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# RESEARCH MEMORANDUM

PRESSURE DISTRIBUTIONS OVER A SERIES OF RELATED AFTERBODY  
SHAPES AS Affected BY A PROPULSIVE JET  
AT TRANSONIC SPEEDS

By Beverly Z. Henry, Jr., and Maurice S. Cahn

Langley Aeronautical Laboratory  
Langley Field, Va.

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NATIONAL ADVISORY COMMITTEE  
FOR AERONAUTICS

WASHINGTON

January 22, 1957

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## PRESSURE DISTRIBUTIONS OVER A SERIES OF RELATED AFTERBODY

## SHAPES AS Affected BY A PROPULSIVE JET

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## SUMMARY

Investigations have been conducted at transonic speeds to determine the effects of a sonic propulsive jet on the aerodynamic characteristics of the body from which it issues. Presented herein are the pressure distributions over the related series of afterbody shapes used in these investigations.

These results indicate that the effects of the jet on body surface pressures will be confined to the rearmost 15 to 20 percent of the length for bodies with fineness ratios of the order of 10. On low-drag shapes, those with large extents of low-angle boattailing and small base sizes, the effect of the jet is to cause an increase in body pressures in the vicinity of the base, while on the blunt shapes the predominate effect was to reduce these local pressures within the range of this investigation. Increases in jet temperature from cold to 1,200° F resulted in local-pressure increases which were negligible on the low-drag shapes but became significant on the blunt shapes. Increasing stream Mach number tended to reduce the extent of body surface influenced by the jet.

## INTRODUCTION

Investigations have been conducted in the Langley 8-foot transonic tunnel to evaluate some of the effects of a sonic propulsive jet on the body from which it issues and to determine the influence of afterbody shape on these jet effects. All results were obtained at an angle of attack of 0° throughout the Mach number range from 0.80 to 1.10 and at each test point jet pressure ratio and temperature were varied. Initial results of the investigations have been reported in references 1 and 2. These papers present the variation with jet pressure ratio of base-pressure coefficient and afterbody-drag coefficient at different values

of stream Mach number and jet temperature for each of the configurations tested.

The results presented herein are the pressure-distribution measurements obtained over the bodies investigated. The pressure measurements are presented in coefficient form and have been tabulated for each afterbody at each test condition. These results are presented with limited analysis in order to expedite their availability to those concerned with afterbody-jet-exit design.

#### SYMBOLS

$C_p$	pressure coefficient, $\frac{p_l - p_\infty}{q_\infty}$
M	Mach number
R	Reynolds number, based on body length
d	diameter
l	length
p	static pressure
$p_t$	total pressure
q	dynamic pressure, $\frac{1}{2}pM^2$
t	total temperature, °F
$\beta$	afterbody boattail angle, deg
$\gamma$	ratio of specific heats

#### Subscripts:

b	base
j	jet
$\infty$	free stream
l	local
max	model maximum

## APPARATUS AND TESTS

### Wind Tunnel

These investigations were conducted in the Langley 8-foot transonic tunnel which has a dodecagonal, slotted test section that permitted continuous testing up to a Mach number of approximately 1.10 for these models. The tunnel is vented to the atmosphere through an air-exchange tower which permits the exhausting of combustion gases from the model into the stream with no detrimental effects on the characteristics of the stream. Maximum deviation from the indicated free-stream Mach number is  $\pm 0.003$  (ref. 3).

### Models

The models used in these investigations were bodies of revolution, the rear portions of which were removed to provide an exit for the jet. These bodies had fineness ratios from 10.0 to 10.7. A single forebody (see table I) was used throughout and the model design allowed the ready interchange of afterbodies of various geometric shape. The models were mounted in the tunnel by means of two support struts. These support struts, with a chord of 11.25 inches and an NACA 65-010 airfoil section measured parallel to the airstream, were placed so that the leading edge intersected the body at a point 21.7 inches from the nose and were swept back  $45^\circ$ . A sketch of the general arrangement of the model in the tunnel is shown in figure 1.

Presented in table II is the equation utilized to define the external shapes of the afterbodies investigated. Also shown are the design points used to assign values to the equation. The ordinates from which the body shapes were constructed are given in table I. Drawings of the afterbody shapes are shown in figure 2. The models were instrumented with base-pressure orifices and with three rows of static-pressure orifices located at  $0^\circ$ ,  $45^\circ$ , and  $72^\circ$  from the plane of symmetry as shown in figure 1.

### Turbojet Simulator

Contained within the models was a device for the simulation of a turbojet exhaust which burns a mixture of ethylene and air and exhausts the combustion products through a sonic nozzle. Details of the simulator are given in reference 1.

### Tests and Measurements

The models were tested at an angle of attack of  $0^\circ$  throughout the Mach number range from 0.80 to 1.10. At each test Mach number the jet pressure ratio was varied from a no-flow condition to 11 or to the maximum obtainable at jet temperatures of "cold,"  $800^\circ F$ , and  $1,200^\circ F$ . The term "cold" flow is used herein to define the temperature of the air coming from the source, normally  $75^\circ$  to  $80^\circ F$ , and corresponds to a fuel-air ratio of 0. The Reynolds number based on body length varied from  $15.0 \times 10^6$  to  $17.4 \times 10^6$ . (See fig. 3.)

At each test point, body-pressure distributions, base pressures, and free-stream conditions were photographically recorded from multiple-tube manometers. Tunnel total temperature was obtained from a recording potentiometer.

Jet total pressure was obtained from a calibrated probe mounted in the combustion chamber and was referenced to a static-pressure orifice on the tunnel wall for the determination of jet pressure ratio. Jet temperature was obtained from a shielded chromel-alumel thermocouple near the exit station. All values defining the jet condition were photographically recorded by a camera synchronized with that used to record pressure data.

### RESULTS AND DISCUSSION

Presented in table III are the measured values of local-pressure coefficient at each test condition over each afterbody depicted in figure 2. Measured values of base-pressure coefficient for these afterbodies have been published in references 1 and 2. In table IV are presented the pressure distributions over the model forebody obtained in conjunction with afterbodies I and VI. These two configurations were arbitrarily chosen to indicate that large changes in conditions over the afterbody caused no change in the forebody distribution.

In figure 4 are presented the variations in local-pressure coefficient along the  $0^\circ$  meridian of each afterbody for several representative jet pressure ratios. This row has been selected as typical since it may be observed that over the rear portions of the bodies, downstream of the local flow field of the strut, the measurements are generally the same for each row within the experimental accuracy of the data (normally  $\pm 0.005$ ).

In the pressure distributions over afterbody II it will be seen that a displacement of the local pressures occurs rearward of the extension parting line. Since this displacement did not occur for the no-jet-flow

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condition, it may be assumed that the displacement is due to leakage through this juncture. The curves in figure 4(a) have consequently been faired accordingly.

As was noted in reference 2, at a Mach number of 1.10, a disturbance originating at the support-body juncture was reflected from the tunnel wall to strike the models at a point varying from about  $x/l_{\max} = 0.90$  to  $x/l_{\max} = 0.97$  depending on body length (approximately 1 to 4 jet diameters upstream of the base). This reflected disturbance resulted in more positive local pressures and, consequently, in lower drag values. While the absolute values of local-pressure coefficient are incorrect in the region of this disturbance, examination of the drag values indicated no alterations of the jet effects which could be attributed to the disturbance. It will be observed that the effect of this disturbance is more readily apparent on those bodies which have cylindrical shape or which closely approach this shape (see afterbodies X, XII, XIII, and XIV). It is on these bodies, however, that the drag contribution of the boattail is reduced in proportion to the contribution of the body base.

The effect of the jet is confined generally to the rearmost 15 to 20 percent of the body length. For the low-drag shapes, bodies with extensive low-angle boattailing ( $8^\circ$  to  $16^\circ$ ) and small base annulus sizes ( $d_j/d_b \approx 0.5$  or larger), external expansion of the jet at pressure ratios of about 3 and higher resulted in an outward deflection of the external stream which caused an increase in pressure over the rear portion of the bodies with the accompanying drag reduction (see, for example, afterbodies I and XI). For the blunt shapes, bodies with lesser extent of boattailing and large base sizes ( $d_j/d_b < 0.5$ ), the action of the jet was to aspirate the low-energy regions at the rear of these bodies to lower pressures with a resulting increase in drag (see, for example, afterbodies X, XII, and XIII). This unfavorable effect existed with large-based models even though the boattail angle was of a favorable magnitude and increased with increasing jet pressure ratio until the point was reached where the jet deflected the external stream in a favorable manner. The pressure ratio at which the jet interacts with the external stream is dependent on the size of the base annulus, being about 3 for small-based models similar to afterbody I and above the maximum obtainable during this investigation for a cylindrical shape such as afterbody X.

The effect of increasing jet temperature was generally to cause a pressure increase in the region of the body base. For the low-drag shapes, this effect was so small as to be considered negligible. For the blunt shapes, however, the effects of changes in temperature became significant.

Reference 2 indicated that no major variation in the character of the jet effects on drag resulted due to changes in stream Mach number within the range of this investigation. The pressure distributions evidence a trend towards a lesser extent of the body surface being affected as the Mach number was increased.

#### CONCLUDING REMARKS

From pressure-distribution measurements made over the surfaces of a related series of afterbodies as influenced by a propulsive jet, the following observations are made:

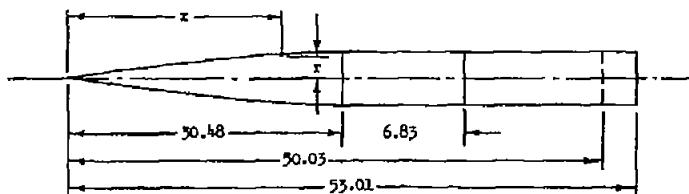
1. The effect of the jet on local body-surface pressures was confined generally to the rearmost 15 to 20 percent of the length for bodies with fineness ratios of the order of 10.
2. For bodies with large extents of low-angle boattailing and small base sizes, the effect of the jet was to increase the local pressure in the vicinity of the base.
3. For bodies with lesser extents of boattailing and large base sizes, the predominate effect of the jet within the range of this investigation was to reduce the local pressures in the vicinity of the base.
4. Increasing jet temperature from cold to 1,200° F resulted in a local-pressure increase which was negligible for the low-drag shapes but which became significant for the more blunt shapes.
5. Increases in stream Mach number tended to reduce the extent of body surface influenced by the jet.

Langley Aeronautical Laboratory,  
National Advisory Committee for Aeronautics,  
Langley Field, Va., October 19, 1956.

## REFERENCES

1. Henry, Beverly Z., Jr., and Cahn, Maurice S.: Preliminary Results of an Investigation at Transonic Speeds To Determine the Effects of a Heated Propulsive Jet on the Drag Characteristics of a Related Series of Afterbodies. NACA RM L55A24a, 1955.
2. Henry, Beverly Z., Jr., and Cahn, Maurice S.: Additional Results of an Investigation at Transonic Speeds To Determine the Effects of a Heated Propulsive Jet on the Drag Characteristics of a Series of Related Afterbodies. NACA RM L56G12, 1956.
3. Ritchie, Virgil S., and Pearson, Albin O.: Calibration of the Slotted Test Section of the Langley 8-Foot Transonic Tunnel and Preliminary Experimental Investigation of Boundary-Reflected Disturbances. NACA RM L51K14, 1952.

TABLE I.- BODY ORDINATES



## Forebody Ordinates

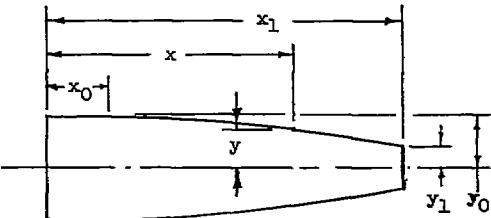
Station, x, in.	Radius, r, in.	Station, x, in.	Radius, r, in.
0.50	0.139	12.00	1.054
.45	.179	15.00	2.079
.75	.257	18.00	2.245
1.50	.433	21.00	2.360
3.00	.725	24.00	2.458
4.50	.968	27.00	2.486
6.00	1.183	30.00	2.500
9.00	1.556	50.48	2.500

## Afterbody Ordinates

Station, x, in.	Radius, r, in.													
	I	II	III	IV	V	VI	VII	VIII	IX	X	XI	XII	XIII	XIV
30.48	2.500	2.500	2.500	2.500	2.500	2.500	2.500	2.500	2.500	2.500	2.500	2.500	2.500	2.500
33.12	—	—	—	—	—	—	—	—	—	—	—	—	—	—
36.12	—	—	—	—	—	—	—	—	—	—	—	—	—	—
37.51	2.500	2.500	2.500	2.500	2.500	2.500	2.500	2.500	—	—	—	—	—	—
39.12	—	—	—	—	—	—	—	—	—	—	—	—	—	—
40.12	2.500	2.500	—	—	2.499	2.500	—	—	—	2.505	—	—	—	—
42.12	2.469	2.493	—	—	2.446	2.488	2.500	2.492	2.500	2.437	—	—	—	—
44.12	2.364	2.458	2.500	2.295	2.414	2.498	2.419	2.484	—	—	2.030	—	—	—
45.12	—	—	—	—	—	—	—	—	—	—	—	—	—	—
46.12	2.176	2.259	2.496	2.041	2.211	2.469	2.260	2.361	1.877	—	—	1.774	2.500	2.500
48.12	1.902	2.150	2.459	1.694	1.814	2.235	2.006	2.175	1.516	—	1.506	2.432	2.499	—
50.03	—	—	—	—	1.162	1.182	1.182	—	—	1.257	—	—	—	2.500
50.12	1.534	1.758	2.268	—	—	—	1.654	1.654	—	—	1.235	2.214	2.392	—
51.12	1.315	1.490	2.013	—	—	—	—	1.140	1.650	—	—	1.058	2.043	2.259
52.12	1.073	1.172	1.545	—	—	—	—	1.201	1.416	—	—	.960	1.883	2.067
53.01	.836	.836	.836	—	—	—	—	.963	1.182	—	2.500	.836	1.600	1.845

TABLE II.- AFTERBODY DESIGN

Equation:

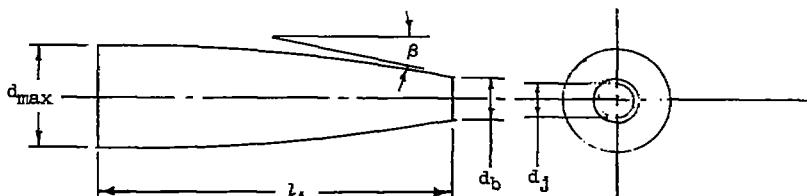


$$y = y_0 - (y_0 - y_1) \left( \frac{x - x_0}{x_1 - x_0} \right)^{\frac{(x_1 - x_0)}{y_0 - y_1} \tan \beta}$$

where:

 $x$  = any afterbody station $y_1$  = body base radius $x_1$  = body base station $y_0$  = maximum body radius $x_0$  = body tangency point $\beta$  = boattail angle $y$  = radius at station  $x$  $\frac{x_1 - x_0}{y_0 - y_1}$  = Constant = 7.747

Design points:



Afterbody	$d_{\max}$ , in.	$l_A$ , in.	$\beta$ , deg	$d_j$ , in.	$d_b$ , in.	$\frac{d_j}{d_b}$	$\frac{d_j}{d_{\max}}$	$x_0$ , in.
IE	5.0	16.40	16	1.240	1.240	1.000	0.248	2.81
I	5.0	15.70	16	1.240	1.672	.742	.248	2.81
II	5.0	15.70	24	1.240	1.672	.742	.248	2.81
III	5.0	15.70	45	1.240	1.672	.742	.248	2.81
IV	5.0	12.72	16	1.754	2.364	.742	.351	2.51
V	5.0	12.72	24	1.754	2.364	.742	.351	2.51
VI	5.0	12.72	45	1.754	2.364	.742	.351	2.51
VII	5.0	15.70	16	1.240	1.930	.643	.248	3.81
VIII	5.0	15.70	16	1.240	2.364	.525	.248	5.49
IX	5.0	19.55	7.7	1.754	2.513	.698	.351	Not defined by this equation
X	5.0	15.70	0	1.240	5.000	.248	.248	
XI	5.0	15.70	8	1.240	1.672	.742	.248	2.81
XII	5.0	15.70	16	1.240	3.200	.388	.248	8.73
XIII	5.0	15.70	16	1.240	3.690	.336	.248	10.63
XIV	5.0	12.72	0	1.754	5.000	.351	.351	12.72

TABLE III.- AFTERSHOCK PRESSURE COEFFICIENTS

(a) Afterbody IE

 $t_j = \text{Cold}$ 

$\frac{x}{d_j}$	$\frac{x}{t_{\max}}$	Pressure coefficients for -											
		$M_\infty = 0.80$			$M_\infty = 0.90$			$M_\infty = 1.00$			$M_\infty = 1.10$		
		$\theta = 0^\circ$			$\theta = 45^\circ$			$\theta = 72^\circ$			$\theta = 0^\circ$		
		$P_{t,j}/P_m = 1.07$			$P_{t,j}/P_m = 1.00$			$P_{t,j}/P_m = 1.09$			$P_{t,j}/P_m = 1.00$		
$P_{t,j}/P_m = 1.07$													
12.56	.720	-0.041	-0.031	-0.025	-0.036	-0.028	-0.019	-0.101	-0.093	-0.085	-0.076	-0.072	-0.065
10.96	.747	-0.078	-0.070	-0.068	-0.075	-0.071	-0.071	-0.109	-0.105	-0.103	-0.078	-0.075	-0.069
9.36	.764	-0.122	-0.117	-0.112	-0.123	-0.123	-0.122	-0.176	-0.174	-0.168	-0.158	-0.155	-0.151
7.72	.821	-0.163	-0.158	-0.152	-0.165	-0.165	-0.164	-0.208	-0.205	-0.202	-0.197	-0.199	-0.193
6.11	.829	-0.193	-0.188	-0.182	-0.190	-0.189	-0.188	-0.236	-0.235	-0.234	-0.229	-0.229	-0.223
4.50	.866	-0.204	-0.203	-0.202	-0.205	-0.204	-0.203	-0.276	-0.275	-0.274	-0.270	-0.270	-0.268
3.90	.923	-0.233	-0.231	-0.229	-0.233	-0.231	-0.230	-0.307	-0.306	-0.305	-0.298	-0.298	-0.295
2.88	.922	-0.232	-0.231	-0.229	-0.233	-0.231	-0.230	-0.306	-0.305	-0.304	-0.298	-0.298	-0.295
1.30	.970	-0.112	-0.110	-0.107	-0.126	-0.126	-0.125	-0.190	-0.190	-0.188	-0.186	-0.186	-0.186
.87	.980	-0.132	-0.130	-0.128	-0.138	-0.136	-0.135	-0.204	-0.204	-0.203	-0.200	-0.200	-0.198
.74	.983	-0.140	-0.140	-0.138	-0.154	-0.155	-0.156	-0.208	-0.210	-0.212	-0.218	-0.216	-0.215
.39	.992	-0.154	-0.154	-0.152	-0.169	-0.169	-0.169	-0.216	-0.216	-0.218	-0.218	-0.218	-0.216
.17	.996	-0.162	-0.162	-0.162	-0.178	-0.176	-0.176	-0.220	-0.222	-0.222	-0.222	-0.222	-0.222
$P_{t,j}/P_m = 1.87$													
12.56	.720	-0.038	-0.031	-0.021	-0.035	-0.028	-0.017	-0.105	-0.097	-0.087	-0.074	-0.069	-0.063
10.96	.747	-0.075	-0.068	-0.065	-0.080	-0.074	-0.071	-0.111	-0.105	-0.103	-0.075	-0.064	-0.063
9.36	.764	-0.117	-0.112	-0.110	-0.121	-0.116	-0.115	-0.180	-0.174	-0.170	-0.157	-0.155	-0.150
7.72	.821	-0.157	-0.150	-0.148	-0.164	-0.157	-0.157	-0.200	-0.199	-0.198	-0.187	-0.186	-0.183
6.11	.829	-0.190	-0.188	-0.186	-0.195	-0.190	-0.189	-0.242	-0.240	-0.238	-0.227	-0.226	-0.223
4.50	.866	-0.208	-0.206	-0.205	-0.212	-0.207	-0.206	-0.279	-0.278	-0.277	-0.267	-0.266	-0.264
3.90	.923	-0.238	-0.235	-0.233	-0.241	-0.238	-0.237	-0.307	-0.306	-0.305	-0.298	-0.298	-0.295
2.88	.922	-0.236	-0.234	-0.232	-0.240	-0.238	-0.237	-0.306	-0.305	-0.304	-0.298	-0.298	-0.295
1.30	.970	-0.157	-0.157	-0.155	-0.161	-0.159	-0.158	-0.204	-0.204	-0.203	-0.206	-0.205	-0.204
.87	.980	-0.164	-0.164	-0.162	-0.171	-0.169	-0.169	-0.218	-0.218	-0.220	-0.222	-0.221	-0.220
.74	.983	-0.174	-0.174	-0.172	-0.180	-0.178	-0.178	-0.224	-0.224	-0.226	-0.226	-0.225	-0.224
.39	.992	-0.187	-0.187	-0.185	-0.193	-0.189	-0.188	-0.230	-0.230	-0.232	-0.232	-0.231	-0.230
.17	.996	-0.204	-0.199	-0.199	-0.219	-0.216	-0.215	-0.236	-0.235	-0.234	-0.234	-0.233	-0.232
$P_{t,j}/P_m = 2.98$													
12.56	.720	-0.041	-0.031	-0.025	-0.037	-0.028	-0.019	-0.101	-0.095	-0.085	-0.078	-0.072	-0.065
10.96	.747	-0.078	-0.070	-0.068	-0.082	-0.075	-0.071	-0.105	-0.103	-0.101	-0.076	-0.067	-0.065
9.36	.764	-0.120	-0.115	-0.110	-0.141	-0.136	-0.132	-0.177	-0.175	-0.169	-0.158	-0.155	-0.151
7.72	.821	-0.167	-0.162	-0.158	-0.184	-0.176	-0.174	-0.200	-0.199	-0.198	-0.187	-0.186	-0.183
6.11	.829	-0.206	-0.204	-0.202	-0.214	-0.206	-0.205	-0.276	-0.275	-0.274	-0.264	-0.263	-0.261
4.50	.866	-0.236	-0.233	-0.231	-0.241	-0.238	-0.237	-0.309	-0.308	-0.307	-0.298	-0.298	-0.295
3.90	.923	-0.264	-0.261	-0.259	-0.278	-0.265	-0.264	-0.332	-0.331	-0.330	-0.320	-0.319	-0.317
2.88	.922	-0.263	-0.261	-0.259	-0.277	-0.265	-0.264	-0.331	-0.330	-0.329	-0.319	-0.318	-0.316
1.30	.970	-0.174	-0.174	-0.172	-0.184	-0.178	-0.178	-0.224	-0.224	-0.226	-0.226	-0.225	-0.224
.87	.980	-0.184	-0.184	-0.182	-0.191	-0.187	-0.186	-0.230	-0.230	-0.232	-0.232	-0.231	-0.230
.74	.983	-0.194	-0.194	-0.192	-0.203	-0.198	-0.197	-0.238	-0.238	-0.240	-0.240	-0.239	-0.238
.39	.992	-0.204	-0.202	-0.201	-0.214	-0.208	-0.206	-0.247	-0.247	-0.249	-0.249	-0.248	-0.247
.17	.996	-0.204	-0.201	-0.201	-0.214	-0.208	-0.206	-0.247	-0.247	-0.249	-0.249	-0.248	-0.247
$P_{t,j}/P_m = 3.01$													
12.56	.720	-0.038	-0.031	-0.021	-0.037	-0.028	-0.019	-0.105	-0.097	-0.089	-0.076	-0.071	-0.065
10.96	.747	-0.075	-0.068	-0.065	-0.082	-0.074	-0.071	-0.105	-0.103	-0.101	-0.076	-0.065	-0.063
9.36	.764	-0.117	-0.112	-0.107	-0.141	-0.136	-0.130	-0.179	-0.175	-0.171	-0.159	-0.155	-0.152
7.72	.821	-0.164	-0.159	-0.152	-0.184	-0.176	-0.174	-0.200	-0.199	-0.198	-0.187	-0.186	-0.183
6.11	.829	-0.206	-0.204	-0.202	-0.214	-0.206	-0.205	-0.276	-0.275	-0.274	-0.264	-0.263	-0.261
4.50	.866	-0.236	-0.233	-0.231	-0.241	-0.238	-0.237	-0.309	-0.308	-0.307	-0.298	-0.298	-0.295
3.90	.923	-0.264	-0.261	-0.259	-0.278	-0.265	-0.264	-0.332	-0.331	-0.330	-0.320	-0.319	-0.317
2.88	.922	-0.263	-0.261	-0.259	-0.277	-0.265	-0.264	-0.331	-0.330	-0.329	-0.319	-0.318	-0.316
1.30	.970	-0.174	-0.174	-0.172	-0.184	-0.178	-0.178	-0.224	-0.224	-0.226	-0.226	-0.225	-0.224
.87	.980	-0.184	-0.184	-0.182	-0.191	-0.187	-0.186	-0.230	-0.230	-0.232	-0.232	-0.231	-0.230
.74	.983	-0.194	-0.194	-0.192	-0.203	-0.198	-0.197	-0.238	-0.238	-0.240	-0.240	-0.239	-0.238
.39	.992	-0.204	-0.202	-0.201	-0.214	-0.208	-0.206	-0.247	-0.247	-0.249	-0.249	-0.248	-0.247
.17	.996	-0.204	-0.201	-0.201	-0.214	-0.208	-0.206	-0.247	-0.247	-0.249	-0.249	-0.248	-0.247
$P_{t,j}/P_m = 4.94$													
12.56	.720							-0.103	-0.097	-0.089	-0.076	-0.071	-0.065
10.96	.747							-0.110	-0.105	-0.103	-0.075	-0.064	-0.063
9.36	.764							-0.117	-0.115	-0.113	-0.137	-0.133	-0.130
7.72	.821							-0.125	-0.123	-0.122	-0.209	-0.200	-0.205
6.11	.829							-0.128	-0.126	-0.125	-0.217	-0.212	-0.215
4.50	.866							-0.129	-0.128	-0.127	-0.227	-0.222	-0.225
3.90	.923							-0.130	-0.129	-0.128	-0.233	-0.231	-0.233
2.88	.922							-0.130	-0.129	-0.128	-0.234	-0.231	-0.232
1.30	.970							-0.130	-0.129	-0.128	-0.235	-0.231	-0.232
.87	.980							-0.130	-0.129	-0.128	-0.236	-0.231	-0.232
.74	.983							-0.130	-0.129	-0.128	-0.237	-0.231	-0.232
.39	.992							-0.130	-0.129	-0.128	-0.238	-0.231	-0.232
.17	.996							-0.130	-0.129	-0.128	-0.239	-0.231	-0.232
$P_{t,j}/P_m = 5.04$													
12.56	.720							-0.103	-0.097	-0.089	-0.076	-0.071	-0.065
10.96	.747							-0.110	-0.105	-0.103	-0.075	-0.064	-0.063
9.36	.764							-0.117	-0.115	-0.113	-0.137	-0.133	-0.130
7.72	.821							-0.125	-0.123	-0.122	-0.209	-0.200	-0.205
6.11	.829							-0.128	-0.126	-0.125	-0.217	-0.212	-0.215
4.50	.866							-0.129	-0.128	-0.127	-0.227	-0.222	-0.225
3.90</													

TABLE III.- AFTERBODY PRESSURE COEFFICIENTS - Continued

(a) Afterbody IB - Concluded

$t_2 = 1,200^{\circ} F$

$\frac{x}{L_{MAX}}$	$\frac{x}{L}$	Pressure coefficients for -											
		M <sub>a</sub> = 0.80			M <sub>a</sub> = 0.90			M <sub>a</sub> = 1.00			M <sub>a</sub> = 1.10		
		s = 0°	s = 45°	s = 72°	s = 0°	s = 45°	s = 72°	s = 0°	s = 45°	s = 72°	s = 0°	s = 45°	s = 72°
		$P_{t,i}/P_a = 2.00$			$P_{t,i}/P_a = 2.03$			$P_{t,i}/P_a = 1.97$			$P_{t,i}/P_a = 1.96$		
12.56	.710	-0.038	-0.031	-0.021	-0.037	-0.028	-0.017	-0.107	-0.101	-0.092	-0.054	-0.071	-0.081
10.96	.747	-0.075	-0.068	-0.056	-0.080	-0.076	-0.071	-0.115	-0.109	-0.107	-0.074	-0.053	-0.062
9.36	.784	-0.117	-0.115	-0.110	-0.141	-0.134	-0.130	-0.182	-0.176	-0.176	-0.139	-0.131	-0.136
7.73	.821	-0.127	-0.122	-0.122	-0.151	-0.145	-0.143	-0.202	-0.194	-0.196	-0.167	-0.159	-0.163
6.11	.859	-0.093	-0.090	-0.090	-0.104	-0.102	-0.104	-0.176	-0.174	-0.176	-0.137	-0.133	-0.135
4.50	.896	-0.056	-0.058	-0.058	-0.059	-0.059	-0.061	-0.134	-0.132	-0.134	-0.093	-0.093	-0.093
2.90	.933	0.035	0.035	0.031	0.045	0.043	0.039	0.119	0.117	0.115	0.091	0.086	0.084
1.30	.952	0.055	0.052	0.050	0.057	0.055	0.052	0.200	0.200	0.202	0.161	0.161	0.161
.74	.963	0.075	0.074	0.074	0.085	0.084	0.082	0.212	0.212	0.215	0.171	0.171	0.171
.39	.974	0.095	0.095	0.095	0.106	0.105	0.103	0.218	0.218	0.220	0.174	0.174	0.174
.17	.986	0.108	0.108	0.105	0.119	0.119	0.115	0.230	0.230	0.230	0.179	0.179	0.179
		$P_{t,i}/P_a = 3.01$			$P_{t,i}/P_a = 3.01$			$P_{t,i}/P_a = 3.02$			$P_{t,i}/P_a = 3.03$		
12.56	.710	-0.038	-0.031	-0.021	-0.037	-0.028	-0.019	-0.105	-0.099	-0.091	-0.054	-0.069	-0.061
10.96	.747	-0.075	-0.068	-0.056	-0.080	-0.076	-0.071	-0.115	-0.106	-0.106	-0.074	-0.065	-0.065
9.36	.784	-0.117	-0.115	-0.107	-0.141	-0.134	-0.130	-0.182	-0.171	-0.171	-0.137	-0.133	-0.136
7.73	.821	-0.127	-0.120	-0.120	-0.147	-0.147	-0.147	-0.202	-0.194	-0.196	-0.167	-0.159	-0.163
6.11	.859	-0.090	-0.090	-0.088	-0.105	-0.104	-0.104	-0.176	-0.174	-0.176	-0.137	-0.133	-0.135
4.50	.896	-0.056	-0.056	-0.056	-0.059	-0.059	-0.061	-0.124	-0.122	-0.124	-0.091	-0.086	-0.088
2.90	.933	0.038	0.038	0.032	0.045	0.043	0.039	0.124	0.122	0.124	0.091	0.087	0.084
1.30	.952	0.057	0.057	0.055	0.067	0.065	0.063	0.203	0.203	0.206	0.177	0.177	0.177
.74	.963	0.076	0.076	0.074	0.085	0.084	0.082	0.218	0.218	0.220	0.178	0.178	0.178
.39	.974	0.096	0.096	0.095	0.106	0.105	0.103	0.224	0.224	0.226	0.186	0.186	0.186
.17	.986	0.108	0.108	0.105	0.119	0.119	0.115	0.230	0.230	0.230	0.187	0.187	0.187
		$P_{t,i}/P_a = 4.08$			$P_{t,i}/P_a = 4.06$			$P_{t,i}/P_a = 5.02$			$P_{t,i}/P_a = 5.00$		
12.56	.710	-0.038	-0.031	-0.021	-0.037	-0.028	-0.019	-0.107	-0.103	-0.093	-0.053	-0.069	-0.061
10.96	.747	-0.075	-0.068	-0.056	-0.080	-0.076	-0.071	-0.115	-0.109	-0.107	-0.074	-0.065	-0.065
9.36	.784	-0.117	-0.115	-0.107	-0.141	-0.134	-0.130	-0.182	-0.176	-0.176	-0.138	-0.134	-0.136
7.73	.821	-0.127	-0.120	-0.120	-0.147	-0.147	-0.147	-0.202	-0.194	-0.196	-0.167	-0.159	-0.163
6.11	.859	-0.090	-0.090	-0.088	-0.105	-0.104	-0.104	-0.176	-0.174	-0.176	-0.137	-0.133	-0.135
4.50	.896	-0.056	-0.056	-0.056	-0.059	-0.059	-0.061	-0.124	-0.122	-0.124	-0.091	-0.086	-0.088
2.90	.933	0.038	0.038	0.032	0.045	0.043	0.039	0.124	0.122	0.124	0.091	0.087	0.084
1.30	.952	0.057	0.057	0.055	0.067	0.065	0.063	0.203	0.203	0.206	0.177	0.177	0.177
.74	.963	0.076	0.076	0.074	0.085	0.084	0.082	0.218	0.218	0.220	0.186	0.186	0.186
.39	.974	0.096	0.096	0.095	0.106	0.105	0.103	0.224	0.224	0.226	0.186	0.186	0.186
.17	.986	0.108	0.108	0.105	0.119	0.119	0.115	0.230	0.230	0.230	0.187	0.187	0.187
		$P_{t,i}/P_a = 6.97$			$P_{t,i}/P_a = 7.00$			$P_{t,i}/P_a = 7.00$			$P_{t,i}/P_a = 6.99$		
12.56	.710	-0.038	-0.031	-0.021	-0.037	-0.028	-0.019	-0.107	-0.101	-0.091	-0.057	-0.060	-0.064
10.96	.747	-0.075	-0.068	-0.056	-0.080	-0.076	-0.071	-0.115	-0.109	-0.107	-0.076	-0.065	-0.065
9.36	.784	-0.117	-0.115	-0.107	-0.141	-0.134	-0.130	-0.182	-0.176	-0.176	-0.138	-0.134	-0.136
7.73	.821	-0.127	-0.120	-0.120	-0.147	-0.147	-0.147	-0.202	-0.194	-0.196	-0.167	-0.159	-0.163
6.11	.859	-0.090	-0.090	-0.088	-0.105	-0.104	-0.104	-0.176	-0.174	-0.176	-0.137	-0.133	-0.135
4.50	.896	-0.056	-0.056	-0.056	-0.059	-0.059	-0.061	-0.124	-0.122	-0.124	-0.091	-0.086	-0.088
2.90	.933	0.038	0.038	0.032	0.045	0.043	0.039	0.124	0.122	0.124	0.091	0.087	0.084
1.30	.952	0.057	0.057	0.055	0.067	0.065	0.063	0.203	0.203	0.206	0.177	0.177	0.177
.74	.963	0.076	0.076	0.074	0.085	0.084	0.082	0.218	0.218	0.220	0.186	0.186	0.186
.39	.974	0.096	0.096	0.095	0.106	0.105	0.103	0.224	0.224	0.226	0.186	0.186	0.186
.17	.986	0.108	0.108	0.105	0.119	0.119	0.115	0.230	0.230	0.230	0.187	0.187	0.187
		$P_{t,i}/P_a = 8.98$			$P_{t,i}/P_a = 9.01$			$P_{t,i}/P_a = 9.00$			$P_{t,i}/P_a = 8.99$		
12.56	.710	-0.038	-0.031	-0.021	-0.037	-0.028	-0.019	-0.109	-0.101	-0.091	-0.059	-0.071	-0.064
10.96	.747	-0.075	-0.068	-0.056	-0.080	-0.076	-0.071	-0.115	-0.109	-0.107	-0.075	-0.065	-0.065
9.36	.784	-0.117	-0.115	-0.107	-0.141	-0.134	-0.130	-0.182	-0.176	-0.176	-0.138	-0.134	-0.136
7.73	.821	-0.127	-0.120	-0.120	-0.147	-0.147	-0.147	-0.202	-0.194	-0.196	-0.167	-0.159	-0.163
6.11	.859	-0.090	-0.090	-0.088	-0.105	-0.104	-0.104	-0.176	-0.174	-0.176	-0.137	-0.133	-0.135
4.50	.896	-0.056	-0.056	-0.056	-0.059	-0.059	-0.061	-0.124	-0.122	-0.124	-0.091	-0.086	-0.088
2.90	.933	0.038	0.038	0.032	0.045	0.043	0.039	0.124	0.122	0.124	0.091	0.087	0.084
1.30	.952	0.057	0.057	0.055	0.067	0.065	0.063	0.203	0.203	0.206	0.177	0.177	0.177
.74	.963	0.076	0.076	0.074	0.085	0.084	0.082	0.218	0.218	0.220	0.186	0.186	0.186
.39	.974	0.096	0.096	0.095	0.106	0.105	0.103	0.224	0.224	0.226	0.186	0.186	0.186
.17	.986	0.108	0.108	0.105	0.119	0.119	0.115	0.230	0.230	0.230	0.187	0.187	0.187
		$P_{t,i}/P_a = 10.99$			$P_{t,i}/P_a = 10.97$								
12.56	.710							-0.109	-0.099	-0.091	-0.059	-0.068	-0.066
10.96	.747							-0.111	-0.107	-0.103	-0.071	-0.081	-0.078
9.36	.784							-0.120	-0.116	-0.112	-0.078	-0.088	-0.084
7.73	.821							-0.126	-0.121	-0.117	-0.082	-0.092	-0.088
6.11	.859							-0.128	-0.124	-0.120	-0.084	-0.094	-0.090
4.50	.896							-0.126	-0.122	-0.118	-0.082	-0.092	-0.088
2.90	.933							-0.124	-0.120	-0.116	-0.080	-0.090	-0.086
1.30	.952							-0.122	-0.118	-0.114	-0.078	-0.088	-0.084
.74	.963							-0.120	-0.116	-0.112	-0.076	-0.086	-0.082
.39	.974							-0.119	-0.115	-0.111	-0.074	-0.084	-0.080
.17	.986							-0.118	-0.114	-0.110	-0.073	-0.083	-0.079

CONFIDENTIAL

TABLE III.- AFTERBODY PRESSURE COEFFICIENTS - Continued

(b) Afterbody I

$t_1 = \text{Cold}$

TABLE III.- AFTERBODY PRESSURE COEFFICIENTS - Continued

(b) Afterbody I - Continued

 $T_f = 800^{\circ} F$ 

$\frac{x}{d_1}$	$\frac{x}{l_{max}}$	Pressure coefficients for -											
		M <sub>∞</sub> = 0.80			M <sub>∞</sub> = 0.90			M <sub>∞</sub> = 1.00			M <sub>∞</sub> = 1.10		
		s = 0°	s = 45°	s = 72°	s = 0°	s = 45°	s = 72°	s = 0°	s = 45°	s = 72°	s = 0°	s = 45°	s = 72°
		$P_{t,i}/P_m = 2.00$			$P_{t,i}/P_m = 1.96$			$P_{t,i}/P_m = 1.96$			$P_{t,i}/P_m = 1.96$		
12.01	.719	-0.059	-0.030	-0.019	-0.039	-0.029	-0.018	-0.107	-0.095	-0.084	-0.097	-0.077	-0.054
10.39	.737	-0.122	-0.070	-0.033	-0.080	-0.077	-0.070	-0.115	-0.101	-0.087	-0.108	-0.076	-0.054
8.76	.757	-0.145	-0.122	-0.111	-0.159	-0.144	-0.134	-0.154	-0.142	-0.130	-0.156	-0.130	-0.124
7.18	.782	-0.128	-0.122	-0.111	-0.145	-0.148	-0.138	-0.154	-0.142	-0.130	-0.156	-0.130	-0.124
5.36	.870	-0.091	-0.090	-0.084	-0.105	-0.109	-0.097	-0.126	-0.120	-0.110	-0.130	-0.110	-0.104
3.95	.908	-0.056	-0.058	-0.042	-0.088	-0.081	-0.065	-0.130	-0.124	-0.114	-0.130	-0.110	-0.104
2.35	.963	-0.024	-0.024	-0.026	-0.043	-0.040	-0.033	-0.171	-0.166	-0.150	-0.170	-0.150	-0.140
1.34	.985	-0.080	-0.076	-0.074	-0.093	-0.090	-0.088	-0.205	-0.195	-0.180	-0.205	-0.180	-0.170
.73	.983	-0.150	-0.129	-0.129	-0.145	-0.144	-0.135	-0.205	-0.195	-0.180	-0.205	-0.180	-0.170
.39	.993	-0.152	-0.151	-0.153	-0.168	-0.168	-0.168	-0.211	-0.211	-0.202	-0.219	-0.198	-0.186
.17	.996	-0.158	-0.160	-0.161	-0.175	-0.176	-0.179	-0.221	-0.222	-0.203	-0.233	-0.163	-0.163
		$P_{t,i}/P_m = 2.97$			$P_{t,i}/P_m = 5.00$			$P_{t,i}/P_m = 2.99$			$P_{t,i}/P_m = 2.99$		
12.01	.719	-0.040	-0.029	-0.020	-0.087	-0.087	-0.024	-0.107	-0.094	-0.084	-0.097	-0.066	-0.055
10.39	.737	-0.073	-0.070	-0.067	-0.108	-0.103	-0.070	-0.112	-0.110	-0.108	-0.097	-0.072	-0.063
8.76	.757	-0.117	-0.113	-0.113	-0.136	-0.135	-0.132	-0.152	-0.142	-0.130	-0.152	-0.132	-0.124
7.18	.782	-0.128	-0.123	-0.114	-0.149	-0.146	-0.136	-0.163	-0.153	-0.143	-0.163	-0.143	-0.135
5.36	.870	-0.091	-0.090	-0.084	-0.105	-0.108	-0.099	-0.177	-0.173	-0.166	-0.186	-0.166	-0.157
3.95	.908	-0.058	-0.060	-0.053	-0.088	-0.089	-0.073	-0.195	-0.193	-0.180	-0.205	-0.180	-0.170
2.35	.963	-0.023	-0.021	-0.023	-0.044	-0.042	-0.037	-0.129	-0.127	-0.118	-0.132	-0.118	-0.108
1.34	.985	-0.078	-0.076	-0.074	-0.095	-0.093	-0.088	-0.170	-0.168	-0.158	-0.170	-0.158	-0.148
.73	.983	-0.149	-0.150	-0.151	-0.168	-0.168	-0.170	-0.216	-0.215	-0.204	-0.218	-0.193	-0.185
.39	.993	-0.152	-0.152	-0.153	-0.170	-0.170	-0.170	-0.221	-0.221	-0.212	-0.233	-0.192	-0.184
.17	.996	-0.157	-0.159	-0.161	-0.175	-0.177	-0.181	-0.221	-0.223	-0.212	-0.233	-0.199	-0.184
		$P_{t,i}/P_m = 5.00$			$P_{t,i}/P_m = 5.00$			$P_{t,i}/P_m = 4.99$			$P_{t,i}/P_m = 4.99$		
12.01	.719	-0.039	-0.031	-0.019	-0.077	-0.077	-0.015	-0.108	-0.095	-0.085	-0.098	-0.067	-0.056
10.39	.737	-0.072	-0.070	-0.069	-0.108	-0.103	-0.071	-0.115	-0.111	-0.109	-0.092	-0.065	-0.053
8.76	.757	-0.115	-0.113	-0.111	-0.137	-0.135	-0.135	-0.153	-0.153	-0.150	-0.176	-0.159	-0.148
7.18	.782	-0.128	-0.123	-0.113	-0.148	-0.145	-0.136	-0.164	-0.162	-0.156	-0.187	-0.166	-0.159
5.36	.870	-0.092	-0.089	-0.086	-0.104	-0.103	-0.101	-0.177	-0.173	-0.167	-0.197	-0.171	-0.161
3.95	.908	-0.057	-0.061	-0.051	-0.087	-0.086	-0.082	-0.199	-0.195	-0.185	-0.205	-0.185	-0.174
2.35	.963	-0.024	-0.024	-0.020	-0.048	-0.048	-0.048	-0.129	-0.128	-0.126	-0.142	-0.128	-0.118
1.34	.985	-0.078	-0.078	-0.076	-0.096	-0.096	-0.094	-0.172	-0.170	-0.168	-0.178	-0.168	-0.158
.73	.983	-0.137	-0.137	-0.137	-0.154	-0.154	-0.154	-0.204	-0.204	-0.202	-0.218	-0.193	-0.182
.39	.993	-0.152	-0.152	-0.153	-0.170	-0.170	-0.170	-0.217	-0.217	-0.215	-0.233	-0.192	-0.182
.17	.996	-0.171	-0.171	-0.171	-0.187	-0.187	-0.187	-0.221	-0.221	-0.218	-0.233	-0.192	-0.184
		$P_{t,i}/P_m = 6.98$			$P_{t,i}/P_m = 6.99$			$P_{t,i}/P_m = 6.97$			$P_{t,i}/P_m = 7.02$		
12.01	.719	-0.040	-0.031	-0.020	-0.087	-0.087	-0.014	-0.108	-0.094	-0.085	-0.098	-0.069	-0.056
10.39	.737	-0.073	-0.070	-0.066	-0.108	-0.103	-0.071	-0.113	-0.111	-0.108	-0.095	-0.072	-0.063
8.76	.757	-0.115	-0.113	-0.113	-0.136	-0.135	-0.132	-0.153	-0.153	-0.150	-0.176	-0.159	-0.148
7.18	.782	-0.128	-0.123	-0.113	-0.147	-0.145	-0.136	-0.164	-0.162	-0.156	-0.187	-0.166	-0.157
5.36	.870	-0.092	-0.089	-0.086	-0.108	-0.103	-0.102	-0.177	-0.173	-0.167	-0.197	-0.171	-0.161
3.95	.908	-0.057	-0.061	-0.051	-0.087	-0.086	-0.082	-0.199	-0.195	-0.185	-0.205	-0.185	-0.174
2.35	.963	-0.024	-0.024	-0.020	-0.048	-0.048	-0.048	-0.129	-0.128	-0.126	-0.142	-0.128	-0.118
1.34	.985	-0.078	-0.078	-0.076	-0.096	-0.096	-0.094	-0.172	-0.170	-0.168	-0.178	-0.168	-0.158
.73	.983	-0.137	-0.137	-0.137	-0.154	-0.154	-0.154	-0.204	-0.204	-0.202	-0.218	-0.193	-0.182
.39	.993	-0.152	-0.152	-0.153	-0.170	-0.170	-0.170	-0.217	-0.217	-0.215	-0.233	-0.192	-0.182
.17	.996	-0.171	-0.171	-0.171	-0.187	-0.187	-0.187	-0.221	-0.221	-0.218	-0.233	-0.192	-0.184
		$P_{t,i}/P_m = 8.98$			$P_{t,i}/P_m = 8.97$			$P_{t,i}/P_m = 8.98$			$P_{t,i}/P_m = 8.99$		
12.01	.719	-0.039	-0.031	-0.020	-0.076	-0.076	-0.013	-0.108	-0.093	-0.085	-0.098	-0.067	-0.055
10.39	.737	-0.072	-0.070	-0.067	-0.108	-0.103	-0.071	-0.113	-0.111	-0.108	-0.095	-0.072	-0.063
8.76	.757	-0.117	-0.113	-0.113	-0.136	-0.135	-0.132	-0.153	-0.153	-0.150	-0.176	-0.159	-0.148
7.18	.782	-0.128	-0.123	-0.113	-0.147	-0.145	-0.136	-0.164	-0.162	-0.156	-0.187	-0.166	-0.157
5.36	.870	-0.092	-0.089	-0.086	-0.108	-0.103	-0.102	-0.177	-0.173	-0.167	-0.197	-0.171	-0.161
3.95	.908	-0.057	-0.061	-0.051	-0.087	-0.086	-0.082	-0.199	-0.195	-0.185	-0.205	-0.185	-0.174
2.35	.963	-0.024	-0.024	-0.020	-0.048	-0.048	-0.048	-0.129	-0.128	-0.126	-0.142	-0.128	-0.118
1.34	.985	-0.078	-0.078	-0.076	-0.096	-0.096	-0.094	-0.172	-0.170	-0.168	-0.178	-0.168	-0.158
.73	.983	-0.137	-0.137	-0.137	-0.154	-0.154	-0.154	-0.204	-0.204	-0.202	-0.218	-0.193	-0.182
.39	.993	-0.152	-0.152	-0.153	-0.170	-0.170	-0.170	-0.217	-0.217	-0.215	-0.233	-0.192	-0.182
.17	.996	-0.171	-0.171	-0.171	-0.187	-0.187	-0.187	-0.221	-0.221	-0.218	-0.233	-0.192	-0.184
		$P_{t,i}/P_m = 10.98$			$P_{t,i}/P_m = 10.99$			$P_{t,i}/P_m = 10.99$			$P_{t,i}/P_m = 10.99$		
12.01	.719							-0.108	-0.096	-0.085	-0.099	-0.069	-0.056
10.39	.737							-0.113	-0.112	-0.109	-0.095	-0.073	-0.063
8.76	.757							-0.123	-0.121	-0.118	-0.108	-0.088	-0.073
7.18	.782							-0.134	-0.132	-0.128	-0.118	-0.098	-0.083
5.36	.870							-0.144	-0.142	-0.138	-0.128	-0.108	-0.093
3.95	.908							-0.154	-0.152	-0.148	-0.138	-0.118	-0.108
2.35	.963							-0.164	-0.162	-0.158	-0.148	-0.128	-0.118
1.34	.985							-0.174	-0.172	-0.168	-0.158	-0.138	-0.128
.73	.983							-0.184	-0.182	-0.178	-0.168	-0.148	-0.138
.39	.993							-0.194	-0.192	-0.188	-0.178	-0.158	-0.148
.17	.996							-0.204	-0.202	-0.200	-0.190	-0.170	-0.160

TABLE III.- AFTERSHOCK PRESSURE COEFFICIENTS - Continued

(b) Afterbody I - Continued

 $t_j = 1,200^{\circ} F$ 

$\frac{x}{d_3}$	$\frac{x}{t_{max}}$	Pressure coefficients for -											
		M <sub>a</sub> = 0.80			M <sub>a</sub> = 0.90			M <sub>a</sub> = 1.00			M <sub>a</sub> = 1.10		
		$\theta = 0^{\circ}$	$\theta = 45^{\circ}$	$\theta = 72^{\circ}$	$\theta = 0^{\circ}$	$\theta = 45^{\circ}$	$\theta = 72^{\circ}$	$\theta = 0^{\circ}$	$\theta = 45^{\circ}$	$\theta = 72^{\circ}$	$\theta = 0^{\circ}$	$\theta = 45^{\circ}$	$\theta = 72^{\circ}$
		$P_{t,j}/P_a = 2.00$			$P_{t,j}/P_a = 1.99$			$P_{t,j}/P_a = 2.01$			$P_{t,j}/P_a = 1.99$		
12.01	.719	-0.039	-0.031	-0.018	-0.058	-0.068	-0.015	-0.109	-0.093	-0.085	-0.059	-0.048	-0.037
10.39	.727	-0.078	-0.070	-0.067	-0.078	-0.076	-0.070	-0.111	-0.107	-0.107	-0.073	-0.065	-0.055
8.76	.729	-0.117	-0.116	-0.113	-0.157	-0.156	-0.132	-0.181	-0.179	-0.176	-0.137	-0.132	-0.129
7.18	.832	-0.125	-0.122	-0.122	-0.150	-0.145	-0.144	-0.183	-0.183	-0.183	-0.146	-0.141	-0.134
5.56	.870	-0.093	-0.093	-0.093	-0.104	-0.103	-0.092	-0.131	-0.129	-0.126	-0.097	-0.091	-0.084
3.93	.908	-0.057	-0.058	-0.044	-0.057	-0.059	-0.042	-0.078	-0.070	-0.065	-0.043	-0.037	-0.030
2.35	.945	.024	.035	.028	.045	.043	.037	.131	.129	.126	.083	.065	.060
1.74	.964	.081	.079	.076	.095	.093	.080	.173	.172	.171	.126	.117	.116
.73	.983	.152	.150	.150	.149	.148	.146	.201	.198	.197	.150	.145	.146
.50	.993	.158	.158	.158	.175	.174	.174	.219	.219	.219	.155	.155	.156
.17	.996	.164	.164	.165	.180	.182	.181	.224	.224	.224	.160	.161	.162
		$P_{t,j}/P_a = 2.99$			$P_{t,j}/P_a = 2.98$			$P_{t,j}/P_a = 2.99$			$P_{t,j}/P_a = 2.99$		
12.01	.719	-0.036	-0.030	-0.018	-0.057	-0.068	-0.015	-0.109	-0.095	-0.086	-0.057	-0.047	-0.036
10.39	.727	-0.078	-0.069	-0.065	-0.077	-0.077	-0.072	-0.111	-0.109	-0.107	-0.073	-0.066	-0.054
8.76	.729	-0.115	-0.115	-0.112	-0.156	-0.151	-0.132	-0.181	-0.179	-0.176	-0.136	-0.132	-0.129
7.18	.832	-0.125	-0.122	-0.121	-0.150	-0.147	-0.146	-0.183	-0.183	-0.183	-0.146	-0.141	-0.134
5.56	.870	-0.090	-0.089	-0.093	-0.105	-0.104	-0.092	-0.130	-0.128	-0.125	-0.090	-0.081	-0.074
3.93	.908	-0.056	-0.058	-0.042	-0.056	-0.054	-0.044	-0.076	-0.073	-0.071	-0.046	-0.036	-0.030
2.35	.945	.024	.034	.028	.044	.042	.036	.127	.125	.123	.083	.065	.060
1.74	.964	.080	.079	.076	.095	.092	.088	.172	.169	.170	.128	.117	.116
.73	.983	.153	.150	.149	.168	.166	.165	.205	.205	.206	.155	.155	.156
.50	.993	.158	.158	.158	.175	.174	.174	.217	.219	.219	.156	.155	.156
.17	.996	.164	.164	.165	.180	.182	.181	.224	.224	.224	.160	.161	.162
		$P_{t,j}/P_a = 4.01$			$P_{t,j}/P_a = 4.97$			$P_{t,j}/P_a = 4.99$			$P_{t,j}/P_a = 4.99$		
12.01	.719	-0.040	-0.032	-0.020	-0.056	-0.066	-0.015	-0.109	-0.095	-0.086	-0.057	-0.048	-0.036
10.39	.727	-0.078	-0.069	-0.065	-0.077	-0.077	-0.070	-0.111	-0.109	-0.107	-0.073	-0.066	-0.054
8.76	.729	-0.115	-0.115	-0.113	-0.157	-0.155	-0.132	-0.181	-0.179	-0.176	-0.136	-0.132	-0.129
7.18	.832	-0.125	-0.122	-0.121	-0.156	-0.153	-0.143	-0.183	-0.183	-0.183	-0.146	-0.141	-0.134
5.56	.870	-0.089	-0.090	-0.092	-0.103	-0.102	-0.092	-0.130	-0.128	-0.125	-0.090	-0.081	-0.074
3.93	.908	-0.056	-0.058	-0.040	-0.055	-0.053	-0.042	-0.077	-0.074	-0.072	-0.046	-0.036	-0.030
2.35	.945	.024	.034	.028	.043	.041	.036	.127	.125	.123	.083	.065	.060
1.74	.964	.080	.079	.076	.095	.092	.088	.172	.170	.172	.128	.117	.116
.73	.983	.153	.150	.149	.168	.166	.165	.205	.205	.206	.155	.155	.156
.50	.993	.158	.158	.158	.175	.174	.174	.217	.219	.219	.156	.155	.156
.17	.996	.164	.164	.165	.180	.182	.181	.224	.224	.224	.160	.161	.162
		$P_{t,j}/P_a = 7.05$			$P_{t,j}/P_a = 7.00$			$P_{t,j}/P_a = 6.99$			$P_{t,j}/P_a = 6.97$		
12.01	.719	-0.040	-0.031	-0.020	-0.059	-0.069	-0.016	-0.109	-0.095	-0.086	-0.057	-0.048	-0.036
10.39	.727	-0.078	-0.068	-0.065	-0.076	-0.076	-0.070	-0.111	-0.109	-0.107	-0.073	-0.065	-0.053
8.76	.729	-0.115	-0.115	-0.109	-0.159	-0.157	-0.137	-0.181	-0.179	-0.176	-0.137	-0.131	-0.126
7.18	.832	-0.125	-0.122	-0.120	-0.150	-0.147	-0.146	-0.183	-0.183	-0.183	-0.146	-0.141	-0.134
5.56	.870	-0.086	-0.086	-0.086	-0.097	-0.097	-0.087	-0.127	-0.125	-0.123	-0.090	-0.081	-0.074
3.93	.908	-0.053	-0.054	-0.041	-0.054	-0.053	-0.042	-0.076	-0.073	-0.071	-0.046	-0.036	-0.030
2.35	.945	.024	.034	.028	.043	.041	.036	.127	.125	.123	.083	.065	.060
1.74	.964	.079	.078	.076	.095	.093	.088	.172	.170	.172	.128	.117	.116
.73	.983	.152	.150	.149	.168	.166	.165	.205	.205	.206	.155	.155	.156
.50	.993	.157	.158	.158	.175	.174	.174	.217	.219	.219	.156	.155	.156
.17	.996	.163	.164	.165	.180	.182	.181	.224	.224	.224	.160	.161	.162
		$P_{t,j}/P_a = 8.99$			$P_{t,j}/P_a = 8.99$			$P_{t,j}/P_a = 9.01$			$P_{t,j}/P_a = 8.98$		
12.01	.719	-0.059	-0.030	-0.018	-0.055	-0.068	-0.013	-0.109	-0.094	-0.085	-0.059	-0.049	-0.036
10.39	.727	-0.078	-0.067	-0.065	-0.075	-0.075	-0.070	-0.111	-0.109	-0.107	-0.073	-0.065	-0.053
8.76	.729	-0.116	-0.116	-0.108	-0.158	-0.152	-0.135	-0.182	-0.179	-0.176	-0.137	-0.131	-0.126
7.18	.832	-0.125	-0.122	-0.120	-0.150	-0.147	-0.146	-0.183	-0.183	-0.183	-0.146	-0.141	-0.134
5.56	.870	-0.086	-0.086	-0.086	-0.097	-0.097	-0.087	-0.127	-0.125	-0.123	-0.090	-0.081	-0.074
3.93	.908	-0.053	-0.054	-0.041	-0.054	-0.053	-0.042	-0.076	-0.073	-0.071	-0.046	-0.036	-0.030
2.35	.945	.024	.034	.028	.043	.041	.036	.127	.125	.123	.083	.065	.060
1.74	.964	.080	.079	.076	.095	.093	.088	.172	.170	.172	.128	.117	.116
.73	.983	.153	.150	.149	.168	.166	.165	.205	.205	.206	.155	.155	.156
.50	.993	.158	.158	.158	.175	.174	.174	.217	.219	.219	.156	.155	.156
.17	.996	.164	.164	.165	.180	.182	.181	.224	.224	.224	.160	.161	.162
		$P_{t,j}/P_a = 10.98$			$P_{t,j}/P_a = 10.98$			$P_{t,j}/P_a = 10.98$			$P_{t,j}/P_a = 10.98$		
12.01	.719							-0.110	-0.096	-0.084	-0.062	-0.050	-0.036
10.39	.727							-0.112	-0.111	-0.109	-0.074	-0.065	-0.057
8.76	.729							-0.183	-0.180	-0.178	-0.139	-0.136	-0.133
7.18	.832							-0.264	-0.256	-0.256	-0.207	-0.201	-0.204
5.56	.870							-0.277	-0.274	-0.269	-0.227	-0.225	-0.222
3.93	.908							-0.015	-0.020	-0.014	-0.026	-0.024	-0.023
2.35	.945							-0.128	-0.125	-0.124	-0.091	-0.088	-0.085
1.74	.964							-0.227	-0.224	-0.224	-0.167	-0.167	-0.167
.73	.983							-0.259	-0.253	-0.254	-0.187	-0.185	-0.187
.50	.993							-0.265	-0.264	-0.264	-0.187	-0.185	-0.187
.17	.996							-0.265	-0.264	-0.264	-0.187	-0.185	-0.187

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TABLE III.- AFTERBODY PRESSURE COEFFICIENTS - Continued

(a) Afterbody II

 $t_j = \text{Cold}$ 

$\frac{x}{d_j}$	$\frac{x}{l_{\max}}$	Pressure coefficients for -											
		$M_\infty = 0.80$			$M_\infty = 0.90$			$M_\infty = 1.00$			$M_\infty = 1.10$		
		$\theta = 0^\circ$	$\theta = 45^\circ$	$\theta = 72^\circ$	$\theta = 0^\circ$	$\theta = 45^\circ$	$\theta = 72^\circ$	$\theta = 0^\circ$	$\theta = 45^\circ$	$\theta = 72^\circ$	$\theta = 0^\circ$	$\theta = 45^\circ$	$\theta = 72^\circ$
		$P_{t,j}/P_\infty = 1.09$			$P_{t,j}/P_\infty = 1.12$			$P_{t,j}/P_\infty = 1.12$			$P_{t,j}/P_\infty = 1.09$		
12.01	.719	-0.006	-0.020	-0.010	-0.008	-0.015	-0.005	-0.100	-0.096	-0.086	-0.056	-0.043	-0.032
10.39	.757	-0.042	-0.071	-0.031	-0.042	-0.057	-0.031	-0.087	-0.083	-0.077	-0.049	-0.044	-0.038
8.76	.795	-0.076	-0.073	-0.073	-0.068	-0.066	-0.061	-0.117	-0.113	-0.113	-0.076	-0.074	-0.074
7.18	.832	-0.121	-0.118	-0.116	-0.114	-0.112	-0.109	-0.171	-0.169	-0.169	-0.119	-0.120	-0.118
5.56	.870	-0.192	-0.152	-0.152	-0.151	-0.151	-0.151	-0.270	-0.270	-0.270	-0.211	-0.210	-0.209
3.93	.908	-0.260	-0.190	-0.190	-0.194	-0.194	-0.194	-0.331	-0.328	-0.328	-0.271	-0.271	-0.270
2.35	.943	-0.324	-0.240	-0.240	-0.243	-0.243	-0.243	-0.409	-0.409	-0.409	-0.347	-0.347	-0.345
1.74	.973	-0.366	-0.280	-0.280	-0.271	-0.271	-0.271	-0.442	-0.442	-0.442	-0.383	-0.383	-0.383
.13	.983	-0.400	-0.308	-0.308	-0.303	-0.303	-0.303	-0.483	-0.483	-0.483	-0.420	-0.420	-0.419
.17	.996	-0.436	-0.324	-0.324	-0.316	-0.316	-0.316	-0.522	-0.522	-0.522	-0.457	-0.457	-0.456
		$P_{t,j}/P_\infty = 1.98$			$P_{t,j}/P_\infty = 1.99$			$P_{t,j}/P_\infty = 2.00$			$P_{t,j}/P_\infty = 1.99$		
12.01	.719	-0.006	-0.021	-0.010	-0.006	-0.017	-0.006	-0.099	-0.096	-0.083	-0.049	-0.046	-0.035
10.39	.757	-0.042	-0.071	-0.031	-0.042	-0.056	-0.030	-0.086	-0.083	-0.077	-0.045	-0.046	-0.040
8.76	.795	-0.076	-0.073	-0.073	-0.066	-0.068	-0.079	-0.115	-0.114	-0.111	-0.079	-0.078	-0.077
7.18	.832	-0.120	-0.117	-0.115	-0.118	-0.119	-0.116	-0.169	-0.167	-0.167	-0.121	-0.122	-0.120
5.56	.870	-0.188	-0.150	-0.150	-0.185	-0.187	-0.185	-0.270	-0.268	-0.270	-0.213	-0.213	-0.212
3.93	.908	-0.256	-0.194	-0.194	-0.217	-0.216	-0.215	-0.368	-0.368	-0.368	-0.311	-0.311	-0.310
2.35	.943	-0.313	-0.218	-0.218	-0.205	-0.205	-0.205	-0.436	-0.436	-0.436	-0.354	-0.354	-0.353
1.74	.973	-0.354	-0.265	-0.265	-0.256	-0.256	-0.256	-0.476	-0.476	-0.476	-0.417	-0.417	-0.416
.13	.983	-0.386	-0.280	-0.280	-0.271	-0.271	-0.271	-0.512	-0.512	-0.512	-0.452	-0.452	-0.451
.17	.996	-0.420	-0.316	-0.316	-0.302	-0.302	-0.302	-0.550	-0.550	-0.550	-0.492	-0.492	-0.491
		$P_{t,j}/P_\infty = 3.00$			$P_{t,j}/P_\infty = 2.96$			$P_{t,j}/P_\infty = 2.99$			$P_{t,j}/P_\infty = 3.02$		
12.01	.719	-0.027	-0.021	-0.009	-0.022	-0.015	-0.004	-0.101	-0.096	-0.084	-0.049	-0.046	-0.035
10.39	.757	-0.042	-0.071	-0.031	-0.040	-0.052	-0.029	-0.089	-0.085	-0.077	-0.050	-0.049	-0.039
8.76	.795	-0.077	-0.074	-0.071	-0.065	-0.063	-0.078	-0.115	-0.115	-0.112	-0.079	-0.077	-0.077
7.18	.832	-0.120	-0.117	-0.117	-0.129	-0.128	-0.127	-0.172	-0.169	-0.167	-0.124	-0.123	-0.120
5.56	.870	-0.188	-0.151	-0.151	-0.186	-0.186	-0.185	-0.270	-0.268	-0.270	-0.213	-0.213	-0.212
3.93	.908	-0.256	-0.194	-0.194	-0.216	-0.216	-0.215	-0.368	-0.368	-0.368	-0.311	-0.311	-0.310
2.35	.943	-0.313	-0.222	-0.222	-0.203	-0.203	-0.203	-0.409	-0.409	-0.409	-0.347	-0.347	-0.346
1.74	.973	-0.354	-0.265	-0.265	-0.256	-0.256	-0.256	-0.447	-0.447	-0.447	-0.388	-0.388	-0.387
.13	.983	-0.386	-0.280	-0.280	-0.271	-0.271	-0.271	-0.485	-0.485	-0.485	-0.425	-0.425	-0.424
.17	.996	-0.420	-0.316	-0.316	-0.302	-0.302	-0.302	-0.523	-0.523	-0.523	-0.463	-0.463	-0.462
		$P_{t,j}/P_\infty = 4.96$			$P_{t,j}/P_\infty = 4.96$			$P_{t,j}/P_\infty = 4.99$			$P_{t,j}/P_\infty = 4.99$		
12.01	.719	-0.028	-0.021	-0.012	-0.023	-0.017	-0.007	-0.103	-0.099	-0.089	-0.051	-0.049	-0.042
10.39	.757	-0.042	-0.071	-0.031	-0.039	-0.071	-0.029	-0.091	-0.087	-0.081	-0.051	-0.049	-0.039
8.76	.795	-0.077	-0.074	-0.071	-0.065	-0.063	-0.079	-0.119	-0.116	-0.116	-0.078	-0.076	-0.076
7.18	.832	-0.120	-0.118	-0.115	-0.110	-0.108	-0.113	-0.172	-0.172	-0.168	-0.124	-0.123	-0.121
5.56	.870	-0.188	-0.149	-0.148	-0.184	-0.184	-0.184	-0.274	-0.273	-0.273	-0.214	-0.213	-0.213
3.93	.908	-0.256	-0.188	-0.188	-0.217	-0.217	-0.217	-0.354	-0.354	-0.354	-0.295	-0.295	-0.295
2.35	.943	-0.313	-0.222	-0.222	-0.203	-0.203	-0.203	-0.393	-0.393	-0.393	-0.333	-0.333	-0.332
1.74	.973	-0.354	-0.265	-0.265	-0.256	-0.256	-0.256	-0.431	-0.431	-0.431	-0.371	-0.371	-0.370
.13	.983	-0.386	-0.280	-0.280	-0.271	-0.271	-0.271	-0.469	-0.469	-0.469	-0.409	-0.409	-0.408
.17	.996	-0.420	-0.316	-0.316	-0.302	-0.302	-0.302	-0.507	-0.507	-0.507	-0.447	-0.447	-0.446
		$P_{t,j}/P_\infty = 6.98$			$P_{t,j}/P_\infty = 6.99$								
12.01	.719							-1.02	-0.99	-0.95	-0.52	-0.52	-0.46
10.39	.757							-1.09	-1.05	-1.01	-0.59	-0.59	-0.53
8.76	.795							-1.19	-1.17	-1.15	-0.60	-0.60	-0.54
7.18	.832							-1.71	-1.71	-1.67	-1.21	-1.21	-1.18
5.56	.870							-2.71	-2.71	-2.71	-2.13	-2.13	-2.13
3.93	.908							-3.50	-3.50	-3.50	-2.79	-2.79	-2.79
2.35	.943							-0.70	-0.69	-0.61	-1.31	-1.31	-1.29
1.74	.973							-1.81	-1.79	-1.75	-0.90	-0.90	-0.88
.13	.983							-1.86	-1.86	-1.87	-0.93	-0.93	-0.91
.17	.996							-1.99	-1.96	-1.99	-0.98	-0.98	-0.97

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TABLE III.- AFTERBODY PRESSURE COEFFICIENTS - Continued

(c) Afterbody II - Continued

 $t_3 = 800^{\circ} F$ 

$\frac{x}{d_3}$	$x$ $\frac{x}{l_{max}}$	Pressure coefficients for -											
		$M_\infty = 0.80$			$M_\infty = 0.90$			$M_\infty = 1.00$			$M_\infty = 1.20$		
		$\theta = 0^{\circ}$	$\theta = 45^{\circ}$	$\theta = 72^{\circ}$	$\theta = 0^{\circ}$	$\theta = 45^{\circ}$	$\theta = 72^{\circ}$	$\theta = 0^{\circ}$	$\theta = 45^{\circ}$	$\theta = 72^{\circ}$	$\theta = 0^{\circ}$	$\theta = 45^{\circ}$	$\theta = 72^{\circ}$
		$P_{t,j}/P_\infty = 1.96$			$P_{t,j}/P_\infty = 2.00$			$P_{t,j}/P_\infty = 2.05$			$P_{t,j}/P_\infty = 2.08$		
12.01	.719	-0.026	-0.021	-0.011	-0.027	-0.019	-0.008	-0.100	-0.097	-0.095	-0.044	-0.043	-0.034
10.39	.757	-.044	-.039	-.021	-.046	-.040	-.035	-.088	-.085	-.078	-.049	-.046	-.040
8.76	.792	-.079	-.076	-.073	-.087	-.087	-.083	-.117	-.117	-.114	-.074	-.072	-.068
7.18	.832	-.120	-.116	-.109	-.145	-.144	-.139	-.171	-.170	-.165	-.128	-.125	-.116
5.56	.870	-.155	-.152	-.151	-.150	-.150	-.150	-.187	-.187	-.185	-.149	-.149	-.140
5.93	.905	-.185	-.182	-.180	-.189	-.188	-.188	-.205	-.205	-.203	-.167	-.167	-.159
2.39	.944	-.014	-.013	-.001	-.009	-.009	-.009	-.077	-.077	-.076	-.035	-.035	-.030
1.73	.983	-.073	-.066	-.061	-.069	-.069	-.069	-.111	-.111	-.109	-.068	-.068	-.063
.50	.995	.125	.121	.120	.128	.128	.128	.157	.157	.154	.101	.101	.094
.17	.996	.188	.187	.188	.197	.196	.196	.205	.205	.203	.160	.160	.158
		.199	.199	.200	.204	.204	.205	.201	.201	.200	.170	.170	.170
		$P_{t,j}/P_\infty = 3.02$			$P_{t,j}/P_\infty = 2.99$			$P_{t,j}/P_\infty = 3.02$			$P_{t,j}/P_\infty = 3.04$		
12.01	.719	-.027	-.022	-.010	-.026	-.017	-.005	-.101	-.096	-.096	-.045	-.044	-.034
10.39	.757	-.042	-.037	-.029	-.042	-.038	-.030	-.088	-.085	-.085	-.049	-.046	-.040
8.76	.792	-.079	-.077	-.072	-.087	-.085	-.080	-.117	-.117	-.114	-.076	-.073	-.069
7.18	.832	-.120	-.118	-.115	-.141	-.141	-.136	-.171	-.170	-.165	-.128	-.126	-.117
5.56	.870	-.155	-.151	-.150	-.158	-.158	-.158	-.187	-.187	-.185	-.149	-.149	-.140
5.93	.905	-.187	-.186	-.180	-.187	-.187	-.187	-.205	-.205	-.203	-.167	-.167	-.158
2.39	.944	-.013	-.017	-.021	-.004	-.006	-.005	-.019	-.019	-.018	-.047	-.047	-.040
1.73	.983	-.068	-.066	-.060	-.067	-.065	-.067	-.123	-.121	-.120	-.068	-.067	-.063
.50	.995	.125	.120	.119	.149	.149	.148	.187	.187	.185	.144	.144	.138
.17	.996	.187	.187	.197	.200	.200	.200	.205	.205	.203	.162	.162	.158
		.197	.197	.201	.211	.211	.211	.210	.210	.209	.170	.170	.170
		$P_{t,j}/P_\infty = 4.99$			$P_{t,j}/P_\infty = 4.99$			$P_{t,j}/P_\infty = 4.98$			$P_{t,j}/P_\infty = 4.98$		
12.01	.719	-.027	-.022	-.011	-.023	-.016	-.008	-.100	-.096	-.096	-.050	-.048	-.038
10.39	.757	-.043	-.038	-.032	-.042	-.036	-.028	-.088	-.085	-.085	-.048	-.046	-.041
8.76	.792	-.078	-.076	-.072	-.084	-.083	-.079	-.117	-.117	-.114	-.075	-.073	-.069
7.18	.832	-.120	-.119	-.116	-.139	-.138	-.135	-.171	-.170	-.165	-.128	-.126	-.117
5.56	.870	-.155	-.151	-.150	-.158	-.158	-.158	-.187	-.187	-.185	-.149	-.149	-.140
5.93	.905	-.187	-.187	-.187	-.188	-.188	-.188	-.205	-.205	-.203	-.167	-.167	-.158
2.39	.944	-.011	-.015	-.019	-.003	-.003	-.003	-.009	-.009	-.008	-.048	-.046	-.038
1.73	.983	-.068	-.068	-.063	-.069	-.068	-.068	-.125	-.125	-.123	-.068	-.067	-.063
.50	.995	.125	.124	.123	.153	.153	.153	.171	.170	.168	.130	.129	.123
.17	.996	.187	.187	.197	.201	.201	.201	.205	.205	.203	.162	.162	.158
		.197	.197	.201	.211	.211	.211	.210	.210	.209	.170	.170	.170
		$P_{t,j}/P_\infty = 6.99$			$P_{t,j}/P_\infty = 7.00$			$P_{t,j}/P_\infty = 6.98$			$P_{t,j}/P_\infty = 6.99$		
12.01	.719	-.029	-.025	-.013	-.025	-.017	-.003	-.100	-.096	-.095	-.046	-.046	-.036
10.39	.757	-.045	-.040	-.032	-.046	-.036	-.028	-.087	-.085	-.085	-.048	-.048	-.042
8.76	.792	-.078	-.076	-.072	-.084	-.083	-.079	-.117	-.117	-.114	-.076	-.075	-.070
7.18	.832	-.120	-.119	-.116	-.141	-.140	-.136	-.171	-.170	-.165	-.128	-.126	-.117
5.56	.870	-.155	-.151	-.150	-.158	-.158	-.158	-.187	-.187	-.185	-.149	-.149	-.140
5.93	.905	-.187	-.187	-.187	-.188	-.188	-.188	-.205	-.205	-.203	-.167	-.167	-.158
2.39	.944	-.011	-.015	-.019	-.005	-.005	-.005	-.009	-.009	-.008	-.048	-.046	-.038
1.73	.983	-.068	-.068	-.063	-.069	-.068	-.068	-.125	-.125	-.123	-.068	-.067	-.063
.50	.995	.125	.124	.123	.153	.153	.153	.171	.170	.168	.130	.129	.123
.17	.996	.187	.187	.197	.201	.201	.201	.205	.205	.203	.162	.162	.158
		.197	.197	.201	.211	.211	.211	.210	.210	.209	.170	.170	.170
		$P_{t,j}/P_\infty = 9.01$			$P_{t,j}/P_\infty = 9.01$			$P_{t,j}/P_\infty = 9.03$			$P_{t,j}/P_\infty = 8.91$		
12.01	.719	-.026	-.022	-.010	-.023	-.016	-.004	-.100	-.096	-.095	-.045	-.045	-.037
10.39	.757	-.042	-.037	-.030	-.043	-.036	-.029	-.088	-.085	-.085	-.049	-.048	-.041
8.76	.792	-.077	-.075	-.071	-.085	-.082	-.078	-.117	-.117	-.114	-.075	-.073	-.069
7.18	.832	-.120	-.117	-.115	-.139	-.139	-.135	-.171	-.170	-.165	-.128	-.126	-.117
5.56	.870	-.155	-.152	-.150	-.158	-.158	-.158	-.187	-.187	-.185	-.149	-.149	-.140
5.93	.905	-.187	-.187	-.187	-.188	-.188	-.188	-.205	-.205	-.203	-.167	-.167	-.158
2.39	.944	-.013	-.013	-.008	-.015	-.009	-.004	-.010	-.010	-.009	-.050	-.048	-.040
1.73	.983	-.068	-.068	-.062	-.069	-.061	-.057	-.123	-.123	-.121	-.068	-.066	-.060
.50	.995	.125	.124	.124	.153	.153	.153	.171	-.170	-.168	.130	.129	.123
.17	.996	.187	.187	.197	.201	.201	.201	.205	.205	.203	.162	.162	.158
		.197	.197	.201	.211	.211	.211	.210	.210	.209	.170	.170	.170
		$P_{t,j}/P_\infty = 10.99$			$P_{t,j}/P_\infty = 11.01$			$P_{t,j}/P_\infty = 10.99$			$P_{t,j}/P_\infty = 11.01$		
12.01	.719							-.102	-.099	-.098	-.045	-.043	-.033
10.39	.757							-.088	-.085	-.078	-.040	-.037	-.030
8.76	.792							-.117	-.115	-.113	-.073	-.071	-.067
7.18	.832							-.171	-.170	-.165	-.117	-.119	-.117
5.56	.870							-.271	-.271	-.271	-.211	-.212	-.211
5.93	.905							-.316	-.315	-.314	-.273	-.273	-.273
2.39	.944							-.094	-.091	-.089	-.057	-.055	-.057
1.73	.983							-.144	-.144	-.144	-.094	-.091	-.089
.50	.995							-.170	-.171	-.172	-.124	-.124	-.123
.17	.996							-.179	-.180	-.180	-.126	-.125	-.126

TABLE III.- AFTERBODY PRESSURE COEFFICIENTS - Continued

(e) Afterbody II - Calculated

 $t_1 = 1,200^{\circ} F$ 

$\frac{x}{d_1}$	$\frac{x}{l_{max}}$	Pressure coefficients for -											
		$M_\infty = 0.80$			$M_\infty = 0.90$			$M_\infty = 1.00$			$M_\infty = 1.10$		
		$\theta = 0^\circ$	$\theta = 45^\circ$	$\theta = 72^\circ$	$\theta = 0^\circ$	$\theta = 45^\circ$	$\theta = 72^\circ$	$\theta = 0^\circ$	$\theta = 45^\circ$	$\theta = 72^\circ$	$\theta = 0^\circ$	$\theta = 45^\circ$	$\theta = 72^\circ$
		$P_{t,J}/P_\infty = 2.01$			$P_{t,J}/P_\infty = 1.96$			$P_{t,J}/P_\infty = 1.98$			$P_{t,J}/P_\infty = 2.09$		
12.01	.719	-0.029	-0.022	-0.011	-0.023	-0.015	-0.006	-0.069	-0.063	-0.065	-0.050	-0.048	-0.037
10.59	.727	-0.041	-0.039	-0.034	-0.040	-0.036	-0.028	-0.065	-0.063	-0.071	-0.051	-0.046	-0.040
8.76	.795	-0.077	-0.074	-0.064	-0.084	-0.082	-0.079	-0.116	-0.114	-0.113	-0.078	-0.079	-0.076
7.18	.832	-0.122	-0.121	-0.117	-0.129	-0.128	-0.125	-0.159	-0.159	-0.154	-0.120	-0.122	-0.120
5.56	.870	-0.152	-0.152	-0.153	-0.153	-0.154	-0.153	-0.185	-0.186	-0.185	-0.143	-0.145	-0.143
3.93	.908	-0.188	-0.188	-0.189	-0.186	-0.186	-0.187	-0.217	-0.217	-0.216	-0.176	-0.178	-0.176
2.35	.945	-0.214	-0.214	-0.215	-0.215	-0.216	-0.215	-0.240	-0.240	-0.240	-0.194	-0.196	-0.194
1.74	.983	-0.238	-0.237	-0.237	-0.236	-0.236	-0.236	-0.260	-0.260	-0.260	-0.214	-0.215	-0.214
.73	.993	-0.253	-0.252	-0.251	-0.251	-0.250	-0.250	-0.274	-0.274	-0.274	-0.223	-0.225	-0.223
.17	.996	-0.258	-0.257	-0.257	-0.257	-0.256	-0.256	-0.289	-0.289	-0.289	-0.237	-0.238	-0.237
		$P_{t,J}/P_\infty = 5.03$			$P_{t,J}/P_\infty = 5.01$			$P_{t,J}/P_\infty = 4.99$			$P_{t,J}/P_\infty = 5.02$		
12.01	.719	-0.028	-0.021	-0.011	-0.022	-0.015	-0.005	-0.101	-0.095	-0.095	-0.052	-0.049	-0.039
10.59	.727	-0.043	-0.040	-0.032	-0.041	-0.037	-0.030	-0.088	-0.085	-0.085	-0.052	-0.051	-0.049
8.76	.795	-0.078	-0.077	-0.073	-0.086	-0.083	-0.080	-0.119	-0.117	-0.115	-0.077	-0.079	-0.076
7.18	.832	-0.121	-0.119	-0.117	-0.126	-0.125	-0.124	-0.156	-0.154	-0.152	-0.122	-0.124	-0.121
5.56	.870	-0.156	-0.154	-0.153	-0.157	-0.156	-0.155	-0.186	-0.187	-0.186	-0.144	-0.145	-0.144
3.93	.908	-0.192	-0.190	-0.189	-0.191	-0.190	-0.189	-0.220	-0.220	-0.220	-0.178	-0.179	-0.178
2.35	.945	-0.215	-0.214	-0.213	-0.215	-0.214	-0.213	-0.245	-0.245	-0.245	-0.196	-0.197	-0.196
1.74	.983	-0.238	-0.237	-0.237	-0.236	-0.236	-0.236	-0.269	-0.269	-0.269	-0.224	-0.225	-0.224
.73	.993	-0.253	-0.252	-0.251	-0.251	-0.250	-0.250	-0.287	-0.287	-0.287	-0.236	-0.237	-0.236
.17	.996	-0.258	-0.257	-0.257	-0.257	-0.256	-0.256	-0.291	-0.291	-0.291	-0.239	-0.240	-0.239
		$P_{t,J}/P_\infty = 4.99$			$P_{t,J}/P_\infty = 5.01$			$P_{t,J}/P_\infty = 4.97$			$P_{t,J}/P_\infty = 4.99$		
12.01	.719	-0.028	-0.022	-0.012	-0.023	-0.016	-0.005	-0.100	-0.095	-0.095	-0.052	-0.049	-0.043
10.59	.727	-0.044	-0.039	-0.033	-0.041	-0.037	-0.030	-0.086	-0.083	-0.083	-0.051	-0.046	-0.040
8.76	.795	-0.078	-0.076	-0.073	-0.084	-0.081	-0.078	-0.118	-0.116	-0.114	-0.078	-0.079	-0.077
7.18	.832	-0.122	-0.120	-0.118	-0.126	-0.125	-0.124	-0.156	-0.154	-0.152	-0.122	-0.124	-0.121
5.56	.870	-0.157	-0.155	-0.153	-0.158	-0.156	-0.155	-0.186	-0.187	-0.186	-0.144	-0.145	-0.144
3.93	.908	-0.192	-0.190	-0.189	-0.191	-0.190	-0.189	-0.220	-0.220	-0.220	-0.178	-0.179	-0.178
2.35	.945	-0.215	-0.214	-0.213	-0.215	-0.214	-0.213	-0.245	-0.245	-0.245	-0.196	-0.197	-0.196
1.74	.983	-0.238	-0.237	-0.237	-0.236	-0.236	-0.236	-0.269	-0.269	-0.269	-0.224	-0.225	-0.224
.73	.993	-0.253	-0.252	-0.251	-0.251	-0.250	-0.250	-0.287	-0.287	-0.287	-0.236	-0.237	-0.236
.17	.996	-0.258	-0.257	-0.257	-0.257	-0.256	-0.256	-0.291	-0.291	-0.291	-0.239	-0.240	-0.239
		$P_{t,J}/P_\infty = 5.01$			$P_{t,J}/P_\infty = 5.00$			$P_{t,J}/P_\infty = 4.99$			$P_{t,J}/P_\infty = 5.00$		
12.01	.719	-0.028	-0.022	-0.012	-0.023	-0.016	-0.005	-0.100	-0.095	-0.095	-0.052	-0.049	-0.044
10.59	.727	-0.044	-0.039	-0.033	-0.040	-0.036	-0.030	-0.086	-0.083	-0.083	-0.051	-0.046	-0.041
8.76	.795	-0.078	-0.076	-0.073	-0.084	-0.081	-0.078	-0.117	-0.115	-0.113	-0.079	-0.080	-0.079
7.18	.832	-0.122	-0.120	-0.118	-0.126	-0.125	-0.124	-0.156	-0.154	-0.152	-0.122	-0.124	-0.121
5.56	.870	-0.157	-0.155	-0.153	-0.158	-0.156	-0.155	-0.186	-0.187	-0.186	-0.144	-0.145	-0.144
3.93	.908	-0.192	-0.190	-0.189	-0.191	-0.190	-0.189	-0.220	-0.220	-0.220	-0.178	-0.179	-0.178
2.35	.945	-0.215	-0.214	-0.213	-0.215	-0.214	-0.213	-0.245	-0.245	-0.245	-0.196	-0.197	-0.196
1.74	.983	-0.238	-0.237	-0.237	-0.236	-0.236	-0.236	-0.269	-0.269	-0.269	-0.224	-0.225	-0.224
.73	.993	-0.253	-0.252	-0.251	-0.251	-0.250	-0.250	-0.287	-0.287	-0.287	-0.236	-0.237	-0.236
.17	.996	-0.258	-0.257	-0.257	-0.257	-0.256	-0.256	-0.291	-0.291	-0.291	-0.239	-0.240	-0.239
		$P_{t,J}/P_\infty = 5.00$			$P_{t,J}/P_\infty = 4.99$			$P_{t,J}/P_\infty = 4.98$			$P_{t,J}/P_\infty = 5.01$		
12.01	.719	-0.028	-0.022	-0.012	-0.023	-0.016	-0.005	-0.100	-0.095	-0.095	-0.052	-0.049	-0.044
10.59	.727	-0.044	-0.039	-0.033	-0.040	-0.036	-0.030	-0.086	-0.083	-0.083	-0.051	-0.046	-0.041
8.76	.795	-0.078	-0.076	-0.073	-0.084	-0.081	-0.078	-0.117	-0.115	-0.113	-0.079	-0.080	-0.079
7.18	.832	-0.122	-0.120	-0.118	-0.126	-0.125	-0.124	-0.156	-0.154	-0.152	-0.122	-0.124	-0.121
5.56	.870	-0.157	-0.155	-0.153	-0.158	-0.156	-0.155	-0.186	-0.187	-0.186	-0.144	-0.145	-0.144
3.93	.908	-0.192	-0.190	-0.189	-0.191	-0.190	-0.189	-0.220	-0.220	-0.220	-0.178	-0.179	-0.178
2.35	.945	-0.215	-0.214	-0.213	-0.215	-0.214	-0.213	-0.245	-0.245	-0.245	-0.196	-0.197	-0.196
1.74	.983	-0.238	-0.237	-0.237	-0.236	-0.236	-0.236	-0.269	-0.269	-0.269	-0.224	-0.225	-0.224
.73	.993	-0.253	-0.252	-0.251	-0.251	-0.250	-0.250	-0.287	-0.287	-0.287	-0.236	-0.237	-0.236
.17	.996	-0.258	-0.257	-0.257	-0.257	-0.256	-0.256	-0.291	-0.291	-0.291	-0.239	-0.240	-0.239
		$P_{t,J}/P_\infty = 4.98$			$P_{t,J}/P_\infty = 4.97$			$P_{t,J}/P_\infty = 4.99$			$P_{t,J}/P_\infty = 5.01$		
12.01	.719	-0.028	-0.022	-0.012	-0.023	-0.016	-0.005	-0.100	-0.095	-0.095	-0.052	-0.049	-0.044
10.59	.727	-0.044	-0.039	-0.033	-0.040	-0.036	-0.030	-0.086	-0.083	-0.083	-0.051	-0.046	-0.041
8.76	.795	-0.078	-0.076	-0.073	-0.084	-0.081	-0.078	-0.117	-0.115	-0.113	-0.079	-0.080	-0.079
7.18	.832	-0.122	-0.120	-0.118	-0.126	-0.125	-0.124	-0.156	-0.154	-0.152	-0.122	-0.124	-0.121
5.56	.870	-0.157	-0.155	-0.153	-0.158	-0.156	-0.155	-0.186	-0.187	-0.186	-0.144	-0.145	-0.144
3.93	.908	-0.192	-0.190	-0.189	-0.191	-0.190	-0.189	-0.220	-0.220	-0.220	-0.178	-0.179	-0.178
2.35	.945	-0.215	-0.214	-0.213	-0.215	-0.214	-0.213	-0.245	-0.245	-0.245	-0.196	-0.197	-0.196
1.74	.983	-0.238	-0.237	-0.237	-0.236	-0.236	-0.236	-0.269	-0.269	-0.269	-0.224	-0.225	-0.224
.73	.993	-0.253	-0.252	-0.251	-0.251	-0.250	-0.250	-0.287	-0.287	-0.287	-0.236	-0.237	-0.236
.17	.996	-0.258	-0.257	-0.257	-0.257	-0.256	-0.256	-0.291	-0.291	-0.291	-0.239	-0.240	-0.239
		$P_{t,J}/P_\infty = 4.97$			$P_{t,J}/P_\infty = 4.96$			$P_{t,J}/P_\infty = 4.98$			$P_{t,J}/P_\infty = 5.01$		
12.01	.719	-0.028	-0.022	-0.012	-0.023	-0.016	-0.005	-0.100	-0.095	-0.095	-0.052	-0.049	-0.044
10.59	.727	-0.044	-0.039	-0.033	-0.040	-0.036	-0.030	-0.086	-0.083	-0			

TABLE III.- AFTERBODY PRESSURE COEFFICIENTS - Continued

(d) Afterbody III

 $t_j = \text{Cold}$ 

$\frac{x}{d_j}$	$\frac{x}{L_{\text{max}}}$	Pressure coefficients for -											
		$M_\infty = 0.80$			$M_\infty = 0.90$			$M_\infty = 1.00$			$M_\infty = 1.10$		
		$\theta = 0^\circ$	$\theta = 45^\circ$	$\theta = 72^\circ$	$\theta = 0^\circ$	$\theta = 45^\circ$	$\theta = 72^\circ$	$\theta = 0^\circ$	$\theta = 45^\circ$	$\theta = 72^\circ$	$\theta = 0^\circ$	$\theta = 45^\circ$	$\theta = 72^\circ$
		$P_{t,j}/P_\infty = 1.04$			$P_{t,j}/P_\infty = 1.04$			$P_{t,j}/P_\infty = 2.01$			$P_{t,j}/P_\infty = 0.94$		
12.01	0.719	-0.028	-0.012	.000	-0.024	-0.006	.008	-0.101	-0.097	-0.080	-0.050	-0.043	-0.050
10.39	.757	-.024	-.019	-.013	-.020	-.014	-.005	-.026	-.020	-.014	-.020	-.016	-.014
8.76	.795	-.026	-.020	-.017	-.026	-.020	-.012	-.024	-.022	-.017	-.026	-.023	-.022
7.18	.832	-.028	-.024	-.020	-.028	-.024	-.017	-.026	-.024	-.019	-.028	-.026	-.025
5.36	.870	-.029	-.029	-.025	-.029	-.025	-.019	-.029	-.027	-.023	-.029	-.027	-.026
3.35	.908	-.031	-.031	-.026	-.031	-.026	-.023	-.033	-.029	-.026	-.031	-.029	-.028
1.34	.935	-.030	-.022	-.027	-.026	-.021	-.014	-.027	-.023	-.019	-.026	-.024	-.023
.73	.963	-.029	-.023	-.020	-.029	-.023	-.014	-.027	-.023	-.019	-.026	-.024	-.023
.56	.995	-.029	-.020	-.018	-.026	-.020	-.014	-.026	-.023	-.019	-.026	-.024	-.023
.17	.996	-.028	-.018	-.018	-.026	-.020	-.014	-.026	-.023	-.019	-.026	-.024	-.023
		$P_{t,j}/P_\infty = 1.97$			$P_{t,j}/P_\infty = 2.00$			$P_{t,j}/P_\infty = 2.10$			$P_{t,j}/P_\infty = 2.00$		
12.01	.719	-.019	-.033	-.000	-.013	-.006	.008	-.101	-.094	-.079	-.049	-.043	-.050
10.39	.757	-.023	-.019	-.014	-.019	-.013	-.007	-.026	-.020	-.014	-.027	-.020	-.022
8.76	.795	-.024	-.019	-.015	-.027	-.018	-.012	-.025	-.020	-.015	-.026	-.020	-.022
7.18	.832	-.027	-.015	-.015	-.028	-.018	-.012	-.024	-.021	-.015	-.029	-.024	-.023
5.36	.870	-.029	-.022	-.016	-.029	-.022	-.016	-.029	-.027	-.023	-.029	-.027	-.026
3.35	.908	-.029	-.020	-.016	-.029	-.022	-.016	-.029	-.027	-.023	-.029	-.027	-.026
1.34	.935	-.028	-.019	-.015	-.028	-.021	-.015	-.028	-.026	-.022	-.028	-.026	-.025
.73	.963	-.028	-.016	-.015	-.028	-.021	-.015	-.027	-.025	-.021	-.028	-.026	-.025
.56	.995	-.026	-.016	-.015	-.026	-.020	-.015	-.026	-.024	-.020	-.026	-.024	-.023
.17	.996	-.027	-.013	-.013	-.027	-.021	-.013	-.027	-.025	-.021	-.027	-.025	-.024
		$P_{t,j}/P_\infty = 3.01$			$P_{t,j}/P_\infty = 2.99$			$P_{t,j}/P_\infty = 3.00$			$P_{t,j}/P_\infty = 3.00$		
12.01	.719	-.019	-.022	.002	-.013	-.004	.009	-.101	-.098	-.080	-.049	-.043	-.048
10.39	.757	-.024	-.018	-.013	-.020	-.014	-.007	-.026	-.020	-.014	-.027	-.020	-.024
8.76	.795	-.031	-.018	-.016	-.026	-.018	-.012	-.028	-.022	-.016	-.032	-.026	-.029
7.18	.832	-.046	-.015	-.014	-.043	-.024	-.014	-.042	-.034	-.026	-.046	-.039	-.040
5.36	.870	-.100	-.055	-.054	-.104	-.100	-.059	-.059	-.059	-.051	-.073	-.063	-.063
3.35	.908	-.202	-.052	-.051	-.202	-.195	-.052	-.052	-.052	-.045	-.158	-.133	-.133
1.34	.935	-.202	-.052	-.051	-.202	-.195	-.052	-.052	-.052	-.045	-.158	-.133	-.133
.73	.963	-.028	-.016	-.015	-.028	-.021	-.015	-.027	-.025	-.021	-.028	-.026	-.025
.56	.995	-.028	-.016	-.015	-.028	-.021	-.015	-.027	-.025	-.021	-.028	-.026	-.025
.17	.996	-.028	-.016	-.015	-.028	-.021	-.015	-.027	-.025	-.021	-.028	-.026	-.025
		$P_{t,j}/P_\infty = 4.96$			$P_{t,j}/P_\infty = 4.97$			$P_{t,j}/P_\infty = 4.97$			$P_{t,j}/P_\infty = 5.00$		
12.01	.719	-.021	-.013	.000	-.018	-.007	.007	-.100	-.098	-.076	-.049	-.043	-.050
10.39	.757	-.023	-.020	-.013	-.020	-.014	-.008	-.027	-.022	-.017	-.027	-.020	-.024
8.76	.795	-.023	-.029	-.027	-.027	-.026	-.014	-.028	-.022	-.017	-.026	-.029	-.024
7.18	.832	-.048	-.005	-.015	-.043	-.042	-.014	-.042	-.034	-.026	-.051	-.049	-.049
5.36	.870	-.102	-.099	-.096	-.104	-.100	-.099	-.096	-.095	-.090	-.178	-.166	-.166
3.35	.908	-.203	-.094	-.093	-.203	-.194	-.093	-.092	-.091	-.086	-.255	-.238	-.238
1.34	.935	-.203	-.094	-.093	-.203	-.194	-.093	-.092	-.091	-.086	-.255	-.238	-.238
.73	.963	-.028	-.016	-.015	-.028	-.021	-.015	-.027	-.025	-.021	-.028	-.026	-.025
.56	.995	-.028	-.016	-.015	-.028	-.021	-.015	-.027	-.025	-.021	-.028	-.026	-.025
.17	.996	-.028	-.016	-.015	-.028	-.021	-.015	-.027	-.025	-.021	-.028	-.026	-.025
		$P_{t,j}/P_\infty = 6.98$			$P_{t,j}/P_\infty = 6.99$								
12.01	.719							-.102	-.095	-.082	-.049	-.043	-.049
10.39	.757							-.056	-.051	-.073	-.037	-.039	-.042
8.76	.795							-.076	-.071	-.067	-.061	-.060	-.059
7.18	.832							-.062	-.061	-.060	-.053	-.050	-.050
5.36	.870							-.055	-.050	-.050	-.073	-.059	-.069
3.35	.908							-.159	-.157	-.157	-.155	-.154	-.154
1.34	.935							-.358	-.360	-.427	-.108	-.396	-.384
.73	.963							-.036	-.028	-.033	-.159	-.150	-.150
.56	.995							-.032	-.029	-.033	-.141	-.142	-.142
.17	.996							-.036	-.035	-.037	-.148	-.148	-.148

TABLE III.-- AFTERBODY PRESSURE COEFFICIENTS - Continued

(e) Afterbody III - Continued

 $t_3 = 800^{\circ} F$ 

$\frac{x}{d_3}$	$\frac{x}{d_{max}}$	Pressure coefficients for -											
		$M_\infty = 0.80$			$M_\infty = 0.90$			$M_\infty = 1.00$			$M_\infty = 1.10$		
		$\theta = 0^\circ$		$\theta = 45^\circ$		$\theta = 72^\circ$		$\theta = 0^\circ$		$\theta = 45^\circ$		$\theta = 72^\circ$	
		$P_{t,j}/P_m = 1.97$			$P_{t,j}/P_m = 2.00$			$P_{t,j}/P_m = 1.99$			$P_{t,j}/P_m = 1.98$		
12.01	.719	-0.020	-0.012	0.001	-0.015	-0.005	0.007	-0.102	-0.097	-0.081	-0.056	-0.031	-0.037
10.39	.737	-0.024	-0.019	-0.013	-0.020	-0.014	-0.008	-0.087	-0.082	-0.072	-0.059	-0.053	-0.049
8.76	.759	-0.032	-0.029	-0.026	-0.038	-0.025	-0.022	-0.073	-0.072	-0.069	-0.063	-0.053	-0.058
7.18	.832	-0.047	-0.043	-0.044	-0.053	-0.043	-0.042	-0.084	-0.082	-0.061	-0.051	-0.050	-0.051
5.36	.870	-0.100	-0.095	-0.094	-0.103	-0.099	-0.099	-0.093	-0.091	-0.092	-0.076	-0.070	-0.071
3.93	.908	-0.203	-0.200	-0.199	-0.203	-0.204	-0.204	-0.200	-0.198	-0.198	-0.158	-0.154	-0.154
2.75	.936	-0.256	-0.259	-0.259	-0.269	-0.267	-0.267	-0.262	-0.251	-0.251	-0.208	-0.207	-0.202
1.54	.964	-0.313	-0.309	-0.309	-0.313	-0.303	-0.303	-0.304	-0.290	-0.290	-0.245	-0.241	-0.237
.73	.983	-0.384	-0.382	-0.382	-0.384	-0.386	-0.386	-0.380	-0.311	-0.311	-0.264	-0.262	-0.252
.50	.993	-0.459	-0.479	-0.476	-0.476	-0.473	-0.473	-0.460	-0.300	-0.302	-0.211	-0.209	-0.195
.17	.996	-0.479	-0.476	-0.475	-0.475	-0.473	-0.473	-0.460	-0.311	-0.309	-0.211	-0.209	-0.195
		$P_{t,j}/P_m = 3.02$			$P_{t,j}/P_m = 2.98$			$P_{t,j}/P_m = 3.00$			$P_{t,j}/P_m = 3.02$		
12.01	.719	-0.021	-0.015	-0.003	-0.015	-0.007	-0.005	-0.104	-0.098	-0.084	-0.054	-0.031	-0.035
10.39	.737	-0.027	-0.020	-0.015	-0.028	-0.013	-0.009	-0.098	-0.094	-0.088	-0.062	-0.037	-0.046
8.76	.759	-0.036	-0.031	-0.028	-0.039	-0.027	-0.022	-0.097	-0.091	-0.071	-0.053	-0.037	-0.045
7.18	.832	-0.049	-0.047	-0.046	-0.046	-0.044	-0.042	-0.087	-0.085	-0.063	-0.050	-0.030	-0.030
5.36	.870	-0.102	-0.095	-0.095	-0.105	-0.099	-0.100	-0.096	-0.093	-0.098	-0.073	-0.070	-0.070
3.93	.908	-0.203	-0.203	-0.203	-0.203	-0.203	-0.203	-0.200	-0.198	-0.198	-0.158	-0.154	-0.154
2.75	.936	-0.262	-0.262	-0.262	-0.273	-0.272	-0.272	-0.266	-0.250	-0.250	-0.215	-0.209	-0.204
1.54	.964	-0.324	-0.323	-0.323	-0.324	-0.323	-0.323	-0.321	-0.261	-0.261	-0.221	-0.218	-0.200
.73	.983	-0.393	-0.393	-0.393	-0.394	-0.393	-0.393	-0.392	-0.291	-0.291	-0.221	-0.219	-0.205
.50	.993	-0.469	-0.473	-0.473	-0.473	-0.473	-0.473	-0.460	-0.319	-0.319	-0.219	-0.217	-0.195
.17	.996	-0.473	-0.473	-0.472	-0.472	-0.471	-0.471	-0.460	-0.319	-0.319	-0.219	-0.217	-0.195
		$P_{t,j}/P_m = 4.96$			$P_{t,j}/P_m = 4.97$			$P_{t,j}/P_m = 4.97$			$P_{t,j}/P_m = 4.97$		
12.01	.719	-0.018	-0.012	0.002	-0.013	-0.008	0.008	-0.102	-0.096	-0.082	-0.054	-0.031	-0.034
10.39	.737	-0.022	-0.018	-0.012	-0.019	-0.013	-0.007	-0.087	-0.082	-0.073	-0.063	-0.032	-0.046
8.76	.759	-0.031	-0.026	-0.024	-0.026	-0.020	-0.016	-0.074	-0.073	-0.068	-0.053	-0.032	-0.037
7.18	.832	-0.046	-0.044	-0.042	-0.043	-0.042	-0.041	-0.064	-0.063	-0.051	-0.039	-0.030	-0.031
5.36	.870	-0.099	-0.092	-0.092	-0.103	-0.098	-0.099	-0.097	-0.092	-0.092	-0.076	-0.070	-0.071
3.93	.908	-0.201	-0.201	-0.201	-0.201	-0.201	-0.201	-0.200	-0.198	-0.198	-0.158	-0.155	-0.155
2.75	.936	-0.264	-0.264	-0.264	-0.271	-0.271	-0.271	-0.265	-0.217	-0.217	-0.187	-0.184	-0.184
1.54	.964	-0.328	-0.327	-0.327	-0.331	-0.331	-0.331	-0.326	-0.266	-0.266	-0.227	-0.224	-0.212
.73	.983	-0.396	-0.395	-0.395	-0.398	-0.397	-0.397	-0.396	-0.271	-0.271	-0.231	-0.228	-0.212
.50	.993	-0.473	-0.473	-0.472	-0.472	-0.471	-0.471	-0.460	-0.322	-0.322	-0.222	-0.219	-0.195
.17	.996	-0.473	-0.473	-0.472	-0.472	-0.471	-0.471	-0.460	-0.319	-0.319	-0.219	-0.217	-0.195
		$P_{t,j}/P_m = 6.99$			$P_{t,j}/P_m = 6.96$			$P_{t,j}/P_m = 6.98$			$P_{t,j}/P_m = 6.97$		
12.01	.719	-0.018	-0.011	0.008	-0.015	-0.006	0.006	-0.102	-0.097	-0.081	-0.056	-0.031	-0.036
10.39	.737	-0.023	-0.019	-0.011	-0.020	-0.014	-0.008	-0.087	-0.082	-0.073	-0.063	-0.036	-0.049
8.76	.759	-0.031	-0.029	-0.026	-0.027	-0.023	-0.022	-0.074	-0.073	-0.068	-0.053	-0.032	-0.037
7.18	.832	-0.046	-0.043	-0.042	-0.044	-0.042	-0.041	-0.064	-0.063	-0.051	-0.039	-0.030	-0.049
5.36	.870	-0.099	-0.092	-0.092	-0.103	-0.098	-0.099	-0.097	-0.092	-0.092	-0.076	-0.070	-0.071
3.93	.908	-0.203	-0.201	-0.201	-0.203	-0.204	-0.204	-0.200	-0.198	-0.198	-0.158	-0.155	-0.155
2.75	.936	-0.267	-0.267	-0.267	-0.271	-0.271	-0.271	-0.265	-0.229	-0.229	-0.189	-0.186	-0.186
1.54	.964	-0.331	-0.329	-0.329	-0.331	-0.330	-0.330	-0.326	-0.287	-0.287	-0.247	-0.244	-0.232
.73	.983	-0.398	-0.397	-0.397	-0.400	-0.399	-0.399	-0.398	-0.342	-0.342	-0.302	-0.299	-0.289
.50	.993	-0.469	-0.473	-0.473	-0.473	-0.473	-0.473	-0.460	-0.340	-0.340	-0.300	-0.297	-0.289
.17	.996	-0.473	-0.473	-0.472	-0.472	-0.471	-0.471	-0.460	-0.319	-0.319	-0.319	-0.317	-0.313
		$P_{t,j}/P_m = 8.97$			$P_{t,j}/P_m = 8.99$			$P_{t,j}/P_m = 8.97$			$P_{t,j}/P_m = 8.97$		
12.01	.719	-0.025	-0.016	-0.003	-0.013	-0.006	0.007	-0.103	-0.097	-0.083	-0.054	-0.030	-0.036
10.39	.737	-0.030	-0.025	-0.017	-0.020	-0.013	-0.008	-0.088	-0.084	-0.077	-0.063	-0.035	-0.048
8.76	.759	-0.037	-0.034	-0.028	-0.036	-0.026	-0.022	-0.074	-0.073	-0.068	-0.053	-0.035	-0.038
7.18	.832	-0.051	-0.050	-0.049	-0.044	-0.044	-0.041	-0.064	-0.063	-0.052	-0.043	-0.030	-0.050
5.36	.870	-0.105	-0.098	-0.098	-0.108	-0.099	-0.100	-0.097	-0.092	-0.091	-0.073	-0.070	-0.071
3.93	.908	-0.209	-0.206	-0.207	-0.206	-0.205	-0.205	-0.200	-0.199	-0.199	-0.158	-0.155	-0.155
2.75	.936	-0.272	-0.270	-0.269	-0.266	-0.265	-0.265	-0.263	-0.229	-0.229	-0.184	-0.181	-0.181
1.54	.964	-0.341	-0.341	-0.341	-0.347	-0.346	-0.346	-0.344	-0.295	-0.295	-0.251	-0.247	-0.246
.73	.983	-0.402	-0.402	-0.401	-0.407	-0.402	-0.402	-0.401	-0.342	-0.342	-0.302	-0.299	-0.297
.50	.993	-0.469	-0.473	-0.473	-0.473	-0.473	-0.473	-0.460	-0.340	-0.340	-0.300	-0.297	-0.295
.17	.996	-0.473	-0.473	-0.472	-0.472	-0.471	-0.471	-0.460	-0.319	-0.319	-0.319	-0.317	-0.313
		$P_{t,j}/P_m = 10.97$			$P_{t,j}/P_m = 11.01$			$P_{t,j}/P_m = 10.97$			$P_{t,j}/P_m = 11.01$		
12.01	.719							-0.101	-0.096	-0.082	-0.059	-0.039	-0.049
10.39	.737							-0.096	-0.091	-0.079	-0.059	-0.039	-0.048
8.76	.759							-0.091	-0.087	-0.077	-0.059	-0.039	-0.045
7.18	.832							-0.084	-0.082	-0.069	-0.053	-0.039	-0.040
5.36	.870							-0.093	-0.090	-0.081	-0.075	-0.050	-0.070
3.93	.908							-0.109	-0.107	-0.100	-0.099	-0.075	-0.075
2.75	.936							-0.108	-0.105	-0.103	-0.103	-0.075	-0.075
1.54	.964							-0.106	-0.104	-0.102	-0.102	-0.075	-0.075
.73	.983							-0.093	-0.091	-0.088	-0.086	-0.063	-0.069
.50	.993							-0.080	-0.078	-0.075	-0.073	-0.050	-0.055
.17	.996							-0.070	-0.067	-0.065	-0.063	-0.040	-0.045

TABLE III.- AFTERBODY PRESSURE COEFFICIENTS - Continued

(d) Afterbody III - Continued

 $t_j = 1,200^{\circ} F$ 

$\frac{x}{d_j}$	$\frac{x}{x_{\max}}$	Pressure coefficients for -											
		M <sub>a</sub> = 0.80			M <sub>a</sub> = 0.90			M <sub>a</sub> = 1.00			M <sub>a</sub> = 1.10		
		s = 0°	s = 45°	s = 72°	s = 0°	s = 45°	s = 72°	s = 0°	s = 45°	s = 72°	s = 0°	s = 45°	s = 72°
		$P_{t,j}/P_m = 1.99$			$P_{t,j}/P_m = 2.02$			$P_{t,j}/P_m = 2.00$			$P_{t,j}/P_m = 1.99$		
12.01	.719	-0.015	-0.009	0.002	-0.015	-0.006	0.005	-0.101	-0.092	-0.083	-0.064	-0.039	-0.027
10.39	.757	-0.021	-0.017	-0.011	-0.021	-0.016	-0.009	-0.089	-0.083	-0.076	-0.056	-0.047	-0.040
8.76	.795	-0.029	-0.027	-0.023	-0.032	-0.027	-0.023	-0.076	-0.073	-0.070	-0.061	-0.059	-0.053
7.18	.832	-0.043	-0.048	-0.042	-0.045	-0.044	-0.042	-0.066	-0.063	-0.063	-0.054	-0.051	-0.051
5.56	.870	-0.097	-0.094	-0.095	-0.106	-0.100	-0.100	-0.097	-0.098	-0.098	-0.076	-0.069	-0.068
3.93	.908	-0.199	-0.199	-0.196	-0.237	-0.235	-0.235	-0.201	-0.199	-0.199	-0.156	-0.153	-0.153
2.35	.943	-0.253	-0.253	-0.261	-0.263	-0.276	-0.293	-0.296	-0.240	-0.276	-0.207	-0.196	-0.189
1.74	.964	-0.314	-0.316	-0.307	-0.318	-0.301	-0.006	-0.013	-0.020	-0.014	-0.110	-0.123	-0.114
.73	.983	-0.385	-0.388	-0.391	-0.395	-0.397	-0.401	-0.010	-0.011	-0.008	-0.099	-0.108	-0.098
.50	.992	-0.455	-0.455	-0.456	-0.455	-0.455	-0.455	-0.013	-0.012	-0.011	-0.102	-0.100	-0.096
.17	.996	-0.692	-0.694	-0.693	-0.695	-0.695	-0.695	-0.011	-0.011	-0.010	-0.100	-0.097	-0.097
		$P_{t,j}/P_m = 3.02$			$P_{t,j}/P_m = 3.02$			$P_{t,j}/P_m = 3.02$			$P_{t,j}/P_m = 3.02$		
12.01	.749	-0.019	-0.011	.000	-0.011	-0.004	.009	-0.101	-0.094	-0.082	-0.062	-0.042	-0.028
10.39	.757	-0.024	-0.018	-0.013	-0.019	-0.018	-0.008	-0.089	-0.082	-0.077	-0.056	-0.049	-0.048
8.76	.795	-0.029	-0.026	-0.026	-0.027	-0.026	-0.024	-0.074	-0.074	-0.070	-0.056	-0.052	-0.052
7.18	.832	-0.045	-0.046	-0.045	-0.046	-0.045	-0.040	-0.063	-0.063	-0.063	-0.051	-0.051	-0.051
5.56	.870	-0.099	-0.094	-0.095	-0.100	-0.099	-0.099	-0.098	-0.098	-0.098	-0.075	-0.070	-0.070
3.93	.908	-0.204	-0.201	-0.201	-0.233	-0.232	-0.232	-0.201	-0.198	-0.198	-0.157	-0.154	-0.154
2.35	.943	-0.265	-0.265	-0.268	-0.271	-0.263	-0.266	-0.293	-0.293	-0.293	-0.256	-0.254	-0.254
1.74	.964	-0.334	-0.334	-0.338	-0.340	-0.325	-0.315	-0.201	-0.208	-0.208	-0.158	-0.155	-0.155
.73	.983	-0.397	-0.398	-0.395	-0.400	-0.393	-0.399	-0.033	-0.030	-0.030	-0.190	-0.187	-0.187
.50	.992	-0.467	-0.461	-0.462	-0.462	-0.459	-0.459	-0.016	-0.015	-0.015	-0.105	-0.105	-0.105
.17	.996	-0.747	-0.749	-0.751	-0.753	-0.753	-0.753	-0.015	-0.015	-0.015	-0.107	-0.107	-0.107
		$P_{t,j}/P_m = 4.96$			$P_{t,j}/P_m = 4.99$			$P_{t,j}/P_m = 4.97$			$P_{t,j}/P_m = 4.99$		
12.01	.749	-0.019	-0.010	.000	-0.012	-0.004	.006	-0.100	-0.093	-0.082	-0.063	-0.049	-0.027
10.39	.757	-0.023	-0.018	-0.012	-0.021	-0.018	-0.009	-0.088	-0.083	-0.076	-0.056	-0.048	-0.040
8.76	.795	-0.029	-0.026	-0.026	-0.032	-0.027	-0.024	-0.076	-0.073	-0.070	-0.059	-0.050	-0.049
7.18	.832	-0.045	-0.044	-0.044	-0.045	-0.045	-0.042	-0.066	-0.065	-0.063	-0.054	-0.051	-0.051
5.56	.870	-0.099	-0.094	-0.095	-0.100	-0.099	-0.099	-0.098	-0.098	-0.098	-0.075	-0.072	-0.072
3.93	.908	-0.204	-0.201	-0.201	-0.231	-0.231	-0.231	-0.201	-0.198	-0.198	-0.157	-0.154	-0.154
2.35	.943	-0.265	-0.265	-0.268	-0.271	-0.263	-0.266	-0.293	-0.293	-0.293	-0.256	-0.254	-0.254
1.74	.964	-0.334	-0.334	-0.338	-0.340	-0.325	-0.315	-0.201	-0.208	-0.208	-0.158	-0.155	-0.155
.73	.983	-0.397	-0.398	-0.395	-0.400	-0.393	-0.399	-0.033	-0.030	-0.030	-0.190	-0.187	-0.187
.50	.992	-0.467	-0.461	-0.462	-0.462	-0.459	-0.459	-0.016	-0.015	-0.015	-0.105	-0.105	-0.105
.17	.996	-0.747	-0.749	-0.751	-0.753	-0.753	-0.753	-0.015	-0.015	-0.015	-0.107	-0.107	-0.107
		$P_{t,j}/P_m = 7.00$			$P_{t,j}/P_m = 7.02$			$P_{t,j}/P_m = 7.00$			$P_{t,j}/P_m = 7.02$		
12.01	.749	-0.019	-0.010	.001	-0.012	-0.006	.006	-0.099	-0.093	-0.082	-0.063	-0.043	-0.027
10.39	.757	-0.023	-0.018	-0.012	-0.021	-0.013	-0.008	-0.088	-0.080	-0.073	-0.056	-0.046	-0.036
8.76	.795	-0.029	-0.026	-0.026	-0.032	-0.027	-0.024	-0.076	-0.070	-0.068	-0.051	-0.048	-0.039
7.18	.832	-0.044	-0.044	-0.044	-0.045	-0.045	-0.042	-0.066	-0.065	-0.063	-0.054	-0.051	-0.051
5.56	.870	-0.099	-0.094	-0.095	-0.100	-0.099	-0.099	-0.098	-0.098	-0.098	-0.075	-0.072	-0.072
3.93	.908	-0.204	-0.201	-0.201	-0.231	-0.231	-0.231	-0.201	-0.198	-0.198	-0.157	-0.154	-0.154
2.35	.943	-0.265	-0.265	-0.268	-0.271	-0.271	-0.271	-0.293	-0.293	-0.293	-0.256	-0.254	-0.254
1.74	.964	-0.334	-0.334	-0.338	-0.340	-0.325	-0.315	-0.201	-0.208	-0.208	-0.158	-0.155	-0.155
.73	.983	-0.397	-0.398	-0.395	-0.400	-0.393	-0.399	-0.033	-0.030	-0.030	-0.190	-0.187	-0.187
.50	.992	-0.467	-0.461	-0.462	-0.462	-0.459	-0.459	-0.016	-0.015	-0.015	-0.105	-0.105	-0.105
.17	.996	-0.747	-0.749	-0.751	-0.753	-0.753	-0.753	-0.015	-0.015	-0.015	-0.107	-0.107	-0.107
		$P_{t,j}/P_m = 8.96$			$P_{t,j}/P_m = 9.00$			$P_{t,j}/P_m = 9.04$			$P_{t,j}/P_m = 9.01$		
12.01	.749	-0.017	-0.009	.002	-0.010	-0.005	.009	-0.099	-0.093	-0.082	-0.060	-0.037	-0.020
10.39	.757	-0.023	-0.017	-0.012	-0.017	-0.011	-0.005	-0.086	-0.082	-0.074	-0.054	-0.046	-0.037
8.76	.795	-0.031	-0.026	-0.026	-0.028	-0.023	-0.019	-0.073	-0.073	-0.069	-0.056	-0.049	-0.041
7.18	.832	-0.046	-0.044	-0.043	-0.046	-0.045	-0.038	-0.063	-0.063	-0.061	-0.052	-0.048	-0.042
5.56	.870	-0.099	-0.093	-0.093	-0.101	-0.096	-0.097	-0.099	-0.091	-0.089	-0.073	-0.068	-0.070
3.93	.908	-0.204	-0.200	-0.199	-0.231	-0.231	-0.231	-0.209	-0.198	-0.197	-0.157	-0.154	-0.154
2.35	.943	-0.265	-0.265	-0.268	-0.271	-0.271	-0.271	-0.293	-0.293	-0.293	-0.256	-0.254	-0.254
1.74	.964	-0.334	-0.334	-0.338	-0.340	-0.325	-0.315	-0.201	-0.208	-0.208	-0.158	-0.155	-0.155
.73	.983	-0.397	-0.398	-0.395	-0.400	-0.393	-0.399	-0.033	-0.030	-0.030	-0.190	-0.187	-0.187
.50	.992	-0.467	-0.461	-0.462	-0.462	-0.459	-0.459	-0.016	-0.015	-0.015	-0.105	-0.105	-0.105
.17	.996	-0.747	-0.749	-0.751	-0.753	-0.753	-0.753	-0.015	-0.015	-0.015	-0.107	-0.107	-0.107
		$P_{t,j}/P_m = 10.98$			$P_{t,j}/P_m = 11.06$			$P_{t,j}/P_m = 11.06$			$P_{t,j}/P_m = 11.06$		
12.01	.749				-0.010	-0.002	.009	-0.102	-0.094	-0.080	-0.061	-0.038	-0.027
10.39	.757				-0.016	-0.012	-0.005	-0.088	-0.083	-0.073	-0.055	-0.046	-0.038
8.76	.795				-0.028	-0.026	-0.019	-0.076	-0.073	-0.063	-0.052	-0.049	-0.042
7.18	.832				-0.040	-0.041	-0.040	-0.065	-0.063	-0.062	-0.056	-0.052	-0.047
5.56	.870				-0.096	-0.095	-0.097	-0.095	-0.095	-0.095	-0.074	-0.068	-0.062
3.93	.908				-0.260	-0.251	-0.250	-0.200	-0.198	-0.197	-0.157	-0.154	-0.154
2.35	.943				-0.267	-0.259	-0.259	-0.205	-0.205	-0.205	-0.166	-0.166	-0.166
1.74	.964				-0.315	-0.304	-0.303	-0.248	-0.248	-0.248	-0.196	-0.196	-0.196
.73	.983				-0.375	-0.362	-0.361	-0.305	-0.305	-0.305	-0.257	-0.257	-0.257
.50	.992				-0.473	-0.458	-0.458	-0.398	-0.398	-0.398	-0.348	-0.348	-0.348
.17	.996				-0.949	-0.936	-0.936	-0.890	-0.890	-0.890	-0.849	-0.849	-0.849

TABLE III.- AFTERBODY PRESSURE COEFFICIENTS - Continued

(a) Afterbody IV

 $t_j = \text{Cold}$ 

$\frac{x}{c_j}$	$\frac{x}{l_{\max}}$	Pressure coefficients for -												
		M <sub>a</sub> = 0.80			M <sub>a</sub> = 0.90			M <sub>a</sub> = 1.00			M <sub>a</sub> = 1.10			
		$\theta = 0^\circ$		$\theta = 45^\circ$	$\theta = 72^\circ$	$\theta = 0^\circ$		$\theta = 45^\circ$	$\theta = 72^\circ$	$\theta = 0^\circ$		$\theta = 45^\circ$	$\theta = 72^\circ$	
		$P_{t,j}/P_m = 1.06$			$P_{t,j}/P_m = 1.08$			$P_{t,j}/P_m = 1.11$			$P_{t,j}/P_m = 1.08$			
$P_{t,j}/P_m = 1.99$														
7.95	.722	-0.043	-0.027	-0.006	-0.036	-0.049	0.003	-0.150	-0.108	-0.097	-0.075	-0.090	-0.019	
7.36	.742	-0.042	-0.028	-0.016	-0.036	-0.041	0.009	-0.119	-0.107	-0.093	-0.055	-0.043	-0.022	
6.22	.762	-0.059	-0.041	-0.017	-0.059	-0.061	-0.006	-0.099	-0.091	-0.088	-0.052	-0.044	-0.038	
5.08	.822	-0.128	-0.121	-0.121	-0.146	-0.144	-0.140	-0.174	-0.176	-0.171	-0.129	-0.123	-0.121	
3.94	.862	-0.147	-0.148	-0.146	-0.176	-0.178	-0.176	-0.263	-0.266	-0.263	-0.215	-0.219	-0.215	
2.80	.902	-0.116	-0.109	-0.113	-0.125	-0.122	-0.127	-0.311	-0.302	-0.305	-0.265	-0.271	-0.269	
1.65	.942	-0.058	-0.058	-0.061	-0.051	-0.052	-0.057	-0.087	-0.087	-0.083	-0.057	-0.057	-0.056	
1.08	.962	.012	.009	.005	.005	.005	.005	.016	.016	.016	.008	.008	.008	
.51	.982	.067	.063	.065	.065	.065	.076	.129	.129	.118	.082	.082	.082	
.25	.992	.098	.095	.095	.119	.115	.115	.158	.158	.158	.107	.107	.107	
.11	.996	.113	.113	.113	.130	.130	.130	.144	.145	.144	.093	.093	.093	
$P_{t,j}/P_m = 2.00$														
7.95	.722	-0.040	-0.025	-0.003	-0.036	-0.040	.004	-0.153	-0.131	-0.100	-0.077	-0.051	-0.000	
7.36	.742	-0.037	-0.028	-0.012	-0.035	-0.035	-0.008	-0.120	-0.108	-0.093	-0.056	-0.043	-0.024	
6.22	.762	-0.056	-0.046	-0.024	-0.059	-0.059	-0.009	-0.101	-0.094	-0.089	-0.053	-0.043	-0.040	
5.08	.822	-0.128	-0.119	-0.116	-0.147	-0.143	-0.139	-0.176	-0.177	-0.175	-0.125	-0.119	-0.117	
3.94	.862	-0.139	-0.131	-0.140	-0.173	-0.174	-0.178	-0.265	-0.268	-0.265	-0.207	-0.210	-0.208	
2.80	.902	-0.103	-0.100	-0.104	-0.118	-0.115	-0.120	-0.214	-0.209	-0.208	-0.161	-0.163	-0.160	
1.65	.942	-0.024	-0.023	-0.026	-0.019	-0.019	-0.024	-0.047	-0.047	-0.046	-0.026	-0.026	-0.026	
1.08	.962	.026	.026	.026	.042	.039	.039	.083	.083	.083	.043	.043	.043	
.51	.982	.086	.082	.079	.104	.102	.099	.159	.159	.158	.103	.102	.102	
.25	.992	.117	.114	.112	.140	.139	.139	.194	.194	.194	.132	.132	.132	
.11	.996	.128	.128	.121	.154	.148	.148	.199	.199	.199	.142	.142	.142	
$P_{t,j}/P_m = 2.01$														
7.95	.722	-0.040	-0.025	-0.003	-0.036	-0.040	.004	-0.153	-0.131	-0.100	-0.077	-0.051	-0.000	
7.36	.742	-0.037	-0.028	-0.012	-0.035	-0.035	-0.008	-0.120	-0.108	-0.093	-0.056	-0.043	-0.024	
6.22	.762	-0.056	-0.046	-0.024	-0.059	-0.059	-0.009	-0.101	-0.094	-0.089	-0.053	-0.043	-0.040	
5.08	.822	-0.128	-0.119	-0.116	-0.147	-0.143	-0.139	-0.176	-0.177	-0.175	-0.125	-0.119	-0.117	
3.94	.862	-0.139	-0.131	-0.140	-0.173	-0.174	-0.178	-0.265	-0.268	-0.265	-0.207	-0.210	-0.208	
2.80	.902	-0.103	-0.100	-0.104	-0.118	-0.115	-0.120	-0.214	-0.209	-0.208	-0.161	-0.163	-0.160	
1.65	.942	-0.024	-0.023	-0.026	-0.019	-0.019	-0.024	-0.047	-0.047	-0.046	-0.026	-0.026	-0.026	
1.08	.962	.026	.026	.026	.042	.039	.039	.083	.083	.083	.043	.043	.043	
.51	.982	.086	.082	.079	.104	.102	.099	.159	.159	.158	.103	.102	.102	
.25	.992	.117	.114	.112	.140	.139	.139	.194	.194	.194	.132	.132	.132	
.11	.996	.128	.128	.121	.154	.148	.148	.199	.199	.199	.142	.142	.142	
$P_{t,j}/P_m = 5.00$														
7.95	.722													
7.36	.742													
6.22	.762													
5.08	.822													
3.94	.862													
2.80	.902													
1.65	.942													
1.08	.962													
.51	.982													
.25	.992													
.11	.996													
$P_{t,j}/P_m = 2.99$														
7.95	.722													
7.36	.742													
6.22	.762													
5.08	.822													
3.94	.862													
2.80	.902													
1.65	.942													
1.08	.962													
.51	.982													
.25	.992													
.11	.996													
$P_{t,j}/P_m = 3.29$ (max.)														
7.95	.722													
7.36	.742													
6.22	.762													
5.08	.822													
3.94	.862													
2.80	.902													
1.65	.942													
1.08	.962													
.51	.982													
.25	.992													
.11	.996													

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TABLE III.- AFTERBODY PRESSURE COEFFICIENTS - Continued

(e) Afterbody IV - Continued

 $t_3 = 800^{\circ} F$ 

$\frac{X}{\delta J}$	$\frac{X}{L_{max}}$	Pressure coefficients for -											
		$M_\infty = 0.80$			$M_\infty = 0.90$			$M_\infty = 1.00$			$M_\infty = 1.10$		
		$\theta = 0^{\circ}$	$\theta = 45^{\circ}$	$\theta = 72^{\circ}$	$\theta = 0^{\circ}$	$\theta = 45^{\circ}$	$\theta = 72^{\circ}$	$\theta = 0^{\circ}$	$\theta = 45^{\circ}$	$\theta = 72^{\circ}$	$\theta = 0^{\circ}$	$\theta = 45^{\circ}$	$\theta = 72^{\circ}$
		$P_{t,J}/P_\infty = 1.99$			$P_{t,J}/P_\infty = 1.97$			$P_{t,J}/P_\infty = 1.96$			$P_{t,J}/P_\infty = 2.01$		
7.95	.722	-.040	-.006	-.003	-.036	-.021	.003	-.158	-.130	-.093	-.079	-.053	-.021
7.36	.762	-.039	-.029	-.013	-.034	-.025	-.008	-.181	-.110	-.055	-.059	-.045	-.026
6.22	.782	-.057	-.057	-.032	-.057	-.059	-.094	-.106	-.093	-.090	-.094	-.077	-.041
5.08	.822	-.129	-.120	-.115	-.114	-.114	-.136	-.177	-.176	-.178	-.123	-.122	-.118
3.94	.862	-.143	-.142	-.139	-.170	-.171	-.169	-.263	-.267	-.263	-.207	-.211	-.207
2.80	.902	-.103	-.100	-.102	-.115	-.115	-.117	-.211	-.204	-.206	-.184	-.185	-.186
1.65	.932	-.083	-.021	-.027	-.013	-.013	-.021	-.044	-.034	-.028	-.266	-.265	-.269
1.08	.952	.030	.030	.026	.029	.029	.039	.084	.079	.076	-.153	-.172	-.194
.51	.982	.091	.089	.086	.125	.125	.106	.136	.134	.134	.046	.056	.053
.23	.998	.124	.122	.122	.149	.149	.143	.149	.151	.152	.079	.073	.077
.11	.996	.137	.134	.133	.160	.158	.156	.197	.198	.196	.087	.088	.088
		$P_{t,J}/P_\infty = 2.98$			$P_{t,J}/P_\infty = 2.96$			$P_{t,J}/P_\infty = 2.99$			$P_{t,J}/P_\infty = 3.00$		
7.95	.722	-.039	-.025	-.005	-.036	-.021	.008	-.150	-.127	-.095	-.080	-.058	-.021
7.36	.762	-.038	-.028	-.012	-.035	-.029	-.007	-.116	-.109	-.088	-.098	-.068	-.026
6.22	.782	-.055	-.055	-.032	-.055	-.059	-.095	-.107	-.109	-.105	-.104	-.105	-.117
5.08	.822	-.122	-.119	-.115	-.116	-.116	-.124	-.245	-.245	-.245	-.123	-.121	-.117
3.94	.862	-.158	-.140	-.139	-.170	-.174	-.169	-.263	-.260	-.260	-.207	-.211	-.207
2.80	.902	-.102	-.100	-.102	-.116	-.115	-.117	-.205	-.204	-.202	-.149	-.156	-.149
1.65	.932	-.023	-.023	-.027	-.016	-.016	-.023	-.061	-.071	-.071	-.266	-.269	-.269
1.08	.952	.029	.027	.025	.044	.042	.037	.076	.074	.071	-.176	-.195	-.214
.51	.982	.091	.087	.085	.110	.108	.104	.135	.135	.135	.029	.029	.016
.23	.998	.123	.119	.119	.144	.141	.141	.158	.151	.154	.070	.067	.068
.11	.996	.138	.131	.130	.156	.155	.152	.198	.199	.196	.079	.078	.080
		$P_{t,J}/P_\infty = 4.99$			$P_{t,J}/P_\infty = 4.99$			$P_{t,J}/P_\infty = 4.99$			$P_{t,J}/P_\infty = 4.99$		
7.95	.722							-.145	-.122	-.093	-.080	-.052	-.020
7.36	.744							-.120	-.099	-.083	-.059	-.046	-.020
6.22	.754							-.091	-.084	-.081	-.054	-.047	-.018
5.08	.792							-.171	-.162	-.159	-.125	-.121	-.117
3.94	.852							-.257	-.250	-.253	-.182	-.189	-.187
2.80	.902							-.050	-.048	-.048	-.246	-.245	-.246
1.65	.932							-.071	-.079	-.079	-.265	-.263	-.265
1.08	.952							-.076	-.071	-.069	-.126	-.126	-.126
.51	.982							-.136	-.135	-.135	-.122	-.122	-.122
.23	.998							-.154	-.154	-.154	-.080	-.076	-.079
.11	.996							-.160	-.161	-.163	-.086	-.087	-.089

CONFIDENTIAL

TABLE III.- AFTERBODY PRESSURE COEFFICIENTS - Continued

(e) Afterbody IV-- Concluded

 $t_1 = 1,200^{\circ} F$ 

$\frac{x}{L_{MAX}}$	$\frac{x}{L}$	Pressure coefficients for -											
		M <sub>a</sub> = 0.80			M <sub>a</sub> = 0.90			M <sub>a</sub> = 1.00			M <sub>a</sub> = 1.10		
		$\theta = 0^{\circ}$	$\theta = 45^{\circ}$	$\theta = 72^{\circ}$	$\theta = 0^{\circ}$	$\theta = 45^{\circ}$	$\theta = 72^{\circ}$	$\theta = 0^{\circ}$	$\theta = 45^{\circ}$	$\theta = 72^{\circ}$	$\theta = 0^{\circ}$	$\theta = 45^{\circ}$	$\theta = 72^{\circ}$
		$P_{t,j}/P_a = 1.99$			$P_{t,j}/P_a = 1.99$			$P_{t,j}/P_a = 2.01$			$P_{t,j}/P_a = 2.01$		
7.95	.722	-0.059	-0.023	-0.003	-0.055	-0.027	0.006	-0.152	-0.126	-0.098	-0.083	-0.069	-0.063
7.36	.742	-0.051	-0.026	-0.010	-0.051	-0.021	-0.003	-0.117	-0.107	-0.093	-0.062	-0.048	-0.048
6.22	.762	-0.055	-0.027	-0.013	-0.056	-0.027	-0.011	-0.100	-0.092	-0.090	-0.059	-0.050	-0.053
5.08	.782	-0.058	-0.029	-0.016	-0.058	-0.029	-0.014	-0.103	-0.106	-0.105	-0.125	-0.125	-0.125
5.94	.802	-0.052	-0.026	-0.013	-0.052	-0.026	-0.013	-0.105	-0.105	-0.105	-0.115	-0.115	-0.115
2.80	.902	-0.052	-0.026	-0.013	-0.052	-0.026	-0.013	-0.105	-0.105	-0.105	-0.115	-0.115	-0.115
1.65	.922	-0.052	-0.026	-0.013	-0.052	-0.026	-0.013	-0.105	-0.105	-0.105	-0.115	-0.115	-0.115
1.08	.942	-0.052	-0.026	-0.013	-0.052	-0.026	-0.013	-0.105	-0.105	-0.105	-0.115	-0.115	-0.115
.91	.962	-0.052	-0.026	-0.013	-0.052	-0.026	-0.013	-0.105	-0.105	-0.105	-0.115	-0.115	-0.115
.23	.982	-0.052	-0.026	-0.013	-0.052	-0.026	-0.013	-0.105	-0.105	-0.105	-0.115	-0.115	-0.115
.11	.996	-0.052	-0.026	-0.013	-0.052	-0.026	-0.013	-0.105	-0.105	-0.105	-0.115	-0.115	-0.115
		$P_{t,j}/P_a = 3.00$			$P_{t,j}/P_a = 2.95$			$P_{t,j}/P_a = 3.00$			$P_{t,j}/P_a = 3.04$		
7.95	.722	-0.056	-0.025	-0.003	-0.056	-0.025	0.003	-0.152	-0.126	-0.097	-0.082	-0.068	-0.063
7.36	.742	-0.054	-0.026	-0.012	-0.055	-0.026	-0.008	-0.117	-0.107	-0.093	-0.062	-0.047	-0.047
6.22	.762	-0.054	-0.026	-0.013	-0.056	-0.026	-0.011	-0.100	-0.095	-0.091	-0.056	-0.049	-0.049
5.08	.782	-0.054	-0.026	-0.013	-0.056	-0.026	-0.011	-0.103	-0.103	-0.103	-0.125	-0.125	-0.125
5.94	.802	-0.054	-0.026	-0.013	-0.056	-0.026	-0.011	-0.105	-0.105	-0.105	-0.125	-0.125	-0.125
2.80	.902	-0.054	-0.026	-0.013	-0.056	-0.026	-0.011	-0.105	-0.105	-0.105	-0.125	-0.125	-0.125
1.65	.922	-0.054	-0.026	-0.013	-0.056	-0.026	-0.011	-0.105	-0.105	-0.105	-0.125	-0.125	-0.125
1.08	.942	-0.054	-0.026	-0.013	-0.056	-0.026	-0.011	-0.105	-0.105	-0.105	-0.125	-0.125	-0.125
.91	.962	-0.054	-0.026	-0.013	-0.056	-0.026	-0.011	-0.105	-0.105	-0.105	-0.125	-0.125	-0.125
.23	.982	-0.054	-0.026	-0.013	-0.056	-0.026	-0.011	-0.105	-0.105	-0.105	-0.125	-0.125	-0.125
.11	.996	-0.054	-0.026	-0.013	-0.056	-0.026	-0.011	-0.105	-0.105	-0.105	-0.125	-0.125	-0.125
		$P_{t,j}/P_a = 5.05$			$P_{t,j}/P_a = 4.99$			$P_{t,j}/P_a = 5.01$					
7.95	.722				-0.055	-0.017	.007	-0.151	-0.127	-0.098	-0.078	-0.060	-0.055
7.36	.742				-0.051	-0.022	.004	-0.117	-0.105	-0.092	-0.059	-0.044	-0.044
6.22	.762				-0.051	-0.027	.002	-0.099	-0.094	-0.082	-0.052	-0.043	-0.043
5.08	.782				-0.053	-0.025	.005	-0.117	-0.117	-0.105	-0.065	-0.050	-0.050
5.94	.802				-0.053	-0.025	.005	-0.117	-0.117	-0.105	-0.065	-0.050	-0.050
2.80	.902				-0.055	-0.025	.005	-0.117	-0.117	-0.105	-0.065	-0.050	-0.050
1.65	.922				-0.055	-0.025	.005	-0.117	-0.117	-0.105	-0.065	-0.050	-0.050
1.08	.942				-0.055	-0.025	.005	-0.117	-0.117	-0.105	-0.065	-0.050	-0.050
.91	.962				-0.055	-0.025	.005	-0.117	-0.117	-0.105	-0.065	-0.050	-0.050
.23	.982				-0.055	-0.025	.005	-0.117	-0.117	-0.105	-0.065	-0.050	-0.050
.11	.996				-0.055	-0.025	.005	-0.117	-0.117	-0.105	-0.065	-0.050	-0.050

CONFIDENTIAL

TABLE III.- AFTERBODY PRESSURE COEFFICIENTS - Continued

(f) Afterbody V

 $t_j = \text{Cold}$ 

$\frac{k}{k_{\infty}}$	$\frac{K}{l_{\max}}$	Pressure coefficients for -											
		$M_{\infty} = 0.80$			$M_{\infty} = 0.90$			$M_{\infty} = 1.00$			$M_{\infty} = 1.10$		
		$\theta = 0^\circ$	$\theta = 45^\circ$	$\theta = 72^\circ$	$\theta = 0^\circ$	$\theta = 45^\circ$	$\theta = 72^\circ$	$\theta = 0^\circ$	$\theta = 45^\circ$	$\theta = 72^\circ$	$\theta = 0^\circ$	$\theta = 45^\circ$	$\theta = 72^\circ$
		$P_{t,j}/P_{\infty} = 1.08$			$P_{t,j}/P_{\infty} = 1.10$			$P_{t,j}/P_{\infty} = 2.03$			$P_{t,j}/P_{\infty} = 1.01$		
7.95	.722	-.039	-.025	-.003	-.034	-.017	.005	-.153	-.131	-.100	-.078	-.055	-.082
7.36	.742	-.037	-.026	-.004	-.031	-.020	.005	-.116	-.109	-.080	-.065	-.040	-.086
6.22	.782	-.049	-.045	-.034	-.055	-.041	-.030	-.100	-.095	-.065	-.054	-.031	-.059
5.08	.822	-.039	-.031	-.021	-.036	-.025	-.025	-.102	-.105	-.082	-.070	-.045	-.060
3.94	.862	-.151	-.147	-.141	-.176	-.172	-.157	-.151	-.148	-.129	-.113	-.093	-.141
2.80	.902	-.156	-.152	-.149	-.176	-.172	-.156	-.151	-.148	-.130	-.117	-.094	-.141
1.65	.942	-.148	-.143	-.139	-.176	-.171	-.157	-.150	-.147	-.129	-.114	-.091	-.139
1.08	.982	-.058	-.048	-.031	-.077	-.065	-.051	-.008	-.010	-.007	-.006	-.032	-.086
.51	.982	.073	.076	.065	.105	.102	.092	.039	.039	.030	.012	-.012	-.087
.23	.992	.134	.153	.187	.150	.149	.146	.058	.058	.049	-.009	-.008	-.015
.11	.996	.135	.155	.190	.166	.166	.163	.057	.057	.056	-.009	-.008	-.008
		$P_{t,j}/P_{\infty} = 2.01$			$P_{t,j}/P_{\infty} = 1.99$			$P_{t,j}/P_{\infty} = 2.00$			$P_{t,j}/P_{\infty} = 2.03$		
7.95	.722	-.039	-.023	.000	-.034	-.014	.006	-.153	-.129	-.098	-.079	-.058	-.025
7.36	.742	-.034	-.024	-.002	-.028	-.018	.006	-.116	-.105	-.076	-.053	-.040	-.007
6.22	.782	-.046	-.042	-.031	-.042	-.030	-.027	-.097	-.095	-.066	-.056	-.045	-.021
5.08	.822	-.082	-.077	-.075	-.086	-.084	-.082	-.102	-.100	-.101	-.072	-.066	-.026
3.94	.862	-.145	-.140	-.136	-.171	-.167	-.157	-.154	-.150	-.148	-.124	-.117	-.140
2.80	.902	-.157	-.151	-.146	-.180	-.176	-.162	-.159	-.156	-.143	-.123	-.116	-.143
1.65	.942	-.148	-.143	-.138	-.176	-.171	-.157	-.150	-.147	-.129	-.113	-.091	-.139
1.08	.982	-.140	-.137	-.133	-.176	-.171	-.157	-.150	-.147	-.129	-.113	-.091	-.139
.51	.982	-.040	-.036	-.026	-.065	-.055	-.045	-.008	-.013	.011	.037	.037	-.059
.23	.992	.094	.091	.083	.124	.117	.111	.058	.059	.049	-.029	-.036	-.060
.11	.996	.146	.154	.182	.157	.155	.152	.063	.063	.063	-.013	-.013	-.013
		$P_{t,j}/P_{\infty} = 2.79$ (max.)			$P_{t,j}/P_{\infty} = 3.00$			$P_{t,j}/P_{\infty} = 2.99$			$P_{t,j}/P_{\infty} = 3.00$		
7.95	.722	-.134	-.022	.000	-.035	-.016	.007	-.153	-.129	-.078	-.077	-.058	-.021
7.36	.742	-.054	-.026	-.001	-.030	-.019	-.007	-.116	-.103	-.076	-.053	-.039	-.004
6.22	.782	-.048	-.041	-.038	-.044	-.040	-.030	-.097	-.098	-.068	-.054	-.050	-.046
5.08	.822	-.085	-.077	-.073	-.089	-.085	-.083	-.103	-.102	-.100	-.069	-.066	-.054
3.94	.862	-.144	-.141	-.136	-.172	-.170	-.165	-.158	-.159	-.155	-.143	-.147	-.139
2.80	.902	-.148	-.143	-.138	-.182	-.178	-.164	-.159	-.156	-.152	-.142	-.140	-.143
1.65	.942	-.148	-.143	-.139	-.176	-.171	-.167	-.162	-.159	-.155	-.142	-.140	-.143
1.08	.982	-.081	-.075	-.064	-.090	-.084	-.070	-.016	-.016	-.014	-.007	-.017	-.017
.51	.982	.045	.043	.038	.118	.114	.107	.052	.053	.049	-.021	-.028	-.030
.23	.992	.144	.145	.158	.162	.160	.157	.051	.051	.051	-.013	-.013	-.013
.11	.996	.164	.164	.162	.177	.174	.171	.057	.057	.057	-.009	-.009	-.009

CONT'D. ON PAGE 11

TABLE III.- AFTERSHOCK PRESSURE COEFFICIENTS - Continued

(f) Afterbody V - Continued

 $t_j = 800^{\circ} F$ 

$\frac{R}{L}$	$\frac{r}{L+1}$	Pressure coefficients for -											
		$M_\infty = 0.80$			$M_\infty = 0.90$			$M_\infty = 1.00$			$M_\infty = 1.10$		
		$\theta = 0^\circ$	$\theta = 45^\circ$	$\theta = 72^\circ$	$\theta = 0^\circ$	$\theta = 45^\circ$	$\theta = 72^\circ$	$\theta = 0^\circ$	$\theta = 45^\circ$	$\theta = 72^\circ$	$\theta = 0^\circ$	$\theta = 45^\circ$	$\theta = 72^\circ$
		$P_{t,j}/P_\infty = 2.01$			$P_{t,j}/P_\infty = 1.96$			$P_{t,j}/P_\infty = 1.96$			$P_{t,j}/P_\infty = 1.99$		
7.35	0.722	-0.056	-0.023	0.000	-0.030	-0.016	0.006	-0.154	-0.131	-0.096	-0.077	-0.053	-0.031
7.36	0.722	-0.055	-0.023	0.001	-0.028	-0.018	0.007	-0.153	-0.130	-0.095	-0.076	-0.052	-0.030
6.53	0.722	-0.047	-0.021	-0.001	-0.023	-0.019	-0.007	-0.099	-0.076	-0.064	-0.053	-0.051	-0.026
5.53	0.722	-0.047	-0.021	-0.001	-0.023	-0.019	-0.007	-0.097	-0.075	-0.063	-0.071	-0.067	-0.023
4.53	0.722	-0.047	-0.021	-0.001	-0.023	-0.019	-0.007	-0.096	-0.074	-0.062	-0.070	-0.066	-0.022
3.53	0.722	-0.047	-0.021	-0.001	-0.023	-0.019	-0.007	-0.095	-0.073	-0.061	-0.069	-0.065	-0.021
2.53	0.722	-0.047	-0.021	-0.001	-0.023	-0.019	-0.007	-0.094	-0.072	-0.060	-0.068	-0.064	-0.020
1.53	0.722	-0.047	-0.021	-0.001	-0.023	-0.019	-0.007	-0.093	-0.071	-0.058	-0.067	-0.063	-0.019
0.53	0.722	-0.047	-0.021	-0.001	-0.023	-0.019	-0.007	-0.092	-0.069	-0.056	-0.066	-0.062	-0.018
-0.53	0.722	-0.047	-0.021	-0.001	-0.023	-0.019	-0.007	-0.091	-0.068	-0.055	-0.065	-0.061	-0.017
-1.53	0.722	-0.047	-0.021	-0.001	-0.023	-0.019	-0.007	-0.090	-0.067	-0.054	-0.064	-0.060	-0.016
-2.53	0.722	-0.047	-0.021	-0.001	-0.023	-0.019	-0.007	-0.089	-0.066	-0.053	-0.063	-0.059	-0.015
-3.53	0.722	-0.047	-0.021	-0.001	-0.023	-0.019	-0.007	-0.088	-0.065	-0.052	-0.062	-0.058	-0.014
-4.53	0.722	-0.047	-0.021	-0.001	-0.023	-0.019	-0.007	-0.087	-0.064	-0.051	-0.061	-0.057	-0.013
-5.53	0.722	-0.047	-0.021	-0.001	-0.023	-0.019	-0.007	-0.086	-0.063	-0.050	-0.060	-0.056	-0.012
-6.53	0.722	-0.047	-0.021	-0.001	-0.023	-0.019	-0.007	-0.085	-0.062	-0.049	-0.059	-0.055	-0.011
-7.53	0.722	-0.047	-0.021	-0.001	-0.023	-0.019	-0.007	-0.084	-0.061	-0.048	-0.058	-0.054	-0.010
7.36	0.722	-0.037	-0.022	-0.001	-0.026	-0.017	0.005	-0.153	-0.130	-0.108	-0.079	-0.053	-0.021
7.35	0.722	-0.037	-0.022	-0.001	-0.026	-0.017	0.005	-0.152	-0.129	-0.107	-0.078	-0.052	-0.020
6.53	0.722	-0.037	-0.022	-0.001	-0.026	-0.017	0.005	-0.151	-0.128	-0.106	-0.077	-0.051	-0.019
5.53	0.722	-0.037	-0.022	-0.001	-0.026	-0.017	0.005	-0.150	-0.127	-0.105	-0.076	-0.050	-0.018
4.53	0.722	-0.037	-0.022	-0.001	-0.026	-0.017	0.005	-0.149	-0.126	-0.104	-0.075	-0.049	-0.017
3.53	0.722	-0.037	-0.022	-0.001	-0.026	-0.017	0.005	-0.148	-0.125	-0.103	-0.074	-0.048	-0.016
2.53	0.722	-0.037	-0.022	-0.001	-0.026	-0.017	0.005	-0.147	-0.124	-0.102	-0.073	-0.047	-0.015
1.53	0.722	-0.037	-0.022	-0.001	-0.026	-0.017	0.005	-0.146	-0.123	-0.101	-0.072	-0.046	-0.014
0.53	0.722	-0.037	-0.022	-0.001	-0.026	-0.017	0.005	-0.145	-0.122	-0.100	-0.071	-0.045	-0.013
-0.53	0.722	-0.037	-0.022	-0.001	-0.026	-0.017	0.005	-0.144	-0.121	-0.099	-0.070	-0.044	-0.012
-1.53	0.722	-0.037	-0.022	-0.001	-0.026	-0.017	0.005	-0.143	-0.120	-0.098	-0.069	-0.043	-0.011
-2.53	0.722	-0.037	-0.022	-0.001	-0.026	-0.017	0.005	-0.142	-0.119	-0.097	-0.068	-0.042	-0.010
-3.53	0.722	-0.037	-0.022	-0.001	-0.026	-0.017	0.005	-0.141	-0.118	-0.096	-0.067	-0.041	-0.009
-4.53	0.722	-0.037	-0.022	-0.001	-0.026	-0.017	0.005	-0.140	-0.117	-0.095	-0.066	-0.040	-0.008
-5.53	0.722	-0.037	-0.022	-0.001	-0.026	-0.017	0.005	-0.139	-0.116	-0.094	-0.065	-0.039	-0.007
-6.53	0.722	-0.037	-0.022	-0.001	-0.026	-0.017	0.005	-0.138	-0.115	-0.093	-0.064	-0.038	-0.006
7.35	0.722	-0.022	-0.021	0.001	-0.026	-0.016	0.007	-0.154	-0.131	-0.111	-0.079	-0.054	-0.023
7.36	0.722	-0.022	-0.021	0.001	-0.026	-0.016	0.007	-0.153	-0.130	-0.109	-0.078	-0.053	-0.022
6.53	0.722	-0.022	-0.021	0.001	-0.026	-0.016	0.007	-0.152	-0.129	-0.108	-0.077	-0.052	-0.021
5.53	0.722	-0.022	-0.021	0.001	-0.026	-0.016	0.007	-0.151	-0.128	-0.107	-0.076	-0.051	-0.020
4.53	0.722	-0.022	-0.021	0.001	-0.026	-0.016	0.007	-0.150	-0.127	-0.106	-0.075	-0.050	-0.019
3.53	0.722	-0.022	-0.021	0.001	-0.026	-0.016	0.007	-0.149	-0.126	-0.105	-0.074	-0.049	-0.018
2.53	0.722	-0.022	-0.021	0.001	-0.026	-0.016	0.007	-0.148	-0.125	-0.104	-0.073	-0.048	-0.017
1.53	0.722	-0.022	-0.021	0.001	-0.026	-0.016	0.007	-0.147	-0.124	-0.103	-0.072	-0.047	-0.016
0.53	0.722	-0.022	-0.021	0.001	-0.026	-0.016	0.007	-0.146	-0.123	-0.102	-0.071	-0.046	-0.015
-0.53	0.722	-0.022	-0.021	0.001	-0.026	-0.016	0.007	-0.145	-0.122	-0.101	-0.070	-0.045	-0.014
-1.53	0.722	-0.022	-0.021	0.001	-0.026	-0.016	0.007	-0.144	-0.121	-0.100	-0.069	-0.044	-0.013
-2.53	0.722	-0.022	-0.021	0.001	-0.026	-0.016	0.007	-0.143	-0.120	-0.099	-0.068	-0.043	-0.012
-3.53	0.722	-0.022	-0.021	0.001	-0.026	-0.016	0.007	-0.142	-0.119	-0.098	-0.067	-0.042	-0.011
-4.53	0.722	-0.022	-0.021	0.001	-0.026	-0.016	0.007	-0.141	-0.118	-0.097	-0.066	-0.041	-0.010
-5.53	0.722	-0.022	-0.021	0.001	-0.026	-0.016	0.007	-0.140	-0.117	-0.096	-0.065	-0.040	-0.009
-6.53	0.722	-0.022	-0.021	0.001	-0.026	-0.016	0.007	-0.139	-0.116	-0.095	-0.064	-0.039	-0.008
7.35	0.722	-0.012	-0.021	0.001	-0.026	-0.016	0.007	-0.154	-0.131	-0.111	-0.079	-0.054	-0.023
7.36	0.722	-0.012	-0.021	0.001	-0.026	-0.016	0.007	-0.153	-0.130	-0.110	-0.078	-0.053	-0.022
6.53	0.722	-0.012	-0.021	0.001	-0.026	-0.016	0.007	-0.152	-0.129	-0.109	-0.077	-0.052	-0.021
5.53	0.722	-0.012	-0.021	0.001	-0.026	-0.016	0.007	-0.151	-0.128	-0.108	-0.076	-0.051	-0.020
4.53	0.722	-0.012	-0.021	0.001	-0.026	-0.016	0.007	-0.150	-0.127	-0.107	-0.075	-0.050	-0.019
3.53	0.722	-0.012	-0.021	0.001	-0.026	-0.016	0.007	-0.149	-0.126	-0.106	-0.074	-0.049	-0.018
2.53	0.722	-0.012	-0.021	0.001	-0.026	-0.016	0.007	-0.148	-0.125	-0.105	-0.073	-0.048	-0.017
1.53	0.722	-0.012	-0.021	0.001	-0.026	-0.016	0.007	-0.147	-0.124	-0.104	-0.072	-0.047	-0.016
0.53	0.722	-0.012	-0.021	0.001	-0.026	-0.016	0.007	-0.146	-0.123	-0.103	-0.071	-0.046	-0.015
-0.53	0.722	-0.012	-0.021	0.001	-0.026	-0.016	0.007	-0.145	-0.122	-0.102	-0.070	-0.045	-0.014
-1.53	0.722	-0.012	-0.021	0.001	-0.026	-0.016	0.007	-0.144	-0.121	-0.101	-0.069	-0.044	-0.013
-2.53	0.722	-0.012	-0.021	0.001	-0.026	-0.016	0.007	-0.143	-0.120	-0.100	-0.068	-0.043	-0.012
-3.53	0.722	-0.012	-0.021	0.001	-0.026	-0.016	0.007	-0.142	-0.119	-0.099	-0.067	-0.042	-0.011
-4.53	0.722	-0.012	-0.021	0.001	-0.026	-0.016	0.007	-0.141	-0.118	-0.098	-0.066	-0.041	-0.010
-5.53	0.722	-0.012	-0.021	0.001	-0.026	-0.016	0.007	-0.140	-0.117	-0.097	-0.065	-0.040	-0.009
-6.53	0.722	-0.012	-0.021	0.001	-0.026	-0.016	0.007	-0.139	-0.116	-0.096	-0.064	-0.039	-0.008
7.35	0.722	-0.002	-0.021	0.001	-0.026	-0.016	0.007	-0.154	-0.131	-0.111	-0.079	-0.054	-0.023
7.36	0.722	-0.002	-0.021	0.001	-0.026	-0.016	0.007	-0.153	-0.130	-0.110	-0.078	-0.053	-0.022
6.53	0.722	-0.002	-0.021	0.001	-0.026	-0.016	0.007	-0.152	-0.129	-0.109	-0.077	-0.052	-0.021
5.53	0.722	-0.002	-0.021	0.001	-0.026	-0.016	0.007	-0.151	-0.128	-0.108	-0.076	-0.051	-0.020
4.53	0.722	-0.002	-0.021	0.001	-0.026	-0.016	0.						

TABLE III.- AFTERBODY PRESSURE COEFFICIENTS - Continued

(x) Afterbody Y - Computed

 $t_j = 1,200^{\circ} F$ 

$\frac{x}{L_{\max}}$	$\frac{x}{L_{\max}}$	Pressure coefficients for -											
		$M_\infty = 0.80$			$M_\infty = 0.90$			$M_\infty = 1.00$			$M_\infty = 1.10$		
		$\theta = 0^\circ$	$\theta = 45^\circ$	$\theta = 72^\circ$	$\theta = 0^\circ$	$\theta = 45^\circ$	$\theta = 72^\circ$	$\theta = 0^\circ$	$\theta = 45^\circ$	$\theta = 72^\circ$	$\theta = 0^\circ$	$\theta = 45^\circ$	$\theta = 72^\circ$
		$P_{t,j}/P_\infty = 1.99$			$P_{t,j}/P_\infty = 1.99$			$P_{t,j}/P_\infty = 2.00$			$P_{t,j}/P_\infty = 1.99$		
7.93	.722	-0.035	-0.019	0.002	-0.029	-0.014	0.009	-0.152	-0.130	-0.099	-0.076	-0.050	-0.018
7.36	.742	-.031	-.021	-.001	-.026	-.016	.006	-.118	-.104	-.082	-.052	-.038	-.009
6.22	.762	-.044	-.039	-.030	-.040	-.036	-.025	-.097	-.095	-.084	-.052	-.049	-.037
5.08	.822	-.079	-.070	-.073	-.084	-.080	-.070	-.103	-.108	-.102	-.067	-.063	-.061
3.94	.862	-.142	-.138	-.135	-.153	-.155	-.158	-.194	-.191	-.183	-.145	-.144	-.137
2.80	.902	-.182	-.177	-.176	-.189	-.185	-.184	-.210	-.205	-.204	-.142	-.137	-.136
1.65	.942	-.103	-.102	-.105	-.109	-.108	-.102	-.161	-.165	-.166	-.107	-.103	-.102
1.08	.962	-.046	-.044	-.041	-.045	-.040	-.033	-.062	-.067	-.067	-.035	-.035	-.035
.51	.982	.110	.106	.099	.135	.130	.124	.044	.059	.041	.026	.026	.027
.23	.992	.165	.162	.158	.174	.174	.171	.051	.049	.052	.009	.014	.013
.11	.995	.180	.176	.175	.189	.184	.180	.053	.053	.053	.007	.010	.006
		$P_{t,j}/P_\infty = 3.01$			$P_{t,j}/P_\infty = 2.98$			$P_{t,j}/P_\infty = 3.00$			$P_{t,j}/P_\infty = 3.02$		
7.93	.722	-.036	-.021	-.000	-.050	-.014	.009	-.152	-.151	-.100	-.076	-.069	-.018
7.36	.742	-.032	-.023	-.005	-.027	-.016	.006	-.118	-.109	-.082	-.052	-.051	-.009
6.22	.782	-.046	-.041	-.031	-.051	-.037	-.027	-.097	-.095	-.085	-.050	-.047	-.036
5.08	.822	-.081	-.077	-.076	-.084	-.081	-.079	-.104	-.105	-.102	-.065	-.062	-.060
3.94	.862	-.144	-.140	-.139	-.169	-.165	-.159	-.194	-.191	-.184	-.146	-.145	-.136
2.80	.902	-.185	-.179	-.180	-.189	-.182	-.184	-.211	-.206	-.205	-.140	-.137	-.137
1.65	.942	-.106	-.105	-.113	-.103	-.103	-.112	-.161	-.161	-.161	-.107	-.106	-.105
1.08	.962	-.012	-.016	-.003	.015	.007	-.005	.022	.007	.005	.005	.005	-.015
.51	.982	.105	.103	.096	.133	.129	.122	.044	.039	.042	.003	.003	-.003
.23	.992	.150	.148	.144	.175	.175	.171	.051	.049	.052	.004	.003	-.004
.11	.995	.171	.176	.175	.184	.184	.180	.054	.053	.050	.013	.017	-.013
		$P_{t,j}/P_\infty = 4.55$ (max.)			$P_{t,j}/P_\infty = 5.01$			$P_{t,j}/P_\infty = 4.97$			$P_{t,j}/P_\infty = 4.99$		
7.93	.722	-.036	-.022	-.001	-.031	-.015	.008	-.153	-.150	-.100	-.077	-.070	-.013
7.36	.742	-.032	-.020	-.003	-.028	-.013	.004	-.118	-.109	-.082	-.052	-.050	-.013
6.22	.782	-.042	-.042	-.035	-.044	-.033	-.028	-.098	-.093	-.082	-.052	-.049	-.038
5.08	.822	-.081	-.078	-.076	-.087	-.084	-.080	-.104	-.103	-.102	-.067	-.065	-.063
3.94	.862	-.144	-.140	-.139	-.169	-.165	-.159	-.194	-.191	-.184	-.147	-.144	-.136
2.80	.902	-.183	-.178	-.176	-.189	-.185	-.184	-.210	-.205	-.204	-.140	-.137	-.137
1.65	.942	-.108	-.100	-.107	-.096	-.096	-.105	-.173	-.172	-.167	-.107	-.104	-.104
1.08	.962	-.003	-.008	-.016	.024	.018	.009	.080	.007	.008	.008	.007	-.005
.51	.982	.117	.114	.109	.144	.141	.136	.046	.041	.044	.008	.005	-.005
.23	.992	.159	.158	.159	.182	.181	.181	.055	.052	.056	.014	.010	-.010
.11	.995	.185	.185	.185	.192	.192	.193	.059	.058	.054	.011	.015	-.014

CONFIDENTIAL

TABLE III.- AFTERBODY PRESSURE COEFFICIENTS - Continued

(g) Afterbody VI

 $t_1 = \text{Cold}$ 

$\frac{x}{c_j}$	$\frac{x}{L_{\infty}}$	Pressure coefficients for -											
		M <sub>∞</sub> = 0.80			M <sub>∞</sub> = 0.90			M <sub>∞</sub> = 1.00			M <sub>∞</sub> = 1.10		
		s = 0°	s = 45°	s = 72°	s = 0°	s = 45°	s = 72°	s = 0°	s = 45°	s = 72°	s = 0°	s = 45°	s = 72°
		$P_{t,j}/P_m = 1.05$			$P_{t,j}/P_m = 1.01$			$P_{t,j}/P_m = 0.90$			$P_{t,j}/P_m = 0.87$		
7.95	.722	-.030	-.018	.005	-.005	-.010	.001	-.151	-.189	-.100	-.076	-.088	-.082
7.36	.742	-.025	-.016	.003	-.019	-.008	.007	-.119	-.107	-.097	-.051	-.043	-.030
6.22	.762	-.027	-.024	.015	-.019	-.016	.007	-.087	-.095	-.075	-.050	-.047	-.035
5.08	.822	-.058	-.036	.028	-.028	-.028	.020	-.071	-.072	-.068	-.032	-.033	-.042
3.94	.862	-.062	-.061	.060	-.055	-.054	.054	-.066	-.065	-.065	-.053	-.053	-.056
2.80	.902	-.152	-.158	.150	-.155	-.157	.156	-.125	-.120	-.130	-.086	-.092	-.093
1.69	.942	-.331	-.329	.329	-.453	-.448	.457	-.383	-.376	-.383	-.299	-.306	-.309
1.06	.962	-.239	-.238	.250	-.153	-.172	.190	-.173	-.156	-.157	-.127	-.143	-.149
.51	.982	.036	.034	.040	.003	.000	.007	.058	.067	.061	.122	.125	.125
.25	.992	.043	.042	.043	.007	.008	.012	.083	.088	.084	.124	.123	.124
.11	.995	.045	.044	.045	.008	.009	.012	.086	.084	.084	.124	.127	.125
		$P_{t,j}/P_m = 1.96$			$P_{t,j}/P_m = 1.95$			$P_{t,j}/P_m = 2.00$			$P_{t,j}/P_m = 2.02$		
7.95	.722	-.050	-.017	.004	-.022	-.009	.014	-.152	-.151	-.099	-.078	-.082	-.082
7.36	.742	-.047	-.016	.002	-.019	-.007	.007	-.120	-.109	-.099	-.055	-.059	-.059
6.22	.762	-.051	-.024	.013	-.019	-.013	.009	-.090	-.085	-.078	-.051	-.048	-.045
5.08	.822	-.063	-.059	.053	-.053	-.047	.049	-.062	-.064	-.053	-.033	-.033	-.042
3.94	.862	-.063	-.063	.061	-.056	-.052	.051	-.065	-.065	-.065	-.034	-.034	-.034
2.80	.902	-.150	-.152	.149	-.152	-.144	.155	-.128	-.120	-.130	-.089	-.098	-.093
1.69	.942	-.316	-.321	.328	-.442	-.440	.450	-.385	-.378	-.383	-.302	-.305	-.300
1.06	.962	-.202	-.204	.205	-.109	-.103	.104	-.110	-.112	-.109	-.153	-.162	-.165
.51	.982	.050	.050	.050	.026	.012	.003	-.008	-.007	-.007	-.153	-.162	-.157
.25	.992	.046	.036	.051	.019	.007	.000	-.005	-.003	-.003	-.154	-.157	-.156
.11	.995	.038	.031	.029	.016	.004	-.002	-.061	-.073	-.081	-.104	-.117	-.116
		$P_{t,j}/P_m = 2.66$ (max.)			$P_{t,j}/P_m = 2.87$ (max.)			$P_{t,j}/P_m = 3.01$			$P_{t,j}/P_m = 3.01$		
7.95	.722	-.028	-.015	.004	-.023	-.010	.013	-.153	-.131	-.102	-.078	-.052	-.038
7.36	.742	-.025	-.014	.003	-.019	-.008	.007	-.120	-.108	-.097	-.056	-.041	-.036
6.22	.762	-.028	-.020	.014	-.021	-.017	.006	-.090	-.087	-.079	-.050	-.046	-.035
5.08	.822	-.034	-.034	.026	-.029	-.027	.022	-.073	-.074	-.065	-.032	-.031	-.042
3.94	.862	-.063	-.069	.067	-.057	-.053	.054	-.067	-.066	-.065	-.037	-.036	-.041
2.80	.902	-.154	-.150	.145	-.144	-.143	.144	-.125	-.120	-.130	-.085	-.098	-.093
1.69	.942	-.316	-.312	.313	-.446	-.445	.455	-.381	-.376	-.383	-.301	-.305	-.303
1.06	.962	-.218	-.220	.224	-.122	-.120	.125	-.135	-.131	-.129	-.182	-.192	-.193
.51	.982	.042	.042	.027	.005	-.003	-.012	-.092	-.093	-.094	-.189	-.191	-.192
.25	.992	.038	.028	.029	.005	-.003	-.012	-.092	-.090	-.093	-.197	-.198	-.199
.11	.995	.027	.028	.029	-.005	-.003	-.012	-.090	-.100	-.103	-.196	-.198	-.199

CONFIDENTIAL

TABLE III.- AFTERBODY PRESSURE COEFFICIENTS - Continued

(a) Afterbody VI - Continued

 $t_j = 8000^{\circ} F$ 

$\frac{x}{d_3}$	$\frac{x}{l_{max}}$	Pressure coefficients for -											
		M <sub>∞</sub> = 0.80			M <sub>∞</sub> = 0.90			M <sub>∞</sub> = 1.00			M <sub>∞</sub> = 1.10		
		$\theta = 0^\circ$	$\theta = 45^\circ$	$\theta = 72^\circ$	$\theta = 0^\circ$	$\theta = 45^\circ$	$\theta = 72^\circ$	$\theta = 0^\circ$	$\theta = 45^\circ$	$\theta = 72^\circ$	$\theta = 0^\circ$	$\theta = 45^\circ$	$\theta = 72^\circ$
		$P_{t,j}/P_\infty = 2.00$			$P_{t,j}/P_\infty = 2.00$			$P_{t,j}/P_\infty = 2.01$			$P_{t,j}/P_\infty = 2.00$		
7.95	.722	-0.051	-0.026	0.005	-0.065	-0.030	0.038	-0.152	-0.130	-0.102	-0.082	-0.054	-0.034
7.36	.712	-0.026	-0.016	-0.000	-0.020	-0.010	0.007	-0.119	-0.110	-0.095	-0.061	-0.044	-0.032
6.22	.702	-0.025	-0.016	-0.015	-0.021	-0.017	0.006	-0.089	-0.086	-0.076	-0.053	-0.041	-0.030
5.08	.622	-0.019	-0.016	-0.016	-0.020	-0.019	0.003	-0.075	-0.073	-0.067	-0.056	-0.044	-0.035
5.94	.652	-0.026	-0.018	-0.018	-0.027	-0.024	0.004	-0.067	-0.067	-0.067	-0.056	-0.044	-0.037
2.80	.902	-0.135	-0.119	-0.118	-0.155	-0.157	-0.155	-0.127	-0.151	-0.131	-0.098	-0.098	-0.092
1.65	.942	-0.109	-0.093	-0.093	-0.141	-0.141	-0.140	-0.101	-0.127	-0.121	-0.093	-0.093	-0.087
1.08	.952	-0.181	-0.159	-0.158	-0.207	-0.198	-0.193	-0.160	-0.187	-0.181	-0.142	-0.142	-0.135
.51	.952	.027	.034	.029	.026	.024	.004	.001	.001	.001	.001	.001	.001
.23	.952	.008	.024	.021	.017	.001	.001	.001	.001	.001	.001	.001	.001
.11	.950	.048	.075	.032	.019	.000	.003	.003	.003	.003	.001	.001	.001
		$P_{t,j}/P_\infty = 2.98$			$P_{t,j}/P_\infty = 5.01$			$P_{t,j}/P_\infty = 2.99$			$P_{t,j}/P_\infty = 5.02$		
7.95	.722	-0.009	-0.015	.006	-0.003	-0.009	.013	-0.151	-0.129	-0.099	-0.061	-0.072	-0.080
7.36	.712	-0.009	-0.014	-0.001	-0.018	-0.006	.009	-0.118	-0.107	-0.097	-0.068	-0.051	-0.038
6.22	.702	-0.006	-0.014	-0.013	-0.021	-0.014	-0.003	-0.088	-0.086	-0.076	-0.056	-0.041	-0.030
5.08	.622	-0.005	-0.013	-0.027	-0.026	-0.027	-0.018	-0.071	-0.072	-0.064	-0.057	-0.046	-0.035
5.94	.652	-0.006	-0.019	-0.019	-0.023	-0.021	-0.021	-0.065	-0.064	-0.063	-0.056	-0.044	-0.035
2.80	.902	-0.147	-0.119	-0.118	-0.151	-0.154	-0.153	-0.126	-0.126	-0.130	-0.090	-0.090	-0.084
1.65	.942	-0.132	-0.112	-0.112	-0.141	-0.141	-0.140	-0.116	-0.128	-0.126	-0.093	-0.093	-0.089
1.08	.952	-0.191	-0.177	-0.177	-0.201	-0.192	-0.197	-0.165	-0.189	-0.186	-0.145	-0.145	-0.139
.51	.952	.053	.029	.020	.024	.003	.008	.004	.005	.005	.005	.005	.005
.23	.952	.043	.028	.025	.014	.003	.006	.007	.007	.007	.001	.001	.001
.11	.942	.042	.027	.025	.014	.004	.006	.007	.007	.007	.001	.001	.001
		$P_{t,j}/P_\infty = 4.51$ (max.)			$P_{t,j}/P_\infty = 4.55$ (max.)			$P_{t,j}/P_\infty = 4.56$			$P_{t,j}/P_\infty = 4.56$		
7.95	.722				.029	.030	.014	-0.147	-0.126	-0.098	-0.085	-0.066	-0.050
7.36	.712				.020	.007	.007	-0.115	-0.103	-0.093	-0.062	-0.047	-0.034
6.22	.702				.020	.016	.006	.085	.080	.071	.056	.042	.030
5.08	.622				.029	.027	.020	.057	.057	.059	.036	.026	.016
5.94	.652				.024	.023	.019	.062	.061	.062	.042	.033	.023
2.80	.902				.127	.156	.124	.122	.127	.124	.093	.093	.084
1.65	.942				.124	.144	.124	.121	.123	.121	.091	.091	.081
1.08	.952				.128	.144	.127	.121	.129	.128	.094	.094	.081
.51	.952				.020	.002	.006	.085	.107	.115	.128	.119	.119
.23	.952				.011	.006	.012	.098	.116	.122	.120	.103	.103
.11	.950				.010	.009	.010	.094	.117	.122	.120	.100	.100

TABLE III-- AFTERBODY PRESSURE COEFFICIENTS - Continued

(g) Afterbody VI - Concluded

 $t_j = 1,200^{\circ} F$ 

$\frac{x}{d_j}$	$\frac{x}{l_{max}}$	Pressure coefficients for -											
		M <sub>∞</sub> = 0.80			M <sub>∞</sub> = 0.90			M <sub>∞</sub> = 1.00			M <sub>∞</sub> = 1.10		
		$\theta = 0^{\circ}$	$\theta = 45^{\circ}$	$\theta = 72^{\circ}$	$\theta = 0^{\circ}$	$\theta = 45^{\circ}$	$\theta = 72^{\circ}$	$\theta = 0^{\circ}$	$\theta = 45^{\circ}$	$\theta = 72^{\circ}$	$\theta = 0^{\circ}$	$\theta = 45^{\circ}$	$\theta = 72^{\circ}$
		$P_{t,j}/P_{\infty} = 1.97$			$P_{t,j}/P_{\infty} = 1.96$			$P_{t,j}/P_{\infty} = 2.05$			$P_{t,j}/P_{\infty} = 1.97$		
7.93	.722	-0.051	-0.018	0.005	-0.023	-0.009	0.015	-0.152	-0.130	-0.100	-0.080	-0.094	-0.023
7.36	.742	-0.027	-0.016	-0.002	-0.018	-0.008	0.006	-0.120	-0.108	-0.096	-0.059	-0.043	-0.030
6.22	.782	-0.038	-0.014	-0.015	-0.019	-0.015	-0.006	-0.089	-0.086	-0.074	-0.054	-0.049	-0.057
5.03	.822	-0.036	-0.014	-0.015	-0.019	-0.015	-0.006	-0.072	-0.072	-0.062	-0.051	-0.053	-0.053
3.94	.862	-0.052	-0.010	-0.019	-0.024	-0.021	-0.015	-0.057	-0.056	-0.055	-0.055	-0.055	-0.056
2.80	.902	-0.149	-0.151	-0.149	-0.152	-0.156	-0.154	-0.127	-0.130	-0.129	-0.099	-0.093	-0.094
1.93	.942	-0.312	-0.314	-0.312	-0.311	-0.315	-0.314	-0.281	-0.276	-0.276	-0.204	-0.200	-0.201
1.15	.982	-0.177	-0.180	-0.180	-0.181	-0.180	-0.178	-0.142	-0.142	-0.142	-0.135	-0.135	-0.135
.73	.922	-0.050	-0.053	-0.053	-0.050	-0.053	-0.053	-0.036	-0.036	-0.036	-0.037	-0.036	-0.036
.25	.952	-0.050	-0.053	-0.052	-0.050	-0.053	-0.053	-0.039	-0.039	-0.039	-0.039	-0.039	-0.039
.11	.992	-0.049	-0.054	-0.052	-0.050	-0.051	-0.052	-0.039	-0.039	-0.039	-0.039	-0.039	-0.039
		$P_{t,j}/P_{\infty} = 3.01$			$P_{t,j}/P_{\infty} = 2.97$			$P_{t,j}/P_{\infty} = 2.99$			$P_{t,j}/P_{\infty} = 2.99$		
7.93	.722	-0.051	-0.016	.004	-0.023	-0.009	.015	-0.152	-0.129	-0.100	-0.078	-0.053	-0.023
7.36	.742	-0.027	-0.015	-.001	-0.019	-0.008	0.008	-0.120	-0.108	-0.098	-0.057	-0.042	-0.059
6.22	.782	-0.038	-0.014	-0.016	-0.019	-0.015	-0.007	-0.089	-0.086	-0.074	-0.051	-0.047	-0.053
5.03	.822	-0.037	-0.014	-0.016	-0.019	-0.015	-0.007	-0.072	-0.072	-0.065	-0.054	-0.053	-0.054
3.94	.862	-0.060	-0.056	-0.056	-0.059	-0.057	-0.052	-0.058	-0.058	-0.056	-0.055	-0.056	-0.056
2.80	.902	-0.149	-0.150	-0.148	-0.153	-0.154	-0.155	-0.127	-0.129	-0.129	-0.088	-0.088	-0.089
1.93	.942	-0.318	-0.320	-0.321	-0.315	-0.314	-0.314	-0.283	-0.283	-0.281	-0.205	-0.205	-0.205
1.15	.982	-0.179	-0.180	-0.180	-0.184	-0.185	-0.184	-0.144	-0.144	-0.144	-0.135	-0.135	-0.135
.73	.922	-0.050	-0.053	-0.052	-0.050	-0.053	-0.053	-0.036	-0.036	-0.036	-0.037	-0.036	-0.036
.25	.952	-0.050	-0.053	-0.052	-0.050	-0.053	-0.053	-0.039	-0.039	-0.039	-0.039	-0.039	-0.039
.11	.992	-0.049	-0.050	-0.050	-0.050	-0.050	-0.050	-0.039	-0.039	-0.039	-0.039	-0.039	-0.039
		$P_{t,j}/P_{\infty} = 4.31$ (max.)			$P_{t,j}/P_{\infty} = 4.35$			$P_{t,j}/P_{\infty} = 4.50$			$P_{t,j}/P_{\infty} = 4.56$		
7.93	.722	-0.051	-0.016	.006	-0.023	-0.009	.013	-0.152	-0.130	-0.103	-0.071	-0.054	-0.026
7.36	.742	-0.027	-0.015	-.001	-0.018	-0.007	0.006	-0.120	-0.107	-0.097	-0.059	-0.044	-0.031
6.22	.782	-0.038	-0.014	-0.022	-0.014	-0.014	-0.017	-0.089	-0.086	-0.076	-0.054	-0.041	-0.038
5.03	.822	-0.038	-0.014	-0.027	-0.027	-0.026	-0.020	-0.072	-0.073	-0.065	-0.051	-0.039	-0.035
3.94	.862	-0.061	-0.058	-0.059	-0.059	-0.053	-0.053	-0.056	-0.066	-0.066	-0.057	-0.055	-0.058
2.80	.902	-0.148	-0.151	-0.150	-0.152	-0.153	-0.153	-0.127	-0.130	-0.130	-0.089	-0.089	-0.093
1.93	.942	-0.319	-0.323	-0.320	-0.320	-0.320	-0.321	-0.282	-0.282	-0.282	-0.204	-0.204	-0.205
1.15	.982	-0.179	-0.181	-0.180	-0.184	-0.185	-0.185	-0.144	-0.144	-0.144	-0.135	-0.135	-0.135
.73	.922	-0.050	-0.053	-0.052	-0.050	-0.053	-0.053	-0.036	-0.036	-0.036	-0.037	-0.036	-0.036
.25	.952	-0.050	-0.053	-0.052	-0.050	-0.053	-0.053	-0.039	-0.039	-0.039	-0.039	-0.039	-0.039
.11	.992	-0.049	-0.050	-0.050	-0.050	-0.050	-0.050	-0.039	-0.039	-0.039	-0.039	-0.039	-0.039

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TABLE III.- AFTERBODY PRESSURE COEFFICIENTS - Continued

(h) Afterbody VII

**t<sub>1</sub>** = Cold

x $\frac{d_1}{d_2}$	k $k_{\max}$	Pressure coefficients for -											
		K <sub>m</sub> = 0.80			K <sub>m</sub> = 0.90			K <sub>m</sub> = 1.00			K <sub>m</sub> = 1.10		
		θ = 0°	θ = 45°	θ = 72°	θ = 0°	θ = 45°	θ = 72°	θ = 0°	θ = 45°	θ = 72°	θ = 0°	θ = 45°	θ = 72°
		$P_{t,J}/P_m = 1.07$			$P_{t,J}/P_m = 1.09$			$P_{t,J}/P_m = 1.15$			$P_{t,J}/P_m = 1.12$		
12.01	0.719	-0.036	-0.029	-0.021	-0.081	-0.025	-0.015	-0.115	-0.098	-0.070	-0.029	-0.053	-0.017
10.59	.757	-0.053	-0.049	-0.042	-0.052	-0.047	-0.043	-0.069	-0.063	-0.079	-0.058	-0.054	-0.017
8.76	.797	-0.107	-0.105	-0.102	-0.123	-0.122	-0.119	-0.149	-0.147	-0.147	-0.112	-0.111	-0.105
7.18	.832	-0.127	-0.125	-0.124	-0.135	-0.134	-0.131	-0.151	-0.141	-0.140	-0.117	-0.116	-0.110
5.56	.870	-0.147	-0.145	-0.146	-0.159	-0.159	-0.159	-0.179	-0.177	-0.177	-0.147	-0.146	-0.140
3.93	.908	-0.166	-0.164	-0.165	-0.171	-0.171	-0.171	-0.191	-0.189	-0.189	-0.159	-0.158	-0.153
2.59	.947	-0.185	-0.183	-0.182	-0.191	-0.191	-0.191	-0.211	-0.209	-0.209	-0.179	-0.178	-0.172
1.34	.984	-0.207	-0.205	-0.204	-0.214	-0.214	-0.214	-0.234	-0.232	-0.232	-0.199	-0.198	-0.192
.75	.983	-0.226	-0.224	-0.223	-0.231	-0.231	-0.231	-0.251	-0.249	-0.249	-0.219	-0.218	-0.212
.50	.995	-0.245	-0.243	-0.242	-0.251	-0.251	-0.251	-0.271	-0.269	-0.269	-0.239	-0.238	-0.232
.17	.996	-0.264	-0.263	-0.262	-0.271	-0.271	-0.271	-0.291	-0.289	-0.289	-0.259	-0.258	-0.252
		$P_{t,J}/P_m = 1.98$			$P_{t,J}/P_m = 2.00$			$P_{t,J}/P_m = 1.99$			$P_{t,J}/P_m = 2.00$		
12.01	.719	-0.653	-0.027	-0.017	-0.048	-0.034	-0.016	-0.114	-0.099	-0.090	-0.028	-0.059	-0.048
10.59	.757	-0.650	-0.046	-0.040	-0.050	-0.045	-0.040	-0.067	-0.063	-0.074	-0.056	-0.054	-0.048
8.76	.797	-0.107	-0.103	-0.102	-0.124	-0.122	-0.120	-0.150	-0.149	-0.149	-0.117	-0.116	-0.110
7.18	.832	-0.127	-0.127	-0.124	-0.154	-0.154	-0.150	-0.188	-0.187	-0.187	-0.157	-0.156	-0.150
5.56	.870	-0.147	-0.146	-0.146	-0.157	-0.157	-0.157	-0.186	-0.185	-0.185	-0.155	-0.154	-0.149
3.93	.908	-0.166	-0.165	-0.165	-0.176	-0.176	-0.176	-0.205	-0.204	-0.204	-0.174	-0.173	-0.168
2.59	.947	-0.185	-0.184	-0.183	-0.194	-0.194	-0.194	-0.223	-0.222	-0.222	-0.192	-0.191	-0.186
1.34	.984	-0.207	-0.206	-0.205	-0.216	-0.216	-0.216	-0.245	-0.244	-0.244	-0.214	-0.213	-0.208
.75	.983	-0.226	-0.225	-0.224	-0.234	-0.234	-0.234	-0.263	-0.262	-0.262	-0.232	-0.231	-0.226
.50	.995	-0.245	-0.244	-0.243	-0.253	-0.253	-0.253	-0.282	-0.281	-0.281	-0.251	-0.250	-0.245
.17	.996	-0.264	-0.263	-0.262	-0.271	-0.271	-0.271	-0.291	-0.289	-0.289	-0.259	-0.258	-0.252
		$P_{t,J}/P_m = 2.99$			$P_{t,J}/P_m = 2.99$			$P_{t,J}/P_m = 2.99$			$P_{t,J}/P_m = 3.03$		
12.01	.719	-0.036	-0.035	-0.030	-0.049	-0.045	-0.032	-0.116	-0.107	-0.109	-0.058	-0.059	-0.047
10.59	.757	-0.051	-0.041	-0.040	-0.061	-0.055	-0.040	-0.067	-0.063	-0.079	-0.053	-0.053	-0.048
8.76	.797	-0.108	-0.105	-0.102	-0.123	-0.120	-0.117	-0.149	-0.148	-0.148	-0.113	-0.111	-0.109
7.18	.832	-0.127	-0.127	-0.124	-0.154	-0.154	-0.150	-0.188	-0.187	-0.187	-0.157	-0.156	-0.150
5.56	.870	-0.147	-0.146	-0.146	-0.157	-0.157	-0.157	-0.186	-0.185	-0.185	-0.155	-0.154	-0.149
3.93	.908	-0.166	-0.165	-0.165	-0.176	-0.176	-0.176	-0.205	-0.204	-0.204	-0.174	-0.173	-0.168
2.59	.947	-0.185	-0.184	-0.183	-0.194	-0.194	-0.194	-0.223	-0.222	-0.222	-0.192	-0.191	-0.186
1.34	.984	-0.207	-0.206	-0.205	-0.216	-0.216	-0.216	-0.245	-0.244	-0.244	-0.214	-0.213	-0.208
.75	.983	-0.226	-0.225	-0.224	-0.234	-0.234	-0.234	-0.263	-0.262	-0.262	-0.232	-0.231	-0.226
.50	.995	-0.245	-0.244	-0.243	-0.253	-0.253	-0.253	-0.282	-0.281	-0.281	-0.251	-0.250	-0.245
.17	.996	-0.264	-0.263	-0.262	-0.271	-0.271	-0.271	-0.291	-0.289	-0.289	-0.259	-0.258	-0.252
		$P_{t,J}/P_m = 4.96$			$P_{t,J}/P_m = 4.96$			$P_{t,J}/P_m = 4.97$			$P_{t,J}/P_m = 4.97$		
12.01	.719	-0.046	-0.039	-0.019	-0.056	-0.050	-0.018	-0.114	-0.100	-0.091	-0.056	-0.053	-0.047
10.59	.757	-0.068	-0.048	-0.041	-0.060	-0.054	-0.040	-0.066	-0.063	-0.076	-0.059	-0.052	-0.047
8.76	.797	-0.108	-0.105	-0.102	-0.123	-0.120	-0.117	-0.150	-0.149	-0.149	-0.112	-0.110	-0.106
7.18	.832	-0.127	-0.127	-0.124	-0.154	-0.154	-0.150	-0.188	-0.187	-0.187	-0.157	-0.156	-0.150
5.56	.870	-0.147	-0.146	-0.146	-0.157	-0.157	-0.157	-0.186	-0.185	-0.185	-0.155	-0.154	-0.149
3.93	.908	-0.166	-0.165	-0.165	-0.176	-0.176	-0.176	-0.205	-0.204	-0.204	-0.174	-0.173	-0.168
2.59	.947	-0.185	-0.184	-0.183	-0.194	-0.194	-0.194	-0.223	-0.222	-0.222	-0.192	-0.191	-0.186
1.34	.984	-0.207	-0.206	-0.205	-0.216	-0.216	-0.216	-0.245	-0.244	-0.244	-0.214	-0.213	-0.208
.75	.983	-0.226	-0.225	-0.224	-0.234	-0.234	-0.234	-0.263	-0.262	-0.262	-0.232	-0.231	-0.226
.50	.995	-0.245	-0.244	-0.243	-0.253	-0.253	-0.253	-0.282	-0.281	-0.281	-0.251	-0.250	-0.245
.17	.996	-0.264	-0.263	-0.262	-0.271	-0.271	-0.271	-0.291	-0.289	-0.289	-0.259	-0.258	-0.252
		$P_{t,J}/P_m = 9.81$ (max.)			$P_{t,J}/P_m = 10.41$ (max.)			$P_{t,J}/P_m = 7.00$			$P_{t,J}/P_m = 6.99$		
12.01	.719	-0.047	-0.028	-0.019	-0.042	-0.038	-0.014	-0.114	-0.100	-0.090	-0.056	-0.054	-0.047
10.59	.757	-0.061	-0.047	-0.042	-0.050	-0.046	-0.041	-0.065	-0.063	-0.076	-0.058	-0.052	-0.047
8.76	.797	-0.108	-0.105	-0.102	-0.123	-0.121	-0.118	-0.149	-0.148	-0.148	-0.112	-0.111	-0.106
7.18	.832	-0.127	-0.127	-0.124	-0.154	-0.154	-0.150	-0.188	-0.187	-0.187	-0.157	-0.156	-0.150
5.56	.870	-0.147	-0.146	-0.146	-0.157	-0.157	-0.157	-0.186	-0.185	-0.185	-0.155	-0.154	-0.149
3.93	.908	-0.166	-0.165	-0.165	-0.176	-0.176	-0.176	-0.205	-0.204	-0.204	-0.174	-0.173	-0.168
2.59	.947	-0.185	-0.184	-0.183	-0.194	-0.194	-0.194	-0.223	-0.222	-0.222	-0.192	-0.191	-0.186
1.34	.984	-0.207	-0.206	-0.205	-0.216	-0.216	-0.216	-0.245	-0.244	-0.244	-0.214	-0.213	-0.208
.75	.983	-0.226	-0.225	-0.224	-0.234	-0.234	-0.234	-0.263	-0.262	-0.262	-0.232	-0.231	-0.226
.50	.995	-0.245	-0.244	-0.243	-0.253	-0.253	-0.253	-0.282	-0.281	-0.281	-0.251	-0.250	-0.245
.17	.996	-0.264	-0.263	-0.262	-0.271	-0.271	-0.271	-0.291	-0.289	-0.289	-0.259	-0.258	-0.252
		$P_{t,J}/P_m = 6.14$ (max.)			$P_{t,J}/P_m = 6.14$ (max.)			$P_{t,J}/P_m = 6.14$ (max.)			$P_{t,J}/P_m = 6.14$ (max.)		
12.01	.719										-0.051	-0.055	-0.040
10.59	.757										-0.058	-0.060	-0.024
8.76	.797										-0.114	-0.113	-0.110
7.18	.832										-0.176	-0.175	-0.170
5.56	.870										-0.227	-0.226	-0.222
3.93	.908										-0.284	-0.283	-0.282
2.59	.947										-0.341	-0.340	-0.339
1.34	.984										-0.397	-0.396	-0.395
.75	.983										-0.454	-0.453	-0.452
.50	.995										-0.512	-0.511	-0.510
.17	.996										-0.569	-0.568	-0.567

TABLE III.-- AFTERBODY PRESSURE COEFFICIENTS - Continued

(k) Afterbody VII - Continued

 $t_j = 800^{\circ} F$ 

$\frac{x}{x_1}$	$\frac{x}{x_{max}}$	Pressure coefficients for -											
		M <sub>∞</sub> = 0.80			M <sub>∞</sub> = 0.90			M <sub>∞</sub> = 1.00			M <sub>∞</sub> = 1.10		
		s = 0°	s = 45°	s = 72°	s = 0°	s = 45°	s = 72°	s = 0°	s = 45°	s = 72°	s = 0°	s = 45°	s = 72°
		$P_{t,j}/P_{\infty} = 1.99$			$P_{t,j}/P_{\infty} = 2.01$			$P_{t,j}/P_{\infty} = 2.00$			$P_{t,j}/P_{\infty} = 1.99$		
12.01	.719	-0.042	-0.055	-0.024	0.043	-0.021	-0.012	-0.114	-0.100	-0.092	-0.050	-0.054	-0.055
10.39	.727	-0.047	-0.042	-0.038	-0.048	-0.043	-0.039	-0.085	-0.063	-0.053	-0.054	-0.054	-0.054
8.76	.795	-0.105	-0.105	-0.053	-0.123	-0.120	-0.119	-0.115	-0.147	-0.147	-0.112	-0.110	-0.108
7.18	.852	-0.126	-0.127	-0.127	-0.153	-0.153	-0.149	-0.151	-0.231	-0.230	-0.180	-0.179	-0.177
5.56	.870	-0.116	-0.117	-0.117	-0.136	-0.136	-0.136	-0.136	-0.279	-0.277	-0.227	-0.228	-0.224
3.95	.908	-0.069	-0.070	-0.071	-0.076	-0.076	-0.077	-0.179	-0.187	-0.198	-0.245	-0.245	-0.244
2.35	.911	.011	.006	.006	.021	.017	.015	.107	.105	.104	.056	.058	.019
1.74	.924	.032	.030	.047	.068	.065	.061	.156	.155	.151	.107	.107	.107
.73	.929	.104	.102	.099	.123	.122	.119	.193	.191	.191	.120	.121	.120
.50	.929	.129	.128	.127	.151	.148	.148	.210	.210	.210	.152	.151	.152
.17	.936	.139	.137	.137	.160	.159	.159	.214	.214	.214	.159	.159	.159
		$P_{t,j}/P_{\infty} = 2.99$			$P_{t,j}/P_{\infty} = 5.00$			$P_{t,j}/P_{\infty} = 2.99$			$P_{t,j}/P_{\infty} = 3.01$		
12.01	.719	-0.046	-0.025	-0.016	-0.046	-0.026	-0.011	-0.114	-0.100	-0.091	-0.060	-0.055	-0.043
10.39	.727	-0.049	-0.042	-0.040	-0.049	-0.043	-0.040	-0.066	-0.065	-0.079	-0.059	-0.052	-0.046
8.76	.795	-0.105	-0.105	-0.105	-0.123	-0.123	-0.123	-0.150	-0.150	-0.146	-0.112	-0.109	-0.107
7.18	.852	-0.126	-0.127	-0.127	-0.153	-0.153	-0.153	-0.152	-0.231	-0.231	-0.181	-0.178	-0.176
5.56	.870	-0.116	-0.115	-0.115	-0.136	-0.136	-0.136	-0.150	-0.278	-0.276	-0.226	-0.224	-0.224
3.95	.908	-0.069	-0.070	-0.071	-0.076	-0.076	-0.077	-0.178	-0.186	-0.192	-0.244	-0.244	-0.243
2.35	.911	.010	.006	.006	.017	.013	.012	.105	.102	.102	.054	.054	.015
1.74	.924	.051	.049	.047	.066	.062	.057	.152	.150	.150	.093	.093	.016
.73	.929	.101	.100	.097	.119	.117	.115	.150	.150	.150	.105	.104	.105
.50	.929	.129	.128	.126	.151	.148	.147	.206	.206	.206	.152	.152	.152
.17	.936	.134	.134	.134	.155	.154	.154	.211	.210	.213	.157	.157	.158
		$P_{t,j}/P_{\infty} = 4.99$			$P_{t,j}/P_{\infty} = 4.99$			$P_{t,j}/P_{\infty} = 4.98$			$P_{t,j}/P_{\infty} = 5.01$		
12.01	.719	-0.047	-0.027	-0.019	-0.040	-0.023	-0.012	-0.113	-0.099	-0.090	-0.060	-0.053	-0.044
10.39	.727	-0.050	-0.045	-0.041	-0.049	-0.045	-0.039	-0.065	-0.062	-0.079	-0.058	-0.053	-0.047
8.76	.795	-0.109	-0.106	-0.105	-0.126	-0.126	-0.126	-0.159	-0.158	-0.147	-0.118	-0.116	-0.108
7.18	.852	-0.129	-0.128	-0.127	-0.153	-0.153	-0.153	-0.150	-0.231	-0.231	-0.181	-0.179	-0.177
5.56	.870	-0.117	-0.117	-0.117	-0.136	-0.136	-0.136	-0.150	-0.278	-0.276	-0.226	-0.224	-0.224
3.95	.908	-0.067	-0.070	-0.071	-0.076	-0.076	-0.077	-0.177	-0.185	-0.191	-0.243	-0.243	-0.242
2.35	.911	.011	.007	.007	.021	.018	.015	.105	.103	.103	.053	.053	.017
1.74	.924	.053	.051	.048	.068	.064	.061	.153	.152	.151	.101	.101	.101
.73	.929	.103	.104	.105	.129	.122	.122	.193	.191	.191	.120	.120	.120
.50	.929	.133	.131	.132	.153	.152	.152	.205	.205	.205	.150	.150	.150
.17	.936	.140	.140	.140	.160	.159	.159	.213	.212	.213	.158	.158	.158
		$P_{t,j}/P_{\infty} = 7.01$			$P_{t,j}/P_{\infty} = 5.99$			$P_{t,j}/P_{\infty} = 6.97$			$P_{t,j}/P_{\infty} = 7.00$		
12.01	.719	-0.043	-0.026	-0.015	-0.041	-0.023	-0.012	-0.114	-0.100	-0.090	-0.060	-0.051	-0.043
10.39	.727	-0.047	-0.043	-0.040	-0.049	-0.043	-0.041	-0.066	-0.063	-0.079	-0.058	-0.052	-0.047
8.76	.795	-0.107	-0.108	-0.108	-0.128	-0.128	-0.128	-0.158	-0.158	-0.148	-0.118	-0.116	-0.108
7.18	.852	-0.126	-0.125	-0.124	-0.152	-0.152	-0.152	-0.159	-0.232	-0.231	-0.181	-0.180	-0.178
5.56	.870	-0.115	-0.115	-0.115	-0.135	-0.135	-0.135	-0.150	-0.280	-0.279	-0.228	-0.228	-0.224
3.95	.908	-0.065	-0.066	-0.066	-0.069	-0.073	-0.074	-0.162	-0.162	-0.160	-0.246	-0.245	-0.244
2.35	.911	.019	.015	.014	.021	.018	.015	.080	.079	.078	.046	.046	.016
1.74	.924	.063	.062	.057	.076	.072	.071	.158	.157	.157	.105	.105	.105
.73	.929	.105	.104	.103	.128	.122	.122	.195	.195	.195	.121	.121	.121
.50	.929	.134	.132	.135	.154	.153	.153	.204	.204	.204	.152	.152	.152
.17	.936	.144	.144	.144	.164	.179	.179	.217	.217	.219	.156	.156	.157
		$P_{t,j}/P_{\infty} = 8.90$			$P_{t,j}/P_{\infty} = 5.98$			$P_{t,j}/P_{\infty} = 8.99$			$P_{t,j}/P_{\infty} = 8.96$		
12.01	.719	-0.047	-0.027	-0.019	-0.040	-0.022	-0.012	-0.114	-0.099	-0.090	-0.060	-0.051	-0.042
10.39	.727	-0.051	-0.042	-0.042	-0.048	-0.044	-0.038	-0.067	-0.062	-0.078	-0.059	-0.052	-0.046
8.76	.795	-0.107	-0.103	-0.103	-0.124	-0.124	-0.124	-0.158	-0.158	-0.149	-0.118	-0.113	-0.108
7.18	.852	-0.126	-0.126	-0.124	-0.152	-0.152	-0.151	-0.159	-0.232	-0.231	-0.181	-0.180	-0.178
5.56	.870	-0.113	-0.113	-0.113	-0.135	-0.135	-0.135	-0.150	-0.280	-0.278	-0.228	-0.228	-0.224
3.95	.908	-0.064	-0.065	-0.066	-0.067	-0.072	-0.074	-0.164	-0.164	-0.161	-0.246	-0.246	-0.244
2.35	.911	.018	.021	.019	.033	.031	.028	.082	.082	.081	.050	.049	.017
1.74	.924	.062	.072	.067	.086	.084	.082	.157	.157	.157	.105	.104	.097
.73	.929	.106	.109	.105	.135	.134	.134	.205	.205	.205	.153	.152	.153
.50	.929	.135	.135	.135	.156	.156	.156	.211	.211	.211	.154	.154	.155
.17	.936	.145	.145	.145	.166	.166	.166	.220	.220	.220	.155	.155	.156
		$P_{t,j}/P_{\infty} = 11.04$			$P_{t,j}/P_{\infty} = 10.97$								
12.01	.719												
10.39	.727												
8.76	.795												
7.18	.852												
5.56	.870												
3.95	.908												
2.35	.911												
1.74	.924												
.73	.929												
.50	.929												
.17	.936												

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TABLE III.-- AFTERBODY PRESSURE COEFFICIENTS - Continued

(h) Afterbody VII - Concluded

 $T_J = 1,200^{\circ} F$ 

$\frac{x}{d_j}$	$\frac{x}{x_{max}}$	Pressure coefficients for -											
		K <sub>m</sub> = 0.80			K <sub>m</sub> = 0.90			K <sub>m</sub> = 1.00			K <sub>m</sub> = 1.10		
		s = 0°	s = 45°	s = 72°	s = 0°	s = 45°	s = 72°	s = 0°	s = 45°	s = 72°	s = 0°	s = 45°	s = 72°
		$P_{t,j}/P_m = 2.00$			$P_{t,j}/P_m = 2.00$			$P_{t,j}/P_m = 2.00$			$P_{t,j}/P_m = 2.00$		
12.01	.719	-0.038	-0.077	-0.017	-0.050	-0.088	-0.025	-0.102	-0.100	-0.091	-0.073	-0.051	-0.042
10.39	.757	-0.020	-0.045	-0.039	-0.042	-0.077	-0.041	-0.066	-0.069	-0.073	-0.052	-0.052	-0.046
8.76	.795	-0.107	-0.109	-0.103	-0.125	-0.122	-0.120	-0.189	-0.191	-0.190	-0.112	-0.110	-0.105
7.18	.832	-0.120	-0.126	-0.125	-0.152	-0.153	-0.150	-0.229	-0.234	-0.231	-0.179	-0.178	-0.176
5.36	.870	-0.116	-0.116	-0.115	-0.136	-0.136	-0.136	-0.202	-0.201	-0.202	-0.149	-0.148	-0.146
3.95	.908	-0.066	-0.068	-0.069	-0.073	-0.075	-0.077	-0.188	-0.192	-0.192	-0.146	-0.146	-0.145
2.35	.940	-0.015	-0.012	-0.009	-0.023	-0.020	-0.017	-0.109	-0.107	-0.105	-0.138	-0.140	-0.145
1.34	.964	.099	.072	.092	.069	.068	.065	.158	.157	.155	.142	.140	.138
.75	.983	.110	.106	.107	.129	.128	.122	.158	.159	.159	.150	.149	.146
.30	.992	.108	.104	.104	.129	.121	.122	.169	.169	.169	.156	.156	.156
.17	.996	.104	.104	.104	.126	.126	.126	.163	.163	.163	.143	.143	.144
		$P_{t,j}/P_m = 5.01$			$P_{t,j}/P_m = 2.97$			$P_{t,j}/P_m = 2.99$			$P_{t,j}/P_m = 3.01$		
12.01	.719	-0.036	-0.059	-0.018	-0.050	-0.083	-0.013	-0.104	-0.100	-0.091	-0.095	-0.052	-0.053
10.39	.757	-0.021	-0.047	-0.041	-0.046	-0.086	-0.040	-0.088	-0.086	-0.090	-0.059	-0.059	-0.047
8.76	.795	-0.108	-0.107	-0.104	-0.123	-0.120	-0.118	-0.199	-0.191	-0.191	-0.113	-0.111	-0.109
7.18	.832	-0.127	-0.127	-0.126	-0.151	-0.151	-0.148	-0.235	-0.233	-0.231	-0.179	-0.178	-0.176
5.36	.870	-0.117	-0.117	-0.116	-0.134	-0.134	-0.133	-0.203	-0.203	-0.202	-0.148	-0.147	-0.146
3.95	.908	-0.068	-0.069	-0.071	-0.072	-0.075	-0.075	-0.175	-0.182	-0.186	-0.146	-0.145	-0.144
2.35	.940	.013	.010	.009	.023	.021	.017	.109	.107	.104	.137	.137	.136
1.34	.964	.054	.029	.049	.069	.067	.064	.154	.154	.152	.138	.138	.138
.75	.983	.102	.103	.103	.124	.124	.124	.163	.163	.163	.146	.146	.146
.30	.992	.102	.102	.102	.127	.127	.127	.169	.169	.169	.150	.150	.150
.17	.996	.108	.107	.107	.129	.129	.129	.171	.171	.171	.157	.157	.158
		$P_{t,j}/P_m = 5.03$			$P_{t,j}/P_m = 5.02$			$P_{t,j}/P_m = 5.01$			$P_{t,j}/P_m = 5.02$		
12.01	.719	-0.038	-0.028	-0.018	-0.020	-0.022	-0.013	-0.104	-0.100	-0.099	-0.093	-0.052	-0.053
10.39	.757	-0.049	-0.046	-0.040	-0.046	-0.085	-0.045	-0.086	-0.085	-0.077	-0.061	-0.059	-0.049
8.76	.795	-0.107	-0.105	-0.103	-0.120	-0.120	-0.117	-0.191	-0.190	-0.190	-0.113	-0.111	-0.109
7.18	.832	-0.126	-0.126	-0.126	-0.149	-0.149	-0.147	-0.232	-0.232	-0.232	-0.178	-0.178	-0.177
5.36	.870	-0.118	-0.117	-0.117	-0.134	-0.134	-0.134	-0.203	-0.203	-0.202	-0.147	-0.146	-0.145
3.95	.908	-0.066	-0.066	-0.069	-0.070	-0.072	-0.074	-0.177	-0.181	-0.189	-0.146	-0.145	-0.144
2.35	.940	.013	.010	.010	.026	.026	.026	.107	.104	.102	.130	.130	.130
1.34	.964	.058	.029	.052	.073	.071	.068	.154	.154	.150	.139	.139	.138
.75	.983	.111	.108	.107	.130	.128	.128	.166	.163	.160	.140	.139	.138
.30	.992	.109	.105	.105	.129	.129	.129	.167	.167	.167	.147	.147	.146
.17	.996	.106	.104	.104	.127	.127	.127	.164	.164	.164	.143	.143	.143
		$P_{t,j}/P_m = 6.98$			$P_{t,j}/P_m = 7.00$			$P_{t,j}/P_m = 6.98$			$P_{t,j}/P_m = 6.98$		
12.01	.719	-0.033	-0.026	-0.017	-0.030	-0.084	-0.010	-0.102	-0.104	-0.093	-0.072	-0.052	-0.049
10.39	.757	-0.048	-0.040	-0.040	-0.046	-0.087	-0.047	-0.084	-0.084	-0.074	-0.058	-0.057	-0.047
8.76	.795	-0.106	-0.103	-0.101	-0.120	-0.120	-0.117	-0.191	-0.191	-0.191	-0.113	-0.112	-0.110
7.18	.832	-0.125	-0.125	-0.125	-0.149	-0.149	-0.147	-0.233	-0.233	-0.232	-0.179	-0.178	-0.176
5.36	.870	-0.112	-0.113	-0.112	-0.133	-0.134	-0.132	-0.203	-0.203	-0.202	-0.148	-0.147	-0.146
3.95	.908	-0.061	-0.061	-0.064	-0.067	-0.069	-0.071	-0.176	-0.186	-0.187	-0.147	-0.146	-0.145
2.35	.940	.022	.019	.016	.032	.028	.024	.113	.110	.108	.125	.125	.124
1.34	.964	.007	.005	.001	.079	.079	.079	.166	.166	.167	.090	.089	.088
.75	.983	.125	.122	.122	.142	.140	.140	.181	.177	.177	.117	.117	.117
.30	.992	.101	.104	.105	.125	.125	.125	.161	.161	.161	.140	.139	.139
.17	.996	.107	.109	.107	.128	.128	.127	.167	.167	.167	.147	.146	.146
		$P_{t,j}/P_m = 8.98$			$P_{t,j}/P_m = 9.01$			$P_{t,j}/P_m = 9.25$			$P_{t,j}/P_m = 8.99$		
12.01	.719	-0.032	-0.024	-0.016	-0.029	-0.083	-0.010	-0.104	-0.103	-0.093	-0.074	-0.052	-0.045
10.39	.757	-0.047	-0.035	-0.038	-0.044	-0.089	-0.046	-0.085	-0.085	-0.076	-0.061	-0.052	-0.046
8.76	.795	-0.104	-0.104	-0.100	-0.125	-0.119	-0.117	-0.191	-0.191	-0.191	-0.115	-0.115	-0.109
7.18	.832	-0.124	-0.124	-0.120	-0.149	-0.149	-0.147	-0.233	-0.233	-0.232	-0.179	-0.178	-0.176
5.36	.870	-0.111	-0.111	-0.108	-0.134	-0.134	-0.131	-0.203	-0.203	-0.202	-0.146	-0.145	-0.144
3.95	.908	-0.060	-0.062	-0.064	-0.066	-0.066	-0.068	-0.188	-0.187	-0.187	-0.144	-0.143	-0.142
2.35	.940	.005	.006	.005	.076	.075	.071	.147	.147	.147	.084	.083	.082
1.34	.964	.076	.076	.076	.092	.091	.087	.168	.168	.167	.109	.108	.108
.75	.983	.101	.100	.101	.129	.129	.127	.166	.166	.166	.133	.133	.134
.30	.992	.106	.107	.107	.129	.129	.128	.167	.167	.167	.134	.134	.134
.17	.996	.107	.107	.107	.128	.128	.128	.168	.168	.168	.135	.135	.135
		$P_{t,j}/P_m = 10.95$			$P_{t,j}/P_m = 11.04$								
12.01	.719							-0.106	-0.101	-0.093	-0.079	-0.052	-0.042
10.39	.757							-0.096	-0.091	-0.082	-0.061	-0.052	-0.046
8.76	.795							-0.110	-0.101	-0.101	-0.113	-0.110	-0.107
7.18	.832							-0.234	-0.231	-0.231	-0.179	-0.178	-0.176
5.36	.870							-0.082	-0.081	-0.081	-0.082	-0.082	-0.082
3.95	.908							-0.146	-0.146	-0.146	-0.146	-0.146	-0.146
2.35	.940							-0.124	-0.124	-0.124	-0.124	-0.124	-0.124
1.34	.964							-0.176	-0.176	-0.176	-0.176	-0.176	-0.176
.75	.983							-0.212	-0.212	-0.212	-0.212	-0.212	-0.212
.30	.992							-0.223	-0.223	-0.223	-0.223	-0.223	-0.223
.17	.996							-0.230	-0.233	-0.237	-0.161	-0.162	-0.172

TABLE III--AFTERSHOCK PRESSURE COEFFICIENTS - Continued

(1) Afterbody VIII

 $t_j = \text{Cold}$ 

$\frac{x}{d_s}$	$\frac{x}{l_{\max}}$	Pressure coefficients for -											
		$M_\infty = 0.80$			$M_\infty = 0.90$			$M_\infty = 1.00$			$M_\infty = 1.10$		
		$\theta = 0^\circ$	$\theta = 45^\circ$	$\theta = 72^\circ$	$\theta = 0^\circ$	$\theta = 45^\circ$	$\theta = 72^\circ$	$\theta = 0^\circ$	$\theta = 45^\circ$	$\theta = 72^\circ$	$\theta = 0^\circ$	$\theta = 45^\circ$	$\theta = 72^\circ$
		$P_{t,j}/P_\infty = 1.05$			$P_{t,j}/P_\infty = 1.05$			$P_{t,j}/P_\infty = 1.14$			$P_{t,j}/P_\infty = 1.10$		
12.01	.719	-.023	-.026	-.012	-.020	-.020	-.008	-.103	-.111	-.097	-.046	-.058	-.045
10.59	.727	-.026	-.032	-.005	-.024	-.024	-.008	-.057	-.084	-.076	-.048	-.052	-.043
8.76	.795	-.063	-.055	-.024	-.068	-.059	-.006	-.083	-.079	-.072	-.063	-.055	-.051
7.18	.822	-.136	-.133	-.133	-.170	-.165	-.165	-.176	-.174	-.173	-.128	-.125	-.125
5.56	.870	-.143	-.143	-.140	-.181	-.181	-.176	-.202	-.202	-.196	-.194	-.195	-.190
3.93	.908	-.114	-.111	-.114	-.154	-.154	-.158	-.198	-.198	-.195	-.203	-.200	-.201
2.35	.945	-.033	-.036	-.038	-.035	-.035	-.004	-.010	-.010	-.010	-.277	-.269	-.269
1.58	.984	.018	.015	.018	.024	.022	.018	.103	.099	.099	-.036	-.112	-.127
.73	.985	.071	.069	.082	.082	.080	.078	.197	.195	.195	.054	.047	.045
.17	.995	.100	.100	.098	.124	.112	.110	.177	.177	.175	.087	.085	.085
		$P_{t,j}/P_\infty = 1.98$			$P_{t,j}/P_\infty = 1.97$			$P_{t,j}/P_\infty = 1.91$			$P_{t,j}/P_\infty = 2.00$		
12.01	.719	-.024	-.028	-.013	-.018	-.019	-.007	-.103	-.111	-.096	-.050	-.060	-.046
10.59	.727	-.027	-.033	-.027	-.028	-.028	-.007	-.057	-.085	-.076	-.059	-.064	-.055
8.76	.795	-.064	-.056	-.035	-.067	-.059	-.004	-.083	-.075	-.071	-.064	-.066	-.057
7.18	.822	-.138	-.135	-.137	-.167	-.167	-.162	-.177	-.175	-.173	-.129	-.127	-.127
5.56	.870	-.144	-.144	-.141	-.177	-.177	-.173	-.202	-.202	-.195	-.193	-.197	-.190
3.93	.908	-.112	-.112	-.116	-.159	-.159	-.155	-.198	-.198	-.195	-.203	-.201	-.201
2.35	.945	-.055	-.056	-.057	-.090	-.089	-.036	-.093	-.093	-.091	-.093	-.096	-.096
1.58	.984	.017	.015	.011	.028	.026	.021	.105	.105	.105	-.042	-.110	-.128
.73	.985	.057	.055	.062	.084	.082	.081	.158	.157	.157	.042	.039	.039
.17	.995	.091	.090	.089	.113	.112	.110	.177	.177	.175	.073	.071	.071
		$P_{t,j}/P_\infty = 3.00$			$P_{t,j}/P_\infty = 2.97$			$P_{t,j}/P_\infty = 2.90$			$P_{t,j}/P_\infty = 3.01$		
12.01	.719	-.025	-.025	-.024	-.018	-.019	-.006	-.103	-.110	-.096	-.058	-.068	-.046
10.59	.727	-.027	-.033	-.027	-.029	-.029	-.021	-.056	-.083	-.076	-.059	-.063	-.054
8.76	.795	-.064	-.056	-.034	-.065	-.057	-.004	-.083	-.075	-.071	-.064	-.066	-.055
7.18	.822	-.136	-.134	-.134	-.167	-.165	-.161	-.177	-.175	-.172	-.150	-.148	-.148
5.56	.870	-.142	-.142	-.142	-.176	-.176	-.172	-.202	-.202	-.195	-.193	-.195	-.190
3.93	.908	-.115	-.115	-.115	-.157	-.157	-.153	-.198	-.198	-.195	-.203	-.201	-.201
2.35	.945	-.059	-.059	-.059	-.091	-.091	-.037	-.093	-.093	-.091	-.093	-.096	-.096
1.58	.984	.018	.018	.008	.026	.026	.020	.108	.108	.108	-.046	-.112	-.129
.73	.985	.062	.060	.062	.081	.080	.079	.158	.157	.157	.044	.038	.038
.17	.995	.083	.084	.082	.106	.107	.105	.175	.175	.175	.073	.076	.076
		$P_{t,j}/P_\infty = 4.99$			$P_{t,j}/P_\infty = 4.96$			$P_{t,j}/P_\infty = 4.98$			$P_{t,j}/P_\infty = 4.96$		
12.01	.719	-.022	-.023	-.012	-.018	-.018	-.006	-.103	-.111	-.096	-.050	-.060	-.047
10.59	.727	-.025	-.031	-.026	-.028	-.029	-.023	-.057	-.083	-.076	-.059	-.064	-.056
8.76	.795	-.062	-.054	-.032	-.063	-.057	-.004	-.083	-.075	-.071	-.063	-.067	-.053
7.18	.822	-.136	-.133	-.132	-.166	-.165	-.161	-.177	-.175	-.172	-.150	-.148	-.148
5.56	.870	-.142	-.142	-.140	-.173	-.173	-.172	-.202	-.202	-.195	-.193	-.195	-.190
3.93	.908	-.111	-.110	-.114	-.158	-.158	-.152	-.198	-.198	-.195	-.203	-.201	-.201
2.35	.945	-.052	-.052	-.056	-.089	-.089	-.076	-.096	-.096	-.095	-.099	-.102	-.102
1.58	.984	.017	.016	.011	.027	.026	.021	.101	.100	.100	-.049	-.104	-.121
.73	.985	.056	.055	.061	.082	.081	.078	.158	.157	.157	.059	.059	.059
.17	.995	.086	.086	.085	.107	.105	.104	.172	.172	.172	.077	.077	.077
		$P_{t,j}/P_\infty = 6.94$			$P_{t,j}/P_\infty = 7.01$			$P_{t,j}/P_\infty = 6.94$			$P_{t,j}/P_\infty = 7.01$		
12.01	.719							-.103	-.112	-.097	-.049	-.059	-.046
10.59	.727							-.089	-.099	-.093	-.053	-.064	-.048
8.76	.795							-.084	-.086	-.073	-.054	-.066	-.043
7.18	.822							-.178	-.176	-.174	-.131	-.129	-.124
5.56	.870							-.233	-.237	-.237	-.195	-.196	-.191
3.93	.908							-.310	-.305	-.309	-.294	-.290	-.282
2.35	.945							-.004	-.001	-.000	-.277	-.270	-.268
1.58	.984							-.103	-.101	-.100	-.103	-.116	-.134
.73	.985							-.174	-.174	-.173	-.074	-.076	-.076
.17	.995							-.180	-.180	-.180	-.090	-.090	-.090

CONFIDENTIAL

TABLE III.- AFTERBODY PRESSURE COEFFICIENTS - Continued

(i) Afterbody VIII - Continued

 $t_j = 600^\circ F$ 

$\frac{x}{d_3}$	$\frac{x}{r_{max}}$	Pressure coefficients for -											
		M <sub>∞</sub> = 0.80			M <sub>∞</sub> = 0.90			M <sub>∞</sub> = 1.00			M <sub>∞</sub> = 1.10		
		$\theta = 0^\circ$	$\theta = 45^\circ$	$\theta = 72^\circ$	$\theta = 0^\circ$	$\theta = 45^\circ$	$\theta = 72^\circ$	$\theta = 0^\circ$	$\theta = 45^\circ$	$\theta = 72^\circ$	$\theta = 0^\circ$	$\theta = 45^\circ$	$\theta = 72^\circ$
		$P_{t,j}/P_\infty = 1.96$											
$P_{t,j}/P_\infty = 1.96$													
12.01	.719	-.023	-.009	-.018	-.018	-.019	-.006	-.109	-.111	-.098	-.096	-.095	-.096
10.59	.757	-.039	-.023	-.027	-.031	-.028	-.022	-.084	-.084	-.077	-.077	-.072	-.072
8.76	.792	-.065	-.026	-.023	-.063	-.026	-.023	-.076	-.075	-.064	-.064	-.059	-.059
7.18	.832	-.141	-.137	-.136	-.165	-.163	-.162	-.179	-.178	-.175	-.175	-.170	-.170
5.56	.870	-.145	-.147	-.142	-.175	-.176	-.174	-.254	-.253	-.247	-.247	-.194	-.194
3.95	.908	-.116	-.115	-.117	-.128	-.129	-.133	-.511	-.508	-.510	-.511	-.451	-.450
2.35	.945	-.034	-.037	-.036	-.032	-.036	-.036	.013	.016	.011	.009	-.029	-.027
1.54	.964	.014	.014	.011	.020	.027	.027	.207	.206	.193	.193	-.056	-.112
.75	.983	.059	.059	.063	.087	.082	.082	.160	.159	.156	.156	.053	.050
.50	.993	.094	.095	.092	.113	.115	.111	.179	.179	.179	.179	.091	.084
.17	.996	.104	.105	.105	.124	.124	.126	.195	.195	.195	.195	.101	.102
$P_{t,j}/P_\infty = 5.03$													
12.01	.719	-.005	-.005	-.011	-.017	-.018	-.009	-.101	-.110	-.095	-.095	-.095	-.095
10.59	.757	-.038	-.028	-.026	-.039	-.029	-.026	-.088	-.088	-.082	-.082	-.078	-.078
8.76	.792	-.065	-.027	-.024	-.065	-.026	-.024	-.076	-.076	-.063	-.063	-.056	-.056
7.18	.832	-.137	-.138	-.136	-.166	-.164	-.163	-.176	-.176	-.173	-.173	-.160	-.160
5.56	.870	-.144	-.146	-.142	-.178	-.178	-.176	-.233	-.233	-.246	-.246	-.195	-.195
3.95	.908	-.115	-.113	-.118	-.138	-.132	-.132	-.308	-.307	-.309	-.309	-.251	-.251
2.35	.945	-.033	-.040	-.040	-.031	-.037	-.037	.013	.008	.009	.009	-.274	-.237
1.54	.964	.013	.013	.008	.022	.019	.019	.108	.104	.104	.104	.051	.053
.75	.983	.068	.068	.060	.086	.079	.078	.198	.197	.197	.197	.061	.063
.50	.993	.089	.087	.086	.109	.108	.106	.177	.177	.177	.177	.083	.083
.17	.996	.096	.096	.097	.117	.116	.119	.185	.184	.185	.185	.093	.093
$P_{t,j}/P_\infty = 5.01$													
12.01	.719	-.005	-.005	-.011	-.017	-.018	-.009	-.101	-.110	-.095	-.095	-.095	-.095
10.59	.757	-.038	-.028	-.026	-.039	-.029	-.026	-.088	-.088	-.082	-.082	-.078	-.078
8.76	.792	-.065	-.027	-.024	-.065	-.026	-.024	-.076	-.076	-.063	-.063	-.056	-.056
7.18	.832	-.137	-.138	-.136	-.166	-.164	-.163	-.176	-.176	-.173	-.173	-.160	-.160
5.56	.870	-.144	-.146	-.142	-.178	-.178	-.176	-.233	-.233	-.246	-.246	-.195	-.195
3.95	.908	-.115	-.113	-.118	-.138	-.132	-.132	-.308	-.307	-.309	-.309	-.251	-.251
2.35	.945	-.033	-.040	-.040	-.031	-.037	-.037	.013	.008	.009	.009	-.274	-.237
1.54	.964	.011	.011	.007	.024	.023	.018	.105	.104	.104	.104	.044	.039
.75	.983	.062	.062	.056	.081	.076	.073	.198	.196	.196	.196	.078	.077
.50	.993	.084	.083	.080	.106	.105	.102	.179	.178	.178	.178	.083	.083
.17	.996	.094	.094	.090	.116	.115	.112	.185	.184	.185	.185	.088	.089
$P_{t,j}/P_\infty = 4.99$													
12.01	.719	-.027	-.006	-.013	-.017	-.018	-.009	-.104	-.110	-.096	-.096	-.095	-.095
10.59	.757	-.056	-.034	-.028	-.056	-.034	-.028	-.087	-.087	-.076	-.076	-.071	-.071
8.76	.792	-.094	-.056	-.053	-.094	-.056	-.053	-.076	-.076	-.063	-.063	-.054	-.054
7.18	.832	-.129	-.128	-.126	-.165	-.164	-.162	-.178	-.178	-.176	-.176	-.162	-.162
5.56	.870	-.146	-.146	-.142	-.178	-.178	-.176	-.233	-.233	-.246	-.246	-.195	-.195
3.95	.908	-.115	-.113	-.118	-.138	-.132	-.132	-.308	-.307	-.309	-.309	-.251	-.251
2.35	.945	-.033	-.040	-.040	-.031	-.037	-.037	.013	.008	.009	.009	-.274	-.237
1.54	.964	.017	.016	.012	.032	.028	.026	.103	.101	.101	.101	.046	.046
.75	.983	.069	.066	.067	.088	.085	.085	.199	.196	.196	.196	.078	.078
.50	.993	.092	.093	.090	.117	.115	.113	.179	.178	.178	.178	.079	.078
.17	.996	.101	.100	.100	.126	.126	.124	.185	.184	.185	.185	.089	.089
$P_{t,j}/P_\infty = 5.01$													
12.01	.719	-.034	-.024	-.015	-.019	-.020	-.007	-.104	-.110	-.096	-.096	-.095	-.095
10.59	.757	-.056	-.037	-.028	-.056	-.037	-.028	-.078	-.078	-.063	-.063	-.054	-.054
8.76	.792	-.094	-.058	-.053	-.094	-.058	-.053	-.076	-.076	-.062	-.062	-.053	-.053
7.18	.832	-.129	-.128	-.126	-.165	-.164	-.162	-.178	-.178	-.176	-.176	-.162	-.162
5.56	.870	-.146	-.146	-.142	-.178	-.178	-.176	-.233	-.233	-.246	-.246	-.195	-.195
3.95	.908	-.115	-.113	-.118	-.138	-.132	-.132	-.308	-.307	-.309	-.309	-.251	-.251
2.35	.945	-.033	-.040	-.040	-.031	-.037	-.037	.013	.008	.009	.009	-.274	-.237
1.54	.964	.017	.016	.012	.032	.028	.026	.103	.101	.101	.101	.046	.046
.75	.983	.068	.066	.067	.088	.085	.085	.199	.196	.196	.196	.078	.078
.50	.993	.092	.093	.090	.117	.115	.113	.179	.178	.178	.178	.079	.078
.17	.996	.101	.100	.100	.126	.126	.124	.185	.184	.185	.185	.089	.089
$P_{t,j}/P_\infty = 5.02$													
12.01	.719	-.034	-.024	-.015	-.019	-.020	-.007	-.104	-.110	-.096	-.096	-.095	-.095
10.59	.757	-.056	-.037	-.028	-.056	-.037	-.028	-.078	-.078	-.063	-.063	-.054	-.054
8.76	.792	-.094	-.058	-.053	-.094	-.058	-.053	-.076	-.076	-.062	-.062	-.053	-.053
7.18	.832	-.129	-.128	-.126	-.165	-.164	-.162	-.178	-.178	-.176	-.176	-.162	-.162
5.56	.870	-.146	-.146	-.142	-.178	-.178	-.176	-.233	-.233	-.246	-.246	-.195	-.195
3.95	.908	-.115	-.113	-.118	-.138	-.132	-.132	-.308	-.307	-.309	-.309	-.251	-.251
2.35	.945	-.033	-.040	-.040	-.031	-.037	-.037	.013	.008	.009	.009	-.274	-.237
1.54	.964	.017	.016	.012	.032	.028	.026	.103	.101	.101	.101	.046	.046
.75	.983	.068	.066	.067	.088	.085	.085	.199	.196	.196	.196	.078	.078
.50	.993	.092	.093	.090	.117	.115	.113	.179	.178	.178	.178	.079	.078
.17	.996	.101	.100	.100	.126	.126	.124	.185	.184	.185	.185	.089	.089
$P_{t,j}/P_\infty = 5.02$													
12.01	.719	-.034	-.024	-.015	-.019	-.020	-.007	-.104	-.110	-.096	-.096	-.095	-.095
10.59	.757	-.056	-.037	-.028	-.056	-.037	-.028	-.078	-.078	-.063	-.063	-.054	-.054
8.76	.792	-.094	-.058	-.053	-.094	-.058	-.053	-.076	-.076	-.062	-.062	-.053	-.053
7.18	.832	-.129	-.128	-.126	-.165	-.164	-.162	-.178	-.178	-.176	-.176	-.162	-.162
5.56	.870	-.146	-.146	-.142	-.178	-.178	-.176	-.233	-.233	-.246	-.246	-.195	-.195
3.95	.908	-.115	-.113	-.118	-.138	-.132	-.132	-.308	-.307	-.309	-.309	-.251	-.251
2.35	.945	-.033	-.040	-.040	-.031	-.037	-.037	.013	.008	.009	.009	-.274	-.237
1.54	.964	.017	.016	.012	.032	.028	.026	.103	.101	.101	.101	.046	.046
.75													

CONFIDENTIAL

TABLE III.- AFTERBODY PRESSURE COEFFICIENTS - Continued

(1) Afterbody VIII - Concluded

 $t_j = 1,200^{\circ} F$ 

$\frac{x}{x_j}$	$\frac{x}{l_{max}}$	Pressure coefficients for -													
		M <sub>a</sub> = 0.80			M <sub>a</sub> = 0.90			M <sub>a</sub> = 1.00			M <sub>a</sub> = 1.10				
		$\theta = 0^{\circ}$	$\theta = 45^{\circ}$	$\theta = 72^{\circ}$	$\theta = 0^{\circ}$	$\theta = 45^{\circ}$	$\theta = 72^{\circ}$	$\theta = 0^{\circ}$	$\theta = 45^{\circ}$	$\theta = 72^{\circ}$	$\theta = 0^{\circ}$	$\theta = 45^{\circ}$	$\theta = 72^{\circ}$		
$P_{t,j}/P_a = 2.04$				$P_{t,j}/P_a = 2.02$				$P_{t,j}/P_a = 2.06$				$P_{t,j}/P_a = 1.99$			
12.01	.719	-0.025	-0.026	-0.016	-0.019	-0.021	-0.007	-0.102	-0.108	-0.097	-0.047	-0.055	-0.055	-0.045	
10.39	.757	-0.039	-0.036	-0.029	-0.036	-0.031	-0.024	-0.086	-0.083	-0.073	-0.059	-0.052	-0.044	-0.033	
8.76	.795	-0.066	-0.059	-0.056	-0.068	-0.059	-0.057	-0.082	-0.073	-0.072	-0.063	-0.055	-0.048	-0.038	
7.18	.832	-0.142	-0.132	-0.138	-0.129	-0.129	-0.124	-0.176	-0.173	-0.176	-0.174	-0.150	-0.126	-0.124	
5.36	.870	-0.148	-0.142	-0.146	-0.152	-0.152	-0.159	-0.176	-0.173	-0.176	-0.174	-0.159	-0.136	-0.130	
3.99	.908	-0.171	-0.165	-0.171	-0.171	-0.171	-0.177	-0.193	-0.190	-0.193	-0.191	-0.174	-0.151	-0.148	
2.35	.943	-0.197	-0.191	-0.193	-0.193	-0.193	-0.197	-0.203	-0.200	-0.203	-0.201	-0.187	-0.164	-0.161	
1.36	.964	-0.201	-0.198	-0.198	-0.198	-0.198	-0.197	-0.203	-0.203	-0.203	-0.201	-0.188	-0.165	-0.163	
.73	.983	-0.070	-0.068	-0.069	-0.067	-0.068	-0.068	-0.083	-0.081	-0.081	-0.081	-0.069	-0.058	-0.058	
.36	.993	-0.099	-0.093	-0.095	-0.101	-0.101	-0.107	-0.116	-0.116	-0.116	-0.116	-0.099	-0.089	-0.088	
.17	.996	-0.107	-0.105	-0.107	-0.109	-0.109	-0.111	-0.117	-0.117	-0.117	-0.117	-0.099	-0.089	-0.088	
$P_{t,j}/P_a = 3.03$				$P_{t,j}/P_a = 3.01$				$P_{t,j}/P_a = 3.03$				$P_{t,j}/P_a = 2.99$			
12.01	.719	-0.026	-0.026	-0.016	-0.022	-0.021	-0.008	-0.108	-0.109	-0.109	-0.045	-0.056	-0.056	-0.045	
10.39	.757	-0.039	-0.031	-0.026	-0.031	-0.029	-0.023	-0.089	-0.083	-0.076	-0.058	-0.052	-0.042	-0.032	
8.76	.795	-0.069	-0.061	-0.058	-0.068	-0.059	-0.056	-0.088	-0.079	-0.070	-0.065	-0.056	-0.049	-0.038	
7.18	.832	-0.145	-0.139	-0.139	-0.172	-0.166	-0.165	-0.177	-0.176	-0.176	-0.174	-0.153	-0.126	-0.124	
5.36	.870	-0.148	-0.150	-0.146	-0.181	-0.181	-0.180	-0.177	-0.177	-0.177	-0.176	-0.154	-0.130	-0.129	
3.99	.908	-0.118	-0.119	-0.121	-0.133	-0.133	-0.136	-0.136	-0.136	-0.136	-0.137	-0.124	-0.104	-0.103	
2.35	.943	-0.038	-0.042	-0.042	-0.033	-0.036	-0.037	-0.019	-0.019	-0.019	-0.018	-0.017	-0.016	-0.016	
1.36	.964	-0.014	-0.012	-0.008	-0.008	-0.008	-0.008	-0.019	-0.019	-0.019	-0.018	-0.017	-0.016	-0.016	
.73	.983	-0.064	-0.064	-0.061	-0.061	-0.061	-0.061	-0.080	-0.080	-0.080	-0.083	-0.071	-0.065	-0.065	
.36	.993	-0.090	-0.089	-0.086	-0.089	-0.089	-0.089	-0.107	-0.107	-0.107	-0.107	-0.091	-0.078	-0.078	
.17	.996	-0.097	-0.095	-0.096	-0.100	-0.100	-0.102	-0.119	-0.119	-0.119	-0.119	-0.091	-0.071	-0.071	
$P_{t,j}/P_a = 3.01$				$P_{t,j}/P_a = 3.06$				$P_{t,j}/P_a = 3.02$				$P_{t,j}/P_a = 3.15$			
12.01	.719	-0.024	-0.026	-0.015	-0.020	-0.020	-0.009	-0.108	-0.110	-0.106	-0.044	-0.054	-0.054	-0.043	
10.39	.757	-0.039	-0.030	-0.026	-0.030	-0.029	-0.023	-0.089	-0.083	-0.077	-0.066	-0.051	-0.043	-0.032	
8.76	.795	-0.066	-0.058	-0.055	-0.067	-0.059	-0.055	-0.088	-0.079	-0.072	-0.065	-0.053	-0.043	-0.032	
7.18	.832	-0.140	-0.139	-0.136	-0.159	-0.166	-0.165	-0.177	-0.175	-0.175	-0.174	-0.150	-0.126	-0.124	
5.36	.870	-0.147	-0.148	-0.141	-0.179	-0.179	-0.176	-0.177	-0.177	-0.177	-0.176	-0.155	-0.131	-0.129	
3.99	.908	-0.117	-0.117	-0.118	-0.132	-0.132	-0.134	-0.134	-0.134	-0.134	-0.135	-0.122	-0.104	-0.103	
2.35	.943	-0.037	-0.035	-0.034	-0.034	-0.035	-0.036	-0.038	-0.038	-0.038	-0.038	-0.027	-0.026	-0.026	
1.36	.964	-0.014	-0.012	-0.008	-0.008	-0.008	-0.008	-0.019	-0.019	-0.019	-0.018	-0.013	-0.012	-0.012	
.73	.983	-0.062	-0.061	-0.061	-0.063	-0.063	-0.063	-0.076	-0.076	-0.076	-0.076	-0.065	-0.058	-0.058	
.36	.993	-0.088	-0.089	-0.086	-0.090	-0.090	-0.090	-0.107	-0.107	-0.107	-0.107	-0.091	-0.078	-0.078	
.17	.996	-0.097	-0.095	-0.096	-0.100	-0.100	-0.101	-0.119	-0.119	-0.119	-0.119	-0.091	-0.071	-0.071	
$P_{t,j}/P_a = 7.05$				$P_{t,j}/P_a = 7.00$				$P_{t,j}/P_a = 7.01$				$P_{t,j}/P_a = 7.05$			
12.01	.719	-0.026	-0.026	-0.021	-0.025	-0.026	-0.008	-0.108	-0.109	-0.106	-0.049	-0.053	-0.053	-0.046	
10.39	.757	-0.039	-0.030	-0.026	-0.033	-0.037	-0.023	-0.089	-0.081	-0.076	-0.061	-0.052	-0.046	-0.035	
8.76	.795	-0.066	-0.056	-0.055	-0.068	-0.067	-0.059	-0.088	-0.079	-0.072	-0.068	-0.058	-0.049	-0.038	
7.18	.832	-0.140	-0.137	-0.137	-0.167	-0.164	-0.163	-0.177	-0.175	-0.175	-0.174	-0.150	-0.126	-0.124	
5.36	.870	-0.145	-0.146	-0.141	-0.176	-0.176	-0.174	-0.176	-0.176	-0.176	-0.175	-0.155	-0.131	-0.129	
3.99	.908	-0.117	-0.118	-0.118	-0.129	-0.126	-0.124	-0.132	-0.132	-0.132	-0.132	-0.121	-0.104	-0.103	
2.35	.943	-0.033	-0.035	-0.033	-0.039	-0.031	-0.031	-0.047	-0.047	-0.047	-0.047	-0.036	-0.026	-0.026	
1.36	.964	-0.014	-0.012	-0.008	-0.008	-0.008	-0.008	-0.019	-0.019	-0.019	-0.018	-0.012	-0.011	-0.011	
.73	.983	-0.063	-0.063	-0.063	-0.063	-0.063	-0.063	-0.076	-0.076	-0.076	-0.076	-0.061	-0.056	-0.056	
.36	.993	-0.087	-0.085	-0.086	-0.088	-0.089	-0.089	-0.107	-0.107	-0.107	-0.107	-0.091	-0.072	-0.072	
.17	.996	-0.098	-0.095	-0.095	-0.100	-0.101	-0.101	-0.119	-0.119	-0.119	-0.119	-0.091	-0.071	-0.071	
$P_{t,j}/P_a = 9.04$				$P_{t,j}/P_a = 9.06$				$P_{t,j}/P_a = 9.05$				$P_{t,j}/P_a = 9.05$			
12.01	.719	-0.026	-0.026	-0.019	-0.020	-0.021	-0.007	-0.108	-0.111	-0.107	-0.049	-0.058	-0.058	-0.049	
10.39	.757	-0.039	-0.030	-0.026	-0.033	-0.035	-0.023	-0.089	-0.081	-0.076	-0.061	-0.052	-0.046	-0.035	
8.76	.795	-0.066	-0.056	-0.055	-0.068	-0.059	-0.056	-0.088	-0.079	-0.072	-0.068	-0.058	-0.049	-0.038	
7.18	.832	-0.141	-0.137	-0.136	-0.167	-0.164	-0.163	-0.177	-0.175	-0.175	-0.174	-0.150	-0.127	-0.125	
5.36	.870	-0.146	-0.147	-0.142	-0.176	-0.175	-0.174	-0.182	-0.182	-0.182	-0.181	-0.155	-0.131	-0.129	
3.99	.908	-0.115	-0.116	-0.116	-0.128	-0.126	-0.124	-0.131	-0.131	-0.131	-0.131	-0.121	-0.104	-0.103	
2.35	.943	-0.033	-0.031	-0.029	-0.029	-0.029	-0.029	-0.047	-0.047	-0.047	-0.047	-0.036	-0.026	-0.026	
1.36	.964	-0.014	-0.012	-0.008	-0.008	-0.008	-0.008	-0.019	-0.019	-0.019	-0.018	-0.012	-0.008	-0.008	
.73	.983	-0.063	-0.063	-0.063	-0.063	-0.063	-0.063	-0.076	-0.076	-0.076	-0.076	-0.061	-0.052	-0.052	
.36	.993	-0.087	-0.085	-0.086	-0.088	-0.089	-0.089	-0.107	-0.107	-0.107	-0.107	-0.091	-0.072	-0.072	
.17	.996	-0.098	-0.095	-0.095	-0.100	-0.101	-0.101	-0.119	-0.119	-0.119	-0.119	-0.091	-0.071	-0.071	
$P_{t,j}/P_a = 10.87$ (max.)				$P_{t,j}/P_a = 10.90$				$P_{t,j}/P_a = 10.90$				$P_{t,j}/P_a = 10.90$			
12.01	.719				-0.027	-0.026	-0.022	-0.108	-0.108	-0.106	-0.046	-0.056	-0.056	-0.045	
10.39	.757				-0.039	-0.038	-0.037	-0.089	-0.089	-0.087	-0.063	-0.077	-0.077	-0.064	
8.76	.795				-0.066	-0.065	-0.062	-0.089	-0.089	-0.087	-0.072	-0.083	-0.083	-0.074	
7.18	.832				-0.145	-0.143	-0.142	-0.176	-0.176	-0.174	-0.174	-0.173	-0.173	-0.166	
5.36	.870				-0.142	-0.142	-0.142	-0.							

TABLE III.- AFTERBODY PRESSURE COEFFICIENTS - Continued

(j) Afterbody IX

 $t_j = \text{Cold}$ 

$\frac{x}{d_4}$	$\frac{K}{l_{\max}}$	Pressure coefficients for -											
		$M_\infty = 0.80$			$M_\infty = 0.90$			$M_\infty = 1.00$			$M_\infty = 1.10$		
		$\theta = 0^\circ$	$\theta = 45^\circ$	$\theta = 72^\circ$	$\theta = 0^\circ$	$\theta = 45^\circ$	$\theta = 72^\circ$	$\theta = 0^\circ$	$\theta = 45^\circ$	$\theta = 72^\circ$	$\theta = 0^\circ$	$\theta = 45^\circ$	$\theta = 72^\circ$
		$P_{t,j}/P_\infty = 1.01$			$P_{t,j}/P_\infty = 1.02$			$P_{t,j}/P_\infty = 1.08$			$P_{t,j}/P_\infty = 1.09$		
16.95	0.60	-0.118	---	-0.226	-0.167	---	-0.350	-0.069	---	-0.294	0.059	---	-0.118
15.22	.644	-1.120	-0.140	-0.157	-0.213	-0.239	-0.261	-0.207	-0.267	-0.292	-0.074	-0.115	-0.192
15.21	.684	-0.079	-0.079	-0.068	-0.093	-0.084	-0.019	-0.261	-0.267	-0.258	-0.139	-0.143	-0.077
11.80	.724	-0.029	-0.045	-0.035	-0.030	-0.042	-0.026	-0.269	-0.265	-0.266	-0.136	-0.099	-0.070
10.09	.764	-0.022	-0.043	-0.035	-0.031	-0.042	-0.029	-0.270	-0.265	-0.265	-0.138	-0.095	-0.065
8.78	.804	-0.022	-0.043	-0.042	-0.056	-0.047	-0.043	-0.264	-0.264	-0.264	-0.139	-0.109	-0.066
6.67	.844	---	-0.050	---	---	-0.054	---	---	-0.154	---	---	-0.156	---
4.96	.884	---	-0.052	---	-0.052	---	-0.052	---	-0.157	---	-0.141	---	-0.135
3.23	.924	-0.036	-0.013	-0.035	-0.015	-0.013	-0.017	-0.088	-0.079	-0.082	-0.140	-0.137	-0.140
2.31	.964	.008	.008	.005	.007	.006	.007	.039	.038	.038	.123	.126	.120
1.54	.964	.023	.021	.023	.028	.028	.028	.027	.087	.089	.089	.089	.089
.17	.996	.028	.028	.026	.026	.026	.022	.111	.111	.111	.028	.028	.028
		$P_{t,j}/P_\infty = 2.00$			$P_{t,j}/P_\infty = 2.07$			$P_{t,j}/P_\infty = 1.99$			$P_{t,j}/P_\infty = 2.01$		
16.95	.60	-1.120	-0.181	-0.225	-0.168	-0.225	-0.269	-0.090	-0.248	-0.256	.041	---	-0.125
15.22	.644	-1.121	-0.182	-0.209	-0.235	-0.254	-0.265	-0.203	-0.248	-0.298	-0.074	-0.115	-0.190
15.21	.684	-0.077	-0.077	-0.077	-0.068	-0.081	-0.018	-0.260	-0.268	-0.268	-0.134	-0.096	---
11.80	.724	-0.025	-0.044	-0.044	-0.050	-0.051	-0.022	-0.263	-0.265	-0.265	-0.132	-0.099	-0.070
10.09	.764	-0.021	-0.041	-0.035	-0.031	-0.041	-0.027	-0.263	-0.265	-0.265	-0.133	-0.091	-0.069
8.78	.804	-0.021	-0.041	-0.040	-0.055	-0.053	-0.035	-0.264	-0.264	-0.264	-0.139	-0.103	-0.070
6.67	.844	---	-0.07	---	---	-0.071	---	---	-0.168	---	---	-0.136	---
4.96	.884	---	-0.032	---	-0.020	---	-0.034	---	-0.166	---	---	-0.141	---
3.23	.924	-0.012	-0.008	-0.012	-0.010	-0.007	-0.011	-0.042	-0.055	-0.055	-0.142	-0.137	-0.142
2.31	.964	.008	.008	.008	.013	.012	.014	.062	.059	.060	.128	.128	.128
1.54	.964	.026	.026	.026	.026	.026	.026	.021	.100	.098	.099	.087	.087
.17	.996	.007	.009	.010	.019	.021	.021	.113	.113	.113	.032	.030	.033
		$P_{t,j}/P_\infty = 2.90$			$P_{t,j}/P_\infty = 3.00$			$P_{t,j}/P_\infty = 2.98$			$P_{t,j}/P_\infty = 2.97$		
16.95	.60	-1.121	---	-0.228	-0.168	---	-0.326	-0.091	---	-0.293	-0.059	---	-0.180
15.22	.644	-1.122	-0.180	-0.209	-0.235	-0.254	-0.265	-0.205	-0.248	-0.298	-0.075	-0.115	-0.191
15.21	.684	-0.079	-0.061	-0.079	-0.085	-0.064	-0.018	-0.261	-0.268	-0.268	-0.140	-0.095	-0.077
11.80	.724	-0.062	-0.044	-0.026	-0.060	-0.041	-0.022	-0.269	-0.265	-0.265	-0.136	-0.099	-0.070
10.09	.764	-0.053	-0.042	-0.035	-0.051	-0.041	-0.033	-0.271	-0.264	-0.264	-0.138	-0.101	-0.066
8.78	.804	-0.053	-0.043	-0.042	-0.055	-0.049	-0.044	-0.264	-0.269	-0.261	-0.139	-0.109	-0.066
6.67	.844	---	-0.03	---	---	-0.024	---	---	-0.157	---	---	-0.136	---
4.96	.884	---	-0.035	---	-0.031	---	-0.021	---	-0.157	---	---	-0.140	---
3.23	.924	-0.013	-0.003	-0.013	-0.011	-0.007	-0.018	-0.046	-0.057	-0.058	-0.141	-0.137	-0.142
2.31	.964	.006	.006	.009	.013	.012	.013	.060	.057	.058	.125	.125	.125
1.54	.964	.084	.084	.084	.085	.084	.082	.032	.097	.095	.096	.089	.088
.17	.996	-.005	-.001	.001	.014	.013	.017	.104	.104	.104	.001	.007	.006

TABLE III-- AFTERSHOCK PRESSURE COEFFICIENTS - Continued

(1) Afterbody IX - Continued

 $T_J = 800^{\circ} F$ 

$\frac{X}{C_d}$	$\frac{X}{r_{max}}$	Pressure coefficients for -											
		M <sub>∞</sub> = 0.80			M <sub>∞</sub> = 0.90			M <sub>∞</sub> = 1.00			M <sub>∞</sub> = 1.10		
		$\theta = 0^{\circ}$	$\theta = 45^{\circ}$	$\theta = 72^{\circ}$	$\theta = 0^{\circ}$	$\theta = 45^{\circ}$	$\theta = 72^{\circ}$	$\theta = 0^{\circ}$	$\theta = 45^{\circ}$	$\theta = 72^{\circ}$	$\theta = 0^{\circ}$	$\theta = 45^{\circ}$	$\theta = 72^{\circ}$
		$P_{t,i}/P_{\infty} = 1.98$			$P_{t,i}/P_{\infty} = 2.07$			$P_{t,i}/P_{\infty} = 1.99$			$P_{t,i}/P_{\infty} = 1.99$		
16.93	.60	-0.119	-0.121	-0.226	-0.165	-0.229	-0.226	-0.092	-0.230	-0.256	0.041	-0.111	-0.120
15.22	.61	-0.121	-0.139	-0.157	-0.204	-0.229	-0.249	-0.205	-0.230	-0.256	-0.073	-0.111	-0.146
15.31	.62	-0.076	-0.060	-0.035	-0.084	-0.053	-0.071	-0.256	-0.250	-0.159	-0.138	-0.142	-0.094
11.80	.72	-0.060	-0.043	-0.024	-0.069	-0.040	-0.060	-0.211	-0.187	-0.160	-0.134	-0.099	-0.070
10.09	.78	-0.050	-0.041	-0.023	-0.059	-0.039	-0.052	-0.173	-0.165	-0.157	-0.106	-0.099	-0.094
8.38	.88	-0.050	-0.042	-0.024	-0.053	-0.044	-0.041	-0.166	-0.156	-0.151	-0.120	-0.108	-0.104
6.67	.94	—	-0.046	—	—	-0.049	—	—	-0.170	—	—	-0.126	—
4.96	.98	—	-0.035	—	—	-0.032	—	—	-0.158	-0.156	—	-0.142	-0.141
3.25	.99	—	-0.002	-0.005	-0.009	-0.007	-0.004	-0.003	-0.001	-0.004	-0.002	-0.002	-0.002
2.51	.99	—	-0.012	-0.011	-0.015	-0.017	-0.015	-0.018	0.006	0.005	0.004	-0.004	-0.004
1.74	.99	—	-0.011	-0.011	-0.011	-0.009	-0.008	-0.008	0.001	0.000	0.000	-0.003	-0.002
.17	.99	—	-0.004	-0.005	-0.005	-0.007	-0.007	-0.007	0.000	0.000	0.000	-0.003	-0.001
		$P_{t,i}/P_{\infty} = 2.98$			$P_{t,i}/P_{\infty} = 2.98$			$P_{t,i}/P_{\infty} = 2.97$			$P_{t,i}/P_{\infty} = 2.99$		
16.93	.60	-0.120	-0.121	-0.227	-0.167	-0.229	-0.229	-0.091	-0.230	-0.256	0.041	-0.111	-0.122
15.22	.61	-0.121	-0.139	-0.158	-0.204	-0.229	-0.249	-0.207	-0.249	-0.256	-0.074	-0.112	-0.149
15.31	.62	-0.077	-0.060	-0.038	-0.084	-0.054	-0.071	-0.256	-0.250	-0.160	-0.139	-0.144	-0.095
11.80	.72	-0.062	-0.044	-0.026	-0.068	-0.041	-0.062	-0.211	-0.187	-0.160	-0.135	-0.100	-0.070
10.09	.78	-0.051	-0.042	-0.023	-0.059	-0.041	-0.053	-0.173	-0.165	-0.157	-0.109	-0.100	-0.094
8.38	.88	-0.051	-0.043	-0.024	-0.053	-0.043	-0.042	-0.166	-0.156	-0.152	-0.120	-0.109	-0.096
6.67	.94	—	-0.047	—	—	-0.050	—	—	-0.170	—	—	-0.137	—
4.96	.98	—	-0.033	-0.031	—	-0.034	—	—	-0.158	-0.166	—	-0.143	-0.141
3.25	.99	—	-0.011	-0.008	-0.012	-0.008	-0.006	-0.003	-0.049	-0.041	-0.041	-0.043	-0.039
2.51	.99	—	-0.009	-0.009	-0.011	-0.013	-0.014	-0.015	0.009	0.017	-0.027	-0.026	-0.026
1.74	.99	—	-0.008	-0.008	-0.009	-0.008	-0.009	-0.008	0.000	0.006	-0.007	-0.006	-0.006
.17	.99	—	-0.012	-0.013	-0.013	-0.027	-0.028	-0.028	0.011	0.012	0.013	0.004	0.004
		$P_{t,i}/P_{\infty} = 5.05$			$P_{t,i}/P_{\infty} = 5.01$			$P_{t,i}/P_{\infty} = 5.05$			$P_{t,i}/P_{\infty} = 5.01$		
16.93	.60	—	—	—	—	—	—	-0.092	-0.257	0.041	-0.072	-0.112	-0.121
15.22	.61	—	—	—	—	—	—	-0.083	-0.256	-0.073	-0.112	-0.142	-0.142
15.31	.62	—	—	—	—	—	—	-0.263	-0.250	-0.159	-0.138	-0.143	-0.094
11.80	.72	—	—	—	—	—	—	-0.211	-0.187	-0.159	-0.134	-0.099	-0.071
10.09	.78	—	—	—	—	—	—	-0.173	-0.163	-0.157	-0.107	-0.100	-0.093
8.38	.88	—	—	—	—	—	—	-0.166	-0.153	-0.151	-0.119	-0.108	-0.103
6.67	.94	—	—	—	—	—	—	—	-0.159	—	—	-0.126	—
4.96	.98	—	—	—	—	—	—	—	-0.167	-0.164	—	-0.141	-0.140
3.25	.99	—	—	—	—	—	—	—	-0.162	-0.169	-0.161	-0.127	-0.126
2.51	.99	—	—	—	—	—	—	—	-0.167	-0.167	-0.167	-0.129	-0.128
1.74	.99	—	—	—	—	—	—	—	-0.167	-0.167	-0.167	-0.128	-0.128
.17	.99	—	—	—	—	—	—	—	-0.163	-0.163	-0.163	-0.128	-0.128

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TABLE III.- AFTERBODY PRESSURE COEFFICIENTS - Continued

(i) Afterbody IX - Concluded

$$t_j = 1,200^{\circ} F$$

$\frac{x}{d_3}$	$\frac{x}{r_{max}}$	Pressure coefficients for -											
		M <sub>∞</sub> = 0.60			M <sub>∞</sub> = 0.90			M <sub>∞</sub> = 1.00			M <sub>∞</sub> = 1.10		
		$\theta = 0^{\circ}$	$\theta = 45^{\circ}$	$\theta = 72^{\circ}$	$\theta = 0^{\circ}$	$\theta = 45^{\circ}$	$\theta = 72^{\circ}$	$\theta = 0^{\circ}$	$\theta = 45^{\circ}$	$\theta = 72^{\circ}$	$\theta = 0^{\circ}$	$\theta = 45^{\circ}$	$\theta = 72^{\circ}$
		$P_{t,j}/P_{\infty} = 1.99$			$P_{t,j}/P_{\infty} = 2.07$			$P_{t,j}/P_{\infty} = 1.99$			$P_{t,j}/P_{\infty} = 2.01$		
16.95	.604	-0.119	----	-0.226	-0.167	----	-0.350	-0.091	----	-0.286	0.059	----	-0.127
15.22	.594	-.182	-0.146	-0.246	-0.212	-0.244	-0.262	-0.205	-0.230	-0.254	-.071	-0.117	-0.182
15.51	.584	-.077	-0.059	-0.17	-0.089	-0.054	-0.018	-0.050	-0.050	-0.159	-0.155	-0.156	-0.211
11.80	.784	-.063	-0.047	-0.026	-0.060	-0.011	-0.030	-0.111	-0.187	-0.159	-0.151	-0.097	-0.070
10.09	.764	-.063	-0.042	-0.034	-0.051	-0.011	-0.038	-0.172	-0.156	-0.157	-0.105	-0.097	-0.098
8.36	.504	-.098	-0.04	-0.041	-0.054	-0.043	-0.042	-0.169	-0.156	-0.158	-0.116	-0.106	-0.105
6.67	.584	----	-0.046	----	----	-0.051	----	-0.170	----	----	----	-0.126	----
4.96	.584	----	-0.032	----	-0.030	----	-0.033	-0.022	----	-0.158	----	-0.142	-0.141
3.29	.584	-.010	-0.007	-0.010	-0.008	-0.005	-0.008	-0.066	-0.050	-0.059	-0.142	-0.137	-0.142
2.51	.584	.011	.010	.012	.017	.016	.018	.084	.082	.082	.125	.124	.118
1.54	.584	.032	.030	.030	.039	.038	.039	.105	.101	.101	.084	.084	.083
.17	.595	.026	.025	.027	.025	.025	.025	.127	.125	.125	.093	.093	.093
		$P_{t,j}/P_{\infty} = 2.97$			$P_{t,j}/P_{\infty} = 3.03$			$P_{t,j}/P_{\infty} = 2.98$			$P_{t,j}/P_{\infty} = 2.99$		
16.95	.504	-.120	----	-0.226	-0.166	----	-0.350	-0.090	----	-0.286	-.095	----	-0.128
15.22	.584	-.121	-0.139	-0.249	-0.212	-0.258	-0.269	-0.205	-0.249	-0.254	-.172	-0.107	-0.182
15.51	.584	-.077	-0.059	-0.077	-0.063	-0.060	-0.060	-0.213	-0.187	-0.159	-0.155	-0.157	-0.211
11.80	.784	-.063	-0.047	-0.063	-0.058	-0.060	-0.060	-0.172	-0.156	-0.157	-0.105	-0.097	-0.098
10.09	.764	-.063	-0.042	-0.035	-0.049	-0.039	-0.031	-0.166	-0.156	-0.157	-0.115	-0.105	-0.105
8.36	.504	-.098	-0.044	-0.041	-0.051	-0.045	-0.042	----	-0.170	----	----	----	----
6.67	.584	----	-0.046	----	----	-0.050	----	----	-0.159	-0.166	----	-0.142	----
4.96	.584	----	-0.031	----	-0.031	----	-0.033	-0.021	----	-0.159	-0.166	-0.142	-0.140
3.29	.584	-.010	-0.007	-0.010	-0.007	-0.004	-0.007	-0.053	-0.044	-0.044	-0.142	-0.139	-0.142
2.51	.584	.011	.010	.013	.018	.016	.018	.099	.097	.097	.124	.124	.118
1.54	.584	.030	.029	.031	.039	.038	.039	.100	.097	.098	.088	.087	.087
.17	.595	.016	.017	.020	.022	.022	.024	.119	.117	.119	.055	.053	.053
		$P_{t,j}/P_{\infty} = 4.98$			$P_{t,j}/P_{\infty} = 4.98$			$P_{t,j}/P_{\infty} = 4.98$			$P_{t,j}/P_{\infty} = 4.98$		
16.95	.604							-.090	-.099	-.096	.041	----	-0.126
15.22	.594							-.206	-.249	-.254	-.075	-.111	-0.147
15.51	.584							-.201	-.250	-.259	-.127	-.142	-0.055
11.80	.784							-.212	-.188	-.159	-.148	-.140	-0.072
10.09	.764							-.172	-.156	-.159	-.105	-.100	-0.098
8.36	.504							-.166	-.156	-.158	-.120	-.109	-0.106
6.67	.584							----	-.172	----	----	-.257	----
4.96	.584							----	-.159	-.166	----	-.143	-.141
3.29	.584							-.036	-.036	-.036	-.134	-.140	-0.142
2.51	.584							-.069	-.069	-.066	-.125	-.125	-0.125
1.54	.584							.110	.108	.109	.089	.088	.088
.17	.595							.140	.140	.141	.061	.059	.059

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TABLE III.-- AFTERSHOCK PRESSURE COEFFICIENTS - Continued

## (k) Afterbody X

 $t_j = \text{Cold}$ 

$\frac{x}{d_j}$	$\frac{x}{l_{\max}}$	Pressure coefficients for -												
		$M_\infty = 0.50$			$M_\infty = 0.90$			$M_\infty = 1.00$			$M_\infty = 1.10$			
		$\theta = 0^\circ$	$\theta = 45^\circ$	$\theta = 72^\circ$	$\theta = 0^\circ$	$\theta = 45^\circ$	$\theta = 72^\circ$	$\theta = 0^\circ$	$\theta = 45^\circ$	$\theta = 72^\circ$	$\theta = 0^\circ$	$\theta = 45^\circ$	$\theta = 72^\circ$	
		$P_{t,j}/P_\infty = 0.94$			$P_{t,j}/P_\infty = 0.92$			$P_{t,j}/P_\infty = 0.88$			$P_{t,j}/P_\infty = 0.80$			
12.01	.719	-0.017	-0.011	-0.001	-0.008	-0.002	0.003	-0.102	-0.096	-0.089	-0.050	-0.046	-0.038	
10.39	.727	-0.018	-0.012	-0.007	-0.007	-0.006	0.001	-0.083	-0.077	-0.076	-0.056	-0.053	-0.048	
8.76	.793	-0.019	-0.011	-0.014	-0.011	-0.004	-0.007	-0.070	-0.064	-0.063	-0.053	-0.053	-0.051	
7.18	.852	-0.019	-0.017	-0.017	-0.012	-0.011	-0.010	-0.025	-0.019	-0.019	-0.016	-0.016	-0.015	
5.56	.870	-0.020	-0.021	-0.022	-0.019	-0.016	-0.016	-0.023	-0.023	-0.023	-0.013	-0.013	-0.013	
3.95	.905	-0.021	-0.026	-0.026	-0.021	-0.016	-0.022	-0.028	-0.028	-0.028	-0.017	-0.017	-0.017	
2.35	.945	-0.024	-0.043	-0.043	-0.042	-0.039	-0.039	-0.042	-0.042	-0.042	-0.025	-0.025	-0.025	
1.75	.964	-0.023	-0.026	-0.026	-0.026	-0.025	-0.025	-0.025	-0.025	-0.025	-0.019	-0.019	-0.019	
.73	.983	-0.026	-0.072	-0.073	-0.070	-0.070	-0.070	-0.113	-0.113	-0.113	-0.065	-0.065	-0.065	
.50	.993	-0.026	-0.096	-0.097	-0.096	-0.095	-0.095	-0.149	-0.149	-0.149	-0.099	-0.099	-0.099	
.17	.996	-0.028	-0.105	-0.105	-0.113	-0.113	-0.108	-0.167	-0.167	-0.167	-0.113	-0.113	-0.113	
		$P_{t,j}/P_\infty = 1.99$			$P_{t,j}/P_\infty = 2.00$			$P_{t,j}/P_\infty = 2.00$			$P_{t,j}/P_\infty = 2.00$			
12.01	.719	-0.018	-0.006	.004	-0.007	-0.001	.011	-0.098	-0.095	-0.089	-0.058	-0.056	-0.046	
10.39	.727	-0.019	-0.006	-0.006	-0.006	-0.003	.003	-0.097	-0.094	-0.089	-0.061	-0.059	-0.049	
8.76	.793	-0.019	-0.014	-0.016	-0.015	-0.010	-0.006	-0.097	-0.094	-0.089	-0.063	-0.061	-0.052	
7.18	.852	-0.020	-0.014	-0.013	-0.013	-0.011	-0.010	-0.098	-0.095	-0.090	-0.063	-0.061	-0.053	
5.56	.870	-0.020	-0.019	-0.018	-0.019	-0.013	-0.019	-0.099	-0.096	-0.091	-0.064	-0.062	-0.054	
3.95	.905	-0.021	-0.026	-0.026	-0.025	-0.023	-0.023	-0.100	-0.100	-0.100	-0.065	-0.063	-0.055	
2.35	.945	-0.024	-0.043	-0.043	-0.043	-0.039	-0.039	-0.101	-0.101	-0.101	-0.068	-0.066	-0.068	
1.75	.964	-0.026	-0.064	-0.062	-0.067	-0.062	-0.060	-0.102	-0.101	-0.101	-0.070	-0.068	-0.070	
.73	.983	-0.029	-0.089	-0.087	-0.091	-0.086	-0.087	-0.116	-0.116	-0.116	-0.089	-0.087	-0.086	
.50	.993	-0.030	-0.119	-0.112	-0.121	-0.121	-0.113	-0.160	-0.160	-0.160	-0.113	-0.113	-0.113	
.17	.996	-0.033	-0.143	-0.135	-0.149	-0.149	-0.139	-0.166	-0.166	-0.166	-0.113	-0.113	-0.113	
		$P_{t,j}/P_\infty = 3.08$			$P_{t,j}/P_\infty = 5.00$			$P_{t,j}/P_\infty = 5.02$			$P_{t,j}/P_\infty = 5.01$			
12.01	.719	-0.011	-0.006	.005	-0.007	-0.003	.009	-0.100	-0.096	-0.089	-0.058	-0.056	-0.046	
10.39	.727	-0.009	-0.006	.003	-0.005	-0.002	.001	-0.098	-0.095	-0.089	-0.061	-0.059	-0.049	
8.76	.793	-0.018	-0.007	-0.010	-0.009	-0.004	.006	-0.098	-0.095	-0.089	-0.063	-0.061	-0.053	
7.18	.852	-0.019	-0.014	-0.012	-0.013	-0.011	-0.011	-0.098	-0.095	-0.090	-0.064	-0.062	-0.054	
5.56	.870	-0.020	-0.018	-0.018	-0.018	-0.014	-0.014	-0.098	-0.095	-0.090	-0.065	-0.063	-0.055	
3.95	.905	-0.021	-0.026	-0.026	-0.025	-0.023	-0.023	-0.100	-0.100	-0.100	-0.066	-0.064	-0.066	
2.35	.945	-0.024	-0.043	-0.043	-0.043	-0.039	-0.039	-0.101	-0.101	-0.101	-0.067	-0.065	-0.067	
1.75	.964	-0.026	-0.064	-0.062	-0.067	-0.062	-0.063	-0.102	-0.101	-0.101	-0.073	-0.071	-0.073	
.73	.983	-0.029	-0.089	-0.087	-0.091	-0.086	-0.087	-0.113	-0.112	-0.112	-0.089	-0.087	-0.086	
.50	.993	-0.030	-0.127	-0.126	-0.128	-0.126	-0.120	-0.164	-0.163	-0.163	-0.109	-0.109	-0.109	
.17	.996	-0.033	-0.151	-0.142	-0.158	-0.158	-0.148	-0.166	-0.166	-0.166	-0.113	-0.113	-0.113	
		$P_{t,j}/P_\infty = 4.95$			$P_{t,j}/P_\infty = 4.98$			$P_{t,j}/P_\infty = 5.00$			$P_{t,j}/P_\infty = 5.02$			
12.01	.719	-0.012	-0.007	.003	-0.006	-0.001	.011	-0.099	-0.095	-0.089	-0.059	-0.056	-0.047	
10.39	.727	-0.013	-0.009	.003	-0.004	-0.002	.005	-0.098	-0.094	-0.089	-0.061	-0.059	-0.049	
8.76	.793	-0.015	-0.009	-0.011	-0.010	-0.005	-0.007	-0.098	-0.095	-0.089	-0.066	-0.064	-0.056	
7.18	.852	-0.017	-0.016	-0.012	-0.012	-0.011	-0.010	-0.098	-0.095	-0.090	-0.068	-0.065	-0.057	
5.56	.870	-0.020	-0.021	-0.021	-0.021	-0.018	-0.018	-0.098	-0.095	-0.090	-0.070	-0.068	-0.060	
3.95	.905	-0.024	-0.050	-0.049	-0.050	-0.045	-0.045	-0.100	-0.100	-0.100	-0.071	-0.069	-0.069	
2.35	.945	-0.026	-0.072	-0.072	-0.073	-0.069	-0.069	-0.101	-0.101	-0.101	-0.072	-0.070	-0.072	
1.75	.964	-0.028	-0.093	-0.092	-0.093	-0.088	-0.088	-0.102	-0.101	-0.101	-0.073	-0.071	-0.073	
.73	.983	-0.030	-0.105	-0.103	-0.105	-0.103	-0.103	-0.164	-0.163	-0.163	-0.109	-0.109	-0.109	
.50	.993	-0.032	-0.130	-0.128	-0.132	-0.128	-0.128	-0.166	-0.165	-0.165	-0.111	-0.111	-0.111	
.17	.996	-0.036	-0.162	-0.156	-0.176	-0.155	-0.150	-0.167	-0.166	-0.166	-0.113	-0.113	-0.113	
		$P_{t,j}/P_\infty = 5.28 (\text{max.})$			$P_{t,j}/P_\infty = 6.26 (\text{max.})$			$P_{t,j}/P_\infty = 6.33$			$P_{t,j}/P_\infty = 7.03$			
12.01	.719	-0.012	-0.007	.003	-0.007	-0.002	.010	-0.099	-0.095	-0.089	-0.059	-0.056	-0.047	
10.39	.727	-0.013	-0.008	.003	-0.006	-0.003	.001	-0.099	-0.095	-0.089	-0.061	-0.059	-0.049	
8.76	.793	-0.015	-0.009	-0.011	-0.010	-0.005	-0.007	-0.098	-0.095	-0.089	-0.063	-0.061	-0.052	
7.18	.852	-0.017	-0.016	-0.015	-0.013	-0.012	-0.012	-0.098	-0.095	-0.090	-0.065	-0.063	-0.054	
5.56	.870	-0.020	-0.021	-0.021	-0.021	-0.018	-0.018	-0.098	-0.095	-0.090	-0.070	-0.068	-0.060	
3.95	.905	-0.024	-0.050	-0.049	-0.050	-0.045	-0.045	-0.100	-0.100	-0.100	-0.071	-0.069	-0.069	
2.35	.945	-0.026	-0.072	-0.072	-0.073	-0.069	-0.069	-0.101	-0.101	-0.101	-0.072	-0.070	-0.072	
1.75	.964	-0.028	-0.093	-0.092	-0.093	-0.088	-0.088	-0.102	-0.101	-0.101	-0.073	-0.071	-0.073	
.73	.983	-0.030	-0.105	-0.103	-0.105	-0.103	-0.103	-0.164	-0.163	-0.163	-0.111	-0.111	-0.111	
.50	.993	-0.032	-0.130	-0.128	-0.132	-0.128	-0.128	-0.166	-0.165	-0.165	-0.111	-0.111	-0.111	
.17	.996	-0.036	-0.162	-0.156	-0.176	-0.155	-0.150	-0.167	-0.166	-0.166	-0.113	-0.113	-0.113	
		$P_{t,j}/P_\infty = 7.95 (\text{max.})$												
12.01	.719											-0.057	-0.053	-0.044
10.39	.727											-0.060	-0.056	-0.043
8.76	.793											-0.066	-0.060	-0.049
7.18	.852											-0.068	-0.064	-0.050
5.56	.870											-0.074	-0.069	-0.050
3.95	.905											-0.077	-0.073	-0.051
2.35	.945											-0.079	-0.075	-0.053
1.75	.964											-0.081	-0.077	-0.055
.73	.983											-0.084	-0.079	-0.058
.50	.993											-0.086	-0.081	-0.060
.17	.996											-0.087	-0.087	-0.060

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TABLE III.- AFTERBODY PRESSURE COEFFICIENTS - Continued

(k) Afterbody X - Continued

 $t_j = 800^\circ F$ 

$\frac{x}{d_j}$	$\frac{x}{l_{max}}$	Pressure coefficients for -											
		M <sub>∞</sub> = 0.80			M <sub>∞</sub> = 0.90			M <sub>∞</sub> = 1.00			M <sub>∞</sub> = 1.10		
		θ = 0°			θ = 45°			θ = 72°			θ = 0°		
		$P_{t,j}/P_{\infty} = 2.01$			$P_{t,j}/P_{\infty} = 2.02$			$P_{t,j}/P_{\infty} = 2.00$			$P_{t,j}/P_{\infty} = 1.99$		
12.01	.719	-0.011	-0.003	0.005	-0.006	0.000	0.018	-0.102	-0.091	-0.088	-0.094	-0.093	-0.083
10.59	.737	-0.009	-0.007	-0.002	-0.004	-0.002	0.003	-0.080	-0.080	-0.076	-0.088	-0.080	-0.073
8.76	.793	-0.012	-0.007	-0.010	-0.008	-0.002	-0.003	-0.069	-0.061	-0.066	-0.066	-0.063	-0.059
7.18	.832	-0.024	-0.012	-0.011	-0.011	-0.009	-0.009	-0.036	-0.031	-0.030	-0.034	-0.032	-0.033
5.56	.870	-0.021	-0.017	-0.017	-0.018	-0.014	-0.014	-0.034	-0.031	-0.036	-0.033	-0.038	-0.049
5.93	.908	-0.029	-0.024	-0.023	-0.026	-0.021	-0.021	-0.042	-0.046	-0.047	-0.047	-0.050	-0.057
2.22	.945	-0.046	-0.042	-0.042	-0.043	-0.040	-0.040	-0.051	-0.051	-0.055	-0.051	-0.052	-0.052
1.54	.954	-0.085	-0.071	-0.071	-0.076	-0.063	-0.063	-0.086	-0.081	-0.086	-0.088	-0.083	-0.077
.73	.983	-0.085	-0.082	-0.081	-0.082	-0.081	-0.080	-0.105	-0.101	-0.108	-0.108	-0.103	-0.102
.50	.993	-0.109	-0.109	-0.101	-0.102	-0.112	-0.112	-0.104	-0.106	-0.105	-0.105	-0.104	-0.103
.17	.996	-0.132	-0.131	-0.122	-0.138	-0.137	-0.128	-0.099	-0.099	-0.093	-0.093	-0.091	-0.089
		$P_{t,j}/P_{\infty} = 3.01$				$P_{t,j}/P_{\infty} = 3.00$				$P_{t,j}/P_{\infty} = 3.00$			
18.01	.719	-0.113	-0.068	0.003	-0.007	-0.001	0.010	-0.103	-0.091	-0.087	-0.097	-0.096	-0.087
10.59	.737	-0.111	-0.069	-0.005	-0.006	-0.003	0.001	-0.083	-0.083	-0.079	-0.086	-0.083	-0.086
8.76	.793	-0.115	-0.070	-0.012	-0.009	-0.005	-0.007	-0.071	-0.063	-0.067	-0.067	-0.061	-0.067
7.18	.832	-0.116	-0.071	-0.014	-0.012	-0.010	-0.010	-0.071	-0.061	-0.067	-0.067	-0.064	-0.066
5.56	.870	-0.123	-0.070	-0.020	-0.019	-0.016	-0.016	-0.073	-0.065	-0.073	-0.074	-0.070	-0.071
5.93	.908	-0.132	-0.077	-0.028	-0.028	-0.023	-0.023	-0.074	-0.065	-0.074	-0.074	-0.072	-0.072
2.25	.945	-0.160	-0.046	-0.046	-0.047	-0.045	-0.045	-0.089	-0.082	-0.113	-0.101	-0.089	-0.089
1.54	.954	-0.161	-0.050	-0.053	-0.052	-0.051	-0.051	-0.089	-0.081	-0.105	-0.105	-0.092	-0.092
.73	.983	-0.193	-0.052	-0.052	-0.052	-0.051	-0.051	-0.107	-0.102	-0.112	-0.112	-0.099	-0.097
.50	.993	-0.193	-0.052	-0.052	-0.052	-0.051	-0.051	-0.107	-0.102	-0.112	-0.112	-0.099	-0.097
.17	.996	-0.195	-0.052	-0.052	-0.052	-0.051	-0.051	-0.109	-0.103	-0.113	-0.113	-0.095	-0.093
		$P_{t,j}/P_{\infty} = 5.01$				$P_{t,j}/P_{\infty} = 5.00$				$P_{t,j}/P_{\infty} = 5.00$			
18.01	.719	-0.153	-0.068	0.003	-0.007	-0.001	0.010	-0.103	-0.091	-0.087	-0.097	-0.096	-0.087
10.59	.737	-0.151	-0.069	-0.005	-0.006	-0.003	0.001	-0.081	-0.081	-0.077	-0.088	-0.086	-0.086
8.76	.793	-0.153	-0.071	-0.012	-0.011	-0.009	-0.007	-0.068	-0.061	-0.069	-0.069	-0.063	-0.069
7.18	.832	-0.154	-0.072	-0.014	-0.012	-0.010	-0.010	-0.068	-0.061	-0.069	-0.069	-0.064	-0.066
5.56	.870	-0.159	-0.071	-0.021	-0.021	-0.017	-0.017	-0.074	-0.065	-0.074	-0.074	-0.071	-0.074
5.93	.908	-0.168	-0.079	-0.029	-0.029	-0.023	-0.023	-0.075	-0.067	-0.075	-0.075	-0.072	-0.075
2.25	.945	-0.169	-0.053	-0.053	-0.053	-0.051	-0.051	-0.089	-0.081	-0.119	-0.103	-0.092	-0.092
1.54	.954	-0.169	-0.073	-0.063	-0.067	-0.066	-0.066	-0.089	-0.081	-0.077	-0.077	-0.068	-0.077
.73	.983	-0.196	-0.053	-0.053	-0.053	-0.051	-0.051	-0.107	-0.102	-0.113	-0.103	-0.091	-0.093
.50	.993	-0.196	-0.053	-0.053	-0.053	-0.051	-0.051	-0.107	-0.102	-0.113	-0.103	-0.091	-0.093
.17	.996	-0.197	-0.053	-0.053	-0.053	-0.051	-0.051	-0.109	-0.103	-0.113	-0.104	-0.095	-0.093
		$P_{t,j}/P_{\infty} = 7.01$				$P_{t,j}/P_{\infty} = 7.00$				$P_{t,j}/P_{\infty} = 6.97$			
18.01	.719	-0.177	-0.068	0.006	-0.006	0.009	-0.102	-0.091	-0.086	-0.093	-0.093	-0.084	-0.084
10.59	.737	-0.175	-0.070	-0.005	-0.007	-0.004	0.001	-0.081	-0.081	-0.077	-0.088	-0.086	-0.084
8.76	.793	-0.175	-0.071	-0.012	-0.011	-0.009	-0.007	-0.068	-0.061	-0.069	-0.069	-0.063	-0.069
7.18	.832	-0.176	-0.072	-0.014	-0.012	-0.010	-0.010	-0.068	-0.061	-0.069	-0.069	-0.064	-0.066
5.56	.870	-0.180	-0.068	-0.022	-0.022	-0.018	-0.019	-0.074	-0.065	-0.074	-0.074	-0.071	-0.074
5.93	.908	-0.180	-0.068	-0.025	-0.025	-0.021	-0.021	-0.074	-0.065	-0.074	-0.074	-0.071	-0.074
2.25	.945	-0.180	-0.068	-0.026	-0.026	-0.021	-0.021	-0.075	-0.065	-0.075	-0.075	-0.072	-0.075
1.54	.954	-0.180	-0.068	-0.026	-0.026	-0.021	-0.021	-0.075	-0.065	-0.075	-0.075	-0.072	-0.075
.73	.983	-0.186	-0.136	-0.130	-0.117	-0.113	-0.112	-0.124	-0.124	-0.124	-0.124	-0.106	-0.104
.50	.993	-0.186	-0.136	-0.130	-0.117	-0.113	-0.112	-0.124	-0.124	-0.124	-0.124	-0.106	-0.104
.17	.996	-0.187	-0.136	-0.130	-0.117	-0.113	-0.112	-0.124	-0.124	-0.124	-0.124	-0.106	-0.104
		$P_{t,j}/P_{\infty} = 8.98$				$P_{t,j}/P_{\infty} = 9.00$				$P_{t,j}/P_{\infty} = 9.03$			
12.01	.719	-0.207	-0.068	.005	-0.006	.000	.011	-0.101	-0.091	-0.088	-0.093	-0.092	-0.084
10.59	.737	-0.201	-0.070	-0.005	-0.004	-0.003	.002	-0.081	-0.080	-0.076	-0.086	-0.085	-0.078
8.76	.793	-0.201	-0.071	-0.012	-0.011	-0.009	-0.007	-0.068	-0.061	-0.069	-0.069	-0.063	-0.069
7.18	.832	-0.202	-0.072	-0.014	-0.012	-0.010	-0.010	-0.068	-0.061	-0.069	-0.069	-0.064	-0.066
5.56	.870	-0.206	-0.068	-0.023	-0.023	-0.018	-0.019	-0.074	-0.065	-0.074	-0.074	-0.071	-0.074
5.93	.908	-0.206	-0.068	-0.026	-0.026	-0.021	-0.021	-0.074	-0.065	-0.074	-0.074	-0.071	-0.074
2.25	.945	-0.206	-0.068	-0.026	-0.026	-0.021	-0.021	-0.075	-0.065	-0.075	-0.075	-0.072	-0.075
1.54	.954	-0.206	-0.068	-0.026	-0.026	-0.021	-0.021	-0.075	-0.065	-0.075	-0.075	-0.072	-0.075
.73	.983	-0.206	-0.068	-0.026	-0.026	-0.021	-0.021	-0.075	-0.065	-0.075	-0.075	-0.072	-0.075
.50	.993	-0.206	-0.068	-0.026	-0.026	-0.021	-0.021	-0.075	-0.065	-0.075	-0.075	-0.072	-0.075
.17	.996	-0.206	-0.068	-0.026	-0.026	-0.021	-0.021	-0.075	-0.065	-0.075	-0.075	-0.072	-0.075
		$P_{t,j}/P_{\infty} = 11.02$				$P_{t,j}/P_{\infty} = 10.99$				$P_{t,j}/P_{\infty} = 11.02$			

TABLE III.- AFTERBODY PRESSURE COEFFICIENTS - Continued

(k) Afterbody X - Concluded

 $t_3 = 1,200^{\circ} F$ 

$\frac{x}{d_L}$	$\frac{x}{L_{max}}$	Pressure coefficients for -											
		M <sub>a</sub> = 0.80			M <sub>a</sub> = 0.90			M <sub>a</sub> = 1.00			M <sub>a</sub> = 1.10		
		s = 0°	s = 45°	s = 72°	s = 0°	s = 45°	s = 72°	s = 0°	s = 45°	s = 72°	s = 0°	s = 45°	s = 72°
$P_{t,j}/P_m = 1.99$		$P_{t,j}/P_m = 1.99$				$P_{t,j}/P_m = 2.00$				$P_{t,j}/P_m = 2.01$			
12.01	.739	-.009	-.005	.006	-.005	.002	.013	-.100	-.096	-.088	-.049	-.055	-.037
10.39	.737	-.009	-.007	-.008	-.003	-.001	.004	-.081	-.081	-.076	-.055	-.052	-.046
8.76	.735	-.012	-.006	.008	-.006	-.001	-.003	-.071	-.064	-.058	-.063	-.065	-.051
7.18	.832	-.013	-.013	-.011	-.010	-.008	-.006	-.027	-.023	-.021	-.055	-.053	-.053
5.56	.870	-.003	-.016	-.016	-.017	-.013	-.013	.032	.025	.023	-.053	-.049	-.049
2.92	.908	-.020	-.016	-.015	-.017	-.019	-.019	.049	.046	.046	-.050	-.044	-.041
2.39	.906	-.024	-.017	-.017	-.019	-.019	-.019	.052	.049	.049	-.051	-.046	-.042
1.84	.904	-.024	-.018	-.018	-.020	-.020	-.020	.052	.049	.049	-.051	-.047	-.047
.73	.903	-.023	-.019	-.019	-.020	-.020	-.020	.051	.048	.048	-.050	-.046	-.046
.30	.903	-.107	-.107	-.106	-.108	-.109	-.101	.056	.053	.044	.006	.009	.021
.17	.996	-.127	-.129	-.121	-.135	-.135	-.125	-.037	-.036	-.036	-.043	-.042	-.023
$P_{t,j}/P_m = 3.00$		$P_{t,j}/P_m = 2.99$				$P_{t,j}/P_m = 3.02$				$P_{t,j}/P_m = 2.99$			
12.01	.739	-.010	-.005	.004	-.004	.001	.018	-.099	-.094	-.085	-.092	.008	-.040
10.39	.737	-.009	-.006	.005	-.005	-.002	.003	-.090	-.080	-.076	-.095	-.053	-.053
8.76	.735	-.011	-.006	.009	-.008	-.003	-.005	-.057	-.059	-.055	-.064	-.058	-.053
7.18	.832	-.013	-.012	-.011	-.010	-.009	-.008	-.001	-.000	-.001	-.004	-.004	-.004
5.56	.870	-.022	-.016	-.017	-.019	-.021	-.021	.035	.036	.040	.038	-.033	-.031
3.93	.908	-.029	-.029	-.028	-.027	-.027	-.028	.042	.046	.047	-.049	-.048	-.048
2.39	.905	-.046	-.044	-.043	-.044	-.042	-.041	.031	.034	.034	.109	-.032	-.030
1.84	.904	-.050	-.048	-.048	-.050	-.050	-.050	.037	.037	.037	.042	-.034	-.032
.73	.903	-.050	-.049	-.048	-.050	-.050	-.050	.037	.037	.037	.042	-.034	-.032
.30	.903	-.050	-.049	-.048	-.050	-.050	-.050	.037	.037	.037	.042	-.034	-.032
.17	.996	-.140	-.139	-.138	-.139	-.139	-.138	-.106	-.106	-.106	-.051	-.049	-.031
$P_{t,j}/P_m = 4.98$		$P_{t,j}/P_m = 4.98$				$P_{t,j}/P_m = 4.99$				$P_{t,j}/P_m = 4.98$			
12.01	.739	-.008	-.002	.005	-.005	.000	.012	-.099	-.093	-.083	-.095	-.049	-.041
10.39	.737	-.006	-.001	.004	-.004	-.002	.003	-.098	-.092	-.082	-.092	-.049	-.040
8.76	.735	-.009	-.004	.006	-.009	.005	.015	-.098	-.093	-.083	-.094	-.053	-.045
7.18	.832	-.011	-.010	.008	-.012	-.009	-.008	-.003	-.003	-.003	-.033	-.034	-.034
5.56	.870	-.019	-.015	-.015	-.020	-.015	-.015	.037	.040	.039	-.053	-.050	-.050
3.93	.908	-.027	-.023	-.023	-.028	-.028	-.028	.043	.045	.047	-.047	-.049	-.049
2.39	.905	-.046	-.045	-.045	-.046	-.045	-.045	.032	.035	.034	.111	-.049	-.048
1.84	.904	-.050	-.048	-.048	-.050	-.050	-.050	.032	.035	.035	.047	-.048	-.046
.73	.903	-.050	-.049	-.048	-.050	-.050	-.050	.032	.035	.035	.047	-.048	-.046
.30	.903	-.131	-.130	-.129	-.130	-.130	-.129	-.125	-.125	-.125	-.054	-.052	-.030
.17	.996	-.160	-.157	-.151	-.160	-.160	-.157	-.117	-.117	-.117	-.102	-.095	-.058
$P_{t,j}/P_m = 7.01$		$P_{t,j}/P_m = 6.95$				$P_{t,j}/P_m = 7.01$				$P_{t,j}/P_m = 6.95$			
12.01	.739	-.013	-.008	.002	-.009	.000	.011	-.099	-.093	-.083	-.091	-.047	-.039
10.39	.737	-.011	-.009	.006	-.004	-.002	.003	-.078	-.078	-.076	-.096	-.046	-.039
8.76	.735	-.014	-.009	.012	-.009	-.005	-.007	-.066	-.066	-.066	-.095	-.055	-.051
7.18	.832	-.017	-.013	-.013	-.012	-.013	-.009	-.002	-.003	-.003	-.005	-.028	-.024
5.56	.870	-.022	-.022	-.022	-.020	-.016	-.016	.037	.039	.039	-.053	-.049	-.049
3.93	.908	-.036	-.035	-.035	-.035	-.035	-.035	.051	.051	.051	-.053	-.049	-.049
2.39	.905	-.057	-.055	-.055	-.050	-.048	-.048	.051	.054	.054	-.110	-.058	-.058
1.84	.904	-.064	-.063	-.063	-.065	-.065	-.065	.051	.054	.054	-.064	-.062	-.062
.73	.903	-.064	-.063	-.063	-.065	-.065	-.065	.051	.054	.054	-.064	-.062	-.062
.30	.903	-.117	-.116	-.114	-.118	-.118	-.117	-.103	-.103	-.103	-.077	-.077	-.048
.17	.996	-.193	-.192	-.184	-.193	-.193	-.189	-.181	-.181	-.181	-.128	-.127	-.095
$P_{t,j}/P_m = 9.01$		$P_{t,j}/P_m = 8.99$				$P_{t,j}/P_m = 8.99$				$P_{t,j}/P_m = 8.96$			
12.01	.739	-.011	-.005	.006	-.006	.000	.011	-.101	-.094	-.085	-.093	-.060	-.082
10.39	.737	-.009	-.006	.002	-.005	-.005	.002	-.080	-.080	-.076	-.098	-.056	-.092
8.76	.735	-.012	-.007	.009	-.009	-.005	-.006	-.068	-.068	-.065	-.098	-.058	-.093
7.18	.832	-.013	-.013	.012	-.012	-.011	-.010	-.013	-.011	-.009	-.004	-.054	-.055
5.56	.870	-.023	-.020	-.020	-.019	-.017	-.018	.034	.037	.037	-.004	-.000	-.001
3.93	.908	-.043	-.040	-.039	-.031	-.027	-.026	.042	.045	.046	-.047	-.049	-.049
2.39	.905	-.059	-.059	-.059	-.050	-.049	-.049	.052	.052	.052	-.050	-.049	-.049
1.84	.904	-.064	-.063	-.063	-.064	-.064	-.064	.052	.052	.052	-.064	-.063	-.063
.73	.903	-.126	-.124	-.124	-.126	-.126	-.124	-.117	-.117	-.117	-.077	-.077	-.048
.30	.903	-.206	-.205	-.205	-.217	-.217	-.216	-.203	-.203	-.203	-.057	-.057	-.037
.17	.996	-.226	-.225	-.217	-.217	-.216	-.215	-.199	-.198	-.197	-.057	-.057	-.037
$P_{t,j}/P_m = 11.01$		$P_{t,j}/P_m = 10.91$				$P_{t,j}/P_m = 11.01$				$P_{t,j}/P_m = 10.91$			
12.01	.739							-.101	-.094	-.085	-.094	-.051	-.082
10.39	.737							-.090	-.084	-.076	-.086	-.057	-.091
8.76	.735							-.067	-.060	-.054	-.063	-.058	-.063
7.18	.832							-.009	-.008	-.007	-.005	-.003	-.003
5.56	.870							-.036	-.036	-.037	-.034	-.020	-.027
3.93	.908							-.042	-.043	-.046	-.043	-.026	-.036
2.39	.905							-.030	-.033	-.032	-.030	-.018	-.027
1.84	.904							-.019	-.018	-.017	-.015	-.011	-.015
.73	.903							-.023	-.019	-.017	-.015	-.011	-.015
.30	.903							-.078	-.075	-.064	-.069	-.057	-.065
.17	.996							-.159	-.141	-.120	-.159	-.057	-.057

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TABLE III.- AFTERBODY PRESSURE COEFFICIENTS - Continued

(i) Afterbody XI

$t_3 = \text{Cold}$

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TABLE III.—AFTERBODY PRESSURE COEFFICIENTS - Continued

(1) Afterbody XI - Continued

$t_1 = 800^{\circ} F$

$\frac{x}{d_J}$	$\frac{x}{L_{max}}$	Fracture coefficients for -											
		M <sub>a</sub> = 0.80			M <sub>a</sub> = 0.90			M <sub>a</sub> = 1.00			M <sub>a</sub> = 1.10		
		$\theta = 0^{\circ}$	$\theta = 45^{\circ}$	$\theta = 72^{\circ}$	$\theta = 0^{\circ}$	$\theta = 45^{\circ}$	$\theta = 72^{\circ}$	$\theta = 0^{\circ}$	$\theta = 45^{\circ}$	$\theta = 72^{\circ}$	$\theta = 0^{\circ}$	$\theta = 45^{\circ}$	$\theta = 72^{\circ}$
		$P_{t,J}/P_m = 2.00$				$P_{t,J}/P_m = 1.99$				$P_{t,J}/P_m = 1.99$			
12.01	.719	-	-	-	-	-	-	-	-	-	-	-	-
10.39	.757	-.018	-.008	-.067	-.004	-.002	-.009	-.009	-.009	-.009	-.009	-.009	-.009
8.76	.792	-.065	-.053	-.052	-.054	-.053	-.052	-.053	-.053	-.053	-.053	-.053	-.053
7.18	.826	-.010	-.009	-.014	-.004	-.003	-.004	-.004	-.004	-.004	-.004	-.004	-.004
5.56	.860	-.002	-.002	-.002	-.002	-.002	-.002	-.002	-.002	-.002	-.002	-.002	-.002
3.95	.894	.001	.001	.002	.001	.001	.002	.002	.002	.002	.002	.002	.002
2.35	.925	.009	.009	.004	.009	.009	.006	.006	.006	.006	.006	.006	.006
1.75	.954	.009	.008	.008	.009	.008	.007	.007	.007	.007	.007	.007	.007
.75	.983	.009	.009	.009	.009	.009	.008	.008	.008	.008	.008	.008	.008
.35	.995	.009	.009	.009	.009	.009	.008	.008	.008	.008	.008	.008	.008
.17	.995	.009	.009	.008	.009	.009	.008	.008	.008	.008	.008	.008	.008
		$P_{t,J}/P_m = 2.99$				$P_{t,J}/P_m = 2.99$				$P_{t,J}/P_m = 3.00$			
12.01	.719	-	-	-	-	-	-	-	-	-	-	-	-
10.39	.757	-.018	-.017	-.299	-.004	-.003	-.004	-.004	-.004	-.004	-.004	-.004	-.004
8.76	.792	-.065	-.063	-.061	-.054	-.053	-.052	-.053	-.053	-.053	-.053	-.053	-.053
7.18	.826	-.011	-.011	-.013	-.001	-.001	-.004	-.004	-.004	-.004	-.004	-.004	-.004
5.56	.860	.020	.026	.023	.030	.030	.030	.030	.030	.030	.030	.030	.030
3.95	.894	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004
2.35	.925	.004	.004	.004	.007	.007	.007	.007	.007	.007	.007	.007	.007
1.75	.954	.004	.004	.004	.007	.007	.007	.007	.007	.007	.007	.007	.007
.75	.983	.004	.004	.004	.007	.007	.007	.007	.007	.007	.007	.007	.007
.35	.995	.004	.004	.004	.007	.007	.007	.007	.007	.007	.007	.007	.007
.17	.995	.004	.004	.004	.007	.007	.007	.007	.007	.007	.007	.007	.007
		$P_{t,J}/P_m = 4.98$				$P_{t,J}/P_m = 4.99$				$P_{t,J}/P_m = 5.00$			
12.01	.719	-	-	-	-	-	-	-	-	-	-	-	-
10.39	.757	-.007	-.007	-.007	-.001	-.001	-.006	-.006	-.006	-.006	-.006	-.006	-.006
8.76	.792	-.112	-.113	-.296	-.005	-.005	-.005	-.005	-.005	-.005	-.005	-.005	-.005
7.18	.826	-.006	-.006	-.006	-.003	-.003	-.003	-.003	-.003	-.003	-.003	-.003	-.003
5.56	.860	.007	.008	.007	.007	.007	.007	.007	.007	.007	.007	.007	.007
3.95	.894	.003	.004	.004	.006	.006	.006	.006	.006	.006	.006	.006	.006
2.35	.925	.003	.004	.004	.006	.006	.006	.006	.006	.006	.006	.006	.006
1.75	.954	.003	.004	.004	.006	.006	.006	.006	.006	.006	.006	.006	.006
.75	.983	.003	.004	.004	.006	.006	.006	.006	.006	.006	.006	.006	.006
.35	.995	.003	.004	.004	.006	.006	.006	.006	.006	.006	.006	.006	.006
.17	.995	.003	.004	.004	.006	.006	.006	.006	.006	.006	.006	.006	.006
		$P_{t,J}/P_m = 6.99$				$P_{t,J}/P_m = 6.99$				$P_{t,J}/P_m = 6.98$			
12.01	.719	-	-	-	-	-	-	-	-	-	-	-	-
10.39	.757	-.010	-.009	-.009	-.004	-.004	-.004	-.004	-.004	-.004	-.004	-.004	-.004
8.76	.792	-.065	-.063	-.062	-.053	-.053	-.052	-.053	-.053	-.053	-.053	-.053	-.053
7.18	.826	-.006	-.006	-.006	-.003	-.003	-.003	-.003	-.003	-.003	-.003	-.003	-.003
5.56	.860	.027	.029	.027	.030	.030	.030	.030	.030	.030	.030	.030	.030
3.95	.894	.005	.006	.006	.007	.007	.007	.007	.007	.007	.007	.007	.007
2.35	.925	.005	.006	.006	.007	.007	.007	.007	.007	.007	.007	.007	.007
1.75	.954	.005	.006	.006	.007	.007	.007	.007	.007	.007	.007	.007	.007
.75	.983	.005	.006	.006	.007	.007	.007	.007	.007	.007	.007	.007	.007
.35	.995	.005	.006	.006	.007	.007	.007	.007	.007	.007	.007	.007	.007
.17	.995	.005	.006	.006	.007	.007	.007	.007	.007	.007	.007	.007	.007
		$P_{t,J}/P_m = 9.01$				$P_{t,J}/P_m = 8.99$				$P_{t,J}/P_m = 8.98$			
12.01	.719	-	-	-	-	-	-	-	-	-	-	-	-
10.39	.757	-.007	-.006	-.006	-.002	-.002	-.006	-.006	-.006	-.006	-.006	-.006	-.006
8.76	.792	-.062	-.061	-.061	-.052	-.052	-.051	-.051	-.051	-.051	-.051	-.051	-.051
7.18	.826	-.006	-.006	-.006	-.003	-.003	-.003	-.003	-.003	-.003	-.003	-.003	-.003
5.56	.860	.023	.026	.026	.029	.029	.029	.029	.029	.029	.029	.029	.029
3.95	.894	.005	.006	.006	.007	.007	.007	.007	.007	.007	.007	.007	.007
2.35	.925	.005	.006	.006	.007	.007	.007	.007	.007	.007	.007	.007	.007
1.75	.954	.005	.006	.006	.007	.007	.007	.007	.007	.007	.007	.007	.007
.75	.983	.005	.006	.006	.007	.007	.007	.007	.007	.007	.007	.007	.007
.35	.995	.005	.006	.006	.007	.007	.007	.007	.007	.007	.007	.007	.007
.17	.995	.005	.006	.006	.007	.007	.007	.007	.007	.007	.007	.007	.007
		$P_{t,J}/P_m = 10.97$				$P_{t,J}/P_m = 10.97$				$P_{t,J}/P_m = 10.97$			
12.01	.719	-	-	-	-	-	-	-	-	-	-	-	-
10.39	.757	-	-	-	-	-	-	-	-	-	-	-	-
8.76	.792	-	-	-	-	-	-	-	-	-	-	-	-
7.18	.826	-	-	-	-	-	-	-	-	-	-	-	-
5.56	.860	-	-	-	-	-	-	-	-	-	-	-	-
3.95	.894	-	-	-	-	-	-	-	-	-	-	-	-
2.35	.925	-	-	-	-	-	-	-	-	-	-	-	-
1.75	.954	-	-	-	-	-	-	-	-	-	-	-	-
.75	.983	-	-	-	-	-	-	-	-	-	-	-	-
.35	.995	-	-	-	-	-	-	-	-	-	-	-	-
.17	.995	-	-	-	-	-	-	-	-	-	-	-	-

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TABLE III.-- AFTERBODY PRESSURE COEFFICIENTS - Continued

(1) Afterbody XI - Concluded

 $T_0 = 1,200^{\circ}$  F

$\frac{x}{d_1}$	$\frac{x}{d_{max}}$	Pressure coefficients for --											
		M <sub>a</sub> = 0.80			M <sub>a</sub> = 0.90			M <sub>a</sub> = 1.00			M <sub>a</sub> = 1.10		
		$\theta = 0^{\circ}$	$\theta = 45^{\circ}$	$\theta = 72^{\circ}$	$\theta = 0^{\circ}$	$\theta = 45^{\circ}$	$\theta = 72^{\circ}$	$\theta = 0^{\circ}$	$\theta = 45^{\circ}$	$\theta = 72^{\circ}$	$\theta = 0^{\circ}$	$\theta = 45^{\circ}$	$\theta = 72^{\circ}$
		$P_{t,J}/P_a = 1.99$				$P_{t,J}/P_a = 1.98$				$P_{t,J}/P_a = 1.98$			
12.01	.719	-0.009	-0.070	-0.062	-0.004	-0.064	-0.061	-0.108	-0.095	-0.101	-0.188	-0.167	-0.096
10.39	.757	-0.313	-0.318	-0.297	-0.101	-0.377	-0.356	-0.272	-0.260	-0.262	-0.182	-0.188	-0.167
8.76	.795	-0.068	-0.064	-0.061	-0.057	-0.056	-0.055	-0.315	-0.311	-0.301	-0.251	-0.248	-0.241
7.18	.832	-0.011	-0.010	-0.015	-0.003	-0.003	-0.007	-0.208	-0.211	-0.215	-0.194	-0.189	-0.190
5.56	.870	.024	.024	.027	.035	.034	.034	.018	.018	.019	.127	.125	.125
3.93	.908	.051	.044	.042	.059	.059	.059	.147	.147	.148	.046	.045	.045
2.35	.946	.097	.089	.084	.087	.087	.087	.156	.156	.156	.125	.125	.125
1.75	.984	.175	.170	.172	.168	.179	.179	.163	.160	.162	.123	.123	.123
.75	.995	.200	.194	.193	.190	.189	.189	.167	.167	.166	.122	.122	.122
.17	.996	.200	.196	.196	.196	.196	.196	.154	.154	.154	.122	.122	.122
		$P_{t,J}/P_a = 2.97$				$P_{t,J}/P_a = 2.98$				$P_{t,J}/P_a = 3.00$			
12.01	.719	-0.007	-0.069	-0.069	-0.004	-0.060	-0.060	-1.100	-0.096	-0.096	-0.091	-0.091	-0.094
10.39	.757	-0.314	-0.319	-0.298	-0.106	-0.376	-0.356	-0.270	-0.279	-0.261	-0.186	-0.187	-0.169
8.76	.795	-0.067	-0.068	-0.061	-0.056	-0.056	-0.053	-0.313	-0.310	-0.300	-0.249	-0.249	-0.249
7.18	.832	-0.011	-0.010	-0.013	-0.003	-0.003	-0.006	-0.212	-0.211	-0.214	-0.186	-0.187	-0.187
5.56	.870	.028	.023	.026	.033	.034	.034	.018	.019	.019	.124	.124	.124
3.93	.908	.068	.044	.042	.079	.079	.079	.118	.115	.114	.046	.046	.046
2.35	.946	.099	.092	.092	.067	.067	.067	.146	.145	.145	.099	.099	.099
1.75	.984	.169	.168	.168	.177	.177	.177	.157	.157	.157	.121	.121	.121
.75	.995	.171	.168	.169	.182	.182	.182	.159	.159	.160	.113	.113	.113
.17	.996	.171	.168	.169	.182	.182	.182	.160	.160	.161	.113	.113	.113
		$P_{t,J}/P_a = 4.98$				$P_{t,J}/P_a = 4.97$				$P_{t,J}/P_a = 4.97$			
12.01	.719	-0.006	-0.058	-0.068	-0.001	-0.061	-0.055	-0.099	-0.099	-0.099	-0.052	-0.052	-0.045
10.39	.757	-0.314	-0.319	-0.296	-0.104	-0.375	-0.353	-0.270	-0.278	-0.261	-0.186	-0.187	-0.166
8.76	.795	-0.067	-0.062	-0.060	-0.054	-0.053	-0.052	-0.313	-0.310	-0.302	-0.243	-0.243	-0.243
7.18	.832	-0.011	-0.010	-0.012	-0.006	-0.006	-0.006	-0.206	-0.209	-0.214	-0.186	-0.187	-0.187
5.56	.870	.028	.024	.028	.036	.036	.037	.025	.026	.026	.122	.122	.122
3.93	.908	.068	.045	.045	.068	.068	.068	.121	.119	.116	.045	.045	.045
2.35	.946	.093	.073	.073	.085	.085	.085	.150	.148	.147	.100	.100	.100
1.75	.984	.164	.173	.173	.182	.182	.182	.162	.162	.162	.126	.126	.126
.75	.995	.164	.173	.173	.182	.182	.182	.160	.160	.160	.124	.124	.124
.17	.996	.164	.173	.173	.182	.182	.182	.157	.157	.157	.123	.123	.123
		$P_{t,J}/P_a = 6.99$				$P_{t,J}/P_a = 6.99$				$P_{t,J}/P_a = 6.99$			
12.01	.719	-0.005	-0.058	-0.062	-0.002	-0.050	-0.055	-0.099	-0.099	-0.099	-0.052	-0.052	-0.045
10.39	.757	-0.313	-0.317	-0.295	-0.103	-0.374	-0.350	-0.271	-0.280	-0.263	-0.188	-0.189	-0.200
8.76	.795	-0.067	-0.061	-0.061	-0.056	-0.055	-0.054	-0.313	-0.311	-0.301	-0.246	-0.246	-0.246
7.18	.832	-0.010	-0.009	-0.012	-0.001	-0.001	-0.002	-0.207	-0.204	-0.210	-0.186	-0.187	-0.187
5.56	.870	.028	.027	.028	.036	.036	.037	.025	.026	.026	.122	.122	.122
3.93	.908	.068	.047	.046	.066	.066	.066	.122	.121	.122	.046	.046	.046
2.35	.946	.093	.066	.066	.080	.077	.078	.156	.154	.154	.111	.111	.111
1.75	.984	.164	.168	.168	.177	.177	.177	.171	.171	.171	.140	.140	.140
.75	.995	.164	.168	.168	.177	.177	.177	.162	.162	.162	.125	.125	.125
.17	.996	.164	.168	.168	.177	.177	.177	.160	.160	.160	.121	.121	.121
		$P_{t,J}/P_a = 9.00$				$P_{t,J}/P_a = 8.99$				$P_{t,J}/P_a = 8.96$			
12.01	.719	-0.007	-0.069	-0.069	-0.003	-0.057	-0.057	-0.100	-0.096	-0.096	-0.050	-0.050	-0.044
10.39	.757	-0.313	-0.317	-0.295	-0.103	-0.374	-0.350	-0.271	-0.280	-0.263	-0.187	-0.188	-0.219
8.76	.795	-0.067	-0.061	-0.061	-0.056	-0.055	-0.054	-0.313	-0.311	-0.301	-0.246	-0.246	-0.246
7.18	.832	-0.010	-0.009	-0.012	-0.001	-0.001	-0.002	-0.207	-0.204	-0.210	-0.186	-0.187	-0.187
5.56	.870	.028	.027	.028	.036	.036	.037	.025	.026	.026	.122	.122	.122
3.93	.908	.068	.047	.046	.066	.066	.066	.122	.121	.122	.046	.046	.046
2.35	.946	.093	.062	.062	.080	.077	.078	.156	.154	.154	.122	.122	.122
1.75	.984	.164	.161	.161	.170	.170	.170	.163	.163	.163	.120	.120	.120
.75	.995	.164	.161	.161	.170	.170	.170	.159	.159	.159	.118	.118	.118
.17	.996	.164	.161	.161	.170	.170	.170	.157	.157	.157	.117	.117	.117
		$P_{t,J}/P_a = 10.96$				$P_{t,J}/P_a = 10.97$							
12.01	.719							-0.271	-0.101	-0.097	-0.050	-0.050	-0.045
10.39	.757							-0.271	-0.260	-0.264	-0.194	-0.194	-0.194
8.76	.795							-0.218	-0.210	-0.203	-0.168	-0.168	-0.168
7.18	.832							-0.208	-0.194	-0.190	-0.159	-0.159	-0.159
5.56	.870							-0.164	-0.164	-0.167	-0.127	-0.127	-0.127
3.93	.908							-0.156	-0.156	-0.156	-0.126	-0.126	-0.126
2.35	.946							-0.178	-0.170	-0.171	-0.137	-0.137	-0.137
1.75	.984							-0.152	-0.149	-0.155	-0.121	-0.121	-0.121
.75	.995							-0.153	-0.153	-0.157	-0.120	-0.120	-0.120
.17	.996							-0.140	-0.144	-0.148	-0.111	-0.111	-0.111

TABLE III.- AFTERSHOOT PRESSURE COEFFICIENTS - Continued

(n) Afterbody XII

 $t_1 = \text{Cold}$ 

$\frac{x}{d_0}$	$\frac{x}{l_{\text{max}}}$	Pressure coefficients for -											
		M <sub>∞</sub> = 0.80			M <sub>∞</sub> = 0.90			M <sub>∞</sub> = 1.00			M <sub>∞</sub> = 1.10		
		$\theta = 0^\circ$	$\theta = 45^\circ$	$\theta = 72^\circ$	$\theta = 0^\circ$	$\theta = 45^\circ$	$\theta = 72^\circ$	$\theta = 0^\circ$	$\theta = 45^\circ$	$\theta = 72^\circ$	$\theta = 0^\circ$	$\theta = 45^\circ$	$\theta = 72^\circ$
		$P_{t,j}/P_\infty = 1.04$			$P_{t,j}/P_\infty = 1.06$			$P_{t,j}/P_\infty = 1.10$			$P_{t,j}/P_\infty = 0.99$		
12.01	.719	-.016	-.010	.004	-.009	-.005	.012	-.097	-.091	-.073	-.059	-.056	-.039
10.39	.737	-.027	-.019	-.016	-.023	-.014	-.011	-.065	-.070	-.070	-.054	-.052	-.052
8.76	.755	-.027	-.024	-.027	-.028	-.027	-.025	-.079	-.078	-.077	-.059	-.063	-.061
7.18	.782	-.008	-.026	-.024	-.018	-.017	-.019	-.125	-.122	-.110	-.062	-.059	-.058
5.36	.810	-.114	-.110	-.103	-.128	-.125	-.122	-.110	-.103	-.100	-.054	-.058	-.076
2.92	.918	-.156	-.141	-.140	-.177	-.171	-.174	-.267	-.253	-.261	-.105	-.109	-.129
1.54	.924	-.087	-.087	-.092	-.090	-.090	-.095	-.084	-.087	-.089	-.159	-.154	-.142
.73	.933	-.002	-.004	-.007	.011	.008	.003	.093	.079	.079	-.208	-.198	-.188
.30	.933	.051	.045	.043	.065	.060	.058	.120	.118	.115	-.093	-.102	-.092
.17	.936	.068	.063	.064	.069	.069	.060	.132	.131	.151	-.051	-.056	-.053
		$P_{t,j}/P_\infty = 2.00$			$P_{t,j}/P_\infty = 2.00$			$P_{t,j}/P_\infty = 2.00$			$P_{t,j}/P_\infty = 2.00$		
12.01	.719	-.016	-.007	.009	-.010	.001	.012	-.100	-.090	-.076	-.056	-.052	-.036
10.39	.737	-.026	-.019	-.016	-.022	-.014	-.011	-.066	-.078	-.077	-.059	-.048	-.048
8.76	.755	-.027	-.030	-.028	-.023	-.027	-.023	-.065	-.070	-.067	-.054	-.059	-.057
7.18	.782	-.057	-.056	-.051	-.057	-.055	-.049	-.071	-.067	-.061	-.058	-.054	-.049
5.36	.810	-.114	-.109	-.111	-.126	-.122	-.125	-.107	-.101	-.100	-.080	-.074	-.074
3.93	.908	-.179	-.180	-.182	-.227	-.224	-.230	-.348	-.342	-.351	-.202	-.207	-.205
2.35	.905	-.159	-.159	-.152	-.179	-.172	-.174	-.363	-.359	-.359	-.198	-.200	-.193
1.54	.905	-.094	-.091	-.097	-.098	-.098	-.095	-.076	-.076	-.076	-.056	-.052	-.052
.73	.903	-.014	-.015	-.018	.003	.003	.003	.071	-.063	-.063	-.119	-.119	-.119
.30	.903	.053	.048	.045	.055	.049	.048	.126	.121	.119	-.126	-.129	-.119
.17	.906	.046	.044	.043	.071	.068	.068	.135	.133	.133	-.082	-.085	-.079
		$P_{t,j}/P_\infty = 3.00$			$P_{t,j}/P_\infty = 2.96$			$P_{t,j}/P_\infty = 2.96$			$P_{t,j}/P_\infty = 2.99$		
12.01	.719	-.016	-.005	.005	-.011	-.001	.011	-.101	-.090	-.076	-.058	-.051	-.031
10.39	.737	-.026	-.015	-.015	-.023	-.015	-.012	-.086	-.078	-.077	-.051	-.047	-.049
8.76	.755	-.026	-.029	-.027	-.029	-.028	-.023	-.067	-.059	-.067	-.056	-.060	-.056
7.18	.782	-.057	-.054	-.049	-.079	-.077	-.070	-.105	-.071	-.067	-.061	-.068	-.069
5.36	.810	-.114	-.108	-.110	-.130	-.128	-.125	-.108	-.101	-.101	-.068	-.073	-.072
3.93	.908	-.179	-.180	-.181	-.229	-.221	-.231	-.349	-.342	-.342	-.208	-.207	-.206
2.35	.905	-.157	-.150	-.153	-.183	-.176	-.179	-.366	-.362	-.362	-.144	-.144	-.145
1.54	.904	-.093	-.094	-.093	-.099	-.098	-.098	-.093	-.096	-.096	-.135	-.135	-.135
.73	.903	-.003	-.001	-.003	-.003	-.003	-.003	-.040	-.038	-.038	-.126	-.126	-.126
.30	.903	.039	.034	.034	.057	.057	.057	.120	.120	.120	-.036	-.037	-.039
.17	.906	.039	.034	.034	.061	.061	.061	.126	.126	.126	-.137	-.137	-.139
		$P_{t,j}/P_\infty = 4.99$			$P_{t,j}/P_\infty = 4.96$			$P_{t,j}/P_\infty = 4.96$			$P_{t,j}/P_\infty = 4.99$		
12.01	.719	-.016	-.006	.004	-.009	.000	.012	-.102	-.093	-.076	-.050	-.048	-.031
10.39	.737	-.026	-.018	-.013	-.021	-.013	-.011	-.067	-.078	-.077	-.062	-.068	-.068
8.76	.755	-.026	-.029	-.027	-.033	-.027	-.025	-.068	-.071	-.068	-.057	-.059	-.056
7.18	.782	-.055	-.055	-.049	-.078	-.073	-.070	-.104	-.071	-.068	-.051	-.053	-.058
5.36	.810	-.111	-.109	-.110	-.128	-.122	-.125	-.105	-.101	-.100	-.068	-.072	-.070
3.93	.908	-.156	-.152	-.155	-.189	-.176	-.180	-.349	-.342	-.342	-.202	-.201	-.202
2.35	.905	-.100	-.100	-.104	-.103	-.102	-.107	-.028	-.028	-.028	-.106	-.106	-.107
1.54	.904	-.051	-.053	-.056	-.057	-.057	-.057	.063	.065	.065	-.124	-.124	-.125
.73	.903	-.003	-.000	-.000	.023	.023	.023	.109	.106	.106	-.105	-.105	-.105
.30	.903	.003	.003	.002	.027	.027	.027	.110	.108	.108	-.107	-.107	-.107
.17	.906	.008	.003	.002	.027	.027	.027	.110	.108	.108	-.109	-.109	-.109
		$P_{t,j}/P_\infty = 5.82$ (max.)			$P_{t,j}/P_\infty = 6.51$ (max.)			$P_{t,j}/P_\infty = 6.54$			$P_{t,j}/P_\infty = 6.56$		
12.01	.719	-.016	-.006	.004	-.002	-.002	.010	-.102	-.099	-.077	-.057	-.052	-.032
10.39	.737	-.026	-.019	-.017	-.024	-.016	-.014	-.067	-.079	-.077	-.059	-.068	-.069
8.76	.755	-.026	-.029	-.028	-.035	-.026	-.024	-.067	-.071	-.067	-.053	-.059	-.056
7.18	.782	-.057	-.056	-.050	-.084	-.078	-.075	-.101	-.067	-.061	-.053	-.055	-.048
5.36	.810	-.114	-.110	-.111	-.130	-.125	-.125	-.105	-.101	-.100	-.060	-.062	-.060
3.93	.908	-.156	-.151	-.154	-.186	-.176	-.173	-.348	-.342	-.342	-.201	-.201	-.202
2.35	.905	-.101	-.101	-.106	-.107	-.107	-.107	-.028	-.028	-.028	-.122	-.122	-.123
1.54	.904	-.051	-.053	-.056	-.057	-.057	-.057	.063	.065	.065	-.121	-.121	-.121
.73	.903	-.003	-.000	-.000	.023	.023	.023	.109	.106	.106	-.120	-.120	-.120
.30	.903	.003	.003	.002	.027	.027	.027	.110	.108	.108	-.121	-.121	-.121
.17	.906	.008	.003	.002	.027	.027	.027	.110	.108	.108	-.121	-.121	-.121

CONFIDENTIAL

TABLE III.- AFTERBODY PRESSURE COEFFICIENTS - Continued

(a) Afterbody XII - Continued

 $t_3 = 800^{\circ} F$ 

$\frac{x}{d_1}$	$x$ $t_{max}$	Pressure coefficients for -											
		$M_\infty = 0.80$			$M_\infty = 0.90$			$M_\infty = 1.00$			$M_\infty = 1.10$		
		$\theta = 0^\circ$	$\theta = 45^\circ$	$\theta = 72^\circ$	$\theta = 0^\circ$	$\theta = 45^\circ$	$\theta = 72^\circ$	$\theta = 0^\circ$	$\theta = 45^\circ$	$\theta = 72^\circ$	$\theta = 0^\circ$	$\theta = 45^\circ$	$\theta = 72^\circ$
		$P_{t,J}/P_\infty = 2.01$			$P_{t,J}/P_\infty = 1.98$			$P_{t,J}/P_\infty = 2.01$			$P_{t,J}/P_\infty = 2.00$		
12.01	.719	-0.014	-0.009	0.005	-0.010	-0.004	0.011	-0.006	-0.002	-0.007	-0.010	-0.002	-0.009
10.39	.757	-.020	-.018	-.014	-.023	-.016	-.015	-.006	-.006	-.005	-.009	-.005	-.006
8.76	.795	-.026	-.029	-.027	-.025	-.029	-.025	-.006	-.006	-.007	-.009	-.006	-.007
7.18	.832	-.036	-.034	-.034	-.036	-.037	-.030	-.011	-.011	-.011	-.015	-.011	-.010
5.36	.870	-.056	-.054	-.054	-.060	-.057	-.050	-.017	-.017	-.017	-.020	-.017	-.017
3.93	.908	-.086	-.087	-.087	-.109	-.130	-.128	-.108	-.108	-.108	-.100	-.108	-.108
2.35	.935	-.125	-.126	-.126	-.128	-.132	-.132	-.108	-.108	-.108	-.100	-.108	-.108
1.54	.963	-.166	-.168	-.170	-.178	-.173	-.174	-.146	-.146	-.146	-.137	-.146	-.146
.73	.983	-.207	-.211	-.212	-.202	-.194	-.197	-.161	-.161	-.161	-.151	-.161	-.161
.36	.995	-.240	-.245	-.245	-.253	-.252	-.254	-.226	-.226	-.226	-.216	-.226	-.226
.17	.996	-.266	-.263	-.264	-.276	-.273	-.273	-.238	-.238	-.238	-.237	-.238	-.238
		$P_{t,J}/P_\infty = 3.01$			$P_{t,J}/P_\infty = 3.00$			$P_{t,J}/P_\infty = 2.98$			$P_{t,J}/P_\infty = 3.02$		
12.01	.719	-.018	-.009	.006	-.008	-.002	.013	-.008	-.002	-.007	-.010	-.002	-.009
10.39	.757	-.026	-.028	-.024	-.021	-.015	-.010	-.005	-.005	-.005	-.007	-.005	-.007
8.76	.795	-.032	-.034	-.037	-.022	-.026	-.024	-.006	-.006	-.007	-.008	-.006	-.008
7.18	.832	-.046	-.044	-.049	-.049	-.054	-.047	-.012	-.012	-.012	-.011	-.012	-.012
5.36	.870	-.074	-.071	-.071	-.109	-.128	-.121	-.122	-.122	-.122	-.100	-.122	-.122
3.93	.908	-.118	-.120	-.120	-.128	-.130	-.128	-.128	-.128	-.128	-.128	-.128	-.128
2.35	.935	-.159	-.161	-.161	-.178	-.180	-.178	-.148	-.148	-.148	-.140	-.148	-.148
1.54	.963	-.201	-.200	-.207	-.179	-.179	-.174	-.147	-.147	-.147	-.137	-.147	-.147
.73	.983	-.242	-.246	-.247	-.271	-.271	-.264	-.234	-.234	-.234	-.224	-.234	-.234
.36	.995	-.273	-.269	-.267	-.302	-.302	-.297	-.262	-.262	-.262	-.252	-.262	-.262
.17	.996	-.298	-.294	-.294	-.307	-.307	-.307	-.271	-.271	-.271	-.261	-.271	-.271
		$P_{t,J}/P_\infty = 5.01$			$P_{t,J}/P_\infty = 4.99$			$P_{t,J}/P_\infty = 4.98$			$P_{t,J}/P_\infty = 5.03$		
12.01	.719	-.014	-.009	.005	-.009	-.003	.019	-.009	-.002	-.007	-.011	-.002	-.008
10.39	.757	-.024	-.021	-.015	-.022	-.018	-.010	-.005	-.005	-.005	-.007	-.005	-.007
8.76	.795	-.032	-.030	-.027	-.023	-.027	-.024	-.007	-.007	-.007	-.008	-.006	-.008
7.18	.832	-.057	-.054	-.054	-.064	-.064	-.058	-.027	-.027	-.027	-.031	-.027	-.027
5.36	.870	-.114	-.108	-.108	-.129	-.122	-.123	-.110	-.110	-.110	-.100	-.110	-.110
3.93	.908	-.179	-.182	-.181	-.229	-.231	-.230	-.194	-.194	-.194	-.184	-.194	-.194
2.35	.935	-.237	-.237	-.237	-.253	-.253	-.253	-.218	-.218	-.218	-.208	-.218	-.218
1.54	.963	-.309	-.309	-.308	-.320	-.320	-.319	-.286	-.286	-.286	-.276	-.286	-.286
.73	.983	-.363	-.363	-.363	-.387	-.387	-.387	-.354	-.354	-.354	-.344	-.354	-.354
.36	.995	-.403	-.402	-.402	-.426	-.426	-.426	-.393	-.393	-.393	-.383	-.393	-.393
.17	.996	-.424	-.424	-.424	-.450	-.450	-.450	-.419	-.419	-.419	-.409	-.419	-.419
		$P_{t,J}/P_\infty = 7.02$			$P_{t,J}/P_\infty = 7.00$			$P_{t,J}/P_\infty = 6.97$			$P_{t,J}/P_\infty = 6.99$		
12.01	.719	-.015	-.011	.005	-.006	-.002	.015	-.009	-.002	-.007	-.011	-.002	-.008
10.39	.757	-.026	-.020	-.017	-.021	-.018	-.010	-.006	-.006	-.006	-.009	-.007	-.007
8.76	.795	-.047	-.031	-.029	-.033	-.037	-.034	-.016	-.016	-.016	-.020	-.016	-.016
7.18	.832	-.076	-.071	-.071	-.091	-.095	-.093	-.063	-.063	-.063	-.066	-.063	-.063
5.36	.870	-.137	-.110	-.111	-.126	-.121	-.122	-.109	-.109	-.109	-.101	-.109	-.109
3.93	.908	-.181	-.184	-.184	-.228	-.230	-.229	-.194	-.194	-.194	-.184	-.194	-.194
2.35	.935	-.245	-.245	-.245	-.266	-.266	-.266	-.234	-.234	-.234	-.224	-.234	-.234
1.54	.963	-.304	-.304	-.304	-.330	-.330	-.330	-.298	-.298	-.298	-.288	-.298	-.298
.73	.983	-.364	-.364	-.364	-.390	-.390	-.390	-.358	-.358	-.358	-.348	-.358	-.358
.36	.995	-.423	-.423	-.423	-.450	-.450	-.450	-.418	-.418	-.418	-.408	-.418	-.418
.17	.996	-.444	-.444	-.444	-.471	-.471	-.471	-.439	-.439	-.439	-.429	-.439	-.439
		$P_{t,J}/P_\infty = 9.03$			$P_{t,J}/P_\infty = 9.00$			$P_{t,J}/P_\infty = 8.96$			$P_{t,J}/P_\infty = 8.98$		
12.01	.719	-.016	-.010	.003	-.006	-.002	.016	-.008	-.002	-.007	-.011	-.002	-.008
10.39	.757	-.028	-.020	-.016	-.023	-.015	-.010	-.005	-.005	-.005	-.009	-.007	-.007
8.76	.795	-.048	-.033	-.028	-.042	-.037	-.030	-.016	-.016	-.016	-.020	-.016	-.016
7.18	.832	-.086	-.076	-.071	-.101	-.105	-.104	-.071	-.071	-.071	-.061	-.071	-.071
5.36	.870	-.146	-.116	-.111	-.143	-.143	-.143	-.122	-.122	-.122	-.109	-.122	-.122
3.93	.908	-.194	-.194	-.194	-.235	-.235	-.235	-.198	-.198	-.198	-.188	-.198	-.198
2.35	.935	-.253	-.253	-.253	-.285	-.285	-.285	-.252	-.252	-.252	-.242	-.252	-.252
1.54	.963	-.312	-.312	-.312	-.343	-.343	-.343	-.301	-.301	-.301	-.291	-.301	-.301
.73	.983	-.372	-.372	-.372	-.400	-.400	-.400	-.359	-.359	-.359	-.349	-.359	-.359
.36	.995	-.431	-.431	-.431	-.459	-.459	-.459	-.418	-.418	-.418	-.408	-.418	-.418
.17	.996	-.452	-.452	-.452	-.479	-.479	-.479	-.437	-.437	-.437	-.427	-.437	-.437
		$P_{t,J}/P_\infty = 10.96$			$P_{t,J}/P_\infty = 11.01$								
12.01	.719							-.008	-.002	-.007	-.002	-.008	-.008
10.39	.757							-.005	-.005	-.005	-.005	-.004	-.004
8.76	.795							-.006	-.007	-.007	-.006	-.006	-.007
7.18	.832							-.010	-.007	-.007	-.006	-.007	-.008
5.36	.870							-.014	-.010	-.010	-.009	-.008	-.009
3.93	.908							-.024	-.022	-.022	-.021	-.020	-.021
2.35	.935							-.035	-.033	-.033	-.031	-.030	-.031
1.54	.963							-.046	-.045	-.045	-.044	-.043	-.044
.73	.983							-.065	-.065	-.065	-.064	-.063	-.064
.36	.995							-.114	-.114	-.114	-.113	-.113	-.114
.17	.996							-.139	-.139	-.139	-.139	-.139	-.139

TABLE LII.— AFTERBODY PRESSURE COEFFICIENTS — Continued

(n) Afterbody XII - Concluded

 $t_j = 1,200^{\circ} F$ 

$\frac{x}{d_j}$	$\frac{x}{l_{max}}$	Pressure coefficients for —											
		$M_\infty = 0.80$			$M_\infty = 0.90$			$M_\infty = 1.00$			$M_\infty = 1.10$		
		$\theta = 0^{\circ}$	$\theta = 45^{\circ}$	$\theta = 72^{\circ}$	$\theta = 0^{\circ}$	$\theta = 45^{\circ}$	$\theta = 72^{\circ}$	$\theta = 0^{\circ}$	$\theta = 45^{\circ}$	$\theta = 72^{\circ}$	$\theta = 0^{\circ}$	$\theta = 45^{\circ}$	$\theta = 72^{\circ}$
		$P_{t,j}/P_\infty = 2.00$			$P_{t,j}/P_\infty = 1.90$			$P_{t,j}/P_\infty = 2.09$			$P_{t,j}/P_\infty = 2.05$		
12.01	.719	-.014	-.009	.007	-.012	-.006	.010	-.006	-.001	-.007	-.001	-.006	-.007
10.39	.727	-.024	-.017	-.014	-.024	-.016	-.012	-.006	-.006	-.006	-.007	-.006	-.007
8.76	.735	-.023	-.018	-.021	-.026	-.020	-.021	-.006	-.009	-.006	-.007	-.006	-.007
7.18	.742	-.025	-.019	-.017	-.026	-.021	-.021	-.012	-.009	-.010	-.006	-.005	-.006
5.35	.750	-.178	-.177	-.176	-.178	-.176	-.176	-.126	-.126	-.126	-.126	-.126	-.126
4.25	.758	-.177	-.181	-.186	-.175	-.170	-.170	-.110	-.110	-.110	-.105	-.105	-.105
3.18	.765	-.083	-.082	-.083	-.087	-.087	-.087	-.048	-.048	-.048	-.048	-.048	-.048
2.12	.764	-.001	-.006	-.007	-.003	-.007	-.007	.001	.004	.008	-.119	-.119	-.119
1.16	.765	-.005	-.005	-.005	-.005	-.005	-.005	-.005	-.005	-.005	-.121	-.121	-.121
.10	.765	-.005	-.005	-.005	-.005	-.005	-.005	-.005	-.005	-.005	-.125	-.125	-.125
.17	.765	.011	.011	.010	.011	.011	.011	.128	.128	.128	.129	.129	.129
		$P_{t,j}/P_\infty = 3.00$			$P_{t,j}/P_\infty = 3.01$			$P_{t,j}/P_\infty = 2.97$			$P_{t,j}/P_\infty = 3.02$		
12.01	.719	-.016	-.010	.009	-.009	-.006	.011	-.008	-.001	-.007	-.000	-.005	-.007
10.39	.727	-.026	-.018	-.015	-.022	-.014	-.011	-.016	-.016	-.017	-.006	-.015	-.017
8.76	.735	-.027	-.019	-.016	-.024	-.017	-.012	-.017	-.017	-.017	-.007	-.016	-.018
7.18	.742	-.026	-.019	-.016	-.025	-.019	-.019	-.011	-.011	-.011	-.009	-.016	-.018
5.35	.750	-.113	-.115	-.109	-.127	-.125	-.125	-.109	-.109	-.109	-.103	-.103	-.103
4.25	.758	-.115	-.118	-.110	-.127	-.125	-.125	-.109	-.109	-.109	-.103	-.103	-.103
3.18	.765	-.175	-.180	-.180	-.185	-.187	-.187	-.128	-.128	-.128	-.122	-.122	-.122
2.12	.765	-.150	-.145	-.149	-.174	-.170	-.172	-.055	-.055	-.055	-.057	-.057	-.057
1.16	.764	-.089	-.068	-.059	-.088	-.069	-.069	-.009	-.009	-.009	-.052	-.052	-.052
.10	.765	-.009	-.012	-.013	-.006	-.003	-.000	.065	.081	.081	-.101	-.101	-.101
.17	.765	.035	.030	.020	.029	.029	.029	.123	.119	.118	-.097	-.097	-.097
		$P_{t,j}/P_\infty = 5.00$			$P_{t,j}/P_\infty = 5.01$			$P_{t,j}/P_\infty = 5.02$			$P_{t,j}/P_\infty = 5.00$		
12.01	.719	-.015	-.012	.005	-.010	-.006	.015	-.008	-.000	-.007	-.003	-.000	-.007
10.39	.727	-.027	-.018	-.015	-.029	-.017	-.012	-.016	-.016	-.017	-.003	-.012	-.017
8.76	.735	-.029	-.019	-.016	-.029	-.018	-.013	-.017	-.017	-.017	-.003	-.012	-.018
7.18	.742	-.028	-.019	-.016	-.028	-.018	-.013	-.017	-.017	-.017	-.003	-.012	-.018
5.35	.750	-.115	-.112	-.109	-.129	-.125	-.125	-.109	-.109	-.109	-.103	-.103	-.103
4.25	.758	-.115	-.118	-.110	-.127	-.125	-.125	-.109	-.109	-.109	-.103	-.103	-.103
3.18	.765	-.176	-.181	-.181	-.186	-.187	-.187	-.129	-.129	-.129	-.124	-.124	-.124
2.12	.765	-.094	-.071	-.061	-.097	-.076	-.076	-.017	-.017	-.017	-.067	-.067	-.067
1.16	.764	-.094	-.072	-.061	-.097	-.076	-.076	-.017	-.017	-.017	-.137	-.137	-.137
.10	.765	-.022	-.026	-.026	-.006	-.010	-.012	.072	.072	.072	-.072	-.072	-.072
.17	.765	.017	.012	.010	.039	.034	.034	.122	.122	.122	-.103	-.103	-.103
		$P_{t,j}/P_\infty = 0.99$			$P_{t,j}/P_\infty = 7.05$			$P_{t,j}/P_\infty = 6.98$			$P_{t,j}/P_\infty = 7.02$		
12.01	.719	-.017	-.012	.005	-.010	-.005	.011	-.007	-.001	-.007	-.003	-.000	-.008
10.39	.727	-.028	-.019	-.016	-.028	-.018	-.013	-.017	-.017	-.017	-.003	-.012	-.018
8.76	.735	-.029	-.019	-.016	-.029	-.018	-.013	-.017	-.017	-.017	-.003	-.012	-.018
7.18	.742	-.028	-.019	-.016	-.028	-.018	-.013	-.017	-.017	-.017	-.003	-.012	-.018
5.35	.750	-.116	-.113	-.110	-.129	-.125	-.125	-.110	-.110	-.110	-.104	-.104	-.104
4.25	.758	-.116	-.121	-.110	-.126	-.124	-.124	-.110	-.110	-.110	-.104	-.104	-.104
3.18	.765	-.179	-.181	-.181	-.186	-.187	-.187	-.129	-.129	-.129	-.124	-.124	-.124
2.12	.765	-.095	-.072	-.061	-.097	-.076	-.076	-.017	-.017	-.017	-.067	-.067	-.067
1.16	.764	-.095	-.073	-.061	-.097	-.076	-.076	-.017	-.017	-.017	-.137	-.137	-.137
.10	.765	-.023	-.027	-.026	-.006	-.010	-.012	.073	.073	.073	-.103	-.103	-.103
.17	.765	.017	.012	.010	.042	.038	.038	.116	.116	.116	-.142	-.142	-.142
		$P_{t,j}/P_\infty = 5.98$			$P_{t,j}/P_\infty = 5.00$			$P_{t,j}/P_\infty = 5.94$			$P_{t,j}/P_\infty = 5.98$		
12.01	.719	-.015	-.016	.005	-.010	-.006	.012	-.006	-.001	-.007	-.003	-.000	-.011
10.39	.727	-.026	-.017	-.014	-.022	-.013	-.010	-.016	-.016	-.016	-.003	-.011	-.016
8.76	.735	-.026	-.017	-.014	-.022	-.013	-.010	-.016	-.016	-.016	-.003	-.011	-.016
7.18	.742	-.026	-.017	-.014	-.022	-.013	-.010	-.016	-.016	-.016	-.003	-.011	-.016
5.35	.750	-.114	-.112	-.109	-.127	-.125	-.125	-.110	-.110	-.110	-.104	-.104	-.104
4.25	.758	-.114	-.121	-.110	-.126	-.124	-.124	-.110	-.110	-.110	-.104	-.104	-.104
3.18	.765	-.178	-.180	-.180	-.185	-.187	-.187	-.129	-.129	-.129	-.124	-.124	-.124
2.12	.765	-.094	-.071	-.060	-.097	-.076	-.076	-.017	-.017	-.017	-.067	-.067	-.067
1.16	.764	-.094	-.072	-.061	-.097	-.076	-.076	-.017	-.017	-.017	-.137	-.137	-.137
.10	.765	-.023	-.027	-.026	-.006	-.010	-.012	.072	.072	.072	-.103	-.103	-.103
.17	.765	.017	.012	.010	.042	.038	.038	.116	.116	.116	-.142	-.142	-.142
		$P_{t,j}/P_\infty = 10.76$			$P_{t,j}/P_\infty = 10.99$			$P_{t,j}/P_\infty = 10.99$			$P_{t,j}/P_\infty = 10.76$		
12.01	.719												
10.39	.727												
8.76	.735												
7.18	.742												
5.35	.750												
4.25	.758												
3.18	.765												
2.12	.765												
1.16	.764												
.10	.765												
.17	.765												

CONFIDENTIAL

TABLE III.- AFTERBODY PRESSURE COEFFICIENTS - Continued

(n) Afterbody XIII

 $T_1 = \text{Cold}$ 

$\frac{x}{d_1}$	$\frac{x}{r_{\text{max}}}$	Pressure coefficients for -											
		M <sub>∞</sub> = 0.80			M <sub>∞</sub> = 0.90			M <sub>∞</sub> = 1.00			M <sub>∞</sub> = 1.10		
		$\theta = 0^\circ$	$\theta = 45^\circ$	$\theta = 72^\circ$	$\theta = 0^\circ$	$\theta = 45^\circ$	$\theta = 72^\circ$	$\theta = 0^\circ$	$\theta = 45^\circ$	$\theta = 72^\circ$	$\theta = 0^\circ$	$\theta = 45^\circ$	$\theta = 72^\circ$
		$P_{t,J}/P_\infty = 1.02$			$P_{t,J}/P_\infty = 1.04$			$P_{t,J}/P_\infty = 1.05$			$P_{t,J}/P_\infty = 1.08$		
12.01	.719	-0.013	-0.010	-0.001	-0.007	-0.005	0.007	-0.006	-0.001	-0.001	-0.006	-0.009	-0.010
10.39	.757	-.021	-.023	-.016	-.015	-.015	-.005	-.005	-.002	-.002	-.005	-.007	-.004
8.76	.795	-.027	-.023	-.020	-.018	-.018	-.016	-.016	-.008	-.008	-.005	-.005	-.005
7.18	.832	-.041	-.037	-.037	-.039	-.033	-.037	-.037	-.016	-.016	-.005	-.005	-.005
5.56	.870	-.059	-.070	-.069	-.071	-.072	-.078	-.078	-.005	-.005	-.004	-.004	-.004
3.95	.908	-.160	-.155	-.156	-.158	-.164	-.191	-.191	-.106	-.106	-.147	-.152	-.156
2.35	.942	-.238	-.240	-.237	-.237	-.235	-.219	-.219	-.267	-.267	-.127	-.106	-.107
1.54	.954	-.187	-.187	-.197	-.204	-.207	-.237	-.237	-.365	-.365	-.205	-.193	-.193
.73	.953	-.045	-.046	-.042	-.042	-.042	-.047	-.047	-.005	-.005	-.004	-.004	-.004
.53	.939	.018	.014	.013	.007	.023	.082	.082	.032	.032	.200	.201	.193
.17	.936	.058	.059	.058	.051	.048	.047	.047	.054	.051	.130	.124	.127
		$P_{t,J}/P_\infty = 2.01$			$P_{t,J}/P_\infty = 1.99$			$P_{t,J}/P_\infty = 2.00$			$P_{t,J}/P_\infty = 2.00$		
12.01	.719	-.018	-.009	-.000	-.006	-.002	.006	-.038	-.009	-.009	-.053	-.051	-.043
10.39	.757	-.020	-.019	-.024	-.017	-.013	-.007	-.004	-.002	-.002	-.011	-.012	-.008
8.76	.795	-.026	-.028	-.028	-.018	-.019	-.015	-.009	-.003	-.003	-.003	-.003	-.006
7.18	.832	-.040	-.035	-.035	-.035	-.032	-.031	-.031	-.053	-.053	-.059	-.054	-.054
5.56	.870	-.067	-.071	-.070	-.068	-.070	-.068	-.068	-.023	-.023	-.024	-.024	-.043
3.95	.908	-.158	-.157	-.159	-.187	-.183	-.186	-.186	-.135	-.135	-.148	-.144	-.135
2.35	.942	-.238	-.243	-.241	-.317	-.317	-.308	-.308	-.271	-.271	-.204	-.196	-.186
1.54	.954	-.197	-.198	-.204	-.229	-.234	-.242	-.242	-.307	-.307	-.119	-.100	-.107
.73	.953	-.084	-.085	-.088	-.071	-.071	-.078	-.078	-.086	-.086	-.022	-.022	-.022
.53	.939	-.004	-.007	-.007	.014	-.010	.010	.010	.049	.049	.220	.217	.204
.17	.936	.017	.017	.024	.055	.053	.054	.054	.044	.044	.197	.194	.191
		$P_{t,J}/P_\infty = 3.00$			$P_{t,J}/P_\infty = 3.00$			$P_{t,J}/P_\infty = 2.98$			$P_{t,J}/P_\infty = 3.02$		
12.01	.719	-.014	-.009	-.003	-.007	-.001	.008	-.036	-.009	-.009	-.056	-.052	-.043
10.39	.757	-.025	-.024	-.024	-.017	-.018	-.012	-.017	-.004	-.004	-.051	-.051	-.051
8.76	.795	-.043	-.043	-.043	-.034	-.034	-.031	-.031	-.044	-.044	-.051	-.051	-.051
7.18	.832	-.084	-.088	-.088	-.084	-.082	-.081	-.081	-.056	-.056	-.054	-.054	-.054
5.56	.870	-.069	-.072	-.072	-.067	-.069	-.069	-.069	-.057	-.057	-.052	-.052	-.049
3.95	.908	-.162	-.159	-.160	-.190	-.189	-.187	-.187	-.161	-.161	-.153	-.153	-.159
2.35	.942	-.246	-.246	-.246	-.321	-.320	-.320	-.320	-.267	-.267	-.263	-.263	-.184
1.54	.954	-.203	-.203	-.211	-.258	-.252	-.248	-.248	-.304	-.304	-.200	-.201	-.194
.73	.953	-.095	-.093	-.095	-.080	-.080	-.083	-.083	-.108	-.108	-.387	-.395	-.216
.53	.939	-.012	-.017	-.020	.009	.009	.003	.003	.022	.013	.014	.257	.240
.17	.936	.005	.005	.005	.048	.048	.048	.048	.041	.040	.175	.173	.167
		$P_{t,J}/P_\infty = 4.56$			$P_{t,J}/P_\infty = 5.00$			$P_{t,J}/P_\infty = 4.99$			$P_{t,J}/P_\infty = 5.00$		
12.01	.719	-.013	-.011	-.001	-.010	-.003	.005	-.036	-.006	-.004	-.055	-.050	-.044
10.39	.757	-.025	-.020	-.013	-.019	-.014	-.009	-.007	-.005	-.005	-.008	-.006	-.007
8.76	.795	-.045	-.045	-.042	-.039	-.039	-.034	-.034	-.027	-.027	-.040	-.040	-.040
7.18	.832	-.087	-.087	-.087	-.084	-.084	-.082	-.082	-.063	-.063	-.069	-.069	-.069
5.56	.870	-.071	-.071	-.071	-.069	-.071	-.069	-.069	-.056	-.056	-.063	-.063	-.063
3.95	.908	-.165	-.165	-.165	-.191	-.191	-.189	-.189	-.143	-.143	-.146	-.146	-.146
2.35	.942	-.247	-.247	-.247	-.327	-.333	-.329	-.329	-.272	-.272	-.269	-.269	-.187
1.54	.954	-.205	-.206	-.210	-.287	-.290	-.289	-.289	-.367	-.367	-.190	-.200	-.200
.73	.953	-.100	-.100	-.103	-.091	-.094	-.097	-.097	-.122	-.122	-.385	-.399	-.206
.53	.939	-.025	-.028	-.028	.010	-.013	-.012	-.012	.002	-.007	-.004	-.291	-.227
.17	.936	-.007	-.008	-.008	.010	-.009	.008	.008	.022	-.023	-.020	-.199	-.150
		$P_{t,J}/P_\infty = 7.85$ (max.)			$P_{t,J}/P_\infty = 6.45$ (max.)			$P_{t,J}/P_\infty = 6.97$			$P_{t,J}/P_\infty = 6.95$		
12.01	.719	-.015	-.008	-.000	-.008	-.001	.007	-.036	-.009	-.001	-.056	-.054	-.044
10.39	.757	-.021	-.019	-.017	-.017	-.013	-.005	-.003	-.002	-.002	-.005	-.006	-.007
8.76	.795	-.043	-.043	-.043	-.039	-.038	-.032	-.032	-.024	-.024	-.030	-.030	-.030
7.18	.832	-.087	-.087	-.087	-.084	-.084	-.081	-.081	-.067	-.067	-.071	-.071	-.071
5.56	.870	-.072	-.072	-.072	-.069	-.072	-.069	-.069	-.056	-.056	-.063	-.063	-.063
3.95	.908	-.164	-.164	-.164	-.195	-.195	-.191	-.191	-.143	-.143	-.145	-.145	-.145
2.35	.942	-.248	-.248	-.248	-.329	-.332	-.329	-.329	-.265	-.265	-.264	-.264	-.199
1.54	.954	-.206	-.210	-.220	-.293	-.295	-.293	-.293	-.367	-.367	-.368	-.368	-.269
.73	.953	-.109	-.112	-.115	-.105	-.108	-.105	-.105	-.194	-.194	-.331	-.307	-.226
.53	.939	-.036	-.043	-.043	-.024	-.024	-.024	-.024	-.017	-.017	-.270	-.261	-.245
.17	.936	-.021	-.028	-.028	-.005	-.005	-.005	-.005	.007	-.009	-.238	-.230	-.222
		$P_{t,J}/P_\infty = 8.15$ (max.)											
12.01	.719										-.025	-.023	-.013
10.39	.757										-.063	-.057	-.034
8.76	.795										-.004	-.002	-.017
7.18	.832										-.024	-.024	-.023
5.56	.870										-.044	-.043	-.043
3.95	.908										-.044	-.043	-.043
2.35	.942										-.145	-.145	-.145
1.54	.954										-.126	-.126	-.126
.73	.953										-.203	-.201	-.199
.53	.939										-.329	-.306	-.293
.17	.936										-.278	-.266	-.261
		$P_{t,J}/P_\infty = 8.15$ (max.)									-.245	-.234	-.223

TABLE III.- AFTERSHOCK PRESSURE COEFFICIENTS - Continued

(a) Afterbody XIII - Continued

 $t_j = 800^{\circ} \text{ F}$ 

$\frac{x}{d_1}$	$\frac{x}{l_{\max}}$	Pressure coefficients for -												
		M <sub>a</sub> = 0.80			M <sub>a</sub> = 0.90			M <sub>a</sub> = 1.00			M <sub>a</sub> = 1.10			
		θ = 0°		θ = 45°	θ = 72°	θ = 0°		θ = 45°	θ = 72°	θ = 0°		θ = 45°	θ = 72°	
		$P_{t,j}/P_m = 1.99$			$P_{t,j}/P_m = 1.99$			$P_{t,j}/P_m = 2.01$			$P_{t,j}/P_m = 1.98$			
12.01	.719	-0.011	-0.009	0.000	-0.009	-0.004	0.005	-0.009	-0.009	-0.009	-0.009	-0.010	-0.010	
10.59	.757	-.012	-.016	-.013	-.019	-.013	-.013	-.017	-.014	-.013	-.013	-.013	-.013	-.013
8.76	.795	-.019	-.023	-.019	-.022	-.021	-.018	-.012	-.012	-.012	-.012	-.012	-.012	-.012
7.18	.832	-.037	-.036	-.029	-.039	-.032	-.033	-.065	-.060	-.060	-.060	-.060	-.060	-.060
5.56	.870	-.066	-.068	-.068	-.070	-.072	-.070	-.059	-.059	-.057	-.057	-.057	-.057	-.057
3.95	.908	-.136	-.134	-.138	-.130	-.135	-.139	-.161	-.156	-.154	-.153	-.156	-.156	-.156
2.55	.935	-.154	-.156	-.158	-.150	-.155	-.157	-.171	-.169	-.168	-.168	-.169	-.169	-.169
1.54	.964	-.191	-.191	-.201	-.205	-.200	-.204	-.263	-.263	-.267	-.267	-.267	-.267	-.267
.73	.983	-.079	-.077	-.085	-.088	-.089	-.087	-.080	-.078	-.078	-.078	-.078	-.078	-.078
.50	.993	.008	-.001	-.001	-.015	-.013	-.012	.034	.027	.028	.028	.029	.029	.029
.17	.996	.023	.023	.024	.026	.026	.029	.029	.029	.029	.029	.029	.029	.029
		$P_{t,j}/P_m = 2.99$			$P_{t,j}/P_m = 3.00$			$P_{t,j}/P_m = 3.01$			$P_{t,j}/P_m = 3.00$			
12.01	.739	-.015	-.011	-.001	-.010	-.004	.009	-.006	-.005	-.004	-.005	-.004	-.005	-.005
10.59	.777	-.022	-.018	-.019	-.016	-.011	-.011	-.005	-.001	-.001	-.001	-.001	-.001	-.001
8.76	.815	-.026	-.023	-.023	-.021	-.018	-.018	-.008	-.005	-.005	-.005	-.005	-.005	-.005
7.18	.852	-.042	-.040	-.039	-.040	-.035	-.035	-.063	-.060	-.060	-.060	-.060	-.060	-.060
5.56	.870	-.071	-.074	-.073	-.071	-.071	-.070	-.097	-.097	-.096	-.096	-.096	-.096	-.096
3.95	.908	-.162	-.158	-.163	-.152	-.156	-.150	-.199	-.195	-.194	-.194	-.194	-.194	-.194
2.55	.935	-.189	-.184	-.184	-.180	-.180	-.180	-.207	-.207	-.206	-.206	-.206	-.206	-.206
1.54	.964	-.197	-.199	-.209	-.212	-.212	-.212	-.256	-.256	-.256	-.256	-.256	-.256	-.256
.73	.983	-.087	-.086	-.091	-.093	-.093	-.092	-.085	-.080	-.080	-.080	-.080	-.080	-.080
.50	.993	-.007	-.012	-.012	-.006	-.005	-.005	.028	.019	.019	.019	.019	.019	.019
.17	.996	.014	-.012	-.009	.030	-.003	.029	.045	.045	.045	.045	.045	.045	.045
		$P_{t,j}/P_m = 5.00$			$P_{t,j}/P_m = 5.03$			$P_{t,j}/P_m = 5.02$			$P_{t,j}/P_m = 5.00$			
12.01	.719	-.014	-.010	.000	-.010	-.003	.006	-.006	-.006	-.006	-.006	-.006	-.006	-.006
10.59	.757	-.021	-.019	-.013	-.015	-.015	-.015	-.005	-.005	-.005	-.005	-.005	-.005	-.005
8.76	.795	-.024	-.024	-.024	-.023	-.023	-.023	-.019	-.017	-.017	-.017	-.017	-.017	-.017
7.18	.832	-.040	-.036	-.036	-.040	-.036	-.036	-.063	-.063	-.063	-.063	-.063	-.063	-.063
5.56	.870	-.063	-.068	-.068	-.072	-.074	-.073	-.099	-.099	-.099	-.099	-.099	-.099	-.099
3.95	.908	-.162	-.157	-.160	-.159	-.159	-.159	-.199	-.199	-.199	-.199	-.199	-.199	-.199
2.55	.935	-.194	-.197	-.202	-.202	-.202	-.202	-.246	-.246	-.246	-.246	-.246	-.246	-.246
1.54	.964	-.203	-.204	-.205	-.206	-.206	-.206	-.254	-.254	-.254	-.254	-.254	-.254	-.254
.73	.983	-.097	-.097	-.100	-.087	-.088	-.088	-.098	-.100	-.100	-.100	-.100	-.100	-.100
.50	.993	-.024	-.024	-.028	-.028	-.028	-.028	-.007	.014	.014	.014	.014	.014	.014
.17	.996	-.008	-.006	-.003	.015	-.013	.015	.034	.034	.034	.034	.034	.034	.034
		$P_{t,j}/P_m = 6.99$			$P_{t,j}/P_m = 7.00$			$P_{t,j}/P_m = 7.00$			$P_{t,j}/P_m = 6.91$			
12.01	.719	-.012	-.008	.001	-.010	-.004	.006	-.006	-.006	-.006	-.006	-.006	-.006	-.006
10.59	.757	-.021	-.019	-.013	-.015	-.015	-.015	-.007	-.007	-.007	-.007	-.007	-.007	-.007
8.76	.795	-.024	-.024	-.024	-.023	-.023	-.023	-.019	-.019	-.019	-.019	-.019	-.019	-.019
7.18	.832	-.037	-.036	-.036	-.037	-.037	-.037	-.063	-.063	-.063	-.063	-.063	-.063	-.063
5.56	.870	-.066	-.073	-.073	-.071	-.073	-.073	-.099	-.099	-.099	-.099	-.099	-.099	-.099
3.95	.908	-.161	-.159	-.159	-.151	-.156	-.156	-.199	-.199	-.199	-.199	-.199	-.199	-.199
2.55	.935	-.193	-.193	-.204	-.204	-.204	-.204	-.256	-.256	-.256	-.256	-.256	-.256	-.256
1.54	.964	-.203	-.204	-.205	-.206	-.206	-.206	-.254	-.254	-.254	-.254	-.254	-.254	-.254
.73	.983	-.097	-.097	-.100	-.087	-.088	-.088	-.098	-.100	-.100	-.100	-.100	-.100	-.100
.50	.993	-.024	-.024	-.028	-.028	-.028	-.028	-.007	.014	.014	.014	.014	.014	.014
.17	.996	-.008	-.006	-.003	.015	-.013	.015	.034	.034	.034	.034	.034	.034	.034
		$P_{t,j}/P_m = 9.00$			$P_{t,j}/P_m = 9.02$			$P_{t,j}/P_m = 9.03$			$P_{t,j}/P_m = 9.02$			
12.01	.719	-.013	-.009	.000	-.011	-.006	.004	-.007	-.006	-.005	-.005	-.005	-.005	-.005
10.59	.757	-.022	-.021	-.015	-.022	-.017	-.017	-.010	-.009	-.009	-.009	-.009	-.009	-.009
8.76	.795	-.026	-.026	-.026	-.026	-.026	-.026	-.019	-.019	-.019	-.019	-.019	-.019	-.019
7.18	.832	-.039	-.038	-.038	-.038	-.037	-.037	-.063	-.063	-.063	-.063	-.063	-.063	-.063
5.56	.870	-.069	-.072	-.071	-.070	-.073	-.073	-.099	-.099	-.099	-.099	-.099	-.099	-.099
3.95	.908	-.162	-.157	-.162	-.159	-.167	-.167	-.199	-.199	-.199	-.199	-.199	-.199	-.199
2.55	.935	-.194	-.194	-.207	-.207	-.207	-.207	-.256	-.256	-.256	-.256	-.256	-.256	-.256
1.54	.964	-.211	-.212	-.221	-.221	-.221	-.221	-.266	-.266	-.266	-.266	-.266	-.266	-.266
.73	.983	-.116	-.117	-.122	-.111	-.109	-.113	-.188	-.188	-.188	-.188	-.188	-.188	-.188
.50	.993	-.052	-.056	-.051	-.056	-.053	-.056	-.038	-.038	-.038	-.038	-.038	-.038	-.038
.17	.996	-.039	-.041	-.040	-.040	-.019	-.019	-.017	-.004	-.004	-.004	-.004	-.004	-.004
		$P_{t,j}/P_m = 11.05$			$P_{t,j}/P_m = 11.01$			$P_{t,j}/P_m = 11.05$			$P_{t,j}/P_m = 11.01$			
12.01	.719							-.058	-.059	-.059	-.059	-.059	-.059	-.059
10.59	.757							-.065	-.065	-.065	-.065	-.065	-.065	-.065
8.76	.795							-.069	-.069	-.069	-.069	-.069	-.069	-.069
7.18	.832							-.069	-.069	-.069	-.069	-.069	-.069	-.069
5.56	.870							-.069	-.069	-.069	-.069	-.069	-.069	-.069
3.95	.908							-.069	-.069	-.069	-.069	-.069	-.069	-.069
2.55	.935							-.069	-.069	-.069	-.069	-.069	-.069	-.069
1.54	.964							-.069	-.069	-.069	-.069	-.069	-.069	-.069
.73	.983							-.069	-.069	-.069	-.069	-.069	-.069	-.069
.50	.993							-.069	-.069	-.069	-.069	-.069	-.069	-.069
.17	.996							-.069	-.069	-.069	-.069	-.069	-.069	-.069

CONFIDENTIAL

TABLE III.- AFTERBODY PRESSURE COEFFICIENTS - Continued

(a) Afterbody XIII - Concluded

 $t_j = 1,200^{\circ} F$ 

$\frac{x}{d}$	$x_{max}$	Pressure coefficients for -											
		$M_\infty = 0.80$			$M_\infty = 0.90$			$M_\infty = 1.00$			$M_\infty = 1.10$		
		$s = 0^\circ$	$s = 45^\circ$	$s = 72^\circ$	$s = 0^\circ$	$s = 45^\circ$	$s = 72^\circ$	$s = 0^\circ$	$s = 45^\circ$	$s = 72^\circ$	$s = 0^\circ$	$s = 45^\circ$	$s = 72^\circ$
$P_{t,j}/P_\infty = 2.00$				$P_{t,j}/P_\infty = 2.00$				$P_{t,j}/P_\infty = 1.90$				$P_{t,j}/P_\infty = 2.00$	
12.01	.719	-0.013	-0.011	0.000	-0.007	-0.005	0.008	-0.038	-0.033	-0.033	-0.049	-0.045	-0.040
10.39	.737	-0.020	-0.018	-0.015	-0.017	-0.015	-0.009	-0.051	-0.053	-0.079	-0.051	-0.054	-0.052
8.76	.795	-0.026	-0.025	-0.023	-0.020	-0.021	-0.016	-0.074	-0.071	-0.066	-0.063	-0.059	-0.052
7.18	.832	-0.041	-0.037	-0.037	-0.036	-0.036	-0.033	-0.064	-0.060	-0.060	-0.054	-0.053	-0.052
5.56	.870	-0.059	-0.069	-0.069	-0.067	-0.071	-0.070	-0.088	-0.099	-0.096	-0.093	-0.091	-0.089
3.95	.908	-0.102	-0.106	-0.106	-0.100	-0.102	-0.105	-0.160	-0.160	-0.168	-0.183	-0.193	-0.176
2.35	.942	-0.238	-0.239	-0.238	-0.214	-0.221	-0.219	-0.268	-0.268	-0.260	-0.199	-0.195	-0.189
1.34	.964	-0.191	-0.191	-0.199	-0.220	-0.224	-0.233	-0.277	-0.253	-0.264	-0.180	-0.183	-0.161
.73	.985	-0.073	-0.074	-0.076	-0.066	-0.062	-0.068	-0.044	-0.042	-0.060	-0.115	-0.104	-0.092
.30	.995	.008	.008	.004	.022	.020	.019	.041	.034	.034	.194	.182	.165
.17	.996	.038	.038	.027	.045	.043	.043	.057	.055	.057	.130	.126	.126
$P_{t,j}/P_\infty = 2.98$				$P_{t,j}/P_\infty = 3.00$				$P_{t,j}/P_\infty = 5.01$				$P_{t,j}/P_\infty = 5.00$	
12.01	.719	-0.017	-0.012	-0.003	-0.008	-0.009	.008	-0.097	-0.093	-0.093	-0.053	-0.047	-0.040
10.39	.737	-0.024	-0.022	-0.017	-0.017	-0.015	-0.010	-0.068	-0.068	-0.078	-0.060	-0.054	-0.052
8.76	.795	-0.029	-0.027	-0.024	-0.020	-0.023	-0.015	-0.071	-0.069	-0.061	-0.060	-0.057	-0.054
7.18	.832	-0.044	-0.039	-0.041	-0.038	-0.033	-0.042	-0.064	-0.059	-0.079	-0.065	-0.062	-0.059
5.56	.870	-0.071	-0.073	-0.071	-0.069	-0.070	-0.069	-0.088	-0.089	-0.097	-0.092	-0.092	-0.088
3.95	.908	-0.163	-0.158	-0.160	-0.159	-0.158	-0.168	-0.170	-0.164	-0.171	-0.144	-0.144	-0.140
2.35	.942	-0.240	-0.245	-0.245	-0.238	-0.238	-0.231	-0.265	-0.265	-0.260	-0.199	-0.199	-0.170
1.34	.964	-0.199	-0.199	-0.209	-0.228	-0.232	-0.240	-0.260	-0.264	-0.264	-0.211	-0.211	-0.190
.73	.985	-0.065	-0.065	-0.090	-0.069	-0.071	-0.077	-0.062	-0.070	-0.078	-0.111	-0.108	-0.090
.30	.995	-0.008	-0.008	-0.010	-0.015	-0.020	-0.011	.011	.013	.026	.036	.036	.024
.17	.996	.034	.034	.012	.037	.036	.036	.091	.048	.049	.116	.114	.116
$P_{t,j}/P_\infty = 4.99$				$P_{t,j}/P_\infty = 5.01$				$P_{t,j}/P_\infty = 5.01$				$P_{t,j}/P_\infty = 5.04$	
12.01	.719	-0.015	-0.011	-0.001	-0.007	-0.001	.008	-0.095	-0.094	-0.094	-0.049	-0.047	-0.039
10.39	.737	-0.023	-0.020	-0.017	-0.017	-0.012	-0.007	-0.068	-0.068	-0.066	-0.060	-0.054	-0.050
8.76	.795	-0.027	-0.025	-0.020	-0.020	-0.019	-0.012	-0.072	-0.070	-0.067	-0.062	-0.056	-0.052
7.18	.832	-0.040	-0.037	-0.040	-0.036	-0.035	-0.032	-0.065	-0.064	-0.061	-0.054	-0.053	-0.050
5.56	.870	-0.069	-0.071	-0.071	-0.069	-0.070	-0.069	-0.099	-0.099	-0.097	-0.094	-0.093	-0.089
3.95	.908	-0.163	-0.158	-0.158	-0.159	-0.158	-0.166	-0.169	-0.169	-0.175	-0.146	-0.146	-0.143
2.35	.942	-0.241	-0.245	-0.244	-0.239	-0.239	-0.232	-0.266	-0.266	-0.262	-0.197	-0.197	-0.177
1.34	.964	-0.199	-0.199	-0.209	-0.228	-0.232	-0.240	-0.260	-0.264	-0.264	-0.222	-0.222	-0.200
.73	.985	-0.077	-0.076	-0.098	-0.060	-0.060	-0.066	-0.098	-0.101	-0.112	.105	.105	.097
.30	.995	-0.022	-0.022	-0.022	.003	.001	.001	.017	.011	.011	.022	.022	.020
.17	.996	.004	.001	.003	.023	.021	.021	.036	.034	.034	.173	.169	.164
$P_{t,j}/P_\infty = 6.99$				$P_{t,j}/P_\infty = 7.01$				$P_{t,j}/P_\infty = 7.00$				$P_{t,j}/P_\infty = 7.02$	
12.01	.719	-0.010	-0.006	.005	-0.007	-0.001	.008	-1.100	-0.034	-0.066	-0.058	-0.050	-0.041
10.39	.737	-0.018	-0.016	-0.011	-0.016	-0.012	-0.007	-0.088	-0.085	-0.082	-0.069	-0.064	-0.052
8.76	.795	-0.022	-0.021	-0.020	-0.020	-0.018	-0.013	-0.072	-0.070	-0.067	-0.063	-0.061	-0.057
7.18	.832	-0.039	-0.034	-0.037	-0.036	-0.035	-0.032	-0.063	-0.062	-0.065	-0.060	-0.056	-0.053
5.56	.870	-0.068	-0.071	-0.071	-0.069	-0.069	-0.068	-0.098	-0.098	-0.097	-0.096	-0.095	-0.093
3.95	.908	-0.163	-0.162	-0.162	-0.159	-0.158	-0.165	-0.168	-0.168	-0.176	-0.146	-0.146	-0.143
2.35	.942	-0.242	-0.245	-0.244	-0.239	-0.239	-0.232	-0.266	-0.266	-0.262	-0.198	-0.198	-0.178
1.34	.964	-0.199	-0.199	-0.209	-0.228	-0.232	-0.240	-0.260	-0.264	-0.264	-0.222	-0.222	-0.200
.73	.985	-0.077	-0.076	-0.098	-0.060	-0.060	-0.066	-0.098	-0.101	-0.112	.105	.105	.097
.30	.995	-0.022	-0.022	-0.022	.003	.001	.001	.017	.011	.011	.022	.022	.020
.17	.996	.004	.001	.003	.023	.021	.021	.036	.034	.034	.173	.169	.164
$P_{t,j}/P_\infty = 9.00$				$P_{t,j}/P_\infty = 9.03$				$P_{t,j}/P_\infty = 9.03$				$P_{t,j}/P_\infty = 9.04$	
12.01	.719	-0.015	-0.007	-0.001	-0.007	-0.000	.009	-0.098	-0.094	-0.095	-0.098	-0.091	-0.081
10.39	.737	-0.024	-0.021	-0.018	-0.018	-0.018	-0.014	-0.071	-0.070	-0.067	-0.063	-0.061	-0.053
8.76	.795	-0.026	-0.025	-0.021	-0.021	-0.021	-0.019	-0.063	-0.062	-0.060	-0.056	-0.054	-0.052
7.18	.832	-0.036	-0.037	-0.037	-0.039	-0.031	-0.030	-0.063	-0.062	-0.060	-0.057	-0.055	-0.053
5.56	.870	-0.068	-0.071	-0.070	-0.068	-0.069	-0.068	-0.098	-0.099	-0.097	-0.096	-0.094	-0.091
3.95	.908	-0.163	-0.162	-0.162	-0.159	-0.158	-0.165	-0.168	-0.168	-0.176	-0.146	-0.146	-0.143
2.35	.942	-0.241	-0.245	-0.244	-0.239	-0.239	-0.232	-0.266	-0.266	-0.262	-0.198	-0.198	-0.178
1.34	.964	-0.199	-0.199	-0.209	-0.228	-0.232	-0.240	-0.260	-0.264	-0.264	-0.222	-0.222	-0.200
.73	.985	-0.077	-0.076	-0.098	-0.060	-0.060	-0.066	-0.098	-0.101	-0.112	.105	.105	.097
.30	.995	-0.022	-0.022	-0.022	.003	.001	.001	.017	.011	.011	.022	.022	.020
.17	.996	.004	.001	.003	.023	.021	.021	.036	.034	.034	.173	.169	.164
								$P_{t,j}/P_\infty = 11.02$				$P_{t,j}/P_\infty = 11.05$	
12.01	.719							-0.099	-0.091	-0.093	-0.090	-0.088	-0.089
10.39	.737							-0.084	-0.081	-0.078	-0.061	-0.054	-0.051
8.76	.795							-0.087	-0.086	-0.082	-0.061	-0.050	-0.049
7.18	.832							-0.063	-0.061	-0.057	-0.057	-0.054	-0.052
5.56	.870							-0.051	-0.051	-0.051	-0.052	-0.053	-0.052
3.95	.908							-0.051	-0.051	-0.051	-0.052	-0.053	-0.052
2.35	.942							-0.051	-0.051	-0.051	-0.052	-0.053	-0.052
1.34	.964							-0.051	-0.051	-0.051	-0.052	-0.053	-0.052
.73	.985							-0.051	-0.051	-0.051	-0.052	-0.053	-0.052
.30	.995							-0.051	-0.051	-0.051	-0.052	-0.053	-0.052
.17	.996							-0.051	-0.051	-0.051	-0.052	-0.053	-0.052

TABLE III.-- AFTERBODY PRESSURE COEFFICIENTS - Continued

(c) Afterbody XIV

 $t_d = \text{Cald}$ 

$\frac{x}{d_1}$	$\frac{x}{l_{max}}$	Pressure coefficients for -												
		M <sub>∞</sub> = 0.80			M <sub>∞</sub> = 0.90			M <sub>∞</sub> = 1.00			M <sub>∞</sub> = 1.10			
		$\theta = 0^\circ$	$\theta = 45^\circ$	$\theta = 72^\circ$	$\theta = 0^\circ$	$\theta = 45^\circ$	$\theta = 72^\circ$	$\theta = 0^\circ$	$\theta = 45^\circ$	$\theta = 72^\circ$	$\theta = 0^\circ$	$\theta = 45^\circ$	$\theta = 72^\circ$	
		$P_{t,J}/P_m = 0.94$			$P_{t,J}/P_m = 0.92$			$P_{t,J}/P_m = 0.90$			$P_{t,J}/P_m = 0.84$			
7.93	.722	-0.015	-0.003	0.017	-0.012	0.005	0.023	-0.153	-0.127	-0.098	-0.083	-0.098	-0.027	
7.56	.742	-0.005	.000	—	.002	.008	—	-0.104	-0.096	—	-.092	-0.042	—	
6.79	.762	-0.014	-0.005	0.000	-0.008	-0.001	.005	-0.102	-0.095	-0.069	-0.077	-0.052	-0.044	
5.65	.802	-0.014	-0.011	-0.008	-0.008	-0.005	-0.001	-0.051	-0.051	-0.077	-0.061	-0.055	-0.033	
4.31	.842	-0.016	-0.012	-0.010	-0.011	-0.007	-0.009	-0.070	-0.065	-0.079	-0.064	-0.059	-0.035	
3.37	.882	-0.016	-0.012	-0.010	-0.017	-0.007	-0.003	-0.066	-0.066	-0.076	-0.064	-0.064	-0.037	
2.22	.922	-0.016	-0.012	-0.010	-0.017	-0.007	-0.003	-0.066	-0.066	-0.076	-0.064	-0.064	-0.037	
1.65	.962	-0.015	-0.010	-0.008	-0.017	-0.007	-0.003	-0.066	-0.066	-0.076	-0.064	-0.064	-0.037	
.51	.982	-0.018	-0.009	-0.007	-0.017	-0.009	-0.003	-0.066	-0.066	-0.076	-0.064	-0.064	-0.037	
.23	.992	-0.018	-0.008	-0.007	-0.017	-0.009	-0.003	-0.066	-0.066	-0.076	-0.064	-0.064	-0.037	
.11	.996	-0.109	-0.112	-0.109	-0.117	-0.118	-0.115	-0.061	-0.062	-0.076	-0.074	-0.065	-0.068	
		$P_{t,J}/P_m = 1.96$			$P_{t,J}/P_m = 1.97$			$P_{t,J}/P_m = 1.96$			$P_{t,J}/P_m = 1.96$			
7.93	.722	-0.019	-0.009	0.013	-0.014	0.002	0.025	-0.152	-0.129	-0.099	-0.083	-0.095	-0.025	
7.56	.742	-0.007	.000	—	.000	.008	—	-0.106	-0.098	—	-.091	-0.041	—	
6.79	.762	-0.013	-0.008	0.000	-0.008	-0.001	.007	-0.101	-0.093	-0.068	-0.055	-0.051	-0.043	
5.65	.802	-0.013	-0.011	-0.008	-0.009	-0.005	-0.003	-0.082	-0.079	-0.077	-0.062	-0.055	-0.031	
4.31	.842	-0.017	-0.013	-0.010	-0.012	-0.008	-0.011	-0.070	-0.064	-0.069	-0.062	-0.056	-0.031	
3.37	.882	-0.022	-0.013	-0.008	-0.018	-0.019	-0.019	-0.044	-0.045	-0.042	-0.030	-0.021	-0.028	
2.22	.922	-0.022	-0.013	-0.008	-0.018	-0.019	-0.019	-0.044	-0.045	-0.042	-0.030	-0.021	-0.028	
1.65	.962	-0.022	-0.013	-0.008	-0.018	-0.019	-0.019	-0.044	-0.045	-0.042	-0.030	-0.021	-0.028	
.51	.982	-0.022	-0.013	-0.008	-0.018	-0.019	-0.019	-0.044	-0.045	-0.042	-0.030	-0.021	-0.028	
.23	.992	-0.155	-0.131	-0.131	-0.131	-0.129	-0.128	-0.050	-0.050	-0.058	-0.052	-0.041	-0.009	.001
.11	.996	-0.169	-0.169	-0.166	-0.171	-0.173	-0.168	-0.115	-0.113	-0.104	-0.052	-0.062	-0.048	
		$P_{t,J}/P_m = 2.72$ (max.)			$P_{t,J}/P_m = 2.99$			$P_{t,J}/P_m = 2.98$						
7.93	.722	-0.020	-0.006	0.014	-0.015	0.000	0.023	-0.154	-0.130	-0.100				
7.56	.742	-0.007	.001	—	.002	.006	—	-0.107	-0.099	—	-.091	-0.041	—	
6.79	.762	-0.013	-0.009	-0.001	-0.010	-0.003	.005	-0.103	-0.096	—	-.090	-0.051	—	
5.65	.802	-0.016	-0.011	-0.009	-0.011	-0.007	-0.004	-0.083	-0.081	-0.079	-0.070			
4.31	.842	-0.018	-0.014	-0.017	-0.014	-0.010	-0.012	-0.071	-0.069	-0.070				
3.37	.882	-0.023	-0.018	-0.013	-0.020	-0.021	-0.020	-0.044	-0.045	-0.041				
2.22	.922	-0.023	-0.018	-0.013	-0.020	-0.021	-0.020	-0.044	-0.045	-0.042				
1.65	.962	-0.023	-0.018	-0.013	-0.020	-0.021	-0.020	-0.044	-0.045	-0.042				
.51	.982	-0.024	-0.018	-0.017	-0.020	-0.021	-0.020	-0.044	-0.045	-0.042				
.23	.992	-0.104	-0.103	-0.102	-0.103	-0.098	-0.095	-0.048	-0.047	-0.042				
.11	.996	-0.142	-0.140	-0.140	-0.144	-0.141	-0.140	-0.056	-0.054	-0.057				
		$P_{t,J}/P_m = 3.79$ (max.)												
7.93	.722										-0.09	-0.095	-0.025	
7.56	.742										-.091	-0.082	—	
6.79	.762										-.093	-0.091	-0.043	
5.65	.802										-.099	-0.093	-0.028	
4.31	.842										-.061	-0.077	-0.061	
3.37	.882										-.049	-0.051	-0.031	
2.22	.922										-.032	-0.048	-0.048	
1.65	.962										-.041	-0.047	-0.034	
.51	.982										-.047	-0.059	-0.038	
.23	.992										-.013	-0.017	-0.018	
.11	.996										-.048	-0.052	-0.049	

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TABLE III.- AFTERBODY PRESSURE COEFFICIENTS - Continued

(e) Afterbody XIV - Continued

 $t_j = 800^{\circ} F$ 

$\frac{x}{d}$	$\frac{x}{l_{max}}$	Pressure coefficients for -											
		$K_m = 0.80$			$K_m = 0.90$			$K_m = 1.00$			$K_m = 1.10$		
		$\theta = 0^{\circ}$	$\theta = 45^{\circ}$	$\theta = 72^{\circ}$	$\theta = 0^{\circ}$	$\theta = 45^{\circ}$	$\theta = 72^{\circ}$	$\theta = 0^{\circ}$	$\theta = 45^{\circ}$	$\theta = 72^{\circ}$	$\theta = 0^{\circ}$	$\theta = 45^{\circ}$	$\theta = 72^{\circ}$
		$P_{t,j}/P_m = 1.99$			$P_{t,j}/P_m = 2.05$			$P_{t,j}/P_m = 2.53$					
7.93	.722	-0.019	-0.005	0.015	-0.018	0.005	0.026	-0.128	-0.132	-0.101			
7.36	.742	-0.007			-0.003	-0.003		-0.108	-0.100				
6.79	.762	-0.013	-0.008	-0.001	-0.008	-0.003	.007	-0.105	-0.096	-0.089			
5.65	.802	-0.013	-0.011	-0.008	-0.009	-0.005	.000	-0.093	-0.081	-0.078			
4.51	.842	-0.016	-0.018	-0.013	-0.011	-0.007	-0.010	-0.070	-0.065	-0.069			
3.37	.882	-0.022	-0.022	-0.021	-0.017	-0.017	-0.016	-0.044	-0.043	-0.040			
2.22	.922	-0.026	-0.023	-0.024	-0.024	-0.020	-0.020	-0.009	-0.012	-0.012			
1.08	.942	-0.045	-0.036	-0.029	-0.037	-0.031	-0.030	-0.021	-0.026	-0.027			
.51	.962	-0.059	-0.048	-0.038	-0.051	-0.045	-0.045	-0.016	-0.016	-0.011			
.25	.992	-0.100	-0.081	-0.068	-0.087	-0.075	-0.075	-0.017	-0.016	-0.011			
.11	.996	-0.152	-0.135	-0.129	-0.159	-0.139	-0.134	-0.112	-0.112	-0.102			
		$P_{t,j}/P_m = 2.98$			$P_{t,j}/P_m = 2.99$			$P_{t,j}/P_m = 2.87$			$P_{t,j}/P_m = 2.99$		
7.93	.722	-0.023	-0.010	.011	-0.015	.005	.003	-0.155	-0.150	-0.100	-0.068	-0.055	-0.025
7.36	.742	-0.011			-0.001	-0.008		-0.107	-0.099		-0.050	-0.041	
6.79	.762	-0.017	-0.010	-0.001	-0.009	-0.002	.007	-0.104	-0.096		-0.053	-0.049	-0.043
5.65	.802	-0.017	-0.014	-0.009	-0.010	-0.007	-0.002	-0.083	-0.082	-0.077	-0.038	-0.032	-0.030
4.51	.842	-0.016	-0.013	-0.013	-0.012	-0.009	-0.011	-0.071	-0.066	-0.070	-0.031	-0.026	-0.025
3.37	.882	-0.020	-0.021	-0.019	-0.019	-0.019	-0.018	-0.056	-0.055	-0.053	-0.021	-0.022	-0.023
2.22	.922	-0.026	-0.022	-0.020	-0.024	-0.020	-0.021	-0.011	-0.012	-0.012	-0.002	-0.002	-0.002
1.08	.942	-0.056	-0.044	-0.034	-0.059	-0.048	-0.048	-0.021	-0.021	-0.019	-0.004	-0.003	-0.003
.51	.962	-0.089	-0.077	-0.064	-0.094	-0.083	-0.083	-0.018	-0.018	-0.013	-0.003	-0.003	-0.003
.25	.992	-0.121	-0.119	-0.118	-0.134	-0.131	-0.139	-0.029	-0.027	-0.023	-0.011	-0.011	-0.011
.11	.996	-0.153	-0.135	-0.131	-0.174	-0.173	-0.170	-0.111	-0.112	-0.104	-0.083	-0.076	-0.076
		$P_{t,j}/P_m = 4.00$						$P_{t,j}/P_m = 3.98$					
7.93	.722				-0.013	.003	.005				-0.081	-0.053	-0.085
7.36	.742				-0.001	-0.008					-0.048	-0.039	
6.79	.762				-0.009	-0.001	.006				-0.053	-0.048	-0.061
5.65	.802				-0.008	-0.007		-0.001			-0.027	-0.022	-0.048
4.51	.842				-0.018	-0.009	-0.011				-0.019	-0.022	-0.050
3.37	.882				-0.018	-0.008	-0.018				-0.019	-0.021	-0.050
2.22	.922				-0.024	-0.014	-0.024				-0.019	-0.027	-0.047
1.08	.942				-0.040	-0.025	-0.034				-0.042	-0.037	-0.033
.51	.962				-0.067	-0.044	-0.061				-0.049	-0.044	-0.039
.25	.992				-0.099	-0.068	-0.095				-0.053	-0.061	-0.000
.11	.996				-0.127	-0.105	-0.125				-0.093	-0.093	-0.057
		$P_{t,j}/P_m = 4.57$ (max.)			$P_{t,j}/P_m = 5.01$			$P_{t,j}/P_m = 4.99$			$P_{t,j}/P_m = 4.97$		
7.93	.722	-0.021	-0.007	.013	-0.013	.003	.003	-0.152	-0.149	-0.100	-0.083	-0.073	-0.040
7.36	.742	-0.008	-0.002		-0.001	-0.007		-0.107	-0.099		-0.049	-0.040	
6.79	.762	-0.015	-0.008	.000	-0.010	-0.002	.006	-0.104	-0.095		-0.053	-0.049	-0.043
5.65	.802	-0.015	-0.013	-0.007	-0.010	-0.007	-0.002	-0.085	-0.082	-0.077	-0.052	-0.049	
4.51	.842	-0.016	-0.011	-0.016	-0.015	-0.010	-0.012	-0.070	-0.065	-0.069	-0.060	-0.056	-0.052
3.37	.882	-0.021	-0.021	-0.020	-0.021	-0.018	-0.020	-0.049	-0.047	-0.046	-0.032	-0.032	-0.032
2.22	.922	-0.025	-0.022	-0.020	-0.027	-0.022	-0.024	-0.016	-0.013	-0.010	-0.008	-0.008	-0.008
1.08	.942	-0.040	-0.037	-0.029	-0.042	-0.037	-0.036	-0.023	-0.027	-0.022	-0.015	-0.017	-0.015
.51	.962	-0.066	-0.054	-0.061	-0.070	-0.067	-0.064	-0.023	-0.022	-0.015	-0.010	-0.012	-0.010
.25	.992	-0.100	-0.092	-0.098	-0.102	-0.104	-0.101	-0.016	-0.015	-0.013	-0.012	-0.012	-0.009
.11	.996	-0.133	-0.114	-0.104	-0.155	-0.152	-0.149	-0.070	-0.067	-0.060	-0.071	-0.072	-0.018
		$P_{t,j}/P_m = 5.81$ (max.)			$P_{t,j}/P_m = 6.75$ (max.)								
7.93	.722							-0.155	-0.130	-0.100	-0.083	-0.073	-0.043
7.36	.742							-0.107	-0.093		-0.049	-0.042	
6.79	.762							-0.104	-0.093	-0.088	-0.050	-0.043	
5.65	.802							-0.083	-0.082	-0.078	-0.056	-0.051	-0.049
4.51	.842							-0.070	-0.065	-0.068	-0.050	-0.044	-0.039
3.37	.882							-0.064	-0.063	-0.068	-0.046	-0.042	-0.040
2.22	.922							-0.043	-0.043	-0.041	-0.048	-0.046	-0.048
1.08	.942							-0.024	-0.027	-0.023	-0.031	-0.029	-0.029
.51	.962							-0.007	-0.011	-0.014	-0.017	-0.010	-0.016
.25	.992							-0.020	-0.019	-0.014	-0.021	-0.011	-0.009
.11	.996							-0.074	-0.071	-0.064	-0.058	-0.039	-0.003

TABLE III.-- AFTERBODY PRESSURE COEFFICIENTS - Concluded

(c) Afterbody XIV - Concluded

$t_j = 1,200^{\circ} F$

$\frac{x}{L_{max}}$	$\frac{x}{L_{max}}$	Pressure coefficients for -											
		$M_\infty = 0.80$			$M_\infty = 0.90$			$M_\infty = 1.00$			$M_\infty = 1.10$		
		$\theta = 0^\circ$	$\theta = 45^\circ$	$\theta = 72^\circ$	$\theta = 0^\circ$	$\theta = 45^\circ$	$\theta = 72^\circ$	$\theta = 0^\circ$	$\theta = 45^\circ$	$\theta = 72^\circ$	$\theta = 0^\circ$	$\theta = 45^\circ$	$\theta = 72^\circ$
		$P_{t,j}/P_m = 2.22$ (min.)			$P_{t,j}/P_m = 2.76$ (min.)			$P_{t,j}/P_m = 2.87$ (min.)					
7.93	.722	-.018	-.002	.018	-.013	.005	.026	-.158	-.129	-.099			
7.36	.742	-.003	.005	---	-.005	.009	---	-.105	-.098	-.087			
6.79	.762	-.012	-.006	.008	-.007	.001	.009	-.105	-.094	-.087			
5.93	.802	-.013	-.011	-.018	-.012	-.004	-.004	-.062	-.055	-.048			
5.37	.822	-.019	-.018	-.018	-.019	-.018	-.014	-.050	-.049	-.046			
4.31	.842	-.013	-.011	-.018	-.012	-.004	-.004	-.040	-.038	-.033			
2.22	.862	-.019	-.018	-.018	-.019	-.018	-.014	-.030	-.028	-.026			
1.65	.882	-.015	-.014	-.014	-.016	-.015	-.014	-.022	-.021	-.019			
1.08	.902	-.017	-.016	-.016	-.018	-.016	-.014	-.017	-.016	-.015			
.51	.922	-.006	-.005	-.005	-.005	-.005	-.005	-.013	-.012	-.010			
.23	.932	-.117	-.114	-.114	-.125	-.119	-.118	-.057	-.054	-.049			
.11	.936	-.147	-.148	-.143	-.159	-.158	-.152	-.107	-.108	-.099			
		$P_{t,j}/P_m = 2.98$			$P_{t,j}/P_m = 3.00$			$P_{t,j}/P_m = 2.99$			$P_{t,j}/P_m = 2.97$ (min.)		
7.93	.722	-.018	-.004	.015	-.012	.005	.026	-.159	-.134	-.103	-.081	-.093	-.082
7.36	.742	-.006	.001	---	-.005	.009	---	-.109	-.101	-.090	-.065	-.070	-.061
6.79	.762	-.014	-.006	.005	-.008	.001	.011	-.082	-.089	-.081	-.067	-.071	-.068
5.93	.802	-.012	-.010	-.007	-.008	-.005	.009	-.063	-.064	-.060	-.058	-.063	-.058
5.37	.822	-.012	-.008	-.005	-.010	-.003	-.004	-.046	-.045	-.041	-.039	-.045	-.040
4.31	.842	-.013	-.011	-.014	-.015	-.012	-.014	-.038	-.037	-.034	-.032	-.038	-.034
2.22	.862	-.019	-.018	-.018	-.019	-.018	-.014	-.030	-.029	-.027	-.025	-.030	-.027
1.65	.882	-.015	-.014	-.014	-.016	-.015	-.014	-.022	-.021	-.019	-.017	-.023	-.019
1.08	.902	-.017	-.016	-.016	-.018	-.016	-.014	-.017	-.016	-.015	-.013	-.017	-.014
.51	.922	-.008	-.007	-.006	-.006	-.006	-.006	-.019	-.018	-.016	-.017	-.020	-.018
.23	.932	-.114	-.113	-.113	-.123	-.118	-.118	-.065	-.060	-.053	-.067	-.073	-.068
.11	.936	-.146	-.148	-.145	-.163	-.155	-.159	-.118	-.113	-.103	-.087	-.093	-.084
		$P_{t,j}/P_m = 3.98$											
7.93	.722												
7.36	.742												
6.79	.762												
5.93	.802												
5.37	.822												
4.31	.842												
2.22	.862												
1.65	.882												
1.08	.902												
.51	.922												
.23	.932												
.11	.936												
		$P_{t,j}/P_m = 5.01$			$P_{t,j}/P_m = 5.07$			$P_{t,j}/P_m = 4.99$			$P_{t,j}/P_m = 4.97$		
7.93	.722	-.017	-.003	.017	-.010	.005	.028	-.153	-.129	-.100	-.082	-.092	-.084
7.36	.742	-.006	.002	---	-.005	.005	.011	-.105	-.103	-.087	-.063	-.070	-.063
6.79	.762	-.012	-.005	.004	-.005	.003	.004	-.076	-.074	-.061	-.053	-.060	-.056
5.93	.802	-.012	-.007	-.003	-.009	-.003	-.007	-.054	-.052	-.045	-.040	-.049	-.045
5.37	.822	-.017	-.015	-.015	-.016	-.012	-.013	-.042	-.041	-.038	-.037	-.047	-.041
4.31	.842	-.010	-.008	-.008	-.010	-.006	-.008	-.034	-.032	-.031	-.031	-.036	-.034
2.22	.862	-.010	-.008	-.008	-.010	-.006	-.008	-.026	-.024	-.023	-.023	-.026	-.024
1.65	.882	-.017	-.014	-.014	-.016	-.012	-.014	-.034	-.032	-.031	-.031	-.037	-.034
1.08	.902	-.017	-.014	-.014	-.016	-.012	-.014	-.034	-.032	-.031	-.031	-.036	-.033
.51	.922	-.007	-.006	-.006	-.006	-.006	-.006	-.016	-.015	-.014	-.014	-.017	-.014
.23	.932	-.159	-.157	-.158	-.170	-.162	-.165	-.058	-.059	-.059	-.065	-.070	-.068
.11	.936	-.180	-.182	-.179	-.197	-.186	-.199	-.129	-.130	-.118	-.120	-.127	-.120
		$P_{t,j}/P_m = 5.73$ (max.)			$P_{t,j}/P_m = 6.31$ (max.)			$P_{t,j}/P_m = 6.99$			$P_{t,j}/P_m = 6.99$		
7.93	.722	-.019	-.005	.024	-.012	.002	.023	-.153	-.130	-.101	-.063	-.075	-.065
7.36	.742	-.007	-.001	---	-.000	.009	---	-.106	-.099	-.067	-.050	-.062	-.053
6.79	.762	-.014	-.007	.002	-.007	.001	.009	-.103	-.098	-.064	-.052	-.060	-.053
5.93	.802	-.013	-.011	-.013	-.008	-.003	-.009	-.061	-.061	-.051	-.051	-.061	-.051
5.37	.822	-.019	-.018	-.017	-.007	-.004	-.007	-.051	-.050	-.046	-.046	-.051	-.049
4.31	.842	-.013	-.011	-.013	-.008	-.003	-.008	-.042	-.041	-.038	-.038	-.041	-.039
2.22	.862	-.014	-.009	-.007	-.008	-.003	-.006	-.035	-.034	-.032	-.032	-.036	-.034
1.65	.882	-.017	-.014	-.014	-.016	-.012	-.014	-.034	-.032	-.031	-.031	-.037	-.034
1.08	.902	-.017	-.014	-.014	-.016	-.012	-.014	-.034	-.032	-.031	-.031	-.036	-.033
.51	.922	-.007	-.006	-.006	-.006	-.006	-.006	-.016	-.015	-.014	-.014	-.017	-.014
.23	.932	-.155	-.155	-.151	-.152	-.149	-.145	-.077	-.073	-.065	-.071	-.077	-.069
.11	.936	-.198	-.200	-.197	-.207	-.206	-.199	-.147	-.147	-.132	-.151	-.177	-.159

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TABLE IV.- FOREBODY PRESSURE COEFFICIENTS

[No jet flow]

$\frac{y}{d_3}$	$\frac{y}{l_{max}}$	Pressure coefficients for -											
		M <sub>∞</sub> = 0.80			M <sub>∞</sub> = 0.90			M <sub>∞</sub> = 1.00			M <sub>∞</sub> = 1.10		
		$\theta = 0^\circ$	$\theta = 45^\circ$	$\theta = 72^\circ$	$\theta = 0^\circ$	$\theta = 45^\circ$	$\theta = 72^\circ$	$\theta = 0^\circ$	$\theta = 45^\circ$	$\theta = 72^\circ$	$\theta = 0^\circ$	$\theta = 45^\circ$	$\theta = 72^\circ$
Afterbody 1													
40.96	0.042	0.120	0.119	0.117	0.137	0.136	0.131	0.170	0.166	0.165	0.180	0.177	0.183
38.56	.058	.065	.064	.064	.072	.072	.072	.096	.095	.095	.115	.124	.118
36.16	.122	.103	.098	.098	.095	.095	.095	.094	.093	.093	.085	.085	.099
33.76	.211	.093	.088	.088	.086	.086	.086	.080	.080	.080	.074	.074	.080
31.36	.268	.086	.083	.083	.083	.083	.083	.073	.073	.073	.073	.073	.073
28.96	.324	.088	.088	.085	.084	.084	.084	.086	.086	.086	.082	.082	.088
26.56	.381	.082	.083	.087	.085	.085	.085	.078	.078	.078	.109	.101	.068
24.16	.438	.006	.014	.021	.023	.023	.023	.012	.012	.012	.097	.128	.119
21.76	.494	.059	.117	.159	.079	.105	.137	.095	.109	.109	.083	.084	.087
20.36	.552	.157	.188	.239	.163	.215	.269	.075	.126	.126	.178	.006	.060
18.96	.570	.122	.161	.199	.106	.260	.333	.114	.201	.201	.288	.014	.073
16.56	.606	.090	.108	.125	.110	.160	.173	.188	.227	.261	.058	.085	.111
15.22	.634	.027	.043	.004	.064	.046	.008	.228	.218	.199	.102	.106	.032
15.04	.681	.025	.019	.005	.033	.015	.009	.157	.131	.099	.085	.094	.021
12.63	.703	.031	.080	.001	.088	.015	.005	.113	.059	.085	.047	.032	.019
Afterbody 6													
27.27	.084	.113	.112	.118	.131	.130	.136	.157	.159	.168	.179	.178	.186
25.56	.104	.057	.059	.062	.073	.070	.073	.095	.095	.096	.116	.120	.124
23.85	.154	.005	.005	.007	.011	.005	.010	.014	.014	.016	.044	.040	.042
22.15	.226	.005	.003	.001	.007	.004	.002	.015	.002	.010	.013	.018	.020
20.45	.284	.005	.003	.001	.022	.007	.007	.015	.015	.019	.063	.031	.032
18.75	.341	.011	.005	.005	.035	.010	.003	.002	.015	.015	.030	.030	.038
17.00	.404	.009	.031	.033	.031	.031	.031	.072	.093	.108	.135	.124	.095
15.29	.454	.008	.013	.018	.023	.022	.018	.105	.105	.108	.132	.123	.113
15.06	.469	.119	.159	.176	.105	.105	.132	.005	.019	.039	.059	.059	.009
12.44	.506	.126	.188	.239	.159	.218	.269	.070	.120	.171	.008	.043	.069
11.20	.606	.118	.154	.199	.103	.265	.310	.113	.201	.201	.288	.015	.072
10.21	.642	.091	.107	.139	.130	.150	.150	.168	.225	.260	.055	.085	.114
9.07	.682	.055	.042	.002	.058	.043	.001	.223	.212	.134	.101	.103	.030

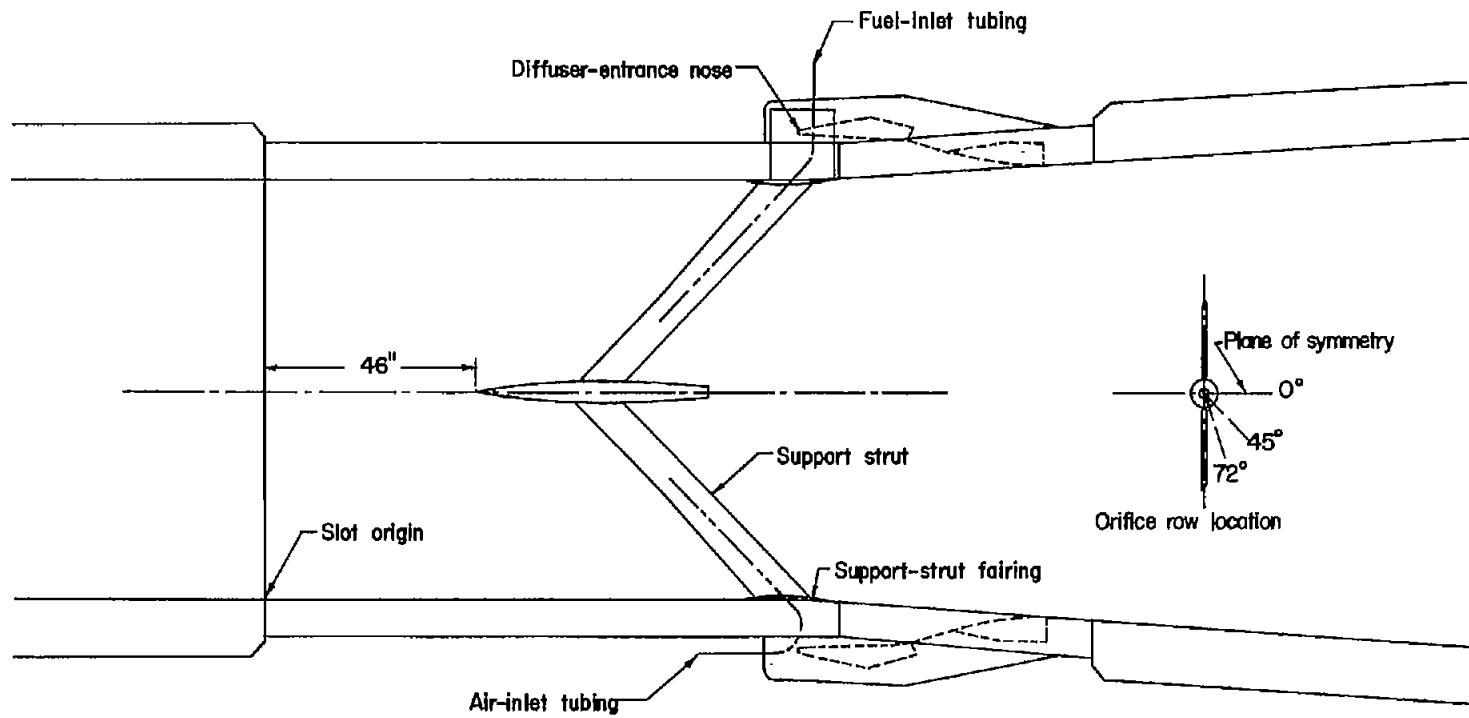
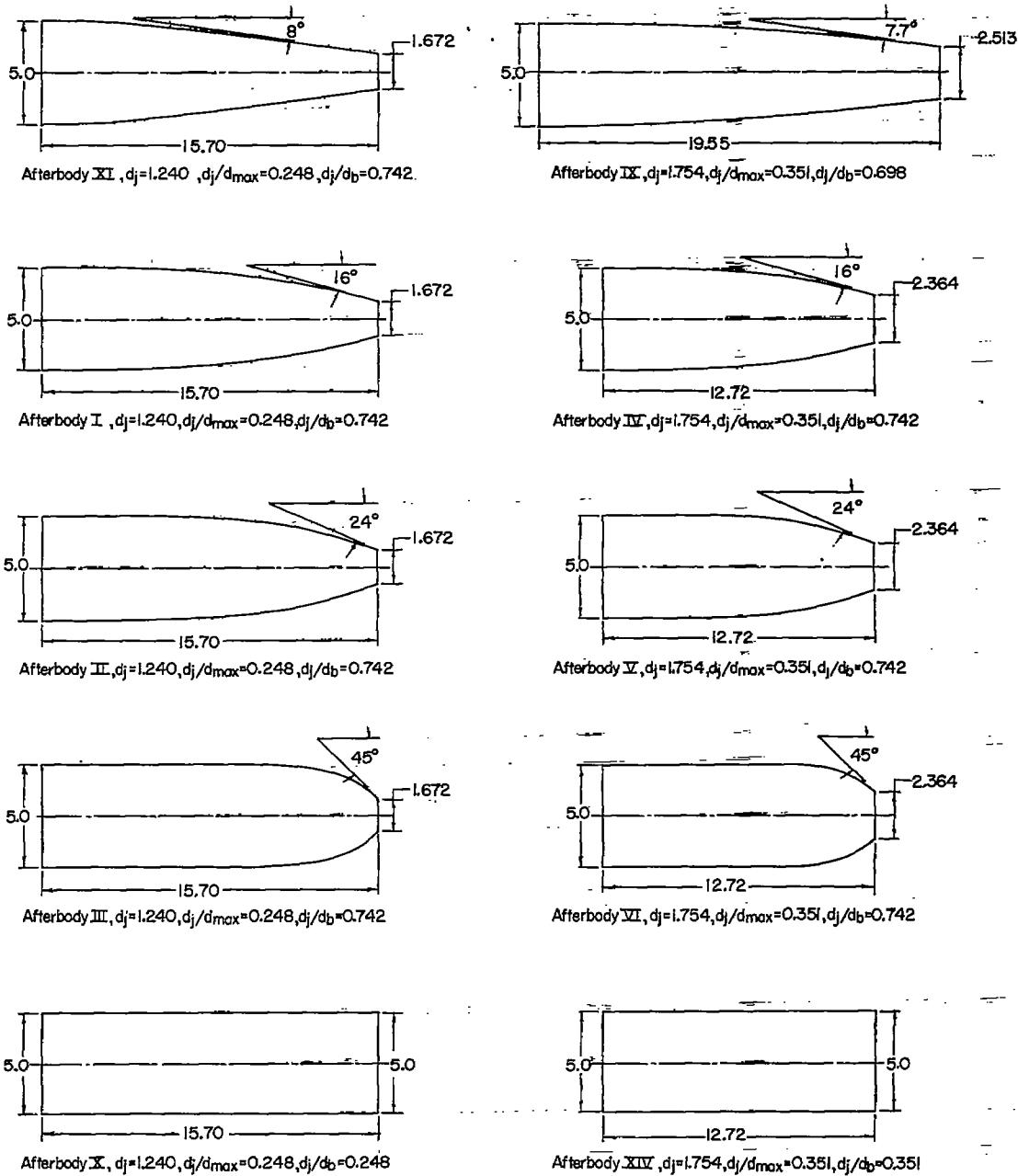


Figure 1.- Turbojet-simulator model in Langley 8-foot transonic tunnel.



(a) Shapes used to study the effects of  $\beta$  and  $d_j/d_{max}$ .

Figure 2.- Drawing of afterbody shapes investigated. All dimensions are in inches unless otherwise noted.

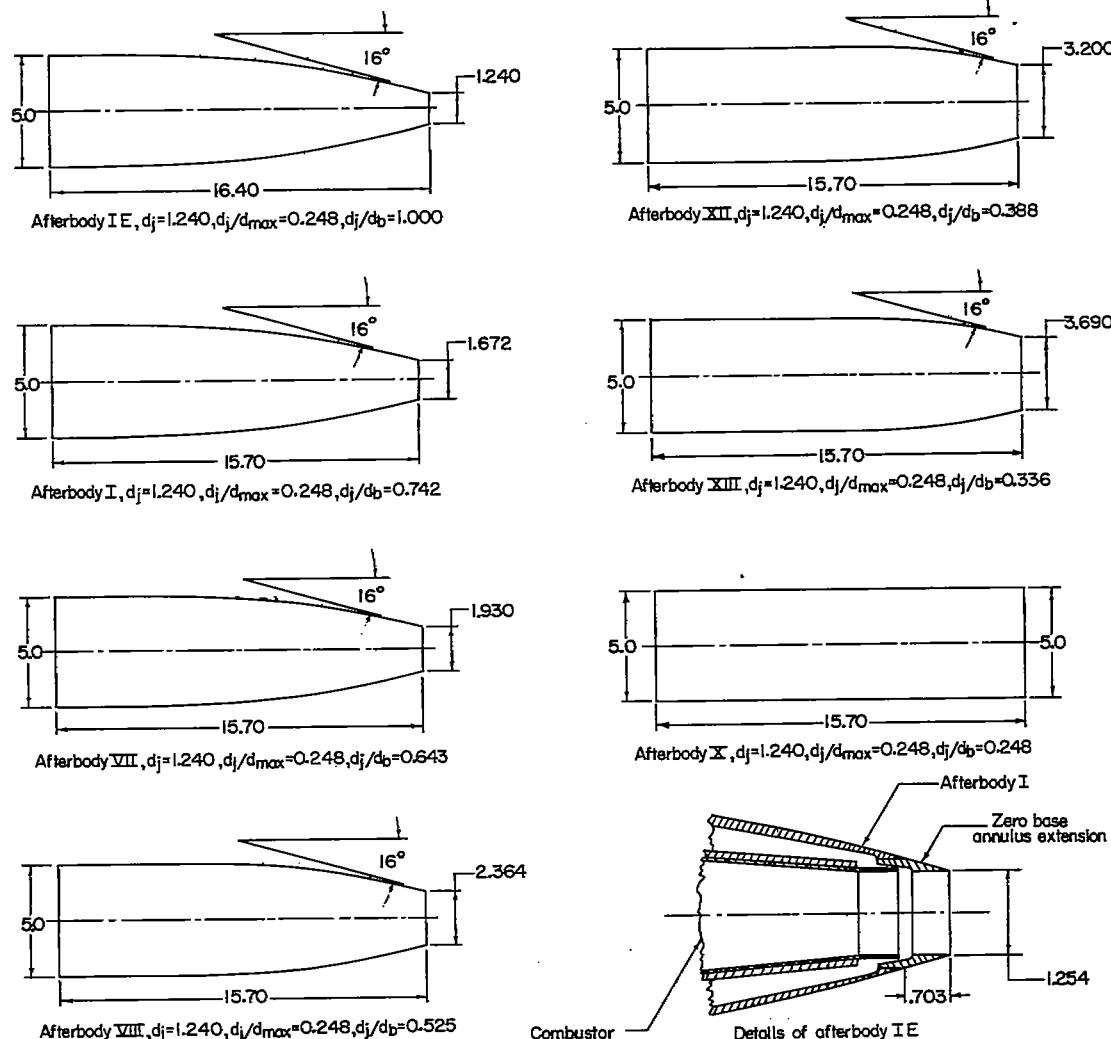
(b) Shapes used to study the effects of  $d_j/d_b$ .

Figure 2.- Concluded.

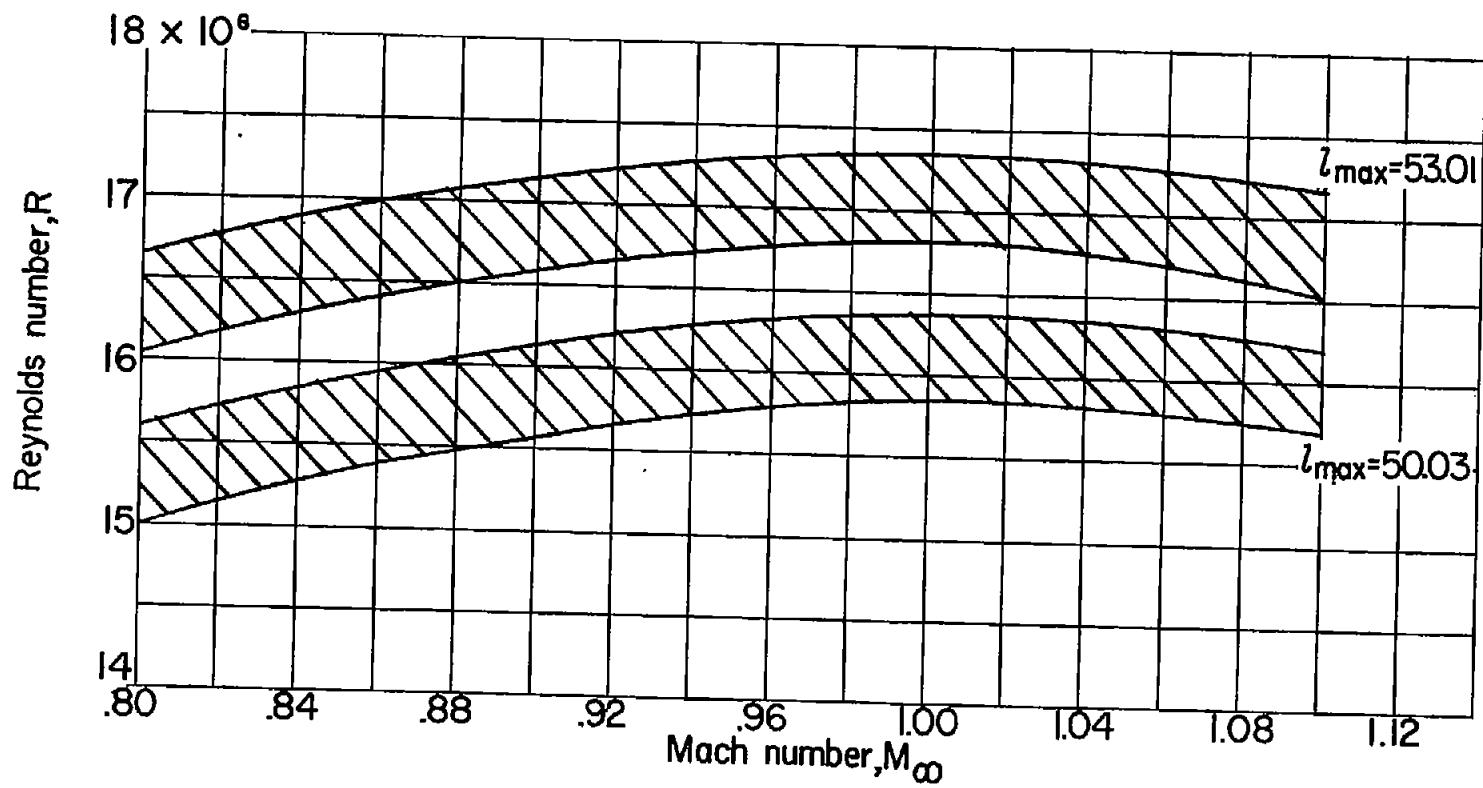
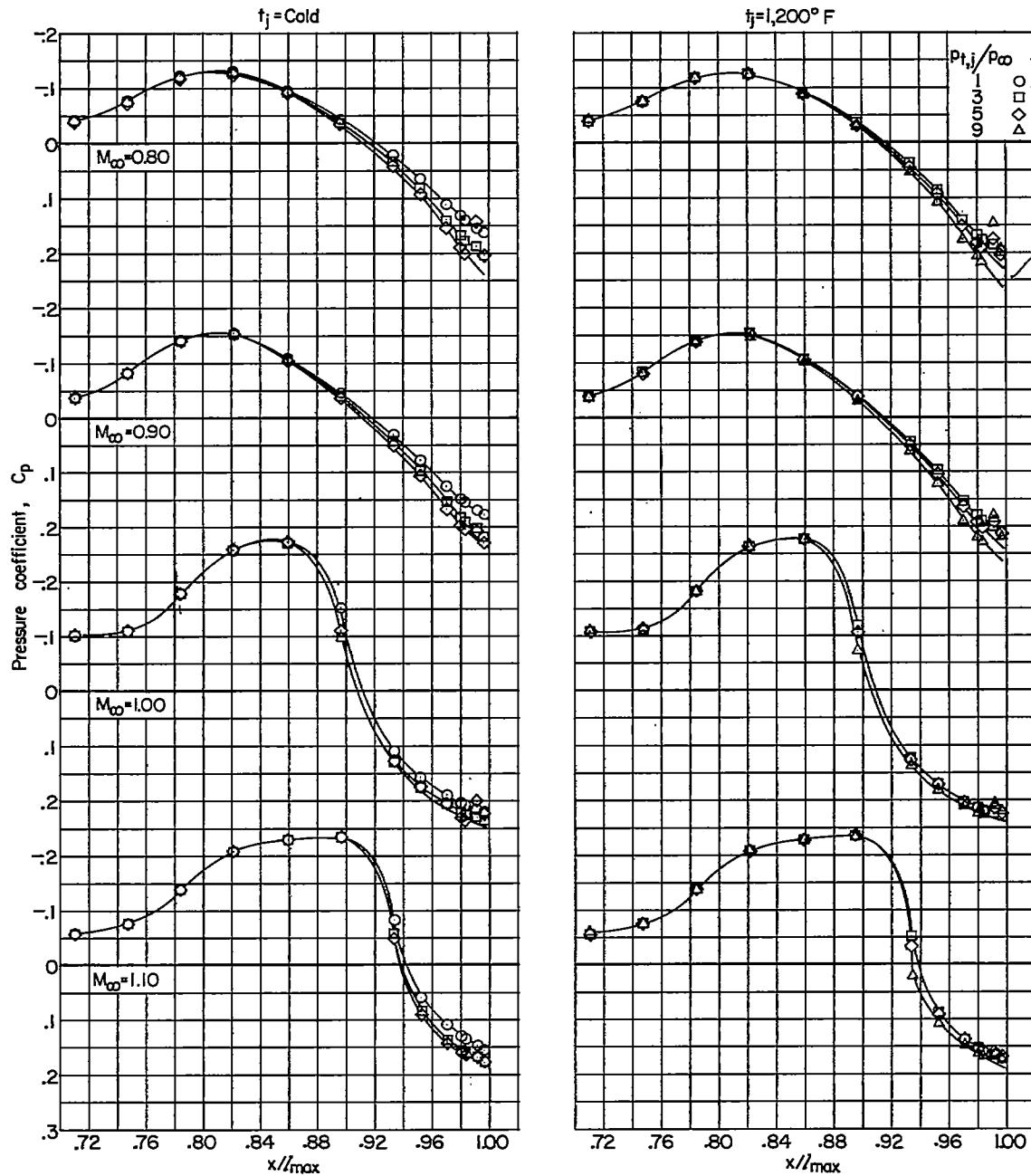
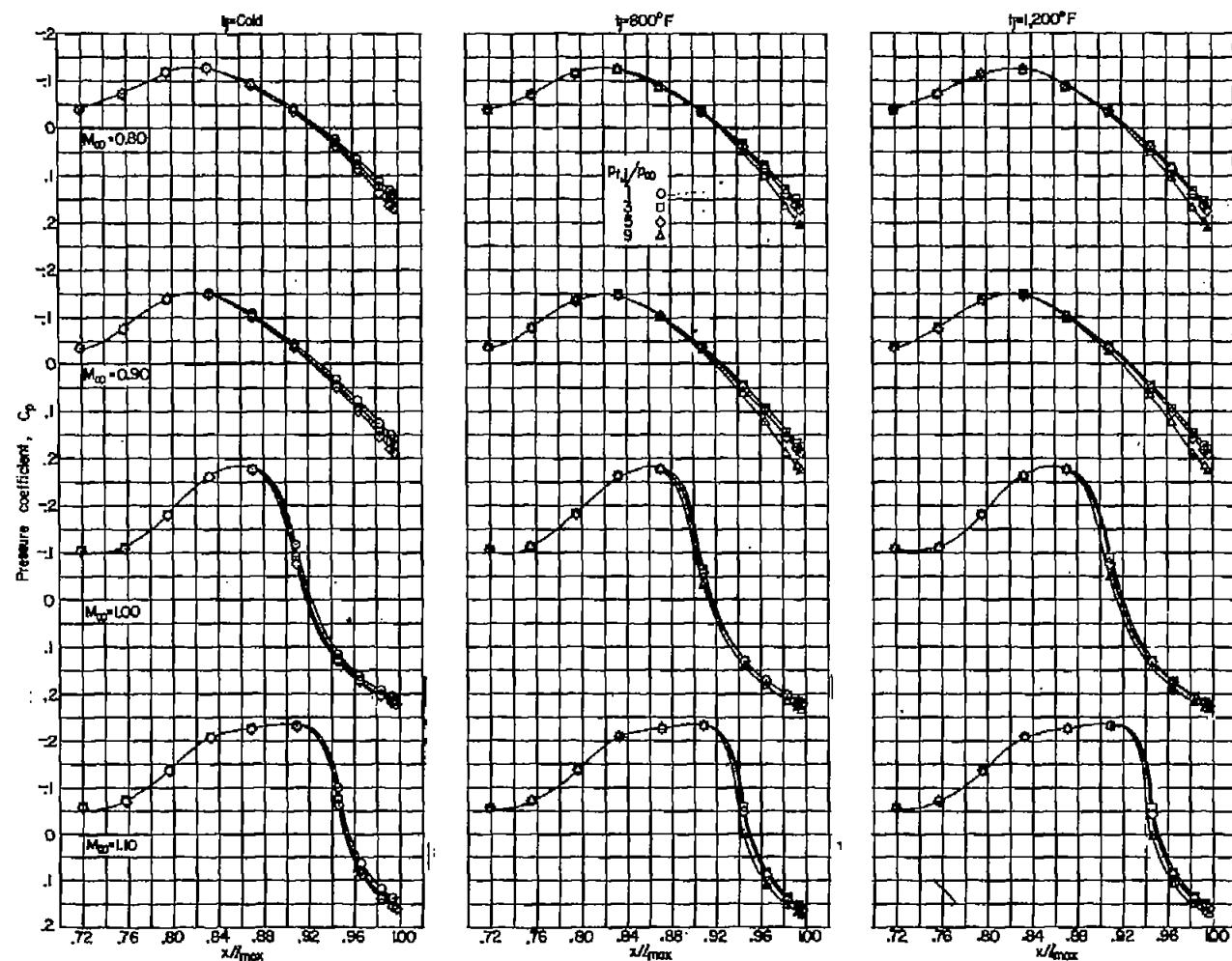


Figure 3.- Variation of Reynolds number, based on body length, with Mach number.



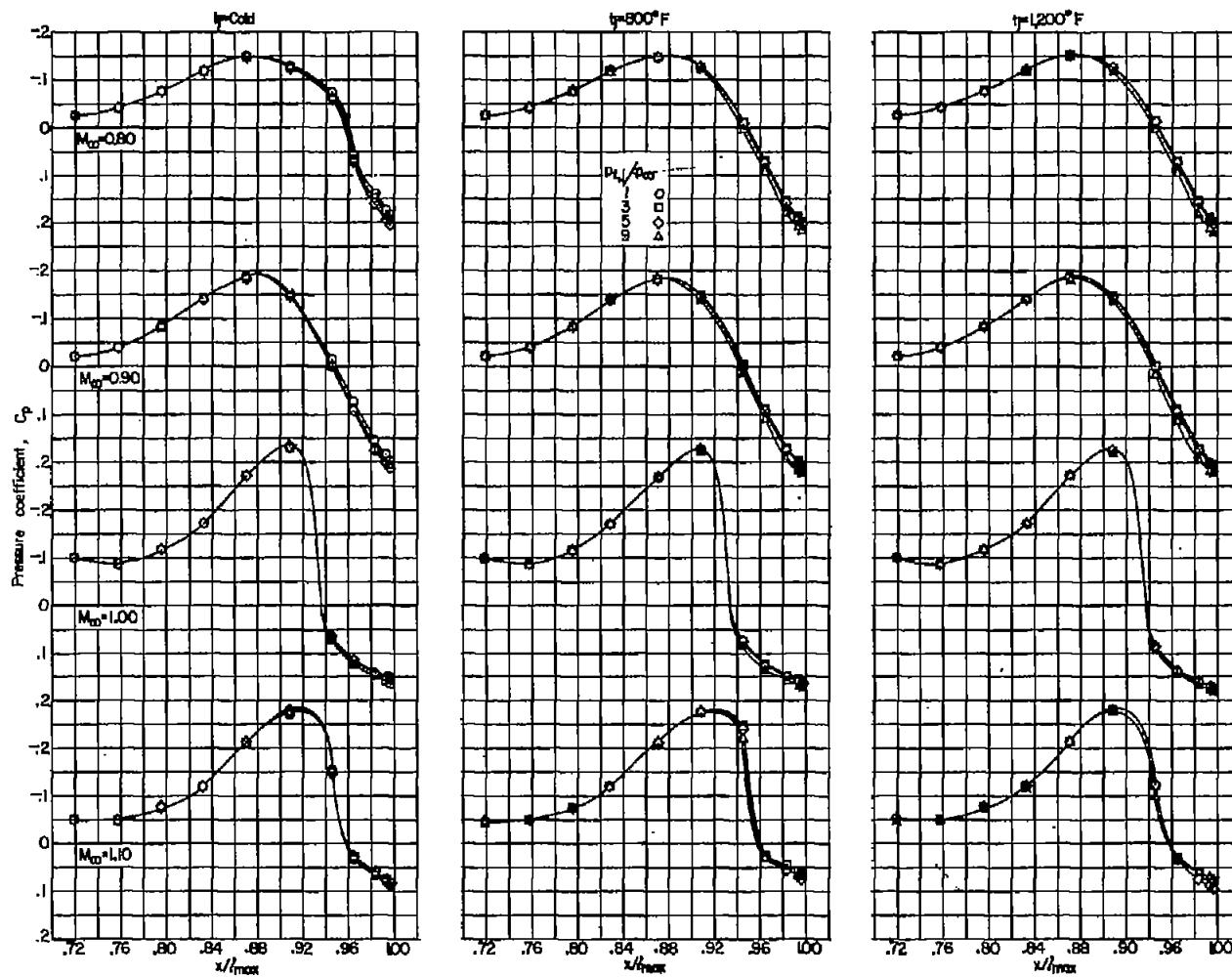
(a) Afterbody IE.

Figure 4.- Variation of local-pressure coefficients along the 0° meridian for the afterbodies investigated.



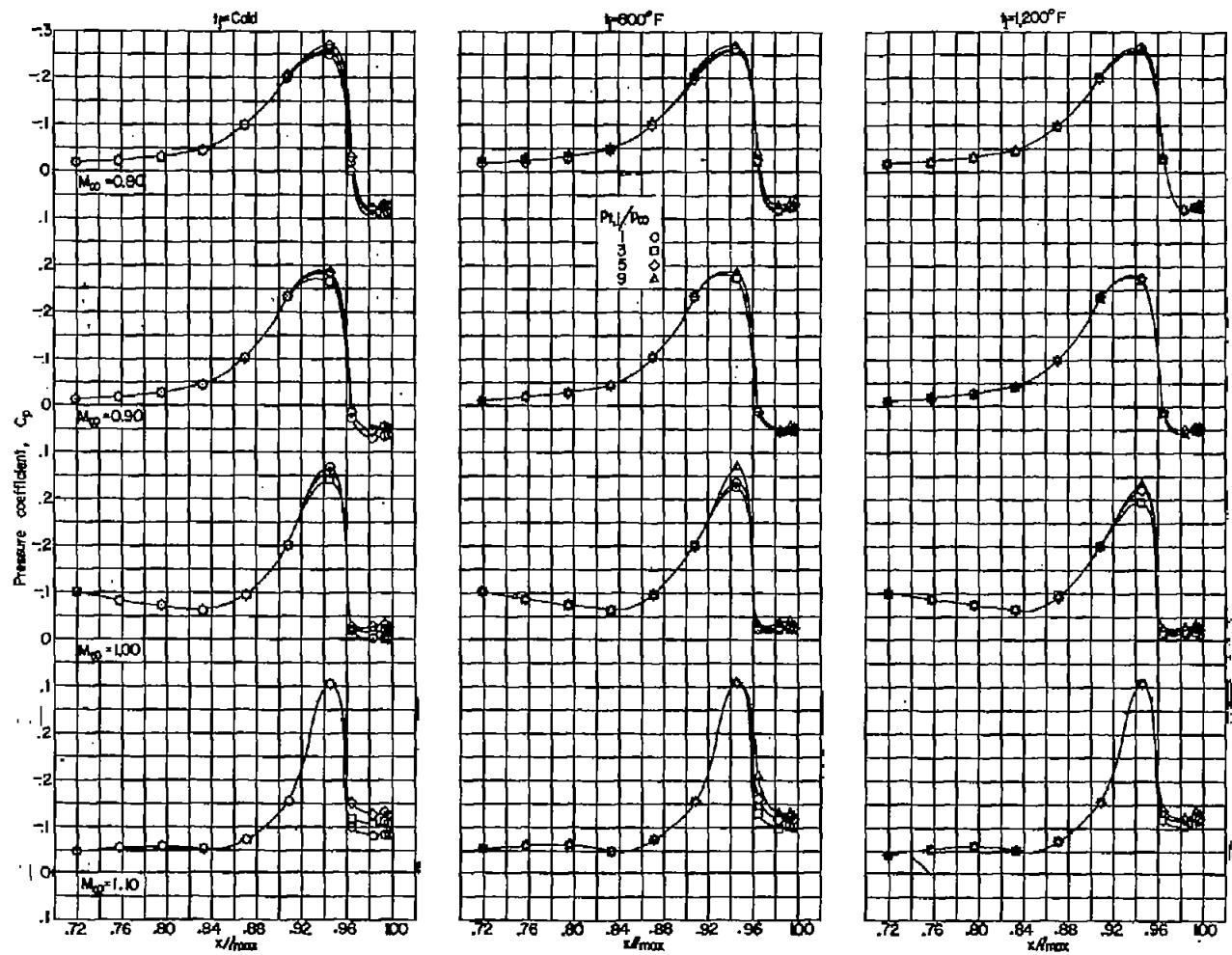
(b) Afterbody I.

Figure 4.- Continued.

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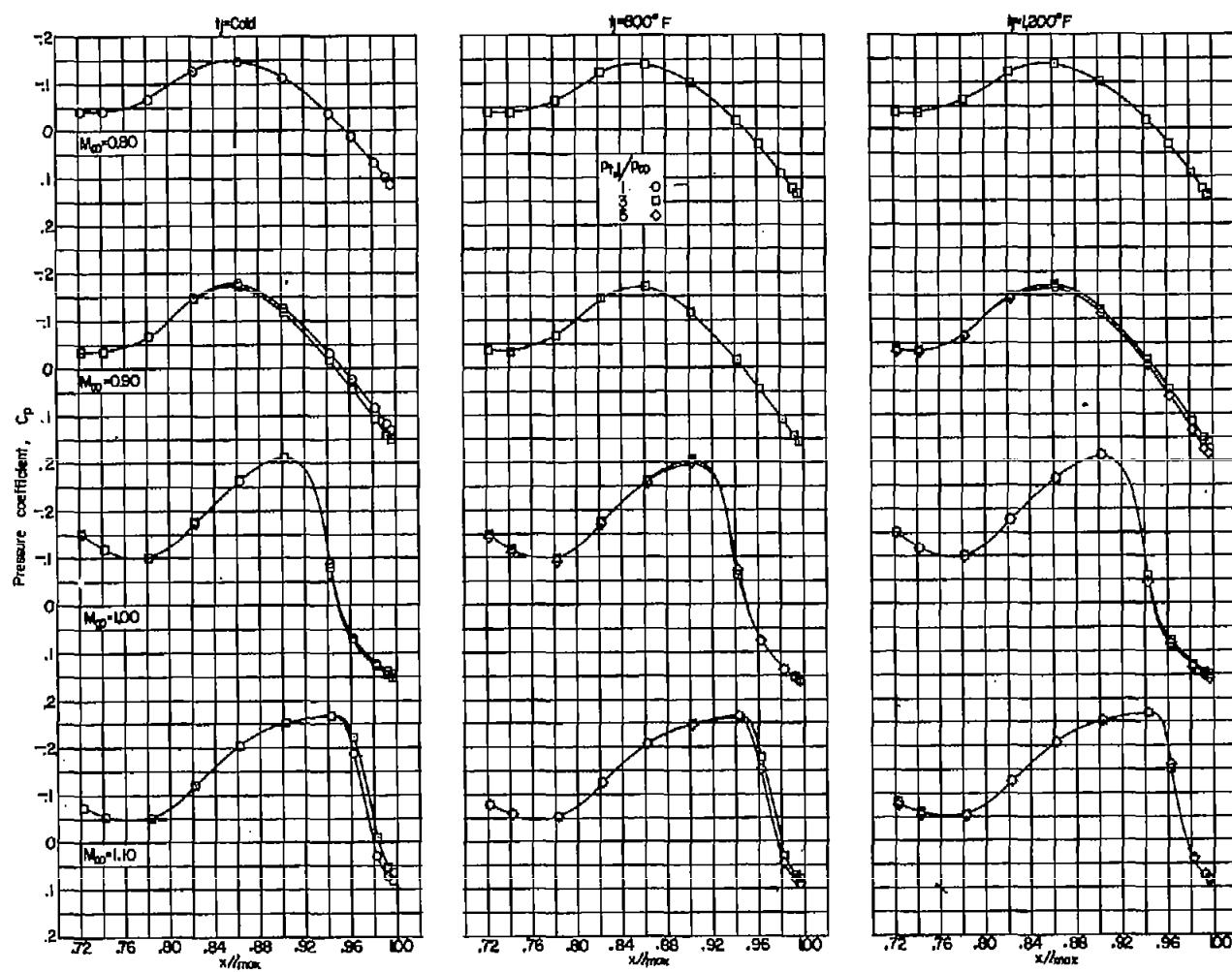
(c) Afterbody II.

Figure 4.- Continued.



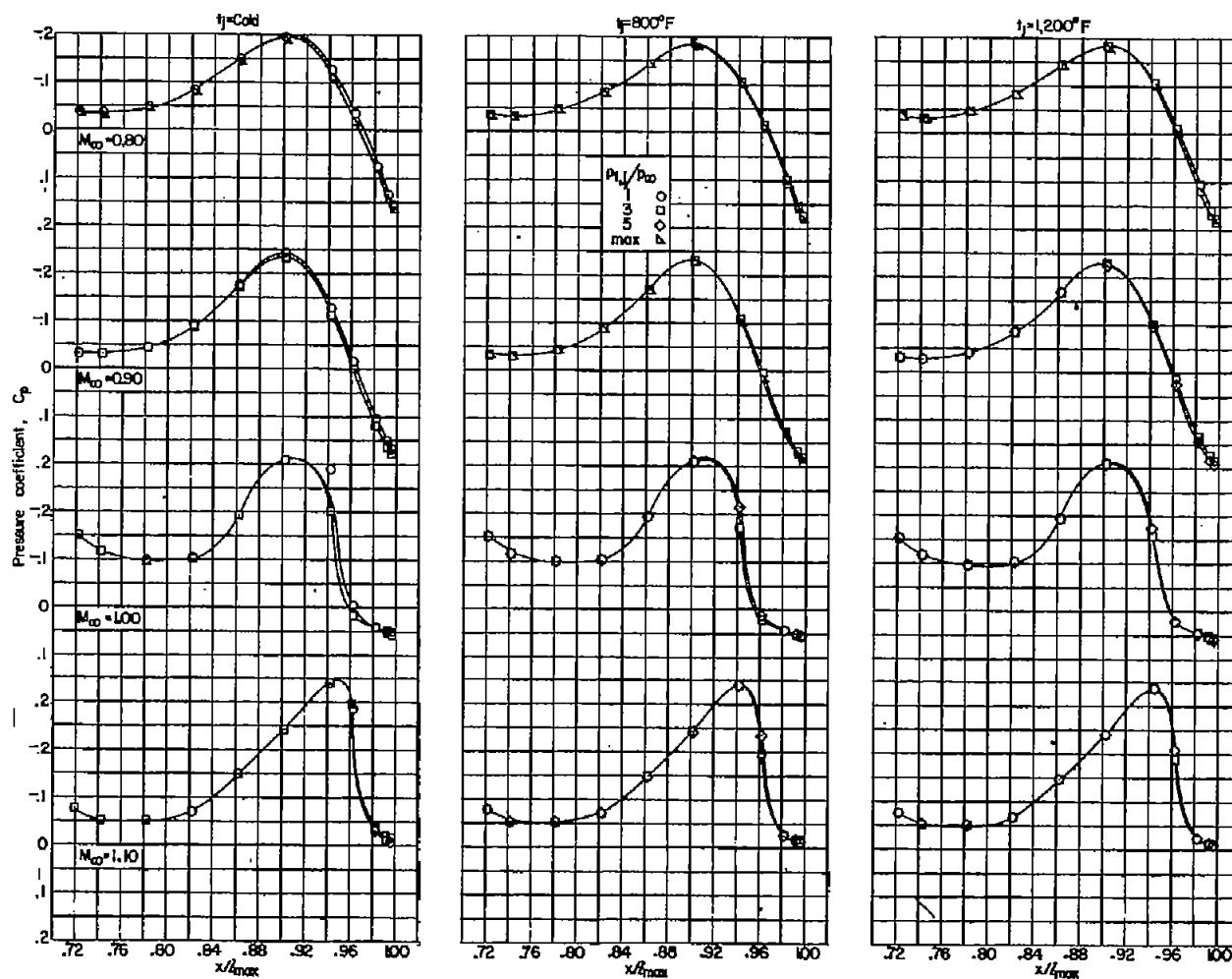
(d) Afterbody III.

Figure 4.- Continued.



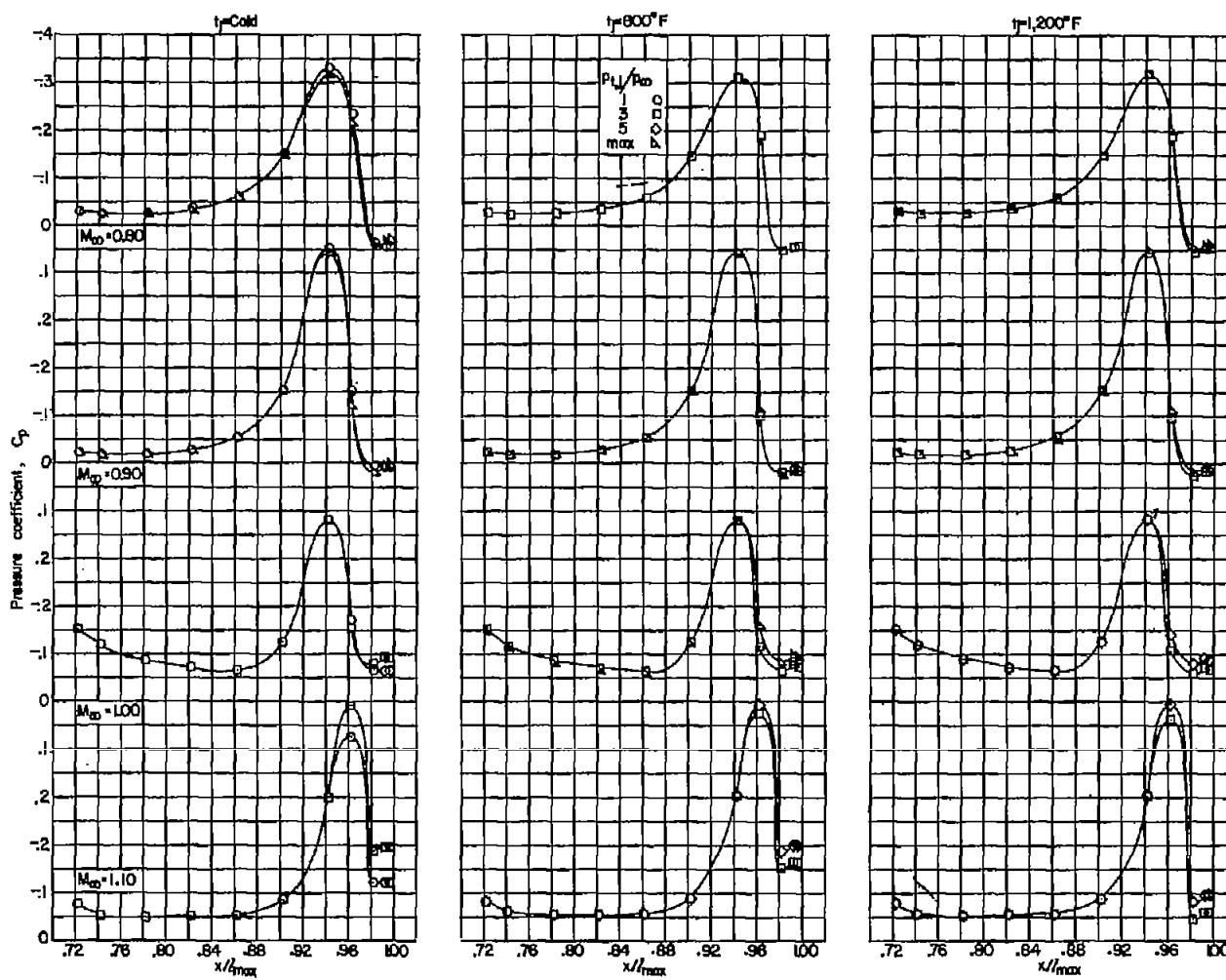
(e) Afterbody IV.

Figure 4.- Continued.



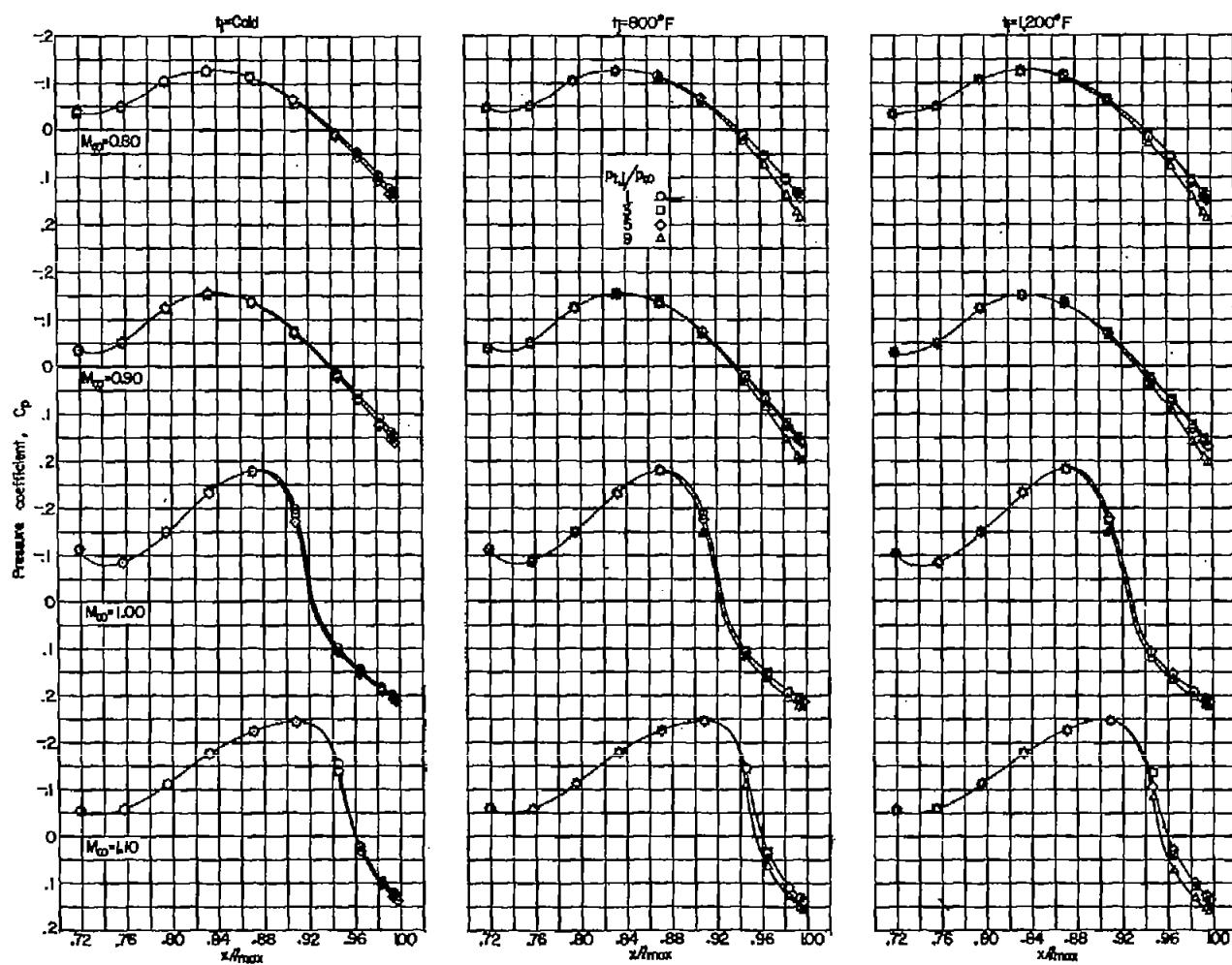
(f) Afterbody V.

Figure 4.- Continued.



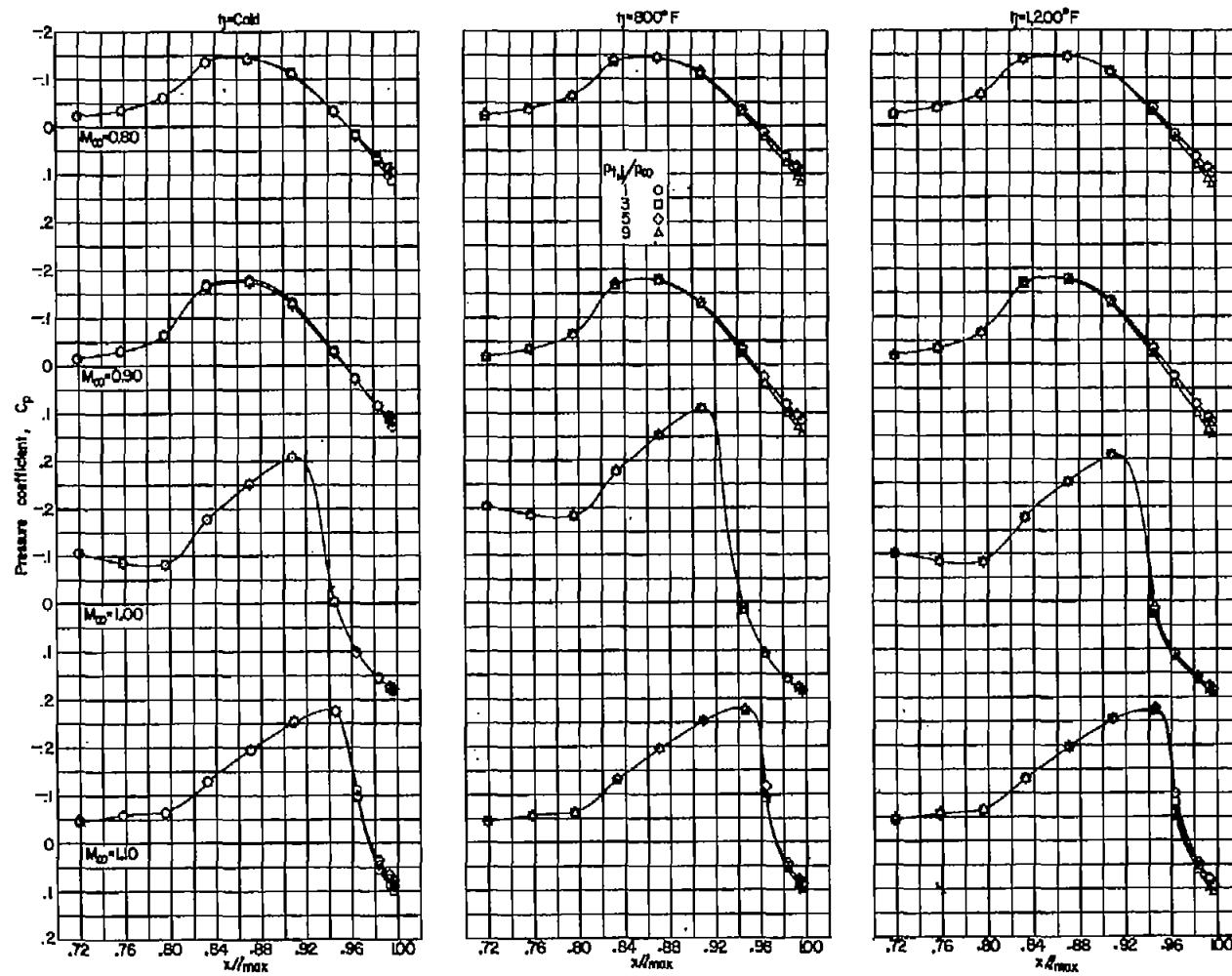
(g) Afterbody VI.

Figure 4.- Continued.



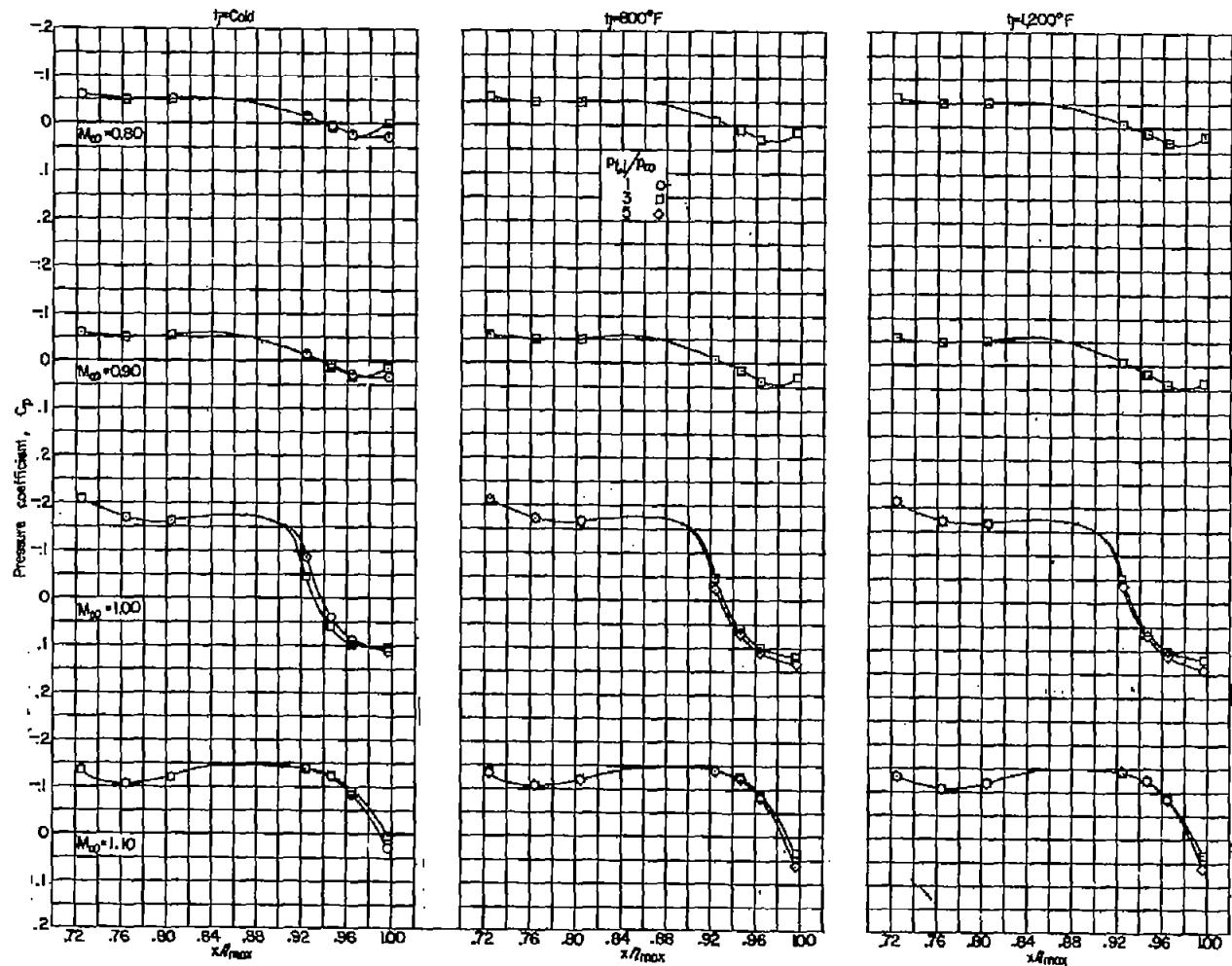
(h) Afterbody VII.

Figure 4.- Continued.



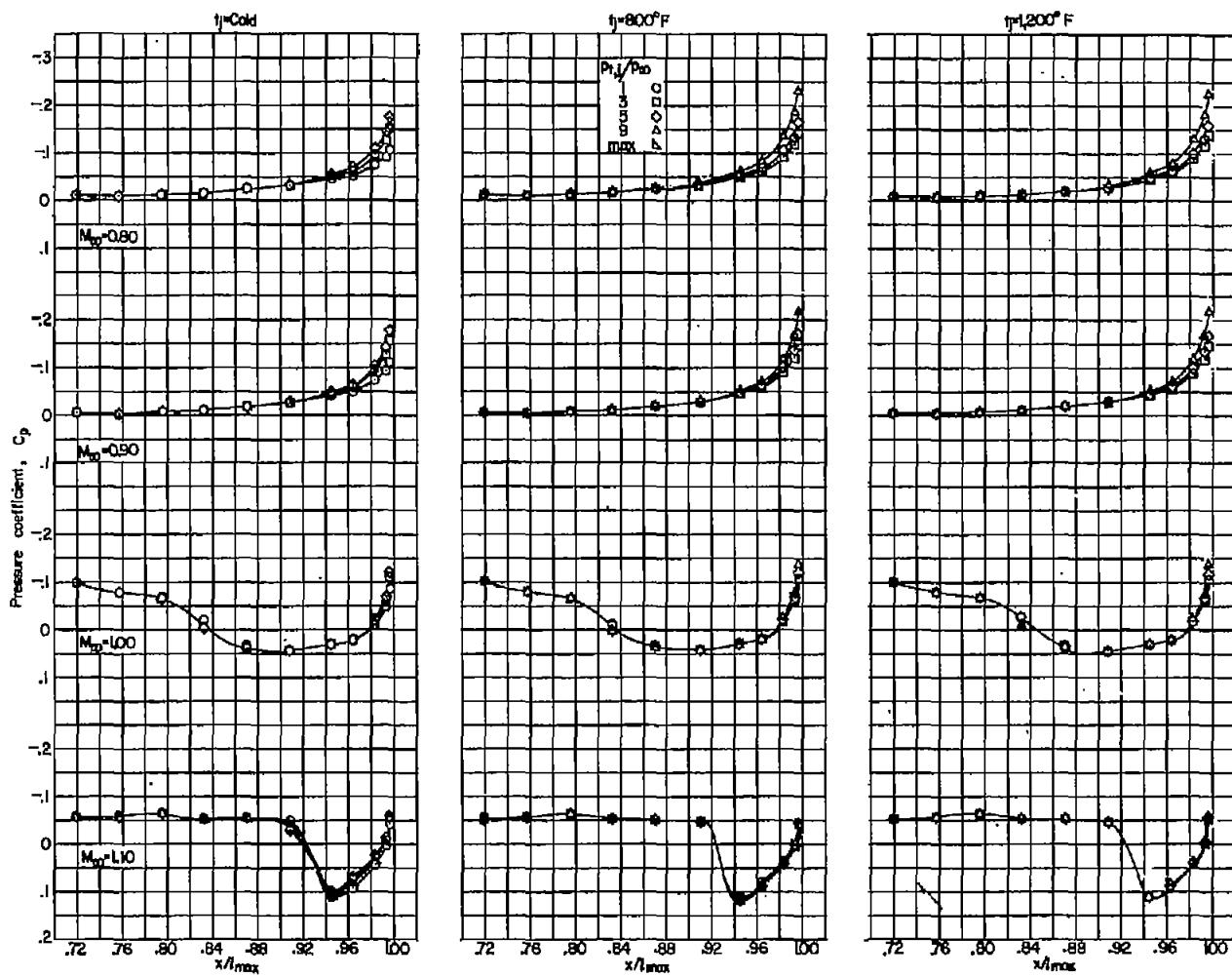
(i) Afterbody VIII.

Figure 4.- Continued.



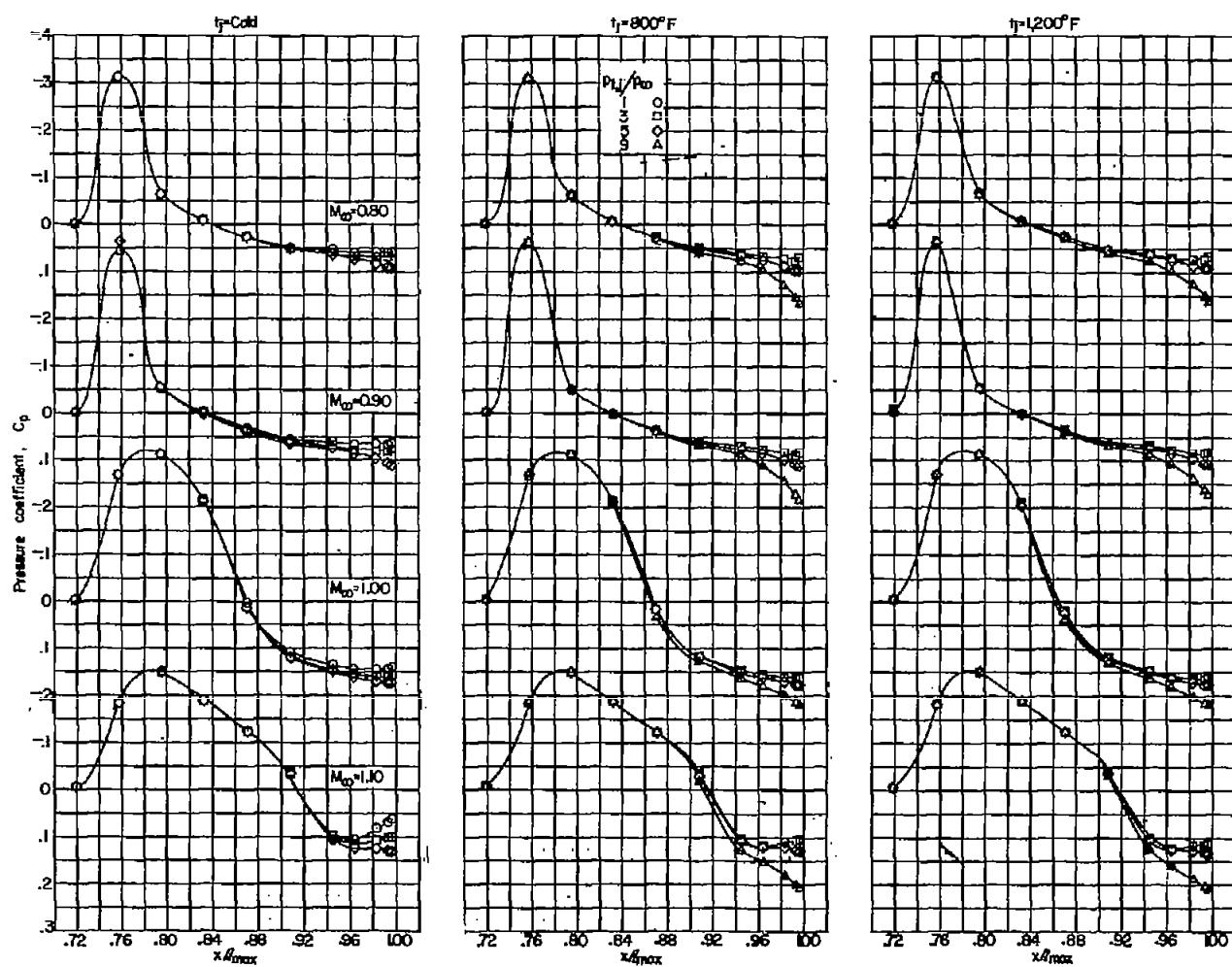
(j) Afterbody IX.

Figure 4.- Continued.



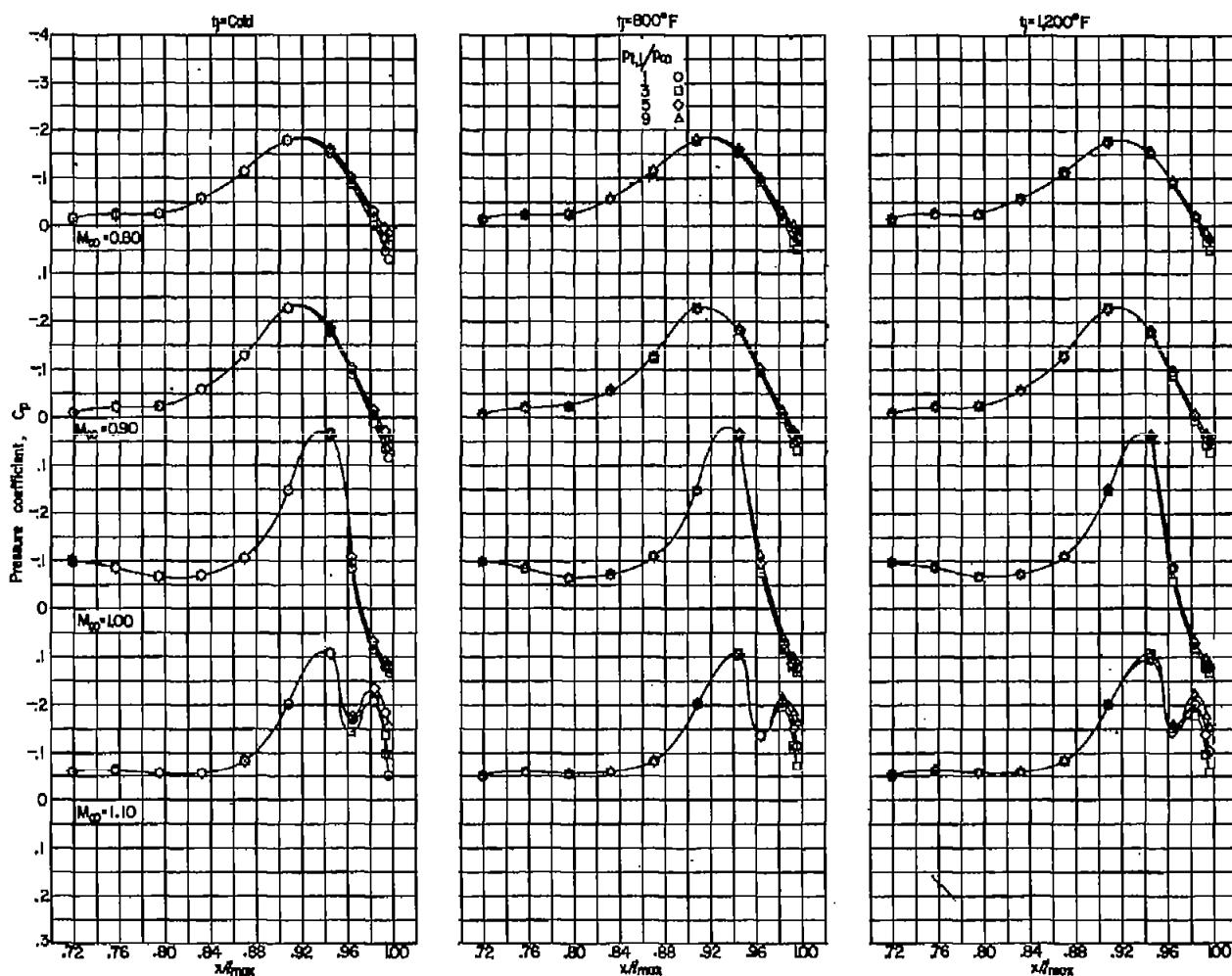
(k) Afterbody X.

Figure 4.- Continued.



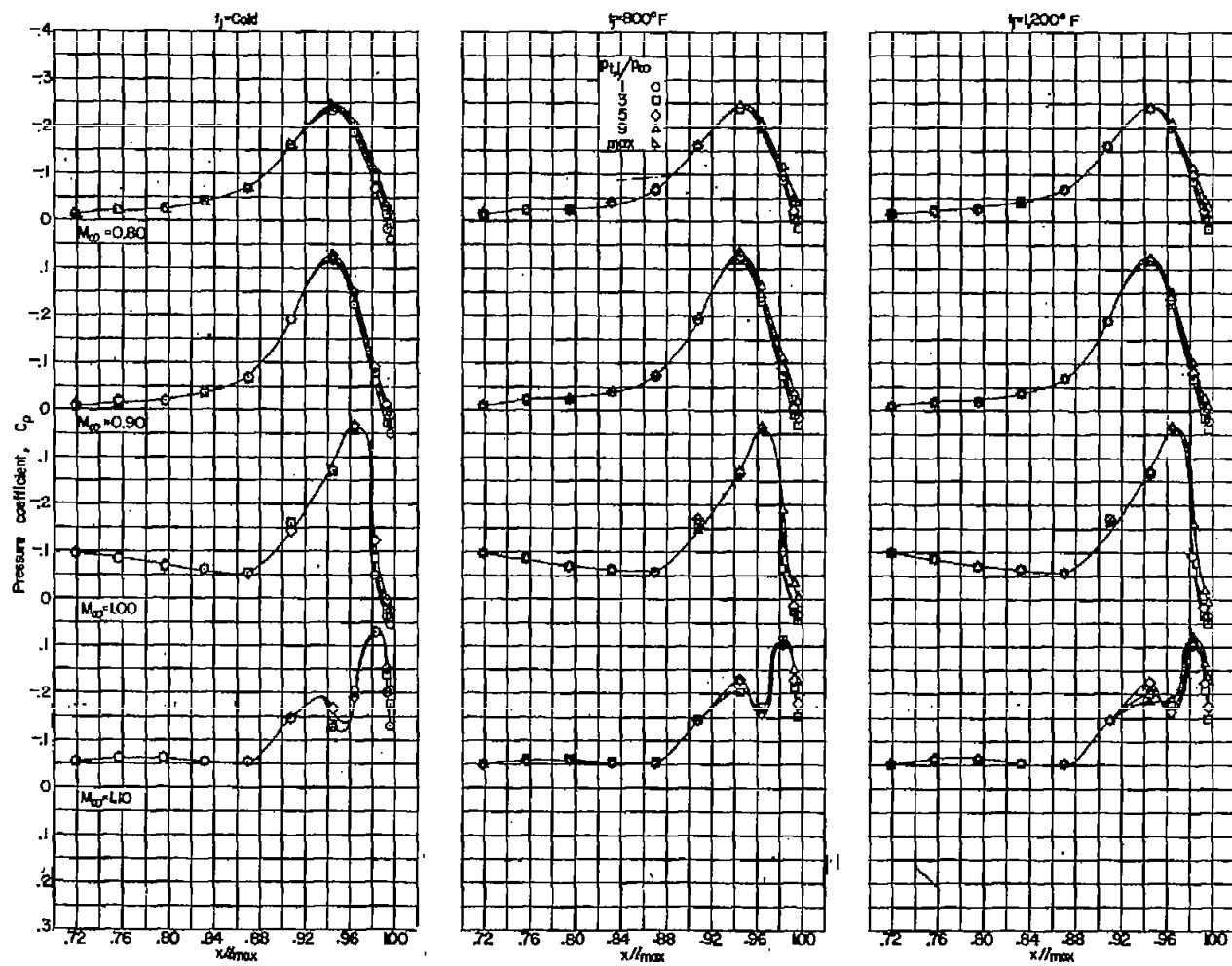
(i) Afterbody XI.

Figure 4.- Continued.



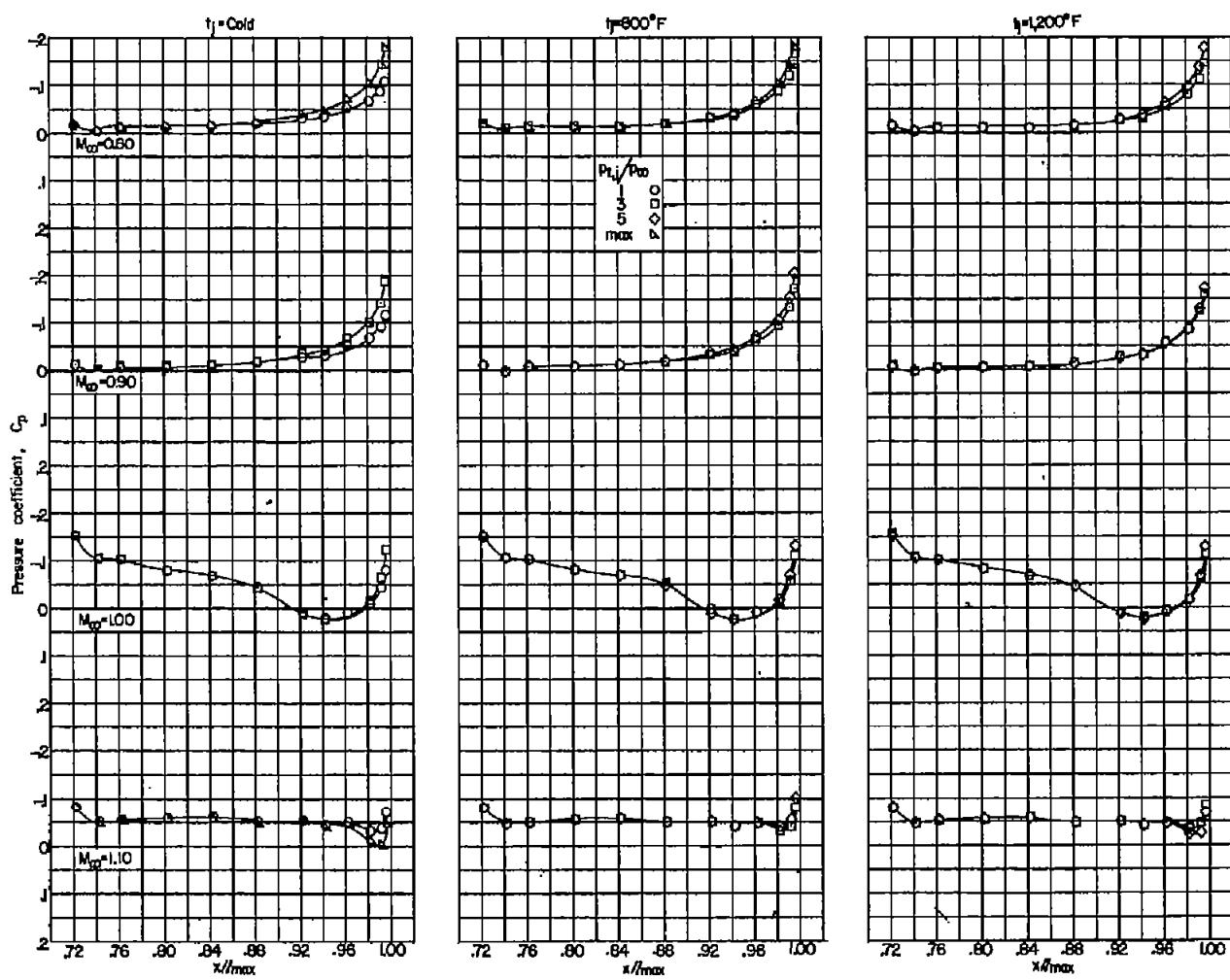
(m) Afterbody XII.

Figure 4.- Continued.



(n) Afterbody XIII.

Figure 4.- Continued.



(o) Afterbody XIV.

Figure 4.- Concluded.