

RESEARCH MEMORANDUM

EFFECTS OF VERTICAL LOCATION OF THE WING AND HORIZONTAL
TAIL ON THE STATIC LATERAL AND DIRECTIONAL STABILITY
OF A TRAPEZOIDAL-WING AIRPLANE MODEL AT
MACH NUMBERS OF 1.41 AND 2.01

By Ross B. Robinson

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NATIONAL ADVISORY COMMITTEE
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SUMMARY

An investigation has been conducted to determine the effects of vertical location of the wing and horizontal tail on the static lateral and directional stability at various combined angles of attack and sideslip for a supersonic airplane configuration at Mach numbers of 1.41 and 2.01. The wing had a trapezoidal plan form with an aspect ratio of 3.00, a taper ratio of 0.25, and 4-percent-thick circular-arc sections. The horizontal tail was also a trapezoid with an aspect ratio of 4, a taper ratio of 0.6, and NACA 65A006 airfoil sections.

The configurations investigated were a high-wing, a midwing, and a low-wing arrangement, in combination with horizontal-tail positions varying from a location 0.208 wing semispan below to 0.556 semispan above the body center line. Tests were made both with and without the horizontal tail, vertical tail, and wing. The investigation was conducted in the Langley 4- by 4-foot supersonic pressure tunnel.

In general, the directional stability is increased for the low-wing configurations and decreased for the high-wing configurations primarily as a result of the induced sidewash effects on the vertical tail. The high wing provided a positive dihedral effect and the low wing provided a negative dihedral effect for the configuration, either with or without the vertical tail.

The effects of wing vertical position on the directional stability and effective dihedral were, in general, the same as those obtained at subsonic speeds and for a similar configuration having a 45° swept wing at supersonic speeds.

INTRODUCTION

The experimentally determined effects of wing and tail locations on the aerodynamic characteristics of generalized aircraft configurations can be of considerable usefulness to the designer in the estimation of the stability and performance of similar specific configurations. In addition, such generalized results may be useful in the evaluation of various calculative methods for the prediction of the aerodynamic characteristics of airplanes.

Results of several investigations of various arrangements of wing-body-tail combinations at subsonic, transonic, and supersonic speeds are given in references 1 to 20.

An investigation has been made in the 4- by 4-foot supersonic pressure tunnel at Mach numbers of 1.41 and 2.01 to determine the effects of vertical location of wing and horizontal tail on the aerodynamic characteristics of a complete airplane model having a trapezoidal wing and horizontal tail with unswept 0.75-chord lines. Six-component force and moment data were obtained for combined angles of attack and sideslip for complete models and various combinations of components. The static longitudinal stability characteristics are given in reference 21. The present report gives the static lateral and directional stability characteristics. Comparisons are made with results previously obtained for a similar configuration having a 45° swept wing and horizontal tail.

COEFFICIENTS AND SYMBOLS

The results are presented as coefficients of forces and moments with the reference center of moments at the longitudinal body station corresponding to the quarter-chord point of the mean geometric chord. Tabulated data are presented for both body- and stability-axis systems (fig. 1). The results presented in most of the figures are based on the body-axis system.

The coefficients and symbols are defined as follows:

- C_L lift coefficient, F_L/qS
- C_N normal-force coefficient, F_N/qS
- C_D' approximate drag coefficient, equal to true drag coefficient at zero sideslip, F_D'/qS

C_A	axial-force coefficient, F_A/qS
C_Y	side-force coefficient, F_Y/qS
C_m	pitching-moment coefficient, $M_Y/qS\bar{c}$
$C_{l,s}$	rolling-moment coefficient, stability-axis system, M_{X_S}/qSb
C_l	rolling-moment coefficient, body-axis system, M_X/qSb
$C_{n,w}$	yawing-moment coefficient, stability-axis system, M_{Z_S}/qSb
C_n	yawing-moment coefficient, body-axis system, M_Z/qSb
F_L	lift
F_N	normal force
F'_D	approximate drag
F_A	axial force
F_Y	side force
M_Y	pitching moment
M_{X_S}	rolling moment, stability-axis system
M_X	rolling moment, body-axis system
M_{Z_S}	yawing moment, stability-axis system
M_Z	yawing moment, body-axis system
b	wing span
\bar{c}	wing mean geometric chord
S	total wing area, including body intercept
x	longitudinal distance from nose
q	free-stream dynamic pressure

M	Mach number
α	angle of attack of body center line, deg
β	angle of sideslip of body center line, deg
i_t	horizontal-tail incidence (deflection with respect to body center line), positive when trailing edge is down, deg
$C_{l\beta}$	effective-dihedral parameter, $\partial C_l / \partial \beta$
$C_{n\beta}$	directional-stability parameter, $\partial C_n / \partial \beta$
$C_{Y\beta}$	side-force parameter, $\partial C_Y / \partial \beta$
$\Delta C_{l\beta}, \Delta C_{n\beta}, \Delta C_{Y\beta}$	incremental values of $C_{l\beta}$, $C_{n\beta}$, and $C_{Y\beta}$

Component designations:

B	body
W	wing
H	horizontal tail
V	vertical tail and ventral fin

Subscripts:

H	denotes high position when used with W or H
h	denotes incremental value due to addition of the horizontal tail when used with $\Delta C_{l\beta}$, $\Delta C_{n\beta}$, and $\Delta C_{Y\beta}$
L	denotes low position of the wing or horizontal tail
M	denotes mid position of wing
T	denotes tip position of the horizontal tail
V	denotes incremental values due to addition of the vertical tail and ventral fin

W denotes incremental values due to addition of the wing

i_t denotes incremental values due to deflection of the horizontal tail

MODELS AND APPARATUS

Details of the unswept-wing model are shown in figure 2 and the geometric characteristics of the models are given in tables I and II.

The model fuselage was a body of revolution having a length-diameter ratio of 11 and was composed of a 3.5-caliber tangent ogive nose, a cylindrical midsection, and a 2.63-caliber boattail rear section. The wing had an unswept 0.75-chord line, an aspect ratio of 3.00, a taper ratio of 0.25, and 4-percent-thick circular-arc sections in the stream direction. The horizontal tail had a trapezoidal plan form with an unswept 0.75-chord line, an aspect ratio of 4, a taper ratio of 0.6, and NACA 65A006 airfoil sections. The model was equipped with a vertical tail and a small ventral fin having relatively thick wedge-slab sections to facilitate mounting of the horizontal tail. The horizontal tail (fig. 2(b)) could be moved from a position on the ventral fin ($0.208b/2$ below the body center line; designated the low tail position) to two positions on the vertical tail ($0.382b/2$ and $0.556b/2$; designated the high and tip tail positions, respectively). Provision was made for varying the incidence angle of the horizontal tail.

The wing position could be varied to provide high-, mid-, or low-wing configurations. The angles of incidence and dihedral were zero for all wing positions.

Force and moment measurements were made through the use of a six-component internal strain-gage balance. Base pressures were measured by a tube placed just inside the base of the model. The model was mounted on a rotary sting to permit testing at combined angles of attack and sideslip.

TESTS, CORRECTIONS, AND ACCURACY

The conditions for the tests were:

Mach number	1.41	2.01
Stagnation temperature, °F	100	100
Stagnation pressure, lb/sq in. abs	10	10
Reynolds number based on \bar{c}	2.23×10^6	1.84×10^6

The stagnation dewpoint was maintained at -25° F or less so that no significant condensation effects were encountered in the test section.

Tests were made through combined angles of attack and sideslip to about 15° at $M = 1.41$ and to about 28° at $M = 2.01$.

The angles of attack and sideslip were corrected for deflection of the balance and sting under load. Base pressures were measured, and the axial force measured by the balance was adjusted to a base pressure equal to the free-stream static pressure.

The Mach number variation in the test section was less than ± 0.015 and the variation of the flow angles in vertical and horizontal planes did not exceed about $\pm 0.1^{\circ}$.

Estimated errors in the individual measured quantities are as follows:

	<u>M = 1.41</u>	<u>M = 2.01</u>
C_L	± 0.0056	± 0.0069
C_D }	± 0.0005	± 0.0006
C_A }		
C_Y	± 0.0021	± 0.0015
C_m	± 0.0022	± 0.0027
C_l }	± 0.0002	± 0.0001
$C_{l,s}$ }		
C_n }	± 0.0010	± 0.0005
$C_{n,w}$ }		
$i_t, \text{ deg}$ }	± 0.2	± 0.2
$\alpha, \text{ deg}$ }		
$\beta, \text{ deg}$ }		

PRESENTATION OF RESULTS

Tabulated data for Mach numbers of 1.41 and 2.01 are presented in tables III and IV based on the stability-axis system and in tables V and VI based on the body-axis system. Table VII is a run log giving the configurations tested during each run.

Typical plots of the basic data for various combinations of components are presented as follows:

	Figure
Typical variations of C_n , C_l , and C_y with β for various combinations of model components. $M = 1.41$	3
Typical variation of C_n , C_l , and C_y with β for various combinations of model components. $M = 2.01$	4
Typical variations of C_m , C_D^i , and C_L with β for various combinations of model components. $M = 1.41$	5
Typical variations of C_m , C_D^i , and C_L with β for various combinations of model components. $M = 2.01$	6

The remainder of the results are presented as values of the sideslip derivatives $C_{n\beta}$, $C_{l\beta}$, and $C_{y\beta}$ for various combinations of model components, and incremental values of these derivatives due to various components, as follows:

	Figure
Effect of wing position on the sideslip derivatives. Horizontal tail off; $M = 1.41$	7
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Effect of wing position on the sideslip derivatives. Complete model; $M = 1.41$	9
Effect of wing position on the sideslip derivatives. Complete model; $M = 2.01$	10
Effect of wing position on the contribution of the vertical tail to the sideslip derivatives. Horizontal tail off . . .	11
Effect of wing plan form on the sideslip derivatives. Horizontal tail off; $M = 1.41$	12
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Effect of horizontal-tail position on the sideslip derivatives. Complete model with high wing; $i_t = 0^\circ$; $M = 2.01$. .	16
Effect of wing position on the contribution of the horizontal tail to the sideslip derivatives. Complete model; $i_t = 0^\circ$	17

Figure

Effect of wing position on the contribution of the horizontal tail to the sideslip derivatives. Complete model; $i_t = 0^\circ$; $M = 2.01$	18
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Effect of wing position on the contribution of deflection of the horizontal tail to the sideslip derivatives. Complete model; $M = 2.01$	20
Effect of horizontal-tail plan form on the sideslip derivatives. Wing off; $i_t = 0^\circ$; $M = 2.01$	21
Effect of vertical-tail airfoil section on the sideslip derivatives. Complete model with high wing and low horizontal tail; $i_t = 0^\circ$; $M = 2.01$	22

All the sideslip characteristics (C_n , C_l , and C_Y) and sideslip derivatives ($C_{n\beta}$, $C_{l\beta}$, and $C_{Y\beta}$) are based on the body-axis system.

DISCUSSION

The typical variations of C_n , C_l , and C_Y with β shown in figures 3 and 4 indicate the linearity of the results for $M = 1.41$ and $M = 2.01$, respectively, for the maximum and minimum angles of attack at each Mach number. Values of the sideslip derivatives $C_{n\beta}$, $C_{l\beta}$, and $C_{Y\beta}$ were measured from similar curves for a small sideslip range near $\beta = 0^\circ$.

Effects of Wing Position and Plan Form

Effects of wing position.- The effects of wing position on the directional stability parameter $C_{n\beta}$ (figs. 7 and 8) were similar to those indicated by subsonic tests of configurations with unswept and 45° swept wings (ref. 1) and by supersonic tests of a 45° swept-wing configuration (ref. 20). In general, the values of $C_{n\beta}$ with the vertical tail on were highest for the low-wing configuration and lowest for the high-wing configuration at both Mach numbers. At the higher angles of attack $C_{n\beta}$ decreases for each wing position. With the vertical tail off, an opposite effect occurs in that the level of instability at

angle of attack is less for the high wing and greater for the low wing at both Mach numbers. These characteristics apparently result in part from the sidewash disturbance caused by the wing-body juncture. This sidewash, as pointed out in reference 1, results from the differential wing pressures near the wing root that are created by the lateral component of velocity due to sideslip. For the high-wing case this sidewash is adverse above and favorable below the center of the wing wake. The reverse is true for the low-wing case. Hence, at zero angle of attack, the afterbody lies in the same type of flow region for either wing position and the values of $C_{n\beta}$ for the tail-off configurations are essentially unchanged by wing position. With increasing angle of attack, the low-wing arrangement becomes increasingly unstable since the afterbody moves down through a region of adverse sidewash (figs. 7 and 8). For the high-wing arrangement, there is a reduction in the instability with increasing angle of attack as the afterbody moves down through a region of favorable sidewash and into an undisturbed flow region. At $M = 2.01$ the high-wing arrangement becomes directionally stable above $\alpha \approx 18^\circ$.

With the addition of the vertical tail at $\alpha = 0^\circ$, each configuration becomes stable at both Mach numbers (figs. 7 and 8). However, the tail contribution to $C_{Y\beta}$ and $C_{n\beta}$ is less with the high wing since this arrangement places the tail in a region of adverse sidewash (fig. 11). With increasing angle of attack, the tail contribution decreases rapidly at both Mach numbers for the high-wing arrangement as the tail passes through the region of adverse sidewash. For the low-wing arrangement, the decrease in tail contribution with increasing angle of attack is greatly alleviated as the tail passes through a region of favorable sidewash.

There is relatively little change in $C_{n\beta}$ with angle of attack for the midwing and wing-off configurations with the tail removed, except at the higher angles of attack at $M = 2.01$. This result might be expected since at the lower angles of attack these arrangements are essentially symmetric whereas at the higher angles of attack asymmetric vorticity appears in the body flow field.

The midwing and wing-off configurations become stable when the vertical tail is added. However, with increasing angle of attack, the tail contributions to $C_{Y\beta}$ and $C_{n\beta}$ for these configurations also decrease (figs. 8 and 11) and, in fact, the wing-off model at $M = 2.01$ becomes directionally unstable (fig. 8). This result is an indication of the effect of forebody vorticity on the tail contribution. This effect is also present for the wing-on cases and the resultant directional characteristics are caused by a combination of the forebody vorticity and the wing-body induced disturbance. It is interesting to note that, at the higher angles of attack for $M = 2.01$, the addition of the wing to

the tail-on configurations resulted in greater stability than that obtained for the wing-off case. The fact that this was true even for the high-wing arrangement, which in itself provides a destabilizing sidewash at the tail, indicates that the position and possibly the existence of the forebody vortex is affected by the presence of the high wing.

It might be pointed out that, in addition to the expected difference between the levels of $C_{n\beta}$ and $C_{y\beta}$ at $M = 1.41$ and those at $M = 2.01$, the effects of wing height appear to be less at the higher Mach number. This condition may result in part from a reduction in vortex strength for the wing-body induced flows as the lift-curve slope of the wing decreases. However, the decrease in wing-height effects at $M = 2.01$ might also be expected because of the lower lift-curve slope of the tail which, even for a constant sidewash angle at the tail, would result in a smaller incremental change in tail contribution.

An additional effect to be considered is the change with angle of attack of the dynamic pressure in the wing flow field. As noted in reference 22, this change involves an increase in dynamic pressure below the wing and a decrease in dynamic pressure above the wing for positive angles of attack. The effects of these changes are relatively small up to $M \approx 2$. Above $M \approx 2$, however, the dynamic-pressure changes become large and, when coupled with the fact that the wing Mach lines are swept back more over the afterbody and tail, may outweigh the effects of vorticity. Under these conditions high-wing configurations may have more favorable directional characteristics than low-wing configurations.

At both Mach numbers, for the wing-body configuration and the configuration of wing, body, and vertical tail, the effects of the wing position on the rolling-moment characteristics is to increase the effective dihedral $-C_{l\beta}$ for the high wing and reduce the effective dihedral for the low wing (figs. 7 and 8). The results are similar to that obtained at subsonic speeds (ref. 1) and at supersonic speeds for a similar configuration having a 45° swept wing (ref. 20). This dihedral effect results from the asymmetric flow about a yawed body which induces a positive increment of lift on the leading wing and a negative increment of lift on the trailing wing for the high-wing configuration, whereas the opposite effect occurs for the low-wing configuration. As expected, the addition of the vertical tail increases the effective dihedral for all configurations (fig. 11). For all but the highest angles of attack at $M = 2.01$, the tail contribution $\Delta C_{l\beta, V}$ is greatest for the low wing and least for the high wing, probably as a result of the favorable or adverse sidewash induced by the low and high wings, respectively. Above $\alpha = 16^\circ$ at $M = 2.01$, the value of $\Delta C_{l\beta, V}$ decreases rapidly to zero as the body vortices alter the flow field in the vicinity of

the vertical tail. Both the vertical-tail contribution and the wing effects are smaller at $M = 2.01$, probably as a result of the decreased lift-curve slope of the tail.

The effects of wing vertical location on the variation of C_L and C_m with β shown in figures 5 and 6 are similar to those obtained for a 45° swept-wing configuration (ref. 18). For low angles of attack, the lift and moment variations induced by the body flow field indicate an increase in body interference effects up to $\beta \approx 12^\circ$ and a decrease thereafter for both high and low wing positions. At the higher angles of attack, the values of C_m are essentially constant for the low wing but become significantly more positive for the high wing as the sideslip angle increases.

Effect of wing plan form.- The sideslip derivatives for a similar airplane model with a 45° swept wing and horizontal tail (ref. 20) and for the present trapezoidal (unswept) wing configuration are presented in figures 12 to 15. The results for the swept-wing model have been recomputed by using the wing geometry and center-of-gravity location of the unswept-wing configuration.

It should be noted that the 45° swept-wing and unswept-wing configurations represent two distinct airplanes, since the differences in the wing plan forms are not restricted to the change in sweep. The swept wing had 25 percent less wing area, a 65A004 airfoil section, higher aspect ratio, and a lower taper ratio than the unswept wing, while the horizontal tails varied only in sweep angle and thickness ratio (ref. 20 and table I). Both configurations had the same body, vertical tail, and ventral fin, with exactly the same provisions for varying the position of the wing and horizontal tail.

In general, for the configurations with horizontal tail off, the swept-wing configurations have larger values of $C_{n\beta}$ and $-C_{y\beta}$ than the unswept-wing configurations (figs. 12 and 13). At $M = 2.01$ the level of $C_{n\beta}$ was essentially constant for the swept wing to $\alpha \approx 12^\circ$, in contrast to the progressive decrease in $C_{n\beta}$ for the unswept wing. These results appear to be produced by the larger vertical-tail contributions for the swept-wing airplane (fig. 14), since the effects of plan form on the wing-body characteristics are relatively small for both Mach numbers (fig. 15).

Effects of Horizontal-Tail Position, Incidence, and Plan Form

Effects of tail position.- The variation of the sideslip derivatives with angle of attack for various wing and horizontal-tail positions when

$i_t = 0^\circ$ and -6° are shown in figures 9 and 10, and the contributions of the horizontal tail at $i_t = 0^\circ$ to the sideslip derivatives are shown in figures 17 and 18. At $M = 1.41$, addition of the horizontal tail in both the high and low positions generally produced positive increments of directional stability and negative increments of C_{Y_β}

because of the end-plate effect on the vertical tail. With increasing angle of attack the increments provided by the low tail generally decreased while the increments due to the high tail became larger.

Similar trends were obtained for $M = 2.01$, but the effects were smaller, as would be expected, since at the higher Mach number a much smaller portion of the vertical tail is affected by the horizontal tail. Mounting the horizontal tail at zero incidence near the tip of the vertical tail (fig. 16) produced trends similar to those obtained for the high tail position. The larger values of C_{N_β} and $-C_{Y_\beta}$ at higher angles of attack are a result of the larger end-plate effect of the tip-mounted tail.

Addition of the horizontal tail has a significant effect on the rolling-moment characteristics at $M = 1.41$ (fig. 17). The low tail provides a negative increment in effective dihedral ($+C_{l_\beta}$) whereas the high tail produces a positive increment ($-C_{l_\beta}$). These effects result from the interference of the horizontal tail on the vertical tail and ventral fin, respectively. Similar results are obtained at $M = 2.01$, but the increments in C_{l_β} are much smaller (fig. 18). As the angle of attack increases, the values of $C_{l_{\beta,h}}$ generally become more negative for both Mach numbers. As the horizontal-tail location is varied from the low to the tip position, the values of positive effective dihedral progressively increase (fig. 16).

The variations of C_m , C_L , and C_D' with β for both the high and low positions of the horizontal tail at $i_t = 0^\circ$ are presented in figures 5(c), 5(d), 6(c), and 6(d) for the configuration with high wing, vertical tail, and horizontal tail. For small sideslip angles the variation of C_m with β for the complete model is similar to that for the wing-body combination. However, for angles of attack to about 8° the values of C_m at the higher sideslip angles for the low horizontal-tail arrangement become increasingly positive, and for the high horizontal tail they become increasingly negative or remain about constant. Similar effects were obtained for the low-wing configuration.

Effects of tail incidence.- Deflection of the horizontal tail in the direction to provide longitudinal trim produced increasing directional

stability (more positive $C_{n\beta}$) and side force (more negative $C_{Y\beta}$) for the low tail and decreasing values for the high tail (figs. 19 and 20). The effects of tail deflection on the effective dihedral $C_{l\beta}$ were very small at both Mach numbers.

Effects of tail plan form.- The effects of horizontal-tail plan form on the sideslip derivatives of the wing-off configuration at $M = 2.01$ were small (fig. 21). The slightly higher values of $C_{n\beta}$ and $-C_{Y\beta}$ for the unswept tail indicate an increase in the end-plate effect.

Effects of Vertical-Tail Airfoil Section

The vertical tail had a wedge-slab airfoil section to permit changes of vertical location and incidence angle of the horizontal tail. In order to determine the effects of airfoil section on the sideslip characteristics, a vertical tail with the same plan form and a 65A004 airfoil section (fig. 2(b)) was tested at $M = 2.01$ with the configuration having a high wing and low horizontal tail. The results (fig. 22) indicated that altering the airfoil section had no significant effects on the sideslip characteristics of this configuration.

CONCLUSIONS

The results of an investigation of the effects of wing and tail height on the static lateral and directional stability characteristics of a trapezoidal-wing airplane at Mach numbers of 1.41 and 2.01 indicated the following conclusions:

1. In general, the directional stability is increased for the low-wing configurations and decreased for the high-wing configurations, primarily as a result of the induced sidewash effects on the vertical tail.
2. The use of the high wing provided a positive dihedral effect, whereas the use of the low wing provided a negative dihedral effect for the configuration, either with or without the vertical tail.
3. The effects of wing vertical position on the directional stability and effective dihedral were, in general, the same as those obtained at subsonic speeds, and for a similar configuration having a 45° swept wing at supersonic speeds.

4. Addition of the horizontal tail in any location resulted in increased directional stability and had significant effects on the rolling-moment characteristics. The high horizontal tail produced larger increments of directional stability and effective dihedral than the low tail.

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21. Foster, Gerald V.: Investigation of the Longitudinal Aerodynamic Characteristics of a Trapezoidal-Wing Airplane Model With Various Vertical Positions of Wing and Horizontal Tail at Mach Numbers of 1.41 and 2.01. NACA RM L58A07, 1958.
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TABLE I.- MODEL DIMENSIONS

	Unswept	45° Swept
Wing:		
Area, sq in.	192	144
Span, in.	24	24
Root chord, in.	12.80	10
Tip chord, in.	3.20	2
Taper ratio	0.25	0.20
Aspect ratio	3.00	4.00
Mean geometric chord, in.	8.96	6.89
Spanwise location of M.G.C., in.	4.80	4.67
Incidence, deg	0	0
Sweep of leading edge, deg	30.97	49.40
Sweep of 0.75-chord line, deg	0	-----
Sweep of 0.25-chord line, deg	-----	45.0
Section	4-percent circular arc	NACA 65A004
Horizontal tail:		
Area, sq in.	28.6	28.6
Span, in.	10.73	10.73
Root chord, in.	3.35	3.35
Tip chord, in.	2.01	2.01
Taper ratio	0.6	0.6
Aspect ratio	4	4
Sweep of quarter-chord line, deg	-----	45.0
Sweep of leading edge, deg	10.62	-----
Section	NACA 65A004	NACA 65A006
Vertical tail (excluding ventral fin):		
Area to body center line, sq in.		41.9
Span from body center line, in.		7.29
Root chord, in.		8.17
Tip chord, in.		3.44
Taper ratio		0.42
Aspect ratio		1.27
Sweep of leading edge, deg		34.8
Section (slab)	Wedge nose, slab side with constant thickness of 0.437 in.	65A004
Section (airfoil)		
Ventral fin:		
Exposed area, sq in.		8.54
Tip chord, in.		3.25
Sweep of leading edge, deg		70.1
Section	Same as slab vertical tail	
Body:		
Length, in.		36.64
Diameter (maximum), in.		3.33
Diameter (base), in.		2.69
Length-diameter ratio		11.00

TABLE II.- FUSELAGE COORDINATES

Longitudinal station, in.	Radius, in.
0	0
2.000	.530
4.000	.956
6.000	1.280
8.000	1.506
10.000	1.634
11.667	1.667
27.750	1.667
36.640	1.344

TABLE III
AERODYNAMIC CHARACTERISTICS IN SIDESLIP FOR VARIOUS ANGLES OF ATTACK.
STABILITY AXES; M = 1.41

Run	Pt.	q	β , deg	α , deg	C_L	C_D	C_m	C_{l_s}	C_{n_w}	C_Y
2	20	623.09	-2.02	.00	.0063	.0062	-.0022	.0000	.0026	.0023
2	19	623.09	.00	.00	.0066	.0062	-.0024	.0000	.0001	-.0009
2	18	623.30	2.02	.00	.0068	.0068	-.0026	.0000	-.0025	-.0033
2	17	623.30	4.03	.00	.0071	.0071	-.0029	.0000	-.0048	-.0065
2	16	623.30	6.04	.00	.0062	.0074	-.0028	.0000	-.0068	-.0113
2	15	623.09	8.08	.00	.0067	.0075	-.0032	.0000	-.0085	-.0176
2	14	623.30	10.09	.00	.0073	.0074	-.0035	.0000	-.0101	-.0254
2	13	623.30	12.14	.00	.0069	.0073	-.0031	.0000	-.0120	-.0354
2	12	623.30	14.14	.00	.0077	.0072	-.0036	.0000	-.0143	-.0453
2	22	623.09	-2.01	4.02	.0141	.0094	.0107	.0001	.0019	.0026
2	23	623.09	-.01	4.03	.0127	.0096	.0106	.0000	-.0004	-.0008
2	24	623.30	2.01	4.03	.0096	.0099	.0109	-.0002	-.0027	-.0038
2	25	623.09	4.02	4.02	.0111	.0113	.0099	-.0003	-.0048	-.0082
2	26	623.30	6.05	4.04	.0109	.0102	.0093	-.0002	-.0068	-.0121
2	27	623.09	8.09	4.03	.0119	.0099	.0086	-.0006	-.0089	-.0191
2	28	623.09	10.11	4.06	.0120	.0106	.0083	-.0007	-.0102	-.0272
2	29	623.09	12.14	4.07	.0133	.0102	.0082	-.0008	-.0119	-.0361
2	30	623.30	14.14	4.05	.0146	.0095	.0083	-.0010	-.0143	-.0467
2	39	623.09	-2.04	8.07	.0191	.0160	.0217	.0002	.0015	.0036
2	38	623.09	.00	8.05	.0179	.0157	.0215	-.0001	-.0007	-.0001
2	37	623.09	2.03	8.08	.0191	.0163	.0211	-.0004	-.0026	-.0044
2	36	623.09	4.03	8.08	.0191	.0163	.0206	-.0007	-.0047	-.0101
2	35	623.09	6.06	8.07	.0202	.0165	.0200	-.0009	-.0065	-.0151
2	34	623.52	8.07	8.07	.0192	.0217	.0197	-.0012	-.0083	-.0216
2	33	623.09	10.25	7.90	.0211	.0221	.0189	-.0014	-.0102	-.0312
2	32	622.01	12.12	8.09	.0228	.0227	.0196	-.0018	-.0125	-.0386
2	31	623.95	14.15	8.08	.0258	.0242	.0186	-.0020	-.0138	-.0513
2	40	623.74	-2.01	12.10	.0345	.0215	.0307	.0003	.0013	.0048
2	41	623.30	-.02	12.12	.0334	.0213	.0308	-.0001	-.0005	-.0010
2	42	623.09	1.99	12.10	.0336	.0213	.0303	-.0005	-.0024	-.0062
2	43	623.09	4.02	12.14	.0334	.0213	.0302	-.0009	-.0043	-.0122
2	44	623.30	6.06	12.12	.0353	.0219	.0299	-.0013	-.0063	-.0188
2	45	623.09	8.09	12.12	.0354	.0219	.0309	-.0018	-.0084	-.0263
2	46	623.09	10.10	12.11	.0385	.0227	.0298	-.0022	-.0101	-.0348
4	18	622.66	-2.04	8.07	.0212	.0104	.0213	.0002	.0015	.0036
4	17	622.66	.00	8.06	.0200	.0107	.0213	-.0001	-.0007	-.0001
4	16	622.87	2.03	8.08	.0199	.0106	.0210	-.0004	-.0028	-.0043
4	15	622.66	4.05	8.08	.0212	.0106	.0202	-.0007	-.0047	-.0095
4	14	622.66	6.06	8.07	.0222	.0109	.0193	-.0009	-.0066	-.0144
4	13	622.22	8.07	8.07	.0234	.0107	.0186	-.0012	-.0084	-.0209
4	12	621.14	10.25	7.90	.0240	.0102	.0179	-.0014	-.0103	-.0297
4	11	623.09	12.12	8.09	.0258	.0107	.0189	-.0018	-.0126	-.0385
4	10	621.14	14.15	8.08	.0293	.0108	.0180	-.0020	-.0138	-.0509
4	19	622.87	-2.01	12.09	.0371	.0154	.0304	.0003	.0014	.0048
4	20	622.44	.00	12.11	.0361	.0152	.0304	-.0001	-.0007	-.0002
4	21	622.44	2.01	12.09	.0363	.0151	.0301	-.0005	-.0025	-.0062
4	23	622.66	4.04	12.12	.0361	.0151	.0300	-.0010	-.0046	-.0114
4	24	622.66	6.06	12.12	.0380	.0153	.0295	-.0014	-.0064	-.0180
4	25	622.66	8.08	12.11	.0381	.0153	.0303	-.0018	-.0085	-.0256
4	26	622.66	10.10	12.11	.0413	.0158	.0291	-.0021	-.0100	-.0349

TABLE III - Continued
 AERODYNAMIC CHARACTERISTICS IN SIDESLIP FOR VARIOUS ANGLES OF ATTACK.
 STABILITY AXES; M = 1.41

Run	Pt.	q	β , deg	α , deg	C_L	C_D	C_m	C_{L_s}	$C_{n,w}$	C_y
5	26	622.01	-2.04	.00	-.0312	.0186	.0122	.0017	.0024	.0061
5	25	622.22	-1.01	.00	-.0326	.0186	.0118	.0004	.0012	.0026
5	24	622.01	-.01	.00	-.0327	.0186	.0115	-.0008	.0000	-.0010
5	23	622.01	1.01	.00	-.0328	.0186	.0117	-.0021	-.0013	-.0036
5	22	622.22	2.03	.00	-.0342	.0185	.0125	-.0034	-.0025	-.0071
5	21	621.79	3.04	.00	-.0342	.0186	.0134	-.0045	-.0037	-.0106
5	20	622.44	4.04	.00	-.0354	.0186	.0154	-.0057	-.0048	-.0142
5	19	620.93	6.07	-.01	-.0382	.0190	.0197	-.0080	-.0069	-.0214
5	18	622.44	8.10	.00	-.0418	.0188	.0252	-.0102	-.0087	-.0298
5	17	622.01	10.12	.00	-.0442	.0192	.0297	-.0124	-.0105	-.0407
5	16	622.44	12.17	.00	-.0454	.0188	.0318	-.0146	-.0121	-.0523
5	15	622.01	14.19	.00	-.0429	.0186	.0304	-.0166	-.0139	-.0654
5	27	622.66	-1.38	4.63	.2684	.0411	-.0348	.0013	.0007	.0047
5	28	622.01	.00	4.35	.2461	.0375	-.0310	-.0006	-.0003	-.0004
5	29	622.44	2.13	4.26	.2337	.0367	-.0273	-.0040	-.0016	-.0096
5	30	622.44	4.18	4.18	.2264	.0358	-.0233	-.0073	-.0032	-.0183
5	31	622.44	6.20	4.14	.2209	.0351	-.0186	-.0098	-.0049	-.0275
5	32	622.87	8.22	4.10	.2169	.0351	-.0140	-.0125	-.0067	-.0369
5	33	622.22	10.24	4.11	.2146	.0346	-.0105	-.0151	-.0088	-.0475
5	34	622.22	12.29	4.10	.2115	.0342	-.0078	-.0174	-.0109	-.0595
5	35	622.22	14.27	4.09	.2105	.0335	-.0073	-.0196	-.0136	-.0713
5	44	622.22	-2.17	8.65	.4955	.0942	-.0739	.0019	.0008	.0107
5	43	622.44	.00	8.67	.4899	.0936	-.0728	-.0007	-.0004	.0007
5	42	622.22	2.16	8.65	.4848	.0930	-.0715	-.0036	-.0015	-.0099
5	41	622.44	4.28	8.58	.4841	.0923	-.0703	-.0059	-.0028	-.0198
5	40	622.22	6.35	8.46	.4778	.0902	-.0670	-.0088	-.0043	-.0307
5	39	622.22	8.40	8.40	.4720	.0887	-.0625	-.0115	-.0063	-.0413
5	38	622.44	10.56	8.17	.4548	.0843	-.0551	-.0141	-.0086	-.0536
5	37	622.66	12.46	8.32	.4604	.0854	-.0522	-.0165	-.0111	-.0654
5	36	622.44	14.45	8.26	.4555	.0841	-.0493	-.0183	-.0123	-.0829
5	45	622.22	-4.32	12.95	.7203	.1829	-.1143	.0029	.0020	.0246
5	46	622.44	-2.38	12.98	.7155	.1823	-.1139	.0010	.0005	.0135
5	47	622.22	-.02	13.01	.7117	.1820	-.1135	-.0007	-.0004	.0011
5	48	622.22	2.16	12.97	.7077	.1805	-.1128	-.0024	-.0013	-.0110
5	49	622.22	4.31	12.93	.7045	.1790	-.1113	-.0046	-.0030	-.0219
5	50	622.22	6.43	12.84	.7008	.1773	-.1084	-.0068	-.0047	-.0336
5	51	622.22	8.51	12.74	.6952	.1746	-.1035	-.0089	-.0066	-.0458
5	52	623.09	10.57	12.67	.6872	.1712	-.0985	-.0119	-.0078	-.0602
6	28	622.87	-3.03	-.01	-.0081	.0182	-.0053	-.0044	.0034	.0103
6	27	622.44	-2.04	.00	-.0086	.0182	-.0040	-.0032	.0023	.0067
6	26	622.87	-1.01	.00	-.0092	.0183	-.0033	-.0020	.0012	.0033
6	25	623.09	.01	.00	-.0097	.0184	-.0030	-.0009	.0001	-.0001
6	24	622.66	1.01	.00	-.0090	.0183	-.0034	.0002	-.0010	-.0035
6	23	623.09	2.03	.01	-.0097	.0182	-.0040	.0013	-.0022	-.0068
6	22	622.66	3.03	.01	-.0090	.0186	-.0054	.0024	-.0032	-.0104
6	21	622.87	4.04	.01	-.0085	.0187	-.0073	.0036	-.0043	-.0138
6	20	622.66	6.07	.00	-.0088	.0189	-.0115	.0060	-.0063	-.0215
6	19	623.09	8.10	.01	-.0064	.0193	-.0173	.0083	-.0081	-.0305
6	18	622.44	10.12	.02	-.0063	.0192	-.0217	.0105	-.0100	-.0412
6	17	622.44	12.17	.00	-.0101	.0194	-.0238	.0128	-.0120	-.0526
6	16	622.44	14.19	.00	-.0163	.0190	-.0235	.0152	-.0139	-.0669
6	29	622.66	-2.14	4.29	.2741	.0385	-.0475	-.0017	.0024	.0058
6	30	622.66	.00	4.35	.2681	.0382	-.0459	.0002	-.0006	.0004
6	31	622.66	2.14	4.28	.2619	.0376	-.0458	.0015	-.0032	-.0048
6	32	622.87	4.18	4.18	.2561	.0373	-.0465	.0027	-.0058	-.0097
6	33	623.09	6.20	4.12	.2533	.0373	-.0499	.0042	-.0080	-.0166
6	34	622.66	8.21	4.10	.2533	.0373	-.0550	.0061	-.0100	-.0251
6	35	623.52	10.25	4.09	.2520	.0366	-.0583	.0080	-.0115	-.0351
6	36	623.52	12.25	4.08	.2452	.0364	-.0599	.0100	-.0128	-.0471
6	37	622.22	14.23	4.07	.2360	.0355	-.0578	.0124	-.0138	-.0617
6	46	623.30	-2.16	8.68	.5242	.0971	-.0876	-.0012	.0023	.0061
6	45	623.74	-.02	8.70	.5191	.0965	-.0863	.0002	-.0009	.0015
6	44	623.52	2.18	8.67	.5174	.0964	-.0872	.0011	-.0041	-.0023
6	43	623.30	4.30	8.58	.5141	.0953	-.0886	.0020	-.0066	-.0077
6	42	623.52	6.37	8.49	.5115	.0941	-.0914	.0032	-.0092	-.0132
6	41	623.52	8.38	8.41	.5083	.0928	-.0953	.0048	-.0110	-.0218
6	40	622.87	10.53	8.15	.4893	.0879	-.0951	.0068	-.0125	-.0329
6	39	623.30	12.40	8.28	.4925	.0893	-.0955	.0087	-.0133	-.0446
6	38	623.30	14.39	8.22	.4788	.0866	-.0928	.0110	-.0133	-.0595
6	54	618.12	-.02	13.05	.7486	.1896	-.1183	.0001	-.0014	-.0033
6	49	623.09	2.14	13.02	.7450	.1885	-.1200	.0007	-.0045	-.0012
6	50	622.87	4.33	12.97	.7432	.1876	-.1229	.0015	-.0073	-.0062
6	51	623.09	6.44	12.87	.7403	.1858	-.1259	.0023	-.0097	-.0136
6	52	623.09	8.54	12.78	.7365	.1839	-.1292	.0032	-.0122	-.0213
6	53	623.09	10.55	12.64	.7280	.1795	-.1315	.0046	-.0138	-.0301

TABLE III - Continued
 AERODYNAMIC CHARACTERISTICS IN SIDESLIP FOR VARIOUS ANGLES OF ATTACK.
 STABILITY AXES; M = 1.41

Run	Pt.	q	β , deg	α , deg	C_L	C_D	C_m	$C_{l,s}$	$C_{n,w}$	C_y
7	27	623.74	-4.04	.00	-.0155	.0163	.0029	-.0013	.0041	.0071
7	26	623.52	-2.01	.00	-.0164	.0156	.0030	-.0014	.0021	.0031
7	25	623.52	-1.01	.00	-.0163	.0156	.0031	-.0015	.0011	.0018
7	24	623.52	.00	.00	-.0160	.0156	.0032	-.0015	.0000	-.0002
7	23	623.52	1.02	.00	-.0158	.0156	.0031	-.0016	-.0010	-.0022
7	22	623.30	2.01	.00	-.0157	.0158	.0031	-.0016	-.0022	-.0034
7	21	623.30	4.02	.00	-.0152	.0160	.0031	-.0017	-.0041	-.0075
7	20	623.52	6.06	.00	-.0161	.0164	.0032	-.0017	-.0058	-.0131
7	19	623.30	8.08	.00	-.0169	.0162	.0035	-.0017	-.0074	-.0186
7	18	623.09	10.09	.00	-.0163	.0163	.0031	-.0017	-.0089	-.0265
7	17	623.09	12.13	.00	-.0156	.0165	.0028	-.0016	-.0105	-.0358
7	16	622.44	14.15	.00	-.0204	.0160	.0030	-.0013	-.0127	-.0472
7	29	623.30	-4.18	4.18	.2664	.0359	-.0415	-.0005	.0038	.0075
7	30	623.30	-2.14	4.28	.2619	.0353	-.0398	-.0007	.0018	.0037
7	31	623.30	-.01	4.34	.2561	.0353	-.0389	-.0010	-.0002	-.0004
7	32	623.30	2.13	4.27	.2477	.0349	-.0365	-.0021	-.0020	-.0043
7	33	623.52	4.18	4.18	.2435	.0344	-.0356	-.0028	-.0038	-.0086
7	34	623.52	6.18	4.11	.2414	.0341	-.0354	-.0032	-.0055	-.0141
7	35	623.30	8.19	4.10	.2404	.0341	-.0356	-.0034	-.0072	-.0197
7	36	623.09	10.22	4.08	.2386	.0342	-.0350	-.0038	-.0088	-.0276
7	37	623.30	12.23	4.08	.2349	.0337	-.0339	-.0042	-.0105	-.0374
7	38	623.30	14.22	4.07	.2309	.0332	-.0321	-.0042	-.0125	-.0486
7	48	623.74	-4.30	8.58	.5145	.0931	-.0844	-.0006	.0040	.0095
7	47	623.52	-2.18	8.66	.5086	.0930	-.0814	-.0007	.0019	.0040
7	46	623.52	-.02	8.69	.5038	.0926	-.0803	-.0010	-.0003	-.0001
7	45	623.74	2.18	8.67	.5018	.0922	-.0801	-.0016	-.0022	-.0040
7	44	623.74	4.29	8.57	.5005	.0915	-.0810	-.0020	-.0042	-.0087
7	43	623.52	6.34	8.48	.4999	.0909	-.0810	-.0026	-.0058	-.0143
7	42	623.52	8.39	8.39	.4963	.0897	-.0793	-.0032	-.0075	-.0207
7	41	623.74	10.54	8.13	.4913	.0850	-.0752	-.0037	-.0092	-.0295
7	40	623.52	12.41	8.29	.4852	.0867	-.0737	-.0039	-.0110	-.0393
7	39	623.52	14.39	8.22	.4758	.0849	-.0708	-.0038	-.0118	-.0533
7	49	623.09	-4.35	12.95	.7413	.1846	-.1231	-.0003	.0048	.0094
7	50	623.52	-2.16	13.00	.7372	.1847	-.1210	-.0007	.0021	.0051
7	51	623.52	.00	13.04	.7329	.1843	-.1196	-.0011	-.0002	.0003
7	52	623.52	2.16	12.99	.7313	.1832	-.1199	-.0016	-.0026	-.0043
7	53	623.52	4.30	12.96	.7300	.1830	-.1215	-.0019	-.0049	-.0092
7	54	623.74	6.43	12.86	.7285	.1811	-.1208	-.0023	-.0069	-.0151
7	55	623.74	8.52	12.76	.7213	.1781	-.1166	-.0028	-.0088	-.0229
7	56	623.52	10.56	12.66	.7124	.1748	-.1126	-.0037	-.0100	-.0309
8	26	624.82	-3.94	.05	-.0193	.0308	.0160	.0041	-.0286	.0637
8	25	624.39	-1.98	.01	-.0206	.0317	.0152	.0013	-.0146	.0327
8	24	623.52	-.99	.00	-.0225	.0317	.0155	-.0001	-.0078	.0174
8	23	623.09	-.01	.00	-.0219	.0309	.0151	-.0014	-.0009	.0018
8	22	624.82	.99	.00	-.0226	.0310	.0153	-.0027	.0060	-.0130
8	21	623.52	1.97	.00	-.0219	.0312	.0157	-.0041	.0127	-.0280
8	20	623.95	3.94	.00	-.0229	.0306	.0164	-.0069	.0272	-.0601
8	19	625.25	5.91	.00	-.0227	.0303	.0164	-.0095	.0416	-.0928
8	18	625.25	7.90	.01	-.0225	.0296	.0157	-.0121	.0566	-.1279
8	17	625.03	9.88	.00	-.0224	.0287	.0148	-.0145	.0714	-.1638
8	16	624.39	11.87	.00	-.0237	.0280	.0141	-.0169	.0849	-.1989
8	27	624.82	-4.15	4.15	.2631	.0491	-.0314	.0026	-.0288	.0631
8	28	624.82	-2.14	4.28	.2578	.0493	-.0295	.0007	-.0132	.0287
8	29	624.39	-.01	4.36	.2521	.0495	-.0287	-.0014	.0020	-.0039
8	30	624.39	2.12	4.26	.2432	.0485	-.0264	-.0039	.0165	-.0353
8	31	624.39	4.13	4.13	.2392	.0475	-.0256	-.0061	.0307	-.0666
8	32	624.60	6.08	4.05	.2359	.0469	-.0255	-.0081	.0451	-.0992
8	33	624.39	8.06	4.02	.2364	.0460	-.0266	-.0098	.0602	-.1340
8	34	624.17	10.04	4.01	.2370	.0455	-.0270	-.0116	.0748	-.1693
8	35	624.39	12.00	4.00	.2328	.0438	-.0259	-.0132	.0887	-.2048
8	36	624.17	13.95	3.99	.2279	.0433	-.0236	-.0144	.0993	-.2367
8	46	624.39	-4.29	8.56	.5083	.1050	-.0750	.0001	-.0275	.0624
8	45	624.39	-2.18	8.67	.5016	.1060	-.0717	-.0004	-.0130	.0259
8	44	624.39	-.02	8.69	.4970	.1056	-.0705	-.0010	.0016	-.0027
8	43	624.60	2.18	8.66	.4947	.1051	-.0705	-.0018	.0157	-.0346
8	42	625.25	4.29	8.55	.4941	.1035	-.0721	-.0028	.0300	-.0658
8	41	624.17	6.30	8.42	.4938	.1017	-.0730	-.0038	.0450	-.0998
8	40	624.17	8.30	8.30	.4906	.0999	-.0723	-.0048	.0593	-.1344
8	39	624.17	10.40	8.01	.4761	.0946	-.0690	-.0058	.0752	-.1724
8	38	624.39	12.23	8.16	.4811	.0959	-.0681	-.0061	.0957	-.2019
8	37	624.17	14.17	8.09	.4726	.0937	-.0657	-.0062	.1000	-.2401
8	47	624.17	-4.32	12.96	.7332	.1943	-.1140	-.0021	-.0252	.0606
8	48	624.60	-2.16	13.00	.7273	.1959	-.1109	-.0016	-.0115	.0286
8	49	624.82	.00	13.05	.7245	.1961	-.1095	-.0011	.0018	-.0031
8	50	624.60	2.16	13.00	.7225	.1951	-.1105	-.0007	.0152	-.0346
8	51	624.39	4.31	12.93	.7224	.1932	-.1130	-.0001	.0288	-.0667
8	52	624.39	6.38	12.82	.7214	.1904	-.1136	.0001	.0415	-.0979
8	53	624.82	8.47	12.68	.7166	.1871	-.1114	.0002	.0545	-.1297
8	54	624.60	10.47	12.55	.7094	.1828	-.1081	-.0001	.0687	-.1641

TABLE III - Continued
 AERODYNAMIC CHARACTERISTICS IN SIDESLIP FOR VARIOUS ANGLES OF ATTACK.
 STABILITY AXES; M = 1.41

Run	Pt.	q	β , deg	α , deg	C_L	C_D	C_m	$C_{l,s}$	$C_{n,w}$	C_Y
9	26	625.25	-3.95	-0.1	-0.0378	0.0343	0.0461	0.0053	-0.0299	0.0660
9	25	625.90	-1.98	0.01	-0.0383	0.0343	0.0471	0.0018	-0.0150	0.0335
9	24	625.25	-0.99	0.00	-0.0400	0.0340	0.0475	0.0002	-0.0077	0.0174
9	23	625.03	0.00	0.00	-0.0393	0.0340	0.0471	-0.0013	-0.0340	0.0254
9	22	625.03	0.99	0.00	-0.0396	0.0337	0.0473	0.0029	0.0059	-0.0131
9	21	625.25	1.98	0.00	-0.0400	0.0342	0.0478	-0.0045	0.0131	-0.0288
9	20	625.25	3.94	0.00	-0.0381	0.0341	0.0462	-0.0079	0.0279	-0.0616
9	19	625.25	5.91	0.00	-0.0363	0.0339	0.0424	-0.0112	0.0433	-0.0961
9	18	625.47	7.90	0.00	-0.0345	0.0326	0.0383	-0.0144	0.0595	-0.1329
9	17	625.47	9.86	0.00	-0.0302	0.0316	0.0325	-0.0175	0.0752	-0.1697
9	16	625.25	11.85	0.00	-0.0260	0.0308	0.0264	-0.0204	0.0895	-0.2070
9	27	625.25	-4.14	4.14	0.2766	0.0530	-0.0542	0.0039	-0.0328	0.0696
9	28	625.25	-2.13	4.26	0.2888	0.0527	-0.0487	0.0013	-0.0353	0.0321
9	29	625.68	0.00	4.35	0.2593	0.0524	-0.0443	-0.0014	0.0020	-0.0038
9	30	625.25	2.12	4.25	0.2535	0.0518	-0.0428	-0.0045	0.0182	-0.0380
9	31	625.47	4.13	4.13	0.2512	0.0514	-0.0444	-0.0074	0.0340	-0.0713
9	32	625.25	6.08	4.06	0.2503	0.0508	-0.0459	-0.0099	0.0497	-0.1064
9	33	625.47	8.03	4.02	0.2513	0.0496	-0.0487	-0.0124	0.0659	-0.1430
9	34	625.25	10.01	3.99	0.2524	0.0484	-0.0519	-0.0147	0.0815	-0.1802
9	35	625.47	11.98	4.01	0.2523	0.0480	-0.0550	-0.0167	0.0961	-0.2172
9	36	625.25	13.93	3.99	0.2486	0.0468	-0.0569	-0.0182	0.1062	-0.2492
9	46	625.47	-4.26	8.50	0.5422	0.1122	-0.1381	0.0013	-0.0330	0.0712
9	45	625.25	-2.16	8.62	0.5382	0.1137	-0.1365	0.0004	-0.0163	0.0346
9	44	625.25	0.00	8.64	0.5326	0.1130	-0.1340	-0.0010	0.0016	-0.0023
9	43	625.25	2.16	8.61	0.5296	0.1121	-0.1333	-0.0025	0.0190	-0.0386
9	42	625.25	4.26	8.49	0.5306	0.1107	-0.1341	-0.0039	0.0348	-0.0733
9	41	625.25	6.27	8.38	0.5289	0.1092	-0.1350	-0.0055	0.0517	-0.1099
9	40	625.47	8.27	8.27	0.5277	0.1071	-0.1348	-0.0068	0.0683	-0.1472
9	39	625.25	10.35	7.98	0.5177	0.1014	-0.1295	-0.0086	0.0843	-0.1862
9	38	625.25	12.18	8.13	0.5182	0.1033	-0.1317	-0.0091	0.0949	-0.2166
9	37	625.47	14.12	8.10	0.5122	0.1011	-0.1310	-0.0096	0.1078	-0.2536
9	47	625.25	-4.29	12.86	0.7847	0.2093	-0.2079	-0.0011	-0.0306	0.0696
9	48	625.25	-2.15	12.92	0.7839	0.2105	-0.2113	-0.0011	-0.0142	0.0326
9	49	625.68	0.00	12.96	0.7821	0.2102	-0.2129	-0.0011	0.0019	-0.0033
9	50	625.47	2.15	12.93	0.7765	0.2087	-0.2086	-0.0013	0.0180	-0.0391
9	51	625.47	4.29	12.85	0.7728	0.2062	-0.2040	-0.0011	0.0340	-0.0754
9	52	625.47	6.37	12.74	0.7691	0.2026	-0.1998	-0.0012	0.0483	-0.1086
9	53	625.25	8.43	12.63	0.7654	0.1994	-0.1990	-0.0012	0.0619	-0.1421
10	26	623.74	-2.96	0.00	-0.0812	0.0418	0.1285	0.0032	-0.0211	0.0479
10	25	623.74	-1.98	0.00	-0.0830	0.0416	0.1296	0.0017	-0.0142	0.0325
10	24	623.95	-0.98	0.00	-0.0835	0.0413	0.1300	0.0001	-0.0076	0.0176
10	23	624.17	0.00	0.00	-0.0826	0.0401	0.1301	-0.0013	-0.0007	0.0020
10	22	623.95	0.98	0.00	-0.0832	0.0400	0.1305	-0.0028	0.0058	-0.0128
10	21	623.95	1.98	0.00	-0.0825	0.0406	0.1301	-0.0042	0.0126	-0.0282
10	20	623.95	2.98	0.00	-0.0817	0.0412	0.1291	-0.0058	0.0192	-0.0431
10	19	624.17	3.95	0.00	-0.0809	0.0407	0.1273	-0.0073	0.0264	-0.0595
10	18	623.95	5.92	0.00	-0.0794	0.0402	0.1249	-0.0103	0.0409	-0.0930
10	17	623.95	7.91	0.00	-0.0780	0.0389	0.1208	-0.0132	0.0559	-0.1274
10	16	624.17	9.86	0.00	-0.0739	0.0376	0.1146	-0.0163	0.0707	-0.1640
10	15	624.17	11.88	0.00	-0.0700	0.0365	0.1075	-0.0188	0.0849	-0.2004
10	14	624.17	13.86	0.00	-0.0665	0.0355	0.0999	-0.0212	0.0967	-0.2356
10	27	623.52	-4.19	4.18	0.2285	0.0539	0.0338	0.0032	-0.0289	0.0637
10	28	623.95	-2.16	4.32	0.2225	0.0539	0.0374	-0.0010	-0.0132	0.0288
10	29	624.17	0.00	4.42	0.2162	0.0545	0.0400	-0.0012	0.0017	-0.0035
10	30	623.52	2.15	4.31	0.2086	0.0536	0.0424	-0.0040	0.0158	-0.0342
10	31	624.82	4.16	4.18	0.2031	0.0528	0.0428	-0.0066	0.0299	-0.0655
10	32	624.17	6.12	4.07	0.2034	0.0516	0.0407	-0.0090	0.0450	-0.0992
10	33	623.30	8.08	4.03	0.2031	0.0503	0.0378	-0.0113	0.0604	-0.1351
10	34	623.95	10.05	4.03	0.2062	0.0497	0.0333	-0.0135	0.0755	-0.1710
10	35	624.60	12.02	4.00	0.2045	0.0484	0.0295	-0.0154	0.0893	-0.2072
10	36	623.74	13.97	4.00	0.2023	0.0472	0.0271	-0.0169	0.0998	-0.2393
10	46	624.39	-4.31	8.56	0.4963	0.1075	-0.0522	0.0007	-0.0286	0.0644
10	45	623.95	-2.18	8.69	0.4896	0.1083	-0.0476	-0.0001	-0.0137	0.0306
10	44	624.17	0.00	8.72	0.4842	0.1078	-0.0452	-0.0009	0.0012	-0.0023
10	43	624.60	2.18	8.69	0.4836	0.1078	-0.0457	-0.0020	0.0159	-0.0347
10	42	624.17	4.29	8.56	0.4819	0.1058	-0.0471	-0.0033	0.0303	-0.0669
10	41	623.74	6.32	8.43	0.4805	0.1036	-0.0483	-0.0048	0.0462	-0.1019
10	40	623.30	8.31	8.31	0.4794	0.1021	-0.0481	-0.0062	0.0617	-0.1375
10	39	623.52	10.41	8.02	0.4641	0.0969	-0.0439	-0.0080	0.0773	-0.1756
10	38	623.52	12.22	8.19	0.4719	0.0985	-0.0476	-0.0087	0.0872	-0.2051
10	37	623.52	14.16	8.12	0.4673	0.0963	-0.0495	-0.0091	0.1012	-0.2432
10	47	623.95	-4.34	12.94	0.7372	0.1988	-0.1199	-0.0010	-0.0274	0.0639
10	48	623.95	-2.17	13.01	0.7341	0.1996	-0.1174	-0.0011	-0.0126	0.0295
10	49	624.17	0.00	13.03	0.7297	0.1990	-0.1144	-0.0011	0.0017	-0.0030
10	50	624.17	2.16	13.00	0.7267	0.1980	-0.1153	-0.0009	0.0162	-0.0363
10	51	623.95	4.31	12.93	0.7250	0.1961	-0.1161	-0.0008	0.0305	-0.0700
10	52	624.17	6.38	12.82	0.7242	0.1936	-0.1164	-0.0010	0.0435	-0.1013
10	53	624.17	8.47	12.68	0.7215	0.1898	-0.1177	-0.0013	0.0567	-0.1340
10	54	623.95	10.45	12.57	0.7157	0.1861	-0.1180	-0.0019	0.0713	-0.1685

TABLE III - Continued
 AERODYNAMIC CHARACTERISTICS IN SIDESLIP FOR VARIOUS ANGLES OF ATTACK.

STABILITY AXES: M = 1.41

Run	Pt.	q	β , deg	α , deg	C_L	C_D	C_m	$C_{l,s}$	$C_{n,w}$	C_Y
11	28	622.87	-2.95	.01	-.0687	.0384	.1079	.0013	-.0283	.0578
11	27	622.87	-1.96	.00	-.0707	.0387	.1091	.0003	-.0187	.0379
11	26	623.09	-.98	.00	-.0714	.0390	.1096	-.0005	-.0095	.0189
11	25	622.87	.01	.00	-.0711	.0387	.1095	-.0014	-.0010	.0014
11	24	622.87	.97	.00	-.0707	.0388	.1090	-.0021	.0077	-.0168
11	23	622.87	1.98	.00	-.0689	.0389	.1081	-.0030	.0165	-.0350
11	22	622.87	2.95	.01	-.0684	.0396	.1074	-.0039	.0255	-.0541
11	21	622.87	3.93	.00	-.0680	.0392	.1066	-.0048	.0343	-.0724
11	20	621.79	5.88	.00	-.0671	.0388	.1055	-.0066	.0528	-.1115
11	19	623.09	7.87	.00	-.0671	.0377	.1049	-.0084	.0707	-.1509
11	18	623.30	9.82	.00	-.0668	.0369	.1055	-.0104	.0884	-.1911
11	17	622.66	11.81	.00	-.0680	.0363	.1071	-.0124	.1046	-.2304
11	16	622.87	13.78	.00	-.0720	.0358	.1116	-.0141	.1173	-.2666
11	29	622.87	-4.16	4.16	.2419	.0518	.0126	.0003	-.0358	.0735
11	30	622.87	-2.04	4.31	.2803	.0523	.0152	-.0001	-.0166	.0323
11	31	622.87	-.01	4.39	.2530	.0518	.0112	-.0001	-.0166	-.0042
11	32	622.87	2.13	4.28	.2246	.0509	.0152	-.0023	.0199	-.0404
11	33	622.87	4.15	4.15	.2192	.0506	.0182	-.0033	.0378	-.0781
11	34	622.87	6.08	4.06	.2145	.0501	.0209	-.0041	.0550	-.1146
11	35	622.87	8.04	4.03	.2125	.0486	.0232	-.0052	.0726	-.1539
11	36	622.87	10.02	4.00	.2094	.0484	.0272	-.0064	.0902	-.1938
11	37	623.09	11.97	3.98	.2055	.0473	.0320	-.0075	.1064	-.2337
11	45	622.44	-4.28	8.54	.5121	.1071	-.0777	-.0016	-.0314	.0677
11	44	622.44	-2.18	8.66	.5080	.1079	-.0769	-.0012	-.0149	.0326
11	43	622.44	.00	8.69	.5032	.1076	-.0762	-.0009	.0018	-.0035
11	42	622.44	2.16	8.66	.5022	.1072	-.0765	-.0007	.0176	-.0374
11	41	622.66	4.28	8.54	.5007	.1056	-.0763	-.0006	.0337	-.0724
11	40	622.44	6.31	8.40	.4973	.1038	-.0728	-.0005	.0509	-.1094
11	39	622.66	8.29	8.32	.4926	.1023	-.0666	-.0003	.0682	-.1485
11	38	622.44	10.39	8.01	.4722	.0964	-.0550	-.0005	.0866	-.1905
11	46	622.66	-4.31	12.92	.7627	.2010	-.1595	-.0031	-.0269	.0629
11	47	623.09	-2.16	12.97	.7582	.2008	-.1579	-.0019	-.0120	.0283
11	48	622.66	-.02	13.01	.7548	.2005	-.1570	-.0008	.0021	-.0036
11	49	622.44	2.14	12.97	.7525	.1996	-.1572	.0004	.0162	-.0363
11	50	622.44	4.30	12.89	.7511	.1978	-.1580	.0014	.0306	-.0703
11	51	622.87	6.38	12.80	.7483	.1957	-.1562	.0023	.0442	-.1027
11	52	622.66	8.45	12.65	.7406	.1911	-.1486	.0029	.0584	-.1366
11	53	622.66	10.43	12.55	.7307	.1874	-.1390	.0037	.0744	-.1739
12	24	623.09	-3.92	.03	-.0180	.0336	.0195	.0024	-.0336	.0703
12	23	622.87	-1.98	.00	-.0199	.0335	.0171	.0005	-.0171	.0351
12	22	622.87	-.98	.00	-.0182	.0334	.0162	-.0004	-.0090	.0178
12	21	622.87	.00	.00	-.0190	.0335	.0161	-.0005	-.0006	.0005
12	20	623.09	.99	.00	-.0186	.0336	.0162	.0022	.0075	-.0169
12	19	623.30	1.97	.00	-.0181	.0337	.0168	-.0031	.0153	-.0335
12	18	622.87	3.93	.00	-.0209	.0331	.0196	-.0050	.0320	-.0692
12	17	622.87	5.90	.00	-.0211	.0327	.0214	-.0067	.0485	-.1049
12	16	623.52	7.89	.00	-.0224	.0321	.0230	-.0086	.0647	-.1417
12	15	622.87	9.85	.02	-.0224	.0310	.0251	-.0106	.0802	-.1787
12	14	622.22	10.86	.02	-.0297	.0302	.0292	-.0113	.0882	-.1977
12	25	622.87	-4.13	4.13	.2891	.0533	-.0743	.0012	-.0317	.0666
12	26	622.87	-2.12	4.25	.2847	.0541	-.0735	.0002	-.0146	.0306
12	27	622.87	.00	4.32	.2779	.0537	-.0724	-.0011	.0020	-.0044
12	28	622.87	2.12	4.24	.2706	.0526	-.0707	-.0028	.0180	-.0373
12	29	623.30	4.12	4.12	.2664	.0520	-.0688	-.0043	.0336	-.0716
12	30	622.87	6.07	4.04	.2619	.0513	-.0660	-.0054	.0492	-.1064
12	31	622.87	8.04	4.01	.2587	.0503	-.0615	-.0065	.0656	-.1433
12	32	623.09	10.00	3.99	.2552	.0490	-.0557	-.0075	.0814	-.1805
12	33	623.30	11.97	3.99	.2488	.0475	-.0486	-.0086	.0970	-.2188
12	34	620.93	13.92	3.98	.2385	.0463	-.0364	-.0093	.1086	-.2527
12	44	623.30	-4.26	8.49	.5528	.1145	-.1585	-.0007	-.0286	.0639
12	43	622.66	-2.16	8.61	.5481	.1154	-.1568	-.0007	-.0135	.0306
12	42	622.66	.00	8.62	.5447	.1146	-.1565	-.0008	.0013	-.0022
12	41	623.09	2.14	8.60	.5435	.1149	-.1567	.0012	.0160	-.0351
12	40	622.66	4.25	8.48	.5427	.1128	-.1575	-.0015	.0307	-.0676
12	39	622.66	6.28	8.37	.5414	.1108	-.1567	-.0019	.0462	-.1020
12	38	622.66	8.27	8.27	.5381	.1093	-.1534	-.0024	.0617	-.1379
12	37	622.66	10.35	8.01	.5399	.1033	-.1427	-.0027	.0778	-.1771
12	36	622.87	12.19	8.14	.5191	.1033	-.1342	-.0024	.0892	-.2086
12	35	623.09	14.14	8.08	.5070	.1009	-.1226	-.0020	.1044	-.2486
12	45	622.87	-4.31	12.84	.7992	.2127	-.2377	-.0024	-.0253	.0608
12	46	622.87	-2.12	12.90	.7953	.2129	-.2357	-.0016	-.0113	.0279
12	47	622.87	.00	12.94	.7938	.2135	-.2355	-.0009	.0018	-.0031
12	48	622.87	2.12	12.90	.7913	.2122	-.2361	-.0001	.0149	-.0348
12	49	622.66	4.28	12.83	.7888	.2102	-.2378	.0005	.0279	-.0656
12	50	622.66	6.36	12.72	.7880	.2073	-.2373	.0009	.0407	-.0972
12	51	623.09	8.43	12.62	.7819	.2039	-.2316	.0014	.0539	-.1293
12	52	622.87	10.42	12.49	.7711	.1989	-.2238	.0014	.0683	-.1641

TABLE III - Continued
 AERODYNAMIC CHARACTERISTICS IN SIDESLIP FOR VARIOUS ANGLES OF ATTACK.
 STABILITY AXES; M = 1.41

Run	Pt.	q	β , deg	α , deg	C_L	C_D	C_m	C_{L_s}	$C_{n,w}$	C_Y
15	31	625.68	-3.97	.00	-.0500	.0365	.0536	.0089	-.0253	.0642
15	30	625.68	-2.97	.00	-.0498	.0365	.0528	.0066	-.0190	.0480
15	29	625.90	-1.99	.00	-.0496	.0365	.0522	.0041	-.0130	.0326
15	28	625.25	.00	.00	-.0494	.0364	.0514	.0018	-.0070	.0165
15	27	625.25	.00	.00	-.0495	.0365	.0511	-.0006	-.0009	.0012
15	26	625.25	1.00	.00	-.0492	.0364	.0512	-.0030	.0052	-.0142
15	25	625.25	1.99	.00	-.0503	.0364	.0513	-.0053	.0112	-.0297
15	24	625.68	2.97	.00	-.0499	.0359	.0521	-.0077	.0173	-.0459
15	23	625.68	3.96	.00	-.0509	.0358	.0531	-.0102	.0238	-.0621
15	22	625.47	5.95	.01	-.0500	.0356	.0530	-.0151	.0379	-.0978
15	21	625.47	7.94	-.01	-.0494	.0351	.0522	-.0199	.0522	-.1345
15	20	625.68	9.91	.00	-.0484	.0341	.0519	-.0248	.0666	-.1723
15	18	624.17	11.92	.00	-.0460	.0332	.0503	-.0300	.0808	-.2115
15	19	625.25	13.91	.00	-.0438	.0319	.0495	-.0348	.0926	-.2478
15	32	625.90	-4.15	4.15	.2633	.0549	-.0423	.0075	-.0274	.0675
15	33	625.25	-2.13	4.26	.2551	.0544	-.0386	.0054	-.0124	.0299
15	34	625.47	.00	4.34	.2461	.0543	-.0351	-.0007	.0015	-.0237
15	35	625.47	2.12	4.25	.2353	.0529	-.0318	-.0054	.0148	-.0372
15	36	625.25	4.14	4.14	.2317	.0522	-.0314	-.0099	.0281	-.0715
15	37	625.68	6.11	4.07	.2288	.0515	-.0311	-.0142	.0421	-.1069
15	38	625.68	8.09	4.03	.2286	.0509	-.0309	-.0181	.0563	-.1438
15	39	625.25	10.06	4.02	.2300	.0503	-.0309	-.0223	.0701	-.1812
15	40	625.47	12.04	4.03	.2280	.0486	-.0290	-.0264	.0837	-.2195
15	41	626.12	14.02	4.01	.2264	.0478	-.0261	-.0303	.0935	-.2525
15	51	625.47	-4.27	8.52	.5242	.1135	-.1225	.0050	-.0269	.0689
15	50	625.68	-2.16	8.62	.5193	.1140	-.1216	.0023	-.0133	.0338
15	49	625.68	-.02	8.64	.5128	.1130	-.1193	-.0007	.0008	-.0022
15	48	625.47	2.15	8.61	.5117	.1124	-.1200	-.0040	.0146	-.0369
15	47	625.68	4.26	8.49	.5080	.1107	-.1189	-.0069	.0281	-.0717
15	46	625.47	6.30	8.40	.5074	.1086	-.1184	-.0099	.0417	-.1076
15	45	625.25	8.29	8.29	.5048	.1066	-.1166	-.0130	.0553	-.1450
15	44	625.25	10.41	8.02	.4874	.1012	-.1093	-.0164	.0700	-.1858
15	43	625.25	12.27	8.19	.4920	.1025	-.1057	-.0190	.0795	-.2173
15	42	624.60	14.22	8.12	.4890	.1008	-.1019	-.0217	.0931	-.2590
15	52	625.47	-4.30	12.88	.7549	.2060	-.1850	.0020	-.0229	.0654
15	53	625.47	-2.17	12.92	.7532	.2063	-.1877	.0005	-.0102	.0294
15	54	625.47	.00	12.99	.7526	.2063	-.1878	-.0007	.0014	-.0032
15	55	625.25	2.15	12.91	.7462	.2047	-.1862	-.0020	.0132	-.0366
15	56	625.25	4.29	12.86	.7424	.2026	-.1828	-.0034	.0255	-.0713
15	57	625.47	6.39	12.77	.7389	.1999	-.1798	-.0051	.0370	-.1052
15	58	625.25	8.44	12.64	.7372	.1961	-.1795	-.0064	.0484	-.1404
15	59	622.87	10.46	12.54	.7318	.1930	-.1775	-.0089	.0630	-.1806
16	30	623.74	-3.97	.00	-.0893	.0435	.1355	.0086	-.0242	.0642
16	29	623.74	-2.99	.01	-.0893	.0435	.1348	.0063	-.0183	.0486
16	28	623.95	-2.01	.00	-.0893	.0439	.1345	.0041	-.0129	.0343
16	27	623.74	-1.00	.00	-.0891	.0432	.1342	.0016	-.0069	.0189
16	26	623.74	.00	.00	-.0902	.0427	.1346	-.0006	-.0010	.0028
16	25	623.74	1.00	.00	-.0901	.0428	.1344	-.0029	.0049	-.0125
16	24	623.74	1.99	.00	-.0887	.0431	.1336	-.0052	.0105	-.0271
16	23	623.74	2.99	.00	-.0898	.0432	.1342	-.0075	.0164	-.0432
16	22	623.95	3.97	.00	-.0895	.0434	.1346	-.0099	.0226	-.0594
16	21	623.74	5.95	-.01	-.0890	.0425	.1352	-.0145	.0358	-.0935
16	20	623.74	7.94	.00	-.0885	.0418	.1353	-.0190	.0493	-.1289
16	19	623.74	9.92	.00	-.0879	.0406	.1350	-.0237	.0628	-.1652
16	18	623.52	11.93	.00	-.0859	.0392	.1333	-.0285	.0758	-.2022
16	17	623.52	13.92	.00	-.0838	.0381	.1317	-.0333	.0873	-.2381
16	31	623.74	-4.21	4.20	.2191	.0564	.0453	.0070	-.0243	.0642
16	32	623.95	-2.17	4.34	.2126	.0565	.0470	.0032	-.0110	.0291
16	33	623.95	-.01	4.42	.2030	.0561	.0498	-.0007	.0014	-.0027
16	34	623.95	2.15	4.33	.1944	.0549	.0528	-.0051	.0132	-.0342
16	35	623.95	4.19	4.19	.1893	.0542	.0550	-.0094	.0254	-.0666
16	36	623.74	6.15	4.10	.1838	.0530	.0574	-.0133	.0382	-.1003
16	37	623.74	8.12	4.05	.1833	.0523	.0578	-.0171	.0517	-.1361
16	38	623.74	10.09	4.05	.1843	.0511	.0571	-.0212	.0648	-.1724
16	39	623.74	12.09	4.03	.1835	.0501	.0578	-.0253	.0781	-.2100
16	40	623.74	14.04	4.05	.1832	.0489	.0594	-.0291	.0875	-.2422
16	50	624.39	-4.31	9.60	.4769	.1082	-.0339	.0043	-.0237	.0647
16	49	623.95	-2.18	8.69	.4733	.1091	-.0326	.0019	-.0114	.0315
16	48	624.39	.00	8.72	.4671	.1086	-.0308	-.0007	.0006	-.0004
16	47	623.95	2.18	8.68	.4643	.1079	-.0300	-.0035	.0127	-.0332
16	46	623.95	4.30	8.58	.4628	.1065	-.0301	-.0065	.0248	-.0662
16	45	623.95	6.34	8.44	.4606	.1043	-.0296	-.0091	.0375	-.1010
16	44	623.74	8.35	8.35	.4575	.1023	-.0276	-.0122	.0505	-.1367
16	43	624.17	10.46	8.09	.4424	.0975	-.0205	-.0158	.0647	-.1770
16	42	624.17	12.49	8.21	.4456	.0983	-.0187	-.0184	.0739	-.2085
16	41	623.95	14.25	8.14	.4432	.0971	-.0165	-.0212	.0866	-.2483
16	51	623.95	-4.34	12.94	.7131	.1966	-.1039	.0018	-.0218	.0647
16	52	624.17	-2.16	13.00	.7102	.1962	-.1040	.0004	-.0098	.0296
16	53	624.39	.00	13.04	.7070	.1961	-.1034	-.0007	.0006	-.0006
16	54	624.39	2.14	12.98	.7055	.1952	-.1032	-.0020	.0116	-.0322
16	55	624.82	4.30	12.95	.7008	.1940	-.1019	-.0033	.0234	-.0667
16	56	624.60	6.42	12.82	.6967	.1910	-.0971	-.0049	.0346	-.1005
16	57	623.09	8.46	12.72	.6934	.1880	-.0956	-.0063	.0453	-.1342
16	58	624.39	10.50	12.59	.6876	.1844	-.0935	-.0088	.0589	-.1732

TABLE III - Continued
 AERODYNAMIC CHARACTERISTICS IN SIDESLIP FOR VARIOUS ANGLES OF ATTACK.

STABILITY AXES: M = 1.41

Run	Pt.	q	β , deg	α , deg	C_L	C_D	C_m	C_{L_s}	C_{n_w}	C_Y
17	27	625.33	-3.94	0.01	-0.0853	0.0407	0.1145	0.0056	-0.0343	0.0788
17	26	625.68	-1.97	0.00	-0.0870	0.0414	0.1152	0.0024	-0.0176	0.0407
17	25	625.68	-1.00	0.00	-0.0872	0.0418	0.1157	0.0008	-0.0091	0.0208
17	24	625.68	0.00	0.00	-0.0873	0.0420	0.1153	-0.0008	-0.0005	0.0013
17	23	626.12	1.97	0.00	-0.0875	0.0414	0.1150	-0.0024	0.0077	-0.0174
17	22	625.68	1.97	0.00	-0.0868	0.0411	0.1138	-0.0038	0.0156	-0.0355
17	21	625.68	3.93	0.00	-0.0857	0.0407	0.1126	-0.0072	0.0332	-0.0755
17	20	625.68	5.90	-0.01	-0.0872	0.0400	0.1137	-0.0105	0.0499	-0.1147
17	19	625.68	7.89	0.00	-0.0872	0.0392	0.1156	-0.0138	0.0662	-0.1545
17	18	626.12	9.86	0.00	-0.0878	0.0383	0.1188	-0.0176	0.0826	-0.1956
17	16	625.90	10.88	0.00	-0.0940	0.0379	0.1229	-0.0197	0.0903	-0.2151
17	17	625.68	10.88	0.00	-0.0874	0.0379	0.1204	-0.0198	0.0906	-0.2160
17	28	623.95	-4.17	4.17	0.2301	0.0532	0.0136	0.0037	-0.0316	0.0749
17	29	624.82	-2.14	4.29	0.2273	0.0541	0.0101	0.0016	-0.0145	0.0345
17	30	624.60	0.00	4.38	0.2195	0.0538	0.0102	-0.0005	0.0023	-0.0041
17	31	624.82	2.14	4.27	0.2077	0.0519	0.0101	0.0004	0.0012	-0.0022
17	32	625.12	4.17	4.27	0.2006	0.0519	0.0101	-0.0004	0.0012	-0.0022
17	33	624.60	6.10	4.07	0.1948	0.0510	0.0261	-0.0085	0.0498	-0.1171
17	34	624.60	8.08	4.03	0.1916	0.0506	0.0318	-0.0112	0.0657	-0.1567
17	35	624.82	10.05	4.01	0.1886	0.0492	0.0375	-0.0141	0.0819	-0.1982
17	16	624.60	12.03	4.01	0.1842	0.0485	0.0450	-0.0173	0.0979	-0.2393
17	37	624.60	13.98	4.00	0.1769	0.0475	0.0574	-0.0207	0.1096	-0.2758
17	47	624.82	-4.28	8.54	0.4967	0.1071	-0.0801	0.0020	-0.0265	0.0687
17	46	624.17	-2.17	8.64	0.4951	0.1082	-0.0824	0.0008	-0.0126	0.0336
17	45	624.60	0.00	8.67	0.4907	0.1082	-0.0824	-0.0006	0.0016	0.0019
17	44	624.60	2.17	8.64	0.4881	0.1076	-0.0809	-0.0023	0.0146	-0.0357
17	43	624.17	4.28	8.53	0.4841	0.1056	-0.0787	-0.0038	0.0286	-0.0715
17	42	624.60	6.30	8.43	0.4799	0.1036	-0.0728	-0.0054	0.0434	-0.1091
17	41	624.60	8.31	8.31	0.4740	0.1019	-0.0640	-0.0066	0.0589	-0.1492
17	40	624.17	10.40	8.05	0.4539	0.0963	-0.0502	-0.0088	0.0754	-0.1927
17	39	625.03	12.27	8.19	0.4546	0.0972	-0.0401	-0.0105	0.0873	-0.2290
17	38	624.60	14.21	8.12	0.4450	0.0955	-0.0266	-0.0121	0.1030	-0.2734
17	48	624.17	-4.30	12.89	0.7427	0.1981	-0.1655	0.0002	-0.0213	0.0637
17	49	624.60	-2.17	12.93	0.7398	0.1979	-0.1670	-0.0003	-0.0096	0.0300
17	50	624.39	0.00	12.96	0.7366	0.1975	-0.1674	0.0006	0.0016	-0.0019
17	51	624.17	2.13	12.92	0.7335	0.1966	-0.1665	-0.0009	0.0127	-0.0345
17	52	624.17	4.29	12.86	0.7315	0.1951	-0.1647	-0.0014	0.0244	-0.0685
17	53	624.60	6.39	12.78	0.7270	0.1923	-0.1608	-0.0021	0.0362	-0.1025
17	54	624.17	8.45	12.65	0.7190	0.1884	-0.1529	-0.0025	0.0486	-0.1395
17	55	624.39	10.47	12.55	0.7092	0.1852	-0.1390	-0.0036	0.0637	-0.1808
18	24	625.68	-3.96	0.00	-0.0403	0.0356	0.0336	0.0058	-0.0309	0.0730
18	23	623.95	-1.98	0.00	-0.0387	0.0354	0.0290	0.0025	-0.0163	0.0373
18	22	625.55	-1.00	0.00	-0.0376	0.0360	0.0274	0.0009	-0.0088	0.0200
18	21	625.12	0.00	0.00	-0.0378	0.0360	0.0269	-0.0008	0.0008	0.0011
18	20	625.12	1.99	0.00	-0.0382	0.0358	0.0270	-0.0023	0.0066	-0.0160
18	19	625.12	1.97	0.00	-0.0382	0.0354	0.0277	-0.0041	0.0143	-0.0339
18	18	625.33	3.95	0.00	-0.0408	0.0355	0.0320	-0.0075	0.0299	-0.0714
18	17	626.33	5.92	0.00	-0.0421	0.0350	0.0355	-0.0108	0.0447	-0.1080
18	16	625.12	7.92	-0.01	-0.0447	0.0342	0.0401	-0.0143	0.0596	-0.1447
18	15	625.12	9.88	0.00	-0.0481	0.0329	0.0467	-0.0179	0.0743	-0.1827
18	14	626.33	11.89	0.00	-0.0506	0.0317	0.0560	-0.0220	0.0894	-0.2237
18	25	625.68	-4.14	4.14	0.2753	0.0549	-0.0682	0.0049	-0.0272	0.0670
18	26	625.90	-2.12	4.25	0.2705	0.0559	-0.0685	0.0021	-0.0121	0.0301
18	27	625.12	0.00	4.31	0.2616	0.0548	-0.0675	0.0007	0.0019	-0.0044
18	28	625.90	2.11	4.22	0.2538	0.0538	-0.0653	-0.0041	0.0156	-0.0380
18	29	626.33	4.11	4.13	0.2477	0.0525	-0.0622	-0.0072	0.0292	-0.0722
18	30	625.90	6.09	4.06	0.2408	0.0513	-0.0560	-0.0099	0.0433	-0.1079
18	31	625.90	8.06	4.04	0.2363	0.0508	-0.0473	-0.0126	0.0582	-0.1456
18	32	625.68	10.06	4.04	0.2334	0.0497	-0.0405	-0.0154	0.0728	-0.1847
18	33	625.68	12.03	4.03	0.2278	0.0480	-0.0303	-0.0185	0.0876	-0.2249
18	34	625.25	13.99	4.00	0.2181	0.0458	-0.0139	-0.0217	0.0995	-0.2601
18	43	626.55	-4.26	8.49	0.5396	0.1149	-0.1577	0.0029	-0.0235	0.0640
18	42	626.98	-2.16	8.59	0.5386	0.1161	-0.1592	0.0013	-0.0109	0.0299
18	41	626.33	-0.02	8.60	0.5338	0.1156	-0.1589	-0.0006	0.0010	-0.0020
18	40	626.33	2.15	8.58	0.5301	0.1151	-0.1582	-0.0027	0.0132	-0.0342
18	39	626.33	4.25	8.48	0.5284	0.1130	-0.1573	-0.0048	0.0255	-0.0674
18	38	626.76	6.27	8.38	0.5254	0.1107	-0.1548	-0.0070	0.0385	-0.1023
18	37	626.33	8.29	8.29	0.5198	0.1085	-0.1485	-0.0088	0.0522	-0.1390
18	36	625.68	10.41	8.02	0.4990	0.1024	-0.1322	-0.0111	0.0674	-0.1816
18	35	626.33	12.25	8.20	0.5007	0.1030	-0.1223	-0.0130	0.0777	-0.2146
18	44	626.33	-4.30	12.83	0.7831	0.2108	-0.2423	0.0011	-0.0194	0.0607
18	45	626.76	-2.14	12.87	0.7791	0.2106	-0.2419	0.0001	-0.0090	0.0280
18	46	625.68	0.00	12.91	0.7759	0.2105	-0.2414	-0.0007	0.0013	-0.0022
18	47	625.68	2.14	12.86	0.7727	0.2090	-0.2411	-0.0014	0.0119	-0.0339
18	48	625.90	4.25	12.82	0.7728	0.2082	-0.2425	-0.0022	0.0223	-0.0660
18	49	625.90	6.37	12.73	0.7690	0.2054	-0.2392	-0.0033	0.0331	-0.0991
18	50	626.55	8.43	12.63	0.7637	0.2016	-0.2329	-0.0044	0.0446	-0.1335
18	51	626.33	10.45	12.52	0.7544	0.1973	-0.2227	-0.0061	0.0577	-0.1721

TABLE III - Continued
 AERODYNAMIC CHARACTERISTICS IN SIDESLIP FOR VARIOUS ANGLES OF ATTACK.
 STABILITY AXES; M = 1.41

Run	Pt.	q	β , deg	α , deg	C_L	C_D	C_m	$C_{l,s}$	$C_{n,w}$	C_y
19	26	625.03	-3.97	.03	-.0332	.0331	.0263	.0083	-.0248	.0639
19	25	625.25	-1.98	.00	-.0359	.0332	.0242	.0039	-.0129	.0336
19	24	625.25	-.99	.00	-.0345	.0331	.0233	.0015	-.0070	.0179
19	23	624.82	.00	.00	-.0345	.0328	.0230	-.0007	-.0011	.0027
19	22	624.39	.99	-.01	-.0359	.0328	.0232	-.0025	.0049	-.0130
19	21	624.60	1.98	-.01	-.0357	.0324	.0233	-.0051	.0108	-.0284
19	20	626.12	3.96	-.01	-.0365	.0325	.0253	-.0096	.0230	-.0598
19	19	625.03	5.96	.00	-.0374	.0319	.0271	-.0141	.0361	-.0939
19	18	625.47	7.95	.00	-.0381	.0311	.0291	-.0184	.0498	-.1295
19	17	625.03	9.91	.00	-.0388	.0305	.0308	-.0229	.0634	-.1660
19	16	625.25	11.93	.00	-.0366	.0295	.0317	-.0274	.0767	-.2030
19	27	623.95	-4.16	4.16	.2488	.0502	-.0203	.0068	-.0245	.0636
19	28	622.87	-2.13	4.27	.2424	.0506	-.0199	.0031	-.0111	.0290
19	29	625.47	.00	4.35	.2358	.0504	-.0190	-.0008	.0016	-.0038
19	30	625.03	2.13	4.26	.2273	.0493	-.0168	-.0052	.0137	-.0347
19	31	625.03	4.15	4.15	.2219	.0480	-.0150	-.0094	.0259	-.0670
19	32	625.68	6.11	4.07	.2185	.0478	-.0130	-.0130	.0384	-.1004
19	33	625.68	8.10	4.06	.2193	.0472	-.0123	-.0167	.0516	-.1353
19	34	625.47	10.09	4.03	.2189	.0461	-.0119	-.0204	.0651	-.1719
19	35	625.47	12.07	4.02	.2181	.0450	-.0108	-.0242	.0787	-.2102
19	44	625.47	-4.29	8.57	.4901	.1058	-.0641	.0041	-.0232	.0641
19	43	625.47	-2.18	8.66	.4860	.1062	-.0634	.0019	-.0112	.0316
19	42	625.90	-.02	8.69	.4810	.1054	-.0625	-.0007	.0010	-.0011
19	41	625.47	2.17	8.65	.4793	.1050	-.0623	-.0035	.0128	-.0330
19	40	625.47	4.29	8.55	.4767	.1033	-.0624	-.0062	.0249	-.0659
19	39	625.47	6.32	8.42	.4742	.1008	-.0621	-.0090	.0374	-.0999
19	38	625.68	8.33	8.33	.4733	.0993	-.0613	-.0117	.0502	-.1361
19	37	625.47	10.45	8.05	.4567	.0939	-.0570	-.0150	.0643	-.1758
19	36	625.68	12.28	8.20	.4623	.0951	-.0551	-.0172	.0738	-.2079
19	45	625.25	-4.32	12.95	.7117	.1936	-.1044	.0014	-.0203	.0622
19	46	625.03	-2.16	12.95	.7051	.1935	-.1035	.0002	-.0094	.0295
19	47	625.03	.00	13.02	.7031	.1927	-.1029	-.0008	.0016	-.0038
19	48	625.47	2.16	12.98	.7022	.1921	-.1036	-.0018	.0120	-.0330
19	49	625.25	4.31	12.93	.6991	.1904	-.1039	-.0028	.0230	-.0659
19	50	624.25	6.42	12.82	.6992	.1880	-.1041	-.0043	.0337	-.0980
19	51	626.98	8.48	12.70	.6967	.1844	-.1035	-.0058	.0445	-.1333
19	52	626.33	10.50	12.59	.6914	.1818	-.1009	-.0081	.0582	-.1717
21	29	624.39	-3.96	.00	-.0239	.0332	.0106	.0007	-.0298	.0727
21	28	624.60	-2.97	.00	-.0238	.0333	.0110	.0004	-.0225	.0555
21	27	624.60	-1.98	.00	-.0235	.0333	.0111	-.0001	-.0150	.0368
21	26	624.60	-.99	.00	-.0235	.0339	.0111	-.0004	-.0077	.0197
21	25	624.17	.00	.00	-.0234	.0338	.0108	-.0008	.0001	-.0163
21	24	624.39	.98	.00	-.0221	.0335	.0106	-.0012	.0071	-.0216
21	23	624.17	1.98	.00	-.0220	.0338	.0101	.0016	.0142	-.0341
21	22	624.60	2.97	.00	-.0219	.0335	.0095	-.0019	.0215	-.0512
21	21	624.60	3.95	.00	-.0218	.0328	.0089	-.0023	.0289	-.0698
21	20	623.95	5.93	.00	-.0205	.0324	.0061	-.0030	.0435	-.1065
21	19	623.95	7.91	.00	-.0193	.0317	.0028	-.0036	.0581	-.1430
21	18	623.95	9.90	.00	-.0181	.0310	-.0014	-.0041	.0724	-.1810
21	17	623.95	11.90	.00	-.0183	.0305	-.0037	-.0044	.0858	-.2188
21	30	624.17	-4.16	4.14	.2666	.0512	-.0371	-.0001	-.0302	.0701
21	31	624.17	-2.14	4.28	.2623	.0512	-.0354	-.0001	-.0139	.0326
21	32	624.39	.00	4.34	.2562	.0507	-.0346	-.0003	.0025	-.0048
21	33	624.39	2.13	4.26	.2496	.0506	-.0337	-.0009	.0183	-.0410
21	34	624.17	4.13	4.13	.2442	.0496	-.0333	-.0014	.0330	-.0754
21	35	624.17	6.09	4.06	.2409	.0488	-.0351	-.0017	.0473	-.1101
21	36	624.17	8.06	4.02	.2398	.0473	-.0383	-.0016	.0621	-.1472
21	37	624.17	10.03	4.01	.2411	.0466	-.0421	-.0012	.0767	-.1847
21	38	624.60	12.02	4.00	.2374	.0455	-.0448	-.0003	.0901	-.2215
21	47	624.39	-4.29	8.56	.5143	.1070	-.0778	-.0012	-.0293	.0687
21	46	624.39	-2.18	8.68	.5120	.1089	-.0766	-.0008	-.0138	.0330
21	45	624.60	.00	8.70	.5064	.1081	-.0756	-.0002	.0022	-.0029
21	44	624.17	2.16	8.65	.5050	.1077	-.0762	.0002	.0182	-.0397
21	43	624.39	4.27	8.36	.5026	.1056	-.0772	.0005	.0325	-.0733
21	42	624.17	6.31	8.40	.4988	.1032	-.0790	.0015	.0481	-.1097
21	41	624.17	8.30	8.33	.4976	.1020	-.0821	.0026	.0630	-.1466
21	40	624.17	10.38	8.00	.4811	.0962	-.0827	.0036	.0780	-.1861
21	39	624.17	12.23	8.16	.4844	.0969	-.0843	.0056	.0882	-.2165
21	48	624.39	-4.33	12.97	.7422	.1994	-.1120	-.0030	-.0282	.0678
21	49	624.39	-2.17	13.04	.7392	.1992	-.1091	-.0014	-.0124	.0308
21	50	624.17	.00	13.07	.7354	.1989	-.1080	.0001	.0026	-.0043
21	51	624.17	2.17	13.02	.7338	.1984	-.1097	.0014	.0178	-.0392
21	52	624.39	4.32	12.95	.7326	.1970	-.1125	.0028	.0325	-.0745
21	53	624.39	6.41	12.80	.7307	.1934	-.1160	.0042	.0458	-.1075
21	54	624.39	8.48	12.69	.7272	.1900	-.1187	.0058	.0580	-.1400
21	55	624.17	10.47	12.55	.7193	.1857	-.1199	.0076	.0722	-.1753

TABLE III - Continued
 AERODYNAMIC CHARACTERISTICS IN SIDESLIP FOR VARIOUS ANGLES OF ATTACK.

STABILITY AXES; M = 1.41

Run	Pt.	q	β , deg	α , deg	C_L	C_D	C_m	C_{l_s}	C_{n_w}	C_Y
22	30	623.52	-3.95	.00	-.0281	.0350	.0158	-.0002	-.0322	.0764
22	29	623.52	-2.97	.00	-.0269	.0352	.0155	-.0003	-.0244	.0576
22	28	623.74	-1.98	.00	-.0269	.0352	.0156	-.0004	-.0164	.0388
22	27	623.30	-1.00	.00	-.0256	.0358	.0148	-.0006	-.0084	.0200
22	26	623.09	.00	.00	-.0257	.0358	.0147	-.0007	-.0002	.0011
22	25	623.52	.98	.00	-.0256	.0355	.0153	-.0009	.0079	-.0177
22	24	623.09	1.98	.00	-.0258	.0358	.0147	-.0010	.0154	-.0358
22	23	623.09	2.96	.00	-.0257	.0354	.0147	-.0012	.0237	-.0546
22	22	623.52	3.94	.00	-.0257	.0353	.0144	-.0013	.0320	-.0750
22	21	623.09	5.92	.00	-.0247	.0350	.0124	-.0016	.0473	-.1118
22	20	623.09	7.91	.00	-.0236	.0340	.0084	-.0018	.0633	-.1516
22	19	623.09	9.86	.00	-.0225	.0330	.0050	-.0020	.0783	-.1906
22	18	623.52	11.87	.00	-.0243	.0324	.0032	-.0019	.0925	-.2291
22	31	623.30	-4.13	4.13	.2809	.0545	-.0718	-.0010	-.0321	.0730
22	32	623.74	-2.12	4.24	.2769	.0545	-.0702	-.0005	-.0147	.0330
22	33	623.52	.00	4.32	.2718	.0548	-.0694	-.0003	.0026	-.0053
22	34	623.74	2.11	4.24	.2675	.0543	-.0685	-.0002	.0133	-.0426
22	35	623.52	4.11	4.11	.2625	.0533	-.0693	-.0004	.0353	-.0789
22	36	623.74	6.07	4.04	.2580	.0521	-.0695	-.0001	.0504	-.1147
22	37	623.52	8.02	4.00	.2572	.0513	-.0713	.0005	.0662	-.1536
22	38	623.52	10.02	4.00	.2547	.0508	-.0708	.0014	.0816	-.1929
22	39	623.52	11.90	3.96	.2486	.0494	-.0699	.0025	.0954	-.2300
22	48	624.17	-4.26	8.50	.5480	.1147	-.1489	-.0019	-.0302	.0694
22	47	623.95	-2.16	8.61	.5462	.1167	-.1485	-.0011	-.0140	.0329
22	46	623.95	.00	8.63	.5425	.1161	-.1480	.0000	.0026	-.0048
22	45	624.17	2.14	8.60	.5423	.1159	-.1494	.0008	.0186	-.0409
22	44	623.95	4.25	8.49	.5393	.1133	-.1498	.0015	.0335	-.0755
22	43	623.95	6.27	8.36	.5370	.1112	-.1514	.0028	.0496	-.1129
22	42	623.95	8.27	8.27	.5345	.1098	-.1528	.0043	.0648	-.1500
22	41	623.95	10.35	7.98	.5145	.1036	-.1475	.0059	.0806	-.1905
22	40	623.95	12.19	8.14	.5156	.1044	-.1445	.0082	.0915	-.2219
22	49	624.39	-4.30	12.87	.7946	.2128	-.2189	-.0035	-.0282	.0679
22	50	624.17	-2.15	12.93	.7920	.2135	-.2169	-.0016	-.0124	.0301
22	51	624.17	.00	12.96	.7894	.2132	-.2164	.0002	.0027	-.0051
22	52	624.17	2.13	12.92	.7867	.2124	-.2177	.0018	.0180	-.0409
22	53	624.39	4.29	12.85	.7871	.2112	-.2204	.0035	.0329	-.0756
22	54	624.17	6.36	12.72	.7847	.2071	-.2225	.0050	.0458	-.1087
22	55	624.17	8.43	12.62	.7790	.2035	-.2215	.0068	.0586	-.1414
22	56	624.39	10.39	12.50	.7707	.1994	-.2207	.0089	.0730	-.1774
23	22	623.30	-3.94	.00	-.0779	.0415	.1140	-.0003	-.0349	.0809
23	21	623.30	-1.99	.00	-.0765	.0415	.1148	-.0006	-.0178	.0422
23	20	623.30	-1.00	.00	-.0778	.0423	.1149	-.0007	-.0091	.0218
23	19	623.74	.00	.00	-.0778	.0423	.1146	-.0008	-.0006	.0029
23	18	622.87	.98	.00	-.0767	.0420	.1140	-.0009	.0079	-.0168
23	17	622.01	1.98	.00	-.0755	.0422	.1129	-.0010	.0164	-.0366
23	16	624.17	3.93	.00	-.0741	.0417	.1109	-.0012	.0335	-.0757
23	15	623.52	5.90	.00	-.0742	.0409	.1081	-.0015	.0516	-.1183
23	14	623.52	7.89	.00	-.0731	.0399	.1038	-.0017	.0687	-.1592
23	13	623.52	9.86	.00	-.0707	.0391	.0996	-.0018	.0854	-.2006
23	23	623.09	-4.16	4.16	.2314	.0539	.0115	-.0018	-.0361	.0800
23	24	623.09	-2.16	4.30	.2297	.0543	.0136	-.0009	-.0168	.0373
23	25	623.09	.00	4.40	.2234	.0540	.0185	-.0002	.0028	-.0052
23	26	623.30	2.14	4.30	.2177	.0539	.0235	.0002	.0213	-.0451
23	27	623.52	4.15	4.15	.2113	.0529	.0274	.0005	.0390	-.0840
23	28	623.74	6.10	4.06	.2096	.0522	.0266	.0010	.0559	-.1224
23	29	623.52	8.05	4.02	.2074	.0511	.0255	.0016	.0731	-.1638
23	30	623.74	10.02	4.00	.2051	.0504	.0256	.0026	.0900	-.2047
23	31	623.30	11.99	3.99	.2032	.0496	.0251	.0037	.1054	-.2453
23	39	623.30	-4.29	8.55	.5016	.1085	-.0684	-.0029	-.0333	.0756
23	38	623.30	-2.18	8.66	.4997	.1096	-.0674	-.0015	-.0159	.0365
23	37	623.30	.00	8.70	.4959	.1090	-.0654	.0000	.0026	-.0038
23	36	623.30	2.18	8.66	.4947	.1088	-.0634	.0013	.0207	-.0434
23	35	623.74	4.29	8.55	.4925	.1070	-.0607	.0025	.0367	-.0797
23	34	623.52	6.31	8.41	.4890	.1052	-.0587	.0041	.0542	-.1189
23	33	623.30	8.29	8.29	.4819	.1031	-.0561	.0060	.0715	-.1595
23	32	623.09	10.37	8.02	.4633	.0978	-.0507	.0078	.0891	-.2026
23	40	623.74	-4.31	12.93	.7520	.2018	-.1399	-.0042	-.0304	.0716
23	41	621.79	-2.16	12.99	.7489	.2016	-.1367	-.0020	-.0135	.0329
23	42	623.09	.00	13.03	.7472	.2018	-.1352	.0002	.0027	-.0041
23	43	623.52	2.14	12.98	.7452	.2011	-.1350	.0023	.0188	-.0409
23	44	621.79	4.31	12.93	.7430	.1995	-.1355	.0043	.0350	-.0783
23	45	623.52	6.40	12.79	.7418	.1984	-.1364	.0062	.0492	-.1129
23	46	623.52	8.44	12.69	.7336	.1926	-.1314	.0083	.0626	-.1473
23	47	623.30	10.45	12.52	.7236	.1877	-.1272	.0109	.0785	-.1854

TABLE III - Continued
 AERODYNAMIC CHARACTERISTICS IN SIDESLIP FOR VARIOUS ANGLES OF ATTACK.
 STABILITY AXES; M = 1.41

Run	Pt.	q	β , deg	α , deg	C_L	C_D	C_m	C_{l_s}	C_{n_w}	C_Y
24	23	624.39	-3.97	.01	-.0853	.0435	.1241	.0016	-.0286	.0725
24	22	624.39	-1.99	.00	-.0884	.0430	.1293	.0003	-.0149	.0384
24	21	624.17	-1.00	.00	-.0894	.0428	.1306	-.0002	-.0073	.0197
24	20	623.95	.00	.00	-.0892	.0431	.1308	-.0008	-.0053	.0026
24	19	623.95	.99	.00	-.0890	.0429	.1306	-.0014	.0068	-.0144
24	18	624.17	1.97	.00	-.0888	.0434	.1292	-.0020	.0137	-.0314
24	17	623.95	3.95	.00	-.0861	.0433	.1237	-.0032	.0277	-.0665
24	16	623.95	5.94	.00	-.0808	.0421	.1147	-.0044	.0426	-.1045
24	15	624.39	7.93	.00	-.0770	.0407	.1048	-.0055	.0572	-.1424
24	14	623.95	9.90	.00	-.0711	.0393	.0922	-.0063	.0716	-.1804
24	13	623.52	11.91	.00	-.0640	.0380	.0793	-.0068	.0849	-.2183
24	25	624.17	-2.15	4.31	.2219	.0552	.0298	.0004	-.0130	.0312
24	26	624.39	.00	4.40	.2150	.0557	.0339	-.0003	.0026	-.0052
24	28	624.17	2.15	4.31	.2100	.0541	.0347	-.0014	.0176	-.0391
24	29	623.30	4.16	4.16	.2045	.0541	.0337	-.0024	.0327	-.0744
24	30	623.74	6.12	4.07	.2044	.0527	.0283	-.0034	.0477	-.1101
24	31	624.82	8.08	4.03	.2060	.0517	.0202	-.0040	.0632	-.1485
24	32	623.95	10.05	4.01	.2092	.0502	.0119	-.0040	.0782	-.1871
24	33	624.17	12.02	4.00	.2108	.0494	.0028	-.0036	.0918	-.2247
24	34	624.60	13.97	4.00	.2083	.0480	-.0048	-.0024	.1016	-.2570
24	44	624.60	-4.29	8.57	.5016	.1089	-.0635	.0000	-.0309	.0710
24	43	624.82	-2.18	8.68	.4968	.1100	-.0593	-.0002	-.0146	.0345
24	42	624.39	-.02	8.71	.4905	.1089	-.0563	-.0001	.0028	-.0046
24	41	624.03	2.18	8.67	.4922	.1092	-.0547	.0004	.0188	-.0406
24	40	624.39	4.28	8.54	.4890	.1070	-.0596	-.0007	.0342	-.0759
24	39	624.17	6.30	8.42	.4886	.1053	-.0633	-.0004	.0505	-.1139
24	38	623.74	8.30	8.30	.4861	.1033	-.0674	.0000	.0661	-.1519
24	37	623.30	10.40	8.01	.4717	.0979	-.0697	.0005	.0813	-.1916
24	35	623.95	11.69	9.05	.5295	.1140	-.0905	.0029	.0879	-.2121
24	36	624.60	12.20	8.17	.4792	.0987	-.0779	.0022	.0916	-.2223
24	45	624.60	-4.32	12.94	.7504	.2017	-.1342	-.0017	-.0314	.0729
24	46	624.17	-2.19	13.00	.7459	.2012	-.1342	-.0008	-.0150	.0352
24	47	624.17	.00	13.04	.7450	.2015	-.1328	.0000	.0033	-.0057
24	48	624.17	2.16	13.00	.7410	.2004	-.1327	.0008	.0202	-.0432
24	49	624.82	4.31	12.92	.7367	.1988	-.1310	.0015	.0350	-.0793
24	50	624.60	6.40	12.80	.7335	.1951	-.1301	.0026	.0488	-.1131
24	51	624.39	8.45	12.66	.7308	.1916	-.1333	.0036	.0607	-.1448
24	52	624.82	10.45	12.52	.7290	.1879	-.1430	.0050	.0764	-.1825
25	25	624.82	-3.96	.00	-.0303	.0359	.0430	.0023	-.0309	.0758
25	24	624.60	-1.98	.00	-.0317	.0358	.0469	.0007	-.0150	.0382
25	23	625.03	-1.00	.00	-.0340	.0362	.0477	.0001	-.0078	.0203
25	22	624.60	.01	.00	-.0324	.0361	.0472	-.0007	-.0006	.0032
25	21	625.03	.99	.00	-.0320	.0358	.0468	-.0014	.0067	-.0147
25	20	624.82	1.97	.00	-.0316	.0364	.0460	-.0021	.0141	-.0326
25	19	624.39	3.94	.00	-.0285	.0359	.0416	-.0037	.0294	-.0693
25	18	624.82	5.93	.00	-.0241	.0352	.0322	-.0053	.0458	-.1091
25	17	625.03	7.92	.00	-.0187	.0345	.0221	-.0067	.0614	-.1480
25	16	625.03	9.89	.00	-.0122	.0334	.0116	-.0078	.0767	-.1876
25	15	624.60	10.91	.00	-.0097	.0329	.0067	-.0082	.0840	-.2079
25	26	624.82	-4.14	4.14	.2824	.0546	-.0613	.0020	-.0349	.0778
25	27	624.60	-2.13	4.27	.2739	.0544	-.0543	.0008	-.0161	.0361
25	28	624.82	.00	4.35	.2653	.0539	-.0495	-.0004	.0031	-.0055
25	29	624.82	2.12	4.24	.2582	.0533	-.0486	-.0018	.0206	-.0437
25	30	625.25	4.11	4.11	.2552	.0526	-.0521	-.0033	.0376	-.0815
25	31	624.60	6.08	4.05	.2519	.0515	-.0554	-.0044	.0533	-.1189
25	32	624.82	8.03	4.01	.2541	.0508	-.0621	-.0050	.0692	-.1584
25	33	624.82	10.01	3.99	.2572	.0497	-.0695	-.0053	.0846	-.1976
25	41	625.25	-4.26	8.49	.5404	.1130	-.1440	.0004	-.0357	.0786
25	40	624.60	-2.16	8.61	.5401	.1147	-.1450	.0003	-.0181	.0396
25	39	625.47	.00	8.63	.5340	.1139	-.1426	-.0003	.0033	-.0057
25	38	625.25	2.14	8.60	.5336	.1132	-.1418	-.0008	.0225	-.0468
25	37	624.60	4.25	8.49	.5321	.1117	-.1417	-.0011	.0390	-.0840
25	36	625.90	6.27	8.36	.5296	.1096	-.1443	-.0010	.0566	-.1235
25	34	624.82	10.35	7.98	.5132	.1021	-.1470	.0000	.0882	-.2020
25	43	625.25	-4.29	12.86	.7863	.2100	-.2115	-.0017	-.0343	.0778
25	42	623.95	-4.24	12.87	.7856	.2101	-.2112	-.0017	-.0341	.0772
25	44	623.95	-2.15	12.92	.7869	.2113	-.2173	-.0008	-.0158	.0360
25	45	625.25	.00	12.95	.7866	.2119	-.2210	.0000	.0032	-.0058
25	46	624.17	2.15	12.91	.7786	.2092	-.2133	.0006	.0211	-.0451
25	47	624.82	4.26	12.85	.7751	.2071	-.2093	.0015	.0386	-.0847
25	48	625.25	6.35	12.75	.7699	.2030	-.2058	.0025	.0521	-.1185
25	49	624.82	8.41	12.60	.7638	.1987	-.2069	.0037	.0647	-.1505
25	50	623.30	10.41	12.48	.7621	.1956	-.2160	.0053	.0823	-.1913

TABLE III - Continued
 AERODYNAMIC CHARACTERISTICS IN SIDESLIP FOR VARIOUS ANGLES OF ATTACK.
 STABILITY AXES: M = 1.41

Run	Pt.	q	β , deg	α , deg	C_L	C_D	C_m	$C_{L\beta}$	$C_{n\omega}$	C_Y
26	30	623.95	-3.95	.00	-.0263	.0251	.0457	.0062	-.0271	.0618
26	29	624.39	-2.97	.00	-.0266	.0251	.0463	.0046	-.0199	.0460
26	28	623.95	-1.99	.00	-.0272	.0248	.0466	.0031	-.0135	.0313
26	27	624.17	-1.00	.01	-.0263	.0246	.0462	.0015	-.0065	.0154
26	26	624.17	.00	.00	-.0269	.0244	.0462	.0000	.0000	.0008
26	25	623.95	.99	.00	-.0273	.0246	.0462	-.0016	.0066	-.0147
26	24	624.17	1.98	.00	-.0279	.0246	.0466	-.0031	.0125	-.0286
26	23	623.95	2.97	-.01	-.0272	.0247	.0460	-.0046	.0189	-.0434
26	22	624.17	3.95	.00	-.0277	.0247	.0456	-.0061	.0258	-.0590
26	21	623.95	4.93	.00	-.0249	.0245	.0417	-.0092	.0395	-.0909
26	20	623.95	5.93	-.01	-.0219	.0233	.0372	-.0123	.0548	-.1262
26	19	624.39	6.92	.00	-.0177	.0224	.0314	-.0153	.0697	-.1620
26	18	623.95	7.92	.00	-.0137	.0211	.0248	-.0183	.0841	-.1987
26	17	624.17	8.91	.00	-.0110	.0208	.0190	-.0209	.0972	-.2356
26	31	624.17	-3.97	3.97	.0182	.0258	-.0042	.0042	-.0289	.0626
26	32	624.17	-2.00	4.01	.0142	.0251	-.0006	.0018	-.0131	.0277
26	33	623.95	.00	4.02	.0115	.0249	.0024	-.0004	.0018	-.0042
26	34	624.17	2.00	4.00	.0105	.0248	.0024	-.0027	.0164	-.0358
26	35	623.95	3.96	3.96	.0125	.0251	-.0005	-.0050	.0312	-.0686
26	36	624.17	5.94	3.97	.0146	.0246	-.0042	-.0071	.0462	-.1021
26	37	623.74	7.92	3.95	.0185	.0237	-.0092	-.0094	.0617	-.1372
26	38	623.74	9.91	3.96	.0239	.0230	-.0153	-.0114	.0772	-.1747
26	39	623.74	11.91	3.96	.0275	.0221	-.0197	-.0133	.0919	-.2113
26	48	623.52	-4.00	7.98	.0608	.0325	-.0534	.0027	-.0309	.0646
26	47	623.95	-2.01	8.00	.0570	.0323	-.0492	.0012	-.0152	.0306
26	46	623.52	-.03	8.00	.0536	.0317	-.0453	-.0004	-.0024	-.0055
26	45	623.74	2.00	7.97	.0562	.0317	-.0479	-.0021	.0193	-.0408
26	44	623.74	3.98	7.98	.0592	.0315	-.0521	-.0034	.0346	-.0745
26	43	623.74	5.97	7.96	.0615	.0313	-.0541	-.0045	.0499	-.1090
26	42	623.74	7.93	7.96	.0645	.0305	-.0574	-.0055	.0651	-.1440
26	41	623.74	10.07	7.76	.0660	.0294	-.0586	-.0066	.0808	-.1825
26	40	623.74	11.90	7.94	.0696	.0294	-.0606	-.0070	.0915	-.2130
26	49	623.52	-3.99	11.99	.1012	.0453	-.0909	.0011	-.0300	.0645
26	50	623.95	-1.99	12.01	.1025	.0462	-.0937	.0005	-.0143	.0298
26	51	623.52	.00	12.01	.1047	.0468	-.0986	-.0004	.0021	-.0052
26	52	623.52	1.99	11.99	.1012	.0456	-.0924	-.0013	.0185	-.0406
26	53	623.74	4.00	12.00	.1016	.0444	-.0921	-.0017	.0334	-.0742
26	54	623.52	5.98	11.98	.1031	.0434	-.0922	-.0017	.0474	-.1076
26	55	623.52	7.97	11.95	.1053	.0432	-.0928	-.0017	.0617	-.1421
26	57	623.52	9.94	11.96	.1098	.0432	-.0975	-.0014	.0758	-.1774
27	28	624.17	-3.96	.00	-.0773	.0331	.1284	.0057	-.0258	.0608
27	27	624.39	-2.98	.00	-.0777	.0331	.1291	.0041	-.0187	.0444
27	26	624.39	-1.98	.00	-.0783	.0329	.1295	.0027	-.0120	.0296
27	25	624.17	-1.00	.00	-.0789	.0320	.1305	.0013	-.0060	.0150
27	24	624.17	.00	.00	-.0795	.0317	.1308	-.0001	.0004	.0003
27	23	624.17	.98	.00	-.0789	.0321	.1303	-.0015	.0066	-.0136
27	22	624.60	1.97	.00	-.0781	.0319	.1295	-.0029	.0129	-.0290
27	21	624.17	2.97	.00	-.0778	.0328	.1282	-.0042	.0188	-.0422
27	20	624.17	3.95	.00	-.0756	.0330	.1269	-.0057	.0256	-.0585
27	19	624.60	5.92	.01	-.0742	.0320	.1239	-.0086	.0393	-.0903
27	18	624.60	7.92	.00	-.0716	.0308	.1195	-.0114	.0537	-.1246
27	17	624.17	9.88	.00	-.0676	.0296	.1137	-.0143	.0680	-.1596
27	16	624.60	11.87	.00	-.0650	.0281	.1074	-.0170	.0819	-.1958
27	15	624.39	13.86	.00	-.0617	.0270	.1010	-.0193	.0918	-.2270
27	29	624.17	-4.02	4.01	-.0362	.0263	.0830	.0035	-.0246	.0565
27	30	624.39	-2.02	4.03	-.0396	.0264	.0854	.0015	-.0111	.0252
27	31	624.82	.00	4.08	-.0415	.0259	.0872	-.0004	.0016	-.0031
27	32	623.74	2.01	4.05	-.0418	.0258	.0881	-.0022	.0140	-.0320
27	33	623.74	4.01	4.01	-.0416	.0259	.0869	-.0042	.0267	-.0613
27	34	624.17	5.97	3.99	-.0398	.0251	.0837	-.0060	.0403	-.0922
27	35	623.09	7.96	3.98	-.0349	.0239	.0775	-.0081	.0553	-.1272
27	36	624.82	9.96	3.98	-.0294	.0232	.0711	-.0101	.0702	-.1634
27	37	624.17	11.94	4.00	-.0246	.0224	.0654	-.0120	.0846	-.2006
27	38	623.74	13.88	4.00	-.0209	.0214	.0607	-.0135	.0949	-.2313
27	47	624.17	-4.03	8.04	.0088	.0253	.0326	.0020	-.0255	.0575
27	46	623.95	-2.02	8.07	.0043	.0253	.0367	.0009	-.0121	.0271
27	45	624.60	.00	8.06	.0035	.0255	.0393	-.0003	.0015	-.0029
27	44	623.74	2.02	8.06	.0051	.0255	.0366	-.0015	.0147	-.0328
27	43	624.17	4.03	8.04	.0064	.0250	.0346	-.0026	.0278	-.0630
27	42	624.17	6.01	8.01	.0097	.0242	.0302	-.0037	.0424	-.0964
27	41	624.17	7.97	8.00	.0137	.0235	.0257	-.0047	.0567	-.1304
27	40	624.39	10.11	7.79	.0168	.0225	.0233	-.0060	.0727	-.1703
27	39	624.39	11.94	7.97	.0216	.0220	.0184	-.0065	.0836	-.2000
27	48	623.74	-4.02	12.06	.0549	.0321	-.0120	.0009	-.0258	.0578
27	49	624.17	-2.00	12.06	.0500	.0318	-.0069	.0002	-.0120	.0265
27	50	624.39	-.02	12.07	.0477	.0314	-.0042	-.0003	.0016	-.0042
27	51	623.95	2.00	12.06	.0517	.0321	-.0090	-.0009	.0155	-.0351
27	52	624.17	4.01	12.05	.0540	.0311	-.0124	-.0015	.0287	-.0660
27	53	624.17	6.02	12.04	.0554	.0304	-.0126	-.0015	.0418	-.0976
27	54	624.17	7.99	12.03	.0598	.0301	-.0170	-.0016	.0556	-.1319
27	55	623.74	9.95	11.98	.0680	.0305	-.0260	-.0016	.0693	-.1671

TABLE III - Continued
 AERODYNAMIC CHARACTERISTICS IN SIDESLIP FOR VARIOUS ANGLES OF ATTACK.

STABILITY AXES; M = 1.41

Run	Pt.	q	β , deg	α , deg	C_L	C_D	C_m	$C_{l,s}$	$C_{n,w}$	C_y
28	28	623.52	-3.93	.00	-.0671	.0298	.1066	.0029	-.0342	.0733
28	27	623.30	-2.97	.00	-.0659	.0300	.1064	.0022	-.0263	.0567
28	26	623.30	-1.97	.00	-.0664	.0301	.1064	.0014	-.0172	.0376
28	25	623.52	-1.00	.00	-.0674	.0301	.1069	.0006	-.0087	.0202
28	24	623.30	.00	.00	-.0670	.0302	.1068	-.0001	-.0001	.0013
28	23	623.30	.97	.00	-.0679	.0302	.1068	-.0009	.0084	-.0162
28	21	623.52	1.96	.00	-.0662	.0299	.1055	-.0017	.0165	-.0343
28	22	623.30	2.95	.00	-.0659	.0296	.1046	-.0025	.0252	-.0525
28	20	623.30	3.92	-.01	-.0655	.0302	.1047	-.0033	.0339	-.0708
28	19	623.30	5.89	.00	-.0645	.0296	.1041	-.0049	.0515	-.1087
28	18	623.52	7.86	.00	-.0635	.0288	.1030	-.0067	.0685	-.1465
28	17	623.30	9.84	.00	-.0647	.0280	.1040	-.0086	.0857	-.1860
28	29	624.17	-3.99	3.99	-.0200	.0242	.0563	.0008	-.0304	.0655
28	30	623.74	-2.91	4.03	-.0208	.0243	.0549	.0002	-.0140	.0298
28	31	623.95	-.00	4.06	-.0216	.0242	.0547	.0003	.0019	-.0038
28	32	623.74	2.01	4.02	-.0230	.0236	.0552	-.0007	.0176	-.0372
28	33	623.95	3.98	3.98	-.0250	.0239	.0571	-.0011	.0332	-.0707
28	34	623.74	5.95	3.96	-.0264	.0237	.0587	-.0017	.0496	-.1061
28	35	623.74	7.93	3.95	-.0255	.0231	.0599	-.0026	.0660	-.1436
28	36	624.17	9.92	3.96	-.0269	.0221	.0633	-.0033	.0826	-.1819
28	45	623.52	-4.04	8.02	.0249	.0251	.0077	-.0003	-.0269	.0603
28	44	621.79	-2.02	8.05	.0230	.0261	.0083	-.0003	-.0126	.0283
28	43	622.44	.00	8.05	.0211	.0259	.0088	-.0002	.0015	-.0027
28	42	623.95	2.01	8.02	.0216	.0257	.0081	-.0002	.0155	-.0336
28	41	623.95	4.00	8.02	.0231	.0247	.0087	.0003	.0296	-.0662
28	40	623.95	5.98	7.99	.0229	.0244	.0079	.0003	.0445	-.0998
28	39	624.39	7.98	7.98	.0228	.0237	.0104	.0007	.0600	-.1356
28	38	623.09	10.08	7.79	.0188	.0222	.0177	.0007	.0768	-.1752
28	37	624.17	11.91	7.98	.0176	.0218	.0240	.0011	.0897	-.2096
28	46	623.52	-4.04	12.05	.0705	.0339	-.0347	-.0013	-.0225	.0528
28	47	623.74	-2.00	12.04	.0690	.0346	-.0344	-.0006	-.0104	.0241
28	48	624.39	.00	12.05	.0674	.0344	-.0350	-.0002	.0014	-.0032
28	49	623.95	2.00	12.04	.0678	.0338	-.0348	.0004	.0133	-.0316
28	50	623.74	3.99	12.06	.0689	.0329	-.0355	.0009	.0254	-.0609
28	51	624.17	5.98	12.03	.0705	.0320	-.0357	.0019	.0386	-.0924
28	52	623.95	8.00	11.99	.0696	.0311	-.0317	.0030	.0527	-.1277
28	53	623.52	9.99	11.98	.0691	.0309	-.0261	.0038	.0665	-.1622
29	23	622.87	-3.94	.00	-.0055	-.0244	.0161	.0034	-.0310	.0680
29	22	623.30	-1.98	.00	-.0048	-.0246	.0142	.0016	-.0154	.0341
29	21	623.09	-.98	.00	-.0045	-.0244	.0133	.0008	-.0078	.0176
29	20	622.87	.00	.00	-.0041	-.0243	.0127	-.0002	-.0001	.0011
29	19	622.87	.98	.00	-.0051	-.0243	.0128	-.0011	.0077	-.0154
29	18	622.87	1.96	.00	-.0046	-.0242	.0129	-.0020	.0152	-.0320
29	17	623.09	3.93	.00	-.0065	-.0244	.0141	-.0037	.0303	-.0651
29	16	622.87	5.90	.01	-.0079	-.0237	.0171	-.0054	.0466	-.1013
29	15	622.87	7.89	.00	-.0095	-.0230	.0190	-.0072	.0622	-.1368
29	14	623.30	9.86	.00	-.0121	-.0221	.0221	-.0090	.0776	-.1735
29	13	623.09	11.85	.00	-.0169	-.0213	.0288	-.0109	.0929	-.2119
29	24	623.09	-3.96	3.96	.0427	.0274	-.0357	.0017	-.0270	.0603
29	25	623.30	-1.99	3.98	.0396	.0272	-.0343	.0007	-.0121	.0270
29	26	623.30	.00	3.99	.0376	.0264	-.0342	-.0003	.0019	-.0040
29	27	623.30	1.98	3.97	.0362	.0262	-.0348	-.0012	.0159	-.0348
29	28	622.22	3.94	3.94	.0343	.0262	-.0343	-.0022	.0296	-.0660
29	29	623.09	5.94	3.95	.0355	.0258	-.0345	-.0031	.0441	-.0987
29	30	623.52	7.93	3.96	.0360	.0252	-.0337	-.0041	.0590	-.1336
29	31	623.09	9.92	3.98	.0334	.0237	-.0290	-.0049	.0737	-.1695
29	32	623.30	11.90	3.96	.0306	.0229	-.0219	-.0059	.0885	-.2061
29	41	623.74	-4.01	7.97	.0805	.0355	-.0799	.0005	-.0246	.0567
29	40	623.09	-2.00	7.98	.0787	.0363	-.0795	.0002	-.0115	.0263
29	39	623.09	.00	7.97	.0782	.0360	-.0794	-.0002	.0014	-.0029
29	38	623.09	2.00	7.97	.0788	.0356	-.0801	-.0005	.0145	-.0329
29	37	623.30	3.99	7.96	.0791	.0350	-.0808	-.0008	.0272	-.0631
29	36	623.09	5.96	7.95	.0790	.0340	-.0805	-.0007	.0407	-.0943
29	35	623.09	7.94	7.94	.0801	.0330	-.0793	-.0009	.0547	-.1277
29	34	623.09	10.07	7.76	.0773	.0314	-.0742	-.0013	.0698	-.1653
29	33	623.09	11.93	7.96	.0771	.0310	-.0693	-.0014	.0806	-.1959
29	42	621.58	-3.99	11.99	.1214	.0499	-.1205	-.0007	-.0210	.0503
29	43	622.44	-1.99	11.98	.1208	.0508	-.1212	-.0004	-.0097	.0231
29	44	624.39	.00	12.00	.1206	.0509	-.1214	-.0002	.0017	-.0042
29	45	627.20	1.99	11.97	.1202	.0501	-.1216	.0001	.0129	-.0318
29	46	624.17	3.99	11.98	.1218	.0494	-.1223	.0004	.0240	-.0579
29	47	623.74	5.98	11.97	.1226	.0478	-.1224	.0009	.0358	-.0886
29	48	623.23	7.98	11.96	.1237	.0475	-.1207	.0012	.0478	-.1202
29	49	625.25	9.97	11.95	.1231	.0473	-.1151	.0020	.0617	-.1553

TABLE III - Concluded
 AERODYNAMIC CHARACTERISTICS IN SIDESLIP FOR VARIOUS ANGLES OF ATTACK.
 STABILITY AXES; $M = 1.41$

Run	Pt.	q	β , deg	α , deg	C_L	C_D	C_m	$C_{l,s}$	$C_{n,w}$	C_Y
30	26	623.95	-3.95	.01	-.0067	.0221	.0117	.0051	-.0254	.0585
30	25	623.74	-1.98	.00	-.0056	.0223	.0107	.0026	-.0123	.0290
30	24	623.95	-.99	.00	-.0050	.0221	.0102	.0012	-.0058	.0142
30	23	623.95	.00	.00	-.0056	.0219	.0102	-.0001	.0007	-.0013
30	22	623.30	.99	.00	-.0051	.0220	.0101	-.0014	.0072	-.0154
30	21	622.87	1.98	.00	-.0057	.0222	.0103	-.0027	.0137	-.0310
30	20	623.95	3.93	.00	-.0057	.0222	.0106	-.0053	.0269	-.0613
30	19	622.01	5.91	.00	-.0045	.0220	.0101	-.0079	.0407	-.0928
30	18	623.95	7.91	.00	-.0045	.0212	.0088	-.0103	.0551	-.1269
30	17	621.36	9.88	.00	-.0045	.0201	.0080	-.0128	.0693	-.1611
30	16	624.82	11.88	.02	-.0041	.0194	.0078	-.0152	.0830	-.1966
30	15	622.87	13.86	.02	-.0041	.0187	.0076	-.0175	.0955	-.2319
30	27	624.82	-3.99	3.99	.0010	.0220	.0246	.0028	-.0243	.0547
30	28	623.95	-2.00	4.01	.0007	.0221	.0239	.0012	-.0109	.0241
30	29	624.82	.00	4.03	.0002	.0219	.0227	-.0005	.0019	-.0051
30	30	624.60	2.00	4.01	-.0010	.0216	.0220	-.0020	.0146	-.0333
30	31	622.87	3.98	3.98	-.0001	.0215	.0211	-.0035	.0276	-.0627
30	32	623.95	5.95	3.96	-.0001	.0214	.0204	-.0049	.0409	-.0937
30	33	623.09	7.94	3.98	.0020	.0207	.0186	-.0064	.0554	-.1278
30	34	624.60	9.93	3.96	.0046	.0199	.0168	-.0079	.0697	-.1625
30	35	623.74	11.92	3.97	.0053	.0193	.0159	-.0094	.0836	-.1983
30	36	624.17	13.88	3.97	.0068	.0183	.0161	-.0105	.0944	-.2303
30	46	624.39	-4.03	8.05	.0109	.0232	.0330	.0011	-.0238	.0549
30	45	624.39	-2.02	8.07	.0106	.0241	.0324	.0005	-.0107	.0246
30	44	623.95	-.01	8.05	.0087	.0237	.0319	-.0004	.0018	-.0036
30	43	624.60	2.02	8.07	.0109	.0237	.0310	-.0011	.0141	-.0326
30	42	624.17	4.01	8.04	.0113	.0231	.0302	-.0015	.0263	-.0611
30	41	624.17	6.00	8.00	.0127	.0223	.0288	-.0020	.0401	-.0937
30	40	624.17	8.00	8.00	.0137	.0218	.0271	-.0025	.0535	-.1254
30	39	624.29	10.12	7.79	.0157	.0208	.0248	-.0032	.0687	-.1628
30	38	623.74	11.94	7.97	.0194	.0209	.0250	-.0034	.0800	-.1943
30	37	623.74	13.92	7.95	.0221	.0205	.0235	-.0039	.0930	-.2299
30	48	623.95	-4.05	12.10	.0263	.0271	.0406	-.0003	-.0208	.0503
30	49	623.95	-2.01	12.11	.0237	.0280	.0418	-.0003	-.0095	.0219
30	50	623.74	-.02	12.14	.0239	.0282	.0412	-.0003	.0017	-.0045
30	51	623.74	1.99	12.10	.0241	.0276	.0404	-.0002	.0126	-.0311
30	52	623.74	4.01	12.11	.0268	.0269	.0377	-.0001	.0243	-.0594
30	53	623.74	6.03	12.07	.0287	.0261	.0361	.0002	.0363	-.0901
30	54	623.74	8.04	12.06	.0300	.0254	.0367	.0007	.0495	-.1228
30	55	624.17	10.03	12.02	.0345	.0255	.0345	.0011	.0627	-.1569

TABLE IV
AERODYNAMIC CHARACTERISTICS IN SIDESLIP FOR VARIOUS ANGLES OF ATTACK.
STABILITY AXES; M = 2.01

Run	Pt.	q	β , deg	α , deg	C_L	C_D	C_m	C_{l_s}	C_{n_w}	C_Y
39	35	511.11	.00	.00	.0078	.0220	.0164	.0002	-.0012	.0015
39	34	510.93	.99	.00	.0075	.0221	.0163	-.0007	.0029	-.0093
39	33	511.11	1.99	.00	.0091	.0219	.0158	-.0017	.0073	-.0232
39	32	511.11	2.97	.00	.0106	.0221	.0151	-.0027	.0114	-.0321
39	31	510.40	3.96	.00	.0105	.0217	.0146	-.0037	.0159	-.0449
39	30	510.40	5.97	-.01	.0134	.0214	.0124	-.0056	.0245	-.0687
39	29	510.76	8.01	.00	.0150	.0210	.0100	-.0077	.0340	-.0960
39	28	510.93	10.00	.00	.0181	.0202	.0068	-.0097	.0428	-.1233
39	27	510.58	12.01	.00	.0200	.0200	.0040	-.0118	.0513	-.1534
39	26	510.58	14.00	-.02	.0222	.0193	.0004	-.0140	.0598	-.1898
39	25	510.58	16.01	.00	.0243	.0186	-.0038	-.0160	.0676	-.2259
39	24	510.76	18.04	.00	.0281	.0175	-.0092	-.0181	.0757	-.2630
39	23	510.76	20.03	.00	.0301	.0172	-.0149	-.0200	.0845	-.3021
39	22	510.58	22.07	.00	.0336	.0174	-.0216	-.0217	.0937	-.3414
39	21	510.93	24.11	.00	.0371	.0174	-.0287	-.0234	.1033	-.3814
39	20	510.58	26.10	.00	.0422	.0172	-.0366	-.0252	.1134	-.4219
39	19	510.40	28.11	.00	.0473	.0174	-.0456	-.0271	.1221	-.4621
39	36	510.76	.00	4.03	.0334	.0243	.0008	.0000	-.0001	-.0010
39	37	510.76	2.00	4.01	.0318	.0245	-.0004	-.0013	.0077	-.0231
39	38	510.76	4.01	4.01	.0328	.0239	-.0031	-.0025	.0160	-.0456
39	39	510.76	6.01	4.00	.0344	.0231	-.0070	-.0039	.0249	-.0703
39	40	510.93	8.03	4.01	.0367	.0227	-.0102	-.0054	.0338	-.0964
39	41	510.58	10.02	4.00	.0412	.0227	-.0136	-.0069	.0427	-.1238
39	42	510.76	12.05	4.01	.0456	.0223	-.0186	-.0085	.0516	-.1565
39	43	510.93	14.03	4.01	.0498	.0219	-.0220	-.0100	.0603	-.1920
39	44	510.76	16.02	4.03	.0539	.0215	-.0254	-.0114	.0676	-.2280
39	45	511.11	18.05	3.99	.0577	.0206	-.0298	-.0128	.0755	-.2625
39	46	510.40	20.05	4.02	.0648	.0205	-.0349	-.0141	.0847	-.3012
39	47	510.76	22.09	3.97	.0700	.0210	-.0441	-.0153	.0947	-.3404
39	48	510.76	24.14	4.01	.0768	.0217	-.0533	-.0163	.1050	-.3814
39	41	510.58	.00	8.08	.0636	.0321	-.0230	.0001	-.0001	-.0009
39	40	510.58	2.02	8.07	.0645	.0318	-.0244	-.0006	.0076	-.0230
39	39	510.40	4.03	8.05	.0669	.0311	-.0268	-.0015	.0157	-.0465
39	38	510.76	6.02	8.06	.0702	.0304	-.0292	-.0023	.0245	-.0709
39	37	510.58	8.04	8.04	.0730	.0305	-.0324	-.0033	.0332	-.0973
39	36	510.58	10.19	7.85	.0803	.0303	-.0366	-.0045	.0419	-.1285
39	35	510.58	12.02	8.02	.0902	.0310	-.0439	-.0053	.0503	-.1592
39	34	510.93	14.03	8.01	.0954	.0310	-.0467	-.0064	.0588	-.1928
39	33	510.76	16.03	8.01	.1019	.0314	-.0508	-.0072	.0670	-.2279
39	32	510.58	18.05	8.02	.1061	.0313	-.0554	-.0078	.0751	-.2635
39	31	510.76	20.08	8.02	.1117	.0313	-.0626	-.0084	.0845	-.3008
39	30	510.93	22.13	8.05	.1189	.0323	-.0713	-.0090	.0949	-.3407
39	49	510.76	24.10	8.02	.1229	.0326	-.0775	-.0094	.1047	-.3796
39	62	511.11	.00	12.10	.0996	.0447	-.0432	.0001	-.0002	-.0008
39	63	510.58	2.01	12.09	.1001	.0438	-.0460	-.0003	.0065	-.0229
39	64	510.40	4.02	12.08	.1034	.0437	-.0510	-.0007	.0139	-.0461
39	65	510.58	6.02	12.05	.1077	.0432	-.0536	-.0013	.0217	-.0712
39	66	510.76	8.04	12.06	.1127	.0433	-.0567	-.0018	.0301	-.0986
39	67	510.76	10.04	12.04	.1201	.0443	-.0610	-.0024	.0391	-.1308
39	68	510.93	12.05	12.05	.1267	.0449	-.0653	-.0028	.0480	-.1629
39	69	510.76	14.03	12.04	.1326	.0452	-.0695	-.0031	.0570	-.1966
39	70	510.58	16.05	12.01	.1399	.0461	-.0758	-.0033	.0668	-.2322
39	71	510.76	18.07	12.05	.1477	.0477	-.0819	-.0033	.0759	-.2681
39	72	510.76	20.08	12.06	.1534	.0488	-.0882	-.0029	.0842	-.3028
39	73	510.76	22.18	12.07	.1594	.0494	-.0946	-.0028	.0938	-.3412
39	74	510.58	24.72	12.38	.1705	.0527	-.1032	-.0016	.1059	-.3910
39	87	510.40	-.03	16.13	.1492	.0665	-.0592	.0000	-.0002	-.0009
39	86	510.58	1.98	16.15	.1505	.0672	-.0618	.0001	.0055	-.0224
39	85	510.58	4.03	16.14	.1583	.0669	-.0732	-.0001	.0112	-.0454
39	84	510.58	6.03	16.11	.1661	.0669	-.0836	-.0004	.0192	-.0722
39	83	510.58	8.02	16.11	.1699	.0670	-.0846	-.0006	.0284	-.1033
39	82	510.58	10.07	16.11	.1742	.0675	-.0877	-.0005	.0376	-.1338
39	81	510.58	12.07	16.07	.1812	.0688	-.0931	-.0004	.0472	-.1672
39	80	510.76	14.06	16.08	.1859	.0696	-.0966	.0000	.0571	-.2015
39	79	510.76	16.10	16.10	.1902	.0705	-.0987	.0004	.0660	-.2356
39	78	510.58	18.12	16.09	.1934	.0716	-.1023	.0011	.0738	-.2686
39	76	510.76	20.14	16.10	.1977	.0720	-.1086	.0022	.0820	-.3032
39	75	510.76	22.19	16.10	.2019	.0729	-.1143	.0034	.0907	-.3397
39	88	511.46	-.04	20.16	.1932	.0936	-.0670	.0001	-.0004	-.0000
39	89	510.23	1.99	20.17	.1957	.0935	-.0708	.0003	.0041	-.0220
39	90	510.76	4.04	20.15	.2037	.0947	-.0843	.0004	.0102	-.0475
39	91	510.40	6.04	20.16	.2106	.0956	-.0935	.0007	.0171	-.0735
39	92	510.58	8.05	20.14	.2159	.0965	-.1022	.0013	.0264	-.1040
39	93	510.93	10.11	20.17	.2215	.0975	-.1064	.0018	.0355	-.1355
39	94	509.69	12.11	20.17	.2228	.0971	-.1066	.0024	.0439	-.1676
39	95	511.29	14.11	20.16	.2255	.0980	-.1067	.0030	.0528	-.2007
39	96	511.29	16.12	20.17	.2269	.0981	-.1065	.0041	.0616	-.2334
39	97	511.11	18.12	20.17	.2290	.0989	-.1079	.0052	.0695	-.2661
39	98	509.34	20.04	20.04	.2330	.0995	-.1126	.0065	.0777	-.2989
39	106	510.76	.00	24.27	.2369	.1289	-.0824	-.0002	-.0006	-.0009
39	105	510.76	2.03	24.30	.2395	.1293	-.0867	.0001	.0030	-.0208
39	104	510.93	4.04	24.30	.2465	.1307	-.0969	.0007	.0082	-.0459
39	103	510.58	6.07	24.26	.2518	.1311	-.1033	.0015	.0148	-.0725
39	102	510.40	8.07	24.22	.2553	.1313	-.1101	.0025	.0230	-.1024
39	101	510.76	10.04	24.21	.2600	.1322	-.1160	.0039	.0319	-.1334
39	100	511.29	12.13	24.26	.2627	.1331	-.1195	.0055	.0406	-.1664
39	99	510.58	14.13	24.17	.2636	.1327	-.1196	.0071	.0501	-.2001

TABLE IV - Continued
AERODYNAMIC CHARACTERISTICS IN SIDESLIP FOR VARIOUS ANGLES OF ATTACK.

STABILITY AXES; M = 2.01

Run	Pt.	q	β , deg	α , deg	C_L	C_D	C_m	C_{L_s}	C_{n_w}	C_y
40	32	509.16	.01	.00	-.0247	.0242	.0747	.0001	-.0014	.0022
40	31	508.45	.99	.00	-.0250	.0244	.0746	-.0008	.0028	-.0087
40	30	508.81	1.99	.00	-.0234	.0247	.0742	-.0018	.0071	-.0206
40	29	508.99	3.97	.00	-.0237	.0249	.0735	-.0037	.0154	-.0434
40	28	508.45	5.97	.00	-.0208	.0243	.0713	-.0056	.0242	-.0681
40	27	509.16	8.00	.00	-.0195	.0234	.0686	-.0075	.0333	-.0936
40	26	508.63	10.01	.02	-.0164	.0232	.0649	-.0095	.0418	-.1210
40	25	508.81	12.01	.02	-.0143	.0223	.0611	-.0114	.0498	-.1509
40	24	508.63	13.89	.02	-.0130	.0216	.0572	-.0132	.0577	-.1854
40	23	508.63	16.02	.00	-.0109	.0204	.0525	-.0153	.0655	-.2227
40	22	508.81	18.03	.00	-.0074	.0192	.0471	-.0171	.0731	-.2589
40	21	508.81	20.03	.00	-.0040	.0185	.0411	-.0187	.0816	-.2971
40	20	508.81	22.08	.00	-.0008	.0181	.0350	-.0201	.0903	-.3354
40	19	508.81	24.10	.00	.0024	.0178	.0295	-.0215	.0992	-.3747
40	18	508.63	26.12	.00	.0057	.0172	.0217	-.0229	.1086	-.4142
40	17	508.81	28.11	.00	.0077	.0176	.0163	-.0245	.1184	-.4553
40	33	508.81	.00	4.06	.0024	.0232	.0563	.0000	-.0002	-.0013
40	34	508.63	2.01	4.03	.0007	.0226	.0555	-.0011	.0073	-.0224
40	35	508.63	4.03	4.03	.0017	.0221	.0525	-.0023	.0153	-.0448
40	36	508.63	6.03	4.01	.0032	.0218	.0490	-.0037	.0241	-.0693
40	37	508.81	8.03	4.01	.0070	.0209	.0447	-.0051	.0329	-.0954
40	38	508.99	10.04	4.01	.0080	.0203	.0417	-.0065	.0412	-.1216
40	39	508.81	12.07	4.02	.0136	.0204	.0362	-.0079	.0494	-.1524
40	40	508.81	14.04	4.02	.0193	.0196	.0314	-.0093	.0576	-.1860
40	41	508.99	16.04	4.01	.0247	.0191	.0267	-.0106	.0646	-.2220
40	42	508.81	18.07	4.00	.0298	.0199	.0207	-.0117	.0716	-.2567
40	43	508.99	20.06	4.06	.0364	.0177	.0133	-.0127	.0800	-.2938
40	44	509.16	22.12	3.97	.0400	.0172	.0070	-.0137	.0895	-.3332
40	45	508.99	24.16	4.02	.0449	.0174	-.0001	-.0144	.0988	-.3724
40	56	509.16	.00	8.13	.0315	.0256	.0320	.0000	-.0002	-.0012
40	55	508.63	2.03	8.11	.0323	.0253	.0313	-.0006	.0071	-.0224
40	54	508.63	4.05	8.08	.0329	.0245	.0295	-.0015	.0149	-.0449
40	53	508.63	6.05	8.05	.0404	.0242	.0225	-.0030	.0313	-.0945
40	52	508.81	8.05	8.04	.0572	.0242	.0098	-.0048	.0473	-.1561
40	51	508.81	10.04	8.02	.0637	.0243	.0052	-.0057	.0551	-.1879
40	50	508.63	12.05	8.02	.0713	.0246	-.0011	-.0064	.0623	-.2219
40	49	508.81	14.04	8.04	.0766	.0244	-.0072	-.0069	.0691	-.2544
40	48	508.63	16.06	8.03	.0836	.0244	-.0146	-.0071	.0772	-.2908
40	47	508.63	18.06	8.06	.0907	.0245	-.0222	-.0075	.0866	-.3288
40	46	508.81	20.13	8.03	.0944	.0243	-.0275	-.0077	.0961	-.3676
40	57	508.99	.00	12.12	.0672	.0343	.0124	.0000	-.0003	-.0012
40	58	508.63	2.01	12.13	.0689	.0342	.0097	-.0003	.0057	-.0221
40	59	508.81	4.03	12.11	.0735	.0337	.0043	-.0007	.0124	-.0444
40	60	508.81	6.06	12.07	.0843	.0332	-.0027	-.0018	.0272	-.0957
40	61	508.63	8.08	12.08	.0991	.0351	-.0142	-.0025	.0432	-.1570
40	62	508.81	10.09	12.04	.1144	.0362	-.0271	-.0029	.0587	-.2219
40	63	508.81	12.09	11.52	.1169	.0352	-.0333	-.0031	.0707	-.2733
40	64	508.81	14.09	11.52	.1169	.0352	-.0333	-.0031	.0707	-.2733
40	65	508.99	16.09	12.39	.1473	.0411	-.0622	-.0006	.0975	-.3789
40	73	508.99	.00	16.14	.1192	.0532	-.0063	.0000	-.0002	-.0012
40	72	508.99	2.01	16.18	.1220	.0538	-.0093	.0001	.0041	-.0206
40	71	508.99	4.01	16.17	.1277	.0531	-.0195	-.0005	.0082	-.0406
40	70	508.99	6.03	16.14	.1386	.0531	-.0305	-.0009	.0227	-.0943
40	69	508.99	8.07	16.11	.1508	.0543	-.0395	-.0007	.0387	-.1550
40	68	509.16	10.13	16.13	.1621	.0559	-.0519	.0002	.0557	-.2203
40	67	508.81	12.18	16.13	.1773	.0590	-.0696	.0022	.0733	-.2903
40	66	508.99	14.19	16.16	.1843	.0608	-.0791	.0038	.0827	-.3278
40	74	508.99	.00	20.19	.1719	.0797	-.0266	.0000	-.0004	-.0003
40	75	509.16	1.99	20.20	.1747	.0798	-.0306	-.0002	.0016	-.0191
40	76	508.99	3.97	20.19	.1811	.0799	-.0414	-.0004	.0049	-.0394
40	77	508.99	5.97	20.18	.1930	.0810	-.0569	.0001	.0182	-.0917
40	78	508.99	8.07	20.19	.2004	.0815	-.0642	.0014	.0350	-.1531
40	79	508.99	10.14	20.19	.2097	.0837	-.0721	.0034	.0539	-.2218
40	80	508.99	12.07	20.07	.2163	.0855	-.0808	.0058	.0705	-.2882
40	86	508.99	.00	24.28	.2206	.1143	-.0485	-.0002	-.0011	.0008
40	85	508.81	1.99	24.33	.2239	.1148	-.0536	-.0004	-.0004	-.0158
40	84	508.81	3.97	24.32	.2295	.1147	-.0634	-.0003	.0028	-.0368
40	83	508.81	5.97	24.23	.2407	.1161	-.0800	.0015	.0169	-.0823
40	82	508.99	8.07	24.29	.2499	.1187	-.0901	.0043	.0338	-.1565
40	81	508.99	10.11	24.22	.2516	.1185	-.0916	.0058	.0432	-.1891

TABLE IV - Continued
AERODYNAMIC CHARACTERISTICS IN SIDESLIP FOR VARIOUS ANGLES OF ATTACK.

STABILITY AXES: M = 2.01

Run	Pt.	q	β , deg	α , deg	C_L	C_D	C_m	C_{L_s}	$C_{n,w}$	C_Y
41	21	509.34	.00	.00	-.0118	.0241	.0511	.0001	-.0013	+.0022
41	20	509.16	1.99	.00	-.0123	.0252	.0519	-.0012	.0087	-.0227
41	19	508.99	3.96	.00	-.0112	.0249	.0524	-.0025	.0188	-.0486
41	18	509.16	5.96	.00	-.0118	.0241	.0530	-.0038	.0287	-.0744
41	17	509.16	8.00	.00	-.0120	.0236	.0541	-.0052	.0393	-.1031
41	16	509.16	11.98	.00	-.0154	.0234	.0597	-.0075	.0585	-.1637
41	15	509.16	15.98	.03	-.0223	.0229	.0712	-.0096	.0767	-.2385
41	14	509.34	19.99	.00	-.0322	.0222	.0843	-.0117	.0950	-.3162
41	13	508.99	24.07	.00	-.0394	.0225	.0953	-.0135	.1105	-.3907
41	12	508.99	28.12	.00	-.0471	.0241	.1042	-.0155	.1180	-.4561
41	22	509.34	.00	4.05	.0150	.0235	.0321	.0000	.0000	-.0012
41	23	509.52	2.01	4.03	.0139	.0229	.0324	-.0005	.0085	-.0235
41	24	509.69	4.01	4.01	.0120	.0227	.0333	-.0012	.0178	-.0472
41	25	509.34	8.02	4.00	.0111	.0217	.0352	-.0025	.0370	-.1003
41	26	509.34	12.05	4.01	.0132	.0213	.0388	-.0039	.0553	-.1606
41	27	509.34	16.01	4.00	.0115	.0209	.0482	-.0047	.0722	-.2324
41	28	509.52	20.03	4.01	.0082	.0201	.0611	-.0052	.0890	-.3085
41	29	509.52	24.14	4.01	.0003	.0205	.0742	-.0059	.1094	-.3880
41	37	509.87	.00	8.10	.0415	.0268	.0146	.0000	.0000	-.0012
41	36	509.69	2.03	8.10	.0423	.0260	.0146	-.0001	.0080	-.0234
41	35	509.69	4.05	8.08	.0431	.0251	.0140	-.0003	.0162	-.0469
41	34	509.34	8.04	8.04	.0457	.0247	.0147	-.0002	.0337	-.0979
41	33	509.69	12.04	8.03	.0542	.0251	.0153	-.0002	.0506	-.1598
41	32	509.52	16.05	8.02	.0559	.0250	.0249	-.0001	.0663	-.2268
41	31	509.69	20.10	8.03	.0532	.0249	.0372	.0004	.0821	-.2976
41	30	509.52	24.12	8.03	.0475	.0247	.0497	.0011	.1021	-.3767
41	38	509.52	.00	12.12	.0771	.0357	-.0040	.0000	-.0002	-.0002
41	39	509.69	4.03	12.11	.0804	.0344	-.0062	.0004	.0125	-.0434
41	40	509.69	8.03	12.09	.0873	.0341	-.0076	.0011	.0277	-.0958
41	41	509.52	12.06	12.10	.0938	.0353	-.0049	.0025	.0438	-.1573
41	42	509.52	16.07	12.07	.0967	.0358	.0028	.0035	.0593	-.2223
41	43	510.05	20.12	12.12	.0961	.0362	.0128	.0052	.0745	-.2897
41	44	509.52	24.76	12.40	.0952	.0373	.0246	.0080	.0966	-.3784
41	52	509.87	.00	16.14	.1287	.0550	-.0232	.0000	-.0003	-.0002
41	51	509.69	2.01	16.17	.1315	.0549	-.0250	.0004	.0036	-.0195
41	50	509.52	4.04	16.16	.1343	.0539	-.0292	.0007	.0075	-.0395
41	49	509.52	8.05	16.13	.1414	.0538	-.0328	.0020	.0214	-.0924
41	48	509.87	12.12	16.13	.1446	.0544	-.0282	.0042	.0366	-.1520
41	47	509.69	16.16	16.16	.1465	.0550	-.0220	.0065	.0521	-.2163
41	46	509.69	20.21	16.15	.1439	.0544	-.0123	.0091	.0673	-.2821
41	45	510.05	22.26	16.16	.1435	.0557	-.0075	.0106	.0764	-.3195
41	53	510.23	.00	20.17	.1809	.0825	-.0435	.0000	-.0003	-.0002
41	54	509.87	1.99	20.18	.1820	.0823	-.0458	.0002	.0005	-.0169
41	55	509.87	4.01	20.19	.1864	.0823	-.0507	.0002	.0027	-.0343
41	56	510.05	7.96	20.02	.1891	.0800	-.0541	.0020	.0149	-.0856
41	57	509.87	12.09	20.22	.1947	.0818	-.0534	.0053	.0289	-.1456
41	58	509.87	16.15	20.21	.1952	.0822	-.0479	.0087	.0449	-.2101
41	59	509.69	20.09	20.09	.1928	.0824	-.0399	.0124	.0610	-.2757
41	65	509.69	.00	24.28	.2324	.1189	-.0683	-.0002	-.0010	-.0009
41	64	509.69	2.03	24.31	.2351	.1195	-.0717	-.0004	-.0023	-.0135
41	63	509.69	4.04	24.32	.2386	.1193	-.0771	-.0001	-.0007	-.0315
41	62	509.87	8.08	24.26	.2431	.1182	-.0821	.0023	.0102	-.0827
41	61	509.87	12.15	24.31	.2452	.1186	-.0808	.0063	.0238	-.1418
41	60	510.05	14.12	24.25	.2445	.1185	-.0784	.0084	.0317	-.1731

TABLE IV - Continued
 AERODYNAMIC CHARACTERISTICS IN SIDESLIP FOR VARIOUS ANGLES OF ATTACK.
 STABILITY AXES; M = 2.01

Run	Pt.	q	β ,deg	α ,deg	C_L	C_D	C_m	$C_{l,s}$	$C_{n,w}$	C_y
42	21	512.00	.00	.00	.0102	.0215	.0044	.0010	-.0012	.0016
42	20	511.82	.99	.00	.0099	.0216	.0043	.0003	.0034	-.0103
42	19	511.46	1.99	.00	.0112	.0220	.0042	-.0005	.0079	-.0221
42	18	511.11	3.96	.00	.0122	.0218	.0042	-.0019	.0167	-.0450
42	17	510.58	5.97	.00	.0119	.0214	.0045	-.0034	.0262	-.0707
42	16	512.35	8.00	.00	.0116	.0209	.0053	-.0048	.0356	-.0978
42	15	511.82	11.99	.00	.0119	.0195	.0096	-.0076	.0533	-.1561
42	14	512.17	16.00	.00	.0017	.0182	.0200	-.0103	.0700	-.2293
42	13	511.29	20.02	.00	-.0062	.0170	.0325	-.0130	.0870	-.3041
42	12	512.17	24.08	.00	-.0154	.0173	.0459	-.0154	.1062	-.3847
42	11	512.17	28.12	.05	-.0209	.0166	.0558	-.0174	.1186	-.4561
42	22	511.64	.00	4.01	.0367	.0248	-.0147	.0000	-.0001	-.0009
42	23	511.82	2.00	4.01	.0341	.0240	-.0144	-.0007	.0078	-.0230
42	24	511.64	4.00	4.00	.0337	.0236	-.0147	-.0012	.0164	-.0464
42	25	511.82	8.02	4.00	.0344	.0225	-.0144	-.0026	.0339	-.0962
42	26	511.64	12.05	4.01	.0367	.0215	-.0112	-.0043	.0511	-.1552
42	27	511.64	16.01	4.00	.0354	.0203	-.0025	-.0057	.0664	-.2246
42	28	511.82	20.04	4.05	.0325	.0184	.0092	-.0069	.0823	-.2972
42	29	511.64	24.16	4.02	.0265	.0184	.0218	-.0082	.1013	-.3764
42	37	512.17	.00	8.06	.0654	.0314	-.0367	.0000	-.0001	-.0008
42	36	512.53	2.00	8.05	.0647	.0309	-.0365	-.0002	.0072	-.0228
42	35	512.17	4.03	8.05	.0656	.0301	-.0369	-.0005	.0150	-.0452
42	34	512.00	8.03	8.03	.0702	.0290	-.0371	-.0008	.0314	-.0958
42	33	511.64	12.01	8.02	.0788	.0289	-.0364	-.0010	.0471	-.1555
42	32	512.35	16.05	8.02	.0792	.0282	-.0269	-.0015	.0618	-.2208
42	31	511.64	20.09	8.03	.0785	.0268	-.0171	-.0017	.0763	-.2896
42	30	511.82	24.13	8.03	.0746	.0260	-.0063	-.0016	.0948	-.3660
42	38	512.17	.00	12.07	.1030	.0447	-.0594	.0001	-.0002	-.0007
42	39	512.00	1.98	12.08	.1031	.0442	-.0601	-.0001	.0049	-.0196
42	40	512.00	4.02	12.08	.1048	.0431	-.0613	.0000	.0115	-.0427
42	41	512.17	8.03	12.04	.1136	.0430	-.0627	.0004	.0256	-.0938
42	42	512.35	12.06	12.06	.1188	.0431	-.0594	.0012	.0410	-.1538
42	43	512.00	16.09	12.04	.1223	.0430	-.0519	.0017	.0556	-.2176
42	44	512.17	20.13	12.08	.1222	.0423	-.0427	.0029	.0696	-.2828
42	45	512.17	24.76	12.40	.1246	.0431	-.0341	.0046	.0901	-.3686
42	53	511.11	-.03	16.10	.1577	.0687	-.0846	.0001	-.0004	-.0007
42	52	511.11	1.97	16.12	.1587	.0689	-.0860	.0001	.0030	-.0189
42	51	510.93	4.03	16.13	.1635	.0683	-.0899	.0002	.0066	-.0388
42	50	513.94	8.05	16.11	.1683	.0668	-.0921	.0009	.0197	-.0900
42	49	512.35	12.10	16.10	.1713	.0663	-.0868	.0027	.0340	-.1486
42	48	512.00	16.13	16.13	.1724	.0661	-.0790	.0043	.0487	-.2117
42	47	512.17	20.19	16.13	.1728	.0658	-.0716	.0063	.0630	-.2759
42	46	512.00	22.24	16.14	.1715	.0657	-.0679	.0075	.0717	-.3124
42	54	511.11	.00	20.13	.2109	.1014	-.1091	.0001	-.0005	-.0006
42	55	511.29	2.02	20.13	.2120	.1006	-.1111	-.0001	.0001	-.0164
42	56	511.64	4.04	20.14	.2166	.1004	-.1165	-.0003	.0023	-.0346
42	57	511.82	8.05	20.13	.2225	.0998	-.1208	.0009	.0139	-.0865
42	58	511.46	12.11	20.17	.2242	.0989	-.1179	.0034	.0270	-.1426
42	59	511.64	16.09	20.20	.2263	.0995	-.1133	.0062	.0421	-.2048
42	60	511.64	20.08	20.08	.2229	.0982	-.1047	.0094	.0572	-.2690
42	66	511.46	.00	24.22	.2627	.1420	-.1368	-.0002	-.0011	.0004
42	65	511.11	2.03	24.26	.2642	.1417	-.1398	-.0006	-.0027	-.0129
42	64	510.76	3.99	24.29	.2693	.1428	-.1457	-.0007	-.0014	-.0308
42	63	510.40	8.05	24.18	.2715	.1401	-.1500	.0010	.0089	-.0810
42	62	511.46	12.13	24.26	.2751	.1401	-.1494	.0044	.0222	-.1387
42	61	511.82	14.14	24.19	.2745	.1399	-.1472	.0065	.0300	-.1699

TABLE IV - Continued
 AERODYNAMIC CHARACTERISTICS IN SIDESLIP FOR VARIOUS ANGLES OF ATTACK.
 STABILITY AXES; M = 2.01

Run	Pt.	q	β ,deg	α ,deg	C_L	C_D	C_m	C_{L_s}	$C_{n,w}$	C_Y
43	23	510.76	.00	.00	-.0067	.0303	.0080	.0003	-.0008	.0015
43	22	510.58	2.00	.00	-.0064	.0299	.0075	.0000	.0084	-.0259
43	21	510.76	3.98	.00	-.0046	.0295	.0055	-.0002	.0174	-.0532
43	20	510.40	5.98	.01	-.0027	.0293	.0030	-.0004	.0267	-.0815
43	19	510.76	8.01	.01	-.0010	.0290	.0003	-.0003	.0358	-.1106
43	18	510.40	12.03	.02	.0035	.0282	-.0049	.0008	.0523	-.1722
43	17	510.58	16.04	.00	.0096	.0270	.0012	.0031	.0654	-.2385
43	16	510.23	20.07	.00	-.0288	.0270	.0114	.0058	.0791	-.3106
43	15	510.76	24.14	.00	-.0525	.0275	.0259	.0069	.0951	-.3881
43	14	510.23	28.17	.00	-.0756	.0275	.0420	.0072	.1116	-.4665
43	24	510.76	.00	4.17	.1901	.0433	-.0484	.0001	.0001	-.0011
43	25	510.23	2.06	4.12	.1843	.0426	-.0482	.0003	.0078	-.0241
43	26	510.40	4.08	4.08	.1791	.0418	-.0479	.0006	.0158	-.0480
43	27	510.23	6.08	4.06	.1800	.0411	-.0496	.0012	.0242	-.0742
43	28	510.58	8.07	4.04	.1802	.0412	-.0516	.0018	.0329	-.1022
43	29	510.05	12.11	4.03	.1828	.0408	-.0547	.0041	.0482	-.1596
43	30	510.23	16.05	4.01	.1681	.0387	-.0468	.0067	.0611	-.2236
43	31	510.23	20.09	4.03	.1459	.0362	-.0330	.0092	.0759	-.2971
43	32	510.05	24.19	4.02	.1157	.0346	-.0124	.0104	.0943	-.3779
43	41	509.87	.00	8.38	.3765	.0846	-.1059	.0004	-.0001	.0006
43	40	510.23	2.09	8.34	.3753	.0841	-.1062	.0013	.0074	-.0230
43	39	510.05	4.16	8.30	.3738	.0830	-.1070	.0021	.0148	-.0458
43	38	510.23	6.17	8.25	.3750	.0824	-.1088	.0027	.0224	-.0698
43	37	509.87	8.20	8.20	.3741	.0818	-.1099	.0036	.0297	-.0948
43	36	510.05	12.16	8.11	.3689	.0796	-.1091	.0057	.0433	-.1505
43	35	510.05	16.16	8.07	.3517	.0759	-.0996	.0081	.0579	-.2164
43	34	509.87	20.16	8.10	.3257	.0720	-.0821	.0104	.0727	-.2866
43	33	510.40	24.19	8.06	.2924	.0666	-.0594	.0118	.0913	-.3651
43	42	510.23	.00	12.57	.5564	.1531	-.1625	.0003	-.0005	.0023
43	43	509.87	2.08	12.53	.5547	.1526	-.1626	.0009	.0063	-.0200
43	44	510.05	4.14	12.50	.5531	.1516	-.1633	.0015	.0129	-.0419
43	45	510.05	6.22	12.43	.5511	.1497	-.1634	.0020	.0193	-.0658
43	46	509.87	8.24	12.38	.5520	.1483	-.1660	.0025	.0252	-.0893
43	47	510.40	12.29	12.29	.5388	.1434	-.1598	.0045	.0385	-.1448
43	48	510.05	16.26	12.22	.5221	.1385	-.1492	.0065	.0534	-.2089
43	49	510.05	20.29	12.19	.4968	.1322	-.1327	.0089	.0685	-.2754
43	50	509.69	24.88	12.52	.4703	.1289	-.1094	.0107	.0889	-.3611
43	58	510.23	.00	16.71	.7279	.2478	-.2180	.0003	-.0008	.0041
43	57	510.05	2.08	16.72	.7287	.2481	-.2192	.0004	.0052	-.0185
43	56	509.69	4.18	16.70	.7282	.2472	-.2201	.0004	.0112	-.0411
43	55	510.05	6.21	16.65	.7262	.2448	-.2201	.0006	.0164	-.0633
43	54	509.69	8.27	16.60	.7228	.2425	-.2183	.0008	.0216	-.0870
43	53	510.05	12.28	16.47	.7103	.2357	-.2100	.0018	.0343	-.1395
43	52	509.87	16.42	16.42	.6960	.2298	-.2004	.0030	.0490	-.1988
43	51	509.87	20.46	16.36	.6674	.2206	-.1834	.0049	.0646	-.2642
43	59	510.05	.00	20.88	.8896	.3679	-.2758	.0000	-.0014	.0059
43	60	510.05	2.06	20.88	.8876	.3670	-.2766	-.0001	.0042	-.0173
43	61	510.23	4.19	20.82	.8859	.3646	-.2777	-.0007	.0096	-.0391
43	62	509.69	6.26	20.83	.8831	.3634	-.2760	-.0015	.0145	-.0605
43	63	510.05	8.32	20.77	.8800	.3606	-.2733	-.0015	.0189	-.0821
43	64	509.87	12.46	20.71	.8650	.3533	-.2614	-.0005	.0304	-.1327
43	65	509.52	16.51	20.64	.8467	.3441	-.2498	.0006	.0447	-.1898
43	65	510.05	20.40	20.47	.8182	.3307	-.2330	.0022	.0605	-.2505
43	72	510.40	.00	25.10	1.0381	.5145	-.3339	-.0005	-.0023	.0078
43	71	510.05	2.11	25.14	1.0386	.5158	-.3345	-.0011	.0022	-.0132
43	70	510.23	4.20	25.13	1.0372	.5143	-.3348	-.0018	.0072	-.0345
43	69	510.05	6.30	25.06	1.0326	.5098	-.3330	-.0022	.0116	-.0553
43	68	510.40	8.31	25.01	1.0259	.5054	-.3288	-.0026	.0152	-.0753
43	67	510.05	12.53	24.99	1.0116	.4976	-.3156	-.0018	.0262	-.1235

TABLE IV - Continued
AERODYNAMIC CHARACTERISTICS IN SIDESLIP FOR VARIOUS ANGLES OF ATTACK.

STABILITY AXES; M = 2.01

Run	Pt.	q	β ,deg	α ,deg	C_L	C_D	C_m	$C_{l,s}$	$C_{n,w}$	C_y
44	22	510.58	.00	.00	-.0399	.0340	.0586	.0002	-.0010	+.0012
44	21	510.58	.99	.00	-.0388	.0340	.0584	.0001	.0040	-.0126
44	20	510.58	2.00	.00	-.0379	.0335	.0578	.0000	.0089	-.0263
44	19	510.40	3.97	.00	-.0361	.0336	.0565	-.0001	.0185	-.0538
44	18	510.05	5.98	.00	-.0359	.0328	.0549	-.0001	.0283	-.0832
44	17	510.93	8.01	.00	-.0341	.0324	.0526	.0000	.0381	-.1142
44	16	510.76	12.01	.02	-.0312	.0325	.0493	.0015	.0565	-.1779
44	15	510.76	16.02	.03	-.0443	.0319	.0577	.0043	.0716	-.2464
44	14	510.40	20.05	.00	-.0653	.0320	.0681	.0074	.0875	-.3227
44	13	510.23	24.13	.00	-.0866	.0322	.0791	.0091	.1036	-.4007
44	12	510.40	28.15	.00	-.1101	.0328	.0917	.0096	.1190	-.4774
44	23	510.58	-.01	4.20	.1551	.0425	.0020	.0001	.0000	-.0005
44	24	510.58	2.07	4.15	.1525	.0419	.0016	.0004	.0003	-.0245
44	25	510.58	4.08	4.09	.1489	.0413	.0015	.0009	.0169	-.0494
44	26	510.58	6.07	4.06	.1465	.0409	.0014	.0015	.0258	-.0758
44	27	510.58	8.08	4.03	.1486	.0409	-.0003	.0024	.0353	-.1049
44	28	510.40	12.12	4.04	.1496	.0409	-.0005	.0051	.0519	-.1652
44	29	510.58	16.05	4.01	.1334	.0393	.0102	.0081	.0670	-.2323
44	30	510.40	20.07	4.02	.1092	.0373	.0249	.0114	.0839	-.3091
44	31	510.58	24.18	4.02	.0819	.0361	.0421	.0131	.1034	-.3908
44	40	510.58	.00	8.41	.3450	.0800	-.0532	.0004	-.0002	+.0002
44	39	510.93	2.11	8.39	.3438	.0796	-.0535	.0014	.0080	-.0234
44	38	510.58	4.18	8.33	.3408	.0784	-.0535	.0023	.0159	-.0472
44	37	510.58	6.18	8.27	.3406	.0778	-.0546	.0031	.0237	-.0713
44	36	510.40	8.20	8.23	.3408	.0776	-.0557	.0042	.0317	-.0972
44	35	510.58	12.18	8.13	.3343	.0753	-.0534	.0067	.0464	-.1550
44	34	510.76	16.16	8.08	.3153	.0720	-.0420	.0097	.0628	-.2230
44	33	510.58	20.17	8.06	.2892	.0685	-.0240	.0129	.0799	-.2974
44	41	510.93	.00	12.61	.5243	.1445	-.1056	.0002	-.0005	+.0020
44	42	510.40	2.09	12.57	.5213	.1430	-.1053	.0010	.0066	-.0204
44	43	510.93	4.18	12.53	.5194	.1422	-.1057	.0017	.0137	-.0433
44	44	510.76	6.21	12.47	.5172	.1406	-.1059	.0023	.0204	-.0672
44	45	510.23	8.25	12.41	.5169	.1389	-.1080	.0032	.0269	-.0917
44	46	510.93	12.29	12.29	.5050	.1345	-.1020	.0057	.0413	-.1493
44	47	510.76	16.26	12.22	.4880	.1303	-.0911	.0084	.0576	-.2154
44	48	510.93	20.26	12.22	.4624	.1247	-.0736	.0115	.0746	-.2848
44	49	510.93	24.88	12.52	.4350	.1224	-.0505	.0142	.0961	-.3722
44	57	510.93	-.03	16.74	.6957	.2336	-.1578	.0001	-.0008	+.0037
44	56	510.76	2.09	16.76	.6964	.2340	-.1590	.0004	.0054	-.0189
44	55	510.93	4.19	16.74	.6968	.2335	-.1603	.0007	.0116	-.0424
44	54	510.58	6.23	16.69	.6940	.2313	-.1597	.0009	.0174	-.0647
44	53	510.76	8.28	16.63	.6899	.2285	-.1579	.0014	.0228	-.0884
44	52	510.93	12.41	16.51	.6790	.2230	-.1491	.0031	.0364	-.1437
44	51	510.93	16.43	16.43	.6612	.2164	-.1389	.0049	.0523	-.2049
44	50	511.29	20.47	16.37	.6349	.2090	-.1223	.0074	.0692	-.2721
44	58	510.40	-.04	20.93	.8581	.3493	-.2125	-.0002	-.0016	+.0064
44	59	510.93	2.11	20.92	.8569	.3486	-.2135	-.0002	.0043	-.0177
44	60	510.93	4.16	20.89	.8554	.3466	-.2144	-.0006	.0099	-.0403
44	61	510.76	6.23	20.87	.8532	.3459	-.2135	-.0010	.0150	-.0626
44	62	510.76	8.34	20.82	.8477	.3428	-.2100	-.0010	.0198	-.0844
44	63	510.76	12.48	20.75	.8338	.3357	-.1981	.0007	.0319	-.1358
44	64	511.11	16.52	20.66	.8154	.3270	-.1857	.0024	.0467	-.1936
44	65	510.93	20.46	20.46	.7849	.3140	-.1684	.0047	.0639	-.2567
44	72	511.29	.00	25.15	1.0090	.4929	-.2690	-.0006	-.0024	+.0082
44	71	511.29	2.12	25.19	1.0076	.4927	-.2692	-.0011	.0024	-.0135
44	69	510.93	4.20	25.17	1.0059	.4909	-.2698	-.0016	.0076	-.0358
44	70	511.11	6.31	25.10	1.0032	.4879	-.2681	-.0019	.0119	-.0565
44	68	510.93	8.33	25.05	.9949	.4823	-.2638	-.0021	.0161	-.0775
44	67	511.11	12.54	25.02	.9804	.4755	-.2519	-.0008	.0275	-.1265
44	66	510.93	14.59	24.89	.9682	.4668	-.2425	.0000	.0338	-.1524

TABLE IV - Continued
 AERODYNAMIC CHARACTERISTICS IN SIDESLIP FOR VARIOUS ANGLES OF ATTACK.
 STABILITY AXES; M = 2.01

Run	Pt.	q	β , deg	α , deg	C_L	C_D	C_m	$C_{i,s}$	$C_{n,w}$	C_Y
45	23	511.64	-0.01	0.00	-.0589	.0347	.0868	.0003	-.0013	.0030
45	22	511.64	.99	0.00	-.0594	.0347	.0869	.0001	.0035	-.0116
45	21	511.64	1.99	0.00	-.0585	.0343	.0860	-.0001	.0078	-.0243
45	20	511.64	3.98	0.01	-.0566	.0344	.0834	-.0006	.0165	-.0506
45	19	511.64	5.99	0.01	-.0547	.0339	.0795	-.0011	.0255	-.0788
45	18	511.64	8.01	0.01	-.0514	.0331	.0735	-.0014	.0343	-.1078
45	17	511.64	12.04	0.02	-.0404	.0319	.0575	-.0013	.0508	-.1701
45	16	511.82	16.04	0.03	-.0486	.0305	.0535	-.0002	.0629	-.2341
45	15	511.82	20.07	0.00	-.0583	.0296	.0475	.0010	.0760	-.3057
45	14	510.76	24.16	0.00	-.0674	.0287	.0382	.0012	.0907	-.3819
45	13	511.29	28.18	0.05	-.0724	.0277	.0261	.0006	.1058	-.4579
45	24	510.76	.00	4.22	.1277	.0422	.0448	.0001	-.0002	.0002
45	25	511.64	2.08	4.17	.1233	.0416	.0434	-.0001	.0072	-.0227
45	26	512.00	4.11	4.11	.1228	.0411	.0395	.0001	.0152	-.0464
45	27	511.64	8.11	4.04	.1302	.0402	.0261	.0005	.0318	-.0996
45	28	512.00	12.13	4.04	.1421	.0394	.0085	.0015	.0470	-.1583
45	29	510.58	16.07	4.02	.1370	.0377	-.0020	.0027	.0597	-.2215
45	30	511.29	20.10	4.06	.1316	.0350	-.0132	.0038	.0744	-.2944
45	31	510.93	24.20	4.07	.1177	.0330	-.0223	.0042	.0930	-.3750
45	39	510.93	.00	8.45	.3176	.0781	-.0069	.0005	-.0004	.0018
45	38	510.76	2.11	8.42	.3157	.0771	-.0087	.0007	.0073	-.0217
45	37	510.76	4.17	8.35	.3155	.0762	-.0135	.0010	.0146	-.0443
45	36	510.76	8.22	8.22	.3232	.0751	-.0316	.0015	.0273	-.0932
45	35	510.93	12.19	8.14	.3306	.0736	-.0508	.0021	.0430	-.1486
45	34	511.11	16.13	8.10	.3270	.0711	-.0662	.0032	.0583	-.2160
45	33	510.76	20.17	8.06	.3161	.0672	-.0760	.0047	.0745	-.2883
45	32	511.11	24.18	8.05	.2989	.0634	-.0784	.0055	.0918	-.3654
45	40	510.76	.00	12.62	.5046	.1411	-.0738	.0003	-.0006	.0027
45	41	510.93	2.09	12.59	.5031	.1401	-.0756	-.0001	.0066	-.0204
45	42	510.76	4.16	12.55	.5038	.1392	-.0805	-.0003	.0134	-.0423
45	43	510.76	8.28	12.40	.5079	.1364	-.0949	-.0010	.0269	-.0906
45	44	510.93	12.31	12.31	.5091	.1336	-.1094	-.0002	.0419	-.1490
45	45	510.76	16.28	12.19	.5056	.1302	-.1236	.0015	.0590	-.2161
45	46	510.76	20.28	12.18	.4948	.1264	-.1293	.0036	.0738	-.2823
45	47	510.76	24.89	12.47	.4830	.1254	-.1344	.0054	.0933	-.3665
45	55	510.93	-0.03	16.76	.6839	.2313	-.1434	.0001	-.0011	.0055
45	54	510.76	2.12	16.77	.6840	.2311	-.1438	-.0002	.0059	-.0190
45	53	510.76	4.19	16.75	.6823	.2299	-.1436	-.0009	.0129	-.0425
45	52	510.76	8.32	16.62	.6850	.2260	-.1519	-.0022	.0265	-.0925
45	51	510.76	12.39	16.49	.6854	.2228	-.1634	-.0021	.0417	-.1497
45	50	510.76	16.42	16.42	.6793	.2179	-.1714	-.0009	.0573	-.2099
45	49	510.76	20.46	16.36	.6624	.2117	-.1736	.0011	.0702	-.2719
45	48	510.76	22.47	16.32	.6513	.2077	-.1746	.0024	.0783	-.3062
45	56	510.76	-0.04	20.93	.8377	.3435	-.1837	-.0003	-.0019	.0072
45	57	510.76	2.07	20.94	.8395	.3437	-.1884	-.0008	.0055	-.0179
45	58	510.76	4.16	20.89	.8429	.3431	-.1979	-.0017	.0128	-.0435
45	59	510.76	8.34	20.83	.8426	.3411	-.2032	-.0033	.0261	-.0925
45	60	510.58	12.47	20.74	.8401	.3359	-.2102	-.0029	.0391	-.1440
45	61	510.76	16.52	20.65	.8300	.3289	-.2138	-.0013	.0527	-.2007
45	62	511.11	20.44	20.44	.8094	.3177	-.2131	.0006	.0670	-.2603
45	68	510.93	-0.05	25.17	.9902	.4868	-.2380	-.0008	-.0028	.0100
45	67	510.76	2.12	25.20	.9830	.4841	-.2363	-.0017	.0043	-.0149
45	66	510.76	4.16	25.20	.9888	.4864	-.2387	-.0025	.0117	-.0402
45	65	510.76	8.38	25.05	.9815	.4785	-.2400	-.0037	.0214	-.0838
45	64	511.11	12.54	25.02	.9777	.4732	-.2491	-.0029	.0353	-.1358
45	63	510.58	14.57	24.86	.9661	.4632	-.2455	-.0022	.0409	-.1616

TABLE IV - Continued
AERODYNAMIC CHARACTERISTICS IN SIDESLIP FOR VARIOUS ANGLES OF ATTACK.

STABILITY AXES; M = 2.01

Run	Pt.	q	β , deg	α , deg	C_L	C_D	C_m	$C_{l,s}$	$C_{n,w}$	C_Y
46	23	510.58	-0.01	0.00	-0.0281	.0299	.0297	.0003	-.0010	.0016
46	22	509.69	.99	0.00	-0.0272	.0300	.0294	.0001	.0033	-.0112
46	21	509.34	1.99	0.00	-0.0261	.0300	.0284	-.0002	.0080	-.0259
46	20	510.23	3.97	0.01	-0.0241	.0296	.0280	-.0007	.0169	-.0522
46	19	509.34	5.98	0.01	-0.0222	.0289	.0222	-.0012	.0257	-.0797
46	18	510.40	8.03	0.01	-0.0187	.0281	.0171	-.0015	.0350	-.1097
46	17	509.16	12.04	0.02	-0.0106	.0278	.0044	-.0016	.0516	-.1716
46	16	509.16	16.04	0.03	-0.0184	.0266	.0023	-.0009	.0644	-.2371
46	15	509.16	20.08	0.04	-0.0277	.0266	-.0045	-.0001	.0781	-.3100
46	14	508.81	24.15	0.04	-0.0347	.0268	-.0158	-.0004	.0940	-.3872
46	13	508.99	28.18	0.00	-0.0412	.0267	-.0306	-.0017	.1104	-.4662
46	24	510.40	.00	4.19	.1563	.0404	-.0058	.0001	-.0001	-.0004
46	25	510.05	2.07	4.14	.1505	.0397	-.0070	.0000	.0075	-.0234
46	26	509.52	4.09	4.09	.1502	.0393	-.0106	.0001	.0155	-.0473
46	27	510.40	8.10	4.04	.1560	.0385	-.0224	.0005	.0323	-.1005
46	28	510.05	12.11	4.03	.1668	.0385	-.0393	.0012	.0481	-.1597
46	29	510.23	16.06	4.01	.1650	.0376	-.0501	.0017	.0616	-.2237
46	30	510.05	20.08	4.02	.1558	.0359	-.0614	.0020	.0788	-.3013
46	31	510.23	24.17	4.02	.1485	.0351	-.0736	.0020	.0986	-.3847
46	39	510.23	-0.01	8.42	.3404	.0790	-.0508	.0004	-.0003	.0012
46	38	510.40	2.11	8.39	.3400	.0784	-.0528	.0006	.0075	-.0223
46	37	510.23	4.17	8.31	.3402	.0772	-.0579	.0008	.0152	-.0461
46	36	510.23	8.19	8.19	.3495	.0771	-.0779	.0011	.0307	-.0960
46	35	510.05	12.16	8.11	.3574	.0766	-.0967	.0016	.0453	-.1527
46	34	510.23	16.15	8.07	.3545	.0754	-.1128	.0022	.0646	-.2248
46	33	510.40	20.16	8.06	.3438	.0728	-.1213	.0033	.0813	-.2988
46	32	510.05	24.17	8.05	.3300	.0698	-.1262	.0039	.0978	-.3754
46	40	510.23	-0.02	12.58	.5254	.1449	-.1160	.0004	-.0006	.0021
46	41	510.23	2.09	12.56	.5258	.1449	-.1189	-.0002	.0072	-.0212
46	42	510.40	4.17	12.52	.5265	.1437	-.1242	-.0005	.0146	-.0441
46	43	510.23	8.26	12.37	.5345	.1426	-.1398	-.0014	.0304	-.0957
46	44	508.45	12.27	12.27	.5352	.1406	-.1566	-.0008	.0493	-.1592
46	45	509.52	16.25	12.17	.5292	.1380	-.1653	.0006	.0664	-.2271
46	46	508.99	20.26	12.17	.5184	.1346	-.1712	.0024	.0789	-.2905
46	47	509.87	24.86	12.46	.5084	.1351	-.1785	.0042	.0985	-.3744
46	56	509.87	.00	16.73	.7119	.2417	-.1957	.0002	-.0009	.0040
46	54	510.05	2.02	16.74	.7116	.2414	-.1946	.0000	.0075	-.0218
46	55	509.87	2.08	16.73	.7121	.2415	-.1946	.0001	.0078	-.0219
46	53	510.05	4.18	16.70	.7108	.2404	-.1958	-.0006	.0176	-.0497
46	52	510.05	8.30	16.59	.7099	.2364	-.1992	-.0020	.0340	-.1039
46	51	510.23	12.38	16.46	.7059	.2322	-.2031	-.0022	.0488	-.1603
46	50	509.52	16.41	16.41	.6925	.2265	-.2000	-.0016	.0597	-.2144
46	49	509.69	21.26	17.02	.7033	.2378	-.2153	.0010	.0759	-.2880
46	48	509.69	22.46	16.31	.6700	.2184	-.2110	.0021	.0823	-.3121
46	57	510.05	-0.04	20.89	.8656	.3574	-.2353	-.0003	-.0023	.0077
46	58	510.05	2.10	20.89	.8691	.3586	-.2434	-.0001	.0085	-.0228
46	59	509.87	4.19	20.85	.8693	.3573	-.2484	-.0005	.0184	-.0528
46	60	509.87	8.30	20.81	.8588	.3513	-.2370	-.0023	.0296	-.0988
46	61	509.87	12.46	20.71	.8565	.3468	-.2435	-.0020	.0442	-.1525
46	62	509.87	16.47	20.66	.8386	.3382	-.2329	-.0018	.0520	-.1999
46	63	509.69	20.42	20.42	.8223	.3287	-.2393	.0003	.0696	-.2642
46	69	510.23	.00	25.14	1.0103	.5015	-.2813	-.0008	-.0022	.0084
46	68	510.05	2.12	25.18	1.0065	.4997	-.2754	-.0012	.0059	-.0178
46	67	509.69	4.20	25.17	1.0030	.4984	-.2714	-.0016	.0142	-.0443
46	66	509.52	8.37	25.04	.9942	.4894	-.2699	-.0027	.0223	-.0869
46	65	510.05	12.48	25.00	.9916	.4859	-.2786	-.0017	.0381	-.1402
46	64	509.69	14.57	24.86	.9767	.4748	-.2673	-.0016	.0414	-.1629

TABLE IV - Continued
 AERODYNAMIC CHARACTERISTICS IN SIDESLIP FOR VARIOUS ANGLES OF ATTACK.
 STABILITY AXES; M = 2.01

Run	Pt.	q	β , deg	α , deg	C_L	C_D	C_m	$C_{l,s}$	$C_{n,w}$	C_y
47	23	508.63	.00	.00	-.0166	.0280	.0118	.0003	-.0008	.0014
47	22	508.10	.99	.00	-.0157	.0280	.0115	.0002	.0034	-.0114
47	21	508.45	2.00	.00	-.0163	.0280	.0112	.0000	.0081	-.0252
47	20	508.10	3.98	.00	-.0146	.0277	.0093	-.0002	.0168	-.0517
47	19	508.28	5.99	.00	-.0127	.0275	.0067	-.0005	.0256	-.0790
47	18	508.45	8.02	.00	-.0109	.0267	.0035	-.0006	.0344	-.1082
47	17	508.28	12.03	.00	-.0046	.0261	-.0050	-.0001	.0504	-.1691
47	16	508.81	16.04	.00	-.0170	.0255	.0000	.0011	.0624	-.2343
47	15	507.92	20.07	.00	-.0341	.0255	.0076	.0025	.0747	-.3038
47	14	508.99	24.15	.00	-.0515	.0259	.0128	.0026	.0887	-.3790
47	13	507.39	28.19	.00	-.0660	.0259	.0143	.0023	.1028	-.4534
47	24	508.45	.00	4.18	.1642	.0394	-.0176	.0001	.0000	-.0004
47	25	508.10	2.06	4.14	.1590	.0388	-.0181	.0002	.0074	-.0233
47	26	508.63	4.08	4.08	.1565	.0384	-.0191	.0005	.0153	-.0471
47	27	508.45	8.10	4.04	.1590	.0376	-.0243	.0015	.0320	-.0994
47	28	508.28	12.12	4.04	.1650	.0376	-.0313	.0030	.0467	-.1576
47	29	508.28	16.07	4.02	.1521	.0360	-.0276	.0043	.0590	-.2198
47	30	508.28	20.10	4.03	.1319	.0335	-.0187	.0055	.0729	-.2915
47	31	508.28	24.20	4.07	.1139	.0327	-.0123	.0061	.0895	-.3701
47	40	508.45	.00	8.43	.3423	.0779	-.0478	.0004	-.0002	.0011
47	39	508.10	2.11	8.39	.3397	.0771	-.0483	.0012	.0075	-.0225
47	38	508.10	4.17	8.32	.3376	.0758	-.0493	.0019	.0147	-.0453
47	37	508.28	8.21	8.21	.3386	.0749	-.0540	.0031	.0295	-.0933
47	36	508.28	12.18	8.13	.3365	.0732	-.0585	.0047	.0426	-.1480
47	35	508.10	16.16	8.08	.3225	.0702	-.0556	.0061	.0565	-.2129
47	34	508.28	17.11	8.57	.3366	.0744	-.0567	.0063	.0595	-.2281
47	33	508.10	20.18	8.07	.3027	.0660	-.0483	.0073	.0707	-.2822
47	32	508.28	24.20	8.06	.2768	.0626	-.0388	.0077	.0876	-.3568
47	41	507.92	.00	12.61	.5044	.1404	-.0735	.0002	-.0004	.0027
47	42	508.28	2.09	12.59	.5035	.1398	-.0737	.0009	.0066	-.0206
47	43	507.04	4.18	12.55	.5031	.1386	-.0756	.0014	.0134	-.0427
47	44	507.92	8.29	12.41	.5036	.1355	-.0809	.0021	.0258	-.0891
47	45	508.81	12.32	12.32	.4961	.1319	-.0795	.0036	.0388	-.1445
47	46	507.04	16.31	12.21	.4787	.1268	-.0773	.0048	.0535	-.2083
47	47	508.28	20.31	12.20	.4627	.1232	-.0732	.0060	.0680	-.2732
47	48	508.28	24.93	12.49	.4439	.1213	-.0646	.0075	.0871	-.3567
47	56	508.28	.00	16.79	.6631	.2265	-.0965	.0001	-.0008	.0051
47	55	508.45	2.09	16.79	.6632	.2265	-.0972	.0005	.0055	-.0185
47	54	508.45	4.20	16.78	.6619	.2256	-.0985	.0004	.0117	-.0410
47	53	508.28	8.31	16.67	.6579	.2213	-.0999	.0006	.0226	-.0870
47	52	508.28	12.40	16.55	.6499	.2167	-.0973	.0015	.0357	-.1413
47	51	508.28	16.45	16.45	.6395	.2116	-.0975	.0021	.0505	-.2006
47	50	508.45	20.49	16.38	.6209	.2047	-.0946	.0031	.0656	-.2649
47	49	508.28	22.48	16.38	.6070	.2008	-.0908	.0040	.0730	-.2982
47	57	508.10	-.04	20.98	.8062	.3351	-.1209	-.0001	-.0017	.0068
47	58	508.10	2.11	20.97	.8058	.3348	-.1221	-.0002	.0041	-.0164
47	59	508.28	4.21	20.94	.8054	.3333	-.1241	-.0008	.0099	-.0392
47	60	508.10	8.36	20.86	.8019	.3301	-.1255	-.0013	.0201	-.0842
47	61	508.10	12.51	20.80	.7923	.3245	-.1220	-.0004	.0322	-.1347
47	62	508.10	16.52	20.73	.7814	.3180	-.1191	.0005	.0463	-.1907
47	63	508.45	20.45	20.51	.7587	.3064	-.1144	.0016	.0620	-.2515
47	69	508.10	.00	25.23	.9474	.4718	-.1533	-.0005	-.0021	.0084
47	68	508.10	2.12	25.26	.9474	.4719	-.1534	-.0011	.0025	-.0116
47	67	508.10	4.22	25.24	.9446	.4702	-.1537	-.0016	.0076	-.0339
47	66	508.28	8.40	25.12	.9384	.4640	-.1537	-.0020	.0163	-.0766
47	65	507.92	12.58	25.09	.9263	.4570	-.1491	-.0010	.0280	-.1258
47	64	507.92	14.62	24.94	.9150	.4480	-.1446	-.0003	.0346	-.1527

TABLE IV - Continued
 AERODYNAMIC CHARACTERISTICS IN SIDESLIP FOR VARIOUS ANGLES OF ATTACK.

STABILITY AXES; M = 2.01

Run	Pt.	q	β , deg	α , deg	C_L	C_D	C_m	$C_{l,s}$	$C_{n,w}$	C_y
48	21	511.11	.00	.00	.0054	.0189	.0087	.0002	-.0011	.0023
48	20	510.76	1.99	.00	.0065	.0195	.0088	-.0016	.0073	-.0204
48	19	510.93	3.97	.00	.0078	.0197	.0084	-.0033	.0155	-.0430
48	18	510.76	5.97	.00	.0092	.0193	.0080	-.0051	.0244	-.0677
48	17	510.76	8.00	-.01	.0107	.0184	.0073	-.0069	.0335	-.0943
48	16	510.76	12.00	.00	.0106	.0175	.0068	-.0103	.0501	-.1504
48	15	510.93	16.01	.03	.0102	.0159	.0076	-.0137	.0852	-.2216
48	14	510.93	20.04	.00	.0098	.0153	.0084	-.0170	.0806	-.2949
48	13	510.93	24.11	.00	.0091	.0152	.0089	-.0197	.0973	-.3711
48	12	511.29	28.12	.00	.0072	.0153	.0107	-.0225	.1160	-.4510
48	22	510.93	.00	4.04	.0142	.0208	.0225	.0000	.0000	-.0011
48	23	510.93	2.01	4.02	.0132	.0207	.0218	-.0009	.0075	-.0221
48	24	510.93	4.00	4.01	.0105	.0199	.0217	-.0019	.0156	-.0442
48	25	511.29	6.01	4.00	.0119	.0195	.0206	-.0030	.0244	-.0695
48	26	510.93	8.01	4.01	.0123	.0193	.0198	-.0041	.0329	-.0944
48	27	510.93	12.06	4.02	.0174	.0185	.0160	-.0065	.0494	-.1522
48	28	510.93	16.02	4.00	.0221	.0175	.0159	-.0086	.0639	-.2204
48	29	510.93	20.06	4.02	.0264	.0165	.0151	-.0105	.0785	-.2910
48	30	510.93	24.17	4.02	.0275	.0166	.0149	-.0121	.0957	-.3670
48	39	511.46	.00	8.10	.0236	.0237	.0338	.0000	.0001	-.0013
48	38	510.93	2.03	8.09	.0237	.0228	.0330	-.0004	.0073	-.0223
48	37	510.40	4.05	8.09	.0255	.0225	.0319	-.0009	.0151	-.0447
48	36	510.76	6.04	8.06	.0266	.0217	.0305	-.0014	.0233	-.0689
48	35	510.93	8.05	8.05	.0292	.0217	.0294	-.0018	.0315	-.0948
48	34	511.11	12.04	8.03	.0419	.0222	.0226	-.0028	.0468	-.1541
48	33	510.93	16.05	8.02	.0511	.0224	.0203	-.0039	.0608	-.2185
48	32	510.23	20.09	8.03	.0572	.0226	.0183	-.0043	.0741	-.2853
48	31	511.11	24.11	8.08	.0589	.0223	.0177	-.0047	.0915	-.3600
48	40	510.76	.00	12.14	.0393	.0291	.0463	.0000	-.0002	-.0005
48	41	510.40	2.02	12.14	.0406	.0288	.0445	-.0001	.0057	-.0204
48	42	509.52	4.02	12.13	.0431	.0278	.0410	-.0001	.0121	-.0426
48	43	510.23	6.04	12.10	.0483	.0275	.0377	-.0002	.0193	-.0674
48	44	510.93	8.07	12.09	.0539	.0279	.0341	-.0002	.0264	-.0934
48	45	510.93	12.09	12.09	.0664	.0298	.0293	.0001	.0416	-.1542
48	46	510.93	16.09	12.09	.0749	.0306	.0262	.0004	.0555	-.2157
48	47	510.58	20.15	12.10	.0831	.0325	.0224	.0010	.0690	-.2810
48	48	510.40	24.79	12.41	.0911	.0337	.0207	.0025	.0887	-.3649
48	49	510.58	20.22	16.16	.1155	.0472	.0252	.0056	.0640	-.2766
49	8	510.05	.00	16.16	.0745	.0421	.0514	-.0002	-.0002	-.0006
49	7	510.05	2.01	16.21	.0766	.0428	.0498	.0000	.0035	-.0189
49	6	509.69	4.04	16.18	.0809	.0418	.0443	.0001	.0073	-.0389
49	5	509.69	6.02	16.18	.0849	.0414	.0388	.0002	.0137	-.0643
49	4	509.69	8.08	16.16	.0899	.0417	.0363	.0007	.0209	-.0923
49	3	510.23	12.12	16.14	.0978	.0435	.0333	.0023	.0351	-.1505
49	2	509.52	16.15	16.15	.1040	.0438	.0302	.0038	.0497	-.2127
49	1	510.93	20.21	16.15	.1092	.0454	.0266	.0055	.0636	-.2763
49	9	509.69	.00	20.22	.1168	.0639	.0537	-.0001	-.0002	.0001
49	10	510.05	2.03	20.23	.1191	.0637	.0509	.0000	.0007	-.0166
49	11	510.05	4.06	20.23	.1236	.0636	.0446	-.0001	.0032	-.0358
49	12	509.69	6.06	20.22	.1255	.0623	.0403	.0005	.0088	-.0597
49	13	510.23	8.04	20.22	.1297	.0632	.0370	.0013	.0149	-.0867
49	14	509.52	12.12	20.26	.1369	.0639	.0327	.0040	.0286	-.1448
49	15	509.69	16.14	20.26	.1425	.0664	.0300	.0067	.0437	-.2070
49	16	509.52	20.11	20.11	.1458	.0671	.0274	.0096	.0587	-.2712
49	21	509.69	2.09	24.37	.1508	.0913	.0505	-.0005	-.0022	-.0133
49	20	510.05	4.06	24.39	.1636	.0914	.0445	-.0002	-.0003	-.0322
49	19	509.52	6.10	24.39	.1663	.0913	.0396	.0007	.0047	-.0567
49	18	509.34	8.10	24.32	.1689	.0916	.0363	.0020	.0105	-.0834
49	17	510.23	12.18	24.36	.1735	.0915	.0321	.0056	.0240	-.1421

TABLE IV - Continued
 AERODYNAMIC CHARACTERISTICS IN SIDESLIP FOR VARIOUS ANGLES OF ATTACK.
 STABILITY AXES; M = 2.01

Run	Pt.	q	β , deg	α , deg	C_L	C_D	C_m	C_{L_s}	$C_{n,w}$	C_Y
50	21	509.34	.00	.00	-.0129	.0274	.0148	.0001	-.0012	.0033
50	20	509.52	2.00	.00	-.0122	.0270	.0153	-.0027	.0063	-.0211
50	19	509.52	3.98	.00	-.0129	.0272	.0168	-.0058	.0140	-.0456
50	18	509.69	5.98	.00	-.0133	.0270	.0190	-.0091	.0220	-.0720
50	17	509.52	8.03	.01	-.0151	.0268	.0218	-.0124	.0302	-.0992
50	16	509.52	12.04	.00	-.0178	.0266	.0291	-.0197	.0463	-.1593
50	15	509.87	16.04	-.03	-.0069	.0262	.0249	-.0274	.0622	-.2310
50	14	509.69	20.06	.00	.0144	.0246	.0164	-.0355	.0809	-.3124
50	13	509.34	24.15	.00	.0315	.0254	.0105	-.0422	.0977	-.3928
50	12	509.34	28.16	.00	.0446	.0252	.0101	-.0476	.1137	-.4708
50	22	509.16	.00	4.18	.1612	.0388	-.0132	-.0001	-.0003	-.0003
50	23	509.16	2.07	4.14	.1553	.0379	-.0116	-.0031	.0065	-.0238
50	24	509.34	4.10	4.10	.1536	.0377	-.0105	-.0059	.0140	-.0492
50	25	508.99	6.10	4.07	.1505	.0370	-.0081	-.0087	.0219	-.0760
50	26	509.34	8.10	4.04	.1471	.0366	-.0052	-.0115	.0302	-.1038
50	27	508.99	12.13	4.06	.1493	.0370	-.0001	-.0181	.0470	-.1694
50	28	508.99	16.10	4.05	.1612	.0373	-.0025	-.0248	.0620	-.2384
50	29	508.81	20.13	4.03	.1769	.0368	-.0071	-.0321	.0792	-.3162
50	30	509.16	24.24	4.03	.1917	.0382	-.0109	-.0385	.0967	-.3973
50	39	508.99	-.01	8.43	.3422	.0770	-.0471	-.0001	-.0006	.0022
50	38	509.16	2.11	8.39	.3407	.0766	-.0461	-.0027	.0063	-.0247
50	37	509.34	4.18	8.34	.3381	.0758	-.0445	-.0054	.0136	-.0509
50	36	508.99	6.20	8.29	.3361	.0743	-.0419	-.0079	.0214	-.0793
50	35	509.34	8.23	8.23	.3348	.0739	-.0385	-.0107	.0299	-.1115
50	34	508.81	12.23	8.16	.3386	.0743	-.0346	-.0167	.0454	-.1755
50	33	508.99	16.24	8.12	.3422	.0743	-.0298	-.0231	.0592	-.2435
50	32	509.16	20.27	8.10	.3467	.0730	-.0284	-.0296	.0756	-.3189
50	31	508.99	24.28	8.18	.3560	.0757	-.0312	-.0357	.0928	-.3960
50	40	508.99	.00	12.62	.5100	.1410	-.0782	-.0003	-.0008	.0020
50	41	508.99	2.07	12.61	.5073	.1404	-.0767	-.0031	.0060	-.0264
50	42	509.34	4.19	12.57	.5039	.1388	-.0743	-.0057	.0128	-.0545
50	43	509.16	6.23	12.52	.4999	.1366	-.0707	-.0085	.0199	-.0846
50	44	508.99	8.28	12.44	.4994	.1359	-.0677	-.0112	.0275	-.1155
50	45	508.99	12.36	12.36	.4964	.1342	-.0594	-.0173	.0416	-.1797
50	46	508.81	16.39	12.28	.4935	.1323	-.0502	-.0232	.0553	-.2484
50	47	508.99	20.42	12.27	.4958	.1318	-.0484	-.0285	.0716	-.3234
50	48	509.16	25.06	12.57	.5102	.1387	-.0520	-.0340	.0914	-.4107
50	56	509.52	.00	16.79	.6702	.2280	-.1105	-.0004	-.0011	.0045
50	55	509.87	2.06	16.81	.6695	.2281	-.1092	-.0033	.0050	-.0241
50	54	509.52	4.20	16.79	.6688	.2275	-.1067	-.0060	.0120	-.0556
50	53	509.52	6.24	16.74	.6667	.2262	-.1036	-.0086	.0158	-.0868
50	52	509.69	8.33	16.71	.6654	.2249	-.1011	-.0116	.0239	-.1165
50	51	509.52	12.47	16.59	.6585	.2200	-.0929	-.0166	.0366	-.1837
50	50	509.52	16.50	16.56	.6515	.2185	-.0812	-.0216	.0500	-.2535
50	49	508.99	20.58	16.51	.6443	.2150	-.0746	-.0273	.0653	-.3246
50	57	509.69	.00	20.96	.8092	.3346	-.1397	-.0005	-.0013	.0042
50	58	509.52	2.11	20.95	.8085	.3338	-.1398	-.0034	.0038	-.0247
50	59	509.69	4.17	20.94	.8052	.3327	-.1375	-.0065	.0089	-.0542
50	60	509.52	6.29	20.91	.8014	.3294	-.1347	-.0096	.0133	-.0833
50	61	509.34	8.37	20.87	.7973	.3261	-.1326	-.0122	.0194	-.1158
50	62	509.34	12.50	20.86	.7886	.3236	-.1229	-.0161	.0317	-.1847
50	63	509.34	16.63	20.79	.7791	.3195	-.1115	-.0201	.0442	-.2533
50	64	508.99	20.56	20.62	.7654	.3105	-.1006	-.0239	.0596	-.3234
50	70	509.52	.00	25.17	.9331	.4635	-.1763	-.0009	-.0019	.0079
50	69	509.52	2.07	25.20	.9314	.4622	-.1733	-.0044	.0018	-.0214
50	68	509.34	4.16	25.21	.9294	.4605	-.1723	-.0076	.0057	-.0494
50	67	509.69	6.33	25.15	.9259	.4566	-.1696	-.0100	.0106	-.0799
50	66	509.34	8.40	25.11	.9212	.4532	-.1663	-.0122	.0154	-.1107
50	65	509.52	12.58	25.09	.9093	.4469	-.1551	-.0157	.0264	-.1780

TABLE IV - Continued
AERODYNAMIC CHARACTERISTICS IN SIDESLIP FOR VARIOUS ANGLES OF ATTACK.

STABILITY AXES; M = 2.01

Run	Pt.	q	β , deg	α , deg	C_L	C_D	C_m	$C_{l,s}$	$C_{n,w}$	C_Y
51	22	510.05	.00	.00	-.0155	.0294	.0229	.0002	-.0012	.0034
51	21	510.40	.99	.00	-.0151	.0294	.0227	-.0013	.0027	-.0093
51	20	510.23	2.00	.00	-.0163	.0295	.0232	-.0029	.0067	-.0211
51	19	510.05	3.98	.01	-.0153	.0292	.0235	-.0061	.0144	-.0463
51	18	509.87	5.99	.01	-.0159	.0291	.0242	-.0094	.0224	-.0718
51	17	509.87	8.02	-.03	-.0176	.0290	.0247	-.0131	.0310	-.1004
51	16	510.05	12.04	.00	-.0137	.0287	.0244	-.0210	.0482	-.1621
51	15	510.05	16.03	.00	.0036	.0280	.0121	-.0293	.0652	-.2359
51	14	510.23	20.06	.00	.0251	.0266	-.0038	-.0386	.0849	-.3184
51	13	510.23	24.13	.04	.0518	.0267	-.0240	-.0460	.1042	-.4035
51	12	509.87	26.15	.05	.0661	.0267	-.0337	-.0491	.1126	-.4438
51	23	510.05	.00	4.18	.1725	.0414	-.0289	-.0001	-.0003	-.0002
51	24	510.05	2.06	4.13	.1675	.0408	-.0284	-.0033	.0068	-.0248
51	25	510.23	4.08	4.08	.1646	.0405	-.0291	-.0063	.0144	-.0493
51	26	510.05	8.11	4.04	.1652	.0401	-.0304	-.0126	.0316	-.1071
51	27	510.05	12.12	4.06	.1705	.0401	-.0317	-.0195	.0495	-.1729
51	28	509.45	16.08	4.05	.1847	.0404	-.0385	-.0269	.0659	-.2437
51	29	509.52	20.11	4.03	.2039	.0401	-.0488	-.0352	.0849	-.3250
51	30	509.87	24.22	4.07	.2266	.0421	-.0642	-.0423	.1039	-.4082
51	38	509.69	.00	8.39	.3685	.0832	-.0904	.0000	-.0006	.0016
51	37	509.87	2.10	8.36	.3642	.0818	-.0890	-.0028	.0067	-.0254
51	36	509.87	4.15	8.32	.3638	.0813	-.0888	-.0055	.0141	-.0517
51	35	510.40	8.23	8.23	.3656	.0806	-.0882	-.0115	.0315	-.1135
51	34	510.76	12.21	8.15	.3681	.0806	-.0860	-.0180	.0489	-.1804
51	33	509.87	16.20	8.10	.3732	.0805	-.0841	-.0252	.0648	-.2501
51	32	510.05	20.24	8.09	.3782	.0794	-.0850	-.0323	.0825	-.3287
51	31	510.05	24.25	8.08	.3895	.0807	-.0931	-.0387	.1008	-.4088
51	39	509.69	-.02	12.58	.5493	.1509	-.1454	-.0002	-.0008	.0024
51	40	509.69	2.09	12.55	.5458	.1499	-.1434	-.0030	.0062	-.0261
51	41	510.05	4.17	12.52	.5426	.1485	-.1411	-.0058	.0136	-.0553
51	42	509.87	8.29	12.41	.5406	.1463	-.1373	-.0116	.0301	-.1195
51	43	509.87	12.31	12.35	.5400	.1452	-.1323	-.0183	.0466	-.1860
51	44	509.87	16.35	12.24	.5398	.1438	-.1266	-.0249	.0632	-.2590
51	45	510.05	20.38	12.24	.5366	.1416	-.1194	-.0304	.0799	-.3351
51	53	510.05	.00	16.73	.7153	.2427	-.1941	-.0004	-.0011	.0041
51	52	510.23	2.05	16.74	.7140	.2424	-.1916	-.0033	.0057	-.0256
51	51	510.05	4.16	16.73	.7129	.2421	-.1903	-.0059	.0131	-.0573
51	50	510.05	6.23	16.69	.7097	.2405	-.1868	-.0085	.0205	-.0897
51	49	510.23	8.29	16.65	.7089	.2388	-.1845	-.0113	.0271	-.1215
51	48	510.23	12.43	16.54	.7032	.2346	-.1772	-.0171	.0421	-.1911
51	47	510.40	16.50	16.50	.6957	.2322	-.1670	-.0225	.0576	-.2642
51	46	510.05	20.53	16.47	.6929	.2298	-.1611	-.0278	.0731	-.3362
51	54	509.87	.00	20.89	.8560	.3535	-.2306	-.0004	-.0017	.0068
51	55	509.87	2.10	20.88	.8556	.3524	-.2310	-.0036	.0047	-.0253
51	56	510.05	4.19	20.86	.8570	.3524	-.2343	-.0061	.0105	-.0569
51	57	509.87	6.26	20.84	.8549	.3499	-.2324	-.0090	.0158	-.0872
51	58	509.87	8.31	20.84	.8506	.3476	-.2290	-.0121	.0221	-.1189
51	59	508.28	12.50	20.79	.8391	.3430	-.2144	-.0170	.0353	-.1895
51	60	508.99	16.55	20.75	.8340	.3408	-.2084	-.0206	.0486	-.2591
51	61	508.99	20.55	20.55	.8183	.3307	-.1970	-.0240	.0638	-.3295
51	68	508.99	.00	25.09	.9959	.4926	-.2967	-.0008	-.0018	.0068
51	67	509.16	2.11	25.13	.9954	.4926	-.2936	-.0043	.0025	-.0228
51	66	508.81	4.19	25.12	.9916	.4892	-.2916	-.0074	.0071	-.0521
51	65	508.81	6.26	25.08	.9902	.4862	-.2899	-.0097	.0128	-.0838
51	64	508.81	8.36	25.01	.9844	.4813	-.2845	-.0121	.0182	-.1149
51	63	509.16	12.55	25.03	.9714	.4754	-.2672	-.0165	.0283	-.1803
51	62	508.81	14.61	24.92	.9608	.4688	-.2563	-.0184	.0337	-.2113

TABLE IV - Continued
AERODYNAMIC CHARACTERISTICS IN SIDESLIP FOR VARIOUS ANGLES OF ATTACK.

STABILITY AXES; M = 2.01

Run	Pt.	q	β , deg	α , deg	C_L	C_D	C_m	C_{L_s}	C_{N_w}	C_Y
52	24	510.23	.00	.00	-.0513	.0343	.0818	.0002	-.0012	.0039
52	23	509.52	.99	.00	-.0511	.0339	.0816	-.0012	.0025	-.0078
52	22	509.16	1.99	.00	-.0523	.0336	.0821	-.0028	.0064	-.0205
52	21	510.23	3.98	.00	-.0511	.0336	.0835	-.0060	.0143	-.0458
52	20	509.87	5.98	.00	-.0517	.0336	.0835	-.0093	.0223	-.0712
52	19	509.16	8.03	.00	-.0519	.0332	.0840	-.0129	.0306	-.0995
52	18	510.93	12.03	.02	-.0513	.0325	.0850	-.0205	.0469	-.1597
52	17	509.69	16.04	.00	-.0344	.0312	.0725	-.0286	.0631	-.2328
52	16	508.28	20.06	.04	-.0087	.0296	.0552	-.0371	.0822	-.3150
52	15	510.05	24.14	.00	.0128	.0291	.0373	-.0443	.0997	-.3970
52	14	510.05	26.16	.00	.0237	.0281	.0287	-.0472	.1078	-.4360
52	25	510.23	.00	4.21	.1380	.0418	.0274	-.0001	-.0002	-.0006
52	26	510.23	2.07	4.17	.1328	.0411	.0281	-.0032	.0066	-.0240
52	27	510.23	4.12	4.11	.1317	.0405	.0271	-.0061	.0140	-.0486
52	28	510.23	8.11	4.05	.1320	.0401	.0263	-.0122	.0308	-.1052
52	29	509.87	12.15	4.07	.1358	.0393	.0255	-.0190	.0478	-.1707
52	30	510.23	16.10	4.02	.1492	.0395	.0188	-.0264	.0631	-.2396
52	31	510.58	20.13	4.07	.1726	.0389	.0055	-.0340	.0808	-.3186
52	32	510.58	24.25	4.08	.1934	.0405	-.0081	-.0406	.0989	-.4017
52	40	510.40	.00	8.42	.3355	.0793	-.0352	.0000	-.0005	.0012
52	39	509.87	2.09	8.41	.3314	.0786	-.0341	-.0027	.0064	-.0247
52	38	510.05	4.19	8.36	.3310	.0778	-.0341	-.0054	.0138	-.0519
52	37	510.05	8.23	8.23	.3297	.0761	-.0321	-.0112	.0303	-.1117
52	36	509.87	12.23	8.16	.3339	.0756	-.0306	-.0178	.0463	-.1765
52	35	509.87	16.22	8.11	.3396	.0757	-.0300	-.0248	.0608	-.2455
52	34	509.87	20.26	8.10	.3473	.0749	-.0336	-.0317	.0780	-.3221
52	33	509.87	24.29	8.09	.3568	.0760	-.0400	-.0377	.0957	-.4012
52	41	510.05	.00	12.62	.5171	.1440	-.0903	-.0002	-.0009	.0021
52	42	510.23	2.09	12.59	.5148	.1433	-.0888	-.0029	.0062	-.0272
52	43	510.76	4.16	12.55	.5111	.1417	-.0865	-.0056	.0129	-.0543
52	44	510.40	8.29	12.42	.5076	.1385	-.0830	-.0116	.0281	-.1163
52	45	510.23	12.35	12.35	.5101	.1382	-.0797	-.0184	.0430	-.1815
52	46	510.40	16.35	12.29	.5088	.1363	-.0745	-.0249	.0573	-.2500
52	47	510.23	20.39	12.30	.5087	.1351	-.0711	-.0301	.0744	-.3271
52	54	510.23	.00	16.77	.6836	.2323	-.1402	-.0002	-.0011	.0047
52	53	510.23	2.09	16.77	.6812	.2316	-.1375	-.0033	.0054	-.0249
52	52	510.40	4.20	16.76	.6812	.2312	-.1372	-.0061	.0121	-.0563
52	51	510.58	8.33	16.65	.6770	.2275	-.1326	-.0119	.0248	-.1174
52	50	510.58	12.45	16.56	.6721	.2238	-.1269	-.0176	.0381	-.1855
52	49	510.40	16.52	16.52	.6676	.2219	-.1202	-.0230	.0528	-.2567
52	48	510.40	20.58	16.46	.6646	.2190	-.1160	-.0281	.0686	-.3303
52	55	510.40	.00	20.93	.8293	.3412	-.1822	-.0003	-.0014	.0055
52	56	510.40	2.10	20.90	.8289	.3399	-.1830	-.0037	.0041	-.0254
52	57	510.58	4.20	20.89	.8285	.3391	-.1867	-.0064	.0092	-.0549
52	58	510.40	8.36	20.86	.8237	.3350	-.1817	-.0127	.0201	-.1166
52	59	510.23	12.52	20.81	.8153	.3319	-.1715	-.0177	.0327	-.1855
52	60	510.58	16.61	20.76	.8082	.3273	-.1670	-.0214	.0455	-.2549
52	61	510.23	20.53	20.60	.7952	.3195	-.1577	-.0245	.0611	-.3252
52	67	510.23	.00	25.13	.9742	.4786	-.2570	-.0006	-.0019	.0075
52	66	510.40	2.11	25.15	.9726	.4771	-.2549	-.0046	.0018	-.0219
52	65	510.40	4.20	25.15	.9708	.4748	-.2534	-.0076	.0057	-.0499
52	64	510.40	8.33	25.05	.9629	.4680	-.2464	-.0126	.0159	-.1113
52	63	510.40	12.57	25.06	.9492	.4620	-.2289	-.0169	.0266	-.1776
52	62	510.58	16.62	24.94	.9369	.4540	-.2170	-.0187	.0329	-.2121

TABLE IV - Continued
AERODYNAMIC CHARACTERISTICS IN SIDESLIP FOR VARIOUS ANGLES OF ATTACK.

STABILITY AXES; M = 2.01

Run	Pt.	q	β , deg	α , deg	C_L	C_D	C_m	C_{l_s}	C_{n_w}	C_Y
53	28	509.52	.00	.00	-.0356	.0318	.0527	.0002	-.0012	.0023
53	27	509.34	.98	.00	-.0355	.0319	.0527	-.0009	.0035	-.0106
53	26	510.40	2.00	.00	-.0351	.0319	.0533	-.0021	.0085	-.0244
53	25	510.58	3.99	.01	-.0362	.0320	.0556	-.0044	.0179	-.0517
53	24	509.34	5.98	.00	-.0387	.0314	.0589	-.0070	.0276	-.0796
53	23	508.63	8.01	.01	-.0393	.0312	.0620	-.0097	.0373	-.1090
53	22	510.40	12.01	-.02	-.0481	.0312	.0771	-.0159	.0564	-.1749
53	21	510.58	16.01	.00	-.0459	.0318	.0891	-.0232	.0737	-.2483
53	20	510.58	20.03	.00	-.0403	.0323	.1034	-.0315	.0934	-.3315
53	19	510.76	24.12	.00	-.0298	.0333	.1115	-.0383	.1111	-.4140
53	18	509.69	26.13	.05	-.0235	.0325	.1108	-.0411	.1179	-.4507
53	29	510.58	.00	4.18	.1580	.0410	-.0064	.0000	-.0003	-.0004
53	30	510.58	2.07	4.15	.1519	.0406	-.0043	-.0024	.0079	-.0261
53	31	510.76	4.11	4.11	.1484	.0394	-.0022	-.0047	.0165	-.0528
53	32	510.40	8.09	4.03	.1434	.0394	.0038	-.0095	.0349	-.1120
53	33	510.40	12.13	4.04	.1408	.0390	.0147	-.0152	.0528	-.1788
53	34	510.76	16.09	4.05	.1436	.0394	.0257	-.0216	.0687	-.2485
53	35	509.16	20.11	4.03	.1513	.0393	.0386	-.0286	.0874	-.3281
53	36	510.76	24.23	4.07	.1498	.0409	.0583	-.0342	.1081	-.4151
53	44	510.58	-.01	8.42	.3434	.0798	-.0523	.0000	-.0007	.0023
53	43	510.58	2.11	8.39	.3403	.0788	-.0511	-.0021	.0075	-.0267
53	42	510.40	4.17	8.32	.3380	.0776	-.0493	-.0042	.0155	-.0541
53	41	510.40	8.23	8.23	.3371	.0764	-.0450	-.0084	.0334	-.1162
53	40	510.23	12.22	8.15	.3359	.0757	-.0376	-.0138	.0494	-.1822
53	39	510.40	16.47	8.24	.3422	.0767	-.0282	-.0203	.0648	-.2550
53	38	510.40	20.25	8.10	.3341	.0737	-.0160	-.0264	.0813	-.3278
53	37	509.34	24.27	8.09	.3323	.0748	-.0024	-.0318	.1002	-.4087
53	45	510.23	-.02	12.61	.5209	.1446	-.0983	-.0002	-.0009	.0021
53	46	510.23	2.09	12.58	.5184	.1434	-.0970	-.0024	.0068	-.0274
53	47	510.40	4.18	12.54	.5132	.1421	-.0939	-.0044	.0145	-.0576
53	48	510.76	8.30	12.43	.5107	.1395	-.0885	-.0087	.0304	-.1207
53	49	511.11	12.35	12.35	.5086	.1376	-.0807	-.0143	.0449	-.1849
53	50	510.23	16.37	12.28	.5034	.1354	-.0672	-.0197	.0591	-.2540
53	51	510.76	20.39	12.30	.5009	.1347	-.0603	-.0248	.0759	-.3306
53	52	510.40	25.03	12.60	.5089	.1400	-.0533	-.0303	.0960	-.4191
53	60	510.58	.00	16.74	.6888	.2331	-.1499	-.0003	-.0011	.0048
53	59	510.58	2.09	16.77	.6902	.2342	-.1493	-.0026	.0056	-.0259
53	58	510.58	4.17	16.76	.6883	.2332	-.1464	-.0048	.0127	-.0575
53	57	510.76	8.33	16.65	.6818	.2290	-.1393	-.0091	.0260	-.1198
53	56	510.93	12.45	16.56	.6769	.2252	-.1313	-.0131	.0394	-.1881
53	55	510.40	16.51	16.51	.6681	.2224	-.1171	-.0180	.0530	-.2584
53	54	510.58	20.59	16.47	.6589	.2186	-.1047	-.0235	.0688	-.3319
53	53	510.93	22.64	16.45	.6543	.2174	-.0982	-.0257	.0782	-.3713
53	61	509.34	.00	20.92	.8417	.3453	-.2020	-.0005	-.0015	.0066
53	62	509.69	2.11	20.91	.8403	.3443	-.2016	-.0030	.0041	-.0283
53	63	510.40	4.20	20.88	.8375	.3429	-.1991	-.0053	.0094	-.0560
53	64	510.23	8.32	20.87	.8325	.3386	-.1947	-.0098	.0203	-.1179
53	65	510.40	12.51	20.80	.8211	.3341	-.1820	-.0128	.0335	-.1881
53	66	510.23	16.57	20.78	.8099	.3294	-.1683	-.0163	.0460	-.2568
53	67	510.23	20.56	20.56	.7906	.3185	-.1488	-.0201	.0620	-.3289
53	73	510.05	.00	25.10	.9802	.4808	-.2639	-.0009	-.0021	.0085
53	72	510.05	2.11	25.15	.9765	.4797	-.2605	-.0040	.0018	-.0220
53	71	510.05	4.20	25.15	.9755	.4783	-.2596	-.0066	.0058	-.0501
53	70	510.05	8.38	25.05	.9671	.4700	-.2525	-.0103	.0156	-.1127
53	69	510.40	12.56	25.05	.9529	.4635	-.2372	-.0127	.0271	-.1802
53	68	510.40	14.62	24.94	.9431	.4577	-.2266	-.0136	.0338	-.2168

TABLE IV - Continued
 AERODYNAMIC CHARACTERISTICS IN SIDESLIP FOR VARIOUS ANGLES OF ATTACK.
 STABILITY AXES; M = 2.01

Run	Pt.	q	β , deg	α , deg	C_L	C_D	C_m	C_{L_s}	$C_{n,w}$	C_y
54	20	510.23	.01	.00	-.0052	.0293	.0075	-.0003	-.0014	.0035
54	19	510.40	2.00	.00	-.0065	.0290	.0079	-.0022	.0071	-.0220
54	18	510.23	3.97	.00	-.0092	.0292	.0099	-.0047	.0153	-.0475
54	17	510.23	5.99	.00	-.0100	.0290	.0123	-.0074	.0241	-.0740
54	16	510.40	8.01	.00	-.0135	.0285	.0160	-.0104	.0332	-.1032
54	15	510.76	12.03	.00	-.0192	.0285	.0293	-.0169	.0508	-.1670
54	14	510.40	16.03	.00	-.0138	.0273	.0390	-.0246	.0670	-.2379
54	13	510.23	20.05	.00	-.0047	.0262	.0523	-.0333	.0869	-.3213
54	12	510.23	24.12	.00	.0029	.0262	.0641	-.0402	.1058	-.4053
54	11	510.58	28.15	.00	.0099	.0259	.0720	-.0451	.1208	-.4826
54	21	509.69	-.01	4.17	.1898	.0427	-.0539	.0001	-.0003	-.0001
54	22	510.40	2.06	4.12	.1851	.0421	-.0528	-.0025	.0069	-.0248
54	23	510.58	4.08	4.08	.1800	.0411	-.0507	-.0050	.0146	-.0495
54	24	510.40	6.08	4.06	.1766	.0408	-.0483	-.0074	.0230	-.0776
54	25	510.23	8.11	4.04	.1735	.0402	-.0447	-.0099	.0317	-.1066
54	26	510.76	12.15	4.05	.1694	.0396	-.0325	-.0160	.0486	-.1723
54	27	510.40	16.09	4.02	.1728	.0394	-.0204	-.0227	.0640	-.2414
54	28	509.69	20.12	4.07	.1821	.0384	-.0093	-.0303	.0820	-.3202
54	29	510.40	24.23	4.07	.1855	.0388	.0046	-.0366	.1013	-.4041
54	38	510.76	.00	8.37	.3775	.0846	-.1073	.0000	-.0006	.0017
54	37	510.23	2.10	8.35	.3744	.0837	-.1063	-.0022	.0065	-.0244
54	36	510.23	4.16	8.31	.3719	.0829	-.1047	-.0044	.0139	-.0517
54	35	510.05	6.18	8.27	.3712	.0819	-.1023	-.0066	.0221	-.0804
54	34	510.05	8.22	8.22	.3698	.0814	-.0986	-.0091	.0305	-.1128
54	33	509.69	12.21	8.15	.3706	.0807	-.0902	-.0147	.0460	-.1476
54	32	510.23	16.22	8.11	.3683	.0800	-.0765	-.0212	.0602	-.1851
54	31	510.40	20.24	8.14	.3676	.0778	-.0643	-.0281	.0767	-.2451
54	30	510.58	24.28	8.09	.3637	.0772	-.0520	-.0339	.0950	-.3205
54	39	510.23	.00	12.57	.5555	.1531	-.1595	-.0002	-.0008	.0016
54	40	510.23	2.09	12.54	.5495	.1516	-.1574	-.0025	.0060	-.0260
54	41	510.05	4.17	12.51	.5479	.1507	-.1551	-.0049	.0129	-.0552
54	42	509.87	6.23	12.46	.5454	.1488	-.1517	-.0073	.0202	-.0846
54	43	510.76	8.27	12.40	.5421	.1473	-.1475	-.0096	.0278	-.1163
54	44	510.23	12.33	12.33	.5380	.1449	-.1364	-.0153	.0415	-.1790
54	45	510.23	16.35	12.29	.5325	.1424	-.1193	-.0212	.0554	-.2486
54	46	510.40	20.38	12.29	.5295	.1408	-.1096	-.0267	.0720	-.3247
54	47	510.40	25.02	12.60	.5387	.1467	-.1034	-.0326	.0918	-.4120
54	55	510.23	-.03	16.70	.7283	.2475	-.2179	-.0002	-.0011	.0043
54	54	509.69	2.08	16.72	.7273	.2472	-.2170	-.0028	.0048	-.0245
54	53	511.11	4.18	16.71	.7268	.2469	-.2144	-.0052	.0115	-.0560
54	52	509.69	6.25	16.67	.7219	.2448	-.2096	-.0075	.0180	-.0867
54	51	510.05	8.31	16.61	.7189	.2423	-.2054	-.0101	.0238	-.1166
54	50	510.05	12.43	16.53	.7101	.2376	-.1931	-.0147	.0362	-.1840
54	49	510.05	16.50	16.50	.6995	.2338	-.1740	-.0199	.0496	-.2533
54	48	509.69	20.57	16.45	.6887	.2291	-.1572	-.0256	.0652	-.3264
54	56	510.40	-.04	20.86	.8799	.3636	-.2757	-.0002	-.0015	.0061
54	57	510.40	2.10	20.85	.8772	.3621	-.2753	-.0031	.0035	-.0240
54	58	510.76	4.19	20.84	.8752	.3614	-.2728	-.0059	.0083	-.0545
54	59	510.40	6.26	20.82	.8714	.3581	-.2690	-.0087	.0126	-.0828
54	60	509.52	8.33	20.79	.8683	.3553	-.2661	-.0109	.0182	-.1147
54	61	509.87	12.48	20.76	.8553	.3502	-.2495	-.0146	.0306	-.1839
54	62	509.87	16.58	20.73	.8417	.3441	-.2304	-.0184	.0428	-.2517
54	63	509.87	20.51	20.58	.8227	.3339	-.2068	-.0227	.0586	-.3229
54	69	509.87	.00	25.06	1.0178	.5047	-.3422	-.0006	-.0018	.0061
54	68	510.23	2.11	25.09	1.0167	.5039	-.3397	-.0043	.0014	-.0215
54	67	509.87	4.14	25.09	1.0149	.5021	-.3388	-.0071	.0050	-.0496
54	66	509.34	6.30	25.04	1.0114	.4984	-.3356	-.0094	.0096	-.0795
54	65	510.23	8.31	25.00	1.0074	.4943	-.3308	-.0116	.0140	-.1093
54	64	510.05	12.54	25.01	.9917	.4871	-.3124	-.0147	.0245	-.1760

TABLE IV - Continued
 AERODYNAMIC CHARACTERISTICS IN SIDESLIP FOR VARIOUS ANGLES OF ATTACK.
 STABILITY AXES; M = 2.01

Run	Pt.	q	β , deg	α , deg	C_L	C_D	C_m	C_{l_s}	C_{n_w}	C_y
55	21	509.87	.00	.00	-.0105	.0289	.0086	-.0001	-.0011	.0015
55	20	510.23	1.99	.00	-.0080	.0284	.0078	-.0015	.0078	-.0213
55	19	509.87	3.97	-.01	-.0088	.0285	.0079	-.0028	.0168	-.0452
55	18	510.23	5.96	-.01	-.0077	.0282	.0082	-.0041	.0260	-.0699
55	17	510.05	7.99	-.01	-.0080	.0279	.0091	-.0054	.0354	-.0965
55	16	510.05	12.00	.00	-.0082	.0270	.0128	-.0081	.0530	-.1548
55	15	510.05	16.00	.00	-.0115	.0257	.0228	-.0108	.0705	-.2286
55	14	510.05	20.01	.00	-.0176	.0248	.0359	-.0138	.0873	-.3022
55	13	510.05	24.08	.00	-.0263	.0243	.0483	-.0170	.1074	-.3838
55	12	510.23	28.10	.00	-.0301	.0242	.0573	-.0191	.1227	-.4578
55	22	509.87	.00	4.17	.1906	.0419	-.0510	-.0003	.0000	-.0011
55	23	510.40	2.05	4.12	.1814	.0410	-.0489	-.0015	.0077	-.0223
55	24	510.40	4.08	4.08	.1798	.0406	-.0487	-.0025	.0160	-.0444
55	25	510.23	6.06	4.04	.1768	.0401	-.0475	-.0033	.0244	-.0680
55	26	510.23	8.06	4.02	.1766	.0396	-.0463	-.0042	.0332	-.0933
55	27	510.23	12.10	4.03	.1749	.0390	-.0402	-.0060	.0508	-.1539
55	28	510.23	16.04	4.04	.1663	.0376	-.0273	-.0078	.0677	-.2241
55	29	509.87	20.07	4.02	.1544	.0359	-.0127	-.0096	.0856	-.3004
55	30	510.05	24.16	4.06	.1402	.0347	.0042	-.0120	.1053	-.3811
55	39	510.05	.00	8.39	.3831	.0848	-.1121	-.0002	.0001	-.0012
55	38	509.69	2.10	8.36	.3815	.0844	-.1122	-.0009	.0077	-.0229
55	37	510.23	4.16	8.31	.3801	.0835	-.1121	-.0017	.0150	-.0448
55	36	509.87	6.17	8.25	.3794	.0829	-.1116	-.0023	.0226	-.0670
55	35	509.69	8.19	8.19	.3781	.0816	-.1101	-.0032	.0307	-.0922
55	34	509.69	12.15	8.11	.3704	.0795	-.1000	-.0050	.0468	-.1503
55	33	510.05	16.16	8.07	.3536	.0758	-.0833	-.0062	.0640	-.2219
55	32	510.05	20.17	8.06	.3327	.0716	-.0646	-.0074	.0818	-.2973
55	31	510.23	24.19	8.06	.3147	.0691	-.0460	-.0087	.1019	-.3779
55	40	509.69	.00	12.56	.5666	.1552	-.1731	-.0003	.0000	-.0004
55	41	510.23	2.08	12.53	.5648	.1544	-.1732	-.0011	.0070	-.0235
55	42	509.69	4.16	12.48	.5637	.1532	-.1732	-.0022	.0142	-.0456
55	43	509.69	6.22	12.43	.5608	.1516	-.1719	-.0033	.0211	-.0687
55	44	509.69	8.25	12.36	.5585	.1496	-.1700	-.0046	.0279	-.0932
55	45	509.69	12.29	12.29	.5487	.1461	-.1591	-.0062	.0421	-.1489
55	46	510.23	16.30	12.21	.5330	.1408	-.1405	-.0069	.0590	-.2195
55	47	509.87	20.31	12.20	.5133	.1358	-.1185	-.0075	.0773	-.2929
55	48	510.05	24.91	12.54	.5013	.1359	-.0974	-.0081	.1003	-.3822
55	56	509.87	.00	16.71	.7393	.2506	-.2313	-.0004	-.0005	.0014
55	55	509.34	2.08	16.72	.7413	.2517	-.2331	-.0017	.0058	-.0211
55	54	509.16	4.15	16.71	.7415	.2510	-.2331	-.0028	.0124	-.0447
55	53	510.76	6.24	16.65	.7388	.2495	-.2310	-.0045	.0185	-.0677
55	52	510.76	8.27	16.60	.7379	.2470	-.2295	-.0058	.0239	-.0913
55	51	511.11	12.40	16.50	.7275	.2416	-.2173	-.0077	.0364	-.1461
55	50	510.93	16.44	16.44	.7100	.2346	-.2000	-.0091	.0524	-.2118
55	49	510.76	20.49	16.38	.6884	.2272	-.1771	-.0098	.0721	-.2841
55	57	510.58	.00	20.86	.8989	.3712	-.2916	-.0003	-.0007	.0014
55	58	510.23	2.06	20.87	.8955	.3699	-.2906	-.0021	.0053	-.0217
55	59	510.05	4.19	20.83	.8964	.3696	-.2911	-.0037	.0106	-.0443
55	60	510.40	6.22	20.84	.8930	.3674	-.2888	-.0053	.0158	-.0674
55	61	509.87	8.29	20.79	.8865	.3631	-.2848	-.0068	.0209	-.0901
55	62	510.40	12.46	20.72	.8782	.3578	-.2732	-.0089	.0309	-.1399
55	63	510.05	16.52	20.66	.8599	.3494	-.2552	-.0099	.0447	-.2003
55	64	510.58	20.46	20.46	.8307	.3355	-.2296	-.0104	.0646	-.2708
55	70	510.58	.00	25.07	1.0429	.5161	-.3552	-.0006	-.0010	.0023
55	69	510.76	2.11	25.12	1.0445	.5181	-.3568	-.0023	.0040	-.0204
55	68	510.58	4.19	25.12	1.0411	.5164	-.3556	-.0042	.0082	-.0415
55	67	510.05	6.30	25.04	1.0366	.5116	-.3523	-.0058	.0122	-.0621
55	66	509.87	8.35	24.99	1.0322	.5074	-.3479	-.0072	.0165	-.0840
55	65	512.00	12.52	24.97	1.0185	.4999	-.3332	-.0089	.0258	-.1320

TABLE IV - Continued
AERODYNAMIC CHARACTERISTICS IN SIDESLIP FOR VARIOUS ANGLES OF ATTACK.

STABILITY AXES; M = 2.01

Run	Pt.	q	β , deg	α , deg	C_L	C_D	C_m	$C_{l,s}$	$C_{n,w}$	C_Y
56	20	509.87	.00	.00	-.0407	.0319	.0572	-.0002	-.0010	.0021
56	19	509.87	1.99	.00	-.0397	.0315	.0570	-.0014	.0091	-.0237
56	18	509.87	3.95	.00	-.0388	.0316	.0574	-.0025	.0188	-.0476
56	17	510.05	5.96	.00	-.0378	.0312	.0580	-.0036	.0287	-.0734
56	16	509.87	7.99	.00	-.0382	.0308	.0596	-.0048	.0388	-.1010
56	15	509.87	11.99	.00	-.0399	.0302	.0649	-.0071	.0582	-.1625
56	14	509.34	15.97	.00	-.0452	.0301	.0766	-.0092	.0775	-.2388
56	13	509.87	19.99	.00	-.0499	.0300	.0889	-.0115	.0958	-.3152
56	12	510.05	24.07	.00	-.0562	.0302	.0988	-.0143	.1128	-.3924
56	11	509.69	28.11	.00	-.0594	.0286	.1004	-.0167	.1213	-.4571
56	21	510.40	.00	4.19	.1556	.0408	-.0009	-.0003	.0000	-.0014
56	22	510.23	2.07	4.15	.1498	.0400	.0004	-.0013	.0087	-.0237
56	23	510.40	4.08	4.08	.1466	.0395	.0016	-.0022	.0174	-.0468
56	24	510.23	6.08	4.05	.1451	.0389	.0029	-.0028	.0247	-.0715
56	25	510.40	8.08	4.03	.1433	.0385	.0053	-.0036	.0360	-.0978
56	26	510.40	12.10	4.03	.1430	.0382	.0112	-.0050	.0550	-.1595
56	27	510.23	16.02	4.03	.1343	.0376	.0247	-.0063	.0731	-.2318
56	28	510.23	20.05	4.02	.1205	.0370	.0410	-.0073	.0926	-.3110
56	29	510.40	24.16	4.02	.1058	.0359	.0577	-.0091	.1132	-.3929
56	38	509.87	-0.1	8.41	.3491	.0788	-.0585	-.0003	-.0001	-.0006
56	37	509.87	2.10	8.38	.3474	.0783	-.0585	-.0008	.0084	-.0234
56	36	509.87	4.17	8.32	.3481	.0777	-.0591	-.0015	.0162	-.0463
56	35	510.05	6.20	8.26	.3470	.0768	-.0587	-.0021	.0244	-.0695
56	34	510.23	8.21	8.21	.3468	.0762	-.0576	-.0027	.0329	-.0955
56	33	508.99	12.17	8.12	.3382	.0741	-.0481	-.0041	.0499	-.1549
56	32	510.93	16.16	8.07	.3217	.0715	-.0307	-.0047	.0683	-.2281
56	31	510.05	20.17	8.06	.3010	.0684	-.0117	-.0052	.0874	-.3059
56	30	510.23	24.18	8.05	.2809	.0661	.0077	-.0057	.1086	-.3886
56	39	510.05	-0.2	12.60	.5317	.1443	-.1150	-.0004	-.0003	.0003
56	40	509.87	2.09	12.57	.5294	.1434	-.1146	-.0011	.0075	-.0240
56	41	510.05	4.16	12.55	.5272	.1429	-.1142	-.0019	.0151	-.0469
56	42	509.87	6.21	12.47	.5263	.1409	-.1138	-.0029	.0224	-.0700
56	43	509.87	8.28	12.40	.5240	.1393	-.1125	-.0041	.0296	-.0956
56	44	509.69	12.31	12.31	.5158	.1362	-.1037	-.0054	.0447	-.1542
56	45	509.87	16.31	12.21	.5001	.1314	-.0865	-.0058	.0623	-.2250
56	46	509.69	20.32	12.20	.4779	.1272	-.0638	-.0055	.0816	-.2995
56	47	509.69	24.92	12.49	.4657	.1273	-.0426	-.0050	.1060	-.3920
56	55	510.05	-0.3	16.74	.7017	.2348	-.1663	-.0005	-.0007	.0020
56	54	510.05	2.08	16.75	.7032	.2356	-.1679	-.0017	.0061	-.0215
56	53	510.05	4.16	16.74	.7030	.2351	-.1680	-.0026	.0130	-.0450
56	52	509.87	6.25	16.67	.7016	.2330	-.1663	-.0041	.0195	-.0692
56	51	509.87	8.32	16.62	.6990	.2308	-.1649	-.0054	.0254	-.0939
56	50	509.87	12.41	16.51	.6902	.2260	-.1554	-.0069	.0385	-.1489
56	49	509.87	16.46	16.46	.6765	.2209	-.1414	-.0079	.0548	-.2156
56	48	510.05	20.50	16.39	.6557	.2136	-.1212	-.0081	.0753	-.2898
56	56	509.87	-0.4	20.92	.8589	.3501	-.2200	-.0006	-.0009	.0028
56	57	509.87	2.10	20.89	.8584	.3492	-.2199	-.0020	.0056	-.0221
56	58	509.87	4.19	20.86	.8558	.3475	-.2196	-.0034	.0112	-.0457
56	59	510.23	6.27	20.85	.8538	.3460	-.2183	-.0049	.0165	-.0679
56	60	509.87	8.34	20.81	.8499	.3429	-.2159	-.0061	.0222	-.0925
56	61	509.87	12.48	20.76	.8420	.3385	-.2060	-.0078	.0327	-.1424
56	62	510.05	16.55	20.69	.8241	.3305	-.1904	-.0084	.0471	-.2046
56	63	510.05	20.45	20.51	.7979	.3184	-.1695	-.0087	.0670	-.2742
56	69	510.23	.00	25.11	1.0051	.4906	-.2807	-.0008	-.0013	.0038
56	68	510.23	2.11	25.15	1.0057	.4919	-.2817	-.0021	.0041	-.0208
56	67	510.23	4.20	25.15	1.0036	.4905	-.2812	-.0039	.0083	-.0419
56	66	510.05	6.31	25.08	.9994	.4866	-.2784	-.0053	.0127	-.0635
56	65	510.23	8.32	25.04	.9953	.4832	-.2744	-.0064	.0172	-.0853
56	64	510.40	12.53	25.00	.9826	.4756	-.2610	-.0077	.0271	-.1347

TABLE IV - Continued
 AERODYNAMIC CHARACTERISTICS IN SIDESLIP FOR VARIOUS ANGLES OF ATTACK.
 STABILITY AXES; M = 2.01

Run	Pt.	q	β , deg	α , deg	C_L	C_D	C_m	$C_{l,s}$	$C_{n,w}$	C_Y
57	23	510.76	.00	.00	-.0529	.0330	.0863	-.0002	-.0011	.0029
57	22	510.23	.99	.00	-.0515	.0330	.0859	-.0011	.0033	-.0090
57	21	510.23	1.99	.00	-.0517	.0330	.0855	-.0020	.0074	-.0199
57	20	510.23	3.97	.00	-.0505	.0331	.0845	-.0038	.0159	-.0426
57	19	510.05	5.97	.01	-.0477	.0325	.0821	-.0055	.0245	-.0670
57	18	510.05	7.99	.01	-.0449	.0321	.0788	-.0074	.0332	-.0916
57	17	510.76	12.00	.00	-.0388	.0306	.0684	-.0113	.0499	-.1496
57	16	510.23	16.00	.03	-.0273	.0288	.0537	-.0150	.0664	-.2222
57	15	510.76	20.03	.00	-.0187	.0269	.0410	-.0186	.0826	-.2955
57	14	510.58	25.09	.00	-.0098	.0261	.0245	-.0232	.1060	-.3941
57	13	510.58	28.10	.00	-.0013	.0255	.0135	-.0257	.1202	-.4544
57	24	510.40	.00	4.21	.1434	.0414	.0292	-.0004	.0000	-.0007
57	25	510.58	2.07	4.16	.1394	.0410	.0281	-.0022	.0075	-.0216
57	26	510.76	4.10	4.10	.1396	.0403	.0247	-.0038	.0155	-.0435
57	27	510.58	6.10	4.08	.1413	.0395	.0205	-.0051	.0237	-.0667
57	28	510.58	10.09	4.03	.1460	.0388	.0126	-.0083	.0404	-.1176
57	29	510.58	12.10	4.03	.1508	.0386	.0085	-.0101	.0494	-.1512
57	30	510.40	16.05	4.01	.1542	.0373	.0004	-.0129	.0660	-.2213
57	31	510.40	20.07	4.02	.1553	.0355	-.0096	-.0149	.0838	-.2980
57	32	510.58	24.14	4.01	.1598	.0350	-.0213	-.0177	.1027	-.3768
57	40	510.40	.00	8.44	.3439	.0799	-.0375	-.0003	-.0001	.0002
57	39	510.76	2.11	8.41	.3440	.0798	-.0389	-.0017	.0077	-.0223
57	38	510.23	4.17	8.36	.3435	.0791	-.0412	-.0029	.0151	-.0441
57	37	510.23	8.23	8.23	.3445	.0771	-.0469	-.0056	.0308	-.0920
57	36	510.23	12.17	8.12	.3449	.0754	-.0508	-.0085	.0474	-.1508
57	35	510.76	16.16	8.08	.3403	.0727	-.0533	-.0108	.0653	-.2222
57	34	510.23	20.19	8.07	.3388	.0706	-.0616	-.0121	.0837	-.2995
57	33	510.40	24.19	8.06	.3319	.0686	-.0680	-.0139	.1034	-.3800
57	41	510.40	.00	12.62	.5295	.1460	-.0968	-.0003	-.0001	.0001
57	42	510.40	2.07	12.61	.5270	.1454	-.0968	-.0017	.0073	-.0230
57	43	510.58	4.19	12.56	.5271	.1441	-.0986	-.0031	.0148	-.0459
57	44	510.40	8.29	12.41	.5275	.1412	-.1025	-.0064	.0295	-.0942
57	45	510.23	12.31	12.31	.5246	.1383	-.1041	-.0094	.0447	-.1526
57	46	510.58	16.32	12.22	.5195	.1348	-.1052	-.0106	.0635	-.2261
57	47	510.23	20.30	12.19	.5139	.1318	-.1086	-.0113	.0824	-.2995
57	48	510.40	24.91	12.48	.5168	.1341	-.1156	-.0113	.1051	-.3887
57	49	510.58	.00	16.77	.6975	.2356	-.1473	-.0005	-.0005	.0018
57	54	510.76	4.20	16.76	.6996	.2357	-.1515	-.0041	.0136	-.0459
57	53	510.76	8.32	16.63	.7016	.2323	-.1577	-.0076	.0263	-.0936
57	52	510.40	12.41	16.51	.6984	.2288	-.1589	-.0101	.0411	-.1515
57	51	510.58	16.45	16.45	.6940	.2249	-.1582	-.0115	.0590	-.2200
57	50	510.23	20.49	16.38	.6806	.2192	-.1526	-.0117	.0792	-.2943
57	49	510.76	22.51	16.35	.6735	.2169	-.1506	-.0115	.0890	-.3322
57	58	510.05	.00	20.94	.9509	.3491	-.1950	-.0006	-.0008	.0027
57	59	510.05	2.11	20.92	.9519	.3495	-.1968	-.0024	.0060	-.0223
57	60	510.40	4.20	20.89	.9542	.3492	-.2016	-.0047	.0129	-.0477
57	61	510.93	8.34	20.83	.9567	.3463	-.2123	-.0081	.0254	-.0963
57	62	510.23	12.49	20.77	.9507	.3417	-.2070	-.0100	.0376	-.1492
57	63	510.40	16.55	20.69	.9375	.3346	-.2003	-.0113	.0525	-.2113
57	64	510.23	20.48	20.48	.9161	.3236	-.1890	-.0107	.0708	-.2790
57	70	510.40	-.05	25.17	.9888	.4870	-.2386	-.0009	-.0011	.0035
57	69	510.58	2.07	25.21	.9898	.4884	-.2407	-.0029	.0050	-.0211
57	68	510.58	4.21	25.18	.9900	.4877	-.2436	-.0053	.0105	-.0440
57	67	510.23	8.38	25.05	.9879	.4818	-.2492	-.0082	.0223	-.0923
57	66	510.40	12.55	25.04	.9775	.4754	-.2423	-.0098	.0316	-.1405
57	65	510.58	14.60	24.91	.9682	.4674	-.2374	-.0105	.0375	-.1670

TABLE IV - Continued
 AERODYNAMIC CHARACTERISTICS IN SIDESLIP FOR VARIOUS ANGLES OF ATTACK.
 STABILITY AXES; M = 2.01

Run	Pt.	q	β , deg	α , deg	C_L	C_D	C_m	$C_{l,s}$	$C_{n,w}$	C_y
58	22	511.29	-0.01	.00	-.0202	.0289	.0298	-.0002	-.0012	.0023
58	21	511.11	1.00	.00	-.0205	.0284	.0296	-.0010	.0031	-.0086
58	20	511.11	1.99	.00	-.0191	.0284	.0290	-.0020	.0073	-.0204
58	19	511.29	3.97	.00	-.0194	.0285	.0282	-.0038	.0159	-.0431
58	18	511.11	5.96	.00	-.0166	.0282	.0259	-.0056	.0244	-.0667
58	17	511.29	8.00	.00	-.0137	.0275	.0226	-.0076	.0332	-.0922
58	16	511.11	11.99	.02	-.0057	.0265	.0129	-.0117	.0506	-.1503
58	15	511.29	16.00	.00	-.0032	.0256	-.0010	-.0159	.0682	-.2249
58	14	511.11	20.02	.00	-.0137	.0253	-.0146	-.0201	.0853	-.2994
58	13	511.46	24.09	.00	.0231	.0248	-.0302	-.0245	.1052	-.3806
58	12	510.76	28.09	.00	.0366	.0249	-.0481	-.0283	.1247	-.4616
58	23	511.64	.00	4.18	.1714	.0404	-.0216	-.0003	-.0001	-.0012
58	24	511.29	2.06	4.13	.1693	.0401	-.0232	-.0023	.0076	-.0218
58	25	511.29	4.08	4.08	.1697	.0394	-.0270	-.0039	.0158	-.0441
58	26	511.29	8.09	4.03	.1727	.0389	-.0367	-.0071	.0327	-.0926
58	27	511.64	12.09	4.03	.1825	.0388	-.0462	-.0106	.0518	-.1549
58	28	510.93	16.03	4.00	.1849	.0382	-.0530	-.0137	.0702	-.2274
58	29	512.17	20.04	4.02	.1878	.0379	-.0615	-.0163	.0886	-.3044
58	30	511.82	24.15	4.01	.1915	.0372	-.0758	-.0200	.1090	-.3864
58	38	511.46	.00	8.41	.3711	.0828	-.0890	-.0003	-.0001	-.0004
58	37	511.46	2.10	8.37	.3701	.0823	-.0902	-.0019	.0079	-.0230
58	36	511.82	4.17	8.31	.3708	.0817	-.0930	-.0033	.0156	-.0447
58	35	511.46	8.19	8.19	.3738	.0804	-.0998	-.0063	.0324	-.0938
58	34	511.64	12.15	8.11	.3748	.0793	-.1037	-.0094	.0517	-.1566
58	33	511.46	16.15	8.07	.3696	.0769	-.1030	-.0117	.0708	-.2303
58	32	512.00	20.15	8.05	.3660	.0753	-.1110	-.0132	.0903	-.3090
58	31	511.64	24.17	8.05	.3631	.0748	-.1202	-.0157	.1106	-.3907
58	39	511.46	.00	12.58	.5571	.1522	-.1506	-.0004	-.0004	.0005
58	40	511.46	2.07	12.56	.5548	.1517	-.1505	-.0017	.0077	-.0237
58	41	511.64	4.15	12.53	.5535	.1509	-.1510	-.0034	.0159	-.0476
58	42	511.64	8.27	12.40	.5543	.1481	-.1540	-.0068	.0326	-.0991
58	43	511.46	12.28	12.28	.5507	.1450	-.1542	-.0096	.0508	-.1616
58	44	511.82	16.27	12.19	.5445	.1418	-.1536	-.0110	.0707	-.2361
58	45	511.64	20.28	12.18	.5387	.1399	-.1568	-.0120	.0891	-.3092
58	46	512.00	24.89	12.47	.5414	.1432	-.1635	-.0122	.1115	-.3989
58	54	511.82	.00	16.72	.7220	.2445	-.2008	-.0004	-.0006	.0013
58	53	511.64	2.08	16.74	.7244	.2451	-.2026	-.0022	.0068	-.0222
58	52	511.82	4.18	16.72	.7260	.2451	-.2049	-.0037	.0149	-.0477
58	51	512.17	8.31	16.60	.7283	.2429	-.2116	-.0070	.0318	-.1017
58	50	511.82	12.39	16.45	.7245	.2394	-.2110	-.0096	.0490	-.1636
58	49	511.82	16.42	16.42	.7158	.2353	-.2043	-.0111	.0663	-.2311
58	48	511.82	20.47	16.36	.7035	.2296	-.1973	-.0120	.0843	-.3018
58	47	511.46	22.50	16.34	.6947	.2267	-.1943	-.0118	.0940	-.3401
58	55	511.46	.00	20.91	.8751	.3615	-.2464	-.0005	-.0014	.0031
58	56	511.46	2.10	20.89	.8771	.3618	-.2486	-.0022	.0080	-.0260
58	57	511.64	4.16	20.87	.8762	.3612	-.2508	-.0038	.0168	-.0528
58	58	511.46	8.33	20.80	.8760	.3577	-.2576	-.0068	.0305	-.1035
58	59	511.46	12.44	20.76	.8674	.3528	-.2483	-.0088	.0428	-.1572
58	60	511.82	16.52	20.66	.8531	.3451	-.2400	-.0105	.0581	-.2201
58	61	510.93	20.46	20.46	.8349	.3360	-.2266	-.0106	.0757	-.2869
58	67	511.64	.00	25.13	1.0027	.4966	-.2781	-.0008	-.0013	.0037
58	66	511.64	2.12	25.17	1.0041	.4984	-.2792	-.0025	.0055	-.0219
58	65	511.64	4.20	25.15	1.0019	.4963	-.2781	-.0046	.0125	-.0469
58	64	511.46	8.37	25.04	.9973	.4909	-.2788	-.0074	.0231	-.0941
58	63	511.82	12.54	25.02	.9886	.4847	-.2735	-.0090	.0334	-.1433
58	62	510.58	14.58	24.88	.9791	.4773	-.2701	-.0096	.0407	-.1722

TABLE IV - Continued
 AERODYNAMIC CHARACTERISTICS IN SIDESLIP FOR VARIOUS ANGLES OF ATTACK.
 STABILITY AXES; M = 2.01

Run	Pt.	q	β , deg	α , deg	C_L	C_D	C_m	C_{l_s}	C_{n_w}	C_Y
59	23	513.77	-.01	.00	-.0199	.0272	.0145	-.0002	-.0009	.0023
59	22	513.77	.98	.00	-.0202	.0267	.0145	-.0010	.0032	-.0095
59	21	513.77	1.99	.00	-.0189	.0268	.0144	-.0018	.0075	-.0203
59	20	513.94	3.97	.00	-.0193	.0269	.0145	-.0035	.0159	-.0429
59	19	513.59	5.97	.00	-.0181	.0270	.0141	-.0051	.0243	-.0664
59	18	513.24	8.00	.01	-.0168	.0260	.0137	-.0067	.0330	-.0918
59	17	513.94	12.00	.00	-.0152	.0253	.0128	-.0101	.0495	-.1486
59	16	513.59	16.01	.03	-.0140	.0242	.0133	-.0134	.0655	-.2206
59	15	513.41	20.03	.00	-.0127	.0237	.0131	-.0171	.0806	-.2918
59	14	513.41	24.10	.00	-.0109	.0239	.0130	-.0207	.0984	-.3697
59	13	513.77	28.11	.00	-.0096	.0239	.0140	-.0236	.1171	-.4484
59	24	513.77	.00	4.18	.1584	.0381	-.0136	-.0005	-.0003	.0006
59	25	513.59	2.06	4.13	.1528	.0375	-.0129	-.0020	.0074	-.0204
59	26	513.94	4.08	4.08	.1512	.0371	-.0133	-.0032	.0151	-.0421
59	27	513.41	8.08	4.03	.1532	.0366	-.0139	-.0056	.0318	-.0913
59	28	513.59	12.09	4.03	.1530	.0359	-.0126	-.0079	.0489	-.1503
59	29	513.59	16.05	4.01	.1521	.0351	-.0099	-.0104	.0645	-.2189
59	30	513.41	20.08	4.02	.1462	.0341	-.0060	-.0129	.0810	-.2932
59	31	513.41	24.19	4.02	.1405	.0333	-.0039	-.0156	.0990	-.3705
59	39	513.41	-.01	8.43	.3398	.0768	-.0457	-.0004	-.0001	.0003
59	38	513.24	2.11	8.40	.3384	.0763	-.0462	-.0014	.0075	-.0212
59	37	513.41	4.17	8.32	.3374	.0757	-.0470	-.0023	.0147	-.0438
59	36	513.77	8.22	8.22	.3364	.0742	-.0462	-.0043	.0303	-.0914
59	35	513.41	12.17	9.12	.3335	.0724	-.0438	-.0066	.0461	-.1479
59	34	513.41	16.18	8.09	.3232	.0700	-.0360	-.0084	.0625	-.2181
59	33	513.41	20.19	8.07	.3112	.0676	-.0294	-.0099	.0795	-.2935
59	32	513.59	24.20	8.06	.2988	.0656	-.0248	-.0119	.0982	-.3714
59	40	513.41	-.02	12.62	.5090	.1405	-.0771	-.0005	-.0004	.0009
59	41	513.24	2.10	12.60	.5082	.1403	-.0770	-.0015	.0070	-.0221
59	42	513.24	4.19	12.56	.5065	.1396	-.0767	-.0027	.0142	-.0448
59	43	513.24	8.29	12.42	.5047	.1362	-.0763	-.0052	.0281	-.0919
59	44	513.41	12.30	12.34	.4978	.1335	-.0714	-.0073	.0424	-.1496
59	45	513.41	16.33	12.23	.4874	.1294	-.0621	-.0085	.0592	-.2198
59	46	513.41	20.33	12.21	.4743	.1256	-.0546	-.0098	.0768	-.2913
59	47	513.06	24.95	12.50	.4695	.1273	-.0481	-.0105	.0989	-.3792
59	55	512.88	.00	16.78	.6664	.2267	-.1061	-.0006	-.0007	.0025
59	54	513.06	2.09	16.79	.6677	.2275	-.1076	-.0020	.0057	-.0198
59	53	513.41	4.20	16.77	.6689	.2273	-.1083	-.0034	.0127	-.0440
59	52	513.59	8.34	16.66	.6674	.2238	-.1075	-.0065	.0246	-.0912
59	51	513.41	12.44	16.55	.6587	.2198	-.1004	-.0085	.0372	-.1465
59	50	513.06	16.48	16.48	.6472	.2150	-.0911	-.0100	.0533	-.2117
59	49	513.06	20.52	16.41	.6327	.2094	-.0811	-.0110	.0731	-.2853
59	48	513.59	22.55	16.38	.6233	.2061	-.0756	-.0112	.0830	-.3229
59	56	513.06	.00	20.96	.8148	.3372	-.1404	-.0007	-.0009	.0032
59	57	513.41	2.11	20.97	.8148	.3376	-.1406	-.0023	.0055	-.0214
59	58	513.59	4.21	20.94	.8136	.3368	-.1410	-.0041	.0112	-.0447
59	59	513.41	8.37	20.87	.8098	.3327	-.1383	-.0071	.0219	-.0909
59	60	513.41	12.51	20.80	.8008	.3268	-.1303	-.0092	.0320	-.1403
59	61	513.41	16.57	20.72	.7849	.3196	-.1187	-.0105	.0462	-.2018
59	62	513.24	20.51	20.51	.7607	.3078	-.1032	-.0109	.0665	-.2719
59	67	513.24	2.12	25.24	.9494	.4725	-.1784	-.0024	.0041	-.0194
59	66	513.41	4.22	25.24	.9487	.4717	-.1789	-.0044	.0084	-.0411
59	65	512.88	8.40	25.11	.9404	.4638	-.1736	-.0074	.0172	-.0841
59	64	513.41	12.59	25.10	.9282	.4574	-.1627	-.0090	.0270	-.1329
59	63	513.41	14.63	24.95	.9162	.4491	-.1544	-.0098	.0325	-.1591

TABLE IV - Continued
 AERODYNAMIC CHARACTERISTICS IN SIDESLIP FOR VARIOUS ANGLES OF ATTACK.
 STABILITY AXES; M = 2.01

Run	Pt.	q	β ,deg	α ,deg	C_L	C_D	C_m	C_{l_s}	$C_{n,w}$	C_Y
60	21	510.23	.00	.00	-.0161	.0134	.0019	-.0003	-.0003	.0008
60	20	509.87	2.00	.00	-.0140	.0133	.0016	-.0004	-.0024	-.0042
60	19	509.87	4.01	.00	-.0136	.0138	.0016	-.0004	-.0042	-.0093
60	18	510.23	6.04	.00	-.0130	.0138	.0016	-.0004	-.0061	-.0152
60	17	509.87	8.09	.00	-.0124	.0139	.0016	-.0004	-.0080	-.0230
60	16	510.23	12.14	.00	-.0117	.0143	.0018	-.0005	-.0107	-.0496
60	15	510.23	16.19	.00	-.0118	.0148	.0024	-.0006	-.0133	-.0899
60	14	509.87	20.24	.00	-.0101	.0153	.0022	-.0006	-.0149	-.1332
60	13	510.05	24.39	.00	-.0112	.0151	.0014	-.0010	-.0146	-.1813
60	12	510.05	28.40	.00	-.0108	.0157	.0009	-.0010	-.0137	-.2296
60	22	509.69	.00	4.17	.1661	.0257	-.0255	-.0004	-.0005	-.0002
60	23	509.87	2.05	4.12	.1584	.0249	-.0243	-.0013	-.0025	-.0041
60	24	509.87	4.10	4.10	.1549	.0253	-.0236	-.0019	-.0043	-.0094
60	25	509.69	6.12	4.07	.1553	.0254	-.0236	-.0021	-.0061	-.0163
60	26	510.05	8.15	4.07	.1539	.0260	-.0231	-.0026	-.0080	-.0232
60	27	510.05	12.21	4.07	.1539	.0264	-.0211	-.0029	-.0109	-.0504
60	28	509.69	16.20	4.05	.1532	.0266	-.0201	-.0033	-.0137	-.0888
60	29	509.69	20.28	4.07	.1491	.0267	-.0183	-.0034	-.0140	-.1361
60	30	509.87	24.42	4.06	.1406	.0256	-.0160	-.0043	-.0139	-.1844
60	39	509.52	.00	8.42	.3433	.0650	-.0554	-.0005	-.0003	-.0005
60	38	509.52	2.10	8.37	.3430	.0649	-.0560	-.0015	-.0024	-.0063
60	37	509.69	4.18	8.34	.3432	.0655	-.0567	-.0025	-.0043	-.0122
60	36	509.87	6.21	8.28	.3409	.0647	-.0557	-.0033	-.0060	-.0191
60	35	509.34	8.26	8.26	.3400	.0648	-.0540	-.0043	-.0079	-.0279
60	34	509.69	12.26	8.22	.3359	.0641	-.0519	-.0059	-.0119	-.0525
60	33	509.69	16.30	8.15	.3239	.0618	-.0433	-.0070	-.0137	-.0924
60	32	509.87	20.37	8.15	.3133	.0605	-.0415	-.0075	-.0135	-.1407
60	31	510.05	24.42	8.14	.3009	.0592	-.0377	-.0085	-.0124	-.1898
60	40	509.52	.00	12.61	.5147	.1310	-.0860	-.0006	-.0002	.0001
60	41	508.81	2.09	12.58	.5097	.1296	-.0849	-.0022	-.0019	-.0075
60	42	509.16	4.19	12.56	.5092	.1293	-.0853	-.0038	-.0041	-.0146
60	43	509.69	6.25	12.50	.5078	.1284	-.0851	-.0057	-.0060	-.0226
60	44	509.52	8.30	12.44	.5060	.1278	-.0836	-.0075	-.0081	-.0322
60	45	509.16	12.38	12.38	.4964	.1249	-.0756	-.0104	-.0115	-.0607
60	46	510.05	16.43	12.30	.4831	.1213	-.0652	-.0121	-.0119	-.1015
60	47	508.63	20.48	12.31	.4721	.1192	-.0624	-.0138	-.0126	-.1433
60	48	508.10	25.12	12.60	.4697	.1217	-.0607	-.0155	-.0113	-.1972
60	56	509.34	.00	16.77	.6703	.2178	-.1134	-.0007	-.0001	.0007
60	55	509.34	2.09	16.78	.6705	.2180	-.1145	-.0032	-.0030	-.0062
60	54	509.69	4.17	16.77	.6718	.2187	-.1154	-.0055	-.0047	-.0159
60	53	509.52	6.24	16.74	.6704	.2179	-.1149	-.0078	-.0057	-.0274
60	52	509.34	8.31	16.67	.6660	.2155	-.1115	-.0102	-.0074	-.0393
60	51	509.69	12.47	16.58	.6571	.2117	-.1038	-.0146	-.0107	-.0675
60	50	509.52	16.54	16.54	.6452	.2083	-.0928	-.0178	-.0106	-.1057
60	49	509.69	20.64	16.51	.6309	.2033	-.0867	-.0209	-.0110	-.1459
60	57	509.34	.00	20.96	.8191	.3293	-.1475	-.0005	.0002	.0003
60	58	509.52	2.11	20.94	.8172	.3283	-.1476	-.0032	-.0007	-.0121
60	59	509.69	4.21	20.93	.8150	.3273	-.1468	-.0062	-.0023	-.0231
60	60	509.87	6.29	20.91	.8126	.3260	-.1447	-.0087	-.0035	-.0347
60	61	509.34	8.37	20.87	.8083	.3241	-.1416	-.0116	-.0048	-.0468
60	62	509.34	12.54	20.84	.7981	.3199	-.1318	-.0170	-.0083	-.0723
60	63	509.69	16.63	20.79	.7805	.3129	-.1189	-.0213	-.0086	-.1081
60	64	509.52	20.60	20.60	.7579	.3023	-.1074	-.0254	-.0092	-.1440
60	71	509.52	.00	25.18	.9536	.4632	-.1856	-.0004	.0005	.0001
60	70	509.52	2.12	25.21	.9523	.4631	-.1853	-.0033	-.0005	-.0131
60	69	509.52	4.21	25.22	.9498	.4620	-.1841	-.0060	-.0008	-.0268
60	68	509.34	6.28	25.17	.9462	.4602	-.1812	-.0085	-.0012	-.0399
60	67	509.52	8.40	25.11	.9411	.4564	-.1769	-.0115	-.0020	-.0533
60	66	509.52	12.55	25.13	.9259	.4508	-.1631	-.0174	-.0046	-.0795
60	65	509.16	14.64	24.97	.9133	.4416	-.1535	-.0204	-.0058	-.0944

TABLE IV - Continued
AERODYNAMIC CHARACTERISTICS IN SIDESLIP FOR VARIOUS ANGLES OF ATTACK.

STABILITY AXES; M = 2.01

Run	Pt.	q	β , deg	α , deg	C_L	C_D	C_m	$C_{l,s}$	$C_{n,w}$	C_y
61	21	509.34	-01	.00	-.0126	.0148	-.0014	.0002	-.0003	-.0001
61	20	509.52	2.02	.00	-.0117	.0148	-.0026	.0018	-.0024	-.0086
61	19	509.34	4.03	.01	-.0094	.0152	-.0059	.0035	-.0044	-.0162
61	18	509.69	6.06	.00	-.0071	.0155	-.0100	.0052	-.0064	-.0249
61	17	509.16	8.10	.00	-.0033	.0159	-.0155	.0071	-.0085	-.0353
61	16	508.28	12.16	.02	-.0010	.0163	-.0212	.0107	-.0110	-.0655
61	15	509.52	16.20	.00	-.0177	.0169	-.0088	.0143	-.0137	-.1056
61	14	508.99	20.28	.04	-.0360	.0175	.0012	.0181	-.0153	-.1534
61	13	509.87	24.40	.00	-.0552	.0183	.0062	.0206	-.0162	-.2037
61	12	508.28	28.45	.00	-.0700	.0183	.0064	.0229	-.0176	-.2522
61	22	509.16	.00	4.16	.1670	.0273	-.0294	.0001	-.0007	-.0001
61	23	509.34	2.06	4.13	.1620	.0271	-.0300	.0010	-.0032	-.0058
61	24	509.34	4.10	4.10	.1624	.0275	-.0323	.0022	-.0055	-.0128
61	25	509.34	6.12	4.07	.1615	.0274	-.0354	.0037	-.0077	-.0204
61	26	509.34	8.15	4.09	.1653	.0282	-.0403	.0052	-.0095	-.0300
61	27	509.52	12.22	4.07	.1687	.0292	-.0452	.0083	-.0125	-.0581
61	28	509.16	16.22	4.05	.1517	.0283	-.0352	.0112	-.0131	-.1007
61	29	508.99	20.28	4.07	.1315	.0270	-.0243	.0139	-.0146	-.1479
61	30	509.69	24.43	4.07	.1113	.0257	-.0194	.0158	-.0155	-.1976
61	39	509.34	-01	8.41	.3455	.0666	-.0580	.0003	-.0009	.0004
61	38	509.16	2.10	8.37	.3426	.0660	-.0587	.0012	-.0038	-.0052
61	37	509.52	4.18	8.33	.3416	.0659	-.0609	.0021	-.0061	-.0119
61	36	509.16	6.21	8.28	.3417	.0662	-.0639	.0028	-.0084	-.0197
61	35	508.81	8.25	8.25	.3424	.0662	-.0673	.0036	-.0100	-.0295
61	34	509.69	12.26	8.18	.3375	.0654	-.0680	.0054	-.0119	-.0591
61	33	509.69	16.28	8.14	.3189	.0625	-.0599	.0072	-.0120	-.1012
61	32	509.52	20.35	8.14	.2954	.0595	-.0492	.0090	-.0136	-.1448
61	31	509.34	24.41	8.14	.2715	.0558	-.0438	.0101	-.0153	-.1898
61	40	509.16	-02	12.61	.5094	.1311	-.0828	.0002	-.0009	.0010
61	41	509.52	2.09	12.58	.5084	.1305	-.0839	.0003	-.0038	-.0046
61	42	509.34	4.21	12.54	.5073	.1296	-.0863	.0004	-.0064	-.0117
61	43	509.34	6.24	12.49	.5065	.1297	-.0888	.0004	-.0076	-.0218
61	44	509.52	8.30	12.44	.5065	.1290	-.0908	.0002	-.0094	-.0324
61	45	509.34	12.36	12.36	.4932	.1248	-.0849	.0009	-.0101	-.0644
61	46	509.34	16.37	12.30	.4796	.1219	-.0822	.0014	-.0119	-.1005
61	47	509.34	20.44	12.28	.4580	.1170	-.0755	.0022	-.0130	-.1412
61	48	509.34	25.11	12.59	.4375	.1150	-.0679	.0023	-.0142	-.1908
61	56	509.87	.00	16.78	.6664	.2176	-.1044	.0001	-.0009	.0015
61	55	510.05	2.06	16.80	.6668	.2178	-.1058	-.0007	-.0033	-.0065
61	54	509.16	4.20	16.78	.6658	.2175	-.1074	-.0013	-.0047	-.0174
61	53	508.63	6.24	16.72	.6625	.2162	-.1066	-.0017	-.0045	-.0311
61	52	507.92	8.34	16.66	.6561	.2136	-.1036	-.0024	-.0058	-.0442
61	51	509.69	12.43	16.59	.6509	.2111	-.1021	-.0040	-.0079	-.0709
61	50	509.52	16.51	16.51	.6378	.2061	-.1027	-.0051	-.0097	-.1025
61	49	509.52	20.58	16.46	.6151	.1989	-.0988	-.0060	-.0108	-.1392
61	57	508.45	.00	20.97	.8133	.3282	-.1290	-.0002	-.0013	.0040
61	58	508.99	2.11	20.95	.8111	.3269	-.1293	-.0012	-.0029	-.0077
61	59	509.52	4.21	20.94	.8089	.3264	-.1296	-.0027	-.0042	-.0198
61	60	509.52	6.26	20.94	.8070	.3260	-.1300	-.0042	-.0057	-.0305
61	61	509.16	8.33	20.90	.8032	.3238	-.1290	-.0054	-.0061	-.0438
61	62	509.69	12.49	20.85	.7926	.3190	-.1245	-.0073	-.0056	-.0740
61	63	508.99	16.59	20.74	.7772	.3116	-.1231	-.0096	-.0071	-.1036
61	64	509.52	20.57	20.57	.7526	.3003	-.1187	-.0115	-.0087	-.1358
61	70	508.99	-05	25.23	.9503	.4641	-.1605	-.0005	-.0021	.0048
61	69	509.52	2.12	25.26	.9487	.4643	-.1591	-.0022	-.0033	-.0068
61	68	508.99	4.22	25.25	.9464	.4628	-.1581	-.0039	-.0046	-.0177
61	67	508.99	6.29	25.20	.9417	.4600	-.1575	-.0057	-.0060	-.0290
61	66	509.34	8.40	25.12	.9365	.4565	-.1573	-.0075	-.0065	-.0416
61	65	508.81	12.59	25.10	.9246	.4506	-.1516	-.0099	-.0056	-.0717

TABLE IV - Continued
AERODYNAMIC CHARACTERISTICS IN SIDESLIP FOR VARIOUS ANGLES OF ATTACK.

STABILITY AXES; M = 2.01

Run	Pt.	q	β , deg	α , deg	C_L	C_D	C_m	$C_{i,s}$	$C_{n,w}$	C_y
62	21	510.40	-01	00	-.0118	.0147	.0033	-.0001	-.0002	-.0028
62	20	508.81	2.02	00	-.0130	.0148	.0047	-.0018	-.0023	-.0097
62	19	511.64	4.03	00	-.0140	.0149	.0078	-.0035	-.0044	-.0174
62	18	510.23	6.06	00	-.0163	.0152	.0125	-.0053	-.0066	-.0262
62	17	510.40	8.12	00	-.0201	.0156	.0181	-.0071	-.0086	-.0367
62	16	510.40	12.17	00	-.0226	.0155	.0245	-.0106	-.0108	-.0662
62	71	510.58	12.17	00	-.0274	.0160	.0256	-.0106	-.0106	-.0681
62	15	510.76	16.22	-03	-.0077	.0164	.0134	-.0143	-.0133	-.1066
62	14	510.76	20.28	00	.0146	.0166	.0025	-.0179	-.0145	-.1562
62	13	509.52	24.40	00	.0288	.0168	-.0028	-.0212	-.0153	-.2055
62	12	510.40	28.46	00	.0412	.0172	-.0031	-.0235	-.0151	-.2561
62	22	510.58	00	4.17	.3659	.0270	-.0242	-.0002	-.0004	-.0029
62	23	510.40	2.06	4.13	.1595	.0263	-.0219	-.0029	-.0018	-.0125
62	24	510.40	4.11	4.11	.1541	.0262	-.0182	-.0053	-.0032	-.0226
62	25	510.23	6.14	4.10	.1513	.0260	-.0137	-.0073	-.0050	-.0332
62	26	510.58	8.17	4.08	.1456	.0258	-.0078	-.0095	-.0071	-.0439
62	27	510.40	12.25	4.08	.1489	.0264	-.0032	-.0135	-.0101	-.0766
62	28	510.40	16.24	4.09	.1647	.0285	-.0128	-.0177	-.0141	-.1146
62	29	509.69	20.32	4.11	.1845	.0302	-.0223	-.0219	-.0159	-.1617
62	30	510.05	24.49	4.08	.1951	.0312	-.0236	-.0260	-.0157	-.2146
62	39	510.23	00	8.41	.3460	.0662	-.0568	-.0003	-.0004	-.0032
62	38	510.23	2.11	8.39	.3424	.0654	-.0551	-.0031	-.0017	-.0155
62	37	510.23	4.18	8.34	.3399	.0651	-.0519	-.0058	-.0029	-.0278
62	36	510.23	6.23	8.31	.3378	.0653	-.0470	-.0085	-.0045	-.0394
62	35	510.23	8.28	8.28	.3339	.0648	-.0406	-.0115	-.0064	-.0545
62	34	510.58	12.32	8.22	.3348	.0650	-.0347	-.0165	-.0102	-.0873
62	33	509.87	16.37	8.18	.3418	.0661	-.0345	-.0218	-.0139	-.1268
62	32	510.23	20.45	8.18	.3483	.0667	-.0380	-.0269	-.0162	-.1716
62	31	510.05	24.50	8.17	.3545	.0684	-.0419	-.0315	-.0150	-.2226
62	40	510.23	00	12.61	.5157	.1312	-.0876	-.0005	-.0002	-.0035
62	41	510.23	2.09	12.59	.5117	.1301	-.0856	-.0038	-.0012	-.0184
62	42	510.05	4.19	12.57	.5075	.1290	-.0820	-.0072	-.0022	-.0329
62	43	510.05	6.26	12.51	.5038	.1275	-.0768	-.0107	-.0037	-.0483
62	44	510.05	8.33	12.47	.4990	.1264	-.0697	-.0141	-.0055	-.0642
62	45	510.40	12.42	12.42	.4953	.1259	-.0593	-.0211	-.0087	-.1005
62	46	510.05	16.48	12.35	.4942	.1248	-.0517	-.0289	-.0096	-.1458
62	47	510.23	20.55	12.35	.4961	.1254	-.0519	-.0326	-.0115	-.1912
62	48	510.76	25.24	12.66	.5167	.1336	-.0676	-.0380	-.0093	-.2490
62	56	510.40	00	16.76	.6751	.2188	-.1189	-.0005	-.0001	-.0029
62	54	510.05	4.20	16.78	.6712	.2175	-.1135	-.0082	-.0007	-.0400
62	53	510.05	6.28	16.74	.6698	.2170	-.1117	-.0115	-.0001	-.0608
62	52	510.40	8.36	16.70	.6660	.2154	-.1063	-.0151	-.0007	-.0800
62	51	509.69	12.50	16.62	.6541	.2115	-.0896	-.0233	-.0050	-.1188
62	50	509.87	16.60	16.60	.6453	.2086	-.0772	-.0297	-.0030	-.1706
62	49	509.69	20.72	16.57	.6402	.2072	-.0732	-.0367	-.0050	-.2148
62	57	509.87	00	20.95	.8127	.3250	-.1482	-.0004	.0002	-.0023
62	58	509.69	2.11	20.93	.8101	.3238	-.1497	-.0037	.0027	-.0280
62	59	509.69	4.17	20.92	.8101	.3237	-.1486	-.0077	.0032	-.0502
62	60	510.05	6.29	20.92	.8062	.3226	-.1450	-.0114	.0035	-.0729
62	61	511.11	8.37	20.87	.7999	.3193	-.1381	-.0154	.0038	-.0948
62	62	511.11	12.56	20.89	.7934	.3183	-.1219	-.0246	.0002	-.1370
62	63	507.92	16.66	20.82	.7716	.3093	-.1061	-.0308	.0020	-.1859
62	64	510.23	20.66	20.66	.7597	.3029	-.0966	-.0372	.0011	-.2305
62	70	510.40	00	25.17	.9418	.4558	-.1887	-.0001	.0005	-.0026
62	69	510.23	2.12	25.21	.9395	.4552	-.1853	-.0040	.0036	-.0308
62	68	510.05	4.21	25.19	.9376	.4542	-.1835	-.0077	.0047	-.0555
62	67	510.05	6.33	25.15	.9312	.4508	-.1783	-.0112	.0060	-.0788
62	66	510.05	8.39	25.10	.9248	.4467	-.1727	-.0149	.0069	-.1023
62	65	510.23	12.60	25.12	.9078	.4399	-.1539	-.0226	.0084	-.1516

TABLE IV - Continued
 AERODYNAMIC CHARACTERISTICS IN SIDESLIP FOR VARIOUS ANGLES OF ATTACK.
 STABILITY AXES: M = 2.01

Run	Pt.	q	β , deg	α , deg	C_L	C_D	C_m	C_{Ls}	C_{nW}	C_Y
63	23	510.23	-0.1	0.0	-0.0044	0.184	-0.0069	0.0000	-0.0004	0.0003
63	22	510.23	.99	0.0	-0.0043	0.184	-0.0065	-0.0012	0.0036	-0.0115
63	21	510.23	1.99	0.0	-0.0040	0.185	-0.0062	-0.0024	0.0078	-0.0241
63	20	510.23	3.97	0.0	-0.0038	0.187	-0.0058	-0.0049	0.0158	-0.0487
63	19	510.23	5.99	0.0	-0.0042	0.186	-0.0031	-0.0078	0.0244	-0.0761
63	18	510.05	8.01	0.0	-0.0063	0.187	0.0009	-0.0108	0.0331	-0.1036
63	17	510.23	12.02	-0.2	-0.0132	0.192	0.0158	-0.0175	0.0506	-0.1676
63	16	510.05	16.02	0.3	-0.0061	0.190	0.0269	-0.0251	0.0660	-0.2372
63	15	510.23	20.06	0.0	0.0011	0.182	0.0425	-0.0335	0.0839	-0.3175
63	14	509.69	24.13	0.0	0.0050	0.180	0.0564	-0.0400	0.1011	-0.3978
63	13	509.69	28.14	0.0	0.0108	0.174	0.0692	-0.0448	0.1181	-0.4778
63	24	510.23	-0.1	4.14	0.1927	0.0328	-0.0677	-0.0002	0.0005	-0.0029
63	25	510.23	2.05	4.11	0.1852	0.0326	-0.0650	-0.0029	0.0074	-0.0263
63	26	510.40	4.08	4.08	0.1825	0.0322	-0.0631	-0.0054	0.0152	-0.0522
63	27	510.23	8.09	4.03	0.1789	0.0318	-0.0559	-0.0104	0.0319	-0.1084
63	28	509.87	12.15	4.05	0.1749	0.0319	-0.0417	-0.0166	0.0487	-0.1740
63	29	509.87	16.10	4.02	0.1783	0.0318	-0.0283	-0.0233	0.0633	-0.2417
63	30	509.87	20.12	4.07	0.1867	0.0322	-0.0157	-0.0305	0.0790	-0.3160
63	31	510.76	24.25	4.08	0.1930	0.0324	-0.0028	-0.0366	0.0967	-0.3974
63	39	509.69	-0.1	8.37	0.3885	0.0770	-0.1217	-0.0001	0.0002	-0.0021
63	38	510.76	2.09	8.34	0.3866	0.0771	-0.1207	-0.0024	0.0070	-0.0280
63	37	509.52	4.16	8.31	0.3827	0.0759	-0.1178	-0.0047	0.0144	-0.0542
63	36	510.58	8.20	8.20	0.3790	0.0750	-0.1096	-0.0095	0.0307	-0.1145
63	35	510.23	12.21	8.15	0.3764	0.0746	-0.0979	-0.0153	0.0460	-0.1781
63	34	510.23	16.23	8.11	0.3744	0.0737	-0.0826	-0.0218	0.0592	-0.2449
63	33	509.87	20.28	8.07	0.3703	0.0717	-0.0680	-0.0287	0.0740	-0.3175
63	32	510.40	24.29	8.09	0.3704	0.0722	-0.0567	-0.0343	0.0906	-0.3947
63	40	510.05	-0.2	12.56	0.5676	0.1484	-0.1738	-0.0003	0.0002	-0.0022
63	41	510.05	2.06	12.53	0.5644	0.1465	-0.1723	-0.0028	0.0067	-0.0297
63	42	510.05	4.15	12.52	0.5607	0.1457	-0.1687	-0.0054	0.0137	-0.0587
63	43	509.87	8.25	12.41	0.5535	0.1430	-0.1586	-0.0101	0.0283	-0.1196
63	44	510.05	12.34	12.34	0.5498	0.1410	-0.1461	-0.0160	0.0414	-0.1817
63	45	510.40	16.36	12.25	0.5419	0.1382	-0.1265	-0.0219	0.0539	-0.2488
63	46	510.76	20.41	12.26	0.5369	0.1365	-0.1135	-0.0276	0.0689	-0.3223
63	47	510.40	25.04	12.55	0.5462	0.1412	-0.1085	-0.0334	0.0875	-0.4085
63	55	510.40	0.0	16.70	0.7355	0.2430	-0.2311	-0.0003	-0.0002	0.0005
63	54	510.40	2.08	16.71	0.7350	0.2427	-0.2301	-0.0030	0.0059	-0.0282
63	53	510.40	4.18	16.71	0.7332	0.2423	-0.2261	-0.0054	0.0127	-0.0607
63	52	510.40	8.28	16.63	0.7279	0.2389	-0.2164	-0.0106	0.0252	-0.1209
63	51	510.76	12.43	16.53	0.7195	0.2348	-0.2022	-0.0154	0.0362	-0.1858
63	50	510.58	16.50	16.50	0.7073	0.2302	-0.1815	-0.0206	0.0482	-0.2545
63	49	509.87	20.58	16.45	0.6916	0.2243	-0.1613	-0.0264	0.0622	-0.3244
63	48	510.05	22.63	16.44	0.6886	0.2235	-0.1540	-0.0289	0.0707	-0.3618
63	56	510.05	0.0	20.86	0.8913	0.3616	-0.2902	-0.0002	-0.0007	0.0014
63	57	510.23	2.10	20.84	0.8900	0.3605	-0.2899	-0.0031	0.0057	-0.0316
63	58	510.76	4.19	20.82	0.8880	0.3592	-0.2865	-0.0060	0.0113	-0.0632
63	59	509.87	8.33	20.79	0.8773	0.3540	-0.2762	-0.0113	0.0197	-0.1201
63	60	510.58	12.48	20.76	0.8664	0.3491	-0.2598	-0.0153	0.0309	-0.1868
63	61	509.69	16.55	20.76	0.8517	0.3439	-0.2393	-0.0192	0.0423	-0.2536
63	62	510.76	20.56	20.56	0.8308	0.3323	-0.2135	-0.0234	0.0565	-0.3229
63	68	510.40	0.0	25.04	1.0304	0.5039	-0.3575	-0.0005	-0.0011	0.0024
63	67	510.58	2.11	25.10	1.0298	0.5040	-0.3542	-0.0043	0.0033	-0.0281
63	66	510.40	4.19	25.09	1.0259	0.5020	-0.3522	-0.0071	0.0071	-0.0572
63	65	509.87	8.31	25.00	1.0160	0.4942	-0.3422	-0.0117	0.0152	-0.1148
63	64	509.34	12.54	25.01	0.9991	0.4868	-0.3215	-0.0152	0.0250	-0.1805
63	63	510.93	14.56	24.93	0.9891	0.4805	-0.3086	-0.0164	0.0308	-0.2153

TABLE IV - Continued
 AERODYNAMIC CHARACTERISTICS IN SIDESLIP FOR VARIOUS ANGLES OF ATTACK.
 STABILITY AXES: M = 2.01

Run	Pt.	q	β , deg	α , deg	C_L	C_D	C_m	$C_{l,s}$	$C_{n,w}$	C_y
64	21	512.88	.00	.00	-.0081	.0295	.0129	.0002	-.0008	.0006
64	20	512.70	2.01	.00	-.0072	.0296	.0130	-.0030	.0072	-.0247
64	19	512.88	3.98	.00	-.0079	.0293	.0136	-.0061	.0150	-.0490
64	18	512.35	5.98	.00	-.0067	.0291	.0142	-.0095	.0234	-.0754
64	17	512.35	8.02	.00	-.0067	.0290	.0147	-.0132	.0322	-.1045
64	16	510.93	12.03	.00	-.0014	.0285	.0118	-.0211	.0495	-.1667
64	15	511.64	16.03	.00	.0226	.0277	-.0101	-.0306	.0577	-.2422
64	14	512.70	20.04	.00	.0511	.0268	-.0335	-.0408	.0905	-.3301
64	13	511.64	22.09	.00	.0651	.0271	-.0441	-.0454	.1012	-.3749
64	22 ¹	512.70	.00	4.18	.1750	.0410	-.0283	.0000	-.0001	-.0012
64	23	512.35	2.06	4.13	.1729	.0408	-.0293	-.0035	.0074	-.0268
64	24	512.35	4.09	4.09	.1697	.0401	-.0308	-.0067	.0151	-.0525
64	25	512.53	8.10	4.04	.1730	.0397	-.0378	-.0133	.0328	-.1106
64	26	512.53	12.14	4.04	.1848	.0402	-.0494	-.0211	.0519	-.1794
64	27	512.00	16.07	4.02	.2040	.0413	-.0657	-.0297	.0714	-.2548
64	28	512.35	20.09	4.06	.2280	.0416	-.0795	-.0381	.0919	-.3371
64	35	512.70	.00	8.39	.3636	.0814	-.0873	.0000	-.0002	-.0003
64	34	512.70	2.10	8.36	.3627	.0811	-.0884	-.0033	.0074	-.0282
64	33	512.17	4.17	8.31	.3625	.0800	-.0909	-.0065	.0154	-.0555
64	32	512.53	8.22	8.22	.3703	.0805	-.1033	-.0135	.0343	-.1187
64	31	512.53	12.19	8.14	.3811	.0814	-.1126	-.0209	.0542	-.1899
64	30	512.35	16.20	8.10	.3892	.0820	-.1124	-.0282	.0719	-.2633
64	29	512.53	20.22	8.08	.3992	.0818	-.1178	-.0355	.0914	-.3448
64	36	512.53	.00	12.56	.5538	.1512	-.1563	-.0003	-.0003	-.0004
64	37	512.70	2.09	12.54	.5536	.1506	-.1577	-.0039	.0079	-.0308
64	38	512.53	4.17	12.52	.5528	.1506	-.1594	-.0074	.0164	-.0619
64	39	512.53	8.27	12.39	.5556	.1486	-.1629	-.0143	.0348	-.1272
64	40	512.53	12.31	12.31	.5605	.1486	-.1633	-.0215	.0542	-.1989
64	41	512.53	16.33	12.23	.5608	.1473	-.1558	-.0279	.0731	-.2759
64	47	512.53	.00	16.71	.7348	.2477	-.2240	-.0002	-.0005	.0005
64	46	512.70	2.08	16.71	.7341	.2473	-.2241	-.0035	.0082	-.0322
64	45	512.53	4.18	16.71	.7322	.2466	-.2217	-.0067	.0170	-.0659
64	44	512.53	8.32	16.62	.7279	.2433	-.2184	-.0133	.0335	-.1323
64	43	512.35	12.41	16.51	.7263	.2401	-.2159	-.0193	.0523	-.2080
64	42	512.35	16.48	16.48	.7153	.2372	-.1973	-.0249	.0696	-.2842
64	48	512.53	.00	20.88	.8851	.3634	-.2753	-.0003	-.0008	.0023
64	49	513.24	2.10	20.86	.8842	.3622	-.2742	-.0032	.0075	-.0336
64	50	511.64	4.19	20.84	.8816	.3611	-.2741	-.0064	.0143	-.0655
64	51	512.70	8.29	20.80	.8822	.3584	-.2765	-.0124	.0315	-.1363
64	52	513.06	12.49	20.77	.8699	.3542	-.2585	-.0171	.0481	-.2104
64	53	512.70	16.57	20.72	.8554	.3478	-.2355	-.0214	.0628	-.2830
64	58	512.53	.00	25.09	1.0103	.4989	-.3149	-.0008	-.0010	.0031
64	57	512.53	2.11	25.12	1.0093	.4986	-.3121	-.0041	.0057	-.0305
64	56	512.53	4.20	25.13	1.0074	.4974	-.3112	-.0070	.0111	-.0606
64	55	512.70	8.32	25.02	1.0017	.4904	-.3078	-.0114	.0247	-.1279
64	54	512.35	12.55	25.03	.9884	.4834	-.2926	-.0152	.0392	-.1996

TABLE IV - Concluded
 AERODYNAMIC CHARACTERISTICS IN SIDESLIP FOR VARIOUS ANGLES OF ATTACK.
 STABILITY AXES; $M = 2.01$

Run	Pt.	q	β , deg	α , deg	C_L	C_D	C_m	$C_{l,s}$	$C_{n,w}$	C_y
65	21	510.40	.00	.00	.0112	.0092	-.0048	.0000	-.0001	-.0011
65	20	510.23	2.01	.00	.0131	.0059	-.0051	.0000	-.0027	-.0041
65	19	510.58	4.01	.00	.0136	.0063	-.0051	.0000	-.0050	-.0090
65	18	510.05	6.05	.00	.0141	.0063	-.0050	.0000	-.0073	-.0140
65	17	510.23	8.09	.00	.0163	.0064	-.0054	.0000	-.0093	-.0217
65	16	510.23	12.14	.00	.0150	.0066	-.0050	.0000	-.0136	-.0444
65	15	510.05	16.19	.00	.0150	.0066	-.0045	.0000	-.0148	-.0877
65	14	510.05	20.25	.00	.0138	.0064	-.0037	.0000	-.0156	-.1347
65	13	510.23	24.37	.00	.0124	.0068	-.0043	.0000	-.0155	-.1628
65	12	510.05	28.41	.05	.0129	.0077	-.0037	.0000	-.0144	-.2320
65	22	510.23	.00	4.02	.0205	.0079	.0099	.0000	-.0005	-.0009
65	23	510.58	2.01	4.03	.0183	.0080	.0096	-.0002	-.0028	-.0056
65	24	510.05	4.03	4.03	.0169	.0078	.0093	-.0004	-.0051	-.0101
65	25	510.23	6.05	4.04	.0169	.0082	.0093	-.0005	-.0072	-.0159
65	26	510.40	8.08	4.03	.0180	.0082	.0088	-.0007	-.0094	-.0226
65	27	510.58	12.17	4.05	.0198	.0081	.0086	-.0009	-.0132	-.0472
65	28	510.05	16.17	4.07	.0252	.0086	.0076	-.0010	-.0143	-.0881
65	29	510.40	20.25	4.10	.0290	.0092	.0068	-.0011	-.0153	-.1343
65	30	510.58	24.42	4.06	.0310	.0092	.0043	-.0011	-.0152	-.1838
65	39	510.93	.00	8.09	.0293	.0108	.0219	-.0001	-.0004	-.0011
65	38	509.69	2.01	8.08	.0292	.0108	.0215	-.0004	-.0027	-.0054
65	37	510.58	4.05	8.08	.0308	.0112	.0211	-.0007	-.0050	-.0116
65	36	510.40	6.05	8.10	.0323	.0113	.0213	-.0010	-.0071	-.0186
65	35	510.58	8.09	8.12	.0335	.0116	.0214	-.0014	-.0095	-.0264
65	34	510.23	12.13	8.10	.0434	.0131	.0184	-.0017	-.0123	-.0559
65	33	510.05	16.18	8.09	.0516	.0142	.0150	-.0019	-.0136	-.0956
65	32	511.11	20.27	8.10	.0573	.0150	.0131	-.0021	-.0147	-.1383
65	31	510.76	24.33	8.11	.0612	.0157	.0095	-.0021	-.0146	-.1852
65	40	510.40	.00	12.14	.0473	.0173	.0337	-.0001	-.0005	-.0003
65	41	510.05	2.02	12.14	.0491	.0176	.0327	-.0005	-.0023	-.0077
65	42	510.05	4.02	12.13	.0507	.0179	.0317	-.0009	-.0042	-.0160
65	43	510.05	6.06	12.12	.0531	.0183	.0312	-.0014	-.0064	-.0250
65	44	510.58	8.06	12.13	.0576	.0196	.0289	-.0016	-.0076	-.0372
65	45	510.40	12.14	12.14	.0669	.0216	.0255	-.0023	-.0105	-.0663
65	46	510.05	16.20	12.13	.0763	.0233	.0234	-.0026	-.0122	-.1041
65	47	510.58	20.28	12.18	.0827	.0247	.0200	-.0029	-.0135	-.1437
65	48	510.40	24.95	12.50	.0936	.0281	.0151	-.0029	-.0131	-.1968
65	56	510.58	.00	16.17	.0910	.0332	.0361	-.0001	-.0003	-.0005
65	55	510.76	2.01	16.21	.0915	.0334	.0361	-.0006	-.0020	-.0104
65	54	510.93	4.05	16.19	.0918	.0334	.0350	-.0011	-.0036	-.0217
65	53	510.58	6.06	16.19	.0933	.0344	.0340	-.0014	-.0050	-.0337
65	52	510.40	8.09	16.18	.0978	.0360	.0320	-.0017	-.0060	-.0478
65	51	510.40	12.16	16.18	.1056	.0378	.0301	-.0026	-.0089	-.0774
65	50	510.40	16.23	16.23	.1103	.0388	.0277	-.0031	-.0108	-.1117
65	49	510.40	20.33	16.25	.1171	.0413	.0232	-.0034	-.0118	-.1514
65	57	510.58	.00	20.22	.1323	.0556	.0382	.0000	-.0001	-.0007
65	58	510.40	2.03	20.23	.1322	.0555	.0382	-.0006	-.0015	-.0133
65	59	510.23	4.06	20.23	.1320	.0554	.0380	-.0010	-.0027	-.0272
65	60	510.40	6.07	20.23	.1342	.0571	.0375	-.0015	-.0039	-.0404
65	61	510.05	8.09	20.24	.1352	.0573	.0367	-.0019	-.0052	-.0540
65	62	510.05	12.17	20.27	.1406	.0597	.0330	-.0027	-.0074	-.0845
65	63	510.40	16.19	20.32	.1466	.0619	.0294	-.0034	-.0092	-.1189
65	64	511.11	20.17	20.23	.1503	.0632	.0253	-.0037	-.0100	-.1561
65	70	510.23	.00	24.32	.1702	.0847	.0387	-.0001	-.0003	-.0008
65	69	510.93	2.04	24.36	.1706	.0851	.0385	-.0006	-.0014	-.0143
65	68	510.40	4.05	24.37	.1701	.0848	.0383	-.0012	-.0026	-.0289
65	67	510.40	6.10	24.35	.1724	.0855	.0373	-.0016	-.0036	-.0437
65	66	510.58	8.11	24.33	.1728	.0856	.0365	-.0020	-.0045	-.0588
65	65	510.93	12.19	24.38	.1771	.0887	.0326	-.0028	-.0062	-.0903

TABLE V
AERODYNAMIC CHARACTERISTICS IN SIDESLIP FOR VARIOUS ANGLES OF ATTACK.
BODY AXES; M = 1.41

Run	PI	q	β ,deg	α ,deg	C _N	C _A	C _m	C _l	C _n	C _y
2	20	623.09	-2.02	4.00	.0063	.0062	-.0022	.0000	.0026	.0023
2	19	623.09	.00	4.00	.0066	.0062	-.0024	.0000	.0001	-.0009
2	18	623.30	2.02	4.00	.0068	.0065	-.0026	.0000	-.0025	-.0033
2	17	623.30	4.03	4.00	.0071	.0071	-.0029	.0000	-.0048	-.0065
2	16	623.30	6.04	4.00	.0062	.0074	-.0028	.0000	-.0068	-.0113
2	15	623.09	8.08	4.00	.0067	.0075	-.0032	.0000	-.0085	-.0176
2	14	623.30	10.09	4.00	.0073	.0074	-.0035	.0000	-.0101	-.0254
2	13	623.30	12.14	4.00	.0069	.0073	-.0031	.0000	-.0120	-.0354
2	12	623.30	14.14	4.00	.0077	.0072	-.0036	.0000	-.0143	-.0453
2	22	623.09	-2.01	4.02	.0147	.0084	.0107	.0000	.0019	.0026
2	23	623.09	-.01	4.03	.0133	.0087	.0106	.0000	-.0004	-.0008
2	24	623.30	2.01	4.03	.0102	.0092	.0109	.0000	-.0027	-.0038
2	25	623.09	4.02	4.02	.0118	.0105	.0099	.0000	-.0048	-.0082
2	26	623.30	6.05	4.04	.0116	.0094	.0093	.0000	-.0068	-.0121
2	27	623.09	8.09	4.03	.0125	.0090	.0086	.0000	-.0085	-.0191
2	28	623.09	10.11	4.06	.0127	.0097	.0093	.0000	-.0102	-.0272
2	29	623.09	12.14	4.07	.0140	.0092	.0082	.0000	-.0115	-.0361
2	30	623.30	14.14	4.05	.0152	.0084	.0083	.0000	-.0143	-.0467
2	39	623.09	-2.04	8.07	.0211	.0131	.0217	.0000	.0015	.0036
2	38	623.09	.00	8.05	.0199	.0130	.0215	.0000	-.0007	-.0001
2	37	623.09	2.03	8.08	.0212	.0134	.0211	.0000	-.0026	-.0044
2	36	623.09	4.03	8.08	.0212	.0134	.0206	.0000	-.0047	-.0101
2	35	623.09	6.06	8.07	.0223	.0135	.0200	.0000	-.0066	-.0151
2	34	623.52	8.07	8.07	.0220	.0188	.0197	.0000	-.0084	-.0216
2	33	623.09	10.25	7.90	.0239	.0190	.0189	.0000	-.0103	-.0312
2	32	622.01	12.12	8.09	.0258	.0193	.0196	.0000	-.0126	-.0386
2	31	623.95	14.15	8.08	.0290	.0203	.0186	.0000	-.0139	-.0513
2	40	623.74	-2.01	12.10	.0382	.0138	.0307	.0000	.0013	.0048
2	41	623.30	-.02	12.12	.0371	.0138	.0308	.0000	-.0005	-.0010
2	42	623.09	1.99	12.10	.0373	.0138	.0303	.0000	-.0025	-.0062
2	43	623.09	4.02	12.14	.0371	.0138	.0302	.0000	-.0044	-.0122
2	44	623.30	6.06	12.12	.0391	.0140	.0299	.0000	-.0064	-.0188
2	45	623.09	8.09	12.12	.0392	.0140	.0309	.0000	-.0086	-.0263
2	46	623.09	10.10	12.11	.0424	.0141	.0298	.0000	-.0103	-.0348
4	18	622.66	-2.04	8.07	.0224	.0074	.0213	.0000	.0015	.0036
4	17	622.66	.00	8.06	.0213	.0078	.0213	.0000	-.0007	-.0001
4	16	622.87	2.03	8.08	.0212	.0077	.0210	.0000	-.0028	-.0043
4	15	622.66	4.05	8.08	.0225	.0075	.0202	.0000	-.0047	-.0094
4	14	622.66	6.06	8.07	.0235	.0077	.0193	.0000	-.0067	-.0144
4	13	622.22	8.07	8.07	.0246	.0073	.0186	.0000	-.0085	-.0209
4	12	621.14	10.25	7.90	.0251	.0069	.0179	.0000	-.0104	-.0297
4	11	623.09	12.12	8.09	.0271	.0070	.0189	.0000	-.0127	-.0385
4	10	621.14	14.15	8.08	.0305	.0066	.0180	.0000	-.0139	-.0509
4	19	622.87	-2.01	12.09	.0395	.0073	.0304	.0000	.0014	.0048
4	20	622.44	.00	12.11	.0385	.0073	.0304	.0000	-.0007	-.0002
4	21	622.44	2.01	12.09	.0387	.0072	.0301	.0000	-.0026	-.0062
4	23	622.66	4.04	12.12	.0385	.0072	.0300	.0000	-.0047	-.0114
4	24	622.66	6.06	12.12	.0404	.0070	.0295	.0000	-.0065	-.0180
4	25	622.66	8.08	12.11	.0405	.0070	.0303	.0000	-.0087	-.0256
4	26	622.66	10.10	12.11	.0437	.0067	.0291	.0000	-.0102	-.0349

TABLE V - Continued
 AERODYNAMIC CHARACTERISTICS IN SIDESLIP FOR VARIOUS ANGLES OF ATTACK.
 BODY AXES: M = 1.41

Run	Pt.	q	β , deg	α , deg	C_N	C_A	C_m	C_l	C_n	C_y
5	26	622.01	-2.04	+0.0	-.0312	.0186	.0122	.0017	.0024	.0061
5	25	622.22	-1.01	+0.0	-.0326	.0186	.0118	.0004	.0012	.0026
5	24	622.01	-.01	+0.0	-.0327	.0186	.0115	-.0008	.0000	-.0010
5	23	622.01	1.01	+0.0	-.0328	.0186	.0117	-.0021	-.0013	-.0036
5	22	622.22	2.03	+0.0	-.0342	.0185	.0125	-.0034	-.0025	-.0071
5	21	621.79	3.04	+0.0	-.0342	.0186	.0134	-.0045	-.0037	-.0106
5	20	622.44	4.04	+0.0	-.0354	.0186	.0154	-.0057	-.0048	-.0142
5	19	620.93	6.07	-0.1	-.0382	.0190	.0197	-.0080	-.0069	-.0214
5	18	622.44	8.10	+0.0	-.0418	.0188	.0252	-.0102	-.0087	-.0298
5	17	622.01	10.12	+0.0	-.0442	.0192	.0297	-.0124	-.0105	-.0407
5	16	622.44	12.17	+0.0	-.0454	.0188	.0318	-.0146	-.0121	-.0523
5	15	622.01	14.19	+0.0	-.0429	.0186	.0304	-.0166	-.0139	-.0654
5	27	622.66	-1.38	4.63	.2709	.0193	-.0348	.0012	.0008	.0047
5	28	622.01	.00	4.35	.2482	.0188	-.0310	-.0006	-.0003	-.0004
5	29	622.44	2.13	4.26	.2358	.0193	-.0273	-.0039	-.0019	-.0096
5	30	622.44	4.18	4.18	.2284	.0193	-.0233	-.0070	-.0037	-.0183
5	31	622.44	6.20	4.14	.2229	.0190	-.0186	-.0094	-.0056	-.0275
5	32	622.87	8.22	4.10	.2189	.0194	-.0140	-.0120	-.0076	-.0369
5	33	622.22	10.24	4.11	.2166	.0191	-.0105	-.0144	-.0098	-.0475
5	34	622.22	12.29	4.10	.2134	.0189	-.0078	-.0165	-.0121	-.0595
5	35	622.22	14.27	4.09	.2123	.0184	-.0073	-.0185	-.0149	-.0713
5	44	622.22	-2.17	8.65	.5040	.0186	-.0739	.0017	.0011	.0107
5	43	622.44	.00	8.67	.4984	.0187	-.0728	-.0006	-.0005	.0007
5	42	622.22	2.16	8.65	.4933	.0190	-.0715	-.0033	-.0020	-.0099
5	41	622.44	4.28	8.58	.4924	.0190	-.0703	-.0055	-.0036	-.0198
5	40	622.22	6.35	8.46	.4859	.0189	-.0670	-.0081	-.0056	-.0307
5	39	622.22	8.40	8.40	.4798	.0188	-.0625	-.0104	-.0079	-.0413
5	38	622.44	10.56	8.17	.4622	.0188	-.0551	-.0127	-.0105	-.0536
5	37	622.66	12.46	8.32	.4679	.0179	-.0522	-.0148	-.0133	-.0654
5	36	622.44	14.45	8.26	.4629	.0178	-.0493	-.0164	-.0149	-.0829
5	45	622.22	-4.32	12.95	.7430	.0168	-.1143	.0024	.0026	.0246
5	46	622.44	-2.18	12.98	.7382	.0169	-.1139	.0008	.0007	.0135
5	47	622.22	-.02	13.01	.7343	.0171	-.1135	-.0006	-.0005	.0011
5	48	622.22	2.16	12.97	.7301	.0170	-.1128	-.0021	-.0018	-.0110
5	49	622.22	4.31	12.93	.7267	.0168	-.1113	-.0038	-.0040	-.0219
5	50	622.22	6.43	12.84	.7227	.0171	-.1084	-.0055	-.0061	-.0336
5	51	622.22	8.51	12.74	.7165	.0170	-.1035	-.0072	-.0084	-.0458
5	52	623.09	10.57	12.67	.7080	.0163	-.0985	-.0099	-.0102	-.0602
6	28	622.87	-3.03	-.01	-.0081	.0182	-.0053	-.0044	.0034	.0103
6	27	622.44	-2.04	.00	-.0086	.0182	-.0040	-.0032	.0023	.0067
6	26	622.87	-1.01	.00	-.0092	.0183	-.0033	-.0020	.0012	.0033
6	25	623.09	.01	.00	-.0097	.0184	-.0030	-.0009	.0001	-.0001
6	24	622.66	1.01	.00	-.0090	.0183	-.0034	.0002	-.0010	-.0035
6	23	623.09	2.03	.01	-.0097	.0182	-.0040	.0013	-.0022	-.0068
6	22	622.66	3.03	.01	-.0090	.0186	-.0054	.0024	-.0032	-.0104
6	21	622.87	4.04	.01	-.0085	.0187	-.0073	.0036	-.0043	-.0138
6	20	622.66	6.07	.00	-.0088	.0189	-.0115	.0060	-.0063	-.0215
6	19	623.09	8.10	.01	-.0064	.0193	-.0173	.0083	-.0081	-.0305
6	18	622.44	10.12	.02	-.0063	.0192	-.0217	.0105	-.0100	-.0412
6	17	622.44	12.17	.00	-.0101	.0194	-.0238	.0128	-.0120	-.0526
6	16	622.44	14.19	.00	-.0163	.0190	-.0235	.0152	-.0139	-.0669
6	29	622.66	-2.14	4.29	.2762	.0178	-.0475	-.0019	.0023	.0058
6	30	622.66	.00	4.35	.2703	.0178	-.0459	.0002	-.0006	.0004
6	31	622.66	2.14	4.28	.2639	.0180	-.0458	.0017	-.0031	-.0048
6	32	622.87	4.18	4.18	.2581	.0185	-.0465	.0031	-.0056	-.0097
6	33	623.09	6.20	4.12	.2554	.0189	-.0499	.0048	-.0077	-.0166
6	34	622.66	8.21	4.10	.2554	.0190	-.0550	.0068	-.0095	-.0251
6	35	623.52	10.25	4.09	.2539	.0185	-.0583	.0088	-.0109	-.0351
6	36	623.52	12.25	4.08	.2471	.0188	-.0593	.0109	-.0120	-.0471
6	37	622.22	14.23	4.07	.2379	.0186	-.0578	.0133	-.0129	-.0617
6	46	623.30	-2.16	8.68	.5329	.0169	-.0876	-.0015	.0021	.0061
6	45	623.74	-.02	8.70	.5278	.0169	-.0863	.0003	-.0009	.0015
6	44	623.52	2.18	8.67	.5260	.0173	-.0872	.0017	-.0038	-.0023
6	43	623.30	4.30	8.58	.5225	.0175	-.0884	.0029	-.0063	-.0077
6	42	623.52	6.37	8.49	.5198	.0176	-.0914	.0046	-.0086	-.0132
6	41	623.52	8.38	8.41	.5165	.0175	-.0953	.0064	-.0102	-.0218
6	40	622.87	10.53	8.15	.4968	.0177	-.0951	.0085	-.0114	-.0329
6	39	623.30	12.40	8.28	.5002	.0175	-.0955	.0105	-.0119	-.0446
6	38	623.30	14.39	8.22	.4863	.0173	-.0928	.0128	-.0116	-.0595
6	54	618.12	-.02	13.05	.7720	.0157	-.1183	.0004	-.0013	.0033
6	49	623.09	2.14	13.02	.7684	.0158	-.1200	.0016	-.0042	-.0012
6	50	622.87	4.33	12.97	.7664	.0160	-.1229	.0031	-.0068	-.0062
6	51	623.09	6.44	12.87	.7631	.0162	-.1259	.0044	-.0089	-.0136
6	52	623.09	8.54	12.78	.7589	.0164	-.1292	.0058	-.0112	-.0213
6	53	623.09	10.55	12.64	.7497	.0159	-.1315	.0075	-.0125	-.0301

TABLE V - Continued
AERODYNAMIC CHARACTERISTICS IN SIDESLIP FOR VARIOUS ANGLES OF ATTACK.

BODY AXES: M = 1.41

Run	Pt.	q	β , deg	α , deg	C_N	C_A	C_m	C_l	C_n	C_y
7	27	623.74	-4.04	4.00	-.0155	.0163	.0029	-.0013	.0041	.0071
7	26	623.52	-2.01	4.00	-.0164	.0156	.0030	-.0014	.0021	.0031
7	25	623.52	-1.01	4.00	-.0163	.0156	.0031	-.0015	.0011	.0018
7	24	623.52	.00	4.00	-.0160	.0160	.0032	-.0015	.0000	-.0002
7	23	623.30	1.02	4.00	-.0158	.0156	.0031	-.0016	-.0010	-.0022
7	22	623.30	2.01	4.00	-.0157	.0158	.0031	-.0016	-.0022	-.0034
7	21	623.30	4.02	4.00	-.0152	.0160	.0031	-.0017	-.0041	-.0075
7	20	623.52	6.06	4.00	-.0161	.0164	.0032	-.0017	-.0058	-.0131
7	19	623.30	8.08	4.00	-.0169	.0162	.0035	-.0017	-.0074	-.0186
7	18	623.09	10.09	4.00	-.0163	.0163	.0031	-.0017	-.0089	-.0265
7	17	623.09	12.13	4.00	-.0156	.0165	.0028	-.0016	-.0105	-.0358
7	16	622.44	14.15	4.00	-.0204	.0160	.0030	-.0013	-.0127	-.0472
7	29	623.30	-4.18	4.18	.2683	.0163	-.0415	-.0008	.0037	.0075
7	30	623.30	-2.14	4.28	.2638	.0156	-.0398	-.0008	.0017	.0037
7	31	623.30	-.01	4.34	.2580	.0158	-.0389	-.0010	-.0003	-.0004
7	32	623.30	2.13	4.27	.2496	.0163	-.0365	-.0019	-.0021	-.0043
7	33	623.52	4.18	4.18	.2454	.0165	-.0356	-.0025	-.0040	-.0086
7	34	623.52	6.18	4.11	.2432	.0167	-.0354	-.0028	-.0057	-.0141
7	35	623.30	8.19	4.10	.2422	.0168	-.0356	-.0029	-.0074	-.0197
7	36	623.09	10.22	4.08	.2404	.0171	-.0350	-.0032	-.0090	-.0276
7	37	623.30	12.23	4.08	.2367	.0169	-.0339	-.0034	-.0107	-.0374
7	38	623.30	14.22	4.07	.2327	.0167	-.0321	-.0033	-.0127	-.0486
7	48	623.74	-4.30	8.58	.5226	.0153	-.0844	-.0012	.0038	.0095
7	47	623.52	-2.18	8.66	.5168	.0154	-.0814	-.0010	.0017	.0040
7	46	623.52	-.02	8.69	.5120	.0154	-.0803	-.0009	-.0004	-.0001
7	45	623.74	2.18	8.67	.5099	.0155	-.0801	-.0012	-.0024	-.0040
7	44	623.74	4.29	8.57	.5086	.0159	-.0810	-.0013	-.0044	-.0087
7	43	623.52	6.34	8.48	.5079	.0162	-.0810	-.0017	-.0062	-.0143
7	42	623.52	8.39	8.39	.5041	.0163	-.0793	-.0020	-.0079	-.0207
7	41	623.74	10.54	8.13	.4885	.0161	-.0752	-.0023	-.0096	-.0295
7	40	623.52	12.41	8.29	.4926	.0159	-.0737	-.0023	-.0114	-.0393
7	39	623.52	14.39	8.22	.4831	.0160	-.0708	-.0021	-.0122	-.0533
7	49	623.09	-4.35	12.95	.7638	.0138	-.1231	-.0013	.0046	.0094
7	50	623.52	-2.16	13.00	.7599	.0142	-.1210	-.0011	.0019	.0051
7	51	623.52	.00	13.04	.7556	.0142	-.1196	-.0010	-.0004	.0003
7	52	623.52	2.16	12.99	.7538	.0142	-.1199	-.0009	-.0029	-.0043
7	53	623.52	4.30	12.96	.7525	.0146	-.1215	-.0007	-.0052	-.0092
7	54	623.74	6.43	12.86	.7505	.0145	-.1208	-.0007	-.0073	-.0151
7	55	623.74	8.52	12.86	.7428	.0144	-.1166	-.0008	-.0092	-.0229
7	56	623.52	10.56	12.66	.7334	.0145	-.1126	-.0014	-.0106	-.0309
8	26	624.82	-3.94	4.05	-.0193	.0308	.0160	.0041	-.0286	.0637
8	25	624.39	-1.98	4.01	-.0206	.0317	.0152	.0013	-.0146	.0327
8	24	623.52	-.99	4.00	-.0225	.0317	.0155	-.0001	-.0078	.0174
8	23	623.09	-.01	4.00	-.0219	.0309	.0151	-.0014	-.0009	.0018
8	22	624.82	.99	4.00	-.0226	.0310	.0153	-.0027	.0060	-.0130
8	21	623.95	1.97	4.00	-.0219	.0312	.0157	-.0041	.0127	-.0280
8	20	623.95	3.94	4.00	-.0229	.0306	.0166	-.0069	.0272	-.0601
8	19	625.25	5.91	4.00	-.0227	.0303	.0164	-.0095	.0416	-.0928
8	18	625.25	7.90	4.01	-.0225	.0296	.0157	-.0121	.0566	-.1279
8	17	625.03	9.88	4.00	-.0224	.0287	.0148	-.0145	.0714	-.1638
8	16	624.39	11.87	4.00	-.0237	.0280	.0141	-.0169	.0849	-.1989
8	27	624.82	-4.15	4.15	.2660	.0299	-.0314	.0047	-.0286	.0631
8	28	624.82	-2.14	4.28	.2607	.0299	-.0295	.0017	-.0131	.0287
8	29	624.39	-.01	4.36	.2551	.0302	-.0287	-.0015	-.0019	-.0039
8	30	624.39	2.12	4.26	.2462	.0303	-.0264	-.0051	.0161	-.0353
8	31	624.39	4.13	4.13	.2420	.0302	-.0256	-.0083	.0302	-.0666
8	32	624.60	6.08	4.05	.2386	.0301	-.0255	-.0112	.0444	-.0992
8	33	624.39	8.06	4.02	.2391	.0293	-.0266	-.0140	.0593	-.1340
8	34	624.17	10.04	4.01	.2396	.0288	-.0270	-.0168	.0738	-.1693
8	35	624.39	12.00	4.00	.2353	.0275	-.0259	-.0193	.0876	-.2048
8	36	624.17	13.95	3.99	.2304	.0274	-.0236	-.0213	.0980	-.2367
8	46	624.39	-4.29	8.56	.5183	.0282	-.0750	.0041	-.0272	.0624
8	45	624.39	-2.18	8.67	.5119	.0291	-.0717	.0015	-.0129	.0299
8	44	624.39	-.02	8.69	.5072	.0293	-.0705	-.0012	.0014	-.0027
8	43	624.60	2.18	8.66	.5049	.0294	-.0705	-.0041	.0153	-.0346
8	42	625.25	4.29	8.55	.5040	.0289	-.0721	-.0072	.0292	-.0658
8	41	624.17	6.30	8.42	.5033	.0283	-.0730	-.0103	.0440	-.0998
8	40	624.17	8.30	8.30	.4998	.0280	-.0723	-.0133	.0585	-.1344
8	39	624.17	10.40	8.01	.4846	.0274	-.0690	-.0163	.0736	-.1724
8	38	624.39	12.23	8.16	.4899	.0267	-.0681	-.0182	.0839	-.2019
8	37	624.17	14.17	8.09	.4811	.0263	-.0657	-.0202	.0982	-.2401
8	47	624.17	-4.32	12.96	.7585	.0269	-.1140	.0036	-.0250	.0606
8	48	624.60	-2.16	13.00	.7527	.0273	-.1109	.0010	-.0116	.0286
8	49	624.82	.00	13.05	.7501	.0274	-.1095	-.0014	.0015	-.0031
8	50	624.60	2.16	13.00	.7479	.0276	-.1105	-.0041	.0147	-.0346
8	51	624.39	4.31	12.93	.7474	.0267	-.1130	-.0066	.0280	-.0667
8	52	624.39	6.38	12.82	.7457	.0255	-.1136	-.0091	.0405	-.0979
8	53	624.82	8.47	12.68	.7402	.0252	-.1114	-.0118	.0532	-.1297
8	54	624.60	10.47	12.55	.7322	.0243	-.1081	-.0151	.0670	-.1641

TABLE V - Continued
 AERODYNAMIC CHARACTERISTICS IN SIDESLIP FOR VARIOUS ANGLES OF ATTACK.
 BODY AXES; M = 1.41

Run	Pt.	q	β , deg	α , deg	C_N	C_A	C_m	C_l	C_n	C_Y
9	26	625.25	-3.95	-0.01	-0.0378	0.0343	0.0461	0.0053	-0.0299	0.0660
9	25	625.90	-1.98	0.01	-0.0383	0.0343	0.0471	0.0018	-0.0150	0.0335
9	24	625.25	-0.99	0.00	-0.0400	0.0340	0.0475	0.0002	-0.0077	0.0174
9	23	625.03	0.00	0.00	-0.0393	0.0340	0.0471	-0.0013	-0.0010	0.0025
9	22	625.03	0.99	0.00	-0.0396	0.0337	0.0473	-0.0029	0.0059	-0.0131
9	21	625.25	1.98	0.00	-0.0400	0.0342	0.0478	-0.0045	0.0131	-0.0288
9	20	625.25	3.94	0.00	-0.0381	0.0341	0.0462	-0.0079	0.0279	-0.0616
9	19	625.25	5.91	0.00	-0.0363	0.0339	0.0424	-0.0112	0.0433	-0.0961
9	18	625.47	7.90	0.00	-0.0345	0.0326	0.0383	-0.0144	0.0595	-0.1329
9	17	625.47	9.86	0.00	-0.0302	0.0316	0.0325	-0.0175	0.0752	-0.1697
9	16	625.25	11.85	0.00	-0.0260	0.0308	0.0264	-0.0204	0.0895	-0.2070
9	27	625.25	-4.14	4.14	0.2797	0.0329	-0.0542	0.0062	-0.0325	0.0696
9	28	625.25	-2.13	4.26	0.2720	0.0326	-0.0487	0.0024	-0.0151	0.0321
9	29	625.68	0.00	4.35	0.2626	0.0326	-0.0443	-0.0015	0.0019	-0.0038
9	30	625.25	2.12	4.25	0.2566	0.0329	-0.0428	-0.0058	0.0178	-0.0380
9	31	625.47	4.13	4.13	0.2543	0.0332	-0.0444	-0.0098	0.0334	-0.0713
9	32	625.25	6.08	4.06	0.2532	0.0330	-0.0459	-0.0134	0.0489	-0.1064
9	33	625.47	8.03	4.02	0.2541	0.0319	-0.0487	-0.0169	0.0649	-0.1430
9	34	625.25	10.01	3.99	0.2551	0.0308	-0.0519	-0.0203	0.0803	-0.1802
9	35	625.47	11.98	4.01	0.2550	0.0303	-0.0550	-0.0234	0.0947	-0.2172
9	36	625.25	13.93	3.99	0.2512	0.0294	-0.0569	-0.0256	0.1047	-0.2492
9	46	625.47	-4.26	8.50	0.5529	0.0308	-0.1381	0.0062	-0.0325	0.0712
9	45	625.25	-2.16	8.62	0.5492	0.0318	-0.1365	0.0028	-0.0161	0.0346
9	44	625.25	0.00	8.64	0.5436	0.0317	-0.1340	-0.0012	0.0014	-0.0023
9	43	625.25	2.16	8.61	0.5404	0.0316	-0.1333	-0.0054	0.0184	-0.0386
9	42	625.25	4.26	8.49	0.5411	0.0311	-0.1341	-0.0090	0.0339	-0.0733
9	41	625.25	6.27	8.38	0.5392	0.0309	-0.1350	-0.0129	0.0503	-0.1099
9	40	625.47	8.27	8.27	0.5376	0.0301	-0.1348	-0.0166	0.0666	-0.1472
9	39	625.25	10.35	7.98	0.5208	0.0294	-0.1295	-0.0202	0.0823	-0.1862
9	38	625.25	12.18	8.13	0.5276	0.0290	-0.1317	-0.0224	0.0926	-0.2166
9	37	625.47	14.12	8.10	0.5213	0.0279	-0.1310	-0.0247	0.1054	-0.2536
9	47	625.25	-4.29	12.86	0.8116	0.0294	-0.2079	0.0057	-0.0301	0.0696
9	48	625.25	-2.15	12.92	0.8111	0.0299	-0.2113	0.0022	-0.0141	0.0326
9	49	625.68	0.00	12.96	0.8093	0.0295	-0.2129	-0.0015	0.0016	-0.0033
9	50	625.47	2.15	12.93	0.8035	0.0297	-0.2086	-0.0052	0.0172	-0.0391
9	51	625.47	4.29	12.85	0.7993	0.0291	-0.2040	-0.0086	0.0329	-0.0754
9	52	625.47	6.37	12.74	0.7949	0.0280	-0.1998	-0.0118	0.0469	-0.1086
9	53	625.25	8.43	12.63	0.7905	0.0273	-0.1990	-0.0148	0.0602	-0.1421
10	26	623.74	-2.96	0.00	-0.0812	0.0418	0.1285	0.0032	-0.0211	0.0479
10	25	623.74	-1.98	0.00	-0.0830	0.0416	0.1296	0.0017	-0.0142	0.0325
10	24	623.95	-0.98	0.00	-0.0835	0.0413	0.1300	0.0001	-0.0076	0.0176
10	23	624.17	0.00	0.00	-0.0826	0.0401	0.1301	-0.0013	-0.0007	0.0020
10	22	623.95	0.98	0.00	-0.0832	0.0400	0.1305	-0.0028	0.0058	-0.0128
10	21	623.95	1.98	0.00	-0.0825	0.0406	0.1301	-0.0042	0.0126	-0.0282
10	20	623.95	2.98	0.00	-0.0817	0.0412	0.1291	-0.0058	0.0192	-0.0431
10	19	624.17	3.95	0.00	-0.0809	0.0407	0.1273	-0.0073	0.0264	-0.0595
10	18	623.95	5.92	0.00	-0.0794	0.0402	0.1249	-0.0103	0.0409	-0.0930
10	17	623.95	7.91	0.00	-0.0780	0.0389	0.1208	-0.0132	0.0559	-0.1274
10	16	624.17	9.86	0.00	-0.0739	0.0376	0.1146	-0.0160	0.0707	-0.1640
10	15	624.17	11.88	0.00	-0.0700	0.0365	0.1079	-0.0188	0.0849	-0.2004
10	14	624.17	13.86	0.00	-0.0665	0.0355	0.0999	-0.0212	0.0967	-0.2356
10	27	623.52	-4.19	4.18	0.2318	0.0371	0.0338	0.0053	-0.0286	0.0637
10	28	623.95	-2.16	4.32	0.2259	0.0370	0.0374	0.0020	-0.0130	0.0288
10	29	624.17	0.00	4.42	0.2198	0.0377	0.0400	-0.0013	0.0016	-0.0035
10	30	623.52	2.15	4.31	0.2120	0.0378	0.0424	-0.0052	0.0154	-0.0342
10	31	624.82	4.16	4.18	0.2064	0.0379	0.0428	-0.0087	0.0294	-0.0655
10	32	624.17	6.12	4.07	0.2065	0.0370	0.0407	-0.0121	0.0442	-0.0992
10	33	623.30	8.08	4.03	0.2061	0.0359	0.0378	-0.0155	0.0594	-0.1351
10	34	623.15	10.05	4.03	0.2092	0.0351	0.0333	-0.0187	0.0744	-0.1710
10	35	624.60	12.02	4.00	0.2074	0.0340	0.0295	-0.0216	0.0880	-0.2072
10	36	623.74	13.97	4.00	0.2051	0.0330	0.0271	-0.0239	0.0983	-0.2393
10	46	624.39	-4.31	8.56	0.5067	0.0325	-0.0522	0.0050	-0.0282	0.0644
10	45	623.95	-2.13	8.69	0.5003	0.0331	-0.0476	0.0020	-0.0136	0.0306
10	44	624.17	0.00	8.72	0.4949	0.0332	-0.0452	-0.0011	0.0010	-0.0020
10	43	624.60	2.18	8.69	0.4944	0.0335	-0.0457	-0.0044	0.0154	-0.0347
10	42	624.17	4.29	8.56	0.4923	0.0329	-0.0471	-0.0078	0.0294	-0.0669
10	41	623.74	6.32	8.43	0.4905	0.0320	-0.0483	-0.0115	0.0450	-0.1019
10	40	623.30	8.31	8.31	0.4891	0.0317	-0.0481	-0.0151	0.0601	-0.1375
10	39	623.52	10.41	8.02	0.4731	0.0312	-0.0439	-0.0187	0.0754	-0.1756
10	38	623.52	12.22	8.19	0.4811	0.0303	-0.0476	-0.0210	0.0851	-0.2051
10	37	623.52	14.16	8.12	0.4762	0.0293	-0.0495	-0.0233	0.0989	-0.2432
10	47	623.95	-4.34	12.94	0.7630	0.0286	-0.1199	0.0051	-0.0270	0.0639
10	48	623.95	-2.17	13.01	0.7602	0.0292	-0.1174	0.0017	-0.0125	0.0295
10	49	624.17	0.00	13.03	0.7558	0.0294	-0.1144	-0.0014	0.0014	-0.0030
10	50	624.17	2.16	13.00	0.7526	0.0295	-0.1153	-0.0045	0.0156	-0.0363
10	51	623.95	4.31	12.93	0.7505	0.0289	-0.1161	-0.0076	0.0296	-0.0700
10	52	624.17	6.38	12.82	0.7491	0.0281	-0.1164	-0.0106	0.0421	-0.1013
10	53	624.17	8.47	12.68	0.7456	0.0268	-0.1177	-0.0137	0.0550	-0.1340
10	54	623.95	10.45	12.57	0.7390	0.0259	-0.1180	-0.0174	0.0692	-0.1685

TABLE V - Continued
 AERODYNAMIC CHARACTERISTICS IN SIDESLIP FOR VARIOUS ANGLES OF ATTACK.
 BODY AXES; M = 1.41

Run	Pt.	q	β ,deg	α ,deg	C_N	C_A	C_m	C_l	C_n	C_Y
11	28	622.87	-2.95	.01	-.0687	.0384	.1079	.0013	-.0283	.0578
11	27	622.87	-1.96	.00	-.0707	.0387	.1091	.0003	-.0187	.0379
11	26	623.09	-.98	.00	-.0714	.0390	.1096	-.0005	-.0095	.0189
11	25	622.87	.01	.00	-.0711	.0387	.1095	-.0014	-.0010	.0014
11	24	622.87	.97	.00	-.0707	.0388	.1090	-.0021	.0077	-.0168
11	23	622.87	1.98	.00	-.0689	.0389	.1081	-.0030	.0165	-.0350
11	22	622.87	2.95	.01	-.0684	.0396	.1074	-.0039	.0255	-.0541
11	21	622.87	3.93	.00	-.0680	.0392	.1066	-.0048	.0343	-.0724
11	20	621.79	5.88	.00	-.0671	.0388	.1055	-.0066	.0528	-.1115
11	19	623.09	7.87	.00	-.0671	.0377	.1049	-.0084	.0707	-.1509
11	18	623.30	9.82	.00	-.0668	.0369	.1055	-.0104	.0884	-.1911
11	17	622.66	11.81	.00	-.0689	.0363	.1071	-.0124	.1046	-.2304
11	16	622.87	13.78	.00	-.0720	.0358	.1116	-.0141	.1173	-.2666
11	29	622.87	-4.16	4.16	.2450	.0341	.0126	.0029	-.0357	.0735
11	30	622.87	-2.14	4.31	.2434	.0341	.0110	.0010	-.0165	.0335
11	31	622.87	-.01	4.39	.2363	.0338	.0114	-.0012	.0019	-.0042
11	32	622.87	2.13	4.29	.2277	.0340	.0152	-.0038	.0197	-.0404
11	33	622.87	4.15	4.15	.2223	.0346	.0182	-.0060	.0375	-.0781
11	34	622.87	6.08	4.06	.2175	.0348	.0209	-.0080	.0545	-.1146
11	35	622.87	8.04	4.03	.2154	.0336	.0232	-.0103	.0721	-.1539
11	36	622.87	10.02	4.00	.2123	.0337	.0272	-.0126	.0895	-.1938
11	37	623.09	11.97	3.98	.2083	.0329	.0320	-.0148	.1057	-.2337
11	45	622.44	-4.28	8.54	.5223	.0298	-.0777	.0030	-.0313	.0677
11	44	622.44	-2.18	8.66	.5184	.0301	-.0759	.0010	-.0149	.0326
11	43	622.44	.00	8.69	.5137	.0303	-.0762	-.0011	.0016	-.0035
11	42	622.44	2.16	8.66	.5126	.0303	-.0765	-.0033	.0173	-.0374
11	41	622.66	4.28	8.54	.5109	.0300	-.0763	-.0056	.0333	-.0724
11	40	622.44	6.31	8.40	.5071	.0300	-.0728	-.0079	.0502	-.1094
11	39	622.66	8.29	8.32	.5022	.0299	-.0666	-.0102	.0674	-.1485
11	38	622.44	10.39	8.01	.4810	.0297	-.0550	-.0125	.0857	-.1905
11	46	622.66	-4.31	12.92	.7884	.0253	-.1595	.0030	-.0269	.0629
11	47	623.09	-2.16	12.97	.7839	.0256	-.1579	.0008	-.0121	.0283
11	48	622.66	-.02	13.01	.7805	.0255	-.1570	-.0012	.0018	-.0036
11	49	622.44	2.14	12.97	.7781	.0257	-.1572	-.0033	.0159	-.0363
11	50	622.44	4.30	12.89	.7763	.0252	-.1580	-.0054	.0302	-.0703
11	51	622.87	6.38	12.80	.7730	.0250	-.1562	-.0076	.0436	-.1027
11	52	622.66	8.45	12.65	.7645	.0243	-.1486	-.0099	.0576	-.1366
11	53	622.66	10.43	12.55	.7540	.0242	-.1390	-.0126	.0735	-.1739
12	24	623.09	-3.92	.03	-.0180	.0336	.0195	.0024	-.0336	.0703
12	23	622.87	-1.98	.00	-.0199	.0335	.0171	.0005	-.0171	.0351
12	22	622.87	-.98	.00	-.0182	.0334	.0162	-.0004	-.0090	.0178
12	21	622.87	.00	.00	-.0190	.0335	.0162	-.0013	-.0006	.0005
12	20	623.09	.99	.00	-.0186	.0336	.0162	-.0022	.0075	-.0169
12	19	623.30	1.97	.00	-.0181	.0337	.0168	-.0031	.0153	-.0335
12	18	622.87	3.93	.00	-.0209	.0331	.0196	-.0050	.0320	-.0692
12	17	622.87	5.90	.00	-.0211	.0327	.0214	-.0067	.0485	-.1049
12	16	623.52	7.89	.00	-.0224	.0321	.0230	-.0086	.0647	-.1417
12	15	622.87	9.85	.02	-.0224	.0310	.0251	-.0105	.0805	-.1787
12	14	622.22	10.86	.02	-.0297	.0302	.0292	-.0113	.0882	-.1977
12	25	622.87	-4.13	4.13	.2922	.0324	-.0743	.0035	-.0315	.0666
12	26	622.87	-2.12	4.25	.2879	.0329	-.0735	.0013	-.0145	.0306
12	27	622.87	.00	4.32	.2812	.0326	-.0724	-.0012	.0019	-.0044
12	28	622.87	2.12	4.24	.2738	.0325	-.0707	-.0041	.0177	-.0373
12	29	623.30	4.12	4.12	.2694	.0327	-.0688	-.0067	.0332	-.0716
12	30	622.87	6.07	4.04	.2649	.0327	-.0660	-.0088	.0487	-.1064
12	31	622.87	8.04	4.01	.2615	.0321	-.0615	-.0110	.0650	-.1433
12	32	623.09	10.00	3.99	.2580	.0311	-.0557	-.0131	.0807	-.1805
12	33	623.30	11.97	3.99	.2515	.0301	-.0486	-.0153	.0961	-.2188
12	34	620.93	13.92	3.98	.2412	.0297	-.0364	-.0168	.1077	-.2527
12	44	623.30	-4.26	8.49	.5637	.0316	-.1585	.0035	-.0284	.0639
12	43	622.66	-2.16	8.61	.5592	.0321	-.1568	.0013	-.0135	.0306
12	42	622.66	.00	8.62	.5558	.0317	-.1565	-.0010	.0012	-.0022
12	41	623.09	2.14	8.60	.5545	.0324	-.1567	-.0035	.0157	-.0351
12	40	622.66	4.25	8.49	.5533	.0315	-.1575	-.0060	.0301	-.0676
12	39	622.66	6.28	8.37	.5518	.0308	-.1567	-.0086	.0454	-.1020
12	38	622.66	8.27	8.27	.5482	.0307	-.1534	-.0112	.0607	-.1379
12	37	622.66	10.35	8.01	.5293	.0298	-.1427	-.0135	.0766	-.1771
12	36	622.87	12.19	8.14	.5285	.0288	-.1342	-.0151	.0880	-.2086
12	35	623.09	14.14	8.08	.5161	.0287	-.1226	-.0167	.1031	-.2486
12	45	622.87	-4.31	12.84	.8265	.0297	-.2377	.0033	-.0252	.0608
12	46	622.87	-2.12	12.90	.8228	.0300	-.2357	.0009	-.0114	.0279
12	47	622.87	.00	12.94	.8215	.0303	-.2355	-.0012	.0015	-.0031
12	48	622.87	2.12	12.90	.8187	.0302	-.2361	-.0034	.0145	-.0348
12	49	622.66	4.28	12.83	.8158	.0297	-.2378	-.0057	.0273	-.0656
12	50	622.66	6.36	12.72	.8143	.0287	-.2373	-.0081	.0399	-.0972
12	51	623.09	8.43	12.62	.8076	.0282	-.2316	-.0105	.0529	-.1293
12	52	622.87	10.42	12.49	.7958	.0274	-.2238	-.0134	.0670	-.1641

TABLE V - Continued
 AERODYNAMIC CHARACTERISTICS IN SIDESLIP FOR VARIOUS ANGLES OF ATTACK.
 BODY AXES; M = 1.41

Run	Pt.	q	β , deg	α , deg	C_N	C_A	C_m	C_l	C_n	C_Y
15	31	625.68	-3.97	.00	-.0500	.0365	.0536	.0089	-.0253	.0642
15	30	625.68	-2.97	.00	-.0498	.0365	.0528	.0066	-.0190	.0480
15	29	625.90	-1.99	.00	-.0496	.0365	.0522	.0041	-.0130	.0326
15	28	625.25	-.99	.00	-.0495	.0365	.0514	.0018	-.0070	.0165
15	27	625.25	.00	.00	-.0494	.0364	.0511	-.0006	-.0009	.0012
15	26	625.25	1.00	.00	-.0492	.0364	.0512	-.0030	.0052	-.0142
15	25	625.25	1.99	.00	-.0503	.0364	.0513	-.0053	.0112	-.0297
15	24	625.68	2.97	.00	-.0499	.0359	.0521	-.0077	.0173	-.0459
15	23	625.68	3.96	.00	-.0509	.0358	.0531	-.0102	.0238	-.0621
15	22	625.47	5.95	.01	-.0500	.0356	.0530	-.0151	.0379	-.0978
15	21	625.47	7.94	-.01	-.0494	.0351	.0519	-.0248	.0522	-.1345
15	20	625.68	9.91	.00	-.0484	.0341	.0519	-.0248	.0566	-.1723
15	18	624.17	11.92	.00	-.0460	.0332	.0503	-.0300	.0808	-.2115
15	19	625.25	13.91	.00	-.0438	.0319	.0495	-.0348	.0926	-.2478
15	32	625.90	-4.15	4.15	.2666	.0357	-.0423	.0094	-.0268	.0675
15	33	625.25	-2.13	4.26	.2584	.0353	-.0386	.0043	-.0121	.0299
15	34	625.47	.00	4.34	.2495	.0355	-.0351	-.0008	.0014	-.0037
15	35	625.47	2.12	4.25	.2386	.0353	-.0318	-.0065	.0143	-.0372
15	36	625.25	4.14	4.14	.2348	.0353	-.0314	-.0119	.0273	-.0715
15	37	625.68	6.11	4.07	.2319	.0351	-.0311	-.0171	.0410	-.1069
15	38	625.68	8.09	4.03	.2316	.0347	-.0309	-.0221	.0548	-.1438
15	39	625.25	10.06	4.02	.2330	.0338	-.0309	-.0272	.0684	-.1812
15	40	625.47	12.04	4.03	.2309	.0325	-.0290	-.0322	.0816	-.2195
15	41	626.12	14.02	4.01	.2292	.0319	-.0261	-.0368	.0911	-.2525
15	51	625.47	-4.27	8.52	.5352	.0346	-.1225	.0089	-.0259	.0689
15	50	625.68	-2.16	8.62	.5305	.0349	-.1216	.0042	-.0128	.0358
15	49	625.68	-.02	8.64	.5239	.0347	-.1193	-.0008	.0007	-.0022
15	48	625.47	2.15	8.61	.5228	.0345	-.1200	-.0062	.0139	-.0369
15	47	625.68	4.26	8.49	.5188	.0345	-.1189	-.0110	.0268	-.0717
15	46	625.47	6.30	8.40	.5179	.0333	-.1184	-.0159	.0398	-.1076
15	45	625.25	8.29	8.29	.5149	.0327	-.1166	-.0208	.0529	-.1450
15	44	625.25	10.41	8.02	.4968	.0322	-.1162	-.0261	.0671	-.1858
15	43	625.25	12.47	8.19	.5016	.0313	-.1057	-.0301	.0760	-.2173
15	42	624.60	14.22	8.12	.4983	.0307	-.1019	-.0346	.0891	-.2590
15	52	625.47	-4.30	12.88	.7818	.0325	-.1850	.0071	-.0219	.0654
15	53	625.47	-2.17	12.92	.7804	.0326	-.1877	.0028	-.0099	.0294
15	54	625.47	.00	12.95	.7778	.0328	-.1878	-.0010	.0012	-.0032
15	55	625.25	2.15	12.91	.7730	.0328	-.1862	-.0049	.0124	-.0366
15	56	625.25	4.29	12.86	.7689	.0323	-.1828	-.0090	.0241	-.0713
15	57	625.47	6.39	12.77	.7648	.0316	-.1798	-.0131	.0350	-.1052
15	58	625.25	8.44	12.64	.7623	.0300	-.1795	-.0168	.0458	-.1404
15	59	622.87	10.46	12.54	.7562	.0295	-.1775	-.0223	.0596	-.1806
16	30	623.74	-3.97	.00	-.0893	.0435	.1355	.0086	-.0242	.0642
16	29	623.74	-2.99	.01	-.0893	.0435	.1348	.0063	-.0183	.0486
16	28	623.95	-2.01	.00	-.0893	.0439	.1345	.0041	-.0129	.0343
16	27	623.74	-1.00	.00	-.0891	.0432	.1342	.0016	-.0069	.0189
16	26	623.74	.00	.00	-.0902	.0427	.1346	-.0006	-.0010	.0028
16	25	623.74	1.00	.00	-.0901	.0428	.1344	-.0029	.0049	-.0125
16	24	623.74	1.99	.00	-.0887	.0431	.1336	-.0052	.0105	-.0271
16	23	623.74	2.99	.00	-.0898	.0432	.1342	-.0075	.0164	-.0432
16	22	623.95	3.97	.00	-.0895	.0434	.1342	-.0099	.0226	-.0594
16	21	623.74	5.95	-.01	-.0890	.0425	.1352	-.0145	.0358	-.0935
16	20	623.74	7.94	.00	-.0885	.0418	.1353	-.0190	.0493	-.1289
16	19	623.74	9.92	.00	-.0879	.0406	.1350	-.0237	.0628	-.1652
16	18	623.52	11.93	.00	-.0859	.0392	.1333	-.0285	.0758	-.2022
16	17	623.52	13.92	.00	-.0838	.0381	.1317	-.0333	.0873	-.2381
16	31	623.74	-4.21	4.20	.2226	.0402	.0453	.0087	-.0238	.0642
16	32	623.95	-2.17	4.34	.2162	.0402	.0470	.0040	-.0107	.0291
16	33	623.95	-.01	4.42	.2067	.0403	.0498	-.0008	.0013	-.0027
16	34	623.95	2.15	4.33	.1980	.0401	.0528	-.0061	.0127	-.0342
16	35	623.95	4.19	4.19	.1927	.0402	.0550	-.0112	.0247	-.0686
16	36	623.74	6.15	4.10	.1871	.0397	.0574	-.0160	.0372	-.1003
16	37	623.74	8.12	4.05	.1866	.0392	.0578	-.0208	.0503	-.1361
16	38	623.74	10.09	4.05	.1875	.0380	.0571	-.0258	.0632	-.1724
16	39	623.74	12.09	4.03	.1866	.0371	.0578	-.0307	.0761	-.2100
16	40	623.74	14.04	4.05	.1862	.0358	.0594	-.0352	.0852	-.2422
16	50	624.39	-4.31	8.60	.4877	.0357	-.0339	.0078	-.0228	.0647
16	49	623.95	-2.18	8.69	.4844	.0363	-.0326	.0036	-.0110	.0315
16	48	624.39	.00	8.72	.4781	.0365	-.0308	-.0008	.0005	-.0004
16	47	623.95	2.18	8.68	.4752	.0366	-.0300	-.0054	.0120	-.0332
16	46	623.95	4.20	8.58	.4735	.0363	-.0301	-.0099	.0236	-.0662
16	45	623.95	6.34	8.44	.4709	.0356	-.0296	-.0146	.0358	-.1010
16	44	623.74	8.35	8.35	.4676	.0348	-.0276	-.0194	.0482	-.1367
16	43	624.17	10.46	8.09	.4517	.0342	-.0205	-.0247	.0618	-.1770
16	42	624.17	12.29	8.21	.4551	.0336	-.0187	-.0288	.0708	-.2085
16	41	623.95	14.25	8.14	.4525	.0333	-.0165	-.0332	.0827	-.2483
16	51	623.95	-4.34	12.94	.7390	.0319	-.1039	.0067	-.0208	.0647
16	52	624.17	-2.16	13.00	.7362	.0314	-.1040	.0026	-.0094	.0296
16	53	624.39	.00	13.04	.7330	.0315	-.1034	-.0008	.0004	-.0006
16	54	624.39	2.14	12.98	.7313	.0317	-.1032	-.0045	.0109	-.0322
16	55	624.82	4.30	12.95	.7265	.0320	-.1019	-.0085	.0221	-.0667
16	56	624.60	6.42	12.82	.7217	.0317	-.0971	-.0124	.0326	-.1002
16	57	623.09	8.46	12.72	.7178	.0307	-.0956	-.0161	.0429	-.1342
16	58	624.39	10.50	12.59	.7113	.0301	-.0935	-.0214	.0555	-.1732

TABLE V - Continued
 AERODYNAMIC CHARACTERISTICS IN SIDESLIP FOR VARIOUS ANGLES OF ATTACK.
 BODY AXES; M = 1.41

Run	Pt.	q	β , deg	α , deg	C_N	C_A	C_m	C_l	C_n	C_y
17	27	626.33	-3.94	.01	-.0853	.0407	.1145	.0056	-.0343	.0788
17	26	625.68	-1.97	.00	-.0870	.0414	.1152	.0024	-.0176	.0407
17	25	625.68	-1.00	.00	-.0872	.0418	.1157	.0008	-.0091	.0208
17	24	625.68	.00	.00	-.0873	.0420	.1153	-.0008	-.0005	.0013
17	23	626.12	.97	.00	-.0875	.0414	.1150	-.0024	.0077	-.0174
17	22	625.68	1.97	.00	-.0868	.0411	.1138	-.0038	.0156	-.0355
17	21	625.68	3.93	.00	-.0857	.0407	.1126	-.0072	.0332	-.0755
17	20	625.68	5.90	-.01	-.0872	.0400	.1137	-.0105	.0499	-.1147
17	19	625.68	7.89	.00	-.0872	.0392	.1156	-.0138	.0662	-.1545
17	18	626.12	9.86	.00	-.0878	.0383	.1188	-.0176	.0826	-.1956
17	16	625.90	10.88	.00	-.0940	.0379	.1228	-.0197	.0903	-.2151
17	17	625.68	10.88	.00	-.0874	.0379	.1204	-.0198	.0906	-.2160
17	28	623.95	-4.17	4.17	.2333	.0363	.0136	.0060	-.0313	.0749
17	29	624.82	-2.14	4.29	.2307	.0369	.0101	.0027	-.0143	.0345
17	30	624.60	.00	4.38	.2230	.0369	.0102	-.0007	.0022	-.0041
17	31	624.60	2.13	4.27	.2111	.0372	.0151	-.0047	.0179	-.0412
17	32	625.03	4.14	4.14	.2038	.0371	.0206	-.0084	.0337	-.0797
17	33	624.60	6.10	4.07	.1979	.0371	.0261	-.0120	.0490	-.1171
17	34	624.60	8.08	4.03	.1947	.0370	.0318	-.0158	.0648	-.1567
17	35	624.82	10.05	4.01	.1916	.0359	.0375	-.0197	.0807	-.1982
17	36	624.60	12.03	4.01	.1872	.0355	.0450	-.0241	.0964	-.2393
17	37	624.60	13.98	4.00	.1797	.0351	.0574	-.0283	.1079	-.2758
17	47	624.82	-4.28	8.54	.5071	.0322	-.0801	.0059	-.0259	.0687
17	46	624.17	-2.17	8.64	.5057	.0326	-.0824	.0026	-.0123	.0336
17	45	624.60	.00	8.67	.5014	.0330	-.0821	-.0008	.0010	-.0010
17	44	624.60	2.17	8.64	.4988	.0331	-.0809	-.0045	.0141	-.0357
17	43	624.17	4.28	8.53	.4945	.0327	-.0787	-.0080	.0277	-.0715
17	42	624.60	6.30	8.43	.4899	.0321	-.0728	-.0117	.0422	-.1091
17	41	624.60	8.31	8.31	.4838	.0323	-.0640	-.0151	.0573	-.1492
17	40	624.17	10.40	8.05	.4630	.0318	-.0502	-.0193	.0734	-.1927
17	39	625.03	12.27	8.19	.4638	.0314	-.0401	-.0228	.0850	-.2290
17	38	624.60	14.21	8.12	.4541	.0317	-.0266	-.0266	.1002	-.2734
17	48	624.17	-4.30	12.89	.7682	.0274	-.1655	.0049	-.0207	.0637
17	49	624.60	-2.17	12.93	.7653	.0274	-.1674	.0018	-.0094	.0300
17	50	624.39	.00	12.96	.7621	.0273	-.1674	-.0009	.0014	-.0019
17	51	624.17	2.13	12.92	.7589	.0276	-.1665	-.0037	.0122	-.0345
17	52	624.17	4.29	12.86	.7566	.0274	-.1647	-.0068	.0235	-.0685
17	53	624.60	6.39	12.78	.7515	.0268	-.1608	-.0100	.0349	-.1025
17	54	624.17	8.45	12.66	.7428	.0262	-.1529	-.0131	.0468	-.1395
17	55	624.39	10.47	12.55	.7325	.0266	-.1390	-.0173	.0614	-.1808
18	24	625.68	-3.96	.00	-.0403	.0356	.0336	.0058	-.0309	.0730
18	23	623.95	-1.98	.00	-.0387	.0354	.0290	.0025	-.0163	.0373
18	22	626.55	-1.00	.00	-.0376	.0360	.0274	.0009	-.0088	.0200
18	21	626.12	.00	.00	-.0378	.0360	.0269	-.0008	-.0008	.0011
18	20	626.12	.99	.00	-.0382	.0358	.0270	-.0023	.0066	-.0160
18	19	626.12	1.97	.00	-.0382	.0354	.0277	-.0041	.0143	-.0339
18	18	626.33	3.95	.00	-.0408	.0355	.0320	-.0075	.0299	-.0714
18	17	626.33	5.92	.00	-.0421	.0350	.0359	-.0108	.0447	-.1080
18	16	626.12	7.92	-.01	-.0447	.0342	.0401	-.0143	.0596	-.1447
18	15	626.12	9.88	.00	-.0481	.0329	.0467	-.0179	.0743	-.1827
18	14	626.33	11.89	.00	-.0506	.0317	.0560	-.0220	.0894	-.2237
18	25	625.68	-4.14	4.14	.2785	.0349	-.0682	.0068	-.0268	.0670
18	26	625.90	-2.12	4.25	.2739	.0357	-.0685	.0030	-.0119	.0301
18	27	626.12	-.01	4.31	.2649	.0350	-.0675	-.0008	.0018	-.0044
18	28	625.90	2.11	4.22	.2571	.0350	-.0653	-.0052	.0152	-.0380
18	29	626.33	4.11	4.13	.2509	.0345	-.0622	-.0093	.0286	-.0722
18	30	625.90	6.09	4.06	.2438	.0341	-.0560	-.0129	.0425	-.1079
18	31	625.90	8.06	4.04	.2393	.0340	-.0473	-.0166	.0571	-.1456
18	32	625.68	10.06	4.04	.2363	.0332	-.0405	-.0205	.0716	-.1847
18	33	625.68	12.03	4.03	.2306	.0319	-.0303	-.0247	.0861	-.2249
18	34	625.25	13.99	4.00	.2207	.0305	-.0139	-.0286	.0977	-.2601
18	43	626.55	-4.26	8.49	.5506	.0340	-.1577	.0064	-.0229	.0640
18	42	626.98	-2.16	8.59	.5499	.0344	-.1592	.0029	-.0106	.0299
18	41	626.33	-.02	8.60	.5451	.0345	-.1589	-.0007	.0009	-.0020
18	40	626.33	2.15	8.58	.5414	.0347	-.1582	-.0047	.0126	-.0342
18	39	626.33	4.25	8.48	.5393	.0339	-.1573	-.0085	.0245	-.0674
18	38	626.76	6.27	8.38	.5359	.0330	-.1548	-.0125	.0371	-.1023
18	37	626.33	8.29	8.29	.5300	.0324	-.1485	-.0163	.0503	-.1390
18	36	625.68	10.41	8.02	.5084	.0318	-.1322	-.0204	.0652	-.1816
18	35	626.33	12.25	8.20	.5103	.0305	-.1223	-.0239	.0751	-.2146
18	44	626.33	-4.30	12.83	.8103	.0317	-.2423	.0054	-.0187	.0607
18	45	626.76	-2.14	12.87	.8065	.0318	-.2419	.0021	-.0087	.0280
18	46	625.68	.00	12.91	.8033	.0318	-.2414	-.0009	.0011	-.0022
18	47	625.68	2.14	12.86	.7999	.0316	-.2411	-.0040	.0113	-.0339
18	48	625.90	4.25	12.82	.7977	.0316	-.2425	-.0071	.0212	-.0660
18	49	625.90	6.37	12.73	.7953	.0309	-.2392	-.0106	.0316	-.0991
18	50	626.55	8.43	12.63	.7893	.0297	-.2329	-.0140	.0425	-.1335
18	51	626.33	10.45	12.52	.7792	.0291	-.2227	-.0184	.0550	-.1721

TABLE V - Continued
 AERODYNAMIC CHARACTERISTICS IN SIDESLIP FOR VARIOUS ANGLES OF ATTACK.
 BODY AXES: M = 1.41

Run	Pt.	q	β , deg	α , deg	C_N	C_A	C_m	C_l	C_n	C_Y
19	26	625.03	-3.97	.03	-.0332	.0331	.0263	.0083	-.0248	.0639
19	25	625.25	-1.98	.00	-.0359	.0332	.0242	.0039	-.0129	.0336
19	24	625.25	-.99	.00	-.0345	.0331	.0233	.0015	-.0070	.0179
19	23	624.82	.00	.00	-.0345	.0328	.0230	-.0007	-.0011	.0027
19	22	624.39	.99	-.01	-.0359	.0328	.0232	-.0028	.0049	-.0130
19	21	624.60	1.98	-.01	-.0357	.0324	.0233	-.0051	.0108	-.0284
19	20	626.12	3.96	-.01	-.0365	.0325	.0253	-.0096	.0230	-.0598
19	19	625.03	5.96	.00	-.0374	.0319	.0271	-.0141	.0361	-.0939
19	18	625.47	7.95	.00	-.0381	.0311	.0291	-.0184	.0498	-.1295
19	17	625.03	9.91	.00	-.0388	.0305	.0308	-.0229	.0634	-.1660
19	16	625.25	11.93	.00	-.0366	.0295	.0317	-.0274	.0767	-.2030
19	27	623.95	-4.16	4.16	.2518	.0320	-.0203	.0085	-.0240	.0636
19	28	622.87	-2.13	4.27	.2455	.0324	-.0199	.0039	-.0108	.0290
19	29	625.47	.00	4.35	.2390	.0324	-.0190	.0009	.0015	-.0038
19	30	625.03	2.13	4.26	.2303	.0323	-.0168	-.0062	.0132	-.0347
19	31	625.03	4.15	4.15	.2248	.0318	-.0150	-.0112	.0252	-.0670
19	32	625.68	6.11	4.07	.2214	.0322	-.0130	-.0157	.0374	-.1004
19	33	625.68	8.10	4.06	.2221	.0316	-.0123	-.0204	.0503	-.1353
19	34	625.47	10.09	4.03	.2216	.0306	-.0119	-.0250	.0635	-.1719
19	35	625.47	12.07	4.02	.2207	.0296	-.0108	-.0297	.0768	-.2102
19	44	625.47	-4.29	8.57	.5004	.0316	-.0641	.0075	-.0224	.0641
19	43	625.47	-2.18	8.66	.4965	.0318	-.0634	.0035	-.0108	.0316
19	42	625.90	-.02	8.69	.4914	.0316	-.0625	-.0008	.0009	-.0011
19	41	625.47	2.17	8.65	.4897	.0317	-.0623	-.0054	.0121	-.0330
19	40	625.47	4.29	8.55	.4867	.0312	-.0624	-.0098	.0237	-.0659
19	39	625.47	6.32	8.42	.4838	.0303	-.0621	-.0144	.0357	-.0999
19	38	625.68	8.33	8.33	.4827	.0297	-.0613	-.0189	.0480	-.1361
19	37	625.47	10.45	8.05	.4654	.0290	-.0570	-.0238	.0616	-.1758
19	36	625.68	12.28	8.20	.4711	.0282	-.0551	-.0276	.0706	-.2079
19	45	625.25	-4.32	12.95	.7369	.0292	-.1044	.0060	-.0195	.0622
19	46	625.03	-2.16	12.98	.7314	.0293	-.1035	.0023	-.0091	.0295
19	47	625.03	.00	13.02	.7284	.0294	-.1029	-.0010	.0011	-.0015
19	48	625.47	2.16	12.98	.7274	.0295	-.1036	-.0044	.0113	-.0330
19	49	625.25	4.31	12.93	.7240	.0291	-.1039	-.0079	.0218	-.0659
19	50	625.25	6.42	12.82	.7235	.0282	-.1041	-.0117	.0319	-.0980
19	51	626.98	8.48	12.70	.7202	.0268	-.1035	-.0155	.0424	-.1333
19	52	626.33	10.50	12.59	.7144	.0267	-.1009	-.0206	.0550	-.1717
21	29	624.39	-3.96	.00	-.0239	.0332	.0106	.0007	-.0298	.0727
21	28	624.60	-2.97	.00	-.0238	.0333	.0110	.0004	-.0225	.0555
21	27	624.60	-1.98	.00	-.0235	.0333	.0111	-.0001	-.0150	.0368
21	26	624.60	-.99	.00	-.0235	.0339	.0111	-.0004	-.0077	.0197
21	25	624.17	.00	.00	-.0234	.0338	.0108	-.0008	-.0001	.0010
21	24	624.39	.98	.00	-.0221	.0335	.0106	-.0012	.0071	-.0163
21	23	624.17	1.98	.00	-.0220	.0338	.0101	-.0016	.0142	-.0341
21	22	624.60	2.97	.00	-.0219	.0335	.0095	-.0019	.0215	-.0512
21	21	624.60	3.95	.00	-.0218	.0328	.0089	-.0023	.0289	-.0698
21	20	623.95	5.93	.00	-.0205	.0324	.0061	-.0030	.0435	-.1065
21	19	623.95	7.91	.00	-.0193	.0317	.0028	-.0036	.0581	-.1430
21	18	623.95	9.90	.00	-.0181	.0310	-.0014	-.0041	.0724	-.1810
21	17	623.95	11.90	.00	-.0183	.0305	-.0037	-.0044	.0858	-.2188
21	30	624.17	-4.16	4.14	.2696	.0318	-.0371	.0071	-.0301	.0701
21	31	624.17	-2.14	4.28	.2654	.0315	-.0354	.0009	-.0138	.0326
21	32	624.39	.00	4.34	.2593	.0312	-.0346	-.0005	.0025	-.0048
21	33	624.39	2.13	4.26	.2527	.0319	-.0337	-.0022	.0181	-.0410
21	34	624.17	4.13	4.13	.2471	.0319	-.0333	-.0038	.0328	-.0754
21	35	624.17	6.09	4.06	.2437	.0316	-.0351	-.0050	.0470	-.1101
21	36	624.17	8.06	4.02	.2425	.0304	-.0383	-.0059	.0619	-.1472
21	37	624.17	10.03	4.01	.2438	.0297	-.0421	-.0065	.0764	-.1847
21	38	624.60	12.02	4.00	.2400	.0289	-.0448	-.0066	.0898	-.2215
21	47	624.39	-4.29	8.56	.5244	.0292	-.0778	.0031	-.0291	.0687
21	46	624.39	-2.18	8.68	.5226	.0303	-.0766	.0013	-.0138	.0330
21	45	624.60	.00	8.70	.5169	.0302	-.0756	-.0005	.0021	-.0029
21	44	624.17	2.16	8.65	.5155	.0305	-.0762	-.0025	.0180	-.0397
21	43	624.39	4.27	8.56	.5127	.0296	-.0772	-.0043	.0323	-.0733
21	42	624.17	6.31	8.40	.5086	.0292	-.0790	-.0056	.0478	-.1097
21	41	624.17	8.30	8.33	.5071	.0288	-.0821	-.0066	.0627	-.1466
21	40	624.17	10.38	8.00	.4898	.0283	-.0827	-.0073	.0778	-.1861
21	39	624.17	12.23	8.16	.4933	.0272	-.0843	-.0070	.0881	-.2165
21	48	624.39	-4.33	12.97	.7680	.0277	-.1120	.0034	-.0281	.0678
21	49	624.39	-2.17	13.04	.7651	.0273	-.1091	.0014	-.0124	.0308
21	50	624.17	.00	13.07	.7613	.0274	-.1080	-.0005	.0026	-.0043
21	51	624.17	2.17	13.02	.7596	.0280	-.1097	-.0027	.0177	-.0392
21	52	624.39	4.32	12.95	.7581	.0278	-.1125	-.0045	.0323	-.0745
21	53	624.39	6.41	12.80	.7554	.0267	-.1160	-.0061	.0455	-.1075
21	54	624.39	8.48	12.69	.7512	.0256	-.1187	-.0071	.0578	-.1400
21	55	624.17	10.47	12.55	.7424	.0250	-.1199	-.0083	.0721	-.1753

TABLE V - Continued
 AERODYNAMIC CHARACTERISTICS IN SIDESLIP FOR VARIOUS ANGLES OF ATTACK.
 BODY AXES; M = 1.41

Run	Pt.	q	β , deg	α , deg	C_N	C_A	C_m	C_l	C_n	C_y
22	30	623.52	-3.95	.00	-.0281	.0350	.0158	-.0002	-.0322	.0764
22	29	623.52	-2.97	.00	-.0269	.0352	.0155	-.0003	-.0244	.0576
22	28	623.74	-1.98	.00	-.0269	.0352	.0156	-.0004	-.0164	.0388
22	27	623.30	-1.00	.00	-.0256	.0358	.0148	-.0006	-.0084	.0200
22	26	623.09	.00	.00	-.0257	.0358	.0147	-.0007	-.0002	.0011
22	25	623.52	.98	.00	-.0256	.0355	.0153	-.0010	.0079	-.0177
22	24	623.09	1.98	.00	-.0258	.0358	.0147	-.0010	.0154	-.0358
22	23	623.09	2.96	.00	-.0257	.0354	.0147	-.0012	.0237	-.0546
22	22	623.52	3.94	.00	-.0257	.0353	.0144	-.0013	.0320	-.0750
22	21	623.09	5.92	.00	-.0247	.0350	.0124	-.0016	.0473	-.1118
22	20	623.09	7.91	.00	-.0236	.0340	.0084	-.0018	.0633	-.1516
22	19	623.09	9.86	.00	-.0225	.0330	.0050	-.0020	.0783	-.1906
22	18	623.52	11.87	.00	-.0243	.0324	.0032	-.0019	.0925	-.2291
22	31	623.30	-4.13	4.13	.2841	.0341	-.0718	.0013	-.0321	.0730
22	32	623.74	-2.12	4.24	.2802	.0339	-.0702	.0006	-.0147	.0330
22	33	623.52	.00	4.32	.2752	.0342	-.0694	-.0005	.0026	-.0053
22	34	623.74	2.11	4.24	.2707	.0344	-.0695	-.0018	.0193	-.0426
22	35	623.52	4.11	4.11	.2657	.0344	-.0693	-.0029	.0352	-.0789
22	36	623.74	6.07	4.04	.2610	.0338	-.0695	-.0036	.0502	-.1147
22	37	623.52	8.02	4.00	.2601	.0333	-.0713	-.0041	.0661	-.1536
22	38	623.52	10.02	4.00	.2576	.0329	-.0708	-.0043	.0815	-.1929
22	39	623.52	11.90	3.96	.2514	.0321	-.0699	-.0041	.0953	-.2300
22	48	624.17	-4.26	8.50	.5589	.0325	-.1489	.0025	-.0301	.0694
22	47	623.95	-2.16	8.61	.5575	.0336	-.1485	.0010	-.0141	.0329
22	46	623.95	.00	8.63	.5538	.0334	-.1480	-.0004	.0025	-.0048
22	45	624.17	2.14	8.60	.5535	.0335	-.1494	-.0020	.0185	-.0409
22	44	623.95	4.25	8.49	.5501	.0325	-.1498	-.0034	.0334	-.0755
22	43	623.95	6.27	8.36	.5474	.0319	-.1514	-.0044	.0495	-.1129
22	42	623.95	8.27	8.27	.5448	.0317	-.1528	-.0051	.0648	-.1500
22	41	623.95	10.35	7.98	.5239	.0312	-.1475	-.0054	.0807	-.1905
22	40	623.95	12.19	8.14	.5252	.0303	-.1445	-.0048	.0917	-.2219
22	49	624.39	-4.30	12.87	.8221	.0305	-.2189	.0029	-.0283	.0679
22	50	624.17	-2.15	12.93	.8197	.0309	-.2169	.0012	-.0124	.0301
22	51	624.17	.00	12.96	.8171	.0307	-.2164	-.0004	.0027	-.0051
22	52	624.17	2.13	12.92	.8143	.0311	-.2177	-.0023	.0180	-.0409
22	53	624.39	4.29	12.85	.8144	.0309	-.2204	-.0039	.0328	-.0756
22	54	624.17	6.36	12.72	.8110	.0292	-.2225	-.0052	.0458	-.1087
22	55	624.17	8.43	12.62	.8046	.0284	-.2215	-.0061	.0587	-.1414
22	56	624.39	10.39	12.50	.7956	.0279	-.2207	-.0071	.0732	-.1774
23	22	623.30	-3.94	.00	-.0779	.0415	.1140	-.0003	-.0349	.0809
23	21	623.30	-1.99	.00	-.0765	.0415	.1148	-.0006	-.0178	.0422
23	20	623.30	-1.00	.00	-.0778	.0423	.1149	-.0007	-.0091	.0218
23	19	623.74	.00	.00	-.0778	.0423	.1146	-.0008	-.0006	.0029
23	18	623.87	.98	.00	-.0767	.0420	.1140	-.0009	.0079	-.0168
23	17	622.01	1.98	.00	-.0755	.0422	.1129	-.0010	.0164	-.0366
23	16	624.17	3.93	.00	-.0741	.0417	.1109	-.0012	.0335	-.0757
23	15	623.52	5.90	.00	-.0742	.0409	.1081	-.0015	.0516	-.1183
23	14	623.52	7.89	.00	-.0731	.0399	.1038	-.0017	.0687	-.1592
23	13	623.52	9.86	.00	-.0707	.0391	.0996	-.0018	.0854	-.2006
23	23	623.09	-4.16	4.16	.2347	.0370	.0115	.0008	-.0361	.0800
23	24	623.09	-2.16	4.30	.2332	.0369	.0136	.0004	-.0168	.0373
23	25	623.09	.00	4.40	.2269	.0367	.0185	-.0004	.0028	-.0052
23	26	623.30	2.14	4.30	.2211	.0374	.0235	-.0014	.0213	-.0451
23	27	623.52	4.15	4.15	.2146	.0375	.0274	-.0023	.0389	-.0840
23	28	623.74	6.10	4.06	.2127	.0372	.0266	-.0030	.0558	-.1224
23	29	623.52	8.05	4.02	.2105	.0364	.0255	-.0035	.0731	-.1638
23	30	623.74	10.02	4.00	.2081	.0360	.0256	-.0037	.0899	-.2047
23	31	623.30	11.99	3.99	.2062	.0354	.0251	-.0036	.1054	-.2453
23	39	623.30	-4.29	8.55	.5122	.0328	-.0684	.0021	-.0334	.0756
23	38	623.30	-2.18	8.66	.5105	.0331	-.0674	.0009	-.0160	.0365
23	37	623.30	.00	8.70	.5067	.0328	-.0654	-.0004	.0026	-.0038
23	36	623.30	2.18	8.66	.5055	.0331	-.0634	-.0018	.0206	-.0434
23	35	623.74	4.29	8.55	.5029	.0326	-.0607	-.0030	.0367	-.0797
23	34	623.52	6.31	8.41	.4992	.0326	-.0587	-.0038	.0542	-.1189
23	33	623.30	8.29	8.29	.4917	.0325	-.0561	-.0043	.0716	-.1595
23	32	623.09	10.37	8.02	.4724	.0322	-.0507	-.0047	.0893	-.2026
23	40	623.74	-4.31	12.93	.7781	.0284	-.1399	.0027	-.0306	.0716
23	41	621.79	-2.16	12.99	.7750	.0281	-.1367	.0011	-.0136	.0329
23	42	623.09	.00	13.03	.7734	.0281	-.1352	-.0004	.0027	-.0041
23	43	623.52	2.14	12.98	.7713	.0286	-.1350	-.0020	.0189	-.0409
23	44	621.79	4.31	12.93	.7688	.0282	-.1355	-.0037	.0351	-.0783
23	45	623.52	6.40	12.79	.7668	.0273	-.1364	-.0048	.0493	-.1129
23	46	623.52	8.44	12.69	.7580	.0268	-.1314	-.0056	.0629	-.1473
23	47	623.30	10.45	12.52	.7471	.0263	-.1272	-.0063	.0790	-.1854

TABLE V - Continued
 AERODYNAMIC CHARACTERISTICS IN SIDESLIP FOR VARIOUS ANGLES OF ATTACK.
 BODY AXES: M = 1.41

Run	Pt.	q	β ,deg	α ,deg	C_N	C_A	C_m	C_l	C_n	C_Y
24	23	624.39	-3.97	.01	-.0853	.0435	.1241	.0016	-.0286	.0725
24	22	624.39	-1.99	.00	-.0884	.0430	.1293	.0003	-.0149	.0384
24	21	624.17	-1.00	.00	-.0894	.0428	.1306	-.0002	-.0073	.0197
24	20	623.95	.00	.00	-.0892	.0431	.1308	-.0008	-.0003	.0026
24	19	623.95	.99	.00	-.0890	.0429	.1306	-.0014	.0068	-.0144
24	18	624.17	1.97	.00	-.0888	.0434	.1292	-.0020	.0137	-.0314
24	17	623.95	3.95	.00	-.0861	.0433	.1237	-.0032	.0277	-.0665
24	16	623.95	5.94	.00	-.0808	.0421	.1147	-.0044	.0426	-.1045
24	15	624.39	7.93	.00	-.0770	.0407	.1048	-.0055	.0572	-.1424
24	14	623.95	9.90	.00	-.0711	.0393	.0922	-.0063	.0716	-.1804
24	13	623.52	11.91	.00	-.0640	.0380	.0793	-.0068	.0849	-.2183
24	25	624.17	-2.15	4.31	.2254	.0384	.0298	.0014	-.0129	.0312
24	26	624.39	.00	4.40	.2186	.0390	.0339	-.0005	.0026	-.0052
24	28	624.17	2.15	4.31	.2135	.0392	.0347	-.0027	.0174	-.0391
24	29	623.30	4.16	4.16	.2078	.0391	.0337	-.0048	.0325	-.0744
24	30	623.74	6.12	4.07	.2076	.0381	.0283	-.0068	.0473	-.1101
24	31	624.82	8.08	4.03	.2091	.0371	.0202	-.0084	.0628	-.1485
24	32	623.95	10.05	4.01	.2122	.0355	.0119	-.0094	.0777	-.1871
24	33	624.17	12.02	4.00	.2137	.0346	.0028	-.0100	.0913	-.2247
24	34	624.60	13.97	4.00	.2111	.0334	-.0048	-.0095	.1011	-.2570
24	44	624.60	-4.29	8.57	.5122	.0330	-.0635	.0046	-.0305	.0710
24	43	624.82	-2.18	8.68	.5077	.0338	-.0593	.0020	-.0145	.0345
24	42	624.39	-0.02	8.71	.5014	.0334	-.0563	-.0005	.0027	-.0046
24	41	624.82	2.18	8.67	.5032	.0342	-.0583	-.0032	.0185	-.0406
24	40	624.39	4.28	8.54	.4994	.0332	-.0596	-.0058	.0337	-.0759
24	39	624.17	6.30	8.42	.4988	.0327	-.0633	-.0078	.0499	-.1139
24	38	623.74	8.30	8.30	.4959	.0320	-.0674	-.0095	.0654	-.1519
24	37	623.30	10.40	8.01	.4807	.0312	-.0697	-.0108	.0806	-.1916
24	36	624.60	12.40	8.17	.4884	.0296	-.0779	-.0108	.0910	-.2223
24	45	624.60	-4.32	12.94	.7765	.0285	-.1342	.0053	-.0310	.0729
24	46	624.17	-2.19	13.00	.7720	.0282	-.1342	.0026	-.0148	.0352
24	47	624.17	.00	13.04	.7713	.0282	-.1328	-.0007	.0032	-.0057
24	48	624.17	2.16	13.00	.7671	.0285	-.1327	-.0038	.0198	-.0432
24	49	624.82	4.31	12.92	.7625	.0290	-.1310	-.0064	.0349	-.0793
24	50	624.60	6.40	12.80	.7585	.0278	-.1301	-.0083	.0482	-.1131
24	51	624.39	8.45	12.66	.7551	.0267	-.1333	-.0098	.0601	-.1448
24	52	624.82	10.45	12.52	.7524	.0254	-.1430	-.0117	.0757	-.1825
25	25	624.82	-3.96	.00	-.0303	.0359	.0430	.0023	-.0309	.0758
25	24	624.60	-1.98	.00	-.0317	.0358	.0469	.0007	-.0150	.0382
25	23	625.03	-1.00	.00	-.0340	.0362	.0477	.0011	-.0078	.0203
25	22	624.60	-.01	.00	-.0324	.0361	.0472	-.0007	-.0006	.0032
25	21	625.03	.99	.00	-.0320	.0358	.0468	-.0014	.0067	-.0147
25	20	624.82	1.97	.00	-.0316	.0364	.0460	-.0021	.0141	-.0326
25	19	624.39	3.94	.00	-.0285	.0359	.0416	-.0037	.0294	-.0693
25	18	624.82	5.93	.00	-.0241	.0352	.0322	-.0053	.0458	-.1091
25	17	625.03	7.92	.00	-.0187	.0345	.0221	-.0067	.0614	-.1480
25	16	625.03	9.89	.00	-.0122	.0334	.0116	-.0078	.0767	-.1876
25	15	624.60	10.91	.00	-.0097	.0329	.0067	-.0082	.0840	-.2079
25	26	624.82	-4.14	4.14	.2856	.0341	-.0613	.0045	-.0347	.0778
25	27	624.60	-2.13	4.27	.2772	.0339	-.0543	.0020	-.0160	.0361
25	28	624.82	.00	4.35	.2686	.0336	-.0495	-.0006	.0031	-.0055
25	29	624.82	2.12	4.24	.2614	.0341	-.0486	-.0033	.0205	-.0437
25	30	625.25	4.11	4.11	.2584	.0342	-.0521	-.0060	.0373	-.0815
25	31	624.60	6.08	4.05	.2549	.0336	-.0554	-.0081	.0528	-.1189
25	32	624.82	8.03	4.01	.2570	.0329	-.0621	-.0098	.0687	-.1584
25	33	624.82	10.01	3.99	.2600	.0317	-.0695	-.0111	.0840	-.1976
25	41	625.25	-4.26	8.49	.5511	.0319	-.1440	.0057	-.0353	.0786
25	40	624.60	-2.16	8.61	.5512	.0326	-.1450	.0030	-.0179	.0396
25	39	625.47	.00	8.63	.5451	.0325	-.1426	-.0008	.0032	-.0057
25	38	625.25	2.14	8.60	.5445	.0322	-.1418	-.0041	.0221	-.0468
25	37	624.60	4.25	8.49	.5427	.0320	-.1417	-.0069	.0384	-.0840
25	36	625.90	6.27	8.36	.5399	.0314	-.1443	-.0092	.0559	-.1235
25	35	624.39	8.26	8.26	.5380	.0308	-.1470	-.0109	.0717	-.1618
25	34	624.82	10.35	7.98	.5225	.0299	-.1470	-.0122	.0873	-.2020
25	43	625.25	-4.29	12.86	.8133	.0297	-.2115	.0059	-.0338	.0778
25	42	623.95	-4.24	12.87	.8126	.0298	-.2112	.0059	-.0336	.0772
25	44	623.95	-2.15	12.92	.8142	.0301	-.2173	.0028	-.0156	.0360
25	45	625.25	.00	12.95	.8141	.0303	-.2210	-.0007	.0031	-.0058
25	46	624.17	2.15	12.91	.8057	.0300	-.2139	-.0041	.0207	-.0451
25	47	624.82	4.26	12.85	.8018	.0295	-.2093	-.0072	.0380	-.0847
25	48	625.25	6.35	12.75	.7957	.0281	-.2058	-.0090	.0514	-.1185
25	49	624.82	8.41	12.60	.7888	.0273	-.2069	-.0105	.0639	-.1505
25	50	623.30	10.41	12.48	.7864	.0263	-.2160	-.0126	.0815	-.1913

TABLE V - Continued
AERODYNAMIC CHARACTERISTICS IN SIDESLIP FOR VARIOUS ANGLES OF ATTACK.

BODY AXES: M = 1.41

Run	Pt.	q	β ,deg	α ,deg	C_N	C_A	C_m	C_l	C_n	C_Y
26	30	623.95	-3.95	.00	-.0263	.0251	.0497	.0062	-.0271	.0618
26	29	624.39	-2.97	.00	-.0266	.0251	.0463	.0046	-.0199	.0460
26	28	623.95	-1.99	.00	-.0272	.0248	.0466	.0031	-.0135	.0313
26	27	624.17	-1.00	.01	-.0263	.0246	.0462	.0015	-.0065	.0154
26	26	624.17	.00	.00	-.0269	.0244	.0462	.0000	.0000	.0008
26	25	623.95	.99	.00	-.0273	.0246	.0462	-.0016	.0066	-.0147
26	24	624.17	1.98	.00	-.0279	.0246	.0466	-.0031	.0125	-.0286
26	23	623.95	2.97	-.01	-.0272	.0247	.0460	-.0046	.0189	-.0434
26	22	624.17	3.95	.00	-.0277	.0247	.0456	-.0061	.0258	-.0590
26	21	623.95	5.93	.00	-.0249	.0245	.0417	-.0092	.0395	-.0909
26	20	623.95	7.92	-.01	-.0219	.0233	.0372	-.0123	.0548	-.1262
26	19	624.39	9.89	.00	-.0177	.0224	.0314	-.0153	.0897	-.1620
26	18	623.95	11.86	.00	-.0137	.0211	.0248	-.0183	.0841	-.1987
26	17	624.17	13.85	.00	-.0110	.0208	.0190	-.0209	.0972	-.2356
26	31	624.17	-3.97	3.97	.0199	.0245	-.0042	.0062	-.0286	.0626
26	32	624.17	-2.00	4.01	.0159	.0241	-.0006	.0027	-.0129	.0277
26	33	623.95	.00	4.02	.0132	.0241	.0024	-.0005	.0018	-.0042
26	34	624.17	2.00	4.00	.0122	.0240	.0024	-.0038	.0161	-.0358
26	35	623.95	3.96	3.96	.0142	.0242	-.0005	-.0071	.0308	-.0686
26	36	624.17	5.94	3.97	.0162	.0233	-.0042	-.0103	.0456	-.1021
26	37	623.74	7.92	3.95	.0200	.0224	-.0092	-.0136	.0609	-.1372
26	38	623.74	9.91	3.96	.0255	.0213	-.0153	-.0167	.0762	-.1747
26	39	623.74	11.91	3.96	.0290	.0201	-.0197	-.0196	.0907	-.2113
26	48	623.52	-4.00	7.98	.0647	.0237	-.0534	.0070	-.0302	.0646
26	47	623.95	-2.01	8.00	.0609	.0240	-.0492	.0033	-.0148	.0306
26	46	623.52	-.03	8.00	.0575	.0239	-.0453	-.0007	.0023	-.0055
26	45	623.74	2.00	7.97	.0601	.0236	-.0479	-.0047	.0188	-.0408
26	44	623.74	3.98	7.98	.0630	.0230	-.0521	-.0082	.0338	-.0745
26	43	623.74	5.97	7.96	.0652	.0225	-.0541	-.0114	.0488	-.1090
26	42	623.74	7.93	7.96	.0681	.0213	-.0574	-.0144	.0637	-.1440
26	41	623.74	10.07	7.76	.0693	.0202	-.0586	-.0175	.0791	-.1825
26	40	623.74	11.90	7.94	.0730	.0195	-.0606	-.0196	.0897	-.2130
26	49	623.52	-3.99	11.99	.1084	.0233	-.0909	.0073	-.0291	.0645
26	50	623.95	-1.99	12.01	.1099	.0238	-.0937	.0035	-.0139	.0298
26	51	623.52	.00	12.01	.1122	.0240	-.0986	-.0008	.0019	-.0052
26	52	623.52	1.99	11.99	.1085	.0236	-.0924	-.0051	.0178	-.0406
26	53	623.74	4.00	12.00	.1086	.0223	-.0921	-.0086	.0323	-.0742
26	54	623.52	5.98	11.98	.1099	.0211	-.0922	-.0114	.0460	-.1076
26	55	623.52	7.97	11.95	.1119	.0204	-.0928	-.0144	.0600	-.1421
26	57	623.52	9.94	11.96	.1163	.0195	-.0975	-.0171	.0739	-.1774
27	28	624.17	-3.96	.00	-.0773	.0331	.1284	.0057	-.0258	.0608
27	27	624.39	-2.98	.00	-.0777	.0331	.1291	.0041	-.0187	.0444
27	26	624.39	-1.98	.00	-.0783	.0329	.1295	.0027	-.0120	.0296
27	25	624.17	-1.00	.00	-.0789	.0320	.1305	.0013	-.0060	.0150
27	24	624.17	.00	.00	-.0795	.0317	.1308	.0001	.0004	.0003
27	23	624.17	.98	.00	-.0789	.0321	.1303	-.0015	.0066	-.0136
27	22	624.60	1.97	.00	-.0781	.0319	.1295	-.0029	.0129	-.0290
27	21	624.17	2.97	.00	-.0778	.0328	.1282	-.0042	.0188	-.0422
27	20	624.17	3.95	.00	-.0756	.0330	.1269	-.0057	.0256	-.0585
27	19	624.60	5.92	.01	-.0742	.0320	.1239	-.0086	.0393	-.0903
27	18	624.60	7.92	.00	-.0716	.0308	.1195	-.0114	.0537	-.1246
27	17	624.17	9.88	.00	-.0676	.0296	.1137	-.0143	.0680	-.1596
27	16	624.60	11.87	.00	-.0650	.0281	.1074	-.0170	.0819	-.1958
27	15	624.39	13.86	.00	-.0617	.0270	.1010	-.0193	.0918	-.2270
27	29	624.17	-4.02	4.01	-.0343	.0288	.0830	.0052	-.0243	.0565
27	30	624.39	-2.02	4.03	-.0377	.0291	.0854	.0023	-.0109	.0252
27	31	624.82	.00	4.08	-.0396	.0288	.0872	-.0005	.0016	-.0031
27	32	623.74	2.01	4.05	-.0399	.0287	.0881	-.0032	.0138	-.0320
27	33	623.74	4.01	4.01	-.0397	.0288	.0889	-.0060	.0264	-.0613
27	34	624.17	5.97	3.99	-.0380	.0278	.0897	-.0088	.0398	-.0922
27	35	623.09	7.96	3.98	-.0332	.0263	.0775	-.0119	.0546	-.1272
27	36	624.82	9.96	3.98	-.0278	.0252	.0711	-.0149	.0694	-.1634
27	37	624.17	11.94	4.00	-.0230	.0241	.0654	-.0178	.0836	-.2006
27	38	623.74	13.88	4.00	-.0193	.0228	.0607	-.0200	.0937	-.2313
27	47	624.17	-4.03	8.04	.0122	.0238	.0326	.0056	-.0249	.0575
27	46	623.95	-2.02	8.07	.0078	.0244	.0367	.0026	-.0118	.0271
27	45	624.60	.00	8.06	.0071	.0247	.0383	-.0005	.0014	-.0029
27	44	623.74	2.02	8.06	.0086	.0245	.0366	-.0035	.0143	-.0328
27	43	624.17	4.03	8.04	.0098	.0238	.0346	-.0065	.0272	-.0630
27	42	624.17	6.01	8.01	.0129	.0226	.0302	-.0096	.0415	-.0964
27	41	624.17	7.97	8.00	.0169	.0213	.0257	-.0125	.0555	-.1304
27	40	624.39	10.11	7.79	.0197	.0200	.0233	-.0158	.0713	-.1703
27	39	624.39	11.94	7.97	.0244	.0188	.0184	-.0181	.0819	-.2000
27	48	623.74	-4.02	12.06	.0604	.0199	-.0120	.0062	-.0251	.0578
27	49	624.17	-2.00	12.06	.0555	.0207	-.0069	.0027	-.0117	.0265
27	50	624.39	-.02	12.07	.0532	.0208	-.0042	-.0006	.0015	-.0042
27	51	623.95	2.00	12.06	.0573	.0206	-.0090	-.0041	.0149	-.0351
27	52	624.17	4.01	12.05	.0593	.0191	-.0124	-.0075	.0277	-.0660
27	53	624.17	6.02	12.04	.0605	.0182	-.0126	-.0102	.0406	-.0976
27	54	624.17	7.99	12.03	.0647	.0170	-.0170	-.0132	.0540	-.1319
27	55	623.74	9.95	11.98	.0729	.0157	-.0260	-.0159	.0675	-.1671

TABLE V - Continued
 AERODYNAMIC CHARACTERISTICS IN SIDESLIP FOR VARIOUS ANGLES OF ATTACK.

BODY AXES; M = 1.41

Run	Pt.	q	β , deg	α , deg	C_N	C_A	C_m	C_l	C_n	C_y
28	28	623.52	-3.93	.00	-.0671	.0298	.1066	.0029	-.0342	.0733
28	27	623.30	-2.97	.00	-.0669	.0300	.1064	.0022	-.0263	.0567
28	26	623.30	-1.97	.00	-.0664	.0301	.1064	.0014	-.0172	.0376
28	25	623.52	-1.00	.00	-.0674	.0301	.1069	.0006	-.0087	.0202
28	24	623.30	.00	.00	-.0670	.0302	.1068	-.0001	-.0001	.0013
28	23	623.30	.97	.00	-.0679	.0302	.1068	-.0009	.0084	-.0162
28	21	623.52	1.96	.00	-.0662	.0299	.1055	-.0017	.0168	-.0343
28	22	623.30	2.95	.00	-.0659	.0296	.1046	-.0025	.0252	-.0525
28	20	623.30	3.92	-.01	-.0655	.0302	.1047	-.0033	.0339	-.0708
28	19	623.30	5.89	.00	-.0645	.0296	.1041	-.0049	.0515	-.1087
28	18	623.52	7.86	.00	-.0635	.0288	.1030	-.0067	.0685	-.1465
28	17	623.30	9.84	.00	-.0647	.0280	.1040	-.0086	.0857	-.1860
28	29	624.17	-3.99	3.99	-.0182	.0256	.0563	.0029	-.0303	.0655
28	30	623.74	-2.01	4.03	-.0190	.0257	.0549	.0012	-.0139	.0298
28	31	623.95	.00	4.06	-.0198	.0257	.0547	-.0004	.0019	-.0038
28	32	623.74	2.01	4.02	-.0213	.0252	.0552	-.0019	.0175	-.0372
28	33	623.95	3.98	3.98	-.0233	.0256	.0571	-.0034	.0331	-.0707
28	34	623.74	5.95	3.96	-.0247	.0255	.0587	-.0051	.0493	-.1061
28	35	623.74	7.93	3.95	-.0239	.0248	.0599	-.0071	.0657	-.1436
28	36	624.17	9.92	3.96	-.0253	.0239	.0633	-.0090	.0822	-.1819
28	45	623.52	-4.04	8.02	.0282	.0214	.0077	.0034	-.0267	.0603
28	44	621.79	-2.02	8.05	.0265	.0226	.0083	.0015	-.0125	.0283
28	43	622.44	.00	8.05	.0245	.0227	.0088	-.0004	.0014	-.0027
28	42	623.95	2.01	8.02	.0249	.0224	.0081	-.0023	.0153	-.0336
28	41	623.95	4.00	8.02	.0264	.0212	.0067	-.0041	.0293	-.0662
28	40	623.95	5.98	7.99	.0261	.0210	.0079	-.0059	.0441	-.0998
28	39	624.39	7.98	7.98	.0259	.0203	.0104	-.0077	.0595	-.1356
28	38	623.09	10.08	7.79	.0216	.0195	.0177	-.0097	.0762	-.1752
28	37	624.17	11.91	7.98	.0205	.0192	.0240	-.0114	.0890	-.2096
28	46	623.52	-4.04	12.05	.0760	.0184	-.0347	.0035	-.0223	.0528
28	47	623.74	-2.00	12.04	.0746	.0194	-.0344	.0015	-.0103	.0241
28	48	624.39	.00	12.05	.0731	.0195	-.0350	-.0005	.0013	-.0032
28	49	623.95	2.00	12.04	.0733	.0189	-.0348	-.0024	.0131	-.0316
28	50	623.74	3.99	12.06	.0742	.0178	-.0355	-.0044	.0251	-.0609
28	51	624.17	5.98	12.03	.0757	.0166	-.0357	-.0061	.0381	-.0924
28	52	623.95	8.00	11.99	.0745	.0159	-.0317	-.0080	.0521	-.1277
28	53	623.52	9.99	11.98	.0740	.0158	-.0261	-.0101	.0658	-.1622
29	23	622.87	-3.94	.00	-.0055	.0244	.0161	.0034	-.0310	.0680
29	22	623.30	-1.98	.00	-.0048	.0246	.0142	.0016	-.0154	.0341
29	21	623.09	-.98	.00	-.0045	.0244	.0133	.0008	-.0078	.0176
29	20	622.87	.00	.00	-.0041	.0243	.0127	-.0002	-.0001	.0011
29	19	622.87	.98	.00	-.0051	.0243	.0128	-.0011	.0077	-.0154
29	18	622.87	1.96	.00	-.0046	.0242	.0129	-.0020	.0152	-.0320
29	17	623.09	3.93	.00	-.0065	.0244	.0141	-.0037	.0303	-.0651
29	16	622.87	5.90	.01	-.0079	.0237	.0171	-.0054	.0466	-.1013
29	15	622.87	7.89	.00	-.0095	.0230	.0190	-.0072	.0622	-.1368
29	14	623.30	9.86	.00	-.0121	.0221	.0221	-.0090	.0776	-.1735
29	13	623.09	11.85	.00	-.0169	.0213	.0288	-.0109	.0929	-.2119
29	24	623.09	-3.96	3.96	.0445	.0244	-.0357	.0036	-.0269	.0603
29	25	623.30	-1.99	3.98	.0414	.0244	-.0343	.0015	-.0120	.0270
29	26	623.30	.00	3.99	.0394	.0238	-.0342	-.0004	.0019	-.0040
29	27	623.30	1.98	3.97	.0379	.0237	-.0348	-.0023	.0157	-.0348
29	28	622.22	3.94	3.94	.0360	.0238	-.0343	-.0042	.0294	-.0660
29	29	623.09	5.94	3.95	.0372	.0233	-.0345	-.0061	.0438	-.0987
29	30	623.52	7.93	3.96	.0377	.0227	-.0337	-.0081	.0585	-.1336
29	31	623.09	9.92	3.98	.0350	.0214	-.0290	-.0100	.0732	-.1695
29	32	623.30	11.90	3.96	.0321	.0207	-.0219	-.0120	.0879	-.2061
29	41	623.74	-4.01	7.97	.0846	.0240	-.0799	.0039	-.0243	.0567
29	40	623.09	-2.00	7.98	.0830	.0250	-.0795	.0018	-.0114	.0263
29	39	623.09	.00	7.97	.0824	.0248	-.0794	-.0004	.0013	-.0029
29	38	623.09	2.00	7.97	.0830	.0243	-.0801	-.0025	.0143	-.0329
29	37	623.30	3.99	7.96	.0832	.0237	-.0808	-.0045	.0269	-.0631
29	36	623.09	5.96	7.95	.0829	.0227	-.0805	-.0064	.0402	-.0943
29	35	623.09	7.94	7.94	.0839	.0216	-.0793	-.0085	.0540	-.1277
29	34	623.09	10.07	7.76	.0808	.0207	-.0742	-.0107	.0690	-.1653
29	33	623.09	11.93	7.96	.0807	.0200	-.0693	-.0125	.0797	-.1959
29	42	621.58	-3.99	11.99	.1291	.0236	-.1205	.0037	-.0207	.0503
29	43	622.44	-1.99	11.98	.1287	.0246	-.1212	.0016	-.0096	.0231
29	44	624.39	.00	12.00	.1285	.0247	-.1214	-.0005	.0016	-.0042
29	45	627.00	1.99	11.97	.1280	.0241	-.1216	-.0026	.0127	-.0316
29	46	624.17	3.99	11.98	.1294	.0230	-.1223	-.0046	.0235	-.0579
29	47	623.74	5.98	11.97	.1298	.0214	-.1224	-.0065	.0353	-.0886
29	48	624.60	7.98	11.96	.1308	.0209	-.1207	-.0087	.0470	-.1202
29	49	625.25	9.97	11.95	.1302	.0208	-.1151	-.0108	.0608	-.1553

TABLE V - Concluded
 AERODYNAMIC CHARACTERISTICS IN SIDESLIP FOR VARIOUS ANGLES OF ATTACK.
 BODY AXES: M = 1.41

Run	Pt.	q	β ,deg	α ,deg	C_N	C_A	C_m	C_l	C_n	C_Y
30	26	623.95	-3.95	.01	-.0067	.0221	.0117	.0051	-.0254	.0585
30	25	623.74	-1.98	.00	-.0056	.0223	.0107	.0026	-.0123	.0290
30	24	623.95	-.49	.00	-.0050	.0221	.0102	.0012	-.0058	.0142
30	23	623.95	.00	.00	-.0056	.0219	.0102	-.0001	.0007	-.0013
30	22	623.30	.99	.00	-.0051	.0220	.0101	-.0014	.0072	-.0154
30	21	622.87	1.98	.00	-.0057	.0222	.0103	-.0027	.0137	-.0310
30	20	623.95	3.93	.00	-.0057	.0222	.0106	-.0053	.0269	-.0613
30	19	622.01	5.91	.00	-.0045	.0220	.0101	-.0079	.0407	-.0928
30	18	623.95	7.91	.00	-.0045	.0212	.0088	-.0103	.0551	-.1269
30	17	621.36	9.88	.00	-.0045	.0201	.0080	-.0128	.0693	-.1611
30	16	624.82	11.88	.02	-.0041	.0194	.0078	-.0152	.0830	-.1966
30	15	622.87	13.86	.02	-.0041	.0187	.0076	-.0175	.0955	-.2319
30	27	624.82	-3.99	3.99	.0025	.0219	.0246	.0045	-.0241	.0547
30	28	623.95	-2.00	4.01	.0022	.0220	.0239	.0020	-.0108	.0241
30	29	624.82	.00	4.03	.0017	.0219	.0227	-.0006	.0019	-.0051
30	30	624.60	2.00	4.01	.0005	.0217	.0220	-.0030	.0144	-.0333
30	31	622.87	3.98	3.98	.0014	.0215	.0211	-.0054	.0273	-.0627
30	32	623.95	5.95	3.96	.0014	.0214	.0204	-.0077	.0405	-.0937
30	33	623.09	7.94	3.98	.0034	.0205	.0186	-.0102	.0548	-.1278
30	34	624.60	9.93	3.96	.0059	.0195	.0168	-.0127	.0690	-.1625
30	35	623.74	11.92	3.97	.0066	.0188	.0159	-.0151	.0828	-.1983
30	36	624.17	13.88	3.97	.0080	.0177	.0161	-.0170	.0934	-.2303
30	46	624.39	-4.03	8.05	.0140	.0214	.0330	.0044	-.0234	.0549
30	45	624.39	-2.02	8.07	.0138	.0224	.0324	.0020	-.0105	.0246
30	44	623.95	-.01	8.05	.0119	.0222	.0319	-.0006	.0017	-.0036
30	43	624.60	2.02	8.07	.0141	.0219	.0310	-.0030	.0138	-.0326
30	42	624.17	4.01	8.04	.0144	.0213	.0302	-.0052	.0259	-.0611
30	41	624.17	6.00	8.00	.0157	.0203	.0288	-.0076	.0394	-.0937
30	40	624.17	8.00	8.00	.0166	.0197	.0271	-.0099	.0526	-.1254
30	39	624.39	10.12	7.79	.0184	.0185	.0248	-.0125	.0676	-.1628
30	38	623.74	11.94	7.97	.0221	.0180	.0250	-.0144	.0788	-.1943
30	37	623.74	13.92	7.95	.0247	.0173	.0235	-.0168	.0916	-.2299
30	48	623.95	-4.05	12.10	.0314	.0210	.0406	.0041	-.0204	.0503
30	49	623.95	-2.01	12.11	.0290	.0224	.0418	.0017	-.0093	.0219
30	50	623.74	-.02	12.14	.0293	.0225	.0412	-.0006	.0016	-.0045
30	51	623.74	1.99	12.10	.0294	.0219	.0404	-.0029	.0123	-.0311
30	52	623.74	4.01	12.11	.0318	.0207	.0377	-.0052	.0237	-.0594
30	53	623.74	6.03	12.07	.0335	.0195	.0361	-.0074	.0356	-.0901
30	54	623.74	8.04	12.06	.0347	.0185	.0367	-.0097	.0486	-.1228
30	55	624.17	10.03	12.02	.0391	.0178	.0345	-.0120	.0615	-.1569

TABLE VI
AERODYNAMIC CHARACTERISTICS IN SIDESLIP FOR VARIOUS ANGLES OF ATTACK.
BODY AXES; M = 2.01

Run	Pl.	q	β , deg	α , deg	C_N	C_A	C_m	C_l	C_n	C_y
39	35	511.11	.00	.00	.0078	.0220	.0164	.0002	-.0012	.0015
39	34	510.93	.99	.00	.0075	.0221	.0163	-.0007	.0029	-.0093
39	33	511.11	1.99	.00	.0091	.0219	.0158	-.0017	.0073	-.0212
39	32	511.11	2.97	.00	.0106	.0221	.0151	-.0027	.0114	-.0321
39	31	510.40	3.96	.00	.0105	.0217	.0146	-.0037	.0159	-.0449
39	30	510.40	5.97	.01	.0134	.0214	.0124	-.0056	.0245	-.0687
39	29	510.76	8.01	.00	.0150	.0210	.0100	-.0077	.0340	-.0960
39	28	510.93	10.00	.00	.0181	.0202	.0068	-.0097	.0428	-.1233
39	27	510.58	12.01	.00	.0200	.0200	.0040	-.0118	.0513	-.1534
39	26	510.58	14.00	-.02	.0222	.0193	.0004	-.0140	.0598	-.1898
39	25	510.58	16.01	.00	.0243	.0186	-.0038	-.0160	.0676	-.2259
39	24	510.76	18.04	.00	.0281	.0175	-.0092	-.0181	.0757	-.2630
39	23	510.76	20.03	.00	.0301	.0172	-.0149	-.0200	.0845	-.3021
39	22	510.58	22.07	.00	.0336	.0174	-.0216	-.0217	.0937	-.3414
39	21	510.93	24.11	.00	.0371	.0174	-.0287	-.0234	.1033	-.3814
39	20	510.58	26.10	.00	.0422	.0172	-.0366	-.0252	.1134	-.4219
39	19	510.40	28.11	.00	.0473	.0174	-.0456	-.0271	.1221	-.4621
39	36	510.76	.00	4.03	.0350	.0219	.0008	.0000	-.0001	-.0010
39	37	510.76	2.00	4.01	.0335	.0223	-.0004	-.0018	.0076	-.0231
39	38	510.76	4.01	4.01	.0344	.0216	-.0031	-.0036	.0157	-.0456
39	39	510.76	6.01	4.00	.0359	.0207	-.0070	-.0056	.0246	-.0703
39	40	510.93	8.03	4.01	.0382	.0200	-.0102	-.0077	.0334	-.0964
39	41	510.58	10.02	4.00	.0427	.0197	-.0136	-.0098	.0421	-.1238
39	42	510.76	12.05	4.01	.0470	.0190	-.0186	-.0121	.0509	-.1565
39	43	510.93	14.03	4.01	.0512	.0183	-.0220	-.0142	.0594	-.1920
39	44	510.76	16.02	4.03	.0552	.0176	-.0254	-.0161	.0667	-.2260
39	45	511.11	18.05	3.99	.0589	.0165	-.0298	-.0180	.0744	-.2625
39	46	510.40	20.05	4.02	.0661	.0159	-.0369	-.0200	.0835	-.3012
39	47	510.76	22.09	3.97	.0713	.0161	-.0441	-.0219	.0934	-.3404
39	48	510.76	24.14	4.01	.0781	.0162	-.0533	-.0236	.1036	-.3814
39	61	510.58	.00	8.08	.0675	.0228	-.0230	.0001	-.0001	-.0009
39	60	510.58	2.02	8.07	.0683	.0224	-.0244	-.0017	.0075	-.0230
39	59	510.40	4.03	8.05	.0706	.0214	-.0268	-.0037	.0154	-.0465
39	58	510.76	6.02	8.06	.0737	.0203	-.0292	-.0058	.0239	-.0709
39	57	510.58	8.04	8.04	.0766	.0200	-.0324	-.0079	.0324	-.0973
39	56	510.58	10.19	7.85	.0837	.0193	-.0386	-.0102	.0413	-.1285
39	55	510.58	12.02	8.02	.0936	.0181	-.0439	-.0123	.0491	-.1592
39	54	510.93	14.03	8.01	.0988	.0174	-.0467	-.0145	.0574	-.1928
39	53	510.76	16.03	8.01	.1053	.0169	-.0508	-.0165	.0653	-.2279
39	52	510.58	18.05	8.02	.1095	.0162	-.0554	-.0182	.0733	-.2635
39	51	510.76	20.08	8.02	.1150	.0155	-.0626	-.0201	.0825	-.3008
39	50	510.93	22.13	8.05	.1223	.0154	-.0713	-.0222	.0927	-.3407
39	49	510.76	24.10	8.02	.1262	.0151	-.0775	-.0239	.1024	-.3796
39	62	511.11	.00	12.10	.1068	.0228	-.0432	.0001	-.0002	-.0008
39	63	510.58	2.01	12.09	.1071	.0219	-.0460	-.0016	.0063	-.0229
39	64	510.40	4.02	12.08	.1102	.0211	-.0510	-.0036	.0134	-.0461
39	65	510.58	6.02	12.05	.1143	.0197	-.0536	-.0058	.0210	-.0712
39	66	510.76	8.04	12.06	.1192	.0188	-.0567	-.0081	.0290	-.0986
39	67	510.76	10.04	12.04	.1267	.0183	-.0610	-.0105	.0377	-.1308
39	68	510.93	12.05	12.05	.1333	.0175	-.0653	-.0128	.0463	-.1629
39	69	510.76	14.03	12.04	.1392	.0166	-.0695	-.0149	.0551	-.1966
39	70	510.58	16.05	12.01	.1464	.0160	-.0758	-.0171	.0646	-.2322
39	71	510.76	18.07	12.05	.1544	.0158	-.0819	-.0190	.0735	-.2681
39	72	510.76	20.08	12.06	.1602	.0156	-.0882	-.0205	.0817	-.3028
39	73	510.76	22.18	12.07	.1662	.0149	-.0946	-.0223	.0911	-.3412
39	74	510.58	24.72	12.38	.1778	.0149	-.1032	-.0243	.1031	-.3910
39	87	510.40	-.03	16.13	.1618	.0224	-.0592	.0001	-.0002	-.0009
39	86	510.58	1.98	16.15	.1632	.0227	-.0618	-.0015	.0053	-.0224
39	85	510.58	4.03	16.14	.1706	.0203	-.0732	-.0032	.0107	-.0454
39	84	510.58	6.03	16.11	.1782	.0182	-.0836	-.0057	.0183	-.0722
39	83	510.58	8.02	16.11	.1818	.0173	-.0846	-.0084	.0272	-.1033
39	82	510.58	10.07	16.11	.1861	.0166	-.0877	-.0109	.0360	-.1338
39	81	510.58	12.07	16.07	.1931	.0159	-.0931	-.0134	.0453	-.1672
39	80	510.76	14.06	16.08	.1979	.0154	-.0966	-.0158	.0548	-.2015
39	79	510.76	16.10	16.10	.2023	.0150	-.0987	-.0179	.0635	-.2356
39	78	510.58	18.12	16.09	.2057	.0152	-.1023	-.0194	.0712	-.2686
39	76	510.76	20.14	16.10	.2099	.0144	-.1086	-.0206	.0794	-.3032
39	75	510.76	22.19	16.10	.2142	.0141	-.1143	-.0219	.0881	-.3397
39	88	511.46	-.04	20.16	.2136	.0213	-.0670	.0002	-.0003	-.0000
39	89	510.23	1.99	20.17	.2159	.0204	-.0708	-.0011	.0039	-.0220
39	90	510.76	4.04	20.15	.2238	.0187	-.0843	-.0031	.0097	-.0475
39	91	510.40	6.04	20.16	.2306	.0172	-.0935	-.0052	.0163	-.0735
39	92	510.58	8.05	20.14	.2359	.0163	-.1022	-.0079	.0252	-.1040
39	93	510.93	10.11	20.17	.2415	.0151	-.1064	-.0106	.0339	-.1355
39	94	509.69	12.11	20.17	.2426	.0143	-.1064	-.0129	.0421	-.1676
39	95	511.29	14.11	20.16	.2454	.0143	-.1067	-.0153	.0506	-.2007
39	96	511.29	16.12	20.17	.2468	.0138	-.1065	-.0174	.0592	-.2334
39	97	511.11	18.12	20.17	.2491	.0139	-.1079	-.0191	.0670	-.2661
39	98	509.34	20.04	20.04	.2530	.0136	-.1126	-.0205	.0753	-.2989
39	106	510.76	.00	24.27	.2690	.0201	-.0824	.0001	-.0007	-.0009
39	105	510.76	2.03	24.30	.2714	.0193	-.0867	-.0011	.0027	-.0208
39	104	510.93	4.04	24.30	.2785	.0177	-.0969	-.0027	.0078	-.0459
39	103	510.58	6.07	24.26	.2834	.0161	-.1033	-.0047	.0141	-.0725
39	102	510.40	8.07	24.22	.2867	.0150	-.1101	-.0071	.0220	-.1024
39	101	510.76	10.04	24.21	.2913	.0139	-.1160	-.0095	.0307	-.1334
39	100	511.29	12.13	24.26	.2942	.0134	-.1195	-.0116	.0393	-.1664
39	99	510.58	14.13	24.17	.2948	.0132	-.1196	-.0140	.0487	-.2001

TABLE VI - Continued
 AERODYNAMIC CHARACTERISTICS IN SIDESLIP FOR VARIOUS ANGLES OF ATTACK.

BODY AXES; M = 2.01

Run	Pl.	q	β ,deg	α ,deg	C_N	C_A	C_m	C_l	C_n	C_y
40	32	509.16	.01	.00	-.0247	.0242	.0747	.0001	-.0014	.0022
40	31	508.45	.99	.00	-.0250	.0244	.0746	-.0008	.0028	-.0087
40	30	508.81	1.99	.00	-.0234	.0247	.0742	-.0018	.0071	-.0296
40	29	508.99	3.97	.00	-.0237	.0249	.0735	-.0037	.0154	-.0434
40	28	508.45	5.97	.00	-.0208	.0243	.0713	-.0056	.0242	-.0681
40	27	509.16	8.00	.00	-.0195	.0234	.0686	-.0075	.0333	-.0936
40	26	508.63	10.01	.02	-.0164	.0232	.0649	-.0095	.0418	-.1210
40	25	508.81	12.01	.02	-.0149	.0223	.0611	-.0114	.0498	-.1509
40	24	508.63	13.89	.02	-.0130	.0216	.0572	-.0132	.0577	-.1854
40	23	508.63	16.02	.00	-.0109	.0204	.0525	-.0153	.0655	-.2227
40	22	508.81	18.03	.00	-.0074	.0192	.0471	-.0171	.0731	-.2589
40	21	508.81	20.03	.00	-.0040	.0185	.0411	-.0187	.0816	-.2971
40	20	508.81	22.08	.00	-.0008	.0181	.0350	-.0201	.0903	-.3354
40	19	508.81	24.10	.00	.0024	.0178	.0283	-.0215	.0992	-.3747
40	18	508.63	26.12	.00	.0057	.0172	.0217	-.0229	.1086	-.4142
40	17	508.81	28.11	.00	.0077	.0176	.0163	-.0245	.1184	-.4553
40	33	508.81	.00	4.06	.0040	.0230	.0563	.0000	-.0002	-.0013
40	34	508.63	2.01	4.03	.0023	.0225	.0555	-.0016	.0072	-.0224
40	35	508.63	4.03	4.03	.0032	.0220	.0525	-.0034	.0151	-.0448
40	36	508.63	6.03	4.01	.0047	.0216	.0490	-.0054	.0238	-.0693
40	37	508.81	8.03	4.01	.0084	.0203	.0447	-.0074	.0325	-.0954
40	38	508.99	10.04	4.01	.0094	.0196	.0417	-.0093	.0406	-.1216
40	39	508.81	12.07	4.02	.0150	.0193	.0362	-.0113	.0487	-.1524
40	40	508.81	14.04	4.02	.0207	.0181	.0314	-.0133	.0568	-.1880
40	41	508.99	16.04	4.01	.0260	.0173	.0267	-.0151	.0637	-.2220
40	42	508.81	18.07	4.00	.0310	.0157	.0207	-.0166	.0706	-.2567
40	43	508.99	20.06	4.06	.0376	.0150	.0133	-.0183	.0789	-.2938
40	44	509.16	22.12	3.97	.0411	.0144	.0070	-.0198	.0883	-.3332
40	45	508.99	24.16	4.02	.0460	.0142	-.0001	-.0213	.0975	-.3724
40	56	509.16	.00	8.13	.0349	.0209	.0320	.0000	-.0002	-.0012
40	55	508.63	2.03	8.11	.0356	.0205	.0313	-.0016	.0070	-.0224
40	54	508.63	4.05	8.08	.0361	.0196	.0295	-.0035	.0145	-.0449
40	53	508.63	6.05	8.05	.0434	.0183	.0225	-.0074	.0306	-.0945
40	52	508.81	12.05	8.04	.0600	.0160	.0098	-.0114	.0462	-.1561
40	51	508.81	14.04	8.02	.0664	.0151	.0052	-.0133	.0537	-.1879
40	50	508.63	16.05	8.02	.0740	.0144	-.0011	-.0150	.0608	-.2219
40	49	508.81	18.08	8.04	.0793	.0134	-.0072	-.0165	.0675	-.2544
40	48	508.63	20.10	8.03	.0861	.0125	-.0146	-.0178	.0754	-.2908
40	47	508.63	22.15	8.06	.0932	.0115	-.0222	-.0196	.0847	-.3288
40	46	508.81	24.13	8.03	.0968	.0109	-.0275	-.0210	.0941	-.3676
40	57	508.99	.00	12.12	.0729	.0194	.0124	.0001	-.0003	-.0012
40	58	508.63	2.01	12.13	.0746	.0189	.0097	-.0015	.0055	-.0221
40	59	508.81	4.03	12.11	.0790	.0175	.0043	-.0033	.0120	-.0444
40	60	508.81	6.06	12.07	.0894	.0148	-.0027	-.0075	.0262	-.0957
40	62	508.63	12.08	12.08	.1042	.0136	-.0142	-.0115	.0417	-.1570
40	63	508.81	16.09	12.04	.1194	.0116	-.0271	-.0151	.0569	-.2219
40	64	508.81	19.24	11.52	.1215	.0111	-.0333	-.0171	.0687	-.2733
40	65	508.99	24.74	12.39	.1527	.0085	-.0622	-.0215	.0951	-.3789
40	73	508.99	.00	16.14	.1293	.0180	-.0063	.0001	-.0002	-.0012
40	72	508.99	2.01	16.18	.1321	.0177	-.0093	-.0012	.0040	-.0206
40	71	508.99	4.01	16.17	.1374	.0154	-.0195	-.0027	.0077	-.0406
40	70	508.99	6.03	16.14	.1479	.0125	-.0305	-.0072	.0216	-.0943
40	69	508.99	12.10	16.11	.1600	.0103	-.0395	-.0114	.0370	-.1550
40	68	509.16	16.13	16.13	.1712	.0086	-.0519	-.0153	.0535	-.2203
40	67	508.81	20.18	16.13	.1868	.0074	-.0696	-.0182	.0710	-.2903
40	66	508.99	22.19	16.16	.1940	.0071	-.0791	-.0194	.0805	-.3278
40	74	508.99	.00	20.19	.1888	.0155	-.0266	.0001	-.0004	-.0003
40	75	509.16	1.99	20.20	.1915	.0146	-.0306	-.0007	.0015	-.0191
40	76	508.99	4.05	20.19	.1975	.0125	-.0414	-.0021	.0045	-.0394
40	77	508.99	8.07	20.18	.2091	.0095	-.0569	-.0062	.0172	-.0917
40	78	508.99	12.12	20.19	.2162	.0073	-.0642	-.0108	.0333	-.1531
40	79	508.99	16.14	20.19	.2257	.0062	-.0721	-.0155	.0518	-.2218
40	80	508.99	20.07	20.07	.2325	.0061	-.0808	-.0187	.0682	-.2882
40	86	508.99	.00	24.28	.2481	.0135	-.0485	.0003	-.0011	.0008
40	85	508.81	1.99	24.33	.2513	.0124	-.0536	-.0002	-.0006	-.0158
40	84	508.81	4.04	24.32	.2564	.0100	-.0634	-.0014	.0024	-.0368
40	83	508.81	8.07	24.23	.2571	.0071	-.0800	-.0056	.0160	-.0923
40	82	508.99	12.14	24.29	.2766	.0054	-.0901	-.0100	.0326	-.1565
40	81	508.99	14.11	24.22	.2781	.0048	-.0916	-.0124	.0418	-.1891

TABLE VI - Continued
 AERODYNAMIC CHARACTERISTICS IN SIDESLIP FOR VARIOUS ANGLES OF ATTACK.
 BODY AXES; M = 2.01

Run	Pt.	q	β , deg	α , deg	C_N	C_A	C_m	C_l	C_n	C_y
41	21	509.34	.00	.00	-.0118	.0241	.0511	.0001	-.0013	.0022
41	20	509.16	1.99	.00	-.0123	.0252	.0519	-.0012	.0087	-.0227
41	19	508.99	3.96	.00	-.0112	.0249	.0524	-.0025	.0188	-.0486
41	18	509.16	5.96	.00	-.0118	.0241	.0530	-.0038	.0287	-.0744
41	17	509.16	8.00	.00	-.0120	.0236	.0541	-.0052	.0393	-.1031
41	16	509.16	11.98	.00	-.0154	.0234	.0597	-.0076	.0585	-.1637
41	15	509.16	15.98	.03	-.0223	.0229	.0712	-.0096	.0767	-.2385
41	14	509.34	19.99	.00	-.0322	.0222	.0843	-.0117	.0950	-.3162
41	13	508.99	24.07	.00	-.0394	.0225	.0953	-.0135	.1105	-.3907
41	12	508.99	28.12	.00	-.0471	.0241	.1042	-.0155	.1180	-.4561
41	22	509.34	.00	4.05	.0166	.0224	.0321	.0000	.0000	-.0012
41	23	509.52	2.01	4.03	.0154	.0219	.0324	-.0011	.0084	-.0235
41	24	509.69	4.01	4.01	.0135	.0219	.0333	-.0024	.0176	-.0472
41	25	509.34	8.02	4.00	.0126	.0209	.0352	-.0051	.0367	-.1003
41	26	509.34	12.05	4.01	.0146	.0203	.0388	-.0077	.0549	-.1606
41	27	509.34	16.01	4.00	.0129	.0200	.0482	-.0097	.0717	-.2324
41	28	509.52	20.03	4.01	.0096	.0194	.0611	-.0115	.0884	-.3065
41	29	509.52	24.14	4.01	.0017	.0205	.0742	-.0135	.1088	-.3880
41	37	509.87	.00	8.10	.0448	.0207	.0146	.0000	.0000	-.0012
41	36	509.69	2.03	8.10	.0456	.0198	.0146	-.0012	.0079	-.0234
41	35	509.69	4.05	8.08	.0462	.0188	.0140	-.0025	.0160	-.0469
41	34	509.34	8.04	8.04	.0487	.0181	.0147	-.0049	.0333	-.0979
41	33	509.69	12.04	8.03	.0572	.0173	.0153	-.0073	.0501	-.1598
41	32	509.52	16.05	8.02	.0589	.0170	.0249	-.0094	.0656	-.2268
41	31	509.69	20.10	8.03	.0562	.0172	.0372	-.0111	.0813	-.2976
41	30	509.52	24.12	8.03	.0505	.0178	.0497	-.0132	.1013	-.3767
41	38	509.52	.00	12.12	.0828	.0187	-.0040	.0000	-.0002	-.0002
41	39	509.69	4.03	12.11	.0858	.0168	-.0062	-.0023	.0123	-.0434
41	40	509.69	8.03	12.09	.0924	.0150	-.0076	-.0047	.0273	-.0958
41	41	509.52	12.06	12.10	.0991	.0148	-.0049	-.0068	.0434	-.1573
41	42	509.52	16.07	12.07	.1021	.0147	.0028	-.0090	.0587	-.2223
41	43	510.05	20.12	12.12	.1016	.0152	.0128	-.0105	.0739	-.2897
41	44	509.52	24.76	12.40	.1010	.0160	.0246	-.0129	.0960	-.3784
41	52	509.87	.00	16.14	.1390	.0171	-.0232	.0001	-.0003	-.0002
41	51	509.69	2.01	16.17	.1416	.0161	-.0250	-.0006	.0035	-.0195
41	50	509.52	4.04	16.16	.1440	.0144	-.0292	-.0015	.0074	-.0395
41	49	509.52	8.06	16.13	.1507	.0124	-.0328	-.0041	.0211	-.0924
41	48	509.87	12.12	16.13	.1541	.0121	-.0282	-.0061	.0363	-.1520
41	47	509.69	16.16	16.16	.1561	.0121	-.0220	-.0082	.0518	-.2163
41	46	509.69	20.21	16.15	.1533	.0123	-.0123	-.0100	.0671	-.2821
41	45	510.05	22.26	16.16	.1534	.0135	-.0075	-.0110	.0763	-.3195
41	53	510.23	.00	20.17	.1983	.0150	-.0435	.0001	-.0003	-.0002
41	54	509.87	1.99	20.18	.1992	.0145	-.0458	.0000	.0005	-.0169
41	55	509.87	4.01	20.19	.2034	.0129	-.0507	-.0007	.0027	-.0343
41	56	510.05	7.96	20.02	.2051	.0104	-.0541	-.0032	.0147	-.0856
41	57	509.87	12.09	20.22	.2110	.0095	-.0534	-.0050	.0290	-.1456
41	58	509.87	16.15	20.21	.2116	.0097	-.0479	-.0073	.0452	-.2101
41	59	509.69	20.09	20.09	.2093	.0112	-.0399	-.0093	.0615	-.2757
41	65	509.69	.00	24.28	.2608	.0128	-.0683	.0002	-.0010	.0009
41	64	509.69	2.03	24.31	.2635	.0121	-.0717	.0006	-.0023	-.0135
41	63	509.69	4.04	24.32	.2666	.0104	-.0771	.0002	-.0007	-.0315
41	62	509.87	8.08	24.26	.2702	.0079	-.0821	-.0021	.0102	-.0827
41	61	509.87	12.15	24.31	.2722	.0071	-.0808	-.0041	.0242	-.1418
41	60	510.05	14.12	24.25	.2716	.0076	-.0784	-.0054	.0324	-.1731

TABLE VI - Continued
 AERODYNAMIC CHARACTERISTICS IN SIDESLIP FOR VARIOUS ANGLES OF ATTACK.
 BODY AXES; M = 2.01

Run	Pt.	q	β ,deg	α ,deg	C_N	C_A	C_m	C_l	C_n	C_Y
42	21	512.00	.00	.00	.0102	.0215	.0044	.0010	-.0012	.0016
42	20	511.82	.99	.00	.0099	.0216	.0043	.0003	.0034	-.0103
42	19	511.46	1.99	.00	.0112	.0220	.0042	-.0005	.0079	-.0221
42	18	511.11	2.96	.00	.0122	.0218	.0042	-.0019	.0167	-.0450
42	17	510.58	3.97	.00	.0119	.0214	.0045	-.0034	.0262	-.0707
42	16	512.35	8.00	.00	.0116	.0209	.0053	-.0048	.0356	-.0978
42	15	511.82	11.99	.00	.0083	.0195	.0096	-.0076	.0533	-.1561
42	14	512.17	16.00	.00	.0017	.0182	.0200	-.0103	.0700	-.2293
42	13	511.29	20.02	.00	-.0062	.0170	.0325	-.0130	.0870	-.3041
42	12	512.17	24.08	.00	-.0154	.0173	.0459	-.0154	.1062	-.3847
42	11	512.17	28.12	.05	-.0209	.0166	.0558	-.0175	.1186	-.4561
42	22	511.64	.00	4.01	.0384	.0222	-.0147	.0000	-.0001	-.0003
42	23	511.82	2.00	4.01	.0357	.0216	-.0144	-.0012	.0077	-.0230
42	24	511.64	4.00	4.00	.0353	.0212	-.0147	-.0023	.0162	-.0464
42	25	511.82	8.02	4.00	.0359	.0200	-.0144	-.0050	.0337	-.0962
42	26	511.64	12.05	4.01	.0381	.0188	-.0112	-.0078	.0507	-.1552
42	27	511.64	16.01	4.00	.0367	.0177	-.0025	-.0103	.0659	-.2246
42	28	511.82	20.04	4.05	.0337	.0160	.0092	-.0127	.0816	-.2972
42	29	511.64	24.16	4.02	.0278	.0165	.0218	-.0152	.1004	-.3764
42	37	512.17	.00	8.06	.0692	.0219	-.0367	.0000	-.0001	-.0008
42	36	512.53	2.00	8.05	.0684	.0215	-.0365	-.0012	.0071	-.0228
42	35	512.17	4.03	8.05	.0692	.0206	-.0369	-.0026	.0147	-.0452
42	34	512.00	8.03	8.03	.0735	.0189	-.0371	-.0051	.0310	-.0958
42	33	511.64	12.01	8.02	.0821	.0176	-.0364	-.0076	.0465	-.1555
42	32	512.35	16.05	8.02	.0824	.0169	-.0269	-.0101	.0610	-.2208
42	31	511.64	20.09	8.03	.0815	.0156	-.0171	-.0123	.0753	-.2896
42	30	511.82	24.13	8.03	.0776	.0154	-.0063	-.0148	.0936	-.3660
42	38	512.17	.00	12.07	.1100	.0222	-.0594	.0001	-.0002	-.0007
42	39	512.00	1.98	12.08	.1100	.0217	-.0601	-.0011	.0048	-.0196
42	40	512.00	4.02	12.08	.1115	.0202	-.0613	-.0024	.0112	-.0427
42	41	512.17	8.03	12.04	.1200	.0184	-.0627	-.0050	.0252	-.0938
42	42	512.35	12.06	12.06	.1252	.0173	-.0594	-.0074	.0404	-.1538
42	43	512.00	16.09	12.04	.1286	.0166	-.0519	-.0099	.0547	-.2176
42	44	512.17	20.13	12.08	.1283	.0157	-.0427	-.0118	.0686	-.2828
42	45	512.17	24.76	12.40	.1310	.0154	-.0341	-.0148	.0690	-.3686
42	53	511.11	-.03	16.10	.1706	.0223	-.0846	.0002	-.0003	-.0007
42	52	511.11	1.97	16.12	.1716	.0222	-.0860	-.0007	.0029	-.0189
42	51	510.93	4.03	16.13	.1760	.0202	-.0899	-.0017	.0064	-.0388
42	50	513.94	8.05	16.11	.1803	.0175	-.0921	-.0046	.0192	-.0900
42	49	512.35	12.10	16.10	.1830	.0162	-.0868	-.0069	.0334	-.1486
42	48	512.00	16.13	16.13	.1839	.0156	-.0790	-.0094	.0480	-.2117
42	47	512.17	20.19	16.13	.1843	.0152	-.0716	-.0115	.0623	-.2759
42	46	512.00	22.24	16.14	.1830	.0154	-.0679	-.0127	.0710	-.3124
42	54	511.11	.00	20.13	.2329	.0226	-.1091	.0002	-.0004	-.0006
42	55	511.29	2.02	20.13	.2337	.0215	-.1111	-.0001	.0001	-.0164
42	56	511.64	4.04	20.14	.2380	.0197	-.1165	-.0011	.0020	-.0346
42	57	511.82	8.05	20.13	.2433	.0172	-.1208	-.0039	.0134	-.0865
42	58	511.46	12.11	20.17	.2446	.0156	-.1179	-.0061	.0265	-.1426
42	59	511.64	16.09	20.20	.2467	.0152	-.1133	-.0087	.0417	-.2048
42	60	511.64	20.08	20.08	.2431	.0157	-.1047	-.0109	.0570	-.2690
42	66	511.46	.00	24.22	.2978	.0217	-.1368	.0003	-.0011	.0004
42	65	511.11	2.03	24.26	.2991	.0194	-.1398	.0005	-.0027	-.0129
42	64	510.76	3.99	24.29	.3042	.0166	-.1457	-.0001	.0015	-.0308
42	63	510.40	8.05	24.18	.3051	.0147	-.1500	-.0027	.0086	-.0810
42	62	511.46	12.13	24.26	.3083	.0147	-.1494	-.0050	.0220	-.1387
42	61	511.82	14.14	24.19	.3077	.0151	-.1472	-.0064	.0300	-.1699

TABLE VI - Continued
 AERODYNAMIC CHARACTERISTICS IN SIDESLIP FOR VARIOUS ANGLES OF ATTACK.
 BODY AXES; M = 2.01

Run	Pt.	q	β , deg	α , deg	C_N	C_A	C_m	C_l	C_n	C_Y
43	23	510.76	.00	.00	-.0067	.0303	.0080	.0003	-.0008	.0015
43	22	510.58	2.00	.00	-.0064	.0299	.0075	.0000	.0084	-.0259
43	21	510.76	3.98	.00	-.0046	.0295	.0055	-.0002	.0174	-.0532
43	20	510.40	5.98	.01	-.0027	.0293	.0030	-.0004	.0267	-.0815
43	19	510.76	8.01	.01	-.0010	.0290	.0003	-.0003	.0358	-.1106
43	18	510.40	12.03	.02	.0035	.0282	-.0049	.0008	.0523	-.1722
43	17	510.58	16.04	.00	-.0096	.0270	.0012	.0031	.0654	-.2385
43	16	510.23	20.07	.00	-.0288	.0270	.0114	.0058	.0791	-.3106
43	15	510.76	24.14	.00	-.0525	.0275	.0259	.0069	.0951	-.3881
43	14	510.23	28.17	.00	-.0756	.0275	.0420	.0072	.1116	-.4665
43	24	510.76	.00	4.17	.1927	.0294	-.0484	.0001	.0001	-.0011
43	25	510.23	2.06	4.12	.1869	.0293	-.0482	-.0003	.0078	-.0241
43	26	510.40	4.08	4.08	.1817	.0290	-.0479	-.0005	.0158	-.0480
43	27	510.23	6.08	4.06	.1825	.0283	-.0496	-.0005	.0243	-.0742
43	28	510.58	8.07	4.04	.1827	.0284	-.0516	-.0005	.0330	-.1022
43	29	510.05	12.11	4.03	.1853	.0279	-.0547	.0007	.0483	-.1596
43	30	510.23	16.05	4.01	.1704	.0269	-.0468	.0024	.0615	-.2236
43	31	510.23	20.09	4.03	.1481	.0259	-.0330	.0038	.0764	-.2971
43	32	510.05	24.19	4.02	.1179	.0264	-.0124	.0038	.0948	-.3779
43	41	509.87	.00	8.38	.3848	.0288	-.1059	.0004	.0000	.0006
43	40	510.23	2.09	8.34	.3836	.0288	-.1062	.0002	.0075	-.0230
43	39	510.05	4.16	8.30	.3819	.0282	-.1070	-.0001	.0150	-.0458
43	38	510.23	6.17	8.25	.3830	.0277	-.1088	-.0005	.0225	-.0698
43	37	509.87	8.20	8.20	.3819	.0276	-.1099	-.0007	.0299	-.0948
43	36	510.05	12.16	8.11	.3765	.0268	-.1091	-.0005	.0436	-.1505
43	35	510.05	16.16	8.07	.3589	.0258	-.0996	-.0001	.0585	-.2164
43	34	509.87	20.16	8.10	.3326	.0254	-.0821	.0001	.0734	-.2866
43	33	510.40	24.19	8.06	.2989	.0249	-.0594	-.0011	.0920	-.3651
43	42	510.23	.00	12.57	.5764	.0284	-.1625	.0004	-.0004	.0023
43	43	509.87	2.08	12.53	.5746	.0286	-.1626	-.0005	.0064	-.0200
43	44	510.05	4.14	12.50	.5728	.0283	-.1633	-.0013	.0129	-.0419
43	45	510.05	6.22	12.43	.5704	.0275	-.1634	-.0023	.0193	-.0658
43	46	509.87	8.24	12.38	.5710	.0265	-.1660	-.0030	.0252	-.0893
43	47	510.40	12.29	12.29	.5570	.0254	-.1598	-.0038	.0386	-.1448
43	48	510.05	16.26	12.22	.5396	.0249	-.1492	-.0049	.0536	-.2089
43	49	510.05	20.29	12.19	.5136	.0244	-.1327	-.0057	.0689	-.2754
43	50	509.69	24.88	12.52	.4871	.0239	-.1094	-.0088	.0891	-.3611
43	58	510.23	.00	16.71	.7685	.0280	-.2180	.0005	-.0007	.0041
43	57	510.05	2.08	16.72	.7693	.0280	-.2192	-.0011	.0051	-.0185
43	56	509.69	4.18	16.70	.7685	.0276	-.2201	-.0028	.0109	-.0411
43	55	510.05	6.21	16.65	.7659	.0265	-.2201	-.0042	.0159	-.0633
43	54	509.69	8.27	16.60	.7620	.0259	-.2183	-.0054	.0210	-.0870
43	53	510.05	12.38	16.47	.7480	.0246	-.2100	-.0080	.0334	-.1395
43	52	509.87	16.42	16.42	.7326	.0237	-.2004	-.0109	.0478	-.1988
43	51	509.87	20.46	16.36	.7025	.0237	-.1834	-.0135	.0634	-.2642
43	59	510.05	.00	20.88	.9623	.0267	-.2758	.0005	-.0013	.0059
43	60	510.05	2.06	20.88	.9600	.0265	-.2766	-.0016	.0039	-.0173
43	61	510.23	4.19	20.82	.9576	.0259	-.2777	-.0041	.0087	-.0391
43	62	509.69	6.26	20.83	.9546	.0256	-.2760	-.0065	.0130	-.0605
43	63	510.05	8.32	20.77	.9507	.0251	-.2733	-.0081	.0171	-.0821
43	64	509.87	12.46	20.71	.9341	.0246	-.2614	-.0112	.0282	-.1327
43	66	509.52	16.51	20.64	.9136	.0236	-.2498	-.0152	.0420	-.1898
43	65	510.05	20.40	20.47	.8822	.0237	-.2330	-.0191	.0574	-.2505
43	72	510.40	.00	25.10	1.1583	.0255	-.3339	.0005	-.0023	.0078
43	71	510.05	2.11	25.14	1.1593	.0257	-.3345	-.0020	.0016	-.0132
43	70	510.23	4.20	25.13	1.1574	.0252	-.3348	-.0046	.0057	-.0345
43	69	510.05	6.30	25.06	1.1513	.0244	-.3330	-.0069	.0096	-.0553
43	68	510.40	8.31	25.01	1.1434	.0243	-.3288	-.0088	.0127	-.0753
43	67	510.05	12.53	24.99	1.1271	.0236	-.3156	-.0127	.0230	-.1235

TABLE VI - Continued
 AERODYNAMIC CHARACTERISTICS IN SIDESLIP FOR VARIOUS ANGLES OF ATTACK.
 BODY AXES; M = 2.01

Run	Pt.	q	β , deg	α , deg	C_N	C_A	C_m	C_l	C_n	C_Y
44	22	510.58	.00	.00	-.0399	.0340	.0586	.0002	-.0010	.0012
44	21	510.58	.99	.00	-.0388	.0340	.0584	.0001	.0040	-.0126
44	20	510.58	2.00	.00	-.0379	.0335	.0578	.0000	.0089	-.0263
44	19	510.40	3.97	.00	-.0361	.0336	.0565	-.0001	.0185	-.0538
44	18	510.05	5.98	.00	-.0359	.0328	.0549	-.0001	.0283	-.0832
44	17	510.93	8.01	.00	-.0341	.0324	.0526	.0000	.0381	-.1142
44	16	510.76	12.01	.02	-.0312	.0325	.0493	.0015	.0565	-.1779
44	15	510.76	16.02	.03	-.0443	.0319	.0577	.0043	.0716	-.2464
44	14	510.40	20.05	.00	-.0653	.0320	.0681	.0074	.0875	-.3227
44	13	510.23	24.13	.00	-.0866	.0322	.0791	.0091	.1036	-.4007
44	12	510.40	28.15	.00	-.1101	.0328	.0917	.0096	.1190	-.4774
44	23	510.58	-.01	4.20	.1578	.0310	.0020	.0001	.0000	-.0005
44	24	510.58	2.07	4.15	.1551	.0308	.0016	-.0002	.0083	-.0245
44	25	510.58	4.08	4.09	.1515	.0306	.0015	-.0003	.0169	-.0494
44	26	510.58	6.07	4.06	.1491	.0304	.0014	-.0003	.0259	-.0758
44	27	510.58	8.08	4.03	.1511	.0304	-.0003	-.0001	.0354	-.1049
44	28	510.40	12.12	4.04	.1521	.0303	-.0005	.0014	.0521	-.1652
44	29	510.58	16.05	4.01	.1358	.0299	.0102	.0034	.0674	-.2323
44	30	510.40	20.07	4.02	.1116	.0296	.0249	.0055	.0845	-.3091
44	31	510.58	24.18	4.02	.0842	.0303	.0421	.0058	.1041	-.3908
44	40	510.58	.00	8.41	.3530	.0287	-.0532	.0004	-.0001	.0002
44	39	510.93	2.11	8.39	.3518	.0286	-.0535	.0002	.0081	-.0234
44	38	510.58	4.18	8.33	.3486	.0282	-.0535	.0000	.0161	-.0472
44	37	510.58	6.18	8.27	.3482	.0280	-.0546	-.0003	.0239	-.0713
44	36	510.40	8.20	8.23	.3484	.0280	-.0557	-.0004	.0319	-.0972
44	35	510.58	12.18	8.13	.3416	.0273	-.0534	.0001	.0469	-.1550
44	34	510.76	16.16	8.08	.3223	.0270	-.0420	.0008	.0635	-.2230
44	33	510.58	20.17	8.06	.2959	.0273	-.0240	.0016	.0809	-.2974
44	41	510.93	.00	12.61	.5432	.0265	-.1056	.0003	-.0004	.0020
44	42	510.40	2.09	12.57	.5399	.0261	-.1053	-.0005	.0067	-.0204
44	43	510.93	4.18	12.53	.5379	.0261	-.1057	-.0013	.0137	-.0433
44	44	510.76	6.21	12.47	.5353	.0256	-.1059	-.0021	.0204	-.0672
44	45	510.23	8.25	12.41	.5347	.0246	-.1080	-.0027	.0269	-.0917
44	46	510.93	12.29	12.29	.5221	.0240	-.1020	-.0033	.0416	-.1493
44	47	510.76	16.26	12.22	.5045	.0240	-.0911	-.0040	.0581	-.2154
44	48	510.93	20.26	12.22	.4783	.0240	-.0736	-.0045	.0753	-.2848
44	49	510.93	24.88	12.52	.4512	.0252	-.0505	-.0070	.0969	-.3722
44	57	510.93	-.03	16.74	.7335	.0233	-.1578	.0003	-.0007	.0037
44	56	510.76	2.09	16.76	.7343	.0233	-.1590	-.0011	.0053	-.0189
44	55	510.93	4.19	16.74	.7345	.0229	-.1603	-.0027	.0113	-.0424
44	54	510.58	6.23	16.69	.7312	.0222	-.1597	-.0042	.0169	-.0647
44	53	510.76	8.28	16.63	.7265	.0215	-.1579	-.0052	.0222	-.0884
44	52	510.93	12.41	16.51	.7144	.0209	-.1491	-.0074	.0358	-.1437
44	51	510.93	16.43	16.43	.6954	.0205	-.1389	-.0101	.0515	-.2049
44	50	511.29	20.47	16.37	.6681	.0216	-.1223	-.0124	.0685	-.2721
44	58	510.40	-.04	20.93	.9262	.0197	-.2125	.0004	-.0016	.0064
44	59	510.93	2.11	20.92	.9249	.0197	-.2135	-.0017	.0040	-.0177
44	60	510.93	4.16	20.89	.9227	.0188	-.2144	-.0041	.0090	-.0403
44	61	510.76	6.23	20.87	.9205	.0193	-.2135	-.0063	.0137	-.0626
44	62	510.76	8.34	20.82	.9142	.0192	-.2100	-.0080	.0182	-.0844
44	63	510.76	12.48	20.75	.8987	.0185	-.1981	-.0107	.0301	-.1358
44	64	511.11	16.52	20.66	.8784	.0183	-.1857	-.0142	.0446	-.1936
44	65	510.93	20.46	20.46	.8451	.0198	-.1684	-.0179	.0615	-.2567
44	72	511.29	.00	25.15	1.1229	.0173	-.2690	.0004	-.0024	.0082
44	71	511.29	2.12	25.19	1.1214	.0170	-.2692	-.0020	.0017	-.0135
44	69	510.93	4.20	25.17	1.1192	.0165	-.2698	-.0046	.0062	-.0358
44	70	511.11	6.31	25.10	1.1154	.0162	-.2681	-.0067	.0100	-.0565
44	68	510.93	8.33	25.05	1.1055	.0157	-.2638	-.0087	.0137	-.0775
44	67	511.11	12.54	25.02	1.0895	.0162	-.2519	-.0124	.0246	-.1265
44	66	510.93	14.59	24.89	1.0747	.0160	-.2425	-.0142	.0307	-.1524

TABLE VI - Continued
 AERODYNAMIC CHARACTERISTICS IN SIDESLIP FOR VARIOUS ANGLES OF ATTACK.
 BODY AXES; M = 2.01

Run	Pt.	q	β , deg	α , deg	C_N	C_A	C_m	C_l	C_n	C_Y
45	23	511.64	-.01	.00	-.0589	.0347	.0868	.0003	-.0013	.0030
45	22	511.64	.99	.00	-.0594	.0347	.0869	.0001	.0035	-.0116
45	21	511.64	1.99	.00	-.0585	.0343	.0860	-.0001	.0078	-.0243
45	20	511.64	3.98	.01	-.0566	.0344	.0834	-.0006	.0165	-.0506
45	19	511.64	5.99	.01	-.0547	.0339	.0795	-.0011	.0255	-.0788
45	18	511.64	8.01	.01	-.0514	.0331	.0735	-.0014	.0343	-.1078
45	17	511.64	12.04	.02	-.0404	.0319	.0575	-.0013	.0508	-.1701
45	16	511.82	16.04	.03	-.0486	.0305	.0535	-.0002	.0629	-.2341
45	15	511.82	20.07	.00	-.0583	.0296	.0475	.0010	.0760	-.3057
45	14	510.76	24.16	.00	-.0674	.0287	.0382	.0012	.0907	-.3819
45	13	511.29	28.18	.05	-.0724	.0278	.0261	.0005	.1058	-.4579
45	24	510.76	.00	4.22	.1305	.0327	.0448	.0001	-.0002	.0002
45	25	511.64	2.08	4.17	.1260	.0325	.0434	-.0006	.0072	-.0227
45	26	512.00	4.11	4.11	.1254	.0322	.0395	-.0010	.0151	-.0464
45	27	511.64	8.11	4.04	.1327	.0310	.0261	-.0017	.0318	-.0996
45	28	512.00	12.13	4.04	.1446	.0293	.0085	-.0018	.0470	-.1583
45	29	510.58	16.07	4.02	.1393	.0280	-.0020	-.0015	.0597	-.2215
45	30	511.29	20.10	4.06	.1337	.0256	-.0132	-.0015	.0745	-.2944
45	31	510.93	24.20	4.07	.1197	.0246	-.0223	-.0024	.0930	-.3750
45	39	510.93	.00	8.45	.3256	.0306	-.0069	.0005	-.0003	.0018
45	38	510.76	2.11	8.42	.3236	.0300	-.0087	-.0004	.0073	-.0217
45	37	510.76	4.17	8.35	.3232	.0296	-.0135	-.0011	.0146	-.0443
45	36	510.76	8.22	8.22	.3306	.0281	-.0316	-.0027	.0294	-.0932
45	35	510.93	12.19	8.14	.3377	.0261	-.0508	-.0040	.0428	-.1486
45	34	511.11	16.13	8.10	.3337	.0243	-.0662	-.0050	.0582	-.2160
45	33	510.76	20.17	8.06	.3224	.0222	-.0760	-.0058	.0744	-.2883
45	32	511.11	24.18	8.05	.3048	.0209	-.0784	-.0074	.0917	-.3654
45	40	510.76	.00	12.62	.5232	.0275	-.0738	.0004	-.0005	.0027
45	41	510.93	2.09	12.59	.5215	.0271	-.0756	-.0015	.0065	-.0204
45	42	510.76	4.16	12.55	.5220	.0264	-.0805	-.0032	.0130	-.0423
45	43	510.76	8.28	12.40	.5254	.0242	-.0949	-.0068	.0260	-.0906
45	44	510.93	12.31	12.31	.5259	.0220	-.1094	-.0091	.0409	-.1490
45	45	510.76	16.28	12.19	.5217	.0205	-.1236	-.0109	.0580	-.2161
45	46	510.76	20.28	12.18	.5103	.0191	-.1293	-.0121	.0728	-.2823
45	47	510.76	24.89	12.47	.4987	.0181	-.1344	-.0149	.0923	-.3665
45	55	510.93	-.03	16.76	.7215	.0242	-.1434	.0004	-.0010	.0055
45	54	510.76	2.12	16.77	.7216	.0239	-.1438	-.0019	.0056	-.0190
45	53	510.76	4.19	16.75	.7196	.0235	-.1436	-.0046	.0121	-.0425
45	52	510.76	8.32	16.62	.7210	.0207	-.1519	-.0097	.0247	-.0925
45	51	510.76	12.39	16.49	.7204	.0191	-.1634	-.0139	.0394	-.1497
45	50	510.76	16.42	16.42	.7132	.0170	-.1714	-.0171	.0547	-.2099
45	49	510.76	20.46	16.36	.6952	.0166	-.1736	-.0187	.0576	-.2719
45	48	510.76	22.47	16.32	.6834	.0164	-.1746	-.0197	.0759	-.3062
45	56	510.76	-.04	20.93	.9051	.0216	-.1837	.0004	-.0019	.0072
45	57	510.76	2.07	20.94	.9069	.0210	-.1884	-.0027	.0048	-.0179
45	58	510.76	4.16	20.89	.9098	.0200	-.1979	-.0061	.0113	-.0435
45	59	510.76	8.34	20.83	.9088	.0191	-.2032	-.0123	.0232	-.0925
45	60	510.58	12.47	20.74	.9046	.0167	-.2102	-.0166	.0355	-.1440
45	61	510.76	16.52	20.65	.8927	.0151	-.2138	-.0198	.0488	-.2007
45	62	511.11	20.44	20.44	.8693	.0150	-.2131	-.0228	.0630	-.2603
45	68	510.93	-.05	25.17	1.1032	.0194	-.2380	.0004	-.0029	.0100
45	67	510.76	2.12	25.20	1.0956	.0195	-.2363	-.0034	.0032	-.0149
45	66	510.76	4.16	25.20	1.1017	.0191	-.2387	-.0072	.0095	-.0402
45	65	510.76	8.38	25.05	1.0918	.0179	-.2400	-.0124	.0178	-.0838
45	64	511.11	12.54	25.02	1.0861	.0153	-.2491	-.0175	.0308	-.1358
45	63	510.58	14.57	24.86	1.0713	.0141	-.2455	-.0192	.0362	-.1616

TABLE VI - Continued
 AERODYNAMIC CHARACTERISTICS IN SIDESLIP FOR VARIOUS ANGLES OF ATTACK.
 BODY AXES; M = 2.01

Run	Pt.	q	β , deg	α , deg	C_N	C_A	C_m	C_l	C_n	C_y
46	23	510.58	-0.1	0.00	-0.0281	0.0299	0.0297	0.0003	-0.0010	0.0016
46	22	509.69	0.99	0.00	-0.0272	0.0300	0.0294	0.0001	0.0033	-0.0112
46	21	509.34	1.99	0.00	-0.0261	0.0300	0.0284	-0.0002	0.0080	-0.0259
46	20	510.23	3.97	0.01	-0.0241	0.0296	0.0260	-0.0007	0.0169	-0.0522
46	19	509.34	5.98	0.01	-0.0222	0.0289	0.0222	-0.0012	0.0257	-0.0797
46	18	510.40	8.03	0.01	-0.0187	0.0281	0.0171	-0.0015	0.0350	-0.1097
46	17	509.16	12.04	0.02	-0.0106	0.0278	0.0044	-0.0016	0.0516	-0.1716
46	16	509.16	16.04	0.03	-0.0184	0.0266	0.0023	-0.0009	0.0644	-0.2371
46	15	509.16	20.08	0.04	-0.0277	0.0266	-0.0045	-0.0002	0.0781	-0.3100
46	14	508.81	24.15	0.04	-0.0347	0.0268	-0.0158	-0.0005	0.0940	-0.3872
46	13	508.99	28.18	0.00	-0.0412	0.0267	-0.0306	-0.0017	0.1104	-0.4662
46	24	510.40	0.00	4.19	0.1588	0.0289	-0.0058	0.0001	-0.0001	-0.0004
46	25	510.05	2.07	4.14	0.1530	0.0288	-0.0070	-0.0005	0.0075	-0.0234
46	26	509.52	4.09	4.09	0.1526	0.0285	-0.0106	-0.0010	0.0154	-0.0473
46	27	510.40	8.10	4.04	0.1583	0.0274	-0.0224	-0.0018	0.0323	-0.1005
46	28	510.05	12.11	4.03	0.1691	0.0267	-0.0393	-0.0022	0.0480	-0.1597
46	29	510.23	16.06	4.01	0.1672	0.0260	-0.0501	-0.0026	0.0616	-0.2237
46	30	510.05	20.08	4.02	0.1579	0.0249	-0.0614	-0.0035	0.0788	-0.3013
46	31	510.23	24.17	4.02	0.1506	0.0246	-0.0736	-0.0049	0.0985	-0.3847
46	39	510.23	-0.1	8.42	0.3483	0.0283	-0.0508	0.0004	-0.0002	0.0012
46	38	510.40	2.11	8.39	0.3478	0.0280	-0.0528	-0.0005	0.0075	-0.0223
46	37	510.23	4.17	8.31	0.3478	0.0272	-0.0579	-0.0014	0.0152	-0.0461
46	36	510.23	8.19	8.19	0.3569	0.0266	-0.0779	-0.0032	0.0305	-0.0960
46	35	510.05	12.16	8.11	0.3646	0.0255	-0.0967	-0.0048	0.0451	-0.1527
46	34	510.23	16.15	8.07	0.3616	0.0248	-0.1128	-0.0069	0.0642	-0.2248
46	33	510.40	20.16	8.06	0.3506	0.0238	-0.1213	-0.0082	0.0810	-0.2988
46	32	510.05	24.17	8.05	0.3365	0.0229	-0.1262	-0.0098	0.0974	-0.3754
46	40	510.23	-0.2	12.58	0.5444	0.0269	-0.1160	0.0005	-0.0005	0.0021
46	41	510.23	2.09	12.56	0.5447	0.0270	-0.1189	-0.0017	0.0070	-0.0212
46	42	510.40	4.17	12.52	0.5452	0.0261	-0.1242	-0.0037	0.0141	-0.0441
46	43	510.23	8.26	12.37	0.5526	0.0248	-0.1398	-0.0079	0.0294	-0.0957
46	44	508.45	12.27	12.27	0.5528	0.0236	-0.1566	-0.0113	0.0480	-0.1592
46	45	509.52	16.25	12.17	0.5464	0.0233	-0.1653	-0.0134	0.0651	-0.2271
46	46	508.99	20.26	12.17	0.5351	0.0223	-0.1712	-0.0143	0.0776	-0.2905
46	47	509.87	24.86	12.46	0.5256	0.0222	-0.1785	-0.0172	0.0971	-0.3744
46	56	509.87	0.00	16.73	0.7513	0.0265	-0.1957	0.0004	-0.0008	0.0040
46	54	510.05	2.02	16.74	0.7509	0.0262	-0.1946	-0.0022	0.0072	-0.0218
46	55	509.87	2.08	16.73	0.7515	0.0263	-0.1946	-0.0022	0.0075	-0.0219
46	53	510.05	4.18	16.70	0.7499	0.0260	-0.1958	-0.0056	0.0167	-0.0497
46	52	510.05	8.30	16.59	0.7478	0.0239	-0.1992	-0.0116	0.0320	-0.1039
46	51	510.23	12.38	16.46	0.7427	0.0227	-0.2031	-0.0160	0.0462	-0.1603
46	50	509.52	16.41	16.41	0.7283	0.0216	-0.2000	-0.0183	0.0568	-0.2144
46	49	509.69	21.26	17.02	0.7421	0.0215	-0.2153	-0.0212	0.0729	-0.2880
46	48	509.69	22.46	16.31	0.7043	0.0215	-0.2110	-0.0211	0.0796	-0.3121
46	57	510.05	-0.4	20.89	0.9361	0.0253	-0.2353	0.0005	-0.0022	0.0077
46	58	510.05	2.10	20.89	0.9399	0.0252	-0.2434	-0.0031	0.0079	-0.0228
46	59	509.87	4.19	20.85	0.9395	0.0245	-0.2484	-0.0071	0.0170	-0.0528
46	60	509.87	8.30	20.81	0.9276	0.0233	-0.2370	-0.0127	0.0269	-0.0988
46	61	509.87	12.46	20.71	0.9238	0.0215	-0.2435	-0.0175	0.0406	-0.1525
46	62	509.87	16.47	20.66	0.9040	0.0206	-0.2329	-0.0200	0.0480	-0.1999
46	63	509.69	20.42	20.42	0.8853	0.0211	-0.2393	-0.0240	0.0653	-0.2642
46	69	510.23	0.00	25.14	1.1276	0.0248	-0.2813	0.0002	-0.0023	0.0084
46	68	510.05	2.12	25.18	1.1235	0.0240	-0.2754	-0.0036	0.0049	-0.0178
46	67	509.69	4.20	25.17	1.1197	0.0245	-0.2714	-0.0075	0.0122	-0.0443
46	66	509.52	8.37	25.04	1.1079	0.0226	-0.2699	-0.0119	0.0191	-0.0869
46	65	510.05	12.48	25.00	1.1040	0.0213	-0.2786	-0.0176	0.0339	-0.1402
46	64	509.69	16.57	24.86	1.0858	0.0202	-0.2673	-0.0189	0.0369	-0.1629

TABLE VI - Continued
 AERODYNAMIC CHARACTERISTICS IN SIDESLIP FOR VARIOUS ANGLES OF ATTACK.
 BODY AXES; M = 2.01

Run	Pt.	q	β , deg	α , deg	C_N	C_A	C_m	C_l	C_n	C_y
47	23	508.63	.00	.00	-.0166	.0280	.0118	.0003	-.0008	.0014
47	22	508.10	.99	.00	-.0157	.0280	.0115	.0002	.0034	-.0114
47	21	508.45	2.00	.00	-.0163	.0280	.0112	.0000	.0081	-.0252
47	20	508.10	3.98	.00	-.0146	.0277	.0093	-.0002	.0188	-.0517
47	19	508.28	5.99	.00	-.0127	.0275	.0067	-.0005	.0256	-.0750
47	18	508.45	8.02	.00	-.0109	.0267	.0035	-.0006	.0344	-.1082
47	17	508.28	12.03	.00	-.0046	.0261	-.0050	-.0001	.0504	-.1691
47	16	508.81	16.04	.00	-.0170	.0255	.0000	.0011	.0624	-.2343
47	15	507.92	20.07	.00	-.0341	.0255	.0076	.0025	.0747	-.3038
47	14	508.99	24.15	.00	-.0515	.0259	.0128	.0026	.0887	-.3790
47	13	507.39	28.19	.00	-.0660	.0259	.0143	.0023	.1028	-.4534
47	24	508.45	.00	4.18	.1666	.0274	-.0176	.0001	.0000	-.0004
47	25	508.10	2.06	4.14	.1614	.0272	-.0181	-.0003	.0074	-.0233
47	26	508.63	4.08	4.08	.1588	.0272	-.0191	-.0006	.0153	-.0471
47	27	508.45	8.10	4.04	.1613	.0263	-.0243	-.0008	.0320	-.0994
47	28	508.28	12.12	4.04	.1672	.0259	-.0313	-.0003	.0468	-.1576
47	29	508.28	16.07	4.02	.1543	.0253	-.0276	.0002	.0591	-.2198
47	30	508.28	20.10	4.03	.1339	.0242	-.0187	.0004	.0731	-.2915
47	31	508.28	24.20	4.07	.1159	.0246	-.0123	-.0003	.0897	-.3701
47	40	508.45	.00	8.43	.3500	.0269	-.0478	.0004	-.0001	.0011
47	39	508.10	2.11	8.39	.3473	.0267	-.0483	.0001	.0076	-.0225
47	38	508.10	4.17	8.32	.3450	.0262	-.0493	-.0003	.0149	-.0453
47	37	508.28	8.21	8.21	.3458	.0258	-.0540	-.0011	.0296	-.0933
47	36	508.28	12.18	8.13	.3435	.0249	-.0585	-.0014	.0428	-.1480
47	35	508.10	16.16	8.08	.3292	.0241	-.0556	-.0019	.0568	-.2129
47	34	508.28	17.11	8.57	.3439	.0235	-.0567	-.0026	.0598	-.2281
47	33	508.10	20.18	8.07	.3090	.0228	-.0483	-.0027	.0710	-.2822
47	32	508.28	24.20	8.06	.2828	.0231	-.0388	-.0046	.0879	-.3588
47	41	507.92	.00	12.61	.5229	.0268	-.0735	.0003	-.0003	.0027
47	42	508.28	2.09	12.59	.5218	.0267	-.0737	-.0006	.0067	-.0206
47	43	507.04	4.18	12.55	.5212	.0259	-.0756	-.0015	.0134	-.0427
47	44	507.92	8.29	12.41	.5210	.0241	-.0809	-.0035	.0256	-.0891
47	45	508.81	12.32	12.32	.5128	.0230	-.0795	-.0048	.0387	-.1445
47	46	507.04	16.31	12.21	.4947	.0227	-.0773	-.0067	.0533	-.2083
47	47	508.28	20.31	12.20	.4783	.0226	-.0732	-.0085	.0677	-.2732
47	48	508.28	24.93	12.49	.4596	.0224	-.0646	-.0115	.0866	-.3567
47	56	508.28	.00	16.79	.7002	.0253	-.0965	.0003	-.0007	.0051
47	55	508.45	2.09	16.79	.7004	.0253	-.0972	-.0012	.0054	-.0185
47	54	508.45	4.20	16.78	.6989	.0249	-.0985	-.0030	.0113	-.0410
47	53	508.28	8.31	16.67	.6938	.0233	-.0999	-.0060	.0218	-.0870
47	52	508.28	12.40	16.55	.6847	.0226	-.0973	-.0088	.0346	-.1413
47	51	508.28	16.45	16.45	.6733	.0218	-.0975	-.0123	.0490	-.2006
47	50	508.45	20.49	16.38	.6534	.0213	-.0946	-.0155	.0638	-.2649
47	49	508.28	22.48	16.38	.6390	.0215	-.0908	-.0168	.0712	-.2982
47	57	508.10	-.04	20.98	.8728	.0242	-.1209	.0005	-.0016	.0068
47	58	508.10	2.11	20.97	.8723	.0242	-.1221	-.0017	.0038	-.0164
47	59	508.28	4.21	20.94	.8713	.0234	-.1241	-.0043	.0090	-.0392
47	60	508.10	8.36	20.86	.8669	.0229	-.1255	-.0084	.0183	-.0842
47	61	508.10	12.51	20.80	.8559	.0220	-.1220	-.0119	.0300	-.1347
47	62	508.10	16.52	20.73	.8434	.0208	-.1191	-.0159	.0435	-.1907
47	63	508.45	20.45	20.51	.8179	.0211	-.1144	-.0202	.0586	-.2515
47	69	508.10	.00	25.23	1.0582	.0229	-.1533	.0004	-.0021	.0084
47	68	508.10	2.12	25.26	1.0582	.0224	-.1534	-.0021	.0018	-.0116
47	67	508.10	4.22	25.24	1.0549	.0225	-.1537	-.0046	.0062	-.0339
47	66	508.28	8.40	25.12	1.0467	.0218	-.1537	-.0087	.0139	-.0766
47	65	507.92	12.58	25.09	1.0326	.0211	-.1491	-.0128	.0249	-.1258
47	64	507.92	14.62	24.94	1.0186	.0204	-.1446	-.0149	.0312	-.1527

TABLE VI - Continued
 AERODYNAMIC CHARACTERISTICS IN SIDESLIP FOR VARIOUS ANGLES OF ATTACK.

BODY AXES; M = 2.01

Run	Pt.	q	β ,deg	α ,deg	C_N	C_A	C_m	C_l	C_n	C_Y
48	21	511.11	.00	.00	.0054	.0189	.0087	.0002	-.0011	.0023
48	20	510.76	1.99	.00	.0066	.0195	.0088	-.0016	.0073	-.0204
48	19	510.93	3.97	.00	.0078	.0197	.0084	-.0033	.0155	-.0430
48	18	510.76	5.97	.00	.0092	.0193	.0080	-.0051	.0244	-.0877
48	17	510.76	8.00	-.01	.0107	.0184	.0073	-.0069	.0335	-.0942
48	16	510.76	12.00	.00	.0106	.0175	.0068	-.0103	.0501	-.1504
48	15	510.93	16.01	.03	.0102	.0159	.0076	-.0137	.0652	-.2216
48	14	510.93	20.04	.00	.0098	.0153	.0084	-.0170	.0806	-.2949
48	13	510.93	24.11	.00	.0091	.0152	.0089	-.0197	.0973	-.3711
48	12	511.29	28.12	.00	.0072	.0153	.0107	-.0225	.1160	-.4510
48	22	510.93	.00	4.04	.0156	.0197	.0225	.0000	.0000	-.0011
48	23	510.93	2.01	4.02	.0146	.0197	.0218	-.0014	.0074	-.0221
48	24	510.93	4.00	4.01	.0118	.0191	.0217	-.0030	.0154	-.0442
48	25	511.29	6.01	4.00	.0132	.0186	.0206	-.0047	.0242	-.0695
48	26	510.93	8.01	4.01	.0136	.0183	.0198	-.0064	.0326	-.0944
48	27	510.93	12.06	4.02	.0186	.0172	.0160	-.0099	.0488	-.1522
48	28	510.93	16.02	4.00	.0233	.0159	.0159	-.0130	.0632	-.2204
48	29	510.93	20.06	4.02	.0275	.0146	.0151	-.0159	.0776	-.2910
48	30	510.93	24.17	4.02	.0286	.0146	.0149	-.0187	.0946	-.3670
48	39	511.46	.00	8.10	.0267	.0201	.0338	.0000	.0001	-.0013
48	38	510.93	2.03	8.09	.0267	.0192	.0330	-.0014	.0072	-.0223
48	37	510.40	4.05	8.09	.0284	.0187	.0319	-.0030	.0148	-.0447
48	36	510.76	6.04	8.06	.0294	.0178	.0305	-.0046	.0229	-.0689
48	35	510.93	8.05	8.05	.0319	.0174	.0294	-.0062	.0309	-.0948
48	34	511.11	12.04	8.03	.0446	.0162	.0226	-.0093	.0459	-.1541
48	33	510.93	16.05	8.02	.0537	.0150	.0203	-.0123	.0597	-.2185
48	32	510.23	20.09	8.03	.0598	.0143	.0183	-.0146	.0728	-.2853
48	31	511.11	24.11	8.08	.0614	.0138	.0177	-.0175	.0899	-.3600
48	40	510.76	.00	12.14	.0445	.0201	.0463	.0000	-.0002	-.0005
48	41	510.40	2.02	12.14	.0457	.0196	.0445	-.0013	.0055	-.0204
48	42	509.52	4.02	12.13	.0480	.0181	.0410	-.0027	.0118	-.0426
48	43	510.23	6.04	12.10	.0530	.0168	.0377	-.0042	.0188	-.0674
48	44	510.93	8.07	12.09	.0586	.0160	.0341	-.0057	.0258	-.0934
48	45	510.93	12.09	12.09	.0712	.0152	.0293	-.0086	.0407	-.1542
48	46	510.93	16.09	12.09	.0797	.0142	.0262	-.0113	.0543	-.2157
48	47	510.58	20.15	12.10	.0881	.0143	.0224	-.0135	.0677	-.2810
48	48	510.40	24.79	12.41	.0962	.0133	.0207	-.0166	.0871	-.3649
48	49	510.58	20.22	16.16	.1241	.0132	.0252	-.0124	.0630	-.2766
49	8	510.05	.00	16.16	.0833	.0197	.0514	-.0001	-.0002	-.0006
49	7	510.05	2.01	16.21	.0855	.0197	.0498	-.0009	.0033	-.0189
49	6	509.69	4.04	16.18	.0893	.0176	.0443	-.0020	.0070	-.0389
49	5	509.69	6.02	16.18	.0931	.0161	.0388	-.0036	.0132	-.0643
49	4	509.69	8.08	16.16	.0970	.0153	.0363	-.0051	.0203	-.0923
49	3	510.23	12.12	16.14	.1061	.0146	.0333	-.0076	.0344	-.1505
49	2	509.52	16.15	16.15	.1120	.0131	.0302	-.0102	.0488	-.2127
49	1	510.93	20.21	16.15	.1175	.0132	.0266	-.0124	.0627	-.2763
49	9	509.69	.00	20.22	.1317	.0196	.0537	.0000	-.0002	.0001
49	10	510.05	2.03	20.23	.1338	.0185	.0509	-.0002	.0006	-.0166
49	11	510.05	4.06	20.23	.1379	.0169	.0446	-.0012	.0030	-.0358
49	12	509.69	6.06	20.22	.1393	.0151	.0403	-.0026	.0084	-.0597
49	13	510.23	8.04	20.22	.1436	.0145	.0370	-.0039	.0145	-.0867
49	14	509.52	12.12	20.26	.1506	.0126	.0327	-.0062	.0282	-.1448
49	15	509.69	16.14	20.26	.1567	.0129	.0300	-.0089	.0433	-.2070
49	16	509.52	20.11	20.11	.1600	.0129	.0274	-.0112	.0584	-.2712
49	21	509.69	2.09	24.37	.1823	.0177	.0505	.0004	-.0022	-.0133
49	20	510.05	4.06	24.39	.1868	.0157	.0445	-.0001	-.0003	-.0322
49	19	509.52	6.10	24.33	.1892	.0147	.0396	-.0013	.0046	-.0567
49	18	509.34	8.10	24.32	.1916	.0139	.0363	-.0025	.0104	-.0834
49	17	510.23	12.18	24.36	.1958	.0118	.0321	-.0048	.0242	-.1421

TABLE VI - Continued
 AERODYNAMIC CHARACTERISTICS IN SIDESLIP FOR VARIOUS ANGLES OF ATTACK.
 BODY AXES; M = 2.01

Run	Pt.	q	β , deg	α , deg	C_N	C_A	C_m	C_l	C_n	C_y
50	21	509.34	.00	.00	-.0129	.0274	.0148	.0001	-.0012	.0033
50	20	509.52	2.00	.00	-.0122	.0270	.0153	-.0027	.0063	-.0211
50	19	509.52	3.98	.00	-.0129	.0272	.0168	-.0058	.0140	-.0456
50	18	509.69	5.98	.00	-.0153	.0270	.0190	-.0091	.0220	-.0720
50	17	509.52	8.03	.01	-.0151	.0268	.0218	-.0124	.0302	-.0992
50	16	509.52	12.04	.00	-.0178	.0266	.0291	-.0197	.0463	-.1593
50	15	509.87	16.04	-.03	-.0069	.0262	.0249	-.0274	.0622	-.2310
50	14	509.69	20.06	.00	.0144	.0246	.0164	-.0355	.0809	-.3124
50	13	509.34	24.15	.00	.0315	.0254	.0105	-.0422	.0977	-.3928
50	12	509.34	28.16	.00	.0446	.0252	.0101	-.0476	.1137	-.4708
50	22	509.16	.00	4.18	.1636	.0270	-.0132	-.0001	-.0003	-.0003
50	23	509.16	2.07	4.14	.1576	.0266	-.0116	-.0035	.0062	-.0238
50	24	509.34	4.10	4.10	.1559	.0267	-.0105	-.0069	.0135	-.0492
50	25	508.99	6.10	4.07	.1528	.0263	-.0081	-.0102	.0213	-.0760
50	26	509.34	8.10	4.04	.1493	.0262	-.0052	-.0136	.0293	-.1038
50	27	508.99	12.13	4.06	.1516	.0264	-.0001	-.0214	.0456	-.1694
50	28	508.99	16.10	4.05	.1634	.0259	-.0025	-.0291	.0601	-.2384
50	29	508.81	20.13	4.03	.1790	.0243	-.0071	-.0376	.0768	-.3162
50	30	509.16	24.24	4.03	.1939	.0247	-.0109	-.0452	.0937	-.3973
50	39	508.99	-.01	8.43	.3498	.0260	-.0471	.0000	-.0006	.0022
50	38	509.16	2.11	8.39	.3482	.0261	-.0461	-.0036	.0059	-.0247
50	37	509.34	4.18	8.34	.3456	.0260	-.0445	-.0073	.0126	-.0509
50	36	508.99	6.20	8.29	.3433	.0251	-.0419	-.0109	.0200	-.0793
50	35	509.34	8.23	8.23	.3419	.0253	-.0385	-.0149	.0281	-.1115
50	34	508.81	12.23	8.16	.3457	.0255	-.0346	-.0229	.0425	-.1755
50	33	508.99	16.24	8.12	.3493	.0253	-.0298	-.0312	.0554	-.2435
50	32	509.16	20.27	8.10	.3535	.0234	-.0284	-.0400	.0707	-.3189
50	31	508.99	24.28	8.18	.3631	.0242	-.0312	-.0485	.0868	-.3960
50	40	508.99	.00	12.62	.5285	.0261	-.0782	-.0001	-.0008	.0020
50	41	508.99	2.07	12.61	.5257	.0262	-.0767	-.0043	.0052	-.0264
50	42	509.34	4.19	12.57	.5220	.0258	-.0743	-.0084	.0113	-.0545
50	43	509.16	6.23	12.52	.5176	.0250	-.0707	-.0126	.0176	-.0846
50	44	508.99	8.28	12.44	.5169	.0251	-.0677	-.0169	.0245	-.1155
50	45	508.99	12.36	12.36	.5136	.0249	-.0594	-.0258	.0370	-.1797
50	46	508.81	16.39	12.28	.5104	.0243	-.0502	-.0344	.0491	-.2484
50	47	508.99	20.42	12.27	.5125	.0234	-.0484	-.0431	.0639	-.3234
50	48	509.16	25.06	12.57	.5282	.0243	-.0520	-.0531	.0818	-.4107
50	56	509.52	.00	16.79	.7075	.0247	-.1105	-.0001	-.0011	.0045
50	55	509.87	2.06	16.81	.7069	.0248	-.1092	-.0046	.0039	-.0241
50	54	509.52	4.20	16.79	.7060	.0246	-.1067	-.0092	.0097	-.0556
50	53	509.52	6.24	16.74	.7036	.0245	-.1036	-.0136	.0152	-.0868
50	52	509.69	8.33	16.71	.7019	.0241	-.1011	-.0180	.0195	-.1165
50	51	509.52	12.47	16.59	.6939	.0229	-.0929	-.0264	.0304	-.1837
50	50	509.52	16.50	16.56	.6868	.0237	-.0812	-.0350	.0417	-.2535
50	49	508.99	20.58	16.51	.6788	.0230	-.0746	-.0447	.0549	-.3246
50	57	509.69	.00	20.96	.8753	.0230	-.1397	.0000	-.0014	.0062
50	58	509.52	2.11	20.95	.8744	.0227	-.1398	-.0046	.0024	-.0247
50	59	509.69	4.17	20.94	.8709	.0229	-.1375	-.0092	.0060	-.0542
50	60	509.52	6.29	20.91	.8661	.0217	-.1347	-.0137	.0090	-.0833
50	61	509.34	8.37	20.87	.8612	.0207	-.1326	-.0183	.0138	-.1158
50	62	509.34	12.50	20.86	.8522	.0215	-.1229	-.0263	.0239	-.1847
50	63	509.34	16.63	20.79	.8417	.0221	-.1115	-.0344	.0342	-.2533
50	64	508.99	20.56	20.62	.8257	.0211	-.1006	-.0434	.0473	-.3234
50	70	509.52	.00	25.17	1.0416	.0226	-.1763	.0000	-.0021	.0079
50	69	509.52	2.07	25.20	1.0395	.0217	-.1733	-.0048	-.0002	-.0214
50	68	509.34	4.16	25.21	1.0371	.0208	-.1723	-.0093	.0019	-.0494
50	67	509.69	6.33	25.15	1.0322	.0198	-.1696	-.0136	.0053	-.0799
50	66	509.34	8.40	25.11	1.0264	.0194	-.1663	-.0176	.0087	-.1107
50	65	509.52	12.58	25.09	1.0130	.0191	-.1551	-.0254	.0172	-.1780

TABLE VI - Continued
 AERODYNAMIC CHARACTERISTICS IN SIDESLIP FOR VARIOUS ANGLES OF ATTACK.
 BODY AXES; M = 2.01

Run	Pt.	q	β ,deg	α ,deg	C_N	C_A	C_m	C_l	C_n	C_y
51	22	510.05	.00	.00	-.0155	.0294	.0229	.0002	-.0012	.0034
51	21	510.40	.99	.00	-.0151	.0294	.0227	-.0013	.0027	-.0093
51	20	510.23	2.00	.00	-.0163	.0295	.0232	-.0029	.0067	-.0211
51	19	510.05	3.98	.01	-.0153	.0292	.0235	-.0061	.0144	-.0463
51	18	509.87	5.99	.01	-.0159	.0291	.0242	-.0094	.0224	-.0718
51	17	509.87	8.02	-.03	-.0176	.0290	.0247	-.0131	.0310	-.1004
51	16	510.05	12.04	.00	-.0137	.0287	.0244	-.0210	.0482	-.1621
51	15	510.05	16.03	.00	.0036	.0280	.0121	-.0293	.0652	-.2359
51	14	510.23	20.06	.00	.0251	.0266	-.0038	-.0386	.0849	-.3184
51	13	510.23	24.13	.04	.0518	.0267	-.0240	-.0461	.1042	-.4035
51	12	509.87	26.15	.05	.0661	.0266	-.0337	-.0492	.1126	-.4438
51	23	510.05	.00	4.18	.1751	.0287	-.0289	-.0001	-.0003	-.0002
51	24	510.05	2.06	4.13	.1700	.0287	-.0284	-.0038	.0065	-.0248
51	25	510.23	4.08	4.08	.1670	.0287	-.0291	-.0073	.0139	-.0493
51	26	510.05	8.11	4.04	.1676	.0284	-.0304	-.0148	.0307	-.1071
51	27	510.05	12.12	4.06	.1729	.0280	-.0317	-.0230	.0480	-.1729
51	28	508.45	16.08	4.05	.1871	.0273	-.0385	-.0315	.0639	-.2437
51	29	509.52	20.11	4.03	.2062	.0257	-.0488	-.0411	.0822	-.3250
51	30	509.87	24.22	4.07	.2290	.0259	-.0642	-.0495	.1007	-.4082
51	38	509.69	.00	8.39	.3767	.0285	-.0904	.0001	-.0006	.0016
51	37	509.87	2.10	8.36	.3723	.0280	-.0890	-.0037	.0063	-.0254
51	36	509.87	4.15	8.32	.3717	.0278	-.0888	-.0075	.0131	-.0517
51	35	510.40	8.23	8.23	.3733	.0275	-.0882	-.0159	.0295	-.1135
51	34	510.76	12.21	8.15	.3758	.0276	-.0860	-.0247	.0459	-.1804
51	33	509.87	16.20	8.10	.3808	.0271	-.0841	-.0340	.0606	-.2501
51	32	510.05	20.24	8.09	.3856	.0254	-.0850	-.0436	.0772	-.3287
51	31	510.05	24.25	8.08	.3969	.0252	-.0931	-.0525	.0943	-.4088
51	39	509.69	-.02	12.58	.5690	.0277	-.1454	.0000	-.0008	.0024
51	40	509.69	2.09	12.55	.5653	.0278	-.1434	-.0043	.0054	-.0261
51	41	510.05	4.17	12.52	.5619	.0273	-.1411	-.0086	.0120	-.0553
51	42	509.87	8.29	12.41	.5594	.0267	-.1373	-.0178	.0269	-.1195
51	43	509.87	12.31	12.35	.5585	.0263	-.1323	-.0278	.0417	-.1860
51	44	509.87	16.35	12.24	.5580	.0261	-.1266	-.0378	.0565	-.2590
51	45	510.05	20.38	12.24	.5544	.0247	-.1194	-.0467	.0716	-.3351
51	53	510.05	.00	16.73	.7549	.0265	-.1941	-.0001	-.0012	.0041
51	52	510.23	2.05	16.74	.7535	.0265	-.1916	-.0048	.0045	-.0256
51	51	510.05	4.16	16.73	.7524	.0266	-.1903	-.0094	.0109	-.0573
51	50	510.05	6.23	16.69	.7489	.0265	-.1868	-.0140	.0172	-.0897
51	49	510.23	8.29	16.65	.7476	.0257	-.1845	-.0186	.0228	-.1215
51	48	510.23	12.43	16.54	.7409	.0247	-.1772	-.0284	.0355	-.1911
51	47	510.40	16.50	16.50	.7330	.0250	-.1670	-.0380	.0488	-.2642
51	46	510.05	20.53	16.47	.7296	.0240	-.1611	-.0474	.0623	-.3362
51	54	509.87	.00	20.89	.9257	.0250	-.2306	.0002	-.0017	.0068
51	55	509.87	2.10	20.88	.9251	.0243	-.2310	-.0050	.0031	-.0253
51	56	510.05	4.19	20.86	.9263	.0242	-.2343	-.0094	.0077	-.0569
51	57	509.87	6.26	20.84	.9234	.0229	-.2324	-.0140	.0116	-.0872
51	58	509.87	8.31	20.84	.9186	.0223	-.2290	-.0191	.0164	-.1189
51	59	508.28	12.50	20.79	.9062	.0229	-.2144	-.0284	.0270	-.1895
51	60	508.99	16.55	20.75	.9006	.0232	-.2084	-.0365	.0382	-.2591
51	61	508.99	20.55	20.55	.8823	.0224	-.1970	-.0449	.0513	-.3295
51	68	508.99	.00	25.09	1.1108	.0238	-.2967	.0000	-.0020	.0068
51	67	509.16	2.11	25.13	1.1104	.0232	-.2936	-.0050	.0004	-.0228
51	66	508.81	4.19	25.12	1.1055	.0220	-.2916	-.0097	.0033	-.0521
51	65	508.81	6.26	25.08	1.1030	.0207	-.2899	-.0142	.0075	-.0838
51	64	508.81	8.36	25.01	1.0956	.0200	-.2845	-.0186	.0114	-.1149
51	63	509.16	12.55	25.03	1.0813	.0198	-.2672	-.0269	.0187	-.1803
51	62	508.81	14.61	24.92	1.0689	.0203	-.2563	-.0309	.0228	-.2113

TABLE VI - Continued
 AERODYNAMIC CHARACTERISTICS IN SIDESLIP FOR VARIOUS ANGLES OF ATTACK.
 BODY AXES; M = 2.01

Run	Pt.	q	β , deg	α , deg	C_N	C_A	C_m	C_l	C_n	C_y
52	24	510.23	.00	.00	-.0513	.0343	.0818	.0002	-.0012	.0039
52	23	509.52	.99	.00	-.0511	.0339	.0816	-.0012	.0025	-.0078
52	22	509.16	1.99	.00	-.0523	.0336	.0821	-.0028	.0064	-.0205
52	21	510.23	3.98	.00	-.0511	.0336	.0824	-.0060	.0143	-.0458
52	20	509.87	5.98	.00	-.0517	.0336	.0835	-.0093	.0223	-.0712
52	19	509.16	8.03	.00	-.0519	.0332	.0840	-.0129	.0306	-.0995
52	18	510.93	12.03	.02	-.0513	.0325	.0850	-.0205	.0469	-.1597
52	17	509.69	16.04	.00	-.0344	.0312	.0725	-.0286	.0631	-.2328
52	16	508.28	20.06	.04	-.0087	.0296	.0552	-.0372	.0822	-.3150
52	15	510.05	24.14	.00	.0128	.0291	.0373	-.0443	.0997	-.3970
52	14	510.05	26.16	.00	.0237	.0281	.0287	-.0472	.1078	-.4360
52	25	510.23	.00	4.21	.1407	.0316	.0274	-.0001	-.0002	-.0006
52	26	510.23	2.07	4.17	.1355	.0313	.0281	-.0037	.0063	-.0240
52	27	510.23	4.12	4.11	.1342	.0310	.0271	-.0071	.0135	-.0486
52	28	510.23	8.11	4.05	.1345	.0307	.0263	-.0143	.0299	-.1052
52	29	509.87	12.15	4.07	.1382	.0296	.0255	-.0224	.0463	-.1707
52	30	510.23	16.10	4.02	.1516	.0290	.0188	-.0308	.0611	-.2396
52	31	510.58	20.13	4.07	.1749	.0266	.0055	-.0397	.0782	-.3186
52	32	510.58	24.25	4.08	.1958	.0267	-.0081	-.0475	.0957	-.44017
52	40	510.40	.00	8.42	.3435	.0293	-.0352	.0001	-.0005	.0012
52	39	509.87	2.09	8.41	.3393	.0293	-.0341	-.0036	.0060	-.0247
52	38	510.05	4.19	8.36	.3388	.0288	-.0335	-.0074	.0128	-.0519
52	37	510.05	8.23	8.23	.3372	.0281	-.0321	-.0155	.0284	-.1117
52	36	509.87	12.23	8.16	.3413	.0275	-.0306	-.0241	.0433	-.1765
52	35	509.87	16.22	8.11	.3469	.0271	-.0300	-.0331	.0567	-.2455
52	34	509.87	20.26	8.10	.3544	.0253	-.0336	-.0423	.0727	-.3221
52	33	509.87	24.29	8.09	.3639	.0250	-.0400	-.0508	.0895	-.4012
52	41	510.05	.00	12.62	.5360	.0276	-.0903	.0000	-.0009	.0021
52	42	510.23	2.09	12.59	.5336	.0277	-.0888	-.0042	.0054	-.0272
52	43	510.76	4.16	12.55	.5297	.0272	-.0865	-.0083	.0114	-.0543
52	44	510.40	8.29	12.42	.5255	.0261	-.0830	-.0174	.0250	-.1163
52	45	510.23	12.35	12.35	.5278	.0259	-.0797	-.0271	.0381	-.1815
52	46	510.40	16.35	12.29	.5262	.0249	-.0745	-.0365	.0507	-.2500
52	47	510.23	20.39	12.30	.5258	.0236	-.0711	-.0452	.0663	-.3271
52	54	510.23	.00	16.77	.7216	.0252	-.1402	.0001	-.0012	.0047
52	53	510.23	2.09	16.77	.7191	.0252	-.1375	-.0047	.0042	-.0249
52	52	510.40	4.20	16.76	.7189	.0250	-.1372	-.0093	.0098	-.0563
52	51	510.58	8.33	16.65	.7138	.0240	-.1326	-.0185	.0204	-.1174
52	50	510.58	12.45	16.56	.7081	.0230	-.1269	-.0278	.0315	-.1855
52	49	510.40	16.52	16.52	.7031	.0229	-.1202	-.0370	.0441	-.2567
52	48	510.40	20.58	16.46	.6994	.0217	-.1160	-.0464	.0579	-.3303
52	55	510.40	.00	20.93	.8964	.0225	-.1822	.0002	-.0014	.0055
52	56	510.40	2.10	20.90	.8956	.0218	-.1830	-.0049	.0026	-.0254
52	57	510.58	4.20	20.89	.8949	.0214	-.1867	-.0092	.0063	-.0549
52	58	510.40	8.36	20.86	.8890	.0197	-.1817	-.0190	.0142	-.1166
52	59	510.23	12.52	20.81	.8800	.0206	-.1715	-.0281	.0243	-.1855
52	60	510.58	16.61	20.76	.8717	.0196	-.1670	-.0361	.0350	-.2549
52	61	510.23	20.93	20.60	.8568	.0192	-.1577	-.0444	.0486	-.3252
52	67	510.23	.00	25.13	1.0852	.0195	-.2570	.0002	-.0020	.0075
52	66	510.40	2.11	25.15	1.0832	.0186	-.2549	-.0050	-.0003	-.0219
52	65	510.40	4.20	25.15	1.0805	.0172	-.2534	-.0093	.0019	-.0499
52	64	510.40	8.33	25.05	1.0705	.0162	-.2464	-.0182	.0091	-.1113
52	63	510.40	12.57	25.06	1.0555	.0164	-.2289	-.0266	.0169	-.1776
52	62	510.58	14.62	24.94	1.0410	.0165	-.2170	-.0309	.0220	-.2121

TABLE VI - Continued
 AERODYNAMIC CHARACTERISTICS IN SIDESLIP FOR VARIOUS ANGLES OF ATTACK.
 BODY AXES; M = 2.01

Run	Pt.	q	β , deg	α , deg	C_N	C_A	C_m	C_l	C_n	C_y
53	28	509.52	.00	.00	-.0356	.0318	.0527	.0002	-.0012	.0023
53	27	509.34	.98	.00	-.0355	.0319	.0527	-.0009	.0035	-.0106
53	26	510.40	2.00	.00	-.0351	.0319	.0533	-.0021	.0085	-.0244
53	25	510.58	3.99	.01	-.0362	.0320	.0556	-.0044	.0179	-.0517
53	24	509.34	5.98	.00	-.0387	.0314	.0589	-.0070	.0276	-.0796
53	23	508.63	8.01	.01	-.0393	.0312	.0620	-.0097	.0373	-.1090
53	22	510.40	12.01	-.02	-.0481	.0312	.0771	-.0159	.0564	-.1749
53	21	510.58	16.01	.00	-.0459	.0318	.0891	-.0232	.0737	-.2483
53	20	510.58	20.03	.00	-.0403	.0323	.1034	-.0315	.0934	-.3315
53	19	510.76	24.12	.00	-.0298	.0333	.1115	-.0383	.1111	-.4140
53	18	509.69	26.13	.05	-.0235	.0325	.1108	-.0412	.1179	-.4507
53	29	510.58	.00	4.18	.1605	.0294	-.0064	.0000	-.0003	-.0004
53	30	510.58	2.07	4.15	.1544	.0295	-.0043	-.0030	.0077	-.0261
53	31	510.76	4.11	4.11	.1509	.0287	-.0022	-.0059	.0161	-.0528
53	32	510.40	8.09	4.03	.1459	.0292	.0038	-.0119	.0342	-.1120
53	33	510.40	12.13	4.04	.1432	.0290	.0147	-.0188	.0516	-.1788
53	34	510.76	16.09	4.05	.1461	.0292	.0257	-.0264	.0670	-.2485
53	35	509.16	20.11	4.03	.1537	.0286	.0386	-.0347	.0852	-.3281
53	36	510.76	24.23	4.07	.1523	.0302	.0583	-.0418	.1054	-.4151
53	44	510.58	-.01	8.42	.3514	.0286	-.0523	.0001	-.0007	.0023
53	43	510.58	2.11	8.39	.3481	.0283	-.0511	-.0031	.0071	-.0267
53	42	510.40	4.17	8.32	.3456	.0279	-.0493	-.0064	.0148	-.0541
53	41	510.40	8.23	8.23	.3445	.0274	-.0450	-.0131	.0318	-.1162
53	40	510.23	12.22	8.15	.3433	.0273	-.0376	-.0207	.0470	-.1822
53	39	510.40	16.47	8.24	.3497	.0269	-.0282	-.0294	.0612	-.2550
53	38	510.40	20.25	8.10	.3411	.0259	-.0160	-.0376	.0768	-.3278
53	37	509.34	24.27	8.09	.3395	.0273	-.0024	-.0456	.0947	-.4087
53	45	510.23	-.02	12.61	.5399	.0274	-.0983	.0000	-.0009	.0021
53	46	510.23	2.09	12.58	.5372	.0270	-.0970	-.0038	.0061	-.0274
53	47	510.40	4.18	12.54	.5318	.0272	-.0939	-.0075	.0132	-.0576
53	48	510.76	8.30	12.43	.5288	.0263	-.0885	-.0151	.0277	-.1207
53	49	511.11	12.35	12.35	.5263	.0256	-.0807	-.0235	.0408	-.1849
53	50	510.23	16.37	12.26	.5207	.0254	-.0672	-.0318	.0535	-.2540
53	51	510.76	20.39	12.30	.5181	.0249	-.0603	-.0404	.0689	-.3306
53	52	510.40	25.03	12.60	.5272	.0256	-.0533	-.0505	.0871	-.4191
53	50	510.58	.00	16.74	.7268	.0249	-.1499	.0000	-.0012	.0048
53	59	510.58	2.09	16.77	.7284	.0251	-.1493	-.0041	.0046	-.0259
53	58	510.58	4.17	16.76	.7264	.0248	-.1464	-.0082	.0108	-.0575
53	57	510.76	8.33	16.65	.7188	.0240	-.1393	-.0162	.0223	-.1198
53	56	510.93	12.45	16.56	.7131	.0230	-.1313	-.0238	.0340	-.1881
53	55	510.40	16.51	16.51	.7037	.0234	-.1171	-.0323	.0457	-.2584
53	54	510.58	20.59	16.47	.6939	.0228	-.1047	-.0420	.0593	-.3319
53	53	510.93	22.64	16.45	.6891	.0233	-.0982	-.0468	.0677	-.3713
53	61	509.34	.00	20.92	.9096	.0220	-.2020	.0001	-.0016	.0066
53	62	509.69	2.11	20.91	.9078	.0217	-.2016	-.0043	.0028	-.0263
53	63	510.40	4.20	20.88	.9047	.0219	-.1991	-.0083	.0069	-.0560
53	64	510.23	8.32	20.87	.8986	.0198	-.1947	-.0164	.0155	-.1179
53	65	510.40	12.51	20.80	.8863	.0207	-.1820	-.0239	.0267	-.1881
53	66	510.23	16.57	20.78	.8741	.0206	-.1683	-.0315	.0372	-.2568
53	67	510.23	20.56	20.56	.8521	.0206	-.1488	-.0406	.0509	-.3289
53	73	510.05	.00	25.10	1.0916	.0196	-.2639	.0001	-.0023	.0085
53	72	510.05	2.11	25.15	1.0878	.0192	-.2605	-.0044	-.0001	-.0220
53	71	510.05	4.20	25.15	1.0863	.0183	-.2596	-.0084	.0024	-.0501
53	70	510.05	8.38	25.05	1.0751	.0163	-.2525	-.0159	.0098	-.1127
53	69	510.40	12.56	25.05	1.0595	.0164	-.2372	-.0230	.0192	-.1802
53	68	510.40	14.62	24.94	1.0481	.0173	-.2266	-.0266	.0249	-.2168

TABLE VI - Continued
 AERODYNAMIC CHARACTERISTICS IN SIDESLIP FOR VARIOUS ANGLES OF ATTACK.
 BODY AXES; M = 2.01

Run	Pt.	q	β , deg	α , deg	C_N	C_A	C_m	C_l	C_n	C_y
54	20	510.23	.01	.00	-.0052	.0293	.0075	.0003	-.0014	.0035
54	19	510.40	2.00	.00	-.0065	.0290	.0079	-.0022	.0071	-.0220
54	18	510.23	3.97	.00	-.0092	.0292	.0099	-.0047	.0153	-.0475
54	17	510.23	5.99	.00	-.0100	.0290	.0123	-.0074	.0241	-.0740
54	16	510.40	8.01	.00	-.0135	.0285	.0160	-.0104	.0332	-.1032
54	15	510.76	12.03	.00	-.0192	.0285	.0293	-.0169	.0508	-.1670
54	14	510.40	16.03	.00	-.0138	.0273	.0390	-.0246	.0670	-.2379
54	13	510.23	20.05	.00	-.0047	.0262	.0523	-.0333	.0869	-.3213
54	12	510.23	24.12	.00	.0029	.0262	.0641	-.0402	.1058	-.4053
54	11	510.58	28.15	.00	.0099	.0259	.0720	-.0451	.1208	-.4826
54	21	509.69	-.01	4.17	.1924	.0288	-.0539	.0001	-.0003	-.0001
54	22	510.40	2.06	4.12	.1877	.0287	-.0528	-.0030	.0067	-.0248
54	23	510.58	4.08	4.08	.1825	.0282	-.0507	-.0060	.0142	-.0495
54	24	510.40	6.08	4.06	.1792	.0282	-.0483	-.0090	.0225	-.0776
54	25	510.23	8.11	4.04	.1759	.0279	-.0447	-.0121	.0309	-.1066
54	26	510.76	12.15	4.05	.1717	.0276	-.0325	-.0193	.0473	-.1723
54	27	510.40	16.09	4.02	.1751	.0272	-.0204	-.0272	.0623	-.2414
54	28	509.69	20.12	4.07	.1844	.0254	-.0093	-.0361	.0796	-.3202
54	29	510.40	24.23	4.07	.1878	.0256	.0046	-.0437	.0984	-.4041
54	38	510.76	.00	8.37	.3858	.0287	-.1073	.0001	-.0006	.0017
54	37	510.23	2.10	8.35	.3826	.0284	-.1063	-.0031	.0061	-.0244
54	36	510.23	4.16	8.31	.3800	.0283	-.1047	-.0064	.0131	-.0517
54	35	510.05	6.18	8.27	.3791	.0277	-.1023	-.0097	.0209	-.0804
54	34	510.05	8.22	8.22	.3777	.0277	-.0986	-.0133	.0289	-.1128
54	33	509.69	12.21	8.15	.3783	.0274	-.0902	-.0211	.0434	-.1761
54	32	510.23	16.22	8.11	.3760	.0273	-.0765	-.0295	.0566	-.2451
54	31	510.40	20.24	8.14	.3749	.0250	-.0643	-.0387	.0719	-.3205
54	30	510.58	24.28	8.09	.3710	.0253	-.0520	-.0470	.0893	-.4005
54	39	510.23	.00	12.57	.5755	.0286	-.1595	.0000	-.0008	.0016
54	40	510.23	2.09	12.54	.5693	.0287	-.1574	-.0038	.0053	-.0260
54	41	510.05	4.17	12.51	.5676	.0285	-.1551	-.0076	.0116	-.0552
54	42	509.87	6.23	12.46	.5647	.0276	-.1517	-.0115	.0181	-.0846
54	43	510.76	8.27	12.40	.5611	.0274	-.1475	-.0154	.0251	-.1163
54	44	510.23	12.33	12.33	.5565	.0267	-.1364	-.0238	.0373	-.1790
54	45	510.23	16.35	12.29	.5506	.0258	-.1193	-.0325	.0496	-.2486
54	46	510.40	20.38	12.29	.5473	.0249	-.1096	-.0415	.0647	-.3247
54	47	510.40	25.02	12.60	.5577	.0256	-.1034	-.0518	.0825	-.4120
54	55	510.23	-.03	16.70	.7687	.0278	-.2179	.0001	-.0012	.0043
54	54	509.69	2.08	16.72	.7677	.0275	-.2170	-.0041	.0038	-.0245
54	53	511.11	4.18	16.71	.7671	.0275	-.2144	-.0082	.0095	-.0560
54	52	509.69	6.25	16.67	.7618	.0275	-.2096	-.0123	.0151	-.0867
54	51	510.05	8.31	16.61	.7581	.0267	-.2054	-.0165	.0199	-.1166
54	50	510.05	12.43	16.53	.7483	.0258	-.1931	-.0244	.0306	-.1840
54	49	510.05	16.45	16.50	.7371	.0254	-.1740	-.0332	.0419	-.2533
54	48	509.69	20.57	16.45	.7254	.0247	-.1572	-.0431	.0553	-.3264
54	56	510.40	-.04	20.86	.9517	.0264	-.2757	.0003	-.0015	.0061
54	57	510.40	2.10	20.85	.9486	.0262	-.2753	-.0041	.0021	-.0240
54	58	510.76	4.19	20.84	.9465	.0264	-.2728	-.0084	.0057	-.0545
54	59	510.40	6.26	20.82	.9418	.0250	-.2690	-.0126	.0087	-.0828
54	60	509.52	8.33	20.79	.9379	.0240	-.2661	-.0167	.0132	-.1147
54	61	509.87	12.48	20.76	.9239	.0243	-.2495	-.0245	.0234	-.1839
54	62	509.87	16.58	20.73	.9090	.0240	-.2304	-.0324	.0335	-.2517
54	63	509.87	20.51	20.58	.8875	.0234	-.2068	-.0419	.0469	-.3229
54	69	509.87	.00	25.06	1.1358	.0261	-.3422	.0002	-.0019	.0061
54	68	510.23	2.11	25.09	1.1344	.0253	-.3397	-.0045	-.0005	-.0215
54	67	509.87	4.14	25.09	1.1320	.0244	-.3388	-.0085	.0015	-.0496
54	66	509.34	6.30	25.04	1.1272	.0235	-.3356	-.0126	.0048	-.0795
54	65	510.23	8.31	25.00	1.1219	.0223	-.3308	-.0164	.0078	-.1093
54	64	510.05	12.54	25.01	1.1047	.0222	-.3124	-.0237	.0160	-.1760

TABLE VI - Continued
 AERODYNAMIC CHARACTERISTICS IN SIDESLIP FOR VARIOUS ANGLES OF ATTACK.

BODY AXES; M = 2.01

Run	Pt.	q	β ,deg	α ,deg	C_N	C_A	C_m	C_l	C_n	C_y
55	21	509.87	.00	.00	-.0105	.0289	.0086	-.0001	-.0011	.0015
55	20	510.23	1.99	.00	-.0080	.0284	.0078	-.0015	.0078	-.0213
55	19	509.87	3.97	-.01	-.0088	.0285	.0079	-.0028	.0168	-.0452
55	18	510.23	5.96	-.01	-.0077	.0282	.0082	-.0041	.0260	-.0699
55	17	510.05	7.99	-.01	-.0080	.0279	.0091	-.0054	.0354	-.0965
55	16	510.05	12.00	.00	-.0082	.0270	.0128	-.0081	.0530	-.1548
55	15	510.05	16.00	.00	-.0115	.0257	.0228	-.0108	.0705	-.2286
55	14	510.05	20.01	.00	-.0176	.0248	.0359	-.0138	.0873	-.3022
55	13	510.05	24.08	.00	-.0263	.0243	.0483	-.0170	.1074	-.3838
55	12	510.23	28.10	.00	-.0301	.0242	.0573	-.0191	.1227	-.4578
55	22	509.87	.00	4.17	.1931	.0280	-.0510	-.0003	.0000	-.0011
55	23	510.40	2.05	4.12	.1839	.0279	-.0489	-.0020	.0076	-.0223
55	24	510.40	4.08	4.08	.1823	.0277	-.0487	-.0036	.0157	-.0444
55	25	510.23	6.06	4.04	.1791	.0276	-.0475	-.0050	.0241	-.0680
55	26	510.23	8.06	4.02	.1789	.0272	-.0463	-.0065	.0328	-.0933
55	27	510.23	12.10	4.03	.1772	.0266	-.0402	-.0095	.0502	-.1539
55	28	510.23	16.04	4.04	.1685	.0258	-.0273	-.0125	.0670	-.2241
55	29	509.87	20.07	4.02	.1566	.0250	-.0127	-.0155	.0847	-.3004
55	30	510.05	24.16	4.06	.1423	.0247	.0042	-.0194	.1042	-.3811
55	39	510.05	.00	8.39	.3914	.0280	-.1121	-.0002	.0001	-.0012
55	38	509.69	2.10	8.36	.3897	.0280	-.1122	-.0020	.0075	-.0229
55	37	510.23	4.16	8.31	.3882	.0277	-.1121	-.0038	.0147	-.0448
55	36	509.87	6.17	8.25	.3874	.0276	-.1116	-.0056	.0220	-.0670
55	35	509.69	8.19	8.19	.3858	.0269	-.1101	-.0076	.0299	-.0922
55	34	509.69	12.15	8.11	.3779	.0265	-.1000	-.0115	.0457	-.1503
55	33	510.05	16.16	8.07	.3608	.0255	-.0833	-.0151	.0625	-.2219
55	32	510.05	20.17	8.06	.3395	.0242	-.0646	-.0188	.0800	-.2973
55	31	510.23	24.19	8.06	.3213	.0243	-.0460	-.0229	.0997	-.3779
55	40	509.69	.00	12.56	.5868	.0283	-.1731	-.0003	-.0001	-.0004
55	41	510.23	2.08	12.53	.5848	.0282	-.1732	-.0026	.0066	-.0235
55	42	509.69	4.16	12.48	.5835	.0278	-.1732	-.0052	.0134	-.0456
55	43	509.69	6.22	12.43	.5803	.0273	-.1719	-.0078	.0199	-.0687
55	44	509.69	8.25	12.36	.5776	.0266	-.1700	-.0104	.0263	-.0932
55	45	509.69	12.29	12.29	.5672	.0260	-.1591	-.0150	.0398	-.1489
55	46	510.23	16.30	12.21	.5508	.0249	-.1405	-.0192	.0562	-.2195
55	47	509.87	20.31	12.20	.5304	.0242	-.1185	-.0236	.0740	-.2929
55	48	510.05	24.91	12.54	.5189	.0238	-.0974	-.0297	.0962	-.3822
55	56	509.87	.00	16.71	.7801	.0275	-.2313	-.0002	-.0006	.0014
55	55	509.34	2.08	16.72	.7824	.0278	-.2331	-.0033	.0051	-.0211
55	54	509.16	4.15	16.71	.7823	.0273	-.2331	-.0063	.0111	-.0447
55	53	510.76	6.24	16.65	.7793	.0273	-.2310	-.0096	.0164	-.0677
55	52	510.76	8.27	16.60	.7777	.0259	-.2295	-.0124	.0213	-.0913
55	51	511.11	12.40	16.50	.7661	.0250	-.2173	-.0177	.0327	-.1461
55	50	510.93	16.44	16.44	.7474	.0241	-.2000	-.0236	.0476	-.2118
55	49	510.76	20.49	16.38	.7245	.0239	-.1771	-.0297	.0664	-.2841
55	57	510.58	.00	20.86	.9721	.0268	-.2915	-.0001	-.0007	.0014
55	58	510.23	2.06	20.87	.9685	.0266	-.2906	-.0038	.0042	-.0217
55	59	510.05	4.19	20.83	.9692	.0267	-.2911	-.0073	.0086	-.0443
55	60	510.40	6.22	20.84	.9652	.0257	-.2888	-.0106	.0128	-.0674
55	61	509.87	8.29	20.79	.9576	.0248	-.2848	-.0138	.0171	-.0901
55	62	510.40	12.46	20.72	.9480	.0240	-.2732	-.0192	.0258	-.1399
55	63	510.05	16.52	20.66	.9279	.0235	-.2552	-.0250	.0384	-.2003
55	64	510.58	20.46	20.46	.8956	.0239	-.2296	-.0323	.0569	-.2708
55	70	510.58	.00	25.07	1.1633	.0256	-.3552	-.0001	-.0011	.0023
55	69	510.76	2.11	25.12	1.1656	.0257	-.3568	-.0037	.0026	-.0204
55	68	510.58	4.19	25.12	1.1619	.0256	-.3556	-.0073	.0056	-.0415
55	67	510.05	6.30	25.04	1.1557	.0247	-.3523	-.0104	.0086	-.0621
55	66	509.87	8.35	24.99	1.1500	.0238	-.3479	-.0135	.0119	-.0840
55	65	512.00	12.52	24.97	1.1343	.0233	-.3332	-.0190	.0196	-.1320

TABLE VI - Continued
 AERODYNAMIC CHARACTERISTICS IN SIDESLIP FOR VARIOUS ANGLES OF ATTACK.
 BODY AXES; M = 2.01

Run	Pt.	q	β ,deg	α ,deg	C_N	C_A	C_m	C_l	C_n	C_Y
56	20	509.87	.00	.00	-.0407	.0319	.0572	-.0002	-.0010	.0021
56	19	509.87	1.99	.00	-.0397	.0315	.0570	-.0014	.0091	-.0237
56	18	509.87	3.95	.00	-.0388	.0316	.0574	-.0025	.0188	-.0476
56	17	510.05	5.96	.00	-.0378	.0312	.0580	-.0036	.0287	-.0734
56	16	509.87	7.99	.00	-.0382	.0308	.0596	-.0048	.0388	-.1010
56	15	509.87	11.99	.00	-.0399	.0302	.0649	-.0071	.0582	-.1625
56	14	509.34	15.97	.00	-.0452	.0301	.0766	-.0092	.0775	-.2388
56	13	509.87	19.99	.00	-.0499	.0300	.0889	-.0115	.0958	-.3152
56	12	510.05	24.07	.00	-.0562	.0302	.0988	-.0143	.1128	-.3924
56	11	509.69	28.11	.00	-.0594	.0286	.1004	-.0167	.1213	-.4571
56	21	510.40	.00	4.19	.1581	.0293	-.0009	-.0003	.0000	-.0014
56	22	510.23	2.07	4.15	.1523	.0291	.0004	-.0019	.0086	-.0237
56	23	510.40	4.08	4.08	.1491	.0290	.0016	-.0034	.0172	-.0468
56	24	510.23	6.08	4.05	.1475	.0286	.0029	-.0047	.0265	-.0715
56	25	510.40	8.08	4.03	.1457	.0284	.0053	-.0061	.0357	-.0978
56	26	510.40	12.10	4.03	.1454	.0281	.0112	-.0088	.0545	-.1595
56	27	510.23	16.02	4.03	.1366	.0281	.0247	-.0114	.0725	-.2318
56	28	510.23	20.05	4.02	.1228	.0285	.0410	-.0137	.0918	-.3110
56	29	510.40	24.16	4.02	.1081	.0284	.0577	-.0170	.1123	-.3929
56	38	509.87	-.01	8.41	.3568	.0269	-.0585	-.0003	-.0001	-.0006
56	37	509.87	2.10	8.38	.3551	.0268	-.0585	-.0020	.0082	-.0234
56	36	509.87	4.17	8.32	.3556	.0265	-.0591	-.0038	.0159	-.0463
56	35	510.05	6.20	8.26	.3545	.0262	-.0587	-.0056	.0238	-.0695
56	34	510.23	8.21	8.21	.3541	.0259	-.0576	-.0074	.0321	-.0955
56	33	508.99	12.17	8.12	.3453	.0256	-.0481	-.0111	.0488	-.1549
56	32	510.93	16.16	8.07	.3286	.0257	-.0307	-.0142	.0670	-.2281
56	31	510.05	20.17	8.06	.3076	.0256	-.0117	-.0174	.0858	-.3059
56	30	510.23	24.18	8.05	.2874	.0262	.0077	-.0209	.1068	-.3886
56	39	510.05	-.02	12.60	.5504	.0248	-.1150	-.0003	-.0004	.0003
56	40	509.87	2.09	12.57	.5479	.0248	-.1146	-.0027	.0071	-.0240
56	41	510.05	4.16	12.55	.5456	.0249	-.1142	-.0051	.0143	-.0469
56	42	509.87	6.21	12.47	.5443	.0240	-.1138	-.0077	.0212	-.0700
56	43	509.87	8.28	12.40	.5416	.0235	-.1125	-.0103	.0281	-.0956
56	44	509.69	12.31	12.31	.5330	.0231	-.1037	-.0148	.0425	-.1542
56	45	509.87	16.31	12.21	.5166	.0226	-.0865	-.0188	.0596	-.2250
56	46	509.69	20.32	12.20	.4940	.0233	-.0638	-.0226	.0786	-.2995
56	47	509.69	24.92	12.49	.4822	.0236	-.0426	-.0278	.1024	-.3920
56	55	510.05	-.03	16.74	.7396	.0228	-.1663	-.0003	-.0008	.0020
56	54	510.05	2.08	16.75	.7413	.0230	-.1679	-.0033	.0053	-.0215
56	53	510.05	4.16	16.74	.7409	.0227	-.1680	-.0063	.0117	-.0450
56	52	509.87	6.25	16.67	.7390	.0219	-.1663	-.0095	.0175	-.0692
56	51	509.87	8.32	16.62	.7358	.0212	-.1649	-.0124	.0229	-.0939
56	50	509.87	12.41	16.51	.7259	.0205	-.1554	-.0175	.0349	-.1489
56	49	509.87	16.46	16.46	.7114	.0201	-.1414	-.0231	.0504	-.2156
56	48	510.05	20.50	16.49	.6893	.0199	-.1212	-.0290	.0699	-.2898
56	56	509.87	-.04	20.92	.9272	.0203	-.2200	-.0002	-.0011	.0028
56	57	509.87	2.10	20.89	.9265	.0201	-.2199	-.0038	.0045	-.0221
56	58	509.87	4.19	20.86	.9234	.0200	-.2196	-.0072	.0092	-.0457
56	59	510.23	6.27	20.85	.9210	.0195	-.2183	-.0105	.0137	-.0679
56	60	509.87	8.34	20.81	.9163	.0186	-.2159	-.0136	.0186	-.0925
56	61	509.87	12.48	20.76	.9073	.0181	-.2060	-.0189	.0278	-.1424
56	62	510.05	16.55	20.69	.8877	.0181	-.1904	-.0245	.0410	-.2046
56	63	510.05	20.45	20.51	.8589	.0187	-.1695	-.0316	.0597	-.2742
56	69	510.23	.00	25.11	1.1183	.0177	-.2807	-.0002	-.0015	.0038
56	68	510.23	2.11	25.15	1.1194	.0179	-.2817	-.0037	.0028	-.0208
56	67	510.23	4.20	25.15	1.1169	.0174	-.2812	-.0071	.0059	-.0419
56	66	510.05	6.31	25.08	1.1114	.0171	-.2784	-.0102	.0093	-.0635
56	65	510.23	8.32	25.04	1.1063	.0166	-.2744	-.0131	.0129	-.0853
56	64	510.40	12.53	25.00	1.0916	.0158	-.2610	-.0184	.0213	-.1347

TABLE VI - Continued
 AERODYNAMIC CHARACTERISTICS IN SIDESLIP FOR VARIOUS ANGLES OF ATTACK.
 BODY AXES; M = 2.01

Run	Pt.	q	β , deg	α , deg	C_N	C_A	C_m	C_l	C_n	C_y
57	23	510.76	.00	.00	-.0529	.0330	.0863	-.0002	-.0011	.0029
57	22	510.23	.99	.00	-.0515	.0330	.0859	-.0011	.0033	-.0090
57	21	510.23	1.99	.00	-.0517	.0330	.0855	-.0020	.0074	-.0199
57	20	510.23	3.97	.00	-.0505	.0321	.0845	-.0038	.0159	-.0426
57	19	510.05	5.97	.01	-.0477	.0325	.0821	-.0055	.0245	-.0670
57	18	510.05	7.99	.01	-.0449	.0321	.0788	-.0074	.0332	-.0916
57	17	510.76	12.00	.00	-.0388	.0306	.0684	-.0113	.0499	-.1496
57	16	510.23	16.00	.03	-.0273	.0288	.0537	-.0150	.0664	-.2222
57	15	510.76	20.03	.00	-.0187	.0269	.0410	-.0186	.0826	-.2955
57	14	510.58	25.09	.00	-.0098	.0261	.0245	-.0232	.1060	-.3941
57	13	510.58	28.10	.00	-.0013	.0255	.0135	-.0257	.1202	-.4544
57	24	510.40	.00	4.21	.1461	.0308	.0292	-.0004	.0000	-.0007
57	25	510.58	2.07	4.16	.1420	.0308	.0281	-.0027	.0073	-.0216
57	26	510.76	4.10	4.10	.1422	.0302	.0247	-.0049	.0151	-.0435
57	27	510.58	6.10	4.08	.1438	.0294	.0205	-.0068	.0233	-.0667
57	28	510.58	10.09	4.03	.1484	.0285	.0126	-.0111	.0397	-.1176
57	29	510.58	12.10	4.03	.1532	.0279	.0085	-.0135	.0486	-.1512
57	30	510.40	16.05	4.01	.1565	.0265	.0004	-.0174	.0650	-.2213
57	31	510.40	20.07	4.02	.1574	.0246	-.0096	-.0208	.0825	-.2980
57	32	510.58	24.14	4.01	.1619	.0238	-.0213	-.0249	.1012	-.3768
57	40	510.40	.00	8.44	.3519	.0286	-.0375	-.0003	-.0001	.0002
57	39	510.76	2.11	8.41	.3520	.0286	-.0389	-.0028	.0074	-.0223
57	38	510.23	4.17	8.36	.3513	.0283	-.0412	-.0051	.0146	-.0441
57	37	510.23	8.23	8.23	.3520	.0270	-.0469	-.0100	.0297	-.0920
57	36	510.23	12.17	8.12	.3521	.0260	-.0508	-.0152	.0458	-.1508
57	35	510.76	16.16	8.08	.3471	.0241	-.0533	-.0199	.0631	-.2222
57	34	510.23	20.19	8.07	.3453	.0223	-.0616	-.0237	.0812	-.2995
57	33	510.40	24.19	8.06	.3382	.0214	-.0680	-.0283	.1004	-.3800
57	41	510.40	.00	12.62	.5486	.0267	-.0968	-.0003	-.0002	.0001
57	42	510.40	2.07	12.61	.5461	.0268	-.0968	-.0033	.0068	-.0230
57	43	510.58	4.19	12.56	.5459	.0260	-.0986	-.0063	.0137	-.0459
57	44	510.40	8.29	12.41	.5455	.0246	-.1025	-.0128	.0273	-.0942
57	45	510.23	12.31	12.31	.5420	.0232	-.1041	-.0187	.0417	-.1526
57	46	510.58	16.32	12.22	.5363	.0218	-.1052	-.0238	.0599	-.2261
57	47	510.23	20.30	12.19	.5302	.0203	-.1086	-.0284	.0782	-.2995
57	48	510.40	24.91	12.48	.5336	.0193	-.1156	-.0338	.1002	-.3887
57	57	510.58	.00	16.77	.7358	.0243	-.1473	-.0003	-.0006	.0018
57	54	510.76	4.20	16.76	.7378	.0239	-.1515	-.0078	.0119	-.0459
57	53	510.76	8.32	16.63	.7387	.0218	-.1577	-.0148	.0231	-.0936
57	52	510.40	12.41	16.51	.7346	.0209	-.1589	-.0214	.0365	-.1515
57	51	510.58	16.45	16.45	.7292	.0192	-.1582	-.0277	.0534	-.2200
57	50	510.23	20.49	16.38	.7148	.0183	-.1526	-.0336	.0726	-.2943
57	49	510.76	22.51	16.35	.7073	.0186	-.1506	-.0361	.0821	-.3322
57	58	510.05	.00	20.94	.9195	.0220	-.1950	-.0002	-.0010	.0027
57	59	510.05	2.11	20.92	.9206	.0223	-.1968	-.0044	.0047	-.0223
57	60	510.40	4.20	20.89	.9225	.0217	-.2016	-.0090	.0104	-.0477
57	61	510.93	8.34	20.83	.9239	.0190	-.2123	-.0166	.0209	-.0963
57	62	510.23	12.49	20.77	.9166	.0179	-.2070	-.0227	.0317	-.1492
57	63	510.40	16.55	20.69	.9017	.0171	-.2003	-.0291	.0451	-.2113
57	64	510.23	20.48	20.48	.8778	.0176	-.1890	-.0348	.0626	-.2790
57	70	510.40	-.05	25.17	1.1020	.0202	-.2386	-.0003	-.0013	.0035
57	69	510.58	2.07	25.21	1.1035	.0203	-.2407	-.0047	.0033	-.0211
57	68	510.58	4.21	25.18	1.1035	.0201	-.2436	-.0093	.0072	-.0440
57	67	510.23	8.38	25.05	1.0990	.0182	-.2492	-.0169	.0167	-.0923
57	66	510.40	12.55	25.04	1.0869	.0170	-.2423	-.0223	.0245	-.1405
57	65	510.58	14.60	24.91	1.0750	.0161	-.2374	-.0254	.0296	-.1670

TABLE VI - Continued
 AERODYNAMIC CHARACTERISTICS IN SIDESLIP FOR VARIOUS ANGLES OF ATTACK.
 BODY AXES; M = 2.01

Run	Pt.	q	β ,deg	α ,deg	C_N	C_A	C_m	C_l	C_n	C_Y
58	22	511.29	-0.01	0.00	-0.0202	0.0289	0.0298	-0.0002	-0.0012	0.0023
58	21	511.11	1.00	0.00	-0.0205	0.0284	0.0296	-0.0010	-0.0031	-0.0086
58	20	511.11	1.99	0.00	-0.0191	0.0284	0.0290	-0.0020	-0.0073	-0.0204
58	19	511.29	3.97	0.00	-0.0194	0.0285	0.0282	-0.0038	-0.0159	-0.0431
58	18	511.11	5.96	0.00	-0.0166	0.0282	0.0259	-0.0056	-0.0244	-0.0667
58	17	511.29	8.00	0.00	-0.0137	0.0275	0.0226	-0.0076	-0.0332	-0.0922
58	16	511.11	11.99	0.02	-0.0057	0.0265	0.0129	-0.0117	-0.0506	-0.1503
58	15	511.29	16.00	0.00	0.0032	0.0256	-0.0010	-0.0159	-0.0682	-0.2249
58	14	511.11	20.02	0.00	0.0137	0.0253	-0.0146	-0.0201	-0.0853	-0.2994
58	13	511.46	24.09	0.00	0.0231	0.0248	-0.0302	-0.0245	-0.1052	-0.3806
58	12	510.76	28.09	0.00	0.0366	0.0249	-0.0481	-0.0283	-0.1247	-0.4616
58	23	511.64	0.00	4.18	0.1739	0.0278	-0.0216	-0.0003	-0.0001	-0.0012
58	24	511.29	2.06	4.13	0.1717	0.0278	-0.0232	-0.0028	-0.0074	-0.0213
58	25	511.29	4.08	4.08	0.1720	0.0273	-0.0270	-0.0050	-0.0154	-0.0441
58	26	511.29	8.09	4.03	0.1750	0.0267	-0.0367	-0.0094	-0.0321	-0.0926
58	27	511.64	12.09	4.03	0.1848	0.0259	-0.0462	-0.0142	-0.0509	-0.1549
58	28	510.93	16.03	4.00	0.1872	0.0252	-0.0530	-0.0185	-0.0691	-0.2274
58	29	512.17	20.04	4.02	0.1900	0.0247	-0.0615	-0.0225	-0.0872	-0.3044
58	30	511.82	24.15	4.01	0.1937	0.0238	-0.0758	-0.0276	-0.1074	-0.3864
58	38	511.46	0.00	8.41	0.3792	0.0276	-0.0890	-0.0003	-0.0001	-0.0004
58	37	511.46	2.10	8.37	0.3781	0.0276	-0.0902	-0.0030	-0.0076	-0.0230
58	36	511.82	4.17	8.31	0.3787	0.0273	-0.0930	-0.0056	-0.0150	-0.0447
58	35	511.46	8.19	8.19	0.3815	0.0264	-0.0998	-0.0108	-0.0312	-0.0938
58	34	511.64	12.15	8.11	0.3822	0.0257	-0.1037	-0.0166	-0.0499	-0.1566
58	33	511.46	16.15	8.07	0.3767	0.0242	-0.1030	-0.0215	-0.0685	-0.2303
58	32	512.00	20.15	8.05	0.3730	0.0233	-0.1110	-0.0258	-0.0876	-0.3090
58	31	511.64	24.17	8.05	0.3699	0.0232	-0.1202	-0.0310	-0.1074	-0.3907
58	39	511.46	0.00	12.58	0.5769	0.0273	-0.1506	-0.0003	-0.0005	-0.0005
58	40	511.46	2.07	12.56	0.5746	0.0274	-0.1505	-0.0034	-0.0072	-0.0237
58	41	511.64	4.15	12.53	0.5731	0.0273	-0.1510	-0.0068	-0.0148	-0.0476
58	42	511.64	8.27	12.40	0.5732	0.0256	-0.1540	-0.0136	-0.0304	-0.0991
58	43	511.46	12.28	12.28	0.5689	0.0246	-0.1542	-0.0202	-0.0476	-0.1616
58	44	511.82	16.27	12.19	0.5622	0.0236	-0.1536	-0.0257	-0.0668	-0.2361
58	45	511.64	20.28	12.18	0.5561	0.0231	-0.1568	-0.0305	-0.0846	-0.3092
58	46	512.00	24.89	12.47	0.5595	0.0229	-0.1635	-0.0359	-0.1062	-0.3989
58	54	511.82	0.00	16.72	0.7618	0.0264	-0.2008	-0.0002	-0.0007	-0.0013
58	53	511.64	2.08	16.74	0.7643	0.0261	-0.2026	-0.0041	-0.0058	-0.0222
58	52	511.82	4.18	16.72	0.7659	0.0259	-0.2049	-0.0078	-0.0133	-0.0477
58	51	512.17	8.31	16.60	0.7674	0.0247	-0.2116	-0.0158	-0.0285	-0.1017
58	50	511.82	12.39	16.49	0.7627	0.0239	-0.2110	-0.0231	-0.0442	-0.1636
58	49	511.82	16.42	16.42	0.7531	0.0234	-0.2043	-0.0294	-0.0605	-0.2311
58	48	511.82	20.47	16.36	0.7397	0.0221	-0.1973	-0.0352	-0.0775	-0.3018
58	47	511.46	22.50	16.34	0.7304	0.0221	-0.1943	-0.0377	-0.0869	-0.3401
58	55	511.46	0.00	20.91	0.9465	0.0254	-0.2464	0.0000	-0.0015	-0.0031
58	56	511.46	2.10	20.89	0.9484	0.0253	-0.2486	-0.0049	-0.0067	-0.0260
58	57	511.64	4.16	20.87	0.9474	0.0254	-0.2508	-0.0095	-0.0143	-0.0528
58	58	511.46	8.33	20.80	0.9459	0.0233	-0.2576	-0.0172	-0.0261	-0.1035
58	59	511.46	12.44	20.76	0.9362	0.0225	-0.2483	-0.0234	-0.0369	-0.1572
58	60	511.82	16.52	20.66	0.9200	0.0219	-0.2400	-0.0303	-0.0507	-0.2201
58	61	510.93	20.46	20.46	0.8996	0.0230	-0.2266	-0.0364	-0.0672	-0.2869
58	67	511.64	0.00	25.13	1.1187	0.0238	-0.2781	-0.0002	-0.0015	-0.0037
58	66	511.64	2.12	25.17	1.1207	0.0241	-0.2782	-0.0046	-0.0039	-0.0219
58	65	511.64	4.20	25.15	1.1178	0.0234	-0.2781	-0.0094	-0.0092	-0.0469
58	64	511.46	8.37	25.04	1.1114	0.0226	-0.2788	-0.0165	-0.0178	-0.0941
58	63	511.82	12.54	25.02	1.1008	0.0211	-0.2735	-0.0223	-0.0265	-0.1433
58	62	510.58	14.58	24.88	1.0890	0.0210	-0.2701	-0.0258	-0.0328	-0.1722

TABLE VI - Continued
AERODYNAMIC CHARACTERISTICS IN SIDESLIP FOR VARIOUS ANGLES OF ATTACK.

BODY AXES; M = 2.01

Run	Pl.	q	β ,deg	α ,deg	C_N	C_A	C_m	C_l	C_n	C_Y
59	23	513.77	-0.01	0.00	-0.0199	0.0272	0.0145	-0.0002	-0.0009	0.0023
59	22	513.77	0.98	0.00	-0.0202	0.0267	0.0145	-0.0010	0.0032	-0.0095
59	21	513.77	1.99	0.00	-0.0189	0.0268	0.0144	-0.0018	0.0075	-0.0203
59	20	513.94	3.97	0.00	-0.0193	0.0269	0.0145	-0.0035	0.0159	-0.0429
59	19	513.59	5.97	0.00	-0.0181	0.0270	0.0141	-0.0051	0.0243	-0.0664
59	18	513.24	8.00	0.01	-0.0168	0.0260	0.0137	-0.0067	0.0330	-0.0918
59	17	513.94	12.00	0.00	-0.0152	0.0253	0.0128	-0.0101	0.0495	-0.1486
59	16	513.59	16.01	0.03	-0.0140	0.0242	0.0133	-0.0134	0.0655	-0.2206
59	15	513.41	20.03	0.00	-0.0127	0.0237	0.0131	-0.0171	0.0806	-0.2918
59	14	513.41	24.10	0.00	-0.0109	0.0239	0.0130	-0.0207	0.0984	-0.3697
59	13	513.77	28.11	0.00	-0.0096	0.0239	0.0140	-0.0236	0.1171	-0.4484
59	24	513.77	0.00	4.18	0.1607	0.0265	-0.0136	-0.0005	-0.0003	0.0006
59	25	513.59	2.06	4.13	0.1551	0.0264	-0.0129	-0.0025	0.0072	-0.0204
59	26	513.94	4.08	4.08	0.1535	0.0263	-0.0133	-0.0043	0.0148	-0.0421
59	27	513.41	8.08	4.03	0.1554	0.0258	-0.0139	-0.0078	0.0314	-0.0913
59	28	513.59	12.09	4.03	0.1552	0.0251	-0.0126	-0.0113	0.0482	-0.1503
59	29	513.59	16.05	4.01	0.1542	0.0244	-0.0099	-0.0149	0.0637	-0.2189
59	30	513.41	20.08	4.02	0.1483	0.0238	-0.0060	-0.0185	0.0799	-0.2932
59	31	513.41	24.19	4.02	0.1425	0.0234	-0.0039	-0.0225	0.0976	-0.3705
59	39	513.41	-0.01	8.43	0.3474	0.0262	-0.0457	-0.0004	-0.0002	0.0003
59	38	513.24	2.11	8.40	0.3459	0.0261	-0.0462	-0.0025	0.0072	-0.0212
59	37	513.41	4.17	8.32	0.3448	0.0261	-0.0470	-0.0044	0.0143	-0.0438
59	36	513.77	8.22	8.22	0.3435	0.0254	-0.0462	-0.0086	0.0294	-0.0914
59	35	513.41	12.17	8.12	0.3404	0.0245	-0.0438	-0.0130	0.0447	-0.1479
59	34	513.41	16.18	8.09	0.3298	0.0238	-0.0360	-0.0171	0.0607	-0.2181
59	33	513.41	20.19	8.07	0.3176	0.0232	-0.0294	-0.0210	0.0774	-0.2935
59	32	513.59	24.20	8.06	0.3050	0.0230	-0.0248	-0.0256	0.0955	-0.3714
59	40	513.41	-0.02	12.62	0.5274	0.0259	-0.0771	-0.0004	-0.0004	0.0009
59	41	513.24	2.10	12.60	0.5266	0.0260	-0.0770	-0.0030	0.0065	-0.0221
59	42	513.24	4.19	12.56	0.5248	0.0261	-0.0767	-0.0057	0.0133	-0.0448
59	43	513.24	8.29	12.42	0.5222	0.0245	-0.0763	-0.0112	0.0263	-0.0919
59	44	513.41	12.30	12.34	0.5149	0.0241	-0.0714	-0.0162	0.0398	-0.1496
59	45	513.41	16.33	12.23	0.5037	0.0232	-0.0621	-0.0209	0.0561	-0.2198
59	46	513.41	20.33	12.21	0.4901	0.0224	-0.0546	-0.0258	0.0730	-0.2913
59	47	513.06	24.95	12.50	0.4859	0.0226	-0.0481	-0.0316	0.0943	-0.3792
59	55	512.88	0.00	16.78	0.7035	0.0247	-0.1061	-0.0004	-0.0008	0.0025
59	54	513.06	2.09	16.79	0.7049	0.0250	-0.1076	-0.0036	0.0049	-0.0198
59	53	513.41	4.20	16.77	0.7060	0.0246	-0.1083	-0.0069	0.0112	-0.0440
59	52	513.59	8.34	16.66	0.7035	0.0231	-0.1075	-0.0133	0.0217	-0.0912
59	51	513.41	12.44	16.55	0.6941	0.0231	-0.1004	-0.0188	0.0332	-0.1465
59	50	513.06	16.48	16.48	0.6816	0.0225	-0.0911	-0.0247	0.0483	-0.2117
59	49	513.06	20.52	16.41	0.6660	0.0221	-0.0811	-0.0312	0.0670	-0.2853
59	48	513.59	22.55	16.38	0.6561	0.0220	-0.0756	-0.0342	0.0765	-0.3229
59	56	513.06	0.00	20.96	0.8815	0.0235	-0.1404	-0.0003	-0.0011	0.0032
59	57	513.41	2.11	20.97	0.8817	0.0237	-0.1406	-0.0041	0.0043	-0.0214
59	58	513.59	4.21	20.94	0.8802	0.0238	-0.1410	-0.0078	0.0090	-0.0447
59	59	513.41	8.37	20.87	0.8752	0.0224	-0.1383	-0.0145	0.0179	-0.0909
59	60	513.41	12.51	20.80	0.8646	0.0212	-0.1303	-0.0199	0.0266	-0.1403
59	61	513.41	16.57	20.72	0.8472	0.0213	-0.1187	-0.0262	0.0395	-0.2018
59	62	513.24	20.51	20.51	0.8203	0.0218	-0.1032	-0.0335	0.0585	-0.2719
59	67	513.24	2.12	25.24	1.0602	0.0226	-0.1784	-0.0039	0.0026	-0.0194
59	66	513.41	4.22	25.24	1.0592	0.0221	-0.1789	-0.0075	0.0057	-0.0411
59	65	512.88	8.40	25.11	1.0484	0.0209	-0.1736	-0.0140	0.0125	-0.0841
59	64	513.41	12.59	25.10	1.0346	0.0204	-0.1627	-0.0196	0.0206	-0.1329
59	63	513.41	14.63	24.95	1.0201	0.0207	-0.1544	-0.0226	0.0254	-0.1591

TABLE VI - Continued
 AERODYNAMIC CHARACTERISTICS IN SIDESLIP FOR VARIOUS ANGLES OF ATTACK.
 BODY AXES; M = 2.01

Run	Pt.	q	β , deg	α , deg	C_N	C_A	C_m	C_l	C_n	C_y
60	21	510.23	.00	.00	-.0161	.0134	.0019	-.0003	-.0003	.0008
60	20	509.87	2.00	.00	-.0140	.0133	.0016	-.0004	-.0024	-.0042
60	19	509.87	4.01	.00	-.0136	.0138	.0016	-.0004	-.0042	-.0093
60	18	510.23	6.04	.00	-.0130	.0138	.0016	-.0004	-.0061	-.0152
60	17	509.87	8.09	.00	-.0124	.0139	.0016	-.0004	-.0080	-.0230
60	16	510.23	12.14	.00	-.0117	.0143	.0018	-.0005	-.0107	-.0496
60	15	510.23	16.19	.00	-.0118	.0148	.0024	-.0006	-.0133	-.0899
60	14	509.87	20.24	.00	-.0101	.0153	.0022	-.0006	-.0149	-.1332
60	13	510.05	24.39	.00	-.0112	.0151	.0014	-.0010	-.0146	-.1813
60	12	510.05	28.40	.00	-.0108	.0157	.0009	-.0010	-.0137	-.2296
60	22	509.69	.00	4.17	.1675	.0135	-.0255	-.0004	-.0005	-.0002
60	23	509.87	2.05	4.12	.1598	.0134	-.0243	-.0011	-.0026	-.0041
60	24	509.87	4.10	4.10	.1563	.0141	-.0236	-.0016	-.0044	-.0094
60	25	509.69	6.12	4.07	.1567	.0143	-.0236	-.0017	-.0062	-.0163
60	26	510.05	8.15	4.07	.1554	.0150	-.0231	-.0020	-.0081	-.0232
60	27	510.05	12.21	4.07	.1554	.0154	-.0211	-.0021	-.0110	-.0504
60	28	509.69	16.20	4.05	.1547	.0157	-.0201	-.0023	-.0139	-.0888
60	29	509.69	20.28	4.07	.1506	.0160	-.0183	-.0024	-.0142	-.1361
60	30	509.87	24.42	4.06	.1421	.0155	-.0160	-.0033	-.0141	-.1844
60	39	509.52	.00	8.42	.3492	.0141	-.0554	-.0004	-.0004	-.0005
60	38	509.52	2.10	8.37	.3488	.0143	-.0560	-.0011	-.0026	-.0063
60	37	509.69	4.18	8.34	.3491	.0151	-.0567	-.0018	-.0046	-.0122
60	36	509.87	6.21	8.28	.3467	.0150	-.0557	-.0024	-.0064	-.0191
60	35	509.34	8.26	8.26	.3458	.0153	-.0540	-.0031	-.0084	-.0279
60	34	509.69	12.26	8.22	.3416	.0155	-.0519	-.0041	-.0126	-.0525
60	33	509.69	16.30	8.15	.3294	.0153	-.0433	-.0049	-.0145	-.0924
60	32	509.87	20.37	8.15	.3187	.0155	-.0415	-.0056	-.0144	-.1407
60	31	510.05	24.42	8.14	.3063	.0160	-.0377	-.0067	-.0134	-.1898
60	40	509.52	.00	12.61	.5309	.0155	-.0860	-.0005	-.0003	.0001
60	41	508.81	2.09	12.58	.5257	.0155	-.0849	-.0017	-.0024	.0075
60	42	509.16	4.19	12.56	.5252	.0155	-.0853	-.0029	-.0048	.0146
60	43	509.69	6.25	12.50	.5236	.0155	-.0851	-.0043	-.0071	.0226
60	44	509.52	8.30	12.44	.5216	.0158	-.0836	-.0056	-.0095	.0322
60	45	509.16	12.38	12.38	.5116	.0156	-.0756	-.0077	-.0135	.0607
60	46	510.05	16.43	12.30	.4978	.0157	-.0652	-.0093	-.0142	.1015
60	47	508.63	20.48	12.31	.4867	.0158	-.0624	-.0107	-.0153	.1433
60	48	508.10	25.12	12.60	.4850	.0163	-.0607	-.0127	-.0144	.1972
60	56	509.34	.00	16.77	.7047	.0151	-.1134	-.0006	-.0003	.0007
60	55	509.34	2.09	16.78	.7049	.0151	-.1145	-.0022	-.0038	.0062
60	54	509.69	4.17	16.77	.7063	.0156	-.1154	-.0039	-.0061	.0159
60	53	509.52	6.24	16.74	.7048	.0156	-.1149	-.0058	-.0077	.0274
60	52	509.34	8.31	16.67	.6998	.0155	-.1115	-.0076	-.0100	.0393
60	51	509.69	12.47	16.58	.6902	.0154	-.1038	-.0110	-.0144	.0675
60	50	509.52	16.54	16.54	.6778	.0160	-.0928	-.0141	-.0152	.1057
60	49	509.69	20.64	16.51	.6626	.0156	-.0867	-.0169	-.0165	.1459
60	57	509.34	.00	20.96	.8827	.0145	-.1475	-.0005	.0000	.0003
60	58	509.52	2.11	20.94	.8806	.0146	-.1476	-.0028	-.0018	.0121
60	59	509.69	4.21	20.93	.8781	.0146	-.1468	-.0049	-.0044	.0231
60	60	509.87	6.29	20.91	.8755	.0145	-.1447	-.0069	-.0064	.0347
60	61	509.34	8.37	20.87	.8707	.0149	-.1416	-.0091	-.0086	.0468
60	62	509.34	12.54	20.84	.8597	.0151	-.1318	-.0129	-.0138	.0723
60	63	509.69	16.63	20.79	.8407	.0155	-.1189	-.0169	-.0156	.1081
60	64	509.52	20.60	20.60	.8158	.0163	-.1074	-.0205	-.0175	.1440
60	71	509.52	.00	25.18	1.0600	.0135	-.1856	-.0006	.0002	.0001
60	70	509.52	2.12	25.21	1.0589	.0134	-.1853	-.0028	-.0019	.0131
60	69	509.52	4.21	25.22	1.0562	.0133	-.1841	-.0051	-.0033	.0268
60	68	509.34	6.28	25.17	1.0521	.0140	-.1812	-.0072	-.0048	.0399
60	67	509.52	8.40	25.11	1.0458	.0139	-.1769	-.0096	-.0067	.0533
60	66	509.52	12.55	25.13	1.0297	.0149	-.1631	-.0138	-.0116	.0795
60	65	509.16	14.64	24.97	1.0143	.0148	-.1535	-.0160	-.0139	.0944

TABLE VI - Continued
AERODYNAMIC CHARACTERISTICS IN SIDESLIP FOR VARIOUS ANGLES OF ATTACK.

BODY AXES; M = 2.01

Run	Pt.	q	β , deg	α , deg	C_N	C_A	C_m	C_l	C_n	C_y
61	21	509.34	-0.1	0.0	-0.126	0.148	-0.014	0.002	-0.003	-0.001
61	20	509.52	2.02	0.0	-0.117	0.148	-0.026	0.018	-0.024	-0.086
61	19	509.34	4.03	0.1	-0.094	0.152	-0.059	0.035	-0.044	-0.162
61	18	509.69	6.06	0.0	-0.071	0.155	-0.100	0.052	-0.064	-0.249
61	17	509.16	8.10	0.0	-0.033	0.159	-0.155	0.071	-0.085	-0.353
61	16	508.28	12.16	0.2	-0.010	0.163	-0.212	0.107	-0.110	-0.655
61	15	509.52	16.20	0.0	-0.177	0.169	-0.088	0.143	-0.137	-1.056
61	14	508.99	20.28	0.4	-0.360	0.175	0.012	0.181	-0.153	-1.534
61	13	509.87	24.40	0.0	-0.552	0.183	0.062	0.206	-0.162	-2.037
61	12	508.28	28.45	0.0	-0.700	0.183	0.064	0.229	-0.176	-2.522
61	22	509.16	0.0	4.16	0.1685	0.151	-0.294	0.002	-0.007	-0.001
61	23	509.34	2.06	4.13	0.1635	0.153	-0.300	0.012	-0.031	-0.058
61	24	509.34	4.10	4.10	0.1639	0.158	-0.323	0.026	-0.053	-0.128
61	25	509.34	6.12	4.07	0.1630	0.158	-0.354	0.042	-0.074	-0.204
61	26	509.34	8.15	4.09	0.1669	0.163	-0.403	0.058	-0.091	-0.300
61	27	509.52	12.22	4.07	0.1703	0.171	-0.452	0.091	-0.119	-0.581
61	28	509.16	16.22	4.05	0.1533	0.175	-0.352	0.121	-0.122	-1.007
61	29	508.99	20.28	4.07	0.1330	0.176	-0.243	0.149	-0.135	-1.479
61	30	509.69	24.43	4.07	0.1129	0.177	-0.194	0.168	-0.143	-1.976
61	39	509.34	-0.1	8.41	0.3516	0.154	-0.580	0.004	-0.008	0.004
61	38	509.16	2.10	8.37	0.3486	0.155	-0.587	0.017	-0.036	-0.052
61	37	509.52	4.18	8.33	0.3476	0.157	-0.609	0.029	-0.058	-0.119
61	36	509.16	6.21	8.28	0.3476	0.163	-0.639	0.039	-0.079	-0.197
61	35	508.81	8.25	8.25	0.3484	0.164	-0.673	0.050	-0.094	-0.295
61	34	509.69	12.26	8.18	0.3434	0.167	-0.680	0.071	-0.110	-0.591
61	33	509.69	16.28	8.14	0.3246	0.167	-0.599	0.088	-0.109	-1.012
61	32	509.52	20.35	8.14	0.3008	0.171	-0.492	0.108	-0.122	-1.448
61	31	509.34	24.41	8.14	0.2767	0.168	-0.438	0.121	-0.137	-1.898
61	40	509.16	-0.2	12.61	0.5257	0.167	-0.828	0.004	-0.008	0.010
61	41	509.52	2.09	12.58	0.5246	0.166	-0.839	0.011	-0.037	-0.046
61	42	509.34	4.21	12.54	0.5234	0.164	-0.863	0.017	-0.061	-0.117
61	43	509.34	6.24	12.49	0.5226	0.171	-0.888	0.020	-0.074	-0.218
61	44	509.52	8.30	12.44	0.5224	0.169	-0.908	0.023	-0.091	-0.324
61	45	509.34	12.36	12.36	0.5085	0.164	-0.849	0.031	-0.096	-0.644
61	46	509.34	16.37	12.30	0.4945	0.170	-0.822	0.039	-0.114	-1.005
61	47	509.34	20.44	12.28	0.4724	0.169	-0.755	0.049	-0.123	-1.412
61	48	509.34	25.11	12.59	0.4521	0.169	-0.679	0.053	-0.133	-1.908
61	56	509.87	0.0	16.78	0.7008	0.160	-1.044	0.003	-0.008	0.015
61	55	510.05	2.06	16.80	0.7013	0.158	-1.058	0.003	-0.033	-0.065
61	54	509.16	4.20	16.78	0.7002	0.161	-1.074	0.001	-0.049	-0.174
61	53	508.63	6.24	16.72	0.6967	0.165	-1.066	-0.003	-0.048	-0.311
61	52	507.92	8.34	16.66	0.6898	0.165	-1.036	-0.006	-0.063	-0.442
61	51	509.69	12.43	16.59	0.6841	0.165	-1.021	-0.016	-0.088	-0.709
61	50	509.52	16.51	16.51	0.6701	0.164	-1.027	-0.022	-0.107	-1.025
61	49	509.52	20.58	16.46	0.6463	0.165	-0.988	-0.027	-0.121	-1.392
61	57	508.45	0.0	20.97	0.8769	0.154	-1.290	0.003	-0.013	0.040
61	58	508.99	2.11	20.95	0.8744	0.153	-1.293	-0.001	-0.031	-0.077
61	59	509.52	4.21	20.94	0.8721	0.157	-1.296	-0.010	-0.049	-0.198
61	60	509.52	6.26	20.94	0.8703	0.161	-1.300	-0.019	-0.068	-0.305
61	61	509.16	8.33	20.90	0.8659	0.159	-1.290	-0.029	-0.076	-0.438
61	62	509.69	12.49	20.85	0.8542	0.161	-1.245	-0.048	-0.078	-0.740
61	63	508.99	16.59	20.74	0.8372	0.161	-1.231	-0.065	-0.100	-1.036
61	64	509.52	20.57	20.57	0.8102	0.167	-1.187	-0.077	-0.122	-1.358
61	70	508.99	-0.5	25.23	1.0575	0.147	-1.605	0.004	-0.021	0.048
61	69	509.52	2.12	25.26	1.0561	0.150	-1.591	-0.005	-0.039	-0.068
61	68	508.99	4.22	25.25	1.0534	0.149	-1.581	-0.015	-0.058	-0.177
61	67	508.99	6.29	25.20	1.0479	0.152	-1.575	-0.027	-0.078	-0.290
61	66	509.34	8.40	25.12	1.0417	0.158	-1.573	-0.040	-0.091	-0.416
61	65	508.81	12.59	25.10	1.0284	0.159	-1.516	-0.066	-0.093	-0.717

TABLE VI - Continued
 AERODYNAMIC CHARACTERISTICS IN SIDESLIP FOR VARIOUS ANGLES OF ATTACK.
 BODY AXES; M = 2.01

Run	Pt.	q	β , deg	α , deg	C_N	C_A	C_m	C_l	C_n	C_Y
62	21	510.40	-0.1	0.0	-0.118	0.147	0.033	-0.001	-0.002	-0.028
62	20	508.81	2.02	0.0	-0.130	0.148	0.047	-0.018	-0.023	-0.097
62	19	511.64	4.03	0.0	-0.140	0.149	0.078	-0.035	-0.044	-0.174
62	18	510.23	6.06	0.0	-0.163	0.152	0.125	-0.053	-0.066	-0.262
62	17	510.40	8.12	0.0	-0.201	0.156	0.181	-0.071	-0.086	-0.367
62	16	510.40	12.17	0.0	-0.226	0.155	0.245	-0.106	-0.108	-0.662
62	71	510.58	12.17	0.0	-0.274	0.160	0.256	-0.106	-0.106	-0.681
62	15	510.76	16.22	-0.3	-0.077	0.164	0.134	-0.143	-0.133	-0.166
62	14	510.76	20.28	0.0	0.146	0.166	0.025	-0.179	-0.145	-0.1562
62	13	509.52	24.40	0.0	0.288	0.168	-0.028	-0.212	-0.153	-0.2055
62	12	510.40	28.46	0.0	0.412	0.172	-0.031	-0.235	-0.151	-0.2561
62	22	510.58	0.0	4.17	0.1674	0.148	-0.0242	-0.002	-0.004	-0.029
62	23	510.40	2.06	4.13	0.1610	0.147	-0.0219	-0.028	-0.020	-0.125
62	24	510.40	4.11	4.11	0.1556	0.150	-0.0182	-0.050	-0.036	-0.226
62	25	510.23	6.14	4.10	0.1528	0.151	-0.0137	-0.069	-0.055	-0.332
62	26	510.58	8.17	4.08	0.1471	0.153	-0.0078	-0.090	-0.077	-0.439
62	27	510.40	12.25	4.08	0.1504	0.157	-0.0032	-0.127	-0.110	-0.766
62	28	510.40	16.24	4.09	0.1663	0.166	-0.0128	-0.166	-0.153	-0.1146
62	29	509.69	20.32	4.11	0.1862	0.169	-0.0223	-0.208	-0.174	-0.1617
62	30	510.05	24.49	4.08	0.1968	0.172	-0.0236	-0.249	-0.175	-0.2146
62	39	510.23	0.0	8.41	0.3520	0.149	-0.0568	-0.002	-0.004	-0.032
62	38	510.23	2.11	8.39	0.3483	0.148	-0.0551	-0.028	-0.021	-0.155
62	37	510.23	4.18	8.34	0.3458	0.151	-0.0519	-0.054	-0.037	-0.278
62	36	510.23	6.23	8.31	0.3437	0.158	-0.0470	-0.078	-0.057	-0.394
62	35	510.23	8.28	8.28	0.3397	0.161	-0.0406	-0.104	-0.080	-0.545
62	34	510.58	12.32	8.22	0.3407	0.165	-0.0347	-0.149	-0.124	-0.873
62	33	509.87	16.37	8.18	0.3477	0.168	-0.0345	-0.196	-0.169	-1.268
62	32	510.23	20.45	8.18	0.3542	0.165	-0.0380	-0.243	-0.199	-0.1716
62	31	510.05	24.50	8.17	0.3607	0.173	-0.0419	-0.291	-0.193	-0.2226
62	40	510.23	0.0	12.61	0.5319	0.155	-0.0876	-0.004	-0.003	-0.035
62	41	510.23	2.09	12.59	0.5278	0.155	-0.0856	-0.035	-0.020	-0.184
62	42	510.05	4.19	12.57	0.5234	0.155	-0.0820	-0.066	-0.037	-0.329
62	43	510.05	6.26	12.51	0.5194	0.154	-0.0768	-0.096	-0.059	-0.483
62	44	510.05	8.33	12.47	0.5145	0.157	-0.0697	-0.126	-0.084	-0.642
62	45	510.40	12.42	12.42	0.5108	0.164	-0.0593	-0.187	-0.130	-1.005
62	46	510.05	16.48	12.35	0.5095	0.162	-0.0517	-0.242	-0.152	-1.458
62	47	510.23	20.55	12.35	0.5114	0.164	-0.0519	-0.294	-0.182	-1.912
62	48	510.76	25.24	12.66	0.5334	0.171	-0.0676	-0.351	-0.174	-2.490
62	56	510.40	0.0	16.76	0.7095	0.148	-0.1189	-0.004	-0.002	-0.029
62	54	510.05	4.20	16.78	0.7054	0.145	-0.1135	-0.076	-0.030	-0.400
62	53	510.05	6.28	16.74	0.7039	0.149	-0.1117	-0.110	-0.034	-0.608
62	52	510.40	8.36	16.70	0.6998	0.149	-0.1063	-0.143	-0.050	-0.800
62	51	509.69	12.50	16.62	0.6873	0.156	-0.0896	-0.209	-0.115	-1.188
62	50	509.87	16.60	16.60	0.6781	0.156	-0.0772	-0.275	-0.114	-1.706
62	49	509.69	20.72	16.57	0.6727	0.161	-0.0732	-0.338	-0.152	-2.148
62	57	509.87	0.0	20.95	0.8752	0.130	-0.1482	-0.004	0.001	-0.023
62	58	509.69	2.11	20.93	0.8724	0.131	-0.1497	-0.044	0.012	-0.280
62	59	509.69	4.17	20.92	0.8723	0.131	-0.1486	-0.083	0.002	-0.502
62	60	510.05	6.29	20.92	0.8682	0.135	-0.1450	-0.119	-0.008	-0.729
62	61	511.11	8.37	20.87	0.8612	0.134	-0.1381	-0.157	-0.019	-0.948
62	62	511.11	12.56	20.89	0.8547	0.144	-0.1219	-0.230	-0.086	-1.370
62	63	507.92	16.66	20.82	0.8312	0.149	-0.1061	-0.295	-0.091	-1.859
62	64	510.23	20.66	20.66	0.8177	0.154	-0.0966	-0.352	-0.121	-2.305
62	70	510.40	0.0	25.17	1.0462	0.119	-0.1887	-0.003	0.004	-0.026
62	69	510.23	2.12	25.21	1.0439	0.117	-0.1853	-0.052	0.016	-0.308
62	68	510.05	4.21	25.19	1.0418	0.119	-0.1835	-0.089	0.010	-0.555
62	67	510.05	6.33	25.15	1.0345	0.123	-0.1783	-0.127	0.007	-0.788
62	66	510.05	8.39	25.10	1.0270	0.122	-0.1727	-0.164	-0.001	-1.023
62	65	510.23	12.60	25.12	1.0087	0.129	-0.1539	-0.241	-0.020	-1.516

TABLE VI - Continued
 AERODYNAMIC CHARACTERISTICS IN SIDESLIP FOR VARIOUS ANGLES OF ATTACK.
 BODY AXES; M = 2.01

Run	Pt.	q	β , deg	α , deg	C_N	C_A	C_m	C_l	C_n	C_Y
63	23	510.23	-.01	.00	-.0044	.0184	-.0069	.0000	-.0004	.0003
63	22	510.23	.99	.00	-.0043	.0184	-.0065	-.0012	.0036	-.0115
63	21	510.23	1.99	.00	-.0040	.0185	-.0062	-.0024	.0078	-.0241
63	20	510.23	3.97	.00	-.0038	.0187	-.0058	-.0049	.0158	-.0487
63	19	510.23	5.99	.00	-.0042	.0186	-.0031	-.0078	.0244	-.0761
63	18	510.05	8.01	.00	-.0063	.0187	.0009	-.0108	.0331	-.1036
63	17	510.23	12.02	-.02	-.0132	.0192	.0158	-.0175	.0506	-.1676
63	16	510.05	16.02	.03	-.0061	.0190	.0269	-.0251	.0660	-.2372
63	15	510.23	20.06	.00	.0011	.0182	.0425	-.0335	.0839	-.3175
63	14	509.69	24.13	.00	.0050	.0180	.0564	-.0400	.1011	-.3978
63	13	509.69	28.14	.00	.0108	.0174	.0692	-.0448	.1181	-.4778
63	24	510.23	-.01	4.14	.1946	.0188	-.0677	-.0002	.0005	-.0029
63	25	510.23	2.05	4.11	.1871	.0192	-.0650	-.0034	.0072	-.0263
63	26	510.40	4.08	4.08	.1844	.0191	-.0631	-.0064	.0147	-.0522
63	27	510.23	8.09	4.03	.1806	.0191	-.0559	-.0126	.0311	-.1084
63	28	509.87	12.15	4.05	.1767	.0194	-.0417	-.0199	.0474	-.1740
63	29	509.87	16.10	4.02	.1800	.0192	-.0283	-.0277	.0616	-.2417
63	30	509.87	20.12	4.07	.1885	.0188	-.0157	-.0360	.0766	-.3160
63	31	510.76	24.25	4.08	.1948	.0185	-.0028	-.0434	.0938	-.3974
63	39	509.69	-.01	8.37	.3956	.0196	-.1217	-.0001	.0002	-.0021
63	38	510.76	2.09	8.34	.3937	.0202	-.1207	-.0034	.0066	-.0280
63	37	509.52	4.16	8.31	.3897	.0198	-.1178	-.0068	.0135	-.0542
63	36	510.58	8.20	8.20	.3858	.0202	-.1096	-.0137	.0290	-.1145
63	35	510.23	12.21	8.15	.3832	.0205	-.0979	-.0216	.0433	-.1781
63	34	510.23	16.23	8.11	.3810	.0202	-.0826	-.0299	.0556	-.2449
63	33	509.87	20.28	8.07	.3767	.0190	-.0680	-.0388	.0693	-.3175
63	32	510.40	24.29	8.09	.3769	.0194	-.0567	-.0467	.0848	-.3947
63	40	510.05	-.02	12.56	.5863	.0214	-.1738	-.0003	.0001	-.0022
63	41	510.05	2.06	12.53	.5828	.0206	-.1723	-.0042	.0059	-.0297
63	42	510.05	4.15	12.52	.5790	.0207	-.1687	-.0082	.0122	-.0587
63	43	509.87	8.25	12.41	.5713	.0207	-.1586	-.0160	.0255	-.1196
63	44	510.05	12.34	12.34	.5672	.0203	-.1461	-.0245	.0371	-.1817
63	45	510.40	16.36	12.25	.5589	.0201	-.1265	-.0328	.0480	-.2488
63	46	510.76	20.41	12.26	.5536	.0193	-.1135	-.0416	.0615	-.3223
63	47	510.40	25.04	12.55	.5639	.0192	-.1085	-.0516	.0782	-.4085
63	55	510.40	.00	16.70	.7743	.0214	-.2311	-.0002	-.0003	.0005
63	54	510.40	2.08	16.71	.7738	.0211	-.2301	-.0046	.0048	-.0282
63	53	510.40	4.18	16.71	.7719	.0213	-.2261	-.0088	.0106	-.0607
63	52	510.40	8.28	16.63	.7658	.0206	-.2164	-.0173	.0211	-.1209
63	51	510.76	12.43	16.53	.7566	.0203	-.2022	-.0250	.0304	-.1858
63	50	510.58	16.50	16.50	.7435	.0198	-.1815	-.0335	.0404	-.2545
63	49	509.87	20.58	16.45	.7268	.0193	-.1613	-.0430	.0521	-.3244
63	48	510.05	22.63	16.44	.7237	.0195	-.1540	-.0478	.0596	-.3618
63	56	510.05	.00	20.86	.9616	.0206	-.2902	.0000	-.0007	.0014
63	57	510.23	2.10	20.84	.9600	.0203	-.2899	-.0049	.0043	-.0316
63	58	510.76	4.19	20.82	.9576	.0201	-.2865	-.0096	.0084	-.0632
63	59	509.87	8.33	20.79	.9459	.0196	-.2762	-.0175	.0144	-.1201
63	60	510.58	12.48	20.76	.9339	.0194	-.2598	-.0252	.0235	-.1868
63	61	509.69	16.55	20.76	.9183	.0197	-.2393	-.0329	.0327	-.2536
63	62	510.76	20.56	20.56	.8946	.0193	-.2135	-.0418	.0446	-.3229
63	68	510.40	.00	25.04	1.1468	.0204	-.3575	.0000	-.0012	.0024
63	67	510.58	2.11	25.10	1.1463	.0196	-.3542	-.0053	.0012	-.0281
63	66	510.40	4.19	25.09	1.1419	.0196	-.3522	-.0094	.0034	-.0572
63	65	509.87	8.31	25.00	1.1296	.0185	-.3422	-.0170	.0088	-.1148
63	64	509.34	12.54	25.01	1.1112	.0188	-.3215	-.0243	.0162	-.1805
63	63	510.93	14.56	24.93	1.0995	.0188	-.3086	-.0279	.0210	-.2153

TABLE VI - Continued
 AERODYNAMIC CHARACTERISTICS IN SIDESLIP FOR VARIOUS ANGLES OF ATTACK.
 BODY AXES; M = 2.01

Run	Pt.	q	β ,deg	α ,deg	C_N	C_A	C_m	C_l	C_n	C_Y
64	21	512.88	.00	.00	-.0081	.0295	.0129	-.0002	-.0008	.0006
64	20	512.70	2.01	.00	-.0072	.0296	.0130	-.0030	.0072	-.0247
64	19	512.88	3.98	.00	-.0079	.0293	.0136	-.0061	.0150	-.0490
64	18	512.35	5.98	.00	-.0067	.0291	.0142	-.0095	.0234	-.0754
64	17	512.35	8.02	.00	-.0067	.0290	.0147	-.0132	.0322	-.1045
64	16	510.93	12.03	.00	-.0014	.0285	.0118	-.0211	.0495	-.1667
64	15	511.64	16.03	.00	.0226	.0277	-.0101	-.0306	.0677	-.2422
64	14	512.70	20.04	.00	.0511	.0268	-.0335	-.0408	.0905	-.3301
64	13	511.64	22.09	.00	.0651	.0271	-.0441	-.0454	.1012	-.3749
64	22	512.70	.00	4.18	.1776	.0282	-.0283	.0000	-.0001	-.0012
64	23	512.35	2.06	4.13	.1754	.0283	-.0293	-.0040	.0071	-.0268
64	24	512.35	4.09	4.09	.1721	.0279	-.0308	-.0077	.0146	-.0525
64	25	512.53	8.10	4.04	.1753	.0275	-.0378	-.0155	.0318	-.1106
64	26	512.53	12.14	4.04	.1872	.0271	-.0494	-.0247	.0503	-.1794
64	27	512.00	16.07	4.02	.2064	.0269	-.0657	-.0347	.0692	-.2548
64	28	512.35	20.09	4.06	.2304	.0254	-.0795	-.0445	.0889	-.3371
64	35	512.70	.00	8.39	.3716	.0275	-.0873	.0000	-.0002	-.0003
64	34	512.70	2.10	8.36	.3706	.0275	-.0884	-.0043	.0069	-.0282
64	33	512.17	4.17	8.31	.3703	.0268	-.0909	-.0087	.0142	-.0555
64	32	512.53	8.22	8.22	.3780	.0268	-.1033	-.0183	.0320	-.1187
64	31	512.53	12.19	8.14	.3888	.0266	-.1126	-.0284	.0507	-.1899
64	30	512.35	16.20	8.10	.3969	.0264	-.1124	-.0381	.0672	-.2633
64	29	512.53	20.22	8.08	.4067	.0248	-.1178	-.0480	.0855	-.3448
64	36	512.53	.00	12.56	.5734	.0271	-.1563	-.0002	-.0003	-.0004
64	37	512.70	2.09	12.54	.5731	.0268	-.1577	-.0055	.0069	-.0308
64	38	512.53	4.17	12.52	.5723	.0271	-.1594	-.0108	.0144	-.0619
64	39	512.53	8.27	12.39	.5746	.0259	-.1629	-.0214	.0309	-.1272
64	40	512.53	12.31	12.31	.5793	.0257	-.1633	-.0325	.0484	-.1989
64	41	512.53	16.33	12.23	.5792	.0252	-.1558	-.0428	.0655	-.2759
64	47	512.53	.00	16.71	.7750	.0260	-.2240	-.0001	-.0005	.0005
64	46	512.70	2.08	16.71	.7742	.0258	-.2241	-.0057	.0069	-.0322
64	45	512.53	4.18	16.71	.7722	.0257	-.2217	-.0113	.0144	-.0659
64	44	512.53	8.32	16.62	.7670	.0249	-.2184	-.0223	.0283	-.1323
64	43	512.35	12.41	16.51	.7646	.0238	-.2159	-.0334	.0446	-.2080
64	42	512.35	16.48	16.48	.7532	.0245	-.1973	-.0436	.0597	-.2842
64	48	512.53	.00	20.88	.9565	.0241	-.2753	.0000	-.0009	.0023
64	49	513.24	2.10	20.86	.9552	.0237	-.2742	-.0057	.0059	-.0336
64	50	511.64	4.19	20.84	.9524	.0239	-.2741	-.0110	.0111	-.0655
64	51	512.70	8.29	20.80	.9519	.0218	-.2765	-.0228	.0250	-.1363
64	52	513.06	12.49	20.77	.9389	.0227	-.2585	-.0330	.0389	-.2104
64	53	512.70	16.57	20.72	.9231	.0227	-.2355	-.0422	.0512	-.2830
64	58	512.53	.00	25.09	1.1265	.0234	-.3149	-.0003	-.0012	.0031
64	57	512.53	2.11	25.12	1.1255	.0230	-.3121	-.0061	.0034	-.0305
64	56	512.53	4.20	25.13	1.1233	.0225	-.3112	-.0110	.0071	-.0606
64	55	512.70	8.32	25.02	1.1151	.0207	-.3078	-.0208	.0175	-.1279
64	54	512.35	12.55	25.03	1.1001	.0199	-.2926	-.0303	.0291	-.1996

TABLE VI - Concluded
 AERODYNAMIC CHARACTERISTICS IN SIDESLIP FOR VARIOUS ANGLES OF ATTACK.
 BODY AXES; M = 2.01

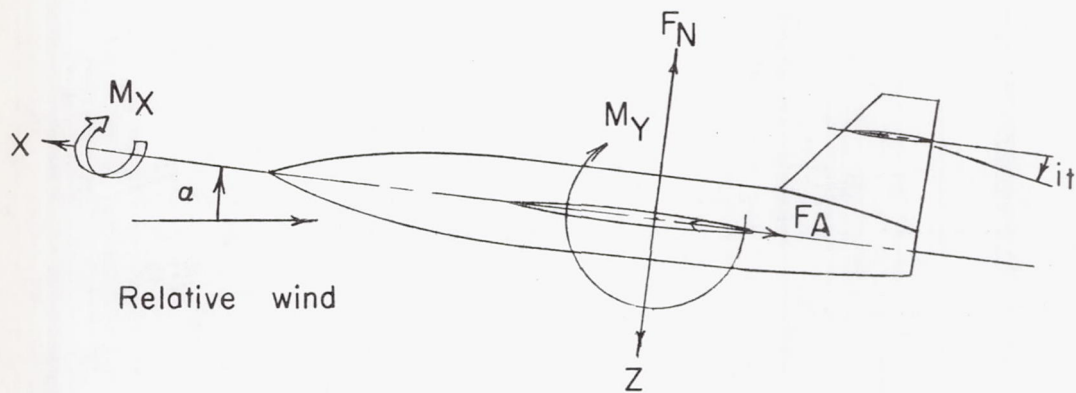
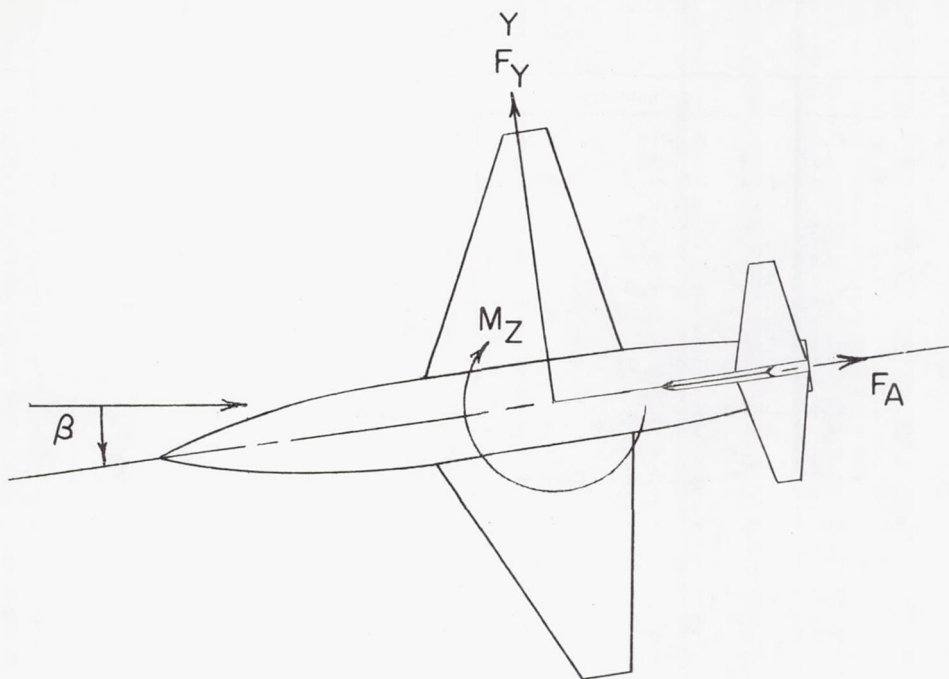
Run	Pt.	q	β , deg	α , deg	C_N	C_A	C_m	C_l	C_n	C_y
65	21	510.40	.00	.00	.0112	.0052	-.0048	.0000	-.0001	-.0011
65	20	510.23	2.01	.00	.0131	.0059	-.0051	.0000	-.0027	-.0041
65	19	510.58	4.01	.00	.0136	.0063	-.0051	.0000	-.0050	-.0090
65	18	510.05	6.05	.00	.0141	.0063	-.0050	.0000	-.0073	-.0140
65	17	510.23	8.09	.00	.0163	.0064	-.0054	.0000	-.0093	-.0217
65	16	510.23	12.14	.00	.0150	.0066	-.0050	.0000	-.0136	-.0444
65	15	510.05	16.19	.00	.0150	.0066	-.0045	.0000	-.0148	-.0877
65	14	510.05	20.25	.00	.0138	.0064	-.0037	.0000	-.0156	-.1347
65	13	510.23	24.37	.00	.0124	.0068	-.0043	.0000	-.0155	-.1828
65	12	510.05	28.41	.05	.0129	.0077	-.0037	.0000	-.0144	-.2320
65	22	510.23	.00	4.02	.0210	.0064	.0099	.0000	-.0005	-.0009
65	23	510.58	2.01	4.03	.0188	.0067	.0096	.0000	-.0028	-.0056
65	24	510.05	4.03	4.03	.0174	.0066	.0093	.0000	-.0051	-.0101
65	25	510.23	6.05	4.04	.0174	.0070	.0093	.0000	-.0072	-.0159
65	26	510.40	8.08	4.03	.0185	.0069	.0088	.0000	-.0094	-.0226
65	27	510.58	12.17	4.05	.0204	.0067	.0086	.0000	-.0132	-.0472
65	28	510.05	16.17	4.07	.0258	.0068	.0076	.0000	-.0143	-.0881
65	29	510.40	20.25	4.10	.0296	.0071	.0068	.0000	-.0153	-.1343
65	30	510.58	24.42	4.06	.0316	.0070	.0043	.0000	-.0152	-.1838
65	39	510.93	.00	8.09	.0305	.0066	.0219	.0000	-.0004	-.0011
65	38	509.69	2.01	8.08	.0304	.0066	.0215	.0000	-.0027	-.0054
65	37	510.58	4.05	8.08	.0321	.0068	.0211	.0000	-.0050	-.0116
65	36	510.40	6.05	8.10	.0335	.0067	.0213	.0000	-.0072	-.0186
65	35	510.58	8.09	8.12	.0348	.0068	.0214	.0000	-.0096	-.0264
65	34	510.23	12.13	8.10	.0448	.0069	.0184	.0000	-.0124	-.0559
65	33	510.05	16.18	8.09	.0531	.0068	.0150	.0000	-.0137	-.0956
65	32	511.11	20.27	8.10	.0589	.0068	.0131	.0000	-.0148	-.1383
65	31	510.76	24.33	8.11	.0628	.0069	.0095	.0000	-.0147	-.1852
65	40	510.40	.00	12.14	.0499	.0070	.0337	.0000	-.0005	-.0003
65	41	510.05	2.02	12.14	.0513	.0069	.0327	.0000	-.0024	-.0077
65	42	510.05	4.02	12.13	.0533	.0069	.0317	.0000	-.0043	-.0160
65	43	510.05	6.06	12.12	.0557	.0068	.0312	.0000	-.0065	-.0250
65	44	510.58	8.06	12.13	.0605	.0071	.0289	.0000	-.0078	-.0372
65	45	510.40	12.14	12.14	.0700	.0071	.0255	.0000	-.0107	-.0663
65	46	510.05	16.20	12.13	.0795	.0068	.0234	.0000	-.0125	-.1041
65	47	510.58	20.28	12.18	.0860	.0068	.0200	.0000	-.0138	-.1437
65	48	510.40	24.95	12.50	.0975	.0072	.0151	.0000	-.0134	-.1968
65	56	510.58	.00	16.17	.0966	.0066	.0361	.0000	-.0003	-.0005
65	55	510.76	2.01	16.21	.0972	.0066	.0361	.0000	-.0021	-.0104
65	54	510.93	4.05	16.19	.0975	.0065	.0350	.0000	-.0038	-.0217
65	53	510.58	6.06	16.19	.0992	.0070	.0340	.0000	-.0052	-.0337
65	52	510.40	8.09	16.18	.1039	.0073	.0320	.0000	-.0062	-.0478
65	51	510.40	12.16	16.18	.1119	.0069	.0301	.0000	-.0093	-.0774
65	50	510.40	16.23	16.23	.1168	.0065	.0277	.0000	-.0112	-.1117
65	49	510.40	20.33	16.25	.1240	.0069	.0232	.0000	-.0123	-.1514
65	57	510.58	.00	20.22	.1433	.0065	.0382	.0000	-.0001	-.0007
65	58	510.40	2.03	20.23	.1432	.0064	.0382	.0000	-.0016	-.0133
65	59	510.23	4.06	20.23	.1430	.0064	.0380	.0000	-.0029	-.0272
65	60	510.40	6.07	20.23	.1457	.0071	.0375	.0000	-.0042	-.0404
65	61	510.05	8.09	20.24	.1467	.0069	.0367	.0000	-.0055	-.0540
65	62	510.05	12.17	20.27	.1526	.0073	.0330	.0000	-.0079	-.0845
65	63	510.40	16.19	20.32	.1590	.0071	.0294	.0000	-.0098	-.1189
65	64	511.11	20.17	20.23	.1629	.0074	.0253	.0000	-.0107	-.1561
65	70	510.23	.00	24.32	.1900	.0071	.0387	.0000	-.0003	-.0008
65	69	510.93	2.04	24.36	.1905	.0071	.0385	.0000	-.0015	-.0143
65	68	510.40	4.05	24.37	.1899	.0070	.0383	.0000	-.0028	-.0289
65	67	510.40	6.10	24.35	.1923	.0068	.0373	.0000	-.0040	-.0437
65	66	510.58	8.11	24.33	.1927	.0068	.0365	.0000	-.0049	-.0588
65	65	510.93	12.19	24.38	.1980	.0077	.0326	.0000	-.0068	-.0903

TABLE VII.- RUN LOG

Run	Configuration	i_t , deg	Mach number	
2, 4	B	H off	1.41	
5	BW _H	↓	↓	
6	BW _L	0		
7	BW _M	0		
8	BW _M ^V	↓		
9	BW _M VH _H	0		
10	BW _M VH _H	-6		
11	BW _M VH _L	-6		
12	BW _M VH _L	0		
15	BW _H VH _H	0		
16	BW _H VH _H	-6		
17	BW _H VH _L	-6		
18	BW _H VH _L	0		
19	BW _H ^V	H off		
21	BW _L ^V	↓		
22	BW _L VH _L	0		
23	BW _L VH _L	-6		
24	BW _L VH _H	-6		
25	BW _L VH _H	0		
26	BVH _H	0		
27	BVH _H	-6		
28	BVH _L	-6		
29	BVH _L	0		
30	BV	H off		2.01
39	BVH _H	0		
40	BVH _H	-6		
41	BVH _L	-6		
42	BVH _L	0		
43	BW _L VH _L	0		
44	BW _L VH _L	-6		
45	BW _L VH _H	-6		
46	BW _L VH _H	0		
47	BW _L ^V	H off		
48, 49	BV	↓		
50	BW _H ^V	0		
51	BW _H VH _H	-6		
52	BW _H VH _H	-6		
53	BW _H VH _L	0		
54	BW _H VH _L	0		
55	BW _M VH _L	-6		
56	BW _M VH _L	-6		
57	BW _M VH _H	0		
58	BW _M VH _H	H off		
59	BW _M ^V	↓		
60	BW _M	0		
61	BW _L	↓		
62	BW _H	0		
63	BW _H VH _L *	0		
64	BW _H VH [†]	0		
65	B	H off	↓	

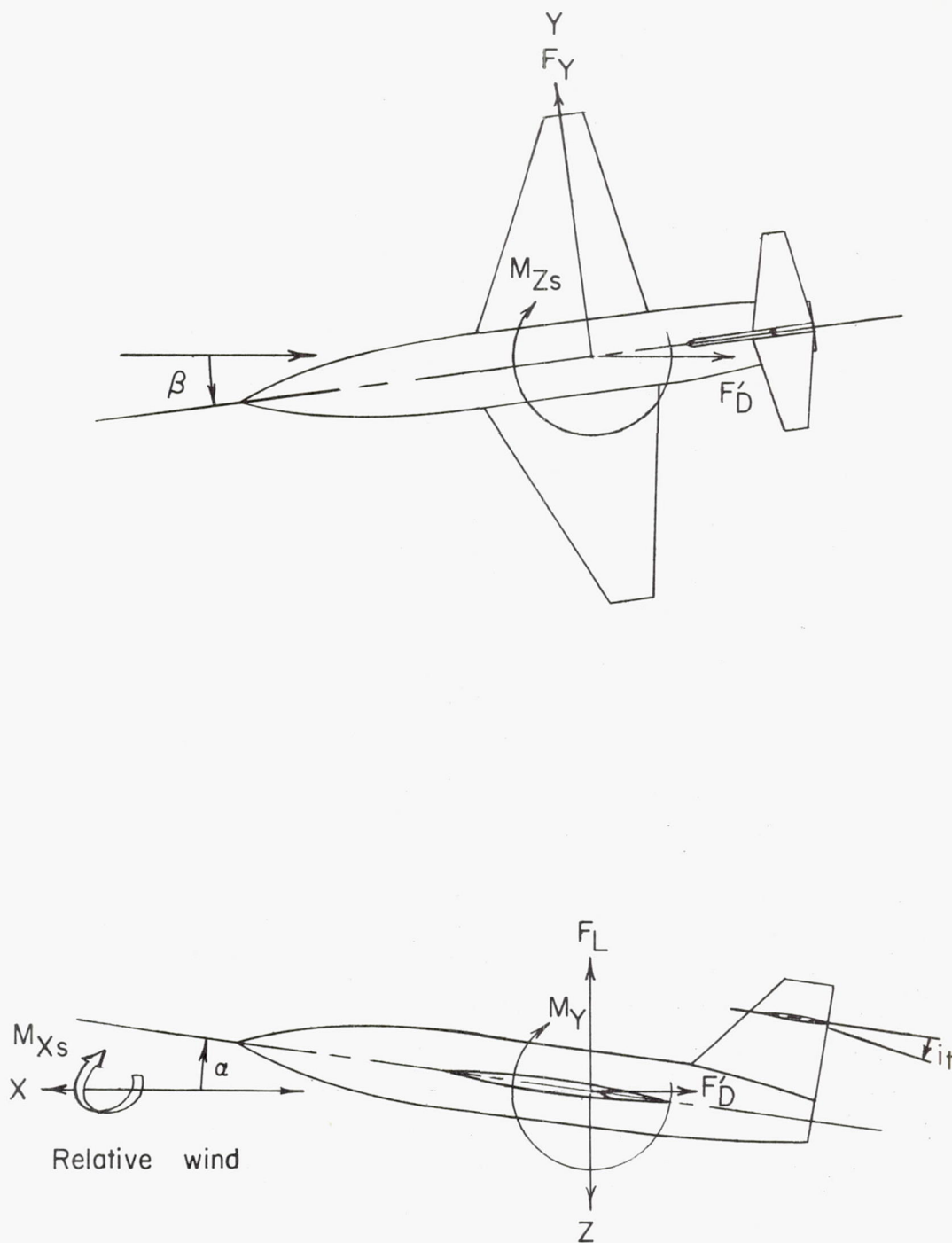
*Airfoil-section vertical tail; slab ventral fin.

†Horizontal tail at tip of vertical tail; slab vertical tail and ventral fin.



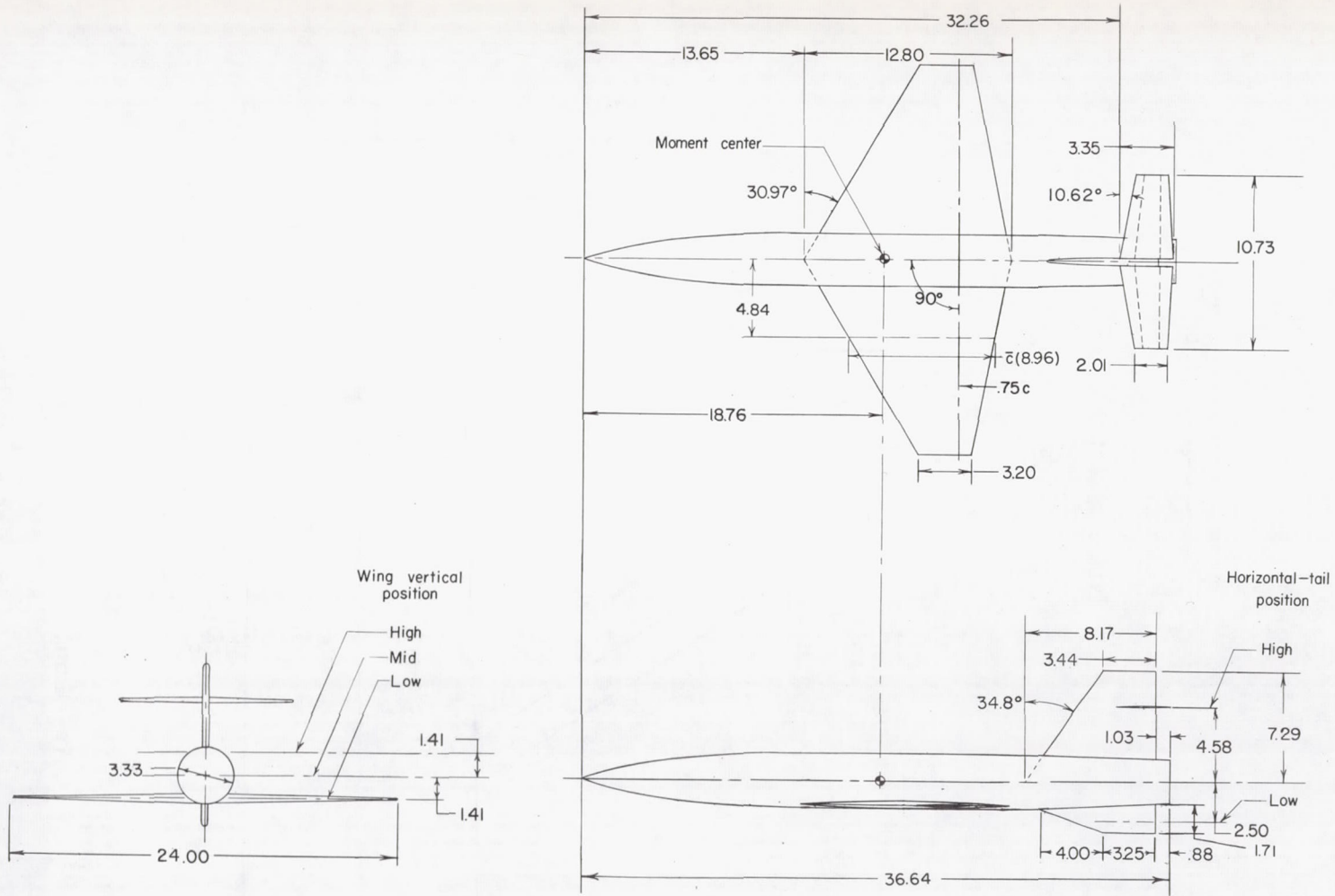
(a) Body axes.

Figure 1.- Axis systems. Arrows indicate positive values.



(b) Stability axes.

Figure 1.- Concluded.



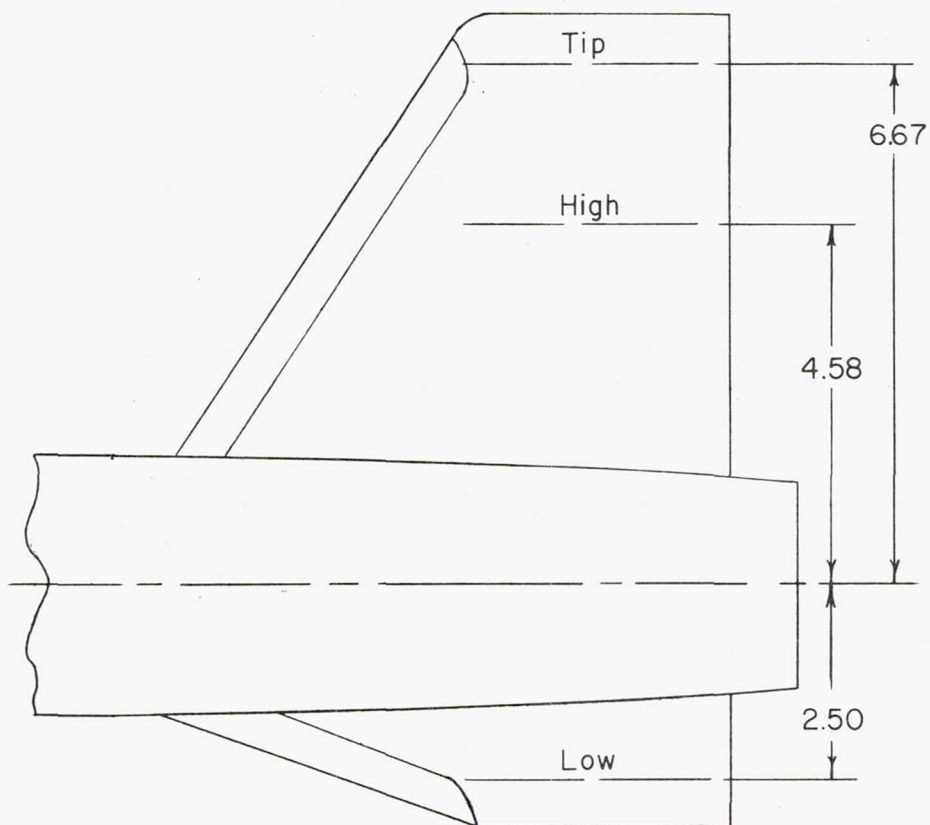
(a) Details of complete model.

Figure 2.- Geometry of complete model. All linear dimensions are in inches.

— Slab
- - - Airfoil, 65 A 004

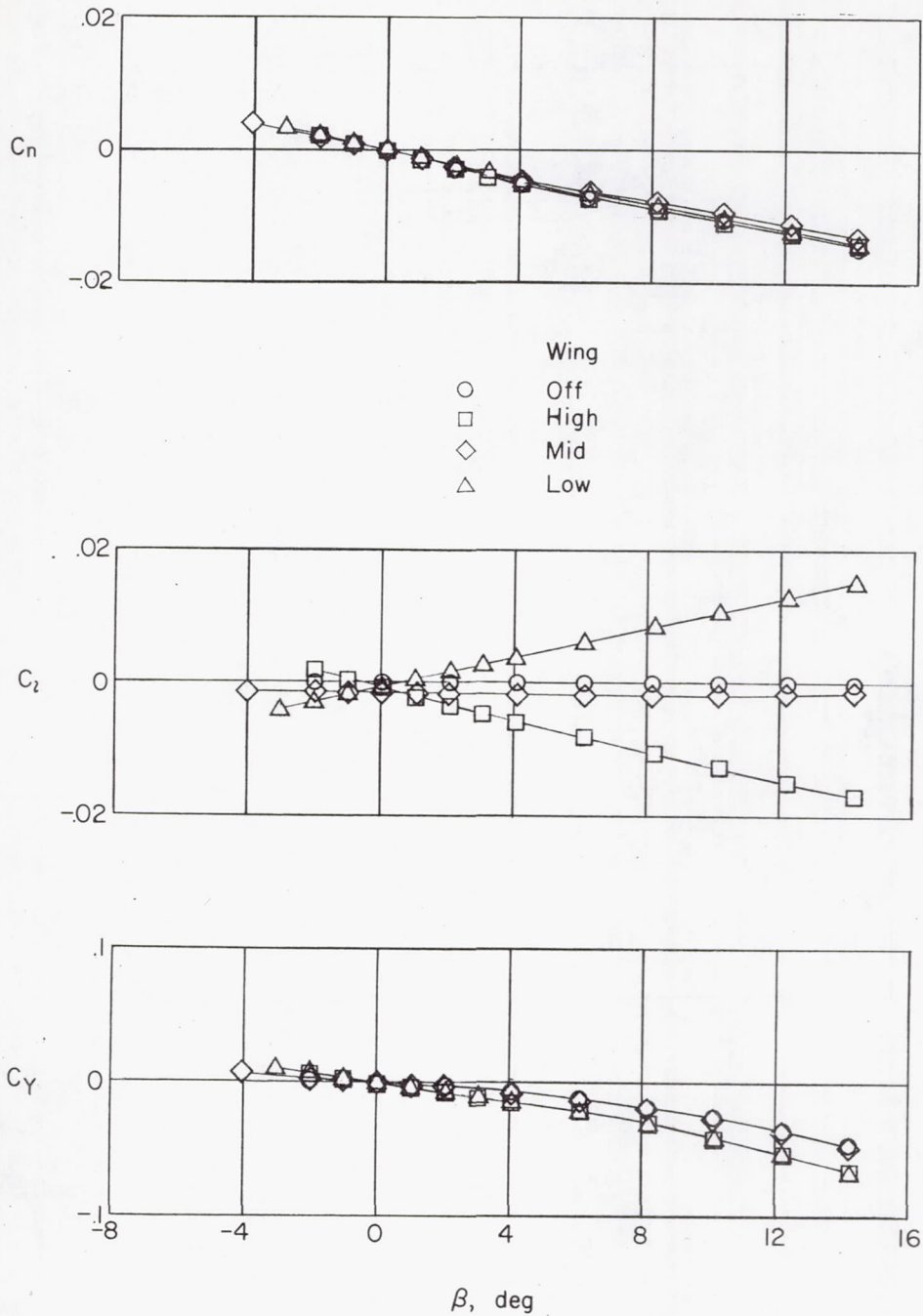


Typical section



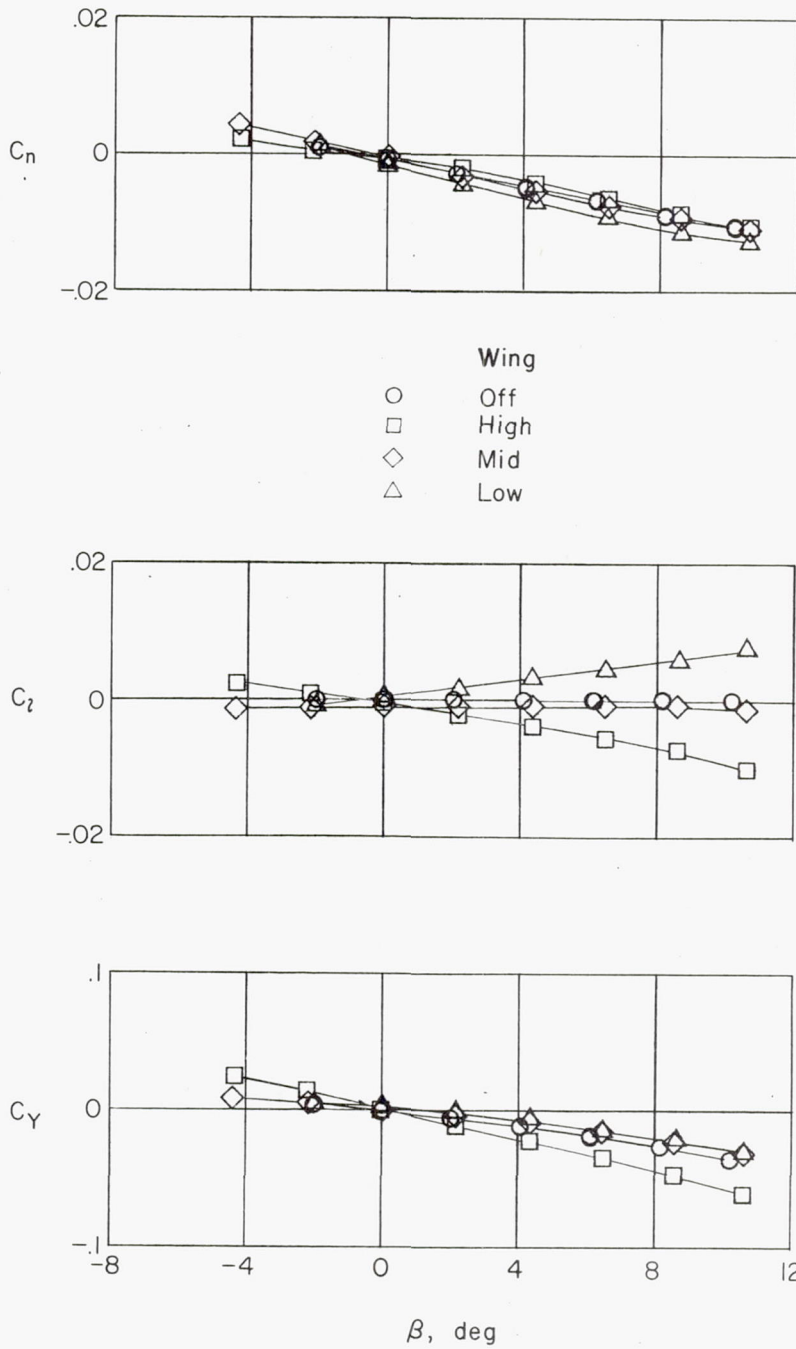
(b) Horizontal-tail positions (slab only).

Figure 2.- Concluded.



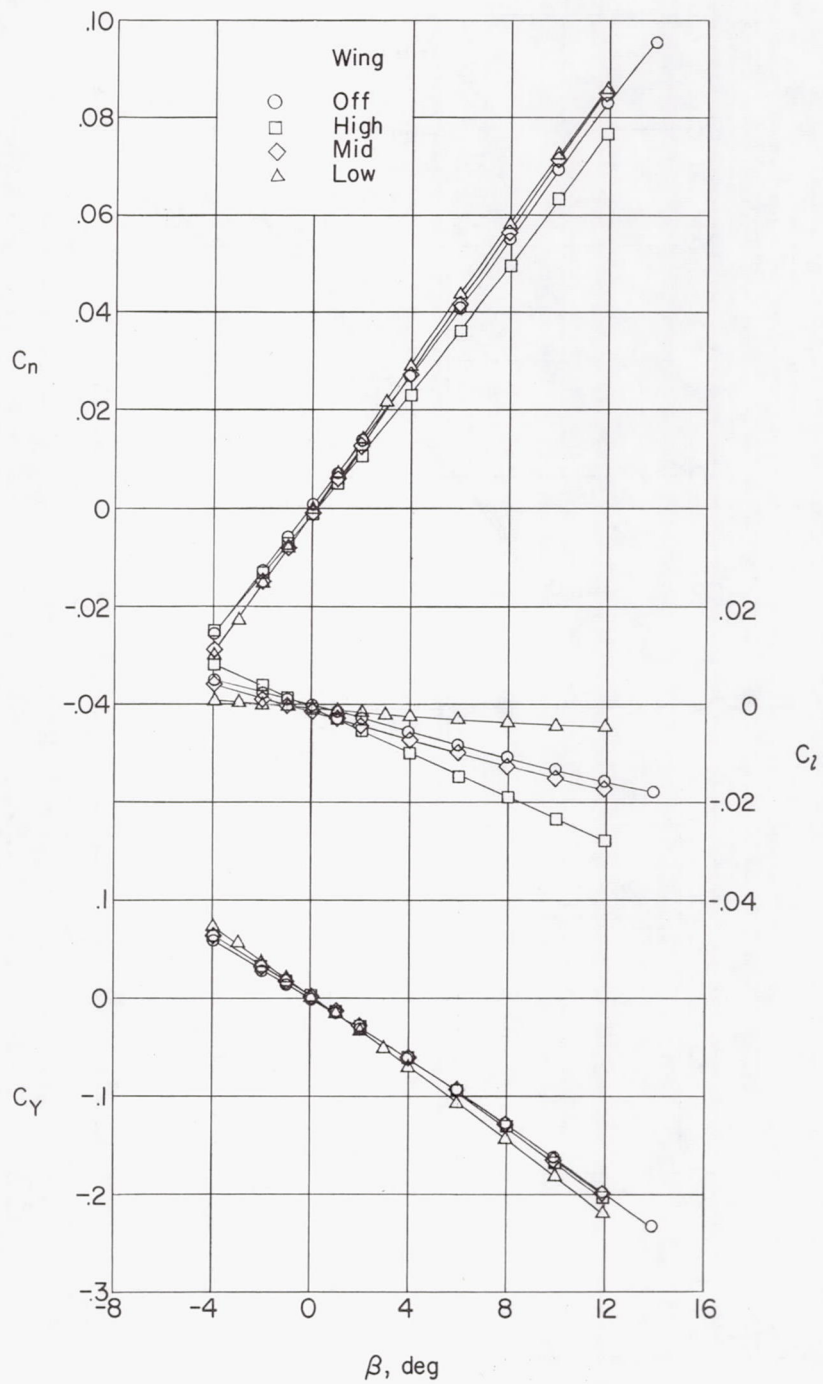
(a) B and BW; $\alpha \approx 0^\circ$.

Figure 3.- Typical variations of C_n , C_l , and C_y with β for various combinations of model components. $M = 1.41$.



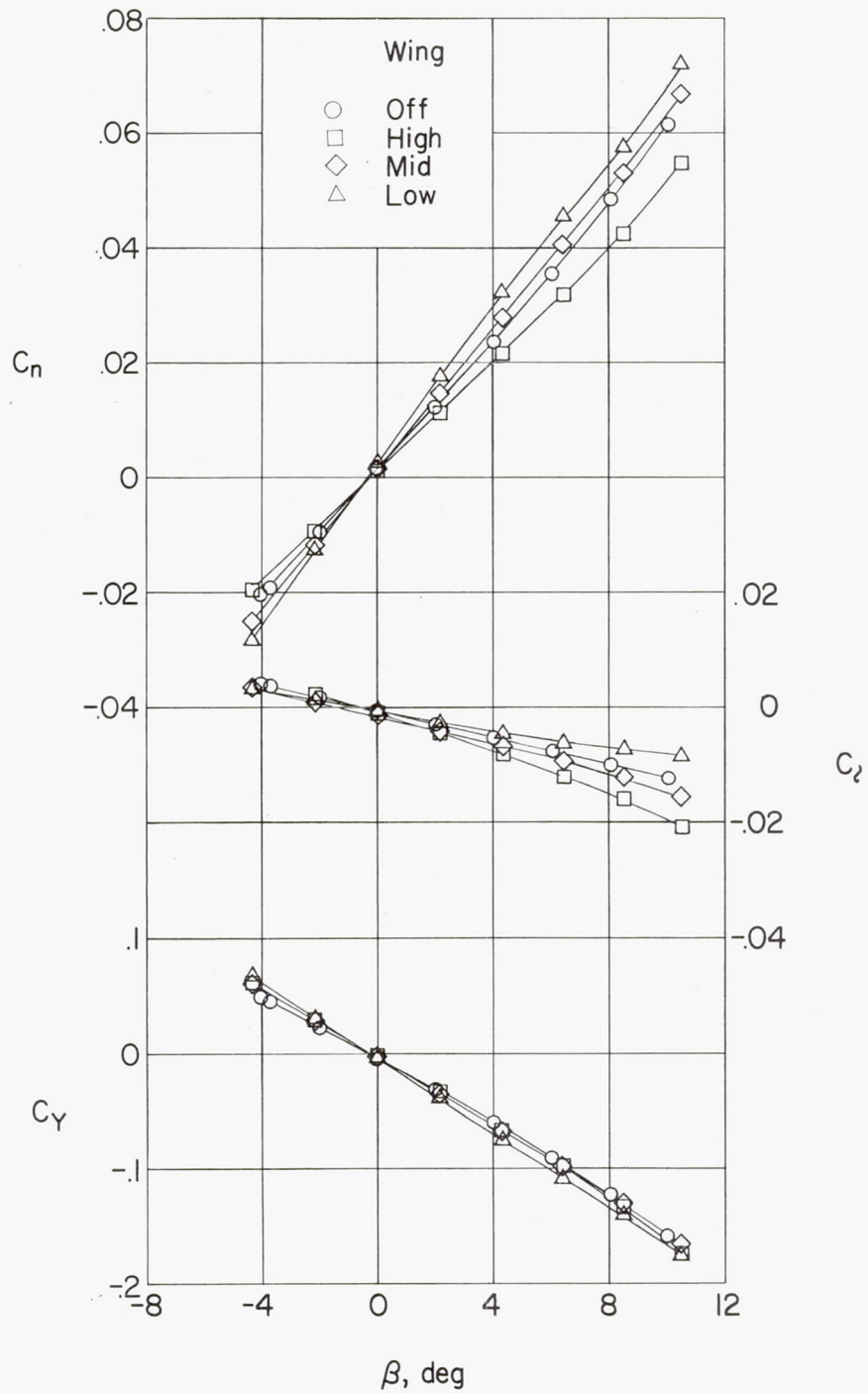
(b) B and BW; $\alpha \approx 12.9^\circ$.

Figure 3.- Continued.



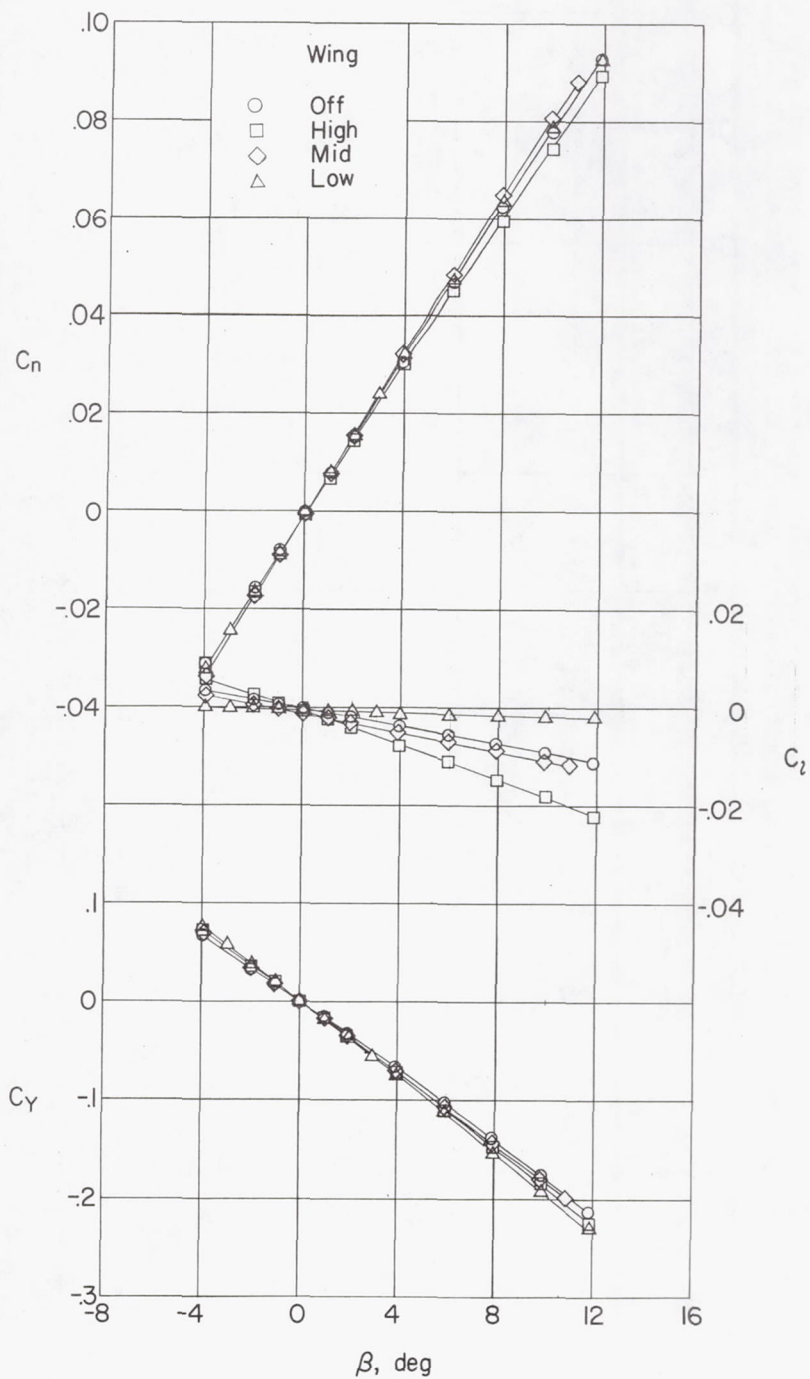
(c) BV and BWV; $\alpha \approx 0^\circ$.

Figure 3.- Continued.



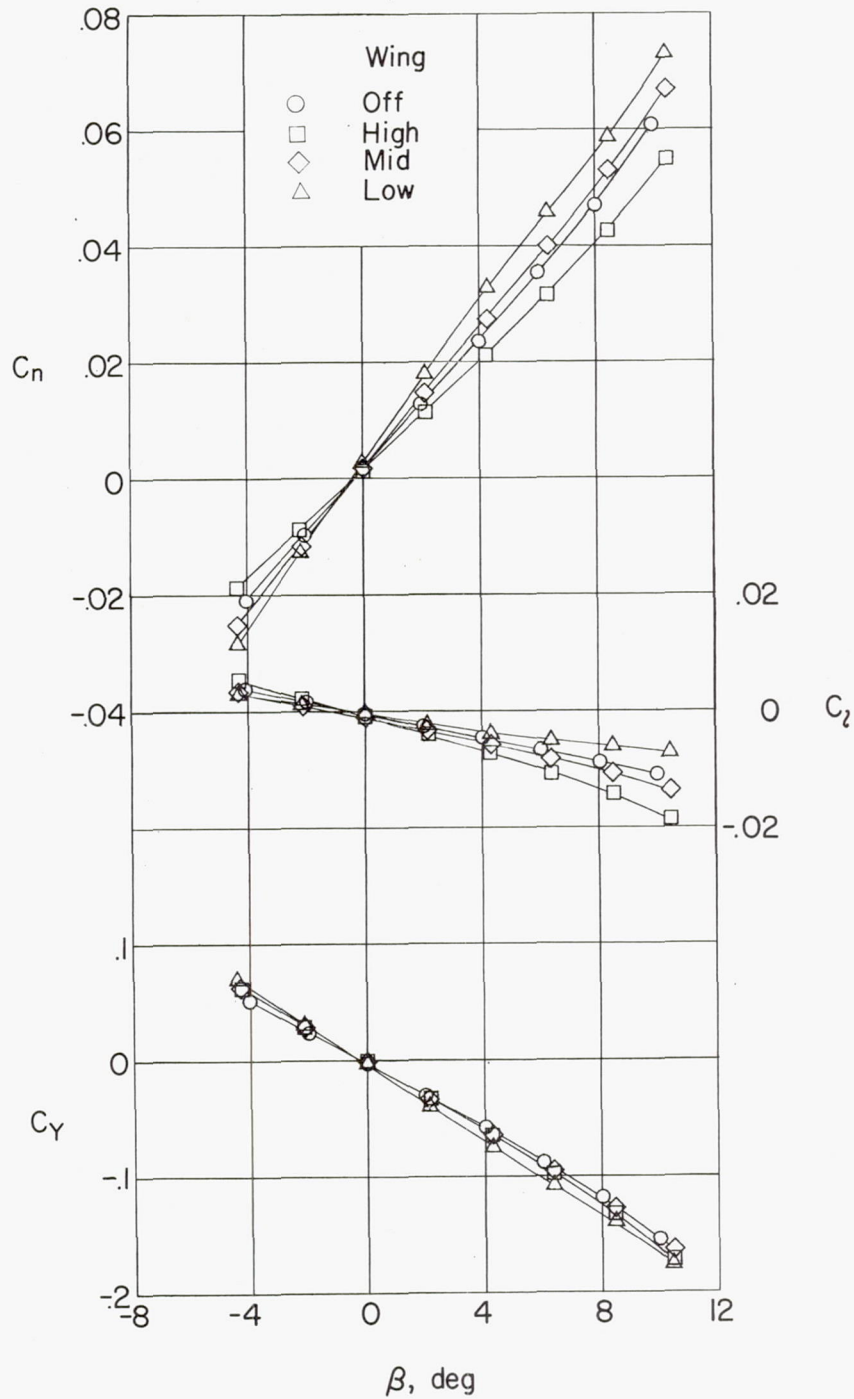
(d) BV and BWV; $\alpha \approx 12.9^\circ$.

Figure 3.- Continued.



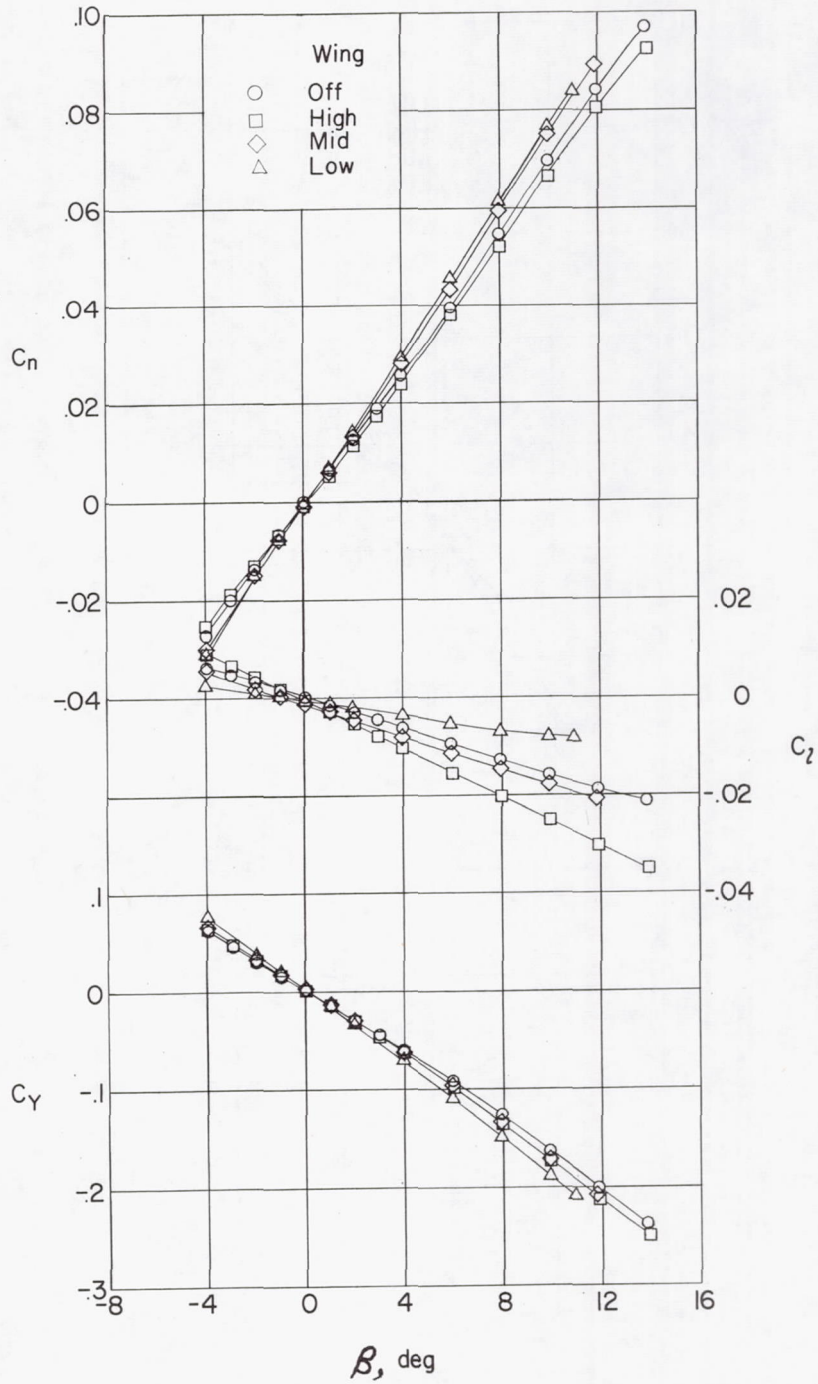
(e) BVH_L and $BWVH_L$; $i_t = 0^\circ$; $\alpha \approx 0^\circ$.

Figure 3.- Continued.



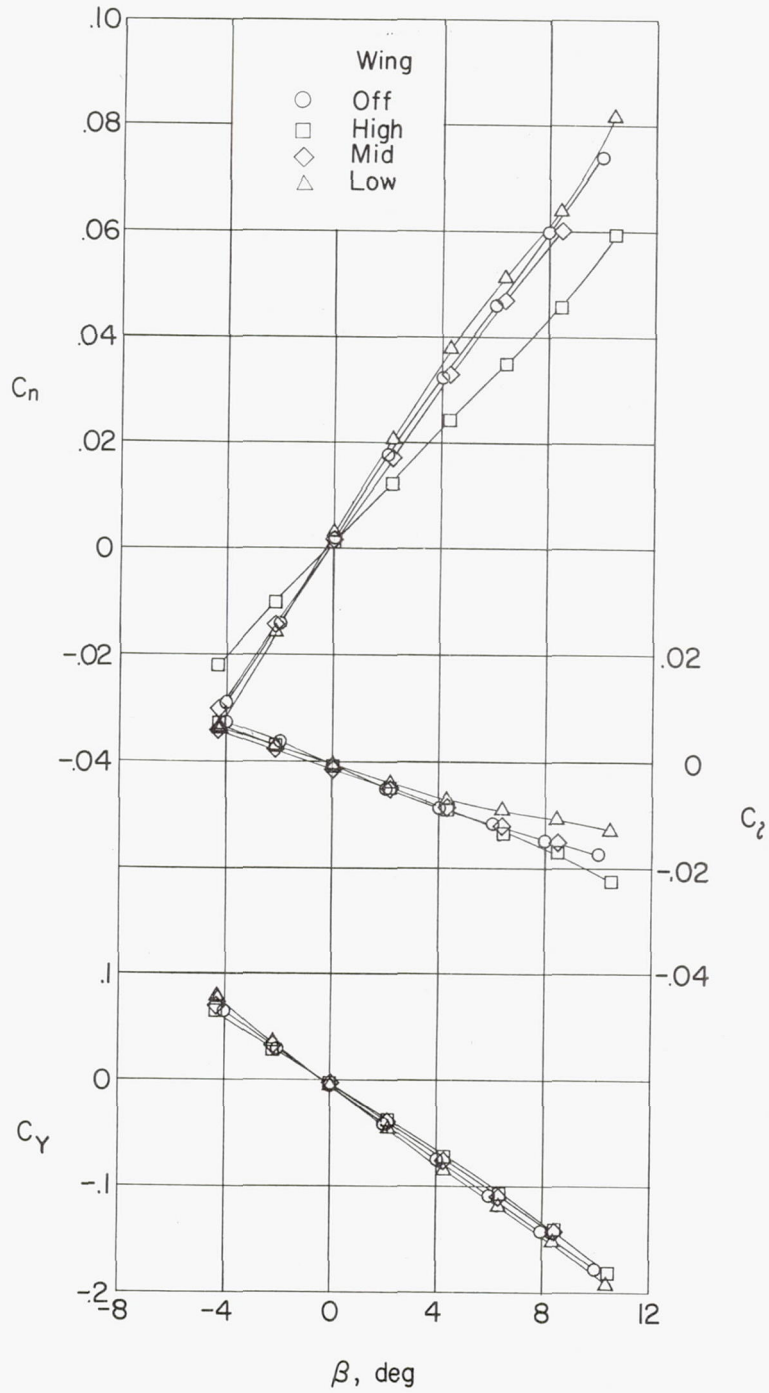
(f) BVH_L and $BWVH_L$; $i_t = 0^\circ$; $\alpha \approx 12.8^\circ$.

Figure 3.- Continued.



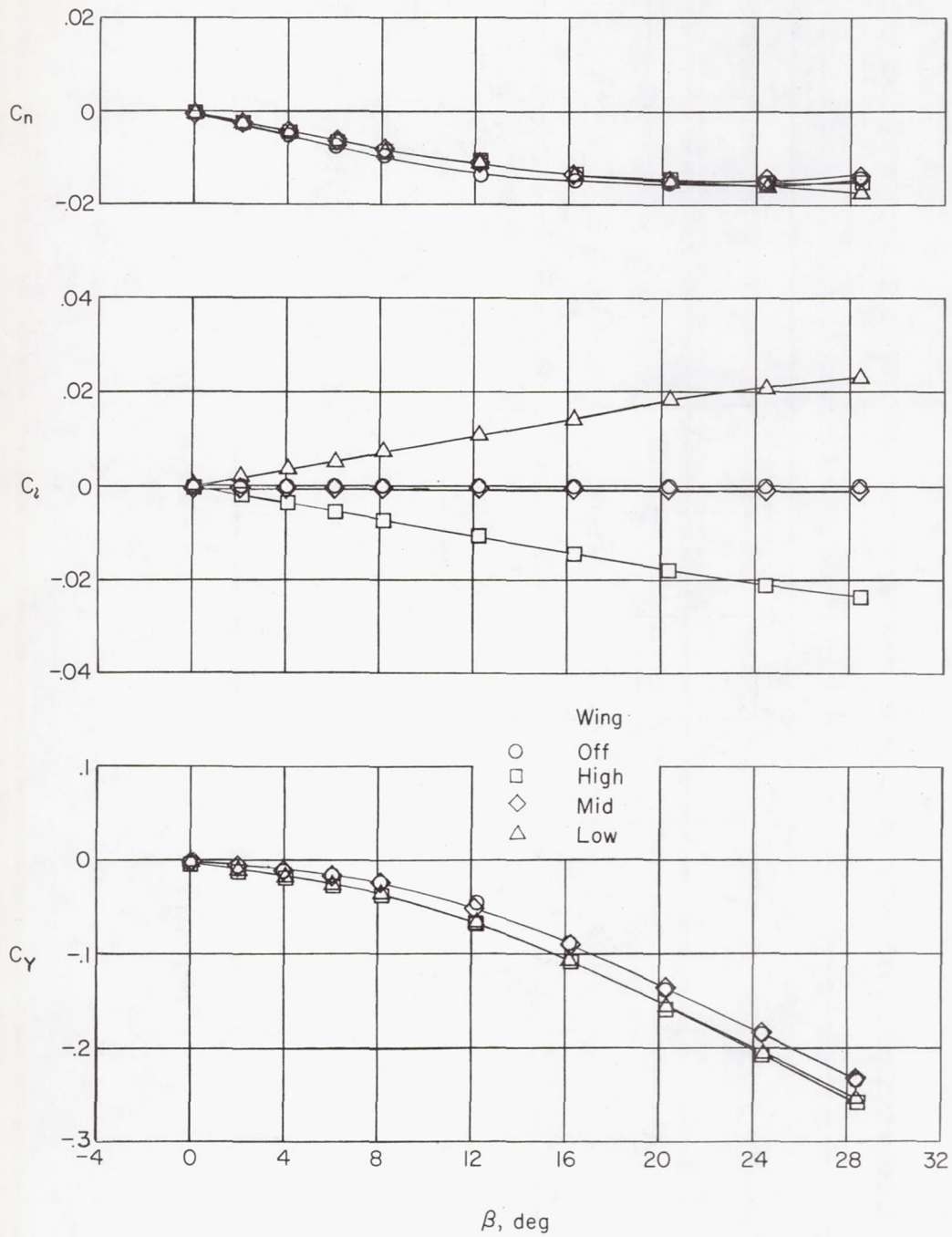
(g) BV_{H_H} and BWV_{H_H} ; $i_t = 0^\circ$; $\alpha \approx 0^\circ$.

Figure 3.- Continued.



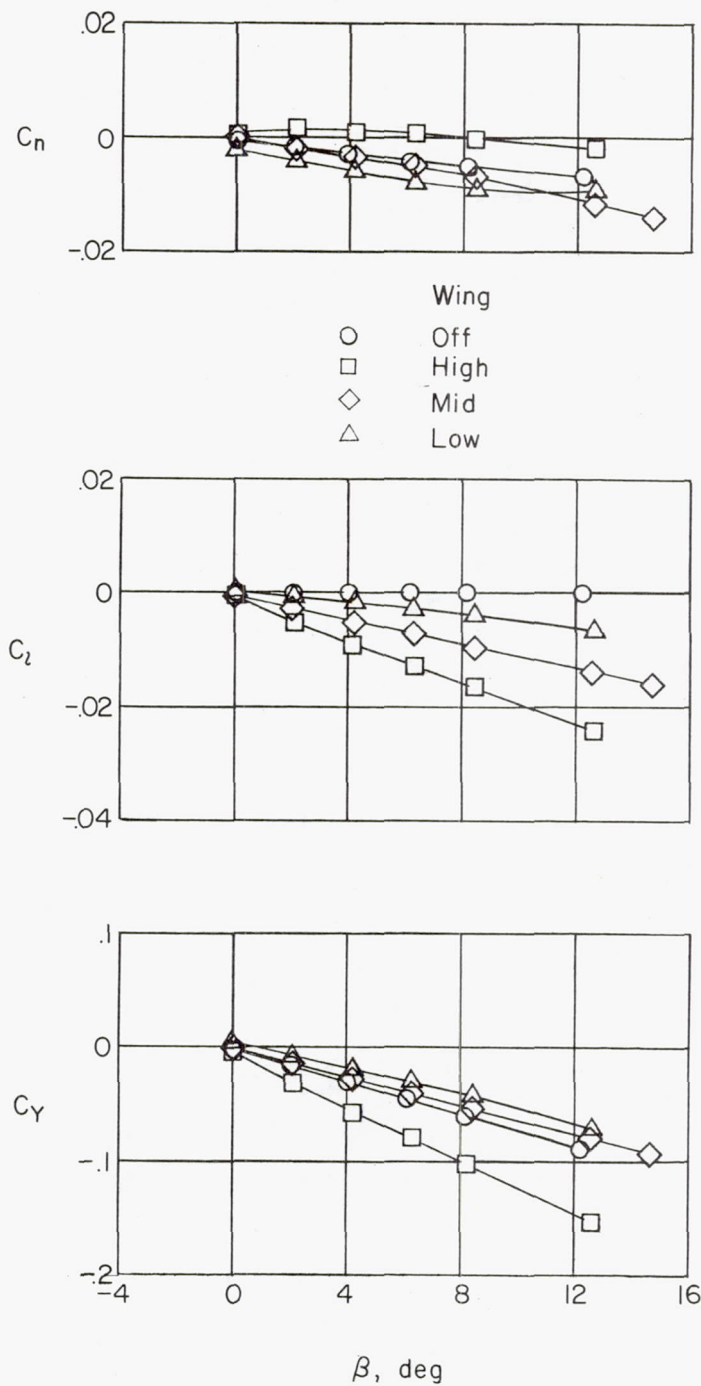
(h) BVH_H and $BWVH_H$; $i_t = 0^\circ$; $\alpha \approx 12^\circ$.

Figure 3.- Concluded.



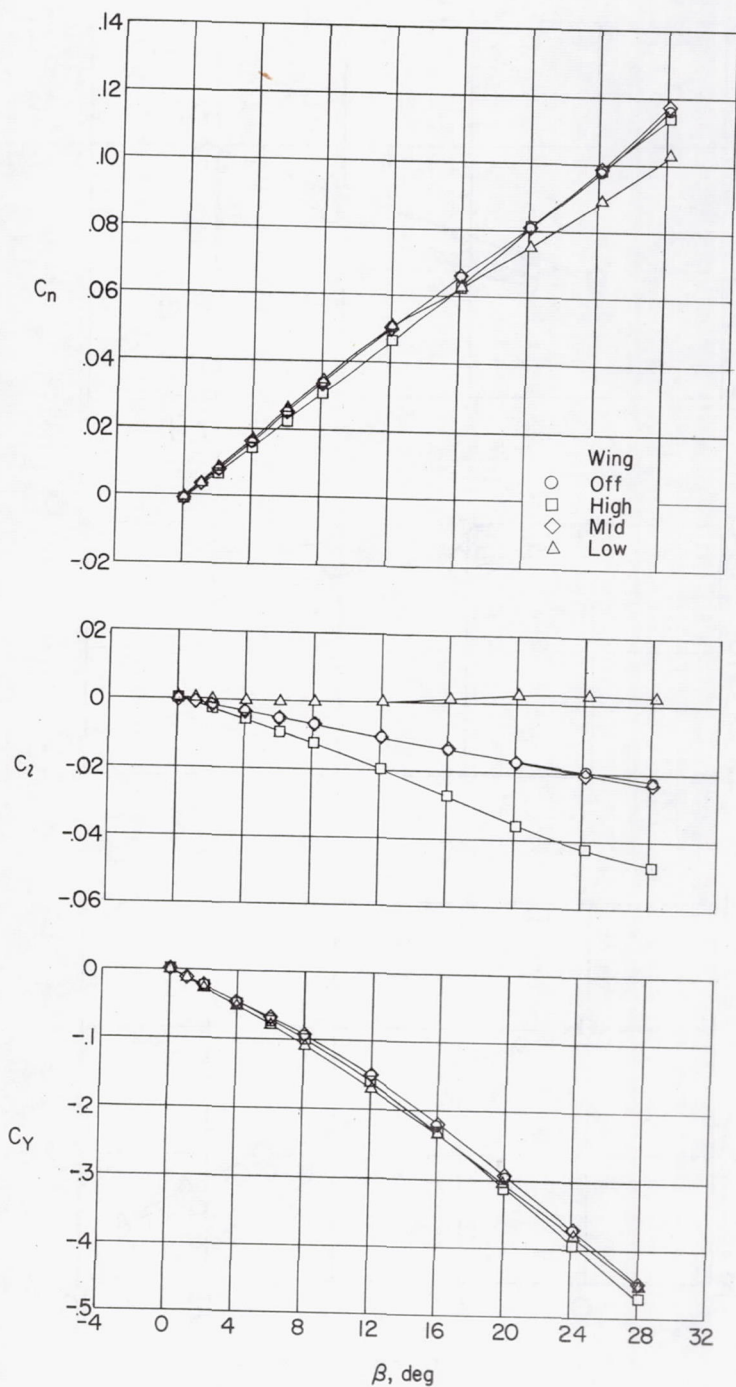
(a) B and BW; $\alpha \approx 0^\circ$.

Figure 4.- Typical variations of C_n , C_l , and C_y with β for various combinations of model components. $M = 2.01$.



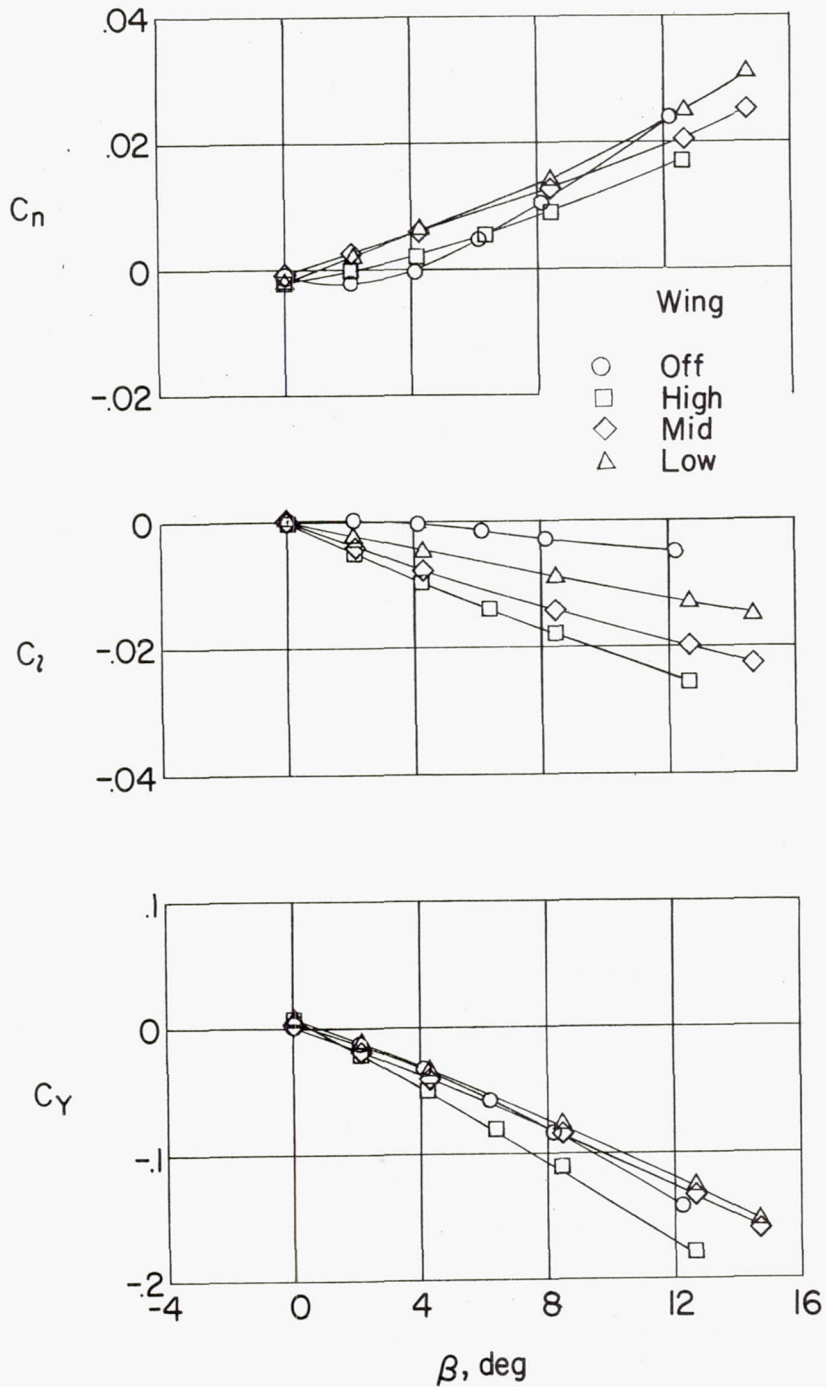
(b) B and BW; $\alpha \approx 25.2^\circ$.

Figure 4.- Continued.



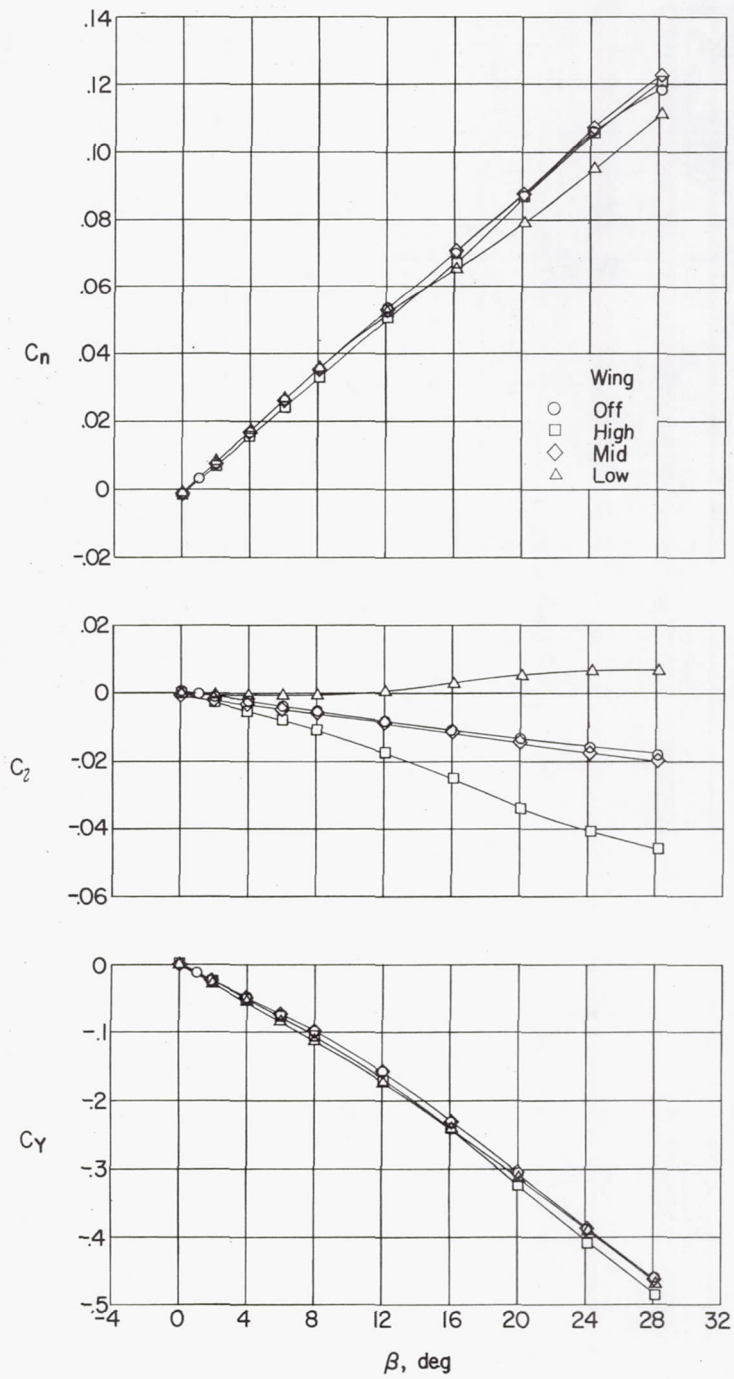
(c) BV and BWV; $\alpha \approx 0^\circ$.

Figure 4.- Continued.



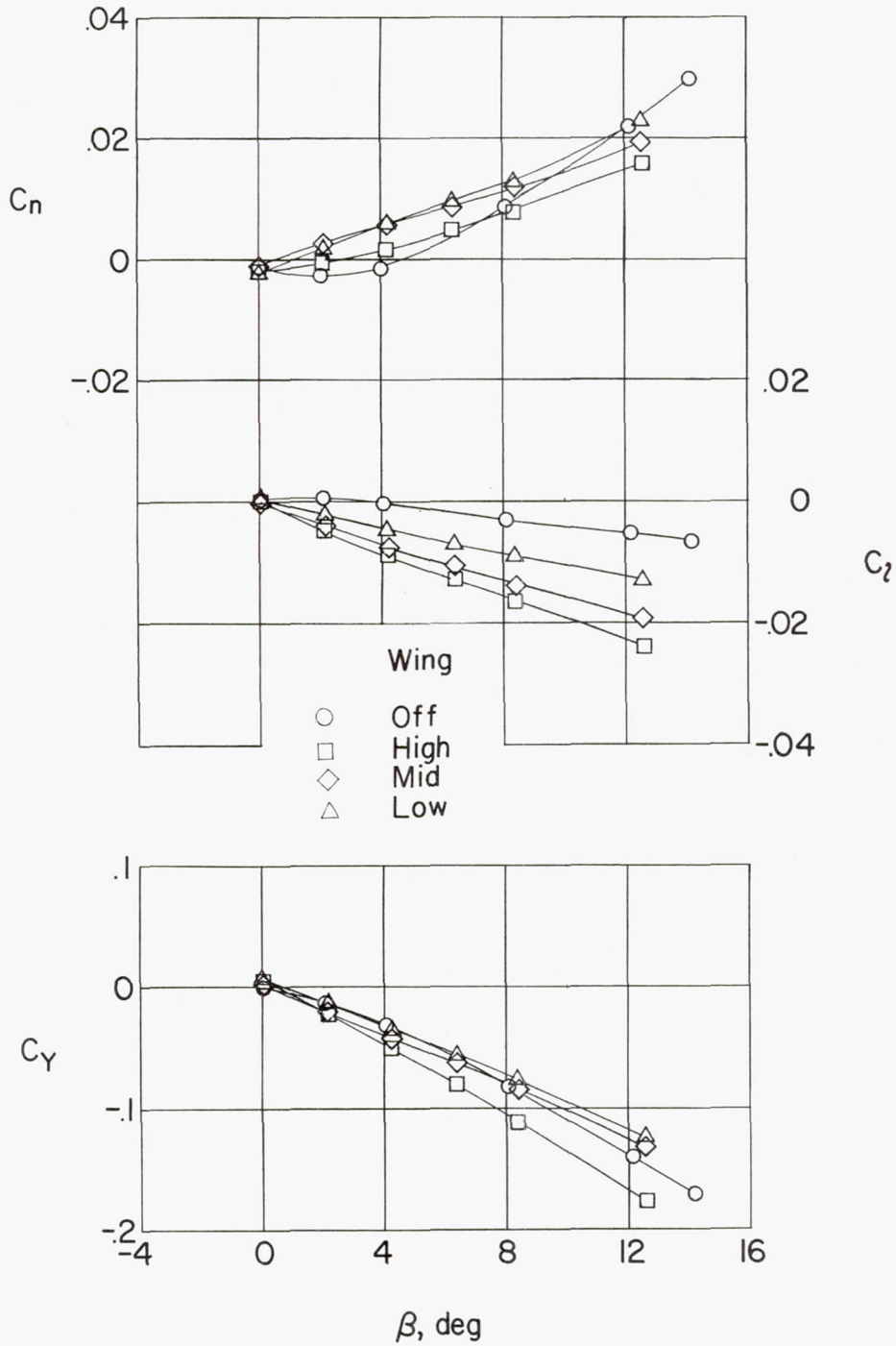
(d) BV and BWV; $\alpha \approx 25.2^\circ$.

Figure 4.- Continued.



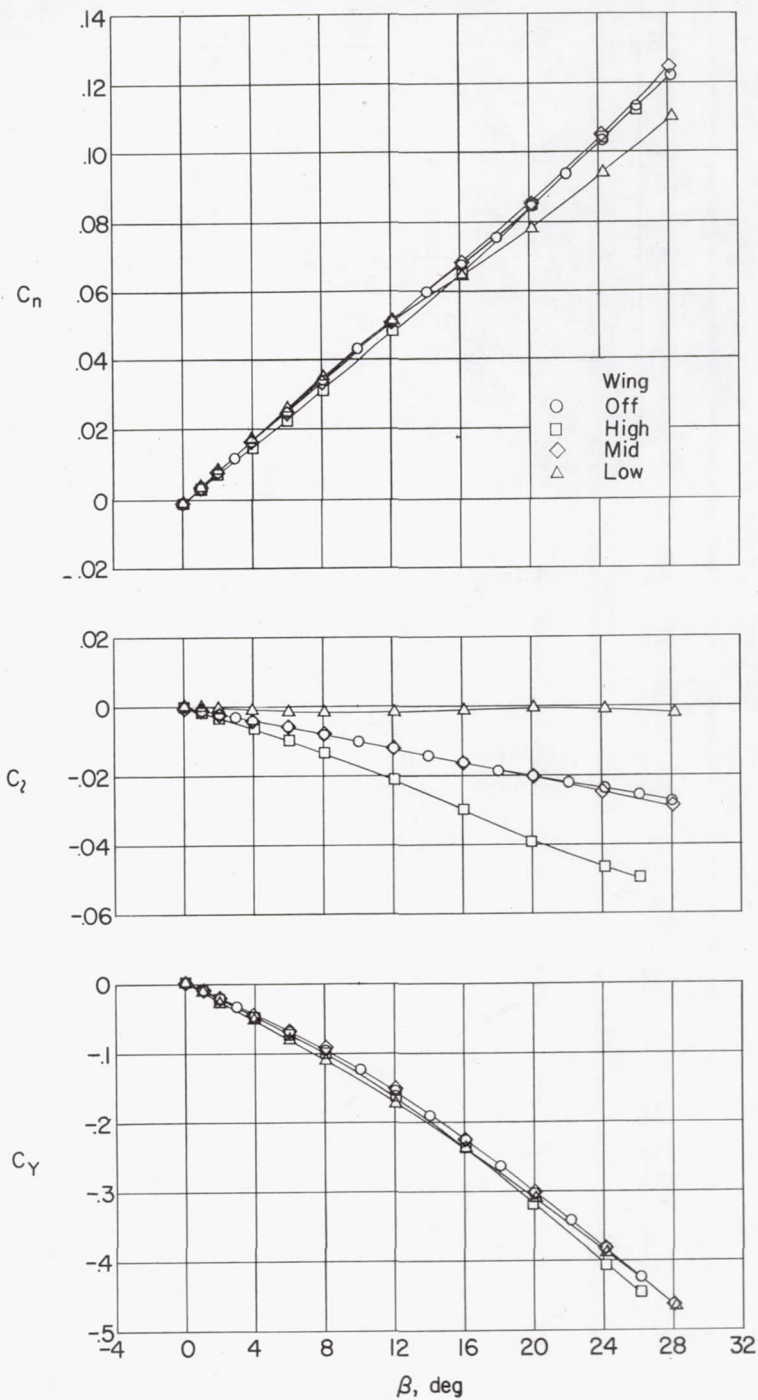
(e) BVH_L and $BWVH_L$; $i_t = 0^\circ$; $\alpha \approx 0^\circ$.

Figure 4.- Continued.



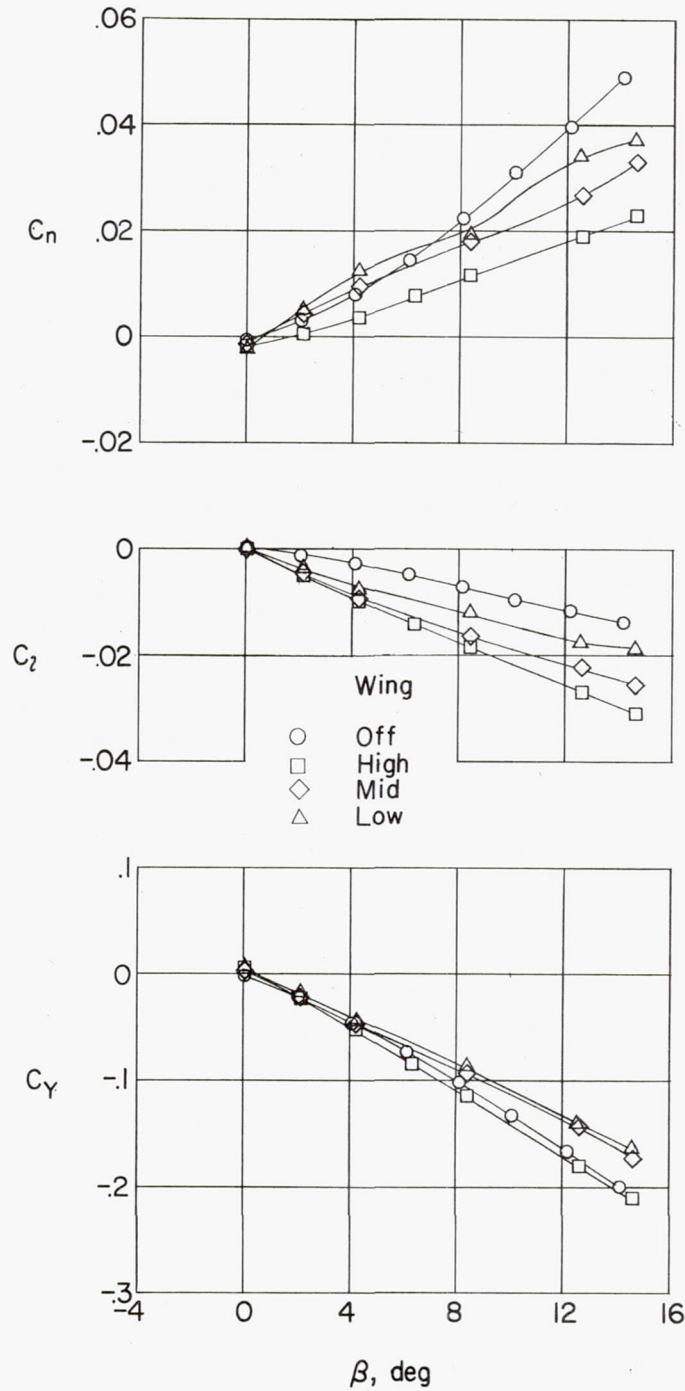
(f) BVH_L and $BWVH_L$; $i_t = 0^\circ$; $\alpha \approx 25.0^\circ$.

Figure 4.- Continued.



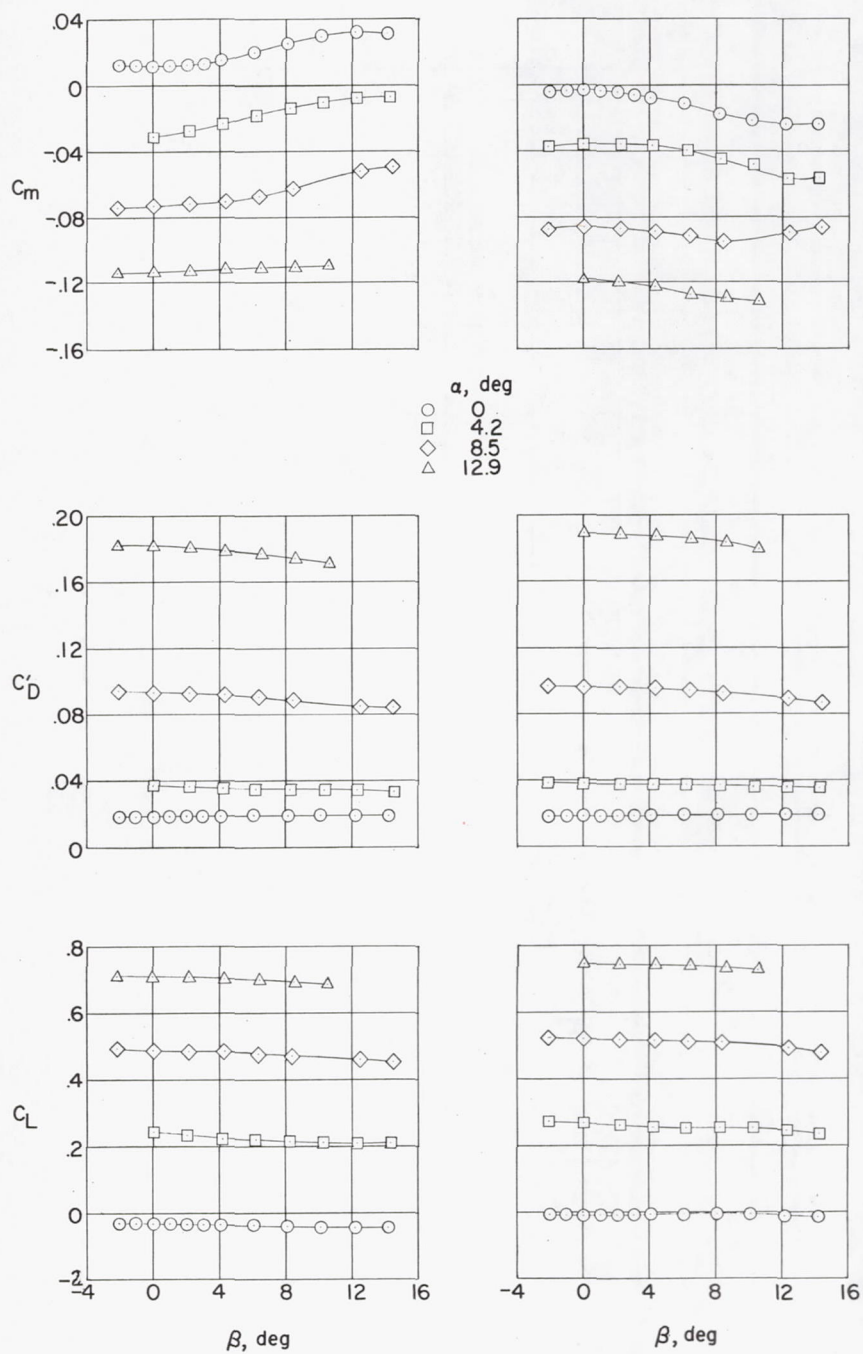
(g) BVH_H and $BWVH_H$; $i_t = 0^\circ$; $\alpha \approx 0^\circ$.

Figure 4.- Continued.



(h) BVH_H and $BWVH_H$; $i_t = 0^\circ$; $\alpha \approx 25.0^\circ$.

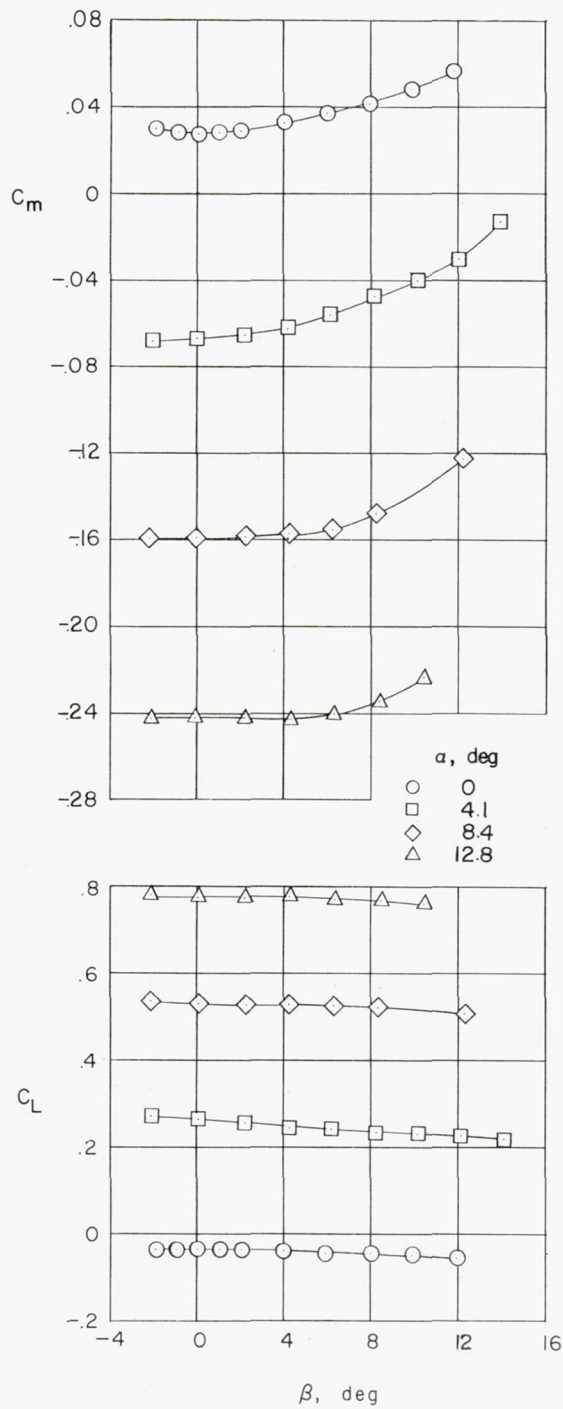
Figure 4.- Concluded.



(a) BW_H.

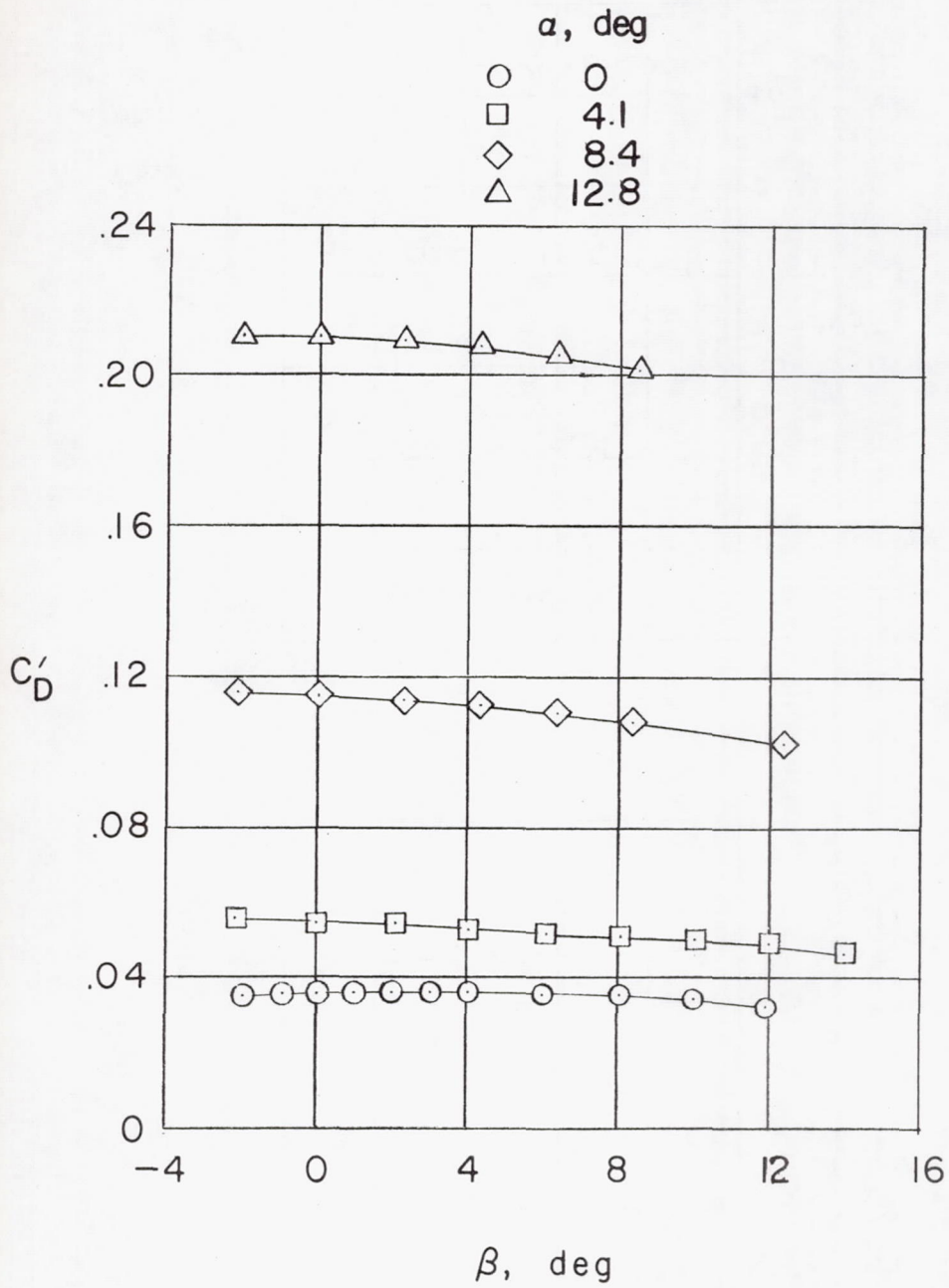
(b) BW_L.

Figure 5.- Typical variations of C_m , C_D , and C_L with β for various combinations of components at several angles of attack. $M = 1.41$.



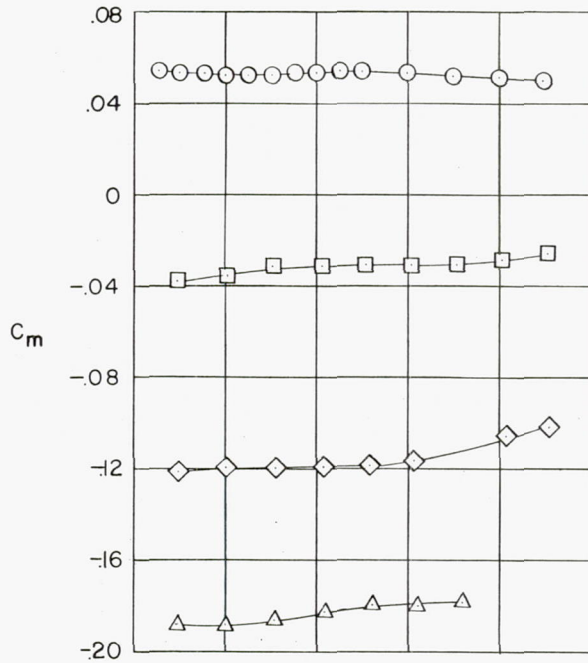
(c) $BW_{H^VH_L}; i_t = 0^\circ$.

Figure 5.- Continued.

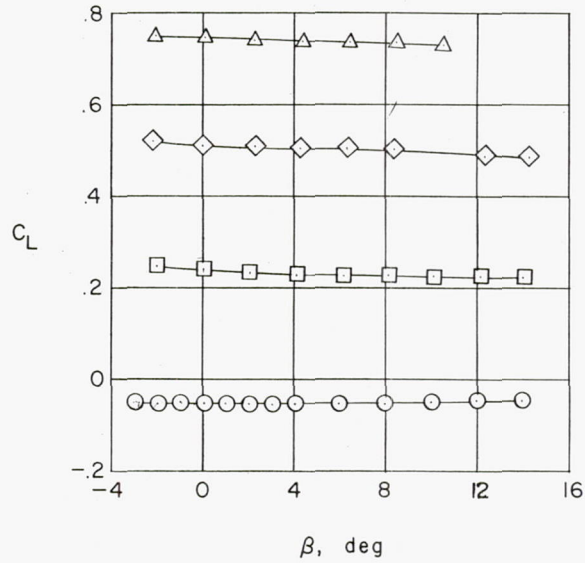


(c) Concluded.

Figure 5.- Continued.

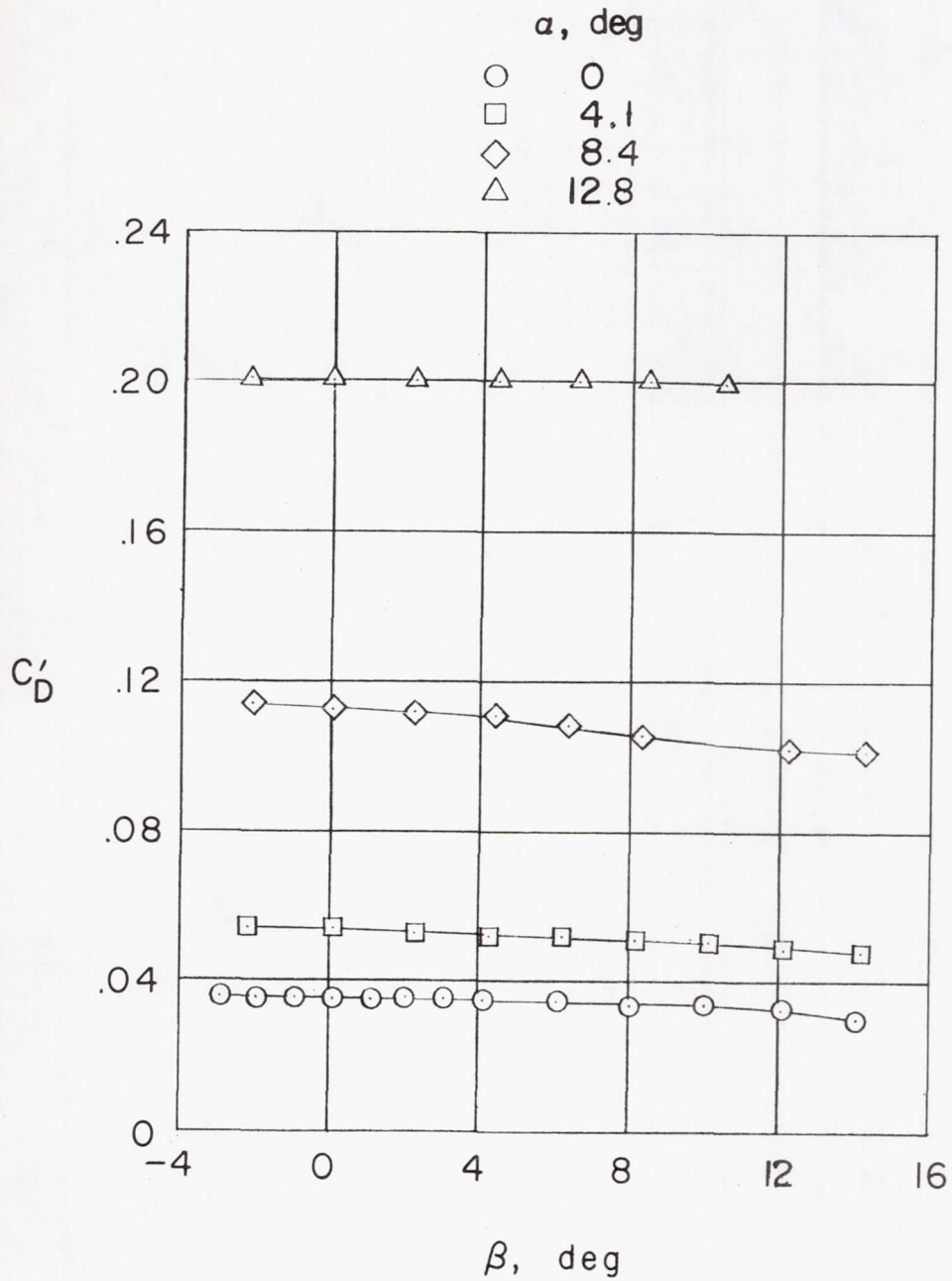


α , deg
 ○ 0
 □ 4.1
 ◇ 8.4
 △ 12.8



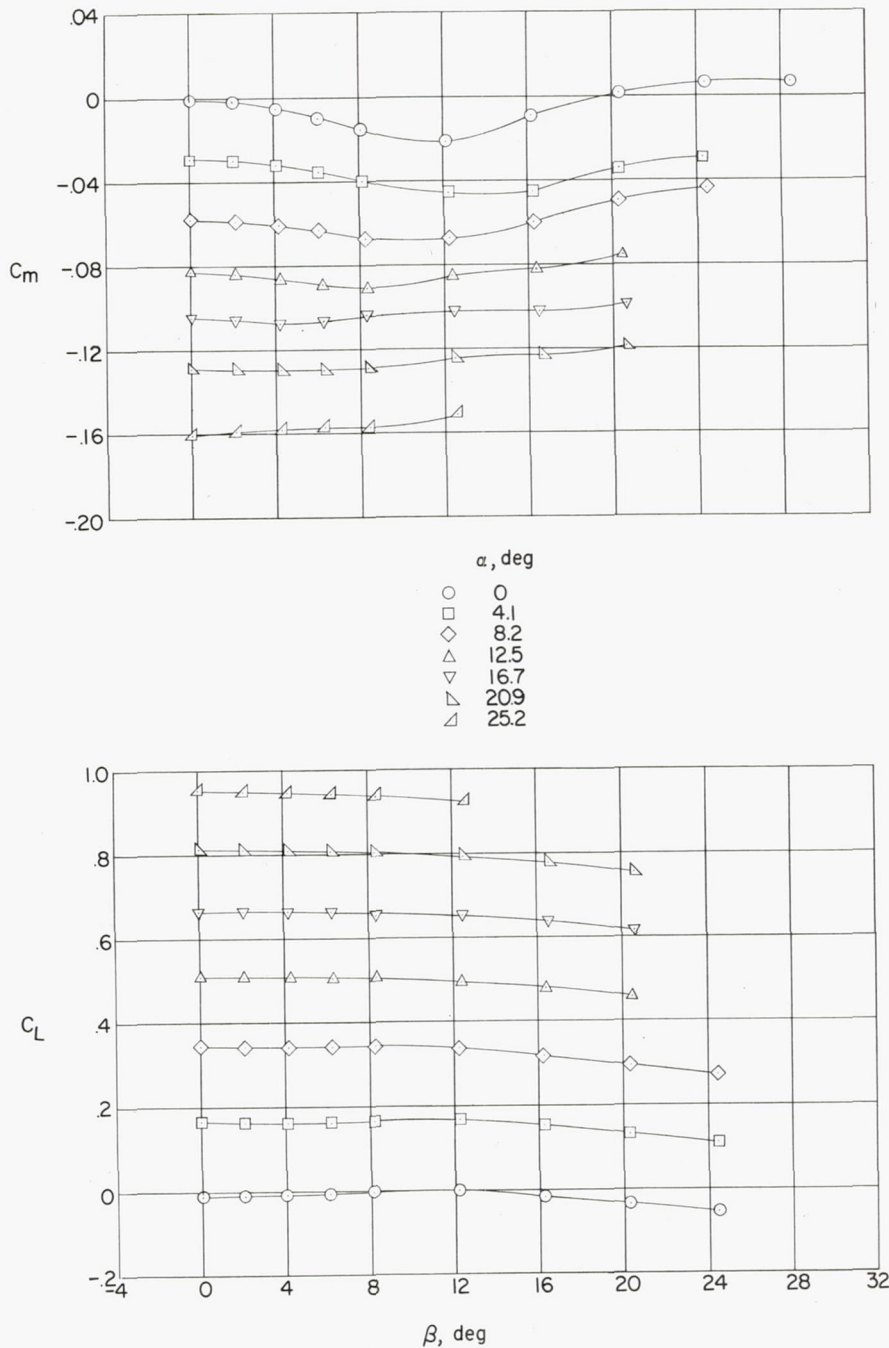
(d) $BW_H V H_H; i_t = 0^\circ$.

Figure 5.- Continued.



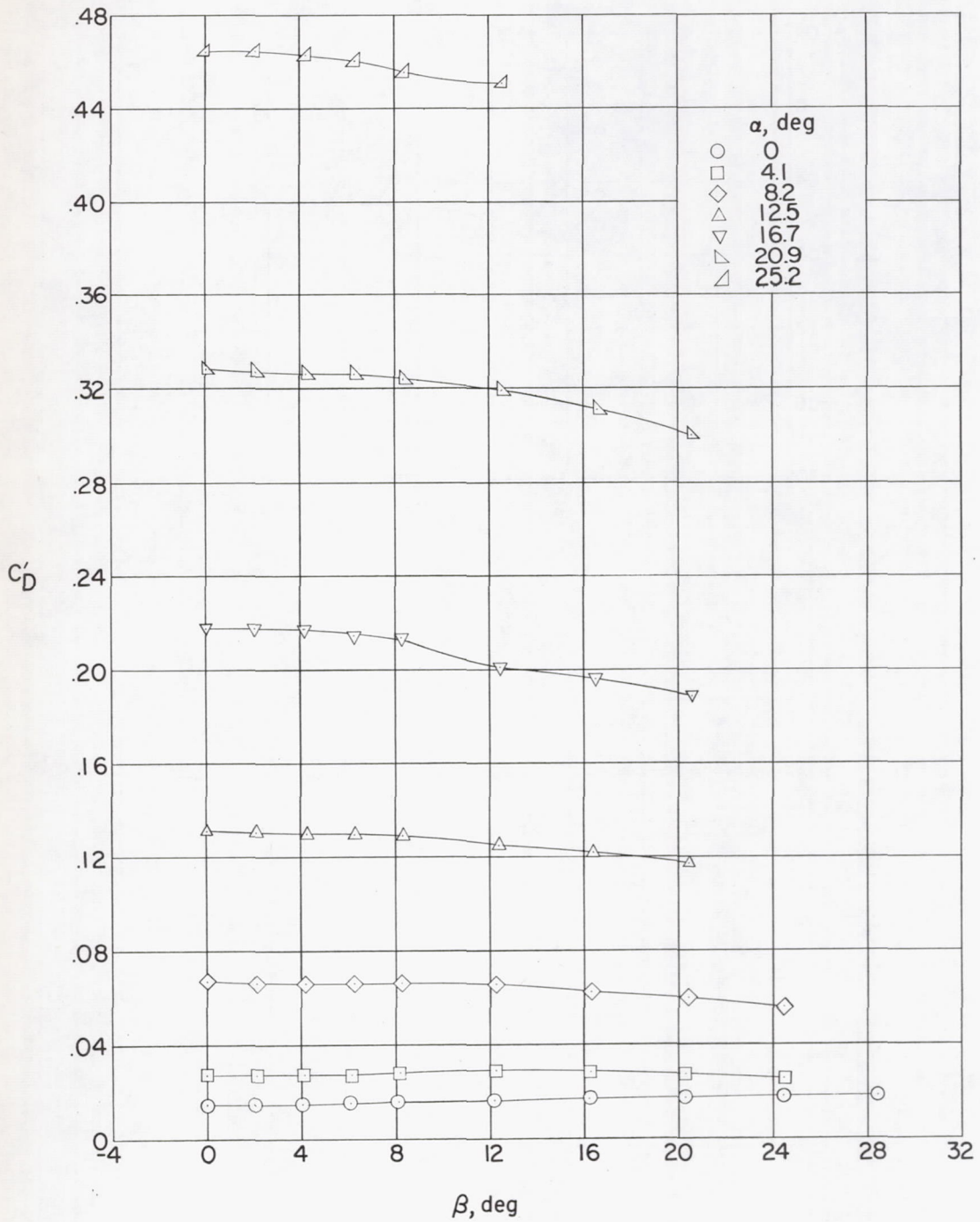
(a) Concluded.

Figure 5.- Concluded.



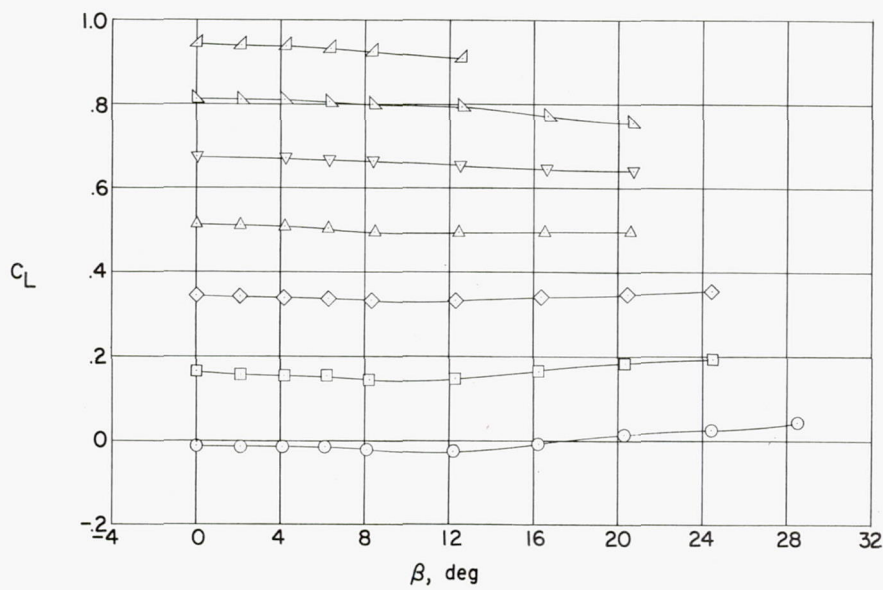
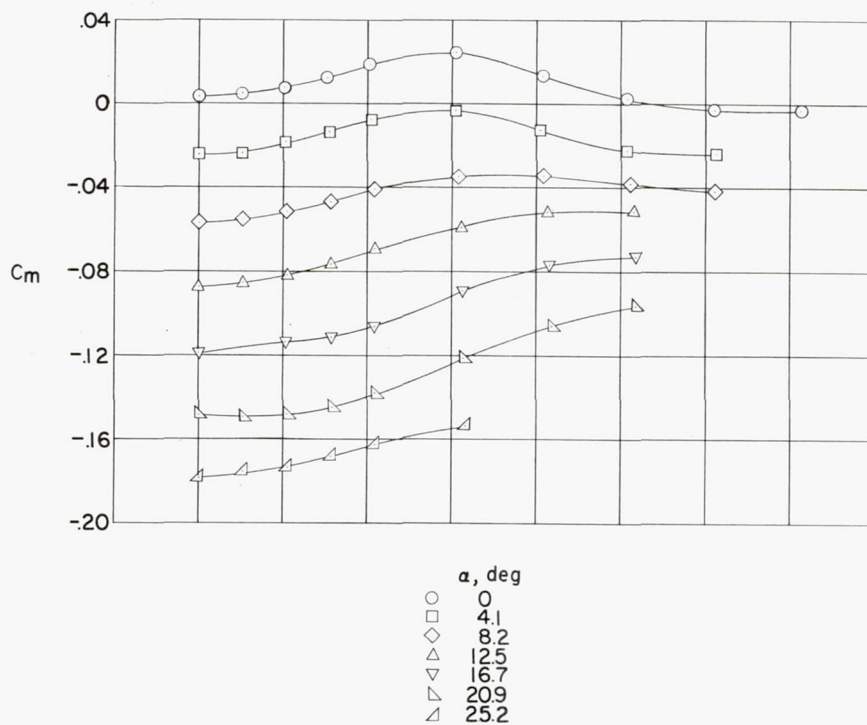
(a) BW_L .

Figure 6.- Typical variations of C_m , C_D' , and C_m with β for various combinations of components at several angles of attack. $M = 2.01$.



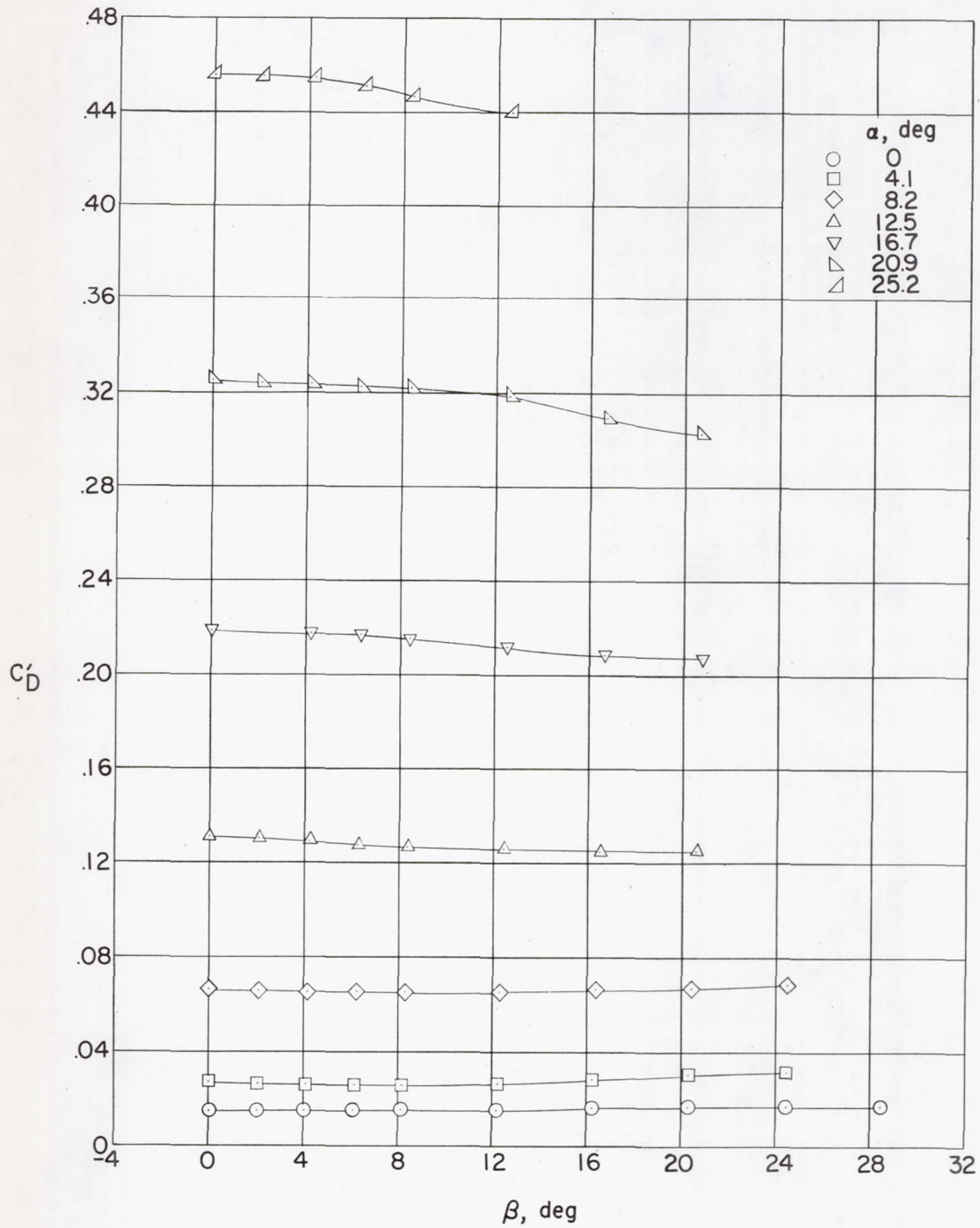
(a) Concluded.

Figure 6.- Continued.



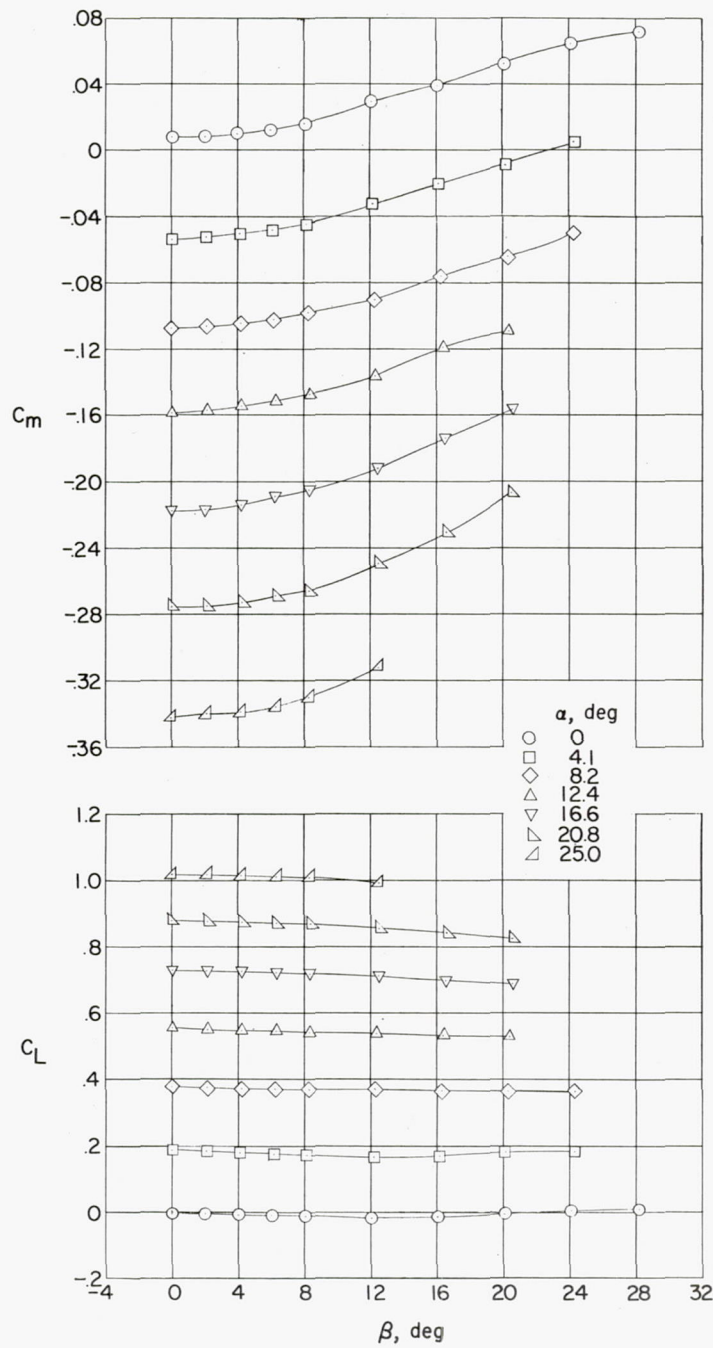
(b) BW_H .

Figure 6.- Continued.



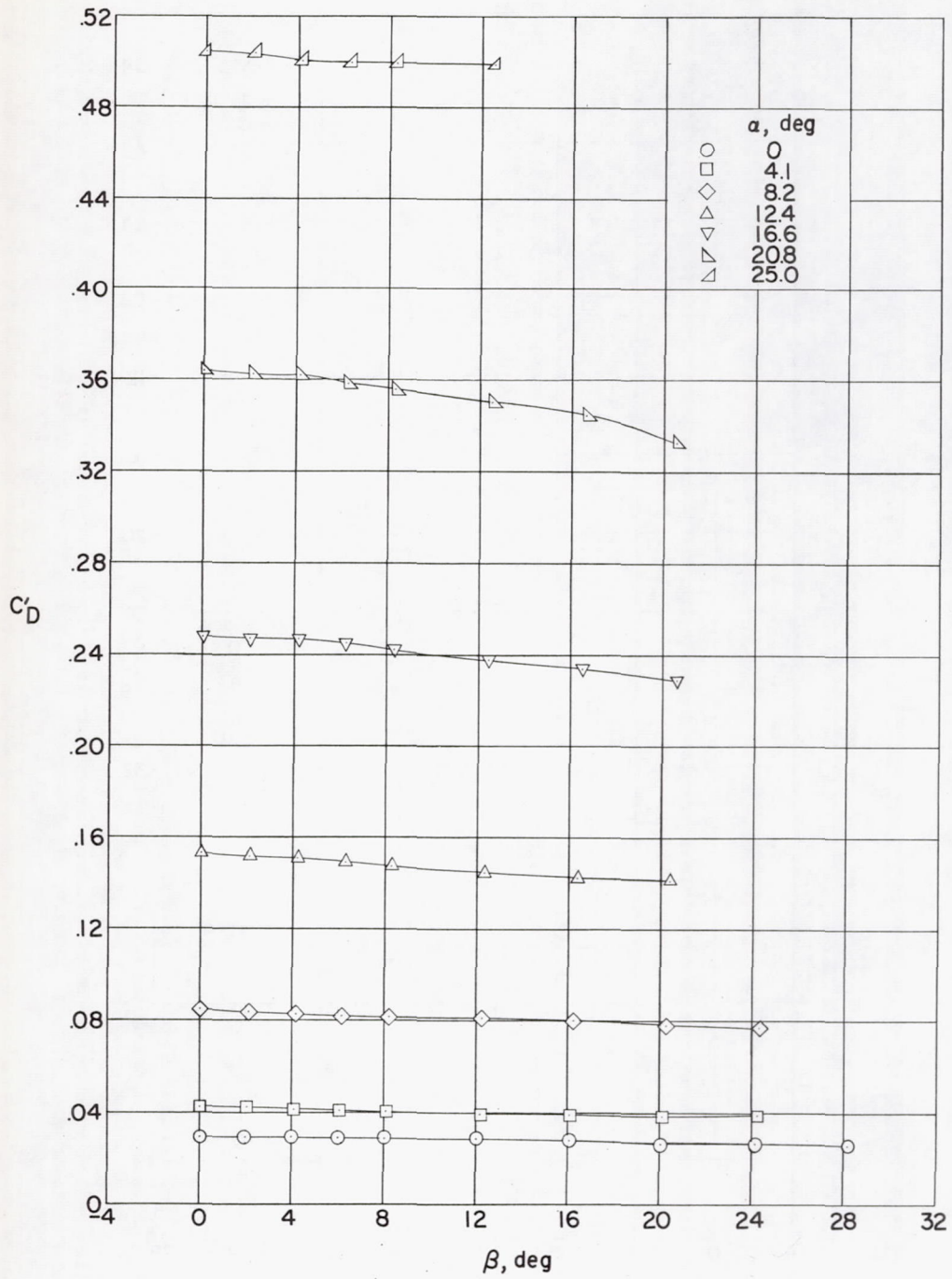
(b) Concluded.

Figure 6.- Continued.



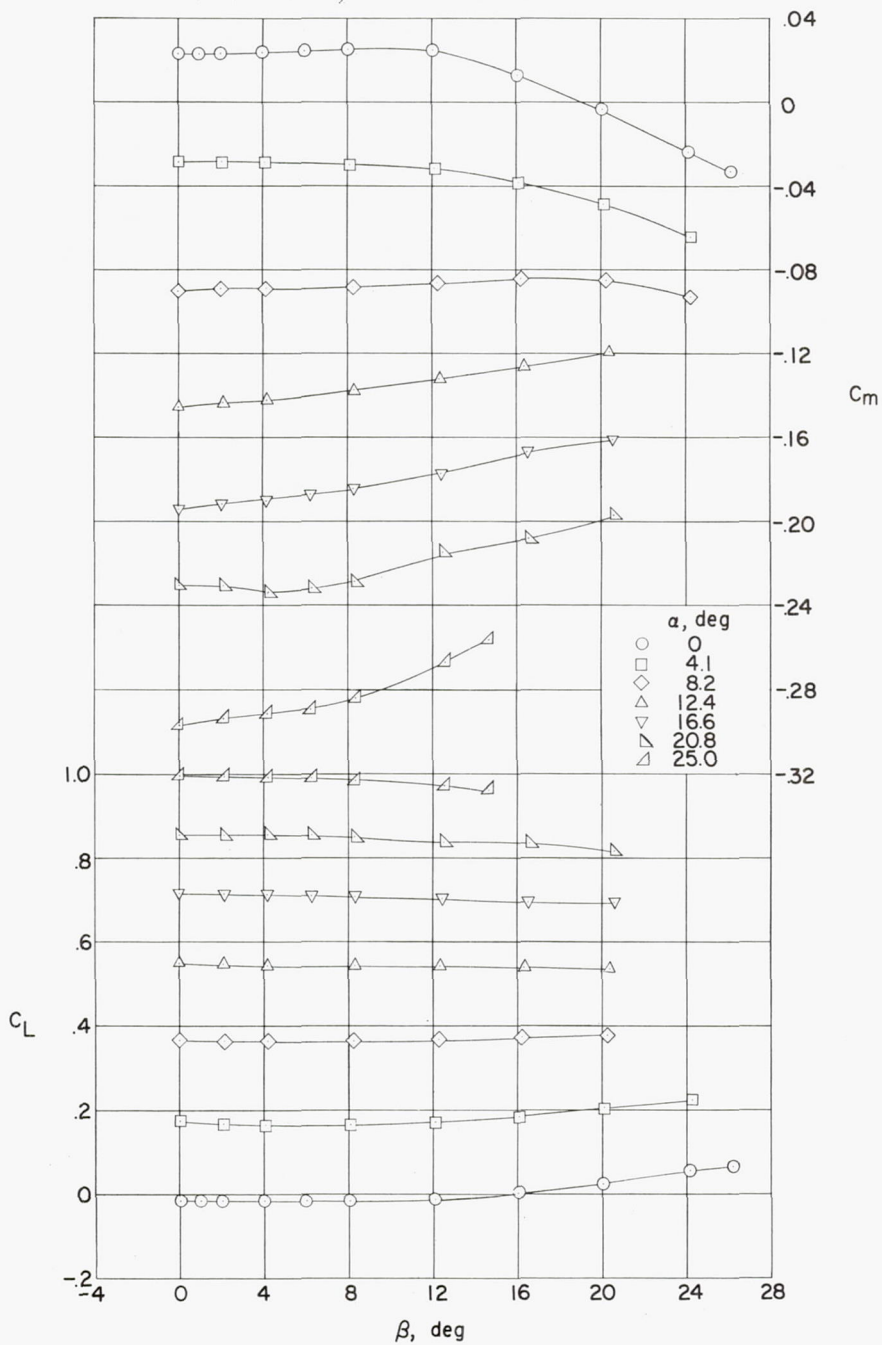
(c) BW_{HVL} ; $i_t = 0^\circ$.

Figure 6.- Continued.



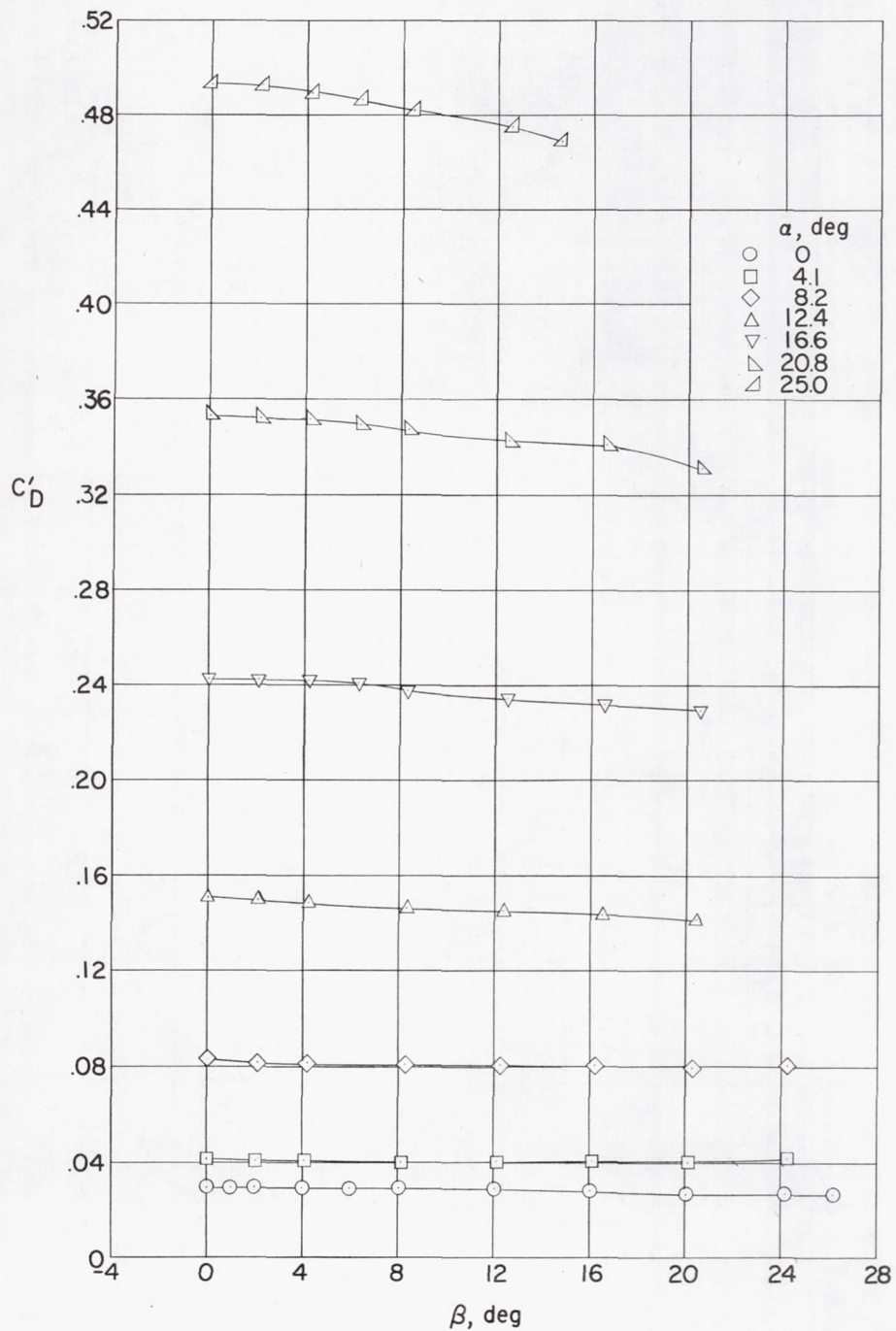
(c) Concluded.

Figure 6.- Continued.



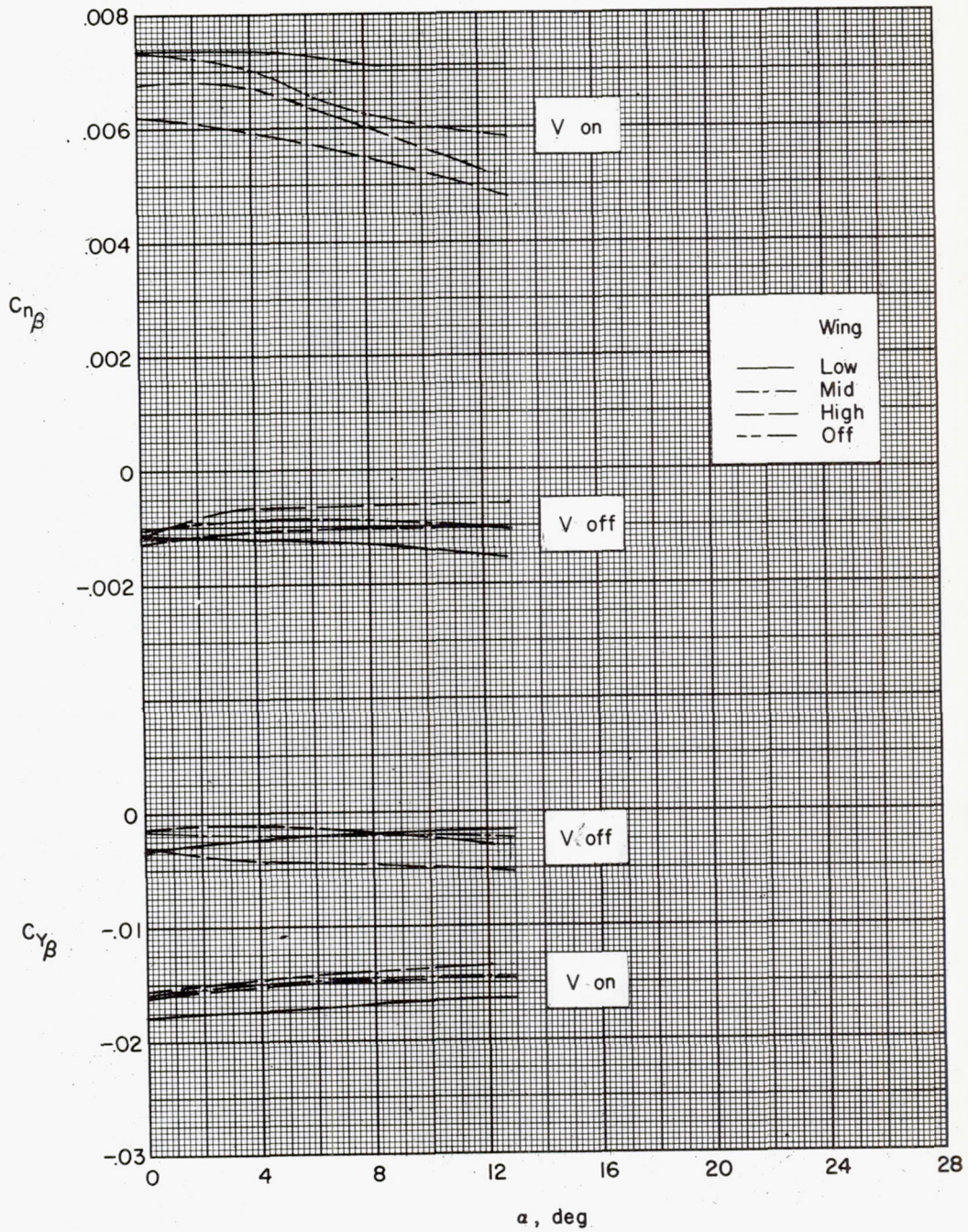
(d) $BW_{H-VH_H}; i_t = 0^\circ$.

Figure 6.- Continued.



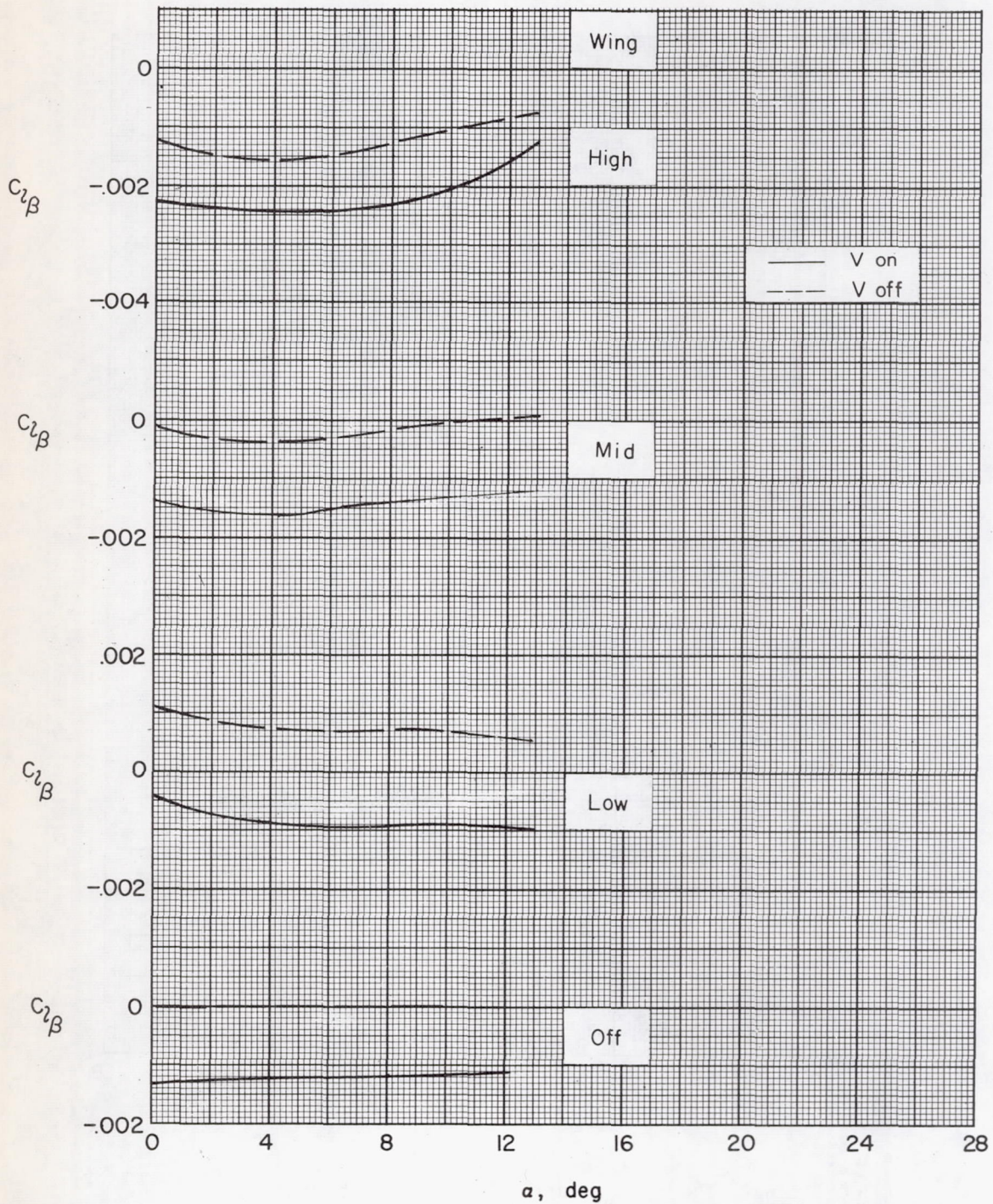
(d) Concluded.

Figure 6.- Concluded.



(a) $C_{n\beta}$ and $C_{y\beta}$ against α .

Figure 7.- Effect of wing position on the sideslip derivatives. Horizontal tail off; $M = 1.41$.



(b) $C_{l\beta}$ against α .

Figure 7.- Concluded.

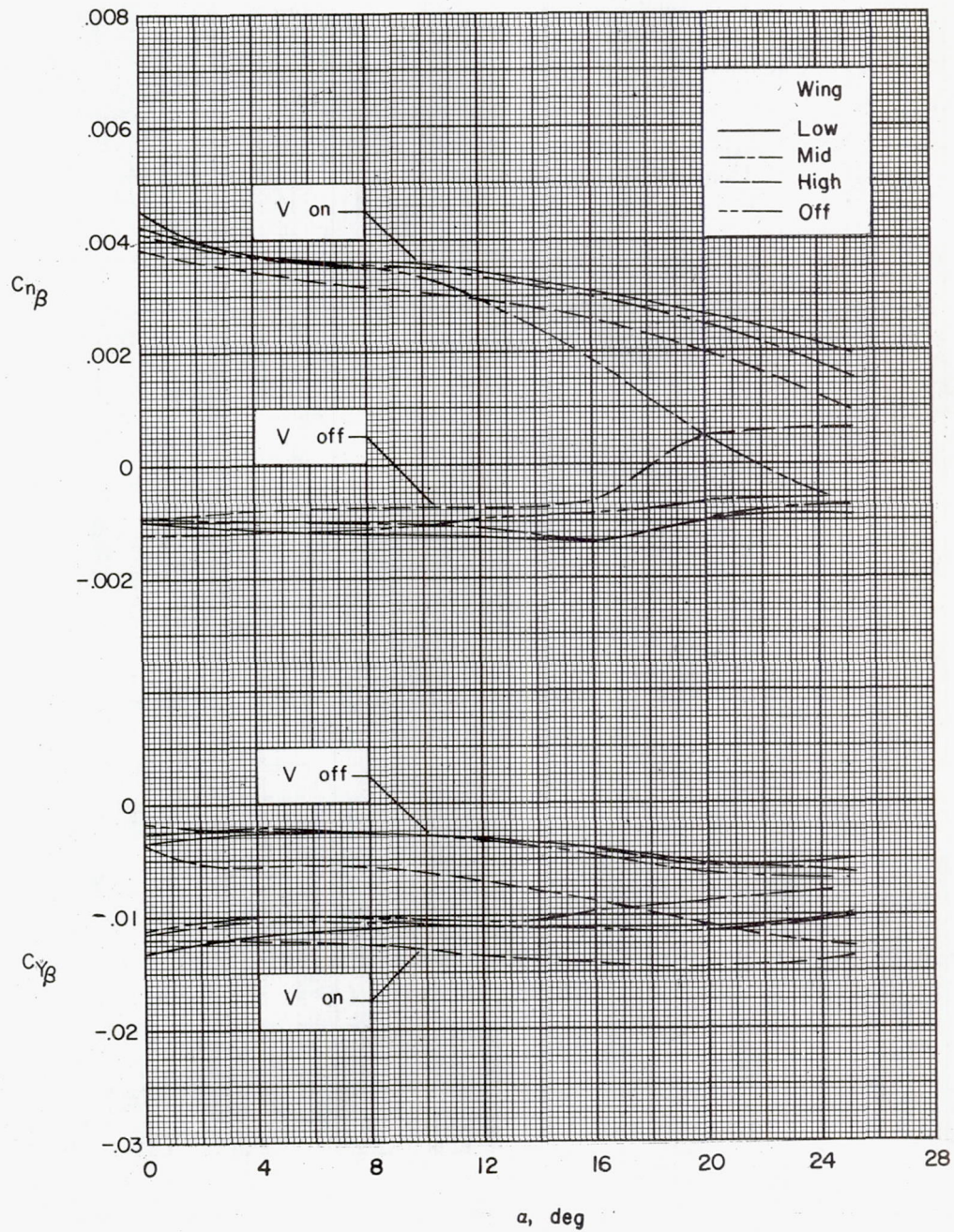
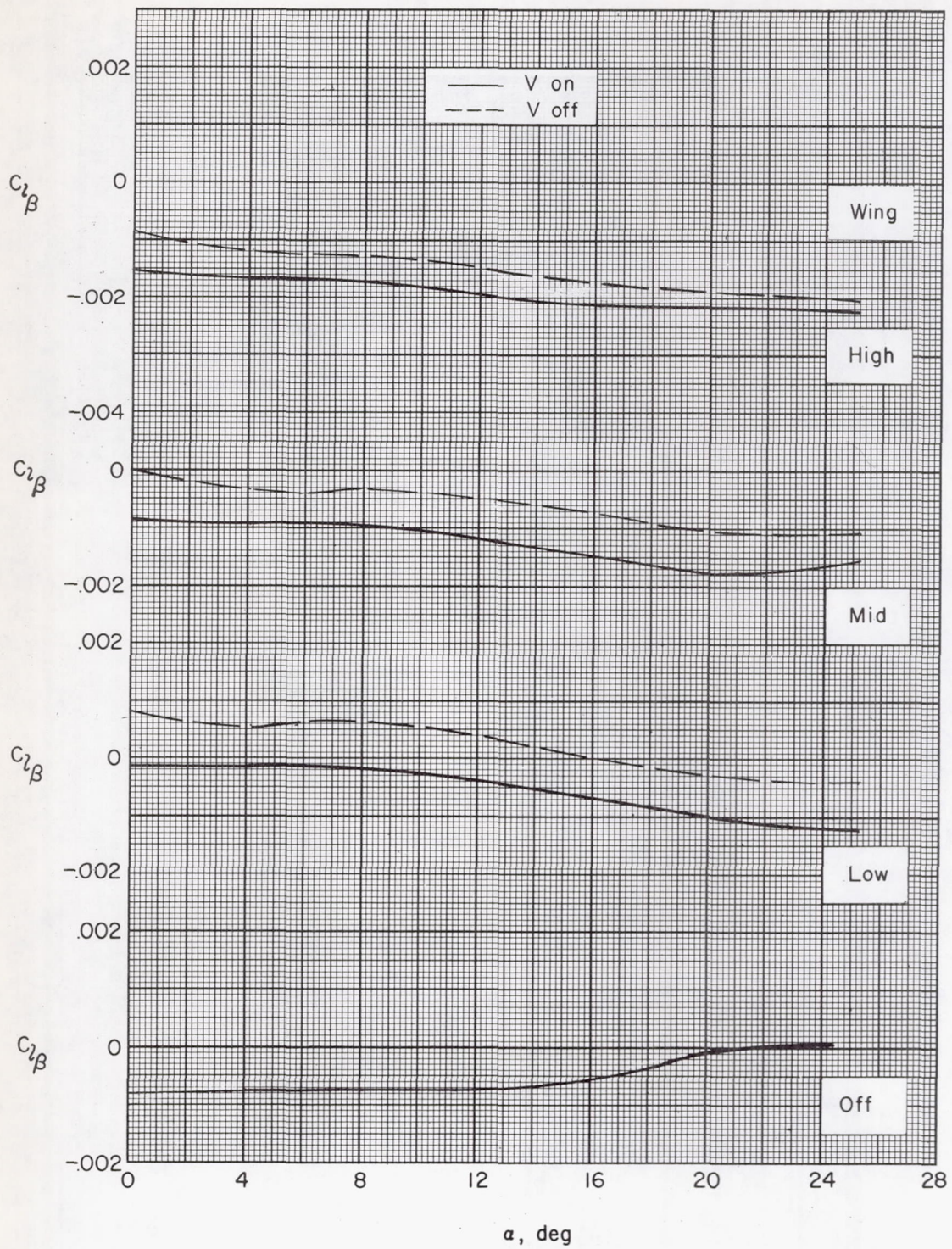
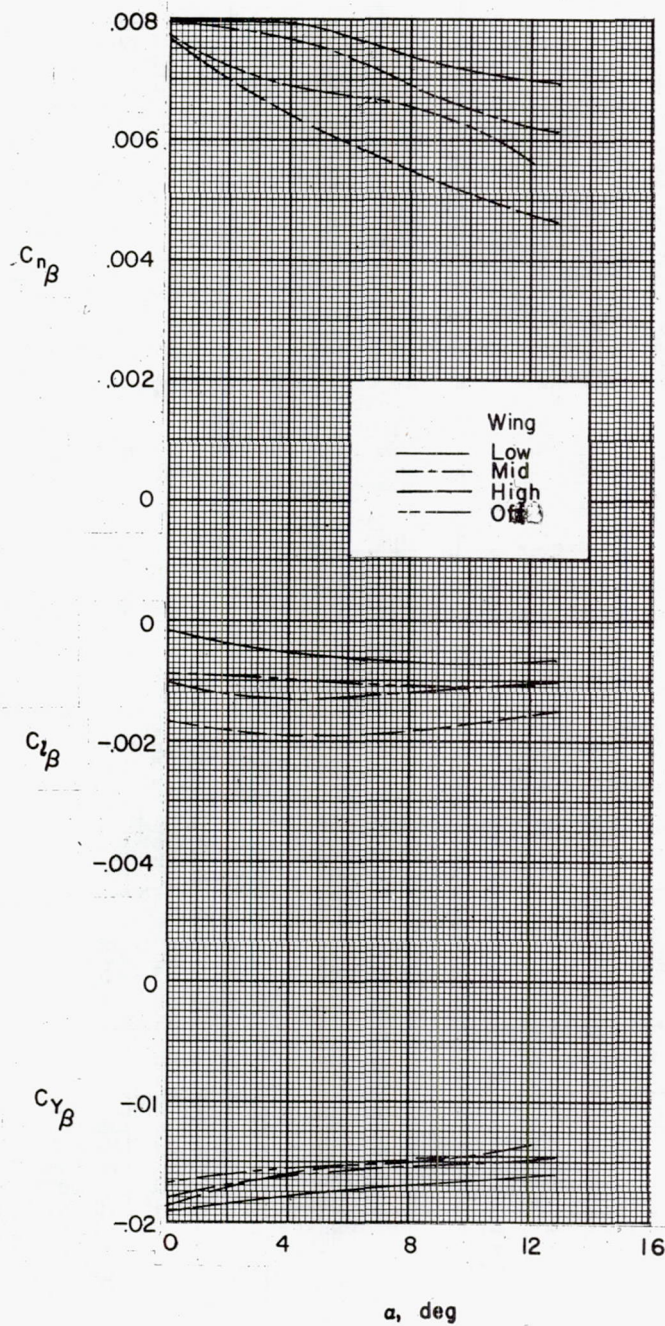
(a) $C_{n\beta}$ and $C_{y\beta}$ against α .

Figure 8.- Effect of wing position on the sideslip derivatives. Horizontal tail off; $M = 2.01$.



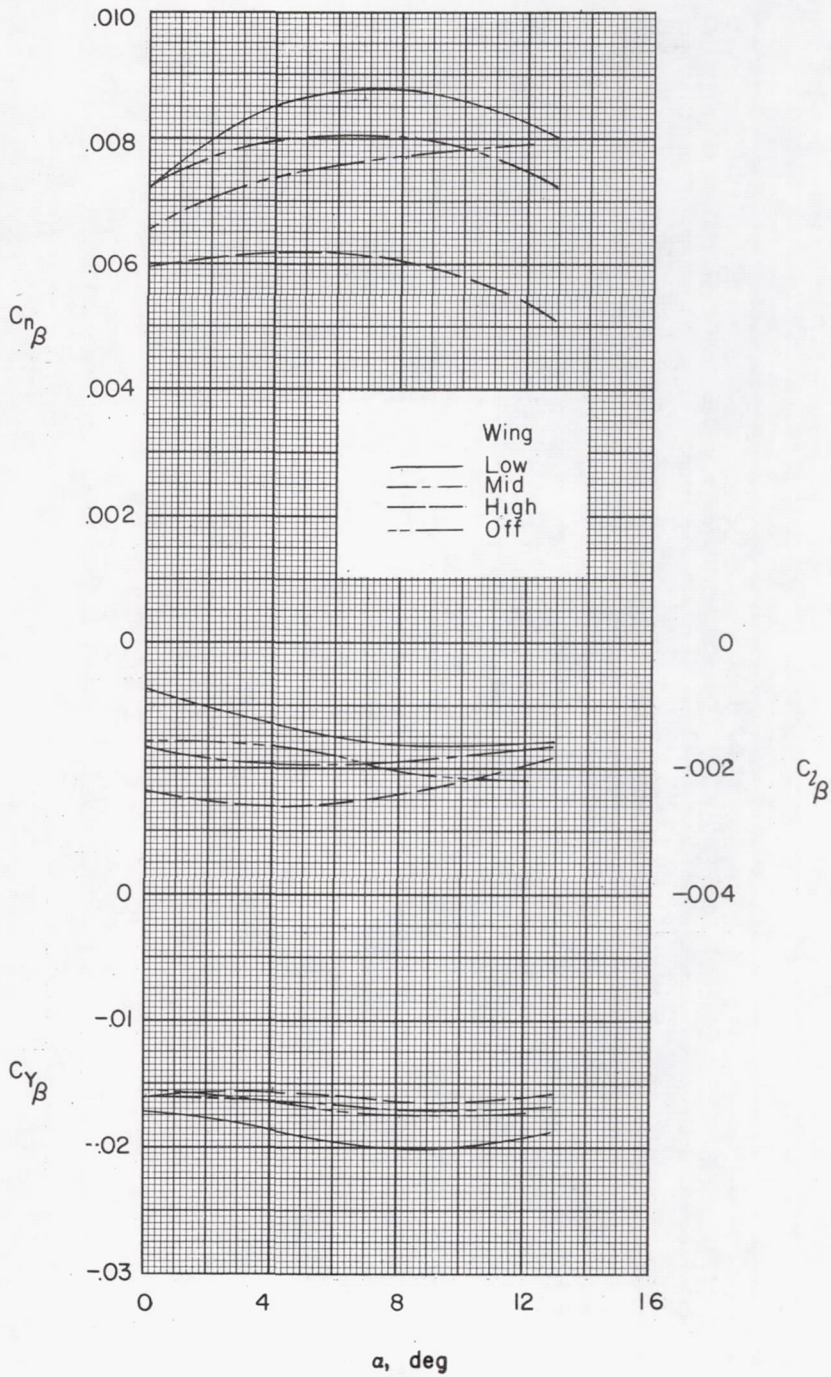
(b) $C_{l\beta}$ against α .

Figure 8.- Concluded.



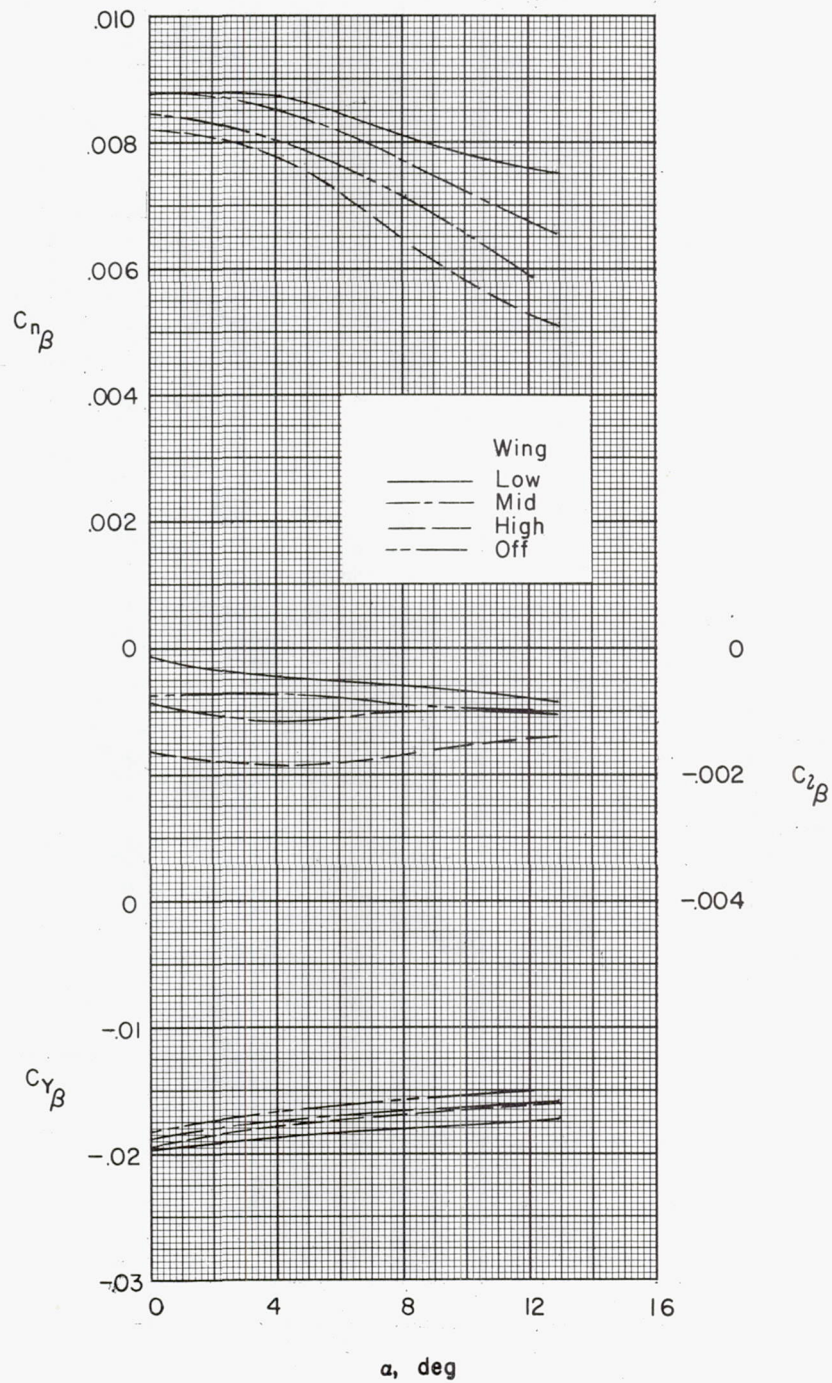
(a) H_L ; $i_t = 0^\circ$.

Figure 9.- Effect of wing position on the sideslip derivatives. Complete model; $M = 1.41$.



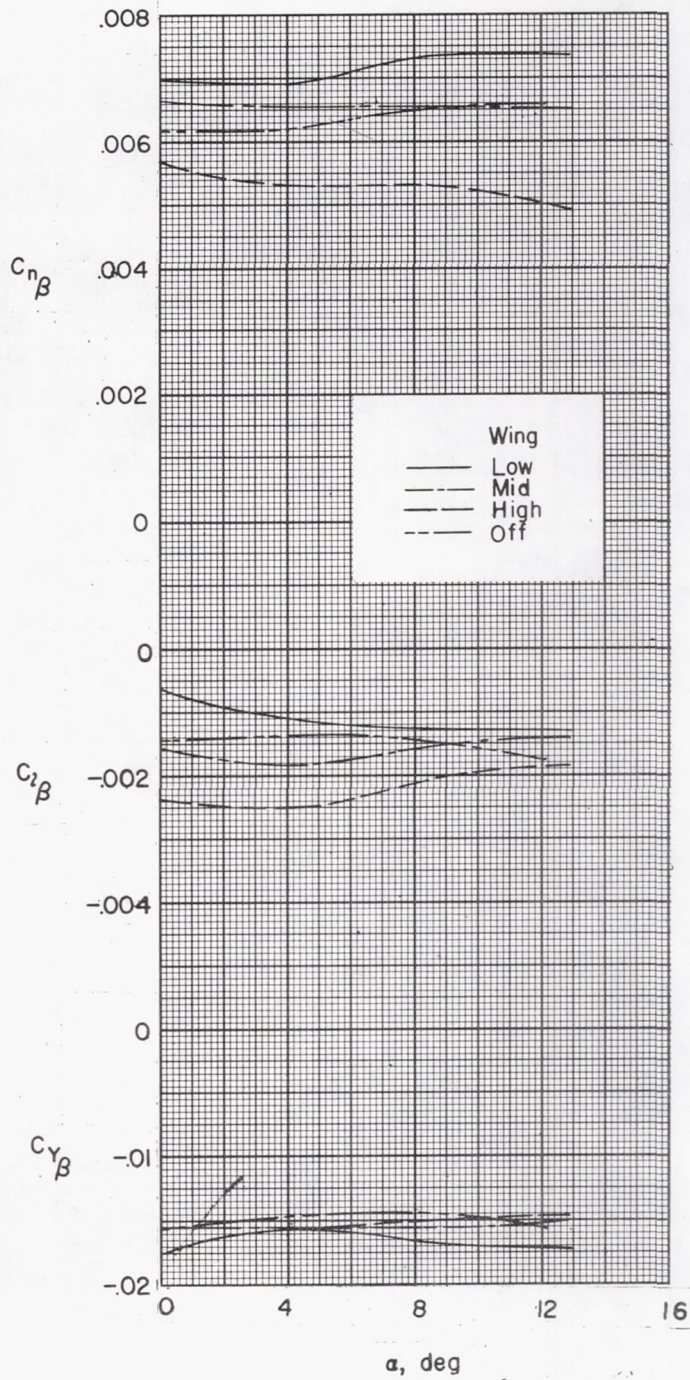
(b) $H_H; i_t = 0^\circ$.

Figure 9.- Continued.



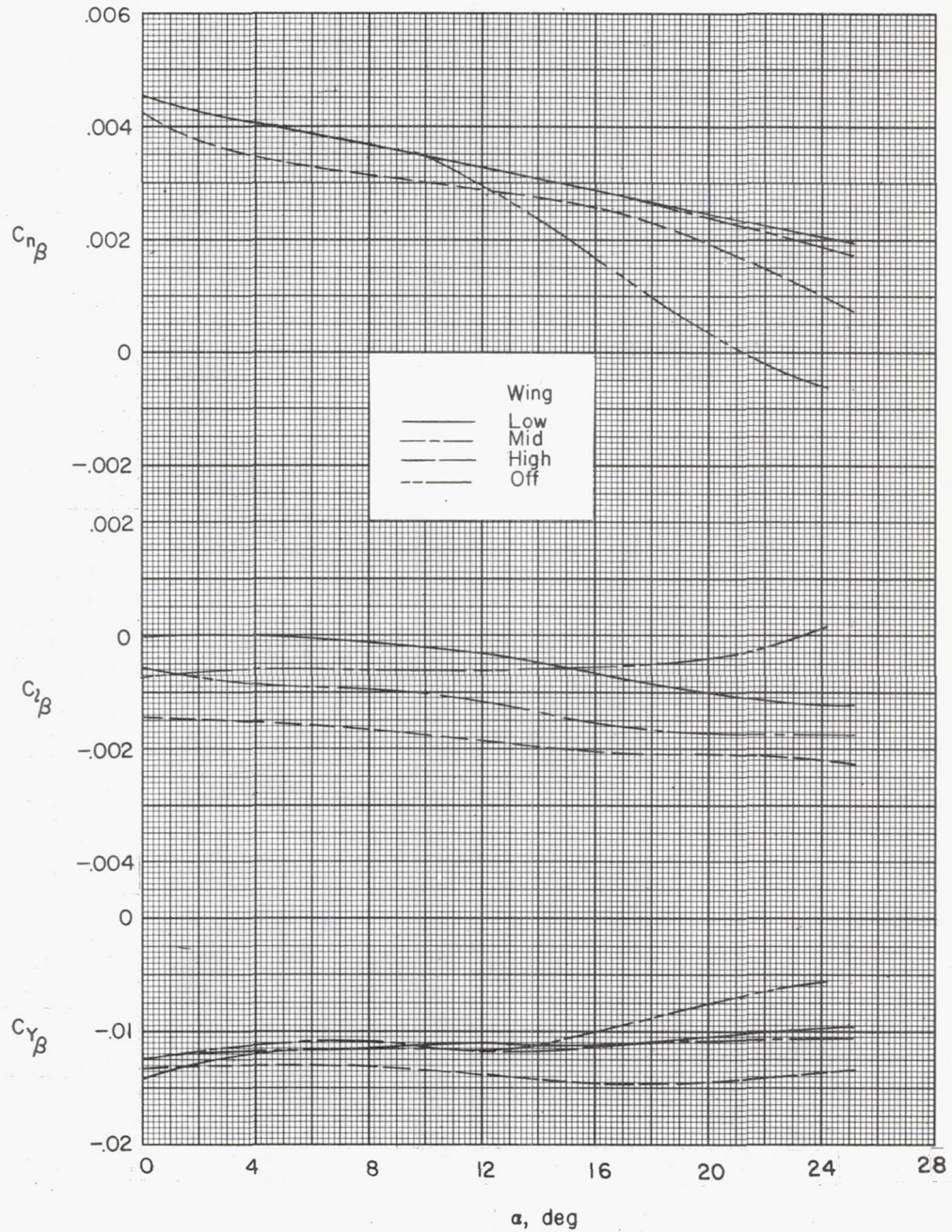
(c) $H_L; i_t = -6^\circ$.

Figure 9.- Continued.



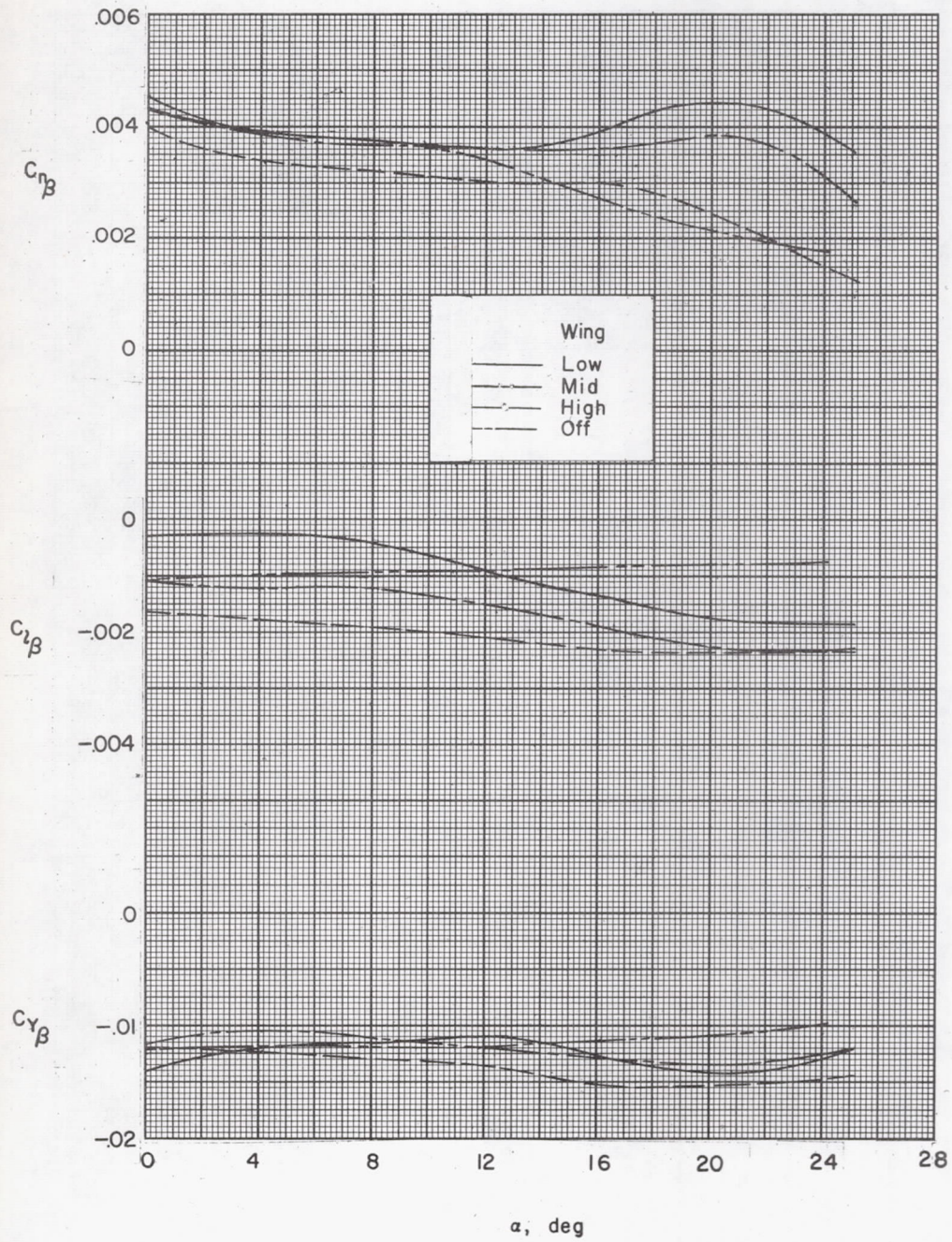
(d) $H_H; i_t = -6^\circ$.

Figure 9.- Concluded.



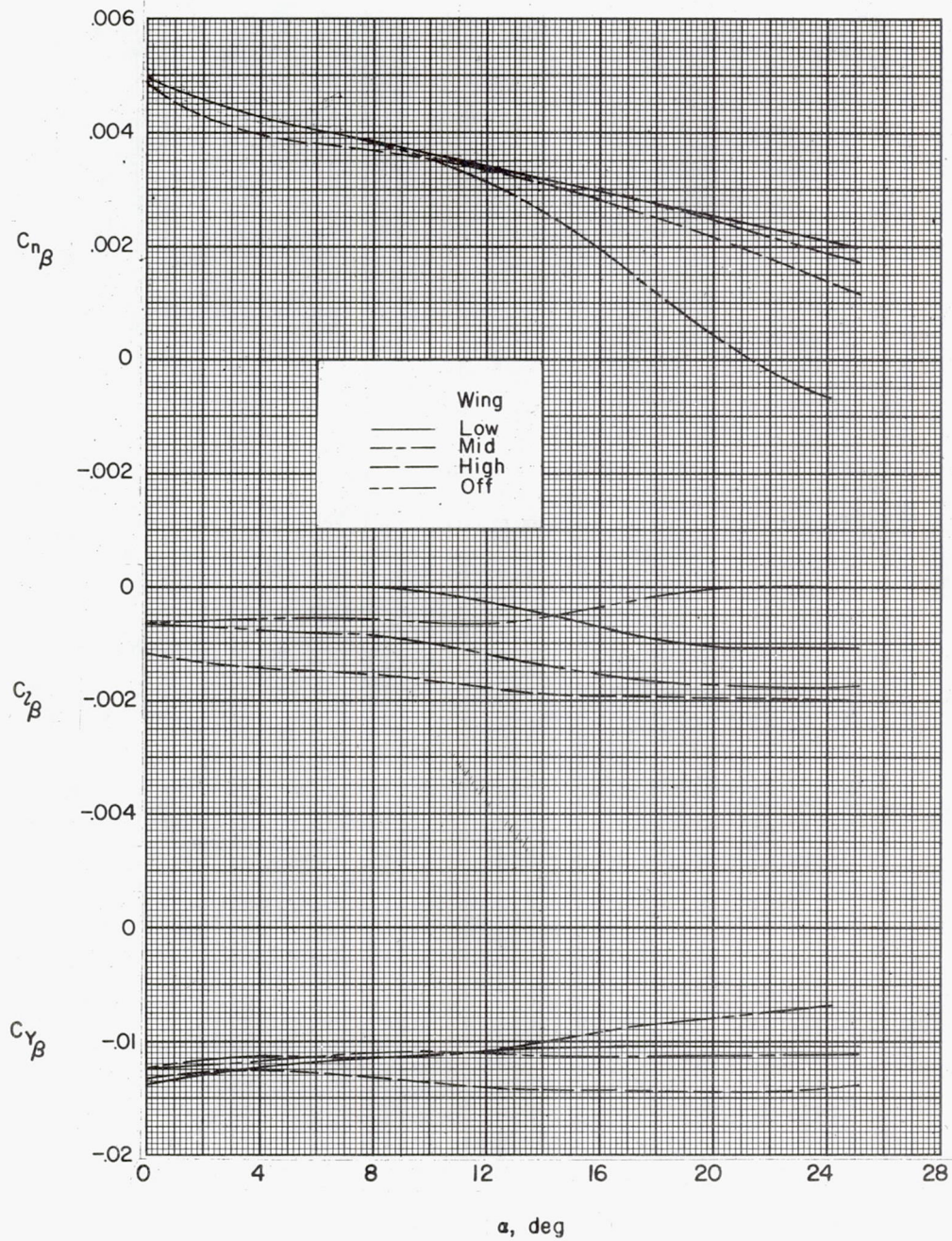
(a) H_L ; $i_t = 0^\circ$.

Figure 10.- Effect of wing position on the sideslip derivatives. Complete model; $M = 2.01$.



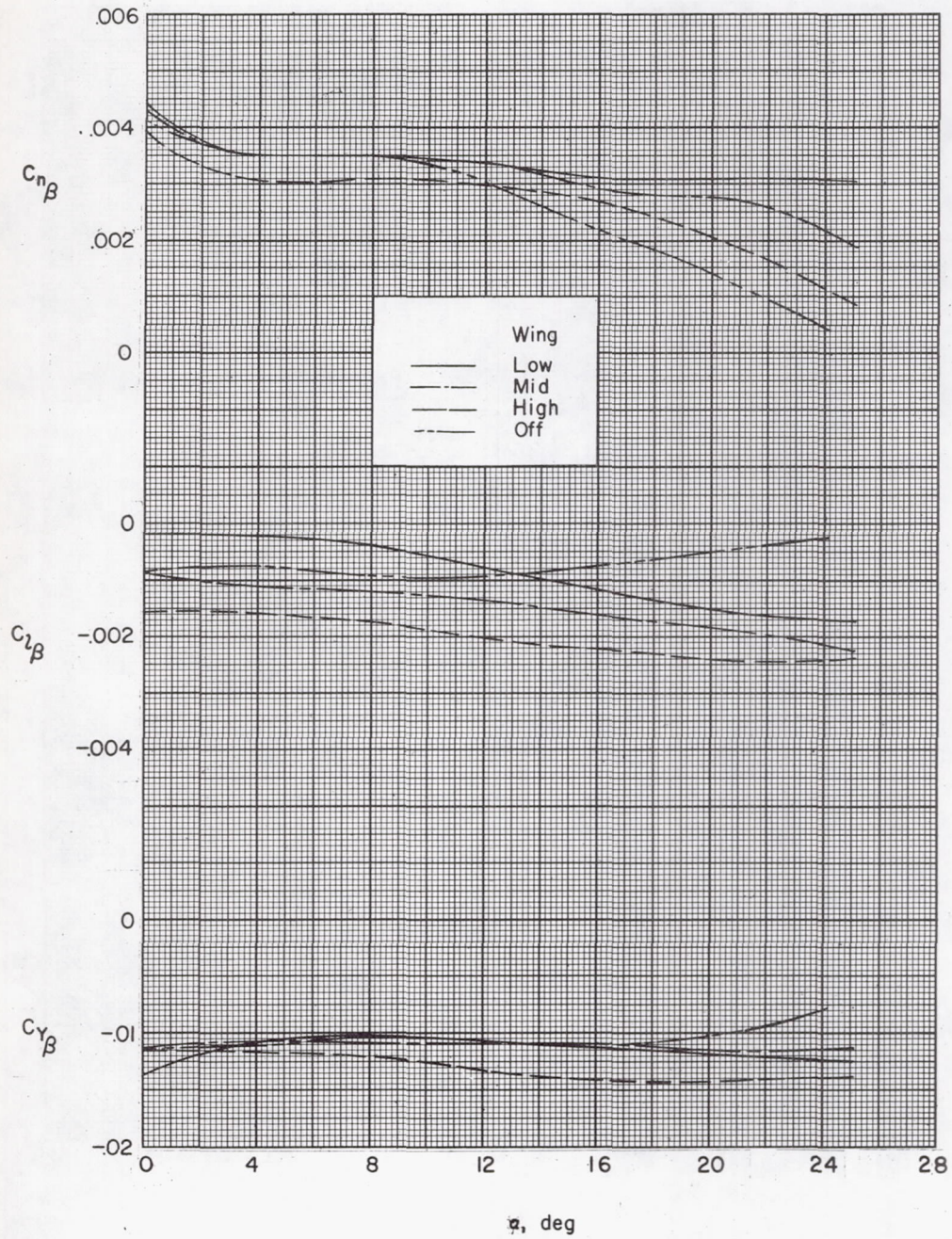
(b) $H_H; i_t = 0^\circ$.

Figure 10.- Continued.



(c) H_L ; $i_t = -6^\circ$.

Figure 10.- Continued.



(d) $H_H; i_t = -6^\circ$.

Figure 10.- Concluded.

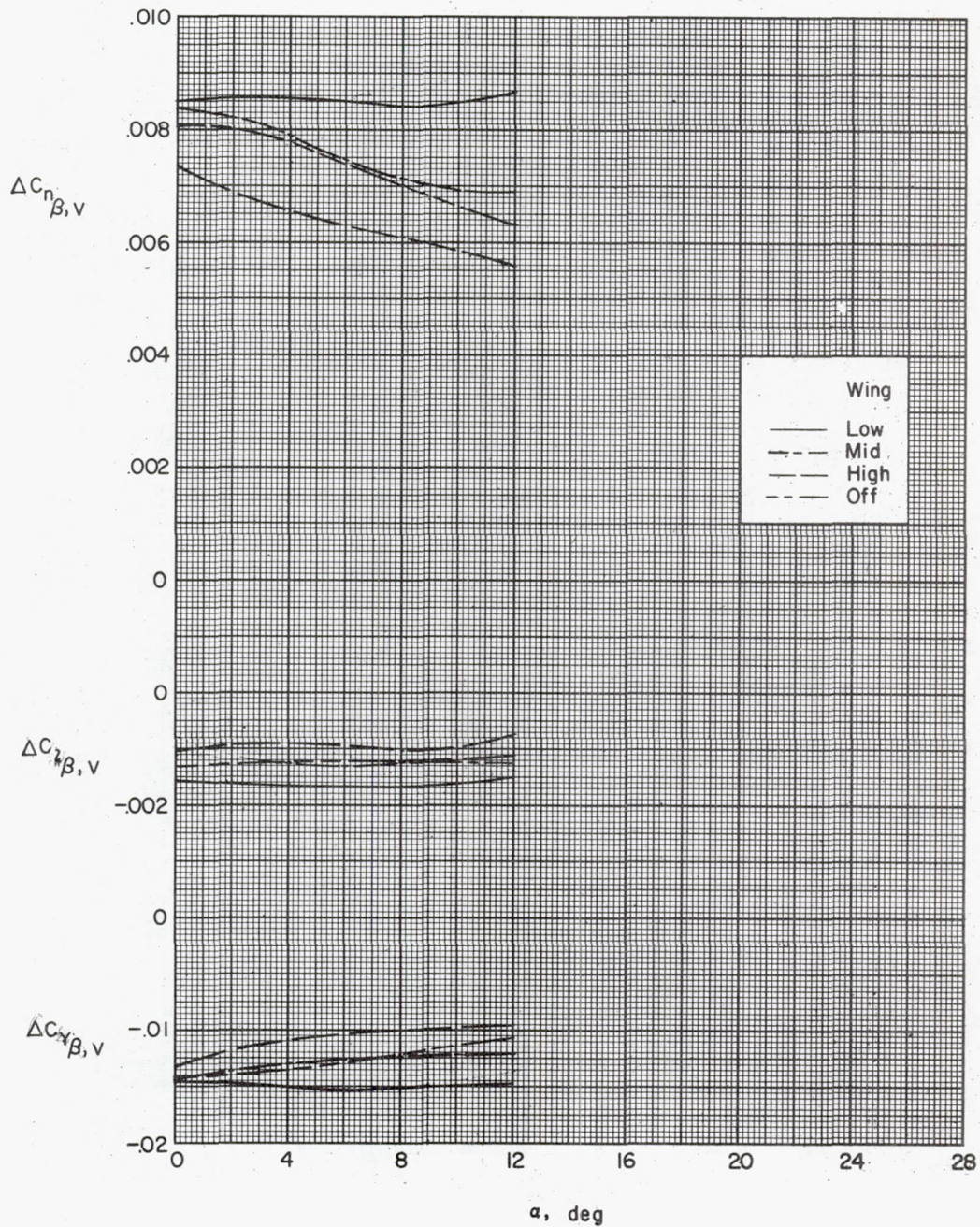
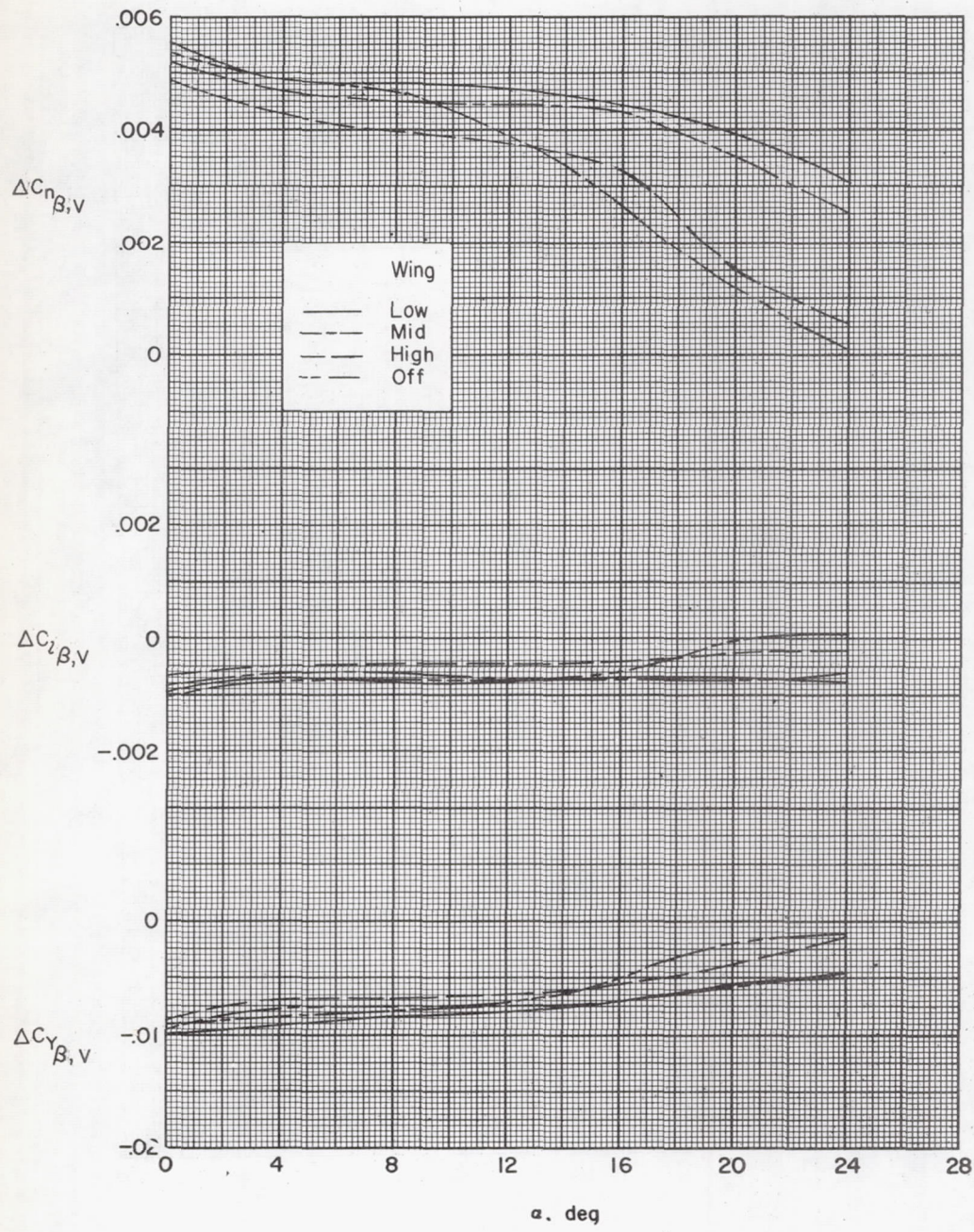
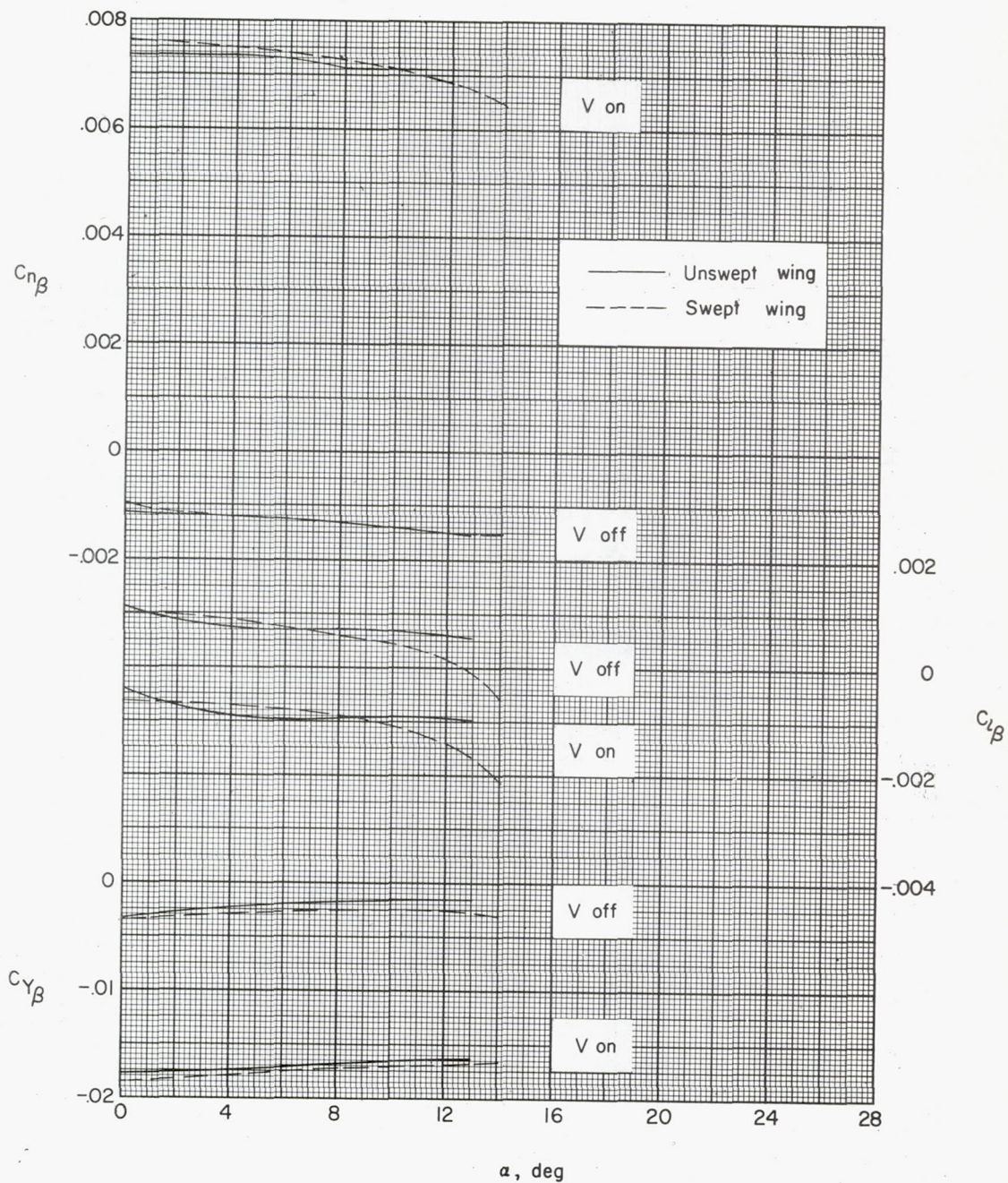
(a) $M = 1.41$.

Figure 11.- Effect of wing position on the contribution of the vertical tail to the sideslip derivatives. Horizontal tail off.



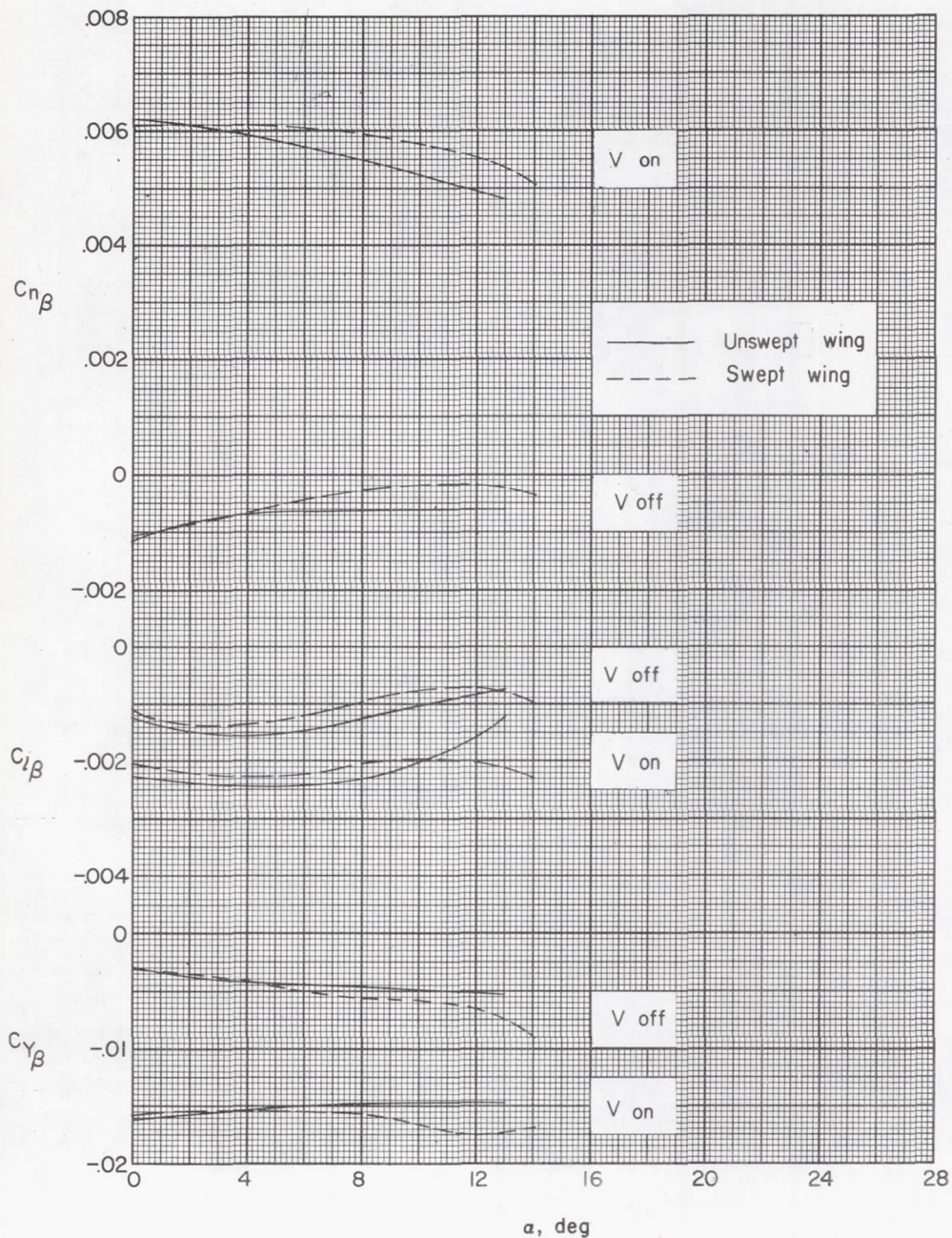
(b) M = 2.01.

Figure 11.- Concluded.



(a) W_L .

Figure 12.- Effect of wing plan form on the sideslip derivatives. Horizontal tail off; $M = 1.41$.



(b) W_H .

Figure 12.- Concluded.

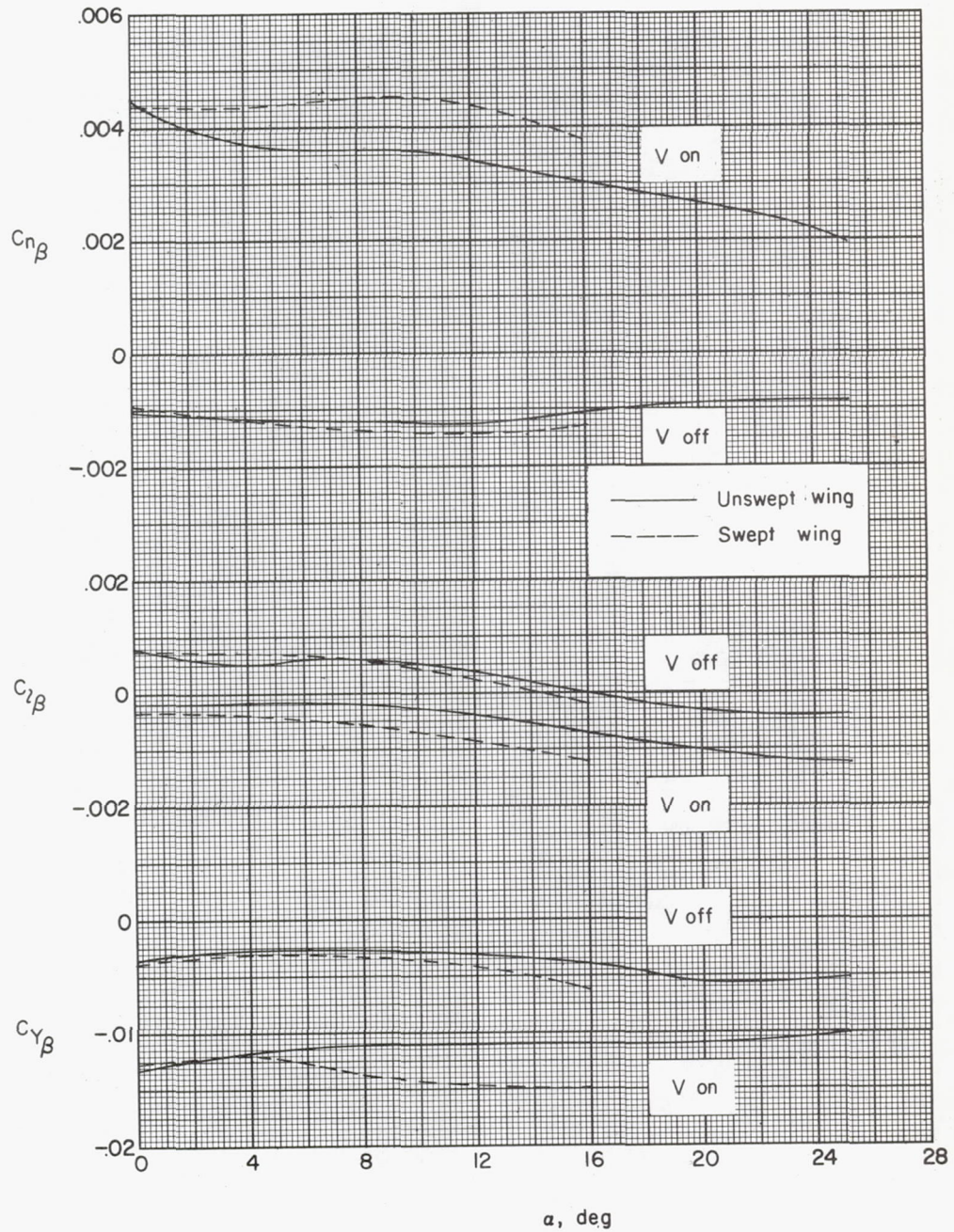
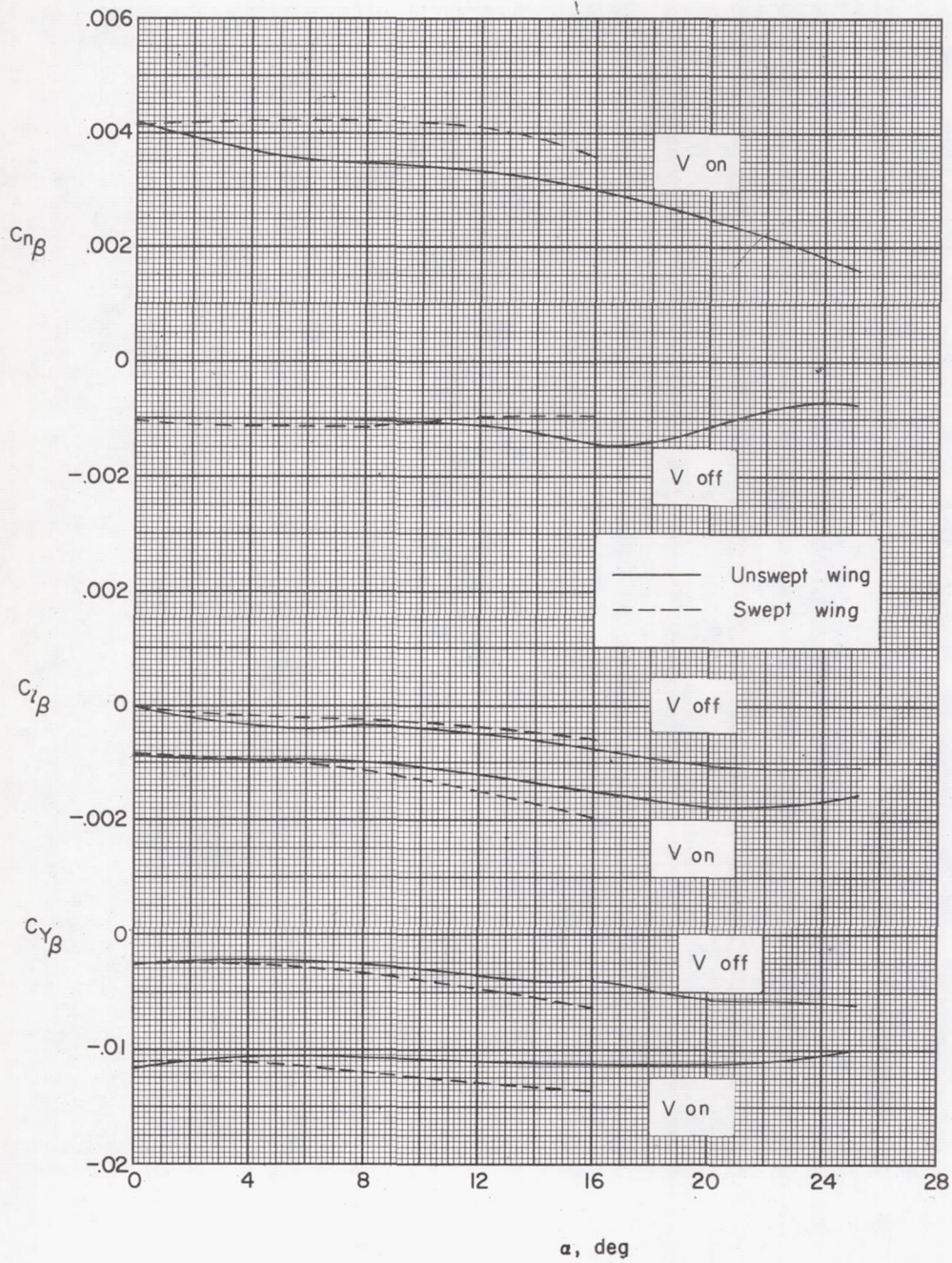
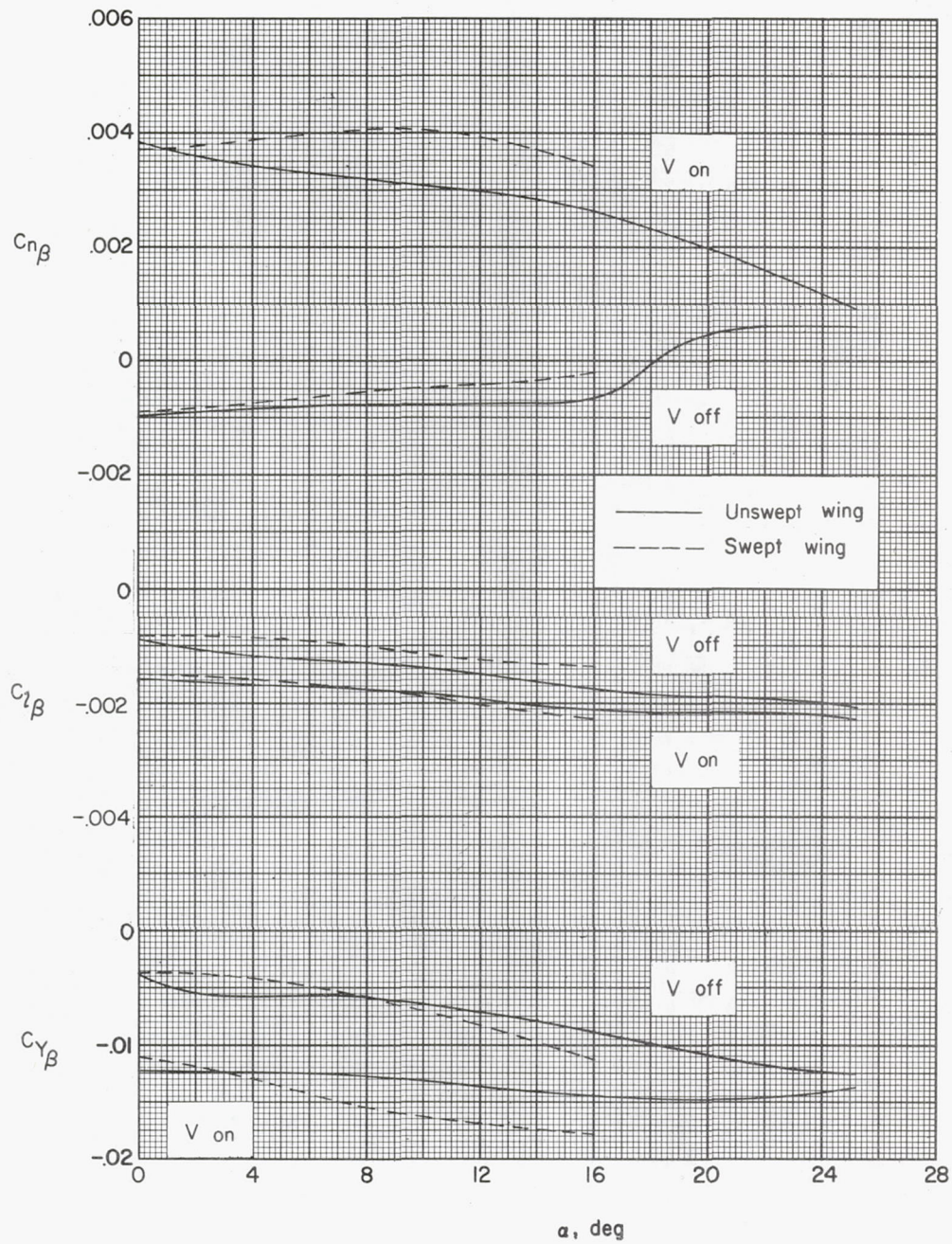
(a) W_L .

Figure 13.- Effect of wing plan form on the sideslip derivatives. Horizontal tail off; $M = 2.01$.



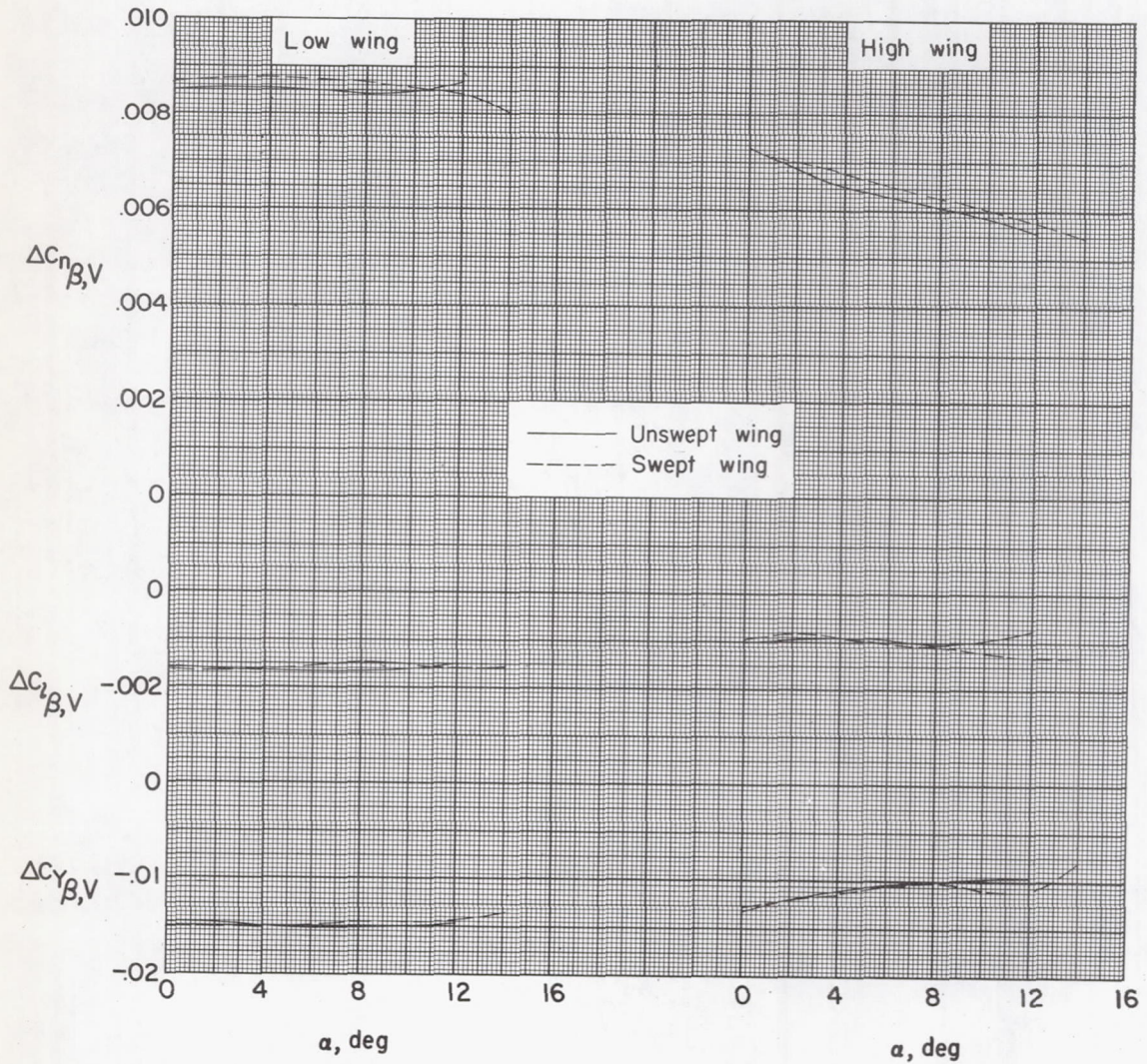
(b) W_M .

Figure 13.- Continued.



(c) W_H .

Figure 13.- Concluded.



(a) $M = 1.41$.

Figure 14.- Effect of wing plan form on the contribution of the vertical tail to the sideslip derivatives. Horizontal tail off.

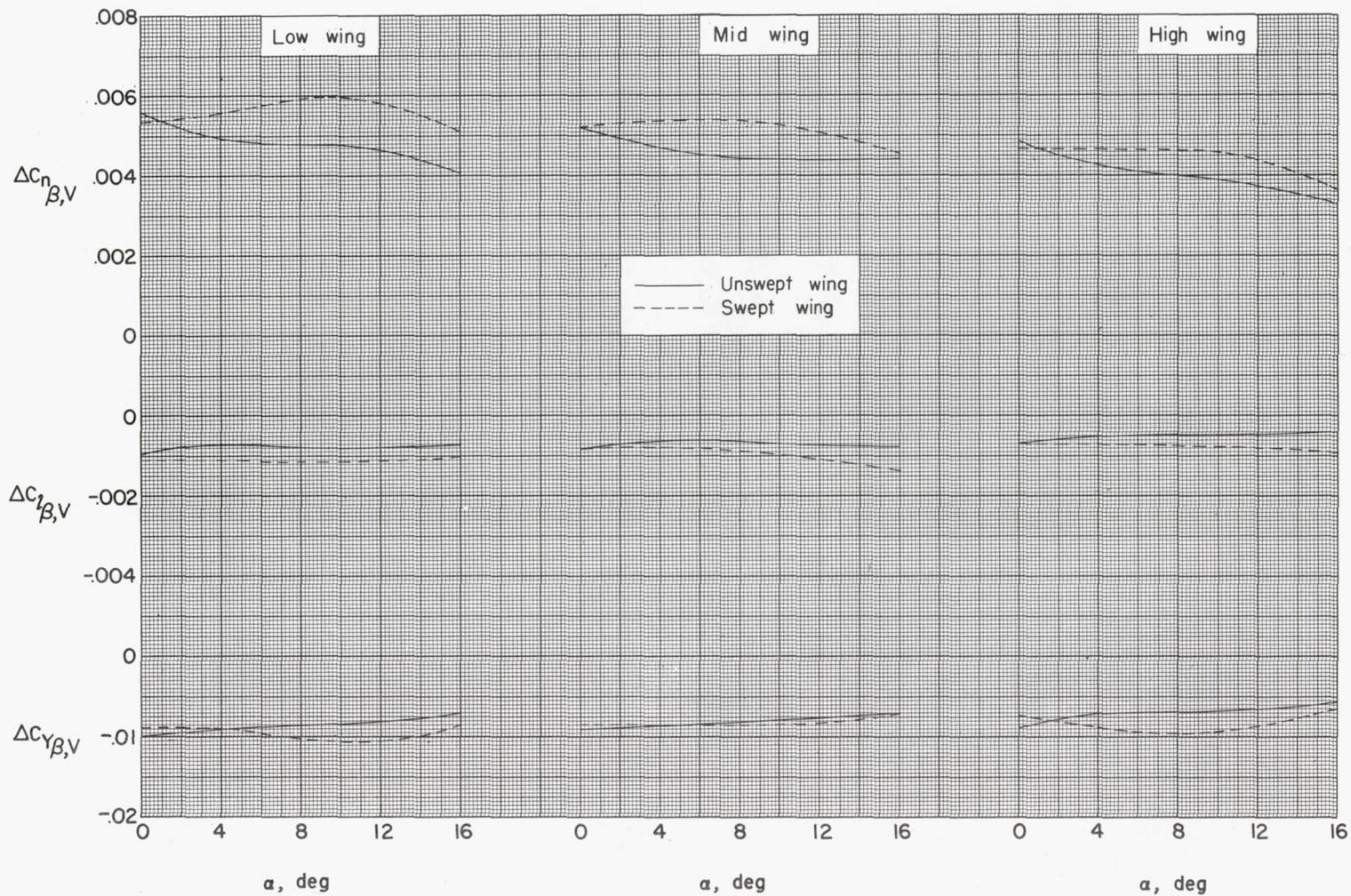
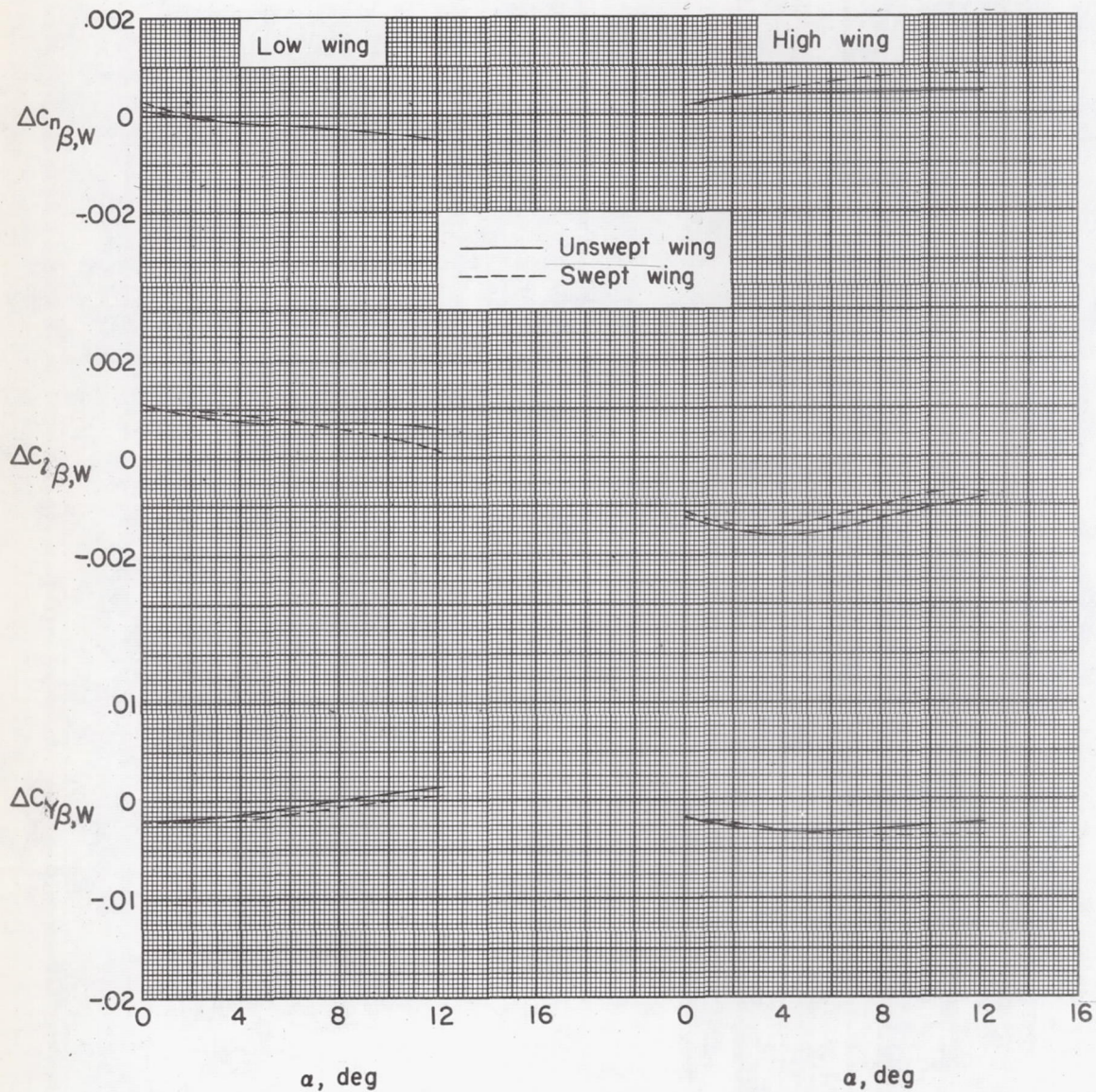
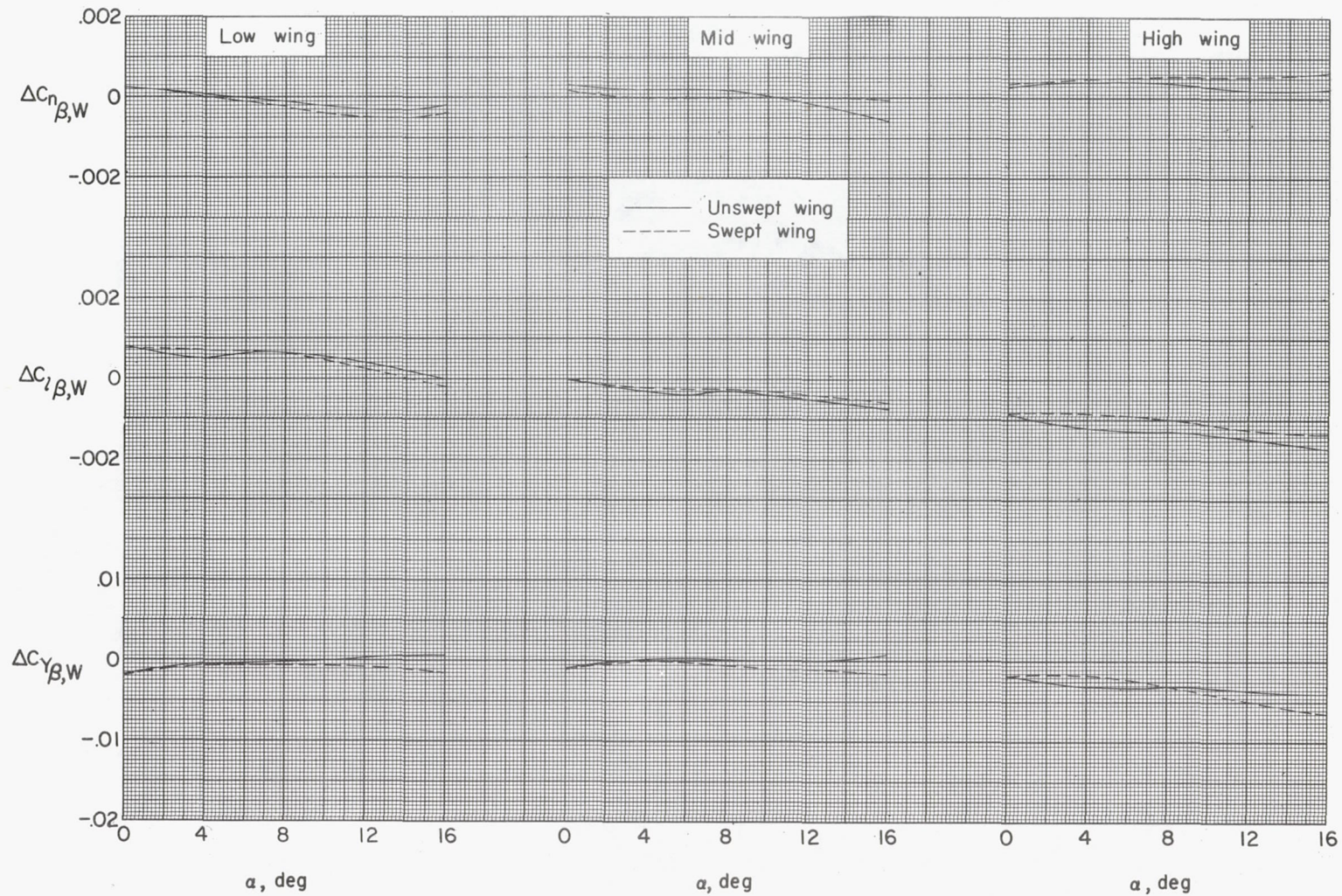
(b) $M = 2.01$.

Figure 14.- Concluded.



(a) $M = 1.41$.

Figure 15.- Effect of wing plan form on the contribution of the wing to the sideslip derivatives. Vertical and horizontal tails off.



(b) $M = 2.01$.

Figure 15.- Concluded.

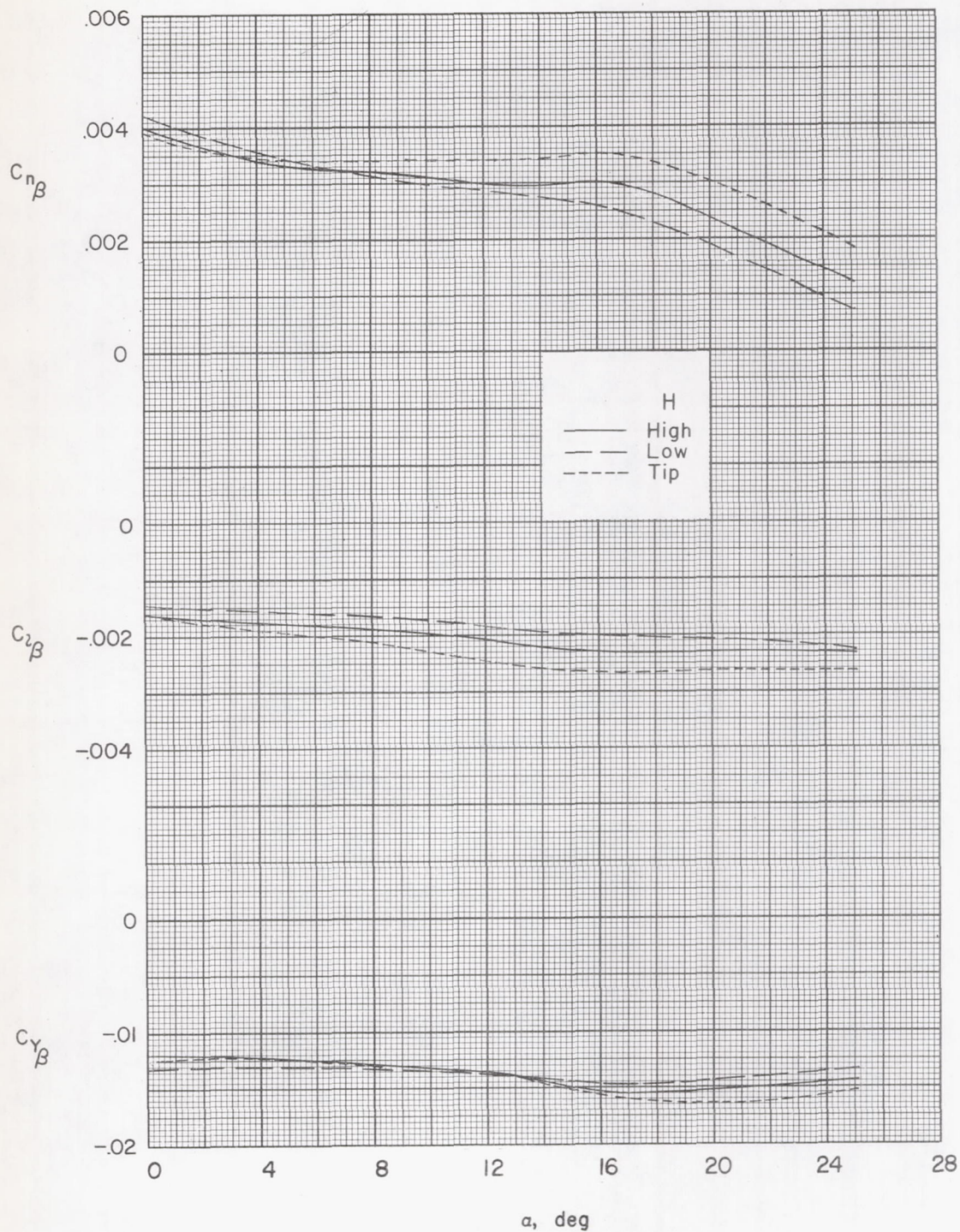


Figure 16.- Effect of horizontal-tail position on the sideslip derivatives. Complete model with high wing; $i_t = 0^\circ$; $M = 2.01$.

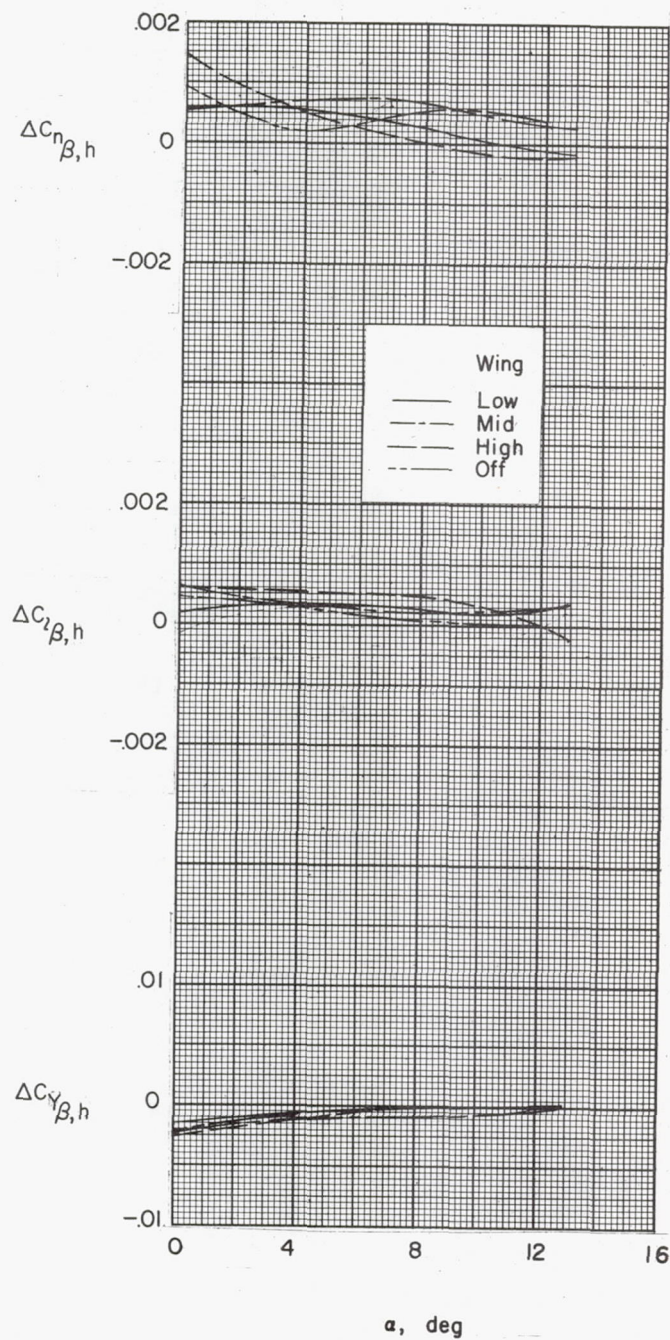
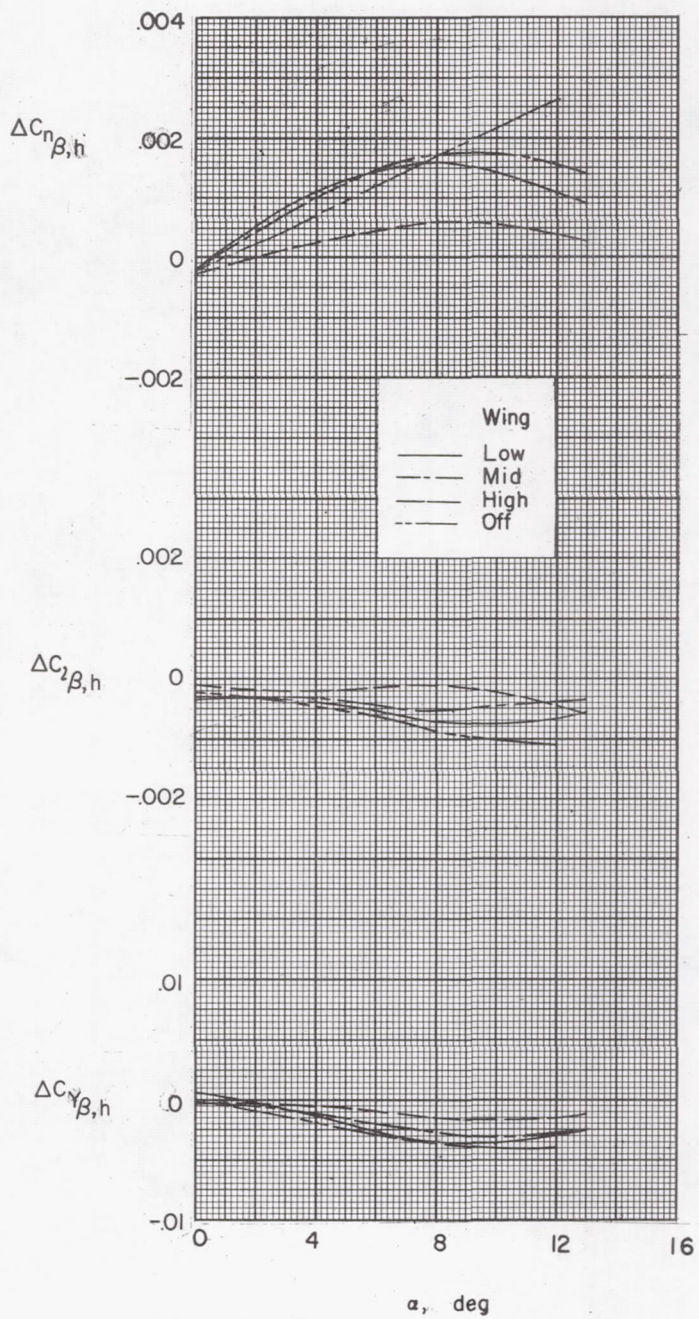
(a) H_L .

Figure 17.- Effect of wing position on the contribution of the horizontal tail to the sideslip derivatives. Complete model; $i_t = 0^\circ$; $M = 1.41$.



(b) H_H .

Figure 17.- Concluded.

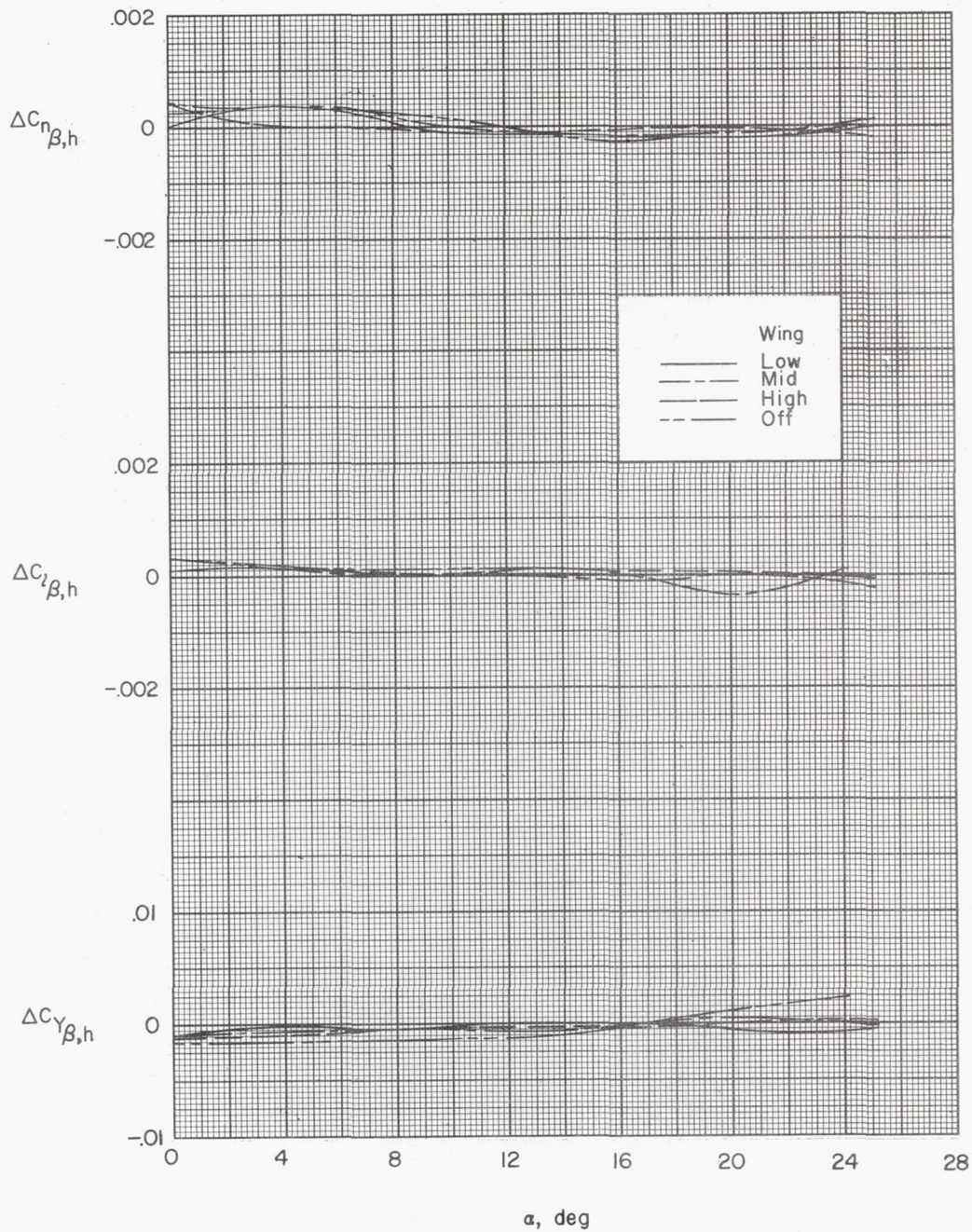
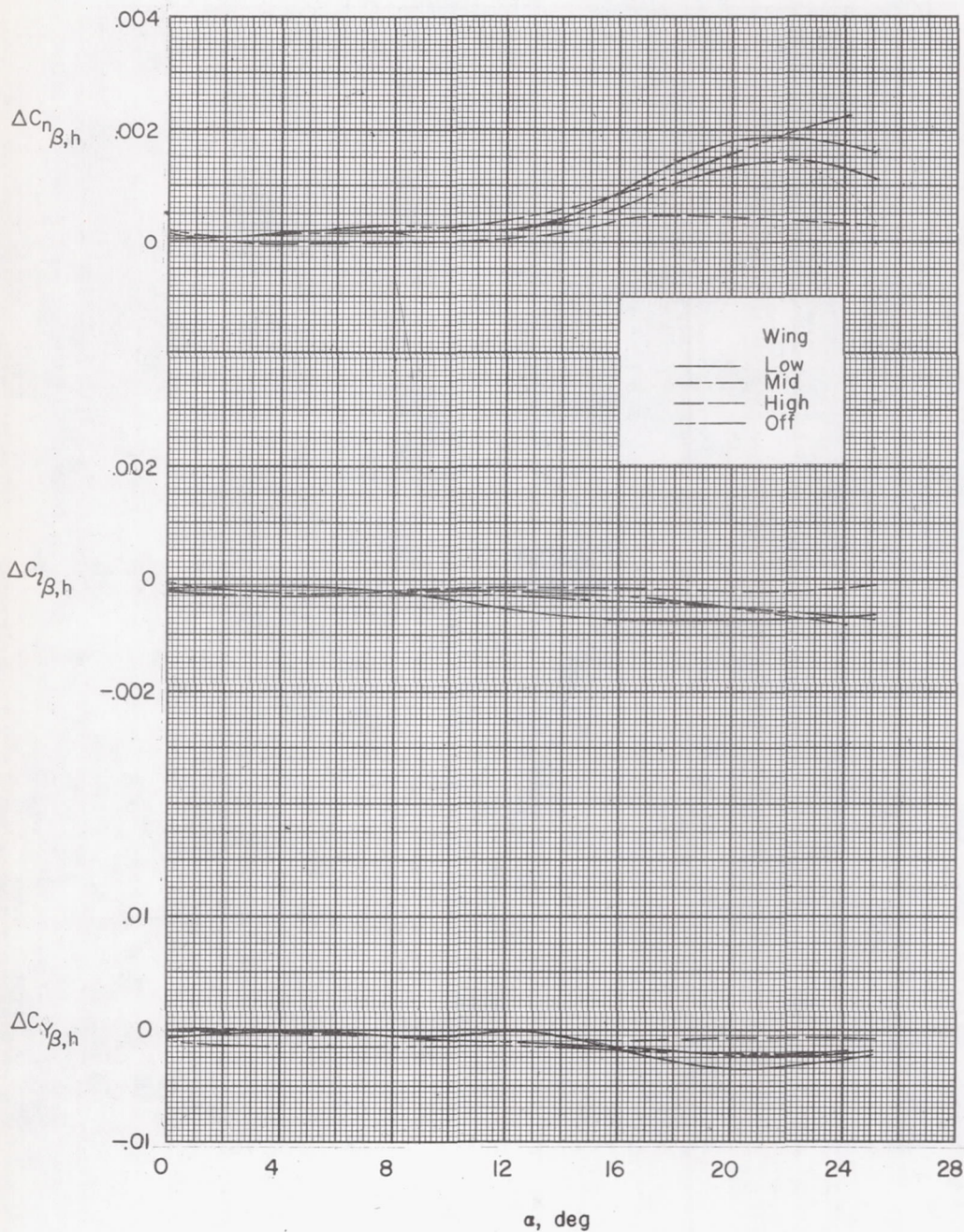
(a) H_L .

Figure 18.- Effect of wing position on the contribution of the horizontal tail to the sideslip derivatives. Complete model; $i_t = 0^\circ$; $M = 2.01$.



(b) H_H .

Figure 18.- Concluded.

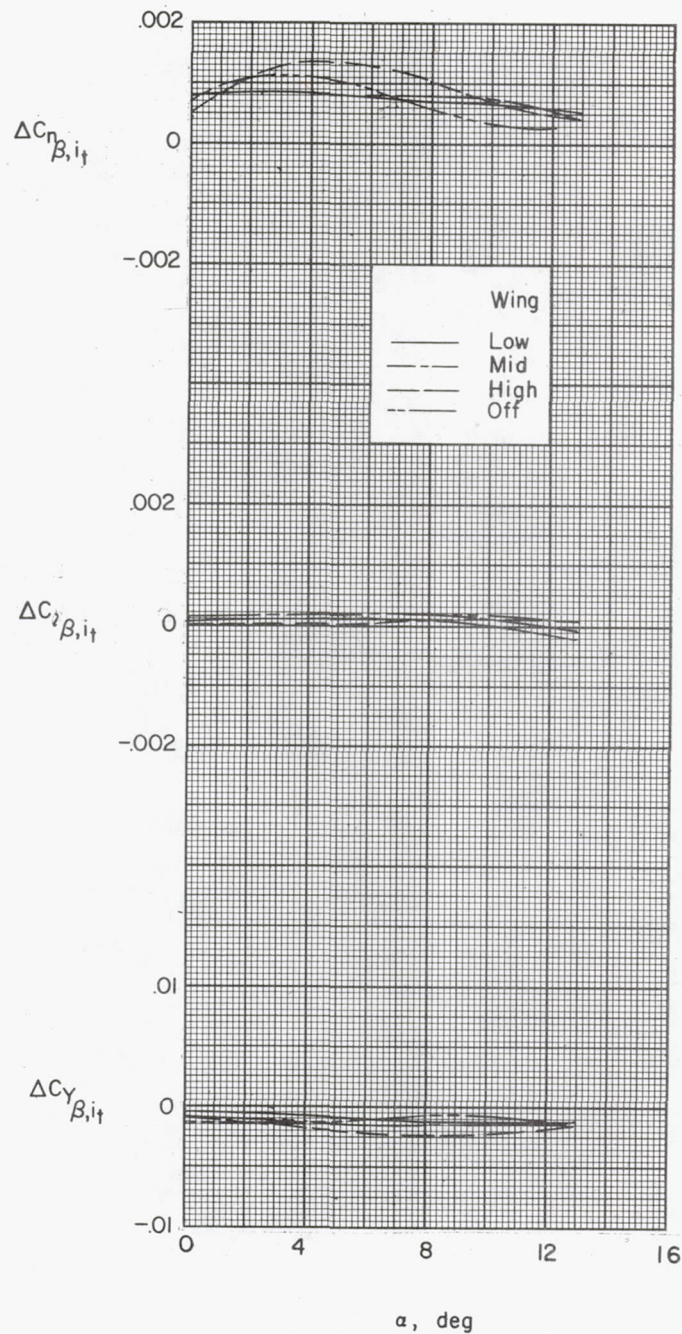
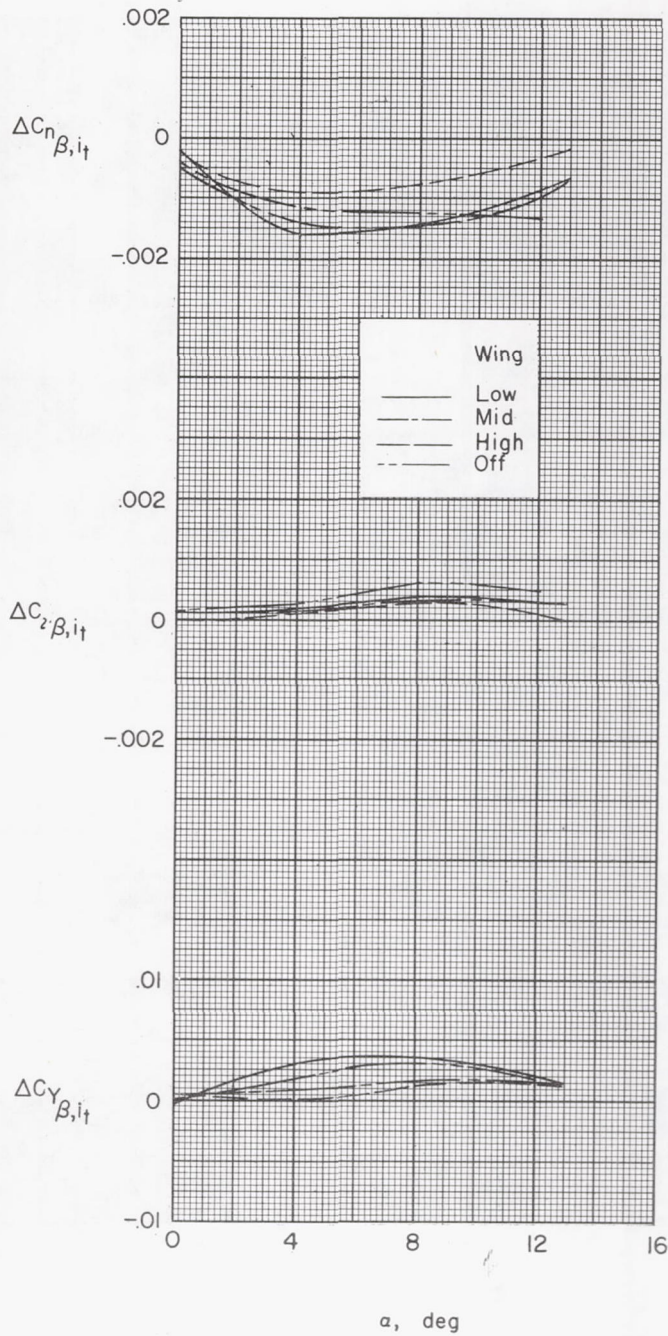
(a) H_L .

Figure 19.- Effect of wing position on the contribution of deflection of the horizontal tail to the sideslip derivatives. Complete model; $M = 1.41$.



(b) H_H .

Figure 19.- Concluded.

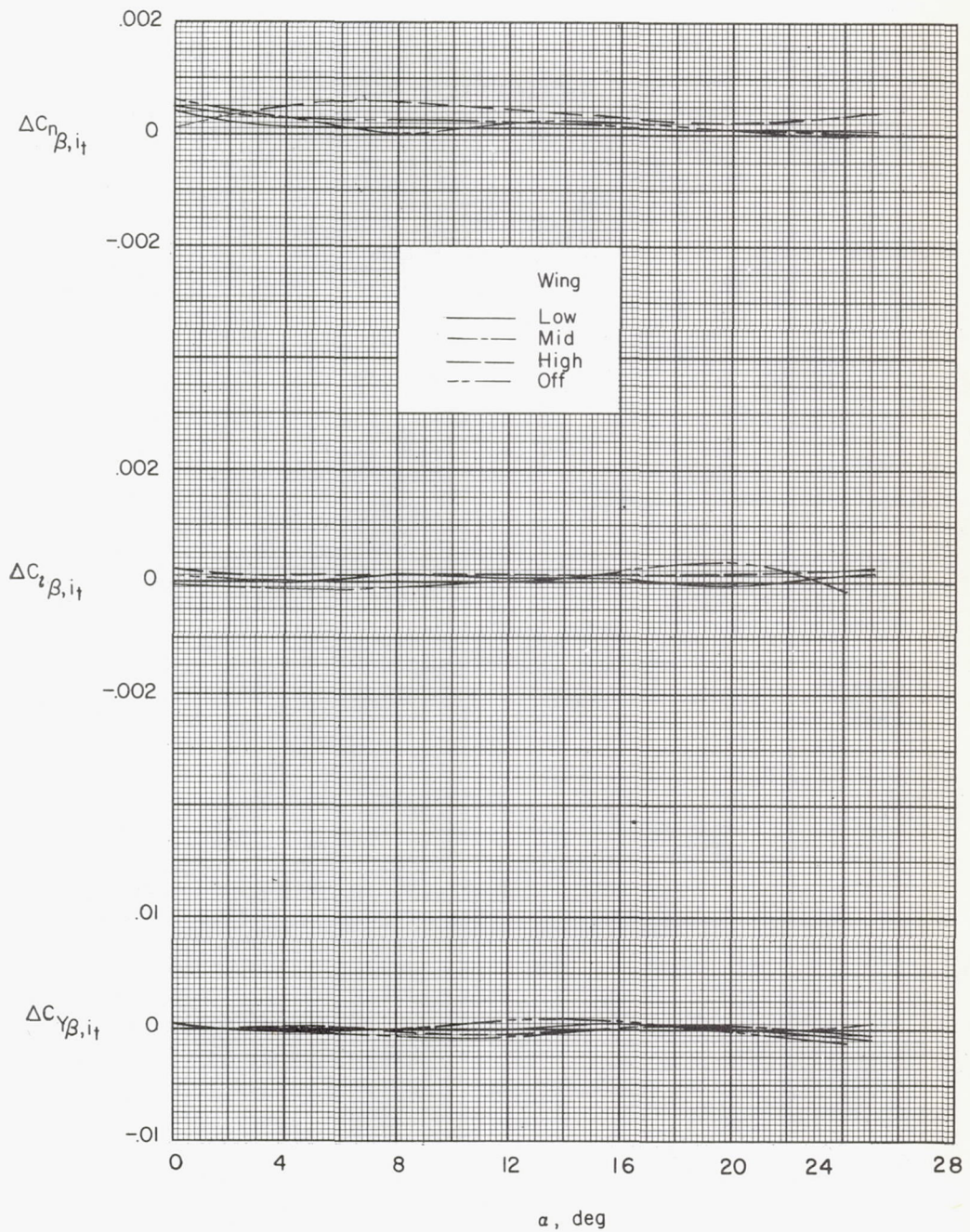
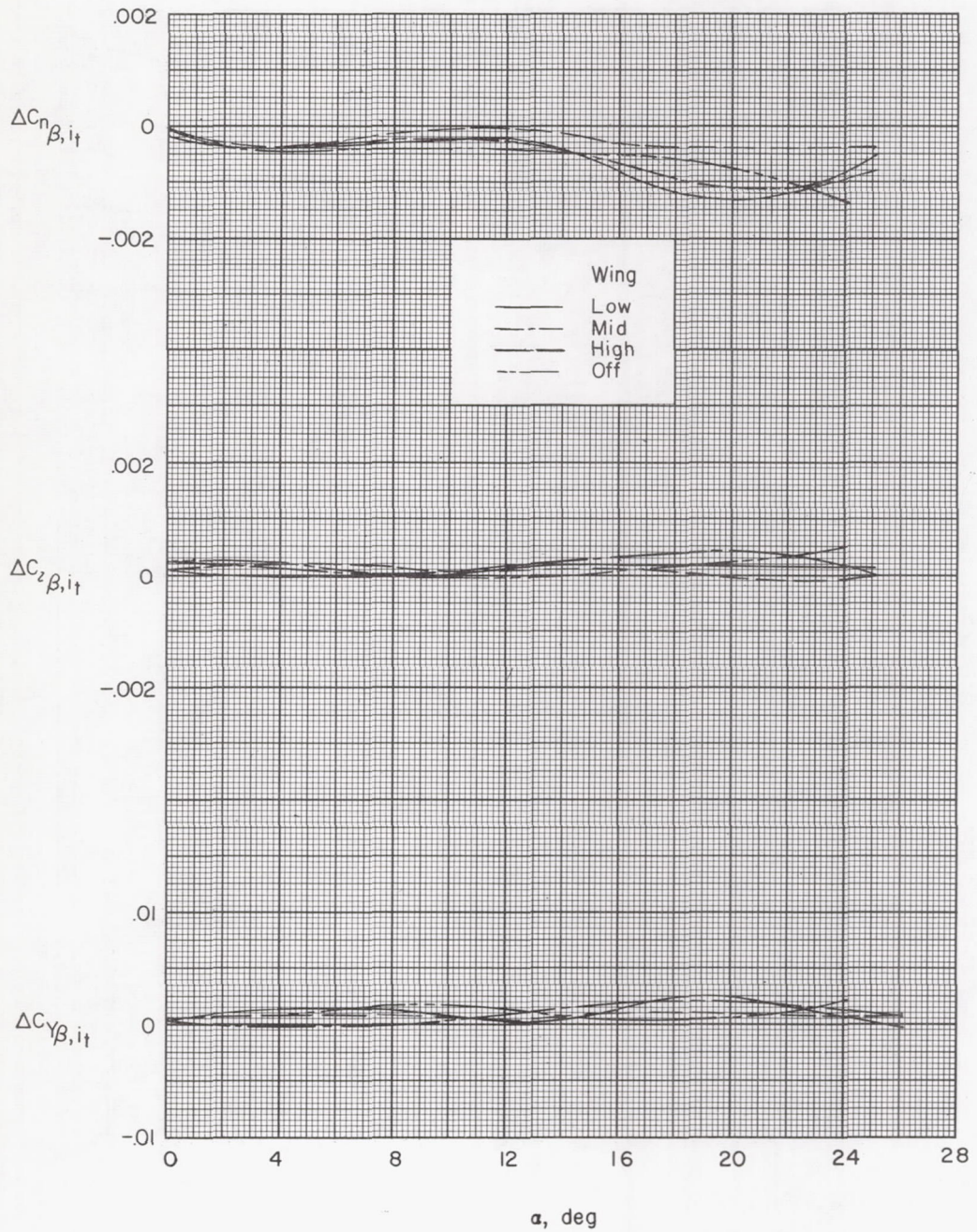
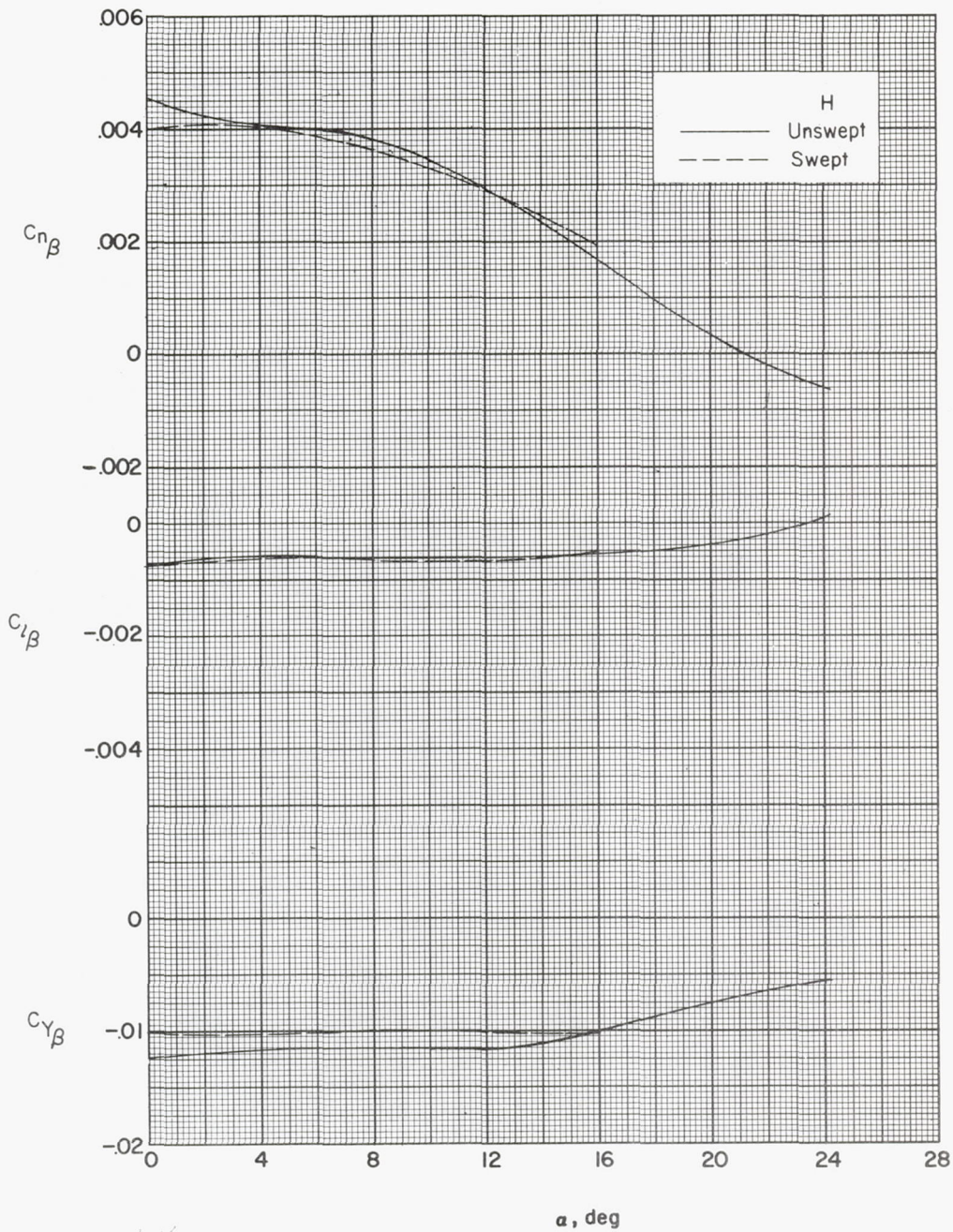
(a) H_L .

Figure 20.- Effect of wing position on the contribution of deflection of the horizontal tail to the sideslip derivatives. Complete model; $M = 2.01$.



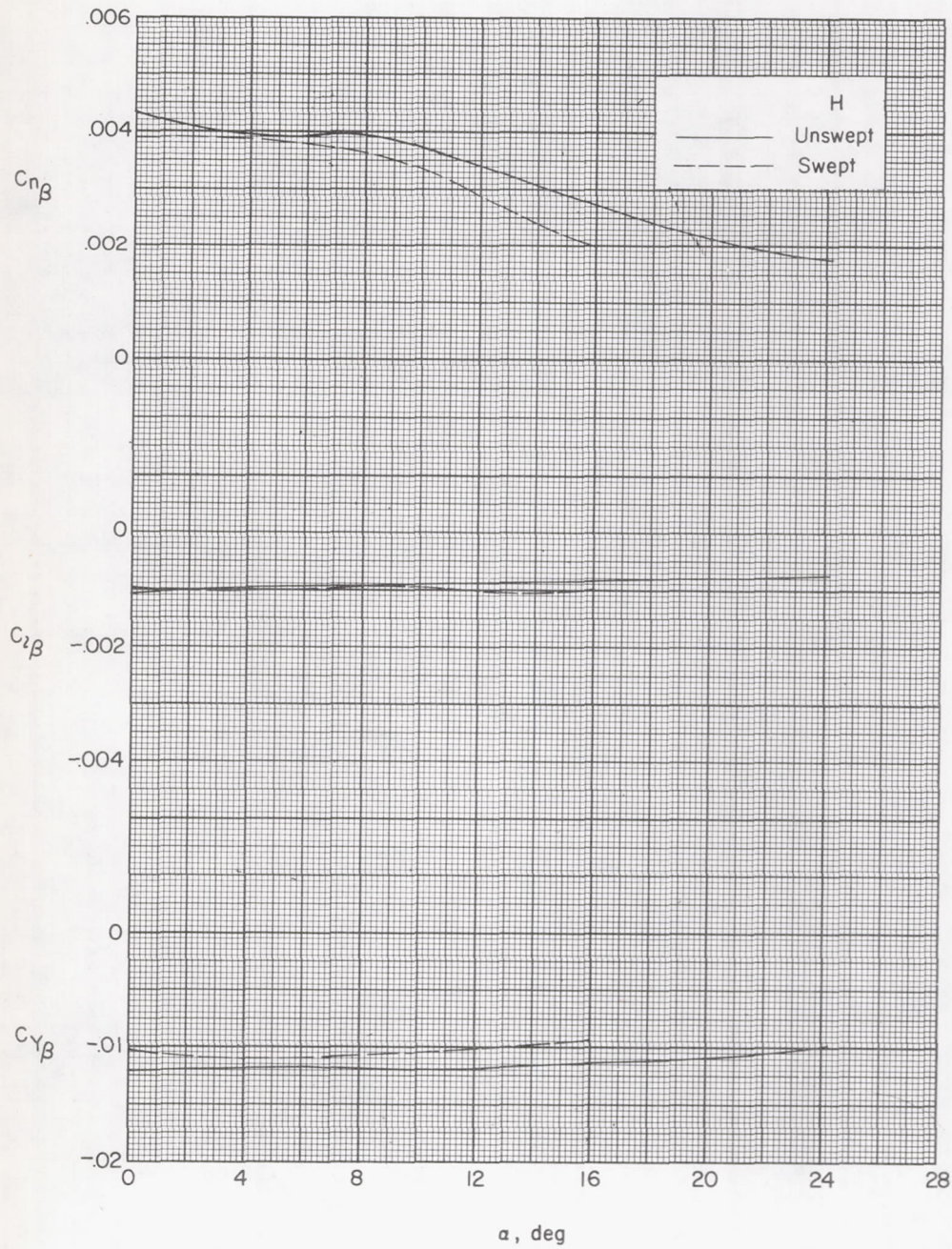
(b) H_H .

Figure 20.- Concluded.



(a) H_L .

Figure 21.- Effect of horizontal-tail plan form on the sideslip derivatives. Wing off; $i_t = 0^\circ$; $M = 2.01$.



(b) H_H .

Figure 21.- Concluded.

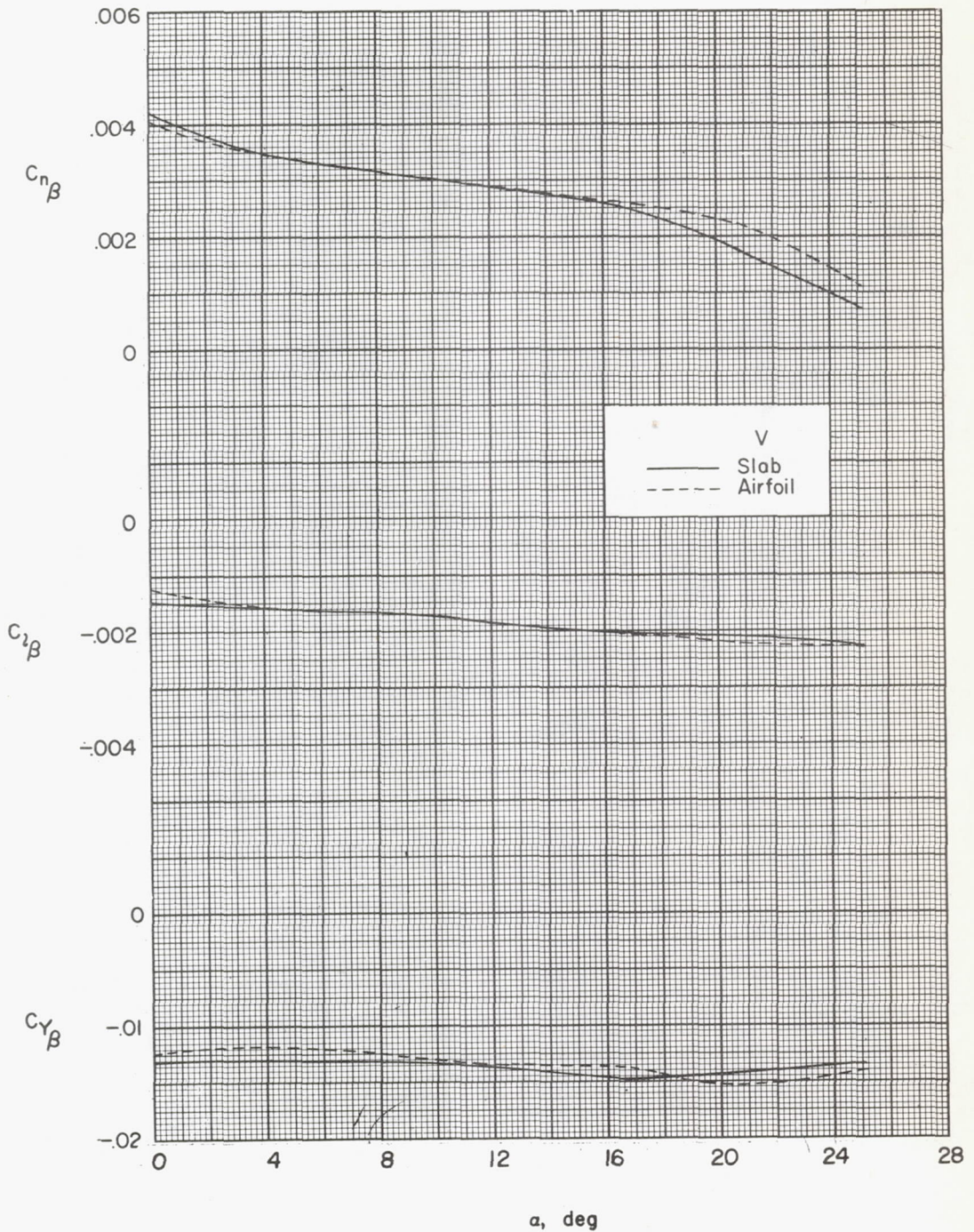


Figure 22.- Effect of vertical-tail airfoil section on the sideslip derivatives. Complete model with high wing and low horizontal tail; $i_t = 0^\circ$; $M = 2.01$.