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NATIONAL ADVISORY COMMITTEE FOR AERONAUTICS

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FLIGHT INVESTIGATION OF NACA D_S COWLINGS ON THE
XP-42 AIRPLANE. IV - HIGH-INLET-VELOCITY COWLING
TESTED IN CLIMB WITH AND WITHOUT PROPELLER CUFFS AND
IN HIGH-SPEED LEVEL FLIGHT WITHOUT PROPELLER CUFFS

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WASHINGTON

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ADVANCE ~~RESTRICTED~~ REPORT

FLIGHT INVESTIGATION OF NACA D_S COWLINGS ON THE
XP-42 AIRPLANE. IV - HIGH-INLET-VELOCITY COWLING
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SUMMARY

Results are presented of flight measurements of the performance and cooling characteristics of a short-nose high-inlet-velocity cowling on the XP-42 airplane for conditions of climb with and without propeller cuffs and for high speed without cuffs. This cowling is one of a series being tested at LMAL.

The airplane speed was approximately 1 mile per hour greater without propeller cuffs than the previously measured value with cuffs. The pressure recovery on the front of the engine averaged 0.74 airplane impact pressure at high speed without cuffs as compared with 0.80 airplane impact pressure with cuffs.

In full-power climb, at 140-miles-per-hour indicated airspeed, the pressure recoveries averaged 0.70 impact pressure with cuffs and 0.60 impact pressure without cuffs.

Oil-in and spark-plug-elbow temperatures were critical in the ground run without cuffs.

INTRODUCTION

The NACA is conducting an extensive flight investigation of several types of cowling for radial aircraft engines. The conditions so far investigated are given as follows:

<u>Test</u>	<u>Type of cowling and flight condition</u>
1	Long-nose high-inlet-velocity cowling with propeller cuffs and small cowl flaps; high speed
2	Long-nose high-inlet-velocity cowling with cuffs and modified cowl flaps; climb
3	Short-nose high-inlet-velocity cowling with cuffs and small cowl flaps; high speed
4	Short-nose low-inlet-velocity cowling with spinner-mounted axial-flow fan, cuff 1, and small cowl flaps; high speed
5	Short-nose low-inlet-velocity cowling with fan, cuff 1 and modified cowl flaps; climb
6	As in test 4, cuff 1 except with modified cowl flaps; high speed
7	As in test 6, but with baffle seal strips at base of cylinders removed; high speed
8	Short-nose low-inlet-velocity cowling with fan only; high speed
9	As in test 8; climb
10	Short-nose low-inlet-velocity cowling without fan or cuffs; climb
11	As in test 10; high speed
12	Short-nose low-inlet-velocity cowling with cuff 1, without fan; high speed
13	As in test 12; climb
14	Short-nose low-inlet-velocity cowling with cuff 2, without fan; climb
15	As in test 14; high speed
16	Short-nose high-inlet-velocity cowling with propeller cuffs; climb
16A	Short-nose high-inlet-velocity cowling without cuffs; climb
16B	Short-nose high-inlet-velocity cowling without cuffs; high speed

Where not otherwise noted, the tests were made with the modified cowl flaps.

The results of tests 1 and 2 are reported in reference 1. The results of test 3 are presented in reference 2; of tests 4 to 7, in reference 3; and of tests 8 to 15, in reference 4.

The present paper covers the results of tests 16, 16A, and 16B. In conjunction with reference 2, it represents a completion of the investigation contemplated for the short-nose (D_S) high-inlet-velocity cowling.

The design of the cowling and engine installation was a project of the Air-Cooled Engine-Installation Group stationed at the Laboratory. The portion of this group associated with this project included Mr. Howard S. Ditsch, of the Curtiss-Wright Corporation, Mr. Peter Torraco, of the Republic Aviation Corporation, Mr. William S. Richards, of the Wright Aeronautical Corporation, and Mr. James R. Thompson, of Pratt & Whitney Aircraft. The Materiel Command, Army Air Forces, sponsored the investigation and supplied the XP-42 airplane. The airplane division of the Curtiss-Wright Corporation handled the construction as well as the structural and detail design of the cowling and supplied personnel to assist in the servicing and maintenance of the airplane and cowling during the tests. Pratt & Whitney Aircraft prepared the engine and torque meter for the tests and assisted in the operation and servicing of the engine. The propeller, cuffs, and spinner were supplied by the propeller division of the Curtiss-Wright Corporation.

This paper was originally issued as a memorandum report for Army Air Forces, Materiel Command.

XP-42 AIRPLANE WITH SHORT-NOSE HIGH-INLET-VELOCITY COWLING

The airplane, engine, and cowling were the same as described in reference 2 except that the cowl skirt had been cut for the addition of extra cowl flaps, of which the position could be changed on the ground only. The airplane with the modified cowl flaps fixed open is shown in figure 1.

TEST APPARATUS AND PROCEDURE

The installation of the test equipment was described in reference 2. The method used for making the climb cooling tests was the same as described in references 3 and 4. For the cowling with cuffs, full-power climbs were made at indicated airspeeds of 155 and 140 miles per hour in automatic rich and at 140 miles per hour in full rich. For the cowling without cuffs, the climbs were limited to one at 155 miles per hour in automatic rich and one at 140 miles per hour in full rich.

The high-speed tests were conducted as described in reference 2 and ground cooling tests, as described in reference 4.

SYMBOLS

bhp brake horsepower

σ density ratio

η propulsive efficiency

S wing area, square feet

C_D drag coefficient

p observed pressure above free-stream static pressure,
inches of water

q_c airplane impact pressure, inches of water

RESULTS

The data obtained during the high-speed runs and during the climbs are presented in tables I and II. In addition, the chief climb-test data are shown in figures 2 and 3 in the form of time histories of the climbs.

It will be noted that all temperature data for the 155-mile-per-hour climb with cuffs (flight 16-1) are missing. Analysis of the data from this flight indicated that cold-junction temperatures had not stabilized and that temperatures were uncertain within a range of about 15° F.

A leak in one of the 12 pressure-selector switches invalidated some of the engine cooling-air pressure data, as indicated by omissions in table I(a).

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DISCUSSION

Maximum Speed

The values of maximum speed and power observed during the full-throttle level runs without cuffs are plotted against density altitude in figure 4. The figure also in-

cludes the parameters $\left(\frac{bhp}{\sigma}\right)^{1/3}$, representative of the effective power, and $52.73 \left(\frac{\eta}{C_{DS}}\right)^{1/3}$, representative of the

airplane cleanliness, as explained in references 1 and 2. The product of these two parameters is the speed of the airplane. The installation having the highest value of the parameter of airplane cleanliness will evidently have the highest speed at a given power and altitude.

It was shown in reference 3 that the installation of the modified cowl flaps in the closed position caused an increase of form drag, resulting in a decrease of approximately two-thirds of 1 percent in the parameter

$52.73 \left(\frac{\eta}{C_{DS}}\right)^{1/3}$. This increase in drag is attributed to

air leakage around the modified flaps and would not be present in a well-designed flap installation. Hence, for comparison with the results of previous tests with the original cowl flaps, it is desirable to increase by two-

thirds of 1 percent the values of speed and $52.73 \left(\frac{\eta}{C_{DS}}\right)^{1/3}$

observed in the present tests. Values corrected in this way are shown by the dashed lines of figure 4. Comparison of the corrected value of the cleanliness factor with that obtained from reference 2 for the cowling with cuffs shows an increase of approximately one-third of 1 percent, or 1 mile per hour, due to removal of the cuffs.

Pressures and Temperatures

The cooling-air pressures on the front of the engine in full-power level flight without cuffs averaged approximately $0.74q_c$ as compared with $0.80q_c$ with cuffs for the same locations of pressure measurement. The distributions of the cooling-air pressures for each case are shown in figure 5. The pressure distributions for the cowling with cuffs are taken from reference 2. It is evident from this figure that the pattern of pressure distribution is the same in either case except for slight dissimilarities behind the engine resulting from the change in cowl flaps.

The distributions of cooling-air pressures for the full-power-climb condition are shown in figure 6, in which the points are taken from individual runs in the 140-mile-per-hour climbs at approximately 16,000 feet. Here, again, there is no apparent change in distribution due to the cuffs.

It is to be noted, particularly, that either with or without cuffs, the pressure recovery on the front of the engine in climb was less than that observed for the high-speed condition. For the runs plotted in figure 6, the pressure recovery was $0.70q_c$ with cuffs and $0.59q_c$ without cuffs. The pressure loss between the survey in the annulus and the front of the engine depends upon the air flow. For this reason, the loss through the annulus, in terms of q_c , is higher in the climb condition. When cuffs are used, this increased pressure loss is usually more than offset by the increased cuff loading at the lower velocity. In the present case, however, although the cuffs caused high pressures in the carburetor and oil-cooler scoops, the pressure increment at the annulus was comparatively small. The boundary layer on the spinner is believed to have blanketed an appreciable part of the narrow annular opening. This condition resulted in an energy absorption from the incoming air and a consequent pressure loss at the inlet. Further pressure losses were introduced by gaps between the spinner and the roots of the cuffs. At the low-pitch angles for climb, the gaps between the spinner and the trailing edges of the cuffs extended almost halfway across the annular opening.

Typical distributions of the cylinder head and barrel temperatures are shown in figure 7 for the high-speed level-flight condition without cuffs and in figures 8 and 9 for the climb condition with and without cuffs. The temperature-distribution patterns are evidently similar and bear little

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apparent relation to the cooling-air pressure-distribution patterns. The engine temperatures observed during these tests are of doubtful significance since the pilot reported rough engine operation at and near full throttle and the power developed, especially during the climbs, was relatively low.

Ground Cooling

Representative temperatures observed during the ground-cooling tests are shown on figure 10 for the run with cuffs and on figure 11 for the run without cuffs. It is apparent that the use of cuffs materially reduces the engine and accessory temperatures. The difference in cooling is probably greater than is indicated since excessive indicated oil-in temperatures caused the operator to throttle back to idling only 5 minutes after the start of the run without cuffs, when cylinder temperatures had not yet stabilized. Under these conditions, only the oil-in temperature exceeded the Army limit, but it is probable that the spark-plug elbow would also have gone over the Army limit after cut-off if the engine had been run at 1400 rpm for the full 10 minutes. Of the six elbows for which temperatures were recorded, the front elbow of cylinder 11 and the rear elbow of cylinder 1 reached the same maximum of 215° F during the run without cuffs. The rear elbow was hottest during the idling period and the front elbow was hottest after cut-off.

Cylinder head and barrel temperatures did not closely approach their limits in either test.

CONCLUSIONS

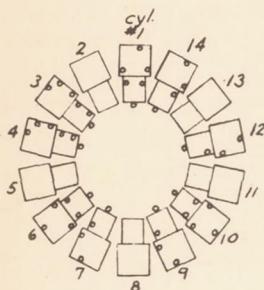
1. The maximum speed of the XP-42 airplane with the short-nose high-inlet-velocity cowling was about 1 mile per hour greater without propeller cuffs than with the cuffs.
2. The cooling-air pressure recoveries on the front of the engine in full-power climb at 140-miles-per-hour indicated airspeed averaged about 70 percent of airplane impact pressure with cuffs and 60 percent without cuffs. The corresponding pressure recoveries in high-speed level flight were 80 percent and 74 percent airplane impact pressure.

REFERENCES

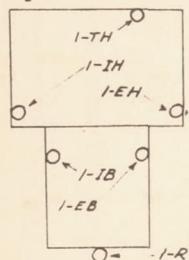
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2. Bailey, F. J., Jr., and Johnston, J. Ford: Flight Investigation of NACA D_S Cowlings on the XP-42 Airplane. I - High-Inlet-Velocity Cowling with Propeller Cuffs Tested in High-Speed Level Flight. NACA A.R.R., Jan. 1943.
3. Johnston, J. Ford, and Voglewede, T. J.: Flight Investigation of NACA D_S Cowlings on the XP-42 Airplane. II - Low-Inlet-Velocity Cowling with Axial-Flow Fan and Propeller Cuffs. NACA A.R.R., Jan. 1943.
4. Johnston, J. Ford, and Voglewede, T. J.: Flight Investigation of NACA D_S Cowlings on the XP-42 Airplane. III - Low-Inlet-Velocity Cowling without Fan or Propeller Cuffs, with Axial-Flow Fan Alone, and with Two Different Sets of Propeller Cuffs. NACA A.R.R., Jan. 1943.

XP-42 Airplane Short-Nose High-Inlet Velocity Cowling	Test No - Flight No. Run No.	16A-1					16A-2				
		1	2	3	4	5	1	2	3	4	5
True Airspeed, mph.	328	331	332	331	327		330	328	327	330	328
q_c , impact pressure, in. H ₂ O	344	33.7	32.8	31.4	29.6		33.5	32.1	30.8	30.1	28.8
Atm. pressure, in. Hg	17.13	16.38	15.69	15.01	14.47		16.38	15.75	15.10	14.47	13.92
Ambient Air Temp., °F	20	17	14	11	8		16	13	10	9	6
σ , density ratio	.619	.596	.574	.555	.536		.597	.578	.557	.535	.518
Density Altitude, st.	15500	16650	17750	18800	19800		16650	17550	18700	19850	20800
R.P.M.						26	80				
Bhp	895	872	840	811	770		862	820	798	770	737
Manifold pressure, in. Hg	40.3	38.9	37.5	36.1	34.6		38.9	37.5	36.0	34.7	33.3
						High Speed - Without Cuffs					

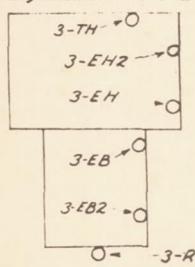
Engine Pressure Tube Locations



Cylinder no. 1



Cylinder no. 3



*Method of designating tube locations
for typical cylinders*

1-R		.29	.29	.29	.28	.27	.28	.28	.28	.29	.28
3-R		.28	.28	.28	.28	.27	.28	.28	.27	.28	.28
4-R		.28	.28	.27	.28	.27	.28	.28	.27	.28	.27
6-R	sheltered	.30	.30	.30	.30	.29	.30	.30	.30	.31	.30
7-R	tubes	.30	.30	.30	.30	.29	.30	.30	.30	.31	.30
9-R	behind	.32	.31	.31	.32	.31	.31	.32	.32	.32	.32
10-R	engine	.32	.31	.31	.32	.31	.31	.32	.32	.32	.32
12-R		.30	.30	.29	.29	.28	.28	.29	.28	.29	.29
14-R		.29	.29	.28	.28	.27	.28	.28	.28	.29	.28
1-EB		.80	.79	.79	.78	.79	.79	.80	.80	.80	.79
3-EB		.62	.61	.61	.61	.60	.62	.62	.62	.62	.62
4-EB	exhaust	.73	.72	.72	.72	.72	.72	.73	.72	.73	.72
6-EB	side	.80	.79	.78	.78	.79	.79	.79	.79	.79	.79
7-EB	of	.72	.72	.72	.72	.72	.72	.73	.72	.73	.72
9-EB	barrel	.80	.79	.79	.79	.79	.80	.80	.79	.80	.79
10-EB		.73	.72	.72	.72	.72	.72	.73	.72	.74	.72
12-EB		.73	.72	.73	.72	.72	.72	.72	.72	.73	.72
14-EB		.71	.71	.72	.71	.71	.71	.71	.71	.71	.70
1-EH		.83	.82	.82	.83	.82	.82	.83	.82	.82	.81
3-EH		.73	.72	.72	.72	.72	.72	.72	.71	.72	.71
4-EH	exhaust	.82	.82	.82	.81	.82	.81	.81	.81	.82	.81
6-EH	side	.73	.72	.72	.72	.72	.71	.71	.72	.73	.71
7-EH	of	.78	.77	.78	.78	.77	.77	.77	.78	.78	.76
9-EH	head	.76	.76	.76	.76	.75	.76	.75	.76	.76	.76
10-EH		.84	.82	.83	.82	.81	.82	.83	.83	.82	.81
12-EH		.80	.79	.79	.79	.78	.78	.79	.78	.79	.78
14-EH		.79	.78	.77	.77	.78	.77	.78	.77	.78	.77
1-TH		.70	.69	.69	.70	.69	.69	.69	.69	.69	.70
3-TH		.71	.71	.70	.71	.71	.70	.70	.70	.71	.70
4-TH		.65	.64	.65	.65	.65	.64	.65	.65	.65	.65
6-TH	top	.66	.65	.65	.66	.66	.65	.66	.65	.66	.66
7-TH	of	.76	.75	.76	.76	.75	.75	.75	.74	.76	.75
9-TH	head										
10-TH											
12-TH											
14-TH											
1-IH	intake side										
6-IH	of head										
10-IH											
1-IB	intake side	.69	.69	.69	.68	.69	.68	.68	.70	.71	.70
6-IB	of barrel	.80	.79	.80	.80	.79	.79	.79	.80	.79	.78
10-IB		.76	.75	.74	.74	.73	.74	.74	.74	.75	.73
3-EH2		.78	.78	.77	.78	.77	.78	.77	.77	.78	.77
4-EH2		.80	.79	.79	.79	.79	.79	.79	.79	.79	.79
3-EB2		.54	.54	.55	.55	.54	.54	.55	.56	.56	.56
4-EB2		.63	.63	.65	.65	.64	.64	.64	.65	.65	.66

Table I(a) (concluded)

	16B-1				16B-2				16-1				16-2				16-3				
	1	2	3	4	1	2	3	4	1	2	3	4	1	2	3	4	1	2	3	4	
Indicated Airspeed mph	158	155	155	154	140	140	138	138	156	156	157	158	143	142	140	140	139	142	138	138	
Pressure Altitude Range ft}	12.3	11.8	11.8	11.6	9.7	9.7	9.4	9.4	12.0	12.0	12.2	12.3	10.0	9.9	9.6	9.7	9.5	9.9	9.4	9.3	
Av. Free Air Temp F	4900	8800	15700	19450	5650	13850	16950	19200	6350	10950	14650	19400	8750	11950	16150	19450	4250	8750	15200	19150	
Av. bhp	5900	9700	16400	20000	9400	14300	17300	19500	7950	11100	15450	19750	9700	12800	16900	19100	5450	9750	15800	19850	
Av. Manifold Pressure R.P.M	49	37	16	3	39	24	13	4	49	37	16	8	61	41	20	7	820	860	770	675	
	820	860	770	675	875	760	665	610	870	890	810	705	830	860	765	710	890	830	740	610	
	39.8	40.0	34.5	30.0	42.3	36.3	32.3	29.5	40.0	39.8	36.1	30.5	38.8	38.7	34.0	31.2	43.0	40.0	35.0	29.5	
	2530	2520	2520	2525	2500	2500	2500	2500	2500	2500	2500	2500	2500	2500	2500	2500	2500	2500	2500	2500	
	Auto Rich Climb	Full Rich Climb	Auto Rich Climb	Full Rich Climb	Without Cuffs	With Cuffs															
Tube designation	pressure ratio, %																				
Sheltered tubes behind engine	1-R	.32	.34	.33	.34	.38	.34	.37	.37	.31	.28	.29	.28	.32	.30	.30	.30	.38	.36	.38	.39
	3-R	.28	.30	.31	.29	.33	.32	.35	.35	.27	.25	.26	.25	.28	.27	.28	.28	.31	.32	.31	.33
	4-R	.29	.31	.33	.31	.35	.34	.37	.37	.29	.27	.27	.27	.27	.28	.27	.27	.34	.34	.33	.33
	6-R	.19	.20	.24	.22	.26	.25	.28	.28	.17	.16	.16	.16	.18	.16	.18	.18	.19	.20	.22	.26
	7-R	.19	.20	.22	.22	.26	.25	.28	.28	.16	.16	.17	.16	.18	.16	.17	.18	.19	.21	.22	.23
	9-R	.20	.22	.24	.22	.26	.25	.28	.28	.20	.19	.18	.18	.22	.21	.21	.21	.26	.25	.26	.26
	10-R	.22	.24	.24	.23	.29	.27	.30	.30	.20	.20	.19	.19	.24	.21	.21	.23	.27	.27	.29	.29
	12-R	.32	.34	.33	.31	.38	.37	.40	.37	.31	.28	.28	.27	.32	.29	.30	.30	.36	.36	.36	.36
	14-R	.32	.34	.33	.31	.38	.37	.37	.37	.31	.29	.29	.28	.32	.30	.30	.29	.36	.36	.36	.39
	1-EH	.74	.75	.71	.71	.75	.69	.67	.64	.82	.81	.78	.78	.77	.78	.77	.77	.80	.75	.78	.73
exhaust side of barrel	3-EB	.38	.36	.37	.36	.36	.35	.34	.34	.34	.48	.46	.45	.48	.48	.48	.47	.52	.42	.44	.41
	4-EB	.61	.59	.58	.60	.62	.58	.55	.55	.65	.62	.62	.62	.68	.66	.67	.72	.65	.66	.63	
	6-EB	.76	.75	.73	.75	.77	.76	.71	.71	.78	.75	.73	.75	.78	.76	.76	.78	.80	.75	.76	.78
	7-EB	.65	.61	.58	.60	.64	.61	.57	.57	.78	.79	.74	.69	.79	.80	.78	.75	.80	.79	.78	.76
	9-EB	.80	.78	.75	.75	.77	.78	.74	.74	.73	.76	.74	.73	.78	.78	.84	.76	.76	.73	.73	.73
	10-EB	.61	.59	.58	.60	.62	.63	.57	.57	.67	.69	.67	.63	.73	.73	.75	.72	.71	.69	.66	.68
	12-EB	.62	.60	.58	.62	.58	.57	.53	.53	.73	.72	.69	.66	.82	.84	.76	.73	.85	.73	.76	.66
	14-EB	.65	.62	.60	.62	.64	.63	.58	.58	.72	.69	.71	.65	.72	.76	.74	.72	.80	.67	.72	.67
	1-EH	.74	.73	.71	.72	.69	.65	.63	.68	.85	.77	.80	.78	.72	.74	.74	.74	.78	.70	.74	.72
	3-EH	.60	.56	.53	.56	.60	.57	.53	.51	.73	.68	.68	.64	.70	.72	.68	.69	.76	.71	.68	.62
exhaust side of head	4-EH	.77	.75	.73	.75	.78	.74	.70	.70	.84	.84	.79	.80	.85	.86	.83	.90	.85	.83	.83	.83
	6-EH	.63	.64	.58	.62	.62	.59	.59	.58	.73	.72	.68	.66	.68	.68	.66	.63	.70	.65	.66	.64
	7-EH	.74	.73	.68	.69	.73	.70	.65	.68	.83	.80	.78	.77	.82	.83	.79	.83	.82	.78	.77	
	9-EH	.70	.70	.69	.68	.70	.69	.64	.64	.66	.67	.68	.68	.68	.72	.73	.69	.71	.64	.69	.63
	10-EH	.80	.80	.75	.78	.81	.80	.76	.73	.95	.91	.90	.86	.93	.88	.96	.91	.105	.94	.96	.92
	12-EH	.72	.70	.69	.70	.68	.66	.64	.66	.102	.96	.90	.83	.116	.113	.109	.105	.124	.107	.105	.100
	14-EH	.80	.75	.74	.76	.84	.82	.81	.73	.86	.87	.84	.80	.92	.92	.91	.89	.97	.89	.85	.80
	1-TH	.57	.55	.53	.55	.55	.56	.52	.52	.62	.59	.62	.59	.73	.63	.58	.62	.69	.62	.60	.60
	3-TH	.61	.57	.55	.57	.59	.58	.55	.52	.64	.63	.60	.59	.62	.62	.66	.64	.67	.64	.63	.63
	4-TH	.48	.46	.44	.47	.47	.44	.46	.46	.53	.53	.52	.50	.53	.56	.52	.53	.52	.51	.51	
top of head	6-TH	.50	.48	.46	.49	.45	.44	.46	.46	.53	.54	.51	.50	.51	.54	.56	.53	.52	.49	.49	.49
	7-TH	.72	.70	.66	.68	.70	.66	.62	.64	.77	.74	.74	.73	.74	.74	.73	.73	.78	.76	.70	.72
	9-TH									.78	.77	.78	.75	.82	.80	.83	.82				
	10-TH									.58	.54	.59	.56	.57	.60	.62	.58				
	12-TH									.59	.58	.62	.58	.68	.66	.66	.65				
	14-TH									.52	.53	.55	.50	.62	.62	.59	.57				
	1-IH									.80	.82	.81	.78	.87	.88	.90	.88				
intake side of head	6-IH									.82	.80	.86	.81	.83	.85	.88	.84				
	10-IH									.93	.92	.94	.90	.101	.98	.92	.96				
	1-ID	.58	.59	.54	.56	.62	.61	.58	.54	.70	.69	.70	.68	.75	.76	.74	.73	.74	.65	.70	.64
	6-ID	.79	.78	.76	.77	.79	.78	.74	.77	.83	.80	.80	.78	.80	.85	.83	.80	.91	.77	.85	.81
intake side of barrel	10-ID	.62	.59	.58	.61	.60	.59	.52	.56	.76	.72	.73	.71	.80	.80	.78	.76	.83	.72	.74	.72
	3-EH2	.69	.67	.64	.66	.64	.65	.61	.61	.74	.69	.41	.68	.70	.72	.72	.76	.70	.71	.71	
	4-EH2	.69	.67	.65	.66	.69	.63	.63	.61	.77	.75	.76	.72	.77	.79	.78	.75	.78	.74	.76	.73
	3-EB2	.38	.37	.35	.37	.27	.28	.24	.24	.34	.34	.34	.34	.32	.37	.37	.35	.37	.39	.31	.31
	4-EB2	.52	.50	.48	.52	.53	.50	.49	.51	.47	.45	.48	.49	.52	.52	.53	.52	.50	.49	.50	.51

Table I(b) - Pressure Data

XP-42 Airplane Short-Nose High-Inlet- Velocity Cowling	Test No - Flight No. Run No.	16A-1					16A-2				
		1	2	3	4	5	1	2	3	4	5
True Airspeed, mph		328	331	332	331	327	330	328	327	330	328
q_c , impact press., in. H ₂ O		34.4	33.7	32.8	31.4	29.6	33.5	32.1	30.8	30.1	28.8
Atm Pressure, in H ₂ O		17.13	16.38	15.69	15.07	14.47	16.38	15.75	15.10	14.47	13.92
Ambient Air Temp. °F		20	17	14	11	8	16	13	10	9	6
σ , density ratio		.619	.596	.574	.555	.536	.597	.578	.557	.535	.518
Density Altitude, ft.		15500	16650	17750	18800	19800	16650	17750	18800	19800	20800
R.P.M.						26.80					
Bhp.		895	872	840	811	770	862	820	798	770	737
Manifold Press., in. Hg.		40.3	38.9	37.5	36.1	34.6	38.9	37.5	36.0	34.7	33.3
		High Speed					Without Cuffs				

PRESSURE RATIO, P/P ₀											
<i>Location of Pressure Tubes in Annulus</i>											
<i>Oil Cooler Pressure Tube Locations</i>											
<i>CARBURETOR SCOOP</i>											
<i>Impact tubes</i>											
<i>Static tubes</i>											
<i>Impact pressure in carb throat</i>											

Table II(b) (concluded)

Test No.-Flight No. Run No.	16B-1				16B-2				16-1				16-2				16-3				
	1	2	3	4	1	2	3	4	1	2	3	4	1	2	3	4	1	2	3	4	
Indicated Airspeed, mph.	158	155	155	154	140	140	138	138	156	156	157	158	143	142	140	140	139	142	138	138	
qc	12.3	11.8	11.8	11.6	9.7	9.7	9.4	9.4	12.0	12.0	12.2	12.3	10.0	9.9	9.6	9.7	9.5	9.9	9.4	9.3	
Pressure Altitude Range, ft.	4900-8800-15700-19450	8650-13850-18450-19200			6250-10950-14450-19400	8750-11950-16150-19450			7950-11950-15450-19750	9700-12800-16900-19100			4250-8750-15200-19150								
Average Free Air Temp, °F.	5900 9700 16400 20000	9400 14300 17300 19500			7950 11950 15450 19750	9700 12800 16900 19100			39 27 16 8	61 41 20 7			5450 9750 15800 19850								
Average bhp	820	860	770	675	875	760	665	610	870	890	810	705	830	860	765	710	890	830	740	610	
Average Manifold Press. R. P. M.	39.8	40.0	34.5	30.0	42.3	36.3	32.3	29.5	40.0	39.8	36.1	30.5	38.8	38.7	34.0	31.2	43.0	40.0	35.0	29.5	
	25 30				25 20				25 25				25 00								
	Auto Rich Climb	Full Rich Climb				Auto Rich Climb				With Cuffs				Full Rich Climb							
	Without Cuffs																				
Tube designation	pressure ratio, $\frac{P_{turbine}}{P_{atmosphere}}$																				
Top Survey	A-TPI	.85	.85	.81	.84	.86	.82	.78	.78	.92	.92	.90	.87	.88	.91	.90	.88	.92	.91	.91	.88
	2	.94	.97	.91	.90	.93	.89	.87	.87	1.05	1.01	1.02	1.00	.99	1.02	1.01	1.01	1.12	1.00	1.03	.99
	3	.93	.91	.89	.90	.94	.93	.88	.88	1.01	.98	.94	.94	.98	.98	.97	.98	1.09	.99	.98	1.00
	4	.89	.86	.83	.84	.87	.86	.81	.81	.93	.91	.89	.88	.90	.92	.93	.91	.92	.90	.90	.89
	5	.61	.59	.58	.58	.60	.59	.56	.56	.62	.60	.62	.60	.58	.60	.62	.60	.61	.54	.56	.58
Right Survey	A-T51	.42	.42	.40	.43	.42	.43	.43	.40	.49	.52	.50	.49	.52	.55	.54	.53	.55	.50	.47	.48
	2	.35	.34	.34	.37	.34	.37	.34	.34	.40	.40	.43	.41	.41	.42	.45	.43	.37	.39	.39	.39
	3	.43	.46	.44	.47	.45	.46	.44	.44	.54	.53	.50	.53	.57	.56	.54	.54	.60	.53	.53	.53
	A-RPI	.72	.70	.66	.68	.72	.66	.64	.66	.84	.80	.76	.74	.79	.77	.73	.73	.92	.80	.84	.74
	2	.91	.88	.86	.87	.90	.87	.83	.85	1.07	.98	1.00	.94	1.00	.97	.97	.96	1.13	.98	1.03	.99
Left Survey	A-R51	.97	.92	.91	.90	.96	.95	.88	.90	1.10	1.10	1.02	.97	1.08	1.03	1.04	.98	1.14	1.10	1.06	1.09
	2	.94	.95	.92	.93	1.00	.95	.90	.90	.94	1.06	1.03	1.01	1.07	1.08	1.05	1.01	1.14	1.07	1.07	1.03
	3	.79	.75	.73	.75	.77	.74	.72	.72	.86	.85	.85	.82	.87	.87	.87	.83	.95	.79	.83	.81
	4	.44	.42	.40	.43	.40	.41	.40	.38	.41	.39	.41	.41	.37	.39	.40	.40	.36	.33	.34	.36
	5	.46	.45	.43	.45	.42	.45	.43	.43	.44	.41	.43	.43	.40	.41	.44	.42	.35	.35	.37	.39
Oil Cooler	A-LPI	.76	.79	.74	.76	.76	.80	.78	.76	.75	.79	.81	.79	.82	.1.02	.85	.1.01	.82	.76	.82	.77
	2	.94	.92	.91	.93	.97	.96	.95	.99	.96	.96	.93	.92	.96	.95	.93	.93	.98	.98	.93	.94
	3	1.02	1.02	.98	.97	1.02	1.03	1.00	.98	1.01	1.04	1.02	1.00	1.02	1.04	1.07	1.02	1.08	1.04	1.04	1.05
	4	1.00	1.02	.96	.97	1.02	1.01	.98	.96	1.01	1.01	1.02	1.01	1.04	1.08	1.08	1.04	1.12	1.00	1.03	1.00
	5	.79	.76	.76	.78	.77	.78	.77	.72	.87	.85	.82	.82	.86	.85	.83	.82	.90	.95	.81	.81
Rear	A-L51	.51	.48	.49	.50	.50	.47	.47	.45	.58	.56	.54	.55	.57	.57	.58	.57	.46	.54	.55	.55
	2	.47	.47	.43	.47	.44	.45	.34	.43	.56	.54	.54	.54	.56	.58	.58	.56	.46	.52	.50	.53
	3	.43	.42	.41	.44	.39	.40	.39	.39	.49	.51	.52	.53	.46	.49	.51	.48	.48	.49	.49	.47
	O-FPI	.84	.86	.83	.87	.85	.81	.79	.79	1.12	1.17	1.14	1.10	1.25	1.28	1.23	1.16	1.26	1.18	1.18	1.08
	2	.87	.88	.86	.89	.85	.86	.82	.82	1.17	1.21	1.18	1.12	1.28	1.34	1.30	1.22	1.35	1.20	1.23	1.15
Carburetor Scoop	O-FSI	.87	.88	.86	.89	.87	.86	.84	.84	1.19	1.21	1.18	1.12	1.28	1.32	1.27	1.19	1.40	1.22	1.21	1.17
	2	.67	.65	.65	.69	.65	.63	.61	.61	.95	.98	.98	.92	1.02	1.03	1.05	.97	1.01	.97	.95	
	3	.70	.70	.70	.72	.69	.70	.68	.68	.94	.97	.98	.93	1.02	1.04	1.04	.99	1.05	1.00	.99	.96
	O-AP1	.28	.29	.27	.28	.27	.26	.24	.24	.50	.46	.45	.41	.50	.49	.48	.47	.53	.46	.45	.41
	2	.21	.20	.20	.22	.21	.20	.18	.18	.33	.34	.33	.29	.35	.37	.38	.33	.35	.35	.32	.32
	O-SP	.18	.18	.16	.19	.16	.16	.13	.13	.32	.34	.33	.27	.37	.39	.38	.35	.35	.33	.32	.30
	C-P1	.98	.95	.93	.96	.91	.92	.89	.89	1.23	1.17	1.17	1.17	1.14	1.17	1.16	1.11	1.23	1.17	1.11	1.08
	2	.98	.98	.97	.97	.95	.94	.93	.93	1.25	1.21	1.21	1.21	1.19	1.22	1.17	1.15	1.30	1.19	1.19	1.10
	3	.98	.98	.97	.97	.91	.96	.93	.93	1.28	1.21	1.21	1.21	1.22	1.25	1.22	1.19	1.37	1.19	1.20	1.13
	4	.98	.98	.99	.99	.95	.96	.95	.93	1.31	1.21	1.21	1.21	1.22	1.25	1.23	1.20	1.40	1.19	1.20	1.14
	5	.98	.95	.97	.97	.95	.96	.93	.95	1.29	1.21	1.21	1.21	1.25	1.25	1.23	1.21	1.39	1.19	1.18	1.14
	C-S1	.67	.61	.61	.67	.45	.46	.48	.48	.94	.80	.80	.80	.78	.75	.76	.75	.91	.76	.73	.71
	2	.63	.55	.58	.61	.38	.42	.44	.46	.87	.74	.74	.74	.71	.68	.71	.72	.83	.55	.67	.66
	3	.60	.51	.53	.59	.35	.38	.40	.45	.88	.73	.73	.73	.66	.64	.65	.66	.76	.68	.60	.64
	4	.60	.49	.51	.59	.35	.36	.37	.40	.85	.73	.73	.73	.70	.60	.65	.64	.74	.68	.60	.62
	5																				
	C-TH	.67	.59	.58	.67	.41	.44	.44	.48	.93	.81	.80	.78	.79	.73	.73	.73	.88	.77	.70	.68

Table II - Temperature Data

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1
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XP-42 Airplane Short-Nose-High-Inlet Velocity Cowling	Test No. - Flight No. Run No.	16A-1					16A-2				
		1	2	3	4	5	1	2	3	4	5
True Airspeed, mph.		328	331	332	331	327	330	328	327	330	328
q_c , impact press., in. H ₂ O		34.4	33.7	32.8	31.4	29.6	33.5	32.1	30.8	30.1	28.8
Atm. Pressure, in Hg.		17.13	16.38	15.69	15.07	14.47	16.38	15.75	15.10	14.47	13.92
Ambient Air Temp. °F		20	17	14	11	8	16	13	10	9	6
σ , density ratio		.619	.596	.574	.555	.536	.597	.578	.557	.535	.518
Density Altitude, ft.		15500	16650	17750	18800	19800	1650	17550	18700	19850	20800
R.P.M.							2	6	8	0	
Bhp		895	872	840	811	770	862	820	798	770	737
Manifold Press., in. Hg.		40.3	38.9	37.5	36.1	34.6	38.9	37.5	36.0	34.7	33.3
							High Speed				
							Without Cuffs				
Cylinder No. - Point of Measurement		Temperature °F									
1 - gasket thermocouple at rear spark plug		356	356	361	367	378	376	373	378	382	393
2 -		359	359	367	372	385	382	384	386	391	400
3 -		367	367	372	374	387	384	384	389	391	400
4 -											
5 -		384	385	389	391	400	400	402	402	404	411
6 -		356	359	363	365	369	369	371	373	376	382
7 -		387	396	393	393	398	404	402	404	404	411
8 -		374	369	374	376	383	386	386	389	391	398
9 -		372	376	378	380	387	386	386	389	393	400
10 -		391	391	398	400	407	395	404	406	409	415
11 -		383	383	387	395	404	391	395	395	398	411
12 -		376	380	383	389	398	391	395	395	400	406
13 -		383	387	390	396	405	396	399	402	405	415
14 -		378	383	384	391	402	398	400	402	404	411
1 - rear & flange at base of cylinder.											
2 -		288	288	288	291	295	297	297	297	299	301
3 -		284	282	286	286	291	292	292	292	294	297
4 -		273	273	275	275	277	279	281	281	281	283
5 -		288	288	288	291	295	292	294	294	297	299
6 -											
7 -		280	284	288	288	293	290	292	290	294	294
8 -		295	293	295	297	299	299	299	299	301	305
9 -		302	302	304	304	308	305	308	308	310	312
10 -		282	282	282	286	291	283	288	286	290	292
11 -		299	299	302	304	308	303	308	308	310	312
12 -		286	286	288	293	297	290	294	294	297	299
13 -		297	297	299	302	306	303	305	305	308	310
14 -											
10 - intake port		213	213	213	213	215	216	219	214	219	219
Mixture at blower rim		155	151	153	150	150	160	156	155	156	156
Fuel on suction side of pump		74	75	78	78	84	78	81	81	84	91
" " pressure " " "		77	78	81	84	87	84	84	84	84	94
" in carburetor float chamber											
11 - front spark plug elbow		46	42	42	36	36	41	41	38	37	31
11 - rear " " "		93	91	90	90	90	94	94	91	91	91
Recorded free air		38	35	32	29	26	34	31	28	27	24
Air in carburetor scoop		39	38	36	32	29	37	34	31	31	27
" at top annular take		43	42	39	36	36	41	41	35	34	31
" in front of cylinder #1		158	160	163	163	172	163	165	168	172	178
" behind cyl #1		68	65	61	58	58	64	64	61	61	61
" at exit of oil cooler											
Oil-in line		133	135	135	132	135	137	133	133	137	133
Oil out		203	201	203	203	203	208	207	206	207	207
Accessory compartment		105	107	106	103	106	108	107	107	107	107
Lest magneto		96	97	97	97	97	101	104	100	101	98
Pilot's cockpit		68	75	78	75	71	71	74	74	74	78
Recording instrument compartment		68	71	71	68	68	68	71	71	71	71

Table II (concluded)

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Figure 1.- XP-42 airplane with short-nose high-inlet-velocity cowling.

Fig. 1

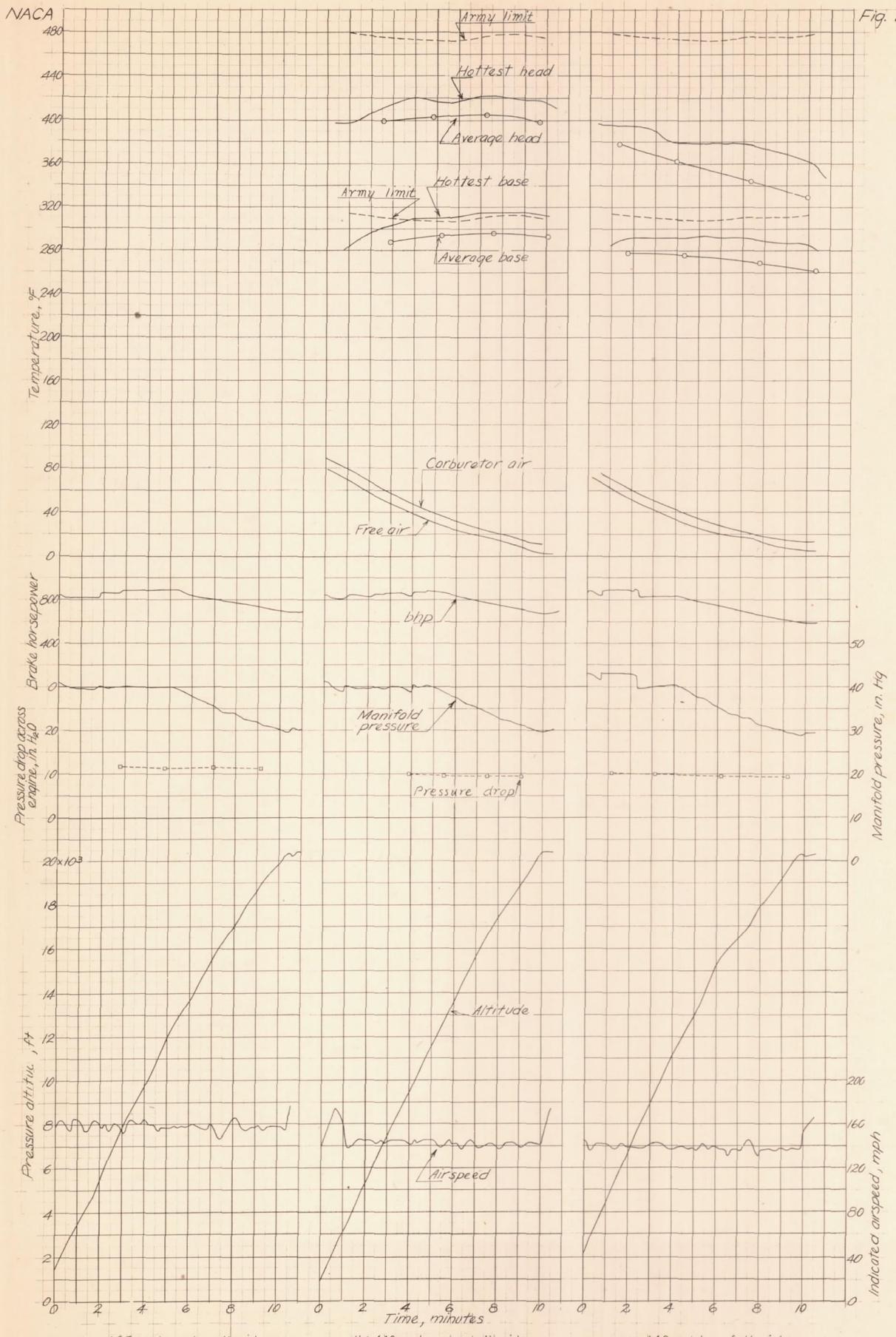


Figure 2 - Time histories of climbs. Test 16 (with cuffs).

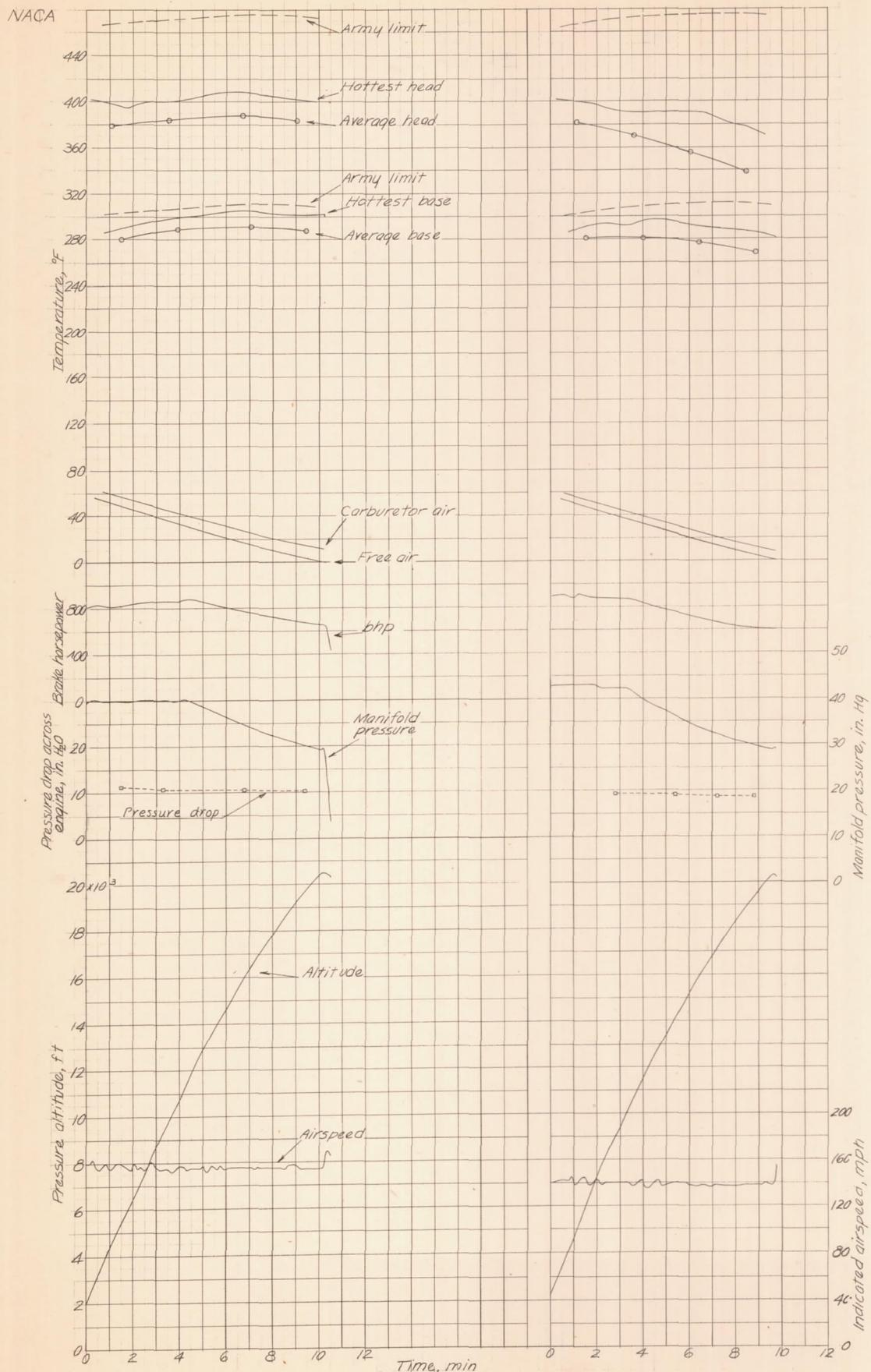


Fig. 3

(a) 155 mph, automatic rich
 (b) 140 mph, full rich

Figure 3-Time histories of climbs. Test 16B (without cuts).

NACA

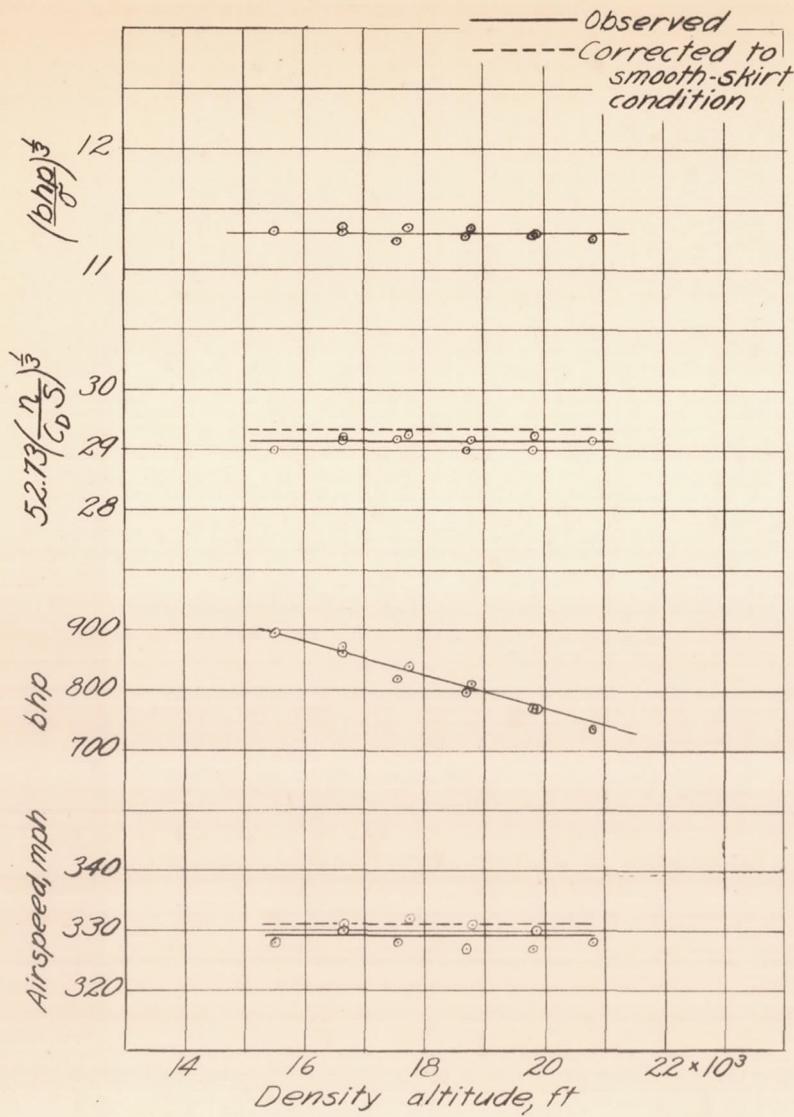


Figure 4. - High-speed performance without cuffs.

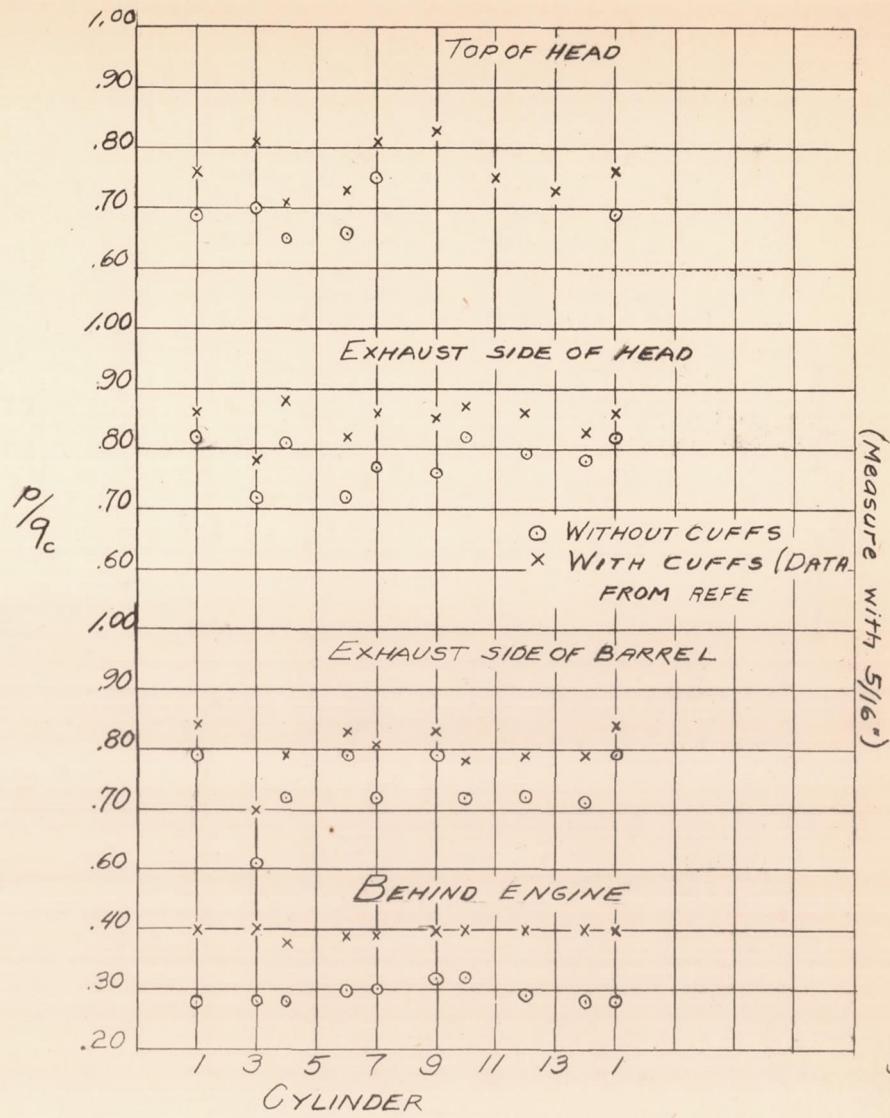


Figure 5. - Engine cooling-air pressure distributions at high speed.

Figs. 4, 5



Figure 6. - Engine cooling-air pressure distributions in full-power climb at 140 miles per hour.

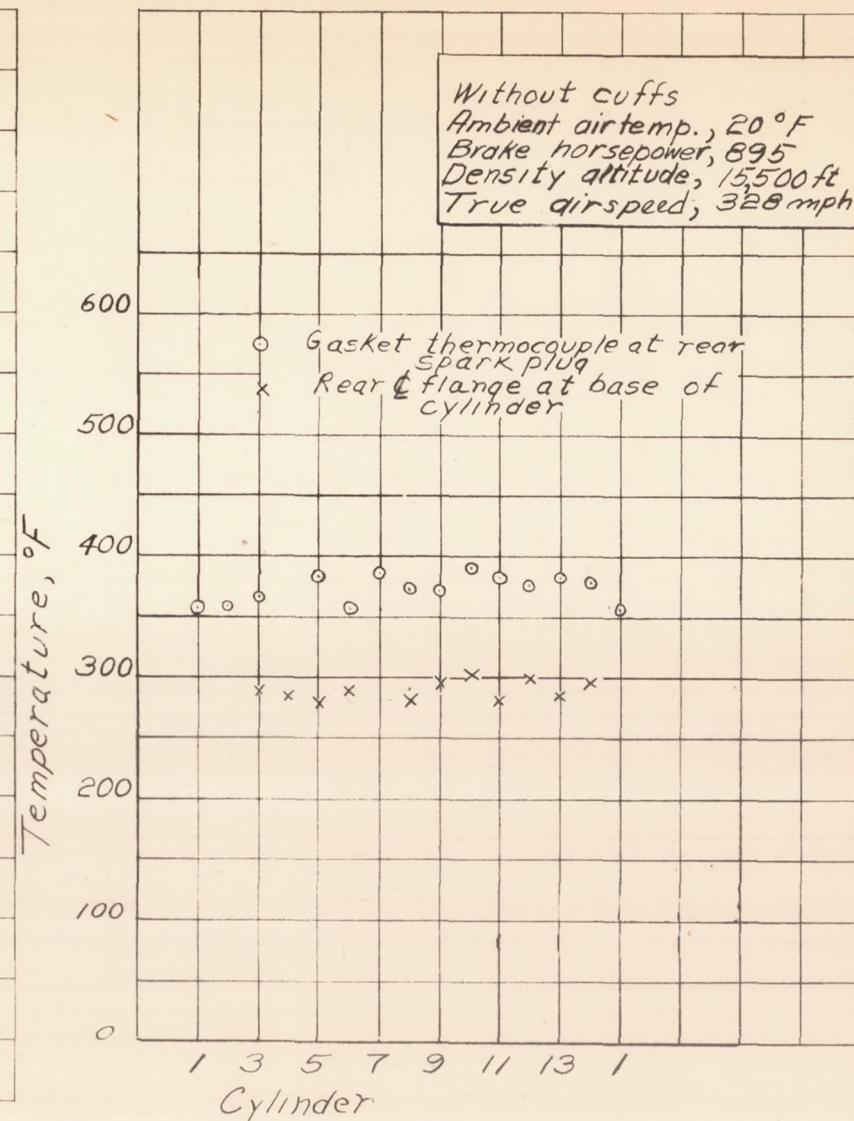


Figure 7. - Observed cylinder-temperature distribution at high speed without cuffs.
(Measure with $5/16$ "')

Figs. 6,7

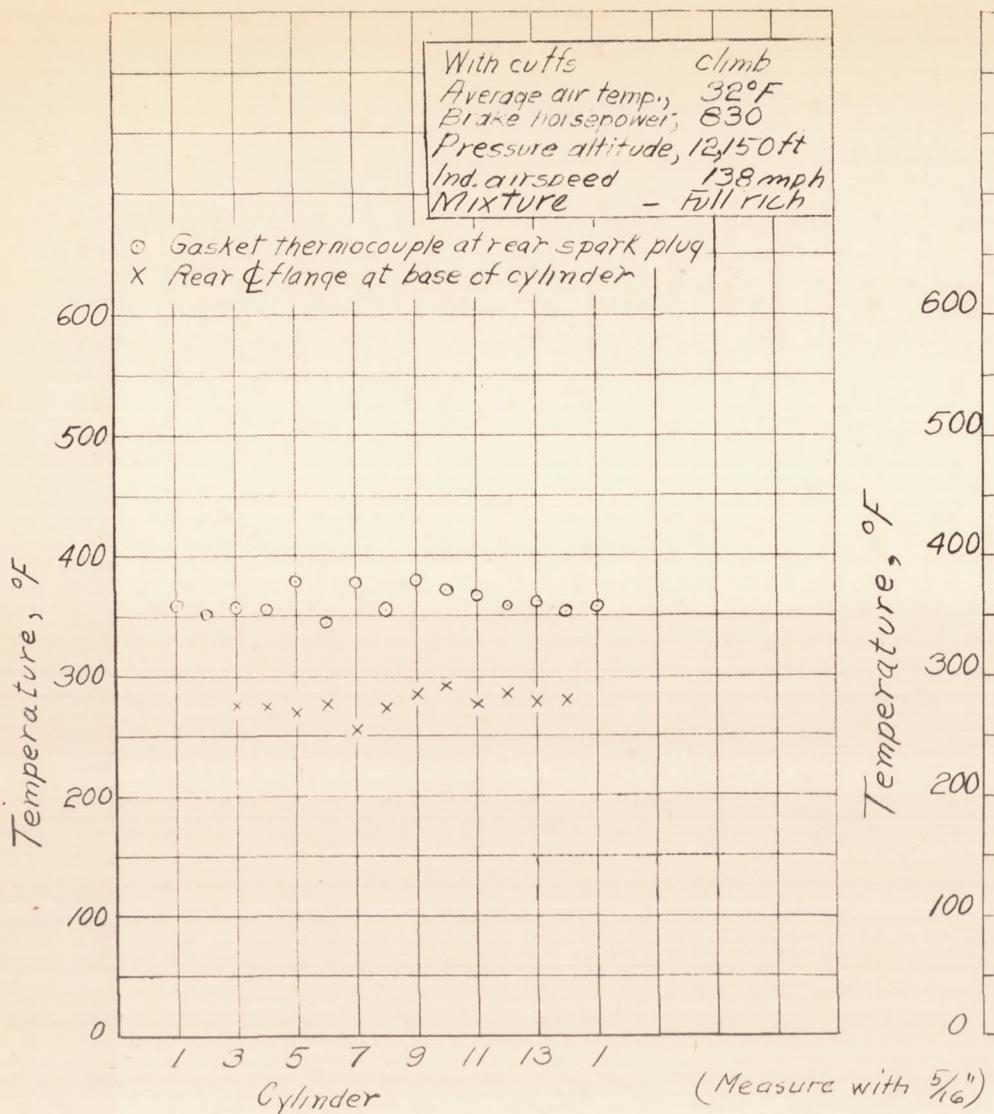


Figure 8. - Cylinder-temperature distribution in climb with cuffs.

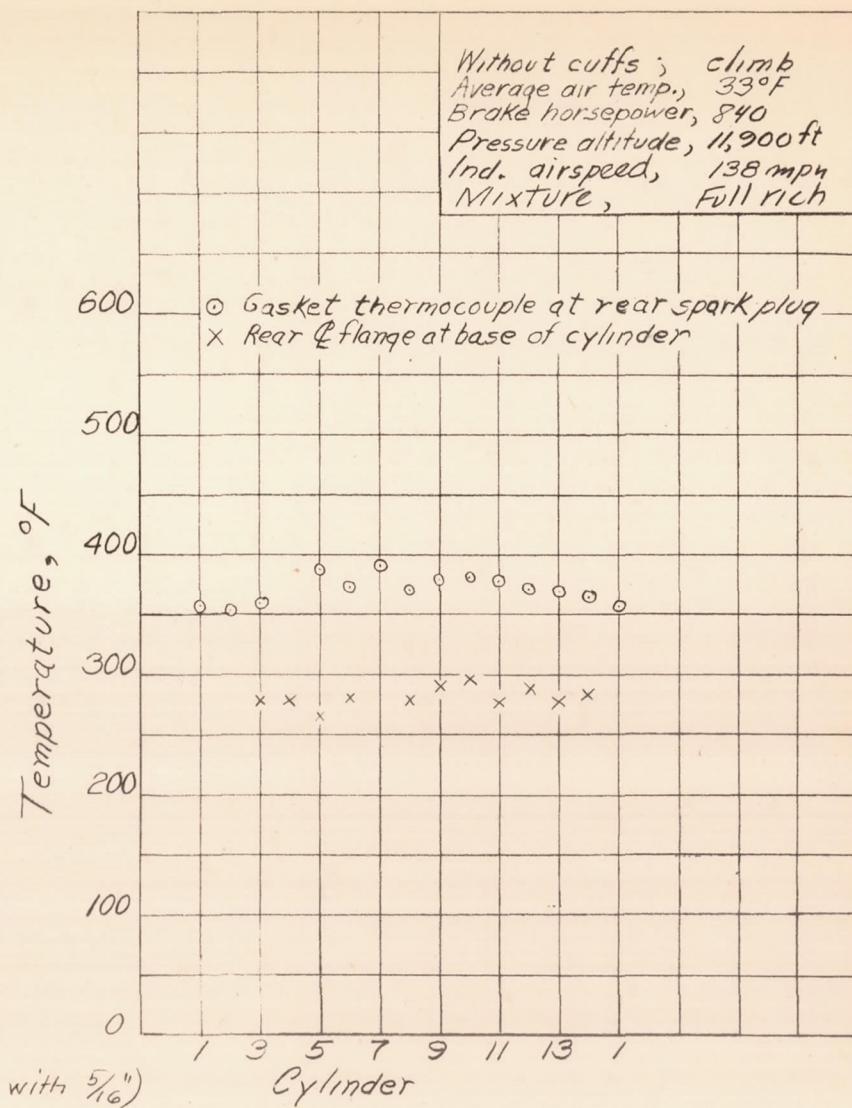


Figure 9. - Cylinder temperature distribution in climb without cuffs.

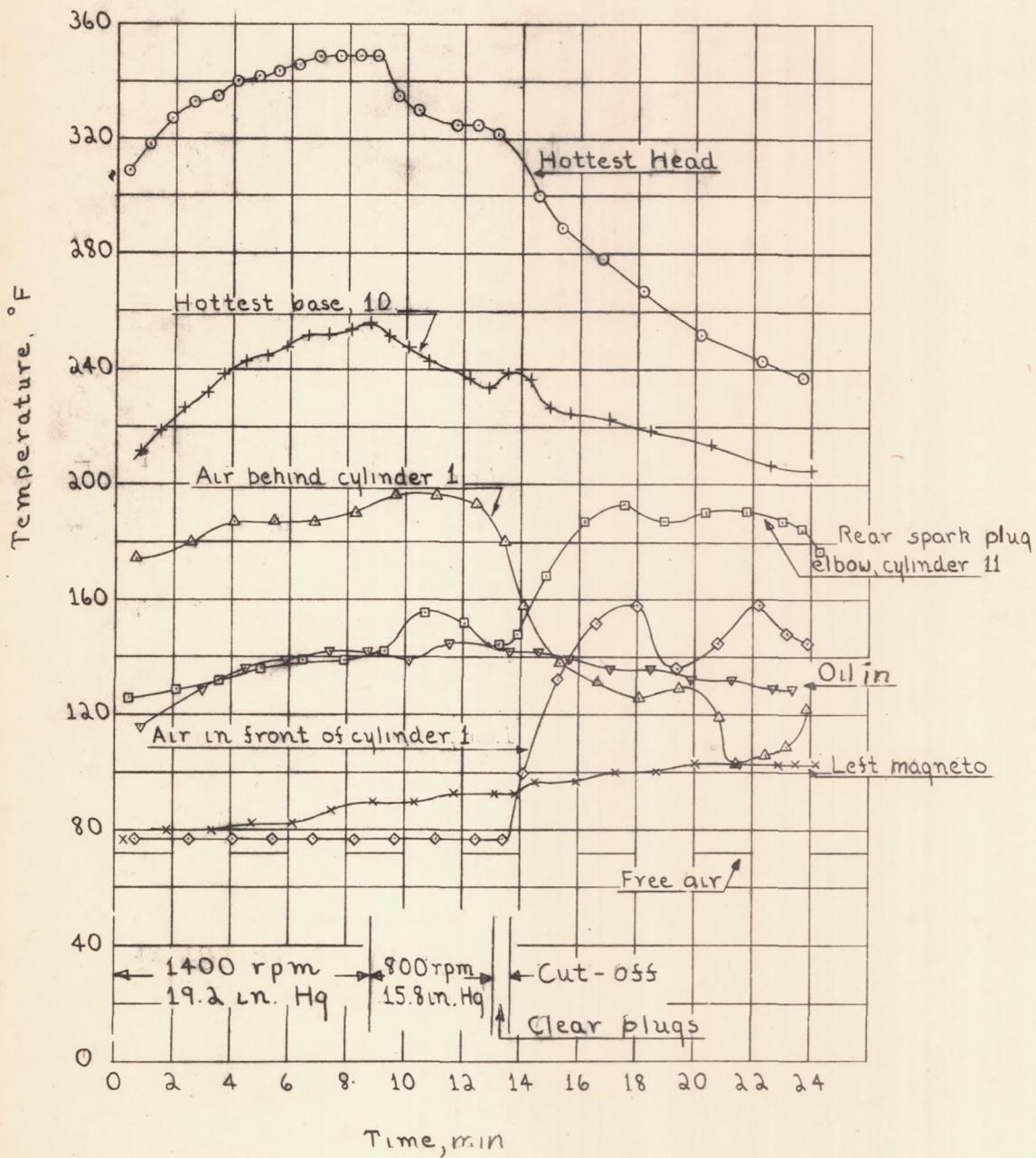
(Measure with $\frac{1}{30}$ "")

Figure 10.- Temperatures in ground run with cuffs.

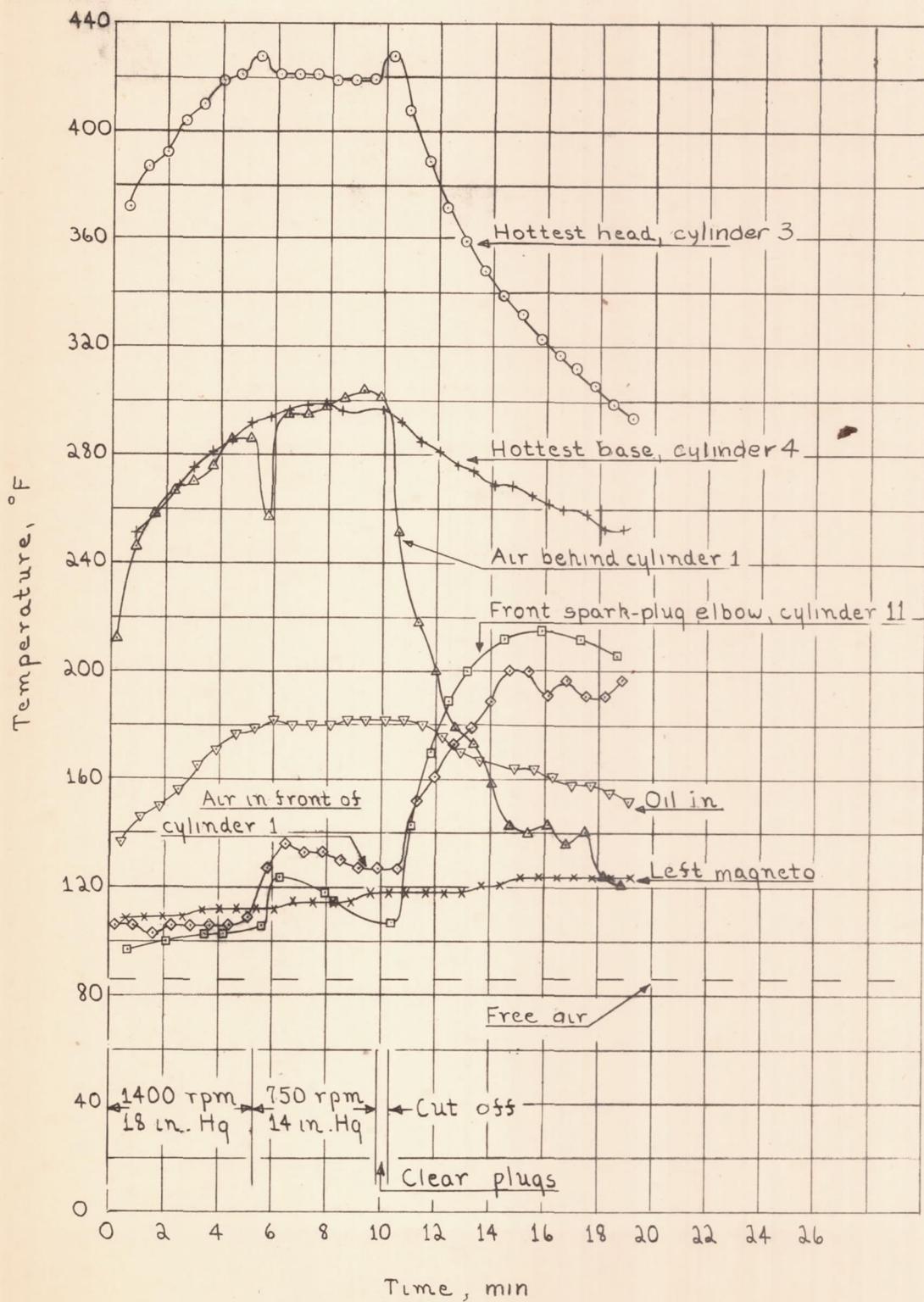
(Measure with $\frac{1}{30}$ "")

Figure 11-Temperatures in ground run without cuffs.