## NATIONAL ADVISORY COMMITTEE FOR AERONAUTICS

# WARTIME REPORT 

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PRESSURE-DISTRIBUTION MEASUREMENIS OF A LOW-DRAG AIRFOII.
WITH SLOTMED FIAP SUBMITTED BY CURTISS-WRIGETT CORPORATION
By I. H. Abbott

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WASHINGTON

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# NATIONAL ADVISORY COMMITTEE FOR AERONAUTICS 

MEMORANDUM REPORT
for the
Materiel Division, Army Air Corps
PRESSURE--DISTRIBUIION MEASUREMENTS OF A LOW-DRAG ATRFOIL
WITH SLOTTED FLAP SUBMITTED BY CURTISS-WRIGEP CORPORATION
By I. H. ABBOTT

INTRODUCTION

Pressure-distribution measurements were made at the request of the Materiel Division, U. S. Army Air Corps, on a 24 -inchchord wooden model equipped with a slotted flap and submitted by the Curtiss-Wright Corporation. The tests were made in the Langley two-dimensional tunnel at a Reynolds number of about 5,600,000.

The model wes the one described in reference 1 and represented a wing section of the $P-60 A$ airplane. The model was equipped with a 0.25 c slotted flap with the lip on the upper airfoil surface at approximately 90 percent of the airfoil chord. The model was equipped with pressure-distribution orifices.

## RESULTS AND DISCUSSION

Pressure-distribution diagrams are presented in figures 1 to 5 for the model at about $-16^{\circ}, 0^{\circ}$, and $16^{\circ}$ with a flap deflection of $15^{\circ}$, and for angles of attack of $0^{\circ}$ and $12^{\circ}$ for a flap deflection of $30^{\circ}$. Pressures are plotted directly as obtained from the manometer in terms of $1 / 2$-inch units of carbon tetrachloride. The abscissa is the projection on the chord line of the pressure orifices. The values of the corrected dynamic pressure $q$ and the impact pressure level in terms of the same units are given on each figure. The static pressure level is obtained jy adding the value of $q$ to the impact pressure level. The value $\left(\frac{v}{V}\right)^{2}$, where $v$ is the local velocity and $V$ is the free-stream velocity, is obtained by dividing the local pressure, measured from the impect pressure level, by the value of $q$.

The normal-force coefficient, as obtained by integration of the pressure diagrams, is given on each figure and fis in essential agreement with the lift coefficients presented in reference 1. Moment coefficients about the quarter-chord point are also presented as obtained for integration of the diagrams. These moment coefficients do not contain the component of moment due to the chord force which may be appreciable, especially at the larger flap deflection.

The projections of the pressure orifices of the model on the chord are given in table I in percentage of chord for flap deflections of $0^{\circ}, 15^{\circ}$, and $30^{\circ}$.

Langley Memorial Aeronautical Laboratory, National Advisory Committee for Aeronautics, Langley Field, Va., December 11, 1941.

REFERENCE

1. Abbott, I. H.: Lift and Drag Characteristics of a Low-Drag Airfoil Model with Slotted Flap Submitted by Curtissm Wright Corporation. NACA MR, Dec. 2, 1941.

TABLE I
PROJECTION ON CHORD OF PRSSSURE ORIFICES
CURTISS-WRIGITT 24 -INCH CHORD FTAP WODEL FOR PGO-A AIRPLANE

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| Airpoil |  |  |  |
| :---: | :---: | :---: | :---: |
| Upper Surface |  | Lower Surface |  |
| Orifice No. | Percent Chord | Orifice No. | Percent Chord |
| $\begin{aligned} & L, E, \\ & 1 T \\ & 2 T \\ & 3 T \\ & 4 T \\ & 5 T \\ & 6 T \\ & 7 T \\ & 8 T \\ & 9 T \\ & 10 T \\ & 11 T \\ & 12 T \\ & 13 T \\ & 14 T \\ & 15 T \\ & 16 T \\ & 17 T \\ & 18 T \\ & 19 T \\ & 20 T \end{aligned}$ | 0 .83 2.45 5.16 7.61 10.06 15.08 19.99 25.05 30.05 35.06 40.00 45.12 50.10 54.95 59.99 65.10 70.06 75.00 80.15 85.10 | $\begin{aligned} & 1 B \\ & 2 B \\ & 3 B \\ & 4 B \\ & 5 B \\ & 6 B \\ & 7 B \\ & 8 B \\ & 9 B \\ & 10 B \\ & 11 B \\ & 12 B \\ & 13 B \\ & 14 B \\ & 15 B \\ & 16 B \\ & 17 B \\ & 18 B \\ & 19 B \\ & 20 B \\ & 21 B \\ & 22 B \\ & 23 B \end{aligned}$ | $\begin{array}{r} .91 \\ 2.62 \\ 5.10 \\ 7.57 \\ 10.17 \\ 15.13 \\ 20.15 \\ 25.15 \\ 30.17 \\ 35.05 \\ 40.08 \\ 45.10 \\ 50.04 \\ 55.00 \\ 60.26 \\ 64.93 \\ 69.90 \\ 75.04 \\ 75.80 \\ 77.95 \\ 80.90 \\ 82.39 \\ 83.72 \end{array}$ |
| Flap, $\delta=0^{\circ}$ |  |  |  |
| $\begin{aligned} & \text { L.E. } \\ & \text { IFT } \\ & 2 F T \\ & 3 F T \\ & 4 \mathrm{FT} \\ & 5 \mathrm{FT} \\ & 6 \mathrm{FT} \\ & 7 \mathrm{FT} \\ & 8 \mathrm{FT} \\ & 9 \mathrm{FT} \end{aligned}$ | $\begin{aligned} & 75.35 \\ & 75.90 \\ & 76.92 \\ & 78.85 \\ & 82.40 \\ & 85.00 \\ & 87.50 \\ & 89.98 \\ & 93.30 \\ & 96.33 \end{aligned}$ | IFFB <br> $2 F B$ <br> 3F'B <br> 4 FB <br> 5FB <br> 6FB <br> 7 FB <br> 8 FB <br> 9F'B <br> T.E. | $\begin{array}{r} 76.09 \\ 77.05 \\ 78.96 \\ 82.54 \\ 84.91 \\ 87.40 \\ 89.90 \\ 93.14 \\ 97.01 \\ 100.00 \end{array}$ |

TABLE I (Concluded)
PROJECTION ON CHORD OF PRESSURE ORIFICES

| Flap, $\delta=15^{\circ}$ |  |  |  |
| :---: | :---: | :---: | :---: |
| Upper Surface |  | Lower Surface |  |
| $\begin{aligned} & \text { Orifice } \\ & \text { No. } \end{aligned}$ | Percent Chord | $\begin{aligned} & \text { Orifice } \\ & \text { No. } \end{aligned}$ | Percent Chord |
| $\begin{aligned} & \text { L.E. } \\ & 1 \mathrm{FT} \\ & 2 \mathrm{FT} \\ & 3 \mathrm{FT} \\ & 4 \mathrm{FT} \\ & 5 \mathrm{FT} \\ & 6 \mathrm{FT} \\ & 7 \mathrm{FT} \\ & 8 \mathrm{FT} \\ & 9 \mathrm{FT} \end{aligned}$ | $\begin{array}{r} 81.75 \\ 82.50 \\ 83.72 \\ 86.10 \\ 89.65 \\ 92.20 \\ 94.70 \\ 97.08 \\ 100.00 \\ 102.85 \end{array}$ | $\begin{aligned} & 1 \mathrm{FB} \\ & 2 \mathrm{FB} \\ & 3 \mathrm{FB} \\ & 4 \mathrm{FB} \\ & 5 \mathrm{FB} \\ & 6 \mathrm{FB} \\ & 7 \mathrm{FB} \\ & 8 \mathrm{FB} \\ & 9 \mathrm{FB} \\ & \mathrm{~T} . \mathrm{E} \end{aligned}$ | $\begin{array}{r} 82.13 \\ 82.95 \\ 84.89 \\ 88.55 \\ 9.05 \\ 93.65 \\ 96.20 \\ 9 . .53 \\ 103.40 \\ 106.22 \end{array}$ |
| Flap, $\delta=30^{\circ}$ |  |  |  |
| $\begin{aligned} & \text { L.E. } \\ & 1 F T \\ & 2 F T M \\ & 3 F T \\ & 4 F T \\ & 4 F T \\ & 6 F T \\ & \hline 7 F T \\ & 8 F T \\ & 9 F T \end{aligned}$ | $\begin{array}{r} 88.72 \\ 89.70 \\ 91.11 \\ 93.60 \\ 97.17 \\ 99.58 \\ 101.70 \\ 103.70 \\ 106.23 \\ 108.60 \end{array}$ | $\begin{aligned} & 1 F B \\ & 2 F B \\ & 3 F B \\ & 4 F B \\ & 4 F B \\ & 6 F B \\ & 7 F B \\ & 7 F B \\ & \hline 8 F B \\ & 9 F B \\ & T . E . \end{aligned}$ | $\begin{array}{r} 88.78 \\ 89.44 \\ 91.19 \\ 94.72 \\ 97.05 \\ 99.54 \\ 102.00 \\ 105.15 \\ 108.81 \\ 111.51 \end{array}$ |

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