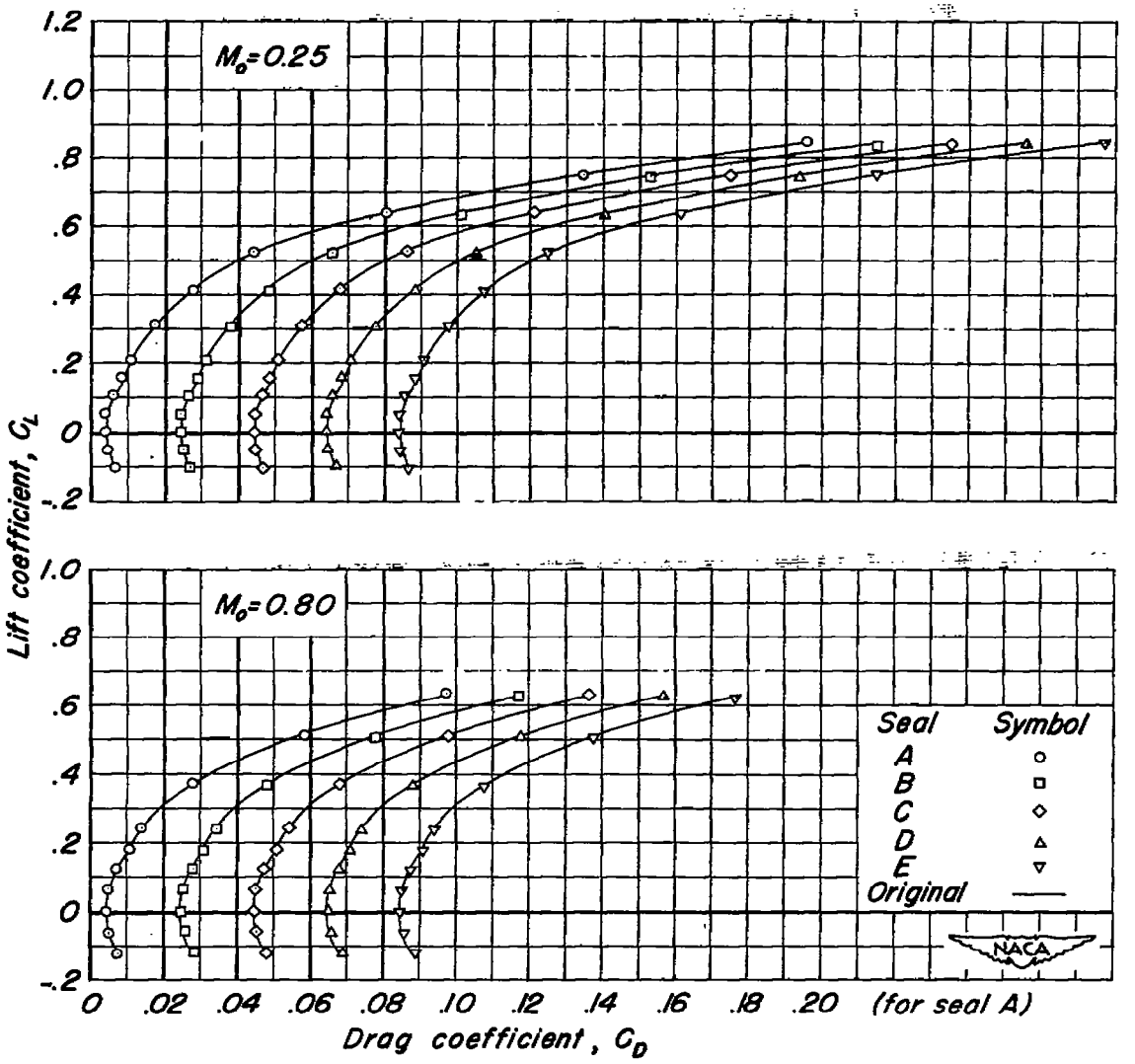
(a) C_L vs α

Figure 25.- The effect of various seals at the base of the model on the aerodynamic characteristics at Mach numbers of 0.25 and 0.80. R, 4,000,000.



(b) C_L vs C_m

Figure 25.–Continued.



(c) C_L vs C_D

Figure 25.- Concluded.

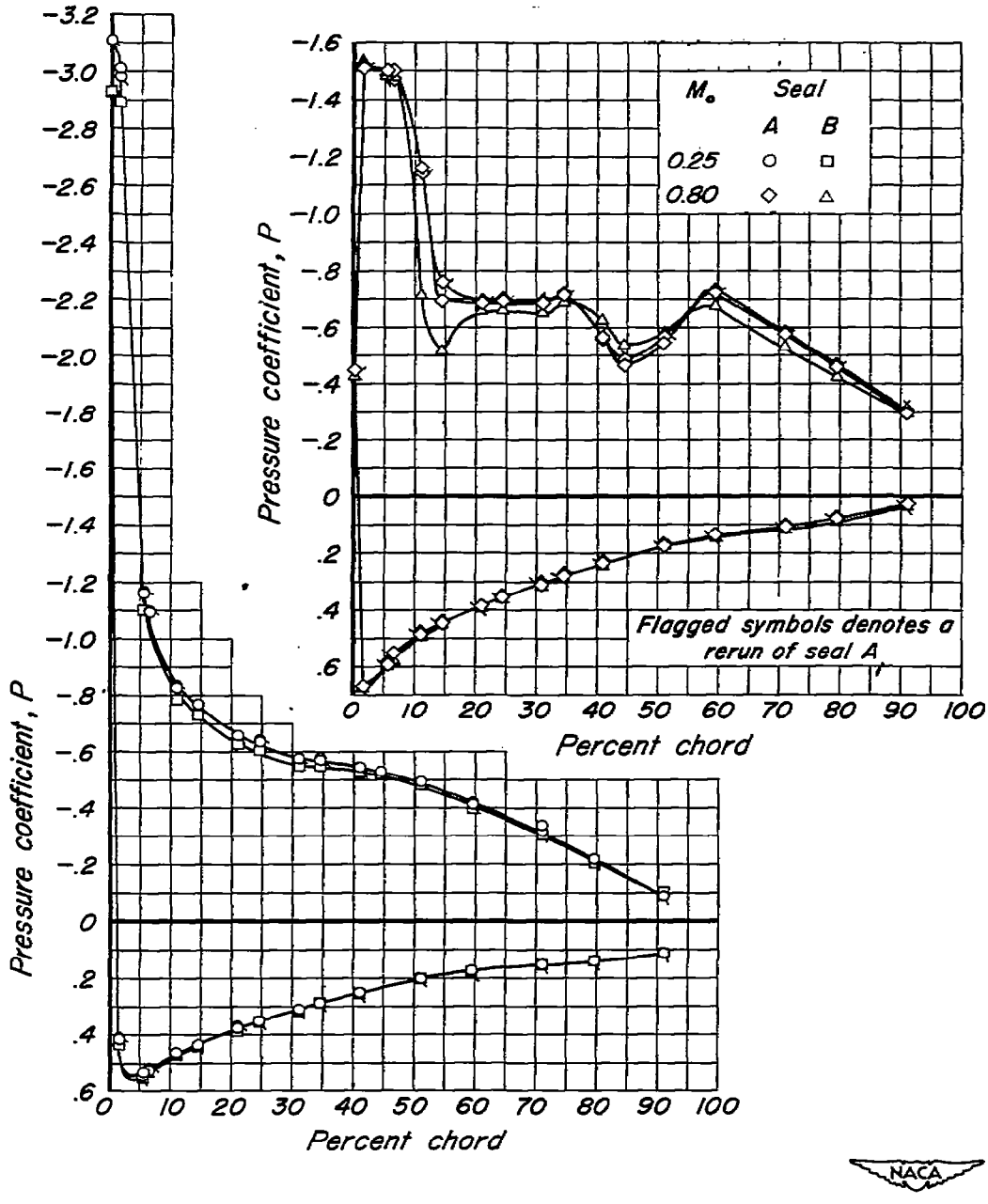


Figure 26.—The chordwise distribution of pressure coefficient at 0.086 b/2 for the model-turntable juncture seals A and B. α_u, 16°; R, 4,000,000.